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HECTIC - A LORAN GRID COMPUTATION PROGRAM FOR IRREGULAR TERRAIN--ETC(U)  
FEB 80 J L HECKSCHER, E J TICHOVOLSKY

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RADC-TR-79-354

# In-House Report

## February 1980

# **HECTIC - A LORAN GRID COMPUTATION PROGRAM FOR IRREGULAR TERRAIN**

JOHN L. HECKSCHER  
ELI J. TICHOVOLSKY

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Air Force Systems Command  
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REPORT DOCUMENTATION PAGE			READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER RADC-TR-79-354	2. GOVT ACCESSION NO. AD-AG89497	3. RECIPIENT'S CATALOG NUMBER	
4. SPONSORING AND SUBMITTING ORGANIZATION HECTIC - A LORAN GRID COMPUTATION PROGRAM FOR IRREGULAR TERRAIN		5. TYPE OF REPORT & PERIOD COVERED In-house	
6. AUTHOR/PERFORMING ORGANIZATION John L. Heckscher Eli J. Tichovolsky		7. CONTRACT OR GRANT NUMBER 17100	
8. PERFORMING ORGANIZATION NAME AND ADDRESS Deputy for Electronic Technology (RADC/EEP) Hanscom AFB Massachusetts 01731		9. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 64728F 450A/0001	
10. CONTROLLING OFFICE NAME AND ADDRESS Deputy for Electronic Technology (RADC/EEP) Hanscom AFB Massachusetts 01731		11. REPORT DATE Feb 1980	
12. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Deputy for Surveillance & Nav Sys (ESD/OCND) Hanscom AFB Massachusetts 01731		13. NUMBER OF PAGES 50	
14. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		15. SECURITY CLASS. (of this report) Unclassified	
16. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) Arcon Corp.		17. DECLASSIFICATION/DOWNGRADING SCHEDULE	
18. KEY WORDS (Continue on reverse side if necessary and identify by block number) LORAN grid prediction Huffman's integral equation Propagation over irregular ground LI navigation			
19. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides documentation for the computer program HECTIC which calculates LORAN time-difference coordinates over rough terrain. Basic equations are given and the various terms are defined. The program system flow is outlined, and a User's Guide describes the input card, database tape, and printed output formats. A complete listing of the program is given.			

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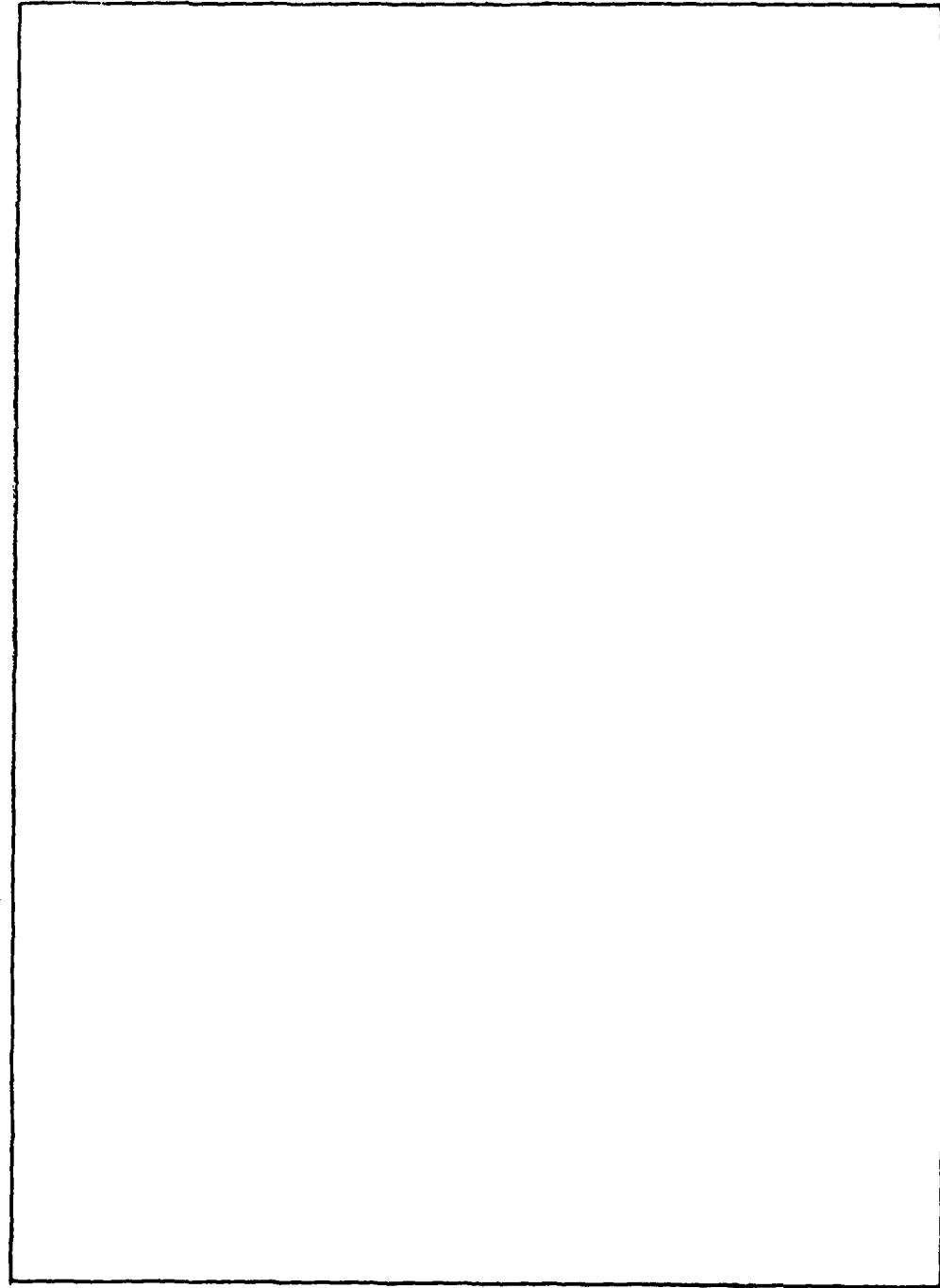
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Preface

The encouragement and support of Dr. E.A. Lewis and the assistance and advice of Mr. W.R. Rustenburg (ESD/OCND) are gratefully acknowledged.

This work was funded in part by the Tactical LORAN System Project Office.

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## HECTIC—A LORAN Grid Computation Program for Irregular Terrain

### 1. INTRODUCTION

Program HECTIC is a software system for computing time-difference coordinates (TD1 and TD2) produced at specified geographic coordinates by a low frequency LORAN triad. The program, an updated version of HUFLOC,<sup>1</sup> utilizes algorithms originally developed by Johler and Berry<sup>2</sup> and later implemented by Horowitz in LORANCO<sup>3</sup> to compute secondary phase correction factors via Hufford's integral equation.<sup>4</sup> A data base is required which specifies the earth impedance and terrain elevation at points within the geographical region of interest. As implemented on a CDC 6600 computer, HECTIC incorporates the following modifications to the LORANCO system configuration:

---

(Received for publication 29 January 1980)

1. HUFLOC (1977) Computer Program from USAF, Tactical LORAN SPO, Hanscom AFB, MA 01731.
2. Johler, J. R., and Berry, L. A. (1967) Loran-D Phase Corrections Over Inhomogeneous, Irregular Terrain, ESSA Technical Report IER 59-ITS A 56, (Suptd. of Documents, U.S. Govt Printing Office, Washington, DC 20402).
3. Horowitz, S. (1977) User's Guide for ESD LORAN Grid Prediction Program, RADC-TR-77-407.
4. Hufford, G. A. (1952) An integral equation approach to the problem of wave propagation over an irregular surface, Quart. Appl. Math. 9(No. 4):391.

- (1) Output has been limited to data necessary for comparing time-difference predictions with measurements,
- (2) New error messages and error recoveries have been added,
- (3) Database handler code no longer is hard-wired for a specific geographic area,
- (4) Targets below the earth's surface are rejected,
- (5) The input card stream was revised, and
- (6) The use of blank and labelled COMMON was made more economical.

## 2. COMPUTER CODE

### 2.1 Time-of-arrival Function TOA

LORAN time-difference coordinates TD1 and TD2 for a prediction grid serviced by a 3-station chain are given by

$$TD1 = TOA1 - TOAM$$

$$TD2 = TOA2 - TOAM$$

where TOA1 and TOA2 and TOAM are the signal time-of-arrival for Slave 1, Slave 2, and Master stations, respectively. Time-of-arrival is determined in the main program HECTIC via

$$TOA = \frac{\eta x}{c} + \frac{10^6 \phi_c}{\omega} + ED \text{ } (\mu\text{sec})$$

where

- $\eta$  = atmospheric index of refraction at the surface ( $= 1.000338$ ),
- $x$  = geodesic distance from transmitter to target's projection onto a spheroidal earth of equatorial radius  $a_o$  and polar radius  $b_o$  (m),
- $c$  = vacuum velocity of light ( $= 2.997925 \times 10^6$  m/ $\mu$ sec),
- $\omega$  = radian frequency ( $= 2\pi f = 2\pi \times 10^5$  Hz),
- ED = emission delay ( $\mu$ sec),

and

$$\begin{aligned} \phi_c &= \text{secondary phase correction factor,} \\ &= -\arg(FW) + k(r_o - x), \end{aligned}$$

where

$F$  = induction field function  $FZ$  or  $FH$ ,  
 $W$  = secondary wave attenuation factor,  
 $k$  = wave number in air ( $\omega\eta/c m^{-1}$ ),

and

$r_o$  = chordal distance (m) from transmitter to target's projection onto a spherical earth of effective radius  $a/\alpha$  where  $a = 6,36739 \times 10^6$  (m)  
and  $\alpha$  is the atmospheric vertical lapse factor.

## 2.2 Induction Field Function F

The induction field is formulated in subroutine INDF as either

$$FZ = \frac{a a_r \sin^2 \theta}{D^2} + \left[ \frac{1}{ikD} + \left( \frac{1}{ikD} \right)^2 \right] \left[ \frac{3a a_r \sin^2 \theta}{D^2} - 2 \cos \theta \right]$$

or

$$FH = \frac{a_r \sin \theta}{Z_o D} \left[ 1 + \frac{1}{ikD} \right]$$

where

$a_r$  =  $a + h_r$ ,  
 $h_r$  = target altitude (m),  
 $D^2$  =  $a_r^2 + a^2 - 2aa_r \cos \theta$ ,  
 $\theta$  =  $x/a$ ,  
 $i$  =  $\sqrt{-1}$ , and  
 $Z_o$  =  $\sqrt{\mu_o/\epsilon_o} \approx 377 \Omega$ .

$FZ$  is used when the phase of the vertical electric field is to be found, and  $FH$  is used when the phase of the azimuthal magnetic field is required.

\* Although  $x$  is the geodesic distance on a spheroidal earth,  $\theta$  is calculated as if  $x$  were the distance on a spherical earth.

### 2.3 Secondary Wave Attenuation Function W, Surface Case

When the target is on the earth's surface, the quantity W is calculated in subroutine INFQ2F from the following integral equation:

$$W(x) = 1 - e^{i\pi/4} \sqrt{\frac{k}{2\pi}} \frac{r_o}{x} \int_0^x ds \cdot W(s) \sqrt{\frac{x}{s(x-s)}} \\ \cdot \left\{ \delta_s \left[ 1 + \left( \frac{\partial h_s}{\partial s} \right)^2 \right]^{-1/2} + \left[ 1 + \frac{1}{ik r_2} \right] \frac{\partial r_2}{\partial n} \right\} \\ \cdot \frac{s(x-s)}{r_1 r_2} \frac{r_o}{x} \left[ 1 + \left( \frac{\partial h_s}{\partial s} \right)^2 \right]^{1/2} e^{-ikr}$$

where

- $s$  = distance along the transmitter-to-target geodesic ( $0 \leq s \leq x$ ),
- $\delta_s$  = normalized impedance at point  $s$ ,  
 $= (k/k_2) (1 - k^2/k_2^2)^{1/2}$ ,
- $k/k_2 = (\epsilon_2 - i\sigma/\omega\epsilon_0)^{-1/2}$ ,
- $\epsilon_2$  = relative dielectric constant,
- $\epsilon_0 = 8.854 \times 10^{-12}$  F/m,
- $\sigma$  = conductivity (mho/m),
- $\frac{\partial h_s}{\partial s}$  = terrain slope at  $s$ ,
- $r = r_1 + r_2 - r_o'$ ,
- $r_1^2 = a_s^2 + a^2 - 2a a_s \cos(s/a)$ ,
- $a_s = a + h_s$ ,
- $h_s$  = terrain elevation at point  $s$  relative to terrain elevation  
at the transmitter,
- $r_2^2 = a_x^2 + a_s^2 - 2a_x a_s \cos(\frac{x-s}{a})$ ,
- $a_x = a + h_x$ ,
- $h_x$  = terrain elevation at point  $x$  relative to terrain elevation  
at the transmitter,
- $r_o^2 = a_x^2 + a^2 - 2a_x a \cos(\frac{x}{a})$ ,

$\frac{\partial r_2}{\partial n}$  = normal derivative of  $r_2$  with respect to the earth's surface,

$$= \frac{1}{r_2} \left[ 1 + \left( \frac{a}{a_s} \frac{\partial h_s}{\partial s} \right)^2 \right]^{-1/2} \left[ a_s - a_x \cos\left(\frac{x-s}{a}\right) - a \frac{\partial h_s}{\partial s} \frac{a}{a_s} \sin\left(\frac{x-s}{a}\right) \right].$$

#### 2.4 Secondary Wave Attenuation Function W, Elevated Case

If the target is above the earth's surface, then subroutine INEQ2E also calculates

$$\begin{aligned} W = & \frac{1}{2} - \frac{e^{i\pi/4}}{2} \sqrt{\frac{k}{2\pi}} \frac{r_o}{x} \int_0^x ds \cdot W(s) \sqrt{\frac{x}{s(x-s)}} \\ & \cdot \left\{ \delta_s \left[ 1 + \left( \frac{\partial h_s}{\partial s} \right)^2 \right]^{-1/2} + \left[ 1 + \frac{1}{ikr_2} \right] \frac{\partial r_2}{\partial n} \right\} \\ & \cdot \frac{s(x-s)}{r_1 r_2} \frac{r_o}{x} \left[ 1 + \left( \frac{\partial h_s}{\partial s} \right)^2 \right]^{1/2} e^{-ikr} \end{aligned}$$

where  $W(s)$  is the previously obtained surface function  $W(x)$ , and the quantity  $a_x$  which enters into calculating  $r_1$ ,  $r_2$ ,  $r_o$ ,  $r$  and  $\partial r_2/\partial n$  is replaced by  $a_r = a + h_r$ , where  $h_r$  is the target altitude relative to terrain elevation at the transmitter.

