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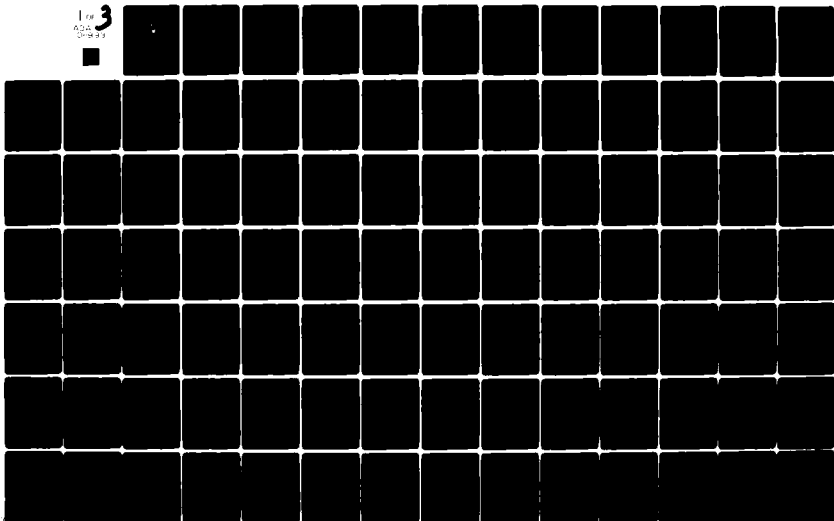
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ECTRACE - THREE DIMENSIONAL ACOUSTIC
RAY TRACE PROGRAM

by

Robert Neal Christianson

Luis Ricardo Erazo

March 1980

Thesis Advisor:

A. B. Coppens

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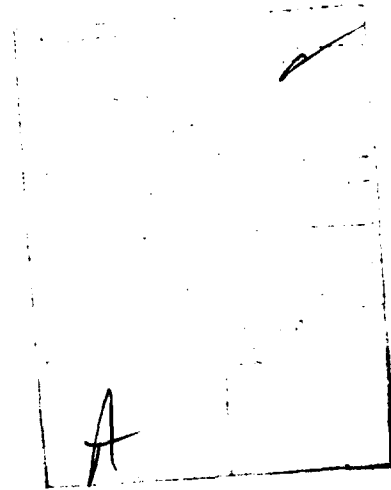
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Acoustic ray paths in the ocean are known to exhibit significant horizontal deflections after repeated reflections from the bottom. The effect may be quantitatively and qualitatively observed through a ray trace model which permits a change in direction of the vertical plane of propagation as a function of bottom slope and grazing angle. ECTRACE is a family of computer programs which traces a bundle of rays in three dimensions and utilizes bottom depth values as a portion of its input. Included are			

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ECTRACE - Three Dimensional Acoustic Ray Trace
Program

by

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Submitted in partial fulfillment of the
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ABSTRACT

Acoustic ray paths in the ocean are known to exhibit significant horizontal deflections after repeated reflections from the bottom. The effect may be quantitatively and qualitatively observed through a ray trace model which permits a change in direction of the vertical plane of propagation as a function of bottom slope and grazing angle. ECTRACE is a family of computer programs which traces a bundle of rays in three dimensions and utilizes bottom depth values as a portion of its input. Included are related programs which develop seabed models from digitized bathymetry data or synthetic bathymetry functions.

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I. INTRODUCTION

ECTRACE is a FORTRAN computer program designed for the investigation of bathymetric effects on horizontal acoustic ray tracing. Its supporting computer programs include routines for constructing a grid model of the sea bed from contour data, ray tracing routines, and associated printed and plotted output. The programs were written for IBM 360/370 series systems with a Versatec plotter and related software. The significant feature of the tracing algorithm is its ability to shift the direction of the vertical plane of propagation after a bottom reflection. A sea bed modeled by triangular facets fitted through three points of a grid cell makes this feature possible with a minimum effect on computation time.

Several models for tracing acoustic rays in the ocean are used in the Navy today. These models are based on a simplified environment because of practical limitations on data and computer run time, and they adequately trace a bundle of rays in a single vertical plane. Some enable intensity calculations at a given distance from the source. TRIMAIN [1], for example, is a model which features range as well as depth dependence of sound speed and accounts for some interaction with irregular bathymetry. These models have a large number of applications in deep ocean cases involving ducts, channels, and convergence zones, and bottom reflections where the plane of the ray path does not exhibit horizontal deflection.

Actual cases of long range propagation over irregular bottoms show any single ray path rarely remains within a single vertical plane. Any application of ray theory to propagation involving bottom interaction must account for a horizontal deflection caused by ray heading changes after repeated reflection from a tilted bottom plane. This effect is most pronounced for long range paths over smoothly sloping surfaces, but any valid ray approximation can be seen to undergo significant heading changes after only a few reflections from an irregular or undulating bottom.

The behavior of sound propagation over troughs, ridges, wedges, and seamounts has been studied analytically by Harrison [2] using normal mode theory and ray invariants. Since actual ocean bottom topography over large area defies practical analytical description, except in the stochastic sense, DeWitt [3] developed numerical techniques for three-dimensional ray tracing in which the bottom consists of triangular facets generated numerically from actual or interpolated bathymetry data. This approximation scheme greatly simplified the problem of calculating the three-dimensional ray path parameters after a bottom reflection and provides a means of constructing reasonably accurate ray traces (for a verification, see Appendix F).

The ECTRACE modeling program is an adaptation of the Dewitt technique for use on an IBM 360/370 series computer. The initial programs may be used to generate synthetic bottom topographical grids or create approximations to real ocean bottom grids from a bathymetric data source file. The

topographical features of the generated grid can be depicted by a contour plot and a perspective surface plot for comparison with the original contours. The primary program is the ray tracing program which accepts the generated bottom grid and performs stepwise ray position calculations from user-selected initial heading and elevation angles. The output is the printed history of each ray, and a two-dimensional plot of the ray paths projected on a vertical plane intersecting the bottom profile along the axis of the ray fan. Additionally, a horizontal plane projection is plotted which may be overlaid on the appropriate contour plot to correlate the horizontal curvature effect with grid bathymetry. Punched card output from several ray tracing runs may be combined in one independent routine for a comprehensive visual inspection of acoustic shadow zones in the horizontal plane.

It is very important to note that ECTRACE permits refraction caused by sound velocity gradients in the vertical plane only and that the sound velocity in the horizontal plane is assumed constant within a well defined water mass. All horizontal bending effects revealed by ECTRACE are the result of bottom reflection only.

With the ability to convert actual bathymetry data to a matrix of depth values, discrete faceted approximations of a selected oceanic region can be used for generating ray traces of operational significance. In addition, qualitative studies of horizontal ray deflections over idealized bottom configurations are enhanced by the computer-generated plots of ray paths over easily modifiable synthetic bathymetry. ECTRACE and the

augmenting programs are envisioned to serve as a basis for future development of three-dimensional ray modeling and investigation efforts.

II. DESCRIPTION OF ECTRACE AND PERIPHERAL PROGRAMS

This chapter describes each of the programs, their primary subroutines, and their interrelationship in producing a ray trace which may be used to investigate the bathymetric effects on horizontal ray curvature. They are presented in their intended order of use. Flow Diagram (Fig. 1) and Table I are provided to assist in understanding program relationships.

A. GENBOT

This program converts contour data into a matrix of depth values for storage on a permanent device. It also makes a two dimensional contour plot of the input data and superimposes reference latitude and longitude lines (Fig. 2). The contour plot can be placed underneath the horizontal ray trace plot of ECTRACE or ECCOM on a light table to aid in the visual investigation of the ray curvature (see Figs. 3 and 4, and Figs. 5, 6, and 7).

The bathymetry contour data used in this research exists as a sequence of data sets representing ten by ten degree regions of the North Atlantic Ocean and were obtained exclusively from a tape compiled in a joint project of the Naval Research Laboratory and the Mobil Oil Company. In their original form the data were sufficient only for producing a computer plot of region contours, thereby reproducing portions of a chart titled "Bathymetry of the Norwegian-Greenland and Western Barents Sea" [4] (see Fig. 8). Their use

in GENBOT required us to insert the depth values of the contour lines and transfer the results to a separate tape (described in Appendix A).

The following subroutines are called by GENBOT:

- 1) CORNER calculates boundary latitudes and longitudes for screening only those data needed for interpolation.
- 2) GEOPLT superimposes reference latitude and longitude lines on the subregion contours.
- 3) GEODST calculates the forward or inverse solutions of the geodetic triangle to accomplish the above.
- 4) RAIN 1, RAIN 2, and RAIN 3 [5] were obtained from the SSP3 program library at NPS and are used to perform interpolations on data points for construction of the depth matrix.

B. SYNGEN

This program produces a synthetic bathymetry grid for storage on a permanent device. It may be used to generate the following types of ideal sea bed configurations: wedge, trough, ridge, conical seamount (Fig. 9), sinusoidal undulation, or parabolic basin (Fig. 10). These grids can be used in the ECTRACE program as a depth matrix in the same manner as the grids of actual bathymetry produced by GENBOT. SYNGEN is discussed in detail in Appendix B.

C. G3DP

Program G3DP produces a perspective of any portion of the generated depth matrix through use of the NPS system subroutine CONTUR [4]. Figures 9, 10, and 11 are examples. G3DP uses

job control commands to link with the GRDSCT subroutine of the ECTRACE load module to extract the desired area (hereafter called the working matrix) to be plotted. Appendix C describes the application of G3DP in detail.

D. GRDCHK

This program is used to check the validity of the depth matrix generated by the programs GENBOT and SYNGEN. It produces a contour plot and a vertical plot of user-selected rows of the generated matrix. By comparing consecutive rows the existence and location of anomalous data points may be determined (Figs. 4 and 12). It contains the previously mentioned subroutine GEODST, CORNER, and a version of GEOPLT (called GEOPLR) to draw reference geographic lines for comparison of the two contour plots (GENBOT vs GRDCHK). Refer to Appendix D for additional discussion of GRDCHK.

E. ECTRACE

The ECTRACE program is a package of subroutines which exist in load module form on a permanent storage device in the NPS computer system user library. Its use requires a user supplied calling program which calls subroutine TRACER and contains the necessary job control language (JCL) to link with the module. These procedures are explained in more detail in Chapter IV of this report.

ECTRACE traces rays in three dimensions. The sound speed field is assumed to vary piecewise-linearly with depth only, yet provisions are made to permit simulation of up the three distinct water masses separated discontinuously by vertical

fronts. The bathymetry structure, generated by one of the two grid-making programs, is a three dimensional surface modeled by discrete triangular facets fitted through cells of adjacent depth values. Rays are traced as piecewise arc segments each with a radius of curvature dependent on the vertically-structured sound speed gradient.

When the rays undergo a bottom bounce, specular reflection is assumed. Bottom loss values can be calculated from the subprogram FBLOSS (described later), a standard Navy model such as the FACT bottom-loss routine, or a user supplied routine. The trace history supplied by ECTRACE includes the location and characteristics of each ray reversal (surface reflections, bottom bounces, and refractive turning points). The printed data lists the new ray parameters determined after the reversal had occurred. Chapter V explains the printed output in more detail.

The ECTRACE plot product includes a plane view of the ray paths projected on a vertical plane, a plot of sound speed profiles, and a horizontal (plane) view of the ray paths (Figs. 5 and 13). The horizontal view can be overlaid on the appropriate contour plot generated by GENBOT or GRDCHK, as in Figs. 12 and 14.

The following subroutines are used by ECTRACE:

- 1) Tracer is the primary tracing subroutine which calls all other subroutines of the ECTRACE program and is capable of processing a bundle of rays separated into ray fans. A ray fan is defined here as a number of

rays (user determined) each with a different initial heading measured clockwise from grid north, but all with the same initial elevation angle. A positive elevation angle describes a ray which is pointed toward increasing depth.

- 2) GRDSCT reads into core a fixed-dimension section of a depth matrix file of arbitrary size. The ray trace is restricted to the boundaries of the core-loaded working matrix. A ray which departs the working matrix boundaries is terminated and program control is passed to the next ray's trace.
- 3) IDTSUB identifies the three matrix subscript pairs whose depth values define a plane triangular bottom facet underneath the ray segment head.
- 4) DEEP calculates the depth at any horizontal position by solving for the z-coordinate on a plane fitted through the three depth matrix values.
- 5) CONTAC calculates the three-dimensional coordinates of the intersection of the ray path and triangular bottom facet.
- 6) BOANG calculates the grazing angle, elevation angle, and new heading of a bottom reflected ray.
- 7) FBLOSS returns bottom loss values in dB as a function of grazing angle for a bottom reflected ray. These values are based on NRL geophysical survey data of the Greenland-Norwegian Sea and Iceland environment collected in the mid-1970's and have been widely averaged for

convenience. The user has the option of substituting a more specialized function if bottom loss values are critical.

- 8) IDPROF determines the water mass, and hence the sound speed profile, affecting the ray with each segment iteration.
- 9) NUPROF initializes calculations for new water mass parameters once the ray has passed the boundary.
- 10) CHNLIM determines in advance the refractive sound channel limits for each ray from its invariant. This is used to test a ray at its turn-around point and to reveal its type (surface reflected, refracted-surface reflected, bottom reflected-surface reflected) in the printed trace history.
- 11) ANGPRT is used to print a summary of selected bottom contact in parameters for each ray fan.
- 12) The following subroutines each have only one calling statement in TRACER. The subroutines they in turn invoke are dependent upon the computer graphic system installed and would require internal modification if exported to a system without Versatec software. For additional information NPS users should consult Ref. 7.
 - a) BGNPLT initializes the plotter and draws all borders, titles, and axes.
 - b) BDTPLT draws a vertical profile of the sea bed centered along the mean heading of the ray bundle, as shown in the upper plot of Figure 13.

- c) RNGPLT traces all ray segment projections on the vertical plot.
- d) T2DPLT plots the horizontal track of each ray. Each ray fan uses one of thirteen symbols to indicate the bottom bounce positions of each ray. Figure 5 shows some of the available symbols.
- e) SSPPLT draws the sound speed profiles.
- f) ENDPLT draws the horizontal plot legend and terminates all plotting.

F. ECCOM

Program ECCOM uses the optionally produced punched card output of one or more ECTRACE jobs to draw a composite horizontal plot of several ray bundles, enabling a comprehensive pictorial study of shadow zones and acoustic convergence in the horizontal plane. The composite horizontal plot is designed to portray the rays which emanate from the same source or from multiple sources along a desired track. The ray numbers assigned and punched for each ray on each ECTRACE run assist the user in singling out rays of interest (or non-interest) before combination. Figures 7 and 18 are examples of this combining technique.

Amplifying remarks on these programs and subroutines can be found in the comments in the computer FORTRAN listings. For additional description of plots and computer printed outputs, refer to the appropriate appendices.

III. PROGRAM LOGIC AND THEORY

ECTRACE traces the three-dimensional paths of a bundle of rays, one ray at a time. The bundle is divided into fans of rays of the same initial elevation angle. A separate ray fan is traced for each fixed increment of initial elevation angle between the limits ELST and ELEND (input constants). A positive elevation angle describes a ray pointed downward. The initial ray headings in each ray fan extend from HDST to HDEND (input constants), measured in degrees clockwise from grid north.

A. BOTTOM AND SOUND FIELD MODELING

Figure III.1 shows the projection of the bottom surface onto the horizontal x-y plane.

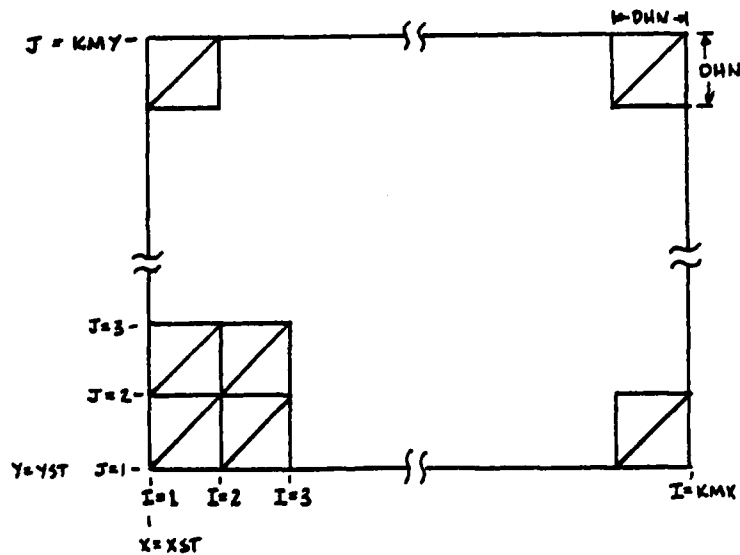


FIGURE III.1 Bottom Surface Projection

The projection of each triangular facet is a right isosceles triangle. The entire surface can be defined by specifying the depth values at the vertices of the projection triangles. ECTRACE stores these depth values (km) in the two-dimensional working array ZB. The parameter DHN (km) represents the spacing between the vertices in both the X (East) and Y (North) directions. Thus, the value of the matrix point ZB(I,J) is the depth at the vertex point with X coordinate $(I - 1) * DHN$ and Y coordinate $(J - 1) * DHN$, relative to the ZB origin.

The matrix values for ZB are read from a source file stored on a permanent storage device such as a disk pack. A matrix of dimensions 151 by 151 with spacing $DHN = km$ has been used for trial runs.

1. Bottom Contact Point

The subroutine CONTAC locates the coordinates and calculates the depth of the bottom bounce point. The parameters describing locations of the ray segment head and tail are among those passed to the main program. In this subroutine, the ray segment is treated as unrefracted (a straight line), a reasonable approximation for the small distances involved in determining the contact point.

First the horizontal positions of the ray segment head (x,y) called CEE and CNN in CONTAC, and (x_1,y_2) and called CRE and CRN in CONTAC, are checked to see if they both lie in the same projection triangle. If not, an iterative routine searches for two points on the segment such that the horizontal coordinates of both points lie inside the same triangular cell and

define the portion of the segment that penetrates the bottom facet. Then the depth of the ray head z , and the depth of the tail z_1 are computed.

Figure III.2. illustrates a profile of a cell bottom with a ray intersecting it in the propagation plane. The solution of the triad (x_c, y_c, z_c) identifying the point of bottom contact proceeds as follows:

Using subroutine DEEP (described in Section 3) compute H_1 and H_2 , the bottom depth at (x_1, y_1) and (x_2, y_2) , respectively. Then compute:

$$\Delta z = z_1 - z_2$$

where (x_c, y_c, z_c) are contact point parameters.

$$z_c = \frac{H_1 z_2 - H_2 z_1}{\Delta z + H_1 - H_2}$$

$$\text{If } \Delta z \neq 0, M = \frac{z_c - z_1}{\Delta z}$$

$$\text{If } \Delta z = 0, M = \frac{z_1 - H_1}{H_1 - H_2}$$

$$\text{Then } x_c = x + M r \sin \phi \quad \text{and}$$

$$y_c = y + M r \cos \phi$$

where ϕ is the ray heading (angle between the y - z plane and the propagation plane).

2. Projection Triangle Vertex Subscripts

The subroutine IDTSUB calculates the I subscripts, IRT, ILT, IVR and the J subscripts JBT, JTP, JVR for the vertices of

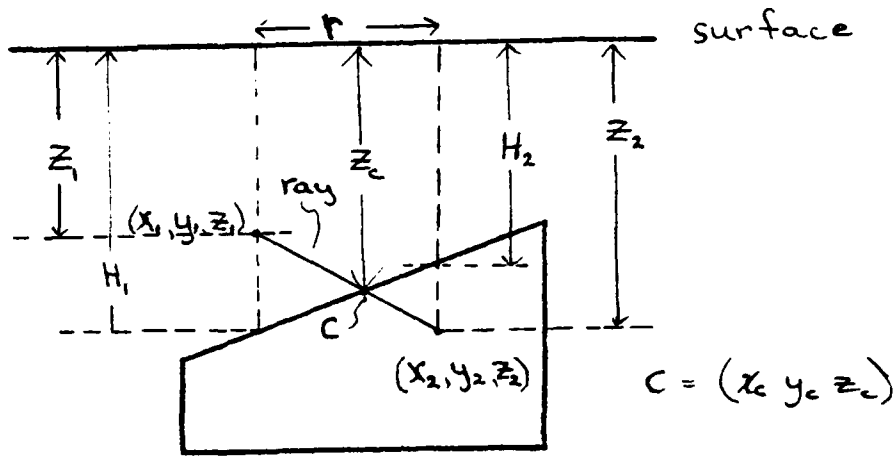


FIGURE III.2. Profile of the bottom cell in the propagation plane, with a ray contact.

of the projection triangle which contains the ray's horizontal coordinates x and y . The subscript parameters are indicated in Figure III.3. The following suffixes identify the relative locations of the vertices of the projection triangle:

RT - right

LT - left

TP - top

BT - bottom

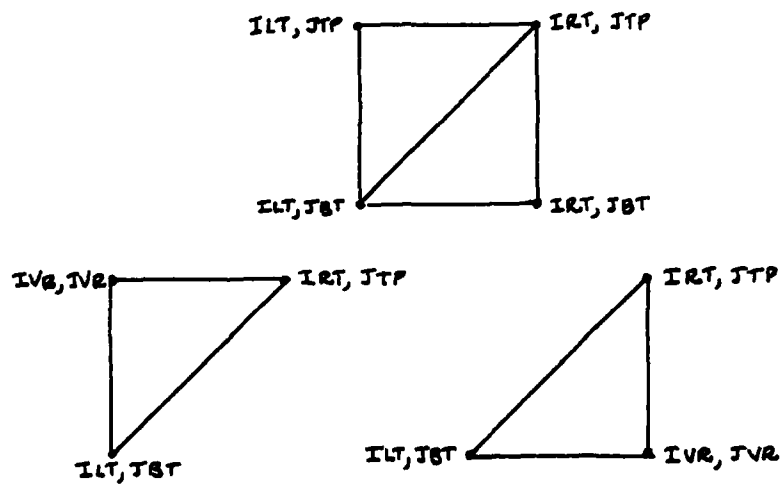


FIGURE III.3. Projection Triangle Vertices

3. Depth Calculation

Subroutine DEEP calculates the depth in kilometers corresponding to the horizontal coordinates x and y . Automatically, IDTSUB is called to identify the projection triangle subscripts. The depth z_c is calculated by solving the equation of a plane defined by the depths at the vertex points (D_1 , D_2 , and D_v). Figure III.4 illustrates the calculations made based on the orientation of the projection triangle outlining the bottom facet plane. The quantities x_c and y_c represent the horizontal position (in units of DHN) of the depth calculation point relative to the horizontal position of the depth calculation point relative to the horizontal position of the depth value D_1 (the lower left vertex of the projection triangle) as calculated in Section 1. The depth values D_x and D_y are normalized by the length of the equilateral side l , in units of DHN. Finally, the depth is solved by

$$z_c = x_c D_x + y_c D_y + D_1$$

B. RAY LOCATION AND DIRECTION PARAMETERS

A three dimensional left hand coordinate system is used (Fig. III.5.), with the positive z axis pointing in the direction of increasing depth and the sea surface level lying in the x - y plane. As the ray is traced through three dimensional space, the program variables which are used to locate the tail of the ray vector are:

DEP1 - depth coordinate

CRE - x coordinate in km

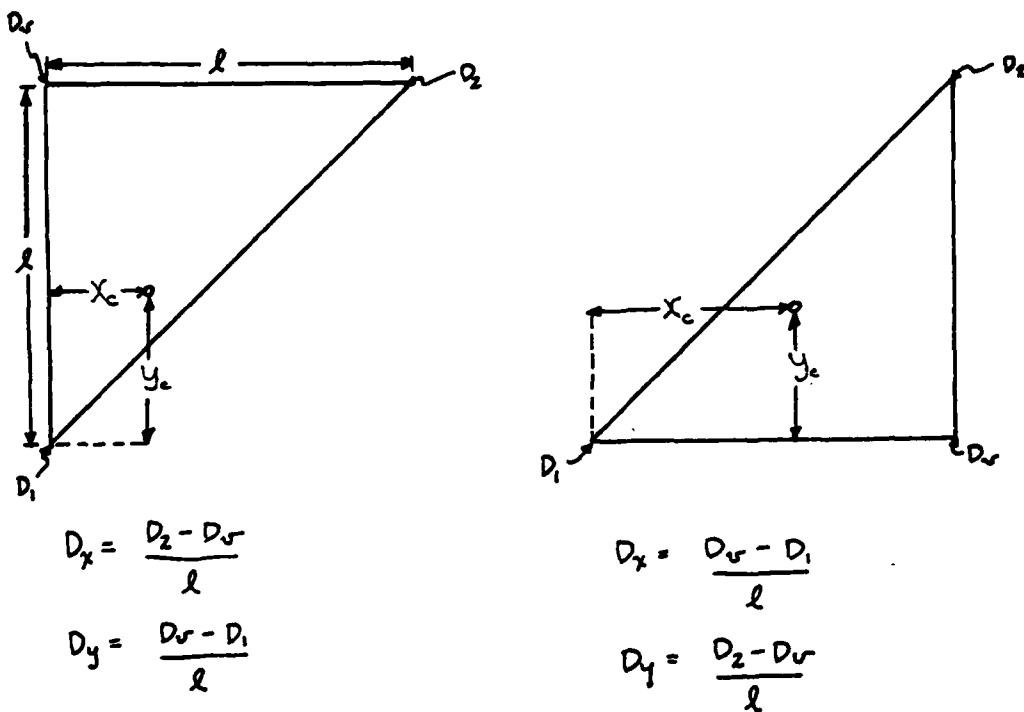


FIGURE III.4. Depth calculation on bottom facet

CRN - y coordinate in km

CRE and CRN are components of the horizontal range increment DR which forms the propagation plane heading angle PHI with the y-axis.

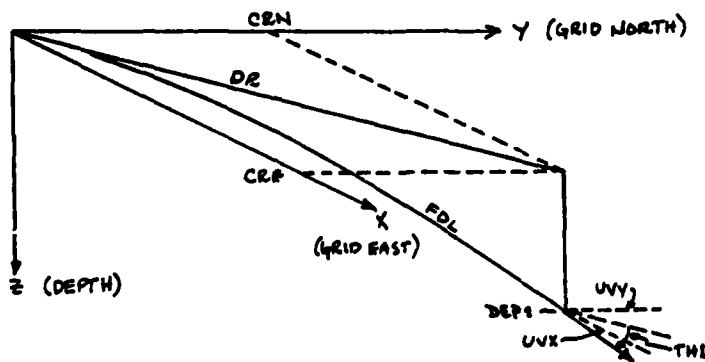


FIGURE III.5. Ray Location Parameters

Given that the ray vector originates at the point with the above coordinates, the direction of the ray vector is specified by the following angles:

TH1 - ray elevation angle in the plane of propagation measured from the ray vector's projection on the xy plane to the ray vector. A ray pointing toward the ocean bottom will have a positive elevation angle. Theta takes on values between $-\pi/2$ and $+\pi/2$ (output values are in degrees).

PHI - ray (propagation plane) heading angle between the positive y-axis and the projection of the ray vector on the xy plane, measured clockwise from the positive y-axis (grid North). PHI takes on values between $-\pi$ and π .

Initial values for TH1 and PHI are calculated from user input values (in degrees), which are converted to radians for computational purposes. The unit vectors in the horizontal plane are given as $UVX = \sin (PHI)$ and $UVY = \cos (PHI)$.

C. RAY PATH CALCULATIONS

1. Path Length

ECTRACE confines refraction to the vertical plane alone. It is recognized that while horizontal sound speed gradients exist, their effects are sufficiently small within a well defined water mass to be neglected compared to the bathymetric effect.

However, while the horizontal gradients are likely to be slight, important discontinuities in water characteristics may occur horizontally across oceanic fronts. For this reason,

ECTRACE has been designed to simulate up to three distinct water masses and two associated frontal boundaries.

Within a water mass having uniform characteristics along fixed depths a ray path conveniently defines a vertical plane within which Snell's Law can be written as

$$V = c(z)/\cos\theta(z) \quad (1)$$

where V is treated as invariant within the water mass (termed the vertex velocity in some texts since it is the speed at the depth at which the ray vector becomes horizontal). The term $c(z)$ is the sound speed at depth z and $\theta(z)$ is the elevation angle at depth z .

Equation (1) uses the simplification that the speed of propagation and the elevation angle are functions of depth only. It is generally possible to define a stratified medium in which each layer's gradient is constant. Although such a model requires a large number of data points to adequately describe a water column of complicated sound speed structure, the piecewise linear gradient approximation greatly simplifies the ray path descriptions.

Taking advantage of the approximations, we use a simple equation for the sound speed gradient, within a layer,

$$g = dc/dz \quad (2)$$

Integrating yields

$$z = c/g \quad (3)$$

where the constant of integration is avoided by arbitrarily specifying the origin of the coordinate axes at the depth where $c = 0$. By applying Snell's Law we obtain

$$z = -\frac{V}{g} \cos\theta \quad (4)$$

and

$$dz = -\frac{V}{g} \sin\theta d\theta \quad (5)$$

Specifying r as the horizontal distance axis of the vertical plane and applying analytical geometry there results

$$dz = \tan\theta dr \quad (6)$$

$$dr = -\frac{V}{g} \cos\theta d\theta \quad (7)$$

and

$$r = -\frac{V}{g} \sin\theta \quad (8)$$

when measuring r from the vertical (z -axis) to the point at which $\theta = 0$ (horizontal projection).

Squaring (4) and (8) and summing yields

$$r^2 - z^2 = \left(\frac{V}{g}\right)^2 \quad (9)$$

This is the equation of a circle of radius (V/g) and whose center is at the origin of the coordinate system just described.

The equation

$$R = -\frac{V}{g} \quad (10)$$

describes the radius of curvature of a ray path in a constant

sound speed gradient. The minus sign has been chosen to allow ρ to be positive when the refracted ray is increasing its elevation angle.

The coordinate system and computer-approximated ray path segments are shown in Fig. III.6.

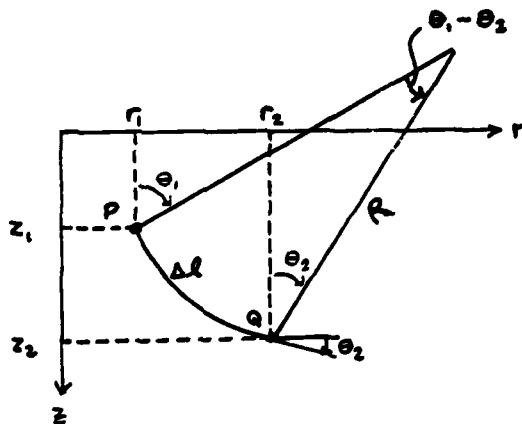


FIGURE III.6. Ray Path Geometry

It can be shown from Fig. III.6. that the ray segment path length between P and Q is

$$\Delta l = \rho \Delta \theta \quad (11)$$

where

$$\Delta \theta = \theta_2 - \theta_1 \quad (12)$$

Since the initial elevation angle of the ray is presumed known, successive values of θ are found iteratively:

$$\theta_2 = \theta_1 + \frac{\Delta l}{\rho} \quad (13)$$

Simple geometry also allows for solution of the depth change,

$$\Delta z = z_2 - z_1 = \rho(\cos\theta_1 - \cos\theta_2) \quad , \quad (14)$$

and likewise the increase in horizontal range,

$$\Delta r = r_2 - r_1 = \rho(\sin\theta_2 - \sin\theta_1) \quad . \quad (15)$$

Note that in the Fig. III.6., $\Delta\theta$, Δz , and Δr must all be positive, so the sign of ρ must agree with that of $\Delta\theta$. Equation (10), which gives ρ the opposite sign of the gradient, satisfied this requirement. Only Δz is allowed to become negative, as when a ray decreases its depth.

2. Travel Time

From the diagram (Fig. III.7.) the sound speed relationship becomes

$$c = \frac{df}{dt} \quad (16)$$

$$dt = \frac{dz}{c \sin\theta} \quad (17)$$

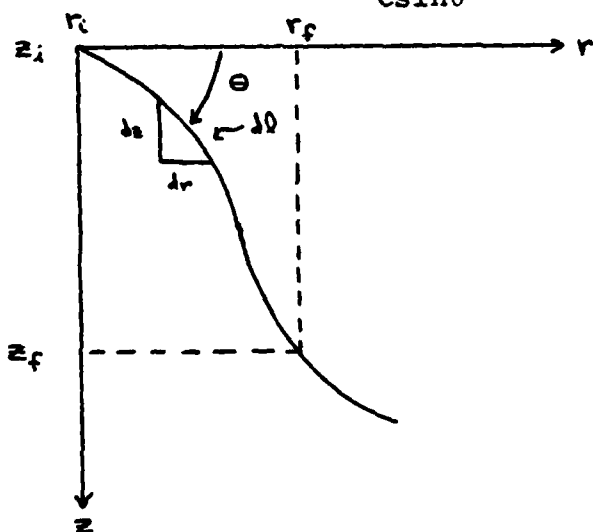


FIGURE III.7. Ray path and sound speed relationship.

The ray invariant

$$a = \frac{1}{V} = \frac{\cos\theta}{c} \quad (18)$$

and the trigonometric identity $\sin\theta = \sqrt{1 - \cos^2\theta}$ combine and give dt as a function of depth

$$dt = \frac{dz}{c(z) \sqrt{1 - [ac(z)]^2}} \quad (19)$$

The time-of-flight of the acoustic ray along the path is found by integrating from the initial point to the final point:

$$t_f - t_i = \int_{z_i}^{z_f} \frac{dz}{c(z) \sqrt{1 - [ac(z)]^2}} \quad (20)$$

Before integrating it is assumed that the gradient is constant along the segment. More generally, ECTRACE assumes a constant gradient in the layer bounded by z_1 and z_2 .

Then

$$c(z) = c(z_1) + g(z_2 - z_1) \quad (21)$$

where $z_1 \leq z \leq z_2$.

The integral may now be evaluated by introducing a new variable

$W = \frac{c(z)}{g}$ such that

$$W = z - z_1 + \frac{c(z)}{g} \quad (22)$$

Then $dW = dz$ and $C(W) = gW$. Therefore,

$$t_f - t_i = \int_{W_i}^{W_f} \frac{dw}{gW \sqrt{1 - a^2 g^2 w^2}}$$

$$= \frac{1}{g} \ln \left\{ \frac{W_f [1 + \sqrt{1 - a^2 g^2 W_c^2}]}{W_i [1 + \sqrt{1 - a^2 g^2 W_f^2}]} \right\} \quad (23)$$

$$= \frac{1}{g} \ln \left[\frac{W_f (1 + \sin \theta_i)}{W_i (1 + \sin \theta_f)} \right] \quad (24)$$

Values for W are restricted to being in the same layer and on the same side of a turning point in the ray path.

D. RAY TRACING PROCEDURE

ECTRACE begins tracing a ray from its given initial coordinates CRE, CRN, and DEPl. First the water mass is identified to determine the local gradient and therefore the ray invariant and radius of curvature. The ray path is constructed in the form of arc segments using an increment DTH calculated from a chosen arc length DL. Then the new θ value is calculated and Equations (14) and (15) are used to determine the ray segment's depth increment and horizontal range increment. The horizontal position is updated using the horizontal unit direction vectors (UVX and UVY) calculated from PHI, the initial heading of the ray's plane of propagation.

The interim update 3-D coordinates of the ray head may now be stated in FORTRAN as

$$CEE = CRE + DR * UVX \quad (25)$$

$$CNN = CRN + DR * UVY \quad (26)$$

$$DEP2 = DEPl \text{ and } DZ \quad (27)$$

where DR represents the horizontal range increment Δr and DZ is the depth increment Δz .

E. RAY CONSTRAINT CONDITIONS

Each time the ray path is incremented, certain constraint conditions must be checked. These constraints are bottom reflections and the sound channel limits.

1. Bottom Reflections

After the interim horizontal coordinates CEE and CNN are calculated, they are passed to DEEP to find the bottom depth WH2 at the ray head. If DEP2 is greater than or equal to WH2, a bottom bounce has occurred. In this case the values of DEP2, CEE, and CNN are adjusted by linear interpolation and a point of bottom contact is established. Subroutine BOANG is then called to calculate new values of TH1, PHI, UVY, and the ray grazing angle GRAZ.

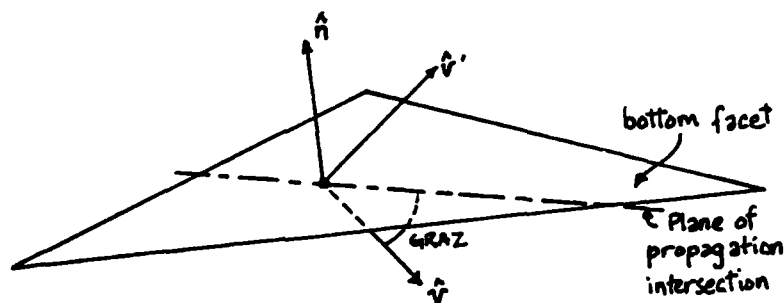


FIGURE III.8. Bottom Bounce Reflection Angles.

The basic calculations of BOANG involve the vectors:

\hat{v} - unit ray vector before bounce

\hat{n} - unit vector normal to triangle facet at the bounce point

\hat{v}' - unit ray vector after bounce

The components of \hat{v} are calculated from TH1 and PHI. The components of \hat{n} are calculated from the equation of the plane of the bottom facet. The new vector \hat{v}' is then calculated from

the vector equation,

$$\hat{v}' = \hat{v} - 2 (\hat{v} \cdot \hat{n}) \hat{n} \quad . \quad (28)$$

New values of TH1, PHI, UVX and UUY are then calculated from the components of \hat{v}' . Finally, the grazing angle GRAZ comes from

$$\sin(\text{GRAZ}) = -(\hat{v} \cdot \hat{n}) \quad . \quad (29)$$

Reflection from a sloping bottom plane facet, as opposed to a surface reflection, forces a reevaluation of the Snell's Law constant V , and therefore the radius of curvature R . The invariant V remains in effect until the next bottom bounce occurs or a new water mass is entered. Thus, after summoning BOANG, the ray tracing continues with the new ray parameters. The sound channel limits CHS and CHD described below are also recalculated at this point since they also depend on V , and GRAZ is passed to function FBLOSS to calculate a bottom loss value.

2. Sound Channel Limits

The Snell's Law equation (1) says that the ray trace is constrained to depths where the speed of sound does not exceed V . A given ray path may be constrained in the sense that it is purely refracted (R), refracted or reflected (RSR or RBR) or purely reflected (BRSR). The determining factors are V and the local sound speed by profile. V is calculated from the sound speed at the initial depth and the initial elevation angle, and is recalculated after a bottom bounce or upon entering a new water mass.

CHS and CHD are the refractive sound channel limits at the shallow and deep extents respectively. Since the sound speed profile is approximated by piecewise continuous linear gradients, the water column is treated as a column of indexed layers, each characterized by upper and lower (shallow and deep) depth boundaries and a constant sound speed gradient. The limiting depths CHS and CHD are found by scanning the water mass layers both above and below the current ray location until a boundary sound speed value is found which exceeds V . The limiting depth is then calculated from

$$z_{lim} = z + (V - c)/g \quad (30)$$

where z and c are evaluated at the top of the layer and g is the gradient of the limiting layer.

For cases where $g = 0$ or where V is not exceeded by any sound speed in the local profile, CHS and CHD are set to the physical limits of the water column.

F. RAY PROPAGATION TERMINATION CONDITIONS

Tests are made during each ray segment iteration for events which terminate the ray trace. These events are:

- Escape from grid - when the ray departs the finite x and y constraints of the working depth array (ZB).
- Depth boundaries - when the depth detected at the ray is less than ten wavelengths or greater than 10 km.
- Bottom loss - when the attenuation due to bottom reflection exceeds a specified input amount in dB.

- Error at bottom contact - when defective program code or anomalous depth data prevent the interpolative routine CONTAC from recovering the bottom depth within a reasonable number (50) of iterative attempts.
- Trapping - when it becomes apparent that the ray will not contact the bottom, rendering further three-dimensional tracing unnecessary.
- Bottom bounce gate - when the total number of bottom reflections exceeds a user specified amount.

The cause of ray termination is specified in the printed ray history, giving the ray parameters at the time of termination.

G. IMPROVEMENTS MADE OVER THE ORIGINAL NRL VERSION

The ray tracing algorithm originally existed as a program called ABOUNC at the Naval Research Laboratory. ECTRACE differs significantly from ABOUNC in the following areas:

1. Ray Path Development

ABOUNC calculates ray parameters through right triangle solutions and Snell's Law, but develops the ray path along fixed depth. Since this prevents rays from becoming horizontal, a reversal is forced when the magnitude of the elevation angle goes below a gate value. In contrast, ECTRACE develops the ray path along arc segments and radii of curvature, fixing only the maximum length of the segments while interrupting the increment as necessary when a segment reaches a reversal point or layer boundary, or to keep the increment within a maximum amount.

2. Computer Word Storage

ABOUNC floating point variables are nearly all FORTRAN double precision. The largest single burden on computer core is the depth matrix, read from a magnetic tape in card image format, each card record containing eight items (fields) ten bytes long. This format permitted a depth range of ± 9999 km with resolution of ± 1 cm. By reducing the depth range to ± 999 km and resolution to ± 10 cm, two unnecessary bytes are removed from each field, enabling a fit of ten items per record and a permanent storage reduction of twenty percent. In addition, ECTRACE reads the matrix into a single precision array to reduce the core requirements for the data by fifty percent.

3. Grid File Manipulation

ABOUNC reads the contents of the entire depth matrix data file into array whose dimensions must be exactly equal to those of the matrix. This requirement is not inconvenient on a large computer with FORTRAN dialect which permits objects time dimensioning. ECTRACE is written in FORTRAN G for an IBM Series/360 Model 67 machine whose limitations required some fundamental modifications of the program and its job control.

To maintain flexibility and reduce run time, ECTRACE was reduced to a package of subprograms which have been pre-compiled and stored on a permanent device in load module form. The user must supply a calling program which serves primarily to establish the dimensions of the depth array. The user's selection of array dimensions are made on the basis of core economy and area of interest rather than the dimensions of the

input matrix. ECTRACE, through its internal subroutine GRDSCT, extracts a rectangular working subregion from any part of the input matrix. Trial runs of ECTRACE used a working array of dimensions 151 by 151 representing a sector of 150 km on a side with a core requirement of less than 250K, while the input matrix was 369 by 443. Without GRDSCT, ECTRACE would have required an allocation of 800K bytes using the same input file.

4. Treatment of Small Elevation Angles

As stated previously, ABOUNC forced a reversal of the ray as the elevation angle of the leading segment approached a gate value close to zero. Since the ECTRACE tracing scheme permits a full range of elevation angles, early trial runs revealed an inherent error phenomenon as θ approached zero in a steep gradient. Specifically, a $\Delta\theta$ on the order of 3 degrees caused by a small radius of curvature or along arc segment traced a ray to its vertex depth in error as much as 50 meters from the Snell's Law prediction. Since the depth change was calculated from the difference in elevation angle cosines, the error was found to arise from the machine inability to retain difference precision for any pair of numbers close to integer values (round off error). Since the difference rather than the actual cosine values is needed for this calculation, the small angle series approximation $\cos \theta \approx 1 - \frac{\theta^2}{2} + \frac{\theta^4}{4!} - \dots$ was used to formulate the equation

$$\cos \theta_1 - \cos \theta_2 \approx \frac{1}{2}(\theta_2^2 - \theta_1^2) - \frac{1}{24}(\theta_2^4 - \theta_1^4). \quad (31)$$

When restricted to small angles, this approximation yields

greater accuracy than the straightforward machine calculation of the left hand side, since the precision retained by the registers is very high.

