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Infrared Optical Properties of Bipropellant Cryocontaminants

J. A. Roux, B. E. Wood, and A. M. Smith ARO, Inc.

August 1979

Interim Report for Period October 1, 1977 - March 15, 1979

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a nonlinear least-squares method. The analytical model treats the germanium as a thick, noninterfering film and the deposit as a thin film. Results from the least-squares method are also compared with a Kramers-Kronig determination of the real part of the index of refraction. The optical properties (n,k) of such cryofilms are essential for predicting the degradation of cryocooled optical surfaces contaminated by liquid propellant exhaust plumes.

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PREFACE

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The research reported herein was performed by the Arnold Engineering Development Center (AEDC), Air Force Systems Command (AFSC). Work and analysis for this research was done by personnel of ARO, Inc. (a Sverdrup Corporation Company), operating contractor of AEDC, AFSC, Arnold Air Force Station, Tennessee. The work covered the period from October 1, 1977 to March 15, 1979 and was done under ARO Project Numbers V32S-R1A, V32K-13A, and P32K-13A. Dr. H. E. Scott was the Air Force project manager. The manuscript was submitted for publication on May 21, 1979.

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1.0 INTRODUCTION

Contamination from the exhaust plume of small thrusters used for attitude control maneuvers can pose severe problems for long-life satellite systems. Engine exhaust products can contaminate sensitive optical surfaces located upstream of the nozzle exit plane (referred to as the backflow region). Sensor systems, which require cryogenic cooling to achieve maximum sensitivity, are particularly susceptible to cryopumping engine exhaust products that reach the backflow region. The contaminants reaching the backflow region are thought to originate from the engine nozzle boundary layer. Gases in the boundary layer travel at low velocities and are therefore able to expand through very large angles and flow upstream of the nozzle exit plane.

To identify better the possible contaminants from bipropellant (MMH/N₂O₄) and monopropellant (N₂H₄) engines, the infrared (IR) spectra of monomethyl hydrazine (MMH), nitrogen tetroxide (N₂O₄), and hydrazine (N₂H₄) propellants were measured. The normal transmission spectra were measured using 20 and 77°K germanium as a substrate material. Germanium was chosen as a substrate because it has an absorption edge at 1.5 μ m, a flat transmission of 47 percent between 2 and 10 μ m, and lattice absorption bands between 10 and 20 μ m. It is one of the most commonly employed substrates for cryocooled optical components because of its higher thermal conductivity as compared to pure dielectrics, the Irtrans[®], or polycrystals, for example.

Complete experimental details have been given in Ref. 1; thus only a basic outline of the chamber and apparatus is presented here. The absolute transmission of thin solid films of MMH, N₂O₄, and N₂H₄, ranging in thickness up to 9 μ m, is presented. Finally, a theoretical model of window plus film transmission is derived and is subsequently employed with the experimental results to determine the complex refractive index ($\bar{n} = n - ik$) of each of the above-mentioned propellants. The subtractive Kramers-Kronig treatment for calculation of the film refractive index has also been employed, and results are compared to those of the least-squares determination.

2.0 INSTRUMENTATION

A schematic drawing of the experimental apparatus, showing the IR interferometer (Digilab Model FTS-14), the high-vacuum chamber containing the cryocooled window, and the IR source location is given in Fig. 1. The chamber is an all-stainless-steel cell equipped with a liquid-nitrogen (LN₂)-cooled liner. A water-vapor-free vacuum of 10^{-8} torr can be routinely obtained. The substrate holder can be actively cooled with either liquid nitrogen (LN₂) (77°K) or gaseous helium (GHe) (20°K). Three platinum resistors located on the window holder gave temperature readouts accurate to 0.5° K.

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The germanium window was mounted for cryogenic cooling as shown in Fig. 2. To ensure that the germanium window did not act as an optical stop in any manner, a stop was located in the "back-of-window" gas baffle. This stop was 1.50 in. in diameter, and the clear aperture of the germanium was 2.0 in. in diameter.

The spectral resolution of the interferometer system could be selected between 16 and 0.5 cm⁻¹, but 4-cm⁻¹ resolution was found to be sufficient for all work reported herein. The wavelength accuracy of the interferometer is near 0.02 cm⁻¹, since the interferogram sampling interval is governed by an auxiliary helium-neon (He-Ne) laser interferometer. Transmission data were recorded in the 500 to 3700-cm⁻¹ wavenumber region. Transmission measurements were performed by rotating the germanium out of the beam and recording a reference power spectrum. Up to 16 interferograms were generally co-added before execution of the Fourier transform, improving the signal-to-noise ratio. Next the window was rotated into the beam and the process repeated. The reference file was then divided into the sample file and plotted by a digital incremental plotter, producing the final data record on a linear ordinate scale of 0- to 100-percent transmission.

Controlled contamination of the cryocooled germanium window was accomplished with the gas induction system shown schematically in Fig. 3. A toroidal-shaped header with thirty-six 1/16-in.-diam orifices spaced 10 deg apart directed the gas toward the germanium window. The upstream pressure was determined from the vapor pressure of the liquid, and the gas flow rate was regulated by the variable leak valve. The chamber pressure would rise from 1 x 10⁻⁸ up to 4 x 10⁻⁸ or from 1 x 10⁻⁷ up to 1 x 10⁻⁶ torr during deposition at 20 and 77°K, respectively, indicating good cryopumping by the liner and substrate. Gas was prevented from condensing on the back of the germanium window by a gas baffle positioned close to the back-of-window holder. This baffle also held the optical stop mentioned earlier. The gas induction system, although quite simple, worked well in that the deposition rate could be easily controlled and the final thin-film thickness was very uniform across the 2-in.-diam exposed window area. Film uniformity and absolute thickness are two important parameters since the ultimate objective of the experiment was to determine the complex refractive index of the thin film, a quantity derived by comparison of experimental transmission versus thickness data with a theoretical model. Any error in absolute film thickness is directly introduced into the film complex refractive index results. A dual-laser-beam technique (Ref. 2) was employed to measure the film thickness and also the film refractive index at 0.6328 μ m. Basically, two He-Ne laser beams are specularly reflected off the germanium window for two different and accurately measured incidence angles. As the gas is condensed two interference patterns of different periods are monitored in the reflected laser light. If the ratio of interference pattern periods is termed β then the refractive index of the film (n) is given by

$$\mathbf{n} = \frac{\left[\sin^2 \theta_{\mathbf{h}} - \beta^2 - \sin^2 \theta_{\mathbf{a}} \right]^{\frac{1}{2}}}{\left[1 - \beta^2 \right]^{\frac{1}{2}}}$$

where θ_a and θ_b (typically 18 and 68 deg) are the two laser-beam incidence angles. Once m_a has been established the thickness, d_1 , of the film is readily calculated from $m_a\lambda = 2nd_1$ [1- $(\sin^2\theta_a/n^2)$]^{1/2}, where m is the order of the interference maxima for incidence angle θ_a . The dual-laser-beam thickness monitor yielded thin-film refractive index values accurate to within two percent. A quartz cyrstal microbalance (QCM) was used in conjunction with the dual-laser-beam technique to determine the density of each contaminant. The QCM operates on the principle of the crystal vibration frequency changing linearly with a change in mass deposited on the crystal. The QCM was located adjacent to and just above the germanium window (see Fig. 2) so that the mass deposition rate would be the same as on the film thickness determined from the interference patterns. From these two values the film density was calculated.

3.0 PROCEDURE

The chamber was initially pumped down to approximately 1 x 10^{-7} torr using the diffusion pump and the LN₂ liners. Chamber pressures in the low 10^{-8} -torr range were obtained when the germanium window, holder, and transfer lines were cooled to approximately 20°K with the Collins cryostat (2-kw capacity).

Samples of MMH, N_2O_4 , and N_2H_4 liquid were obtained from the fuel drums. A laboratory chemical analysis was done on each sample to determine the purity level. The remainder of the sample was transferred to an evacuated cylinder that was then attached to the chamber gas bleed-in system. Absorbed gases and sample impurities were removed from the cylinder and sample using a mechanical pump to pump directly on the sample. The vapor pressure exerted by the sample of propellant supplied the forepressure for the metering valve that was adjusted to give the desired deposition rate.

Deposition of the gas on the cold germanium window was monitored using the two HeNe laser beams with the two-angle interference technique. Generally, transmission measurements were made upon reaching an interference maxima in the lower angle (18-deg) beam, at which point the gas flow was shut off. Upon completion of the transmission measurements, the gas flow was again started and deposition occurred until a film thickness corresponding to the next interference maxima was reached, etc. In some instances in which very strong absorption bands were observed, transmission measurements were alternately made for each interference minima and maxima. This was done since determination of the optical properties (n and k) required the use of as many thicknesses as possible to increase accuracy.

After completion of a series of transmission measurements for all the thicknesses, the cryogenic flow rate to the germanium substrate was turned off and the substrate and deposited film allowed to warm up. Transmission measurements were made at intervals during warmup. The time required for the interferometer to scan the sample (16 scans) was 2 to 3 minutes with a similar time required for the reference beam. With the time required for obtaining the Fourier transform and the plotting of the data, this resulted in a time interval of about 10 minutes between measurements. The temperature given on each warmup data plot is the temperature at the end of the sample interferometer scan.

The main intent was to obtain transmission measurements for as many thicknesses as possible during an experiment on each propellant. The number of thicknesses actually obtained depended considerably on the particular gas. For "well-bchaved" deposits, 16 to 25 thicknesses (interference maxima or minima) were obtained, whereas in some cases only 2 to 3 thicknesses were possible. The so-called fracture or shattering effect was the primary cause of the problem. In other cases the deposit was more highly scattered, which caused the interference patterns to be washed out at thinner film thickness.

4.0 RESULTS - EXPERIMENTAL

4.1 MMH ON 20°K GERMANIUM

Transmission spectra of MMH were obtained for several thicknesses varying from 0.233 μ m (one interference fringe) to 3.27 μ m (14 interference fringes). At the He-Ne wavelength (0.6328 μ m) the refractive index was measured and found to be 1.40 \pm 0.02; in conjunction with the thickness measurement, a QCM measured the mass per unit area giving a density of 0.82 gm/cm³ for the MMH deposit at 20°K. This yields a Lorentz-Lorenz value {[(n² - 1)/(n² + 2)] 1 • 1/g} of 0.294 cm³/gm at 0.6328 μ m.

Transmission data obtained for the 0.47-, 1.17-, and 3.27- μ m-thick deposits are shown in Fig. 4. These thicknesses correspond to interference maxima of 2, 5, and 14, respectively. (The dashed curve is for the bare 20°K germanium transmission.) The absorption bands are listed in Table 1 (the 77°K data are also listed and will be discussed later), and the vibrational assignments of Durig, Harris, and Wertz (Ref. 3) are listed for comparison; their assignments were obtained for liquid MMH, whereas the spectra in the present case were for thin solid films of MMH. The MMH spectra show two wavenumber areas of considerable absorption — the region from 800 to 1700 cm⁻¹ and the region from 2700 to 3400 cm⁻¹. No noticeable absorption is noted between these two regions. The broad dip in transmission centered between 1900 and 2300 cm⁻¹ (Fig. 4c) is actually an interference minimum and is a part of the channel spectra. As shown in Fig. 4c, some of the transmission curve lies at

values higher than the initial germanium base surface transmission. This is the result of the thin MMH film acting as an antireflection coating that increases the transmission over that of the bare germanium.

Comparing the spectral locations of the absorption bands listed in Table 1 with those from Durig et al. (Ref. 3) reveals a few differences. In Fig. 4c a relatively strong band can be observed at 3164 cm⁻¹, whereas no such band was observed by Durig et al.; this may be due to the bands being sharper in the solid phase. Similarly, a weak band at 3032 cm⁻¹ was not observed by Durig et al., nor was the splitting of the ν_4 and ν_5 bands located at 2964 and 2934 cm⁻¹, respectively. The other band locations were nearer to the values obtained for the liquid phase.

After the data in Fig. 4 were obtained, the 20°K GHc flow to the germanium substrate was stopped and the MMH-germanium surface system was allowed to warm up slowly. Spectral transmission measurements were made at intermediate temperatures before the MMH film sublimated. Essentially no change occurred in the transmission for temperatures up to 145°K. Between 145 and 160°K a phase change occurred in the MMH, as is evident from a comparison of Figs. 4c and 5. The overall transmission was reduced considerably. The phase change from an amorphous solid to a crystalline structure caused a large increase in the scattered radiation (Fig. 5), thereby reducing the transmission of radiation through the MMH-germanium composite. Visually at this time the MMH film appeared translucent or milky. The absorption bands also are much less prominent than previously recorded, with some of the weaker bands being undetectable. The ν_{18} band located at 836 cm⁻¹ before the phase change split into two bands located at 845 and 860 cm⁻¹. The relatively broad band located at 1004 cm⁻¹ before the phase change is very sharp and shifted to 985 cm⁻¹ afterward, which makes it agree with the location of the ν_{16} band of Durig et al. (Ref. 3). Considerable variations were seen in the shape and location of the other bands. The two doublet bands near 1104 and 1206 cm⁻¹ before the phase change appeared as a single band after the phase change. The bands in the 2700 to 3400-cm⁻¹ range showed little resemblance to those before the phase change, as shown in Figs. 4 and 5, and thus a comparison of band locations before and after warmup is difficult. In general, the shape of the bands was much sharper after the warmup. This was especially true in the 700 to 1700-cm⁻¹ region. After the phase change, the temperature of the germanium substrate was allowed to increase further until the MMH had completely evaporated, which occurred between 175 and 180°K. The chamber pressure at this time was approximately 5 x 10⁻⁶ torr.

4.2 MMH ON 77°K GERMANIUM

Thin films of MMH were also deposited on LN_2 -cooled germanium, and transmission spectra were obtained as before at each interference maxima. The refractive index at 77°K

and $\lambda = 0.6328 \,\mu\text{m}$ was 1.47 ± 0.02 , the density was 0.98 gm/cm³, and the Lorentz-Lorenz constant 0.284 cm³/gm. For the transmission measurements, film thicknesses up to 40 interference maxima thick (8.84 μ m) were deposited and the spectra recorded. Figure 6 shows the spectra obtained for thicknesses of 0.44, 2.21, and 8.84 μ m, which are representative of the results obtained. The band locations and assignments (see Table 1) are essentially the same as given previously for the 20°K spectra. Essentially all of the bands observed at 77°K are within 10 cm⁻¹ of the corresponding bands observed at 20°K.

For the films formed at 77°K no problems with fracturing occurred. Figure 7 shows the spectra obtained after the film was allowed to warm up to 161°K. A crystalline phase change occurred between 150 and 160°K as previously noted, but the transmission values (see Fig. 7) are considerably higher than that observed in the previous warmup data for the 20°K case (see Fig. 5). This is evidently caused by smaller size particles or crystals being formed when no fracture occurs before the amorphous-crystalline phase change. The fracture evidently increases the particle size, which, in turn, reduces the transmission by increasing the amount of energy scattered out of the radiation path.

There was not much change in the spectra before and after warmup. However, one significant change was the emergence of a strong, sharp absorption band at 3340 cm⁻¹ not present before warmup. Evidence of its presence is found in the 20°K warmup curve (Fig. 5) as a weak band observed at approximately 3340 cm⁻¹. This band appeared prominently during the 77°K warmup in Fig. 7 and is either the ν_1 or ν_2 fundamental. The splitting of the ν_{18} band at approximately 840 cm⁻¹ into bands located at 835 and 860 cm⁻¹ (see Fig. 7) was also observed in the 20°K warmup curve and is the result of the amorphous deposit transforming to the crystalline phase since the splitting of the band was not observed for liquid MMH (Ref. 3). All other band locations were very close for the 20 and 77°K condensed films. Several weak bands appear in the 1700 to 2660-cm⁻¹ range after warmup (see Fig. 7); these were not observed in either the 20 or 77°K data before warmup. These weak bands are combinations or lattice bands whose assignments are unknown at present.

4.3 N₂O₄ ON 20°K GERMANIUM

Shown in Fig. 8 is the IR transmission spectrum of a 1.45- μ m-thick (6 interference maxima) N₂O₄ film deposited on the 20°K germanium window. In contrast to the MMH, the N₂O₄ exhibits strong absorption only at the lower wavenumbers (700 to 2300 cm⁻¹). The refractive index at 0.6328 μ m and the density were measured and found to be 1.53 ± 0.02 and 1.81 gm/cm³, respectively, at 20°K. This yields a Lorentz-Lorenz value of 0.171 cm³/gm. During deposition the N₂O₄ films fractured or changed phase abruptly when a film thickness of 1 to 3 μ m was reached. This behavior was characterized by a sudden change (within five seconds) from a clear transparent film to a highly diffuse scattering film, with

the result that the thin-film laser interference patterns could no longer be observed. Infrared channel spectra were washed out at this time also.

The identifiable N₂O₄ bands are listed in Table 2. These data were compared with 77°K N₂O₄ measurements of Wiener and Nixon (Ref. 4) and the N₂O₄ gas phase measurements of Bibart and Ewing (Ref. 5); band assignments follow those of Wiener and Nixon (Ref. 4) unless indicated otherwise. The major vibration bands are the ν_{12} band located at 750 cm⁻¹, the ν_{11} band at 1260 cm⁻¹, the ν_{5} band at 1720 cm⁻¹, and the ν_{9} band located at 1742 cm⁻¹. The remaining N₂O₄ bands are either weaker fundamentals or combination bands.

To help identify the bands listed in Table 2 it was necessary to consider the transmission of the N₂O₄ film after the substrate had been allowed to warm up from 20 to 153°K (see Fig. 9). Transmission measurements were made at intermediate temperatures, but they are not presented. Upon warmup to 153°K the v_{12} band located at 750 cm⁻¹ in Fig. 8 splits into two bands located at 745 and 765 cm⁻¹ in Fig. 9. The splitting had not occurred at 138°K. When N₂O₄ is deposited at 77°K, this band exists as a doublet (Ref. 6) as observed in AEDC data taken at 77°K (shown later) and also found by Wiener and Nixon (Ref. 4). The three weak bands observed in Fig. 8 at 785, 820, and 850 cm⁻¹ became much sharper after warmup (Fig. 9) and are more easily distinguished. There was a broad absorption band between 940 and 1060 cm⁻¹ before warmup. After warmup to 153°K only a narrow band still remains at 1050 cm⁻¹; this band finally disappeared between 200 and 207°K. The sharp band located at 1050 cm⁻¹ is attributed to some form of nitrate (Ref. 7) (NO₃) that remained on the surface after most of the other film had sublimed.

The broad band initially between 940 and 1060 cm⁻¹ is assigned (Ref. 8) to N₂O₃ since a large part of the band disappeared at an intermediate temperature of 80 to 90°K (not shown) at a chamber pressure of 10^{-6} torr. No vapor pressure curves are available for N₂O₃, but it is known that N₂O₃ vapor pressure is higher than that for N₂O₄. Other gases that sublimate in this temperature region are NO at 60 to 70°K and N₂O at 80 to 90°K; however, neither of these gases exhibits absorption in the 940 to 1060-cm⁻¹ region. (N₂O₄ and NO₂ sublimate at approximately 160°K for a chamber pressure of 10^{-6} torr.)

The two strong, sharp bands in Fig. 8 located at 1260 and 1305 cm⁻¹ are the ν_{11} and $\nu_{11} + R N_2O_4$ bands, where R represents a torsional lattice mode. (The $\nu_{11} + R$ band was not observed for N₂O₄ deposited at 77°K in the AEDC studies.) Both of these bands are still present after warmup to 153°K (Fig. 9). The $\nu_{11} + R$ band of N₂O₄ at 1305 cm⁻¹ (20°K) is also masking a nitrate band. Hence, the 1305-cm⁻¹ band in Table 2 is listed as an N₂O₄ and ν_3 nitrate band.

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The band at 1450 cm⁻¹ in Fig. 8 before warmup shifts to 1385 cm⁻¹ after warmup (Fig. 9). This is the N₂O₄-2 ν_7 band and is evidently highly temperature-dependent. In Fig. 8 a sharp band is located at 1618 cm⁻¹ with a side lobe at 1595 cm⁻¹. In the warmup data between 20 and 90°K these bands became quite distinct, and the 1618-cm⁻¹ band disappeared upon warmup to 90°K. For this reason the 1618-cm⁻¹ band was identified as the ν_2 band (Ref. 8) of N₂O₃. The band at 1595 cm⁻¹ was identified as the NO₂- ν_3 band.

In the region of 1700 cm⁻¹ (Fig. 8) there are three distinct bands located at 1720, 1742, and 1765 cm⁻¹ assigned to be the ν_5 , ν_9 , and $\nu_9 + R N_2O_4$ bands, respectively (Ref. 4). Upon warmup to 153°K the band at 1720 cm⁻¹ has disappeared, as shown in Fig. 9. The 1880-cm⁻¹ band is the N₂O₄ $\nu_4 + \nu_5$ combination band and shifted to 1860 cm⁻¹ upon warmup to 153°K.

The 1980-cm⁻¹ broad band in Fig. 8 disappeared upon warmup to about 90°K and does not appear in Fig. 9. Since it disappears at the same temperature as the 940-to-1060 and the 1618-cm⁻¹ bands, it also is assigned to N_2O_3 even though this band is located some 50 cm⁻¹ from that observed for gaseous N_2O_3 by Bibart and Ewing (Ref. 8).

The band labeled 2135 cm⁻¹ in Fig. 8 was strongly temperature-dependent, shifting some 85 cm⁻¹ to its location of 2220 cm⁻¹ in Fig. 9 at 153°K. Further temperature increases to 180°K caused the band to further shift to 2260 cm⁻¹. At this temperature the N₂O₄ and NO₂ had already sublimated, leaving only a deep blue film on the substrate. This band is most likely a nitrate combination band, possibly $\nu_2 + \nu_3$, which could result from the ν_2 and ν_3 bands recorded by Kato and Rolfe (Ref. 7). Further indications that the film remaining at this temperature was a nitrate were the relatively strong absorption bands at approximately 1340 cm⁻¹ and a weaker one at 1050 cm⁻¹, corresponding to NO₃ fundamentals ν_3 and ν_1 , respectively (Refs. 7, 9, 10, and 11). The film had completely sublimated upon reaching a temperature of 207°K.

Two sharp bands located at 2235 and 2345 cm⁻¹ were also found. These two bands were eliminated when the warmup temperature reached 90°K (not shown). The 2235-cm⁻¹ band is attributed to the strongest N₂O fundamental ν_3 ; the 2345-cm⁻¹ band is assigned to be the strongest CO₂ fundamental ν_3 . Only trace amounts of N₂O and CO₂ are required for these bands to show up. Other weak bands marked in Fig. 8 between 2900 and 3200 cm⁻¹ are attributed to N₂O₄ and are the $\nu_5 + \nu_{11}$ band at 2970 cm⁻¹, the $2\nu_7 + \nu_9$ band at 3115 cm⁻¹, and the $2\nu_7 + \nu_9 + R$ band at 3155 cm⁻¹. These bands appear very weak in Figs. 8 and 9, but they are more prominent when N₂O₄ is deposited on a 77°K surface.

Finally, it should be mentioned that the ν_7 fundamental band, which is located at 685 cm⁻¹ in the gas phase, was not observed in the solid films studied here. This band is considerably weaker in the solid phase (Ref. 4).

4.4 N₂O₄ ON 77°K GERMANIUM

Thin films of N₂O₄ were also condensed at 77°K. For $\lambda = 0.6328 \,\mu\text{m}$ the refractive index was determined to be 1.55 ± 0.02 and the density was 2.01 gm/cm³. These values yield a Lorentz-Lorenz value of 0.159 cm³/gm, which shows only fair agreement with the value of 0.171 cm³/gm obtained for the 20°K measurements. No fracture problems were encountered for the N₂O₄ deposited at this higher temperature. During warmup the N₂O₄ started evaporating at approximately 150°K and a chamber pressure of about 1 x 10⁻⁶ torr.

The infrared transmission spectra for the thin films condensed at 77°K are shown in Fig. 10 for thickness of 0.42, 1.25, and 4.18 μ m. For the smallest thickness, 0.42 μ m, only the bands at 1740 and 1760 cm⁻¹ are very intense. The bands at 1255 cm⁻¹ and the double band at 740 and 760 cm⁻¹ show up strongly at the two larger thicknesses. The latter band existed as a single band located at 750 cm⁻¹ when deposited at 20°K, but the splitting was observed later when the films were warmed up. The 1255-cm⁻¹- ν_{11} band showed up as a singlet until a warmup temperature of between 147 and 155°K (see Fig. 11a) was reached, at which point the 1305-cm⁻¹ (ν_{11} + R) band also became quite strong. This latter band was observed at 20°K before warmup, which is in contrast to the trend observed previously. The general trend is for a film condensed at the lower temperature to be of the amorphous form and to exhibit less spectral structure than the crystalline deposits formed at a higher temperature.

From the spectra for the 4.18- μ m-thick film (Fig. 11a), a weak band is observed at 1460 cm⁻¹ ($2\nu_7 + R$) and a sharp band at 1620 cm⁻¹. A very sharp narrow band is observed at 1700 cm⁻¹ (ν_5) and the strong double band 'located at 1740 (ν_9) and 1760 cm⁻¹ ($\nu_9 + R$). The remainder of the bands are relatively weak and are located at 1840, 2240, 2340, 2580, 2620, 2965 ($\nu_5 + \nu_{11}$), 2985, 3100 ($2\nu_7 + \nu_9$), and 3140 ($\nu_7 + \nu_9 + R$) cm⁻¹. The 2340-cm⁻¹ band is believed to be the ν_3 CO₂ band, and the 2240-cm⁻¹ band is due to N₂O impurities that are absorbed in the liquid N₂O₄. Some of the weak bands, such as the 2580- and 2620-cm⁻¹ bands observed at 77°K and not observed at 20°K, may be due to the much larger film thickness deposited at 77°K.

No significant differences in the warmup spectra were observed from those in the warmup spectra of the films formed at 20°K other than the previously mentioned band at 1305 cm⁻¹. After warmup to 155°K (Fig. 11a) some of the N₂O₄ was already sublimating. Figures 11b and c are spectra obtained after the N₂O₄ had come off but a very thin film remained on the substrate. At 174°K (Fig. 11b) a double band was observed in the region from 1300 to 1400 cm⁻¹ and a weaker band at 2220 cm⁻¹. Further warmup to 183°K (Fig. 11c) completely eliminated the 2220-cm⁻¹ band, but a single band at approximately 1370 cm⁻¹ remained. At this temperature a brilliant, dark blue film was observed on the germanium window and holder. This film had sublimated when the germanium temperature reached 197

to 207°K for a chamber pressure of 1 x 10⁻⁷ torr. This film is probably some type of nitrate impurity in the N_2O_4 .

4.5 N₂H₄ ON 77°K GERMANIUM

The other fuel studied was hydrazine (anhydrous). A sample was collected from a fuel drum of N_2H_4 , and a chemical analysis showed the composition (by weight) to be 99.2-percent N_2H_4 , 0.6-percent H_2O , and 0.2-percent amines.

Deposition was first attempted for the germanium window cryogenically cooled to 20°K. However, only a few (2 to 6) interference maxima were obtained before dying out because of a fracture-type phenomenon. This phenomenon sometimes occurred as a sudden fracture with the immediate cessation of the interference pattern or was a rapid deterioration of the interference pattern quality. The spectra of these deposits before fracturing, however, were not unlike those obtained for the 77°K measurements; therefore, they are not presented here. With the germanium window at 77°K, hydrazine films up to 32 interference maxima thick were obtained before fracture occurred. The refractive index at 0.6328 μ m was found to be 1.50 ± 0.02 and the density 1.17 gm/cm₃ at 77°K. These values yield a Lorentz-Lorenz constant of 0.253 cm³/gm at this wavelength. At a chamber pressure of 3 x 10⁻⁶ torr, the hydrazine films evaporated between 180 and 190°K.

The transmission spectra of hydrazine formed at 77°K germanium for thicknesses of 0.22, 2.16, and 4.74 μ m are shown in Figs. 12a through c. Locations of the major absorption bands are at 890, 1060, 1305, 1345, 1620, 2955, 3180, and 3340 cm⁻¹ and are listed in Table 3. Some of these bands agree with previously published data (Refs. 12 through 14) obtained on solid hydrazine, such as the 3340-, 3180-, and the 890-cm⁻¹ bands. The relatively weak band at 2955 cm⁻¹ shown in Fig. 12c was also observed in Ref. 12, but was not identified.

The two relatively weak bands at 1305 and 1345 cm⁻¹ were observed in Ref. 12, but the relative intensities were reversed. In Fig. 12c the band located at 1305 cm⁻¹ is stronger than that at 1356 cm⁻¹, whereas the relative intensities of the two bands were reversed in the data of Ref. 12. The two simple bands observed in Fig. 12c at 1060 and 1620 cm⁻¹ both appear as doublet bands for solid hydrazine in Ref. 12. The data of Ref. 12 were also obtained for the N₂H₄ condensed at LN₂ temperatures but in a gas cell. Although not stated in Ref. 12, the deposits are believed to have been condensed at a relatively high pressure and formed in the crystalline phase. The N₂H₄ deposits formed in this study were condensed at a chamber pressure of approximately 1 x 10⁻⁷ torr and were of the amorphous form. As such, the spectra may be representative of a supercooled liquid as contrasted to a crystalline solid.

Warmup studies of N_2H_4 condensed at 20°K and subsequently warmed up until it had evaporated showed that the amorphous film changed phase and crystallized at some temperature between 95 and 127°K (see Fig. 13). At 95°K the spectrum was essentially the same as in Fig. 12c, but after warmup to 127°K the deposit had already changed phase at some intermediate temperature, and the band location in the spectra of Fig. 13 agrees with the data of Ref. 12. The single bands at 1060 and 1620 cm⁻¹ became double bands with locations at 1075 and 1130 cm⁻¹ and 1595 and 1650 cm⁻¹, respectively. Also the relative intensities of the two bands at 1305 and 1345 cm⁻¹ reversed, with the 1345-cm⁻¹ band now being the more intense, which also agrees with the spectra presented in Ref. 12.

Noticeably missing in Fig. 12c is the torsional ν_7 band that was observed in Ref. 12 for the solid crystalline phase but is not present in the liquid or gaseous phases. After warmup and phase change (Fig. 13) a strong band at 630 cm⁻¹ was observed that corresponds to the previously missing ν_7 band in Fig. 12c and shown in Ref. 12. This also indicates that the amorphous solid phase is more characteristic of a supercooled liquid than the crystalline solid form.

The fracture phenomenon behaved differently spectrally in a couple of cases. In one instance the spectra obtained after fracture showed no indication of the band at 635 cm⁻¹ nor the splitting of the 1060- and 1620-cm⁻¹ bands. In another experiment, where fracture occurred after a 6.89- μ m-thick N₂H₄ film was continuously deposited at 77°K (see Fig. 14), the first spectra obtained immediately after fracture showed both the presence of the 635-cm⁻¹ band and the splitting of the 1060- and 1620-cm⁻¹ bands. Therefore, whether or not the fracture is directly associated with a crystalline phase change is somewhat uncertain. The two cases where shattering (or fracture) occurred for films condensed at 20°K showed no spectral evidence of a phase change. The film condensed at 77°K before shattering (or fracture) did spectrally show the crystalline change, but this film was also considerably thicker when it fractured than was that at 20°K. The fracture phenomenon occurs while the film is being deposited, e.g., while the film is growing in thickness. The phase change occurs after a certain film thickness is reached and the film temperature then is allowed to increase. The deposit whose transmission is shown in Figs. 12a through c reached a thickness of 22 interference maxima (4.63 μ m). During deposition of the 23rd maxima the film ruptured into many hairlike fibers that curled up from the center of the germanium window back to the outer edge (out of the IR beam). A spectral scan of the germanium window after this occurred showed that all of the film was removed.

5.0 OPTICAL PROPERTIES DETERMINATION

To account for the influence of these fuel constituents as contaminants it is necessary to know the solid condensed-phase optical properties. These properties are needed to compute

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the reflectance change of a surface or to compute the transmission change of an optical component. Knowing these properties can help correct for the effects of condensed constituents on an actual surface. The optical properties desired are the refractive index, n, and the absorption index, k.

