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AN EVALUATION OF THE EFFECT OF SPARES ALLOWANCE POLICY UPON SHI--ETC(U)
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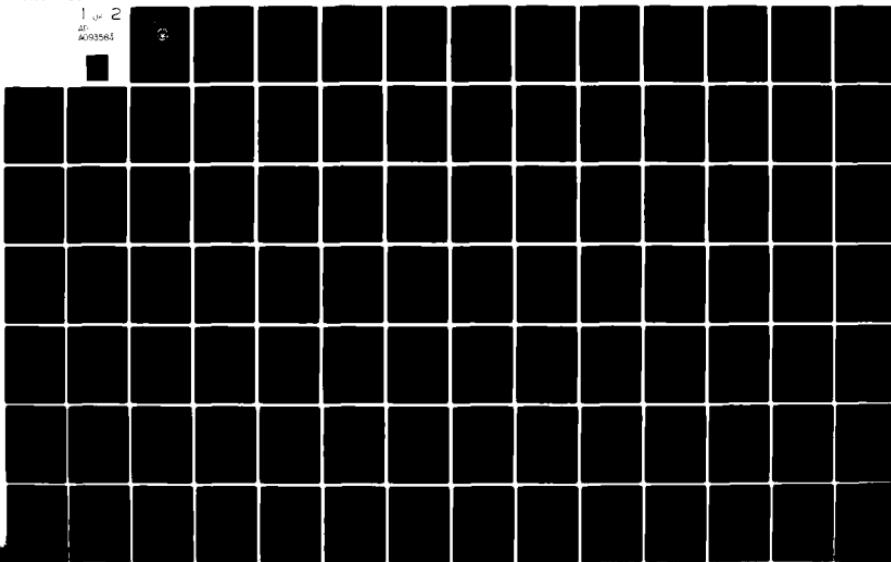
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NAVAL POSTGRADUATE SCHOOL
Monterey, California



LEVEL II



THESIS

AN EVALUATION OF THE EFFECT OF
SPARES ALLOWANCE POLICY UPON
SHIP AVAILABILITY AND RELIABILITY

by

John Edward Leather

September 1980

10116

Thesis Advisor:

F. Russell Richards

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
		AD-A093 584
4. TITLE (and Subtitle) An Evaluation of the Effect of Spares Allowance Policy Upon Ship Availability and Reliability		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis; September 1980
7. AUTHOR(S) John Edward Leather		6. CONTRACT OR GRANT NUMBER(S)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, CA 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, CA 93940		12. REPORT DATE September 1980
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Naval Postgraduate School Monterey, California 93940		15. NUMBER OF PAGES 115
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		18. SECURITY CLASS. (of this report) Unclassified
17. DISTRIBUTION STATEMENT (of the material entered in Block 20, if different from Report)		19a. DECLASSIFICATION/DOWNGRADING SCHEDULE
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Cosal Availability Provisioning Tiger Reliability		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) U.S. ships are provided onboard spare parts for equipment the ship's force is capable of repairing while at sea. The range and depth of spares provided has a pronounced effect on the availability of both ship and weapon systems. The spares suite for a particular ship is the Coordinated Shipboard Allowance List produced by the Ship's Parts Control Center. A mathematical model is used to produce this list, aiming to achieve stocking goals set by the Navy. This thesis examines the relationship between these		

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An Evaluation of the Effect of
Spares Allowance Policy Upon
Ship Availability and Reliability

by

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Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN OPERATIONS RESEARCH

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ABSTRACT

U.S. ships are provided onboard spare parts for equipment the ship's force is capable of repairing while at sea. The range and depth of spares provided has a pronounced effect on the availability of both ship and weapon systems. The spares suite for a particular ship is the Coordinated Shipboard Allowance List produced by the Ship's Parts Control Center. A mathematical model is used to produce this list, aiming to achieve stocking goals set by the Navy. This thesis examines the relationship between these goals and the model in use. A simulation model developed by the Naval Sea Systems Command has been modified so that it is compatible with the Naval Postgraduate School computer system, and this simulation model is used to evaluate the provisioning models. This simulation model is capable of being used for a variety of other projects at the Naval Postgraduate School.

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I. INTRODUCTION

The capability of a modern warship to be combat ready and maintain this readiness over a deployment period depends on logistics support. While this support includes such necessities as food, fuel, medical supplies etc., a crucial element in maintaining the sophisticated shipboard systems is the availability of repair parts. More important, of course, is the necessity of having a skilled technician capable of diagnosing any problems and effecting the required repairs. This thesis will focus entirely upon the 'part' side of this two-way problem, knowing full well that the desired technical expertise is not always available on all ships.

To provide for the capability of repairing equipment while away from port or support ships, each ship is provided a quantity of spares designed to enable it to be self sufficient for a period of 90 days. Budget and storage constraints prohibit stockpiling spares to cover all possible requirements, therefore a choice must be made as to the method to allocate the range and depth of spares to be provided.

Chapter II discusses the way the Navy is currently making this allocation. The method has been successful for a number of years, but less so recently due to changes in

provisioning model parameters. These changes were dictated by the 'high cost' of the allowance list generated by previous parameters.

Chapters III, IV, and V describe the use of a reliability block diagram simulation program to evaluate the effect of changing the spares suite upon the reliability/availability of a shipboard system over a 90 day period with no external spares replenishment. To obtain an upper bound on the spares effectiveness, the 90 day period was simulated with all repairs being instantaneous; thereby placing the entire burden of making the system available on the spares suite and not upon the speed of the repair. From this technique a measure of effectiveness of each given spares suite can be derived.

As an example, a particular reliability block diagram is analyzed in chapter VI using the simulation technique. The nature/configuration of this block diagram has a large effect on the figure of merit results. For example, three different items connected in series would be less reliable than the same three connected in parallel where only two are required to be functioning at once and the third was in cold standby. It is for this type of reason that a provisioning process based on parts counting rather than reliability may provide satisfactory results for one system and unsatisfactory results for another when both systems possibly consist of the same piece parts or perform the same function.

The simulation (called TIGER) is a general reliability simulation model and is capable of many other uses besides the one chosen for this thesis. With the help of the appendices, the program listing, and the TIGER manual (Ref. 1) further use of this program on the Naval Postgraduate School (NPS) computer system or any other FORTRAN IV compatible system with random number generation capability should be feasible.

II. THE COORDINATED SHIPBOARD ALLOWANCE LIST (COSAL)

A. NAVY POLICY FOR PROVIDING SUPPLY SUPPORT OF THE OPERATING FORCES

The amount of logistic support required to support the desired levels of fleet readiness are delineated in Ref. 2. Of concern here are the sections on Shipboard Stock Levels and Criteria for Shipboard Allowances.

All non-Fleet Ballistic Missile (FBM) self-sustaining ships have a stockage objective of 90 days, which is equated to the endurance for the ship. This objective is applicable to repair parts, spares, and equipment related consumables.

The specific criterion for developing a COSAL from a list of those items capable of being repaired by shipboard personnel is the subject of the next section of this thesis.

The measures of effectiveness for COSAL performance as stated in Ref. 2, are to 'fill from onboard stocks 65% (gross effectiveness) of all demands and to provide an overall availability for items allowed to be carried of 85% (net effectiveness)'. It is essential to note that no mention is made of such terms as reliability, availability, or readiness in the context of the supported ship as a measure of COSAL effectiveness.

Net effectiveness is often called 'system' effectiveness, in that it is the effectiveness of the entire logistics

system in replenishing shipboard spares once they are used and reordered. As this is not specifically related to the COSAL provisioning document, but is a function of such diverse items as order and shipping times, specific examination of this measure will not be attempted. Rather, certain stated assumptions will be made regarding the percentage of spares onboard when it is necessary to do so.

The objective of 65% gross effectiveness is the central issue which this thesis will focus upon. As will be shown in the next section, the COSAL mathematical model in no way can be substantiated as a '65% gross effectiveness model'. More important is the question of '65% gross effectiveness' as a measure of effectiveness for shipboard support. One could conceive of ways to fill 75% of the requisitions received in 90 days from shipboard stock and never be able to get underway. Alternatively, a low fill rate could result in a highly successful deployment. The key, obviously, is to stock those items which are important to the ships mission, and not to stock simply to maximize stock turn.

B. CURRENT COSAL MATHEMATICAL MODELS

Several mathematical models are currently being used to generate COSALS. The Fleet Logistic Support Improvement Program (FLSIP) model is used for surface ships and Fast Attack Submarines (SSN) and is the most extensively used technique. The TRIDENT model is used on Fleet Ballistic

Missile Submarines (FBM) and is similar to the Maintenance Criticality Oriented (MCO) COSAL being implemented on the FFG-7 Lo-Mix class of ships.

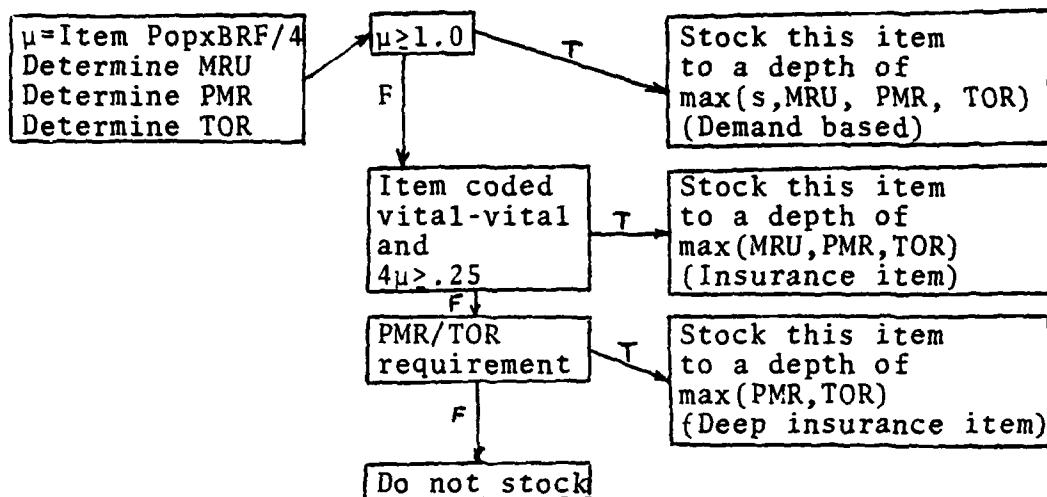
1. FLSIP Model

The FLSIP model has been in use for many years and has proven to be a rapid, workable, and understandable method of generating the large quantity of COSALS that must be run (approximately 50 per month). This model simply processes a list of all repair parts applicable to the particular ship and capable of being replaced by the ship's force. Each part is individually totaled for its' entire installed shipwide population and then is multiplied by its' Best Replacement Factor (BRF) (explained in chapter IV). The resultant value is called the 'mean', and this mean is used with the essentiality of the parent equipment to determine the final allowance quantity. A FLSIP logic diagram is shown in figure 1.

The attempt to incorporate essentiality into this model has been negated by the migration of over 90 percent of the parts on file into the 'vital' category. Technical Overrides (TORS) have been frozen by the Chief of Naval Operations (CNO) as a cost reduction measure.

The currently used model is called a .25 FLSIP model since the insurance cut point is .25 (one expected demand in four years). As over 90 percent of the items stocked onboard a ship are stocked at a depth of one, this cut point is critical to the ability of the model to provide sufficient

FLSIP COSAL LOGIC



Definitions:

Item Pop - Consolidated population of the item throughout the ship's systems

BRF - Best replacement factor

s - minimum stocking depth such that $\Pr(\text{Actual 90-day demand} \geq s) \approx .90$
(Assuming Poisson distribution)

MRU - Minimum replacement 'unit' quantity, if any

PMR - Required preventative maintenance quantity for planned maintenance

TOR - Technical override quantity, if any;
determined by engineers/designers during equipment provisioning review

Vital-Vital code - Item vital to its parent component, and its component vital to a primary mission

Figure 1

support. This cut point was changed from a previous value of .15 due to various budgetary pressures.

Aside from the arbitrary nature of the value chosen as the cut point the main problems which continue to exist are the effectiveness criteria established in Ref. 2 and the fact that the FLSIP model (Figure 1) has no mathematical relationship to these criteria. If the FLSIP is to be continued in use, and indications are that it will (Ref. 3), meaningful effectiveness criteria must be established and a means developed to justify the use of the FLSIP model to meet these criteria.

2. TRIDENT Model

The TRIDENT model incorporates military essentiality codes (MEC) assigned to the parent equipment into the stockage allowance decision. The more essential the equipment, the better it will be supported. The following equation is used to calculate the allowance quantity:

$$\text{Allowance quantity} = \mu + (Zx\mu)$$

Where μ is the mean of the assumed Poisson distribution of repair part requirements in 90 days).

The multiplier Z is a function of essentiality and to a lesser degree the unit price of the part. As in the FLSIP model each candidate part is processed individually and is not subject to budget constraints (although the levels may be adjusted through the manipulation of the various factors which comprise Z).

This model is currently in use; takes essentiality of equipment into account; and provides excellent support. But as could be expected, the resulting COSAL provides generous allocation of spare parts and its cost would be hard to justify outside of the FBM arena.

3. Maintenance Criticality Oriented (MCO) Model

The MCO model is an allowance list to be implemented on an increment of the new FFG-7 Lo-Mix class of ships. The mathematical technique is very similar to the TRIDENT model, the main difference being that essentiality is carried all of the way to the part level. The documentation required to achieve this is extensive and costly and must be maintained throughout the life of the ship. The documentation required to backfit the MCO model to older classes of ships does not exist.

III. THE NAVAL SEA SYSTEMS COMMAND TIGER SIMULATION PROGRAM

A. INTRODUCTION

TIGER is the generic name for a family of computer simulation programs which can be used to evaluate a complex system in order to estimate various reliability, readiness, and availability measures. This program was developed by the Naval Sea Systems Command (NAVSEA) reliability branch. The reliability block diagram of the system/component under study is the foundation from which a TIGER simulation run is constructed. This block diagram may be for a large system (ship) with each block representing a component of the system; or it may be for a single component with each block representing a lowest replacement unit part; or the block diagram may be any type of combination of both. As an input for each block the Mean Time Between Failures (MTBF) and Mean Time to Repair (MTTR) must also be known.

The unique feature about TIGER is the flexibility incorporated into the program. Scenarios with block diagram configurations which change during the time period being simulated are evaluated through a series of different timeline 'phases' in the input. A phase is a specific reliability configuration for the ship being studied. The simulation will accept up to six different phases, and they may be sequenced in any order and be of any interval of time. The

phases may be strung together until the simulation capacity of 95 total phases is reached. MTBF, MTTR, and spares multiplier factors may be entered to perform sensitivity analyses on the system under study.

TIGER uses Monte Carlo random number methods to evaluate the input block diagram. The random numbers are generated through the use of the NPS LLRANDOM routine (Ref.4).

The TIGER simulation is a discrete event step simulation. Exponential failure and repair times are generated using the MTBF and MTTR input data. As equipments fail spares are used; repairs effected (if allowed in the phase); standby equipment turned on/off if required; and different block diagrams initiated as the different phases are encountered during the timeline. Statistics are collected as a result of each event and change of configuration.

The TIGER output includes estimates of reliability, readiness, availability, and critical components which caused the most severe degradation of reliability and availability. The user may change the random number seed and replicate a timeline as many as 1000 times in a single TIGER run. TIGER will calculate and provide a lower confidence limit for the point estimate of reliability.

The inherent limitations to the use of this type of simulation include both the problem of providing accurate input data (MTBF, MTTR) and the exponential failure/repair rate assumption used in the program. Under many scenarios and for many types of equipment this exponential assumption is valid

but certainly many types of equipment exhibit wearout and not all repair times are exponentially distributed.

In addition to the output mentioned above, spares usage may also be displayed as well as several standard and optional outputs of the progress of the simulation. The detail can vary from every event being shown to a much simpler management summary.

Two subroutines of TIGER were omitted in this thesis research but may be useful in different types of analysis. One of these, the GAMMA option, assumes that the system being evaluated has a gamma failure distribution and calculates the two parameters (shape and scale) for the gamma distribution which would exhibit the same mean and variance of mission failure times as the system being modeled. The DEMO option of TIGER provides the capability of generating a sequential probability test ratio plan for the system as prescribed in MIL-STD-781. Detailed information about TIGER including GAMMA; DEMO; and a TIGER/MANNING personnel requirements type program is found in Ref. 1.

B. PRESENT NAVSEA TIGER UTILIZATION

The TIGER program is being used by NAVSEA to evaluate Reliability, Maintainability, Availability (RMA) performance characteristics of new ship classes (Ref. 5). This analysis is performed only on the major mission-essential systems: Navigation, Auxiliary, Electrical, Ship Control, Propulsion,

Exterior Communications, and Combat. Only these systems and equipment which impact the operational readiness of the ship and the ship's ability to perform its assigned primary combatant mission are included in the analysis.

All surface ships constructed since 1970 have reliability block diagrams available (in computer readable form). This eliminates the major undertaking of having to construct the reliability block diagrams prior to using TIGER. The necessary MTBF and MTTR data for existing equipment is found in the Reliability/Maintainability/Availability Design Data Bank (Ref. 6), which is a compilation of data from both engineering design and fleet feedback. Engineering estimates must be used for the many new systems found on a new class of ship, where no feedback data yet exists.

Along with the various reliability block diagram configurations (steaming, in-port, ASW, etc.) and MTBF/MTTR data, the operating rules for the equipment must also be provided. These rules include allowable downtime, spares, mission timelines, and maintenance policy.

A sample RMA timeline (Ref. 5) is shown in figure 2. Timelines are tailored to the class of ship and its designed usage in a period of combat.

Allowable downtime is the time that the system or equipment can be down for maintenance without causing a mission abort. During simulated combat periods this time is usually zero for most mission essential systems.

