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MODIFY: A MODULAR MULTI-DEGREE-OF-FREEDOM TRAJECTORY PROGRAM. (U)

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MODIFLY: A MODULAR MULTI-DEGREE-OF-FREEDOM TRAJECTORY PROGRAM.

9 Final rept.

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BY JOHN E. HOLMES

STRATEGIC SYSTEMS DEPARTMENT

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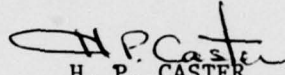
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SUMMARY

MODIFLY is a modular trajectory simulation computer program which was written so as to be effective, efficient, and easily modified. The program was designed primarily for the simulation of typical autonomous guided missiles in which roughly equal consideration is given to the simulation of the seeker, guidance, autopilot, controls, and aerodynamics. It was written in FORTRAN IV language for use on a CDC 6500 computer and uses overlay files and a library edit routine.


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INTRODUCTION

This program was written in order to accomplish two specific tasks. The first was to decrease costs and the second was to increase efficiencies in the simulation of the flight of any vehicle that moves above the earth's surface. These goals were attained by preparing a program which allowed for the condensing of several older NSWC trajectory programs into as small a package as possible in order to eliminate the excessive duplication of trajectory programs and, more importantly, to eliminate the excessive time consumed by the users in the maintenance of familiarity with each of the different programs.

This modular program consists of two main sections. The first, containing the executive routines, provides all of the control logic for the program from the specification of input data clear through to the final calculated results. Standardized, general formats are provided for the inclusion of all data. All necessary standard mathematical operations are coded and included, including means for the numerical integration of up to 28 differential equations, as well as standard generalized formats for the printing of the trajectory results.

The second section is written so that each user can select or program individual modules that meet his particular vehicle requirements. The program has been written in such a manner that it can be used to simulate any type of flight in the atmosphere -- including the simulation of guided vehicles from simple 3 DOF particle trajectories to maneuvering 6 DOF simulations of air-to-air missiles with proportional navigation or maneuvering re-entry bodies flying along evasive trajectories. Several basic modules as well as some specific modules have been written and are included in this report for the aid of the user. This program is efficient and easily modified by the user so that he can use it from the original conception of a system and its preliminary design through to its final flight evaluation.

EXECUTIVE ROUTINES

The primary functions of the executive routines are to control the program flow, establish standardized formats for the insertion of data and modules into the program, and provide for the economic storage of parameters and their use. The flow logic of the program is shown in Figure 1. In order to minimize storage, the program was coded using overlays. The individual subroutines included in each overlay level are shown in Figure 2 and described in the following section.

DESCRIPTION OF ROUTINES.

Program OV. This is the main, zero order overlay. Its function is to call the primary overlays; therefore, it controls the main flow of the program.

Subroutine ZERO. This routine zeros out the entire common storage array, Y(1) through Y(4940), and sets the following default values:

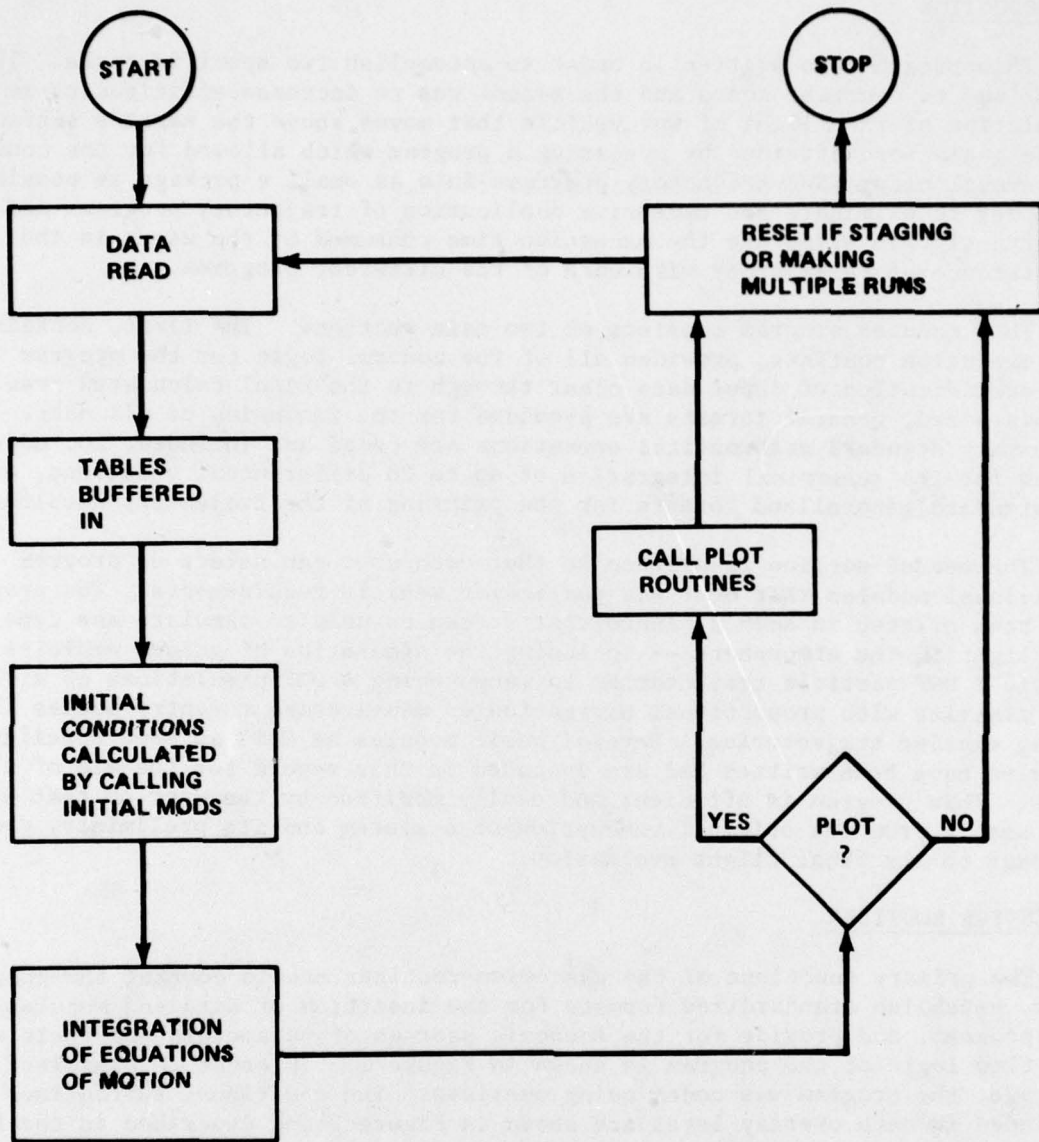


FIGURE 1 EXECUTIVE FLOW LOGIC

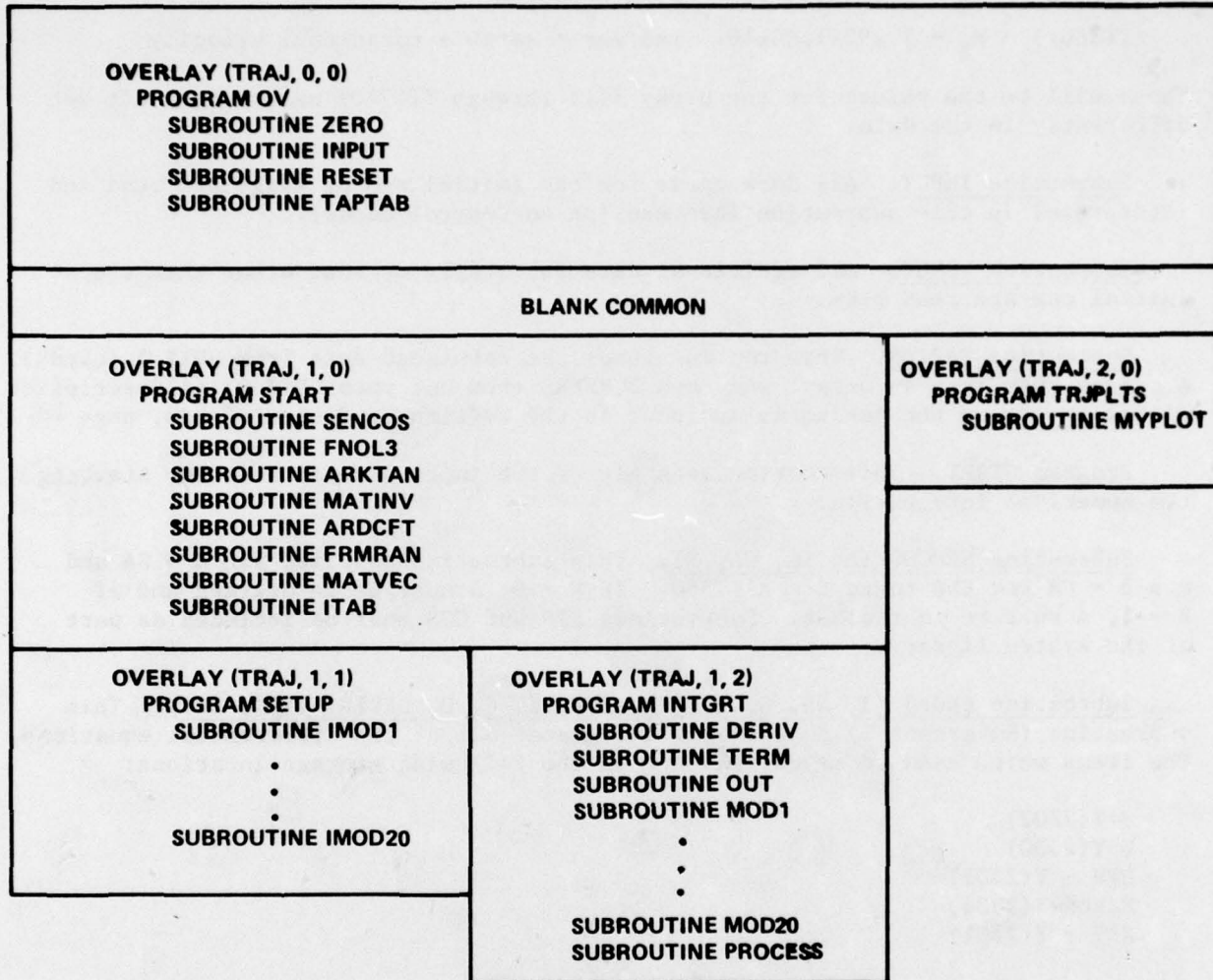


FIGURE 2 OVERLAY FILES

Y(2302) = J = 2	} Integration Controls
Y(2304) = XNE = 0	
Y(2305) = MPR = 1	
Y(2306) = ERROR = 1	
Y(3000) = $R_E = 20925631. \text{ ft} = \text{earth's radius}$	
Y(3001) = $W_E = 7.29211508 \times 10^{-5} \text{ rad/sec} = \text{earth's rotational velocity}$	

These will be the values for the array Y(1) through Y(4940) unless they are set differently in the data.

Subroutine INPUT. All data cards for the initial run or stage are read and interpreted in this subroutine (see section on Control Cards).

Subroutine RESET. All additional data for stages or runs other than the initial one are read here.

Subroutine TAPTAB. This routine reads the tabulated data from UNIT 5 (cards), arranges them into an array, and then BUFFERS them out onto UNIT 9. (A description of how to set up the tables is included in the section on Control Cards, page 13.)

Program START. This routine sets all of the initial conditions for starting the numerical integration.

Subroutine SENCOS (A, SA, CA, N). This subroutine supplies $\sin A = SA$ and $\cos A = CA$ for the range $0 \leq A \leq 360$. If $N = 0$, A must be in degrees and if $N = 1$, A must be in radians. Subroutines SIN and COS must be included as part of the system library.

Subroutine FNOL3 (J, NN, G, L, MPR, XNE, T, C, D, DERIV, TERM, OUT). This subroutine (Reference 1) numerically integrates all of the differential equations. The items which need to be defined are in the following storage locations:

J=Y(2302)
G=Y(2300)
MPR = Y(2305)
ERROR=Y(2306)
XNE = Y(2301)

These parameters are defined as:

J: (INPUT, INTEGER)

This parameter indicates the integration method.

¹Ferguson, R. E. and Orlow, T. A., "FNOL3, A Computer Program to Solve Ordinary Differential Equations," NOLTR 71-2, 1 Mar 1971

J = 1 Use Runge-Kutta method of integration to termination. Truncation errors are not calculated; the step size G is not adjustable.

J = 2 Use Runge-Kutta for the first three steps, then Adams-Moulton for the remainder of the interval of integration. Truncation errors are calculated. The step size is adjustable unless XNE = 0. If the step size is adjusted, new starting values are obtained through the Runge-Kutta method.

J = 3 Use Runge-Kutta throughout. The truncation errors are calculated; the step size is adjustable unless XNE = 0.

G: (INPUT, REAL)

This is the initial step size.

MPR: (INPUT, INTEGER)

This is the print frequency -- the number of integration cycles between printouts. If MPR = 0, then printing is determined by values assigned to Y(2998) and Y(2997), where Y(2998) is set equal to some running variable like T, C(1), D(1), etc. and Y(2997) is a constant interval in Y(2998) between printing cycles.

XNE: (INPUT, REAL)

This is the step size control. The step size is unchanged if the worst of all the errors lies within the window 10^{-XNE-3} , 10^{-XNE} . The step size is increased if the errors are all less than 10^{-XNE-3} . The step size is decreased if for some differential equation the error is greater than 10^{-XNE} . If ERROR < 0 and XNE ≠ 0., the automatic adjustment of the step size is a function of the absolute errors. If ERROR = 0. and XNE ≠ 0., the automatic adjustment of the step size is a function of the relative errors. If ERROR = ε > 0. and XNE ≠ 0., the automatic adjustment of the step size is a function of the relative errors where the relative errors are equal to the absolute errors divided by the maximum ERROR, |C(I)|. This option removes the possibility of using "small" functional values to compute relative error, otherwise this option is identical to the previous option and is to be preferred over it. If XNE = 0., the step size G is not adjustable. The other parameters are either set internally in the program or are defined in the section on Control Cards.

Subroutine ARKTAN (A, B, C, N). This subroutine calculates arctangents defined as $C = \tan^{-1}(A/B)$. If $N = 0$, C is in degrees and if $N = 1$, C is in radians. The range of C is: $-180 < C < +180$. If $A = 0$, $B < 0$, $C = -180$; and if $B > 0$, then $C = +180$. Subroutine ATAN must be in the system library.

Subroutine MATINV (A, B, C). This subroutine computes the transpose (B) and inverse (C) of the (3, 3) matrix (A). If the determinant of A is zero, neither B or C is calculated; instead, a comment is printed and control is returned to the calling program.

Subroutine ARDCFT (H, P, T, D, C, G). The earth's atmospheric properties (Reference 2) are supplied by this subroutine up to an altitude of 10^6 feet. Entering with the altitude (H, ft.) the pressure (P), temperature (T), density (D), speed of sound (C) and acceleration due to gravity (G) are given ratioed to their corresponding sea level values.

Subroutine FRMRAN (TABLE, NUM, MFNC, U, A). This is a linear interpolation routine which extracts tabulated data from TABLE, and then with the NUM independent variables U_1, U_2, \dots, U_{NUM} it linearly interpolates or extrapolates $2^{NUM} - 1$ times and supplies the MFNC values of the functions A.

Subroutine MATVEC (A, B, C, N). Products of matrices, whose orders are (3, 3) and (3, 1) are computed by this subroutine. When:

$N = 0,$	$C = AB^*$
$N = 1,$	$C = A^T B^*$
$N = 2,$	$C = AB$
$N = 3,$	$C = A^T B$
$N = 4,$	$C = AB^T$
$N = 5,$	$C = A^T B^T$

The A, B, and C arrays are stored, column-wise, starting at the left. The symbol * indicates that B, in these cases, is a (3, 1) array. In all other cases A, B, C are (3, 3) arrays.

Subroutine ITAB (NTAB, N, U, V). This routine selects the table designated by NTAB, which is the numerical location of the table in the KTAB array, and for N independent variables of U calls FRMRAN for the linear interpolation of the function V.

Program SETUP. This program calls the initial modules IMOD1 through IMOD20 as designated by the code 1 control cards.

²U.S. Standard Atmosphere, 1969 (NASA, Dec 1969, Washington, DC)

Subroutines IMOD1 through IMOD20. These dummy subroutines are included so that users can substitute their own subroutines for calculating any initial conditions that may be needed before the numerical integration is started.

Program INTGRT. This program sets up the integration controls and calls FNOL3 for the numerical integration of the equations of motion.

Subroutine DERIV. This subroutine calls the appropriate modules, MOD1 through MOD20, as designated by the code 1 control cards.

Subroutine TERM. The termination conditions (code 4 control cards) are checked and if any one of them has been met, the integration is terminated.

Subroutine OUT. The output is prepared and printed here based on the information included on the code 2 control cards.

Subroutines MOD1 through MOD20. These are dummy subroutines. The user should substitute his own subroutines for the dummy ones. These subroutines are to contain all of the definitions for all of the differential equations.

Subroutine PROCESS. Again, this is a dummy subroutine which can be replaced by the user. Any accessory calculations that are not needed for the integration of the differential equations are usually included in this subroutine. The subroutine is called in subroutine OUT everytime that the print conditions have been met.

Program TRJPLTS. This program contains the calls for plotting any of the data designated on the code 5 control cards.

Subroutine MYPLOT. This is a dummy subroutine. If the user wishes to plot any variables he must substitute his own MYPLOT subroutine containing his own GOULD or equivalent plot calls.

A FORTRAN listing of these executive routines has been included in Appendix A.

STORAGE ALLOCATION. As mentioned earlier, the program has been coded using overlay files in order to minimize the machine memory required. The amount of storage needed for execution will vary according to the size of the particular modules used as well as by the size of the arrays that are to be plotted and dimensioned in subroutine MYPLOT. Generally, on WOL's CDC 6500, the user has needed around 45000⁽⁸⁾ locations. The maximum has been on the order of 63000⁽⁸⁾ locations.

All of the parameters stored in the program have been placed into an array dimensioned Y(4940). The first 2299 locations have been allocated to trajectory parameters. These are available for coding in the modules. The locations Y(2300) through Y(4940) are utilized in the executive routines and as such, are not available to the user. As an aid to keeping track of the parameters, the Y array has been broken into several parts. It is not absolutely necessary for the user to retain this designation in his modules; but, it is a great aid to keeping all modules interchangeable. This Y array breakdown is shown in Figure 3. The fixed storage assignments are listed in Appendix B.

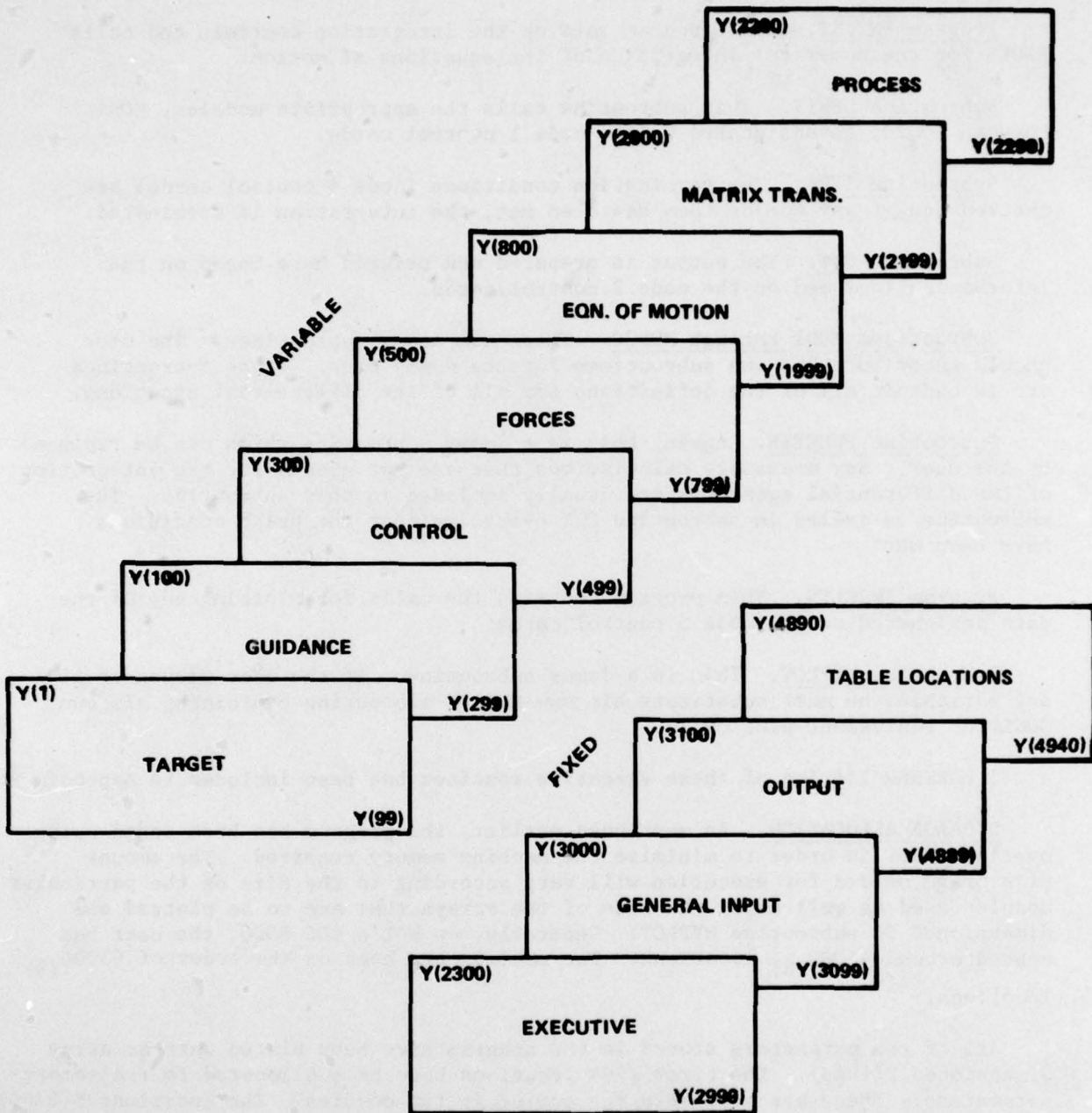


FIGURE 3 Y ARRAY STORAGE

CONTROL CARDS. All data necessary for running this program are entered into the program through the use of standardized formats. Each piece of information, except for tables, is entered on a separate control card. The particular use for each data card is determined by the code punched in the first two columns of the card. The codes, formats, and types of information are tabulated in Table 1 on page 14 and explained in more detail below.

Code 0. Each data deck must contain this card as the first card in the deck. The users title located in columns 3 through 72 will appear in the heading at the top of each page of printout.

Code 1. These are the modules to be used for this particular run or stage. These cards must be read in the order you wish the module to be called. It is not necessary that the mod numbers be in sequence.

Code 2. These are the variables to be listed in the output. The data will be listed in columns with the first column always being time. The first 15 variables will be listed on the first page and the next 15 on a separate page. The number of variables listed can be any number from 1 through 30; but, note that if you print the results of no more than 15 variables you will save paper, time, and money. The columns will be printed in the order that the code 2 control cards appear in the deck. Each code 2 control card is to contain the location of the parameter in the Y array, the heading that you wish to appear at the top of the column, and the format of the parameter. The maximum width of each column is 8 spaces but you can place the decimal depending on what is being listed. If the format is left off the card, the default is F8.0.

Code 3. These cards contain the initial values of any parameters in the program. They may be in any order but the total number for all stages must not exceed 200.

Code 4. This code identifies the termination conditions for the numerical integrations. The program will stop whenever any parameter in the Y array designated as a stop variable goes outside of the lower or upper limits as set by this code. As many as 10 termination conditions may be set for any complete trajectory run.

Code 5. Any variable in the Y array that is to be plotted (other than time) must be designated with a code 5 control card. Whenever any code 5 control card (up to a maximum of 10) appears in the deck, subroutine MYPLOT will be called and the users plot options will be performed.

Codes 6 and 7. A maximum of 28 differential equations can be designated with these codes. The code 6 designates the dependent variables and the code 7 their derivatives. The variable locations in the "C" and "D" arrays must correspond; i.e., the first variable in the "D" array must be the derivative of the first variable in the "C" array.

TABLE 1 CONTROL CARDS

CARD COLUMN	1-2	3	8	9	22	23	36	37	44	45	47	53	54	63	64	72
FORMAT		12	16		E14.6		E14.6		A10		A7		A10		A9	
VARIABLE NAME	IR	IN	IN		VAR	VARR	HED1	HED2	HED3							

IDENTIFICATION, 7A10																	
TITLE	0	MOD NUMBER	LOCATION IN Y ARRAY	NUMERICAL VALUE	UPPER BOUNDARY	LOWER BOUNDARY	LOCATION IN C ARRAY	LOCATION IN D ARRAY	KTAB ARRAY INDEX	TABLE NUMBER	LOCATION IN Y ARRAY	LOCATION IN Y ARRAY	LOCATION IN Y ARRAY	LOCATION IN Y ARRAY	LOCATION IN Y ARRAY	LOCATION IN Y ARRAY	USERS IDENT.
MODULES	1																USERS IDENT.
OUTPUT PARAMETERS	2																FORMAT F8?
DATA	3																USERS IDENT.
TERMINATION CONDITIONS	4																USERS IDENT.
PLOT PARAMETERS	5																USERS IDENT.
DEPENDENT VARIABLES	6																USERS IDENT.
DERIVATIVES	7																USERS IDENT.
TABULATED VARIABLES	8																USERS IDENT.
TABLES TO FOLLOW	9																
END OF DATA FOR RUN	10																
BEGIN NEXT STAGE	11																
IDENTIFICATION, 7A10																	
STOP, END OF DATA	99																

Code 8. These control cards are used to indicate where the tabulated functions appear in the deck of tables. When the modules are coded, an index in the KTAB array is assigned to each tabulated function. For example, maybe the axial force coefficient was coded as having index number 12 in the KTAB array. For this particular run, the axial force coefficient table that you wish to use may be the fourth table in your deck of tables; therefore, IN equals 4 and VAR equals 12.

Code 9. A card with the number 9 in column 2 must precede the deck of tables. It causes the program to read the following cards as tabulated data. The tables should be arranged as follows:

Table 1	{	9		
			Title card	(FORMAT 7A10)
			Control card	(FORMAT 14I5)
			Listing of independent variables	(FORMAT 6E12.7)
			Listing of values of dependent function	(FORMAT 6E12.7)
Table 2	{		Title card	
			Control card	
			Listing of independent variables	
			Listing of values of dependent function	
Table I (I=3, 49)	{		repeat for as many tables as needed	
			BLANK CARD	} at end of tables
			BLANK CARD	

In this program the tabulated functions are functions of 1, 2, or 3 variables, with each function located in a separate table. The tabulation of a function of three variables would be as follows:

a. Control Card

L, N, M, n_1, n_2, \dots, n_N (FORMAT 14I5) where:

L = 0 all cases

N = 3 number of independent variables

M = 1 each table contains only 1 function

n_1, n_2, n_3 numbers of values of each independent variable
for which values of the function are tabulated.

b. Listing of values of independent variables for which function is tabulated

On the first card(s) the n_1 values of the first independent variable are listed. On succeeding cards the n_2 and n_3 values of the second and third independent variables, respectively, are listed.

The following restrictions apply: Values of two different independent variables may not appear on the same card. At least two values of each independent variable must be listed; and, all values must be distinct and must be listed in ascending order. The format for these cards is 6E12.7.

c. Listing of values of dependent function

The three independent variables are designated N_1 , N_2 , and N_3 . The number of values of each of these variables is n_1 , n_2 , and n_3 , respectively. A block of data contains those values of the function for all values of N_3 listed, and for one particular value of N_1 and N_2 . The first block corresponds to the first value of N_1 and N_2 listed; the second block corresponds to the first value of N_1 and the second N_2 , etc. These blocks are repeated until a set of blocks for the first value of N_1 and all values of N_2 have been presented. Sets for the remaining values of N_1 follow until the table is completed. As a check there are n_1 sets, $n_1 \times n_2$ blocks and $n_1 \times n_2 \times n_3$ distinct values of the function. The format for this tabulation is also 6E12.7.

Code 10. This card is to be placed at the end of the data for that particular run or stage of the run. When this card is read, the program will stop reading data cards and start integrating the equations of motion. When one of the termination conditions has been met, the program will stop integrating and start reading the next coded data card. At this point in time, the program still retains the initial conditions as read in at the beginning of the run as well as all of the values as last calculated when the termination conditions were met.

If you wish to stack runs, i.e., start another run with slightly different initial conditions, follow the code 10 card with a new code 0 title card, and then follow this with the necessary changes that you wish to make in the original code 3 data. The program will retain the original initial code 3 conditions except for those that you change here. You must include new code 1, 4, and 8 cards; i.e., tell the program which modules to use, new stop conditions, and which tables to use.

Code 11. This is a title card that is an indication to the program that staging is to take place. The general procedure is that the program will read additional data at this time. These data will then replace the values retained by the program when the last portion of the flight was terminated. This allows you to restart the calculations where you finished. The only code 3 data required are those that you wish to change at that point in the trajectory. You must include new code 1, 4, and 8 cards, i.e., tell the program which modules to use, which tables to use, and new stop conditions. Remember though, the total number of data variables, code 3 cards, must not exceed 200 and the total number of tables must not exceed 49 for all stacked runs or stages.

Code 99. This stops the program.

TRAJECTORY MODULES

The primary reason for writing this program was to build a program which could be utilized and changed by a wide variety of users without them having to spend an inordinate amount of time in learning and adopting the code. It was also envisioned that the program had to be of use to those conducting preliminary design studies (when only the basic fundamentals of the vehicle are known and the vehicle characteristics are constantly changing) as well as for those analyzing the flight mechanics of production systems. In order to refrain from writing a general purpose program that would cover as much detail as possible for all users, but satisfy none, it was decided to program the problem so that different modules, written for specific systems, could be selected or written and inserted by each user.

In order to keep each module as universal in its use as possible, it was necessary to break the system model into several parts and to minimize the linkage between each part. In general, the parts of a system can be divided as is shown in Figure 4.

The logic behind these parts was as follows. The only information that would be passed from the target module to the seeker module would be the target coordinates. The interface between the seeker and autopilot modules would usually consist of a maximum of three error signals. The interface between the autopilot and the force and moment modules would be the two or three control deflections and the only thing that would have to be passed over to the equations of motion are the three forces and three moments.

Note though that this arbitrary division of the modules while appearing to be logical is not permanently locked into the code. For any simulation as many as 20 modules can be used and the quantities exchanged between modules can be chosen at the whim of the programmer. These are just suggested modules which will aid in the exchange of modules among all of the users.

The direction cosine matrix is generally defined in the section called "Matrix Transformations." When using this program for 6DOF simulations the position of the body principal axes with respect to the inertial axes is generally defined by integrating the elements of the direction cosine matrix. These elements and their derivatives are defined in this module as well as other transformation matrices such as the inertial to local axes transformation, and the local to principal axes transformation. Generally, one of two modules will take care of the matrix transformations. One of these is for 3DOF and the other for 6DOF. These have been coded and are included in this report as MOD1 and MOD4.

