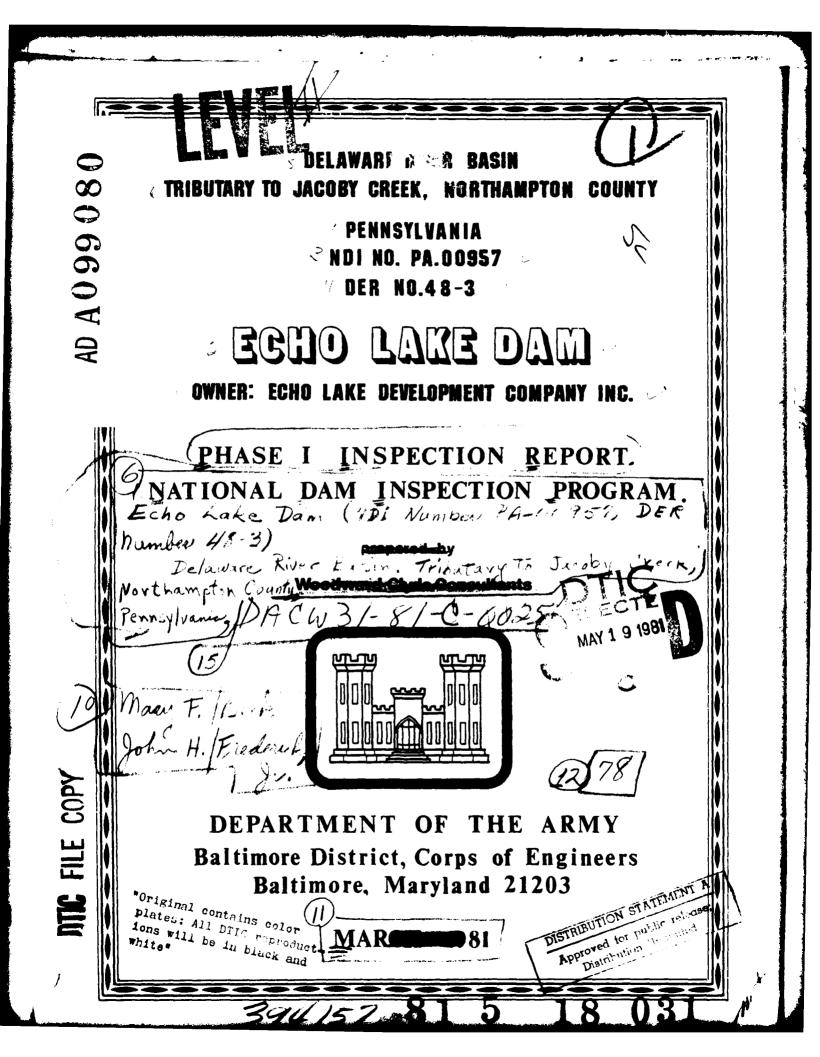
000 2000 200	÷						
				7	1		
			3		£.,		
					END DATE FILMED 6-81 DTIC		



DELAWARE RIVER BASIN

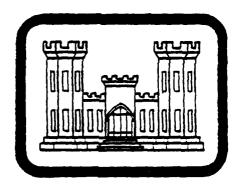
And the second second

TRIBUTARY TO JACOBY CREEK

ECHO LAKE DAM NORTHAMPTON COUNTY, PENNSYLVANIA

> NDI NO. 00957 DER NO. 48-3

PHASE I INSPECTION PROGRAM NATIONAL DAM INSPECTION PROGRAM



PELLO 10PH

Prepared by:

WOODWARD-CLYDE CONSULTANTS 5120 Butler Pike Plymouth Meeting, Pennsylvania 19462

Submitted to:

DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers Baltimore, Maryland 21203

March 1981

OUSTRIBUTION STATEMENT A

Approved for public release;

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of the Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to expeditiously identify those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify the need for more detailed studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected, and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the size and hazard classifications. The selected spillway design flood can range from the 100 Year Flood to the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff). The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

i

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam:	Echo Lake Dam
County Located:	Northampton County
State Located:	Pennsylvania
Stream:	Tributary to
	Jacoby Creek
Coordinates:	Latitude 40° 54.2'
	Longitude 75° 8.7'
Date of Inspection:	November 20, 1980

[Echo Lake Dam and Peservoir are used for recreational purposes. The dam and spillway structure of Echo Lake are currently in fair condition and the outlet structure is in poor condition.]

In accordance with criteria established by Federal (OCE) Guidelines, the recommended spillway design flood for this "Small" size dam and "Significant" hazard potential classification is the 100 Year Flood to one-half the Probable Maximum Flood. Based on the small capacity of the reservoir and the fact that no loss of life is likely during failure of the structure, the 100 Year Event has been selected as the spillway design flood.

Hydrologic and hydraulic computations presented in Appendix D indicate the spillway structure is not capable of discharging the 100 Year Event while confining dam outflow to the designed spillway. With the spillway notch closed (normal pool level), the right abutment area overtops by about 0.3 feet for an estimated five hours. Thus the spillway is considered "Inadequate". If the spillway notch is permanently open, the spillway would be considered "Adequate".

A DESCRIPTION OF A DESC

It is recommended that the following measures be undertaken immediately. Item (1) should be performed under the supervision of a registered professional engineer experienced in the design and construction of dams.

(1) The right abutment area would be the first area to experience overtopping; it should be evaluated from the standpoint of functioning as an emergency spillway. Alternatively, the stop log could be removed permanently.

ii

ECHO LAKE DAM, NDS I.D. NO. PA 00957

- Cracks in the spillway walls and slabs should be sealed to (2) prevent further damage.
- All trees and brush should be removed from the downstream (3) embankment face.
- The pond drain pipe should be fitted with an operational (4) control device at its upstream end.
- (5) Seepage through the dam should be monitored for the development of turbidity and increase in quantity.

Because of the potential for property damage in the event of failure, a formal procedure of observation and warning during periods of high precipitation should be developed and implemented for this facility. This procedure should be coordinated with local authorities and should include a method of warning downstream residents that high flows are expected. In addition, an operation and maintenance procedure should also be developed to insure that all pertinent items are carefully inspected on a regular basis and maintained in the best possible condition.

3/19/1 Date

Mary F. Beck, P.E. Pennsylvania Registration 27447E Woodward-Clyde Consultants

John H. Frederick, Jr., P.E. Dat

Maryland Registration 7301 Woodward-Clyde Consultants

APPROVED BY:

JAMES W. PECK blonel, Corps of Engineers District Engineer

2 APR 81 Date

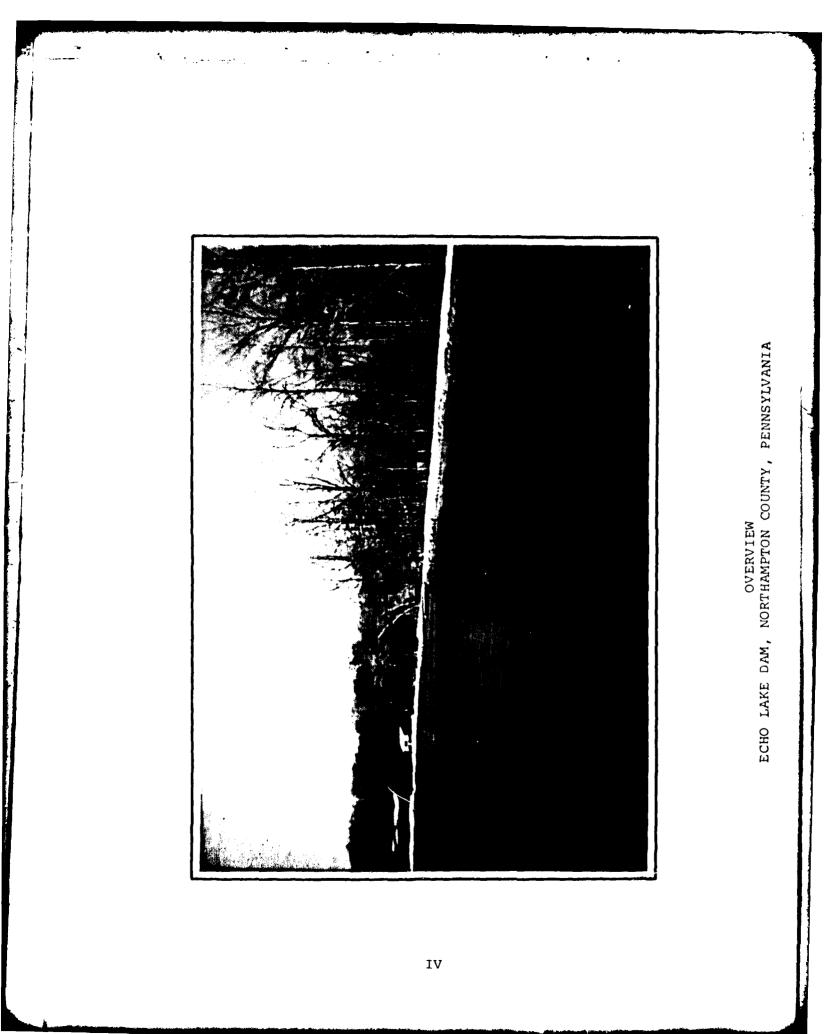


TABLE OF CONTENTS

. .

المراجع المراجع

-

Anna Maria and and

D300	
PAGE	

Preface Assessme Overview		and Recommendations otograph	i ii iv
SECTION 1.1 1.2 1.3		PROJECT INFORMATION General Description of Project Pertinent Data	1 1 3
SECTION 2.1 2.2 2.3 2.4		ENGINEERING DATA Design Construction Operational Data Evaluation	5 5 5 5
SECTION 3.1 3.2		VISUAL INSPECTION Findings Evaluation	6 8
SECTION 4.1 4.2 4.3 4.4 4.5		OPERATIONAL PROCEDURES Procedures Maintenance of the Dam Maintenance of Operating Facilities Warning Systems In Effect Evaluation	9 9 9 9
SECTION 5.1	5 ~	HYDROLOGY/HYDRAULICS Evaluation of Features	11
SECTION 6.1	6 -	STRUCTURAL STABILITY Evaluation of Structural Stability	13
SECTION 7.1 7.2	7 -	ASSESSMENT/REMEDIAL MEASURES Dam Assessment Remedial Measures	15 15
APPENDIX A B C D E F		Visual Inspection Engineering Data, Design, Construction and Operation Photographs Hydrology/Hydraulics Plates Geology	

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM ECHO LAKE DAM NATIONAL I.D. NO. PA 00957 DER NO. 48-3

SECTION 1 PROJECT INFORMATION

1.1 General.

a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.

b. <u>Purpose</u>. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

Echo Lake Dam is an earth Dam and Appurtenances. a. and rockfill dam approximately 10 feet high across the West Fork of Jacoby Creek. The approximately 550-foot long dam impounds a reservoir with an estimated total capacity of 80 acre-feet. The dam crest ranges from 11 to 16 feet wide and is covered by well maintained grass. The crest elevation ranges from 560.7 to 561.4. Surficial upstream embankment materials are broken shale and sod above the waterline. Wave erosion has created a near vertical face, exposing the underlying riprap. The upstream embankment slope below the waterline appears to be fairly flat. The downstream embankment slope ranges from 1.25H:1V to 2.25H:1V, typically about 1.65H:1V. Weeds and light brush are growing between the exposed rock. Small to moderate size trees are growing in the downstream area immediately adjacent to the toe of the dam.

A 49.4-foot wide spillway is located about the middle of the dam. The concrete broad-crest weir located at approximately the dam centerline has a low-flow notch approximately 2.5 feet wide by 14 inches deep. Downstream of the weir the spillway is concrete paving over rockfill. The spillway discharges into the stream bed at the downstream toe. A steel foot bridge crosses the spillway on the downstream side of the weir. About five feet to the right of the spillway is a 12-inch diameter cast iron pipe. Discharge through the pond drain is controlled by a gate valve at the downstream end of the pipe. Pond drain discharge would impact directly upon the ground surface at the toe of the dam. The inlet to this pipe is underwater to the right of the right spillway wall.