5. Travel Time

ABOUNC calculates the travel time of an acoustic signal along a ray segment by dividing the linearly-approximated path length by the mean sound speed. ECTRACE accounts for path curvature and depth dependence of the sound speed through integral evaluation, discussed in detail in section C.2.

6. Track Events

Layer transitions, reflections, and turnarounds are events which may require a change in ray parameters. ABOUNC tests for these events in algorithmic sequence, makes the necessary changes in response to the first event detected and continues the trace from the current position of the ray vector head. ECTRACE retraces a ray segment to the event depth and tests for all other events before beginning the next segment from the transition point. This logic eliminates the possibility of a long ray segment crossing more than one event depth with only one event detected.

IV. USER INSTRUCTIONS (ECTRACE)

A single step ECTRACE job traces a bundle of rays from a single source in the form of ray fans. Each ray fan is a bundle of rays of common initial elevation angle. All ray fans are bounded between to initial heading values measured from grid North (grid North equals true North at the grid center).

During the following discussion the reader may wish to refer to Fortran listing in Appendix M. The user instructions for the other programs (GENBOT, G3DP, SYNGEN, GRDCHK, and ECCOM) are explained in their individual appendices (User Instructions and Output Description).

A. JOB CONTROL CARDS (JCL)

The following JCL cards and parameters are required for an ECTRACE run:

- JOB card - The CPU time parameter should allow 60 seconds for every seven rays to be traced.
- EXEC card - This card must specify the FORTCLGW procedure (Appendix O). 250K bytes of core is required for the standard 22801 (151 by 151) element depth matrix portion plus 4K for every additional 1000 elements.

The computer systems job class definitions should be considered before deciding upon the size of the working matrix and the number of rays. For example,

```
EXEC FORTCLGW,REGION.GO=250K
```

is a class C job at NPS when limited to five minutes of

time, which is adequate for tracing 40 rays.

- Calling program - Following the

```
//FORT.SYSIN DD *
```

card, the calling program must contain cards

```
COMMON/DIMS/KMX,KMY and
```

```
CALL TRACER (ZB) .
```

ZB is a REAL * 4 array dimensioned exactly by KMX,KMY, and these values (KMX,KMY) are initialized to the values of the DIMENSION statement using assignment statements, as in the following example.

```
DIMENSION ZB(151,151)
```

```
COMMON /DIMS/ KMX,KMY
```

```
·  
·  
KMX=151
```

```
KMY=151
```

```
·  
·  
CALL TRACER(ZB)
```

```
·  
·  
STOP
```

```
END
```

KMX and KMY are INTEGER * 4 and should be less than or equal to the dimensions of the data matrix from which the depth values will be taken.

- LINK cards - These cards point to the ECTRACE load module. They must include all members of the module for which the user does not supply a substitute. An example which includes all members is:

```
//LINK.USDD UNIT=3330,VOL=SER=DISK01,DSN=1270.ECTRACE,
```

```
// DISP=SHR,LABEL=(,,,IN)
```

```
//LINK.SYSIN DD *
```

```

INCLUDE USDD (TRACER,GRDSCT, IDPROF, NUPROF, CHNLIM)
INCLUDE USDD (BGNPLT, SSPPLT, BDTPLT, RNGPLT, T2DPLT, ENDPLT)
INCLUDE USDD (IDTSUB, DEEP, CONTAC, BOANG, ANGPRT, FBLOSS)
ENTRY MAIN
/*

```

- GO cards - ECTRACE uses data set reference number one for input of the depth matrix. For example, to point to a depth matrix residing in a data set called S9999.GRID on DISK03, the following DD statement is used:

```

//GO.FT01F001 DD UNIT=330,VOL=SER=DISK03,DSN=S9999.
GRID,DISP=SHR,LABEL=(,,IN)

```

If a depth matrix from an outside source is used, it must be in the format specified in the Output Grid Data Format section of Appendix A. If a punched card output is not desired to make an ECCOM run, include the card

```

//GO.FT07F001 DD DUMMY .

```

ahead of the GO.FT01F001 DD statement shown above.

B. DATA CARDS

Following the

```

//GO.SYSIN DD *

```

card, the user selected data must be provided in the following format. FORTRAN field descriptors are in parentheses. The FORTRAN variable names are listed for reference.

- Card 1 (20A4)
 - OTIT - title of the run
- Card 2 (958.2)
 - X0 - source position for x coordinate (kilometers).

Y0 - source position y coordinate (kilometers).

Z0 - source depth (meters). A source depth which exceeds the water depth will be decreased to one meter above the bottom. Source coordinates in a nonpropagating location will also be adjusted.

XREC - receiver position x coordinate (kilometers).

YREC - receiver position y coordinate (kilometers).

ZREC - receiver depth (meters). The receiver may be positioned at the source if calculations are not desired. Excessive depth is automatically corrected.

FREQ - frequency (Hz). A ray is terminated when the water depth becomes less than ten wavelengths during propagation.

FDL - (optional) segment length (meters). The parameter affects the smoothness of the vertical plot. Smaller values increase smoothness and run time. Large values create the risk of missing a bottom peak. The default value is one wavelength.

• Card 3 (6F8.2)

XMIN - initial x value of horizontal plot (kilometers).

YMIN - initial y value of horizontal plot (kilometers).

The above values are used for drawing the axis of the horizontal plot and for determining the section of the input matrix to be read into a working depth matrix (ZB).

The values for KMX and KMY, recorded cell resolution (DHN), and the limits of the input matrix ultimately

determine the axis ranges. The user should be familiar with these parameters when choosing the origin of the plot.

ZST - initial depth value for vertical plot (kilometers)

ZEND - final depth value for vertical plot (kilometers)

ARST - initial range value for vertical plot (kilometers)

AREND - final range value for vertical plot (kilometers)

The above values are used to draw the axes of the vertical plot. The initial values may be negative. The program adjusts the final values if necessary for plot esthetics.

• Card 4 (6F8.2)

HDST - heading of the first ray in each ray fan (degrees)

HDEND - heading of the last ray in each ray fan (degrees)

ELST - elevation angle of the first ray fan (degrees)

ELEND - elevation angle of the last ray fan (degrees)

Headings are measured from grid north. Elevations are measured from the horizontal plane, positive downward (toward increasing depth).

HORLIM - maximum ducting or channeling range (kilometers).

This is a gate value, like BLMAX CARD 2, which terminates the trace of a ray when exceeded.

HORLIM serves to screen out those rays which do not appear to contact the bottom.

SMNGL - (optional) small angle value for alternative cosine difference calculation (degrees). A

value of less than three degrees is recommended.

See the discussion on "small angle approximations"

in Chapter III. The default value of two degrees is set when left blank.

. Card 5 (6I5)

NHD - number of rays per ray fan (≥ 1)

NEL - number of ray fans per bundle (≥ 1)

NSTOP - maximum number of bottom bounces per ray (≥ 1)

The program restricts NHD to 30 rays, with a maximum total number of 100 rays produced, each with a maximum number of 50 bottom bounces or 200 reversals.

INCPLT - number of ray segments defining one plot segment (≥ 1). With sufficiently small ray segments it is not necessary to use each iteration for plot definition to achieve a smooth plot, so this parameter is provided to enable the user to coordinate FDL and INCPLT for run time economy.

NLEN - length of the longest horizontal plot axis (≤ 19 inches). This value controls the physical size of the plot. A value less than four will suppress the plot (resulting in an ABEND code in the HASP log), but it will not affect the calculations or printed and punched output. A value greater than 15 requires additional JCL for strip plotting, since the total plot width is NLEN plus six inches. Refer to Ref. 7 for strip plotting.

NSSP - number of sound speed profiles (water masses provided as data ($1 \leq \text{NSSP} \leq 3$)).

- Card 6 (A4,I3)

OMAS (1) - name of first water mass

NVAL (1) - number of (depth, sound speed) pairs defining the sound speed profile ($1 \leq \text{NVAL} \leq 50$).

- Card 7 - (through card 16 if necessary) (10F8.2)

These are the data pairs (depth, sound speed), in meters and m/sec., from the sea surface to the last data point in the profile. The gradients will be calculated linearly between these points, with the final gradient below the last point set to 0.01668 m/sec. by the program.

- Next card (4F8.2)

If the previous data is to be followed by the data for another water mass, this card must be included to define the frontal boundary between the two. The order in which the water masses appear as input determines their positions relative to the fronts. Cards which describe the next water mass, follow the frontal definition card and are formatted as described cards 6 and beyond. The last data card is the last string of (depth, sound speed) pairs of the last water mass; refer to Appendix M (second page) for an example of three water masses. The following variables define the boundary between each water mass:

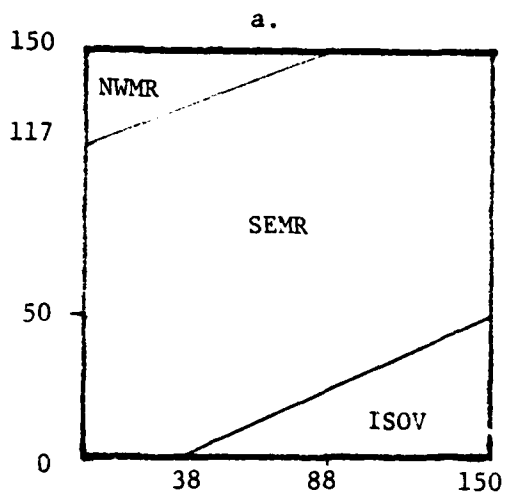
FENTX (1) - x coordinate of front beginning point (km)

FENTY (1) - y coordinate of front beginning point (km)

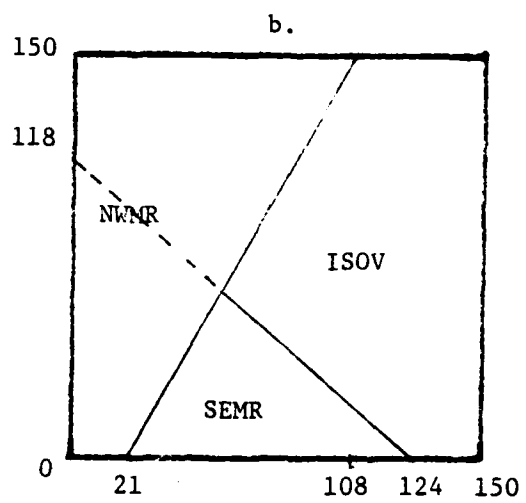
FENTX (l) - x coordinate of front end point (km)

FEXTY (l) - y coordinate of front end point (km)

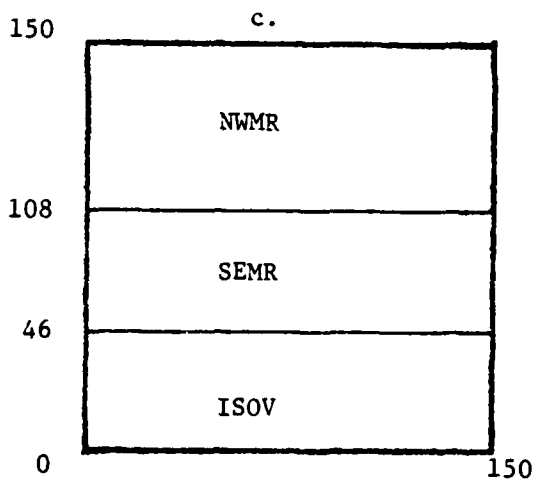
The examples shown in Fig. IV.1 identify the water mass boundaries for various input axis values in the form (FENTX, FENTY), (FENTX, FEXTY) for each water mass boundary. The first example a. represents the data from an original ECTRACE run, refer to the second page of Appendix M. Examples b. and d. show the priority of the water masses. The first water mass defined, Northwestern Mohns Ridge (NWMR), dominates the second, Southeastern Mohns Ridge (SEMR), and the third, isove-locity (ISOV), where they overlap.



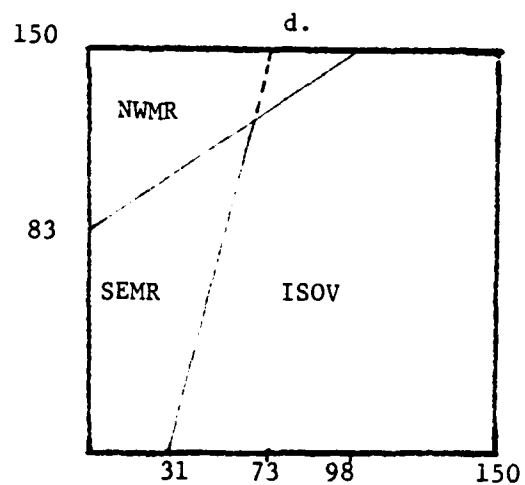
NWMR
 (0,117) (88,150)
 SEMR
 (38,0) (150,50)
 ISOV



NWMR
 (21,0) (108,150)
 SEMR
 (0,118) (124,0)
 ISOV



NWMR
 (0,108) (150,108)
 SEMR
 (0,46) (150,46)
 ISOV



NWMR
 (0,83) (98,150)
 SEMR
 (31,0) (73,150)
 ISOV

FIGURE IV.1. Examples of water mass boundaries for various values of (FENTX,FENTY) and (FEXTX,FEXTY).

V. INTERPRETATION OF ECTRACE OUTPUT

The following discussion refers to an ECTRACE run titled "Trial 67***Synthetic Basin***" (Figure 5), which is a trace conducted in a synthetic parabolic basin (Figure 6). A portion of the printed output is shown in Tables II - V. In this ECTRACE run, eight ray fans were selected to be projected between -30 and +30 degrees elevation. Each ray fan was composed of only one ray, thus the initial heading for each ray was 010 degrees.

A. PRINTED OUTPUT

Refer to Table II through V (Appendix G) as examples of the following discussion.

1. Parameter Tableau (Table II)

After processing and adjusting the input parameters just described, ECTRACE prints a final tableau of these parameters plus some additional parameters calculated from the original input such as layer gradients, the total number of rays to be traced, and the spacing between rays. In addition, the results of the depth matrix-grid load is summarized, revealing data from the header record of the grid file.

2. Ray History Tableau (Table III)

During the trace of each individual ray, this tableau prints a line of ray parameters at each end point and reversal. The following is a description of one line of parameters.

- TYPE identifies the nature of the reversal, and is

abbreviated INIT for initial position, BOTT for bottom bounce, SURF for surface reflection, OVER for turnover, and STOP for terminated position.

- X, Y, and DEPTH are the coordinates in kilometers of the reversal and end point.
- GRID HEADING is the ray heading measured clockwise from grid North at the completion of the reversal.
- ELEV is the ray's elevation angle measured downward (positive toward increasing depth) from the horizontal zero degree reference).
- BRNG TO REC is the bearing from the reversal point to the receiver position.
- DIST TO REC is the slant range distance from the reversal point to the receiver.
- WTR MASS is the water mass identifier indicating the sound speed profile applied in the present calculations.
- LYR is the constant gradient layer number corresponding to the order input as profile data (i.e., layer 1 is the surface layer and indicates that the surface gradient applies.
- DEPTH LIMITS are the physical and refractive sound channel limits of the ray, determined by its invariant. If MIN is 0.0, an upward traveling ray will reflect off the surface before reaching its upper vertex (turnover) depth. If the MAX depth is greater than or equal to 10km, a line of asterisks is printed since the ray could never attain its turnunder depth before reaching the bottom.

Otherwise, these limits are the ray's vertex depths, and if the reversal type is OVER or UNDR, the appropriate limit should exactly match the depth value on the same line.

- C is the sound speed at the reversal point. This is the ray invariant used for tracing.
- GRAZ ANGLE is the angle in degrees between the ray vector and the line of intersection of the bottom facet plane with the vertical plane. This is the angle used to calculate bottom loss and the new ray direction vector.
- BTM ANGLE is the angle between the bottom facet plane normal and the vertical (z-axis), in degrees.
- BTM LOSS is the accumulated intensity loss in dB after the bottom reflection. When this value equals or exceeds BLMAX, the ray's trace will terminate.
- LPS is the number of steps required by the CONTAC subroutine to locate the point of bottom contact. A long ray segment length may require more steps than a shorter one. A maximum number of 50 steps is permitted before the bottom facet is assumed anomalous and the ray's trace is terminated.
- Prior to the final line of an individual ray's trace history, is a summary of plot definition parameters plus data on the ray's CPA to the receiver, and reason for ray trace termination. The CPA calculations are accurate to within one ray segment length.

3. Ray Fan Summary Tableau (Table IV)

At the completion of the trace of one complete ray fan, a table is printed listing each ray's elevation angle and depth in meters before each bottom bounce. All zero values at the bottom of each ray's column indicate blank data.

4. CPA Summary Tableau (Table V)

When all ray traces have been completed, a table is printed listing each ray's heading, time, and distance at CPA to the receiver.

B. PLOTTED OUTPUT

ECTRACE produces a single montage of up to five separate plots (Fig. 13, the total dimensions of which depend upon the user's selection for the maximum size in inches of the longest axis of the horizontal plot (NLEN). The following table lists some sample values for NLEN and the resulting dimensions of the complete plot.

NLEN	Maximum (in.)Height	Maximum Width	Remarks
5	7	8.33	minimum
10	14	16.67	
15	21	25	maximum size without strip plotting [5]
19	26.6	31.67	maximum allowable

Components of the ECTRACE plot follow.

1. Sound Speed Profiles (Figure 13)

A plot of sound speed versus depth is made for each water mass defined.

2. Vertical Plot (Figs. 15 and 16)

Most two-dimensional ray trace programs produce plots of ray paths on graphs of depth versus range. The vertical plot is similar except that all ray paths are projected from three dimensions onto the vertical plane. The plane is oriented along the mean ray fan heading and includes its profile of the sea bed. In ECTRACE trial 65B (Figure 13) the ray fans each contain two rays whose initial headings vary from 360 to 020 degrees as indicated by 10.000 +/- 10.000 on the plot. The bathymetry profile is made along the heading of 010 degrees. On a plot, the heading value (HEADINGS) always indicates the direction of the bathymetry slice. The (+/-) value signifies the initial heading of the first and last rays and that additional rays are evenly spaced in the interval.

Since the rays are actually traced in three dimensions, bottom reflections occurring outside the vertical plot plane may appear to be taking place above or below the bottom surface instead of at the boundary (Fig. 15). Only those bottom contact points which occur in the projection plane must lie on the seabed profile.

The symbols listed on the plot (Fig. 5) are used to identify bottom contact locations in the vertical and horizontal plot, and are unique for each ray fan except that up to thirteen symbols are used before repetition, as shown in Table VI.

3. Horizontal Plot (Fig. 17)

This plot is the most important plot product of ECTRACE and is the plot of the ray paths on a horizontal plane

(topview). This plot displays the X-Y positions of each bottom contact point using the ray's (ray fan) identification symbol and connects them with straight lines, revealing the horizontal deflection effect. Each ray's plot begins at the source, ends up at the last bottom contact point in the grid and is labeled with the ray number (Fig. 17). The ray number can be used to locate its printed and punched output history.

The axes are labeled with respect to the origin of the input matrix. The geographic center position and coordinates of the input matrix, if included in the bounds of the working matrix (FORTRAN array ZB), is also plotted for reference. It is important to note that this plot, without the bottom contact symbols, may combine the results of other ECTRACE runs by combining the optional punched card outputs as input to ECCOM (Figs. 7 and 18).

C. PUNCHED OUTPUT

The punched card output for a single ECTRACE job consists of the following cards:

CARD	DATA CONTENTS
1	The runtitle
2-3	The grid title
4	Grid reference coordinates and scale factor
5	Initial elevation, initial heading, number of points (BB) and ray number of the first ray
6+	X-Y coordinate pairs of plot points of the first ray
(Data for additional rays is repeated as 5 and 6+ above)	
Last	9999., to flag the end of data

These cards may be stacked as a member with those of several ECTRACE jobs as input to a single ECCOM job. For ECCOM to be meaningful, cards 2 through 4 of each stack member should be identical, and the user should verify this himself.

Punched card output may be quite voluminous and should not be produced unless required. The following card, inserted before the first GO card (JCL), will suppress the punched output:

```
//GO.FT07F001 DD DUMMY .
```

VI. SUMMARY

A. POTENTIAL APPLICATIONS

ECTRACE, in its present form, has many potential applications:

- The investigation of asymptotic deflection angles in ocean areas where bathymetry data are well-documented, allows optimum hydrophone positioning. For example, Ref. 6 cites cases where seemingly attractive receiver positions would be affected by shadowing in the horizontal plane.
- Adaptation of ECTRACE ray tracing methods could be incorporated into existing programs which presently rely upon an assumption of radial symmetry of ray propagation about a source or receiver (no horizontal deflection).
- The horizontal deflection effect may lend additional insight into the study of travel times and intensities of acoustic signals, enabling more accurate source fixing information.

B. IMPROVEMENT

There are many areas of improvement which would increase the utility of ECTRACE and its supporting computer programs for the above applications:

- A better routine to convert bathymetry contour data into a matrix of depth values is essential for modeling

regions for which only contour data exists. Most known interpolation algorithms perform best on data which are randomly or regularly spaced rather than in the form of contours. For example RAIN2 [5] would probably perform better with the data used to make the contours than it does with the contours themselves. While the contour data are useful for cartographic and geologic purposes, bathymetry data in a less processed form are significantly better sources for constructing computer models of the sea bed.

- ECTRACE in its present form makes no calculations of intensities or their losses due to spreading, attenuation, or scattering, thus preventing its use as a propagation loss model.
- An improved bottom loss function is recommended over the supplied FORTRAN function subprogram FBLOSS. The user may perform this substitution easily by deleting FBLOSS from the INCLUDE step in the LINK statement of the ECTRACE job control and supplying another function subprogram (added at the end of the calling program) that accepts a double-precision argument for grazing angle and is also called FBLOSS.
- The assumption of specular reflection neglects the phenomenon of transmission into the sediment and its effect on the location of the reflected ray due to sub-bottom boundaries. It would be interesting to incorporate in an improved version of ECTRACE.

APPENDIX A
GENBOT USER INSTRUCTIONS AND OUTPUT DESCRIPTION

GENBOT is used in the construction of a depth grid file from bathymetry contour files. In this discussion, the term "grid" refers to a matrix of depth values whose row and column dimensions represent data point spacing in terms of a desired resolution parameter DHN.

1. Selection of Bathymetry Grid Regions

GENBOT will create a bathymetry grid file for any region of the geoid for which contour data is supplied in the format stated in section A-4. The user must select the latitude and longitude of the center of the region of interest, a radius in kilometers and the cell resolution in kilometers. GENBOT will attempt to create a square matrix whose semi-axes represent the selected radius and whose elements represent depth values in kilometers.

A 30-km data margin, outside the calculated axis limits, is required to begin interpolation. Should this requirement not be met, GENBOT will symmetrically reduce the length of one or both axes until the resulting rectangular matrix plus margins with the desired center position intact is totally encompassed within the data region. The center coordinates, area radius, and cell resolution must be selected so as to avoid generating a grid which is impracticably small. In particular, a generated grid may not overlap a pole, and one with a pole on a margin boundary must be supplied data from eighteen contour files to cover 180 degrees of longitude.

Contour data currently available in usable format cover 40 degrees of longitude of the North Atlantic Ocean, specifically the Norwegian and Greenland Seas, from longitudes 20W to 20E and latitudes 60N to 90N (Fig. 8). The Naval Research Laboratory, Acoustics Division, Arctic Section,

has additional files which cover the entire North Atlantic land and sea regions which may be utilized by GENBOT after modification. However, GENBOT need not be the exclusive means of grid instruction. The only requirement is that the grid exists as a file in the format specified. The user may wish to draw on other sources of bathymetry data, such as SYNBAAPS [8], and tailor other available resources to construct a usable grid.

2. Grid Construction Techniques

Once supplied with the user's selection for the grid title, center coordinates, cell resolution and area radius (TTL, CNLAT, CNLON, DHN, ARAD), GENBOT begins by defining a north-oriented square region whose boundaries are at a distance ARAD from the center. The subscripts of the two dimension matrix depicting this region will represent equal units of DHN spacing from the origin along the x and y axes of the square using a cartesian coordinate system. Thus, while all distances calculated during grid generations are geodetic distances from the center, point positions are made relative to the grid origin or southwest corner. This technique results in a plane projection which is distortion free along straight tracks which pass through the center. Subroutine CORNER then calculates and prints a table of the initial cartesian and geographic coordinates of the grid corners. The cartesian coordinates will always range from (0,0) to their maximum values, initially double the value of ARAD. The geographic coordinates should reflect some meridian convergence. This table will be repeated for the final grid, showing the adjustments made, if any, to meet the data requirements.

Many geographic coordinate pairs in an input file may be well outside the area relevant to the grid, so GENBOT calculates gate values called

SLAT, ELAT, SLON, and ELON for data discrimination. SLAT and ELAT are always one degree beyond the minimum and maximum latitude values calculated by CORNER, but SLON and ELON may extend beyond the minimum and maximum longitudes by 1, 10, or 20 degrees, depending upon the maximum latitude.

The grid region and its data environs recognized by GENBOT at this stage is shown in Fig. A.1. All points within these environs are subject for consideration during interpolation of depth values in the grid.

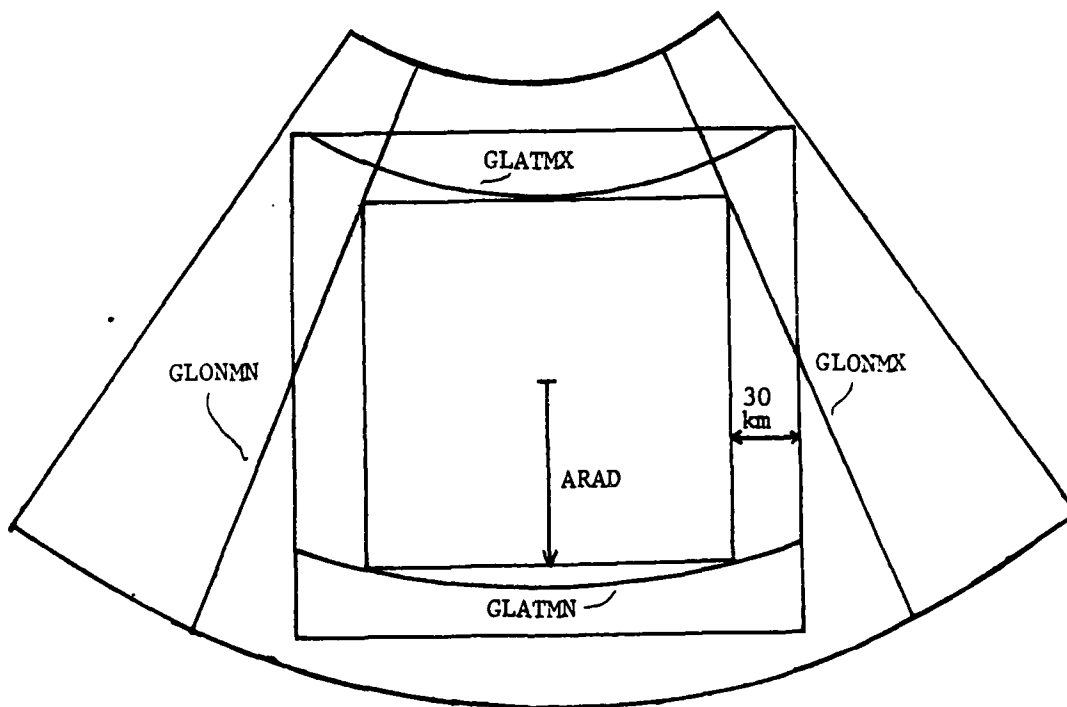


FIGURE A.1. Geographic region used for grid construction.

Data files used as input for GENBOT are digitized representations of an NRL bathymetry chart [4] and were recorded on Mobil Oil Company Tape NAV-78 for use in a computer program to draw portions of the chart in the form of bathymetric contour lines and their depth labels as they exist on the chart. The records are in the card image format and consist of three types:

- NAME - depth value coordinates
- CON - contour line header label
- Chart coordinates of points along the contour line

In the original form the numerical data on the tape consisted of latitude/longitude pairs, providing no means of determining the depth represented by the contour lines without visual inspection of the computer plot. The tape used in this research is similar in format to NAV-78 except that the contour line header records include depth data (provided by NRL), and only the regions shown in Fig. A.2 and listed in Table A.I, are covered. The numerals of the data set names were chosen to reflect the original file number on the source tape, NAV-78.

Using the magnetic tape files selected by the user, GENBOT begins reading the digitized contour data, stopping after each record to discriminate the points, calculate geodetic distances, transform the data to x, y, z coordinates, and load the coordinates into three axis vectors, AX, AY, and AZ (which will be used later for interpolation) while simultaneously keeping a running plot of the contour lines.

After all input files have been processed, the vectors AX and AY are sorted into ascending order by the SSP3 subroutine RAIN1 [5]. The minimum and maximum values are tested to determine if the 30-km outside data margin is included in the range. If not, axis reduction begins until

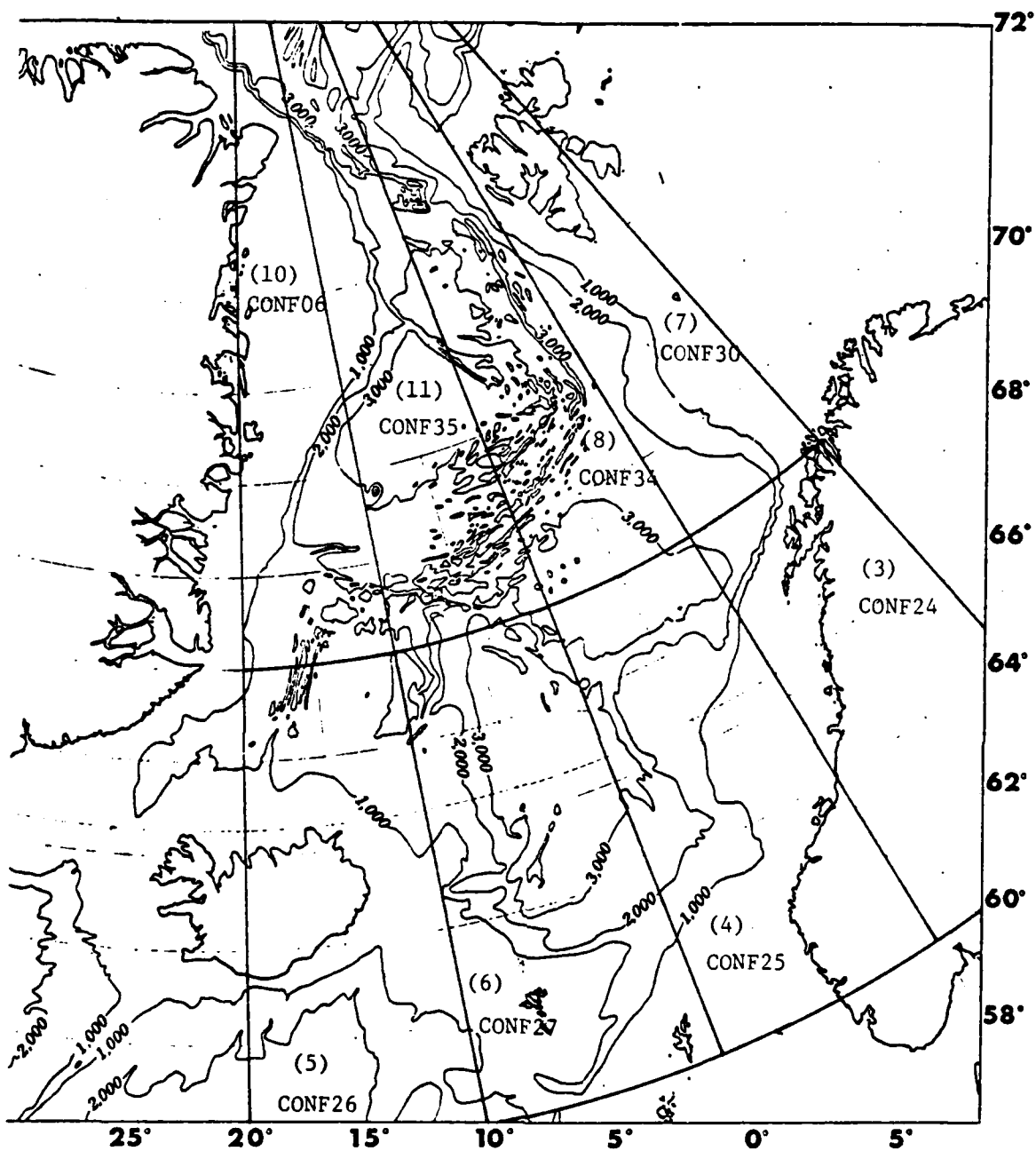


FIGURE A.2. North Atlantic regions, with their magnetic tape file numbers and data set names, available for use by GENBOT. All are 10° by 10°. Other regions available on the same tape are listed in Table A.I.

TABLE A.I
FILE ONE OF CONTOUR DATA RECORDED ON A MAGNETIC TAPE

DATA: BATHYMETRIC CONTOURS OF THE NORWEGIAN AND GREENLAND SEAS FROM
LAT 60N TO 90N and LONG 20W to 20E.

SOURCE: ADAPTED FROM MOBILE OIL CO. TAPE NO. NAV-78 AND NAVAL RESEARCH
LABORATORY DATA.

STRUCTURE: EACH FILE COVERS A 10 X 10 DEGREE REGION. THE FOLLOWING LIST
IDENTIFIES THESE FILES. THE FIRST VALUE IS THE FILE NUMBER, FOLLOWED BY
THE DSN, THEN THE LAT/LONG PAIR OF THE SOUTHWEST CORNER (LABOR,LONOR) OF
THE REGION, AND FINALLY THE NUMBER OF CARD IMAGES CONTAINED IN THE FILE.
THE TAPE IS STANDARD LABELED, DENSITY 1600 BPI, LRECL=80,BLKSIZE=800.

2	CONF13	+80-20	256
5	CONF26	+80-20	4343
8	CONF34	+70+00	12443
11	CONF35	+70-10	9428
3	CONF24	+60+10	569
6	CONF27	+60-10	6001
9	CONF37	+80+00	491
12	CONF36	+80+10	409
4	CONF25	+60+00	3026
7	CONF30	+70+10	857
10	CONF06	+70-20	4454
13	CONF38	+80-10	972

either the margin requirement is met or goes below a 7.5 km semi-axis length, the latter case preventing grid construction although a contour plot may still be produced. Subroutine CORNER is then called again to print the corner coordinate table. If no adjustments were necessary, the second table will be identical to the first.

The interpolation process begins at the southwest corner of the grid and proceeds in a columnar direction (i.e., completing the range of x_i values for each y_j value) via successive calls to the SSP3 subroutine RAIN2. The accuracy of the interpolated values is proportional to the density of data in the given area of interest. Every ten values interpolated are written as a record on the output file. The process continues until the total number of matrix elements has been reached, at which time the output file is closed and the program is terminated.

3. User Instructions

a. JCL and Program Deck.

The program section of a sample deck is printed below. The TIME and REGION.GO parameters were chosen in anticipation of a maximum number of 5000 data points in the area of interest, a square region of 210 km on a side (150 km plus margin). The program listings included in this appendix are part of this example.

```
//(Standard job card),TIME=20
// EXEC FORTCLGW,REGION.GO=250K (See Appendix 0.)
// FORT.SYSIN DD *
(GENBOT, CORNER, GEOPLT, GEODST listings)
(RAIN1, RAIN3, RAIN2 listings)
/*
```

The following DD statements identify the magnetic tape files representing the ten by ten degree regions into which the subroutine

extends. In the example, the area chosen is centered at coordinates 70°-04'N/15°-51' (70.07059/15.85302) with a radius of 75 km. This area requires two data files as input, CONF24 (file 3) and CONF30 (file 7). Since tape data is sequential, the order of the DD cards should be in the order of the file numbers (appearing in the LABEL parameter).

```
//GO.FT01F001 DD UNIT=3400-3, VOL=SER=NPS,DISP=(OLD,PASS),  
// LABEL=(3,SL,,IN),DSN=CONF30  
//GO.FT01F002 UNIT=AFF=FT01F001,VOL=(,RETAIN,REF=*.GO.FT01F001),  
// DISP=(OLD,PASS),LABEL=(7,SL,,IN),DSN=CONF30
```

More information on magnetic tape usage at NPS may be found in Ref. 10.

Next must follow the DD statements specifying the data set and device for permanent storage of the generated grid. The permanent device may be another magnetic tape, a disk, or punched cards. In all cases, the size of the output data set is important, and the DCB parameters should be considered in advance if the grid size is different from the example. GENBOT produces card image out put, meaning the logical record length is 80 bytes.

- Punched cards. If the grid is to be stored on punched cards, the user need only change the data set reference number on the appropriate WRITE statements in GENBOT from a two to a seven. The number of cards punched will equal a $3+[(\text{row dimension})(\text{column dimension})/10]$ rounded up to an integer value. This represents three header cards followed by ten depth values per card in columnar order, as required by ECTRACE. Thus if the input grid radius was 75 km and input cell resolution 1 km, the maximum parameter calculated by GENBOT will be:

XMAX	YMAX	IMAX	JMAX
150	150	151	151

resulting in a matrix of 22801 elements and a punched output of 2284 cards.

- Disk. Grid storage on a disk device is the most convenient form for multiple ECTRACE runs over the same sea bed. The following DD statement stores the example grid on a 3330 disk drive device at NPS as a data set named S999.GRID.

```
//GO.FT02F001 DD UNIT=3330,VOL=SER=DISK03,DISP=(,KEEP),  
// DCB=(FECFM=FB,LRECL=80,BLKSIZE=800),SPACE=(TRK,20),  
// DSN=S9999.GRID
```

Blocked at 800 bytes, the output data requires 14 tracks per 10 records (card images). More information on the DCB and DSN parameters may be found in Ref. 11. When the generated grid is no longer needed, and if the user wishes to generate a new grid, or if space has already been allocated on the device, the DISP parameter should be SHR in place of (KEEP) and the DCB and SPACE specifications may be omitted. Disk data sets are periodically purged by center operations personnel, but obsolete data set space should be cleared or reallocated by the user.

b. Input Data.

The following input data are user selected values and follow the //GO.SYSIN DD* card.

<u>Card</u>	<u>Variable</u>	<u>FORTRAN Field Descriptors</u>	<u>Remarks</u>
1-2	TTL	6A8/6A8	Title
3	CNLAT, CNLON, DHN, ARAD	4F10.5	center latitude, center longitude, cell resolution, radius
4	NFILES, LEN	2I5	Number of input files, plot length

The magnitude of LEN determines the plot size (≤ 19 inches). If LEN is negative, no grid will be constructed. If its magnitude is less than four, no plot will be produced.

c. Printed Output

GENBOT printed output supplies the following:

- A repeat of the user input data.
- A table of the grid corner coordinates and the depth matrix dimensions using the input parameters.
- A summary of results for each contour line, including its depth, and the title from the header label, the number of points on the line (NPTS) and the number of points used from the line (KPTS).
- A corner coordinate table of the final grid.
- A summary of the interpolation results. A line is printed for each interpolated point whose accuracy may be questioned. The meaning of the IER parameter may be found in the RAIN1 listing in Appendix I.

d. Plotted Output

The contour lines of the input file are plotted with the local parallels and meridians overlaid. The resultant subregion represented by the output grid is outlined by a rectangle with labeled axes. The axis values are referenced to the desired grid origin and not the resultant grid origin, the latter being at (0,0) always.

e. Programming Notes on Contour Data Interpolation

Subroutine RAIN2, the interpolation routine used by GENBOT, is aptly suited to interpolate points that are more or less randomly spread in both horizontal directions. The nature of contour data, however, is typically a collection of closely spaced depth values along widely spaced

contour (compare Figures III.1. and A.1.). This type of data arrangement frequently results in a colinearity problem for RAIN2, which can be resolved only by searching ever widening data cells for a non-colinear point, resulting in a degradation of accuracy. In addition, the routine is highly sensitive to contour line kinks which result in right-angle deviations in the interpolated contour lines (which may be plotted by GRDCHK).

Correcting the deficiencies of an interpolating routine is beyond the scope of this research, but the Naval Research Laboratory, Arctic Section, is currently investigating methods for generating grid-matrices from contour data. Users are encouraged to modify the code used in GENBOT as desired to produce results which more closely reflect the actual data supplied.

4. Input Contour Data Format

As stated previously, some contour data already exists in a format usable by GENBOT, but if data is supplied by another source, it must be arranged in a file in the manner and format specified below. All records are 80 byte card images.

The first record of the file contains data on the file itself. GENBOT uses a 4I5 field to represent the origin latitude/longitude pair, the number of contour lines in the file, and the number of card images it may expect to read.

Contour line data exists as separate sequences of cards and may appear in any part of the file as long as each line or line segment is in an unbroken sequence with a header card. The header card must contain the line's depth in hundreds of meters, right justified in a I4 field in columns 41-44. The cards following the header card contain the latitude/longitude pairs in degrees and decimals of degrees of the points along

the contour line in the form of four pairs of coordinates (in FORTRAN fields 8F10.5) per card. South and west values are negative. A value greater than 90.0 in magnitude in any latitude field is interpreted as the end of data for the contour line, and GENBOT expects the next record to be either another contour line header label, the end of the file, or a depth value position record.

Depth value position records are optional and are used during the chart-drawing phase of the program to place alphanumeric symbols on the chart product. They may exist any place after the first record in the file except imbedded in a contour line sequence. Columns 4-8 must contain "NAME" in an A4 field, columns 19-38 contain the latitude and longitude of the symbols in a 2F10.5 field and the symbols themselves must be in columns 46-47. These records are normally used to draw depth values in hundreds of meters on the contour lines.

If the user wishes to use GENBOT on externally supplied contour data, it is recommended that a dump be performed on one of the smaller files (such as CONF13) of the GENBOT data tape to verify the required format for adaptation.

5. Output Grid Data Format

GENBOT constructs the output file in accordance with GRDSCT requirements. Since GRDSCT is the subroutine used by TRACER (of ECTRACE), G3DP and GRDCHK, any externally supplied grid data must all be of the same structure as outlined below in order to be used by those programs. Again, all records are card images.

- a. The first two records contain the input grid title in the 10A8 fields.
- b. The third record contains the input latitude and longitude of the

grid center, the point spacing, and the number of rows and columns of the matrix representing the grid. The record format is (3F10.5,2I5).

c. The fourth and remaining records contain ten depth values per card, in kilometers, as 10F8.4 fields, beginning with column one ($y = 0$) and proceeding all x-values before going to the next column, in accordance with the FORTRAN convention of columnar storage of matrices.

APPENDIX B
SYNGEN DESCRIPTION AND USER INSTRUCTIONS

1. Program Description

a. SYNGEN is a collection of simple functions which may be selectively used to generate and record a matrix of depth values representing a desired synthetic bottom configuration. Six bottom cases are provided (see below), but the program may be easily modified by the user to produce a case not described here. A program listing is provided in Appendix H.

