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CORRELATION OF HELICOPTER NOISE LEVELS WITH PHYSICAL AND PERFOR--ETC(U)
SEP 80 J S NEWMAN

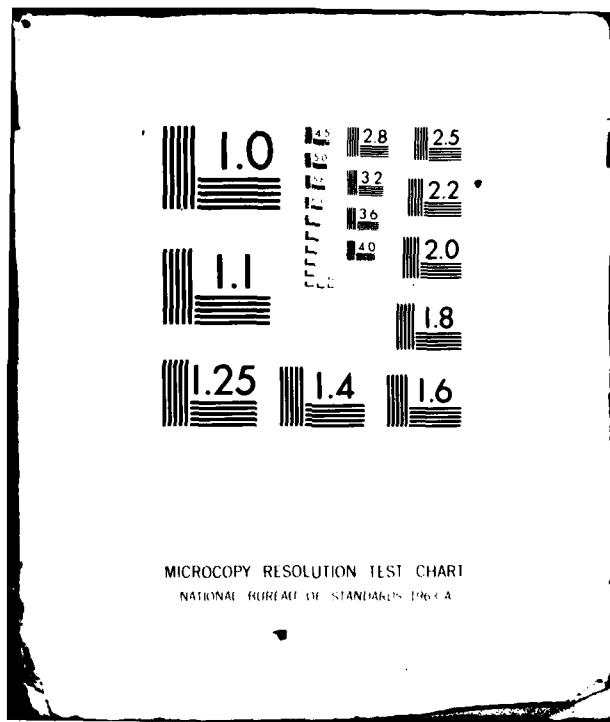
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MICROCOPY RESOLUTION TEST CHART
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Washington, D.C. 20591

LEVEL
(12)

Correlations of Helicopter Noise Levels with Physical and Performance Characteristics

A Preliminary Report

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September 1980

By J. Steven Newman

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16. Abstract This report investigates the correlation between physical and performance characteristics of helicopters and the noise levels which they generate in various operational modes. The analysis is generally empirical although several theoretical functions described in the literature have been examined. The EPNL is the acoustical metric employed in this study. One, two, and three-step multiple regression analyses are conducted for takeoff, approach, and level flyover operations. Plots are provided for the three best single variable regression models for each mode of flight.		
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1.0 INTRODUCTION

This report investigates the correlation between physical and performance characteristics of helicopters and the noise levels which the helicopters generate in various operational modes. The analysis is generally empirical although several theoretical functions described in the technical literature have been examined. The Effective Perceived Noise Level (EPNL) is the acoustical metric employed in this study. It is anticipated that subsequent analyses will examine trends for other metrics, in particular the Noise Exposure Level (single event, integrated A-Weighted Sound Level). This report has been limited to presenting statistical analyses. Parameters are tested for correlation with EPNL, a single event cumulative energy noise metric. The units of most analysis parameters are not energy. However, a limited number of variables dimensionally consistent with power, intensity or energy are tested.

1.1 Input Data Files

This study utilizes a data file assembled for analyses conducted in FAA-AEE-79-3, "Noise Levels and Flight Profiles of Eight Helicopters Using Proposed International Certification Procedures (Newman, J. S., Rickley, E. J.). This data file (Table 1.1) has been expanded to include a variety of physical parameters which may be expected to influence resulting noise levels. The legend for Table 1 is presented below:

NOTE: V_H is the speed at maximum continuous power.
 V_{NE} is the never exceed speed.

LEGEND FOR CROSS CORRELATION MATRIX

TYPE	-	Helicopter designation
EPNL	-	Effective Perceived Noise Level, (level flyover) expressed in decibels
WEIGHT	-	Test weight, lbs.
AREA	-	Total main rotor blade area (square feet)
MACH	-	Mach number of advancing blade; sum .9 (lesser of V_H or V_{NE}) level flyover forward speed and rotational tip speed
SHP	-	Maximum engine shaft horsepower
M-DISC	-	Main disc area, square feet
BRC	-	Best rate of climb, feet/minute
M-FREQ	-	Main rotor blade frequency. Using main rotor rpm (Jane's) and number of blades (Jane's) units in Blade Passages/Sec.
T-BLADE	-	Total tail rotor blade area (square feet)
EPNLA	-	Effective Perceived Noise Level (approach), decibels
LOGW	-	Common logarithm of weight
LOGA	-	Common logarithm of area
LOGS	-	Common logarithm of shaft horsepower
LOGMD	-	Common logarithm of main disc area
DISPL0	-	Main disc loading, lbs/square feet
LOGTB	-	Common logarithm of total tail blade area
MACH6	-	Mach number to sixth power
TSPEED	-	Rotational tip speed of tail rotor (feet/second)
MSPEED	-	Main rotor rotational tip speed (feet/second)
T-MACH	-	Tail rotor, rotational tip mach number
F1	-	$\log_{10} ((T\text{-MACH} \times \text{Weight})^2 / T\text{-Blade})$

- F2 - $\log_{10} ((MACH \times Weight)^2 / AREA)$
- F3 - $\log_{10} (SHP \times M-DISC/MACH)$
- F4 - $\log_{10} (MACH^6 \times T-BLADE)$
- F5 - $\log_{10} (T-MACH^6 \times AREA)$

2.0 CROSS CORRELATION OF ANALYSIS PARAMETERS

This section examines and discusses the interdependence between the parameters used in the regression analyses.

2.1 Cross Correlation Matrix

The matrix displayed as Table 2.1 (four pages) provides insight into the interrelationships between test variables and the relationship of each variable to EPNL for takeoff, approach and level flyover. Each entry in the matrix includes the correlation coefficient "R," the probability that the observed correlation is due merely to chance, and the number of observations. Many of the variables correlate equally well with the acoustical measures for all operational modes. Therefore, it is possible to develop a large number of single variable regression models which predict noise with similar accuracy.

The "good predictor" family of parameters includes:

- Weight: Helicopter Weight
- Area: Main Rotor Area
- SHP: Shaft Horsepower
- MDISC: Main Rotor Disc Area
- LOGW: Log Weight
- LOGA: Log Area

1.1 INPUT DATA FILES

HELICOPTER NOISE REGRESSION ANALYSIS

OBS	TYPE	EPNL	WEIGHT	AREA	MSPEED	SHP	M DISC	BRC	M FREQ	T BLADE	EPNLT	TSPEED
1	SA330J	91.4	15,532	188	682	3,150	1,925	1,400	17.6	15.0	95.4	669
2	B0105	88.4	5,070	116	724	840	804	1,772	22.5	3.7	91.7	730
3	B206L	85.8	4,000	37	763	840	1,075	1,550	13.1	2.2	90.3	691
4	S61	92.6	22,050	232	659	2,800	3,019	2,200	16.9	12.1	94.0	630
5	S65	97.1	37,000	475	700	7,925	4,070	2,180	18.5	19.2	99.9	663
6	B212	94.6	10,500	82	817	1,800	1,809	1,420	10.8	8.1	95.7	740
7	H500C	85.8	2,550	29	667	400	547	1,700	32.3	1.7	87.7	692
8	SA3416	86.1	3,970	51	681	590	931	1,770	18.9	1.9	89.5	696
9	SA350	87.2	4,180	47	671	641	962	1,575	18.3	3.7	91.2	653
10	SA321F	92.0	25,300	298	688	4,650	3,058	1,312	21.2	29.5	98.6	351
11	A109	90.4	5,390	80	727	840	1,023	1,620	25.7	4.4	93.0	-
12	MI6A	103.4	88,440	942	721	11,000	10,386	1,476	10.0	64.9	107.4	-
13	MI2	89.5	7,755	94	623	900	1,772	1,320	12.4	6.5	96.1	-
14	MI8	97.3	25,212	298	702	3,000	3,848	1,102	16.0	16.0	99.6	-
15	MG-13	97.7	9,350	109	699	1,500	1,385	1,200	21.2	8.6	96.9	717
16	B476	90.3	2,728	33	720	220	1,075	800	12.4	2.4	89.6	659
17	H300C	80.6	1,804	23	665	190	566	750	23.7	1.7	-	689
18	S64	96.7	42,812	518	700	9,000	4,070	1,330	18.6	20.2	98.6	-
19	SA365C	89.4	7,480	83	689	1,300	1,116	1,968	23.3	9.8	94.0	-
												725

