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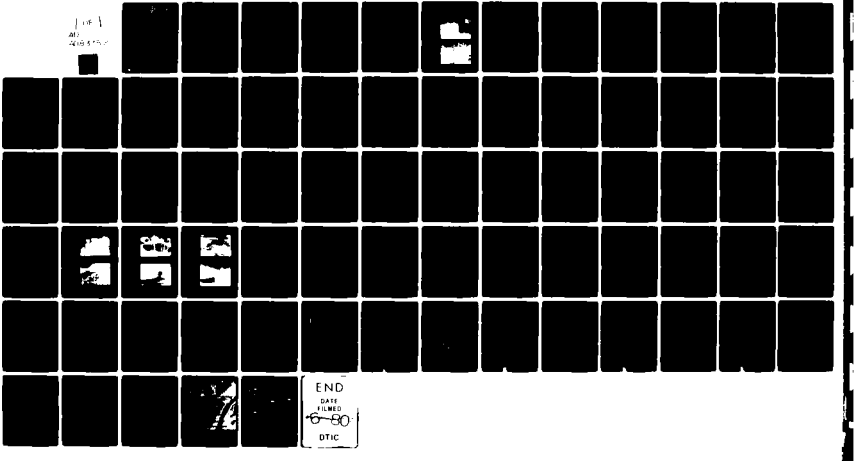

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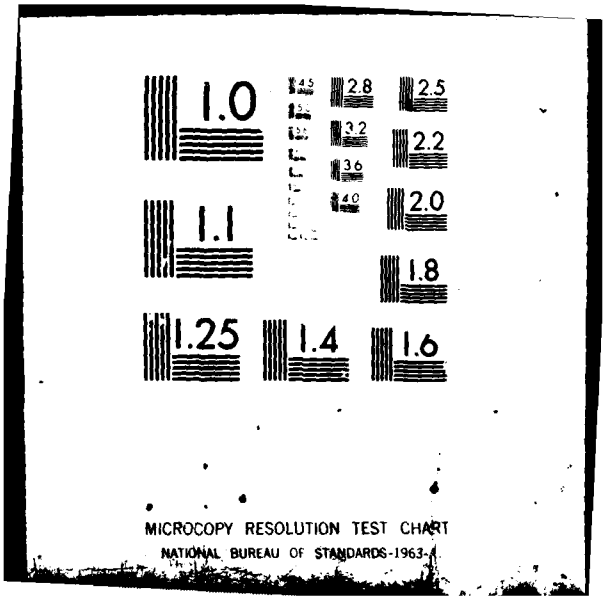
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LEVEL II

OHIO RIVER BASIN
BEAR ROCK RUN, CAMBRIA COUNTY

PENNSYLVANIA

BEAR ROCK NO. 2 DAM

NDI I.D. NO: PA-0441
DER I.D. NO : 11-3

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PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

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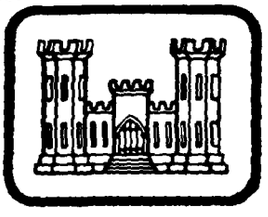

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DEPARTMENT OF THE ARMY
BALTIMORE DISTRICT, CORPS OF ENGINEERS
BALTIMORE, MARYLAND 21203

BY

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Department of the Army, Office of Chief of Engineers, Washington, D.C. 20314.

The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon visual observations and review of available data. Detailed investigations and analyses involving topographic mapping, subsurface investigations, material testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the inspection is intended to identify any need for such studies which should be performed by the owner.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of the dam depends on numerous and constantly changing internal and external factors which are evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

The assessment of the conditions and recommendations was made by the consulting engineer in accordance with generally and currently accepted engineering principles and practices.

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DACW31-80-C-0022

(6) National Dam Inspection Program. Bear Rock Number 2 Dam (NDI I.D. Number PA-0441, DER I.D. Number 11-3) Ohio River Basin, Bear Rock Run, Cambria County, Pennsylvania. Phase I Inspection Report.

PHASE I REPORT
NATIONAL DAM INSPECTION PROGRAM

(10) Lawrence D. Andersen (11) INN (12) 13

NAME OF DAM: Bear Rock No. 2 Dam
STATE LOCATED: Pennsylvania
COUNTY LOCATED: Cambria
STREAM: Bear Rock Run
SIZE CLASSIFICATION: Intermediate
HAZARD CLASSIFICATION: High
OWNER: Highland Sewer and Water Authority
DATE OF INSPECTION: November 13 and December 28, 1979

(13) DACW31-80-C-0022

ASSESSMENT: Based on the evaluation of the existing conditions, the condition of Bear Rock No. 2 Dam is considered to be unsafe/nonemergency due to the seriously inadequate spillway capacity.

The structural condition of the embankment is considered to be good.

The crest and downstream face of the dam were found to be covered with brush and trees which require clearing. No signs of structural distress were observed.

The operational condition of the blow-off valve was not observed. It is therefore recommended that the operational condition of the blow-off valve should be immediately assessed and necessary maintenance performed if required. The flow through the outlet pipes is controlled by valves located downstream of the dam which cause the pipes to be under pressure through the embankment. In view of this condition, concern exists as to the effect of a rupture of these pipes on the embankment stability. Therefore, means for providing upstream control should be developed.

The spillway capacity was evaluated according to the recommended procedure and was found to pass 30 percent of the probable maximum flood (PMF) without overtopping the embankment. This capacity is less than the recommended spillway capacity of full PMF according to the size and hazard classification of the dam. Furthermore, because the spillway capacity is less than 50 percent of the PMF and it was found that failure of the dam due to overtopping would cause failure of Bear Rock No. 1 Dam downstream and the combined discharge would significantly increase the downstream hazard of loss of life compared to that which would exist just before failure, the spillway is considered to be seriously inadequate.

The following recommendations should be implemented immediately or on a continuing basis:

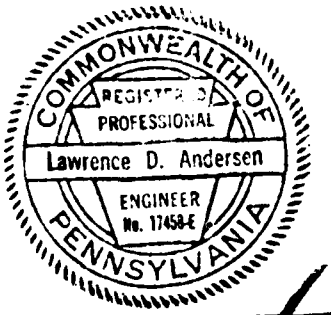
1. The owner should immediately retain a professional engineer to conduct additional studies to more accurately ascertain the spillway capacity and the nature and extent of improvements required to provide adequate spillway capacity.

2. The operational condition of the blow-off valve should be evaluated and necessary maintenance performed. A means for providing upstream control to the outlet pipes should be developed.

3. Brush and trees on the crest and downstream slope of the dam should be cleared.

4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system developed to alert the downstream residents in the event of emergencies. It is also recommended that the owner take necessary measures to improve the accessibility of the site during high flows.

5. The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.



Lawrence D. Andersen, P.E.
Vice President

March 5, 1980
Date

Approved by:

JAMES W. PECK
Colonel, Corps of Engineers
District Engineer

31 March 1980
Date

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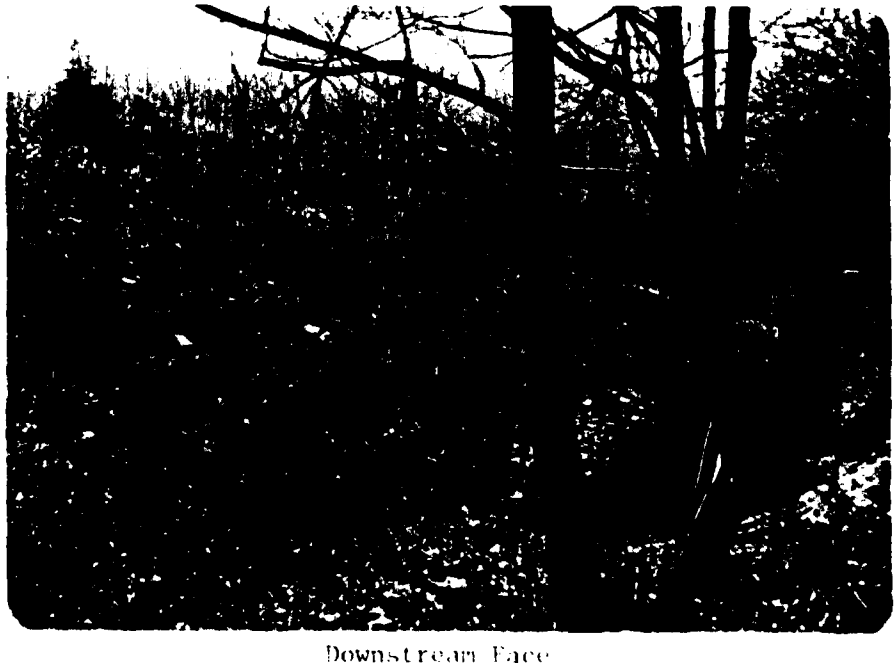
BEAR ROCK [illegible] DAM
NDI I.D. PA-[illegible]
NOVEMBER 13, 1979

Upstream Face



Downstream Face

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PHASE I REPORT
NATIONAL DAM INSPECTION PROGRAM
BEAR ROCK NO. 2 DAM
NDI I.D. PA-441
DER I.D. 11-3

SECTION 1
PROJECT INFORMATION

1.1 General

a. Authority. The inspection was performed pursuant to the authority granted by The National Dam Inspection Act, Public Law 92-367, to the Secretary of the Army, through the Corps of Engineers, to conduct inspections of dams throughout the United States.

b. Purpose. The purpose of this inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project

a. Dam and Appurtenances. Bear Rock No. 2 Dam consists of an earth embankment approximately 760 feet long with a maximum height of about 42 feet from the downstream toe and a crest width of about 6 feet. The crest and upstream and downstream faces of the dam are covered with riprap. The flood discharge facilities of the dam consist of a rectangular stone masonry overflow spillway located on the left abutment (looking downstream). The spillway is 33 feet wide and about 4 feet deep at the control section and uniformly coverges into the spillway discharge channel. The spillway discharge channel is a stone masonry chute, which terminates at a plunge pool. A dike along the right side of the spillway discharge channel is provided to prevent flow towards the toe of the dam. The outlet facilities consist of a 16-inch cast-iron blow-off pipe and a 12-inch cast-iron supply pipe. Flows through these pipes are controlled by valves located in the downstream valve chamber. The 16-inch blow-off pipe constitutes the emergency drawdown facility for the reservoir.

b. Location. The dam is located on Bear Rock Run, a tributary of Little Conemaugh River, immediately upstream of Bear Rock No. 1 Dam, about two miles east of Lilly in Washington Township, Cambria County, Pennsylvania. Plate 1 illustrates the location of the dam.

c. Size Classification. Intermediate (based on 42-foot height and 130 acre-feet maximum storage capacity).

d. Hazard Classification. The dam is classified to be in the high hazard category. Bear Rock Run flows through the town of Lilly approximately 2-1/2 miles downstream from the dam. It is estimated that failure of the dam would result in the failure of the downstream dam and combined discharge would cause large loss of life and property damage in the town of Lilly.

e. Ownership. Highland Sewer and Water Authority (address: Mr. Charles MacDonald, Manager, 400 Luray Avenue, Johnstown, Pennsylvania 15904).

f. Purpose of Dam. Water supply.

g. Design and Construction History. The dam was designed and constructed by Pennsylvania Railroad Company in 1904.

h. Normal Operating Procedure. The reservoir is normally maintained at Elevation 2400, the level of the uncontrolled spillway. When the lake is at or above the spillway level, inflow is discharged through the uncontrolled spillway.

1.3 Pertinent Data

a. Drainage Area	1.4 square miles
b. Discharge at Dam Site (cfs)	
Maximum known flood at dam site	Unknown
Outlet conduit at maximum pool	20
Gated spillway capacity at maximum pool	Not applicable
Ungated spillway capacity at maximum pool	858
Total spillway capacity at maximum pool	858
c. Elevation (USGS Datum) (feet)	
Top of dam	2404.4 (measured low spot) 2404.5 (as designed)
Maximum pool	2404.4
Normal pool	2400
Upstream invert outlet works	2370±
Downstream invert outlet works	2350±
Maximum tailwater	Unknown
Toe of dam	2362±
d. Reservoir Length (feet)	
Normal pool level	900
Maximum pool level	950 (estimated)

e. Storage (acre-feet)

Normal pool level	92
Maximum pool level	130

f. Reservoir Surface (acres)

Normal pool level	7.4
Maximum pool level	9.7±

g. Dam

Type	Earth
Length	760 feet
Height	42 feet
Top width	6 feet
Side slopes	Downstream: 2H:1V; Upstream: 2H:1V
Zoning	No
Impervious core	Yes
Cutoff	Yes
Grout curtain	No

h. Regulating Outlet

Type	16-inch cast-iron pipe
Length	250± feet
Closure	Gate valves
Access	Downstream valve chamber
Regulating facilities	Gate valve

i. Spillway

Type	Rectangular stone masonry channel
Length	33 feet (perpendicular to flow)
Crest elevation	2400
Upstream channel	Lake
Downstream channel	Rectangular stone masonry channel

SECTION 2
DESIGN DATA

2.1 Design

a. Data Available. The available information was provided by the Commonwealth of Pennsylvania, Department of Environmental Resources (PennDER). The information includes correspondence, state inspection reports, and design drawings.

(1) Hydrology and Hydraulics. No design information is available. A state report entitled, Report Upon the Application of the Summit Water Supply Company, dated May 10, 1937, gives the design capacity of the spillway used for the 1937 enlargement of the spillway.

(2) Embankment. Available information consists of limited design drawings.