### 3. SYSTEM DESIGN

Program HECTIC is divided into 3 modules: Driver, Database, Handler and Secondary Phase Calculator.

#### 3.1 Driver Module

The Driver routine HECTIC reads data from input cards, checks their validity and converts them from user to internal format via routines CORDMS and CORRAD. It sets up the three geodesic propagation paths from the stations to each target via routines GEODI and GEOPTS. It retrieves impedance and terrain data from the database via the Database Handler routine GEORET. It also calls the Secondary Phase Calculator routine INEQ2E and prints the final results for TD1 and TD2.

### 3.2 Database Handler Module

The Database Handler routine GEORET reads the database tape and transfers the impedance and terrain data to mass storage via routine GETELV. It also retrieves these data from mass storage via routines GETELV, INDEX, INT, and UNPACK.

### 3.3 Secondary Phase Calculator Module

The secondary Phase Calculator routine INEQ2E performs initial flat-earth calculations via routines FLEAF and WERF. It interpolates the impedance and terrain data via routines CNEVKEN, GROUND, INT, and OMCOS. Then it evaluates Hufford's integral equation and computes the secondary phase via routine CANG and INDF. These operations are diagrammed in the System Flow Chart in Figure 1.

## 4. USER'S GUIDE

Program HECTIC reads input cards and a database tape. It produces printer output. These data sets are described below.

### 4.1 Input Cards

The input file consists of Control, Map, Station, and Target cards. Figure 2 shows a sample input card sequence.

#### 4.1.1 CONTROL CARDS

Cards numbered 1 through 11 in Table 1 are program control cards. These cards specify  $f$ ,  $\eta$ ,  $a$ ,  $a_o$ ,  $b_o$ ,  $c$  and  $\alpha$  which were defined in Section 2. In addition, the flat-earth distance  $F_e$  ( $\sim 1000$  m) specifies how far along the path, flat earth theory is to be used to initialize  $W(s)$  before round earth code begins. There are also two control switches: one selects either the electric field or the magnetic field; the other allows the selection of either a rough or a smooth, inhomogeneous earth model. (In the smooth model terrain variations are ignored.)

#### 4.1.2 MAP CARDS

The database tape format does not include geographic coordinates because HECTIC automatically keys location to data via the database sequence structure (to be described in Section 4.2). In order to implement this keying operation, the user supplies the location of the first data point via Card 12, and the location 30" east and 30" north of the last data point via Card 13. These locations are referred to as the southwest and northeast map corners, respectively. The input

card format for all geographic positions is ddd-mm-ss.sss A, where ddd = 0 to 90° latitude, or 0 to 180° longitude, mm = 0 to 59 min, ss.sss = 00.000 to 59.999 sec, and A = N, S, F or W. The map corners must lie on integral latitude and longitude lines:

dd-00-00.000 N or S

ddd-00-00.000 F or W

with the following restrictions: (1) the northeast corner cannot lie north of 89°N, (2) the southwest corner cannot lie south of 89°S, (3) the map cannot straddle the 180° meridian, and (4) the minimum map region is a zone 1° latitude by 2° longitude, with larger map regions being multiples of this basic zone.

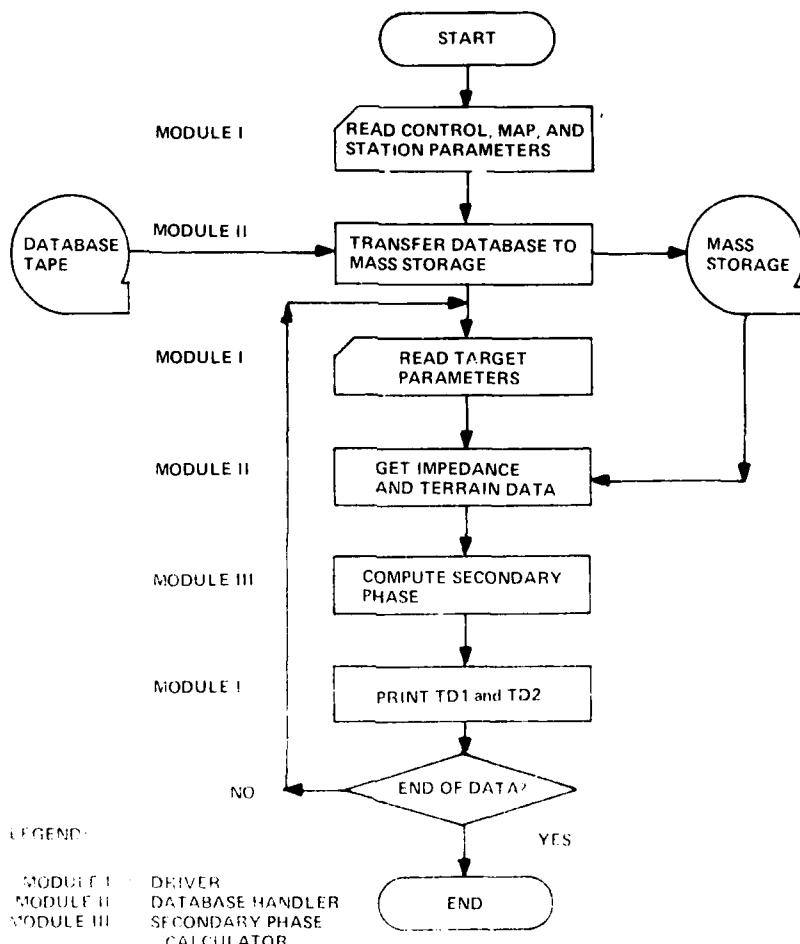


Figure 1. System Flow Chart

1 100. \*FREQUENCY (kHz)  
 2 1.000332 \*INDEX OF REFRACTION OF AIR AT GROUND LEVEL  
 3 6347390. \*SPHERICAL EARTH RADIUS (m)  
 4 6378393. \*SPHEROIDAL EARTH EQUATORIAL RADIUS (m)  
 5 6356911.4 \*SPHEROIDAL EARTH POLAR RADIUS (m)  
 9 .2997927 \*VACUUM SPEED OF LIGHT (km/sec)  
 11 1000. \*FLAT EARTH TEST FACTOR  
 12 .85 \*TRUE RADIUS/EFFECTIVE RADIUS  
 14 1. \*EARTH=FLAT EARTH; 0.75=SPHERICAL EARTH  
 15 0. \*UNITS=SPHERICAL EARTH; 0.75=SPHEROIDAL EARTH.  
 \*CONTOL CARDS TERMINATOR, NAME, STATION, AND TARGET CARDS FOLLOW.  
 MAP S.W. 48 00 00.0001 8 60 00.0001  
 MAP N.E. 54 00 00.0001 14 00 00.0001  
 MASTER 45 36 18.513M 67 19 38.276E  
 SLAVE 1 53 34 13.867M 62 43 46.508E 12537.42  
 SLAVE 2 48 15 48.629M 11 37 44.683E 26164.17  
 TARGET 1 45 44 27.515E 9 2 47.637E 3048.00 10.  
 TARGET 2 45 44 52.655E 9 14 11.627E 3048.00 10.  
 TARGET 3 45 44 23.145E 9 15 25.644E 3048.00 10.  
 TARGET 4 45 39 55.61E 9 28 46.354E 3048.00 10.  
 TARGET 5 44 37 33.185E 9 24 54.484E 3048.00 10.  
 TARGET 6 45 33 34.426E 9 42 7.003E 10.  
 TARGET 7 45 33 8.671E 9 43 24.354E 10.  
 TARGET 8 45 24 17.613E 9 53 1.484E 10.  
 TARGET 9 45 28 50.694E 9 64 4.948E 10.  
 TARGET 10 45 25 6.593E 9 2 22.280E 10.  
 TERMINATOR

Figure 2. Sample Input Card Images

Table 1. Input Card Formats

Card Number	Card Column(s)	Read Format	Data Entry
1	5 6-16	I5 E10.0	1 Loran transmission frequency f (kHz)
2	5 6-16	I5 E10.0	2 Air index of refraction at ground $\eta$
3	5 6-16	I5 E10.0	3 Spherical earth radius a (m)
4	5 6-16	I5 E10.0	4 Spheroidal earth equatorial radius $a_o$ (m)
5	5 6-16	I5 E10.0	5 Spheroidal earth polar radius $b_o$ (m)
6	5 6-16	I5 E10.0	9 Vacuum speed of light c (km/ $\mu$ sec)
7	4-5 6-16	I5 E10.0	11 Flat-earth distance $F_e$ (m)
8	4-5 6-16	I5 E10.0	12 Vertical lapse factor $\alpha$
9	4-5 6-16	I5 E10.0	14 1.0 for electric field prediction; 0.0 for magnetic field prediction.

Table 1. Input Card Formats (Cont)

Card Number	Card Column(s)	Read Format	Data Entry
10	4-5 6-16	I5 F10.0	15 0.0 for data base rough earth terrain; 1.0 for smooth earth.
11	1-5		Blank. Terminates Control Card stream.
12	2-12 13-17 18-20 21-27 28 29-33 34-36 37-43 44	A10 I5 I3 F7.3 A1 I5 I3 F7.3 A1	MAP SW. Map SW corner latitude degrees. Map SW corner latitude minutes. Map SW corner latitude seconds. Map SW corner hemisphere, N or S. Map SW corner longitude degrees. Map SW corner longitude minutes. Map SW corner longitude seconds. Map SW corner hemisphere, E or W.
13	2-12 13-44	A10	MAP NE. Map NE corner. Use the formats of Card 12.
14	2-12 13-44	A10	MASTER. Master Station position. Use the formats of Card 12.
15	2-12 13-44 45-53	A10 F9.2	SLAVE 1. Slave 1 position. Use the formats of Card 12. Slave 1 emission delay ( $\mu$ sec).
16	2-12 13-44 45-53	A10 F9.2	SLAVE 2. Slave 2 position. Use the formats of Card 12. Slave 2 emission delay ( $\mu$ sec)
17	2-12 13-44 45-53 54-62 63-71 72-80	A10 F9.2 F9.2 F9.2 F9.2	Target identifier. Target position. Use the formats of Card 12. Target altitude $h_r$ (m) Hufford's integral equation path increment $\Delta s$ (m) Measured TD1 ( $\mu$ sec) Measured TD2 ( $\mu$ sec)
18, etc.	2-80		Next Target Cards. Use formats of Card 17.
LAST CARD	54-62		Blank. Terminates the Input Card Stream.

## 4.1.3 STATION CARDS

Cards 14, 15, and 16 specify the positions of the Master, Slave 1, and Slave 2, respectively. Cards 15 and 16 also contain the emission delays for the Slaves.

## 4.1.4 TARGET CARDS

Card 17 contains target identifier, position, altitude  $h_r$ , integration path increment size  $\Delta s$ , and measured TD1 and TD2. The latter pair may be omitted.

Any number of additional targets may be specified, one to a card. Any target card with  $\Delta \leq 0$  will prematurely stop the program. To properly end the program, a blank card should be inserted after the last target card.

#### 4.2 Database Tape

Program HECTIC reads terrain elevation, impedance amplitude, and impedance phase from the database tape. The tape contains one such "data triad" for every 30 sec of latitude and longitude. Each triad is packed into 30 bits, and since the word size available on a CDC 6600 computer is 60 bits, two data triads fit into each 60-bit word. The right half-word always contains data for the geographic point 30-sec north of the point in the left half-word, as indicated in Table 2.

One database record contains sixty 60-bit words, for a total of 120 data triads. A record thus spans 1° of latitude from south to north, as shown in Figure 3(a). Two-hundred-forty such records fill a database zone which spans 2° of longitude from west to east in 30-sec steps.

The database tape must contain enough zones to completely cover the region specified via the map corner coordinates. An example of the ordering of zones on the database tape is diagrammed in Figure 3(b). Data pertinent to zone 1 appears in records 1 through 240, to zone 2 in records 241 through 480, and so on.

Table 2. Database Word Packing

Half	Bit Numbers	Data Description	Least Significant Bit
Left	59-49	Terrain Elevation	8 m
	48-41	Impedance Amplitude	0.001 Ω
	40-30	Impedance Phase	0.001 rad
Right	29-19 18-11 10-0	(Repeat above sequence for geographic point 30 sec north)	(as above)

#### 4.3 Printed Output

The printed output consists of Normal Output and Error Messages. Normal Output includes Control, Map, and Station parameters, TD1 and TD2 predictions, and the End Message. Figure 4 shows a sample normal output listing. Error messages may appear in this listing in the event of either fatal or nonfatal errors.