1.1 INPUT DATA FILES
 (Continued)

HELICOPTER NOISE REGRESSION ANALYSIS

OBS	TYPE	LOGM	LOGA	LOGTB	LOGS	LOGMD	DISLO	MACH	MACH6
1	SA330J	4.19	2.27	1.18	3.50	3.28	8.07	0.80	0.26
2	B0105	3.71	2.06	0.57	2.92	2.91	6.31	0.83	0.32
3	B206L	3.60	1.57	0.34	2.92	3.03	3.72	0.86	0.41
4	S61	4.34	2.37	1.08	3.45	3.48	7.30	0.79	0.24
5	S65	4.57	2.68	1.28	3.90	3.61	9.09	0.82	0.31
6	B212	4.02	1.91	0.91	3.26	3.26	5.80	0.87	0.45
7	H500C	3.41	1.46	0.23	2.60	2.74	4.67	0.78	0.22
8	SA341G	3.60	1.71	0.28	2.77	2.97	4.26	0.80	0.27
9	SA350	3.62	1.67	0.57	2.81	2.98	4.35	0.77	0.21
10	SA321F	4.40	2.47	1.47	3.67	3.49	8.27	0.79	0.25
11	A109	3.73	1.90	0.64	2.92	3.01	5.27	0.85	0.37
12	M16A	4.95	2.97	1.81	4.04	4.02	8.52	0.83	0.32
13	M12	3.89	1.97	0.81	2.95	3.25	4.38	0.67	0.09
14	M18	4.40	2.47	1.20	3.48	3.59	6.56	0.79	0.25
15	WG-13	3.97	2.04	0.93	3.18	3.14	6.75	0.82	0.31
16	B47G	3.44	1.52	0.38	2.34	3.03	2.54	0.77	0.21
17	H300C	3.26	1.36	0.23	2.28	2.75	3.19	0.72	0.14
18	S64	4.63	2.71	1.31	3.95	3.61	10.52	0.78	0.22
19	SA365C	3.87	0.92	0.99	3.11	3.05	6.70	0.80	0.27

1.1 INPUT DATA FILES
 (Concluded)

HELICOPTER NOISE REGRESSION ANALYSIS

OBS	TYPE	F1	F2	F3	F4	F5
1	SA330C	6.76189	5.91467	6.87955	1.69328	0.94073
2	B0105	6.47313	5.18251	5.91106	1.57532	0.95841
3	B216L	6.44533	5.50604	6.02063	1.17856	0.31908
4	S61	7.10738	6.11200	7.03169	1.73750	0.87555
5	S65	7.40080	6.29196	7.59247	2.17344	1.31979
6	B212	6.77703	6.01214	6.57093	1.56453	0.84322
7	H500C	6.16752	5.13039	5.45019	0.80152	0.21705
-	SA3416	6.50872	5.30027	5.83467	1.13834	0.47724
9	SA350	6.20865	5.34392	5.90320	0.99310	0.27559
10	SA321F	6.33170	6.13156	7.25312	1.87283	-0.53993
11	A109	6.44866	5.41562	6.00639	1.46970	0.78899
12	M16A	7.71593	6.75620	8.13936	2.48492	1.87869
13	M12	6.47098	5.45619	6.37763	0.92358	0.48732
14	M18	7.23279	6.12854	7.16259	1.87283	1.37530
15	X6-13	6.62283	5.73361	6.40284	1.52566	0.88456
16	B47G	6.03392	5.12583	5.48750	0.83649	0.14584
17	H300C	5.86313	4.86593	5.17393	0.50728	0.10506
18	S64	7.55513	6.32951	7.67348	2.05646	1.50637
19	SA365C	6.38192	5.63898	6.25648	1.34985	0.79512

TABLE 2.1

CORRELATION COEFFICIENTS / FROM IRI UNDER HO: RHU=0 / NUMBER OF OBSERVATIONS									
	EPNL	WEIGHT AREA	M_SPEED	SHP	M_DISC	BRC	M_FREQ	T_BLADE	EPNL
WEIGHT	1.00000	0.79053	0.79117	0.25695	0.77085	0.79268	0.08050	-0.43628	0.74421
	0.00000	0.00001	0.0001	0.28833	0.0001	0.0001	0.7432	0.0618	0.0003
AREA	0.79053	1.00000	0.99371	0.07693	0.94703	0.98737	0.10075	-0.39223	0.95648
	0.00001	0.00000	0.0001	0.7544	0.0001	0.0001	0.6815	0.0967	0.0001
MPEED	0.25695	0.07690	0.05399	1.00000	0.07931	0.08655	-0.05065	-0.28462	0.06807
	0.2883	0.7544	0.8262	0.0100	0.7469	0.7246	0.8369	0.2376	0.7819
SHP	0.77085	0.94703	0.96552	0.07931	1.00000	0.39368	0.15580	-0.31874	0.86709
	0.00001	0.00001	0.0001	0.7469	0.0000	0.0001	0.5242	0.1835	0.0001
BRC	0.79268	0.98737	0.97105	0.08655	0.89368	1.00000	0.06522	-0.45733	0.95913
	0.00001	0.00001	0.0001	0.7246	0.0001	0.0000	0.7908	0.0436	0.0001
T_BLADE	0.74421	0.95648	0.93830	0.06807	0.86709	0.95913	0.03589	-0.36992	1.00000
	0.00003	0.00001	0.0001	0.7819	0.0001	0.0001	0.8840	0.1190	0.0000
EPNL	0.67551	0.84790	0.80291	-0.19970	0.76897	0.85679	0.08042	-0.28833	0.90556
	0.0225	0.0010	0.0029	0.5560	0.0057	0.0008	0.8442	0.3879	0.0001
TSPEED	0.09015	-0.01080	-0.02204	0.31234	-0.08031	-0.00042	0.06069	-0.00522	-0.16209
	0.7136	0.9650	-0.9286	0.1930	0.7438	0.9986	0.8051	0.9831	0.5074
LOGW	0.87708	0.87139	0.88408	0.04854	0.89840	0.84931	0.23246	-0.39572	0.85292
	0.00001	0.00001	0.0001	0.7804	0.0001	0.0001	0.3893	0.0832	0.0000

TABLE 2.1 (continued)

