





MISSISSIPPI-KASKASKIA-ST. LOUIS BASIN

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GUILFORD LAKE DAM ST. LOUIS COUNTY, MISSOURI MO 31137



PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM



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MISSISSIPPI-KASKASKIA-ST. LOUIS BASIN

GUILFORD LAKE DAM ST. LOUIS COUNTY, MISSOURI MO 31137

PHASE 1 INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM.

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Guilford Lake Dam (MC 31137), Mississippi - Kaskaskia - St. Louis Basin, St. Louis County, Missouri. Phase I Inspection Report.



St. Louis District 9 Final rept.

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PREPARED BY: U.S. ARMY ENGINEER DISTRICT. ST. LOUIS

FOR: STATE OF MISSOURI

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DEPARTMENT OF THE ARMY ST. LOUIS DISTRICT, CORPS OF ENGINEERS 210 TUCKER BOULEVARD, NORTH ST. LOUIS, MISSOURI 63101 يات المالية المحمد المحمد المحمد المالية المحمد المحمد المحمد المحمد المحمد المحمد المحمد المحمد المحمد المحمد

SUBJECT:

Dam Phase I Inspection Report

This report presents the results of field inspection and evaluation of the Guilford Lake Dam (MO 31137).

It was prepared under the National Program of Inspection of Non-Federal Dams.

This dam has been classified as unsafe, non-emergency by the St. Louis District as a result of the application of the following criteria:

a. Spillway will not pass 50 percent of the Probable Maximum Flood without overtopping the dam.

b. Overtopping of the dam could result in failure of the dam.

c. Dam failure significantly increases the hazard to loss of life downstream.



GUILFORD LAKE DAM

ST. LOUIS COUNTY, MISSOURI

MISSOURI INVENTORY NO. 31137

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

PREPARED BY:

BLACK & VEATCH CONSULTING ENGINEERS KANSAS CITY, MISSOURI

UNDER DIRECTION OF

ST. LOUIS DISTRICT CORPS OF ENGINEERS

FOR

GOVERNOR OF MISSOURI

NOVEMBER 1980

PHASE I REPORT

NATIONAL DAM SAFETY PROGRAM

Name of Dam State Located County Located Stream Date of Inspection Guilford Lake Dam Missouri St. Louis County Tributary of Fox Creek 19 November 1980

Guilford Lake Dam was inspected by a team of engineers from Black & Veatch, Consulting Engineers for the St. Louis District, Corps of Engineers. The purpose of the inspection was to make an assessment of the general condition of the dam with respect to safety, based upon available data and visual inspection, in order to determine if the dam poses hazards to human life or property.

The guidelines used in the assessment were furnished by the Department of the Army, Office of the Chief of Engineers and developed with the help of several Federal and state agencies, professional engineering organizations, and private engineers. Based on these guidelines, this dam is classified as a small size dam with a high downstream hazard potential. According to the St. Louis District, Corps of Engineers, failure would threaten lives and property. The estimated damage zone extends approximately two miles downstream of the dam. Within the estimated damage zone are eight dwellings, several farm buildings, and State Highway 100. Contents of the estimated downstream damage zone were verified by the inspection team.

Our inspection and evaluation indicates that the spillway does not meet the criteria set forth in the guidelines for a dam having the above size and hazard potential. The spillway will not pass the probable maximum flood without overtopping but will pass 15 percent of the probable maximum flood. The spillway will pass the flood which has a one percent chance of occurrence in any given year (100-year flood). The spillway design flood recommended by the guidelines is 50 to 100 percent of the probable maximum flood. Considering the hazard zone and the volume of water stored, the spillway design flood should be 50 percent of the probable maximum flood. The probable maximum flood is defined as the flood discharge which may be expected from the most severe combination of critical meteorologic and hydrologic conditions which are reasonably possible in the region. Based on visual observations, this dam appears to be in good condition. Deficiencies visually observed by the inspection team were poor erosion protection on the embankment, erosion of the right (southwest) bank of the spillway channel, erosion of the left (northeast) abutment, and erosion of the right (southwest) abutment below the spillway. Seepage and stability analyses required by the guidelines were not available.

There were no observed deficiencies or conditions existing at the time of the inspection which indicated an immediate safety hazard. Future corrective action and regular maintenance will be required to correct or control the described deficiencies. In addition, detailed seepage and stability analyses of the existing dam, as required by the guidelines, should be performed. A detailed report discussing each of these deficiencies is attached.

Eluri Edwin R. Burton, PE

Missouri E-10137

Harpy L. Callahan, Partner Black & Veatch



OVERVIEW OF DAM

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PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM GUILFORD LAKE DAM

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SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

a. <u>Authority</u>. The National Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of safety inspection of dams throughout the United States. Pursuant to the above, the District Engineer of the St. Louis District, Corps of Engineers, directed that a safety inspection of the Guilford Lake Dam be made.

b. <u>Purpose of Inspection</u>. The purpose of the inspection was to make an assessment of the general condition of the dam with respect to safety, based upon available data and visual inspection, in order to determine if the dam poses hazards to human life or property.

c. <u>Evaluation Criteria</u>. Criteria used to evaluate the dam were furnished by the Department of the Army, Office of the Chief of Engineers, in "Recommended Guidelines for Safety Inspection of Dams." These guidelines were developed with the help of several Federal agencies and many state agencies, professional engineering organizations, and private engineers.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances.

(1) The dam is an earth structure located in the valley of a tributary to Fox Creek (See Plate 1). The watershed is an area of low hills with fairly steep slopes consisting of about 65 percent timberland and 35 percent grassland pastures. There are several large houses in the drainage area. The dam is approximately 350 feet long along its crest and is constructed with a curved alignment. The dam is about 32 feet high and is 11 feet wide at its crest. The downstream face of the dam has a nonuniform slope from the crest to the valley floor below.

(2) The spillway is an unlined open channel cut in the natural material of the right abutment. The material excavated from the spillway channel forms a dike along the left bank of the spillway. The spillway channel is nonuniform in width and cross section with an approximate average depth of 4 feet and an approximate average bottom width of 7 feet. Flow through the spillway channel discharges to the natural slope of the abutment then to the stream channel below the dam.

(3) Pertinent physical data are given in paragraph 1.3.

b. Location. The dam is located in western St. Louis County, Missouri, as indicated on Plate 1. The lake formed by the dam is in an area shown on the United States Geological Survey 7.5 minute series quadrangle map for Eureka, Missouri in Section 19 of T44N, R03E.

c. <u>Size Classification</u>. Criteria for determining the size classification of dams and impoundments are presented in the guidelines referenced in paragraph 1.1c above. Based on these criteria, the dam and impoundment are in the small size category. A small size dam is classified as having a height less than 40 feet, but greater than or equal to 25 feet and/or a storage capacity less than 1,000 acre-feet, but greater than or equal to 50 acre-feet.

d. <u>Hazard Classification</u>. The hazard classification assigned by the Corps of Engineers for this dam is as follows: The Guilford Lake Dam has a high hazard potential, meaning that the dam is located where failure may cause loss of life, and serious damage to homes, agricultural, industrial and commercial facilities, and to important public utilities, main highways, or railroads. For the Guilford Lake Dam the estimated flood damage zone extends approximately two miles downstream of the dam. Within the estimated damage zone are eight dwellings, several farm buildings, and State Highway 100. Contents of the estimated downstream damage zone were verified by the inspection team.

e. <u>Ownership</u>. The dam is owned by Mr. Charles F. Guilford, Rural Route 5, Pacific, Missouri 63069.

f. <u>Purpose of Dam</u>. The dam forms a 4.5-acre lake used for recreation and as a livestock water supply.

g. <u>Design and Construction History</u>. Data relating to the design and construction were not available. The dam was constructed in 1976 by Kenneth Pointer with design assistance from the Soil Conservation Service.

h. <u>Normal Operating Procedure</u>. Normal rainfall, runoff, transpiration, evaporation, and overflow through the uncontrolled spillway all combine to maintain a relatively stable water surface elevation.