To determine the complex refractive index ($\bar{n} = n - ik$) of the thin solid film from the transmission versus thickness data for wavenumbers between 700 and 3700 cm⁻¹, an analytical model of film plus substrate normal transmission was developed (Refs. 15 and 16). It was assumed that the germanium window acted as a thick film, and thus there was no phase coherence between multiple internal reflected rays. Moreover, the real part of the germanium complex index, n_g, is known and given by Ref. 17:

$$n_g = A + BI + CL^2 + D\lambda^2 + E\lambda^4$$
 (1)

where

$$L = (\lambda^{2} - 0.028)^{-1}$$

$$\Lambda = 3.99931$$

$$B = 0.391707$$

$$C = 0.163192$$

$$D = -0.000006$$

$$E = 0.00000053$$

The geometry describing the transmission is shown in Fig. 15. For convenience the different layers have been subscripted 0, 1, 2, and 3, where subscripts 0 and 3 are vacuum and 1 and 2 are the thin condensed film and the thick germanium substrate, respectively. The model employed to fit the experimental results is for normal incidence only. As shown in Fig. 15, E_0^+ is the amplitude of the incidence radiation that undergoes an infinite number of multiple reflections after passing into the thin film. Following multiple reflections the total amplitude of reflected and transmitted radiation is given by B1 and E_2^+ , respectively. E_2^+ internally reflects from the back of the germanium window, becomes A1 and C1, and again undergoes thin-film multiple reflection in medium 1. This results in the rays B2 and A2, and so on. Analytically the relationships between the amplitudes of the various waves are the following:

$$E_{2}^{\perp} = r_{012}E_{0}^{\perp}$$

$$A_{2}^{\perp} = A_{1}r_{210}$$

$$A_{4}^{\perp} = A_{3}r_{210}$$

$$A_{6}^{\perp} = A_{5}r_{210}$$

$$A_{6}^{\perp} = A_{5}r_{210}$$

$$A_{7}^{\perp} = A_{7}^{\perp}$$

with

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and with

A3 A5	$= A2 r_2$ $= A4 r_2$	(3)
C1	$= \iota_2 E_2^{\dagger}$	
C2	$= t_2 A2$	
C3	$t = t_2 A4$	(4)
BI	$= E_0^+ r_{012}$	
B 2	= A1 t_{210}	
B3	$= A3 t_{210}$	(5)
B4	$= 45 t_{210}$	

where t_2 designates the amplitude transmission of light traveling from medium 2 to medium 3, r_2 designates the amplitude reflection of light incident upon medium 3 from medium 2, r_{012} designates the amplitude reflection of light that is incident from medium 0 and is reflected back into medium 0 after undergoing thin-film interference in medium 1, r_{210} designates the amplitude reflection of light that is incident from medium 2 and is reflected back into medium 2 after undergoing thin-film interference in medium 1, r_{012} designates the amplitude reflection of light that is incident from medium 2 and is reflected back into medium 2 after undergoing thin-film interference in medium 1, t_{012} designates the amplitude transmission of light incident from medium 0 and transmitted into medium 2 after undergoing thin-film interference in medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1, and t_{210} designates the amplitude transmission of light incident from medium 1.

 $AI = E_2^- r_2$

The power transmitted through the thin-film, thick-film combination is given by

$$\xi = n_3 |C1|^2 + n_3 |C2|^2 + \dots$$
(6)

where $n_3 = n_0$ since medium 3 and medium 0 are both considered as vacuum and with the constant c/4 π (c being the speed of light in vacuum) being omitted for convenience since this constant will be lost when dividing to determine the overall transmittance.

Substituting Eq. (4) into Eq. (6) yields the transmitted power as

$$\xi = |\mathbf{n}_{0}, \mathbf{t}_{2}|^{2} \left[|\mathbf{E}_{2}^{+}|^{2} + |\mathbf{A}2|^{2} + |\mathbf{A}4|^{2} - |\mathbf{A}6|^{2} + \cdots \right]$$
(7)

Next, combining Eqs. (2) and (3) yields

$$|A2|^{2} = R_{2}R_{210}|E_{2}^{+}|^{2}$$

$$|A4|^{2} = R_{2}^{2}R_{210}^{2}|E_{2}^{+}|^{2}$$

$$|A6|^{2} = R_{2}^{3}R_{210}^{3}|E_{2}^{+}|^{2}$$
(8)

where

$$R_2 = |r_2|^2$$
 (9)

$$\mathbf{R}_{210} = |\mathbf{r}_{210}|^2 \tag{10}$$

$$T_2 = |t_2|^2$$
 (11)

Inserting Eq. (11) into Eq. (7) results in the transmitted power being given by

$$\xi = n_{o} T_{2} |E_{2}^{+}|^{2} [1 + R_{2} R_{210} + R_{2}^{2} R_{210}^{2} + R_{2}^{3} R_{210}^{3} + \cdots]$$
(12)

where the infinite sum coverges to the closed-form expression,

$$\xi = \frac{n_o T_2 |E_2^+|^2}{1 - R_2 R_{210}}$$
(13)

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The transmittance is defined as the transmitted power divided by the incident power. The incident power is given by

$$\xi_{o} = n_{o} E_{o}^{-1} E_{o}^{-1}$$
(14)

and the expression for the overall transmittance is obtained by ratioing Eq. (13) to Eq. (14), i.e.,

$$T = \frac{\xi}{\xi_o} = \frac{T_2 |E_2^+|^2}{[1 - R_2 R_{210}] |E_o^+|^2}$$
(15)

But from Eq. (2)

$$\frac{|\mathbf{E}_{2}^{+}|^{2}}{|\mathbf{E}_{0}^{+}|^{2}} = |t_{012}|^{2} = T_{012}$$
(16)

and the final result for the overall normal transmittance is given by

$$T = \frac{T_2 T_{012}}{[1 - R_2 R_{210}]}$$
(17)

The result in Eq. (17) is valid only when the substrate is a nonabsorbing medium. If the substrate is also absorbing, i.e., the imaginary part of the complex refractive index of the substrate is nonzero, then Eq. (17) becomes

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$$T = \frac{T_2 T_{012} e^{-\alpha} g^D}{1 - R_2 R_{210} e^{-2\alpha} g^D}$$
(18)

where

D = the thickness of the substrate (germanium)

$$a_g = (4\pi k_g) /\lambda$$
 is the absorption coefficient of the substrate (germanium)
 $k_g = \text{imaginary component of complex refractive index of the substrate (germanium)}$
 $\lambda = \text{wavelength in vacuum}$

Having developed Eq. (18), which is the normal transmittance of a thin film deposited upon a thick partially transmitting film, it is now necessary to define the expressions T_2 , T_{012} , R_2 , and R_{210} in terms of the optical constants of the thin film, the substrate, and wavelength. The derivation of these quantities is straightforward, although tedious, and is outlined in detail in Ref. 16. For completeness, the expressions required to evaluate Eq. (18) are listed below (Fresnel coefficient for normal incidence):

$$R_{2} = |r_{2}|^{2} = \left| \left(\frac{\bar{n}_{2} - n_{0}}{\bar{n}_{2} + n_{0}} \right) \right|^{2}$$
(19)

$$T_2 = |t_2|^2 = \left|\frac{2\overline{n}_2}{(n_0 + \overline{n}_2)}\right|^2$$
 (20)

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The expressions for T_{012} and R_{210} are somewhat more complicated to evaluate and will be considered separately from R_2 and T_2 . The expressions for T_{012} and R_{210} based on the work of Ref. 16 are given by

$$T_{012} = \frac{|t_a|^2 |t_b|^2 e^{-2b}}{[1 + |r_a|^2 |r_b|^2 e^{-4b} + 2e^{-2b} |\text{Re}(r_a r_b) \cos 2a - Im(r_a r_b) \sin 2a]]}$$
(21)

and

$$R_{210} = \frac{\left[\left|r_{a}\right|^{2} + \left|r_{b}\right|^{2} e^{-4b} + 2e^{-2b} \left\{ \operatorname{Re}(r_{b}r_{a}^{*}) \cos 2a + \operatorname{Im}(r_{b}r_{a}^{*}) \sin 2a \right\} \right]}{\left[1 + \left|r_{a}\right|^{2} \left|r_{b}\right|^{2} e^{-4b} + \left|2e^{-2b}\right| \left[\operatorname{Re}(r_{a}r_{b}) \cos 2a + \operatorname{Im}(r_{a}r_{b}) \sin 2a \right] \right]}$$
(22)

.

where

$$r_{a} = \frac{\bar{n}_{2} - \bar{n}_{1}}{\bar{n}_{2} + \bar{n}_{1}}$$
 (23)

$$r_{\rm h} = \frac{\overline{n}_1 - n_{\rm o}}{\overline{n}_1 + n_{\rm o}}$$
(24)

$$I_{a} = \frac{2\bar{n}_{1}}{\bar{n}_{1} - \bar{n}_{2}}$$
(25)

$$t_{\rm b} = \frac{2 \, n_{\rm o}}{n_{\rm o} - \overline{n}_{\rm o}} \tag{26}$$

$$\overline{n}_1 = n_1 - ik_1 = n - ik = \overline{n}$$
(27)

$$\vec{n}_2 = n_g - \iota k_g$$
(28)

$$a = \frac{2\pi d_1 n_1}{\lambda}$$
 (29)

$$b = \frac{2\pi d_1 k_1}{\lambda}$$
(30)

$$d_1 = cryodeposit thickness$$
 (31)

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and * denotes the complex conjugate. The optical constants of the cryopumped constituents were determined by using this analytical transmission model in conjunction with a nonlinear least-squares convergence routine. Also the subtractive Kramers-Kronig relation (which is based on solid-state physics) between n and k was used in conjunction with (for 20 and 80°K N_2O_4) and in comparison with (for 20 and 80°K MMH, also for 80°K N_2H_4) the nonlinear least-squares determination of n. The subtractive Kramers-Kronig relation is given by

$$\mathbf{n}(\mathbf{v}) = \mathbf{n}(\mathbf{v}_{m}) + \frac{2}{\pi} \Pr \int_{0}^{\infty} \left[\frac{\mathbf{k}(\mathbf{v}')\mathbf{v}' - \mathbf{k}(\mathbf{v})\mathbf{v}}{(\mathbf{v}')^{2} - \mathbf{v}^{2}} - \frac{\mathbf{k}(\mathbf{v}')\mathbf{v}' - \mathbf{k}(\mathbf{v}_{m})\mathbf{v}_{m}}{(\mathbf{v}')^{2} - \mathbf{v}_{m}^{2}} \right] d\mathbf{v}'$$
(32)

where v_m is a reference frequency (2500 cm⁻¹ for 20°K MMH and N₂O₄ and 2200 cm⁻¹ for 80°K MMH, N₂O₄, and N₂H₄) and P indicates the Cauchy principal value of the integral. Integration was performed using the simple trapezoidal rule; the k(v⁺) values used in Eq. (32) were those determined by the nonlinear least-squares technique.

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The transmission data recorded for all deposits discussed here were digitized every 2 cm⁻¹. In the determination of n, transmission spectra at 14 thicknesses (HeNe laser interference fringes) (0 \rightarrow 3.25 μ m) were used; for MMH at 80°K, data at 11 thicknesses (0 \rightarrow 2.29 μ m) were used; and for N₂H₄ at 80°K, data at 22 thicknesses (0 \rightarrow 4.74 μ m) were used. The optical constants are shown in Fig. 16 and Table 4 for 20°K MMH, in Fig. 17 and Table 5 for 80°K MMH, and in Fig. 18 and Table 6 for 80°K N₂H₄. These optical properties were determined solely by use of the analytical model with the nonlinear least-squares convergence technique; the Kramers-Kronig determination of n is shown only for comparison purposes. The results of the two techniques are in excellent agreement.

For N₂O₄, absolute transmission spectra at 7 thicknesses (0 to 1.45 μ m) for the 20°K deposit and 9 thicknesses (0 \rightarrow 6.63 μ m) for the 80°K deposit were used in determining the optical properties. Usually a minimum of about 15 thicknesses is desired for the analytical model to converge upon a well-defined value of n. The n value appears to be primarily defined by the period of the transmission versus thickness curve at each wavenumber. When only a few thicknesses are obtained, the transmission versus thickness (for each wavenumber) curve is not well defined. It was found that for high wavenumbers (>2100 cm⁻¹) the analytical model had no problem in defining n; however, at the lower wavenumbers a neighborhood (range) of n values seemed to satisfy the transmission data. The k value, which is primarily defined by the magnitude of the transmission, did not have this difficulty and was well-defined over the whole spectral region (700 to 3700 cm⁻¹). Thus to determine n, the k values were used with the subtractive Kramers-Kronig relationship to compute n; these new n values were then used in the analytical model (along with the k values) to see if good agreement occurred with the transmission data. For all wavenumbers, the Kramers-Kronig n's along with the least-squares k's yielded good agreement when the

analytical model and transmission data were compared. The optical constants for 20 and 80°K N_2O_4 are shown in Fig. 19 and Table 7 (20°K), and Fig. 20 and Table 8 (80°K), respectively.

The optical properties presented are important for calculating the effects of possible deposits upon cryogenically cooled surfaces. Such surfaces as cryogenically cooled sensor optics and telescopes will be functioning in the wavenumber region investigated. The interpretation of information from these types of instruments, when contaminated with thin films, will require spectral knowledge of n and k. Shown in Fig. 21 are the transmission versus thickness curves at a variety of wavenumbers for the 20 and 80°K data. The excellent agreement between theory and data is typical of the results obtained over the entire spectral region (700 to 3700 cm⁻¹). Figure 21 illustrates the good agreement between theory and data at both high and low wavenumbers and in regions of high absorption.

6.0 SUMMARY

Experimentally determined transmission measurements of condensed propellant gases on a cryogenically cooled germanium window have been made. Thin films of monomethyl hydrazine (MMH), nitrogen tetroxide (N₂O₄), and hydrazine(N₂H₄) were formed at 20 and 77°K. The infrared spectral transmission was studied over the 500 to 3700-cm⁻¹ wavenumber range. The propellant thickness was accurately determined using a two-angle laserinterference technique. The density of the films was determined using quartz-crystal microbalances (QCM's) and by determining the refractive index at 0.6328 μ m to allow accurate thickness determination. Some fracture and shattering effects were observed for the films condensed at 20°K.

From the transmission data, the optical properties n and k, which are the real and imaginary parts of the refractive index, were determined for the 700 to 3700-cm⁻¹ wavenumber range. These results are presented in graphical and tabular form for a wavenumber interval of 2 cm⁻¹. These optical properties can be used to calculate the amount of optical contamination caused by thin films of these gases deposited on any mirror or window substrate, provided the n's and k's of the substrate material are also known.

No major spectral differences were observed between the transmission results of films formed at 20 and 77°K for the same propellant. For MMH, the n's and k's showed little variation: The n values for 77°K were slightly larger than for 20°K; the k values in the absorption bands for 77°K were also slightly larger than for 20°K. The N₂O₄ optical properties showed a stronger variation with temperature than did the MMH. For N₂O₄ the n's and k's were larger at 77°K than 20°K for the three strongest absorption bands.

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- 1. Pyroelectric detector and collection optics.
- Stainless steel high vacuum chamber, 85 cm tall by 70 cm in diameter (33, 5 in. by 27, 5 in. in diameter).
- 3. Cryogenically cooled infrared window; germanium, 4 mm thick by 70 mm square (0, 158 in, by 2, 76 in,) and QCM.
- Helium-neon laser (0.6328 μm) beam (one of two shown) employed to measure cryofilm thickness.
- 5. Infrared beam, 38 mm in diameter (1, 5 in,).
- 6. 2-mw He-Ne laser.
- 7. Michelson interferometer.
- 8. Infrared source and collimator mirror.



Figure 1. Schematic of the Infrared Optical Transmission Chamber (IROTC) with FTS-14 interferometer-spectrometer.

- 1. Infrared beam, 38-mm-diameter (1.5.).
- Optical stop required to underfill cryocooled window with infrared beam. Also, this stop is supported by a 3-in. -ID pipe that prevents gas added to chamber from cryopumping on rear of window.
- 3. Aluminum holder with cryogenic passageways.
- 4. Germanium window heat sunk with an indium gasket to the aluminum holder.
- 5. Cover plate.
- 6. Gaseous helium or liquid nitrogen intet.
- 7. Gaseous helium or liquid nitrogen outlet.
- B. Crosshatched area illustrates area of window heat sunk to holder. Clear diameter is 50, 7 mm (2 in,) while infrared beam diameter is 38 mm (1, 5 in,).
- 9. QCM heat sunk with indium gasket to aluminum holder.



Figure 2. Plan and elevation views of cryogenically cooled sample holder.



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a. 0.47 μm thick





b. 1.17 μ m thick Figure 4. Continued.



c. 3.27 μ m thick Figure 4. Concluded.

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Figure 5. Transmission of 3.27-µm-thick solid MMH formed on 20°K germanium after warmup of the germanium substrate from 20 to 160°K.






b. 2.21 μ m thick Figure 6. Continued.



c. 8.84 μ m thick Figure 6. Concluded.



Figure 7. Transmission of 8.84-µm-thick solid MMH after warmup of germanium substrate from 77 to 161°K.



condensed on 20°K germanium.



Figure 9. Transmission of 1.45-µm-thick solid N₂O₄ film on germanium after warmup from 20 to 153°K.







b. 1.25 μ m thick Figure 10. Continued.



c. 4.18 μ m thick Figure 10. Concluded.



a. 155°K

Figure 11. Transmission spectra of 4.18- μ m-thick N₂O₄ condensed on a 77° K germanium substrate as a function of warmup temperature.



b. 174° K Figure 11. Continued.



c. 183° K Figure 11. Concluded.



a. 0.22 μ m thick

Figure 12. Transmission spectra of hydrazine condensed on 77° germanium.



b. 2.16 μ m thick Figure 12. Continued.



c. 4.74 μ m thick Figure 12. Concluded.



Figure 13. Transmission of \approx 1.8-µm-thick hydrazine condensed on a 20°K germanium substrate and warmed up to 127°K.



Figure 14. Transmission of a 6.89-µm-thick hydrazine film on a 77°K germanium substrate after fracture.



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Figure 15. Geometry depicting analytical model for a thin film formed upon a thick film.

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Figure 16. Complex refractive index for MMH on 20°K germanium.

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Figure 17. Complex refractive index for MMH on 80°K germanium.

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Figure 18. Complex refractive index for $N_2 H_4$ on $80^{\circ} K$ germanium.



Figure 19. Complex refractive index for N_2O_4 on $20^\circ K$ germanium.



Figure 20. Complex refractive index for N_2O_4 on 80° K germanium.











c. $N_2 H_4$ on 80°K germanium Figure 21. Continued.



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e. N₂O₄ on 80° K germanium Figure 21. Concluded.

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<u>20°K</u>	After Warmup to 160°K	<u>77°K</u>	After Warmup to 161°K	Liquid MMH (Ref. 3)	Assignment
836	845	840	835	813	^V 18
	860		860		
1004	985	1015	1010	985	^V 16
1104	1105	1105	1120	1094	v15
1132	1130	1140	1140	1120	^V 13
1206	1220	1220	1220	1194	^۷ 12
1320	1350	1335	1345	1295	×11
1410	1410	1415	1405	1411	V10
1444	1450	1450	1440	1438	v ₉
			1460		
1482	1480	1480	1490	1472	^۷ 8
1624	1620	1630	1620	1608	ν ₇
			1700		·
=			1850		
			2020		
			206 0		
			2140		
			2210		
			2340		
			2660		
2778	2795	2780	2780	2784	^v 6
2854	2865	2860	2860	2858	^v 9 ^{+v} 10
2934	2945	2940	2940	2937	v5 .0
2964	2990	2980	2980	2963	Ň
3032		3020	3020		$v_7^{+}v_{10}$
3164	3165	3160	3140		$v_3^{+\nu}11^{-\nu}10$
3256	3260	3260	3215	3250 ,	v ₃
	3360		3340		$v_1^{\rm or} v_2$

Table 1. Absoprtion Band Locations and Vibrational Assignments for Monomethyl Hydrazine (CN_2H_6)

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<u>20°K</u>	After Warmup to 153°K	<u>77°K</u>	After Warmup to 155°K	<u>195°K (Ref. 4)</u>	Assignment (Ref. 4)
750	740	740	740	738	^v 12
785	760	76 0	760	756	v_{12}^{+R}
	790				
820	825		815	(813 gas)	^v 2
850	860		845		
940-1060	965	<u> </u>	940-1220		
1050	1040	1110	1110		
1260	1260	1255	1260	1256	^v 11
1305	1305		1 30 0	1280	ν ₁₁ +R
1450	1400	1460	1420		
1595	1595		 `		
1618		1620	1620	~	
1720		1700	1690	1696	^۷ 5
1742 `	1740	1740	1745	1734	ν ₉
1765	1760	1760	1760	1760	v9+R
1880	1865	1840	1840	1859	$v_{4}^{+}v_{5}$
1980					
2135					
2235	2220	2240	2220		
2345		2340			
		2580	2575	2584	v1 ^{+v} 11
_ 	2625	2620	2620	2628	$2v_7 + v_{11}$
2970	2965	2965	2960	2958	^v 5 ^{+v} 11
		2985	2985	2986	$v_{5}^{+}v_{11}^{+R}$
			3050	3058	v1 ^{+v} 9
3115		3100	3100	3105	2v7+v9
3155		3140	3135	3136	2v7+v9+R
			3420	3430	v5 ^{+v} 9
			3460	3460	v5+v9+R

Table 2. Absorption Band Locations and Vibrational Assignments for Nitrogen Tetroxide (N_2O_4)

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	After Warmup	Solid at 80°K	Vibration Number
<u>7/°K</u>	<u> </u>	(Ref. 12)	Assignment (Ref. 12)
	630	627	ν ₇
890	890	884	^v 6
1060	1075	1066	v ₁₂
	1130	1126	v ₅
1305	1305	1304	v ₄
1345	1340	1350	v11
1620	1595	1603	v ₃
	1650	1655	۰ 10
2 9 55			
3180	3180	3200	ν ₂
3340	3300	3310	^v 8' ^v 1

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Table 3. Absorption Band Locations and Vibrational Assignments for Hydrazine (N_2H_4)

Table 4. Condensed MMH Optical Properties at 20°K

<u>v, cm⁻¹</u>	<u>n</u>	_ <u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	k
3950		0.011100	3500	1.415077	0.010400
3940	1.422442	0.014800	3490	1.414710	0.010800
930 ك	1.426580	0,015700	3480	1.413943	0.010600
3950	1.421282	0.011100	3470	1.413128	0.011200
3910	1.424758	0.009000	3460	1.412222	0.010900
3300	1,423517	0,013600	3450	1.411101	0.011500
3840	1.424279	0.011100	3440	1,410435	0.012000
3880	1.425719	0.015200	3430	1.409547	0.011300
3870	<u>1.420549</u>	0.010100	3420	1.408593	0.012300
3860	1.425318	0.010900	3410	1.407205	0.011800
3650	1.424410	0.010900	3400	1.404900	0.012000
3840	1.424840	0.011300	3398	1.404884	0.012500
3830	1.424220	0.010600	3396	1.404773	0.012300
3820	1.424306	0.011200	3394	1.404460	0.012100
3810	1.423791	0.013300	3392	1.403891	0.012000
3800	1.423618	0.010900	3390	1.403206	0.012000
3790	1.423591	0.012100	3388	1.402763	0.015300
3770	1.423774	0.010300	3386	1.402530	0.012500
3770	1.423210	0.011800	3.354	1.4021+5	0.015100
3760	1.423728	0.012000	3382	1.401304	0.012000
3760	1+4230+3	0.010900	3380	1.400/53	0.012600
3740	1 + 423073	0.010300	3378	1.400388	0.012400
3730	1.423010	0.012100	3376	1.399709	0.012300
3710	1+423/31	0.011200	3374	1.3989+5	0.012500
3700	1 623654	0.011200	3372	1.398437	0.012600
3690	1.423430	0.010200		1.39//59	0.012500
3030	1 4222 11	0.010200	3346	1.300330	
3670	1.422(0.4	u 010600	3 464	1 394 145	0.012-00
3660	1.421557	0.010500	3362	1 901979	0.013200
3650	1.421805	0.011700	1360	1.342742	0 01 1700
3640	1.421541	0.010000	3358	1.201512	0 014200
3630	1.420073	0.010800	3356	1.390396	0.014200
3620	1.420973	0.011900	3354	1.389508	0.015500
3610	1.421373	0.010500	3352	1.338568	0.016000
3600	1.421138	0.010800	3350	1.387113	0.016200
3590	1.420205	0.009200	3348	1.385.358	0.017200
3580	1.418874	0.003800	3346	1.383959	0.018700
3570	1.418568	0.011000	3344	1.382886	0.020000
3560	1.418803	0.010700	3342	1.381717	0.021200
3550	1.418220	0.010100	3340	1.380309	0.022600
3540	1.417439	0.010500	3338	1.378905	U.024500
3530	1.416770	<u>0.010600</u>	3336	1.378124	0.027000
3520	1.416670	0.011300	3334	1.377669	0.028800
3510	1.410408	0.010800			-

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<u>v, cm⁻¹</u>	. <u>n</u>	_ <u>k</u>	v, cm^{-1}	<u>n</u>	_k_
3332	1.376911	0.030500	3240	1.444343	0.073500
3330	1.376156	0.033000	3238	1.446632	0.071200
3328	1.375974	0 035400	3236	1.448144	0.068500
3326	1.375925	0.037700	3234	1.449042	0.005500
3324	1.375929	0.040000	3232	1.450048	0.064700
3322	1.376313	0.042700	3230	1.451145	0.062800
3320	1.377047	0.044700	3228	1.452178	0.060800
3318	1.377860	0.047000	3559	1.453126	0.058700
3316	1.378703	0.049000	3224	1,453979	0.050300
3314	1.379808	0.051000	3225	1.4542/8	0.053500
3315	1.380982	0.052000	3220	1.454073	0.051000
3310	1.381939	0.053900	<u>_3218</u>	1.453440	0.048700
3308	1,362634	0.055500	3516	1.452603	0.045300
3306	1.333732	0.05/500	3214	1.452034	0.045400
3304	1.385044	0.059000	3212	1.451567	0.043000
3302	1,386489	0.060400	3210	1.450618	0.041690
3300	1.3875-4	0,001500	3209	1.449305	0.04010U
3298	1.388444	0.062800	3206	1.447887	0.039300
3296	1.,390290	0.005500	3204	1.445580	0.038000
3294	1.392557	0.005600	3202	1,445215	0.037100
3292	1.393933	0.066100	-3200	1.443003	0.036300
3290	1.394895	0 <u>.066700</u>	3190	1+441710	0.036000
7540	1.395894	0.057600	3190	1.490400	0.03-000
3280	1-346458	0.058700	3194	1 / 375 30	0.035000
3284	1.348180	0.059700	1190 1190	1.436157	0.0336600
3232	1.399292	0.070700	3188	1 4350137	0 03/000
3200	1.400030	0.072100	4186	1 433974	0.0313000
1276	1,402133	0.073200	3184	1.433227	<u>0.038900</u> 0.040200
1274	1.403040	0.074400	3182	1.432704	10.041500
3272	1.405700	0.07500	3180	1.432571	0.043160
3270	1.404493	0.077000	3178	1.432800	0.044700
3268	-1.411643	0 072100	3176	1.433362	0.045900
992F	1.413739	0.078200	3174	1.434032	0.047100
3264	1.415702	0.0/8800	3172	1 434857	0.048100
3262	1,4179+0	0.079300	3170	1.435925	0.049200
3260	1.420273	0.079400	3168	1.437102	0.049800
3258	1.422447	0.079600	3166	1.438325	0.050300
3256	1.424805	0.077700	3164	1.439005	0.051000
3254	1.427203	0.07 <u>9400</u>	3162	1.441397	0.050700
3252	1.427755	0_079300	3160	1 442277	0.050200
3250	1.4.32203	0.078500	3158	1.443250	0.020400
3248	1.434546	0.051300	3156	1.444885	0.023900
3246	1.4308/1	0,077200	3154	1.446217	0.050000
3244	1.439343	0.070200	3152	1.447294	0.049700
3242	1,441767	0.074900	3150	1.440520	0.049300

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>v, cm⁻¹</u>	<u>n</u>	_k_	<u>v, cm⁻¹</u>	<u>n</u>	k
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3148	1.449741	0.048500	3056	1.435133	0.017500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3146	1.450934	0.043000	3054	1.434328	0.017800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3144	1.452342	0.046900	3052	1.433535	0.013200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3142	1.453203	0.045400	3050	1.432857	0.013700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3140	1.453816	0.044400	3048	1.432321	0.017500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3138	1.454557	0-043400	3040	1.431738	0.019500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3136	1.455200	0.042000	3044	1.431116	0.020200
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3134	1.455664	0.040900	3042	1.430716	0.021100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3132	1.456240	0.034700	3040	1.430658	0,021900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3130	1.456657	0.033200	3038	1_430784	0.022500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3125	1.450/01	0.035700	3036	1,431044	0.023000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3126	1.456845	0.035500	3034	1.431233	0.023100
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3124	1.450887	0.034000	3032	1.431403	0.023400
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3122	1.455605	0.032500	3030	1,431825	0.023400
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3120	1.455040	0.031200	3020	1.431901	0.022900
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3118	1.455457	0.030300	3026	1.431818	0.022500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3116	1.455029	0.029500	3024	1.431573	0.022300
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3114	1.454734	0.028700	3022	1.431191	0.021900
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3112	1.454481	006150.0	3020	1.430738	0.021800
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3110	1.454028	0.026700	3010	1.430332	0.021600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3108	1.453431	0.023900	3016	1.429830	0.021300
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3106	1.453012	0.025300	3014	1.429176	0.021100
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3104	1.452144	0.024400	3012	1.420552	0.021000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3102	1,452135	0.023200	3010	1.427766	0.020700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3100	1,451157	0.022300	3008	1.420057	0.050000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3079	1.450203	0.021900	3006	1.425863	0,020500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3096	1.449493	0.021300	3004	1.424882	0.020000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3094	1.446663	0.021100	200E	1.423619	0.020600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3092	1.440107	0.020600	3000	1.422213	0.050300
3088 1.446991 0.023000 2996 1.419530 0.022300 3086 1.446944 0.019500 2994 1.418009 0.022500 3084 1.445750 0.013600 2992 1.416323 0.023800 3082 1.444922 0.013600 2990 1.416323 0.025300 3082 1.444922 0.013600 2990 1.416323 0.025300 3082 1.44431472 0.013600 2986 1.412122 0.026800 3078 1.442317 0.013100 2986 1.412122 0.024900 3076 1.442317 0.017500 2984 1.410913 0.030900 3074 1.442105 0.017500 2982 1.409858 0.033500 3072 1.440448 0.017200 2978 1.409290 0.039800 3066 1.439948 0.017300 2978 1.409931 0.043100 3066 1.439948 0.017300 29772 1.411139 0.046200 3066 1.437558 0.017200 2978 1.418185 0.052000 3062 1.437558 0.017200 2978 1.418185 0.054400 3065 1.435842 0.017200 2968 1.418185 0.054400 3065 1.435842 0.017200 2968 1.418185 0.054400 3058 1.435842 0.017400 2966 1.421803 0.055700	3040	1.447516	0.020300	2998	1.420919	0.021600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3088	1.446991	0.020000	2396	1.419050	0.022300
3084 1.445750 0.018900 2992 1.416323 0.023800 3082 1.444922 0.018600 2990 1.414849 0.025300 3050 1.444922 0.018400 2986 1.413455 0.026800 3078 1.443514 0.018100 2986 1.412122 0.024800 3076 1.442817 0.017900 2986 1.412122 0.024800 3076 1.442817 0.017900 2986 1.410913 0.030900 3074 1.442105 0.017500 2982 1.409858 0.033500 3072 1.440448 0.017200 2978 1.409264 0.036600 3070 1.440448 0.017200 2978 1.409250 0.039800 3068 1.439642 0.017300 29772 1.412787 0.0443100 3066 1.433948 0.017300 29772 1.412787 0.049100 3062 1.437553 0.017200 2970 1.418185 0.052000 3060 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435832 0.017200 2966 1.421803 0.055700	3086	1.446484	0.019500	2994	1.418009	0.055010
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3084	1.445750	0.019900	2992	1.416323	0.053900
3050 1.444192 0.018400 2488 1.413455 0.028800 3078 1.443514 0.018100 2986 1.412122 0.028000 3076 1.442817 0.017900 2984 1.410913 0.030900 3076 1.442105 0.017900 2982 1.409858 0.033500 3072 1.441319 0.017900 2980 1.409264 0.036600 3070 1.440448 0.017200 2978 1.409290 0.039800 3068 1.439642 0.017300 2976 1.409931 0.046200 3064 1.439040 0.017300 2972 1.412787 0.0443100 3064 1.439303 0.017300 2972 1.412787 0.0449100 3062 1.437553 0.017200 2970 1.418185 0.052000 3063 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3082	1.444922	0.013600	2990	1.414847	0.025300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3050	1.444172	0.018400	2488	1.413455	0.020800
3076 1.442817 0.017900 2984 1.410913 0.030900 3074 1.442105 0.017500 2982 1.409858 0.033500 3072 1.441319 0.017400 2980 1.409264 0.036600 3070 1.440448 0.017200 2978 1.409290 0.039800 3068 1.439642 0.017300 2976 1.409931 0.046200 3066 1.439948 0.017300 2974 1.411139 0.046200 3064 1.437553 0.017200 2972 1.412787 0.049100 3062 1.437553 0.017200 2978 1.418185 0.052000 3063 1.436719 0.017200 2978 1.418185 0.054400 3058 1.435882 0.017200 2966 1.421803 0.055700	3078	1.443514	0.019100	2986	1.412122	0.024300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3076	1.442817	0.017900	2984	1.410913	0.030900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3074	1.442105	0.017500	2982	1.409858	0.033500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-307Ž	1,441314	0.017400	2980	1.409204	0.036600
3068 1.434642 0.017300 2976 1.409931 0.043100 3066 1.438948 0.017300 2474 1.411139 0.046200 3064 1.438303 0.017300 2972 1.412787 0.0449100 3062 1.437553 0.017200 2970 1.415056 0.052000 3060 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3070	1.440448	0.017200	2978	1.409290	0.039900
3066 1.433943 0.017300 2974 1.411139 0.046200 3064 1.43303 0.017300 2972 1.412787 0.0449100 3062 1.437553 0.017200 2970 1.415066 0.052000 3060 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3068	1.434042	0.017300	2976	1,409931	0.043100
3064 1.433303 0.017300 2972 1.412787 0.049100 3062 1.437553 0.017200 2970 1.415056 0.052000 3060 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3066	1.435948	0.017300	2774	1.411133	0.046200
3062 1.437553 0.017200 2970 1.415056 0.052000 3060 1.436719 0.017200 2968 1.418155 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3064	1,434303	0.017300	2972	1.412767	Ú.049100
3060 1.436719 0.017200 2968 1.418185 0.054400 3058 1.435882 0.017400 2966 1.421803 0.055700	3062	1.437553	0.017200	2970	1.415066	0.052000
3058 1.435882 0.017400 2966 1.421803 0.055700	3060	1.436719	0.017200	2968	1.418185	0.054400
	3058	1.435882	0.017400	2966	1.421803	0.055700

