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LEADTIME VARIABILITY IN INVENTORY REQUIREMENT PROJECTIONS.(U)
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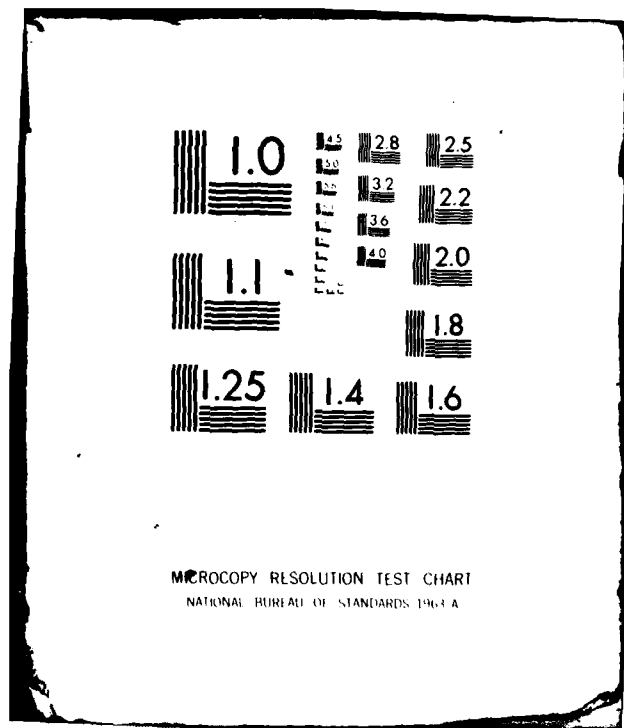
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The AF has experienced inventory support problems apparently because of Leadtime Variability. This study was to find out whether Leadtime Variability had a significant influence on safety stocks. The researcher fitted different distributions to Lead time data of High-Intensity items and found the data to fit the laplace distribution. Previous work of Presutti and Tropp (1970) provide an optimization model for the distribution. Use of this model can raise the average service level significantly. Cost of conversion for AFLC is →

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Phase III (item no. 0004): Air Force Contract F 33615-79-C-5143

LEADTIME VARIABILITY IN INVENTORY REQUIREMENT PROJECTIONS:
FINAL RECHNICAL REPORT AND SUMMARY

Submitted to:

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SUMMARY

This is the Phase III of AF Contract F 33615-79-C-5143: Leadtime Variability in Inventory Requirements Projections -- Final Technical Report and Summary. The report summarizes the first two technical reports and the results of the cost benefit analysis. The study consisted of three phases, and this is the third phase. The purpose of the study was to find out whether leadtime variability had a significant influence on stock safety levels. We found that, indeed, it has.

Currently, AFLC revises its leadtime according to the following model:

$$\hat{L}_t = L_{t-1} ,$$

where $\hat{L}_t$ is the estimate of the required leadtime during period t and L_{t-1} is the actual leadtime observed during the preceding period. This model is inappropriate because it implicitly assumes that leadtime for the next-period-ahead is deterministic, whereas it is stochastic. Cohen, in a similar study for the U. S. Army, makes like observations (Cohen, 1979).

The first phase of the study was concerned with fitting distributions to leadtime data of high-intensity items. The results showed that procurement leadtime can be fitted very well by the lognormal, the gamma, the normal, or the Weibull. The gamma distribution has very often been postulated for the distribution of leadtime (Burgin, 1972, for example) and our results support this assumption.

The second phase was to be a simulation study and an analysis to examine the impact on inventory control levels of the fitted distributions of leadtime. The simulation model was to have been provided by AFLC, but in a February 5, 1980, meeting at WPAFB with Major Paul Gross of AFBRMC and Gloria

Picciano, Diann Lawson, and Carol Hawks of LORRA, it was agreed that it would be more beneficial to do independent simulations as well as look into several important issues not specified in the original contract. The oral agreement was embodied in a memo of understanding received on March 7, 1980. This memo is provided as Appendix A to this report.

Addressing the several issues raised by the memo of understanding, we first conjecture that the "skewed normal" distribution reported upon by Demmy (1979, p. IV-13) in his analysis of forecast error is likely produced by faulty analysis. We support this conjecture by simulation and by an analysis the reader will find in section 3. A good forecasting methodology should produce normally distributed forecast errors.

When leadtime and demand are stochastic, leadtime demand would be a compound distribution or a convolution. We knew the distribution of leadtime for the items in the sample, but we did not have the corresponding distributions for demand. Consequently, we assumed that daily demand at a depot is Poisson-distributed. We then obtained via simulation the compound distribution of leadtime demand for a few representative items. And we succeeded in fitting the right tails of these simulated leadtime distributions to the Laplace. This result is important because it verifies an important assumption in the work of Presutti and Trepp (1970). With Laplace leadtime demand, Presutti and Trepp have already worked out the optimization models. We also found that the normal distribution is a good approximation to the distribution of leadtime, but that the Laplace is better. Optimization techniques concerning the normal have been extensively worked out (see Brown, 1967). Section 5 of this report deals at some length with the distribution of leadtime demand.

Section 6 presents results of a cost-benefit analysis. Using a scenario at WR-ALC with shortage factor $\lambda = 660$, requisition size, $R = 4$, and essentiality parameter, $Z_i = 0.5$, we simulate the current system versus the Presutti-Trepp model IV (1970, pp. 248-249) optimal system. We find that the current system is wanting, the present average service level being 79.6% versus an optimal level of 86.9%. To bring the system to optimality for our sample requires a one-time investment of about \$750,000 in safety stocks and an increase of about \$250,000 in annual operating costs. With an annual procurement of one billion dollars, our sample represents 0.5% of that procurement. Thus, if the sample is representative, AFLC would require a one-time investment of \$150 million in safety stocks and an increase in annual operating cost of \$50 million.

It is also evident that the present mix of stock levels is inappropriate, and that the policy of maintaining an aggregate safety level stock not exceeding a two-month supply is not sound. The reader will discern these details in section 6.

1. DESCRIPTION OF THE STUDY

In recent years, the Air Force Logistics Command (AFLC), with an inventory of economic order quantity (EOQ) of over two billion dollars, has encountered inventory support problem apparently because of leadtime variability. The purpose of this study is to determine whether leadtime variability has a significant impact on inventory support planning and control at AFLC.

Using Air Force leadtime data on high-intensity items, we performed the runs test for randomness (Siegel, pp. 52-56). The leadtime data were random except for a few instances of suspected "pencil-whipping." With random leadtime data, we could then fit statistical distributions to them. This was accomplished by means of the Kolmogorov-Smirnov (KS) goodness-of-fit test (Conover, 1971, pp. 293-298), fitting the data to the exponential, the gamma, the normal, the Weibull, and the lognormal. The results indicated that, in general, the lognormal, the gamma, the normal, and the Weibull could be postulated as good fits to the leadtime data.

The impact of leadtime variability on stock levels can be known exactly if we identify the distribution of leadtime demand. To do that we need to know not only the distribution of leadtime but also of period demand. Since we had no demand data except item monthly demand rates, we assumed that daily demand is Poisson-distributed. Then with the best fit for leadtime and with demand Poisson, we simulated the distribution of leadtime demand for some representative items in the sample. The results indicated that the right half of the simulated distribution can be fitted very well to the Laplace. This is quite an important finding since AFLC would like to use

the Presutti-Trepp Model IV (1970, pp. 248-249) which assumes that leadtime demand is Laplace-distributed.

The final stage of the study was to conduct a cost-benefit analysis of current and proposed stock levels. This was accomplished with the aid of data received from LORRA on May 23, 1980. With that data and using Changes 2 and 3 of AFLC Regulations 57-6 (Department of the Air Force, 29 December 1978 and 22 June 1979), we were able to describe the current system. And by using the Presutti-Trepp Model IV, we were also able to generate a proposed optimal system.

2. SUMMARY OF THE FIRST TWO TECHNICAL REPORTS

According to the contract, the first technical report (Phase I) was to be delivered on December 31, 1979, the second (Phase II) on March 31, 1980. The Phase I report was to address the statistical distributions of leadtime, the Phase II report the AFLC simulation model. But because leadtime data were obtained in two subsets of sizes $n = 16$ and $n = 46$, the first in mid-October 1979 and the second toward the end of November 1979, and because of the memo of understanding (see Appendix A), the first two reports understandably did not conform precisely to the letter of the contract.

The Phase I report (27 pages) advanced the concept of leadtime demand as a compound distribution of period demand and leadtime. It also reported the results of goodness-of-fit tests on the first subset of sixteen items. Before doing the goodness-of-fit, the data were verified to be random.

The Phase II report (96 pages) completed the fitting of statistical distributions to the leadtime data, addressing the second subset of forty-six items. The Phase II report was made of seven technical appendices in order to facilitate future research and to serve as tutorials on the statistical distributions considered. Perhaps a very important Appendix in the Phase II report is the one that theoretically examines the influence of leadtime variability on buffer stocks and service levels, with examples provided on selected items.

3. THE DISTRIBUTION OF FORECAST ERRORS

In his analysis of forecast errors, Demmy (1979) arrived at distributions that are very much skewed to the right, distributions called "skewed normal" by LORRA. The purpose of this section is to show that when there is a mix dominated by declining demands for the many and sharply increasing demands for the few, then the method used by Demmy is very likely to produce distributions of forecast errors that are skewed to the right. We go on to validate our assertion by means of a set of experiments. But first we must say that data must be stationary and also random, that is uncorrelated, before distributions are fitted to them. This was evidently not in the case with Demmy's forecast errors. We concentrate on his Table IV-2 (Demmy, 1979, p. IV-13). The distributions he produced were based on approximately 22,500 items. For each of these items, he calculated a simple average and the MAD of the demands for the first eight quarters, that is, FY 71-72 (Demmy, 1979, pp. III-1 to III-3 and III-9 to III-11). The simple average became the forecast for each quarter in FY 73-75. Thus the forecast errors of quarters 9, 10, . . . , 20 were the actual demands for the quarter in question minus the simple average for the first eight quarters. Demmy then divided this forecast error by the historical MAD for that item in order to obtain standardized scores and in order to be able to aggregate the 22,500 odd forecast errors for each period. He called these standardized scores Z9, Z10, . . . , Z20.

If the demands for these items were stationary, then the distribution of forecast errors would have been symmetric if not normal. But these demands were not stationary, and it seems that most were declining with time. Consequently, the majority of the forecast errors were negative,

which explains the negative bias in forecast errors that Demmy obtained (Demmy, 1979, p. III-16). With declining demands it is obvious that the absolute value of the bias would increase with time: this is precisely what Demmy reports.

In summary we conjecture that the "skewed normal" distributions obtained by Demmy are merely a result of wrong statistical analysis. Any forecasting method worth its salt should yield normally distributed forecast errors. Had Demmy accounted for the trends in demand, his forecast errors would have been normally distributed; and to validate our assertion, we perform a set of experiments.

A Set of Experiments

Eighty items are considered in the set of experiments. The demand function of every item can be described by the following expression:

$$D(t) = D(t-1) + C + X, \quad (3.1)$$

where $D(t)$ = demand in time period t ,

C = a constant,

and X = a normally distributed random variable with zero mean and std. dev. equal to σ_X .

Each item belongs to one of the four classes described below:

Class I : C is negative.

Class II : C is zero.

Class III : C is positive.

Class IV : C is positive, but has a value of C' during the first eight time periods, and a value of C'' during the next twelve time periods. In addition C'' is greater than C' .

Each item has a unique combination of C and σ_X . For each item twenty demand values were generated by a mechanism consistent with (3.1).

Class I items show declining demand with a linear trend. Class II items exhibit no trend, whereas Class III items show increasing demand again with a linear trend. Class IV items also exhibit increasing demand but the trend changes abruptly after the eighth period.

Forecasting Technique 1: Trend not removed. The average demand in the first eight periods was the forecast for each of the next twelve periods. The standardized forecast error $Z(t)$ was computed as follows:

$$Z(t) = \frac{D(t) - F(t)}{MAD}, \quad t = 9, 10, \dots, 20,$$

$$\text{where } F(t) = \text{forecast for period } t = \frac{\sum_{t=1}^8 D(t)}{8},$$

and MAD = mean absolute deviation of demand during the first eight periods.

Forecasting Technique 2: Trend removed. The first difference $S(t) = D(t) - D(t-1)$, was computed for the first eight periods. Values of $D(0)$ were generated by the appropriate mechanism. The average value of $S(t)$ in the first eight periods was a forecast of $S(t)$ in each of the next twelve periods. Let the forecast of $S(t)$ be $FS(t)$, and the forecast of demand be $SF(t)$.

$$\text{Then } FS(t) = \frac{S(1) + S(2) + \dots + S(8)}{8}, \quad t = 9, 10, \dots, 20;$$

$$\text{and } SF(t) = D(t-1) + FS(t), \quad t = 9, 10, \dots, 20.$$

The standardized error $SZ(t)$ is given by

$$SZ(t) = \frac{D(t) - SF(t)}{MAD}.$$

Experiments and Results -- Sample: Type A. Type A samples consisted of items from Classes I, II, and III. Each sample had eighty items. When the proportion of Class I items in the sample was higher than that of Class III, the distribution of $Z(t)$ was found to be skewed to the right with a negative mean. For higher values of t , the mean shifted further away from zero. The distribution of $SZ(t)$, however, was symmetric with a mean very nearly equal to zero.

As more and more Class III items were substituted for Class I items, the distribution of $Z(t)$ became increasingly symmetric. When the proportion of Class III items exceeded that of Class I items, the distribution of $Z(t)$ became skewed to the left with a positive mean.

The distribution of $SZ(t)$ remained symmetric in spite of changes in the mix of items.

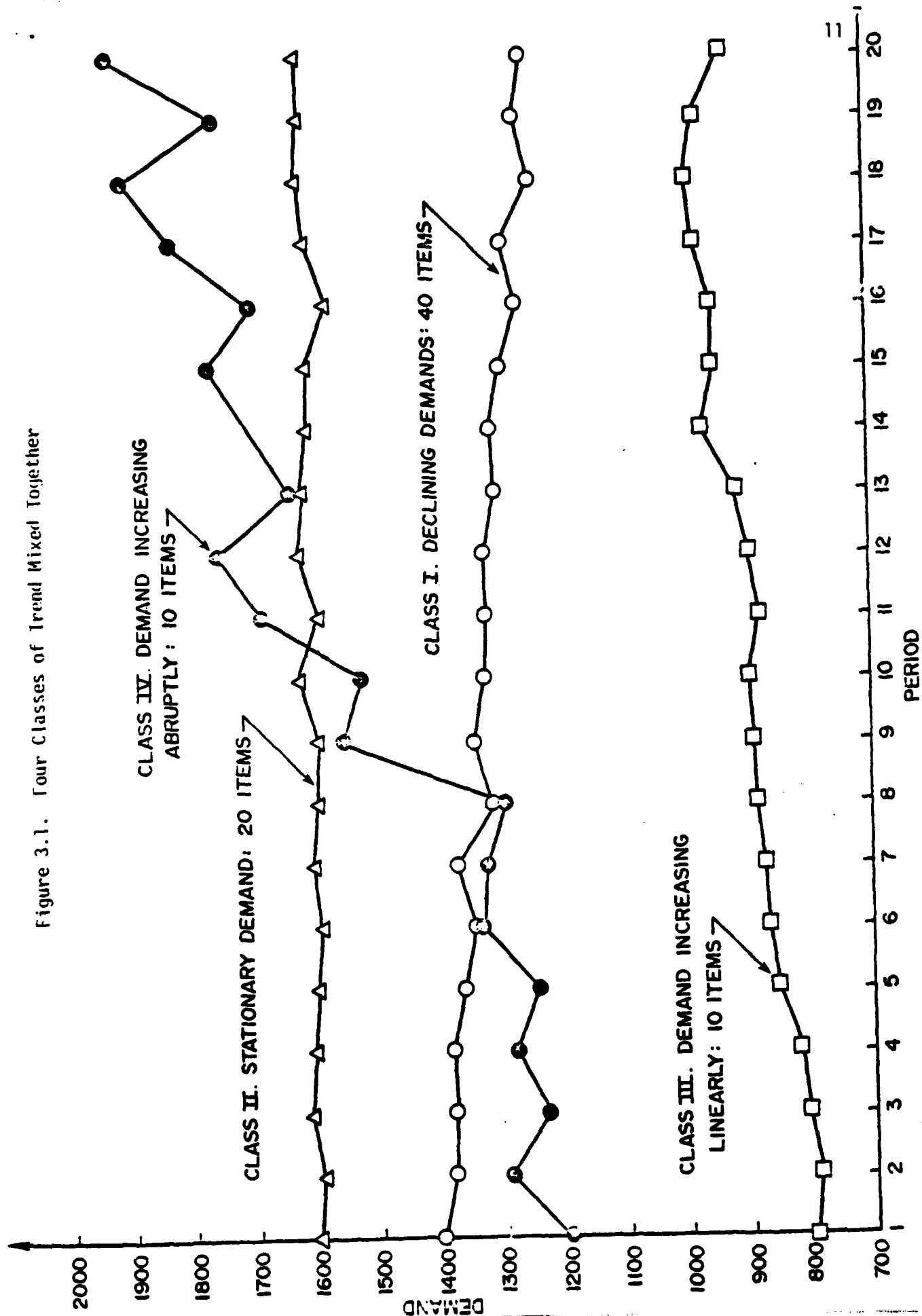
Experiments and Results -- Sample: Type B. Type B samples consisted of items from all four classes. A typical sample had the following composition:

40	Class I items
20	Class II items
10	Class III items
10	Class IV items.

An example of these classes of trend is given in Figure 3.1.

