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6 Ocean Tides, Part II.
A Hydrodynamical Interpolation Model,

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The strictly mathematical ocean tide model developed in Part I of this paper is modified in order to include realistic hydrodynamical barrier effects of narrow ocean ridges and other large bottom irregularities. This modification begins with a hydrodynamical redefinition of the ocean bathymetry at over 3,000 grid points, increasing simultaneously the depth data range to: 10m → 7,000m. In a second step a unique hydrodynamical interpolation technique is developed that incorporates into the model over 2,000 empirical tide data collected around the world at continental and island stations. This interpolation is accomplished by a controlled cell-wise adjustment of the bottom friction coefficient and by allowing a monitored in- or out-flow across the mathematical ocean boundary and so, redefining a more physical shoreline. Extensive computer experiments were conducted to study the characteristics of the novel friction laws and hydrodynamical interpolation methods. The computed M_2 -tide data along with all (specially labeled) empirical constants are tabulated in map form for four typical 30° by 50° ocean areas. It is estimated that the tabulated tidal charts permit a prediction of the M_2 -tide elevation of the ocean surface over the geoidal level with an accuracy of better than 5 cm anywhere

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in the open ocean and with somewhat less accuracy near rough shorelines. With the forthcoming construction of the lesser S_2 , N_2 , and K_2 ; K_1 , O_1 , P_1 , and Q_1 ; and Mf , Mm , and Ssa tidal constituents, the total tide-prediction error can be kept below the 10-cm bound posed by applied researchers of today.

In Part I of this paper (Schwiderski, 1979) a purely hydrodynamical ocean tide model has been developed and tested. This model has been applied to compute a preliminary M_2 ocean tidal chart (Schwiderski, 1976, I). (References listed in Part I are indicated by the added, I, after the year specification.) The results were found encouraging and satisfactory for some applications. However, significant shortcomings still persisted, especially over narrow ocean ridges. The remaining deficiencies were attributed to local distortions and retardations of the tidal waves due to hydrodynamical barrier effects of ocean ridges and other bottom irregularities.

In the following Part II of the paper, an attempt will be made to eliminate the shortcomings of the purely theoretical model by using a hydrodynamically defined bathymetry of the oceans and by incorporating directly empirically known tide data into the discrete tide model described in Part I. The latter modification will be accomplished by a controlled local adjustment of the bottom friction coefficient and by allowing a monitored in- or out-flow across the mathematical ocean boundary, and thus redefining implicitly a more physical shoreline. A detailed discussion of the quality of the new M_2 ocean tidal charts will be given in the sections, "Quality of the Ocean-Tide Model" and "Conclusions."

The complete M_2 ocean tide is published in tabulated map form in Schwiderski (1979c I). Similar charts for the S_2 , N_2 , K_2 , O_1 , P_1 , Q_1 , Mf , Mm , and Ssa ocean tides (see Part I, Table 1) are under construction and will be published in additional papers. A separate tabulation of the new hydrodynamically defined ocean bathymetry may be found in Schwiderski (1978a I). All tidal and bathymetry data will be available in tape form at the Naval Surface Weapons Center, Dahlgren, Virginia 22448.

Hydrodynamically Defined Ocean Bathymetry

A reinspection of the bathymetric data revealed clearly that even a 1° by 1° grid scheme falls far short in representing a narrow ocean ridge in a hydrodynamically proper fashion. The defect is particularly compounded when the narrow ridge parallels a deep trench. The reason for this deficiency is obviously the purely hydrostatic character of the averaging principles employed by Smith *et al.* (1966 I) in order to assign a depth value at the center of a mesh cell that is supposed to be representative for the entire cell. For instance, if the area of a mesh cell is (by subjective sight) more than half land, then it is called a "land cell," and the cell is given (for the present purpose) the depth value "zero." In the alternative case, the cell is declared "oceanic," and a depth value is assigned that conserves the estimated actual water mass. Because of those hydrostatic principles, cells were found that contained elongated islands crossing even several cells, but every cell was declared oceanic. Moreover, an oceanic trench portion of the cell with some 7,000-m true depth produced an average depth of more than 3,500 m. Clearly, for ocean current models the entire cell represents an impassable wall, and the depth value should be "zero" instead of 3,500 m.

In order to eliminate the shortcomings of the bathymetric data compiled by Smith *et al.* (1966 I), the depth values were revised by using the following "hydrodynamical" principles:

- (a) Boundary cells at or near continental shorelines consisting of more than half oceanic areas of depths larger than 5 m were designated ocean cells, and the average oceanic depth values were assigned as the "hydrodynamically" averaged depths to the entire cells. The new depth value is preferable to the "hydrostatically" averaged depth, which preserves the actual water mass but ascribes artificially a shallow shelf character to the cell.
- (b) Island cells were declared terrestrial cells with depths zero if either the island areas were larger than half the mesh

areas or the (elongated) island lengths exceeded the mesh diameters.

(c) Island cells that remained oceanic cells were assigned depth values less than the hydrostatically averaged values. In this case and in situations of submerged seamounts or narrow ocean ridges (e.g., Aleutian, Marianas, and Caribbean), the hydrodynamical depths depended on the assessed "barrier" effects of the obstacles: the longer and/or higher the barrier, the lesser the depth. In general, the average "ridge depth" was assigned to the entire cell.

(d) The assigned minimum depth (Part I, Equation 50) was lowered to

$$H_m = \min H(\lambda, \theta) = 20 \text{ m}, \quad (1)$$

which is further lowered to 10 m by the averaging Equations 65 in Part I. (All notations of Part I are used unchanged in the present paper.)

The hydrodynamically justified principles (a) to (c) are, naturally, quite subjective and by no means free of any error. Nevertheless, some computational experiments indicated only very minor effects of isolated depth data changes. More than 3,000 depth values were changed, but only very few of those required additional readjustments in order to keep some limitation on the first and second derivatives of $H(\lambda, \theta)$; i.e., on the relative differences given by Equation 65 in Part I. Furthermore, the hydrodynamical interpolation of empirical tidal data (section, "Hydrodynamical Interpolation of Empirical Tide Data") known at continental and island stations greatly diminishes the need for precise boundary-depth data. The revised depth data bank used in the new tidal computations are published in Schwiderski (1978a I).

Empirical Tide Data

The new tide model incorporates, by a unique hydrodynamical interpolation procedure (next section), empirical tidal data observed

and harmonically analyzed at numerous continental and island stations. These data were taken from publications by the National Ocean Survey (1942), the International Hydrographic Bureau (1966), the British Admiralty (1977 I), and by Pekeris and Accad (1969 I), Zahel (1970 I, 1973 I), Cartwright (1971), and Luther and Wunsch (1975 I). Unfortunately, the most recent publication by the British Admiralty lists harmonic constants only for the four major tide components M_2 , S_2 , K_1 , and O_1 and excludes the European waters completely.

The voluminous data banks had to be screened in order to eliminate observations that are meaningless or unreliable for the present ocean-tide investigations. For example, tidal constants were excluded that were listed for stations deep inside estuaries or narrow bays (e.g., Hudson River, Bay of Fundy), at the mouths of large rivers (e.g., Amazon), between sheltering islands (e.g., Alexander Archipelago, Solomon Islands), and inside sheltering reefs (e.g., Great Barrier Reef).

