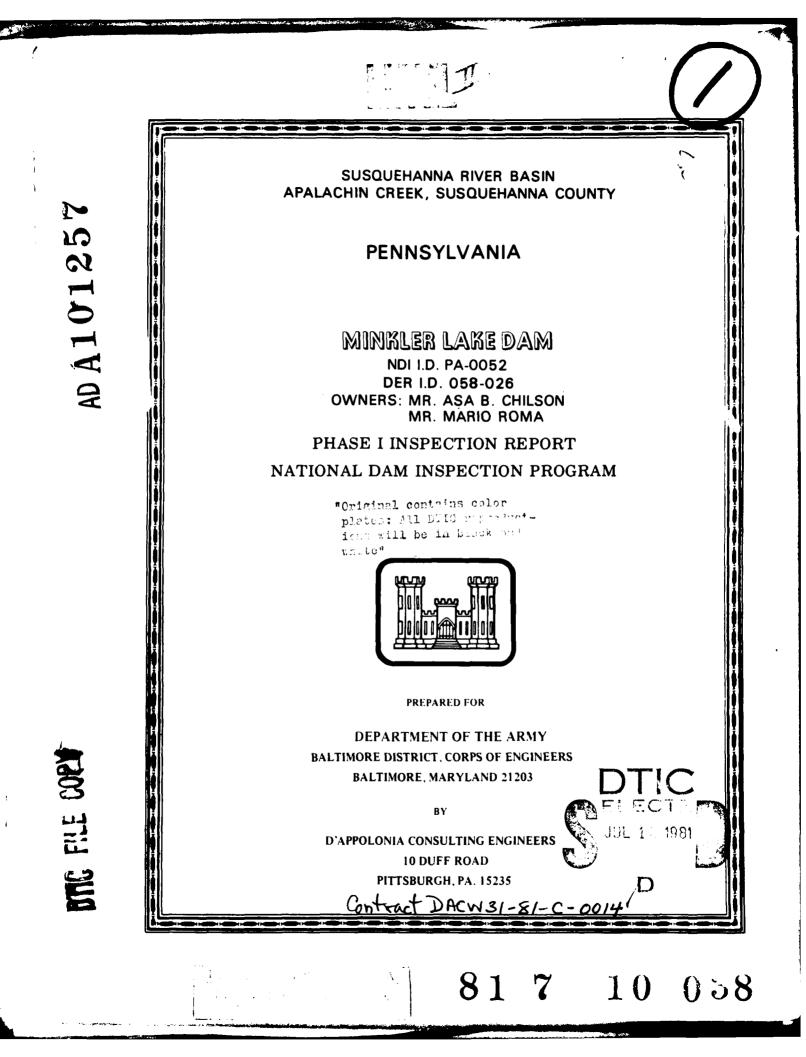
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PREFACE

This report is prepared under guidance contained in the <u>Recommended</u> <u>Guidelines for Safety Inspection of Dams</u>, for Phase I Investigations. Copies of these guidelines may be obtained from the Department of the Army, Office of Chief of Engineers, Washington, D.C. 20314.

The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon visual observations and review of available data. Detailed investigations and analyses involving topographic mapping, subsurface investigations, material testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the inspection is intended to identify any need for such studies which should be performed by the owner.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of the dam depends on numerous and constantly changing internal and external factors which are evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The assessment of the conditions and recommendations was made by the consulting engineer in accordance with generally and currently accepted engineering principles and practices.

PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

NAME OF DAM: Minkler Lake Dam STATE LOCATED: Pennsylvania COUNTY LOCATED: Susquehanna STREAM: Apalachin Creek SIZE CLASSIFICATION: Small HAZARD CLASSIFICATION: Significant OWNER: Mr. Mario Roma and Mr. Asa B. Chilson DATE OF INSPECTION: March 24, 1981 and April 30, 1981 Accession For NTIS GRA&I DTIC TAB Unannounced Justification By R DIIC Form 50 Distribution/on file Availability Codes Avail and/or Dist Special A

ASSESSMENT: Based on the evaluation of existing conditions, the condition of Minkler Lake Dam is considered to be poor. This dam appears to be essentially abandoned and is not being maintained. Upstream and downstream faces are covered with thick brush and trees. The upstream face of the dam lacks erosion protection and significant shoreline erosion exists at various sections along the upstream face. Operating equipment for the low level outlet pipe has collapsed and is not functional. Concrete in the spillway wing walls have deteriorated, requiring repairs.

The spillway capacity was evaluated according to recommended friteria and and found to be inadequate. According to the recommended criteria, small dams in the significant hazard category are required to pass from the 100-year flood to one-half the Probable Maximum Flood (PMF). In view of the potential downstream damage, one-half PMF was selected as the spillway design flood. The flood discharge capacity was evaluated according to the recommended procedure and was found to pass the 100-year flood and 30 percent of the PMF without overtopping the dam. Because the flood discharge capacity of the dam is less than the spillway design flood of 50 percent of the PMF, the spillway is classified to be inadequate.

The following recommendations should be implemented as soon as possible or on a continuing basis.

- 1. Trees and brush should be removed from the dam and erosion protection should be provided on the upstream face. The crest of the dam should be surveyed and low areas should be filled to design elevation.
- The low level outlet facilities should be repaired and restored.



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Assessment - Minkler Lake Dam

- 3. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- 4. The owner should develop a formal operating and maintenance plan for the dam, inspect the dam regularly and perform necessary maintenance.

Lawrence D. Andersen P.E. Vice President Approved by: 1981 1. forps of ingineers. Commander and the first star as a second 17 Jun 188; National Dam Inspection Program. Minkler Lake Dam (NDI I.D. PA-ØØ52 DER I.D. Ø58-Ø26), Susquehanna River Basin, Apalachin Creek, Susquehanna County, Pennsylvania. Phase I Inspection Report, ii: - 171 411001

MINK	CLER	LAKE	DAM
NDI	I.D.	PA-C	052
DER	1.D.	058-	-026
MAF	RCH 2	4, 19	981



Overview

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM MINKLER LAKE DAM NDI 1.D. PA-0052 DER I.D. 058-026

SECTION 1 PROJECT INFORMATION

1.1 General

<u>Authority</u>. The inspection was performed pursuant to the authority granted by The National Dam Inspection Act, Public Law
92-367, to the Secretary of the Army, through the Corps of Engineers, to conduct inspections of dams throughout the United States.

b. <u>Purpose</u>. The purpose of this inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project

a. Dam and Appurtenances. Minkler Lake Dam consists of a concrete ogee-type gravity spillway structure flanked by earth embankments on each side. The dam is approximately 600 feet long with a maximum height of 11 feet from the downstream toe and a crest width of 6 to 8 feet. The upstream face generally has a 1 horizontal to 1 vertical slope, but is locally steeper at various sections due to shoreline erosion. The downstream slope is about 2 horizontal to 1 vertical. The upstream face, crest and downstream face are covered with brush and large trees. The flood discharge facilities for the dam consist of an overflow spillway located near the left abutment (looking downstream). The spillway is a 65-foot-wide ogee-type concrete overflow section. The spillway discharges into a plunge pool at the toe of the dam, which in turn discharges into the natural streambed. The outlet facilities consist of a 24-inch-diameter corrugated metal pipe extending through the embankment to the left of the spillway. The flow through the outlet pipe is controlled by a gate at the upstream end of the pipe. This outlet facility constitutes the emergency drawdown system for the reservoir.

b. Location. Minkler Lake Dam is located across Apalachin Creek, two miles upstream from the central part of Apalachin Township, Susquehanna County, Pennsylvania (N41° 57.7', W76° 06.1°). Plate 1 illustrates the location of the dam.

c. <u>Size Classification</u>. Small (based on 11-foot height and 568 acre-feet storage capacity).

d. <u>Hazard Classification</u>. The dam is classified to be in the significant hazard category. Downstream from the dam, Apalachin Creek

flows through a wide floodplain for about two miles, then flows under a highway bridge on State Route 858 in Little Meadows. All structures located on the floodplain along this reach are approximately 10 feet or more above the streambed. It is estimated that a failure of this dam might damage State Route 858 and cause property damage in Little Meadows. Loss of a few lives is considered possible in this area.

e. Ownership. Mr. Mario Roma, 325 Sky Island Drive, Endicott, New York 13760 and Mr. Asa B. Chilson, 3001 Wayne Street, Endwell, New York 13760.

f. Purpose of Dam. Recreation.

g. Design and Construction History. The dam was designed by Mr. C. P. Allen of Tunkhannock, Pennsylvania, and constructed by the owner, with completion in 1952. The remains of an old earth dam existing at the same location was incorporated into the 1952 construction.

h. <u>Normal Operating Procedure</u>. The reservoir is normally maintained at the spillway crest level (Elevation 1150, USGS Datum), leaving 4.3 feet of freeboard to a low area at the top of the dam at Elevation 1154.3. All inflow occurring when the reservoir level is at the spillway crest elevation or above is discharged over the uncontrolled spillway.

1.3 Pertinent Data. Elevations referred to in this and subsequent sections of the report were calculated based on field measurements, assuming the crest of the spillway to be at Elevation 1150 (USGS Datum), which is the elevation interpolated as the normal pool elevation from the USGS 7.5-minute Friendsville quadrangle.

a. Drainage Area

3.3 square miles

Not applicable

Unknown

Unknown

2318

2318

b. Discharge at Dam Site (cfs)

Maximum known flood at dam site Outlet conduit at maximum pool Gated spillway capacity at maximum pool Ungated spillway capacity at maximum pool Total spillway capacity at maximum pool

c. Elevation (USGS Datum) (feet)

Top of dam.