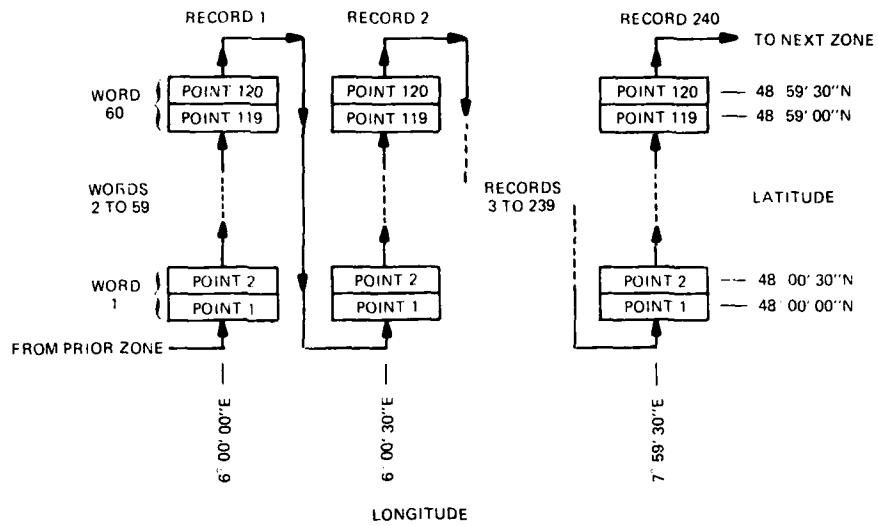


Figure 3(a). Sample Database Zone Structure, Showing Ordered Sequence of Database Words and Corresponding Geographic Coordinates

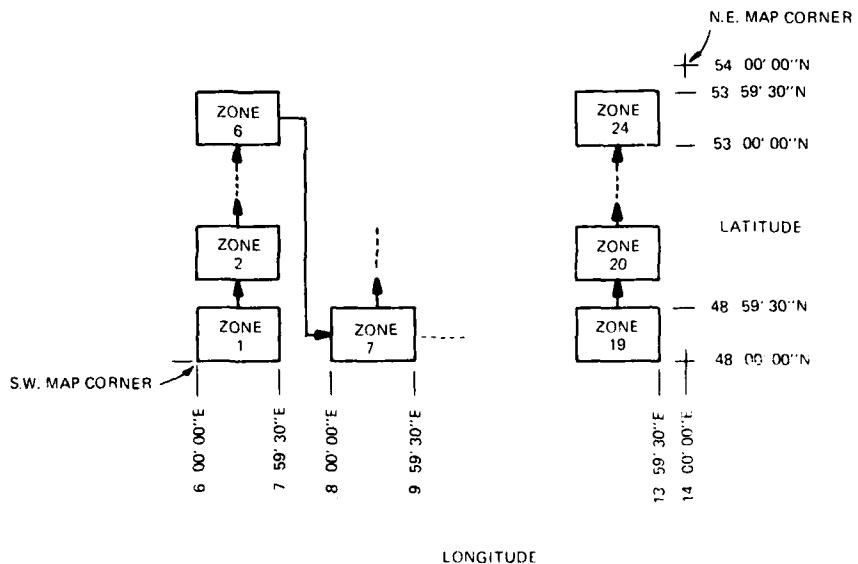


Figure 3(b). Sample Map Structure, Showing Ordered Sequence of Zones and Corresponding Geographic Coordinates. The coordinates of the southwest and northeast map corners determine the number of zones in each direction

- - - - - NAME - CHANNELS - - - -  
IDENTIFIER LATENT CLOUDS  
HIGHLIGHTED (CHROMATOGRAPH)

Model	Mean	SD	Mean	SD	Mean	SD
MAP- $\pi_{\text{MAP}}$	1.0	0.00000000	0.0	0.0	0.0	0.0
MAP- $\pi_{\text{MAP}}$	1.0	0.00000000	0.0	0.0	0.0	0.0

ESTATE PLANNING - TAXES - INVESTMENTS  
FINANCIAL PLANNING - RETIREMENT PLANNING - ESTATE PLANNING  
(PENSION PLANNING) - INVESTMENT PLANNING - (STC)

MASTER	44 34 14.6419	7 17 36.6717	-1.60
SLAVE 1	53 34 13.6671	+3 46.5401	127.17+00
SLAVE 2	44 13 49.4644	11 17 44.2836	26144.17

(a)

IDENTIFIER	LEAPDAY TIME DIFFERENCE PREDICTION										COMPUTER (USFC)	ERROR (USEC)
	LATITUDE	LONGITUDE	ALTITUDE	STEP SIZE	MEASURED (USEC)	T01	T02	T03	T04	T05		
(DEG-MIN-SEC)	(DEC-MIN-SEC)	(MFT-KM)	(KM)									
TARGET 1	49 44 57.54N	6 20 47.637	3040.00	10.00	0.00	6.00	13540.49	26599.87	13540.49	26599.87		
TARGET 2	49 44 52.60N	6 14 11.27E	1046.00	10.00	0.00	0.00	13540.47	26504.72	13530.47	26504.72		
TARGET 3	49 44 23.14N	6 15 25.14E	3046.00	10.00	0.00	0.00	13529.23	26494.36	13529.23	26494.36		
TARGET 4	49 39 55.55N	6 28 46.35E	3040.00	10.00	0.00	0.00	13515.71	26380.66	13515.71	26380.66		
TARGET 5	49 39 13.14N	6 29 54.48E	3048.00	10.00	0.00	0.00	13514.57	26370.93	13514.57	26370.93		
TARGET 6	49 33 34.42N	6 42 7.80E	0.00	10.00	0.00	0.00	13501.30	26264.93	13501.30	26264.93		
TARGET 7	49 33 8.62N	6 43 24.56E	0.00	10.00	0.00	0.00	13499.43	26253.69	13499.43	26253.69		
TARGET 8	49 27 17.21N	6 43 1.49E	0.00	10.00	0.00	0.00	13499.05	26169.26	13499.05	26169.26		
TARGET 9	49 27 50.89N	6 44 4.95E	0.00	10.00	0.00	0.00	13488.00	26159.87	13488.00	26159.87		
TARGET 10	49 26 4.63N	6 47 22.28E	0.00	10.00	0.00	0.00	13488.19	26151.16	13488.19	26151.16		
TERMINATOR	0 0 0.000	0 0 0.000	0.00	0.00	0.00	0.00						

### FNC OF INPUT DATA.

(b)

Figure 4. Sample Normal Output, (a) Control, map, and station parameters corresponding to input sequence of Figure 2. (b) LORAN time-difference predictions for target cards of Figure 2

#### 4. 3. 1 CONTROL PARAMETERS

The control parameters are  $f$ ,  $\eta$ ,  $a$ ,  $a_o$ ,  $b_o$ ,  $c$ ,  $F_e$ ,  $\alpha$ , electric/magnetic field control switch, and rough/smooth earth switch. These were defined in Sections 2 and 3. Also included in this listing are the calculated quantities  $k$  (wavenumber),  $a/\alpha$  (effective earth radius), and the spheroidal flattening

$$f_c = 1 - a_0/b_0$$

and the first spheroidal eccentricity squared

$$e^2 = 1 - a_0^2/b_0^2.$$

#### 4.3.2 MAP PARAMETERS

The Map parameters are the southwest and northeast map corners defined in Section 4.1.2.

#### 4.3.3 STATIONS PARAMETERS

The station parameters are the positions and emissions delays of the Master, Slave 1, and Slave transmitters defined in Section 5.1.3.

#### 4.3.4 TD1 AND TD2 PREDICTIONS

For each target there is one printed line which includes identifier, latitude, longitude, altitude, numerical integration step size, and measured TD1 and TD2 defined in Section 5.1.4. Also included are the computed TD1 and TD2 and the time delay errors (*computed minus measured*) in microseconds.

#### 4.3.5 END MESSAGE

The message "End of Input Data" indicates normal run completion.

#### 4.3.6 ERROR MESSAGES

A fatal error is one from which there is no reasonable recovery. Hence, the program must abort. The user merely corrects the fault described below and re-runs the program. On the other hand, for a nonfatal error the code either takes remedial action or it abandons the current target and advances to the next one. Error messages are grouped below under the routine which generates them. The message number refers to the FORTRAN statement number of the message.

##### 4.3.6.1 Program HECTIC Error Messages

###### Message 9900 (Fatal)

"...Station lies outside map area. Run aborts." Fault: Input station coordinates exceeded the boundaries specified on the map input cords. All three transmitters must lie within the map region.

###### Message 9910 (Fatal)

"Error in data for ... coordinates. Run ends." Fault: Map or station coordinates on input card were not correct. Either the specified latitude degrees exceeded 90, longitude degrees exceed 180, minutes exceeded 59, seconds exceeded 59.999, latitude symbol was neither N nor S, or longitude symbol was neither E nor W.

###### Message 9912 (Nonfatal)

"Error in end-point coordinate. Calculations for this path have been deleted." Fault: Target coordinates on input card were not correct. For diagnosis, see

message 9910 above. Action: The program advances to the next target.

Message 9916 (Nonfatal)

"Error detected during conversion of coordinate for point—from radians to (alphabetic) degrees-minutes-seconds." Fault: A point on a station-to-target path was not correct. Either latitude exceeded 324000.0005 seconds, or longitude exceeded 648000.0005 seconds. Action: The program advances to the next target.

Message 9922 (Nonfatal)

"Target lies outside map area. Get next target." Fault: Input target coordinate exceeded the boundaries specified on the map input cards. Action: The program advances to the next target.

4.3.6.2 Subroutine GEOPTS Error Messages

Message 9800 (Fatal)

"Subroutine GEOPTS called with end-point latitude out of acceptable range  $(-\pi/2, \pi/2)$ . Latitude of A = ... radians, latitude of B = ... radians. Program execution terminated." Fault: GEOPTS encountered a bad latitude.

Message 9802 (Fatal)

"Subroutine GEOPTS called with end-point longitude out of acceptable range  $(-2\pi, +2\pi)$ . Longitude of A = ... radians, longitude of B = ... radians. Program execution terminated." Fault: GEOPTS encountered a bad longitude.

Message 9803 (Fatal)

"Geodesic path includes a geographic pole—subroutine GEOPTS cannot handle this case."

4.3.6.3 Subroutine GETELV Error Messages

Message 9700 (Fatal)

"Database has nnn records. Increase array MSINDEX and variable INDDIM to accommodate. Run Aborts." Fault: Subroutine GETELV computed the number of records which the database tape must contain in order to be compatible with the specified map region. This number exceeded the number of mass-storage record pointer locations available. Consequently, the database could not be loaded. Remedy: the user should increase the size of array MSINDEX to nnn + 1 and reset the value of INDDIM to nnn + 1. Array MSINDEX is in blank common and INDDIM is in a data statement in routine GETELV.

Message 9701 (Nonfatal)

"Lat, lon requested are outside map region - no elevation returned." Fault: The program automatically increments any given path by two stepsizes beyond the target location. Consequently, the path for a target that initially was within the map region ended up crossing a map boundary. Action: The program proceeds, but the results for this target are questionable. The user may try a smaller step size for this target.

Message 9702 (Nonfatal)

"Index requested exceeds scanlines generated, thus previous elevation will be used." Fault: The record pointer returned by subroutine INDEX to GETELV exceeded the number of records on the database tape. Action: The program proceeds, but the results for this target are questionable.

4.3.6.4 Subroutine CNEVKEN Error Messages

Message 9602 (Fatal)

"There are not enough points in the given array." Fault: CNEVKEN tried to interpolate a function which was defined over an insufficient range of values.

Message 9600 (Fatal)

"The X values are not arranged in ascending order.

I = . . . , X(I) = . . . , J = . . . , A(J) = . . .

X	F(X)
.	.
.	.
.	.

Fault: CNEVKEN interpolates the function F(X) over array X from a given function F(A) over array A. Both X and A must be in ascending order. The X array was not in order.

4.3.6.5 Subroutine INDF Error Messages

Message 9500 (Fatal)

"In INDF, distance is zero or negative, XX = . . ." Fault: INDF tried to calculate the induction field for a meaningless distance stored in variable XX.

### 5. PROGRAM LISTING

```
*MODULE 1. 4/22/80
*DECK HECTIC
    PROGRAM HECTIC(INPUT=128,OUTPUT=128,TAPE13=1CR,TAPE2=128)
C INSTRUCTIONS FOR USE:-----
C ATTACH,IN,INPUTCARDS, ID=TICHO,MR=1.
C ATTACH,HECTIC, ID=TICHO,MR=1.
C FTM,I=HECTIC,EL=F,OPT=1,L=0.
C VSN,TAPE13=CC3626.
C LABEL,TAPE13,R=NORING,L=DATABASE.
C LGO,IN.
C END OF INSTRUCTIONS.
C PROGRAM DESCRIPTION:-----
C MODULE 1 READS INPUT CARDS, CALL MODULES 2 AND 3, AND PRINTS
C FINAL RESULTS.
C ROUTINES: CORDMS,CORRAD,GEODI,HECTIC.
C MODULE 2 GETS ALTITUDES AND IMPEDANCES FOR A STATION-TO-TARGET
C PATH. READS DATABASE TAPE IN FIRST PASS ONLY.
C ROUTINES: GEOPTS,PCOORD,GEORET,GETELV,INDEX,INT,UNPACK.
C MODULE 3 COMPUTES THE SECONDARY PHASE FACTOR.
C ROUTINES: CANG,CNEVKEN,GEOM,GROUND,FLEAF,INDF,INEQZ,E,
C OMFCOS,WERF.
C FILES USED:-----
C INPUT - FOR INPUT CARDS.
C OUTPUT - FOR RUN STATUS, ERROR MESSAGES AND DEBUGGING.
C TAPE2 - FOR MASS STORAGE.
C TAPE13 - FOR DATABASE INPUT TAPE.
C REVISED BY:-----
C ELI TICHOVOLSKY, ARCON CORP., WALTHAM, MA., 4/22/80.
C ORIGINAL BY:-----
C J. R. JOHLER, ET. AL.
C ENTRY POINTS:-----
C PCOORD IS IN GEOPTS, GEOM IS IN GROUND.
C -----
DIMENSION TPW(3),ED(2),TD(2),IDENTF(4),TDMEAS(2),TDERP(2),TOA(3)
DIMENSION LDUM(3,4),ADUM(3,4),RLA(3),RL0(3),LATA(3),LONA(3)
COMMON /ZOTA/ARRAY(15)
COMMON /PIS/TWOP1,PI,HAFPI,QRTP1
COMMON /MAP/LATSW,LATNE,LONSW,LONNE
COMMON /PATH/RLATA,RLONA,RLATB,RLONR,RAZA,RAZB,SBM
COMMON /CITCT/ITCT,LTOP,NPTCT,ZXMTR,ZMIN,ALT SW(3),TSW(3)
COMMON LAT(999),LON(999),MSINDEX(5800)
EQUIVALENCE (ARRAY(2),ETA),(ARRAY(11),FLAT)
EQUIVALENCE (ARRAY(12),ALPHA),(ARRAY(14),EORH),(ARRAY(15),SMOOTH)
EQUIVALENCE (ARRAY(1),FKHZ),(ARRAY(13),RAD),(ARRAY(3),SPHRAD)
EQUIVALENCE (ARRAY(4),A0),(ARRAY(5),B0),(ARRAY(9),C)
EQUIVALENCE (ARRAY(6),FL),(ARRAY(7),ESQ),(ARRAY(10),WAVE)
C SEMI-MAJOR AND SEMI-MINOR AXES (METER) OF THE INTERNATIONAL SPHEROID.
DATA A0,B0,SPHRAD/6378388.0, 6356911.9461, 6367390./
DATA LINE,ITCT,PI/50, 1, 3.1415926535898/
DATA FKHZ=ETA,C/100.,1.000338,.2997925/
DATA FLAT,ALPHA,EORH,SMOOTH/1000.,.85,1.,0./
DATA WEST,SOUTH,LWEST,LSOUTH/1HW,1HS,1HW,1HS/
TWOP1=2.*PI SHAFPI=PI/2. $ORTPI=PI/4.
C -----
C READ PROCESSING CONTROLS.
I=0
?0  READ 9919,I,AVALUE $IF (I .LE. 0) GO TO 21
```

```

      APARRAY(I)=AVALUE FOR TO 20
C1      CONTINUE
C RAD=EFFEFFECTIVE EARTH RADIUS. WAVE=AVENUMBER IN AIR AT EARTH SURFACE.
      RAD = SPHRAD/ALPHA SWAVE = TWOPI*FRK7*ETAS*1.E-6/C
C FL=SPHEROIDAL FLATTENING. ESDEFIRST ECCENTRICITY SQUARED.
      FL = 1. - H0/A0 SESQ = 1. - (H0/A0)**2
      PRINT 9920, (APARRAY(I),I=1,6)
      PRINT 9921, (APARRAY(I)*I=7,15)
      PRINT 9925
C READ MAP CORNERS.
      DO 911 I=1,2
      READ 9909,IDENTF(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),
     1           LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4)
      PRINT 9909,IDENTF(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),
     1           LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4)
      MIS=0
      CALL CORRAD(RLA(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),0,MIS)
      CALL CORRAD(RLO(I),LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4),1,MIS)
      IF (MIS .EQ. 0) GO TO 911
C IF MAP COORDINATES ARE BAD, ABORT.
      PRINT 9910, IDENTF(I) $STOP
911      CONTINUE
      LATSW=LDUM(1+1)*10000+LDUM(1+2)*100+IFIX(ADUM(1+1))
      IF (ADUM(1+2) .EQ. 0, SOUTH) LATSW=-LATSW
      LONSW=LDUM(1+3)*10000+LDUM(1+4)*100+IFIX(ADUM(1+3))
      IF (ADUM(1+4) .EQ. 0, WFST) LONSW=-LONSW
      LATNE=LDUM(2+1)*10000+LDUM(2+2)*100+IFIX(ADUM(2+1))
      IF (ADUM(2+2) .EQ. 0, SOUTH) LATNE=-LATNE
      LONNE=LDUM(2+3)*10000+LDUM(2+4)*100+IFIX(ADUM(2+3))
      IF (ADUM(2+4) .EQ. 0, WEST) LONNE=-LONNE
C READ TRANSMITTER COORDINATES FOR MASTER, SLAVE1, AND SLAVE2.
      PRINT 9926
      DO 950 I=1,3
      READ 9909,IDENTF(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),
     1           LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4),DATUM
      PRINT 9909,IDENTF(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),
     1           LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4),DATUM
      IF (I .GE. 2) FD(I-1) = DATUM
      MIS = 0
      CALL CORRAD(RLO(I),LDUM(I+3),LDUM(I+4),ADUM(I+3),ADUM(I+4),1,MIS)
      CALL CORRAD(RLA(I),LDUM(I+1),LDUM(I+2),ADUM(I+1),ADUM(I+2),0,MIS)
      IF (MIS .EQ. 0) GO TO 940
C IF STATION COORDINATES ARE BAD, ABORT.
      PRINT 9910, IDENTF(I) $STOP
940      LATA(I)=LDUM(I+1)*10000+LDUM(I+2)*100+IFIX(ADUM(I+1))
      IF (ADUM(I+2) .EQ. 0, SOUTH) LATA(I)=-LATA(I)
      LONA(I)=LDUM(I+3)*10000+LDUM(I+4)*100+IFIX(ADUM(I+3))
      IF (ADUM(I+4) .EQ. 0, WEST) LONA(I)=-LONA(I)
      IF (LATA(I).GE.LATSW .AND. LONA(I).LT.LATNE .AND.
     1       LONA(I).GE.LONSW .AND. LONA(I).LT.LONNE) GO TO 950
C IF STATION LIES OUTSIDE MAP AREA, ABORT.
      PRINT 9900,IDENTF(I) $STOP
950      CONTINUE
C-----C START LOOP ON TARGETS.
      S CONTINUE
      IF (LINE .LT. 50) GO TO 55

