



PREFACE

This report is prepared under guidance contained in the <u>Recommended</u> <u>Guidelines for Safety Inspection of Dams</u>, for Phase I Investigations. Copies of these guidelines may be obtained from the Department of the Army, Office of Chief of Engineers, Washington, D.C. 20314.

The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon visual observations and review of available data. Detailed investigations and analyses involving topographic mapping, subsurface investigations, material testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the inspection is intended to identify any need for such studies which should be performed by the owner.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of the dam depends on numerous and constantly changing internal and external factors which are evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The assessment of the conditions and recommendations was made by the consulting engineer in accordance with generally and currently accepted engineering principles and practices.

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

NAME OF DAM: Lake Sophia Dam STATE LOCATED: Pennsylvania COUNTY LOCATED: Susquehanna STREAM: Unnamed Creek, tributary of Choconut Creek SIZE CLASSIFICATION: Small HAZARD CLASSIFICATION: High OWNER: Mrs. Sophia Turoski DATE OF INSPECTION: March 23, 1981 and April 30, 1981

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ASSESSMENT: Based on the evaluation of existing conditions, the condition of Lake Sophia Dam is considered to be unsafe/nonemergency due to seriously inadequate spillway capacity.

Swampy areas were observed below the junction of the embankment and the abutments along both abutments. A seepage condition with precipitate was found to be associated with the swampy area along the right abutment toe. The outlet works discharge channel is blocked by debris. A beaver dam below the dam forms a pond that submerges the toe of the dam. Consequently, a portion of the downstream toe could not be adequately inspected for signs of seepage and concerns exist as to the effect of these conditions on the continued stability of the dam. Therefore, further investigation of the condition of the dam by a professional engineer and implementation of necessary remedial measures is recommended.

The spillway capacity was evaluated according to recommended criteria and found to be seriously inadequate. According to the recommended criteria, small dams in the high hazard category are required to pass from one-half to full Probable Maximum Flood (PMF). In view of the size and downstream damage potential, one-half PMF was selected as the spillway design flood. The flood discharge capacity was evaluated according to the recommended procedure and was found to pass approximately 15 percent of the PMF without overtopping the dam. Results of the breach analysis indicate that downstream damage would be significantly increased due to a dam failure. As a result, the flood discharge capacity of the spillway is classified to be seriously inadequate.

The following recommendations should be implemented immediately or on a continuing basis.

1. The owner should immediately retain a professional engineer to conduct additional studies to more accurately ascertain the spillway capacity and the nature and extent of improvements required to provide adequate spillway capacity. In the interim, the spillway weir should be immediately removed and the crest of the dam should be filled to the design level.

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Assessment - Lake Sophia Dam

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- 2. In conjunction with the above work, investigations should be undertaken to prepare and execute plans for controlling seepage along the downstream toe and for evaluating the structural integrity of the embankment in view of observed conditions.
- 3. The owner should confirm the operational condition of the outlet works and perform necessary maintenance, if found inoperative.
- 4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- 5. The owner should develop a formal operating and maintenance plan for the dam, inspect the dam regularly and perform necessary maintenance.



Lawrence D. Andersen, P.E. Vice President

<u>June 1, 1981</u> Date

Approved by:

JAMES W. PECK Colonel, Gorps of Engineers Commander and District Engineer

11 June 1981

Date:

LAKE SOPHIA DAM NDI I.D. PA-0078 DER 1.D. 058-126 MARCH 23, 1981



Upstream Face

1



Downstream Face

TABLE OF CONTENTS

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1 1

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Sec. 1

1. A. c

	PAGE
SECTION 1 - PROJECT INFORMATION	1
1.1 General	1
1.2 Description of Project 1.3 Pertinent Data	1
	_
SECTION 2 - DESIGN DATA	5
2.1 Design	5
2.2 Construction	6
2.3 Operation	6
2.4 Other Investigations	6
2.5 Evaluation	6
SECTION 3 - VISUAL INSPECTION	8
3.1 Findings	8
3.2 Evaluation	. 9
SECTION 4 - OPERATIONAL FEATURES	10
4.1 Procedure	10
4.2 Maintenance of the Dam	10
4.3 Maintenance of Operating Facilities	10
4.4 Warning System	10
4.5 Evaluation	10
SECTION 5 - HYDRAULICS AND HYDROLOGY	11
5.1 Evaluation of Features	11
SECTION 6 - STRUCTURAL STABILITY	13
6.1 Evaluation of Structural Stability	13
SECTION 7 - ASSESSMENT AND RECOMMENDATIONS/	
PROPOSED REMEDIAL MEASURES	14
7.1 Dam Assessment	14
7.2 Recommendations/Remedial Measures	14

TABLE OF CONTENTS (Continued)

APPENDIX A - CHECKLIST, VISUAL INSPECTION, PHASE I
 APPENDIX B - CHECKLIST, ENGINEERING DATA, DESIGN, CONSTRUCTION, OPERATION, AND HYDROLOGIC AND HYDRAULIC, PHASE I
 APPENDIX C - PHOTOGRAPHS
 APPENDIX D - HYDROLOGY AND HYDRAULICS ANALYSES
 APPENDIX E - PLATES
 APPENDIX F - REGIONAL GEOLOGY

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM LAKE SOPHIA DAM NDI I.D. PA-0078 DER I.D. 058-126

SECTION 1 PROJECT INFORMATION

1.1 General

a. <u>Authority</u>. The inspection was performed pursuant to the authority granted by The National Dam Inspection Act, Public Law 92-367, to the Secretary of the Army, through the Corps of Engineers, to conduct inspections of dams throughout the United States.

b. <u>Purpose</u>. The purpose of this inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project

a. Dam and Appurtenances. Lake Sophia Dam consists of an earth embankment approximately 340 feet long with a maximum height of 29 feet from the downstream toe and a crest width of 9 feet. The upstream side of the dam is protected by a small amount of riprap and the downstream face is covered with grass. The flood discharge facilities for the dam consist of a concrete open-channel spillway located near the left abutment. The spillway is a 35-foot-wide concrete rectangular channel. A one-foothigh concrete sill across the base of the spillway channel is the overflow section of the spillway. The overflow section is equipped with a 12-inchhigh steel plate weir. The spillway overflow section discharges into a concrete channel and then to the plunge pool at the toe of the dam, which in turn discharges into an earth channel. The outlet facilities consist of a 12-inch-diameter corrugated metal pipe extending through the embankment along the original streambed. The flow through the outlet pipe is controlled by a sluice at the upstream end and is operated by a valve stem supported by a concrete pier extending above lake level. This outlet facility constitutes the emergency drawdown system for the reservoir.