For this sample the $Z(t)$ distribution was skewed to the right with a long right tail. This may be immediately seen in Figure 3.2; and for comparison we reproduce in Figure 3.3 Demmy's Z9 distribution. The tail vanished when Class IV items were dropped, though the distribution remained skewed to the right. The $SZ(t)$ distribution was also found to have a long

Figure 3.1. Four Classes of Trend Mixed Together



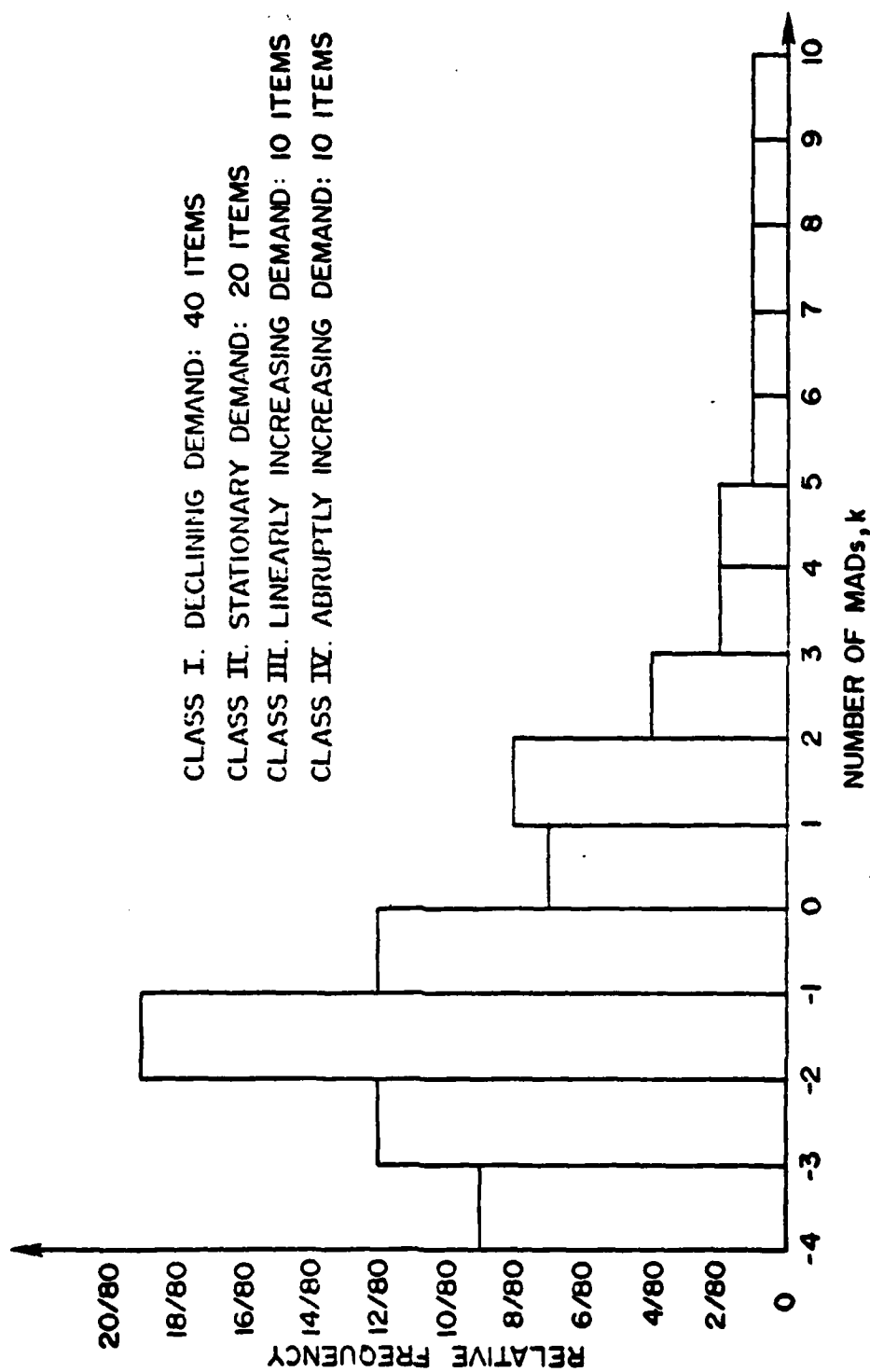


Figure 3.2. The Distribution of Forecast Errors, Z_9 , for the Eighty Hypothetical Items when the Data are Not Detrended.

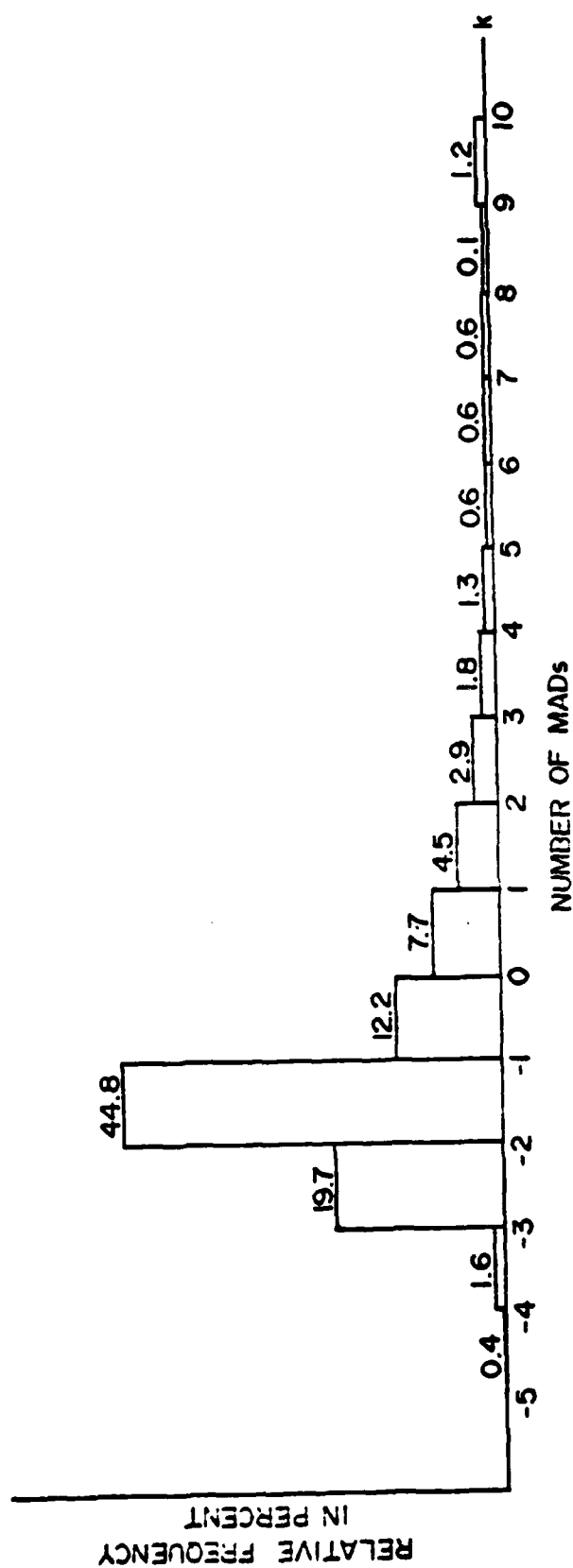


Figure 3.3. The Distribution of Forecast Errors, Z9, for OC-ALC Items with SMGC = 2
(The distribution is based on approximately 22,500 items)

Source: Denny (1979, p. IV-13)

right tail. With the elimination of Class IV items, the tail disappeared and the distribution became symmetric around a mean that was very close to zero, as can be seen in Figure 3.4.

In conclusion, the assertion by LORRA that the distribution of forecast errors is highly skewed to the right does not seem valid. It is contrary to theory, and is most likely based on undue confidence in a very faulty forecast method.

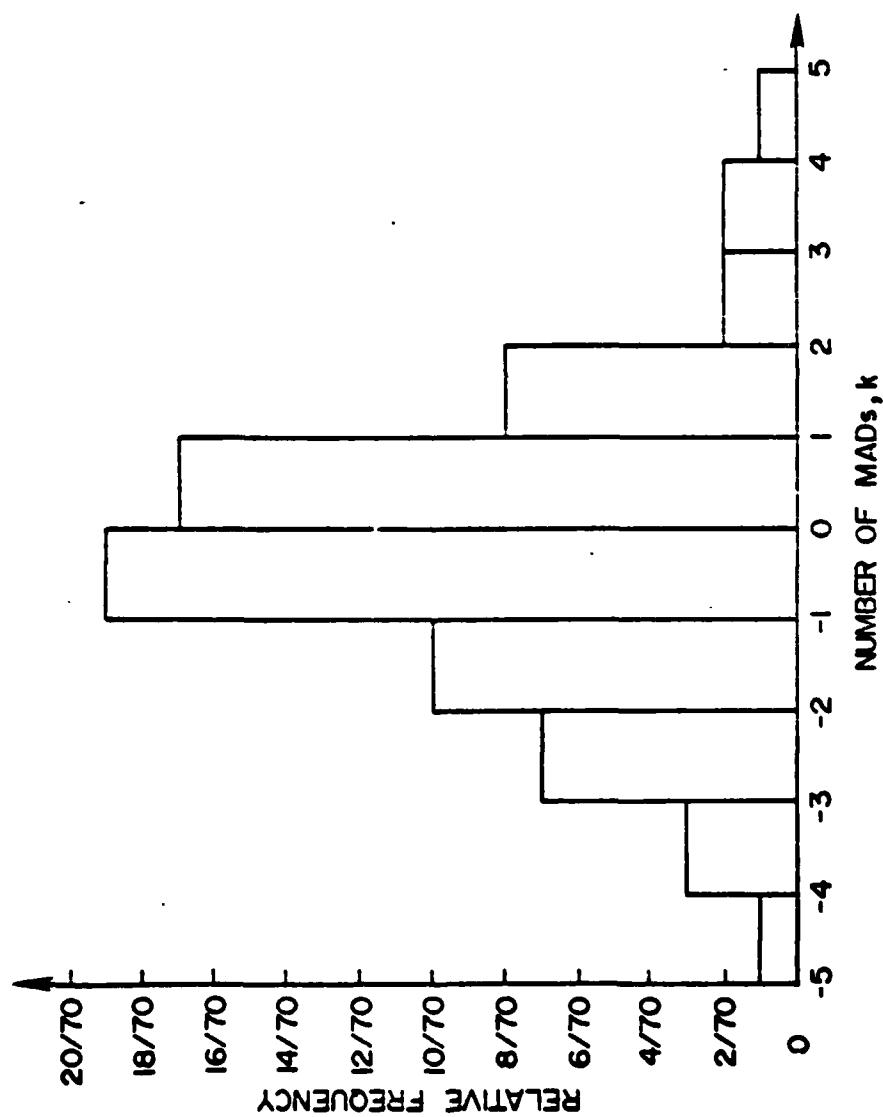


Figure 3.4. The Distribution of Forecast Errors, Z9, for the Same Items when the Linear Trends are Taken Out. (Class 4 is not considered because the pattern of the first eight periods changes abruptly)

4. ABC ANALYSIS

Because of the large number of items in the inventory, it is sometimes convenient to classify them according to the annual dollars of usage; and even though we are dealing only with high intensity items, it would still be useful to classify these. For the fifty-six items in the sample, we find that the total annual usage is \$4,868,000, comprising about 155,000 units of demand. Of these 9.78% account for 54.34% of the annual dollars. We call these Class A items because they should receive the most attention. We similarly see that 25.64% of the number of units account for only 9.58% of the annual dollars. We call these Class C items because managing them can be kept as simple as possible. Between A and C, we have Class B items. For our sample, these comprise 64.58% of the number of units but account for 36.08% of the annual dollars. These results are taken from Table 4.1, and although arbitrary, the classification is consistent with the ABC classification scheme advocated in the literature. See, for example, Brown (1967, pp. 23-24) and Peterson and Silver (1979, pp. 71-73). The ABC classification is also consistent with the Supply Management Grouping Code (SMGC), even though the latter does not appear to be as useful. If we inspect Table 4.1, for example, we see that SMGC code M accounts for 79.46% of the annual dollars but 32.51% of the annual units; SMGC Code P accounts for 20.38% of the annual dollars but 66.66% of the annual units; and SMGC Code T accounts for 0.16% of the annual dollars and 0.83% of the annual units. In terms of the span of control, it should be clear that an ABC classification is superior to the SMGC. Furthermore, it would be easy to do tradeoffs between inventory investment and service level using ABC curves as Herron (1976) shows.

TABLE 4.1. ABC CLASSIFICATION FOR 1980 DATA

Item no.	FSN	Annual \$'s	% of Annual \$'s	Cum % \$'s	Annual Units of Demand	% Units	Cum % Units	A items 9.58% units 54.34% \$'s	B items 64.58% units 36.08% \$'s	C items 25.84% units 9.58% \$'s
37	1005007879802	1922543.17	.3949	.3949	7811.5	.0504	.0504			
15	5895001167508	438165.09	.0900	.4849	5583.0	.0360	.0864			
31	3110006999957	284326.89	.0584	.5434	1772.0	.0114	.0978			
21	1095004335657	170607.03	.0350	.5784	4872.5	.0314	.1292			
7	5960004009106	14757.20	.0030	.6092	4630.0	.0299	.1591			
11	583100803563	144364.62	.0297	.6389	5737.0	.0370	.1960			
19	4210002727415	136725.60	.0281	.6669	5126.5	.0330	.2291			
23	1095009120256	127475.67	.0262	.6931	2151.6	.0141	.2432			
10	5895000894003	119067.36	.0245	.7176	643.6	.0041	.2474			
20	3110009429451	65625.10	.0176	.7351	1166.0	.0075	.2549			
24	1270000831481	78162.39	.0161	.7512	1091.0	.0070	.2619			
18	4310010339204	74917.01	.0154	.7666	8717.0	.0562	.3191			
25	1095010133419	68162.24	.0140	.7806	914.0	.0059	.3240			
28	1095008747369	64053.93	.0130	.7946	174.5	.0011	.3251			
43	1005006999223	49262.77	.0101	.8047	240.0	.0018	.3269			
47	1005003357318	47986.84	.0099	.8146	1534.0	.0094	.3368			
45	1005006999482	46970.71	.0096	.8242	12102.5	.0740	.4144			
27	1095009120243	45314.63	.0093	.8335	5664.0	.0366	.4514			
53	1560009492087	44964.01	.0092	.8427	5373.5	.0346	.4861			
42	1005007016793	44855.47	.0092	.8519	582.5	.0038	.4898			
32	1095000491447	39575.11	.0081	.8601	1072.6	.0069	.4967			
46	1005000511579	39527.64	.0081	.8682	3843.5	.0248	.5215			
12	5821002694508	39247.20	.0081	.8762	13461.0	.0868	.6083			
54	1560007803454	38237.76	.0079	.8841	916.0	.0059	.6142			
17	44400065749186	33322.18	.0068	.8909	14881.5	.1217	.7359			
6	5845009497160	32925.64	.0067	.8977	387.0	.0025	.7384			
35	1005008935230	31919.37	.0066	.9042	792.2	.0051	.7436			
2	5841000736392	29768.72	.0061	.9104	1782.0	.0115	.7551			
26	1095009553210	28340.64	.0058	.9162	660.0	.0043	.7593			
57	1560006117049	26955.40	.0055	.9217	371.5	.0024	.7617			
29	1095008614744	26863.98	.0055	.9272	504.0	.0033	.7650			
40	100500745267	26617.64	.0055	.9327	276.0	.0018	.7668			
50	7045004479020	26595.52	.0055	.9382	4487.0	.0289	.7957			
1	5826000146411	24803.10	.0051	.9433	381.0	.0025	.7982			
22	5365007355943	24077.00	.0050	.9483	2022.5	.0130	.8112			
48	1005000178809	24059.48	.0049	.9532	940.5	.0061	.8173			
59	1560004390187	23145.96	.0048	.9580	351.5	.0023	.8195			
51	3040006211345	20288.91	.0042	.9622	1546.9	.0100	.8295			
61	1440005227651	19964.06	.0041	.9663	2983.6	.0192	.8487			
55	1560006244732	18934.43	.0039	.9702	204.0	.0013	.8500			
34	1095001111640	18432.57	.0038	.9734	1047.5	.0068	.8569			
44	1005006999431	16609.29	.0035	.9774	860.5	.0055	.8623			
13	5821009908461	12294.49	.0025	.9799	2444.5	.0183	.8807			
30	1095005227703	11875.39	.0024	.9824	1638.8	.0106	.8913			
9	583500451349	11098.84	.0023	.9846	301.0	.0019	.8932			
60	1560003101191	10449.05	.0021	.9868	530.5	.0034	.8966			
58	1560006099968	9685.45	.0020	.9888	1307.0	.0084	.9050			
36	1005007889718	8336.04	.0017	.9905	353.0	.0023	.9073			
31	1095005158069	8105.73	.0017	.9922	1456.6	.0096	.9167			
38	100500755574	7920.95	.0016	.9938	1884.5	.0122	.9289			
39	1005007545273	6599.79	.0014	.9951	6773.0	.0437	.9726			
56	1560006720537	5044.80	.0012	.9963	820.6	.0053	.9779			
41	1005007545266	5215.91	.0011	.9974	699.5	.0045	.9824			
62	2530008264648	5114.80	.0011	.9984	1449.0	.0093	.9917			
52	1670007970253	4655.28	.0010	.9994	489.0	.0032	.9949			
3	5962004537739	3093.59	.0006	1.0000	797.5	.0051	1.0000			
		\$4,867,959.50			155,098.2					