(3) Appurtenant Structures. The available information consists of limited design drawings.

b. Design Features

(1) Embankment. Plate 2 shows the plan of the embankment and the reservoir. As shown in Plate 3, the embankment consists of compacted clay beneath the upstream and downstream slopes and a central puddle clay core wall. The dimensions of the puddle clay core wall are shown to be 12 feet at the crest level of the dam, increasing to a width of 16 feet at the original ground surface, and reducing to a 14-foot width at the bottom of the cutoff trench. As shown in the valley cross section in Plate 3, the puddle clay core wall was extended 20 to 30 feet below the original ground surface and into the abutments beyond the limits of the embankment and the spillway.

As designed, the embankment slopes were 2 horizontal to 1 vertical on both the upstream and downstream faces. The design provided an 18-inch-thick layer of riprap on both faces and the crest of the dam for erosion protection.

(2) Appurtenant Structures. The appurtenant structures of the dam consist of an uncontrolled overflow spillway located near the left abutment and outlet works at the center of the dam.

The plan and a typical cross section of the spillway are shown in Plates 2 and 4, respectively.

As shown in Plate 3, the outlet facilities consist of a 16-inch cast-iron blow-off pipe and a 12-inch supply line. The pipes are shown to enter the embankment, passing through a 3-foot-thick masonry wall. In the upstream portion of the dam, the pipes are located through the fill, but enter a cut trench at about the midpoint of the embankment, and then emerge from the toe of the dam at a level about 2 to 3 feet below the original ground surface. Design drawings indicate that the design provided no provisions to prevent leakage along the pipes, such as cutoff collars, other than the masonry wall located on the upstream end of the pipe.

c. Design Data

(1) Hydrology and Hydraulics. The 1937 state report indicates that the spillway improvements undertaken at that time were based on a spillway design capacity of 1100 cfs.

(2) Embankment. Other than limited design drawings, no engineering data are available on the design of the embankment.

(3) Appurtenant Structures. No design calculations are available for the appurtenant structures.

2.2 Construction. Very limited information is available on the construction of the dam. A 1914 state report indicates that the embankment material was placed in thin layers, wetted, and rolled with a horse roller.

Other than the placement of one foot of additional fill on the dam crest for the purpose of increasing the spillway capacity in 1937, no other post-construction changes are reported.

2.3 Operation. No operating records have been kept for the dam.

2.4 Other Investigations. None reported.

2.5 Evaluation

a. Availability. The available information was provided by the Commonwealth of Pennsylvania, Department of Environmental Resources.

b. Adequacy

(1) Hydrology and Hydraulics. The available information consists of the design discharge capacity of the spillway. This information is not considered to be sufficient to assess the adequacy of the spillway.

(2) Embankment. The dam was apparently constructed according to the design drawings. In view of the age of the dam, completed in 1904, the design approach and construction techniques are not likely to be in conformance with currently accepted engineering practices. The design lacks such considerations as embankment slope stability, seepage analyses, and other quantitative data to aid in the assessment of the adequacy of the design. However, the design includes such components as a core wall and a cutoff wall extending to impervious foundation material and slope protection.

(3) Appurtenant Structures. Review of the spillway design drawings indicates that no significant design deficiencies exist that would affect the overall performance of these structures. As for the outlet works, the available information indicates that the design incorporated no special provisions, such as cutoff collars, to control seepage along these pipes, which raises some concern relative to the adequacy of the design to prevent seepage along these pipes. However, no seepage has been reported along these pipes in the past and none was observed at this time, indicating that backfilling around the pipes was adequate to prevent seepage along these pipes.

SECTION 3
VISUAL INSPECTION

3.1 Findings

a. General. The on-site inspection of Bear Rock No. 2 Dam consisted of:

1. Visual inspection of the embankment, abutments, and embankment toe.

2. Visual examination of the spillway structures.

3. Evaluation of downstream area hazard potential.

The specific observations are illustrated in Plate 5.

b. Embankment. The general inspection of the embankment consisted of searching for indications of structural distress, such as cracks, subsidence, bulging, wet areas, seeps and boils, and observing general maintenance conditions, vegetative cover, erosion, and other surficial features.

The embankment was found to be in good condition. Bulges observed in the downstream slope riprap appear to be due to surficial effects, and therefore are not considered to be significant. A wet area observed along the toe of the dam near the right abutment is also considered to be insignificant relative to the overall performance of the embankment. The crest and downstream faces of the dam were covered with trees and brush up to 10 feet high which require clearing.

The top of the dam was surveyed relative to the spillway crest level and was found to be at or slightly above the design crest elevation, assuming the design crest level to be 4.5 feet above the spillway crest elevation. The crest of the dam is illustrated in Plate 6. Several measurements taken along the downstream slope indicated the slope is reasonably within the design slope of 2 horizontal to 1 vertical.

c. Appurtenant Structures. The spillway structures were examined for deterioration or other signs of distress and obstructions that would limit flow. The spillway structures were found to be in good condition. For the outlet structures, the only visible portion was the downstream end of the blow-off pipe. The operational condition of the blow-off valve was not observed.

d. Reservoir Area. A map review indicates that the watershed is predominantly covered by woodlands. A review of the regional geology (Appendix F) indicates that the shorelines of the reservoir are not likely to be susceptible to massive landslides, which would affect the storage volume of the reservoir.

e. Downstream Channel. Discharge from the dam flows into the reservoir of Bear Rock No. 1 Dam, which in turn discharges into Bear Rock Run. Bear Rock Run flows through an uninhabited valley for about two miles where it enters residential areas of the town of Lilly. It is estimated that in excess of 20 houses are located within the potential flood plain of Bear Rock Run in the event of a dam failure. Further description of the downstream conditions is included in Section 1.2d.

3.2 Evaluation. The condition of the embankment and spillway structures is considered to be good. The condition of the outlet facilities could not be assessed.

SECTION 4
OPERATIONAL FEATURES

4.1 Procedure. There are no formal operating procedures for the dam. The reservoir is normally maintained at the uncontrolled spillway crest level with excess inflow discharging over the spillway.

4.2 Maintenance of the Dam. The maintenance of the embankment is considered to be poor. The crest and downstream face of the dam are covered with trees and brush up to 10 feet high.

4.3 Maintenance of Operating Facilities. The only visible portions of the outlet facilities were the downstream end of the 16-inch cast-iron blow-off pipe. The operational condition of the blow-off valve was not observed.

4.4 Warning System. No formal warning system exists for the dam. The dam is accessible via a two-mile jeep trail which is in poor condition. Bear Rock Run crosses the jeep trail at two locations. It is estimated that during severe weather conditions, the trail will not be passable. Telephone communication facilities are available via residences located about one mile downstream from the dam.

4.5 Evaluation. The maintenance of the dam is considered to be poor. It is recommended that the brush and trees on the downstream face of the dam be cleared and that the operational condition of the blow-off valve should be evaluated. It is also recommended that the owner take necessary measures to improve the accessibility of the dam site.

SECTION 5
HYDRAULICS AND HYDROLOGY

5.1 Evaluation of Features

a. Design Data. Bear Rock No. 2 Dam has a watershed area of 1.4 square miles and impounds a reservoir with a surface area of 7.4 acres at normal pool level. The flood discharge facilities for the dam consist of a 33-foot-wide rectangular channel located on the left abutment. The capacity of the spillway was determined to be 858 cfs.

b. Experience Data. As previously stated, Bear Rock No. 2 Dam is classified to be an intermediate dam in the high hazard category. Under the recommended criteria for evaluating spillway discharge capacity, such impoundments are required to pass full PMF.

The PMF inflow hydrograph for the reservoir was determined utilizing the Dam Safety Version of the HEC-1 computer program developed by the Hydrologic Engineering Center of the U.S. Army, Corps of Engineers. Data used for the computer analysis are presented in Appendix D. The inflow hydrographs were found to have peak flows of 2822 cfs and 1411 cfs for full and 50 percent of the PMF, respectively. Computer input and a summary of computer output are also included in Appendix D.

c. Visual Observations. On the date of inspection, no conditions were observed that would indicate that the capacity of the spillway would be significantly reduced in the event of a flood.

d. Overtopping Potential. Various percentages of the PMF inflow hydrograph were routed through the reservoir and it was found that the spillway can pass 30 percent of the PMF without overtopping the low spot on the embankment. For 50 percent PMF, a low spot on the crest would be overtopped for a duration of 4.3 hours with a maximum depth of 0.55 foot. For full PMF, the overtopping duration would be 8.7 hours with a maximum depth of overtopping of 1.1 feet.

e. Spillway Adequacy. Since the spillway cannot pass the recommended spillway design flood of full PMF without overtopping the embankment, the spillway is classified to be inadequate according to the recommended criteria. A breach analysis was conducted to determine if the spillway is seriously inadequate; that is, if dam failure resulting from overtopping would significantly increase loss of life and property damage from that which would exist just before

overtopping failure. The results of the dam break analysis and the valley cross sections used for flood routing are included in Appendix D. It was found that failure of Bear Rock No. 2 Dam would in turn cause the failure of Bear Rock No. 1 Dam downstream. Therefore, for evaluating flood stages downstream of Bear Rock No. 1 Dam, breach discharges from both dams were considered.

Review of the flood stages in the potential damage area before and after failure indicates that flood stages would be raised by about 2 feet due to a dam failure, which is considered to be a significant increase in damage potential. Therefore, the spillway is classified to be seriously inadequate.

SECTION 6
STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

(1) Embankment. As discussed in Section 3, the field observations did not reveal any signs of distress that would significantly affect the performance of the embankment.

(2) Appurtenant Structures. The structural performance of the spillway structures is considered to be satisfactory. Because no portion of the outlet works except the downstream end of the blow-off pipe was visible, no conclusions were reached as to the structural adequacy of the outlet facilities. Flow through the outlet pipes is controlled by valves located on the downstream side; thus the pipes are always under pressure through the embankment. In view of this condition and since no design information is available to assess the structural adequacy of the outlet facilities, it is considered advisable that the structural adequacy of the outlet pipe be evaluated and a means for placing an upstream control on these pipes be developed.

b. Design and Construction Data

(1) Embankment. The dam was constructed in 1904 when limited understanding of geotechnical behavior of earth structures existed. Consequently, available design and construction information does not provide any quantitative data to aid in the assessment of stability. Since the embankment design lacks a positive internal drainage system, some concern exists as to the location of the phreatic surface through the embankment as it affects the stability of the embankment. However, at this time, no signs were observed that would indicate the phreatic surface is intersecting the downstream slope of the dam. As previously noted, the dam appears to have been constructed adequately and has performed satisfactorily since its construction. Therefore, based on visual observations, the static stability of the dam is considered to be adequate.

(2) Appurtenant Structures. Other than limited design drawings, no design and construction data are available for the appurtenant structures.

c. Operating Records. The structural stability of the dam is not considered to be affected by the operational features of the dam.

d. Post-Construction Changes. In 1937, one foot of additional fill was placed on the dam crest to increase the spillway capacity.

e. Seismic Stability. The dam is located in Seismic Zone 1, and based on visual observations, the static stability of the dam appears to be adequate. Therefore, based on the recommended criteria for evaluation of seismic stability of dams, the structure is presumed to present no hazards from earthquakes.

SECTION 7
ASSESSMENT AND RECOMMENDATIONS/PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. Assessment. The visual observations indicate that the embankment of Bear Rock No. 2 Dam is in good condition. However, in view of the seriously inadequate spillway capacity, the condition of the dam is assessed to be unsafe/nonemergency.

The spillway capacity was evaluated according to the recommended criteria and was found to pass 30 percent of the PMF without overtopping the embankment. This capacity is less than the recommended spillway capacity of full PMF according to the size and hazard classification for the dam. Further, because the spillway capacity is less than 50 percent of the PMF and it was found that failure of the dam would significantly increase the downstream damage potential, the spillway is classified to be seriously inadequate.

b. Adequacy of Information. The available information, in conjunction with the visual observations, is considered to be sufficient to make the following recommendations.

c. Urgency. The following recommendations should be implemented immediately or on a continuing basis.

d. Necessity for Additional Data. In view of the seriously inadequate spillway capacity, the owner should immediately initiate additional studies to more accurately ascertain the spillway capacity and the extent of improvements required to provide adequate spillway capacity.

7.2 Recommendations/Remedial Measures.

It is recommended that:

1. The owner should immediately retain a professional engineer to conduct additional studies to more accurately ascertain the spillway capacity and the nature and extent of improvements required to provide adequate spillway capacity.

2. The operational condition of the blow-off valve should be evaluated and necessary maintenance performed. A means for providing upstream control to the outlet pipes should be developed.

3. Brush and trees on the crest and downstream slope of the dam should be cleared.

4. Around-the-clock surveillance should be provided during unusually heavy runoff and a formal warning system developed to alert the downstream residents in the event of emergencies. It is also recommended that the owner take necessary measures to improve the accessibility of the site during high flows.

5. The dam and appurtenant structures should be inspected regularly and necessary maintenance should be performed.

APPENDIX A

CHECKLIST
VISUAL INSPECTION
PHASE I

APPENDIX A

CHECKLIST
VISUAL INSPECTION
PHASE I

NAME OF DAM Bear Rock No. 2 COUNTY Cambria STATE Pennsylvania ID# NDI I.D. PA-441 DER I.D. 11-3

TYPE OF DAM Earth HAZARD CATEGORY High

DATE(S) INSPECTION November 13, 1979 WEATHER Cloudy TEMPERATURE 40s

POOL ELEVATION AT TIME OF INSPECTION 2400 M.S.L. TAILWATER AT TIME OF INSPECTION 2350± M.S.L.