1.3 PERTINENT DATA

a. Drainage Area - 26 acres

b. Discharge at Damsite.

(1) Normal discharge at the damsite is through an unlined, open channel spillway.

(2) Estimated experienced maximum flood at damsite - Unknown.

(3) Estimated ungated spillway capacity at maximum pool elevation 60 cfs (50 Percent Probable Maximum Flood Pool El. 690.9).

c. Elevation (Feet above m.s.l. Approximated from USGS Map contours).

- (1) Top of dam 690.0 (see Plate 3)
- (2) Spillway crest 689.0
- (3) Streambed at toe of dam 658.5
- (4) Maximum tailwater Unknown.
- d. Reservoir.

(1) Length of maximum pool - 790 feet + (Probable maximum flood pool level).

(2) Length of normal pool - 590 feet + (Spillway crest).

e. <u>Storage</u> (Acre-feet).

(1) Top of dam - 52

(2) Spillway crest - 46

(3) Design surcharge - Not available.

f. Reservoir Surface (Acres).

- (1) Top of dam 5.7
- (2) Spillway crest 4.5

g. Dam.

- (1) Type Earth embankment.
- (2) Length 350 feet
- (3) Height 32 feet +
- (4) Top width 11 feet

(5) Side slopes - upstream face 1.0 V on 3.4 H, downstream face varies between 1.0 V on 2.5 H and 1.0 V on 5.0 H (see Plate 4).

- (6) Zoning Unknown.
- (7) Impervious core Unknown.
- (8) Cutoff Unknown.
- (9) Grout curtain Unknown.
- h. Diversion and Regulating Tunnel None.
- i. Spillway.

(1) Type - Unlined, open channel with an approximate 7-foot bottom width and 4-foot height.

- (2) Crest elevation 689.0 feet m.s.l.
- (3) Gates None.
- (4) Upstream channel Unlined earth channel.

(5) Downstream channel - Spillway discharges to natural slope, then to the natural stream downstream of the dam.

j. Emergency Spillway - None.

k. Regulating Outlets - None.

SECTION 2 - ENGINEERING DATA

2.1 DESIGN

Design data were not available. Design assistance was provided by the Soil Conservation Service.

2.2 CONSTRUCTION

Construction records were unavailable. The dam was constructed by Kenneth Pointer.

2.3 OPERATION

Operational records and documentation of past floods were unavailable.

2.4 GEOLOGY

The site of the dam and reservoir is located in a shallow, broad, steep-sided valley. The dam impounds a very short, intermittent tributary of Fox Creek.

There were no data available on the soils in the area of the dam and reservoir. The bedrock consists of limestone of the Osage series of the Pennsylvanian System according to the Geologic Map of Missouri.

2.5 EVALUATION

a. Availability. No engineering data were available.

b. <u>Adequacy</u>. No engineering data were available. Thus, an assessment of the design, construction, and operation could not be made. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency. These seepage and stability analyses should be performed for appropriate loading conditions (including earthquake loads) and made a matter of record.

c. <u>Validity</u>. The validity of the design, construction, and operation could not be determined due to the lack of engineering data.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

a. <u>General</u>. A visual inspection of Guilford Lake Dam was made on 19 November 1980. The inspection team consisted of Edwin Burton, team leader; Robert Pinker, geologist; Gary Van Riessen, geotechnical engineer; and John Ruhl, civil engineer. The dam appeared to be in good condition. Specific observations are discussed below. No observations were made of the condition of the upstream face of the dam below the pool elevation at the time of the inspection.

b. Dam. The inspection team observed the following conditions at the dam. No cracking, sliding, sloughing, unusual irregularities, or other signs of instability or settlement were observed. The grass cover on the dam was very thin to nonexistent in spots. Numerous tracks of cattle and horses were observed which would indicate heavy grazing. There were no trees on the embankment. Small riprap (approximately 3-6 inches in size) has been placed on the upstream face at the waterline. The soft upstream face for several feet above the waterline would indicate that the water level had been higher a short time before the inspection. Erosion exists along the left abutment where runoff from the road and hillside drains into the lake and on the right abutment below the end of the spillway channel. Minor erosion was observed on the downstream slope of the embankment. No areas of seepage were observed. Although the old stream channel was very green, the inspection team believes that this is due to surface drainage rather than seepage. A void exists in the fill material in the old stream channel. There were no animal burrows observed on the embankment. Although the owner stated that the dam was overtopped in 1978 there were no visible signs of overtopping.

c. <u>Appurtenant Structures</u>. The inspection team observed the following items pertaining to the appurtenant structures. The spillway was in good condition. The right bank of the spillway channel is eroding from hillside runoff. Although the grass cover is unsatisfactory, there has been no erosion of the channel floor. There was no development in the spillway area which would suffer damage due to flow through the spillway.

d. <u>Geology</u>. The soils observed in the area of the dam and reservoir consist of silty clay formed in residuum from limestone. For engineering purposes the soils are classified as clayey silt or silty clay of low plasticity. No outcrops were observed in the area. However numerous fragments of chert were present in the soils and on the embankment. A sample of the material in the embankment was taken with an Oakfield sampler near the center of the downstream crest. The materials

sampled consisted of silty clay and were visually classified for engineering purposes as silty clay of low plasticity (CL). Based on these samples, it is surmized that the embankment is constructed of silty clay (CL).

e. <u>Reservoir Area</u>. No slumping or slides of the reservoir banks were observed. Drainage into the reservoir is primarily runoff from the steeply sloping hills around the lake with little defined channelized flow. There was no noticeable lake siltation.

f. <u>Downstream Channel</u>. The spillway discharges to the natural slope, then flows overland to the natural stream channel downstream of the dam. The stream channel has been filled for approximately 200 feet downstream of the toe of the dam.

3.2 EVALUATION

The various deficiencies observed at the time of the inspection are not believed to represent an immediate safety hazard. They do, however, warrant monitoring and control.

The thin grass cover on the embankment and in the spillway has permitted the erosion of the right spillway bank, the right abutment below the spillway, and the left abutment. Each of these areas of erosion should be repaired and adequate erosion protection should be maintained.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

The pool is primarily controlled by rainfall, runoff, evaporation, transpiration, and capacity of the uncontrolled spillway.

4.2 MAINTENANCE OF DAM

According to the owner, the dam was overtopped in 1978 due to blockage of the spillway. Subsequently, the blockage was removed and the embankment was redressed and seeded. No other maintenance has been performed.

4.3 MAINTENANCE OF OPERATING FACILITIES

No operating facilities exist.

4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

There is no existing warning system or preplanned scheme for alerting downstream residents for this dam.

4.5 EVALUATION

A maintenance program should be established to provide adequate erosion protection of the spillway and embankment.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

a. Design Data. No design data were available.

b. Experience Data. The drainage area and the lake surface area are developed from the USGS Eureka, Missouri Quadrangle Map. The dam layout is from a survey made during the inspection.

c. Visual Observations.

(1) The spillway appears to be in good condition. The lake level at the time of the inspection (El. 685.0) was below the spillway crest level. There were no obstructions to flow in the downstream channel.

(2) There is no emergency spillway for this dam.

