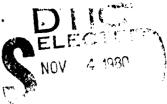


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PREFACE

This report is prepared under guidance contained in the <u>Recommended</u> <u>Guidelines for Safety Inspection of Dams</u>, for Phase I Investigations. Copies of these guidelines may be obtained from the Department of the Army, Office of Chief of Engineers, Washington, D.C. 20314.

The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon visual observations and review of available data. Detailed investigations and analyses involving topographic mapping, subsurface investigations, material testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the inspection is intended to identify any need for such studies which should be performed by the owner.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of the dam depends on numerous and constantly changing internal and external factors which are evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The assessment of the conditions and recommendations was made by the consulting engineer in accordance with generally and currently accepted engineering principles and practices.

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

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NAME OF DAM: Spruce Reservoir STATE LOCATED: Pennsylvania COUNTY LOCATED: Union STREAM: Spruce Run, a Secondary Tributary of the West Branch of the Susquehanna River SIZE CLASSIFICATION: Intermediate HAZARD CLASSIFICATION: High OWNER: Keystone Water Company, White Deer District DATE OF INSPECTION: April 28, 1980 and April 30, 1980

ASSESSMENT: Based on the evaluation of the existing conditions, the condition of Spruce Reservoir is considered to be fair. In view of indications of surficial slumps on the downstream face of the main embankment, combined with the observations that the embankment does not have any internal drainage system to control seepage through the embankment and the downstream slope is relatively steep (2H:1V), concern exists as to the actual location of the phreatic surface through the embankment and its effect on the stability of the dam. Based on these observations, reevaluation of the stability of the embankment is recommended.

According to the recommended criteria, intermediate size dams in the high hazard category are required to pass full probable maximum flood (PMF) without overtopping the embankment. The flood discharge capacity was evaluated according to the recommended criteria and the bypass channel spillway was found to pass 60% percent of the PMF without overtopping the embankment on the upstream side of Spruce Reservoir. For 80 percent of the PMF, it was found that flow entering the reservoir over the upstream embankment can pass through the reservoir overflow spillway without overtopping the main embankment. Because the spillway capacity (80 percent of the PMF) is less than the required capacity of full PMF, the flood discharge capacity of the dam is rated to be inadequate. Therefore, it is considered advisable that the owner retain a professional engineer to conduct additional detailed hydrological and hydraulic studies to determine the need to provide emergency spillway facilities to the reservoir.

The following recommendations should be implemented immediately or on a continuing basis.

> The owner should immediately retain a professional engineer experienced in the design and construction of dams to reevaluate the stability of the embankment in view.

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of the observations noted. The reevaluation of the dam should include, but not be limited to, subsurface investigation, materials testing, installation of instrumentation, and seepage and stability analyses.

- 2. In conjunction with the detailed evaluation of the dam, the crest of the dam should be surveyed and the low spots tilled to design elevation.
- 3. Brush and trees in the bypass channel below the spillway should be removed.
- The operational condition of the outlet pipe gate should be evaluated and necessary maintenance performed.
- Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alort the downstream residents in the event of emergencies.
- 6. The dam and appurtement structures should be inspected regularly and a formal maintenance maintal should be developed for the continued maintenance of the dam.

Lawrence D. Andersen, P.E. Vice President July 30, 1980 Lan Date Approved by: Accession XIIS 011.8 NTC TO JAMES W. PECK Colonel, Corps of Engineers District Engineer Date 1 月代: i i i

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SPRUCE BESERVOIR DAM NDL I.D. PA-487 DER I.D. 69-75 APRIL 28, 1980 AFRILLO, INS APPORT FORS APPORT For Iva nin Fran I In-partin Artite

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Overview (Downstream face of main embankment)

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PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM SPRUCE RESERVOIR NDI I.D. PA-587 DER I.D. 60-7

SECTION 1 PROJECT INFORMATION

1.1 General

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a. <u>Authority</u>. The inspection was performed pursuant to the authority granted by The National Dam Inspection Act, Public Law 92-367, to the Secretary of the Army, through the Corps of Engineers, to conduct inspections of dams throughout the United States.

b. <u>Purpose</u>. The purpose of this inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project

a. Dam and Appurtenances. Spruce Reservoir consists of an earth embankment approximately U-shaped in plan view, impounding an offstream reservoir. The main embankment starts from the left side of the valley (looking downstream), continues across the valley for approximately 800 feet, then turns upstream and continues approximately 3200 feet joining the earth embankment which forms the upstream end of the reservoir. The bypass channel is located between the embankment and the right side of the valley. An ogeecrested overflow weir across the bypass channel in line with the upstream end of the reservoir forms the diversion structure which diverts water through a controlled intake structure into Spruce Reservoir. Excess flow entering the reservoir is discharged through an uncontrolled outlet structure located near the right downstream corner of the reservoir. The portion of the embankment along the downstream end of the reservoir has a maximum height of approximately 46 feet from the downstream toe and a crest elevation 4 feet above the normal pool level of the reservoir. The crest level of the portion of the embankment along the upstream end of the reservoir is 2 feet above the crest level of the main embankment, providing 6 feet of freeboard to the spillway located across the bypass channel.

The outlet facilities for Spruce Reservoir consist of a concrete intake tower, a 24-inch outlet pipe, and a 16-inch supply line. Flow through these pipes is controlled by valves located at the intake tower. The 24-inch outlet pipe constitutes the emergency drawdown facility for the reservoir.

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b. Location. Spruce Reservoir is located on Spruce Run in Buffalo and White Deer Townships, Union County, Pennsylvania. Plate 1 illustrates the location of the dam.

c. <u>Size Classification</u>. Intermediate (based on 46-foot height and 1780 acre-feet maximum storage capacity).

d. <u>Hazard Classification</u>. The dam is classified to be in the high hazard category. At least five houses within a one-mile downstream reach are considered to be within the potential flood plain of Spruce Reservoir. It is estimated that failure of the dam would cause large loss of life and property damage in the downstream rural residential areas.

e. <u>Ownership</u>. Keystone Water Company, White Deer District, (address: Mr. E. L. Guskey, Manager, White Deer District, 114 South Front Street, Milton, PA 17847).

f. Purpose of Dam. Water supply.

g. <u>Design and Construction History</u>. The dam was designed by American Water Works Service Company, Inc., in 1956 and constructed by the owner with completion in 1957.

h. <u>Normal Operating Procedure</u>. Flow into the reservoir is controlled by stop logs across an intake structure at the upstream end of the reservoir. Flow entering the reservoir is maintained at Elevation 672 (USGS Datum) which is the crest level of the uncontrolled overflow spillway.

1.3 <u>Pertinent Data</u>. Elevations referred to in this and subsequent sections of the report were taken from the design drawings.

a. Drainage Area

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13.2 square miles

b. Discharge at Dam Site (cfs)

Maximum known flood at dam site Outlet conduit at maximum pool Gated spillway capacity at maximum pool Ungated spillway capacity at maximum pool Total discharge capacity at maximum pool Unknown 83<u>+</u> Not applicable 9278(1) 9278

(1) Bypass channel spillway capacity based on the current available freeboard. (Reservoir spillway capacity is estimated to be 83 cfs.)

c. Elevation (USGS Datum) (feet)

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	Top of dam Maximum pool Normal pool Upstream invert outlet works Downstream invert outlet works Maximum tailwater Toe of Dam	676 (main embankment) 675.9 672 635.75 630 <u>+</u> Unknown 630 <u>+</u>
d.	Reservoir Length (feet)	
	Normal pool level Maximum pool level	3200 3200 <u>+</u>
e.	Storage (acre-feet)	
	Normal pool level Maximum pool level	1535 1780
f.	<u>Reservoir Surface (acres)</u>	
	Normal pool level Maximum pool level	61 61 <u>+</u>
g٠	Dam	
	Type Length Height Top width Side slopes Zoning Impervious core Cutoff Grout Curtain	Earth 4600 feet 46 feet 15 feet Downstream: 2H:lV; Upstream: 2H:lV Yes Yes Yes
h.	Regulating Outlet	
	Type Length Closure	24-inch cast- iron pipe 350+ feet Sluice gate
	Access	Intake tower
	Regulating facilities	Sluice gate

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i. <u>Spillway</u>

Bypass Channel

Reservoir

Type Length Crest elevation Upstream channel Downstream channel Concrete ogee 212 feet 672 Stream Bypass channel Drop inlet 15 feet(2) 672 Reservoir 24-inch outlet pipe

(2)Perimeter of drop inlet structure.

SECTION 2 DESIGN DATA

2.1 Design

a. <u>Data Available</u>. The available information was provided by the Commonwealth of Pennsylvania, Department of Environmental Resources (PennDER), and by the owner. The available information includes design drawings, correspondence, and maintenance records kept by the owner.

(1) <u>Hydrology and Hydraulics</u>. The available information includes the design capacity of the bypass channel spillway.

(2) <u>Embankment</u>. The available information consists of design drawings, construction progress reports, and the records of postcon-struction grouting work provided by the owner.

(3) <u>Appurtenant Structures</u>. The available information includes design drawings.

b. Design Features

(1) Embankment. Plate 2 shows the plan and the typical cross section of the portion of the embankment along the upstream end of the reservoir. This portion of the embankment and the bypass channel spillway was constructed in 1916 as a diversion dam. During the construction of Spruce Reservoir in 1956, the diversion dam was utilized as a dike to form the upstream end of the reservoir. As shown in Plate 2, the typical cross section of the upstream dike consists of a homogeneous embankment with a central concrete core wall. Plate 4 shows the plan and the typical cross sections of the embankment along the bypass channel and the downstream side of the reservoir. The typical cross section is shown to be essentially a homogeneous embankment with a central impervious core section. The drawings indicate that as designed, the embankment slopes were 2H to 1V on both the upstream and downstream faces. The upstream face was protected with riprap extending from the upstream toe to the crest level, and the outside portion of the embankment along the bypass channel was provided with riprap extending vertically 10 feet up from the downstream toe.

(2) <u>Appurtenant Structures</u>. The appurtenant structures consist of a bypass channel, an intake structure located at the upstream end of the reservoir, and a reservoir spillway and outlet works. The bypass channel is approximately 212 feet wide at the spillway section in line with the upstream end of the reservoir,

enlarging to a width of 275 feet approximately 200 feet downstream from the spillway. The bypass channel spillway crest is at Elevation 672, with an available freeboard of 6 feet (as designed) relative to the upstream dike crest located at Elevation 678. Flow diverted by the bypass channel spillway flows through a diversion channel along the upstream dike and enters into Spruce Reservoir through an intake structure. Stop logs across the intake structure control the flow rate into the reservoir. An overflow drop inlet structure at the reservoir intake tower constitutes the reservoir spillway. Plate 5 shows the plan of the overflow section and the outlet works. The typical cross section of the dam through the outlet works and details of the outlet facilities are included in Plates 6 and 7, respectively. The outlet facilities include a 24-inch cast-iron outlet pipe and a 16-inch supply line. Flow through these pipes is controlled by sluice gates located at the intake tower.

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c. Design Data

(1) <u>Hydrology and Hydraulics</u>. A Commonwealth report dated May 9, 1956, indicates that the bypass channel spillway was sized for a capacity of 10,290 cubic feet per second (cfs), corresponding to a runoff of 763 cfs per square mile in conformance with Commonwealth spillway design criteria applicable at the time.

(2) <u>Embankment</u>. Other than design drawings, the available information includes no engineering data on the design of the embankment.

(3) <u>Appurtenant Structures</u>. Other than design drawings, no design data are available on the appurtenant structures.