b. Location. Lake Sophia Dam is located on an unnamed creek, a tributary of Choconut Creek in the northwestern part of Silver Lake Township, Susquehanna County, Pennsylvania (N41° 58.3', W75° 58.7'). Plate 1 illustrates the location of the dam.

c. <u>Size Classification</u>. Small (based on 29-foot height and 164 acre-feet storage capacity).

d. <u>Hazard Classification</u>. The dam is classified to be in the high hazard category. Below the dam, the unnamed creek flows about

1.4 miles to Route 267 at the Village of Choconut where the stream joins the Choconut Creek. There are three houses, one store, and one mobile home near its confluence with Choconut Creek. In the event of a dam failure, it is estimated there would be extensive economic damage in this reach and the loss of more than a few lives is considered possible.

e. <u>Ownership</u>. Mrs. Sophia Turoski, R.D. #1, Box 92, Brackney, Pennsylvania 18812.

f. Furpose of Dam. Recreation.

g. <u>Design and Construction History</u>. The dam was designed by Scandale and Associates Consulting Engineers of Scranton, Pennsylvania. Construction of the dam was completed in 1957.

h. Normal Operating Procedure. The reservoir is normally maintained at the spillway flashboard crest level (Elevation 1402, USGS Datum), leaving 2.8 feet of freeboard to the top of the dam at Elevation 1404.8. All inflow occurring when the reservoir level is at the spillway crest elevation or above is discharged over the uncontrolled spillway.

1.3 Pertiment Data. Elevations referred to in this and subsequent sections of the report were calculated based on field measurements, assuming the flashboard crest of the spillway to be at Elevation 1402 (USGS Datum), which is the elevation shown as the normal pool elevation on the USGS 7.5-minute Laurel Lake PA-NY quadrangle. Elevations shown in design drawings do not appear to be relative to USGS Datum. In the design drawings, the normal pool level is shown to be at Elevation 1467.2.

a Drainage Area

2

1.47 square miles(1)

Unknown

Unknown

540

540

Not applicable

- b. Discharge at Dam Site (cfs)
- Maximum known flood at dam site Outlet conduit at maximum pool Gated spillway capacity at maximum pool Ungated spillway capacity at maximum pool Total spillway capacity at maximum pool

c. Elevation (USGS Datum) (feet)

Top of dam

Maximum pool Normal pool (with flashboard) Spillway crest (without flashboard) Upstream invert outlet works 1404.8 (low spot) 1406.0 (as designed) 1404.8 1402.0 1401.0 Unknown

⁽¹⁾Draimage area planimetered from USGS topographic map is 1.4 square miles. State records indicate the draimage area to be 1.47 square miles.

	Downstream invert outlet works Maximum tailwater Toe of dam	137 <u>5+</u> (2) Unknown 1376 <u>+</u>
d.	Reservoir Length (feet)	
	Normal pool level Maximum pool level	800 <u>+</u> 1100 <u>+</u>
e.	Storage (acre-feet)	
	Normal pool level (with flashboard) Maximum pool level (measured low point)	120 164
f.	<u>Reservoir Surface (acres)</u>	
	Normal pool level (with flashboard) Maximum pool level (measured low point)	13.8 ⁽³⁾ 19.1
g.	Dam	
	Type Length Height Top width Side slopes Zoning Impervious core Cutoff Grout curtain	Earth embankment 340 feet 29 feet 9 feet Downstream: 2.5H:1V (as designed), 2.0H:1V (as measured) Upstream: Not determinable Yes Yes Yes No
h.	Regulating Outlet Type Length Closure Access Regulating facilities	12-inch-diameter corrugated metal pipe 130 <u>+</u> feet (measured from design drawings) 12-inch gate valve By boat Upstream valve

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 ⁽²⁾Downstream end of the pipe could not be located. Elevation is estimated.
 (3)Planimetered from USGS topographic map. Design drawing indicates the lake area at EL. 1401 to be 6.5 acres (without flashboard) or 10.0 acres at top of dam El. 1406.

i. Spillway

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Length

Crest elevation (flashboard) Upstream channel Downstream channel Concrete overflow with steel plate flashboard. 35 feet (perpendicular to flow) 1402.0 Lake Concrete channel, plunge pool and then earth channel.

SECTION 2 DESIGN DATA

2.1 Design

a. <u>Data Available</u>. The available data consist of files provided by the Commonwealth of Pennsylvania, Department of Environmental Resources (PennDER), which contain design drawings, correspondence and inspection reports.

(1) <u>Hydrology and Hydraulics</u>. Review of the information in the Commonwealth of Pennsylvania files showed that there are no original hydrology and hydraulic design data available for the dam. However, a state inspection report entitled "Report Upon the Application of Frank Turoski," dated August 26, 1957, contains the criteria used to size the spillway.

(2) <u>Embankment</u>. The available information consists of design drawings.

(3) <u>Appurtemant Structures</u>. The available information consists of design drawings.

b. Design Features

(1) Embankment. As designed, the dam is a homogeneous fill with an impervious core along the center line of the embankment, extending for the full length of the earth embankment. The core starts one foot below the crest of the dam and extends into the foundation through a seven-foot-deep cutoff trench. Plates 2 and 3 show the plan and typical cross section of the dam. The core is four feet wide on the top and ten feet wide at the original ground, below which a cutoff trench ten feet wide and seven feet deep was excavated. The specifications required that the core material consist of hardpan thoroughly mixed and compacted. Fill material was to be placed in horizontal layers eight inches in depth, each layer thoroughly incorporated with the material already in place. No internal drainage system was incorporated in the embankment design.

The embankment was designed to have a 2.5:1 (horizontal to vertical) slope on both upstream and downstream faces and a crest width of nine feet. The upstream face of the dam was to be covered with 12-inch hand-placed dry stone riprap not less than 12 inches deep.