The user selected parameters are:

- CNLAT - any desired center latitude value.
- CNLON - any desired center longitude value. These parameters are requested in compliance with the required output file format.
- DMIN - the minimum depth value (D_1) to be attained within a 75 km radius from the grid center.
- DMAX - the maximum depth value (D_0) within the same radius.
- ITYPE - an integer code for the bottom type desired.

b. Table B.1 lists the ITYPE code, the bottom type, the functions used to generate the depth matrix, and the matrix dimensions. All grids represent a region covering a 150 km in both the x and y directions, but the matrix size will be 11 by 11 or 151 by 151, depending upon the bottom type (DHW values are 15 km and 1 km, respectively). In all cases,

$$\Delta D = D_1 - D_0.$$

c. The depth file provided by SYNGEN conforms to the format required by ECTRACE, GRDCHK, and G3DP. When one of these programs uses a SYNGEN product, the array dimension in the program's source code must be checked to conform to the dimensions of the generated matrix.

TABLE B.I
SYNTHETIC SEA BED FUNCTIONS

<u>ITYPE</u>	<u>Type</u>	<u>Function</u>	<u>Parameters</u>	<u>Matrix Dimensions</u>
12	Wedge	$H = D_1 - \gamma$	$\gamma = \Delta D/135$ $0 \leq x \leq 135$	11 x 11
13	Ridge	$H = D_0 + \gamma \delta(x) $ $H = D_0$ elsewhere	$\gamma = \Delta D/15$ $\delta(x) = x - 75$ $60 \leq x \leq 90$	11 x 11
14	Trough	$H = D_1 - \gamma \delta(x) $ $H = D_1$ elsewhere	$\delta = \Delta D/15$ $\delta(x) = x - 75$ $60 \leq x \leq 90$	11 x 11
15	Conical Seamount	$H = D_0 + \gamma r$ $H = D_0$ elsewhere	$\gamma = \Delta D/75$ $r = \sqrt{(x - 75)^2 + (y - 75)^2}$	151 x 151
16	Sinusoidal Undulation	$H = D_0 \gamma [1 + \cos\{\delta(x)/R\}]$	$\gamma = \Delta D/2$ $\delta(x) = 2(x - 75)$ $R = 15$	151 x 151
17	Parabolic basin	$H = D_1 - \gamma r^2$	$\gamma = \Delta D/(75)^2$ $r = \sqrt{(x - 75)^2 + (y - 75)^2}$	151 x 151

2. User Instructions

THE JCL of a sample deck are arranged as follows:

```
//(Standard JOB card),TIME=2
// EXEC FORTCLG, REGION.GO=250K
//FORT.SYSIN DD *
    (SYNGEN source code)
/*
//GO.FT02FO01 DD UNIT=3330,VOL=SER=DISK03,
// DSN=S9999.SYNBED, DCB=(RECFM=FB,LRECL=80,BLKSIZE=800),
// DSP=(NEW,KEEP), SPACE=(TRK,20)
//GO.SYSIN DD *
    (user selected data)
/*
```

Notice that the output data set is directed to DISK03. The DSN is the user's selection for the data set name in accordance with NPS system requirements. A 151 x 151 depth matrix requires twenty tracks of disk space on a 3330 device.

Only one data card is needed to supply the program with the user's parameter selections. Its field descriptor is (4F10.5,I5) and contains the values reflected in the same order as listed in paragraph 1.a.

APPENDIX C
G3DP DESCRIPTION AND USER INSTRUCTIONS

1. Program Description

a. G3DP uses the NPS library subroutine PLT3D1 [Ref. 12] to draw a perspective surface plot of a subset of a depth matrix. This plot is a normal projection of the surface using a focal length and line-of-sight calculated from the user's selections for the viewpoint position angles DEGUP and DEGCW. As the variable names imply, the viewer is elevated DEGUP degrees from a reference depth and rotated DEGCW clockwise from a south-to-north viewing aspect. For example, the standard working matrix (dimensioned 151 by 151) is best viewed with DEGUP and DEGCW values of 30 degrees and 45 degrees respectively, providing the same viewing aspect demonstrated in all the the G3DP products printed in this report. Using a DEGUP value of zero results in an isometric rather than a perspective projection. The DEGCW selection should be between zero and 89 degrees (south-north to west-east viewing aspects).

b. As in ECTRACE and GRDCHK, G3DP requires source code modification by the user to tailor the program to the desired dimensions of the working matrix. Instructions in this regard are included as comments in the FORTRAN listing (Appendix K).

c. An important characteristic of G3DP is that it uses only the odd-numbered rows and columns of the working matrix to produce the surface plot. This reduction in resolution is required to reduce core requirements and unclutter the graphic output caused by typically large (greater than 75 by 75) working matrices.

2. User Instructions

The JCL of a sample program deck are arranged as follows:

```
//(Standard JOB card),TIME=2
//EXEC FORTCLGW,REGION.GO=300K (Appendix O.)
//FORT.SYSIN DD*
    (G3DP source code)
/*
//LINK.USDD UNIT=3330,VOL=SER=DISK01,DSN=1570. ECTRACE,
// DISP=SHR,LABEL=( , , ,IN)
//LINK.SYSIN DD*
    INCLUDE USDD(GRDSCT)
    ENTRY MAIN
/*
//GO.FTOLF

//GO.SYSIN DD*
    (user-selected data)
/*
```

The LINK step provides access to GRDSCT for loading the working matrix from the input file. The input data set is the same example used in ECTRACE and GRDCHK. The card input data are user selected and contained on one card, as follows (FORTRAN field descriptor 5F8.3)

- XST - working grid matrix x-origin relative to that of the input grid (km).
- YST - working grid-matrix y-origin relative to that of the input grid (km).
- DEGUP - viewpoint elevation angle ($0 \leq \text{DEGUP} \leq 89$ degrees).

- DEGCW - viewpoint rotation angle from south to north
($0 \leq \text{DEGCW} \leq 89$ degrees).
- LW - width of the plot ($5 \leq \text{LW} \leq 18$ inches).

APPENDIX D
GRDCHK-USER INSTRUCTIONS AND OUTPUT DESCRIPTION

1. Purpose and Output Description

Cases may arise where the accuracy of depth values in a generated matrix may be in question because of data sparsity, interpolation deficiencies or other reasons. Program GRDCHK assists in evaluating the generated grid by printing and plotting selected columns of the matrix for comparison with that of the source contours. The contour plot may also be used on a light table with an ECTRACE or ECCOM horizontal-ray trace plot (Figs. 5, 6, and 7).

The NPS library routine CONTUR is called for producing the contour plot. Subroutine GEOPLR is a modified version of GEOPLT to accommodate the rotated plot produced by CONTUR..

2. User Instructions

To aid in this discussion refer to a computer listing of GRDCHK code in Appendix J. A listing of the CONTUR subroutine may be found in Ref. 6.

The following example applies to a standard 151 by 151 working grid. Below is a listing of the JCL cards and the position of the program deck.

```
//(Standard job card), TIME=5
// EXEC FORTCGLW,REGION.GO=350K
//FORT.SYSIN DD *
    (GRDCHK,CORNER,GEOPLT,GEODST source decks)
/*
```

The following DD statements link to a member of ECTRACE for allocating a working subregion of the input.

```
//LINK.USDD DD UNIT=3330,VOL=SER=DISK01,
```

```
// DSN=1570.ECTRACE,DISP=SHR,LABEL=(,,IN)
```

```
//LINK.SYSIN DD *
```

```
INCLUDE USDD (GRDSCT)
```

```
ENTRY MAIN
```

```
/*
```

Next follows the DD statement identifying the depth matrix input file.

The same example is used for the GENBOT output file.

```
//GO.FTOFOO1 DD DSN=S9999.GRID,UNIT=3330,VOL=SER=DISK03,
```

```
// DISP=SHR, LABEL=(,,IN)
```

Finally the user input parameters are included. The card

```
//GO.SYSIN DD *
```

is followed by:

<u>Card</u>	<u>Parameter Names</u>	<u>FORTRAN field description</u>
1	NL, LEN	2I5
2	ZST, ZEND, XMIN, YMIN	4F6.1
3	IPS, IPE, JPS, JPE	4I5

where

- NL is the number of contour levels desired. The shallowest and deepest levels, if known, should be read into ZST and ZEND. If the boundary levels are not known, NL should be made negative, and subroutine CONTUR will calculate the boundary and contour levels. If NL is greater in magnitude than 100, no contour plot will be produced.
- LEN is the length of the contour plot's longest side in inches. If LEN is negative, a cartesian grid will be drawn on the contour plot instead of geographic coordinate lines. If LEN is less than 4, no contour plot will be produced. The maximum

magnitude of LEN is 19 inches.

- ZST AND ZEND are estimates of the smallest and largest values in the working matrix (ZB).
- XMIN and YMIN establish the origin of the working matrix relative to that of the input matrix. The program assignments for KMX and KMY, the recorded cell spacing DHN, and the dimensions of the working matrix determine the subregion size parameters in the same manner as they do in ECTRACE, since subroutine GRDSCT is linked to this program. In effect, the user must tailor certain portions of the program cards to compensate for the FORTRAN G inability to perform object time dimensioning.
- IPS, IPE, JPS and JPE identify the beginning and end rows and columns of the working depth matrix to be singled out for inspection. Thus, if ZB is dimensioned (150,150) and the above values are 1, 150, 74, and 78 respectively, GRDCHK will print the depth values of these 750 elements of the ZB matrix and plot five columnar profiles (Fig. 4). If this record is omitted, only the contour plot will be produced.

APPENDIX E
ECCOM OUTPUT DESCRIPTION AND USER INSTRUCTIONS

1. Description of Output

ECCOM allows the user to combine several selected ECTRACE runs and eliminate specific rays as desired to produce an improved horizontal ray path plot for investigation of curvature (Fig. 7 and Fig. 18). The size of the ECCOM plot will be the same size as first ECTRACE run of the input card deck unless the user opts to alter the scale factor (FACT) to control the plot dimensions.

The printed output is a list of all the rays processed for the ECCOM plot, giving each ray's initial elevation angle and heading. Additionally, the number of points used to plot each ray path is printed. This number of points corresponds to the number of reflections plus the starting point of the ray. Refer to Table VII for a sample listing of data for the ECCOM 51 plot, shown in Fig. 7.

2. User Instructions

The following JCL cards and parameters are required for an ECCOM run:

- JOB card - The CPU time parameter should allow four seconds for every 55 rays to be plotted.
- EXEC card - This card must specify FORTCLGW procedure.
- Calling program - Following the

//FORT.SYSIN DD *

is the ECCOM program deck. See Appendix L for the program listing.

- Data cards--Following the

//GO.SYSIN DD *

is the sequence of punched output decks, each individually arranged as described in Chapter V, Section C. The user may change the title

card (card # 1) of the first ECTRACE punched deck to identify the ECCOM run title. In addition, the user may change the scale factor (FACT) on card number 4 to modify the plot size. FACT was calculated by ECTRACE in response to the user's selection for the horizontal plot length (Chapter V, Section B). The following are sample values of FACT and recommended limits:

<u>FACT</u>	<u>Horizontal Plot Axis Length (inches)</u>
0.333	5 (minimum recommended)
1.000	15
1.267	19 (maximum recommended)

If the user desires a plot size outside the range recommended, refer to Ref. 7.

Cards 1 through 4 of each ECTRACE deck after the first are ignored by ECCOM, but the user should verify that they all reference the same portion of the same input grid-matrix in order for the ECCOM plot to be meaningful.

APPENDIX F
ANALYTICAL VERIFICATION OF ECTRACE HORIZONTAL RAY PATHS

The accumulation of ray heading changes after repeated specular reflection from a sloping sea bed describes a faceted horizontal path whose apparent curvature may in some instances be analytically described. Harrison [2] derived some solutions for horizontal ray paths over simple bottom topography cases. Most of these cases may be modeled by SYNGEN and used to test the validity of the horizontal ray paths mapped by ECTRACE. We chose an isovelocity sound speed condition and a conical seamount because its surface geometry effectively challenges the facet method of topographical modeling.

For a conical seamount of arbitrary slope but whose apex just touches the sea surface, Harrison gives the ray paths in polar coordinates (r, ϕ) as

$$r = r_0 (1 - \cos^2 \theta_0 \cos^2 \phi_0)^{\frac{1}{2}} \cdot \operatorname{cosec} \left| \frac{(1 - \cos^2 \theta_0 \cos^2 \phi)^{\frac{1}{2}}}{\sin \phi_0 \cos \theta_0} (\phi + \phi') \right|, \quad (\text{F.1})$$

where

- r_0 = initial distance from the apex
- θ_0 = initial deviation angle
- ϕ_0 = initial azimuthal angle
- ϕ' = a constant given by setting $\phi = 0$ when $r = r_0$,

$$\phi' = \frac{\sin \phi_0 \cos \theta_0}{(1 - \cos^2 \theta_0 \cos^2 \phi_0)^{\frac{1}{2}}} \sin^{-1} (1 - \cos^2 \theta_0 \cos^2 \phi_0)^{\frac{1}{2}} \quad (\text{F.2})$$

Figure F.1. is a diagram of a representative ray path. α is the deflection angle and represents the asymptotic angle of the shadow zone of the ray fan.

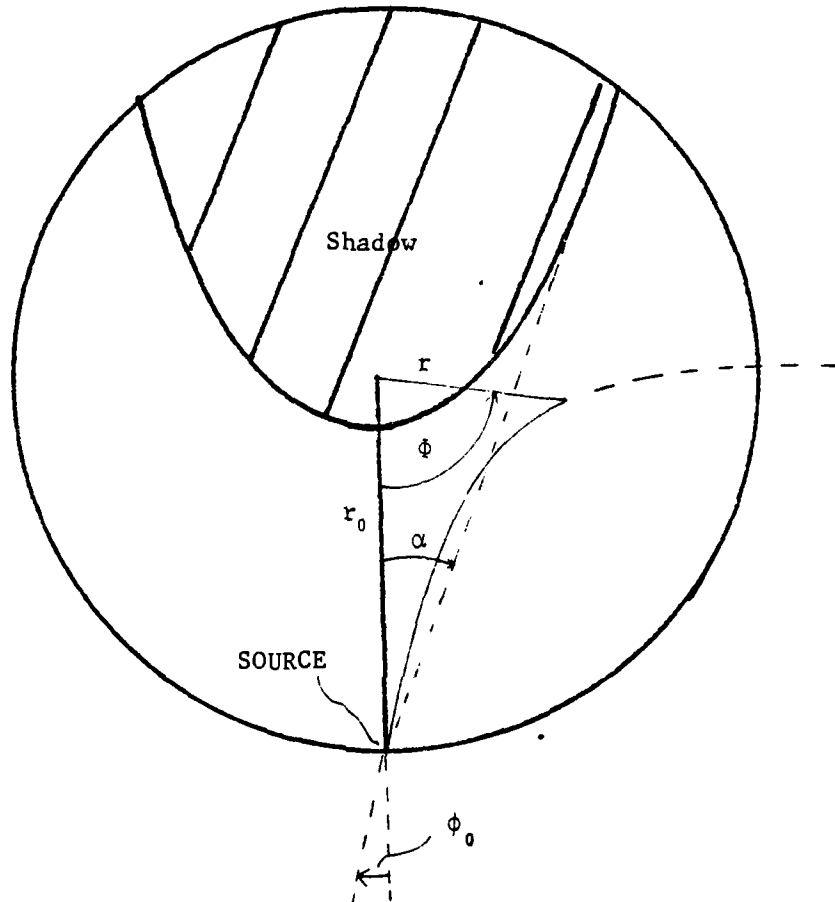


FIGURE F.1. Polar representation of the horizontal projection of a ray path for a conical seamount.

In the test run (Trial 83, Fig. F.2), the source was positioned at a range r_0 of 50 km from the apex, bearing 180° , at a depth just below the surface. The receiver was placed at the apex so that for each ray the ECTRACE range r_E could be read directly from the printed ray history table values for DIST TO REC and ϕ is the reciprocal of BNG TO REC. A zero gradient was used.

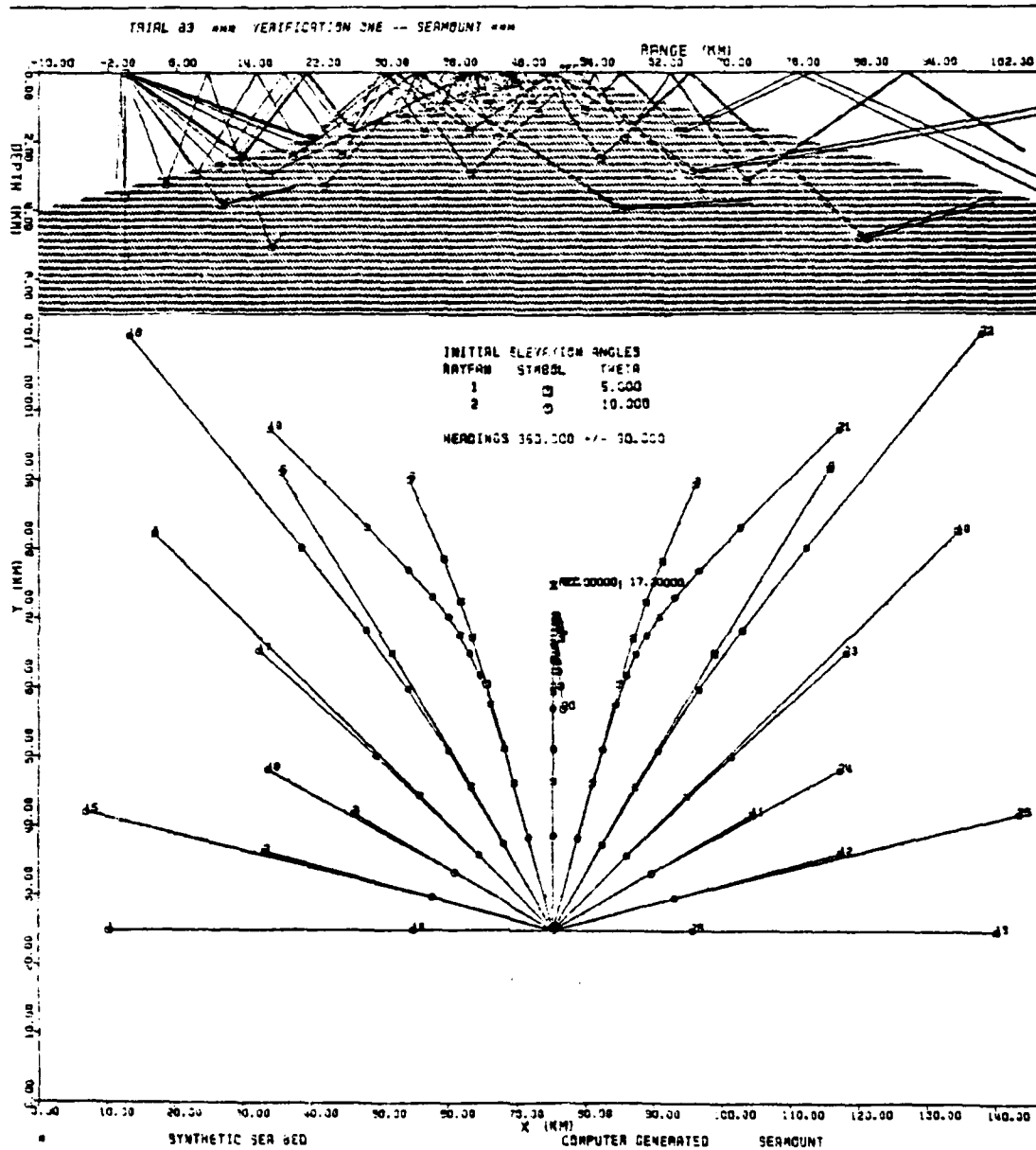


FIGURE F.2. Horizontal Plot of ECTRACE Trial for Harrison Verification.

Two ray lines were projected using $\theta_0 = 5$ degrees for ray fan 1 and $\theta_0 = 10$ degrees for ray fan 2. ϕ_0 ranged from 270° for the first ray to 90° for the last ray in each fan, with an increment of 15° between rays. Two rays were chosen for analysis, ray 6 ($\theta_0 = 5$ degrees, $\phi_0 = -15$ degrees) and ray 21 ($\theta_0 = 10$ degrees, $\phi_0 = 15$ degrees). The relevant portions of their trace histories are reproduced in Table F.I and Table F.II. Only the surface reflection values are used, where the slant range DIST becomes the horizontal range r_E . Inserting θ_0 and ϕ_0 values into Eq. (F.1), loaded in a programmable calculator, we obtained a table of values for r for both rays. The results are shown in Table F.III and Table F.IV alongside the ECTRACE values r_E and the observed error $\epsilon = r - r_E$. These same results are plotted in Figures F.3 and F.4 (r vs ϕ).

TABLE F.I

RAY 6 (6 OF RAY FAN 1) TRACE HISTORY

REV NO.	TYPES	DEPTH (KM)	GRID HEADING	ELEV ANGLE	BRNG TO REC	DIST FM REC
0	INIT	0.001	345.000	5.000	360.000	50.000
1	BOTT	1.943	344.500	-11.825	11.370	29.200
2	SURF	0.0	344.500	11.825	22.736	21.277
3	BOTT	1.153	343.010	-16.653	34.104	17.329
4	SURF	0.0	343.010	16.653	45.508	15.170
5	BOTT	0.934	340.647	-18.460	56.912	14.035
6	SURF	0.0	340.847	18.460	68.425	13.614
7	BOTT	0.919	338.231	-17.062	79.942	13.816
8	SURF	0.0	338.231	17.062	91.462	14.689
9	BOTT	1.096	336.557	-12.677	102.980	16.464
10	SURF	0.0	336.557	12.677	114.448	19.713
11	BOTT	1.729	335.915	-6.020	125.912	25.991
12	SURF	0.0	335.915	6.020	137.458	40.960

TABLE F.II

RAY 21 (8 OF RAY FAN 2) TRACE HISTORY

REV. NO.	TYPES	DEPTH (KM)	GRID HEADING	ELEV ANGLE	BRNG TO REC	DIST FM REC
0	INIT	0.001	15.000	10.000	360.000	50.000
1	BOTT	2.451	15.649	-17.119	354.386	36.838
2	SURF	0.0	15.649	17.119	348.770	29.483
3	BOTT	1.654	17.253	-23.468	343.153	24.866
4	SURF	0.0	17.253	23.468	337.518	21.761
5	BOTT	1.303	20.043	-28.702	331.883	19.590
6	SURF	0.0	20.043	28.702	326.243	18.046
7	BOTT	1.128	24.047	-32.594	320.603	16.949
8	SURF	0.0	24.047	32.594	315.014	16.200
9	BOTT	1.046	28.867	-33.973	309.425	15.723
10	SURF	0.0	28.867	33.973	303.767	15.480
11	BOTT	1.029	34.081	-33.685	298.105	15.459
12	SURF	0.0	34.081	33.685	293.479	15.661
13	BOTT	1.071	38.566	-31.042	286.852	16.097
14	SURF	0.0	38.566	31.042	281.203	16.802
15	BOTT	1.187	41.986	-26.620	275.55	17.834
16	SURF	0.0	41.986	26.620	269.889	19.295
17	BOTT	1.420	44.169	-20.799	264.224	21.345
18	SURF	0.0	44.169	29.799	258.538	24.279
19	BOTT	1.904	45.278	-14.066	252.851	28.620
20	SURF	0.0	45.278	14.066	247.160	35.467
21	BOTT	3.160	45.674	-6.733	241.469	47.511
22	SURF	0.0	45.674	6.733	235.781	73.529

TABLE F.III
 Trial 83 Ray 6

ϕ	r	r_E	ϵ
0.0°	50.0 km	50.0 km	0.0km
-22.736	21.262	21.277	-0.015
-45.408	15.176	15.170	0.006
-68.425	13.616	13.614	0.002
-91.462	14.713	14.689	0.024
-114.49	19.822	19.713	0.109
-137.46	41.571	40.960	0.611

Ray 7 $r_{E_{ce}} = 4.339 \text{ km}$

($\phi = \phi$, constant)

$r_{ce} - r_{E_{ce}} = 0.019 \text{ km}$

TABLE F.IV

Trial 83 Ray 21

ϕ	r	r_E	ϵ
0.0°	50.0 km.	50.0 km	0.0 km
11.230	29.470	29.483	-0.013
22.482	21.745	21.761	-0.016
33.757	18.026	18.046	-0.020
44.986	16.178	16.200	-0.022
56.233	15.548	15.480	-0.022
67.521	15.643	15.661	-0.018
78.797	16.791	16.802	-0.011
90.111	19.309	19.295	0.014
101.46	24.365	24.279	0.086
112.84	35.822	35.467	0.355
124.219	75.857	73.529	2.238

Ray 20 $r_{E_{ce}} = 8.687$ km ($\phi = 0$, constant)

$r_{ce} - r_{E_{ce}} = -0.005$ km

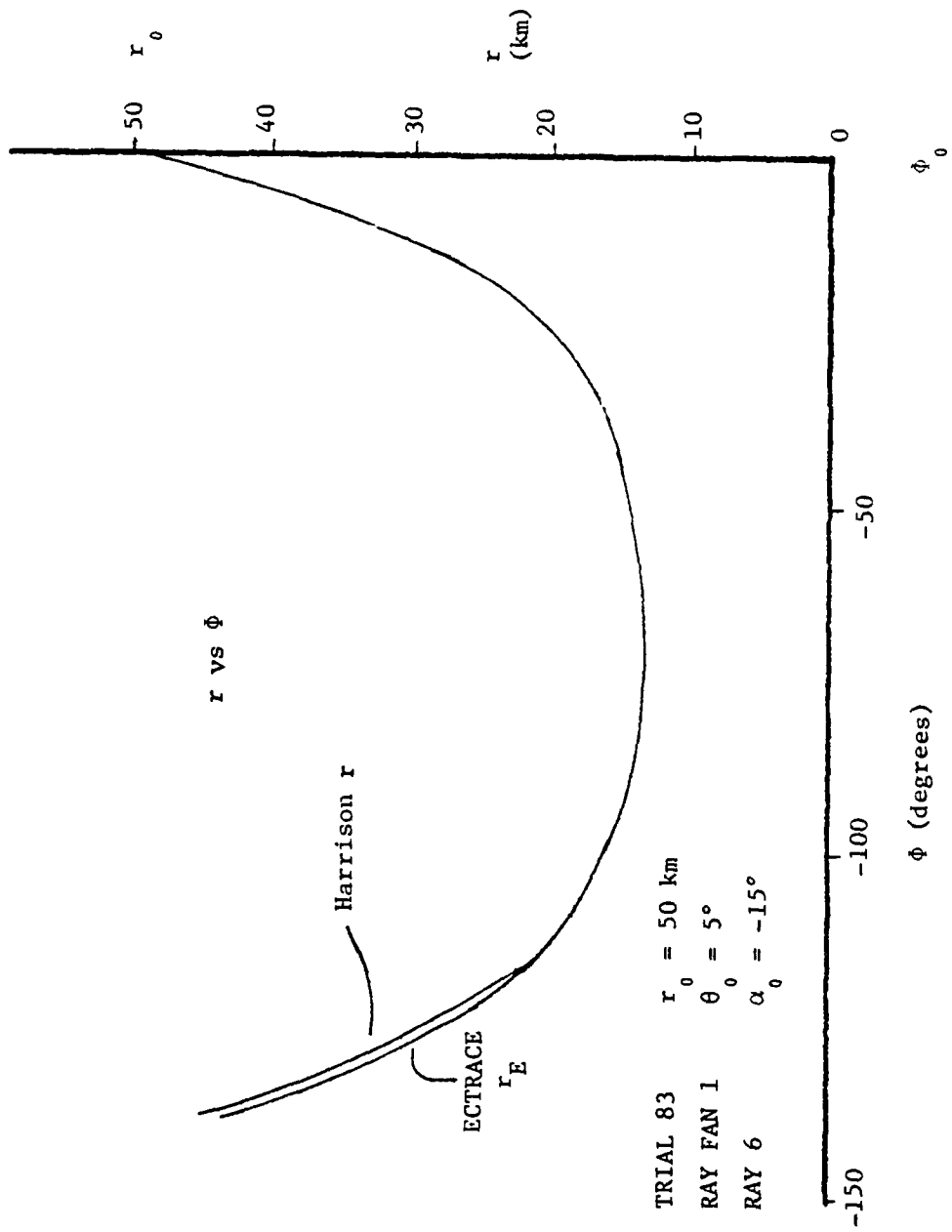


FIGURE F.3. Harrison verification plot of range vs ϕ for ray 6.

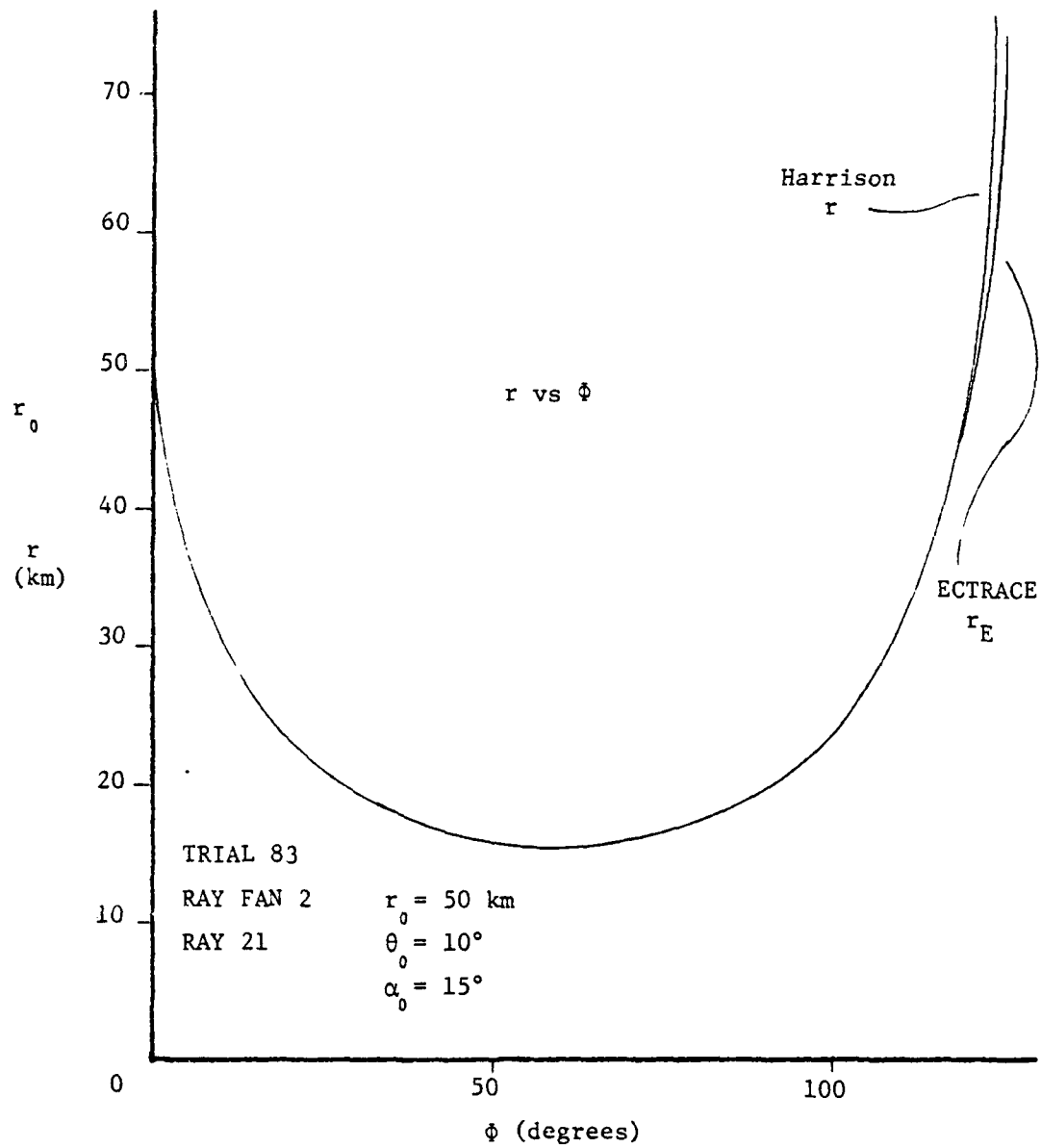


FIGURE F.4. Harrison Verification Plot of range vs ϕ for ray 21

These results show very close agreement up to a distance well past the closest point of approach, and only begin to diverge slightly when the rays approach their asymptotic values for Φ . Investigation of other rays of the same trial supports this observation. Clearly the fact that the plane facets do not all have the same slope as the cone they collectively represent, but vary as much as 4% between their extremes, explains most of the error. The validity of the model decreases near the apex, where fewer data points and hence plane facets are used to approximate the conical surface. In addition, the progressively shallower grazing angles assumed by the rays after CPA cause the horizontal paths to become more sensitive to this facet effect.

Reference 13 also provides an equation for the closest approach of the ray fan envelope to the seamount center, developed by letting $\phi_0 = 0$ in Eq. (F.1). Thus

$$\begin{aligned} r_{ce} &= r_0 \sin \theta_0 \\ &= 8.682 \text{ km.} \end{aligned} \quad (\text{F.3})$$

Ray 21 of Trial 83 was the radial ray ($\phi_0 = 0^\circ$) and its CPA on the printout was 8.687 km, a difference of only four meters after 11 reflections from the bottom model. The ray should have reversed its heading exactly 180 degrees after CPA, but actually experienced a 174 degree heading change, revealing the sensitivity of the model to radially-directed ray paths.

Lastly, Ref. 13 defines the asymptotic angle of the shadow zone of the ray fan (Fig. F.1). A plot of the final azimuthal angle ϕ_f versus θ_0 for ray fan 2 (Fig. F.5) of the test run exhibits an interpolated value for α of 40 degrees for $\phi_0 = 29$ degrees. Testing this value with

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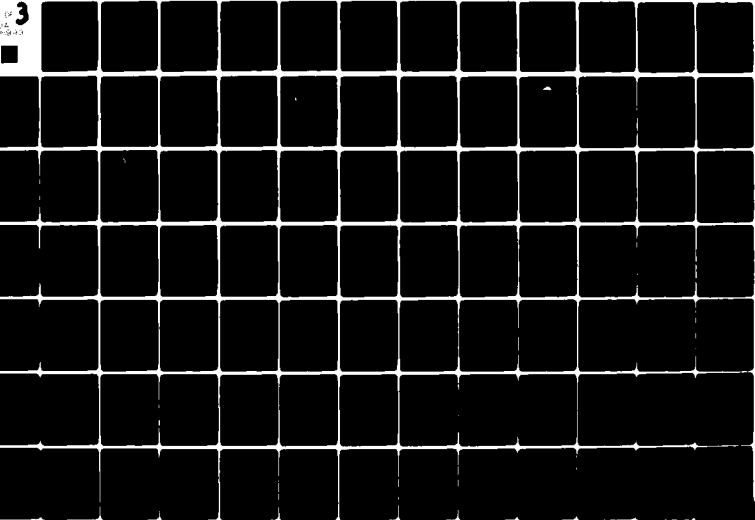
NAVAL POSTGRADUATE SCHOOL MONTEREY CA
ECTRACE - THREE DIMENSIONAL ACOUSTIC RAY TRACE PROGRAM.(U)
MAR 80 R N CHRISTIANSON, L R ERAZO

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2 of 3
3





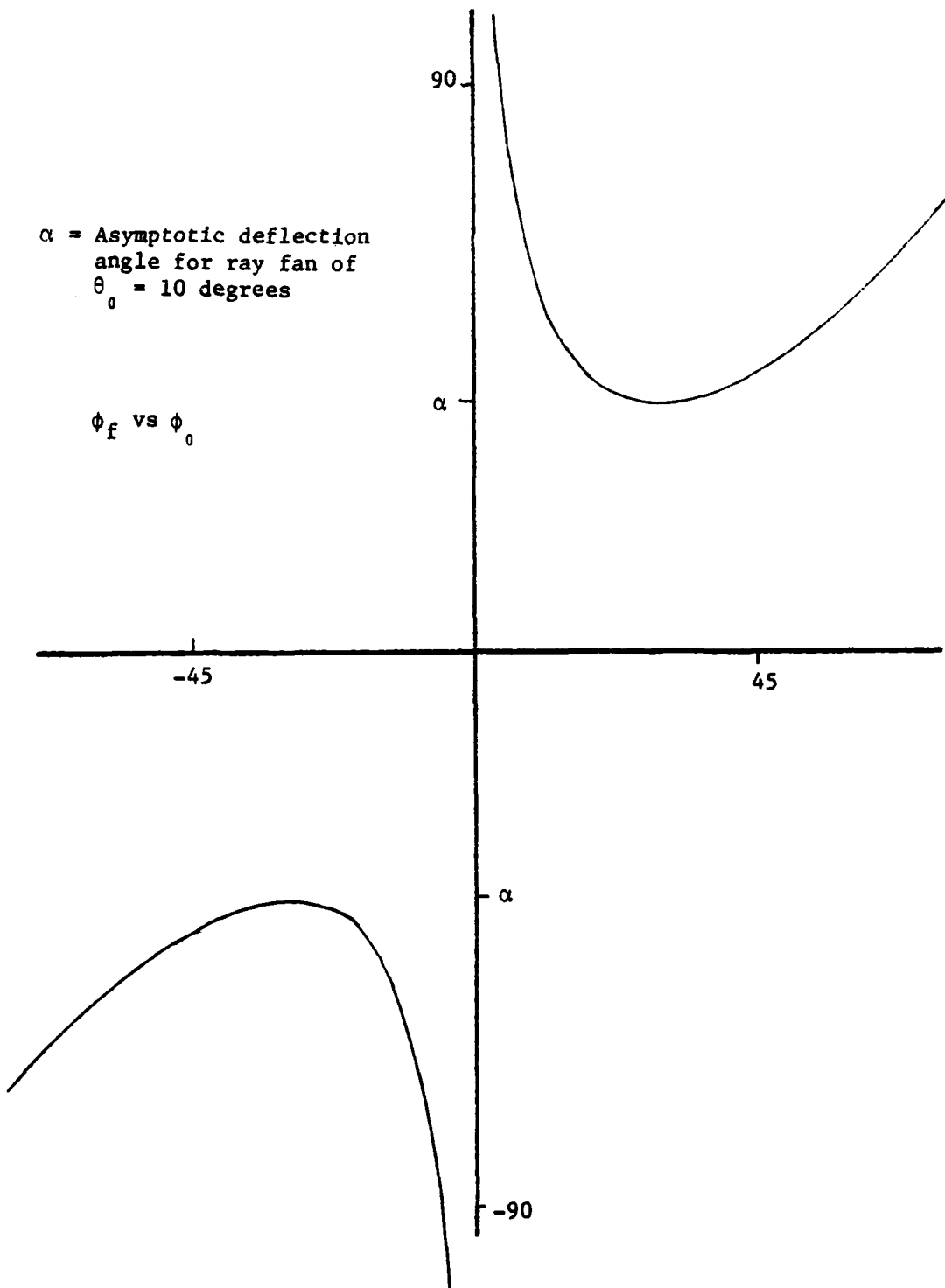


FIGURE F.5. Harrison verification plot of ϕ_f vs ϕ_0 .

the formula

$$\alpha = \frac{3}{2}(\pi \sin^2 \theta_0)^{1/3}$$
$$= 39.187 \text{ degrees} \quad (\text{F.4})$$

shows close agreement with the theoretical value. Figure F.6, an ECCOM composite for the seamount, is a graphic example of the dependence of α on the initial elevation angle.

It is worth noting that the analytical expressions for horizontal projections of ray paths apply only to exact functional bottom topographies and that the curved three dimensional ray path surfaces only approximate an actual surface of vertical planes joined at bottom reflection points.

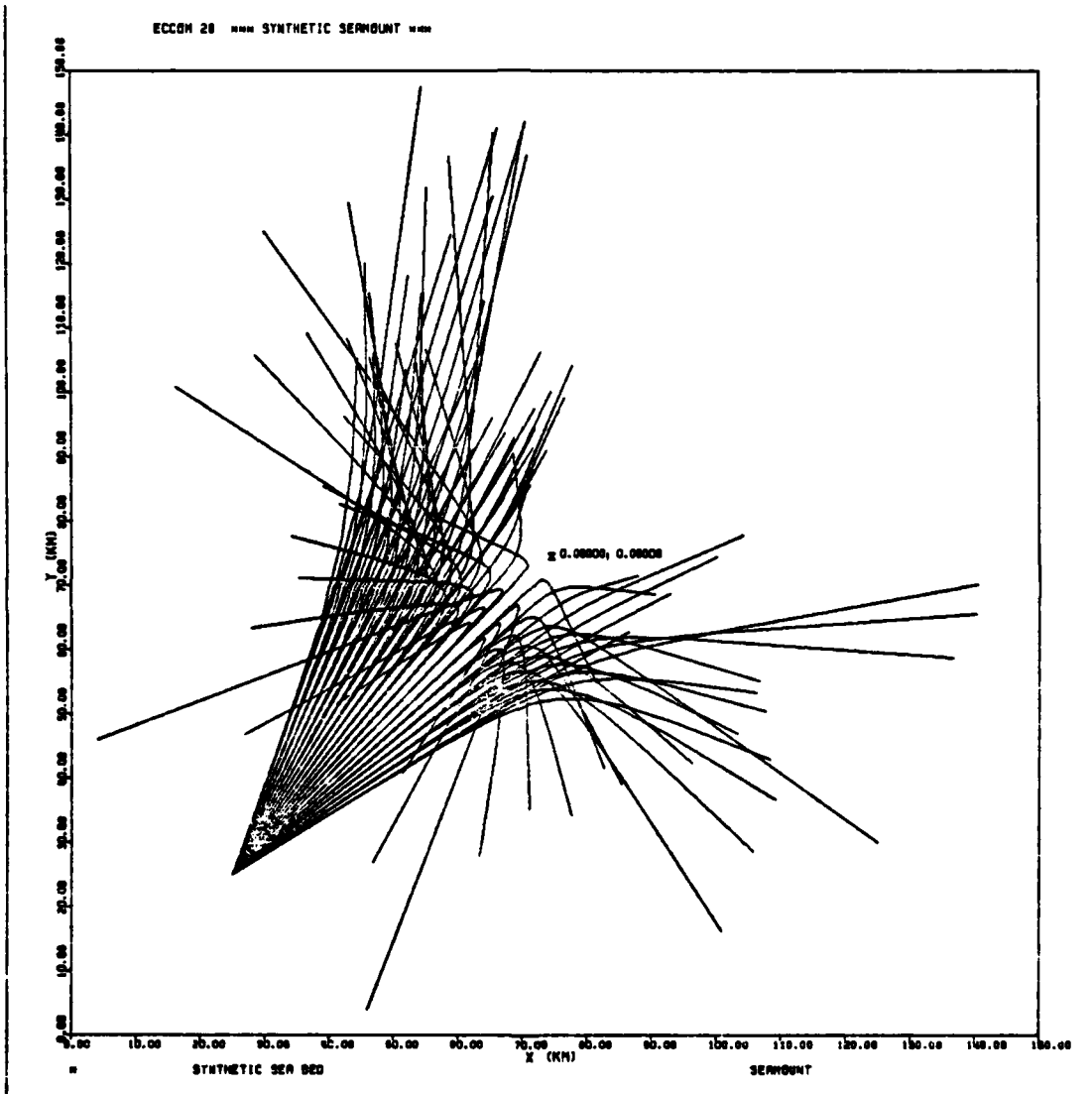


FIGURE F.6. ECCOM Trial 28 showing the effect of a synthetic conical seamount on ray propagation. The ray's initial headings varied from 20° to 58° and the initial elevation varied from 4° to 18° . Selected rays from five ECTRACE runs (100 rays) were combined.