		CORRELATION COEFFICIENTS / PROB > IRI UNDER H0: RHO=0 / NUMBER OF OBSERVATIONS										F	F4	F5
		LNGA	LNGTB	LOGSD	LOGMD	DISLO	MACH	TMACH	MATH6	F1	F2	F	F4	F5
EPNL	0.85276 0.0001	0.85340 0.0001	0.82731 0.0001	0.87489 0.0004	0.72512 0.1579	0.33729 0.1579	0.09015 0.7136	0.30776 0.1999	0.84583 0.0001	0.88044 0.0001	0.86046 0.0001	0.86553 0.0001	0.77495 0.0001	
WEIGHT	0.85554 0.0001	0.82667 0.0001	0.81266 0.0001	0.89632 0.0001	0.70275 0.0001	0.16211 0.0001	-0.01080 0.9650	0.12237 0.6177	0.83365 0.0001	0.84928 0.0001	0.86553 0.0001	0.81561 0.0001	0.67820 0.0014	
AREA	0.89427 0.0001	0.83270 0.0001	0.83315 0.0001	0.89637 0.0001	0.74307 0.0003	0.15438 0.5280	-0.02204 0.9236	0.10794 0.6600	0.84829 0.0001	0.84584 0.0001	0.87861 0.0001	0.83862 0.0001	0.67483 0.0015	
MSPEED	0.01717 0.4444	0.03924 0.8733	0.11961 0.6257	0.08541 0.7231	0.01727 0.9440	0.82387 0.0001	0.31234 0.1930	0.87711 0.0001	0.15912 0.5153	0.19667 0.4197	0.08259 0.7355	0.26621 0.2706	0.23625 0.33205	
SHP	0.89390 0.0001	0.83566 0.0001	0.88327 0.0001	0.88437 0.0001	0.82687 0.0001	0.17251 0.4800	-0.08031 0.7438	0.12451 0.6115	0.85673 0.0001	0.86918 0.0001	0.90433 0.0001	0.94645 0.0001	0.63452 0.0035	
M_DISC	0.82507 0.0001	0.81062 0.0001	0.77031 0.0001	0.90113 0.0001	0.61882 0.0001	0.14875 0.0047	-0.00042 0.5433	0.12152 0.9986	0.81099 0.6202	0.83452 0.0001	0.84173 0.0001	0.78227 0.0001	0.67330 0.0016	
BRC	0.24999 0.3020	0.14655 0.5494	0.32369 0.1764	0.11520 0.6386	0.34516 0.1478	0.34802 0.1443	0.06069 0.8051	0.31324 0.1916	0.31043 0.1958	0.23507 0.3243	0.23710 0.3284	0.33174 0.1653	0.18344 0.4522	
M_FREQ	-0.28834 0.2312	-0.36277 0.1269	-0.31353 0.1912	-0.55503 0.0117	-0.02767 0.9105	-0.03070 0.9007	-0.00522 0.9831	-0.11339 0.6439	-0.40076 0.0891	-0.47037 0.0421	-0.42450 0.0698	-0.26119 0.2301	-0.32912 0.1689	
T_BLADE	0.80852 0.0001	0.84837 0.0001	0.76764 0.0001	0.85189 0.0001	0.65043 0.0001	0.16482 0.5001	-0.16209 0.5074	0.12653 0.6057	0.69194 0.0001	0.81245 0.0001	0.77735 0.0001	0.56792 0.0112		
EPNLA	0.91026 0.0001	0.94305 0.0001	0.88246 0.0001	0.92922 0.0001	0.73837 0.0003	0.06959 0.0003	-0.07047 0.0490	0.07347 0.6238	0.80155 0.0620	0.90649 0.0005	0.92477 0.0001	0.95568 0.0007	0.69888 0.5730	
TSPEED	-0.14272 0.5600	-0.23415 0.3346	-0.15392 0.5293	-0.15240 0.5334	-0.14511 0.5534	0.26467 0.2735	1.00000 0.0000	0.29416 0.2215	0.20866 0.3913	-0.12001 0.6246	-0.16626 0.4965	-0.04759 0.8466	0.58925 0.00779	
LOG4	0.98145 0.0001	0.95213 0.0001	0.97745 0.0001	0.96936 0.0001	0.88872 0.0001	0.21242 0.3826	-0.14994 0.5401	0.17339 0.4778	0.90740 0.0001	0.97752 0.0001	0.99640 0.0001	0.94254 0.0012	0.69491 0.0012	

TABLE 2.1 (Continued)

		CORRELATION COEFFICIENTS / PRED. : IRI UNDER H0:RHO=0 / NUMBER OF OBSERVATIONS											
		WEIGHT	AREA	M SPEED	SHP	M DISC	BRC	M FREQ	T BLADE	EFLA	EPNL T	TSPEED	LOGM
L05A	0.85276	0.85554	0.88427	0.01717	0.38990	0.82507	0.24999	-0.28834	0.80852	0.91026	0.92220	-0.14272	0.98145
L05B	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.3020	0.2312	0.00001	0.00001	0.00001	0.5600	0.0001
L07B	0.85340	0.82667	0.83270	0.03924	0.83566	0.81062	0.14655	-0.36277	0.84837	0.94305	0.95406	-0.23415	0.96313
L08	0.00001	0.00001	0.00001	0.00001	0.00001	0.00001	0.5494	0.1269	0.00001	0.00001	0.00001	0.3346	0.0001
L09	0.82731	0.81266	0.83315	0.11961	0.88327	0.77031	0.32369	-0.31353	0.76764	0.98246	0.90612	-0.15392	0.97745
DISL0	0.72512	0.70275	0.74307	0.01727	0.82687	0.61882	0.34516	-0.02767	0.65043	0.73837	0.88556	-0.14511	0.88872
MACH	0.33729	0.16211	0.15438	0.82287	0.17251	0.14875	0.34802	-0.03070	0.16482	0.06959	-0.13522	0.26467	0.21242
TMACH	0.09015	-0.01080	-0.02204	0.31234	-0.08031	-0.00042	0.06069	-0.00522	-0.16209	-0.07047	-0.60426	1.00000	-0.14994
MACH16	0.30776	0.12237	0.10794	0.87711	0.12451	0.12152	0.31324	-0.11339	0.12653	0.07347	-0.16689	0.29416	0.17339
F1	0.94583	0.83365	0.84829	0.15912	0.85673	0.81099	0.31043	-0.40076	0.69194	0.80155	0.57894	0.20866	0.90740
F2	0.98044	0.84928	0.84584	0.19667	0.86918	0.83452	0.23907	-0.47037	0.81245	0.90649	0.86763	-0.12001	0.97752
F3	0.86046	0.86558	0.87861	0.08299	0.90433	0.84173	0.23710	-0.42490	0.81943	0.92477	0.92252	-0.16626	0.99640
F4	0.86563	0.81501	0.83862	0.26621	0.84945	0.78287	0.33174	-0.26119	0.77375	0.86568	0.96066	-0.04759	0.94254
F5	0.77495	0.67820	0.67488	0.23625	0.63452	0.67330	0.18344	-0.32912	0.56792	0.69888	0.19134	0.58925	0.68491

TABLE 2.1 (Concluded)

CORRELATION COEFFICIENTS / PROB > IRI UNDER H0: RHO=0 / NUMBER OF OBSERVATIONS											
	L1GA	LOGITB	LOGS	LOGMD	DISLO	MACH	TMACH	MACH6	F1	F2	F3
L1GA	1.00000	0.94396	0.95947	0.93423	0.90700	0.18976	-0.14272	0.13980	0.89238	0.92411	0.97157
LOGA	0.00000	0.00001	0.00001	0.00001	0.00001	0.4365	0.5600	0.5681	0.00001	0.00001	0.00001
LOGITB	0.94396	1.00000	0.93472	0.92546	0.86439	0.16785	-0.23415	0.12995	0.78322	0.93861	0.95331
LOGMD	0.93423	0.92546	0.91059	1.00000	0.75781	0.14802	-0.15240	0.12578	0.88673	0.95682	0.96942
LOGS	0.90700	0.86439	0.93432	0.92546	0.90000	0.30681	-0.15392	0.26795	0.88978	0.96577	0.98347
DISLO	0.00001	0.00001	0.00001	0.00001	0.00001	0.2014	0.5293	0.2674	0.00001	0.00001	0.00001
MACH	0.18976	0.16785	0.30681	0.14802	0.25297	1.00000	0.26467	0.97559	0.29190	0.32545	0.21891
TMACH	0.4365	0.4922	0.2014	0.5453	0.2961	0.00000	0.2735	0.00001	0.22523	0.1739	0.3679
MACH6	0.13980	0.12995	0.26795	0.12578	0.17839	0.97559	0.29416	0.20866	-0.12001	-0.16626	-0.04759
F1	0.89238	0.78322	0.88673	0.79363	0.29190	0.20866	0.26339	0.39113	0.6246	0.4963	0.8466
F2	0.92411	0.93881	0.96577	0.95682	0.84466	0.32545	-0.12001	0.29517	0.89562	1.00000	0.98040
F3	0.97157	0.95335	0.98347	0.96442	0.98183	0.21891	-0.16626	0.18678	0.90565	0.98040	1.00000
F4	0.95266	0.89529	0.95200	0.87953	0.89103	0.47894	-0.04759	0.42367	0.88679	0.92584	0.93523
F5	0.57797	0.61193	0.65677	0.60045	0.36725	0.58025	0.84666	0.0707	0.00001	0.00001	0.00001

- LOGTB: Log Tail Blade Area
- LOGS: Log Shaft Horsepower
- LOGMD: Log Main Rotor Disc Area
- DISLO: Main Rotor Disc Loading

Other quantities which are linearly independent of these parameters can be expected to play the roles of second and third variable in the multiple regression analyses. However, it is possible to see more than one of these variables appear in a multiple regression if the two variables are largely independent of each other.

2.2 Summary of Best Correlates

The table provided below identifies those single parameters which best correlate with EPNL for the various operational modes.