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ν, cm ⁻¹	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>
2964	1.425556	0.056100	2872	1.442885	0.038100
2962	1.429101	0.055300	2870	1.442459	0.038600
2400	1,43100/	0.053400	2868	1.441954	0.039300
2959	1.433430	0.051000	2946	1.441335	0.040400
2956	1.433858	0.048700	2864	1.441048	0.042200
2954	1.433231	0.046700	2462	1.441522	0.044400
2425	1.431930	0.045600	2860	1.442734	0.046300
2950	1.430202	0.045200	2050	1.444572	0.047900
2948	1.427959	0.045500	2820	1.440920	0.049000
2946	1.425667	0.047600	2854	1.449417	0.049200
2944	1.424379	0.051100	2452	1,451654	0.048700
2942	1.424481	0.055200	2850	1.453419	0.047300
2940	1.426079	0.054600	2848	1.454686	0.045700
2938	1.429415	0.063300	2846	1.455349	0.045000
2936	1.434326	0.066300	2844	1.455002	0.045000
2934	1.440078	0.064000	2842	1.455030	0.045000
2932	1.445957	0.067500	2840	1.456454	0.045500
2930	1.4511.1	0.055100	28.38	1,457714	0.046200
2928	1.455112	0.061900	2836	1.459843	0.046800
2959	1.458124	0.058300	2034 15653	1.402550	0.046500
2924	1.460075	0.054100	2036		0.043400
2922	1.400090	0.050200	2030	1.408237	0.043200
2920	1.400929	0.040500	2426	1.470300	0.040000
2710	1,400420	0.043500	2620	1 471475	0.030300
2710	1.439321	0.039E00	2822	1.470546	0.032700
2914	1,430321	0.03-03000	7820	1 464240	0.029000
2912	1.450901	0.030100	2814	1 467919	0 025000
2910	1 454010	0.035200	2816	1.465 154	0.023000
2906	1 452348	0.033100	2814	1.454558	0.023400
2404	1.450597	0.042400	2812	1.462624	0.020100
2902 /	1.449282	0.032400	2810	1.460697	0.014200
2900	1.448216	0.033100	2808	1.458741	0.018400
2898	1.44/300	0.033300	2805	1.4565+2	0.017700
2896	1.446007	0.033600	2004	1.454201	0.017600
2894	1.446109	0.033400	2005	1.451957	0.017800
2892	1.445572	0.034000	2300	1.449605	0.018100
2890	1.444937	0.034300	2798	1.447000	0.019900
2989	1.444367	0.034700	2796	1.444447	0.020500
2686	1.443967	0.035300	2794	1.442101	0.022600
2884	1.443757	0.035800	2792	1.440024	0.025400
2842	1,4435 <u>4</u> 8	0.030200	2790	1.438396	0.029000
2480	1.443346	0.036600	2788	1.437601	0.033+00
2878	1,443235	0.037200	2736	1.438130	0.038500
2876	1.443336	0.037/00	2744	1.440523	0.043900
2874	1.443250	0.037700	2782	1.444962	0.048600

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ν, cm ⁻¹	<u>n</u>	k		v ; cm^{-1}	<u>n</u>	k
2780	1.451031	0.051400		2640	1.450213	0,014300
2778	1.45/680	0.051900		2630	1.449939	0.014100
2716	1.403700	0.050100		2620	1.449555	0.013000
2774	1.408726	0,047000		2610	1.449052	0.013100
2772	1.472386	0.042900		2000	1.448444	0.013400
2770	1.474504	0.034200		- 2590	1.448205	0.013000
2768	1.475334	0.034000		2580	1.447845	0.013000
2766	1 475229	0.030000		2570	1.44/444	<u>0,012500</u>
2164	1.474355	0.026600		2500	1.440402	0.012500
2760	1.4/3144	0.024100		2550	1.44044d	0.012300
270U 3760	1.471790	0.021300		2540	1.446003	0.015000
2756	1.470343	0.050500		2530	1.446097	0.015800
2750	1.400039	0.6610.0		2520	1.446089	0.012200
2752	1.401334	0.017800		2500	1.445000	0.011900
2750	1.400210	0.017000		2430	1.444562	0.011800
2744	1 404 71 1	0.010,000		2410	1.444095	0.011600
2746	1.403703	0.010100	C	2460	1.443834	0.011900
2744	1.402770	0.015900		2450	1.44.3057	0.011900
2742	1.402013	0.015600		2440	1.443384	0.011600
2740	1.401372	0.015000		24.30	1,4431+5	0.011800
2738	1.460186	0.015400		2420	1+442727	0.011500
2736	1.459502	0.012000		2410	1.442303	0.011500
2734	1.458967	0.014400		2300	1+4+2127	0.011700
2732	1.458429	0.014800		2370	1 441664	
2730	1.457957	0.014700		2170	1.441426	6 011400
2728	1.457518	0.014600		2360	1.441114	0.011900
2726	1.456 <u>9</u> 63	0.014500		2350	1.441073	0.012300
2124	1.450491	0.014500		2340	1.441170	0.012300
2722	1.455091	0.01.100		2330	1.441101	0.012100
2720	1.455910	0.014700		2320	1.440887	0.012000
2/18	1.455542	0.014600		2310	1.440732	0.012100
2716	1.455335	0.014600		2300	1.440743	0.012200
2714	1.455085	0.014600		2290	1.440698	0.011800
2112	1.454875	0.01440u		2280	1.440259	0.011600
2710	1.454450	0.014300		2270	1.434928	0.011700
2706	1.454215	0.014400		2260	1.439535	0.011700
2700	1.453650	0.014200		2250	1.439095	0.011800
2704	1.403025	0.014300		2240	1.439152	0.012700
2700	1.4530.46	0.014400		2230	1.439430	0.012200
2690	1.403030	0.014500		2220	1.439101	0.012000
2680	1-451456	0.014600		2210	1.438593	0.011900
2670	1.450910	0.014300 0.014300		21.44	1.438351	0.012500
2660	1.450696	0 01/200		5140	1.4343//	0.012600
2650	1.450506	0.010000		2100	1 / 101/00	0.012600
	1.40000	<u>n • 614266</u>		61 I V	1.430100	v.v12500

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Table 4. Continued

<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	k
2160	1.437928	0.012800	1700	1,430353	0.014100
2150	1.437704	0.012800	1698	1.430306	0.014300
2140	1.437640	0.013200	1696	1.430002	0.014000
2130	1.437040	0.013200	1694	1.429814	0.014200
2120	1.437074	0.013300	1692	1.429542	0.013900
2110	1.437629	0.013400	1690	1.428980	0.013600
2100	1.437604	0.013200	1688	1.428320	0.013900
2090	1.437352	0.013300	1680	1.428137	0.014200
2080	1,4372J3	0.013300	1684	1.427850	0.013900
2070	1.437024	0.013500	1682	<u>1.427472</u>	0.013900
2060	1.436897	0.013500	1690	1.420/93	0.013400
2050	1.436660	0.013700	1678	1.425039	0.013200
2040	1.436656	0.014000	1676	1.424599	0.013400
2030	1.436695	0_014100	1674	1.423831	0.014100
2020	1.436059	0,014000	1072	1.422650	0.014300
2010	1.436492	0.014200	10/0	1.4215//	0.015400
2000	1.436406	0.014200	1000	1.420071	0.015100
1990	1.430310	0.014500	1000	1.414343	0.017100
1980	1.436264	0.014500	1663	1 410703	0.019400
1970	1.430323	0.014900	1660	1 417503	0.019300
1960	1.436444	0.014800	1000	1.417018	0.022800
1950	1.430540	0.014900	1656	1.415794	0.024500
1940	1,430039	0.014600	1650	1 416873	0.026500
1930	1.436623	0.014500	1652	1.417.13	0.028400
1720	1 436303	0 014400	1650	1.417876	0.029900
1910	1 436015	0.014100	1648	1.418372	0.031600
1600	1 435642	0_014200	1646	1.419222	0.033500
1880	1.435314	$\frac{0.014200}{0.014300}$	1644	1.420357	0.035100
1870	1.434997	0.014400	1642	1.421655	0.036600
1860	1.434746	0.014800	1640	1.423070	0.038000
1850	1.434677	U.015000	1638	1.424577	0.039200
1840	1.434592	0.015200	1636	1.420333	0.040600
1830	1.434566	0.015400	1634	1.428736	0.041800
1820	1.434541	0.015500	1632	1.430965	0.041700
1810	1.434557	0.015600	1630	1.432631	0.041800
1800	1.434550	0.015600	1628	1.434479	0.042500
1790	1.434382	0.015400	1626	1.436577	0.042400
1780	1.434190	0.015600	1624	1,438792	0_042600-
1770	1.434060	0.015500	1622	1.441205	0.042200
1760	1.433872	0.015500	1620	1.443332	0.041100
1750	1.433664	<u>0.015500</u>	1618	1.445314	0.040500
1740	1.433485	0.015300	1616	1.447219	0.039100
1730	1.433109	<u>0.015100</u>	1614	1.448995	0.039000
1720	1.432642	0.014800	1612	1.450930	0.036700
1710	1.431787	0.014400	1610	1,452797	0.034600

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<u>v, cm⁻¹</u>	<u>n</u>	<u>_k</u>	<u>v, cm⁻¹</u>	<u>_n</u>	_ <u>k</u>
1608	1-454076	0.032300	1516	1.427112	0.019400
1606	1.455051	0.030000	15]4	1.427189	0.019500
1604	1.455772	0-027600	1512	1.427114	0.019900
1602	1.456024	0.024300	1510	1.427009	0.020200
1600	1.455597	0.022300	1508	1.427093	0.020900
1598	1.454893	0.020200	1506	1.427426	0.021300
1596	1.454235	0.018500	1504	1.427042	0.021300
1594	1.453351	0.016400	<u>1502</u>	1.427623	0.021500
1592	1.452072	0.014800	1500	1.427600	0.021700
1590	1.450702	0.013600	1498	1.427503	0.021900
1588	1.449244	0.012500	1496	1.427340	0.022200
1586	1.447900	0.012100	1494	1.427130	0.022600
1584	1.446875	0.011700	1492	1.426971	0.023200
<u>1582</u>	<u>1.445983</u>	0.011200	1490	1.420091	0.023900
1580	1.445186	0.010900	1400	1.427034	0.024600
<u>1578</u>	1.444376	<u>0,010200</u>	1480	1.42/234	0.025700
1576	1.443471	0.009800	1404	1,4203/0	0.020400
<u>1574</u>	1,442427	0.009500	1402	1.429347	0.036700
1572	1.441229	0.003900	1400	1.430432	0.026700
1570	1.440147	0.009000	1476	1 431440	0.020200
1568	1.439337	0,009000	1470	1.431072	0 023900
1566	1.438507	0.008900	1472	1 430502	0.023100
1564	1.43/515	0,008300	1470	1.429174	0.023200
1562 3	1 436330	0.009100	1468	1.428318	0.024200
1200	1.433733	0.003000	1466	1.428046	0.024300
1220	1.435142	0.009700	1464	1.427752	0.025300
1550	1.433954	0.007200	1462	1.427139	0.025700
1552	1.432717	0 000000	1460	1.420378	0.026500
1550	1.431966	0.009400	1458	1.425550	0.027500
1548	1.431287	0.010300	1456	1.424469	0.028700
1546	1.430651	0.011000	1454	1.4229.37	0.030700
1544	1.430163	0.011400	1452	1.421633	0.034300
1542	1.429687	0.011900	1450	1.421713	0.033000
1540	1,429303	0.012400	• 1448	1.424340	0.045600
1538	1.428785	0.012600	1445	1.429936	0.051000
1536	1.428188	0.013200	1444	1.437756	0.053700
1534	1.427765	0.013900	1442	1.446264	0.053400
1532	1.427474	0.014400	1440	1.454346	0.050300
1530	1.427116	0.015000	1438	1.461111	0.044600
1528	1.426721	0.015500	1430	1.405129	0.030500
1526	1.420371	0.016400	1434	1.403/3/	0 031300
1524	1.426241	0.019300	1436	1 464021	0.021500
1520	1 426747	0 014600	1428	1 460913	0.012300
1518	1.426951	0-01-0000	1426	1.453165	0.011200
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Table 4. Continued

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<u>v, cm⁻¹</u>	<u>n</u>	_ <u>k</u> _	v, cm^{-1}	<u>n</u>	<u>k</u>
1424	1.447704	0.010300	1332	1.420241	0.024600
1422	1.447023	0.004400	1330	1.421741	0.025500
1420	1.444502	0.010300	1328	1.421027	0.022600
1418	<u>1.442640</u>	0.011200	1326	1.420538	0.027300
1416	1+4411/0	0.011900	1324	1.422491	0.027300
1414	1.440229	0.013400	1322	1.424413	0,028200
1412	1.440432	0.014900	1320	1,425563	0.059500
1410	1.441350	0,015300	<u>1318</u>	1.421000	0.023000
1408	1.4422+7	0.015000	1316	1.427994	0.027700
1406	1.442899	0.014100	<u>1314</u>	1.429142	0.027200
1404	1.443135	0.015900	1312	1.430040	0.020300
1402	1.442669	0.011200	1310	1,431145	0,020000
1300	1.441787	0.010200	1308	1.431807	0.025000
1306	1.440/07	0.004300	13)6	1.432310	0.05+000
1340	1.439//5	0.008700	1304	1.432/01	0.023100
1377	1 430341	0 003400	1302	1.433173	0.022100
1336	1.437230	0.007000	1300	1.433407	0.020900
1340	1 435442	0 007900	1298	1.433432	0.019500
1386	1.434532	0.007300	1296	1.433055	0.018300
1344	1.433605	0.007800	1294	1.432035	0.017200
1382	1.432673	0.004000	1292	1.432025	0.015200
1360	1.432002	0.008300	1290	1.431419	0.012300
1378	1.431472	0.004500	1260	1.430746	0.014500
1376	1.430900	0.008400	1200	1.430094	0.013000
1374	1.430250	0.008400	1204	1,427070	0.012000
1372	1.429598	0.003+00	1290	1 420029	0.012000
1370	1.428811	0.004300	1278	1,425645	0.011400
1368	1.427954	0.008300	1276	1 424416	0.010900
1366	1.426868	0.008300	1274	1.423310	0.010500
1364	1.425052	0.008700	1272	1.422087	0.010400
1362	1.424966	0.009200	1270	1.420972	0.010400
1360	1.424134	0.009400	1268	1.419809	0.010300
1358	1.423068	<u>0.009900</u>	1266	1.418534	0.010300
1356	1.422108	0.010500	1264	1.417238	0.010+00
<u>1354</u>	1.421019	0.011200	1262	1.415903	0.010700
1352	1.420157	0.012300	1260	1.414783	0.011100
1350	1.419427	0.013400	1258	1.413030	0.011300
1348	1.418970	0.014500	1256	1.412271	0.011500
1346	1.418430	0.015000	1254	1.410893	0.012100
1344	1.418121	0.016800	1252	1.409532	0.012700
1342	1.417727	0.013100	1250	1.408140	0.013300
1340	1.417845	0.019600	1248	1.406696	0.014100
1338	1.417930	0.020900	1246	1.405293	0.015000
1336	1.418510	0.055500	1244	1.403695	0.015800
1334	1.414887	<u>0,02350u</u>	1242	1.401904	0.017100

v, cm^{-1}	<u>n</u>	_ <u>k</u>	v, cm^{-1}	<u>_n</u>	<u>k</u>
1240	1.400209	0.018800	1148	1.384302	0.042600
1238	1.398864	0.020900	1146	1.384305	0.046800
1236	1.397577	0.022700	1144	1.384838	0.051100
1234	1.396407	0.025200	1142	1.386170	0,055600
1232	1.395444	.0.027700	1140	1.388341	0.059000
1230	1.394038	0.030400	1138	1,391156	0.063200
1228	1.394036	0.033700	1130	1.394540	0.065200
1220	1.394159	0.037300	1134	1.398620	0.009000
1224	1.394907	0.040900	21132	1.403148	0.069700
1222	1.370213	0.044300	1130	1,40/5/3	0,069400
1218	1.071766	0.047700	1120	1+411517	0.058000
1215	1.400500	<u>0.051100</u>	1120	1.414192	0.065300
1214	1.403017	0,054100	1127	1.410194	0.055400
1212	1 411737	0.057300	1120	1 410746	0.053300
1210	1.4)5044	0.057800	1118	1.404543	0.053500
1203	1.419523	0.057800	1116	1.197642	0.056100
1206	1.423649	0.058800	1114	1.392013	0.053500
1204	1-424569	0.058600	1112	1.389724	0.074500
1202	1.435356	0.054900	1110	1.392617	0.087300
1200	1.439212	0.050000	1108	1,401040	0-098400
1198	1.441012	0.045000	1106	1.413909	0.106800
1196	1.442836	0.039600	1104	1.429349	0.109900
1194	1.442786	0.034200	1102	1.444967	0.107200
1192	1.441421	0,029200	1100	1.458744	0.100100
1190	1.439105	0.025000	1098	1.469702	0.089500
1188	1.430353	0.021700	1096	1.477095	0.076200
1186	1.433292	0.019000	1094	1.480028	0.061700
1184	1.430056	0.017100	1092	1.478526	0.047800
1182	1.426793	0.015600	1090	1.473446	0.036000
1180	1.423436	0.014700	1088	1.466439	0.027500
<u>1178</u>	<u>1.420298</u>	<u>0.014400</u>	1086	1.458957	0.021500
1176	1.417391	0.014300	1084	1.451425	0.017400
1174	1.414478	0.014200	1082	1.444377	0.015300
1172	1.411505	0.014600	1080	1.438250	0.014300
$\frac{1170}{1160}$	1.408691	0.015200	1078	1.432811	0.013600
1168	1.405849	0.015900	1076	1.42/822	0.013500
1166	1.402919	0.016900	1074	1.423291	0,013500
1104	1.399915	0.018300	1072	1.419004	0.013600
1102	1.397058	0.020200	1070	1,414750	0.013700
1159	1 2024434	0 024000	1044	1.410474	0.014000
1156	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.023000	1000	1 401941	0.014500
1154	1.387927	0.02/000 0.030k00	1067	1 104954	0.014700
1152	1.386170	0.014400	1060	1.201274	0 014400
1150	1.384911	0.074400) NSA	1.386870	0.010400
	1004211	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	+0.0	1000000	A * A TOTAA

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Table 4. Continued

<u>v, cm⁻¹</u>	<u>n</u>	<u>_k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>
1056	1.379536	0.020700	964	1.500439	0.094100
1054	1.373272	0.024300	962	1.501491	0.090900
1052	1.366992	0.029200	960	1.502437	0.087900
1050	1.361263	0.035700	958	1.503680	0.084900
1048	1.356801	0.043700	956	1.504571	0.080900
1040	1.3540d3	0.052100	954	1.504693	0.077100
1044	1.352649	0.060700	952	1.50+712	0.07+100
1042	1.352657	0.069400	950	1.504869	0.070600
1040	1.354351	0.077800	948	1.504829	0.067200
1038	1.350966	0.084500	946	1.504426	0.063500
1036	1.359401	0.090300	944	1.503477	0.059900
1034	1.361545	0.096400	942	1.502493	0.057100
1032	1.364933	0.102200	940	1.501590	0.053900
1030	1.368405	0.107300	938	1.500173	0.050600
1028	1.372112	0.112300	936	1.496610	0.048200
1026	1.376037	0.116800	9.34	1.497542	0.045900
1024	1.380204	0.121100	¥32	1.496599	0.043000
1022	1.384847	0.125100	930	1.495307	0.039900
1020	1.389457	0.120200	928	1.493628	0.036700
1018	1.393986	0-131500	926	1.491639	0.033600
1016	1.398987	0.134700	424	1.489176	0.030300
1014	1.404379	0.137200	922	1.486267	0.027400
1012	1.409687	0.139100	920	1.482712	0.024500
1010	1.414971	0.140900	918	1.478734	0.022500
1008	1.420706	0.142600	916	1.474888	0.021400
1006	1.426577	0.143200	914	1.471221	0.020200
1004	1.432227	0.143400	912	1.467620	0.017700
1002	1.437835	0.143400	910	1.464351	0.019300
1000	1.443274	0.142500	908	1.460908	0.014600
<u></u>	<u>1.448358</u>	0,141600	906	1.457550	0.018800
996	1.453370	0.140400	904	1.454589	0.013900
<u> </u>	1.458219	0.138800	<u>- 902</u>	1,451474	0.013500
992	1.462926	0.137000	900	1.448297	0.019000
990	1.467474	0.134800	898	1.445597	0.019300
988	1.471518	0.132000	896	1.442368	0.019100
946	1.475216	0.129600	894	1,439731	0.018900
984	1.478913	0.126900	892	1.436302	0.013700
982	1.482340	0.123800	490	1.432320	0.014900
980	1.485361	0.120600	858	1.428831	0.019600
978	1.488115	0.117400	896	1.425007	0.020200
9.76	1,490283	0.113800	884	1.421794	0.019900
974	1.492286	0.111100	882	1.417194	0.020200
972	1.494709	0.108300	880	1.412537	0.021300
970	1.497098	0.104600	878	1,407812	0.021700
968	1.498613	0.100600	876	1.402007	002230.0
966	1.499564	U.077100	874	1.395447	0.023900

Table 4. Concluded

<u>v.</u>	_cm ⁻¹	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u> </u>	<u>k</u>
8	72	1.388207	0.026000	780	1.561070	0.040800
8	70	1.380782	0.029800	778	1.556415	0.038600
8	68	1.372965	0.034000	776	1.552100	0.037000
_8	66	1.300437	0.040500	774	1.540418	0.036200
H	64	1.360723	0.045600	772	1.545011	0.035400
8	62	1.350623	0.046500	770	1.542150	0.035200
8	60	1.336091	0.055900	768	1.539608	0.034900
_8	58	1.323013	0.071000	<u>_766</u>	1.537266	<u>0.034500</u>
8	156	1.313643	0.090200	764	1.535351	0.035000
<u> </u>	54	1.307802	0.111900	762	1.533904	0,034500
8	152	1.306292	0.135800	760	1.532353	0.034400
_8	150	<u>1.309310</u>	0.160900	_758	1.531074	0.034200
8	148	1.317713	0.186100	756	1.530161	0.034100
8	46	1.331922	0.210500	754	1.529241	0.033300
8	44	1.351135	0,230300	752	1.527820	0,032400
_8	42	1.373195	0.246000	<u>750</u>	1.526295	0.032300
8	40	1.397124	0,257200	748	1.525184	0,032300
8	38	1.422002	0,264000	746	1.524413	0.032200
8	36	1,446859	0.266300	744	1.523934	0.032000
88	34	1.470876	0.264600	742	1.523406	0.031100
8	32	1.493261	0,259100	740	1.522205	0.030000
8	30	1.512959	0.250300	. /38	1.520739	0.029700
8	528	1.530080	0.240200	130	1.519004	0.029000
8	26	1.544840	0.228400	134	1.510040	0.023300
6	524	1.5500/9	0.215200	730	1.517715	0.029300
	22	1,500005	0.202100	728	1.51/007	0.029200
5	52U	1.5/3005	0.189200	726	1.515912	0.029300
	18	1.5/03+/		724	1.515423	0 028700
e .	310	1.201023	0.154800	722	1.514703	0.028200
	<u>, 14</u>	1 54-7-7	0.154500	720	1.513784	0.027800
с х	21¢ 21¢	1 545425	0.135300	718	1.512753	0.027500
	109	1 586741	0,137300	716	1.511557	0.027500
c ع	106	1.500741	0.127300	714	1.510899	0.024100
	100	1 546478	0 112700	712	1.510512	0.023100
	107	1 586495	0.106400	710	1.509664	0.027500
	302	1.586855	0.100100	708	1.508525	0.028200
-	798	1.587128	0.100100	706	1.507/54	0.028600
	706	1.586744	0 086100	704	1.50/562	0.029900
-	794	1.585936	0.030300	702	1.507667	0.030100
	792	1.584546	0.072100	700		0.030800
-	790	1.582368	0.065000			
	788	1.578935	0,058100			
	786	1.574614	0.052400			
			_ Y = Y Y Y Y Y Y			

 784
 1.570111
 0.043000

 782
 1.565714
 0.044100

Table 5. Condensed MMH Optical Properties at 80° K

v, cm ⁻¹	<u>n</u>	k	v, cm^{-1}	n	k
3700		0.002400	3372	1.402644	0 005100
3690	1.437059	0.001800	3370	1.401617	0.005100
3680	1.436899	0.002200	3368	1 400462	0.005100
3670	1.436474	0.001100	3366	1.300471	0 005000
3660	1.435876	0.001600	3364	1.398416	0.005300
3650	1.435661	0.001600	3362	1.397190	0.006400
3640	1,435365	0.001100	3360	1.395741	0.006700
3630	1.434703	0.001200	3358	1.394245	0.007400
3620	1.434570	0.001300	3356	1.392874	0.008200
3610	1,434100	0.000700	3354	1.391585	0.008900
3600	1.433188	0.000300	⁻ 3352	1,389923	0.009400
3590	1.432317	0.000900	3350	1.387993	0.010400
3580	1.431927	0.000800	3348	1.386141	0.011900
3570	1.431428	0.001000	3346	1.384339	0.013300
3560	1.430575	0.000400	-3344	1.382524	0.015300
3550	1.429794	0.001200	3342	1.381115	0.017600
3540	1,429267	0.001000	3340	1.379941	0.019700
3530	1,428536	0.001000	3338	1.378659	0.021800
3520	1.427590	0.001100	3336	1.377279	0.024300
3510	1.426841	0.001300	3334	1.376199	0.027300
3500	1.425873	0.001300	3332	1.375568	0.030500
3490	1,424796	0.001400	3330	1.375396	0,033700
3480	1.423813	0.002000	3328	1.375731	0.037000
3470	1.422750	0.001800	3326	1.376504	0.039800
3460	1.421499	0.002400	3324	1.377262	0.042200
3450	1.420348	0.002700	3322	1.377877	0.044500
3440	1.4191/0	0.003000	3320	1.378444	0.047000
3430	1 41/033	0.003300	3318	1.379189	0.049600
3420	1.410193	0.003200	3316	1.380765	0.052700
341V "37.00	1.419231	0.003700	3314	1.382556	0.054300
3400	1.411685	0.003400	3312	1.383573	0.055600
3370	1 411005	0.003900	3310	1.384929	0.058400
3304	1.410495	0 004000	3308	1.386967	0.059800
3337	1.409966	0.004000	3300	1.388314	0.060500
1300	1,409470	0.004200	3304	1.389204	0.062200
3388	1.408810	0.004200	3302	1.390/89	0.063900
3386	1.408175	0.004200	3300	1.392047	0.065100
1184	1.407603	0 004500	3270	1.394005	0.065500
3382	1.407009	0.004500	3290	1.374/03	0.066100
3380	1.406340	0.004500		1 306260	U.VO/000
3378	1.405439	0.004300	JC76 7201	1 3076/1	0.070700
3376	1.404279	0.004400	-3270 -7287-	1.37/301	0.010/00
3374	1,403376	0.005000	3286	1.400465	0.073300
				X8,444,44	V . V . J J V V