2.2 <u>Construction</u>. Very limited information is available on the construction of the dam. As can be inferred from the construction progress reports prepared by the owner, the construction of the dam was conducted in conformance with the specifications prepared by the designers. No reference to any construction difficulties was noted.

2.3 Operation. The operating records consist of reservoir stage records remotely monitored and recorded at the water company's treatment plant in Milton, Pennsylvania.

2.4 Other Investigations. None reported.

2.5 Evaluation

a. <u>Availability</u>. The available information was provided by PennDER and the owner.

b. Adequacy

(1) <u>Hydrology and Hydraulics</u>. Available information consists of the design capacity of the bypass channel spillway. This information is not considered to be sufficient to assess the adequacy of the spillway.

(2) <u>Embankment</u>. Other than design drawings, no design data are available to assess the structural design of the embankment.

(3) <u>Appurtement Structures</u>. Based on the review of the design drawings, the structural design of the appurtement structures is considered to be adequate.

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SECTION 3 VISUAL INSPECTION

3.1 Findings

a. <u>General</u>. The on-site inspection of Spruce Reservoir consisted of:

- 1. Visual inspection of the embankment, abutments, and embankment toe.
- 2. Visual examination of the spillway structures.
- 3. Evaluation of downstream area hazard potential.

Plate 8 illustrates some of the existing features of the dam.

b. Embankment. The general inspection of the embankment consisted of searching for indications of structural distress, such as cracks, subsidence, bulging, wet areas, seeps and boils, and observing general maintenance conditions, vegetative cover, erosion, and other surficial features.

The embankment was found to be in fair condition. The conditions noted which require further attention are the indications of surficial slumps along the lower half of the main embankment at the downstream end of the reservoir. It appears that these conditions are caused by saturation of the poorly draining embankment surface material on a relatively steep (2H:1V) slope of the embankment. Although it is possible that a high phreatic surface through the embankment could be contributing to this condition, no noticeable seeps were found on the downstream slope of the dam that would support this observation. At this time, indications of surficial slumps are not considered to be serious relative to the overall stability of the embankment. Another condition noted was the presence of erosion in the areas where the embankment is lacking adequate vegetative cover. At the upstream side of the main embankment at its junction with the left abutment, riprap appears to have dislocated due to wave action, posing a potential for shoreline erosion. A swampy area was found at the toe level of the main embankment-left abutment junction with an associated seepage on the order of 10 to 20 gallons per minute. It was noted by the owner that swampy conditions have existed in the past and a french drain system was installed at the junction of the embankment and abutment to collect the seepage. This appears to be contributing to the swampy conditions along the toe of the dam. The present extent of the swampy condition is not considered to be serious relative to the overall stability of the dam.

The crest of the dam was surveyed relative to the bypass channel spillway crest level and the crest of the embankment along the upstream side of the reservoir was found to be up to 0.9 foot below the design crest elevation. The lowest point occurred adjacent to the bypass channel left abutment wall. The crest levels of the embankment along the bypass channel and the embankment on the downstream side of the reservoir were found to be essentially at or above the design level. The dam crest profile is illustrated in Plate 9. The downstream slopes were surveyed and found to be reasonably within the design slope of 2H to 1V.

c. <u>Appurtenant Structures</u>. The visible portions of the appurtenant structures were examined for deterioration and other signs of distress or obstructions that would limit flow. The structures were found to be in good condition. One condition noted was thick growth of brush and trees in the bypass channel below the spillway. Although at this time this condition is not considered to constitute a significant obstruction affecting the discharge capacity of the bypass channel, clearing brush and trees in the channel in the first 200 feet is recommended. The operational condition of the outlet pipe sluice gate was not observed.

d. <u>Reservoir Area</u>. The visual observations indicated no landslide activity in the vicinity of the dam. The review of the regional geology is included in Appendix F.

f. <u>Downstream Channel</u>. A description of the downstream channel is included in Section 1.2d.

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3.2 Evaluation. The dam was found to be in fair condition. Although the observed conditions are not considered to be serious relative to the overall stability of the dam at this time, further investigation of the causes of slumping on the downstream face of the dam is considered necessary. In conjunction with this further investigation, measures should be taken to prevent erosion of the downstream slope of the dam. Also, brush and trees in the bypass channel for at least 200 feet below the spillway should be cleared.

SECTION 4 OPERATIONAL FEATURES

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4.1 <u>Procedure</u>. There are no formal operating procedures for the dam. The reservoir is normally maintained at the overflow spillway crest level by regulating the inflow into the reservoir. Water levels in the reservoir are remotely monitored and recorded at the water company treatment plant in Milton, Pennsylvania.

4.2 <u>Maintenance of the Dam</u>. The downstream slope of the dam is covered with small brush up to 2 feet high. It appears that taller brush is periodically cut. In areas with poor vegetative cover, surficial erosion of the embankment material was noted. The brush may tend to inhibit the growth of grass which would control this erosion.

4.3 <u>Maintenance of Operating Facilities</u>. The operating facilities were found to be adequately maintained. Because the owner was concerned about the operational condition of the reservoir outlet pipe sluice gate, the operational condition of the gate was not observed.

4.4 <u>Warning System</u>. No formal warning system exists for the dam. However, as previously mentioned, reservoir levels are remotely monitored at the water treatment plant. Telephone communication is available via residences in the vicinity of the dam site.

4.5 Evaluation. The maintenance condition of the dam is considered to be fair. Implementation of measures to control embankment erosion and evaluation of the operational condition of the outlet pipe sluice gate is recommended.

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SECTION 5 HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features

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a. Design Data. Spruce Reservoir has a direct watershed of approximately 30 acres and impounds a reservoir with a surface area of 61 acres at normal pool level. The bypass channel passes flow from a watershed of 13.2 square miles. The capacity of the bypass channel spillway, based on the available head relative to the low spot on the embankment along the upstream end of the reservoir, was determined to be 9278 cfs as indicated in the computer output in Appendix D.

b. Experience Data. As previously stated, Spruce Reservoir is classified as an intermediate size dam in the high hazard category. Under the recommended criteria for evaluating emergency flood discharge capacity, such impoundments are required to pass full PMF.

The PMF inflow hydrograph for the bypass channel was determined utilizing the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army, Corps of Engineers. The PMF hydrograph was found to have a peak flow of 14,777 cfs. This capacity was found to be in excess of the bypass channel spillway capacity, indicating that the flood would spill into the reservoir. The portion of the inflow hydrograph in excess of the capacity of the bypass channel spillway was diverted into the reservoir. The diverted flow was routed through Spruce Reservoir starting from normal pool level. Computer input and a summary of computer output are included in Appendix D.

c. Visual Observations. On the dates of inspection, no conditions were observed that would indicate that the capacity of the bypass channel spillway would be significantly reduced in the event of a flood. However, as previously noted, clearing of brush and trees from the bypass channel is recommended.

For the reservoir drop inlet spillway, which is the only spillway facility for the reservoir, potential exists for blockage of the drop inlet or the 24-inch outlet pipe of the spillway by debris during major floods when the upstream dike may overtop, carrying debris into the reservoir. Although in evaluating the adequacy of the reservoir spillway no reduction in the discharge capacity due to blockage was considered, the owner should conduct additional detailed hydrologic and hydraulic studies to determine the need to provide emergency spillway facilities to the reservoir. d. Overtopping Potential. Various percentages of the PMF inflow hydrograph were routed through the bypass channel spillway, and it was found to pass 60 percent of the PMF without overtopping the low point on the upstream embankment. At full PMF, it was found that the embankment along the upstream side of the reservoir would be overtopped for a duration of 8.75 hours with a maximum depth of 1.3 feet over the low spot of the upstream embankment. Flows entering into Spruce Reservoir (at greater than 60 percent of the PMF) were routed through the outlet facilities, and it was found that the reservoir can pass 80 percent of the PMF without overtopping. For full PMF, the embankment would be overtopped for a duration of 5 hours with a maximum depth of 0.5 foot over a low spot along the crest of the main embankment.

e. <u>Spillway Adequacy</u>. The flood discharge capacity of the dam (80 percent of the PMF) was found to be less than the recommended capacity of full PMF. Therefore, the flood discharge capacity is rated as inadequate. Because the capacity is greater than 50 percent of the PMF, it is not considered to be seriously inadequate.

As previously noted, the owner should to determine the need to provide emergency spillway facilities to the reservoir.

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SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

(1) Embankment. As discussed in Section 3, the field observations indicated signs of surficial slumping which raised concern as to the continued stability of the dam. Therefore, further investigation of the stability of the dam in view of the observed conditions is recommended.

(2) <u>Appurtemant Structures</u>. The structural performance of the spillway structures and the bypass channel is considered to be satisfactory.

b. Design and Construction Data

(1) Embankment. As can be determined from review of the available information, it appears that the design of the embankment was based on experience. The available design and construction information does not provide any quantitative data to aid in the assessment of stability. No references were found as to whether the design included materials testing or stability and seepage analyses. Since the embankment design lacks a positive internal drainage system, some concern exists as to the location of the phreatic line through the embankment as it affects the stability. Although at this time no signs were observed to indicate that the phreatic surface is intersecting the downstream slope of the dam, in view of the indications of surficial slumping on the downstream slope (2H:1V), further investigation of the stability of the dam is considered to be advisable.

(2) <u>Appurtement Structures</u>. Based on the review of the design drawings, the structural design of the appurtement facilities is considered to be adequate.

c. <u>Operating Records</u>. The structural stability of the dam is not considered to be affected by the operational features of the dam. The reservoir operating records are kept by the owner.

d. <u>Post-Construction Changes</u>. The available records indicate that a postconstruction remedial grouting program was undertaken in 1958 to control a seepage condition which existed at the junction of the main embankment and left abutment. Records indicate that approximately 30 holes were drilled and grouted.

e. <u>Seismic Stability</u>. In view of the concern that exists as to the static stability of the dam, the seismic stability of the dam is considered to be questionable. Therefore, the seismic stability of the dam should be reassessed in conjunction with further investigation and evaluation of the embankment. Carle Contractor In

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SECTION 7 ASSESSMENT AND RECOMMENDATIONS/REMEDIAL MEASURES

7.1 Dam Assessment

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a. Assessment. The visual observations indicate that Spruce Reservoir is in fair condition. Indications of surficial slumps along the lower half of the main embankment are not considered to be a serious threat to the overall stability of the dam at this time. However, considering that the embankment lacks an internal drainage system to control seepage through the embankment and the downstream slope is considered to be relatively steep (2H:1V), further investigation of the stability of the dam in view of the observed conditions is recommended.

The flood discharge capacity of the dam was evaluated according to the recommended criteria and was found to pass 80 percent of the PMF without overtopping the main embankment of the reservoir. This capacity is less than the recommended spillway capacity of full PMF, which was based on the size and downstream hazard classification of the dam. Therefore, the spillway capacity is classified to be inadequate. However, because the spillway capacity is in excess of 50 percent of the PMF, it is not considered to be seriously inadequate. As noted before, the owner is advised to consider retaining a professional engineer to conduct additional detailed hydrological and hydraulic studies to determine the need to provide emergency spillway facilities to the reservoir.

b. <u>Adequacy of Information</u>. The available information, in conjunction with visual observations, is considered to be sufficient to make a reasonable assessment of the condition of the dam.

c. <u>Urgency</u>. The following recommendations should be implemented immediately or on a continuing basis.

d. <u>Necessity for Additional Data</u>. In view of the conditions described above it is recommended that the owner should retain an experienced professional engineer to investigate the stability of the embankment.

