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BIPOLAR TRANSISTOR AND DIODE FAILURE TO ELECTRICAL TRANSIENTS---ETC(U)

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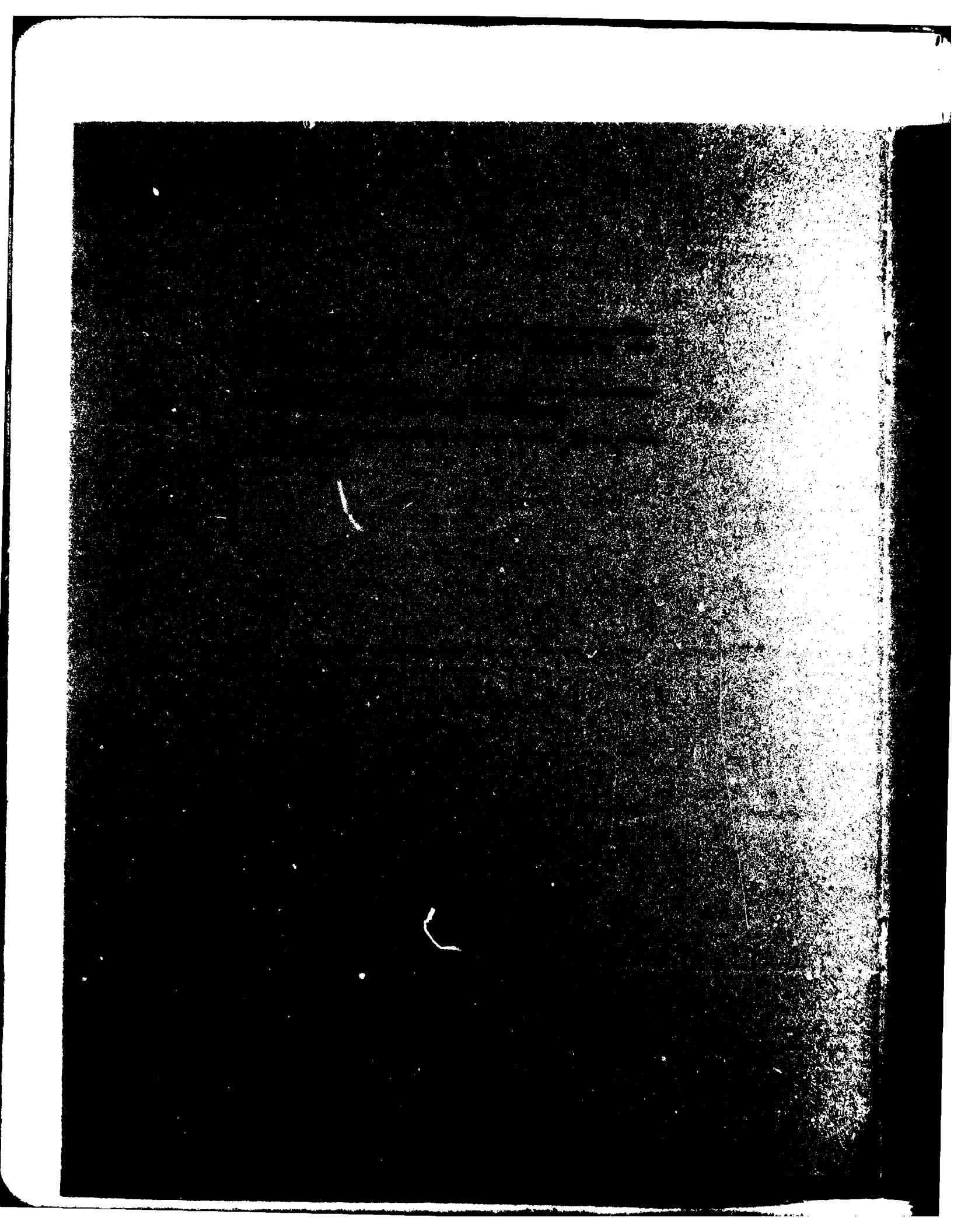
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An investigation of the predictive capability of a new Air Force Weapons Laboratory model for transistor and diode failure under reverse bias was initiated. A comparison with the junction capacitance damage model shows a doubled improvement at high confidence levels based on an Army-generated population of experimental damage data.		

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1. INTRODUCTION

A recent Air Force Weapons Laboratory (AFWL) document, Electronic Component Modeling and Testing Program, AFWL-TR-78-62 Pt.1 (March 1980), contains a new model for predicting bipolar transistor and diode failure for reverse junction bias. This paper examines the capability of this model using as a baseline a library of experimental damage data for devices from the front ends of an array of Army tactical multichannel radios.

2. EXAMINATION

The new model is implemented as follows:

- (1) Calculate doping concentration from room temperature breakdown voltage:

$$N_D = 4.49 \times 10^{18} V_{BD}^{-1.5}$$

where

N_D = doping concentration on lightly doped side of junction
(inverse cubic centimeters),

V_{BD} = room temperature breakdown voltage (volts).

- (2) Calculate breakdown voltage at critical failure temperature:

$$V_{BDC} = 4.07 \times 10^{12} N_D^{-0.67}$$

where

V_{BDC} = breakdown voltage at critical failure temperature
(volts).

- (3) Calculate space charge resistivity:

$$\rho_{SC} = 2.48 \times 10^{25} N_D^{-1.8}$$

where

ρ_{SC} = space charge resistivity (ohm-square centimeters).

- (4) Calculate bulk resistivity:

$$\rho_{BLK} = 3.61 \times 10^{10} N_D^{-0.81} ,$$

where

ρ_{BLK} = bulk resistivity (ohm-square centimeters).

- (5) Calculate failure current density at 100 ns:

Emitter-to-base junction:

$$J_F = 3.84 \times 10^{-11} N_D^{0.88} ,$$

where

J_F = failure current density at 100 ns (amperes/square centimeter).

Collector-to-base or diode junction:

$$J_F = 8.25 \times 10^{-11} N_D^{0.88} .$$

- (6) Calculate junction area:

Emitter-to-base junction:

Priority 1

$$\text{Area} = 1.47 \left(2.3 \times 10^{-6} C_{O_{EB}} V_{BD}^{0.67} \right)^{1.05} ,$$

where

$C_{O_{EB}} = C_{RE RF}^{0.5}$ = corrected emitter-to-base capacitance
(picofarads),

C_{RE} = emitter-to-base capacitance at rated voltage
(picofarads),

V_{RF} = rated voltage (volts),

V_{BD} = rated emitter-to-base breakdown voltage (volts).

Priority 2

$$\text{Area} = 6.34 \times 10^{-4} I_{MAX}^{0.82},$$

where

I_{MAX} = maximum rated transistor collector current (amperes).

Priority 3

$$\text{Area} = 8.75 \times 10^{-3} \left(2 \times 10^{-6} C_{OCB} V_{BDCB}^{0.83} \right)^{0.58},$$

where

$C_{OCB} = C_{RC} V_{RC}^{0.333}$ = corrected collector-to-base capacitance
(picofarads),

C_{RC} = collector-to-base capacitance at rated voltage
(picofarads),

V_{RC} = rated voltage for collector-to-base capacitance (volts),

V_{BDCB} = collector-to-base breakdown voltage (volts).

Priority 4

$$\text{Area} = 1.19 \times 10^{-2} \theta_{JC}^{-0.94},$$

where

θ_{JC} = junction-to-case thermal resistance (degrees
Celsius/watt).