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Table 5. Continued

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<u>v, cm⁻¹</u>	n	k	v, cm^{-1}	<u>n</u>	<u>k</u>
-3284	1.401603	0.074200	3196	1.461593	0.045800
3282	1.402539	0.075600	3194	1.460434	0.045200
3280	1.403758	0.077200	3192	1.459190	0.044900
3278	1.405138	0.078800	3190	1.457779	0.044700
3276	1.406851	0.080500	3188	1.456259	0.045000
3274	1.408971	0.082100	3186	1.455042	0.046000
3272	1.410725	0.082600	3184	1.454166	0.046900
3270	1.411896	0.084000	3182	1.453604	0.048200
3268	1.413718	0.086300	3180	1,453314	0.049400
3266	1.416358	0.088000	3178	1.453135	0.050600
3264	1.418966	0.089100	3176	1.453386	0.052400
3262	1.421848	0.090700	3174	1.454344	0.053800
3260	1.425261	0.091600	3172	1.455251	0,054500
3258	1.428121	0.091400	3170	1.456000	0,055500
3256	1.430748	0.092300	3168	1.457263	0,056900
3254	1.434385	0.093400	3166	1.458971	0,057500
3252	1.438205	0.092600	3164	1.460555	0.057800
3250	1.441538	0.092100	3162	1.462114	0,058100
3248	1.444833	0.091200	3160	1.463813	0.058200
3246	1.447933	0.089800	3158	1.465536	0.058000
3244	1.450627	0.088400	3156	1.466993	0.057500
3242	1.453444	0.087100	3154	1,468416	0.057300
3240	1.456217	0.085200	3152	1.470127	0.057100
3238	1,458540	0.082800	3150	1.471812	0.056200
3236	1.460330	0.080600	3148	1.473364	0,055600
3234	1.461783	0.078300	3146	1.475164	0.054800
-3232 ⁻	1.463033	0.076400	3144	1.476908	0,053400
3230	1.464445	0.074600	3142	1.478258	0.051800
3228	1.465680	0.072300	3140	1.479437	<u>0,050400</u>
3226	1.466616	0.070200	3138	1.480618	0.048800
3224	1.467562	0.068300	3136	1.481747	0.047100
3222	1.468275	0.065800	3134	1.482579	0.045000
3220	1.468698	0.063800	3132	1.483001	0,043000
3218	1.469096	0,061700	3130	1.483280	0.041300
3216	1.469189	0.059300	3128	1,483645	0.039600
3214	1.469016	0.057400	3126	1.483945	0.037700
3212	1.468707	0,055300	3124	1.484026	0.035700
3210	1.468134	0.053400	3122	1.483708	0.033600
3208	1.467300	0.051700	3120	1,483139	0.031900
3206	1.466257	0.050200	3118	1.482527	0.030400
3204	1.465221	0.049300	3116	1,481961	0.029000
3202	1.464511	0.048500	3114	1.481384	0.027700
3200	1.463765	0.047400	3112	1.480719	0.026300
3198	1.462732	0.046400	3110	1.479987	0.025200

v, cm ⁻¹	<u>n</u>	k	<u>v, cm⁻¹</u>	<u>n</u>	k
3108	1.479318	0.024100	3020	1.448119	0.016800
3106	1.478652	0.023000	3018	1.447622	0.016500
3104	1.477908	0,021900	3016	1.446953	0.016100
3102	1.477003	0.020800	3014	1.446073	0.015800
3100	1.476014	0.020000	3012	1.445070	0.015600
3098	1.475178	0.019400	3010	1.443947	0.015500
3096	1.474461	0,018700	3008	1.442823	0.015600
3094	1.473778	0.018000	3006	1.441719	0.015700
3092	1.473017	0.017200	3004	1.440529	0.015700
3090	1.472081	0.016400	3002	1.439144	0.015800
3088	1.471169	0.016000	3000	1.437545	0.015900
3086	1.470448	0.015500	2998	1.435743	0,016300
3084	1.469756	0.014900	2996	1.433740	0.016800
3082	1.468930	0.014200	2994	1,431529	0.017700
3080	1.467984	0.013600	2992	1.429201	0,019000
3078	1.466965	0.013100	2990	1.426938	0.020300
3076	1.465914	0.012700	5288	1.424710	0.022900
3074	1.464936	0.012500	2986	1.422422	0.025400
3072	1.464138	0.012300	2984	1.420303	0.028800
3070	1.463249	0.011800	2982	1.418511	0.032700
3068	1.462171	0.011500	2980	1.417488	0,037300
3066	1.461106	0.011400	2978	1.417359	0.042600
3064	1.460144	0.011300	2976	1.418435	0.047900
3062	1.459166	0.011200	2974	1.420575	0,053000
3060	1.458116	0.011100	2972	i . 4238ï9	0,057800
3058	1.457064	0.011200	2970	1.428121	0,061800
3056	1,456056	0.011300	2968	1.433352	0,064800
3054	1.454978	0.011400	2966	1.439135	0.066300
3052	1.453946	0.011800	2964	1.444914	0.066100
3050	1.452953	0.012100	2962	1.450158	0.064500
3048	1.451969	0.012600	2960	1.454270	0,061300
3046	1,451127	0.013300	2958	1,456801	0.057500
3044	1.450444	0.013900	2956	1.457596	0.053400
3042	1.449804	0.014600	2954	1.456531	0.049700
3040	1,449367	0.015400	2952	1.454021	0.047500
3038	1.449131	0.016100	2950	1.450925	0.047000
3036	1.448949	0.016600	2948	1.447859	0,048100
3034	1.448824	0.017200	2946_	1.445224	0,050700
3032	1.448921	0,017700	2944	1.443602	0.054800
3030	1.449130	0.017900	2942	1.443640	0.060000
3058	1.449246	0.017800	2940	1.445564	0.065300
3026	1.449190	0.017600	2938	1.449311	0.070400
3024	1.448967	0.017300	2936	1.455067	0.074700
3022	1.448571	0.017000	2934	1.462573	0.077100

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Table 5. Continued

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<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	<u>v,</u> cm ⁻¹	n	k
2932	1.470398	0.076400	2844	1.485554	0.041700
2930	1.477320	0.073800	2842	1.485865	0.040800
2928	1.483139	0.069900	2840	1.486238	0.040500
2926	1,487589	0.064700	2838	1.487099	0 040700
2924	1.490278	0.059000	2836	1.488808	0.040700
2922	1.491555	0.053700	2834	1.491376	0.040900
2920	1,491715	0.048600	2832	1.494404	0.030800
2918	1.490970	0.044200	2830	1.497467	0.037600
2916	1.489581	0,040500	2828	1.500076	0.034300
2914	1.487939	0.037600	2826	1.501745	0.030100
2912	1,486252	0.035300	2824	1.502076	0.025500
2910	1.484606	0.033300	2822	1.501211	0.021300
2908	1.482821	0.031600	2820	1.499596	0.017800
2906	1.480994	0.030300	2818	1,497556	0.014800
2904	1.479217	0.029400	2816	1.495252	0.012500
2902	1.477465	0.028600	2814	1.492854	0.010600
2900	1.475639	0.028200	28)2	1.490403	0.009200
2898	1.473942	0.028200	2810	1,487949	0.008100
2896	1.472500	0.028500	2808	1.485566	0.007400
2894	1.471341	0.028900	2806	1.483230	0.006800
2892	1.470313	0.029300	2804	1.480720	0.006300
2890	1.469377	0.029800	2802	1.478007	0.006200
2888	1.468475	0.030400	2800	1.475160	0.006500
2880	1.467694	0.031200	2798	1.472153	0.007200
2884	1.40/213	0.032300	2796	1.469075	0.008700
2002	1.40/058	0.033200	2794	1.466066	0.010800
2000	1.40/095	0.034100	2792	1.463248	0.013900
2010	1.40/288	0.034800	2790	1.460906	0.018000
2010	1.40/482	0.035300	2788	1.459624	0.023400
20/4	1.40/0/3	0.035800	2786	1.460158	0,029700
2016	1.401170	0.036100	2784	1.462972	0.036000
2010	1.40/014	0.036300	2782	1.468182	0.041500
2000	1.40/102	0.036900	2780	1.475331	0.044900
2844	1.400047	0.037900	2778	1.483367	0.045500
2862	1.400231	0.041400	2776	1.490987	0.043300
2860	1 467203	0.0441000	2//4	1.497061	0.038700
2858	1 469375	0.044200	2112	1.501064	0.033100
2856	1.472236	0.040300	21/0	1.502973	0.027000
2854	1.475549	0.040000	2100	1.503056	0.021500
2852	1.478960	0.049500	2100 	1.501982	0.017000
2850	1.481966	0.047100	2743	1.50043/	0.013500
2848	1.487991	0_045000	2102	1.498044	0.010600
2846	1.485053	0.043100	2750	1.490054	0.008300
	49403433	0.043100	2150	1.494652	0.006700

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<u>v, cm⁻¹</u>	n	k	v, cm^{-1}	<u>n</u>	k
2756	1.492823	0.005500	2540	1.462682	0.001300
2754	1.491159	0.004600	2530	1.462443	0.001500
2752	1.489620	0.003900	2520	1.462203	0.001200
2750	1.488202	0.003400	2510	1.461764	0.001000
2748	1.486959	0.003100	2500	1.461302	0.001000
2746	1.485861	0.002800	2490	1.460909	0.000900
2744	1.484869	0.002600	2480	1,460405	0.000800
2742	1.483966	0.002400	2470	1.459993	0.001000
2740	1.483096	0.002200	2460	1.459689	0.001000
2738	1.482244	0.002100	2450	1.459497	0.001100
2736	1.481533	0.002100	2440	1.459234	0.000900
2734	1.480871	0.002000	2430	1.458920	0.000800
2732	1.480255	0.001900	2420	1.458523	0.000700
2730	1.479652	0,001900	2410	1,458052	0.000500
2728	1.479096	0.001800	2400	1.457435	0.000600
2726	1.478532	0.001800	2390	1.456964	0.000800
2724	1.478041	0.001800	2380	1.456578	0.001100
2722	1.477609	0.001800	2370	1,456267	0.001300
2720	1.477157	0.001700	2360	1.456101	0.001800
2718	1.476690	0,001700	2350	1.456189	0.002000
2716	1.476257	0.001700	2340	1.456318	0.002100
2714	1.475862	0.001700	2330	1.456372	0.001900
2712	1.475470	0.001700	2320	1.456288	0.001800
2710	1.475107	0.001700	2310	1.456200	0.001600
2708	1.474739	0.001700	2300	ï.4559d3	0.001400
2706	1.474398	0.001700	2290	1.455741	0.001200
2704	1.474036	0.001700	2280	1,455420	0.001100
2702	1.473679	0.001700	2270	1.454941	0.000800
2700	1.473314	0.001800	5520	1.454530	0.001200
2690	1,472033	0.002000	2250	1.454392	0.001200
2680	1.470996	0.002200	2240	1.454223	0,001200
2670	1.470088	0.002300	2230	1.453963	0.001100
2660	1.469431	0.002500	2550	1.453650	0.001100
2650	1,468968	0.002500	2200	1.453000	0.001300
2640	1.468513	0.005500	2180	1.452652	0.001500
2630	1.467849	0.001900	2170	1.452468	0.001500
2620	1.467265	0,001800	2160	1.452168	0.001500
2610	1.466640	0.001500	2150	1.451984	0.001800
2600	1.465972	0.001300	2140	1,451969	0.001900
2590	1.465316	0.001300	2130	1.451918	0.001800
2580	1,464750	0.001100	2120	1.451771	0.001800
2570	1.464070	0.001100	2110	1.451603	0.001700
2560	1.463464	0.001100	2100	1,451432	0.001700
2550	1.463013	0.001400	2090	1.451240	0.001600

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Table 5. Continued

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	v, cm^{-1}	<u>n</u>	_ <u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	_ <u>k</u>
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2080	1,450984	0.001500	1688	1 427963	0 004000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2070	1.450680	0 001500	1686	1 427343	0.004000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2060	1-450371	0 001500	1684		0.004400
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2050	1.450074	0.001500	1682	1.426035	0.004700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2040	1.449933	0.001800	1680	1.425122	0.005100
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2030	1 449798	0.001700	1678	1.424216	0.005700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2020	1.449587	0.001700	1676	1.423449	0.006300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2010	1.449353	0.001700	1674	1.422563	0.006900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2000	1.449039	0.001600	1672	1.421604	0.007600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1990	1.448690	0.001800	1670	1.420594	0.008600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1980	1,448435	0.002000	1668	1.419717	0.009700
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1970	1,448551	0.002300	1666	1.418821	0.010900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1960	1.448776	0.002200	1664	1.417998	0.012300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1950	1.448791	0.001700	1662	1.417262	0.013900
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1940	1,448481	0.001300	1660	1.416717	0.015600
1920 1.447596 0.000700 1656 1.415860 0.019300 1910 1.446935 0.000400 1654 1.415685 0.021600 1900 1.446192 0.000400 1652 1.416032 0.024000 1890 1.445492 0.000500 1650 1.416551 0.026000 1880 1.444859 0.000700 1648 1.417163 0.028200 1870 1.444859 0.000700 1648 1.417163 0.028200 1870 1.444325 0.001000 1646 1.418115 0.030500 1860 1.443825 0.001700 1642 1.420650 0.032500 1850 1.443519 0.001700 1642 1.420650 0.034500 1840 1.442988 0.002000 1638 1.424087 0.038600 1820 1.442721 $\overline{0.002000}$ 1638 1.428850 0.044300 1800 1.442356 0.001900 1634 1.428850 0.04300 1800 1.441320 0.001700 1632 1.431294 0.042700 1780 1.449830 0.001700 1630 1.434025 0.043600 1770 1.438918 0.001700 1626 1.445971 0.044600 1740 1.438050 0.002000 1622 1.445971 0.044000 1740 1.437090 0.002000 1622 1.445971 0.044000	1930	1,448079	0.001000	1658	1.416249	0.017400
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1920	1.447596	0.000700	1656	1.415860	0.019300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1910	1.446935	0.000400	1654	1,415685	0.021600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1900	1.446192	0.000400	1652	1.416032	0.024000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1890	1.445492	0.000500	1650	1.416551	0.026000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1880	1.444859	0.000700	1648	1.417183	0.028200
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1870	1.444292	0.001000	1646	1.418115	0.030500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1860	1.443825	0.001300	1644	1.419353	0,032500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1850	1.443519	0.001700	1642	1.420650	0.034500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1840	1.443250	0.001800	1640	1.422170	0.036500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1030	1.442998	0.002000	1638	1.424087	0.038600
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1820	1.442721	0.002000	1636	1.426449	0.040300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1010	1:442330	0.001900	1634	1.428850	0,041500
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1700	1.441009	0.001900	1632	1.431294	0.042700
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1790	1.440500	0.001700	1630	1.434025	0.043800
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1730	1 430830	0.001700	1628	1,437037	0.044400
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1760	1.439830	0.001700	1626	1.440075	0.044600
$\frac{1520}{1740} 1.437090 0.002000 \qquad \frac{1622}{1620} \frac{1.445971}{1.449008} 0.044000 0.043400$	1750	1 4390510	0.001700	1024	1.443059	0.044400
1440 14431030 0.002000 1850 1.444008 0.043400	1740	1.437000	0.002000	1022	1.4457/1	0.044000
1730 1.435897 0.000000 1618 1.450167 0.000000	1730	1.435897	0,002000	1020	1.449000	0.043400
$\frac{1730}{1720} \frac{1}{4} \frac{434527}{4} 0.002100 \qquad \frac{1616}{16} 1.452107 0.042300 \qquad \frac{1616}{16} \frac{1}{16} \frac$	1720	1 434527	0.002100	1010	1.402101	0.042300
1710 1.433028 0.002300 1616 1.433176 0.040300	1710	1.433028	0.002300	1010	1.433170	0.030300
1700 1.431411 0.002700 1014 1.437073 0.038200	1700	1.431411	0.002700	1014	1.457075	0.035200
	1698	1.430800	0.003300	1016	1.461712	0000000
1696 1.430397 0.003400 1608 1.463132 0.035200	1696	1.430397	0.003400	1610	1.467172	0 030200
1694 1.429804 0.003400 1606 1.464018 0.027200	1694	1.429804	0.003400	1606	1.464018	0.027200
1692 1.429234 0.003500 1604 1.464460 0.024100	1692	1.429234	0.003500	1604	1.464460	0.024100
1690 1.428532 0.003800 1602 1.464375 0.021100	1690	1.428532	0.003800	1602	1.464375	0.021100

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Table 5. Continued

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ν,	1	<u>n</u>	k	v, cm^{-1}	<u>n</u>	k
ī	600	1.463878	0.018300	1512	1.433783	0.018100
1	598	1.462952	0.015700	1510	1.433944	0.018400
1	596	1.461696	0.013500	1508	1.434234	0.018800
ī	594	1.460334	0.011800	1506	1.434573	0.018900
1	592	1.459006	0.010300	1504	1.434689	0.018800
ī	590	1.457610	0.009000	1502	1.434564	0.018900
1	588	1.456101	0.007900	1500	1.434490	0.019200
1	586	1.454698	0.007300	1498	1.434532	0.019500
1	584	1.453493	0.006700	1496	1.434503	0.019600
1	582	1.452302	0.006100	1494	1.434343	0.019900
1	580	1.451081	0.005700	1492	1.434180	0,020300
1	578	1.449914	0.005400	1490	1.434170	0.020900
1	576	1.448896	0.005300	1488	1.434268	0.021400
1	574	1.448001	0.005100	1486	1.434401	0.021900
1	572	1.447041	0,004800	1484	Ĩ,434703	0.022600
1	570	1.445983	0.004700	1482	1.435361	0.023100
1	568	1,444962	0.004700	1480	1.436200	0.023200
1	566	1.444062	0.004900	1478	1.436757	0.055200
1	564	1_443237	0.005000	1476	1.436691	0.021900
1	562	1.442545	0.005300	1474	1.436014	0.021400
1	560	1.442089	0.005500	1472	1.435046	0.021500
1	558	1.441631	0.005300	1470	1.434155	0.055500
1	556	1.440855	0.005000	1468	1.433623	0.023200
1	554	1.439844	0.004900	1466	1.433589	0.024400
1	552	1.438746	0.005000	1464	1,433867	0.025100
1	550	1.437645	0.005300	1462	1.433919	0.025400
1	548	1.436598	0.005800	1460	1.433680	0.025800
្រា	546	1.435/44	0.006500	1458	1.433085	0.026100
1	544	1.434992	0.007100	1456	1.431610	0,026400
1	542	1.434297	0.007800	1454	1.429274	0.028100
1	540	1,433729	0,008600	1452	1.426983	0.031700
1	538	1.433187	0,009200	1450	1.425997	0.037400
1	536	1.432572	0.010000	1448	1.427595	0_044500
1	534	1.432107	0.011000	1446	1.432501	0.051400
1	532	1,431869	0.012000	1444	1.440354	0,056400
1	530	1.431762	0.012900	1442	1.450046	0.058300
1	528	1.431744	0.013800	1440	1.460194	0.056700
1	526	1.431765	0.014600	1438	1.469340	0.051500
1	524	1,431886	0.015500	1436	1.475850	0.043300
1	522	1.432269	0.016400	1434	1.478758	0.033900
1	520	1.432784	0.013300	1432	1.478286	0.025200
1	518	1.433162	0.017200	1430	1.475408	0.018200
1	516	1.433405	0.017500	1428	1,471574	0.013700
1	514	1.433608	0°011800	1426	1.467896	0.010800

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	700
14201.4582140.00680013321.4282980.023414181.4553620.00680013301.4294060.024414161.4528620.00760013281.4307280.025414141.4513680.00940013261.4321500.025914121.4512440.01100013241.4335520.026314101.4520270.01180013221.4350510.0266	200
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	00
1416 1.452862 0.007600 1328 1.430728 0.0254 1414 1.451368 0.009400 1326 1.432150 0.0259 1412 1.451244 0.011000 1324 1.433552 0.0263 1410 1.452027 0.011800 1322 1.435051 0.0266	+00
1414 1.451368 0.009400 1326 1.432150 0.0259 1412 1.451244 0.011000 1324 1.433552 0.0263 1410 1.452027 0.011800 1322 1.435051 0.0266	+00
1412 1.451244 0.011000 1324 1.433552 0.0263 1410 1.452027 0.011800 1322 1.435051 0.0266	200
1410 1.452027 0.011800 <u>1322 1.435051 0.0266</u>	300
	500
1408 1,453062 0,011600 1320 1.436666 0.0265	500
1406 1.453892 0.010600 1318 1.438160 0.0261	00
1404 1.454169 0.009000 1316 1.439562 0.0255	50Ō
1402 1.453719 0.007200 1314 1.440851 0.0247	700
1400 1.452635 0.005700 1312 1.441997 0.0236	500
<u>1398</u> 1.451303 0.004500 <u>1310</u> 1.442891 0.0224	+0.0
1396 1.449725 0.003700 1308 1.443533 0.0210	000
1394 1.448218 0.003400 1306 1.444062 0.0198	300
1392 1.446882 0.003200 1304 1.444443 0.0182	20Ò
1390 1.445600 0.003100 1302 1.444444 0.0166	500
1388 1.444393 0.003200 1300 1.444267 0.0151	00
<u>1386</u> 1.443375 0.003400 <u>1298</u> 1.443867 0.0136	500
1384 1.442447 0.003500 1296 1.443270 0.0122	200
$\frac{1382}{1.441469} 0.003600 \qquad 1294 \qquad 1.442554 0.0109$	}0 0
1380 1.440513 0.003900 1292 1.441562 0.0095	500
1378 1.439752 0.004300 1290 1.440383 0.0085	500
1376 1.439199 0.004600 1288 1.439272 0.0077	700
<u>1374 1.438740 0.004700 1286 1.438092 0.0067</u>	100
1372 1.438123 0.004500 1284 1.436650 0.0059	90 0
1370 1.437191 0.004300 1282 1.435150 0.0054	+00
	100
$\frac{1300}{1264} = \frac{1.432037}{1.43204} = 0.004600 = 1278 = 1.432204 = 0.0047$	100
1364 1.433964 0.004900 1276 1.430669 0.0045	500
$\frac{1302}{1360} \frac{1.432000}{1.631736} 0.005300 \frac{1274}{1.62770} \frac{1.429178}{1.631736} 0.005900 \frac{1274}{1.63770} \frac{1.4327178}{1.63770} 0.005900$	>00
	500
	200
	100
	200
	100
$\frac{1262}{1.426475} = 0.012000 = \frac{1262}{1.419057} = 0.0059$	≠00 - 05
1346 1.426028 0.0122000 1200 1.410410 0.0005	0UC
$\frac{1344}{1.425712} = 0.013300 = 1256 = 1.410002 = 0.0009$	900 . 00
	+00
	200
1338 1.426055 0.019200 1250 1.409593 0.0109	300

ν , cm ⁻¹	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	k
1248	1.407677	0.012200	<u>115</u> 0	1.403604	0.022600
1246	1.405810	0.014100	1158	1.401248	0.025700
1244	1.404111	0.016100	1156	1 399252	0.029.00
1242	1.402491	0.018300	1154	1.39799+	0.033500
1240	1.400963	0.020900	1152	1.397309	0.037500
1238	1.399666	0.023700	1150	1.396938	0.041500
1236	1.398631	0.026900	1148	1.397181	0.046100
1234	1.397897	0.030200	1146	1.398370	0.050500
1232	1.397537	0.033900	1144	1.400078	0.054400
1230	1.397666	0.037700	1142	1.402353	0.058400
1228	1.398162	0.041500	7140	1.405508	0.062100
1226	1.399078	0.045600	1138	1.409438	0.064900
1224	1.400734	0.049900	1136	1.413938	0.067000
1222	1.403054	0.053900	1134	1.418773	0.067700
1220	1.406035	0.057900	1132	1.423385	0.067200
1218	1.409074	0.061700	1130	1.427557	0.065700
1216	1.414552	0.064300	1158_	1.431236	0.063300
1214	1.419972	0.067300	1126	1.434041	0.059600
1212	1.425996	0.068700	1124	1.435349	0.055000
1210	1.432476	0.069100	1122	1.434404	0.049700
1208	1.439230	0.068100	1120	1.430700	0.045100
1206	1.445805	0.065500	1118	1.4242.91	0.042500
1204	1.451774	0.061500	1116	1.416419	0.043800
1202	1.456866	0.056200	1114	1,409207	0.049600
1200	1.460472	0.049500	1112	1.404805	0.059100
1198	1.462267	0.042400	1110	1.404862	0.071100
1196	1 462315	0.035300	1108	1,410402	0.083200
1194	1.460641	0.028500	1106	1.420902	0.092700
1192	1,457523	0.022900	1104	1.434980	0,098000
1190	1.453664	0.018600	1102	1.450783	0.097900
1188	1.449460	0.015400	<u>1100</u>	1.465674	0.091000
1186	1.445242	0.013300	1098	1.477234	0.080800
1184	1.441248	0.012000	1096	1.484642	0.067600
1182	1.437422	0.011100	1094	1.487665	0.053100
1180	1.433837	0.010900	1092	1,486165	0.038900
1178	1.430563	0.010900	1090	1.480920	0.026900
7776	1.427389	0.011000	1088	1.473493	0.017900
1174	1.424279	0.011500	1086	1.465208	0.011700
1172	T.421290	0.012100	1084	1.457101	0.008100
1170	1,418291	0.012900	1082	1.449885	0.006000
1168°	1.415173	0.013900	1080	1.443402	0.004800
1166	1.411990	0.015400	1078	1.437518	0.004200
1164	1.408909	0.017400	1076	1.432102	0.003800
1162	1.406137	0.014300	1074	1.426957	0.003700

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v, cm^{-1}	<u>n</u>	k	v, cm^{-1}	n	<u>k</u>
1072	1.421861	0.003500	984	1.519998	0.152500
1070	1.416656	0.003700	982	1.525066	0.147400
1068	1.411513	0.004200	980	1.529640	0.142200
1066	1.406401	0.004800	978	1.533955	0.136800
1064	1.401035	0.005400	976	1.538121	0.131400
1062	1.395247	0,006300	974	1,541816	0.125000
1060	1.388974	0.007600	972	1.544618	0.118600
1058	1.382133	0.009500	970	1.546775	0.112400
1056	1.374761	0.012400	- 968	i.548503	0.106200
1054	1.366981	0.016500	966	1.549993	0.100400
1052	1.359149	0.022300	~ 964	1.551151	0.094100
1050	1.351956	0.030000	962	1.551909	0.088100
1048	1.345971	0.039100	960	1.552165	0.081800
1046	1.341543	0.049400	958	1.551778	0.075600
1044	1.338919	0.060300	956	1.550960	0.070000
1042	1.338126	0,071300	954	1.550041	0.064400
1040	1:339010	0.081900	952	1.548721	0.058800
1038	1.341166	0.091600	950	1.546850	0.053300
1036	1.343738	0.100200	948	1.544545	0.048300
1034 -	1.346479	0.108700	946	1.542155	0.043700
1032	1.350122	0.117600	944	1.539322	0.038900
1030	1.354905	0.125600	942	1.535959	0.034800
1028	1.360225	0.132700	940	1,532667	0.031600
1026	1,365557	0.139000	938	1,529805	0.028400
1024	1.370960	0.145200	936	1.526579	0.024800
1022	1.376824	0.151400	934	1.522698	0.021600
1020	1.383469	0.157200	932	1.518783	0.019600
1018	1,390573	0.162200	. 930	1.515284	0.017600
<u>"1016</u>	1,397955	0.166600	928	1.511856	0.015800
1014	1.405625	0.170600	926	1,508361	0.014000
1012	1.413570	0.173800	924	1.504834	0.012600
1010	1,421799	0.176700	922	1.501175	0.011200
1008	1,430535	0.178800	920	1.497624	0.010500
1006	1.439363	0.179700	918	1,494519	0.010000
1004	1.447669	0.179600	916	1.491566	0.004000
1002	1,455641	0.179500	914	1.488427	0.008200
-1000	1,463927	0.179100	912	1.485029	0.007300
998	1.472064	0.177400	910	1.481763	0.007100
996	1.479740	0.175400	908	1.478814	0.006800
994	1.487404	0.173300	906	1.475705	0.005900
992	1.495039	0.170000	904	1.472351	0.005700
990	1.502093	0.166200	902	1.469024	0.005200
988	1.508437	0.161700	900	1.465588	0.005000
986	1.514401	0.157500	898	1.462122	0.004800

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Table 5. Continued

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ν,	1	n	k	v, cm^{-1}	n	k
	896	1.458576	0.004600	808	1-634190	0.096000
	894	1.454811	0.004400	806	1.631549	0.085700
-	892	1.450906	0 004400	804	1.628331	0.075700
	890	1.446779	0.004300	802	1.624558	0.066900
-	888	1.442332	0.004400	800	1.620357	0.058700
	886	1.437453	0.004600	798	1.615954	0.051500
• •	884	1.432502	0.005500	796	1.611409	0.044900
	882	1.427590	0.006300	794	1.606592	0.038700
	880	1.422271	0,006800	792	1.601273	0.033300
	878	1.416081	0.007500	790	1.596002	0.029100
•	876	1.409251	0.008800	788	1,591070	0.025500
	874	1.401700	0.010500	786	1.586241	0.022100
	872	1.393179	0.012800	784	1,581264	0.019300
	870	1.383720	0.016500	782	1.576471	0.017300
	868	1,373535	0.021500	780	1,571814	0.015600
	866	1.362583	0.028300	· 778	1,567377	0.014700
-	864	1.351283	Ö . 037600	776	1.563565	0.014500
	862	1.340477	0.049600	774	1.560548	0.014300
	860	1.330626	0.063900	772	i,557783	0.013800
	858	1.321543	0.080200	770	1.555087	0.013400
	856	1.313675	0.099900	768	1.552633	0.013300
	854	1.307677	0.122600	766	1,550262	0.012900
	852	1.305289	0.149800	764	1.547939	0.013000
	850	1.309641	0.180800	.762	1.546192	0.013500
	848	1.322076	0.210900	760	1,544893	0.013400
	846	1.340825	0.237600	758	1.543609	0.013200
	844	1.364770	0.260800	756	1.542198	0.012800
	842	1.392886	0.278700	754	1.540870	0.012700
	840	1.423766	0,290700	752	1.539714	0.012500
-	838	1.455830	0.296700	750	1.538611	0.012100
	836	1,487429	0.296100	748	1.537443	0.011800
	834	1,516974	0.290500	746	1,536415	0.011500
	832	1.544244	0,280700	744	1,535314	0.011000
-	830	1.568058	0.266500	142	1.534136	0.010600
	020	1.58/521	0.249700	740	1,533019	0.010400
-	020	1.603041	0.216100	138	1.531853	0.009900
	024		0.214100	730	1.530550	0.009800
	926	1 620200	0 730400	734	1.529585	0.010000
	020	1.630300	0.113000	136	1.528955	0.009900
	010	1 637330	0.103300	/30	1.528222	0.009400
	010	1 437910	0.147300	728	1,527239	0.009000
	B13	1 437330	0.132800	120	1.520142	0.008700
	610 012	1 434104	0.102(00	124	1.525022	0.008600
	910	19070130	0°101000	/22	1.524173	u.uu8800

Table 5. Concluded

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<u>v, cm⁻¹</u>	n	<u>k</u>
720	1.523568	0.00a700
718	1.522886	0.008300
716	1.521881	0.007900
714	1.520519	0.007600
712	1.519295	0.009500
710	1.518690	0.008800
708	1.518333	0.008900
706	1.517686	0.008800
704	1.516879	0.009000
702	1.516373	0.009600
700	•	0.009900

Table 6. Condensed $N_2\,H_4$ Optical Properties at $80^\circ\,K$

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v, cm^{-1}	<u>n</u>	<u>_k</u>	v, cm^{-1}	n	k
3700		0.000100	3372	1.374676	0.009200
3690	1.458706	0.000100	3370	1.370461	0.010400
3680	1.458220	0.000300	3368	1.365487	0.011200
3670	1.457710	0.000100	3366	1.359581	0.013000
3660	1.457023	0.000100	3364	1.353338	0.016100
3650	1.456255	0.000100	3362	1.347232	0.019900
3640	1.455415	0.000200	3360	1.340615	0.024200
3630	1.454748	0.000600	3358	1.333710	0.030100
3620	1.454255	0,000700	3356	1.327041	0.037600
3610	1.453624	0.000500	3354	1.320979	0.046300
3600	1,452659	0.000400	3352	1.315430	0.056500
3590	1.451436	0.000300	3350	1.311311	0.068600
3580	1.450414	0.001000	73348	1.308911	0.081600
3570	1.449592	0.001000	3346	1.308350	0.095300
3560	1,448538	0.001100	-3344	1.310184	0.110100
3550	1.447231	0.001200	3342	1.314661	0.124000
3540	1.446064	0.001700	3340	1.320727	0.136800
3530	1.444703	0.001700	3338	1.328845	0.149500
3520	1.443240	0.002200	3336	1.338745	0.160100
3510	1,441753	0.002700	3334	1.349549	0.168700
3500	1.440475	0.003200	3332	1.362134	0.177100
3490	1.438881	0.003400	3330	1.375026	0.180200
3480	1.437163	0.003700	3328	1,385471	0.181600
3470	1.435272	0.004200	3326	1.394743	0.184700
3460	1.433208	0.004100	3324	1.405322	0.187300
3450	1,430485	0.004400	3322	1.417132	0.188800
3440	1,421487	0.004600	3320	1.428247	0.186300
3430	1.424050	0,005200	3318	1.437653	0.183800
3420	1.420031	0.005200	3316	1.445378	0.180000
3410	1.415112	0.005900	3314	1.452472	0.177300
3400	1,408498	0.005700	3312	1.459166	0.174000
3398	1.407231	0.006000	3310	1.464989	0,169600
3396	1.405532	0.006100	3308	1.469286	0.166200
3394	1.404001	0.006200	3306	1.473747	0.163500
3392	1.402093	0.006400	-3304	1.478355	0.161000
3390	1.400353	0.006600	3302	1.482860	0.157400
3388	1.398297	0.006400	3300	7.487452	0,155000
3386	1.396395	0.007100	3298	1.491449	0.149900
3384	1.394253	0.007200	3296	1.493714	0.145900
3382	1.391931	0.007100	3294	1.495587	0.143200
3380	1.388979	0.007100	`32 92 `	1.498052	0.140900
3378	1.385842	0.007400	3290	1.500664	0,138400
3376	1.382494	0.008000	<u>-3588</u>	1.503433	0.136000
3374	1.378850	0.008300	3286	1.506020	0.133200