7.2 <u>Recommendations/Remedial Measures</u>. It is recommended that the following recommendations be implemented immediately or on a continuing basis:

1. The owner should immediately retain a professional engineer experienced in the

design and construction of dams to reevaluate the stability of the embankment in view of the observations noted. The reevaluation of the dam should include, but not be limited to, subsurface investigation, materials testing, installation of instrumentation, and seepage and stability analyses. A BARAN

- 2. In conjunction with the detailed evaluation of the dam, the crest of the dam should be surveyed and the low spots filled to design elevation.
- 3. Brush and trees in the bypass channel below the spillway should be removed.
- The operational condition of the outlet pipe gate should be evaluated and necessary maintenance performed.
- 5. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system should be developed to alert the downstream residents in the event of emergencies.
- 6. The dam and appurtenant structures should be inspected regularly and a formal maintenance manual should be developed for the continued maintenance of the dam.

APPENDIX A CHECKLIST

CHECKLIST VISUAL INSPECTION PHASE I

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APPENDIX A

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CHECKLIST VISUAL INSPECTION PHASE I

NAME OF DAM Spruce Reservoir	COUNTY Union	Union	STATE Pennsylvania	NDI I.D. PA-487 ID# DER I.D. 60-7
TYPE OF DAM Earth		HAZARD CA	HAZARD CATEGORY High	
DATE(S) INSPECTION April 28, 1980	WEATHER Rainy	Rainy	TEMPERATURE 50s	
POOL ELEVATION AT TIME OF INSPECTION 669.4+ M.S.L.	++ 699		TAILWATER AT TIME OF INSPECTION 626±	CCTION 626± M.S.L.

INSPECTION PERSONNEL:

REVIEW INSPECTION PERSONNEL: (April 30, 1980)

B. Erel E. D'Appolonia W. T. Chan L. D. Andersen

J. H. Poellot

B. Erel

OWNER'S REPRESENTATIVE:

Mr. Bruce E. Juergens, Director, Engineering Mr. Edward N. Russell Production Superintendent Mr. William E. Hutcheson Director of Risk and Materials

Management

B. Erel

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VISUAL INSPECTION PHASE I

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VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
surface chacks	None	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None	
SLOUGHING OR EROSION OF Embannment and abutment Slopes	There are indications of surficial sloughing and erosion along the embankment at the downstream side of the reservoir. See Plate 8 for location.	
VERTICAL AND HORIZONTAL Alignment of the crest	See Plate 9.	
RIPRAP PALLURES	See Plate 8 for locations of shoreline erosion.	Adequate riprap should be provided at areas where shoreline erosion is occurring.

Page A2 of 9

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VISUAL INSPECTION PHASE I

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	REMARKS OR RECOMMENDATIONS					
EMBANKOGENT	OBSERVATIONS	No signs of distress.	A swampy area exists along the toe of the main embankment in the vicinity of its junction with the left abutment. An associated seepage is estimated to be 10 to 20 gallons per minute.	Reservoir levels are remotely monifored and recorded at the water treatment plant.	None	
	VISUAL EXAMINATION OF	JUNCTION OF EMBANNMENT AND ABUTHENT, SPILLWAY AND DAM	ANY NOTICEABLE SEEPAGE	STAFF CACE AND RECORDER	DRAINS	

Page A3 of 9

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Page A4 of 9

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	REMARKS OR RECOMMENDATIONS					The owner should evaluate the operational condition of the outlet pipe sluice gate and perform necessary maintenance.
OUTLET WORKS	OBSERVATIONS	Only the downstream end of the pipe was visible.	Submerged	Outlet pipe discharges into a plunge pool.	Zarth chamel	Flow through the outlet pipe is controlled by a sluice gate at the outlet tower. The operational condition of the sluice gate was not observed.
	VISUAL EXAMINATION OF	CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	INTAKE STRUCTURE	OUTLET STRUCTURE	OUTLET CHANNEL	EMERGENCY GATE

VISUAL INSPECTION PHASE I

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VISUAL INSPECTION PHASE I UNCATED SPILLMAY

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VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	Bypass channel spillway weir was submerged. The structural condition could not be assessed.	
APPROACH CHANNEL	Submerged	
DISCHARGE CRANNEL	Earth channel partially blocked by vegetation.	
BRIDGE AND PIERS	None	

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Page A5 of 9

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REMARKS OR RECOMMENDATIONS					
OBSERVATIONS	Not applicable	Not applicable	Not applicable	Not applicable	Not applicable
VISUAL EXAMINATION OF	CONCRETE SILL	APPROACH CHANNEL	DISCHARGE CHANNEL	BRIDGE PIERS	GATES AND OPERATION EQUIPHENT

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VISUAL INSPECTION PHASE I CATED SPILLWAY

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VISUAL INSPECTION PHASE I INSTRUMENTATION

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VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
NONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
P I EZOMET EKS	Nore	
OTHER	None	

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Page A7 of 9

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VISUAL INSPECTION PHASE I RESERVOIR

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PERMANANT AB BECAMENNATIONS	RETAKED UN NEGENIGIANT FURT				-	
RESERVOIR	OBSERVATIONS	Moderately steep. No significant shoreline erosion was noted.	Unknown	None		
	VISIAL EXAMINATION OF	SLOPES	SEDIMENTATION	UPSTREAM RESERVOIRS		

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Page A8 of 9

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Page A9 of 9

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REMARKS OR RECOMMENDATIONS				
ORSERVATIONS	No features pertinent to the safety of the dam.	No features pertinent to the safety of the dam.	Approximately 5 homes within a one-mile reach downstream from the dam are considered to be within the potential flood plain of Spruce Reservoir in the event of a dam failure. Population: approximately 20.	
VISUAL EXAMINATION OF	CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	SEAOUS	APPROXIMATE MUMBER OF HOMES AND POPULATION	

VISUAL INSPECTION PHASE I DOMNSTREAM CHANNEL

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(OBSTRUCTIONS, DEBRIS, ETC.)	STOPES

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APPENDIX B

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CHECKLIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION AND HYDROLOGIC AND HYDRAULIC PHASE I

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Page Bl of 5

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ITEM	REMARKS
AS-BUILT DRAWINGS	Available in Commonwealth files.
REGIONAL VICINITY MAP	See Plate 1.
COMSTRUCTION HISTORY	The dam was designed and constructed by American Water Works Service Company, Inc., with completion in 1957.
TTPICAL SECTIONS OF DAM	See Plates 3 and 4.
OUTLETS - PLAN - DETAILS - CONSTRAINTS - DISCHARGE RATINGS	See Platea 5. 6. and 7.

APPENDIX B

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CHECKLIST ENCINERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

NAME OF DAM Spruce Reservoir 1D# NDI I.D. PA-487 DER I.D. 60-7

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CHECKLIST ENCINFERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

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ITDA	REMARKS
RAINFALL/RESERVOIR RECORDS	Rainfall and reservoir records are maintained by the owner.
DESICN REPORTS	None prepared
CEDLOCY REPORTS	None prepared
DESICH COMPUTATIONS HYDROLOCY & HYDRAULICS DAM STABILITY SEEPACE STUDIES	None reported
MATERIALS INVESTICATIONS BORING RECORDS LABORATORY FIELD	None reported

Page B2 of 5

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CHECKLIST ENCINFERING DATA Design, construction, operation Phase 1

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17.04	REMARKS
POST CONSTRUCTION SURVEYS OF DAM	None reported
borrow sources	Unknown
MONITORING SYSTEMS	The reservoir level is remotely monitored and recorded at the water company's treatment plant in Milton, Pennsylvania.
MODIFICATIONS	None reported
HIGH POOL RECORDS	Flow into Spruce Remervoir is controlled.

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Page B3 of 5

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CHECKLIST ENCINEERING DATA DESIGN, CONSTRUCTION, OPERATION PHASE I

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ITEM	REMARKS
POST CONSTRUCTION ENCINEERING STUDIES AND REPORTS	None reported
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported
MAINTENANCE OPERATION RECORDS	Maintained by the owner.
SPILLWAY PLAN Sections Details	See Plate 2.
OPERATING EQUIPMENT Plans and details	See Plate 7.

Page B4 of 5

CHECKLIST ENGINEERING DATA HYDROLOGIC AND HYDRAULIC

DRAINAGE AREA CHARACTERISTICS: 13.2 square miles (woodlands) ELEVATION, TOP OF NORMAL POOL AND STORAGE CAPACITY: 672 (1535 acre-feet) ELEVATION, TOP OF FLOOD CONTROL POOL AND STORAGE CAPACITY: 676 (1780 acre-feet) ELEVATION, MAXIMUM DESIGN POOL: 676 ELEVATION, TOP OF DAM: 676 (as designed); 675.8 (measured low spot) SPILLWAY: (BYPASS CHANNEL SPILLWAY)

- a. Elevation 672
- b. Type Ogee overflow section
- c. Width 212 feet (perpendicular to flow direction)
- d. Length Not applicable
- e. Location Spillover Adjacent to spillway
- f. Number and Type of Gates None

OUTLET WORKS:

- a. Type 24-inch cast-iron pipe
- b. Location Right of center of main embankment
- c. Entrance Inverts 635.7
- d. Exit Inverts 630±
- e. Emergency Drawdown Facilities 24-inch outlet pipe

HYDROMETEOROLOGICAL GAGES:

- a. Type Rainfall gage
- b. Location Dam site
- c. Records <u>Maintained</u> by the owner

MAXIMUM NONDAMAGING DISCHARGE: 9300+ cfs (bypass channel spillway capacity)

Page B5 of 5

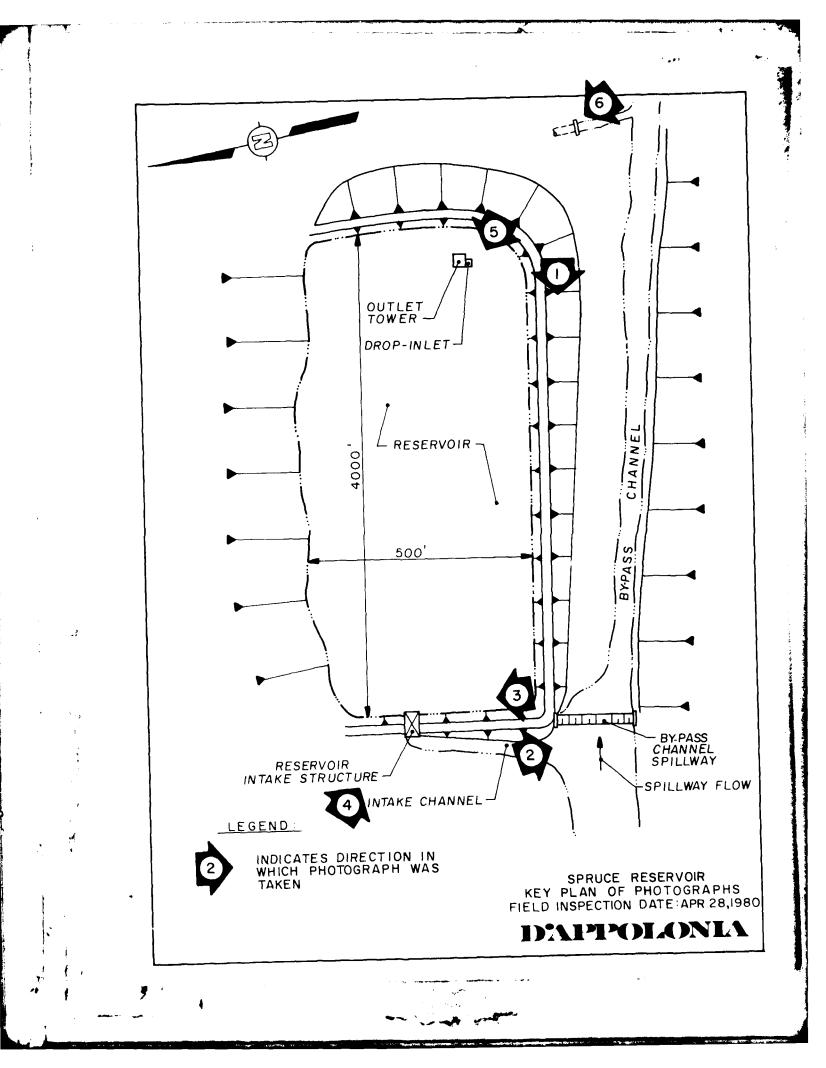
APPENDIX C PHOTOGRAPHS LIST OF PHOTOGRAPHS SPRUCE RESERVOIR DAM NDI I.D. PA-487 DER I.D. 60-7 APRIL 28, 1980

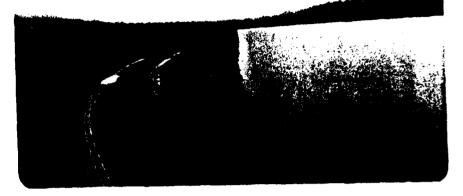
PHOTOGRAPH NO.

