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PENNSYLVANIA

- Dubois Creek Dam

NDI No. PA 00064 PennDER NO. 58-8 Dam Owner: Keystone Water Company

# PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM PACW31-81-C-00111



prepared for

## DEPARTMENT OF THE ARMY

### **Baltimore District, Corps of Engineers**

Baltimore, Maryland 21203

prepared by

## MICHAEL BAKER, JR., INC.

Consulting Engineers 4301 Dutch Ridge Road Beaver, Pennsylvania 15009



February 1981

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#### SUSOUEHANNA RIVER BASIN

DUBOIS CREEK DAM SUSQUEHANNA COUNTY, COMMONWEALTH OF PENNSYLVANIA NDI No. PA 00064 PennDER No. 58-8

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM.

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Baltimore, Maryland 21203

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Prepared by:

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MICHAEL BAKER, JR., INC.V Consulting Engineers 4301 Dutch Ridge Road Beaver, Pennsylvania 15009

**M29**81

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#### PREFACE

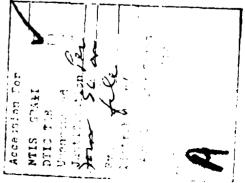
This report is prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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#### PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

#### DuBois Creek Dam, Susquehanna County, Pennsylvania NDI No. PA 00064, PennDER No. 58-8 DuBois Creek Inspected 28 October 1980

#### ASSESSMENT OF GENERAL CONDITIONS

DuBois Creek Dam is a "Significant" hazard - "Small" size dam owned and operated by the Keystone Water Company, Hallstead District. The dam was found to be in poor overall condition at the time of inspection.

Hydraulic/hydrologic evaluations, performed in accordance with procedures established by the Baltimore District, Corps of Engineers, for Phase I Inspection Reports, revealed that the spillway will not pass the spillway design flood (SDF) without overtopping the dam. An SDF in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF) is required for DuBois Creek Dam. The 100-year flood was chosen because the dam is on the low end of the "Small" size category based on storage capacity. During the 100-year flood, the dam is overtopped by a maximum depth of 0.86 feet for a total duration of 4.50 hours. The spillway is therefore considered "Inadequate." It is recommended that the owner immediately initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.

The inspection revealed certain items of remedial work which should be immediately performed by the owner. Items 1 and 2 below should be completed under the direction of a qualified professional engineer experienced in the design and construction of earth dams and appurtenant structures. These include:

- 1) Initiate an engineering study to further evaluate the spillway capacity in order to develop and implement recommendations for remedial measures to reduce the overtopping potential of the dam.
- 2) Provide upstream closure for the intake.
- 3) Repair the spalled and deteriorated portions of the concrete core wall.

#### DUBOIS CREEK DAM

- 4) Repair the spillway structure to prevent seepage and undermining.
- 5) Fill the erosion gullies on the dam and reseed the areas.
- 6) Remove the debris and sediment at the left side of the spillway approach channel.

In addition, the following operational measures are recommended to be undertaken by the owner:

- Develop a detailed emergency operation and warning system.
- During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operational procedures and records be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary. These should be included in a formal maintenance and operations manual for the dam.

JOHN A. DZIUZEK

Submitted by:

MICHAEL BAKER, JR., INC.

John A. Dziubek, P.E.

Engineering Manager-Geotechnical

Date: 19 February 1981

Approved by:

DEPARTMENT OF THE ARMY BALTIMORE DISTRICT, CORPS OF ENGINEERS

JAMES W. PECK ODL, Corps of Engineers District Engineer Date: 13 Mar 81



Overall View of Dam from Left Abutment

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**DuBOIS CREEK DAM** 

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#### APPENDICES

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM DuBOIS CREEK DAM NDI No. PA 00064, PennDER No. 58-8

SECTION 1 - PROJECT INFORMATION

#### 1.1 GENERAL

- a. <u>Authority</u> The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. <u>Purpose of Inspection</u> The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

#### 1.2 DESCRIPTION OF PROJECT

a. <u>Description of Dam and Appurtenances</u> - DuBois Creek Dam is a diaphragm earthfill embankment 321 feet long and 22 feet high. The embankment has a side slope of 3H:1V (Horizontal to Vertical) downstream and 3H:1V upstream. The upstream face of the embankment is protected with riprap. The top of the core wall is 3 feet wide and increases in width to the base which is socketed 5 feet into the foundation. The base width is shown on Plate 5 (Appendix E) to be 6 feet. The top of the core wall extends 3 feet and 5 feet above the upstream and downstream crests of the embankment, respectively. The crest of the dam is 8 feet wide.

The spillway is located at the left abutment and consists of a broad crested concrete weir. The weir is 113.5 feet long perpendicular to the direction of flow. The spillway training walls extend approximately 3.5 feet above the crest of the spillway and are constructed of both concrete and stone. The floor of the spillway channel consists of large stones grouted in place and extends 64 feet downstream of the crest of the weir.

The outlet works for the dam consist of a submerged intake, a 12 inch cast-iron pipe through the embankment to the chlorinator building at the downstream toe of the embankment, a 10 inch service line, and a 20 inch blow-off pipe. Both the 10 and 20 inch lines are operated by gate valves housed in the chlorinator building.

- b. Location ->DuBois Creek Dam is located on DuBois Creek, approximately 2.1 miles southwest of Hartford, Pennsylvania. The structure is located in Liberty Township, Susquehanna County, Pennsylvania and the coordinates of the dam are N 41° 56.4' and W 75° 46.2'. The dam can be located on Franklin Forks, Pennsylvania USGS 7.5 minute topographic quadrangle.
- c. <u>Size Classification</u> The height of the dam is 22 feet. Storage at the top of the dam (Elevation 1085.4 feet Mean Sea Level [ft. M.S.L.]) is 78.0 acre-feet. The dam is therefore in the "Small" size category.
- d. <u>Hazard Classification</u> Loss of life is not likely in the event of failure of DuBois Creek Dam. However, damage will likely occur to one home located 1,000 feet downstream and two additional homes located 3,000 feet downstream of the dam. Therefore, DuBois Creek Dam is classified in the "Significant" hazard category.
- e. <u>Ownership</u> The dam is owned and operated by the Keystone Water Company, Hallstead District, 216 Willow Avenue, Susquehanna, Pennsylvania 18847. Mr. Wallace E. Rhodes is the District Manager.
- f. <u>Purpose of Dam</u> The impoundment created by the dam serves as a water supply source for the Keystone Water Company.
- g. <u>Design and Construction History</u> DuBois Creek Dam was designed by Dunning Engineering Company of Scranton, Pennsylvania in 1905. The contractor and date of construction are not known.
- h. <u>Normal Operational Procedures</u> The reservoir is typically maintained at the spillway crest during the fall, winter and spring, and is drawn down several feet during the summer. The dam is visited every day during fall, winter and spring, and is visited in the summer twice a week.

#### 1.3 PERTINENT DATA

a. Drainage Area (square miles) - 7.77

b.	<u>Discharge at Dam Site (c.f.s.)</u> -	
	Maximum Known Flood - (Tropical Storm Agnes, 3	540 1972)
	Spillway Capacity at Maximum Pool (El. 1085.4 ft. M.S.L.) -	2200
c.	Elevation (feet above M.S.L.)* -	
	Design Top of Dam - Minimum Top of Dam - Maximum Design Pool - Spillway Crest - Streambed at Toe of Dam - Maximum Tailwater of Record -	Unknown 1085.4 Unknown 1082.0 1063.8 Unknown
d.	<u>Reservoir (feet)</u> -	
	Length of Maximum Pool (El. 1085.4 ft. M.S.L.) - Length of Normal Pool (El. 1082.0 ft. M.S.L.) -	1065 890
e.	Storage_(acre-feet)	
	Top of Dam (El. 1085.4 ft. M.S.L.) - Normal Pool (El. 1082.0 ft. M.S.L.) -	78 50
f.	Reservoir Surface (acres) -	
	Top of Dam (El. 1085.4 ft. M.S.L.) - Normal Pool (El. 1082.0 ft. M.S.L.) -	7.4 7.35
g.	Dam -	
	Type - Diaphragm earthfill with concrete con Total Length (feet) - Height (feet) - Design - Field - Top Width (feet) - Side Slopes - Upstream - Downstream -	re wall 321 Unknown 22 8.0 3H:1V 3H:1V

\*All elevations referenced to the spillway crest, El. 1082.0 ft. M.S.L., as estimated from Franklin Forks, Pennsylvania USGS 7.5 minute topographic quadrangle map.

Zoning -None Impervious Core -Concrete Core Wall Cut-off - According to the original report on the dam (dated 11 May 1917), the concrete core wall was extended 5 feet lower than the original streambed. Drains -None h. Diversion and Regulating Tunnel -None i. Spillway -Type - Broad crested weir Location - Left abutment Length of Crest Perpendicular to 113.5 Flow (feet) -Width of Crest Parallel to Flow (feet) -3 Crest Elevation (ft. M.S.L.) -1082.0 Gates -None Downstream Channel - Rectangular channel with stone and concrete walls. The channel bottom consists of large stones concreted in place.

j. <u>Outlet Works</u> - The outlet works consist of a submerged intake with a 12 inch cast-iron pipe (C.I.P.) through the embankment to the chlorinator building at the downstream toe of the embankment. There is a 20 inch ductile iron pipe blow-off line and a 10 inch C.I.P. service line which lead out of the chlorinator building. The gate valves for both these lines are located in the chlorination building.

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#### 2.1 DESIG™

The information reviewed consisted of the Pennsylvania Department of Environmental Resources' (FennDER, File No. 58-8. This file contained the following information:

- Drawing of the dam by Dunning Engineering Company, dated 1905 (Plate 5).
- The earliest inspection report by the Office of the Water Supply Commission of Pennsylvania, dated 13 July 1916.
- 3) A directive from the Water Supply Commission directing the Hallstead & Great Bend Water Company to improve the spillway to handle a higher discharge rate.
- 4) Plans showing the spillway to be widened from 50 feet to 115 feet, dated 1919 (Plate 3). During the field inspection conducted on 28 October 1980, the spillway was measured to be 113.5 feet wide.
- 5) Post Construction inspection reports and photos. The latest inspection, dated 8 August 1965, reported no serious problems. Several earlier inspection reports indicated problems with the spillway channel collapsing, deterioration of the exposed sections of the concrete core wall, and some seepage along the chlorination building.

#### 2.2 CONSTRUCTION

There is no information available regarding construction of the dam from either the owner or PennDER File 58-8.

#### 2.3 OPERATION

The Keystone Water Company is responsible for all operations and maintenance on the dam.

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#### 2.4 EVALUATION

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- a. <u>Availability</u> The information used is readily available from PennDER File 58-8.
- b. <u>Adequacy</u> The information available is adequate for a Phase I Inspection of this dam.
- c. <u>Validity</u> There is no reason at the present time to doubt the validity of the available engineering data.