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Table 6. Continued

v, cm^{-1}	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	_k_
3284	1.508538	0.130600	3196	1.447591	0.107700
3282	1.511358	0.128200	3194	1.451996	0.115900
3280	1.513998	0.124600	3192	1.457365	0.122300
3278	1.515862	0.121300	3190	1.463068	0.128300
3276	1.517998	0.118800	3188	1.469695	0.134300
3274	1.520497	0.115400	3186	1.477660	0.139000
3272	1.522201	0.111100	3184	1.486041	0.142000
3270	1.523183	0.107700	3182	1.493933	0.143500
3268	1,524252	0.104500	3180	1.501413	0.144900
3266	1.525541	0.101300	3178	1.509327	0.146100
3264	7.526655	0.097600	3176	1.517232	0,145800
3262	1,527368	0.093800	3174	1.525054	0.145500
3260-	1.527603	0.090100	3172	1.533732	0.144800
3258	1.527772	0,086700	3170	1.542385	0.141400
3256	1.527943	0.083300	3168	1,549097	0.136700
3254	1.527695	0,079300	3166	1.555135	0.133600
3252	1.527125	0.076100	3164	1,561860	0.129900
3250	1.526680	0.072700	3162	1,568576	0.124500
3248	1.525984	0.068900	3160	1.574159	0.118300
3246	1.524055	0,065100	3158	1.578499	0.111300
3244	1.522790	0.061500	3156	1.581897	0.105000
3242	1.520576	0.058400	3154	1.584518	0.049000
3240	1,518151	0.055500	3152	1,586491	0.091800
3238	1.515677	0.053100	3150	1.588072	0.085400
3236	1.513249	0.050700	3148	1.589006	0,078800
3234	1.510514	0.048100	3146	1.589344	0.072800
3232	1.507172	0,045700	3144	1.589280	0,066600
3230	1.503591	0.044000	3142	1.588488	0.060600
3228	1.499886	0.042400	3140	1.587168	0.055200
3226	1,495866	0.041000	3138	1,585519	0.050100
3224	1.491344	0.040000	3136	1,583595	0.045500
3222	1,486503	0,039600	3134	1.581419	0.041200
3220	1.481443	0.039900	3132	1,579065	0.037400
3218	1.4/6144	0.040600	3130	1.576626	0.034000
3216	1.470403	0.042200	3128	1.574261	0.031000
3214	1.464604	0.045000	3120	1.5/1850	0.028100
3212	1.459185	0.049100	3124	1,569366	0.025500
3210	1.454197	0.053800	<u>J122</u>	1.500119	0.023200
3208	1.449163	0.059900	3120	1.554191	0.021200
3206	1.440105	0.005/00	5118	1.501/29	0.013200
3204	1.443005	0.044900	011C 2336	1.557450	0.012000
3202	1.443124	0.000000	2114	1.00/291	0.010300
3200	1 4443382	0.000400	3112	1.555201	0.014400
2120	1+444133	0.033000	0115	1*223193	V.U14000

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Table 6. Continued

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<u>v, cm ⁻¹</u>	<u>n</u>	<u>k</u>	v, cm^{-1}	n	<u>k</u>
3108	1-551148	0.013800	3020	1.511096	0,009300
3106	1.549371	0.013100	3018	1.510762	0.009500
3104	1.547637	0.012200	3016	1.510433	0.009600
3102	1.545785	0.011500	3014	1.510094	0.009800
3100	1.544066	0.011100	3012	1.509769	0.010000
3098	1.542550	0.010700	3010	1.509539	0.010300
3096	1.541188	0.010300	3008	1.509372	0.010500
3094	1.539827	0.009800	3006	1.509262	0.010700
3092	1.538395	0.009300	3004	1.509135	0.010800
3090	1.536995	0.009100	3002	1.509004	0.010900
3088	1.535708	0.008800	3000	1.508840	0.011000
3086	1.534518	0,008700	2998	1.508716	0.011100
3084	1.533477	0.008200	2996	1.508615	0.011200
3082	1.532442	0.008200	2994	1.508389	0.011100
3080	1.531311	0.007900	2992	1.508061	0.011300
3078	1.530205	0.007800	2990	1.507960	0.011700
3076	1.529211	0.007700	2988	1.508002	0.011800
3074	1.528313	0.007600	2986	1.508015	0.011900
3072	1.527414	0.007400	2984	1.507946	0.011900
3070	1.526428	0.007200	2982	1,507881	0.012000
3068	1.525470	0.007200	2980	1.507830	0.012100
3066	1.524631	0.007200	2978	1.507772	0.015100
3064	1.523826	0.007100	2976	1.507732	0.012300
3062	1.523023	0.007100	2974	1.507743	0.012300
3060	1.522236	0.007000	2972	1.507714	0.012400
3058	1,521424	0.007000	2970	1.507726	0.012500
3056	1.520640	0.007000	2968	1,507808	0.015000
3054	1,519933	0.007100	2966	1.507889	0,012600
3052	1,519166	0.007000	2964	1.507932	0.012600
3050	1.518396	0.007200	2962	1,508042	0.012700
3048	1.51////	0.007400	2960	1.508152	0.012600
3046	1.51/2/3	0.007500	2958	1.508241	0.012600
3044	1.516694	0.007500	2950	1.508403	0.012600
3042	1.516110	0.007600	2954	1.508572	0.012400
3040	1,515582	0.007700	2952	1.508603	0.012200
3038	1.515056	0.007700	2950	1.508611	0.012100
3036	1.514363	0.007700	2948	1.508039	0.012000
3034	1.513/34	0,008000	2940	1.508690	0.011900
3032	1.513268	0.008300	2944	1.508735	0.011800
3030	1.512839	0.008400	2742	1.508808	0.011700
3028	1.512394	0.008700	2740	1.508883	0.011600
3020	1.512055	0.008900	2730	1.20203	0.011500
3024	1.511/3/	0.009100	2730	1.204514	0.011300
JUCC	1*211423	A.AAAAAA	2734	1,509681	0.010200

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Table 6. Continued

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v, cm^{-1}	<u>n</u>	k	<u>v, cm⁻¹</u>	n	<u>k</u>
2932	1.509190	0.010700	2620	1.490629	0.001300
2930	1.509156	0.010600	2610	1.490226	0.001000
2928	1.509322	0.010600	2600	1.489737	0.000900
2926	1.509586	0.010300	2590	1.489238	0.000700
2924	1.509652	0.009800	2580	1.488821	0.000800
2922	1.509568	0.009500	2570	1.488445	0.000600
2920	1,509552	0,009300	2560	1.487751	0.000300
2918	1.509625	0.009000	2550	1,487087	0.000700
2916	1.509617	0.008600	2540	1.486704	0.000000
2914	1.509490	0.008200	2530	1.486349	0.001000
2912	1.509342	0.008000	2520	1,485897	0.001200
2910	1.509358	0.007800	2510	1.485557	0.001500
2908	1.509340	0.007400	2500	1.485386	0.001900
2906	1.509236	0.007000	2490	1.485309	0.002000
2904	1.509031	0.006700	2480	1.485193	0.002200
2902	1.508888	0.006400	2470	1,485130	0.002300
2900	1.508689	0.006200	2460	1.485118	0.002400
2890	1.507968	0.004600	2450	1.485042	0.002300
2880	1,506735	0.003200	2440	1.484887	0.002300
2870	1.505185	0.002200	2430	1,484814	0.002400
2860	1.503772	0.001700	2420	1.484795	0.002300
2850	1.502395	0,001200	2410	1.484725	0.002200
2840	1,501014	0.000900	2400	1.484678	0.002100
2830	<u>1,499805</u>	0.001100	2390	1.484563	0.001800
2820	1.498823	0.001000	2380	1,484350	0.001600
2810	1,497879	0.001200	2370	1.484136	0.001400
2800	1.497075	0.001300	2360	1.483882	0.001100
2790	1.496372	0.001500	2350	1.483477	0.000800
2780	1.495689	0,001600	2340	1.482989	0.000600
2110	1.495129	0.001900	2330	1.482464	0.000500
2760	1.494701	0.002100	2320	1.481896	0.000400
2/30	1.494341	0.002200	2310	1,481291	0.000500
2740	1.494050	0.002400	2300	1.480784	0.000700
2730	1.493/04	0.002300	2290	1.480348	0.000900
2710	1.473757	0.002400	2280	1.479889	0.001100
2700	1.493293	0.002200	2210	1.4/9549	0.001500
2600	1.492073	0.002000	2200	1.479307	0.001800
2070	1.492519	0.002200	2250	1.479001	0.002000
2000	1 492210	0.002000	2240	1.470092	0.002500
2010	1.471707		2CJV 2200-	1-410091	0.002700
2000	1.471703	0.001900	2200	1 470000	0000200
2640	1 401134	0.001000	2200	1-417000	002600.0
2630	1 /0/404	0 001400 0 001400	2100	1.4/7620	0.003100
CO'10	1.470000	A*AAT00Å	CIIV	7*#12517	0.002900

Table 6. Continued

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<u>v, cm⁻¹</u>	n	<u>_k</u>	v, cm^{-1}	<u>n</u>	<u>k</u>
2160	1.479191	0,002600	1720	1.444804	0.006000
2150	1.479065	0.002400	1710	1,441510	0.007000
2140	1.478917	0.005100	1700	1,437155	0.008300
2130	1.478649	0.001700	1698	1,436184	0.008700
2120	1.478244	0.001400	1696	1,435088	0,009100
2110	1.477745	0.001100	1694	1.434000	0.009500_
210 <u>0</u>	1.477135	0,000900	1692	1,432616	0.009800
2090	1.476514	0.000900	1690	<u>1.431109</u>	0.010400
2080	1.475896	0.000900	1688	1.429401	0.011100
2070	1.475333	0.001100	1686_	1_427563	0.012000
5020	1.474834	0,001300	1684	1.425757	0.013500
2050	1.474360	0.001500	1682	1.424044	0,014800
2040	1.474017	0.001900	1680	1.422047	0.016400
2030	1.473790	0.002100	1678	1.420013	0.018600
5050	1.473627	0.002400	1676	1.418229	0.021300
2010	1.473567	0.002500	<u>1</u> 674	<u>1.4</u> 16951	0.024400
2000	1.473469	0.002500	1672	1.415967	0.027400
1990	1.473304	0.002400	1670	1.415293	0.030700
1980	1.473159	0.002+00	1668	1,415089	0.034200
1970	1,472978	0.002100	1666	<u>1.415253</u>	0.037300
1960	1.472700	0.001900	1664	1.415030	0.040500
1950	1.472274	0.001500	1662	1.416415	0.043700
1940	1.4/1/6/	0.001300	1660	1.417299	0.046400
1930	1,471171	0.001000	1658	1.418200	0.049100
1920	1.470521	0.000800	1050	1.419074	0.051700
1910	1.459764	0.000500	1054	1.420059	0.054400
1900	1.468991	0.000500	1052	1.421345	0.057300
1890	1.408124	0.000400	1000	1,422113	0.059000
1880	1.40/199	0.000400	1040	1.424077	0.06/600
1870	1.400320	0.000800	1040	1 20214	0.067000
1000	1.403300	0.000700	1044	1 / 246/4	0.069400
1020	1 467684	0.000000	1640	1.420040	0.009400
1040	1 462753	0.000900	1640	1.430504	0.071900
1830	1 461639	0.000900	1636	1.431000	0.077500
1020	1.460293	0 001.100	1636	1.436286	0.077500
1910	1 459035	0.001500	1612	1 438874	0.082300
1700	1 457744	0.001900	1630	1 441330	0.085400
1788	1 456346	0 002100	1628	1.443937	0.088400
1730	1 454815	0 002700	1626	1.447094	0.091600
1740	1 4537015	0 001200	1624	1.450640	0.094600
1750	1.451468	0 003200	1622	1.454736	0.044000
1740	1.449527	0.004500	1620	1,459511	0.101200
1730	1.447382	0.005300	1618	1.465072	0 104300
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Table 6. Continued

v, cm^{-1}	n	k	v, cm^{-1}	<u>n</u>	k
1616	1.471608	0.107300	1528	1.479512	0.003800
1614	1.479112	0.109300	1526	1.478707	0.003800
1612	1.487443	0.110800	1524	1.477948	0.003900
1610	1.496815	0.111100	1522	1.477386	0.004100
1608	1.506997	0.109800	1520	1.4768.34	0.004000
1606	1.517636	0.106500	1518	1.476236	0.004000
1604	1.528256	0.100900	1516	1.475618	0.004000
1602	1.537855	0.092400	1514	1.474947	0.003900
1600	1.545385	0.081800	1512	1.474261	0.004100
1598	1,550265	0.069800	1510	1.473692	0.004200
1596	1.552122	0.057200	1508	1.473207	0.004400
1594	1.550892	0.045200	1506	1.472835	0.004500
1592	1.547329	0.035000	1504	1.472403	0.004400
1590	1.542305	0.026700	1502	1.471860	0.004400
1588	1,536589	0.020500	1500	1.471331	0.004500
1586	1,531002	0.016300	1498	1.470899	0.004600
1584	1.525915	0.013200	1496	1.470545	0.004700
1582	1,521290	0.011000	1494	1.470169	0.004600
1580	1.517194	0.009600	1492	1.469727	0.004600
1578	1.513635	0.008500	1490	1.469329	0.004600
1576	1.510594	0.007900	1488	1.468918	0.004500
1574	1,507851	0.007100	1486	1.468420	0.004400
1572	1.505410	0.006800	1484	1.467905	0.004400
1570	1.503276	0.006400	1482	1.467440	0.004400
1568	1.501362	0.006000	1480	1.466836	0,004300
1566	1.499530	0.005700	1478	1.466346	0.004400
1564	1.497778	0.005300	1476	1.465871	0.004500
1562	1.496031	0.005200	1474	1.465427	0.004500
1560	1,494647	0.005300	1472	1.464957	0.004600
1558	1.493526	0.005200	1470	1.464513	0.004600
1556	1,492389	0.004800	1468	1.46406Ï	0.004700
1554	1,491119	0.004600	1466	1.463621	0.004700
1552	1,489900	0.004400	1464	1.463182	0.004800
1550	1.488783	0.004400	1462	1.462741	0.004800
1548	1.487710	0.004200	1460	1.462295	0.004900
1546	1.486616	0.004200	1458	1.461936	0.005000
1544	1.485678	0,004300	1456	1.461641	0.005000
1542	1.484887	0.004300	1454	1.461234	0.004800
1540	1.484116	0.004200	1452	1.460039	0.004700
1538	1.483297	0.004100	1450	1.460072	0.004800
1536	1.482445	0.004000	1448	1.459624	0.004900
1534	1.481686	0.004100	1446	1.459138	0.004800
1532	1.481014	0,004000	1444	1.458597	0.004900
1530	1.480298	0.003900	1442	1.458070	0.004900

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Table 6. Continued

v, cm^{-1}	<u>n</u>	k	ν, cm^{-1}	<u>n</u>	k
1440	1.457532	0.005000	1352	1.436638	0.031900
1438	1.457041	0.005100	1350	1.437489	0.032300
1436	1.456620	0.005200	1348	1.438265	0.032600
1434	1.456120	0.005100	1346	1.438910	0.032700
1432	1.455583	0.005200	1344	1.439392	0.032700
1430	1.455069	0.005200	1342	1.439771	0.032800
1428	1.454533	0,005200	1340	1.440179	0.032800
1426	1.453961	0.005200	1338	1.440428	0.032600
1424	1.453379	0.005200	1336	1.440453	0.032400
1422	1.452667	0.005100	1334	1.440278	0.032300
1420	1.451979	0.005300	1332	1.440044	0.032300
1418	1,451305	0.005300	1330	1.439645	0.032300
1416	1,450616	0.005400	1328	1.439046	0.032400
1414	1,449898	0.005500	1326	1.438320	0.032900
1412	1.449119	0.005500	1324″	1.437570	0,033500
1410	1.448263	0.005700	1322	1.436854	0.034600
1408	1.447479	0.005900	1320	1.436381	0.035900
1406	1.446602	0.006000	1318	1.436138	0.037400
1404	1.445676	0.006300	1316	1.436120	0.039000
1402	1.444764	0.006600	1314	1.436489	0.040900
1400	1.443818	0.006900	1312	1.437261	0.042600
1398	1.442773	0.007300	1310	1,438397	0.044300
1396	1,441816	0.007900	1308	1.439807	0.045700
1394	1.440889	0.008400	1306	1.441413	0.046900
1392	1.439870	0.008900	1304	1.443225	0.048000
1390	1.438733	0.009600	1302	1.445344	0.048800
1388	1.437669	0.010500	1300	1.447606	0.049200
1386	1.436681	0.011500	1298	1,449899	0.049200
1384	1,435816	0,012600	1296	1.452226	0.049000
1382	1.434957	0.01370 <u>0</u>	1294	1.454538	0.048300
1380	1.434204	0.015000	1292	1.456791	0.047400
<u>1378</u>	1.433603	0.016400	1290	1.459014	0.046100
1376	1.433136	0.017700	1288	1.461041	0.044300
1374	1.432763	0.019200	1286	1.462686	0.042200
1372	1,432599	0.020600	1284	1,464034	0.040000
1370	1.432534	0.022000	1282	1.465139	0.037600
1368	1.432549	0.023300	1280	1.465965	0.035000
1366	1.432652	0.024700	1278	1.466378	0.032200
1364	1.432885	0.026000	1276	1.466369	0.029400
1362	1.433334	0.027400	1274	1.466023	0.026700
1360	1.433958	0.028500	1272	1.405403	0.024000
1358	1.4345//	0,029400	1270	1.404.369	0.021300
1356	1.435167	0.030300	1268	1.403014	0.018900
1354	1.435828	0.031100	1266	1.401448	0.010100

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v, cm^{-1}	<u>n</u>	<u>k</u>	<u>v,</u> cm ⁻¹	n	k
1264	1.459650	0-014600	1176	1 343914	0 021800
1262	1.457656	0.012900	1174	1.238622	0.025300
1260	1 455624	0,011400	1172	1 222502	0.029400
1258	1.453546	0.010100	1170	1 129542	0.023900
1256	1.451478	0.004000	1168	1 323743	0.033300
1254	1.449309	0.007900	1166	1 310284	0.044800
1252	1.447067	0.007100	1164	1.315306	0.051100
1250	1.444832	0.006500	1162	1.311931	0.057700
1248	1.442663	0.006000	1160	1,309065	0.064400
1246	1.440516	0.005700	1158	1.306516	0.071200
1244	1.438440	0.005400	1156	1.304333	0.078300
1242	1.436405	0.005300	1154	1.302749	0.085700
1240	1,434413	0.005100	1152	1.301699	0.092900
1238	1.432444	0.005100	1150	1.301033	0.100100
1539.	1.430499	0.005000	1148	1.300804	0.107300
1234	1.428516	0.005000	1146	1.300834	0.114100
1232	1,426565	0.005100	1144	1.300974	0.121000
1230	1.424677	0.005200	1142	1.301315	0.127900
1228	1.422837	0.005300	1140	1.301972	0.134900
1226	1.420948	0.005300	1138	1.303031	0.141900
1224	1.418944	0.005300	1136	1.304412	0.148600
1222	1.416913	0.005500	1134	1.305834	0.155100
1220	1.414907	0.005600	1132	1.307370	0.161700
1218	1.412877	0.005800	1130	1.309141	0.168300
1216	1.410799	0.005900	1128	1,311033	0.174700
1214	1.408691	0.006100	1126	1.313043	0,181300
1212	1.406508	0,006200	1124	1.315478	0.188000
1210	1.404178	0.006300	1122	1.318256	0.194300
1208	1.401806	0.006600	1120	1.320911	0.200200
1206	1.399308	0.006700	1118	1.323220	0.206200
1204	1.396614	0.007000	1116	1.325697	0.212900
1202	1.393981	0.007600	1114	1,328825	0.219700
1200	1.391387	0.007900	1112	1.332357	0.226000
1198	1.388529	0.008200	1110	1.335537	0.231800
1196	1.385404	0.008600	1108	1,338484	0.238200
1194	1.382200	0.009300	1106	1.341507	0.244900
1192	1.379004	0.010000	1104	1.344762	0.251900
1190	1.375045	0.010600	1102	1.348208	0.259400
1100	1+3/1710	0.011200	1100	1.352264	0.267300
1100	1.367444	0.012100	1098	1.356757	0.275400
1107	1 352730	V.UIJ20V	1096	1.361684	0.283600
1102	1.353844	V.VI4/00	1044	1.367533	0.292900
1179	1.340063	0.010300	1092	1.374546	0.301400
1110	11342035	A*A13500	1040	1.382238	0.309900

Table 6. Continued

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v, cm^{-1}	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	_ <u>k</u>
1088	1.390024	0.317600	<u>"</u>] 0 0 0"	1.630409	0.012400
1086	1.398266	0.326300	998	1.624462	0.011400
1084	1.408099	0.335500	-996-	1.618780	0.010200
1082	1.419082	0.343100	994	1.613302	0.009400
1080	1.430306	0.350500	- 492	1.608128	0.008700
1078	1-442494	0.358200	990	1.603123	0.008000
1076	1.455838	0.364900		1.598274	0.007700
1074	1.469816	0.371000	986	1.594039	0.007700
1072	1 484855	0.376900	- 984	1,590130	0.007200
1070	1.501312	0.381900	982	1.586130	0.006500
1068	1.518361	0.384900	980	1.582128	0.006200
1066	1.536046	0.387800	978	1.578186	0.005600
1064	1.555072	0.389400	-976	1.574187	0.005400
1062	1.575124	0.388900	974	1.570468	0.005400
1060	1.595373	0.386400	- 972	1.567069	0.005300
1058	1.615640	0.382200	970	1.563547	0.004800
1056	1.636191	0.376700	968-	17559809	0.004600
1054	1.657529	0.369300	966	1.556291	0.004800
1052	1.679052	0.354700	- 964	1.553006	0.004700
1050	1.699626	0.345000	962	1.549613	0.004500
1048	1.718495	0.328700	960	1.546180	0.004500
1046	1.735684	0.310500	958	1.542782	0.004400
1044	1.750690	0.289800	-956	1.539272	0.004300
1042	1.763199	0.267600	954	1.535621	0.004300
1040	1.772989	0.244000	- 952	1.532073	0.004600
1038	1.779405	0.218800	950	1.528589	0.004700
1036	1.782029	0.193900	- 948	1.524924	0.004700
1034	1.781475	0.169700	946	1.521145	0.005000
1032	1.777737	0.146400	944	1.517365	0.005200
1030	1.771255	0.125200	942	1.513392	0.005400
1028	1.762927	0.106400	940	1.509341	0.005800
1026	1.753253	0.089400	938	1.505195	0.006100
1024	1.742413	0.074800	936	1 500640	0.006200
1022	1.731007	0.062400	934	1.495847	0.006900
1020	1.719643	0.052300	932	1.490949	0.007400
1018	1.708540	0.043600	930	1-485712	0-007900
1016	1.697525	0.036300	928	1.479854	0.008400
1014	1.686868	0.030700	926	1.473294	0.009100
1012	1.676955	0.026300	924	1.466039	0.010400
1010	1.667750	0.022700	922	1.458098	0.012000
1008	i.659253	0.019900	920	1.449208	0.014300
1006	1.651450	0.017500	918	1.439272	0_017500
1004	1.644064	0.015300	916	1.428180	0.022100
1002	1.636975	0.013600	914	1.416084	0.028700
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<u>v, cm⁻¹</u>	<u>n</u>	k	v, cm^{-1}	n	<u>k</u>
912	1.403518	0.038000	824	1.615728	0.015900
910	1.391050	0.050000	822	1.612858	0.015600
908	1.379196	0.065100	820	1.610219	0.015200
906	1.368707	0.083500	818	1.607705	0.014900
904	1,360768	0.105300	816	1.605108	0.014300
902	1.356348	0.129600	814	1.602568	0.014400
900 [°]	1.355713	0,155300	812	1.600549	0.014600
898	1.359043	0.182300	810	1.598790	0.014400
896	1.366957	0.209900	808	1.596988	0.014200
894	1.379791	0.237000	806	1,595258	0.014100
892	1,397002	0.262200	804	1.593580	0.013900
890	1.418278	0.285700	802	1.592138	0.014080
888 °	1,444062	0.307000	800	1,590871	0.013700
886	1.474415	0.324300	798	1.589440	0.013200
884	1,508168	0,336300	796	1.587921	0.013000
882	1.543985	0.342500	794	1,586497	0.012700
880	1.581405	0.343300	792	1.584891	0.012300
878	1.619633	0.336900	790	1.583211	0.012300
876	1.656140	0.322300	788	1,581758	0.012500
874	1.688415	0.301000	786	1.580572	0.012600
872	1.715556	0.274800	784	1.579231	0.012400
870	1.736376	0.244000	782	1.577567	0.012400
868	1.749282	0.210600	780	1.576164	0.013200
866	1.754400	0,178400	778	1,575215	0,013700
864	1.753295	0.148700	776	1.574178	0.013900
862	1.747806	0.123000	774	1.573185	0.014700
860	1.739161	0.100800	277	1.572515	0.015300
858	1.728193	0.082500	770	1.572130	0.016000
856	1.716706	0.069200	768	1.571790	0.010300
854	1.705930	0.058400	766	1.571647	0.016800
852	1.695577	0.049700	764	1.571510	0.016900
850	1.685954	0.043400	762	1.571378	0.016900
848	1.677492	0.038300	760	1,571191	0.017100
846	1.669838	0,034000	758	1,570945	0.016800
844	1.662734	0.030400	756	1,571064	0.017500
842	1,656238	0.027600	754	1.571561	0.016900
840	1.650353	0.025200	752	1.571425	0.015900
838	1.645033	0.023200	750	1.570830	0.015500
836	1.640076	0.021300	748	1.570605	0.015400
834	1+032300	0.019600	746	1.570468	0.014800
832	1.630743	0.018400	744	1.570100	0.014100
030	1.620231	0.017400	742	1.569666	0.013700
828	1.022031	0.016/00	740	1.569135	0,012900
020	1.010704	v.U16100	738	1.568316	0.012400

Table 6. Concluded

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v, cm^{-1}	<u>n</u>	<u>k</u>
736	1.567670	0.012300
734	1.567207	0.011900
732	1.566506	0.011300
730	1.565591	0.011100
728	1.564782	0.011100
726	1.564534	0.011500
724	1.564545	0.011000
722	1,564021	0.010000
720	1.562910	0.009500
718	1.562000	0.009500
716	1.561204	0.009300
714	1.560281	0.009000
712	1.559130	0.009100
710	1.557.882	0.009200
708	1.557026	0.010400
706	1,556631	0.010900
704	1,556340	0,011600
702	1.556398	0.012400
700		0,012600

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Table 7. Condensed N₂O₄ Optical Properties at 20° K

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v, cm^{-1}	<u>n</u>	k	<u>v, cm⁻¹</u>	<u>n</u> ,	k
3700		0.008000	3260	1 493966	0 009200
3690	499297	0.004300	3250	1.493678	0.006600
3680	1.497327	0.005700	1240	1.494334	0.006800
3670	1.497484	0.006200	3230	1.493074	0.005400
3660	1.498334	0.006400	3220	1,492219	0.004700
3650	1-498117	0.004400	3210	1.491081	0.006800
3640	1.496201	0.004000	3200	1.491510	0.005300
3630.	-1-494602	0.005600	3190	1.490370	0.007000
3620	1.496845	0,009400	3180	1.490854	0.006400
3610	1,498653	0.005800	3170	1.490838	-0008200-
3600	1.497778	0.004500	3160	1.491640	0.005900
3590	1.497217	0.0580.0	3150	-1-491600	-0-007600-
3580	1.497205	0.003800	3140	1.489125	0.002100
.3570	1+496267	-0-004500	-3-1-30-	-1-486714-	0.009000
3560	1.496333	0.004700	3120	1.488723	0.009800
3550	1.496005	0.003700	-31-1-0.	-1.490038	0.010000
3540	1.495945	0.004500	3100	1.490795	0.008500
.3530	1.495712	0.003000	3090-	-1.491717-	-0010000-
3520	1.494059	0.005500	3080	1.492068	0.007200
3510	1-492410	J*DD3600	3070.	-1.491858	0.007700
3500	1.493002	0.005600	3060	1.490776	0.005300
3490	1-493238	0.004200	_3050_	-1-490147	0.007200
3480	1.492830	0,004800	3040	1.489976	0.007000
. <u>1470</u>	1.491679	0.004400	3030	1.490489	0.007200
3460	1.491199	0.006000	3020	1.489542	0.005600
1450	1,491986	0.007700	_30 <u>10</u>	1.488386	_0_06300_
3440	1.493518	0.006800	3000	1,487241	0.007000
34.30	1.492068	0.005200	2990	1.487150	0+008500-
3420	1.491320	0.005000	2980	1.486709	0.009400
3410	1 492540	0.007.300	2970	1-488862	0.012600
33900	1 492066	0.006300	2960	1.492317	0.012000
3380	1 491510	0 007700	2950	1.493678.	0.007500
3370	1 4000070	0.007700	2940	1.492098	0.006200
7360	1 49222212	0 007500	29.30	1+490021	0.005100.
3350	1 402021	0.007600	2720	1.488710	0.005200
3340	1.492673	0 007000	2900	488555	0-007300
3330	1 491643	0.007000	2800	1.4071/3	0.007000
3320	1 492182	0 000000	2890	1.40.31.31	n•nne300
3310	1.492624	0.000000	2870	1.400001	0.006800
3300	1.492670	0.002100	2860	1 / 80360	0 006000
3290	1.492736	0.008800	2850	1 6802330	0.000000 0.000000
3280	1.493772	0.008400	2840	1_488700	<u></u>
3270	1,493357	0.007400	2830	1.487902	0.003900

v, cm^{-1}	<u>n</u>	_ <u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>
2820	1.486897	0.003900	2370	1.457409	0.004500
2810	1.486539	0.004300	_2368	1.457230	0.004200.
2800	1.486032	0.003900	2366	1.456261	0.004500
2790	1,485481	0.003900	2364	1,455857	0.004800
2780	1,484605	0.004100	2362	1.455149	0.005100
2770	1.484338	0.004500	2360	1-45475d	0+005300
2760	1.484496	0.005300	2358	1.453461	0.005100
2750	1.484322	0.003800	2356	1,451933	0.006000
2740	1.483535	0.004600	2354	1.450379	0.007500
2730	1.483223.	0.004400	2352	1.449122	009800
2720	1.483125	0.004700	2350	1.449168	0.013900
2710	1.482934	0.004400	.2348.	1,451435	0.017400
2700	1,482447	0.003900	2346	1.455404	0.019900
<u>2690</u>	1.482231	0.004400	2344	1,460969	0.020200
2680	1.481437	0.003000	2342	1.465878	0.016700
2670	1.480093	0.003500	2340	1.467379	0.010500
2660	1.479834	0.004900	2338	1.465220	0.006100
2650	1.479401	.D. 003800	2336	1.461969.	0-004400
2640	1.479104	0.005500	2334	1.459804	0.005000
2630	1.479882	0.005500	_2332	1.4589.19	0.005200
2620	1,479776	0.003800	2330	1.458232	0.005000
. <u>2610</u>	1.478554	0.003900	2328	1.457566	0.005100
2600	1.477847	0.004200	2326	1.457168	0.005100
2590	1.478210	0.005000	2324	1,456610	0.004600
2580	1.478471	0.003900	2322	1.455786	0.004500
2570	1.477831	0.002000	2320	1.455213	0.004700
2560	1.476758	0.002600	5318	1.454451	0.004300
2550	1.475536	0.001400	2316	1-453032	0.004700
2540	1.473459	0.002100	2314	1.453200	0.005200
2530	1 472742		2312	1.452911	0.005100
2220	1.472742	0.001900	2310	1.452372	0.005300
2/10/0	1 462044	0 004000	2305		0.005600
2470	1.467778	0.005100	2300	1.451600	0.005000
2440	1-467322	0 004500	2302	1 461020	0 005400
2450	1.467222	0.005500	2302	1.451000	0.005000
2440	1 466634	0 004100	2208	1 450836	0 008500
2440	1 465333	0.004100	2296	1.450170	0.009900
2420	1.464203	0.004200	2294	1 449327	
2410	1.463500	0.004000	2202	1.448952	0.005200
2410-	1 462502	0 004300	2290	1.448367	0.004900
2390	1-460500	0.004600	2288	1.447728	0.005000
2378	1.459551	0.004300	2286	1.446945	0.005000
2376	1.459585	0.004200	2284	1.446359	0.005100
2374	1.458626	0.004000	2282	1.445673	0.005400
2372	1-458223	-0.003900	.2280	1-445167	0.05400