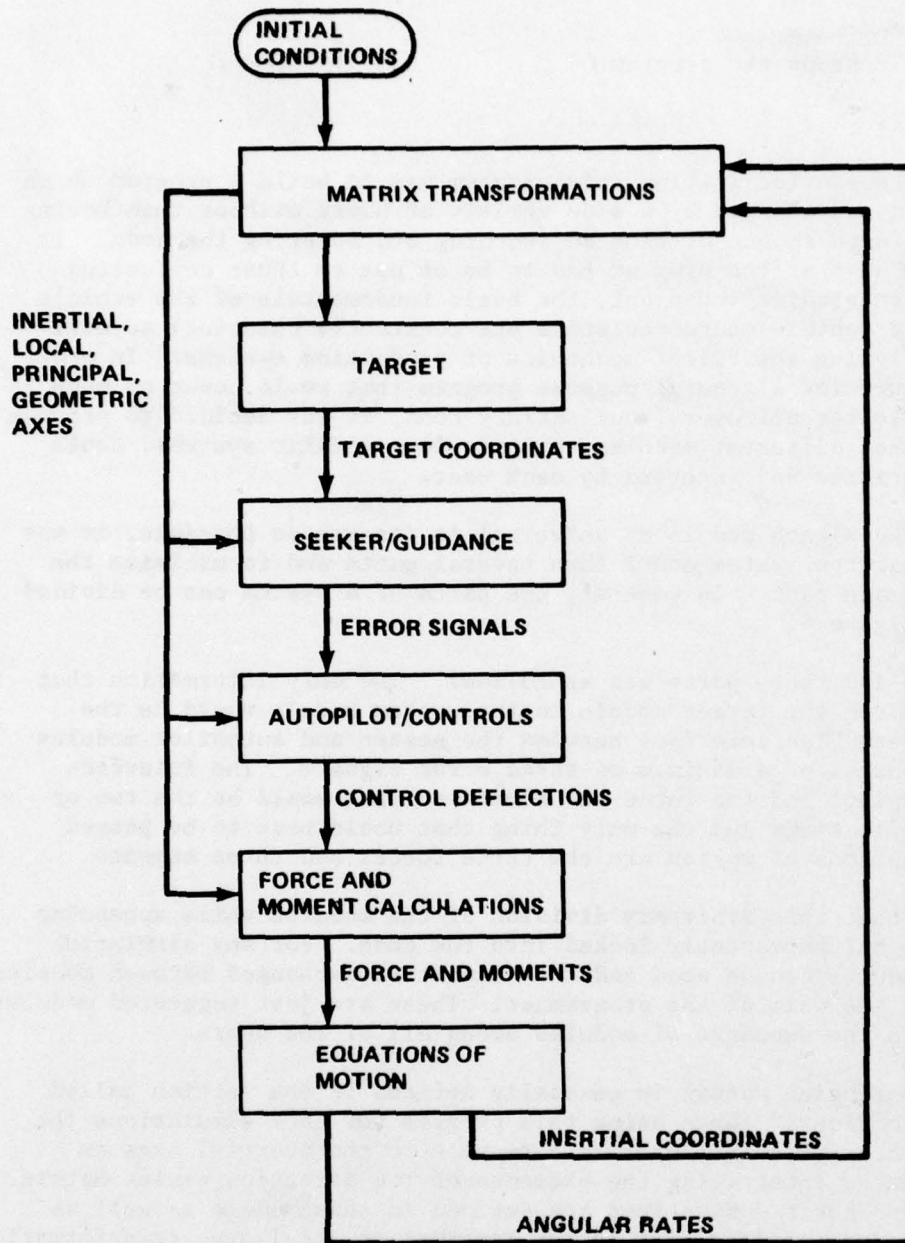


FIGURE 4 MODULE LINKAGE

The target module is also of a general nature. It allows for a target to either remain fixed with respect to the earth or to fly at constant velocity over the earth. This general module is also included in this report as MOD5. If the user desires any particular form of maneuvering target he can easily insert his own module.

The seeker and autopilot are more system oriented; therefore, they are generally coded for a particular system. Some examples are included in this report as MOD6 and MOD7.

Likewise, the forces and moments generated on the vehicle are dependent on what kind of control system, etc., the vehicle has. It could have canard controls, aft fins, swivel nozzle, etc. A sample has been included as MOD8.

The equations of motion are of a more general nature; therefore, examples for modules for both 3DOF and 6DOF are included in this report as MODs 14 and 9.

Remember, you only need to call the modules which pertain to your case. In early studies of a preliminary design, you may only need one or two very simple modules. As the system is developed you can then expand and add to your module package. You can also take advantage of another's modules that have been developed if all parties maintained the general interchangeability features as outlined in this report.

AXIS SYSTEMS AND TRANSFORMATIONS. In general, only four different axis systems are needed. These are inertial, local, principal, and geometric axis. These can be used to specify orientations of the missile with respect to the target and with respect to the earth.

Inertial. The inertial axes are defined as follows. The origin is at the center of the earth and the X_R axis goes through the north pole and the Y_R and Z_R axes go through the equator as is shown in Figure 5. These axes are the ones in which the force equations are integrated.

Local. The local axes, labeled by the subscript "L" have their origin on the earth's surface right below the vehicle. The Z_L axis is perpendicular to a tangent plane located in the earth's surface and passes up through the vehicle's center of gravity. The X_L axis lies in the tangent plane and always points north. The origin of the local axes are defined by the longitude, τ_R , and latitude, ψ_R , of the vehicle. These relationships are shown in Figure 5.

The transformation matrix for transferring a vector in the inertial system to one in the local axes is designated $[\mathcal{L}_{RL}]$ where,

$$\begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_L = [\mathcal{L}_{RL}] \begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_R$$

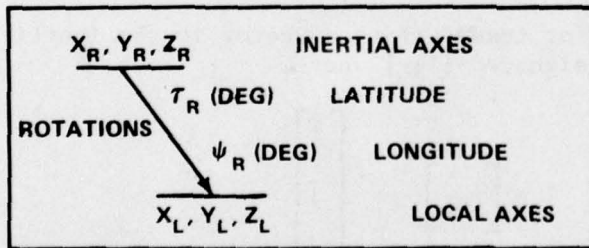
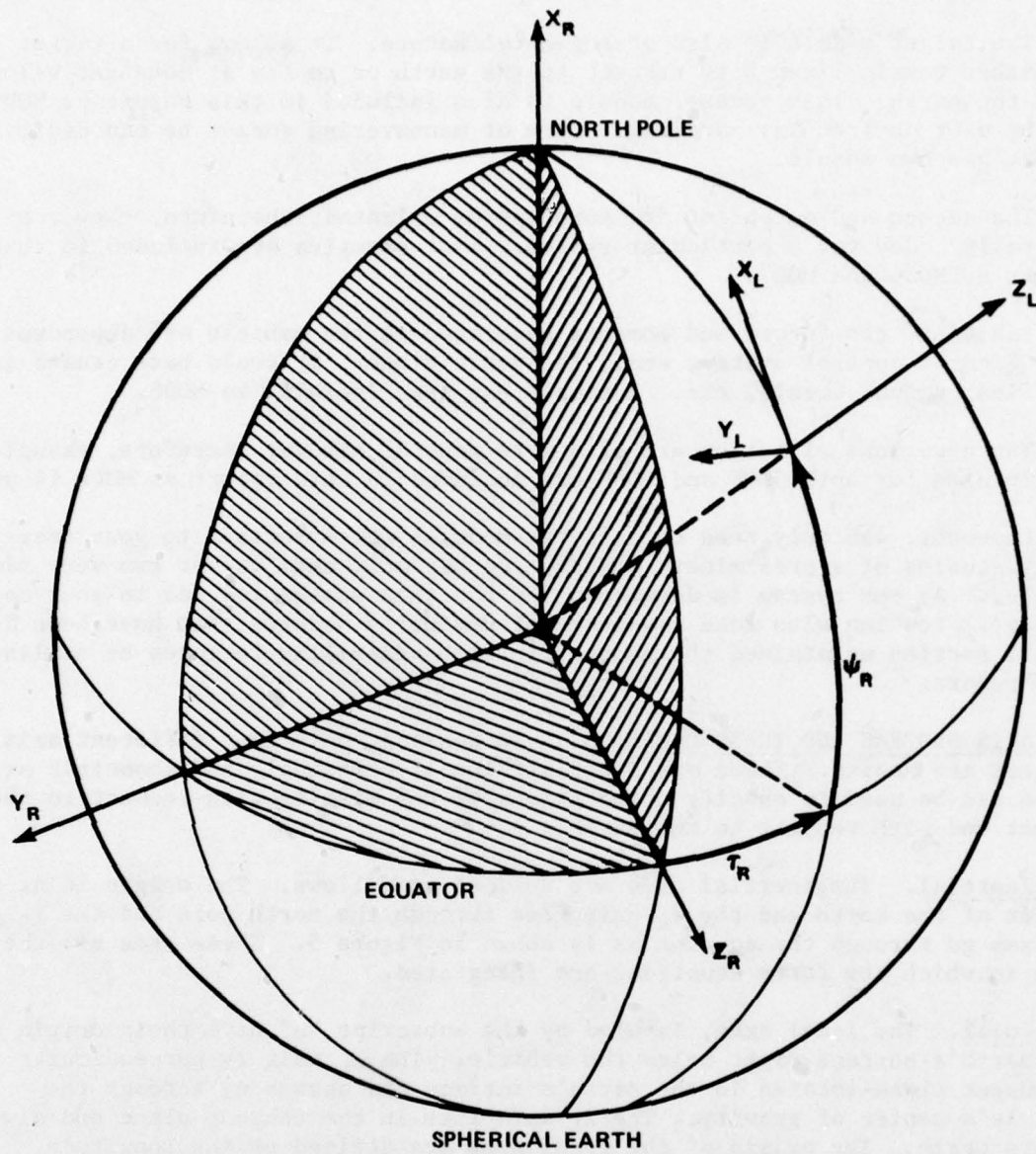


FIGURE 5 INERTIAL AND LOCAL AXES

and

$$[\ell_{RL}] = \begin{bmatrix} \cos\psi_R & \sin\psi_R \sin\tau_R & -\sin\psi_R \cos\tau_R \\ 0 & \cos\tau_R & \sin\tau_R \\ \sin\psi_R & -\cos\psi_R \sin\tau_R & \cos\psi_R \cos\tau_R \end{bmatrix}$$

The winds are generally defined with respect to these local axes as shown in Figure 8.

Principal Axes. These are the principal axes of the vehicle, i.e., their origin is at the center of mass and they consist of a set of cartesian axes for which the inertia tensor will be a diagonal (see Figures 6 and 7). The initial orientation of the principal axes with respect to the local axes is defined by the three angles γ_M , ϵ_M , and ϕ_M (in that order) where,

$$\begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_P = [\ell_{LP}] \begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_L$$

and

$$[\ell_{LP}] = \begin{bmatrix} \cos\epsilon_M \cos\gamma_M & -\cos\epsilon_M \sin\gamma_M & \sin\epsilon_M \\ \cos\phi_M \sin\gamma_M - \sin\phi_M \sin\epsilon_M \cos\gamma_M & \cos\phi_M \cos\gamma_M + \sin\epsilon_M \sin\gamma_M & \sin\phi_M \cos\epsilon_M \\ -\sin\phi_M \sin\gamma_M - \cos\phi_M \sin\epsilon_M \cos\gamma_M & -\sin\phi_M \cos\gamma_M + \cos\phi_M \sin\epsilon_M \sin\gamma_M & \cos\phi_M \cos\epsilon_M \end{bmatrix}$$

The means of arriving at this matrix after the initial time is defined and explained in MOD4.

Geometric Axes. These are a set of orthogonal axes which are defined for maximum convenience in expressing the vehicle aerodynamics. They will generally define a plane of symmetry for the vehicle external configuration and their origin will be located at the moment reference center. The relationship between these axes and the principal axes are shown in Figure 7. The center-of-gravity (c.g.) of the vehicle is defined with respect to the origin of the geometric axes by the lateral transformations X_{cg} , Y_{cg} and Z_{cg} . The angular orientation is expressed through the rotations ϕ_C^{cg} , ψ_C^{cg} , and χ_C^{cg} . These transformations are performed in the force and moment module, MOD8. The transformation matrix is defined as,

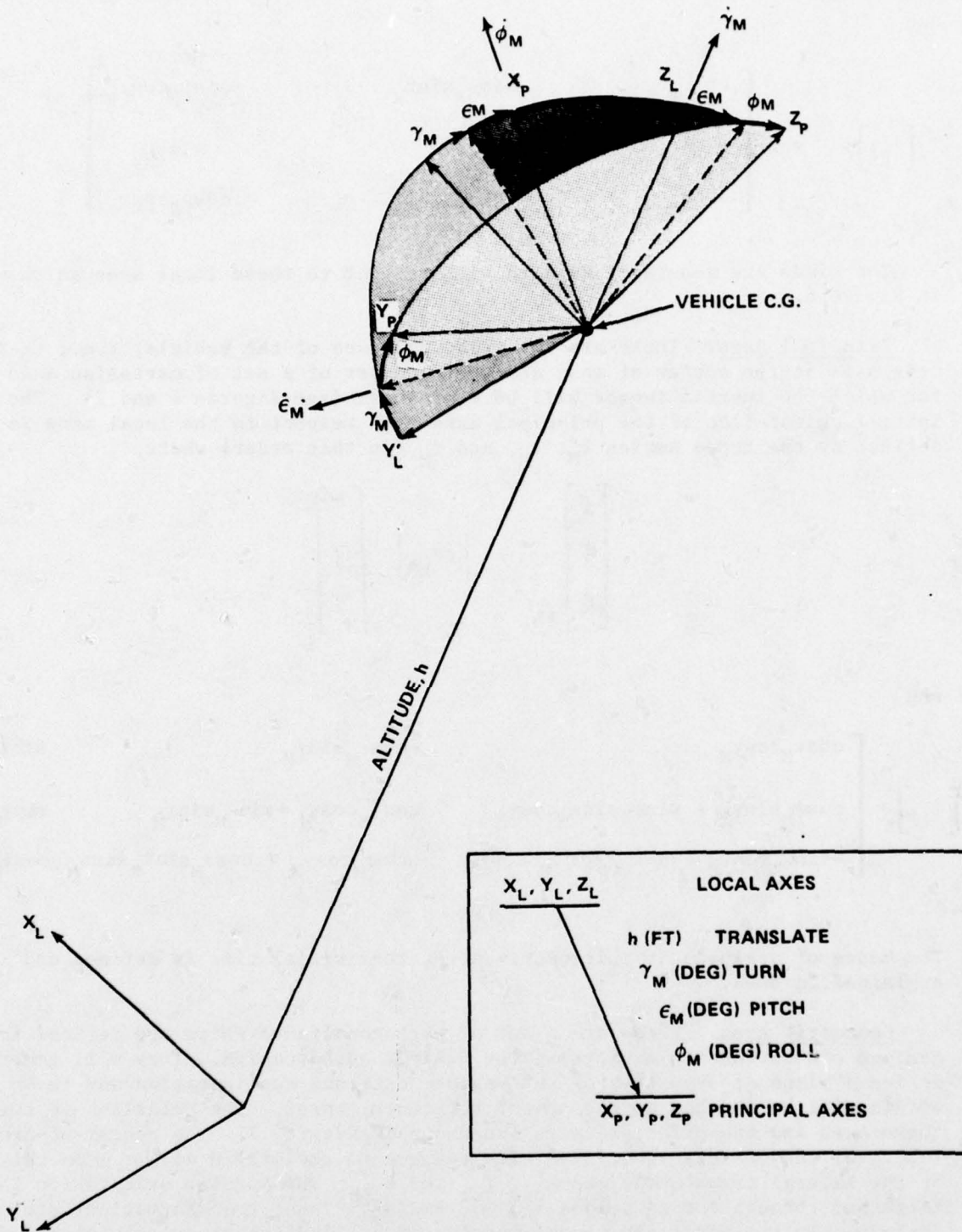


FIGURE 6 LOCAL AND PRINCIPAL AXES

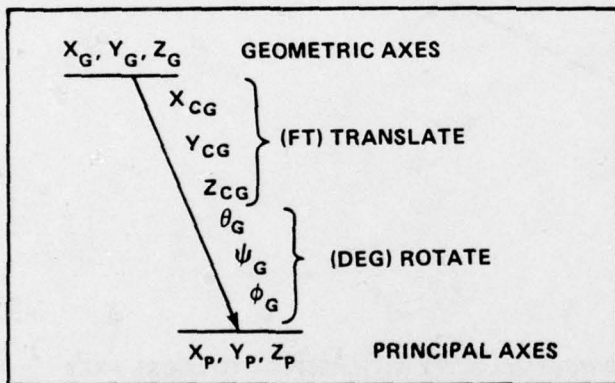
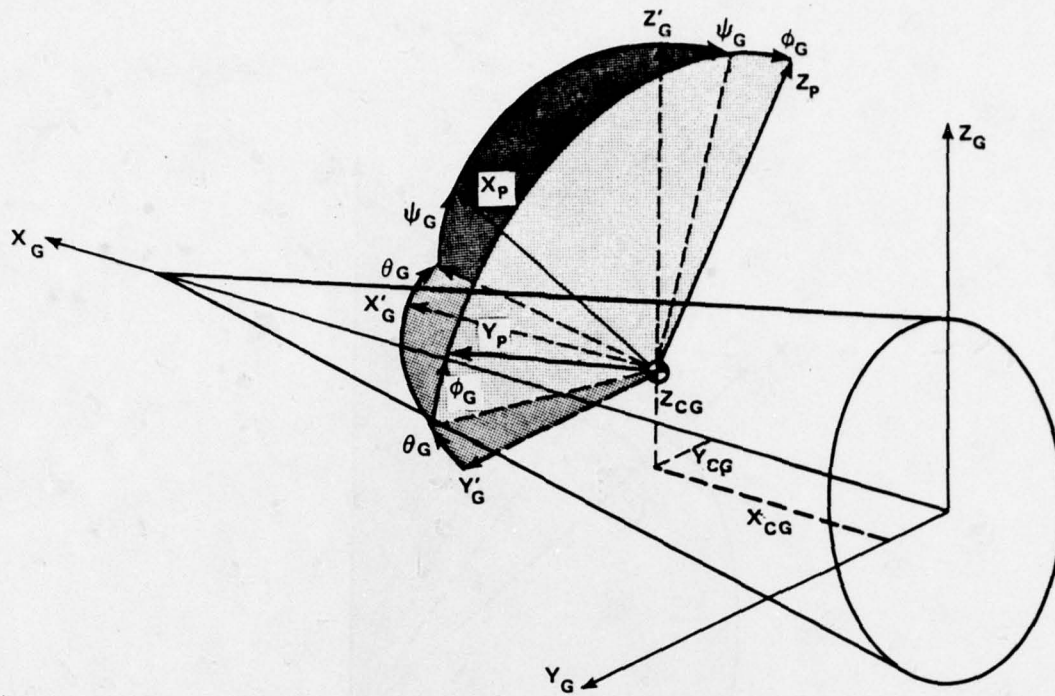


FIGURE 7 PRINCIPAL AND GEOMETRIC AXES

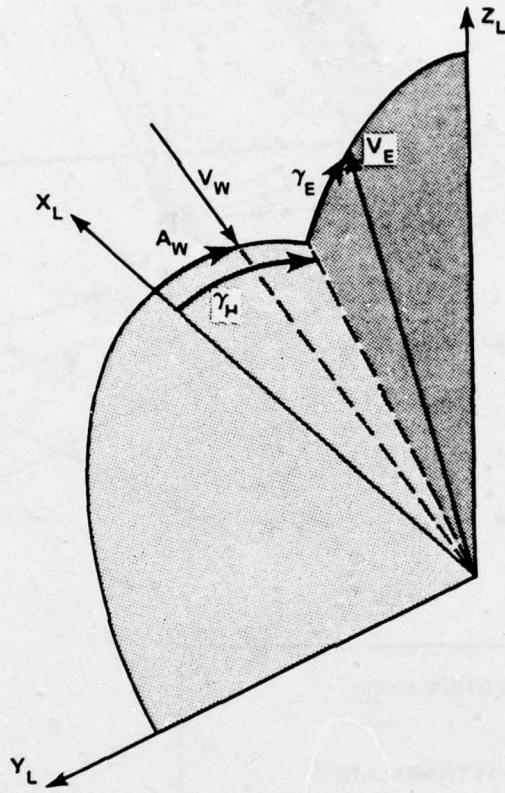


FIGURE 8 INITIAL MISSILE VELOCITY AND WIND VELOCITY WITH RESPECT TO LOCAL AXES

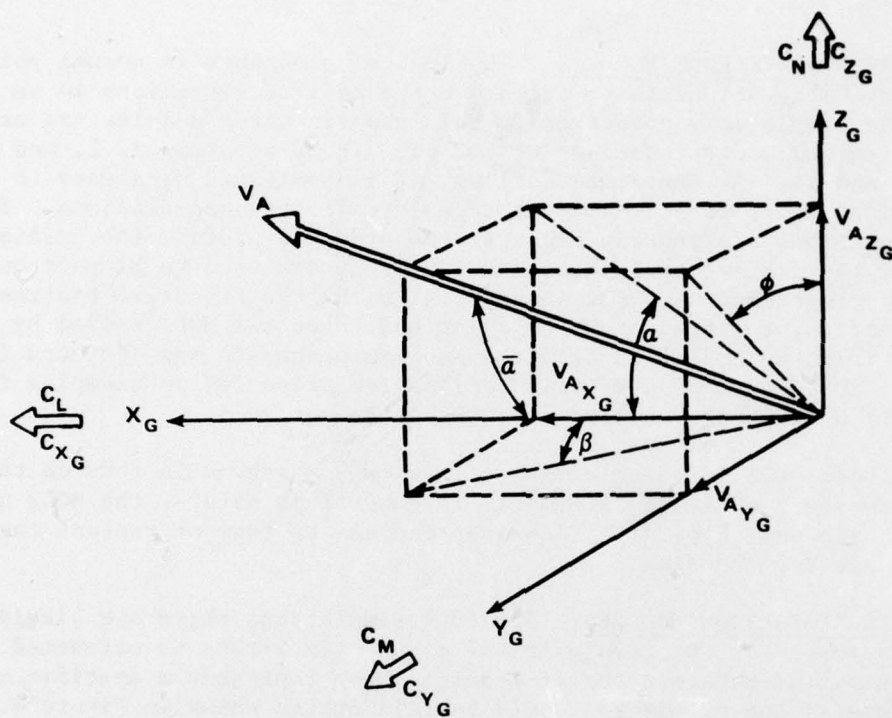


FIGURE 9 AERODYNAMIC COEFFICIENTS AND ANGLES DEFINED IN GEOMETRIC AXES

$$\begin{bmatrix} \lambda_{GP} \end{bmatrix} = \begin{bmatrix} \cos\psi_G \cos\theta_G & -\cos\psi_G \sin\theta_G & \sin\psi_G \\ \cos\phi_G \sin\theta_G - \sin\phi_G \sin\psi_G \cos\theta_G & \cos\phi_G \cos\theta_G + \sin\phi_G \sin\psi_G \sin\theta_G & \sin\phi_G \cos\psi_G \\ -\sin\phi_G \sin\theta_G - \cos\phi_G \sin\psi_G \cos\theta_G & -\sin\psi_G \cos\theta_G + \cos\phi_G \sin\psi_G \sin\theta_G & \cos\phi_G \cos\psi_G \end{bmatrix}$$

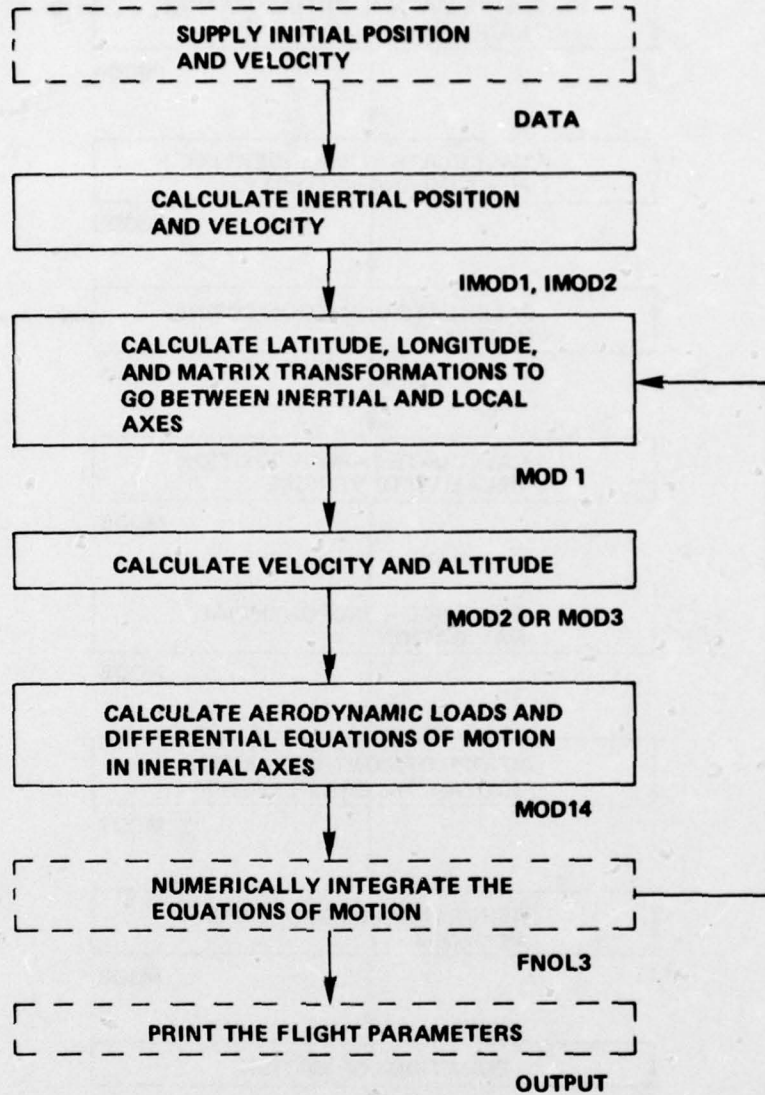
Aerodynamic coefficients and orientations of the vehicle with respect to the flow are generally defined with respect to these geometric axes as is shown in Figure 9.

THREE-DEGREES-OF-FREEDOM MODULES. The logical procedure in normal point-mass trajectory calculations is to integrate the body accelerations in an inertial system. In the sample case presented in this report, three modules are used to define the second order equations of motion. These are MODs 1, 2, and 14 or MODs 1, 3, and 14. As mentioned earlier, it is sometimes necessary to perform some calculations prior to starting the actual trajectory calculations. These types of calculations are usually necessary in order to provide the initial conditions for the differential equations. Since these need to be made only once, they are programmed as IMODs and are called by the executive routine prior to actually starting the trajectory calculations. For all MODs called by the program (identified by code 1 cards), the program checks to see if there is a corresponding IMOD. For the 3DOF calculations (as presented in examples included in this report) an IMOD is required for MODs 1, 2, and 3.

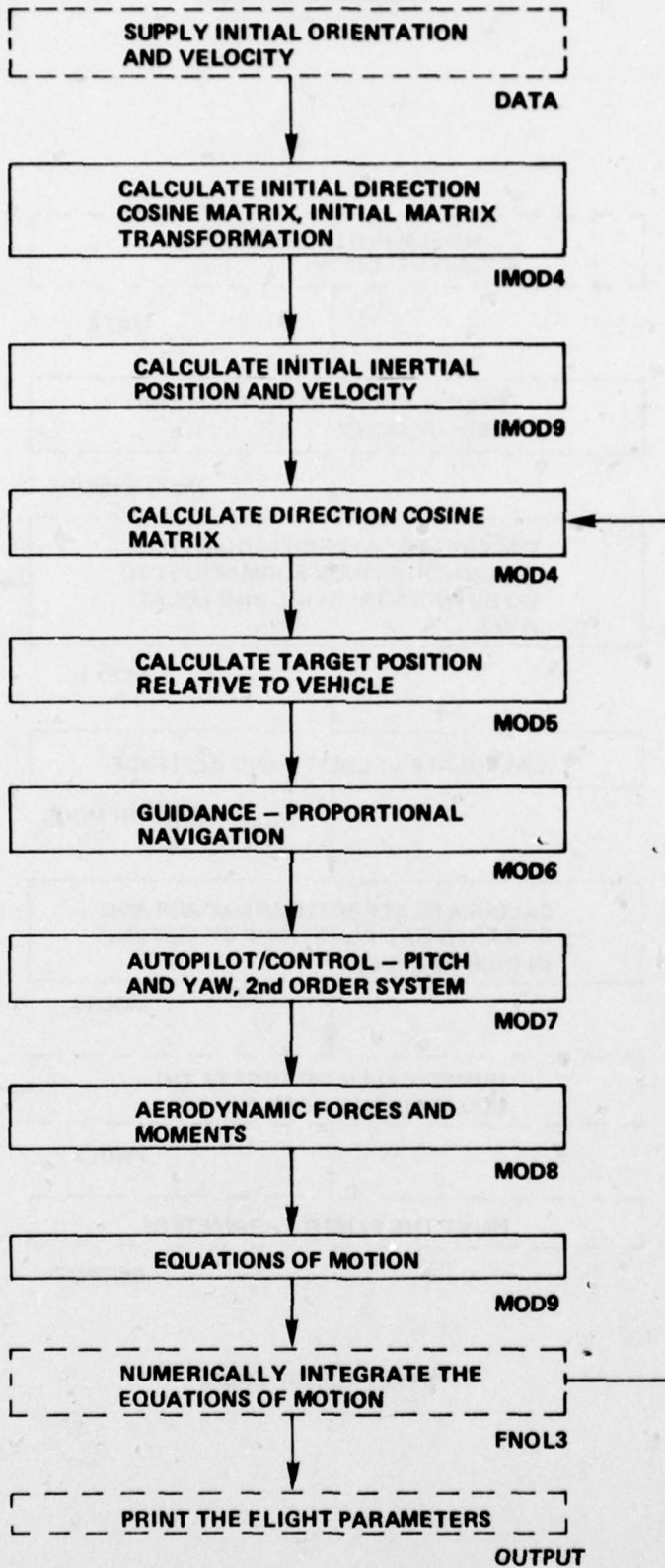
The flow logic used in these examples is shown in schematic form on the next page. Remember, while the schematic is general in nature, the MODs used in this report are only typical. Each user can add to them or replace them with those of his own choosing.

SIX-DEGREES-OF-FREEDOM MODULES. For 6DOF simulations there are likely to be six modules or more. If the complexity of a 6DOF simulation is warranted, it is usually necessary to prepare a set of modules which represent a specific missile system. In general the simulation would be laid out as shown in Figure 4. A group of typical modules have been selected and enclosed with this report in order to aid the user in the compilations of modules for his own simulation. The logic of these sample modules is shown on the following page.

IMOD4 and MOD4 are used to calculate the direction cosine matrix. It is unlikely that any changes or additions would have to be made to these modules since they deal with the mechanics of the situation, not a particular piece of hardware. MOD5 is used to calculate the location of the target. Here again, unless a particular maneuver of the target is to be programmed, it is unlikely that changes would be made to this module. IMOD9 and MOD9 are used to calculate the equations of motion of a vehicle for which the cross products of inertia are zero. MOD19 should be used in place of MOD9 if the cross products of inertia are not zero.



TYPICAL 3DOF LOGIC



TYPICAL 6DOF LOGIC

PROCESS. This routine is used to calculate any quantities that are desired for output but which are not necessary for the running of the program. An example of the type of things which can be calculated here are the longitudinal range along the equator, R_{τ_E} , and the latitudinal range, R_{ψ_E} . These are calculated as:

$$R_{\tau_E} = R_E [\tau_R - \omega_E (t - t_i)] - R_{\tau_{Ei}}$$

$$R_{\psi_E} = R_E \psi_R - R_{\psi_{Ei}}$$

A calculation of the total distance traveled over the earth's curved surface (projection of vehicle's path on the earth's surface) is calculated in the following manner.

$$\tau_E = \tau_R - \omega_E t$$

$$\Delta X^2 = [R_E \sin \psi_{RL} - R_E \sin \psi_R]^2$$

$$\Delta Y^2 = [-R_E \cos \psi_{RL} \sin \tau_E + R_E \cos \psi_R \sin \tau_E]^2$$

$$\Delta Z^2 = [R_E \cos \psi_{RL} \cos \tau_E - R_E \cos \psi_R \cos \tau_E]^2$$

where ψ_{RL} and τ_E are the last latitude and longitude calculated (last time program executed subroutine PROCESS). The increment of the chord of travel over a segment of the earth's surface is then expressed as,

$$\Delta C = \sqrt{\Delta X^2 + \Delta Y^2 + \Delta Z^2}$$

and the angle subtended by the chord as

$$\theta_c = 2 \sin^{-1} \left(\frac{\Delta C}{2R_E} \right)$$

The increment of surface traversed is then equal to

$$\Delta R_S = R_E \theta$$

and

$$R_S = R_S + \Delta R_S$$

is the total distance traveled.