(3) Large spillway discharges will probably erode the spillway and could erode the embankment.

d. Overtopping Potential. The spillway will not pass the probable maximum flood without overtopping the dam. The probable maximum flood is defined as the flood discharge that may be expected from the most severe combination of critical meteorologic and hydrologic conditions that are reasonably possible in the region. The spillway will pass 15 percent of the probable maximum flood without overtopping the dam. The spillway will pass the one percent chance flood estimated to have a peak outflow of 19 cfs developed by a 24-hour, one percent chance rainfall. According to the recommended guidelines from the Department of the Army, Office of the Chief of Engineers, a high hazard dam of small size should pass 50 to 100 percent of the probable maximum flood. Considering the downstream hazard, and the volume of water stored, the appropriate spillway design flood should be 50 percent of the probable maximum flood. The portion of the estimated peak discharge of 50 percent of the probable maximum flood overtopping the dam would be 150 cfs of the total discharge from the reservoir of 210 cfs. The estimated duration of overtopping is 5.6 hours with a maximum height of 0.9 feet. The portion of the estimated peak discharge of the probable maximum flood overtopping the dam would be 420 cfs of the total discharge from the reservoir of 530 cfs. The estimated duration of overtopping is 7.2 hours with a maximum height of 1.4 feet. The embankment could be jeopardized should overtopping occur for these periods of time.

According to the St. Louis District, Corps of Engineers, the effect from rupture of the dam could extend approximately two miles downstream of the dam. Within the estimated damage zone are eight dwellings, several farm buildings, and State Highway 100. Contents of the estimated downstream damage zone were verified by the inspection team. Flood plain regulations under the National Flood Insurance Program restrict development in the flood plain of Fox Creek which is downstream of the dam.

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. <u>Visual Observations</u>. Visual observations of conditions which affect the structural stability of this dam are discussed in Section 3, paragraph 3.1b.

b. <u>Design and Construction Data</u>. No design data relating to the structural stability of the dam were found. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency.

c. Operating Records. No operational records exist.

d. <u>Postconstruction Changes</u>. Repair of erosion due to overtopping included redressing and seeding the embankment crest and slopes. The repairs were made in 1979.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 2 which is a zone of moderate seismic risk. A properly designed and constructed earth dam using sound engineering principles and conservatism should pose no serious stability problems during earthquakes in this zone. The seismic stability of an earth dam is dependent upon a number of factors: embankment and foundation material classifications and shear strengths; abutment materials, conditions, and strengths; embankment zoning; and embankment geometry. Adequate descriptions of embankment design parameters, foundation and abutment conditions, or static stability analyses to assess the seismic stability of this embankment were not available and therefore no inferences will be made regarding the seismic stability. An assessment of the seismic stability should be included as part of the stability analysis required by the guidelines.

SECTION 7 - ASSESSMENT/REMEDIAL MEASURES

7.1 DAM ASSESSMENT

a. <u>Safety</u>. Several conditions observed during the visual inspection by the inspection team should be monitored and/or controlled. These are erosion on the left abutment, the right abutment below the spillway, and the right bank of the spillway, and the poor erosion protection on the embankment. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency.

b. Adequacy of Information. Due to the absence of engineering design data, the conclusions in this report were based only on performance history and visual conditions. The inspection team considers that these data are sufficient to support the conclusions herein. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency.

c. <u>Urgency</u>. It is the opinion of the inspection team that a program should be developed as soon as possible to implement remedial measures recommended in paragraph 7.2b. If the safety deficiencies listed in paragraph 7.1a are not corrected, they will continue to deteriorate and lead to a serious potential of failure. The item recommended in paragraph 7.2a should be pursued on a high priority basis.

d. <u>Necessity for Phase II</u>. The Phase I investigation does not raise any serious questions relating to the safety of the dam nor does it identify any serious dangers which would require a Phase II investigation. However, the additional analyses noted in paragraph 2.5b are necessary for compliance with the guidelines.

• e. <u>Seismic Stability</u>. This dam is located in Seismic Zone 2. Adequate description of embankment design parameters, foundation and abutment conditions, or static stability analyses to assess the seismic stability of this embankment were not available and therefore no inferences will be made regarding the seismic stability. An assessment of the seismic stability should be included as part of the recommended stability analysis.

7.2 REMEDIAL MEASURES

a. <u>Alternatives</u>. The spillway size and/or height of the dam would need to be increased or the lake level would need to be permanently lowered to increase available flood storage in order to effectively pass the recommended spillway design flood. b. <u>Operation and Maintenance Procedures</u>. The following operation and maintenance procedures are recommended and should be carried out under the direction of a professional engineer experienced in the design, construction, and maintenance of earth dams.

(1) An adequate grass cover should be maintained on the embankment and in the spillway to prevent erosion. Overgrazing by cattle should be prevented.

(2) The erosion of the right spillway bank, the left abutment, and the right abutment below the spillway should be backfilled with suitable material and compacted. A paved ditch or some other means of slope protection may be required to control the concentrated runoff at the left abutment.

(3) Seepage and stability analyses should be performed.

(4) A detailed inspection of the dam should be made periodically and the results documented and made a matter of record. More frequent inspections may be required if additional deficiencies are observed or the severity of the reported deficiencies increase.





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PLATE

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PHOTO 1: UPSTREAM FACE OF DAM LOOKING SOUTH



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PHOTO 2: UPSTREAM FACE OF DAM LOOKING NORTH



PHOTO 3: CREST OF DAM LOOKING SOUTH



PHOTO 4: CREST OF DAM LOOKING NORTH



PHOTO 5: DOWNSTREAM FACE OF DAM LOOKING SOUTH



PHOTO 6: DOWNSTREAM FACE OF DAM LOOKING NORTH



PHOTO 7: INLET TO SPILLWAY CHANNEL



PHOTO 8: SPILLWAY CHANNEL LOOKING DOWNSTREAM



PHOTO 9: EROSION ON ABUTMENT SLOPE DOWNSTREAM OF SPILLWAY CHANNEL



PHOTO 10: STREAM CHANNEL BELOW DAM



PHOTO 11: VOID IN FILL OF OLD STREAM CHANNEL BELOW DAM



PHOTO 12: EROSION AT LEFT ABUTMENT



PHOTO 13: EROSION ON DOWNSTREAM SLOPE OF DAM



PHOTO 14: LIVESTOCK TRACKS AND OVERGRAZED AREA

APPENDIX A

HYDROLOGIC AND HYDRAULIC ANALYSES

HYDROLOGIC AND HYDRAULIC ANALYSES

To determine the overtopping potential, flood routings were performed by applying the Probable Maximum Precipitation (PMP) to a synthetic unit hydrograph to develop the inflow hydrograph. The inflow hydrograph was then routed through the reservoir and spillway. The overtopping analysis was determined using the computer program HEC-1 (Dam Safety Version) (1).

The PMP was determined from regional charts prepared by the National Weather Service in "Hydrometeorological Report No. 33" (HMR-33) (2). Reduction factors were not applied. The rainfall distribution for the 24-hour PMP storm was determined according to the procedures outlined in HMR-33 and EM 1110-2-1411 (3). The St. Louis, Missouri rainfall distribution (5 min. interval - 24 hours duration), as provided by the St. Louis District, Corp of Engineers, was used when the one percent chance probability flood was routed through the reservoir and spillway.

The synthetic unit hydrograph for the watershed was developed by the computer program using the Soil Conservation Service (SCS) method. (1 and 4). The parameters for the unit hydrograph are shown in Table 1. Lag time and time of concentration were calculated by two different methods. The results used in the analyses were obtained by using the Kirpich formula.

The SCS curve number (CN) method was used in computing the infiltration losses for the rainfall-runoff relationship. The CN values used, and the result from the computer output, are shown in Table 2.

The reservoir routing was performed using the Modified Puls Method. The initial reservoir pool elevation for the routing of each storm was determined to be equivalent to the crest elevation of the spillway at elevation 689.0 feet m.s.l. in accordance with antecedent storm conditions preceding the one percent probability and probable maximum storms outlined by the U.S. Army Corps of Engineers, St. Louis District (5). The hydraulic capacity of the spillway and the storage capacity of the reservoir were defined by the elevation, surface area, storage, and discharge relationships shown in Table 3.