(2) <u>Appurtement Structures</u>. The appurtement structures consist of a concrete open channel spillway located on the left abutment and the outlet works located near the center of the embankment. Details of the spillway are shown in Plates 2, 3 and 4. As designed, the spillway is a rectangular channel, 35 feet wide and five feet deep, at the control section. A concrete sill across the base of the channel constitutes the overflow section. The overflow section is equipped with a l2-inch-high steel plate flashboard. The spillway discharge channel also is a rectangular concrete channel which terminates at a plunge pool 45 feet downstream from the overflow section. In the foundation of the spillway, a one-foot-thick, five-footdeep cutoff wall extending to impervious material was provided to control seepage.

The outlet works consist of a l2-inch-diameter corrugated metal pipe encased in concrete. The upstream end of the pipe is attached to a concrete pier which supports a sluice gate. Details of the outlet works are shown on Plate 3.

c. Design Data

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(1) <u>Hydrology and Hydraulics</u>. A Commonwealth of Pennsylvania report entitled "Report Upon the Application of Frank Turoski," dated August 26, 1957, indicates that the spillway was sized to pass a discharge of 1377 cfs with the water level two inches below the top of the dam and 1467 cfs with the water level at the top.

(2) <u>Embankment</u>. No engineering data are available on the design of the embankment.

(3) <u>Appurtement Structures</u>. No engineering data are available on the appurtement structures.

2.2 <u>Construction</u>. Available information indicated that construction of the dam was completed in 1957. To the extent that can be determined at this time, the dam appears to be higher than indicated in the design drawing. The design drawing shows the height of the dam to be 24 feet measured from the dam crest to the downstream invert of the outlet works. Field measurement indicates the height of the dam to be approximately 29 feet. Further, the slopes of the dam were designed to be 2.5H:1V, but field measurements indicate a downstream slope of 2H:1V.

2.3 Operation. There are no formal operating records maintained for the dam.

2.4 <u>Other Investigations</u>. The available information indicated no investigations other than the periodic inspections conducted by the state. The last state inspection was conducted in October 1964.

2.5 Evaluation

a. <u>Availability</u>. The available information was provided by the Commonwealth of Pennsylvania, Department of Environmental Resources.

b. Adequacy

(1) <u>Hydrology and Hydraulics</u>. The available information is limited. Only the watershed area reservoir volume and design discharge capacity of the spillway are reported. (2) Embankment. Other than design drawings, no other data is available to assess the adequacy of the embankment design. No reference was found to indicate whether the design included slope stability and seepage analyses. However, the design does incorporate such basic components as an impervious cutoff trench and riprap protection of the upstream slope of the dam.

(3) <u>Appurtement Structures</u>. Review of the design drawings indicate no significant deficiencies that would affect the structural performance of the appurtement structure.

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SECTION 3 VISUAL INSPECTION

3.1 Findings

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a. <u>General</u>. The onsite inspection of Lake Sophia Dam consisted of:

- 1. Visual inspection of the embankment, abutments, and embankment toe.
- 2. Visual examination of the spillway and its components.
- 3. Evaluation of downstream area hazard potential.

The specific observations are illustrated in Plate 5.

b. <u>Embankment</u>. The general inspection of the embankment consisted of searching for indications of structural distress, such as cracks, subsidence, bulging, wet areas, seeps and boils, and observing general maintenance conditions, vegetative cover, erosion, and other surficial features.

In general, the condition of the embankment is considered to be fair. No major signs of distress such as slumps or cracks were found. However, extensive swampy areas were observed below the junction of the embankment with the abutments, which raised concern as to the effect of this apparent underseepage on the continued stability of the dam. A seepage in the amount of 10 to 20 gallons per minute was found to be associated with the swampy area on the right abutment. Precipitate was observed in the right abutment seepage. No measurable seepage was observed in the left abutment swampy area. Further, a portion of the toe of the dam was submerged by a pond formed by debris and a beaver dam blocking the outlet pipe discharge channel. This condition precluded inspection of the vicinity of the downstream end of the outlet pipe for possible seepage. Some shoreline erosion was observed along the upstream slope. Riprap on the upstream slope has partially dislocated and is not effective for controlling erosion, due to wave action.

The top of the dam was surveyed relative to the spillway crest elevation and the center of the dam was found to have apparently settled. While the design freeboard for the dam was 4 feet, the field survey indicated a freeboard of 2.8 feet between the low spot near the right embankment and the normal pool level.

c. <u>Appurtenant Structures</u>. The appurtenant structures were examined for deterioration or other signs of distress and obstructions that would limit flow. In general, the structures were found to be in fair condition. Steel I-beams were placed across the top of the spillway discharge channel, apparently to prevent tilting of the side walls of the channel. Some structural cracks were observed in the side walls of the spillway discharge channel. Riprap in the spillway plunge pool was found to be in poor condition. It appears that the spillway discharge channel below the concrete section was not constructed in accordance with the design drawings which included a riprap channel extending to the original streambed. The operational condition of the outlet works could not be observed. The downstream end of the outlet pipe was submerged in ponded water and could not be inspected.

d. <u>Reservoir Area</u>. A map review indicates that the watershed is predominantly wood and pasturelands. A review of the regional geology is included in Appendix F.

e. <u>Downstream Channel</u>. The downstream channel flows approximately 1.4 miles to a highway bridge of Route 267 at the Village of Choconut. Further description of the downstream conditions is included in Section 1.2 d.

3.2 Evaluation. The condition of Lake Sophia Dam is considered to be fair. Although no major signs of distress were noted, in view of the seepage condition and apparent settlement of the embankment, further detailed evaluation of the condition of the dam by a professional engineer is recommended. Plans should be prepared to control the seepage conditions. In conjunction with this work, necessary work should be performed to restore the outlet facilities.

SECTION 4 OPERATIONAL FEATURES

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4.1 <u>Procedure</u>. There are no formal operating procedures for the dam. The reservoir is normally maintained at the top of the spillway flashboards with excess inflow discharging over the uncontrolled spillway.

4.2 <u>Maintenance of the Dam</u>. The maintenance condition of the dam is considered to be good. It appears that grass on the crest and downstream face is periodically mowed.

