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# ELEVATED- AND ROOM-TEMPERATURE PROPERTIES OF SELECTRON 44 AND 5105XP TRANSPARENT PLASTIC SHEET MATERIALS

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Battelle Memorial Institute

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FOREWORD

This report was prepared by Battelle Memorial Institute under Air Force Contract Number AF 33(038)-10818, Research and Development Order Number 614-12, "Structural Plastics". The work was administered under the direction of the Materials Laboratory, Directorate of Research, Wright Air Development Center, with Mr. H. S. Schwartz acting as project engineer.

#### ABSTRACT

Two transparent plastic sheet materials, Selectron 44, a polyester, and 5105XP, an acrylate, were tested in tensile creep and creep rupture. crazing, short-time tensile, and deterioration at 80°, 160°, and 200°F. Additional short-time tensile tests were made at 250° and 300°F. Vel let

The creep and creep-rupture tosts indicated that the 5105XP material had considerably more strength than Selectron 44 at all three test temperatures. The short-time tensile tests gave a similar indication at  $80^{\circ}$ , 160°, and 200°F, but at 250°F Selectron  $4^{\circ}\mu$  appeared to have a slight superiority in strength. At 300°F, 5105XP had no practical load-carrying ability at all, while Selectron 44 showed a tensile strength of only 204 psi.

Selectron 44 displayed no crazing whatsoever at any temperature or strain rate. The crazing strength of 5105XP was, in general, equal to or greater than the rupture strength of Selectron 44 at all three test temperatures.

#### PUBLICATION REVIEW

linen This report has been reviewed and is approved.

FOR THE COMMANDING GENERAL:

M. E. SORTE Colonel, USAF Chief, Materials Laboratory Directorate of Research

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#### SUMMARY

Tensile creep and creep-rupture, crazing, short-time tensile, and deterioration tests were made on two transparent plastic sheet materials (5105XP, an acrylate, and Selectron 44, a polyester) at room temperature, 160, and 200 F. Short-time tensile tests were also made at 250 and 300 F.

As shown in the tabulation below, the 5105XP material displayed a considerably greater rupture strength than Selectron 44 at all three test temperatures. The creep strength of 5105XP was likewise superior. The 10-, 100-, and 1000-hour rupture and crazing strengths of the two materials are shown in the following tabulation:

		Stress, ps	si, to Produce	e Rupture
	Temperature,		or Crazing in	
Material	F	10 Hours	100 Hours	1000 Hours
	Rupti	ure Strength		
Selectron 44	80	5830	5100	4400
5105 <b>XP</b>	80	7550	6930	6300
Selectron 44	160	1920	1580	1340
5105XP	160	4000	3500	3140 est.
Selectron 44	200	800	670	540 est.
5105 <b>XP</b>	200	2340	1960	1580
	Craz	ing Strength		
5105 <b>XP</b>	80	5400	4650	4150
5105 <b>XP</b>	160	2900 est.	2400	1850
5105 <b>XP</b>	200	1300 est.	1170	1040

No crazing was observed to take place in Selectron 44 under any of the test conditions; therefore, no crazing data can be shown for this material. The stresses necessary to produce crazing in 5105XP at 80 F are only slightly less than those required for rupture in Selectron 44. At 160 and 200 F, the crazing strength of 5105XP is greater than the rupture strength of Selectron 44 by a considerable margin.

The tensile strength of 5105XP is superior to that of Selectron 44 at 80, 160, and 200 F, but inferior at 250 F. Material 5105XP has no practical load-carrying ability at 300 F, while that of Selectron 44 is only 204 psi.

The deterioration tests indicated that Selectron 44 was the more stable of the two materials at 160 and 200 F; however, the maximum loss in weight was only slightly in excess of one per cent in the 5105XP material.

Selectron 44 appeared to be quite notch-sensitive at room temperature.

Compared with some other transparent plastics, such as Lucite HC-201 and HC-202 and Plexiglas Ia and II, the 5105XP material displayed, in general, superior crazing and creep-rupture properties. The tensile strength was comparable at 80 and 160 F, but inferior to Lucite HC-202 and Plexiglas II at 200 F.