<u>Level Flyover</u>		<u>Takeoff</u>		<u>Approach</u>	
<u>Parameter</u>	<u>R²</u>	<u>Parameter</u>	<u>R²</u>	<u>Parameter</u>	<u>R²</u>
F2	.774	LOG TB	.910	LOG TB	.889
LOG W	.769	LOG W	.891	LOG W	.867
LOG MD	.764	F3	.852	LOG MD	.863
F4	.765	LOG A	.850	F3	.856
F3	.739	LOG S	.826	LOG A	.828
LOG TB	.727	LOG MD	.826	F2	.821
LOG A	.727	T BLADE	.819	M DISC	.778
				LOG S	.778
				AREA	.774
				T BLADE	.774

The most apparent trend one observes is the much higher correlation for takeoff and approach EPNL values as compared with level flyover EPNL. One plausible reason for this is that the level flyovers are conducted at a higher speed than the approaches or takeoffs. It is reasonable to assume that forces generating noise in higher speed operation are subject to more variant and anomalous aerodynamic influences.

Another observation is the decline of LOG TB to "fifth place" for the higher speed level flyover. This can be attributed to the diminished tail rotor counter-torque load as the speed increased. This occurs as unbalanced airframe slip stream forces tend to counter the main rotor torque.

2.3 Plots of Best Single Variable Regression

The three best single variable regression models are plotted in Figures 2.3.1 through 2.3.3 for takeoffs, in Figures 2.3.4 through 2.3.6 for approach, and in Figures 2.3.7 through 2.3.9 for level flyover. Each plot includes identification of helicopter type and the line of regression.

3.0 STEPWISE REGRESSION ANALYSES

This analysis investigates the improvement in prediction accuracy associated with adding a second and third variable to the single parameter regression equation. For the correlation coefficient to

improve the added variables (or steps) must be largely independent of previous step(s) but still related to the level of noise. Three-step models are presented below for takeoff, approach, and level flyover.

Approach

1 Step

$$EPNL = 10.2 \log (TB) + 85.9$$

$$R^2 = .89$$

2 Step

$$EPNL = 7.1 \log (TB) + .0007 (M DISC) + 86.9$$

$$R^2 = .93$$

3 Step

$$EPNL = 7.9 \log (TB) + .005 (T SPEED) + .0006 (M DISC)$$

$$R^2 = .94$$

Level Flyover

1 Step

$$EPNL = 9.4 (F2) + 37.4$$

$$R^2 = .76$$

2 Step

$$EPNL = 10.4 \log (MD) + 3.6 (F5) + 59.5$$

$$R^2 = .84$$

3 Step

$$EPNL = 10.7 \log (MD) + 17 (MACH) + 3 (F5) + 44.9$$

$$R^2 = .85$$

Takeoff

1 Step

$$EPNL = 9.6 \log(TB) + 83.87$$

$$R^2 = .91$$

2 Step

$$EPNL = 9.55 \log(TB) - 7.3 (MACH)^6 + 86.1$$

$$R^2 = .93$$

3 Step

$$EPNL = 6.3 \log(TB) + 5.5 \log(MD) - 9.6 (MACH)^6 + 71.97$$

$$R^2 = .95$$

The following table provides a summary of parameters and correlation coefficients associated with each step of the multiple regression analyses for the various operational modes:

Takeoff

<u>Step</u>	<u>R²</u>	<u>Parameter(s)</u>
1	.91	Log TB
2	.93	Log TB, (MACH) ⁶
3	.95	Log TB, (MACH) ⁶ , Log (MD)

Approach

<u>Step</u>	<u>R²</u>	<u>Parameter(s)</u>
1	.89	Log TB
2	.93	Log TB, M DISC
3	.94	Log TB, M DISC, T SPEED

Level Flyover		
Step	R ²	Parameter(s)
1	.76	F2
2	.84	F5, Log MD
3	.85	Log MD, MACH, F5

4.0 DISCUSSION

The empirical noise prediction techniques presented above provide a means to estimate single event cumulative noise exposure for helicopters whose technology and operational characteristics are similar to the helicopters used in this analysis. The obvious advantage of the strictly empirical approach (using the single event cumulative energy metric EPNL) is the averaging out of source directionality, ground interference effects, anomalous air in-flow characteristics, and speed effects. All of these considerations pose significant difficulties in the theoretical approach. On the other hand, the theoretical approach can be more successful in predicting the change in noise level associated with a design change for a specific helicopter.

The parameters appearing (or not appearing) as significant correlates to noise in this study raise some interesting questions. For example, the strength of LOG TB was not anticipated nor is "Tail Blade Area" a particularly good acoustical design parameter. On the other hand, the main rotor advancing tip mach number to the sixth power (considered an important correlate to noise) appears as a weak correlate by itself, although it does strengthen the takeoff correlation in the multiple regression analysis. Interpretation of these results and discussion of application in predicting noise of new design helicopters or reducing levels of existent machines is left for subsequent study.