```

```

      PRINT 9924 $LTME=0
C READ TARGET COORDINATES. /MIN = AIRBORNE-TARGET ALTITUDE (M) ABOVE
C MEAN SEA LEVEL IF NON-ZERO. ADELS = PATH INCREMENT SIZE (KM).
55   READ 9904,IDENTF(4),LATDEGH,LATMINH,SECLATH,LATIDH,
     *          LONDEGH,LONMINH,SECLONH,LONIDH,ZMIN,ADELS,TDMES
     PRINT 9904,IDENTF(4),LATDEGH,LATMINH,SECLATH,LATIDH,
     1          LONDEGH,LONMINH,SECLONH,LONIDH,ZMIN,ADELS,TDMES
     LINE = LINE + 1
C STOP IF PATH INCREMENT SIZE IS ZERO OR LESS.
     IF (ADELS .LE. 0.) GO TO 10
     MIS = 0
     CALL CORRAD(RLATH,LATDEGH,LATMINH,SECLATH,LATIDH,0,MIS)
     CALL CORRAD(RLONH,LONDEGH,LONMINH,SECLONH,LONIDH,1,MIS)
     IF (MIS .NE. 0) GO TO 15
C IF TARGET COORDINATES ARE BAD, GET ANOTHER TARGET.
     PRINT 9912 $LTME=LINE+3
     GO TO 5
-----+
C START LOOP ON 3 STATION-TO-TARGET PATHS.
15 CONTINUE
     RLATA=RLA(ITCT)
     RLONA=RLO(ITCT)
     LTDP=0
     ALTSW(ITCT) = TSW(ITCT) = SHKMS = 0.
C SKIP THIS PATH IF IT IS TOO SHORT.
     IF ((AHS(RLATA-RLATH) .LE. ADELS/SPHRAD) .AND.
     1 (AHS(RLONA-RLONH) .LE. ADELS/SPHRAD)) GO TO 16
C COMPUTE SPHEROIDAL BASELINE AND FORWARD AND BACK AZIMUTHS.
     CALL GFOPTS(0.0,RLATP,RLONP,RAZP)
C COMPUTE SPHEROIDAL BASELINE AND FORWARD AND BACK AZIMUTHS.
     CALL GEODI(RLATA,RLONA,RAZAS,SHMS,RLATB,RLONB,RAZBS)
     SHKMS=SHMS*.001
     SHKM = SHM*1.0E-3
     DSM=SHKM/DSKM
     DSKM = DSM/DSKM
     DSM = DSM*1.0E-3
C SET TRANSMITTER COORDINATES AS POINT NUMBER 1.
     LAT(1)=LATA(ITCT) $LON(1)=LONA(ITCT)
C ADD 2 POINTS BEYOND RECEIVER.
     NPP2=NPTCT+2
     SPM = 0.0
C COMPUTE LATITUDES AND LONGITUDES ALONG HUFFORD'S BASELINE.
     DO 100 IP=1,NPP2
     SPM = SPM+DSM
     CALL PCOORD(SPM,RLATP,RLONP,RAZP)
     MIS = 0
     CALL CORDMS(RLATP,LATDEGP,LATMINP,SECLATP,LATIDP,0,MIS)
     CALL CORDMS(RLONP,LONDEGP,LONMINP,SECLONP,LONIDP,1,MIS)
     IF (MIS .NE. 0) GO TO 35
C IF PATH COORDINATE IS BAD, GET ANOTHER TARGET.
     PRINT 9916,IP $LINE=LINE+4
     GO TO 5
35   CONTINUE
     LAT(IP+1)=LATDEGP*10000+LATMINP*100+IFIX(SECLATP)
     IF (LATIDP .EQ. LSOUTH) LAT(IP+1)=-LAT(IP+1)
     LON(IP+1)=LONDEGP*10000+LONMINP*100+IFIX(SECLONP)
     IF (LONIDP .EQ. LWEST) LON(IP+1)=-LON(IP+1)

```

```

100 CONTINUE
C ADD 1 POINT FOR TRANSMITTER.
1P=NPTCT+3
C IF TARGET IS OUTSIDE MAP AREA. GET ANOTHER TARGET.
IF (LA(IP).GE.LATSW .AND. LAT(IP).LT.LATNE .AND.
    LON(IP).GE.LONSW .AND. LON(IP).LT.LONNE) GO TO 850
    PRINT 9922, IDENTF(4) $LINE=LINE+1 $GO TO 5
C COMPUTE ALTITUDES AND IMPEDANCES ALONG HUFFORD'S BASELINE.
850 CALL GEORET(DSKM,IP)
C ADJUST NUMBER OF POINTS FOR ROUTINE INEQ2E.
NPTCT = NPTCT + 1
C COMPUTE HUFFORD'S EQUATION.
CALL INEQ2E
16 CONTINUE
TPW(ITCT) = ETA*SBKMS/C
ITCT=ITCT+1
IF (ITCT .LT. 4) GO TO 15
C END LOOP ON 3 STATION-TO-TARGET PATHS.
C-----C
C PRINT FINAL RESULTS.
DO 9 I=1,3
IF (LTOP.EQ.0) TOA(I) = TPW(I) + TSW(I)
IF (LTOP.EQ.1) TOA(I) = TPW(I) + ALTSW(I)
9 CONTINUE
DO 710 I =1,2
TD(I) = ED(I) + TOA(I+1) - TOA(I)
710 TDERR(I) = TD(I) - TDMEAS(I)
PRINT 9923,TD,TDERR
C GET NEXT TARGET.
ITCT=1
GO TO 5
C END LOOP ON TARGETS.
C-----C
10 PRINT 9918
STOP
9900 FORMAT (* *A10* STATION LIES OUTSIDE MAP AREA. RUN ABORTS.*)
9909 FORMAT(2X,A10.2(I5,I3,F7.3,A1),4F9.2)
9910 FORMAT(*0 ERROR IN DATA FOR *A10* COORDINATES. RUN ENDS.*)
9912 FORMAT(//11X, 3H***, 9X, 24HERROR IN FNU-POINT COORDINATE. 10Y. 3F
    ***/11X,54H*** CALCULATIONS FOR THIS PATH HAVE BEEN DELETED ***)
9916 FORMAT(//2X, 62H*** ERROR DETECTED DURING CONVERSION OF COORDINAT
    ES FOR POINT. 15. 5H ***/2X, 2H**, 7X, 52HFROM RADIANS TO (ALFHAN
    ERIC) DEGREES-MINUTES-SECONDS. 7X, 3H***/2X, 3H***, 66X, 3H***/2X,
    3H***, 7X, 52HFURTHER CALCULATIONS FOR THIS PATH HAVE BEEN DELETED
    *D. 7X, 3H***)
9918 FORMAT(*0 END OF INPUT DATA.*)
9919 FORMAT(I5,E10.0)
9920 FORMAT (1H1//15(2H-)*CONTROL PARAMETERS#15(2H- )/
    1E22.14.5X*+ARRAY(1) = FKHZ = FREQUENCY (KHZ)/*
    1E22.14.5X*+ARRAY(2) = FTA = AIR INDEX OF REFRACTION AT GROUND/*
    2E22.14.5X*+ARRAY(3) = SPHRAD = SPHERICAL EARTH RADIUS (M)/*
    4E22.14.5X*+ARRAY(4) = AO = SPHEROIDAL EARTH EQUATORIAL RADIUS (M)/*
    5/E22.14.5X*+ARRAY(5) = HO = SPHEROIDAL EARTH POLAR RADIUS (M)/*
    6E22.14.5X* ARRAY(6) = FL = SPHEROIDAL FLATTENING*/
    9921 FORMAT (E22.14,X* ARRAY(7) = ESU = SPHEROIDAL FIRST ECCENTRICITY
    2 SQUARED/*
    2E22.14.5X* ARRAY(8) = NOT USED*/

```

```

4E22.14.5X*+ARRAY(9) = VACUUM SPEED OF LIGHT (KM/USEC) */
5E22.14.5X*+ARRAY(10) = WAVF = WAVENUMPER (1/M) IN AIR AT EARTH SUR
7FACE*/
6E22.14.5X*+ARRAY(11) = FLAT = FLAT EARTH FACTOR (M) */
8E22.14.5X*+ARRAY(12) = ALPHA = VERTICAL LAPSE FACTOR */
9E22.14.5X*+ARRAY(13) = EFFECTIVE EARTH RADIUS (M) */
1E22.14.5X*+ARRAY(14) = EORH = 0. FOR H-FIELD. NON-0. FOR E-FIELD */
9E22.14.5X*+ARRAY(15) = SMOOTH = 1. FOR SMOOTH EARTH. NON-1. FOR HO
UGH EARTH */
327X** ITEMS MARKED WITH * MAY BE CHANGED) VIA INPUT CARDS. */
9922 FORMAT (* *A10* TARGET LIFS OUTSIDE MAP AREA. GET NEXT TARGET.*)
9923 FORMAT (1H*,79X,4F9.2)
9924 FORMAT (1H//22(2H-)*LOWAN TIME DIFFERENCE PREDICTIONS*21(2H- )/
12X*IDENTIFIER*7X*LATITUDE*7X*LONGITUDE ALTITUDE STEPSIZE --MEASUR
2ED(USEC)--COMPUTED(USEC)--ERROR(USEC)-- */
312X,2(3X*(DEG-MIN-SEC)*),2X*(METER)*5X*(KM)*3(6X*T0)*6X*T02*)*/
9925 FORMAT (//8(2H-)*MAP PARAMETERS*H(2H- )/
12X*IDENTIFIER*7X*LATITUDE*7X*LONGITUDE */
212X,2(3X*(DEG-MIN-SEC)*) */
9926 FORMAT (//11(2H-)*STATION PARAMETERS*11(2H- )/
12X*IDENTIFIER*7X*LATITUDE*7X*LONGITUDE EMISSION DELAY*/
212X,2(3X*(DEG-MIN-SEC)*),3X*(USEC)* */
END

```

```

*DECK CORRAD
SUBROUTINE CORRAD(RCOR,IDEF,IIMIN,SEC,1D,IS,IERR)
DIMENSION IDS(4)
DATA (IDS=1H0,1HE,1HS,1HW)
ISS = IS
IF (ISS) 10,5,15
5 IF (ID.EQ.IDS(1)) GO TO 25
IF (ID.EQ.IDS(3)) GO TO 30
10 IERR = 1
RETURN
15 IF (ISS-1) 20,20,10
20 IF (ID.EQ.IDS(2)) GO TO 25
IF (ID.EQ.IDS(4)) GO TO 30
IERR = 1
RETURN
25 SIGN = 1.0
GO TO 35
30 SIGN = -1.0
35 IF (IDEF-1) 40,40,10
40 IF (IIMIN-60) 45,10,10
45 IF (SEC-60.0) 50,10,10
50 RCOR = SIGN*(FLOAT(IDEF)*(1.74532925199433E-4)+FLOAT(IIMIN)*
+ (2.90888208665722E-4)+SEC*4.84813691104536E-6)
RETURN
END

