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EFFECTS OF ARRIVAL TIME ERRORS IN WEIGHTED RANGE EQUATION SOLUT--ETC(U)
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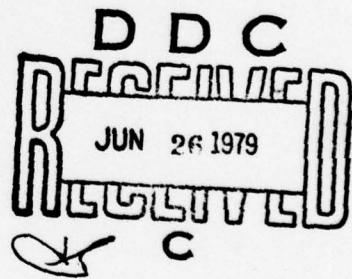
EFFECTS OF ARRIVAL TIME ERRORS
IN WEIGHTED RANGE EQUATION SOLUTIONS
FOR LINEAR BASE SOUND RANGING

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER ASL-TR-0029	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) EFFECTS OF ARRIVAL TIME ERRORS IN WEIGHTED RANGE EQUATION SOLUTIONS FOR LINEAR BASE SOUND RANGING.		5. TYPE OF REPORT & PERIOD COVERED R&D Technical Report
7. AUTHOR(s) Donald M. Swingle		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Atmospheric Sciences Laboratory White Sands Missile Range, NM 88002		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS DA Task No. 1L16211AH-71-26 4
11. CONTROLLING OFFICE NAME AND ADDRESS US Army Electronics Research and Development Command Adelphi, MD 20783		12. REPORT DATE April 1979
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Research and development technical rept.,		13. NUMBER OF PAGES 47
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		15. SECURITY CLASS. (of this report) UNCLASSIFIED
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) ERADCOM/ASL-TR-OPP29		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE 12 52p.
18. SUPPLEMENTARY NOTES 16) 1L162114AH71 17) 26		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Meteorology Target acquisition Sound ranging Errors		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Results of the research discussed in this report show that the errors in target location computed by the Weighted Range Equation Solution, when applied to a regular, linear, six-microphone array, are approximately proportional to the errors in arrival time, relative to the assumptions inherent in the solution model. For most target locations, microphones 2 and 5, in the six-microphone array, are relatively less influential in determining target location than are microphones 1, 3, 4, and 6. The transfer function between arrival time errors		

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20. ABSTRACT (cont)

at one or more microphones is shown to be approximately linear and to possess the property of superposability; i.e., the combined effect of several errors in arrival time is approximately equal to the sum of the effects of each error taken as occurring alone. Several general properties of symmetry and anti-symmetry are demonstrated.

This report provides its readers with the basic vector error response of the Weighted Range Equation Solution for all areas in which the AN/TNS-10 Sound Ranging Set is effective.

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INTRODUCTION

Linear base sound ranging, using the GR-8 or AN/TNS-10 Sound Ranging Set, has been shown to be an effective means for locating enemy firing batteries which are beyond the range of direct visual observation. Development of the USRAN3 solution technique by Swingle, Bellucci, and Crenshaw showed that the present system was not performing to the limits of its accuracy potential. Their evaluations showed that an improvement in accuracy from 2.2 percent of range* to 1.8 percent could be achieved by a simple change in the method by which the final target location (fix) was computed.^{1,2} They noted that further improvements were believed to be achievable.

In response to a request from US Army Materiel Command Headquarters in June 1974, Swingle developed an error analysis for the overall system which was used to estimate the likely improvement which could be achieved for a typical target located centrally to the microphone array and 10,000 meters ahead thereof. This restriction of target location was adopted for reasons of both simplicity and nonavailability of quantitative error sensitivity data for other locations.

The present report covers the first steps in expanding that analysis to include the entire field of potential target locations, including extension of the analysis to points beyond the usual range of sound ranging utility, i.e., to ranges exceeding twice the base length and to flanking angles beyond 15 degrees from the normal of the outlying subbases.

This analysis will develop the ultimate accuracy which can be expected from a variety of sound ranging array configurations having tactical practicality, including, of course, the six-microphone "linear base" system with which the US Army is now equipped. Optimized meteorological correction methods, which take account of the natural variability of the atmosphere, will be considered as parts of the overall sound ranging system input error source.

It will be assumed that the reader is generally acquainted with the principles of sound ranging on artillery weapons based on the use of the AN/TNS-10 or similar system. All six microphones will be assumed to be installed along a straight base at uniform spacings of four sound seconds (about 1350 meters). While solutions for shot time and shot coordinates are unique, within the usual assumptions of an atmosphere having uniform

*Distance target is forward of line of microphones

¹Donald M. Swingle, Craig M. Crenshaw, and Raymond Bellucci, 1972, "Improved Sound Ranging Location of Enemy Artillery," Army Science Conference, US Military Academy, West Point, NJ

²Donald M. Swingle and Raymond Bellucci, 1973, "Improved Sound Ranging Location of Enemy Artillery," R&D Technical Report ECOM-5486, US Army Electronics Command, Fort Monmouth, NJ

wind and uniform temperature (sound speed), when arrival times from only three microphones are used to determine target location, the system is over-determined when more than three arrival times are used. Under these conditions a number of solution methods can be used, yielding generally different target locations.

Following the development and evaluation of the USRAN3 solution, Crenshaw and Swingle engaged in a continuing verbal and correspondence exchange,^{3,4} looking forward to a more general and even more accurate solution and meteorological correction method. This led to the evolution of the Weighted Range Equation Solution (WRAS) which is outlined in the appendix. In brief, this method determines the shot time and coordinates which minimize the sum of the squares of the differences between the square of the geometric range from solution point to each microphone and the square of the "propagation range" computed from the speed of sound along that direction and the difference between computed shot time and measured arrival time.

$$\sum_{i=1}^N w_i \times (R_i^2 - P_i^2)^2 = \text{minimum} \quad (1)$$

where w_i is a weighting factor which may be varied by any desired rule across the microphone array. A simple form for the w_i which was suggested by the known behavior of atmospheric variability as studied by Arnold and Bellucci⁵ and later by Lowenthal and Bellucci⁶ is

$$w_i = R_i^n / \left(\sum_{i=1}^N R_i^n \right) \quad (2)$$

³Personal communications between Dr. Craig M. Crenshaw and Dr. Donald M. Swingle, June 1972-December 1973

⁴Craig M. Crenshaw, 1972, "Sound Ranging Calculations," AMC Chief Scientist Technical Note Number 1, US Army Materiel Command, Alexandria, VA

⁵A. Arnold and R. Bellucci, 1957, "Variability of Ballistic Meteorological Parameters," Technical Memorandum M-1913, US Army Signal Engineering Laboratories, Fort Monmouth, NJ

⁶Marvin J. Lowenthal and Raymond Bellucci, 1970, "Variability of Ballistic Winds, R&D Technical Report ECOM-3259, US Army Electronics Command, Fort Monmouth, NJ

where n is any real number. Experimentation was conducted with n ranging from 0 to -10. When applied to actual sound ranging data, $n = -5$ generally gave the most accurate target locations. In the present study this weighting was used, but the conclusions are equally valid when solutions are computed using $n = 0$.

Earlier studies of sound ranging system error sensitivity had been conducted by Fox,⁷ Lee,⁸ and Bellucci.^{9,10}

All the above utilized solutions depended upon use of differences in arrival time at adjacent microphones. Fox used a least squares minimization of the differences between "true" and perturbed arrival time differences, while Lee minimized the squared differences between "true" and perturbed arrival times. Bellucci used the standard artillery solution. Bellucci's published work was confined to a set of only 12 points in the target area. Lee expressed errors as radial errors (i.e., miss-distance), thus precluding consideration of the vector nature of the error patterns. Fox considered radial and tangential errors relative to the center of the microphone array. Lee presented total radial error contours but provided no data on vector error. None of the researchers provided a dense, ordered array of errors at target points throughout the battle area which might be utilized for error analysis of both current and future tactical sound ranging systems.