Maximum pool Normal pool Upstream invert outlet works Downstream invert outlet works Maximum tailwater Toe of dam 1154.3 (low spot) 1156 (as designed) 1154.3 1150.0 Unknown 1143 Unknown 1143

d.	Reservoir Length (feet)	
	Normal pool level Maximum pool level	3200 4100
e.	Storage (acre-feet)	
	Normal pool level Maximum pool level	24 3 56 8
f.	Reservoir Surface (acres)	
	Normal pool level Maximum pool level	56.0 73.8
g٠	Dam	
	Туре	Earth embankment with concrete gravity spillway.
	Length	600 feet
	Height	ll feet 6 to 8 feet
	Top width Side slopes	Downstream:
	Side Bropes	2H: 1V;
		Upstream: Not determinable
	Zoning	No
	Impervious core	Unknown Unknown
	.Cutoff Grout curtain	No
	Grout curtain	-
ħ.	Regulating Outlet	
	Туре	24-inch-diameter corrugated metal pipe
	Length	73 <u>+</u> feet (measured from design drawings)
	Closure	24-inch gate valve
	Access	None Gate valve
	Regulating facilities	
i.	Spillway	
	Type	Ogee-type concrete structure
	length	65 feet (perpendi-
	Length	cular to flow)
	Crest elevation	1150.0 (low flow)
	Upstream channel	Lake
	Downstream channel	Earth channel

SECTION 2 DESIGN DATA

2.1 Design

a. <u>Data Available</u>. The available data consist of files provided by the Commonwealth of Pennsylvania, Department of Environmental Resources (PennDER), which contain design drawings, correspondence and inspection reports.

(1) <u>Hydrology and Hydraulics</u>. No original hydrology and hydraulic design data are available for the dam. A Commonwealth of Pennsylvania report entitled "Report Upon the Application of Mario Roma and Asa B. Chilson," dated February 14, 1951, contains the criteria used to size the spillway.

(2) <u>Embankment</u>. The available information consists of design drawings.

(3) <u>Appurtemant Structures</u>. The available information consists of design drawings.

b. Design Features

(1) Embankment. Plate 2 shows the location of the dam and the plan of the reservoir. As shown in Plate 3, the earth-fill sections of the dam were to be a homogeneous impervious fill. Material was to be placed in horizontal layers eight inches thick and well compacted. No internal drainage system was incorporated in the embankment design.

The embankment was designed to have a slope of 2 horizontal to 1 vertical both upstream and downstream.

(2) <u>Appurtemant Structures</u>. The appurtemant structures consist of the concrete ogee-type spillway and the outlet works. Details of the spillway are shown in Plates 3 and 4. The overflow section of the spillway is 65 feet wide. As shown in Plate 4, an earth fill was placed on the upstream side of the concrete spillway. The spillway foundation is shown to be founded on hardpan with a two-foot-wide wall three feet deep in the center of the foundation.

The outlet works consist of a 24-inch-diameter corrugated metal pipe encased in concrete. The upstream end of the pipe is equipped with a concrete intake structure. Flow through the pipe is controlled by a gate located at the upstream end of the pipe.

c. Design Data

(1) Hydrology and Hydraulics. A Commonwealth of Pennsylvania report entitled "Report Upon the Application of Mario Roma and Asa B. Chilson, dated February 15, 1951, indicates that the spillway was sized to pass a discharge of 2820 cfs with the water level at the designed top of the dam.

(2) Embankment. No engineering data are available on the design of the embankment.

(3) <u>Appurtement Structures</u>. No engineering data are available on the appurtement structures.

2.2 <u>Construction</u>. Very little information is available concerning construction of the dam. Two state memorandums concerning inspection of the dam during construction, dated December 7, 1951 and May 5, 1952, by W. W. Gruber, cite evidence of poor embankment construction. The embankment width was designed to be 10 feet, but field measurements indicate a width varying from 6 to 8 feet.

Available records indicate no major postconstruction work was performed other than repairs which were made to correct cracks and deterioration of the concrete in the spillway.

2.3 Operation. There are no formal operating records maintained for the dam.

2.4 Other Investigations. The available information indicated no investigations other than the periodic inspections conducted by the state. The last state inspection was conducted in 1965.

2.5 Evaluation

a. <u>Availability</u>. The available information was provided by the Commonwealth of Pennsylvania, Department of Environmental Resources.

b. Adequacy

(1) <u>Hydrology and Hydraulics</u>. The available information is limited. Only the watershed area and design discharge capacity of the spillway are reported.

(2) <u>Embankment</u>. Other than design drawings, no information is available to assess the adequacy of the design of the dam.

(3) <u>Appurtement Structures</u>. Review of the design drawings indicates that, as designed, no significant deficiencies exist that should affect the overall performance of the spillway.

SECTION 3 VISUAL INSPECTION

3.1 Findings

a. <u>General</u>. The onsite inspection of Minkler Lake Dam consisted of:

- 1. Visual inspection of the embankment, abutments, and embankment toe.
- 2. Visual examination of the spillway and its components, the downstream end of the outlet pipe, and the outlet works control structure.
- 3. Evaluation of downstream area hazard potential.

The specific observations are illustrated in Plate 5.

b. Embankment. The general inspection of the embankment consisted of searching for indications of structural distress, such as cracks, subsidence, bulging, wet areas, seeps and boils, and observing general maintenance conditions, vegetative cover, erosion, and other surficial features.

In general, the condition of the embankment is considered to be poor. The upstream area, crest and downstream face are covered with brush and large trees. The upstream face lacks erosion protection and significant shoreline erosion exists at various locations. At some sections the upstream slope is essentially vertical.

The top of the dam was surveyed relative to the spillway crest elevation and was found to have some vertical irregularities. While the design freeboard for the dam was six feet, the field survey indicated a freeboard of 4.3 feet between the low spot of the embankment and the spillway crest. Plate 6 shows the dam crest profile.

c. <u>Appurtemant Structures</u>. The appurtemant structures were examined for deterioration or other signs of distress and obstructions that would limit flow. In general, the structures were found to be in fair condition. While the concrete surfaces on the spillway wing walls have deteriorated, the concrete in the overflow is in fair condition. The outlet pipe gate hoist structure has collapsed and is not functional.

d. <u>Reservoir Area</u>. A map review indicates that the watershed is predominantly wood and swamplands. A review of the regional geology is included in Appendix G.

e. <u>Downstream Channel</u>. Below the dam, the stream flows through a wide valley for about two miles where it flows under a highway. Further description of the downstream conditions is included in Section 1.2 d.

3.2 Evaluation. In view of significant shoreline erosion along the upstream face and due to the presence of thick brush and large trees on the upstream area, crest and downstream face of the dam, the condition of the dam is considered to be poor, requiring repair and restoration. The outlet pipe gate operating equipment has collapsed, also requiring repair and restoration.

SECTION 4 OPERATIONAL FEATURES

4.1 <u>Procedure</u>. There are no formal operating procedures for the dam. The reservoir is normally maintained at the spillway crest level with excess inflow discharging through the uncontrolled spillway.

4.2 <u>Maintenance of the Dam</u>. The maintenance condition of the dam is considered to be poor. It appears that no attempts have been made to clear the brush and trees from the embankment. It also appears that no attempts have been made to alleviate shoreline erosion problems along the upstream face of the embankment or to repair the concrete deterioration on the spillway wing walls.

4.3 <u>Maintenance of Operating Facilities</u>. The only operating facility for the dam is the 24-inch sluice gate value on the outlet pipe. The operating equipment has collapsed and is not functional.

4.4 <u>Warning System</u>. No formal warning system exists for the dam. Telephone communication facilities are available via residences near the dam site.

4.5 Evaluation. The maintenance condition of the dam and the operating facilities are considered to be poor. It appears that no attempts have been made to maintain the dam or the operating equipment. Restoration of the concrete in the spillway structures, clearing of brush and trees from the dam, correction of upstream erosion problems and evaluation of the operational condition of the outlet facilities are required.

SECTION 5 HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features

a. Design Data. Minkler Lake Dam has a watershed area of 3.3 square miles and impounds a reservoir with a surface area of 56.0 acres at normal pool level. Flood discharge facilities for the dam consist of a concrete ogee-type spillway structure. Based on the available head relative to the low spot on the right embankment, the capacity of the spillway is estimated to be 2318 cfs with no freeboard.

b. Experience Data. As previously stated, Minkler Lake Dam is classified as a small dam in the significant hazard category. Under the recommended criteria for evaluating emergency spillway discharge capacity, such impoundments are required to pass flows between the 100-year flood and one-half of the PMF. In view of the potential downstream damage, one-half PMF was selected as the spillway design flood.

The PMF inflow hydrograph for the reservoir was determined utilizing the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army, Corps of Engineers. The data used for the computer analysis are presented in Appendix D. As determined by the computer program, the one-half PMF inflow hydrograph has a peak of 3523 cfs. The 100-year flood peak was determined according to the recommended procedure and was found to be 2030 cfs. Computer input and a summary of computer output and 100-year flood calculations are included in Appendix D.

c. <u>Visual Observations</u>. On the date of inspection, no conditions were observed that would indicate that the spillway capacity would be significantly reduced in the event of a flood.

d. Overtopping Potential. The available spillway capacity was found to be sufficient to pass the peak of a 100-year flood. Various percentages of the PMF inflow were routed through the reservoir and it was found that the dam can pass 30 percent of the PMF without overtopping the dam. For 50 percent of the PMF, it was found that the low area on the right embankment would be overtopped for a duration of 2.8 hours with a maximum depth of 0.7 foot.

e. <u>Spillway Adequacy</u>. Because the spillway cannot pass the recommended spillway design flood of one-half PMF without overtopping the dam, the spillway is classified to be inadequate.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

(1) <u>Embankment</u>. As discussed in Section 3, significant shoreline erosion exists along the upstream face of the dam and the embankment is covered with brush and large trees. These conditions may affect the integrity of the embankment if not adequately corrected.