#### 3.1 FINDINGS

- a. <u>General</u> The inspection was performed on 28 October 1980. A light rain was falling at the time of inspection. The dam and appurtenant structures were found to be in poor overall condition at the time of inspection. Noteworthy deficiencies observed during the visual inspection are described in the following paragraphs. The complete visual inspection check list, field sketch, top of dam profile and typical cross-section are presented in Appendix A.
- b. <u>Dam</u> Seepage was observed at three locations passing through deteriorated portions of the concrete core wall. The most severe of these locations was near Station 2+85 (see Field Sketch in Appendix A) where approximately 10 gallons per minute (g.p.m.) of seepage was occurring. These seepage areas are the result of progressive deterioration of the exposed areas of the concrete core wall. The seepage has caused erosion gullies and slight irregularities on the downstream face of the dam.
- c. <u>Appurtemant Structures</u> Seepage was observed and heard passing under the weir and spillway channel slab on the left side of the spillway. Progressive undermining and future wash-out of portions of this structure may occur if it is not properly repaired. Seepage was observed exiting from the right spillway training wall at the toe of the embankment. This seepage is presumably from flow in or under the spillway channel slab. Some debris and sediment was present at the left side of the spillway approach channel.

The intake structure was submerged during the inspection. No upstream closure is provided for the outlet pipe which passes through the embankment.

d. <u>Reservoir Area</u> - The reservoir side slopes are relatively steep and heavily wooded. No signs of instability were observed. The watershed is primarily forested. The owner's representative indicated that, at the present time, sedimentation has reduced the reservoir storage volume by approximately one-third. e. <u>Downstream Channel</u> - The downstream channel has mild slopes through a wide forested valley. Several small wooden bridges are located over the channel but these bridges should not significantly restrict flow. One home is located 1,000 feet downstream of the dam. Two additional homes are located 3,000 feet downstream of the dam. DuBois Creek flows along the northwest edge of Hallstead, Pennsylvania before its confluence with the Susquehanna River.

#### SECTION 4 - OPERATIONAL PROCEDURES

#### 4.1 PROCEDURES

There are no formal procedures for lowering the reservoir or evacuating the downstream area in case of an impending failure of the dam. It is recommended that formal emergency procedures be adopted, prominently displayed, and furnished to all operating personnel.

#### 4.2 MAINTENANCE OF DAM

Generally, the maintenance procedures followed are adequate; however, a more formal maintenance program and procedures should be developed.

#### 4.3 MAINTENANCE OF OPERATING FACILITIES

The spillway channel is repaired and the blow-off line is cleaned every year. Maintenance is performed on an as-needed basis. It is recommended that a formal operation and preventive maintenance schedule be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary.

#### 4.4 DESCRIPTION OF ANY WARNING SYSTEM IN EFFECT

There is no warning system in the event of a dam failure. An emergency warning system should be developed. ý

#### 4.5 EVALUATION OF OPERATIONAL ADEQUACY

The current operational features are adequate for the purpose they serve. However, it is recommended that a formal maintenance and operations manual be prepared for the dam.

#### SECTION 5 - HYDRAULIC/HYDROLOGIC

#### 5.1 EVALUATION OF FEATURES

- a. <u>Design Data</u> No hydrologic or hydraulic design calculations are available for DuBois Creek Dam.
- b. <u>Experience Data</u> The maximum flood of record occurred during Tropical Storm Agnes in 1972, at which time a depth of 1.0 feet over the spillway was reported. This depth gives a calculated flow of approximately 540 c.f.s. through the spillway.
- c. <u>Visual Observations</u> During the visual inspection, no problems were observed which would indicate that the dam and appurtenant facilities could not perform satisfactorily during a flood event.
- d. <u>Overtopping Potential</u> DuBois Creek Dam is a "Small" size - "Significant" hazard dam requiring evaluation for a spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF). Because the dam is on the low end of the "Small" size category in terms of storage capacity, the 100-year flood was chosen as the SDF.

Using material from "The Hydrologic Study - Tropical Storm Agnes" prepared by the Special Studies Branch, Planning Division, North Atlantic Division, Corps of Engineers, in New York City, December 1975, the peak inflow to the impoundment for the 100-year flood was calculated to be 3750 c.f.s. The hydraulic characteristics of the basin, specifically, the Snyder's unit hydrograph parameters, were obtained from a regionalized analysis conducted by the Baltimore District of the U.S. Army Corps of Engineers. Using these parameters and 1.0 inches initial loss and a constant loss of 0.05 inches/hour, a peak inflow of 3690 c.f.s. was obtained for the 100-year flood. This peak flow is within 2 percent of the peak flow computed previously; therefore, this hydrograph was used for the hydraulic analysis.

The hydraulic capacity of the dam, reservoir, and spillway was then assessed by utilizing the U.S. Army Corps of Engineers' Hydrograph Package, HEC-1 DB. Analyses of the dam and spillway shows that the dam will be overtopped during the 100-year flood by a maximum depth of 0.86 feet for a total duration of 4.50 hours.

e. <u>Spillway Adequacy</u> - As outlined in the above analyses, the spillway will not pass the SDF without overtopping the dam; therefore, the spillway is considered "Inadequate."

#### SECTION 6 - STRUCTURAL STABILITY

#### 6.1 EVALUATION OF STRUCTURAL STABILITY

- a. <u>Visual Observations</u> The seepage observed passing through the deteriorated portions of the core wall indicate that repair of the exposed portions of the core wall should be accomplished. Also, the seepage and undermining of the spillway structure is a long-term progressive type problem which should be corrected.
- b. <u>Design and Construction Data</u> Calculations of slope and structural stability were not available for review. The slopes have had a history of satisfactory performance, including occasional drawdown of the reservoir during the summer season. In view of the modest height of the dam and a history of satisfactory performance of its moderate slopes, no further stability analysis is deemed necessary.
- c. <u>Operating Records</u> Nothing in the procedures described by the owner's representative indicates concern relative to the structural stability of the dam.
- d. <u>Post-Construction Changes</u> No changes adversely affecting the structural stability of the dam have been performed.
- e. <u>Seismic Stability</u> The dam is located in Seismic Zone 1 of the "Seismic Zone Map of the Contiguous United States," Figure 1, page D-30, "Recommended Guidelines for Safety Inspection of Dams." This is a zone of minor seismic activity. Therefore, further consideration of the seismic stability is not warranted.

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SECTION 7 - ASSESSMENT, RECOMMENDATIONS/REMEDIAL MEASURES

#### 7.1 DAM ASSESSMENT

a. <u>Safety</u> - DuBois Creek Dam was found to be in poor overall condition at the time of inspection. DuBois Creek Dam is a "Significant" hazard -"Small" size dam requiring an SDF in the range of the 100-year flood to 1/2 PMF. The 100-year flood was chosen as the SDF because the dam is on the low side of the "Small" size category. As presented in Section 5, the spillway and reservoir are not adequate to pass the 100-year flood without overtopping the dam. During the 100-year flood, the dam is overtopped by a maximum depth of 0.86 feet for a total duration of 4.50 hours. Therefore, the spillway is considered "Inadequate."

The core wall, where the seepage was observed exiting through it, should be repaired. Also, the seepage and undermining of the spillway structure will become progressively worse with time and the spillway structure should be repaired.

- b. <u>Adequacy of Information</u> The information available and the observations and measurements made during the field inspection are considered sufficient for this Phase I Inspection Report.
- c. <u>Urgency</u> The owner should immediately initiate the action discussed in paragraph 7.1.d.
- d. <u>Necessity for Additional Data/Evaluation</u> The hydraulic/hydrologic analysis performed for this dam has indicated the need for additional spillway capacity. It is recommended that the owner of DuBois Creek Dam immediately initiate an engineering study to further evaluate the spillway capacity and to develop recommendations for reducing the overtopping potential of the dam.

#### 7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection and review of information revealed certain items of work which should be performed immediately by the owner. Items 1 and 2 should be designed and completed under the guidance of a qualified professional engineer experienced in the design of earth dams and appurtenant structures.

- Initiate an engineering study to further evaluate the spillway capacity in order to develop and implement recommendations for remedial measures to reduce the overtopping potential of the dam.
- 2) Provide upstream closure for the intake.
- 3) Repair the spalled and deteriorated portions of the concrete core wall.
- 4) Repair the spillway structure to prevent seepage and undermining.
- 5) Fill the erosion gullies on the dam and reseed the areas.
- 6) Remove the debris and sediment at the left side of the spillway approach channel.

In addition, the following operational measures are recommended to be undertaken by the owner:

- 1) Develop a detailed emergency operation and warning system.
- During periods of unusually heavy rainfall, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operational procedures and records be developed and implemented. An emergency drawdown plan should be developed in case emergency drawdown of the reservoir should become necessary. These should be included in a formal maintenance and operations manual for the dam.

#### APPENDIX A

VISUAL INSPECTION CHECK LIST, FIELD SKETCH, TOP OF DAM PROFILE, AND TYPICAL CROSS-SECTION

Check List ual Inspection Phase l	
Checl Visual Pho	

Name of Dam DuBois Creek Dam	County	County Susquehanna State PA	State	PA	Coordinates Lat. N 41°56.4'	Lat.	N 41°56.4'
NDI # PA 00064 PennDER # 58-8						Long.	Long. W 75°46.2'
Date of Inspection 28 October	er 1980	Weath	Weather Rainy	ainy	Tempe	erature	Temperature 35° F.

M.S.L. 1063.83 ft.\* Tailwater at Time of Inspection M.S.L. 1082.0 ft.\* Pool Elevation at Time of Inspection

\*All elevations referenced to assume datum for reservoir level from Franklin Forks, PA U.S.G.S. 7.5 minute topographic quadrangle map.

Inspection Personnel:

Michael Baker, Jr., Inc.:

James G. Ulinski Wayne D. Lasch Jeff S. Maze

**Owner's Representatives:** 

Bruce Juergens, American Water Works Service Co., Inc. Wallace E. Rhodes, Keystone Water Co. William E. Hutcheson, Keystone Water Co.

James G. Ulinski Recorder

7-1

A-2	- Not Applicable	REMARKS OR RECOMMENDATIONS						
	CONCRETE/MASONRY DAMS	OBSERVATIONS						
		VIDI # FA 00004 VISUAL EXAMINATION OF	LEAKAGE	STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS	DRAINS	MATER PASSAGES	FOUNDATION	

Name of Dam: DUBOIS CREEK DAM	CONCRETE/MASONRY DAMS - Not	- Not Applicable
# PA 00064 VL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS Concrete Surfaces		
STRUCTURAL CRACKING		
VERTICAL AND HORIZONTAL Alignment		
STNIOL HITLONOM		
CONSTRUCTION JOINTS		

Λ-3

EMBANKMENT

Name of Dam DUBOIS CREEK DAM

NDI # PA 00064

REMARKS OR RECOMMENDATIONS **OBSERVATIONS** VISUAL EXAMINATION OF

None observed SURFACE CRACKS

None observed

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

Downstream slope is slightly irregular, probably the result of erosion caused by seepage through the core wall. SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES

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Fill in erosion gullies and reseed.