Priority 5

$$\text{Area} = 2.79 \theta_{JA}^{-1.70},$$

where

θ_{JA} = junction-to-ambient thermal resistance (degrees Celsius/watt).

Collector-to-base junction:

Priority 1

$$\text{Area} = 0.047 \theta_{JC}^{-0.89} .$$

Priority 2

$$\text{Area} = 2.72 \times 10^{-3} I_{MAX}^{0.62} .$$

Priority 3

$$\text{Area} = 3.63 \theta_{JA}^{-1.47} .$$

Priority 4

$$\text{Area} = 1.13 \times 10^{-2} \left(2 \times 10^{-6} C_{O_{CB}} V_{BD}^{0.83} \right)^{0.39} .$$

Diode junction:

Priority 1

$$\text{Area} = 8.1 \times 10^{-3} I_{MAX}^{1.16}$$

where

I_{MAX} = maximum rated diode currents (amperes) for Zener diodes
 $= I_{ZM} V_Z$,

I_{ZM} = maximum rated Zener current (amperes),

V_Z = rated Zener voltage (volts).

Priority 2

$$\text{Area} = 0.458 \left(2 \times 10^{-6} C_{O_D} V_{BD}^{0.83} \right)^{0.83} ,$$

where

$$C_{O_D} = C_{RD} V_{RD}^{0.333} ,$$

C_{RD} = diode junction capacitance at rated voltage (picofarads),

V_{RD} = rated voltage (volts).

Priority 3

$$\text{Area} = 0.489\theta_{\text{JL}}^{-1.21} ,$$

where

θ_{JL} = junction-to-lead thermal resistance (degrees Celsius/watt).

Priority 4

$$\text{Area} = 1.963\theta_{\text{JA}}^{-1.32} .$$

(7) Calculate bulk resistance, space charge resistance, and failure current at 100 ns:

$$R_{\text{BLK}} = \rho_{\text{BLK}}/\text{area} ,$$

$$R_{\text{SC}} = \rho_{\text{SC}}/\text{area} ,$$

$$I_{\text{F } 100 \text{ ns}} = J_{\text{F}} \times \text{area} .$$

(8) Calculate power to damage for pulse duration t :

$$P_{\text{D}} = \left[V_{\text{BDC}} \frac{I_{\text{F } 100 \text{ ns}}}{3.162} + \frac{I_{\text{F } 100 \text{ ns}}^2}{10} (R_{\text{SC}} + R_{\text{BLK}}) \right] / 1000 t^{0.5} .$$

3. RESULTS

Appendix A lists a program used to implement the AFWL model, along with the input and resultant data. The model predictions are presented in figure 1 as

$$P_{\text{X}}/P , \text{ for } P_{\text{X}} \geq P ,$$

$$P/P_{\text{X}} , \text{ for } P < P_{\text{X}} ,$$

where

P_{X} = experimental power to damage,

P = corresponding predicted value,

as a function of the percentage confidence level. The percentage confidence level is defined as the percentage of data points with a ratio less than or equal to the given value. The envelope defined by the five priority models is plotted in figure 2 along with the predictions of the junction capacitance damage model for comparison and a plot of the scatter in the experimental data. The scatter in the experimental data is the ratio of the power to damage for the individual devices and the experimentally defined damage curve presented in the mode previously indicated for the AFWL model predictions. The experimental data base used for this projection includes but is larger than that indicated in appendix A. The total base of 822 devices comprised a test population of 82 P-N junction types. This population includes both germanium devices and specialty devices for which AFWL model data are unavailable.

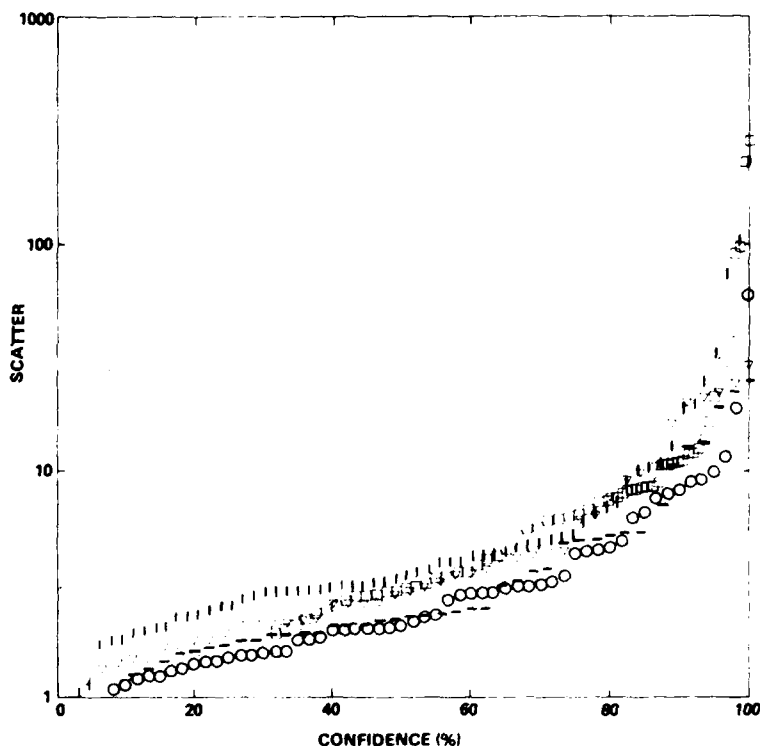


Figure 1. Percentage confidence level versus scatter in data for AFWL model: $\circ$ = priority 1, $\square$ = priority 2, ∇ = priority 3, $|$ = priority 4, and $-$ = priority 5.

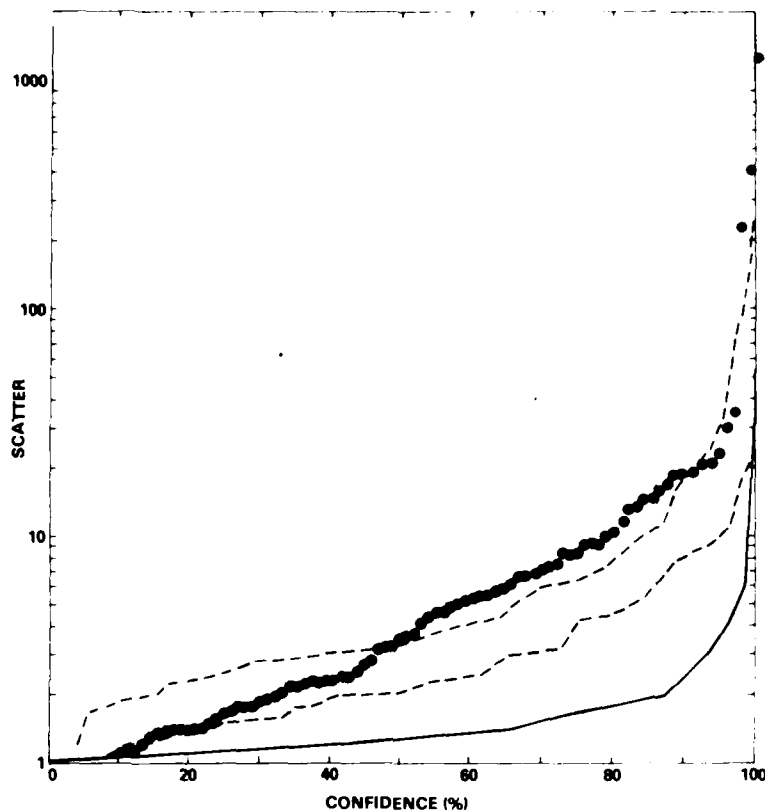


Figure 2. Percentage confidence level versus scatter in data for junction capacitance damage model (solid circles), limits of AFWL damage model (dashed curve), and experimental data (solid curve).