.2

DESCRIPTION

1 Crest of dam (looking upstream) along bypass channel (bypass channel left of crest). 2 Bypass channel overflow section. 3 Upstream diversion dike. Righthand side: reservoir. Lefthand side: diversion channel. Reservoir intake structure. Fore-ground: diversion channel. Back-4 ground: reservoir. 5 Reservoir outlet structure. Downstream end of reservoir outlet 6 pipe.





Photograph No. 1 Crest of dam (looking upstream) along bypass channel (bypass channel left of crest).



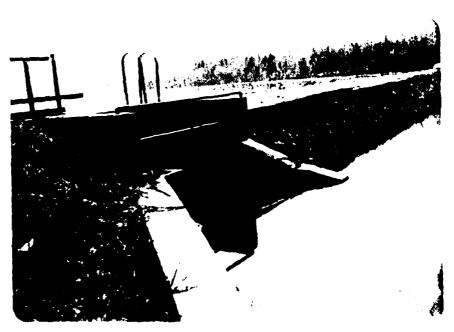
Photograph No. 2 Bypass channel overflow section.



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Photograph No. 3

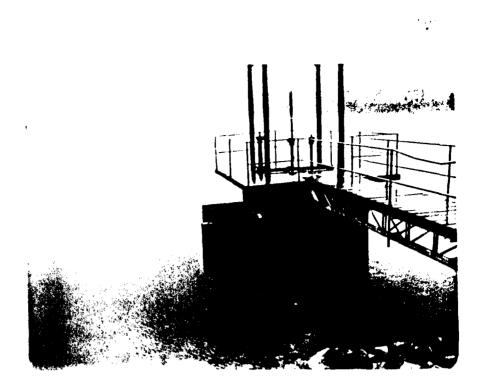
control diversion dike. Righthand side: conceptor continued side: diversion channel.



Photograph No. 7

Respondent Entare seructure. Conservand: Severalou channels Backgroundt reservoir. ÷ 'n

Jacob Street



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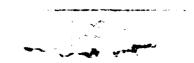
Photograph No. 5 Reservoir outlot structure.



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APPENDIX D Hydrology and hydraulics analyses

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HYDROLOGY AND HYDRAULIC ANALYSIS DATA BASE

NAME OF DAM: Spruce Reservoir (NDI I.D. PA-587)

STATION	1	2	3	4	5
Station Description	Diversion Dike	Diversion Spillway	Spruce Reservoir		
Drainage Area (square miles)	13.2	-	~0		
Cumulative Drainage Area (square miles)	13.2	13.2	13.2		
Adjustment of PMF for Drainage Area (%)	(ZONE 2)				
6 Hours	117	-	-]		
12 Hours	127	-	-		
24 Hours	141	-	-		
48 Hours	151	-			Į
72 Hours	-	-	-		
Snyder Hydrograph Parameters					
Zone ⁽³⁾	18	-	-		
$C_p/C_t^{(4)}$	0.50/2.10	-	-		
L (miles) ⁽⁾	9.9	-	-		ļ
L _{ca} (miles) ⁽⁵⁾	3.6	- 1	-		1
$t_p = C_t (L + L_{ca})^{(i, 3)}$ (hours)	6.1	-	-		
Spillway Data					
Crest Length (ft)	-	212	See spillway		
Freeboard (ft)	-	5.1	rating calculation		
Discharge Coefficient	-	3.8			
Exponent	-	1.5			

PROBABLE MAXIMUM PRECIPITATION (PMP) = 23.0 INCHES/24 HOURS⁽¹⁾

(1) Hydrometeorological Report 33 (Figure 1), U.S. Army, Corps of Engineers, 1956.

(2) <u>Hydrometeorological Report 31</u> (Figure 2), U.S. Army, Corps of Engineers, 1956.
 (3) <u>Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients (C_p and C_t).
 (4) Snyder's Coefficients.
</u>

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(5) L_{ca} = Length of longest water course from outlet to basin divide. L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.

DIVERSION DIKE STORACE VS. ELEVATION

ELEVATION	AH, FEET	AREA (ACRES) ⁽¹⁾	AVOLUME (ACRE-FEET) ⁽²⁾	STORAGE (ACRE-FEET)
672	8	0.9	40.1	0
680		11.0		40.1
			1 1	

(1) Planimetered from USGS maps.

(2) $\Delta Volume = \Delta H/3 (A_1 + A_2 + \sqrt{A_1A_2}).$

PAGE D1 OF 8

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44 70.0 680. U 84.1 n. 64 122 0.0004 1.43 678.0 82.5 DJVERT HYDROSRAPH ABOVE ELEVAIION 677.1 DAT CHEST LO4MEST SPOT 1 9278.4 16ビビーひ 2104.0 2700.0 3000.0 3230.0 676.3 676.4 676.5 676.6 CALCULATION OF SWYDER INFLOW HYDROGRAPH TO SPRUCE RUN DAM 06-0 677.0 .05 7 ROUTING FLOW THROUGH SPRUCE RUN DAM (NDI-I.D.PA.587) 1 DIVENTED HYDROGRAPH IJ SPRUCE RUN RESERVOIR ROUTING DIVERTED FLOW THROUGH SPRUCE RUN RESERVOIR -672.0 676.0 80.9 0**.**80 1.0 -672.0 675.0 80.0 0.70 151 COMPUTER INPUT OVERTOPPING ANALYSIS 0.60 13.2 864.0 679.2 674.0 13299. 14777. 0.2522 J.2934 1.5 4400.0 1500.0 1.5 800.0 750.0 678.2 673.5 78.8 J.59 127 2.0 1600.0 11921. D.1777 5.5 1.5 1.0201 1.676 1.5 675.0 679.0 673.U 48.3 117 ч. В 13.2 u.30 672.5 17.1 17.1 17.1 680.3 15.7 80.0 80.0 676.0 212.0 2.7 425.1 677.7 23. J J.5" -0,-05 68.0.0 11. J 9278.4 ¢ RETRIEVE 10345. 0.0873 A4 SAFETY VERSION JULY 1978 Last 4301/1/Cation of APR 2 ****************************** FLUD HTURDER PACKAGE (HEC-1) ************************** 0.20 Y4 672.0 T5 0.0 \$A 50.6 \$E 672.0 \$1 400.0 \$4 675.9 K 99 300 ·... 672.0 672.0 10 677.1 10 677.1 10 677.1 10 677.1 ~ + **6**") 5 ~ 672.0 +3 9278. \$0 675.9 يد ج : c 7 ĩ F 5 ĩ Ľ, 4 5 5 * 5 t Ş ÷ UAT SAFETY VERSION 2525

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	S NO	84110 7 .80			452. 12.791(11369. 321.93)(452.	2.1310		
	C ONPUT & T I	8.4.110 6 .70	14344. 292.923	10345. 292.861(43. 2.63)(10250.2434	93. 2.63) (.2010		
	0 E CONOMI C S E CONDI	\$0.	8866. 251.75)(8866. 251.05)(0.00.0	8866. 251.US)(0.00.0	0.00.0		
	PLAN-RATI HETERS PER COMETERS)	LIED TO FL Ratio 4 .50	7388. 269.21)(73×7. 209.19)(3. 0, ru) (7387. 209.19)(υ. 0,00,0	0.00.0	ARY	
· · ·	DU) SUMMARY FOR MULTIPLE PLAN-RATID FCONOMIC COMPUTATIONS FFLT PER SECOND (CUBIC MFTERS PER SECOND) Suuart miles (Souare Kilometers)	RATIOS APPLIED TO FLOMS Ratio 3 Ratio 4 Ratio .43 .50	5911. 167.37) (5910. 167.35) (0.00.0	5910. 167.35) (0. 0.00. (0. 0.00.0	FLOOD ROUTING SUMMARY PAGE D3 OF 8	
	SUMMARY FO I PER SECO Are miles	RATIO 2.30	4433. 125.5336	4432. 125.51) (4432. 125.511 (9.00.0		FLOOD ROUTIN PAGE D3	
	Н РЕКІОР) С'JHIC FEE Феа IN Sau		2955. 53.6936	2455. 83.67)(ים. נייזמי נ	2455. 83.67)(0.00.5	0. 0.00.0		
	GE (ENU): PEKIO Flum I PEKIO Anemi	PLAN	- ~	۴Ŭ	- `	~ `	÷ ~	- ~		بالم
	AND SIGRA	AREA	13.20 34.19)	13.20	13.23	13.20	0, 0 0, 0	(0C*0		an a
	PEAK FLOW AND STORAGE (END FLOWS I	51 A 1 1 0 N	- ⁻	~~~	~~~~	ۍ ۲	۔ ۲			
		UPERATION	NYDRJËRAPN AT	KJUTED TJ	DIVENSION TU	NYDROGRAPH AT	NTDRUGRAPH AT	ROUTED TO		

SUMMARY OF DAM SAFETY ANALYSIS

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	TIME OF Failure Hours	00.0	0.00	0.00	00.0	00.0	00.0	0.0	00.00	
TOP OF DAM 677.10 16. 9278.	TIME OF Max Dutflow Hours	65°26	15.50	45.50	45.50	45.50	45.50	45.50	45.50	
	DURATION DVER TOP MJJRS	0.00								
SPILLMAY CREST 572.00 0. 0.	MAKI4UM 0017flow C45	.2355	4432.			1 1 5 1 5	11821.	96411	1177	
	MAXINUM STORAGE AC-FT	*	• •							.03
INTIIAL VALUE 672.0u 0. 0.	MAKIMU4 DEPTH DVER DAM	0.00	00.0	00°0					* · ·	1.50
ELEVATION STORAGE OUTFLOW	MAXIMUM Reservoir N.S.Elev	674.38	675.12	A75.78	676.38	676.95	677.45	5// ° H 6	613.14	678.47
	8 1 1 0 3 6 3 F 4		(,,	. 4.1	. 5.1	• • •	12.	- P -	6.6	1.03
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PAGE D4 OF 8