Λ-4

	EMBANKMENT	
Name of Dam DUBOIS CREEK NDI # PA 00064	DAM	
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	Good horizontal and vertical alignment, however, concrete core wall is cracking and spalling. Some voids are present in the concrete core wall.	Repair spalled concrete and fill voids in core wall.
RIPRAP FAILURES	None observed	

	EMBNNKMENT	V-6
Name of Dam <u>DUBOIS CREEK</u> NDI # PA 00064	( DAM	
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Small amount of erosion along abutments of dam and training wall, along the embankment and abutment, and where water seeps through core wall.	Fill in erosion gullies and seed areas.
ANY NOTICEABLE SEEPAGE	Seepage was observed at the following locations and at the approximate rates: Sta. 1+25 at toe of dam 1.0 g.p.m. Sta. 2+20 at core wall 0.25 g.p.m. Sta. 2+45 at core wall 0.50 g.p.m. Sta. 2+85 at core wall 10.0 g.p.m.	Repair spillway channel. Repair core wall. Repair core wall. Repair core wall.
STAFF GAGE AND RECORDER	None observed	
DRAINS	One drain was observed to the left of the outlet pipe. This drain exits from the chlorinator building. No drains for the embankment were observed.	

WORKS
OUTLET

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064

REMARKS OR RECOMMENDATIONS **OBSERVATIONS** None obsėrved VISUAL EXAMINATION OF

CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT

	-	
INTAKE STRUCTURE	The intake structure was submerged at the time of inspection. No upstream closure was provided for the 12 in. cast iron pipe which passes through the embankment.	Provide upstream closure for che intake pipe.
OUTLET STRUCTURE	A 12 in. cast iron pipe runs to a chlorinator building and valve system downstream. A 20 in. ductile iron pipe blow-off exits into the natural streambed and a 10 in. service line feeds the water distribution system. No problems observed.	
OUTLET CHANNEL	Natural stream channel is in good condition.	

None observed

EMERGENCY GATE

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Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064 VISUAL EXAMINATION OF Top of weir varies in height by + 8 in. Seepage passes under weir at the left side. CONCRETE WEIR

OBSERVATIONS

The weir should be repaired to prevent seepage and undermining.

REMARKS OR RECOMMENDATIONS

Some debris and sediment is located in the left side of spillway channel. APPROACH CHANNEL

Remove debris and sediment.

The structure should be repaired to prevent seepage and undermining. Water is seeping through the concrete and stone channel floor and undermining the structure. DISCHARGE CHANNEL

BRIDGE AND PIERS None

le	REMARKS OR RECOMMENDATIONS		
GATED SPILLWAY - Not Applicable	OBSERVATIONS		
Name of Dam: DUBOIS CREEK DAM	NDI # PA 00064 VISUAL EXAMINATION OF	CONCRETE SILL	APPROACH CHANNEL

DISCHARGE CHANNEL

BRIDGE AND PIERS

GATES AND OPERATION EQUIPMENT 1

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		A-10
Name of Dam: DUBOIS CREEK NDI # PA 00064	INSTRUMENTATION DAM	
VISUAL EXAMINATION	OBSERVATIONS REMARKS OR RECOMMENDATIONS	MENDATIONS
MONUMENTATION/SURVEYS	None observed	
OBSERVATION WELLS	None observed	
WBIRS	None observed	
P I E ZOMET RRS	None observed	
OTHER	None	

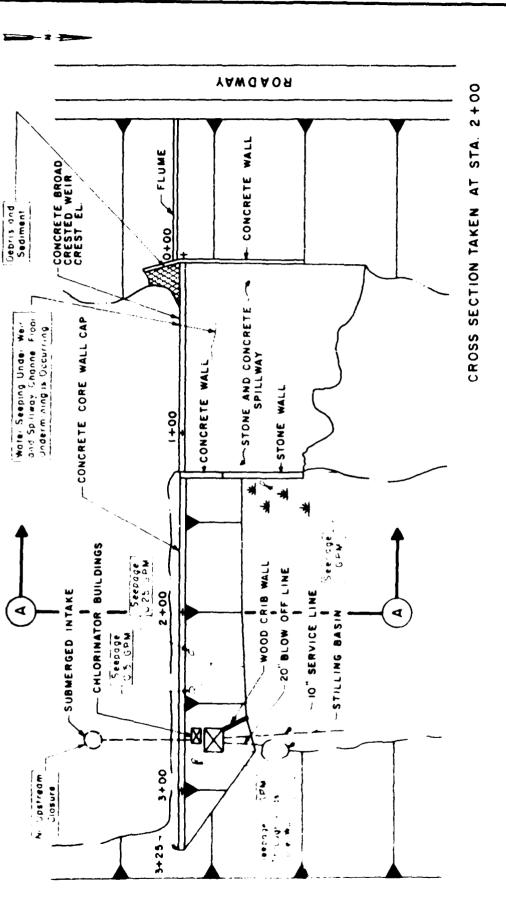
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	NDI * FR 00004 VISUAL EXAMINATION OF OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SI,OPES	The reservoir side slopes are fairly steep (15°- 45°), but no signs of instability were observed.	
SEDIMENTATION	The average depth of the reservoir according to the owner is 6 ft. According to the owner's representative, approximately one-third of the original storage volume has been filled in by sedimentation.	

	DOWNSTREAM CHANNEL	21 4
Name of Dam: DUBO NDI # PA 00064	DUBOIS CREEK DAM 64	
VISUAL EXAMINATION	OF OBSERVATIONS REM	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	No debris was present in the channel. Several small wooden bridges located on the channel will not restrict heavy flows.	
SLOPES	The downstream channel has mild slopes through a wide valley.	
APPROXIMATE NO. OF HOMES AND POPULATION	One home is located 1,000 ft. downstream of the dam. Two additional homes are located 3,000 ft. downstream of the dam.	

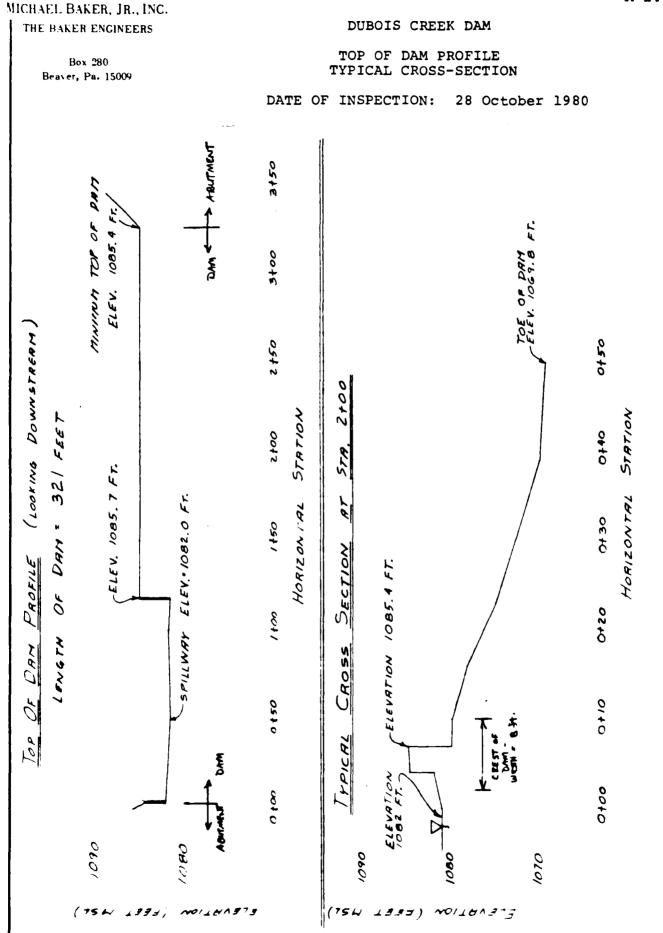
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NDI NO. PADOO64 PennDER NO. 58-8 SCHEMATIC - NOT TO SCALE DUBOIS CREEK DAM FIELD SKETCH



28 OCTOBER 1980

INSPECTED



A-14

APPENDIX B

ENGINEERING DATA CHECK LIST

of Dam: DUBOIS CREEK PA 09064	CHECK LIST ENGINEERING DATA DAM DAM
ITEN	REMARKS
PLAN OF DAM	See Plates 3 and 5 and the Field Sketch (page A-13) of this report.
REGIONAL VICINITY MAP	A USGS 7.5 minute topographic guadrangle, Franklin Forks, Pennsyl- vania, was used to prepare the vicinity map which is enclosed in this report as the Location Plan (Plate 1).
CONSTRICTION HISTORY	No construction information available.
TYPICAL SECTIONS OF DAM	See Flate 5 and Typical Cross Section (page A-14).
HYDROLOGIC/HYDRAULIC DATA	No information available
OUTLETS - PLAN	See Plate 3 and the Field Sketch (page A-13) of this report.
- DETAILS	No information available
- CONSTRAINTS	No information available
- DISCHARGE RATINGS	No information available
RAINFALL/RESERVOIR RECORDS	The owner keeps weekly pumpage and reservoir level records.

Name of Dam: DUBOIS CREEK DAM

NDI # PA 00064	
ITEH	REMARKS
DESIGN REPORTS	No information available
GEOLOGY REPORTS	No information was available. The regional geology is presented as Appendix F of this report.
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	No information available
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	No information available

BORROW SOURCES

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No information available

None

FOST-CONSTRUCTION SURVEYS OF DAM

B-2

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ITEM	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	The spillway was enlarged in 1919. Various post-construction repairs of the spillway have been performed on an as-needed basis, including the right side of the spillway in 1928 and the modifications to the lower right training wall in 1937. In 1941, repairs were performed to portions of the exposed core wall of the dam.
HIGH POOL RECORDS	One of the operators of the dam reported during the visual inspection that the reservoir level had come to within one foot of the top of the core wall in the 1940's.
POST-CONSTRUCTION ENGISIEERING STUDIES AND REPORTS	No detailed engineering reports other than the 13 July 1916 Water Supply Commission Inspection are available. A number of inspection reports are available in the PennDER file, including the latest recorded inspection on 8 August 1965 by PennDER.
PRIOR ACCIDENTS OR FAILURE OF DAM Description Reports	None reported
MAINTENANCE OPERATION RECORDS	No formal records are maintained.

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Name of Dam: DUBOIS CREEK DAM

See Plates 3, 4, and 5 and the Field Sketch (page A-13) of this report. REMARKS SECTIONS, and DETAILS SPILLWAY PLAN, HITEM

OPERATING EQUIPMENT PLANS & DETAILS

No information available

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B-4

#### CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: 7.77 sq.mi. (primarily forested)

ELEVATION	TOP NORMAL POOL (STORAGE CAPACITY): 1082.0 ft. M.S.L.
	(50 acft.)
ELEVATION	TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 1085.4 ft. M.S.L.
	(78 acft.)
ELEVATION	MAXIMUM DESIGN POOL: _Unknown
ELEVATION	TOP DAM: 1085.4 ft. M.S.L. (minimum top of dam)
SPILLWAY:	Rectangular channel
a. b. c.	Crest Elevation 1082.0 ft. M.S.L. Type Concrete broad-crested weir Width of Crest Parallel to Flow 3 ft.
d.	Length of Crest Perpendicular to Flow <u>113.5 ft.</u>
e. £.	Location Spillover Left abutment
OUTLET WO	
a.	12 in. C.I.P. through embankment with 10 in. service Type line and 20 in. blow-off at downstream toe.
a. b.	Location Near right end of dam
	Entrance Inverts Unknown
d.	Exit Inverts 1063.83 ft.
e.	Emergency Drawdown Facilities 20 in. ductile iron blow-off pipe
HYDROMETE	OROLOGICAL GAGES:None
a.	Туре
	Location
	Records
MAXIMUM N	ON-DAMAGING DISCHARGE 540 c.f.s.