THIS TABLE IS A QUALITY MANAGEMENT
FROM DATA ANALYSIS TO DPO

In Figure 4.1 is plotted the cumulative percentage of items along the horizontal axis versus the cumulative percentage of total dollar usage along the vertical axis. Figure 4.1 makes it more convenient to reclassify, if necessary.

According to Brown (1967, p. 23), the distribution of annual dollars of demand is lognormal. This is indeed the case for our data. The Lilliefors (L) test of lognormality yields a $D_{\max} = 0.1097$, less than the critical statistic, $L_{0.95} = 0.886/\sqrt{56} = 0.1184$. Hence we accept the hypothesis of lognormality for the annual dollars of demand. The fit to lognormality is, in fact, quite good. (The parameters of the lognormal are $\mu = 10.369$ and $\sigma = 1.213$.)

In a similar vein, we also fit the number of annual units demanded to the lognormal distribution. This yields $D_{\max} = 0.0890$, as compared to the critical $L_{0.95} = 0.1184$. Thus we also accept the hypothesis of lognormality for the number of items demanded. (The parameters of this lognormal are $\mu = 7.263$ and $\sigma = 1.157$.)

The 1980 Data

The data used to generate the Figure 4.1 were obtained from LORRA on May 23, 1980. In inspecting these data, it became clear that the sample of sixty-two we originally used has now been reduced to one of fifty-six items. This was because five of the items were no longer high-intensity, and one item was inadvertently duplicated in the original sample.

For the sake of future research and in order that our results may be replicated, we organize the data received on May 23, 1980 in Tables 4.2 and 4.3. These tables account for fifty-six items only; we have kept the original item numbers reflecting the listing in the Phase I and Phase II reports.

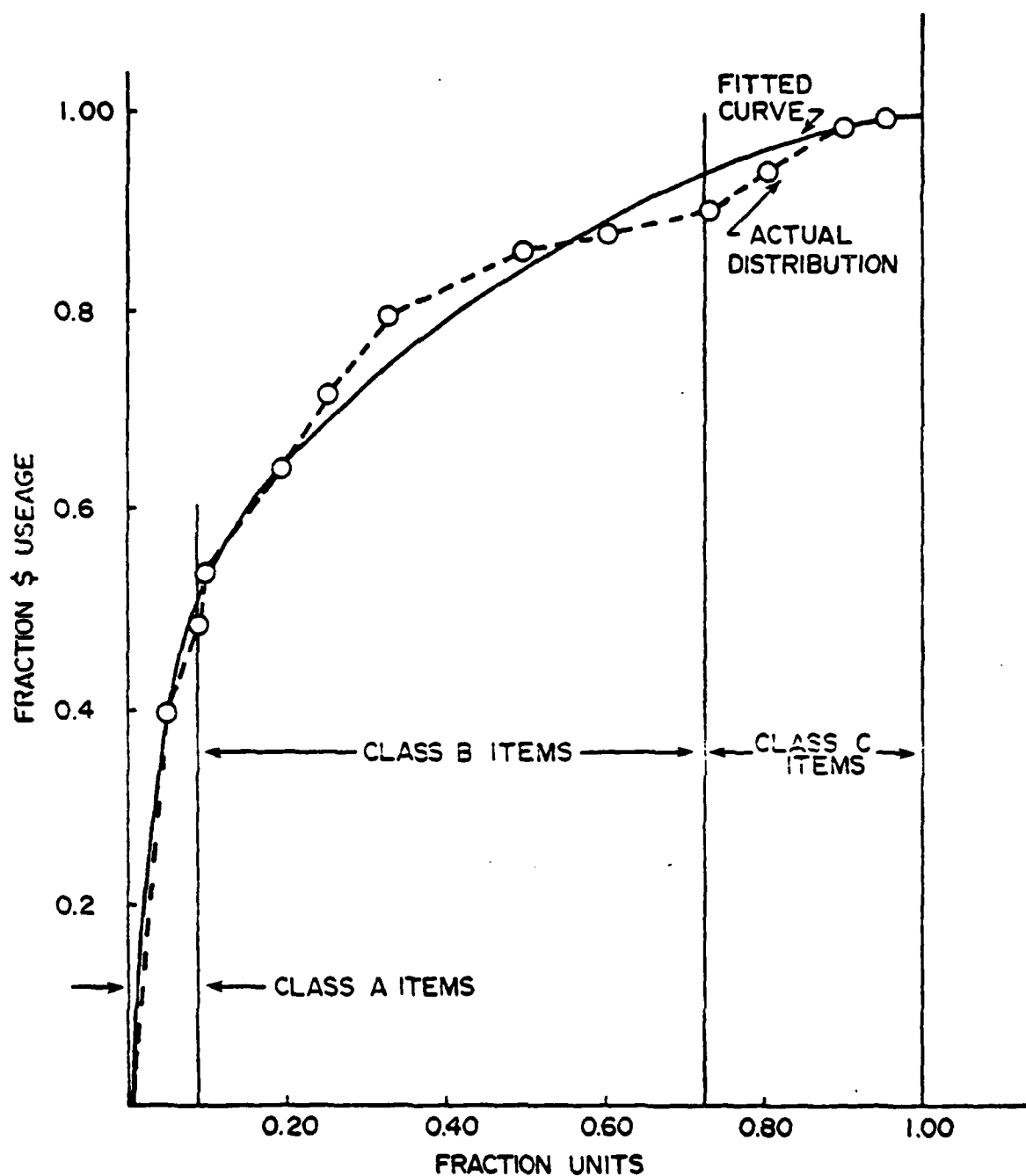


Figure 4.1. ABC Classification of the Sample Items--1980 Data

Source: Table 4.1

TABLE 4.2. DATA OF MAY 23, 1980 BY FSN

20

Item #	FSN	Monthly Demand	Quarterly MAD	Unit Price
46	1005000175504	650.46	443.60	3.08
47	1005000511575	465.25	423.06	7.08
48	1005005357314	147.67	128.75	27.08
49	1005005494442	405.04	371.94	9.64
50	1005005494424	345.43	215.00	10.64
51	1005005494431	478.08	201.25	2.93
52	1005007015743	427.04	109.84	8.72
53	1005007545266	182.63	124.40	2.38
54	1005007545267	53.63	73.07	41.36
55	1005007545243	47.17	85.38	5.66
56	1005007755574	90.42	102.25	7.26
57	1005007874602	726.42	666.50	220.55
58	1005007844713	75.17	82.26	9.12
59	1005004934230	14.54	19.88	182.44
60	1045001111640	23.33	14.75	65.84
61	1045004335557	127.83	68.25	111.22
62	1045004914447	1003.54	1082.13	3.27
63	1045005164064	472.42	244.32	1.43
64	1045005227763	447.74	344.53	2.21
65	1045005414744	43.74	39.72	46.12
66	1045005747364	44.35	135.66	63.45
67	1045005123243	320.29	351.44	11.79
68	1045005123266	1121.75	671.06	4.47
69	1045005455610	75.33	66.00	30.93
70	1045005133414	1573.46	525.47	3.61
71	1045005454141	32.25	19.25	201.97
72	10450054572761	71.71	37.16	23.20
73	10450053101141	157.46	83.47	5.53
74	1045005443147	25.04	24.50	77.04
75	1045005404444	304.42	320.75	1.43
76	1045005411766	66.56	37.04	32.45
77	1045005444432	66.29	45.67	6.07
78	1045005444432	120.75	74.75	13.07
79	1045005444434	24.42	28.07	105.31
80	1045005444437	121.34	43.66	30.87
81	1045005444438	40.75	136.13	9.52
82	1045005444439	66.25	70.14	6.44
83	1045005444440	66.46	30.03	25.44
84	1045005444441	44.21	22.34	435.44
85	1045005444442	144.75	172.44	48.05
86	1045005444443	55.00	64.50	207.16
87	1045005444444	33.46	26.13	201.65
88	1045005444445	42.33	32.25	65.60
89	1045005444446	104.42	70.25	18.75
90	1045005444447	23.00	25.75	142.20
91	1045005444448	373.42	540.75	2.74
92	1045005444449	31.75	14.55	65.10
93	1045005444450	155.54	64.13	71.38
94	1045005444451	75.38	63.88	31.65
95	1045005444452	29.29	29.04	338.76
96	1045005444453	124.91	114.13	263.25
97	1045005444454	248.53	240.40	3.72
98	1045005444455	17.00	17.75	160.91
99	1045005444456	145.67	114.75	41.38
100	1045005444457	237.04	213.55	1.07
101	1045005444458	67.29	115.06	25.39

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FROM THE NATIONAL ARCHIVES

Table 4.3. DATA OF MAY 23, 1980 BY ITEM NUMBER 21

Item #	FSN	Monthly Demand	Quarterly MAD	Unit Price
1	5826000146411	31.75	14.56	65.10
2	5841000738392	78.38	63.88	31.65
3	5962004537739	237.04	219.85	1.07
7	5960004009105	136.57	114.75	91.38
8	5895009497160	17.00	17.75	160.91
9	5895004451349	248.63	240.40	3.72
10	5895000894403	29.29	29.09	338.76
11	5831008903563	168.54	68.13	71.38
12	5821002694508	23.00	25.50	142.20
13	5821009906461	373.92	540.75	2.74
15	5895001167508	128.91	118.13	283.25
17	4440005749186	42.33	32.25	65.60
18	4310010339204	30.96	26.13	201.65
19	4210002727815	55.00	88.50	207.16
20	3110009429451	148.50	172.88	48.05
21	3110006999957	44.21	22.38	535.94
22	5365007355943	108.92	70.25	18.75
23	1095009120256	1121.75	671.06	9.47
24	1270000831981	32.25	19.25	201.97
25	1095010133419	1573.46	525.47	3.61
26	1095009553210	76.33	66.00	30.33
27	1095009120243	320.29	351.99	11.79
28	1095009747369	99.38	136.66	63.46
29	1095008614744	48.54	39.72	46.12
30	1095005227703	447.79	344.53	2.21
31	1095005168069	472.42	299.32	1.43
32	1095004918497	1008.54	1082.13	3.27
33	1095004335657	127.83	68.25	111.22
34	1095001111640	23.33	14.75	65.94
35	1005008238230	14.54	19.98	182.94
36	1005007869718	76.17	82.26	3.12
37	1005007872892	726.42	666.50	220.55
38	1005007766579	90.92	102.25	7.26
39	1005007545293	97.17	85.38	6.66
40	1005007545267	63.63	73.07	41.36
41	1005007545266	182.63	124.40	2.32
42	1005007016793	427.04	109.89	3.72
43	1005006999923	395.83	215.00	10.64
44	1005006999931	479.08	201.25	2.33
45	1005006999922	406.04	371.94	9.64
46	1005000511573	465.25	923.06	7.09
47	1005003357313	147.67	128.75	27.06
48	1005000179809	650.96	483.60	3.09
50	7045009479020	97.29	115.06	25.39
51	3040006211345	66.46	30.03	25.44
52	1670007970253	40.75	136.13	9.52
53	1560009492087	121.38	53.89	30.87
54	1560007803854	29.42	29.07	109.31
55	1560006284732	120.75	74.75	13.07
56	1560006220532	58.29	45.88	8.07
57	1560006117049	68.38	37.09	32.95
58	1560006099969	564.42	320.75	1.43
59	1560004320187	25.09	24.50	77.04
60	1560003161191	157.46	82.47	6.53
61	1440005727651	71.71	37.16	23.00
62	2530004260468	66.25	70.19	6.44

Table 4.2 lists the items by ascending order of stock number; Table 4.3 lists these items by ascending order of item number. Note in Table 4.3 that these items were deleted: item 4 (FSN 302101866582JH: Latch), 5 (FSN 1560005722616JH: Rod Assembly), 6 (FSN 5305001117850AB: Screw Spec), 14 (FSN 589500172114: Antenna), 16 (FSN 7045008479020), and 49 (FSN 4935006506352AB: Cable Assys - 2). Item 16 is in fact item 50 (FSN 7045008479020); the other items are no longer high-intensity.

The 1977-78 Data

We had, prior to obtaining the 1980 data, played detective with 1977-78 order quantities and unit prices originally provided with leadtime data. We thus generated the annual units demanded as well as the dollar values of demand for 1977-78. For the sake of comparison with 1980 data, we provide Table 4.4 and Figure 4.2. Table 4.4 is the analogue of Table 4.1, and Figure 4.2 is the analogue of Figure 4.1. In Table 4.4, we see that 5.68% of the top units account for 63.09% of the dollars; 56.8% of the intermediate units account for 34.79% of the dollars; and 37.52% of the bottom units account for only 2.12% of the dollars. In 1977-78, the sample accounted for an annual usage of \$6,940,000 and comprised 399,528 units of demand. Thus, the demand for these items has fallen, on the average, between 1977 and 1980. An item-by-item comparison, using Tables 4.1 and 4.4, shows that a majority have declined in demand, but that for a few, demand has sharply increased. This is consistent with our conjectures in Section 3.

