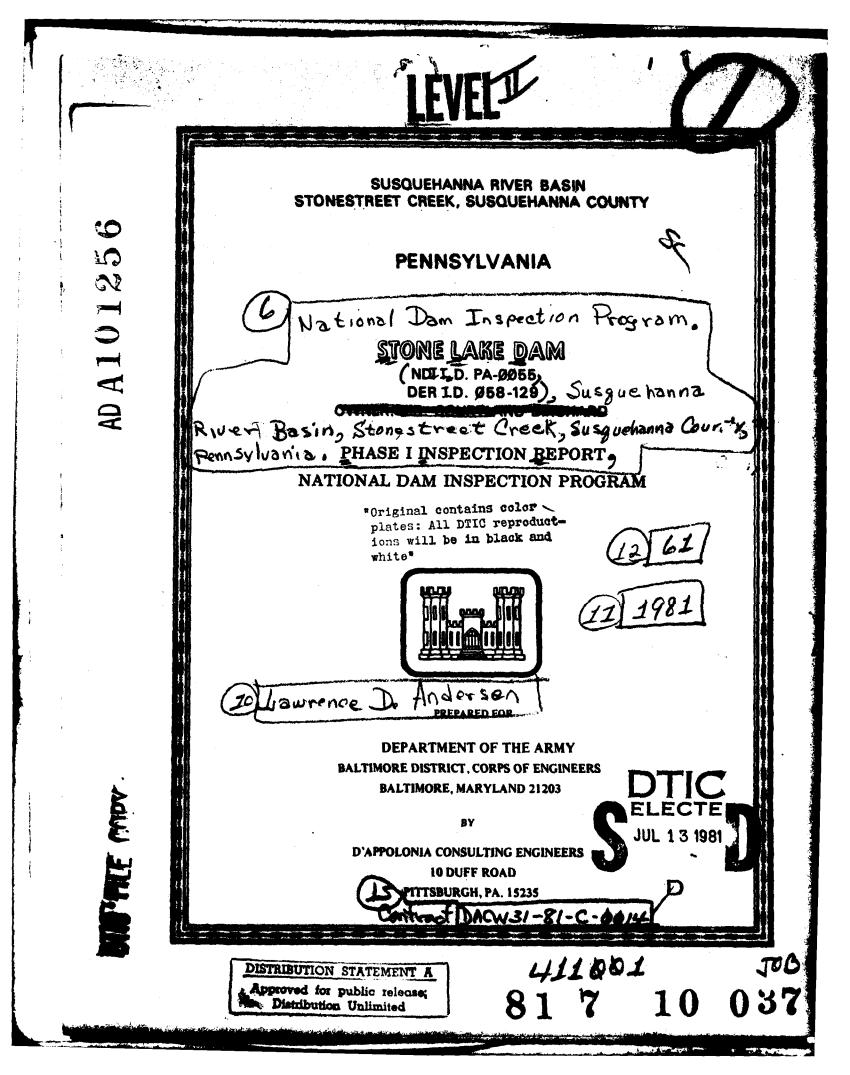
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PREFACE

This report is prepared under guidance contained in the <u>Recommended</u> <u>Guidelines for Safety Inspection of Dams</u>, for Phase I Investigations. Copies of these guidelines may be obtained from the Department of the Army, Office of Chief of Engineers, Washington, D.C. 20314.

The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon visual observations and review of available data. Detailed investigations and analyses involving topographic mapping, subsurface investigations, material testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the inspection is intended to identify any need for such studies which should be performed by the owner.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of the dam depends on numerous and constantly changing internal and external factors which are evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The assessment of the conditions and recommendations was made by the consulting engineer in accordance with generally and currently accepted engineering principles and practices.

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

NAME OF DAM: Stone Lake Dam STATE LOCATED: Pennsylvania COUNTY LOCATED: Susquehanna STREAM: Stonestreet Creek, tributary of Middle Branch of Wyalusing Creek SIZE CLASSIFICATION: Small HAZARD CLASSIFICATION: Significant OWNER: Mr. Courtland Birchard DATE OF INSPECTION: March 24, 1981 and April 30, 1981

ASSESSMENT: Based on the evaluation of the existing conditions, the condition of Stone Lake Dam is considered to be good. At this time, no conditions were observed that would significantly affect the overall performance of the structure.

The spillway capacity was evaluated according to the recommended procedures and was found to pass the required spillway design flood of 50 percent of the PMF. Therefore, the spillway capacity is rated as adequate.

The following recommendations should be implemented immediately or on a continuing basis.

- 1. The owner should confirm the operational condition of the outlet pipe valve and perform maintenance, if required. The need for providing an upstream control to the outlet pipe should be evaluated.
- The swampy area below the toe of the dam should be periodically observed and necessary remedial work should be performed if seepage conditions develop.
- 3. The barbed wire fence across the right abutment emergency spillway should be relocated sufficiently away from the flow control section to prevent possible blockage of the channel by debris.
- 4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- 5. The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.

Assessment - Stone Lake Dam



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Lawrence D. Andersen, P.E. Vice President

June 1, 1981 Date

Approved by:

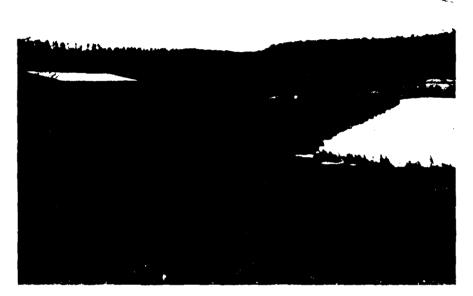
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JAMES W. PECK Golonel, Corps of Engineers Commander and District Engineer

17 June 1981

Date:

STONE LAKE DAM ND1 1.D. PA-0055 DER 1.D. 058-129 MARCH 24, 1981



Upstream Face



Downstream Face

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SECTION 1 PROJECT INFORMATION

1.1 General

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a. <u>Authority</u>. The inspection was performed pursuant to the authority granted by The National Dam Inspection Act, Public Law 92-367, to the Secretary of the Army, through the Corps of Engineers, to conduct inspections of dams throughout the United States.

b. <u>Purpose</u>. The purpose of this inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project

a. Dam and Appurtenances. Stone Lake Dam consists of an earth embankment approximately 500 feet long with a maximum height of 21 feet from the downstream toe and a crest width of 12 feet. Both the upstream and downstream slopes of the dam are covered with grass and are 2.5H:1V. The flood discharge facilities for the dam consist of a drop inlet type primary spillway located near the center of the dam and two trapezoidal earth channel emergency spillways on both abutments. The design drawing indicates that the low level outlet facilities consist of an eight-inch pipe extending through the embankment along the original stream bed and terminating at the downstream toe of the dam. Flow through the pipe is controlled by a valve near the downstream end. Only the outlet valve chamber is visible.

b. Location. Stone Lake Dam is located on Stonestreet Creek, approximately three miles upstream of its confluence with Middle Branch of Wyalusing Creek in Forest Lake Township, Susquehanna County, Pennsylvania (N41° 52.8', W76° 2.1'). Plate 1 illustrates the location of the dam.

c. <u>Size Classification</u>. Small (based on 21-foot height and approximately 160 acre-feet maximum storage capacity).

d. <u>Hazard Classification</u>. The dam is classified to be in the significant hazard category. Downstream from the dam, Stonestreet Creek flows through a wide, essentially uninhabited valley for approximately three miles from the dam and joins the Middle Branch of Wyalusing Creek. One farmhouse, located one mile from the dam along Stonestreet Creek, and two houses near the confluence with the Middle Branch constitute the main impact area of a flood in the event of a dam failure. It is estimated that State Route 267 would also be damaged due to a dam failure. Failure of the dam would probably cause loss of a few lives and property damage in this area.

e. <u>Ownership</u>. Mr. Courtland Birchard, R.D. #5, Box 113, Montrose, Pennsylvania 18801.

f. Purpose of Dam. Recreation and conservation.

g. <u>Design and Construction History</u>. The dam was designed in 1961 by the U.S. Department of Agriculture, Soil Conservation Service, Susquehanna County office. The dam was completed in 1962.

h. <u>Normal Operating Procedure</u>. The reservoir is normally maintained at Elevation 1432, the uncontrolled primary spillway crest elevation, leaving 6.3 feet of freeboard to the low spot of the dam at Elevation 1438.3. Inflow occurring when the lake level is at or above primary spillway level is discharged through the drop inlet spillway up to Elevation 1433.5 and through the emergency spillway when above Elevation 1433.5.