Results obtained herein are in generally good agreement with these studies. They differ in that they present error transfer properties of the WRAS solution in terms of along-array and along-normal components. They also extend the range of the computations to at least five sound base (25 subbase) lengths ahead of the array and to 9 to 18 subbase lengths to either side of the centerline of the array. Additional computations, not covered in detail here, extend the computations out as far as 15 sound base (75 subbase) lengths forward of the array. The properties of linearity and superposability discussed below were also found to extend to such ranges, although

⁷H. L. Fox, 1968, "Meteorological Techniques for Sound Ranging; Theory of Errors," Technical Report ECOM-0233-2, US Army Electronics Command, Fort Monmouth, NJ

⁸Robert P. Lee, 1972, "Artillery Sound Ranging Computer Simulations," R&D Technical Report ECOM-5441, US Army Electronics Command, White Sands Missile Range, NM

⁹Raymond Bellucci, 1966, "Studies of Meteorological Techniques for Sound Ranging: Report II, Error Analysis," Technical Report ECOM-2703, US Army Electronics Command, Fort Monmouth, NJ

¹⁰Personal communications between Raymond Bellucci and Dr. Donald M. Swingle, June 1966-June 1972

errors were generally much larger. These results will be utilized in succeeding reports dealing with errors in microphone position and atmospheric input as well as terrain effects and sound ranging system improvement.

DATA PRESENTATION

The data of this report are uniformly presented as fields of numerical values, to provide, in a reasonably compact form, the detailed information required to assess the effects of various error sources on target location. Those readers whose taste leads to the representation of data in contour maps are invited to add their own analyses of the numerical fields presented. Both horizontal components of target location error are presented at each grid point to facilitate ready analysis of the vector character of the target location error associated with input data errors.

DATA INTERPRETATION

Figure 1 provides a schematic guide to interpretation of the following tables. Tables 1 through 23 provide the field of target location errors due to specified errors in arrival time at given microphones for each of a regular array of assumed "true" target locations. The targets are assumed to be at the points indicated by "+" (except along the left-hand edge of the figure).

These points are uniformly spaced by one subbase length forward of the center of each subbase and laterally from the center of the array. To the left of each target point appear two figures. The upper number is the error in meters which would arise in the solution by WRAS for the target along the X- or along baseline direction, while the lower number is the error in the Y- or normal-to-baseline direction.

Along the top of each figure are listed the subbase length (BL) in sound seconds (4 sound seconds is approximately 1350 meters) and the index number of the perturbed microphone (IP, counting from left to right as one faces the target from the baseline). In this report IP will range from 1 to 6. If two digits are given under IP, these digits indicate the two microphones whose arrival times are simultaneously perturbed. ID is used to indicate the perturbed parameter and will always be 8 in this report, indicating that the perturbation considered is in time of arrival at the microphones indicated by IP. The number of subbase lengths to the right of the array center which characterizes the top row of targets (+) is given by M. As the computations progress down the page, M is incremented for each row and appears at the left-hand edge of the paper abreast of the Y-component of error. Just above these changing values of M appears the value of IP given in the heading line. This value appears just to the left of the first + in each row which marks the point which is M subbase lengths from the array center. In all of the tables N = 25, indicating that the right-most + or target position in each row is 25 subbase lengths

forward of the microphone array. DXY indicates the spacing in both X and Y directions of the grid points in units one subbase long. In all tables herein DXY is 1.000. UP gives the assumed unit perturbation which is applied to the arrival time of the identified microphone(s) expressed in milliseconds. IW is the weighting exponent. In terms of equation (2), $n = -IW$. IW will always be 5 herein. ZZ gives the target height above the plane containing the microphones and is always 0.0 in this report. V1, V2, and V3 are the X-, Y-, and Z- components of the mean wind assumed in the computation, and will remain 0.00 in this report. Finally, TE is the assumed "effective temperature" for sound ranging, assumed to be 10°C herein.

Where **** appears on the tables, the error exceeds ± 999.5 meters, while -0+ appearing in the upper and lower left corners indicates that computations were not made for the point because it occurs at a large flanking angle ($|M| > N + 3$).

EFFECT OF UNIT INPUT ERRORS ON SOLUTIONS

In computing the data for tables 1 through 15, the author assumed that the target was at the plotted grid point, and the arrival time of sound generated at shot time (= 0.000 seconds) was computed for each microphone. Then the arrival time at the specified microphone (IP) was incremented by UP milliseconds, and the target location was computed by using the WRAS solution. At the field point the difference between the computed location and the assumed or "true" location is printed (computed - true). In tables 1 through 6 of "error maps," the unit perturbation was assumed to be 1 millisecond. All errors are rounded to the nearest meter. This value was chosen as small enough to produce few errors exceeding 1000 meters, while also producing few errors less than a few meters in at least one of the component directions. The reader is invited to examine the symmetry of error effects between microphones 1 and 6 (tables 1 and 6), 2 and 5 (tables 2 and 5) and 3 and 4 (tables 3 and 4).

The tables show that errors in arrival time at microphones 2 and 5 have relatively small effects at most target points on either component of target location error and that for all microphones the Y-component error is generally several times the X-component error. Further, both microphones 1 and 6 yield large negative Y-component errors for a small positive change in arrival time, while both microphones 3 and 4 yield large positive errors in Y-component for a small positive change in arrival time.

In the above computations and throughout this report, it does not matter whether the "error" in arrival time be the result of an error in reading the acoustic record or the effect of propagation phenomena in causing the signature's apparent arrival time to be different from that which would be expected after correcting for the assumed meteorological conditions. Either cause will result in the same target location error if it

causes the same error in arrival time. For example, at the point $M = -9$, $N = 25$, the upper right-hand + in table 1, one finds that an arrival time error of 1 millisecond ($UP = 1.00$) causes the X-component of target position to be computed to be 18 meters larger than true and the Y-component to be computed to be 49 meters smaller than true (18, -49). For the same point, tables 2 through 6 show that the same unit error, if it occurs at microphones 2 through 6, produces target location errors of (-5, 17), (-14, 40), (-11, 31), (-1, 1), and (13, -41) meters, respectively.

LINEARITY OF ERROR TRANSFER FUNCTIONS

The analysis of the joint effects of several error sources on the overall sound ranging target location error would be much simplified if the output error could be assumed to be linearly dependent upon the input error, or at least approximately so. Tables 2 through 6 show the error fields for input errors of 1 millisecond occurring in microphones 1 through 6, while tables 7 through 12 show the error fields for input errors of 3 milliseconds.

In view of the symmetry noted for errors in microphones 1 and 6, 2 and 5, and 3 and 4, it becomes apparent that the entire story can be told by just the error fields due to microphones 1, 2, and 3. Thus the error fields due to input errors of 10 and 30 milliseconds, shown in tables 13 through 15 and 16 through 18, respectively, are shown only for microphones 1, 2, and 3.

Through most of the error field, output errors in each horizontal component of target location are approximately proportional to input errors. Over a range of 30:1 in input error, proportionality is quite good. The range selected for illustration includes the range of errors to be expected because of normal atmospheric propagation effects and from errors in reading arrival time records.

In assessing the combined effects of several errors affecting the measured arrival time at any microphone, little error will occur if the target location error due to each contributing error is separately computed and the results summed instead of first summing the several contributing errors in arrival time and then computing the target location error which they will cause.

SUPERPOSABILITY OF ERROR TRANSFER FUNCTIONS

The preceding section demonstrated that several simultaneous arrival time errors occurring at a single microphone could be separately transformed into target location errors and then summed to give the aggregate target location error. To investigate the validity of computing errors due to simultaneous arrival time errors in several microphones as the sum of the effects of errors in each microphone, the author assumed errors occurring in one microphone and an additional error occurring in each of the remaining microphones in turn.

In tables 19 through 23, simultaneous errors of 3 milliseconds are assumed to occur in microphone 2 and in microphones 1, 3, 4, 5, and 6 in turn. The reader will be able to readily verify that the effect of the combined simultaneously occurring error is very closely approximated by the sum of the errors given table 8 and tables 7, 9, 10, 11, and 12, respectively.