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ELEVATED- AND ROOM-TEMPERATURE PROPERTIES OF SELECTRON 44 AND 5105XP TRANSPARENT PLASTIC SHEET MATERIALS

#### INTRODUCTION

This report covers work done under Contract Number AF 33(038)-10818 and is concerned with two transparent plastic materials, 5105XP, an acrylate, and Selectron 44, a polyester. Tensile-creep and creeprupture, short-time tensile, and deterioration tests were made on these two materials at room temperature, 160, and 200 F. Short-time tensile tests were also conducted at 250 and 300 F, and some crazing tests were made on the 5105XP material at 80, 160, and 200 F.

The creep, creep-rupture, and crazing tests vere made in standard Battelle creep frames and furnaces. Deformations were read optically by means of a microscope and platinum-strip type of extensometer. Because of the notch-sensitivity of Selectron 44 at room temperature, the normal manner of attaching the extensometers could not be used. It was necessary to devise other means that would not affect the creep and creeprupture properties. The short-time tensile tests were conducted in a Baldwin-Southwark Universal Testing Machine with deformations recorded, whenever possible, on a Templin Stress-Strain Recorder.

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Testing procedures for the short-time tensile, tensile-creep, and creep-rupture tests are described in the Appendix of a previous report(1).

## SPECIFICATIONS, PREPARATION, AND HEAT TREATMENT OF TEST SPECIMENS

The two transparent materials, Selectron 44 and 5105XP, manufactured by the Pittsburgh Plate Glass Company and Rohm and Haas, respectively, were furnished by the Materials Laboratory, Wright Air Development Center. Three panels of 5105XP,  $36 \times 36 \times 1/4$  inches, and two panels of Selectron 44,  $31-3/4 \times 36 \times 1/4$  inches, were supplied for the evaluation program. No distinction was made as to the panel from which each of the various specimens was obtained. Thus, an average value of properties of the two or three panels was probably obtained.

Extreme care was taken in handling the materials during the machining operations. The protective paper covering was removed because it tended to cause the specimens to slip while being machined. A diagram of the tensile-creep, creep-rupture, and short-time tensile specimens is shown in a previous report(1). No lubricant was used during the machining operation, and care was taken that the specimens did not overheat.

The machined specimens were annealed to relieve internal stresses prior to testing. Selectron 44 was annealed at 125 C (257 F) and the 5105XP material at 155 C (311 F). Both materials were held at the annealing temperatures for 30 minutes and then allowed to cool to room temperature in about 1-1/2 to 2 hours. The specimens were suspended from one end while in the annealing furnace.

### TENSILE-CREEP, CREEP-RUPTURE, AND CRAZING TESTS

A series of tensile-creep and creep-rupture tests was made on both Selectron 44 and 5105XP materials at 80, 160, and 200 F. The creeprupture tests covered rupture times from about one to 1000 hours. Lower stress-creep tests were made to obtain creep-rate data and also low deformation points for the design curves.

Some crazing data were also obtained from the creep and creeprupture tests, but at 160 and 200 F additional crazing tests were required. It was not possible to observe when crazing had started at these higher temperatures, since the specimens were enclosed in a furnace. The

additional crazing tests were made only on the 5105XP material, however, because no crazing was observed to take place on the Selectron 44 material at any test temperature.

The crazing tests were made at various stresses for a period of 75 hours. At the end of 75 hours, the specimens were removed from the furnace and observed for crazing. Based on the crazing characteristics of these 75-hour tests and on the creep and creep-rupture tests, generally of about 1000-hour duration, stresses were estimated at which crazing would start in 75 and 1000 hours. A line passing through these two points on a stress versus log of time plot produced the estimated crazing design curves (Figures 5 and 6).

All of the creep, creep-rupture, and crazing data obtained on Selectron 44 and 5105XP materials at 80, 160, and 200 F are shown in Tables 1 and 2. These data are reproduced as design curves in Figures 1 through 6 and as stress versus creep rate curves in Figure 7. In order to show a comparison of their strength characteristics at 80, 160, and 200 F, rupture and crazing curves for Selectron 44 and 5105XP are shown in Figures 8, 9, and 10.

These curves show that the 5105XP material has about 1000 to 2000 psi greater rupture strength than Selectron 44 at all three test temperatures. The creep strength of 5105XP is also greater than that of Selectron 44 by approximately the same amount.