The rating curve for the spillway is shown in Table 4. The flow over the crest of the dam and through the spillway was determined using the non-level dam crest option (\$L and \$V cards) of the HEC-1 program. The program assumes critical flow over a broad-crested weir.

The result of the routing analysis indicates that a 15 percent PMF flood will not overtop the dam.

A summary of the routing analysis for different ratios of the PMF is shown in Table 5.

The computer input data and a summary of the output data are presented at the back of this appendix.

TABLE 1

SYNTHETIC UNIT HYDROGRAPH

Parameters:

Drainage Area (A) 26 acres Hydraulic Length of 0.16 miles Watercourse (L) Difference in Elevation (H) 90 feet Time of concentration (T_c) 0.05 hours Lag Time (L_{o}) 0.03 hours Duration (D) 0.4 minutes (use 5 minutes) Time (Min.) * Discharge (cfs) * 0 0 5 236 10 66 15 13

* From HEC-1 computer output

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FORMULAS USED:

$$T_{c} = [(11.9 \times L^{3})/H]^{0.385} (6)$$

D = 0.133 T_c
L_g = 0.6 T_c

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TABLE 2

RAINFALL-RUNOFF VALUES

Selected Storm Event	Storm Duration (Hours)	Rainfall (Inches)	Runoff (Inches)	Loss (Inches)
PMP	24	32.89	31.31	1.58
50% PMP	24	17.18	15.65	1.53
1% Probability	24	6.97	4.13	2.84

Additional Data:

No information on soil associations was available for this watershed.
 100 percent of the drainage area was assumed to be in hydrologic soil group C.
 35 percent of the land use was grassland.
 65 percent of the land use was timberland.
 2) SCS Runoff Curve CN = 88 (AMC III) for the PMF.

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3) SCS Runoff Curve CN = 75 (AMC II) for the one percent probability flood (4).

TABLE 3

ELEVATION, SURFACE AREA, STORAGE, AND DISCHARGE RELATIONSHIPS

Elevation	Lake Surface	Lake Storage	Spillway
(feet-msl)	<u>Area (acres)</u>	(acre-ft)	Discharge (cfs)
*689.0	4.5	46	0
**690.0	5.7	52	21

*Spillway Crest Elevation **Top of Dam Elevation

The relationships in Table 3 were developed from the Eureka, Missouri. 7.5 minute quadrangle map and the field measurements.

TABLE 4

SPILLWAY RATING CURVE

Reservoir Elevation (ft-msl)	Spillway Discharge (cfs)
	<u>proceedings</u> (cro)
*689.0	0
689.5	4
689.8	12
**690.0	21

*Spillway Crest Elevation **Top of Dam Elevation

METHOD USED:

Spillway releases were computed by HEC-1 from spillway geometry data input on \$L and \$V cards. Discharges through the spillway for the probable maximum flood and for 50 percent of the probable maximum flood were determined by the equations for flow over a non-level crest.

$$d_{c} = 2/3 (H_{m} + 1/4 \Delta Y)$$

A = 1/2 T (2d_c - ΔY)
Q = (A³g/T)^{0.5}

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where:

d_c = critical depth (feet) H_m = available specific energy which is taken to be the height of the water surface in the reservoir above the bottom of the section (feet) ΔY = change in elevation across the section (feet) A = flow area (sq. ft.) T = top width (feet) Q = flow (cfs) g = 32.2 ft/sec² = acceleration due to gravity.

TABLE 5

RESULTS OF FLOOD ROUTINGS

Ratio of PMF	Peak Inflow (cfs)	Peak Lake Elevation (ftmsl)	Total Storage (acft.)	Peak Outflow (cfs)	Depth (ft.) Over Top of Dam	Duration (hrs.) Over Top of Dam
-	0	*689.0	46	0	-	-
0.15	114	690.0	52	21	0	0
0.50	379	690.9	57	212	0.9	5.6
1.00	757	691.4	59	531	1.4	7.2