```

```

*DECK CORDMS
SUBROUTINE CORDMS(RCOP,IUEG,IMIN,HEC,IL,IS,IERH)
DIMENSION IDS(4)
DATA (IDS=1HN+1HE+1HS,1HW)
RANG = RCOP
SEC = ABS(RANG)*206264.806247096
ISS = IS
IF (ISS) 5,10,15
5 IERR = 1
RETURN
10 IF (SEC<324000.0005) 25,5,5
15 IF (ISS-1) 20,20,5
20 IF (SEC>648000.0005) 25,5,5
25 IF (RANG) 30,35,35
30 ISI = 2
GO TO 40
35 ISI = 0
40 IUEG = SEC/3600.0
IMIN = SEC/60.0-60.0*FLOAT(IUEG)
SEC = SEC-3600.0*FLOAT(IUEG)-60.0*FLOAT(IMIN)
ISEC = SEC
SEC = SEC-FLOAT(ISEC)
IF (SEC<0.9995) 60,45,45
45 SEC = 0.0
ISEC = ISEC+1
IF (ISEC-60) 60,50,50
50 ISFC = 0
IMIN = IMIN+1
IF (IMIN-60) 60,55,55
55 IMIN = 0
IUEG = IUEG+1
60 LDX = ISI+ISS+1
HEC=FLOAT(ISEC)+SEC
ID=IDS(LDX)
RETURN
END

```

```

*DECK GEODI
  SUBROUTINE GEODI(H1, AL1, AZ12, S, H2, AL2, AZ21)
C PURPOSE:
C   CALCULATES INVERSE COMPUTATION FORM (SOUDAN, 1965).
C   SOUTHERN LATITUDES AND WESTERN LONGITUDES ARE NEGATIVE.
C INPUTS:
C   H1 = GEOGRAPHIC LATITUDE (RADIANS) OF FIRST POINT.
C   AL1 = GEOGRAPHIC LONGITUDE (RADIANS) OF FIRST POINT.
C   H2 = GEOGRAPHIC LATITUDE (RADIANS) OF SECOND POINT.
C   AL2 = GEOGRAPHIC LONGITUDE (RADIANS) OF SECOND POINT.
C OUTPUTS:
C   AZ12 = FORWARD AZIMUTH (RADIANS) FROM FIRST POINT.
C   AZ21 = BACK AZIMUTH (RADIANS) FROM SECOND POINT.
C   S = GEODETIC DISTANCE (METER) BETWEEN 2 POINTS.
  COMMON /PI3/TWOP1,PI,HAFPI,ORTPI
  COMMON /ZOTA/ARRAY(15)
  MU=ARRAY(5) $FL=ARRAY(6)
  IF (ABS(H1) .GT. ORTP1) GO TO 1
  TBET1 = TAN(H1) * (1. - FL)
  HFT1 = ATAN(TBET1)
  GO TO 2
1  CHET1 = 1.0 / TAN(H1) / (1. - FL)
  BET1 = ATAN(1. / CHET1)
2  CONTINUE
  ALL1 = AL2 - AL1
  IF (AL2 - AL1 .EQ. 0.) R= 9
8  ALL2 = 0.
  GO TO 3
9  CONTINUE
  ALL2 = AL2 - AL1 - SIGN (TWOP1, AL2 - AL1)
3  IF (ABS(ALL1) .GT. ABS(ALL2)) S= 6
5  ALL = ALL2
  GO TO 7
6  ALL = ALL1
7  CONTINUE
12 IF (ABS(ALL) .EQ. 0. .OR. ABS(ALL) .EQ. PI .OR. ABS(ALL) .EQ. TWOPI) 10+11
10 ALL = ABS(ALL)
11 CONTINUE
  IF (ABS(H2) .GT. ORTP1) GO TO 16
  THFT2 = TAN(H2) * (1. - FL)
  HFT2 = ATAN(THFT2)
  GO TO 17
16 CHET2 = 1.0 / TAN(H2) / (1. - FL)
  BET2 = ATAN(1. / CHET2)
17 CONTINUE
  CHFT1 = COS(BET1)
  SHFT1 = SIN(BET1)
  CHFT2 = COS(BET2)
  SHFT2 = SIN(BET2)
  A = SHFT1 * SHFT2
  H = CHFT1 * CHFT2
  MA = SHFT2 * CHFT1
  COSL = COS(ALL)
  SINL = SIN(ALL)
  CHMI = A + H * COSL
  SPHI = SQRT ((SINL * CHFT2)**2 + (MA - A + * COSL)**2)

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20 IF (SPHI .GE. 0. .AND. CPHT .GE. 0.) 20, 21
20 PHI = ASIN(SPHI)
IF (SPHI .GT. CPHT) PHI = ACOS(CPHT)
GO TO 30
21 IF (SPHI .GE. 0. .AND. CPHT .LT. 0.) 22, 23
22 PHI = PI - ASIN(SPHI)
IF (SPHI .GT. ABS(CPHT)) PHI = ACOS(CPHT)
GO TO 30
23 IF (SPHI .LT. 0. .AND. CPHT .LT. 0.) 24, 25
24 PHI = PI - ASIN(SPHI)
IF (ABS(SPHI) .GT. ABS(CPHT)) PHI = TWOPI + ACOS(CPHT)
GO TO 30
25 IF (SPHI .LT. 0. .AND. CPHT .GE. 0.) 26, 27
26 PHI = TWOPI + ASIN(SPHI)
IF (ABS(SPHI) .GT. CPHT) PHI = TWOPI + ACOS(CPHT)
GO TO 30
27 CALL EXIT
30 CONTINUE
C = M * SINL / SPHI
FL1 = FL * FL
CON1 = FL + FL2
CON2 = 0.5 * FL2
CON3 = SPHI * CPHT
CON4 = PHI**2 / SPHI
CON5 = CON4 * CPHT
FM = 1. - C * * 2
RATIO1 = (1. + CON1) * PHI + A * (CON1 * SPHI + CON2 * CON4)
1 + EM * (-0.5 * CON1 * (PHI + CON3) + CON2 * CON5) - A * A * CON2
2 * CON3 + EM * EM * CON2 * (0.125 * (PHI + CON3) - CON5 - 0.25 *
3 CON3 * CPHT**2) + A * EM * CON2 * (CON4 + CON3 * CPHT)
S = RATIO1 * H0
IF (S .LE. 1.E-4) S = 0.
RATIO2 = CON1 * PHI - A * CON2 * (SPHI + Z. * CON4)
1 + 0.4 * FM * CON2 + (-5.0 * PHI + CON3 + 4.0 * CON5)
ALAM = RATIO2 * C + ALL
SALAM = SIN(ALAM)
CALAM = COS(ALAM)
CTAZ12 = FA - CALAM * AH
CTAZ21 = FA * SALAM - AH
IF (AL1 - AL2 .EQ. 0.) 35, 39
35 A712 = 0.
A721 = 0.
GO TO 34
39 CTAZ12 = CTAZ12 / (SALAM * CHET2)
IF (CTAZ12 .EQ. 0.) 54, 55
54 A712 = HAIFI
GO TO 55
55 CONTINUE
A712 = ATAN(1. / CTAZ12)
56 CONTINUE
CTAZ21 = CTAZ21 / (SALAM * CHET1)
IF (CTAZ21 .EQ. 0.) 57, 58
57 A721 = HAIFI
GO TO 34
58 CONTINUE
A721 = ATAN(1. / CTAZ21)
34 CONTINUE

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      IF (ALL .GE. 0. .AND. CTA712 .GE. 0.) 40, 41
40 A712 = A712
      GO TO 50
41 IF (ALL .GE. 0. .AND. CTA712 .LT. 0.) 42, 43
42 A712 = PI + A712
      GO TO 50
43 IF (ALL .LT. 0. .AND. CTA712 .GE. 0.) 44, 45
44 A712 = PI + A712
      GO TO 50
45 A712 = TWOPI + A712
50 IF (ALL .GE. 0. .AND. CTA721 .GE. 0.) 46, 47
46 A721 = PI + A721
      GO TO 51
47 IF (ALL .GE. 0. .AND. CTA721 .LT. 0.) 48, 49
48 A721 = TWOPI + A721
      GO TO 51
49 IF (ALL .LT. 0. .AND. CTA721 .GE. 0.) 52, 53
52 A721 = A721
      GO TO 51
53 A721 = PI + A721
51 CONTINUE
      A712 = AMOD(A712, TWOPI)
      IF (A712 .LT. 0.) A712 = A712 + TWOPI
      A721 = AMOD(A721, TWOPI)
      IF (A721 .LT. 0.) A721 = A721 + TWOPI
      RETURN
END
```

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*MODULE 2
*DECK GEORET
SUBROUTINE GEORET(DSKM,NP)
COMMON LAT(999),LON(999),MSINDX(5800)
COMMON /GRND1/ZPP,ZD(6),Z(1004),ZH(6),ZH(1004),XU(6),X(1009)
COMMON /TE/ZPP1(1004),NPTS
COMMON /SDRD1/S(499),DR(999),DI(999),LLM
COMMON /CITCT/ITCT,LTOP,NPTCT,ZXMTR,ZMIN,ALTSK(3),TSK(3)
NPTS=NP
S(1)=0.
X(1)=0.
DO 1 I=1,NP
CALL GETELV(LAT(I),LON(I),AAMP,FAZ,Z(I))
IF(I.GT.1) S(I)=S(I-1)+DSKM
DR(I) = AAMP * COS(FAZ)
DI(I) = AAMP * SIN(FAZ)
1 CONTINUE
LLM=NP
C COMPUTE BASELINE TERRAIN ELEVATIONS RELATIVE TO TRANSMITTER ALTITUDE.
ZXMTR=Z(1)
Z(1)=0.
DO 2 I=2,NP
C FOR NOW, CONVERT DISTANCE TO METERS.
S(I)=S(I)*1000.
X(I)=S(I)
Z(I)=Z(I)-ZXMTR
2 CONTINUE
C COMPUTE ELEVATION DERIVATIVES.
NPM1=NP-1
DO 3 L=2,NPM1
CALL INT(L,L)
ZPP1(L)=ZPP
3 CONTINUE
ZP(1)=0.
ZPP1(1)=0.
ZP(NP)=ZP(NP-1)
ZPP1(NP)=ZPP1(NP-1)
RETURN
END

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DECK GEORTS
SUBROUTINE GEORTS(EMPH,RLATB,ALONR,RAZPI)
COMMON /PLATB/ RLATA,RLATB,ALAT,RLATI,RLATR,RLATM,SMH
COMMON /ZLATB/ RAZPI,RLATB,ALAT,RLATI,RLATR,RLATM,SMH
COMMON /ZLATI/ RAZPI,RLATB,ALAT,RLATI,RLATR,RLATM,SMH
COMMON /ZLATR/ RAZPI,RLATB,ALAT,RLATI,RLATR,RLATM,SMH
ALAT = ALDAY(4) ESG = ARDAY(1) FCSEN = 1. - ESG
IF (ALC(RLATA)-RAZPI) 50,16,16
5 IF (ALC(PLATB)-RAZPI) 15,16,16
10 PRINT 4801,RLATA,RLATB
4801 FORMAT(1H0, 4H00, 4HRLATA,4HRLATB)
*OUT OF ACCEPTABLE RANGE (-90+2+4)/10X, 180 LATITUDE OF A = ,
*F4.2, 31H RADEGANS LATITUDE OF B = F4.2, 31H RADEGANS
PRINT 4801
5001 FORMAT(1H0, 2HPROGRAM EXECUTION TERMINATED)
      STOP
15 IF (ALC(PLONR)-TWOPI) 20,20,25
20 IF (ALC(PLONR)-TWOPI) 30,30,25
25 PRINT 4802,PLONR,RLATB
4802 FORMAT(1H0, 4H00, 4HPLONR,4HRLATB)
*OUT OF ACCEPTABLE RANGE (-180+2+4)/10X, 180 LONGITUDE OF A = ,
*F4.2, 31H RADEGANS LONGITUDE OF B = F4.2, 31H RADEGANS
      PRINT 4802
      STOP
30 ALONR=PLONR
   RLONR=PLONR
   IF (ALONR+PI) 35,35,40
35 ALONR=ALONR+TWOPI
40 IF (RLONR+PI) 45,45,50
45 RLONR=RLONR+TWOPI
50 RLON = RLONR-ALONR
   IF (RLON+PI) 55,50,55
55 IF (RLON) 60,65,65
60 RLONR = RLONR+TWOPI
   GO TO 45
65 ALONR = ALONR-TWOPI
   GO TO 95
70 PRINT 4803
4803 FORMAT(1H0, 8H00, 4H00, 4H00, 4H00, 4H00, 4H00, 4H00, 4H00,
*OUTING GEORTS CANNOT HANDLE THIS CASE)
      PRINT 4801
      STOP
75 IF (RLON+PI) 85,70,80
80 IF (RLON+PI) 90,40,85
85 RLONR = RLONR-TWOPI
   GO TO 45
90 ALONR = ALONR+TWOPI
95 SMH = PLATA+RLATH
   META = SIN(0.4*SMH)
   META = (1.0-ESG*HFTA*META)/CFSG
   RLAT = ANG(META*SQRT(META*CFSG))
   RLON = RLONR-ALONR
   ALON = HFTA*RLON
   Q = SIN(ALON)
   RLAT = COS(PLATB)
   ALAT = COS(RLATB)
   SAVB = 0.4*RLAT
   SAVH = 0.4*ALAT