4. CONCLUSION AND DISCUSSION

At high confidence levels, the AFWL model represents approximately a doubled improvement over the junction capacitance damage model based on the device population employed in this study. One note of caution: The AFWL model, like all previous damage models, is for junction reverse bias only. To project from reverse bias failure to failure under forward bias is fraught with great difficulties. Figure 3 is a histogram of the experimental ratio of power to failure for forward and for reverse bias. (All measurements were made at 0.1-, 1-, and 10- μ s pulse durations.) Previous studies have shown that, despite the generally higher power to failure for forward bias, damage is as likely

to occur under forward as under reverse conditions for circuits driven to the failure level,^{1,2} The uncertainty indicated in figure 3 must be included in the uncertainty of the damage model predictions in projecting damage characteristics to forward bias.

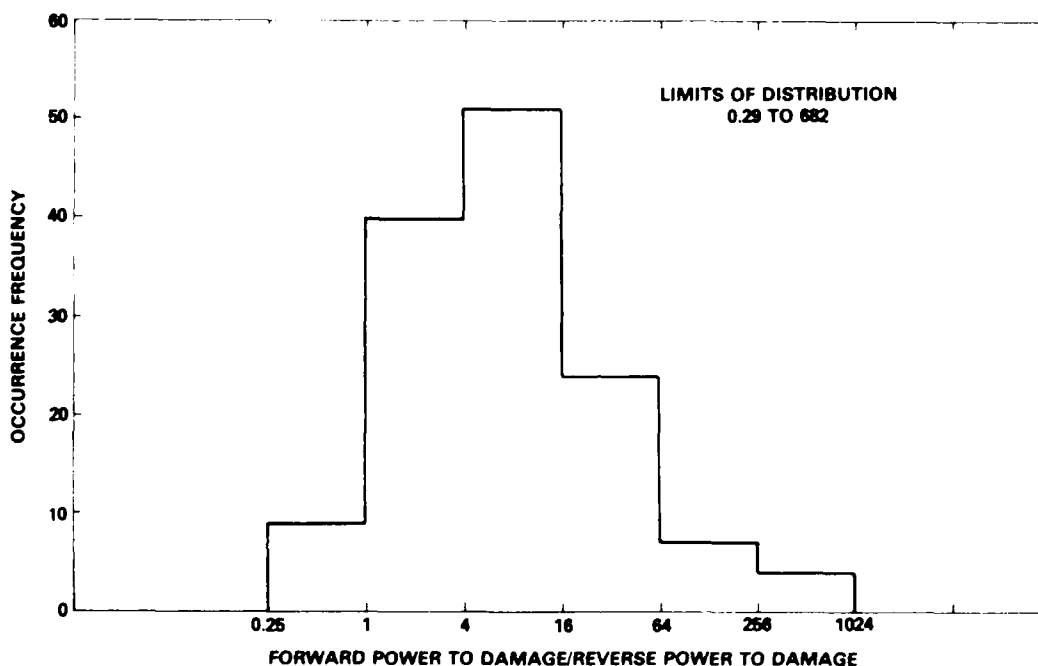


Figure 3. Histogram of ratio of experimental power to damage for forward and reverse junction bias for pulse durations in 0.1- to 10- μ s range for 78 percent of P-N junction types included in appendix A.

¹Michael J. Vrabel, *EMP Assessment for Army Tactical Communications Systems: Transmission Systems Series No. 3 Radio Terminal Sets AN/TRC-112 and AN/TRC-121 (U)*, Harry Diamond Laboratories HDL-TR-1807 (May 1977). (SECRET-RESTRICTED DATA)

²George Gornak et al, *EMP Assessment for Army Tactical Communications Systems: Transmission Systems Series No. 1 Radio Terminal Set AN/TRC-145 (U)*, Harry Diamond Laboratories HDL-TR-1746 (February 1976). (SECRET-RESTRICTED DATA)

APPENDIX A.--AIR FORCE WEAPONS LABORATORY MODEL CODE, INPUT DATA, AND
RESULTS OF PREDICTING BIPOLAR TRANSISTOR AND DIODE FAILURE
FOR REVERSE JUNCTION BIAS

APPENDIX A

```

C DAT(1,N)=-1: DIODE JUNCTION, 0: C-B JUNCTION, 1: E-B JUNCTION
C DAT(2,N)=BREAKDOWN VOLTAGE (V)
C DAT(3,N)= DIODE CAPACITANCE (PF), DEFAULT VALUE=0
C DAT(4,N)=C-B CAPACITANCE, DEFAULT VALUE=0
C DAT(5,N)= E-B CAPACITANCE (PF), DEFAULT VALUE=0
C DAT(6,N)=MAXIMUM RATED COLLECTOR OR DIODE CURRENT(A)
C DAT(7,N)=JUNCTION-TO -CASE THERMAL RESISTANCE(THETA JC) (C/W)
C DAT(8,N)=JUNCTION-TO-AMBIENT THERMAL RESISTANCE(THETA JA) (C/W)
C DAT(9,N)=BREAKDOWN VOLTAGE FOR C-B FOR EMITTER DATA
C DAT(10,N)=EXPERIMENTAL POWER TO DAMAGE AT 0.1US
C DAT(11,N)=EXPERIMENTAL POWER TO DAMAGE AT 1 US
C DAT(12,N)=EXPERIMENTAL POWER TO DAMAGE AT 10 US
      DIMENSION DAT(12,68), DOPE(68), BV(68), RHQSC(68), RHQBLK(68)
      DIMENSION FAILI(68), AREA(5,68), RBLK(5,68), RSC(5,68), CUR(5,68)
      DIMENSION D(5,68), RATIO(5,3,68), BIG(5), MZ(5), NZ(5), SET(5)
      DIMENSION B(5,150), C(5,150), MV(5), RESULT(5,300)
      DIMENSION DEVICE(272), RAT(5,3,68)
      DIMENSION AVG(3,68), BB(200), CC(200), RSLT(400)
      NAMELIST/LISTA/DAT,DEVICE
      READ(5,LISTA)
      WRITE(6,1)
1     FORMAT(20X,10HBREAKDOWN ,10H DIODE ,10H C-B ,
      10H E-B ,10H COLL. CURR,10H THETA JC ,10H THETA JA ,
      10H BV C-B ,10HDAMAGE ,10HDAMAGE ,10HDAMAGE )
      WRITE(6,2)
2     FORMAT(20X,10H VOLTAGE ,10H CAP. ,10H CAP. ,
      10H CAP. ,10H MAX. ,30X,10H (0.1US) ,
      10H (1.0US) ,10H (10.US) )
      WRITE(6,3)
3     FORMAT(20X,10H (VOLTS) ,10H (PF) ,10H (PF) ,
      10H (PF) ,10H (AMP) ,10H (C/WATT) ,10H (C/WATT) ,
      10H (VOLTS) ,10H (WATTS) ,10H (WATTS) ,10H (WATTS) )
      WRITE(6,4)
4     FORMAT(2X)
      DO 201 N=1,65
      M=4*(N-1)+1
      MM=M+1
      MMM=MM+1
      MMMM=MMM+1
      WRITE(6,200)DEVICE(M),DEVICE(MM),DEVICE(MMM),DEVICE(MMMM),
      1(DAT(M,N),M=2,12)
200    FORMAT(2X,4A4,8F10.3,3F10.2)
201    CONTINUE
      DO 100 N=1,68
      IF(DAT(2,N).EQ.0.) GO TO 100
      DOPE(N)=(4.49E+18)*DAT(2,N)**(-1.5)
100    CONTINUE
      DO 101 N=1,68
      IF(DOPE(N).EQ.0.) GO TO 101
      BV(N)=(4.07E+12)*(DOPE(N))**(-0.67)
101    CONTINUE
      DO 102 N=1,68
      IF(DOPE(N).EQ.0.) GO TO 102
      RHQSC(N)=(2.48E+25)*(DOPE(N))**(-1.8)
102    CONTINUE
      DO 103 N=1,68
      IF(DOPE(N).EQ.0.) GO TO 103