(2) <u>Apportenant Structures</u>. No signs of distress were noted that would affect the stability of the appurtenant structure at this time.

b. Design and Construction Data

(1) <u>Embankment</u>. The available design and construction information does not provide any quantitative data to aid in the 'assessment of stability. However, as previously noted, field observations did not reveal any signs of distress that would significantly affect the stability of the embankment at this time and none were reported in the past. Therefore, based on visual observations, the static stability of the embankment is considered to be adequate.

(2) <u>Appurtement Structures</u>. Other than design drawings, no design and construction data exist for the appurtement structures. Review of these drawings indicates that there are no apparent structural deficiencies that would significantly affect the performance of the appurtement structures.

c. Operating Records. None available.

d. <u>Postconstruction Changes</u>. It is reported that repairs were made to the training walls of the spillway. These modifications are not considered to affect the structural stability of the dam.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1, and based on visual observations, the static stability of the dam is considered to be adequate. Therefore, based on the recommended criteria for the evaluation of seismic stability of dams, the structure is presumed to present no hazard as a result of earthquakes.

SECTION 7

ASSESSMENT AND RECOMMENDATIONS/PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. Assessment. The visual observations indicate that Minkler Lake Dam is in poor condition. There is significant erosion along the upstream face due to wave action and lack of erosion protection and the dam is overgrown with brush and large trees. It is considered possible that the integrity of the dam may be significantly affected if these conditions are not corrected. The low level outlet facilities were found to be nonfunctional.

The spillway was evaluated according to the recommended procedure and was found to pass 30 percent of the PMF without overtopping the dam. This capacity is less than the spillway design flood of one-half PMF. Therefore, the flood discharge capacity is classified to be inadequate.

b. <u>Adequacy of Information</u>. The available information, in conjunction with visual observations, is considered to be sufficient to make a Phase I evaluation.

c. <u>Urgency</u>. The following recommendations should be implemented as soon as possible or on a continuing basis.

d. Necessity for Additional Investigations. None required.

7.2 Recommendations/Remedial Measures. It is recommended that:

- Trees and brush should be removed from the dam and erosion protection should be provided on the upstream face. The crest of the dam should be surveyed and low areas be filled to design elevation.
- 2. The low level outlet facilities should be repaired and restored.
- Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- 4. The owner should develop a formal operating and maintenance plan for the dam, inspect the dam regularly and perform necessary maintenance.

APPENDIX A

CHECKLIST VISUAL INSPECTION PHASE I

·	lyania ID# DER: 058-026 icant 35	TAILWATER AT TIME OF INSPECTION 1143 M.S.L.			RECORDER	
APPENDIX A CHECKLIST VISUAL INSPECTION PHASE I	COUNTY Susquehanna STATE Pennsylvania HAZARD CATEGORY Significant WEATHER Cloudy TEMPERATURE 35	1150M.S.L. EVIEW INSPECTION PERSON (April 30, 1981)	Lawrence D. Andersen James H. Poellot	Bilgin Frel	Bilgin Erel	Pake Al of 9
	NAME OF DAMMinkler Luke TYPE OF DAMEarth DATE(S) TNSPECTIONMarch_24, 1981	POOL ELEVATION AT TIME OF INSPECTION INSPECTION PEPSONNEL: R	Arthur Smith Wah-Tak Chan	Bilgin Erel		

					·		
	REMARKS OR RECOMMENDATIONS					Adequate shoreline erosion protection (e.g., riprap) should be provided along the upstream slope of the dam.	
VISUAL INSPECTION Phase I Embankment	OBSERVATIONS	None observed.	None observed.	None observed.	See Plate 6 for dam crest profile. No significant horizontal misalignment observed.	Upstream slope has no shoreline riprap protection.	Page A2 of 9
	VISUAL EXAMINATION OF	SURFACE CRACKS	UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOF	SLOUCHING OR EROSION OF Embankment and abutment Slopes	VERTICAL AND HORIZONTAL ALICNMENT OF THE CREST	RIPRAP FAILURES	

	REMARKS OR RECOMMENDATIONS					
VISUAL INSPECTION PHASE I FMRANKMENT	ORGERVATIONS	No problem observed.	None observed.	Suco	None	
	VISUAL EXAMINATION OF	JUNCTION OF EMBANKMENT AND ARUTMENT, SPILLWAY AND PAM	ANY NOTICEARLE SEEPAGE	STAFF CACF, AND RECORDER	541Vau	

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	ENDATIONS					k outlet be developed	
	REMARKS OR RECOMMENDATIONS					Means for operating outlet pipe valve should be developed	
PHASE 1 OUTLET WORKS	ORSERVATIONS	Name abserved.	Outlet pipe intake was submerged and not visible during inspection.	No structural problems observed.	Outlet channel was not defined and was partially blocked with debris.	According to the owner, flow through the outlet pipe is controlled by an upstream valve which is submerged and not operable.	Paper Ad of 9
	VISUAL EXAMINATION OF	CRACKING AND SFALLING DF CONCRFTE SURFACES IN OUTLUE CONDULT	INTAKE STRIVCTURE	MITLET STRINGTURE	NITLET CUANEL,	EMEPCENCY CATE	

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VISUAL INSPECTION PHASE I OUTLET WORKS

	REMARKS OR RECOMMENDATIONS					
VISHAL, INSPECTION PHASE I UNCATED SPILLMAY	ORGERVATIONS	Concrete spalling on spillway wing walls and crest.	Lake. No obstructions.	Earth channel with some riprap.	None	Page A5 of 9
	VISUAL EXAMINATION OF	CONCRETE WEIR	APPROACH CHANNEL	DISCHARGE CHANNEL	RRIN'E AND PLERS	

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I, INSPECTION	PRASE I	D SPILLWAY
VTSUAL TNSI	PRASE	GATED SPII
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		BENARYC OB BECOMMENDATIONC
VISUAL EXAMINATION OF		CNUTING AND CARACTER
CONCRETE STLL	The dam has no gated spillway.	
APPROACH CHANNEL	N/N	
DISCHARGE CHANNEL	<, ۲	
BRIDGE PIERS		
GATES AND OPERATION FOUTPMENT		

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N	AMINATION OF OR RECOMMENDATIONS REMARKS OR RECOMMENDATIONS	, The New York States and States	ON WELLS Now	Nun	Yana	Hone
	VISUAL EXAMINATION OF	MONIMENTATION/SURVEYS	ORSERVATION WELLS	5 d l i n	PTEZOMETEPS	nture

VISUAL INSPECTION

Page A7 of 9

				2011 T.	and the second party of the	
	REMARKS OR RECOMMENDATIONS					
VISUAL INSPECTION FUASE I RESERVOTR	SIND LAND SIND	No problom observed.	ไหหากพท	One beaver dam located approximately two miles downstream.		Parr AR of 9
	VISUAL EXAMINATION OF	SLOPFG	SFRIMENTATION	HPSTREAM RESERVOIRS		

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and the second second

		and also all				
	REMARKS OR RECOMMENDATIONS		•			
VISUAL INSPECTION Phase I Pownstream Channel	ORGERVATIONS	No problems observed.	No problems observed.	Little Meadows (approximately 20 persons) located two miles downstream.		Pape A9 of 9
	VISUAL EXAMINATION OF	CONDITION (OBSTRUCTIONS, DERRIS, ETC.)	STOPES	APPROXIMATE NIMBER OF HOMES AND POPULATION		

APPENDIX B

CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION AND HYDROLOGIC AND HYDRAULIC PHASE I

N: 250

	NAME OF DAM Minklet Lake IDM <u>NDI: PA-0052</u> DER: 058-026 DER: 058-026 defies.	CHECKLIST ENCINEFRING DATA DESIGN, CONSTRUCTION, OPERATION FILASE 1 The design drawings are available in state See Plate 1. Originally built prior to 1919, restorat See Plates 3 and 4.	ITFY AS-RUILT DRAWINGS AS-RUILT DRAWINGS REGIONAL VICINITY MAP REGIONAL VICINITY MAP CONSTRUCTION HISTORY TYPICAL SECTIONS OF DAM
		Plates 3 and	SECTIONS OF DAM
Originally built DAM See Plates 3 and		<u>م</u>	L VICINITY MAP
WYC			L VICINITY MAP
ξ	te files.	The design drawings are available in sta	r drawings
ξ		REMARKS	
REMARKS The design drawings are available in state files. See Plate 1. See Plate 1. Originally built prior to 1919, restoration completed in 1952. M See Plates 3 and 4.	NAME OF DAM MINKLET Lake ID# ND1: PA-0052 DFR: 058-026		

3 -

	CHECKLIST
	ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION FUASE I
ITEM	REMARKS
RAINFALL/RESERVOIR RECORDS	None available.
DESTCN REPORTS	None available.
GEOLOCY REPORTS	None available.
DESIGN COMPUTATIONS Hydrology & Hydraulics Dam Starility Seepage Studies	No computations available.
MATERIALS INVESTICATIONS Roring Records Laroratory Field	None available.
	Радс R2 of 5

CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PUAGE 1

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ITEN	REMARKS
POST CONSTRUCTION SURVEYS OF DAM	None availahie.
RORROW SOURCES	None available.
MONITORING SYSTEMS	None
MODIFICATIONS	Restoration of old dam and spillway in 1952.
HIGH POOL RECORDS	None recorded.
	Pape B3 of 5

CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PUASE I

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11134	REMARKS
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None available.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported.
MAINTENANCE OFERATION RECORDS	No maintenance records kept for the dam.
SPILIMAY PLAN Sections	See Plates 3 and 4.
DETAILS	
OPERATING EQUIPMENT Plans and details	See Plate 3.
	Parr R4 of 5

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CHECKLIST ENGINEERING DATA HYDROLOGIC AND HYDRAULIC

DRAINAGE AREA CHARACTERISTICS: 3.3 square miles (heavily wooded watershed) ELEVATION, TOP OF NORMAL POOL AND STORAGE CAPACITY: 1150 (243 acre-feet) ELEVATION, TOP OF FLOOD CONTROL POOL AND STORAGE CAPACITY: 1154.3 (568 acre-feet) ELEVATION, MAXIMUM DESIGN POOL: 1156.0 ELEVATION, TOP OF DAM: _____1154.3____ SPILLWAY: a. Elevation 1150[±] b. Type Oree concrete overflow section c. Width 65 feet (perpendicular to flow) d. Length 5 feet at base e. Location Spillover<u>Near_left_abutment</u> f. Number and Type of Gates None OUTLET WORKS: a. Type 24-inch corrugated metal pipe b. Location Near left abutment c. Entrance Inverts Unknown d. Exit Inverts 1143.0[±] e. Emergency Drawdown Facilities 24-inch corrugated metal pipe HYDROMETEOROLOGICAL GAGES: a. Type None b. Location None

c. Records None

MANIMUM NONDAMAGING DISCHARGE: Unknown

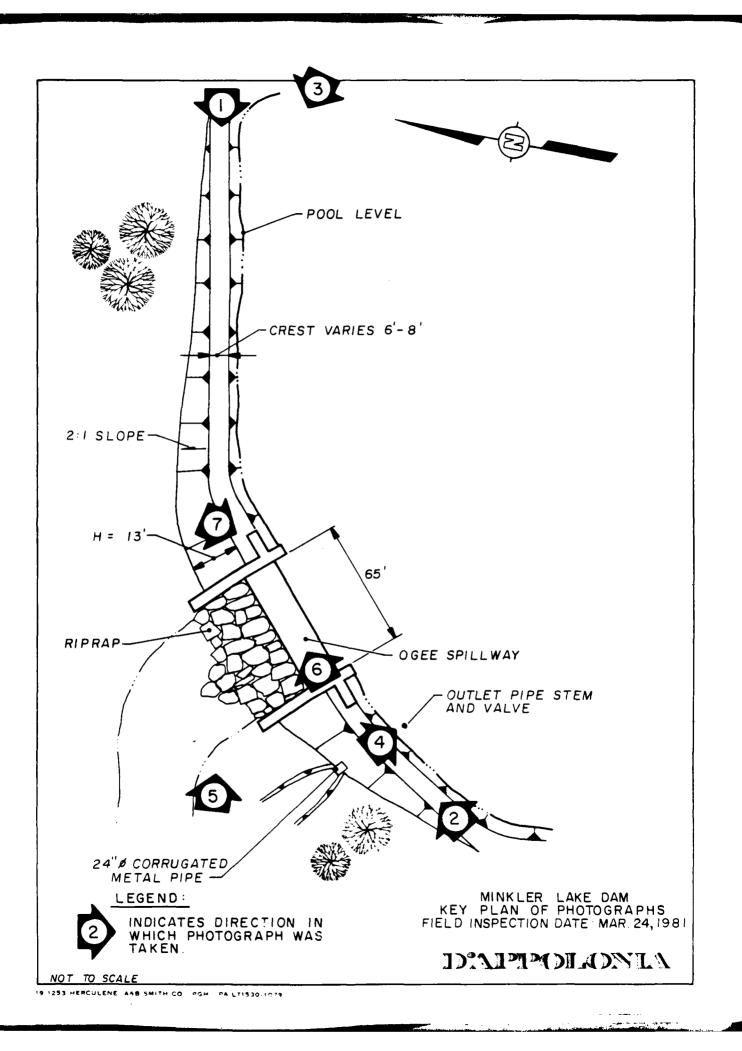
Page B5 of 5

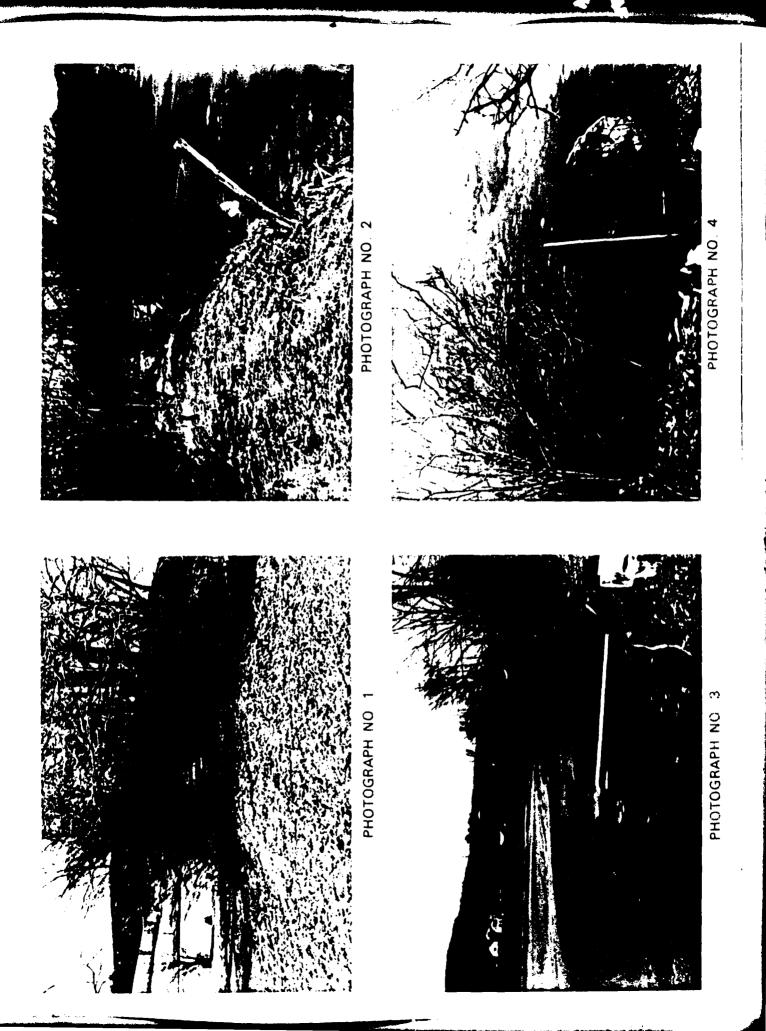
APPENDIX C

PHOTOGRAPHS

LIST OF PHOTOGRAPHS MINKLER LAKE DAM NDI I.D. NO. PA-0052 MARCH 24, 1981

PHOTOGRAPH NO.	DESCRIPTION
1	Dam crest (looking west).
2	Dam crest (looking north).
3	Upstream face.
4	Outlet pipe stem.
5	Ogee spillway (looking upstream).
6	Ogee spillway (right abutment).
7	Right abutment cutoff wall and dam crest low spot.
8	House and trailers along Apalachin Creek (approximately 0.8 míle downstream from dam).















PHOTOGRAPH NO 7

APPENDIX D

HYDROLOGY AND HYDRAULICS ANALYSES

MARE OF DAM. Minkler Lake Dam

di la

PROBABLE MAXIMUM PRECIPITATION (PMP) = 22.2 INCHES/24 HOURS

STATION	1	2	3	4	5
Station Description	Minkler Lake	Minkler Lake Dam			
Drainage Area (aquare milea)	3.3	-			
Gumulative Drainage Area (square miles)	3.3	3.3			
Adjustment of PMF for Drainage Area (2) ⁽¹⁾	952	-	1		
6 Hours	117	-			
12 Hours	127	-			
24 Hours	136	-			
48 Hours	142	- 1			
72 Hours	145	-	}		
Snyder Hydrograph Parameters			1		
Zone ⁽²⁾	11A	-			
Cp'Ct ⁽³⁾	0.62/1.50	-			
L (miles)(1)	3.13	l -			
L _{ca} (miles)(~)	1.08	-			
$t_p = C_t (L \cdot L_{ca})^{0.3}$ (hours)	2.16	-			
Spillway Data	1				
Crest Length (ft)	-	65.0	1 -		
Freeboard (fr)	-	4.3	1		Í
Discharge Coefficient	-	4.2	1		
Exponent	-	1.5			

(1)Hydrometeorological Report 40, U.S. Weather Bureau, 1965.

(2)Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients (C_p and C_t).

(3'Snyder's Coefficients.

(4) L = Length of longest water course from outlet to basin divide. L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.

STORAGE VS. ELEVATION

ELEVATION	AH, FEET	AREA (attes (1)	AVOLUME (acre-feet) ⁽¹⁾	Stühauf (acte-feet)
1:41 1	11. 1			040.5
1:5		51.0		262.7
117131	27.5	(con-	247.7	ç.n

(1) Planimetered from USGS maps.

(2) $AVclume = AH = 3 + A_1 + A_2 + \sqrt{A_1A_1}$

(3. Estimated lave bottom leve.