DAY	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25		
PHASE	A								A				A		B		A		B								
ENGAGEMENT CODE																											
MISSION	TRANSIT								CONVOY ESCORT				TRANSIT														
	CARRIER TASK FORCE												IN PORT														
DAY	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50		
PHASE	A								A				A		B		A		B		C						
ENGAGEMENT CODE																											
MISSION	CARRIER TASK FORCE								TRANSIT				AMPHIBIOUS OPERATIONS		2/5												
	TRANSIT												IN PORT														
DAY	51	52	53	54	55	56	57	58	59	60																	
PHASE									C																		
ENGAGEMENT CODE																											
MISSION																											
	IN PORT												IN PORT														

CODE	PHASE	WARTIME CRUISING	DURATION (HOURS)
1	SOW		0.5
2	SOW		0.5
3	AAW		0.25
4	AAW		0.25
5	AAW		0.5
6	AAW		1
7	ASW		2
8	ASW		3

CODE	PHASE	ENGAGEMENT	DURATION (HOURS)
A	WARTIME CRUISING		
B	ENGAGEMENT		
C	IN PORT		

Figure 2

Maintenance policy limits certain equipment to being capable of repair only during certain phases. For example, repair of the main engine would not be permitted while hunting a submarine, but would be permitted while in-port.

Spares are assumed to be available as needed for initial TIGER analysis. Supportability tradeoff studies are conducted separately to evaluate the effect of different spares efficiency percentages and off-ship logistic delay times.

The results of the TIGER simulation are compared with design specifications to see if any inherent (non-spares related) reliability problems exist. Critical equipments are then identified and closely monitored during the final phases of design and construction.

C. PROPOSED TIGER UTILIZATION FOR COSAL PREPARATION

Reference 7 describes a methodology of using the TIGER program to evaluate a COSAL with respect to reliability. The inputs to the TIGER program would be the same as those in the last section with the exception of the spares input and the indenture level of the reliability block diagram. The diagram must not stop at the equipment level, but be carried out to the repair part level. MTBF/MTTR data must also be provided at the repair part level.

As may be readily apparent, the block design for just the essentail equipment of an entire ship would be very cumbersome and unworkable. This type of TIGER analysis must

be done on a system or equipment basis. The spares input would be that generated by the COSAL model under evaluation, usually FLSIP.

A deployment timeline is simulated and the resulting reliability/availability figures are compared to the design goals. If the goals are not achieved the 'bad apples' list of repair parts indicates the particular parts which caused the most degradation. Additional quantities of these parts are added to the spares suite and the process is repeated until the goal is attained. This method may also be used in reverse, removing spares and observing the resulting changes to reliability/availability.

While this methodology is feasible and would certainly provide better support than an unaugmented FLSIP COSAL, it has several drawbacks. One is the lack of reliability block diagrams down to the repair part level. Although new equipment procurement contracts may specify that this documentation must be provided, the task of assembling it for just one ship's essential equipment would be awesome.

Another problem is the lack of MTBF/MTTR data for each part. Reference 8 may be used to estimate the required parameters, but again this is a large undertaking. As was mentioned earlier in this thesis, current provisioning processes use a BRF vice MTBF to determine logistic support. A further clarification of the differences between these two and a proposed solution will follow in a later section.

A final problem results from the fact that repeated computer runs on a vast network of reliability block diagrams are required to produce a single COSAL. The computer system at the Ships Parts Control Center (SPCC) is saturated and could not begin to process the large quantity of simulation runs necessary to use this proposed method on all COSALs. In addition, a significant number of manhours would be required to review each run and decide which parts to augment and in what quantity. Though this process would undoubtedly produce a COSAL superior to the FSLIP model, practicality prevents its adaption at the present time.

IV. BEST REPLACEMENT FACTOR (BRF)

A. BRF - WHAT IS IT?

The BRF is the projected annual replacement rate for one installed unit of a repair part. Only one BRF exists for each part even if it is used in numerous applications throughout a given ship or the fleet or ashore. The BRF is found by dividing the annual reported usage in the fleet by the total installed population. This yields annual failures per installation. Before any calculations are made the input data are adjusted for inaccuracies caused by bad reporters and inactive ships in overhaul. The BRF is calculated annually for each item in the SPCC files. To prevent rapid fluctuations from occurring the previous value on file is updated with the new value by the use of exponential smoothing.

To illustrate this process suppose that 105 ships in the fleet were each recorded as having two of part 'A' installed. Five ships were in overhaul for this particular year so their data is not used for BRF update. The remaining 100 ships reported a total of 400 failures for item 'A'. Since there are 200 of 'A' installed and 400 were used, the unsmoothed BRF is $400/200 = 2.0$. If the BRF currently on file is 2.4 and exponential smoothing with smoothing constant .25 is used, the updated BRF would be $2.4 \times .75 + 2.0 \times .25 = 2.3$.

This BRF would be put on file for use in all COSALS which contain part 'A'.

B. MEAN TIME BETWEEN FAILURE (MTBF)

MTBF is the expected value of the operating time between failures of an item. It is estimated by dividing the total time in service by the number of failures:

$$\text{MTBF} = \text{total time in service}/\text{number of failures}$$

Sometimes the expression Mean Time to Failure (MTTF) is used for the expected value. Another related measure is the failure (hazard) rate which is the conditional probability that an item surviving to age t will fail in the interval $(t, t+dt)$. A constant failure rate is equivalent to having a failure distribution which is exponential; and for an exponential distribution the failure rate is the reciprocal of MTBF.

C. DIFFERENCES BETWEEN MTBF AND BRF

A MTBF provides an expected value of the length of time an item will operate until failure. It is based on operating time; and failures are not possible while the equipment is not in use or turned on. A BRF is the average number of times an item will fail in an average year in an average installation. Since these differences and similarities are crucial to the analysis in section VI of this thesis, the following example taken from Ref. 9 provides an insight into the MTBF/BRF relationship.

A piece of equipment (lamp) has four repair parts (bulb, socket/switch, cord, plug). It is operated for 1000 hours per year. An arbitrary MTBF and corresponding Failure Rate (expressed in failures per year) are shown below:

<u>ITEM</u>	<u>MTBF</u>	<u>FAILURE RATE</u>
Light Bulb	750 HRS	1.333
Socket/Switch	10,000 HRS	0.100
Electric Cord	15,000 HRS	0.066
Plug	10,000 HRS	0.100
TOTAL		1.599

As shown, the lamp is expected to fail 1.599 times per year. This would be a BRF for the lamp if the maintenance policy were to replace the whole lamp no matter what the cause of the failure. The following table shows how maintenance philosophy can have a pronounced effect on the five BRFs. The 'Replace Failed Part' column represents the way repairs are usually accomplished at the shipboard level. Only catastrophic failure would lead to the attempted replacement of the entire item, usually unsuccessful because the entire assembly would not likely be stocked due to the low BRF.

<u>ITEM</u>	<u>FAILURE RATE PER YEAR</u>	MAINTENANCE PHILOSOPHY		
		<u>REPLACE FAILED PART</u>	<u>REPLACE LAMP</u>	<u>REPLACE FAILED BULB, OTHERWISE REPLACE LAMP</u>
		BRF=0.	BRF=1.599	BRF=.266
LAMP	1.599	BRF=0.	BRF=1.599	BRF=.266
BULB	1.333	BRF=1.333	BRF=0	BRF=1.333
CORD	0.066	BRF=0.066	BRF=0	BRF=0
S/SWITCH	0.100	BRF=0.100	BRF=0	BRF=0
PLUG	0.100	BRF=0.100	BRF=0	BRF=0

D. BRF AS AN INPUT TO TIGER

When MTBF is used as an input to TIGER, various timelines are used to provide scenarios in which the equipment configurations and usage rates are required. When equipment is on, it fails exponentially with the given MTBF, unless the duty cycle is less than 100 percent, in which case the MTBF is divided by the duty cycle. The BRF has incorporated the various reasons the timeline approach must be used with the MTBF; equipment being turned off and on; duty cycles for equipment with cycles of less than one; and the various configuration dependent usage rates for an average installation in an average year.

Consider, for example, an equipment with a duty cycle of one-half (operating 50 percent of the time) exhibiting five failures in a ten year period. The MTBF is calculated as before; total time in-service/failures = $(10 \times .5)/5 = 1$ year. Since the duty cycle is one-half, we would expect to see a failure every other year, or .5 per year. The BRF calculation yields the same result; 5 failures/10 years = .5 failures/year.

To use a BRF in TIGER requires that the entire block diagram, in a typical configuration, be used and equipment/parts be allowed to fail at an annual rate (BRF) which takes the numerous operating scenarios into account. While the results from this type of analysis would be very difficult to defend as providing entirely accurate reliability/

availability measures; they should be suitable for deriving a 'figure of merit' evaluation for the support provided by different COSAL models.

V. TIGER USED TO EVALUATE THE EFFECT OF SPARES ALLOWANCE POLICY UPON RELIABILITY AND AVAILABILITY

A. INTRODUCTION

The current utilization of gross effectiveness as a measure of COSAL effectiveness has been studied in previous sections. An alternative measure will now be proposed. The TIGER program calculates reliability, availability, and readiness figures for each simulation run. The definitions for these three measures, as found in Ref. 1, are summarized below.

B. RELIABILITY (REL)

For a given timeline the reliability (REL), as estimated by TIGER, is the probability that the ship will successfully complete the entire timeline. For example, if the timeline previously shown in figure 2 were used, REL would be the probability of the ship completing all of the different missions assigned during the 60 day period, in the sequence shown.

Reliability is calculated by TIGER as follows:

$$\text{REL (EST)} = 1 - \frac{\text{Number of mission failures (aborts)}}{\text{Total number of simulated missions}}$$

Note that this calculation incorporates logistics support considerations.

C. AVAILABILITY (AVA)

TIGER calculates two AVA parameters: Instantaneous and average. Instantaneous availability is the probability that the system will be 'up' at a specific point in time. Average availability is the probability that the system will be up at a random point in time. Because of the way TIGER is used, average availability is the relevant measure.

Average AVA is estimated as the ratio of total system 'uptime' to the total time simulated. These times are totaled for the entire number of missions simulated (up to 1000). The calculation is made as follows:

$$\begin{aligned} \text{AVA (EST)} &= \frac{\text{Summation of uptime for all missions simulated}}{\text{Summation of total mission calendar time for all missions simulated}} \\ &= \frac{\text{Uptime}}{\text{Calendar time}} \end{aligned}$$

D. READINESS (RED)

RED, like AVA can be measured as instantaneous or average readiness. It is a measure of the probability that there is neither a mission abort nor a system down. The forthcoming methodology for the use of TIGER results in RED equaling AVA, so RED will not be considered any further as an alternative measure of effectiveness.

E. RELIABILITY VS AVAILABILITY AS A MEASURE OF EFFECTIVENESS

A very common measure of effectiveness in use by the Navy today is 'Operational Availability' (Ao). Ao is defined as the probability that an equipment is ready when you need it.

MIL-HDBK-217C (Ref. 8) dictates that it be calculated by:

$$Ao = \frac{MTBF}{MTBF + MTTR}$$

An alternative form of this equation results from breaking the MTTR up into the repair time (MTTR) plus the Mean Supply Response Time (MSRT); the time necessary to provide the required repair part(s). This yields:

$$Ao = \frac{MTBF}{MTBF + MTTR + MSRT}$$

There are problems with the use of this formula for estimating system operational availability (Ref. 10). From a mathematical point of view the formula yields the correct result for the limiting value of operational availability when one considers a single component that transitions between up and down states as an alternating renewal process. If one is interested in the operational availability after a fixed period of time for a system whose components have limited spares support, the formula does not yield correct results. In fact, the formula makes little sense. A simulation like TIGER is precisely what is needed to estimate Ao for a complex system with limited spares support.

Since AVA implicitly considers component reliability, maintenance, spare parts support, system configuration and

operational scenario, it is used in this thesis to evaluate COSAL models.

F. ALLOWANCE POLICY EFFECT

1. Reliability Block Diagram of System

The effect of a parts-counting type allowance policy upon reliability/availability is dependent on the configuration of the system being supported. Parts counting is a method of allocating spares in proportion to the number of each specific repair part in the equipment. In an environment of limited budgets and storage space, a more 'critical' spare (in terms of reliability/availability) may be sacrificed to provide unwarranted depth for another spare.

Figure 3 shows a simple reliability block diagram with two

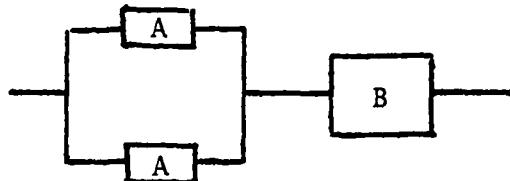


Figure 3

of part A in parallel with each other and then in series with part B. Both A and B have a BRF of 1. If A cost the same as B, and only one spare could be provided, provisioning by parts counting would provide one spare of type A, since there are twice as many A as B. However, the availability of this system would be much greater (all other things considered the same) if the one spare purchased were of type B, due to the parallel redundancy.

2. Proposed Allowance Policy Input

There are two methods of entering the quantity of spares for each part type into the TIGER simulation. One is to input that quantity as part of the input data. For small systems this may be the most efficient method. For larger systems or for those systems requiring a complicated mathematical model, a subroutine has been added to TIGER to calculate the COSAL.

For the FLSIP COSAL, the cut point is input with the other system data and the spares subroutine is used to generate the COSAL for the system. The MTBF is derived from the BRF in the following manner:

$$\text{MTBF} = (1/\text{BRF}) \times 8766 \quad (\text{yr/fail}) \times (\text{hr/year}) = \text{hr/fail}$$

This MTBF is used as the exponential failure rate input for the simulation, and converted back to BRF when necessary to determine COSAL support.

3. Figure of Merit Results

Several simplifying assumptions are made by using TIGER to obtain the output availability measure. The most important are exponential failures; BRF converted to MTBF; zero repair times; a full allowance of spares onboard at the beginning of the mission; and the use of a 'typical' reliability block diagram configuration for the duration of a single mission. Because of these assumptions, the availability figure provided by TIGER should not be considered as the true value for system availability. However, this figure

should be useful as a 'Figure of Merit' for comparisons with the figure derived for the same system using a different methodology or level of logistics support. When used in this context, the figure should provide an accurate assessment of the relative effectiveness of two spares allowance policies.

VI. EXAMPLE OF TIGER ANALYSIS

A. EQUIPMENT CONFIGURATION AND FAILURE RATES

1. Block Diagram and Operating Rules

As an example of the use of TIGER proposed in this thesis a hypothetical video display unit will be analyzed. The unit consists of a power section; signal processing section; and video display section. The required reliability block diagram is shown in figure 4.

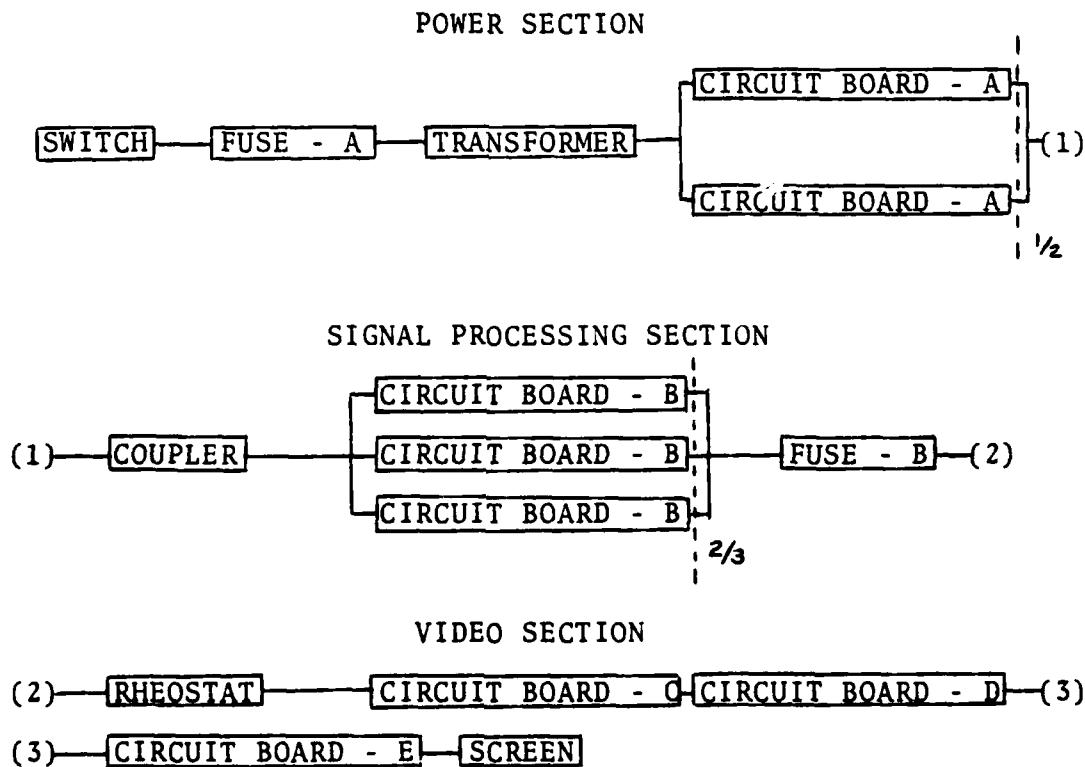


Figure 4

The three sections are connected in series to form the entire unit. Only one of circuit board A is required to be 'up' in the power section, and two of circuit board B in the signal processing section. The failure of two of either circuit board A or B or the failure of any other single part will cause system failure.

2. Failure Rates

The following is a list of the BRF for each part and corresponding MTBF:

ITEM	BRF	MTBF
Switch	.09	97400
Fuse - A	2.50	3506
Transformer	.17	51565
Circuit Board - A	2.10	4174
Coupler	.23	38113
Circuit Board - B	2.50	3506
Fuse - B	3.60	2435
Rheostat	.12	73050
Circuit Board - C	1.20	7305
Circuit Board - D	2.20	3985
Circuit Board - E	1.70	5156
Video Screen	.20	43830

B. LOGISTIC SUPPORT (COSAL) MODELS USED

The COSAL models evaluated were the standard .25 FLSIP and a modified FLSIP as proposed by the CNO Shipboard Parts Allowance Policy Study (Ref. 3). This modification consists of changing the FLSIP cut point to .1 (one demand in ten years) and providing an allowance quantity of two (vice one) for those items with a BRF between 2.0 and 4.0.

C. RESULTS OF ANALYSIS

1. Results of TIGER Simulation

The following tables provide a summary of the relevant output from the two TIGER simulation runs for 90 day missions. The actual computer output is self explanatory and a sample is included as a separate section of this thesis. The percent unavailability column indicates the percent of unavailability caused by each item.