1.3 <u>Pertiment Data</u>. Elevations referred to in this and subsequent sections of the report were calculated based on approximate field measurements, assuming the primary spillway crest to be at Elevation 1432 (USGS Datum), which is the elevation shown as the normal pool elevation on the USGS 7.5-minute Friendsville quadrangle. Elevations shown on the design drawings appear to be relative to an arbitrary site datum.

0.58 square mile⁽¹⁾

- a. Drainage Area
- b. Discharge at Dam Site (cfs)

Maximum known flood at dam site Outlet conduit at maximum pool Gated spillway capacity at maximum pool Ungated spillway capacity at maximum pool Total spillway capacity at maximum pool

c. <u>Elevation (USGS Datum) (feet)</u> Top of dam

> Maximum pool Normal pool Upstream invert outlet works

Unknown Unknown Not applicable 1446 1446

1439.2 (as designed) 1438.3 (measured low spot) 1438.3 1432 1422(2)

(2)Based on design drawing.

⁽¹⁾Planimetered from USGS topographic map. State files indicate the same drainage.

	Downstream invert (primary spillway) Maximum tailwater Toe of dam	1425.3 Unknown 1417.6
d.	Reservoir Length (feet)	
	Normal pool level	1600
	Maximum pool level	1800 <u>+</u>
e.	Storage (acre-feet)	
	Normal pool level	33
	Maximum pool level	160
f.	Reservoir Surface (acres)	
	Normal pool level	16 <u>+</u>
	Maximum pool level	24 <u>+</u>
g.	Dam	
	Туре	Earth embankment
	Length	500 feet
	Height	21 feet
	Top width Side slopes	12 feet
	Side slopes	Downstream: 2.5H:1V; (measured) ⁽³⁾
		Upstream: 2.5H:1V (measured) ⁽³⁾
	Zoning	No
	Impervious core	No
	Cutoff	No
	Grout curtain	No
h.	Regulating Outlet	
	Туре	8-inch steel pipe
	Length	130+ feet
	Closure	Downstream valve chamber
	Access	Downstream toe
	Regulating facilities	Downstream valve

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(3)_{Design} slopes 3H:1V.

i. Spillway

Type

Length Crest elevation Upstream channel Downstream channel Drop inlet

8⁺ foot perimeter 1432 Lake Two-foot-diameter reinforced concrete pipe and earth channel

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Emergency:

Two trapezoidal earth channels 25 feet (each) 1433.5 (4) Lake Earth channel

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(4)Measured spillway crest. State files indicate the crest elevation to be 1435.6 or 3.6 feet above the normal pool Elevation 1432.

2.1 Design

a. <u>Data Available</u>. The available data consist of files provided by the Commonwealth of Pennsylvania, Department of Environmental Resources (PennDER), which contain design drawings, correspondence, and inspection photographs and reports.

(1) <u>Hydrology and Hydraulics</u>. The available information includes the design capacity of the spillway, reservoir storage volume, watershed area and hydrology calculations.

(2) <u>Embankment</u>. The available information consists of various design drawings and past state inspection reports.

(3) <u>Appurtement Structures</u>. The available information consists of design drawings.

b. Design Features

(1) <u>Embankment</u>. Plate 2 illustrates the plan of the embankment and the reservoir. As illustrated in Plate 3, the dam is a homogeneous embankment designed to have a 3:1 (horizontal to vertical) slope on both the downstream and upstream slopes and a crest width of 12 feet. The upstream face was to be protected with riprap extending two feet above and two feet below the normal pool level (Elevation 1432).

(2) <u>Appurtement Structures</u>. The appurtement structures of the dam consist of primary and emergency spillways and the outlet works as shown on Plates 2 and 3. The primary spillway is comprised of a 30-inch-diameter reinforced concrete drop inlet structure at Elevation 1432, discharging into a 24-inch-diameter reinforced concrete pipe through the dam which terminates at the downstream toe. One antiseep collar was provided along the pipe. The design drawings indicate that the upstream end of the pipe is equipped with a reinforced concrete base to serve as a foundation for the drop inlet structure. The emergency spillway discharge channels are trapezoidal earth channels with a base width of 25 feet. The control section of the primary spillway is located at a level 3.6 feet above the primary spillway invert.

The design drawings indicate that the low level outlet facility for the dam consists of an eight-inch steel pipe equipped with a gate valve near the downstream end.

c. Design Data

(1) Hydrology and Hydraulics. A Commonwealth of Pennsylvania report entitled "Report Upon the Application of Carlton E. Birchard,"

dated July 6, 1961, indicates that the capacity of the emergency spillway meets the state's "C" curve criteria. Further, it was noted that sufficient storage was provided between normal pool and emergency spillway crest to store runoff from a 10-year flood.

(2) <u>Embankment</u>. Available information indicates that a material investigation consisting of excavation of test pits and borings were performed by the U.S. Department of Agriculture, Soil Conservation Service. A subsurface profile is shown on Plate 3. No reference was found to indicate whether any engineering analyses, such as slope stability or seepage analyses, were performed based on the results of the soils investigation.

(3) <u>Appurtemant Structures</u>. No design calculations are available for the appurtemant structures.

2.2 <u>Construction</u>. In general, the construction of the dam was apparently conducted in accordance with the drawings and specifications. Based on visual observations, two changes were noted: (1) Riprap called for on the upstream face has not been provided, and (2) Location of the primary spillway was changed from an area near the left abutment to a location right of the center of the dam.

No reports were found to indicate any major postconstruction change of the dam structure.

2.3 <u>Operation</u>. There are no formal operating records maintained for the dam. The normal reservoir water level is maintained by discharge through the primary spillway.

2.4 Other Investigations. None reported.

2.5 Evaluation

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Availability. The available information was provided by PennDER.

b. Adequacy

(1) Hydrology and Hydraulics. The available information is not considered to be sufficient to assess the adequacy of the spillways.

(2) <u>Embankment</u>. Other than design drawings and the material investigation study, no other design information is available to determine the adequacy of the design of the dam. The design apparently lacks such considerations as embankment slope stability and seepage analyses and other quantitative data to aid in the assessment of the design.

(3) <u>Appurtemant Structures</u>. Review of the design drawings indicate that the appurtemant structures are designed and constructed in conformance with currently accepted engineering practice.

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SECTION 3 VISUAL INSPECTION

3.1 Findings

a. <u>General</u>. The onsite inspection of Stone Lake Dam consisted of:

1. Visual inspection of the embankment, abutments, and embankment toe.

2. Visual examination of the spillways and the visible portions of the outlet works.

3. Evaluation of downstream area hazard potential.

The specific observations are illustrated in Plate 4.

b. <u>Embankment</u>. The general inspection of the embankment consisted of searching for indications of structural distress, such as cracks, subsidence, bulging, wet areas, seeps and boils, and observing general maintenance conditions, vegetative cover, erosion, and other surficial features.

In general, the condition of the dam is considered to be good. One wet area was observed at the toe of the dam in an area which appears to be the original streambed. No seepage flow appeared to be associated with this area. The downstream face and the crest are covered with grass and found to be adequately maintained.

The dam crest was surveyed relative to the primary spillway crest elevation and was found to have some vertical irregularities. Although the design freeboard for the dam is 7.2 feet, the field survey indicated freeboards ranging from 6.3 feet to 7.2 feet. The lowest area occurred in a section adjacent to the left emergency spillway. The dam crest profile, according to field measurements, is illustrated in Plate 5.

c. <u>Appurtenant Structures</u>. The appurtenant structures were examined for deterioration or other signs of distress and obstructions that would limit flow. In general, the structures were found to be in good condition. The primary spillway drop inlet structure is equipped with grating at the intake which could be vulnerable to blockage by debris. Similarly, a barbed wire fence across the right emergency spillway control section poses some potential for blockage of the channel by debris during storms.

The owner reported that the low level outlet pipe valve has not been operated since the construction of the dam. Operation of the low level outlet pipe valve was not observed.

d. <u>Reservoir Area</u>. A map review indicates that the watershed is predominantly covered by rural farm areas with some wooded areas. No signs of landslide activity were found in the vicinity of the reservoir. A review of the regional geology is included in Appendix F.

e. <u>Downstream Channel</u>. Downstream from the dam, Stonestreet Creek flows approximately three miles where it passes under State Route 267 and then joins the Middle Branch of Wyalusing Creek. A further description of the downstream conditions is included in Section 1.2 d.

3.2 <u>Evaluation</u>. The Stone Lake Dam was found to be in good condition and adequately maintained. The operational condition of the low level outlet pipe was not observed. Therefore, the owner should evaluate the operational condition of the facility.

SECTION 4 OPERATIONAL FEATURES

4.1 <u>Procedure</u>. There are no formal operating procedures for the dam. The reservoir is normally maintained at the uncontrolled spillway crest level with excess inflow discharging over the spillway.