About 2,500 stations were selected for further examination of their data concerning locally restricted distortions. For instance, some data taken over short distances along a coastline displayed rather drastically alternating times of high water, which are obviously meaningless for oceanic tidal studies. At many stations, different tables give different tidal constants. Some of those discrepancies at island stations are shown for the M_2 -tide in Table 1. Similarly, for some mesh cells, several different station data were available, and only one representative average had to be chosen. This situation is illustrated in Table 2 for the M_2 -tide around Bermuda. Many of those differences can probably be explained as simple errors in printing or computing. For instance, the phase difference of about 1 hr at Port Galets on La Reunion Island (Table 1) seems to be due to some error in observing the correct reference time, which varies from listing to listing. Most differences, such as those shown for Bermuda stations in Table 2, are definitely true local variations. In this connection, the important tidal measurements by Gallagher *et al.* (1971) at Fanning Atoll in the central Pacific may be men-

Table 1
Empirical M₂-tide differences.

Station Latitude, Longitude		B.A.T.(77) ^a		N.O.S.(42) ^b		Others Initialed	
		$\xi(m)$	$\alpha(^{\circ})$	$\xi(m)$	$\alpha(^{\circ})$	$\xi(m)$	$\alpha(^{\circ})$
Tenerife, Canary Island 28°29'N 16°14'W	(A)	0.67				0.69	Z ^c
			18				30
Port Praia, Cape Verde I. 14°55'N 23°31'W	(A)	0.42				0.43	Z ^c
			244				220
Ascension Island 7°55'S 14°25'W	(A)	0.33				0.51	P,Z
			177				174
St. Helena Island 15°55'S 5°42'W	(A)	0.32				0.34	P,Z
			81				87
Tristan da Cunha Island 37°02'S 12°18'W	(A)	0.23				0.34	P,Z
			12				354
Agalega Island 10°28'S 56°40'E	(I)	0.29				0.29	Z
			350				290
Port Galets, La Reunion I. 20°55'S 55°17'E	(I)	0.16		0.14		0.14	Z
			302		328		328
Mawson, Antarctica 67°36'S 62°53'E	(I)	0.04				0.04	Z
			232				155
Wilkes Station, Antarctica 66°15'S 110°31'E	(I)	0.28				0.38	Z
			162				140
Welles Harbor, Midway I. 28°12'N 117°22'W	(P)	0.11				0.11	P,Z
			82				91
Eniwetok Atoll, Marshall I. 11°21'N 162°21'E	(P)	0.36		0.36			
			127		137		
Nes Wallis, Fiji Island 13°22'S 176°11'W	(P)	0.53		0.52			
			178		154		
Suva Harbor, Viti Levu, Fiji Island	(P)	0.56		0.50			
			195		212		

^a B.A.T.(77) = British Admiralty Tables (1977 I).

^b ξ = tidal amplitude.

^c α = tidal phase relative to Greenwich.

^d N.O.S. (42) = National Ocean Survey (1942).

^e Z = Zahel (1970 I).

^f P = Peteris and Accad (1969 I).

tioned. Tides outside and inside the small atoll's lagoon differed by about 50% (20 cm) in amplitude and by a phase lag of about 50° (1 hr, 40 min.).

In general, the most recent listings in the British Admiralty Tide

Tables (1977 I) were chosen over older tabulations as the most reliable. The selection of the data was further aided by earlier and subsequent tidal computations. Altogether, some 1,700 M_2 -tide data were selected and assigned to the centers of their respective mesh cells. Using linear interpolation and tidal computations, the total number of prescribed tide data used in the M_2 -tide construction was increased to more than 2,000. Essentially all continental boundary cells carry empirically supported tide data. The empirical coverage is only marginal at arctic and antarctic shorelines. Most empirical tide data known at island stations are also included in the tide model.

Naturally, it must be remembered that the selection of representative, empirical tidal data (compare depth data, section before "Hydrodynamically Defined Ocean Bathymetry") is not at all free of subjective judgment and may be somewhat erratic. Obviously, only future additional tidal measurements can improve this model

Table 2
Bermuda M_2 -tide observations.

Station Latitude, Longitude	ζ (cm)	θ (°)	Reference
St. George's Island 32.56N, 64.70W	36	359	British Admiralty (1977 I)
St. David's Island 32.37N, 64.65W	34	355	British Admiralty (1977 I)
Great Sound 32.32N, 64.69W	34	6	British Admiralty (1977 I)
St. George's Island 32.37N, 64.70W	35	0	National Ocean Survey (1942)
St. George's Island 32.40N, 64.70W	37	0	Pekeris and Accad (1969 I)
St. George's Island 32.37N, 64.70W	36	359	Zahel (1970 I)
St. George's Island 32.40N, 64.70W	36	358	Zettler et al. (1975)
Deep Sea (GOBI IV) 32.28N, 64.60W	38	11	J. T. Kuo Letter (1977)

ζ = tidal amplitude.

θ = tidal phase relative to Greenwich.

in this respect. Nevertheless, according to the instruction notes accompanying the British Admiralty Tide Tables (1977 I), it can probably be assumed that almost all important tide data selected carry an accuracy that is at least as high as the desired 10 cm. In any case, computational experiments showed that isolated reasonable variations of the boundary-tide data do not affect significantly the adjacent oceanic tides. It was also found insignificant to the overall quality of the tide model whether the empirical data were assigned to the centers or to the shore boundaries of the respective cells.

Attempts were made to incorporate also recent deep-sea tidal measurements into the present model. Since the hydrodynamical interpolation of empirical data is essentially based on bottom and boundary irregularities (see next section (a)–(d)), no physically valid justification was found to include distant offshore deep-sea measurements into the model. However, some deep-sea measurements near rough shore and bottom areas were included. Fortunately, without exception, all excluded offshore deep-sea measurements known to the author agree very well with the computed M_2 -tide data (see Table 3).

Table 3a
Deep-sea M_2 -tide data for the Gulf of Mexico and Caribbean Sea.

Station Latitude, Longitude	Observed		Model		Error	
	ξ (cm)	α (°)	ξ (cm)	α (°)	$\Delta\xi$ (cm)	$\Delta\alpha$ (°)
W. Florida Shelf St. 26.71N, 84.25W	7	97	7	92	0	-5
Deep Gulf St. 24.77N, 89.65W	1.3	226	1.6	225	+0.3	-1
Misteriosa Bank 18.88N, 83.81W	8	84	9	89	+1	+5
Rosalind Bank 16.61N, 80.34W	7	107	8	102	+1	-5
East Carib. St. (6-month) 16.54N, 84.88W	0.5	156	1.6	151	+1	-5
East Carib. St. (1-month) 16.52N, 84.91W	0.6	153	1.5	148	0.9	-5

ξ = tidal amplitude.

α = tidal phase relative to Greenwich.

Table 3b
Deep-sea M_2 -tide data for the Pacific and Atlantic oceans.