4.3 <u>Maintenance of Operating Facilities</u>. The only operating facility for the dam is the outlet pipe valve. The pier supporting the controls was unaccessible. Operation of the gate was not observed.

4.4 <u>Warning System</u>. No formal warning system exists for the dam. Telephone communication facilities are available via residences at the dam site.

4.5 <u>Evaluation</u>. Although the maintenance condition of the embankment is considered to be good, the operating facilities are considered to be in poor condition. Evaluation of the operational condition of the outlet facilities are required.

SECTION 5 HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features

a. <u>Design Data</u>. Lake Sophia Dam has a watershed area of 1.47 square miles and impounds a reservoir with a surface area of 13.8 acres at normal pool level. Flow discharge facilities for the dam consist of a 35-foot-wide overflow spillway equipped with a 12-inch-high weir. Based on the available head relative to the low spot on the left embankment, the capacity of the spillway is estimated to be 540 cfs with no freeboard.

b. Experience Data. As previously stated, Lake Sophia Dam is classified as a small dam in the high hazard category. Under the recommended criteria for evaluating emergency spillway discharge capacity such impoundments are required to pass flows from one-half to full PMF. In view of the size and evaluation of the downstream damage potential, one-half PMF was selected as the spillway design flood.

The PMF inflow hydrograph for the reservoir was determined utilizing the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army, Corps of Engineers. The data used for the computer analysis are presented in Appendix D. As determined by the computer program, the one-half and full PMF inflow hydrograph has a peak of 1956 cfs and 3911 cfs, respectively. Computer input and a summary of computer output are also included in Appendix D.

c. Visual Observations. On the dates of the inspections, no conditions were observed that would indicate that the spillway capacity would be significantly reduced in the event of a flood. It appears that the steel weir across the spillway might not fail under full spillway flow.

d. <u>Overtopping Potential</u>. Various percentages of the PMF inflow were routed through the reservoir and it was found that the dam can pass 15 percent of the PMF without overtopping the dam. For 50 percent of the PMF, it was found that the low area on the embankment would be overtopped for a duration of 5.25 hours with a maximum depth of 1.3 feet. It is estimated that overtopping of the dam by approximately 0.5 foot would initiate breaching of the dam. A further analysis indicates that if the steel weir is removed and the crest of the dam filled to design level, the dam would pass approximately 40 percent of the PMF.

e. <u>Spillway Adequacy</u>. Since the dam cannot pass the recommended design flood of one-half the PMF without overtopping the dam, the flood discharge capacity is classified to be inadequate. A breach analysis was conducted to analyze whether failure resulting from overtopping would significantly increase the potential for loss of life or damage over that which would exist just before overtopping failure. For breach analyses, a trapezoidal breach was assumed with a 200-foot bottom width, 2H:1V side slopes, and a depth of 26 feet. The duration of failure was taken as 0.75 hour, and it was assumed that the breaching would initiate when the dam is overtopped by 0.5 foot. It was found that the dam would be overtopped by 0.5 foot during the passage of 25 percent of the PMF. The computer outputs for the breach analysis are included in Appendix D.

Review of the flood stages in the Village of Choconut resulting from failure of Lake Sophia Dam indicates that while the discharge from the dam before failure (920 cfs, 25 percent of the PMF) would be essentially within the banks of the stream, after failure the discharge from the dam would increase to about 5326 cfs, overtopping the stream banks by about 2.9 feet. This increase is considered to pose a significant increase in downstream damage potential. Therefore, the flood discharge capacity of Lake Sophia Dam is considered to be seriously inadequate.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

(1) <u>Embankment</u>. As discussed in Section 3, in view of the observed swampy and seepage conditions along the downstream toe of the dam and the fact that the embankment design does not include an internal drainage system for controlling the effects of seepage, a concern exists as to the effect of the observed conditions on the continued stability of the dam. Although at this time, no signs of major distress such as cracks, bulging and slumps were observed, detailed evaluation of the seepage conditions by a professional engineer is considered advisable. The dam appears to have settled. This condition should also be evaluated in conjunction with the above recommended work.

(2) <u>Appurtemant Structures</u>. Although some structural cracking was observed on the side walls of the spillway discharge channel, the overall structural condition is considered to be satisfactory. No portions of the outlet facilities were visible to assess their structural conditions.

b. Design and Construction Data

(1) Embankment. The available design and construction information does not provide any quantitative data to aid in the assessment of stability. However, as previously noted, concerns exist as to the continued stability of the dam in view of the observed seepage and swampy conditions. Further detailed investigation of the stability of the dam is considered to be required.

(2) <u>Appurtement Structures</u>. Other than design drawings, no design and construction data exists for the appurtement structures. Review of these drawings indicated no apparent structural deficiencies that would significantly affect the performance of the appurtement structures.

c. Operating Records. None available.

d. <u>Postconstruction Changes</u>. It appears that the spillway flashboards were installed after the completion of the dam.

e. <u>Seismic Stability</u>. The dam is located in Seismic Zone 1; and based on visual observations, the static stability of the dam is considered to be questionable. Therefore, seismic stability of the dam should also be evaluated in conjunction with further investigation of the dam.

SECTION 7 ASSESSMENT AND RECOMMENDATIONS/PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. Assessment. In view of the seriously inadequate spillway capacity, the condition of Lake Sophia Dam is classified to be unsafe/ nonemergency. The condition of the embankment is considered to be fair. Seepage and swampy conditions were observed below the toe of the dam, raising concern relative to the continued stability of the dam. Further detailed investigation of the dam by a professional engineer is recommended.

The spillway was evaluated according to the recommended procedure and was found to pass 15 percent of the PMF without overtopping the dam. This capacity is less than the spillway design flood of one-half PMF. Results of the breach analysis indicate that downstream damage would be significantly increased due to a dam failure and, as a result, the spillway is classified as seriously inadequate.

b. <u>Adequacy of Information</u>. The available information, in conjunction with visual observations, is considered to be sufficient to make a Phase I evaluation.

c. <u>Urgency</u>. The following recommendations should be implemented as soon as possible or on a continuing basis.

d. <u>Necessity for Additional Investigations</u>. In view of the seriously inadequate spillway capacity, the owner should retain a professional engineer to determine the nature and extent of improvements required to provide an adequate spillway and to prepare and execute plans for controlling the seepage conditions and evaluating the stability of the dam.