TAKEOFF REGRESSION OF EPNL VERSUS LOGTA
 EMPIRICAL NOISE PREDICTION ANALYSIS

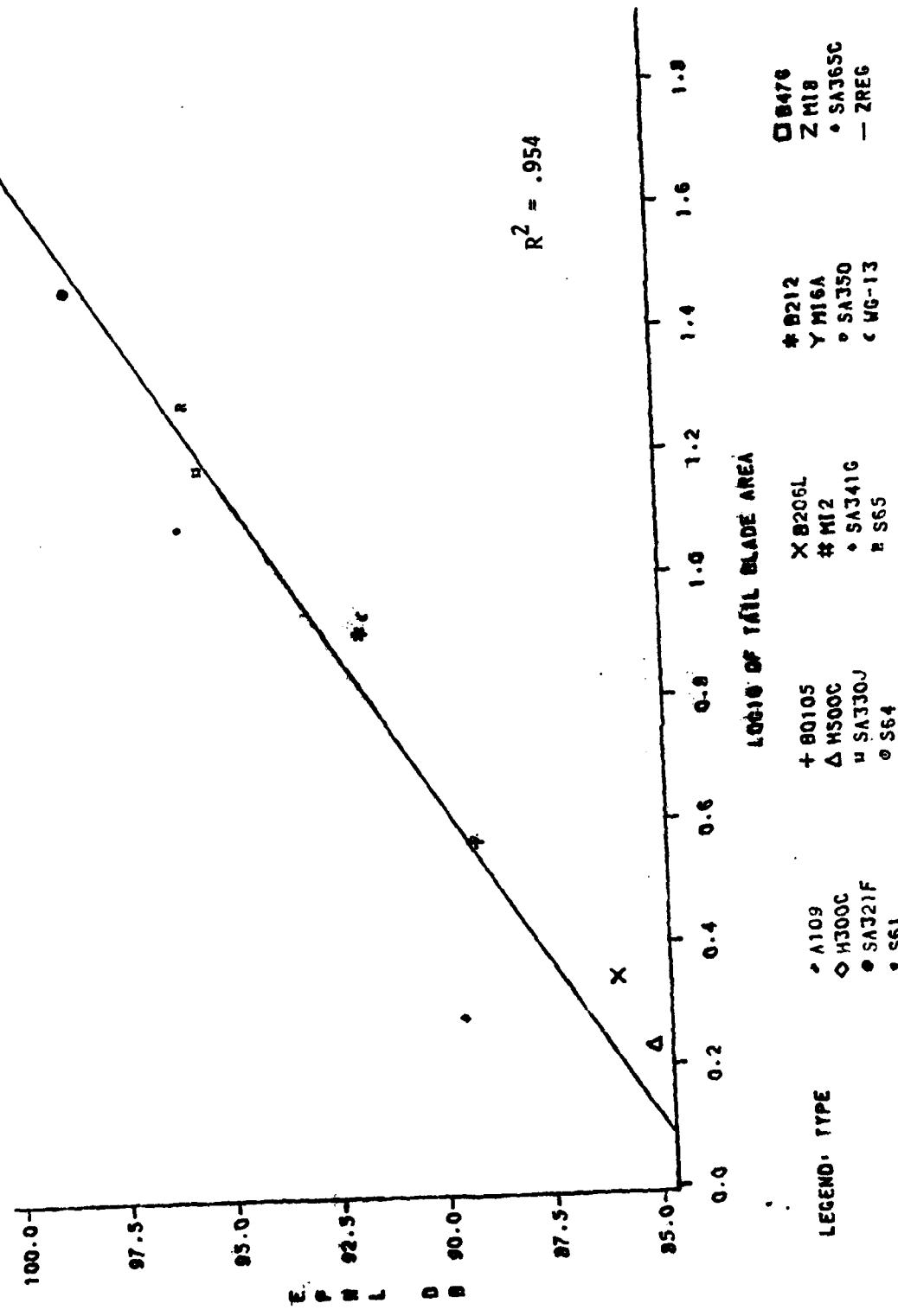


FIGURE 2.3.1

TAKEOFF REGRESSION OF EPNL VERSUS LOGW
 EMPIRICAL NOISE PREDICTION ANALYSIS

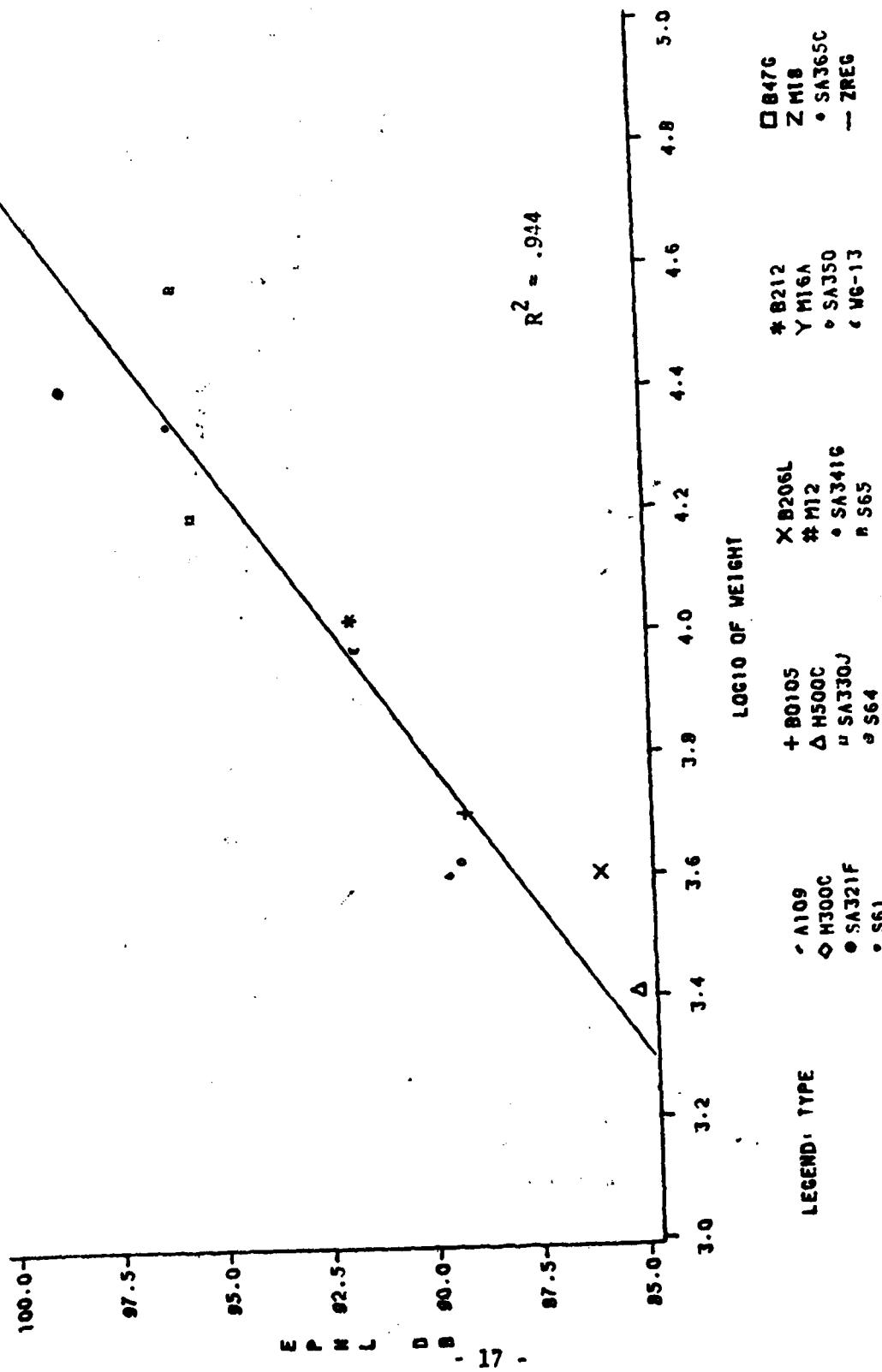
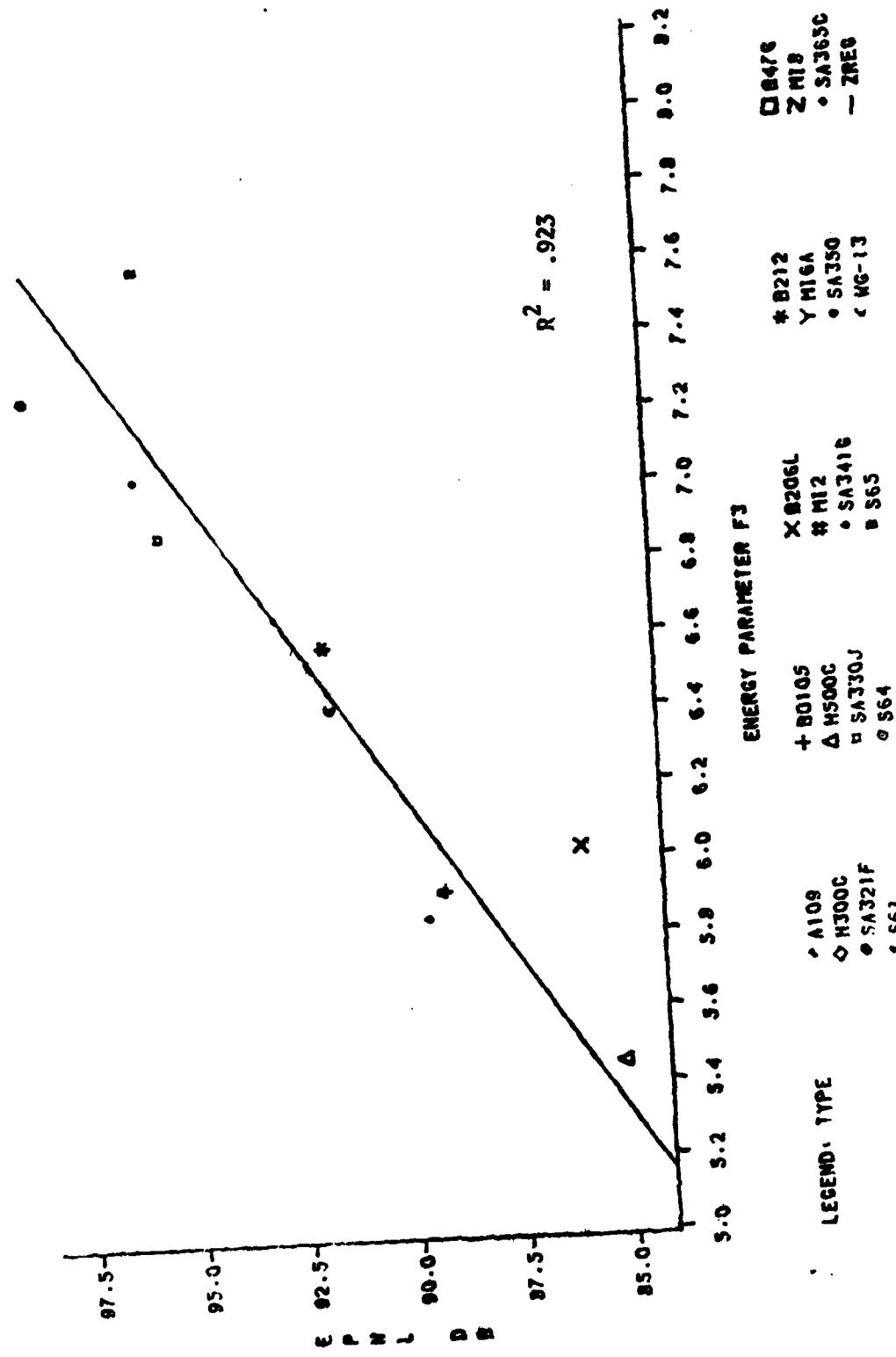