Station Latitude, Longitude	Observed		Model		Error	
	$\xi^a(\text{cm})$	$\delta^b(^\circ)$	$\xi(\text{cm})$	$\alpha(^\circ)$	$\Delta\xi(\text{cm})$	$\Delta\alpha(^\circ)$
Pacific St. 1 (Middleton) 58.76N, 145.71W	110		included			
		284				
Pacific St. 3 (Tofino) 48.97N, 127.29W	99		included			
		239				
Pacific St. (San Francisco) 38.16N, 124.91W	54		included			
		227				
Pacific St. (Josie II) 34.00N, 144.99W	27		27		0	
		267		273		+6
Pacific St. (Flicki) 32.24N, 120.86W	43		included			
		149				
Pacific St. (Josie I) 31.03N, 119.80W	43		included			
		142				
Pacific St. (Kathy) 27.75N, 124.37W	29		27		-2	
		128		130		+2
Pacific St. (Filloux) 24.78N, 129.02W	19		18		-1	
		107		105		-2
Atlantic St. 1 (N.Y. Bight) 39.32N, 64.36W	44		included			
		350				
Atlantic St. (N.C. St. 1) 32.69N, 75.62W	48		46		-2	
		356		358		+2
Atlantic St. (Savannah B) 31.95N, 80.68W	88		included			
		15				
Atlantic St. (Scope) 30.43N, 76.42W	45		46		+2	
		358		3		+5
Atlantic St. (AOML 1) 28.14N, 69.75W	34		35		+1	
		1		6		+5
Atlantic St. (AOML 3) 28.24N, 67.54W	34		34		0	
		359		4		+5
Atlantic St. (MERT) 27.99N, 69.67W	34		34		0	
		360		6		+6
Atlantic St. (REIKO) 27.97N, 69.67W	35		34		-1	
		1		6		+5
Atlantic St. (EDIE-May) 26.46N, 69.33W	32		32		0	
		3		7		+4
Atlantic St. (EDIE-March) 26.45N, 69.32W	31		32		+1	
		1		7		+6

$^a \xi$ = tidal amplitude.
 $^b \delta$ = tidal phase relative to Greenwich.

Of course, the continuity gap (Equation 4) can be attributed to the following major causes which are physically plausible:

- (a) The bottom-friction coefficient, b (in A^4 and B^4 of Equations 62 in Part I), which is most effective in boundary cells, depends on local shore features such as true cell size and bottom slope and roughness.
- (b) The boundary cells are idealized by definition of strictly mathematical boundaries (see Figure 1).
- (c) The depth data of boundary cells are subjectively defined and, hence, faulty (section, "Hydrodynamically Defined Ocean Bathymetry").
- (d) The empirical tidal constants in Equation 3 are also faulty to some degree because of inaccurate measurements, harmonic analyses, and subjective selections and assignments to the centers of the boundary cells (preceding section).
- (e) The discrete ocean-tide model is certainly not an exact description of the true oceanic tide; e.g., at boundaries, non-linear inertial terms assume significance.

Obviously, the last two (hopefully minor) faults can be reduced only through continued future observations and modeling. However, the first two faults, (a) and (b), can be weakened by "hydrodynamically interpolating" the empirical tidal elevations (Equation 3) into the tidal model and narrowing the continuity gap (Equation 4) to an acceptable level as follows:

- (A) Adjusting the velocity field by a locally controlled implicit variation of the bottom-friction coefficient, b , in Equations 62 Part I.
- (B) Lifting the strict condition of no-flow across the mathematical ocean boundary and allowing for a monitored in- or out-flow by implicitly defining a more physical ocean boundary (Figure 1).

As was pointed out in Part I, section, "The Discrete Ocean-Tide Equations (DOTEs)," due to the choice of the finite-difference

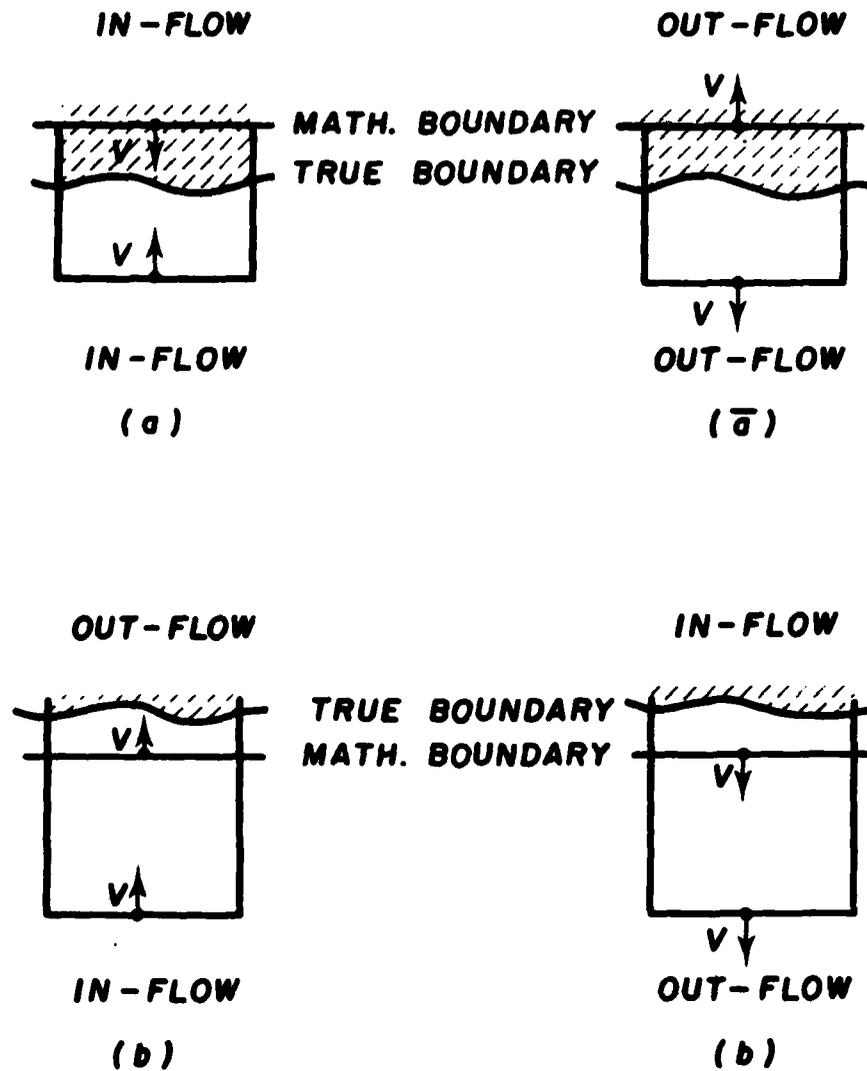


Figure 1. Boundary cell in- and out-flow illustration: (a) and (\bar{a}), also (b) and (\bar{b}) are half-periods apart. (Shaded region is land area.)