Any similar calculations can be made and added to PROCESS. See Appendix P for its current form.

SETUP PROCEDURE

The required parameters in the setup deck will depend on what modules are in use; but, the general procedure and types of cards are usually the same. The following is a generalized listing of the most used setup and control cards. The general procedure is to prepare the deck as follows:

1. Title card, code 0.
2. Select the appropriate modules for your simulation and arrange the code 1 control cards in the order that the modules are to be called.
3. Provide the data cards, code 3, required by the executive routines. These are mostly integration controls and general physical descriptors. These are located in the executive and generalized input sections of the Y array, locations Y(2300) - Y(3099). See Appendix B for specific, required parameters.
4. Determine what the termination conditions are and set their values with code 4 control cards.
5. Specify all of the remaining initial conditions required by the modules with code 3 cards. These are parameters which generally have to do with defining the initial attitude of the vehicle.

- a. Locate the local axes by giving the longitude, τ_R (deg) in Y(3014) and the latitude, ψ_R (deg) in Y(3015).
- b. Define the initial altitude, h(ft) in Y(3013).
- c. Locate the principal axes with respect to the local axes by specifying,

γ_M (deg) in Y(2066)	}	IMOD4
ϵ_M (deg) in Y(2067)		
ϕ_M (deg) in Y(2068)		

- d. Define the initial velocity with respect to the local axes.

V_E (fps) in Y(610)	}	IMOD2 MODs 2, 3
γ_E (deg) in Y(2209)		
γ_H (deg) in Y(2208)		

- e. Define the angular orientation of the principal axes with respect to the geometric axes that you are using.

X_{CG} (ft)	in Y(3006)	}	MOD8
Y_{CG} (ft)	in Y(3007)		
Z_{CG} (ft)	in Y(3008)		
θ_G (deg)	in Y(3019)		
ψ_G (deg)	in Y(3020)		
ϕ_G (deg)	in Y(3021)		

- f. Define all other constants required by the modules you are using.
- Decide what parameters you want listed in the output and identify them, their titles, and formats on code 2 control cards.
 - List all of the dependent variables on code 6 control cards.
 - List all of the derivatives for the above dependent variables on code 7 control cards.
 - Supply the tables that you are using. Define the location (in your deck) of each of the table array numbers on code 8 control cards and then place all of the tables in that specified order behind a single code 9 control card.

FORTRAN LISTINGS OF EXECUTIVE
ROUTINES

NSWC/WOL TR 78-59

```

*DECK TRI
C 03/13/75 12.56.47 JOHN HOLMES TR100010
OVERLAY(TRAJ,0,0) TR100100
PROGRAM OV (INPUT,OUTPUT,TAPE5,TAPE19,TAPE9,TAPE6=OUTPUT)
C 8/2/77 JOHN HOLMES
COMMON Y(4940) TR100140
COMMON/TAB/Z(50) TR100150
EQUIVALENC(Y(2311),NO PLOT) TR100160
100 CALL ZERO TR100170
200 CALL INPUT TR100180
300 CALL OVERLAY(4HTRAJ,1,0,6HRECALL)
IF(NO PLOT.GT.0) GO TO 900 TR100200
500 CALL RESET TR100210
GO TO 300 TR100220
900 CALL OVERLAY(4HTRAJ,2,0,6HRECALL)
GO TO 500 TR100240
1000 STOP TR100250
END TR100260

SUBROUTINE ZERO TR100270
7/2/74 JOHN E. HOLMES TR100280
COMMON Y(4940) TR100290
EQUIVALENC(Y(2302),J),(Y(2305),MPR) TR100300
EQUIVALENC(Y(2304),L),(Y(2301),XNE) TR100310
EQUIVALENC(Y(2306),ERROR) TR100320
EQUIVALENC(Y(3000),RE),(Y(3001),WE) TR100330
DO 1 I=1,4940 TR100340
1 Y(I)=0.0 TR100350
TR100360
C TR100370
C TR100380
C TR100390
C TR100400
C J=2 TR100410
Y(2302)=2.0 TR100420
MPR=1 TR100430
Y(2305)=1.0 TR100440
C I=0 TR100450
Y(2304)=0.0 TR100460
XNE=0.0 TR100470
ERROR=-1.0 TR100480
WF=0.000072921150P TR100490
C TR100500
C MEAN RADIUS FOR SPHERICAL EARTH TR100510
RF=20925631. TR100520
C TR100530
RETURN TR100540
END TR100550

SUBROUTINE INPUT TR100560
7/2/74 JOHN F. HOLMES TR100570
COMMON Y(4940) TR100580
INTEGER OUTNO,STPNO(10),PLOT(10),CVAR(31),DVAR(31) TR100590
EQUIVALENC(Y(2307),NOMOD),(Y(2312),NMCD(1)) TR100600
EQUIVALENC(Y(2308),NOOUT),(Y(2332),RNME1(1)),(Y(2392),OUTNO(1)) TR100610
EQUIVALENC(Y(2309),NOTN),(Y(2422),INNO(1)),(Y(2622),VALVE(1)) TR100620
EQUIVALENC(Y(2310),NOSTOP),(Y(2822),STPNO(1)),(Y(2832),SUP(1)), TR100630
*(Y(2842),SIO(1)) TR100640
EQUIVALENC(Y(2311),NO PLOT),(Y(2852),PLOT(1)) TR100650
EQUIVALENC(Y(2872),LOCC(1)),(Y(2903),CVAR(1)),(Y(2934),LOCD(1)) TR100660
EQUIVALENC(Y(2965),DVAR(1)),(Y(4890),KTAB(1)),(Y(2871),NOTAR) TR100670
EQUIVALENC(Y(2870),NODER),(Y(2869),NOVAR) TR100680
TR100690
TR100700
TR100710

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```

EQUIVALENC(Y(3051),K(1)),(Y(3044),TITL(1))
EQUIVALENC(Y(2996),KEND)
EQUIVALENC(Y(2362),HD1(1)),(Y(2377),HD2(1))
DIMENSION TITL(7),NMOD(20),RNMF1(30),OITNO(30),INNO(200)
+,VALVE(200),SUP(10),SLO(10),K(49)
+LOCC(31),LOCD(31),KTAR(49)
DIMENSION HD1(15),HD2(15)
NOIN=0
NOMOD=0
NOOUT=0
NOSTOP=0
NOPL0T=0
NOVAR=0
NODER=0
NOTAR=0
CK=10H
DO 970 I=1,15
HD1(I)=5HFA.0
970 HD2(I)=5HFA.0
DO 101 I=1,49
101 K(I)=0
RFAD(5,998) IR,(TITL(I),I=1,7)
XDATE=DATE(DIIM)
XTIME=TIME(DUMY)
WRITE(6,5000)
5000 FORMAT(1H1,T56,*NAVAL SURFACE WEAPONS CENTER*/
+T59,*WHITE OAK LAHORATORY*)
WRITE(6,5001) (TITL(I),I=1,7),XDATE,XTIME
5001 FORMAT(1H0,10X,7A10,T87,*RUN DATE*,A10,T107,*TIME*,A10/)
2000 FORMAT(1H1)
998 FORMAT(I2,7A10)
IPRT=1
1 RFAD(5,1000) IR,IN,VAR,VARR,HED1,HED2,HED3
1000 FORMAT(I2,T6,2E14.6,A10,A7,A10)
GO TO(2,3) IPRT
2 IPRT=2
IR1=IR$IN1=IN$VAR]=VAR$VARR]=VARR$HFD1]=HED1$HFD2]=HED2$HFD3]=HED3
GO TO 4
3 IPRT=1
WRITE(6,1001)IR1,IN1,VAR1,VARR1,HED11,HED21,HFD31,IP,IN,VAR,
+VARR,HED1,HED2,HED3
1001 FORMAT(1H ,I2,I6,2E14.6,A10,A7,A10,3X,2H**,3X,I2,I6,
+2F14.6,A10,A7,A10)
4 CONTINUE
C
C MODULE NUMBER
C
5 IF(IR.NE.1) GO TO 10
NOMOD=NOMOD+1
IF(NOMOD.GT.20) GO TO 6
GO TO 7
6 WRITE(6,4001)
4001 FORMAT(1H0,*THE NUMBER OF MODULES EXCEEDS 20*)
STOP
7 CONTINUE
NMOD(NOMOD)=IN
GO TO 1
C
C VARIABLE TO BE LISTED IN OUTPUT
C
10 IF(IR.NE.2) GO TO 15
NOOUT=NOOUT+1
IF(NOOUT.GT.30) GO TO 11
GO TO 12
11 WRITE(6,4002)
4002 FORMAT(1H0,*PRINTOUT OF MORE THAN 30 ITEMS WAS CONSIDERED

```

TR100720
TR100730
TR100735
TR100740
TR100750
TR100760
TR100765
TR100770
TR100780
TR100790
TR100800
TR100810
TR100820
TR100830
TR100840
TR100842
TR100844
TR100845
TR100846
TR100850
TR100860
TR100870
TR100872
TR100874
TR100876
TR100878
TR100879
TR100880
TR100882
TR100890
TR100900
TR100905
TR100910
TR100915
TR100920
TR100925
TR100930
TR100940
TR100945
TR100950
TR100955
TR100960
TR100965
TR100968
TR100970
TR100980
TR100990
TR101000
TR101010
TR101020
TR101030
TR101040
TR101050
TR101060
TR101070
TR101080
TR101090
TR101100
TR101110
TR101120
TR101130
TR101140
TR101150
TR101160
TR101170
TR101180

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	EXCESSIVE AND THEY WERE DROPPED)	TR101190
	NOOUT=NOOUT-1	TR101195
	GO TO 1	TR101200
12	CONTINUE	TR101210
	RNME1(NOOUT)=HED1	TR101220
	IF(HED3.EQ.CK) GO TO 230	TR101222
	IF(NOOUT.GT.15) GO TO 220	TR101225
	HD1(NOOUT)=HED3	TR101227
	GO TO 230	TR101229
220	NOT=NOOUT-15	TR101231
	HD2(NOT)=HED3	TR101233
230	CONTINUE	TR101235
	OUTNO(NOOUT)=IN	TR101240
	GO TO 1	TR101250
C		TR101260
C	DATA LOCATION AND VALUF	TR101270
C		TR101280
	15 IF(IR.NE.3) GO TO 20	TR101290
	NOIN=NOIN+1	TR101300
	IF(NOIN.GT.200) GO TO 16	TR101310
	GO TO 17	TR101320
16	WRITE(6,4003)	TR101330
4003	FORMAT(1H0.*NUMBER OF INPUT VARIABLES EXCEEDS 200*)	TR101340
	STOP	TR101350
17	CONTINUE	TR101360
	INNO(NOIN)=IN	TR101370
	VALVE(NOIN)=VAR	TR101380
	GO TO 1	TR101390
C		TR101400
C	TERMINATION VARIABLE WITH UPPER AND LOWER BOUNDS	TR101410
C		TR101420
	20 IF(IR.NE.4) GO TO 30	TR101430
	NOSTOP=NOSTOP+1	TR101440
	IF(NOSTOP.GT.10) GO TO 21	TR101450
	GO TO 22	TR101460
21	WRITE(6,4004)	TR101470
4004	FORMAT(1H0.*NUMBER OF STOP CONDITIONS EXCEEDS 10*)	TR101480
	STOP	TR101490
22	CONTINUE	TR101500
	STPNO(NOSTOP)=IN	TR101510
	SUP(NOSTOP)=VARR	TR101520
	SLO(NOSTOP)=VAR	TR101530
	GO TO 1	TR101540
C		TR101550
C	VARIABLES TO BE PLOTTED	TR101560
C		TR101570
	30 IF(IR.NE.5) GO TO 40	TR101580
	NOPLOT=NOPLOT+1	TR101590
	IF(NOPLOT.GT.10) GO TO 31	TR101600
	GO TO 32	TR101610
31	WRITE(6,4005)	TR101620
4005	FORMAT(1H0.*NUMBER OF PLOT VARIABLES EXCEEDS 10*)	TR101630
	STOP	TR101640
32	CONTINUE	TR101650
	PLOT(NOPLOT)=IN	TR101660
	GO TO 1	TR101670
C		TR101680
C	DEPENDENT VARIABLES, C ARRAY	TR101690
C		TR101700
	40 IF(IR.NE.6) GO TO 50	TR101710
	NOVAR=NOVAR+1	TR101720
	IF(NOVAR.GT.28) GO TO 42	TR101730
	GO TO 43	TR101740
42	WRITE(6,4000)	TR101750
4000	FORMAT(1H0.*THE NUMBER OF DIFFERENTIAL EQUATIONS EXCFEDS 28*)	TR101760
	STOP	TR101770

43	CONTINUE	TR101780
	LOCC(NOVAR)=VAR	TR101790
	CVAR(NOVAR)=IN	TR101800
	GO TO 1	TR101810
C		TR101820
C	DERIVATIVES, D ARRAY	TR101830
C		TR101840
50	IF(IR.NE.7) GO TO 60	TR101850
	NODER=NODER+1	TR101860
	LOCD(NODER)=VAR	TR101870
	DVAR(NODER)=IN	TR101880
	GO TO 1	TR101890
C		TR101900
C	TABULATED VALUES	TR101910
60	IF(IR.NE.8) GO TO 70	TR101920
	NOTAB=NOTAB+1	TR101930
	IF(NOTAB.GT.49) GO TO 61	TR101940
	GO TO 62	TR101950
61	WRITE(6,4006)	TR101960
4006	FORMAT(1H0,*THE NUMBER OF TABLES EXCEEDS 49*)	TR101970
	STOP	TR101980
62	CONTINUE	TR101990
	IVAR=VAR	TR102000
	KTAB(IVAR)=IN	TR102010
	GO TO 1	TR102020
C		TR102030
C	AN INDICATOR THAT TABLES ARE TO BE READ	TR102040
C		TR102050
70	IF(IR.NE.9) GO TO 80	TR102060
	CALL TAPTAR(K,KEND)	TR102070
	GO TO 1	TR102080
80	CONTINUE	TR102090
C	END OF DATA FOR A SINGLE RUN	TR102100
90	WRITE(6,2000)	TR102110
	RETURN	TR102120
	END	TR102130
		TR102140
		TR102150
		TR102160
		TR102170
		TR102180
		TR102190
C	SUBROUTINE RESFT	TR102200
	7/2/74 JOHN E. HOLMES	TR102210
	COMMON Y(4940)	TR102220
	INTEGER STPNO(10)	TR102230
	EQUIVALENC(Y(2863),STOP)	TR102240
	EQUIVALENC(Y(2307),NOMOD),(Y(2312),NMOD(1))	TR102250
	EQUIVALENC(Y(2309),NOTN),(Y(2422),INNO(1)),(Y(2622),VALVE(1))	TR102260
	EQUIVALENC(Y(2871),NOTAB),(Y(4890),KTAB(1))	TR102270
	EQUIVALENC(Y(2306),ERROR),(Y(2996),STAGE)	TR102280
	EQUIVALENC(Y(3044),TITL(1)),(Y(2301),XNE)	TR102290
	EQUIVALENC(Y(2310),MOSTOP)	TR102300
	EQUIVALENC(Y(2822),STPNO(1)),(Y(2832),SUP(1)),(Y(2842),SLO(1))	TR102310
	DIMENSION TITL(7),NMOD(20),INNO(200),VALVE(200),KTAR(49)	TR102320
	DIMENSION SUP(10),SLO(10)	TR102330
	READ(5,998) IR,(TITL(I),I=1,7)	TR102340
C	IR = 99, STOP, ALL RUNS FINISHED	TR102350
	IF(IR.EQ.99) STOP	TR102360
C	IR = 11, STAGING HAS OCCURRED, NEW MODS AND TABLES ARE TO BE USED	TR102370
	IF(IR.EQ.11) GO TO 80	TR102380
	DO 10 I=1,2307	TR102390
10	Y(I)=0.0	TR102400
	DO 12 I=2862,2868	TR102410
12	Y(I)=0.0	TR102420
	Y(2998)=0.0	TR102430
	Y(2999)=0.0	

```

REWIND 19
DO 14 I=3002,3043
14 Y(I)=0.0
C*****
C   DEFAULT OPTIONS
C
C   J=2
C   Y(2302)=2.0
C   MPR=1
C   Y(2305)=1.0
C   L=0
C   Y(2304)=0.0
C   XNE=0.0
C   ERROR=-1.0
C*****
80 GO TO 85
80 CONTINUE
   STOP=0.
   STAGE=STAGF+1.0
85 CONTINUE
   WRITE(6,999) (TITL(I),I=1,7)
   NOMOD=0
   NOSTOP=0
   NOTAB=0
100 READ(5,1000) IR,IN,VAR,VARR,HED1,HED2,HED3,HED4
   WRITE(6,1001) IR,IN,VAR,VARR,HED1,HED2,HED3,HED4
1000 FORMAT(I2,T6,2F14.6,A10,A7,A10,A9)
1001 FORMAT(IX,T2,I6,2F14.6,A10,A7,A10,A9)
C   MODULE NUMRER
C   IF(IR.NE.1) GO TO 110
C   NOMOD=NOMOD+1
C   NMOD(NOMOD)=IN
C   GO TO 100
C   DATA LOCATON AND VALUF
110 IF(IR.NE.3) GO TO 120
   NOIN=NOIN+1
   INNO(NOIN)=IN
   VALVE(NOIN)=VAR
   GO TO 100
120 IF(IR.NE.4) GO TO 125
C   TERMINATION VARIABLES
   NOSTOP=NOSTOP+1
   STPNO(NOSTOP)=IN
   SUP(NOSTOP)=VARR
   SLO(NOSTOP)=VAR
   GO TO 100
C   TABULATED VALUES
125 IF(IR.NE.8) GO TO 130
   NOTAB=NOTAB+1
   IVAR=VAR
   KTAB(IVAR)=IN
   GO TO 100
C   END OF DATA FOR A SINGLE RUN
130 IF(IR.NE.10) GO TO 100
   WRITE(6,2000)
2000 FORMAT(1H1)
999 FORMAT(1H0,7A10)
99R FORMAT(I2,7A10)
RETURN
END
SUBROUTINE TAPTAB(K,KEND)
C
C   7/2/74   JOHN E. HOLMES
C
C   IT READS THE DATA CARDS FOR THE TABLES , ARRANGES THEM INTO THE
C   TABLE ARRAY, AND WRITES THE TABLE ARRAY ON FILE 9

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TR102435
TR102440
TR102450
TR102460
TR102470
TR102480
TR102490
TR102500
TR102510
TR102520
TR102530
TR102540
TR102550
TR102560
TR102570
TR102580
TR102590
TR102600
TR102610
TR102620
TR102630
TR102640
TR102650
TR102660
TR102670
TR102680
TR102690
TR102700
TR102710
TR102720
TR102730
TR102740
TR102750
TR102760
TR102770
TR102780
TR102790
TR102800
TR102810
TR102820
TR102830
TR102840
TR102850
TR102860
TR102870
TR102880
TR102890
TR102900
TR102910
TR102920
TR102930
TR102940
TR102950
TR102960
TR102970
TR102980
TR102990
TR103000
TR103010
TR103020
TR103030
TR103040
TR103050
TR103060
TR103070
TR103080

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C		TR103090
C	TAPTAR IS A SUBROUTINE TO BE USED WITH FRMRAN.	TR103100
C		TR103110
C		TR103120
C	TABLE (1) = N(1) NUMBER OF ARGUMENTS FOR FIRST VARIABLE	TR103130
C	TABLE (2) = N(2) NUMBER OF ARGUMENTS FOR SECOND VARIABLE	TR103140
C	...	TR103150
C	TABLE (N) = N(N) NUMBER OF ARGUMENTS FOR N-TH VARIABLE	TR103160
C	TABLE(N+1) = U(1,1) FIRST OF ARGUMENTS CORRESPONDING TO	TR103170
C	THE FIRST VARIABLE	TR103180
C	...	TR103190
C	TABLE(N+N(1)) = U(1,N(1)) LAST OF ARGUMENTS CORRESPONDING	TR103200
C	TO THE FIRST VARIABLE	TR103210
C	TABLE(N+N(1)+1) = U(2,1) FIRST OF THE ARGUMENTS CORRESPONDING	TR103220
C	TO THE SECOND VARIABLE	TR103230
C	...	TR103240
C	TABLE(N+N(1)+N(2)) = U(2,N(2)) LAST OF THE ARGUMENTS	TR103250
C	CORRESPONDING TO THE SECOND VARIABLE	TR103260
C	...	TR103270
C	TABLE(N+N(1)+N(2)+...+N(N)) = U(N,N(N)) LAST OF ARGUMENTS	TR103280
C	CORRESPONDING TO THE N TH VARIABLE	TR103290
C	TABLE(N+N(1)+N(2)+...+N(N)+1) = ARG(1,1,...,1) TABLE VALUE	TR103300
C	CORRESPONDING TO THE FIRST ARGUMENT OF	TR103310
C	EACH VARIABLE	TR103320
C	TABLE(N+N(1)+N(2)+...+N(N)+1) = ARG(1,1,...,1,2)	TR103330
C	...	TR103340
C	...	TR103360
C	TABLE(N+N(1)+N(2)+...+N(N)+N(1)+1) = ARG(1,1,...,2,1)	TR103350
C	TABLE(N+N(1)+N(2)+...+N(N)+N(1)*N(2)+...+N(N)) = ARG(N(1),N(2)	TR103370
C,N(N))	TR103380
C		TR103390
C	READS IN THE ADDITIONAL TABLE VALUES STARTING IN THE NEXT	TR103400
C	AVAILABLE LOCATION IN THE TABLE ARRAY AND USING THE SAME	TR103410
C	ARRANGEMENT AS ABOVE	TR103420
C		TR103430
C		TR103440
C	FOR ADDITIONAL TABLES, TAPTAB READS THEM IN AS ABOVE, STARTING	TR103450
C	IN THE NEXT AVAILABLE LOCATION IN THE TABLE ARRAY	TR103460
C		TR103470
C		TR103480
C	L,NUM,MFNC,N(1),N(2),...,N(NUM) (WITH FORMAT 1415)	TR103530
C	THE CONTROL CARDS MUST BE OF THE FOLLOWING FORMAT	TR103520
C		TR103510
C	M(J) = NUMBER OF FUNCTIONS TABULATED FOR THE J-TH TABLE	TR103500
C	NI(J) = NUMBER OF VARIABLES IN THE J-TH TABLE	TR103490
C	L=0,NUM NE 0 ONE TABLE OF NUM INDEPENDENT VARIABLES IS READ	TR103540
C	THE DECK OF THE TABLE IS AS FOLLOWS	TR103550
C	N(1) ARGUMENTS (VALUES) OF THE FIRST	TR103560
C	VARIABLE - IN ASCENDING ORDER WITH SIX PER	TR103570
C	CARD	TR103580
C	N(2) ARGUMENTS OF THE SECOND VARIABLE,	TR103590
C	BEGINNING ON A NEW CARD, IN ASCENDING ORDER	TR103600
C	WITH SIX PER CARD	TR103610
C	...	TR103620
C	N(NUM) ARGUMENTS OF U(NUM), BEGINNING ON A	TR103630
C	NEW CARD, IN ASCENDING ORDER WITH SIX PER	TR103640
C	CARD,	TR103650
C	THE FIRST FUNCTION TABULATED IS PUNCHED IN	TR103660
C	BLOCKS OF N(NUM) WITH SIX PER CARD, THE	TR103670
C	FIRST BLOCK STARTS WITH THE VALUE	TR103680
C	CORRESPONDING TO THE SMALLEST ARGUMENT OF	TR103690
C	EACH VARIABLE AND ALLOWS U(N) TO VARY,	TR103700
C	THE NEXT BLOCK STARTS ON A NEW CARD AND HAS	TR103710
C	U(N-1) INCREMENTED AND ALLOWS U(N) TO VARY	TR103720
C	AND SO ON UNTIL THE ENTIRE TABULATION IS	TR103730
C	COMPLETED.	TR103740

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C	IF MFNC IS GREATER THAN ONE, REPEAT FOR	TR103750
C	EACH SUCCEEDING FUNCTION TO BE INCLUDED IN	TR103760
C	THE TABLE.	TR103770
C		TR103780
C	L=0, NUM=0 TERMINATE THE RUN	TR103790
C		TR103800
C		TR103810
C		TR103820
	DIMENSION K(1), TABLE(100), N(15), M(49), T(7), NI(49)	TR103830
	EQUIVALENCF (NARG, ARG)	TR103840
	KOUNT = 1	TR103850
	NFXLOC = 0	TR103860
	DO 310 I=1, 100	TR103870
310	TABLE(I)=0.	TR103880
300	READ(5, 201) (T(I), I=1, 7), DUM	TR103890
	WRITE(6, 202)	TR103900
	WRITE(6, 201) (T(I), I=1, 7), DUM	TR103910
	READ(5, 100) L, NUM, M(KOUNT), (N(I), I=1, NUM), DUM	TR103920
	WRITE(6, 100) L, NUM, M(KOUNT), (N(I), I=1, NUM), DUM	TR103930
	IF (L.NE.0.OR.NUM.GT.15.OR.M(KOUNT).GT.15) GOTO 800	TR103940
	IF (NUM.EQ.0) RETURN	TR103950
	NT(KOUNT) = NUM	TR103960
	K(KOUNT)=NFXLOC+1	TR103970
C		TR103980
C	TO CALCULATE THE PRODUCT OF THE N(I) S	TR103990
C	AND PUT THE N(I) S IN THE TABLE	TR104000
C		TR104010
	NSUM = 0	TR104020
	NPROD = 1	TR104030
	DO 400 I=1, NUM	TR104040
	NARG = N(I)	TR104050
	NSUM = NSUM + NARG	TR104060
	NPROD = NPROD * NARG	TR104070
	TABLE(I) = ARG	TR104090
400	CONTINUE	TR104100
	BUFFER OUT (9, 1) (TABLE(I), TABLE(NUM))	TR104110
	IF (UNIT(9)) 450, 450, 1000	TR104120
450	CONTINUE	TR104130
C		TR104140
C	TO PUT U(I) S IN THE TABLE	TR104150
C		TR104160
	KSTART = NI(M) + NFXLOC + 1	TR104170
	DO 500 I=1, NUM	TR104180
	KFND = KSTART + N(I) - 1	TR104190
	KKEND=KEND-KSTART+1	TR104200
	IF (KKEND.GE.99) GO TO 400	TR104210
	READ(5, 110) (TABLE(KK), KK=1, KKEND)	TR104220
	WRITE(6, 203) (TABLE(KK), KK=1, KKEND)	TR104230
	BUFFER OUT (9, 1) (TABLE(I), TABLE(KKEND))	TR104240
	IF (UNIT(9)) 490, 490, 1000	TR104250
490	CONTINUE	TR104260
	KSTART = KFND + 1	TR104270
500	CONTINUE	TR104280
C		TR104290
C	TO PUT THE TABULATED VALUES IN THE TABLE	TR104300
C		TR104310
	KADD = N(NI(M)) - 1	TR104320
	IFND = NPROD * M(KOUNT) / N(NUM)	TR104330
	DO 600 I=1, IFND	TR104340
	KEND = KSTART + KADD	TR104350
	KKEND=KEND-KSTART+1	TR104360
	IF (KKEND.GE.99) GO TO 400	TR104370
	READ(5, 110) (TABLE(KK), KK=1, KKEND)	TR104380
	WRITE(6, 203) (TABLE(KK), KK=1, KKEND)	TR104390
	BUFFER OUT (9, 1) (TABLE(I), TABLE(KKEND))	TR104400
	IF (UNIT(9)) 580, 580, 1000	TR104410

580	CONTINUE	TR104420
	KSTART = KFND + 1	TR104430
600	CONTINUE	TR104440
	NFXLOC=KEND	TR104450
	KOUNT = KOUNT + 1	TR104460
	IF(KEND.GE.3000)GO TO 950	TR104470
	GO TO 300	TR104480
800	WRITE(6,200)	TR104490
	STOP	TR104500
900	WRITE(6,220)	TR104510
	STOP	TR104520
950	WRITE(6,230)	TR104530
	STOP	TR104540
1000	WRITE(6,240)	TR104550
	STOP	TR104560
100	FORMAT(14I5,2X,A8)	TR104570
110	FORMAT(6E12.5)	TR104580
200	FORMAT(1H0,* TAPTAB REQUIRES THAT L BE EQUAL TO 0 AND THAT N	TR104590
	+AND M BE BETWEEN 0 AND 15 --ALSO CHECK FOR INCORRECT NUMBER	TR104600
	+OF DATA CARDS *)	TR104610
201	FORMAT(1X,7A10,1X,A8)	TR104620
202	FORMAT(1H0)	TR104630
220	FORMAT(1H0,* TAPTAB IS ATTEMPTING TO READ MORE THAN 99 VALUES	TR104650
	1AT ONE TIME, THE DIMENSION OF THE TABLE ARRAY WILL HAVE TO	
	2BF INCREASED*)	
203	FORMAT(1P6F20.6)	TR104640
230	FORMAT(1H0,* TABLES EXCEED DIMENSIONED SIZE OF 3000 *)	TR104680
240	FORMAT(1H0,* PARITY ERROR OCCURRED DURING THE WRITING	TR104690
	+OF THE TABLES ONTO UNIT 9 *)	TR104700
	END	
	OVERLAY(TRAJ,1,0)	TR104720
	PROGRAM START	
C	7/2/74 JOHN E. HOLMES	TR104740
	COMMON Y(4940)	TR104750
	COMMON/TABL/TABLE(3000)	TR104760
	EQUIVALENCE(Y(2309),NOIN),(Y(2996),STAGE)	TR104770
	EQUIVALENCE(Y(2422),INNO(1)),(Y(2622),VALVE(1)),(Y(2996),KFND)	TR104780
	DIMENSION INNO(200),VALVE(200)	TR104790
	REWIND 9	TR104800
	DO 1001 I=1,NOTN	TR104810
	IN=INNO(I)	TR104820
	VAR=VALVE(I)	TR104830
	Y(IN)=VAR	TR104840
1001	CONTINUE	TR104850
	IF(STAGE.GT.0.0) GO TO 1005	TR104860
	LLEN=0	TR104870
	N=1	TR104880
	M=3000	TR104890
1003	BUFFER IN (9,1)(TABLE(N),TABLE(M))	TR104900
	IF(UNIT(9)) 10,12,11	TR104910
10	LFN=LENGTH(9)	TR104920
	LLEN=LEN+LLFN	TR104930
	IF(LLFN.EQ.3000) GO TO 12	TR104940
	N=LLEN+1	TR104950
	GO TO 1003	TR104960
11	WRITE(6,2000)	TR104970
2000	FORMAT(1H0,* PARITY ERROR OCCURRED WHILE ATTEMPTING TO	TR104980
	+READ TABLES FROM UNIT 9 *)	TR104990
	STOP	TR105000
12	CONTINUE	TR105010
	CALL OVERLAY(4HTRAJ,1,1,6HRECALL)	
1005	CALL OVERLAY(4HTRAJ,1,2,6HRECALL)	
	END	TR105080
	SUBROUTINE SFNCOS(A,SA,CA,KEY)	TR105090
	IF(KEY.NE.0) GO TO 10	TR105100
	AA=A/57.2957795	TR105110

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SA=SIN(AA)
CA=COS(AA)
RETURN
10 SA=SIN(A)
CA=COS(A)
RETURN
END
SUBROUTINE ARKTAN (A,H,C,MODE)
3 IF (A) 10,4,10
4 IF (R) 5,6,6
5 Z=3.14159265
GO TO 18
6 Z=0.
GO TO 21
10 IF (B) 13,11,17
11 Z=SIGN(1.5707963,A)
12 GO TO 18
13 Z=ATAN(A/B)+SIGN(3.14159265,A)
14 IF (Z-3.14159265) 16,15,16
15 Z=-Z
16 GO TO 18
17 Z=ATAN(A/B)
18 IF (MODE) 21,19,21
19 C=57.2957795*Z
20 GO TO 22
21 C=Z
22 IF (ABS(C)-1.F-07) 23,23,24
23 C=0.0
24 RETURN
END
SUBROUTINE MATINV(A,R,C)
DIMENSION A(9),R(9),C(9)
DELA=A(1)*A(5)*A(9)+A(2)*A(6)*A(7)+A(3)*A(8)*A(4)-A(7)*A(5)*A(3)-A(8)*A(6)*A(1)-A(9)*A(2)*A(4)
IF (DELA) 10,20,10
10 J=0
DO 11 I=1,7,3
B(I)=A(J+1)
B(I+1)=A(J+4)
B(I+2)=A(J+7)
11 J=J+1
C(1)=(R(5)*R(9)-R(6)*R(8))/DELA
C(2)=(R(6)*R(7)-R(4)*R(9))/DELA
C(3)=(R(4)*R(8)-R(5)*R(7))/DELA
C(4)=(R(3)*R(8)-R(2)*R(9))/DELA
C(5)=(R(1)*R(9)-R(3)*R(7))/DELA
C(6)=(R(2)*R(7)-R(1)*R(8))/DELA
C(7)=(R(2)*R(6)-R(3)*R(5))/DELA
C(8)=(R(3)*R(4)-R(1)*R(6))/DELA
C(9)=(R(1)*R(5)-R(2)*R(4))/DELA
RETURN
20 WRITE (6,6)
6 FORMAT(34H DETERMINANT OF A IS EQUAL TO ZERO)
RETURN
END
SUBROUTINE ARDCFT(H,PPZ,TTZ,RRZ,CCZ,GGZ)
DIMENSION T(12),A(10)
C**** ATMOS COMPUTES STANDARD PRESSURE, TEMPERATURE, AND DENSITY RATIOS
C**** FOR A GIVEN ALTITUDE H IN FEET.
X(Z,A,B,C)=A*ALOG(Z*(Z-R)+C)
Y(Z,A,B,C)=A*ATAN(Z*R-C)
DATA(A(I),I=1,10)/-3.350145769E-17,3.161762924E-14,-1.269919974E-11,2.848535349E-9,-3.930824139E-7,3.432295909E-5,-1.832962145E-3,15.256403630E-2,-5.232974573E-1,-3.955242007/
Z =0.000304R*H
TM=0.
TR105120
TR105130
TR105140
TR105150
TR105160
TR105170
TR105180
TR105190
TR105200
TR105210
TR105220
TR105230
TR105240
TR105250
TR105260
TR105270
TR105280
TR105290
TR105300
TR105310
TR105320
TR105330
TR105340
TR105350
TR105360
TR105370
TR105380
TR105390
TR105400
TR105410
TR105420
TR105430
TR105440
TR105450
TR105460
TR105470
TR105480
TR105490
TR105500
TR105510
TR105520
TR105530
TR105540
TR105550
TR105560
TR105570
TR105580
TR105590
TR105600
TR105610
TR105620
TR105630
TR105640
TR105650
TR105660
TR105670
TR105680
TR105690
TR105700
TR105710
TR105720
TR105730
TR105740
TR105750
TR105760
TR105770

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DO 5 I=1,10
5 TM=(TM+A(I))*Z
TM= TM+283.7492391
S1=Z+6356.77
T( 1)=-1.4655396E- 7/S1
T( 2)= 2.5653341E-11*ALOG(S1)
T( 3)= 1.4116834E- 4*ALOG( 14.002385+Z)
T( 4)=-3.8282910E- 5*ALOG(216.232250-Z)
T( 5)=X(Z, 1.5084978E-4, 26.414270 , 684.10967 )
T( 6)=Y(Z, 6.7419880E-4, 0.044294588, 0.5850046 )
T( 7)=X(Z, 8.5519675E-5,137.4745 ,10533.544 )
T( 8)=Y(Z, 4.9863416E-5, 0.013120767, 0.90188546)
T( 9)=X(Z,-2.5392354E-4,193.32352 ,10180.367 )
T(10)=Y(Z, 1.1921879E-3, 0.034567717, 3.3413764 )
T(11)=X(Z,-3.3888604E-5,384.32662 ,38131.516 )
T(12)=Y(Z, 8.9812379E-5, 0.02881021 , 5.5362654 )
TINTEG=0.2A016067E-02
DO 10 I=1,12
10 TINTEG=TINTEG+T(I)
QINTEG= -3483.6764*TINTEG
TTZ=TM/288.16
PPZ=EXP(QINTEG)
RRZ=PPZ/TTZ
CZ=SQRT(401.874*TM)/340.294
GGZ=(1./(1.+Z/6356.766))**2
RETURN
END
SUBROUTINE FRMRAN (TABLE,NUM,MFNC,U,A)
DIMENSION TABLE(1),U(1),A(1),T(1),TEMP(15),N(15),IDUM(1)
COMMON /TAR/T
EQUIVALENC (N(1),TEMP(1)),(IDUM(1),T(1))
NUMB = NUM
NINS=?
NSUM = 0
NNPROD = 1
DO 300 I=1,NUMB
TEMP(I) = TABLE(I)
NSUM = NSUM + N(I)
NNPROD = NNPROD * N(I)
300 CONTINUE
C
C *****
C
C TO FILL THE T ARRAY
C
NUMT = 2 * NUMB
JPOS = NUMB
DO 400 I=1,NUMB
C
C TO SPACE TO THE BEGINNING OF ARGUMENTS CORRESPONDING TO
C THE I-TH VARIABLE
C
JSTRT = JPOS + ?
JPOS = JPOS + N(I)
DO 410 J=JSTRT,JPOS
IF (TABLE(J).GT.U(I)) GO TO 420
410 CONTINUE
J=JPOS
420 IJ = NUMT + I
IDUM(IJ) = J - JSTRT +2
C
C T(I) THROUGH T(N) ARE THE ARGUMENTS CORRESPONDING TO THE N
C VARIABLES
C
T(I) = TABLE(J)
IJ = I + NUMB

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TR105780
TR105790
TR105800
TR105810
TR105820
TR105830
TR105840
TR105850
TR105860
TR105870
TR105880
TR105890
TR105900
TR105910
TR105920
TR105930
TR105940
TR105950
TR105960
TR105970
TR105980
TR105990
TR106000
TR106010
TR106020
TR106030
TR106040
TR106050
TR106060
TR106070
TR106080
TR106090
TR106100
TR106110
TR106120
TR106130
TR106140
TR106150
TR106160
TR106170
TR106180
TR106190
TR106200
TR106210
TR106220
TR106230
TR106240
TR106250
TR106260
TR106270
TR106280
TR106290
TR106300
TR106310
TR106320
TR106330
TR106340
TR106350
TR106360
TR106370
TR106380
TR106390
TR106400
TR106410
TR106420
TR106430

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C		TR106440
C	T(N+1) THROUGH T(2*N) ARE THE ARGUMENTS ONE POSITION BELOW THE	TR106450
C	ABOVE ARGUMENTS	TR106460
C		TR106470
	T(IJ) = TARLF(J-1)	TR106480
400	CONTINUE	TR106490
	ISTART = NUMT + 1	TR106500
	NUMTR=NUMT+NUMR	TR106510
	ISUM=IDUM(NUMTB)-1	TR106520
	IF (NUMB.EQ.1) GO TO 440	TR106530
	NJNS=NUMB+1	TR106540
	NTOP=NUMB-1	TR106550
	NPROD = 1	TR106560
	DO 430 I=1,NTOP	TR106570
	IJ=NUMTB-I	TR106580
	IIJ=NJNS-I	TR106590
	NPROD = NPROD * N(IIJ)	TR106600
	ISUM = ISUM + (IDUM(IJ)-2) * NPROD	TR106610
430	CONTINUE	TR106620
440	IIDUM = NUMB + ISUM + NSUM	TR106630
	DO 1000 M= 1,MFNC	TR106640
	IDUM(ISTART) = IIDUM	TR106650
	INDEX = 1	TR106660
	NPROD = 1	TR106670
C		TR106680
C	TO COMPUTE THE INDICES OF THE TABLE VALUES NEEDED FOR THE	TR106690
C	INTERPOLATION	TR106700
C		TR106710
	DO 500 I=1,NUMB	TR106720
	LNDEX = INDEX + NUMT	TR106730
	DO 510 J=1,INDEX	TR106740
	IJ = LNDEX + J	TR106750
	KJ = NUMT + J	TR106760
C		TR106770
C	THE IDUM ARRAY CONTAINS THE VALUES OF THE INDICES OF THE	TR106780
C	TABLE VALUES NEEDED FOR THE INTERPOLATION	TR106790
C		TR106800
	IDUM(IJ) = IDUM(KJ) + NPROD	TR106810
510	CONTINUE	TR106820
	IJ=NJNS-I	TR106830
	NPROD = NPROD * N(II)	TR106840
	INDEX = INDEX + INDEX	TR106850
500	CONTINUE	TR106860
C		TR106870
C	TO PUT THE TABLE VALUES NEEDED FOR THE INTERPOLATION IN THE	TR106880
C	T ARRAY STARTING WITH T(2*N+1)	TR106890
C		TR106900
	DO 600 I=ISTART,IJ	TR106910
	KJ = IDUM(I)	TR106920
	T(I) = TABLE(KJ)	TR106930
600	CONTINUE	TR106940
C		TR106950
C	*****	TR106960
C		TR106970
C	INTERPOLATION	TR106980
C		TR106990
	JFND = 2**NUMR + ISTART - 2	TR107000
	KJ = NUMB + 1	TR107010
	DO 700 I=1,NUMR	TR107020
	IJ = KJ - I	TR107030
	INDEX = NUMB + IJ	TR107040
	TEM = (U(IJ)-T(INDEX))/(T(IJ)-T(INDEX))	TR107050
	I.I = ISTART	TR107060
	DO 710 J=ISTART,JFND,2	TR107070
	T(IJ) = (T(J+1)-T(J))*TEM + T(J)	TR107080
	IJ = IJ + 1	TR107090

710	CONTINUE	TR107100
700	CONTINUE	TR107120
	JFND = (JEMD+JSTA+T)/2	TR107110
	A(M) = T(NIUMT+1)	TR107130
C		TR107140
C	TO SPACE TO THE BEGINNING OF THE NEXT FUNCTION TABULATED	TR107150
C		TR107160
	IIDUM = IIDUM + NNPROD	TR107170
1000	CONTINUE	TR107180
	RETURN	TR107190
	END	TR107200
	SUBROUTINE MATVEC(A,R,C,N)	TR107210
	DIMENSION A(9),R(9),C(9),F(9),G(9),H(9)	TR107220
	IF (N) 10,6,10	TR107230
10	GO TO (5,6,5,6,5),N	TR107240
6	DO 61 J=1,9	TR107250
61	F(J)=A(J)	TR107260
	GO TO 70	TR107270
5	M2=1	TR107280
	DO 36 K=1,3	TR107290
	K1=K+6	TR107300
	DO 36 J=K,K1,3	TR107310
	F(M2)=A(J)	TR107320
36	M2=M2+1	TR107330
70	IF (N-1) 71,71,72	TR107340
71	M4=1	TR107350
	DO 73 J=1,3	TR107360
73	G(J)=R(J)	TR107370
	GO TO 80	TR107380
72	M4=7	TR107390
	GO TO (74,74,74,75,75),N	TR107400
74	DO 76 J=1,9	TR107410
76	G(J)=R(J)	TR107420
	GO TO 80	TR107430
75	M2=1	TR107440
	DO 66 K=1,3	TR107450
	K1=K+6	TR107460
	DO 66 J=K,K1,3	TR107470
	G(M2)=R(J)	TR107480
66	M2=M2+1	TR107490
80	M2=1	TR107500
	DO 30 M1=1,M4,3	TR107510
	DO 30 K=1,3	TR107520
	K1=K+6	TR107530
	M3=M1	TR107540
	H(M2)=0.	TR107550
	DO 20 J=K,K1,3	TR107560
	H(M2)=H(M2)+F(J)*G(M3)	TR107570
20	M3=M3+1	TR107580
30	M2=M2+1	TR107590
	IF (N-1) 95,95,96	TR107600
95	M1=3	TR107610
	GO TO 90	TR107620
96	M1=9	TR107630
90	DO 91 J=1,M1	TR107640
91	C(J)=H(J)	TR107650
	RETURN	TR107660
	END	TR107670
	SUBROUTINE ITAB(NTAB,N,II,V)	TR107680
C	7/2/74 JOHN F. HOLMES	TR107690
	COMMON Y(4940)	TR107700
	COMMON/TAB/7(50)	TR107710
	COMMON/TABI/TABLE(3000)	TR107720
	EQUIVALENC(Y(4890),KTAB(1)),(Y(3051),K(1))	TR107730
	DIMENSION KTAB(49),U(3),K(49)	TR107740
	IN=KTAB(NTAB)	TR107750