.25 FLSIP (Availability = .7229)

<u>ITEM</u>	<u>SPARES STOCKED</u>	<u>SPARES USED</u>	<u>FAIL/MISSION</u>	<u>PERCENT UNAVA</u>
Switch	0	.00	.025	3.35
Fuse - A	1	.50	.637	14.54
Transformer	0	.00	.042	6.42
Cir Bd - A	2	.96	1.05	6.77
Coupler	0	.00	.064	9.35
Cir Bd - B	4	1.84	1.897	.81
Fuse - B	1	.57	.793	24.01
Rheostat	0	.00	.030	3.74
Cir Bd - C	1	.27	.318	3.64
Cir Bd - D	1	.43	.541	11.99
Cir Bd - E	1	.34	.416	7.07
V. Screen	0	.00	.052	8.29
			<u>5.865</u>	<u>99.98</u>

.1 MOD FLSIP (Availability = .9064)

<u>ITEM</u>	<u>SPARES STOCKED</u>	<u>SPARES USED</u>	<u>FAIL/MISSION</u>	<u>PERCENT UNAVA</u>
Switch	0	.00	.017	8.53
Fuse - A	2	.59	.607	5.41
Transformer	1	.05	.054	.75
Cir Bd - A	2	.92	1.015	24.70
Coupler	1	.06	.067	1.23
Cir Bd - B	4	1.84	1.897	2.58
Fuse - B	2	.79	.844	18.19
Rheostat	1	.04	.044	.00
Cir Bd - C	1	.27	.310	13.43
Cir Bd - D	2	.53	.553	5.42
Cir Bd - E	1	.35	.414	18.99
V. Screen	1	.04	.046	.74
			<u>5.868</u>	<u>99.97</u>

2. Interpretation of Results

As would be expected, the .1 Mod FLSIP provided a greater depth and range of spares than the .25 FLSIP. The addition of seven more spares resulted in an increase in AVA from .7229 to .9064, a significant increase. For the .25 FLSIP run, the item accounting for highest percentage of availability is fuse - B, with 24.01 percent. Since FLSIP provides a 90 percent confidence level of protection for those items with a BRF ≥ 4.0 ($\geq 1/qtr$), the BRF of 3.60 places the fuse just below this cut and therefore it is allocated only one spare. For the .1 Mod FLSIP run fuse - B no longer is the largest contributor to unavailability. Circuit board - A is the largest, accounting for 24.70 percent of the unavailability. If further incremental improvements were to be made to the .1 Mod FLSIP COSAL, the first additional spare should be circuit board - A followed by circuit board - B, fuse - B, and so on down the list of unavailability percentages.

The difference in AVA for the two COSALS is the most important statistic. If availability in the range of .9 were required for the system, the .1 Mod FLSIP should be used. If however, the system were not that essential, the .7 availability provided by FLSIP should be used to enable scarce spares funding resources to be used on more essential systems.

VII. SUMMARY AND CONCLUSIONS

This thesis focused on one basic problem; that of providing logistics support for Naval units afloat. Current guidelines and measures of effectiveness were presented along with several of the methodologies by which the policies are being carried out.

The NAVSEA TIGER reliability block diagram simulation program was introduced as a currently used method of evaluating ship reliability and also as a proposed method of generating allowance documents. A key input to any reliability calculation is the MTBF. The use by the Navy of a BRF vice MTBF was reviewed and a solution proposed to enable BRF to be used as an input to the TIGER simulation.

A technique for using TIGER to evaluate the effect of various spares allowance policies upon system availability was introduced, followed by an example of such an analysis.

The Navy is interested in providing logistics support so as to maximize the operational availability of its ships within given resource constraints. Mathematical models designed to allocate spares while maximizing system availability require extensive amounts of data (much of which is either not available or retrievable by computer). They are computationally infeasible to implement on a Navy-wide basis. Thus, it appears that the Navy will continue to use simpler

parts-counting models such as those described in this thesis. No claim of optimality with respect to 'system availability' can be made with such simple models that make no attempt to consider the system as anything other than a collection of parts.

The models that are being used are regulated by controlling the values of certain parameters such as FLSIP cut points or essentiality codes. Since there is no way to analytically relate these models to system effectiveness, a tool such as the TIGER simulator is needed to evaluate the future impact on system availability of a given provisioning or support policy. The assumptions required to perform this type of evaluation have been discussed throughout this thesis.

The following are recommendations for additional work in the topic of this thesis or for additional uses of the TIGER simulation:

1. Use as an evaluation tool for various provisioning models.
2. Use to evaluate maintenance policies and their effect on required manning levels.
3. Use as a system design tool.
4. Use on new equipment being introduced into the fleet to establish a FLSIP cut point. Code equipment with this cut point instead of the vital/non-vital codes currently in use, and use this cut point when preparing the COSAL.

5. Evaluate the effect of the assumptions made in this thesis and other problems such as the gradual degredation of equipment (not simply up or down) and the effect of the annual revisions to the BRFs.

APPENDIX A

ACRONYMS

Ao	Operational Availability
AVA	Availability
BRF	Best Replacement Factor
COSAL	Coordinated Shipboard Allowance List
CNO	Chief of Naval Operations
EST	Estimate
FBM	Fleet Ballistic Missile
FFG	Guided Missile Frigate
FLSIP	Fleet Logistics Support Improvement Program
MCO	Maintenance Criticality Oriented
MEC	Military Essentiality Code
MRU	Minimum Replacement Unit
MTBF	Mean Time Between Failure
MTTF	Mean Time to Failure
MTTR	Mean Time to Repair
NAVSEA	Naval Sea Systems Command
NPS	Naval Postgraduate School
PMR	Preventative Maintenance Requirement
RED	Readiness
REL	Reliability
RMA	Reliability/Maintainability/Availability

SPCC	Ships Parts Control Center
SSN	Fast Attack Submarine (Nuclear)
TIGER	Simulation Program Name
TOR	Technical Overide

APPENDIX B

TIGER PROGRAM VARIABLES LIST

The following is a list of the variables used in the TIGER program and their respective usage/definition. All variables which were used in this thesis are included along with some from other optional parts of the TIGER program. Numbers at the right indicate the data card on which the variable is input into the program.

A	Subroutine DEMO producer risk	21A
ACMMH	Average corrective manhours per mission	
ADT	Administrative delay time	
AENDT1	Downtime in remainder of phase due to abort	
AENDT2	Downtime in remainder of mission due to abort (up to current phase)	
AFM	Average failures per mission	
ALDONE	Sum of three DONE(I); if zero, skips spare printout	
APPL	Bad apple unreliability and unavailability printout	21
AVA	Average availability or availability	
AVAINS	Instant availability	
AVA1	Average availability	
AVAL	Average availability	
AVGCST	Average cost per hour of repairman	7M
B	Subroutine DEMO consumer risk	21A

BAPRIN	Bad Apple printout indicator, when equals -1, print	
BILL	Temporary variable used to integerize the number of spares	
BLNK	Four character alphabetic blank	
COUNTB(I)	Number of failures for equipment I	
DAY(IX)	Occupation symbol	15A,M
DELT	Time Difference	
DEMO	Probability ratio test plan for system	21
DMNO	Same as DEMO	
DNT1	Total system downtime in phase	
DNT2	Total system downtime in mission	
DONE(I)	Average number of spares used from ship, tender, depot(I=1,3)	
DUM(J)	Dummy variable to read F1	
DUMMY	Skill types	
ENDPHA	End of phase time	
EQUIP(I)	Person type numbers of people who could be operating this type of equipment	15G
ETIME	Event time	
EX(I,J)	Administrative delay time (U,W)	
F(I,J)	Same as F1	
FCOUNT	Real value of JCOUNT	
F1	Alphabetic equipment description	8
GMMA	Alphabetic request for GAMMA subroutine	21
HAD	DEMO X-axis accept intercept	21A
HRD	DEMO X-axis reject intercept	21A
I	Various indices; equipment type number	8

IABC	Index	
IAUP	Instant availability (up for entire simulation)	
IAUP1(I)	Instant availability (up at beginning of sequence)	
IAUP2(I)	Instant availability (cumulative up at beginning of sequence)	
IB(I)	Group number and equipment and groups which make up the group	18
IBLANK	14 alphabetic blank spaces	
IBM	Equipment type number	
IBNUM(I,J)	Number of configuration matrix cards in phase	
ICHLD	Child in reliability tree	
ICRI	Subsystems exceeding mission allowable downtime (TAD2)	
ID	Alphabetic system name	16,17
IDIFF	Total equipment failures (all types)	
IDUM	Same as IUT	
IEQ	Absolute value of IEQU(J)	
IEQU(I)	Equipment type array	
IFF	Number of failures	
IFFEOP	Same as ISW	
IFLAG	Repair option in each phase	6
IFR	Number of repairs	
IGRP	Equipment group	
II	Spare location (ship, tender, depot)	
III	II-1	
IIUSED(I,J)	Spares used per equipment type from each location	

IK	Phase indicator	
IK2	Phase indicator	
IK3	Phase indicator	
ILB	Counter for NEQ	
ILL	Phase subscript for VDC(IU,ILL)	
IND	Equipment type	
INDEX	Index; equipment number	
INEWA	Index used to rank equipment by number of failures	
INMI(I)	Number of missions run	
INOABT(I)	Number of aborts in the sequence	
INREJ	Not used	
INUM	Maximum number of mission repetitions (50)	
IOR	Number of equipment operating rules	
IPTR	Parent/Child index	
IPRNT	Parent reliability tree	
IRULE	Equipment operating rule card	19
ISEED	Random number seed	2
ISO	+string; -standby	
ISPARE(I,J)	Quantity of spares at ship, tender, depot	15
ISS	System/subsystem identification number	16,17
ISSA(I)	Phase allowable downtime	
ISTB(I)	Equipment operating rules	19
ISUM	Summation	
ISW	Subsystem status (1=up, -1=down)	
ISSC	Subsystems exceeding allowable downtime	

ISYS(K)	System in phase K	
IITEMP	System status indicator	
IITEMP2	Subsystem status indicator	
ITIME	Number of sets	21A
ITER	Number of simulations per set	21A
ITOTAL	Integer value of total	
IU	Variable duty cycle (IUI(I))	
IUI(I)	Variable duty cycle indicator	8
IUNLIM	Alphabetic 'unlimited spares'	
IUT	Same as IDUM	
IUSED(I,K)	Spares used from ship, tender, depot	
IV	Variable duty cycle indicator (IUI=IV)	9
IVALEUE(I)	Temporary variable for IB or ISTB	
IX	NUM+1	
IXX	Equipment type	
IXXT	Phase type	
J	Various indices; equipment type	
JA	Index for IB	
JB	Index for IB	
JBB	Phase sequence number	
JBB1	JBB-1	
JC	Current timeline	
JCC	Number of timelines	1
JCOUNT	Number of failed equipments	
JIND	Equipment type	
JNUM	Integer of XNUM	

K	Various indices	
KAA	Mission number being simulated	
KAB	Mission number being simulated	
KD	Trucation line accept	
KEQ	Equipment number	
KEQU(I)	Number of failures for equipment type I	
KID	Dummy variable	
KID1	Equipment group	
KID2	Equipment group	
KK	Same as LL; index of equipment number	
KKK	Phase in mission	
KKK2	Same as KKK	
KOPT	Printout option switch	5
KS(I)	Output options for KOPT	5
KSS	Index	
KT	IB(, ,1), or number required up in group	
K1	Equipment type; trail shape parameter	
L	Same as LL	
LCL	Lower confidence limit	
LL	Phase type number	16,17
LLL	Duration of phase sequence	
LOAD(I)	Equipment numbers assigned to equipment type	12
MAXIB	Maximum number of configuration matrix cards (300)	
MAXNEQ	Maximum number of equipments (500)	
MAXNPH	Maximum number of phases (6)	

MAXRUN	Maximum number of mission (1000)	
MAXSEQ	Total number of phases	
MAXSS	Maximum number of subsystems (31)	
MAXSTD	Maximum number of equipment operating rule cards (49)	
MAXTYPE	Maximum number of equipment types (200)	
MDT	Estimator of MTTR	
MKBA	Bad Apple equipment vector	
MM	0	
MTBFMF	Mean time between mission failures	
MUT	Instanteneous MTBF parameter	
M1	Trial scale parameter	
N	Counter; NSS+1	
NEQ	Equipment type counter	
NLINE(I)	Number of configuration cards in phase	
NL1	NLINE(LL)	
NN	Index	
NMAX	Maximum number of missions	2
NOPT	Optimal number of mission	2
NPH	Number of phases	2
NRO	Number required operating	18
NSS	Number of subsystems in phase	16
NTY	Last number of equipment types	
NTYPE	Equipment type	12
NT1	Equipment type number	
NUM	Mission number counter	

PERC	Percent unreliable	
PL	Reliability specification	2
R	Dummy variable used to find next event temporary variable used to calculate VDC; discrimination ratio	21A
RDT	Running down time	
RED	Readiness	
REDAD1(I)	Adjusted time for readiness calculation in phase	
REDAD2	Adjusted time for readiness calculation in mission	
RED1	Readiness	
RED2	Readiness	
REL	Reliability	
RELGA(JBB)	Reliability (RELPY) for phase sequence	
RELPY	Reliability up to and including phase just completed	
REPOL	Percent of repairs performed aboard ship	7
RN	Random number	
RN3	Random number	
RUNID	Alphabetic program identification line	1
SLD	Slope	21A
SPRS	Alphabetic request for SPARES output	21
SR	Intermediate value used to calculate ST	
SSTIME(I,J)	System/subsystem allowable sustained downtime	16,17
ST	Intermediate time	
STEPHAS	Accumulated phase time	
SUMX	Total simulation time	

SUMX2	Sum of SUMX squared (for variance calculation)
SX	Spares multiplier
T	Duration of phase
TABORT	Time of abort
TACMMH	Total average corrective maintenance manhours/mission
TAD1	Same as SSTIME
TAD2	Mission allowable downtime
TAFM	Total average failures per mission
TDEOP	Time down at end of phase
TDOWN	Time system went down
TIMA(I)	Cumulative phase time
TIME	Simulation clock time
TITLE(K,N)	Alphabetic subsystem title
TNMI	Real value of INMI(JBB)
TOTAL	Number of failed missions
TR	Temporary variable used to find maximum unavailability/reliability
TRR	Same as TR
TP	Same as TIME
TTEMP	Downtime
TTF	Time for failure
TTR	Time to repair
TT1	Phase length
TT2(JBB)	Cumulative time of phase lengths
TT3	Cumulative phase times

TYCOON(I)	Downtime for equipment	
TYCUM	Unavailability	
TYCUM2	Percent unavailability	
T1	SSTIME(, ,1)	
T3	Downtime	
T3SUM	Cumulative downtime	
U	Duty cycle utilization	8
UNAVA	Unavailability	
UNREL	Unreliability	
UP1	Time system up in phase	
UP2(JBB)	Cumulative system uptime	
UP3	Cumulative system uptime	
UP4	Cumulative system uptime	
V	Administrative delay time (tender to ship)	8
VAR	MTBF variance	
VDC(I)	Duty cycle utilization during each phase	9
VMTTR(I,J)	Variable mean time to repair	10
W	Administrative delay time (depot to ship)	8
X	Various; XMTBF; event indicator (+ fail; - repair)	
XAV	Instant availability	
XAVI	Instant availability	
XCUM	Successful missions in last 50	
XDWN	Number of mission failures (XNUM-XTCUM)	
XIAUPP	Real of IAUP	

XIAUPI	Real of IAUPI	
XID	Alphabetic ID	
XIFF	Real of IFF	
XIRR	Real of IRR	
XK	Standard deviation for lower confidence limit 2	2
XKAA	Real of KAA	
XLCLA	Lower confidence limit of 90 percent	
XM	XMTBF Multiplier	7
XMDT	System man down time	
XMTBA	Mean time between mission failures	
XMTBF	Mean time between failures	8
XMTTR	Mean time to repair	8
XMUT	System mean up time	
XM1	Same as XT	
XNO	Number of non aborts	
XNUM	Real of NUM (total missions run)	
XPCAP	Reliability	
XPLCL	Lower confidence limit	
XT	XMTBF multiplier	7
XTABT(I)	Time of abort mission I	
XTCUM	Cumulative successful missions	
XXT(I)	Phase type (I odd); Duration (I even)	3
XXX	XMTBF or VMTTR	
X2	X squared	
Y	Same as XMTTR	
YD	Truncation line accept	21A

APPENDIX C

SPARES SUBROUTINE VARIABLE LIST

CUT	FLSIP cut point
DUM	Dummy variable
EX90DD	Expected 90 day demand
ITMPOP(I)	Number of equipment type I in reliability block diagram
K	Counter
KFACT	K factorial
PRBSUM	Poisson probability summation
SPR1-14	Various user defined input variables

APPENDIX D

MODIFICATIONS TO TIGER PROGRAM INPUT

To use the GAMMA and DEMO options, the end of the main section of the program must be changed to the following:

```
1210 IF (GMMA.EQ.BLNK) GO TO 1230
1220 CALL GAMMA
1230 CONTINUE
      IF (DMNO.EQ.BLNK) GO TO 1240
      CALL DEMO
1240 STOP
      END
```

Subroutine GAMMA, function GAMF, subroutine DEMO, function CHISQ, subroutine TGEN, and subroutine CKTP must be added to the program deck (note: none of these have been utilized or verified for use on the NPS computer).

The following changes were made to the original input deck:

Card 2 - INREJ replaced by ISEED; the random number generator seed.

Card 14 - If spares subroutine is desired, enter 999. for SX. Fourteen variables (SPR1,SPR2,...,SPR14) may then be read into the spares subroutine in F4.0 format starting in column 25.

These changes are incorporated into the input requirements shown on the following pages. They should be used when preparing the TIGER data input deck.

All integer fields must be right justified

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(1) Timeline Iteration Card			
1-4	I4	JCC	No. of timeline variations to be run for the data deck. If JCC exceeds 1, only phase type and duration card(s) must be added in the back of the data deck, followed by a blank card.
5-80	19A4	RUNID	Alphanumeric run identifier.
(2) Statistical Parameter Card			
58	1-4	I4	NMAX
			Maximum number of missions to be run (should be in multiples of 50 and must not exceed 1000)
5-8	I4	NOPT	Optimal number of missions (not to exceed NMAX).
9-12	F4.0	PL	Specification requirement for reliability.
13-16	F4.0	XK	Standard deviation to be used in calculating lower control limit.
17-20	I4	ISEED	Random number seed.
21-24	I4	NPH	No. of phase types--not to exceed 6.