parameter $\kappa = 1$, the bottom friction coefficient, b , in A^4 and B^4 of the momentum equations (Part I, Equations 60) can be considered implicitly varied in the mesh cell $S_{m,n}$ by directly replacing the velocity components in Equation 2 as follows:

$$\begin{aligned}
 U_{m,n}^{j+1} &\rightarrow U_{m,n}^{j+1} + |U_{m,n}^{j+1}| (wU_1 + \bar{w}\bar{U}_1), \\
 U_{m+\mu,n}^{j+1} &\rightarrow U_{m+\mu,n}^{j+1} + |U_{m+\mu,n}^{j+1}| (wU_2 + \bar{w}\bar{U}_2), \\
 V_{m,n}^{j+1} &\rightarrow V_{m,n}^{j+1} + |V_{m,n}^{j+1}| (wV_1 + \bar{w}\bar{V}_1),
 \end{aligned} \tag{5}$$

and

$$V_{m,n-1}^{j+1} \rightarrow V_{m,n-1}^{j+1} + |V_{m,n-1}^{j+1}| (wV_2 + \bar{w}\bar{V}_2),$$

provided $\xi_{m,n} \neq 0$; i.e., provided an empirical tidal amplitude is available for the considered mesh cell. In Equation 5, the consistency and scale parameters (u, \bar{u}) and (v, \bar{v}) are defined by

$$\begin{cases}
 u_1 = 1, \bar{u}_1 = 0 & \text{for } \Delta\zeta_{m,n}^{j+1} \cdot U_{m,n}^{j+1} < 0, \\
 u_1 = 0, \bar{u}_1 = A_{m,n}^{\pm} & \text{otherwise, but} \\
 u_1 = 0, \bar{u}_1 = 0 & \text{if } \tilde{\xi}_{m-\mu,n} \neq 0;
 \end{cases} \tag{6a}$$

$$\begin{cases}
 u_2 = 1, \bar{u}_2 = 0 & \text{for } \Delta\zeta_{m,n}^{j+1} \cdot U_{m-\mu,n}^{j+1} > 0, \\
 u_2 = 0, \bar{u}_2 = A_{m+\mu,n}^{\pm} & \text{otherwise;}
 \end{cases} \tag{6b}$$

$$\begin{cases}
 v_1 = 1, \bar{v}_1 = 0 & \text{for } \Delta\zeta_{m,n}^{j+1} \cdot V_{m,n}^{j+1} < 0, \\
 v_1 = 0, \bar{v}_1 = B_{m,n}^{\pm} & \text{otherwise;}
 \end{cases} \tag{6c}$$

and

$$\begin{cases}
 v_2 = 1, \bar{v}_2 = 0 & \text{for } \Delta\zeta_{m,n}^{j+1} \cdot V_{m,n-1}^{j+1} > 0, \\
 v_2 = 0, \bar{v}_2 = B_{m,n-1}^{\pm} & \text{otherwise, but} \\
 v_2 = 0, \bar{v}_2 = 0 & \text{if } \xi_{m,n-1} \neq 0.
 \end{cases} \tag{6d}$$

The continuity gap (Equation 4) will be narrowed when the "control parameters" w and \bar{w} are determined successively by:

$$w = \begin{cases}
 \Delta\zeta_{m,n}^{j+1}/\zeta & \text{for } \zeta \neq 0, \\
 0 & \text{for } \zeta = 0
 \end{cases} \tag{7a}$$

with the first "control limit"

$$|w| \leq k_1 \quad (7b)$$

and

$$w = \begin{cases} [\Delta \zeta_{m,n}^{j+1} - w\zeta] / \bar{\zeta} & \text{for } \bar{\zeta} \neq 0, \\ 0 & \text{for } \bar{\zeta} = 0 \end{cases} \quad (8a)$$

with the second control limit

$$|w| \leq k_1 \quad (8b)$$

where (see Equation 3)

$$\left. \begin{aligned} \zeta &= C_n^1 [u_1 |U_{m,n}^{j+1}| + u_2 |U_{m+\mu,n}^{j+1}|] + v_1 C_n^2 |V_{m,n}^{j+1}| + v_2 C_n^3 |V_{m,n-1}^{j+1}| \\ \text{and} \\ \bar{\zeta} &= C_n^1 [\bar{u}_1 |U_{m,n}^{j+1}| + \bar{u}_2 |U_{m+\mu,n}^{j+1}|] + \bar{v}_1 C_n^2 |V_{m,n}^{j+1}| + \bar{v}_2 C_n^3 |V_{m,n-1}^{j+1}| \end{aligned} \right\} (9)$$

It is important to note that $u_i \cdot \bar{u}_i = 0$ and $v_i \cdot \bar{v}_i = 0$ for $i = 1, 2$. Accordingly, both control limits, k_1 and k_2 , which are at one's disposal, regulate the allowed decrease or, respectively, increase of the velocity components in Equations 5; i.e., the implicitly permitted corresponding increase or decrease of the local bottom-friction coefficients. Since the integration sweeps across the ocean from $m = \mu$ to 360 and $n = 4$ to 168, the special choice of $u_1 = \bar{u}_1 = 0$ and $v_2 = \bar{v}_2 = 0$ in Equations 6a and 6d excludes possible double adjustments of the velocity components. Also, if $u_1 \neq \bar{u}_1$ and/or $v_2 \neq \bar{v}_2$, backward adjustments of the tidal elevations via the corresponding Equation 2 must be made. This requires the replacements

$$\left. \begin{aligned} \zeta_{m-\mu,n}^{j+1} &\rightarrow \zeta_{m-\mu,n}^{j+1} - C_n^1 |U_{m,n}^{j+1}| (w u_1 + \bar{w} \bar{u}_1) \\ \text{and} \\ \zeta_{m,n-1}^{j+1} &\rightarrow \zeta_{m,n-1}^{j+1} - C_n^2 |V_{m,n-1}^{j+1}| (w v_2 + \bar{w} \bar{v}_2). \end{aligned} \right\} (10)$$

Analogous substitutions in the forward directions of m and n follow automatically in the integration process.

The velocity replacements in Equations 5 may be illustrated by the example

$$\left. \begin{aligned} U_{m,n}^{j+1} > 0, U_{m+\mu,n}^{j+1} > 0, V_{m,n}^{j+1} > 0, V_{m,n-1}^{j+1} \cong 0, \\ \Delta \zeta_{m,n}^{j+1} > \tilde{\xi}_{m-\mu,n} = 0, \tilde{\xi}_{m,n-1} \neq 0. \end{aligned} \right\} \quad (11)$$

One finds $w > 0, \bar{w} \geq 0$, and

$$\left. \begin{aligned} U_{m,n}^{j+1} &\rightarrow U_{m,n}^{j+1}(1 + \bar{w}A^4), \\ U_{m+\mu,n}^{j+1} &\rightarrow U_{m+\mu,n}^{j+1}(1 - w), \\ V_{m,n}^{j+1} &\rightarrow V_{m,n}^{j+1}(1 + \bar{w}B_{m,n}^4), \end{aligned} \right\} \quad (12)$$

and

$$\zeta_{m-\mu,n}^{j+1} \rightarrow \zeta_{m-\mu,n}^{j+1} - C_n^1 U_{m,n}^{j+1} \bar{w} A_{m,n}^4$$

At this point, it must be mentioned that attempts were explored to lift the control limits prescribed by k_1 and k_2 in Equations 7b and 8b in an effort to close the continuity gap completely. However, since the bottom-friction coefficient, b , is rather small the control limits, k_1 and k_2 , had to be kept small to achieve best results. Computations conducted with large control limits k_1 (excessive bottom friction) seemed to close the continuity gap, but the tidal and velocity fields in the open oceans assumed unrealistically small values. Large control limits k_2 (insufficient bottom friction) produced strong instabilities as anticipated from the analysis in the section, "Stability Analysis," of Part I. To safely check the possible instability, the second control parameter \bar{w} (Equations 5, 6, and 12) was defined in units of $\bar{u} = A^4$ and $\bar{v} = B^4$, in contrast to $u = 1$ and $v = 1$, used for the first control parameter w .