For example, tables 7 through 12 show that the errors in target location at the point $(M, N) = (-9, 25)$ due to a 3-millisecond error in arrival time at microphones 1 through 6 are $(56, -147)$, $(-15, 50)$, $(-42, 120)$, $(-34, 93)$, $(-3, 2)$, and $(40, -124)$ meters, respectively. For the same target point, table 19 shows that the target location error due to simultaneously occurring 3-millisecond errors in microphones 1 and 2 is $(40, -95)$, almost exactly the sum of the effects of this error acting separately at microphones 1 and 2. The corresponding effect of the combined error in microphones 2 and 3, 2 and 4, 2 and 5, and 2 and 6 are $(-58, 172)$, $(-50, 145)$, $(-19, 53)$ and $(15, -74)$ meters, respectively, as shown in tables 20 through 23. In each case the effect of the simultaneously occurring error is approximately equal to the sum of the effects caused by each error taken as acting alone. Similar results would be found for any selected group of microphones and for any target point.

We have thus shown that the errors in target location resulting from the simultaneous presence of errors in several microphones can be closely approximated by the sum of errors computed as if each error occurred separately in each of the microphones.

CONCLUSIONS

The above analysis has shown that sound ranging solutions obtained by the WRAS solution technique applied to a regular, linear, six-microphone array have the following properties:

1. Errors occurring in arrival time, relative to the assumptions inherent in the solution model, in microphones 1, 3, 4, and 6 have the greatest effect on the solution; while at most field points, microphones 2 and 5 have relatively little effect on the solution.
2. At most field points, the Y-component of target location error due to an error in arrival time at any microphone is generally several times as large as the X-component of error.
3. Positive errors in arrival time at microphones 1 and 6 lead generally to negative Y-component errors, while positive errors in arrival time at microphones 3 and 4 result in positive Y-component errors.
4. Positive errors in arrival time at microphones 1 and 6 lead to positive X-component errors in target locations for left flank targets and negative X-component errors in target locations for right flank targets, while positive errors in arrival time at microphones 3 and 4 lead to positive X-component errors in target location for right flank targets and negative X-component errors in target location for left flank targets.

5. For each horizontal component of target location, the error caused by an error in arrival time at any microphone is approximately proportional to the arrival time error; i.e., the time-to-space error transfer function is approximately linear. Thus the error in target location due to the combined effects of several errors in arrival time at any one microphone is closely approximated by the sum of errors in target location which each of the contributing errors would have caused if acting alone.

6. The error in target location in each component of position resulting from simultaneously occurring errors at two or more microphones is closely approximated by the sum of the errors which each arrival time error would produce if acting alone; i.e., the error contributions are superposable in geometric space.

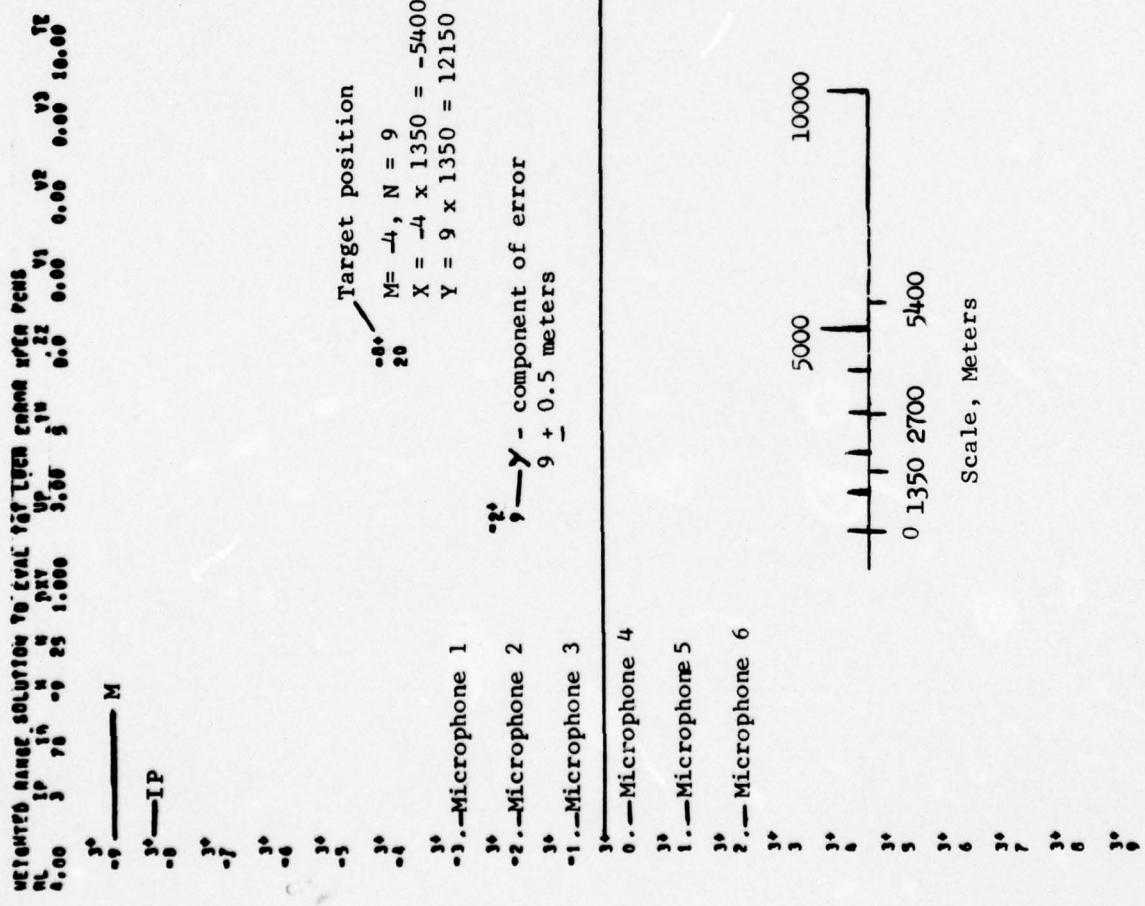


Figure 1. Key to error maps, tables 1 through 23.