SUMMARY OF ROUTING THROUGH BYPASS CHANNEL SPILLWAY

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PAGE D5 OF 8

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SUMMARY OF ROUTING THROUGH SPRUCE RESERVOIR

	TIME OF Failure Hours	
ТОР ОГ ДАМ 675.90 245. 81.	TIME OF Max Outflow Hours	0.00 0.00 0.00 0.00 0.00 4.7.75 4.25
	DURATION Over top Hours	696966688 6969666688
SPILLWAY CHEST 672.00 0. 0.	84X 38 UN 017 FL 04 CFS	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	MAXIMUM Storage Ac-ft	0000 0000 0000 0000 0000 0000 0000 0000 0000
INITIAL VALUE 672.03 0.	MAXJMUM DEPTH Over Dam	000 0000 00 000000000000000000000000000
ELEVATION STORAGE OUTFLOW	MAXIMUM RESERVOIR M.S.ELEV	672.00 672.00 672.00 672.00 672.00 672.21 672.21 672.21 672.21
1	RA 110 01 PMF	200 200 200 200 200 200 200 200 200 200
PLAN		

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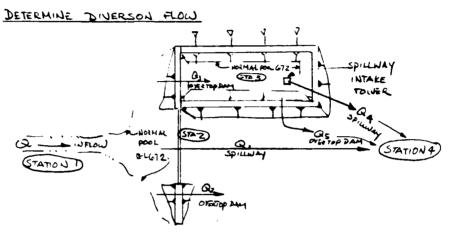
SUMMARY OF DAM SAFETY ANALYSIS

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DAPPOR CONSULTING ENG				\bigcirc
By WTC Date 7/1/180	Subject SPRUCE	RUN DAME	RESERVOIS Sheet No	1_ of 3_
Chkd ByDate	DINERSON	FLOW	Proj. No	79-543-24



DAH CREST	(LOWE	st D	>	677.10		
Spillway CRES	ī		=	672.00		<i>c</i> 1.
THOUR	= G	s	=	C, L, H, ^{1.5}	= (3·8)(212)(5·1) ^{1·5} =	9278

FROM PRELIMINARY HEC. 1 RUNS, Q>0 @ 65% PHF OR GREATER

LAKE		DISCHARGE				+3 CARD	+4 CARD		
ELEVATION	Q.	C, L, H, 'S	Q.	C.L. H.		0-0-0	DISQ(1)	FRACD()	
		(38)(212)(H,)15	=(2.7)(20)(H2)15		Q ⁽³⁾ Q-a,-a ₂		Q-Q,	Q,	
	н, ⁻)	Q,	H2 ⁽²⁾	Q,		Q,		Q-Q.	
	Fr	43	FT	નક	45	ofs	cfs	ريد - ين	
677.45	5 45	10250	-	(10343	93	1065	0.0873	
677.84	5.84	11369	-	-	11821	452	2543	0.1777	
678.14	6.14	12257	014	28	13299	1014	4021	0.2522	
678.40	640	13044	040	137	14777	1397	5499	0.2904	
NOTES - DVRMX, SET @ 1600 -43									

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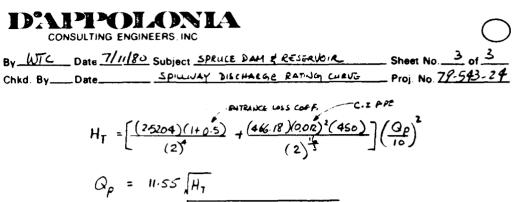
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1) H. : LAKE ELEVATION - 672 .

(2) H2 = LAKE ELEVATION -678 (EVEN. GT8 = CREST LEVEL OF BUBANKHENT, RIGHT OF SPULLAY) (3) Q = IN FLOW OBTAINED FROM HELL RUNS @ 70%, 8% 9% and 100% PMF

PAGE D6 OF 8



FOR QW=QP

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(48.3) (LAKE ELEVATION - 672) 15 = (11 55) LAKE ELEVATION - 627

then	Lake el	EVATION =	673.4	50m 673.5
LAKE	EQ-1	EQ.2	Spilling	REMARK
ELEVATION	QN		DISCHARGE	
	બંડ	ct i	<u>د+،</u>	
672	0		Ø	SPILL WAY (REST CONTROL CHANGED
6725	17.1		171	
673	48.3		483	
6735	_887	78.8	78.8	CONTROLCHANGED
674		79.2	792	
6 JS		800	800	
676		80.9	829	DAM CREST
677		81.7	81.7	DAM CREST
678		82.5	82.5	
679	<u> </u>	83.3	833	

then Lake ELEVATION = 673.4 say 673.5

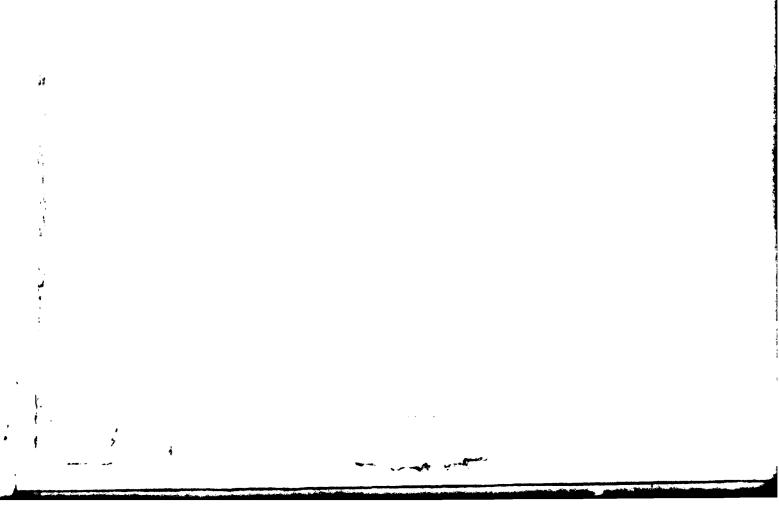
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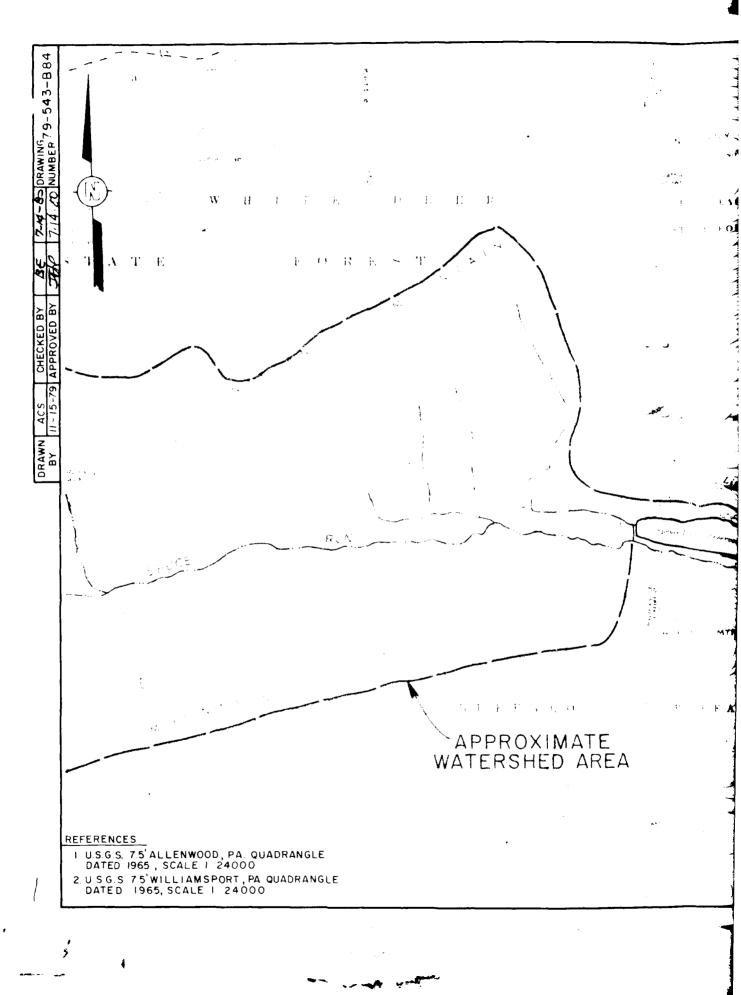
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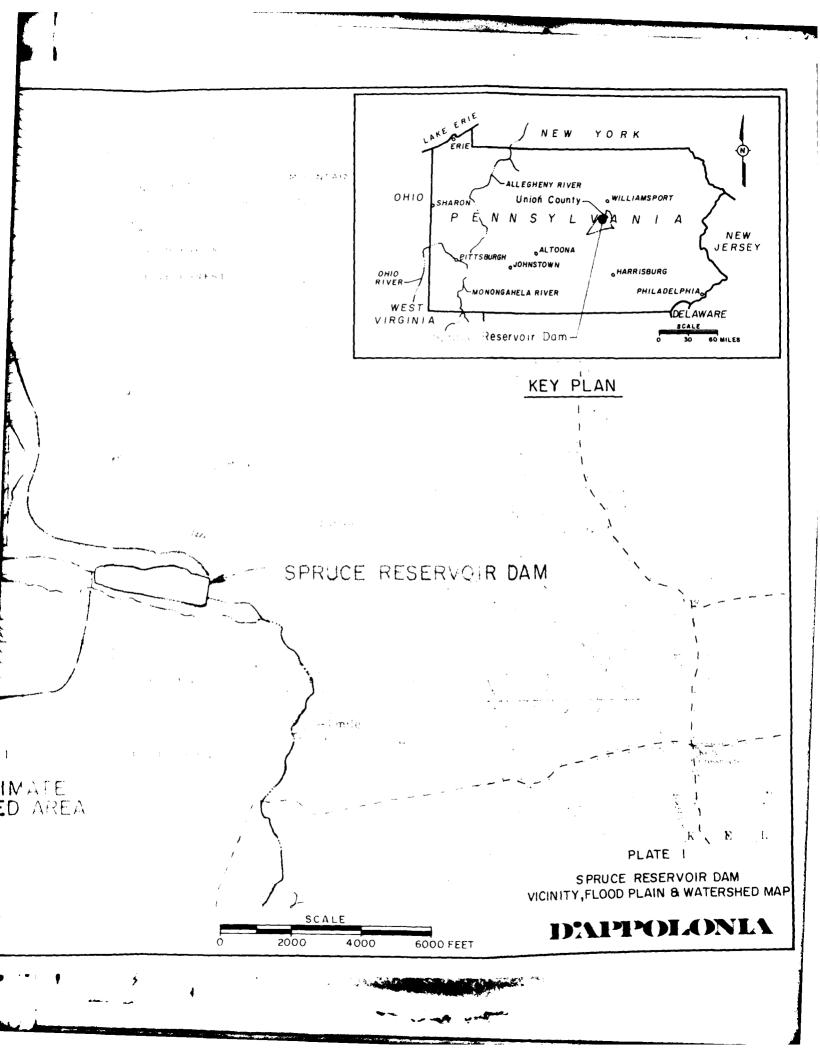
APPENDIX E PLATES