After some trial-and-error computations, the following control limits were chosen for the m_2 -tide model:

$$k_1 = 0.03, k_2 = 0.06. \quad (13)$$

These moderate values reflect the well-known fact that the magnitude of bottom friction has a strong effect on the motions considered. Indeed, with some minor improvements of the tidal field, significant improvements of the continuity gap, velocity field, and convergence of the integration were achieved. This procedure was applied to all oceanic cells with known empirical tide data (Equation 3), provided these cells bordered terrestrial cells or contained small islands or other bottom irregularities. No meaningful reason was seen to apply the same bottom-friction adjustment procedure to distant offshore oceanic cells with available deep-sea tide measurements.

In order to implement the second step (B) of the hydrodynamical interpolation procedure, the following velocity replacements in oceanic mesh cells bordering terrestrial cells were defined:

$$\left. \begin{aligned} U_{m,n}^{j+1} &\rightarrow \tilde{w}\tilde{u}_1 U_{m+\mu,n}^{j+1}, \\ U_{m+\mu,n}^{j+1} &\rightarrow \tilde{w}\tilde{u}_2 U_{m,n}^{j+1}, \\ V_{m,n}^{j+1} &\rightarrow \tilde{w}\tilde{v}_1 V_{m,n-1}^{j+1} \end{aligned} \right\} \quad (14)$$

and

$$V_{m,n-1}^{j+1} \rightarrow wv_2 V_{m,n}^{j+1}$$

provided $\tilde{\xi} \neq 0$ in Equation 3. The parameters ($\tilde{u}\tilde{v}$) are mutually consistent by definition:

$$\left. \begin{aligned} \tilde{u}_1 &= 1 \text{ if } U_{m,n}^{j+1} = 0, \text{ otherwise } \tilde{u}_1 = 0, \\ \tilde{u}_2 &= 1 \text{ if } U_{m+\mu,n}^{j+1} = 0, \text{ otherwise } \tilde{u}_2 = 0, \\ \tilde{v}_1 &= 1 \text{ if } V_{m,n}^{j+1} = 0, \text{ otherwise } \tilde{v}_1 = 0, \end{aligned} \right\} \quad (15)$$

and

$$\tilde{v}_2 = 1 \text{ if } V_{m,n-1}^{j+1} = 0, \text{ otherwise } \tilde{v}_2 = 0.$$

The remaining continuity gap will be further narrowed when the control parameter \tilde{w} is determined to be in agreement with Equations 2, 4, 7, 8, and 9 by

$$\tilde{w} = \begin{cases} [\Delta\zeta_{m,n}^{t+1} - w\zeta - \bar{w}\bar{\zeta}]/\tilde{\zeta} & \text{for } \tilde{\zeta} \neq 0 \\ 0 & \text{for } \tilde{\zeta} = 0 \end{cases} \quad (16a)$$

with the third control limit

$$|\tilde{w}| \leq k_s, \quad (16b)$$

where

$$\tilde{\zeta} = C_n^1[\tilde{u}_1 U_{m,n}^{t+1} - \tilde{u}_2 U_{m,n}^{t+1}] + \tilde{v}_1 C_n^2 V_{m,n-1}^{t+1} - \tilde{v}_2 C_n^3 V_{m,n}^{t+1}. \quad (17)$$

Obviously, the substitutions (Equations 14) specify consistent in- or out-flows across the mathematical boundaries of oceanic coastal cells, as illustrated in Figure 1, without explicitly fixing the physical boundary line. Again, no complete removal of the continuity gap was possible. The most satisfactory results for the M₂-tide were achieved by setting the third control limit (Equation 16b) at

$$k_s = 0.5. \quad (18)$$

While the improvement of the tidal field was again moderate, the remaining continuity gaps and nearshore velocity distortions assumed uniformly satisfactory levels. The remaining small shortcomings of the model can easily be attributed to the boundary inaccuracies (c), (d), and (e) listed above, but for which no simple remedies were found.

It may be emphasized that the rather significant change in the nearshore velocity field permitted by the in- and out-flow specifications (Equations 14) affected the tidal field only in a minor fashion. This important phenomenon is in agreement with the well-known fact that the pressure distribution in a fluid motion is very insensitive to large but local velocity variations. For instance, it is perhaps the most important postulate in Prandtl's boundary-layer theory (see, e.g., Schlichting, 1968 I), and it is the basis of the hydro-

static-pressure assumption invoked here and in the section, "The Continuous Ocean-Tide Equations (COTEs)," of Part I for the present tidal model.

The hydrodynamical interpolation technique considerably accelerated the convergence of the integration procedure toward the steady state amplitudes and phases. In fact, the computation of the new M_2 -tide model (sections, "Quality of the Ocean-Tide Model" and "Conclusions") was terminated when the amplitudes and phases over all open ocean areas differed by less than 1 cm and 1° , respectively. Obviously, this improved convergence feature goes significantly beyond the same property described in Part I, section, "Lateral-Boundary, Initial and Final Data," for the purely mathematical model.

Quality of the Ocean-Tide Model

Since the present tide model incorporates essentially all known empirical data by hydrodynamical interpolation (preceding section), no direct comparison of observed and computed data is feasible. Nevertheless, a comprehensive appraisal of the reality of the present tide model is possible by inspecting the quality of hydrodynamical interpolation; i.e., by evaluating the "smoothness" with which the computed tide "accepts or rejects" the empirical tidal data. In fact, the smoothness characteristics of the novel hydrodynamical interpolation technique are distinctly different from those of other direct interpolation procedures using power or trigonometric polynomials. In the latter case, smoothness of the interpolation can be carried up to any desired degree by simple design. The adjustment of hydrodynamical parameters (preceding section) in the former method does not imply any smoothness of the interpolation, unless both the empirical input data and the hydrodynamical tide model are compatible with each other.

As is well known, local tidal distortions, caused by an isolated roughness (seamount or small island) in the bottom relief, affect the surrounding ocean tide very little. The major level of ocean tides is shaped by continental shorelines and large (in area and/or length) islands and ridges. In contrast to ordinary polynomial in-

terpolations, an important feature of the new hydrodynamical interpolation method is that it preserves those significant properties of ocean tidal currents without any essential alterations.

Extensive computer experiments were conducted to test the important smoothness characteristics of the hydrodynamical interpolation procedure. Faulty input data were deliberately inserted and quickly recognized as rejected by the computed surrounding tide. Indeed, the first computations, which included empirical tidal data, revealed immediately several input errors in the data. Vice versa, smoothly accepted empirical tidal data were randomly deleted to test their backlash reaction on the computed tide. As anticipated, no significant modifications were detected. Consequently, the hydrodynamical interpolation technique permits a check of the reality of both the tide model and the empirical tidal input data. If an input value is rejected by the computed tide, then one or the other or both are defective. Fortunately, only very few discrepancies between the different sources of observed M_2 -tide data (see section, "Empirical Tide Data") have been discovered that way.