No crazing was observed to take place in the Selectron 44 material at any stress or temperature. Crazing in the 5105XP material at 80 and 160 F seemed to occur at about 2 per cent deformation, increasing to perhaps 2-1/2 per cent at the lower strain rates. At 200 F, the crazing characteristics of 5105XP appear to be somewhat more sensitive to strain rate, with crazing starting at 2-3 per cent at the higher strain rates (higher stresses) and 3-4 per cent at the lower strain rates.

Since crazing strength of these transparent plastic materials is often considered a limiting factor from a design standpoint, it might be expected that Selectron 44, which shows no crazing whatsoever, would have a strength advantage over the 5105XP material. This is not necessarily so, however, since at 160 and 200 F, the crazing strength of 5105XP exceeds the rupture strength of Selectron 44 by a margin of 500 to 1000 psi. At room temperature only does the rupture strength of Selectron 44 slightly exceed the crazing strength of 5105XP.

It was observed during the testing of these two transparent plastic materials that Selectron 44 is quite notch sensitive at room temperature. Testing of this material was made more difficult because the extensometer strips could not be attached to the specimen in the normal manner. This

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													σ,	tart of	
	Temper-		Rupture	Minimum	initial								Third	Stage Creep	
Specimen	atura,	Stress,	Time,	Creep Rate,	Deformation,		Hou	rs to Pr	od uce ]	otal Def	ormation of:		Time,	Deformation,	
Number	ы. !	sd	hours	%/hour	₽°	0.5%	1.0%	2.0%	3.0%	5.0%	7,0%	10.0%	hours	8	Remarks
344-01	30	8000	On loading	(E)	1	I	I	I	I	I	1	1	ţ	1	(No crazing was observed to take
S44-C2	30	8000	On loading	(a)	ł	I	I	I	I	I	1	ł	I	I	place on any of the specimens
S44-C3	80	7000	0.5	(a)	I	ł	I	I	1	Ι	ł	I	I	I	tested in creep, or creep-rupture
S44-C4	80	6500	2.0	(a)	1	ł	1	1	1	I	ł	I	ł	I	at room temperature, 160, or
S44-C5	80	6000	3.4	(a)	I	1	1	t	1	1	I	I	ł	I	200F)
544-C30	30	5500	25.8	(C)	1.48	۱	1	1.0	11.4	ł	I	I	I	I	Failed outside gaged section
S44-C6	30	5000	(g)6.9(D)	(a)	I	I	ł	t	I	I	I	1	ł	ł	I
S44-C7	30	5000	4.7	(c)	1.4	I	I	1.5	I	Ι	I	ł	1	ì	I
S44-CR	8	5000	22 1	(c)	1.2	ł	I	3.0	I	I	I	I	I	I	I
S44-C25	80	5000	59.5	0.014	1.1	F	ł	10.0	I	1	I	1	I	I	I
S44-C29	80	5000	129.2	0.010	1.38	I	I	1.5	19.0	1	I	I	ł	I	Failed in grupped section
S44-C28	8Ú	4750	146.3	0.0075	1.20	I	I	6.5	65.0	I	ł	1	ł	I	Failed outside gaged section
S44-C32	80	4750	169.6	0.0070	1.25	I	ł	6.0	57.0	١	1	1	I	I	1
S44-C34	8	4500	752.5	0.0024	1.20	I	I	11.0	64.0	688.0	1	I	ł	I	I
S44-C26	80	4000	1001 9(D)	0.00066	0.82	i	4.0	160.0	I	ł	ł	ł	I	1	1
S44-C13	160	3000	On loading	(c)	I	I	ł	ł	I	I	ł	I	ł	ı	I
S44-€16	16n	2500	2 minutes	(c)	ł	ł	I	I	ł	ł	ł	I	I	I	I
S44-C17	160	2500	1.1	(a)	ł	I	1	I	I	I	I	I	I	I	ł
S44-C18	160	2000	6.9	(c)	3.55	I	I	I	ł	0.03	0.6	ł	I	I	I
S44-C19	160	2000	3.7	(c)	2.70	I	I	I	0.2	3,0	ł	1	1	I	ł
S44-C24	160	1750	5.9	(c)	2.41	I	ł	I	0.3	1	1	ł	ł	I	1
S44-C27	160	1750	29.8	0.057	1.10	I	١	0.4	2.0	14.0	28.0 est	I	ł	I	1
344-C20	160	1500	169.9	0.014	0.10	I	0.3	2.0	6.0	16.0	53.0	I	I	I	ı
S44-C21	160	1250	1083.0 <sup>(D)</sup>	0.00072	0.73	ł	1.5	3.0	170.0	I	ł	ł	ł	I	I
S44-C11	200	1000	<b>J.</b> 3	(c)	2.30	ł	I	I	0.1	I	1	ł	ł	ł	I
S44-C23	200	800	30.6	0.038	3.7	I	I	1	I	0.3	1.4	14.0	I	I	I
S44-C22	200	650	91.6	0800.0	1.0	ł	I	0.5	1.0	3.0	45.0	ł	I	ł	
S44-C14	200	500	686.2	0.00053	ల ల	1	0.1	2.5	5.0	407.0	I	I	ł	I	I