4.2 <u>Maintenance of the Dam</u>. The maintenance of the dam is considered to be good. The crest and slopes of the dam are covered with grass and adequately maintained.

4.3 <u>Maintenance of Operating Facilities</u>. The only operable facility of the dam is the low level outlet pipe valve. The owner reported that the valve was not operated since the construction of the dam. The operational condition of the valve was not observed.

4.4 <u>Warning System</u>. No formal warning system exists for the dam. Telephone communication facilities are available via the owner's residence along the reservoir shoreline.

4.5 <u>Evaluation</u>. The maintenance condition of the dam is considered to be good. The owner should evaluate the operational condition of the low level outlet pipe.

SECTION 5 HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features

a. Design Data. Stone Lake Dam has a watershed of 0.6 square mile and impounds a reservoir with a surface area of 16 acres at normal pool level. The flood discharge facilities for the dam consist of two 25-foot trapezoidal emergency spillway channels, one located on each abutment, and a drop inlet type primary spillway located near the center of the dam. The combined spillway capacity was estimated to be 1446 cfs, based on 6.3 feet of available freeboard relative to the low spot on the crest of the dam.

b. Experience Data. As previously stated, Stone Lake Dam is classified as a small dam in the significant hazard category. Under the recommended criteria for evaluating emergency spillway discharge capacity, such impoundments are required to pass from the 100-year storm up to one-half PMF. In view of the downstream damage potential, one-half PMF is considered to be applicable to this dam.

The PMF inflow hydrograph for the reservoir was determined utilizing the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army, Corps of Engineers. The data used for the computer input are presented in Appendix D. The one-half PMF inflow hydrograph was found to have a peak flow of 910 cfs. The peak flow of the 100-year flood was calculated according to the recommended procedure and was found to be 530 cfs. The computer input, summary of the computer output, and the 100-year flood calculations are included in Appendix D.

c. <u>Visual Observations</u>. On the date of inspection, no conditions were observed that would indicate that the spillway capacity would be significantly reduced in the event of a flood. However, as noted before, a barbed wire fence across the right abutment emergency spillway may pose a potential for blockage of the channel by debris during storms.

d. Overtopping Potential. The available spillway capacity was found to be greater than the 100-year flood peak. Further, various percentages of the PMF inflow hydrograph were routed through the reservoir to determine the percent of PMF inflow that the dam can pass without overtopping the embankment. The computer analyses indicate that the spillway can pass 50 percent PMF without overtopping. This would result in a maximum water surface elevation of 1436.3 within the reservoir, leaving approximately two feet of freeboard to the measured low spot of the dam.

e. <u>Spillway Adequacy</u>. The spillway capacity was found to fulfill the recommended spillway design capacity requirements and is, therefore, classified as adequate.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

(1) <u>Embankment</u>. As discussed in Section 3, the field observations did not reveal any signs of distress that would significantly affect the performance of the structure, and no unsatisfactory conditions have been reported in the past.

(2) <u>Appurtement Structures</u>. No conditions were observed that would affect the structural performance of appurtement structures.

b. Design and Construction Data

(1) Embankment. The available design and construction information does not provide any quantitative data to aid in the assessment of stability. However, as previously noted, the field observations did not reveal any signs of distress which would significantly affect the stability of the dam at this time and none were reported in the past. Therefore, based on visual observation, structural stability of the dam is considered to be adequate.

(2) <u>Appurtement Structures</u>. A review of the design drawings indicates that there are no apparent structural deficiencies that would significantly affect the performance of the appurtement structures.

c. Operating Records. Not maintained.

d. <u>Postconstruction Changes</u>. There have been no reported postconstruction modifications to the original design that would affect the structural stability of the embankment.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1, and based on visual observations, the static stability of the dam is considered to be adequate. Therefore, based on the recommended criteria for evaluation of seismic stability of dams, the structure is presumed to present no hazard as a result of earthquakes.

SECTION 7

ASSESSMENT AND RECOMMENDATIONS/PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. <u>Assessment</u>. The visual observations indicate that the condition of Stone Lake Dam is good. At this time, no conditions were observed that would significantly affect the overall performance of the structure.

The spillway capacity was evaluated according to the recommended procedures and was found to pass the required spillway design flood of 50 percent of the PMF. Therefore, the spillway capacity is rated as adequate.

b. <u>Adequacy of Information</u>. The available information, in conjunction with the visual observations, is considered to be sufficient to make a Phase I evaluation.

c. <u>Urgency</u>. The following recommendations should be implemented as soon as possible or on a continuing basis.

d. <u>Necessity for Additional Investigation</u>. No additional investigation is considered to be required at this time.

7.2 Recommendations/Remedial Measures. It is recommended that:

- 1. The owner should confirm the operational condition of the outlet pipe valve and perform maintenance, if required. The need for providing an upstream control to the outlet pipe should be evaluated.
- 2. The swampy area below the toe of the dam should be periodically observed and necessary remedial work should be performed if seepage conditions develop.
- 3. The barbed wire fence across the right abutment emergency spillway should be relocated sufficiently away from the flow control section to prevent possible blockage of the channel by debris.
- 4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.

APPENDIX A

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CHECKLIST VISUAL INSPECTION PHASE I

APPENDIX A	DIX A
CHECKLIST VISUAL INSPECTION PHASE I	LIST SPECTION E T
NAMF OF DAM Stone Lake COUNTY Susy	NDI: PA-0055 Susquehanna STATE Pennsylvania ID# DER: 058-129
	HAZARD CATEGORY Significant
DATE(S) INSPECTION March 24, 1981 WEATHER Cloudy	udy TEMPERATURE 40
POOL ELEVATION AT TIME OF INSPECTION 1432 M.S.L.	.L. TAILWATER AT TIME OF INSPECTION 1417.6 M.S.L.
INSPECTION PERSONNEL: REVIEW INSPECTION PERSONNEL: (April 30, 1981)	ON PERSONNEL: , 1981)
Arthur Smith Lawrence D. Andersen	. Andersen
Wah-Tak Chan James H. Po	Poellot
Bilgin Erel Bilgin Erel	1
Owner's Representative:	Bilgin Erel RECORDER
Mr. C. Birchard	
Page Al of	1 of 9

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	VISUAL INSPECTION PHASE I EMBANKMENT	
VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OR	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None observed.	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None observed.	<u></u>
SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES	None observed.	
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	See Plate 5 for dam crest profile. No noticeable horizontal misalignment observed.	
RIPRAP FAILURES	Upstream slope has no shoreline riprap protection.	
	Page A2 of 9	

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	REMARKS OR RECOMMENDATIONS		This area should be peri- odically observed to determine if seepage conditions are developing.		-		•
PHASE I EMBANKMENT	OBSERVATIONS	No problems observed.	None. A swampy area is located below the toe of the dam. See Plate 4 for location.	None	None		
	VISUAL EXAMINATION OF	JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	ANY NOTICEABLE SEEPAGE	STAFF GAGE AND RECORDER	DRATNS		

Page A3 of 9

VISUAL INSPECTION PHASE T

	REMARKS OR RECOMMENDATIONS			The owner should locate the downstream end of the outlet pipe.		he The owner should confirm ved. the operational condition of the outlet pipe valve.	
VISUAL INSPECTION PHASE I OUTLET WORKS	OBSERVATIONS	Other than a valve chamber on the downstream slope, no portions of the outlet works were visible.	Submerged.	Downstream end of the outlet pipe could not be located.	Earth channel.	Located in a valve chamber on the downstream face of the dam. Operational condition of the valve was not observed.	Page A4 of 9
	VISUAL EXAMINATION OF	CRACKING AND SPALLING DF CONCRETE SURFACES IN OUTLET CONDUIT	INTAKE STRUCTURE	OUTLET STRUCTURE	OUTLET CHANNEL	EMERGENCY GATE	

REMARKS OR RECOMMENDATIONS				The fence should be relocated away from the control section of the spillway.	
UNGATED SPILLWAY OBSERVATIONS	The emergency spillway is an earth channel.	No problems observed.	In good condition. No obstruction on the left emergency spillway channel.	None. A barbed wire fence across the right abutment spillway is considered to pose a potential for blockage of the channel by debris during floods.	
VISUAL EXAMINATION OF	CONCRETE WEIR	APPROACH CHANNEL	DISCHARGE CHANNEL	BRIDCE AND PIERS	