A Statistics

E-5

APPENDIX C

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PHOTOGRAPH LOCATION PLAN AND PHOTOGRAPHS

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### DETAILED PHOTOGRAPH DESCRIPTIONS

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Overall View of Dam - View of Dam from Left Abutment
Photograph Location Plan
Photo 1 - View of Spillway from Left Abutment
Photo 2 - View of Crest of Spillway from Left Abutment
Photo 3 - View of Spillway Chute and Downstream Channel from Left Training Wall
Photo 4 - View of Spillway Outlet Channel from End of Spillway Chute
Photo 5 - View Looking Upstream at Left Half of Spillway Chute
Photo 6 - View Looking Upstream at Right Half of Spillway Chute
Photo 7 - View of Upstream Face of Dam from Left Shoreline of Reservoir
Photo 8 - View Along Crest of Dam from Right Training Wall of Spillway
Photo 9 - View of Downstream Face of Dam from Right Training Wall of Spillway
Photo 10 - View Along Crest of Dam from Right Abutment
Photo ll - Close-up of Hole in Upstream Side of Concrete Core Wall
Photo 12 - View of Downstream Side of Hole in Concrete Core Wall
Photo 13 - View of Seepage Exiting from Hole in Concrete Core Wall
Photo 14 - View of Seep Located in Concrete Core Wall to Left of Valve House Structure
Photo 15 - View of Outlet Conduit Valve House Structure from Downstream

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Photo 16 - View of Downstream End of Outlet Conduit

Note: Photographs were taken on 28 October 1980.

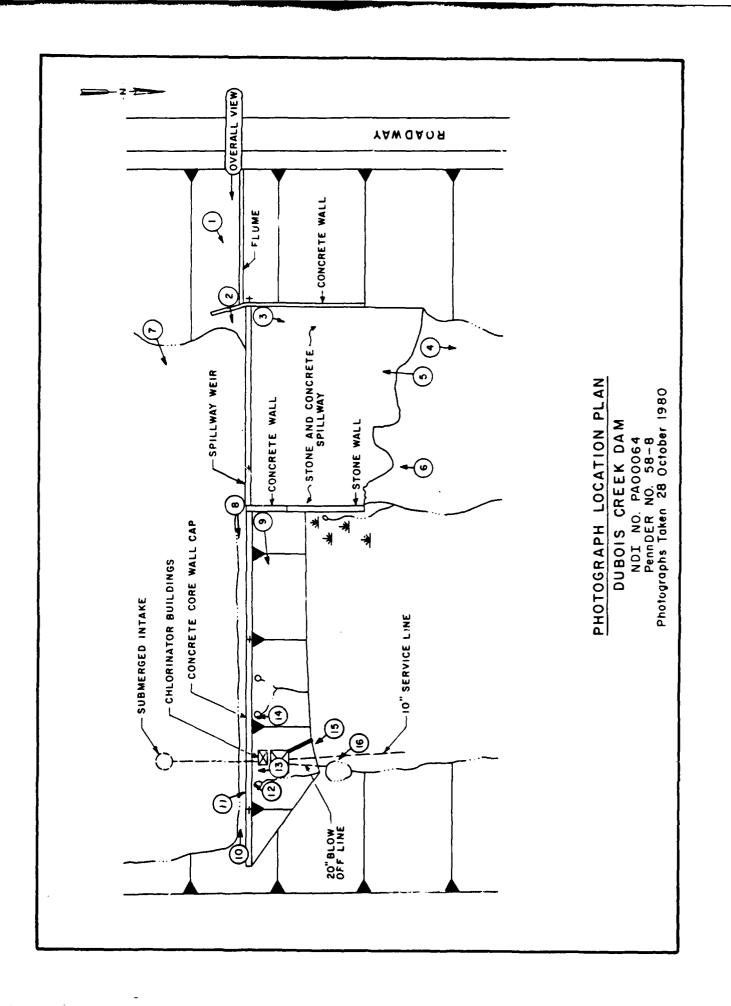




PHOTO 1. View of Spillway from Left Abutment

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PHOTO 2. View of Crest of Spillway from Left Abutment



PHOTO 3. View of Spillway Chute and Downstream Channel from Left Training Wall



PHOTO 4. View of Spillway Outlet Channel from End of Spillway Chute

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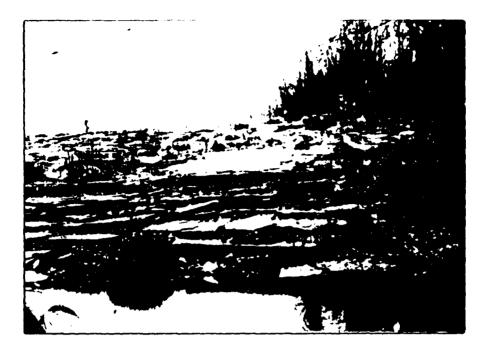


PHOTO 5. View Looking Upstream at Left Half of Spillway Chute



PHOTO 6. View Looking Upstream at Right Haif of Spillway Chute



PHOTO 7. View of Upstream Face of Dam from Left Shoreline of Reservoir

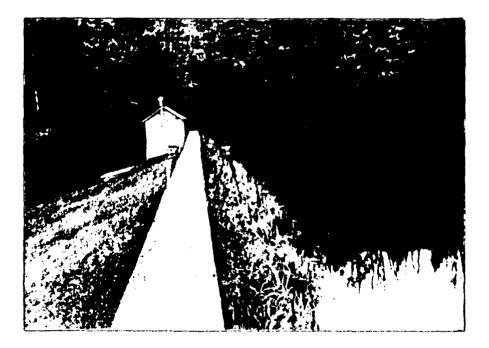


PHOTO 8. View Along Crest of Dam from Right Training Wall of Spillway

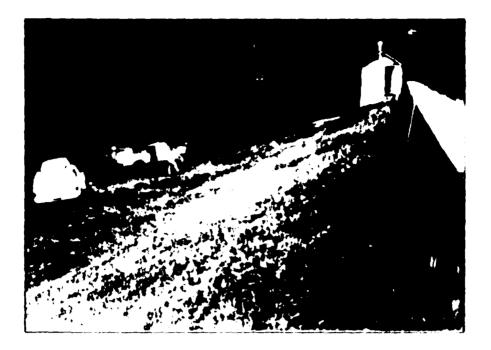


PHOTO 9 View of Downstream Face of Dam from Right Training Walof Spillway



PHOTO 10 View Along Crest of Dam from Right Abutment



PHOTO 11. Close up of Hole in Upstream Side of Concrete Core Wall.



PHOTO 12 View of Downstream Side of Hole in Concrete Core Wall

# Dubois CREEK DAM



PHOTO 13. View of Seepage Exiting from Hole in Concrete Core Wall



PHOTO 14. View of Seep Located in Concrete Core Wall to left of Valve House Structure



PHOTO 15. View of Outlet Conduit Valve Structure from Downstream

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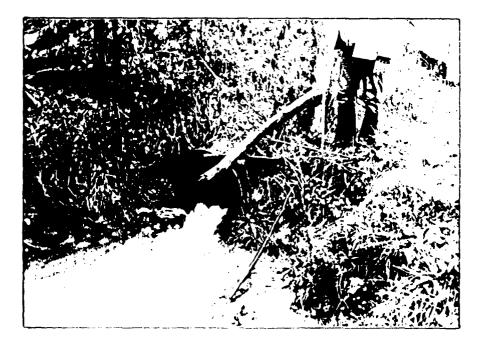


PHOTO 16. View of Downstream End of Outlet Condult

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

MICHAEL BAKER, JR., INC.	Subject DUBDIS CREEK DAM S.O. No.
THE BAKER ENGINEERS	APPENVIX D - HYPPOLOGIC Sheet No of
Box 280	AND HYDRAULIC COMPUTATIONS Drawing No.
Beaver, Pa. 15009	Computed by <u>GUT</u> Checked by Date <u>2-/6-5</u> /

#### PAGE SUBJECT PREFACE i HYDROLOGY AND HYDRAULIC DATA BASE 1 HYDRAULIC DATA 2 3 DRAINAGE AREA AND CENTROID MAP TOP OF DAM PROFILE AND CROSS SECTION 4 5 SPILLWAY DISCHARGE RATING 100-YEAR STORM DISTRIBUTION 6 100-YEAR DISCHARGE CALCULATION 7 HEC-1 SPILLWAY CAPACITY ANALYSIS 8

#### PREFACE

### HYDROLOGIC AND HYDRAULIC COMPUTATIONS

The hydrologic determinations presented in this Phase I Inspection Report are based on the use of a Snyder's unit hydrograph developed by the U.S. Army Corps of Engineers. Due to the limited number of gaging stations available in this hydrologic region and the wide variations of watershed slopes, the Snyder's coefficients may yield results of limited accuracy for this watershed. As directed however, a further refinement of these coefficients is beyond the scope of this Phase I Investigation.

In addition, the conclusions presented pertain to present conditions, and the effect of future development on the hydrology has not been considered.

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#### HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: DUBOIS CREEK DAM

100-YEAR 24 HOUR RAINFALL = 6.4 INCHES<sup>(1)</sup>

STATION	1	2	3	4	ţ
Station Description	DUBOIS CREEK DAM				
Drainage Area (square miles)	7.77				
Cumulative Drainage Area (square miles)	7.77				
Adjustment of PMF (for Drainage Ares (%)					
6 Hours 12 Hours 24 Hours 48 Hours 72 Hours	100-YEAR STORM DISTRIBUTION ON SHEET 6				
Snyder Hydrograph Parameters		·····			
Zone (2)	11A				
c <sub>p</sub> /c <sub>t</sub> (3)	0.62/1.50				
L (miles) (4)	5.19				
L <sub>ca</sub> (miles)(4)	2.27				
$t_p = C_t (L \cdot L_{ca})^{0.3}$ (hours)	3.14				
Spillway Data Grest Length (ft) Freeboard (ft) Discharge Coefficient Exponent	113.5 2.7 RATING CURVE DEVELOPED ON SHEET 5				

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CONTRACTOR

(1) Technical Paper No. 40, Cooperative Studies Section, U.S. Weather Bureau, Washington, D.C., 1961.

(2)Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snycer's Coeff conts (Cp and Ct).

(3) Snyder's Coefficients.