The distribution of annual dollars of demand in Table 4.4 is also lognormal. The Lilliefors (L) test of lognormality yields a $D_{\max}$ of 0.07017. This is much less than the critical statistic $L_{0.95} = 0.886/\sqrt{62} = 0.1125$. Hence we accept the hypothesis of lognormality, the parameters of the

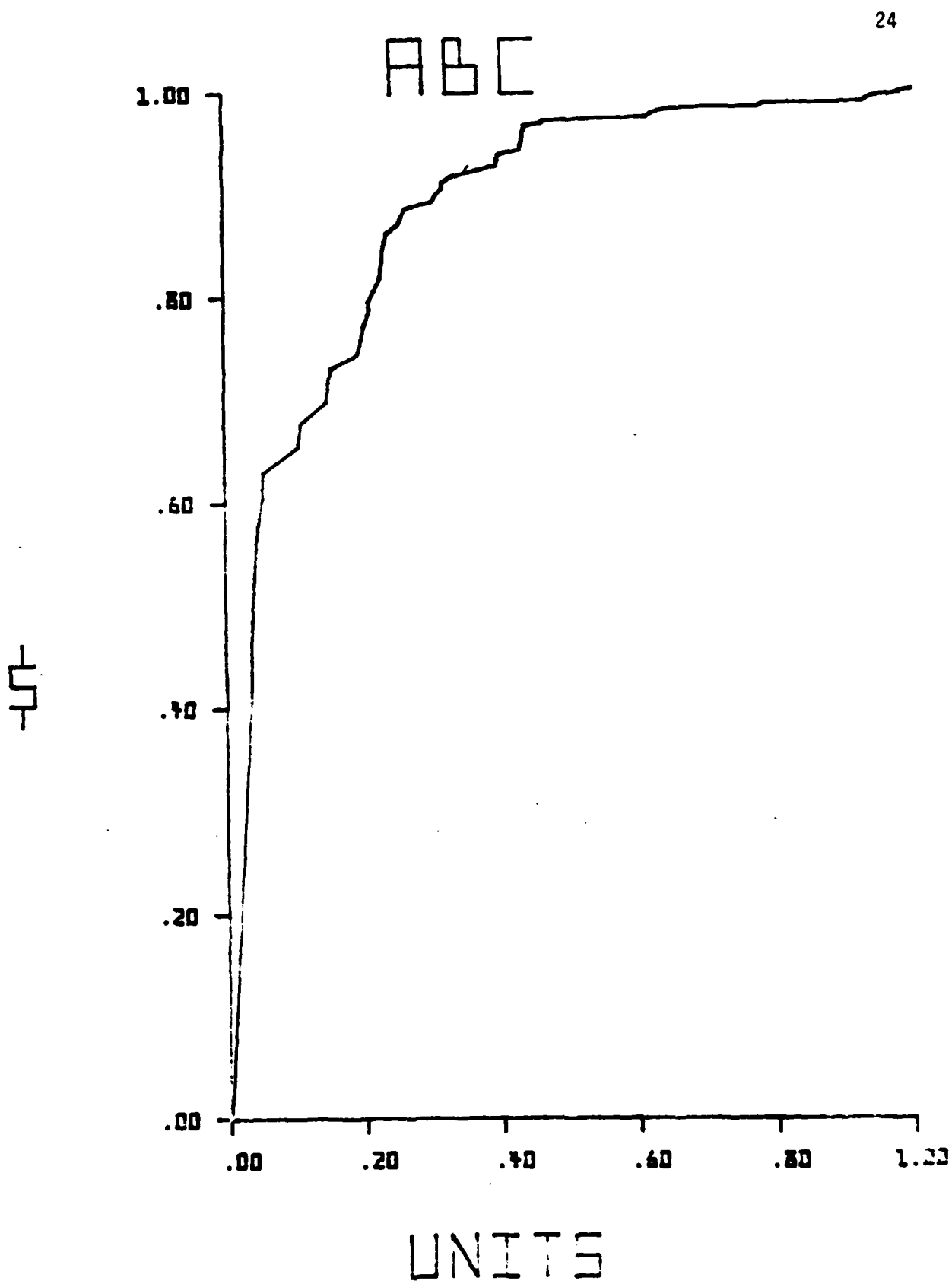


Figure 4.2. ABC Classification of the Sample Items--1977-73 Data
Source: Table 4.4

lognormal being $\mu = 10.595$ and $\sigma = 1.210$. Furthermore, the number of annual units demanded is also lognormal with parameters $\mu = 7.717$ and $\sigma = 1.407$. The L test yields a $D_{\max}$ of 0.1097, less than the critical $L_{0.95} = 0.1125$.

It should be observed that the analysis of the 1977-78 imputed data is based on the original sample of size sixty-two which contains one redundant item (#16) and five items (#4, 5, 6, 14, and 49) that are no longer high-intensity. Since item 16 plays a very minor role, the effect of its presence is negligible.

5. THE DISTRIBUTION OF LEADTIME DEMAND

We may think of leadtime demand as a random sum of demands that are independently and identically distributed. Thus leadtime demand may be written as

$$X = D_1 + D_2 + \dots + D_i + \dots + D_L, \quad i = 1, 2, \dots, L, \quad (5.1)$$

where D and L are random variables denoting demand and leadtime. Thus leadtime demand, X , may be thought of as a mixture, while leadtime, L , is the mixing distribution. More specifically, $f(X)$ may be said to be a compound distribution with $G(L)$ being the compounding distribution (Ord, 1972, pp. 64-66).

It can be shown (Drake, pp. 109-112) that for the structure (5.1)

$$E(X) = E(L) \cdot E(D), \quad (5.2)$$

and

$$V^*(X) = E(L) \cdot V(D) + [E(D)]^2 \cdot V(L), \quad (5.3)$$

the star denoting the variance of leadtime demand with variable leadtime.

If, on the other hand, leadtime is constant at L , then $E(X)$ would be as in (5.2) but

$$V(X) = E(L) \cdot V(D). \quad (5.4)$$

We can immediately see the influence on safety stocks if we begin to consider the variability of leadtime. For the same safety factor, k , this increase would be in the ratio

$$\begin{aligned}
\frac{\sigma^*(X)}{\sigma(X)} &= \left(\frac{E(L) V(D) + [E(D)]^2 V(L)}{E(L) V(D)} \right)^{1/2} \\
&= \left(1 + \frac{VMR(L)}{VMR(D)} \cdot E(D) \right)^{1/2}, \text{ where VMR denotes the } (5.5) \\
&\quad \text{variance to mean ratio} \\
&\approx \sigma(L) \left(\frac{E(D)}{E(L)} \right)^{1/2}, \text{ for } VMR(D) = 1 \text{ and large } VMR(L).
\end{aligned}$$

A similar analysis appears in Appendix G of the Phase II report (Hayya, March 31, 1980, pp. 88-94). An explicit treatment of the impact on safety stocks will be considered in the next section.

Theory of Compound Distributions

It would be easy if compound distributions were readily recognizable: sometimes they are, sometimes they are not. Hadley and Whitin (1963, p. 117) have shown that where the procurement leadtime is gamma-distributed with parameters α , β , and if a Poisson process with mean λt generates demands with units being demanded one at a time, then the distribution of leadtime demand is a negative binomial with parameters $\alpha + 1$, $\beta/(\beta + \lambda)$. Burgin (March 1972) has treated the case with demand normal and leadtime gamma. There is other work (for example: Sherbrooke, 1968; Ord, 1972; Bott, 1977), but the leadtime distributions are too complex for our present purposes.

In the absence of data on daily demands, the assumption of Poisson demands may be appropriate. Furthermore, the fitting of statistical distributions to leadtime data supports the notion that leadtime is gamma-distributed. Consequently, we can assume that leadtime demand is a negative binomial. Better yet, we can use simulation in order to see whether we can fit the distribution of leadtime demand for our items to the normal or the Laplace. Particularly, if we can fit the distribution of leadtime demand to the Laplace, we can take advantage of the models developed for the Air Force by Presutti and Trepp (June 1970)

Simulation Experiment 1: Poisson Demands; Best Fit
for Leadtime--1977-78 Demands

We had no demand distribution data at the writing of this report; and until May 25, 1980, we had no 1980 daily demand data. Consequently we made the assumption that daily demand at the depot is Poisson-distributed, and, at the beginning, we estimated mean daily demand by averaging the quantities ordered over the two most recent years of data: 1977 and 1978. Then we estimated the annual dollars of demand. These ranged from \$6,000 for item no. 3 (Integrated, FSN: 5962004537739) to \$2,825,000 for item no. 37 (20 mm GunBa, FSN: 1005007879802). On the other hand, the standard deviation of leadtime demand, σ_i^* , ranged from 29.33 for item no. 12 (Antenna, FSN: 5821002694508) to 15,385.47 for item no. 23 (PAD-ASSY 1, FSN: 1095009120256). We could see by inspection that dollar value of demand and σ_i^* are hardly related. A calculation of the linear correlation coefficient yields $r = 0.256$, barely significant at the 0.05 level (the calculated value of the test statistic is $t(60) = 2.055$). It may, however, be possible to fit an exponential function to the two variables.

A cross-tabulation of annual dollars of demand versus σ_i^* produces the frequencies given in Figure 5.1. From the cross-tabulation in Figure 5.1, we choose five items for a simulation experiment. These are:

<u>Item no.</u>	<u>Noun: FSN</u>	<u>σ_i^*</u>	<u>Annual \$'s</u>
23	Pad Assy-1: 1095009120256	Very high (15,385)	High (\$173,000)
37	20 mm. Gun Ba: 1005007879802	High (7,423)	Extremely high (\$2,825,000)
39	Guide Rolle: 1005007545293	Low (384)	Very low (\$11,000)
50	Lead Tape: 7045008479020	Very high (10,530)	Very low (\$16,000)
53	Adapter: 15600094987JH	Moderate (1346)	Moderate (\$79,000)

Standard Deviation of Leadtime Demand, $\sigma_i^*(x)$	Annual \$'s (in thousands)						Totals
	Very low 6 - 20	Low 20 - 50	Moderate 50 - 100	High 100 - 200	Very high 200 - 600	Extremely high >600	
Very low (30-200)	//	///	////	///			18
Low (200-800)	/// item #39	///	////		///		18
Moderate (800-2000)	///	///	//// item #50	/			13
High (2,000-10,000)	///	///	///	///		/ item #37	11
Very high (10,000-16,000)	1 item #50			1 item #23			2
Totals	19	18	14	7	3	1	62

Figure 5.1. A Two-Way Classification of Annual Dollars Versus the Standard Deviation of Leadtime Demand--1977-78 Data

The best fit for the leadtimes and corresponding parameters is given in Table 5.1. Table 5.2 gives the mean and variances of leadtime demand. With Poisson demands and with leadtimes as described in Table 5.1, we generate by simulation distributions of leadtime demand, using samples of size $n = 30$ and $n = 100$. We then fit these distributions to the normal and to the Laplace. The results are given in Table 5.3: we see in that table that we are not successful in fitting the normal or the Laplace for the entire distribution of leadtime demand; we are, however, quite successful in fitting the normal and the Laplace to the right half of the distribution of leadtime demand, that is, for $k > 0$.

Simulation Experiment 2: Poisson Demands; Best fit
for Leadtime--1980 Demands

Since demands declined in general from 1977 to 1980, we verified the results of the previous simulation using 1980 demands. Using samples of size $n = 30$, we again simulate daily Poisson demands and the leadtime distributions given in Table 5.1.

The means and variances of leadtime demand, using 1980 data, are given in Table 5.4; it is the analogue of Table 5.2. The goodness-of-fit of the 1980 leadtime data (actually 1980 demands and 1975-78 leadtimes) to the normal and the Laplace are also verified as seen in Table 5.5. It is seen in Table 5.5 that the fit is better in the right tail of the distribution; the fit improves dramatically beyond $k = 1$. This is what we are looking for.

TABLE 5.1
BEST FIT FOR LEADTIME

<u>Item no. FSN</u>	<u>Best Fit</u>	<u>Parameters</u>
23: 1095009120256 (Pad Assy-1)	Normal	$\mu = 384.57; \sigma = 272.00$
37: 1005007879802 (20 mm. Gun Ba)	Gamma	$\alpha = 6.09; \beta = 75.19$
39: 1005007545293 (Guide Rolle)	Lognormal	$\mu = 4.90; \sigma = 0.41$
50: 7045008479020 (Lead tape)	Gamma	$\alpha = 5.63; \beta = 26.60$
53: 1560009492087JH (Adapter)	Gamma	$\alpha = 3.40; \beta = 91.74$

TABLE 5.2
MEANS AND VARIANCES OF LEADTIME DEMAND: 1977-78 DEMAND DATA

Item No.	1977-80 Expected Daily Demand $E(D_i)$	Expected Leadtime in Days $E(L_i)$	Variance Leadtime in Days $V(L_i)$	Expected Leadtime Demand $E(X)$	Variance & St. Dev. Leadtime Demand $V(X); \sigma(X)$
23 (Pad Assy-1) FSN: 1095009120256	56.6 (37.4)*	384.6	73984	21,752.	236,712,811; 15,385.5
37 (20 mm. Gun Ba) FSN: 1005007879802	39.9 (24.2)*	459.3	34615	18,323	55,109,982; 7423.6
39 (Guide Rolle) FSN: 1005007545293	6.3 (3.2)*	145.3	3698	915.5	147,747; 384.4
50 (Lead tape) FSN: 7045008479020	166.7 (2.9)*	149.6	3977	24,982	110,876,427; 10,530
53 (Adapter) FSN: 1560009492087JH	7.9 (4.1)*	312.1	28690	2,478	1,810,423; 1345.5

() * represents 1980 demand data

TABLE 5.3
GOODNESS OF FIT OF LEADTIME DEMAND TO THE NORMAL
AND THE LAPLACE--1977-78 DATA

Item No: FSN	Sample Size	Entire Distribution		Right Half	
		Normal D_{max}	Laplace D_{max}	Normal D_{max}	Laplace D_{max}
23: 1095009120256 (Leadtime normal)	30 100	0.1568 0.0998	0.1143 0.1403*	0.0938 0.0800	0.1143 0.1403**
37: 1005007879802 (Leadtime gamma)	30 100	0.0784 0.0743	0.1326 0.1363*	0.0784 0.0742	0.1001 0.0688
39: 1005007545293 (Leadtime lognormal)	30 100	0.1900 0.0858	0.1941 0.1117	0.1190 0.0858	0.0759 0.0755
50: 7045008479020 (Leadtime gamma)	30 100	0.2171 0.1416*	0.2791* 0.1851	0.1683 0.0901	0.1181 0.1015
53: 1560009492087 (Leadtime gamma)	30 100	0.0955 0.1745*	0.1450 0.2283*	0.0531 0.1311	0.0715 0.0955

¹ From the Table of the Kolmogorov-Smirnov Statistic, two-sided test, the 0.95 critical value for $n=30$ is 0.242, that for $n=100$ is 0.136 (Conover, 1971, p. 397).

* Reject the hypothesis of good fit at the ninety-five percent significance level.

** at $k = 0.37$; beyond that, the fit is quite good.

TABLE 5.4
MEANS AND VARIANCES OF LEADTIME DEMAND:
1980 DATA

<u>Item no.</u>	<u>Expected Daily Demand $E(D_i)$</u>	<u>Expected Leadtime in Days $E(L_i)$</u>	<u>Expected Leadtime Demand $E(X)$</u>	<u>Variance and Standard Deviation of Leadtime Demand $V(X); \sigma(X)$</u>
23	37.4	384.6	14,384.04	103,500,305.7; 10,173.51
37	24.2	459.3	11,115.06	20,283,043.47; 4503.67
39	3.2	145.3	464.96	27,486.32; 195.79
50	2.9	149.6	433.84	33,881.76; 184.07
53	4.1	312.1	1,279.61	434,781.98; 659.38

TABLE 5.5
FIT OF LEADTIME DEMAND TO THE NORMAL AND THE LAPLACE

Item No.	Sample Size	k	Entire Distribution		k	Right Tail	
			Normal $D_{\max}$	Laplace $D_{\max}$		Normal $D_{\max}$	Laplace $D_{\max}$
23	30	$-\infty$ to $+\infty$	0.1594	0.1174	0 to $+\infty$	0.0986	0.1174
					1.00 to $+\infty$	0.0986	0.1174
					1.64 to $+\infty$	0.0173	0.0241
37	30	$-\infty$ to $+\infty$	0.1596	0.1877	0 to $+\infty$	0.0731	0.1163
					1.00 to $+\infty$	0.0608	0.0799
					1.64 to $+\infty$	0.0324	0.0271
39	30	$-\infty$ to $+\infty$	0.1686	0.1893	0 to $+\infty$	0.1471	0.1143
					1.00 to $+\infty$	0.0349	0.0562
					1.64 to $+\infty$	0.0329	0.0290
50	30	$-\infty$ to $+\infty$	0.2089	0.2547*	0 to $+\infty$	0.1876	0.1661
					1.00 to $+\infty$	0.0646	0.0731
					1.64 to $+\infty$	0.0646	0.0580
53	30	$-\infty$ to $+\infty$	0.1510	0.1946	0 to $+\infty$	0.1510	0.1946
					1.00 to $+\infty$	0.1155	0.1504
					1.64 to $+\infty$	0.0938	0.0916

¹ From the Table of the Kolmogorov-Smirnov Statistic, two-sided test, the 0.95 significance level for $n=30$ is 0.242 (Conover, 1971, p. 397).