* Spillway Crest Elevation

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PERMARM AT STA     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     10.61     71.401     72.401     70.61     34.5       741.     1     10.61     71.401     71.41     71.41       741.     1     10.65     10.65     11.65       741.     1     1     10.61     71.41       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1       &lt;</td></td>	33.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31.     31. <td>33.     31.     31.     31.     31.     31.     31.       PERMARM AT STA     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     10.61     71.401     72.401     70.61     34.5       741.     1     10.61     71.401     71.41     71.41       741.     1     10.65     10.65     11.65       741.     1     1     10.61     71.41       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1       &lt;</td>	33.     31.     31.     31.     31.     31.     31.       PERMARM AT STA     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     100 KLM     72.400     72.401     70.61     34.5       741.     1     10.61     71.401     72.401     70.61     34.5       741.     1     10.61     71.401     71.41     71.41       741.     1     10.65     10.65     11.65       741.     1     1     10.61     71.41       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     10.65       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1     1       741.     1     1     1       <
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FIX       d-HOUE       72-HOUE       72-HOUE       3275         245       72       10.15       10.15       11.05         21       10.15       10.15       11.05       11.05         224       21       10.15       11.05       11.05         224       73       10.05       11.05       24.         224       73       70       70       24.         224       73       70       70       24.         224       73       70       70       70         224       77       70       70       70         239       24.       77       70       70         239       11.0       72-HOUH       72-HOUH       705.0         230       50       15.05       15.05       15.05         230.57       507       507.0       207.0       207.0         230.57       507.0       507.0       507.0       207.0         230.57       507.0       507.0       507.0       207.0         230.57       507.0       507.0       507.0       207.0         231.50       11.0       71.0       71.0       71.0         <	FEA       0-HOUR       71-HOUR       70TAL VGLUPE         23.       11.       12.       12.         24.       11.       12.       12.         24.       13.       12.       12.         24.       13.       10.       10.       11.         24.       13.       10.       10.       11.         24.       13.       10.       10.       11.         24.       13.       10.       10.       10.         24.       13.       10.       10.       10.         24.       13.       10.       10.       10.         24.       13.       10.       10.       10.         24.       10.       24.       10.       10.         27.       11.       11.       10.       10.         28.       13.       10.       10.       10.         28.       11.       10.       10.       10.         21.       11.       10.       10.       10.         21.       11.       10.       10.       10.         21.       11.       10.       10.       10.         21.       11.<	FEA       G-HOUR       Zi-HOUR       TOTAL VGLUE         23.       12.       12.       12.         23.       11.       12.       12.         23.       23.       13.       10.05       11.05         23.       23.       13.       10.05       11.05         24.       13.       10.05       11.05       24.         23.       13.       10.05       11.05       24.         23.       13.       10.05       11.05       11.05         23.       11.0       24.       13.05       13.05         33.       11.0       24.       14.01       24.04         33.       10.05       14.04       70.14       24.04         33.       10.05       13.05       13.05       14.04         33.       10.05       14.04       14.04       14.04         33.       10.05       10.04       10.04       14.04         33.       10.05       10.05       10.05       14.04         33.       10.05       10.04       10.04       10.04         33.0       10.05       10.05       10.04       10.04         10.00       10.04 <td>FEM         G-HOUR         72-HOUR         77-HOUR         <th77-hour< th=""> <th77-hour< th=""> <th77-ho< td=""></th77-ho<></th77-hour<></th77-hour<></td>	FEM         G-HOUR         72-HOUR         77-HOUR         77-HOUR <th77-hour< th=""> <th77-hour< th=""> <th77-ho< td=""></th77-ho<></th77-hour<></th77-hour<>
9.     1.     10.00     17.00       224.00     275.18     275.18     275.18       10.00     274.00     777.00     22.       11.     22.     73.00     52.       12.     73.00     27.00     25.       13.     11.00     72.00     77.00       13.     24.00     72.00     72.00       13.     24.00     72.00     72.00       13.     25.00     33.00     34.00       14.     12.00     34.00     34.00       13.00     33.00     33.00     34.00       14.     12.00     34.00     34.00       15.     42.00     42.00     34.00       25.0     33.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00       25.0     34.00     34.00     34.00<	9.     1.     1.     1.     0.     10.     0.       224.40     274.18     274.18     274.18     274.14     274.14       24.     17.     10.     10.     10.     10.       24.     17.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       11.     12.     17.     17.     17.     17.       12.     13.0.57     397.40     397.40     197.40       12.     12.     12.     17.     17.       12.     12.     17.     17.     17.       12.     12.     17.     197.40     197.40       12.     12.     17.     17.     17.       12.     11.     12.     17.     17.       13.     12.     17.     17.     17.0	9.     1.     1.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     <	0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     0.     <
234:00     276:18     275:18     277:18       24.     24.     54.     54.       24.     30.     40.     54.       27.     17.     17.     40.       57.     17.     17.     40.       57.     54.     72.     17.     40.       57.     52.     15.05     17.     40.5       57.     52.     15.05     17.     40.5       57.     52.     15.05     17.     40.5       57.     17.     17.     40.5     14.6       57.     17.     17.     40.5     14.6       70.5     57.5     57.6     57.6     57.6       70.5     57.6     57.6     57.6     57.6       70.5     57.6     57.6     57.6     57.6       75.     42.     42.     42.     42.       75.     42.     70.4     70.4     70.4       75.     51.1     70.4     70.4     70.4       75.6     51.2     52.7     52.7       75.7     51.2     52.7     52.7       75.4     51.2     52.7     52.7       75.5     51.2     52.7     52.7       75.5     5	224.00     276.14     276.14     276.14     22.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.     32.	274.40     276.16     276.16     276.16     24.       24.     24.     24.     24.     24.       24.     24.     24.     24.     25.       24.     24.     24.     24.     25.       24.     24.     24.     24.     25.       27.     24.     72.4046     70141     7014.       27.     17.     17.     17.     470.5       27.     27.     37.45     37.45     15.45       27.     27.     37.45     37.45     15.45       27.     27.     27.     27.     47.45       27.     27.     27.     27.     47.45       27.     27.     27.     27.     47.5       27.     27.     27.     31.27     37.45       27.     27.     31.27     37.45     37.45       27.     27.     31.27     37.45     37.45       27.     27.     31.27     37.45     37.45       27.     27.     31.27     37.45     37.45       27.     37.45     31.27     37.45     37.45       27.     37.45     31.27     37.45     37.45       27.     31.1     74.45	24.40     276.18     775.18     775.18       24.     32.     54.     32.       24.     32.     54.     32.       74.     71.     10.     8110     8       79.     71.     70.     71.     91.       79.     71.     71.     71.     71.       79.     71.     71.     71.     70.       79.     72.     15.55     15.55     15.55       71.     12.52     15.55     15.55     15.55       75.     12.52     15.55     15.55     15.55       75.     12.52     15.55     15.55     15.55       75.     12.5     15.55     15.55     15.55       75.     12.5     15.55     15.55     15.55       75.     12.5     15.55     15.55     15.55       75.     11.     75.     47.5     15.55       757.     111.     75.5     15.55     15.55       757.     111.     75.5     15.55     15.55       757.     111.     75.5     15.55     15.25       757.     111.     75.5     15.55     15.25       751.     111.     75.5     15.55     15.25 </td