Page A5 of 9

SCAL MARKED

VISUAL INSPECTION PHASE I UNCATED SPILLWAY

**

	REMARKS OR RECOMMENDATIONS					
VISUAL INSPECTION PHASE I GATED SPILLWAY	OBSERVATIONS	The dam has no gated spillway.	N/A	N/A .	N/A	N/A
	VISUAL EXAMINATION OF	CONCRETE SILL	APPROACH CHANNEL	DISCHARGE CHANNEL	BRIDGE PIERS	GATES AND OPERATION EQUIPMENT

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VISUAL INSPECTION PHASE I INSTRUMENTATION

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		REMARKS OR RECOMMENDATIONS
VISUAL EXAMINATION OF MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
PIEZOMETERS	None	
OTHER	None	

11-11-11-11-11

Page A7 of 9

	REMARKS OR RECOMMENDATIONS					
PHASE I PHASE I RESERVOIR	OBSERVATIONS	No problems observed.	Unknown	A two- to four-acre pond immediately upstream of the reservoir.		Page A8 of 9
	VISUAL EXAMINATION OF	SLOPES	SEDIMENTATION	UPSTREAM RESERVOIRS		

VISUAL INSPECTION

;

	REMARKS OR RECOMMENDATIONS				-	
DOWNSTREAM CHANNEL	OBSERVATIONS	No problems observed.	No problems observed.	One farm located one mile downstream. (Population estimated at four.)		Page A9 of 9
	VISUAL EXAMINATION OF	CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	SLOPES	APPROXIMATE NUMBER OF HOMES AND POPULATION		

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VISUAL INSPECTION PHASE I DOWNSTREAM CHANNEL

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APPENDIX B

CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION AND HYDROLOGIC AND HYDRAULIC PHASE I

The dam was designed by the Soil Conservation Service in 1961; construction was completed in 1962. 058-129 ID# NDI: PA-0055 NAME OF DAM Stone Lake DER: The design drawings are available in state files. REMARKS CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I ഹ Page Bl of See Plate 2. See Plate 3. See Plate 1. - DISCHARGE RATINGS TYPICAL SECTIONS OF DAM - DETAILS - CONSTRAINTS REGIONAL VICINITY MAP CONSTRUCTION HISTORY AS-BUILT DRAWINGS **OUTLETS - PLAN** ITEM

APPENDIX B

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CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I	REMARKS	Not available.	A state report entitled "Report Upon the Application of Carlton E. Birchard," dated July 6, 1961.	Not available.	Hydrology and hydraulics analysis are available in state files. Stability and seepage analysis are not included.	See Plate 3 for subsurface profile and material classification.
	ITEM	RAINFALL/RESERVOIR RECORDS	DESIGN REPORTS	GEOLOGY REPORTS	DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

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Page B2 of 5

CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

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ITEM	REMARKS
POST CONSTRUCTION SURVEYS OF DAM	None reported.
BORROW SOURCES	Unknown
MONITORING SYSTEMS	None
MODIFICATIONS	None
HIGH POOL RECORDS	According to the owner, Mr. Courtland Birchard, two feet of water flowed through both emergency spillways during tropical storm Agnes in 1972.

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Page B3 of 5

CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

POST CONSTRUCTION ENCINERING None reported. FULURE OF DAM RECORTS None reported. MINTENNICE OFFATION RECORDS None reported. MINTENNICE OFFATION RECORDS Not maintained. MINTENNICE OFFATION RECORDS Not maintained. SFILLANT FLAN See Plate 3. SECTIONS See Plate 3. DETAILS See Plate 3. OFFRATING EQUIPHINT See Plate 3. OFFRATING EQUIPHINT See Plate 3. OFFRATING EQUIPHINT See Plate 3.	ITEN	REMARKS
FATLURE OF DAM	POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None reported.
	PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported.
See Plate See Plate	MAINTENANCE OPERATION RECORDS	Not maintained.
See Plate	SPILLWAY PLAN SECTIONS DETAILS	See Plate 3.
	OPERATING EQUIPMENT PLANS AND DETAILS	See Plate 3.

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Page B4 of 5

CHECKLIST ENGINEERING DATA HYDROLOGIC AND HYDRAULIC

DRAINAGE AREA CHARACTERISTICS: <u>0.58 square mile (partially wooded and pastureland)</u> ELEVATION, TOP OF NORMAL POOL AND STORAGE CAPACITY: <u>1432 (33 acre-feet)</u> ELEVATION, TOP OF FLOOD CONTROL POOL AND STORAGE CAPACITY: <u>1438.3 (approximately</u> ELEVATION, MAXIMUM DESIGN POOL: <u>1439.2 (design top of dam)</u> ELEVATION, TOP OF DAM: <u>1438.3 (low spot)</u> SPILLWAY:

a. Elevation 1432 (primary); 1433.5 (emergency)

- b. Type <u>24-inch-diameter reinforced concrete pipe with 30-inch-diameter</u> reinforced concrete pipe riser (primary), trap. emergency
 c. Width <u>Two 25-foot trap. emergency spillway with 3:1 side slope</u>
- d. Length Approximately 100 feet at 2 percent slope
- e. Location Spillover Both ends of dam
- f. Number and Type of Gates None

OUTLET WORKS:

- a. Type 8-inch-diameter steel pipe
- b. Location Near left abutment
- c. Entrance Inverts 1422 (estimated)
- d. Exit Inverts 1420 (estimated) (downstream end not located)
- e. Emergency Drawdown Facilities 8-inch steel pipe

HYDROMETEOROLOGICAL GAGES:

- a. Type<u>None</u>
- b. Location N/A
- c. Records <u>None</u>

MAXIMUM NONDAMAGING DISCHARGE: <u>Approximately 470 cfs in 1972 (estimated</u> based on 2-foot water depth and 50-foot channel width) APPENDIX C

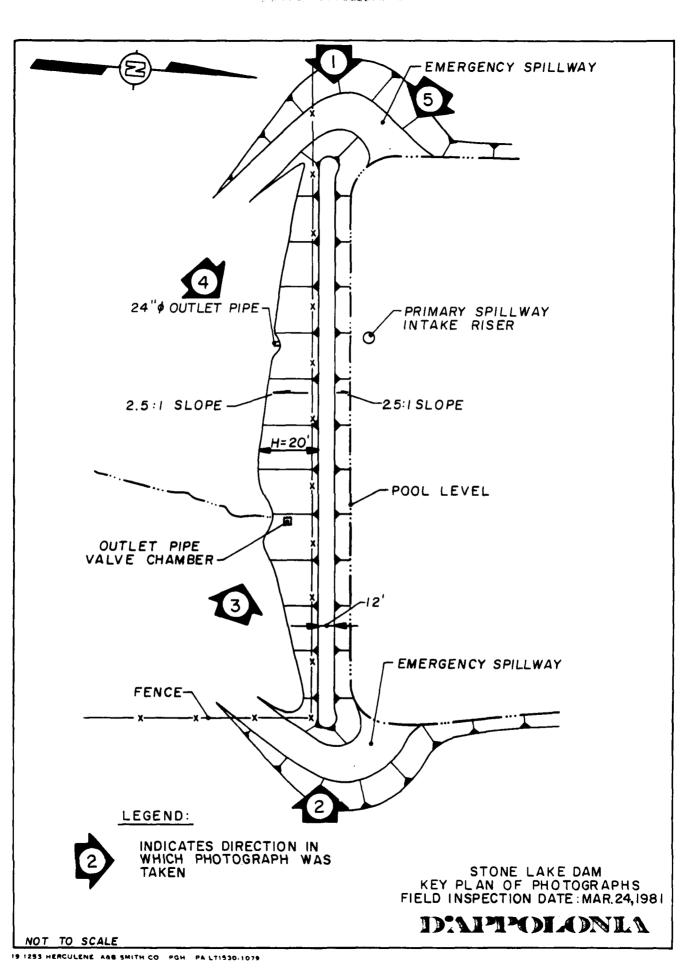
PHOTOGRAPHS

LIST OF PHOTOGRAPHS STONE LAKE DAM NDI I.D. NO. PA-0055 MARCH 24, 1981

PHOTOGRAPH NO.	DESCRIPTION
1	Dam crest (looking east).
2	Dam crest (looking west).
3	Downstream face.
4	24-inch-diameter outlet pipe.
5	Upstream face (note emergency spillway channel at foreground).
6	A house and a barn along Stone- street Creek (approximately 1.0 mile downstream from dam).
7	A house along Stonestreet Creek near State Route 267 underpass (approxi- mately 3.0 miles downstream from dam).