INSPECTION PERSONNEL:

Bilgin Erel

Wah Tak Chan

B. Erel

REVIEW INSPECTION PERSONNEL:
(December 28, 1979)

E. D'Appolonia

L. D. Andersen

J. H. Poellot

B. Erel RECORDER

VISUAL INSPECTION
PHASE I
EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS	None	
UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE	None	
SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES	None	
VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST	No perceivable misalignments. See Plate 6 for dam crest profile.	
RIPRAP FAILURES	None	

VISUAL INSPECTION
PHASE I
EMBANKMENT

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	No signs of distress.	
ANY NOTICEABLE SEEPAGE	A minor wet area along the toe near the right abutment. No associated seepage.	
STAFF GAGE AND RECORDER	None	
DRAINS	None	

VISUAL INSPECTION
PHASE I
OUTLET WORKS

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	The outlet pipe is a 16-inch cast-iron pipe. Only the downstream end of the pipe is visible.	
INTAKE STRUCTURE	Submerged	
OUTLET STRUCTURE	None	
OUTLET CHANNEL	An earth channel.	
EMERGENCY GATE	Operation of the outlet pipe was not observed.	Operational condition of the outlet pipe valve should be evaluated and necessary maintenance performed.

VISUAL INSPECTION
PHASE I
UNGATED SPILLWAY

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	In good condition.	
APPROACH CHANNEL	Submerged. Appears to be free of debris.	
DISCHARGE CHANNEL	A rectangular masonry channel. In good condition.	
BRIDGE AND PIERS	None	

VISUAL INSPECTION
PHASE I
GATED SPILLWAY

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE SILL	Not applicable	
APPROACH CHANNEL	Not applicable	
DISCHARGE CHANNEL	Not applicable	
BRIDGE PIERS	Not applicable	
GATES AND OPERATION EQUIPMENT	Not applicable	

VISUAL INSPECTION
PHASE I
INSTRUMENTATION

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
WEIRS	None	
PIEZOMETERS	None	
OTHER	None	

VISUAL INSPECTION
PHASE I
RESERVOIR

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SLOPES	Gentle to moderately steep. No significant shoreline erosion was noted.	
SEDIMENTATION	Unknown	
UPSTREAM RESERVOIRS	None	

VISUAL INSPECTION
PHASE I
DOWNSTREAM CHANNEL

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)	No apparent obstructions immediately downstream from the dam that would affect the discharge capacity of the spillway.	
SLOPES	No features pertinent to the safety of the dam.	
APPROXIMATE NUMBER OF HOMES AND POPULATION	The town of Lilly is located approximately 2-1/2 miles downstream from the dam. More than 20 homes are located in the potential flood plain. Population: approximately 200.	

APPENDIX B

CHECKLIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
AND HYDROLOGIC AND HYDRAULIC
PHASE I

APPENDIX B

CHECKLIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

NAME OF DAM Bear Rock No. 2

ID# NDI I.D. PA-441
DER I.D. 11-3

ITEM	REMARKS
AS-BUILT DRAWINGS	Limited design drawings are available in the state files.
REGIONAL VICINITY MAP	See Plate 1.
CONSTRUCTION HISTORY	The dam was designed and constructed by Pennsylvania Railroad Company in 1904.
TYPICAL SECTIONS OF DAM	See Plate 3.
OUTLETS - PLAN - DETAILS - CONSTRAINTS - DISCHARGE RATINGS	See Plate 3.

CHECKLIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

ITEM	REMARKS
RAINFALL/RESERVOIR RECORDS	Not available
DESIGN REPORTS	Not available
GEOLOGY REPORTS	Not available
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	Not available
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	Not available

CHECKLIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

ITEM	REMARKS
POST CONSTRUCTION SURVEYS OF DAM	None reported
BORROW SOURCES	Unknown
MONITORING SYSTEMS	None
MODIFICATIONS	In 1937, the crest of the dam was reshaped (see Plate 4).
HIGH POOL RECORDS	Not recorded

CHECKLIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

ITEM	REMARKS
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None reported
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	None reported
MAINTENANCE OPERATION RECORDS	Not maintained
SPILLWAY PLAN SECTIONS DETAILS	See Plate 3.
OPERATING EQUIPMENT PLANS AND DETAILS	Not available

CHECKLIST
ENGINEERING DATA
HYDROLOGIC AND HYDRAULIC

DRAINAGE AREA CHARACTERISTICS: 1.4 square miles

ELEVATION, TOP OF NORMAL POOL AND STORAGE CAPACITY: 2400 (92 acre-feet)

ELEVATION, TOP OF FLOOD CONTROL POOL AND STORAGE CAPACITY: 2404.4 (130 acre-feet)

ELEVATION, MAXIMUM DESIGN POOL: 2404.5 (design dam crest level)

ELEVATION, TOP OF DAM: 2404.4 (measured low spot)

SPILLWAY:

a. Elevation 2400

b. Type Concrete overflow

c. Width 33 feet

d. Length Not applicable

e. Location Spillover Adjacent to spillway

f. Number and Type of Gates None

OUTLET WORKS:

a. Type 16-inch cast-iron pipe

b. Location Center of embankment

c. Entrance Inverts 2370±

d. Exit Inverts 2350±

e. Emergency Drawdown Facilities 16-inch pipe

HYDROMETEOROLOGICAL GAGES:

a. Type None

b. Location None

c. Records None

MAXIMUM NONDAMAGING DISCHARGE: 850± cfs (spillway capacity)

APPENDIX C

PHOTOGRAPHS

LIST OF PHOTOGRAPHS
BEAR ROCK NO. 2 DAM
NDI I.D. PA-441
NOVEMBER 13, 1979

PHOTOGRAPH NO.	DESCRIPTION
1	Crest (looking west).
2	Spillway crest and approach channel.
3	Spillway crest and discharge channel.
4	Spillway plunge pool.
5	Blow-off pipe (16-inch diameter) and valve chamber.
6	Bear Rock No. 1 Dam (0.1 mile downstream).

Photograph No. 1

Crest (looking west).

Photograph No. 2

Spillway crest and approach channel.

Photograph No. 3

Spillway crest and discharge channel.

Photograph No. 4

Spillway plunge pool.

Photograph No. 5

Blow-off pipe (16-inch diameter) and valve chamber.

Photograph No. 6

Bear Rock No. 1 Dam (0.1 mile downstream).

APPENDIX D

HYDROLOGY AND HYDRAULICS ANALYSES

HYDROLOGY AND HYDRAULIC ANALYSIS
DATA BASE

NAME OF DAM: Bear Rock No. 2 Dam (NDI I.D. PA-441)

PROBABLE MAXIMUM PRECIPITATION (PMP) = 23.7 INCHES/24 HOURS[1]

STATION	1	2	3	4	5
Station Description	Reservoir	Dam	Bear Rock No. 1 Reservoir	Bear Rock No. 1 Dam	Downstream Routing[6]
Drainage Area (square miles)	1.42	-	0.55	-	-
Cumulative Drainage Area (square miles)	1.42	1.42	1.97	1.97	-
Adjustment of PMF for Drainage Area (%)[2]	Zone 7		Zone 7		
6 Hours	102	-	102	-	-
12 Hours	120	-	120	-	-
24 Hours	130	-	130	-	-
48 Hours	140	-	140	-	-
72 Hours	-	-	-	-	-
Snyder Hydrograph Parameters					
Zone[3]	24	-	24	-	-
C_p/C_t[4]	0.45/1.60	-	0.45/1.60	-	-
L (miles)[5]	2.3	-	1.4	-	-
L_{ca} (miles)[5]	0.9	-	0.8	-	-
$t_p = C_t(L \cdot L_{ca})^{0.3}$ (hours)	2.0	-	1.66	-	-
Spillway Data					
Crest Length (ft)	-	33.2	-	53.0	-
Freeboard (ft)	-	4.0	-	4.0	-
Discharge Coefficient	-	2.8	-	3.1	-
Exponent	-	1.5	-	1.5	-

(1) Hydrometeorological Report 33 (Figure 1), U.S. Army, Corps of Engineers, 1956.

(2) Hydrometeorological Report 33 (Figure 2), U.S. Army, Corps of Engineers, 1956.

(3) Hydrological zone defined by Corps of Engineers, Baltimore District, for determining Snyder's Coefficients (C_p and C_t).

(4) Snyder's Coefficients.

(5) L = Length of longest water course from outlet to basin divide.
L_{ca} = Length of water course from outlet to point opposite the centroid of drainage area.

(6) See Pages D8 through D18.

STORAGE VS. ELEVATION

ELEVATION	ΔH, FEET	AREA (ACRES)[1]	ΔVOLUME (ACRE-FEET)[2]	STORAGE (ACRE-FEET)
2420.0	15.5	17.5	207.8	333.8
2404.5		9.7[4]		130.5
	4.5		38.4	
2400.0		7.4		92.1
	37.5		92.1[3]	
Reservoir Bottom		-		0

(1) Planimetered from USGS maps.

(2) ΔVolume = $\Delta H/3\ (A_1 + A_2 + \sqrt{A_1 A_2})$.

(3) From PennDER files.

(4) Linearly interpolated.

```
**********
FLOOD HYDROGRAPH PACKAGE (HEC-1)
DAM SAFETY VERSION      JULY 197?
  LAST MODIFICATION   17 JAN 8?
**********
    1                 A1       SNYDER UNIT HYDROGRAPH,FLOOD ROUTING AND DAM OVERTOPPING ANALYSES
    2                 A2       BEAR ROCK NO.1 DAM,CAMBRIA COUNTY,NDI-I.D.PA.439     PROJECT NO.79-543-07
    3                 A3       FOR 20%,30%,40%,50%,60%,70%,80%,90%,AND 100% PMF
    4                 I     300          5        10         0         1         0         0         0        -4         0
    5                 O1      5
    6                 J       2         6         1
    7                 J1    0.30      0.40      0.50      0.70      0.90      1.00
    8                 A                 1                                                 1
    9                 K1       CALCULATION OF SNYDER INFLOW HYDROGRAPH TO BEAR ROCK #2 RESERVOIR(UPPER)
   10                 M       1         1      1.42                 1.42                                        1
   11                 P                23.7       102       120       130       140
   12                 T                                                                 1.0       .05                 0.0081
   13                 W     2.00      0.45
   14                 X     -1.0     -0.05       2.0
   15                 K       1         2                                                 1
   16                 K1       ROUTING FLOW THROUGH BEAR ROCK NO.2 DAM (NDI-I.D.PA.441)(UPPER)
   17                 Y                                       1         1
   18                 Y1      1                                                  -2400.0
   19                 $S    0.0      92.1     130.5     338.3
   20                 $E2362.5    2400.0    2404.5    2420.0
   21                 $$2400.0      33.2      2.80       1.5
   22                 $D2404.4      3.08      1.50     760.0
   23                 $L   50.0     150.0     250.0     450.0     550.0     680.0     760.0
   24                 $V2404.4    2404.5    2404.6    2404.7    2404.8    2404.9    2405.0
   25                 $B 100.0       1.0    2342.5       0.5    2400.0    2404.5
   26                 $B 100.0       1.0    2362.5       0.5    2400.0    2410.0
   27                 K       1         3                                                 1
   28                 K1       ROUTING FLOW THROUGH BEAR ROCK NO.1 DAM (LOWER)(NDI-I.D.PA.439)
   29                 Y                                       1         1
   30                 Y1      1                                                  -2344.0
   31                 $S    0.0      29.8      50.9     146.5
   32                 $E2323.0    2344.0    2348.0    2360.0
   33                 $$2344.0      58.0       3.1       1.5
   34                 $D2348.0      3.08       1.5     560.0
   35                 $L   30.0     210.0     410.0     460.0     560.0
   36                 $V2348.0    2348.1    2348.2    2348.3    2348.4
   37                 $B 100.0      3.33    2320.0       0.5    2344.0    2348.1
   38                 K       1         4                                                 1
   39                 K1       CHANNEL ROUTING USING MODIFIED PLUS: REACH 1-2(MILE 0.04 TO 0.28)
   40                 Y                                       1         1
   41                 Y1      1
   42                 Y6 0.045    0.028     0.045    2220.0    2239.0    1267.00.078914
   43                 Y7    0.0    2239.0      63.0    2230.0     125.0    2221.0     127.0    2220.0     143.0    2220.0
   44                 Y7 145.0    2221.0     220.0    2230.0     295.0    2239.0
   45                 K       1         5                                                 1
   46                 K1       CHANNEL ROUTING USING MODIFIED PLUS: REACH 2-3(MILE 0.28 TO 0.70)
   47                 Y                                       1         1
   48                 Y1      1
   49                 Y6 0.045    0.028     0.045    2120.0    2139.0    2218.00.045094
   50                 Y7    0.0    2139.0      63.0    2130.0     125.0    2121.0     127.0    2120.0     143.0    2120.0
```