The abutments of Echo Lake Dam merge into lawn areas of residences around the lake. There is little topographic relief between the embankment crest and the left abutment. The right abutment is lower than the dam crest. Large flows would be expected to flow around the embankment before overtopping the embankment.

b. Location. The dam is located approximately 2.6 miles northeast of East Bangor in Upper Mount Bethel Township, Northampton County, Pennsylvania. Echo Lake is located on a tributary to Jacoby Creek approximately 3.3 miles upstream from its confluence with the Delaware River. The dam site and reservoir are shown on the USGS Quadrangle Map entitled "Stroudsburg, Pennsylvania-New Jersey" at coordinates North 40° 54.2', West 75° 8.7'. A Regional Location Plan is enclosed as Plate 1, Appendix E.

c. <u>Size Classification</u>. The dam is classified as a "Small" size structure by virtue of its less than 40-foot height and less than 1000 acre-foot total storage capacity.

d. <u>Hazard Classification</u>. A "Significant" hazard classification is assigned consistent with the potential for damage to downstream commercial and residential properties, but with few or no lives lost.

e. <u>Ownership</u>. The dam is owned by the Echo Lake Development Company, Inc. All correspondence should be addressed to Mr. Ralph L. Schlough, President, Echo Lake Development Company, Inc., RD #1, Box 1145, Bangor, Pennsylvania 18013.

f. <u>Purpose of Dam</u>. The dam and reservoir are used for recreational purposes.

g. <u>Design and Construction History</u>. Echo Lake Dam was built by the Portland Ice Company sometime before 1911. The "Report on the Condition of the Dams along Jacoby Creek," dated 1912, described Echo Lake Dam as about 600 feet long, a maximum height of 10 feet and with a spillway at the center of the embankment. The embankment was constructed of earth and field stones with side slopes of 1.5H:1V. The upstream face was riprap with loose stones and the crest of the dam was eight to 10 feet wide. It was noted that the reservoir area was previously a swamp and encompassed approximately 27 acres. The spillway was 49 feet long and two feet below the dam crest. It was reported that in 1911 the spillway had been rebuilt with a concrete upstream apron, weir crest and spillway walls. Downstream of the weir, the spillway was timber planking over rockfilled cribs. No leakage was noted and it was concluded that the dam appeared to be safe.

A 1919 inspection of the dam disclosed no evidence of embankment settlement but both spillway walls were cracked, with serious cracking at the left spillway wall. The timber planking on the downstream side of the spillway was rotted with missing planks. A small amount of leakage was noted and the downstream toe area of the embankment was described as being wet and swampy. A large tree on the downstream embankment slope immediately to the left of the spillway had blown over leaving a large hole. It was recommended that the hole be filled with clay or impervious material. The 1921 inspection report noted the hole filled with loose rock and stone.

Subsequent inspection reports of Echo Lake Dam noted swampy conditions downstream from the dam, seepage at various points along the embankment, poor condition of the spillway planking and also of spillway abutments. By 1934 the timber planking was replaced with concrete. The inspection report of 1938 noted leakage to the left of the spillway and a small stream flowing along the toe of the dam. In 1941, the inspection report noted settlement of the dam crest approximately 12 feet left of the spillway. It was commented that this settlement might be the result of leakage through the embankment.

h. <u>Normal Operating Procedures</u>. Under normal conditions, all flow is discharged over the spillway. The reservoir level is lowered in the late fall by removing the wooden stop log from the notch. Periodically, the lake level is lowered to permit maintenance to the bathing beach area.

1.3 Pertinent Data.

A summary of pertinent data for Echo Lake Dam is presented as follows.

a.	Drainage	Area	(square n	niles)	0.38
----	----------	------	-----------	--------	------

b.	Discharge at Dam Site (cfs)	
	Maximum Known Flood	50
	Tropical Storm Agnes, June 1972	
	At Minimum Embankment Crest	134
	At Minimum Abutment Elevation	150

с.	Elevation (feet above MSL) ⁽¹⁾ Top of Dam Right Abutment Area Along dam centerline Upstream of dam centerlin Spillway Crest (average) Spillway Notch Stream Bed at Spillway	560.7 560.1 560.3 559.9 558.6 550.6
đ.	Reservoir (feet) Length at Normal Pool Length at Maximum Pool (est) 1300 1350
e.	Storage (acre-feet) Normal Pool (est) Right Abutment Elevation (e Top of Dam (est)	est) 62 70 80
f.	Reservoir Surface (acres) Normal Pool	20.8
g.	Dam Data Type Length Slopes Upstream (above water lin Downstream (Average) Volume (est) Height (above stream bed) Crest Width Cutoff Grout Curtain	Earth and rockfill 545 feet (e) Near vertical 1.65H:lV 2100 cu. yd. 10.1 feet 11 to 16 feet Unknown Unknown
h.	Spillway Type Elevation at Crest (Average Notch Length	Concrete over rock 559.9 feet 558.6 feet 49.4 feet
í.	Pond Drain Type Length Inlet Invert Elevation Outlet Invert Elevation	l2-inch conduit with gate valve at down- stream end. Unknown Unknown 551.9

Anne and the second second

į

and the second

and the second second

(1) Right end of spillway weir assumed 560 feet from USGS map, all other elevations relative.

SECTION 2 ENGINEERING DATA

2.1 Design.

a. <u>Availability</u>. There are no original engineering data for Echo Lake Dam. A summary of subsequent evaluation data is presented on the checklist attached as Appendix B. Principal documents containing pertinent data used for this report are limited to periodic state inspection reports, correspondence and photographs. All of these data are contained within the Department of Environmental Resources (DER) files.

b. <u>Design Features</u>. A plan view and section of the dam are presented in Appendix E and profile is presented in Appendix A. This information was obtained from visual inspection. A summary of the design features is included in Section 1.3.

2.2 Construction.

Nothing is known concerning the construction history beyond the information given in Section 1.2, paragraph g.

2.3 Operational Data.

There are no operational records maintained for this dam beyond the periodic applications for permits to draw down the reservoir level.

2.4 Evaluation.

a. <u>Availability</u>. All information presented herein was obtained from DER files and supplemented by conversations with the owner's representative.

b. <u>Adequacy</u>. The available data are not adequate to evaluate the engineering aspects of this dam.

c. <u>Validity</u>. There is no reason to question the validity of the limited available data.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

a. <u>General</u>. The observations and comments of the field inspection team are contained in a checklist presented in Appendix A and are summarized and evaluated in the following subsections. In general, the appearance of the facilities indicates that the embankment and spillway is currently in fair condition and the outlet works are in poor condition.

The vertical alignment of the dam crest was h. Dam. checked and the profile is shown on Sheet 5B, Appendix A. There were no distortions in alignment or grade that would be indicative of movement within the embankment or foundation. The crest elevation ranges from 560.7 to 561.4. The minimum elevation of 560.1 is in the right abutment area beyond the embankment. The minimum elevation in the right abutment area upstream of the dam which must be overtopped before water can flow over the right abutment is 560.3. The crest width ranges from 11 to 16 feet and supports a well maintained growth of It was reported that broken shale covered with topsoil grass. and seeded, has been placed on low areas of the embankment crest and on damaged areas at the waterline. A bench, created by wave erosion, was observed at the summer water line on the upstream embankment face, occasionally exposing underlying riprap. A flatter upstream embankment slope covered with broken shale was observed below the water level.

Light brush and weeds were growing between rocks on the downstream slope. The downstream slope is about 1.65:1V. Steeper slopes (1.25H:1V) occur in areas appearing to have more boulders and cobbles exposed. Flatter slopes (2.25H:1V) were observed as the downstream face transitioned into the abutments.

Midway between the spillway and left abutment at the downstream toe was a set area with lush grass and standing water. Another wet area with ponded water and swampy vegetation was observed approximately 50 feet to the left of the spillway. This area extended to the spillway and about 50 feet downstream. Approximately 75 feet to the right of the spillway, another wet area was noted with standing water and lush grass. Near the downstream toe and slightly up the slope of the dam there were several trees growing ranging in size up to 12 inches in diameter.

c. Appurtenant Structures.

Spillway. The spillway is a concrete structure 1. 49.4 feet wide. The upstream slope is concrete and underwater. The downstream slope is concrete over rock fill. A concrete weir 18.5 inches wide and 16 inches high controls spillway discharge, Plate 3, Appendix E. The weir crest ranges in elevation from 560 to 559.8 and appears to be in good condition. Flow through a notch approximately 30 inches wide by 14 inches deep is controlled by a wooden stop log. A foot bridge across the spillway is about 18.5 inches above the weir crest. The original concrete upstream spillway walls were extended as diving board platforms and the phases of construction can be seen. The spillway walls are cracked. Only the anchor bolts The largest crack in the right spillway wall is remain. approximately one-inch wide, Photograph 5. The downstream The downstream spillway walls also showed occasional cracks. slap of the spillway has a five-inch step at about its midheight. There are several cracks noted in the spillway slab and pieces of concrete have apparently been broken off at the lower end of the slab. Cobbles and boulders underlie the spillway slab, Photograph 7. The spillway discharges directly into the downstream channel. No evidence of channel erosion or undermining of the spillway resulting from spillway discharge was noted.

2. <u>Outlet Works</u>. A 12-inch diameter metal pipe exits the downstream face of the dam approximately five feet to the right of the spillway. Discharge from the pipe impacts directly upon the ground surface at the downstream embankment toe. It was reported that the upstream end of this pipe is near to the right spillway wall and is protected by a screen. During the inspection, the downstream gate valve was exercised and found to be functional although the valve did not seat completely when in a closed position. Also a small crack was noted in the upper valve case such that small streams of water were spurting out. The crack was reported to be at least two years old.

d. <u>Reservoir</u>. The side slopes of the reservoir are at a moderate to gentle slope and are vegetated to the water's edge with grass and trees. There was very little debris noted along the shore line and very little sediment was observed entering the lake. The maximum depth was reported as six feet indicating sedimentation within the reservoir.

e. <u>Downstream Channel</u>. The channel downstream from the dam flows through a broad, flat, wooded, and occasionally swampy, flood plain. Immediately downstream from the dam, the channel is about 11 feet wide and the banks are approximately one-foot high. The valley gradient in the vicinity of the dam

-7-

is about 0.008. There are a few cottages located on the flood The closest residence is plain downstream of the dam. downstream of the embankment near the left abutment and has a floor level at approximately the dam crest elevation. About 48-4, 3000 feet downstream from Echo Lake is Lake Poco, DER No. which is formed by an earth dam approximately six feet high. About 1000 feet downstream from Lake Poco, the stream valley is constricted by an abandoned railroad embankment, such that flood flows would be confined to a small portion of the valley where a few residential dwellings are located. With the constriction on the valley, it is possible that a failure of Echo Lake Dam and, possibly, a consequent failure of Lake Poco Dam would cause damage to homes and buildings. Since no loss of life is envisioned, a "Significant" hazard classification for this structure is indicated.

3.2 Evaluation.

In summary, the visual inspection of the dam disclosed no evidence of incipient failure of the embankment. The embankment is judged to be in fair condition consistent with the trees and brush on the downstream slope and the wet and ponded areas at the downstream toe. Consistent with the reports in the DER file, this seepage is assessed to represent an apparently long-term condition which only requires monitoring for development of turbidity and increase in flow. Although the upstream embankment slope is damaged at the waterline, reported maintenance practices (see Section 4) have resulted in a minimum ll-foot top width, more than adequate for a l0-foot high dam.

The spillway structure appears to be in generally fair condition. This assessment is based upon the lack of any large scale dislocations or structural deficiencies although spillway cracking should be sealed to prevent further deterioration. The channel immediately downstream of the spillway should be checked after large flows for signs of channel erosion or spillway undermining. The outlet works are in poor condition consistent with the cracked valve case and the location of the valve at the downstream end of the outlet conduit.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures.

Normal operating procedures of Echo Lake Dam do not require a dam tender. The reservoir level is lowered during the winter by removing the stop log from the spillway notch. All flow is discharged over the spillway into a tributary of Jacoby Creek. There is no minimum downstream flow requirement.

4.2 Maintenance of Dam.

Dam maintenance provided by the Owner consists of mowing the grass and removing debris as required. Periodically, additional material is dumped on the upstream embankment face to restore the slope at the water line and protect against further wave erosion.

4.3 Maintenance of Operating Facilities.

The operating facilities associated with this structure are the stop log and the gate valve on the outlet conduit. Maintenance to these facilities is provided as needed and the valve is kept oiled and operational. The gate valve is scheduled for repair this spring (1981). The Owner provides the required maintenance.

4.4 Warning Systems in Effect.

There are no formal warning systems or procedures established to be followed during periods of exceedingly heavy rainfall. If potentially dangerous conditions are observed, the Owner's representative reported that the local police would be notified.

4.5 Evaluation.

It is judged that the current operating procedure, which does not require a dam tender, is a realistic means of operating the relatively simple control facilities of Echo Lake Dam.