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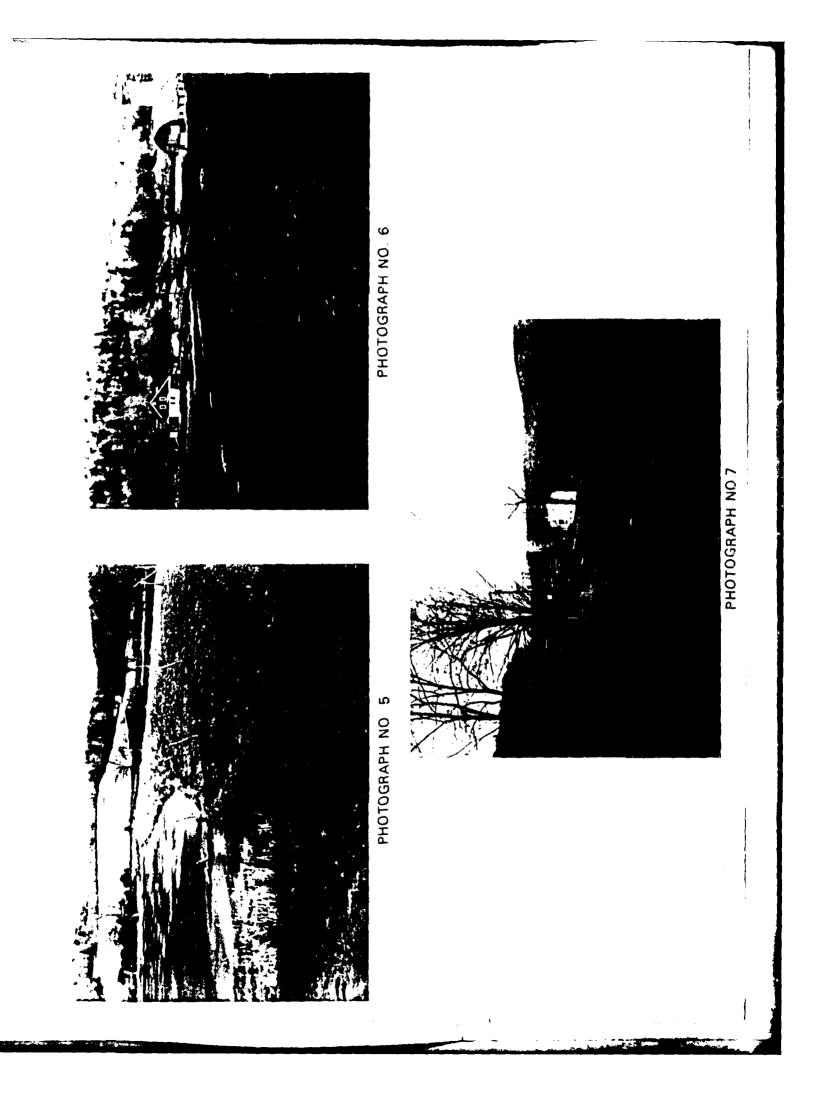


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APPENDIX D

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HYDROLOGY AND HYDRAULICS ANALYSES

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NAME OF DAM: Stone Lake Dam

PROBABLE MAXIMUM PRECIPITATION (PMP) = 22.2 INCHES/24 HOURS

STATION	1	2	3	4	5
Station Description	Stone Lake	Dam			
Drainage Area (square miles)	0.58	-			
Cumulative Drainage Area (square milea)	0.58	0.58			
Adjustment of PMF for Drainage Area (2) ⁽¹⁾	95%				
6 Hours	117	-		Į	
12 Hours	127	-			
24 Hours	136	-		1	
48 Hours	142	-			
72 Hours	145	-			
Snyder Hydrograph Parameters					
Zone ⁽²⁾	11	- 1		1	
c _p /c _t (3)	0.62/1.50	-			
L (miles) ⁽⁴⁾	0.85	-			
L _{ca} (miles) ⁽⁴⁾	0.40	-	ĺ	ļ	
$t_p = C_t (L \cdot L_{ca})^{0.3}$ (hours)	1.08	-	ļ		
Spillway Data	1	Primary Emerg	ncy		<u> </u>
Crest Length (ft)	-	7 50		}	}
Freeboard (ft)	-	6.3 4.8			
Discharge Coefficient	-	3.2 2.65			
Exponent	j -	1.5 1.5			

(1)Hydrometeorological Report 40, U.S. Weather Bureau, 1965.

(2) Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients (C_p and C_t).

(3) Snyder's Coefficients.

(4) L = Length of longest water course from outlet to basin divide.
 L_{cs} = Length of water course from cutlet to point opposite the centroid of drainage area.

ELEVATION	AH, FEET	AREA (acres)(1)	AVOLUME (acre-feet)	STORAGE (acrefeet)(2)
1432		16.3		33.0
1434	·	19.5	<u> </u>	
1436		21.4		
1430	-	24.0		160.0
1440	2	25.3		-

STORAGE VS. ELEVATION

⁽¹⁾From DER files, SCS calculations.

(2) Volume per HEC-1 computer run.

PAGE D1 OF 7

0446 LAKE DAM. (DER 58-129) 1 ö n n ö ó LAKE DAM, (DER 58-129) -1432.0 • m 1440.0 6 6 00 1439 24 0 1438.0 1426.3 400.0 1439.0 0.62 2.0 P. -0.05 2.0 ROUTING FLOW THROUGH STONE 1434.0 2.65 2.65 123.0 1428.7 1432.03 250.03 1438.65 1438.65 1438.65 21.1 1 08 -1 5 -่าวี_่ฐฐีธ∎⊢3×₅ฐี≻>

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COMPUTER INPUT OVERTOPPING ANALYSIS PAGE D2 OF 7 -----!} PEAK FLOW AND STURAGE (END OF PERIDD) SUMMARY FUN MULTIPLE PLAN-RATID ECUNUMIC COMPUTATIONS FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND) AREA IN SQUARE MILES (SQUARE KILOMETERS)

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RATIO 9 1.00	1815.	1493.42.26)
RATIO B	1634. 46. 26) (1325.
RAT10 7 .B0	1452.	1159. 32.81) (
RATIO 6	1271 35, 98) (995. 28. 18) (
RATIO 5	1089 30. 84) (828. 23. 44) (
LIED TO FL RATIO 50	908 25 70)(652. 18. 47) (
RATIOS APPLIED TO FLOWS Ratio 3 Ratio 4 Ratio 5 40 50 50 60	20. 36) (477 13 51)(
8AT 10 2	545. 15:42) (300. 8. 48) (
AREA PLAN RATIO 1 20	363 10.28) (121 3.43) (
PLAN	-	-
AREA	58 1. 50)	1. 50)
STAT ION	, ,	ຊັ
OPERATION	HYDROGRAPH AT	ROUTED TO

FLOOD ROUTING SUMMARY PAGE D3 OF 7

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TINE OF FAILURE HOURS TIME OF MAX OUTFLOW HOURS TOP OF DAM 1438.30 1446. DURATION OVER TOP HOURS SUMMARY OF DAM SAFETY ANALYSIS 8P ILLWAY CREET 1433 50 58. 41. MAXIMUM OUTFLOW CFB 121 121 123 9995 11399 11399 MAXIMUM STORAGE AC-FT 18001000 INITIAL VALUE 1432,00 33. 36. THE COCCOCCC ELEVATION STORAGE OUTFLOM MAXIMUM RESERVOIR W. S. ELEV 4234-25 14344-25 14344-25 14344-25 14344-25 14344-25 1454

OVERTOPPING ANALYSIS RESULTS SUMMARY PAGE D4 OF 7

PLAN

DAPPOLONIA

CONSULTING ENGINEERS, INC

By MB Date 5/1/81 Subject STONE LAKE DAM Sheet No. 1 of 1 Chkd. By WICDate 5/2/81 Flood PEAK DISCHARGE Proj. No. 80-556

FLOOD PEAK DISCHARGE BY REGRESSION EQUATIONS

REFERENCE : HERBERT N.FLIPPO, JR. "FLODS IN PENNSY LVANIA" WATER RESOURCES BULLETIN NO.13, K.S. DEPT. OF THE INTERIOR, GEOLOGICAL SURVEY, OCTOBER 1977

FROM PLATE 1 OF REFERENCE, STONE LARKE DAM IS LOCATED ON FLOOD - FREQUENCY "2", BASED ON THE RECORDS OF SO GAGING STATIONS WITH IN THIS REGION, THE FLOOD PEAK DISCHARGES, QT, AS CHOWN ON FIG 2 OF REFERENCE, ARE DETERMINED AS FOLLOWS

 $Q_T = C A^{\times}$; where A = WATERSHED AREA= 0.58 SQ.MI. X, C = REGRESSION COEF.