COMPUTER INPUT: PLAN 1 - DAM BREAK ANALYSIS AND DOWNSTREAM ROUTING
PLAN 2 - OVERTOPPING ANALYSIS AND DOWNSTREAM ROUTING

```
Y7 145.   2121.0   225.0  2130.0   295.0  2139.0
K      1       6                                                1
K1       CHANNEL ROUTING USING MODIFIED PLUS: REACH 3-4(MILE 0.70 TO 1.24)
Y                                      1       1
Y1     1
Y6 0.035   0.029   0.045  2020.0  2039.0  2851.00.020584
Y7   0.0  2039.0   215.0  2030.0   425.0  2021.0   427.0  2020.0   443.0  2020.0
Y7 445.0  2021.0   495.0  2030.0   545.0  2039.0
K      1       7                                                1
K1       CHANNEL ROUTING USING MODIFIED PLUS: REACH 4-5(MILE 1.24 TO 1.73)
Y                                      1       1
Y1     1
Y6 0.026   0.029   0.045  1940.0  1959.0  2587.00.038652
Y7   0.0  1959.0   100.0  1952.0   150.0  1952.0   300.0  1941.0   302.0  1940.0
Y7 318.0  1940.0   320.0  1941.0   420.0  1959.0
K      1       8                                                1
K1       CHANNEL ROUTING USING MODIFIED PLUS: REACH 5-6(MILE 1.73 TO 2.80)
Y                                      1       1
Y1     1
Y6 0.026   0.029   0.026  1860.0  1879.0  5650.00.014160
Y7   0.0  1879.0   100.0  1861.0   102.0  1860.0   125.0  1860.0   125.0  1861.0
Y7 425.0  1872.0   475.0  1872.0   625.0  1879.0
K     99
```

COMPUTER INPUT: CONTINUED

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATI
FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS					
				RATIO 1 .30	RATIO 2 .40	RATIO 3 .50	RATIO 4 .70	RATIO 5 .90	RATIO 6 1.00
HYDROGRAPH AT	1	1.42	1	847.	1129.	1411.	1975.	2540.	2822.
	(	3.68)	(	23.97)(	31.96)(	39.96)(	55.94)(	71.92)(	79.91)(
			2	847.	1129.	1411.	1975.	2540.	2822.
			(	23.97)(	31.96)(	39.96)(	55.94)(	71.92)(	79.91)(
ROUTED TO	2	1.42	1	827.	5606.	5662.	5692.	5576.	5670.
	(	3.68)	(	23.42)(	158.75)(	160.33)(	161.18)(	157.91)(	160.55)(
			2	827.	1124.	1407.	1974.	2539.	2821.
			(	23.42)(	31.81)(	39.85)(	55.89)(	71.89)(	79.88)(
ROUTED TO	3	1.42	1	825.	6605.	6668.	6692.	6608.	6651.
	(	3.68)	(	23.37)(	187.04)(	188.82)(	189.50)(	187.11)(	188.33)(
			2	825.	1120.	1405.	3968.	4061.	4111.
			(	23.37)(	31.71)(	39.78)(	112.36)(	114.99)(	116.42)(
ROUTED TO	4	1.42	1	826.	6510.	6592.	6624.	6521.	6583.
	(	3.68)	(	23.38)(	184.35)(	186.67)(	187.57)(	184.66)(	186.42)(
			2	826.	1120.	1404.	3666.	3755.	3808.
			(	23.38)(	31.71)(	39.77)(	103.81)(	106.32)(	107.84)(
ROUTED TO	5	1.42	1	826.	6054.	6156.	6200.	6074.	6163.
	(	3.68)	(	23.38)(	171.42)(	174.32)(	175.57)(	171.98)(	174.52)(
			2	826.	1120.	1404.	3563.	3711.	3767.
			(	23.38)(	31.70)(	39.77)(	100.89)(	105.09)(	106.68)(
ROUTED TO	6	1.42	1	825.	6120.	6227.	6275.	6146.	6196.
	(	3.68)	(	23.36)(	173.31)(	176.33)(	177.68)(	174.03)(	175.44)(
			2	825.	1118.	1404.	3551.	3677.	3732.
			(	23.36)(	31.67)(	39.77)(	100.56)(	104.11)(	105.69)(
ROUTED TO	7	1.42	1	825.	6150.	6264.	6315.	6176.	6244.
	(	3.68)	(	23.36)(	174.14)(	177.37)(	178.81)(	174.88)(	176.82)(
			2	825.	1119.	1404.	3369.	3483.	3541.
			(	23.36)(	31.68)(	39.76)(	95.40)(	98.63)(	100.28)(
ROUTED TO	8	1.42	1	823.	5069.	5186.	5246.	5105.	5160.
	(	3.68)	(	23.29)(	143.55)(	146.84)(	148.56)(	144.56)(	146.12)(
			2	823.	1114.	1400.	3173.	3312.	3373.
			(	23.29)(	31.54)(	39.65)(	89.86)(	93.78)(	95.50)(

SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	2400.00	2400.00	2404.40
STORAGE	92.	92.	130.
OUTFLOW	0.	0.	858.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.3[illegible]	2404.29	0.00	129.	827.	0.00	42.17	0.00
.40	2404.55	.15	131.	7424.	.25	41.21	41.00
.50	2404.56	.16	131.	7490.	.25	40.71	40.50
.70	2404.60	.20	132.	7517.	.41	40.04	39.83
.9[illegible]	2404.52	.12	131.	7402.	.24	39.21	39.00
1.00	2404.60	.20	132.	7486.	.41	39.04	38.83

PLAN 2 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	2400.00	2400.00	2404.40
STORAGE	92.	92.	130.
OUTFLOW	0.	0.	858.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.30	2404.29	0.00	129.	827.	0.00	42.17	0.00
.40	2404.77	.37	134.	1124.	3.00	41.83	0.00
.50	2404.95	.55	136.	1407.	4.33	41.67	0.00
.70	2405.18	.78	140.	1974.	6.33	41.67	0.00
.9[illegible]	2405.37	.97	142.	2539.	7.83	41.67	0.00
1.00	2405.45	1.05	143.	2821.	8.67	41.67	0.00

PLAN 1 - DAM BREACH ANALYSIS SUMMARY (BEAR ROCK NO. 2 DAM BREACHED)
PLAN 2 - OVERTOPPING ANALYSIS SUMMARY (BEAR ROCK NO. 1 DAM OVERTOPPED)

SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	2344.00	2344.00	2348.00
STORAGE	30.	30.	51.
OUTFLOW	0.	0.	1438.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.5	2346.76	0.76	44.	825.	0.00	42.33	0.00
.6	2349.45	1.45	62.	7461.	.33	41.41	41.17
.5	2349.46	1.46	63.	7581.	.33	40.91	40.67
.7	2349.47	1.47	63.	7631.	.33	40.25	40.00
.9	2349.43	1.43	62.	7483.	.33	39.41	39.17
1.0	2349.46	1.46	63.	7546.	.33	39.25	39.00

PLAN 2 .....

	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	2344.00	2344.00	2348.00
STORAGE	30.	30.	51.
OUTFLOW	0.	0.	1438.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
.30	2346.76	0.00	44.	825.	0.00	42.33	0.00
.40	2347.38	0.00	48.	1120.	0.00	42.00	0.00
.50	2347.94	0.00	51.	1405.	0.00	41.83	0.00
.70	2348.21	.21	53.	4787.	.42	41.05	40.83
.90	2348.24	.24	53.	4887.	.42	40.55	40.33
1.00	2348.27	.27	53.	4934.	.43	40.38	40.17

PLAN 1 STATION 4

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	826.	2221.9	42.33
.40	6510.	2225.2	41.33
.50	6592.	2225.2	40.83
.70	6624.	2225.2	40.17
.90	6521.	2225.2	39.33
1.00	6583.	2225.2	39.17

DAM BREACH ANALYSIS (BEAR ROCK NO. 1 DAM BREACHED) AND DOWNSTREAM CHANNEL ROUTING
PLAN 1 - BEAR ROCK NO. 2 DAM BREACHED
PLAN 2 - BEAR ROCK NO. 2 DAM OVERTOPPED

PLAN 2 STATION 4

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	826.	2221.9	42.33
.40	1120.	2222.2	42.00
.50	1404.	2222.5	41.83
.70	3666.	2224.0	41.00
.90	3755.	2224.0	40.50
1.00	3808.	2224.1	40.33

PLAN 1 STATION 5

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	826.	2122.2	42.33
.40	6054.	2125.7	41.33
.50	6156.	2125.7	40.83
.70	6200.	2125.8	40.17
.90	6074.	2125.7	39.33
1.00	6163.	2125.7	39.17

PLAN 2 STATION 5

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	826.	2122.2	42.33
.40	1120.	2122.5	42.00
.50	1404.	2122.9	42.00
.70	3563.	2124.5	41.17
.90	3711.	2124.5	40.67
1.00	3767.	2124.6	40.50

PLAN 1 STATION 6

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	825.	2022.5	42.33
.40	6120.	2025.7	41.50
.50	6227.	2025.8	41.00
.70	6275.	2025.8	40.33
.90	6146.	2025.7	39.50
1.00	6196.	2025.7	39.33

PLAN 2 STATION 6

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	825.	2022.5	42.33
.40	1118.	2022.8	42.17
.50	1404.	2023.1	42.00
.70	3551.	2024.6	41.17
.90	3677.	2024.7	40.67
1.00	3732.	2024.7	40.50

PLAN 1 STATION 7

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	825.	1942.3	42.50
.40	6150.	1945.6	41.50
.50	6264.	1945.6	41.00
.70	6315.	1945.6	40.33
.90	6176.	1945.6	39.50
1.00	6244.	1945.6	39.33

PLAN 2 STATION 7

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	825.	1942.3	42.50
.40	1119.	1942.7	42.17
.50	1404.	1943.0	42.00
.70	3369.	1944.4	41.17
.90	3483.	1944.4	40.67
1.00	3541.	1944.5	40.50

PLAN 1 STATION 8

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	823.	1862.5	42.67
.40	5069.	1865.2	41.67
.50	5186.	1865.2	41.17
.70	5246.	1865.3	40.50
.90	5105.	1865.2	39.67
1.00	5160.	1865.2	39.50

PLAN 2 STATION 8

RATIO	MAXIMUM FLOW,CFS	MAXIMUM STAGE,FT	TIME HOURS
.30	823.	1862.5	42.67
.40	1114.	1862.9	42.33
.50	1400.	1863.2	42.17
.70	3173.	1864.3	41.33
.90	3312.	1864.4	40.83
1.00	3373.	1864.4	40.67

DAMPOLONIA
CONSULTING ENGINEERS INC

By MB Date 2/7/80 Subject BEAR ROCK # 2 DAM Sheet No. 1 of 1
Chkd. By BE Date 2/18/80 STATION LOCATIONS. Proj. No. 79-543-07

(8) D 9 of 13

DAMTECHNOLOGY
CONSULTING ENGINEERS INC

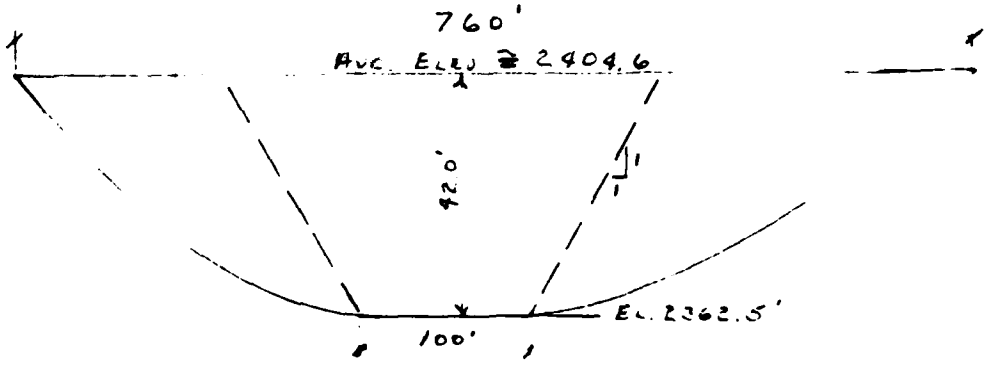
By MB Date 2/6/80 Subject DAM BREACH - Sheet No. 1 of 1
Chkd. By ___ Date ___ BEAR ROCK # 2 DAM Proj No 79-59-08

DAM CREST ELEV. - 2409.5

LENGTH - 760.0'

ASSUME TIME FOR BREACH - 0.5 HOURS

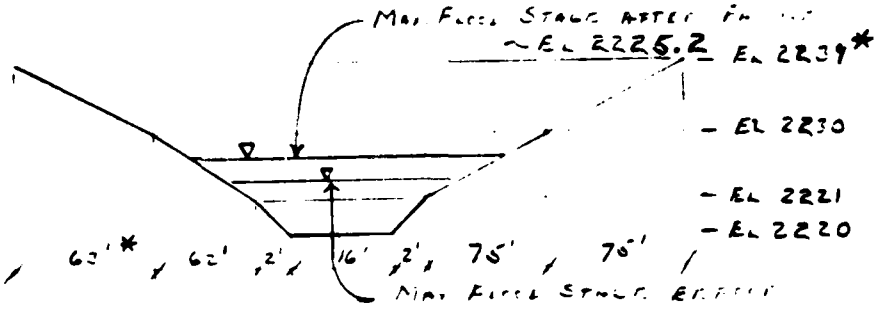
FROM DER DRAWINGS, THE FOLLOWING DAM PROFILE IS ASSUMED



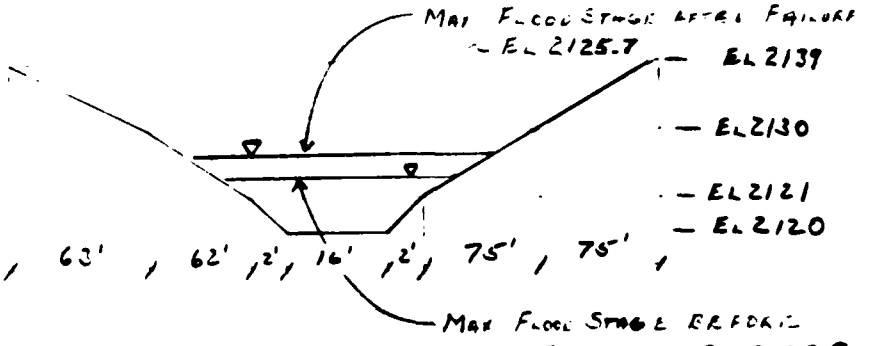
ASSUMED BREACH
BEAR ROCK # 2 DAM

DAMPOLONIA
CONSULTING ENGINEERS INC

By MB Date 2/7/80 Subject SECTIONS USED FOR DOWNSTREAM ROUTING Sheet No. 1 of 3
Chkd By ___ Date ___ Proj. No. 79-593-07