The new discrete tide-model has been applied to compute the global M_2 ocean tide. A complete discussion and tabulation of all amplitudes and phases is presented in Schwiderski (1979c I). In order to display the quality of the tidal model, the computed amplitudes (in cm) and phases (in degrees) along with their adjacent empirical values have been tabulated in "30° by 50° map form" for four typical ocean areas (Tables 4-7). All empirically supported input data along continental shores and at island stations are underlined in the tables. All nearshore deep-sea measurements included in the model are labeled by subbrackets. As was explained in the preceding section, all distant offshore deep-sea measurements are not included in the tide model. However, their approximate locations are marked by wavy underlines, and their corresponding observed data are listed in Table 3. Land points are left blank.

In the evaluation of the tidal accuracy, one must remember that the ocean tide at any fixed location is determined by two harmonic constants. If (ξ, δ) and (ξ', δ') denote the respective local amplitudes and phases of the "true" and "computed" tides

$$\zeta_0 = \xi_0 \cos(\sigma t - \delta_0), \zeta = \xi \cos(\sigma t - \delta), \quad (19)$$

then their time-dependent error is

$$\tilde{\zeta} = \zeta_0 - \zeta = \tilde{\xi} \cos(\sigma t - \tilde{\delta}) \quad (20)$$

with the standard deviation

$$\text{rms}(\tilde{\zeta}) = \frac{1}{2} \sqrt{2\tilde{\xi}}, \quad (21)$$

where

$$\tilde{\xi}^2 = \xi_0^2 - 2\xi_0\xi \cos(\delta_0 - \delta) + \xi^2 \quad (22)$$

and

$$\tan \tilde{\delta} = \frac{\xi_0 \sin \delta_0 - \xi \sin \delta}{\xi_0 \cos \delta_0 - \xi \cos \delta}. \quad (23)$$

Some maximum errors are

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi_0 + \xi \text{ for } \delta_0 - \delta = 180^\circ, \quad (24)$$

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi_0 - \xi \text{ for } \delta_0 - \delta = 0^\circ, \quad (25)$$

$$\tilde{\zeta}_M = \tilde{\xi}_M = 2\xi \sin \frac{1}{2}(\delta_0 - \delta) \text{ for } \xi = \xi_0, \quad (26)$$

and

$$\tilde{\zeta}_M = \tilde{\xi}_M = \xi \text{ for } \xi = \xi_0 \text{ and } \delta_0 - \delta = 60^\circ. \quad (27)$$

Equation 27 expresses the important fact that a 60° phase error results in an amplitude error equal to the tidal amplitude and, hence, renders the computed tidal prediction completely useless. Of course, in regions of sufficiently small amplitudes, any phase error is acceptable.

Tables 4A and 4B depict the tidal amplitudes and phases, respectively, of the northwestern Atlantic Ocean including the eastern Caribbean Sea. As can be verified by earlier tide models, this

entire area was very difficult to model, because its rough bottom topography has a strong effect on the tidal currents that sweep over or across various barriers with rapidly changing water levels. There is the broad and shallow continental shelf along the whole North American shoreline, with Cape Hatteras, Long Island, Cape Cod, Nova Scotia, and Newfoundland all protruding into the ocean basin. Furthermore, there are the Grand Banks, the Bahama Banks, and the long and narrow Caribbean Ridge. Obviously, all of the corresponding local tidal features could not be realistically captured by the tide model without a proper representation of the bathymetry (section, "Hydrodynamically Defined Ocean Bathymetry") and without the hydrodynamical interpolation (preceding section) of the locally collected tidal observations.

Now, if one scans the tidal amplitudes and phases (Tables 4A and 4B) from the north to the south, one gathers the impression that the whole computed ocean tide is completely locked into the array of empirical (underlined) tidal data everywhere along the continental coast and along the many aligned islands separating the Atlantic Ocean from the Gulf of Mexico and the Caribbean Sea. It is particularly impressive to see the observed tide data at the offshore islands (Sable—SI, Barbados—BB, and even as far as Bermuda—BI) and at the included nearshore (subbrackets), deep-sea stations all realistically well-accepted by the computed surrounding tide. Moreover, one finds the excluded offshore deep-sea measurements (locations marked by wavy underlines) in the Atlantic and Caribbean Sea fully verified by the independent tide model.

As can be seen in the special listing of Table 3, the measured and computed amplitudes and phases at the Atlantic stations agree within 2 cm and 6°, respectively. The remaining discrepancy is probably within the experimental error due to short observation times and the use of the distant reference station Bermuda (Zettler *et al.*, 1975), which exhibits even larger gaps between the various tidal observations listed in Table 2.

Attention may be drawn to the existence of considerable slopes between the empirical boundary data and the computed ocean-tide

values in the high-amplitude ranges from Nova Scotia to Cape Cod and from Cape Hatteras to Florida's coast. Yet, these rapid tidal variations can be considered as realistic because throughout the same sections the empirical data, among themselves, display exactly the same roughness. This only substantiates clearly the fundamental difference between polynomial and hydrodynamical interpolation techniques pointed out above.

In the complete report (Schwiderski, 1979c I), the same tidal roughness will be recognized in several similar coastal places around the world. From this typical phenomenon, one can draw the fortunate conclusion that, while some empirical data may be lacking high accuracy (see Table 1 and the British Admiralty Tide Tables, 1977 I), the computed adjacent ocean tide may retain its high quality.

In order to gain a deeper insight into the detailed tidal phenomena from the enclosed table charts (e.g., Tables 4A and 4B), it is helpful to recall the physical meaning of the tabulated tidal constants. The local tidal amplitude, ξ , is defined as half the tidal "range," which measures the total variation of the water level from high to low. Lines of constant amplitudes are called "orange lines." The local phase, δ , specifies the tidal cresting time (in degrees) after the moon's (or sun's) passage over the Greenwich meridian. For the present M_2 -tide one has the following time conversions:

$$\begin{aligned} 360^\circ &= 12.421 \text{ hr (period),} \\ 30^\circ &= 1.035 \text{ hr,} \\ 1^\circ &= 2.070 \text{ min.} \end{aligned} \tag{28}$$

Lines of constant phases (simultaneous cresting times) are called "cotidal lines." In particular, at the $0^\circ = 360^\circ$ cotidal lines, which are conspicuously visible in the phase charts (Tables 4B to 7B), the tide crests simultaneously with the moon's passage over the Greenwich meridian. The tidal crest advances with time normal to the cotidal lines toward larger phases. A point of zero amplitude ($\xi = 0$) around which the tidal crest rotates from 0° to 360° is called an "amphidromic point"; it is marked in the tables by a circled star \odot .

Table BA M₂ Mean amplitudes (mm) of the northeastern Pacific Ocean.

40	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245
41	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140
42	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133
43	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127
44	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121
45	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115
46	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109
47	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103
48	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97
49	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91
50	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85
51	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79
52	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73
53	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67
54	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61
55	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55
56	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49
57	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43
58	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37
59	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
60	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
61	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
62	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
63	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
64	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
65	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
66	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
67	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
68	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
69	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
70	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
71	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
72	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
73	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
74	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
75	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
76	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
77	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
78	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
79	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30

CANADA

QUEEN I.
CHARLOTTE I.
CALS

UNITED STATES

S. FRANCISCO

MEXICO

Table 7A. M₂ tidal amplitudes (cm) of the central Pacific Ocean.