PAGE D2 OF 7

COMPUTER INPUT OVERTOPPING ANALYSIS

ANAL YSES PRUJECT NO 80-55 E MAXIMUH FLOOD(1 0 -4	00 ŀ	ER 56	-	0.0265			
VSES DECT NO XTMUN	7						
~~~~~~		AM, ([					۰.
ANAL PRUL C	0 40	DN OF SNYDER INFLOW HYDROGRAPH TO MINKLER LAKE DAM, (DER 58-26)		n 0			
PING (, PA 10BABL	ě.	ורבא ו	ъ.	<b>&gt;</b>	- (9)	0	90
UNUDER UNTT HYDROGRAPH. SPILLMAY AND DAM OVERTOPING ANALYSES MINNLER LAKE DAM. (DER 38-26).SUSGNUEHENNA COUNTY.PA. FRUJECT I COR 202.302.402.502.602.702.802.902.AND 1002 PROBABLE MAXIMU 0 0 0 0 0	08 O	MINK (	-	-	ROUTING FLOW THROUGH MINNLER LAKE DAM. (DER 38-261	-1150.0	009
WVI O	0 70	PH TC	142		, CDEF	I	500 0 155 6
AND AUEHE POX A		<b>ROGRA</b>			DAM		0611
B02.505	09 0	JUVH 1			I LAKE	-	400 0 155 0
5P IL 8-261 70%	0	NFL UL	~		NKL ER		
алрн. 01 г. 5 2, 602	0 20	DER I	127		IN HE		600 350 1155
DR06	0 <b>4</b> 0	OF SNVI	11	0	HROUG		onop
UNUDER UNTT HYDROGRAPH. SPILLUAY AND DAM HINKLER LAKE DAM. (DER 58-26). SUSGUEHENNA OR 202, 302, 402, 502, 602, 702, 802, 902, AND 1 0 15 0 0	0	NO NO		n¥	LOW		240-4
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PEAN FLOW AND STORAGE (FRD OF PERTON SUMMARY, FOR MULTIPEL PEAN RAFTU FCOMMATC CUMPUTATIONS FLOWS IN COULE FEET PERTOND COUNTCHER, PERTS FORD ANTA IN SQUARE MILLOMETERS)

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RATIO 6 70	04	1 (89, 461	4752
LINUS RATIO 5 60	4000		112 75) (
PL IT D TO F HATTO 4	E.791.	111 66	31115 90-181) (
KATUS API RATIO 3 40	6192	74 8214	2402 68 03)(
RATTO .	<b>11</b> .	99 (16) (	49, 99) (
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PLAN RATIC	-`	-	. ~
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OPERATION	HYDRUGHAPH AT	ROUTED 10	

FLOOD ROUTING SUMMARY PAGE D3 OF 7 1....

	FAILURE HUURS 0 00 0 00 0 00 0 00 0 00 0 00 0 00 0
0P UF DAM 1154 30 275 275	х х х х х х х х х х х х х х х х х х х
CREST 10P 00 0	000 100 100 100 100 100 100 100 100 100
5P ILL WAY CR 1150 00 0	001510 01510 1146 1146 1146 1146 1146 1146 1146 11
VAL UE 00 0	MA X 20 X 2
INITIAL 1150	MAX IMUM DIF PTH O 00 0 00 0 00 0 00 0 00 0 00 0 00 0 0
ELE VATTON 5101AGE 0011-100	HAXIMUM RESERVITE USE 69 1152 69 1155 69 1155 69 1155 89 1155 80 1156 29 1156 29
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

SUMMARY (IF DAM SAFETY ANALYSIS

PLAN 1