SECTION AT STATION 4
(NO SCALE)

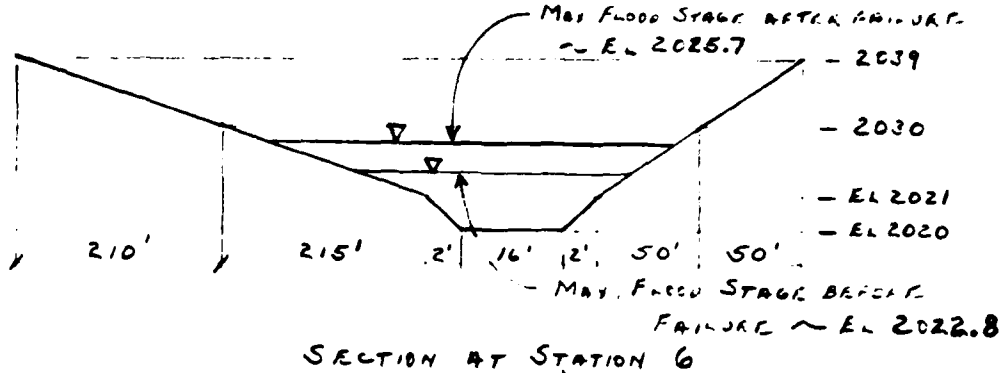


SECTION AT STATION 5
(NO SCALE)

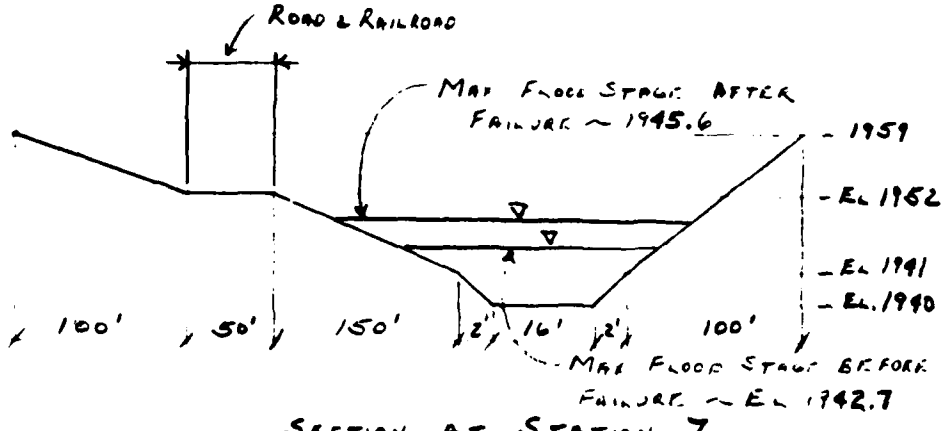
* ALL ELEVATIONS & DISTANCES ARE APPROXIMATE

DAPPOLONIA
CONSULTING ENGINEERS, INC

By MB Date 2/7/80 Subject SECTIONS USED FOR DOWNSTREAM ROUTING Sheet No. 2 of 3
Chkd. By ___ Date ___ Proj No. 79-593-07



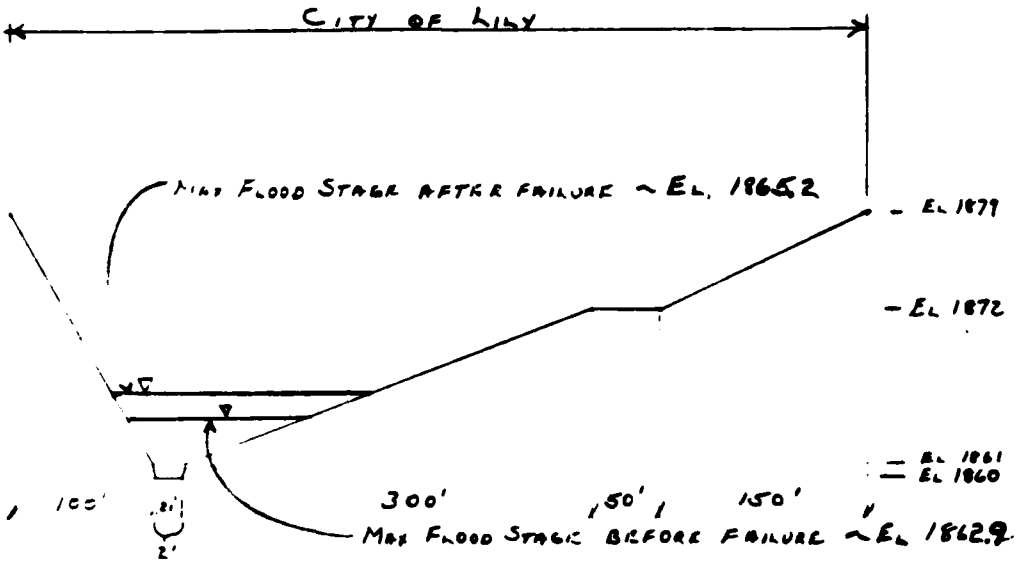
SECTION AT STATION 6
(NO SCALE)



SECTION AT STATION 7
(NO SCALE)

D'APPOLONIA
CONSULTING ENGINEERS, INC

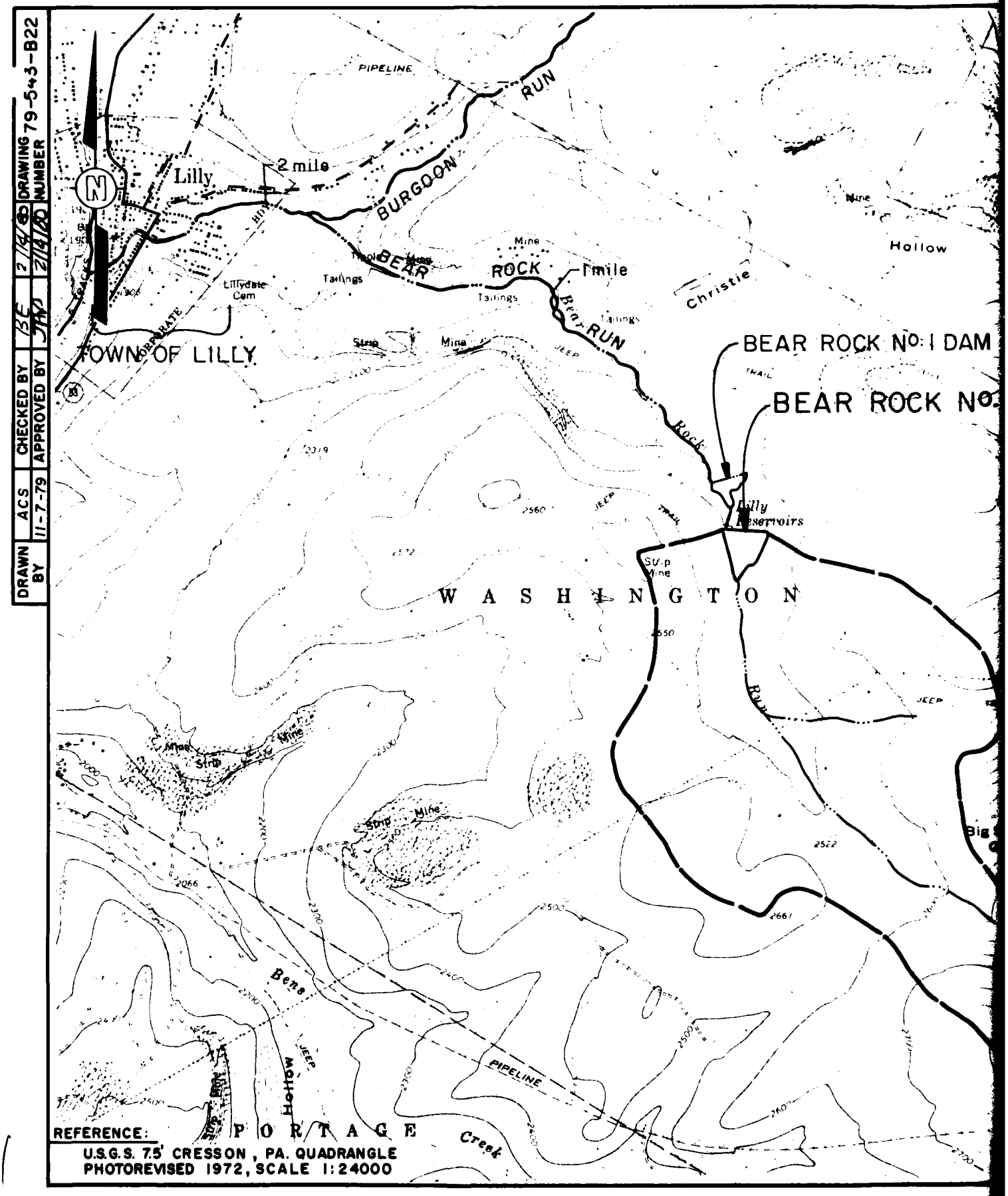
By MB Date 2/7/80 Subject SECTIONS USED FOR Sheet No. 3 of 3
Chkd. By ___ Date ___ DOWNSTREAM ROUTING Proj. No. 79-543-07

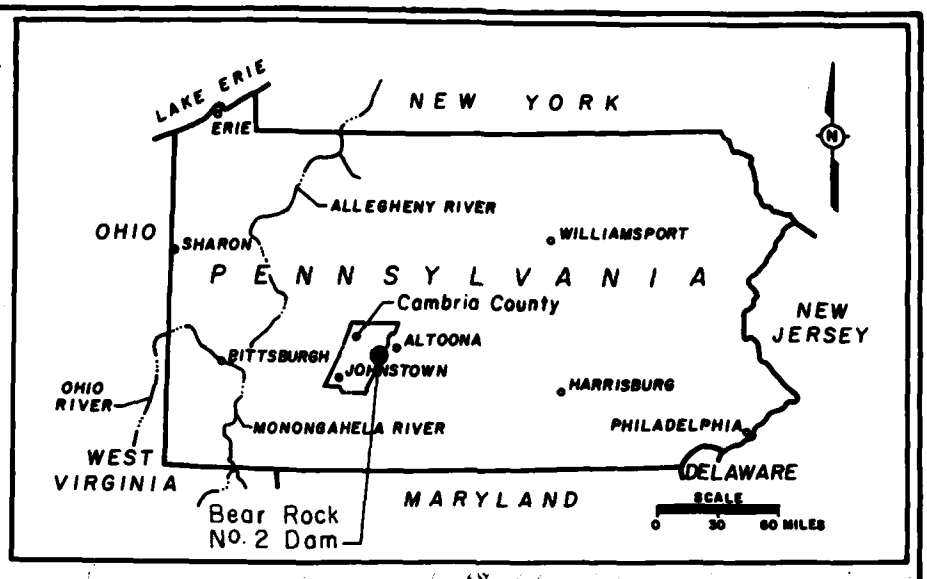


SECTION AT STATION 8
SCALE : VERTICAL : 1" = 10'
HORIZONTAL : 1" = 100'

APPENDIX E

PLATES


DRAWN BY ACS 11-7-79
CHECKED BY JSE 2/14/80
APPROVED BY JHD 2/14/80
DRAWING NUMBER 79-543-B22
PIPELINE
RUN
BURGOON
2 mile
Lilly
BEAR ROCK
1 mile
Tailings
Mine
Hollow
Christie
Bear RUN
TOWN OF LILLY
BEAR ROCK No. 1 DAM
BEAR ROCK No.
Rock
Lilly Reservoirs
Strip Mine
W A S H I N G T O N
Run
JEEP
TRAIL
Bens
Hollow
P O R T A G E
Creek
REFERENCE:
U.S.G.S. 7.5' CRESSON, PA. QUADRANGLE
PHOTOREVISED 1972, SCALE 1:24000