MICHAEL BAKER, JR., INC.	Subject Differs STEER SHIT	5.0. No
THE BAKER ENGINEERS	HYPRAULIC PHITH	Sheet No2 of _ / Z
Box 280 Beaver, Pa. 15009	Computed by <u>Given T</u> Checked by <u>LDL</u>	Drawing No Date <u>/2 - 2 - 2 2</u>

PTSKHGE CALCULA	TIONS
AREA VS. ELEVAT	TION DATA (MEASURED FROM QUAD)
ELEVATION (FT.)	SURFREE FREA (ACRES)
1082	7.35
1100	18.37
1120	54.18

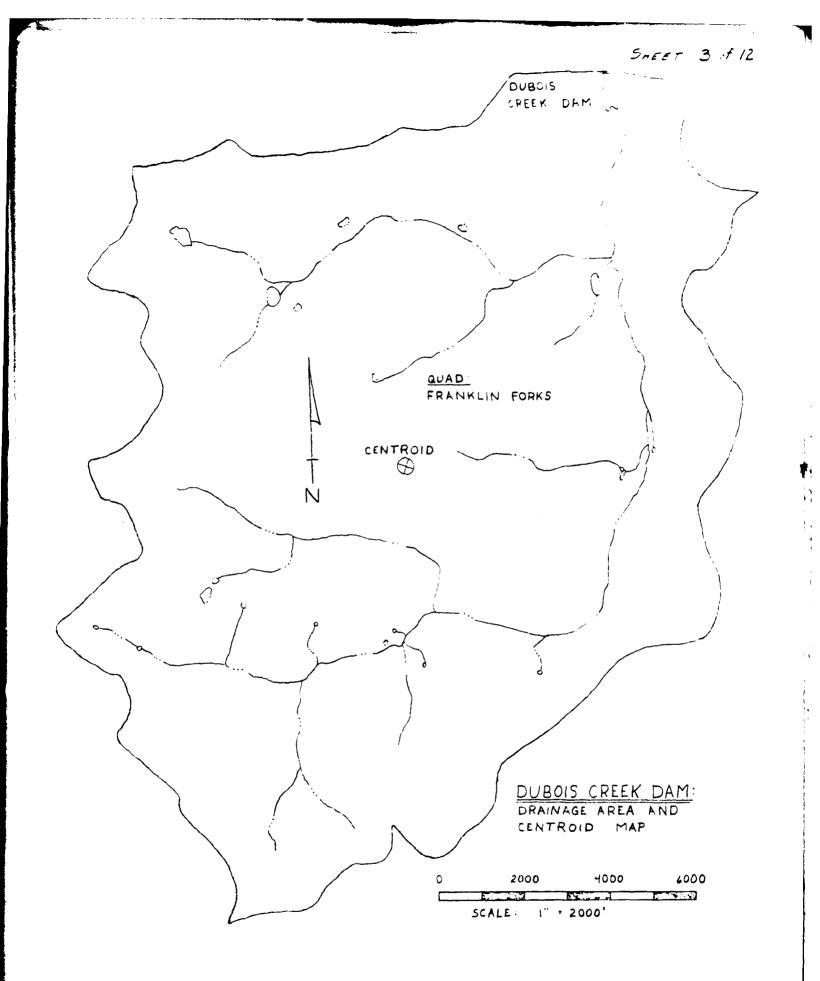
NOPMAL POOL STORAGE

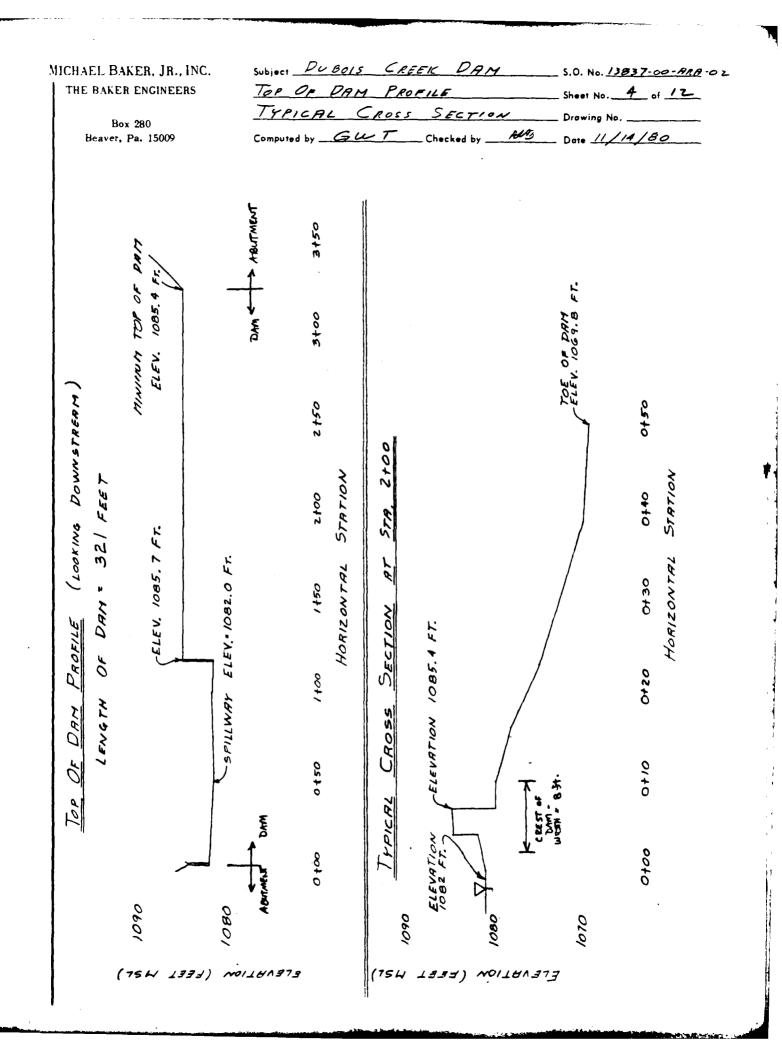
STORAGE VOLUME = VN = 1/3 (A, + A, + VA, A)
h = ESTIMATED AVERAGE DEPTH = 7 Fr.
A, = SURFACE AREA OF NORMAL POOL = 7.35 AC.
AL SURFACE AREA OF RESERVOIR BOTTOM . 7.03 AC.
(ESTIMATED FROM AVERAGE DEPTH
FIND RESERVOIR SIDE SLOPES)
NOKMAL POOL STORAGE = VNP = 1/3 (7.35 + 7.03 + V(7.35 (7.03))
V~= 50.32 AC FT.

TOP OF DAM STORAGE 78 AC.-FT. (FROM HEC-1 ANALYSIS)

 $\frac{SNYDER'S UNIT HYDROGIAPH PARAMETERS}{L=5.19 TT., L_{CR} = 2.27 TT.}$  WATERSHED IS IN ZONE IIF  $C_{p} = 0.62 , C_{4} = 1.50$   $t_{p} = 1.50 (L \times L_{CR})^{-3} = 3.14 H_{R}.$ 

DRAINAGE AREA = 7.77 Sq. Mi.