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C = SIN(0.5*ALON)
Q = 0*C
AA7 = RLATH-RLATA
CA7B = (1.0-Q)*SIN(AA7)
Q = Q*SIN(SMB)
CA7A = CA7B+Q
CA7B = CA7B-Q
Q = SQRT(SAZA*CA7A+CA7A*CA7A)
SMB = HLAT*ASIN(.)
SAZA = SAZA/Q
CAZA = CAZA/Q
SA7B = SA7B/Q
CA7H = CA7H/Q
RA7A = ATAN2(SAZA,CA7A)
RA7B = ATAN2(SAZB,CA7B)
ALON = RA7B-RA7A
IF (AHS(ALON)-PI) 120,105,105
105 IF (ALON) 110,110,115
110 RA7H = RA7B+TWOPI
GO TO 120
115 RAZA = RAZA+TWOPI
120 HLAT = CESQ*ESQ*ALAT*ALAT
HLON = A0/SORT(HLAT)
HLAT = HLON*CESQ/HLAT
HLON = HLON*ALAT
CLAT = CA7A/HLAT
CLON = SA7A/HLON
HLAT = CESQ*ESQ*BLAT*BLAT
HLON = A0/SORT(HLAT)
HLAT = HLON*CESQ/HLAT
HLON = HLON*BLAT
ALAT = CA7B/HLAT
HLAT = (3.0*AA7/SMB-ALAT-2.0*CLAT)/SMB
ALON = SA7B/HLON
BLON = (3.0*BLON/SMB-ALON-2.0*CLON)/SMB
AAZ = 3.0*SMH
ALAT = ((ALAT-CLAT)/SMB-2.0*HLAT)/AAZ
ALON = ((ALON-CLON)/SMB-2.0*BLON)/AAZ
AAZ = (RA7B-RA7A)/SMB
ENTRY PCORD
RLATP = ((ALAT+SMP+RLAT)*SMP+CLAT)*SMP+RLATA
RLONP = ((ALON+SMP+HLON)*SMP+CLON)*SMB+ALONR
RA7P = AAZ*SMP+RA7A
RETURN
END

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*DECK GETELV
      SUBROUTINE GETELV(LATIN,LONIN,AMP,FAZ,ELVTN)

C PURPOSE:
C   COMPUTES ALTITUDE AND IMPEDANCE AT A GIVEN LATITUDE AND LONGITUDE.
C   ASSUMES A DATABASE TAPE WITH 240 RECORDS PER ZONE OF POINTS. 60
C   WORDS PER RECORD, AND 2 DATA POINTS PER WORD. THESE GROUPINGS COVER
C   THE FOLLOWING MAP SECTIONS:
C     A ZONE SPANS 1 DEGREE LATITUDE (SOUTH TO NORTH) AND 2 DEGREES
C     LONGITUDE (WEST TO EAST) OF THE MAP.
C     A RECORD SPANS 1 DEG. LAT. (S. TO N.) AND 30 SEC. LON. (W. TO E.)
C     OF A ZONE.
C     A WORD SPANS 1 MIN. LAT. (S. TO N.) AND 30 SEC. LON. (W. TO E.).
C     OF A RECORD.
C     A POINT LIES ON EVERY 30 SEC. LAT. AND EVERY 30 SEC. LON.
C     ALTITUDE IS INTERPOLATED WITHIN 4 POINTS WHICH LIE NORTHEAST,
C     SOUTHEAST, NORTHWEST, SOUTHWEST OF THE INPUT POINT.

C INPUTS:
C   LATIN = LATITUDE IN DDDMMSS FORMAT.
C   LONIN = LONGITUDE IN DDDMMSS FORMAT.

C OUTPUTS:
C   AMP = IMPEDANCE AMPLITUDE.
C   FAZ = IMPEDANCE PHASE (RADIAN).
C   ELVTN = ALTITUDE (METER).

C CALLS ROUTINE INDEX FOR:
C   INDEX = POINTER TO A RECORD IN THE DATABASE.
C   IXPT = POINTER TO A HALF-WORD IN A RECORD IN THE DATABASE.

      COMMON /MAP/LATSW,LATNE,LONSW,LONNE
      COMMON /GETELV/L(120),IMP(120)
      COMMON /UNPACK/NPACK(60)
      COMMON /FLAGS/IXPT,NFLAG,NRPC,NRPDB
      COMMON LAT(999),LON(999),MSINDEX(5800)
      DATA KPASS1,MASK8,MASK11 /1,377B,3777B/
      DATA INDDIM /5800/

C READ AND STORE DATABASE TAPE IN FIRST PASS ONLY.
      IF (KPASS1 .NE. 1) GO TO 630
      KPASS1=0
      NRPC=240*((LATNE-LATSW)/10000)
      NRPDB=NRPC*((LONNE-LONSW)/20000)
      IF (NRPDB+1 .LE. INDDIM, GO TO 610
      PRINT 9700, NRPDB $STOP
      610  CALL OPENMS(2,MSINDEX,INDDIM,0)
      DO 629 IRT=1,NRPDB
      BUFFERIN(13,1)(NPACK(1),NPACK(60))$IF (UNIT(13)) 620,629,620
      620  CALL WRITMS(2,NPACK,60,IRT)
      629  CONTINUE
C IF LATITUDE AND LONGITUDE LIE OUTSIDE MAP, PREVIOUS DATA ARE USED.
      630  IF(LATIN.LT.LATSW .OR. LATIN.GE.LATNE) GO TO 190
          IF(LONIN.LT.LONSW .OR. LONIN.GE.LONNE) GO TO 190
C CONVERT TO RELATIVE LATITUDE AND LONGITUDE.
      NFLAG=0
      LATX=LATIN-LATSW
      IF (LATIN.GE.0) GO TO 200
C CORRECT FOR NEGATIVE LATITUDES.
      IF (MOD(LATX,10000).EQ.0) GO TO 200
      LATX=LATX-4000
      IF (MOD(LATX,100).EQ.0) GO TO 200
      LATX=LATX-40

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C PROCEED WITH POSITIVE LATITUDES.
200  LATSEC=MOD(LATX,100)
      LATDM=LATX-LATSEC
      IF (LATSEC.GE.30) GO TO 240
      LATSL=LATDM
      LATNL=LATM+30
      GO TO 260
240  LATSL=LATM+30
      LATNL=LATM+100
      LATM=MOD(LATM,1000)
      IF (LATM.EQ.5900) LATN=LATM+4100
260  LONX=LONIN=LONS
      IF (LONIN.GE.0) GO TO 300
C CORRECT FOR NEGATIVE LONGITUDES.
      IF (MOD(LONX,10000).EQ.0) GO TO 300
      LONX=LONX-4000
      IF (MOD(LONX,100).EQ.0) GO TO 300
      LONX=LONX-40
C PROCEED WITH POSITIVE LONGITUDES.
300  LONSEC=MOD(LONX,100)
      LONDm=LONX-LONSEC
      IF (LONSEC.GE.30) GO TO 340
      LONW=LONDm
      LONE=LONDm+30
      GO TO 360
340  LONW=LONDm+30
      LONE=LONDm+100
      LONM=MOD(LONDm,10000)
      IF (LONM.EQ.5900) LONE=LONDm+4100
360  CONTINUE
C GET A DATA POINT NORTHEAST OF THE INPUT POINT.
      INDNE=INDEX(LATN,LONE)
      IF (INFLAG.EQ.1) GO TO 120
      CALL READMS(2,NPACK,60,INDNE)
      CALL UNPACK
      INF=L(IXPT)
C GET 3 POINTS SOUTHEAST, NORTHWEST, AND SOUTHWEST OF THE INPUT POINT.
      IF (MOD(LATN,10000).EQ.0.OR.MOD(LONF,20000).EQ.0) GOTO 120
C ALL 4 POINTS LIE IN THE SAME ZONE.
      ISF=L(IXPT-1)
      CALL READMS(2,NPACK,60,INDNF-1)
      CALL UNPACK
      INW=L(IXPT)
      ISW=L(IXPT-1)
      GO TO 180
C THE 4 POINTS LIE IN DIFFERENT ZONES.
120  CONTINUE
      INDNW=INDEX(LATN,LONW)
      IF (INFLAG.EQ.1) GO TO 140
      CALL READMS(2,NPACK,60,INDNW)
      CALL UNPACK
      INW=L(IXPT)
140  CONTINUE
      INDSE=INDEX(LATS,LONE)
      IF (INFLAG.EQ.1) GO TO 160
      CALL READMS(2,NPACK,60,INDSE)
      CALL UNPACK

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ISE=L(IXPT)
160 CONTINUE
  INDSW=INDEX(LATS,LONW)
  IF (NFLAG.EQ.1) GO TO 180
  CALL READMS(2,NPACK,60,INDSW)
  CALL UNPACK
  ISW=L(IXPT)
180 CONTINUE
  AMP=FLOAT(SHIFT(IMP(IXPT),-11).A,MASK8)*.001
  FAZ=FLOAT(IMP(IXPT).A,MASK11)*.001
  IF (NFLAG.EQ.1) PRINT 9702
  ELEFT=FLOAT(ISE)+FLOAT((INE-ISE)*MOD(LATSEC,30))/30.
  ELWEST=FLOAT(ISW)+FLOAT((INW-ISW)*MOD(LATSEC,30))/30.
  ELVTN=ELWEST+(ELEFT-ELWEST)*FLOAT(MOD(LONSEC,30))/30.
  RETURN
190 PRINT 9701, LATIN,LONIN
  RETURN
9700 FORMAT (* DATABASE HAS *I10* RECORDS. INCREASE ARRAY MSINDEX AND VA
1PIARLF INDDIM TO ACCOMMODATE. RUN ABORTS.*)
9701 FORMAT(* *,4H***,*,LAT=*I10*,LON=*I10* REQUESTED ARE OUTSIDE MAP R
1EGION - NO ELEVATION RETURNED*,//)
9702 FORMAT(* *,4H***,*,INDEX REQUESTED EXCEEDS SCANLINES GENERATED. TH
1US PREVIOUS ELEVATIONS WILL BE USED*)
  END

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```

*DECK INDEX
  FUNCTION INDEX(LAT,LON)
C PURPOSE:
C COMPUTES POINTERS INTO DATABASE FOR A GIVEN LATITUDE AND LONGITUDE.
C INPUTS:
C LAT = RELATIVE LATITUDE IN DDMMSS FORMAT.
C LON = RELATIVE LONGITUDE IN DDMMSS FORMAT.
C NRPC = NUMBER OF RECORDS PER COLUMN OF MAP AREA 2 DEGREES LONGITUDE
C       WIDE.
C NRPDR = NUMBER OF RECORDS IN THE DATABASE.
C OUTPUTS:
C INDEX = POINTER TO RECORD IN DATABASE.
C IXPT = POINTER TO DATA POINT (= HALF-WORD) IN DATABASE RECORD.
C NFLAG = 1 INDICATES COMPUTED RECORD POINTER IS OUT OF RANGE.
  COMMON /FLAGS/IXPT,NFLAG,NRPC,NRPDR
  LATS=MOD(LAT,100)
  LATM=MOD(LAT,10000)-LATs
  LATD=(LAT-LATM-LATs)/10000
  LATM=LATM/100
  LONS=MOD(LON,100)
  LONM=MOD(LON,10000)-LONS
  LOND=(LON-LONM-LONS)/10000
  LONM=LONM/100
  ILOND=(LOND/2)*NRPC+MOD(LOND,2)*120+LONM*2+LONS/30+1
  INDEX=ILOND+LATD*240
  IXPT=LATM*2+LATs/30+1
  IF (INDEX.GT.NRPDR) NFLAG=1
  RETURN
END

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```

*DECK UNPACK
SUBROUTINE UNPACK
COMMON /SETTELVAL/ IZD(6),IPM(120)
COMMON /UNPACK/NPKNA(48)
DATA MASK11/3777777777777777/
I0=PO+MA-1,IO+M=PO(MA-1)+1,NPKNA=MASK11
LIN=AND((MASK11,SHIFT(NPKNA,-44))+8
JMP(M)=AND((MASK11+SHIFT(IPKNA,30))+8
L(M+1)=AND((MASK11+SHIFT(IPKNA,-19))+8
INP(M+1)=AND((MASK11+NPKNA))
20 CONTINUE
RETURN
END

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*DECK INT
SUBROUTINE INT (I,K)
C INPUTS:
C   I = POSITION IN X AND Z ARRAYS ON WHICH TO CENTER CALCULATIONS
C   K = POSITION IN ARRAYS Z AND ZP TO STORE CALCULATED VALUES
COMMON /GRMD1/ZPP,ZD(6),Z(1009),ZPD(6),P(1009),XD(6),X(1009)
IMO=I-1 $XI=MO=X(IMO) $ZI=MO=Z(IMO) +ZI=Z(1)
IP0=I+1 $XIPO=X(IP0) $XI=X(I) $XK=X(K)
C=((Z(IP0)-ZI)-(ZI-ZI)*(XIPO-XI)/(XI-XI))/
1 ((XIPO*XIPO-XIPO*XIM0)-(XI*XI-XIM0*XIM0)*
2 (XIPO-XIM0)/(XI-XIM0))
B=((ZI-ZIM0)-C*(XI*XI-XIM0*XIM0))/(XI-XIM0)
A=ZI-XI*(B+C*X)
Z(K)=A+XK*(B+C*XK)
ZP(K)=R+2.*C*XK
ZPP=2.*C
RETURN
END

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*MODULE 2
*DECK INFO2F
      SUBROUTINE INFO2F
C REFERENCES:
C   (1) JOHLER, J.H., HERRIG, L.A., LOWAN-D PHASE CORRECTIONS OVER
C       INHOMOGENEOUS, IRREGULAR TERRAIN., ESSA TECHNICAL REPORT
C       TEP 39-ITS4 56, NOVEMBER, 1967.
C       COMMON /KIS/TWOP1,PI,HAFFP1,NRTPI
C       COMMON /GKFL1/ZPP,ZI,(6),/(1009),/L1(6),/P(1009),L1(6),X(1009)
C       COMMON /GRAD2/X0,DEN,K,U,OMX,P2,FL1
C       COMMON /T1//PP1(1004),NHTS
C       COMMON /ZOT1/ARRAY(15)
C       COMMON /SDRUI/S(999),DR(499),DI(499),LLM
C       COMMON /CITCT/ITCT,LTOP,NPTCT,ZXMTR,ZMIN,ALTSW(3),TSW(4)
C 7D. ZD. AND XD PROVIDE STORAGE FOR NEGATIVE INDEXES.
C       DIMENSION TZR(1),T(1000),GW(5),GX(5),EX(4),EW(5),XS(9)
C       DIMENSION WT(9),V(1000)
C       COMPLEX DELI,DEN,FLEAF,F1,F2,F3,F1,62,3,SUM,TERM,
C       1,WAVE,VG,wk,x,TS,FIND,FI
C       DATA KPASS1/1/
C       DATA ((GX(K), K = 1, 5) = .02216356881, .1678315575, .4615473E15,
C       1,7483346284, .9484434262)
C       DATA ((GW(K), K = 1, 5) = .5910484449, .5385334386, .438172725,
C       1,.2989026983, .1333426846)
C       DATA ((FX(K), K = 1, 4) = .1051402826, .3762245145, .6484440124,
C       1,.9373342493)
C       DATA ((FW(K), K = 1, 4) = .06568051989, .1460462655, .2425273456,
C       1,1523625357)
C       DATA (TZER(1)=1.0)
9400 FORMAT (* AIRBORNE TARGET ALTITUDE (*9.2*) LIES BELOW TERRAIN FLE-
IVATION (*9.2*). RUN ABORTS.*)
      FI(WAVER) = COMPLX(COS(WAVER), SIN(WAVER))
C - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -
C START FIRST-PASS INITIALIZATION.
      IF (KPASS1 .NE. 1) GO TO 9944
      KPASS1=0
C FREQ IS USED IN MHZ IN THIS PROGRAM.
      FREQ = ARRAY(1)*1.E-3 + R41 = ARRAY(13) $FLAT = ARRAY(1)
      FOPH = ARRAY(14) + SMOOTH = ARRAY(15) $FTA = ARRAY(2)
      N7FPO=0
      T(N7FPO)=1.0
C WAVE NUMBER IN ATMOSPHERE AT SURFACE OF EARTH
      WAVE = ARRAY(10)
      AMICRO = 1.0/(TWOP1*FREQ)
      TX = SQRT(FREQ*ETA)*.0408349549
C INITIALIZE QUANTITIES
      X(1) = 0.
      K(1) = 1.
C TREAT SMOOTH READING EARTH IF SMOOTH=1.
      IF (SMOOTH .EQ. 1.) Z(1)=ZR(1)=ZF1(1)=0.
9944 CONTINUE
C END FIRST-PASS INITIALIZATION.
C - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -
C START INITIALIZATION FOR CURRENT PATH.
C COMPUTE DISTANCE AND DISTANCE INCREMENT (KM) TO TARGET.
      RMAY=X(MPTS)/1000.
      INC=X(2)/1000.

```