There are no written operational or maintenance procedures or any type of warning system. Maintenance and operating procedures should be developed, including a checklist of items to be observed, operated, and inspected on a regular basis. Since a formal warning procedure does not exist, one should be developed and implemented during periods of extreme rainfall. This procedure should consist of a method of notifying residents downstream that potentially high flows are imminent or dangerous conditions are developing.

ţ

SECTION 5 HYDROLOGY/HYDRAULICS

5.1 Evaluation of Features.

a. <u>Design Evaluation Data</u>. There are no original design data for this construction nor subsequent evaluation data for the existing spillway section. The small irregularly shaped watershed is about 1.1 miles long and 0.3 mile wide having a total drainage area of about 0.38 square mile. Elevations range from a high of about 788 in the upper reaches to the normal reservoir level of about 559.9. The watershed is about 65 percent wooded with moderate residential development. While some residential development has recently occurred within the watershed, runoff characteristics are not expected to change significantly in the near future.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended Spillway Design Flood for this "Small" size dam and "Significant" hazard classification is the 100 Year Flood to one half the Probable Maximum Flood. Based on the relatively small capacity of the reservoir and the fact that no loss of life is likely during the failure of this structure, the 100 Year Event has been selected as the Spillway Design Flood.

b. <u>Experience Data</u>. No reservoir level records or rainfall records are maintained for this dam by the Owner. During Tropical Storm "Agnes" in 1972, the reservoir level was reported to just barely reach the top of the right abutment.

c. <u>Visual Observations</u>. At the time of the inspection there were no conditions observed that would indicate a reduced spillway capacity during an extreme event. Overtopping of the right abutment area could be detrimental to the embankment if discharge through the abutment area flows against the downstream toe causing erosion. Other observations regarding the condition of the downstream channel, spillway and reservoir are located in Appendix A and discussed in greater detail in Section 3.

d. Overtopping Potential. The overtopping potential of this dam was estimated using the HEC-1 Dam Safety Version Computer Program. A brief description of the program is included in Appendix D. Calculations for this investigation indicate a maximum spillway capacity of 134 cfs with the stop log in place and 151 cfs without the stop log when the reservoir level is at 560.7, the minimum embankment elevation. Spillway discharge is reduced to 33 and 50 cfs, respectively, when the reservoir level is at 560.3, the elevation at which the right abutment area overtops. The 100 year peak inflow rate was calculated by the computer program as about 188 cfs. This value was checked against the peak inflow value as determined according to procedures contained in "Regional Frequency Study, Upper Delaware and Hudson River Basins, New York District" which resulted in an estimated peak inflow value of about 197 cfs. The computer program indicates that the 100 Year Event will not overtop the embankment. However, the low area at the right abutment, noted on Sheet 5B, Appendix A, will overtop by about 0.3 feet for an estimated five hours with the stop log in the spillway notch. The abutment will not overtop if the notch is left open.

e. <u>Spillway Adequacy</u>. The reservoir level with the spillway notch closed is considered the normal pool level. The spillway is considered to be "Inadequate" as it will not pass the spillway design storm while dam outflow is confined to designed spillways. If the spillway notch is permanently open, the spillway would be considered "Adequate".

Downstream Conditions. f. Immediately downstream of the dam are a few cottages located on the flood plain. About 3,000 feet downstream of Echo Lake is Lake Poco Dam whose spillway is 36.5 feet wide and 23 inches deep with an estimated maximum capacity of 210 cfs. The top of Lake Poco Dam is about two and one-half feet above the first floor of a house downstream of the dam. About 1,000 feet downstream from Lake Poco Dam the stream valley is constricted by an abandoned railroad embankment, thus, flood flows would be confined to a small portion of the valley where residential dwellings are located. It is considered likely an Echo Lake Dam failure and possibly a Lake Poco Dam failure would cause damage to the homes and buildings. Since no loss of life is envisioned, a "Significant" hazard classification for this structure is indicated.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

a. <u>Visual Observations</u>. Visual observations indicate no evidence of existing or pending embankment instability other than that which would result from overtopping. The visual portions of the upstream face and downstream face of the dam appeared to be in fair condition. The concrete spillway cracking does not appear to be serious. The cracks should be sealed to prevent further damage. Although there is no energy dissipator at the spillway discharge, no channel erosion or spillway undermining was noted. The area should be checked after large spillway discharges for signs of undermining or erosion.

Evidence of seepage was observed during the visual inspection. Seepage has been noted in the state inspection reports since 1919. As no evidence of migration of fines through the embankment was noted, the seepage is assessed to represent a long-standing condition for this dam.

b. <u>Design and Construction Data</u>. No design or construction data exist other than the observations and reports concerning spillway reconstruction in the Department of Environmental Resources files. All data concerning the physical features of the dam were obtained from these reports, visual observations of the dam and conversations with the Owner's representative.

c. <u>Operating Records</u>. There are no operational records for this structure.

d. <u>Post-Construction Changes</u>. As discussed in Section 1.2, paragraph g, post-construction changes to Echo Lake Dam are limited to reconstruction of the spillway. No reference is made to a pond drain until 1923, therefore, the 12-inch pond drain may not be original.

e. <u>Embankment Stability</u>. There were no embankment stability evaluations in the files. Based on the low dam height, fairly wide crest (ll feet minimum), even when combined with fairly steep (up to 1.25H:lV) embankment slopes, the dam appears to be stable at the present time, provided that significant overtopping does not occur and that seepage conditions do not change.

f. <u>Seismic Stability</u>. The dam is located in seismic zone 1. Normally it can be considered that if a dam in this zone is stable under static loading conditions, it can be assumed

safe for any expected earthquake conditions. Since the dam is qualitatively assessed to be stable at the present time under static loading conditions, it can also reasonably be considered to be stable under seismic loading conditions.

SECTION 7 ASSESSMENT/REMEDIAL MEASURES

7.1 Dam_Assessment.

a. <u>Evaluation</u>. Visual inspection indicates that Echo Lake Dam and spillway is in fair condition. The outlet works are in poor condition.

In accordance with criteria established by Federal (OCE) Guidelines, the recommended Spillway Design Flood for this "Small" size dam and "Significant" hazard classification is the 100 Year Flood to one half the Probable Maximum Flood. Based on the small capacity of the reservoir and the fact that no loss of life is likely during failure of the structure, the 100 Year Event has been selected as the Spillway Design Flood.

Hydrologic and hydraulic computations presented in Appendix D indicate the spillway structure is not capable of discharging the 100 Year Event while confining dam outflow to the designed spillway. With the spillway notch closed (normal pool level), the right abutment area overtops by about 0.3 feet for an estimated five hours. Thus the spillway is considered "Inadequate". If the spillway notch is permanently open, the spillway would be considered "Adequate".

b. <u>Adequacy of Information</u>. The combined visual inspection and simplified calculations presented in Appendix D were sufficient to indicate that further investigations are required for this structure if the use of stop logs is continued.

c. <u>Urgency</u>. It is recommended that the measures presented in Section 7.2 be implemented as specified.

7.2 Remedial Measures.

a. <u>Facilities</u>. It is recommended that the following measures be undertaken immediately. Item 1 should be performed under the supervision of a Registered Professional Engineer experienced in the design and construction of dams.

- (1) The right abutment area would be the first area to experience overtopping; it should evaluated from the standpoint of functioning as an emergency spillway. Alternatively, the stop log could be removed permanently.
- (2) Cracks in spillway and slab walls should be sealed to prevent further damage.

(3) All trees and brush should be removed from the downstream embankment face.

A

- (4) The pond drain pipe should be fitted with an operational control device at its upstream end.
- (5) Seepage through the dam should be monitored for the development of turbidity and increase in quantity.

b. Operation and Maintenance Procedures. Because of the potential for property damage in the event of a failure, a formal procedure of observation and warning during periods of high precipitation should be developed and implemented for this facility. This procedure should be coordinated with local authorities and should include a method of warning downstream residents that high flows are expected. In addition, an operation and maintenance procedure should also be developed to insure that all pertinent items are carefully inspected on a regular basis and maintained in the best possible condition.

-

-

A

APPENDIX

A

Sheet | of ||

CHECK LIST VISUAL INSPECTION PHASE I

· · ·

Name Dam <u>Echo Lake Dam</u>	
County_Northhampton	State Pennsylvania
NDI#DER#	Type of Dom <u>Earth</u> and <u>Rockfill</u>
Hazard Category <u>Significant</u>	_
Date(s) Inspection <u>Nov.</u> 20, 1980	
Weather <u>Sunny</u> Temperat	ture <u>40's</u>
Pool Elevation at Time of Inspection	559.9 M.S.L.
Tailwater at Time of Inspection 552	.7M.S.L.

Inspection Personnel:

Mary F. Beck (Hydrologist)	Vincent McKeever (Hydrologist)			
Richard E. Mabry (Geotechnical)	John H. Frederick, Principal (2/9/81)			
Raymond S. Lambert, (Geologist)				

Mary F. Beck Recorder

Remarks:

Mr. Ralph L. Schlough, President of Echo Lake Development Company, Inc., was on site and provided assistance to the inspection team.

Sheet 2 of II

.

.

.

CONCRETE/MASONRY DAMS

• . .

An and the second se

_----

OBSERVATIONS	REMARKS OR RECOMMENDATIONS
N/A	
N/A	
N/A	
N/A	
N/a	
	N/A N/A N/A

Sheet 3 of II

CONCRETE/MASONRY DAMS

** • • • • • •

		······
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	N/A	
STRUCTURAL CRACKING	N/A	- <u></u>
VERTICAL AND HORIZONTAL ALIGNMENT	N/A	
MONOLITH JOINTS	N/A	
CONSTRUCTION JOINTS	N/A	

Sheet 4 of II

EMBANKMENT

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS

SURFACE CRACKS

None observed

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE None observed

SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES None observed

VERTICAL AND HORIZONTAL ALIGN-MENT OF THE CREST Vertical alignment shown on Sheet 5B.

RIPRAP FAILURES

Riprap at water line has been covered with small shale fragments, covered with soil and grass established. Upstream slope has a one-foot bench at water line. Waves have eroded shale and exposed some underlying riprap.

Sheet 5 of 11

t

1

1

EMBANKMENT

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATION

Vegetation

The crest is protected by a good grass cover. The downstream slope is brush and tree covered. Some brush has been cut.

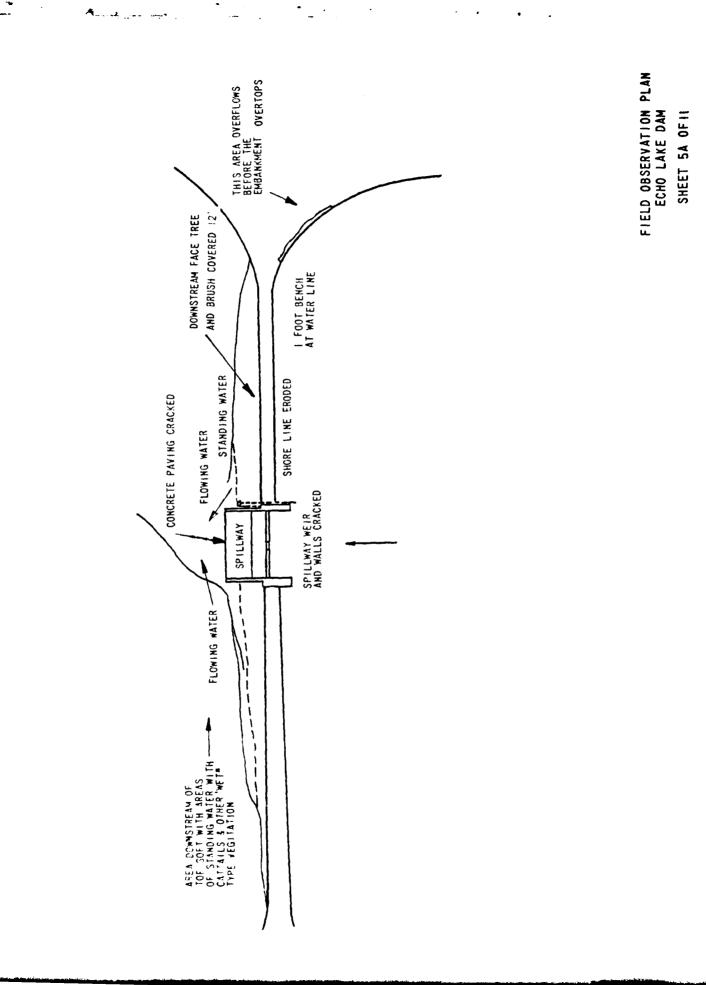
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM Good condition

ANY NOTICE-ABLE SEEPAGE Yes, see sheet 5A

STAFF GAGE AND RECORDER None

DRAINS

None



•

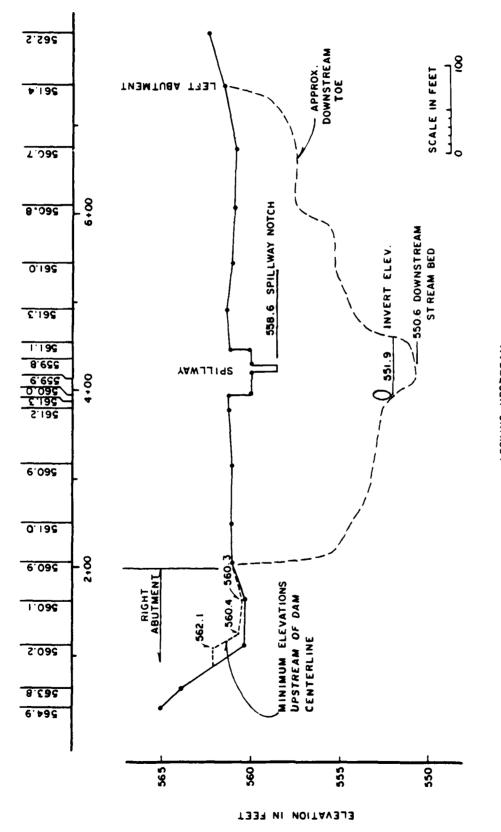
S.