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<u>ν, cm⁻¹</u>	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	<u>k</u>
2278	1.444700	0.005900	2186	1.419168	0.038200
2276	1.444163	0.005400	2184	1.419316	0.039200
2274	1.443580	0.006000	2182	1.419480	0,041300
2272	1.443243	-0.005700	2180	1-420063	0.042300
2270	1.442347	0.005200	2178	1.420254	0.043700
-2268-	1.441316	-0005500	2176	1-420455	0.045000
2266	1.440476	0.005600	2174	1.421111	0.047100
2264	1-439679	-0-005600	2172	1.422005	0.048000
256S	1.438632	0.005600	2170	1.422550	0.049200
2260	1,437537	0,005500	2168	1.423386	0.050700.
2258	1.435983	0.005500	2166	1.424255	0.051500
2256	1.433971	0,005500	2164	1-424683	0.052300
2254	1.431842	0.006900	2162	1.425417	0.054100
2252	1.430080	0.008100	2160	1.426621	0.055000
2250	1.428338	0.010000	2158	1.427276	0.055500
2248	1.426838	0.012200	2156	1.428066	0.057100
2246	1.425801	0.015200	2154	1,429191	0.058000
2244	1.426060	0.018700	2152	1.430339	0.059800
2242	1.427367	0.021400	2150	1.431268	0.059700
2240	1_428614	0.022900	2148	1.432399	0.060500
2238	1.429990	0.025400	2146	1.433620	0.061600
2236	1.433435	0.024000	2144	1.435150	0.062100
2234	1.437767	0.027400	2142	1.436443	0.062600
2232	1.440926	0.024500	2140	1.437798	0.062900
2230	1.442301	0.021400	2138	1.438884	0.063200
2228	1.441846	0.017000	2136	-1-440137	0.063600-
2226	1.439620	0.014500	2134	1.441513	0.064100
2224	1.436513	0.012400	2132	-1.442932	0.063900
2222	1.433114	0.012400	2130	1.444165	0.064000
2220	1.430104	0.013200	-2128	1.445480	0-053800
2218	1.428286	0.015000	2126	1.446363	0.063500
2216	1.426978	0.016100	-2.124	1 447294	0.063500
2214	1.425597	0,017000	2122	1.448477	0.063900
.2212	1.424213	0.018600	2120	1-449776	0-063200
2210	1.423175	0.019900	2118	1.450780	0.063300
2208	1.422193	0.021500	2116	.1.451.919	0.062700
2206	1.421390	0.023000	2114	1.453197	0.062700
2204	1.420975	0.024900	2112	.1.454331	0-061500
2202	1.420510	0.025900	2110	1.454831	0.060700
2200	1.420111	0.027700	2108	1.455453	0.060500
2198	1.419660	0.028900	2106	1.456185	0.059800
2196	1.419550	0.030700	2104	1.456573	0.059100
2194	1.419452	0.032000	2102	1.457126	0.059200
2192	1_419218	0.033000	2100	1_458246	0.054800
2190	1.418658	0.034800	2098	1.458853	0.057600
2188	1.418884	0.036700	2096	1.459207	0.057200
	بيكب القبلك مكاريهي والوتوالي -				

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>v, cm⁻¹</u>	L	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	_k_
20921.4606340.05530020001.4426320.04090020901.4609570.05530019981.4422640.04150020481.4621800.05350019941.4422630.04200020841.4624100.05350019941.4427170.04300020821.4624410.05140019921.4427170.04300020811.4626480.05120019981.4427010.04300020821.4624410.05140019921.442730.04300020811.4626480.05120019861.441941-0.04350020741.4626480.04930019821.442730.04470020711.4635440.04670019781.442730.04570020721.4634540.04570019761.442730.04570020761.4652850.04510019741.4447180.04550020661.4628390.04430019761.4441380.04550020661.4628430.04430019771.44441380.04550020661.4628430.04260019761.44452300.04580020581.4607810.04260019761.44452300.04580020541.4607810.04260019761.44452400.04580020541.4607840.03950019661.44452300.04500020541.4607840.03950019581.44667490.0470020541.4607840.03950019601.446534 </td <td>2094</td> <td>1.459941</td> <td>0.057000</td> <td>2002</td> <td>1.442732</td> <td>0.040300</td>	2094	1.459941	0.057000	2002	1.442732	0.040300
$\begin{array}{llllllllllllllllllllllllllllllllllll$	2092	1.460634.	-0.,-055300	2000	1-442632	-0.040900-
20881.4616890.05350019961.4420800.06200020841.4621800.05350019921.4420800.04320020841.4624100.05350019921.4427170.04340020801.4626480.05160019961.4424570.04300020781.4626490.0550019861.4427010.04300020741.4629290.04990019821.4427010.04500020741.4629290.04990019821.4427010.04510020721.4635440.04570019781.4426800.04540020661.4623920.04570019781.4426800.04540020661.4623930.04570019771.4425890.04550020661.4623930.04430019721.4441380.04550020661.4623930.04430019721.4441380.04580020641.4623930.04430019761.4445890.04580020541.4620290.04260019661.4452300.04580020541.4614120.04400019621.4467250.0460020541.4620490.04260019661.4452300.04400020541.4620490.04260019661.4452300.04520020541.4661420.04200019581.4467240.04230020541.4670410.03700019561.4467240.04230020541.459460.03700019561.446724 <t< td=""><td>2090</td><td>1,460957</td><td>0.055300</td><td>1998</td><td>1.442264</td><td>0.041500</td></t<>	2090	1,460957	0.055300	1998	1.442264	0.041500
$\begin{array}{llllllllllllllllllllllllllllllllllll$	2088	1.461689	.0,05480.0	1996.	1.442050	-0-042000
2084. $1,462410$ $0,052700$ 1992 $1,442717$ 0.043400 2082 $1,462441$ 0.051800 1990 1.442459 0.043000 2080. $1,4626384$ 0.051200 1988 1.441941 0.043502 2078. 1.462934 0.050500 1986 1.441922 0.044700 2074. 1.462929 0.049300 1982 1.442760 0.045000 2074. 1.462929 0.049300 1984 1.442760 0.045000 2072. 1.463454 0.048300 1980 1.442760 0.045100 2070. 1.463502 0.045700 1978 1.442680 0.045400 2066. 1.462585 0.045100 1974 1.442680 0.046400 2064. 1.462309 0.044300 1970 1.444159 0.046500 2064. 1.462309 0.044400 1974 1.445630 0.045500 2065. 1.462043 0.042600 1966 1.445230 0.045500 2058. 1.466711 0.042600 1966 1.446525 0.044000 2052. 1.459966 0.039500 1956 1.446720 0.042300 2048. 1.458048 0.039200 1956 1.446720 0.042300 2044. 1.458048 0.03700 1950 1.446720 0.042300 2044. 1.458048 0.037200 1954 1.446720 0.032500 2034. 1.456344 0.03700 1956 1.446720 0.0325	2086	1.462180	0.053500	1994	1.442080	0.043200
$\begin{array}{llllllllllllllllllllllllllllllllllll$	2084	1,462410	0,052700	-1992-	1.442717.	-0.043400
20801+4626880.05120019861.4419410.04350020781.4629340.05050019861.4419410.04350020741.4629390.04930019841.4427010.04470020741.4629290.04930019821.4427010.04470020741.4634540.04830019801.4427330.04510020701.4635020.04870019781.4427330.04510020701.4635020.04570019781.4426800.04570020651.462550.04510019741.4425890.04580020641.4620430.04510019701.44411580.04580020621.461120.04400019701.44411380.04580020581.4620290.04260019661.4452300.04550020581.46616120.04100019641.4465240.04360020541.4667810.04660019621.4465250.04360020551.4584840.03920019581.4465240.04230020461.4583480.03920019541.4467200.04800020441.4553440.03850019521.44667490.04070020441.4553440.03820019541.4467200.04260020441.4553440.03720019541.4467450.03660020441.4553440.03520019521.44667810.03660020341.4553860.03570019441.444752<	2082	1.462441	0.051800	1990	1.442459	0.043000
2078 1.462934 0.050500 1986 1.441922 0.044700 2074 1.463031 0.049300 1982 1.442760 0.045000 2074 1.4630454 0.048300 1982 1.442733 0.045100 2070 1.4630454 0.046700 1978 1.442733 0.045100 2070 1.46302 0.045700 1978 1.442733 0.045700 2066 1.462309 0.045700 1977 1.442738 0.045500 2064 1.462309 0.044300 1970 1.444138 0.045500 2064 1.462309 0.044300 1976 1.444138 0.045500 2054 1.462043 0.044300 1966 1.445230 0.045500 2054 1.461012 0.044000 1962 1.446524 0.042500 2054 1.461042 0.044000 1962 1.446524 0.042600 2054 1.461042 0.03900 1958 1.446524 0.042600 2054 1.458948 0.039200 1954 1.446740 0.042700	2080	1.462688	0.051200	1988	-1+441941-	-0-043500-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2078	1.462934	0.050500	· 1986	1.441922	0.044700
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2076	1.463031	0.049300	1984.	-1.442660-	-0.045000-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2074	1,462929	0.043900	1982	1.442701	0.044700
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2072	1.463454	-0-048300	1980	1.442733	-0.0451-00-
20681.4631110.04570019761.4430090.04570020641.4625850.04510019741.4435890.04640020641.4623090.044430019721.4441380.04580020621.4619130.04430019701.4441590.04580020581.4620430.04260019661.4452300.04550020581.4620790.04260019661.4452300.04550020541.460120.04100019641.4455550.04360020551.4607810.04060019621.4465550.04360020501.4589450.03930019561.4467200.04380020541.4583680.03920019541.4467200.04380020501.4589450.03920019541.4467200.04380020481.4553480.03920019541.4467490.04070020441.4571780.03850019521.44667490.0380020401.4563940.03790019501.4461370.03830020411.4566410.03620019421.44563120.03660020381.4556620.03720019441.445620.03250020301.4522160.03570019401.4426650.03150020321.4535860.03570019381.4425650.02160020241.4465540.03570019341.4348370.02250020241.4465540.03570019321.42249	2070	1.463502	0.046700	1978	1.442680	0.045400
20661.4625850.04510019741.4435890.04640020641.4623090.04430019721.4441380.04550020621.4619130.04400019701.4441590.04580020581.4620430.04340019661.44452300.04550020581.4620290.04260019661.4452300.04550020541.4607810.04060019621.4465590.04400020521.4509660.03950019661.4465240.04230020501.4589450.03940019581.4465240.04230020481.4583480.03920019541.4467490.04070020441.4577780.03850019521.44664370.03830020421.4577180.03720019481.44664370.03830020411.4556420.03720019441.4447250.03460020381.4556420.03720019441.4447250.03250020381.4556450.03570019441.4447250.03250020301.4522160.03550019381.4415620.02940020221.4485550.03610019341.4373100.02550020241.4447440.03570019381.4426550.02460020321.4554610.03610019341.4437310.02550020241.44561610.03610019341.4415620.02940020251.4465440.03750019321.432149	2068	1.463111	0.045700	1976	-1.443009.	-0+045700-
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2066	1.462585	0.045100	1974	1.443589	0.046400
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2064	1.462309	0.044300	1972	1.444138.	_0_045500_
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2062	1.461913	0.044000	1970	1.444159	0.045800
20581.4620290.04260019661.4452300.04550020561.46016120.04100019641.4459550.04520020541.4607810.04060019621.4462990.04400020521.4599660.03950019601.4465350.04400020501.4589450.03950019581.4465240.04230020481.4589480.03920019541.4467490.04070020441.4571780.03850019521.44664880.03910020421.4571080.03790019501.4461370.03830020421.4571080.03720019481.4456930.03660020381.4556320.03720019461.44451120.03660020341.45553130.03570019441.4447250.03250020341.4556420.03570019441.4445640.03250020341.4558660.03570019441.4447250.02750020301.4522160.03560019381.4415620.02940020221.4485550.03610019341.4373100.02250020241.4497440.03570019261.4298550.02150020241.4465440.03720019381.421490.02350020241.4465440.03720019321.4321490.02250020241.4465440.03720019321.4328710.02100020241.4465640.03720019261.426921<	2060	1,462043	0.043400	<u> 1968 </u>	1.444672	D. U45800
20561.4616120.04100019641.4459550.045200 2054 1.4607810.04060019621.4465950.044000 2052 1.4599660.03950019601.4465550.043600 2050 1.4589450.03940019581.4465240.042300 2048 1.4583480.03920019541.4467200.041800 2044 1.45877780.03850019521.4466480.039100 2044 1.4577780.03850019501.4461370.038300 2042 1.4571080.03790019501.4461370.036600 2034 1.4553940.03720019461.4451120.036600 2034 1.4556320.03720019461.4451120.036000 2034 1.4546610.03620019421.4445040.032500 2034 1.4545610.03570019401.4426650.031500 2034 1.4546610.03570019381.4415620.029400 2032 1.4535860.03570019381.4415620.025500 2026 1.450160.03610019341.4373100.025500 2024 1.4485550.03610019321.4348370.024800 2022 1.4485550.03610019301.4221490.023500 2024 1.4485440.03740019221.4269210.021600 2024 1.4485440.03740019261.4269210.023500 2024 1.4485440.	2058	1.462029	0.042600	1966	1.445230	0.045500
20541.4607810.04060019621.4462590.044000 2052 1.4599660.03950019601.4465350.043600 2050 1.4589450.03940019581.4465350.043600 2048 1.4583480.03930019561.4467200.041800 2046 1.4580880.03920019541.4467490.040700 2044 1.4577780.03850019521.4466480.033100 2042 1.4571080.03790019501.4461370.038300 2040 1.4563980.03720019481.445693D.036600 2038 1.4556320.03720019461.4451120.036000 2034 1.4556360.03570019441.444725D.034200 2034 1.4546610.03620019421.4436040.032500 2032 1.4535860.03570019401.4426650.031500 2034 1.4506160.03610019381.4415620.029400 2028 1.4506160.03610019341.4373100.025500 2024 1.4485550.03610019301.4321490.023500 2022 1.4485550.03720019261.4269210.024800 2022 1.4485550.03720019261.4269210.021600 2014 1.4469470.03720019261.4269210.021600 2016 1.4465650.03790019181.4223710.021000 2016 1.4465650.	2056	1.461612	0.041000	1964	1+445955	-0+045200.
2052 1.459966 0.039500 1960 1.446585 0.043600 2050 1.458945 0.039400 1958 1.446524 0.042300 2048 1.458348 0.039300 1956 1.446720 0.041800 2046 1.458088 0.039200 1954 1.446749 0.040700 2044 1.457178 0.038500 1952 1.446648 0.033100 2042 1.457108 0.037900 1950 1.446633 0.038300 2042 1.457108 0.037200 1948 1.445633 0.036600 2038 1.455632 0.037200 1944 1.445633 0.036000 2034 1.454661 0.036200 1944 1.444565 0.032500 2032 1.453586 0.035700 1944 1.442665 0.032500 2032 1.453586 0.035700 1944 1.443604 0.032500 2032 1.45344 0.035900 1938 1.443604 0.025500 2028 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449744 0.035700 1932 1.434837 0.024800 2024 1.446947 0.037200 1932 1.429855 0.023100 2024 1.446947 0.037200 1926 1.426921 0.021600 2014 1.446947 0.038600 1922 1.420252 0.020400 2014 1.446947 0.038600 1920 1.4169	2054	1.460781	0.040600	1962	1.446259	0.044000
2050 1.458945 0.039400 1958 1.446524 0.042300 2048 1.458348 0.039300 1956 1.446720 0.041800 2046 1.458088 0.039200 1954 1.446749 0.040700 2044 1.457778 0.038500 1952 1.446638 0.033100 2042 1.457108 0.037900 1950 1.446137 0.038300 2040 1.456394 0.037000 1996 1.446137 0.038300 2038 1.455682 0.037200 1948 1.4445593 0.036600 2038 1.455682 0.037200 1944 1.444725 0.034200 2034 1.455682 0.037200 1944 1.444725 0.032500 2034 1.455686 0.035700 1944 1.444725 0.032500 2032 1.453586 0.035700 1940 1.442665 0.032500 2030 1.452216 0.035900 1938 1.441562 0.029400 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.448744 0.037200 1926 1.428871 0.021100 2022 1.446544 0.037200 1928 1.429855 0.021100 2024 1.446747 0.037200 1926 1.426921 0.021600 2024 1.446747 0.037200 1926 1.426921 0.021000 2016 1.446747 0.038600 1922 1.42	2052	1.459966	0.039500	1960	1.446535	0.043600
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2050	1.458945	0.039400	1958	1.446524	0,042300
20461.458088 0.039200 19541.446749 0.040700 20441.457778 0.038500 19521.446688 0.033100 20421.457108 0.037900 19501.446137 0.038300 20401.456394 0.037600 19481.445693 0.036600 20381.455682 0.037200 19461.445112 0.036000 20341.455682 0.037200 19441.444725 0.034200 20341.455661 0.036200 19421.443644 0.032500 20321.453586 0.035700 19401.442665 0.031500 20301.452216 0.035900 19381.441562 0.029400 20281.453616 0.036100 19341.437310 0.025500 20261.449784 0.035700 19321.434837 0.024800 20221.448555 0.036100 19301.432149 0.023500 20241.449784 0.037200 19281.429855 0.023100 20241.449784 0.037200 19281.429855 0.023100 20221.448554 0.037200 19261.426921 0.021600 20141.446987 0.037200 19241.423871 0.021000 20141.446262 0.038600 19201.416999 0.020000 20141.446565 0.037900 19181.412439 0.019500 20141.446265 0.038300 19201.416999 0.022000	2048	1.458348	0.039300	1956	1.446720	_0.041800
2044 1.457778 0.038500 1952 1.446648 0.033100 2042 1.457108 0.037900 1950 1.446137 0.038300 2040 1.456394 0.037600 1948 1.446137 0.038300 2038 1.455682 0.037200 1948 1.445693 0.036000 2036 1.455682 0.037200 1946 1.445112 0.036000 2036 1.455682 0.037200 1944 1.444725 0.034200 2034 1.455661 0.036200 1942 1.443604 0.032500 2032 1.453386 0.035700 1940 1.442665 0.031500 2030 1.452216 0.035500 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439894 0.027500 2026 1.449784 0.035700 1932 1.434837 0.024800 2024 1.449784 0.035700 1932 1.429855 0.023500 2024 1.449784 0.037200 1928 1.429855 0.023100 2020 1.448554 0.037300 1924 1.429855 0.021000 2014 1.446262 0.038200 1922 1.420252 0.02000 2014 1.446241 0.038600 1920 $1.4169u9$ 0.020000 2014 1.446265 0.038300 1918 1.420321 0.019500 2014 1.446276 0.038600 1920 1.4169	2046	1,458088	0.039200	1954	1.446749	0.040700
20421.4571080.03790019501.4461370.038300 2040 1.4563980.03760019481.4456930.036600 2038 1.4556820.03720019461.4451120.036000 2036 1.4553130.03720019441.4447250.034200 2034 1.456610.03620019421.4436040.032500 2032 1.4535860.03570019401.4426650.031500 2030 1.4522160.03560019381.4415620.029400 2028 1.4513440.03590019361.4398980.027500 2026 1.4506160.03610019341.4373100.025500 2024 1.4497840.03570019321.4348370.024800 2022 1.4485550.03610019301.4321490.023500 2020 1.4467870.03720019261.4298550.021000 2016 1.4469870.03780019241.4238710.021000 2014 1.4462620.03860019201.4169990.020000 2014 1.4462640.03780019181.4124390.019500 2008 1.4462650.03790019181.4124390.019500 2008 1.4437760.03880019141.4031210.021300 2004 1.4432720.03950019121.3980180.022200	2044	1,4577.78	0.038500	1952.	1.446688	-0-033100-
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2042	1.457108	0.037900	1950	1.446137	0.038300
2038 1.455682 0.037200 1946 1.445112 0.036000 2036 1.455313 0.037200 1944 1.444725 0.034200 2034 1.455661 0.036200 1942 1.443604 0.032500 2032 1.453586 0.035700 1940 1.442665 0.031500 2030 1.452216 0.035600 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439898 0.027500 2026 1.450616 0.036100 1934 1.437310 0.025500 2022 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.021000 2016 1.446747 0.037200 1926 1.423871 0.021000 2016 1.446544 0.037300 1924 1.4223871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.446745 0.038300 1918 1.412439 0.019500 2008 1.443776 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2040	1.456398	0,037600	<u>1948</u>	1.445693	-0-036600-
2036 1.455313 0.037200 1944 1.4444725 0.034200 2034 1.454661 0.036200 1942 1.443604 0.032500 2032 1.453586 0.035700 1940 1.443605 0.031500 2030 1.452216 0.035600 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439898 0.027500 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.446987 0.037200 1928 1.429855 0.021600 2018 1.446987 0.037200 1926 1.420871 0.021600 2014 1.446544 0.037800 1924 1.420871 0.021000 2014 1.446281 0.038600 1920 1.416909 0.020000 2012 1.446291 0.038600 1920 1.416909 0.020000 2018 1.444745 0.038300 1918 1.423871 0.019500 2008 1.444745 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2038	1.455682	0.037200	1946	1.445112	0.036000
2034 1.454661 0.036200 1942 1.443604 0.032500 2032 1.453586 0.035700 1940 1.442665 0.031500 2030 1.452216 0.035600 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439898 0.027500 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.023100 2010 1.446987 0.037200 1926 1.426921 0.021600 2014 1.446584 0.037300 1924 1.420252 0.02000 2014 1.446262 0.038600 1920 1.416909 0.020000 2012 1.446291 0.038600 1920 1.416909 0.020000 2012 1.446275 0.038300 1918 1.407929 0.019500 2008 1.444745 0.038300 1914 1.403121 0.021300 2004 1.443272 0.039500 1912 1.398018 0.022200	2036	1,455313	0.037200	1944	1.4447.25	-0-0-34200-
2032 1.453586 0.035700 1940 1.442665 0.031500 2030 1.452216 0.035600 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439898 0.021500 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.021100 2018 1.446987 0.037200 1926 1.426921 0.021600 2014 1.446534 0.037800 1924 1.420252 0.02000 2014 1.446565 0.03800 1920 1.416909 0.020000 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.443776 0.038300 1916 1.407929 0.019500 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398018 0.022200	2034	1.454661	0.036200	1942	1.443604	0.032500
2030 1.452216 0.035600 1938 1.441562 0.029400 2028 1.451344 0.035900 1936 1.439898 0.021500 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.023100 2010 1.446987 0.037200 1926 1.426921 0.021600 2014 1.446544 0.037300 1924 1.420252 0.020400 2012 1.446262 0.038600 1920 1.420252 0.02000 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.407929 0.019900 2008 1.443776 0.038300 1914 1.403121 0.021300 2004 1.443272 0.039500 1912 1.398618 0.022200	2032	1.453586	0035700	1940	-1-442665	-0.031500-
2028 1.451344 0.035900 1936 1.439898 0.027500 2026 1.450616 0.036100 1934 1.437310 0.025500 2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.023100 2010 1.446787 0.037200 1926 1.426921 0.021600 2016 1.446584 0.037800 1924 1.423871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.014900 2004 1.443776 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398018 0.022200	2030	1.452216	0.035600	1938	1,441562	0.029400
20261.4506160.03610019341.4373100.02550020241.4497840.03570019321.4348370.02480020221.4485550.03610019301.4321490.02350020201.4477050.03660019281.4298550.02310020181.4469870.03720019261.4269210.02160020161.4465840.03780019241.4238710.02100020141.4462620.03820019221.4202520.02040020121.4462910.03860019201.4169090.02000020101.4456650.03790019181.4124390.01950020081.4437760.03880019141.4031210.0213002004-1.4432720.03950019121.3986180.022200	2028	1.451344	0.035900	1936	1.439898	_0.021500_
2024 1.449784 0.035700 1932 1.434837 0.024800 2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.023100 2018 1.446987 0.037200 1926 1.426921 0.021600 2016 1.446584 0.037800 1924 1.423871 0.021000 2014 1.446584 0.038200 1922 1.420252 0.020400 2014 1.446262 0.038600 1920 1.416909 0.020000 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398018 0.022200	2026	1.450616	0.036100	1934	1.437310	0.025500
2022 1.448555 0.036100 1930 1.432149 0.023500 2020 1.447705 0.036600 1928 1.429855 0.023100 2018 1.446987 0.037200 1926 1.426921 0.021600 2014 1.446584 0.037800 1924 1.423871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038800 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500- 1912 1.398618 0.022200	2024.	1.449784	0.035700	1932	1.434837	0.024800
2020 1.447705 0.036600 1928 1.429855 0.023100 2018 1.446987 0.037200 1926 1.426921 0.021600 2016 1.446584 0.037300 1924 1.423871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398018 0.022200	2022	1.448555	0,036100	1930	1.432149	0.023500
2018 1.446987 0.037200 1926 1.426921 0.021600 2014 1.446584 0.037800 1924 1.423871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2020	<u>1,4477u5</u>	0.036600	<u>1928</u>	1.429855	0.023100
2016 1.446584 0.037800 1924 1.423871 0.021000 2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2018	1.446987	0.037200	1926	1.426921	0.021600
2014 1.446262 0.038200 1922 1.420252 0.020400 2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038300 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398018 0.022200	2016	1.446584	0.037300	<u>1924</u>	1.423871	_0_0_21000_
2012 1.446291 0.038600 1920 1.416909 0.020000 2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2014	1.446262	0.038200	1922	1.420252	0.020400
2010 1.445665 0.037900 1918 1.412439 0.019500 2008 1.444745 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2012	1.446291	0.038600	<u>1920</u>	1.416909	0_020000
2008 1.444/45 0.038300 1916 1.407929 0.019900 2006 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398518 0.022200	2010	1.445665	0.037900	1918	1,412439	0,019500
200b 1.443776 0.038800 1914 1.403121 0.021300 2004 -1.443272 0.039500 1912 1.398618 0.022200	2008	1,444745	0.038300	1619	1.407929	0.019900
2004 -1.443272 0.039500 <u>1912 1.398518 0.022200</u>	2006	1.443776	0.038800	1914	1,403121	0.021300
	-20.04-	-1.443272	0-039500-	1912	1.398618	0.052200

<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	v, cm^{-1}	n	k
1910	1 000400				
1909	1.393402	0.024400	1818	1.388174	0.003400
1906	1 202034	-V-V20700	1816	1,381149	-0-0-0-1800
1900	1.303024	0.029700	1814	1.374900	0.004400
1902	1 271061	0.033000	1815	1.368/5/	0.004600
1902	1 367265	0.045300	1810	1.351350	0.004900
1898	1 262260	0.023300	-1808	-1-354432	-0-005500-
1896	1 3505200	0.052600	1806	1,346233	0.005700
1894	1.355879	0.069500	1903	1-338008	-0+005300
1892	1.354654	0.080700	1902	1.320029	0.005900
1890	1.355531	0.092200	1000	1 334464	-0.000000
1888	1.359107	0.103800	1790	1.300034	0.011000
1886	1.364079	0.113900	1704	1 2703/12	-0-011-300
1884	1.370658	0.123600	1702	1.264056	0.020400
1882	1.378685	0.133000	1790	1 245071	0.026000
1880	1.388427	0.140200	1788	1.224907	0.038000
1878	1.399431	0.147400	1786	1.203689	0.054500
1876	1,412729	0.152000	1784	1.184443	0.075500
1874	1.426224	0.153300	1782	1.164240	0.101000
1872	-1-440082	0.153100	1780	1.149955	0.137400
1870	1,453924	0.150000	1778	1.144651	0.178300
1868	1.467148	-0-143600	1776	1.148784	0.216800
1866	1.477455	0.134500	1774	1.161297	0.258900
1864.	-1-485744.	0.125300	1772	1-191300	0.296400
1862	1.492520	0.115800	1770	1.226440	0.310300
1860	-1.498727_	.0.,105200	1768	1.243997	0.303100
1858	1.502664	0.093100	1766	1.246580	0.316100
-1856.	-1-,505165	-0-081100	1764	1.264544	0.344900
1854	1.505005	0.067900	1762	1.289567	0.347700
1852	1-502302	-0.055100	<u>) 760 </u>	1-308365	0.343200
1850	1.496902	0.044300	1758	1.316026	0.344400
1848.	1.491339	-0,035400	1756	1.317127	0.342600
1846	1.484326	0.026600	1754	1.311884	0.352200
1.844-	-1-476500	-0-019500	1752_	1.297578	.0.3567.00
1842	1.40/046	0.014400	1750	1.274600	0.393100
1020	-1-459410	-0-010500-	1748	1.274460	0.459800
1030	1.451005	0.008300	1746	1.299024	0.520800
1934	1 476407	-V	1744	1.351107	0.590200
1034	1.430402	V.UU5/UU	1742	1.426981	0.641300
1830	1.423550	0 004400	1740	1,534353	-0.644-4-400
1828	1.417760	0.004400 0.004500	1738	1.048354	0.606/00
1826	1.411575	0.004000	メイゼロ- 1734	1003534	
1824	1.405776	0.004000	1134	1 021002	V.35100
1822	1.399658	0.004300	1 -1-3-2- 1720	1 0724476	0.3034000
1820	1 394633	0.004500	1709	1 502370	0.2490VV
		• • • • • • • •		TAGAICAA	-vest1000

<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	ν , cm ⁻¹	<u>n</u>	_ <u>k</u>
1726	1.740178	0.154700	1626	1.385748	0.031900
1724	1.692302	0.1637-00	1624	1.373951	0.047700
1722	1.668821	0.179000.	1622	1.368970	0.062000
1750	1.662639	.0.193700	1620	1.336453.	0.051100
1718	1.665217	0.204200	1618	1.300077	0.107200
1716	1-680276	0.210200	.1.616_	1.301040	_0.,182800.
1714	1.696413	0.205300	1614	1,346900	0.236400
1712	1.718936	_0 <u>_1</u> _90400	16.12.	1.401141	0.264100
1710	1.725987	0.166200	1610	1,466342	0.262200
1700	1.690078	0.040400	1608	1.508262	0.232000
1698	1.677598	0.028700	1606	1.504733	0.169700
1696.	1.655248	0.051800	1604	1.501972	0.208700-
1694	1.643646	0.017100	1602	1.523884	0.181200
1695	1-626929	-0-013900	-7-600-	1.527627	-0-1-62-900-
1690	1.617045	0.011900	1598	1.519945	0.156600
-1688	.1.,603921	0.011600	-1596-	1-520518	-0-1-55000-
1686	1.596453	0.010900	1594	1.520505	0.154300
1684	1.586502	0.011400	_1592_	1-524874	_0.153900
1682	1.580808	0,010600	1590	1.528463	0.153000
1.68.0	1-572241	0.010300	1588	1.5347.96	0.151300
1678	1.566919	0.010100	1586	1.539644	0.147900
1676	1.559405	0.003900	-1584	1 545558	0.144300
1674	1.554644	0.009800	1582	1.550426	0.139800
1672	1.547.778	0.009400	1580-	1.555692	-0.133400
1670	1.543475	0.009700	1578	1.558676	0.127400
1.668	1.537.223	0.003100	.1576.	1,562564	0.122300
1666	1.532799	0.009000	1574	1.565994	0.115100
1664	1.526681	0.009100	1572	1,568685	-0-1-06400-
1662	1.522858	0.009200	1570	1.568252	0.097500
1660	1.516859.	0.008400	.1568.	1.567424	_0090400_
1658	1.512328	0.008600	1566	1.565935	0.083600
1656	1,506214	0.008700	1564	1-564269	_0.076100.
1654	1,501955	0.009100	1562	1.561021	0.069600
1652	1.495879	-0-0091-00	1560	1-557778	0.063500-
1650	1.491199	0.009600	1558	1.553005	0.057400
1648	1,485225	0,010400	1556	1.548199	.0.05.3300.
1646	1.480976	0.010800	1554	1.542757	0,049400
1644	1.474439	_0_010400	1552	1.537890	_0046900_
1642	1.468660	0.011100	1550	1,533330	0.045300
1640	1.461718	0.012200	1548-	1-2529397	_0_042600_
1638	1,455800	0.012500	1546	1.524610	0.040900
1636	1.447411	0.012800	1544.	1.520274	-0-039400-
1634	1.439202	0.014000	1542	1.515190	0.038100
1632	1.428445	0.015000	1540	1.510782	_0,038300.
1630	1.416995	0.018000	1538	1.507156	0.038800
1628	1,401832	0.021700	1536	1.503905.	0.037800