* Reject the hypothesis of good fit at the ninety-five percent significance level.

6. COST-BENEFIT ANALYSIS

In doing the cost-benefit analysis, we compare the current system at AFLC with an optimal system. Because of arguments presented in the previous section, we choose the Presutti-Trepp Model IV (1970, pp. 248-249) as the optimal system. One simulation, using 1980 data and with $\lambda = 660$, $Z_i = 0.5$, $a_i = 0.23$, is presented in Table 6.1, which is sorted by FSN for convenience. And based on the same parameters and upon an understanding of the present procedures at LORRA, Table 6.2 presents a description of the current system. How each column in these tables is calculated may be respectively seen in Appendices B and C of this report.

The question concerning the mix of items at an ALC and how that mix would change is answered by comparing the corresponding columns in Tables 6.1 and 6.2. The mix will change.

It may be worthwhile to compare the current system with the equivalent optimal system. This comparison is presented in Table 6.3 in terms of several attributes: service level, number of backorders, fill ratio, value of safety stock, and so on.

It may also be worthwhile to study the behavior of the optimal system for different shortage factors, λ_i , and different item essentiality, Z_i . Table 6.4 presents this behavior for $Z_i = 0.5$ and for $\lambda = 660, 600, 500, 400, 300, 200$. Table 6.5 gives a similar comparison for $Z_i = 1$.

From Tables 6.4 and 6.5 we produce the exchange curves in Figures 6.1 and 6.2. These exchange curves should give an idea of the additional investment in safety stock required to reduce the number of backorders or to improve the service levels. The reader should keep in mind that these tables and exchange curves are based on a sample of size $n = 56$. This sample represents

TABLE 6.1. OPTIMAL SYSTEM

(1) Item #	(2) ISN	(3) Daily Demand	(4) Mean Lead time Days	(5) Variance Lead time	(6) Mean Lead time Demand	(7) Variance Lead time Demand	(8) Std. Dev. Lead time Demand $\sigma^*(K)$	(9) Unit Cost c_i	(10) The Wilson EOQ Q_w	(11) Optimal EOQ Q^*	(12) Optimal Safety factor k_i
43	1005000178809	21.70	183.25	535.00	1976	255370	505.84	3.08	3118.9	3497.0	2.247
44	1005000178809	15.51	215.50	5305.67	1342	1279499	1111.11	7.08	1710.1	2710.0	2.378
45	1005000178809	4.92	411.40	5111.07	2025	1259497	1122.41	27.08	501.0	1732.2	1.681
46	1005000178809	13.53	300.48	4445.21	4072	8416782	2974.39	4.64	1392.3	4632.0	2.407
47	1005000178809	12.86	251.70	1834.99	3237	1041599	1744.49	10.64	1291.9	3019.8	2.281
48	1005000178809	15.94	276.33	4074.44	4404	1140379	1086.31	2.93	2229.0	3125.8	2.485
49	1005000178809	14.23	289.17	6582.08	4116	1337414	1156.64	8.12	1531.3	2527.5	2.288
50	1005000178809	1.09	171.99	4397.16	1077	149340	591.05	2.19	1528.6	2002.6	2.923
51	1005000178809	1.79	367.50	2785.81	657	93677	299.46	41.16	244.3	535.0	1.303
52	1005000178809	1.24	145.29	1697.06	471	19265	194.15	5.66	721.0	876.6	2.126
53	1005000178809	1.03	293.00	1692.46	888	156687	195.84	7.26	617.5	957.9	2.354
54	1005000178809	24.21	459.29	34614.60	11121	20306279	4506.25	220.55	389.3	6396.5	2.219
55	1005000178809	2.54	184.67	10511.70	474	7259	85.20	9.12	504.3	568.1	1.500
56	1005000178809	4.8	203.00	10310.37	98	2520	182.94	105.6	60.5	105.6	1.158
57	1005000178809	7.8	235.33	24339.12	181	14902	122.08	65.84	103.9	221.4	1.966
58	1005000178809	4.26	201.50	875.57	859	16756	129.44	111.22	230.0	339.1	1.375
59	1005000178809	33.62	253.00	8508.22	8505	9624237	3102.10	3.27	3767.6	6553.4	3.001
60	1005000178809	15.75	208.43	5068.60	3282	1359378	1165.92	1.43	3171.7	4101.6	3.257
61	1005000178809	14.63	166.17	5540.76	2525	1218763	1113.00	2.21	2483.9	3392.6	3.046
62	1005000178809	1.62	290.00	2084.44	469	5927	76.99	46.12	220.1	281.2	1.776
63	1005000178809	2.98	272.50	35676.56	812	317048	561.07	63.45	254.6	870.8	1.077
64	1005000178809	10.68	260.00	1255.84	2776	374000	611.47	11.79	1118.2	1631.2	1.950
65	1005000178809	37.39	384.57	71944.00	14380	103854328	10171.24	9.47	2334.9	14753.8	2.455
66	1005000178809	2.54	408.17	146773.27	1039	951195	975.29	30.91	337.0	1657.2	1.603
67	1005000178809	57.45	147.29	2466.12	7225	6791670	2606.08	3.61	4478.9	6685.9	2.812
68	1005000178809	1.07	248.60	3254.70	267	4028	63.47	201.97	85.7	141.6	1.051
69	1005000178809	2.39	289.56	4668.44	692	57077	239.91	23.20	377.2	502.2	1.529
70	1005000178809	5.25	217.29	4399.67	1140	122145	349.78	5.53	931.2	1210.8	2.312
71	1005000178809	1.84	270.13	5521.98	226	4085	63.91	77.04	122.4	175.7	1.601
72	1005000178809	18.41	179.17	1058.20	3371	377949	614.77	1.43	3466.9	3928.7	2.840
73	1005000178809	2.28	307.17	7440.79	700	34548	198.39	32.85	309.5	480.1	1.287
74	1005000178809	1.94	209.86	7637.01	408	29249	171.00	8.07	469.0	605.2	2.030
75	1005000178809	4.02	139.57	14570.90	562	236620	486.44	13.07	530.4	976.1	2.052
76	1005000178809	5.98	254.50	1423.29	250	2003	44.76	108.31	111.8	147.8	1.240
77	1005000178809	4.05	312.14	20609.54	1263	470915	686.21	10.87	425.4	1130.5	1.554
78	1005000178809	1.16	276.80	8828.44	376	16665	129.09	9.52	361.0	461.7	1.903
79	1005000178809	2.21	147.50	13280.26	436	65200	255.34	6.44	559.7	768.7	2.298
80	1005000178809	2.22	254.33	4900.00	572	24620	156.91	25.44	346.8	475.0	1.323
81	1005000178809	1.47	350.25	5004.15	516	49764	106.69	535.94	61.6	172.9	1.090
82	1005000178809	4.95	332.72	3596.40	1647	14995	122.45	207.16	110.5	227.0	1.413
83	1005000178809	1.83	143.33	4761.28	336	14995	122.45	207.16	110.5	227.0	1.413
84	1005000178809	1.03	463.25	9156.58	474	10230	321.11	65.60	122.3	181.9	1.179
85	1005000178809	1.41	465.72	51524.46	657	143238	187.69	18.75	517.1	666.5	1.431
86	1005000178809	3.63	230.00	2609.17	835	35228	187.69	18.75	517.1	666.5	1.431
87	1005000178809	7.7	154.13	2653.28	118	1678	40.96	142.20	86.3	120.0	1.268
88	1005000178809	12.46	210.18	2152.03	2620	336941	580.47	2.74	2038.5	2889.9	2.661
89	1005000178809	1.06	379.00	4046.23	401	4933	70.24	65.10	149.8	207.5	1.675
90	1005000178809	5.62	275.55	7487.41	1548	2258144	1502.71	71.38	329.7	512.0	1.292
91	1005000178809	2.61	234.17	6041.95	612	41854	204.58	31.65	337.6	512.0	1.292
92	1005000178809	1.98	284.67	1718.06	778	11448	106.99	338.76	63.1	174.2	1.000
93	1005000178809	4.30	261.80	9211.17	1125	17155	134.22	283.25	144.7	619.6	1.036
94	1005000178809	8.29	234.33	9510.15	1942	65151	809.41	3.72	1426.6	2109.5	2.780
95	1005000178809	1.57	248.50	10005.60	141	1611	60.09	160.91	69.7	124.1	1.260
96	1005000178809	4.55	270.10	6240.00	1210	1296256	1138.51	91.38	202.3	1631.8	1.852
97	1005000178809	7.90	378.72	131965.09	2676	8291398	2870.78	1.07	2597.3	5326.4	3.866
98	1005000178809	2.91	149.63	1976.16	415	14102	184.67	25.39	397.8	549.2	1.336
99	1005000178809	430.83	14818.50	1062211.62	110377	177103950	49070.76	7726.22	51665.0	102529.4	86.902
100	1005000178809	7.69	264.62	18968.06	1971	1162571	876.26	66.54	922.6	1830.9	1.552

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TABLE 6.1. OPTIMAL SYSTEM (Continued)

(13) Safety Stock, K ₀	(14) Safety Stock	(15) Service Level	(16) Weighted Backorders B ₁	(17) Fill Ratio	(18) Inventory on Hand I ₀	(19) Ordering Cost Annual	(20) Annual Holding Cost Inventory Position	(21) Annual Operating Cost	(22) Annual No. of Backorders B ₀	(23) FSN	(24) Item #
1134.07	1032.92	.979	.34	.994	8880.66	945.25	4858.80	544.06	16.77	1005000178809	48
2639.26	1933.99	.983	1.97	.995	28675.51	407.33	12031.33	12318.46	27.55	1005000511579	46
1466.29	5100.82	.954	7.49	.981	74940.61	451.21	29755.85	1007.06	33.45	1005003357318	47
1171.30	6937.12	.983	7.08	.993	91399.88	461.97	31065.72	1029.68	32.74	1005006999822	45
1970.52	4233.51	.980	4.57	.993	58493.99	676.26	2151.10	2229.15	14.33	1005006999823	43
3133.98	4142.44	.992	.78	.998	11766.35	515.59	6112.79	6664.18	11.72	1005006999931	44
2615.93	2337.55	.980	2.49	.994	34135.80	894.26	16396.79	1691.06	31.14	1005007016793	42
1727.85	4131.33	.992	.35	.996	6496.33	319.35	2191.20	2402.54	3.64	1005007545266	41
160.27	1611.70	.921	3.05	.971	27658.81	530.53	12507.06	1337.59	18.55	1005007545267	40
421.20	7384.44	.975	.28	.996	4868.80	389.37	1711.63	2119.81	4.60	1005007545293	39
931.99	6766.26	.982	.71	.995	10251.74	132.18	1818.75	4171.13	5.52	1005007755579	38
1078.53	23702.58	.944	244.90	.846	1051202.29	601.08	78132.54	70373.62	1339.95	1005007873802	37
127.70	1165.42	.940	.19	.994	3759.61	464.89	1664.71	2334.22	5.81	1005007883718	36
7.94	1352.51	.900	2.26	.872	11942.36	728.97	6696.96	7424.63	22.25	100500893210	35
117.96	776.34	.873	1.48	.954	15314.99	369.04	6233.80	6602.93	12.85	100500893210	34
46.88	5091.44	.706	3.55	.927	25016.61	1995.41	27480.21	29215.62	118.91	100500893210	33
931.34	1048.20	.993	2.50	.998	41175.32	814.95	15964.16	16678.91	27.58	100500918487	32
3797.92	5030.85	.995	.41	.999	8164.67	403.34	3007.33	3406.47	5.65	100500918487	31
1390.81	7192.84	.993	.61	.998	11244.38	462.20	3164.09	4311.30	8.28	1005009227703	30
592.71	2753.73	.933	.87	.968	9131.02	913.76	7101.88	8315.64	18.72	1005008614744	29
636.60	13494.47	.991	8.80	.956	67236.47	543.59	27055.44	2758.73	47.43	100500877369	28
1124.18	14055.82	.968	1.78	.992	21313.41	1034.24	12971.91	18311.05	31.58	1005009120283	27
2996.66	23614.10	.984	3.74	.992	38674.34	902.42	10376.99	102170.91	88.85	1005009551210	26
1503.17	40455.04	.948	7.43	.978	11350.70	277.24	23692.83	2370.39	19.75	1005009551210	25
1527.17	26451.70	.991	2.32	.997	30516.65	1245.61	15271.74	16319.37	47.51	1005010133419	24
3.35	676.67	.936	3.16	.859	16256.63	1205.09	15359.91	17664.99	54.48	1270000831981	23
305.70	1472.53	.942	1.37	.984	15284.56	651.91	7145.31	7047.22	13.91	1440005727451	61
308.68	4423.00	.987	.88	.997	16256.66	455.41	1249.11	3704.54	7.28	1560003101191	60
1745.97	2991.74	.991	1.21	.946	9923.70	755.62	6240.95	6396.57	16.16	1560004190187	59
255.31	9307.60	.919	1.63	.977	16378.30	503.10	2124.01	2332.11	6.75	1560006099964	58
347.04	2430.62	.972	.34	.994	5244.22	137.76	1962.67	2299.93	3.93	1560006220512	56
928.14	13045.75	.973	1.57	.991	19005.71	431.19	6156.43	6383.62	13.20	1560006284732	55
10.75	1164.27	.944	1.19	.925	9029.43	1053.20	4326.70	979.90	26.65	1560007803954	54
1066.14	23119.30	.944	5.22	.978	50691.63	564.26	20551.80	21120.90	31.34	1560008492087	53
245.42	2318.31	.966	.30	.994	4551.17	407.76	1368.70	2176.46	3.24	1670007970253	52
536.86	3779.29	.981	.41	.996	6759.56	301.82	2084.52	2386.34	3.57	253000264468	62
207.60	5281.31	.923	.94	.994	11371.64	740.52	5952.99	6091.51	14.14	3040006211345	51
326.68	15697.17	.993	7.40	.982	54250.67	1353.73	74272.51	75011.24	104.07	3110006999957	21
17.57	6518.81	.993	3.55	.967	11520.69	1219.65	25372.77	26392.42	55.68	3110009429051	20
18.15	3660.08	.992	6.25	.956	29741.30	1202.38	22592.27	23441.65	95.29	4210002727815	19
333.54	23400.35	.805	5.03	.859	24025.30	900.92	2732.60	28131.52	52.21	4310010319204	18
268.61	5036.50	.934	.87	.954	39167.23	417.28	19312.52	1249.81	23.22	4440005749186	17
5.25	745.92	.983	1.44	.991	11317.22	864.90	6196.81	7361.71	17.08	5365007855943	22
1344.37	4231.57	.988	.19	.998	9644.28	1014.66	5998.25	7012.93	27.35	5821002694508	12
47.40	1045.72	.807	1.13	.955	7644.85	525.89	3408.75	3336.64	8.57	5821009906461	13
1543.89	11020.07	.983	26.43	.950	19160.16	410.12	8268.99	4078.84	17.29	583100803563	11
264.48	8167.65	.920	1.60	.978	16570.37	810.11	8241.61	9051.94	20.75	5841000738352	2
.00	.00	.500	7.19	.805	14509.43	890.13	28439.99	29310.12	68.70	5895001167508	15
15.10	4276.05	.525	28.91	.803	10840.43	1101.20	9435.04	9555.24	30.53	5895004451349	9
2250.97	8313.75	.990	.70	.997	12100.90	412.74	4014.55	4302.29	7.74	5895004451349	8
15.60	2510.70	.654	2.14	.888	11265.57	724.78	8086.25	8611.03	22.80	5895004451349	7
969.54	8360.60	.950	25.64	.936	16875.60	437.62	6374.83	68016.45	104.36	5960004009106	3
1109.00	11076.79	.998	.76	.999	18728.03	155.84	4045.72	4201.56	2.12	5962004537739	3
246.75	6265.04	.924	1.16	.982	11296.38	841.18	5587.12	6428.30	18.54	704500479020	50
105351.51	124788.92	.48-.677	474.79	53.671	3013490.99	39009.75	1742644.37	178159.12	3284.44	TOTALS	
1081.11	2116.45	.864	8.48	.978	51012.42	696.60	11118.65	31315.25	58.65	AVERAGES	

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FROM COST TO QUALITY PRACTICABLE