```

KK=K(IN)
MFNC=1
CALL FRMRAN(TABLE(KK),N,MFNC,U,V)
RETURN
END
SUBROUTINE FNOL3(J,NN,G,L,MPR,XNF,X,Y,D,DERIV,TERM,OUTPUT)
COMMON YY(4940)
DIMENSION C(3),Y(31),YD(31),YP(31),YC(31),D(51),DM(31,4),DK(31,4)
*,ERROR(31),YK(31)
DATA EP6,EP11,M4/1.E-6,1.E-11,-4/
DATA (C(K),K=1,3)/2*.5,1./
DATA HMAX5/1.E35/
NHTS=0
FP2=0.
N=NN
J,I=J-2
H=G
HN=H
MK=1
NRET=M4
JTEST=1
IF (JJ .LT. 0) JTEST=4
IF (XNF.EQ. 0.) GO TO 15
FC=Y(N+3)
EUP=10.**(-XNF)
EL0=EUP*.001
FM=EL0*31.6227766
15 XD=X
XS=XD
DO 20 I=1,N
ERROR(I)=0.
20 YD(I)=Y(I)
CALL DERIV(X,Y,D)
CALL TERM(X,Y,D,F)
C PRINT
50 CALL OUTPUT(X,Y,D,ERROR,N,I,H)
*****
* NOTE CHANGE MADE TO ORIGINAL FNOL3 FOR MODIFY
IF(YY(2863).EQ.1.0) RETURN
*****
IF (NRET) 65,60,55
55 PRINT 3000, HN
3000 FORMAT(108#1EXECUTION TERMINATED BECAUSE INTERVAL OF INTEGRATION I
1ESS THAN 1.0F -6 TIMES INDEPENDENT VARIABLE (X). H =.1PE15.7)
STOP
60 RETURN
65 NPR=0
IF (MPR .LE. 0) PC=Y(N+1)
100 IF (JTEST .EQ. 5 .AND. H .NE. HN) GO TO 455
IF (JJ .GE. 0) H=HN
IF (MK .NE. 0 .OR. JJ .NE. 0) GO TO 300
C-----THE ADAMS MOULTON METHOD
200 HD24=H/24.
JAM=0
DO 210 I=1,N
YPI=(55.*DM(I,1)+37.*DM(I,2))-(59.*DM(I,3)+9.*DM(I,4))
YP(I)=YD(I)+HD24*YPI
Y(I)=YP(I)
210 CONTINUE
X=XD+H
CALL DERIV(X,Y,DM(1,4))
DO 220 I=1,N
YPI=(9.*DM(I,4)+19.*DM(I,1)+DM(I,2))-5.*DM(I,3)
YC(I)=YD(I)+HD24*YPI
ERROR(I)=(YP(I)-YC(I))/14.
C THIS ADDS IN A 2D CORRECTION

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TR107755
TR107760
TR107800
TR107810
TR107820
TR107830
TR107840
TR107850
TR107860
TR107870
TR107880
TR107890
TR107900
TR107910
TR107920
TR107930
TR107940
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TR107960
TR107970
TR107980
TR107990
TR108000
TR108010
TR108020
TR108030
TR108040
TR108050
TR108080
TR108090
TR108100
TR108110
TR108120
TR108130
TR108140
TR108150
TR108160
TR108170
TR108180
TR108190
TR108200
TR108210
TR108220
TR108230
TR108240
TR108250
TR108260
TR108270
TR108280
TR108290
TR108300
TR108310
TR108320
TR108330
TR108340
TR108350
TR108360
TR108370
TR108380
TR108390
TR108400

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YC(I)=YC(I)+ERROR(I)	TR108410
220 CONTINUE	TR108420
IF (XNE.NE..0) GO TO 700	TR108430
GO TO 455	TR108440
C-----THE RUNGE KUTTA METHOD	TR108450
300 GO TO (301,309,308,309,303),JTFST	TR108460
301 DO 302 I=1,N	TR108470
YK(I)=YD(I)	TR108480
302 CONTINUE	TR108490
XDS=XD	TR108500
GO TO 309	TR108510
303 DO 304 I=1,N	TR108520
YK(I)=YC(I)	TR108530
304 CONTINUE	TR108540
XDS=XD+H	TR108550
308 HS=H	TR108560
H=2.*H	TR108570
GO TO 320	TR108580
309 X=XD	TR108590
JAM=1	TR108600
DO 310 I=1,N	TR108610
Y(I)=YD(I)	TR108620
DK(I,1)=D(I)	TR108630
310 CONTINUE	TR108640
IF (JTFST .LE. 2) CALL DERIV(X,Y,DK)	TR108650
IF (MK .GT. 1 .OR. JTEST .GT. 1) GO TO 320	TR108660
DO 315 I=1,N	TR108670
DM(I,4)=DK(I,1)	TR108680
315 CONTINUE	TR108690
320 DO 335 K=2,4	TR108700
HC=H*C(K-1)	TR108710
DO 330 I=1,N	TR108720
Y(I)=YD(I) + HC*DK(I,K-1)	TR108730
330 CONTINUE	TR108740
X=XD+HC	TR108750
CALL DERIV(X,Y,DK(1,K))	TR108760
335 CONTINUE	TR108770
HD6=H/6.	TR108780
DO 340 I=1,N	TR108790
YPI=DK(I,1)+DK(I,4)+2.*(DK(I,2)+DK(I,3))	TR108800
YC(I)=YD(I)+HD6*YPI	TR108810
340 CONTINUE	TR108820
GO TO (360,390,370,455,370),JTEST	TR108830
360 DO 365 I=1,N	TR108910
YP(I)=YC(I)	TR108920
365 CONTINUE	TR108930
JTEST=3	TR108940
GO TO 308	TR108950
370 DO 380 I=1,N	TR108960
YD(I)=YP(I)	TR108970
YP(I)=YC(I)	TR108980
380 CONTINUE	TR108990
H=HS	TR109000
XD=XD+H	TR109010
JTEST=2	TR109020
IF (MK .EQ. 1) GO TO 309	TR109030
GO TO 451	TR109040
390 DO 400 I=1,N	TR109050
ERROR(I)=(YC(I)-YP(I))/15.	TR109060
YC(I)=YC(I)+ERROR(I)	TR109070
YP(I)=YC(I)	TR109080
400 CONTINUE	TR109090
JTEST=5	TR109100
IF (XNE.NE..0) GO TO 700	TR109110
C-----ACCEPT THE STEP SIZE	TR109120
450 IF (JAM .EQ. 0) GO TO 455	TR109130

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IF (MK .EQ. 3 .AND. JJ .EQ. 0) GO TO 455	TR109140
IF (MK .NE. 1) GO TO 303	TR109150
IF (JTEST .EQ. 1) GO TO 455	TR109160
451 DO 452 I=1,N	TR109170
Y(I)=YD(I)	TR109180
452 CONTINUE	TR109190
GO TO 466	TR109200
455 DO 459 NQ=1,N	TR109210
YD(NQ)=YC(NQ)	TR109220
Y(NQ)=YD(NQ)	TR109230
459 CONTINUE	TR109240
IF (JJ .GE. 0) JTFST=1	TR109250
IF (MK .NE. 0 .OR. JJ .NE. 0 .OR. NRET .NE. M4) GO TO 465	TR109260
DO 460 I=1,N	TR109270
DM(I,4)=DM(I,2)	TR109280
DM(I,2)=DM(I,3)	TR109290
DM(I,3)=DM(I,1)	TR109300
460 CONTINUE	TR109310
465 XD=XD+H	TR109320
466 X=XD	TR109330
IF (MK .EQ. 3) MK=0	TR109340
CALL DERIV(X,Y,D)	TR109350
DO 470 I=1,N	TR109360
DM(I,MK+1)=D(I)	TR109370
470 CONTINUE	TR109380
480 FP=F	TR109390
CALL TERM (X,Y,D,F)	TR109400
C-----DO YOU TERMINATE	TR109410
500 IF (ABS(F) .LE. EP6) GO TO 800	TR109420
IF (FP .EQ. 0.) GO TO 510	TR109430
IF (NRET .NE. M4 .OR. F*FP .LT. FP11) GO TO 805	TR109440
510 XS=XD	TR109450
IF (MK .NE. 0 .AND. H .EQ. HN) MK=MK+1	TR109460
C-----DO YOU PRINT	TR109470
600 NPR=NPR+1	TR109480
IF (MPR .EQ. 0) GO TO 610	TR109490
IF (NPR .GE. MPR) GO TO 50	TR109750
GO TO 100	TR109760
610 IF (ABS(Y(N+1)-PC) .GE. Y(N+2)) GO TO 50	TR109770
GO TO 100	TR109780
C-----DETERMINING THE STEP SIZE	TR109790
700 HR = HMAX5	TR109800
DO 760 I = 1,N	TR109810
Z=ABS(ERROR(I))	TR10 820
IF(YC(I).EQ.0.) GO TO 720	TR109825
ZZ=YC(I)	TR109830
ZZ=ABS(ZZ)	TR109840
IF (EC) 720,710,705	TR109850
705 IF (EC .GT. ZZ) ZZ=EC	TR109860
710 Z=Z/ZZ	TR109870
720 IF (Z.GT.EL0.AND.Z.LT.EMP) GOTO 750	TR109880
HR = AMIN1(HR,EM/(Z+EP11))	TR109890
GOTO760	TR109900
750 HR=AMIN1(HR,1.)	
760 CONTINUE	TR109920
IF(HB.NE.1.) GO TO 765	TR110130
NHTS=0	TR110140
GO TO 450	TR110150
765 HN=H*HR**.2	TR110160
IF (MK .NE. 1) JTFST=1	TR110180
MK=1	TR110190
IF (HR.LT.1.) GOTO 770	TR110200
IF (ABS(HN) .GT. ABS(4.*H)) HN=4.*H	TR110210
NHTS=0	TR110220
GOTO 450	TR110230
770 HEPS=ABS(X*EP6) + FP11	TR110240

IF (ABS(HN) .LT. ABS(H/4.)) HN=H/4.	TR110250
IF (ARS(HN) .GT. HEPS) GO TO 790	TR110260
NHTS = NHTS + 1	TR110270
IF (NHTS .LE. 10) GO TO 780	TR110280
NRET = 1	TR110290
GO TO 450	TR110300
780 HN=SIGN(HEPS*HN)	TR110310
IF (NHTS .GT. 1) GO TO 450	TR110320
790 IF (NHTS .GT. 1) NHTS=0	TR110330
IF (JAM .EQ. 0) GO TO 100	TR110340
DO 795 I=1,N	TR110350
YD(I)=YK(I)	TR110360
795 CONTINUE	TR110370
XD=XDS	TR110380
JTEST=1	TR110390
GO TO 100	TR110400
C-----THE TERMINATION LOOP	TR110410
800 NRET=0	TR110420
805 IF (NRET .LT. 0) GO TO 806	TR110430
H=XD-XS	TR110440
GO TO 50	TR110450
806 IF (F*FP.LT.0.) GOTO 810	TR110460
IF (F*FP2.LT.0.) GOTO 820	TR110470
GO TO 800	TR110480
810 FP2 =FP	TR110490
HP =H	TR110500
GOTO 830	TR110510
820 FP =FP2	TR110520
HP =H + HP	TR110530
830 NRET=NRET+1	TR110540
H=HP*F/(FP-F)	TR110550
JTEST=4	TR110560
GOTO 300	TR110570
END	TR110580
RFAL FUNCTION KLMT(EI,L,K)	
C	
C THIS IS USED FOR MODELING A RATE GYRO OR ANY OTHER PROPORTIONAL.	
C LIMITED OUTPUT DEVICE	
C	
C FI = THE INPUT	
C L = THE LIMIT ON THE OUTPUT	
C K = THE GAIN OF THE DEVICE	
C	
RFAL L,K	
KLMT=K*EI	
IF (ARS(KLMT).GE.L) KLMT=SIGN(L,KLMT)	
END	

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*DECK TR2	
C *****	TR200010
C 03/13/75 12.56.47 JOHN HOLMES	TR200012
C *****	TR200014
OVERLAY(TRAJ,1,1)	TR200100
PROGRAM SETUP	TR200110
C 8/2/77 JOHN E. HOLMES	
COMMON Y(4940)	TR200130
EQUIVALENC (Y(2307),NOMOD), (Y(2312),NMOD(1))	TR200140
DIMENSION NMOD(20)	TR200150
DO 1000 I=1,NOMOD	TR200160
L=NMOD(I)	TR200170
GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20),L	TR200180
1 CALL IMOD1	TR200190
GO TO 1000	TR200200
2 CALL IMOD2	TR200210
GO TO 1000	TR200220
3 CALL IMOD3	TR200230
GO TO 1000	TR200240
4 CALL IMOD4	TR200250
GO TO 1000	TR200260
5 CALL IMOD5	TR200270
GO TO 1000	TR200280
6 CALL IMOD6	TR200290
GO TO 1000	TR200300
7 CALL IMOD7	TR200310
GO TO 1000	TR200320
8 CALL IMOD8	TR200330
GO TO 1000	TR200340
9 CALL IMOD9	TR200350
GO TO 1000	TR200360
10 CALL IMOD10	TR200370
GO TO 1000	TR200380
11 CALL IMOD11	TR200390
GO TO 1000	TR200400
12 CALL IMOD12	TR200410
GO TO 1000	TR200420
13 CALL IMOD13	TR200430
GO TO 1000	TR200440
14 CALL IMOD14	TR200450
GO TO 1000	TR200460
15 CALL IMOD15	TR200470
GO TO 1000	TR200480
16 CALL IMOD16	TR200490
GO TO 1000	TR200500
17 CALL IMOD17	TR200510
GO TO 1000	TR200520
18 CALL IMOD18	TR200530
GO TO 1000	TR200540
19 CALL IMOD19	TR200550
GO TO 1000	TR200560
20 CALL IMOD20	TR200570
1000 CONTINUE	TR200580
END	TR200590
	TR200600
	TR200610
SUBROUTINE IMOD1	TR200620
RETURN	TR200630
END	TR200640
	TR200650
	TR200660
SUBROUTINE IMOD2	TR200670

RETURN	TR200680
END	TR200690
	TR200700
	TR200710
SUBROUTINE IMOD3	TR200720
RETURN	TR200730
END	TR200740
	TR200750
	TR200760
SUBROUTINE IMOD4	TR200770
RFTURN	TR200780
END	TR200790
	TR200800
	TR200810
SUBROUTINE IMOD5	TR200820
RFTURN	TR200830
END	TR200840
	TR200850
	TR200860
SUBROUTINE IMOD6	TR200870
RETURN	TR200880
END	TR200890
	TR200900
	TR200910
SUBROUTINE IMOD7	TR200920
RFTURN	TR200930
END	TR200940
	TR200950
	TR200960
SUBROUTINE IMOD8	TR200970
RETURN	TR200980
END	TR200990
	TR201000
	TR201010
SUBROUTINE IMOD9	TR201020
RFTURN	TR201030
END	TR201040
	TR201050
	TR201060
SUBROUTINE IMOD10	TR201070
RFTURN	TR201080
END	TR201090
	TR201100
	TR201110
SUBROUTINE IMOD11	TR201120
RFTURN	TR201130
END	TR201140
	TR201150
	TR201160
SUBROUTINE IMOD12	TR201170
RFTURN	TR201180
END	TR201190
	TR201200
	TR201210
SUBROUTINE IMOD13	TR201220
RFTURN	TR201230
END	TR201240
	TR201250
	TR201260
SUBROUTINE IMOD14	TR201270
RETURN	TR201280
END	TR201290
	TR201300
	TR201310
SUBROUTINE IMOD15	TR201320
RETURN	TR201330

END	TR201340
	TR201350
SUBROUTINE IMOD16	TR201360
RETURN	TR201370
END	TR201380
	TR201390
	TR201400
	TR201410
SUBROUTINE IMOD17	TR201420
RETURN	TR201430
END	TR201440
	TR201450
	TR201460
	TR201470
SUBROUTINE IMOD18	TR201480
RETURN	TR201490
END	TR201500
	TR201510
	TR201520
SUBROUTINE IMOD19	TR201530
RETURN	TR201540
END	TR201550
	TR201560
	TR201570
	TR201580
	TR201590
	TR201600
	TR201610
OVERLAY(TRAJ,1,2)	TR201620
PROGRAM INTGRT	TR201630
C 7/2/74 JOHN E. HOLMFS	TR201640
COMMON Y(4940)	TR201650
INTEGER CVAR(31),DVAR(31)	TR201660
EQUIVALENCE(Y(2300),G),(Y(2301),XNE)	TR201670
EQUIVALENCE(Y(2999),T)	TR201680
EQUIVALENCE(Y(2306),ERROR),(Y(2903),CVAR(1)),(Y(2934),LOCD(1))	TR201690
EQUIVALENCE(Y(2965),DVAR(1)),(Y(2872),LOCC(1)),(Y(2870),NODER)	TR201700
EQUIVALENCE(Y(2869),NOVAR)	TR201710
EQUIVALENCE(Y(2862),TI),(Y(2996),STAGE)	TR201720
EQUIVALENCE(Y(2868),DELT)	TR201730
DIMENSION LOCC(31),LOCD(31)	TR201740
DIMENSION C(31),D(31)	TR201750
EXTERNAL DERIV,TERM,OUT	TR201760
DO 10 I=1,31	TR201770
C(I)=0.0	TR201780
10 D(I)=0.0	TR201790
DO 2000 I=1,NOVAR	TR201800
JJ=LOCC(I)	TR201810
JK=CVAR(I)	TR201820
C(JJ)=Y(JK)	TR201830
2000 CONTINUE	TR201840
DO 3000 I=1,NODER	TR201850
JJ=LOCD(I)	TR201860
JK=DVAR(I)	TR201870
D(JJ)=Y(JK)	TR201880
3000 CONTINUE	TR201890
IF(STAGE.GT.0.0) TI=T	
T=TI	TR201900
C(NOVAR+2)=Y(2997)	TR201930
C(NOVAR+3)=ERROR	TR201940
NN=NOVAR	TR201950
DFLT=G	TR201960
J=IFIX(Y(2302))	TR201970
L=IFIX(Y(2304))	TR201980
MPR=IFIX(Y(2305))	TR201990
400 CALL FNOL3(J,NN,G,L,MPR,XNF,T,C,D,DERIV,TERM,OUT)	TR202000