FIGURE 2.3.2

TAKEOFF REGRESSION OF EPNL VERSUS F3
 EMPIRICAL NOISE PREDICTION ANALYSIS



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F3=LOG10(15HP*MAIN DISC AREA/MACH)

FIGURE 2.3.3

LEVEL FLYOVER REGRESSION OF EPNL VERSUS F2
EMPIRICAL NOISE PREDICTION ANALYSIS

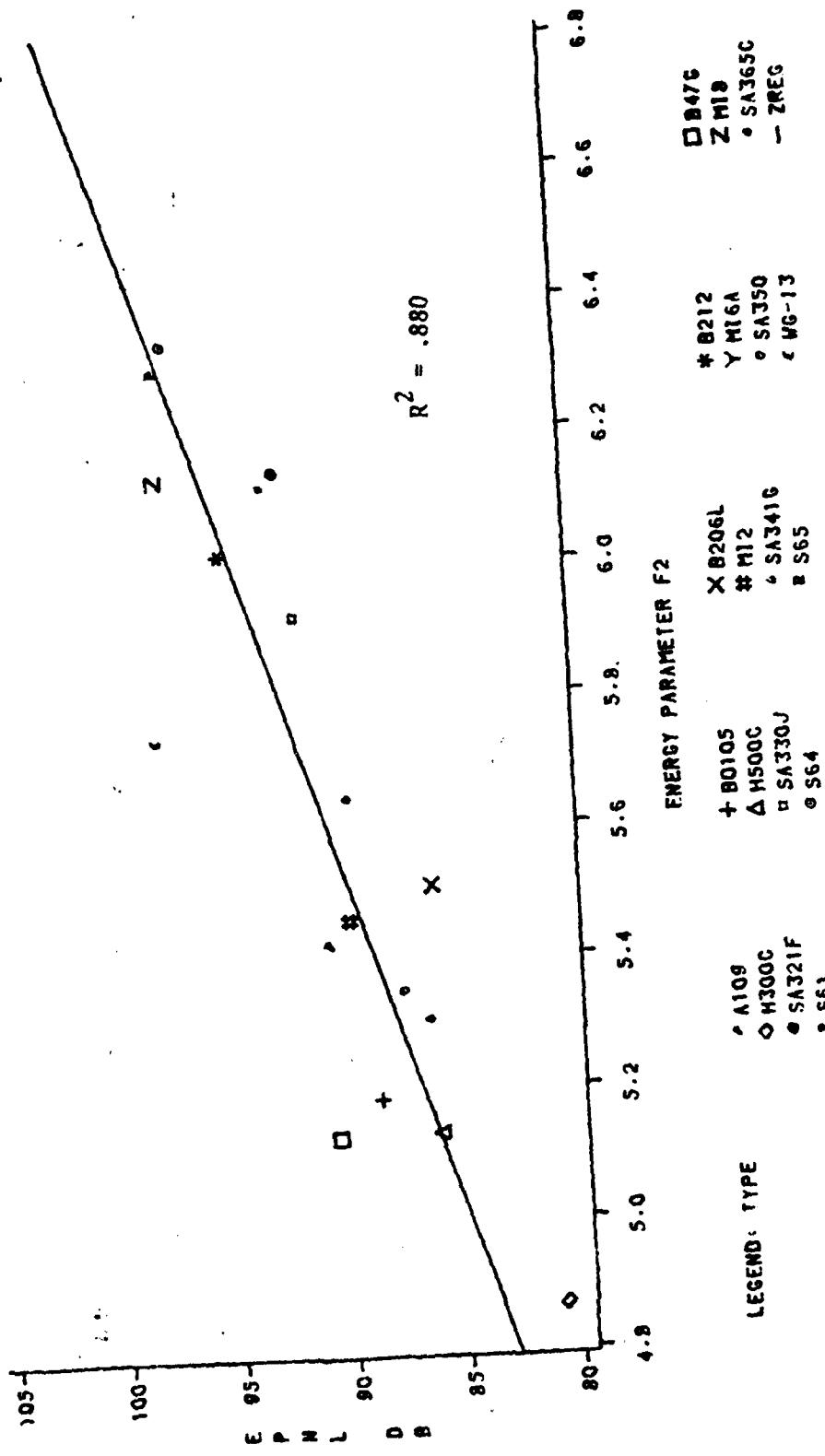


FIGURE 2.3.4

F2=L00101(MACH*WEIGHT)*2/AREA)