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Table 7. Continued

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<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>
1534	1.499771	0.037800	1442	1.458066	0.153800
1532	1.496124	0.038100	1440	-1.464355	-0-155200-
1530	1.492458	0.038600	1438	1,470590	0.154200
1528	1,489361	0.039400	-1436-	-1-4767-06	-0-151-300-
1526	1.486338	0.039900	1434	1.480285	0.147700
<u>1524</u>	1.483281	0.040200	1432	-1-,483451	-0-144700
1522	1.479301	0.040600	1430	1.486396	0.142900
1520	1.476485	0.043200	1428	1,490034.	0,138700
1518	1,474277	0,044000	1426	1,491803	0.134500
<u>1516</u>	1,471957	0,044600	1424	1,493061	0.130100
1514	1,468553	0.045400	1422	1,492368	0.125700
1512	1.466438.	0.047700	1420	1.492189	-0-123500
1510	1.463989	0.048200	1418	1.491498	0.120300
1508	1.461392	0.049200	1416	1,491288	0.117700
1506	1.458784	0.051000	1414	1.489803	0.115000
1504	1.457231	0.052300	1412.	1.488513	0.112400
1502	1.453790	0.052900	1410	1.486641	0.111800
1500	1-451046	0.055500	1408	1.486098.	0.109900
1498	1.448889	0.058200	1406	1.484817	0.109000
1496	1.447102	0.058900	1404	1-484047	-0.,106900
1494	1.444786	0.062100	1402	1.482743	0.106200
1492	1,4428-6	0.062600	1400	1-482100	0-104100
1490	1.439918	0.065500	1398	1.479667	0.102000
1488.	1.438194	0.068200	1396	1.47.7954.	0.101900
1486	1,436953	0,070900	1394	1.476493	0.101400
1484	1.434842	0.071300	1392	1-475229	0.099800
1482	1.431591	0,074500	1390	1.473168	0.100200
1480	1,429543	0.078000	1388	1.472859	0.100200
1478	1.427676	0.081100	1386	1.472875	0.100000
1476	1.425192	0.083900	1384	1.473890	0.098200
1474	1.423480	0.089600	1382	1.473425	0.095000
1472	-]_423194	0-093400	.1.380.	1.472106	_0.091700
1470	1.422727	0.096900	1378	1.469547	0.089400
-1-468-	- 1 _422081-	0.100600-	1376	1.469057	.0.+089000
1466	1,420131	0,103300	1374	1.467574	0.083300
-1464-	1-41-8692	0.109900	1372	1.464926	<u>.0.,07.4900</u>
1462	1.419444	0,116300	1370	1.460193	0.074900
1460	1.420594	-0120400-	1368.	1-456627	-0-072500
1458	1,421616	0.126700	1366	1.451537	0,068000
.1456	1.424411	0.132700-	1364	1-447132	_0_065400
1454	1.427408	0,137000	1362	1.441044	0.050900
1452	1.431554	0.143100	1360	1.434.040	0.056100
1450	1.436860	0,146800	1358	1.424446	0.053000
.1448.	1.442829	0.150000	1356	1-415840	-0-021300
1446	1,447637	0.150700	1354	1,404250	0.049000
1444.	1.452945.	0,153500	1352	1.392642	-0.049600

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ν, cm ⁻¹	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	k
1350	1.380736	0.052800	1258	1.692505	1.050200
1348	1.371121	.0.,055600_	<u>.1256</u> _	1.815905	1.056700
1346	1.359229	0.058300	1254	1.935321	1,054900
1344	1.348749	0.063900	1252	2.077381	1.026200
1342	1.337737	0,069600	1250	2.211649	0.973000
1340	1.328800	0.075800	1248_	-2-374649	0.873700
1338	1.318591	0.082300	1246	2.553176	0.744800
_1_336_	1-310050-	-0-0-56800-	1244	2.555391	0.320000
1334	1.298564	0.094200	1242	2.394396	0.216200
-1-335-	1.287516	-0101000-	1240	2,272919	0.153500
1330	1.275334	0.111200	1238	2.210900	0,129300
-1358-	-1-,264287-	0-118300-	.1236_	2.148242	0.105400
1326	1.249452	0.128600	1234	2.110494	0.085200
1324-	1.234309.	-0.139600-	1232	2.065501	0.069700
1322	1.215532	0.154700	1230	2.036674	0.057700
-1-320-	-1-195664	-0-173700	1228	2.002502	0047600
1318	1.175208	0,202900	1226	1.979851	0,039600
.1.3.1.6_	1.161743	0.239500	1224	1,952419	0.033100
1314	1.151171	0.278600	1222	1.934182	0.027800
.1312	1.152134.	.0.,330500-	1220	1.911860	0.023700
1310	1.168616	0.383300	1218	1.896991	0.019800
1308	1-203089	-0.427400-	1216	1.878200	-0-017000-
1306	1.246053	0.460000	1214	1.865843	0.014500
1304	.1_297.071	0.476000	1212	1.850205	0,012400
1302	1.346231	0.476600	1210	1.839950	0.010000
1300	1.391206	.0.,458600-	1508	-1-824946	0.006800
1298	1.419504	0.428000	1206	1.812627	0.005600
1296-	1-433499	-0393600-	-1-2-04-	-179921-6-	-0.,009300-
1294	T.434835	0,362400	1202	1.793832	0.011900
1292	1,424147	0.323900-	-1-500-	-1-,-785488-	0.010000
1290	1.379094	0.282900	1198	1.779830	0,010200
1288	1.320484	-0.289300-	_1196.	-1771175	-0.008900
1286	1.268154	0.318200	1194	1.765505	0.008200
1284	1-234176	-0-361500-	-1192	1.757567	0,008900
1282	1.207789	0.413700	1190	1.752915	0.007400
1280	1-201306	_0_47160.0_	-1-1-88-	-1.745071	-0.007600
1278	1.202387	0.529200	1186	1.740771	0.007900
1276	.1.214129	.0.,578800_	11-84-	-1-,734844	0.008300
1274	1,228476	0.639300	1182	1.731021	0.007000
1212.	.1.25561 <u>8</u>	0.688400	-4-180-	-1.7247-15	0.007600
1270	1.274627	0,739000	1178	1.721457	0.007700
1268	1.314135	0.810200	-1176.	-1.716696-	-00-0-7-800-
1266	1.367464	0.870400	1174	1.713567	0.006700
_1264	1.433910	0.913400	_1.1.7.2	_1_708217_	0006600-
1595	1.502440	0.972900	1170	1.705521	0.007000
1590	1-593700	1.005900	_1168 .	.1.700784	-0.+0057-0-0-
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v, cm^{-1}	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	<u>k</u>
1166	1.697432	0.005900	1074	1.599520	0.004000
1164	1.692754	-0-0-0-0-2-0-	-1-0-7-2	-1.,5963 75	-0.007600
1162	1.690391	0.006400	1070	1.596341	0.007300
.1160.	1.686262	0.006400	-1-0-68-	1.594518	-0.006300
1158	1.683957	0.006400	1066	1.592116	0.005400
.1156.	1.679941	_ J_005600 _	-1-064	1-588440	0.006000
1154	1.677871	0.006800	1062	1,585259	0.006200
_1152-	1-67.4458.	-0-0-7-300-	1060	-1-,582462	0,010100
1150	1.673123	0.007200	1058	1,581212	0.010200
]]48_	4-670259	-0.007000	-1.056-	1.580249	-0-014000
1146	1.668050	0.005400	1054	1.580683	0.012300
1144	1.664164	0,006100	1052	1-218918	-U-U12200
1142	1.662076	0,005800	1050	1.574087	0.014300
1140	1-658640	0.006100	1048-	1-208024	-0-014200
1138	1.656763	0.006700	1046	1.504043	0.027100
1136	1.654127	0.007000	-1-044-	4-503204	-V.VCJOVV
1134	1.652673	0.007100	1042	1.501333	0.026700
1132	1.649.960	0.007000	1040-	1	0.037000
1130	1.648193	0.007200	1030	1.570720	0 040200
1128	1.645083	0,00/300	1030	1 570973	0.035600
1120	1.044052	0.009600	1034	1.5/07/2	0.034200
1129	1.440706	0.007.300	1030	1.565119	0.047500
1122	1 4 3 4 4 4 7 3 0	0.001300	1028	1.572839	0.048800
1118	1 430260	0 007500	1026	1-578248	0.049500
1110	1 436839	0.007300	1024	1.578696	_0042400
1114	1 435116	0 008300	1022	1.578699	0.049100
1112	1.634066	0.008200	1020	1.583724	.0.048000
1110	1 633631	0.005500	1018	1.588448	0.045900
1104	1.629514	0.005500	1016	1.588747	.0.038100
1106	1-627235	0.005100	1014	1.585778	0.036400
1104	1-623609	0.005000	1012	1.580888	.0.033900.
1102	1.622457	0.008100	1010	1.579997	0.040900
1100	1.6227.04	0.008500	1008	1.582669.	.0.040600.
1098	1.622275	0.005800	1006	1.584525	0.038900
1096	1.619284.	0.005200	1.004	1.583133.	-0-036600-
1094	1.617108	0.005100	1002	1.582799	0.038100
1092	1.614785	0.005300	1000	1.583023	0.037000
1090	1.613141	0.005600	998	1.582977	0,035900
1088	1.610202	0004900	996_	1-578452	-0+033300
1086	1.609365	0.008000	994	1.574364	0.039400
1084	1.607520	0.005800	992	1.581998	0.052200
1082	1.607856	0.003900	990	1,592471	0.044500
1080	1.606277	0.005300	988	1.593994	0.035100
1078	1.603398	0.003800	986	1.596/68	0.037300
1076	1-600664	0.007800	984.	1.593917	<u>0.018300</u>

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Table 7. Continued

<u>v, cm⁻¹</u>	<u>n</u>	_ <u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>_k</u>
982	1.583136	0.018500	890	1,524393	0.000001
<u>980</u>	1,577999	0.024900	_888_	1.514780	100000-0
978	1.575938	0.022000	886	1.510694	0.006300
976	1.5729.05	0.028200	884	1.507636	-0-00-3300
974	1.574094	0.030300	882	1.505685	0.009100
972	1.571452	0.00650.0	_880_	1,500600	0002800
970	1.569807	0.036400	878	1.494607	0.007800
968	1-577805	0.044500-	876	1.486478	0.007200
966	1.588011	0.037700	874	1.478515	0.013300
.964.	1.589471	0.027900	872	1.473470	_0_025100
962	1,583855	0,019700	870	1.474701	0.031400
-960-	1.5781.08	0.022100	868	1.472433_	.0.0.35500
958	1,576005	0.023600	866	1,468931	0,042300
956	1-5//034.	0.025100	_864_	1.468474	_0_056400
954	1.577104	0.022200	862	1.482503	0.071400
.952	1.5(31.6.	TO 01 300	_860_	1.499004	_0.065700
950	1.575432	0.024700	858	1.501332	0.047600
948	1.573018	0.015000	<u>850</u>	1.491467	0,045400
940	1.570103	0.021900	854	1.486774	0.049800
	1-7-070	-0-+-05-3400-	852	1.4456.32	0.053100
946	1.519010	0.013000	85V 3/8	1.485569	0.053800
_340~	1 57 64-10	-V -VI 3VVV	<u>040</u> 946	1.404710	
730	1.564177	0.000000	. 040 844	1.404174	0.063400
-7-30-	1 552345	-VVVVVV-1-	8/2	1.400301	
757	1.553250	0.000000	840	1.4900272	0.057500
-7-32-	1 560039	0 020700	838	1 484023	0.054600
928.	1.563032	0.015400	836	1-484428	0.055300
926	1.559598	0.014300	834	1.480659	0.047900
224	1.559668	0.014100	832	1.472124	0.044700
922	1.563351	0.013100	830	1.457641	0.046400
920.	1-501600	0.000900	828	1.451977	0.059900
918	1.554646	0.007300	826	1.455167	0.070600
-916	1-552985	0.004000	824	1.452363	0.057900
914	1.549131	0.002200	822	1.442294	0.071400
912.	1-539644	.0.000001	820	1.437298	0.075100
910	1.538414	0.014800	818	1.436159	0.088900
-908-	1.546258	0.015500	816	1.436714	0.094000
906	1.549261	0.005500	814	1.438726	0.101700
904	1.543140	0.000001	812	1.442478	0,108700
902	1.536951	0.000001	810	1.446129	0.108000
900	1-532585	0.000001	_808_	1.445197	-0-110200
898	1.526810	0.000001	806 8	1.450553	0.117200
.896	1.,519624.	0.001900	_804-	1.456234	-0.110500-
894	1.522051	0.015400	802	1.447613	0.095400
.892	1,528656.	0.08800.0	_ B .0 V	1.433002-	-0.,103+00-

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Table 7. Concluded

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<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	<u>k</u>
798].426403	0.111600	706	1.728410	0.033000
.7.96.	1,421243	0,115900-	704	1.709982	0.056600
794	1.411204	0.122700	702	1.714605	0.067700
-792-	-1-405181-	0.140400-	700		0.0665.00
790	1.407999	0.158200			
788	-1-419335	0.170700-			
786	1.433717	0.175100			
-784-	1.4487-86	0.168300-			
782	1.452278	0.147700			
780	1-438102-	0-125000-			
778	1.407410	0.115600			
<u>776</u>	1.377107	0,124100-			
774	1.352937	0.140200			
772	1.325826	0.147600			
770	1.284990	0.169800			
768	1.247588	0.219000-			
766	1.227981	0.285200			
_764	1.231862	0,355200-			
762	1,249166	0.416900			
760	1.283432	0.431400			
758	1.321189	0.524600			
.756.	1.3687.48	J.576200-			
754	1.420791	0.616400			
152	1.489047	0.652200-			
750	1.564527	0.680700			
<u>748</u>	1.646607	0.674300			
746	1.716405	0,674800			
144	<u>1.799191</u>	0.659200			
742	1.874199	0,634100			
740	1.975029	0.596600			
738	2.086542	0.526600			
<u>_736</u>	2,119870	0.306800			
734	2.057575	0.223200			
732	1.969515	0.133300			
730	1.923767	0.178800			
728	1.916525	0.150200			
726	1,908514	0.121100			
724	1.880579	0:103600			
722	1,866783	0.084700			
720	1:842905	0,072300			
718	1.821935	0.054900			
.716	1.798801	u_060800.			
714	1.790910	0.057200			
712	1-122733	0.047000			
710	1.767195	0.051600			
7.08	1.752021	n * n3e3no-			

Table 8. Condensed N_2O_4 Optical Properties at $80^\circ\,K$

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	v, cm^{-1}	<u>n</u>	<u>k</u>	v, cm^{-1}	n	k
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3690		0.000100	3250	1.531317	u <u>.ov</u> 1∎70
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3680	1.537580	0.000100	3240	1.529993	0.002654
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3670	1.537455	0.000637	3230	1.530051	0.003294
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3660	1.537535	0.000100	3550	1.530103	0.003657
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3650	1.536958	0.000339	3210	1.529700	0.002399
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3640	1.536140	0.000100	3200	1.528644	0.003355
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3630	1,537063	0.003014	3190	1.528301	0.003192
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3620	1.538148	0.000606	3180	1.526786	0.002925
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3610	1.537757	0.000255	3170	1.525064	0.004094
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3600	1.536909	0.000100	3160	1.523422	0.000427
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3590	1,536821	0.000100	3150	1.522805	0.009300
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3580	1.536319	0.000181	3140	1.526781	0.015801
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3570	1.536246	0.000212	3130	1.531234	0.012301
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3560	1,535975	0.000366	3120	1.530665	0.003935
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3550	1.535899	0.000100	3110	1.531611	0.013817
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3540	1.535367	0.000100	3100	1.534380	0.009765
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3530	1.535248	0.000306	1090 1	1.535431	0.008771
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3520	1.534841	0.000100	3080	1.534176	0.005118
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3510	1.534498	0.000100	3070	1.532686	0.004643
3490 1.533231 0.000517 3050 1.531441 0.004345 3480 1.533158 0.001812 3040 1.529387 0.003165 3470 1.533470 0.001312 3030 1.527538 0.003191 3460 1.532983 0.001462 3020 1.524851 0.004963 3450 1.532711 0.002302 3000 1.522672 0.009108 3440 1.532771 0.002302 3000 1.522672 0.009108 3420 1.531956 0.001403 2990 1.522117 0.014736 3420 1.531224 0.003508 2980 1.522117 0.01478 3410 1.532234 0.003508 2980 1.522117 0.02322 3400 1.533172 0.003736 2950 1.549516 0.034650 3390 1.5332744 0.003119 2940 1.540858 0.003410 3380 1.532703 0.004162 2930 1.535266 0.003172 3360 1.533112 0.003916 2920 1.533006 0.00394 3330 1.533097 0.003859 2890 1.531214 0.002467 3310 1.532653 0.002881 2860 1.531214 0.002467 3310 1.532477 0.002881 2860 1.530401 0.002467 3300 1.532477 0.002881 2860 1.531214 0.002467 3300 1.532477 0.002881 2860 1.53042	3500	1.533759	0.000261	3060	1.531216	0.005121
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3490	1.533231	0.000517	-305U	1.531441	0.004345
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3480	1.533158	0.001812	3040	1.529387	0.003165
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3470	1.533470	0.001312	3030	1.527538	0.003191
3450 1.532744 0.001805 3010 1.524354 0.006775 3440 1.532771 0.002302 3000 1.522672 0.009108 3430 1.531956 0.001403 2990 1.523903 0.012163 3420 1.531420 0.003508 2980 1.522117 0.014478 3410 1.532234 0.004356 2970 1.524751 0.020322 3400 1.533172 0.003999 2960 1.540516 0.034650 3390 1.533254 0.003736 2950 1.549048 0.003112 3380 1.532894 0.003119 2940 1.540858 0.003410 3370 1.532703 0.004162 2930 1.535246 0.003109 3360 1.533112 0.003916 2920 1.535048 0.003610 3350 1.533149 0.003396 2900 1.533006 0.002877 3320 1.532530 0.002881 2880 1.531214 0.002467 3310 1.5322426 0.003192 2870 1.530062 0.002392 3300 1.532477 0.003784 2860 1.530401 0.002911 3290 1.532247 0.003193 2860 1.528141 0.002567 3260 1.532247 0.003193 2860 1.528141 0.002567 3260 1.532247 0.003193 2860 1.528141 0.002567 3260 1.532246 0.003193 2840 1.52	3460	1.532983	0.001462	3020	1.524851	0.004963
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3450	1.532/44	0.001805	3010	1.524354	0.006775
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3440	1.532171	0.002302	3000	1,522672	0.009108
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3430	1,531730	0.001403	2990	1,523903	0.012163
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3420	1.531420	0.003508	2980	1.522117	0.014478
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3410	1.032234	0.004355	2970	1.524/51	0.020322
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3400 3300	1 5030572	0.001794	2960	1.540510	0.034650
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3340	1.033604	0.003130	2950	1.549040	0.005112
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3300	1.532074	0.0003119	2940	1.040000	0.003410
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3370	1.532103	0.003014	2930	1.232200	0.003172
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3350	1.623244	0.003710	2920	1.535040	0.003010
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3330	1.533149	0.003717	2910	1 533006	0.003109
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1120	1 533047	0 003559	2700	1.535000	0.003374
3310 1.532536 0.002881 2860 1.532424 0.002407 3300 1.532426 0.003912 2870 1.5300624 0.003305 3300 1.532426 0.003189 2860 1.530401 0.002911 3290 1.5322477 0.003784 2850 1.529320 0.002385 3280 1.532226 0.003195 2840 1.528869 0.002557 3270 1.532614 0.003668 2830 1.528141 0.002604 3260 1.532236 0.002390 2820 1.528113 0.002557	3330	1 532653	0.003393	2070	1 531214	0.002467
3300 1.532426 0.003189 2860 1.530401 0.002911 3290 1.532477 0.003784 2850 1.529320 0.002385 3280 1.532226 0.003195 2840 1.528869 0.002557 3270 1.532614 0.002390 2820 1.528141 0.002604 3260 1.532236 0.002390 2820 1.528113 0.002557	1110	1.532510	0 001912	2000	7	0.002407
3290 1.532477 0.003784 2850 1.529320 0.002385 3280 1.532226 0.003195 2840 1.528869 0.002557 3270 1.532614 0.002390 2820 1.528141 0.002604 3260 1.532236 0.002390 2820 1.528113 0.002552	3300	1.532426	0 004189	201V 2440	1,530401	0.003303
3280 1.532226 0.003195 2840 1.528869 0.002557 3270 1.532614 0.003668 2830 1.528141 0.002604 3260 1.532236 0.002390 2820 1.528113 0.002552	-3200	1.532477	0.003784	עשמני	1.529320	-0.002711 -0.002711
3270 1.532614 0.003668 2830 1.528141 0.002304 3260 1.532230 0.002390 2820 1.528113 0.002552	3280	1.532226	0.004145	2030	1.528864	0.002567
3260 1.532236 0.002390 2820 1.528113 0.002552	3270	1.532614	0.00.1668	2040	1.528141	0.002331
	3260	1.532230	0.002390	2820	1.528113	0.002552

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>k</u>
$\begin{array}{c} 2800 & 1.527155 & 0.002403 & 2392 & 1.501657 & 0.002427 \\ 2790 & 1.526232 & 0.002073 & 2388 & 1.501427 & 0.002560 \\ 2760 & 1.525033 & 0.002447 & 2388 & 1.500434 & 0.002425 \\ 2750 & 1.525032 & 0.002488 & 2382 & 1.500243 & 0.002427 \\ 2750 & 1.526232 & 0.002488 & 2382 & 1.500243 & 0.002427 \\ 2750 & 1.5263947 & 0.002401 & 2380 & 1.499849 & 0.0022428 \\ 2730 & 1.523165 & 0.002504 & 2378 & 1.499849 & 0.0022458 \\ 2730 & 1.523211 & 0.002534 & 2376 & 1.499138 & 0.002578 \\ 2710 & 1.52376 & 0.002205 & 2374 & 1.499849 & 0.002578 \\ 2710 & 1.521916 & 0.002334 & 2372 & 1.498250 & 0.002691 \\ 2100 & 1.521916 & 0.002542 & 2376 & 1.499138 & 0.002578 \\ 2640 & 1.520910 & 0.002549 & 2366 & 1.497105 & 0.003025 \\ 2670 & 1.519305 & 0.002693 & 2366 & 1.497105 & 0.003025 \\ 2670 & 1.519305 & 0.002693 & 2366 & 1.496498 & 0.003163 \\ 2660 & 1.519300 & 0.00321 & 2364 & 1.495575 & 0.003361 \\ 2660 & 1.516324 & 0.004351 & 2360 & 1.497572 & 0.003819 \\ 2640 & 1.516324 & 0.004351 & 2360 & 1.497575 & 0.003364 \\ 2630 & 1.51970 & 0.002646 & 2352 & 1.494749 & 0.002837 \\ 2650 & 1.518420 & 0.002636 & 2352 & 1.494749 & 0.002837 \\ 2590 & 1.518796 & 0.002646 & 2354 & 1.494719 & 0.002876 \\ 2500 & 1.518400 & 0.002636 & 2355 & 1.494713 & 0.012391 \\ 2590 & 1.51970 & 0.002646 & 2364 & 1.507473 & 0.018509 \\ 2570 & 1.518808 & 0.001591 & 2346 & 1.507473 & 0.003758 \\ 2550 & 1.518482 & 0.001232 & 2338 & 1.502345 & 0.003464 \\ 2530 & 1.51210 & 0.001192 & 2344 & 1.503583 & 0.003464 \\ 2530 & 1.51210 & 0.001192 & 2334 & 1.507472 & 0.003758 \\ 2550 & 1.518482 & 0.00153 & 2340 & 1.503583 & 0.003464 \\ 2560 & 1.517210 & 0.001232 & 2338 & 1.502345 & 0.003677 \\ 2480 & 1.50734 & 0.002589 & 2322 & 1.499274 & 0.002777 \\ 2480 & 1.50734 & 0.002589 & 2322 & 1.499274 & 0.002777 \\ 2480 & 1.50734 & 0.002589 & 2322 & 1.497280 & 0.002605 \\ 2430 & 1.50748 & 0.002347 & 2336 & 1.50724 & 0.002777 \\ 2480 & 1.50734 & 0.002589 & 2322 & 1.497280 & 0.002680 \\ 2430 & 1.50748 & 0.002347 & 2316 & 1.496514 & 0.002763 \\ 2440 & 1.502649 & 0.002397 & 2316 & 1.496514 & 0.002763 \\ 2440 & 1.502649 & 0.$	2810	1.527320	0-002475	2394	1.502004	0.002435
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2800	1.527155	0.002463	2392	1.501657	0.002427
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2790	1.526232	0.002073	2390	1.501427	0.002562
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2780	1.525937	0.002507	2388	1.501194	0.002465
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2770	1.525214	0.002271	2386	1.5009.34	0.002500
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2760	1.525083	0.002487	2384	1.500608	0.002422
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2750	1.524232	0.002188	2382	1.500243	0.002424
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2740	1.523947	0.002401	2380	1.499849	0.002496
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2730	1.523165	07002504	2300	1.499524	0.002588
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2720	1.523211	0.002584	2376	1.499134	0.002578
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2710	1.522276	0.002205	2376	1.498755	0.002691
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2/00	1.521916	0.002334	2372	1.498226	0.002619
2640 1.520716 0.002542 2366 1.497105 0.003025 2670 1.519305 0.0032693 2366 1.496498 0.003163 2660 1.519305 0.003527 2362 1.496575 0.003367 2660 1.519305 0.003527 2362 1.494240 0.003819 2640 1.516324 0.004351 2362 1.494259 0.005246 2630 1.519903 0.012112 2358 1.49259 0.005246 2620 1.523263 0.003153 2356 1.494795 0.001762 2610 1.520714 0.002636 2352 1.494213 0.012391 2590 1.518450 0.002636 2352 1.494213 0.012391 2590 1.518796 0.002636 2352 1.494213 0.012391 2590 1.518796 0.002636 2352 1.494213 0.012391 2590 1.518796 0.002636 2352 1.494213 0.012391 2590 1.518712 0.003249 2348 1.504773 0.018101 2580 1.519172 0.003249 2344 1.507872 0.003756 2550 1.518808 0.001232 2338 1.502345 0.003464 2530 1.514245 0.001232 2336 1.501272 0.0027777 2510 1.51322 0.002477 2336 1.501272 0.0027777 2510 1.50733 0.002486 2334 1.499697 0.002271 <tr< td=""><td>2690</td><td>1.520910</td><td>D 002542</td><td>2370</td><td>1 497672</td><td>0.002455</td></tr<>	2690	1.520910	D 002542	2370	1 497672	0.002455
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2680	1.520716	0.002342	2370	1.4971052	0.002035
$\begin{array}{c} 2610 & 1.517303 & 0.002673 \\ 2660 & 1.517352 & 0.003321 \\ 2650 & 1.517552 & 0.003527 \\ 2640 & 1.516324 & 0.004351 \\ 2640 & 1.516324 & 0.004351 \\ 2640 & 1.516324 & 0.004351 \\ 2630 & 1.519903 & 0.012112 \\ 2358 & 1.492119 & 0.005246 \\ 2630 & 1.523263 & 0.003153 \\ 2610 & 1.523263 & 0.003153 \\ 2610 & 1.520714 & 0.002636 \\ 2550 & 1.518796 & 0.002636 \\ 2550 & 1.518796 & 0.002636 \\ 2550 & 1.518796 & 0.002636 \\ 2550 & 1.518796 & 0.002636 \\ 2550 & 1.518796 & 0.002636 \\ 2550 & 1.5180808 & 0.001591 \\ 2580 & 1.517210 & 0.001192 \\ 2560 & 1.517210 & 0.001192 \\ 2560 & 1.517210 & 0.001192 \\ 2560 & 1.517210 & 0.001192 \\ 2550 & 1.518085 & 0.000446 \\ 2530 & 1.514842 & 0.001053 \\ 2550 & 1.516085 & 0.000846 \\ 2332 & 1.502345 & 0.003667 \\ 2520 & 1.512138 & 0.000872 \\ 2530 & 1.512138 & 0.000872 \\ 2530 & 1.512138 & 0.000872 \\ 2530 & 1.510710 & 0.000976 \\ 2332 & 1.499697 & 0.002990 \\ 2490 & 1.509830 & 0.001694 \\ 2332 & 1.499697 & 0.002990 \\ 2490 & 1.509830 & 0.001694 \\ 2332 & 1.499697 & 0.002990 \\ 2490 & 1.509830 & 0.002143 \\ 2326 & 1.499244 & 0.002284 \\ 2500 & 1.50734 & 0.002389 \\ 2470 & 1.5096830 & 0.002345 \\ 2326 & 1.494823 & 0.002787 \\ 2480 & 1.50734 & 0.002397 \\ 2470 & 1.506688 & 0.002345 \\ 2324 & 1.499244 & 0.002787 \\ 2460 & 1.50734 & 0.002397 \\ 2470 & 1.506630 & 0.002345 \\ 2324 & 1.498279 & 0.002280 \\ 2430 & 1.50734 & 0.002345 \\ 2326 & 1.497260 & 0.002767 \\ 2420 & 1.50734 & 0.002345 \\ 2326 & 1.497260 & 0.002767 \\ 2420 & 1.50734 & 0.002345 \\ 2316 & 1.496914 & 0.002767 \\ 2420 & 1.502478 & 0.002342 \\ 2314 & 1.496914 & 0.002767 \\ 2328 & 1.496041 & 0.002767 \\ 2328 & 1.496041 & 0.002767 \\ 2320 & 1.496041 & 0.002767 \\ 2320 & 1.496041 & 0.002767 \\ 2316 & 1.496014 & 0.002767 \\ 2316 & 1.496014 & 0.002767 \\ 2398 & 1.502264 & 0.002342 \\ 2314 & 1.496017 & 0.002767 \\ 2398 & 1.502264 & 0.002342 \\ 2314 & 1.496014 & 0.002767 \\ 2304 & 1.502478 & 0.002319 \\ 2312 & 1.496007 & 0.002767 \\ 2304 & 1.502478 & 0.002319 \\ 2312 & 1.496007 & 0.002762 \\ 2304 & 1.502478 & 0.002319 \\ 2312 & 1.496007 & 0.002762 \\ 2304 & 1.502478 & 0.002319 \\ 2312 & 1.4960$	2670	1.520710	0.002400	2300	1.491100	0.003025
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2660	1 610300	0.002073	2300	1.470470	0.003103
2630 1.517322 0.003527 2362 1.494240 0.003819 2640 1.516324 0.004351 2360 1.492599 0.005246 2630 1.519903 0.012112 2358 1.492119 0.005377 2620 1.523263 0.003153 2356 1.493770 0.011158 2610 1.523714 0.002767 2354 1.494795 0.010762 2600 1.518450 0.002636 2352 1.494730 0.012391 2590 1.518796 0.002496 2350 1.497287 0.018101 2580 1.519172 0.001249 2348 1.504773 0.018509 2570 1.518808 0.001591 2346 1.507872 0.005756 2550 1.516035 0.0001192 2344 1.507872 0.003464 2530 1.514842 0.001232 2338 1.502345 0.003464 2530 1.514842 0.001232 2338 1.502345 0.002775 2520 1.513322 0.00872 2336 1.501272 0.002771 2510 1.51710 0.00976 2332 1.499697 0.002990 2490 1.509830 0.002143 2328 1.4992411 0.002371 2480 1.507334 0.002366 2324 1.4996740 0.002767 2460 1.507334 0.002369 2326 1.497260 0.002767 2450 1.507472 0.0022397 2316 1.49	2650	1.519500	0.003321	2304	1.493273	0.003301
2640 1.516324 0.004351 2360 1.492559 0.005246 2630 1.519903 0.012112 2358 1.492119 0.008377 2620 1.523263 0.003153 2356 1.493770 0.011158 2610 1.520714 0.002636 2352 1.494795 0.010762 2600 1.518450 0.002636 2352 1.494213 0.012391 2590 1.518796 0.002636 2352 1.494213 0.012391 2590 1.518796 0.003249 2348 1.504773 0.018509 2570 1.518808 0.001591 2346 1.509216 0.003755 2550 1.517210 0.001192 2344 1.507872 0.005756 2550 1.516035 0.000848 2342 1.505197 0.004456 2530 1.514245 0.001232 2338 1.502345 0.003464 2530 1.514245 0.001232 2338 1.502345 0.002440 2500 1.510710 0.00976 2332 1.499697 0.002990 2490 1.509830 0.002143 2328 1.499697 0.002990 2490 1.509830 0.002345 2326 1.499647 0.002717 2480 1.507334 0.002345 2326 1.4997260 0.0025613 2440 1.507334 0.002345 2326 1.497744 0.002767 2420 1.507346 0.002397 2316 1.49	2030		0.003527	2362	1.494240	0.003814
2630 1.519903 0.012112 2358 1.492119 0.008377 2620 1.523263 0.003153 2356 1.494795 0.010762 2600 1.518450 0.002636 2352 1.494795 0.012391 2590 1.518796 0.004296 2350 1.494795 0.018101 2580 1.519172 0.003249 2348 1.504773 0.018509 2570 1.518808 0.001591 2346 1.509216 0.002756 2550 1.517210 0.001192 2344 1.507872 0.005756 2550 1.516035 0.000848 2342 1.505197 0.004255 2540 1.514842 0.001232 2338 1.502345 0.003464 2530 1.514842 0.001232 2336 1.501272 0.002777 2510 1.512138 0.00466 2334 1.502345 0.002840 2500 1.510710 0.000976 2332 1.499697 0.002840 2500 1.510710 0.002143 2328 1.499697 0.002840 2490 1.509830 0.002143 2326 1.494823 0.002613 2460 1.50734 0.002345 2326 1.494823 0.002787 2480 1.50734 0.002345 2326 1.494823 0.002605 2450 1.50734 0.002345 2326 1.4996914 0.002763 2440 1.506430 0.002345 2326 1.496914	2040	1,516324	0.004351	2360	1.492559	0.005245
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2030	1.519903	511510.0	2358	1.492119	0.008377
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2020	1.523263	0.003153	2356	1.493//0	0.011158
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2610	1.520714	0.002767	2354	1.494795	0.010762
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2600	1.518450	0.005636	2352	1.494213	0.012391
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2590	1.518/90	0.004296	2350	1.497287	0.018101
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2580	1.519172	0.003249	2348	1.504773	0.018509
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2570	1.518808	0.001591	2346	1.509216	0.011246
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2560	1.517210	0.001192	2344	1.507872	0.005756
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2550	1.516085	ີ0.00084ອີ	2342	1.505197	0.004255
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2540	1.514842	0.001053	2340	1.503558	0.003464
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2530	1.514205	0.001232	2338	<u>1,502345</u>	0.003067
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2520	1.513322	0.000872	2336	1.501272	0.002777
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2510	1.512138	0.000646	2334	1,500360	0.002840
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2500	1.510710	0.000976	2332	1.499697	0.002990
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	2490	1.509830	0.001694	2330	1.499411	0.003271
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2480	1.509269	0.002143	2328	1.499204	0.003027
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2470	1.504668	0.002093	2326	1.498823	0.002787
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2460	1.50/803	0.002366	2324	1.498279	0.002005
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2450	1.507334	0.002589	2322	1.49/788	0.002613
2430 1.505721 0.002360 2318 1.496914 0.002747 2420 1.504792 0.002397 2316 1.496614 0.002763 2410 1.503806 0.002342 2314 1.496306 0.002694 2400 1.502478 0.002319 2312 1.496007 0.002772 2398 1.502264 0.002423 2310 1.495732 0.002606	2440	1.506630	0.002345	2320	1.497200	0.002580
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2430	1.505721	0.002300	2318	1.496914	U.002747
2410 1.503806 0.002342 2314 1.496306 0.002694 2400 1.502478 0.002319 2312 1.496007 0.002772 2398 1.502264 0.002423 2310 1.495732 0.002606	2420	1.504792	0.002397	2316	1.496614	0.002763
2400 1.502478 0.002319 2312 1.496007 0.002772 2398 1.502264 0.002423 2310 1.495732 0.002606	2410	1.503806	0.002342	2314	1.496306	0.002694
2398 1.502264 0.002423 2310 1.495732 0.002606	2400	1.502478	0.002319	2312	1.496007	u.002772
	~2398	1.502264	0.002423	2310	1.4957.12	0.002606
CJYD 1.5UCICC 0.002650 2308 1.495181 0.002422	2396	1.502122	0.002650	2308	1.495161	0.002422