E BAKER ENGINEER	s <u>5</u>	SPILLN	VAY DIS	сна	RGE	RATING Shi	eet No.	5 01 12
						_	awing No.	
Box 280 Beaver, Pa. 15009			GUT			ALL Do	•	
				0.		D6		
	SPIL	LWAY	PROFILE	F				
	FLOW		•	_	CREST	ELEV. = 10	82.01	FT.
1080		-		- ELE	V. = 1081.			
1000		s:152	078		E	51 <i>0PE</i> = 0.096	EN	D OF SPIL
							E	LEV. =1075
								CHANN
1070								
	0+00	01	120	0+40	0	+60	0+80	1+00
DEVELO						FLOW O		NL WAY
DEVELO		(CHO) 9 = 32	N, <u>OPENC</u>	HANN	EL HYDI	RAULICS	P. 43	
DEVELO		(Сно) д = 32 D = МЕА	N, <u>OPENC.</u> .2 FT/SEC N HYPRAL	HANN = 1216 1	DEPTH = )	RAULICS FLOW AREA FEE SUARGE	P. 43	
		(Сно) д = 32 D = МЕА	N, <u>OPENC</u>	HANN = 1216 1	DEPTH = )	RAULICS FLOW AREA FEE SUARGE	P. 43	
I	V= 49 D	(CHO) g = 32 D = MEA V • ME	W, <u>OPENC</u> .2 FT/SEC IN HYPRAL FAN FLOW	HANN =. = /LIC I V VE	REPTH = ) ELOCITY	RAULICS FLOW AREA FEE SUARGE	P. 43	
SPILLWRY	V = GD Q = AV Flow DEPTM	(CHU) 9 = 32 D = MEA V • ME	N, <u>OPENC</u> 2 FT/SEC N HYPAAL FAN FLOW TOP WIDTH	HANN =. = /LIC I V VE	REPTH = ) ELOCITY	<u>RAULICS</u> FLOW AREA FREE SUMACE	P. 43	RESERV SURFRC
SPILLWRY FLEVRTION, FT.	V = GD Q = AV FLOW DEPTH, FT.	(CHON g = 32 D = MEA V • ME RRER FT <sup>2</sup>	N, <u>OPENC</u> 2 FT/SEC N HYPAAL FAN FLOW TOP WIDTH	HANN ~ VIC I V VE	V <u>EL HYDI</u> DEPTH = ) ELOCITY V, <sup>F</sup> Ysec	RAULICS FLOW AREA FREE SUMPRIE	P. 43 TOPWID	RESERV SURFAC
SPILLWRY FLEVRTION, FT. 1082.0	V = 690 Q = AV Flow DEPTH, Fr. C C.5 1.0	(CHU) 9 = 32 D = MEA V • ME FT2 0 43.75 100.50	N, <u>OPENC</u> 2 FT/SEC N HYPARL FAN FLOW TOP WIDTH, FT. O	HANN  VIC I VIC	VEL HYDI DEPTH = ) ELOCITY V, <sup>F</sup> JSEC 0 3. 63 5. 35	RAULICS FLOW AREA FREE SURFACE Q, CFS 0 158.81 537, 68	P. 43 Topwie V <sup>*</sup> /2 8 0.20 0.44	RESERV SURFAC 1082. 1083.4
59166WRY FLEVRTION, FT. 1082.0 1082.5 1083.0 1083.5	V = 690 Q = AV FLOW DEPTH Fr. C C.5 1.0 1.5	(CHON $g = 32     D = MEA     V • ME     FTERFTERG43.75100.50157.25$	N, <u>OPENC</u> .2 FT/SEC IN HYPAAU FAN FLOW TOP WIDTH, FT. 0 107.5	HRNN =. * 1/1C 1 V VE . R/T 0 .41	VEL HYDN DEPTH = ) = LOCITY V, FJ/SEC 0 3, 63	RAULICS FLOW AREA FREE SUMALE Q, CFS 0 158.81 537, 68 1,047.29	P. 43 TOPWID V <sup>*</sup> /28 0,20	RESERV SURFRC 1082. 1083.4 1084.1
SPILLWAY FLEVATION, FT. 1082.0 1082.5 1083.0 1083.5 1084.0	V = 690 Q = AV FLOW DEPTH, FT. C C.5 1.0 1.5 2.0	(CHON) g = 32 D = MEA $V \cdot ME$ RRER $FT^{2}$ 0 43.75 100.50 157.25 214.00	W, <u>OPENC</u> .2 FT/SEC W HYPAAU FAN FLOW TOP WIDTH, FT. 0 107.5 113.5 113.5 113.5	HRNN 2 2 2. C 2. C 3. C 3. C 4.1 1.38 1.38 1.88	VEL HYDN DEPTH = ) = LOCITY V, FJ/SEC 0 3. 63 5. 35 6, 66 7. 7 8	RAULICS FLOW AREA FREE SUMALE Q, CFS 0 158.81 537,68 1,047.29 1,664.92	P. 43 TOPWIE V <sup>+</sup> /2 8 0.20 0.44 0.69 C.94	RESERV SURFAC 1082. 1083.4 1084.1 1084.9
59122WRY FLEVATION, FT. 1082.0 1082.5 1083.0 1083.5 1084.0 1084.5	V = 690 Q = AV Flow DEPTM Fr. C C.5 1.0 1.5 2.0 2.5	(CHU) g = 32 D = MEA V • ME AREA FT2 0 43.75 100.50 157.25 214.00 270.75	W, <u>OPEN C</u> .2 FT/SEC W HYPAAU FAN FLOW TOP WIDTH, FT. 0 107.5 113.5 113.5 113.5 113.5	HRNN  VIIC I VV VE .41 .89 1.38 1.88 2.38	V, FT/SEC 0 3.63 5.35 6,66 7.78 8.75	RAULICS FLOW AREA REF SUMPACE Q, CFS 0 158.81 537, 68 1,047.29 1,664.92 2,369.06	P. 43 Topwie V/2 8 0.20 0.44 0.69 C.94 1.19	RESERV SURFAC 1082. 1083.4 1084.1 1084.9 1085.6
SPILLWRY FLEVRTION, FT. 1082.0 1082.5 1083.0 1083.5 1084.0 1084.5 1084.7	V = 690 Q = AV Flow DEPTM Fr. C C.5 1.0 1.5 2.0 2.5 2.7	(CHON) g = 32 D = MER $V \cdot ME$ RRER $FT^2$ O 43.75 100.50 157.25 214.00 270.75 327.50	W, <u>OPENC</u> .2 FT/SEC WHYPARD FAN FLOW TOP WIDTH, FT: 0 107.5 113.5 113.5 113.5 113.5 113.5 113.5	HRNN   	VEL HYDN DEPTN = ) ELOCITY V, FT/SEC 0 3. 63 5. 35 6, 66 7. 7 B 8. 75 9. 65	RAULICS FLOW AREA FREE SURFACE 0 158.81 537.68 1,047.29 1,664.92 2,367.06 3,160.38	P. 43 TOPWID V <sup>*</sup> /28 0.20 0.44 0.69 0.94 1.19 1.45	RESERV SURFRC 1082. 1083.4 1084.1 1084.9 1085.6 1086.1
SPILLWAY FLEVATION, FT. 1082.0 1082.5 1083.5 1083.5 1084.0 1084.5 1084.7 1085.2	V = 690 Q = AV FLOW DEPTH, FT. C C.5 1.0 1.5 2.0 2.5 2.7 3.2	(CHUN g = 32 D = MEA V • ME AREA Fr2 0 4375 100.50 157.25 214.00 270.75 327.50 384.63	W, <u>OPEN C</u> .2 FT/SEC W HYPAAU FAN FLOW TOP WIDTH, FT. 0 107.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5	HRNN  - - - - - - - - - - - - -	V. F. SFC V. F. SFC V. F. SFC 0 3. 63 5. 35 6. 66 7. 7 B 8. 75 9. 65 10. 37	RAULICS FLOW AREA FLOW AREA FREE SUMALE Q, CFS 0 158.81 537,68 1,047.29 1,664.92 2,367.06 3,160.38 3,988.61	P. 43 Torwie 0.20 0.44 0.69 1.45 1.67	RESERV SURFAC 1082. 1083.4 1084.1 1084.9 1085.6 1086.8
SPILLWRY FIFVATION, FT. 1082.0 1082.5 1083.0 1083.5 1084.0 1084.5 1084.7 1085.2 1085.7	V = 690 Q = AV F20W DEPTH, FT. C C.5 1.0 1.5 2.0 2.5 2.7 3.2 3.7	(CHON) g = 32 D = ITEA $V \cdot ITE$ RRER $FT^2$ 0 43.75 100.50 157,25 214.00 270.75 327.50 384.63 442.63	W, <u>OPEN C</u> .2 FT/SEC W HYPAAU FAN FLOW TOP WIDTH, FT. 0 107.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5 113.5	HRNN  VIIC I VV VE VE .41 .32 1.32 1.38 2.38 2.38 3.34 3.78	V, FT/SEC 0 3, 63 5, 35 6, 66 7, 7 8 8, 75 9, 65 10, 37 11, 03	RULICS FLOW AREA REF SUMACE 9, CFS 0 158.81 537, 68 1,047.29 1,664.92 2,369.06 3,160.38 3,988.61 1,862.21	P. 43 TOPWIE V 2 8 0.20 0.44 0.69 1.19 1.45 1.67 1.89	RESERV SURFAC 1082. 1083.4 1084.1 1084.9 1085.6 1086.1 1086.5 1087.5
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Subject PUBOIS CREEK DAM S.O. No. MICHAEL BAKER, JR., INC. THE BAKER ENGINEERS 100-YEAR STORM DISTRIBUTION Shoel No. 6 of 12 \_ Drawing No. Box 280 \_ Checked by \_ UDL\_ Date 11-25-80 Computed by \_ GUT Beaver, Pa. 15009 2.0-Z. 1 100 - Y R. TP-40:----RAINFALL AMOUNTS FROM \_\_\_\_. 30 MIN : 2.1 /M. . . . . . . . . . . . . . . . . 1 HR. \_\_\_\_ 2.6 IN. 1.5 -----\_\_\_\_ . . . . . . . . . . . . . . . . 3 H.R. 3.6 J.N. \_\_\_\_ ------ -----------12 HR \_\_\_\_\_ 5, 5, 10. . -- . . . . . . . . . .... \_\_\_\_\_ -----24 HK 1:0 -----...... -----. . . a service and the second second second ..... . . . ~ . \_ . \_ . . --------• - • ..... ----. . . . . . --------------------. . . . . . .... Ċ۶ 05 . . . . -0.25 . . ---------0.15 -0.15 .... 0.083 where is not all a second of \_\_\_\_ 10.037 . ..... المدرب فالمتدر فالمحتم مستحام مسالحا -0- 2 - 4 - 6- 8- 10- 12 14 - 16 - 18 - 20 - 22 - 24 - ----. . . . . . - ---TIME, HRS. \_\_\_\_ . .. RAINFALL DISTRIBUTION ..... (30 MINUTE INTERVALS) -----····· · · TOTAL RE OCCURING IN EACH INTERVAL INTERVEL NUMBERS 1-17 0.6 18-25 حاؤهر بينا فانتارا المحصور فالاستقام ما 1.3 -----------2.3 26-29 2.3 30 اليمانون ألوارد الرابا الاستبيار يوتعمنا وتحا الفرسانا أوالك أيوفن وتنفيا وتعاري 5:4 7.8. TOTAL = 100 % \_\_\_\_\_ 32 . . . . . . ; ---- -32.8 5.4 \_\_\_\_\_ -----2.9 ------>6=37 ----------2.7 ........ 38-47 والصابية والعاد العاري والمسور مترج المسج الاردان بالمصرد المساديين ومراجب . . . . . . . . 1.3 ----\_\_\_\_\_ •••• 0.6 42 - 48 ----------····· · ···· -----. . . . . . . . . . . . . . . . . . the second s . . . . . . . . . ------ - -المسجاد المتعمد الجالم والدارية - ÷ -----. . . . . د به از ارتبطیت میداد از بایدید. میکند او میشان باید و ماند. ••••• -----. . ... . **.** . . . . . . . . ار در بیش و میشد. در مار از میرده بر داران از میاند میشود و میشوشی . \_ . \_ . . . . . . . . . - -المتبحا السرقاتين فيتسبب والوالي الاسترادة والتها -. . . . . . 

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Subject DORCIS CREEK DAM S.O. No. MICHAEL BAKER, JR., INC. THE BAKER ENGINEERS 100- YEAF DISCHARGE CALCULATION Sheet No. 7 of 12 \_\_ Drawing No. \_\_\_\_ Box 280 Computed by Gur T Checked by Will Dote 11-26-80 Beaver, Pa. 15009 THE INFLOW TO THE IMPOUNDMENT FOR THE 100-YEAR FLOOD WAS CALCULATED USING MATERIAL FROM "THE HYDROLOGIC STUDY - TROPICAL STORM AGNES" PREPARED BY THE SPECIAL STUDIES BRANCH, PLANNING DIVISION, NORTH ATLANTIC DIVISION, COPPS OF ENGINEERS, IN NEW YORK CITY. DRPINAGE AREA - 7.77 SQ Mi O COMPUTE THE MEAN LOGARITHM LOG (Q,) : C, + 0.75 LOG A LOG (qm) = MEAN LOGARITHM OF ANNUAL FLOOD PEAKS A : DRAINAGE AREA, SQ. Mi = 7.77 Sq. M. C. : MAP COEFFICIENTS FOR MEAN LOG OF ANNUAL PEAKS FROM FIG. ZI = 2,15  $Log(q_{1}) = 2.15 + 0.75 (Log 7.77)$ = 2.818 Z COMPUTE STANDARD DEVIATION S=C. - 0.05 (LOGA) S: STANDARD DEVIATION OF THE LOGARITHMS OF THE ANNUAL PERKS. CS = MAP COEFFICIENT FOR STANDARD DEVIRTION FROM F1G. 22 = 0.349A = DFAINAGE AREA, Sq. M. = 7.77 Sq. M. 5= 0.349 - 0.05 ( LOG 7.77) = 0.305  $\Im$ SELECT SKEW COEFFICIENT FROM FIG. 23 =+0.20 A  $LOG(q_{100}) = LOG(q_{10}) + K(P_{10})5$ K(P,g) = STANDARD DEVIATE FOR A GIVEN EXCEEDENCE FREQUENCY PERCENTAGE (P) AND SKEW COEFFICIENT (g) FROM EXHIBIT 39 OF BEARD'S "STATISTICAL NETHODS IN HYDROLOGY " LOG ( Q100) = 2,818 + 2.48 (0.305) Q100 = 3,755 CFS USING THE SNYPER'S UNIT HYDROGRAFH PARAMETERS DEFINED FOR THIS BASIN PRODUCED A PEAK FLOW OF 3690 CFS. THIS VALUE IS WITHIN 2 % OF THE PREVIOUSLY COMPUTED PEAK FLOW OF 3755 CFS AND IS WITHIN THE 10 % LIMIT SUGGESTED BY CORPS GUIDLINES.