OVERTOPPING ANALYSIS PAGE D& OF 7

# IDAIPIPOILONIA

CONSULTING ENGINEERS, INC.

By MB __ Date 5/1/81 Subject __ MINKLER LAKE DAM Sheet No. __ of __ Chkd. By __ Date _____ Flood PEAK DISCHARGE _____ Proj. No. 80-556_

FLOOD PEAK DISCHARGE BY REGRESSION EQUATIONS

REFERENCE : HERBERT N.FLIPPO, JR. "FLODDS IN PENNSYLVANIA" WATER RESOURCES BULLETIN NO.13, K.S. DEPT. OF THE INTERIOR, GEOLOGICAL SURVEY, OCTOBER 1977

FROM PLATE 1 OF REFERENCE, MINKLER LAKE DAM IS LOCATED ON FLOOD - FREQUENCY "2", BASED ON THE RECORDS OF SO GAGING STATIONS WITH IN THIS REGION, THE FLOOD PEAK DISCHARGES, QT, AS CHOWN ON FIG 2 OF REFERENCE, ARE DETERMINED AS FOLLOWS

 $Q_T = C A^{\times}$ ; where A = WATERSHED AREA= 3.3 SQ.MI. X, C = RE GRESSION COEF.

FREQUENCY	REGRESS	$Q_{T}$		
T-YEAR	С	×	standard Error	efs
10	240	0.782	26%±	611
25	349	0.765	27%±	870
50	448	0.754	29%±	1102
100	564	0.744	31%±	1371

PAGE D5 OF 7

# IDAIPIPOLIDNIA

CONSULTING ENGINEERS, INC.

By MB Date 4/29/81 Subject MINKLER LAKE DAM Sheet No. 1 of 2 Chkd. By WIC Date 4/29/81 100 YR FLOOD PIEAK Proj. No. 80-556

100 YEAR FLOOD PEAK CALCULATION

REF 1: "HYDROLOGIC STUDY TROPICAL STORM AGNES", ARMY CORPS OF ENGINEERS, DEC., 1975

 $Los(P) = Los(Q_m) + K(P, s)s$ 

WHERE

- LOG (Qm) = MEAN LOG OF ANNUAL FLOOD PRAKS
- $Loc(Q_m) = C_m + 0.75 Loc(A)$ 
  - CM = A MAP LOEFFICIENT (FIG. ZI, RIEFI)

A = DRAINAGE AREA IN SQ. MILES

- K(P,G) = STANDARD DEVIATE FOR & GIVEN P AND SKEW COEFFICIENT G.
  - S = STANDARD DRUIATION  $S = C_S - 0.05 Log(A)$   $C_S = A MAP CORFRICIENT (FIG. 22, REF. 1)$ G = SKEW CORFRICIENT (FIG. 23, REF. 1)

PAGE D6 OF 7

# IDAIPIPOLONIA CONSULTING ENGINEERS INC By MB Date 4/20/81 Subject ______ MINKLER LAKE DAM Sheet No. 2 of 2 Chkd. By WTC Date 4/29/81 100 YR FLOOD PEAK Proj. No. 80-556 MINKLER LAKE DAM 100 YEAR FLOOD P=0.01 DRAINAGE AREA = 3.3 SQ MILES $C_{M} = 2.18$ $C_{S} = 0.37$ G = 0.26LOG QM = 2.18 + 0.75 LOG (3.3) = 2.57 S = 0.37 - 0.05 Log(3.3) = 0.34From RRF. 1, EXHIBIT 39 K(P, G) = K(0.01, 0.26) = 2.515 $L_{CG} Q_{0.01} = 2.57 + 2.515(0.34)$ = 3.43 $Q_{100YR} = 10^{3.93} = 2690 CFS$ PER CORPS OF ENGINEER MILMO, DATED 4/22/81, THE ADDATED 100 YEAR FLOOD FRAK IS THE AUERAGE OF

METHODS A AND B

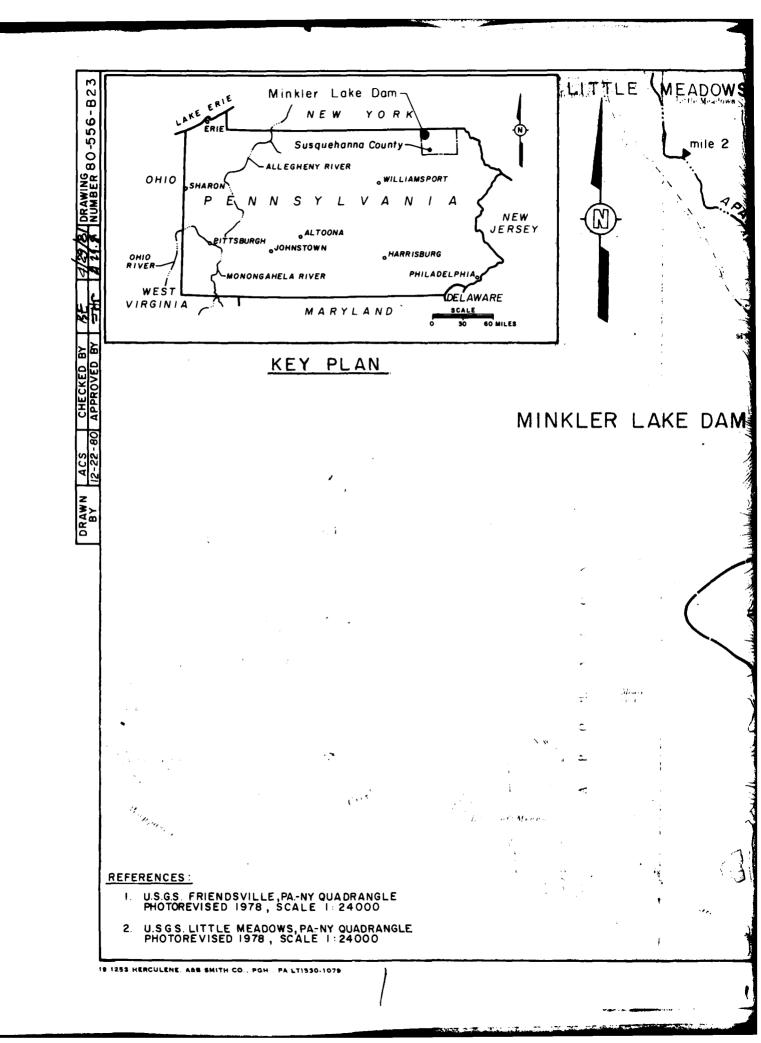
$$Q_{100} = \frac{-690 + 1371}{z}$$
  