7.2 Recommendations/Remedial Measures. It is recommended that:

- 1. The owner should immediately retain a professional engineer to conduct additional studies to more accurately ascertain the spillway capacity and the nature and extent of improvements required to provide adequate spillway capacity. In the interim, the spillway weir should be immediately removed and the crest of the dam should be filled to the design level.
- 2. In conjunction with the above work, investigations should be undertaken to prepare and execute plans for controlling seepage along the downstream toe and for evaluating the structural integrity of the embankment in view of observed conditions.

- 3. The owner should confirm the operational condition of the outlet works and perform necessary maintenance, if found inoperative.
- 4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of an emergency.
- 5. The owner should develop a formal operating and maintenance plan for the dam, inspect the dam regularly and perform necessary maintenance.

APPENDIX A

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CHECKLIST VISUAL INSPECTION PHASE I APPENDIX A

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CHECKLIST VISUAL INSPECTION PHASE I

NAME OF DAM <u>Lake Sophia</u> TYPE OF DAM <u>Earth</u>	na AZARD CAT
DATE(S) INSPECTION March 23, 1981	WEATHER <u>Cloudy</u> TEMPERATURE <u>40</u>
POOL ELEVATION AT TIME OF INSPECTION 1402 (Top of Flashboard)	1402 M.S.L. TAILWATER AT TIME OF INSPECTION 1376^{\pm} M.S.L.
INSPECTION PERSONNLL: RE	REVIEW INSPECTION PERSONNEL: (April 30, 1981)
Arthur Smith	Lawrence D. Andersen
Wah-Tak Chan	James H. Poellot
Bilgin Erel	Bilgin Erel
Owner's Representative:	Bilgin Erel RECORDER
None	

Page Al of 9

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VISUAL INSPECTION PHASE I EMBANKMENT

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REMARKS OR RECOMMENDATIONS					Adequate shoreline erosion protection (e.g., riprap) should be provided along the upstream slope of the dam.
CENERALIANI OBSERVATIONS	None observed.	None observed.	None observed.	See Plate 6 for dam crest profile. No significant horizontal misalignment observed.	Existing riprap is not effective against wave action.
VISUAL EXAMINATION OF	SURFACE CRACKS	UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	SLOUGHING OR FROSTON OF Embankment and abutment Slopes	VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	RIPRAP FAILURES

Page A2 of 9

VISUAL INSPECTION PHASE I

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	REMARKS OR RECOMMENDATIONS		Further investigation of this condition is recommended.			
EMBANKMENT	OBSERVATIONS	No problem observed.	Swampy areas below the toe of the dam along both abutments. See Plate 5 for location.	None	None observed.	
	VISUAL EXAMINATION OF	JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	ANY NOTICEABLE SEEPAGE	STAFF GAGE AND RECORDER	DRAINS	

Page A3 of 9

Further investigation of this condition is recommended. REMARKS OR RECOMMENDATIONS Swampy areas below the toe of the dam along both abutments. See Plate 5 for location. VISUAL INSPECTION EMBANKMENT OBSERVATIONS PHASE I No problem observed. None observed. None STAFF GAGE AND RECORDER ANY NOTICEABLE SEEPAGE JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM VISUAL EXAMINATION OF DRAINS

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Page A3 of 9

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REMARKS OR RECOMMENDATIONS				The pond in the outlet channel should be drained.	Operational condition of the outlet pipe gate should be confirmed by the owner.
OBSERVATIONS	Downstream end of the outlet pipe is submerged. Not visible.	Submerged. Not visible.	None	Earth channel. Channel is blocked by debris and a beaver dam, ponding water in the channel.	Upstream end sluice gate. Operating equipment accessible by boat only. Operation of the gate not observed.
VISUAL EXAMINATION OF	CRACKING AND SPALLING DF CONCRETE SURFACES IN OUTLET CONDUIT	INTAKE STRUCTURE	OUTLET STRUCTURE	OUTLET CHANNEL	EMERGENCY GATE

Page A4 of 9

VISUAL INSPECTION PHASE I OUTLET WORKS

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VISUAL INSPECTION PHASE I UNGATED SPILLWAY

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	REMARKS OR RECOMMENDATIONS	The flashboard should be removed.			-	
UNGATED SPILLWAY	OBSERVATIONS	Concrete overflow section equipped with a 12-inch steel plate flashboard.	Lake. No problems observed.	Rectangular concrete channel in fair condition.	None	
	VISUAL EXAMINATION OF	CONCRETE WEIR	APPROACH CHANNEL	DISCHARGE CHANNEL	BRIDGE AND PIERS	

Page A5 of 9

REMARKS OR RECOMMENDATIONS OBSERVATIONS The dam has no gated spillway. None None None None VISUAL EXAMINATION OF GATES AND OPERATION EQUIPMENT DISCHARGE CHANNEL APPROACH CHANNEL CONCRETE SILL BRIDGE PIERS

VISUAL INSPECTION PHASE I GATED SPILLWAY

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Page A6 of 9

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	REMARKS OR RECOMMENDATIONS							
PHASE I INSTRUMENTATION	OBSERVATIONS	None		None	None	None	None	Page A7 of 9
	VISUAL EXAMINATION OF	MONUMENTATION/SURVEYS		OBSERVATION WELLS	WEIRS	 PI EZOMETERS	OTHER	

VISUAL INSPECTION PHASE I INSTRUMENTATION

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	REMARKS OR RECOMMENDATIONS					
VISUAL INSPECTION PHASE I RESERVOIR	OBSERVATIONS	No problems observed.	Unknown	None		Page A8 of 9
	VISUAL EXAMINATION OF	SLOPES	SEDIMENTATION	UPSTREAM RESERVOIRS		

والمعرب والمتركما تعراقهما أأطرو وروافت فتستعطف المتحرثات ستاريه فخلطت

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VISUAL INSPECTION PHASE I DOWNSTREAM CHANNEL

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VISILAL EXAMINATION OF	DOWNSTREAM CHANNEL OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	No problems observed.	
slopes	No problems observed.	
APPROXIMATE NUMBER OF HOMES AND POPULATION	Village of Choconut is about 1.4 miles downstream from the dam. Population: 10 to 20.	
		-