```

APPENDIX A

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      RHOBK(N)=(3.61E+10)*(DOPE(N))*(-0.81)
103  CONTINUE
      DO 104 N=1,68
      IF(DAT(1,N))105,105,106
105  FAIL1(N)=(8.26E-11)*(DOPE(N))*(-0.88)
      GO TO 104
106  FAIL1(N)=(3.84E-11)*(DOPE(N))*(-0.88)
104  CONTINUE
      DO 107 N=1,68
      IF(DAT(1,N))110,109,108
108  AREA(1,N)=1.47*((2.3E-06)*DAT(5,N)*DAT(2,N)**0.67)**1.05
      AREA(2,N)=(6.34E-04)*(DAT(6,N))*0.82
      AREA(3,N)=(8.75E-03)*(2.E-06)*DAT(4,N)*(DAT(9,N))*0.83**0.58
      IF(DAT(7,N).EQ.0.) GO TO 150
      AREA(4,N)=(1.19E-2)*(DAT(7,N))*(-0.94)
150  IF(DAT(8,N).EQ.0.) GO TO 107
      AREA(5,N)=2.79*DAT(8,N)*(-1.7)
      GO TO 107
109  IF(DAT(7,N).EQ.0.) GO TO 151
      AREA(1,N)=0.047*(DAT(7,N))*(-0.89)
151  AREA(2,N)=(2.72E-03)*(DAT(6,N))*(-0.62)
      IF(DAT(8,N).EQ.0.) GO TO 152
      AREA(3,N)=3.63*(DAT(8,N))*(-1.47)
152  AREA(4,N)=(1.13E-02)*(2.E-06)*DAT(4,N)*DAT(2,N)*0.83**0.39
      GO TO 107
110  AREA(1,N)=(8.1E-03)*DAT(6,N)**1.16
      AREA(2,N)=0.458*(2.E-06)*DAT(3,N)*DAT(2,N)*0.83**0.83
      IF(DAT(7,N).EQ.0.) GO TO 153
      AREA(3,N)=0.489*DAT(7,N)*(-1.21)
153  IF(DAT(8,N).EQ.0.) GO TO 107
      AREA(4,N)=1.963*DAT(8,N)*(-1.32)
107  CONTINUE
      DO 111 N=1,68
      DO 112 M=1,5
      IF(AREA(M,N).EQ.0.) GO TO 112
      RBLK(M,N)=RHOBK(N)/AREA(M,N)
      RSC(M,N)=RHOSC(N)/AREA(M,N)
      CUR(M,N)=FAIL1(N)*AREA(M,N)
112  CONTINUE
111  CONTINUE
      DO 116 N=1,68
      DO 113 M=1,5
      D(M,N)=(BV(N)*(CUR(M,N)/3.162)+(CUR(M,N)**2)/10.)*
      (RSC(M,N)+RBLK(M,N))/1000.
113  CONTINUE
116  CONTINUE
      DO 117 N=1,68
      DO 118 M=1,3
      DO 114 K=1,5
      MM=9+M
      AM=M-1
      IF(D(K,N).EQ.0.) GO TO 114
      RATIO(K,M,N)=DAT(MM,N)/(D(K,N)*3162.**(10.)*(-0.5*AM))
      RAT(K,M,N)=RATIO(K,M,N)
      IF(RATIO(K,M,N).EQ.0.) GO TO 114
      IF(RATIO(K,M,N).GE.1.) GO TO 114
      RATIO(K,M,N)=1./RATIO(K,M,N)
114  CONTINUE
118  CONTINUE
117  CONTINUE

```

APPENDIX A

```

      WRITE(6,15)
15  FORMAT(2X////)
      WRITE(6,5)
5   FORMAT(2X,123HRATIO OF EXPERIMENTAL POWER TO DAMAGE TO PREDICTED V
      EALUE FOR 0.1, 1.0, AND 10 USEC PULSE DURATIONS FOR FIVE PRIORITY M
      ODEL5//)
      WRITE(6,6)
6   FORMAT(26X,12H  PRTY 1  ,12H  PRTY 2  ,12H  PRTY 3  ,
      12H  PRTY 4  ,12H  PRTY 5  /)
      DO 312 L=1,3
      DO 311 N=1,65
      M=4*(N-1)+1
      MM=M+1
      MMM=MM+1
      MMMM=MMM+1
      WRITE(6,310)DEVICE(M),DEVICE(MM),DEVICE(MMM),DEVICE(MMMM),
      C(RAT(K,L,N),K=1,5)
310  FORMAT(10X,4A4,5F12.4)
311  CONTINUE
      WRITE(6,313)
313  FORMAT(2X//)
312  CONTINUE
      DO 800 N=1,68
      DO 801 M=1,3
      AJ=0.
      DO 802 K=1,5
      AVG(M,N)=RATIO(K,M,N)+AVG(M,N)
      IF(RATIO(K,M,N).EQ.0.) GO TO 802
      AJ=1.+AJ
802  CONTINUE
      IF(AVG(M,N).EQ.0.) GO TO 801
      AVG(M,N)=AVG(M,N)/AJ
801  CONTINUE
800  CONTINUE
      DO 803 LL=1,200
      DO 804 N=1,68
      DO 805 M=1,3
      IF(AVG(M,N).EQ.0.) GO TO 805
      IF(AVG(M,N).LE.BIGG) GO TO 805
      BIGG=AVG(M,N)
      MAVG=M
      NAVG=N
805  CONTINUE
804  CONTINUE
      NZAA=1+NZAA
      IF(SETT.EQ.1.) GO TO 806
      IF(BIGG.NE.0.) GO TO 806
      SETT=1.
      MVV=NZAA-1
      MAV=MVV
806  CONTINUE
      BB(NZAA)=BIGG
      BIGG=0.
      AVG(MAVG,NAVG)=0.
803  CONTINUE
      DO 808 N=1,200
      BN=N-1
      AMV=MVV
      CC(N)=100.-BN*(100./AMV)
808  CONTINUE

```

APPENDIX A