TABLE 1, CREEP AND CREEP-RUPTURE DATA FOR SELECTRON 44 AT ROOM TEMPERATURE, 160, AND 200 F

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(a) No extensioneter was used.
(b) Discontinued.
(c) Failed in too shart a time to establish a creep rate.

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AND 200 F
160,
TEMPERATURE,
r room
.≺ A
5105 X
FOR
DATA
AND CRAZING
CREEP-RUP TURE,
CREEP,
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TABLE

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			Remarks	Started to craze at 0.2 hour	Started to craze at 0.1 hour	Started to craze at 1.0 hour	Started to craze at 2.0 hours	Started to craze at 2.0 hours	Started to craze at 20.0 hours	No crazing observed	No crazing observed	Heavily crazed	Heavily crazed	Heavily crazed	Heavily crazed	Medium crazed	Lightly crazed	Medium crazed	Lightly crazed	No crazing observed	Lightly crazed	No crazing observed	Heavily crazed	Heavily crazed	Heavily crazed	Heavily crazed	Medium crazed	Heavily crazed	Lightly crazed	Lightly crazed	Very lightly crazed	No crazing	No crazing	ep rate.
srt of	age Creep	eformation,	8	ł	ł	1	ł	ı	1	t	I	3.8	6.8	11.0	1	I	ı	i	I	1	ł	ł	I	I	3.35	1	ł	I	t	I	I	ł	-	tablish a cre
Ste	Third St	Time, C	hours	I	I	I	I	1	ı	I	I	0.2	3.5	94.0	ł	I	ì	ł	ł	1	I	i	I	I	19.0	I	1	ł	1	I	I	1	1	me to es
			10.0%	I	ł	ł	I	I	I	1	1	I	<b>4.</b> 6 est.	78.0	1	I	ł	I	I	t	ł	I	I	1	I	I	I	I	I	I	ł	I	1	short a ti
		ion of:	۲.0%	I	1	ł	1	1	I	I	I	I	3.6	33.0	ł	ł	1	I	I	1	1	ł	I	ł	1	1	ł	I	ł	t	ł	I	I	d in too
		al Deformat	5.0%	ł	I	1	I	800.0	ł	I	I	0.3	1.9	17.5	058 est.	1	I	ı	1	I	ł	I	I	ł	26.8 est.	1	760.0	ł	I	ł	ł	I	9	(c) Faile
	-	uce Tote	3.0%	I	0.4	I	1	15.0	1	I	ł	0.1	0.6	6.0	38.0 1	i	628.0	ł	1	ł	I	ł	I	0.9	14.4	1	140.0	1	}	118.0	1	١	425.0	
		to Prod	2.0%	I	0	1	ł	4.0	25.0	230.0	1	1	0.1	1.0	5.0	I	12.0	I	I	1	1	ł	I	0.5	2.6	ł	20.0	I	I	17.0	I	I	75.0	
		Hours	1.0%	I	ł	I	I	I	I	I	ł	ł	۱	I	I	i	I	I	1	I	18.0	475.0	I	I	I	I	5 5.0	ł	I	I	ł	ł	5.0	
			0.5%	I	I	I	1	ſ	I	ł	I	I	I	ł	I	I	ł	I	1	1	I	2.5	I	1	I	I	I	I	1	I	1	I	1	ontinued
	Initial	Deformation,	%	1	2.0	I	I	1.4	1.2	1.2	ł	1.44	1.55	1.40	1.05	1	1.30	I	ł	I	0.65	0.31	1	1.0	1.0	I	0.65	I	1	1.25	1	ı	0.50	(b) Disco
	Minimum	Creep Rate,	%/hour	(a)	0.195	(a)	(a)	0.0013	0.00035	0.0002	(c)	) (j	1_10	0.069	0.00105	(a)	0.00051	(a)	(a)	(a)	0.00016	000000	(c)	<u>)</u>	0.08	(a)	0.00138	(a)	(a)	0.00057	(a)	(a)	0.00128	
	Rupture	Time.	hours	2.0	16.9	81.7	24 2(b)	$1015.0^{(b)}$	$1007, 5^{(b)}$	1005.1 <sup>(b)</sup>	On loading	011 10000	1 00	150.0	1012.6 <sup>(b)</sup>	92 D(b)	985.3 <sup>(b)</sup>	75.0 <sup>(b)</sup>	75.0 <sup>(b)</sup>	75.0 <sup>(b)</sup>	1031 2 <sup>(b)</sup>	1177.0 <sup>(b)</sup>	0.7	2.0	9.67	75.0 <sup>(b)</sup>	1034.5 <sup>(b)</sup>	$73.0^{(b)}$	75.0 <sup>(b)</sup>	1059_9 <sup>(b)</sup>	75.0 <sup>(b)</sup>	75 (l)	959.3 <sup>(b)</sup>	sed.
		Stress,	psi	NUN	7500	UUUZ	enno,		5000	4000	5000	4500	ADOD	3500	3000	2000	2500	2500	2500	2400	2000	1200	3000	2500	200	1750	1500	1500	1300	1250	1200	1100	1000	er was u
	Temper-	ature.	Ľ	N N	80	80	8	808	6	88	100	160	160	150	160	150	160	160	160	160	150	160	200			002	200			38		ŝ	8	tensomet
the state of the s		Specimen	Number	YP_L	XP-C16	XP-C?	XP-C3	XP-C4	XP-C11	XP-C18	YD. CE	XP-C17	XP.C7	XP-C14	XP-C10		XP-C12	XP-C30	XP-C34	XP-C35	YP-C77	XP-C20	XP-C6	XP-C8	XP-C15	XP-C23	SD-dX	XP-C26	XP-C27	XP-C21	XP-C33	XP-C36	XP-C13	(a) No exi