SHEET 38 OF 11

. . .

PROFILE ALONG CREST ECHO LAKE DAM

LOOKING UPSTREAM



Sheet 6 of II

OUTLET WORKS

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS

N/A

CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT

.....

INTAKE STRUCTURE

Upstream end of conduit is under water and could not be seen.

OUTLET STRUCTURE

A 12-inch gate valve is at the downstream end of the conduit. The gate valve operated easily. Valve does not completely seat. The upper part of the Crane valve was cracked with water jetting out.

OUTLET CHANNEL

The conduit discharges into the channel below the spillway.

EMERGENCY GATE

The above.

Sheet 7 of II

UNGATED SPILLWAY

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS

CONCRETE WEIR The concrete broad crested weir has a 30-inch wide, 14-inch deep low flow notch. At the time of the inspection, a wooden board was in the notch. The lake level is lowered for the winter months.

APPROACH CHANNEL

A REAL PROPERTY OF A REAL PROPER

All at an and

None

DISCHARGE CHANNEL

The spillway discharges directly into the downstream channel.

BRIDGE AND PIERS

A foot bridge is 18.5 inches above the concrete weir. The bridge is supported by two sets of steel angle members.

Sheet 8 of II

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS TYPE N/A N/A APPROACH CHANNEL N/ADISCHARGE CHANNEL N/A BRIDGE AND PIERS N/A GATES AND OPERATION EQUIPMENT

GATED SPILLWAY

. .

na in the second

Sheet 9 of II

INSTRUMENTATION

• . .

.

٠

.

•

A Statement of the second s

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATION
MONUMENTATION/ SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
PIEZOMETERS	None	
OTHER	None	

Sheet 10 of 11

RESERVOIR

• • • • •

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS

SLOPES

And the second s

The reservoir side slopes are moderate and generally grassed to water's edge. Very little debris along shore line.

· .

•

SEDIMENTATION

Little sediment is coming into the lake.

WATERSHED

About 65 percent wooded with moderate residential development.

Sheet II of II

DOWNSTREAM CHANNEL

• .

VISUAL EXAMINATION OF OBSERVATIONS REMARKS OR RECOMMENDATIONS

CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)

And the second s

The downstream channel flows through a broad, wooded flood plain. The channel is about 10 feet wide with one-foot high banks.

SLOPES

The valley gradient is approximately 0.013.

APPROXIMATE NO. OF HOMES AND POPULATION About 3000 feet downstream of Echo Lake Dam is Lake Poco, a 6 foot high earth dam. About 1000 feet downstream of Lake Poco, the downstream valley is constricted by an abandoned railroad embankment, thus flood flows are confined to a small portion of the valley and it is considered likely an Echo Lake Dam failure, and possibly a Lake Poco failure, would cause additional damage to homes and buildings.

APPENDIX

B

Sheet 1 of 4

CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

•

NAME OF	DAM	Ech	o Lake	Dam			
NDI NO	PA	00957			DER NO.	48-4	
					_		
<u> </u>							
ITEM				RE	MARKS		

AS-BUILT DRAWINGS

None available

REGIONAL VICINITY MAP

Plate 1, Appendix E

CONSTRUCTION HISTORY

See text, Section 1.2

TYPICAL SECTIONS OF DAM

None available

OUTLETS - PLAN

DETAILS

CONSTRAINTS

No data avaílable

DISCHARGE RATINGS

ITEM	Sheet 2 of 4
RAINFALL/ RESERVOIR RECORDS	None maintained by Owner
DESIGN REPORTS	None
GEOLOGY REPORTS	See Appendix F
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	No original studies, see Appendix D for Hydrology/ Hydraulics evaluation.
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	None
POST CONSTRUCTION SURVEYS OF DAM	None known

ITEM	Sheet 3 of 4 REMARKS
BORROW SOURCES	Unknown
MONITORING SYSTEMS	None
MODIFICATIONS	Limited to replacement of spillway
HIGH POOL RECORDS	None
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None except state dam inspection reports
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None
MAINTENANCE OPERATION RECORDS	None

Sheet 4 of 4 TTEM REMARKS SPILLWAY PLAN SECTIONS DETAILS

OPERATING EQUIPMENT PLANS AND DETAILS

All a second sec

None

MISCELLANEOUS

The following are located in DER files.

 "Report on the Condition of the Dams along Jacoby Creek", Dated April 9, 1912. X

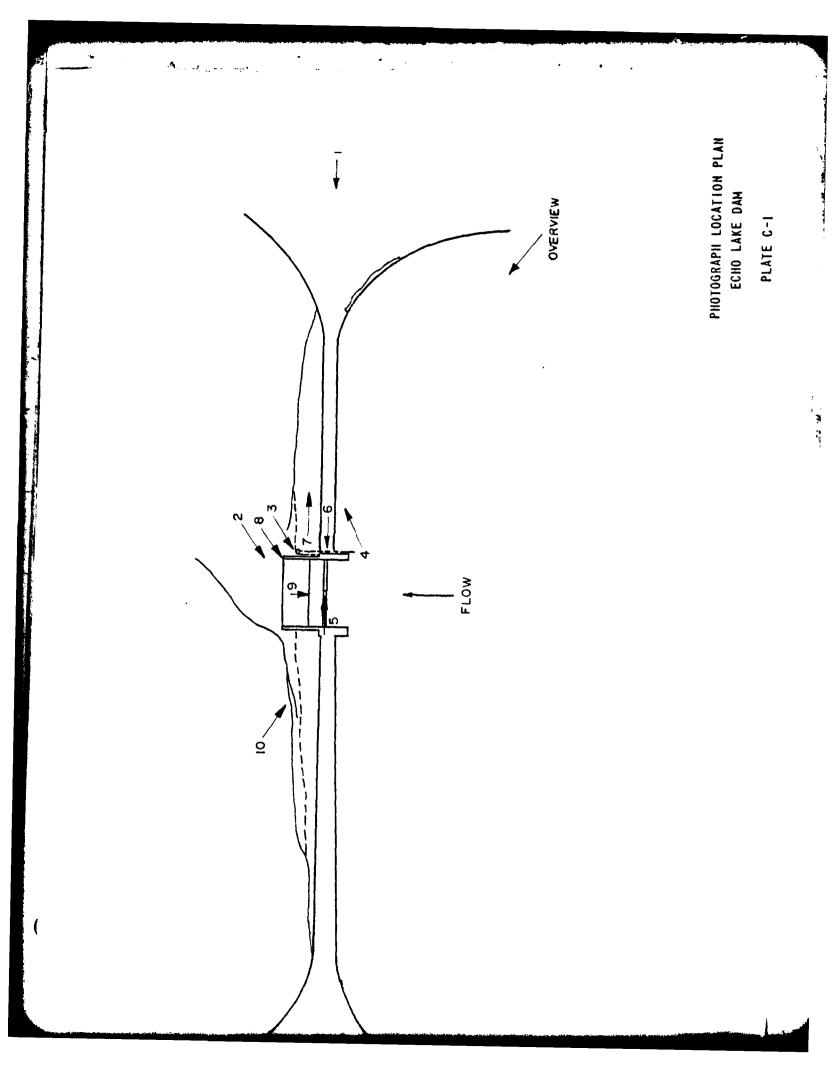
- 2. "Inspection Report Dams" from 1919 to 1964.
- Correspondence between the state and various owners of the dam.
- 4. Several "Application for Permit to Draw Dam"
- 5. Seven black and white photographs.

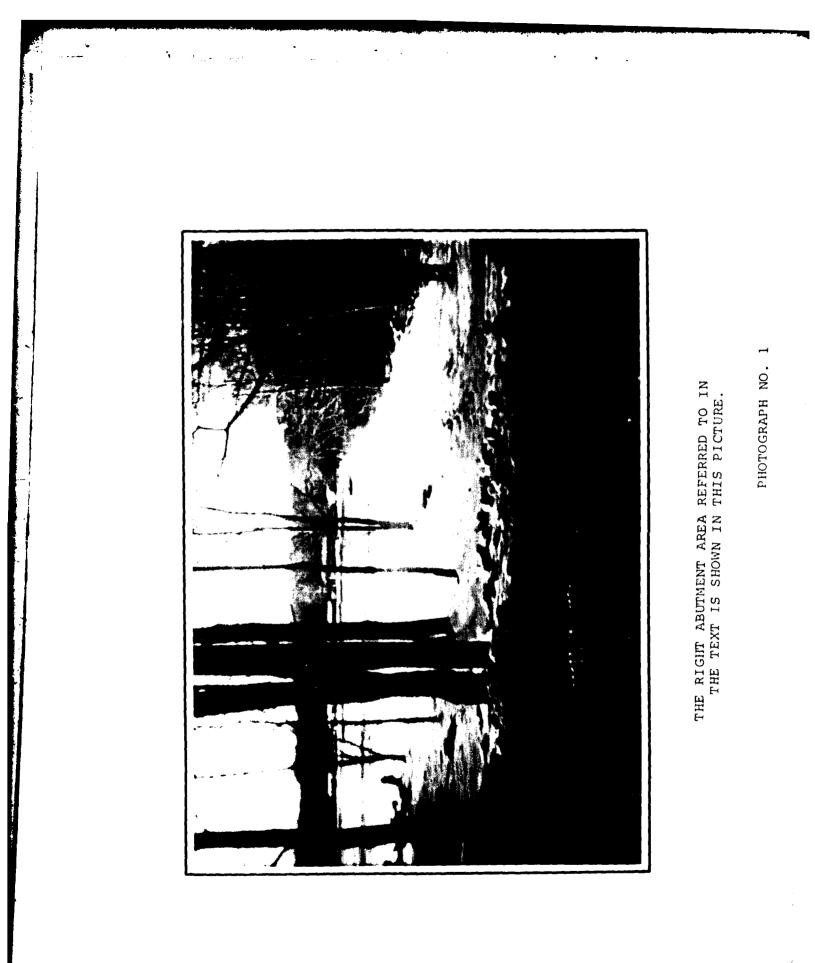
APPENDIX

A. S. S.

....