```

MM=0
DO 880 N=1,MVV
AVERAG=BB(N)+AVERAG
880 CONTINUE
AVERAG=AVERAG/AMV
DO 809 N=1,MVV
MM=1+MM
RSLT(MM)=BB(N)
MM=1+MM
RSLT(MM)=CC(N)
809 CONTINUE
DO 130 LL=1,150
DO 123 N=1,68
DO 124 M=1,3
DO 120 K=1,5
IF(RATIO(K,M,N).EQ.0.) GO TO 120
IF(RATIO(K,M,N).LE.BIG(K)) GO TO 120
BIG(K)=RATIO(K,M,N)
MZ(K)=M
NZ(K)=N
120 CONTINUE
124 CONTINUE
123 CONTINUE
NZA=1+NZA
DO 131 KK=1,5
IF(SET(KK).EQ.1.) GO TO 131
IF(BIG(KK).NE.0.) GO TO 131
SET(KK)=1.
MV(KK)=NZA-1
131 CONTINUE
DO 132 KK=1,5
B(KK,NZA)=BIG(KK)
BIG(KK)=0.
132 CONTINUE
DO 133 KK=1,5
MZZ=MZ(KK)
NZZ=NZ(KK)
RATIO(KK,MZZ,NZZ)=0.
133 CONTINUE
130 CONTINUE
DO 140 N=1,150
DO 135 K=1,5
BN=N-1
AMV=MV(K)
C(K,N)=100.-BN*(100./(AMV+.0000001))
135 CONTINUE
140 CONTINUE
DO 142 K=1,5
MVV=MV(K)
MM=0
DO 141 N=1,MVV
MM=1+MM
RESULT(K,MM)=B(K,N)
MM=1+MM
RESULT(K,MM)=C(K,N)
141 CONTINUE
142 CONTINUE
WRITE(6,11)
11 FORMAT(2X////)
WRITE(6,10)

```

APPENDIX A

```

10  FORMAT(2X,128HRATIO EXPERIMENTAL AND PREDICTED POWER TO DAMAGE VS
    PERCENTAGE CONFIDENCE LEVEL FOR ALL PULSE DURATIONS FOR FIVE PRIOR
    CITY MODELS//)
    DD 145 K=1,5
    MJV=(MV(K)+1)*2
    WRITE(6,146)(RESULT(K,M),M=1,MJV)
146  FORMAT(5X,2F9.2,3X,2F9.2,3X,2F9.2,3X,2F9.2,2X,2F9.2)
    WRITE(6,12)
12  FORMAT(2X//)
145  CONTINUE
    WRITE(6,810)
810  FORMAT(2X////)
    WRITE(6,811)
811  FORMAT(2X,124HRATIO OF EXPERIMENTAL AND PREDICTED POWER TO DAMAGE
    VS PERCENTAGE CONFIDENCE LEVEL FOR AVERAGE VALUE OF FIVE PRIORITY
    MODELS//)
    MJV=(MAV+1)*2
    WRITE(6,146)(RESULT(M),M=1,MJV)
    WRITE(6,810)
    WRITE(6,881)AVERAG
881  FORMAT(15X,31ARITHMETIC MEAN OF ABOVE DATA =,F9.2)
    STOP
    END

```

```

/*
//GD.SYSIN DD *
ELISTA DAT=0,120,0,11,0,.05,0,357,120,140,52,20,
1,33,0,0,9,.05,0,357,120,30,16,9,
0,250,0,16,0,.025,0,0,250,300,80,20,
1,27,0,0,9,.025,0,0,250,100,44,20,
0,54,0,17,0,0,0,1000,54,160,70,30,
1,7,0,0,22,0,0,1000,54,625,112,70,
0,200,0,4,3,0,.05,0,500,200,50,46,42,
1,10,2,0,0,5,3,.05,0,500,200,160,48,15,
0,107,0,142,0,1,5,0,345,107,115,72,44,
1,7,8,0,0,53,1,5,0,345,107,590,255,110,
0,45,0,8,0,.03,0,500,45,180,74,30,
1,5,0,0,0,.03,0,500,45,230,60,16,
0,108,0,57,0,0,0,476,108,10,10,10,
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APPENDIX A

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 4H2N33,4H5(C-,4HB),4H,
 4H2N33,4H5(E-,4HB),4H,
 4H2N33,4H6:JA,4HN(C-,4HB),
 4H2N33,4H6:JA,4HN(E-,4HB),
 4H2N24,4H84(C,4H-B),4H,
 4H2N24,4H84(E,4H-B),4H,
 4H2N37,4H36(C,4H-B),4H,
 4H2N37,4H36(E,4H-B),4H,
 4H2N93,4H0(C-,4HB),4H,
 4H2N93,4H0(E-,4HB),4H,
 4H2N24,4H81(C,4H-B),4H,
 4H2N24,4H81(E,4H-B),4H,
 4H2N29,4H07A(,4HC-B),4H,
 4H2N29,4H07A(,4HE-B),4H,
 4H2N22,4H22A(,4HC-B),4H,
 4H2N22,4H22A(,4HE-B),4H,
 4H1N43,4H84,4H,4H,
 4HF591,4H1-34,4H65,4H,
 4H1N81,4H6,4H,4H,
 4H1N21,4HWE,4H,4H,
 4H1N91,4H4A,4H,4H,
 4H1N75,4H2A,4H,4H,
 4HPC11,4H5,4H,4H,
 4H1N30,4H26B:,4HJAN,4H,
 4H1N36,4H11,4H,4H,
 4H1N39,4H95A,4H,4H,
 4H1N30,4H16B,4H,4H,
 4H1N41,4H41,4H,4H,

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4H1002,4H      ,4H      ,4H      .
4H2N28,4H57(C,4H-B) ,4H      .
4H2N28,4H57(E,4H-B) ,4H      .
4H2N33,4H75(C,4H-B) ,4H      .
4H2N33,4H75(E,4H-B) ,4H      .
4H2N14,4H90:J,4HAN(C,4H-B) .
4H2N14,4H90:J,4HAN(E,4H-B) .
4H2N35,4H84(C,4H-B) ,4H      .
4H2N35,4H84(E,4H-B) ,4H      .
4H2N28,4H94(C,4H-B) ,4H      .
4H2N28,4H94(E,4H-B) ,4H      .
4H2N58,4H29(C,4H-B) ,4H      .
4H2N58,4H29(E,4H-B) ,4H      .
4H2N30,4H13:J,4HAN(C,4H-B) .
4H2N30,4H13:J,4HAN(E,4H-B) .
4HCA30,4H18(C,4H-B) ,4H      .
4HCA30,4H18(E,4H-B) ,4H      .
4H2N16,4H13:J,4HAN(C,4H-B) .
4H2N16,4H13:J,4HAN(E,4H-B) .
4H2N14,4H85:J,4HAN(C,4H-B) .
4H2N14,4H85:J,4HAN(E,4H-B) .
4H2N34,4H39(C,4H-B) ,4H      .
4H2N34,4H39(E,4H-B) ,4H      .
4H2N70,4H6:JA,4HN(C-,4HB) .
4H2N70,4H6:JA,4HN(E-,4HB) .
4H1N25,4H80      ,4H      ,4H      .
4H1N75,4H1A:J,4HAN      ,4H      .
4H1N48,4H5B:J,4HAN      ,4H      .
4H1N29,4H918: 4HJAN ,4H      .
4H1N30,4H25E:,4HJAN ,4H      .
4HMO10,4H54      ,4H      ,4H      .
4H1N74,4H6A:J,4HAN      ,4H      .
4H1N64,4H5:JA,4HN      ,4H      .
4H1N12,4H02RA,4H:JAN,4H      .
4H1N17,4H31A:,4HJAN ,4H      .
END.
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APPENDIX A