APPENDIX G
TABLES
TABLE I

A SUMMARY OF THE PROGRAMS AND THEIR COMPONENT SUBPROGRAMS

- I. GENBOT - plots source contour data and generates depth matrix
 - A. CORNER - calculates boundary coordinates
 - B. GEOPLT - plots geometric grid lines
 - C. GEODST - solves geodetic triangle
 - D. RAIN 1/2/3 - perform sorting and interpolation (from SSP3)

- II. SYNGEN - produces synthetic sea bed depth matrices

- III. G3DP - produces perspective surface plot of depth matrix
 - A. GRDSCT - loads working surface plot of depth matrix
 - B. PLT3D1 - draws surface plot (from NPS)

- IV. GRDCHK - allows inspection of depth matrix and draws contour plot of same
 - A. GRDSCT - see above
 - B. CORNER - see above
 - C. GEOPLR - same as GEOPLT but for a rotated plot
 - D. GEODST - see above
 - E. CONTUR - draws a contour plot of depth matrix (from NPS)

- V. ECTRACE - a collection of subprograms which perform ray tracing
 - A. TRACER - controls all subprograms and manages ray traces
 - B. GRDSCT - see above
 - C. IDTSUB - identifies subscripts of depth matrix
 - D. DEEP - calculates depth at given coordinates
 - E. IDPROF - identifies water mass
 - F. NUPROF - calculates water mass parameters
 - G. CHNLIM - calculates sound channel limits
 - H. CONTAC - calculates point of bottom contact
 - I. BOANG - calculates direction and grazing angle of bottom reflected ray
 - J. FBLOSS - calculates bottom loss
 - K. ANGPRT - prints ray fan bottom bounce table
 - L. BNGPLT - initializes plotting and draws plot borders
 - M. BDTPLT - draws bathymetry profile
 - N. RNGPLT - draws vertical plot
 - O. T2DPLT - draws horizontal plot
 - P. SSPPLT - draws sound speed profiles
 - Q. ENDPLT - draws plot legend and terminates plotting

(L through Q call subroutines from the Versatec software package.)

TABLE II
INPUT PARAMETERS TABLEAU (COMPUTER PRINT OUTPUT)

ECTRACE TRIAL 67 *** SYNTHETIC BASIN ***

SOUND SPEED PROFILES

ZC	C(ZC)	GRAD
0.0	1461.08	0.0
50.00	1461.00	-1.40000
60.00	1447.00	-0.20000
70.00	1445.00	0.10000
90.00	1447.00	0.01780
500.00	1454.30	0.01218
1050.00	1461.00	0.02000
1500.00	1470.00	0.01668
4000.00	1511.70	0.01668

NWMR (Northwest Mohns Ridge)

ZC	C(ZC)	GRAD
0.0	1490.00	-0.16000
50.00	1482.00	-0.05000
200.00	1474.50	-0.00286
375.00	1474.00	-0.02133
750.00	1466.00	-0.00444
975.00	1465.00	0.00727
1250.00	1467.00	0.01200
1500.00	1470.00	0.01668
4000.00	1511.70	0.01668

SEMR (Southeast Mohns Ridge)

ZC	C(ZC)	GRAD
0.0	1470.00	0.0
1500.00	1470.00	0.01668
4000.00	1511.70	0.01668

ISOV (Isovelocity)

(Table II continued)

continued TABLE II

FRONT/BOUNDARY INTERSECTIONS

FRONT		FRONT	
ENTRY	EXIT	ENTRY	EXIT
(0.0, 50.0)	(100.0,150.0)	(50.0, 0.0)	(150.0, 100.0)

GRID FILE CALLED *****
*
* SYNTHETIC SEA BED *
* COMPUTER GENERATED BASIN *

HAD BEEN READ. CENTER LAT/LONG IS 70.07059/ 15.85032 AT
(75.000, 75.000) KM. RANGES ARE 0.0 TO 150.0 KM IN Y (22801 ITEMS).

THE FOLLOWING ADDITIONAL PARAMETERS WERE INPUT:

SOURCE DATA: FREQUENCY 150.00 HZ, GRID COORDINATES (40.00,40.00),
DEPTH 0.850 KM. 8 RAY FANS WILL BE TRACED, FROM -30.0 TO 30.0 DEGREES
ELEVATION, INCREMENTING EVERY 8.6 DEG. 1 RAYS MAKE A RAY FAN FROM 10.0
TO 10.0 DEGREES TRUE HEADING, INCREMENTING EVERY 0.0 DEGREES.

RECEIVER DATA: GRID COORDINATES (125.0, 40.0), DEPTH 1.749 KM.

GRID ARRAY: MAXIMUM ARRAY SIZE (151,151).DEPTH VALUES RESOLVED BY 1.0
KM. SPACING.

TRACE PARAMETERS: PROPAGATION WILL CONTINUE UNTIL A BOTTOM BOUNCE LOSS
OF 150.0 DB OR 21 BOTTOM CONTACTS EXCEEDED FOR EACH
RAY. PATH INCREMENT IS 100.0 M. POSITION ERROR AFTER
BOTTOM CONTACT WITHIN 0.05000 KM. CHANNEL RANGE
LIMIT 200.0 KM. SMALL ANGLE 2.0 DEG.

PLOT OPTION SELECTED.

PLOT PARAMETERS:	X	Y	Z	R
AXES:	0.0	0.0	-1.0	-10.0
	10.0	10.0	2.0	7.00
	150.0	150.0	6.0	123.00

SCALING: LENGTH 4 IN., FACTOR=0.2667

EACH SEGMENT REPRESENTS 10 POSITION CALCULATIONS.

(program parameters are user supplied via DATA cards)

TABLE III

Ray History Tableau ECTRACE Trail 67 (computer print output)
 Ray 8 (of Ray Fan 8) TRACE HISTORY

REV. NO.	TYPE	X(KM)	Y(KM)	DEPTH(KM)	HEADING	ELEV. ANG.
0	INIT	40.000	40.000	0.850	10.000	30.000
1	BOTT	40.722	44.097	3.161	12.533	-20.323
2	SURF	42.397	51.631	0.0	12.533	21.104
3	BOTT	44.611	61.591	4.043	14.157	-14.658
4	SURF	47.628	73.549	0.0	14.157	17.615
5	BOTT	50.933	86.652	4.344	15.556	-14.938
6	SURF	54.384	99.050	0.0	15.556	18.425
7	BOTT	57.154	109.001	3.628	17.472	-22.313
8	SURF	59.508	116.479	0.0	17.472	26.133
9	BOTT	61.260	122.046	2.780	20.496	-31.868
10	SURF	62.747	126.024	0.0	20.496	33.698
11	BOTT	63.904	129.119	2.190	25.415	-41.798
12	SURF	64.930	131.279	0.0	25.415	42.680
13	BOTT	65.778	133.064	1.823	33.460	-51.533
14	SURF	66.569	134.260	0.0	33.460	51.978
15	BOTT	67.260	135.305	1.606	46.953	-60.129
16	SURF	67.933	135.934	0.0	46.953	60.372
17	BOTT	68.551	136.511	1.490	69.313	-65.773
18	SURF	69.182	136.749	0.0	69.313	65.930
19	BOTT	69.787	136.977	1.452	97.778	-66.103
20	SURF	70.428	136.890	0.0	97.778	66.244
21	BOTT	71.073	136.802	1.482	121.284	-61.160
22	SURF	71.771	136.378	0.0	121.284	61.347
23	BOTT	72.510	135.929	1.587	135.723	-53.031
24	SURF	73.338	135.080	0.0	135.723	53.338
25	BOTT	74.265	134.129	1.786	144.372	-43.592
26	SURF	75.339	132.631	0.0	144.372	44.152
27	BOTT	76.618	130.845	2.127	149.526	-34.065
28	SURF	78.158	128.228	0.0	149.526	35.164
29	BOTT	80.046	125.020	2.664	153.024	-26.290
30	SURF	82.376	120.443	0.0	153.024	26.244
31	BOTT	85.445	114.414	3.452	155.238	-19.001
32	SURF	89.145	106.392	0.0	155.238	20.346
33	BOTT	93.855	96.179	4.247	156.763	-15.037
34	SURF	98.821	84.615	0.0	156.763	18.321
35	BOTT	103.807	73.002	4.261	158.297	-17.529
36	SURF	107.968	62.549	0.0	158.297	20.418
37	BOTT	111.257	54.284	3.486	160.557	-25.605
38	SURF	113.497	47.940	0.0	160.557	28.126
39	BOTT	115.211	43.084	2.713	164.103	-35.243
40	SURF	116.231	39.501	0.0	164.103	36.331
41	BOTT	117.049	36.630	2.188	169.812	-45.355

BOTTOM LOSS GATE EXCEED. TERMINATING RAYTRACE AFTER 3311
 SEGMENTS. PLOT BASED ON 367 POINTS, 41 REVERSALS AND 21
 BOTTOM BOUNCES. MINIMUM DISTANCE TO RECEIVER, 8.57 KM,
 OCCURS AT TIME 166.244

(TABLE III continued)

continued TABLE III

BRING TO SRC*	DIST FM SRC*	TIME	WTR MASS	LYR	DEPTH_ MIN	LIMITS MAX
0.0	0.0	0.0	SEMR	5	0.0	*****
190.00	4.759	3.270	SEMR	8	0.0	*****
191.646	11.906	8.802	SEMR	1	0.0	*****
192.056	23.308	16.265	SEMR	9	0.0	7.093
192.809	34.416	24.931	SEMR	1	0.0	7.093
193.189	48.043	34.520	SEMR	9	0.0	7.526
193.690	60.783	43.604	SEMR	1	0.0	7.526
193.961	71.155	51.036	NWMR	8	0.0	*****
194.310	78.932	56.802	NWMR	1	0.0	*****
194.572	84.778	61.279	NWMR	8	0.0	*****
194.812	88.984	64.648	NWMR	1	0.0	*****
195.015	92.279	67.440	NWMR	8	0.0	*****
195.276	94.626	69.600	NWMR	1	0.0	*****
195.483	96.573	71.568	NWMR	8	0.0	*****
195.741	97.936	73.103	NWMR	1	0.0	*****
195.962	99.130	74.624	NWMR	8	0.0	*****
196.234	99.921	75.814	NWMR	1	0.0	*****
196.480	100.647	77.058	NWMR	7	0.0	*****
196.784	101.058	78.109	NWMR	1	0.0	*****
197.074	101.451	79.258	NWMR	7	0.0	*****
197.435	101.559	80.307	NWMR	1	0.0	*****
197.796	101.669	81.494	NWMR	7	0.0	*****
198.245	101.483	82.550	NWMR	1	0.0	*****
198.721	101.290	83.914	NWMR	8	0.0	*****
199.322	100.758	85.183	NWMR	1	0.0	*****
200.003	100.176	86.827	NWMR	8	0.0	*****
200.882	99.146	88.467	NWMR	1	0.0	*****
201.954	97.956	90.673	NWMR	8	0.0	*****
203.388	96.130	93.144	NWMR	1	0.0	*****
205.222	93.996	96.346	SEMR	8	0.0	*****
207.779	90.926	100.139	SEMR	1	0.0	*****
211.412	87.232	105.373	SEMR	8	0.0	*****
216.510	82.606	111.713	SEMR	1	0.0	*****
223.790	77.898	110.854	SEMR	9	0.0	7.469
232.820	73.832	128.722	SEMR	1	0.0	7.469
242.651	71.917	137.727	SEMR	9	0.0	8.687
251.646	71.615	145.718	SEMR	1	0.0	8.687
258.664	72.722	152.236	ISOV	2	0.0	*****
263.834	73.929	157.358	ISOV	1	0.0	*****
267.652	75.297	161.318	ISOV	2	0.0	*****
270.375	76.237	164.413	ISOV	1	0.0	*****
272.504	77.134	166.955	ISOV	2	0.0	*****

*For this run range and bearing of the rays were referenced to the source. As explained in Chapter V, in the current version of ECTRACE, these values are now referenced from the receiver (REC).

(TABLE III continued)

continued TABLE III

C (KM/S)	GRAZ ANGLE	BTM ANGLE	BTM LOSS	LPS
1.46556				
1.49770	24.081	4.678	4.1	0
1.49000				
1.51242	16.731	3.392	6.1	0
1.49000				
1.51743	14.465	2.756	7.2	0
1.49000				
1.50549	19.479	3.935	10.0	1
1.46100				
1.49135	27.785	5.015	15.1	1
1.46100				
1.48151	37.224	5.651	22.2	1
1.46100				
1.47539	46.949	6.015	30.0	0
1.46100				
1.47177	56.159	6.182	40.9	0
1.46100				
1.46980	63.522	6.272	50.9	0
1.46100				
1.46904	66.735	6.262	60.0	0
1.46100				
1.46963	64.227	6.248	70.9	0
1.46100				
1.47145	57.381	6.141	80.9	0
1.46100				
1.47477	48.418	6.040	89.9	0
1.46100				
1.48045	38.786	5.639	97.3	0
1.46100				
1.48941	30.571	5.162	103.0	2
1.49000				
1.50255	22.176	4.155	106.6	0
1.49000				
1.51582	16.287	2.886	108.3	0
1.49000				
1.51606	16.298	2.906	110.1	1
1.49000				
1.50313	22.375	4.256	113.8	0
1.47000				
1.49023	30.985	5.212	119.5	0
1.47000				
1.48147	40.627	5.821	127.3	0

TABLE IV

Ray fan Summary Tableau for ECTRACE Trail 67 ray number 8. (computer print output)

ANGLES BEFORE BOUNCE. INITIAL ELEVATION ANGLE = 30.00

HEADINGS:	10.00
BOUNCE	
1	27.78
2	18.77
3	13.96
4	16.60
5	23.63
6	32.51
7	42.10
8	51.66
9	60.18
10	65.80
11	66.12
12	61.15
13	52.96
14	43.36
15	34.76
16	25.30
17	17.50
18	15.03
19	19.09
20	26.64
21	35.75

DEPTH IN METERS AT BOUNCE. INITIAL ELEVATION ANGLE = 30.00

HEADINGS:	10.00
BOUNCE	
1	3160.6
2	4042.9
3	4343.8
4	3627.9
5	2780.2
6	2190.1
7	1823.4
8	1606.3
9	1490.1
10	1452.0
11	1481.7
12	1586.9
13	1785.7
14	2126.5
15	2663.6
16	3451.5
17	4246.8
18	4261.3
19	3486.1
20	2713.1
21	2187.8

TABLE V

CPA Summary Tableau for ECTRACE Trial 67 (computer printed output)

8 RAY TRACES COMPLETED

H HEADING AT CLOSEST APPROACH TO RECEIVER
 T TIME AT CLOSEST APPROACH TO RECEIVER
 D MINIMUM DISTANCE TO RECEIVER

RAY NUMBER	INITIAL HEADING	INITIAL ELEVATION	NUMBER OF BOUNCES	H	T	D
1	10.000	-30.000	21	164.266	166.534	7.888
2	10.000	-21.429	21	158.372	165.018	1.339
3	10.000	-12.857	21	146.487	163.575	6.884
4	10.000	-4.286	21	145.103	160.945	7.175
5	10.000	4.286	12	144.811	160.593	7.803
6	10.000	12.857	21	149.200	163.395	6.676
7	10.000	21.429	21	157.810	163.22	1.139
8	10.000	30.000	21	164.103	166.244	8.575

TABLE VI

RAY FAN SYMBOLS - used to denote location of bottom reflections in the ECTRACE plots. Thirteen different symbols are used before repetition. All rays of the same ray fan (initial elevation angle) will indicate a bottom reflection with the same symbol. Each ECTRACE plot lists the symbols used for the horizontal and vertical plots.

INITIAL ELEVATION ANGLES		
RAYFAN	SYMBOL	THETA
1	☐	-10.000
2	⊙	-9.000
3	△	-8.000
4	+	-7.000
5	×	-6.000
6	◇	-5.000
7	⋈	-4.000
8	⊗	-3.000
9	Z	-2.000
10	Y	-1.000
11	⋈	0.000
12	*	1.000
13	⊗	2.000
14	☐	3.000
15	⊙	4.000
16	△	5.000
17	+	6.000
18	×	7.000
19	◇	8.000
20	⋈	9.000
21	⊗	10.000

HEADINGS 90.000 +/- 0.000

TABLE VII

ECCOM printed output. The rays which are plotted are listed, and their initial heading, initial elevation, and the number of points (initial plus reflections) are indicated. In this run the plot produced is shown in Fig. 7.

ECCOM 51 *** SYNTHETIC BASIN ***
 SYNTHETIC SEA BED
 COMPUTER GENERATED

XST	XDV	YST	YDV	CNX	CNY	BASIN CNLAT	CNLOX
0.0	10.000	0.0	10.000	75.000	75.000	0.0	0.0

INITIAL ELEVATION	INITIAL HEADING	POINTS	SCALE FACTOR= 0.340
40.000	40.000	21	
40.000	44.000	21	
40.000	48.000	21	
38.000	42.000	21	
38.000	46.000	21	
36.000	40.000	21	
36.000	44.000	21	
36.000	48.000	21	
34.000	42.000	21	
34.000	46.000	21	
60.000	40.000	21	
60.000	44.000	21	
60.000	48.000	21	
51.333	42.000	21	
51.333	46.000	21	
42.667	40.000	21	
42.667	44.000	21	
42.667	48.000	21	
34.000	42.000	21	
34.000	46.000	21	
60.000	5.000	21	
60.000	9.000	21	
60.000	13.000	21	
62.000	7.000	21	
62.000	11.000	21	
64.000	5.000	21	
64.000	9.000	21	
64.000	13.000	21	
66.000	7.000	21	
66.000	11.000	21	

APPENDIX H
FIGURES

- FIGURE 1. Program and Data Utilization Flowchart
- FIGURE 2. Contour Plot of Lofoten Basin (GENBOT)
- FIGURE 3. Horizontal Ray Plot Over Mohns Ridge (ECTRACE)
- FIGURE 4. Contour Plot of Mohns Ridge (GRDCHK)
- FIGURE 5. Complete ECTRACE Plot for a Synthetic Basin
- FIGURE 6. Contour Plot of a Synthetic Basin (GRDCHK)
- FIGURE 7. ECCOM Plot for a Synthetic Basin
- FIGURE 8. NRL N. Atlantic Contour Chart
- FIGURE 9. Perspective Surface Plot - Seamount (SYNGEN)
- FIGURE 10. Perspective Surface Plot - Basin (SYNGEN)
- FIGURE 11. Perspective Surface Plot - Mohns Ridge (SYNGEN)
- FIGURE 12. Contour Plot of a Synthetic Seamount (GRDCHK)
- FIGURE 13. Complete ECTRACE plot for a Synthetic Seamount.
- FIGURE 14. Horizontal Ray Plot over a Synthetic Seamount (ECTRACE)
- FIGURE 15. Vertical Ray Plot in a Basin (ECTRACE)
- FIGURE 16. Vertical Ray Plot over a Seamount (ECTRACE)
- FIGURE 17. Horizontal Ray Plot in a Basin (ECTRACE)
- FIGURE 18. ECCOM Plot for a Synthetic Wedge

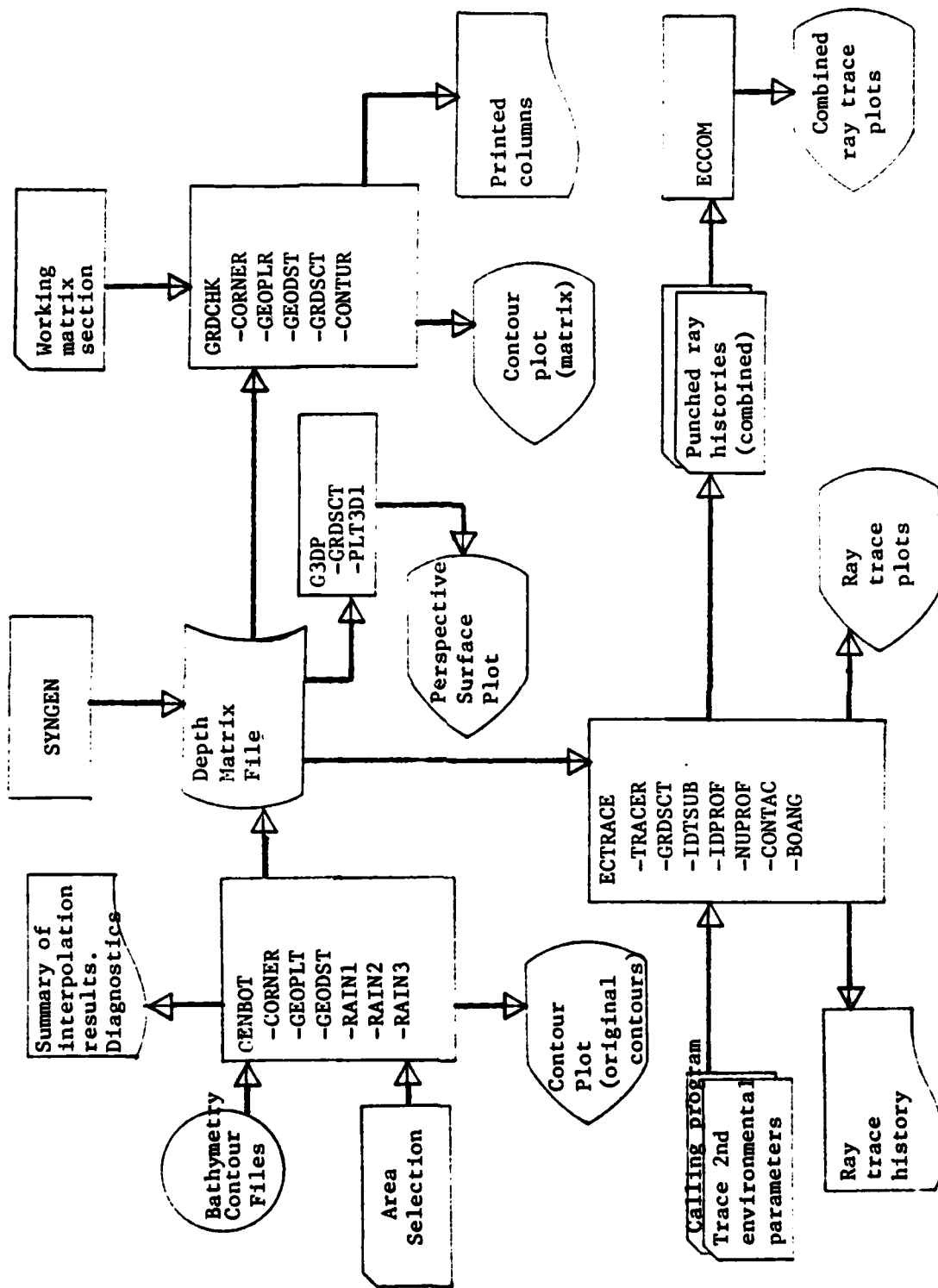


FIGURE 1. Program and Data Utilization Flowchart.

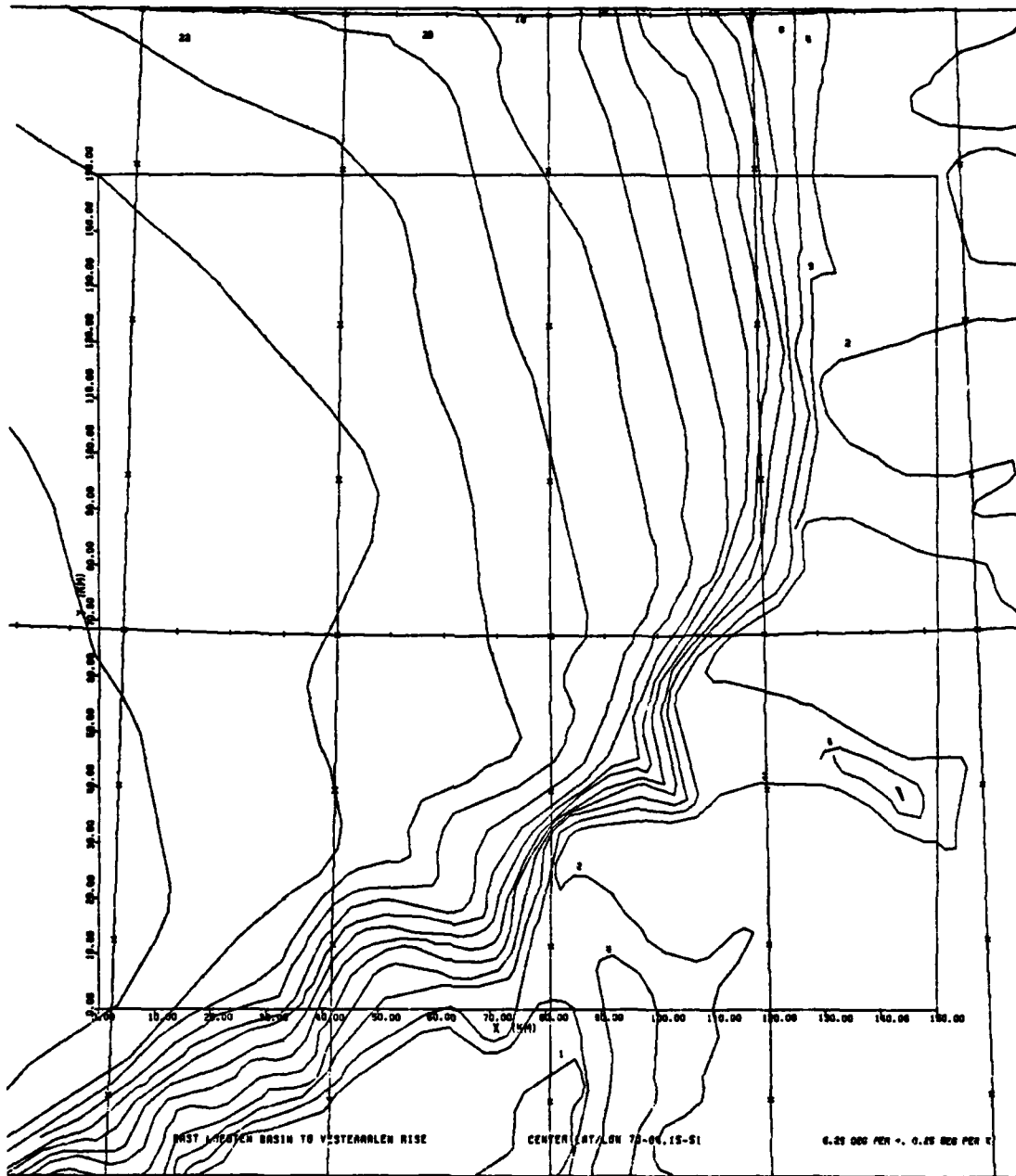


FIGURE 2. A contour plot of the eastern Lofoten Basin produced by GENBOT from magnetic tape data. The rectangular labeled axis denotes the region for which GENBOT generated a matrix representing evenly spaced depth values. A geographic coordinate grid is superimposed.

INITIAL ELEVATION ANGLES
 RAYFAN SYMBOL THETA
 1 □ 25.000
 2 ○ 30.000
 3 ▲ 35.000
 HEADINGS 50.000 +/- 30.000

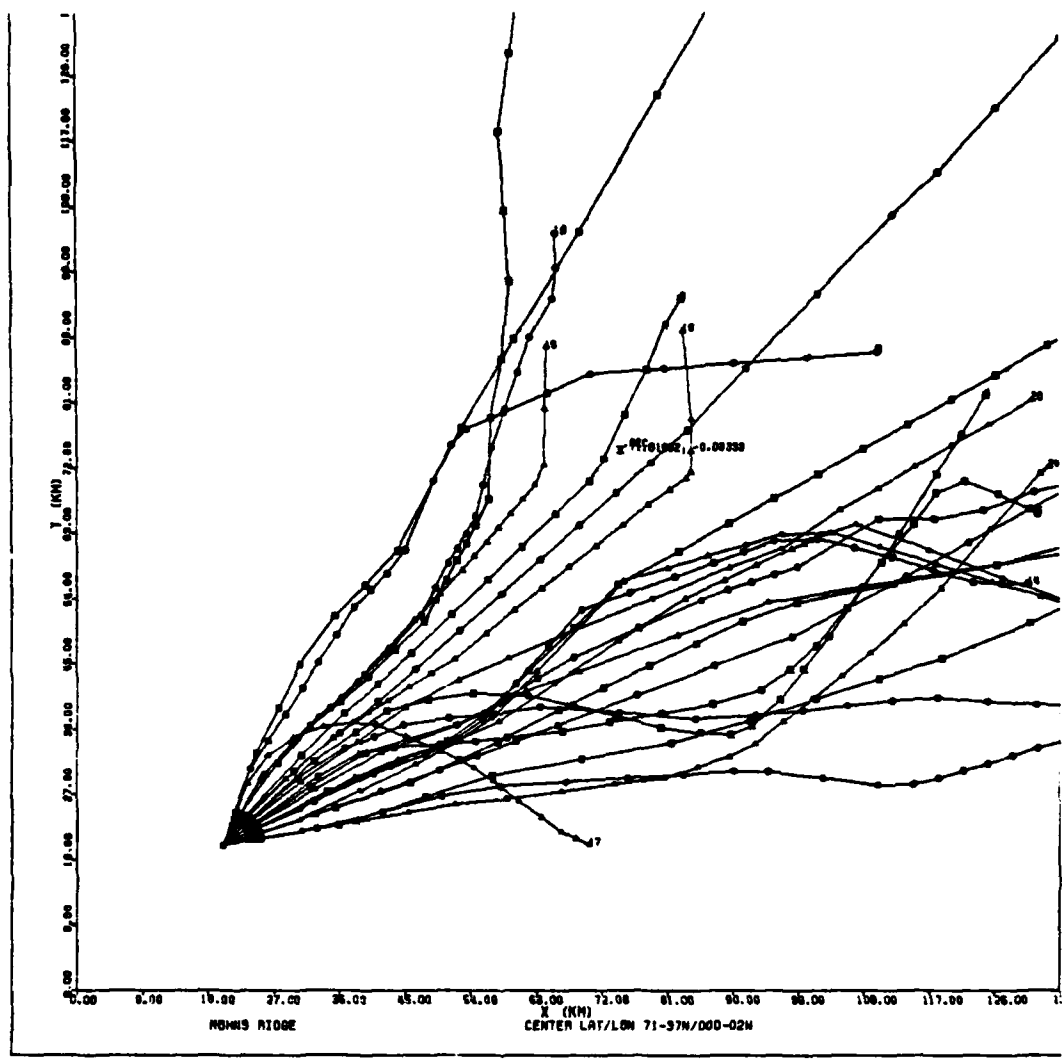


FIGURE 3. ECTRACE TRIAL 82C performed over a depth-grid matrix of the Mohns Ridge. In this run three ray fans are used with eight rays per ray fan. This may be overlaid on a contour plot of this area (Fig. 2).

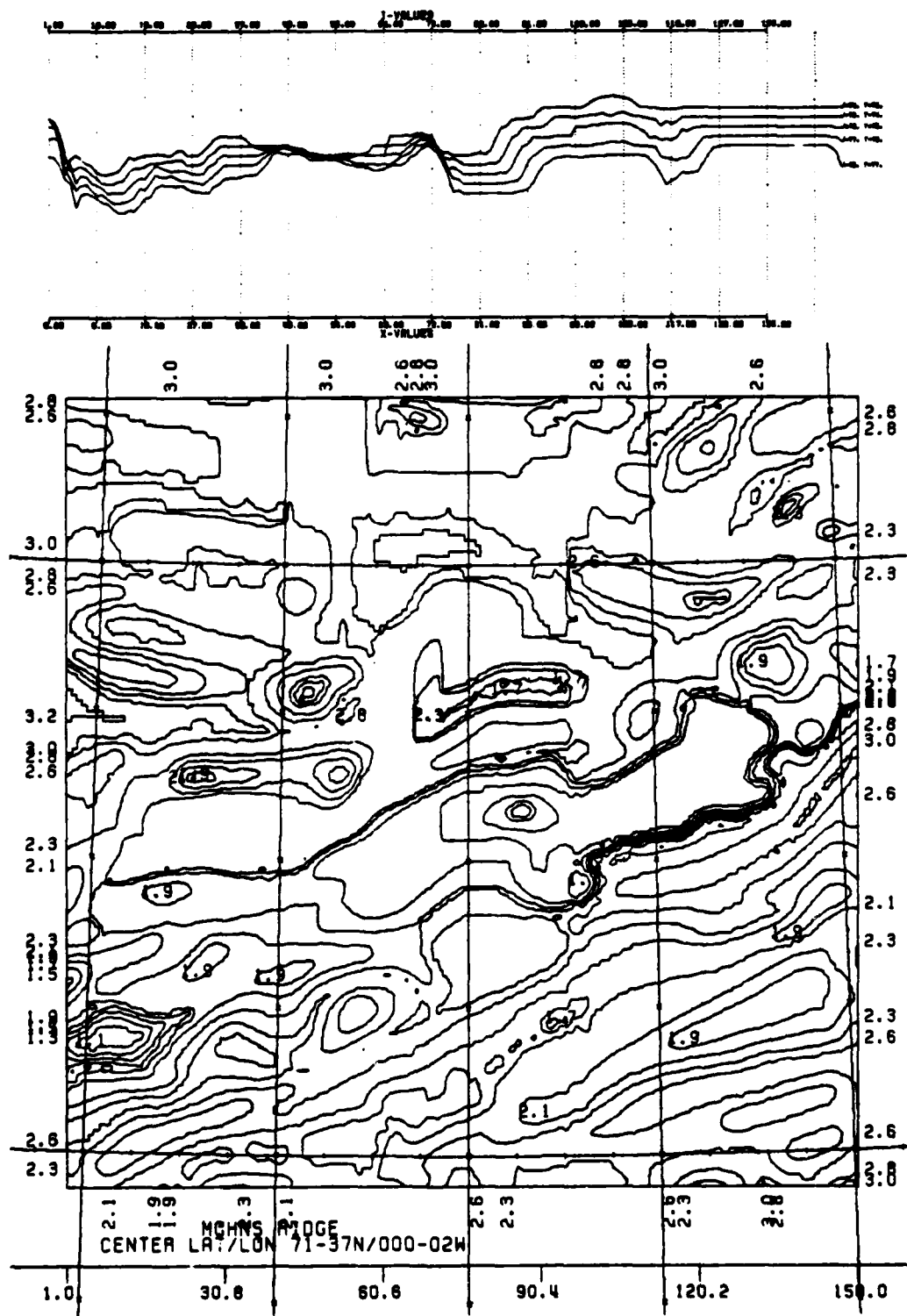


FIGURE 4. A GRDCHK plot made on a matrix generated from contour data. In this example, rows 1 through 150 of columns 74 through 78 were selected for profile analysis and printing.

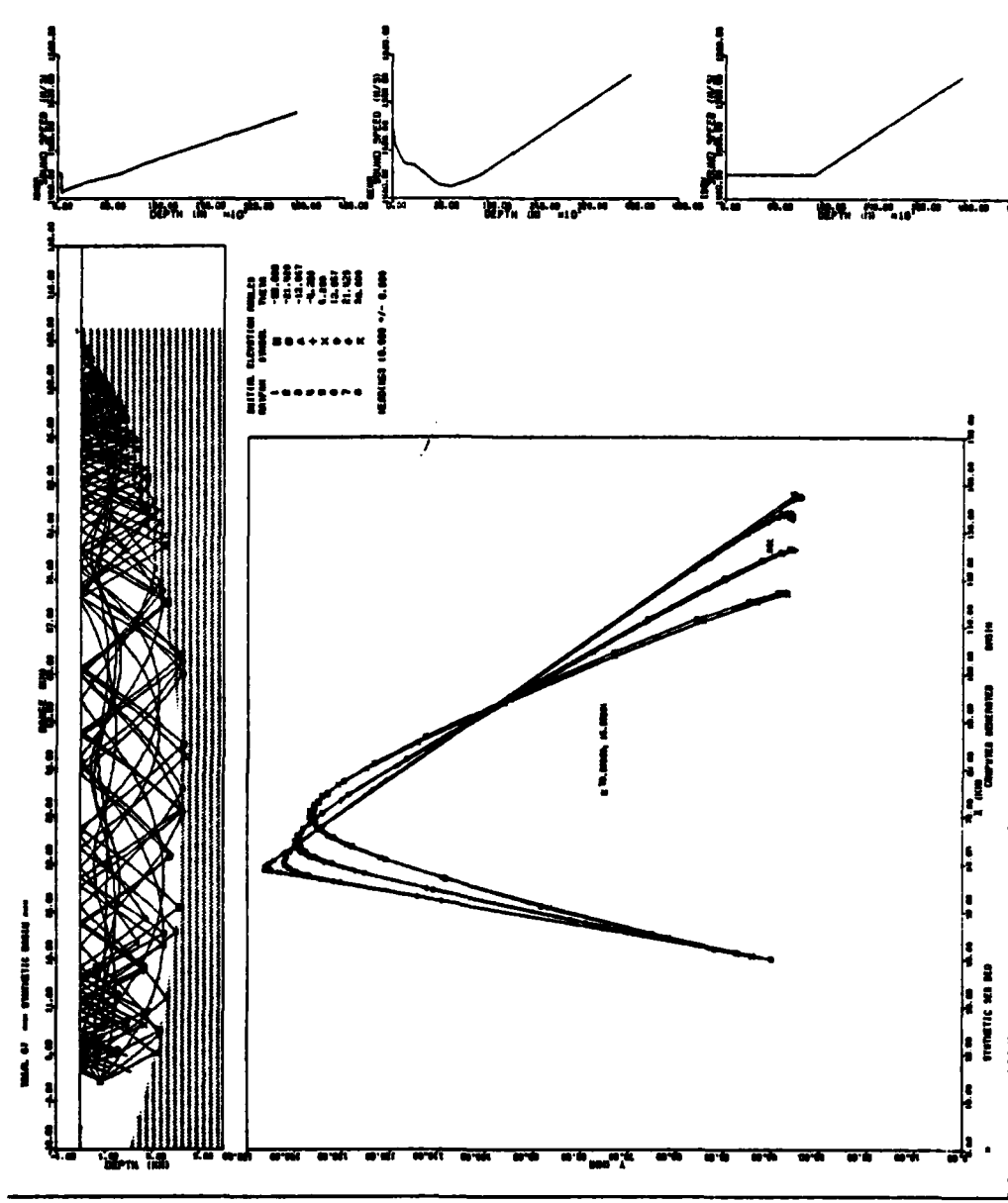


FIGURE 5. ECTRACE TRIAL 67, performed in a synthetic parabolic basin (FIGURE 6). In this run eight ray fans are used with initial elevation angles varying between -30 and +30 degrees. Since there is only one ray in each fan, the initial heading for the rays will be 10 degrees. The vertical plot reveals CZ, sofar ducted, and SRBR rays.

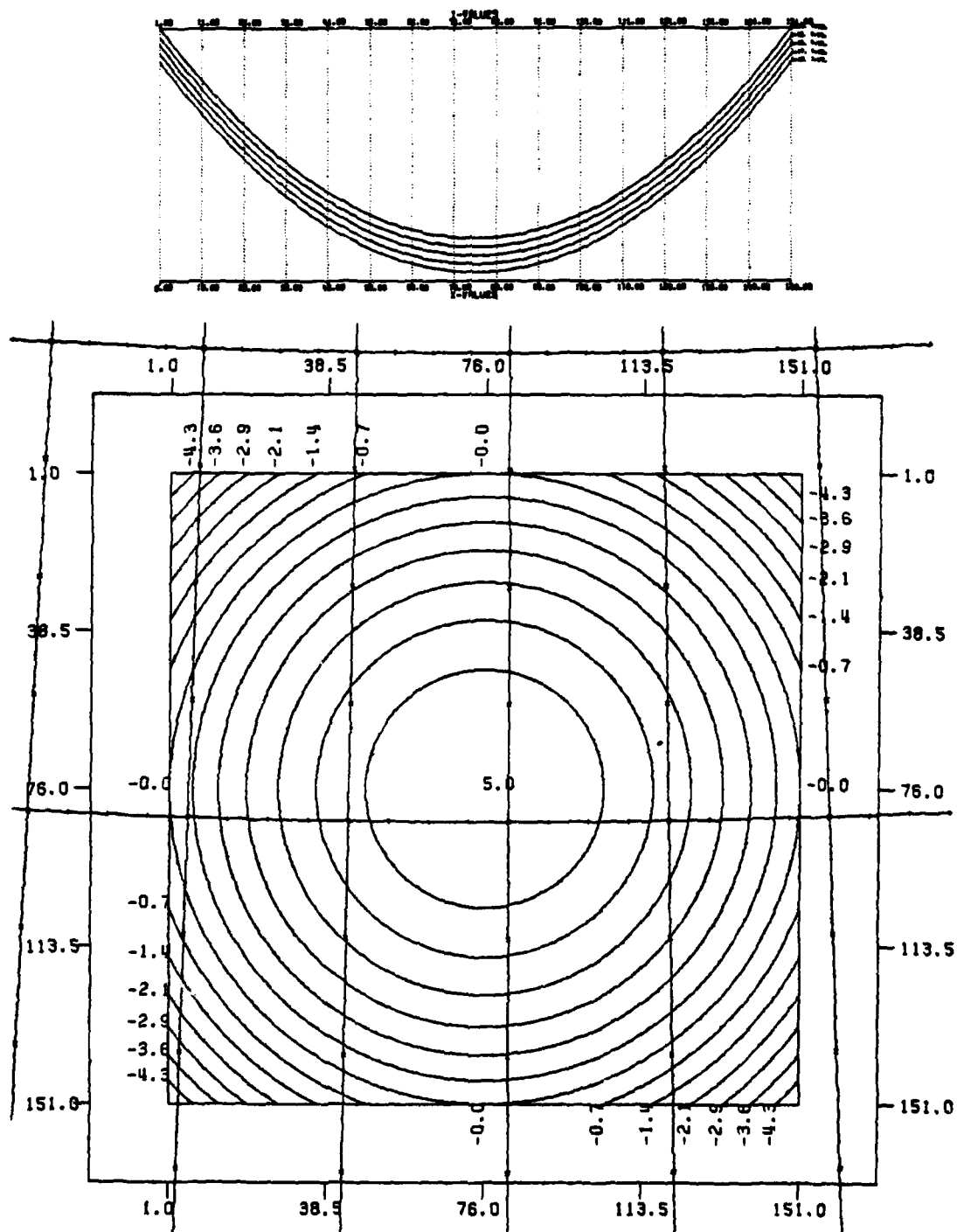


FIGURE 6. A graphical analysis performed by GRDCHK of a synthetic parabolic basin (Fig. 10) created by SYNGEN. The upper plot is a series of displaced depth curves of selected columns of the matrix.