С







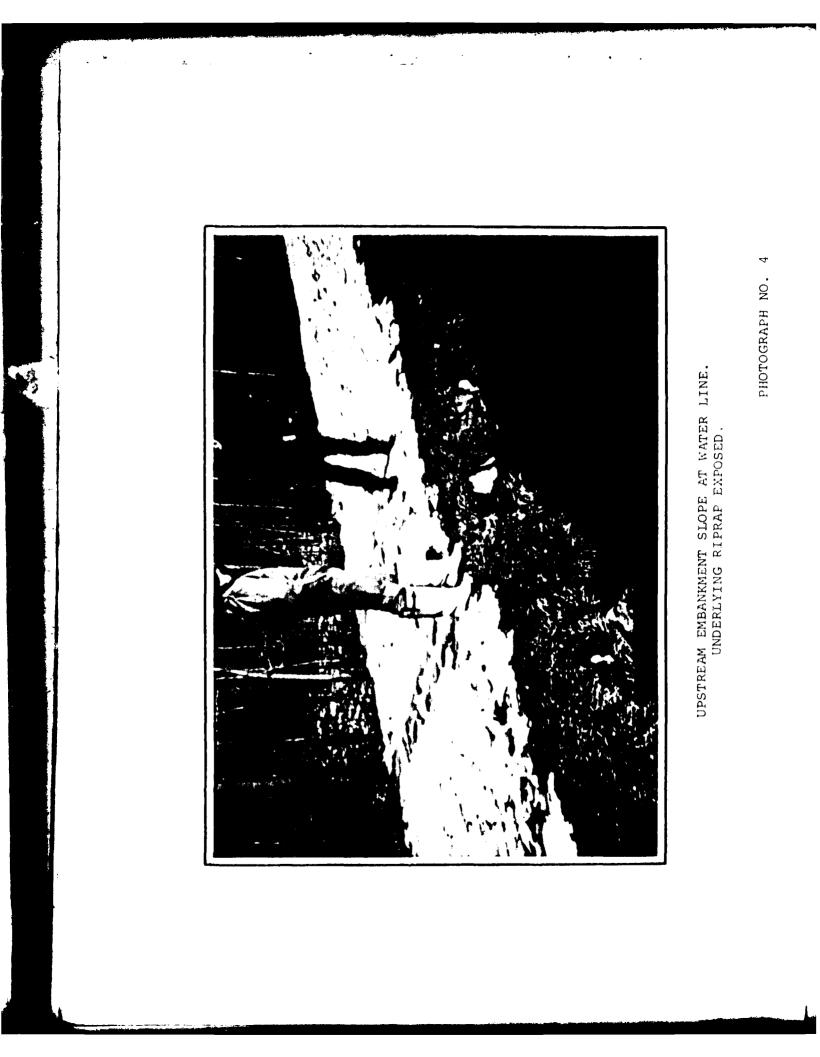
VIEW OF DOWNSTREAM SIDE OF SPILLWAY. POND DRAIN GATE VALVE ADJACENT TO NEAR SIDE OF SPILLWAY. PHOTOGRAPH NO. 2

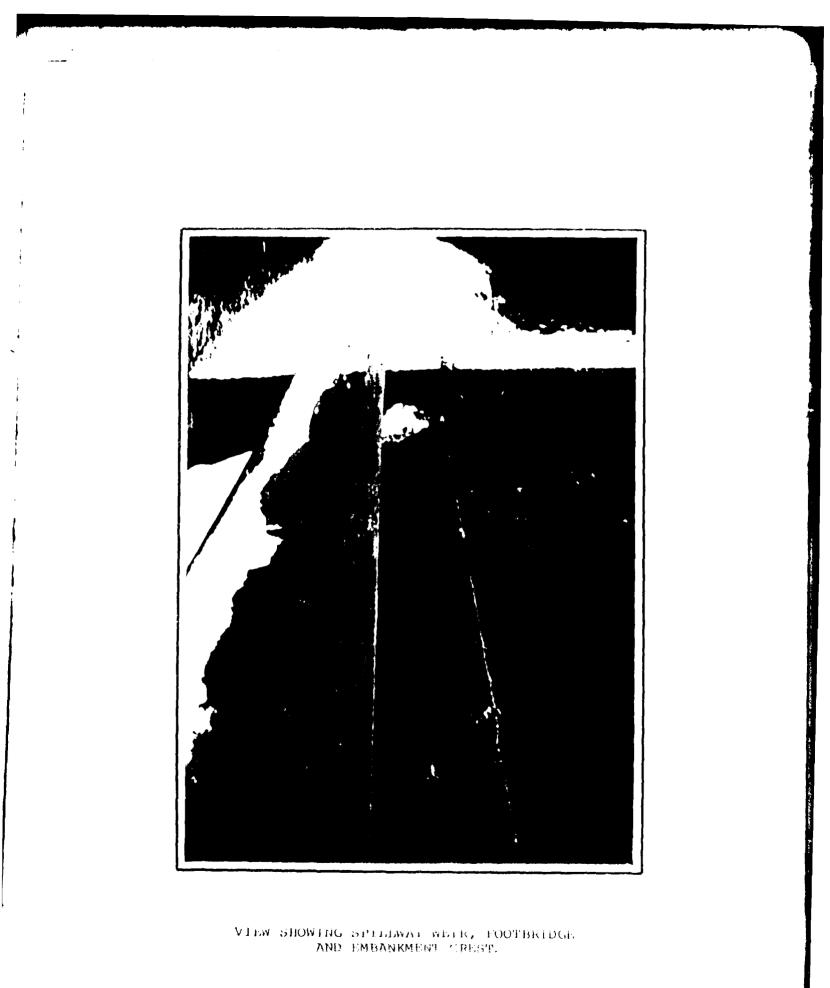
;

ļ



12-INCH GATE CALV. AL DOWNSTREAM FOR







SPILLWAY CREST SHOWING LOW FLOW NOTCH. NOTE CRACK IN SPILLWAY WALL.



TYPICAL DOWNSTREAM EMBANKMENT SLOPE. ROCK FILL SHOWS THROUGH SNOW.



.

1

1

(1) A submitted of the set of

· .

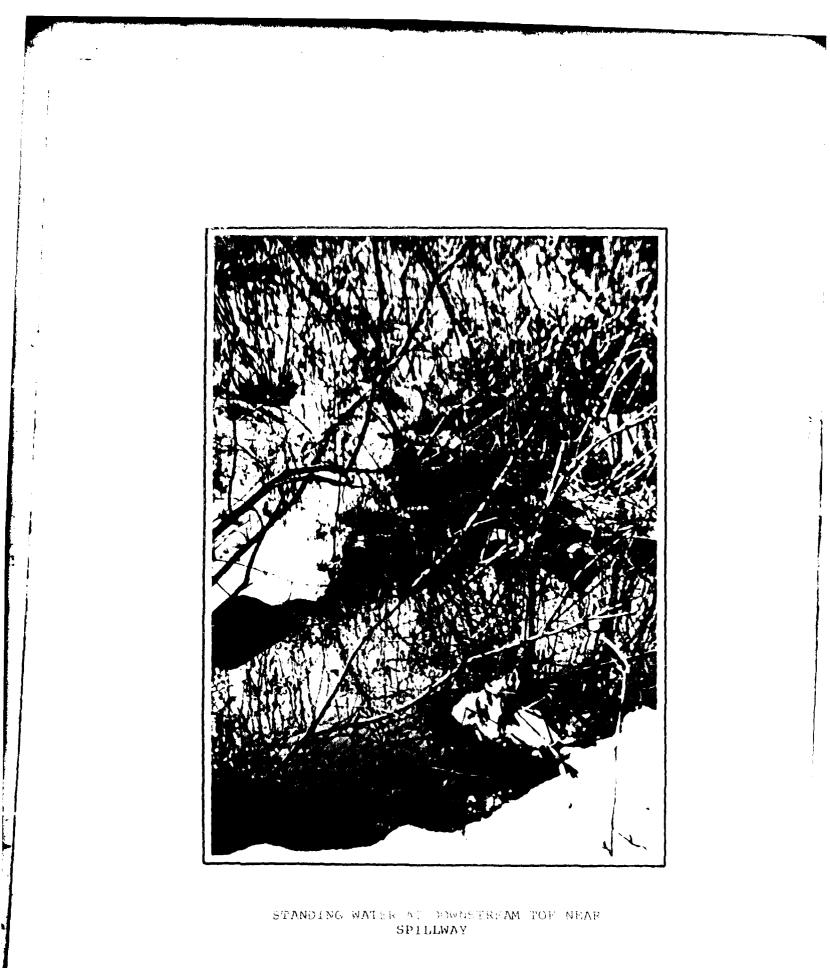


• .

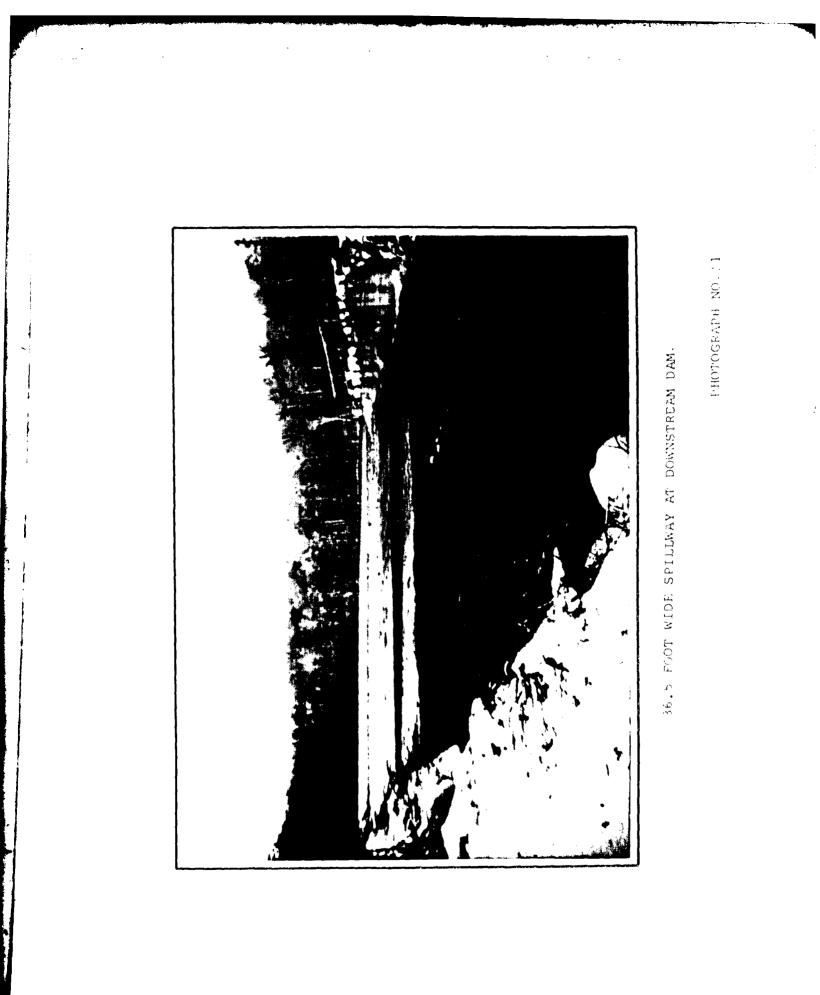
SPILLWAY CONCRETE PAVING CRACKS.

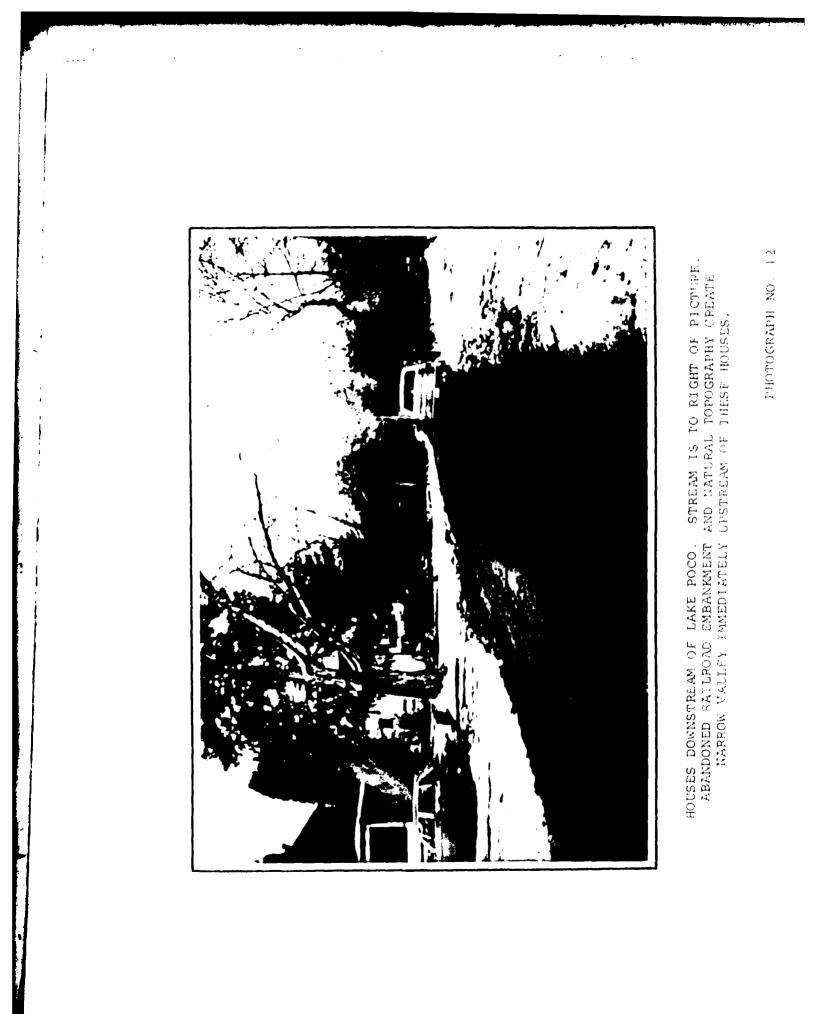
PHOTOGRAPH NO. 9

· · ·



PHOTOGRAPH NO. 10





APPENDIX

.,

.