Page A9 of 9

APPENDIX B

CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION AND HYDROLOGIC AND HYDRAULIC PHASE I

States Street

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NDI: PA-0078 058-126 NAME OF DAM Lake Sophia Construction was completed in November 1957. The dam was designed by V. S. Scandale and N. C. Scandale, professional engineers. DER: #QI Three design drawings are available in state files. REMARKS CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I Page B1 of 5 APPENDIX B See Plates 2, 3 and 4. See Plate 3. See Plate 1. DETAILS
 CONSTRAINTS
 DISCHARGE RATINGS TYPICAL SECTIONS OF DAM REGIONAL VICINITY MAP CONSTRUCTION HISTORY S-BUILT DRAWINGS – PI.AN OUTLETS ITEM

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CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

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	REMARKS
RAINFALL/RESERVOIR RECORDS	None
DESIGN REPORTS	None
GEOLOGY REPORTS	None
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	Limited hydrology and hydraulics calculations are available in state files.
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	None reported
	Page B2 of 5

REMARKS Unknown Unknown None None None POST CONSTRUCTION SURVEYS OF DAM MONITORING SYSTEMS HIGH POOL RECORDS BORROW SOURCES MODIFICATIONS ITEM

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Page B3 of 5

CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

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ITEM	REMARKS
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None reported.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported.
MAINTENANCE OPERATION RECORDS	No maintenance records kept for the dam.
SPILLWAY PLAN SECTIONS DETAILS	See Plate 4.
OPERATING EQUIPMENT PLANS AND DETAILS	See Plates 3 and 4.
	Page B4 of 5

CHECKLIST ENGINEERING DATA HYDROLOGIC AND HYDRAULIC

DRAINAGE AREA CHARACTERISTICS: Partly wooded and pastureland
ELEVATION, TOP OF NORMAL POOL AND STORAGE CAPACITY: <u>1402 (120 acre-feet</u>)
ELEVATION, TOP OF FLOOD CONTROL POOL AND STORAGE CAPACITY: 1404.8 (164 acre-feet)
ELEVATION, MAXIMUM DESIGN POOL: 1406 (design top of dam)
ELEVATION, TOP OF DAM:1404.8 (low spot)
SPILLWAY:

a. Elevation 1401, top of flashboard 1402

- b. Type <u>Sharp crested overflow section</u>
- c. Width <u>35 feet (perpendicular to flow direction)</u>
- d. Length 45 feet
- e. Location Spillover <u>Near left abutment</u>

f. Number and Type of Gates <u>None</u>

OUTLET WORKS:

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- a. Type <u>12-inch corrugated metal pipe</u>
- b. Location <u>Near center of dam, along original streambed</u>
- c. Entrance Inverts<u>Unknown</u>
- d. Exit Inverts Unknown

e. Emergency Drawdown Facilities <u>12-inch-diameter corrugated met</u>al pipe HYDROMETEOROLOGICAL GAGES:

- a. Type<u>None</u>_____
- b. Location None
- c. Records<u>None</u>

MAXIMUM NONDAMAGING DISCHARGE: 540 cfs existing spillway capacity

Page B5 of 5

APPENDIX C

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PHOTOGRAPHS

LIST OF PHOTOGRAPHS LAKE SOPHIA DAM NDI I.D. NO. PA-0078 MARCH 23, 1981

PHOTOGRAPH NO.

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1

DESCRIPTION

1	Dam crest (looking south).
2	Dam crest (looking north).
3	Spillway overflow section, note steel plate flashboards.
4	Spillway wall.
5	Downstream slope of dam and spillway.
6	Gate stem.
7	Ponded water at toe of dam.
8	Houses approximately 1.4 miles downstream from dam.



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APPENDIX D

HYDROLOGY AND HYDRAULICS ANALYSES

HYDROLOGY AND HYDRAULIC ANALYSIS Data base

NAME OF DAM: Lake Sophia Dam

PROBABLE MAXIMUM PRECIPITATION (PMP) = 22.2 INCHES/24 HOURS

STATION	1	2	3	4	5
Station Description	Lake Sophia	Lake Sophia Dam			
Drainage Area (square miles)	1.47	-			
Cumulative Drainage Area (square miles)	1.47	1.47			
Adjustment of PMF for Drainage Ares (%)(1)	947				
6 Hours	117	-			
12 Hours	127	-	1		
24 Hours	136	-	1		
48 Hours	142	-			
72 Hours	145	-			
Snyder Hydrograph Parameters					
Zone ⁽²⁾	11A	-			
c _p /c _t (3)	0.62/1.50	-	}		
L (miles)(4)	1.65	-			
L _{ca} (miles) ⁽⁴⁾	0.51	-			
$t_p = C_t (L \cdot L_{ca})^{0.3} \text{ (hours)}$	1.42	-			
Spillway Data	<u> </u>	<u> </u>	<u> </u>		
Crest Length (ft)	-	35.0	1		1
Freeboard (ft)	-	2.8			
Discharge Coefficient	-	3.3			
Exponent	-	1.5			

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(4) L = Length of longest water course from outlet to basin divide. L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.

ELEVATION	AH, FEET	AREA (acres)(1)	AVOLUME (acre-feet)(2)	STORAGE (acre-feet)
1420.0		47.8		643.6
1402.0	18.0	13.8	524.0	119.6
1376.0	26.0	0	119.6	0

STORAGE VS. ELEVATION

(1) Planimetered from USGS maps.