LEVEL FLYOVER REGRESSION OF EPNL VERSUS LOGW
EMPIRICAL NOISE PREDICTION ANALYSIS

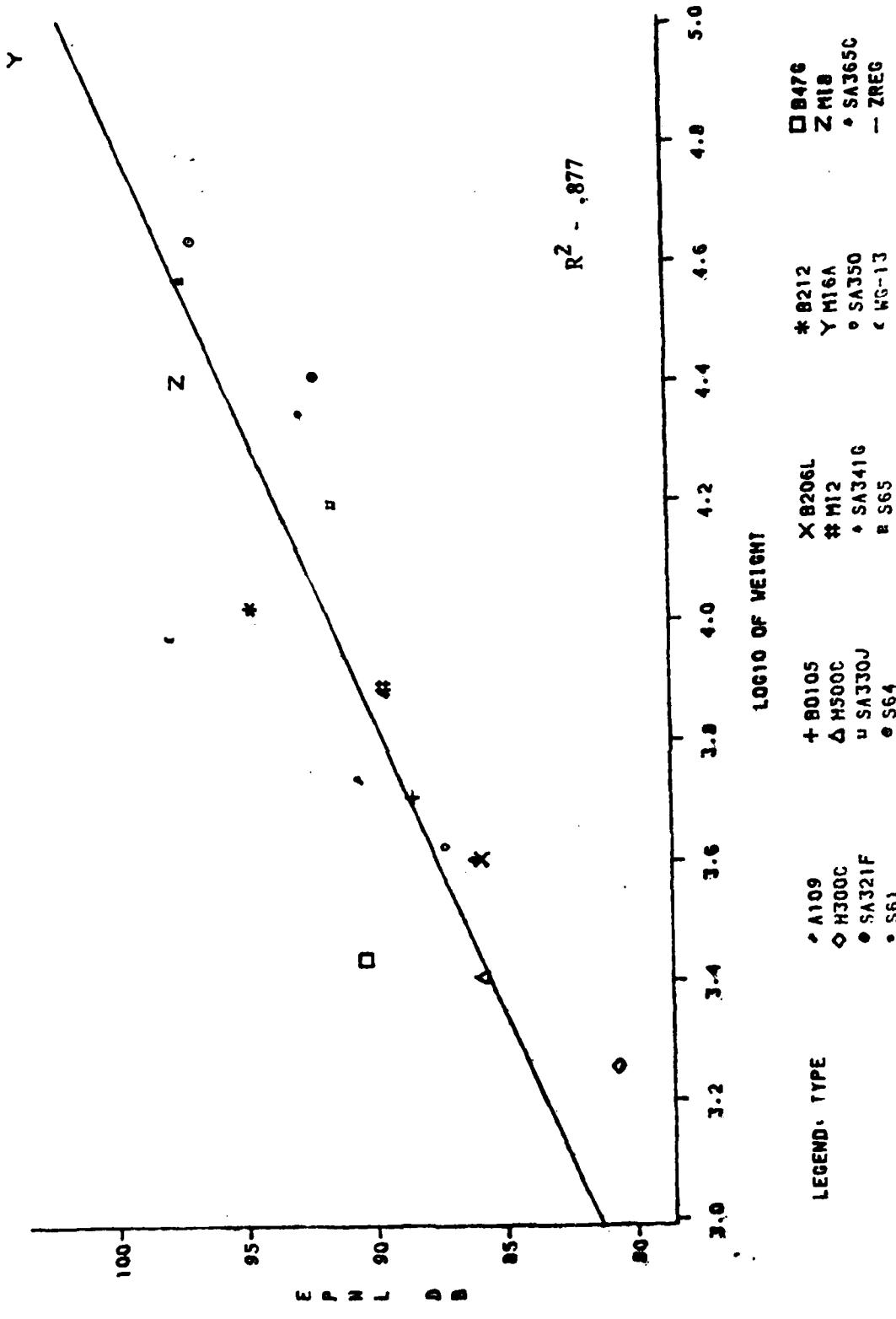


FIGURE 2.3.5

LEVEL FLYOVER REGRESSION OF EPNL VERSUS LOGMD
EMPIRICAL NOISE PREDICTION ANALYSIS

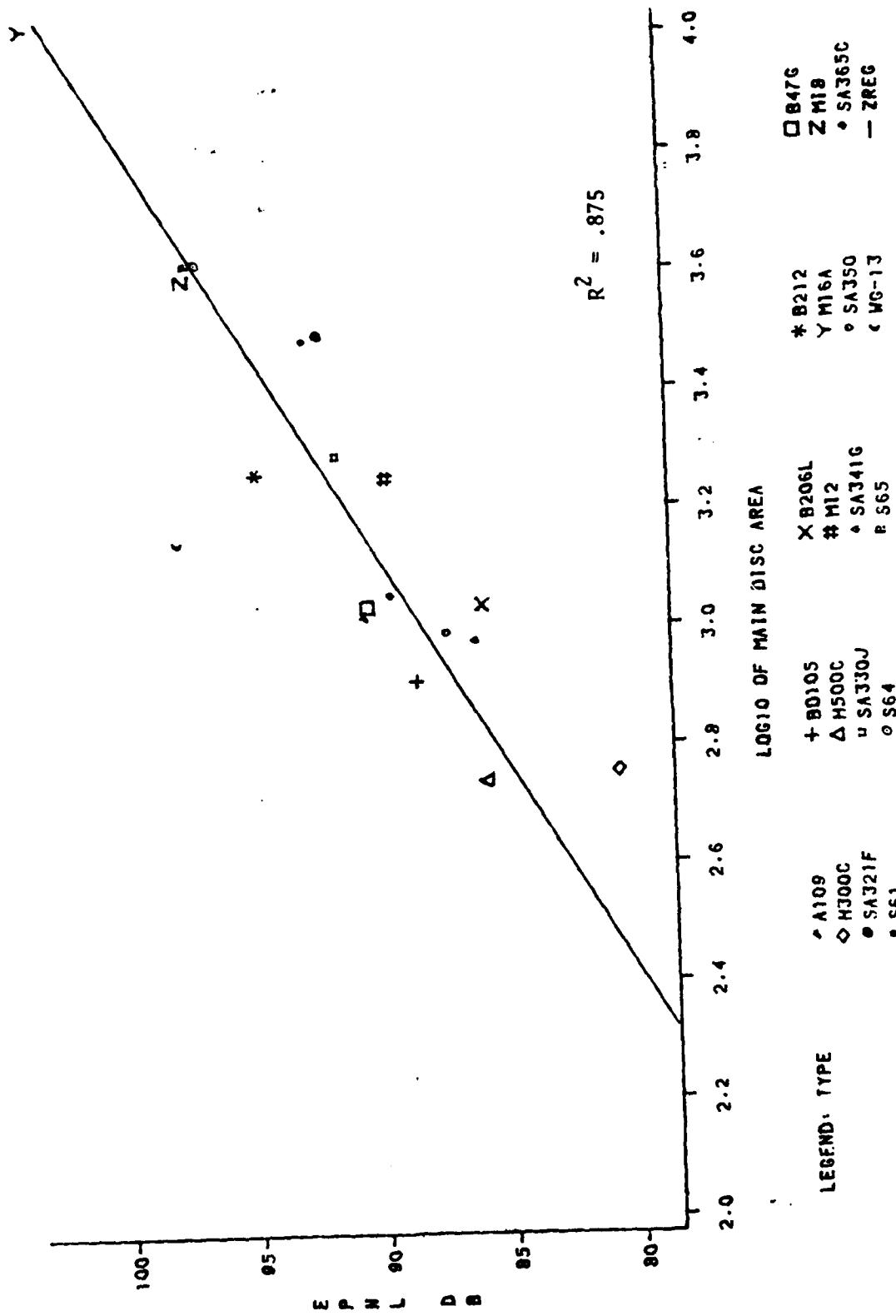


FIGURE 2.3.6

APPROACH REGRESSION OF EPNL VERSUS LOGTB
EMPIRICAL NOISE PREDICTION ANALYSIS