24.       73.       10.       55.         106068APH AT STA       1 FGF FLAN 1, 8110 8       9000568APH AT STA       1 FGF FLAN 1, 8110 8         579.       5.       71.       77.       17.       79.         579.       5.       15.65       15.65       15.65       15.65         11.       12.62       15.65       397.65       15.65       15.65         12.62       15.65       397.65       15.65       15.65       15.65         13.       12.65       397.65       15.65       15.65       15.65         20.25       397.45       397.45       15.65       15.65         21.0       23.25       397.45       37.42       37.25         21.1       79.45       31.25       31.25       31.25         21.1       74.45       74.45       31.25       31.25         21.1       74.45       74.45       31.25       31.25         21.1       74.45       74.45       31.25       31.25         21.1       74.45       31.26       31.25       31.25         21.1       74.45       74.45       31.27       31.27         21.1       74.45       31.26       31.26<	24. 73. 79. 10. 50. 50. 50. PEAC 6-moun 70-mount Total Volume 57. 50. 11. 20. 17. 000 11. 12.00 11. 12.00 13. 50. 11. 12.00 13. 50. 13. 50. 14. 47. 47. 40. 14. 17. 47. 40. 14. 10. 11. 21. 22. 33. 14. 50. 11. 21. 22. 23. 21. 23. 24. 40. 25. 47. 47. 40. 25. 47. 47. 26. 95. 21. 22. 25. 21. 25. 22. 25. 23. 11. 25. 24. 10. 25. 26. 95. 27. 25. 27. 25. 28. 25. 28. 25. 29. 25. 20. 10. 20. 0. 0. 0. 0	24.       13.       10.       35.         TBAGGARM AT STA       1 6.6 FLAN 1, 0110 8       72.4004       TOTAL VOLUE         29.       5.       17.       17.       49.6         29.       5.       17.       17.       49.6         11.       12.02       15.05       15.05       15.45         29.       5.       15.05       15.45       15.45         29.       12.02       15.45       15.45       15.45         20.       12.02       15.45       15.45       15.45         20.       30.45       17.45       97.40       97.40         20.       30.5       15.45       17.45       97.40         20.       31.45       17.45       97.40       97.40         21.1       11.4       11.4       11.4       99.1.29       97.20         221.       23.21       11.4       91.29       97.20       94.20         221.       23.22       11.4       94.4       94.4       94.4         221.       74.4       94.4       94.4       94.4       94.4         221.       74.4       94.4       94.4       94.4       94.4         22	24.       13.       10.       32.         78.058APH A1 STA       1 56 FLAN 1, 8110 8       200.       200.         29.       5.       17.       17.       200.         29.       5.       17.       17.       200.         29.       5.       1565       1565       1565         11.       1267       1565       1565       1565         2027       39760       1965       1565         2125       1565       1565       1565         2125       1565       1565       1565         2225       1170       10.741       9160         2125       1127       1127       9127         2125       1129       1129       1129         2125       1129       1129       1120         2125       1129       1129       1120         2125       1129       1129       1120         2125       1129       1120       1120         2125       1129       1120       1120         2125       1120       1120       1120         2125       1120
WTDEKOGRAPH AT STA       1 FGR FLAN 1, 8710 8         FFAK       6-HCUB       ZL-HCUB       7Z-HOU4       TOTAL VOLUTE         579.       4.       4.055       17.055       17.055         11.       12.05       15.55       15.05       15.65         12.05       15.55       15.05       15.65       15.65         11.       12.05       15.55       15.65       15.65         370.57       57.50       597.40       597.40       547.45         370.57       57.5       15.05       597.40       54.2         370.57       37.45       397.40       54.2       54.2         27.0       27.10       72.400       707.41       707.41       47.2         27.0       31.27       31.27       31.27       31.27       21.27         21.11       74.45       74.45       794.45       201.7       201.2         27.11       74.45       74.45       74.45       201.2       201.2         21.11       74.45       74.45       74.45       201.2       201.2         21.12       74.45       74.45       74.45       201.2       201.2         21.12       74.45       74.45	ИРАНОСКАРН АТ 51A Т ГСК FLAN 1, ЯТІО 8 FTAK 6-4000 21-4004 7014 VOLUFE 279. 54. 11. 12.02 15.05 15.05 15.05 13.02 57.50 37.40 230.57 37.40 37.40 230.57 37.40 1. РТІО 9 21. 221 11. 74. 6-4002 21-4004 72-4004 0910 74.6 31.29 21. 2.21 11. 74.6 4002 21-4004 72-4004 0910 74.6 6-4002 21-4004 72-4004 0910 74.6 71.0 74.6 71.0 9 74.6 71.0 74.6 71.0 9 74.6 71.0 74.6 71.0 9 74.6 71.0 11.0 0 0 0 0 0 2. 10.0 0 0 0 0	ИРАЮGRAPH AT STA 1 ГСК Р.LAN 1, ЯТІО 8 FYAK 6-4009 72-4004 7014 V0107 379. 52. 15.05 15.05 15.05 11. 12.02 15.05 15.05 15.05 12.02 15.05 15.05 15.05 12.02 15.05 15.05 15.05 14.1 12.05 15.05 15.05 14.2 12.02 15.05 15.05 14.2 12.02 15.04 1. 8720 9 14.1 11. 14.1 2010 25.21 11. 14.1 2011 25.22 11. 24.2 794.2 794.2 25.21 11. 794.5 794.2 794.2 25.21 794.5 794.5 794.5 794.5 25.21 794.5 794.5 794.5 794.5 794.5 25.21 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5 794.5	ИРАЮСКАРН АТ STA 1 ГСК Р.LMM 1, ЯТІО 8 FRAK 6-4009 Z.L.HUL 72-4004 ТОТАГ VOLUFE 279. 56. 17. 77. 77. 77. 606. 171. 12.62 15.65 15.65 15.65 172. 27. 17. 77. 17. 17. 60 282. 77.65 15.65 15.65 15.65 282. 77.65 15.65 15.65 75.65 282. 77.65 15.65 15.65 75.65 282. 77.6 2.HUL 72-404 ТОТАГ VOLUE 757. 111. 7.4.57 75.65 211. 7.4.57 75.75 212. 22 213. 25 213. 25 213. 25 213. 25 214. 5.7 75.75 214. 5.7 75.75 215. 25 215. 25
PFAK       6-HOUP       71-12.05       17.17.       17.15.05         579.       52.5       15.05       15.05       15.05         11.       12.02       15.05       15.05       15.05         12.02       15.05       15.05       15.05       15.05         28.       37.40       397.40       97.40       34.05         28.       34.       17.00       11.15       34.05         34.       17.1       17.00       14.01       14.1         754.       5-HOUP       74.40       77.40       54.         755.       11.1       74.1       77.1       9000         757.       13.1       74.1       74.1       74.1         757.       13.1       74.2       9000       26.0         21.       25.1       34.1       74.2       26.1         21.       25.1       34.1       74.2       26.1         21.       25.1       74.2       94.1       26.1         21.       25.1       34.1       94.1       26.1         21.       25.1       26.0       94.1       94.1         25.1       25.1       34.1       94.1       94.1	PFAK       6-4004       71-17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.       17.	Frak       6-HOUB       Z-HOUB       Z-HOUB       T-HOUB       Z-HOUB       T-HOUB       T-HOUB <tht-houb< th="">       T-HOUB</tht-houb<>	РЕАК         6-ноце         2-ноце         72-ноце         Тотк         40 чче           379         50         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.65         15.6
J79.       40.5         J11.       12.05       15.05       15.05       15.05         J30.57       J97.40       J97.45       19.15       15.05         J30.57       J97.40       J97.45       19.15       15.05         J30.57       J97.45       J97.45       J97.45       19.05         Zbb       J4.       1       10.01       42         Zbb       J4.       1       10.01       42         Zbb       J11.       Zbb       J12.05       J12.05         Zbb       J11.       Zbb       J12.05       J12.05         Zbb       J11.1       Zbb       J12.05       J22.05         Zbb       J11.1       Tco       J4.01       J4.01         Zbb       Zbb       J12.05       J4.20       J4.20         Zbb       Zbb       J4.01       J4.20       J22.05         Zbb       Zbb       J4.20       J4.20       J4.20         Zbb	579.       5.0       17.       17.       17.       17.         11.       12.62       15.65       15.65       15.65       15.65       15.65         370.5       5.5       15.65       15.65       15.65       15.65       15.65         370.5       55.       52.       37.40       17.45       17.45       15.65         840058APH AT STA       1       1       1       17.4       15.4       15.4         757.       111.       74.404       72.4044       107AL VOLUE       2910.         757.       111.       74.404       71.20       910.       2010.         757.       111.       74.404       71.20       910.       2010.         757.       111.       74.404       71.20       910.       2010.         757.       111.       74.40       91.20       91.20       91.20         757.       111.       74.40       91.20       91.20       91.20         757.       111.       74.40       91.20       94.20       94.20         757.       21.21       71.20       71.20       71.20       94.20         759.       54.20       94.20       94.20	17.     17.     17.     17.     10.5.       11.     12.02     15.05     15.05     15.05     15.05       25.     37.     37.     37.     37.       25.     37.     37.     37.     37.       36.     13.     17.     17.     17.65       37.     17.     17.65     37.40     37.40       77.     111.     7.     72.     37.25       77.     111.     74.     72.404     70.14       77.     111.     74.     70.14     99.0       77.     111.     74.     70.14     99.0       77.     111.     74.40     71.20     77.20       77.     111.     74.40     71.20     79.20       77.     111.     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71.     74.40     74.40     74.40     74.40       71. <td>770.     770.     770.     770.       11.     12.07     15.05     15.05     15.05       12.07     15.05     15.05     15.05     15.05       370.     370.     370.     371.     31.05       370.     31.     42.     37.05     17.05       31.     32.     42.     37.05     17.05       31.     10.     72.000     101.11     101.12       777     111.     74.00     72.000     17.05       777     111.     74.00     74.00     9010       777     111.     74.00     74.00     9010       777     111.     74.00     11.12     74.00       711.     74.05     74.00     12.05     12.05       711.     74.05     74.00     12.05     12.05       711.     74.05     74.00     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05</td>	770.     770.     770.     770.       11.     12.07     15.05     15.05     15.05       12.07     15.05     15.05     15.05     15.05       370.     370.     370.     371.     31.05       370.     31.     42.     37.05     17.05       31.     32.     42.     37.05     17.05       31.     10.     72.000     101.11     101.12       777     111.     74.00     72.000     17.05       777     111.     74.00     74.00     9010       777     111.     74.00     74.00     9010       777     111.     74.00     11.12     74.00       711.     74.05     74.00     12.05     12.05       711.     74.05     74.00     12.05     12.05       711.     74.05     74.00     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05       711.     74.05     74.05     12.05     12.05