```

LTOP = 0
NOFLAT = 1
C IMPEDANCE SHOULD BE REFERENCED TO 100 KHZ
C FREQUENCY DEPENDENCE OF IMPEDANCE = *SQRT(FREQ/0.1)
DELI = CMPLX(DR(1), DI(1))*SQRT(FREQ/0.1)
IMOST = DMAX/DINC + .01
DELTX = 1000.*DINC
T(1) = 1./SQRT(DELTX)
C FLAT EARTH THEORY DESCRIBED IN REFERENCE 3
DO 32 K = 1, 5
C ATTENUATION FOR FLAT EARTH THEORY
X(-K) = DELTX*GX(K)
CALL GROUND (-K, 2, 0, 0)
32 WG(K) = FLEAF(WAVE, 0., 0., X(-K), DELI)
I = 2
C END INITIALIZATION FOR CURRENT PATH.
C - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - - -
C START LOOP ON SURFACE POINTS ALONG HUFFORD BASELINE.
37 CONTINUE
C TREAT SMOOTH ROUND EARTH IF SMOOTH=1.
IF (SMOOTH .EQ. 1.) Z(I)=P(I)=ZPP1(I)=0.
ZPP=ZPP1(I)
T(I) = 1./SQRT(X(I) + DELTX)
OMX = OM COS(X(I)/RAD)
IGO = I - MOD(I, 2)
IL = I - IGO - 1
C EQUATION 2.1B, REFERENCE 1
R0 = SQRT(2.*RAD*(RAD + Z(I))*OMX + Z(I)**2)
IF (NOFLAT .EQ. 2) GO TO 45
C FLAT DETERMINES DISTANCE TO WHICH FLAT EARTH THEORY IS USED BEFORE
C IRREGULAR, INHOMOGENEOUS TERRAIN MAY BE INSERTED.
40 IF(I.LT.4.OR.FLAT.GT.X(I)) 41,45
41 W(I) = FLEAF(WAVE, 0., 0., X(I), DELI)
GO TO 90
C SPHERICAL EARTH THEORY
45 SUM = 0.
NOFLAT = 2
DO 50 K = 1, 5
C R, DEN AND II ARE FROM GROUND
CALL GEOM(I, -K, 1, 0.)
C EQUATION 2.27, REFERENCE 1
TERM = WG(K)*FI(-WAVE*R)*DEN
50 SUM = (II*GW(K))/SQRT(X(I) - X(-K))*TERM + SUM
C SIMPSONS RULE
SUM = 3.*T(1)*SUM
KK = 1
IF (IL .LT. 3) GO TO 100
DO 60 K = 3, IL
CALL GEOM(I, K, 1, 0.)
TERM = U*T(K-1)*W(K)*EI(-WAVE*R)*DEN
IF (KK .EQ. 2) GO TO 55
SUM = 4.*T(I-K)*TERM + SUM
KK = 2
GO TO 60
55 SUM = 2.*T(I-K)*TERM + SUM
KK = 1
60 CONTINUE.

```

```

100 CONTINUE
    CALL GEOM(I, 2, 1, 0.)
    SUM = T(I-2)*T(1)*W(2)*EI(-WAVE*R)*DEN + SUM
    CALL GEOM(I, I - IGO, 1, 0.)
    F2 = U*T(IL)*W(I-IGO)*EI(-WAVE*R)*DEN
    SUM = (SUM + T(IGO)*F2)*.33333333*DELTX
    IF (IGO .EQ. 2) GO TO 66
    F1 = F2
    F2 = TTERM
    GO TO 70
66  CALL GEOM(I, I - 1, 1, 0.)
    F1 = U*T(I-2)*W(I-1)*EI(-WAVE*R)*DEN
    SUM = SUM + .0033333333*DELTX*(5.*T(1)*F1 + E.*T(2)*F2
    1 - T(3)*TERM)
70  Q = TX/T(I-1)
    RHO = 1. + ZP(I)**2
    KHO = 7PP/RHO
    TERM = 1.2/T(1)*T(I-1)*(CMPLX(0,Q)*(DFLI + CMPLX(0., -RHO/WAVE)))
    WX = 1. - CMPLX(0,0)*(SUM + 2./T(1)*(.466666667*F1
    1 - .066666667*F2))/(1. + TERM)
    W(I) = WX
90  DIST = .001*X(I)
    CALL INDF(0., X(I), ENDH, FIND)
    TS=W(I)*FIND
    PHA=CANG(TS)
C PHIC IS THE SECONDARY PHASE CORRECTION IN RADIANS.
    PHIC = -(PHA - WAVE*(RD - X(I)))
C SEC IS THE SECONDARY PHASE CORRECTION IN MICROSECONDS.
    SEC = PHIC*AMICRO
C SAVE SECONDARY PHASE FACTOR AT TARGET GROUND POINT.
    IF(I.NE.NPTCT) GO TO 987
    TSW(ITCT)=SEC
987  CONTINUE
    I = I + 1
    IF(I.LE.NPTS) GO TO 47
C END LOOP ON SURFACE POINTS ALONG BUFFERD BASELINE.
C -----
C START AIRBORNE TARGET COMPUTATION.
    IF (ZMIN.LT.0.) RETURN
    LTOP = 1
    F2=(0.,0.)
    G2=(0.,0.)
    OLDR=0.
    II = I = NPTCT
    IGO = 2 - MOD(I, 2)
    DO 155 K = 1, 4
    X(1000 + K) = X(1) - DELTX*FX(K)
    XS(K) = X(1000 + K)
155  CALL GROUND(1000+K,II,0,0)
    CALL REVREN(X, W, IMUST, XS, E, 4, 5, 1)
    HL = YMINT - XMINT
C ABORT IF TARGET ALTITUDE IS BELOW TERRAIN.
    IF (HL .GT. Z(I)) GO TO 154
    PRINT 9400,HL,Z(I) $STOP
154  ZZ = RAD + HL
    RD = SQRT(Z.*RAD**2 + ZZ**2 + 2*Z*ZZ*COS(X(I))/RAD) + HL*E
    SUM = P.

```

```

DO 157 K = 1, 5
CALL GEOM(I, -K, 2, HL)
TERM = AVE(K)*F(I-1)*AVE(K)*DF(I)
157 SUM = UPGV(K)*TERM/SQRT(X(I) - X(-K)) + SUM
C SIMPSONS RULE
SUM = 3.*T(I)*S1*I
CALL GEOM(I, 3, 2, HL)
F1 = T(I)*T(I-2)*U*DEN*W(2)
G1 = F1*(-WAVE*R)
SUM = SUM + F1*G1
ILO = I - 160
KGO = 1
IF (ILO .LT. 3) GO TO 115
DO 182 K = 3, ILO
F3 = F2
G3 = G2
F2 = F1
G2 = G1
CALL GEOM(I, K, 2, HL)
G1 = F1*(-WAVE*R)
F1 = T(K-1)*T(I-K)*U*DEN*N(K)
DELTG = WAVE*(R - OLDR)
IF (KGO-2) 158, 159, 172
158 SUM = SUM + 4.*F1*G1
KGO = 2
GO TO 182
159 SUM = SUM + 2.*F1*G1
KGO = 1
IF (ABS(DELTG) .GT. .2) 170, 182
170 KGO = 3
SUM = SUM + F1*G1
GO TO 182
C EQUATION 2.35, REFERENCE 1
172 SUM = SUM + CMPLX(0., 3./DELTG)*(G1*(F1 - .5*(F1*CMPLX(2
1., 3.*DELTG) - 4.*F2*CMPLX(1., DELTG) + F3*CMPLX(2., DELTG
2.)/DELTG**2) - G2*(F2 - .5*(F1*CMPLX(2., DELTG) - 4.*F2
+ F3*CMPLX(2., -DELTG))/DELTG**2))
182 OLDR = R
115 CONTINUE
IF (ILO .EQ. 1) GO TO 188
F3 = F2
G3 = G2
F2 = F1
G2 = G1
CALL GEOM(I, I - 1, 2, HL)
G1 = F1*(-WAVE*R)
F1 = T(I-2)*T(I)*U*DEN*W(I-1)
DELTG = WAVE*(R - OLDR)
IF (ABS(DELTG) .GT. .2) 184, 185
C EQUATION 2.35, REFERENCE 1
184 SUM = SUM + CMPLX(0., 3./DELTG)*(G1*(F1 - .5*(F1*CMPLX(2
1., 3.*DELTG) - 4.*F2*CMPLX(1., DELTG) + F3*CMPLX(2., DELTG
2.)/DELTG**2) - G2*(F2 - .5*(F1*CMPLX(2., DELTG) - 4.*F2
+ F3*CMPLX(2., -DELTG))/DELTG**2))
GO TO 184
185 SUM = SUM + 1.25*F1*G1 + 2.*F2*G2 - .25*F3*G3
188 DO 190 K = 1, 4

```

```
CALL GEOM(I+1000+K, 3, ML)
SUM = SUM + 1.0*FW(K)*VE(K)*EI*(-WAVE*R)*DEN*U/(SIURT(XS(K))*T(I))
130 CONTINUE
SUM = .33333333*FLTX*SUM
R = TX/T(I-1)
WV = (1.0 - CMPLX(I,I)*SUM)*.5
CALL IDFT(ML+X(I)*EORM+FIND)
TCS=I*FIND
FRAD = -(LAMU(TS) - WAVE*(R0 - X(I)))
C FMSEC IS THE PHASE IN MICROSECONDS WHILE FRAD IS THE PHASE IN RADIANS
FMSEC = FRAD*AMICRO
C SAVE PHASE AT TARGET POINT FOR TIME DIFFERENCE CALCULATION.
ALTSV(TTCT) = FMSEC
RETURN
END
```

```

*DECK GROUND
      SUBROUTINE GROUND(I, K, IGO, HH)
C THIS SUBROUTINE USES VARIABLE IMPEDANCE AND TERRAIN TO CALCULATE
C GROUND WAVE FIELDS
      COMMON /GRND1/ ZPP, D(6), Z(1009), ZPD(6), P(1009), XD(6), X(1009)
      COMMON /GRND2/ P0, LFN, L, U, OMX, R2, DELTA
      COMMON /ZOTA/ ARRAY(15)
      COMMON /SDRDI/ S(999), DR(999), DI(999), LLM
      COMPLEX DELTA, DEN
C
      CALL INT (K+I)
      FREQ = ARRAY(1)*1.E-3 SWAVE = ARRAY(10) SA = ARRAY(13)
      RETURN
C
      ENTRY GEOM
      HIT = Z(I) + HH
      IF (I .EQ. K) GO TO 20
      T = (X(I) - X(K))/A
      GS = A + Z(K)
      GX = A + HIT
      CT = COS(T)
      ST = SIN(T)
      OT = OM COS(T)
C EQUATION 2.23, REFERENCE 1
      R2 = SQRT(2.*GS*GX*OT + (HIT - Z(K))**2)
C EQUATION 2.22, REFERENCE 1
C EQUATION 2.30, REFERENCE 1
      R1 = SQRT(2.*A*GS*OM COS(X(K)/A) + Z(K)**2)
      R = R1 + R2 - P0
C EQUATION 2.30, REFERENCE 1
C U = PROJECTION FACTOR TO THE SURFACE OF INTEGRATION.
      U = X(K)*R0*SQRT(1. + ZP(K)**2)/(R1*R2*X(I))
      IF (IGO .LT. 3) U = U*(X(I) - X(K))
C EQUATION 2.30, REFERENCE 1
C PD = NORMAL PARTIAL DERIVATIVE TO THE SURFACE OF THE GROUND.
      PD = (A*OT + Z(K) - HIT*CT + GX*ZP(K)*A*ST/GS)/R2
      XK = X(K)
      IF (XK .GE. S(LLM)) GO TO 12
      LLL = 1
      IF (XK .LT. S(1)) GO TO 10
      LLM0 = LLM - 1
      IF (LLM0 .LT. 1) GO TO 100
      DO 13 LLL = 1, LLM0
      IF (XK .LT. S(LLL + 1) .AND. XK .GE. S(LLL)) GO TO 10
13  CONTINUE
100 CONTINUE
      GO TO 21
C FREQUENCY DEPENDENCE OF IMPEDANCE = *SQRT(FREQ/0.1)
C DELTA = COMPLEX LOCAL GROUND IMPEDANCE THAT IS ADDED TO A
C FUNCTION INVOLVING WAVE, R2 AND PD.
      10  DELTA = CMPLX(DR(LLL), DI(LLL))*SQRT(FREQ/0.1)
      GO TO 21
C FOR VALUES OF X GREATER THAN THE LAST S VALUE READ IN, THE LAST
C IMPEDANCE IS USED
C FREQUENCY DEPENDENCE OF IMPEDANCE = *SQRT(FREQ/0.1)
      12  DELTA = CMPLX(DR(LLM), DI(LLM))*SQRT(FREQ/0.1)
      21  CONTINUE

```