TABLE 1. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

		REFINED ZONE SOLUTION TO EQUIL. VAR WITH ERROR AFTER FCNS									
SL.	IP	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴	10 ⁻⁴
1.	1	6	4	25	1.0000	1.000	9	0.3	0.00	0.00	0.00
2.	6	26	20	51	63	32	26	20	10	16	16
3.	7	6	23	19	16	17	17	10	10	22	25
4.	8	25	63	29	22	18	16	13	13	13	13
5.	9	22	15	14	13	14	14	15	16	16	16
6.	10	15	14	13	12	11	10	10	10	11	11
7.	11	10	11	11	12	13	14	15	16	17	17
8.	12	11	11	11	11	11	11	11	11	11	11
9.	13	11	11	11	11	11	11	11	11	11	11
10.	14	11	11	11	11	11	11	11	11	11	11
11.	15	11	11	11	11	11	11	11	11	11	11
12.	16	11	11	11	11	11	11	11	11	11	11
13.	17	11	11	11	11	11	11	11	11	11	11
14.	18	11	11	11	11	11	11	11	11	11	11
15.	19	11	11	11	11	11	11	11	11	11	11
16.	20	11	11	11	11	11	11	11	11	11	11
17.	21	11	11	11	11	11	11	11	11	11	11
18.	22	11	11	11	11	11	11	11	11	11	11
19.	23	11	11	11	11	11	11	11	11	11	11
20.	24	11	11	11	11	11	11	11	11	11	11
21.	25	11	11	11	11	11	11	11	11	11	11
22.	26	11	11	11	11	11	11	11	11	11	11
23.	27	11	11	11	11	11	11	11	11	11	11
24.	28	11	11	11	11	11	11	11	11	11	11
25.	29	11	11	11	11	11	11	11	11	11	11
26.	30	11	11	11	11	11	11	11	11	11	11
27.	31	11	11	11	11	11	11	11	11	11	11
28.	32	11	11	11	11	11	11	11	11	11	11
29.	33	11	11	11	11	11	11	11	11	11	11
30.	34	11	11	11	11	11	11	11	11	11	11
31.	35	11	11	11	11	11	11	11	11	11	11
32.	36	11	11	11	11	11	11	11	11	11	11
33.	37	11	11	11	11	11	11	11	11	11	11
34.	38	11	11	11	11	11	11	11	11	11	11
35.	39	11	11	11	11	11	11	11	11	11	11
36.	40	11	11	11	11	11	11	11	11	11	11
37.	41	11	11	11	11	11	11	11	11	11	11
38.	42	11	11	11	11	11	11	11	11	11	11
39.	43	11	11	11	11	11	11	11	11	11	11
40.	44	11	11	11	11	11	11	11	11	11	11
41.	45	11	11	11	11	11	11	11	11	11	11
42.	46	11	11	11	11	11	11	11	11	11	11
43.	47	11	11	11	11	11	11	11	11	11	11
44.	48	11	11	11	11	11	11	11	11	11	11
45.	49	11	11	11	11	11	11	11	11	11	11
46.	50	11	11	11	11	11	11	11	11	11	11
47.	51	11	11	11	11	11	11	11	11	11	11
48.	52	11	11	11	11	11	11	11	11	11	11
49.	53	11	11	11	11	11	11	11	11	11	11
50.	54	11	11	11	11	11	11	11	11	11	11
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81.	85	11	11	11	11	11	11	11	11	11	11
82.	86	11	11	11	11	11	11	11	11	11	11
83.	87	11	11	11	11	11	11	11	11	11	11
84.	88	11	11	11	11	11	11	11	11	11	11
85.	89	11	11	11	11	11	11	11	11	11	11
86.	90	11	11	11	11	11	11	11	11	11	11
87.	91	11	11	11	11	11	11	11	11	11	11
88.	92	11	11	11	11	11	11	11	11	11	11
89.	93	11	11	11	11	11	11	11	11	11	11
90.	94	11	11	11	11	11	11	11	11	11	11
91.	95	11	11	11	11	11	11	11	11	11	11
92.	96	11	11	11	11	11	11	11	11	11	11
93.	97	11	11	11	11	11	11	11	11	11	11
94.	98	11	11	11	11	11	11	11	11	11	11
95.	99	11	11	11	11	11	11	11	11	11	11
96.	100	11	11	11	11	11	11	11	11	11	11

TABLE 2. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

WEIGHTED AVERAGE SENSITIVITY TO EQUAL TGT LOGIC ERROR RMS											
BL	12	10	8	6	4	2	1	UP	DOWN	LEFT	RIGHT
0.00	2	9	-9	25	1.00	1.00	9	0.5	0.00	0.30	0.00
-2	-6	-8	-97	-52	-34	-56	-20	-16	-14	-6	-6
-6	-2	-9	33	26	19	15	15	14	14	14	14
-2	-6	-125	-58	-36	-25	-18	-12	-10	-9	-5	-5
-6	-2	-15	24	20	16	14	13	12	12	12	12
-2	-6	-77	-34	-23	-16	-12	-8	-7	-6	-4	-4
-6	-2	-10	16	14	12	12	11	10	10	10	10
-2	-6	-155	-63	-43	-22	-14	-10	-8	-6	-3	-3
-6	-2	-15	14	12	11	10	9	8	6	6	6
-2	-6	-71	-12	-6	-5	-4	-3	-2	-2	-1	-1
-6	-2	-12	15	9	7	7	7	6	7	7	7
-2	-2	-19	-4	-4	-3	-2	-2	-1	-1	-1	-1
-4	-2	-7	6	6	5	5	5	5	6	6	6
-2	-4	-2	-2	-1	-1	-1	-1	-1	-1	-1	-1
-3	-3	-4	4	4	3	3	3	2	2	2	2
-2	-2	-9	3	6	6	6	6	5	5	5	5
-2	-1	-2	2	2	2	2	2	2	2	2	2
-1	-2	-3	0	0	0	0	0	0	0	0	0
0	0	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
2	2	0	0	0	0	0	0	0	0	0	0
3	1	0	0	0	0	0	0	0	0	0	0
2	0	0	0	0	0	0	0	0	0	0	0
4	2	0	0	0	0	0	0	0	0	0	0
2	-5	-2	-1	-1	-1	-1	-1	-1	-1	-1	-1
2	-16	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2
6	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2
2	-30	-11	-6	-4	-3	-2	-2	-2	-2	-2	-2
9	-3	-2	-5	-4	-4	-4	-4	-4	-4	-4	-4
2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2

TABLE 3. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

TABLE 4. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 4

TABLE 5. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 5

BL	WEIGHTED RANGE SOLUTION TO EVAL TGT LOCN ERROR XFER FNS										TE 0.00 10. 20. 30. 40. 50. 60. 70. 80. 90. 100.	
	1P	10	25	50	1,000	1,000	5IN	22	V1	V2	V3	
5	0.0	-0.9	25	1,000	1,000	0.0	0.00	0.00	0.00	0.00	0.00	10.00
6	0.0	-0.9	17*	10*	7*	6*	5*	4*	3*	2*	2*	1*
7	0.0	-0.7	6*	5*	4*	3*	2*	1*	0*	0*	0*	0*
8	0.0	20*	10*	7*	5*	4*	3*	2*	1*	0*	0*	0*
9	0.0	-0.6	5*	4*	3*	2*	1*	0*	0*	0*	0*	0*
10	0.0	38*	11*	6*	4*	3*	2*	1*	0*	0*	0*	0*
11	0.7	-0.4	-3	-3	-3	-3	-3	-3	-3	-3	-3	1*
12	0.5	16*	5*	3*	2*	2*	1*	1*	0*	0*	0*	0*
13	0.6	-0.4	-2	-2	-2	-2	-2	-2	-2	-2	-2	0*
14	0.5	5*	2*	1*	1*	1*	0*	0*	0*	0*	0*	0*
15	0.5	-1	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
16	0.5	1*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
17	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
18	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
19	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
20	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
21	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
22	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
23	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
24	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
25	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
26	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
27	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
28	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
29	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
30	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
31	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
32	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
33	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
34	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
35	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
36	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
37	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
38	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
39	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
40	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
41	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
42	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
43	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
44	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
45	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
46	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
47	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
48	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
49	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
50	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
51	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
52	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
53	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
54	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
55	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
56	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
57	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
58	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
59	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
60	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
61	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
62	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
63	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
64	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
65	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
66	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
67	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
68	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
69	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
70	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
71	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
72	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
73	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
74	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
75	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
76	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
77	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
78	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
79	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
80	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
81	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
82	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
83	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
84	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
85	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
86	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
87	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
88	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
89	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
90	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
91	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
92	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
93	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
94	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
95	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
96	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
97	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
98	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
99	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
100	0.5	0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*

TABLE 6. X- AND Y-COMPONENT ERRORS DUE TO A 1-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 6

TABLE 7. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE

WEIGHTED RANGE SOLUTION TO EVAL PAR LUCH FANN XPER PCNS											
AL	IP	T _h	N	DXY	UP	IN	22	V ₁	V ₂	V ₃	TE
4.00	1	0	-9	25	1,000	3.00	5	0.00	0.00	0.00	10.00
-9	-156	-92	-69	-58	-55	-52	-50	-49	-48	-48	-48
1	450	130	66	66	66	66	66	-63	-67	-71	-76
-8	-111	-65	-44	-42	-41	-42	-43	-40	-41	-42	-43
1	881	145	78	95	88	88	88	-60	-66	-69	-75
-7	-73	-88	-35	-32	-32	-32	-32	-54	-54	-58	-69
1	935	75	48	33	26	26	23	-36	-40	-46	-53
-6	-63	-27	-28	-23	-20	-20	-30	-33	-35	-40	-53
1	93	23	19	17	17	17	17	-16	-16	-16	-16
-5	-21	-15	-16	-16	-16	-20	-22	-25	-25	-25	-25
1	26	13	11	11	10	11	11	-12	-12	-14	-14
-4	-8	-10	-12	-14	-14	-10	-9	-24	-27	-31	-35
1	4	5	5	6	6	6	6	-10	-10	-10	-10
-3	-2	-6	-7	-9	-11	-13	-15	-15	-15	-15	-15
1	1	2	2	3	3	3	3	-10	-12	-14	-14
-2	-1	-3	-5	-6	-8	-10	-12	-12	-12	-12	-12
1	0	0	0	0	0	0	0	-10	-12	-14	-14
-1	-1	-2	-3	-4	-5	-6	-7	-7	-8	-9	-9
1	0	0	0	0	0	0	0	-10	-12	-14	-14
0	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
-1	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
0	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
2	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
3	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
4	0	0	0	0	0	0	0	-10	-12	-14	-14
1	0	0	0	0	0	0	0	-10	-12	-14	-14
5	0	0	0	0	0	0	0	-10	-12	-14	-14
1	288	-9	-6	-5	-5	-4	-4	-74	-68	-68	-68
6	-28	-4	-5	-6	-7	-10	-13	-16	-20	-24	-28
1	976	-93	-13	-10	-10	-10	-10	-12	-12	-12	-12
1	1039	-92	-48	-33	-21	-21	-22	-22	-22	-22	-22
9	-86	-22	-19	-16	-15	-15	-15	-16	-16	-16	-16