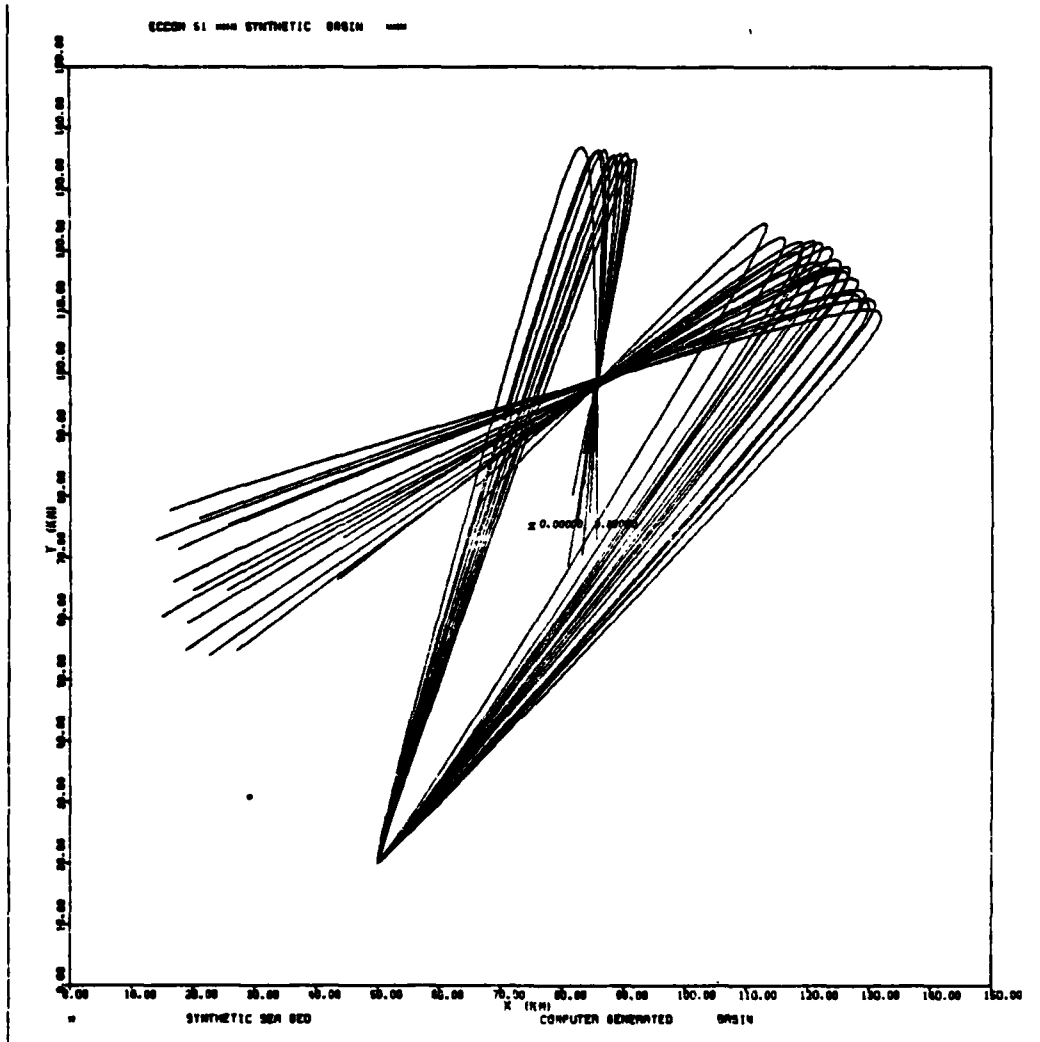


FIGURE 7. Convergence in a parabolic basin (Fig. 10). This is an ECCOM product using punched output from three separate ECTRACE runs. TABLE VII identifies the ray headings, elevation angles, and number of points.

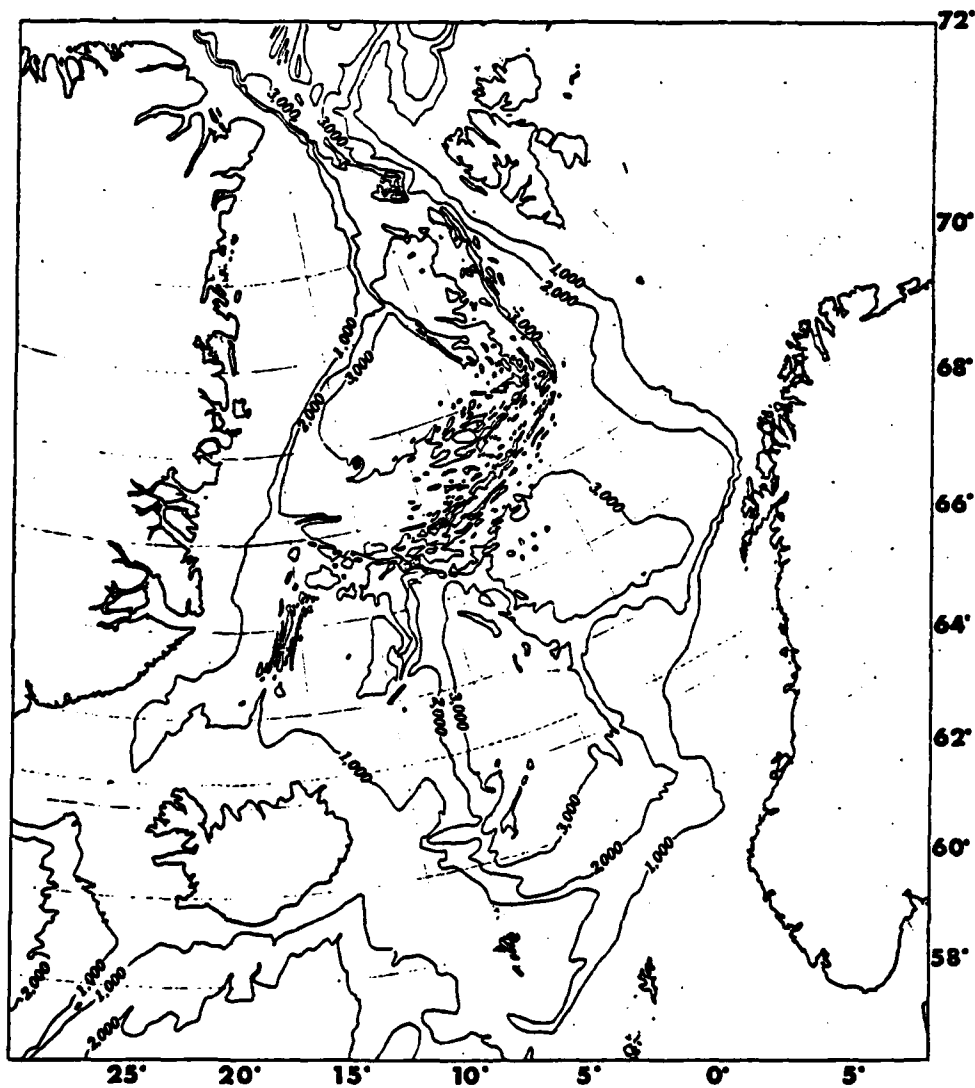
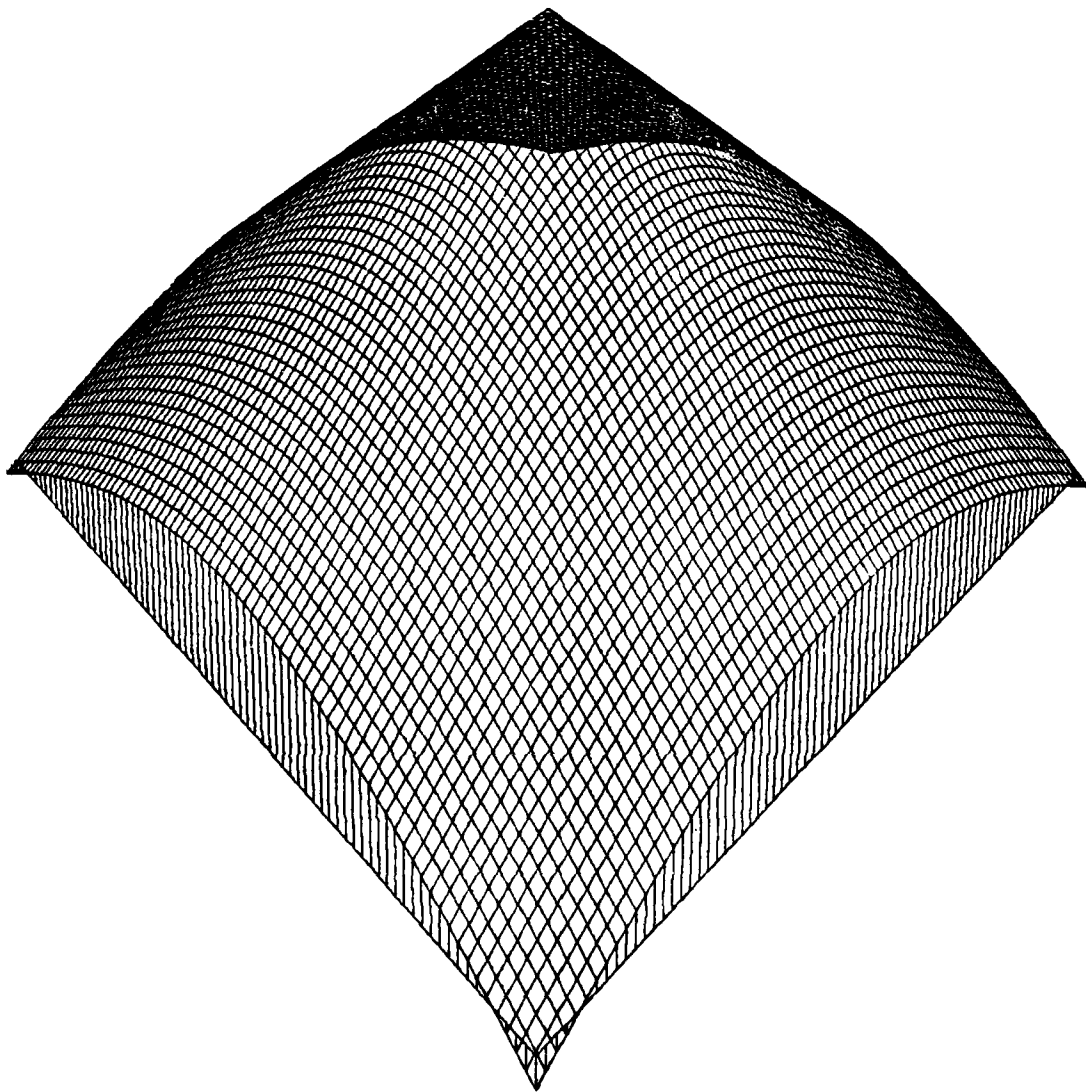


FIGURE 8. A reduced representation of a chart titled "Bathymetry of the Norwegian-Greenland and Western Barents Seas" published by NRL (Washington, D.C.). The actual chart measures 4 by 3 feet depicting finely grained contours. GENBOT uses bathymetry data files of this area to generate the matrix grids used by ECTRACE.

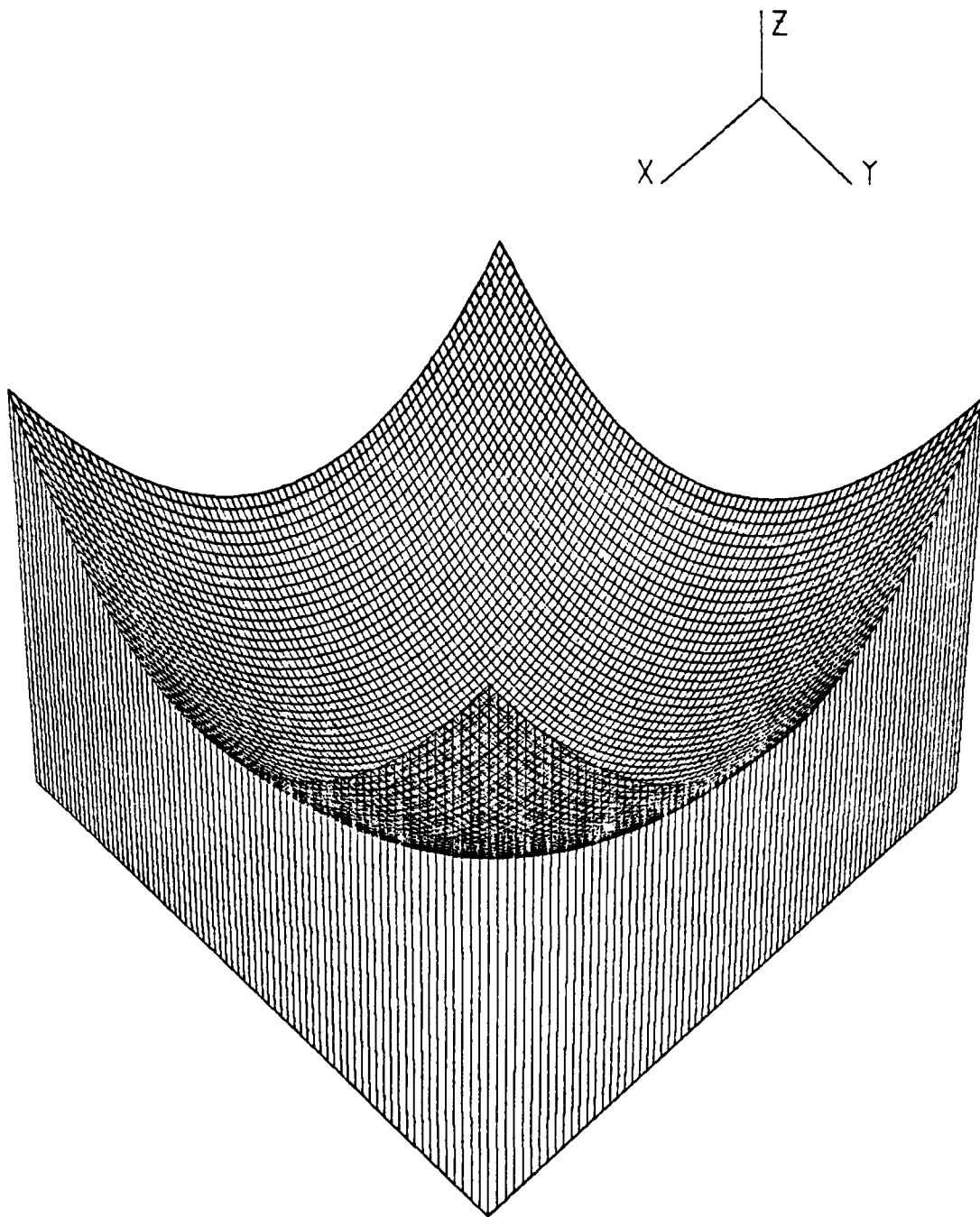


*

SYNTHETIC SEA BED
COMPUTER GENERATED

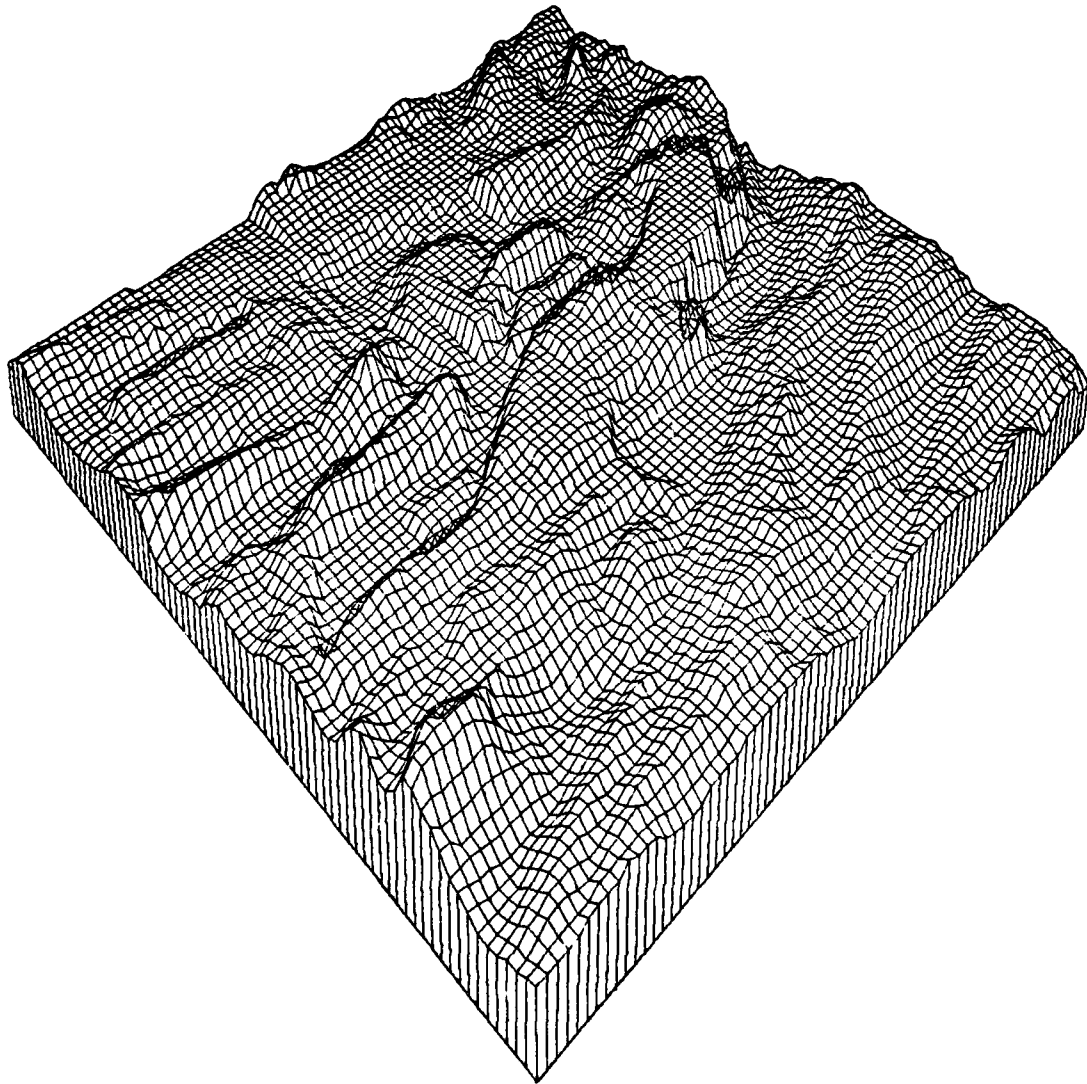
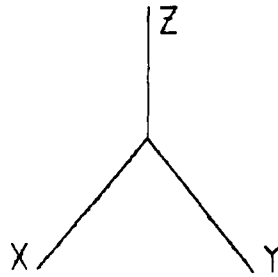
SEAMOUNT

FIGURE 9. A perspective surface plot produced by G3DP of a conical seamount generated by SYNGEN.



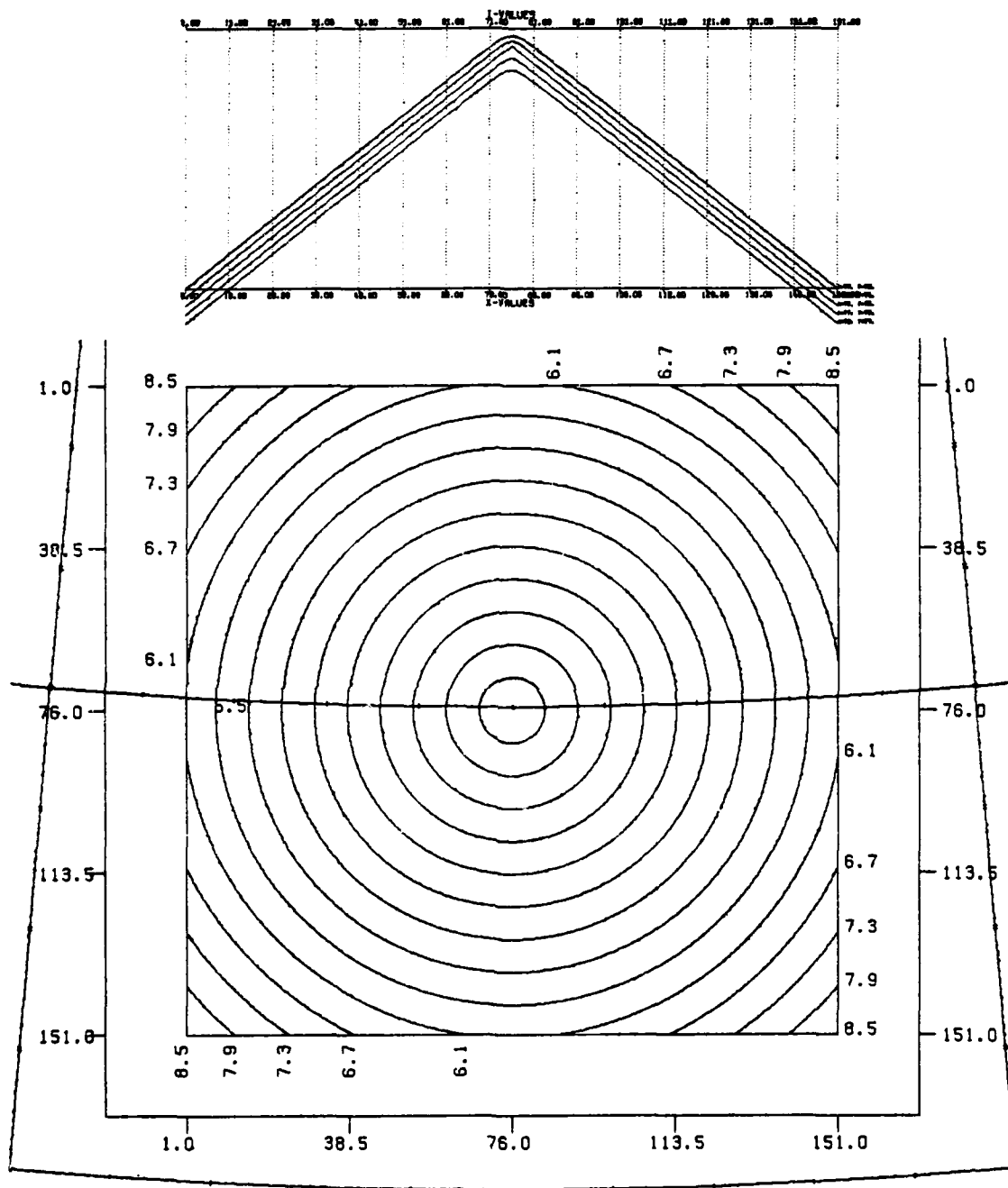
SYNTHETIC SEA BED
COMPUTER GENERATED BASIN

FIGURE 10. A perspective surface plot of a synthetic parabolic basin produced by SYNGEN.



MØHNS RIDGE
CENTER LAT/LØN 71-37N/000-02W

FIGURE 11. A perspective surface plot produced by G3DP of a depth matrix representing a portion of the Mohns Ridge, see Fig. 2.



SYNTHETIC SEA BED SEAMOUNT
COMPUTER GENERATED

FIGURE 12. A graphical analysis performed by GRDCHK of a depth matrix representing a conical seamount. The upper portion is a series of displaced plots of selected columns of the matrix. The lower portion is a contour plot. The seamount was created by SYNGEN, see Fig. 9.

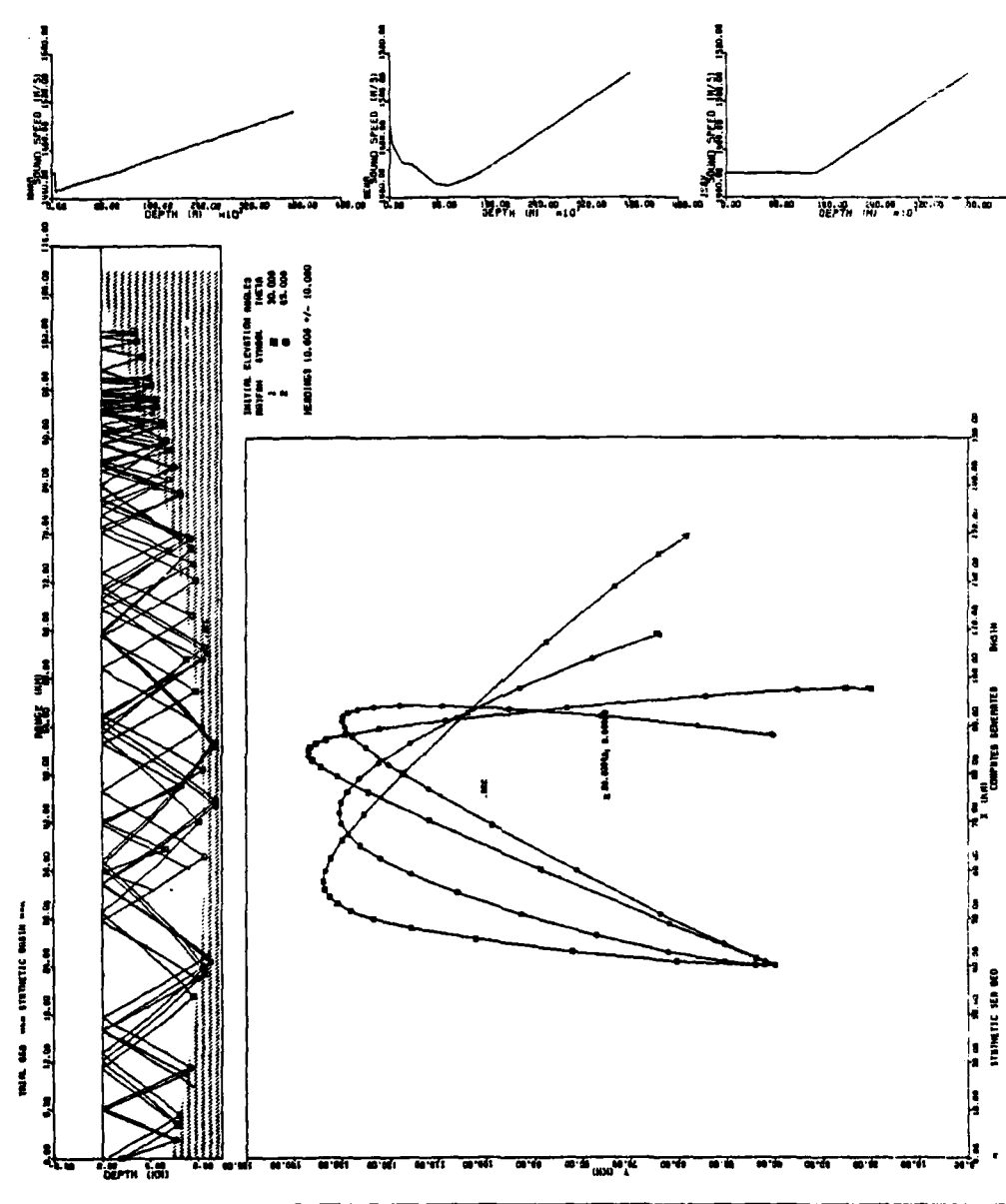


FIGURE 13. An ECTRACE plot of two ray fans in a synthetic parabolic basin (FIGURE 10) generated by SYNGEN. The ray fans have initial elevation angle of 30 and 45 degrees (positive angle downward). Each ray fan contains two rays with initial headings 360 and 020 degrees, respectively. The plot was terminated after each ray had accumulated 23 bottom bounces.

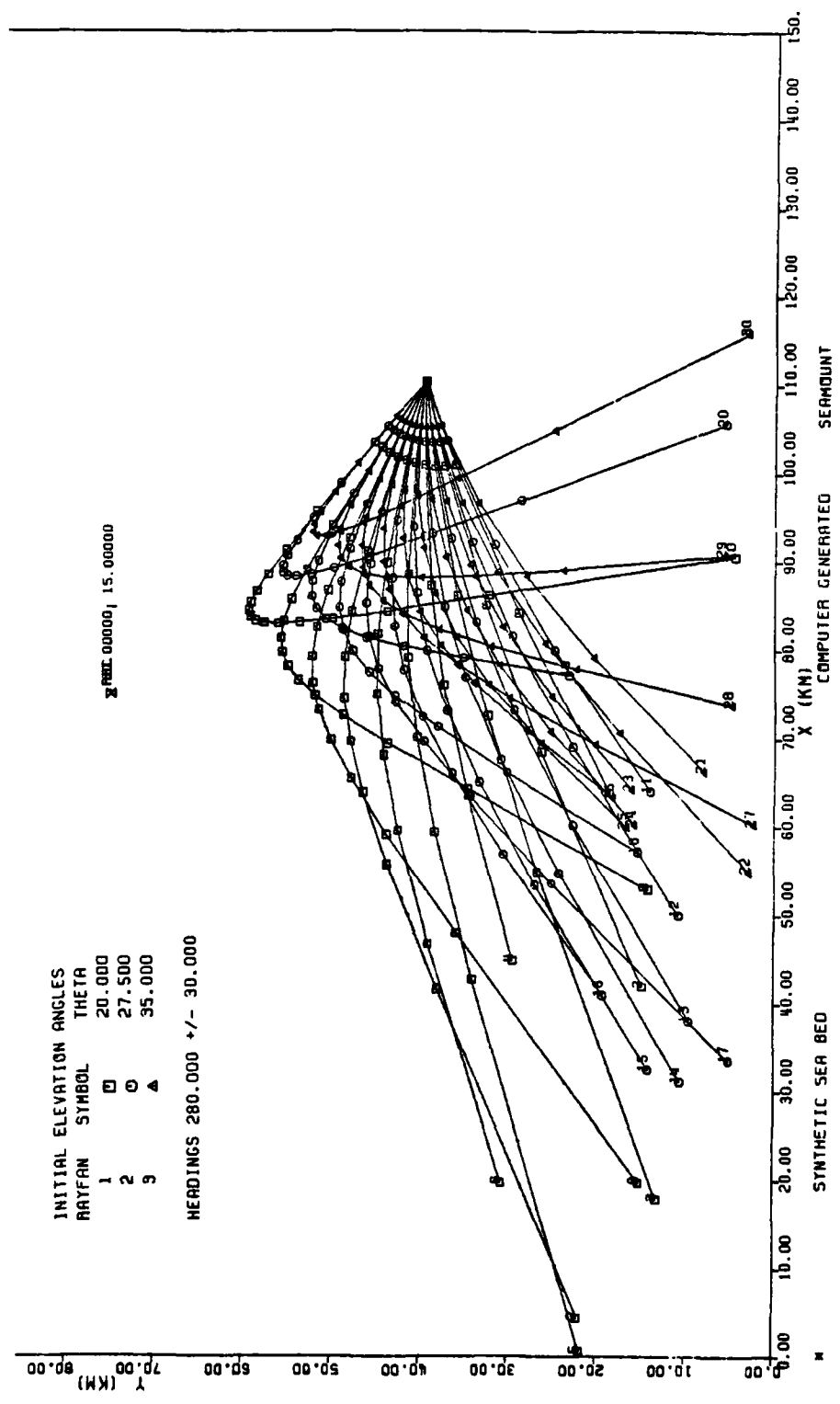


FIGURE 14. An ECTRACE horizontal product of three ray fans contacting a synthetic seamount, see Figs. 9 and 12.

TRIAL 54 *** SYNTHETIC BASIN ***

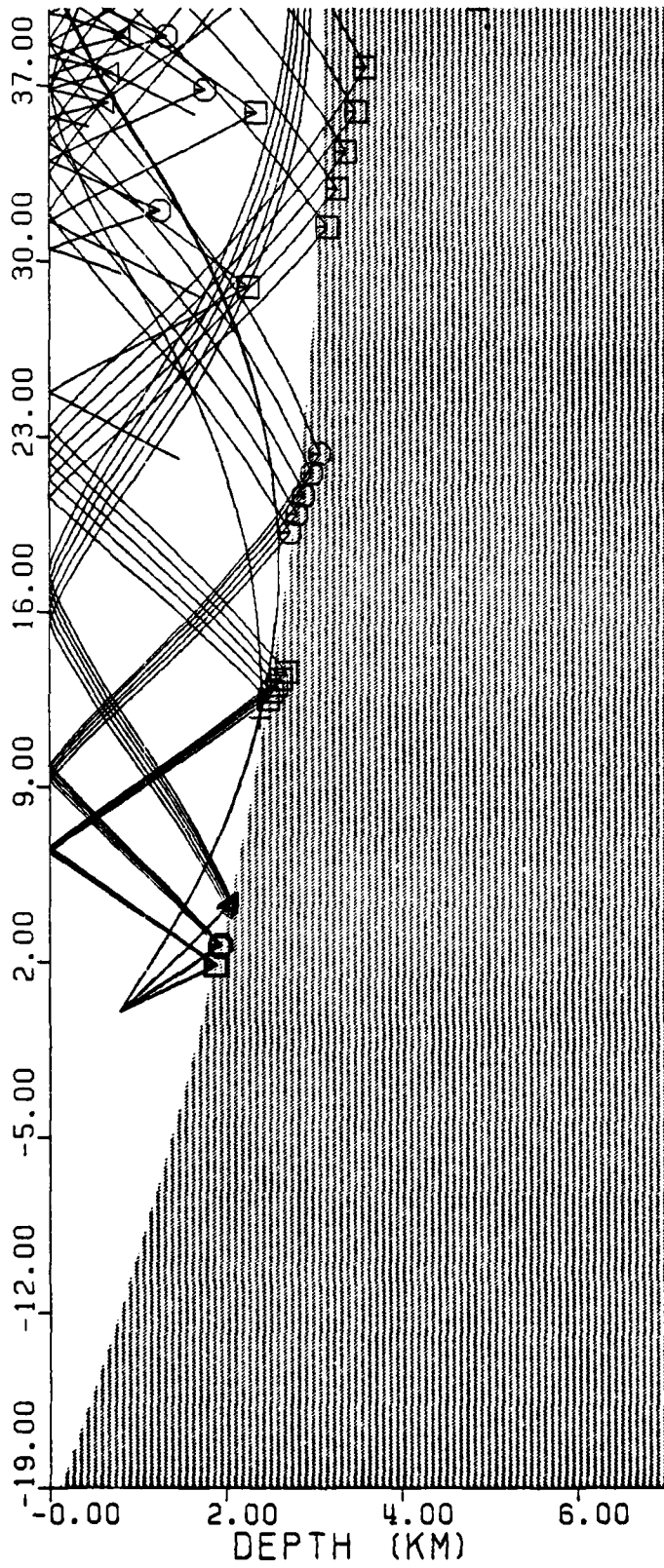
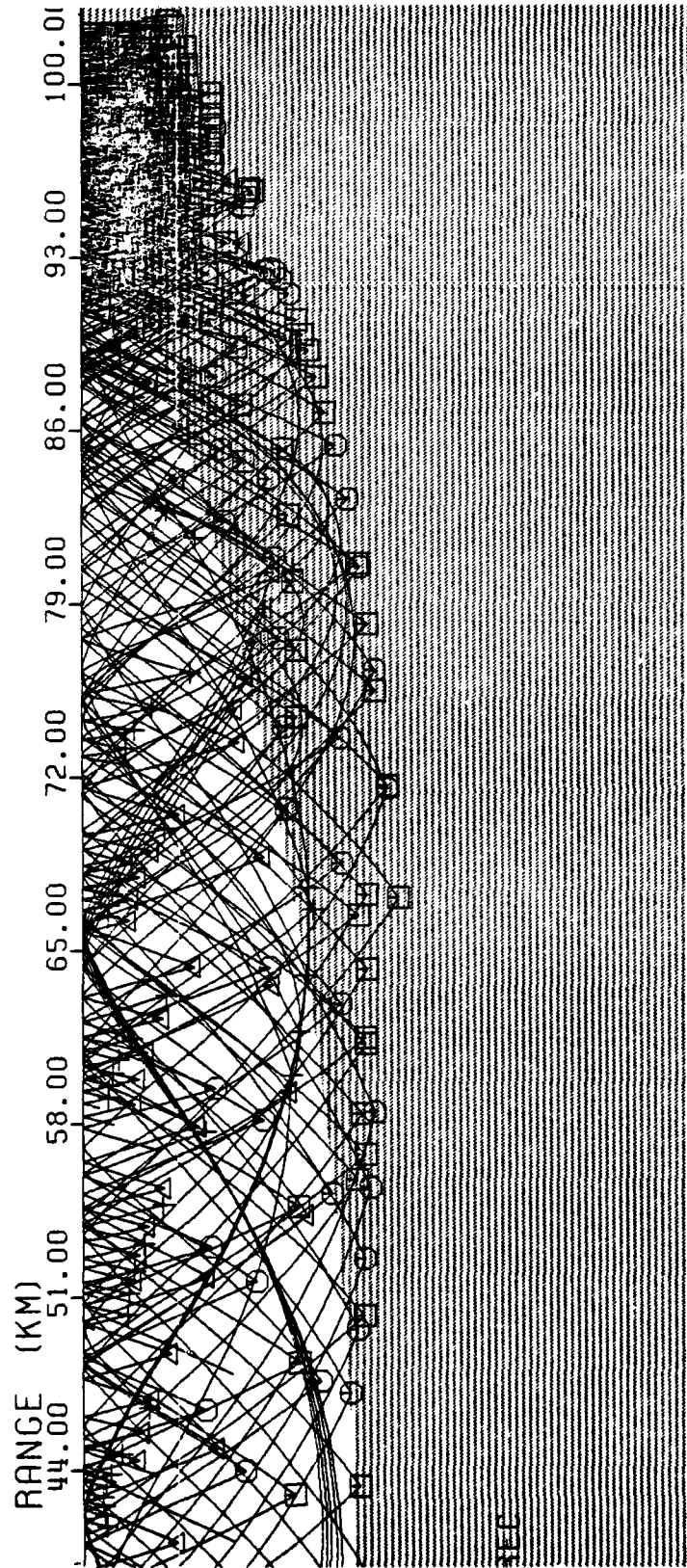


FIGURE 15. ECTRACE TRIAL 54. There are 3 ray fans of 5 rays per fan. The ray fan depicted with the square symbol, can be seen first to curve clockwise away from the bathymetry slice, and then reverse and curve counterclockwise. Eventually, the rays can be seen to appear to approach the source. Since the bottom profile is taken only along the mean heading of the ray fan, most bounce symbols will not lie on the profile surface. (FIGURE 15 continued)



continued FIGURE 15.