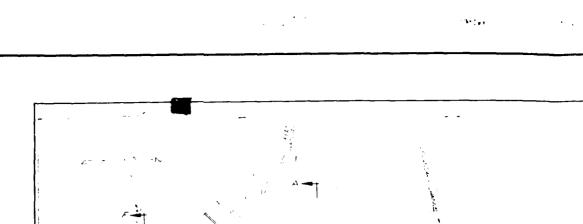
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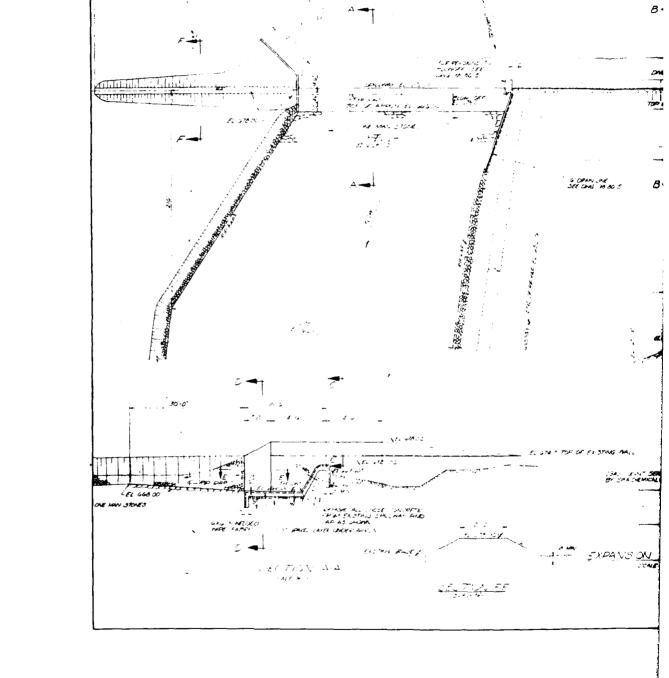
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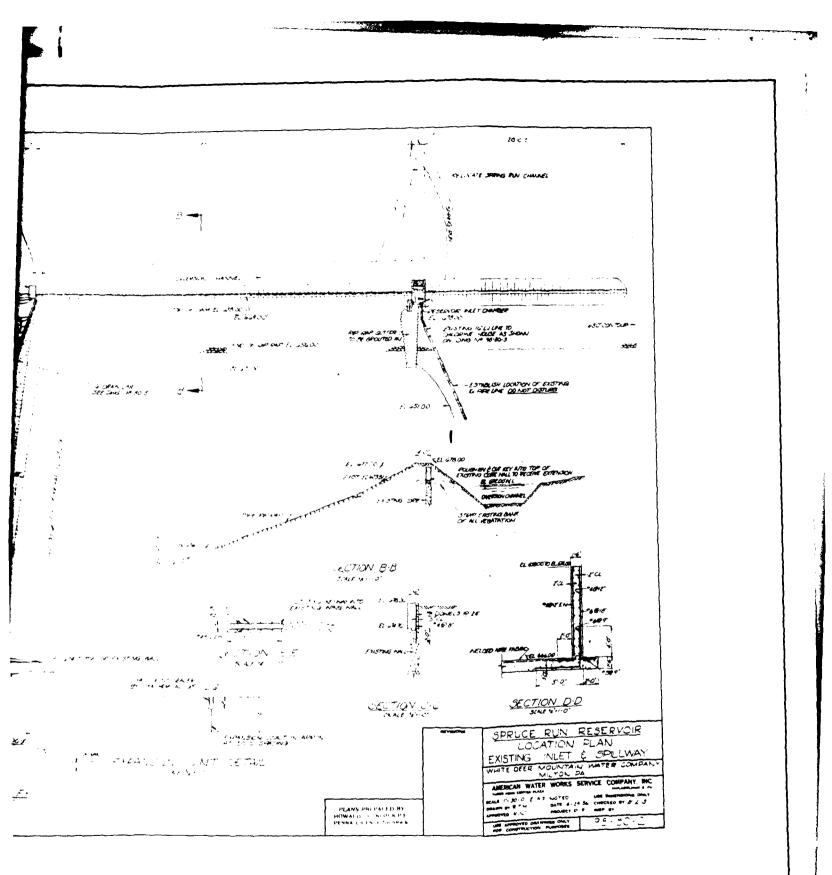
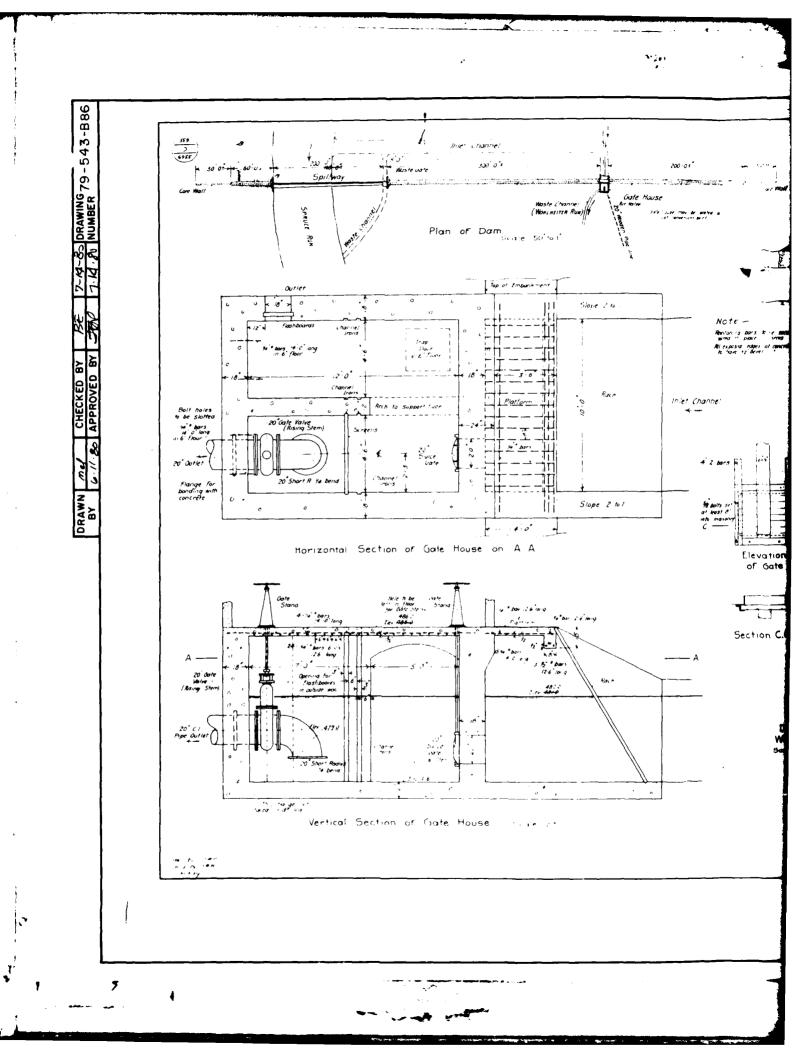
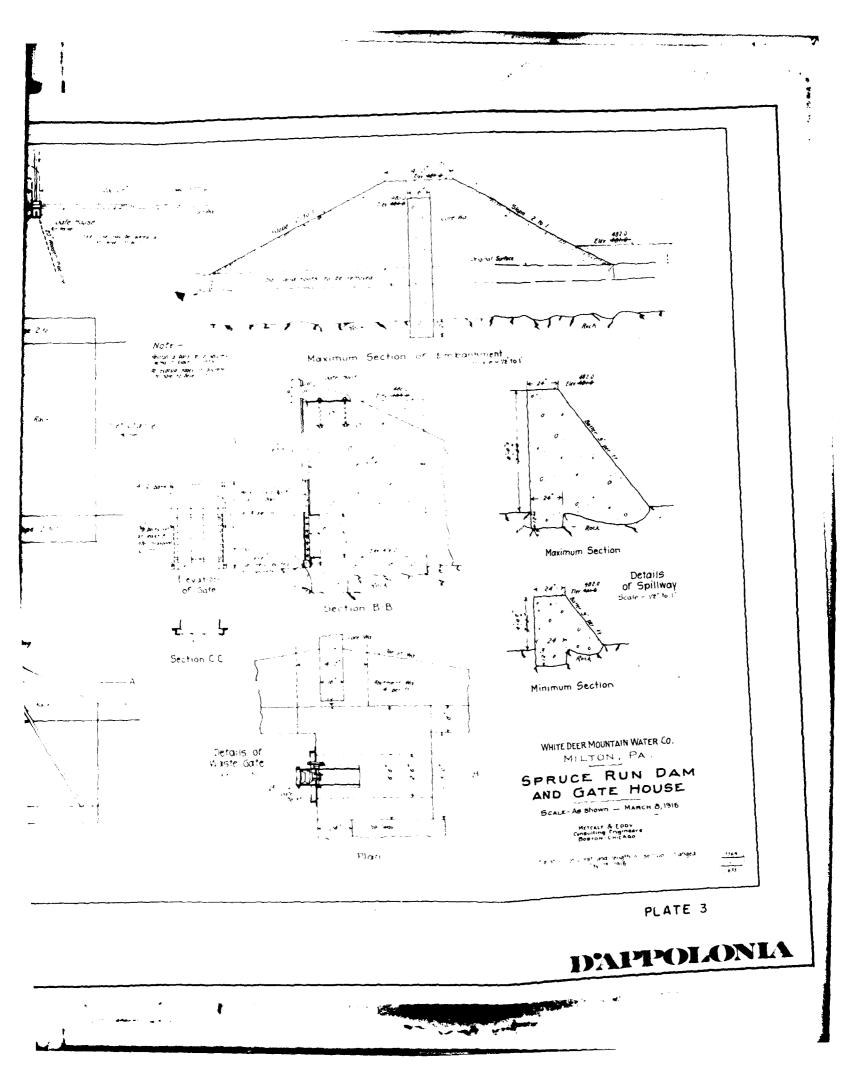
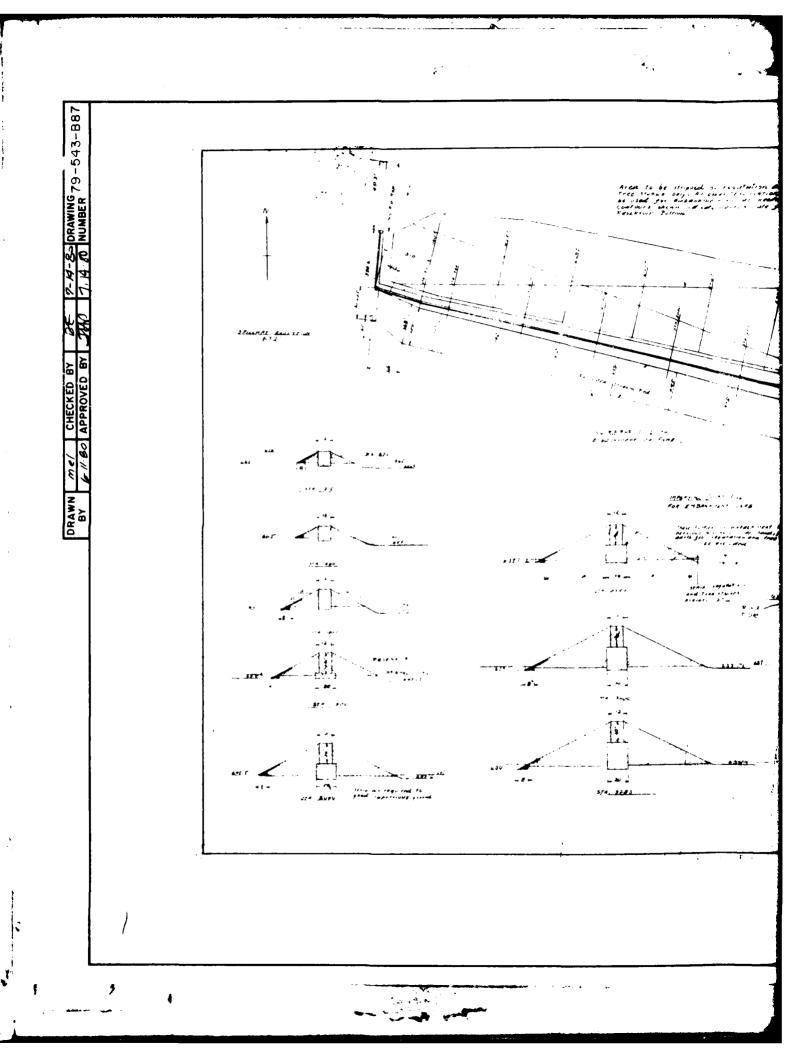