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ν, <u>cm</u> ⁻¹	<u>n</u>	<u>k</u>	<u>v, cm⁻¹</u>	<u>n</u>	<u>_k</u>
2306	1.494715	0.002726	-2218	1.481954	0.005012
2304	1.494525	0.002919	2216	1.481605	0.005314
2302	1.494409	0.002819	2214	1.481383	0.005484
2300	1.494142	0.002683	2212	1,481064	0.005487
2298	1.493754	0.002405	-2510-	1-480609	0.005446
2296	1.493242	0.002425	2208	1.480103	0.0056/5
2294	1.492771	0.002446	-2502	1.479660	0.005011
2292	1.492300	0.002517	2204	1.479239	0.006099
2290	1.491846	0.002616	2200	1.47884Ŭ	0.006487
2289	1,491470	0.002815	2196	1.477845	0.006701
2286	1.491134	0.002930	2194	1.477641	0.007067
2244	1.490817	0.003092	2192	1.477476	0.007215
2282	1.490780	0.003379	<u>51.30</u>	1.477253	0.007315
55a0	1.490606	0.002939	2188	1.477029	0.007465
2278	1.489950	0.002647	-2186	1.476866	0.007521
2276	1.489345	0.003056	2184	1.470507	0.007396
227+	1.489083	0.003155	2182	1.476024	0.007361
2272	1.488723	0.003090	5180	1.475031	0.007±17
2270	1.488209	0.003051	- 2178	1.475554	620600.0
2268	1.487648	0.003142	2176	1.475409	0.007899
2266	1.487114	0.003225	2174	1.475011	0.00/815
2264	1.406512	0.003262	2172	1.474553	0.007915
2262	1,485474	0.003147	2170	1.474114	<u> 660600.0</u>
2260	1.484093	0.003796	2168	1.473911	0.003432
2258	1,483283	0.005497	2166	1.473750	0.003447
2256	1.483608	0.007052	2164	1.473355	0.004320
2254	-1.484373	0.007615	2162	1.473157	ٕ003770
2252	1.484384	0.007275	2160	1.473095	0.008585
2220	1.483485	0.007749	2158	1.472719	0.008327
2248	1.483292	0.009916	2156	1.472176	0.008390
2246	1.485097	0.012038	2154	1.471847	ປ.ປປຊວງຊີ
2244	1.487922	0.011942	2152	1.471539	0.008515
2242	1.489800	0 . 00994Ŭ	2150	1.471150	0.003497
2240	1.490102	u.007696	2148	1.470556	0.008448
	1,489317	0.006026	2146	1.470005	003470
2236	1.488272	0.005174	2144	1.469481	0.003794
2234	1.487289	0.004744	2142	1.469085	0.009117
2232	1.486378	0.004371	2140	1.468978	0.009569
2230	1.485552	0.004469	2138	1.468886	0.009440
5559	1.484899	0.004378	2136	1.468420	0.009265
255	1.484227	0.004454	2134	1.468023	0.009698
2224	1.483629	0.004536	2132	1.467919	0.009786
-2222	1.483132	0.004740	2130	1.467704	0.009583
2220	1.482561	0.004663	2129	1.407187	0.009472

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v, cm^{-1}	<u>n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	_ <u>k</u>
2126	1.466622	0.009573	2038	1.443294	0.010574
2124	1.466307	0.010005	2036	1.442443	0.010370
2122	1.466134	0.009805	2034	1.441452	0.010497
2120	1.465682	0.009797	2032	1.440671	0.010870
2118	1.465324	0.010111	2030	1.440078	0.010980
2116	1.40514d	0.010047	5029	1.439359	0.010914
2114	1.404940	0.010082	2026	1.438533	0.010991
2112	1.464602	0.009744	202+	1.437718	0.011045
2110	1.464061	0.007654	2752	1.435010	0.011045
2108	1.4630d5	0.009734	5050	1.435554	c65110.0
2106	1.463234	0.009423	2013	1.435240	0.011712
2104	1.462565	0.009322	2016	1.434550	0.011460
2105	1.461958	0.009489	2014	1.434410	V.011307
210J	1.461434	0.009450	2012	1.432249	0 .011865
5089	1.460834	0.009554	<u>201</u> 0	1.431755	0.012529
2096	1.460296	0.009712	2008	1.431153	0.012245
2094	1.459895	0,009932	2006	1.430127	0.012243
2075	1.459529	0.009932	2004	1.429296	0.012853
2020	1.459128	0.009965	2002	1.428795	0.012931
2088	1.458773	0.009972	2000	1.427890	0.012628
2086	1.458300	0.009754	1998	1,426813	0,012916
2054	1.457723	0.009527	1996	1.426052	0.013351
2082	1.455941	0.009487	1994	1.425514	0.013364
2080	1.456300	0.009707	1992	1.424700	0.013139
2078	1.455731	0.009717	1990	1.423526	0.012940
2076	1.455123	0.009779	1988	1.422347	0.013329
2074	1.454517	0.009943	1986	1.421525	0.013700
2072	1.454071	0.010033	1984	1.420775	0.013752
2075	1.453530	0.010010	1982	1.419899	0,013761
601.2	1.452711	0.004705	1980	1.418942	0.013816
2056	1.452045	J.UIJ484	1975	1.417050	0.013801
206+	1.451013	0.010431	1976	1.416923	0.014233
2062	1.451335	0.010585	1974	1.416240	0.014399
2050	1.450602	0.010253	1972	1.415457	0.014073
2058	1.450062	0.010325	1970	1.41440/	0.014035
2056	1.449455	0.010300	1963	1.413438	0.013762
2054	1.448875	0.010349	1700	1.412300	0.013705
2052	1.448258	0.010193	1964	1.411070	0.013430
2050	1.447468	0.010102	1962	1.410289	0.014355
2048	.440040	0.010217	1960	1.409886	0.014232
2040	1.445963	0.010384	1958	1.409237	0.013510
2044	1.445278	0.010340	1956	1.408226	0.012721
2042	1.444537	0.010468	1954	1.407043	0.011993
2040	1.443869	0.010611	1952	1.405468	0.010810

v, cm^{-1}	<u>n</u>	k	<u>v, cm</u> -1	<u>n</u>	<u>k</u>
T95 0	1.403344	0.010040	1862	1.288042	0.040633
1948	1.401134	0.009812	1860	1.285734	0.040897
1946	1.399054	0.009706	1858	1.282548	0.041285
1944	1.397213	0.009863	1856	1.279429	0.041561
1942	1.395400	0.009653	1854	1.276222	0.041843
1940	1.393339	0.009440	1852	1.273140	0.041632
1938	1.391310	0.009583	1850	1.269619	0.040900
1936	1.389326	0.009593	1848	1.265627	0.039771
1934	1.367223	0.00.003	1846	1.254882	0.037996
1932	1.385376	0.010119	1844	1.254408	0.038948
1930	1.383642	0.010061	1842	1.250332	0.039402
1928	1.381733	0.009858	1840	1.245032	0.036615
1926	1.379667	0.009825	1838	1.234656	0.035031
1924	1.377691	0.009641	1536	1.233657	0.033126
1955_	1,375367	0.009151	1834	1.225624	0.028947
1920	1.372821	0.008924	1632	1.2154+2	0.026432
1918	1.369936	0.008724	1430	1.204070	0.025024
1916	1.367009	0.009900	1828	1.193283	0.025610
1914	1.364371	0.009604	1826	1.182022	0.025945
1412	1.362004	0.009513	1824	1.171029	0.026141
1910	<u>1</u> 359170	0.004352	1855	1.158749	0.026178
1968	1.355849	0.009152	1820	1.146342	0.026398
1900	1.352154	0.007552	1818	1.132447	0.026703
1904	1.346015	0.010597	1816	1.118217	0.026948
1902	1.345001	0.011218	1814	1.102023	0.027429
1400	1.3423od	0.011488	1812	1.085312	0.028085
1495	1.338095	0.012/65	1810 -	1.066253	0.029139
1840	1.335357	0.013587	1808	1.046818	0.030598
1894	1.331651	0.014853	1806	1.024526	0.032038
1892	1.327851	0.015921	1804	1.001039	0.033436
1890	1.323881	0.017866	1805	0.972924	0.035474
1888	1.320504	0.020126	1800	0.943533	0.039985
1886	1.317280	0.022111	1798	0.908349	0.042524
1884	1.314192	0.024238	1796	0.873057	0.046795
1882	1.311250	0.026649	1794	0.824703	0.046522
1880	1.308673	0.028714	1792	0.741137	0.036491
1878	1.306092	0.030953	1790	0.649981	0,107070
1876	1.303829	0.032930	<u>1788</u>	0.590441	0,186060
1874	1.301593	0.034906	1780	0,551237	0.266820
1872	1.299581	0.036503	1784	0.521005	0,351190
1870	1.27/245	0.030108	1734	0.502058	0.436380
1868	1.295/11	0.0391(3	עאז 1	0.488009	0.521900
1860	1.293024	0.040023	1/10	0.407043	V.01440V
1864	1=521413	V.V4V209	1110	0.441410	0.103040

Table 8. Continued

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v, cm^{-1}	<u>n</u>	<u>k</u>	<u>v, cm</u> -1	n	<u>k</u>
1774	0.504538	0.793420	1686	2:019632	0-020621
1772	0.523106	0.885960	1684	2.000203	0.018355
1770	0.552421	0.983340	1682	1.982500	0.016727
1760	0.595650	1.082100	1680	1.9657=5	0.015755
1766	0.649039	1.1/4600	1678	1.950817	0.014863
1764	0.711919	1.267900	1676	1.936770	0.014260
1762	0.194305	1.371200	1674	1.923969	0.012933
1760	0.405443	1.461500	1672	1,911226	0.011942
1750	1.047115	1.532200	1670	1-899630	0.011103
1756	1.203543	1.552500	1658	1.888072	0.009941
1754	1.351627	1.538100	1666	1,877226	0.009180
1752	1.479045	1.485700	1664	1.866396	0.008645
1750	1.574821	1.407800	7662	1,856677	0.003446
1748	1.631670	1,320000	1660	1.846945	0.008077
1746	1.64416J	1.228100	1658	1.838075	0.007808
1744	1.608154	1.157400	1656	1.829124	0.007798
1742	1.523547	1.126900	1654	1.951591	0,007701
1740	1.405468	1.172200	1652	1,812859	0.00/133
1738	1.287126	1,334200	1650	1-804959	0.006941
1736	1.238801	1.629300	1648	1.796670	0.000804
1734	1.445720	2,105300	1646	1.789143	0.005980
1732	2.038287	2.445300	1644	1.781025	0.000784
1730	2.764084	2.267600	1642	1.773095	0.006962
1728	3.169884	1.65580U	1640	1.764240	0.007483
1726	3,193401	1.151300	1638	1.755078	0.008840
1724	3.067915	0.841540	1030	1.745032	
1722	2.920185	0.625740	1034	1.734421	0.014915
1720	2.794111	0.523070	1032		0.023437
1/10	2.100109	0.451000	1030	1.720121	0.044754
1710	2.043434	0.374510	1620	1.020161	0.046756
1712	2.505000	0.027000	1626	1.732707	0.040733
	70 625435	V+C1407V	1622	1.132313	
1710	2 469721	0.201200	1022	1 703484	0 047550
1706	2.402046	0.047383	1614	1 732470	0 041333
1704	2.334302	0.061312	1616	1 731640	0.040535
1702	2.277156	0,001312	1614	1 7 1 34 4	0.040303
1700	2.224779	0.027329	1612	1 730568	0.045174
1698	2.176767	0.021595	1610	1 729898	0.043718
1696	2.135405	0.021234	1608	1 728072	0.042131
1694	2.102072	0.025977	1606	1.726543	0.040877
1692	2.074529	0.031454	1604	1.724423	0.039938
1690	2.060046	0.028919	1602	1.723073	0.036963
1688	2.040126	0.023593	1600	1.720960	0,037808

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Table 8. Continued

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ν, <u>cm</u> ⁻¹	n	<u>k</u>	v, cm^{-1}	<u>n</u>	k
1598	1.719496	0.037036	1510	1.634102	0.003262
1596	1.717723	0.036250	1508	1.631832	0.003191
1594	1.716538	0.034870	1506	1.630489	0.003178
1592	1.714430	0.033623	1504	1.628311	0.002772
1590	1.712920	0.032504	1502	1.626663	0.002459
1588	1.710469	0.031091	1500	1.624113	0.002424
1586	1.708405	0.030369	1498	1.622531	0.002584
1584	1.706203	0.030375	1496	1.620355	0.002755
1582	1.705430	0.030055	1494	1.618934	0.002621
1580	1.704557	0.029377	1492	1.616597	0.002760
1578	1.704252	0.027488	1490	1.615209	0.002956
1576	1.702742	0.025264	1488	1.613058	0.003053
1574	1.700919	0,022673	1486	1.611/02	0.003118
1572	.1.697692	0.023748	1484	1.609403	0.003216
1570	1.695402	0.020169	1482	1.607938	0.003433
1564	1,692983	0.018923	1480	1.605084	0.003841
1566	1.690956	0.01/615	1478	1.604345	0.004110
1564	1.687966	0.016608	1476	1.602202	0.004736
1562	1.685735	0.016072	1474	1.601047	0.004931
1560	1.683357	0.015918	1472	1.599132	0.005691
1558	1.682123	0.015277	1470	1.598155	0.005901
1556	1,680026	0.014020	1468	1.596220	0.006226
1554	1.678090	0.012796	1466	1.595193	0.006787
1552	1.6/5100	0.011903	1464	1.573202	0.000952
1550	1.573000	0.011001	1462	1 600504	0.007730
1548	1.670423	0.011295	146U 17770	1.530304	0.000072
1546	1.608/92	0.010056	1400	1 544547	0.0000500
1544	1.666772	0.010404	1430 1467	1.500557	0 0000432
1542	1.605/33	0.00471	1434	1.286384	0.000303
1540	1.603000	0.007341	1432	1.5858.9	0.003371
1535	1.001767	0.002955	1450	1.584527	N NN0026
1530	1.03401	0.001905	1448	17583854	0,009920
1534	1 - 037000	0.007072	1440	1.581981	0.009433
1532	1 653603	0.006476	1444 1877	1.581378	0.010057
1225	1 651241	0.006036	1442	1.580045	0 010314
1520	1.001201	0.005806	1440	1.579696	0 004462
1520	1 647284	0.005592	1436	1.578177	0 009742
1527	1.545914	0.005326	1414	1.577560	0.00911u
1526	1.64 1847	0.004922	1432	1.575690	0.004419
<u>ד</u> קואר קלואר	1.642155	0.004106	1470	1.574881	0.008705
1516	1.634757	0.004102	1428	1.573109	0.008245
<u>1514</u>	1.638445	0.003703	1426	1.572054	0.007576
1512	1.635828	0.003284	1424	1.569794	0.007416
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v, cm^{-1}	<u>n</u>	k	<u>v, cm⁻¹</u>	<u> </u>	k
1422	1.568672	0.007191	1 774	1-419551	0.003816
1420	1.566555	0.007055	1372	1.410737	0.004592
1418	1.565726	0.007043	1370	1.403208	0.004733
1416	1.563627	0.006248	1328	1.392307	0.004855
1414	1,562525	0.006137	1326	1.382080	0.005505
1412	1.560124	0.005341	1324	1.36/932	0.006435
1410	1.558542	0.004965	1322	1.354014	0.008784
1408	1.555761	0.004965	1320	1.335462	0.012754
1406	1.554672	0.005159	1318	1.31/013	0.020306
1404	1.552277	0.004607	1316	1.295522	0.033280
1402	1.550965	0.004333	1314	1.278386	0.051915
1400	1.548269	0.003926	1312	1.265518	0.076438
T398	1.546602	0.003244	1310	1.264302	0.099460
1396	1.543235	0.003107	1308	1.263605	0.112200
1394	1.541385	0.003182	1306	1.259610	0.119320
1392	1.538049	0.003286	1304	1.247240	0.129670
1360	1,536275	0.003971	1302	1.236552	0.145190
1388	1.533892	0.004912	1300	1.225939	0.162590
1386	1.533536	0.004841.	1298	1.218007	0.178510
1384	1.531281	0.003678	1296	1.206672	0,194580
1382	1.529404	0.002306	1294	1.195314	0,212560
1380	1.525598	0.001624	1292	1,182014	0.232100
1378	1.5231.47	0.001226	1290	1.167611	0.252830
1376	1.519240	0.000925	1288	1,151851	0.273480
1374	1.516901	0.000867	1286	1,121265	0.293700
1372	1.512990	0.000297	1284	1.046817	0.312710
1370	1,510203	0.000100	1282	1.027262	0.483410
1368	1.505830	0.000100	1280	1.077959	0.560590
1366	1.503050	0.000100	1278	1.136493	0.607550
1364	1.498586	0.000100	1276	1.169533	0.654040
1362	1.495634	0.000100	1274	1,215428	0.683850
1360	1.490906	0.000100	1272	1.244755	0.729820
1358	1.487693	0.000100	1270	1.290050	0.770760
1356	1.482623	0.000100	1268	1.329273	0.811390
1354	1.479070	0.000100	1266	1,382752	0.847340
1352	1.473504	0.000100	1264	1.418700	0.882540
1350	1,469504	0.000100	1262	1.494571	0,948100
1348	1.463490	0.000100	1260	1.551210	0.959750
1346	1.458814	0.000100	1258	1,626553	1.011100
1344	1.451603	0.000149	1256	1.645899	1.073100
1342	1.446170	0.001284	1254	1.846693	1.144800
1340	1.439160	0.002342	1252	2.021496	1-503900
1338	1.433940	0.002808	1250	2.310445	1.155400
1330	1.426018	0.003252	1248	2.687009	1.098200

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Table 8. Continued

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v, cm^{-1}	<u>n</u> -	<u>k</u>	v, cm^{-1}	<u>n</u>	k
1245	2.760905	0.340720	1158	1.718722	0-006229
1244	2-514939	0.236170	1156	1 717526	0.005834
1242	2.3445 10	0.151400	1154	1 713346	0.00549H
1240	2.271951	0.105250	1152	1 712107	0 005095
1236	2.176122	0.089690	1150	1 708150	0.005060
1236	2.137226	0.075158	1148	1 707344	0 0049449
1234	2-080599	0.050380	1146	3 75 16 12	0.004047 70 004147
1232	2.050738	0.051932	1144	1.702479	0.003828
1230	2.004978	0-047149	T142"	1 604462	0.003632
1228	1.949663	0.043413	1140	1 6977-7	0.004025
T226	1.959020	0.040114	11-18	1.694474	0.004025
1224	1,945904	0.037332	1136	1 693263	0.002784
1222	1.922690	0.034758	1134	1.075245	0.003118
1220	1.912353	n 011087	1137	1 444045	0.003209
1218	1.842745	n n 2 2 2 7	1136	1 425675	0.003207
1216	1.884056	0.027689	1150	1 686696	0.002639
1214	1-863069	0.026060	1126		TA TATA 3700
1212	1 861322	0.024080	1124	1.001100	0.003500
1210	1 847203	0.022340	יייייי	1.000000	0.003563
1208	1 841240	0 021084	1120	1.676663	0.003303
1200	1 0 20036	0.021004	1120	1,070000	0.003707
1200	1 020330	0.019/14	1110	1.0/302/	
1204	1 012004	0.012380	1110	1.674591	0.006639
1202	1 0/0/20	0.017004	1114	1.6/3905	0.00549
1108	1 700006	0.01/034	1112	1.674791	0.005134
1190	1 705702	0.010922	1110	1.672736	0.003781
1190	1.73772	0.010301	1108	1.672003	0.002184
1102	1 794216	0.01-000	1106	1.668520	0.001215
1192	7777733	0.013090	1104	1.667334	0.001480
1190	1 776500	0.014021	1102	1.604023	0.001419
1100	1.747613	0.014031	1100	1.003441	0.001382
1100	1.755216	0.010400	1098	1.001940	0.001835
1104	1.105210	0.012470	1090	1.001370	
1102	1 764000	0.012107	1094	1.000049	0.001033
1100	1.120761	0.011393	1092	1.658304	0.001938
1170	1 760161	0.010003	1090	1.656629	0.000576
1170	1 7/7/41	0.010400	1088	1.655/3/	0.000100
1114	1.143004	0.009829	1086	1.652984	0.000100
11/2	10/4203/	0.009400	1084	1.652457	0.000242
1170	1 1300/3	0.008/21	1082	1.650144	0.000100
1100	1.733403	0.008432	1080	1.649608	0.000100
1100	1.700001	0.00//24	1078	1.647304	0.000100
1164	1.154000	0.007249	1076	1.646822	0.000100
1102	1.724310	0.006333	1074	1.644570	0.000100
1100	1.123484	0.00611	1072	1.644021	0.000100

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v, em	_ <u>n</u>	<u></u>	ν , cm	<u>n</u>	<u>_k</u>
1070	1.641801	0.000272	982	1.590104	0.001015
1068	1.641353	0.000371	980	1.594518	0.000851
1066	1.639123	0.000447	978	1.591647	0.002556
1064	1.638543	0.000842	976	1.591785	0.004327
1062	1.636935	0.001655	974	1.591005	0.004077
1060	1.637365	0.001627	972	1.590525	0.004160
1058	1.635655	0.000831	970	1.588717	0.004777
1056	1.635210	0.000309	968	1.588938	0.005336
1054	1.633322	0.000563	966	1.587916	0.005403
1052	1.632778	0.000100	964	1.587930	0.003322
1050	1.630506	0.000100	962	1,586419	0.004920
1048	1.629871	0.000100	960	1.585720	0.004877
1046	1.627778	0.000160	958	1.584212	0.005485
1044	1.626999	0.000100	956	1.584237	0.005519
1042	1.624481	0.000315	- 954	1.582933	0.005195
1040	1.623908	0.001475	952	1.582339	0.004934
1038	1.622557	0.002009	950	1.580931	0.002210
1036	1.622318	0.001826	_948	1.580840	0.004858
1034	1.620197	0.002181	946	1.578589	0.003539
1032	1.620219	0.003417	944	1.576799	0.004259
1030	1.014150	0.003242	942	1.57545.1	0.006094
1020	1.019019	0.003202	940	1.576305	0.006253
1020		0.003419	938	1.575424	0.005021
1024	1.011210	0.003000	936	1.574523	0.004376
1022	1.010020	0 003660	934	1.573001	0,004605
1020	1.610194	0 003007	932	1.5/2/43	0.003768
1010	1.614155	0 0000547	930	1.569///	0.001991
1014	1.01-1.00	0 004004	928	1.50/039	0.003711
5161	1 612926	0 004105	720	1.50/010	0.005030
1010	1.611445	0.004010	<u>724</u>	1.508/01	0.003476
1008	1.611259	0.004713	- 722	1.503700	0.000744
1005	1.6100.39	0.003761	919	1.505204	"N 007777"
1004	1.610052	0.003101	916	1.500988	0.002327
1002	1.608384	0-002644	914.	1.554176	a.aa)429
1000	1.607946	0.002316	912	1.557620	0.000100
998	1.606139	0.001393	910-	1.554706	
996	1.605375	0.001555	908	1.553031	0_000100
994	1.603517	0.001647	906	1.550586	0.000100
992	1.602707	0.001335	904	1.549003	0.000100
990	1.600773	0.001108	902	1.546531	0.000100
988	1.5990od	U.001436	900	1.544905	0.000100
9996	1.597917	0.001623	848	1.542356	0.000100
984	1.59/615	0.002175	896	1.540628	0.000100

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Table 8. Continued

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v, cm^{-1}	<u>_n</u>	<u>k</u>	v, cm^{-1}	<u>n</u>	<u>k</u>
894	1.537949	0.000100	806	1.325596	0.030736
892	1.536035	0.000100	804	1.311993	0.030634
-390	1.532896	0.000100	802	1.296103	0.030184
886	1.530655	0.000785	800	1.275672	0.031734
886	1.528473	0.002032	798	1.256049	0.035634
384	1.527205	0.001424	796	1.229065	0.036287
_ <u>_</u> 845	1-524443	0.001245	794	1,196241	0.042019
840	1.522421	0.001023	792	1.158324	0.062518
373	1.518906	0.000129	790	1.128056	0.087216
376	1.515258	0.000139	788	1.096304	0.118380
874	175T1362	0.001693	786	1.080551	0.156960
872	1.508003	0.002297	784	1.066054	0.135000
870	1,505082	0.003411	782	1.077471	0.204090
868	1.502445	0.004809	780	1.030262	u.159220
366	1.499717	0.005166	778	0.846503	0.097661
864	1.497311	0.000486	776	0.715188	0.399190
362	1.493717	0.007495	774	0.755577	0.562360
860	1.491114	0.009244	772	0.831371	0.682910
858	1,489117	0.010971	770	0.895798	0.773770
856	1.48/238	0.010505	708	0.950278	0.839620
854	1.404lol	0.011023	766	0.984950	0.904020
852	1.481931	0.011733	764	1.090314	1.073100
850	1.479195	0.010721	762	1.202958	1.062700
845	1.475337	0.003760	760	1.287977	1.117600
546	1.410399	0.003877	758	1.385140	1.184600
844	1.405882	0.010660	756	1.535766	1.201200
842	1.462244	0 . 012530	754	1.6535//	1.174600
H4U	1,459022	0.011715	752	1.771181	1.1297.00
838	1.453845	0.010191	750	1.843371	1.058800
836	1.447850	0.010399	748	1.875033	0.967510
834	1.442503	0.011939	746	1.838123	0,939750
832	1.437531	0.012095	744	1.827380	0.991020
830	1.431426	0.011469	742	1.850478	1.089200
828	1.423308	0.011180	740	2.030000	1.248200
826	1.415986	0.014012	7.10	2.24/849	1.235800
824	1.409524	0.015781	017	2,558198	1.197000
822	1.402850	0.015690	7.59	2.413134	1.027700
820	1.394432	0.017280	730	2.92/400	0.270190
818	1.385895	0.017400	130	2.032132	0.184480
816	1.376808	0.020735	160	2,402344	0.124730
814	1.366903	0.019698	120	2.3023/1	0.072487
812	1.355398	0.024281	(24 232	2.279133	
810	1.345734	0.027229	176	2.244200	0.000110
808	1.35661	0.070180	120	2.100125	0.040943

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ν , cm ⁻¹	<u>n</u>	<u>k</u>
718	2.148431	0.034379
716	2.107234	0.027786
714	2.076719	0.022106
712	2.045769	0.021133
710	2.025604	0.021104
708	2.002274	0.019039
700	1.985149	0.017309
704	1.965526	0.018504
702	1.952507	0.017913
700		0.018784

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Table 8. Concluded

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