END		TR202010
		TR202020
		TR202030
		TR202040
C	SUBROUTINE DERIV(T,C,D)	TR202050
	7/2/74 JOHN E. HOLMES	TR202060
	COMMON Y(4940)	TR202070
	INTEGER CVAR(31),DVAR(31)	TR202080
	EQUIVALENC(Y(2307),NOMOD),(Y(2312),NMOD(1))	TR202090
	EQUIVALENC(Y(2903),CVAR(1)),(Y(2934),LOCD(1))	TR202100
	EQUIVALENC(Y(2965),DVAR(1)),(Y(2872),LOCC(1)),(Y(2870),NODER)	TR202110
	EQUIVALENC(Y(2869),NOVAR)	TR202120
	DIMENSION LOCC(31),LOCD(31)	TR202130
	DIMENSION C(31),D(31),NMOD(20)	TR202140
	DO 2000 I=1,NOVAR	TR202150
	JJ=LOCC(I)	TR202160
	JK=CVAR(I)	TR202170
	Y(JK)=C(JJ)	TR202180
2000	CONTINUE	TR202190
	DO 1000 I=1,NOMOD	TR202200
	L=NMOD(I)	TR202210
	GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20),L	TR202220
1	CALL MOD1	TR202230
	GO TO 1000	TR202240
2	CALL MOD2	TR202250
	GO TO 1000	TR202260
3	CALL MOD3	TR202270
	GO TO 1000	TR202280
4	CALL MOD4	TR202290
	GO TO 1000	TR202300
5	CALL MOD5	TR202310
	GO TO 1000	TR202320
6	CALL MOD6	TR202330
	GO TO 1000	TR202340
7	CALL MOD7	TR202350
	GO TO 1000	TR202360
8	CALL MOD8	TR202370
	GO TO 1000	TR202380
9	CALL MOD9	TR202390
	GO TO 1000	TR202400
10	CALL MOD10	TR202410
	GO TO 1000	TR202420
11	CALL MOD11	TR202430
	GO TO 1000	TR202440
12	CALL MOD12	TR202450
	GO TO 1000	TR202460
13	CALL MOD13	TR202470
	GO TO 1000	TR202480
14	CALL MOD14	TR202490
	GO TO 1000	TR202500
15	CALL MOD15	TR202510
	GO TO 1000	TR202520
16	CALL MOD16	TR202530
	GO TO 1000	TR202540
17	CALL MOD17	TR202550
	GO TO 1000	TR202560
18	CALL MOD18	TR202570
	GO TO 1000	TR202580
19	CALL MOD19	TR202590
	GO TO 1000	TR202600
20	CALL MOD20	TR202610
1000	CONTINUE	TR202620
	DO 4500 I=1,NODER	TR202630
	JJ=LOCD(I)	TR202640
	JK=DVAR(I)	TR202650
	D(JJ)=Y(JK)	TR202660
4500	CONTINUE	

RETURN		TR202670
END		TR202680
		TR202690
		TR202700
		TR202710
C	SUBROUTINE OUT(T,C,D,ERROR,DMY,DNYX,DELT)	TR202720
	7/2/74 JOHN E. HOLMFS	TR202730
	COMMON Y(4940)	TR202740
	INTEGER CVAR(31),DVAR(31),PLOT(10),OUTNO(30)	TR202745
	INTEGER PLCT	TR202750
	EQUIVALENC(Y(2862),TI),(Y(2863),STOP),(Y(2864),TS)	
	EQUIVALENC(Y(2866),RUNN),(Y(2867),DATE)	
	EQUIVALENC(Y(2308),NOOUT),(Y(2332),NA1(1)),	TR202770
	(Y(2392),OUTNO(1))	TR202780
	EQUIVALENC(Y(2311),NOPLOT),(Y(2852),PLOT(1))	TR202790
	EQUIVALENC(Y(2903),CVAR(1)),(Y(2934),LOCD(1))	TR202800
	EQUIVALENC(Y(2965),DVAR(1)),(Y(2872),LOCC(1)),(Y(2870),NODER)	TR202810
	EQUIVALENC(Y(3044),TITL(1))	TR202820
	EQUIVALENC(Y(2869),NOVAR)	TR202830
	EQUIVALENC(Y(3043),PLCT),(Y(2362),HD1(1)),(Y(2377),HD2(1))	TR202835
	DIMENSION LOCC(31),LOCD(31)	TR202840
	DIMENSION TITL(7),HD1(15),HD2(15),FOR1(31),FOR2(31)	TR202850
	DIMENSION NA1(30),C(31),D(31)	TR202860
	REAL PL(10)	TR202870
1	FORMAT(3X,4HRUN ,F12.2,10X,7A10,6X,7HFORMAT ,I1)	TR202880
2	FORMAT(3X,F12.2,92X,5HPAGE ,I3)	TR202890
4	FORMAT(1H1)	TR202910
5	FORMAT(1H0,2X,5HTIME ,15A8/)	TR202920
**	K7 = NO. LINES STORED FOR CURRENT PAGE	
**	NUM = NO. FORMATS	
**	NP = NO. PAGES OF EACH FORMAT	
**	J,J2 = SUBSCRIPTS FOR OUTPUT ARRAYS	
	DO 3000 I=1,NODER	TR202940
	JJ=LOCD(I)	TR202950
	JK=DVAR(I)	TR202960
	Y(JK)=D(JJ)	TR202970
3000	CONTINUE	TR202980
	DO 2000 I=1,NOVAR	TR202990
	JJ=LOCC(I)	TR203000
	JK=CVAR(I)	TR203010
	Y(JK)=C(JJ)	TR203020
2000	CONTINUE	TR203030
	Y(2868)=DELT	TR203040
	Y(2999)=T	TR203060
	IF(T-TI) 105,100,105	TR203080
100	CONTINUE	
	NP=0	TR203100
	K7=0	TR203110
	J2=0	
	J=0	TR203120
105	CALL PROCESS	
***	STORE OUTPUT IN Y(3100+) ARRAY UNTIL FULL PAGE IS ACCUMULATED	
115	KZ=KZ+1	
200	J=J+1	
	J2=J2+1	
	Y(J+3100)=T	
	Y(J2+3980)=T	
	DO 330 I=1,NOOUT	
	IN=OUTNO(I)	
	IF(I.LE.15) J=J+1	
	IF(I.LE.15) Y(J+3100)=Y(IN)	
	IF(I.GT.15) J2=J2+1	
	IF(I.GT.15) Y(J2+3980)=Y(IN)	
330	CONTINUE	
599	IF(NOPLOT.EQ.0) GO TO 331	
	DO 600 I=1,NOPLOT	
	II=PLOT(I)	

```

600 PL(I)=Y(II)
    PLCT=PLCT+1
    WRITE(19) RUNN,T,(PL(I),I=1,NOPL0T)
331 IF(STOP) 332,332,15
332 IF(KZ.LT.51) GO TO 333
*** WRITE PAGE OF OUTPUT IN EACH FORMAT..ARRAYS DIMENSIONED FOR 55 LINES
15 NP=NP+1
    IF(NP.GT.1) GO TO 22
    NUM=(14+NOOUT)/15
    FOR1(1)=9H(1X,F7.2,
    FOR2(1)=9H(1X,F7.2,
    DO 19 N=1,15
    I=2*N
    FOR1(I)=HD1(N)
    FOR1(I+1)=1H,
    IF(NOOUT.GF.N) GO TO 18
    FOR1(I)=10H
    FOR1(I+1)=1H
18 FOR2(I)=HD2(N)
    FOR2(I+1)=1H,
    IF((NOOUT-15).GE.N) GO TO 19
    FOR2(I)=10H
    FOR2(I+1)=1H
19 CONTINUE
    IF(NOOUT.GF.15) FOR1(31)=1H)
    IF(NOOUT.LT.15) FOR1(NOOUT*2+1)=1H)
    IF(NOOUT.LF.15) FOR2(1)=9H(1X)
    IF(NOOUT.GT.15) FOR2((NOOUT-15)*2+1)=1H)
22 DO 30 L=1,NUM
    WRITE(6,1) RUNN,(TITL(I),I=1,7),L
    WRITE(6,2) DATE,NP
    IF(L.GT.1) GO TO 21
20 WRITE(6,5) (NA1(I),I=1,15)
    M=J+3100
    WRITE(6,F0R1) (Y(I),I=3101,M)
    GO TO 26
21 WRITE(6,5) (NA1(I),I=16,30)
    M=J2+3980
    WRITE(6,F0R2) (Y(I),I=3981,M)
26 WRITE(6,4)
30 CONTINUE
    J=0
    J2=0
    KZ=0
    GO TO 333
333 RETURN
    FND

SUBROUTINE TERM(T,C,D,F)
C 7/2/74 JOHN E. HOLMES
COMMON Y(4940)
INTEGER CVAR(31),DVAR(31),STPNO(10)
EQUIVALENC (Y(2862),T1)
EQUIVALENC (Y(2863),STOP)
EQUIVALENC (Y(2310),NOSTOP),(Y(2822),STPNO(1)),(Y(2832),SUP(1)),
+(Y(2842),SLO(1))
EQUIVALENC (Y(2903),CVAR(1)),(Y(2934),LOCD(1)),(Y(2869),NOVAR)
EQUIVALENC (Y(2965),DVAR(1)),(Y(2872),LOCC(1)),(Y(2870),NGNER)
EQUIVALENC (Y(2009),LRP(1))
DIMENSION LOCC(31),LOCD(31)
DIMENSION SUP(10),SLO(10),C(31),D(31),H(9),RPT(9),RPI(9)
REAL LRP(9)
Y(2999)=T
7 F=1.0
DELA=LRP(1)*LRP(5)*LRP(9)+LRP(2)*LRP(6)*LRP(7)+LRP(3)*

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+LRP(8)*LRP(4)-LRP(7)*LRP(5)*LRP(3)-LRP(8)*LRP(6)*LRP(1)-
+LRP(9)*LRP(2)*LRP(4)
IF(DELA) 50,60,50
50 CONTINUE
C****TO INSURE ORTHOGONALITY OF LRP MATRIX *****
DO 9 I=1,3
CALL MATINV(LRP,RPT,R)
CALL MATINV(RPT,R,RPI)
DO 8 J=1,9
8 LRP(J)=(LRP(J)+RPT(J))/2.
9 CONTINUE
60 CONTINUE
DO 15 I=1,NODER
JJ=LOCD(I)
JK=DVAR(I)
Y(JK)=D(JJ)
15 CONTINUE
DO 10 I=1,NOVAR
JJ=LOCC(I)
JK=CVAR(I)
Y(JK)=C(JJ)
10 CONTINUE
IPRVA=IFIX(Y(2998))
C(NOVAR+1)=Y(IPRVA)
SGN=1.
DO 20 I=1,NOSTOP
IN=STPNO(I)
HALF=ABS(SUP(I)-SLO(I))/2.
SMID=(SUP(I)+SLO(I))/2.
FF=HALF-ABS(Y(IN)-SMID)
IF(FF.LT.0.) SGN=-1.
IF(FF.LE.0.) STOP=1.
F=F*ARS(FF)
20 CONTINUE
F=F*SGN
32 RETURN
END

SUBROUTINE MOD1
RETURN
END

SUBROUTINE MOD2
RETURN
END

SUBROUTINE MOD3
RETURN
END

SUBROUTINE MOD4
RETURN
END

SUBROUTINE MOD5
RETURN
END

SUBROUTINE MOD6
RETURN
END

```

TR204300
TR204310
TR204320
TR204330
TR204340
TR204350
TR204360
TR204370
TR204380
TR204390
TR204400
TR204410
TR204420
TR204430
TR204440
TR204450
TR204460
TR204470
TR204480
TR204490
TR204500
TR204510

TR204520
TR204530

TR204590
TR204600
TR204610
TR204620
TR204630
TR204640
TR204650
TR204660
TR204670
TR204680
TR204690
TR204700
TR204710
TR204720
TR204730
TR204740
TR204750
TR204760
TR204770
TR204780
TR204790
TR204800
TR204810
TR204820
TR204830
TR204840
TR204850
TR204860
TR204870
TR204880
TR204890

END	TR204900
	TR204910
	TR204920
SUBROUTINE MOD7	TR204930
RETURN	TR204940
END	TR204950
	TR204960
	TR204970
	TR204980
SUBROUTINE MOD8	TR204990
RRETURN	TR205000
END	TR205010
	TR205020
	TR205030
SUBROUTINE MOD9	TR205040
RETURN	TR205050
END	TR205060
	TR205070
	TR205080
SUBROUTINE MOD10	TR205090
RETURN	TR205100
END	TR205110
	TR205120
	TR205130
SUBROUTINE MOD11	TR205140
RETURN	TR205150
END	TR205160
	TR205170
	TR205180
SUBROUTINE MOD12	TR205190
RRETURN	TR205200
END	TR205210
	TR205220
	TR205230
SUBROUTINE MOD13	TR205240
RETURN	TR205250
END	TR205260
	TR205270
	TR205280
SUBROUTINE MOD14	TR205290
RETURN	TR205300
END	TR205310
	TR205320
	TR205330
SUBROUTINE MOD15	TR205340
RRETURN	TR205350
END	TR205360
	TR205370
	TR205380
SUBROUTINE MOD16	TR205390
RETURN	TR205400
END	TR205410
	TR205420
	TR205430
SUBROUTINE MOD17	TR205440
RETURN	TR205450
END	TR205460
	TR205470
	TR205480
SUBROUTINE MOD18	TR205490
RETURN	TR205500
END	TR205510
	TR205520
	TR205530
SUBROUTINE MOD19	TR205540
RETURN	TR205550
END	

	SUBROUTINE MOD20	TR205560
	RETURN	TR205570
	END	TR205580
		TR205590
		TR205600
		TR205610
		TR205620
	SUBROUTINE PROCESS	TR205630
	RETURN	TR205640
	END	TR205650
		TR205660
	OVERLAY(TRAJ,2,0)	TR205670
	PROGRAM TRJPLTS	TR205680
C	7/2/74 JOHN F. HOLMES	TR205690
	COMMON Y(4940)	TR205700
	CALL MYPLOT	TR205710
	FND	TR205720
	SUBROUTINE MYPLOT	TR205730
C	11/13/74 JOHN F. HOLMES	TR205740
	COMMON Y(4940)	TR205750
	INTEGER PLOT(10),PLCT	TR205760
	EQUIVALENC(Y(2311),NOPLT),(Y(2852),PIOT(1))	TR205770
	EQUIVALENC(Y(3043),PLCT)	TR205775
	RFAL PL(10)	TR205780
	RFWIND 19	TR205785
C		TR205790
C	THE INFORMATION TO BE PLOTTED SHOULD BE READ AS FOLLOWS.	TR205800
C		TR205810
C	DO 20 J=1,PLCT	TR205815
C	READ(19) RUNN,T,(PL(I),I=1,NOPLT)	TR205820
C	20 CONTINUE	TR205825
C	20 CONTINUE	TR205830
C	PLCT ARE THE NUMBER OF DATA POINTS TO BE PLOTTED	TR205835
C	SUPPLY YOUR OWN GOULD CALLS	TR205840
C		TR205850
	RETURN	TR205860
	FND	TR205870

APPENDIX B

FIXED STORAGE ASSIGNMENTS

Y ARRAY LOCATIONS 2300 - 4940

NOTE:

An asterisk after the Y array location of the parameter indicates that the parameter is to be placed in the data as an input parameter.

<u>PARAMETER</u>	<u>IDENTIFICATION</u>	<u>LOCATION IN Y ARRAY</u>
G		2300 *
XNE	INTEGRATION	2301 *
J	CONTROLS	2302 *
NN	SEE PAGE	2303 *
L		2304
MPR		2305 *
ERROR		2306 *
NOMOD	Number of modules	2307
NOOUT	Number of output parameters	2308
NOIN	Number of code 3 parameters	2309
NOSTOP	Number of STOP conditions	2310
NO PLOT	Number of plot variables	2311
NMOD(1)		2312
↓	MOD controls, see subroutine INPUT	↓
NMOD(20)		2331
RNME1(1)		2332
↓	Header controls, see subroutine INPUT	↓
RNME1(30)		2361
HD1(1)		2362
↓		↓
HD1(15)	Header controls, see subroutine INPUT	2376
HD2(1)		2377
↓		↓
HD2(15)		2391
OUTND(1)		2392
↓	Output controls, see sub- routine INPUT	↓
OUTNO(30)		2421
INNO(1)		2422
↓	Input controls, see sub- routine INPUT	↓
INNO(200)		2621
VALVE(1)		2622
↓	Input controls, see sub- routine INPUT	↓
VALVE(200)		2821
STPNO(1)		2822
↓	Stop (termination) controls, see subroutine INPUT	↓
STPNO(10)		2831
SUP(1)		2832
↓	Upper bound termination locations	↓
SUP(10)		2841
SLO(1)	Lower bound termination locations	2842
↓		↓
SLO(10)		2851

<u>PARAMETER</u>	<u>IDENTIFICATION</u>	<u>LOCATION IN Y ARRAY</u>
PLOT(1)	Plot variable locations	2852
↓		↓
PLOT(10)		2861
TI	Initial time	2862 *
STOP	Termination parameters	2863
TS		2864
PRFR	Print control, see	2865 *
RUNN	RUN Number	2866 *
DATE	Date	2867 *
DELT	Integration time step (see)	2868
NOVAR	Number of dependent variables	2869
NODER	Number of derivatives	2870
NOTAB	Number of tables	2871
LOCC(1)		2872
↓	Locations of dependent variables	↓
LOCC(31)	in C array	2902
CVAR(1)	Y array locations of	2903
↓	dependent variables	↓
CVAR(31)		2933
LOCD(1)	Locations of derivatives	2934
↓	in D array	↓
LOCD(31)		2964
DVAR(1)	Y array locations of	2965
↓	derivatives	↓
DVAR(31)		2995
KEND	Size of table array	2996
--	Print increment when MPR=0	2997 *
PRVA	Print variable when MPR=0	2998 *
T	Time (sec)	2999 *
RE	Earth's radius, default value is 20925631 ft	3000 *
WE	Earth's spin rate, default value is $7.29211508 \times 10^{-5}$ rad/sec	3001 *
		3002
		3003
D	Aerodynamic reference length (ft)	3004 *
A	Aerodynamic reference area (ft ²)	3005 *
DXG		3006 *
DYG	Center of gravity location w/r to geometric axes, see Figure 7	3007 *
DZG		3008 *
IXX		3009 *
IYY	Principal moments of inertia (slug-ft ²)	3010 *
IZZ		3011 *
MS	Vehicle mass (slug)	3012 *
H	Vehicle altitude (ft)	3013 *
TAUR	Longitude (deg)	3014 *
PSIR	Latitude (deg)	3015 *
I _{XY}		3016 *
I _{XZ}	Cross products of inertia	3017 *
I _{YZ}		3018 *

<u>PARAMETER</u>	<u>IDENTIFICATION</u>	<u>LOCATION IN Y ARRAY</u>
		3019
		3020
		3021
		3022
		3023
		3024
		3025
		3026
		3027
		3028
		3029
		3030
		3031
		3032
		3033
		3034
		3035
		3036
		3037
		3038
		3039
		3040
		3041
		3042
PLCT	Number of data points being plotted	3043
TITL(1)	Storage location for title	3044
↓		↓
TITL(7)	Intermediate table identification; see subroutine ITAB	3050
K(1)		3051
↓		↓
K(49)	Output array storage	3099
--		3100
↓		↓
--	Assigned array locations for tabulated functions	4889
KTAB(1)		4890
↓		↓
KTAB(49)		4938
		4939
		4940

APPENDIX C

IMOD1; INITIAL DIRECTION COSINE MATRIX FOR
3DOF OVER A ROTATING SPHERICAL EARTH

As mentioned previously, MOD1 contains the direction cosine matrix. Since it would be unwieldy to read in the initial values of the direction cosine matrix, IMOD1 is used to calculate these values from the initial latitude and longitude which must be read from the input cards. This transform matrix for transforming vectors from the inertial axes to the local axes is presented as:

$$[\ell_{RL}] = \begin{bmatrix} \cos\psi_R & \sin\psi_R \sin\tau_R & -\sin\psi_R \cos\tau_R \\ 0 & \cos\tau_R & \sin\tau_R \\ \sin\psi_R & -\cos\psi_R \sin\tau_R & \cos\psi_R \cos\tau_R \end{bmatrix}$$

IMOD1 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>			
	ψ_R	Degree	3015
	τ_R	Degree	3014
<u>Output</u>			
	$[\ell_{RL}]$		2000-2008

	SUBROUTINE IMOD1	TR300100
C		
C	3/10/78	
C		TR300110
C	THIS ROUTINE CALCULATES THE INITIAL DIRECTION COSINE MATRICE LRL	TR300150
C	FOR 3DOF SIMULATIONS	TR300160
C		TR300170
C	IT REQUIRES THE FOLLOWING INITIAL CONDITIONS ON CODE 3 CONTROL	TR300180
C	CARDS	TR300190
C		TR300200
C	TAUR=Y(3014) , LONGITUDE (DEG)	
C	PSIR=Y(3015) , LATITUDE (DEG)	
C		TR300230
C	COMMON Y(4940)	
	EQUIVALENC(Y(3015),PSIR),(Y(3014),TAUR)	
	EQUIVALENC(Y(2000),LRL(1))	TR300260
	REAL LRL(9)	TR300270
	CALL SENCOS(PSIR,SP,CP,0)	TR300280
	CALL SENCOS(TAUR,ST,CT,0)	TR300290
	LRL(1)=CP	TR300300
	LRL(2)=0.	TR300310
	LRL(3)=SP	TR300320
	LRL(4)=SP*ST	TR300330
	LRL(5)=CT	TR300340
	LRL(6)=-CP*ST	TR300350
	LRL(7)=-SP*CT	TR300360
	LRL(8)=ST	TR300370
	LRL(9)=CP*CT	TR300380
	RETURN	TR300390
	END	TR300400
		TR300410
		TR300420
		TR300420

APPENDIX D

MOD1; DIRECTION COSINE MATRIX FOR 3DOF OVER A
ROTATING SPHERICAL EARTH

The purpose of this module is to calculate the direction cosine matrix for a vehicle flying a 3DOF particle trajectory over a rotating spherical earth.

The longitude and latitude of the vehicle are calculated from the inertial coordinates as,

$$\tau_R = \tan^{-1} \frac{-Y_R}{Z_R}$$

$$\psi_R = \tan^{-1} \left(\frac{X_R}{\sqrt{Y_R^2 + Z_R^2}} \right)$$

The direction cosine matrix which allows for transforming vectors from the inertial axes to the local axes is calculated as,

$$[\ell_{RL}] = \begin{bmatrix} \cos\psi_R & \sin\psi_R \sin\tau_R & -\sin\psi_R \cos\tau_R \\ 0 & \cos\tau_R & \sin\tau_R \\ \sin\psi_R & -\cos\psi_R \sin\tau_R & \cos\psi_R \cos\tau_R \end{bmatrix}$$

The transfer matrix $[\ell_{LR}]$ is expressed as $[\ell_{LR}] = [\ell_{RL}]^{-1}$.

<u>MOD1 Parameters</u>			
	<u>Parameters</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	X_R	feet	803
	Y_R	feet	804
	Z_R	feet	805
<u>Output</u>	τ_R	radian	3014
	ψ_R	radian	3015
	$[\ell_{RL}]$		2000-2008
	$[\ell_{LR}]$		2039-2047

C	SUBROUTINE MOD1	TR300930
C		TR300940
C	THIS ROUTINE CALCULATES THE DIRECTION COSINE MATRIX LRL FOR A	TR300980
C	3DOF SIMULATION OVER A ROTATING SPHERICAL EARTH	TR300990
C		TR301000
C	3/10/78	
C	COMMON Y(4940)	
	EQUIVALENC(Y(803),XR),(Y(804),YR),(Y(805),ZR)	TR301020
	EQUIVALENC(Y(3015),PSIR),(Y(3014),TAUR)	
	EQUIVALENC(Y(2000),LRL(1))	TR301040
	EQUIVALENC(Y(2039),LLR(1))	TR301050
	RFAL LRL(9),LLR(9)	TR301060
	DIMENSION R(9)	TR301070
C		
C	LATITUDE AND LONGITUDE CALCULATED	
C		
10	CALL ARKTAN(-YR,ZR,TAUR,1)	TR301080
	CALL ARKTAN(XR,(SQRT(ZR**2+YR**2)),PSIR,1)	TR301090
C		
C	INERTIAL TO LOCAL AXES TRANSFER MATRIX	
C		
20	CALL SENCOS(TAUR,STAR,CTAR,1)	TR301100
	CALL SENCOS(PSIR,SPSR,CPSR,1)	TR301110
	LPL(1)=CPSR	TR301120
	LPL(2)=0.	TR301130
	LRL(3)=SPSR	TR301140
	LRL(4)=SPSR*STAR	TR301150
	LRL(5)=CTAR	TR301160
	LPL(6)=-CPSR*STAR	TR301170
	LPL(7)=-SPSR*CTAR	TR301180
	LRL(8)=STAR	TR301190
	LPL(9)=CPSR*CTAR	TR301200
	CALL MATINV(LRL,R,LLR)	TR301210
	RETURN	TR301220
	END	TR301230
		TR301240
		TR301250
		TR301260

APPENDIX E

IMOD2; INITIAL CONDITIONS FOR A 3DOF OR 6DOF TRAJECTORY

The purpose of this module is to calculate the initial values for the inertial coordinates and velocities of the vehicle flying over a spherical earth.

Since the initial altitude latitude, and longitude of the vehicle are specified in the input conditions, the inertial coordinates can be expressed as,

$$\begin{aligned} X_R &= \sin\psi_R(h + R_E) \\ Y_R &= -\cos\psi_R(h + R_E)\sin\tau_R \\ Z_R &= \cos\psi_R(h + R_E)\cos\tau_R \end{aligned}$$

Likewise, the velocity components with respect to the inertial axes can be expressed as functions of the initial inputted flight path angles and resultant velocity as,

$$\begin{bmatrix} \dot{X}_R \\ \dot{Y}_R \\ \dot{Z}_R \end{bmatrix} = [l_{RL}]^{-1} \begin{bmatrix} V_E \cos\gamma_E \cos\gamma_H \\ -V_E \cos\gamma_E \sin\gamma_H - \omega_E (R_E + h) \cos\psi_R \\ V_E \sin\gamma_E \end{bmatrix}$$

The initial starting point of the vehicle's flight path as projected onto the earth's surface is defined as,

$$\begin{aligned} R_{\tau_{E_i}} &= R_E \tau_R \left(\frac{\pi}{180} \right) \\ R_{\psi_{E_i}} &= R_E \psi_R \left(\frac{\pi}{180} \right) \end{aligned}$$

This IMOD serves for MOD3 and MOD9 also.

IMOD2 Parameters

<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>		
h	feet	3013
R _E	feet	3000
(R _E default value = 20925631 feet)		
V _E	feet/second	610
γ _H	degree	2208
γ _E	degree	2209
ω _E	radians/sec	3001
(ω _E default value = 0.0000729211508 rad/sec)		
τ _R	degree	3014
ψ _R	degree	3015
<u>Output</u>		
X _R	feet	803
Y _R	feet	804
Z _R	feet	805
\dot{X}_R	feet/second	800
\dot{Y}_R	feet/second	801
\dot{Z}_R	feet/second	802
R _{τE_i}	feet	818
R _{ψE_i}	feet	819

```

C          SURROUTINE IMOD2
C          3/10/78
C          THIS ROUTINE CALCULATES THE INITIAL VALUES OF XR, YP, ZP
C          AND XRD, YPD, AND ZRD, AND THE INITIAL EARTH POSITIONS
C          RTEI, AND RPEI
C          THE FOLLOWING INITIAL CONDITIONS ARE REQUIRED ON CODE 3
C          CONTROL CARDS
C          PSIR=Y(3015) . LATITUDE (DEG)
C          TAUR=Y(3014) . LONGITUDE (DEG)
C          H=Y(3013) . ALTITUDE (FT)
C          RF=Y(3000) . RADIUS OF EARTH (FT), DEFAULT VALUE = 20925631.
C          WF=Y(3001) . EARTH'S SPIN RATE (RAD/SEC), DEFAULT VALUE =
C          0.0000729211508
C          VF=Y(610) . INITIAL VELOCITY W/R TO EARTH (FPS)
C          GAMAE=Y(2209) . VELOCITY ELEVATION ANGLE (DEG)
C          GAMAH=Y(2208) . VELOCITY HEADING ANGLE (DEG)
C
C          COMMON Y(4940)
C          EQUIVALENC(Y(803),XR), (Y(804),YP), (Y(805),ZR)
C          EQUIVALENC(Y(2039),LLR(1)), (Y(2000),LPL(1))
C          EQUIVALENC(Y(3015),PSTR), (Y(3014),TAUR)
C          EQUIVALENC(Y(3001),WF)
C          EQUIVALENC(Y(818),RTEI), (Y(819),RPEI)
C          EQUIVALENC(Y(3000),RF), (Y(3013),H)
C          EQUIVALENC(Y(2213),OT), (Y(2214),OP)
C          EQUIVALENC(Y(654),MI), (Y(3012),MS)
C          EQUIVALENC(Y(2208),GAMAH), (Y(2209),GAMAE)
C          REAL LLR(9),LRL(9),LR
C          DIMENSION R(9)
C          ENTRY IMOD3
C          ENTRY IMOD0
C
C          INITIAL INFRTIAL POSITION
C          CALL SFNCOS(TAUR,STAR,CTAR,0)
C          CALL SFNCOS(PSTR,SPSR,CPSR,0)
C          XR=SPSR*(H+RF)
C          LR=CPSR*(H+RF)
C          YP=-LR*STAR
C          ZP=LR*CTAR
C
C          INITIAL INFRTIAL VELOCITIES
C          CALL SFNCOS(GAMAE,SE,CF,0)
C          CALL SFNCOS(GAMAH,SH,CH,0)
C          Y(512)=Y(610)*CF*CH
C          Y(513)=-Y(610)*CF*SH
C          Y(514)=Y(610)*SE
C          Y(513)=Y(513)-WF*(RE+H)*CPSR
C          CALL MATINV(LRL(1),R,LIR)
C          CALL MATVEC(LIR,Y(512),Y(800),0)
C          DO 20 I=1,3
C          Y(I+514)=Y(I+511)
C
C          INITIAL RANGES
C          RAD=3.141592653589/180.