TRIAL 31 *** SYNTHETIC SEAMOUNT ***

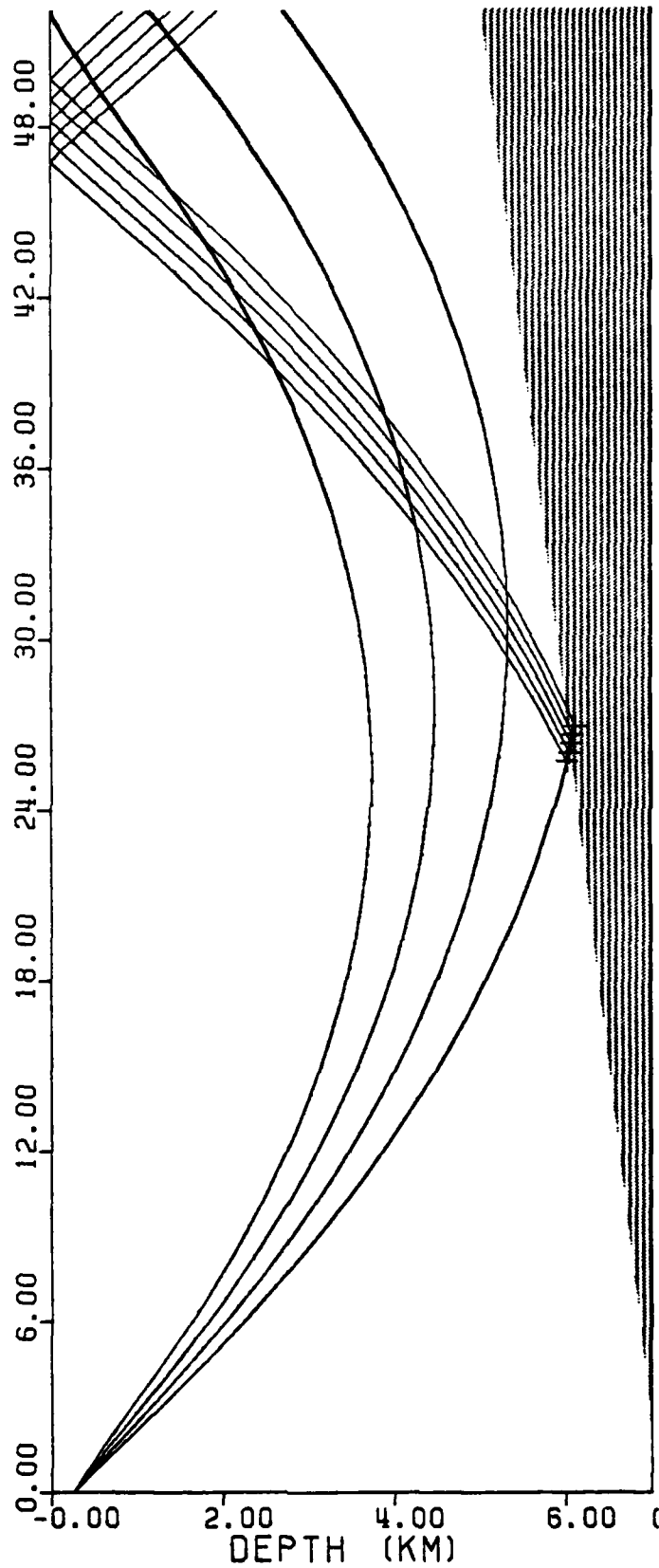
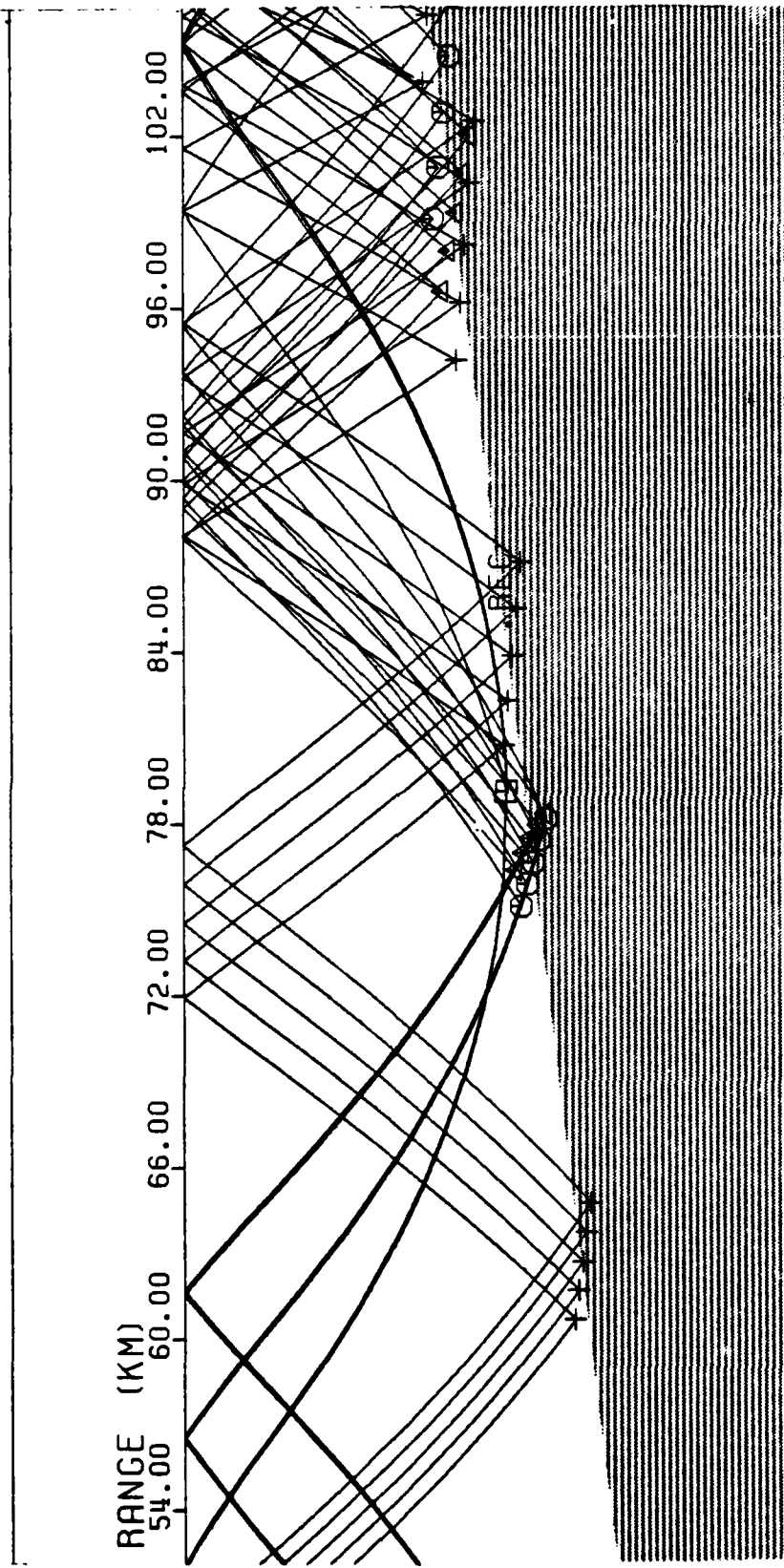
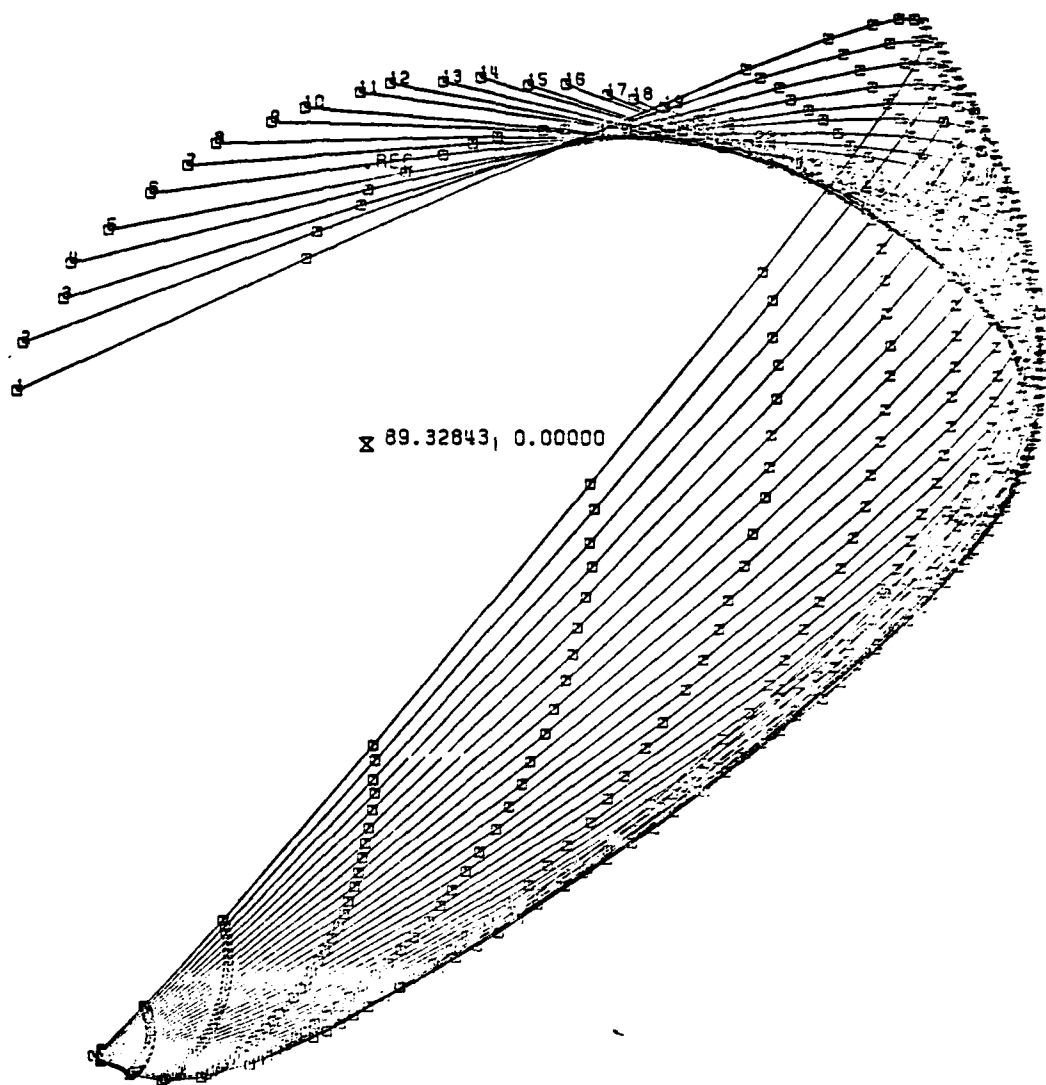


FIGURE 16. The vertical plot of an ECTRACE run over a synthetic grid representing a seamount. The axis of the ray fan was aimed at the center of the seamount. Rays in a single narrow ray fan are nearly indistinguishable until the first bottom contact is made. (FIGURE 16 continued)



continued FIGURE 16



40.00 50.00 60.00 70.00 80.00 90.00 100.00 110.00 120.00 130.00

FIGURE 17. An ECTRACE horizontal plot product of a single wide ray fan in a synthetic basin. All rays share the same bottom contact symbol. The number at the last symbol identifies the ray's order in the printed and punched history.

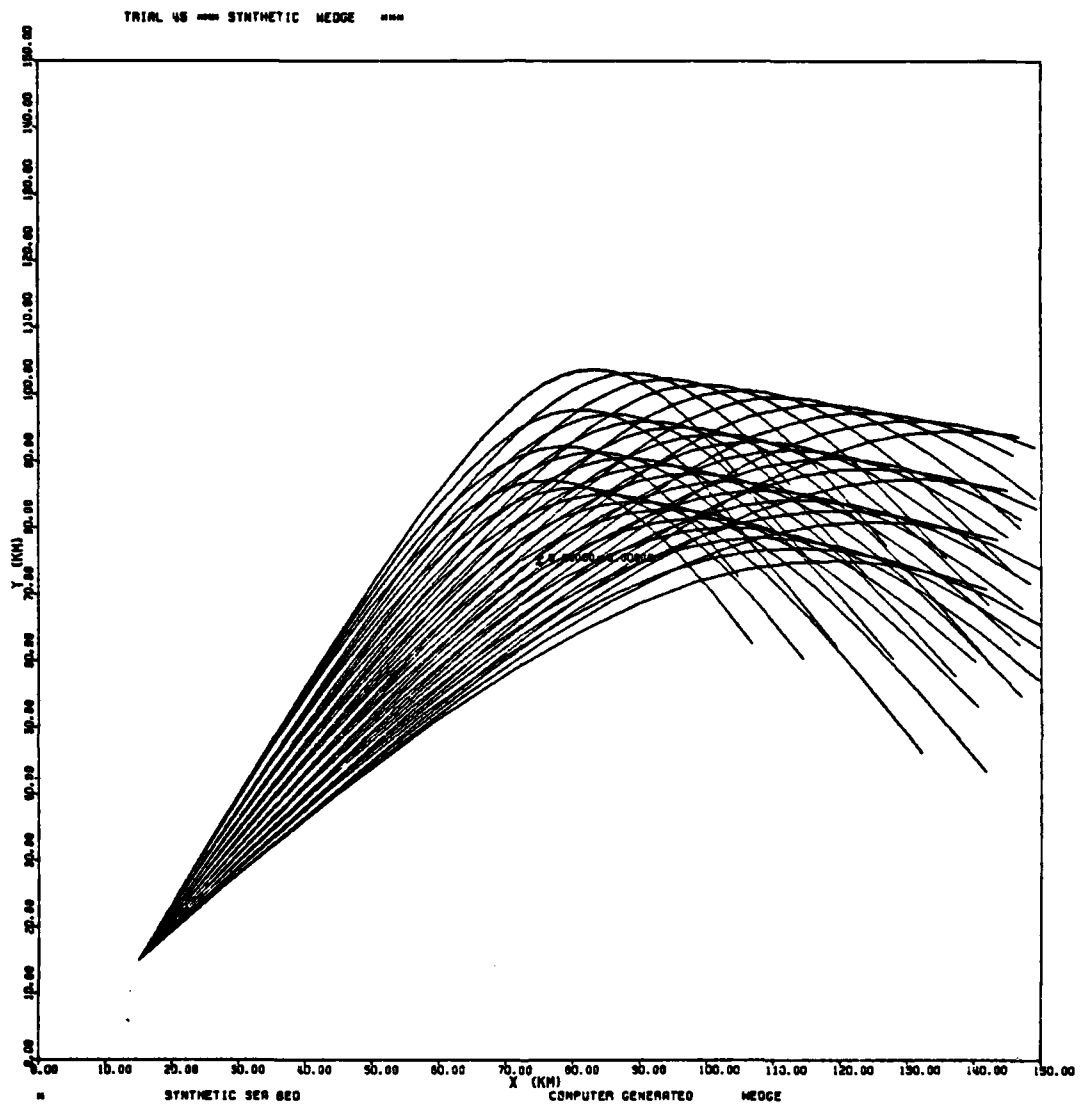


FIGURE 18. A horizontal plot produced by ECCOM of four ray fans propagating over a six degree wedge. The punched output of three ECTRACE runs was combined and then every other ray data history card sequence was removed. There are a total of 40 rays depicted varying in initial elevation angles from 20 to 26 degrees in two degree increments. The initial headings vary from 31 to 49 in two degree increments. The main purpose of ECCOM is to display the horizontal curvature effect of a large number of rays.


```

500C FCFMAT(6AE/6A8/4F10.5)
      READ 5CJC,NFILES,LEN
501C FCFMAT(11615)
      LGRI=LEN*GT.0
      LFLCT=LEN*LEN*4
      IF(.NOT.LGRI) GC TC 1 CNLCN,NFILES
      PRINT(10X) GRID FILE, CALLEC, 2(T40,6A8/), 10X, 'WILL BE CONSTRUCTE
6000 1C ARFCUNC LAT=, F10.5, LEN=, F10.5/10X, USING , 15, FILES.//)
      ARAC=ANINT(ARAD*ARAC)
      IF(ARAC.LT.7.5) GO TC 5CC
      1 JMAX=IMAX
      XMAX=(IMAX-1)*DHN
      YMIN=C
      YRG=YMAY
      APCV=APAC
      CNY=ARAC
      CALL FLCT GECGRAPHIC ELCUNCARY LINES.
      LLT=1.25
      ABL=CMAX1(CABS(GLATMX),CABS(GLATMN))
      DLN=20.
      IF(AEL.LT.85.) DLN=DLN/2
      IF(AEL.LT.75.) GC TC 310
      CLN=1
      CLAD=CLT
      SLCN=GLCNMAY-DLN
      ELAT=GLATMX+DLN
      IF(SLCN.GT.CALCN-90.) SLCN=SLON+DLN
      SLAT=CMAX1(SLAT,DBLE(-85.))
      IF(.NOT.LFLCT) GC TC 5
      AFAZ=LEN*21.
      ASIZE=AFAC*21.
      CALL WINDC(C.,ASIZE,C.,ASIZE)

```



```

CALL FUCT(C,0,99,72,3)
CALL FUCT(C,0,99,20,3,2)
CALL FUCT(C,0,99,20,3,3)
CALL FUCT(C,0,99,23)
CALL SYMBCL(1,2,4,12,TTL,0,96)
C
LJ=DLNLT(SLAT)
GJ1=CLNLT(SLCN)
IF(CLN,AE,1) GJ1=1C*DIAT(GJ1/10.)
IF(G,1,EE,GJ2) GC TC EC
340 CALL GJ1+CLT
IF(G,1,EE,ELAT) GC TC 340
C
CJ=DLNLT(SLAT)
GJ1=CLNLT(SLCN)
GJ2=ELNLT(SLCN)
CALL GJ1+CLN
IF(G,1,EE,ELN) GC TC 350
CALL SYMBCL(99,99,1,1,SNGL(DLTD),0,2)
CALL SYMBCL(99,99,1,1,DEG PER X,0,12)
CALL SYMBCL(99,99,1,1,SNGL(DLND),0,2)
CALL SYMBCL(99,99,1,1,DEG PER X,0,10)
C
IF(ILE=IFILE+1)
ICCN=0
KPTF=0
NPTF=0
READ(LC,ACR+1)
LATE=LCACR+1)
PRINT(1,1)
FORM(1,1)
2,1)
C THE NEXT RECORD IS EITHER A LINE LABEL OR THE FEEDER RECORD
C IF A NEW RECORD LINE
C IF(1,140) ENO=100) (NAME(1),I=1,3),CLAT,CLON,INDEP,METER
1400 FORMAT(A2,A4,A4,7X,2F10.5,2X,14,1X,A2)
IF(NAME(2).EQ.NAME(1)) GO TO 85

```

```

C          PROCESS A NEW CONTOUR LINE.
IPLTST=0
KPTS=C
NPTS=C
LEND=.FALSE.
ICCN=ICCN+1
CDC=INDEX(LAT/LCN,ALONG CONTOUR LINE.  EACH RECCD
      HAS FCLR LAY/LCN PAIRS.
      REAC(I),I=1,4) (GLAT(I),GLCN(I),I=1,4)
      FORMAT(1F10.5)
150C      KE=4
      DO 50 K=1,KE
      DC=GLAT(K).GT.90..CR.GLAT(K).LT.-90.
      LEF(LINE) GC TC 6C
      CCNCRE LINE DATA FCLLWS.  BUT FIRST:
C          GO TO 6C
C          ENCCF CONTOUR LINE.  SET KE TO NUMBER OF POINTS IN RECORD.
6C      KE=K-1
      IF (KE.LT.1) GO TO 6C
      IF (CHECK .LE. LEVANCE CF FCINTS.
C          DC TC 6C
      IF (GLAT(K).LT. SLAT.CR.GLAT(K).GT.ELAT) GC TC 70
      IF (GLCN(K).LT. SLCN.CR.GLCN(K).GT.ELON) GC TC 70
      IF (INCFIN POSITION CN GRID.
      CALL GECST(CNLAT,CNLGN,GLAT(K),GLON(K),HS,FF,DIST,-1)
      KPTS=KPTS+1
      KPTT=KPTT+1
      IF (KPTT.LT.4558) GC TC 6C
655E      PRINT(1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36,37,38,39,40,41,42,43,44,45,46,47,48,49,50,51,52,53,54,55,56,57,58,59,60,61,62,63,64,65,66,67,68,69,70,71,72,73,74,75,76,77,78,79,80,81,82,83,84,85,86,87,88,89,90,91,92,93,94,95,96,97,98,99,100)
      FORMAT(100X,110,111,112,113,114,115,116,117,118,119,120,121,122,123,124,125,126,127,128,129,130,131,132,133,134,135,136,137,138,139,140,141,142,143,144,145,146,147,148,149,150)
      LSTP=.TRUE.
      LEND=.TRUE.
      IF (IPLTST.EC.0) IPLTST=KPTT
      AY(IPLTEN)=DIST*DCOS(PS)+CNY
      AX(IPLTEN)=DIST*DSIN(PS)+CNX
      ACCNTINLE
      ACCNTINLE
      NPTS=NPTS+KE
      YF(ACI.LEND) GO TC 45
      PRINT(100X,110,111,112,113,114,115,116,117,118,119,120,121,122,123,124,125,126,127,128,129,130,131,132,133,134,135,136,137,138,139,140,141,142,143,144,145,146,147,148,149,150)
      NPTS=NPTS+1
      IF (KPTS.LE.71) GC TC 40
      KPTF=KPTF+KPTS
      IF (.NOT.LFLCT.CR.KPTS.LE.1).AND..NOT.LLSTP) GO TC 40

```

```

C      PLCT CCNTCUR LINE.
      KPFF1=KPTT1+1
      KPFF2=KPTT1+2
      AX(KPFF1)=XMIN
      AY(KPFF1)=YMIN
      AX(KPFF2)=XFCV
      AY(KPFF2)=YFCV
      CALL LINE(AX(IPLTST),AY(IPLTST),KPTS,1,0,0)
      IF(.NOT. LSTP) GO TO 40
      IF(.NOT. CP CCNTCUR FILE.
C      100 PRINT 1700,KPTF,NP TF,KPTT,ICCN
C      1700 FORMAT(10X,'NUMBER OF BOTTOM PCINTS USEC=',17,' (CUT OF ',15,')',A
C      25) ICCUM TCTAL =',17/10X,'NO. OF CONTOUR LINES PROCESSED FROM FILE=',1
      IF(1(IFILE.LT.NFILES).AND..NOT.LSTP) GC TC 9
      IJ=0
      IJRT=0
      CALL RAIN1(KPTT,AX,AY,AT,KEYX,KEYY,IER)
      XI=AX(KPTT(1))+30.
      YI=AY(KPTT(1))+30.
      X2=AX(KPTT(1))-30.
      Y2=AY(KPTT(1))-30.
      I=1
      J=1
      IF(XMIN.GE.X1.AND.XMAX.LE.X2) GO TO 401
      IHAF=IMAX/2
      I=2, IHAF
      XMIN=XMIN+CFN
      XMAX=XMAX-CFN
      IF(XMIN.LE.XMAX) GC TC 401
      IF(XMIN.GE.X1.AND.XMAX.LE.X2) GO TO 401
C      400
C      401 CCNTINLE=IMAX-2*(I-1)
      IMAX=CFN+FLCAT(IMAX-1)/2
      IF(YMIN.GE.Y1.AND.YMAX.LE.Y2) GO TO 411
      JHAF=JMAX/2
      J=2, JHAF
      YMIN=YMIN+CFN
      YMAX=YMAX-CFN
      IF(YMIN.LE.YMAX) GC TC 411
      IF(YMIN.GE.Y1.AND.YMAX.LE.Y2) GO TO 411
C      410
C      411 CCNTINLE=JMAX-2*(J-1)
      JMAX=CFN+FLCAT(JMAX-1)/2
      CNV=CFN+LFLCAT GO TC 210
      IF(.NOT. GRIC BOUNDARY LINES.
      XST=XMIN/APCV

```

```

YST=YMIN/APDV
XEND=XMAX/APDV
YEND=YMAX/APDV
YVAL=Z*(CNX)/APDV
XVAL=X*(CNY)/APDV
CALL FLCT(XST,YST,X (KM),6,YVAL,90.,YMIN,APDV)
CALL FLCT(XST,YST,X (KM),-6,XVAL,0.,XMIN,APDV)
CALL FLCT(XEND,YEND,Z)
CALL FLCT(XST,YST,Z)
CALL FLCT(XEND,YEND,Z)
CALL FLCT(CZ,CZ,CLATMN,CLATMX,GLONMN,GLONMX,IMAX,JMAX)
CALL CENFR(CZ,CZ,CLATMN,CLATMX,CLONMN,CLONMX,IMAX,JMAX)
210 ARAD=CNX*(7.5) GC TC 215
5CC PRINT 6CC,ARAD
65CC FORMAT(10X,'SEMI-AXIS LENGTH OF ',F6.2,' KM TOO SMALL. '/10X,
      'ANG GRID WILL BE PRODUCED.')
      1 STCP
C 215 IF (.NOT. LGRID) STOP
      WRITE(2,5030)TTL,CALAT,CNLCN,CHN,IMAX,JMAX
5030 NREC=Z
      FORMAT(6A8/6A8/3F10.5,2I5)
      GC 200 J=1,JMAX
      AYJ=CFN*(J-1)+YMIN
      CO 201 J=1,IMAX
      IJ=IJ+1
      AXI=CFN*(I-1)+XMIN
      CALL RAIN2 (KFTT,AX,AY,AZ,KEYX,KFYX,AXI,AYJ,AZK,IER)
      IERT=IER+1
      PRINT 6C30, AXI,AYJ,I,J,AZK,IER
      FORMAT(10X,'X=',F8.4,' Y=',F8.4,' ZB(',I3,',',I3,',')=',F8.4,' IFR=',
      I5)
C 6030 1,IF(IERT,6E,1000) GC TC 205
      202 AZE(IJ)=AZK
      IF(IJ.LT.10) GO TO 201
      WRITE(2,1020) AZB
      NREC=NREC+1
      IJ=0
      201 CONTINUE
      200 CONTINUE
      IF(I,2,1020) (AZB(I),I)=1,IJ)
      WRITE(2,1020) NREC+1
      NREC=NREC+1
      1020 PRINT (10CFE,4)
      205 PRINT (CIC, NREC, IERT

```

```

6010 FORMAT(1/CX,'GRID CONSTRUCTION COMPLETED.',15,' RECORDS IN FILE. '/
110X,15,' FCPTS IN QUESTION. ')
ENCFILE 2
STOP
C      85 IF(.NOT. LE(CT)) GO TC 40
IF(DLGN.LT.SLAT.OR.DLGN.GT.ELAT) GO TC 40
IF(DLGN.LT.SLAT.OR.DLGN.GT.FLON) GO TO 40
CALL GECEST(CNLAT,CNLGN,ELAT,DLON,FS,FF,DIST,-1)
AXS=(DIST*DSIN(HS)+CNX)/APDV
AYS=(DIST*DCOS(HS)+CNY)/APDV
CALL SYMPECL(AXS,AYS,.1,METER,0.,2)
GO TC 40
ENCL
SUBROUTINE CCNRP(GLATM,GLATMX,GLONM,GLONMX,IMAX,JMAX)
IMPLICIT REAL*8(B-F),REAL*8(C-W)
DIMENSION TTL(12)
COMMON /FLCTIT/ TTL,CNX,CNY,CNLAT,CNLGN
COMMON /CFART/ XMIN,YMIN,XMAX,YMAX,XRG,YRG,APDV
DIST=DCALCULATE(LAT/LCN OF GRID CORNERS. CI IS SW AND C2 IS SE.
FS=LATANZ(CNX,CNY)
CALL GECEST(CNLAT,CNLGN,C3Y,C3X,HS,HF,DIST,1)
FS=LATANZ(CNX,-CNY)
CALL GECEST(CNLAT,CNLGN,C2Y,C2X,HS,HF,DIST,1)
C1Y=C2Y
C4Y=C3Y
LGN=CNLGN-X-CNLGN
C4X=CNLGN-LGN
LGN=CNLGN-CNLGN
C1X=CNLGN-LGN
CALCULATE BOUNDARY LATS/LONS THAT FORM SPHERICAL RECTANGLE
IF(CNLAT.EQ.
GLATMX=C1X
GLGNM=C2X
CALL GECEST(CNLAT,CNLGN,GLATM,CNLON,18C.,HFC,CNY,2)
GO TC 6
GLATM=C2Y
GLONM=C4X
GLGNM=C2X
CALL GECEST(CNLAT,CNLGN,GLATMX,CNLON,0.,HF,CNY,1)
FRINT(C3Y,C3X,XMIN,YMIN,C1Y,C1X,XMAX,YMIN,C2Y,C2X,XMAX,YMAX,
1  IMAX,JMAX
1  FORMAT(1/11,'VALUES AT GRID CORNERS: /121,'X,'131,'Y,'14C,
1  'LAT',15,'LCN: /4(17X,4F10.5)/114,'MIN,LON: /3X,'MAX,LON:
2  'LAT',15,'MIN,LAT',3X,'MAX,LAT',3X,'IMAX',3X,'JMAX /11,4F10.5,217/)

```

```

RETURN
SUBROUTINE GEOPLOT(GI,GJ1,GJ2,DJ,X,Y,LLL)
  DIMENSION X(183),Y(183),TTL(12)
  COMMON /FLCTIT/ TTL,CNX,CNY,CNLAT,CNLN
  COMMON /CFART/ XMIN,YMIN,XMAX,YMAX,XRG,YRG,APCV
  INTEC=LLL+2
  IF(LLL.NE.1) GO TO 19
  PLAT=PLCI
  FLCN=GJ1
  CLAT=GI
  CLCN=GJ2
  LLAT=0.
  CLCN=CJ
  GO TO 20
10 PLAT=GI
  FLCN=GJ1
  CLAT=GI
  CLCN=GJ2
  LLAT=CJ
  CLCN=C
  NPTS=C
20 CALL GE CCST(CNLAT,CNLN,PLAT,PLON,HS,HF,DIST,-1)
21 IF(PLAT.GT.CLAT.CR.FLCN.GT.CLCN) GO TO 30
  NPTS=NPTS+1
  X(NPTS)=T*CSIN(PS)+CNY
  Y(NPTS)=DIST*DCOS(PS)+CNY
  PLAT=PLAT+LLAT
  FLCN=FLCN+CLCN
  GO TO 21
30 APF1=NPTS+1
  APF2=NPTS+2
  X(NPF1)=XMIN
  X(NPF2)=APCV
  Y(NPF1)=YMIN
  Y(NPF2)=APCV
  CALL LINECX,Y,NPTS,1,1,INTEC)
  RETURN
END
SUBROUTINE GECDST(SLAT,SLON,FLAT,FLOX,AZ1,AZ2,DKM,MODE)
  DIMENSION REAL*8(A-H),REAL*8(C-Z)
  LOGICAL LCEG
  DATA EPSI/081819356/,EPAVO/6356.75023/
  FUNK(EPSI)=DATAN(DATAK(EPSI/SPSI/RIMEZ)/2.)*2
  FUNK=1.

```

```
HAFI=CATAN(CNEI)*2
PTUFI=2*PI*I/EC.
DEPS2=EC*PI(CNE-EPS2) SLAT=1.E-5
RIME2=SLAT*DETRA
IF(I)=SLCN(SLAT) LT.50.) GC TO 1
XLAN(CABS(SLAT)) GC(LELE(5.E9),SLAT)
TPSII=CATAN(CNE)
GOPTI=CATAN(FHII)*RIME2
TPSII=CATAN(TPSII)
PSIG=YABS(CKM).NF.1
LKM=CCE) 200 100 100
IF(FCRWARD SCLUTICK.
C 100 ALFAI=AZI*DETRA
IF(LLEGI) ALFAI=AZI*DETRA
IF(ALFAI) EC.TUPI) ALFAI=C.
IF(ALFAI) LT.0.) ALFAI=ALFAI+TUPI
IF(ALFAI) LE.PI) GC TC ICI
LKM=-CKM
ALFAI=ALFAI*FAN(ALFAI)
SALFAI=EC*PSII)*SALFAI
CALFAI=EC*CALFAI
SIGI=CATAN2(-CALFAI,TPSII)
XPSI=CATAN2(CALFAI,TPSII)
XK=FCI)*EPSII
TWSI=TK*SIGI
TWSF=(1.-XK)*CKM/BRVC
LWSF=TK*SI*CF
LWSIG=LWSF*XK*(XK*5*DSIN(2*DPI)*DCOS(2*TWSP)/E.-DCCS(TWSP)*DSIN(DSF)
1) SIGI+DSIG
SIG=CATAN2(DSIN(SIG),DCCS(SIG)*CPSIM)
XLB2=XLB2-XLB1
SPSI2=CATAN(CPSI2)
PSI2=CATAN(CPSI2)/RIME2
XLAN2=XLAN+CLP-CPSIM*(DSIG*(1.-RIME2)-EPS2*XK*(DSIN(2*DSIG)*DCOS(4*
PSI2))*K/(4*DETRA
FLAT=PHI2/DE
```

```

C
C
C      20C      FLCN=XLN2/CETFA
TC GET AZ2:
C      30C      INVERSE SOLUTION.
C      40C      XLN2=FLCN* CETFA
C      50C      XLN=XLN2- XLN1
C      60C      IF(C) XLN=GT.PI) DXLN=TLEI-DXLN
C      70C      DXLN=DSIGN(CMAX1(DABS(CXLN),DBLE(2.E-4)),DXLN)
C      80C      FDLB1=FCXLN/2
C      90C      PHIS12=FLCATAN(CETRA
C     100C      TFSI2=FCATAN(TFSI2)
C     110C      TEMF=CATAN2((TFSI1-TFSI2)/DTAN(HDLB1),TFSI1+TFSI2)
C     120C      XLE1=TEMPF+FDLB1
C     130C      XLB2=DCCS(XLB1)
C     140C      FSI1=CATAN(TFSI1/CLE1)
C     150C      CPSIM=DCCS(CPSIM)
C     160C      SIG1=CATAN2(CPSIM*CSIN(XLB1),CLB1)
C     170C      SIG2=CATAN2(CPSIM*CSIN(XLB2),CCOS(XLB2))
C     180C      CSIG=(SIG2+SIG1)/2
C     190C      XK=FLNK(CCSIN(PSIM))
C     200C      TERM=XK*(CDSIG)/CSIG) *CSIN(DSIG)
C     210C      FDLB2=(CXLN+FPS2*CSIM*(2.)/(RIME2+1.)-XK/2.)-TERM/2./2.) /2.
C     220C      IF(DABS(FDLB2-HDLB1).LT.1.E-7) GC TO 20
C     230C      FDLB1=FLB2
C     240C      GC TO 10
C     250C      CKM=BRAND*(CSIG+TERM-(XK**2)*DSIN(2*DSIG)*DCCS(4*SIG)/8.)/(1.-XK)
C     260C      ALFA1=CATAN2(CNE,-CTAN(XLB1))*DSIN(PSI1)
C     270C      AZ1=ALFA1
C     280C      IF(CKM.LT.C) AZ1=AZ1+PI
C     290C      IF(LDEGS(L1)Z1=AZ1/DEGFA
C     300C      ALFA2=ALFA1
C     310C      CATAN2(CNE,DTAN(XLE2))*SPSI2)
C     320C      AZ2=ALFA2
C     330C      IF(LDEGS(L2)Z2=AZ2/DEGFA
C     340C      CKM=LN
C     350C      RETURN
C     360C      SUBROUTINE RAIN1 (N,X,Y,Z,KEYX,KEYY,IER)
C     370C      THIS ROUTINE PUTS ASCENDING INTEGERS INTO KEYX(N) AND KEYY(N)
C     380C      SO THAT RAIN3 CAN ARRANGE THE X'S AND Y'S IN ASCENDING ORDER.
C     390C      DIMENSION X(N),Y(N),Z(N)
C     400C      INTEGER*2 KEYX(N),KEYY(N)

```

RAIN1940
RAIN1950
RAIN1960
RAIN1970
RAIN1980
RAIN1990

RAIN2000
 RAIN2010
 RAIN2020
 RAIN2030
 RAIN2040
 RAIN2050
 RAIN2060
 RAIN2070
 RAIN2080
 RAIN2090
 RAIN2100
 RAIN2110
 RAIN2120
 RAIN2130
 RAIN2140
 RAIN2150
 RAIN2160
 RAIN2170
 RAIN2180
 RAIN2190
 RAIN2200
 RAIN2210
 RAIN2220
 RAIN2230
 RAIN2240
 RAIN2250
 RAIN2260
 RAIN2270
 RAIN2280
 RAIN2290
 RAIN2300
 RAIN2310
 RAIN2320
 RAIN2330
 RAIN2340
 RAIN2350
 RAIN2360
 RAIN2370
 RAIN2380
 RAIN2390
 RAIN2400
 RAIN2410
 RAIN2420
 RAIN2430
 RAIN2440
 RAIN2450
 RAIN2460
 RAIN2470

```

    IFF = C
    IF (N .LE. 2767) GC TC 1
    RETURN
    DO 2 I=1,N
    KEYX(I) = X(I)
    CALL RAIN3 (Z,KEYX,N)
    DO 3 I=1,N
    KEYY(I) = Y(I)
    CALL RAIN3 (Z,KEYY,N)
    RETURN
    ENDC
    SUBROUTINE RAIN3 (A,KEY,N)
    THIS ROUTINE RETURNS THE ARRAYS, KEYX(N) AND KEYY(N), OF INTEGERS
    WHICH SPECIFY ASCENDING VALUES OF X(N),Y(N).
    INTEGER*2 KEY(N),IT
    DIMENSION A(N)
    DIM I,M1,M2,N
    I = 1
    M1 = (M1+2)
    M2 = (M2-1)
    GO TO 1
    M1 = MAXC(M1/2,1)
    M2 = MINC(M2,1)
    GO TO 2
    M1 = (M1+M2)
    M2 = (M2-M1)
    GO TO 1
    I = I+1
    IF (A(I)) .GE. A(I+1)) GC TO 5
    TEMP = A(I+1)
    A(I+1) = A(I)
    A(I) = TEMP
    KEY(I) = KEY(I+1)
    KEY(I+1) = KEY(I)
    IF (I .GT. 0) GO TO 4
    CONTINUE
    RETURN
    END
    SUBROUTINE RAIN2 (N,X,Y,Z,KEYX,KEYY,XI,YI,ZI,IER)
    DIMENSION KEY(4),X(N),Y(N),Z(N),X(12),Y(12),Z(12),A(9),NX(4)
    AMX(3,3),EMX(3)
  
```

CC

RAIN248C
 RAIN249C
 RAIN250C
 RAIN251C
 RAIN252C
 RAIN253C
 RAIN254C
 RAIN255C
 RAIN256C
 RAIN257C
 RAIN258C
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 RAIN289C
 RAIN290C
 RAIN291C
 RAIN292C
 RAIN293C
 RAIN294C
 RAIN295C

```

EQUIVALENCE (A(1), AMX(1,1)), (NX(1), N1), (NX(2), N2), (NX(3), N3),
(NX(4), N4)
1 INTEGERR(2) KEYX(N), KEYY(N), NUMOOD(4,3), KEYS(4), KBOUND(4),
1 NDIRT(12)
1 DATA JX/-1/, JY/1/, SIZE/15.0/, JSTCEL/0/

IER IS THE ERROR RETURN: N3 IS THE MINIMUM NUMBER OF POINTS ALLOW-
ED BEFOR THE INTERPOLATION: N1, N2, N3, N4 COUNT THE NUMBER OF POINTS IN
EACH OF THE FOUR QUADRANTS SURROUNDING XI, YI: AND NUMOOD IS A
4X2 MATRIX WHICH STORES THE KEY OF EACH POINT USED FOR INTERPOLATION
ACCORDING TO THE QUADRANT IT IS IN, AND HOLDS A MAXIMUM OF 3
POINTS PER QUADRANT.
IER=C
N3=C
N1=0
N2=0
N3=0
N4=0
DO 55 J=1,3
EMX(J) = C.C
CO 1 I=1,3
1 AMX(I,J) = 0.0
55 NUMOOD(I,J)=C

DEFINE MIN. AND MAX. X AND Y: DEFINE RANGE X AND RANGE Y: VARIES OF
DEFINING AREAS WITHIN 5% OF THE BOUNDARIES, AND BOUNDARY OF
EXTRAPOLATION WHICH EXTEND A MAXIMUM OF 5% BEYOND THE RANGE
OF POINTS.
IF (JX.NE.-1) GC TC 8
JX = 1
XMIN = X(KEYX(1))
XMAX = X(KEYX(N))
YMIN = Y(KEYY(1))
YMAX = Y(KEYY(N))
RANGEX = .05 * (XMAX - XMIN)
RANGEX = .05 * (YMAX - YMIN)
AUXY = XMIN + RANGEX
AUXY = XMAX - RANGEX
CNGRYL = XMIN + RANGEX
CNGRYR = XMAX - RANGEX
CNGRYB = YMIN + RANGEX
CNGRYT = YMAX - RANGEX
ENDX1 = XMAX + RANGEX
ENDX2 = XMIN - RANGEX
ENDY1 = YMAX + RANGEX
ENDY2 = YMIN - RANGEX
  
```

C C C C C C C
 C C
 C C C C C C C

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RAIN2956C
RAIN2957C
RAIN2958C
RAIN2959C
RAIN3000C
RAIN3010C
RAIN3020C
RAIN3030C
RAIN3040C
RAIN3050C
RAIN3060C
RAIN3070C
RAIN3080C
RAIN3090C
RAIN3100C
RAIN3110C
RAIN3120C
RAIN3130C
RAIN3140C
RAIN3150C
RAIN3160C
RAIN3170C
RAIN3180C
RAIN3190C
RAIN3200C
RAIN3210C
RAIN3220C
RAIN3230C
RAIN3240C
RAIN3250C
RAIN3260C
RAIN3270C
RAIN3280C
RAIN3290C
RAIN3300C
RAIN3310C
RAIN3320C
RAIN3330C
RAIN3340C
RAIN3350C
RAIN3360C
RAIN3370C
RAIN3380C
RAIN3390C
RAIN3400C
RAIN3410C
RAIN3420C
RAIN3430C

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```

C      ENDBY = YMIN - AUXY
C      ENCYT = YMAX + AUXY
C
C      KNUM IS A COUNTER FOR THE NUMBER OF POINTS WE SEARCH THROUGH TO
C      FIND POINTS IN THE CELL.
C      USE N/IC IN PLACE OF N/20 IN THE FOLLOWING STATEMENT WHEN GRID
C      TYPE DATA IS USED.  FOR EXAMPLE:
C      KNUM=MAX(C(3),N/10)
C      KNUM=MAX(C(3),N/20)
C      KBCUAC(1)=0
C      KBCUAC(2)=N-1
C      KBCUAC(3)=C
C      KBCUAC(4)=N-1
C      NPQ=3
C      TOL = 1.E-7 * (ABS(XMAX) +ABS(XMIN) +ABS(YMAX) + ABS(YMIN))
C
C      NOW CHECK TO SEE IF XI CF YI ARE WITHIN 5% OF THE RANGE DISTANCE
C      FROM THE BOUNDARY LINES DEFINED BY THE RANGE OF POINTS.
C      NOCFIL IS THE NUMBER OF QUADRANTS WE WANT TO FILL.
C      NOCFIL=4
C      IF (XI .LE. ENGRXL .CR. XI .GE. DNGRXR) GO TO 11
C      IF (XI .LT. XMTN .CR. XI .GT. XMAX) GO TO 6
C      IF (YI .LE. DNGRYB .CR. YI .GT. DNGRYT) GO TO 10
C      IF (YI .LT. YMIN .CR. YI .GT. YMAX) GO TO 7
C      GO TO 2
C      NOCFIL = MAX( NOCFIL-2,1)
C      IER=5
C      GO TO 74
C      NOCFIL = 2
C      IER=4
C      GO TO 5
C
C      IF THE POINT IS BEYOND CUR RANGE, SEE IF IT IS WITHIN 5% OVER THE
C      BOUNDARY.  IF SO, WE CAN EXTRAPOLATE, IF NOT THEN ERROR RETURN.
C      IF (XI .LT. BNDXL .CR. XI .GT. BNDXR) GO TO 66
C      IER=7
C      XI IS BEYOND THE BOUNDARY, BUT 5% OF LESS.
C      IER=7
C      GO TO 75
C
C      IER=2
C      XI IS OUT OF RANGE
C      IER=2
C      RETURN
C      IF (YI .LT. ENDBY .CR. YI .GT.BNDYT) GO TO 67
C      IER=8
C      YI IS BEYOND THE BOUNDARY, BUT 5% OF LESS.
C      IER=8
C      GO TO 68

```

```

RAIN344C
RAIN345C
RAIN346C
RAIN347C
RAIN348C
RAIN349C
RAIN350C
RAIN351C
RAIN352C
RAIN353C
RAIN354C
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C      IER = 3      Y1 IS CUT OF RANGE
C      RETURN
C      FIND THE AREA OF OUR X,Y GRID WHERE THE UNKNWN PCINT XI,YI FITS.
2     IF (X(I)I) .LE. XI) GC TC 3
      JX = JX - 1
      IF (JX .GE. 1) GC TC 2
      JX = 1
      GO TC 4
3     IX = KEYX(JX+1)
      IF (X(I)I) .GE. XI) GO TC 4
      JX = JX + 1
      IF (JX .LE. N) GC TC 3
      JX = N
      GO TC 4
4     IY = KEYI(JY)
      IF (Y(I)I) .LE. YI) GC TC 5
      JY = JY - 1
      IF (JY .GE. 1) GC TC 4
      JY = 1
      GO TC 12
5     IY = KEYI(JY+1)
      IF (Y(I)I) .GE. YI) GC TC 12
      JY = JY + 1
      IF (JY .LE. N) GO TC 5
      JY = N
C      APC IS THE NUMBER OF PCINTS FOUND IN THE CELL.
12    NODFM1 = PA)C(INCDFIL-1,1)
      NUPINC = 0
C      THIS DEFINES THE CELL SIZE.
13    SFN = FLCAT(N)/SIZE
C      DEFINE THE CELL LENGTH AND HEIGHT AS A FUNCTION OF THE SMALLER OF
THE TWO RANGES.
      XR = RANGEY
      IF (RANGEX .GT. RANGEY) XR = RANGEY
      YR = XE / SFN
      YR = XE
C      K COUNTS THE NUMBER OF CYCLES OF 4 POINTS WE SEARCH.
C      K = 0

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```

C          NCW  WE  CCLNT  CYCLES  OF  4  PCINTS.
      KEY(I,J)=KEYX(JX)
      KEYADS(1)=JX
      KEY(2)=KEYX(JX+1)
      KEYADS(2)=JX+1
      KEY(3)=KEYY(JY)
      KEYADS(3)=JY
      KEY(4)=KEYY(JY+1)
      KEYADS(4)=JY+1
C          ESTABLISH  THE  FOUR  LINES  OF  CELL  LIMIT,  A  SQUARE  CENTERED  CN  THE
      FCINT(1,YI),YI).  FCR  NCM,  XR  =  YR.
      >RT=XI+XR
      XLFT=XI-XR
      YTOP=YI+YR
      YBTM=YI-YR
C          THIS  LOOP  CHECKS  TO  SEE  IF  THE  4  POINTS  ARE  IN  THE  CFL,  IF  SO,
      IT  PUTS  EACH  IN  IT'S  PROPER  QUADRANT.
      14  DO  21  I=1,4
C          CCN'T  CHECK  THE  FIRST  CELL  SIZE  FOR  REPETITIONS
      IF  JX  OR  JY  ARE  NOT  AT  THE  BOUNDARIES  OF  THEIR  ARRAYS,
      CR  IF  THE  CELL  SIZE  HASN'T  BEEN  INCREASED.
      CR  IF  THERE  ARE  NO  PCINTS  IN  THE  CELL...
      KEVACS  IS  THE  KEY  ADDRESS,  KBOUND  IS  THE  BOUNDARY  OF  X  AND  Y
      ARRAYS,  NUMINC  IS  THE  NUMBER  OF  CELL  SIZE  INCREASES.
      IF  (KEYACS(I).LE.KBCLND(I))  GO  TO  21
      IF  (NUMINC.EC.O.AND.NFC.EC.O)  GO  TO  16
      DO  15  J=1,NPC
      IF  (IFC(J).FC.KEY(I))  GO  TO  21
      15  CONTINUE
C          SEE  IF  THE  PCINTS  ARE  IN  THE  CFL.
      16  XVALUE=X(KEY(I))
      YVALUE=Y(KEY(I))
      IF  (XVALUE.GT.XPT.OR.XVALUE.LT.XLFT.OR.YVALUE.GT.YTOP.OR.YVALUE.LT
      1.YBTM)  GO  TO  21
C          IF  YOU  GET  THIS  FAR,  THE  PCINT  IS  IN  THE  CELL,
      YOU  CAN  TAKE  A  CCFEE  BREAK  NOW.
C          PLACE  THE  FCINT  IN  IT'S  PROPER  QUADRANT  USING  A  MAXIMUM  OF  NPO
      PCINTS  PER  QUADRANT.  FCP  NOW,  NPQ  =  3.