NOTE: - If a predefined fixed number of missions is to be run, set PL =1.0, and NOPT and NMAX to the desired number of missions.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(3) Phase Type and Duration Card(s)			
1-2	F2.0	XXT(1)	Phase type number for first simulation sequence.
3-10	F8.0	XXT(2)	Duration of first sequence.
11-12	F2.0	XXT(3)	Phase type number for second simulation sequence (if any).
13-20	F8.0	XXT(4)	Duration of second sequence.
21-22	F2.0	XXT(5)	Phase type number for third simulation sequence (if any).
23-30	F8.0	XXT(6)	Duration of third sequence.
31-32	F2.0	XXT(7)	Phase type number for fourth sequence (if any).
33-40	F8.0	XXT(8)	Duration of fourth sequence.
41-42	F2.0	XXT(9)	Phase type no. for fifth sequence (if any).
43-50	F8.0	XXT(10)	Duration of fifth sequence.
Note: If more than 5 phase sequences are needed, continue on additional cards using the same fields. No more than 95 phase sequences are permitted.			
(4) *****Blank Card*****			

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>																																												
(5) Printout Option Card 1-4	I4	KOPT	<p>Printout option switch</p> <ul style="list-style-type: none"> = 1 for management summary printout. = 2 for engineering summary printout. = 3 for TIGER complete details printout. (For debugging only) = 4 to suppress printout of input data. = 5 to specify printout using the KS variables (see below) = 6 for TIGER/MANNING complete details printout. (For debugging only). <p>If KOPT=5, select from the following output options as needed (otherwise leave the field(s) blank):</p> <table> <tbody> <tr> <td>5-8</td><td>I4</td><td>KS(1)</td><td>= 1: Input Data</td></tr> <tr> <td>9-12</td><td>I4</td><td>KS(2)</td><td>= 1: equipment down at time of mission failure.</td></tr> <tr> <td>13-16</td><td>I4</td><td>KS(3)</td><td>= 1: down time at end of phase.</td></tr> <tr> <td>17-20</td><td>I4</td><td>KS(4)</td><td>= 1: abort messages.</td></tr> <tr> <td>21-24</td><td>I4</td><td>KS(5)</td><td>= 1: all events.</td></tr> <tr> <td>25-28</td><td>I4</td><td>KS(6)</td><td>= 1: ETIME Matrix. (For debugging only.)</td></tr> <tr> <td>29-32</td><td>I4</td><td>KS(7)</td><td>= 1: Not used.</td></tr> <tr> <td>33-36</td><td>I4</td><td>KS(8)</td><td>= 1: Not used.</td></tr> <tr> <td>37-40</td><td>I4</td><td>KS(9)</td><td>= 1: Not used.</td></tr> <tr> <td>41-44</td><td>I4</td><td>KS(10)</td><td>= 1: System & subsystem status.</td></tr> <tr> <td>45-48</td><td>I4</td><td>KS(11)</td><td>= 1: TIGER/MANNING debugging printout.</td></tr> </tbody> </table>	5-8	I4	KS(1)	= 1: Input Data	9-12	I4	KS(2)	= 1: equipment down at time of mission failure.	13-16	I4	KS(3)	= 1: down time at end of phase.	17-20	I4	KS(4)	= 1: abort messages.	21-24	I4	KS(5)	= 1: all events.	25-28	I4	KS(6)	= 1: ETIME Matrix. (For debugging only.)	29-32	I4	KS(7)	= 1: Not used.	33-36	I4	KS(8)	= 1: Not used.	37-40	I4	KS(9)	= 1: Not used.	41-44	I4	KS(10)	= 1: System & subsystem status.	45-48	I4	KS(11)	= 1: TIGER/MANNING debugging printout.
5-8	I4	KS(1)	= 1: Input Data																																												
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21-24	I4	KS(5)	= 1: all events.																																												
25-28	I4	KS(6)	= 1: ETIME Matrix. (For debugging only.)																																												
29-32	I4	KS(7)	= 1: Not used.																																												
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41-44	I4	KS(10)	= 1: System & subsystem status.																																												
45-48	I4	KS(11)	= 1: TIGER/MANNING debugging printout.																																												

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
Printout Option Card (Cont.)			
49-52	I4	KS(12)	= 1: Status of all groups
53-56	I4	KS(13)	= 1: Downtime message.
(6) Phase Repair Card			
1-4	I4	IFLAG(1)	Repair option for each phase type, up to 6: = 0 if on-board repair allowed in the phase. = 1 if no on-board repair allowed. = 2 if on-board repair allowed but failure inhibited.
5-8	I4	IFLAG(2)	
9-12	I4	IFLAG(3)	
13-16	I4	IFLAG(4)	
17-20	I4	IFLAG(5)	
21-24	I4	IFLAG(6)	
(7) Repair Policy Card			
1-4	F4.0	REPOL	Decimal fraction of repairs to be performed
5-12	F8.2	TAD2	aboard ship, i.e. organizational level.
13-16	F4.0	XM	Mission allowable downtime
17-20	F4.0	XT	MTBF Multiplier. Default = 1.0 MTTR Multiplier. Default = 1.0

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(8) Equipment Type Cards (one card for each equipment type)			
1-4	I4	I	Equipment type numbers - should be assigned sequentially starting at 1, not to exceed 200.
5-20	4A4	F1	Equipment type description/nomenclature.
21-28	F8.0	XMTBF	Mean time between failure (MTBF).
29-32	F4.0	XMTTR	Mean time to repair (MTTR). Precede by negative sign and include the variable MTTR card if variable MTTR option desired. Non-repairable is indicated by a value of 9999.
33-36	F4.0	U	Duty cycle/Utilization (non-zero decimal fraction).
37-40	F4.0	V	Administrative delay time from tender to ship.
41-44	F4.0	W	Administrative delay time from depot to ship.
45-48	I4	IUI	If a variable duty cycle (VDC) for this equipment type is desired, assign a sequential number (between 1 and 50) and include the VDC card following. Otherwise leave this field blank.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(9) <u>Variable Duty Cycle (VDC) Card</u>			(Optional - If IUI on previous type card is non-zero, place this card immediately behind the type card to which it refers. A maximum of 50 VDC cards per deck are allowed.)
1-4	I4	IV	VDC Identifier-sequential number, same as the value of IUI on the preceding equipment type card.
5-8	F4.0	VDC(1)	Duty cycle/utilization of the equipment type during each phase type 1-6. These values override the value of U on the preceding Equipment Type Card.
9-12	F4.0	VDC(2)	
13-16	F4.0	VDC(3)	
17-20	F4.0	VDC(4)	
21-24	F4.0	VDC(5)	
25-28	F4.0	VDC(6)	
(10) <u>Variable Mean Time to Repair (MTTR) Card</u> (Optional - If XMTTR is negative on the Equipment Type Card place this card behind the VDC Card or, if there is no VDC Card, behind the Equipment Type Card.)			
1-4	F4.0	VMTTR(1)	MTTR values of the equipment type during each phase type 1-6. Non-repairable is indicated by 9999.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
<u>Variable Mean Time to Repair (MTTR) Card (Cont.)</u>			
5-8	F4.0	VMTTR(2)	
9-12	F4.0	VMTTR(3)	
13-16	F4.0	VMTTR(4)	
17-20	F4.0	VMTTR(5)	
21-24	F4.0	VMTTR(6)	
(11) *****Blank Card***** (This indicates the end of the equipment type cards.)			
(12) <u>Equipment Cards</u> (One for each equipment type - Place sequentially by type number)			
1-4	I4	NTYPE	The type number associated with the equipment listed in the next field(s).
5-8	I4	LOAD(1)	Equipment numbers of those equipment which belong to the designated equipment type -
9-12	I4	LOAD(2)	up to 19 equipment per card (if there are
13-16	I4	LOAD(3)	more than 19 equipment associated with a given type, use additional equipment cards
17-20	I4	LOAD(4)	and repeat the same type number). The
21-24	I4	LOAD(5)	largest equipment number allowed by the
25-28	I4	LOAD(6)	program is 500. The total number of equipment must not exceed 500. No gaps are
29-32	I4	LOAD(7)	allowed between equipment number 1 and the largest assigned equipment number.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
Equipment Cards (Cont.)			
33-36	I4	LOAD(8)	
37-40	I4	LOAD(9)	
41-44	I4	LOAD(10)	
45-48	I4	LOAD(11)	
49-52	I4	LOAD(12)	
53-56	I4	LOAD(13)	
57-60	I4	LOAD(14)	
61-64	I4	LOAD(15)	
65-68	I4	LOAD(16)	
69-72	I4	LOAD(17)	
73-76	I4	LOAD(18)	
77-80	I4	LOAD(19)	

(13) *****Blank Card***** (This indicates end of equipment cards.)

(14) Blank Card or literal "UNLIMITED SPARES" starting in column 1. If Blank Card is used then the spares multiplier (SX) may be inserted in Col. 21-24. The format for SX is F4.0 and the default value is 1.0; Use 999. to call SPARES subroutine. Variables SPR1-SPR14 may be inserted in F4.0 format starting in Col. 25.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(15) Spares Cards (Omit if unlimited spares specified above. One spares card for each equipment type-program assumes these cards are in sequential order starting with Type 1)			
1-4	I4	ISPARE(1)	Number of organizational level spares (on-board) for the equipment type.
5-8	I4	ISPARE(2)	Number of spares at the tender for the equipment type.
9-12	I4	ISPARE(3)	Number of spares at the base (depot) for the equipment type.
NOTE: For each phase type, a set of the remaining cards (except the optional output and demo cards which appear once) must be placed consecutively in the data deck.			
(16) System Card			
1-4	A4	ID	Any alphanumeric, e.g., the literal "SYST"
5-8	I4	LL	Phase type number (sequential) - Maximum value is 6.
9-12	I4	NSS	Number of subsystems in the phase (varies only from 1 to 31)
13-16	I4	ISS	System identification number (usually last group number on the configuration matrix cards).

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
System Card (Cont.)			
17-24	F8.0	SSTIME	System allowable sustained down time TAD1 (should not be less than subsystem TAD1 values). This value should be less than or equal to TAD2 (Repair Policy Card). To inhibit aborts use a value of 100000.
(17) Subsystem Cards (One for each subsystem - up to 31.) At least one subsystem is required.			
1-4	A4	ID	Any alphanumeric, e.g., the literal "SS1", "SS2", ... "SS31".
5-8	I4	LL	Phase type number.
13-16	I4	ISS	Subsystem identification number. This is a group number for a group defined on a Configuration Matrix Card (see below). Each designated subsystem group must be a group that, upon its failure, causes the system to fail.
17-24	F8.0	SSTIME(2)	Subsystem allowable sustained down time (TAD1). This value should be less than or equal to STIME on the System Card. To inhibit aborts use a value of 100000.

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(18) <u>Configuration Matrix Cards</u>		(One card for each group, up to 300 cards)	<p>1-4 I4 NRO The number of members in the group defined on this card that are required to be operating and in an upstate.</p> <p>5-8 I4 IB(1) The group number assigned to the group of members defined on this card. It may vary from 501 to 1000 in any order.</p> <p>9-12 I4 IB(2) The numbers of the equipment and groups which make up the group defined on this card. The maximum number of members in a group is unlimited; however, if there are more than 7, a continuation card is required, which is of the same format.</p> <p>13-16 I4 IB(3) The number required and master group number must be identical on all continuation cards.</p> <p>17-20 I4 IB(4) </p> <p>21-24 I4 IB(5) </p> <p>25-28 I4 IB(6) </p> <p>29-32 I4 IB(7) </p> <p>33-36 I4 IB(8) </p>
(19) <u>Equipment Operating Rule Cards</u>			<p>(Optional - Usually this card is placed immediately behind the configuration matrix card which refers to the equipment and groups on this card.)</p> <p>These cards indicate the equipment operating rules for string or standby equipment. The string equipment operating rule causes shutdown of a designated series equipment upon failure of any of the other equipment or equipment groups on the card. The standby</p>

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
Equipment Operating Rule Cards (Cont.)			
			equipment operating rule causes designated equipment to be energized upon failure of any of the other equipment or equipment groups on the card. The maximum number of equipment operating rules is 49. (One rule defined per card.)
1-4	I4	ISTB(1)	The designated equipment number. If it is a standby equipment, it must be preceded by a minus sign.
5-8	I4	ISTB(2)	The other equipment or equipment group numbers.
9-12	I4	ISTB(3)	
13-16	I4	ISTB(4)	
17-20	I4	ISTB(5)	
21-24	I4	ISTB(6)	
25-28	I4	ISTB(7)	
29-32	I4	ISTB(8)	
33-36	I4	ISTB(9)	
37-40	I4	ISTB(10)	
41-44	I4	IRULE	Place any non-zero integer in this field (to distinguish Equipment Operating Rule Cards from Configuration Matrix Cards).

	<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
(20)	*****Blank Card*****			(This indicates end of phase configuration and operating rules.)
(21)	Optional Output Card	(Optional - Appears once in computer job deck)		
	1-4	A4	SPRS	Place any alphanumeric, e.g., "SPR", in this field if a table of spares usage is desired.
	5-8	A4	APPL	Place any alphanumeric, e.g., "APL", in this field if a summary table of equipment that caused mission failures (unreliability) and system down times (unavailability) is desired.
	9-12	A4	GMMA	Place any alphanumeric, e.g., "GMA", in this field if the gamma distribution output is desired.
	13-16	A4	DEMO	Place any alphanumeric, e.g., "DEMO", in this field if a sequential probability ratio test plan for the system being analyzed is desired. If this option is exercised, an additional card, 21A, is required.
(22)	DEMO Information Card	(Optional - must be included if DEMO is specified on the Optional Output Card.)		
	1-4	F4.0	A	Producer Risk.
	5-8	F4.0	B	Consumer Risk

DEMO Information Card (Cont.)

<u>Columns</u>	<u>Format</u>	<u>Variable Name</u>	<u>Description</u>
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9-12 F4.0 R Discrimination Ratio.

The following are optional inputs:

13-16	F4.0	HAD	X-Axis accept intercept (Delta).
17-20	F4.0	HRD	X-Axis reject intercept (Delta).
21-24	F4.0	YD	Truncation line accept (Delta).
25-28	F4.0	SLD	Slope (Delta).
29-32	I4	KD	Truncation line reject (Delta).
33-36	I4	ITIME	Number of sets (explained in Appendix C).
37-40	I4	ITER	Number of simulations per set.
41-44	I4	N	Random number initializer.

TIGER COMPUTER OUTPUT (SAMPLE)

EQUIP FAILURES	TYPE NO.	TOTAL EQUIP.	Avg. No. FAILURES PER MISSION	SUMMARY	Avg. CM MANHOURS PER MISSION
1	1	25	0.025	0.0	
2	2	637	0.637	0.0	
3	3	642	0.642	0.0	
4	4	525	0.525	0.0	
5	5	525	0.525	0.0	
6	6	64	0.64	0.0	
7	7	636	0.636	0.0	
8	8	582	0.582	0.0	
9	9	582	0.582	0.0	
10	10	679	0.679	0.0	
11	11	793	0.793	0.0	
12	12	30	0.30	0.0	
13	13	318	0.318	0.0	
14	14	541	0.541	0.0	
15	15	416	0.416	0.0	
16	16	52	0.52	0.0	
		5865	5865	5.865	5.865
					0.0

AVERAGE NUMBER OF SPARES USED PER MISSION

SPARES TYPE	SHIP STOCK	USED	TENDER STOCK	USED	BASE STOCK	USED
1	0.50	0.0	0.0	0.0	0.0000000	0.0
2	0.96	0.0	0.0	0.0	0.0000000	0.0
3	1.84	0.0	0.0	0.0	0.0000000	0.0
4	0.57	0.0	0.0	0.0	0.0000000	0.0
5	0.27	0.0	0.0	0.0	0.0000000	0.0
6	0.43	0.0	0.0	0.0	0.0000000	0.0
7	0.34	0.0	0.0	0.0	0.0000000	0.0
8	0.00	0.0	0.0	0.0	0.0000000	0.0
9	0.00	0.0	0.0	0.0	0.0000000	0.0
10	0.00	0.0	0.0	0.0	0.0000000	0.0
11	0.00	0.0	0.0	0.0	0.0000000	0.0

CRITICAL EQUIPMENTS
UNAVAILABILITY AND
PERCENT OF UNAVAILABILITY

NAME	NUM HRS	UNA V	PERCENT	EQU TYPE	EQU NUM
PULSE - P	143678.1250	0.0665	24.01	7	10
PULSE - A	86987.9375	0.0432	10.99	2	13
CIRCUIT BD - D	71777.3125	0.0370	9.97	3	14
COUPLER	55935.4648	0.0305	8.40	4	15
VIDEO SCREEN	42291.3203	0.0297	7.63	5	16
CIRCUIT BD - E	38421.7227	0.0297	7.63	6	17
TRANSPORTER	24414.9943	0.0284	7.00	7	18
CIRCUIT BD - A	22381.9844	0.0284	7.00	8	19
RHEOSTAT	21809.2867	0.0280	6.97	9	20
CIRCUIT BD - C	20024.2867	0.0274	6.83	10	21
SWITCH	16121.3148	0.0274	6.83	11	22
CIRCUIT BD - A	1640.4794	0.0274	6.83	12	23
CIRCUIT BD - B	1433.9836	0.0274	6.83	13	24
CIRCUIT BD - B	1433.9836	0.0274	6.83	14	25

CRITICAL EQUIPMENTS
UNRELIABILITY AND
PERCENT OF MISSION FAILURES

DESCRIPTION	NO. FAILURES	UNREL.	PERCENT	EQUIP NO.	TYPE
FUSE - B	162.0	0.1620	26.30	10	1073465964247-076
FUSE - A	102.0	0.1020	16.30	12	1276656977011-066
CIRCUIT BD - D	78.0	0.0780	12.00	11	1151500000000000000
CIRCUIT BD - E	49.0	0.0490	8.00	12	1277777777777777777
COUPLER	48.0	0.0480	8.00	13	1377777777777777777
VIDEO SCREEN	34.0	0.0340	5.40	14	1477777777777777777
TRANSPORTER	30.0	0.0300	5.00	15	1577777777777777777
CIRCUIT BD - A	25.0	0.0250	5.00	16	1677777777777777777
CIRCUIT BD - B	24.0	0.0240	4.80	17	1777777777777777777
CIRCUIT BD - C	22.0	0.0220	4.40	18	1877777777777777777
RHOSTAT	20.0	0.0200	4.00	19	1977777777777777777
SWITCH	15.0	0.0150	3.00	20	2077777777777777777
CIRCUIT BD - B	3.0	0.0030	0.30	21	2177777777777777777
CIRCUIT BD - B	2.5	0.0025	0.25	22	2277777777777777777
CIRCUIT BD - B	1.5	0.0015	0.15	23	2377777777777777777

TOTAL NO. MISSIONS=1000
TOTAL NO. MISSION FAILURES= 616

RELIABILITY PHASE 1,	1,	IS 0.3840	INSTANT AVAILABILITY	IS 1.0000
READINESS		IS 0.7229	RELIABILITY UP TO PHASE 1	IS 0.3840
AVERAGE AVAILABILITY		IS 0.7229	READINESS	IS 0.7229
			AVERAGE AVAILABILITY	IS 0.7229
			INSTANT AVAILABILITY	IS 0.3840

A GRAND TOTAL OF 1000 MISSIONS HAVE BEEN RUN.