= 2030 CFS

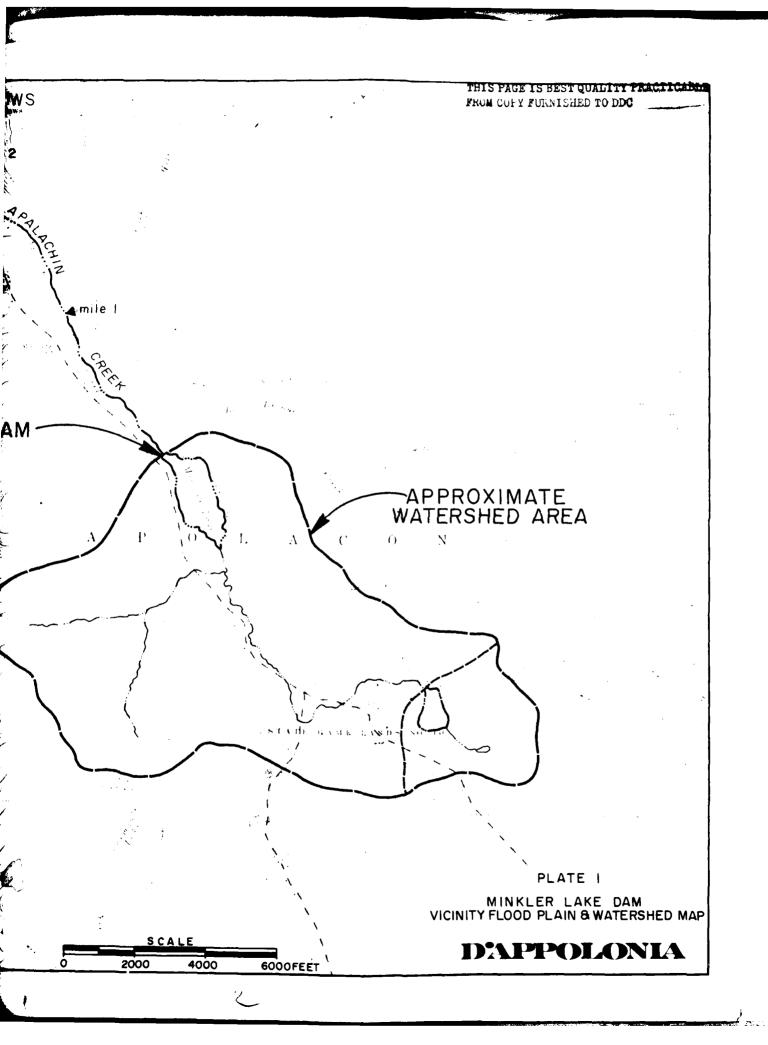
#### PAGE D7 OF 7

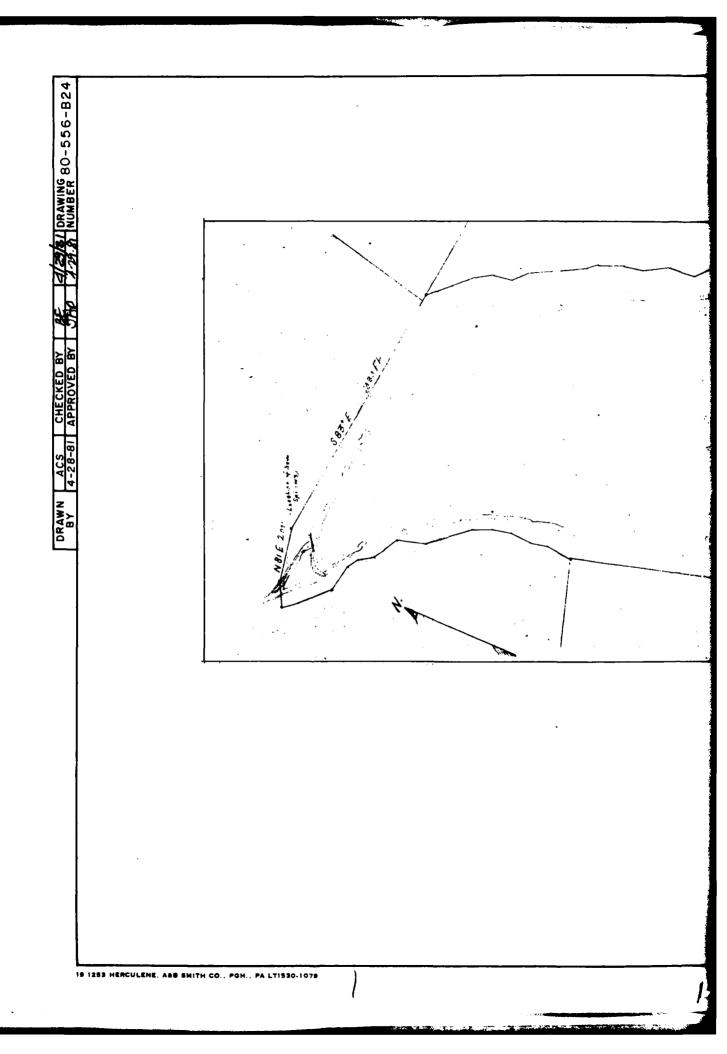
#### APPENDIX E

### PLATES

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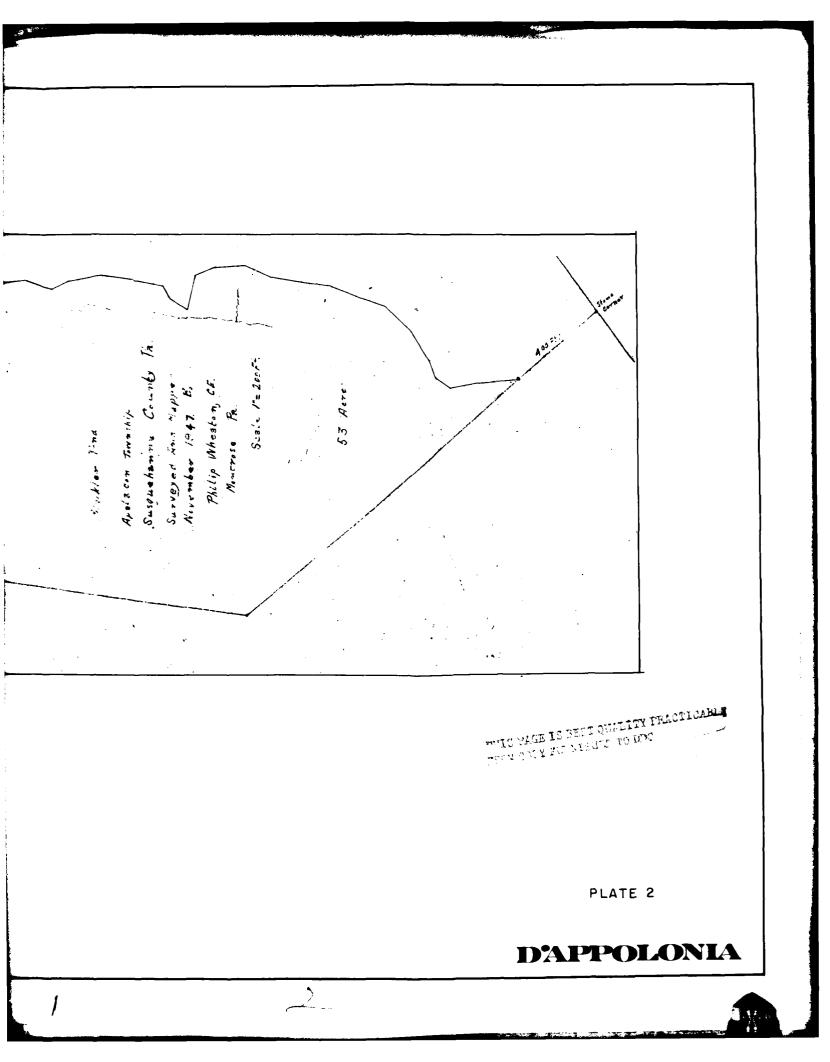


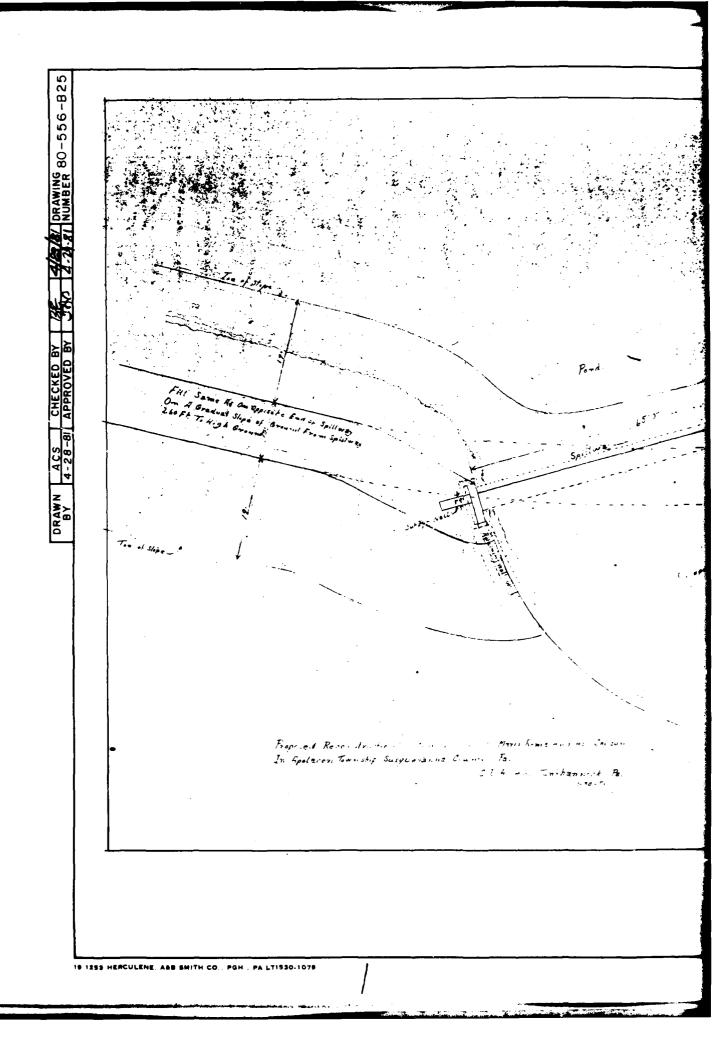


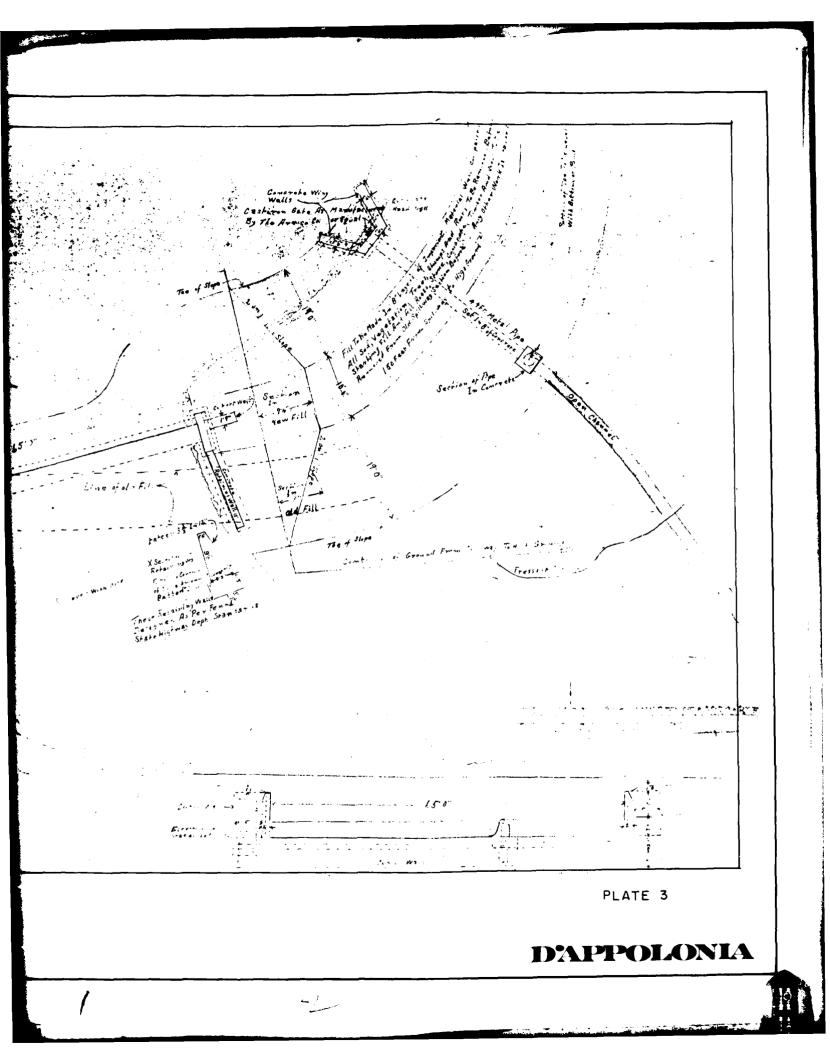
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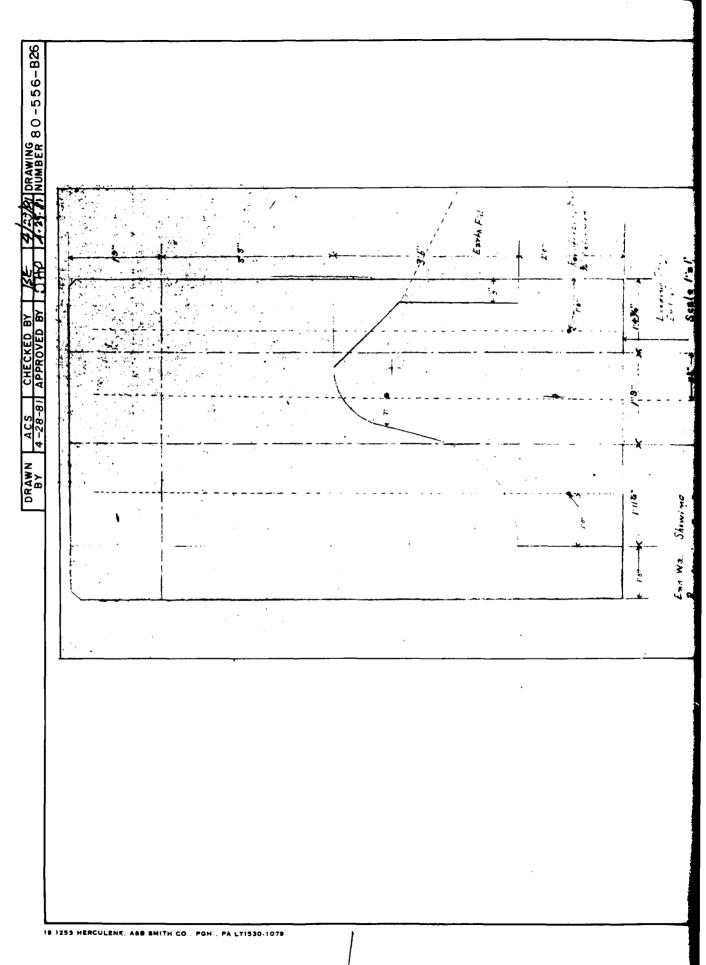
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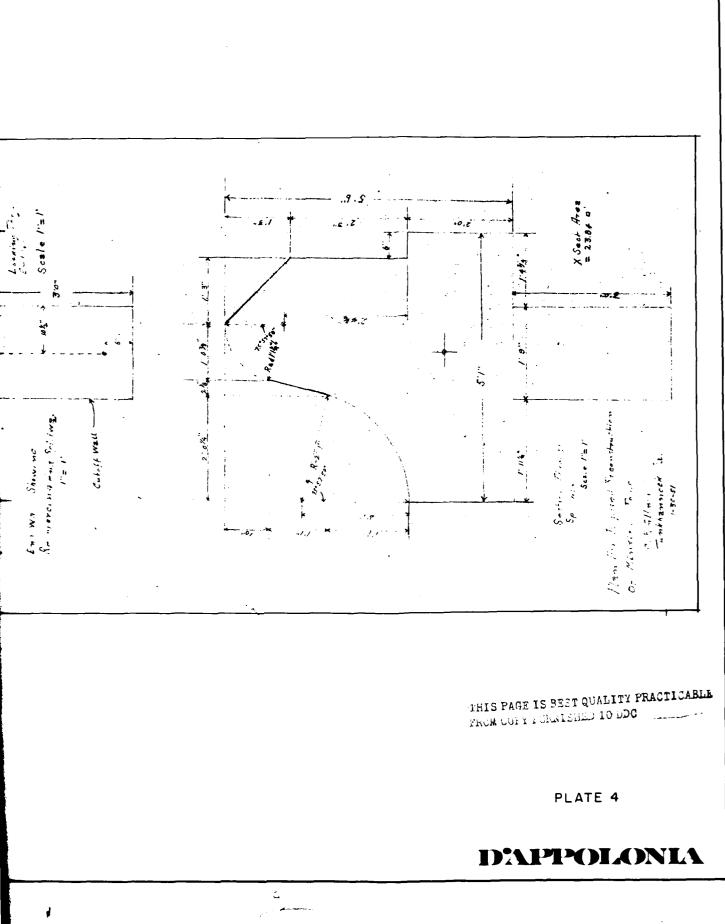
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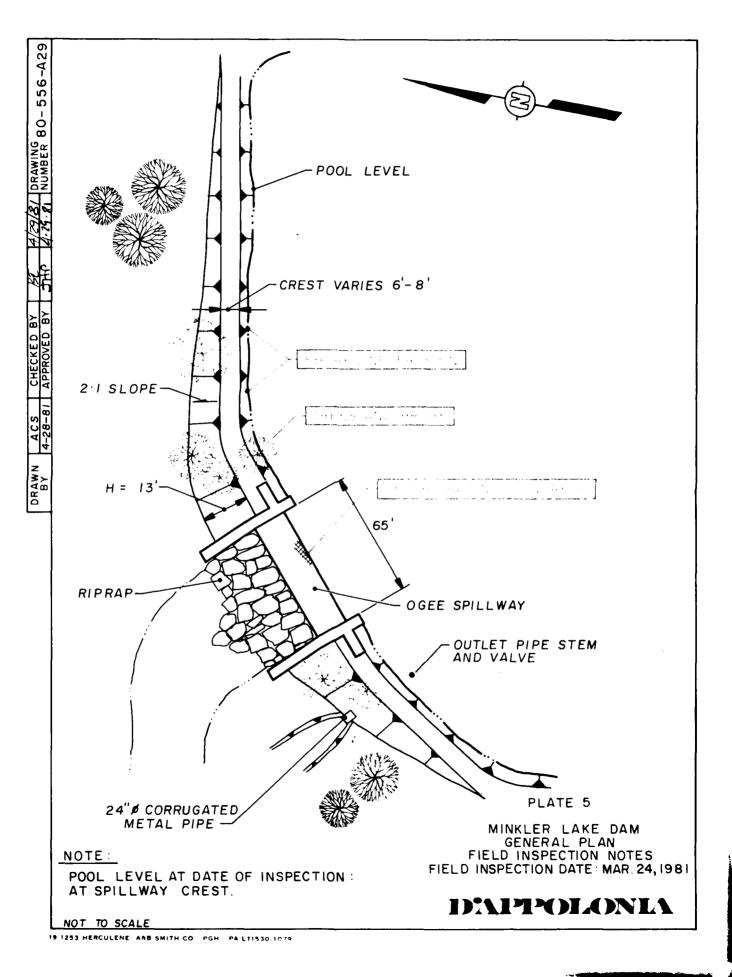






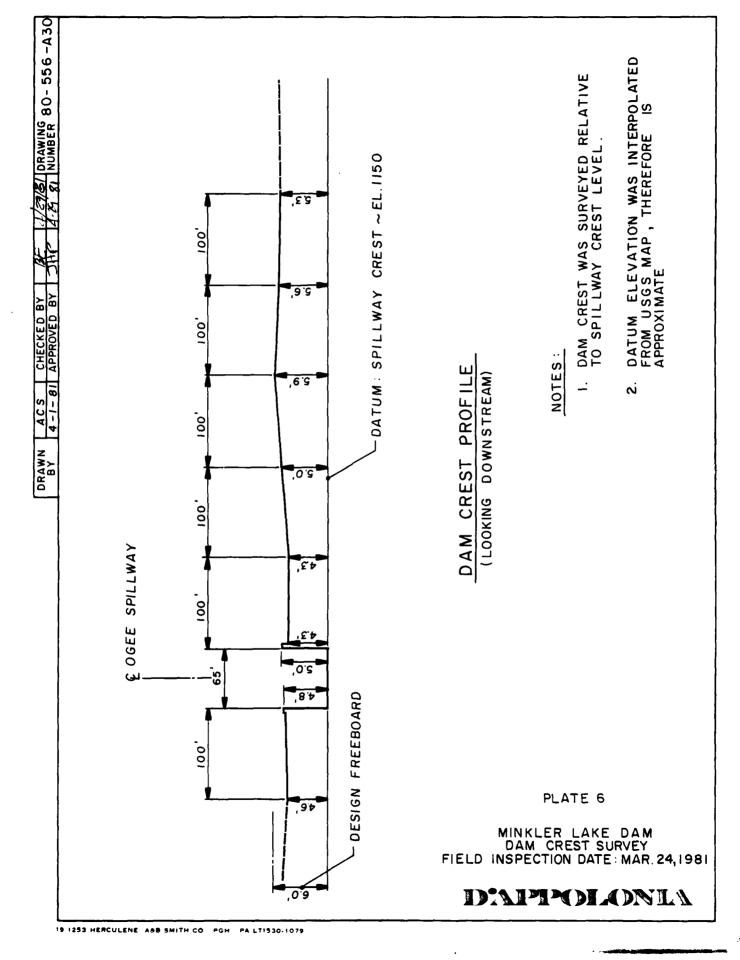






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A DESCRIPTION OF THE OWNER OF THE

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## APPENDIX F

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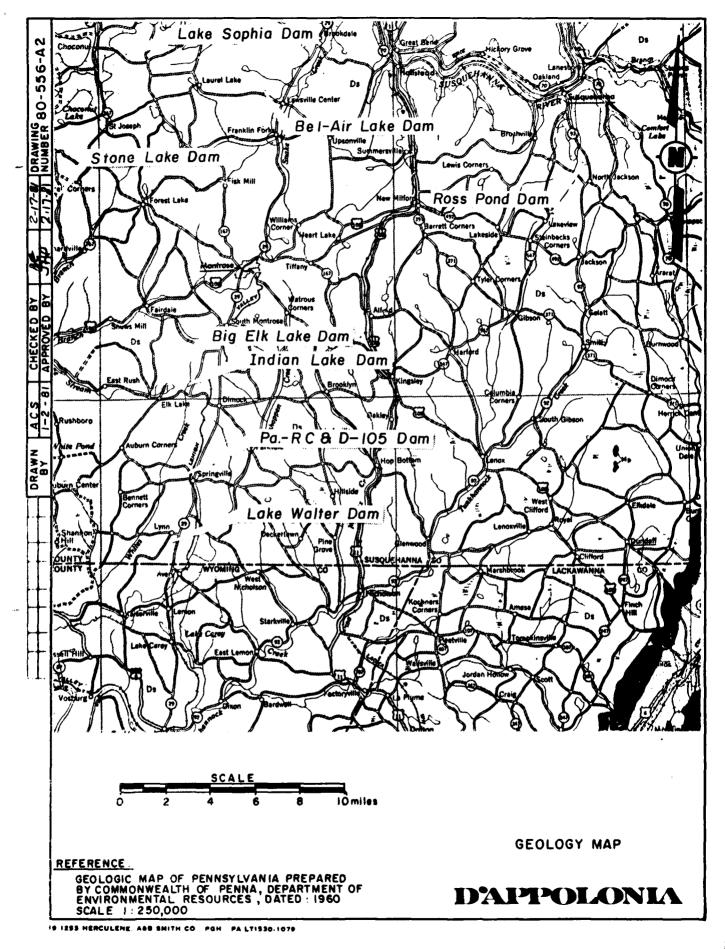
#### REGIONAL GEOLOGY

#### REGIONAL GEOLOGY MINKLER LAKE DAM

The Minkler Lake Dam is located in the glaciated low plateaus section of the Appalachian Plateau physiographic province, characterized as a mature glaciated plateau of moderate relief.

The geologic structure consists of a series of northeast trending folds (approximately N70°E) which plunge gently to the southwest. The dip of the limbs of the folds in the vicinity of the Minkler Lake Dam is less than two degrees, with the southeast limb slightly steeper than the northwest limb. The dam is located south of the Windham Syncline. In general, the discontinuity trends are northeast and northwest.

The stratigraphy consists of glacial till which will range in thickness from very thin to approximately 200 feet. The glacial till is underlain by the Devonian Chemung Formation, which is approximately 380 feet thick in this area. The Chemung Formation is marine in origin, consisting of interbedded green-gray sandstone, sandy shale and shale. The shale strata tend to weather rapidly when exposed.



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#### PENNSYLVANIAN

#### APPALACHIAN PLATEAU

Po

Allegheny Group Cicle sequences of sandstone, shale, time-stone, and coal, numerous commercial coals, investores thicken vestward; Yon-port Lim stone in lower part of section, includes Freeport, Kitlanning, and Clarion Formations.