BREAKDOWN VOLTAGE (VOLTS)	DIODE CAP. (PF)	C-B CAP. (PF)	F-B CAP. (PF)	COLL. CURR MAX. (AMP)	THETA JC (C/MATT)	THETA JA (C/MATT)	BY C-B (VOLTS)	DAMAGE (0.1US) (WATTS)	DAMAGE (1.0US) (WATTS)	DAMAGE (10.0US) (WATTS)
2N328A1C(-B)	0.0	11.000	0.0	0.050	0.0	357.000	120.000	140.00	52.00	20.00
2N328A1E(-B)	0.0	0.0	9.000	0.050	0.0	357.000	120.000	16.00	16.00	9.00
2N3351C(-B)	0.0	16.000	0.0	0.025	0.0	0.0	250.000	300.00	80.00	20.00
2N3351E(-B)	0.0	0.0	9.000	0.025	0.0	0.0	250.000	100.00	44.00	20.00
2N3362JAN1C(-B)	0.0	17.000	0.0	0.0	0.0	1000.000	54.000	160.00	70.00	30.00
2N3362JAN1E(-B)	0.0	0.0	22.000	0.0	0.0	1000.000	54.000	625.00	112.00	70.00
2N3641C(-B)	0.0	4.300	0.0	0.050	0.0	500.000	200.000	50.00	46.00	42.00
2N3641E(-B)	0.0	0.0	5.300	0.050	0.0	500.000	200.000	160.00	48.00	15.00
2N37361C(-B)	0.0	142.000	0.0	1.500	0.0	345.000	107.000	115.00	72.00	44.00
2N37361E(-B)	0.0	0.0	53.000	1.500	0.0	345.000	107.000	590.00	255.00	110.00
2N9301C(-B)	0.0	8.000	0.0	0.030	0.0	500.000	45.000	180.00	74.00	30.00
2N9301E(-B)	0.0	0.0	0.0	0.030	0.0	500.000	45.000	230.00	60.00	16.00
2N24811C(-B)	0.0	57.000	0.0	0.0	0.0	476.000	108.000	10.00	10.00	10.00
2N24811E(-B)	0.0	0.0	8.000	0.0	0.0	476.000	108.000	53.00	30.00	18.00
2N2907A1C(-B)	0.0	18.000	0.0	0.600	0.0	434.000	93.000	135.00	53.00	20.00
2N2907A1E(-B)	0.0	0.0	23.000	0.600	0.0	434.000	93.000	110.00	78.00	53.00
2N2222A1C(-B)	0.0	15.000	0.0	0.800	0.0	303.000	107.000	220.00	85.00	32.00
2N2222A1E(-B)	0.0	0.0	31.000	0.800	0.0	303.000	107.000	400.00	135.00	40.00
1M6384	0.0	0.0	0.0	1.000	0.0	0.0	0.0	2800.00	2300.00	2100.00
F5911-3465	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4100.00	2700.00	1600.00
1M816	0.0	0.0	0.0	0.0	0.0	0.0	0.0	6400.00	2700.00	1400.00
1M218E	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.40	2.00	1.10
1M914A	0.0	0.0	0.0	0.075	0.0	0.0	0.0	420.00	80.00	15.00
1M752A	5.700	40.000	0.0	0.0	0.0	0.0	0.0	2300.00	340.00	83.00
PC115	154.000	0.0	0.0	0.0	0.0	0.0	0.0	3300.00	1350.00	510.00
1N3026B5-JAN	18.000	2320.000	0.0	0.0	0.0	0.0	0.0	170000.00	53720.00	17000.00
1N3811	0.0	0.0	0.0	2.000	0.0	0.0	0.0	3000.00	3000.00	3000.00
1N3995A	4.700	0.0	0.0	0.0	0.0	0.0	0.0	262446.00	83000.00	26244.00
1N3016B	6.800	0.0	0.0	0.0	0.0	0.0	0.0	130000.00	41079.00	13000.00
1M4141	0.0	0.0	0.0	3.000	0.0	0.0	0.0	80000.00	25280.00	8000.00
1002	0.0	0.0	0.0	1.000	0.0	132.000	40.000	6700.00	2117.00	670.00
2N28571C(-B)	40.000	1.000	0.0	0.040	0.0	909.000	40.000	120.00	16.00	12.40
2N28571E(-B)	5.400	0.0	0.0	0.040	0.0	909.000	40.000	8.20	2.60	0.84
2N33751C(-B)	87.000	0.0	0.0	1.500	15.000	0.0	87.000	1800.00	1000.00	500.00
2N33751E(-B)	6.000	0.0	0.0	1.500	15.000	0.0	87.000	1300.00	440.00	230.00
2N14902JAN1C(-B)	120.000	0.0	0.0	6.000	2.400	0.0	120.000	7000.00	2300.00	700.00
2N14902JAN1E(-B)	14.000	0.0	0.0	6.000	2.400	0.0	120.000	13000.00	3808.00	1300.00
2N35841C(-B)	315.000	0.0	0.0	5.000	5.000	0.0	315.000	1200.00	370.00	120.00
2N35841E(-B)	9.100	0.0	0.0	5.000	5.000	0.0	315.000	10000.00	2150.00	490.00
2N28941C(-B)	36.000	0.0	0.0	0.200	0.0	500.000	36.000	170.00	50.00	14.00
2N28941E(-B)	6.400	0.0	0.0	0.200	0.0	500.000	36.000	30.00	19.00	12.00
2N58291C(-B)	30.000	0.800	0.0	0.030	0.0	909.000	30.000	47.00	17.00	6.00
2N58291E(-B)	3.000	0.0	0.0	0.030	0.0	909.000	30.000	10.00	10.00	4.30
2N3013JAN1C(-B)	40.000	5.000	0.0	0.200	0.0	500.000	40.000	100.00	21.00	4.30
2N3013JAN1E(-B)	5.000	0.0	0.0	0.200	0.0	500.000	40.000	52.00	31.50	20.00
CA30181C(-B)	53.000	0.580	0.0	0.050	0.0	200.000	53.000	64.00	20.00	5.80
CA30181E(-B)	7.100	0.0	0.460	0.050	0.0	200.000	53.000	22.00	10.00	4.00
2N1613JAN1C(-B)	123.000	0.0	0.0	0.500	0.0	222.000	123.000	3200.00	2100.00	1400.00
2N1613JAN1E(-B)	8.800	0.0	0.0	0.500	0.0	222.000	123.000	750.00	340.00	160.00
2N14852JAN1C(-B)	205.000	0.0	0.0	3.000	7.000	0.0	205.000	1700.00	1100.00	700.00
2N14852JAN1E(-B)	18.000	0.0	0.0	3.000	7.000	0.0	205.000	290000.00	30000.00	3100.00
2N34391C(-B)	575.000	0.0	0.0	1.000	36.000	0.0	575.000	78.00	27.00	10.00
2N34391E(-B)	9.400	0.0	0.0	1.000	36.000	0.0	575.000	2200.00	620.00	180.00
2N7062JAN1C(-B)	25.000	0.0	0.0	0.0	0.0	500.000	25.000	93.00	17.00	2.80
2N7062JAN1E(-B)	5.000	0.0	0.0	0.0	0.0	500.000	25.000	50.00	18.00	6.80