KEY PLAN

Gap

Laurel Gap

M

0.2 DAM

STATE GAME LANDS
NO 198

APPROXIMATE WATERSHED AREA

INDEFINITE

CAMBRIA CO
BLAIR CO

ig Spring Gap

Spring

SCALE
0 1000 2000 3000 4000 5000 FEET

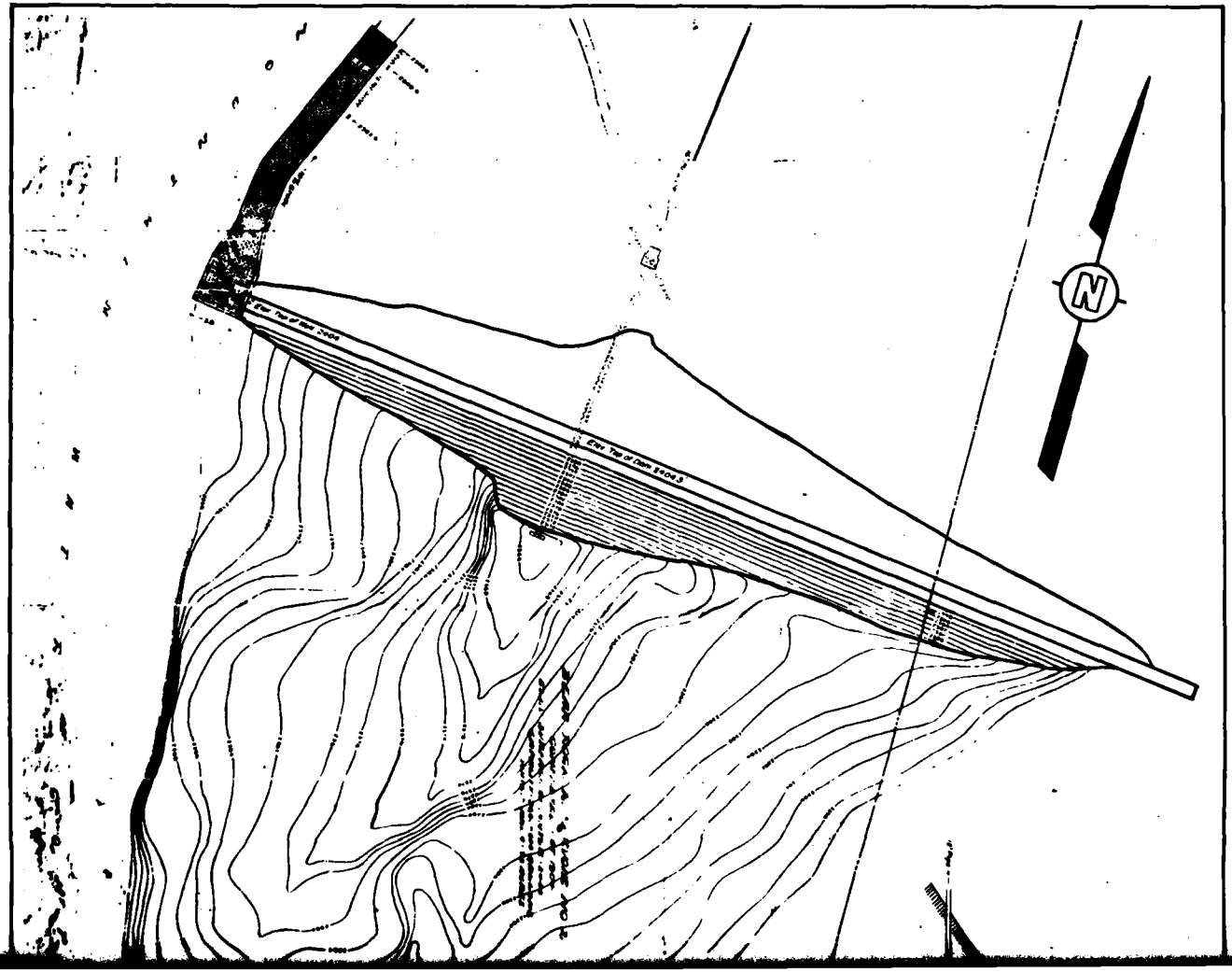
PLATE 1

BEAR ROCK No. 2 DAM
VICINITY, FLOOD PLAIN & WATERSHED MAP

D'APPOLONIA

2

DRAWN BY	ACS	CHECKED BY	BC	2/9/80	DRAWING NUMBER	79-543-B23
	11-8-79	APPROVED BY	JHP	2/14/80		



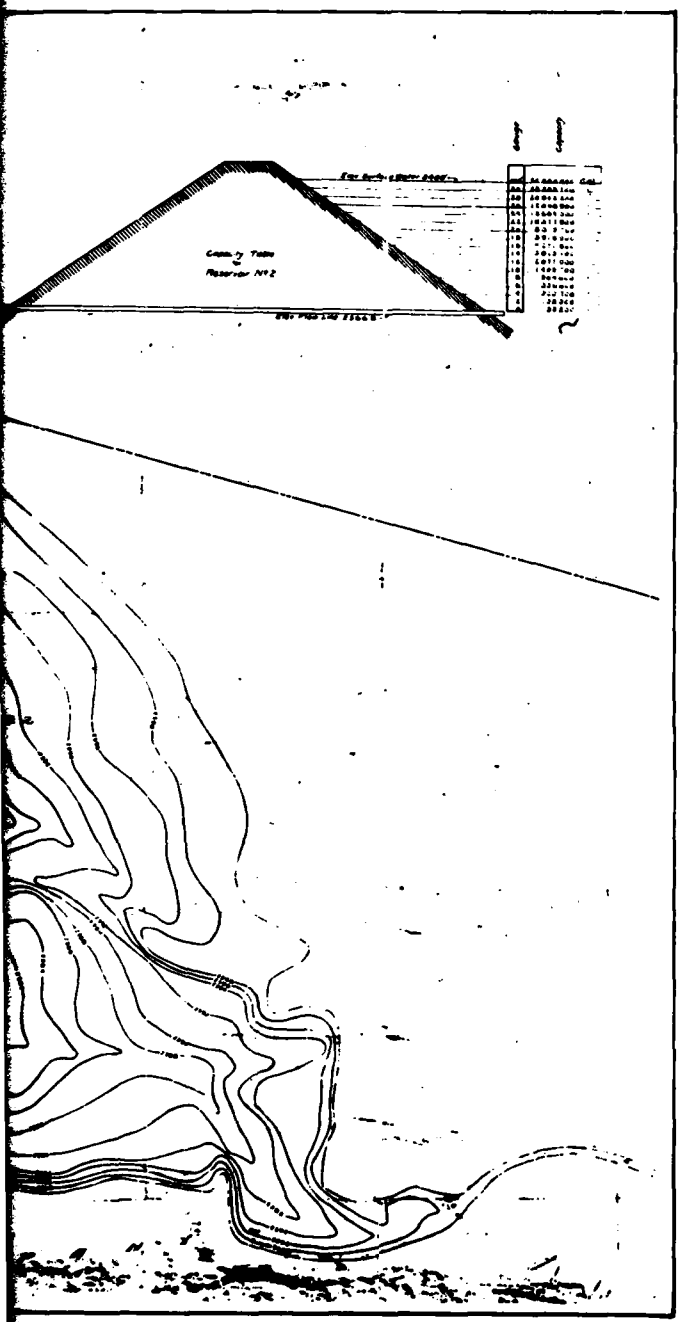


PLATE 2

D'APPOLONIA

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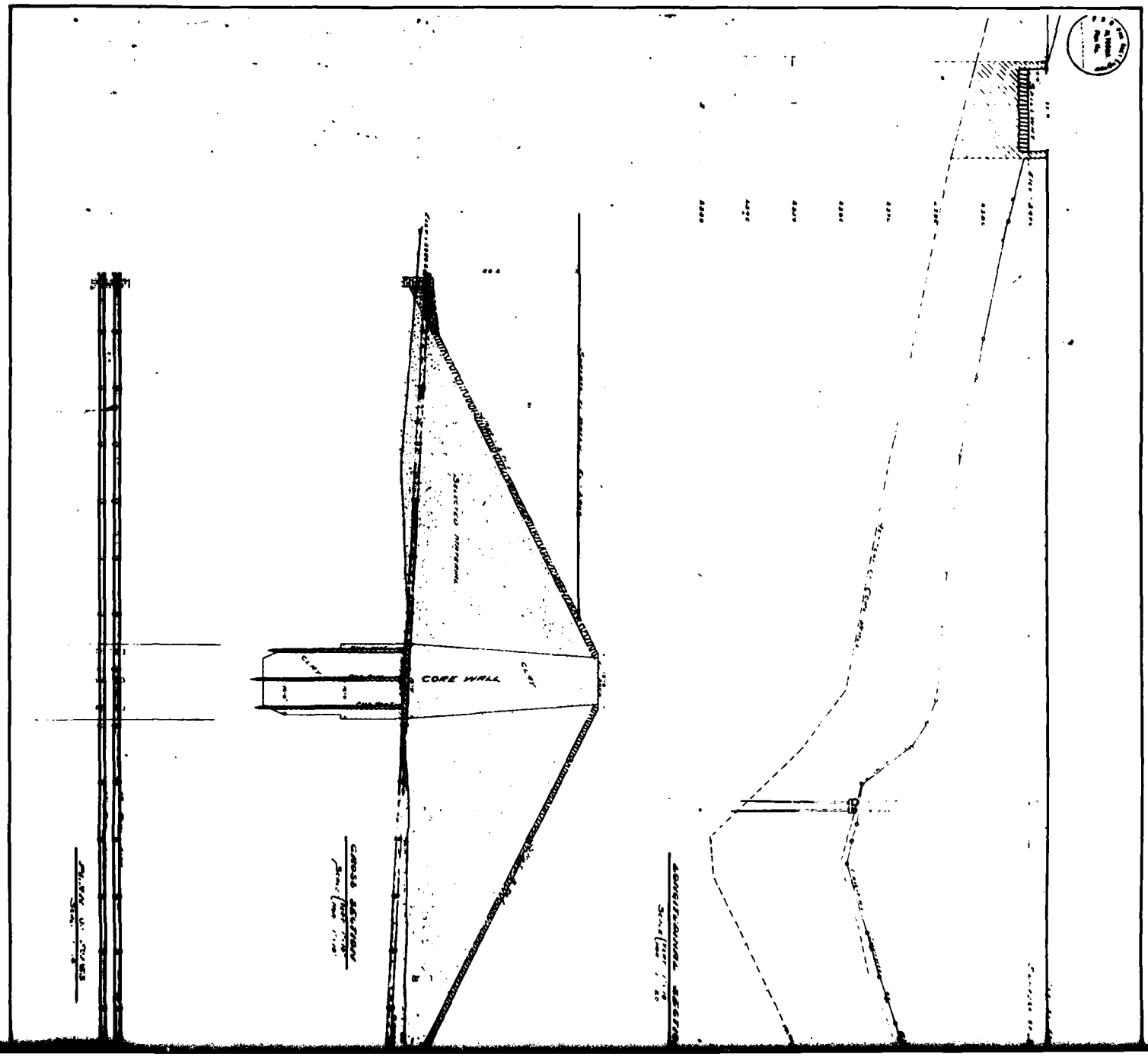
	11-8-79	APPROVED BY	JAP	2/14/80	