TABLE 8. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

WEIGHTED RANGE SOLUTION TO EVAL TEF LOCN ERRN XPER FCNS											
RL	TP	T ¹	T ²	V ¹	V ²	IN	22	V ¹	V ²	V ³	TE
0.00	2	8	25	1.00	3.00	9	0	0.00	0.00	0.00	16.00
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-9	70	144	99	78	66	58	53	49	47	15*
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-8	220	111	78	62	53	46	41	39	37	12*
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-7	161	92	59	48	42	38	36	34	32	9*
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-6	106	47	43	37	33	31	28	27	26	6*
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-5	61	16	30	27	25	21	22	21	20	35
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-4	29	21	20	19	19	17	16	16	17	31
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-3	10	12	13	12	11	11	12	12	13	28
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-2	3	7	8	7	7	7	6	6	6	24
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	-1	1	2	2	2	2	2	2	2	2	23
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	0	-1	-1	0	0	0	0	0	0	0	24
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	1	0	0	0	0	0	0	0	0	0	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	2	0	0	0	0	0	0	0	0	0	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	3	0	0	0	0	0	0	0	0	0	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	4	-1	1	2	2	2	2	3	4	5	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	5	0	0	0	0	0	0	0	0	0	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	6	-12	0	0	0	0	0	0	0	0	25
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	7	-23	-13	-10	-9	-10	-10	-10	-10	-10	2
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	8	-39	-20	-15	-13	-12	-12	-12	-11	-10	4
2 ⁰ *0.95*+3.61*+7.63*+10.61*+10.61*+10.61*+10.61*	9	-57	-29	-18	-16	-14	-14	-13	-12	-11	2

TABLE 9. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

WEIGHTED RANGE SOLUTION TO EVAL 749 LOEN-EARRA XFER PENS											
RL	IP	IN	M	N	PKV	UP	DN	IN	V1	V2	Y3
4.00	3	8	-9	25	1,000	3.00	5	0.0	0.00	0.00	10.00
3+ 1480+ 105+ 0+ 67+ -92+ -44+ -40+ -36+ -35+ -35+ -35+ -35+ -35+	-9	11	23	23	24	24	31	34	81	45	49
-9	11	23	23	24	24	24	31	34	81	45	49
3+ 127+ -42+ -33+ -29+ -27+ -27+ -27+ -27+ -27+ -27+ -27+ -27+	-8	9	12	15	18	22	25	29	32	40	44
-8	9	12	15	18	22	25	29	32	40	44	48
3+ 43+ -6+ -13+ -16+ -16+ -17+ -16+ -19+ -20+ -21+ -21+ -21+	-7	12	0	5	9	13	17	21	24	28	32
-7	12	0	5	9	13	17	21	24	28	32	35
3+ 68+ 7+ -3+ -6+ -10+ -12+ -14+ -14+ -15+ -16+ -16+ -17+	-6	16	5	0	5	9	14	17	21	25	28
-6	16	5	0	5	9	14	17	21	25	28	32
3+ 50+ 9+ 0+ -4+ -7+ -9+ -10+ -11+ -11+ -12+ -12+ -13+	-5	17	-7	-1	3	7	11	15	18	22	25
-5	17	-7	-1	3	7	11	15	18	22	25	29
3+ 24+ 5+ 0+ -2+ -4+ -6+ -6+ -6+ -6+ -6+ -6+ -6+	-4	12	-6	-2	2	6	10	13	16	20	23
-4	12	-6	-2	2	6	10	13	16	20	23	26
3+ 5+ 1+ 0+ -2+ -3+ -4+ -4+ -4+ -4+ -4+ -4+ -4+	-3	6	-4	-1	2	6	9	12	15	18	21
-3	6	-4	-1	2	6	9	12	15	18	21	24
3+ 0+ 0+ 0+ -1+ -2+ -3+ -3+ -3+ -3+ -3+ -3+ -3+	-2	-2	1	4	7	9	11	14	16	19	22
-2	-2	1	4	7	9	11	14	16	19	22	25
3+ -1+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	-1	1	3	4	5	6	8	10	12	15	17
-1	1	3	4	5	6	8	10	12	15	17	20
3+ 1+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	0	1	2	3	4	5	6	8	10	13	16
0	1	2	3	4	5	6	8	10	13	16	19
3+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	1	-1	0	0	0	0	0	0	0	0	0
1	-1	0	0	0	0	0	0	0	0	0	0
3+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	2	0	-1	-1	0	0	0	0	0	0	0
2	0	-1	-1	0	0	0	0	0	0	0	0
3+ -1+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	3	-1	-2	-2	-1	0	0	0	0	0	0
3	-1	-2	-2	-1	0	0	0	0	0	0	0
3+ -9+ -3+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	4	-4	-4	-4	-3	-2	-2	-2	-2	-2	-2
4	-4	-4	-4	-3	-2	-2	-2	-2	-2	-2	-2
3+ -33+ -10+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	5	-11	-7	-5	-4	-3	-2	-1	0	0	0
5	-11	-7	-5	-4	-3	-2	-1	0	0	0	0
3+ -60+ -22+ -10+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	6	-20	-11	-8	-6	-4	-2	0	0	0	0
6	-20	-11	-8	-6	-4	-2	0	0	0	0	0
3+ -131+ -17+ -16+ 0+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	7	-10	-15	-10	-7	-5	-3	-1	0	0	0
7	-10	-15	-10	-7	-5	-3	-1	0	0	0	0
3+ -235+ -56+ -23+ -11+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	8	-51	-19	-12	-8	-5	-2	0	0	0	0
8	-51	-19	-12	-8	-5	-2	0	0	0	0	0
3+ -165+ -74+ -28+ -12+ 0+ 0+ 0+ 0+ 0+ 0+ 0+	9	-53	-22	-13	-8	-5	-2	0	0	0	0
9	-53	-22	-13	-8	-5	-2	0	0	0	0	0