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2N28941E-B)	0.0	0.1313	0.0	0.0	0.3090
2N58291E-B)	0.0	0.1184	0.0	0.1963	0.0
2N58291E-B)	0.0	0.2229	0.0	0.0	0.3058
2N3013:JAN1E-B)	0.0	0.0912	0.2337	0.2185	0.0
2N3013:JAN1E-B)	0.0	0.1837	0.0	0.0	0.4323
2A30181E-B)	0.0	0.1587	0.0448	0.3406	0.0
2A30181E-B)	4.3243	0.3267	0.0	0.0	0.0519
2N1013:JAN1E-B)	0.0	2.7184	3.7253	4.2633	0.0
2N1013:JAN1E-B)	0.0	1.9870	0.0	0.0	2.4925
2N1013:JAN1E-B)	0.3695	0.5718	0.0	0.0	0.0
2N1485:JAN1E-B)	0.0	279.2483	0.0	228.1203	0.0
2N36391E-B)	0.1022	0.0728	0.0	0.0	0.0
2N36391E-B)	0.0	3.4632	0.0	5.3573	0.0
2N706:JAN1E-B)	0.0	0.0	0.1657	0.2169	0.0
2N706:JAN1E-B)	0.0	0.0	0.0	0.0	0.4157
1M2580	2.9173	0.0	0.0	0.0	0.0
1M7514:JAN	0.0	1.6703	0.0	0.0	0.0
1M4858:JAN	3.1721	2.2258	0.0	0.0	0.0
1M29918:JAN	0.0	3.6068	0.0	0.0	0.0
1M30258:JAN	0.0	10.6319	0.0	0.0	0.0
401054	0.0	0.0043	0.0	0.0	0.0
1M746A:JAN	0.0	6.5441	0.0	0.0	0.0
1M645:JAN	1.5848	0.5301	0.0	0.0	0.0
1M12028A:JAN	0.1524	0.0	0.0	0.0	0.0
1M1731A:JAN	8.2311	0.0	0.0	0.0	0.0

2N328A1E-B)	0.0	0.5765	0.3813	0.3013	0.0
2N328A1E-B)	0.4950	1.8913	0.0	0.0	0.8052
2N3351E-B)	0.0	1.7722	0.0	0.4107	0.0
2N3351E-B)	1.4284	8.3658	0.0	0.0	0.0
2N336:JAN1E-B)	0.0	0.0	1.6650	0.3164	0.0
2N24841E-B)	0.0	0.6141	0.0	0.0	12.7532
2N24841E-B)	3.0773	2.9519	0.0	0.3925	0.0
2N37361E-B)	0.0	0.0927	0.4803	0.1528	2.2284
2N37361E-B)	1.4465	0.7926	0.0	0.0	0.0
2N9301E-B)	0.0	0.7351	0.5812	0.4354	5.1785
2N9301E-B)	0.0	3.1767	0.0	0.0	1.5774
2N2481E-B)	0.0	0.0	0.1075	0.0303	0.0
2N2481E-B)	1.2343	0.0	0.0	0.0	1.0107
2N2907A1E-B)	0.0	0.1139	0.4685	0.2491	0.0
2N2907A1E-B)	1.0679	0.5485	0.0	0.0	2.4972
2N2222A1E-B)	0.0	0.1416	0.4685	0.4333	0.0
2N2222A1E-B)	1.3380	0.6672	0.0	0.0	2.0879
1M4384	0.0	0.0	0.0	0.0	0.0
F5911-3465	0.0	0.0	0.0	0.0	0.0
1M816	0.0	0.0	0.0	0.0	0.0
1M214E	0.0	0.0	0.0	0.0	0.0
1M914A	0.9229	0.3899	0.0	0.0	0.0
1M752A	0.0	0.3535	0.0	0.0	0.0
PC115	0.0	0.0	0.0	0.0	0.0
1M3026B:JAN	0.0	2.4421	0.0	0.0	0.0
1M3611	0.0	0.0	0.0	0.0	0.0
1M3995A	0.0	0.0	0.0	0.0	0.0
1M3016B	0.0	0.0	0.0	0.0	0.0
1M4141	0.0	0.0	0.0	0.0	0.0
1002	0.0	0.0	0.0	0.0	0.0
2N28571E-B)	0.0	0.1251	0.2847	0.2071	0.0

	2N2857(F-B)	0.0	0.1165	0.0	0.0	0.0	0.0	0.2023
	2N3375(C-B)	0.9819	1.1850	0.0	0.0	0.0	0.0	0.0
	2N3375(F-B)	0.0	1.1057	0.0	0.0	1.0474	0.0	0.0
	2N1490=JAN(C-B)	0.5020	1.3104	0.0	0.0	0.0	0.0	0.0
	2N1490=JAN(I-B)	0.0	5.6643	0.0	0.0	2.9865	0.0	0.0
	2N3584(C-B)	0.2140	0.3316	0.0	0.0	0.0	0.0	0.0
	2N3584(F-B)	0.0	2.7937	0.0	0.0	2.5288	0.0	0.0
	2N2894(C-B)	0.0	0.1362	0.0	0.3492	0.3146	0.0	0.0
	2N2894(F-B)	0.0	0.2631	0.0	0.0	0.0	0.0	0.6189
	2N5829(C-B)	0.0	0.1354	0.0	0.2577	0.2245	0.0	0.0
	2N5829(F-B)	0.0	0.3205	0.0	0.0	0.0	0.0	0.4396
	2N3013=JAN(C-B)	0.0	0.0606	0.0	0.1552	0.1451	0.0	0.0
	2N3013=JAN(I-B)	0.0	0.3520	0.0	0.0	0.0	0.0	0.4822
	CA3018(C-B)	0.0	0.1568	0.0	0.0443	0.3365	0.0	0.0
	CA3018(F-B)	6.2214	0.4696	0.0	0.0	0.0	0.0	0.0
	2N1613=JAN(C-B)	0.0	5.6372	7.7308	0.0	8.8474	0.0	0.0747
	2N1613=JAN(I-B)	0.0	2.8485	0.0	0.0	0.0	0.0	0.0
	2N1485=JAN(C-B)	0.7561	1.1699	0.0	0.0	0.0	0.0	3.5732
	2N1485=JAN(I-B)	0.0	91.3512	0.0	0.0	76.6255	0.0	0.0
	2N3439(C-B)	0.1119	0.0797	0.0	0.0	0.0	0.0	0.0
	2N3439(F-B)	0.0	3.0864	0.0	0.0	4.7743	0.0	0.0
	2N7062=JAN(C-B)	0.0	0.0	0.0958	0.0	0.0971	0.0	0.0
	2N7062=JAN(F-B)	0.0	0.0	0.0	0.0	0.0	0.0	0.4732
	1W2580	2.9152	0.0	0.0	0.0	0.0	0.0	0.0
	1W751A=JAN	0.0	0.5178	0.0	0.0	0.0	0.0	0.0
	1W485B=JAN	2.1818	1.5309	0.0	0.0	0.0	0.0	0.0
	1W2918=JAN	0.0	3.6042	0.0	0.0	0.0	0.0	0.0
	1W3025B=JAN	0.0	3.3621	0.0	0.0	0.0	0.0	0.0
	M01054	0.0	0.0104	0.0	0.0	0.0	0.0	0.0
	1W748A=JAN	0.0	2.6911	0.0	0.0	0.0	0.0	0.0
	1W645C=JAN	1.7887	0.5983	0.0	0.0	0.0	0.0	0.0
	1W1202RA=JAN	0.0535	0.0	0.0	0.0	0.0	0.0	0.0
	1W1731A=JAN	9.1330	0.0	0.0	0.0	0.0	0.0	0.0
	2N328A(C-B)	0.0	0.7011	0.4637	0.0	0.3665	0.0	0.0
	2N328A(F-B)	0.6906	3.3641	0.0	0.0	0.0	0.0	1.4324
	2N333(C-B)	0.0	1.4011	0.0	0.0	0.3247	0.0	0.0
	2N333(F-B)	2.0532	12.0251	0.0	0.0	0.0	0.0	0.0
	2N336=JAN(C-B)	0.0	0.0	2.2565	0.0	0.4288	0.0	0.0
	2N336=JAN(I-B)	3.1326	0.0	0.0	0.0	0.0	0.0	25.2057
	2N2484(C-B)	0.0	1.7731	1.9242	0.0	1.1331	0.0	0.0
	2N2484(F-B)	3.0431	2.9171	0.0	0.0	0.0	0.0	2.2021
	2N3736(C-B)	0.0	0.1791	0.9281	0.0	0.2952	0.0	0.0
	2N3736(F-B)	1.9731	1.0811	0.0	0.0	0.0	0.0	7.0640
	2N930(C-B)	0.0	0.9424	0.7451	0.0	0.5582	0.0	0.0
	2N930(F-B)	0.0	2.6788	0.0	0.0	0.0	0.0	1.3302
	2N2481(C-B)	0.0	0.0	0.3398	0.0	0.0958	0.0	0.0
	2N2481(F-B)	2.3419	0.0	0.0	0.0	0.0	0.0	1.9177
	2N2907A(C-B)	0.0	0.1359	0.5591	0.0	0.2972	0.0	0.0
	2N2907A(F-B)	2.2947	1.1785	0.0	0.0	0.0	0.0	5.2658
	2N2222A(C-B)	0.0	0.1924	0.5577	0.0	0.5159	0.0	1.9563
	2N2222A(F-B)	1.2536	0.6251	0.0	0.0	0.0	0.0	0.0
	1W6364	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	5S911-3465	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1W816	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1M216	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	1W915A	0.5672	0.2312	0.0	0.0	0.0	0.0	0.0
	1W752A	0.0	0.2729	0.0	0.0	0.0	0.0	0.0