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FIGURE 3. DESIGN CURVES FOR SELECTRON 44 AT 200 F





FIGURE 4. DESIGN CURVES FOR 5105 XP AT 80 F

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FIGURE 6. DESIGN CURVES FOR 5105 XP AT 200 F

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STRESS VERSUS CREEP-RATE CURVES FOR SELECTRON 44 AND 5105 XP MATERIALS AT 80, 160, AND 200 F で FIGURE

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RUPTURE AND CRAZING CURVES FOR SEVERAL TRANSPARENT PLASTIC MATERIALS AT 200 F FIGURE 10.

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notch sensitivity of Selectron 44 may necessitate its handling, during fabrication and installation, with extreme care.

Also shown in Figures 8, 9, and 10 are the rupture and crazing curves representing data obtained previously on some other transparent plastic materials<sup>(1)</sup>, Lucite HC-201 and HC-202 and Plexiglas Ia and II. These additional data are presented here for purposes of showing a comparison of the strength characteristics of the various transparent materials at room temperature, 160, and 200 F.

An inspection of Figure 8 will show the rupture curves of 5105XP, Lucite HC-202, and Plexiglas II grouped together near the top of the plot. This indicates that the strengths of these three materials at room temperature are about the same and are also the highest of all the materials shown. The rupture strengths of the other three materials, Plexiglas Ia, Lucite HC-201 and Selectron 44, are also about the same, but approximately 2000 psi lower in strength than the first group.

The 5105XP material displays a superior crazing strength by a considerable margin when compared with the other materials at room temperature. Furthermore, the stresses required to produce start of crazing in the 5105XP material are very nearly the same as the stresses required to cause failure in Lucite HC-201, Plexiglas Ia, and in Selectron 44.

At 160 F, the 5105XP material has the highest strength of all six materials shown in Figure 9, with Plexiglas II and Lucite HC-202 being about 500 psi lower in rupture strength. The 5105XP material also displays a superior crazing strength when compared with Lucite HC-202 and Plexiglas Ia. No crazing data are available for the other materials.