TABLE 10. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 4

WEIGHTED RANGE SOLUTION TO EVAL TAY LOCN EROR XPER FCNS											
PL	IP	T _n	M _n	D _{XV}	Up	V ₂₂	V ₁	V ₂	V ₃	TE	
4.00	4	6	-9	25	1.000	3.00	-5	0.0	0.00	10.00	
4 ⁺	363 ⁺	74 ⁺	26 ⁺	12 ⁺	4 ⁺	-7 ⁺	-9 ⁺	-11 ⁺	-15 ⁺	-17 ⁺	
-9	-53	-22	-13	-8	-4	-1	5	8	12	16	
4 ⁺	295 ⁺	56 ⁺	23 ⁺	11 ⁺	6 ⁺	-5 ⁺	-5 ⁺	-9 ⁺	-13 ⁺	-14 ⁺	
-6	-41	-19	-12	-6	-5	-2	0	4	7	11	
4 ⁺	151 ⁺	37 ⁺	16 ⁺	8 ⁺	3 ⁺	-2 ⁺	-4 ⁺	-6 ⁺	-9 ⁺	-11 ⁺	
-7	-30	-15	-10	-7	-4	-2	0	3	6	10	
4 ⁺	80 ⁺	22 ⁺	10 ⁺	5 ⁺	2 ⁺	0 ⁺	-1 ⁺	-2 ⁺	-3 ⁺	-4 ⁺	
-6	-20	-11	-6	-4	-2	-1	0	3	6	10	
4 ⁺	33 ⁺	10 ⁺	5 ⁺	3 ⁺	1 ⁺	-1 ⁺	-3 ⁺	-4 ⁺	-6 ⁺	-8 ⁺	
-5	-11	-7	-5	-4	-3	-1	1	4	7	10	
4 ⁺	9 ⁺	3 ⁺	2 ⁺	1 ⁺	0 ⁺	-2 ⁺	-3 ⁺	-4 ⁺	-5 ⁺	-6 ⁺	
-4	-4	-4	-3	-2	-2	0	2	4	7	11	
4 ⁺	1 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	-1 ⁺	-1 ⁺	-2 ⁺	-3 ⁺	-4 ⁺	
-3	-1	-2	-2	-1	0	3	5	8	11	15	
4 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	-1 ⁺	-1 ⁺	-2 ⁺	-3 ⁺	-4 ⁺	
-2	0	-1	-1	0	2	4	7	10	13	16	
4 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	
-1	-1	-1	0	2	4	6	9	11	14	17	
4 ⁺	-1 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	
0	1	2	3	4	5	6	8	10	13	16	
4 ⁺	1 ⁺	0 ⁺	0 ⁺	0 ⁺	0 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	-1 ⁺	
1	1	3	4	5	6	8	10	12	15	17	
4 ⁺	0 ⁺	0 ⁺	0 ⁺	1 ⁺	2 ⁺	3 ⁺	3 ⁺	3 ⁺	3 ⁺	3 ⁺	
2	-2	-1	4	7	6	11	14	16	19	22	
4 ⁺	-5 ⁺	-1 ⁺	0 ⁺	2 ⁺	3 ⁺	4 ⁺	4 ⁺	4 ⁺	4 ⁺	4 ⁺	
3	-6	-4	-1	2	6	9	12	15	18	21	
4 ⁺	-24 ⁺	-5 ⁺	0 ⁺	2 ⁺	4 ⁺	6 ⁺	8 ⁺	8 ⁺	9 ⁺	10 ⁺	
4	-12	-6	-2	2	6	10	13	16	20	23	
4 ⁺	-50 ⁺	-9 ⁺	0 ⁺	4 ⁺	7 ⁺	11 ⁺	12 ⁺	13 ⁺	14 ⁺	15 ⁺	
5	-17	-7	-1	3	7	11	15	18	22	25	
4 ⁺	-64 ⁺	-7 ⁺	3 ⁺	6 ⁺	10 ⁺	14 ⁺	15 ⁺	17 ⁺	18 ⁺	19 ⁺	
6	-18	-5	0	5	9	13	17	19	21	25	
4 ⁺	-43 ⁺	6 ⁺	13 ⁺	16 ⁺	17 ⁺	18 ⁺	19 ⁺	20 ⁺	21 ⁺	22 ⁺	
7	-12	0	5	9	13	17	21	24	28	32	
4 ⁺	27 ⁺	42 ⁺	33 ⁺	29 ⁺	27 ⁺	27 ⁺	28 ⁺	29 ⁺	30 ⁺	31 ⁺	
8	-2	9	12	15	19	22	25	29	32	36	
4 ⁺	140 ⁺	105 ⁺	67 ⁺	52 ⁺	46 ⁺	38 ⁺	36 ⁺	35 ⁺	34 ⁺	33 ⁺	
9	11	23	24	28	31	34	36	41	45	49	

TABLE 11. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 5

WEIGHTED RANGE SOLUTION TO EVAL TGY LOCN EGNR XFER FCHS											
RL	IP	T _n	W	D _N	UP	V ₁	V ₂	V ₃	V ₄	V ₅	V ₆
0.00	3	8	-9	25	1,000	3.00	9	0.0	0.00	0.00	0.00
5*	132*	51*	32*	23*	18*	-15*	-13*	-11*	-9*	-7*	-5*
-9	-57	-29	-21	-18	-16	-15	-14	-13	-12	-11	-10
5*	233*	62*	32*	21*	16*	13*	11*	9*	7*	5*	4*
-8	-39	-20	-15	-13	-12	-12	-12	-11	-10	-9	-8
5*	117*	33*	18*	12*	10*	8*	7*	6*	5*	4*	3*
-7	-23	-13	-10	-10	-9	-9	-10	-10	-10	-9	-8
5*	50*	15*	9*	7*	6*	5*	4*	3*	2*	1*	0*
-6	-12	-7	-6	-7	-8	-8	-8	-8	-7	-6	-5
5*	16*	6*	4*	3*	3*	3*	2*	2*	1*	0*	0*
-5	-5	-4	-4	-5	-6	-7	-7	-6	-5	-4	-3
5*	3*	1*	1*	1*	2*	1*	1*	1*	0*	0*	0*
-4	-1	-2	-3	-4	-5	-5	-5	-4	-3	-2	-1
5*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
-3	0	0	-1	-2	-3	-4	-4	-3	-2	-1	0
5*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
-2	0	0	-1	-2	-3	-3	-2	-1	0	1	2
5*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
-1	0	0	-1	-2	-2	-1	0	0	1	2	3
5*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
0	-1	-1	0	-1	0	0	1	0	1	2	3
5*	-1*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
1	1	2	2	2	3	3	4	5	6	7	8
5*	1*	1*	1*	1*	1*	0*	0*	0*	0*	0*	0*
2	3	7	7	7	7	7	7	7	7	7	7
5*	12*	8*	7*	5*	4*	3*	3*	2*	2*	1*	1*
3	10	12	13	12	11	11	11	12	12	13	13
5*	67*	26*	17*	13*	10*	8*	7*	6*	4*	3*	3*
4	29	21	19	18	17	16	16	16	17	18	19
5*	922*	236*	64*	36*	25*	19*	14*	12*	10*	8*	6*
5	61	16	30	27	25	21	21	20	21	22	23
5*	485*	132*	68*	48*	32*	25*	20*	17*	14*	11*	8*
6	106	57	43	37	30	28	27	26	25	26	27
5*	922*	236*	114*	71*	50*	36*	31*	25*	22*	19*	14*
7	161	62	59	48	42	34	32	31	31	31	32
5*	568*	263*	156*	104*	74*	61*	40*	42*	36*	24*	17*
9	970	144	99	78	66	54	53	49	47	45	43

TABLE 12. X- AND Y-COMPONENT ERRORS DUE TO A 3-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 6

TABLE 13. X- AND Y-COMPONENT ERRORS DUE TO A 10-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