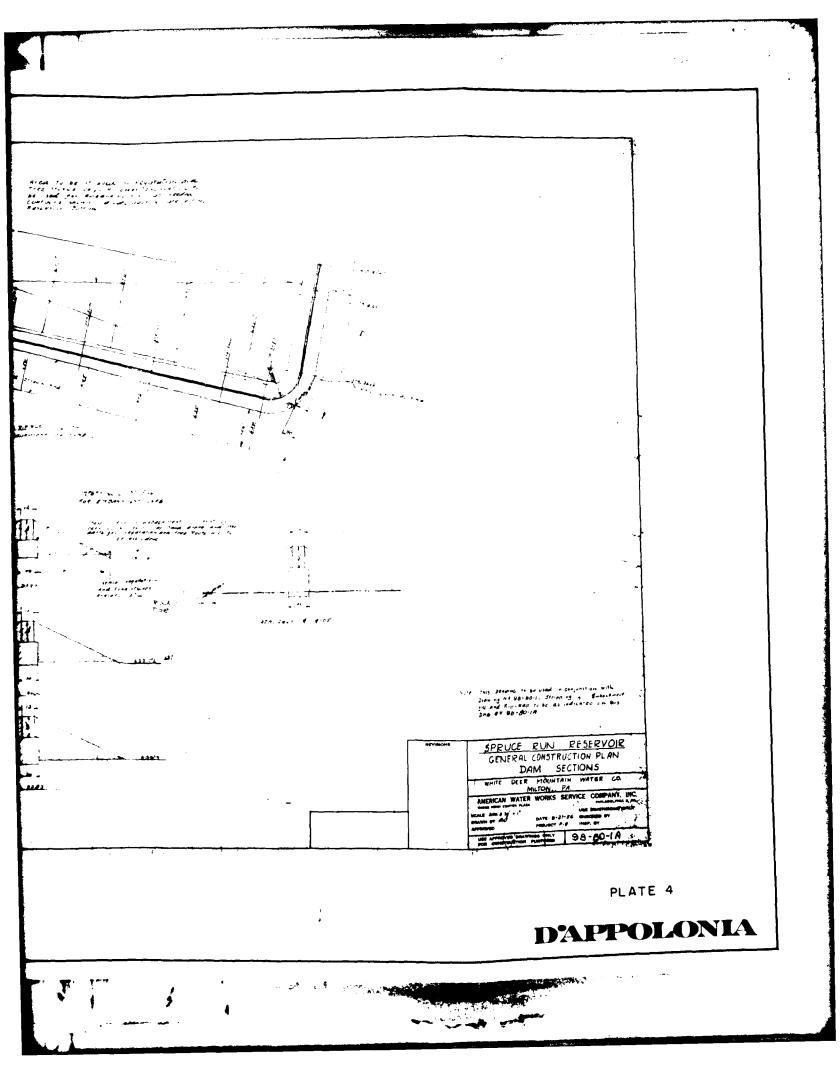
PLATE 2

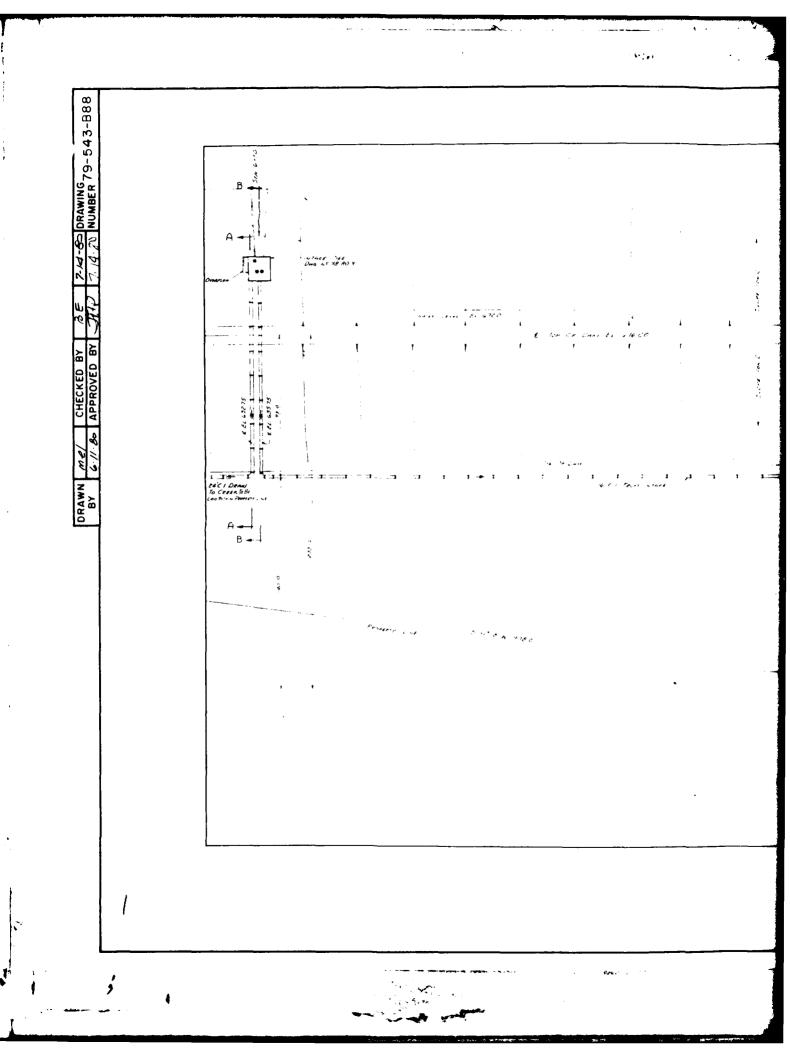
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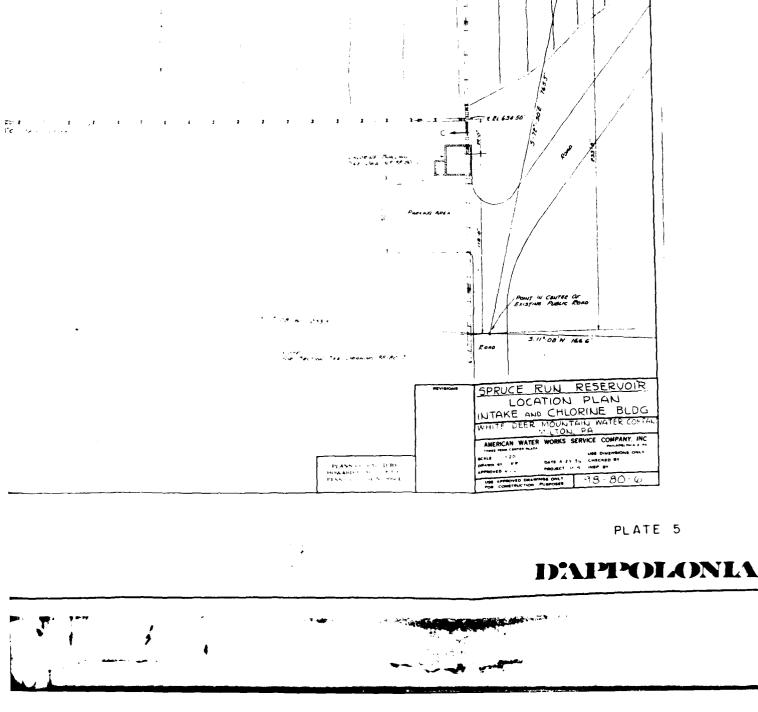












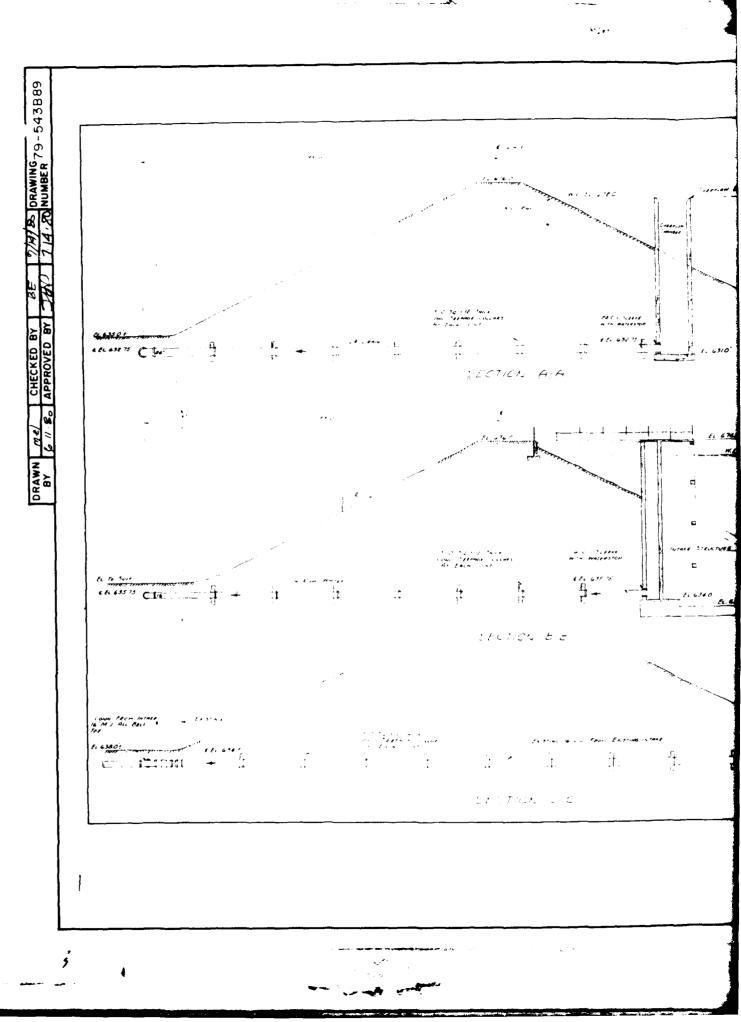
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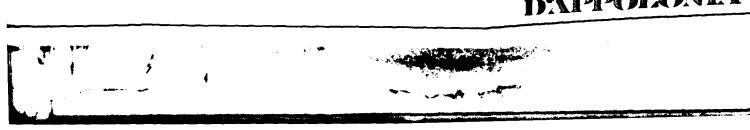
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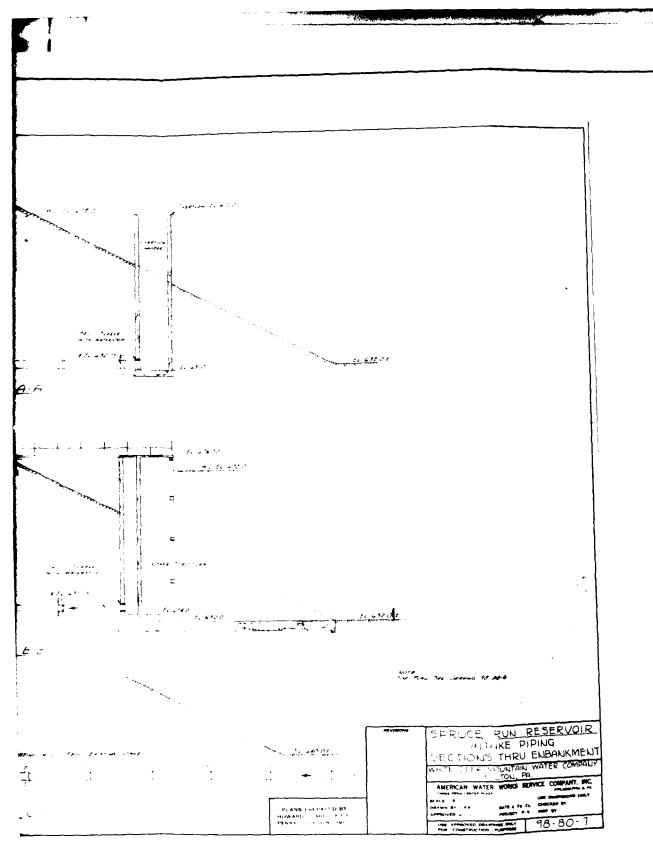