(2) $\Delta Volume = \Delta H/3 (A_1 + A_2 + \sqrt{A_1A_2}).$

COMPUTER INPUT PAGE D2 OF 10

450.0 SNYDER UNIT HYDROGRAPH, SPILLUAY, OVERTOPPING AND DAM BREACH ANALYSES Lake Sophia Dam, Ider 58-1261, susquehenna county, pa. project NO.80-556-19 Fon 15x,25x,50x,60x,80x, and 100x probable maximum flodd (pmf)] 0 15 0 -4 0 1260.0 1090.0 0-0146 LAKE SOPHIA DAM. (DER 58-126) 74+653 CHANNEL ROUTING USING MODIFIED PULS: REACH 1 (STATION 0+00 TO 34+00) 350.0 375.0 425.0 1406.0 1406.4 1406.5 300.0 0.66 2 CHANNEL ROUTING USING MODIFIED PULS: REACH 2 (STATION 34+00 0.5 1280.0 1090.0 0.0390 200.0 0.0590 91.0 ROUTING FLOW THROUGH LAKE SOPHIA DAM+(DER 58-126) 1 1:0 --1402.0 DF SNYDER INFLON HYDROGRAPH TO 1.47 117 127 136 142 3400 •0 1290 •0 1300 •0 325 0 1405 8 1420 0 1465 3 4065.0 1095.0 1120.0 1.00 300.0 1405.5 1402.0 1269.5 100.0 450.0 1099.5 90.0 1050.0 0.80 1090.0 1100.0 1100.0 1260.0 1290.0 1280.0 450.0 200.0 0.75 09-0 1.5 0-045 80-0 390-0 0.035 50.0 250.0 47.8 1420.0 3.3 1.5 1.5 150.0 1405.3 1380.0 1380.0 0.50 2.0 CALCULATION 13.8 1402.0 35.0 100.0 1404.9 0.045 1300.0 1260.0 0.040 1120.0 1095.0 0.0 ہ 0.25 -0-05 20.9 FLOOD HYDHOGRAPH PACKAGE (HEC-1) Dan Safety Version July 1978 Last Moulfication (1) APR UI) ******************************* -68 200.00. Y7 0.0 Y7 310.0 100.0 99 **c1.**0 76 0-045 77 0-0 Y6 0-045 Y7 0-045 20 1.42 0-0 5 ~ _ LE1376.0 \$\$1402.0 601404.8 50.0 SV1404.8 \$8 2U0.0 Ţ ĩ γ Υ A2 Α5 a 5 5 ± ī Ξ 5 2 11 ΞE 7 × ۵ ****C=~~?

FLOOD ROUTING SUMMARY PAGE D3 OF 10

3911. 110.75) (3911. 110.75) (3867. 109-5016 5950-3881. 109.9134 6025. 168-4936 109.8434 170-623 (10 ¢ 181.673 3879. 6416. RATIO 3129. 88.60)(3102. 87.84)(5768. 163.33)(3129. 88.60)(3092. 87.5531 5677. 160.7531 87.8636 174-6536 RATIOS APPLIED TO FLOUS Ratio 3 Ratio 4 Ratio 5 •50 •60 •80 6168. 3103. 2318. 65.6316 5715. 161.7616 2347. 06.45)(2347. 66.45)(2319. 65.6716 5708. 161-6426 65.8416 174.5936 2325. 6166. 54.80) (6541. 1956. 55.38) (1928. 54.60)(6081. 54.7016 185.2234 172.1914 55.3836 172-8034 1932. 1956. 1935. 923. 26.13)(5108. 144.64)(26.26)(5662. 160.32)(922. 26.10)(5326. 150.81)(978. 27.6911 27.691(978. 927. RATIO 1 RATIO 2 •15 •25 587. 16.61)(14.12) (499. 14.12) (501. 14.18) (501. 587. 16.61)(14.1736 14.18) (14.1726 501. 501. 499. PLAN N 1.47 1.47 1.47 AREA 1.47 m STATION MYDROGRAPH AT OPER ATION ROUTED TO ROUTED TO ROUTED TO

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PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS flows in cubic feet per second (cubic meters per second) area in sourke miles (square Kilometers)

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SUMMARY

PLAN 1

	TINE OF Failure Hours			TIME OF Fatlure Mours	0.00 41.00 40.00 39.50 39.75 39.75
TOP OF DAM 1404-80 164- 541-	TIME DF Max Outflou Hours	41.75 41.25 41.25 41.25 41.25	TOP OF DAM 1404-80 164- 541-	TIME DF Max Outflow Hours	41.75 41.38 40.38 39.88 39.58 39.19 39.13
	DURATION Over top Hours	0.00 3.00 5.25 5.75 6.75		DURATION Over top Hours	0.00 .93 1.19 .93 .94
SP1LLWAY CREST 1402,00 120, 0.	MAXIMUM Outflou CFS	501. 923. 1932. 2319. 3092. 3867.	SP ILL VAY CREST 1402-00 120- 0-	MAXIMUM Outflou CfS	501. 6970. 7686. 7311. 7389. 7646.
INITIAL VALUE 1402.00 120. 0.	MAXIMUM Storage AC-FT	161. 175. 189. 193. 200.	INITIAL VALUE 1402.00 120. 0.	MAXIMUM Storage AC-FT	161. 174. 177. 174. 176.
	MAXIMUM DEPTH Over Dam	0.00 64 1.34 1.54 1.88 2.17	INITIA 140	NAXINUM DEPTH Over dam	0.00 .57 .72 .59 .59 .68
ELEVATION Storage Outfloy	MAXIMUM RE SER VOIR N•S•ELEV	1404.66 1405.44 1406.14 1406.34 1406.68 1406.97	- ELEVATION Storage Outflou	NAXINUN RESERVOIR N.S.ELEV	1404.06 1405.37 1405.52 1405.48 1405.48 1405.49 1405.59
	R A T 1 O O F P M F	•15 •25 •60 •80 •80		RATIO 0f Phf	• • 5 • • 5 • • 6 • • • 6
PLAN			PLAN		

PAGE D4 OF 10

OVERTOPPING AND DAM BREACH RESULTS LAKE SOPHIA DAM PLAN 1: OVERTOPPING ANALYSIS PLAN 2: DAM BREACH ANALYSIS

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PAGE D5 OF 10

DOWNSTREAM CHANNEL ROUTING RESULTS DUE TO OVERTOPPING ONLY DUE TO DAM BREACH PLAN 1: PLAN 2:

1	TIME	41.75	41.50	40.50	40-00	39.50	39.25	
	STAGE .FT	1 094.4	1098.9	1099.1	1099.0	1099.0	1099.1	
	FLOU.CFS	499.	5326.	6081.	5713.	5768.	6025.	
	RATIO	.15	•25	•50	•60	.80	1.00	

•			
STAT ION	MAXIMUM STAGE "FT	1094.4 1094.9 1099.1	1099-0
PLAN 2	MAX I MUN FLOU , CFS	499. 5326. 6081.	5768.
٩L	ATIO	•15 •50	0.8.