12.02     15.05     15.05     15.05     15.05       320.57     307.40     307.40     307.40     34.       34.     42.     42.     42.     42.       34.     42.     42.     42.     42.       34.     42.     42.     42.     42.       34.     42.     42.     42.     42.       34.     42.     42.     42.     42.       34.     51.     74.40     70141     9010.41       757.     111.     74.41     72.4044     70141       757.     111.     74.41     72.4044     70141       757.     111.     74.45     794.63     794.63       757.     111.     74.63     794.63     794.63       757.     21.1     794.63     794.63     794.63       757.     25.     54.31     794.63     794.63       66.     68.     68.     68.     68.       65.     74.63     794.63     794.63       757.     794.63     794.63     794.63       757.     68.     68.     68.       65.     68.     68.     68.       75.     71.1     70.0     0       74.1	11.02       15.05       15.05       15.05       15.05       15.05         320.57       397.40       31.       31.       31.         47       42.       42.       42.       42.         47       42.       42.       42.       42.         47       42.       42.       42.       42.         47       11       42.       42.       42.         757       111       74.       72.404       701.41         757       111       74.       72.404       701.41         757       111       74.       72.404       950.         757       111       74.       72.404       950.         757       111       74.       72.440       950.         71       21.29       31.29       31.20       31.20         21.23       794.60       96.       96.       96.         65.       64.       74.60       97.60       96.         65.       64.       94.       94.       94.         65.       64.       74.60       94.       94.         65.       64.       94.       94.       94.         66.	12.02     15.05     15.05     15.05     15.05       320.57     397.40     397.40     397.40       34.     47     42     54       35.     47     42     54       34.     47     47     42       34.     10.8     74.40     10.14       757     111     14     74       757     111     14     74       757     111     14     74       757     111     14     74       757     111     74     74       71     14     74     74       71     74     74     74       71     74     74     74       71     74     74     74       71     74     74     74       71     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74       75     74     74     74	12.02       15.05       15.05       15.05       15.05         31.       12.       12.       12.       12.       12.         31.       12.       12.       12.       12.       12.         31.       12.       12.       12.       12.       12.         31.       12.       12.       12.       12.       12.         31.       12.       12.       12.       12.       12.         11.       12.       11.       12.       12.       12.         127.       111.       12.       12.       12.       12.         127.       111.       12.       12.       12.       12.         127.       111.       12.       12.       12.       12.         127.       111.       12.       12.       12.       12.         127.       11.       12.       12.       12.       12.       12.         127.       11.       12.       12.       12.       12.       12.       12.         127.       12.       12.       12.       12.       12.       12.       12.         128.       12.       12.       <
32-57     397.00     34.       34.     42.     42.     42.       34.     42.     42.     42.       34.     42.     42.     42.       34.     42.     42.     42.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       757.     111.     74.     75.       751.     25.     58.     58.       64.     74.     79.     74.       65.     68.     68.     64.       65.     74.     74.     77.       66.     74.     79.     74.       66.     74.     74.     74.       66.     74.     74.     74.       75.     74.     74.     74.       75.     74.	323-57     397.40     397.40     397.40       **DRGGRAPH AT STA     1     09     47       **DRGGRAPH AT STA     1     1     104       **TORGGRAPH AT STA     1     104     1       **TORGGRAPH AT STA     1     104     1       **TORGGRAPH AT STA     1     104     1       **TORGGRAPH AT STA     1     1     101       **TORGGRAPH AT STA     1     1     101       **TORGGRAPH AT STA     1     1     101       757     111     7     1     2       757     111     7     1     2       757     111     7     1     2       757     111     7     1     2       757     111     7     1     2       251     25.24     11.29     7     3       251     25.24     11.29     7     3       25     7     3     3     2       64     7     3     3     3       65     7     3     3     3       66     68     64     3       66     68     64     3       7     10     0     0       7	320-57     397.45     34       34     34     47     34       34     34     47     34       751     1     1     1     1       752     111     74     70     9010       753     111     74     70     9010       751     111     74     74     9010       752     111     74     71     9010       753     111     74     74     9010       751     25     31.29     31.29     31.20       751     25     31.29     31.20     794.80       751     74     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     25     794.80     794.80     794.80       751     26	37-57     397-55     397-55     34       34     47     42     34       34     47     42     34       34     47     42     34       34     47     42     404       754     410     74     9930       755     3     31.29     31.29       21     3     31.29     31.29       21     3     74.40     74.40       64     94     94     94       64     74.40     94     94       64     74.40     94     94       64     74.40     74.40     94       64     74.40     94     94       64     74.40     94     94       64     74.40     94     94       64     74.40     94     94       75     74.40     94     94       75     74     94     94       75     74     94     94       75     74     94     94       75     74     94     94       75     74     94     94       76     74     94     94       76     74     74     94
34.     42.     42.     42.     42.       #IDAUGRAPH AT STA     1 rog PLAN 1. PTIO 9     20.00     20.00       Pffax     6-400m     24-400m     72-400m     70.10m       757.     111.     74.     72-400m     70.10m       757.     111.     74.     72.400m     72.400m       757.     111.     74.     72.400m     70.00m       757.     111.     74.     72.400m     70.00m       757.     111.     74.57     70.20     70.20       751.     25.     54.     95.     95.       65.     66.     66.     66.     66.       66.     94.     94.     94.       66.     74.60     94.     94.       66.     74.60     94.     94.       66.     74.60     94.     94.       67.     94.     94.     94.       68.     74.60     74.60     74.60       74.60     11.40     11.40     11.40       74.60     10.0     0     0     0       72.     10.0     0     0     0	34.     42.     42.     42.     42.     42.       **100068APH AT STA     1 rog PLAN 1. PT20 P     9030.     9030.       757.     111.     74.     72.     9030.       757.     111.     74.     71.     72.       757.     111.     74.     71.     74.       757.     111.     74.     71.     74.       757.     111.     74.     71.     74.       757.     111.     74.     71.     74.       751.     25.     11.     74.     75.       65.     68.     68.     68.     68.       65.     74.     74.     84.       66.     74.     34.     84.       66.     74.     34.     10.       66.     74.     34.     10.       66.     74.     34.     10.       66.     74.     34.     10.       67.     94.     10.     10.       68.     68.     64.     10.       69.     74.     10.     10.       71.     10.     10.     10.       72.     10.     0.     0.       73.     10.     0.     0.	34.     42.     42.     42.     42.       #IDRGGRAPH AT STA     1 row plan     1 row plan     11.       757.     111.     74.     72.       757.     111.     74.     72.       757.     111.     74.     72.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       757.     111.     74.     74.       75.     64.     74.     64.       64.     64.     64.     64.       65.     74.     34.     64.       66.     74.     34.     64.       65.     74.     34.     64.       65.     74.     34.     64.       64.     74.     64.     64.       65.     74.     64.     64.       64.     74.     74.     74.       65.     74.     74.	34.     42.     42.     42.       #IDRGGAAPH AT STA     1 rog PLAN 1. PTIO 9     40.4     70141 VOLVE       754.     6-HOUR     74.40.4     70141 VOLVE       757.     3.     3.     3.       757.     3.     3.     3.       757.     3.     3.     3.       757.     3.     3.     3.       757.     3.     3.     3.       757.     3.     3.     3.       757.     3.     3.     3.       757.     5.     9.     3.       65.     94.     94.       65.     94.     94.       65.     94.     94.       65.     94.     94.       65.     94.     94.       65.     94.     94.       65.     94.     94.       66.     1116.     1116.       7     10.     0.     0.       2     1     10.     0.       2     1     10.     0.