D

ECHO LAKE DAM CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

.

٠

. • . · ·

•

÷.

.

DRAINAGE AREA CHARACTERISTICS About 65% wooded with moderate residential development
ELEVATION NORMAL POOL (STORAGE CAPACITY): 559.9* feet (62 Acres-feet)
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY):560.3 feet (70 Acre-feet)
ELEVATION MAXIMUM DESIGN POOL:
ELEVATION TOP DAM: 560.7 feet
SPILLWAY
a. Elevation 560 feet
b. TypeConcrete weir, with concreted fockfill chute
c. Width 49.4 feet
d. Length 36.5 feet
e. Location Spillover <u>Approximately 330 feet from right abutment</u>
f. Number and Type of GatesNone
OUTLET WORKS:
a. Type <u>12-inch pipe with gate valve at downstream end</u>
b. Location adjacent to right spillway wall
c. Entrance inverts Unknown, under water
, d. Exit inverts541.9 feet
e. Emergency draindown facilitiesthe 12-inch pipe
HYDROMETEOROLOGICAL GAGES:
a. TypeNone
b. LocationN/A
c. RecordsN/A
MAXIMUM NON-DAMAGING DISCHARGE: Not determined
*Right end of weir estimated as 560.0 feet from USGS map,

Sheet | of |4

:

FCHO LAKE DAM CHECK LIST HYDROLOGIC AND HYDRAULIC

Sheet 2 of 14

DRAINAGE AREA:(1)	0.38 sq. miles
100 YEAR PRECIPITATION ⁽²⁾	
30 MINUTES	2.3 inches
Hour	3.0
2 Hours	3.7
3 Hours	4.1
6 Hours	5.0
12 Hours	6.0
24 Hours	7.0
SNYDER HYDROGRAPH PARAMETE	Rs: ⁽³⁾
Zone	2
C _p , C _t 0.	45, 1.23
ر ⁽⁴⁾	1.37 miles
L _{cq} (5)	0.61 miles
$t_{p}=C_{t}(L\cdot L_{ca})^{0.3}$	1.16
SPILLWAY CAPACITY AT MAXIMUM	134 cfs

(1) Measured from USGS maps.

(2) TP 40 - Rainfall Frequency

Atlas of the United States

(3) Information received from Corps of Engineers, Baltimore District.

(4) Length of longest water course from outlet to basin divide, measured from USGS maps.(5) Length of water course from outlet to point opposite the centroid of drainage area, (see Plate 1, Appendix E) measured from USGS maps.

(6) See Sheet <u>11</u> of this Appendix.

SHEET 3 of 14

HEC-1, REVISED FLOOD HYDROGRAPH PACKAGE

The original "Flood Hydrograph Package" (HEC-1), developed by the Hydrologic Engineering Center, Corps of Engineers, has been modified for use under the National Dam Inspection Program. The "Flood Hydrograph Package (HEC-1), Dam Safety Version", hereinafter referred to as, HEC-1, Rev., has been modified to require less detailed input and to include a dam breach analysis. The required input is obtained from the field inspection of a dam, any available design/evaluation data, relatively simple hydraulic calculations, or information from the USGS Quandrangle maps. The input format is flexible in order to reflect any unique characteristics of an individual dam.

HEC-1, Rev. computes a reservoir inflow hydrograph based on individual watershed characteristics such as: area, percentage of impervious surface area, watershed shape, and hydrograph characteristics determined from regional correlation studies by the Corps of Engineers, Baltimore Dist-rict. The inflow is routed through the reservoir using spillway discharge data obtained from the field inspection or design data. Flood storage capacity is determined from USGS maps or design information and verified by the field inspec-In the event a spillway cannot discharge 0.5 PMF tion. without overtopping and failure of the dam, downstream channel characteristics obtained from the field inspection and USGS maps are inputed and flows are routed downstream to the damage center and a dam breach analysis is performed. If the 100 year event is selected as the appropriate spillway design flood, the peak inflow value is correlated with other studies by adjusting hydrograph parameters.

Included in this Appendix are the HEC-1, Rev. pertinent input values and a summary print-out tables.

BY PFM DATE 2/25/81	SUBJECT	SHEET OF 14
CHKD. BY MEB DATE 2/24/81	ECHO LAKE DAM	JOB NO
	HYDROLOGY HYDRAULICS	

CLASSIFICATION (REF. - RECOMMENDED GUIDELINES FOR SAFETY INSPECTION OF DAMS)

- I. THE HAZARD GLASSIFICATION IS RATED AS "SIGNIFICANT" AS THERE WOULD BE APPRECIABLE ECONOMIC LOSS WITH FEW OR NO LIVES LOST IN THE EVENT OF FAILURE OF THE DAM.
- 2. THE SIZE CLASSIFICATION IS "SMALL" BASED ON ITS 10.1 FT. HEIGHT AND LESS THAN 1000 AC-FT. TOTAL STORAGE CAPACITY.
- 3. THE SELECTED SPILLWAY DESIGN FLOOD, BASED ON SIZE AND HAZARD CLASSIFICATION, IS THE 100 YR. EVENT

HYDROLOGY AND HYDRAULIC ANALYSIS

- 1. NO ORIGINAL DATA OR SUBSEQUENT EVALUATION DATA ARE KNOWN TO EXIST
- 2. ELEVATION DISCHARGE DATA

A second se

SPILLWAY WIDTH 49.4 FT. CREST OF WEIR 18.5 IN. MAXIMUM DISCHARGE Q = CLH^{3/2} *

н	<u>c</u>	<u> </u>	Q
			0
1 1	260	49.4	4
	•		12
Ca			136
			423
	<u>Н</u> 0.1 0.2 1 2	0 0.1 2.62 0.2 2.62 1 2.75	0 0.1 2.62 49.4 0.2 2.62 " 1 2.75 "

IN WINTER, FLASH BOARD IS TAKEN OUT OF NOTCH IN SPILLWAY NOTCH WIDTH 2.5 FT. BOTTOM ELE. 558.6

* REF. HAND BOOK OF HYDRAULICS, BRATER AND KING, 1976, TABLE 5-3

WOCDWARD-CLYDE CONSULTANTS CONSULTING ENGINEERS, GEOLOGISTS AND ENVIRONMENTAL SUIENTISTS A. B. Same and

BY_PFM_DATE 2/25/81	SUBJECT	sheet <u>5</u> of <u>14</u>
CHKD. BY MES DATE 2/26/81	ECHO LAKE DAM	JOB No
	HYDROLOGY / HYDRAULICS	

	WINTER	WATER	LEVEL	WITH 2.5'	WIDE NOTCH
--	--------	-------	-------	-----------	------------

WATER	Low Flow Notch				Remainder of Spillway				
SURFACE	<u>c</u>	L	<u>_H</u>	व	<u> </u>	<u>L</u>	<u>H</u>	<u>q</u>	TOTAL
558.6				0				1	0
559.1	2.61	2.5	0.5	3.03					3
559.9	2.9	4	1.3	10.7			•	0	11
560.5	3.03	"	1.9	19.8	2.61	46.9	0.6	56.9	77
561.2	3.03	4.	2.6	31.8	2.9		1.3	201.6	233
562.0	3.03	4	3.4	47.5	3.03	"	2.0	401.9	449

3. EVALUATION DATA

RAINFALL AND SNYDER HYDROGRAPH PARAMETERS ARE SHOWN ON SHEET 2.

THE VALUE OF THE PEAK FLOW WAS CHECKED AGAINST THE VALUE OF THE 100 YR. INFLOW DETERMINED BY PROCEDURES CONTAINED IN "REGIONAL FREQUENCY STUDY, UPPER DELAWARE AND HUDSON RIVER BASINS, NEW YORK DISTRICT "BY THE CORPS OF ENGINEERS, NOVEMBER, 1974.

log (Qm) = Cm + 0.87 log AWHERE Cm = 1.65 FROM FIG. 2A = 0.38 SQ. MILES FROM USGS MAPlog (Qm) = 1.284S = Cs = 0.05 log ACs = 0.355 FROM FIG. 3S = 0.376g = + 0.5 FROM FIG. 5log (Qim) = log (Qm) + K(P,g) · SK(P,g) = 2.686 FROM PEARSON TYPE III DISTRIBUTION(STANDARD TABLE FOUND IN MOST HYDROLOGY TEXTS)log (Qim) = 1.284 + 2.686 · 0.376= 2.294

BY_PFM_DATE 3/16/81	SUBJECT	SHEET OF 14
CHKD. BY HFB DATE 3/19/87	ECHO LAKE DAM	JOB No
	HYDROLOGY / HYDRAULICS	

ELEVATION - STORAGE DATA

· .

And a series

ELEVATION	SURFACE AREA (ACRES)
551.0	0
559.9	21
560.0	23
562.0	25 (est)

THESE AREAS WERE OBTAINED FROM USGS MAPS.

4. RESULTS OF COMPUTER ANALYSIS

THE PEAK INFLOW (QIOD) CALCULATED BY THE HEC-1 PROGRAM IS 188 2FS, WITHIN 570 OF THE VALUE COMPUTED ABOVE, THE PROGRAM INDICATES THAT THE 100 YR. EVENT WILL NOT OVERTOP THE EMBANKMENT, HOWEVER, THE LOW AREA AT THE RIGHT ABUITMENT, NOTED ON SHEET 58, APPENDIX A, WILL OVERTOP BY ABOUT 0.3 FEET FOR MORE THAN 5 HOURS WITH THE STOP LOG IN THE SPILLWAY NOTCH. THE ABUTMENT WILL NOT OVERTOP 15 THE SPILLWAY NOTCH IS LEFT OPEN.

5. SPILLWAY ADEQUACY

THE RESERVOIR LEVEL WITH THE SPILLWAY NOTCH CLOSED IS CONSIDERED THE NORMAL POOL LEVEL. THE SPILLWAY IS CONSIDERED TO BE "INADEQUATE" AS IT WILL NOT PASS THE SPILLWAY DESIGN STORM WHILE DAM OUTFLOW IS CONFINED TO DESIGN SPILLWAYS, IF THE SPILLWAY NOTCH IS PERMANENTLY OPEN, THE SPILLWAY WOULD BE CONSIDERED "ADEQUATE"

MAXIMUM TAILWATER ELEVATION DURING THE SPILLWAY DESIGN FLOOD, BASED ON MAXIMUM STAGE AT DOWNSTREAM STATION DS 1, 13 549.1. THE DOWNSTREAM STAGE JUST PRIOR TO OVERTOPPING IS ABOUT 548.7.

KUN BAFE* 81/02/24. |IME* 12.55.42. ECHU LAKE DAM Nui No. Pa 00957 der Nd. 48-3 Overtopping Analysis

• .

.**--** .