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C C NUMCCD(I,J) FC LDCS THE KEY CF A POINT IN QUADRANT I, AND MAXIMUM J
IS 3 (FCINTS PER QUADRANT).
IF (XVALLE.LE.XI) GC TC 18
IF (YVALLE.LE.YI) GC TC 17
NUMCCD(I,N1+1)=KEY(I)
N1=N1+1
GO TC 20
17 IF (N4.GE.3) GO TO 21
NUMOCC(4,N4+1)=KEY(I)
N4=N4+1
GO TC 19
18 IF (YVALLE.LE.YI) GC TC 19
NUMOCC(2,N2+1)=KEY(I)
N2=N2+1
GO TC 20
19 IF (N3.GE.3) GO TO 21
NUMOCC(3,N3+1)=KEY(I)
N3=N3+1
20 NPC=NPC+1
IFC(INPC)=KEY(I)
21 CONTINUE

C C IF NODFIL QUADRANTS ARE FILLED, INTERPLATE.
C C NQPTS IS THE NUMBER CF QUADRANTS WITH POINTS IN THEM.
C C NQPTS=FC
DO 22 I=1,4
IF (NUMCC(I,1).NE.C) NQPTS=NUMPTS+1
22 CONTINUE
C C IF (NCWPTS.GE.NODFIL.AND.NPC.GE.NN3) GO TO 25
23 K = R+1
IF K.GE.KNUM WF'LL INCREASE CELL SIZE. OTHERWISE, THESE ARE IN
THE NEXT FCUR FCINTS, GC BACK TC SEE IF ANY OF THESE ARE IN
THE CELL
IF (K.GE.KNUM) GO TC 28
KEYACS(1)=MAYC(JX-K,C)
IF (KEYACS(1).EQ.O) GC TC 24
IF (KEYACS(1).NE.O) KEYACS(1)
KEYACS(2)=MING(JX+1+K,N+1)
24 IF (KEYACS(2).EQ.N+1) GC TO 25
KEY(2)=KEYX(KEYADS(2))
KEYACS(2)=-KEYADS(2)
25

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KEYADS(2)=MAXC(JX-I,C)
IF (KEYADS(2).EQ.0) GO TC 26
KEY(2)=KEYY(KEYADS(2))
KEYADS(4)=MINC(JX+I+K,A+1)
26 IF (KEYADS(4).EQ.N+1) GO TO 27
KEY(4)=KEYY(KEYADS(4))
27 KEYADS(4)=-KEYADS(4)
GO TC 14

C C THIS INCREASES OUR CELL SIZE.
C C JSTCEL COUNTS THE NUMBER OF PCINTS INTERPLATED WITHOUT A CELL
C C INCREASE. WHEN IT REACHES 3, THE CELL SIZE IS DECREASED.
28 SIZE=I.1*SIZE
JSTCEL=C
NUMINC=NUMINC+1

C C SETTLE FOR ONE FEWER QUADRANTS AT THIS PCINT,
C C CR GO BACK FOR MORE PCINTS.
IF (INCRPTS.LT.NCDFMI.CF.NPC.LT.NN3) GO TO 13

C C NOW FIT THE LEAST SQUARES PLANE THROUGH THE PCINTS TO CALCULATE
C C A VALUE FOR ZI.
C C IF THERE ARE 3 PCINTS IN ALL 4 QUADRANTS GO TO 27, OTHERWISE TAKE
C C THE CLOSEST 3 PCINTS, PUT A LEAST SQUARES PLANE THROUGH THEM
C C AND EXTRAPOLATE.
29 IF (INCRPTS.EQ.4) GO TC 27

C C CO 2C I=1,NPC
C C K2=IFC(I)
2C DIST(I)=SQRT((XI-X(K2))**2+(YI-Y(K2))**2)

C C DO 31 I=1,NPC
C C NDIST(I)=I

C C CALL RAIN3 (DIST,NDIST,NFC)

C C PUT THE 3 CLOSEST PCINTS INTO A MATRIX.
LCCPING EFFCN 3 TO NPC WILL CONTINUE UNTIL A NON-COLINEAR SET OF
PCINTS IS FOUND. IF ALL PCINTS ARE COLINEAR, MORE POINTS MUST BE
SEARCHED.

C C IHCPE = 3
55 K2=IFC(NDIST(I))
AMX(1,1) = X(K2)
AMX(1,2) = Y(K2)
  
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C
AMX(1,3) = 1.0
BMX(1) = -Z(K2)
K2=IFC(NCIST(2))
AMX(2,1) = X(K2)
AMX(2,2) = Y(K2)
AMX(2,3) = 1.0
BMX(2) = -Z(K2)
C
K2=IFC(NCIST(IFOPF))
AMX(3,1) = X(K2)
AMX(3,2) = Y(K2)
AMX(3,3) = 1.0
BMX(3) = -Z(K2)
GC TC 58
C
IF ALL ELSE FAILS, COME HERE. THE 3 POINTS ARE CO-LINEAR. OR
IF THE POINTS ARE COLLINEAR, ANOTHER POINT MUST BE CHOSEN, OR
MORE POINTS MUST BE SEARCHED FOR NON-COLLINEARITY.
22 IER=6
IF (IFCFE .LT. NPC) GC TO 33
NN=NN+1
GO TO 22
33 IHCPE = IHCPE + 1
IF (IFCFE .EQ. 7) GC TO 68
GC TC 59
C
IF WE GET HERE, TOO MANY POINTS ARE COLINEAR, ERROR RETURN.
68 IER = 9
RETURN
C
IF THESE ARE POINTS IN ALL 4 QUADRANTS, TAKE THE NEAREST ONE IN
EACH QUAD. AND FIT A LEAST SQUARES PLANE THROUGH THEM.
37 DO 44 I=1,4
K2=NUMCC(I,1)
NG = NX(I)
IF (AS .EQ. 1) GO TO 35
TO = SCRT ((XI-X(K2))**2 + (YI-Y(K2))**2)
C
SEARCH FOR THE CLOSEST POINT IN QUADRANT I.
40 DO 41 J=2,NC
K2 = NUMCC(I,J)
TFC = SCRT ((XI-X(K2))**2 + (YI-Y(K2))**2)
IF (TFC .GE. TO) GC TO 41
K2 = K2
41 CONTINUE

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35 AMX(1,1) = AMX(1,1) + X(K2)**2
   AMX(2,1) = AMX(2,1) + X(K2)*Y(K2)
   AMX(3,1) = AMX(3,1) + X(K2)**2
   AMX(2,2) = AMX(2,2) + Y(K2)**2
   AMX(3,2) = AMX(3,2) + Y(K2)*Z(K2)
   BMX(1) = BMX(1) - X(K2)*Z(K2)
   BMX(2) = BMX(2) - Y(K2)
   BMX(3) = BMX(3) - Z(K2)
44 CONTINUE = AMX(2,1)
   AMX(1,2) = AMX(1,2)
   AMX(3,1) = AMX(3,1)
   AMX(2,2) = AMX(2,2) + 4.
   CONTINUE
   FCRVARC SOLUTICN
58 JJ=-2 J=1,2
   DO 62 J=J+1
   JY=J+1
   JJ=JJ+4
   BIGA=C.
   IT=JJ-1=.3
   DO 70 I=1,3
   SEARCH FCR MAXIMUM COEFFICIENT IN COLUMN
   IJ=1111 (BIGA) .GE. AES(A(IJ)) GO TC 70
   BIGA=A(IJ)
   IMAX=I
70 CONTINUE
   TEST FCR PIVOT LESS THAN TOLERANCE (SINGULAR MATRIX)
   IF (ABS(BIGA) .GT. 1CL) GO TO 80
   GC TC 22
   INTERCHANGE ROWS IF NECESSARY
80 I1=J+2*(J-2)
   IT=ITMAX-J
   DO 90 KK=J,2

```

```

CCCCCCCC

```

```

CCC

```

```

CCC

```

```

CCC

```

RAIN630C
RAIN6310
RAIN6320
RAIN6330
RAIN6340
RAIN6350
RAIN6360
RAIN6370
RAIN6380
RAIN6390
RAIN6400
RAIN6410
RAIN6420
RAIN6430
RAIN6440
RAIN6450
RAIN6460
RAIN6470
RAIN6480
RAIN6490
RAIN6500
RAIN6510
RAIN6520
RAIN6530
RAIN6540
RAIN6550
RAIN6560
RAIN6570
RAIN6580
RAIN6590
RAIN6600
RAIN6610
RAIN6620
RAIN6630
RAIN6640
RAIN6650
RAIN6660
RAIN6670
RAIN6680
RAIN6690
RAIN6700
RAIN6710
RAIN6720
RAIN6730
RAIN6740
RAIN6750
RAIN6760

```
11=I1+Z
I2=I1+I1
SAVE=A(I1)
A(I1)=A(I2)
A(I2)=SAVE
CC CC
      DIVIDE EQUATION BY LEADING COEFFICIENT
50 A(I1)=A(I1)/RIGA
   SAVE=BMX(IMAX)
   BMX(IMAX)=EMX(J)
   BMX(J)=SAVE/EIGA
CC CC
      ELIMINATE NEXT VARIABLE
IF (J,EC,3) GO TO I1C
IGS=3*(J-1)
DO 65 I)=JYY,3
  IXJ=IGS+IX
  IT=J-1)
  JXX=JYY,3
  IXX=3*(JXX-1)+IX
  JXX=JXX+IT
  IXX=IXJ)+A(IXJX))-A(IXJ)+A(JJX)
100 A(IXJX)=BMX(IX) -(BMX(J))*A(IXJ)
65 BMX(IX)=BMX(IX)
CC CC
      BACK SOLUTION
110 DO 120 J=1,2
   IA=9-J
   IB=3-J
   IC=3
   DO 120 KK=1,J
     BMX(IB)=EMX(IA)-A(IA)*BMX(IC)
   IA=IA-1
120 IC=IC-1
CC CC
      THIS IS THE ANSWER
      NOW WE COMPLETE THE CALCULATION OF ZI.
      ZI = -BMX(1)*XI -BMX(2)*YI -BMX(3)
CC CC
      IF 3 POINTS ARE CALCULATED WITHOUT A CELL INCREASE, DECREASE IT.
      JUSTCEL=JUSTCEL+1
      IF (JUSTCEL>LT.3) RETURN
      JSIZER=SIZER*C.5
      JUSTCEL=C
      RETURN
      DEBUG INIT, SURCHK, TRACE
      C
```

CCC
AT 2 TRACE CN
AT 120
TRACE CFF
END

FAIN677C

```
C/*  
//GC.FIOFCC1  DD UNIT=3330,VCL=SER=DISK03,DSN=S2648.CCNF30,  
//DISP=SF  
//GC.FIOF002  CC UNIT=3330,VCL=SER=DISK03,DSN=S2648.CCNF24,  
//DISP=SF  
//GC.FIOZF001  CC UNIT=3330,VCL=SER=DISK01,DISP=SHR,DSN=S2648.GFID2  
//GC.SYSIN  DD *  
EAST LOFTEN BASIN TO VESTERAALEN RISE  
EAST CENTER LAT/LON 70-04.15-51  
70.07000 15.85000 I.C  
2  
C/*
```



```

IMAX=11
JMAX=11
SLOCPE=C IF/5.
CO 120 I=1,11
ZB(I,J)=CMAX-SLOCPE*(I-1)
ZC(I,J)=CMIN
C 15 IF(I,TYPE,TYPE 15) GO TC 16
      MCMIN,TYPE 15
      .NE.15) GO TC 16
JMAX=11
SLOCPE=C IF/75.
CO 150 I=1,151
ZB(I,J)=CMIN+SLOCPE*SQRT(RSQ)
ZC(I,J)=CMIN+ATCN,TYPE 16
C 16 IF(I,TYPE,TYPE 16) GC TC 14
      UNTYPE,TYPE 16
      .NE.16) GC TC 14
JMAX=11
SLOCPE=C IF/2.
DEP=CMIN+SLOCPE*(COS((I-76)*0.2094395)+1.)
CO 160 I=1,151
ZB(I,J)=DEP
ZC(I,J)=DEP
C 14 IF(I,TYPE,TYPE 14) GC TC 17
      TRCLGF,TYPE 14
      .NE.14) GC TC 17
JMAX=11
CMN=1.
CO 40 I=1,11
ZB(I,J)=CMIN
ZC(I,J)=DEP
C 17 IF(I,TYPE,TYPE 17) GC TC 151
      BASIN,TYPE 17
      .NE.17) GC TC 151
JMAX=11

```

```

LHN=1. C I F / 5625
SLCFE=1. I 1 E 1
COG I 1 7 0 - 1 6 1 - 1 1 1 1 1
CO I 1 7 0 - 1 6 1 - 1 1 1 1 1
XSC=(I 1 7 0 - 1 6 1 - 1 1 1 1 1) * # 2
FSC=X(I 1 7 0 - 1 6 1 - 1 1 1 1 1) * FSC
ZB(I 1 7 0 - 1 6 1 - 1 1 1 1 1)=C(NCC)
$$$ WRITE(2,2) F10.5,2I15)
2000 FORMAT(2) (A8/3) F10.5,2I15)
1000 FORMAT(2) ((ZB(I,J), I=1, IMAX), J=1, JMAX)
ENCFILE(C)
PRINT(C)
6000 PRINT(C)
1 2 3
STOP
ENC
C/*
//GC, FT02ECQ1 DC UNIT=333C, VCL=SER=DISK03, DSN=S2648.SYNBED16,
// LCB=(RECFM=FE, LRECL=8C, BLKSIZE=800), DISP=SFR,
// SFACE=(TRF,(20,5))
//GC.SYSIN DD *
85.3
C/*
1. 5. 12

```



```

EO CC 10 I=1; NRCW
II=ICT-2*I
CO 20 J=1; ACCL
JJ=JCT-2*J
2C C(I,J)=(ZEND-ZB(II,JJ))*Z
1C X(I)=I
Y(I)=I
1 CALL FLTC(I,X,NROW,Y,NCOL,D,DFGUP,DEGCCA,F,TTL,SIZE,WK,ICN,
KX,*Y,2000,2)
1 STOP
END
C/* LINK.USDC CC UNIT=3330,VCL=SER=DISK01,DSN=S2648.ECTLMCD,
//CISF=SHF,LAEL=(,,IN)
//LINK.SYSIN CC *
INCLUDE USECC(GRCSCT)
ENTFY MAIN
C/*
//GC.F101F001 CC DSN=S264E.GRID2,UNIT=3330,VCL=SER=DISK01,
//CISP=SHF,LAEL=(,,IN)
//GC.SYSIN CC *
C/*
4. 4. 45. 6

```


GFD00049
GFD00050
GFD00060
GFD00070
GFD00080
GFD00090
GFD00100
GFD00110
GFD00120
GFD00130
GFD00140
GFD00150
GFD00160
GFD00170
GFD00180
GFD00190
GFD00200
GFD00210
GFD00220
GFD00230
GFD00240
GFD00250
GFD00260
GFD00270
GFD00280
GFD00290
GFD00300
GFD00310
GFD00320
GFD00330
GFD00340
GFD00350
GFD00360
GFD00370
GFD00380
GFD00390
GFD00400
GFD00410
GFD00420
GFD00430
GFD00440
GFD00450
GFD00460
GFD00470
GFD00480
GFD00490
GFD00500
GFD00510

SUBROUTINE: GRDSCT

SUBROUTINE GRDSCT(XST,YST,XMAX,YMAX,IMAX,JMAX,DHN,ZB)

EXTRACTS KMX*KMY SECTION OF LARGER 2D DATA MATRIX.
XST,YST MUST BE MULTIPLES OF 10*DHN.
IMAX,JMAX MUST BE GF XST+KMX, YST+KMY, RESPECTIVELY.

GRDSCT IS CALLED BY THE FOLLOWING PROGRAMS:
G3ECP
GRCCPK
ECTRACE -CALLED BY TRACE

```
REAL*8 TTL(I12),CNX,CNY,CNLAT,CNLNG,DHN  
COMMON /DIM5/ KMX,KMY  
DIMENSION ICA(10),TTL,CNLAT,CNLNG,DHN,IMAX,JMAX  
FORMAT(4E16/6A8/3F10.5,2I5)  
CNX=(IMAX-1)*DHN/2  
CNY=(JMAX-1)*DHN/2  
IF (KMX.EC.IMAX.AND.KMY.EC.JMAX) GO TO 80  
IF (KMX.CNLY A SECTION OF INPUT GRID.  
FAR=LFAC*(KMX,IMAX)  
KMX=MINI(KMY,JMAX)  
KMY=MINI(XST,(IMAX-KMX)*FAR)  
YST=AMINI(YST,(JMAX-KMY)*FAR)  
GRFL=ICFL*LFAC*(XST/GRFL)  
YST=GRFL*IFIX(YST/GRFL)  
NYSZ=NCSS=NC OF ITEMS SKIPPED  
KSAZ=NC OF ITEMS SKIPPED  
KSAZC=ITEM THRESHOLD, DUMMY FULL OF NEEDED DATA (SKIP NO  
KSAZC=ITEM THRESHOLD, DUMMY FULL OF NEEDED DATA (SKIP NO
```

1010

C

CCCCC

CCCCCCCCC CCCCCCCCCC

GF001000
GF001010

RETURN
ENC


```

ZDV=(ZENC-ZST)/IANL
CALL GRDCCT(XMIN,YMIN,XMAX,YMAX,IMAX,JMAX,CFK,ZB)
NRCM=MIND(JPF-IPB+1,KMX)
NCCM=MIND(JPF-JPS+1,KMY)
JPE=JPS+NRCM-1
JRG=JMAX-XMIN
JGEC=JMAX-YMIN
LEA=IAEN*GT.0
LEPLOT=LEN*GE.4.AND.IANL.LE.100
CALL FLCT(LEN,19)
AFCT=LEN/IE.2
YOR=(Z1-UE)/2
CALL AMAXI(IE,YOR,-1)
AR15=AXY/IE
APCV=AINT(AR15)
AFCT=AFCT+AFACV
CALL FATCR(AFCT)
IF(XMIN+LFN*(IPE-1) XFS,XFE,DFN BY COLUMNS: RCWS,IB,TC,IB,
XPE=XMIN+LFN*(IPE-1) XFS,XFE,DFN BY COLUMNS: RCWS,IB,TC,IB,
PRINT 6010,IPB,APRAY,FLCWS,TO,PF.1,; DHN=,PF.1, KM.//)
6010 1  AICV=AMAXI(AICV,1.)
      AICV=AICV+LFN
      FVAL=IFS
      XMCVE=C
      NX=0
CALL AXIS(0.,0.,I-VALUES,8,15.,90.,FVAL,AICV)
CALL FLCT(0.,15.,2)
CALL IFS(-1)
IRE=IPB-1
DC 7C I=IFS,IRE
7C  ZV(I+1)=I
   ZV(I+2)=AICV
   AZCV=ZENC/3.
   IVS=NRCM+AFCK-1
   IVE=IVE+1)=0.
   ZV(IVE+2)=AZCV

```

```

CO 1C JJ=1,NCCL
    J=J+1
    YKM=YMIN+DHN*(J-1)
    PRINAT(C2C,J,YKM
    PRINAT(C2C,J,I3,Y=,F5.1)
    PRINAT(C2C,(ZB(I,J),I=IPS,IPE)
    PRINAT(C2C,(ZB(I,J),I=IPS,IPE)
    II=IP
    IC(I)=I=IVS,IVE
    I=I+1
    ZE(I,I)=ZE(I,I,J)
    ZV(I)=ZV(I,IVS),ZV(IPS),NROW,1,0,0)
    CALL WERE(XNOW,YACW,AFCT)
    CALL SYMBCL(XNCH,YNCH,.08,J=,90.,2)
    FFN=J
    CALL NUMBER(999.,555.,.08,FPN,90.,-1)
    CALL SYMBCL(999.,555.,.08,J=,90.,4)
    CALL NUMBER(999.,555.,.08,YKM,90.,4)
    XMCVF=XMCVF+.2
    NX=NX+1
    CALL FLCT(.2,0.,-3)
    CCNT INLE+5
    CALL FLCT(.2,0.,-3)
    NX=NX+2
    CALL AXIS(0.,0.,'X-VALUES',-8,15.,90.,XPS,AXDV)
    CALL FLCT(C.,15.,2)
    CALL GRID(-XMCVF,0.,-NX,.2,NY,1.,LMASK)
    IPEN=555
    IF(LFLCT) IPEN=IPEN
    CALL FLCT(C.,C.,IPEN)
    IF(.NOT. LFLCT) STCF
    TRANSPOSE ARRAY TO PUT NORTH AT TCF
C 25 CO 4C K=1,KMY
    I=K+1,I-K
    CO 4C J=1,KMX
    IJ=K+1,(J-1)+I
    ZV(IJ)=ZV(I,J)
    LTG(1)=.TRUE
    LTG(2)=.FALSE
    IF(LTG(3)) GO TO 5C
    FLENT=1
    XOR=LENCT+1
    CALL FLENTS(0,0,0)
    CALL FLCT(XCF,YCF,-3)
    CALL SYMBCL(.3,-.5,.08,TTL,50.,48)

```

```

SYABCL(.4,.5,.5,.CE,TTL(7),90.,.48)
CALL FACTR(AFCT)
CALL CCFNER(GLATMX, GLATMX, GLCMN, GLONMX, IMAX, JMAX)
DLT=1.25
CLTC=CMAX1(CABS(GLATMX), CABS(GLATMN))
ABL=ZC.
CLN=ZC.
IF(AEL.LT.65.) CLN=CLN/2
IF(ABL.LT.60.) DLN=CLN/2
CLNC=1.
IF(AEL.GT.75.) GO TC 210
CLN=1.
CLNC=.25
SLCN=GLCMN-CLN
ELCN=GLCMN+DLN
SLAT=GLATMX+DLT
ELAT=GLATMX-DLT
IF(SLCN.LT.CNLCN-90.) SLCN=SLOCN+DLN
IF(ELCN.GT.CNLCN+90.) ELCN=ELCN-DLN
SLAT=CMAX1(SLAT, DBLE(-85.))
ELAT=CMIN1(ELAT, DBLE(+85.))
LRAW LATITUDE LINE
CJ=DLN
GJ=DLN
GJ1=DLN
GJ2=ELCN
CALL GECFLR(GI, GJ1, GJ2, D., AX, AY, 1)
GJ=GI+LLT
IF(GI.LE.ELAT) GC TC 240
LJ=DLN
GJ1=DLN
GJ2=ELAT
IF(GJ1.GE.GJ2) GC TC 50
CALL GECFLR(GI, GJ1, GJ2, D., AX, AY, 2)
GJ=GI+LLN
IF(GI.LE.ELCN) GC TC 250
AX(I)=ZST
IF(ALL.LT.2) GO TO 35
CO 3C I=2, NL
IM1=I-1
AX(I)=AX(IM1)+ZCV
IH=IF(I)(YRG*AFCT/APCV+.1)
IH=IF(I)(XRG*AFCT/APCV+.1)
CALL CCNCLR(ZV, KMY, KMX, KMY, AX, NL, TTL, LEN, LEN, LTN, LTN)
STCP

```

210

240

250

290


```

DIMENSION TIL(12), XNEW(183), YNEW(183)
COMMON /FLC/ TIL, CNX, CNY, CNLAT, CNLCA
COMMON /CF/ XMIN, YMIN, XMAX, YMAX, XRG, YRG, APDV
INTEC=L1L1+2
IF(L1L1.NE.1) GO TO 1C
FLC/LATITUDE LINE GI FROM LONGITUDE GJ1 TO GJ2
PLAT=GI
PLCN=GJ1
GLAT=GI
GLCA=GJ2
CLCA=0.
GO TO 2C
LONGITUDE LINE GI FROM LATITUDE GJ1 TO GJ2
PLAT=GI
PLCN=GJ1
GLAT=GI
GLCA=GJ2
CLCA=0.
GO TO 3C
CALL GECDCST(CNLAT, CNLCA, FLAT, PLCN, HS, HF, DIST, -1)
IF(PLAT.GT.CLAT.OR.FLCA.GT.CLCA) GO TO 30
NPTS=NFTS+1
YNEW(NPTS)=CIST*DSIN(FS)+CNX
XNEW(NPTS)=YRG-(DIST*CCOS(FS)+CNY)
FLAT=FLAT+CLAT
PLCA=PLCA+CLCA
GO TO 21
NFFT=NFTS+1
NFFT=NFTS+2
YNEW(NFFT)=XMIN
YNEW(NFFT)=APCV
XNEW(NFFT)=YRG-YMIN
CALL LINE(XNEW, YNEW, NPTS, 1, 1, INTEO)
RETURN
END
SUBROUTINE GECDCST(SLAT, SLCN, FLAT, FLON, AZ1, AZ2, DKM, MODE)
IMPLICIT REAL*8(A-H), REAL*8(C-Z)
LOGICAL LCEG
DATA EPS/, .C81819356/, EPAVC/6356.75023/
FUNK(SPSI)=CTAN(DATAN(EPS*SPSI/R1ME2)/2.)*2

```

```

CNE=1.0
HAPI=2.0
TUPI=2.0
CETRA=PI/180.
EPS2=EPS2*PI/180.
RIME2=EPS2*PI/180.
PHI=SLAT*PI/180.
XLAN=SLCN*DETRA
IF(CABS(SLAT).LT.50.) GO TO 1
TPSI1=ESIGN(CBLE(5.ES),SLAT)
GO TO 2
TPSI1=CATAN(PHI)*RIME2
PSI1=CATAN(TPSI1)
LDEG=IAES(MCDE)*NE.1
LKP=LAE(LKM)
IF(MCDE) ZCC,100,100
IF(CRW) ZRE, SCLUT,ICN.
ALFA1=AZI*DETRA
IF(LDEG) ALFA1=ALFA1+TUPI
IF(ALFA1.LT.0.) ALFA1=ALFA1+TUPI
IF(ALFA1.LE.PI) GO TO 101
LKP=-LKP
ALFA1=ALFA1-PI
SALFA1=COS(ALFA1)
CPSIM=COS(PSI1)*SALFA1
CALFA1=COS(ALFA1)
XLAN=CATAN2(-CALFA1,TPSI1)
SPSIM=COS(XLAN)
XK=FUNK(SESIM)
TWSIG1=2*SIG1
TWSIF=TWSIG1+XK*(DSIN(TWSIG1)-XK*(DSIN(2*TWSIG1)/8.))
LWSP=(1.-XK)*LWSP
LWSP=TWSIF+DSP
LWSP=LWSP+XK*(XK*5*DSIN(2*DCSP)*DCOS(2*TWSP)/8.-DCOS(TWSP)*DSIN(DSP)
1)
SIG2=SIG1+DSIG
XLB2=CATAN2(DSIN(SIG2),CCS(SIG2)*CPSIM)
LLE=XLB2-XLBI
SPSI2=COS(SIG2)*SPSIM
PHI2=CATAN(LTAN(CPSI2)/RIME2)
XLAN2=XLAN1+CBLE-CPSIM*(CPSI2)*DCOS(2*SIG1)-EPS2*XK*(DSIN(2*DSIG)*DCOS(2*
1)PSI2)*XK/(4*DSIN(DSIG)*DCOS(2*SIG1)-DSIG*(1.+XK/2.))*CPSIM/4.)

```

```

C
C
C 200 XLN2=FLCN*CETRA
      DXLN=XLN2-XLN1 DXLN=TLPI-DXLN
      IF(DXLN>0) DXLN=TLPI-DXLN
      HDLBI=CXLN*(DAES(CXLN),DBLE(2.E-4)),DXLN)
      HDLBI=CXLN*(DAES(CXLN),DBLE(2.E-4)),DXLN)
      TFSI2=FLATAN(FHY2)*PRIME2
      PSI2=CATAN(TPSI2)
      TEMP=CATAN2((TPSI1-TFSI2)/DTAN(HDLBI),TPSI1+TPSI2)
10  XLBI=TEMP-FCLBI
      CLEI=COS(XLBI)
      CPSIM=CATAN(TFSI1/CLEI)
      SIG1=CATAN2((CFSIM*DSIN(XLBI),CLBI)
      SIG2=CATAN2((CPSIM*DSIN(XLBI),CCOS(XLBI)))
      SIG=(SIG2+SIG1)/2
      XK=FUNK(DSIN(PSIM))
      TERM=XK*CCOS(2*SIG)*CFSIM*(CFSIN(DSIG)
      HDLB2=(CXLN+EPS2)*CFSIM*(2./(RIME2+1.)-XK/2.)-TERM/2.)/2.
      IF(CABS(FCLR2-HDLBI).LT.1.E-7) GO TO 20
      HDLBI=FLC
      CKN=PRAVC*(CSIG+TERM-(XK*2)*DSIN(2*DSIG)*CCOS(4*SIG)/8.)/(1.-XK)
20  ALFAI=CATAN2(CNE,-CTAN(XLBI)*DSIN(PSI))
      AZI=ALFAI
      IF(CKN.LT.0) AZI=AZI+PI
      IF(CDEG) AZI=AZI/DETRA
30  IF(DABS(CABS(XLB2)-HAFI).GE.1.E-7) GC TO 35
      GO TO 36
35  ALFA2=CATAN2(ONE,DTAN(XLE2)*SPSI2)
36  AZ2=ALFA2
      LKM=CAES(LKM)
      RETURN
      ENDC
C/*
//LINK USCL LC UNIT=3330, VCL=SFR=DISK01, DSN=S2648.ECTLMOD,
//DISP=SHR, LAPEL=(, , IN)
//LINK SYSIN LCC
INCLUDE USCL(GFCSCT)

```

```
ENTFY MAIN
C/*
//GC .FIC1FC01 CC ESN=S2648.CR1D2,UNIT=3330,VCL=SER=DISK01,
// CISP=SPR;LAEEL=(,.,IN)
//GC.SYSIN CC *
-10
C; 4. C. 0.
i 151 15. 23
C/*
```


APPENDIX M

ETRACE

```

EC TRACE JCE (0354,IX82), 'ERAZO SMC1704', TIME=5
// EXEC FC CLG*, PFGICN, GC=250K
// FCFT.SYSIN UNIVERSAL MAIN FPGFAM
      FSTABLISHES SIZE CF DEPTH MATRIX IN LIEL CF OBJECT
      TIME LIMS/ KMX, KMY
      COMENSICN ZE (151, 151)
      DIMX=151
      KMY=151
      CALL TRACER (ZB)
      STCP
      END

```

```

C/* LINK .USDC DD UNIT=3320, VCL=SER=DISK01, CSN=S2648.FCTLM00,
// CISP=SFH LABEL=(, , , IN)
// IAK.SYSIN DD (TFACFR, IDPROF, NLPROF, CHNLIM)
// INCLUDE USDC (CCNTAG, BCANC, ANGRPT, IDTSUB, DFEF)
// INCLUDE USDC (EGNF1, PCTFLT, PACPLT, T2DPLT, ENDFLT)
// INCLUDE USDC (GFCSC1, SSPPL1, FBLCSS)
ENTFY MAIN
C/* REMOVE CR NULLIFY THE FOLLOWING CARD TO PRODUCE PUNCHED SUMMARY
// GC.F107FC01 CC DUMMY
// GC.F101FC01 DD CSN=S2648.GFID2, UNIT=3330, VCL=SER=DISK01,
// CISP=SFH LABEL=(, , , IN)
// GC.SYSIN CC

```


CCCCC

REFER TO CHAPTER V 'USER INSTRUCTIONS' FOR A DESCRIPTION OF THE FOLLOWING 5 DATA INPUT CARDS.

TRIAL 84 *** GENBCT GENERATED GRID2 *** 150. 150.
 125. 800. 125. 75. 5000. 150.
 C. 0. 2. -10. 200. 1. 1.
 015. 3 125. 21 10. 6 10. 3

C FIRST WATER MASS SOUND SPEED PROFILE

NWNR 5
 C. 1461. 50. 1461. 60. 1447. 70. 1445. 90. 1447.
 500. 1454. 2 1050. 1461. 1500. 1470. 4000. 1511. 7
 C BOUNDRY BETWEEN FIRST AND SECOND WATER MASS
 C FENTX FENTX FENTX
 C. 140. 10.

C SECOND WATER MASS SOUND SPEED PROFILE

SFMR 5
 C. 1450. 50. 1482. 200. 1474. 5 375. 1474. 750. 1466.
 975. 1465. 1250. 1467. 1500. 1470. 4000. 1474. 7
 C BOUNDRY BETWEEN SECOND AND THIRD WATER MASS
 C FENTX FENTX FENTX
 C. 150. 20.

C THIRD WATER MASS SOUND SPEED PROFILE

ISCV 2
 C. 1470. 5000. 1470.

C/*
 CCCC

LISTING FOR GRIDCT MAY BE FOUND IN G3CP APPENDIX

TFA00040
TFA00050
TFA00060
TFA00070
TFA00080
TFA00090
TFA00100
TFA00110
TFA00120
TFA00130
TFA00140
TFA00150
TFA00160
TFA00170
TFA00180
TFA00190
TFA00200
TFA00210
TFA00220
TFA00230
TFA00240
TFA00250
TFA00260
TFA00270
TFA00280
TFA00290
TFA00300
TFA00310
TFA00320
TFA00330
TFA00340
TFA00350
TFA00360
TFA00370
TFA00380
TFA00390
TFA00400
TFA00410
TFA00420
TFA00430
TFA00440
TFA00450
TFA00460
TFA00470
TFA00480
TFA00490
TFA00500

TRACER

```

*****
SUBROUTINE TRACER(ZE)
  L=0; FRAZC=0
  SOURCE: READS ALL USER INPUT DATA, PERFORMS ACTUAL PLOT
  PURPOSE: TRACING AND CUTPLTS TRACE HISTORY. INVOKES PLOT ROUTINES.
  IMPLICIT REAL*8(C-D), REAL*8(G), REAL*8(P-W)
  COMMON /CIPX/ KMX, KMY
  COMMON /PRINTS/ FBCT(30,50), FAAGLE(30,50)
  COMMON /PARAM/ C(50,3), GRADV(50,3), PYDT,ZC(50,3)
  COMMON /FLCTIT/ TTT,CAX,CNY,CNLAT,CNLCN
  COMMON /PRCFIL/ JMA(3), LNO1(2), LEW(2), LNS(2), FENTY(2), FENTX(2),
  1 COMMCN /SUBS/ CX,CY,ILT,IRT,IVR,JBT,JTP,JVR,XMIN,YMIN
  COMMON /CHANEL/ CC,CRE,CRN,VV,DEPL,CFS,CHD,
  1 ZENCL,LCAL(3),NVAL(2),MUP,KLW,ISSP,KMAX
  DIMENSION XFUN(103), YFUN(103)
  DIMENSION FXTX(100), FEITY(2), FXGAP(2), FYGAP(2), GRM(100)
  DIMENSION FXSURF(2), CECIT(2), UNDR(2), OSTCP(2), STCF(2), JCPCK(2)
  DATA CCVER/0.0/, SURF(2), CECIT(2), UNDR(2), OSTCP(2), STCF(2), JCPCK(2)
  1 READ 5000,CC,CTIT
  PRINT 6000,CTIT
  FCFMAT(1)/,ICX,20A4,/(/)
  6000 PLUNCH 5000,CTIT
  C
  SEE DOCUMENTATION FOR DESCRIPTION OF INPUT PARAMETERS.
  READ 5010,XC,ZO,XREC,YREC,ZREC,AREC,ELMAX,FOL
  READ 5020,XMIN,YMIN,ZST,ZEND,ARST,AREND,SMNGL
  READ 5030,NFC,NEL,NSTCP,INCPLOT,NLEN,ASSF
  FCFMAT(1)CFE(2)
  FCFMAT(1)CFE(3)
  FCWIC=FCLEN-FCST
  FCWIC=FCLEN-FCST
  IF(FCWIL.LT.0.) HDWIC=FCWID+360.
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TFA00520
 TFA00530
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 TFA00990

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    HDCV=C.
    ELDV=C.
    NHD=MIN(NEL,30)
    NSTOP=MIN(NSTOP,50)
    NSTOP=MAX(NSTOP,1)
    IF(NHD.GT.1) ELDV=ELMID/FLGAT(NHD-1)
    IF(NEL.GT.1) ELDV=ELMID/FLGAT(NEL-1)

    C
    MEAN LEADING OF WAVES
    CIRA=FCDST+HDCV*FLGAT(NHD-1)/2.
    LCSS=RLMAX*LT*1000
    IF(CSMNGL.EC.C.) SMNGL=2.

    C
    FEL DEFAULTS TO TEN WAVELENGTHS.
    WVLN=1./FRFQ
    IF(FTL.EC.O.) FDL=10000*WVLN

    C
    INPLT WATER MASS DATA
    MAXV=1
    DO 20 J=1,NSSP
      IF(J.LE.NSSP) GC TC 10
      KVAL(J)=C
      GC TC ZC
      LOCAL(J)=.FALSE.
      READ(5)GC5,GMAS(J),KMAX
      NMAXV(J)=KMAX
      REAL(5)GC10,ZC(I,J),C(I,J),I=1,KMAX
      IF(J.EC.NSSP) GC TC 20
      REAL(5)GC10,FENTX(J),FENTY(J)
      REAL(5)GC10,FEXTX(J),FEXTY(J)
      FCGAF(J)=FEXTX(J)-FENTX(J)
      FXGAF(J)=FEXTX(J).EC.O.
      LEW(J)=FXGAF(J).EC.O.
      LNCT(J)=LEW(J).AND.LNS(J)
      IF(LNCT(J)) GO TC 20
      IF(LEK(J),CR.LNS(J)) GO TO 20
      FV(J)=FXGAF(J)/FXGAF(J)
      CCNTLINE

    C
    CALCULATE GRADIENTS AND OUTPUT WATER MASS DATA.
    DO 40 J=1,NSSP
      KMAX=NVAL(J)
      KE=KMAX-1
    DO 30 I=1,KE
      K=I+1
      GRADV(I,J)=(C(K,J)-C(I,J))/(ZC(K,J)-ZC(I,J))
      GRADV(KMAX,J)=.01668
  
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TFA0100C
TFA0101C
TFA0102C
TFA0103C
TFA0104C
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TFA0141C
TFA0142C
TFA0143C
TFA0144C
TFA0145C
TFA0146C
TFA0147C

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PRINT 604C
CC 5C I=1, MAXV
IF(I,GT,NVAL(1)) GC TC 41
IF(I,GT,NVAL(2)) GC TC 42
IF(I,GT,NVAL(3)) GC TC 50
IF(I,GT,NVAL(4)) GC TC 51
PRINT 604E, ZC(I,3), C(I,3), GRADV(I,3)
50 FCFMAT(,+, , 12X,F8.2,EX,FE.2,3X,F8.5)
6041 FCFMAT(,+, , 12X,F8.2,EX,FE.2,3X,F8.5)
6042 FCFMAT(,+, , 50X,F8.2,EX,FE.2,3X,F8.5)
604E PRINT 604C, (CMAS(I), I=1,NSSP)
NFRG=N SPC-I (FENTX(I),FENTY(I),FEXTX(I),FEXTY(I),I=1,NFRG)
FORMAT(, , 7X,GRAD, //)
6040 1 FCFMAT(, , (FENTX(I),FENTY(I),FEXTX(I),FEXTY(I),I=1,NFRG)
607C FCFMAT(, , (22X,A4,13X))
608C 1 FCFMAT(, , (FRCNT/BOUNDARY INTERSECTIONS, //T12,2(27X, 'FRONT ', //T22,
2(18X, 'ENTRY, ', //T23,4(2X, ', ', F6.2, ', ', F6.2, ', ', //T22,
2REC=(XREC/1000.
Z0=ZC/1000.
C INFLT DEPTH VALUE GRID FROM FILE.
CALL GRIDSC(XMIN,YMIN,XMAX,YMAX,IMAX,JMAX,CHN,ZB)
FUNCT=ICIC,TTL
FORMAT(6A8/6A8)
X0=APAX)(XC,XMIN)
Y0=APAY)(YC,YMIN)
Z0=APAZ)(ZC,YMAX)
C PULL SOURCE CUT CF MUC.
CRE=XO
CRN=Y0
WHO=DEEF(CRE,CRN,CHN,ZB,IER)
WIF(70,CT,WFC) ZC=WFC-CC1
PICT = LATAN(CBLE(1.))
PI = 4 * PICT
TUFI = 2 * PI
DETRA = FI/180.
C MINIMUM DEPTH MUST BE AT LEAST TEN WAVELENGTHS.
FSTOP=10.*WLEN
C ATTEMPT TO PUT A MISPLACED SOURCE INTO GRID, UNDER WATER.

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C 10C ESTABLISH PLOT PARAMETERS.
      NLEN=MIN(NLEN,15)
      FAXY=AMAX1(15.,AMAX1(XMAX-XMIN,YMAX-YMIN))
      AR15=AXY/15.
      FADV=AINV/AR15
      AFACF=FACT*AFACF
      PUNCH 7C2C,XMIN,YMIN,FEV,CNX,CNY,CNLAT,CNLEN,FACT
7020 FORMAT(1CFC,3)
      ZDV=AINV/(ZENC-ZST)/2.5)
      IF(AMOD(ZEND-ZST,3.5).NE.0.) ZDV=ZDV+1.
      IF(ZST.EC.0.) ZST=-.001
      ZEND=ZST+5*ZDV
      ARCV=AINV/(AREND-ARST)/15.)
      IF(ANCC(ARCV).NE.0.) ARDV=ARCV+1.
      AREN=ARST+15.*ARDV
      PRINT 6170,XMIN,YMIN,ZST,ARST,FDV,ZDV,ARCV,XMAX,YMAX,ZEND,
1      AREN,NLEN,FACT
1 INCPLT=MAXC(1,INCPLT)
      PRINT 6200,INCPLT
6170 FORMAT(10I,118.,SELECTED.,/T6.,PLOT PARAMETERS:.,T37,'X',T47,'Y',
1 T57,'Z',T67,'R',/T12.,AXES:
2 T25,,'START',T32,4(F8.2,2X)/T25,,'DELTA',T2,4(F8.2,2X)/T25,
3 'END',T2,4(F8.2,2X)/T13,,'SCALING:.',T25,,'LENGTH:.',T3,,'IN.',FAC
4 TOR=.,FC,4)
6180 FCFMATT(/T6.,PLOT CFTICN ')
6190 FCFMATT(/T6.,T18.,REFUSED.')
6200 FORMAT(/T6.,EACH SEGMENT REPRESENTS',I3,,' POSITION CALCULATIONS.'.)
C
      INITIAL RECEIVER DISTANCE.
      XD1S=XREC-XC
      YD1S=YREC-YC
      STR=ATAN2(XC1S,YC1S)
      CBR=STR-PI
      IF(DBR.LT.-PI) DBP=CBR+TLPI
      C1ST=SCET(XC1S**2+YC1S**2)
      AREC=DIS*DCCSIDBR)
C
      FLOT INITIALIZATION ROUTINES
1 CALL XREC,YREC,ARCV,ARST,ARDV,ZST,ZDV,ZEND,
1 CALL B-TFLT(C1RX,C1RY,C1FN,WFO,XO,YO,ZENC,XMIN,XMAX,YMIN,YMAX,ZST,
1 CALL ZDV,ARST,ARDV,ZB)
      CALL SFFFLT(NVAL,NSSF,CMAS)
      KRAY=C
      FCL=FCL/1000.