FREQUENCY	REGRESS (ON COEFFICIENTS		QT	
T-YEAR	С	×	Standard Error	efs
10	240	0.782	26%±	157
25	349	0.765	27%±	230
50	448	0.754	29%±	297
100	564	0.744	31%±	376

PAGE D5 OF 7

PAGE D6 OF 7

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EXERCISES
DONSULTING ENGINEERS. INC.
By MCS Date 4/25/81 Subject STONG LAKE DAM Sheet NO. 2 of 2
(Third ByUR Date 4/29/81 100 YZ FLOOD PRAX Proj. NO. 80-555
STONE LAKE DAM 100 YEAR FLOOD PE0.01

$$PRFINGEL AREA = 0.555 sig mines
 $CM = 2.13$
 $CS = 0.35$
 $G = 0.20$
 $Loc Q_M = 2.13 + 0.75 Loc (0.55) = 1.95$
 $S = 0.35 - 0.05 Loc (0.55) = 0.36$
FROM REF.1, EVINGIT 39
 $K(P, 0) = K(0.01, 0.20) = 2.472$
 $Loc Q_{0.01} = 1.95 + 2.472(0.36)$
 $= 2.84$
 $Q_{100VE} = 10^{284} = 690 CFS$
PRA CORPS OF ENGINEERS MEMO, PATED $4/22/81$, THE
ADOPTIED 100 YEAR FLOOD PEAK IS THE AUERAGE OF
METHODS A AND B.
 $Q_{100} = \frac{376+670}{233 CFS}$$$

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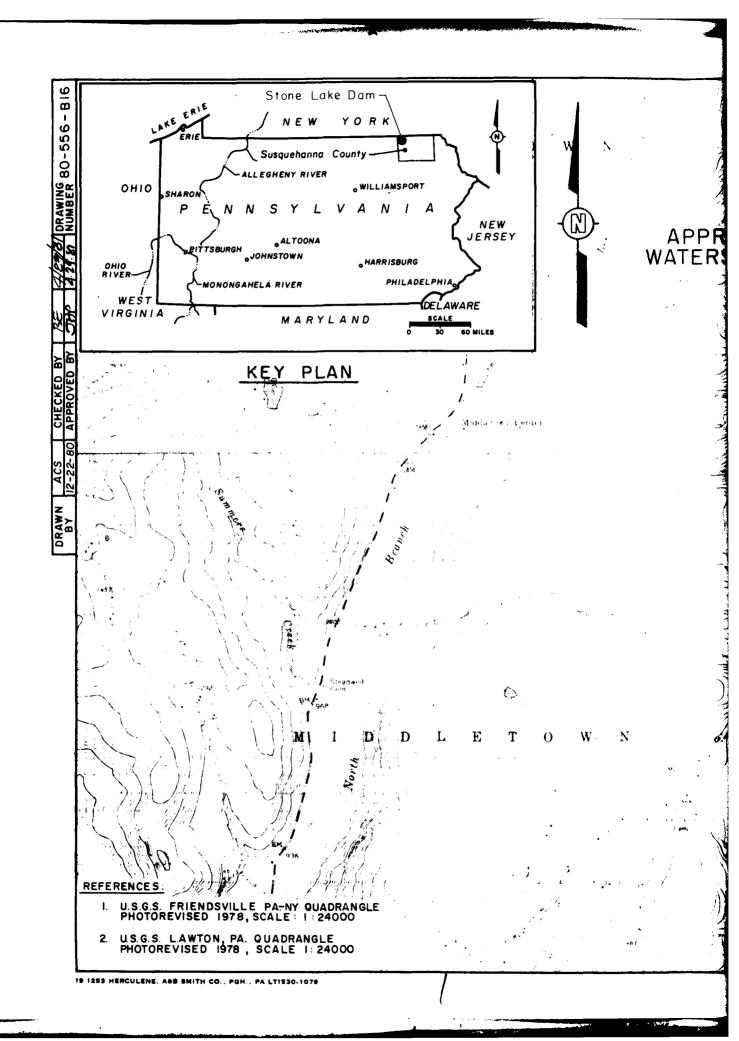
PAGE D7 OF 7

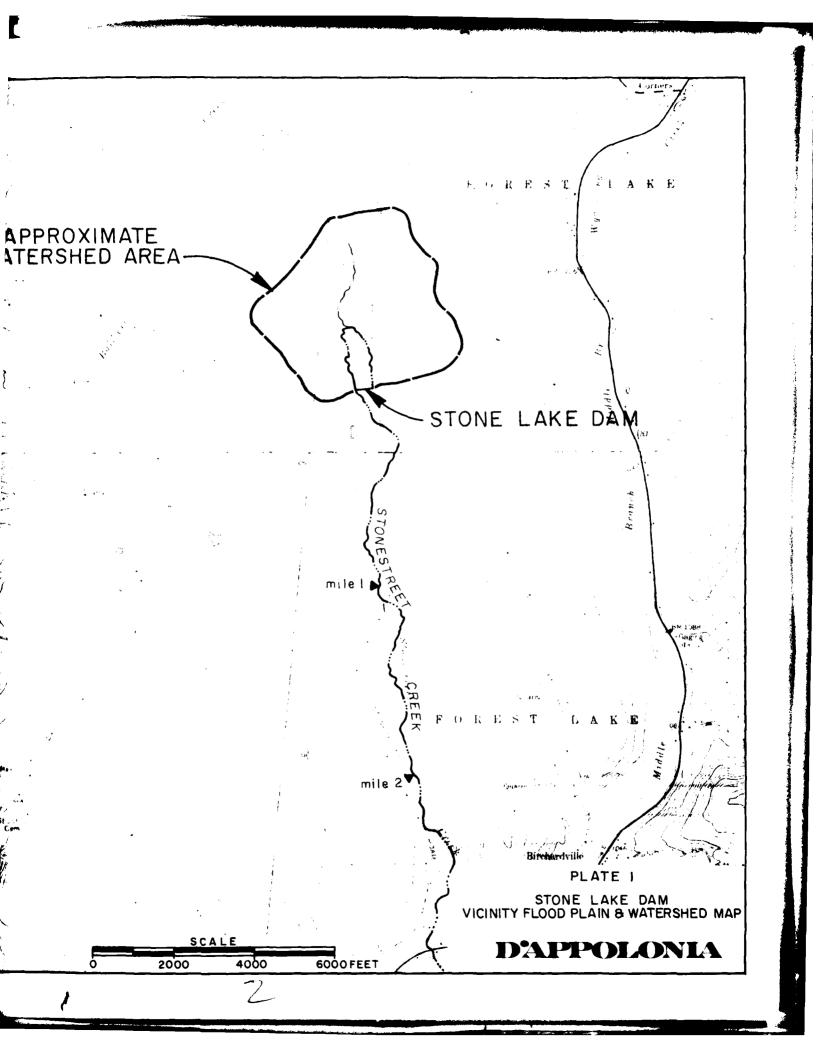
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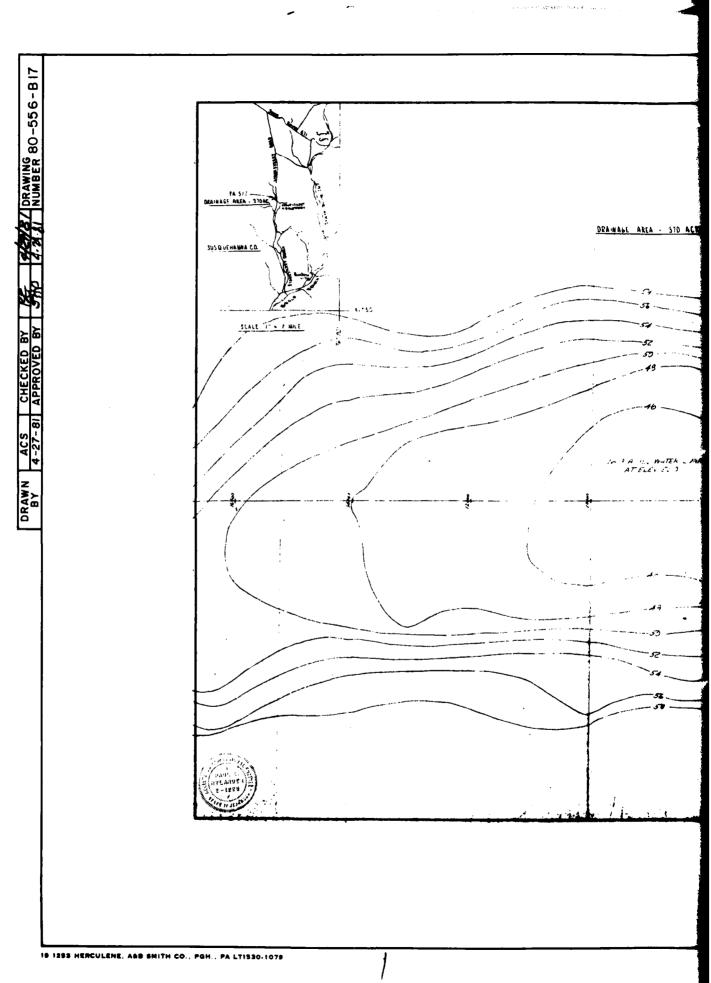
APPENDIX E