WEIGHTED RANGE SOLUTION TO EQUATION OF STATE FOR PCNS									
SL	IP	X	Y	UP	DOWN	UP	DOWN	V1	V2
4.00	1	0	25	1.000	10.00	9	0.0	0.00	0.00
1	-67	423	316	237	221	196	186	163	161
2	-51	281	191	176	171	179	177	187	187
3	-215	115	107	106	109	114	110	115	117
4	-7	215	140	121	130	140	152	165	179
5	-68	51	61	76	64	106	118	111	117
6	-215	162	167	162	161	148	139	136	131
7	-205	205	203	217	192	181	161	129	131
8	-137	167	164	159	151	135	145	152	157
9	-137	162	167	164	159	137	137	162	173
10	-215	113	114	126	115	108	106	102	101
11	-56	56	61	66	56	106	118	132	140
12	-27	53	60	67	54	106	118	132	140
13	-27	53	60	67	54	106	118	132	140
14	-27	53	60	67	54	106	118	132	140
15	-15	23	30	36	43	60	66	70	74
16	-3	6	9	10	11	13	14	15	16
17	-4	11	17	23	26	30	33	35	37
18	-1	2	3	4	5	6	7	8	9
19	-1	1	2	2	3	4	5	6	7
20	-2	5	10	16	22	30	35	39	42
21	-1	1	2	3	4	5	6	7	8
22	-1	1	2	3	4	5	6	7	8
23	-1	1	2	3	4	5	6	7	8
24	-1	1	2	3	4	5	6	7	8
25	-1	1	2	3	4	5	6	7	8
26	-1	1	2	3	4	5	6	7	8
27	-1	1	2	3	4	5	6	7	8
28	-1	1	2	3	4	5	6	7	8
29	-1	1	2	3	4	5	6	7	8
30	-1	1	2	3	4	5	6	7	8
31	-1	1	2	3	4	5	6	7	8
32	-1	1	2	3	4	5	6	7	8
33	-1	1	2	3	4	5	6	7	8
34	-1	1	2	3	4	5	6	7	8
35	-1	1	2	3	4	5	6	7	8
36	-1	1	2	3	4	5	6	7	8
37	-1	1	2	3	4	5	6	7	8
38	-1	1	2	3	4	5	6	7	8
39	-1	1	2	3	4	5	6	7	8
40	-1	1	2	3	4	5	6	7	8
41	-1	1	2	3	4	5	6	7	8
42	-1	1	2	3	4	5	6	7	8
43	-1	1	2	3	4	5	6	7	8
44	-1	1	2	3	4	5	6	7	8
45	-1	1	2	3	4	5	6	7	8
46	-1	1	2	3	4	5	6	7	8
47	-1	1	2	3	4	5	6	7	8
48	-1	1	2	3	4	5	6	7	8
49	-1	1	2	3	4	5	6	7	8
50	-1	1	2	3	4	5	6	7	8
51	-1	1	2	3	4	5	6	7	8
52	-1	1	2	3	4	5	6	7	8
53	-1	1	2	3	4	5	6	7	8
54	-1	1	2	3	4	5	6	7	8
55	-1	1	2	3	4	5	6	7	8
56	-1	1	2	3	4	5	6	7	8
57	-1	1	2	3	4	5	6	7	8
58	-1	1	2	3	4	5	6	7	8
59	-1	1	2	3	4	5	6	7	8
60	-1	1	2	3	4	5	6	7	8
61	-1	1	2	3	4	5	6	7	8
62	-1	1	2	3	4	5	6	7	8
63	-1	1	2	3	4	5	6	7	8
64	-1	1	2	3	4	5	6	7	8
65	-1	1	2	3	4	5	6	7	8
66	-1	1	2	3	4	5	6	7	8
67	-1	1	2	3	4	5	6	7	8
68	-1	1	2	3	4	5	6	7	8
69	-1	1	2	3	4	5	6	7	8
70	-1	1	2	3	4	5	6	7	8
71	-1	1	2	3	4	5	6	7	8
72	-1	1	2	3	4	5	6	7	8
73	-1	1	2	3	4	5	6	7	8
74	-1	1	2	3	4	5	6	7	8
75	-1	1	2	3	4	5	6	7	8
76	-1	1	2	3	4	5	6	7	8
77	-1	1	2	3	4	5	6	7	8
78	-1	1	2	3	4	5	6	7	8
79	-1	1	2	3	4	5	6	7	8
80	-1	1	2	3	4	5	6	7	8
81	-1	1	2	3	4	5	6	7	8
82	-1	1	2	3	4	5	6	7	8
83	-1	1	2	3	4	5	6	7	8
84	-1	1	2	3	4	5	6	7	8
85	-1	1	2	3	4	5	6	7	8
86	-1	1	2	3	4	5	6	7	8
87	-1	1	2	3	4	5	6	7	8
88	-1	1	2	3	4	5	6	7	8
89	-1	1	2	3	4	5	6	7	8
90	-1	1	2	3	4	5	6	7	8
91	-1	1	2	3	4	5	6	7	8
92	-1	1	2	3	4	5	6	7	8
93	-1	1	2	3	4	5	6	7	8
94	-1	1	2	3	4	5	6	7	8
95	-1	1	2	3	4	5	6	7	8
96	-1	1	2	3	4	5	6	7	8
97	-1	1	2	3	4	5	6	7	8
98	-1	1	2	3	4	5	6	7	8
99	-1	1	2	3	4	5	6	7	8
100	-1	1	2	3	4	5	6	7	8
101	-1	1	2	3	4	5	6	7	8
102	-1	1	2	3	4	5	6	7	8
103	-1	1	2	3	4	5	6	7	8
104	-1	1	2	3	4	5	6	7	8
105	-1	1	2	3	4	5	6	7	8
106	-1	1	2	3	4	5	6	7	8
107	-1	1	2	3	4	5	6	7	8
108	-1	1	2	3	4	5	6	7	8
109	-1	1	2	3	4	5	6	7	8
110	-1	1	2	3	4	5	6	7	8
111	-1	1	2	3	4	5	6	7	8
112	-1	1	2	3	4	5	6	7	8
113	-1	1	2	3	4	5	6	7	8
114	-1	1	2	3	4	5	6	7	8
115	-1	1	2	3	4	5	6	7	8
116	-1	1	2	3	4	5	6	7	8
117	-1	1	2	3	4	5	6	7	8
118	-1	1	2	3	4	5	6	7	8
119	-1	1	2	3	4	5	6	7	8
120	-1	1	2	3	4	5	6	7	8
121	-1	1	2	3	4	5	6	7	8
122	-1	1	2	3	4	5	6	7	8
123	-1	1	2	3	4	5	6	7	8
124	-1	1	2	3	4	5	6	7	8
125	-1	1	2	3	4	5	6	7	8
126	-1	1	2	3	4	5	6	7	8
127	-1	1	2	3	4	5	6	7	8
128	-1	1	2	3	4	5	6	7	8
129	-1	1	2	3	4	5	6	7	8
130	-1	1	2	3	4	5	6	7	8
131	-1	1	2	3	4	5	6	7	8
132	-1	1	2	3	4	5	6	7	8
133	-1	1	2	3	4	5	6	7	8
134	-1	1	2	3	4	5	6	7	8
135	-1	1	2	3	4	5	6	7	8
136	-1	1	2	3	4	5	6	7	8
137	-1	1	2	3	4	5	6	7	8
138	-1	1	2	3	4	5	6	7	8
139	-1	1	2	3	4	5	6	7	8
140	-1	1	2	3	4	5	6	7	8
141	-1	1	2	3	4	5	6	7	8
142	-1	1	2	3	4	5	6	7	8
143	-1	1	2	3	4	5	6	7	8
144	-1	1	2	3	4	5	6	7	8
145	-1	1	2	3	4	5	6	7	8
146	-1	1	2	3	4	5	6	7	8
147	-1	1	2	3	4	5	6	7	8
148	-1	1	2	3	4	5	6	7	8
149	-1	1	2	3	4	5	6	7	8
150	-1	1	2	3	4	5	6	7	8
151	-1	1	2	3	4	5	6	7	8
152	-1	1	2	3	4	5	6	7	8
153	-1	1	2	3	4	5	6	7	8
154	-1	1	2	3	4	5	6	7	8
155	-1	1	2	3	4	5	6	7	8
156	-1	1	2	3	4	5	6	7	8
157	-1	1	2	3	4	5	6	7	8
158	-1	1	2	3	4	5	6	7	8
159	-1	1	2	3	4	5	6	7	8
160	-1	1	2						

TABLE 14. X- AND Y-COMPONENT ERRORS DUE TO A 10-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

TABLE 15. X- AND Y-COMPONENT ERRORS DUE TO A 10-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