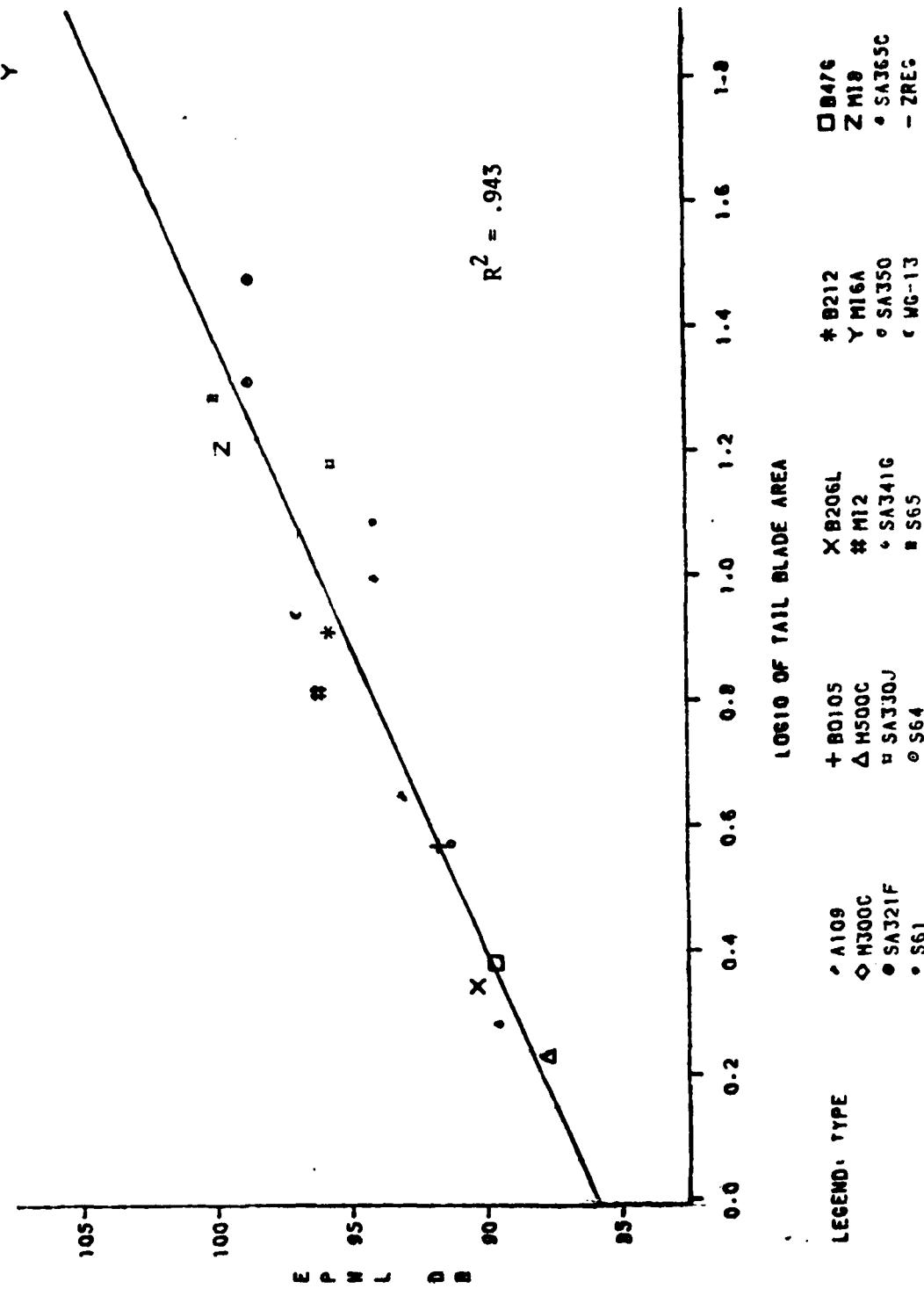


FIGURE 2.3.7

APPROACH REGRESSION OF EPNL VERSUS LOGW
EMPIRICAL NOISE PREDICTION ANALYSIS

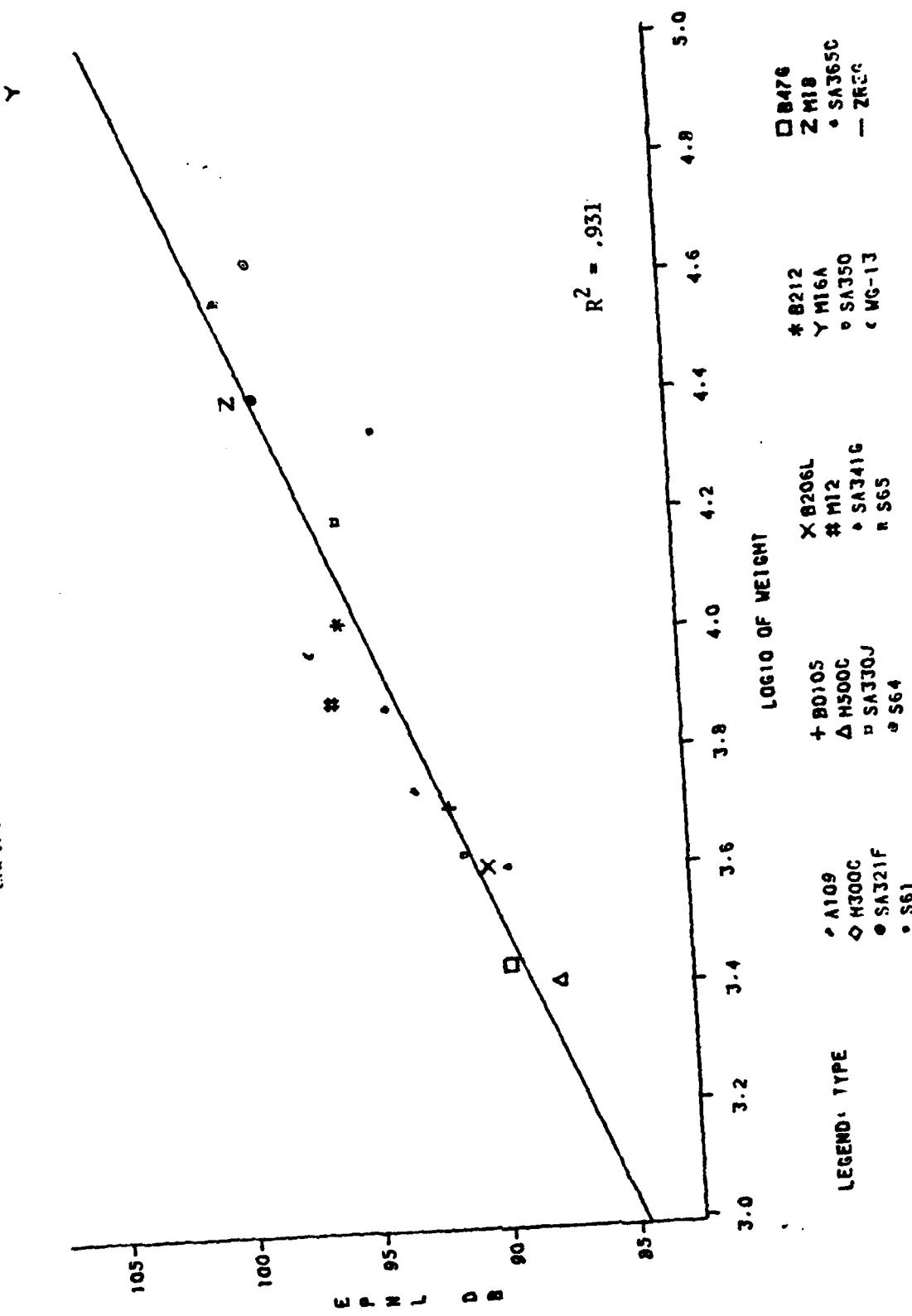


FIGURE 2.3.8

APPROACH REGRESSION OF EPNL VERSUS LOGMD
EMPIRICAL NOISE PREDICTION ANALYSIS

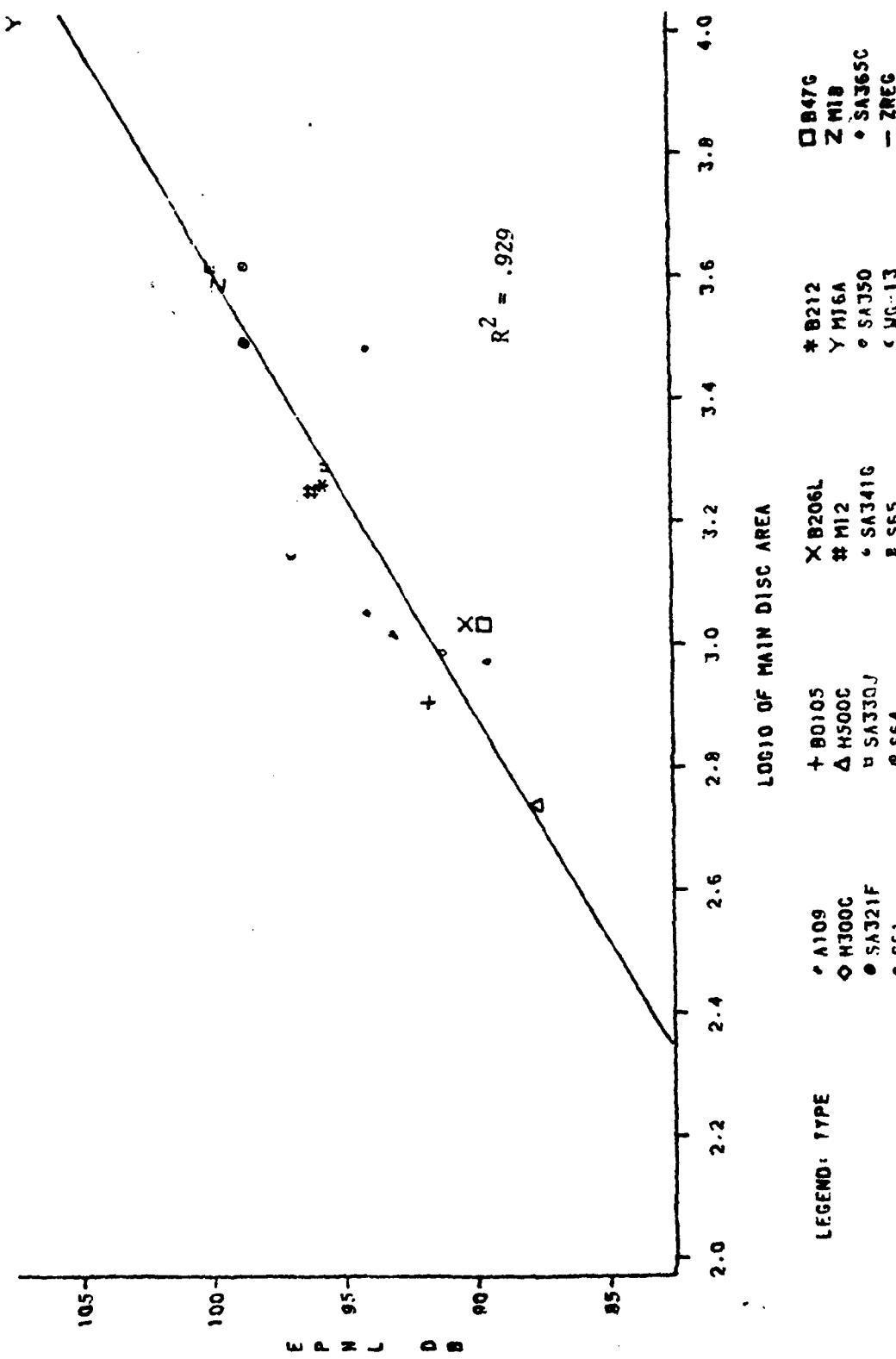


FIGURE 2.3.9

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