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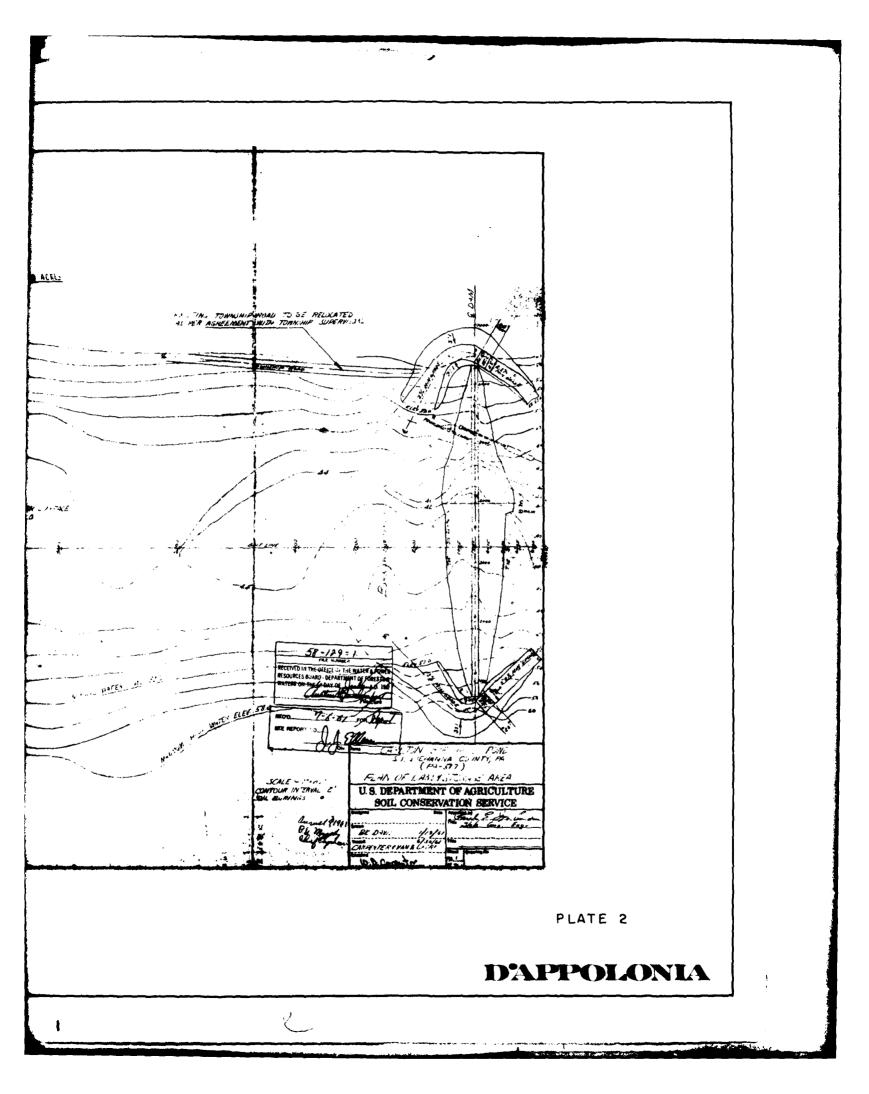
PLATES