[illegible]

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 3.23 44.44 3.23 42.86 3.18 41.27 3.16 39.68 3.08 38.10

APPENDIX A

RATIO OF EXPERIMENTAL AND PREDICTED POWER TO DAMAGE VS PERCENTAGE CONFIDENCE LEVEL FOR AVERAGE VALUE OF FIVE PRIORITY MODELS

2.99	36.51	2.99	34.92	2.97	33.33	2.96	31.75	2.94	30.16
2.82	28.57	2.73	26.98	2.55	25.40	2.53	23.81	2.43	22.22
2.33	20.63	2.31	19.05	2.30	17.46	2.05	15.87	2.04	14.29
1.97	12.70	1.94	11.11	1.82	9.52	1.79	7.94	1.73	6.35
1.13	4.76	1.05	3.17	1.02	1.59	0.0	0.0		
25.21	100.00	22.51	97.78	19.25	95.56	13.39	93.33	12.75	91.11
10.59	88.89	7.06	86.67	5.37	84.44	5.32	82.22	5.16	80.00
4.96	77.78	4.94	75.56	4.84	73.33	3.79	71.11	3.57	68.89
3.27	66.67	3.24	64.44	2.50	62.22	2.49	60.00	2.41	57.78
2.35	55.56	2.31	53.33	2.27	51.11	2.23	48.89	2.20	46.67
2.11	44.44	2.09	42.22	2.09	40.00	1.96	37.78	1.94	35.56
1.92	33.33	1.91	31.11	1.77	28.89	1.77	26.67	1.67	24.44
1.66	22.22	1.62	20.00	1.58	17.78	1.43	15.56	1.33	13.33
1.24	11.11	1.24	8.89	1.21	6.67	1.11	4.44	1.01	2.22
0.0	0.0								
253.68	100.00	231.38	99.39	96.10	98.79	82.99	98.18	66.88	97.58
59.05	96.97	40.72	96.36	27.12	95.76	21.15	95.15	19.91	94.55
18.67	93.94	15.61	93.33	15.37	92.73	14.17	92.12	12.81	91.52
12.65	90.91	11.76	90.30	11.61	89.70	11.55	89.09	10.74	88.48
10.65	87.88	10.63	87.27	10.57	86.67	10.37	86.06	9.95	85.45
9.17	84.85	9.13	84.24	8.88	83.64	8.23	83.03	7.41	82.42
7.25	81.82	7.17	81.21	7.04	80.61	6.78	80.00	6.76	79.39
6.71	78.79	6.69	78.18	6.62	77.58	6.61	76.97	6.56	76.36
6.34	75.76	6.27	75.15	6.36	74.55	6.18	73.94	6.00	73.33
5.39	72.73	5.51	72.12	5.44	71.52	5.42	70.91	5.24	70.30
5.04	69.70	4.98	69.09	4.90	68.48	4.78	67.88	4.70	67.27
4.68	66.67	4.68	66.06	4.46	65.45	4.41	64.85	4.33	64.24
4.33	63.64	4.17	63.03	4.15	62.42	3.93	61.82	3.91	61.21
3.88	60.61	3.88	60.00	3.80	59.39	3.71	58.79	3.71	58.18
3.66	57.58	3.61	56.97	3.61	56.36	3.61	55.76	3.60	55.15
3.57	54.55	3.54	53.94	3.52	53.33	3.37	52.73	3.36	52.12
4.35	51.52	3.25	50.91	3.21	50.30	3.08	49.70	3.01	49.09
2.98	48.46	2.95	47.88	2.92	47.27	2.92	46.67	2.92	46.06
2.90	45.45	2.88	44.85	2.83	44.24	2.79	43.64	2.75	43.03
2.72	42.42	2.71	41.82	2.70	41.21	2.70	40.61	2.69	40.00
2.66	39.39	2.63	38.79	2.56	38.18	2.44	37.58	2.44	36.97
2.44	36.36	2.43	35.76	2.41	35.15	2.41	34.55	2.38	33.94
2.33	33.33	2.30	32.73	2.29	32.12	2.24	31.52	2.24	30.91
2.23	30.30	2.22	29.70	2.21	29.09	2.19	28.48	2.13	27.88
2.11	27.27	2.10	26.67	2.10	26.06	2.08	25.45	2.02	24.85
2.00	24.24	1.98	23.64	1.98	23.03	1.94	22.42	1.93	21.82
1.92	21.21	1.89	20.61	1.86	20.00	1.82	19.39	1.80	18.79
1.79	18.18	1.76	17.58	1.77	16.97	1.74	16.36	1.73	15.76
1.72	15.15	1.71	14.55	1.67	13.94	1.67	13.33	1.67	12.73
1.65	12.12	1.64	11.52	1.64	10.91	1.61	10.30	1.61	9.70
1.60	9.09	1.60	8.48	1.57	7.88	1.54	7.27	1.54	6.67

1.90	6.06	1.35	5.45	1.32	4.85	1.25	4.24	1.12	3.64
1.11	3.03	1.10	2.42	1.08	1.82	1.06	1.21	1.03	0.61
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