TABLE 6.2. CURRENT SYSTEM

(1) Item No.	(2) FSN	(3) Monthly Demand	(4) Months Lead time	(5) Lead time Demand	(6) Quarterly MAU	(7) Std. Dev. Lead time	(8) Q	(9) Unit Cost	(10) K	(11) Safety Stock K ₀
46	1005000178809	650.96	6.11	3976	943.60	945.19	3906	3.08	2.63	7550.27
46	1005000511579	465.25	7.18	3342	923.06	2142.28	2791	7.08	2.71	3342.05
47	10050003157318	147.67	13.11	2025	128.75	510.46	886	47.08	1.82	826.23
48	10050006999882	406.04	10.03	4072	371.94	1127.43	2836	9.64	2.22	2506.74
43	1005000699923	385.83	8.19	3237	215.00	562.40	2335	10.64	1.73	972.91
44	10050006999431	478.08	9.21	4404	201.25	564.10	2868	2.91	2.50	1420.27
42	10050007036793	427.04	9.68	4116	139.88	122.20	2567	9.72	1.41	453.37
41	10050007545266	182.63	5.90	1077	124.40	246.80	1490	2.38	2.52	621.89
40	10050017545267	53.63	12.25	657	73.07	262.61	322	41.36	1.49	391.63
39	10050017545293	47.17	9.44	471	85.18	146.59	723	5.66	2.05	300.51
38	1005001755579	90.42	9.77	888	102.25	301.14	633	7.26	2.44	741.02
37	100500179902	726.42	15.31	11121	666.50	2912.12	4359	220.55	2.21	620.52
36	1005001889718	76.17	6.29	479	42.26	171.38	533	9.12	2.07	354.64
35	1005003434230	14.54	6.77	98	19.88	41.82	47	162.94	1.19	8.36
34	1005003111640	23.33	7.44	183	14.75	36.54	140	45.84	4.49	17.94
33	1005004135657	127.83	6.77	859	68.25	149.59	767	111.22	3.00	8505.33
32	1005004938487	1008.54	8.43	8505	1042.13	2842.51	6051	1.27	3.00	2013.93
31	1005005163069	472.42	6.95	3282	298.32	671.11	3118	1.43	3.00	1884.00
30	1005005527703	447.79	5.64	2525	394.53	661.04	2637	2.21	2.85	120.02
29	10050058634744	48.54	9.67	469	39.72	116.75	291	46.12	1.03	429.15
28	1005006747349	69.34	9.08	812	116.66	381.49	536	43.45	1.12	2000.94
27	1005006129243	120.29	8.67	2776	151.84	945.12	1922	11.79	2.12	5270.27
26	1005006129256	1123.75	12.47	14380	673.06	2508.53	6730	9.47	2.10	394.04
25	100500653210	76.33	13.61	1034	66.00	259.47	458	40.93	1.52	1679.65
24	100500653210	1573.86	4.91	7725	525.47	911.09	9441	1.61	1.84	131.81
23	100500653210	32.25	8.29	267	19.25	49.45	193	201.97	2.08	402.81
22	100500653210	71.71	9.65	692	17.16	109.09	410	43.20	2.95	1894.31
21	100500653210	157.46	7.24	1140	43.47	194.05	945	5.53	1.03	117.59
20	100500653210	25.40	9.00	226	26.50	67.90	150	17.04	1.34	167.50
19	100500653210	54.42	5.97	3371	120.75	642.51	3522	1.43	2.63	375.99
18	100500653210	48.30	10.24	700	17.09	114.40	410	22.85	2.18	330.71
17	100500653210	48.29	7.00	408	45.88	101.80	476	8.07	1.85	192.09
16	100500653210	120.75	4.65	562	74.75	124.71	724	13.07	1.34	167.50
15	100500653210	24.42	8.48	250	28.07	74.09	177	138.31	4.45	33.57
14	100500653210	121.38	10.40	1263	53.48	168.45	728	40.97	1.94	158.77
13	100500653210	40.75	9.23	376	116.13	104.95	372	9.52	2.63	375.99
12	100500653210	66.25	6.58	436	10.14	151.47	541	6.44	2.18	330.71
11	100500653210	66.46	4.61	572	10.03	80.33	399	25.44	1.11	4.92
10	100500653210	44.21	11.67	1647	22.38	77.17	265	53.94	3.00	2619.68
9	100500653210	148.50	11.09	1647	172.88	570.53	891	48.05	1.27	724.01
8	100500653210	55.00	6.11	336	88.50	140.39	330	237.16	1.15	27.21
7	100500653210	30.96	15.44	478	26.13	115.04	106	201.65	2.24	27.32
6	100500653210	42.33	15.52	657	32.25	142.66	254	45.60	1.98	139.67
5	100500653210	108.92	7.67	835	70.25	170.88	654	18.75	1.38	235.86
4	100500653210	23.00	5.14	114	25.50	45.69	138	142.20	1.11	4.92
3	100500653210	373.92	7.01	2620	540.75	1224.44	2244	2.74	3.00	2619.68
2	100500653210	31.75	12.61	401	14.56	53.74	190	45.10	1.27	724.01
1	100500653210	168.94	9.19	1548	68.13	191.94	1011	71.38	1.15	27.21
0	100500653210	78.34	7.81	612	63.88	151.64	470	1.65	1.18	185.75
0	100500653210	29.29	9.44	278	29.09	84.19	176	138.76	1.18	185.75
0	100500653210	128.91	11.25	1125	114.13	319.08	773	233.25	2.80	1664.05
0	100500653210	248.63	7.81	1942	240.40	593.56	1492	3.72	2.22	9.96
0	100500653210	17.00	8.28	141	17.75	45.95	102	160.91	1.15	27.21
0	100500653210	136.57	9.00	1230	114.75	318.00	819	51.38	1.15	27.21
0	100500653210	237.04	11.29	2676	214.85	716.68	2512	1.07	3.00	2210.05
0	100500653210	87.29	4.99	435	115.06	201.77	574	25.19	1.42	287.50
0	100500653210	12924.85	493.95	110377	10127.38	27274.03	40141	3726.22	80.28	49776.59
0	100500653210	230.40	8.82	1471	180.85	447.04	1431	46.54	1.43	888.87

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TABLE 6.2. CURRENT SYSTEM (Continued)

(12) Value Safety Stock	(13) True K	(14) Actual Weighted F _i	(15) Actual Service Level	(16) Inventory on hand	(17) Fill Ratio	(18) Annual Ordering Cost	(19) Annual Holding Cost (Inventory Position)	(20) Annual Operating Cost	(21) Annual Units Backordered	(22) FSN	(23) Item no.
7993.14	5.129	.01	1.00	14005.25	1.000	982.14	6034.00	6920.14	-25	1005000178809	48
23661.68	5.107	.04	1.00	3344.17	1.000	982.14	13157.21	14032.35	.57	1005000511579	46
22174.31	7.16	42.21	.82	36656.76	.894	982.14	20514.12	21402.26	188.47	1005003357318	47
2165.00	.341	94.44	.85	37748.87	.910	982.14	17247.89	19170.03	439.33	100500699882	45
10151.74	.558	63.24	.77	24013.25	.897	982.14	13115.52	14017.52	474.74	100500699923	43
4161.40	1.397	7.90	.92	4410.02	.979	982.14	4091.24	5474.88	118.02	100500699931	44
3951.40	.192	35.86	.71	15750.13	.912	982.14	11744.22	12616.36	449.35	1005007016793	42
1160.99	1.352	6.43	.99	3284.11	.969	429.15	1117.77	1766.92	67.43	1005007545261	41
16197.67	1.104	4.20	.92	23206.23	.960	982.14	11505.58	12387.72	26.02	1005007545267	40
1700.37	1.517	.74	.94	3755.75	.989	470.64	1474.18	1943.06	13.16	1005007545292	39
5371.77	1.072	1.46	.96	7705.36	.946	501.14	3244.41	3751.57	15.31	1005007755579	38
14695.41	1.148	35.74	.59	775078.90	.716	982.14	796164.98	707047.12	1954.72	1005007755579	38
3234.36	4.163	.01	1.00	5526.46	1.000	530.58	2275.98	2806.56	.15	1005007849718	36
1523.55	.166	2.61	.60	10463.22	.853	982.14	6126.72	7203.86	25.65	1005008938230	35
1181.14	.147	4.47	.59	6511.71	.799	583.64	4102.91	4686.55	56.27	1095001111440	34
.00	.000	2.73	.50	43259.05	.940	982.14	11771.19	12652.33	91.51	1095004335857	33
27812.51	2.746	3.83	.99	17731.35	.997	982.14	15064.32	15951.46	42.29	1095004918487	32
2079.91	1.777	4.63	.96	5122.50	.989	530.58	2594.65	2782.23	63.66	1095005168069	31
4164.65	1.693	5.09	.95	1318.98	.987	583.64	2023.98	3507.62	69.47	1095005227703	30
3535.94	1.559	.20	.94	12277.21	.990	982.14	7795.14	8677.28	5.97	1095008614744	29
2721.56	.762	14.11	.93	46606.64	.907	982.14	22021.90	22906.04	100.27	1095008747369	28
23591.04	1.272	.23	1.00	44925.23	.994	982.14	15554.79	16441.93	4.18	1095009120243	27
49905.86	.514	56.15	.76	42406.54	.844	982.14	50129.44	51011.62	2100.53	1095009120246	23
12107.63	.304	71.15	.72	2371.54	.794	982.14	11920.11	12702.25	188.99	109500953210	26
6061.53	.145	35.93	.80	2361.51	.961	982.14	11724.35	12616.24	736.26	1095010133419	25
.00	.000	2.57	.80	20577.70	.846	982.14	16908.70	17793.84	44.28	1270000831981	24
3659.99	.552	7.00	.77	4374.10	.937	982.14	5594.58	6426.72	71.36	1440005727651	61
2227.52	1.352	3.11	.90	4874.14	.975	982.14	2563.73	3147.37	47.46	1560003101191	60
3661.24	.745	1.08	.84	4825.90	.952	982.14	6221.25	7102.39	14.37	1560004190187	59
2704.47	1.141	.17	.99	5227.58	.999	561.19	2310.92	2472.11	5.35	1560006099968	58
3662.74	.593	4.91	.76	10524.05	.930	982.14	7724.30	8616.44	57.41	156006117049	57
1250.14	1.123	1.54	.90	1494.21	.975	429.15	1550.80	1932.94	17.40	156006220532	56
4189.24	.344	22.03	.64	7499.80	.872	583.64	1201.22	1464.86	185.64	15600624732	55
3636.46	.750	4.49	.83	13301.85	.969	982.14	9752.41	10134.55	10.91	156007803854	54
4901.24	.231	45.28	.84	14937.85	.813	982.14	12679.56	13561.70	271.84	156009492087	53
3571.39	7.136	.00	1.00	5348.40	1.000	383.97	2051.39	2437.37	.00	1670007970253	52
2324.79	1.295	2.29	.92	3500.06	.975	429.15	1536.20	1962.39	20.20	2530008269468	62
2301.11	.532	3.64	.75	7263.92	.933	982.14	4076.04	5850.22	53.05	3040006211345	51
34784.77	.00	.00	.50	7660.90	.862	982.14	79972.86	80852.00	73.20	3110006999957	21
5037.74	.222	.41	.58	56234.14	.996	982.14	11176.24	12002.42	6.44	3110009429451	29
5209.47	.770	4.06	.63	41499.76	.906	982.14	25172.74	26054.84	61.84	421000272815	15
4162.62	.435	18.49	.73	75992.38	.878	982.14	27787.74	28622.86	45.18	4310010339204	18
4322.80	1.257	1.13	.92	19919.37	.837	982.14	13938.22	14426.36	82.69	4440005749146	17
693.64	.120	1.27	.58	1071.04	.983	982.14	6027.47	6402.61	22.28	5365007855943	22
7177.93	6.330	.00	1.00	10251.57	.912	982.14	6282.39	7164.53	24.23	5621002694508	12
1932.09	.923	1.74	.72	8359.72	1.000	583.64	4008.78	4594.42	.05	582100906461	13
2993.70	.027	164.95	.52	62572.62	.690	982.14	7876.35	8750.49	26.73	5826000146411	11
5871.14	.908	2.96	.86	13508.77	.959	982.14	34381.31	35263.45	627.91	5831008803563	11
.00	.000	7.14	.50	34743.04	.806	982.14	28501.45	29392.54	68.24	5841000712392	2
.00	.000	25.75	.50	124129.12	.824	982.14	98482.47	99164.61	272.01	5895000894403	10
6190.76	.256	2.78	.97	8585.61	.990	583.64	3721.56	4307.20	28.95	5895004451349	9
3602.59	.166	3.18	.60	10113.26	.850	982.14	7461.58	8349.72	30.56	5895009497160	8
15225.19	.146	102.67	.59	71429.07	.745	982.14	17955.52	18417.66	418.02	5960004009106	7
2364.75	.770	97.63	.63	3528.07	.904	327.89	1534.05	1841.94	273.61	5962004537739	3
7294.52	1.557	.88	.94	13991.78	.986	982.14	5750.54	6632.72	14.18	7045008479020	50
570065.48	73.106	186.84	.84	2056602.10	51.586	41044.41	1490135.65	1541426.07	10187.26	TOTALS	
10180.10	1.105	13.17	.00	16725.04	.921	769.36	26755.99	27522.16	181.20	AVERAGES	

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TABLE 6.3

CURRENT VERSUS OPTIMAL SYSTEM
 $\lambda=660$, $\sqrt{R}=2$, $Z_i=0.5$, $n=56$, WR-ALC

	<u>Current</u>	<u>Optimal</u>	<u>Difference</u>
1. Average Service Level	79.6%	86.9%	7.3%
2. No. of Units backordered at any time, β_T	3,738	950	-2788
3. Annual number of backorders, β_N	10,147	3284	-6863
4. Fill ratio	92.1%	95.8%	3.7%
5. Value of Average Inventory on Hand	\$1,923,768	\$3,013,490	\$1,089,722
6. Value of Safety Stocks	\$570,085	\$1,297,489	\$727,404
7. Annual Operating Cost	\$1,541,420	\$1,781,654	\$240,234
8. Two Months of Demand	25,850	25,850	--
9. Safety Stock, units	49,777	105,354	55,577

TABLE 6.4

OPTIMAL SYSTEM, $Z_1=1/2$

	<u>$\lambda=660$</u>	<u>$\lambda=600$</u>	<u>$\lambda=500$</u>	<u>$\lambda=400$</u>	<u>$\lambda=300$</u>	<u>$\lambda=200$</u>
1. Service Level	.869	.859	.840	.822	.798	.757
2. No. of Units Backordered at any time, β_T	950	1039	1225	1375	1552	1902
3. Annual no. of Backorders, β_N	3284	3580	4170	4670	5251	6369
4. Fill Ratio	.958	.954	.948	.943	.936	.924
5. Value of Inventory on Hand	\$3013490	\$2905441	\$2712119	\$2577232	\$2451861	\$2281986
6. Value of Safety Stocks	\$1297488	\$1175499	\$954049	\$805215	\$672074	\$487044
7. Annual Operating Cost	\$1781654	\$1753596	\$1702563	\$1668431	\$1637809	\$1595252
8. Two Months of Demand in Units	25850	25850	25850	25850	25850	25850
9. Safety Stock in Units	105354	102075	95850	88795	79979	67590

TABLE 6.5

OPTIMAL SYSTEM, $Z_i=1$

	<u>$\lambda=660$</u>	<u>$\lambda=600$</u>	<u>$\lambda=500$</u>	<u>$\lambda=400$</u>	<u>$\lambda=300$</u>	<u>$\lambda=200$</u>
1. Service Level	.930	.923	.909	.889	.859	.822
2. No. of Units Backordered at any time, β_T	483	531	634	789	1039	1375
3. Annual no. of Backorders, β_N	1696	1861	2213	2740	3580	4670
4. Fill Ratio	.977	.975	.970	.964	.954	.943
5. Value of Inventory on Hand	\$3867276	\$3745094	\$3516640	\$3241695	\$2905441	\$2577232
6. Value of Safety Stocks	\$2227341	\$2097106	\$1851772	\$1551507	\$1,175499	\$805215
7. Annual Operating Cost	\$1995520	\$1965566	\$1909139	\$1840078	\$1753596	\$1668431
8. Two Months of Demand in Units	25850	25850	25850	25850	25850	25850
9. Safety Stock in Units	129342	126038	119726	112000	102075	88795

Figure 6.1. Exchange Curves for Safety Stock versus Expected Number of Units Backordered at any Time, β_T