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TRAD196C
TRAD1970
TRAD1980
TRAD1990
TRAD2000
TRAD2010
TRAD2020
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TRAD2080
TRAD2090
TRAD2100
TRAD2110
TRAD2120
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TRAD2140
TRAD2150
TRAD2160
TRAD2170
TRAD2180
TRAD2190
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TFA02445C
TFA02446C
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TFA02491C

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C
IEL=C
SMNGL=SMNGL*DETRA
      BEGIN NEXT RAYFAN.
110 IEL=IEL+1
      INK=ACC(IEL-1,13)
      NBNCFC=C
      IFC=0
      DO 120 I=1, D
      DO 120 J=1, -0
      FRCT(I,J)=0.0
      FANGLE(I,J)=C.0
      CCNT INCL
120 ELEV=IELST+(IEL-1)*ELCV
      ELEV=IELEVCHDETRA
      BEGIN NEXT RAY IN RAYFAN. NBNC COUNTS BCTTCM BOUNCES.
C
      NREV CCNTS ALL FEVERSALS.
C
130 KRAY=KRAY+1
      ISSP=C
      NBNC=0
      NCTFL=C
      NREV=-1
      BTMLSS=0.0
      LREV=.TRUE.
      LPORZ=.FALSE.
      LLR=.FALSE.
      LBR=.TRUE.
      NPTS=1
      NSEG=1
      FRANGE=C.
      CR=0.
      ELAP=C.
      WFI=WFC
      CEPI=ZC
      CTYPC=INIT
      IFC=IFC+1
C
      INITIAL HEADING*FCV
      ALCG=FCV*(IFD-1)*FCV
      IF(ALCG.CE.0.) ALCG=AHDCG+360.
      IF(ALFCGG.GT.360.) ALCG=AHDCG-360.
      ALCG=ALCG
      CHD(KRAY)=ALCG
      CEL(KRAY)=ELEV0
      THI=THC
      PHI=ALCG*DETRA
      IF(PHI.GT.PI) PHI=PHI-TUPI

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C C HCRIZCENTAL DIRECTION VECTOR.
LVX=DCSIN(PFI)
LVY=ECOS(PFI)
C C HCRIZCENTAL TRACERS.
CRE=XO
CRN=YC
CRMIN=ICCC.
PRINT 6220,KRAY,IHC,IEL
PRINT 6223C
PRINT 6224C
PRINT 6225C
622C FORMAT('IRAY ',I3,' (',I3,' CF RAYFAN ',I3,') TRACE HISTCRY',/
2177,'X',I24,'Y DEPTH C',/
623C FORMAT(' ',I3,' T1C8,'GRAZ',I2(4X,'BTM'))
624C FCFMATE(' NC TYPE (KM) ',I2,' (KM) ') MASS LYR MIN MAX
1 HEADING ANGLE TC REC FM REC TIME MASS LYR MIN MAX
2M/S) )
625C FORMAT(' ',I17,2(' ANGLE ',I), 'LOSS LPS',/IX,I29('--'))
C C HCRIZCENTAL PLOT FCINT.
XPLN(NFTS)=CFE
YPLN(NFTS)=CRN
C C DEPTH DIRECTION VECTOR.
CTI=ECOS(TFI)
STI=ESIN(TFI)
C C TEST BCTTCM DEPTH AND ITERATE NEXT RAY SEGMENT.
16C IF(MFI.LT.FSTCP.CR.FI.GE.10.) GO TO 530
16Z CALL ICPRCF(LNUP)
IF(LAUF) GC TC 165
IF(LLR) GC TC 170
IF(.NOT.LBB) GO TO 16C
C C RAY TAKES ON NEW PARAMETERS FROM NEW WATER MASS
OF A ECTTCM BOUNCE.
16S CI=COC
PDIS=O.
C C VERTEX VELOCITY (FAY INVARIANT).
VV=C I/CTI
CALL CFNLIN
17C G=GRADV(KUP,ISSP)
CL=FFCL
IF(KLW.LE.KMAX)CL=AMIN1(FDL,(ZC(KLW,ISSP)-ZC(KUP,ISSP)))

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TFA0252C
TFA0253C
TFA0254C
TFA0255C
TFA0256C
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TFAO3409C
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 TFAO3486C
 TFAO3487C

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180C LRFR=(CT1,NE,0.)*ANC.(G,NE,0.)
      IF(.ACT.LFR) GC TC 180
      TRAVEL TIME INTEGRATION LIMITS.
      W2P=C1/G
      W2=W2P
      RADIUS OF CURVATURE.
      RHC=-VV/G
      CTH=CL/FFC
      MAX THETA INCREMENT IS .001
      CTH=CSIGN(DMINI(DABS(CTH),DELE(.001)),CTH)
      CTH=.FALSE.
      DISTANCE CALCULATIONS.
      XDIS=CFE-XREC
      YDIS=CRN-YREC
      ZDIS=CFE1-ZREC
      RSC=XDIS**2+YDIS**2
      IF(RSC.NE.C.1) GO TC 181
      BTR=0.
      GO TC 182
      IF(ATAN2(XDIS,YDIS)/DETRA+180.
      IF(BTR.GT.260.) BTR=ETR-260.
      IF(BTR.LE.0.) BTR=ETR+260.
      IF(CRIST=CRIT(CRIST*(ZDIS**2)))
      IF(LACR.CR.DIST.GE.CRMN) GC TC 183
      MINIMUM DISTANCE WAS DETECTED.
      CTHC=AFDGE
      CTIME=ELAST
      CRMIN=ELAST
      183C IF(LREV) GC TO 19C
      IF(MCCEINSEG,INCLPT).EC.0) GO TO 195
      GO TC 20C
      REVEFSAL FCINT.
      NREV=NREV+1
      FLEV=THJ/CTETRA
      FRINT=FC4G.NREV,CTYFE,CRE,CRN,DEPI,AFDG,ELEV,BTR,DIST,ELAPS,
      1 GMAI(I,SSPI),KUP,CFS,CHC,C1
      5040C FCFMVAI(IX,I3,IX,A4,2FS,3,FW,3,5F8.3,IX,A4,2(2X,F5.3),F8.5)
      IF(CTYFE.NE.CBCTT) GC TC 185
      ENCL=18C.-EANGLE
      FRINT=5060.FRAZ,BNGL,BTMLSS,NLPS
      506C FORMAT(I+,TIC6,2FE,3,FC,1,I3)
  
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TRAC388C
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 TRAC434C
 TRAC435C

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185 IF(NBAC-GE.NSTCF.CF.ETMLSS.GE.BLMAX) GC TO 510
    IF(LBB) FCIS=0.
    IF(FCIS.(CE.PCRLIM) GC TO 550
    LREV=.FALSE.
    IF(LRFR) W2=K2P
    ACTFL=NCTFL+1
    IF(.NCT.LPLCT) GO TC 200
C
    PLOT DEFINITION PCINT.
    IF(LACRE) GC TO 191
    XDIS=CFE-X0
    YDIS=CFN-Y0
    RSC=XDIS**2+YDIS**2
    IF(RSC.NE.C.) GO TC 192
    STB=CTR
    GO TC 192
191 STB=ATAN2(XDIS,YDIS)
C
    PROJECT SEGMENT CNTC VERTICAL PLOT PLANE.
    DIF=STE-CIR
    IF(DIF.LT.-PI) DIF=DIF+TLPI
    COSDIF=DCOS(DIF)
    RNC=LSCRT(RSC)
    FDEFTH=(ZENC-DFPI)/ZCV
    FRANGE=(RNC*COSDIF-ARST)/ARDV
    CALL RNCFLT(FRANGE,FCFPT,OTYPE,LBB,IMK)
C
    SORRY, ONLY 200 REVERSALS OR 100 BCTTCM ECUNCES PERMITTED.
200 IF(NREV.EC.200.CR.NFTS.EC.101) GO TO 540
    LBB=.FALSE.
    IF(LRFR) GC TO 225
C
    STRAIGHT RAY SEGMENT.
    LLF=LL
    TH2=TH1
    CT2=CT1
    CZ=DLP*CT1
    CR=TC 250
C
    REFRACTEC RAY SEGMENT.
225 IF(TH1) 226,235,226
226 IF(DABS(TH1-DDTH) 22C,225,235
    STCF TH2 AT TURNAPCUNC POINT.
22C TH2=C.
    CT2=C1.
  
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TFA0436C
 TFA0437C
 TFA0438C
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 TFA0440C
 TFA0441C
 TFA0442C
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 TFA0445C
 TFA0446C
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 TFA0449C
 TFA0450C
 TFA0451C
 TFA0452C
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 TFA0483C

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    ST2=C
    IF(LFCRZ) GO TO 245
    GO TO 240
    ELEVATION ANGLF.
    C 235 TH2=TH1+LTH
    CT2=LCCS(TH2)
    ST2=LCSIN(TH2)
    DIFFERENCE IN CCSINES. CHOOSE ALTERNATE CALCULATION
    TH1 IS SMALL.
    C 240 CCT=(TH1-CT2)
    IF(DABS(TH1).LE.SMGL) CCT=(TH2**2-TH1**2)/2.--(TH2**4-TH1**4)/24.
    ER=RFC*(ST2-ST1)
    C 245
    INTERIM DEPTH AND HORIZONTAL COMPONENTS OF RAY SEGMENT FEAC.
    DX=DR*LVX
    DY=DR*LVY
    DEP2=DEF1+CZ
    IF(LRBI) GC TC 255
    CEE=CRE+CX
    CNK=CRA+CY
    IF(LLR) GC TC 265
    C 255
    LAYER LIMITS TEST.
    IF(KLP.EC.KMAX) GC TC 260
    IF(DEP2.GT.ZC(KLW,ISSP)) GO TO 450
    IF(KLP.EC.1) GO TC 265
    IF(DEP2.LT.ZC(KUP,ISSP)) GO TO 440
    IF(LEE) GC TC 300
    IF(LFCRZ) GC TO 280
    C
    CHANNEL LIMITS TEST. CHECK FOR RAY TURNAROUND OR REFLECTION.
    DEP IS THE BACKLIP FCINT.
    IF(.ACT.LFR.OR.(TH2.NE.C.)) GO TO 270
    DEP=CFS
    IF(DZ.GT.C.) DEP=CFC
    GC TC 220
    C 270 IF(DEP2.LT.CFS) GC TC 410
    IF(DEP2.GT.CFD) GO TC 415
    C
    TEST FOR BOTTOM CONTACT.
    WH2=CEEF(CNN,DH,ZB,IER)
    IF(ITER.NE.0) GC TC 220
    IF(DEP2.GE.WH2) GO TC 350
    C
    ADVANCE THE TRACE POSITION, TAIL TC FEAC.
    PDIS=FCIS+CP
    CRE=CE
    C 300
  
```

TFA04840
 TFA04850
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 TFA05300
 TFA05310

```

CRN=CNA
DEF1=DEF2
W1=W13
NSEG=NS*EG+1
C 310 TIME CALCULATION.
      IF(LFRF) GC TO 320
      CT=DLF/CI
      GO TO 330
      C2=C1+C*LZ
      C1=C2
      W1=W2+C2/G
      W2=DZ*(1.+ST1)/(W1*(1.+ST2))/G
      CT=CLCG(W2*(1.+ST1)/(W1*(1.+ST2)))/G
      ELAPS=ELAPS+CT
C 320 IF AT A REVERSAL FCINT, A DIRECTION CHANGE IS NECESSARY.
      IF(LFRZ) GC TO 380
      IF(LPCRZ) GC TO 360
      IF(LREV) GC TO 370
C 330 NC REVERSAL.
      CT1=CT2
      ST1=ST2
      TH1=TH2
      CTTYPE=CCFK
      GO TO 160
C 340 TURN AROUND.
      CT1=1.
      ST1=0.
      TH1=C.
      CTTYPE=CCVER
      IF(DZ.GT.0.)CTTYPE=CLNCR
      GO TO 160
C 350 SURFACE REFLECTION.
      ST1=-ST2
      TH1=-TH2
      CT1=CT2
      CTTYPE=CSLRF
      GO TO 160
C 360 BCTTCM BCUNCE CHANGES RAY PARAMETERS.
      NBNC=NBNC+1
      FBCT(IFL,NBNC)=DEP2*1000.
      FLEV = TH1/DETRA
      FANGLE(IFL,NBNC)=FLEV
  
```

TRA05320
 TRA05340
 TRA05350
 TRA05360
 TRA05370
 TRA05380
 TRA05390
 TRA05400
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 TRA05720
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 TRA05740
 TRA05750
 TRA05760
 TRA05770
 TRA05780
 TRA05790

CALL ECANG(PH1,TH1,CT1,ST1,DHN,UVX,UVY,GRAZ,SLOPE,ZB)
 AFDC = PH1/DETRA
 IF(AFDG.LE.0)AHDG=AFDC+360.
 FRAZ=GFRAZ/DETRA
 RANGLE=SLCFE/DETRA
 IF(LCSS)ETMLSS=BTMLSS+FELOSS(FRAZ)
 CO=C1
 CTYPE=CBCTT
 NPPTS=NPPTS+1
 GO TC 150

C 350 BCTTCN CONTACT. BACKTRACK TO BOTTOM DEPTH.
 LREV=.TRUE.
 LHCRZ=.FALSE.
 LLR=.FALSE.
 IF(DEF2)EC.WF2) GO TC 250
 CALL CONTACT(CRF,CRA,DEPI,WF1,CFF,CNN,DEF2,WF2,UVX,UVY,
 1 DEF=DEF2
 GO TC 425

C 410 CHANNEL LIMIT REACHED: FORCE A REVERSAL.
 DEP=CHC
 GO TC 220
 C 415
 C 420 LREV=.FALSE.
 LLR=.FALSE.
 LHCRZ=CEC.GT.0) GO TC 340
 C 425
 C 426 IF(DEF1)EC.DEPI) GO TC 340
 C 427
 C 428 IF(DEF2)EC.DEPI) GO TC 230
 C 429 IF(LRFR) GO TO 430
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C 430 BECAUSE OF REFRACTION, RAY HEAD ELEVATION ANGLE CHANGES
 AFTER DEPTH CHANGE.
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TFA0622C
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TFA0627C

```

C      KUF=KLF-1
      KLA=KLA-1
      GC TC 460
      RAY PENETRATES NEXT DEEPER LAYER.
      DEF=ZC(KLA,ISSP)
      KLF=KLF+1
      KLA=KLA+1
      LLR=2*TFLE*FALSE.
      LHCRZ=.FALSE.
      LREV=.FALSE.
      LBE=.FALSE.
      IF(DEP1.EC.DEP) GO TC 164
      GC TC 426
C      TRANSFER TO THE FOLLOWING SECTION ABORTS THE RAYTRACE.
      PRINT 6260
      FORMAT(/,1CX,'ERROR AT BOTTOM CONTACT,')
      GC TC 560
      PRINT 6270
      FORMAT(/,1CX,'BOTTOM LCSS GATE EXCEEDED,')
      GC TC 560
      PRINT 6280
      FORMAT(/,1CX,'RAY LEFT GRID,')
      GO TC 560
      PRINT 6290,WH2,HSTCP
      PRINT 6300,'BOTTOM DEPTH OF ',F7.3,' KM CUT OF ',F7.3,' TO 10.0 K
      FORMAT(/,1CX,'TRACE DATA EXCEEDS OUTPUT PARAMETERS,')
      GC TC 560
      PRINT 6310
      FORMAT(/,1CX,'RAY BECAME TRAPPED IN DUCT CR SCUND CHANNEL,')
      CCNT INLECC,ELEVO,AFCCO,NPTS,KRAY
      FUNCT 7020,(XPUN(I),YFUN(I),I=1,NPTS)
      PRINT 6320,NSEG
      PRINT 6330,'TERMINATING RAYTRACE AFTER ',I5,' SEGMENTS. '
      PRINT 6340,'ACTPL,NREV,NENC
      PRINT 6350,'PLOT BASEC ON ',I5,' POINTS, ',I5,' REVERSALS ANC
      IF(.NOT.LFLOCT) GC TC 570
C      FLCT RAY'S HORIZONTAL TRACK.
      CALL T2CFLT(XPUN,YPLN,XMIN,YMIN,FDV,NPTS,IMK,KRAY)
      IF(LNGRI) GC TO 575
      57C

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```

6340 PRINT 6340, CRMIN, CTIME
      FORMAT( '10X, 'MINIMUM DISTANCE TO RECEIVER, ',F8.2, ' KM, OCCURS AT
      TIME, ',F10.3, /)
      NR8(KRAY)=ABNC
      CB8(KRAY)=CTIME
      CT1(KRAY)=CRMIN
      CTYPE=CSICE
      EL=TL/CETRA
      PRINT 6040, NREV, OTYPE, CRE, CRN, DEPI, AHDG, EL, BTR, DIST, ELAPS,
1 ABNCF=MAX(NBNC, NENC)
  IF( IFC.LT.NFC) GO TC 13C
      RAY TRACES FOR RAYFAN COMPLETE.
580 IF(NBNC.EC.0) GO TC 610
      NTIME=NFC/15*NTIMES
      NLEFT=NFC-15*NTIMES
      PRINT 6350, TEL, ELEVO
      FORMAT( '1, 'SX, 'RAYFAN, '13, ' COMPLETE. INITIAL ELEVATION ANGLE =
1, 'F8.3, ' DEGREES. //)
      LO=90
      KE=(J-1)*15+1
      CALL ANCFRT(KS, KE, NBNC, CFD, 1)
      CALL ANCFRT(KS, KE, NBNC, CFD, 2)
      CALL ANGLE
      GO TC 61C
590 KE=15*NTIMES+1
      CALL ANCFRT(KS, KE, NBNC, CFD, 1)
      CALL ANCFRT(KS, KE, NBNC, CFD, 2)
      GO TC 610
      IF(TEL.LT.NEL) GO TC 110
      ALL TRACES COMPLETE. OUTPUT RAY SUMMARY.
6360 PRINT 7020, FEND
      PRINT 6360, KRAY
      PRINT 6370
      PRINT 6380
      FORMAT( '1, 'T4, ' RAY TRACES COMPLETED. '//10X, 'F HEADING AT CLOSEST APPROX
1, 'D MINIMUM DISTANCE TO RECEIVER, '//10X, 'T TIME AT CLOSEST APPROX TC RECEIVER, '
2, 'D TC RECEIVER, '//10X, 'T SX, ' RAY, '3X, ' INITIAL, '1X, ' NUMBER OF, '5X,
6370 PRINT 6380, 'T, 'SX, 'C, '
1, 'F, 'SX, 'T, 'SX, 'C, '
      PRINT 6390, 'NUMBER, '2X, ' HEADING, '1X, ' ELEVATION, '3X, ' ROUNCES, '
      EC 630 '=1, KRAY
      EC 635

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TFA0687C
TFA0688C
TFA0689C

```
6350 PRINT 6ESC,J,OH0(J),CEL(J),NRB(J),OBB(J),CTT(J),ORM(J)
6360 FORMAT(16X,I3,2F10.3,7X,I3,3F10.3)
6370 CONTINUE
640 IF(.NOT.LFLCT) RETURN
C      PLOT LEGEND, THEN LEAVE PLOT ENVIRONMENT.
CALL ENDFLT(SNGL(DIRA),ELST,ELDV,H0WID,NEL)
RETLFN
END
C
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C
SUBROUTINE GRDSCT MAY BE FOUND IN THE G3DF APPENDIX LISTING
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*****  
SUBROUTINES FOLLOW:  ICFFCF  
                    ALPACF  
                    CHNLIM  
                    GRESCT  
*****  
SUBROUTINE ICFFCF(LNLF)  
    DETERMINES WATER MASS INDEX BASED CN FRONTAL PENETRATION.  
    IMPLICIT REAL*8(C-I), REAL*8(G), REAL*8(P-W)  
    IMPLICIT LOGICAL*4(L)  
    COMMON /FRGFIL/CMAS(3), LNOT(2), LEW(2), LNS(2), FENTY(2), FENTX(2),  
    FPA(2)  
    COMMON/CFANEL/CO, CPE, CRN, VV, DEPI, CHS, CHD,  
    ZMPX, LCAL(3), NVAL(3), KUP, KLW, ISSP, KMAX  
    X=CRN  
    YPRG=ISSP  
    ISSP=1  
    DO 1 I=1,2  
    IF(LACT(I)) GC TC 4  
    IF(LNS(I)) GC TC 3  
    ERND=(Y-FENTY(I))/FM(I)+FENTX(I)  
    IF(X,LT,ERND) GO TC 4  
    GC TC 1  
    IF(Y,LT,FENTY(I)) GC TC 4  
    GO TC 1  
    IF(X,LT,FENTX(I)) GC TC 4  
    ISSP=ISSP+1  
    LNLF=IFFC.NF.ISSP  
    KMAX=NVAL(ISSP)  
    IF(LNLF) CALL NUPRCF  
    RETURN  
    END  
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    3  
    4  
SUBROUTINE NUPRCF  
C
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CC
CC
CC
      CALCULATES NEW WATER MASS PARAMETERS.
      IMPLICIT REAL*8(C-D), REAL*8(G), REAL*8(P-W)
      COMMON/FARFAM/C(50,2), GRADV(50,3), PIQT, ZC(50,3)
      COMMON/CHANNEL/CO, CRE, CRN, VV, DEPI, CHS, CFC,
      ZPMX, LICAL(3), NVAL(3), KUP, KLV, ISSP, KMAX
      LOGICAL LICAL
      IF(LICAL(ISSP)) GO TO 15
      IC(K)=I,KMAX
      C(K,I,ISSP)=C(K,I,ISSP)/1000.
      ZC(K,I,ISSP)=ZC(K,I,ISSP)/1000.
      LICAL(I,ISSP)=.TRUE.
10  CONTINUE
      IDENTIFY LAYER
20  K=1, KMAX
      IF(DEFI.LT.ZC(K,ISSP)) GC TO 30
      CONTINUE
      KMI=K
      GO TO 31
30  KMI=K-1
31  CO=C(KMI,ISSP)+ (DEFI-ZC(KMI,ISSP))*GRADV(KMI,ISSP)
      KUP=KMI
      KLV=KUP+1
      RETURN
      END
      SUBROUTINE CHALIM
      SOURCE:  CALCULATES REFRACTIVE SOUND CHANNEL LIMITS BASED ON A
      PLURFCS:  L' S LAW CONSTANT. ABSOLUTE LIMITS SURFACE TO 10 KM.
      NEW SNELL'S LAW CONSTANT. REAL*8(G), REAL*8(P-W)
      IMPLICIT LOGICAL*4(L)
      COMMON/FARFAM/C(50,2), GRADV(50,3), PIQT, ZC(50,3)
      COMMON/CHANNEL/CO, CRE, CRN, VV, DEPI, CHS, CFC,
      ZPMX, LICAL(3), NVAL(3), KUP, KLV, ISSP, KMAX
      GRAD=GRAD*NE.0.
      LRFR=GRAD*NE.0.
      LVFR=VV*EG*CC
      IF(.NOT.LVFR) GO TO 10
      LNFG=GRAD*LE.0.
      LPCS=GRAD*GE.0.

```



```

REAL*8 LFN
COMMON /DIM/ KMX,KMY
DIMENSION ZB(KMX,KMY), DIO(10)
LHN=1.
XST=0.
YST=C:145.
XMAX=145.
YMAX=150.
JMAX=150
READ(1,JCC0) ZB
FORMAT(1CFE.4)
1000 RETURN
END

```

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0-AD09 931

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
ECTRACE - THREE DIMENSIONAL ACOUSTIC RAY TRACE PROGRAM.(U)
MAR 80 R N CHRISTIANSON; L R ERAZO

F/G 20/1

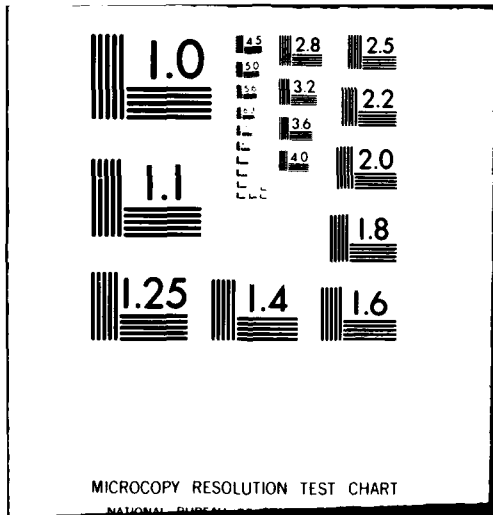
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SUBROUTINES FOLLOW:

ICTSUB
DEEPTAC
CCANAC
ECANPAT
FELCSS

SUBROUTINE ICTSUB(X,Y,CFN,IER)

SOURCE: GEORGE GIELIS, ARL
PURPOSE: ICS BALLPARK SUBSCRIPTS UNDER HORIZONTAL COORDINATES.

REAL*8 CX,CY,CHN,X,Y,XX,YY
COMMON /SUBS/ CX, DY, ILT, IRT, IVR, JBT, JTP, JVR, XST, YST
COMMON /CINS/ KMX, KMY, KITR

XX=X-YST
YY=Y-XST
ILT=XX/CFN+1.0
IRT=YY/CFN+1.0
JBT=JBT+1
JTP=JTP+1
XX=XX-(ILT-1)*DHN
YY=YY-(IRT-1)*DHN
IF (XX.LT.YY) GO TC 10
IVR=JBT
JVR=JTP
GO TC INE

10

20

CONTINUE
JVR=JTP
IER=C
IF (ILT.LT.1) IER=IER-1
IF (IRT.LT.1) IER=IER-1
IF (JBT.GT.KMX) IER=IER+1
IF (JTP.GT.KMY) IER=IER+2
RETURN
END

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 AFL00530C
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FUNCTION DEEP(CRE,CFN,CHN,ZR,IER)
SOURCE: GEORGE GIELIS, NRL
PURPOSE: GETS WATER COLUMN DEPTH UNDER HORIZONTAL COORDINATES.
IMPLICIT REAL*8(C-D),REAL*8(G),REAL*8(P-W)
COMMON /SUBZ/ KMX,KMY,KIIR
DIMENSION ZB(KMX,KMY)
CALL IRTN(CRE,CFN,IER)
IF(IER.NE.0) RETURN
CX=CRN-(IRT-1)*DHN-YST
CY=CRN-(IRT-1)*DHN-YST
DZ=ZB(IRT,JTP)
DZ=ZB(IIR,JTP)
IF(JVR.EC.JTP) GO TO 10
CY=(DZ-CY)/CFN
GO TO 20
CONTINUE
CX=(DZ-CX)/DHN
CY=(DZ-CY)/DHN
CONTINUE
RETURN
END

10
20

SUBROUTINE CCNTAC(CFE,CRN,DEP1,WH1,X2,Y2,Z2,F2,ORE,QRN,
1 THETA,CELR,DHN,ZR,NLPS,*)
SOURCE: ERIC RAZC
PURPOSE: GETS 3D COORDINATES AT BOTTOM CONTACT POINT.
IMPLICIT REAL*8(A-E),REAL*8(G-H),REAL*8(P-Z)
REAL*4 ZB
COMMON /SUBZ/ KMX,KMY,KIIR
DIMENSION ZB(KMX,KMY)
CONTINUE
LCCCK=STEP HALF OF SEGMENT LENGTH.
MOVE=CELR/ZETA
TTT=CELR
NLPS=CE
XI=CRN
YI=CFN
ZI=DEP1
  
```



```

210 CR=DSCFT1((X2-X1)**2+(Y2-Y1)**2)
211 ZF=(CZ-Z1)/(CZ+P1-P2)
212 DMCVE=(Z1-P1)/(H1-P2)
213 GO T C Z1
214 DMCVE=(Z1-P1)/CZ
215 DMCVE=DMCVE*DR
216 X2=X1+DMCVE*CRN
217 Y2=Y1+DMCVE*CRN
218 Z2=Z1+DMCVE*CRN
219 RETURN
220 PRINT *,CCC,X1,Y1,Z1,P1,X2,Y2,Z2,H2,DR,DZ,CMCVE,NLPS
221 END

SUBROUTINE BCANG(PHI,THETA,COST,SINT,DHN,UVX,UVY,GRAZ,SLCPE,ZB)
SOURCE: GEORGE GIELIS, L. R. ERAZC
PURPOSE: CALCULATES NEW RAY DIRECTION AFTER BOTTOM CONTACT.
INFLUENT REAL*8(C-D),REAL*8(G),REAL*8(F-W)
COMMON /EARS/ C(50,3),GRACV(50,3),PIQT,ZC(50,3)
COMMON /SLBS/DX,DY,IL1,IRT,IVR,JBT,JTP,JVR
COMMON /CN LAIT VECTOR IN RAY DIRECTION.
LVR=CCST
VX=UVX*LVR
VY=UVY*LVR
VZ=SINT
AREAL=AREA
ALCNG=ALCNG
JLECT=JLECT
CZ=-1.0
DSCFT((CX**2+DY**2+CZ**2)
FNL=LCX/FNL
FNY=CY/FNL
FNZ=CZ/FNL
WITH THE SLOPE OF THE FACET IS THE ANGLE THE UNIT NORMAL MAKES
WITH THE Z AXIS.
SLCPE=CAFCC(FNZ)
DOT=VX*FNX+VY*PNY+VZ*FNZ
GRAZ=CAFCC(DOT)
VFX=VX+CCN*FNX

```

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N FL 01566
 N FL 01570
 N FL 01580
 N FL 01590
 N FL 02000
 N FL 02010
 N FL 02020
 N FL 02030
 N FL 02040
 N FL 02050
 N FL 02060
 N FL 02070
 N FL 02080
 N FL 02090
 N FL 02100
 N FL 02110
 N FL 02120
 N FL 02130
 N FL 02140
 N FL 02150
 N FL 02160
 N FL 02170
 N FL 02180
 N FL 02190
 N FL 02200
 N FL 02210
 N FL 02220
 N FL 02230
 N FL 02240
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 N FL 02400
 N FL 02410
 N FL 02420

```

VPY=VY+CCN*FNX
VPZ=VZ+CCN*FNZ
TPETA=CAPSIN(VPZ)
VPR=DCOS(TPETA)
SINT=VFX/VFR
CVX=VFX/VFR
UVX=SINT
LVY=CCSINT
PHI=CATAN2(SINT,COST)
RETURN
END

SUBROUTINE ANGPRT(LS,LE,ABCUNC,HEAD,ITYPE)
SOURCE: GEORGE GIELIS, NRL
REVISED: L. R. ERAZC, FEB 1980
PLFCSE: LUTPUT OF BOUNCE DATA.
COMEN/FRINTE/FBCT(2C,50);FANGLE(30,50)
COMPEN/FRINTE/FEAC(100);KE(5C)
ITYPE=14CC
PRINT 14CC
FCFMT(1/10X,'ELEVATION ANGLES IN DEGREES BEFORE BOUNCE:')
GC TC 15CC
PRINT 15CC
FCFMT(1/10X,'DEPTH IN METERS AT BOUNCE:')
PRINT 11CC;((HEAD(I),I=LS,LE)
FCFMT(1/10X,'HEADINGS:',15FE.2)
PRINT 1011
FCFMT(1/10X,'BOUNCE')
CO 20 I=1,ABCUNC
KB(I)=I
CONTINUE I=1,LE
CO 40 GC TC 40
LE 10 I=1,ABCUNC
PRINT 1200;KE(I);((FANGLE(J,K),J=LS,LE),K=I,I)
FCFMT(1/10X,16.6X,15FE.2)
CONTINUE I=1,ABCUNC
RETURN I=1,ABCUNC
CO 40 I=1,ABCUNC
PRINT 1300;KE(I);((FECT(J,K),J=LS,LE),K=I,I)
FCFMT(1/10X,16.6X,15FE.1)
CONTINUE I=1,ABCUNC
RETURN
END
  
```

C C C C C
 C
 C

AFLO24450
 AFLO24460
 AFLO24470
 AFLO24480
 AFLO24490
 AFLO24500
 AFLO24510
 AFLO24520
 AFLO24530
 AFLO24540
 AFLO24550
 AFLO24560
 AFLO24570
 AFLO24580
 AFLO24590
 AFLO24600
 AFLO24610
 AFLO24620

```

C
C
FUNCTION FELCSS(ANGLE)
  DIMENSION ENDS(8), ELCSS(8)
  DATA ENDS/0.0,11.0,20.0,25.0,35.0,45.0,56.0,90.0/
  DATA ELCSS/0.0,0.0,3.0,4.4,6.7,8.3,10.0,10.0/
  DC I,1,7
  IF (ANGLE.GT. ENDS(I).AND.ANGLE.LE.ENDS(I+1)) GO TC 20
  IF (I.GT. 7) GO TO 30
  SLCFPE= (ELCSS(I+1)-ELCSS(I))/(ENDS(I+1)-ENDS(I))
  FELCSS=ELCSS(I)+SLCFPE*(ANGLE-ENDS(I))
  GO TC 40
  CCNT=INLE
  RETURN
  END
  10
  20
  30
  40
  
```

CP000040
 CP000050
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 CP000090
 CP000100
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 CP000310
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 CP000360
 CP000370
 CP000380
 CP000390
 CP000400
 CP000410
 CP000420
 CP000430
 CP000440
 CP000450
 CP000460
 CP000470
 CP000480
 CP000490
 CP000500

```

*****
SUBROUTINES FOLLO:
  RGAFLLT
  BCTFLLT
  SSEFLLT
  RANGFLLT
  T2CFLLT
  ENCFLLT
*****
SUBROUTINE BGNPLT(CTII,XST,YST,FDV,RST,RDV,ZST,ZDV,ZEND,
1  XREC,YREC,ZREC,FACT)
  REAL*8 YTL(12),CNX,CNY,CNLAT,CNLON
  COME N ICACT(20)
  CALL WINDC(0,25,FACT)
  CALL FLCTC(FACT)
  CALL FLCTC(0,0,95,2)
  CALL FLCTC(24,55,0,2)
  CALL FLCTC(1,0,20,6,FLCTEORDER)
  CALL DRAN FLCTC(1,CNLAT)
  CALL AXIT(0,0,1,3)
  CALL AXIT(0,0,1,2)
  CALL AXIT(0,0,1,2)
  CALL FLCTC(0,15,2)
  CALL SYMFLCTC(0,15,2)
  CALL SYMFLCTC(0,15,2)
  XSYM=(XREC-YST)/FDV
  YSYM=(YREC-XST)/FDV
  XCEN=(CNLT-YST)/FDV
  YCEN=(CNY-YST)/FDV
  IF(XCEN.GT.15.) GO TO 10
  IF(YCEN.GT.15.) GO TO 10
  CALL SYMBL(XCEN,YCEN,12,0,-1)
  C

```

000530
 000540
 000550
 000560
 000570
 000580
 000590
 000600
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 000620
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 000690
 000700
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 000980
 000990

```

CALL NUMBER(SS9, YCEN, 10, CNLAT, 0, 5)
CALL SYMBCL(SSS, YCEN, 10, 13, 0, 1)
CALL NUMVERT(CAL, PLCT, YCEN, 10, CNLCN, 0, 5)
CALL FRFLCT(15, 5, 1, RANGE (KM), 10, 19, 0, RST, RDV)
CALL AXI(15, 3, 5, 1, Z)
CALL AXIS(10, 3, 5, 1, FTH (KM), -10, 3, 5, -5C, ZST, ZDV)
CALL FLCT(15, 0, 2)
CALL FLCT(15, 0, 2)
CALL FLCT(15, 3, 5, 1, RST)
PSYM = (ZEND - RST) / RECI / ZDV
ZSYM = (ZEND - ZST - ZRECI) / ZDV
CALL SYMCL(RSYM, ZSYM, 10, REC, 0, 4)
END
  
```

SUBROUTINE BCTPLT(CTRX, CTRY, DHN, WHO, XO, YO, ZEND, XMIN, XMAX, YMIN,

```

1 YMAX, ZST, ZCV, ARST, APCV, ZB)
REAL*8 CFA, DTR, WHO, CTRY, TRKX, TRKY, TRKX, TRKY
COMMON /CIMP/ KMX, KMY
DIMENSION ICA, ITRK(193), ITRK(193), IPAT(4), ZB(KM), KMY)
DATA ITRK / 27, 514, 122, 2056 /
CTRX = CSCFT(CTRX, *2 + CTRY, *2) / ARDV
HTRK(1) = C
HTRK(10) = 2
RST = CTRY
TRKX = XQ + ARST * DTRY
TRKY = YC + AXI(SNGL(CTRX)), XMIN)
TRKX = APAXI(SNGL(CTRX)), YMIN)
TRKX = APAXI(SNGL(CTRX)), XMAX)
TRKY = APAXI(SNGL(CTRX)), YMAX)
RPTH = CEEP(CTRX, TRKY, CFA, ZB, IER)
CPTH = CEEP(CPTH, ZST)
CPTH = APAXI(CPTH, ZEND)
CPTH(2) = (ZEND - DPTH) / ZCV
FC 10 I = 3, 192
IMI = I - 1
ISTOF = I
TRKX = TRKX + CTRX
IF(CTRX) .GT. XMAX .OR. TRKX .LT. XMIN) GO TC 20
TRKY = TRKY + CTRY
IF(CTRX) .GT. YMAX .OR. TRKY .LT. YMIN) GO TC 20
PTR = RTRK(IMI) + DTR
  
```

C

C

C

CP01480
 CP01490
 CP01500
 CP01510
 CP01520
 CP01530
 CP01540
 CP01550
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 CP01590
 CP01600
 CP01610
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 CP01860
 CP01870
 CP01880
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 CP01940
 CP01950

```

10 YLCC=-7
    CALL FLCT(-20.,10.5,-2)
    RETURN
    ENC

C C
SUBROUTINE RNGPLT(FRANGE,FDEPTH,OTYPE,LBB,IMK)

    LCGICAL LEB
    DATA CINIT/,INIT,/
    IPEN=2
    IF(CTYPE.EC.CINIT) YPEN=3
    IF(FRANGE.LT.0.) IPEN=3
    IF(FRANGE.GT.15.) IPEN=3
    IF(FLEFTF.GT.3.5) IPEN=3
    IF(FLEFTF.LT.0.1) IPEN=3
    CALL FLCT(FRANGE,FDEPTH,IPEN)
    IF(CTYPE.EC.CINIT) GC T( 10
    IF(.NOT.LEB) CRIPEN,ECST, RETURN
    CALL SYRPL(FRANGE,FLEFTF,.10,IMK,0.,-1)
    RETURN
    ENC

10

C C
SUBROUTINE T2CPLT(XFUN,YFUN,XST,YST,FDV,NPTS,IMK,KRAY)

    DIMENSION XFUN(103),YFUN(103)
    FPA=KRAY
    CALL FLCT(C.,-15.5,-2)
    NPTS=NPTS+1
    XFUN(NPTS)=XST
    YFUN(NPTS)=FDV
    YPLN(NPTS)=YST
    YPLN(NPTS)=FCV
    CALL LINE(XFUN,YFUN,NPTS,1,1,IMK)
    XNCH=XFUN(NPTS)/FDV
    YNCH=YFUN(NPTS)/FDV
    CALL NUPER(XNOW,YNCH,.10,FPN,0.,-1)
    CALL FLCT(C.,15.5,-2)
    RETURN
    ENC

C C
SUBROUTINE ENCPLOT(CIRA,ELST,ELDV,HOWID,NFL)

C C

```



```

AND THE DATA.
/*
//GC.SYSIN CC *
FOLLOWING THIS CARD THE USER WILL PLACE THE ECTRACE TRIALS TO
BE COMBINED IN ONE ECCCM FLCT.
NO CARD CHANGES ARE NEEDED, HOWEVER IF THE USER DESIRES TO
HAVE THE FLCT TITLE C'ECCCM VICE ECTRACE , CHANGE THE FIRST
ECTRACE TITLE CARD TO 'ECCCM TRIAL' FROM 'ECTRACE TRIAL'.
AT THE END OF ECTRACE DATA HISTORY CARDS PLACE END OF JOB CARD
*****

```

CCCCCCCCCCCCCCCC

APPENDIX O
FORTCLGW JCL

The job control language (JCL) card for FORTCLGW used in several of the programs was

```
//EXEC FORTCLGW.REGION.GO=250K .
```

This JCL card identifies and calls the following JCL:

```
XXFORTCLGW PROC DEST=A,IMSL=SF
XXFORT EXEC PGM=IEYFORT,REGION=180K
XXSYSRINT DD SYSOUT=&DEST,DCB=(RECFM=FBA,LRECL=120,BLKSIZE=3360)
SSSYSLIN DD UNIT=SYSDA,SPACE=(CYL,(1,1)),DISP=(,PASS),DSN=&&SYSLIN,
XX DOE=(RECFM=FB,LRECL=80,BKJSUZE=800)
XXLINK EXEC PGM=IEWL,REGION=180K,PARM='MAP,LIST',COND=(4,LT)
XXSYSLIB DD DISP=SHR,DSN=SYS1.FORTLIB
XX DD DISP=SHR,DSN=SYS1.MPSLIB
XX DD DISP=SHR,DSN=SYS3.IMSL.&IMSL
XX DD DISP=SHR,DSN=SYS1.VTECPLOT
XXSYSLMOD DD DSN=&T(PROGRAM),UNIT=SYSDA,DISP=(,PASS),
XX SPACE=(CYL,(3,1,1))
XXSYSLIN DD DSN=*.FORT.SYSLIN,DISP=(OLD,DELETE)
XX DD DISP=SHR,DSN=SYS1.PROCLIE(VMAPP)
XX DD DDNAME=SYSIN
XXSYSRINT DD SYSOUT=&DEST,DOE=(RECFM=FBA,LRECL=121,BLKSIZE=1210),
XX SPACE=(CYCL,(1,1)),UNIT=(SYSOUT,SEP=SYSLIN)
XXSYSUT1 DD UNIT=(SYSDA,SEP=(SYSLIN,SYSLMOD,SYSLIB)),
XX SPACE=(TRK,(10,5))
XXPLOT EXEC PGM=IEVMAPP,COND=(4LT)
XXSTEPLIB DD DSN=SYS1.VTECPLOT,DISP=SHR
XXPLOTLOG DD SYSOUT=A
XXVECTR1 DD DISP=(OLD,DELETE),DSN=&&VECTR1
XXSYSVECTR DD DISP=(OLD,DELETE),DSN=&&VECTR2
XXSYSVECTOR DD SYSOUT=(A,,5555)
XXVECTTAPE DD DUMMY
```

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