```

TR300430
TR300440

TR300460
TR300490
TR300500
TR300510

TR300560
TR300570
TR300590
TR300600
TR300610
TR300620
TR300630
TR300640
TR300650
TR300660
TR300665

TR300670
TR300680
TR300690
TR300700
TR300710
TR300720

TR300730
TR300740
TR300750
TR300760
TR300770
TR300780
TR300790
TR300800
TR300860
TR300870

TR300810

NSWC/WOL TR 78-59

RTEI=RE*TAUR*RAD
RPEI=RE*PSTR*RAD
OT=TAUR*RAD
OP=PSIR*RAD
MI=MS
RETURN
END

TR300820
TR300830
TR300840
TR300850
TR300880
TR300890
TR300900
TR300910
TR300920

APPENDIX F

MOD2; 3DOF PARTICLE TRAJECTORY ALONG A
PROGRAMMED FLIGHT PATH

The purpose of this module is to calculate the transformation matrix for a vehicle flying along a 3DOF particle trajectory over a spherical earth where the elevation angle of the velocity vector is preprogrammed. This elevation angle, γ_E , is taken from a table of γ_E as a function of time which is to be supplied by the user as Table Array Number 10. The heading angle, γ_H , is maintained constant. The altitude is calculated as,

$$h = \sqrt{X_R^2 + Y_R^2 + Z_R^2} - R_E$$

The local velocities with respect to the earth are calculated as,

$$\begin{bmatrix} v_{X_{LE}} \\ v_{Y_{LE}} \\ v_{Z_{LE}} \end{bmatrix} = [l_{RL}] \begin{bmatrix} \dot{X}_R \\ \dot{Y}_R \\ \dot{Z}_R \end{bmatrix} + \begin{bmatrix} 0 \\ \omega_E (R_E + h) \cos \psi_R \\ 0 \end{bmatrix}$$

The resultant velocity is then calculated as,

$$v_E = \sqrt{v_{X_{LE}}^2 + v_{Y_{LE}}^2 + v_{Z_{LE}}^2}$$

The $[l_{PL}]$ matrix, necessary for transforming vectors from the principal axes to the local axes is written in terms of γ_H and γ_E as,

$$[l_{PL}] = \begin{bmatrix} \cos \gamma_H \cos \gamma_E & \sin \gamma_H & -\cos \gamma_H \sin \gamma_E \\ -\sin \gamma_H \cos \gamma_E & \cos \gamma_H & \sin \gamma_H \sin \gamma_E \\ \sin \gamma_E & 0 & \cos \gamma_E \end{bmatrix}$$

MOD2 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	γ_E	degree	2209
	γ_H	degree	2208
	X_R	feet	803
	Y_R	feet	804
	Z_R	feet	805
	\dot{X}_R	feet/second	800
	\dot{Y}_R	feet/second	801
	\dot{Z}_R	feet/second	802
	R_E	feet	3000
	<u>Output</u>	$[\ell_{PL}]$	
h		feet	3013
$V_{X_{1e}}$		feet/second	512
$V_{Y_{LE}}$		feet/second	513
$V_{Z_{LE}}$		feet/second	514
V_E		feet/second	610

```

SUBROUTINE MOD2
C
C      POSITION MODULE FOR A 3DOF PARTICLE TRAJ. WITH PROGRAMMED
C      PITCH ANGLE
C
C      3/10/78
C
C      GAMAF (DEG) IS TABULATED AS A FUNCTION OF TIME (SEC) IN
C      TABLE ARRAY NO. 10
C      GAMAH (DEG) IS A CONSTANT IN LOCATION Y(2208)
C
C
C      COMMON Y(4940)
C      EQUIVALENC (Y(3013),H)
C      EQUIVALENC (Y(803),XR), (Y(804),YR), (Y(805),ZR)
C      EQUIVALENC (Y(3015),PSTR), (Y(3014),TAUP)
C      EQUIVALENC (Y(3001),WE), (Y(3000),RE)
C      EQUIVALENC (Y(512),VXLE), (Y(513),VYLE), (Y(514),VZLE)
C      EQUIVALENC (Y(2999),T)
C      EQUIVALENC (Y(2208),GAMAH), (Y(2209),GAMAE)
C      EQUIVALENC (Y(2057),LPL(1))
C      EQUIVALENC (Y(2000),LRL(1)), (Y(610),VE)
C      DIMENSION H(2)
C      REAL      LRL(9),LPL(9)
C
C      FLIGHT PATH ANGLES
C
C      10 U(1)=T
C      CALL ITAB(10,1,T,GAMAE)
C      CALL SENCOS(GAMAH,SH,CH,0)
C      CALL SENCOS(GAMAE,SE,CF,0)
C
C      PRINCIPAL TO LOCAL TRANSFER MATRIX
C
C      20 LPL(1)=CH*CE
C      LPL(2)=-SH*CF
C      LPL(3)=SE
C      LPL(4)=SH
C      LPL(5)=CH
C      LPL(6)=0.0
C      LPL(7)=-CH*SF
C      LPL(8)=SH*SE
C      LPL(9)=CE
C
C      ALTITUDE
C
C      30 H=SQRT(XR**2+YR**2+ZR**2)-PE
C
C      LOCAL VELOCITY COMPONENTS
C
C      40 CALL MATVEC(LRL(1),Y(800),Y(512),0)
C      VXLE=Y(512)
C      VYLE=Y(513)+WE*(RF+H)*COS(PSIR)
C      VZLE=Y(514)
C      VF=SQRT(VXLE**2+VYLE**2+VZLE**2)
C      RETURN
C      END

```

TR301280

TR301460

TR301500

TR301560

TR301610

TR301650

TR302160

TR302170

TR302180

TR302190

TR302200

TR302210

TR302220

TR302230

TR302240

TR302250

TR302260

TR301740

TR301750

TR301760

TR301770

TR302320

TR302330

APPENDIX G

MOD3; 3DOF PARTICLE TRAJECTORY WITH THRUST

The purpose of this module is to calculate the altitude, local velocity components, flight path angles, and the principal-to-local transfer matrix for a vehicle flying along a 3DOF, point-mass, ballistic trajectory.

The altitude is calculated from the inertial coordinates which have been obtained through the integration of the equations of motion;

$$h = \sqrt{X_R^2 + Y_R^2 + Z_R^2} - R_E$$

Since the velocity of the vehicle with respect to the inertial axes are also known from the integration of the equations of motion, the local velocities with respect to the earth's surface are calculated by transforming the inertial velocities as,

$$\begin{bmatrix} v_{X_{LE}} \\ v_{Y_{LE}} \\ v_{Z_{LE}} \end{bmatrix} = [l_{RL}] \begin{bmatrix} \dot{X}_R \\ \dot{Y}_R \\ \dot{Z}_R \end{bmatrix} + \begin{bmatrix} 0 \\ \omega_E (R_E + h) \cos \psi_R \\ 0 \end{bmatrix}$$

The total velocity with respect to the earth is then,

$$v_E = \sqrt{v_{X_{LE}}^2 + v_{Y_{LE}}^2 + v_{Z_{LE}}^2}$$

The flight path angles, angles of the velocity vector with respect to the local axes, are then calculated as,

$$\gamma_H = \tan^{-1} \left(\frac{-v_{Y_{LE}}}{v_{X_{LE}}} \right),$$

$$\gamma_E = \tan^{-1} \left(\frac{v_{Z_{LE}}}{\sqrt{v_{X_{LE}}^2 + v_{Y_{LE}}^2}} \right)$$

The transfer matrix for transforming a vector from the principal axes to the local axes can then be written in terms of the flight path angles as,

$$[\ell_{PL}] = \begin{bmatrix} \cos\gamma_H \cos\gamma_E & \sin\gamma_H & -\cos\gamma_H \sin\gamma_E \\ -\sin\gamma_H \cos\gamma_E & \cos\gamma_H & \sin\gamma_H \sin\gamma_E \\ \sin\gamma_E & 0 & \cos\gamma_E \end{bmatrix}$$

MOD3 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>	
<u>Input</u>	X_R	feet	803	
	Y_R	feet	804	
	Z_R	feet	805	
	R_E	feet	3000	
	\dot{X}_R	feet/second		
	\dot{Y}_R	feet/second		
	\dot{Z}_R	feet/second		
	$[\ell_{RL}]$			
	ω_E	rad/sec		
	ψ_R	radian		
	<u>Output</u>	h	feet	3013
		$V_{X_{LE}}$	feet/second	512
		$V_{Y_{LE}}$	feet/second	513
$V_{Z_{LE}}$		feet/second	514	
V_E		feet/second	610	
γ_H		degree	2208	
γ_E		degree	2209	
$[\ell_{PL}]$			2057-2065	

```

SUBROUTINE MOD3
C
C      POSITION MODULE FOR A 3DOF BALLISTIC PARTICLE TRAJ.
C
C      3/10/78
C
C      COMMON Y(4940)
EQUIVALENC (Y(3013),H)
EQUIVALENC (Y(2057),LPL(1))
EQUIVALENC (Y(803),XR),(Y(804),YR),(Y(805),ZR)
EQUIVALENC (Y(3015),PSTR),(Y(3014),TAUP)
EQUIVALENC (Y(3001),WE),(Y(3000),RE)
EQUIVALENC (Y(512),VXLF),(Y(513),VYLF),(Y(514),VZLF)
EQUIVALENC (Y(2208),GAMAH),(Y(2209),GAMAE)
EQUIVALENC (Y(2000),LRL(1)),(Y(610),VE)
RFAL LPL(9),LRL(9)
C
C      ALTITUDE
C
C      10 H=SQRT(XR**2+YR**2+ZR**2)-RE
C
C      LOCAL VFLOCITY COMPONENTS
C
C      20 CALL MATVEC(LRL(1),Y(800),Y(512),0)
VXLE=Y(512)
VYLE=Y(513)+WE*(RE+H)*COS(PSTR)
VZLE=Y(514)
VF=SQRT(VXLE**2+VYLE**2+VZLE**2)
C
C      FLIGHT PATH ANGLES
C
C      30 CALL ARKTAN(-VYLE,VXLE,GAMAH,0)
ZZZ=SQRT(VXLE**2+VYLE**2)
CALL ARKTAN(VZLE,ZZZ,GAMAE,0)
CALL SENCOS(GAMAH,SH,CH,0)
CALL SENCOS(GAMAE,SE,CE,0)
C
C      PRINCPAL TO LOCAL TRANSFER MATRIX
C
C      40 LPL(1)=CH*CE
LPL(2)=-SH*CF
LPL(3)=SE
LPL(4)=SH
LPL(5)=CH
LPL(6)=0.0
LPL(7)=-CH*SF
LPL(8)=SH*SF
LPL(9)=CE
C
C      RFTURN
END

```

TR301300

TR301330

TR302530

TR302570

TR302640

TR302730

TR302810

TR302820

TR302830

TR302840

TR303100

TR303110

TR303220

TR303230

TR303240

TR303250

TR303260

TR303270

TR303280

TR303290

TR303300

TR303310

TR303320

TR303380

TR303390

APPENDIX H

IMOD4; 6DOF INITIAL DIRECTION
COSINE MATRIX

The purpose of this routine is to calculate the initial direction cosine matrices for transforming vectors from the inertial to the local to the principal axes for a 6DOF trajectory simulation over a spherical rotating earth. The inertial to local transform matrix is defined as,

$$[l_{RL}] = \begin{bmatrix} \cos\psi_R & \sin\psi_R \sin\tau_R & -\sin\psi_R \cos\tau_R \\ 0 & \cos\tau_R & \sin\tau_R \\ \sin\psi_R & -\cos\psi_R \sin\tau_R & \cos\psi_R \cos\tau_R \end{bmatrix}$$

and the local to principal transform matrix as

$$[l_{LP}] = \begin{bmatrix} \cos\epsilon_M \cos\gamma_M & -\cos\epsilon_M \sin\gamma_M & \sin\epsilon_M \\ \cos\phi_M \sin\gamma_M - \sin\phi_M \sin\epsilon_M \cos\gamma_M & \cos\phi_M \cos\gamma_M + \sin\phi_M \sin\epsilon_M \sin\gamma_M & \sin\phi_M \cos\epsilon_M \\ -\sin\phi_M \sin\gamma_M - \cos\phi_M \sin\epsilon_M \cos\gamma_M & -\sin\epsilon_M \cos\gamma_M + \cos\phi_M \sin\epsilon_M \sin\gamma_M & \cos\phi_M \cos\epsilon_M \end{bmatrix}$$

The angles ψ_R and τ_R are the latitude and longitude angles in degrees and the angles γ_M , ϵ_M , ϕ_M are the position angles of the principal axes with respect to the local angles. These angles are shown in Figures 5 and 6.

The inertial to principal axis transfer matrix can then be expressed as

$$[l_{RP}] = [l_{LP}][l_{RL}]$$

IMOD4 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	τ_R	degree	3014
	ψ_R	degree	3015
	γ_M	degree	2066
	ϵ_M	degree	2067
	ϕ_M	degree	2068
<u>Output</u>			
	ℓ_{RL}		2000-2008
	ℓ_{RP}		2009-2017
	ℓ_{LP}		2027-2035

C	SUBROUTINE IMOD4	SIX00150
C		SIX00160
C		SIX00180
C	MOD PACKAGE SIXDG. A GENERAL PURPOSE 6DOF GUIDED OR	SIX00190
C	UNGUIDED TRAJECTORY PROGRAM	SIX00200
C		SIX00210
C	3/10/78	
C		
C	THIS ROUTINE CALCULATES THE INITIAL DIRECTION COSINE MATRICES LRL,	SIX00220
C	LLP,LRP	SIX00230
C		SIX00240
C	IT REQUIRES THE FOLLOWING INITIAL CONDITIONS ON CODE 3 CONTROL	SIX00250
C	CARDS	SIX00260
C		SIX00270
C	PSIR=Y(3015) . LATITUDE (DEG)	
C	TAUR=Y(3014) . LONGITUDE (DEG)	
C	GAMAM=Y(2066) . HEADING ANGLE (DEG) OF PRINCIPAL AXES	
C	EPSILM=Y(2067) . ELEVATION ANGLE (DEG) OF PRINCIPAL AXES	
C	PHIM=Y(2068) . ROLL ANGLE OF PRINCIPAL AXES	
C		SIX00330
C	COMMON Y(4940)	SIX00340
C	EQUIVALENC(Y(3015),PSIR),(Y(3014),TAUR)	SIX00350
C	EQUIVALENC(Y(2066),GAMAM),(Y(2067),EPSILM),(Y(2068),PHIM)	
C	EQUIVALENC(Y(2000),LRL(1)),(Y(2009),LRP(1)),(Y(2027),LLP(1))	SIX00370
C	REAL LRL(9),LRP(9),LLP(9)	SIX00380
C	CALL SENCOS(PSIR,SP,CP,0)	SIX00390
C	CALL SENCOS(TAUR,ST,CT,0)	SIX00400
C	LRL(1)=CP	SIX00410
C	LRL(2)=0.	SIX00420
C	LRL(3)=SP	SIX00430
C	LRL(4)=SP*ST	SIX00440
C	LRL(5)=CT	SIX00450
C	LRL(6)=-CP*ST	SIX00460
C	LRL(7)=-SP*CT	SIX00470
C	LRL(8)=ST	SIX00480
C	LRL(9)=CP*CT	SIX00490
C	CALL SENCOS(GAMAM,SG,CG,0)	
C	CALL SENCOS(EPSILM,SE,CE,0)	
C	CALL SENCOS(PHIM,SP,CP,0)	
C	LIP(1)=CE*CG	
C	LIP(2)=CP*SG-SP*SE*CG	
C	LIP(3)=-SP*SG-CP*SE*CG	
C	LIP(4)=-CE*SG	
C	LIP(5)=CP*CG+SP*SE*SG	
C	LIP(6)=-SP*CG+CP*SE*SG	
C	LIP(7)=SE	
C	LIP(8)=SP*CF	
C	LIP(9)=CP*CE	
C	CALL MATVEC(LIP(1),LRL(1),LPP(1),2)	SIX00620
C	RETURN	SIX00630
C	END	SIX00640

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APPENDIX I

MOD4; 6DOF DIRECTION COSINE MATRIX

The purpose of this module is to calculate the direction cosine matrices l_{RL} , l_{RP} , and l_{LP} for a 6DOF simulation of a vehicle flying over a rotating spherical earth.

First, the latitude and longitude of the vehicle are calculated as,

$$\tau_R = \tan^{-1} \left(\frac{-Y_R}{Z_R} \right)$$

$$\psi_R = \tan^{-1} \left(\frac{X_R}{\sqrt{Y_R^2 + Z_R^2}} \right)$$

The inertial to local transfer matrix can then be written as,

$$[l_{RL}] = \begin{bmatrix} \cos\psi_R & \sin\psi_R \sin\tau_R & -\sin\psi_R \cos\tau_R \\ 0 & \cos\tau_R & \sin\tau_R \\ \sin\psi_R & -\cos\psi_R \sin\tau_R & \cos\psi_R \cos\tau_R \end{bmatrix}$$

In order to calculate the position of the principal axes with respect to the inertial axes, it is necessary to define the direction cosine matrix as follows.

$$\begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_P = [l_{RP}] \begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_R$$

where

$$\begin{bmatrix} \vec{i} \\ \vec{j} \\ \vec{k} \end{bmatrix}_R$$

is a unit vector along the inertial axes

and

$$\begin{bmatrix} \vec{j} \\ \vec{i} \\ \vec{k} \end{bmatrix}_P \text{ is a unit vector along the principal axes}$$

and

$$[l_{RP}] = \begin{bmatrix} l_{11} & l_{12} & l_{13} \\ l_{21} & l_{22} & l_{23} \\ l_{31} & l_{32} & l_{33} \end{bmatrix}$$

When the above are expanded, the equations look as follows:

$$\vec{i}_P = l_{11} \vec{i}_R + l_{12} \vec{j}_R + l_{13} \vec{k}_R$$

$$\vec{j}_P = l_{21} \vec{i}_R + l_{22} \vec{j}_R + l_{23} \vec{k}_R$$

$$\vec{k}_P = l_{31} \vec{i}_R + l_{32} \vec{j}_R + l_{33} \vec{k}_R$$

If these are now differentiated with respect to time the following equations result:

$$\dot{\vec{i}}_P = \dot{l}_{11} \vec{i}_R + \dot{l}_{12} \vec{j}_R + \dot{l}_{13} \vec{k}_R$$

$$\dot{\vec{j}}_P = \dot{l}_{21} \vec{i}_R + \dot{l}_{22} \vec{j}_R + \dot{l}_{23} \vec{k}_R$$

$$\dot{\vec{k}}_P = \dot{l}_{31} \vec{i}_R + \dot{l}_{32} \vec{j}_R + \dot{l}_{33} \vec{k}_R$$

If the following relationships are substituted into the above equations

$$\dot{\vec{i}}_P = \vec{\omega} \times \vec{i}_P = r_{j_P}^{\vec{\omega}} - q \vec{k}_P$$

$$\dot{\vec{j}}_P = \vec{\omega} \times \vec{j}_P = p_{k_P}^{\vec{\omega}} - r \vec{i}_P$$

$$\dot{\vec{k}}_P = \vec{\omega} \times \vec{k}_P = q \vec{i}_P - p \vec{j}_P$$

and the individual components are separated the following nine differential equations are formed.

$$\dot{l}_{11} = r l_{21} - q l_{31}$$

$$\dot{l}_{21} = p l_{31} - r l_{11}$$

$$\dot{l}_{31} = q l_{11} - p l_{21}$$

$$\dot{l}_{12} = r l_{22} - q l_{32}$$

$$\dot{l}_{22} = p l_{32} - r l_{12}$$

$$\dot{l}_{32} = q l_{12} - p l_{22}$$

$$\dot{l}_{18} = r l_{23} - q l_{33}$$

$$\dot{l}_{23} = p l_{33} - r l_{13}$$

$$\dot{l}_{33} = q l_{13} - p l_{23}$$

These nine equations can then be integrated numerically in order to define the individual elements of the direction cosine matrix l_{RP} . The other matrices can then be calculated as,

$$[l_{LR}] = [l_{RL}]^{-1}$$

$$[l_{LP}] = [l_{RP}][l_{LR}]$$

$$[l_{PL}] = [l_{LP}]^{-1}$$

MOD4 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	X_R	ft	803
	Y_R	ft	804
	Z_R	ft	805
	P	rad/sec	806
	q	rad/sec	807
	r	rad/sec	808
	$[\ell_{RP}]$		2009-2017
<u>Output</u>	τ_R	deg	3014
	ψ_R	deg	3015
	$[\ell_{RL}]$		2000-2008
	$[\ell_{LP}]$		2027-2035
	$[\ell_{LR}]$		2039-2047
	$[\ell_{PL}]$		2057-2065

```

C          SUBROUTINE MOD4                                SIX01260
C          3/10/78                                       SIX01270
C
C          MOD PACKAGE SIXDG, A GENERAL PURPOSE 6DOF GUIDED OR SIX01290
C          UNGUIDED TRAJECTORY PROGRAM                   SIX01300
C          SIX01310
C          SIX01320
C          THIS ROUTINE CALCULATES THE DIRECTION COSINE MATRICES LRL,LRP, SIX01330
C          LLP FOR A 6DOF SIMULATION OVER A ROTATING SPHERICAL EARTH SIX01340
C          SIX01350
C          NOTE" THE LRPD(9) MATRIX ELEMENTS ARE DERIVATIVES AND MUST BE SIX01360
C          IDENTIFIED ON CODE 6 AND 7 CONTROL CARDS SIX01370
C          SIX01380
C          COMMON Y(4940)                                SIX01390
C          EQUIVALENC(Y(803),XR),(Y(804),YR),(Y(805),ZR) SIX01400
C          EQUIVALENC(Y(2036),PHIL),(Y(2037),THETAL),(Y(2038),PSIL) SIX01410
C          EQUIVALENC(Y(3014),TAUR),(Y(3015),PSIR)       SIX01420
C          EQUIVALENC(Y(2000),LRL(1)),(Y(2009),LRP(1)),(Y(2018),LRPD(1)) SIX01430
C          EQUIVALENC(Y(806),PP),(Y(807),QP),(Y(808),RP) SIX01440
C          EQUIVALENC(Y(2027),LLP(1)),(Y(2039),LLR(1)),(Y(2057),LPL(1)) SIX01450
C          REAL LRL(9),LRPD(9),LRP(9),LLP(9),LIR(9),LPL(9) SIX01480
C          DIMENSION R(9)                                SIX01490
C          DFG=180./3.141592653589                       SIX01500
C
C          LATITUDE AND LONGITUDE
C
C          10 CALL ARKTAN(-YR,ZR,TAUR,0)                  SIX01510
C          CALL ARKTAN(XR,(SQRT(ZR**2+YR**2)),PSIR,0)   SIX01520
C          20 CALL SENCOS(TAUR,STAR,CTAR,0)              SIX01530
C          CALL SENCOS(PSIR,SPSR,CPSR,0)                SIX01540
C
C          INERTIAL TO LOCAL, LOCAL TO PRINCIPAL, AND INERTIAL TO
C          PRINCIPAL TRANSFER MATRICES
C
C          LRL(1)=CPSR                                    SIX01550
C          LRL(2)=0.                                       SIX01560
C          LRL(3)=SPSR                                    SIX01570
C          LRL(4)=SPSR*STAR                                SIX01580
C          LRL(5)=CTAR                                    SIX01590
C          LRL(6)=-CPSR*STAR                              SIX01600
C          LRL(7)=-SPSR*CTAR                             SIX01610
C          LRL(8)=STAR                                    SIX01620
C          LRL(9)=CPSR*CTAR                              SIX01630
C          30 LRPD(1)=RP*LRP(2)-QP*LLP(3)                SIX01640
C          LRPD(2)=PP*LRP(3)-RP*LLP(1)                  SIX01650
C          LRPD(3)=QP*LRP(1)-PP*LLP(2)                  SIX01660
C          LRPD(4)=RP*LRP(5)-QP*LLP(6)                  SIX01670
C          LRPD(5)=PP*LRP(6)-RP*LRP(4)                  SIX01680
C          LRPD(6)=QP*LRP(4)-PP*LRP(5)                  SIX01690
C          LRPD(7)=RP*LRP(8)-QP*LLP(9)                  SIX01700
C          LRPD(8)=PP*LLP(9)-RP*LLP(7)                  SIX01710
C          LRPD(9)=QP*LRP(7)-PP*LLP(8)                  SIX01720
C          CALL MATINV(LRL,B,LLR)                         SIX01730
C          40 CALL MATVEC(LRP,LIR,LLP,2)                  SIX01740
C
C          ORIENTATION OF PRINCIPAL AXES W/R TO LOCAL AXES
C
C          CALL ARKTAN(-LLP(7),LLP(1),THETAL,0)         SIX01750
C          IF(THETAL) 43,44,44                            SIX01760
C          43 THETAL=THETAL+360.                          SIX01770
C          44 CONTINUE                                    SIX01780
C          CALL ARKTAN(-LLP(6),LLP(5),PHIL,0)           SIX01790

```

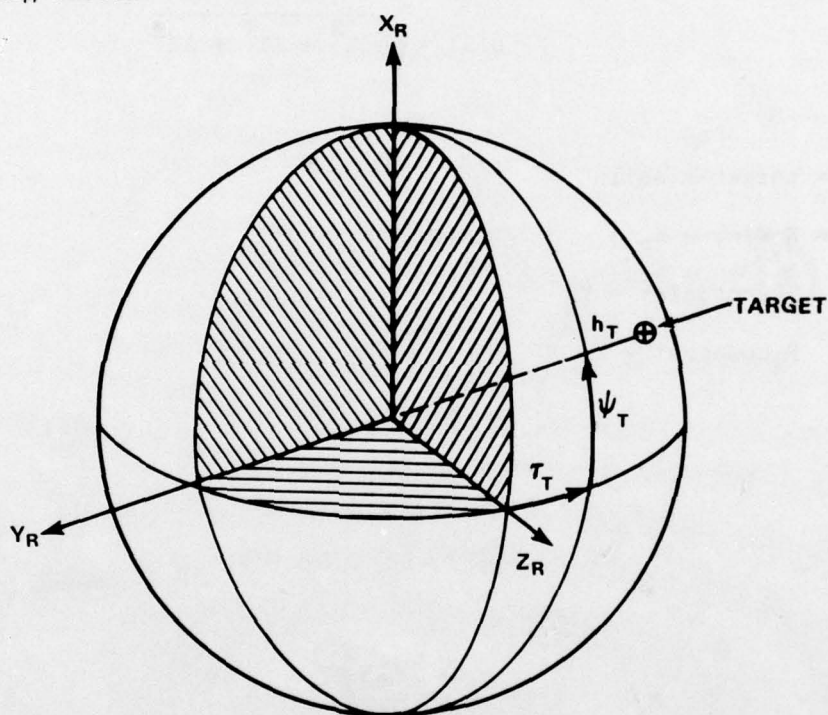
NSWC/WOL TR 78-59

	IF (PHIL) 46,48,48	SIX01800
46	PHIL=PHIL+360.	SIX01810
48	CONTINUE	SIX01820
	CALL SENCOS (PHIL,SPH,CPH,0)	SIX01830
	PSIL=ASIN (LLP(4))*DEG	SIX01840
50	CALL MATINV (LLP,R,LPL)	SIX01850
	RETURN	SIX01860
	END	SIX01870

APPENDIX J

MOD5; TARGET MODULE

This module provides for the locating of a target with respect to the vehicle. The target can be either fixed with respect to the earth or moving at a constant velocity. The initial position of the target is given by the initial altitude, h_T , latitude, ψ_{Ti} , and longitude, τ_{Ti} . The velocities are presented as vertical, \dot{R}_T , longitudinal, $V_{T\tau}$; and latitudinal, $V_{T\psi}$. These relationships are shown in the following sketch:



The inertial coordinates of the target are calculated as,

$$X_{TR} = R_T \sin \psi_T$$

$$Y_{TR} = -R_T \cos \psi_T \sin \tau_T$$

$$Z_{TR} = R_T \cos \psi_T \cos \tau_T$$

where

$$R_T = R_e + h_{T_i} + \dot{R}_T(t - t_i)$$

$$\psi_T = \psi_{T_i} + \frac{V_T \psi_i}{R_T} \left(\frac{180}{\pi} \right) (t - t_i)$$

$$\tau_T = \tau_{T_i} + \frac{V_T \tau_i}{R_T \cos \psi} \left(\frac{180}{\pi} \right) (t - t_i) + \omega_E \left(\frac{180}{\pi} \right) (t - t_i)$$

The distance between the target and the vehicle are expressed as,

$$\text{DIST} = \sqrt{\Delta X^2 + \Delta Y^2 + \Delta Z^2}$$

where,

Δ = target-missile

$$\Delta X = R_T \sin \psi - X_R$$

$$\Delta Y = -R_T \cos \psi \sin \tau - Y_R$$

$$\Delta Z = R_T \cos \psi \cos \tau - Z_R$$

MOD5 Parameters

<u>Input</u>	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
	h_{T_i}	ft	1
	τ_{T_i}	deg	2
	ψ_{T_i}	deg	3
	V_{T_τ}	fps	4
	V_{T_ψ}	fps	5
	\dot{R}_T	fps	6
	R_E	ft	3000
	ω_E	rad/sec	3001
	t_i	sec	2862
	X_R	ft	803
	Y_R	ft	804
	Z_R	ft	805
<u>Output</u>			
	X_{TR}	ft	10
	Y_{TR}	ft	11
	Z_{TR}	ft	12
	ΔX	ft	13
	ΔY	ft	14
	ΔZ	ft	15
	DIST	ft	19

C	SUBROUTINE MON5	SIX01910
C	3/10/78	SIX01920
C	TARGET FIXED OR MOVING AT A CONSTANT VELOCITY	SIX01940
C	THE REQUIRED INPUTS ARE.	SIX01950
C	HTI = INITIAL HEIGHT OF THE TARGET (FT)	SIX01960
C	TAUTI = INITIAL LONGITUDE (DEG)	SIX01970
C	PSITI = INITIAL LATITUDE (DEG)	SIX01980
C	VTTAU = LONGITUDINAL VELOCITY OF TARGET (FPS)	SIX01990
C	VTPSI = LATITUDINAL VELOCITY OF TARGET (FPS)	SIX02000
C	RTDOT = VERTICAL VELOCITY OF TARGET (FPS)	SIX02010
C	COMMON Y(4940)	SIX02020
	EQUIVALENC(Y(1),HTI),(Y(2),TAUTI),(Y(3),PSITI)	SIX02030
	EQUIVALENC(Y(4),VTTAU),(Y(5),VTPSI),(Y(6),RTDOT)	SIX02040
	EQUIVALENC(Y(3000),RE),(Y(3001),WE)	SIX02050
	EQUIVALENC(Y(2868),DELT),(Y(2999),T)	SIX02060
	EQUIVALENC(Y(2862),TI)	SIX02070
	EQUIVALENC(Y(7),RT),(Y(8),TAU),(Y(9),PSI)	SIX02080
	EQUIVALENC(Y(10),XTR),(Y(11),YTR),(Y(12),ZTR)	SIX02090
	EQUIVALENC(Y(13),DX),(Y(14),DY),(Y(15),DZ)	SIX02100
	EQUIVALENC(Y(R03),XR),(Y(R04),YR),(Y(R05),ZR)	SIX02110
	EQUIVALENC(Y(19),DIST)	SIX02120
C	INERTIAL COORDINATES OF TARGET	SIX02130
C	DFG=180./3.14159265358979	SIX02140
C	RT=RE+HTI+RTDOT*(T-TI)	SIX02150
	PSI=PSITI+(VTPSI/RT)*DFG*(T-TI)	SIX02160
	CALL SENCOS(PSI,SP,CP,0)	SIX02170
	TAU=TAUTI+(VTTAU/(RT*CP))*DFG*(T-TI)	SIX02180
	TAU=TAU+WE*(T-TI)*DFG	SIX02190
	CALL SENCOS(TAU,ST,CT,0)	SIX02200
	XTR=RT*SP	SIX02210
	YTR=-RT*CP*ST	SIX02220
	ZTR=RT*CP*CT	SIX02230
C	INERTIAL DISTANCES BETWEEN TARGET AND MISSILE	SIX02240
C	DX=XTR-XR	SIX02250
C	DY=YTR-YR	SIX02260
	DZ=ZTR-ZR	SIX02270
	DIST=SQRT(DX**2+DY**2+DZ**2)	SIX02280
	RETURN	SIX02290
	END	SIX02300
		SIX02310

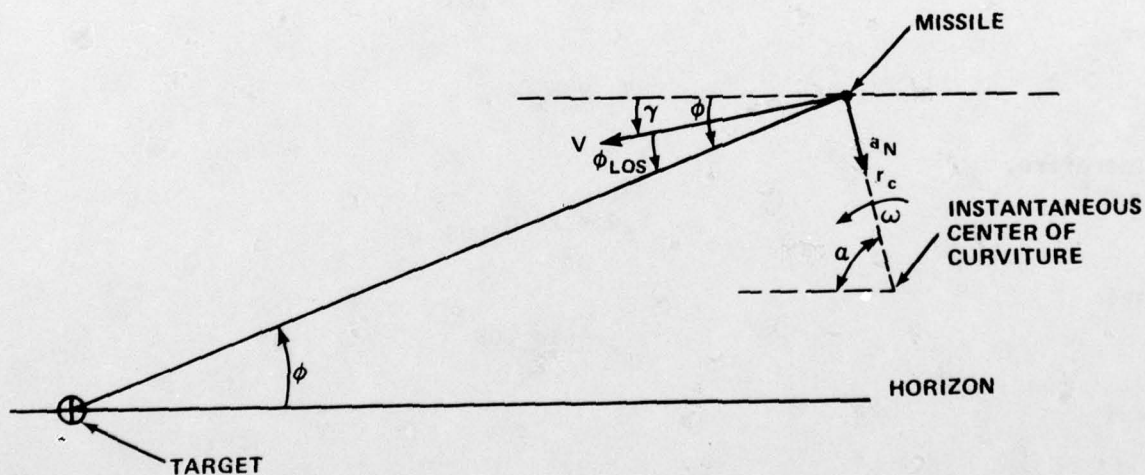
APPENDIX K

MOD6; PROPORTIONAL NAVIGATION SEEKER MODULE

This module takes the relative locations of the target and missile, converts these linear displacements into angular relationships and utilizing the laws of proportional navigation calculates error signals suitable for a control system. The definition of proportional navigation is that the angular rate of the vehicle should be proportional to the rate of change of the line-of-sight angle. In order to rotate the vehicle, or more appropriately its velocity vector, it is necessary to generate an acceleration at right angles to the velocity vector. Based on the turning radius of the vehicle,

$$a_N = \frac{V^2}{r_c}$$

where the following sketch shows the definitions of the parameters.