THE RELIABILITY IS 0.3840
THE LOWER CONFIDENCE LIMIT IS 0.3646
THE SPEC REQUIREMENT IS 0.10000
THE READINESS IS 0.7229
THE AVERAGE AVAILABILITY IS 0.7229
THE INSTANT AVAILABILITY IS 0.3840

THE MEAN TIME BETWEEN MISSION FAILURES IS 1033.9
THE LC190 MTBF IS 1033.9
THE HTBMP VARIANCE IS 0.189

THE SYSTEM HUT IS 2535.0
THE SYSTEM HDT IS 0.189
SIMULATION COMPLETE-OPTIMUM NUMBER MISSIONS WERE RUN

TIGER IBM/360 FORTRAN IV COMPUTER PROGRAM

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MAIN0010
MAIN0020
MAIN0030
MAIN0040
MAIN0050
MAIN0060
MAIN0070
MAIN0080
MAIN0090
MAIN0100
MAIN0110
MAIN0120
MAIN0130
MAIN0140
MAIN0150
MAIN0160
MAIN0170
MAIN0180
MAIN0190
MAIN0200
MAIN0210
MAIN0220
MAIN0230
MAIN0240
MAIN0250
MAIN0260
MAIN0270
MAIN0280
MAIN0290
MAIN0300
MAIN0310
MAIN0320
MAIN0330
MAIN0340
MAIN0350
MAIN0360
MAIN0370
MAIN0380
MAIN0390
MAIN0400
MAIN0410
MAIN0420
MAIN0430
MAIN0440
MAIN0450
MAIN0460
MAIN0470

MAIN /ALL PHADNT2 ENDOPHA !CKI IFF IFR INUM IOP! JBB KEQ KKK KZZ
1 KKJ KS JLL LLLAS NEQ NPH NTYPET NUM FREDAD1(100) RELP,RED2
2 REEL PV REPOL STPHAS T1 XCUM T3 UP? IF? CP, T3, TIME,T3SUM

COMMON/EXTRA/ K$(20) ISW(31)
COMMON/NPH/ SEQ/INDAB(100) INM(100) IAUP(100) ITT2(100)
LAUP2(100)
COMMON/TYP/EX(200) ISPARSE(3,200) IUSED(3,200)
COMMON/MAX/XNEQ MAXIB MAXSD
COMMON/GAMMA/XMTBA:YAR,RELGA(100),TIMA(100),XT(200),IT,ISEED
COMMON/TABORT/XTABT(1000) RDT
COMMON/TIGAP/ UP4,XNUM,BAPRIN,AVA,XPCAP,RUNID(19),TYCOON(500)
+ COUNTB(500) XTCUM
COMMON/DONE/DONE(3)
DATA BLNK/4H

MAXRUN=1000
MAXNPH=6
MAXSTD=50
MAXNEQ=500
MAXTYP=200
MAXIB=300
MAXSS=31
MAXSEQ=100
CALL QYFLOW
READ(5,10) JCC, (RUNID(I),I=1,19)
10 WRITE(6,19A4)
      WRITE(6,220) JCC
      DO 1230 J=30,19A4
12 FORMAT(1H1,30,(RUNID(I),I=1,19))
      FORMAT(1H1,30,19A4//)
      WRITE(6,40)
      WRITE(6,50)
      WRITE(6,55)
      FORMAT(1X,'5 OH' +++++++ +++++++ +++++++ +++++++ +++++++ )
      FORMAT(1X,50H+' NAVSEC 6112 LUET JEN+MANDEL+VAIL+ALLEY+BROWN' +++)
55 FORMAT(1X,50H+NPS IBM/360 VERSION LT. J. LEATHER THESIS 9/80++)
      BAPRIN=0.0
      DO 70 I=1,MAXNEQ
60 COUNTB(I)=0.0
      TYCOON(I)=0.0

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```

KQU(I)=0
ETIME(I)=100000.
70  NUM=0
    IFF=0
    IFR=0
    UP4=0.0
    T3=0.0
    T3SUM=0.0
    SUMX2=0.0
    DO 80 I=1,100
        TMA(I)=0.
80   DO 90 I=1,3
        DO 90 J=1,MAXTYP
        USED(I,J)=0
        DO 100 I=1,MAXSEQ
        T2(I)=0.0
        UP2(I)=0.0
        IAUP1(I)=0
        IAUP2(I)=0
        READ(I,I)=0.0
        INM(I)=0
        INOABT(I)=0
        IAUP=0
        XTCUM=0
        IF (JC-1) 110,110,140
        IF (5,120) NMAX,NOPT,PL,XK,I SEED,NPH
110  READ(5,120)
120  FORMAT(12(2F4.0))
130  FORMAT(1X216,2XF4.2,2XF5.2,2XI6,2XI4)
140  CONTINUE
150  WRITE(6,170) I SEED
160  FORMAT(1/1X15HRANDOM,SEED,IS,14)
170  IF (NMAX-MAXRUN) 190,180
180  NMAX=1000
190  NOPT=1000
    DO 200 I=1,NMAX
200  XTAB(I)=100000
    WRITE(6,130) NMAX,NOPT,PL,XK,I SEED,NPH
    IF (MAXNPH-NPH) 1240,210,210
210  I NUM=50
    FORMAT(4(1I10)
220  DO 250 I=1,191,10
        READ(5,140) XXT(I),XXT(I+J),J=1,9
230  IF (XXT(I),260,260,250)
240  FORMAT(5(F2.0,F8.0))
250  CONTINUE
260  WRITE(6,270)
270  FORMAT(1H1,10X40Hphase,SEQUENCE,TYPE,DURATION,CUM TIME)

```

```

IK=1
IK2=2*IK
IK3=IK2-1
IXXT=XXT(IK3)
TIMA(1)=XXT(2)
WRITE(6,280) IK,IXXT,XXT(IK2),TIMA(IK)
280 FORMAT(19X,14,2X,14,2XF8.2,2XF8.2)
DO 300 IK=2,100
IK2=2*IK
IK3=IK2-1
IF (IXXT(IK2))=TIMA(IK-1)+XXT(IK2)
290 IXXT=XXT(IK3)
WRITE(6,280) IK,IXXT,XXT(IK2),TIMA(IK)
300 CONTINUE
310 CONTINUE
IF (JC-1) 320,320,330
320 CALL PACK
C 330 CONTINUE
JBB=1
RELPY=1.0
RELP=1.0
UP3=0.0
TT3=0.0
READ02=0.0
DO 340 I=1,MAXSS
340 ISW(I)=1
ICR1=0
DNT2=0.0
350 STPHAS=0
T1=0.0
C RDT IS RUNNING DOWNTIME
RDT=0.0
C KKK = 0 INDICATES FIRST PHASE IN MISSION.
C C C C C START OF MISSION INDICATION
C C C C C IF (KS(8)) 380,380,360
360 KAB=NUM+1
WRITE(6,370) KAB
370 FORMAT(1X,16HSTART OF MISSION,(5,20H*****))
380 KKK=0
I=1
390

```

```

400 LL=XXT(I)
410 IF(LL)450,450,410
410 ENDPA=S+X*XT(I+1)
I=I+2
C CALL RUN
C I=X=NUM+1
C IF(I>XTABT(I)) 420,420,440
420 WRITE(6,430)
430 FORMAT(1X44HTHE ABORT TIME IS ZERO, CHECK THE INPUT DATA.)
430 GOTO 1240
440 S+PHAS=ENDPHA
N=NSS(LL)+1
GOTO 400
C
C STATISTICAL SUMMARY BEGINS HERE
C
450 NUM=NUM+1
450 IF(I>EOP) 460,460,480
460 IFF=IFF+1
460 IF(IFF>1) 470,480,470
470 CONTINUE
470 T3SUM=T3SUM+T3
T3=0.0
480 XTCUM=XTCUM+X*NUM
480 UP6=UP6+ENDPA-DNT2
JBB IS THE PHASE SEQUENCE NUMBER
490 IF(XTABT(INUM)-1000000.) 500,490,500
490 X=ENDPA
490 GO TO 510
500 XXTABT(INUM)
510 X2=X**2
510 SUMX=SUMX+X
510 SUMX2=SUMX2+X*X
510 IF(LISW(N)) 530,530,520
520 IAUP=IAUP+1
520 IF(NUM-1>NUM) 330,540,540
540 INUM=INUM+50
550 WRITE(6,560)
560 FORMAT(1IX16HA GRAND TOTAL OF,16,24H MISSIONS HAVE BEEN RUN.)
570 XNUM=NUM
580 XPCAP=XT*CUM/XNUM
580 WRITE(6,590)
590 WRITE(6,590) XPCAP
590 FORMAT(1X24HTHE RELIABILITY IS F8.4)
600 XPLCL=XPCAP-XK*SQRT(XPCAP*(1.-XPCAP))
610 IF(XPLCL) 620,630,630
620 XPLCL=0.0
630 WRITE(6,640)
640 FORMAT(1X24HTHE LOWER CUNF LIMIT IS ,F8.4)

```

```

      WRITE (6,650) PL
650  FORMAT (1X24HTHE SPEC REQUIREMENT IS ,F8.4)
      WRITE (6,660) RED2
660  FORMAT (1X17HTHE READINESS IS ,7XF8.4)
      AVA=UP4/T13
      WRITE (6,670) AVA
670  FORMAT (1X28HTHE AVERAGE AVAILABILITY IS ,F8.4)
      XIAUP=IAUP
      AVAINS=XIAUP/XNUM
      WRITE (6,680) AVAINS
680  FORMAT (1X28HTHE INSTANT AVAILABILITY IS ,F8.4)
      XDWN=XNUM-XTCUM
      IF (XDWN) 690,690,700
690  XMTBA=2.0*SUMX
      XLCLCA=0.434*SUMX
      VAR=(0.5*SUMX)**2
      XMTBA=SUMX/XDWN
      VAR=(SUMX**2/XNUM)-(SUMX/XNUM)**2
      CORR=(SUMX*(1/XDWN-1/XNUM))**2
      VAR=VAR+CORR
      XLCLCA=XMTBA-(1.28*SQRT(VAR))
710  WRITE (6,720) XMTBA
720  FORMAT (1IX41HTHE MEAN TIME BETWEEN MISSION FAILURES IS ,F20.1)
      WRITE (6,730) XLCLCA
730  FORMAT (1IX21HTHE LCL,90, MTBF IS ,F20.1)
      WRITE (6,740) VAR
740  FORMAT (1IX27HTHE MTBF VARIANCE IS ,F20.1)
      XIFF=IFF
      XIFF=IFF
      IF (IFF) 760,750,760
750  XMUT=2.0*UP4
      XMDT=0.0
      GO TO 790
760  XMUT=UP4/XIFF
      IF (IFF) 780,770,780
770  XMDT=(TT3-UP4-T3SUM)/XIFF
      GO TO 790
780  XMDT=(TT3-UP4-T3SUM)/XIFF
      790 WRITE (6,810) XMUT
      800 WRITE (6,820) XMDT
      810 FORMAT (1IX18HTHE SYSTEM MDT IS ,F20.1)
      820 FORMAT (1IX18HTHE SYSTEM MDT IS ,F20.3)
      830 IF (XPCAP-PL) 840,840,850
      840 IF (NOPT-NUK) 870,870,850
      850 WRITE (6,860)
      860 FORMAT (1IX14HANOTHER SET OF 3H 50 20MISSIONS WILL BE RUN,43H TO MAIN2380
1BTAIN REQUIRED STATISTICAL CONFIDENCE.)

```

```

GO TO 330
870 WRITE (6,880)
880 FORMAT (1X,2H SIMULATION COMPLETE-OPTIMUM NUMBER MISSIONS WERE RUN)
     IF(IPL.EQ.1) GO TO 910
890 FORMAT (1X,3H WEAPON SYSTEM FAILS REQUIREMENTS.)
910 GO TO 1010
920 IF(ANMAX-NUM) 930,930,960
930 WRITE (6,940)
940 FORMAT (1X,52H SIM COMPLETE-P REDEFINED MAX NUMBER MISSIONS WERE RUN)
     IF((XPCLCL-PL) 890,990,990
     IF((XPCLCL-PL) 850,970,970
950 IF(IPL.EQ.1) GO TO 1010
960 IF(IPL.EQ.1) GO TO 1010
970 WRITE (6,980)
980 FORMAT (2X,2H SIMULATION COMPLETE - )
     IF(IPL.EQ.1) GO TO 1010
990 WRITE (6,1000)
1000 FORMAT (1X,3H WEAPON SYSTEM MEETS REQUIREMENTS.)
1010 CONTINUE
C*** READ CARD CONTAINING PRINTOUT OPTIONS
C*** SPRS=SPARES GIVES PRINTOUT OF AVG. SPARES USED PER MISSION
C*** BY EQUIPMENT TYPE
C*** APP=APPL GIVES PRINTOUT OF CRITICAL EQUIPMENTS AND UNREL.
C*** GMMA=GMMA GIVES PRINTOUT OF GAMMA FUNCTION WHICH REPRESENTS THE
C*** SYSTEM OR SUBSYSTEM CONFIGURATION AND VALUES AT TIME INTERVALS
C*** SPECIFIED ON PHASE CARD
C   IF(LJC-1) 1020,1020,1040
C1020 READ (5,1030) SPRS,APPL,GMMA
C1020 READ (5,1030) SPRS,APPL,GMMA,DMMO
C1030 FORMAT (3A4)
C1030 FORMAT (4A4)
C1040 IF((SPRS.EQ.BLNK) GO TO 1190
C1040 IF((SPRS.EQ.1050) 1190,1050
C
C EQUIP FAILURE AND CORRECTIVE MAINTENANCE SUMMARY
C
1050 LDIFF=0
     TAFM=0.0
     TACMMH=0.0
     WRITE (6,1060)
1060 FORMAT (1H1,4X,53HEQUIP FAILURES AND CORRECTIVE MAINTENANCE(CMH) SUMMA
     LMARY/BX71HEQUIP; NO. TYPE NO. TOTAL EQUIP AVG. NO. FAILURES, AMAIN2800
     2VG. CM MANHOURS / 32X8HFAILURES, 7X11HPER MISSION, 5X11HPER MISSION/1
     DQI 1090 I=1,NEQ
     IF(XMTTR(I,EQUIP(I)) EQ 9999) GO TO 1090
     IF(KEQUIP(I) EQ 1090,1090,1070
     IF(KEQUL(I) EQ 1090,1090,1070
     IF(IEQ=1ABS(IEQUIP(I))
     ACMMH=AFM#ABS(XMTTR(IEQ))

```

```

      WRITE(6,1080) 1,IEQ,KEQU(1),AFM,ACMMH
      FORMAT(10X,14.6X,14.6X,10.6XF10.3,6XF10.3)
      IDIFF=IDIFF+KEQU(1)
      TAFM=TAFM+AFM
      TACMMH=TACMMH+ACMMH

1090  CONTINUE
      WRITE(6,1100) IDIFF,TAFM,TACMMH
      FORMAT(31X,10H-----,6X10H-----,6X10H-----,6X10H-----)
      1F10.3,6XF10.3)

1110  CONTINUE
      WRITE(6,1120)
      FORMAT(11H,3X,41HAVERAGE NUMBER OF SPARES USED PER MISSION)
      1120  FORMAT(11H,3X,41)
      WRITE(6,1130)
      FORMAT(1/4X6HSPARES,7X4HSHIP,18X6HTENDER,16X4HBASE)
      1130  FORMAT(6,1140)
      WRITE(8X4HTYPE! 4X3(5HSSTOCK,3X4HUUSED,10X))
      1140  FORMAT(8X4HTYPE! 4X3(5HSSTOCK,3X4HUUSED,10X))
      DO 1170 J=1,NTYPE
      ALDONE=0.0
      DO 1150 I=1,3
      DONE(I)=IUSED(I,J)/XNUM
      ALDONE=ALDONE+DONE(I)
      1150  CONTINUE
      IF(ALDONE)1155 1170,1155
      1155  WRITE(6,1160)J,(ISPAKE(I,J),DONE(I),I=1,3)
      1160  FORMAT(8XI4,4X1)
      1180  CONTINUE
      1170  CONTINUE
      C1190  IF(APPL)1200 1210,1200
      C1190  IF(APPL.EQ.BLNK) GO TO 1210
      1200  BAPRIN=-1.0
      CALL APPL