```
C DELTA2 = DERIVATIVE PART OF IMPEDANCE
C EQUATION 21. REFERENCE 2
    DELTA2 = CMPLX(1., -1. / (WAVE*R2)) * PI
C EQUATION 20. REFERENCE 2
19  UFN = DELTA2 + DELTA
    RETURN
20  U = 0.
    R2 = GX - A - Z(I)
    RETURN
END
```

```
*DECK OMCOS
FUNCTION OMCOS(X)
C OMCOS(X) = 1 - COS(X)
    IF (ABS(X) .GT. .15) GO TO 40
    IF (X .EQ. 0.) GO TO 50
    S = X*X
    OMCOS = T = .5*S
    R = 4.
10  T = -T*S/(R*(R - 1.))
    OMCOS = OMCOS + T
    IF (T/OMCOS .LE. .5E-9) GO TO 51
    R = R + 2.
    GO TO 10
40  OMCOS = 1. - COS(X)
    RETURN
50  OMCOS = 0.
51  RETURN
END
```

```

*DECK CNFKRKA
      SUBROUTINE CNFKRKA(A, FA, NA, X, FX, NX, NPT, KASE)
C INTERPOLATION OF F(X) FOR AN X ARRAY USING AITKEN'S METHOD FOR
C EXTRAPOLATION OR INTERPOLATION NEAR THE ENDS OF THE GIVEN ARRAY AND
C NEVILLE'S METHOD FOR ALL OTHER INTERPOLATION.
C INPUT
C   A = THE ARRAY OF GIVEN ABSISSA IN ASCENDING ORDER.
C   FA = THE ARRAY OF GIVEN VALUES OF F(A). FA IS COMPLEX.
C   NA = THE NUMBER OF ELEMENTS IN EACH OF THE ARRAYS A AND F(A).
C   X = THE VALUES OF X IN ASCENDING ORDER FOR WHICH ONE WISHES TO
C       DETERMINE F(X).
C   NX = THE NUMBER OF ELEMENTS IN EACH OF THE ARRAYS X AND F(X).
C   NPT = THE ODD NUMBER OF POINTS USED FOR INTERPOLATION. NPT CAN
C       NOT BE GREATER THAN NA.
C   KASE = 1, THE PROGRAM PROCEEDS NORMALLY
C   KASE = 2, F(X) IS CALCULATED ONLY FOR THOSE X VALUES THAT REQUIR
C   A(NA) FOR INTERPOLATION
C OUTPUT
C   FX = THE ARRAY OF VALUES APPROXIMATED FOR F(X). FX IS COMPLEX.
      COMPLFX FA, FX, FUNCT, POLY
      DIMENSION A(NA), FA(NA), X(NX), FX(NX), FUNCT(15), ABSC(15), DIF(1
      15), POLY(15)
9600  FORMAT (1H0/5OH THE X VALUES ARE NOT ARRANGED IN ASCENDING ORDER./
      1/5X,4H1 = E20.9,5X,7HJ(I) = E20.9+5X,4HJ = E20.9,5X,7HA(J) = E20.9
      2///14X,1H4X,20X,4HF(X))
9601  FORMAT (5X,2E20.9)
9602  FORMAT (1H0* THEREF ARE NOT ENOUGH POINTS IN THE GIVEN ARRAY.*)
      LOOP = 1
      IF (NPT - 15) 3, 3, 9
      9  NPT = 15
      3  IF (NPT - NA) 8, 8, 4
      4  NPT = NPT - 2
      5  IF (NPT - 1) 5, 5, 6
      5  PRINT 9602
      CALL EXIT
      6  IF (LOOP .EQ. 2) GO TO 3
      7  LOOP = 2
      GO TO 3
      8  NPT2 = NPT/2
      IF (KASE .EQ. 2) GO TO 12
11  NSTART = 1
      MX = 1
      GO TO 16
12  NSTART = NA - 3
      TEST = A(NSTART) + (A(NSTART + 1) - A(NSTART))/2
      IF (NX .LT. 1) GO TO 170
      DO 14 I = 1, NX
      IF (X(I) - TEST) 14, 14, 13
      13  MX = I
      GO TO 16
      14  CONTINUE
170  CONTINUE
      16  NSTOP = NA - 1
      IF (NX .LT. MX) GO TO 175
      DO 125 I = MX, NX
      IF (X(I) - A(I)) 135, 15, 10
      10  IF (X(I) - A(NA)) 25, 20, 130

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15 FX(I) = FA(I)
GO TO 125
20 FX(I) = FA(NA)
GO TO 125
25 IF (NSTOP .LT. NSTART) GO TO 180
DO 85 J = NSTART, NSTOP
IF (X(I) - A(J)) 32, 35, 30
30 IF (X(I) - A(J + 1)) 45, 40, 85
32 II = I - 1
PRINT 9600, I, X(I), J, A(J)
IF (II) 34, 34, 33
33 PRINT 9601, (X(N), FX(N), N = 1, II)
34 CALL EXIT
35 FX(I) = FA(J)
NSTART = J
GO TO 125
40 FX(I) = FA(J + 1)
NSTART = J + 1
GO TO 125
45 NSTART = J
IF (ABS(X(I) - A(J)) - ABS(X(I) - A(J + 1))) 50, 50, 55
50 JJ = J
GO TO 60
55 JJ = J + 1
GO TO 60
85 CONTINUE
180 CONTINUE
60 IF (JJ - NPT2) 135, 135, 70
70 IF (JJ + NPT2 - NA) 80, 80, 130
80 KK = JJ - NPT2 - 1
90 IF (NPT .LT. 1) GO TO 185
DO 95 K = 1, NPT
KK = KK + 1
FUNCT(K) = FA(KK)
ABSC(K) = A(KK)
95 DIF(K) = ABSC(K) - X(I)
185 CONTINUE
NTOP = NPT - 1
LL = 1
100 IF (NTOP .LT. 1) GO TO 190
DO 105 L = 1, NTOP
LLL = L + LL
105 POLY(L) = (FUNCT(L)*DIF(LLL) - FUNCT(L+1)*DIF(L))/ (ABSC(LLL))
1 - ABSC(L))
190 CONTINUE
IF (NTOP - 1) 120, 120, 110
110 DO 115 M = 1, NTOP
115 FUNCT(M) = POLY(M)
NTOP = NTOP - 1
LL = LL + 1
GO TO 100
130 INC = - 1
KK = NA + 1
GO TO 140
135 INC = 1
KK = 0
140 IF (NPT .LT. 1) GO TO 215

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DO 145 K = 1, NPT
KK = KK + INC
FUNCT(K) = FA(KK)
ABSC(K) = A(KK)
145 DIF(K) = ABSC(K) - X(I)
215 CONTINUE
NTOP = NPT - 1
LL = 1
150 IF (NTOP .LT. 1) GO TO 220
DO 155 L = 1, NTOP
LLL = L + LL
155 POLY(L) = (FUNCT(1)*DIF(LLL) - FUNCT(L+1)*DIF(LL)) / (ABSC(LLL)
1 - ABSC(LL))
220 CONTINUE
IF (NTOP = 1) 120, 120, 160
160 DO 165 M = 1, NTOP
165 FUNCT(M) = POLY(M)
NTOP = NTOP - 1
LL = LL + 1
GO TO 150
120 FX(I) = POLY(1)
125 CONTINUE
175 CONTINUE
RETURN
END

```

```

*DECK FLEAF
COMPLEX FUNCTION FLEAF(WAVE, H1, H2, XD, DELTAR)
C FLAT EARTH THEORY. REFERENCE 3
C COMPLEX TEMP, Q, Z, Z2, Z7, HWERF, WERFZ, WERF, ZWERF, DELTAR
H1 = H2 - H1
TEMP = (0.7071067812 - 0.7071067812)*SQR(1.5*WAVE)
XD2 = SQR(XD)
Q = -TEMP*HD/XD2
Z = TEMP*DELTAR*XD2 + 0
Z1 = -Z
ZI = AIMAG(ZZ)
IF (ZI.LT.0.0K, (ARS(REAL(ZZ)).LT.6.0 AND ZI.LT.6.0)) GO TO 10
Z2 = ZZ**2
HWERF = (Z2 - 2.0)/(Z7*(Z2 - 3.5))
GO TO 12
C WERF = COMPLEMENTARY ERROR FUNCTION
10 WERFZ = WERF(ZZ)
HWERF = Z7 - 0.5*WERFZ/(Z7*WERFZ + (0.0 - 0.5641895H))
12 ZWERF = Z + HWERF
FLEAF = (6*ZWERF - 0.5)/(7*ZWERF - 0.5)
RETURN
END

```

```

*DECK WERF
      COMPLEX FUNCTION WERF(Z77)
C  COMPLEMENTARY ERROR FUNCTION
      COMPLEX Z, ZZ7, ZV, V, Z2, C, W, S
      DIMENSION C(12), W(5, 4)
      EQUIVALENCE (S, C(12)),
      DATA (C(1) = (.0, -.5641895835))
      DATA W/(1..0.0),
1  (3.674794411714423E-01,6.071577058413937E-01),
2  (1.831563888873418E-02,3.400262170660662E-01),
3  (1.234098040866788E-04,2.011573170376004E-01),
4  (1.125351747192646E-07,1.459535899001528E-01),
5  (4.275835761558070E-01,0.000000000000000E+00),
6  (3.047442052569126E-01,2.082189382028316E-01),
7  (1.402395813662779E-01,2.22134401798991E-01),
8  (6.531777728904697E-02,1.739183154163490E-01),
9  (3.628145648998864E-02,1.358389510006551E-01),
A  (2.553456763105058E-01,0.000000000000000E+00),
B  (2.184426152748907E-01,9.299780939260186E-02),
C  (1.479527595120158E-01,1.311797170842178E-01),
D  (9.271076642644332E-02,1.283169622282615E-01),
E  (5.968692961044590E-02,1.132100561244882E-01),
F  (1.790011511813930E-01,0.000000000000000E+00),
G  (1.642611363929861E-01,5.019713513524966E-02),
H  (1.307574696698522E-01,8.111265047745472E-02),
I  (9.640250558304439E-02,9.123632600421258E-02),
J  (6.974096164964750E-02,8.934000024036461E-02)/
      XX = REAL(ZZZ)
      YY = AIMAG(ZZZ)
      X = ABS(XX)
      Y = ABS(YY)
      Z = CMPLX(X, Y)
      L72 = 0
      IF (X .GE. 4.5 .OR. Y .GE. 3.5) GO TO 100
      I = X + .5
      J = Y + .5
      V = CMPLX(FLOAT(I), FLOAT(J))
      ZV = 7 - V
      C(2) = W(I + 1, J + 1)
      AI = 0.
      DO 10 I = 3, 12
      AI = AI + .5
      C(I) = (V*C(I - 1) + C(I - 2))/AI
10    CONTINUE
      J = 12
      DO 11 I = 2, 11
      J = J - 1
11    S = S*ZV + C(J)
20    IF (YY .GE. 0.) GO TO 30
      IF (L72 .EQ. 0) Z2 = 7*7
      S = 2.*CEXP(-Z2) - S
      IF (XX .GT. 0.) S = CONJG(S)
      GO TO 200
30    IF (XX .LT. 0.) S = CONJG(S)
200   WERF = S
      RETURN
100   L72 = 1

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```

Z2 = Z*Z
S = Z*((0..0.4613135279)/(Z2 - 0.1901635092) + (0..0.09999216168)
     /((Z2 - 1.7844927485) + (0..0.0028838938748)/(Z2 - 5.52534374379))
GO TO 20
END

```

```

*DECK CANG
FUNCTION CANG(Z)
C PURPOSE:
C COMPUTES THE ARGUMENT OF A COMPLEX NUMBER Z SUCH THAT
C -PI .LT. THETA .LE. PI.
COMMON /PIS/TWOPi,PI,HAFPi,ORTPi
COMPLEX Z
X=REAL(Z)
Y=AIMAG(Z)
IF (X) 20,30,10
10 CANG=ATAN2(Y,X)
RETURN
20 IF (Y.NE.0.) GO TO 10
CANG=PI
RETURN
30 IF (Y.GT.0.) GO TO 40
IF (Y.LT.0.) GO TO 50
CANG=0.
RETURN
40 CANG=HAFPi
RETURN
50 CANG=-HAFPi
RETURN
END

```

```

*DECK INDF
      SUBROUTINE INDF (HH,XX,EORH,F)
C THIS SUBROUTINE CALCULATES THE INDUCTION FIELDS FOR E SUB R AND
C H SUB PHI
C THESE INDUCTION FIELDS ARE FOR POSITIVE TIME FUNCTION
C EORH = 1. GIVES INDUCTION FIELD FOR E SUB R (TOWEL HAR)
C EORH = 0. GIVES INDUCTION FIELD FOR H SUB PHI (LOOP)
C FZ = INDUCTION FIELD FOR E SUB R
C FH = INDUCTION FIELD FOR H SUB PHI
COMMON /ZOTA/ARRAY(15)
COMMON /PIS/TWOP1,PI,HAFPI,ORTPI
DOUBLE THETAD,SINTH,COSTH,R,CONS
COMPLFX FZ,FH,F
A =ARRAY(3) SC = ARRAY(9)*1.E+9 $WAVE = ARRAY(10)
IF(XX.LE.0.)3*4
3 PRINT 9500
9500 FORMAT (///* IN INDF, DISTANCE IS ZERO OR NEGATIVE, XX = *,F20.10)
CALL EXIT
4 THETAD=1.D0*XX/A
SINTH=DSIN(THETAD)
COSTH=DCOS(THETAD)
R=A+HH
CONS=A*R*SINTH**2
D2=R*R+A*A-2.*A*R*COSTH
IF(D2.GT.0.) GO TO 30
DD=XX
D2=XX*XX
GO TO 40
30 CONTINUE
DD=SQRT(D2)
40 CONTINUE
D3=DD*D2
D4=D2*D2
FZR=-2.*COSTH/DD+3.*CONS/D3
FZI=(WAVE*CONS+2.*COSTH/WAVE)/D2-3.*CONS/(D4*WAVE)
FZ=CMPLX(FZR,FZI)
FZ=FZ/CMPLX(0.,WAVE)
FHR=R*SINTH*DD/D3
FHI=WAVE*R*SINTH*DD/D2
FH=CMPLX(FHI,-FHR)
C1=2.E-7*TWOP1*WAVE*C
FH=FH/C1
IF(EORH)1,2
1 F=FZ
RETURN
2 F=FH
RETURN
END

```

MISSION  
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*Rome Air Development Center*

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