و. هره، ما

A____2

Ę

	NSTAN	•		
	I N A I	- 4		
	IPLT	0		
N	NETRO	0	TRACE	0
IFICATIO	ININ NEV	0	L K U F T	0
JOH SPECIFICATION	IHR	0	NUT	0
	IDAY	0	JOFER	T
	NINN	15		
	NHR	0		
	NU	100		

NULTI-PLAN ANALYSES TO BE PERFURMED NPLAN= 1 NRTID= 1 LRTID= 1

,

•

KTI0S= 1.00

SUB-AREA RUNDEF COMPUTATION

A.

and the second

- Annine

-t₂

•• :• •

INFLOU HYDRUGRAPH - 100 YR STORM

1AU10 0 0 INAME 1STAGE ----JPRI 0 JPUI 0 ICOMP IECON LIAFE 0 0 0 ISTA0 N

0 LOCAL. ISANE **ISNUN** 0 **KATIO** 0.00.0 1.00 HYDROGRAPH DATA TRSPC .38 TKSDA SNAP 0.00 IAKEA .38 10HG -1H7DG 0

ANTLY 0.00 ALSAX 0.00 CNSTL 1.00 SIRIL 1.50 STRKS RIDK 1.00 LOSS DATA 0.00 EKALK 0.00 RTIOL 1.00 DL IKR 0.00 5 I K K K 0.00 LKOFT 0

NIA= 0 UNIT HYDROGRAPH DATA CP= .45 1.16 =dl

k1108= 2.00 --.50 RECESSION DATA ORCSN= -1.50 51610=

.45 VOL: 1.00 UNIT HYDROGRAPH 43 END-OF-PERIOD ONDIRATES, LAG= 1.17 HOURS. CP=

· · · · · ·· · · · · 59. 16. ÷. .-6.'. . 17 88. 43. 27. 84. 30. 2. 59. 35. 3 -30. 40. 3. - 4 5 . . -

1055 RALN EXCS NU.UA HR.AN PERIOD ENU-OF-FERIOD FLOW CUMP 0 1055 EXCS KAIN MU.BA HK.MN FEKIUD

021 021 021 021 021 022 023 .021 .021 .021 .041 .042 .042 .021 .021 .021 .021 .021 .041 .021 .021 .021 .021 .021 .021 .021 .021 .021 .021 .021 .021 .041 .041 .041 .021 .021 .021 1.0. 120. 120. 10 1.0. 1.0. 10 1.0. 1.0. 10 1.0. 25. 10 21. 25. 15 21. 021. 021 1.021. 1021 96 7.0 .021 .021 .02 01 .02

5

Y ... R. P. A.M. M.L. W. M.M. R. V.

120. 140. 140. 120. 120. 120. 120. 120. 120.

SHECT y 1 14

(11, 19) 514.

0.128.01 04.01 124.01

SUA 7.00 2.11 4.89

CUNE R

KOULING
нүркобкагн і

•

-

Istant Istont Istont<				OUTFL	AUY NU	OUTFLUN HYDROGRAPH - EXISTING CONDITIONS	- EXISI	114G C0	11111	1,45		
BLDSS CLOSS AVU IRES IDAT IDA 0.0 0.000 0.000 1 1 1 0 0 851FS KSIFS KSIFS KSIFS KSIFS 156 0.000 550. 559.40 560.00 560.10 560.70 551.70 0.000 550. 559.40 560.00 560.10 560.70 551.70 0.000 550. 0.00 4.00 12.00 136.00 423.00 0.000 550. 0.0 21. 23. 54. 112. 25. 0 0.00 0.0				LS CAU DUT		IE (M 114		JFL.T 0	JPRI I	151A6F 0	1,411,11,1 Ú
NSIFS NSIFL LA6 ANSKK N ISh Jikk J			0°0 55070	000.0 0.000	4Vb 0.00	4	5 154 1		10F1 0	1Frail 0	151 0	
559.40 560.00 560.10 560.40 551.40 0.00 4.00 12.00 136.00 425.00 0. 21. 23. 25. 0. 62. 64. 112. 550. 550. 550. 552. 551. 550. 550. 552. 112. 550. 550. 550. 552. 112. 114. 0. 1/5. 550.7 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0				NSTPS 1				385 200 û	х 000.(151, 0.000.0		
0.00 4.00 12.00 136.00 425.00 0. 21. 23. 25. 0. 62. 64. 112. 550. 550. 552. 551. 550. 552. 552. 552. 552. 112. 552. 64. 112. 552. 64. 112. 555. 112. 11		9.40	560.00		160.10	560.	05-	. 161.	,90			
0. 21. 23. 25. 0. 62. 64. 112. 551. 560. 550. 552. 551. 560. 550. 552. 559.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 10.11 0.0 0.0 0.0 0.0 0.0 0.0 0.0 11. 0. 175. 350. 0.0 0.0 0.0 0.0 0.0 0.0 12. 550.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 13. 550.1 0.0 0.0 0.0 0.0 0.0 0.0	2	0.00	4.0(~	12.00	136	.00	42.5	00			
0. 62. 64. 112. 551. 560. 560. 552. 551. 560. 552. 552. CKEL SFUID 600. 600. 0.0 CKEL SFUID 600. 6.0 0.0 0.0 559.9 0.0 0.0 0.0 0.0 0.0 0.0 6. 1/5. 560.7 0.0 0.0 0.0 5.0 5.0 0. 1/5. 5.0.1 0.0 0.0 0.0 5.0 5.0 0. 1/5. 5.0.1 0.0 0.0 5.0 5.0 5.0	E AKEA=	0.		. 13	23.	5						
551. 550. 550. 552. CKEL SPUID CONU EXPL FRUL 1011 LANTA CKEL SPUID CONU EXPL FRUL 1011 LANTA 559.9 0.0 0.0 0.0 0.0 0.0 0.0 bin bin 10FLL CONU EXPL DAMUTE 560.7 0.0 0.0 0.0 0.0 5.00.3 1.61.0 561.1 1.5.0	₽ÂŬITY=	.0		52 -	ó ł.	112						
CHEL SFWIN COUL EXEV EXEV EXEV EXEV EAD EAD <thead< th=""> EAD EAD <the< td=""><td>VATION=</td><td>551.</td><td></td><td>·0.</td><td>560.</td><td>503</td><td></td><td></td><td></td><td></td><td></td><td></td></the<></thead<>	VATION=	551.		·0.	560.	503						
6.00 1.01 10.01 560.7 0.0 0.0 500.3 10.1 500.3 10.1 10.1 10.1 10.0			2255				E XI N 0 0	61 EVI v. (1.1X 9.0	
0. 175. 350. 5a0.3 561.0 561.1						10FL. 560.	5	-	ли ЕхРи 0.0	DANUTN 0,		
5a0.3 (51.0 (561.1	SI LENGTH		.0	1/5.	300-		10.					
	UK BELUW Vâljun			0-191	1.161.1		0					

mar 1 .1

					A NROAR	нистина Каларарны	-							1
				SECTION 300		FEET DOURSTREAM OF BAN	n uf la	E						
			ISTAU DS1	I COMP 1	IECUN 0		0 1 741	0 1 X-IC	LNAME I	151A6E 0	() (i H I 0			•
		0.0 0.0	000°0 55073	AV6 0.00	KOUTI IKES 1	KOUTING DATA Es Isane 1 1 1	1011 0	7 7 7 0		0 1818				•
			NSTPS 1	0 NSTDL	LAG 0	ANSKK 0.000 0	x 0.000.0	15K (ылока О.	LSFKAT 0				•
NURMAL DEFT	NOKNAL DEFTH CHANNEL ROUTING	5 N J												
00.	анст) анс2) с .0/50 .0750 .	ur:3) .0750	ELNV F 548.0	ЕГМАХ Н 558.0	НГИТН 	. 00900								
C	CK055 SECTION COURDINATESSTA,ELEV,STA,ELEV 0.00 558.00 125.00 549.20 214.00 54 493.00 552.40 593.00 556.30 665.00 56	DRUTHATES 125.00 593.00	5STA,EL 549.20 556.30	.LEV,STA,E 214.00 665.00	ELEVETC 549.20 562.00	243.00	548.00	34.5.00	549.10					•
510KAGE	0.00	.11 11.80		.44 13.54	1.18	<u>47</u>	2.12 17.24	3.18 19.20	C1	4.36 21.25	5.64 25.34	7.05 25.49	8.55 27.70	
uuifrau	0.00 6287.788	12.33 7927.62	6	78.32 9747.24	27 4.35 11/49.27	637.20 13936.48	-	1148.75 16311.77	1808.71 18684.15	1808.71 8684.15	2021 . 44 21567.50	3591.75 24040.94	4825.20 27804.16	
51A6E	548,00 553.26	548.53 553.79		549.05 554.32	549.56 554.84	550.11 555.37	.11 .57	550.63 555.89	ניח ביי ביי כוי	551.16 556.42	351.68 506.75	552.21 557.47	552,74 558,00	• .
F L U U	0°0 82°7829	12.33	6	78.32 9747.24	274.35 11749.27	637.20 13936.48		1148.76 15311.79	180 1888	1808.91 18884.15	2621.44 21667.60	3571.73 24640.94	4825.20 27804.18	c
MAXIMUN STAGE	16E IS 547.1	_												

							LLME UF FALLUKL HOUKS	00-0	
						10F 0F BA M 560.70 80. 154.	TTME OF MAX OUTFLOU HOUKS	18,25	
(KS)	S#014_0				1515		BURATJÛN Övek Tuf Hours	0-00	ust Tine Hilles
AREA IN SOUARE MILES (SOUARE KILUNETERS)	KATIOS APPLIED TO FLOUS				BAN SAFETY ANAL Noten Closed	5P111.WAY CREST 559.90 62. 0.	MAX LMUM UUTELUU LES	1()4.	STAFTUN I nextnun starf.et
miles (sour	KALIL				10		MAXIMUM Sickage Ac-11	7 8 .	FLAN 1 NAXIMUN FLOREFS
AREA IN SOUAKE MILLES (SOUARE KILUNETEKS)	KATL0 1 1.00	188. 5.32)(104. 2.94)(104. 2.941(SUMMARY SPILL WAY	INIFIAL VALUE 559-20 62. 0.	NAXINUN DEFTH OVEK DAM	0.00	FL. PALLO
AFE	FLAN KA	- ~	1	- ~		ELEVATION STURAGE UUTFLUU	MAXIMUM Keservoik 4.5.elev	J 60.60	
	AREA	.38 .98)	.38	.98°.		2 2 2 3	KATLO A UF KE PMF H	1.00	
	SIATION	LN ,	00 T)	151			ά.Υ. Α. Α. Α. Α.	-	
	UP-ERALION	нуркобкарн ат	k0U1ED 10	kouteli To		FLAN 1			

• <u>-</u>~ ·

.

• -

PEAK FIND AND SIDKANE (END DE PERIDE) SUMMARY FOR NULTERE ELANGUIC COMPUTATIONS

.

SHEET ILST 14

18.25

549.1

104.

1.00

HYDRUGRAPH RUUTING

OUTFLON HYDROGRAPH - NUTCH DPEN, STOP LOGS REMOVED

.. . ..

•

.

-

			151AU 007	LCOMP 1		IECUN LIAFE	Ť,		JFK I 1	l nane 1	LINAME ISTAGE 1 0	LAUTU 0
		0°0 0'0	000°0 CL055	AV6 0.00		ULING D Isan	DI.		IFMF 0		0 TS1K	
			t Saten	NSTDL	LA6	AMSKK 0.000	К X 0 0.000		000.0	510kà ~559.	15PKAT - 1	
SIA0E 558	3.50	559.10		559.90	560.50	50	561.20	••	562.00			
FLÚU 0	00.00	3.00		11.00	27.00	00	233.00	·	00°842			
SURFALE AREAs	.0	C1	21.	23.	25.							
CAFACITY=	.0	ý0	62.	6- 1 .	-21							
elevatium=		τú	560.	560.	362.							
		GWEL 553.6		0*0 1711.45	0.0 0.0	0 0 0	0-0 0-1	0*0 010	CARÉG 0.0	ш	EXFL v.0	
					TOPEL. 540.7		1 11	30	U ANULU 0.			
LKEST LENGTH	0.		125.	350.	10.	. 0.						
HI UN BELUM Elèvatiun	540.5		561.0	561.1	562.0	0						

166 12-114

								2112	eri
						8.15 22.20	4825-20 27804-18	552.74 558.00	4625.20 20305.18
						\$0°. \$1°9	3591.73 24640.74	52,21 557,47	5591.75 2444 44
	1 A U I U 0					5 - 64 40 - 5 40 - 5	2621.44 21667.00	551.68 556.95	262].44 21467_00
	E ISTABE 1 0 LSTR 0 0	а Ізркан - 0			.10	4.36 21.25	1808.91 13884.15	551.16 556.42	1808.91
	I NAME 1	STURA 0.			343.00 547.10	18 20		55	
)AN	JPKI 0 1FMP 0	15K 00000				3.18 19.20	1148.25 15311.29	550.53 555.89	1148.76
AM UF I	0 1401 0 0	x 0 0 0 0			548.00	2.12 12.24	637.20 936.48	550.11 555.37	63/120 011/10
300 FEET DOUNSTREAM UF DAN	CUN LTAFE 0 0 0 Kouting Daia (es isame 1 1	Ariskk 0.000		.00900	C 243.00		537.20 13936.48	1 1 1 1 1 1 1 1	637.20 1307 30
300 FEET	ILCUN 0 rout ikes i	0 9 U T		КLИГН .300	.ELEVETC) 549.20) 552.00	1 18 15 - 55	274.35	544.58 554.84	2/4.35
SECTION	1 9,00 0,00	0 NSTUL		ELMAX 558.0	ELEV,STA,E 20 214.00 30 655.00	15.24	78.32 7747.24	549.05 554.52	5°8'.
	ISTAU 151 151 6L055 0.000	N51F5 1		ELNV 548.0	ES51A,EL 549.20 556.30		4		3
	0.0 81.055		17 LAG	(18 (3) . 0750	00.8.01.04.15. 0 125.00 0 593.00	.11.80	12.33	548.53 553.77	12.33
			ANNEL KOL	UN (2) . 0750	<pre>ck055 5EUTION COURDINATES5TA.ELEV,STA.ELEVETC 0.00 558.00 125.00 549.20 4Y3.00 552.40 593.00 556.30 665.00 552.00</pre>	0.00 16.14	0.00 0287.7820	548.00 555.26	00.0
			NORMAL VEFTH CHANNEL, KOUFLAG	4141 - 0750	CK01855 SE1 0.00 473.00	STUKAGE	ourflou o	5 linet	F L 04

•

HEET 11

PLAK FLUU AND STURAUE (END UP PERTUD) SUMMARY FOR MULTIFLE FLAR RATIO ECUNUNTI. COMPUTATIORS FLOUS IN CUBIC FEEL PER SECOND (CUBIC AETERS PER SECURD) AREA IN SQUARE MILES (SQUARE KILUMATERS)

j an

*

*

•

.