At 200 F, the 5105XP material again displays the highest strength of all the materials tested (Figure 10), with Lucite HC-202 and Plexiglas II appearing somewhat weaker. Crazing data are shown only for Lucite HC-202 and 5105XP. Lucite HC-202 appears to have the higher crazing strength at the higher strain rates, while the 5105XP material appears to require higher stresses for start of crazing at the lower strain rates.

#### SHORT-TIME TENSILE PROPERTIES

Short-time tensile tests were made on both 5105XP and Selectron 44 at 80, 160, 200, 250, and 300 F. Results of these tests are shown in Table 3 and Figure 11. The testing procedure as discussed in the Appendix of a previous report<sup>(1)</sup> was generally followed. The only departure from

Manual         Tanalia         Tanalia         Tanalia         Tanalia         Tanalia         Tanalia         Surroph, pai         Elastic         Propertional           Manual         Number         F         q In         Number         F         q In $0.13$ $0.13$ $0.13$ $0.13$ $0.13$ $0.13$ $0.13$ $0.13$ $0.13$ $0.028$ $0.13$ $0.028$ $0.13$ $0.028$ $0.028$ $0.028$ $0.028$ $0.028$ $0.0128$						Åverage	Ύk	bid			
Specimen         Tamperators         Area         Strength, statil         Strength, statil         Strength, statil         Strength, statil         Strength, statil $0.15x$ statil $0.15x$ statil $0.15x$ statil $0.15x$ statil         Strength, statil $0.15x$ statil         Strength, statil $0.15x$ statil         Strength, statil $0.15x$ statil         Strength, statil $0.15x$ statil $0.12253$ statil $9.30$ statil $9.10$ statil $0.1253$ statil $0.12253$ statil $0.12254$ statil $0.12540$ statil $0.12540$ statil $0.12540$ statil $0.12540$ statil $0.12540$ statil $0.12540$ statil $0.12540$ statil					Tensile	Tensile	Strengt	th, psi	Elastic	Proportional	
		Specimen	Temperature,	Area,	Strength,	Strength,	0.1%	0.2%	Modulus,	L.imit,	
Selection 44         S4+Ti3         80         0.12452         9,910         -         (a)         -         -         -         -         -         -         -         -         -         -         0.12452         9,500         9,705         (a)         -<	Material	Number	Ľ	sq in.	psi	ps:	Offset	Offset	psi	psi	Remarks
34+71         80         0.1223         9,500         9,705         (a) $   -$ <t< td=""><td>Selectron 44</td><td>S44-T13</td><td>80</td><td>0.12452</td><td>9.910</td><td>I</td><td>(a)</td><td>ı</td><td>ł</td><td>ł</td><td>No crazing</td></t<>	Selectron 44	S44-T13	80	0.12452	9.910	I	(a)	ı	ł	ł	No crazing
$ \begin{array}{llllllllllllllllllllllllllllllllllll$		S44-T14	80	0.12223	9,500	9,705	(a)	I	ł	ļ	Ditto
34476       16       0.12350       3,230       2,942       (a)       - <td></td> <td>S44-T5</td> <td>160</td> <td>0.12425</td> <td>2.655</td> <td>I</td> <td>(a)</td> <td>I</td> <td>I</td> <td>1</td> <td>•</td>		S44-T5	160	0.12425	2.655	I	(a)	I	I	1	•
544-17       200       0.12225       1,638       -       (a)       -		S44-T6	160	0.12350	3,230	2,942	(a))	ł	ł	I	٠
544-T8       200       0.12450       1,805       1,712       (a)       - </td <td></td> <td>244-17</td> <td>200</td> <td>0.12225</td> <td>1,638</td> <td>I</td> <td>(a)</td> <td>I</td> <td>I</td> <td>I</td> <td>•</td>		244-17	200	0.12225	1,638	I	(a)	I	I	I	•
54473       250       0.12221       368       -       (a)       -		S44-T8	200	0.12450	1,805	1,712	(a)	I	I	I	•
S44-T10       250       0.12365       607       482       (a)       -       10810       1,880       - <t< td=""><td></td><td>S44-T9</td><td>250</td><td>0,12221</td><td>368</td><td>I</td><td>(a)</td><td>I</td><td>I</td><td>ł</td><td>•</td></t<>		S44-T9	250	0,12221	368	I	(a)	I	I	ł	•
S44-T12       300       0.12350       204       204       (a)       - <td></td> <td>S44-T10</td> <td>250</td> <td>0.12365</td> <td>607</td> <td>482</td> <td>(a)</td> <td>ł</td> <td>1</td> <td>I</td> <td>•</td>		S44-T10	250	0.12365	607	482	(a)	ł	1	I	•