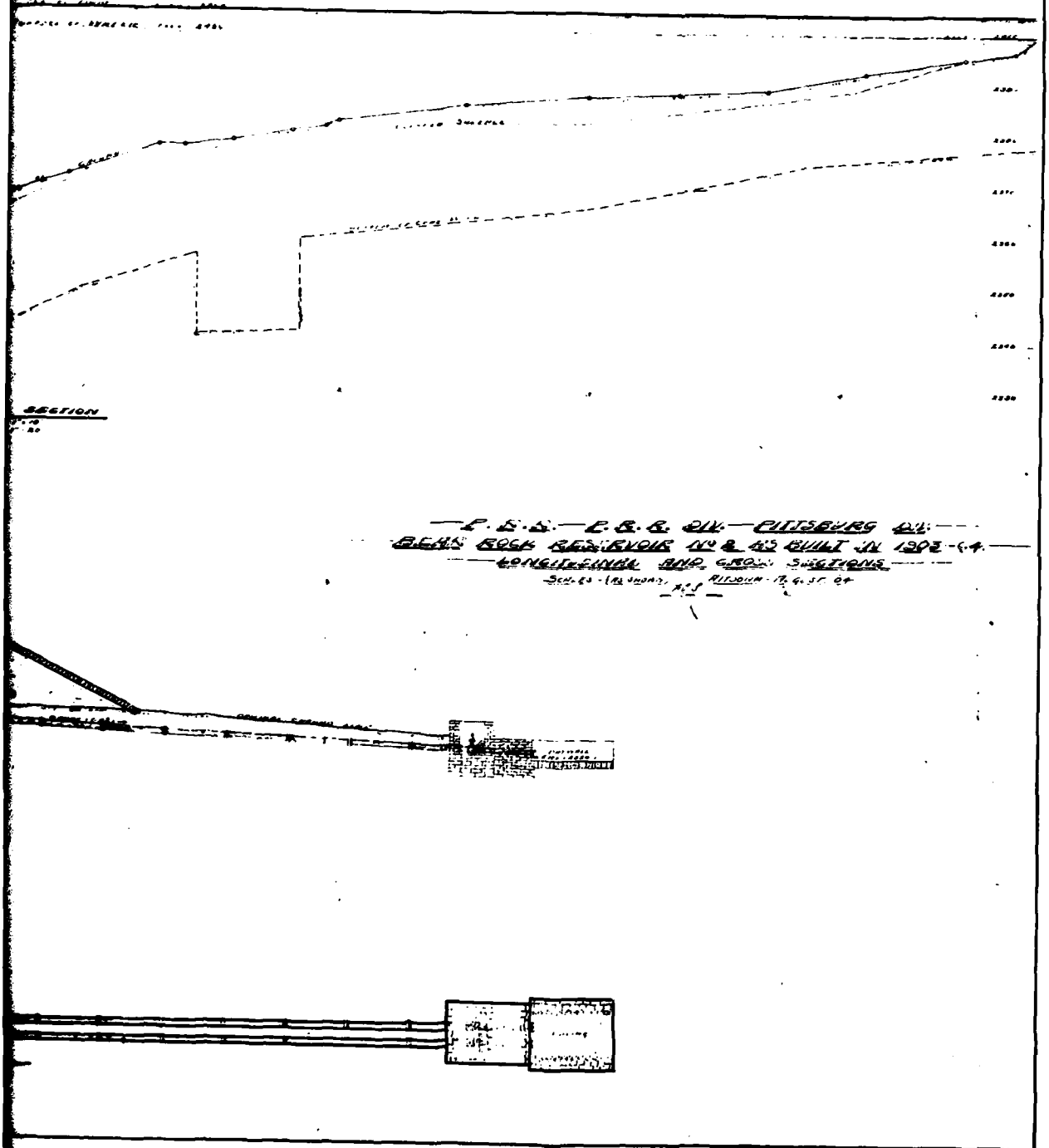


PLATE 3

D'APPOLONIA

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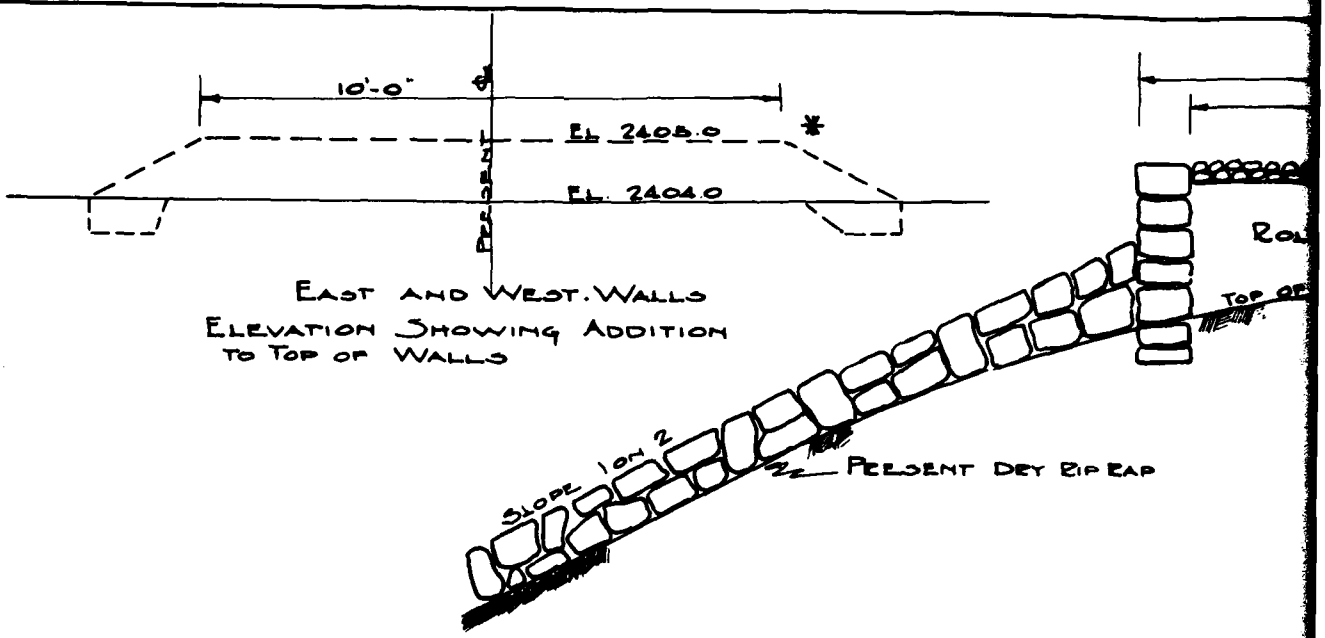
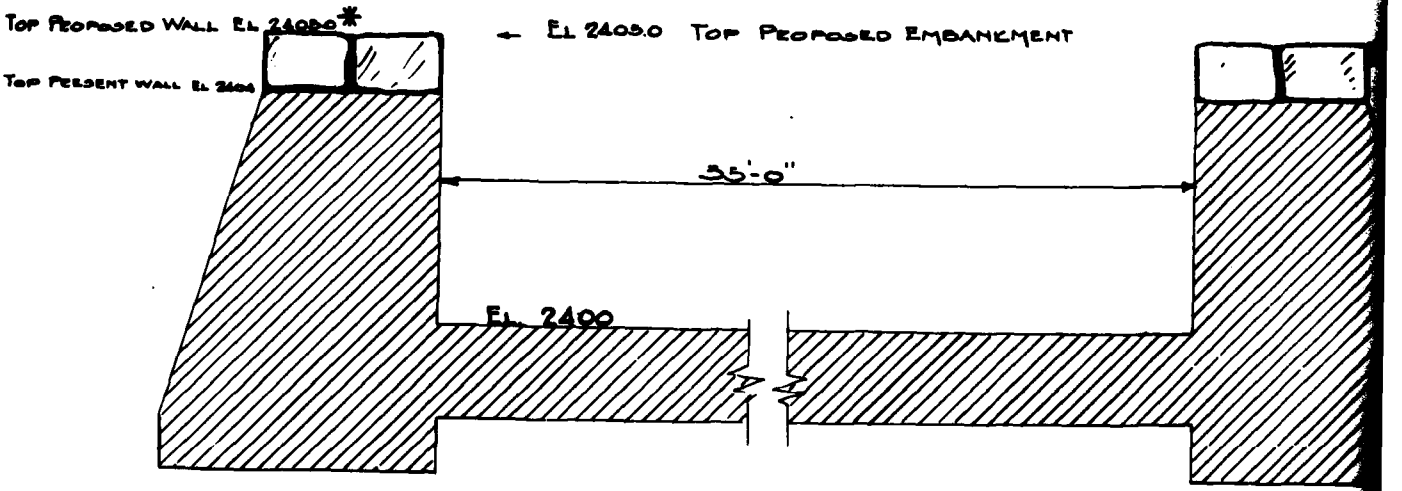
	11-8-79	APPROVED BY	JAD	

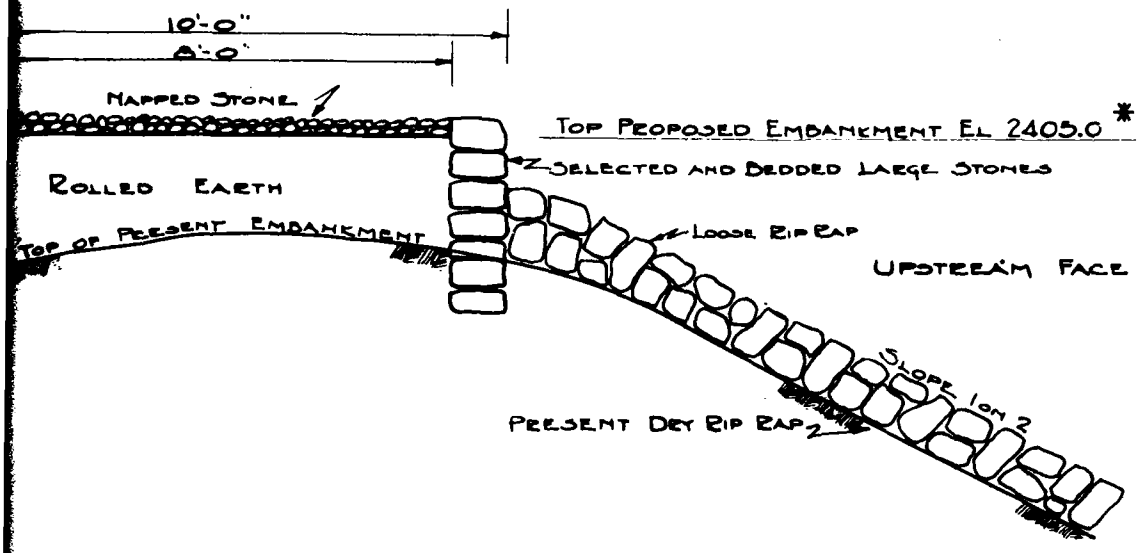


EAST AND WEST WALLS
ELEVATION SHOWING ADDITION
TO TOP OF WALLS



CROSS SECTION OF SPILLWAY
LOOKING UPSTREAM

* ASSUMING THE SPILLWAY CREST TO BE AT EL. 2400
THE ELEVATION WAS SURVEYED TO BE AT EL. 2404.5

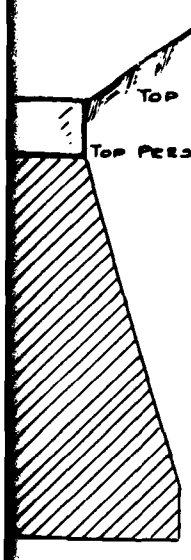


Note:

All stone to be cleaned from top of embankment and same to be thoroughly harrowed before depositing new earth.

New earth to be placed in not over 6" layers, dampened and rolled with not less than 10 passes on each layer of 5 ton roller.

Earth to be placed full and hand dressed after bringing to El 2405.



Summit Water Supply Company
Bear Rock Dam No. 2
Proposed Increase in Height

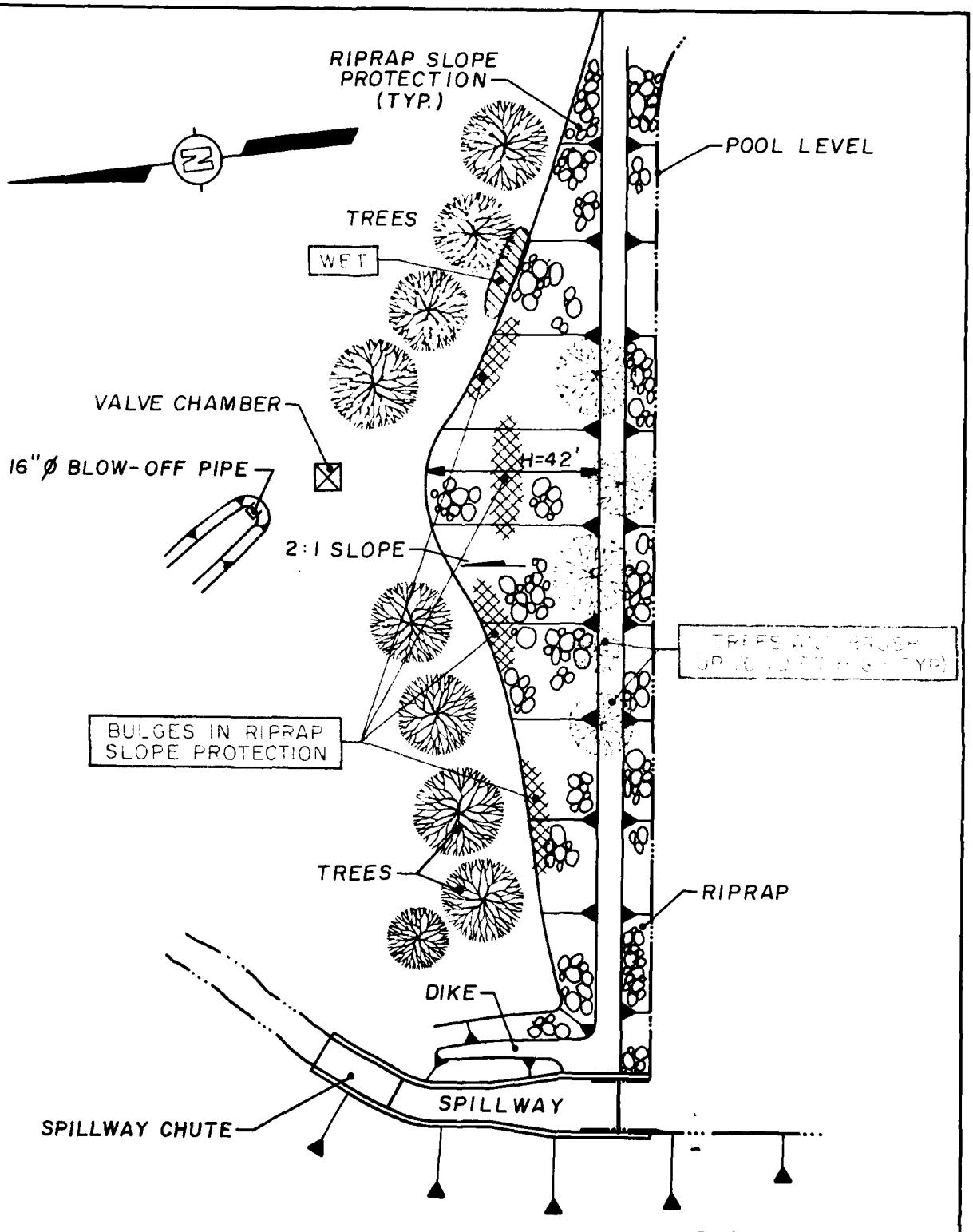
Scale 1"=2' E.E.W. Apr. 20, 1937
Office of Manager

24
TT

PLATE 4

D'APPOLONIA

DRAWN BY	ACS	CHECKED BY	RSC	DRAWING NUMBER	79-543-A21
	11-30-79	APPROVED BY	JAD	2/14/80	



NOTES:

1. POOL LEVEL DATE OF INSPECTION: AT SPILLWAY CREST

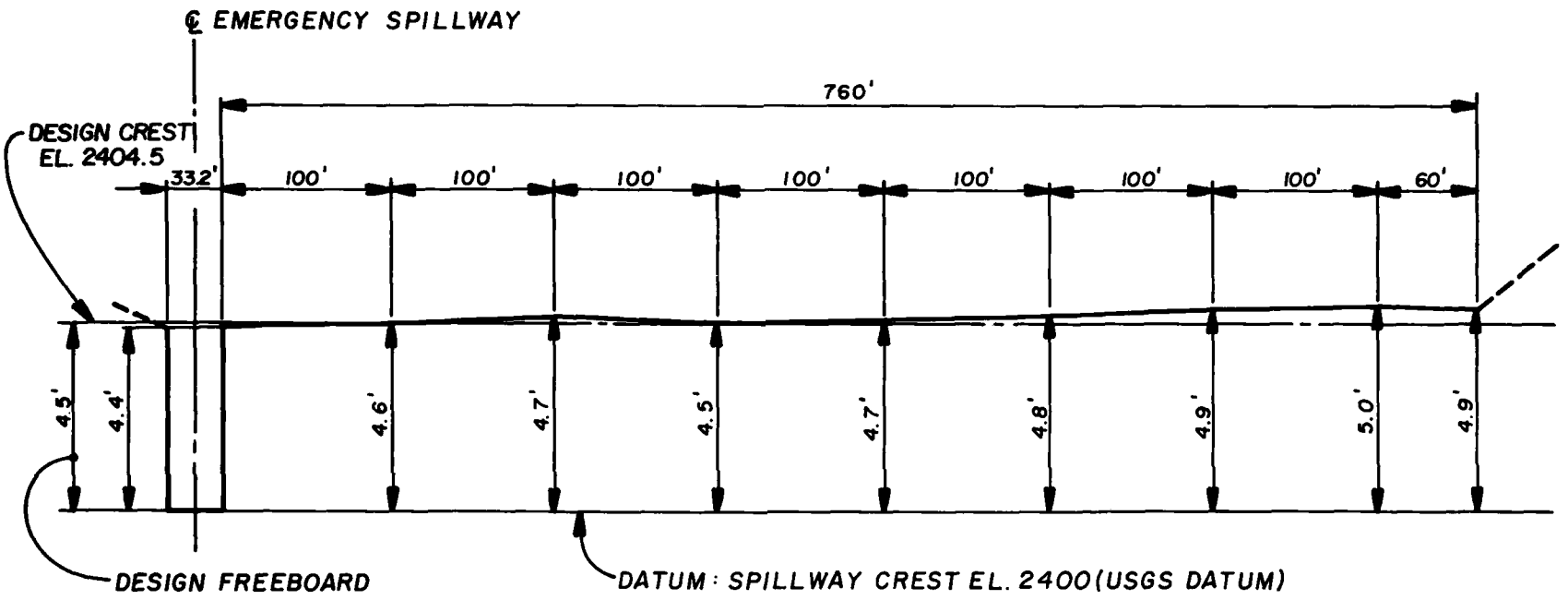
NOT TO SCALE

PLATE 5

BEAR ROCK Nº 2 DAM
GENERAL PLAN
FIELD INSPECTION NOTES
FIELD INSPECTION DATE: NOV. 13, 1979

D'APPOLONIA

DRAWN BY	ACS	CHECKED BY			DRAWING NUMBER 79-[illegible].3-A22
	11-30-79	APPROVED BY		2/14/80	



DAM CREST PROFILE
(LOOKING DOWNSTREAM)

NOTES:

1. DAM CREST IS SURVEYED RELATIVE TO SPILLWAY CREST LEVEL.
2. DATUM ELEVATION PER DESIGN DRAWINGS.

PLATE 6

BEAR ROCK No. 2 DAM
DAM CREST SURVEY
FIELD INSPECTION DATE: NOV. 13 & 20, 79

DAMPLONIA

APPENDIX F

REGIONAL GEOLOGY

APPENDIX F

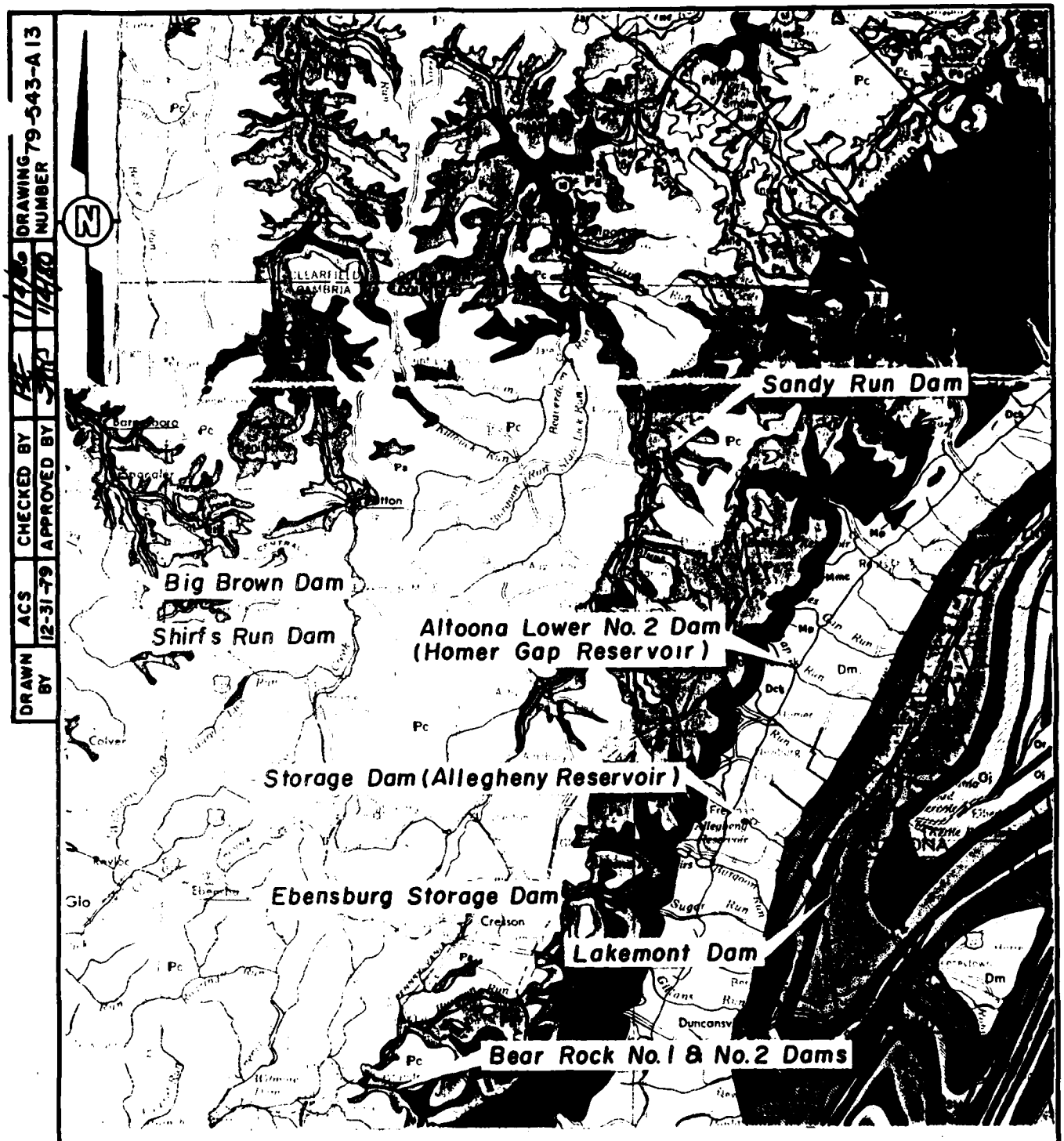
REGIONAL GEOLOGY

Bear Rock Nos. 1 and 2 dams are located in the eastern portion of Cambria County. The dams are located in the Allegheny Mountains section of the Appalachian Plateau Physiographic Province, an area characterized by parallel ridge and valley sequences controlled by the relatively gentle folding of the strata. The fold axis trends north-northeast and the strata dip in the area of the dams approximately 500 feet per mile to the northwest. Approximately one mile east of the reservoirs is the Allegheny Front, which separates the more gentle geologic folding to the west from the tight folding and faulting east of the front. In general, the discontinuities trend north-northeast and northwest.

The strata underlying the dams and reservoir consist of the Upper Pottsville Group and the Allegheny Group (Pennsylvanian Age). The Pottsville Group consists of two massive sandstone beds, shales, and one thin coal seam (the Mercer bed). The higher portion of the Pottsville Group consists of the Upper Conoquenessing Sandstone, a thick-bedded micaceous sandstone which is generally resistant to weathering. The thickness ranges from 15 to 25 feet. Below the sandstone is approximately 15 to 40 feet of thin-bedded shale with interbedded sandstone. These strata weather easily. Below the shale is the Lower Conoquenessing Sandstone, which is approximately 50 feet thick and is similar to the upper sandstone.

The strata overlying the Pottsville Group are the Allegheny Group, consisting of sandstone, shale, and at least seven coal seams. The group is approximately 250 feet thick. The strata from the base up consist of the Brookville coal seam, the Clarion Sandstone, the Clarion coal, and a thick sandstone below the Lower Kittanning coal bed, which is approximately 75 feet above the Brookville coal bed. The middle portion of the Allegheny Group consists of the Lower, Middle, and Upper Kittanning coal seams, and the Lower and Upper Worthington sandstones. One limestone bed is present below the Upper Kittanning coal seam. The upper portion of the group consists of the Lower and Upper Freeport coal seams and the Freeport and Rutlen sandstone beds. The overlying Conemaugh Group consist predominantly of shale and claystone with thin sandstone, limestone, and coal seams.

There is no minable coal beneath the dams and reservoirs. The strip mines on the slopes west and northeast of the reservoirs are probably the Lower Kittanning coal beds. The slopes above the reservoirs are relatively gentle, in general greater than 5 to 1, and probably consist predominantly of sandstone. Therefore, there should be no danger of large slides.



DRAWN BY	ACS	CHECKED BY		DRAWING NUMBER	79-343-A13
	12-31-79	APPROVED BY			

SCALE

0 2 4 6 8 10 miles

REFERENCE:

GEOLOGIC MAP OF PENNSYLVANIA PREPARED BY COMMONWEALTH OF PENNA., DEPT. OF INTERNAL AFFAIRS, DATED 1960, SCALE 1" = 4 MILES

SANDY RUN, BIG BROWN, SHIRFS RUN EBENSBURG STORAGE, LAKEMONT, BEAR ROCK NO. 1 AND NO. 2 DAMS, (ALLEGHENY RESERVOIR) STORAGE DAM AND ALTOONA LOWER NO. 2 (HOMER GAP RESERVOIR)

GEOLOGY MAP

D'APPOLONIA

11

DRAWN BY	ACS	CHECKED BY		DRAWING NUMBER 79-543-A18
	12-31-79	APPROVED BY		

LEGEND

Pc — **Conemaugh Formation**
Cyclic sequences of red and gray shales and siltstones with thin limestones and coals; massive Mahoning Sandstone commonly present at base; Ames Limestone present in middle of sections; Brush Creek Limestone in lower part of section.

Pottsville Group
Light gray to white, coarse grained sandstones and conglomerates with some mineable coal; includes Sharp Mountain, Schuylkill, and Tumbling Run Formations.

Allegheny Group
Cyclic sequences of sandstone, shale, limestone and coal; numerous commercial coals; limestones thicken westward; Vanport Limestone in lower part of section; includes Freeport, Kittanning, and Clarion Formations.

Clinton Group
Predominantly Rose Hill Formation - Reddish purple to greenish gray, thin to medium bedded, fossiliferous shale with interlonguing "iron sandstones" and local gray, fossiliferous limestone, above the Rose Hill is Keyser to white quartzite sandstone (Keyser) interbedded upward with dark gray shale (Rochester).

Dm — **Marine beds**
Gray to olive brown shales, graywackes, and sandstones, contains "Chemung" beds and "Portage" beds including Burket, Brallier, Harrell, and Trimmers Rock; Tully Limestone at base

Pocono Group
Predominantly gray, hard, massive, cross-bedded conglomerate and sandstone with some shale; includes in the Appalachian Plateau Burgoon, Shenango, Cuyahoga, Cussewago, Corry, and Knapp Formations, includes part of "Oneanta" of M. L. Fuller in Potter and Tioga counties.

Oriskany Formation
White to brown, fine to coarse grained, partly calcareous, locally conglomeratic, fossiliferous sandstone (Ridgeley) at the top; dark gray, cherty limestone with some interbedded shales and sandstones below (Shriver)

Tuscarora Formation
White to gray, medium to thick bedded, fine grained, quartzitic sandstone, conglomeratic in part.

Marcellus Formation
Black, fissile, carbonaceous shale with thick, brown sandstone (Turkey Ridge) in parts of central Pennsylvania.

Onondaga Formation
Greenish blue, thin bedded shale and dark blue to black, medium bedded limestone with shale predominant in most places; includes Selinsgrove Limestone and Needmore Shale in central Pennsylvania and Buttermilk Falls Limestone and Esopus Shale in easternmost Pennsylvania; in Lehigh Gap area includes Palmerton Sandstone and Bowmanstown Chert.

Dmo

Wills Creek Formation
Greenish gray, thin bedded, fissile shale with local limestone and sandstone zones, contains red shale and siltstone in the lower part.

Bloomsburg Formation
Red, thin and thick bedded shale and siltstone with local units of sandstone and thin impure limestone, some green shale in places.

McKenzie Formation
Greenish gray, thin bedded shale interbedded with gray, thin bedded, fossiliferous limestone, shale predominant at the base; intraformational breccia in the lower part. Absent in Harrisburg quadrangle and to the east

Keyser Formation
Dark gray, highly fossiliferous, thick bedded, crystalline to nodular limestone, passes into Manlius, Rondout, and Decker Formations in the east.

Tonoloway Formation
Gray, highly laminated, thin bedded, argillaceous limestone; passes into Bossardville and Pozono Island beds in the east

Dck — **Catskill Formation**
Chiefly red to brownish shales and sandstones, includes gray and greenish sandstone tongues named Elk Mountain, Honesdale, Shohola, and Delaware River in the east.

REFERENCE:
GEOLOGIC MAP OF PENNSYLVANIA PREPARED BY COMMONWEALTH OF PENNA. DEPT. OF INTERNAL AFFAIRS, DATED 1960, SCALE 1" = 4 MILES

GEOLOGY MAP LEGEND

D'APPOLONIA