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7.21. . I C. • 0. • . . . . EAU-U-PERTUJ-HUM ULMP - MJAUA HMAMA PINTUJ MAAM AKUJ LUVO \*\*\*\*\*\*\*\*\* 2 IAUIU 4 1 1 X UNIT HYJAGGAPH 35 E40-UF-PERTUD UKUINALS, LAUE 3.13 HUUKS, LPE 4.69 VUE 1.00 . 211. 419. 641. 440. 970. 1300. 727. 770. . 434. 393. 333. 278. 135. 190. 103. 130. . . . ה נטראנ 5 N N I N N LIAME LOLANE 2 4 F - J 4 0 - 0 LAAL .... K X 1 -11.52.7 \*\*\*\*\*\*\*\*\* -0.00 KILOK= 2.00 NUNC 4 ; **ว** 1141 7 INGO + 1655 JATA ULIAR ATIGL LAAIN JATA ATIUN JATIL U.) 1.00 U.U 0.J 1.3U 1.0U MULII-PLAY ANALYSES IU DE PEREURMEU NPLAJE | AKIEUE | EKIEUE | 4411U U.J UMIT НҮВКОЗКАРН ∪АТА ТР≈ 3.14 СР≖0.02 №13× О NAL LAUPL INAL HYDRUKAPH JAIA SNAP THSDA THJPL AALI 0.0 1.11 J.O U.J IMIN MITHL SUB-AKEA RUNULE LUMPULAIJUN l l d f 7 1 , 53. 41. JUB SPECIFICATION -1-50 NECEDSAUN UATA. \*\*\*\*\*\*\* 5 LAN ICOMP LECON ITAPE , . , . 1 0 į 0 0 0 0 0 0 0 2 2 58-58-RJILFF HYJAUGRAPH TO DAM 11.00 LUAY 1 Э \*\*\*\*\*\*\*\*\* 1 446 A STRIUE 40.01 HA.44 PERTOD EALS NINN 50 -.UL.I. = \$LII. 11164 4 Ϋ́́ ELUUL HYDRLUP APLL PALKANL LIFL-LI DA4 SAFETY VERSIUN JULY 1973 LAST 400[F1CATIUN 26 FL3 79 44J UPDATE 04 JUA 79 LKUPI SIAAA ..... 00411 200 \*\*\*\*\*\*\*\*\* 1 ł į 5, 1. 18. 17. 5.4. RUN DATE 12201240 ł ÷ i i ł ł 2 ł t ł •]: : . : : :1 • : 7 : : : 2 1 : į, ; . : :. : £. : : : ÷ : - -

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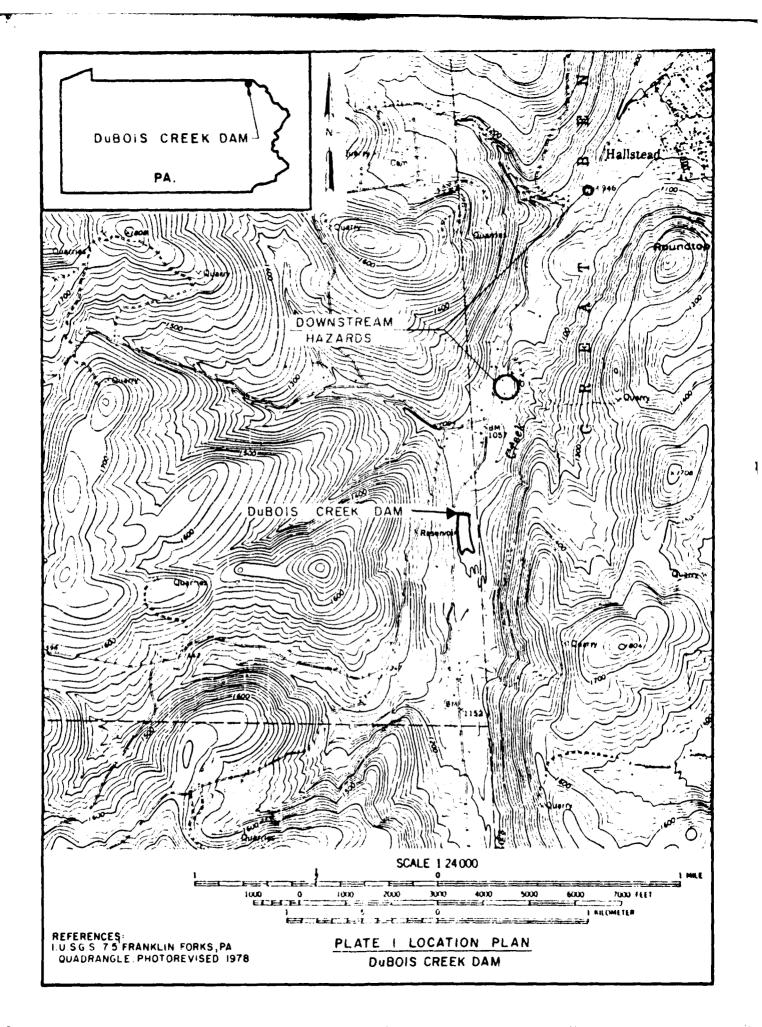
APPENDIX E

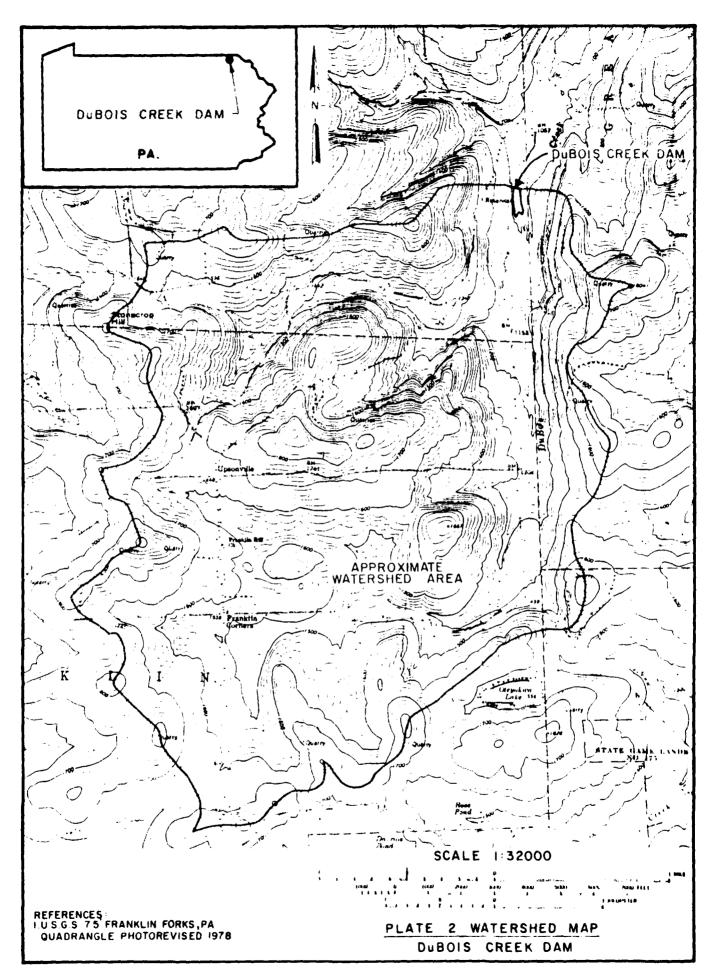
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PLATES

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- Plate 1 Location Plan
- Plate 2 Watershed Map
- Plate 3 Profile and Plan of Dam (1919)
- Plate 4 Reconstruction Drawing of Right Spillway Training Wall (1930)
- Plate 5 Plan, Profile, and Cross Section of Dam (1905)