STATION -PLAN

4

MAXIMUN Flowscfs RATIO

TIME HOURS

1094.4 1096.0 1097.5 1097.5 1097.9

NA XIMUM STAGE »FT

MAXIMUM FLOU.CFS

RATIO

1262.5 1267.6 1267.6 1268.0 1267.8 1267.8

TIME HOURS MAXIMUN STAGE .FT

1

41.75 41.50 40.60 39.25

STATION

PLAN 2

41.75 41.50 41.25 41.25 41.25

1262.5 1263.4 1264.7 1264.7 1265.8 1265.8

501. 927. 1935. 2325. 3103.

TINE HOURS

NAXINUN Stage ft

MAXIMUN FLOU,CFS

RATIO

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STATION

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PLAN

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1.00 1.00

499. 922. 1928. 2318. 3102. 3881.

41.75 41.25 41.25 41.25 41.25











DISTANCE	ELENATION	人 = 3900,0
0,0	1300.0	5 = 0.0390
80,0	12 9 0.0	
100,0	1290,0	
200,0	1280.0	
300.0	1260.0 -+ 5.	TIMATED 10 FT. STREAM WIDTH
310,0	1260.0	TIMATED TOPE. STREAM WIDIA
390.0	/2 80.0	
450.0	/ 3 00.0	

(1) REFERENCE: USGS MAP, 7,5 MINUTE SERIES, SCALE: 1"= 2000 FT (1) FRIENDSUILLE QUADRANGLE, PA.-N.Y., PHOTOREUSED 1978 (2) LAUREL HAKE QUADRANGLE, PA.-N.Y., PHOTOREUSED 1978 PAGE D8 OF 10



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TIME OF BREACH 0.75 HOURS

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APPENDIX E

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 PLATES

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19 1253 HERCULENE, AND SMITH CO., PGH., PA LTISSO, 1079





19 1253 HERCULENE, AAB SMITH CO., PGH., PA LT1530-1079

Marine Contactory and







19 1233 HERCULENE, AAS SMITH CO., PGH., PA LTISSO-1079



PLATE 3



.2



19 1255 HERCULENE, AAB SMITH CO., PGH., PA LTI530-1079

D'APPOLONIA

PLATE 4



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19 1253 HERCULENE, AND SMITH CO., PGH ... PA LTISSO-1079

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APPENDIX F

REGIONAL GEOLOGY

REGIONAL GEOLOGY LAKE SOPHIA DAM

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The Lake Sophia Dam is located in the glaciated low plateaus section of the Appalachian Plateau physiographic province, characterized as a mature glaciated plateau of moderate relief.

The geologic structure consists of a series of northeast trending folds (approximately N70°E) which plunge gently to the southwest. The dip of the limbs of the folds in the vicinity of the Lake Sophia Dam is less than two degrees, with the southeast limb slightly steeper than the northwest limb. The dam is located north of the Rome Anticline. In general, the discontinuity trends are northeast and northwest.

The stratigraphy consists of glacial till which will range in thickness from very thin to approximately 200 feet. The glacial till is underlain by the Devonian Catskill Formation, which is approximately 1,800 feet thick in this area. The Catskill Formation is continental in origin, consisting of red shale and cross-bedded red and green sandstone and siltstone. The shale strata tend to weather rapidly when exposed.



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PENNSYLVANIAN

APPALACHIAN PLATEAU

Allegheny Group P.

Curlis sequences of annihione, shale, lime-stone and coal, assertuas commercial coals, limestones thicken westword, Van-port Limestones in lower part of section, includes Freeport, Killanning, and Clarion Formations.



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DRAWING

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Pottsville Group Predominantly sandstones and conglomer-ates with thin shales and couls; some couls mineable locally.

ANTHRACITE REGION

Ppo.

Post-Pottsville Formations Brown or gray sandstones and sholes with some conformerate and numerous mine-able coals.

Pottsville Group

Light gray to white, coarse grained sand-stones and conglowerates with some mine-able coal, includes Sharp Mountain, Schuylkill, and Tumbling Run Forma-tions.

DEVONIAN

UPPER

CENTRAL AND EASTERN PENNSYLVANIA

Oswayo Formation

Oswayo rormation Broanish and greenish gray, fire and medium orained sandstones with some shales and scattered calcarecus lenses, includes red shules which become more numerous castward. Relation to type Onwayo not proved.

-	*******	
	Dck	

Catskill Formation

Calskill Formation Chiefly red to brownish shales and sand-slones, includes gray and greenish sand-slone tongues named Elk Mountain, Honesdale, Shohola, and Delaware River in the east.



Marine beds

MBRINE DOOS Gray to olive brown shales, oraywackes, and malatunes, contains "Chemung" beds and "Portage" beds including Burket, Brallier, Harrell, and Trimmers Rock; Tully Limestone at base

MISSISSIPPIAN



Mauch Chunk Formation

MARCH CHURK FORMATION Red shales with brown to grounsk grav flaggy sandstanes, includes tree-drive Limestane in Fagette, Westmoreland, and Somerset constrict, Logalhanna Limestane at the base in southwestern Pennsylvania.



Pocono Group

Predonio Group Predoniounity grup, hard, massive, cross-budded conglumerate and sandstone with some shale, includes in the Appalachian Plateau Burgaon, Shenanao, Cuyahoga, Cusseurago, Cory, and Koopp Forma-tions, includes part of "Ownersot" of M. L. Fuller in Polter and Tioga counties,

Ds Susquehanna Group

Barbed line is "Chemung. Catshill" con-net of Second Pennsylvania Survey County reports, barbs on "Chemung" side of line

REFERENCE:

GEOLOGIC MAP OF PENNSYLVANIA PREPARED BY COMMONWEALTH OF PENNA., DEPARTMENT OF ENVIRONMENTAL RESOURCES, DATED : 1960 SCALE 1 : 250,000

GEOLOGY MAP LEGEND



19 1293 HERCULENE, AAB SMITH CO., PGH., PA LTISSO-1078