180	181	182	183	184	185	186	187	188	189	190	191
192	193	194	195	196	197	198	199	200	201	202	203
204	205	206	207	208	209	210	211	212	213	214	215
216	217	218	219	220	221	222	223	224	225	226	227
228	229	230	231	232	233	234	235	236	237	238	239
240	241	242	243	244	245	246	247	248	249	250	251
252	253	254	255	256	257	258	259	260	261	262	263
264	265	266	267	268	269	270	271	272	273	274	275
276	277	278	279	280	281	282	283	284	285	286	287
288	289	290	291	292	293	294	295	296	297	298	299
300	301	302	303	304	305	306	307	308	309	310	311
312	313	314	315	316	317	318	319	320	321	322	323
324	325	326	327	328	329	330	331	332	333	334	335
336	337	338	339	340	341	342	343	344	345	346	347
348	349	350	351	352	353	354	355	356	357	358	359
360	361	362	363	364	365	366	367	368	369	370	371
372	373	374	375	376	377	378	379	380	381	382	383
384	385	386	387	388	389	390	391	392	393	394	395
396	397	398	399	400	401	402	403	404	405	406	407
408	409	410	411	412	413	414	415	416	417	418	419
420	421	422	423	424	425	426	427	428	429	430	431
432	433	434	435	436	437	438	439	440	441	442	443
444	445	446	447	448	449	450	451	452	453	454	455
456	457	458	459	460	461	462	463	464	465	466	467
468	469	470	471	472	473	474	475	476	477	478	479
480	481	482	483	484	485	486	487	488	489	490	491
492	493	494	495	496	497	498	499	500	501	502	503
504	505	506	507	508	509	510	511	512	513	514	515
516	517	518	519	520	521	522	523	524	525	526	527
528	529	530	531	532	533	534	535	536	537	538	539
540	541	542	543	544	545	546	547	548	549	550	551
552	553	554	555	556	557	558	559	560	561	562	563
564	565	566	567	568	569	570	571	572	573	574	575
576	577	578	579	580	581	582	583	584	585	586	587
588	589	590	591	592	593	594	595	596	597	598	599
600	601	602	603	604	605	606	607	608	609	610	611
612	613	614	615	616	617	618	619	620	621	622	623
624	625	626	627	628	629	630	631	632	633	634	635
636	637	638	639	640	641	642	643	644	645	646	647
648	649	650	651	652	653	654	655	656	657	658	659
660	661	662	663	664	665	666	667	668	669	670	671
672	673	674	675	676	677	678	679	680	681	682	683
684	685	686	687	688	689	690	691	692	693	694	695
696	697	698	699	700	701	702	703	704	705	706	707
708	709	710	711	712	713	714	715	716	717	718	719
720	721	722	723	724	725	726	727	728	729	730	731
732	733	734	735	736	737	738	739	740	741	742	743
744	745	746	747	748	749	750	751	752	753	754	755
756	757	758	759	760	761	762	763	764	765	766	767
768	769	770	771	772	773	774	775	776	777	778	779
780	781	782	783	784	785	786	787	788	789	790	791
792	793	794	795	796	797	798	799	800	801	802	803
804	805	806	807	808	809	810	811	812	813	814	815
816	817	818	819	820	821	822	823	824	825	826	827
828	829	830	831	832	833	834	835	836	837	838	839
840	841	842	843	844	845	846	847	848	849	850	851
852	853	854	855	856	857	858	859	860	861	862	863
864	865	866	867	868	869	870	871	872	873	874	875
876	877	878	879	880	881	882	883	884	885	886	887
888	889	890	891	892	893	894	895	896	897	898	899
900	901	902	903	904	905	906	907	908	909	910	911
912	913	914	915	916	917	918	919	920	921	922	923
924	925	926	927	928	929	930	931	932	933	934	935
936	937	938	939	940	941	942	943	944	945	946	947
948	949	950	951	952	953	954	955	956	957	958	959
960	961	962	963	964	965	966	967	968	969	970	971
972	973	974	975	976	977	978	979	980	981	982	983
984	985	986	987	988	989	990	991	992	993	994	995
996	997	998	999	1000	1001	1002	1003	1004	1005	1006	1007

In the area of Tables 4A and 4B, a major amphidromic point is visible in the Caribbean Sea southeast of the island of Puerto Rico (PRI) near the marked deep-sea gauge station. The loosely connected Caribbean and Atlantic tides rotate counterclockwise around this point with the $0^\circ = 360^\circ$ cotidal line running northeastward. As a result of this rotation, the whole Caribbean Sea appears to be trapped and unable to develop any significant M_2 -tide. In agreement with the observations, the M_2 tidal crest sweeps across the Caribbean Sea essentially from north to south with very little variation in water level.

If one follows the tidal crest around the amphidromic point from the Atlantic Ocean to the Caribbean Sea and back to the Atlantic, one recognizes a major tidal distortion caused by ocean ridges, which has long been discovered by practical tidalists (see, e.g., Harris, 1904 I; Bogdanov, 1961 I; Defant, 1961 I; and Luther and Wunsch, 1974 I). As the tide crosses the ridge between the islands, it suffers a distinct amplitude jump and a significant phase shift. For example, north of Puerto Rico (PRI) and Hispaniola and in the southeast around Barbados (BB), the computed and empirical Atlantic tide data display a higher water level and an earlier or, respectively, a delayed cresting time than the adjacent tide data on the Caribbean side. In particular, in full agreement with the observations, the tidal retardation time can easily exceed 30° (~ 1 hour). The distortion seems to depend on the angle with which the tidal crest spills over the ridge. Maximum distortion appears to be associated with a normal crossing. It may be pointed out that the realistic resolution of tidal distortions by ocean ridges (see below) constitutes probably the most significant improvement of the new model over all earlier hydrodynamical models.

The Atlantic portion of the Caribbean-Atlantic amphidromic rotation is opposed by a southward advancing tide from about Newfoundland in the north and by an eastward progressing tide from about Cape Cod to Cape Hatteras in the west. As a result of this interaction of three opposing tidal waves, the middle latitudes (around $n = 60^\circ$) of the Atlantic display very small variations in tidal amplitudes and phases. In the high-amplitude sections be-

tween Nova Scotia and Cape Cod and between Cape Hatteras and Florida's coast, the Caribbean-Atlantic rotation wave seems to be less affected by the opposing tidal waves and progresses frontally against the corresponding shallow coastal corners.

Since the tide-generating M_2 -potential is a single progressing wave from east to west, the ocean responds with amphidromic tidal waves that cannot reverse their directions. Thus, at shore points tidal waves are either incoming or outgoing without reversals. In the first case tidal crests always move from sea to shore. In the second case tides always swell to their crests at the shore first and then move out to sea. The incoming tide between Nova Scotia and Cape Cod seems to produce high and rough waters. The outgoing tide between Cape Cod and Cape Hatteras is distinctly lower.

Although the computed tide in the Gulf of St. Lawrence displays the well-known amphidromic point (Defant, 1961 I), the grid system is much too crude to attach a high accuracy to the tidal constants in this border sea. For the same reason, the tidal data listed between Florida, Cuba, and the Bahamas are naturally less accurate than those in the open oceans.