#1 BROGRAFM AT STA       1 rog FLAM 1. FTTO 9         #1 BROGRAFM AT STA       1 rog FLAM 1. FTTO 9         757.       111.       74.       79.0         757.       111.       74.       74.       9910.         757.       111.       74.       74.       9910.         757.       111.       74.       74.       9910.         757.       111.       74.       74.       9910.         757.       112.       74.       74.       91.20         6411       7450       79450       79450       79450         65.       66.       66.       67.       64.         65.       66.       66.       66.       64.         65.       66.       66.       64.       64.         65.       66.       66.       64.       64.         65.       66.       66.       64.       64.         65.       66.       7460       64.       64.         65.       66.       7460       64.       64.         65.       66.       7460       64.       64.         65.       66.       7460       64.       64. <td>**PROGRAPH AT STA       1 FOR PLAN 1. PTIO 9         **PROGRAPH AT STA       1 FOR PLAN 1. PTIO 9         777.       111.       14.       9030.         777.       111.       14.       14.       9030.         777.       111.       14.       14.       9030.         777.       111.       14.       14.       9030.         778.       31.27       31.27       221.       221.         71.       74.57       31.27       31.27       221.         74.53       54.55       794.55       794.52       521.         66.       68.       68.       68.       68.         68.       64.       94.       84.       84.         08.       74.53       794.53       794.53       54.53         75.       64.       94.       94.       84.         08.       74.53       64.53       744.53       64.53         75.       74.53       74.53       74.53       744.53         75.       74.53       74.53       744.53       744.53         75.       74.53       744.53       744.53       744.53         74.53       744.54       744.54</td> <td>#FAR Gran I. FTIO 9         FFAR G-HOUR 24-HOUR 72-HOUR TOTAL VOLVEL         757         757         757         757         757         757         757         757         757         757         74         757         757         711         74         757         74         757         74         74         74         74         757         74         74         74         75         74         75         74         75         74         75         74         75         74         75         74         74         75         74         74         74         75         74         75         74         74         74         74         74</td> <td>«НОВОСБАРН АТ STA T ГОЯ РLAN T. #T20 9 # 4 4 6-HOUR 24-MOUR 72-MOUR 72-MOUR 757 757. 3 1. 1. 1. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.</td>	**PROGRAPH AT STA       1 FOR PLAN 1. PTIO 9         **PROGRAPH AT STA       1 FOR PLAN 1. PTIO 9         777.       111.       14.       9030.         777.       111.       14.       14.       9030.         777.       111.       14.       14.       9030.         777.       111.       14.       14.       9030.         778.       31.27       31.27       221.       221.         71.       74.57       31.27       31.27       221.         74.53       54.55       794.55       794.52       521.         66.       68.       68.       68.       68.         68.       64.       94.       84.       84.         08.       74.53       794.53       794.53       54.53         75.       64.       94.       94.       84.         08.       74.53       64.53       744.53       64.53         75.       74.53       74.53       74.53       744.53         75.       74.53       74.53       744.53       744.53         75.       74.53       744.53       744.53       744.53         74.53       744.54       744.54	#FAR Gran I. FTIO 9         FFAR G-HOUR 24-HOUR 72-HOUR TOTAL VOLVEL         757         757         757         757         757         757         757         757         757         757         74         757         757         711         74         757         74         757         74         74         74         74         757         74         74         74         75         74         75         74         75         74         75         74         75         74         75         74         74         75         74         74         74         75         74         75         74         74         74         74         74	«НОВОСБАРН АТ STA T ГОЯ РLAN T. #T20 9 # 4 4 6-HOUR 24-MOUR 72-MOUR 72-MOUR 757 757. 3 1. 1. 1. 1. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2. 2.
Ff.K       6-HOUR       24-HOUR       72-HOUR       70.14       YOLUL         757.       111.       74.57       94.69       950.         21.       25.24       11.29       31.29       32.29         21.       25.24       11.29       31.29       32.29         641.11       794.65       98.       64.       64.         65.       64.       94.60       64.       84.         65.       74.65       64.       84.       84.         65.       74.65       64.       84.       84.         65.       74.65       94.       84.       84.         65.       74.65       94.       84.       84.         66.       74.65       94.       84.       84.         65.       74.65       94.       84.       94.         66.       74.65       74.65       74.65       74.65         67.       94.       94.       94.       94.       94.         74.147       74.145       74.145       74.145       74.145         74.147       74.145       74.145       74.145       74.145         74.147       74.145       74.145	Ff4k       6-HOUP       24-HOUP       74-HOUP       74-HOUP       74-HOUP         757       111       74-1       74-1       74-1         757       111       74-1       74-1       74-1         757       641-17       74-15       794.80       794.80         641-17       74-15       794.80       794.80       794.80         655       68       68       68       68       68         655       794.80       794.80       794.80       794.80         65       68       68       68       68       68         65       74       84       84       84       84         65       74       84       84       84       84         66       74       74       84       84       84         66       74       74       74       74       74         66       74       74       74       74       74         66       74       74       74       74       74         74       74       74       74       74       74         74       74       74       74       74       74 <td>Ff4x       6-HOUR       24-HOUR       74-HOUR       74-HOUR       74-HOUR         757.       111.       74.       51.2       52.2         21.       23.2       31.2       31.2       31.2         21.       23.2       31.2       31.2       31.2         21.       79.2       31.2       31.2       31.2         21.       79.2       51.2       31.2       31.2         411       74.2       794.8       794.2       51.2         55.       65.       74.5       94.2       64.2         55.       65.       74.5       94.2       64.2         66.       74.5       94.2       64.2       64.2         55.       74.5       94.2       94.2       94.2         66.       74.5       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         74.1       14.1       17.1       14.1       14.2         7       10.0       0       0       0       <t< td=""><td>Pf4x       5-HOUR       24-HOUR       72-HOUR       72-HOUR       9930         757       111       74.5       74.5       31.29       3.29         21.2       23.24       31.29       31.29       31.29         25.24       11.7       74.65       794.65       31.29         641.11       794.65       794.65       794.65       31.29         65.       68.       68.       68.       68.         64.       70.65       84.       84.         65.       794.65       794.65       794.63         64.       70.65       84.       84.         64.       70.65       94.       94.         64.       70.65       94.65       94.65         75.       68.       68.       64.         64.       70.       94.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.1.       74.6</td></t<></td>	Ff4x       6-HOUR       24-HOUR       74-HOUR       74-HOUR       74-HOUR         757.       111.       74.       51.2       52.2         21.       23.2       31.2       31.2       31.2         21.       23.2       31.2       31.2       31.2         21.       79.2       31.2       31.2       31.2         21.       79.2       51.2       31.2       31.2         411       74.2       794.8       794.2       51.2         55.       65.       74.5       94.2       64.2         55.       65.       74.5       94.2       64.2         66.       74.5       94.2       64.2       64.2         55.       74.5       94.2       94.2       94.2         66.       74.5       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         61.1       94.2       94.2       94.2       94.2         74.1       14.1       17.1       14.1       14.2         7       10.0       0       0       0 <t< td=""><td>Pf4x       5-HOUR       24-HOUR       72-HOUR       72-HOUR       9930         757       111       74.5       74.5       31.29       3.29         21.2       23.24       31.29       31.29       31.29         25.24       11.7       74.65       794.65       31.29         641.11       794.65       794.65       794.65       31.29         65.       68.       68.       68.       68.         64.       70.65       84.       84.         65.       794.65       794.65       794.63         64.       70.65       84.       84.         64.       70.65       94.       94.         64.       70.65       94.65       94.65         75.       68.       68.       64.         64.       70.       94.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.1.       74.6</td></t<>	Pf4x       5-HOUR       24-HOUR       72-HOUR       72-HOUR       9930         757       111       74.5       74.5       31.29       3.29         21.2       23.24       31.29       31.29       31.29         25.24       11.7       74.65       794.65       31.29         641.11       794.65       794.65       794.65       31.29         65.       68.       68.       68.       68.         64.       70.65       84.       84.         65.       794.65       794.65       794.63         64.       70.65       84.       84.         64.       70.65       94.       94.         64.       70.65       94.65       94.65         75.       68.       68.       64.         64.       70.       94.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       94.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.       74.65       74.65       74.65         74.11.1.       74.6
21.       3.       327       327       327         641.11       7965       7965       7965       7965         641.11       7965       7965       7965       7965         65.       64.       34.       64.       64.         65.       7465       7965       7965       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       64.       64.         65.       74.       34.       74.       74.         65.       74.       37.       37.       74.         65.       70.0       0       0       0       0         7       7 <td>ZI. 25.24 1.27 31.27 31.27 31.27 31.27 31.27 31.27 31.27 31.27 31.27 31.27 31.27 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