Since,

$$\vec{V} = \vec{\omega} \times r_c$$

$$\dot{\alpha} = -\dot{\gamma}$$

$$\omega \equiv -\dot{\alpha} = \dot{\gamma}$$

the radius of curvature is

$$r_c = V/\dot{\gamma}$$

The normal acceleration then becomes

$$a_N = V \dot{\gamma}$$

or since the definition of proportional navigation is

$$\dot{\gamma} \equiv K \dot{\phi}$$

$$a_N = VK \dot{\phi}$$

The velocity component of the missile at right angles to the line-of-sight can be defined in two ways.

$$V_{\perp} = V \sin \phi_{LOS}$$

or

$$V_{\perp} = R_S \dot{\phi}$$

Therefore,

$$R_S \dot{\phi} = V \sin \phi_{LOS}$$

and

$$\dot{\phi} = \frac{V \sin \phi_{LOS}}{R_S}$$

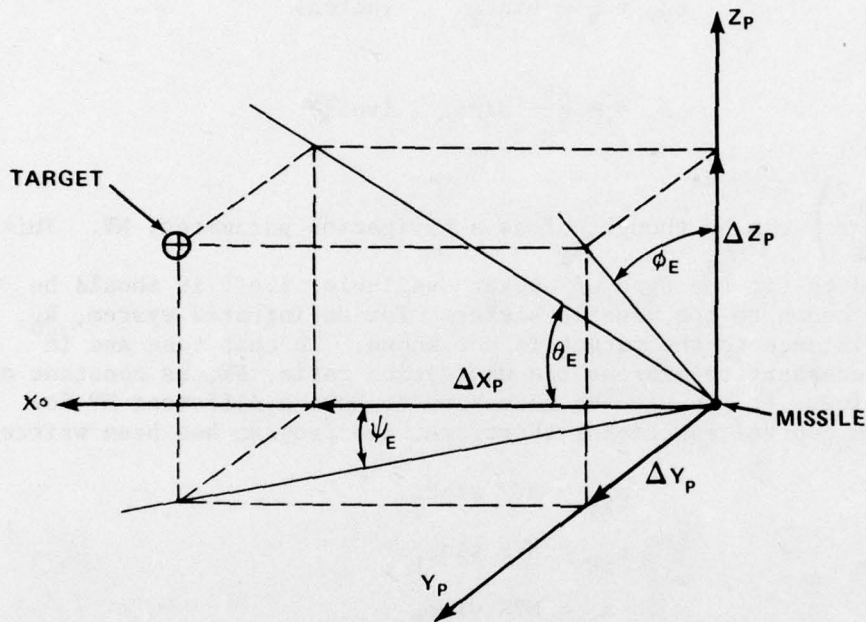
and

$$a_N = \frac{KV^2}{R_S} \sin \phi_{LOS}$$

The relative locations between the target and the missile with respect to the inertial axes were calculated in the Target Module. These "position errors" can be transformed into "body" related displacements by,

$$\begin{bmatrix} \Delta X_P \\ \Delta Y_P \\ \Delta Z_P \end{bmatrix} = [{}^R_P] \begin{bmatrix} \Delta X_R \\ \Delta Y_R \\ \Delta Z_R \end{bmatrix}$$

where



The angular relationships can then be calculated as

$$\psi_E = \tan^{-1} \left(\frac{\Delta Y_P}{\Delta X_P} \right)$$

$$\theta_E = \tan^{-1} \left(\frac{\Delta Z_P}{\Delta X_P} \right)$$

$$\phi_E = \tan^{-1} \left(\frac{\Delta Y_P}{\Delta Z_P} \right)$$

It is now possible to express the required normal accelerations in terms of the angular displacements. For a bi-planar control system these would be,

$$a_{ZP} = \frac{KV^2}{R_S} \sin\theta_E$$

$$a_{YP} = \frac{KV^2}{R_S} \sin\psi_E$$

If the vehicle had only planar lift and roll capability these would be,

$$a_{ZP} = \frac{KV^2}{R_S} \sin\theta_E \quad (\text{pitch})$$

$$a_L = -\frac{KV^2}{R_S} \sin\phi_E \quad (\text{roll})$$

The factor $\left(\frac{KV^2}{R_S}\right)$ can be thought of as a navigation parameter, NV. This is usually tailored to fit the type of seeker available; i.e., it should be expressed in terms known to the missile seeker. For an infrared system, R_S , or the remaining distance to the target is not known. In that case and in others it may be necessary to express the navigation ratio, NV, as constant or as a function of time. It may also be necessary to have a different NV for each of the missile control functions; therefore, the program has been written as,

$$a_{ZP} = NVP \sin\theta_E$$

$$a_{YP} = NVP \sin\psi_E$$

$$a_L = NVR \sin\phi_E$$

Each user will have to program the navigation ratios to suit his particular system.

MOD6 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	ΔX	ft	13
	ΔY	ft	14
	ΔZ	ft	15
	NVP	ft/sec ²	126
	NVY	ft/sec ²	127
	NVR	ft/sec ²	128
<u>Output</u>	AZP	ft/sec ²	102
	AYP	ft/sec ²	101
	AL	ft/sec ²	100
	ϕ_E	rad	123
	θ_E	rad	124
	ψ_E	rad	125

C	SUBROUTINE MOD6	S1100110
C	3/10/78	
C		S1100130
C	PROPORTIONAL NAVIGATION	S1100140
C		S1100150
C	THIS PROGRAM TAKES THE TARGET DISPLACEMENTS, CALCULATES THE	S1100160
C	ANGULAR DISPLACEMENT, AND THEN PROCESSES IT IN ORDER TO ARRIVE	S1100170
C	AT ERROR SIGNALS FOR THE AUTOPILOT	S1100180
C		S1100190
	COMMON Y(4940)	
	EQUIVALENC(Y(2009),LRP)	S1100210
	EQUIVALENC(Y(126),NVP),(Y(127),NVY),(Y(128),NVR)	S1100220
	EQUIVALENC(Y(100),AL),(Y(101),AYP),(Y(102),AZP)	
	EQUIVALENC(Y(123),PHIE),(Y(124),THETA), (Y(125),PSTE)	S1100230
	REAL LRP(9),NVP,NVY,NVR	S1100250
	CALL MATVEC(LRP,Y(13),Y(100),0)	
	CALL ARKTAN(Y(101),Y(102),PHIE,1)	S1100270
	CALL ARKTAN(Y(102),Y(100),THETA,1)	S1100280
	CALL ARKTAN(Y(101),Y(100),PSTE,1)	S1100290
C.....	NOTE.....	S1100310
C	PROGRAM THE NAVIGATION RATIOS TO SUIT YOUR MISSILE	S1100320
	NVP=Y(126)	S1100330
	NVY=Y(127)	S1100340
	NVR=Y(128)	S1100350
C.....	S1100360
	A7P=NVP*SIN(THETA)	S1100370
	AYP=NVY*SIN(PSTE)	S1100380
	AI=NVP*SIN(PHIE)	S1100390
	RETURN	S1100400
	END	S1100410

APPENDIX L

MOD7; AUTOPILOT/CONTROL MODULE

This module is representative of an autopilot or control system for a 6DOF simulation. In this elementary example, it is assumed that the vehicle has a bi-planar control system and that the vehicle does not roll. This module demonstrates how a lead-lag network can be incorporated for handling the seeker error signals, how the missile heave and pitching motion can be incorporated, and how the actuator dynamics can be included. This module has just the two channels, one for pitch and the other for yaw. The easiest way to describe the system is to refer to Figures L-1 and L-2. The basic input to this module would consist of two error signals received from the seeker. A positive error signal in the "Z" channel arriving from the seeker is calling for a correction in the missile attitude such that would cause the vehicle to be displaced in the direction of the positive Z_p axis of the vehicle. A similar arrangement exists for the yaw channel.

AD-A073 901

NAVAL SURFACE WEAPONS CENTER WHITE OAK LAB SILVER SP--ETC F/G 16/2
MODIFY: A MODULAR MULTI-DEGREE-OF-FREEDOM TRAJECTORY PROGRAM. (U)

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2 OF 2

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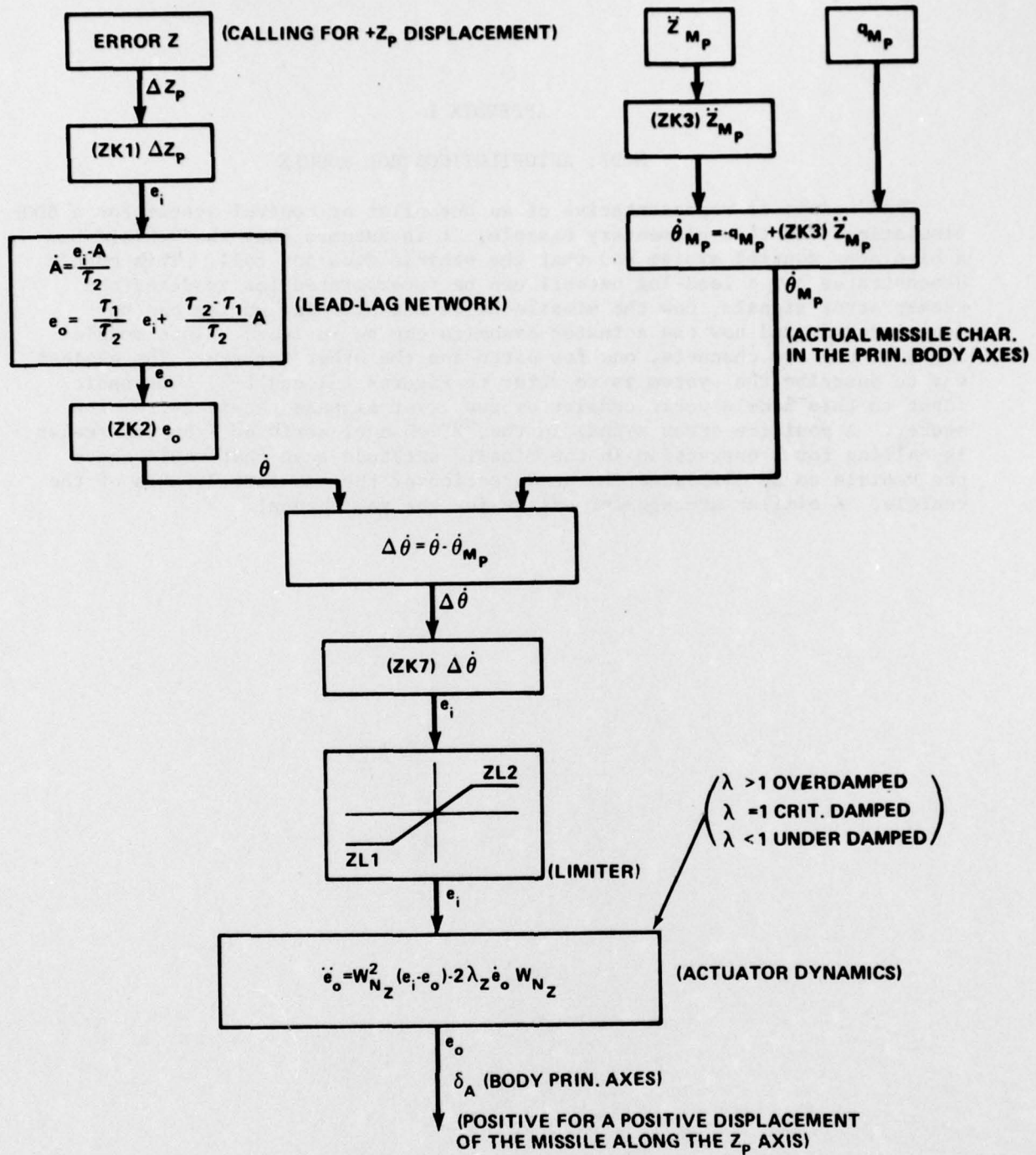


FIGURE L-1 Z CONTROL CHANNEL

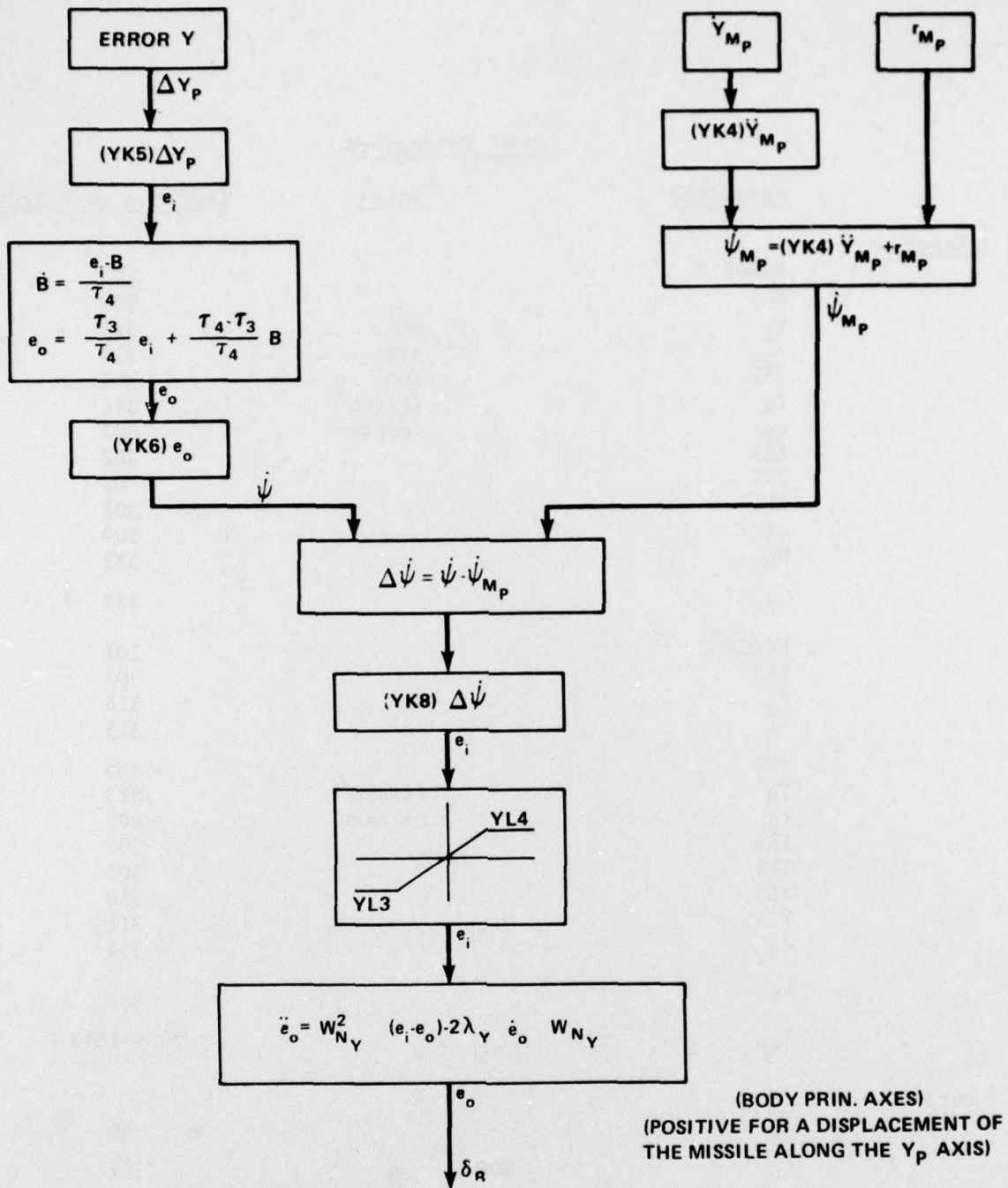


FIGURE L-2 Y CONTROL CHANNEL

MOD7 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>	ERROR Z		102
	ZK1		300
	τ_1	sec	312
	τ_2	sec	313
	ZK2	sec	301
	\ddot{Z}_R	ft/sec ²	814
	q_p	rad/sec	807
	ZK3		302
	ZK7		306
	ZL1		308
	ZL2		309
	ω_{Nz}		332
	λ_z		333
	ERROR Y		101
	YK5		304
	τ_3	sec	314
	τ_4	sec	315
	YK6		305
	\ddot{Y}_R	ft/sec ²	813
	r_p	rad/sec	808
	YK4		303
	YK8		307
	YL3		310
YL4		311	
ω_{Ny}		334	
λ_y		335	
ℓ_{RP}		2009-2017	
<u>Output</u>	δ_A		386
	δ_B		387

C	SUBROUTINE MOD7	S1100450
C		S1100480
C		S1100490
C	AUTOPILOT RASE1,RI-PLANAR CONTROL DEFLECTIONS	S1100500
C		S1100460
C	3/10/78	
C		S1100510
C	NOTE THAT THIS PROGRAM REQUIRES CODE 6 AND CODE 7 CONTROL	
C	CARDS FOR A,AD,B,BD,E07,E0ZD,E0ZDD,E0Y,E0YD,E0YDD	
C		
	COMMON Y(4940)	
	EQUIVALENCF(Y(100),ERRORX),(Y(101),ERRORY),(Y(102),FRRORZ)	S1100530
	EQUIVALENCF(Y(300),ZK1),(Y(301),ZK2),(Y(302),ZK3)	S1100540
	EQUIVALENCF(Y(303),YK4),(Y(304),YK5),(Y(305),YK6)	S1100550
	EQUIVALENCF(Y(306),ZK7),(Y(307),YK8),(Y(308),ZL1)	S1100560
	EQUIVALENCF(Y(309),ZL2),(Y(310),YL3),(Y(311),YL4)	S1100570
	EQUIVALENCF(Y(312),T1),(Y(313),T2),(Y(314),T3),(Y(315),T4)	S1100580
	EQUIVALENCF(Y(332),WNZ),(Y(333),LZ),(Y(334),WNY),(Y(335),IY)	S1100590
	EQUIVALENCF(Y(316),AD),(Y(317),A)	S1100600
	EQUIVALENCF(Y(318),BD),(Y(319),B)	S1100610
	EQUIVALENCF(Y(806),PP),(Y(807),QP),(Y(808),RP)	S1100620
	EQUIVALENCF(Y(812),XDD),(Y(813),YDD),(Y(814),ZDD)	S1100630
	EQUIVALENCF(Y(2000),LRL(1)),(Y(2009),LRP(1))	S1100640
	EQUIVALENCF(Y(359),THED),(Y(360),PSID)	S1100650
	EQUIVALENCF(Y(329),E0ZDD),(Y(330),E0ZD),(Y(331),E07)	S1100660
	EQUIVALENCF(Y(336),E0YDD),(Y(337),E0YD),(Y(338),E0Y)	S1100670
	EQUIVALENCF(Y(380),PMP),(Y(381),QMP),(Y(382),RMP)	S1100680
	EQUIVALENCF(Y(386),DA),(Y(387),DB)	S1100690
	EQUIVALENCF(Y(2057),LPL(1))	S1100700
	RFAL LRL(9),LRP(9),LPL(9),LZ,LY	S1100710
C		
C	PITCH CHANNEL	
C		
10	EI=ZK1*ERRORZ	S1100720
	AD=(EI-A)/T2	S1100730
	E0=(T1/T2)*EI+((T2-T1)/T2)*A	S1100740
20	THED=ZK2*E0	S1100750
C		
C	YAW CHANNEL	
C		
30	EI=YK5*ERRORY	S1100760
	BD=(EI-B)/T4	S1100770
	E0=(T3/T4)*EI+((T4-T3)/T4)*B	S1100780
40	PSID=YK6*E0	S1100790
C		
C	MISSILE ANGULAR RATES IN PRINCIPAL AXES	
C		
	CALL MATVEC(LRP,Y(812),Y(383),0)	S1100800
50	PMP=PP	S1100810
	QMP=-QP+ZK3*Y(385)	S1100820
	RMP=RP+YK4*Y(384)	S1100830
100	Y(323)=0.	S1100840
	Y(324)=(THED-QMP)*ZK7	S1100850
	Y(325)=(PSID-RMP)*YK8	S1100860
C		
C	LIMITS ON ACTUATOR SIGNALS	
C		
	IF(Y(324).GE.7L2) Y(324)=ZL2	S1100870
	IF(Y(324).LE.ZL1) Y(324)=ZL1	S1100880
	IF(Y(325).GE.YL4) Y(325)=YL4	S1100890
	IF(Y(325).LE.YL3) Y(325)=YL3	S1100900
C		

C ACTUATOR DYNAMICS
C

EOYDD=(WNY**2)*(Y(325)-EOY)-2.0*LY*FOYD*WNY
EOZDD=(WNZ**2)*(Y(324)-EOZ)-2.0*LZ*EOZD*WNZ
DA=EOZ
DR=EOY
RFTURN
END

S1100910
S1100920
S1100930
S1100940
S1100950
S1100960

APPENDIX M

MOD8; 6DOF FORCE AND MOMENT MODULE

The purpose of this module is to calculate the external forces and moments acting on a vehicle in a 6DOF simulation. It provides for nonlinear aerodynamics, winds, thrust, and relatively small control moments.

The velocity of the vehicle with respect to the earth is calculated by transforming the inertial velocities as follows,

$$\begin{bmatrix} V_{X_{LE}} \\ V_{Y_{LE}} \\ V_{Z_{LE}} \end{bmatrix} = [{}^l_{RL}] \begin{bmatrix} \dot{X}_R \\ \dot{Y}_R \\ \dot{Z}_R \end{bmatrix} + \begin{bmatrix} 0 \\ \omega_E (R_E + h) \cos \psi_R \\ 0 \end{bmatrix}$$

Winds are then introduced in tabular form as a function of altitude. The wind velocity, V_W is tabulated as a function of altitude in Table Array No. 3, and the heading angle of the wind is tabulated in Table Array No. 4 (see Figure 8). The velocity of the vehicle with respect to the air is then calculated as,

$$\begin{bmatrix} V_{A_{XL}} \\ V_{A_{YL}} \\ V_{A_{ZL}} \end{bmatrix} = \begin{bmatrix} V_{Y_{LE}} \\ V_{Y_{LE}} \\ V_{Z_{LE}} \end{bmatrix} - \begin{bmatrix} V_W \cos(A_W) \\ V_W \sin(A_W) \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} V_{A_{XP}} \\ V_{A_{YP}} \\ V_{A_{ZP}} \end{bmatrix} = [{}^l_{LP}] \begin{bmatrix} V_{A_{XL}} \\ V_{A_{YL}} \\ V_{A_{ZL}} \end{bmatrix}$$

If the geometric axes in which the aerodynamic data were measured are skewed with respect to the principal axes, the velocity can be further transformed as

$$\begin{bmatrix} v_{AXG} \\ v_{AYG} \\ v_{AZG} \end{bmatrix} = [l_{PG}] \begin{bmatrix} v_{AXP} \\ v_{AYP} \\ v_{AZP} \end{bmatrix}$$

and the total velocity of the vehicle with respect to the air is,

$$v_A = \sqrt{v_{AXG}^2 + v_{AYG}^2 + v_{AZG}^2}$$

In order to calculate the Mach number and dynamic pressure it is necessary to calculate the flow properties such as speed of sound and density. These values are derived from the 1969 U.S. Standard Atmospheric Tables.

The angles between the body and the flow vector are defined as:

$$\begin{aligned} \alpha &= \tan^{-1} \left[\frac{v_{AZG}}{v_{AXG}} \right] \\ \beta &= \tan^{-1} \left[\frac{v_{AYG}}{v_{ZYG}} \right] \\ \phi_A &= \tan^{-1} \left[\frac{v_{AYG}}{v_{AZG}} \right] \\ \bar{\alpha} &= \tan^{-1} \left[\frac{\sqrt{v_{AYG}^2 + v_{AZG}^2}}{v_{AXG}} \right] \end{aligned} \quad \left. \vphantom{\begin{aligned} \alpha \\ \beta \\ \phi_A \\ \bar{\alpha} \end{aligned}} \right\} \text{see Figure 9}$$

The aerodynamic forces and moments are entered into the program through a set of tables. These tables are as follows:

AERO COEFF.TABLE ARRAY NO.

$C_x(M, \bar{\alpha})$	12
$C_y(M, \bar{\alpha}, \phi_A)$	13
$C_z(M, \bar{\alpha}, \phi_A)$	14
$C_{y_p}(M, \bar{\alpha})$	15
$C_{\ell}(M, \bar{\alpha}, \phi_A)$	16
$C_{\ell_p}(M, \bar{\alpha})$	17
$C_{\ell_\delta}(M, \bar{\alpha})$	18
$C_m(M, \bar{\alpha}, \phi_A)$	19
$C_n(M, \bar{\alpha}, \phi_A)$	20
$C_{m_q}(M, \bar{\alpha})$	21
$C_{n_p}(M, \bar{\alpha})$	22

The forces along the vehicle geometric axes can then be defined as:

$$\begin{bmatrix} F_{XG} \\ F_{YG} \\ F_{ZG} \end{bmatrix} = \left(\frac{1}{2} \rho V_A^2 \right) * (A) * \begin{bmatrix} C_{XG} \\ C_{YG} \\ C_{ZG} \end{bmatrix} - \begin{bmatrix} \text{THRUST} \\ 0 \\ 0 \end{bmatrix}$$

where

$$C_{XG} = C_x$$

$$C_{YG} = C_y \cos \phi_A + C_y \sin \phi_A + C_{y_p} \frac{pd}{2V_A} \cos \phi_A$$

$$C_{ZG} = C_z \cos \phi_A - C_y \sin \phi_A - C_{y_p} \frac{pd}{2V_A} \sin \phi_A$$

The aerodynamic moment coefficients are written as

$$C_{LG} = C_{\ell} + C_{\ell_p} \frac{pd}{2V_A} + C_{\ell_\delta} \delta$$

$$C_{MG} = C_m \cos\phi_A + C_n \sin\phi_A + C_{M_p} \frac{pd}{2V_A} \sin\phi_A + C_{m_q} \frac{qd}{2V_A} - C_{m_\delta} \delta_A$$

$$C_{NG} = C_n \cos\phi_A - C_m \sin\phi_A + C_{n_p} \frac{pd}{2V_A} \cos\phi_A + C_{m_q} \frac{rd}{2V_A} + C_{M_\delta} \delta_B$$

Then, the moments about the center of gravity can be written as:

$$\begin{bmatrix} M_{LG} \\ M_{MG} \\ M_{NG} \end{bmatrix} = \begin{bmatrix} C_{L_G} + C_{Y_G} \Delta z - C_{Z_G} \Delta Y \\ C_{M_G} + C_{Z_G} \Delta X \\ C_{N_G} - C_{Y_G} \Delta X \end{bmatrix} \quad (\text{Q A d})$$

where ΔX , ΔY , ΔZ are the nondimensional lengths (ft/D) from the origin of the geometric axes to the origin of the principal axes (see Figure 8).