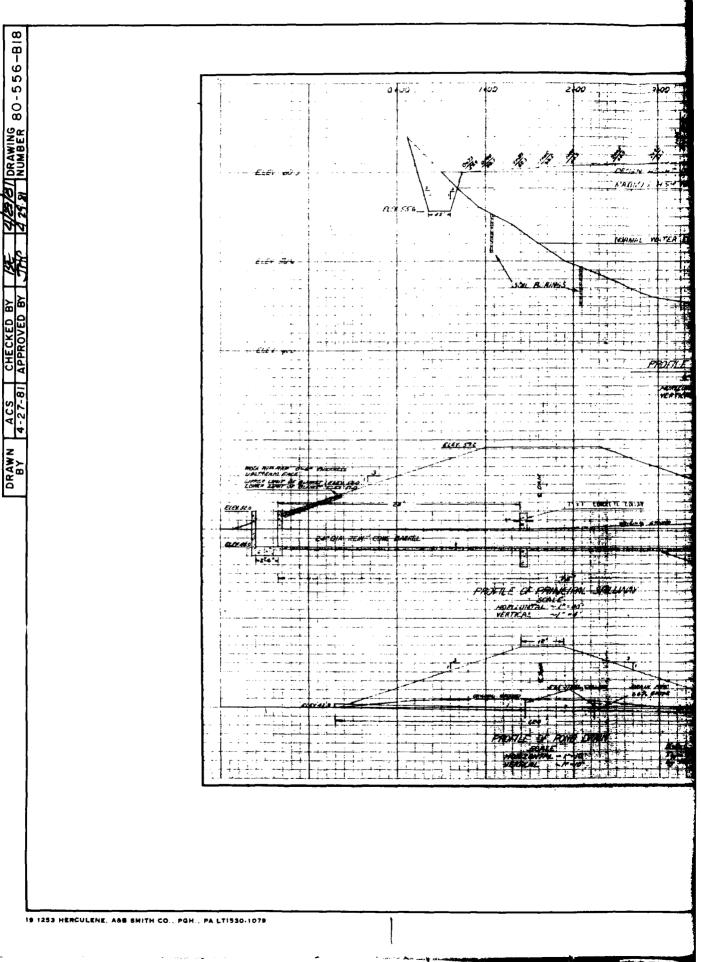






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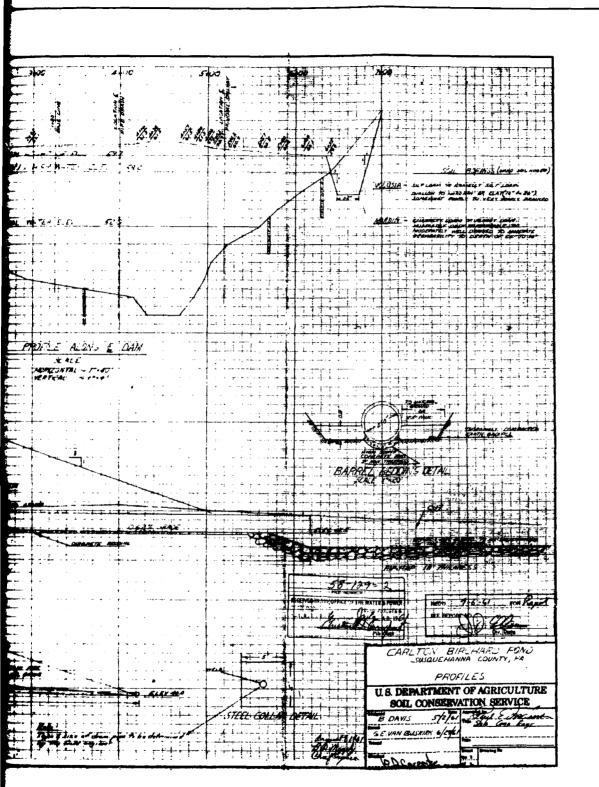
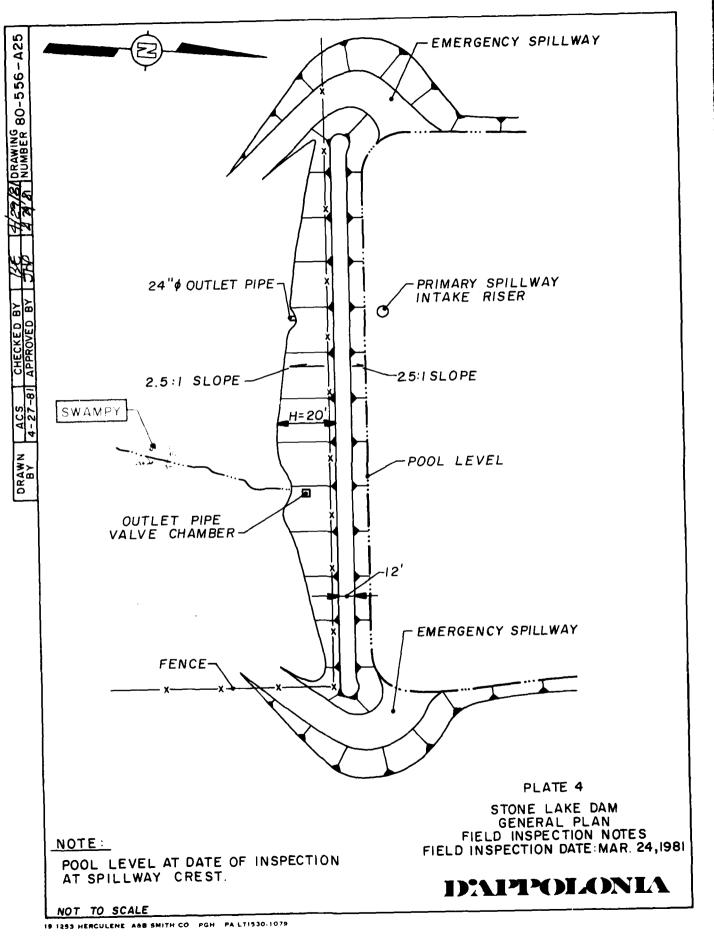
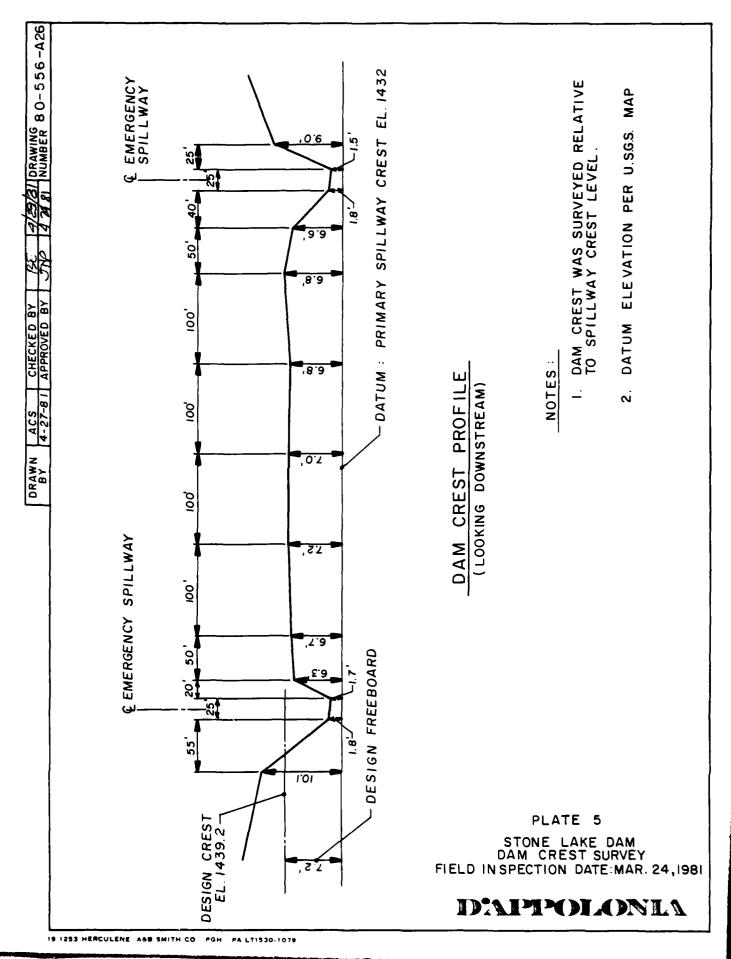


PLATE 3

DAPPOLONIA

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APPENDIX F

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REGIONAL GEOLOGY

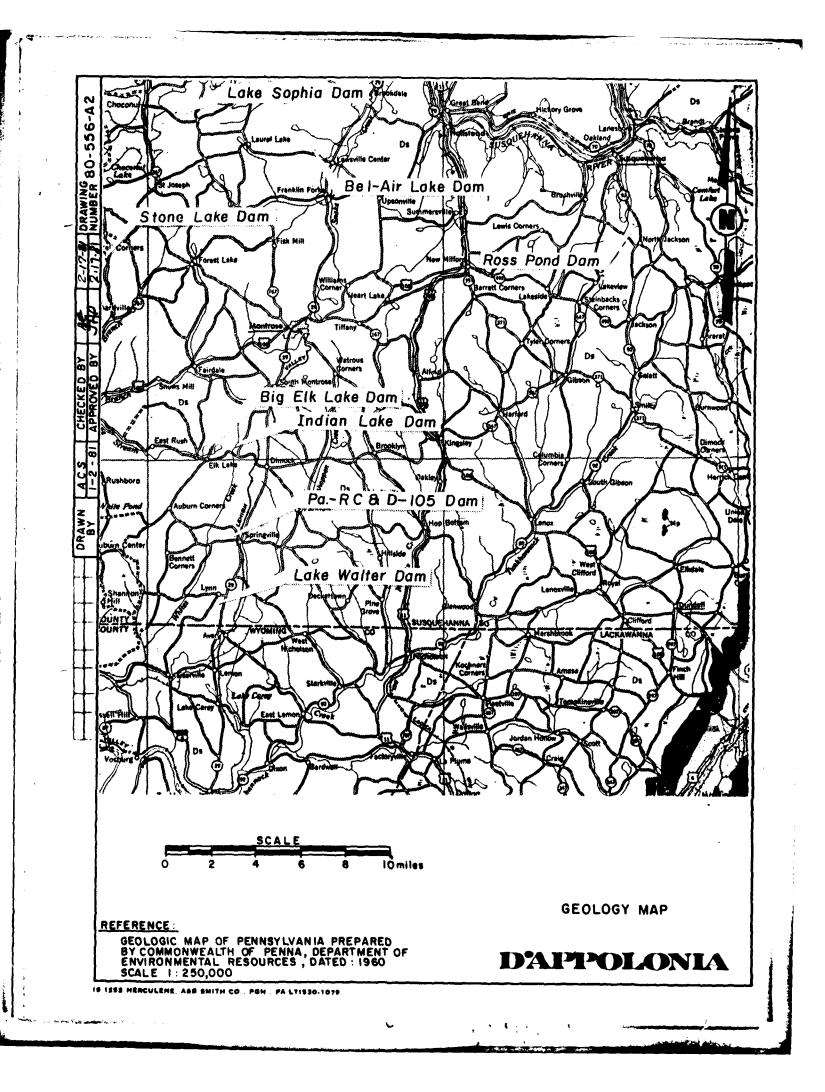
REGIONAL GEOLOGY STONE LAKE DAM

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The Stone Lake Dam is located in the glaciated low plateaus section of the Appalachian Plateau physiographic province, characterized as a mature glaciated plateau of moderate relief.

The geologic structure consists of a series of northeast trending folds (approximately N70°E) which plunge gently to the southwest. The dip of the limbs of the folds in the vicinity of the Stone Lake Dam is less than two degrees, with the southeast limb slightly steeper than the northwest limb. The dam is located south of the Rome Anticline and north of the Raysville Syncline. In general, the discontinuity trends are northeast and northwest.

The stratigraphy consists of glacial till which will range in thickness from very thin to approximately 200 feet. The glacial till is underlain by the Devonian Catskill Formation, which is approximately 1,800 feet thick in this area. The Catskill Formation is continental in origin, consisting of red shale and cross-bedded red and green sandstone and siltstone. The shale strata tend to weather rapidly when exposed.



		MISSISSIPPIAN
		MISSISSIPPIAN
	ALACHIAN PLATEAU Allegheny Group Curite sequences of anuitatione, shale, time- staine and could, numerous commercial could functione in theorem purit of architecture transmercial could functione in theorem purities architecture curite formative encoded Pottsville Group Predominantly sandatones and conglomer- alce with this shales and coals; some coals mineable locally. ANTHRACITE REGION Post-Pottsville Formations Brown or gray annelatones and shales with Rome conglomerate and numerous mine- able coals. Pottsville Group Light gray to while, coarse grained sand- mines and conglomerate with some mine- able coals.	Mauch Chunk Formation Red aboles with brown to groups from Ingge moniforms, includes Groups and Simerar counties, Layathouse Limedone at the base in another to remain and the base in another to remain endone at the base in another to remain endone Productionally gray, hard, mansue, cross- based considerers and annihilation with moniform Burgoon, Shenano, Chunhaga, Cuaseungo, Corry, and Koupp Forma- tions, includes and Koupp Forma- tions, includes and Formation.
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EFERENCE GEOLOGIC BY COMMC EN VI RONN	MAP OF PENNSYLVANIA PREPARED NWEALTH OF PENNA., DEPARTMENT OF ENTAL RESOURCES, DATED : 1960 : 250,000	GEOLOGY MAP LEGEND