C     SEE APPENDIX TO THESIS ON PROCEDURE TO ADD GAMMA AND DEMO

      1210  CONTINUE
      1220  CONTINUE
      1230  CONTINUE
      1240  STOP
      END

```

```

SUBROUTINE RUN
COMMON /MAXNNEQ, MAXTYP, MAXIB, MAXSTD
COMMON /ALPHA/DNT2, ENDPH, ICR, IFF, INUM, IOPT, JBB, KEQ, KZZ
COMMON /KELKKS/LISTPHAS, T1X, CUM, REND2, REDAD, T3, T3SUM, RED2
COMMON /RELPP, REPO, L3001, IB16300, 8, NLINE(6)
COMMON /EXTRA/KS(20), ISW(31), KEQU(500), ETIME(1000), XMTBF(200),
COMMON /NPHE/NS(6), IFLAG(6), TITLE(631), SSTIME(631), ISS(631),
COMMON /SEQ/INOAB(100), INM(100), IAUP(100), UP2(100),
1 LAUP2(100)
COMMON /TYP/EX(2,200), ISPAIR(31200), IUSED(31200), IUSED(31200),
COMMON /GAMWA/XMTBA, VAR, RELGA(100), TIMA(100), Xf(200), If, ISEED
COMMON /TABORT/XTABT(1000), RDT
COMMON /DELT/TA/KKK2
COMMON /XXX/XXX
COMMON /VDC/VDC(50,6), UU(200), VMTRK(200,6), TAD2
COMMON /STAN/ISTB(60,10,6)
COMMON /RUNAP/ITEMP2, DELT, ISSA(31), ISSC

```

C START OF PHASE LL

```

IODEP=0
TP=STPHAS
KAA=NUM+1
XKAA=KAA
NX=NSS(LL)
N=NX+1
ITEMP=0
ITEMP2=0
IF (KKK) 40,10,40
10 DO 20 I=1,3
      DO 20 J=1,NTYPE
      IUSED(I,J)=0
20 CONTINUE
      DO 30 I=1,NEQ
30 ETIME(I)=100000.
40 CONTINUE

```

C CCCCCCCCC

KKK = 0 INDICATES FIRST PHASE IN MISSION.
 IFLAG = 0 INDICATES REPAIR IS ALLOWED DURING PHASE.

DEFINE EVENT TIME VECTOR PREVIOUSLY INHIBITED, GENERATE TIR.

I. IF REPAIR WAS PREVIOUSLY INHIBITED, GENERATE TIR.

50 DO 120 ILB=1,NEQ
 KEQ=ILB

```

      IF(ETIME(KEQ)+100001,001)55,120,55
      IF(ETIME(KEQ)+99999,160,120
      IF((IFLAG(LL))120,70,120
      IF A NEGATIVE ETIME IS PASSED TO THE TTFF IS GENERATED SO A POSITIVE ETIME
      TO START REPAIR AT THE BEGINNING OF THE PHASE WE WANT
      MUST BE PASSED*
      ETIME(KEQ)=STP(HS
      IABC=IABS(IEQU(KEQ))
      XMTR(LLABC)180,80,100
      IF(XMTR(LLABC,LL)
      XXX=VMTTR(LLABC,LL)
      IF(XXX-999,120,90,120
      ETIME(KEQ)=-99999
      GO TO 120
      XXX=XMTR(LLABC)
      CALL TT
      CONTINUE
      120
      C
      III. TAG ALL EQUIPMENTS PREVIOUSLY FAILED OR OPERATING, NOT STANDBY.
      DO 140 ILB=1,NEQ
      KEQ=ILB
      IEQU(KEQ)=IABS(IEQU(KEQ))
      IF(ETIME(KEQ)-100001,130,140,130
      IEQU(KEQ)=IABS(IEQU(KEQ))
      130 CONTINUE
      140 CONTINUE
      150 CONTINUE
      C
      III. FOR EQUIPMENTS USED IN CURRENT PHASE CONFIGURATION
      A. THAT WERE USED IN PRIOR PHASE
      1. IF EQUIPMENT IS UP, LEAVE AS IS
      2. IF EQUIPMENT IS DOWN AND REPAIR IS ALLOWED, LEAVE AS IS
      3. IF EQUIPMENT IS DOWN AND REPAIR IS DISALLOWED, ADD
      CURRENT PHASE DURATION
      B. THAT WERE NOT USED IN PRIOR PHASE
      1. IF EQUIPMENT IS DOWN AND REPAIR IS ALLOWED, LEAVE AS IS
      2. IF EQUIPMENT IS DOWN AND REPAIR IS DISALLOWED, ADD
      CURRENT PHASE DURATION
      3. OTHERWISE, GENERATE TT
      CCCCCCCCCCCCCCCCCCCCC
      KKK2=KKK
      K=NLIN(LL)
      DO 250 I=1,K
      DO 250 J=1,8
      KEQ=IABS(I8(LL,1,J))
      IF((KEQ-MAXEQ)151,151,250
      151 IF(KEQ)250,250,155
      RUN 0490
      RUN 0500
      RUN 0510
      RUN 0520
      RUN 0530
      RUN 0540
      RUN 0550
      RUN 0560
      RUN 0570
      RUN 0580
      RUN 0590
      RUN 0600
      RUN 0610
      RUN 0620
      RUN 0630
      RUN 0640
      RUN 0650
      RUN 0660
      RUN 0670
      RUN 0680
      RUN 0690
      RUN 0700
      RUN 0710
      RUN 0720
      RUN 0730
      RUN 0740
      RUN 0750
      RUN 0760
      RUN 0770
      RUN 0780
      RUN 0790
      RUN 0800
      RUN 0810
      RUN 0820
      RUN 0830
      RUN 0840
      RUN 0850
      RUN 0860
      RUN 0870
      RUN 0880
      RUN 0890
      RUN 0900
      RUN 0910
      RUN 0920
      RUN 0930
      RUN 0940
      RUN 0950
      RUN 0960
      C

```

```

155 IF(ETIME(KEQ)+100001*EQU(KEQ)) 160,250,160
160 IEQU(KEQ)=IABS(IEQU(KEQ))
    IABC=IEQU(KEQ)
    IF((YMTTR(IABC,LL)-9999,1) 180,190,180
170 IF((CONTINUE(IABC,LL)-1) 170,170,180
180 IF((IFLAG(LL)-1) 210,190,210
190 IF((ETIME(KEQ)=ETIME(KEQ)-(ENDPHAS))
200 IF((ETIME(KEQ)-10000,1) 220,240,220
210 IF((ABS(ETIME(KEQ)-STPHAS)) 240,240,230
220 IF((STPHAS)=250,240,250
230 IF((TIME(KEQ)=EQU(KEQ))
240 IABC=IABS(IEQU(KEQ))
    XXX=XMTBF(IABC)
    CALL XTT
    CONTINUE
250 KK2=1
CCCCCCCC

```

IV. FOR EQUIPMENTS NOT IN CURRENT PHASE CONFIGURATION

A. IF EQUIPMENT IS UP, PUT IN STANDBY.

B. IF EQUIPMENT IS DOWN

1. IF REPAIR IS ALLOWED, LEAVE AS IS

2. IF REPAIR IS DISALLOWED, ADD DURATION OF CURRENT PHASE

```

      RUN 0970
      RUN 0980
      RUN 0990
      RUN 10000
      RUN 10100
      RUN 10200
      RUN 10300
      RUN 10400
      RUN 10500
      RUN 10600
      RUN 10700
      RUN 10800
      RUN 10900
      RUN 11000
      RUN 11100
      RUN 11200
      RUN 11300
      RUN 11400
      RUN 11500
      RUN 11600
      RUN 11700
      RUN 11800
      RUN 11900
      RUN 12000
      RUN 12100
      RUN 12200
      RUN 12300
      RUN 12400
      RUN 12500
      RUN 12600
      RUN 12700
      RUN 12800
      RUN 12900
      RUN 13000
      RUN 13100
      RUN 13200
      RUN 13300
      RUN 13400
      RUN 13500
      RUN 13600
      RUN 13700
      RUN 13800
      RUN 13900
      RUN 14000
      RUN 14100
      RUN 14200
      RUN 14300
      RUN 14400

```

V. SET STANDBY EQUIPMENTS ETIME TO 100000.

```

C CALL STATUS
C CALL STNDBY
C CALCULATIONS FOR INSTANT AVA AT START OF PHASE.
C IF (ISW(N))=350 IAUPL(350)=340
340 IAUPL(JBB)=IAUP1(JBB)+1
350 XIAUPI=XIAUPI/XKAA

C DNTI IS TOTAL SYSTEM DOWNTIME IN PHASE.
C DNTI=0.0
D0 360 KSS=1,N
360 SSTIME(LL,KSS,1)=0.0

C THE ACTUAL MISSION SIMULATION BEGINS HERE
C 370 TP=TIME
CALL STNDBY
380 IF (KS(6))=390 TP=40,390
390 WRITE(6,430)
DO 410 J=1,NEQ
IF (ETIME(J)-100000.) 400,410,400
400 IEQ=IABS(IEQU(J))
WRITE(6,420) J,IEQ,ETIME(J)
410 CONTINUE
420 FORMAT(1X,15,1X,15,5XF22.4)
430 FORMAT(1XF12.4)
440 CALL EVENT(TIME=ABSI(ETIME(KEQ)))
TIF(KS(5))=450,470,450
450 WRITE(6,460) KEQ,ETIME(KEQ),KAA
460 FORMAT(10X,5HEQUIP,15,F12.4,5X,KAA,MISSION,110)
470 DELT=TIME-TP
CALL STATUS

C SET TIME CLOCKS
C 480 DO 510 KSS=1,NX
481 IF (ISW(KSS))=490 KSS=500
490 SSTIME(LL,KSS,1)=STIME(LL,KSS,1)+DELT
500 GOSTO 510
510 SONTINUE
511 IF (ISW(N)) 520,530
520 SSTIME(LL,N,1)=STIME(LL,N,1)+DELT

```

```

T3=T3+DELT
IF((T3-ENDPHAI)>522,522,521
521 T3=T3-ENDPHAI-DELT
522 RDT=RDT+DELT
GO TO 550
530 T3=0.0
RDT=0.0
IF(SSTIME(LL,N,1)) 1140,550,540
540 SSTIME(LL,N,1)=0.0
550 CONTINUE
C SYSTEM FAILURE AND REPAIR TALLY
C IF(SSTIME(LL,N,1)) 570,560,570
560 IF(LL>620,580
570 IF(LL>610,620
580 IFF=IFF+1
590 IFR=IFR+1
600 TI=0.0
GO TO 620
610 TI=SSTIME(LL,N,1)
620 CONTINUE
C CHECK IF ANY DOWN TIMES HAVE EXCEEDED CRITERIA
C IF(ICRI) 640,640,660
C TAD2 - MISSION ALLOWABLE DOWNTIME
C 640 ISSC=1
ISSA(1)=N
IF(RDT-TAD2)>645,645,930
645 ICRI=0
IF(SSTIME(LL,N,1)-SSTIME(LL,N,2)) 650,650,960
650 ICRI=0
ISSC=0
DO 655 KSS=1,NX
IF(SSTIME(LL,KSS,1)-SSTIME(LL,KSS,2)) 655,655,652
652 ISSC=ISSC+1
ISSA(ISSC)=KSS
655 CONTINUE
IFISSC) 660,660,962
660 CONTINUE
C CHECK IF TIME GREATER THAN END OF PHASE
C IF ((TIME-ENDPHAI) 670,670,1140

```

```

C IFLAG = 0 INDICATES REPAIR IS ALLOWED DURING PHASE.
C REPOL IS THE PROBABILITY THAT A REPAIR IS PERFORMED.

C 670 IF (ISW(N)) 680,680,730
    680 CALL APPLE
    730 IF (ETIME(KEQ)) 810,810,740
    740 IF (ABC=IABS(IEQU(KEQ))-1) 750,760,750
    750 CALL IRANDOM(ISEED,RN)
    760 IF (RN-REPOL) 770,770,800
    760 ETIME(KEQ)=99999.
    GO TO 830
    770 IF (XMTTR(ABC)) 780,780,790
    780 XXX=XMTTR(ABC,L)
    780 IF (XXX=999) 820,760,820
    790 XXX=XMTTR(ABC)
    790 GO TO 820
    800 ETIME(KEQ)=-100001.001
    GO TO 830
    810 ABC=IABS(IEQU(KEQ))
    810 XXX=XMTBF(ABC)
    820 IF (IEQU(KEQ)) 811,821,821
    811 IEQU(KEQ)=IABS(IEQU(KEQ))
    811 ETIME(KEQ)=100000.
    GO TO 830
    821 CALL TTE
    830 IF (ETIME(KEQ)) 840,1150,870
C EVENT WAS FAILURE
C
    C 840 KEQU(KEQ)=KEQU(KEQ)+1
    C 850 DNT=DNT+DELT
    C 860 REDAD(JBB)=REDAD(JBB)+DELT
    C 870 GO TO 370
C EVENT WAS REPAIR
C
    C 870 CONTINUE
    C 880 IF (ISW(N)) 880,880,370
    C 890 IF (ICR1=890,900) 890
    C 900 TDOWN=TIME-SSTIME(LL,N,1)
    C 900 TTEMP=SSTIME(LL,N,1)
    C 900 IF (KS(13)) 370,370,910

```

```

910 WRITE(6,920) LL,TDOWN,TTEMP,KAA
920 FORMAT(13H DURING PHASE 16,20H SYSTEM WENT DOWN AT ,F14.4,13H DOWNR
1 TIME IS ,F14.4,3X7HMISSION,16)
GO TO 370

C ABORT PROCEDURE

C 930 ICRI=5
    TABORT=TIME-(RD T-TAD2)
    IF(TABORT-ENDP(HA)-1940,645,645
940 IF(XTABT(KAA)-100000.1,660,950,660
950 ITEMP=1
    ITEMP2=1
    WRITE(6,1010)LL,JBB,KAA,TABORT,TITLE(LL,N),TAD2
    GOTO 1020
960 ICRI=4
    GOTO 964
962 ICRI=2
    TABORT=TIME-(SSTIME(LL,ISSA(1),1)-SSTIME(LL,ISSA(1),2))
964 IF(TABORT-ENDP(HA)-990,980,980
970 IF(ICRI-2)-650,985,650
985 ICRI=0
    GOTO 660
990 IF(XTABT(KAA)-100000.1,660,1000,660
1000 ITEMP=1
    ITEMP2=1
    DO 1005 I=1,ISSC
    WRITE(6,1009)LL,JBB,KAA,TABORT,TITLE(LL,ISSA(1))
1005 WRITETIME(LL,ISSA(1),2)
1009 FORMAT(1X9HIN PHASE 12,1X3HSEQ,13,4X7HMISSION 16,4X15HABORTED AT
1 TIME F10.4,10H BECAUSE ,A4,35H EXCEEDED PHASE ALLOWABLE DOWNTIMERUN
2 2XF10.3,5H HRS.)
1010 FORMAT(1X9HIN PHASE 12,1X3HSEQ,13,4X7HMISSION 16,4X15HABORTED ATRUN
1 TIME F10.4,10H BECAUSE ,A4,37H EXCEEDED MISSION ALLOWABLE DOWNTRUN
2 TIME 2XF10.3,5H HRS.)
1020 XTABT(KAA)=TABORT
    IF(TABORT)=1590,1590,1040
1040 DO 1110 I=1,NEQ
    IF(ETIME(I)) 1050 1110 1110
1050 11F(LIEQU(I)) 1080 110 1080
1080 11F(KS(2)) 1090 110 1090
1090 WRITE(6,100) ETIME(I)
1100 FORMAT(17X9HEQUIPMENT,15,24H DOWN IT WILL COME UP AT ,F16.4)
1110 CONTINUE
1120 CALL APPL
    ITEMP2=0
1130 GO TO 660
C

```

```

C END OF PHASE PROCEDURE AT END OF PHASE
C TDEOP IS TIME DOWN AT END TIME IN MISSION.
C DNT2 IS TOTAL SYSTEM DOWNTIME IN MISSION. DUE TO ABORT
C AEND1 IS DOWNTIME IN MISSION DUE TO ABORT (UP TO CURRENT PHASE)
C AEND2 IS DOWNTIME IN MISSION DUE TO ABORT (UP TO CURRENT PHASE)
C REDAD1 IS ADJUSTMENT TIME FOR REDINESS CALCULATION IN PHASE
C REDAD2 IS ADJUSTMENT TIME FOR REDINESS CALCULATION IN MISSION
C

1140 CONTINUE
    IF (ISW(N)) 1160,1270
1150 CONTINUE
1160 TDEOP=ENDPDA-TP
1170 IF (KS(3)) 1210,1210,1180
1180 IF (TDEOP) 1190,1210,1190
1190 WRITE (6,1200) LLTDEOP,KAA
1200 FORMAT (IX27H SYSTEM DOWN AT END OF PHASE,16,13H FOR DURATION, F10.4
1       16X7HMISSION,16)
1210 CONTINUE
    DNT1=DNT1+TDEOP
    RDT=RDT+TDEOP-DELT
    DELT=TDEOP
    CALL APPL
1270 CONTINUE
    IF (ICR1) 1280,1290,1280
1280 REDAD1(JBB)=REDAD1(JBB)+TDEOP
1290 DNT2=DNT2+DNT1
1300 IF (DNT2) 1310,1330,1310
1310 IF (KS(6)) 1325,1325,1325
1325 WRITE (6,1320) LLKAA,DNT2
1320 FORMAT (IX5HPHASE,15,1X29HTOTAL SYS DOWNTIME IN MISSION,15,1X3HWA SRUN
1       1FL2:4'4H HRS)
1330 CONTINUE
C COMPUTE RELIABILITY FOR EACH PHASE *****
C JBB IS THE PHASE SEQUENCE NUMBER *****
C
1340 IF (ICR1) 1350,1350,1340
1350 XCUM=1-ITEMP
    INOABT(JBB)=INOABT(JBB)+1-ITEMP
    INMI(JBB)=INMI(JBB)+1
1360 CONTINUE
    XNO=INOABT(JBB)
    TNMI=INMI(JBB)
    IF (TNMI) 1380,1380,1370
1370 RELY=XNO/TNMI

```