Tables 5A and 5B illustrate the smoothness with which the computed tide of the northeastern Pacific Ocean attaches itself to the empirical tide data along the North American west coast. The tidal constants observed at the islands of Guadalupe (GI) and Farallon (FI), at the Cobb Seamount (CS), and at the included nearshore deep-sea stations fit realistically well into the computed surrounding tide. The amplitudes and phases of the excluded offshore deep-sea measurements in the Pacific agree within 2 cm and 6°, respectively, with the computed data (Table 3), which is just the same accuracy as in the Atlantic.

Perhaps the most prominent feature of this area is the amphidromic point , around which the M_2 -tide rotates counterclockwise. This amphidromic system was predicted by Munk *et al.* (1970) and Irish *et al.* (1971) in almost identical geographical position. Earlier hydrodynamical tide models failed to resolve this system on proper location, although several models matched the empirical data along the coast quite well. Since the northeastern

Pacific falls short in major bottom and coastal irregularities when compared to the northwestern Atlantic, the indicated rapid loss of quality in westerly direction seemed disappointing. Yet, as will be demonstrated below, this shortcoming could have been concluded from the obvious failure of those models to reasonably reproduce the tide over most of the north and central Pacific Ocean.

As was mentioned before, the author's preliminary tide model (Schwidorski, 1976 I) used a bathymetry that failed to represent the hydrodynamical barrier effects of the Marianas, Nampo, Kuril, Aleutian, and Hawaiian ridges, as well as of other seamount chains. Consequently, the M_2 -tide of almost the whole central, western, and northern Pacific area was modeled as a single huge amphidromic system, as pictured by the similar maps of other numerical tidalists such as Zahel (1971 I) and Estes (1975 I, 1977 I). The clockwise-rotating Pacific tide was free to sweep undisturbed into the Philippine, Okhotsk, and Bering seas. By the time the computed tidal crest reached the Aleutian Islands, it was just about 180° out of phase. When the original bathymetry was replaced by hydrodynamically defined depth data (section, "Hydrodynamically Defined Ocean Bathymetry"), the entire Pacific Ocean resembled a whirlpool after some continued computations over several quarter periods. The amphidromic system weakened, and its center slipped slowly southward, but drastically improved phases appeared gradually along the Aleutian Ridge, confirming the anticipated effect of ocean ridges.

The complete turnaround of the Pacific M_2 tide near the Aleutian Islands was speeded up when the empirical tidal constants were introduced into the model. In fact, a repeat of the same computations settled the Pacific Ocean tide into its final position in a rather dramatic fashion. Striking improvements were registered over the whole Pacific and, of course, also over the Atlantic and Indian oceans.

As is depicted in Tables 6A and 6B for the north-central Pacific, the amphidromic system is replaced by a low-amplitude tide. It appears to be locked in between the Aleutian and Hawaiian ridges in the north and south and also between the Emperor Seamount

chain in the west and the high-amplitude tide in the east, which progresses in a westerly direction from the west coast of North America (Tables 5A and 5B). The amplitude topography of this area resembles the low-amplitude tide in the Caribbean Sea (Table 4A). When the westward-advancing tidal wave enters the region between the Aleutian and Hawaiian ridges, it suffers a remarkable, almost symmetric retardation at both ridges. In fact, as the visible ($0^\circ = 360^\circ$) cotidal line in Table 6B reveals, the crest front of the tidal wave assumes the shape of an almost symmetric wedge. If one traces the 0° phase line westward beginning at both ridges, one can infer a definite idea about the realistic reproduction of the tide in this region. At both ends, the 0° phase is in full agreement with the empirical data. As the observed phases grow westward along both ridges, so grow proportionally the distances of the 0° phase line from the ridges.

The new computed M_2 -tide model no longer indicates any symptoms of the original phase problems at the Aleutian and Hawaiian ridges. The computed amplitudes and phases approach the empirical tidal constants from both sides of the ridges as smoothly as could be desired. As the tidal wave spills over both ridges in north-westward or southwestward directions, respectively, it suffers a tidal distortion similar to that found before at the Caribbean Ridge. Amplitude jumps and major phase shifts are again in complete agreement with observations (see the remarks of Luther and Wunsch, 1974 I). It is particularly gratifying to find the phase shift well developed along the whole length of the Hawaiian Ridge from the island of Hawaii to Midway, even though only few stations of data were used at both ends. Also, it may be noticed that the observed tidal constants at the distant and isolated island stations of Pribilof (PF), Midway (MW), and Johnston (JI) are all realistically well integrated by the surrounding computed tide.

Ironically, the old and new M_2 -tide maps constructed by Bogdanov (1961 I) and Luther and Wunsch (1974 I) by pure intuition and simple rules of thumb from empirical data came closest to the present charts. Indeed, their maps display no amphidromic system in the north-central Pacific. As is verified in Schwiderski

(1979c I), the computed amphidromic points between the Cook and Society islands and near the southern edge of the Solomon Islands are both in almost identical positions with those charted by the same authors. Nevertheless, their detailed distribution of amplitudes and phases is still significantly different from the present one.

Perhaps the most spectacular display of the high quality of both the computed and the observed tidal data is brought out by Tables 7A and 7B depicting the high-amplitude tide of the central Pacific. Indeed, unlike any other open ocean area, the tabulated region is dotted with numerous tide-gauge stations at island groups and at scattered isolated islands. In addition to the fully listed island chains, there are the isolated islands: Johnston (JI), Wake (WI), Kudaie (KI), Ocean (OI), Funafuti (FI), Wallis (WI), Niue (NI), and Norfolk (NF). The corresponding observed tidal constants listed in nongeographical arrangement appeared incoherent and, hence, uncorrelated, giving rise to doubt their true value. Yet, the computed tidal wave sweeps across the whole area in a southwesterly direction with little variation of its high amplitude. As the wave crest passes through the many checkpoints with correct height and in right time, it integrates and correlates without a single exception all the empirical data into one coherent unity.

Conclusions

The quality evaluation of the constructed M_2 ocean tide model described in Parts I and II of this paper leads to the conclusion that it is now possible to compute detailed and accurate global ocean tides which fulfill the application requirements of contemporary researchers. In fact, it is estimated that the computed M_2 -tide charts permit an M_2 -tide prediction anywhere in the open oceans with an accuracy of better than 5 cm. This accuracy leaves ample room for superposable errors due to the additional smaller tidal constituents listed in Table 1 of Part I, which are presently under construction with equivalent relative accuracy. When all those partial tides become available, the total tide-prediction error is expected to fall well below the 10-cm limit needed in many applications.

Naturally, the achieved high accuracy of the M_2 -tide in the open

oceans drops somewhat near continental or island stations where empirical data are missing or are less accurate themselves (see the introduction to the British Admiralty Tide Tables, 1977 I). This is particularly true near Antarctica and in the Arctic Ocean, where reliable measurements of ocean tides and depths are sparse. Also, less accurate predictions must be anticipated in small border seas, bays, estuaries, and channels where the 1° by 1° grid system precludes a sufficient resolution. To improve the present tide model in those areas, significantly improved observations will be needed along with a locally refined network and corresponding bathymetric data.

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