,

٠

TINE OF FATLURE HOURS

00.0

.

					TUP DF 14AM 560./0 80. 151.	11rtE 0F A.X BUTELOU HOUKS 20.75	
010 F LUND				117515		UURATIUN UVEK TUR HUURS 0.00	
RATIUS APPLIEM TO FLUDS				SUMMARY OF UGN SAFETY ANALYSIS Spilway Notch Open	58-11LUMAY СКЕ 5 1 36. 0.	MAXINUN UUTFLUU CFS 50.	
а А				IMMARY OF LIE SPILLWAY NO	IMITIAL VALUE 558.60 58. 0.	MAXINUM Slukabe AC-FI 70.	
ƙAII0 1 1.00	188. 5.32)(50. 1.43)(50. 1.43)(51	14171AU 558	MAXINUM Defith Dver Dam 0.00	
рган	_ ~	- ~	- ~		ELEVATIUN Stokaŭe Outflou	MAXINUM Keservoir U.S.Elev 550.25	
0N ÅREA	IN .38 (.48)	001	1151 .38 (3938)			KATLU DF HAG 1.00	
5 f Å I 1 0 k	I A I	0	9			-	
OFERALLUR	HYDROGKAPH AI	KUUTED IU	RUCLEN 10	_	FLAN		

MAXINUM MAXINUM TIME FLOW, 1545 STADE, FT HUUKG

kà f f û

20.70

548.8

50.

1.00

FLAN 1 STALLON

051

۲ 1 :

ן א ו

APPENDIX

•

. .

4

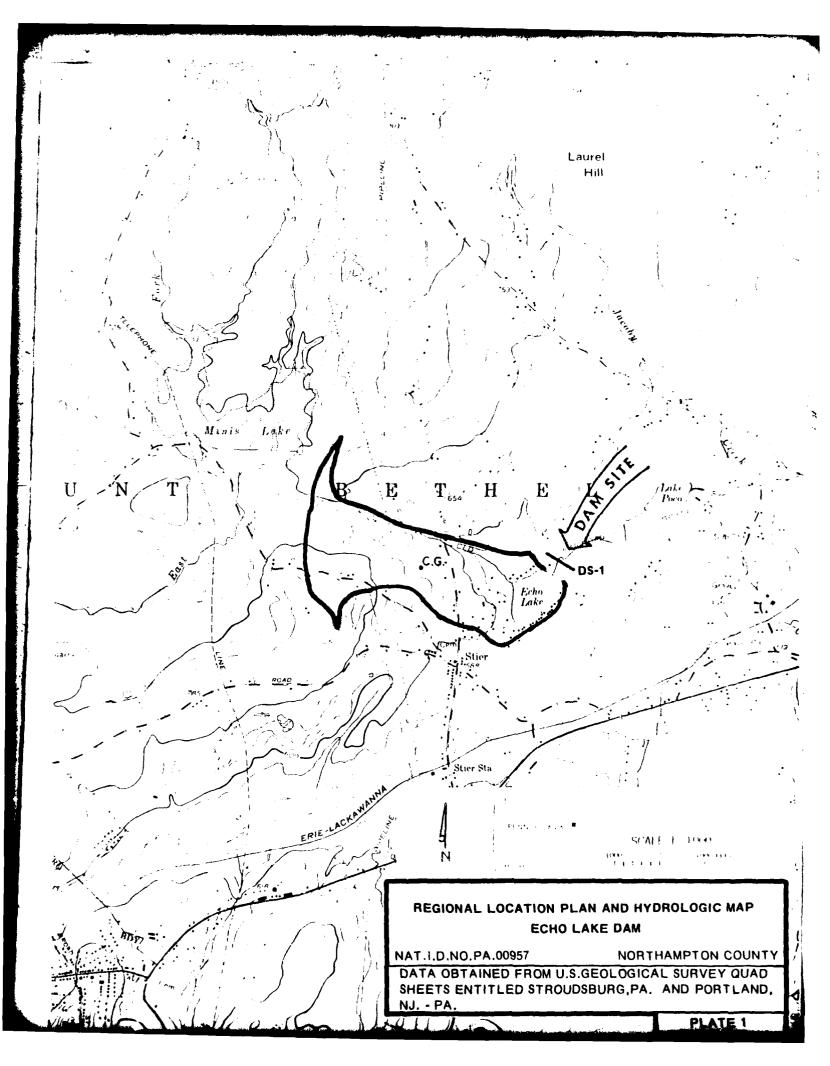
× .

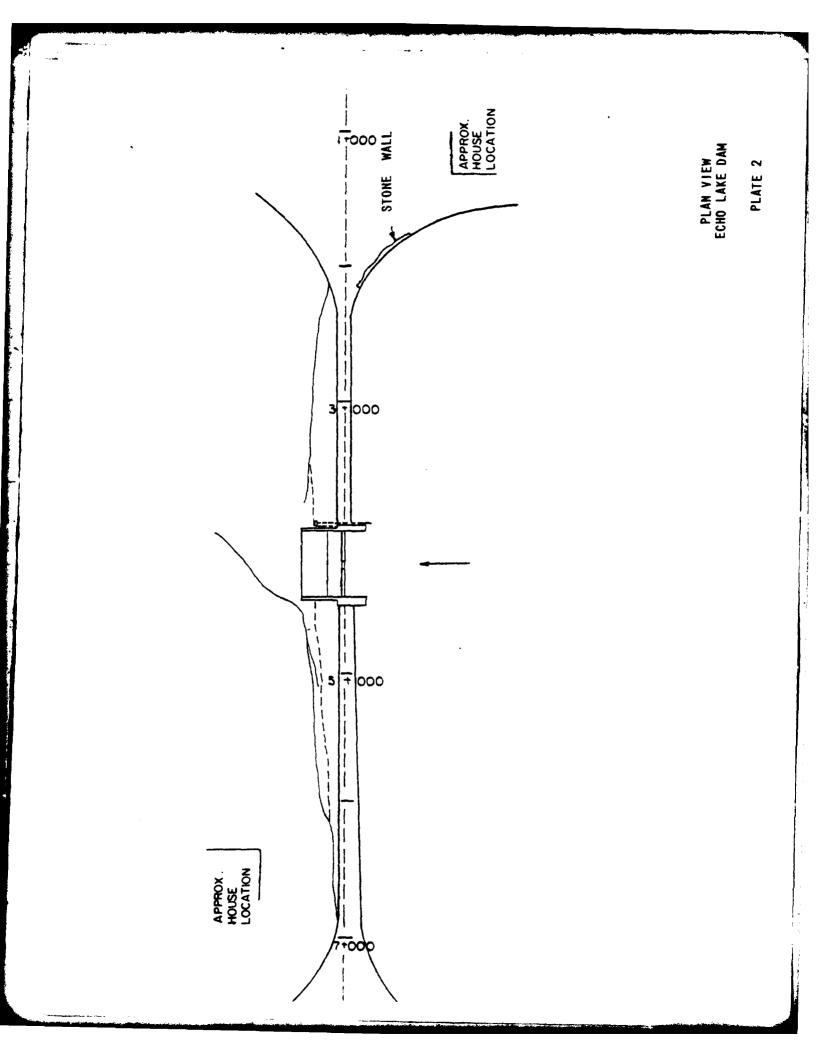
. .

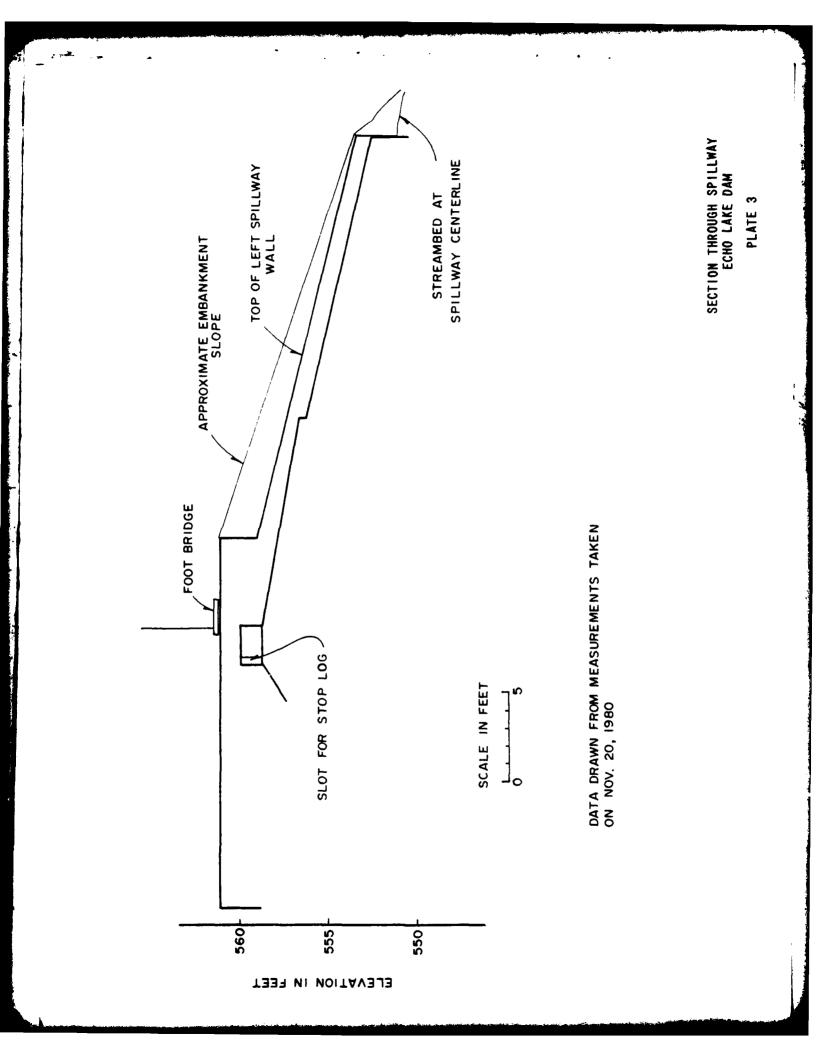
.

4

E







APPENDIX

_ · •

57

F

ECHO LAKE DAM

SITE GEOLOGY

Echo Lake Dam is located in the Great Valley section of the Valley and Ridge physiographic province. As shown on Plate F-1, the dam site and much of the surrounding areas are underlain by glacial deposits of Pleistocene age. These deposits consist of varying amounts of gravel, sand, silt and clay. Locally, in the vicinity of the dam, concentrations of boulders were noted during the field inspection. No bedrock exposures were observed near the dam site. Slate and siltstone deposits of the Martinsburg Formation are exposed elsewhere in the area, however, regional geologic mapping indicates the dam site to be underlain by the limestone and dolomite of the Allentown Formation. Consistent with the variable compositional character of glacial deposits, there exists the potential for reservoir seepage through these deposits in addition to seepage along the bedrock interface if bedrock is in fact relatively close to the surface.