```

GO TO 1390
1380 RELY=0.0
1390 RELPY=RELPY*RELV
      TT2=(JBB1)-ONT1
      UP1=TT1-(JBB1)=UP2(JBB)+TT1
      UP2(JSH(N))=1410,1410,1400
      IF IAUP2(JBB)=IAUP2(JBB)+1
      1400 IAUP2(JBB)=IAUP2(JBB)
      XAV=XIAUPP/XKAA
      IF XKAA-I NUMI 1570,1420,1570
      1420 WRITE(6,1430) XAV1
      1430 FORMAT(6,1420)HINSTANT AVAILABILITY,5X2X4H IS ,F6.4)
      1440 WRITE(6,1450)LLJBB RELPY
      1450 FORMAT(9X17HRELIABILITY PHASE I3,1H,13,5H,1S ,F6.4,3X25HRELIABIRUN
      1LLITY UP TU PHASE ,12,4H IS ,F6.4)
      RELGA(JBB)=RELPY
      AENDT1=0.0
      DO 1520 I=1,KAA
      1460 IF (XTABT(I)-100000,1 1470,1520,1520
      1470 IF (XTABT(I)-TIMA(JBB)) 1480,1520,1520
      1480 AENDT2=AENDT2+TIMA(JBB)-XTABT(I)
      JBB1=JBB-1
      1490 IF (TIMA(JBB1)-XTABT(I)) 1500,1500,1510
      1500 AENDT1=AENDT1+TIMA(JBB)-XTABT(I)
      GO TO 1520
      1510 AENDT1=AENDT1+TIMA(JBB1)-TIMA(JBB1)
      1520 CONTINUE
      TT3=TT3+TT2(JBB)
      UP3=UP3+UP2(JBB)
      REDAD2=REDAD2+REDAD1(JBB)
      RED1=(UP2(JBB)-AENDT1+REDAD1(JBB))/TT2(JBB)
      RED2=(UP3-AENDT2+REDAD2)/TT3
      1530 WRITE(6,1540)RED1,RED2
      1540 FORMAT(9X16HREADINESS ,9X4H IS ,F6.4,3X25HREADINESS
      ,AVAI=UP2(JBB)/TT2(JBB)
      AVA2=UP3/TT3
      1550 WRITE(6,1550) AVAI,AVA2
      1AFORMAT(9X23HAVERAGE AVAILABILITY ,2X4H IS ,F6.4)
      1AWRITE(6,1560) XAV
      1560 FORMAT(14,20HINSTANT AVAILABILITY,5X2X4H IS ,F6.4)
      1570 CONTINUE
      1580 KKK=1

```

JBB=JBB+1
T1=SSTIME(LL,N,1)
1590 RETURN
END

RUN 4330
RUN 4340
RUN 4350
RUN 4360

```

SUBROUTINE PACK
COMMON /ALPHA/DNT2,ENDOPHA,ICRI,IFF,IFR,INUM,ICP,JBBB,KEQ,KZZ
COMMON /KS1/LL,LLAST,NEQ,NPH,NTYPE,NUM,REDAD2,REFAD1,1001,RELPC,T3,TIME,.3SUM
COMMON /RELPY,REPOL,STP,TP,T1,XCUM,T3,UP3,IFFECP,T3,TIME,.3SUM
COMMON /EXTRA/ KS(20),LSW(31)
COMMON /NIEQU/(500) IEEQU(500) ETIME(1000) XMIBF(200) XMTIR(200)
COMMON /NPX/ NSS(6) IFLAG(6) ITLE(6,31) SSTIME(6,31) ISS(6,31)
COMMON /TYP/ EX(200) ISPAR(3,200) IUSED(3,200) IUSED(3,200)
COMMON /MAX/MAXNEQ,MAXTYP,MAXIB,MAXSTD
COMMON /VDC/VDC(50,6),IUI(200),VMTR(200,6),TAD2
COMMON /PACKAP/IBNUM(6,500),ISYS(6,1),F(200,4)
COMMON /STAN/ISTB(60,10,6)
COMMON /CSPARE/SPR1,SPR2,SPR3,SPR4,SPR5,SPR6,SPR7,SPR8,SPR9
1 SPRI1,SPR12,SPR13,SPR14,ITMPUP(200)
DIMENSION LOAD(19)
DIMENSION DUM(4)
DIMENSION IVAL(10)
DATA 1BLANK/4H /
CCCCCCCC
KOPT OBTAINS ONE OF SUNDRY COMBINATIONS OF SWITCHES
KOPT=1 GIVES MANAGEMENT SUMMARY PRINTOUT
KOPT=2 GIVES ENGINEERING SUMMARY PRINTOUT
KOPT=3 GIVES COMPLETE DETAIL PRINTOUT
KOPT=4 INPUTS SUPRESSED ON OUTPUT PRINTOUT
KOPT=5 DESIGN YOUR OWN OUTPUT PRINTOUT
READ (5,10) KOPIT,(KS(I)),I=1,13
WRITE (6,20) KOPIT,(KS(I)),I=1,13
10 FORMAT (20I4)
20 FORMAT (1H1,10,5X19I4)

CC IFLAG = 0 INDICATES REPAIR IS ALLOWED DURING PHASE.
CC
READ (5,10) (IFLAG(I),I=1,NPH)
WRITE (6,30) (IFLAG(I),I=1,NPH)
30 FORMAT (10I4)

CC REPOL IS THE PROBABILITY THAT A REPAIR IS PERFORMED.
CC
READ (5,40) REPOL,XM,XM1
40 FORMAT (F4.0,F8.0,2F4.0)
50 FORMAT (20F4.0)
1F(XM) 35,35,55
25 XM=1.0
35 1F(XM1) 36,36,56
36 WRITE(6,60) REPOL,TAD2,XM,XM1

```

AD-A093 584

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
AN EVALUATION OF THE EFFECT OF SPARES ALLOWANCE POLICY UPON SHI--ETC(U)
SEP 80 J E LEATHER

F/G 15/5

UNCLASSIFIED

2 or 2
40
403684

NL

END
DATE
FILED
2 81
DTIC

```
60 FORMAT(1X,'4F10.2')
GO TO (70,90,100,120,130),KOPT
C KS SWITCHES ARE ON WHEN SET=1
C C
```

```

C FILL EQUIPMENT AND TYPE TABLES
C
130 NEG=0          140 I=1 MAXNEQ
DO 140 I=1 MAXNEQ
      ETIME(I)=0
      EQUIV(I)=0
      CONTINUE
140 DO 150 I=1,6
      DO 150 J=1,MAXTYP

```

```

XMTBF(I,J)=0.0
YMTTR(I,J)=0.0
150 XMTTR(I,J)=0.0
155 CONTINUE

```

C READ TYPE CARDS

```

C 160 WRITE (6,170)
170 FORMAT (11H TYPE NAME,18X4HMTBF,5X4HMTTR,7X2HDC,8X4HADT1,4X4HADT2)

```

```

180 READ (5,190) I, (DUM(J), J=1,4), X, Y, U, V, W, IDUM
190 FORMAT (I14,4A4,F8.0,4F4.0,[4])
1F(1,1) 200,490,200
200 IF(I=MAXTYPE) 220,220,210
210 WRITE (6,440)
220 GO TO 1000
220 DO 230 J=1,4
230 F(I,I,J)=DUM(J)
240 IF(I=5) 150,1 TU, (VDC(IU,ILL), ILL=1, NPH)
240 READ(Y,150,1 TU, (VDC(IU,ILL), ILL=1, NPH)
2250 IF(I=5) 250,1 TU, (VDC(IU,ILL), ILL=1, NPH)
2260 IF(I=1) 280,490,280
270 EX(1,1)=V
280 EX(2,1)=W
290 IF(IKS(1,1)=310,310,290)
310 IF(IKS(1,1)=300,300,320)
320 IF(IKS(1,1)=340,340,330)
330 IF(IKS(1,1)=460,460,310)
340 DO 370 ILL=1,NPH
350 VDC(IU,ILL)=(X,VDC(IU,ILL)) * XH
360 GO TO 370
370 VDC(IU,ILL)=(X/.0001)*XH
380 CONTINUE
380 IF(IKS(1,1)=410,410,390)
390 IF(IKS(1,1)=470,470,400)
400 IF(XM(1,1)=420,430,420)
410 IF(1,1)=420,430,420
420 WRITE (6,440)
430 IF(U,435,435,633)
433 XMTBF(I,J)=X*(X,U)
435 XMTTR(I,J)=Y*XH
GO TO 180

```

```

440 FORMAT (9X39H EQUIP TYPES HAVE EXCEEDED MAX ALLOWABLE)
450 FORMAT (14X16H VARIABLE DUTY CYCLE '4F10.3')
460 FORMAT (14X16H VARIABLE MITR '4F10.3')
470 FORMAT (1X4H TYPE,15,1X13H DEFINED TWICE)
480 FORMAT (1X4H TYPE,15,1X13H DEFINED TWICE)

C AFTER LAST TYPE CARD MUST BE A BLANK CARD, THEN FOLLOWS EQU CARDS.

C   490 WRITE (6,500)
500 FORMAT (1/1X15H TYPE EQUIPMENT)
510 READ (5,10) NTYPE (LOAD(1),I=1,19)
520 DO 10 LOAD(1)=1,19
530 10 IF (LOAD(1)=1) 520, 650, 520
540 WRITE (15,550)
550 FORMAT (55H EQUIPMENT NUMBER GREATER THAN 500 ****)
560 GO TO 100
560 1F (IBH-NEQ) 580, 580, 570
570 NEQ=IBH
580 IF (1EQU(1BHI)) 590, 610, 590
590 WRITE (16,600) 1BH
600 FORMAT (1X9HEQUIPMENT,15,1X34HDEFINED TWICE ****)
610 CONTINUE (IBHI)=NTYPE
620 CONTINUE (IBHI)=NTYPE
630 WRITE (6,10) NTYPE, (LOAD(1),I=1,19)
640 NTYPE=TYPE
650 GO TO 510

C ALL EQUIPMENT & TYPE CARDS HAVE BEEN READ IN.
C THE LAST CARD AT THIS POINT MUST BE A BLANK CARD.

C   650 WRITE (6,660)
660 FORMAT (1/1X1HSPARES TYPE,6X4HSHIP,4X6HTENDER,6X4HBASE,12X6HFACTOR)
670 DO 670 J=1,3
       NTYPE=NTYPE
670 1 USED(J)=J=0
      READ (5,675) IUNLIMSSX,SPR1,SPR2,SPR3,SPR4,SPR5,SPR6,SPR7,SPR8,SPR9
      1 SPR10,SPR11,SPR12,SPR13,SPR14
675 FORMAT (A4-,16X15F4.0)
676 IF (SSX-999=1) 681, 676, 681
676 CALL (SPR11) 740, 740, 677

```

PACK 1930
PACK 1940
PACK 1950
PACK 1960
PACK 1970
PACK 1980
PACK 1990
PACK 2000
PACK 2010
PACK 2020
PACK 2030
PACK 2040
PACK 2050
PACK 2060
PACK 2070
PACK 2080
PACK 2090
PACK 2100
PACK 2110
PACK 2120
PACK 2130
PACK 2140
PACK 2150
PACK 2160
PACK 2170
PACK 2180
PACK 2190
PACK 2200
PACK 2210
PACK 2220
PACK 2230
PACK 2240
PACK 2250
PACK 2260
PACK 2270
PACK 2280
PACK 2290
PACK 2300
PACK 2310
PACK 2320
PACK 2330
PACK 2340
PACK 2350
PACK 2360
PACK 2370
PACK 2380
PACK 2390
PACK 2400

677 DO 678 I=1,NTYPE
678 WRITE(6,750) I,(ISPARE(J,I),J=1,3),SX
681 GO TO 740
682 LSF(SX) 684, 682, 684
684 UNL IM-1 BLANK 690,720,690
690 FORMAT(6,700)
700 FORMAT(14X4) HALL EQUIPMENT TYPES HAVE UNLIMITED SPARES!
DO 710 I=1,NTYPE
710 ISPARE(J,I)=90000
720 GO TO 760
720 READ(5,10) (ISPARE(J,J),J=1,3)
BILL=FLOAT(ISPARE(1,1)*SX
14 ISPARE(1,1)=BILL
725 GO TO 728
727 ISPARE(1,1)=INT(BILL)+1
728 CONTINUE
14 IF(KS(1,1)=740,740,730)
730 WRITE(6,750) I,(ISPARE(J,I),J=1,3),SX
740 CONTINUE
750 FORMAT(5X,14,2X,3I10,13X,F6.2)
C 760 WRITE(6,770) NPH
770 FORMAT(1H1,3X28) THE MISSION WILL BE RUN WITH,14,7H PHASE ,27H TYPE PAU
15 IN VARIABLE SEQUENCE.
C PHASE CARDS APPEAR NEXT.
DO 777 I=1,6
DO 776 J=1,10
14 STBLK,K,I=0
775 CONTINUE
776 CONTINUE
DO 790 K=1,NPH
READ(5,780) XIDS(L,NSS(K),ISS(K,NSS(K)+1),SSTIME(K,NSS(K)+1,2))
14 SYS(K)=ISS(K,NSS(K)+1)
780 FORMAT(1A4,3I4,F8.0)
NX=NX+1
14 IF(KS(1,1)=820,820,790)
790 WRITE(6,810) XIDL,NSS(K),ISS(K,N),SSTIME(K,N,2)
800 FORMAT(1XA4,3I4,F10.2)
810 FORMAT(1/1XA4,3I4,F10.2)

```

820 TITLE(K,N)=X1
DO 840 IK=1,NK
READ(5,1780) TITLE(K,IK),KK,MM,ISS(K,IK),SSTIME(K,IK,2)
IF(KS(1)=840)TITLE(830,K,IK),LL,MM,ISS(K,IK),SSTIME(K,IK,2)
830 WRITE(6,800)TITLE(830,K,IK),LL,MM,ISS(K,IK),SSTIME(K,IK,2)
840 CONTINUE

C EQUIPMENT & GROUP CONFIGURATION MATRIX
C
DO 850 JA=1,MAX16
DO 850 JB=1,8
IB(K,JA,JB)=0
NRO(K,JA,J)=0
850 CONTINUE
C=0
I=0
860 READ(5,101) IVAL(JJ),J=1,10,1
IF(IVAL(1)=0)GO TO 990
C** GROUP CARD. CHECK IF MORE THAN ALLOWED.
IF(I=1)THEN
  MAXIB GO TO 880
  WRITE(6,1870) MAXIB
FORMAT(1H1,10X,29H# OF GROUP CARDS GREATER THAN, I4)
  STOP
END IF
880 NRO(K,I)=IVAL(1)
DO 890 J=1,8
IB(K,I,J)=IVAL(J+1)
890 CONTINUE
IENUM(K,I)=IB(K,I,1)-5001=1
NLINEN(K,I)=1
IF(KS(1)=860)860,860,910,(IB(K,I,J),J=1,8)
900 WRITE(6,1920)NRO(K,I),IB(K,I,J),J=1,8
910 FORMAT(1X,13,8)14
920 FORMAT(1X,13,8)16
930 CONTINUE
I=I-1
IF(I=0)THEN
  C** OPERATE RULE CARD. CHECK IF MORE THAN ALLOWED.
  IF(I=0)MAXSTD GO TO 950
  WRITE(6,1940)MAXSTD
  FORMAT(1H1,10X,36H# OF OPERATE RULE CARDS GREATER THAN, I4)
  STOP
END IF
950 CONTINUE
DO 960 J=1,10
LISTB(IOR,J,K)=IVAL(J)
960 CONTINUE
IF(KS(1)=860,860,970

```

PACK28900
PACK29000
PACK29100
PACK29200
PACK29300
PACK29400
PACK29500

970 WRITE(6,980),10{1\$TE(IOR,J,K),J=1,10}
980 FORMAT(1\$0X,10{1\$TE(IOR,J,K),J=1,10})
980 GO TO 860
990 CONTINUE
1000 RETURN
END

```

SUBROUTINE EVENT /ALPHA/DNT2,ENDOPHA,ICR1,IFF,IIFR,INUM,IOPT,JBB,KEQ,KZZ
COMMON /ALPH/LLLAST,NEQ,NPH,NTYPE,PNUM,REDAD1(100),RELPP,RED2
1,KK1,KS1,LLLAST,NEQ,NPH,NTYPE,PNUM,REDAD2(RED2)
2,RELPP,REPO,STPHAS,TPT,XCUM,TT34UP34FF,EOP,T3TIME,T3SUM
COMMON /N/IEQU(500),KEQU(500),ETIME(1000),XHTBF(200),XHTTR(200)

C DETERMINES SMALLEST VALUE IN ETIME VECTOR

R=ABS(ETIME(1))
KEQ=1
DO 20 I=2,NEQ
RR=ABS(ETIME(I))
1F IR-RR) 20,2D,10
10 R=RR
KEQ=I
20 CONTINUE
END

```

```

SUBROUTINE TTE
COMMON /ALPHA/DNT2,ENDPHA,ICR1,IFF,FRINUM,IOPTR,BB,KEQ,KZZ
1  KKI,KS,ILL,LASt,NEQ,NPH,NTYPE,PNUM,FRDAD2,REDA01(100),REL01
2  RELPY,REP0LST,PHAS,TPT,XCYM,ETIME,UP3,IFFECP,T3TIME,3SUN
COMMON /N/IEQU(500),KEQU(500),ETIME(1000),XNTBF(200),XNTTR(200)
COMMON /EXTRA/KS(20),IESSW(31)
COMMON /NPH/NSS(6),IFLAG(6),TITLE(6),STIME(6),ISS(6,31)
COMMON /TYP/EX(2,200),ISPAR(3,200),IUSED(3,200),IUSED(3,200)
COMMON /DELTA/KK2
COMMON /XX/VDC/VOC(50,6),IUI(200),VMTIR(200,6),TAD2
COMMON /GAMMA/XMTBA,YAR,RELGA(100),TIMA(100),XXT(200),ITI,ISEED

C      10 K=KEQ
      20 J=IABS(IEQU(K))-100000,30,120,30
      30 IF (ETIME(K),120,120,40
C      CHECK IF ANY SPARES REMAIN

      IF INFINITE REPAIR TIME, NO SPARE IS USED
      40 IF (ABS(XXX)-9999,.) 41,120,41
      41 DO 60 I=1,2
      42 IF (ISPAR(I,J)-IUSED(I,J)) 60,60,50
      50 IUSED(I,J)=IUSED(I,J)+1
      51 IUSED(I,J)=IUSED(I,J)+1
      52 I=10,120
      60 CONTINUE
      61 IF (ISPAR(3,J)-IUSED(3,J)) 60,70,70,110
      62 IF (ETIME(K)-100000,) 80,120,80
      80 ETIME(K)=-500000
      81 IF (KS(12),1340,340,90
      90 WRITE(6,100)
      100 FORMAT(1X15HEQUIPMENT TYPE ,14,25H HAS CONSUMED ALL SPARES.)
      110 GOTO 340
      111 IUSED(3,J)=IUSED(3,J)+1
      112 I=3
C      GENERATE TIME-TO-EVENT
      120 XXX=ABS(XXX)
C      KKK = 0 INDICATES FIRST PHASE IN MISSION.

```