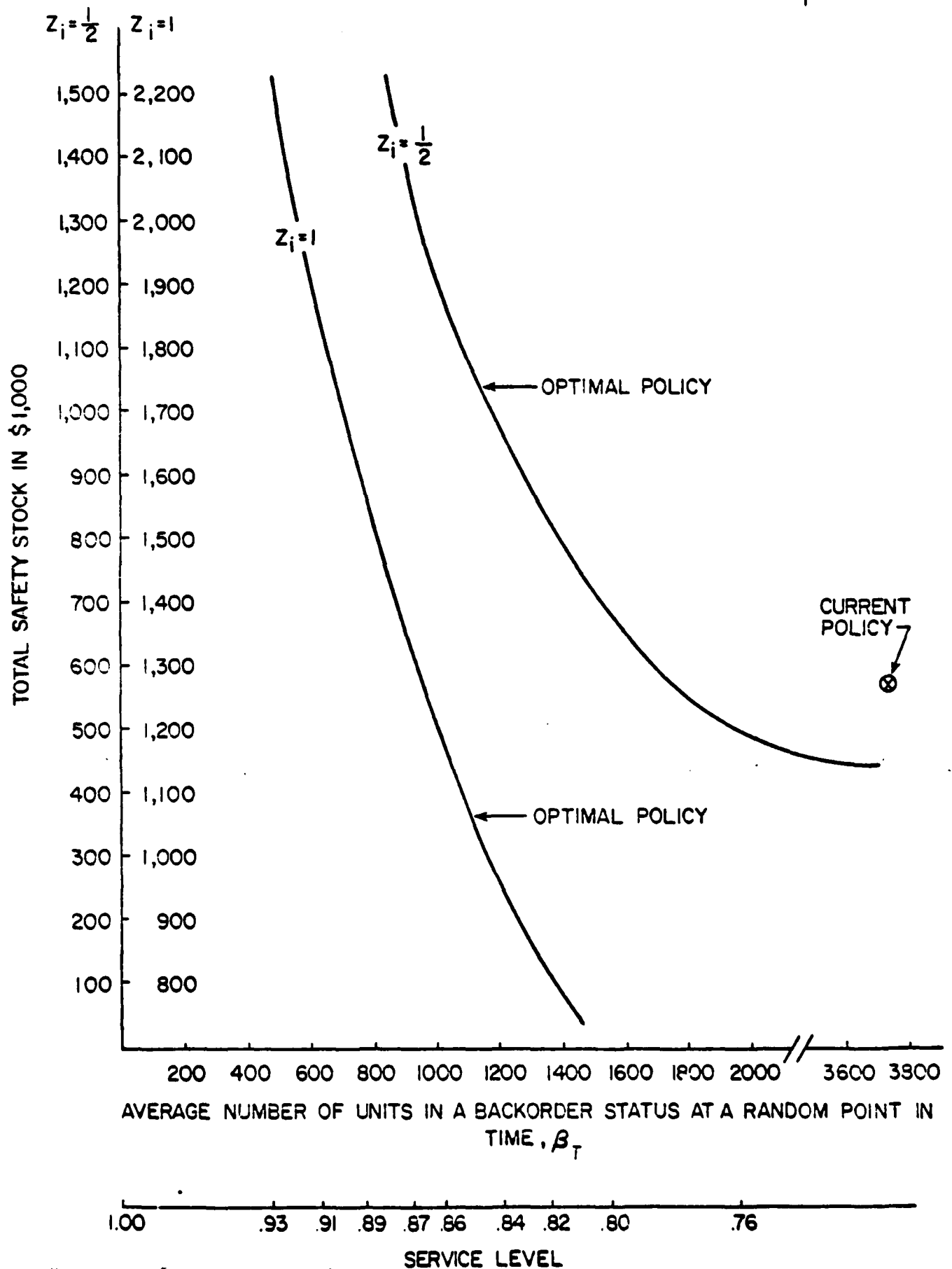
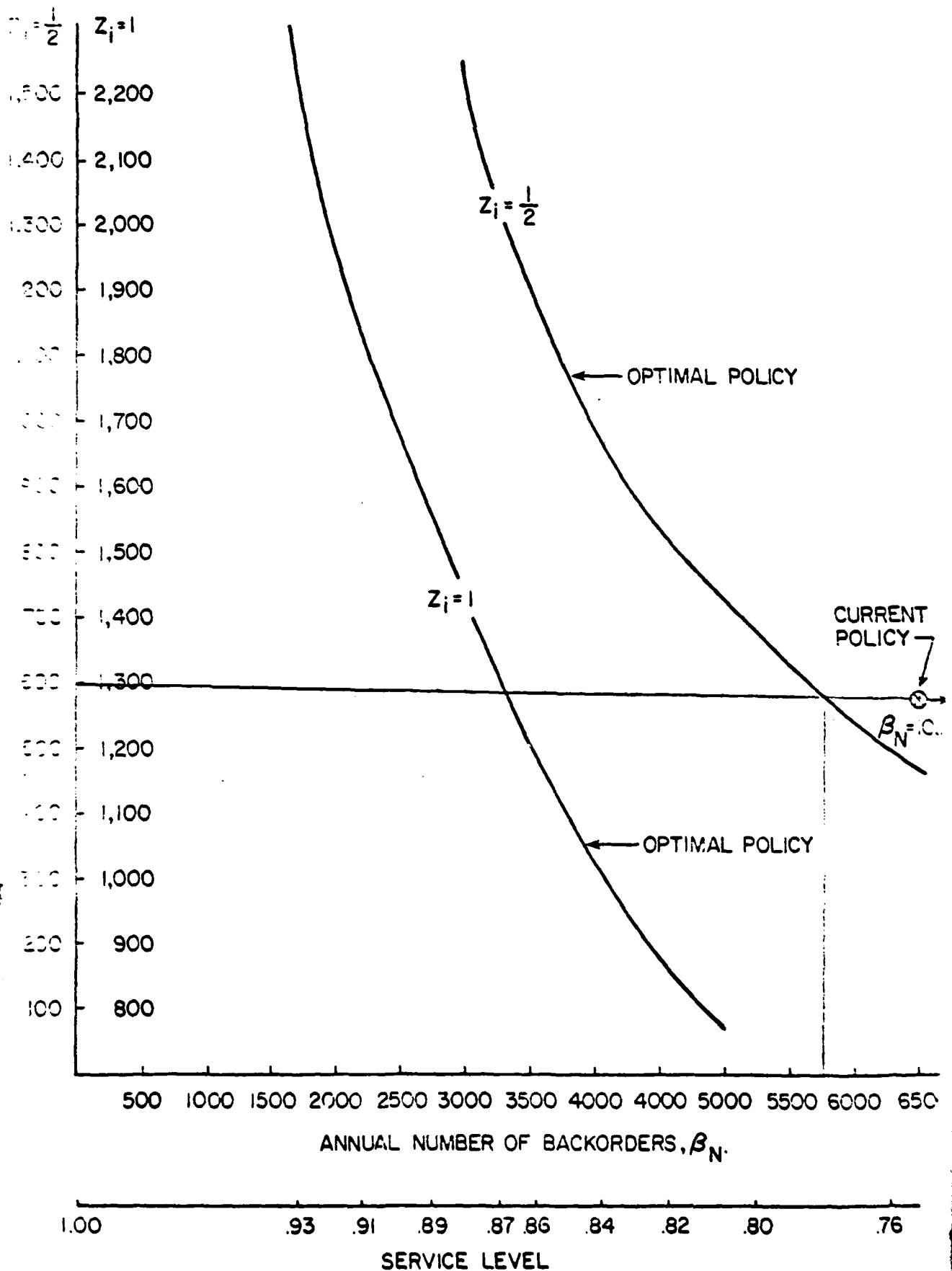


Figure 6.2. Exchange curves for safety stock versus annual Number of Backorders, β_N



an annual procurement of \$4.9 million. Since total annual procurement is one billion dollars, our sample represents about one-half of one percent of total procurement. Consequently, the numbers in this section must be multiplied by 200 in order to fathom the impact on the total inventory system. Returning to Table 6.3, for example, we see that to bring the system to optimality would require a one-time additional procurement for safety stocks of $\$727,400 \times 200 \approx \150 million. We can also see that the annual operating cost will increase by $\$240,234 \times 200 \approx \50 million. This is the price to pay in order to reduce backorders by $6863 \times 200 \approx 1,400,000$ units per year.

In Figures 6.1 and 6.2, we see that the current policy itself is not on the optimal curve. Thus, AFLC can presently reduce the number of backorders without any additional investment in safety stocks. Conversely, with the current number of backorders, AFLC can reduce its investment in safety stocks. We illustrate by means of Figure 6.2. At present, the total number of annual backorders for the sample is about 10,000; the total safety stock is about \$600,000. With the same investment in safety stock, we can immediately reduce our annual backorders to about 5750 units per year. This translates to a reduction of backorders for the total system of about $(10,000 - 5750) \times 200 = 850,000$ units per year. Thus the number of backorders can be almost halved by incorporating leadtime variability and by adhering to the Presutti-Trepp optimal model.

7. LIMITATIONS, ASSUMPTIONS, RESEARCH QUESTIONS, METHODS AND ANALYSES USED

Limitations

The uninvolved reader may find fault with a study of this kind, but considering the limited scope originally envisaged, that reader may perhaps discern the amount of work that was nevertheless put in it. We are dealing here with inventories whose worth runs into the billions and whose management is necessarily very complex. Consequently, it would be vain to claim that this modest study will resolve all the problems of shortages encountered by AFLC.

Assumptions

Since we did not have daily demand, but only demand rates, it was convenient to assume that daily demand was Poisson-distributed. LORRA had supplied us with daily shipment data on two items, but shipment data are not demand data. The daily shipment data do not appear to conform to the Poisson distribution..

We had also assumed that leadtimes and demand rates were statistically independent. Lacking simultaneous demand and leadtime data, it was impossible to validate that assumption.

Finally, we implicitly assumed that the sample of fifty-six high-intensity items is representative of the population of such items. In fact, it was not a random but a convenience sample.

Research Questions

In a study of this kind, the questions raised by the research overwhelm the answers provided, and this study is no exception. Also the questions raised depend very much on the reader's point of view. From our point of view, there are numerous questions, and as an example we ask only two:

1. Why the incongruities in the mathematics of the current system?

In calculating the safety factors, AFLC relies on a Presutti-Trepp formula which in turn is based on leadtime demand being Laplace-distributed. But in calculating the quarterly MAD, AFLC pretends that leadtime demand is normally distributed. One effect of this incongruity is in the calculation of the standard deviation of leadtime demand, σ , from MAD. We see that for the normal,

$$\hat{\sigma} = 1.25 \text{ MAD} \quad , \quad (7.1)$$

whereas for the Laplace,

$$\hat{\sigma} = \text{MAD} \quad . \quad (7.2)$$

Thus, with Laplace leadtime demand, we should use (7.2) rather than (7.1).

2. What is a proper definition of fill ratio? Does fill ratio address the percentage of requisitions filled or the annual fraction of demand satisfied? Using the latter as a definition of theoretical fill ratio does not produce results that are compatible with actual fill rates, as may be seen in Table 7.1. Of course, the calculation of theoretical fill ratio in Table 7.1 does not consider customer priority.

TABLE 7.1
CURRENT FILL RATES: REPORTED VS. THEORETICAL

Item no.	FSN	Fill Rates		
		Reported ¹	Theoretical ²	$1 - \beta_T/Q$
9	5895004451349	81.90	99.0%	99.6
8	5895009497160	63.06	85.0	93.8
7	5960004009106	98.79	74.5	74.9
3	5962004537739	67.80	90.4	92.3
10	5895000894403	98.75	80.6	91.7
2	5841000738392	100.00	95.9	98.74
15	589001167508	73.29	82.4	93.33
11	5831008803563	99.76	69.0	67.4
13	5821009906461	100.00	100.0	100.0
12	5821002694508	87.28	91.2	98.2
50	7045008479020	99.41	93.6	99.7
51	3040006211345	17.09	93.3	98.2
52	1670007970253	72.57	100.0	100.0
53	1560009492087	95.08	81.3	87.6
28	1095008747369	100.00	90.7	93.1
27	1095009120243	95.92	99.9	100.0
29	1095008614744	100.00	99.0	99.8
30	1095005227703	100.00	98.7	99.6

TABLE 7.1 (Continued)

Item no.	FSN	Fill Rates		
		Reported ¹	Theoretical ²	$1 - \beta_T/Q$
31	1095105168069	98.49%	98.9%	99.7
32	1095004918487	96.47	99.7	99.9
33	1095004335657	77.70	94.0	99.3
34	1095001111640	84.73	79.9	87.6
35	1005008938230	95.55	85.3	94.0
36	1005007889718	99.25	100.0	100.0
37	1005007879802	93.55	97.6	83.6
38	1005007755579	98.96	98.6	99.4
39	1005007545293	100.00	98.9	99.7
40	1005007545267	100.00	96.0	99.4
41	1005007545266	100.00	96.9	99.1
42	1005007016793	100.00	91.2	97.2
43	1005006999923	100.00	89.7	94.5
44	1005006999931	100.00	97.9	99.4
45	1005006999882	100.00	91.0	92.2
46	1005000511579	96.15	100.0	100.0
47	1005003357318	100.00	89.4	90.5
48	1005000178809	100.00	100.0	100.0

¹From fill rates for April 1979 - March 1980 obtained from LORRA

²From a computer simulation of the current system

Indeed, there are several methods of calculating theoretical fill ratios. Brown (1967, pp. 91-92) comments on this, suggesting to us the use of $1-\beta_T/Q$. This alternative computation is also given in Table 7.1.

Methods and Analyses Used

In fitting leadtime data to the exponential, the gamma, the normal, the Weibull, and the lognormal, we used an existing U.S. Army computer program (1971). In testing the leadtime data for randomness, we wrote our own program. We similarly wrote our own computer programs in simulating leadtime demand, fitting leadtime demand to the normal and the Laplace, doing ABC classification of inventory, and in simulating the current and optimal systems. Furthermore, we wrote a simulation program to show that the long right tail of the distribution of forecast errors produced by Demmy (1979) was due to a wrong statistical procedure.

8. FINDINGS AND CONCLUSIONS

The major finding of this study is that leadtime variability does indeed influence safety stocks, and in order to maintain these at appropriate levels, a one-time investment of about \$150 million is necessary. Also necessary would be an increase in annual operating expenditure of approximately \$50 million.

Even if AFLC does not wish to build up its stocks, it can immediately halve its number of backorders by explicitly incorporating leadtime variability in its calculations and by adhering to the Presutti-Trepp optimal model. This would require a different mix of items and, in general, larger order quantities.

We have also found it worthwhile to use an ABC classification of the high-intensity items. On the one hand, ABC classification is dynamic and thus much superior to the static SMGC in current use at AFLC. On the other, the ABC classification points directly to the few high-intensity items management should really concentrate its attention upon. In this regard the SMGC seems anachronistic.

APPENDIX A
MEMO OF UNDERSTANDING
(MARCH 7, 1980)

MEMO OF UNDERSTANDING

SUBJECT: Hayya Leadtime Variability Study - AF Contract
F33615-79-C-5143

1. The results from Phase I of AF Contract F33615-79-C-5143, Lead-time Variability in Inventory Requirements Projection, were discussed in the 5 Feb meeting of contractor Dr. Jack C. Hayya, Capt Paul Gross/AFBRMC and representatives from LORRA. During the meeting it was determined that Phases II & III could not be conducted as originally planned. The leadtime distributions found in Phase I were for 16 specific items during the 76-79 time period. Thus the simulation model, INSSIM, which has 71-75 data cannot be used in Phase II.
2. Leadtime data on 46 more items have been given to Dr. Hayya and he has agreed to curve fit their distribution using the same methods as were used on the original 16 items. Also he will determine and analyze the convolution of the leadtime distributions with demand distributions assumed to be Normal, Laplace, or "skewed Normal". Dr. W. Steven Denny's results in "Statistical Characteristics of Forecasting Techniques for D062 Economic Order Quantity Items" shows distributions for demands that are near normal but skewed. The one in Table IV-2 for OC with SMGC=2 will be used for this study.
3. A data request for 76-79 demands for the 62 items on which Hayya has leadtime is being processed and should be available in March. Hayya will use this to determine the actual leadtime demands for the items and test the fit of the curves to the p.d.f.s specified in the original contract. This also will be compared to the p.d.f.s of the convoluted distributions discussed in paragraph two above.
4. Dr. Hayya has also agreed to investigate our Variable Safety Level formula. He will conduct an analysis of the sensitivity of the safety level to changes in variance from demand variance to leadtime demand variance. Typical holding costs range from .15 to .25. The implied shortage factor or Lagrangian multiplier normally ranges from 350 to 600. The Lagrangian multiplier is always adjusted so that each ALC will have a total current safety level stock of dollar value equivalent to 2 months supply of all stock at that ALC. Any indication of how the mix of items at an ALC will change when using leadtime demand variance is important. Dr. Hayya will also make recommendations on possible marginal analysis techniques which will use variable leadtime demands to minimize back orders.
5. A copy of "More Ado About Economic Order Quantities (EOQ)" by Victor J. Presutti Jr and Richard C. Trepp was furnished Dr. Hayya when he visited W-P AFB on 5 Feb 1980. Copies of the EOQ briefing, Vic Presutti's VSL briefing, and "Measurement and Implications of Production Leadtime Variability", by the US Army Inventory Research Office will be furnished Dr. Hayya along with a copy of this memo. Demand data on the 62 items will be furnished as soon as available.