#### **Pottsville Group**

Predominantly sandstones and conglomer-nies with this shales and couls; some coals mineable locally.

ANTHRACITE REGION



**Post-Pottsville Formations** Brown or gray sandsiones and shales with some conglomerate and numerous mineable coals



**Pottsville Group** Light gray to while, coarse grained sand-stones and conglomerates with some mine-able coal; includes Sharp Mountain, Schuylkill, and Tumbling Run Forma-tions.

MISSISSIPPIAN	I
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#### Mauch Chunk Formation

Matter Calute Formation Red shales with bouwn to greenish gray flaggy soudstonis, includes treenbrus Limestone in Fayette, Westmoreland, and Sourcest counties Logathanna Limestone at the base in southwestern Pennsylvania.

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#### Pocono Group

Perdonium this gray, hard, massive, cross-bedded condomeratic and sondstanic with some shule, includes in the Appalachian Plateau Burgoon, Shenanao, Cuyabago, Cussewago, Cory, and Koopp Forma-tions, includes part of "Owango" of M. L. Fuller in Potter and Tioga counties.

#### **DEVONIAN** UPPER

CENTRAL AND EASTERN PENNSYLVANIA



Dck

#### **Oswayo** Formation

Oswayo formation Brownish and greenish pray, fine and medium grained sandstones with some shales and sentlered calcarcous lenses, includes red shales which become more numerous castward. Relation to type Orwayo not proved.

#### **Catskill Formation**

Chiefly red to brownish shales and sand-stones, includes gray and greenish sand-stone tongues named Etk Mountain, Honesdale, Shohola, and Delaware River in the east,



Marine beds Gray to olive brown shales, graywackes, and sandstones, contains "Chemung" beds and "Portage" beds including Burket, Brallier, Harrell, and Trimmers Rock; Tully Limestone at base.

## Ds

Susquehanna Group

Barbed line in "Chemung- Catakill" con-tact of Second Pennsylvania Survey County reports; barbs on "Chemung" side of line.

REFERENCE:

GEOLOGIC MAP OF PENNSYLVANIA PREPARED BY COMMONWEALTH OF PENNA, DEPARTMENT OF ENVIRONMENTAL RESOURCES, DATED : 1960 SCALE 1 : 250,000





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