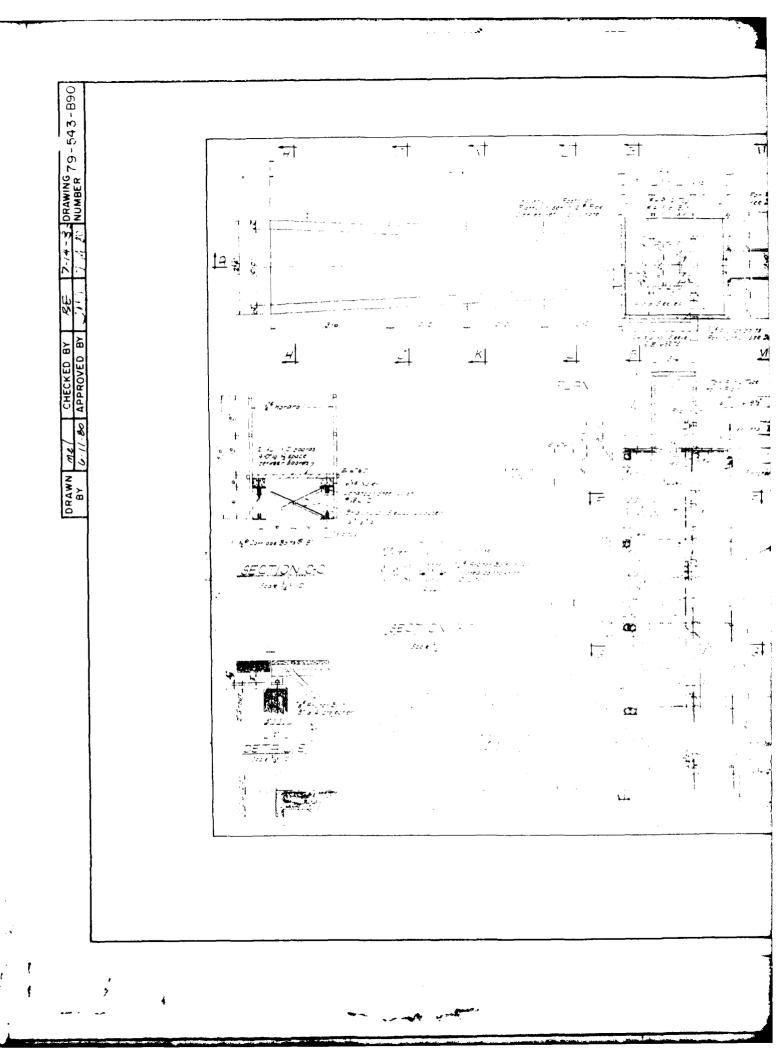
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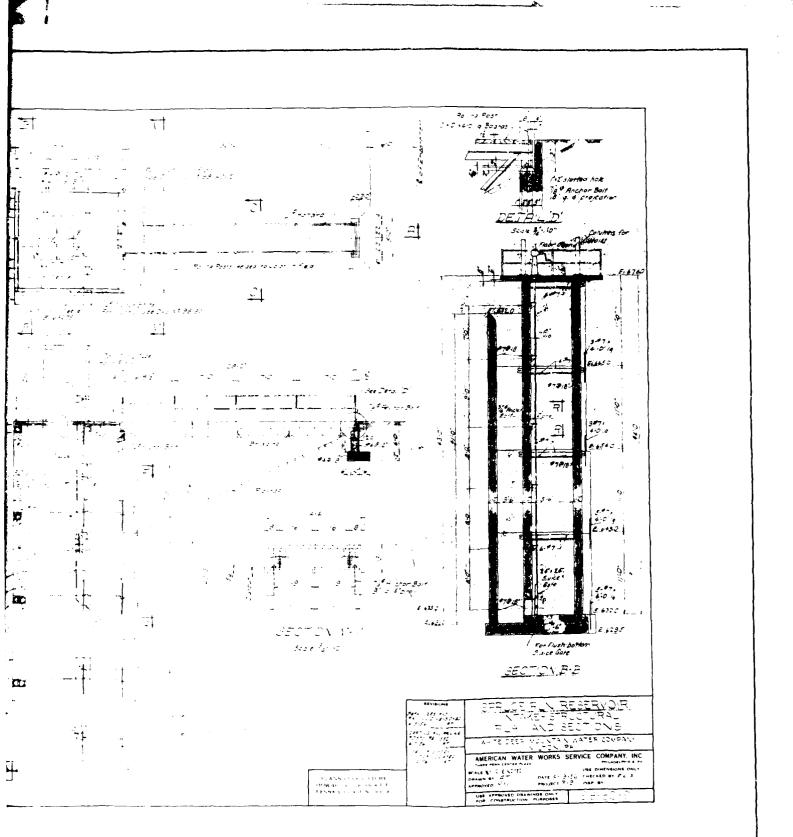


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PLATE 6



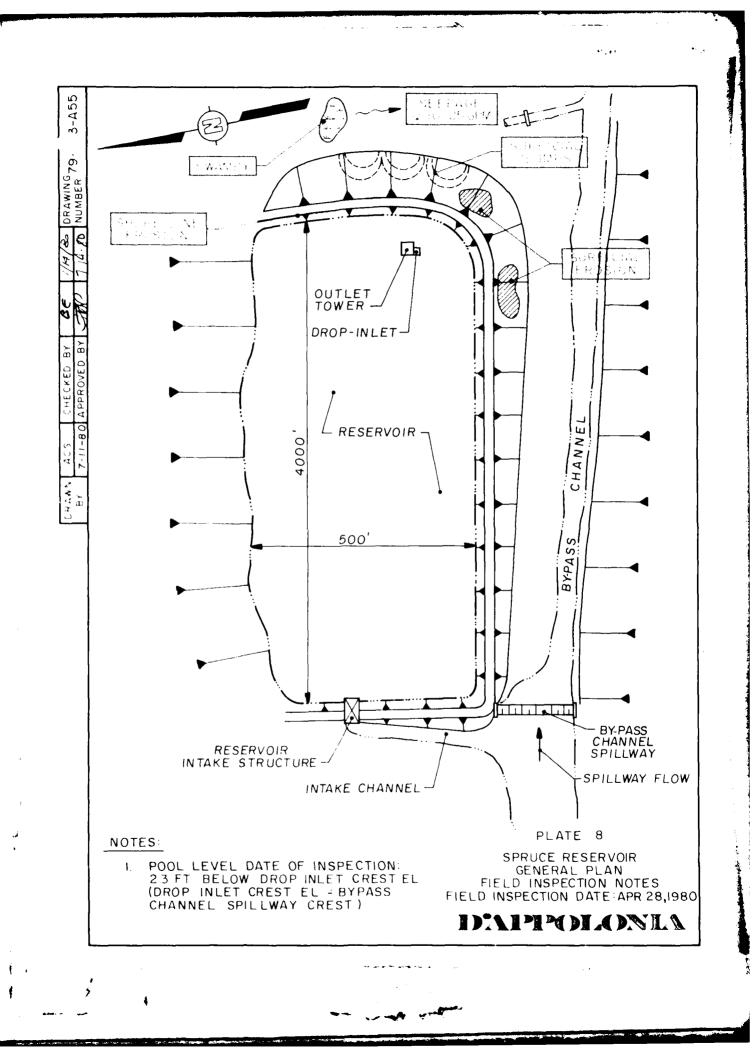


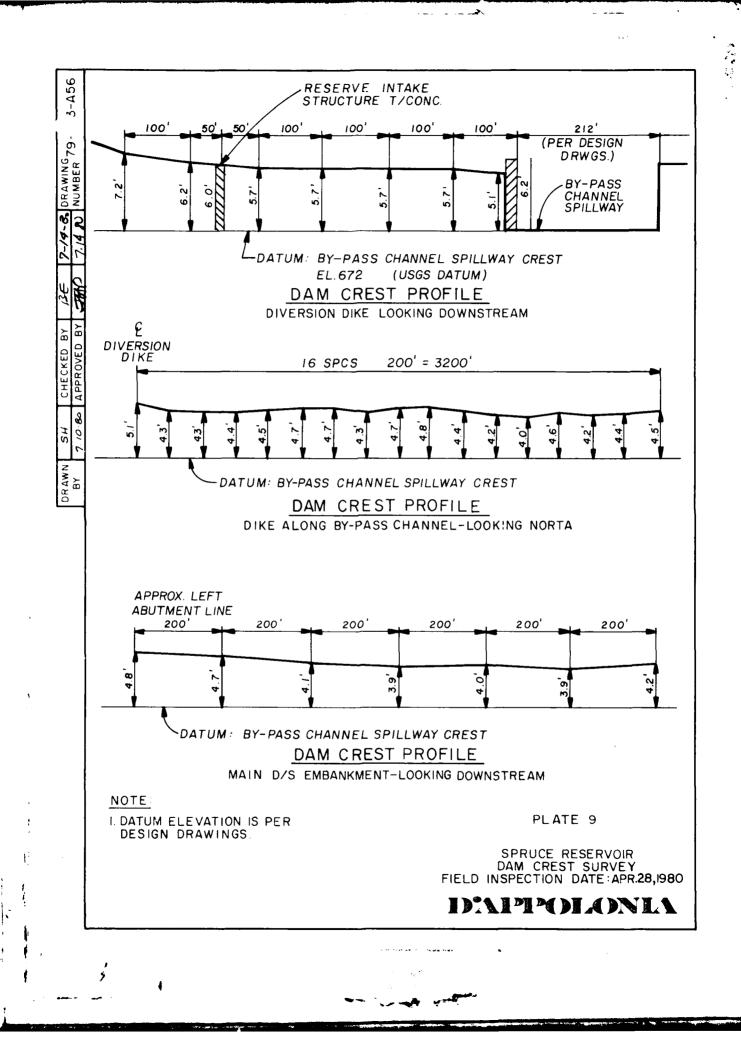


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PLATE 7

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APPENDIX F REGIONAL GEOLOGY

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APPENDIX F REGIONAL GEOLOGY SPRUCE RESERVOIR

Spruce Reservoir is located in the north-central section of the Valley and Ridge Province. The Valley and Ridge is an area that has undergone moderate to intense folding of strata. The dam is located near the nose of the Buffalo Mountain Anticline which plunges to the east. The dam lies near the contact of the bloomsburg and McKenzie formations and the Clinton Group.

The Clinton Group is composed primarily by the Rose Hill Formation, a reddish-purple to greenish-gray fossiliferous shale. The shale is fissile and well jointed. The McKenzie Formation is a fissile greenish-gray shale with well-developed joints. The Bloomsburg Formation is comprised of red shale and siltstone with local occurrences of Sandstone. Bedding is fissile to thin and joints are well developed and open.

Strata dip moderately to the north at the dam. Thus, along the north side of the reservoir, strata dip away from the reservoir. Strata dip toward the reservoir along the emergency spillway, an unfavorable situation which enhances the possibility of sliding along bedding planes. However, sliding into the reservoir is minimized by the relatively wide emergency spillway.