APPENDIX B

EXPLANATION OF TABLE 6.1: OPTIMAL SYSTEM

This table can be sorted by item no. or by FSN. The table has 24 columns, 12 on page 1 and 12 on page 2. I shall use the data for item #48 to illustrate.

Col. 1: Item no., following the sequence in the Phase II report

Col. 2: FSN

Col. 3: Daily Demand, $E(d)$

Col. 4: Average leadtime in days, $E(L)$

Col. 5: Variance of leadtime, $V(L)$

Col. 6: Mean of leadtime Demand

$$\begin{aligned} E(x) &= E(L) \cdot E(D) \\ &= (183.25) (21.70) \\ &= 3976 , \quad \text{for item \#48} \end{aligned}$$

Col. 7: Variance of leadtime Demand

$$\begin{aligned} V^*(x) &= E(L) \cdot V(D) + [E(D)]^2 V(L) \\ &= E(L) \cdot E(D) + [E(D)]^2 V(L) , \text{ for Poisson demands} \\ &= E(x) + [E(D)]^2 V(L) \\ &= 3976 + (21.70)^2 (535) \\ &= 255,902 . \end{aligned}$$

(The computer result of 255,870 is more accurate)

Col. 8: The standard deviation of leadtime demand, $\sigma^*(x)$

$$\begin{aligned} \sigma^*(x) &= \sqrt{V^*(x)} \\ &= \sqrt{255870} \\ &= 505.84 . \end{aligned}$$

Col. 9: Unit cost, c_i

Col. 10: The Wilson Formula

$$Q_w = \sqrt{\frac{2A_i D_i}{a_i c_i}},$$

where $A_i = \$441.07$, if $c_i D_i > \$19,500$, $\$291.82$ otherwise

(See AFLCR 57-6 (C3), 22 June 1979),

D_i = Annual demand,

a_i = holding cost factor, which is 0.23 in this example,

c_i = unit cost .

Hence

$$Q_w = \sqrt{\frac{2(441.07)(650.96)(12)}{(0.23)(3.08)}}$$

$$= 3118.9 .$$

Col. 11: Optimal EOQ, Q_i^* , calculated according to formula (14) in Presutti and Trepp (1970, p. 249):

$$Q_i^* = 0.707 \sigma_i^* + \left\{ (2A_i D_i / a_i c_i) + \sigma_i^{*2} / 2 \right\}^{1/2}$$

$$= 0.707 \sigma_i^* + \left\{ Q_w^2 + \sigma_i^{*2} / 2 \right\}^{1/2}$$

$$= 0.707 (505.84) + \left\{ (3118.9)^2 + 255870 / 2 \right\}^{1/2}$$

$$= 3497 .$$

What is necessary in order to use the above formula is for $\frac{Q_i^*}{\sigma_i^*} > 2$ or 3.

For item =43, $\frac{Q_i^*}{\sigma_i^*} = \frac{3497}{505.84} = 6.9$.

Col. 12: Optimal safety factor, k_i^* , calculated according to formula IV.2 in Presutti and Trepp (1970, p. 249):

$$k_i = -\frac{1}{\sqrt{2}} \ln \left[\frac{\sqrt{2} Q_i^* a_i c_i}{0.5(-\lambda) Z_i \sigma_i (1 - \exp(-\sqrt{2} \frac{Q_i^*}{\sigma_i}))} \right]$$

Here we are using

$$-\lambda = 660, \quad Z_i = \frac{1}{2}, \quad a_i = 0.23$$

Then

$$k_i = -0.707 \ln \left[\frac{\sqrt{2}(3497)(0.23)(3.08)}{0.5(660)(0.5)(505.84)(1 - e^{-\sqrt{2}(3497)(505.84)})} \right]$$

$$= -0.707 \ln \left[\frac{3503.39}{83,458.86} \right]$$

$$= -0.707 \ln 0.04197$$

$$= 2.242$$

Col. 13: Safety stock k_{σ}^{**}

$$k_{\sigma}^{**} = (2.242)(505.84)$$

$$= 1134, \quad \text{for item \#48}$$

Col. 14: Value of safety stock,

$$c_i k_{\sigma}^{**} = \$3.08 (1134)$$

$$= \$3492$$

Col. 15: Service level. This is

$$\begin{aligned}
 1 - \frac{1}{2} e^{-\sqrt{2} k_i^*} &= 1 - \frac{1}{2} e^{-\sqrt{2} (2.242)} \\
 &= 0.979 \\
 &= 0.98 .
 \end{aligned}$$

Col. 16: Weighted Backorders at any time, β_T . We may think of this as the number of requisitions backordered when $Z_i \neq 1$. If $Z_i = 1$, β_T would be the average number of units backordered at any time.

We use formula IV.2 (Presutti and Trepp, p. 249) or formula (10) (Presutti and Trepp, p. 246). From formula IV.2, we have

$$\beta_T = \frac{0.5}{2} \frac{Z_i \sigma_i^2}{Q_i^*} \left(1 - e^{-\sqrt{2} \frac{Q_i^*}{\sigma_i}} \right) e^{-\sqrt{2} k_i^*} .$$

For item #48,

$$\begin{aligned}
 \beta_T &= \frac{0.5}{2} \frac{(\frac{1}{2})(255870)}{3497} \left(1 - e^{-\sqrt{2} \frac{3497}{505.84}} \right) e^{-\sqrt{2} (0.242)} \\
 &= 0.38 .
 \end{aligned}$$

The actual units backordered at any time would be

$$\frac{0.38}{Z_i} = \frac{0.38}{\frac{1}{2}} = 0.76 .$$

Col. 17: The fill ratio is

$$\frac{\text{Annual Demand} - \text{Annual backorders}}{\text{Annual Demand}}$$

Annual backorders are given in Col. 22. They are calculated according to formula (9) in Presutti and Trepp (1970, p. 246):

$$\begin{aligned} B_N &= \frac{0.5}{\sqrt{2}} \frac{D_i \sigma_i^*}{Q_i^*} \left(1 - e^{-\sqrt{2} Q_i^* / \sigma_i^*} \right) e^{-\sqrt{2} k_i^*} \\ &= \frac{0.5}{\sqrt{2}} \frac{(21.70 \times 360)(505.34)}{3497} (0.999943)(0.041976) \\ &= 16.77 \text{ units per year .} \end{aligned}$$

Actually,

$$\begin{aligned} B_N &= \sqrt{2} \beta_T D_i / Z_i \sigma_i^* \\ &= \sqrt{2} (0.38)(7812) / \left(\frac{1}{2}\right)(505.84) \\ &= 16.60 \text{ (the difference is due to rounding) .} \end{aligned}$$

Hence, the fill ratio is

$$\frac{7812 - 16.77}{7812} = 0.998 \text{ .}$$

Col. 18: Average value of inventory on hand.

The formula is from Presutti and Trepp (1970, p. 247),
where

$$\begin{aligned}\text{Value } E[OH] &= (k\sigma + Q/2 + \beta_T) c_i \\ &= (k\sigma + Q/2 + \beta_T/Z_i) c_i .\end{aligned}$$

For item #48, this would be

$$\begin{aligned}\text{Value } [OH] &= [1134 + \frac{3497}{2} + 2(0.38)] 3.08 \\ &= \$8880.44 .\end{aligned}$$

Col. 19: Annual Ordering Cost. This is

$$\begin{aligned}\frac{A_i D_i}{Q_i} &= (\$441) \frac{7812}{3497} \\ &= \$985.15 .\end{aligned}$$

Col. 20: Annual holding cost, based on average inventory position. This is

$$\begin{aligned}a_i c_i \left(\mu_i + k_i \sigma_i + \frac{Q_i}{2} \right) \\ = 0.23(3.08) \left(3976 + 1134 + \frac{3497}{2} \right) = \$4858.56 .\end{aligned}$$

Col. 21: Annual Operating Cost. This is from Formula IV.1 (Presutti and Trepp, p. 249):

$$\frac{A_i D_i}{Q_i} + a_i c_i \left(\mu_i + k_i \sigma_i + \frac{Q_i}{2} \right)$$

$$= 985.25 + 4858.80$$

$$= \$5844.05 .$$

Col. 22: Annual no. of backorders.

Col. 23: FSN

Col. 24: Item #

APPENDIX C

EXPLANATION OF TABLE 6.2: AFLC'S CURRENT SYSTEM

This table can also be sorted by item no. or by FSN. The table has 23 columns, 11 on page 1 and 12 on page 2. Again I use the data for item #48 to illustrate.

Col. 1: Item no.

Col. 2: FSN

Col. 3: Monthly demand, $E(D)$

Col. 4: Months leadtime, $E(L)$

Col. 5: Leadtime Demand:

$$\begin{aligned} E(x) &= E(L) \cdot E(D) \\ &= (6.11)(650.96) \\ &= 3977, \text{ for item no. 48} \end{aligned}$$

Col. 6: Quarterly MAD

Col. 7: The std. deviation of leadtime demand, according to AFLCR 57-6(C2), 29 December 1978. It is

$$\begin{aligned} \sigma &= 0.5945 \text{ MAD } (0.82375 + 0.42625 L) \\ &= 0.5945 (483.60) \{0.82375 + 0.42625 (6.11)\} \\ &= 985.59 . \end{aligned}$$

Col. 8: The EOQ. Using the EOQ table for WR-ALC (AFLCR 57-6(C3) 22 June 1979), we have

$$\begin{aligned} Q &= 0.50 \quad , \quad \text{since } c_i D_i > \$10,000 \\ &= 0.5(650.96)(12) \\ &= 3906 \text{ units} . \end{aligned}$$

Col. 9: Unit cost

Col. 10: The safety factor, according to AFLCR 57-6(C2), 29 December 1978, p. 7-2. It is

$$K = -0.707 \ln \frac{2\sqrt{Z} Q a_i c_i}{\lambda \left(\frac{1}{\sqrt{R}}\right) \sigma (1 - e^{-\sqrt{Z} Q / \sigma})} ,$$

where for our example

R = the average requisition size, 4 in this case,

$\lambda = 660$,

and the other terms as before. Hence

$$\begin{aligned} K &= -0.707 \ln \frac{2\sqrt{Z}(3906)(0.23)(3.08)}{660\left(\frac{1}{\sqrt{2}}\right)(985.39)\left(1 - e^{-\sqrt{Z}\frac{(3906)}{985.39}}\right)} \\ &= -0.707 \ln \frac{7826.29}{323,983.2} \\ &= -0.707 \ln 0.024156 \\ &= 2.63 . \end{aligned}$$

The value of K must be between zero and three.

Col. 11: Safety Stock

$$\begin{aligned} k\sigma &= 2.63 (985.39) \\ &= 2591.58, \quad \text{for item \#48.} \end{aligned}$$

This value must not exceed that for leadtime demand.

Col. 12: \$ Safety Stock. This is

$$\begin{aligned} c_i K_i \sigma_i &= 3.08 (2594.27) \\ &= \$7990.35. \end{aligned}$$

Col. 13: True K. The K-value of Col. 10 is not based on the true standard deviation of leadtime demand, σ^* . The value of σ^* obtained from Table 6.1, Col. 8 is 505.84 not 985.39. Hence the true K is

$$\begin{aligned} \text{True K} &= \frac{\text{Safety Stock}}{\sigma^*} \\ &= \frac{2594.27}{505.84} \\ &= 5.129. \end{aligned}$$

Col. 14: Actual β_T weighted by essentiality, Z_i . To be consistent, we set

$$Z_i = \frac{1}{\sqrt{R}} = \frac{1}{2}.$$

Then using formula IV.2 in Presutti and Trepp (1970, p. 249), we have

$$\begin{aligned} \beta_T &= \frac{0.5}{2} \frac{Z_i \sigma_i^2}{Q_i} \left(1 - e^{-\sqrt{2} \frac{Q_i}{\sigma_i^*}} \right) e^{-\sqrt{2} k_i^*} \\ &= \frac{0.5}{2} \frac{\left(\frac{1}{2}\right)(505.84)^2}{3906} \left(1 - e^{-\sqrt{2} \left(\frac{3906}{505.84}\right)} \right) e^{-\sqrt{2} (5.129)} \\ &= 0.006 \end{aligned}$$

The actual number of backorders expected at any time is actually

$$\beta_T/Z_i = 0.006/0.5 = 0.012 .$$

Col. 15: Actual Service Level

$$1 = \frac{1}{2} e^{-\sqrt{2} k_i^*}$$

$$= 1 - (0.5) (0.00070769)$$

$$= 1.00 .$$

Col. 16: \$ Inventory on hand. This is

$$c_i \left(\text{Safety stock} + \frac{Q}{2} + \beta_T/Z_i \right)$$

$$= 3.08 \left(2594.27 + \frac{3906}{2} + 0.012 \right)$$

$$= \$14,005.$$

Col. 17: Fill Ratio. This is

$$\frac{\text{Annual Demand} - \text{Annual Number of backorders}}{\text{Annual Demand}}$$

We obtain the annual number of backorders using formula (9) in Presutti-Trepp (1970, p. 246):

$$\beta_N = \frac{0.5}{\sqrt{2}} \frac{D_i \sigma_i^*}{Q} \left(1 - e^{-\sqrt{2} Q/\sigma^*} \right) \left(e^{-\sqrt{2} k^*} \right)$$

$$= \frac{0.5}{\sqrt{2}} \frac{(12)(650.96)(505.84)}{3906} (0.99998) (0.00070769)$$

$$= 0.25 .$$

You see this value in Column 21.

Hence,

$$\text{Fill Ratio} = \frac{12(650.96) - 0.25}{12(650.96)}$$

$$\approx 1.00 .$$

Col. 18: Annual Ordering Cost

$$\begin{aligned} \frac{A_i D_i}{Q_i} &= \frac{441.07(650.96)(12)}{3906} \\ &= \$882.09 \approx \$882.14 . \end{aligned}$$

It is strange that the ordering cost for so many items is \$882.14 or \$583.64. Apparently an annual ordering cost of \$882.14 corresponds to an ordering cost of \$441.07, whereas an annual ordering cost of \$583.74 corresponds to an ordering cost of \$291.82. Thus

$$\frac{\$291.82}{441.07} (\$882.14) = \$583.64 .$$

Consider item #3 where the dollar value of annual demands is $373.92 \times (12)(\$2.74) = \$12,294.49 < \$19,500$. Hence, the ordering cost, $A = \$291.82$; and the annual ordering cost would be

$$\begin{aligned} \frac{AD}{Q} &= \frac{(291.82)(373.92)(12)}{2244} \\ &= \$583.52 . \end{aligned}$$

It seems that the EOQ table for WR-ALC (AFLCR 57-6(C3), 22 June 1979, p. 7-14-1) is designed to produce precisely these annual order costs.

Col. 19: Annual Holding Cost based on the Inventory Position. This is

$$\begin{aligned} & a_i c_i \left(\mu + \text{Safety Stock} + \frac{Q}{2} \right) \\ &= \$0.23(3.08)(3976 + 2594.27 + \frac{3906}{2}) \\ &= \$6037.88 . \end{aligned}$$

Col. 20: Annual operating cost. This is the sum of the annual ordering cost and the annual holding cost.

Col. 21: Annual number of units backordered. This has already been calculated under Col. 17.

Col. 22: FSN

Col. 23: Item no.

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