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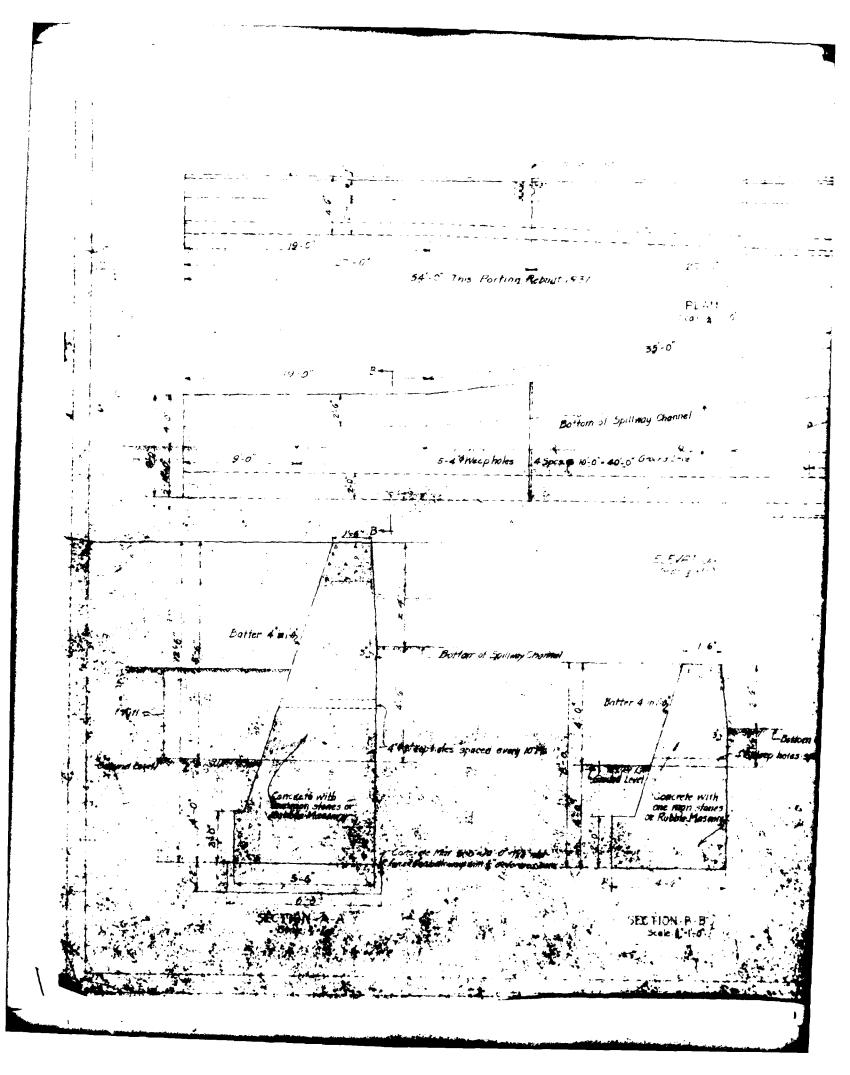
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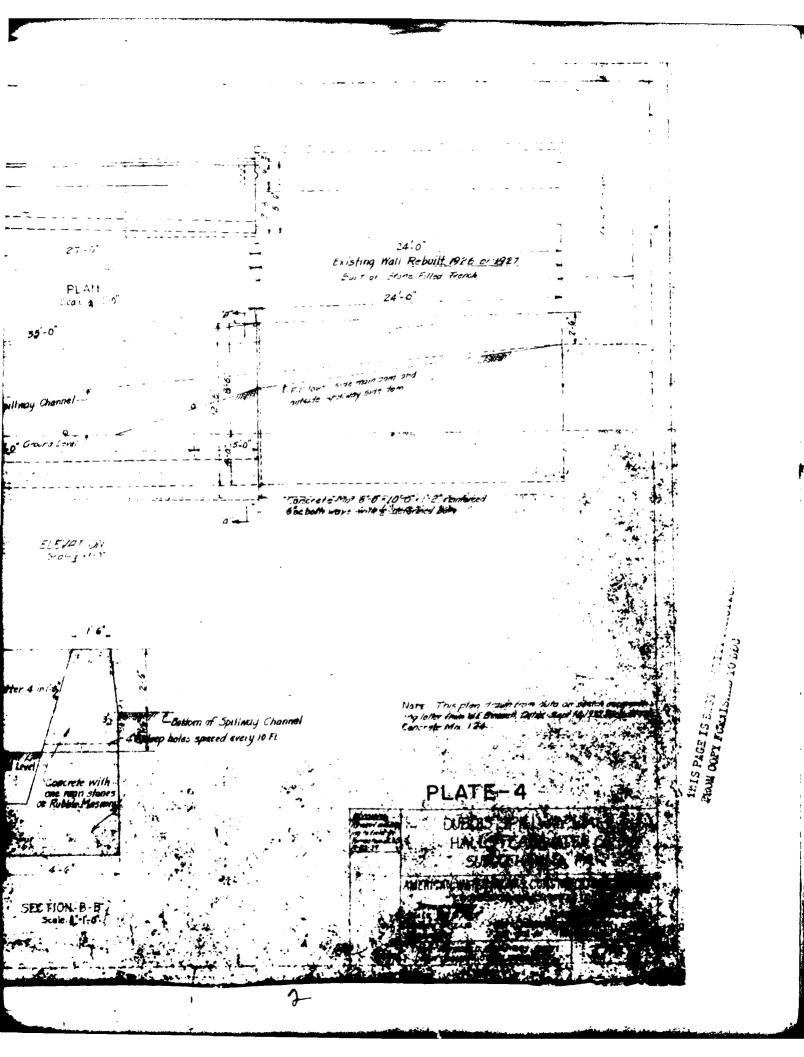
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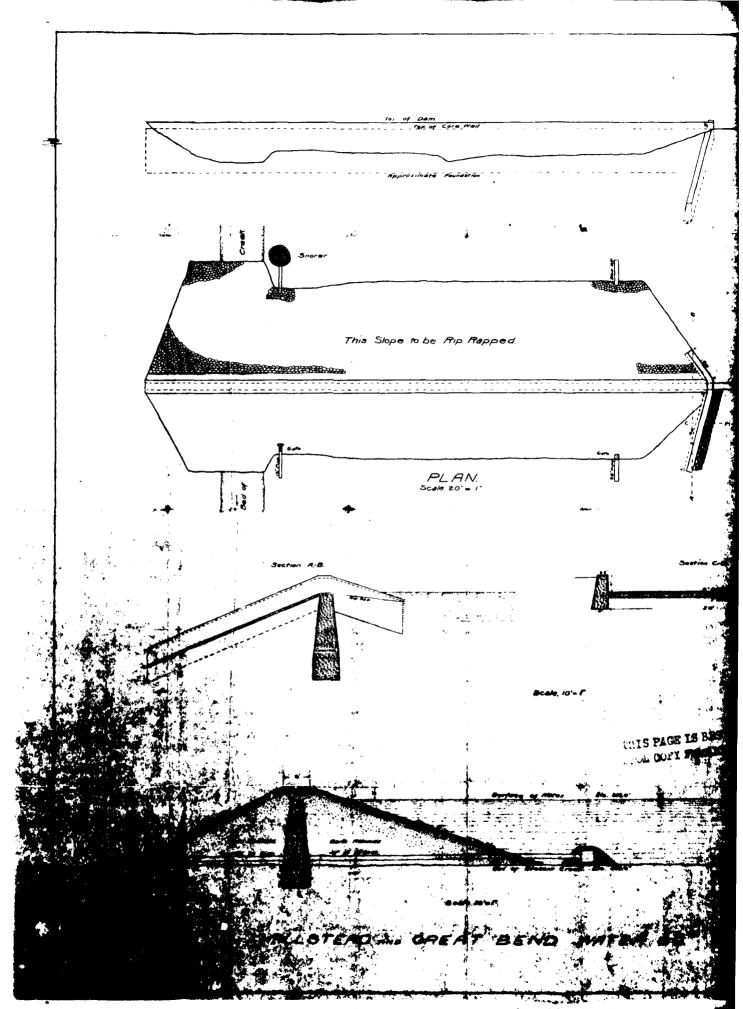
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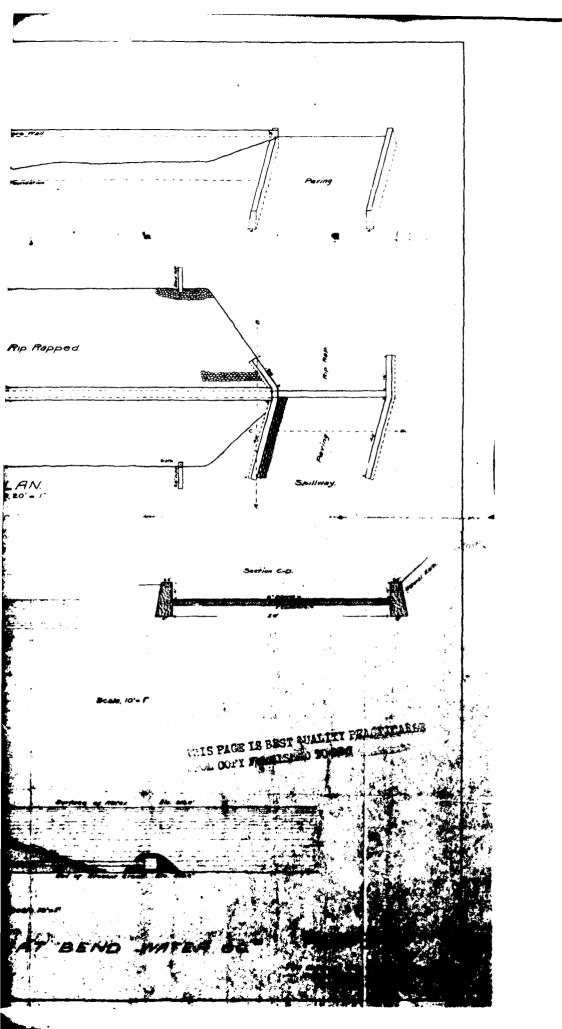
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APPENDIX F

REGIONAL GEOLOGY

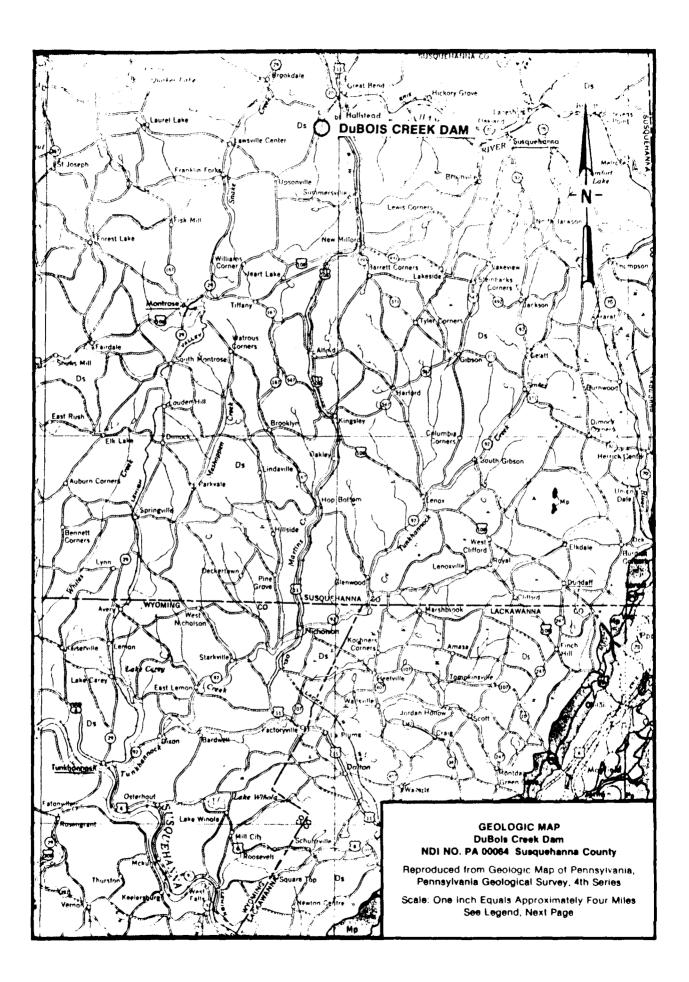
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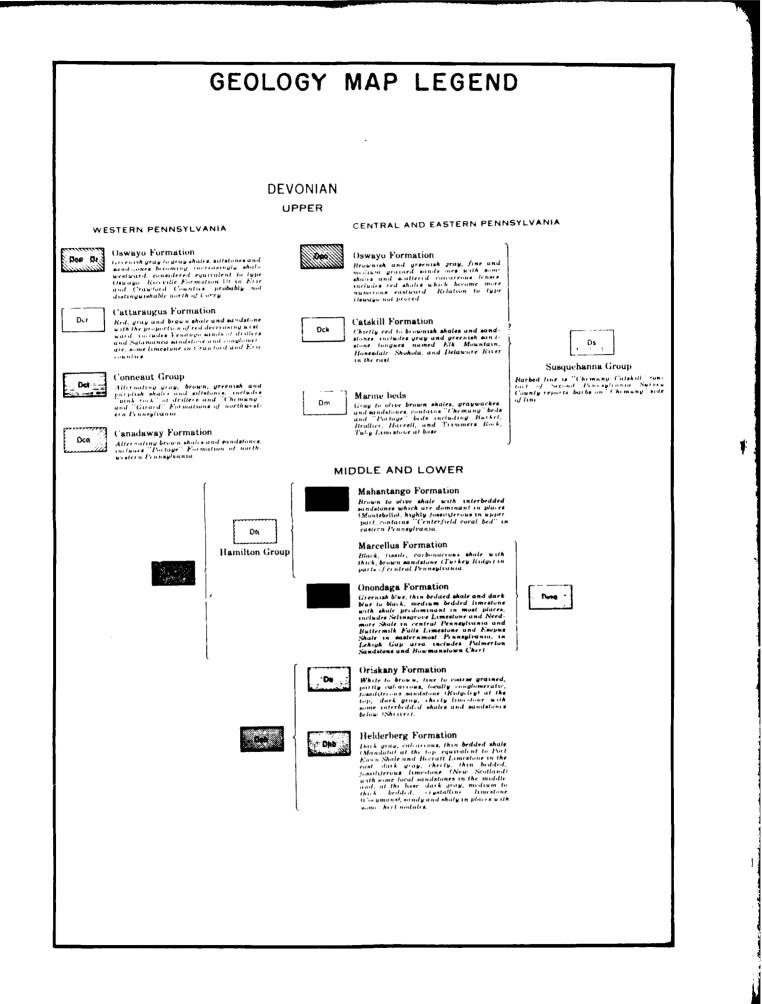
#### DuBOIS CREEK DAM NDI No. PA 00064, PennDER No. 58-8

### REGIONAL GEOLOGY

DuBois Creek Dam is in a steep walled valley located in the Glaciated Low Plateaus physiographic province. The area has undergone glaciation at least three times and is presently covered with Wisconsin Stage glacial deposits. According to the Soil Conservation Service's Soil Survey for Susquehanna County, the surface soils consist primarily of very stoney, silt loams of the Mardin-Volusia-Oquaga association. No test boring data were available for review, thus, the thickness of this overburden is difficult to ascertain.

Geologic references indicate bedrock in the vicinity of the dam to be composed of the lower members of the Catskill Formation and the upper members of the Chemung Formation; both belonging to the Susquehanna Group. The dam lies near the contact between the Catskill, which outcrops in the upper reaches of the valley as red and gray shales and sandstones, and the Chemung, which underlies most of the valley floor downstream of the dam. The Chemung Formation consists of prodelta, fossiliferous, gray, sandy shales and gray to olive green sandstones of Upper Devonian age. A bedrock sample obtained from the valley floor downstream of the dam was a hard, olive green fine to medium grained sandstone, probably of the Chemung Formation. The strata underlying the dam may be dipping slightly to the southeast on the southern limb of the Rome Anticline which extends northeast from Friendsville and fades out near Hallstead.





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