5105XP       XP-T1       80       0.12594       9,890       -       3,770       4,850       516,000       1,350       Lightly         XP-T1       80       0.12026       9,880       -       (a)       -       <		S44-T12	300	0.12350	204	204	(a)	ł	ŧ	ı	•
XP-T3       80       0.12026       9,880       -       (a)       -       -       -       Lightly         XP-T10       80       0.12624       10,840       -       3,280       4,083       318,000       1,900       Lightly         XP-T11       80       0.12524       10,840       -       3,280       4,083       318,000       1,900       Lightly         XP-T3       160       0.12550       5,550       -       (a)       -       -       -       -       Lightly         XP-T5       160       0.12550       5,550       -       (a)       -       -       -       Lightly         XP-T6       160       0.12550       5,860       5,705       2,750       3,580       319,000       630       Heavily         XP-T8       200       0.12445       2,090       2,090       (a)       -       -       -       Lightly         XP-T6       250       0.12315       206 <sup>(b)</sup> 2,090       (a)       -       -       Lightly         XP-T6       300       0.12315       206 <sup>(b)</sup> 2,090       (a)       -       -       -       Lightly         XP-T6       300	5105XP	XP-T1	8	0.12594	068'6	1	3,770	4,850	516,000	1,350	Lightly crazed
XP-T1080 $0.12624$ $10,840$ $ 3,280$ $4,083$ $318,000$ $1,900$ LightlyXP-T1180 $0.12474$ $11,030$ $10,410$ $(a)$ $   -$ <		XP-T3	80	0.12026	9,880	ł	(a)	I	I	I	Lightly crazed
XP-T1180 $0.12474$ $11,030$ $10,410$ $(a)$ $  -$ LightlyXP-T9160 $0.12350$ $5,550$ $ (a)$ $  -$ HeavilyXP-T5160 $0.12350$ $5,860$ $5,705$ $2,750$ $3,580$ $319,000$ $630$ HeavilyXP-T8200 $0.12445$ $2,090$ $2,090$ $(a)$ $  -$ MediumXP-T7250 $0.12315$ $206^{(b)}$ $206$ $(a)$ $   -$ LightlyXP-T6300 $0.12500$ $(c)$ $ (a)$ $   -$ Lightly		XP-T10	80	0.12624	10,840	I	3,280	4,083	318,000	1,900	Lightly crazed
XP-T9       160       0.12550       5,550       -       (a)       -       -       -       Heavily         XP-T5       160       0.12550       5,860       5,705       2,750       3,580       319,000       680       Heavily         XP-T8       200       0.12445       2,090       2,090       (a)       -       -       Medium         XP-T8       200       0.12315       2,090       2,090       (a)       -       -       Medium         XP-T7       250       0.12315       206 <sup>(b)</sup> 206       (a)       -       -       Lightly         XP-T6       300       0.12315       206 <sup>(b)</sup> 206       (a)       -       -       Lightly		XP-T11	80	0.12474	11,030	10,410	(a)	I	ł	ŧ	Lightly crazed
XP-T5       160       0.12550       5,860       5,705       2,750       3,580       319,000       630       Heavily         XP-T8       200       0.12445       2,090       2,090       (a)       -       -       -       Medium         XP-T7       250       0.12315       206 <sup>(b)</sup> 206       (a)       -       -       Lightly         XP-T6       300       0.12500       (c)       -       (a)       -       -       Lightly		6T-73	160	0.12350	5,550	ł	(a)	ì	I	1	Heavily crazed
XP-T8     200     0.12445     2,090     2,090     (a)     -     -     -     Medium       XP-T7     250     0.12315     206 <sup>(b)</sup> 206     (a)     -     -     Lightly       XP-T6     300     0.12500     (c)     -     (a)     -     -     -     Lightly		XP-T5	160	0.12550	5,860	5,705	2,750	3,580	319,000	680	Heavily crazed
XP-T7         250         0.12315         206 <sup>(b)</sup> 206         (a)         -         -         Lightly           XP-T6         300         0.12500         (c)         -         (a)         -         -         Lightly		XP-T8	200	0.12445	2,090	2,090	(a)	I	ı	I	Medium crazed
XP-T6 300 0.12500 (c) - (a)		XP-T7	250	0.12315	206 <sup>(b)</sup>	206	(a)	I	1	ł	Lightly crazed
		XP-T6	300	0.12500	(c)	1	(a)	I	ł	1	,