MOD8 Parameters

<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
<u>Input</u>		
$\Delta X, \Delta Y, \Delta Z$		3006, 3007, 3008
X_R	ft	803
Y_R	ft	804
Z_R	ft	805
R_E	ft	3000
\dot{X}_R	ft/sec	800
\dot{Y}_R	ft/sec	801
\dot{Z}_R	ft/sec	802
ω_E	rad/sec	3001
ψ_R	deg	3015
ϕ_G	deg	3002
θ_G	deg	3003
d	ft	3004
A	ft ²	3005
δ	deg	604
δ_A	deg	386
δ_B	deg	387
l_{LP}		2007-2035
l_{RL}		2000-2008
p, q, r		806, 807, 808
<u>Output</u>		
M		577
Q	lb/ft ²	576
α	deg	572
β	deg	573
$\bar{\alpha}$	deg	599
ϕ_A	deg	574
F_{X_R}	lb	550
F_{Y_R}	lb	551
F_{Z_R}	lb	552

<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
M_{LP}	ft-lb	547
M_{MP}	ft-lb	548
M_{NP}	ft-lb	
l_{GP}	ft-lb	563-571
V_A	fps	575

MOD8 TABLES

<u>Table Array No.</u>	<u>Table</u>	<u>Units</u>
3	$V_W(h)$	fps
4	$A_W(h)$	deg
12	$C_x(M, \bar{\alpha})$	
13	$C_y(M, \bar{\alpha}, \phi_A)$	
14	$C_z(M, \bar{\alpha}, \phi_A)$	
15	$C_{y_p}(M, \bar{\alpha})$	
16	$C_{l_1}(M, \bar{\alpha}, \phi_A)$	
17	$C_{l_p}(M, \bar{\alpha})$	
18	$C_{l_\delta}(M, \bar{\alpha})$	
19	$C_m(M, \bar{\alpha}, \phi_A)$	
20	$C_M(M, \bar{\alpha}, \phi_A)$	
21	$C_{m_q}(M, \bar{\alpha})$	
22	$C_{M_p}(M, \bar{\alpha})$	
23	THRUST (t)	lb
24	$m_s(t)$	slug
25	$I_{xx}(t)$	slug/ft ²
26	$I_{yy}(t)$	slug/ft ²
27	$I_{zz}(t)$	slug/ft ²
28	$\Delta X(t)$	
29	$\Delta X(t)$	
30	$\Delta Z(t)$	

SUBROUTINE MOD8

```

C
C   A GENERAL PURPOSE 6DOF FORCE AND MOMENT MODULE FOR A
C   MISSILE WITH MOMENT CONTROL IN TWO PLANES
C
C   3/10/78
C
C   TABLES.  KTAR(3)=VW(H) . WIND SPEED (FPS)
C               KTAR(4)=AW(H) . WIND AZIMUTH (DEG)
C               KTAB(12)=CX(M,ALPHA BAR)
C               KTAR(13)=CY(M,ALPHA BAR,PHIA)
C               KTAB(14)=CZ(M,ALPHA BAR,PHIA)
C               KTAR(15)=CYP(M,ALPHA BAR)
C               KTAR(16)=CL(M,ALPHA BAR,PHIA)
C               KTAR(17)=CLP(M,ALPHA BAR)
C               KTAR(18)=CLD(M,ALPHA BAR)
C               KTAR(19)=CM(M,ALPHA BAR,PHIA)
C               KTAR(20)=CN(M,ALPHA BAR,PHIA)
C               KTAR(21)=CMQ(M,ALPHA BAR)
C               KTAR(22)=CNP(M,ALPHA BAR)
C               KTAR(23)=THRUST(T) . (LR)
C               KTAR(24)=MS(T) . TOTAL MASS.(SLUG)
C               KTAR(25)=JXX(T) . (SLUG-FT**2)
C               KTAR(26)=IYY(T) . (SLUG-FT**2)
C               KTAR(27)=IZZ(T) . (SLUG-FT**2)
C               KTAR(28)=DXG(T)
C               KTAR(29)=DYG(T)
C               KTAR(30)=DZG(T)
C
C   D=REFERENCE LT. (FT)
C   A=REFERENCE AREA (FT**2)
C   DXG *LOCATION OF GEOM. AXES W/R TO AERODYN. DATA AXES
C   DYG *
C   DZG *(NONDIMENSIONAL. FT/D)
C   PHG YAW ANGLE (DEG) BETWN GEOM. AXES AND PRIN. AXES
C   THG PITCH .....
C
C   COMMON Y(4940)
C   COMMON/TAB/7(50)
C   EQUIVALENC(Y(578),GRAV) . (Y(577),VMACH)
C   EQUIVALENC(Y(800),XRD) . (Y(801),YRD) . (Y(802),ZRD)
C   EQUIVALENC(Y(3015),PSTR) . (Y(3014),TAUR)
C   EQUIVALENC(Y(3001),WF) . (Y(3000),RE) . (Y(2027),LLP(1))
C   EQUIVALENC(Y(2000),LRL(1)) . (Y(3013),H) . (Y(563),LGP(1))
C   EQUIVALENC(Y(3019),THETA6) . (Y(3020),PS16) . (Y(3021),PHI6)
C   EQUIVALENC(Y(803),XR) . (Y(804),YR) . (Y(805),ZR)
C   EQUIVALENC(Y(806),P) . (Y(807),Q) . (Y(808),R)
C   EQUIVALENC(Y(3004),D) . (Y(3005),A)
C   EQUIVALENC(Y(3006),DXG) . (Y(3007),DYG) . (Y(3008),DZG)
C   EQUIVALENC(Y(547),MLP) . (Y(548),MMP) . (Y(549),MNP)
C   EQUIVALENC(Y(550),FXR) . (Y(551),FYR) . (Y(552),FZR)
C   EQUIVALENC(Y(512),VXLF) . (Y(513),VYLF) . (Y(514),VZLF)
C   EQUIVALENC(Y(500),XED) . (Y(501),YED) . (Y(502),ZED)
C   EQUIVALENC(Y(2057),LPI(1)) . (Y(2039),LLP(1)) . (Y(2048),LPG(1))
C   EQUIVALENC(Y(572),ALPHA) . (Y(573),PHIA) . (Y(574),PHIA)
C   EQUIVALENC(Y(575),VA) . (Y(576),QP) . (Y(520),VAXL)
C   EQUIVALENC(Y(521),VAYI) . (Y(522),VAZI)
C   EQUIVALENC(Y(3451),K(1))
C   EQUIVALENC(Y(2999),T)
C   EQUIVALENC(Y(544),FXG) . (Y(545),FYG) . (Y(546),FZG)
C   EQUIVALENC(Y(590),THRUST) . (Y(599),ALPH)

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	EQUIVALENCF (Y (529), CX), (Y (532), CY), (Y (533), CZ)	S1101580
	EQUIVALENCF (Y (534), CLP), (Y (536), CM), (Y (537), CMQ)	S1101590
	EQUIVALENCF (Y (535), CLD), (Y (539), CN)	S1101600
	EQUIVALENCF (Y (614), CYP), (Y (615), CNP), (Y (616), CL)	S1101610
	EQUIVALENCF (Y (518), VW), (Y (519), AW)	S1101620
	EQUIVALENCF (Y (2037), THFTAL), (Y (3012), MS)	S1101630
	EQUIVALENCF (Y (526), VAXG), (Y (527), VAYG), (Y (528), VAZG)	S1101640
	EQUIVALENCF (Y (2009), LHP), (Y (556), PHIAD), (Y (604), DAF)	S1101650
	EQUIVALENCF (Y (605), PD2V), (Y (606), QD2V), (Y (607), RD2V)	S1101660
	EQUIVALENCF (Y (386), DA), (Y (387), DR)	S1101670
	EQUIVALENCF (Y (608), CMDA), (Y (609), CNDR)	S1101680
	EQUIVALENCF (Y (611), MLG), (Y (612), MMG), (Y (613), MNG)	S1101690
	EQUIVALENCF (Y (3009), IXX), (Y (3010), IYY), (Y (3011), IZZ)	S1101700
	EQUIVALENCF (Y (610), VE)	S1101710
	DIMENSION K (49)	S1101720
	DIMENSION R (9)	S1101730
	DIMENSION U (3)	S1101740
	RFAL LLR (9), LPG (9), LPL (9)	S1101750
	RFAL LRL (9), LGP (9), MLP, MMP, MNP, LLP (9)	S1101760
	RFAL LRP (9), MS, IXX, IYY, IZZ	S1101770
	RFAL MLG, MMG, MNG	S1101780
	RAD=3.141592653589/180.	S1101790
C		
C	VELOCITIES	
C		
10	CALL MATVEC (LRL (1), Y (H00), Y (512), 0)	S1101800
	H=SQRT (XR**2+YR**2+ZR**2)-RF	S1101810
	VXLE=Y (512)	S1101820
	VYLE=Y (513)+WE*(RF+H)*COS (RAD*PSTR)	S1101830
	VZLE=Y (514)	S1101840
	VF=SQRT (VXLE**2+VYLE**2+VZLE**2)	S1101850
	CALL ITAB (3, 1, H, VW)	S1101860
	CALL ITAB (4, 1, H, AW)	S1101870
	AW=AW*RAD	S1101880
60	VWXLE=-VW*COS (AW)	S1101890
	VWYLE=VW*STN (AW)	S1101900
	VWZLE=0.0	S1101910
70	VAXL=VXLE-VWXLE	S1101920
	VAYL=VYLE-VWYLE	S1101930
	VAZL=VZLE-VWZLF	S1101940
80	CALL MATVEC (Y (2027), Y (520), Y (523), 0)	S1101950
C		
C	PRINCIPAL AXIS MISALIGNMENT	
C		
	CALL SENCOS (THETA, STG, CTG, 0)	
	CALL SENCOS (PSIG, SPG, CPG, 0)	
	CALL SENCOS (PHIG, SPHG, CPHG, 0)	
	LGP (1)=CPG*CTG	
	LGP (2)=CPHG*STG-SPHG*SPG*CTG	
	LGP (3)=-SPHG*STG-CPHG*SPG*CTG	
	LGP (4)=-CPG*STG	
	LGP (5)=CPHG*CTG+SPHG*SPG*STG	
	LGP (6)=-SPG*CTG+CPHG*SPG*STG	
	LGP (7)=SPG	
	LGP (8)=SPHG*CPG	
	LGP (9)=CPHG*CPG	
	CALL MATINV (LGP, R, LPG)	S1102070
100	CALL MATVEC (LPG, Y (523), Y (526), 0)	S1102080
C		
C	ATMOSPHERIC/FLOW PROPERTIES	
C		
	VA=SQRT (Y (526)**2+Y (527)**2+Y (528)**2)	S1102090
	IF (H.GE.500000.) GO TO 115	S1102100
110	CALL ARDCFT (H, PP, TT, DD, VS, G)	S1102110
	VMACH=VA/(VS*1116.4)	S1102120
	RHO=DD*0.0023769	S1102130

```

QP=0.5*RHO*VA**2
GO TO 118
115 VMACH=0.0
RHO=0.0
QP=0.0
118 GRAV=(32.174*RF**2)/((SQRT(XR**2+YR**2+ZR**2))**2)
C
C ANGULAR RELATIONSHIP BETWEEN MISSILE AND VELOCITY VECTOR
C
120 CALL ARKTAN(Y(528),Y(526),ALPHA,0)
CALL ARKTAN(Y(527),Y(526),HETA,0)
CALL ARKTAN(Y(527),Y(528),PHIA,0)
CALL ARKTAN((SQRT(Y(527)**2+Y(528)**2)),Y(526),ALPH,0)
C
C FORCE AND MOMENT GENERATION: *****
C
C TABULATED AERODYNAMIC COEFFICIENTS
C
U(1)=VMACH
U(2)=ALPB
CALL TTAB(12.2,U,CX)
CALL TTAB(15.2,U,CYP)
CALL TTAB(17.2,U,CLP)
CALL TTAB(18.2,U,CLU)
CALL TTAB(2).2,U,CMQ)
CALL TTAB(22.2,U,CNP)
IF (PHIA) 140,150,150
140 PHIA=PHIA+360.
150 CONTINUE
U(3)=AMOD(PHIA,90.)

CALL ITAB(13.3,U,CY)
CALL ITAB(14.3,U,CZ)
CALL ITAB(16.3,U,CI)
CALL ITAB(19.3,U,CM)
CALL ITAB(20.3,U,CN)

C
C ANGULAR RATES OF BODY W/R TO FLOW
C
CALL SENCOS(PHIA,SPH,CPH,0)
CALL MATVEC(IPP,Y(812),Y(553),0)
CALL MATVEC(IPG,Y(553),Y(553),0)
CALL MATVEC(IPG,Y(806),Y(820),0)
IF (VA7G**2+VAYG**2) 160,160,170
160 PHIAD=Y(820)
GO TO 175
170 CONTINUE
PHIAD=(VAZG*(Y(554)-Y(822)*VAXG)-VAYG*(Y(555)+Y(821)*VAXG)
+/(VA7G**2+VAYG**2)+Y(820))
175 CONTINUE
PD2V=PHIAD*D/(2.0*VA)
QD2V=Y(821)*D/(2.0*VA)
RD2V=Y(822)*D/(2.0*VA)

C
C AERO COEFFICIENTS
C
CXG=CX
CYG=CY*CPH+C7*SPH+CYP*PD2V*CPH
C7G=C7*CPH-CY*SPH-CYP*PD2V*SPH
CLG=CL+CLP*PD2V
CMG=CM*CPH+CN*SPH+CNP*PD2V*SPH+CMQ*QD2V-CMDA*PA
CNG=CN*CPH-CM*SPH+(CNP*PD2V*CPH+CMQ*PD2V+CNDR)*PH

C
C THRUST AND MASS PROPERTIES
C
U(1)=T

```


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	CALL ITAB(23.1.0.THRUST)	S1102660
	CALL ITAB(24.1.0.MS)	S1102670
	CALL ITAB(25.1.0.TXX)	S1102680
	CALL ITAB(26.1.0.IYY)	S1102690
	CALL ITAB(27.1.0.1ZZ)	S1102700
C		
C	FORCES AND MOMENTS	
C		
	FXG=CXG*QP*A+THRUST	S1102710
	FYG=CYG*QP*A	S1102720
	F7G=CZG*QP*A	S1102730
	CALL ITAB(28.1.0.0XG)	S1102740
	CALL ITAB(29.1.0.0YG)	S1102750
	CALL ITAB(30.1.0.0ZG)	S1102760
	MI G=(CLG+CYG*0ZG-CZG*0Y6)*QP*A*0	S1102770
	MMG=(CMG+C7G*0XG)*QP*A*0	S1102780
	MNG=(CNG-CYG*0XG)*QP*A*0	S1102790
	CALL MATVEC(IGP.Y(611).Y(547).0)	S1102800
200	CONTINUE	S1102810
	CALL MATVEC(LGP.Y(544).Y(550).0)	S1102820
	CALL MATVEC(LPL.Y(550).Y(550).0)	S1102830
	CALL MATVEC(ILR.Y(550).Y(550).0)	S1102840
		S1102850
	RETURN	S1102860
	END	

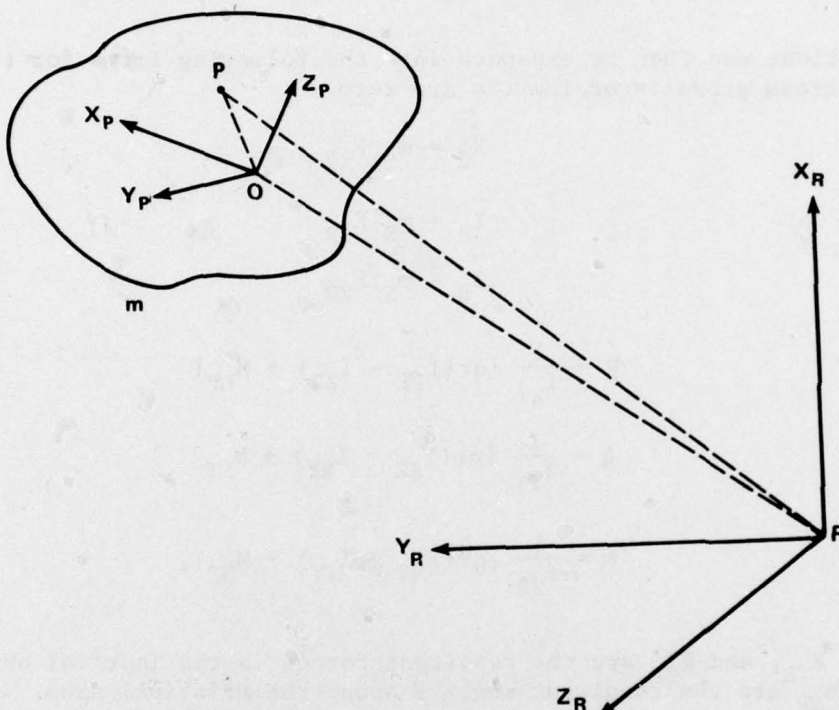
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APPENDIX N

MOD9; EQUATIONS OF MOTION MODULE

The purpose of this module is to express the equations of motion for a 6DOF simulation of a fairly general body. The force equations are written for integration in the inertial frame and the moment equations for integration in the principal axes.

For a mass, m , with the following characteristics,



where X_p, Y_p, Z_p are the principal axes of the mass, and X_R, Y_R, Z_R are the inertial axes, the general acceleration of point, p is,

$$(\vec{a})_R = (\vec{a}_o)_R + \vec{\omega} \times (\vec{\omega} \times \vec{OP}) + \vec{\dot{\omega}} \times \vec{OP} + (\vec{a}_p)_o + 2\vec{\omega} \times (\vec{V}_p)_o$$

In this equation, $(\vec{a}_p)_R$ is the acceleration of P with respect to R ,

$(\vec{a}_o)_R$ is the acceleration of o with respect to R ,

$(\vec{a}_p)_o$ is the acceleration of P with respect to o , and

$(\vec{V}_p)_o$ is the velocity of P with respect to o .

If the assumption is made that m is a rigid body, then

$$\begin{aligned} \vec{a}_P &= 0 \\ (\vec{v}_P)_O &= 0 \end{aligned}$$

and if O is the center of gravity of m , then the following force and moment equations can be written.

$$\vec{F} = \int_m (\vec{a})_r dm = m(\vec{a}_O)_R$$

$$\vec{M} = \int_m [\vec{OP} \times (\vec{a})_R] dm = \int_m \vec{OP} \times [\vec{\omega} \times \vec{OP} + \ddot{\vec{\omega}} \times (\vec{\omega} \times \vec{OP})] dm$$

These equations can then be expanded into the following forms for the case where the cross products of inertia are zero.

$$\ddot{X}_R = m_S F_{XR}$$

$$\ddot{Y}_R = m_S F_{YR}$$

$$\ddot{Z}_R = m_S F_{ZR}$$

$$\dot{p} = \frac{1}{I_{XX}} [qr(I_{YY} - I_{ZZ}) + M_{LP}]$$

$$\dot{q} = \frac{1}{I_{YY}} [pr(I_{ZZ} - I_{XX}) + M_{MP}]$$

$$\dot{r} = \frac{1}{I_{ZZ}} [qp(I_{XX} - I_{YY}) + M_{NP}],$$

where F_{XR} , F_{YR} , and F_{ZR} are the resultant forces in the inertial system, and M_{LP} , M_{MP} , M_{NP} are the resultant moments about the principal axes. In the force equations the resultant forces can be separated into those due to gravity and those due to all other forces. The force equations then become,

$$\ddot{X}_R = \frac{F_{XR}}{m_S} - g \sin\psi_R$$

$$\ddot{Y}_R = \frac{F_{YR}}{m_S} + g \cos\psi_R \sin\tau_R$$

$$\ddot{Z}_R = \frac{F_{ZR}}{m_S} - g \cos\psi_R \cos\tau_R,$$

where F_{XR} , F_{YR} , F_{ZR} consist of all external forces except those caused by gravity.

MOD9 Parameters

	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>	
<u>Input</u>	ψ_R	degree	3015	
	τ_R	degree	3014	
	F_{XR}	pound	550	
	F_{YR}	pound	551	
	F_{ZR}	pound	552	
	m_S	slug	3012	
	GRAV	feet/second ²	578	
	P	rad/sec	806	
	q	rad/sec	807	
	r	rad/sec	808	
	I_{XX}	slug-ft ²	3009	
	I_{YY}	slug-ft ²	3010	
	I_{ZZ}	slug-ft ²	3011	
	M_{LP}	feet/pound	547	
	M_{MP}	feet/pound	548	
	M_{NP}	feet/pound	549	
	<u>Output</u>	\ddot{X}_R	feet/second ²	812
		\ddot{Y}_R	feet/second ²	813
		\ddot{Z}_R	feet/second ²	814
\dot{p}		rad/sec ²	815	
\dot{q}		rad/sec ²	816	
\dot{r}		rad/sec ²	817	

C	SUBROUTINE MOD9	SIX06450
C	3/10/78	SIX06460
C		
C	EQUATIONS OF MOTION	SIX06480
C		SIX06490
C	MOD PACKAGE SIX06. A GENERAL PURPOSE 6DOF GUIDED OR	SIX06500
C	UNGUIDED TRAJECTORY PROGRAM	SIX06510
C		SIX06520
C	THE MASS,MS AND MOMENTS OF INERTIA IXX,IYY,IZZ ARE REQUIRED	SIX06530
C		SIX06540
C	NOTE" DERIVATIVES XRDD,YRDD,ZRDD,XRD,YRD,ZRD,PD,QD,RD,P,Q,R	SIX06550
C		SIX06560
C	COMMON Y(4940)	SIX06570
	EQUIVALENC(Y(547),MLP),(Y(548),MMP),(Y(549),MNP)	SIX06580
	EQUIVALENC(Y(550),FXR),(Y(551),FYR),(Y(552),FZR)	SIX06590
	EQUIVALENC(Y(812),XPDD),(Y(813),YRDD),(Y(814),ZRDD)	SIX06600
	EQUIVALENC(Y(815),PD),(Y(816),QD),(Y(817),RD)	SIX06610
	EQUIVALENC(Y(3009),IXX),(Y(3010),IYY),(Y(3011),IZZ)	SIX06620
	EQUIVALENC(Y(806),P),(Y(807),Q),(Y(808),R)	SIX06630
	EQUIVALENC(Y(3012),MS)	SIX06640
	EQUIVALENC(Y(3015),PSTR),(Y(3014),TAUP),(Y(578),GRAV)	SIX06650
	EQUIVALENC(Y(2999),T)	SIX06660
	REAL MS,MLP,MMP,MNP,IXX,IYY,IZZ	SIX06670
		SIX06680
C		
C	LINEAR EQUATIONS OF MOTION	
C		
	CALL SENCOS(PSIR,SPS,CPS,0)	SIX06690
	CALL SENCOS(TAUR,STA,CTA,0)	SIX06700
	XPDD=FXR/MS-GRAV*SPS	SIX06710
	YRDD=FYR/MS+GRAV*CPS*STA	SIX06720
	ZRDD=FZR/MS-GRAV*CTA	SIX06730
C		
C	ANGULAR EQUATIONS OF MOTION	
C		
30	PD=(Q*R*(IYY-IZZ)+MLP)/IXX	SIX06740
	QD=(P*R*(I77-IXX)+MMP)/IYY	SIX06750
	RD=(Q*P*(IXX-IYY)+MNP)/IZZ	SIX06760
40	CONTINUE	SIX06770
	RETURN	SIX06780
	END	SIX06790

APPENDIX O

MOD14; 3DOF FORCE AND EQUATIONS
OF MOTION MODULE

The purpose of this module is to calculate the forces acting on the vehicle flying along a particle (3DOF) trajectory and to set up the equations of motion.

If winds are desired, they may be input in tabular form. The wind velocity, V_w , and the heading angle, A_w (measured clockwise from the north) can be tabulated as a function of altitude, h in TABLE ARRAYS NO. 3 and 4 respectively. In that case the velocity of the vehicle with respect to the air is,

$$\begin{bmatrix} V_{A_{XL}} \\ V_{A_{YL}} \\ V_{A_{ZL}} \end{bmatrix} = \begin{bmatrix} V_{X_{LE}} \\ V_{Y_{LE}} \\ V_{Z_{LE}} \end{bmatrix} - \begin{bmatrix} -V_w \cos A_w \\ V_w \sin A_w \\ 0 \end{bmatrix}$$

or

$$V_A = \sqrt{V_{A_{XL}}^2 + V_{A_{YL}}^2 + V_{A_{ZL}}^2}$$

The atmospheric properties such as the speed of sound and density are gotten from the 1969 Standard Atmospheric Properties Tables.

The forces along the body principal axes are then expressed as

$$F_{XP} = \text{THRUST} - \left(\frac{1}{2} \rho V_A^2 \right) (A_{REF}) (C_D)$$

$$F_{YP} = 0$$

$$F_{ZP} = 0$$

C_D is the drag coefficient input in tabular form as a function of Mach number in TABLE ARRAY No. 5.

Other associated necessary quantities are the mass of the vehicle and the acceleration due to gravity. These are,

$$m_S = m_I + \dot{m}(t - t_i)$$

where

m_I = initial mass

\dot{m} = mass depletion rate

t_i = initial time

m_S = system mass

t = current time

and

$$g = \frac{g_{O R E}^2}{\left(\sqrt{X_R^2 + Y_R^2 + Z_R^2} \right)^2}$$

The equations of motion can then be written as,

$$\begin{bmatrix} \ddot{X}_R \\ \ddot{Y}_R \\ \ddot{Z}_R \end{bmatrix} = [l_{LR}][l_{PL}] \begin{bmatrix} F_{XP} \\ F_{YP} \\ F_{ZP} \end{bmatrix} + g \begin{bmatrix} \sin\psi_R \\ \cos\psi_R \sin\tau_R \\ \cos\psi_R \cos\tau_R \end{bmatrix}$$

MOD14 Parameters

<u>Input</u>	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
	H	ft	3013
	V _{X_{LE}}	fps	512
	V _{Y_{LE}}	fps	513
	V _{Z_{LE}}	fps	514
	X _R	ft	803
	Y _R	ft	804
	Z _R	ft	805
	M _I	slug	658
	\dot{m}	slug/sec	589
	t _i	sec	2863
	t	sec	2999
	THRUST	lb	590
<u>Output</u>			
	V _{A_{XL}}	fps	520
	V _{A_{YL}}	fps	521
	V _{A_{ZL}}	fps	522
	V _A	fps	575
	M	fps	577
	C _D	fps	529
	F _{XP}	lb	601
	F _{YP}	lb	602
	F _{ZP}	lb	603
	F _{XR}	lb	550
	F _{YR}	lb	551
	F _{ZR}	lb	552
	X _{..R}	ft/sec ²	812
	Y _{..R}	ft/sec ²	813
	Z _{..R}	ft/sec ²	814


```

SUBROUTINE MOD14
C
C   FORCE MODULE FOR A 3DOF PARTICAL TRAJ.
C
C   3/10/78
C
C   TABLES,  KTAR(3)=VW(H) , WIND SPEED (FPS)          TR301360
C              KTAR(4)=AW(H) , WIND AZIMUTH (DEG)       TR301370
C              KTAR(5)=CD(M) , DRAG COEFF.
C              KTAR(23)=THRUST(T) (LB)
C
C   INPUT PARAMETERS
C
C   MT=Y(658) , INITIAL MASS (SLUG)
C   MDOT=Y(589), RATE OF CHANGE OF MASS (SLUGS/SEC)
C   TT=Y(2862) . INITIAL TIME (SEC)
C   THRUST=Y(590) , CONSTANT THRUST (LB)
C   A=Y(3005) , RFF. AREA (FT**2)
C
C   COMMON Y(4940)
C   EQUIVALENCF (Y(3013),H) , (Y(2999),T)
C   EQUIVALENCF (Y(512),VXLF) , (Y(513),VYLF) , (Y(514),VZLF)
C   EQUIVALENCF (Y(2057),LPL(1)) , (Y(2039),LLR(1))
C   EQUIVALENCF (Y(803),XR) , (Y(804),YR) , (Y(805),ZR)
C   EQUIVALENCF (Y(578),GRAV) , (Y(577),VMACH)          TR301450
C   EQUIVALENCF (Y(812),XRDD) , (Y(813),YRDD) , (Y(814),ZRDD) TR301480
C   EQUIVALENCF (Y(3012),MS)                             TR301520
C   EQUIVALENCF (Y(550),FXR) , (Y(551),FYR) , (Y(552),FZR) TR301530
C   EQUIVALENCF (Y(3005),A) , (Y(3000),RE)
C   EQUIVALENCF (Y(349),PSIR) , (Y(348),TAUR)
C   EQUIVALENCF (Y(575),VA) , (Y(576),QP) , (Y(520),VAXL) TR301580
C   EQUIVALENCF (Y(521),VAYL) , (Y(522),VAZL)           TR301590
C   EQUIVALENCF (Y(601),FXP) , (Y(602),FYP) , (Y(603),FZP) TR301620
C   EQUIVALENCF (Y(589),MDOT) , (Y(590),THRUST)         TR301630
C   EQUIVALENCF (Y(529),CD)                             TR301640
C   EQUIVALENCF (Y(658),MI) , (Y(2862),TI)              TR301670
C   DIMENSION II(2)
C   RFAL LLR(9),LPL(9),MS,MI,MDOT
C
C   RAD=3.141592653589/180.                              TR301820
C
C   WINDS
C
C   CALL JTAB(3.1,H,VW)
C   CALL ITAB(4.1,H,AW)
C   AW=AW*RAD
C   60 VWXLE=-VW*COS(AW) TR301830
C   VWYLE=VW*STN(AW) TR301840
C   VWZLE=0.0 TR301850
C   TR301860
C
C   VELOCITY W/R TO AIR
C
C   70 VAXL=VXLE-VWXLE TR301870
C   VAYL=VYLE-VWYLE TR301880
C   VAZL=VZLE-VWZLE TR301890
C   VA=SQRT(Y(520)**2+Y(521)**2+Y(522)**2) TR301900
C
C   ENVIRONMENTAL PROPERTIES
C
C   IF(H.GE.500000.) GO TO 115 TR301910
C   110 CALL ARDCFT(H,PP,TT,DD,VS,G) TR301920

```

	VMACH=VA/(VS*1116.4)	TR301930
	RHO=DN*0.0023769	
	QP=0.5*RHO*VA**2	TR301970
	GO TO 118	TR301980
115	VMACH=0.0	TR301990
	RHO=0.0	TR302000
	QP=0.0	TR302010
118	GRAV=(32.174*RE**2)/((SQRT(XR**2+YR**2+ZR**2))**2)	TR302020
C		TR302030
C	MASS	
C	MS=MI+MDOT*(T-TI)	TR302080
C		
C	FORCES	
C		
	U(1)=VMACH	TR302090
	CALL ITAB(5,1,U,CD)	
	FYP=THRUST-QP*A*CD	TR302130
	FYP=0.0	TR302140
	FZP=0.0	TR302150
	CALL MATVEC(LPL,Y(601),Y(550),0)	TR302270
	CALL MATVEC(LLR,Y(550),Y(550),0)	TR302280
C		
C	EQUATIONS OF MOTION	
C		
	XRDD=FXR/MS-GRAV* (SIN(PSIR))	TR302290
	YRDD=FYR/MS+GRAV* (COS(PSIR)*SIN(TAUR))	TR302300
	ZRDD=FZR/MS-GRAV* (COS(PSIR)*COS(TAUR))	TR302310
	RETURN	
	END	

APPENDIX P
PROCESS, 3DOF AND 6DOF

PROCESS PARAMETERS

<u>Input</u>	<u>Parameter</u>	<u>Units</u>	<u>Location in Y Array</u>
	RE	FT	3000
	WE	rad/sec	3001
	TAUR	deg.	3014
	PSIR	deg.	3015
	TI	sec.	2862
	T	sec.	2999
	VXLE	fps	512
	VYLE	fps	513
	VZLE	fps	514

Output

	GX	g's	2205
	GY	g's	2206
	GZ	g's	2207
	GAMAH	deg.	2208
	GAMAE	deg.	2209

C	SUBROUTINE PROCESS	SIX06820
C	3/13/78	SIX06830
C	MOD PACKAGE SIXDG. A GENERAL PURPOSE 6DOF GUIDED OR	SIX06850
C	UNGUIDED TRAJECTORY PROGRAM	SIX06860
C		SIX06870
C		SIX06880
	COMMON Y(4940)	SIX06890
	EQUIVALENCF (Y(2863),STOP), (Y(3012),MS), (Y(658),MI)	SIX06900
	EQUIVALENCF (Y(2213),OT), (Y(2214),OP), (Y(2215),RS)	SIX06910
	EQUIVALENCF (Y(3000),RE), (Y(2862),TI), (Y(3001),WE)	SIX06920
	EQUIVALENCF (Y(504),OLAL), (Y(505),OLR), (Y(506),OTIM), (Y(2999),T)	
	EQUIVALENCF (Y(3014),TAUR), (Y(3015),PSIR)	SIX06940
	EQUIVALENCF (Y(818),RTEI), (Y(819),RPET)	SIX06950
	EQUIVALENCF (Y(803),XRM), (Y(804),YRM), (Y(805),ZRM)	SIX06960
	EQUIVALENCF (Y(2200),RTE), (Y(2201),RPE)	SIX06970
	EQUIVALENCF (Y(2205),GX), (Y(2206),GY), (Y(2207),GZ)	SIX06980
	EQUIVALENCF (Y(512),VXLF), (Y(513),VYLE), (Y(514),VZLF)	SIX06990
	EQUIVALENCF (Y(2204),GAMAH), (Y(2209),GAMAE)	SIX07000
	EQUIVALENCF (Y(2204),GT)	
	EQUIVALENCF (Y(651),CXA), (Y(652),CYA), (Y(653),CZA)	
	EQUIVALENCF (Y(526),VXG), (Y(527),VYG), (Y(528),VZG)	
	EQUIVALENCF (Y(648),CXG), (Y(649),CYG), (Y(650),CZG)	
	EQUIVALENCF (Y(660),LGA(1)), (Y(3005),A), (Y(578),GRAV)	
	EQUIVALENCF (Y(3012),MS), (Y(654),BALC)	
	REAL MI,MS,LGA(9)	
C		SIX07020
C	EQUATORIAL RANGES	SIX07030
C		
	RAD=3.141592653589/180.	SIX07040
	RTE=(RE*(TAUR*RAD-WE*(T-TI)))	SIX07050
	RPE=(RE*PSIR*RAD)	SIX07060
C		SIX07070
C	BODY ACCELFRATIONS IN THE PRINCIPAL AXES. (G,S)	SIX07080
C		
	CALL MATVEC(Y(2009),Y(812),Y(2202),0)	SIX07090
	GX=Y(2202)/32.174	SIX07100
	GY=Y(2203)/32.174	SIX07110
	GZ=Y(2204)/32.174	SIX07120
	GT=SQRT(GY**2+GZ**2)	
C		SIX07130
C	LOCAL FLIGHT PATH ANGLES. (DEG)	SIX07140
C		
	CALL ARKTAN(-VYLE,VXLF,GAMAH,0)	SIX07150
	ZZZ=SQRT(VXLF**2+VYLE**2)	SIX07160
	CALL ARKTAN(VZLE,ZZZ,GAMAE,0)	SIX07170
C		SIX07180
C	TRUE DISTANCE TRAVELED W/R TO THE EARTHS SURFACE	SIX07190
C		
	TAUR=TAUR*RAD	SIX07200
	PSIR=PSIR*RAD	SIX07210
	TAUE=TAUR-WE*T	SIX07220
	DX2=(RE*SIN(OP)-RE*SIN(PSIR))**2	SIX07230
	DY2=(-RE*COS(OP)*SIN(OT)+RE*COS(PSIR)*SIN(TAUE))**2	SIX07240
	DZ2=(RE*COS(OP)*COS(OT)-RE*COS(PSIR)*COS(TAUE))**2	SIX07250
	DC=SQRT(DX2+DY2+DZ2)	SIX07260
	THETA=2.0*ASIN(DC/(2.0*RE))	SIX07270
	DRS=RF*THETA	SIX07280
	RS=RS+DRS	SIX07290
C		
	OT=TAUE	SIX07300
	OP=PSIR	SIX07310

TAUR=TAUR/RAD
PSIR=PSIR/RAD
IF (STOP) 20,20,10
10 TI=T
MI=MS
20 CONTINUE
RETURN
END

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