```

130 IF (KKK2) 140,130,140
140 I=0 ETIME(K)-Tp 160,150,160
150 ETIME(K)=Tp
160 GO TO 170
160 IF (ETIME(K)) 170,170,180
170 GO TO 190
180 X=-1
190 CALL RANDOM(ISEED,RN,1)
200 ADT=0.
200 GO TO 220
210 I=I-1
210 AUT=EX(LII,J)
220 CONTINUE
220 IF (ETIME(K)) 230,230,330
230 K1=IABS(IEQU(K))
230 IF (IUI(K1)) 330,330,240
240 IU=IUI(K1)
240 ST=0.0
SR=1.0
RN3=RN
DO 310 I=JBB,100
310 XT=XT/2*I
IF (ST) 250,320,250
250 T=TIME(I)+ETIME(K)
260 IF (T) 270,310,300
270 T=0
GO TO 310
300 LLL=XXT(IU(LL)
XH=VDC(IU(LL)
IF (XH) 280,320,280
280 R=EXP(-T/XH)
SR=SR*R
SF=(SR-RN) 320,320,290
290 ST=ST+T
RN3=RN/SR
310 CONTINUE
320 ETIME(K)=ST-(XH*ALOG(RN3))+ABS(ETIME(K))+ADT
320 GO TO 340
330 ETIME(K)=X*(-XXX*ALOG(RN))+ABS(ETIME(K))+ADT
340 IF (FLAG(LL)-1) 370,350
350 IF (ETIME(K)+500.00.) 360,370,360
360 ETIME(K)=100000.
370 CONTINUE

```

**RETURN
END**

**TTE 0978
TTE 0988**

```

SUBROUTINE EVENT
COMMON /ALPHA/ DNT2,ENDPHA,I CRI,IFF,IFR,INUM,I OPT,JBB,KEQ,KZZ
1,KK1,K51,L1LLLAST,NEQ,NPH,NTYPE,NUM,REDAD1(100),REL,P,RED2
2,REL,P,Y,REPOL,STPHAS,TPI,T1,XCUM,TTUP31FFEOP,T3TIME,T3SUM
COMMON /N/NEQ(500),KEQU(500),ETIME(1000),XMT&F(200),XMTTR(200)

C DETERMINES SMALLEST VALUE IN ETIME VECTOR
C
R=ABS(ETIME(1))
KEQ=1
DO 20 I=2,NEQ
RR=ABS(ETIME(I))
IF (RR-RR) 20,20,10
10 R=RR
20 CONTINUE
END

```

```

SUBROUTINE STNDBY ALPHADNT2,ENDPAH,I CRI,IFF,IFR,I NUM,I OPT,JBB,KEQ,KZZ
COMMON /ALPHADNT2,NEQ,NPH,NTYPE,I NUM,REDAD1(100),REL1(100),RED2
      KK1,KSL,LL,LL,LL,AS3,TPI,TI,XCM,TT3,UP3,IFF,ECP,T3SUW
      2'RELPY,REP0,LST,PHAS,TP1(500),KEQU(500),ETIME(1000),XMTBF(200)
COMMON /N/IEQU(500),ETIME(1000),XMTBF(200),STND0050
COMMON /XXX/XXX,XXX
COMMON /STAN/ISTB(60,10,6)
DO 170 I=1,50
   IF (ISTB(I,1,LL)) 10 180 10
10 INDEX=1 INDICATES ALL EQUIPMENTS IN STRING ARE UP.
   DC 50 STB(I,J,LL)
   KK=1
20 IF (ETIME(KK)) 30 60 20
   C INDEX=0 INDICATES AT LEAST ONE OF THE EQUIPMENTS IN THE STRING IS DOWN
30 KK=1ABS(KK)
   IF (ETIME(KK)) 40,40,50
40 INDEX=0
   50 GOTO 60
   C K IS THE EQUIPMENT NUMBER WHICH WILL BE PUT UP OR STANDBY.
   C 60 K=1ABS(ISTB(I,LL))
   C 150 PLUS QR MINUS INDICATES STRING OR STANDBY LOGIC.
   C IF EQUIPMENT DOWN (ETIME MINUS) LEAVE ALONE.
   C 70 IF (ETIME(K)-100,0,0) 120,90,120
   80 IF (ETIME(K)-100,0,0) 170,170,80
   90 IF (INDEX) 170,110,100
   100 IF (ISO) 170,170,150
   110 IF (INDEX) 150,170,170
   120 IF (ISO) 170,170,140,130
   130 IF (ISO) 160,170,170
   140 IF (ISO) 170,170,160
   C CALL TTE TO PUT ON EQUIPMENT THAT WAS OFF(STANDBY).
   C 150 IABC=1ABS(IEQU(K))
   KEQ=K
   XXX=XMTBF(IABC)
   CALL TTE
   GO TO 170
   C TO PUT OFF(STANDBY) EQUIPMENT THAT WAS ON.
   160 ETIME(K)=100000.
   170 CONTINUE
   180 RETURN
END

```

```

SUBROUTINE STATUS
COMMON /ALPHA/DNT2,ENDP,ICR,IFF,IFR,INUM,IOPT,JBB,KEQ,KZZ
1,KK1,K$1,LL1,LL2,NEQ,NPH,NTYPE1,NUM,REDAD2,REDAD3,T1,T2,T3,T4,T5,T6
2,REL,PY,REPOL,STPHA$1,NTP,T1,XCUM,T3,UP3,IFFEOP,T3,TIME,T3,SUM
CCMHON/BETRA/NRO(630),IB(1630,8),NLIN(6)
COMMON/EXTRA/KSS(20),ISW(31)
COMMON/NSEQUS(500),KEQU(500),ETIME(1000),XMTBF(200),XMTTR(200),
COMMON/NPH/NSS(6),IFLAG(6),TITLE(6,31),SSTIME(6,31,2),ISS(6,31)

C KID=0
NL1=NLIN(LL)
10 DO 130 K=1,NL1
12 KT=IB(LL,K)
14 IF(KID-KT)16,18,16
16 ISUM=0

C NRO IS NUMBER OF EQUIPMENTS REQUIRED UP
C 18 IF(NRO(LL,K))130,130,20
20 DO 60 J=2,8
30 IF(KK)70,70,40
40 IF(ETIME(KK))60,60,50
50 ISUM=ISUM+1
60 CONTINUE
70 IF(ISUM-NRO(LL,K)) 80,90,90
80 ETIME(KT)=-1.
90 GETIME(100)
100 IF(KS(12)=125125110
110 WRITE(6,120)KT,ETIME(KT)
120 FCRMAT(IX3HKK=15,7H ETIME=.F10.5)
125 KID=KT
130 CONTINUE
N= NSS(LL)+1
DO 160 I=1,N
J=1SS(LL,I)
IF(J=ETIME(I)) 140,140,150
140 ISW(I)=-
150 GO TO 160
150 ISW(I)=1
160 CONTINUE
KZZ=0
RETURN
END

```

```

SUBROUTINE APPLE ICHLD(50) MKBA(100)
DIMENSION IPR(50),ICR(50),IFR(50),INUM(100),
COMMON /ALPHAD/NT2,ENDPHA,ICR,IIFP,IFR,INUM,IREDADE,
J,KK,KS,LL,LLA,ST,NEQ,NPH,NTY,PE,T3,TIME,T3UH,
2,RELPLY,REPOL,STOP,XTCP,T1,XCUM,T3,U3,IFFEOP,T3,TIME,T3UH,RED2
COMMON /BETA/NRD(600),IB(600),IEQU(500),IET(600),LINE(6)
COMMON /N/IEQU(500),IEQU(500),IET(600),LINE(6)
COMMON /TIGAP/UP4,XNUM,BAPRIN,AVA,XPCAP,RUNID(19),TYCOON(500)
+COUNTB(500),XTCP
COMMON /RUNAP/ITEMP2,DELT,ISSA(31),ISSC
COMMON /NPH/NS(6),IFLAG(6),TITLE(6),SSTIME(6,31),ISS(6,31)
COMMON /PACKAP/IBNUM(6,500),ISYS(6,500),F(200,4)
COMMON /PACKAP/IBNUM(6,500),ISYS(6,500),F(200,4)

C IF(BAPR).NE.1790,90,90
90 JCOUNT=0
C**** INITIALIZE NUM PRIORITY FAIL=0, SET PHASE,SET TREE PARENT TO
C 100 PTR=0
L=LL
IF(ITEMP2).GT.40,105,107
105 K=IBNUM(L,ISYS(L)-500)
GOTO 108
107 KSS=ISSA(ISSC)
K=IBNUM(L,ISSC(L,K,1))
108 KID1=IB(L,K,1)
110 NN=2
C**** LOOK AT CHILDREN OF PARENT
C 120 DO 210 N=NN,B
IFRP=IB(L,K,NI)
IF(IFRP).GT.40,212,140
140 IF(ITEME(IFRP).LT.150,150,210
150 IF(IFRP-500).LT.170,160,210
C *** HAVE WE SEEN THIS EQ. BEFORE
C 170 IF(JCOUNT).GT.240,200,180
180 DO 190 I=1,JCOUNT
IF(MKBA(I)-IFRP).LT.190,210,190
190 CONTINUE
200 CONTINUE
C *** ADD TO LIST OF FAILED PRIORITY EQ.
C JCOUNT=JCOUNT+1
MKBA(JCOUNT)=IFRP
210 CONTINUE
212 IF((K-1).GT.220,220,214
214 KID2=IB(L,K-1)
IF(KIDI-KID2).GT.220,216,220
216 K=K-1

```

```

GOTO 108
220 IF ((IPTR) > 40260, 230
C***# GO BACK TO LAST PARENT
230 K=IPRNT(IPTR)
KID1=IB(L,K1)
NNZICHLD(IPTR)
IPTR=IPTR-1
GOTO 120
C***# LOOK AT CHILDREN OF FAILED CHILD
160 IF (N-8) 165 167 240
C ***# PUT PARENT INTO STACK AND MAKE CHILD NEXT PARENT
165 IPTR=IPTR+1
IPRN((IPTR))=K
ICHLDOUM(L,IGRP-500)
167 K=IBNUML(L,IGRP-500)
GOTO 108
240 WRITE(6,250)
250 FORMAT(12H APPLE ERROR)
GOTO 300
C***#BOOKKEEPING
260 IF (ITEMP2) 240, 265, 262
262 ISSC=ISSC-1
IF (ISSC) 240, 265, 100
265 FCOUNT(JCOUNT)
IF (ITEMP2) 270, 270, 280
C ***# SUMMING COUNT TIME BY EQ
C 270 DO 275 I=1, JCOUNT
C 275 TYCOON(MKBA(I))=TYCOON(MKBA(I))+DELT/FCOUNT
C 280 DO 290 I=1, JCOUNT
C 290 COUNTB(MKBA(I))=COUNTB(MKBA(I))+1/FCOUNT
C 300 CONTINUE
C RETURN
C BEGINNING OF FINAL PRINTOUT
C 790 CONTINUE
WRITE(6,800) (RUNID(I), I=1,19)
800 FORMAT(1H13X,19A4/)
810 WRITE(6,810)
FORMAT(32X19HCritical Equipments/32X,18HUnavailability AND/
1X25HPERCENT OF Unavailability/)
1WRITE(6,820)
FORMAT(26X4HNAME,17X7HNUM HRS,11X5HUNAV,2X7HPERCENT,6X8HEQU TYPEAPPL0920
1,5X7HEQU NUM/)
820 FORMAT(26X4HNAME,17X7HNUM HRS,11X5HUNAV,2X7HPERCENT,6X8HEQU TYPEAPPL0930
APPL0940
APPL0950
APPL0960
C SKIPS BAD APPLE PRINTOUT WHEN AVA OR REL = 1.0

```

```

C IF (AVA-1) 830,880,830
 830 INDEX=1
     DO 850 I=2,NEQ
     TRR=TYCOON(1)
     IF (TR-TRR) 840,850,850
 840 TR=TRR
 850 CONTINUE
     TYCUM=TYCOON(INDEX)/TT3
     TYCUM2=TYCOON(INDEX)/(TT3-UP4)*100.
 860 IXX=IABS(IEQ((INDEX))
     WRITE(6,870) (F(IXX,J),J=1,4),TYCOON(INDEX),TYCUM,TYCUM2,IXX
 870 FORMAT(120X4A4,F20.4,4XF8.4,F8.2,8X14,1)
     GO TO 830
 880 WRITE(6,890) (RUNID(I),I=1,19)
 910 FORMAT(32X,19HCRITICAL EQUIPMENT//32X,17HNRELIABILITY AND/
     127PERCENT OF MISSION FAILURES//)
     WRITE(6,920)
 920 FORMAT(12X,11HDESCRIPTION,8X3HNO. 6X6HUNREL ,3X7HPERCENT,2X13HEQUIP
     1P EQUIP/28X8HFAILURES,22X10HTYPE NO.)
     IF (XPCAP-1.) 930,1090,930
C****THROW OUT EQUIPMENT WITH ZERO FAILURES
C 930 INEWA=0
     DO 950 I=1,NEQ
     IF (COUNTB(I)) 950,950,940
 940 INEWA=INEWA+1
     MKBA(INEWA)=I
 950 CONTINUE
C****RANK LIST BY NO. FAILURES
C 955 TOTAL=XNUM-XTCUM
     IF (INEWA-1) 1010,975,952
 952 INDEX=HKBA(1)
     NN=L
     TR=COUNTB(INDEX)
     DO 970 I=2,INEWA
     IF (TR-COUNTB(MKBA(I))) 960,970,970
 960 INDEX=MKBA(I)
     NN=I

```

```

TR=COUNTB( INDEX )
970  CONTINUE
971  CONREL=TR/XNUM
      PERC=TR/TOTAL*100
      IND=1ABS(IEQU(IND-EX))
      WRITE(901,14) TR,UNREL,PERC,IND,INDEX
      FORMAT(9X4A4,3XF6.1,5XF6.4,3Xi4)
      MKBA(NV)=MKBA(INEWA)
      INEWA=INEWA-1
      GOTO 955
975  INDEX=MKBA(1)
      TR=COUNTB( INDEX )
      GOTO 977
977  JNUMH=IFIX(XNUM)
1010  WRITE(6,1020) JNUM
1020  FORMAT(6,9X19H TOTAL NO. MISSIONS=,I4)
      TOTAL=TOTAL
      WRITE(6,1030) TOTAL
1030  FORMAT(9X27H TOTAL NO. MISSION FAILURES=,I4)
1090  RETURN
END

```

SUBROUTINE SPARES

```

      FLSIP COSAL MODEL WITH INSURANCE CUT POINT READ IN WITH DATA
      COMMON /ALPHA/DNT1F,ENDP,HA,JCR,IFFF,IFR,INUM,IOP,IJOB,KEQ,KEQ,KZZ
      1,KX1,KSL,LLAS,T,NEQ,NPH,NTYPE,I,REDAD,I,RED2
      2,RELPY,REPOL,STPHAS,T,P,Q,T1,XCUM,T3,UP3,IFFE,OP,IT3,SUN
      COMMON /N/IEQU(500),KEQU(500),ETIME(100),XMTBF(200),XMTTR(200)
      COMMON /TYP/EX(2,200),ISPACE(3,200),IUSED(3,200)
      COMMON /CSPAR/SPR1,SPR2,SPR3,SPR4,SPR5,SPR6,SPR7,SPR8,SPR9
      1,SPR10,SPR11,SPR12,SPR13,SPR14,ITMPDP(200)
      1,SPUT=SPR1,1,OPT=1,1,NTYPE
      1,ITMPDP(1)=0
      10 CONTINUE
      1ITMPDP(IEQU(1))=ITMPDP(IEQU(1))+1
      20 CONTINUE
      2DO90 I=1,NTYPE
      EX9000=(18766./XMTBF(1))/4.)*ITMPDP(1)
      IF(EX9000-1.)60,30,30
      30 DEMAND BASED ITEM
      30 PRBSUM=EXP(1-EX9000)
      DUM=PRBSUM
      KFACT=1
      K=0
      40 K=K+1
      KFACT=KFACT**K
      PRBSUM=PRBSUM+DUM*(EX9000**K)/KFACT
      50 ISPACE(1,1)=K
      GO TO 90
      60 IF(4.*EX9000-CUT) 80,80,70
      70 INSURANCE ITEM
      70 ISPACE(1,1)=1
      80 ISPACE(1,1)=0
      90 CONTINUE
      100 DO100 J=1,3
      100 ISPACE(1,J,1)=0
      100 CONTINUE
      END
      100 RETURN

```

LIST OF REFERENCES

1. Naval Sea Systems Command Report TE660-AA-MMD-010, Tiger Manual, January 1980.
2. Chief of Naval Operations Instruction 4441.12A, Supply Support of the Operating Forces, 9 August 1973.
3. Center for Naval Analysis Memorandum (CNA)80-0881, Third Advisory Committee Briefing on Shipboard Parts Allowance Policy Study, by Cdr. J. Bagby, 19 June 1980.
4. Learmonth, G. P. and Lewis, P. A. W., 'Naval Postgraduate School Random Number Generator Package', Naval Postgraduate School Report NPS55LW3061A, June 1973
5. Buckberg, M. L. and Vail, J. A., 'DDG-47 Reliability Engineering Analysis,' Naval Engineers Journal, v. 90, no. 3, p. 85-90, June 1978.
6. Naval Sea Systems Command Report 313-110-79, Reliability/Maintainability/Availability Design Data Bank, September 1979.
7. Judge, S. D. and Luetjen, P., 'Determination of Shipboard Repair Parts Level,' Naval Engineers Journal, v. 91, no. 2, p. 37-43, April 1979.
8. Department of Defense Military Standardization Handbook MIL-HDBK-217C, Reliability Prediction of Electronic Equipment, 9 April 1979.
9. Straub, D. R., 'Differences Between Failure Rates and Best Replacement Factors,' Navy Supply Corps Newsletter, v. 42, no. 5, p. 35-38, May 1979.
10. Esary, J. D. and Richards, F. R., Some Hostile Comments About the Definition of Operational Availability, paper presented at 44th Symposium of MORS, Vandenberg AFB California, 5 December 1979.

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