TABLE 3. SHORT-TIME TENSILE DATA FOR SELECTRON 44 AND 5105 XP AT ROOM TEMPERATURE, 160, AND 200 F

.

(a) No extensionater was used.(b) Tensile machine reached limit of travel.

(c) Too low to obtain value.



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the described procedure was in the method of strain measurement. Rather than using the microformer extensometer, a Templin Autographic Stress-Strain Recorder was employed whenever measurements were made.

Because of the notch-sensitivity of Selectron 44 at room temperature, no extensometer was attached to the specimens of this material during testing; therefore, yield strength, modulus of elasticity, and proportional limit values were not obtainable. At elevated temperatures, both Selectron 44 and 5105XP materials soften too excessively to allow attachment of an extensometer to the specimens.

The tensile strength of the 5105XP material ranged from about 10,400 psi at room temperature to 206 psi at 250 F. No reliable figure could be obtained at 300 F because of the extremely low strength at this temperature. The tensile strength of Selectron 44 is somewhat lower than that of 5105XP at 80, 160, and 200 F, but slightly higher at 250 F. The tensile strength of this material ranged from 9700 psi at room temperature to 204 psi at 300 F. The tensile strength of 5105XP compares favorably with the transparent acrylate, Lucite HC-202, at 80 and 160 F, but at 200 F it appears to be somewhat weaker.

The room-temperature yield strength (0.2 per cent offset) of 5105XP averages about 4460 psi, which is somewhat low when compared with Lucite HC-202 and Plexiglas II which showed values of 5845 and 5460 psi, respectively. The room-temperature elastic modulus of 4.17 x  $10^5$  psi, and the proportional limit of 1625 psi for 5105XP material are comparable to those of Plexiglas II.

### DETERIORATION PROPERTIES

A series of deterioration tests was made on the two transparent plastic materials, 5105XP and Selectron 44, at 160 and 200 F. The purpose of these tests was to determine the stability of these two materials by exposing them for 24, 200, and 1000 hours at 160 and 200 F. After each period of time, the samples, one inch square by 1/4 inch thick, were weighed and the differences in weight noted. These tests were made in duplicate. The results in per cent weight loss for each exposure are shown in Table 4. All percentages are based on the original weight of the sample.

Of the two materials, 5105XP consistently displays the greater weight loss, although the difference between the two materials is small. The maximum reduction in weight is only slightly in excess of one per cent which is probably negligible from a design standpoint. It is pointed out that

the 5105XP material shows the same loss in weight after the 1000-hour exposure as it does after 200 hours when heated at 200 F.

		Per	Cent Weight L	oss,
Specimen	Temperature,	A	fter Exposure	of
Number*	F	24 Hours	200 Hours	1000 Hours
SEL-A	160	0.29	0.58	0.64
SEL-B	160	0.26	0.59	0.63
XP-A	160	0.33	0.74	0.89
XP-B	160	0.32	0.80	0.92
SEL-C	200	0.54	0.89	1.02
SEL-D	200	0.57	0.80	0.98
XP-C	200	0.67	1.07	1.07
XP-D	200	0.61	1.29	1.29

TABLE 4.	DETERIORATION DATA ON SELECTRON 44
	AND 5105XP AT 160 AND 200 F

\*SEL designates Selectron 44

XP designates 5105XP

When compared with four other transparent plastic materials, Plexiglas Ia and II and Lucite HC-201 and HC-202, Selectron 44 and 5105XP display the greatest loss in weight after each exposure. In some cases, the loss is more than twice as great for comparable conditions of exposure.

### REFERENCE

 WADC Technical Report 52-38 of February, 1952, entitled
 "Elevated- and Room-Temperature Properties of Transparent Acrylic Sheet Materials".