WEIGHTED GROSS SUGAR TO GROWER FOB CS											
SL.	YR	QTR	Up	1W	22	V1	V2	V3	V4	Up	TE
90.	91.	92.	93.	94.	95.	96.	97.	98.	99.	90.	91.
37	695	700	705	710	715	720	725	730	735	700	705
38	710	715	720	725	730	735	740	745	750	710	715
39	720	725	730	735	740	745	750	755	760	720	725
40	730	735	740	745	750	755	760	765	770	730	735
41	740	745	750	755	760	765	770	775	780	740	745
42	750	755	760	765	770	775	780	785	790	750	755
43	760	765	770	775	780	785	790	795	800	760	765
44	770	775	780	785	790	795	800	805	810	770	775
45	780	785	790	795	800	805	810	815	820	780	785
46	790	795	800	805	810	815	820	825	830	790	795
47	800	805	810	815	820	825	830	835	840	800	805
48	810	815	820	825	830	835	840	845	850	810	815
49	820	825	830	835	840	845	850	855	860	820	825
50	830	835	840	845	850	855	860	865	870	830	835
51	840	845	850	855	860	865	870	875	880	840	845
52	850	855	860	865	870	875	880	885	890	850	855
53	860	865	870	875	880	885	890	895	900	860	865
54	870	875	880	885	890	895	900	905	910	870	875
55	880	885	890	895	900	905	910	915	920	880	885
56	890	895	900	905	910	915	920	925	930	890	895
57	900	905	910	915	920	925	930	935	940	900	905
58	910	915	920	925	930	935	940	945	950	910	915
59	920	925	930	935	940	945	950	955	960	920	925
60	930	935	940	945	950	955	960	965	970	930	935
61	940	945	950	955	960	965	970	975	980	940	945
62	950	955	960	965	970	975	980	985	990	950	955
63	960	965	970	975	980	985	990	995	1000	960	965
64	970	975	980	985	990	995	1000	1005	1010	970	975
65	980	985	990	995	1000	1005	1010	1015	1020	980	985
66	990	995	1000	1005	1010	1015	1020	1025	1030	990	995
67	1000	1005	1010	1015	1020	1025	1030	1035	1040	1000	1005
68	1010	1015	1020	1025	1030	1035	1040	1045	1050	1010	1015
69	1020	1025	1030	1035	1040	1045	1050	1055	1060	1020	1025
70	1030	1035	1040	1045	1050	1055	1060	1065	1070	1030	1035
71	1040	1045	1050	1055	1060	1065	1070	1075	1080	1040	1045
72	1050	1055	1060	1065	1070	1075	1080	1085	1090	1050	1055
73	1060	1065	1070	1075	1080	1085	1090	1095	1100	1060	1065
74	1070	1075	1080	1085	1090	1095	1100	1105	1110	1070	1075
75	1080	1085	1090	1095	1100	1105	1110	1115	1120	1080	1085
76	1090	1095	1100	1105	1110	1115	1120	1125	1130	1090	1095
77	1100	1105	1110	1115	1120	1125	1130	1135	1140	1100	1105
78	1110	1115	1120	1125	1130	1135	1140	1145	1150	1110	1115
79	1120	1125	1130	1135	1140	1145	1150	1155	1160	1120	1125
80	1130	1135	1140	1145	1150	1155	1160	1165	1170	1130	1135
81	1140	1145	1150	1155	1160	1165	1170	1175	1180	1140	1145
82	1150	1155	1160	1165	1170	1175	1180	1185	1190	1150	1155
83	1160	1165	1170	1175	1180	1185	1190	1195	1200	1160	1165
84	1170	1175	1180	1185	1190	1195	1200	1205	1210	1170	1175
85	1180	1185	1190	1195	1200	1205	1210	1215	1220	1180	1185
86	1190	1195	1200	1205	1210	1215	1220	1225	1230	1190	1195
87	1200	1205	1210	1215	1220	1225	1230	1235	1240	1200	1205
88	1210	1215	1220	1225	1230	1235	1240	1245	1250	1210	1215
89	1220	1225	1230	1235	1240	1245	1250	1255	1260	1220	1225
90	1230	1235	1240	1245	1250	1255	1260	1265	1270	1230	1235
91	1240	1245	1250	1255	1260	1265	1270	1275	1280	1240	1245
92	1250	1255	1260	1265	1270	1275	1280	1285	1290	1250	1255
93	1260	1265	1270	1275	1280	1285	1290	1295	1300	1260	1265
94	1270	1275	1280	1285	1290	1295	1300	1305	1310	1270	1275
95	1280	1285	1290	1295	1300	1305	1310	1315	1320	1280	1285
96	1290	1295	1300	1305	1310	1315	1320	1325	1330	1290	1295
97	1300	1305	1310	1315	1320	1325	1330	1335	1340	1300	1305
98	1310	1315	1320	1325	1330	1335	1340	1345	1350	1310	1315
99	1320	1325	1330	1335	1340	1345	1350	1355	1360	1320	1325
100	1330	1335	1340	1345	1350	1355	1360	1365	1370	1330	1335
101	1340	1345	1350	1355	1360	1365	1370	1375	1380	1340	1345
102	1350	1355	1360	1365	1370	1375	1380	1385	1390	1350	1355
103	1360	1365	1370	1375	1380	1385	1390	1395	1400	1360	1365
104	1370	1375	1380	1385	1390	1395	1400	1405	1410	1370	1375
105	1380	1385	1390	1395	1400	1405	1410	1415	1420	1380	1385
106	1390	1395	1400	1405	1410	1415	1420	1425	1430	1390	1395
107	1400	1405	1410	1415	1420	1425	1430	1435	1440	1400	1405
108	1410	1415	1420	1425	1430	1435	1440	1445	1450	1410	1415
109	1420	1425	1430	1435	1440	1445	1450	1455	1460	1420	1425
110	1430	1435	1440	1445	1450	1455	1460	1465	1470	1430	1435
111	1440	1445	1450	1455	1460	1465	1470	1475	1480	1440	1445
112	1450	1455	1460	1465	1470	1475	1480	1485	1490	1450	1455
113	1460	1465	1470	1475	1480	1485	1490	1495	1500	1460	1465
114	1470	1475	1480	1485	1490	1495	1500	1505	1510	1470	1475
115	1480	1485	1490	1495	1500	1505	1510	1515	1520	1480	1485
116	1490	1495	1500	1505	1510	1515	1520	1525	1530	1490	1495
117	1500	1505	1510	1515	1520	1525	1530	1535	1540	1500	1505
118	1510	1515	1520	1525	1530	1535	1540	1545	1550	1510	1515
119	1520	1525	1530	1535	1540	1545	1550	1555	1560	1520	1525
120	1530	1535	1540	1545	1550	1555	1560	1565	1570	1530	1535
121	1540	1545	1550	1555	1560	1565	1570	1575	1580	1540	1545
122	1550	1555	1560	1565	1570	1575	1580	1585	1590	1550	1555
123	1560	1565	1570	1575	1580	1585	1590	1595	1600	1560	1565
124	1570	1575	1580	1585	1590	1595	1600	1605	1610	1570	1575
125	1580	1585	1590	1595	1600	1605	1610	1615	1620	1580	1585
126	1590	1595	1600	1605	1610	1615	1620	1625	1630	1590	1595
127	1600	1605	1610	1615	1620	1625	1630	1635	1640	1600	1605
128	1610	1615	1620	1625	1630	1635	1640	1645	1650	1610	1615
129	1620	1625	1630	1635	1640	1645	1650	1655	1660	1620	1625
130	1630	1635	1640	1645	1650	1655	1660	1665	1670	1630	1635
131	1640	1645	1650	1655	1660	1665	1670	1675	1680	1640	1645
132	1650	1655	1660	1665	1670	1675	1680	1685	1690	1650	1655
133	1660	1665	1670	1675	1680	1685	1690	1695	1700	1660	1665
134	1670	1675	1680	1685	1690	1695	1700	1705	1710	1670	1675
135	1680	1685	1690	1695	1700	1705	1710	1715	1720	1680	1685
136	1690	1695	1700	1705	1710	1715	1720	1725	1730	1690	1695
137	1700	1705	1710	1715	1720	1725	1730	1735	1740	1700	1705
138	1710	1715	1720	1725	1730	1735	1740	1745	1750	1710	1715
139	1720	1725	1730	1735	1740	1745	1750	1755	1760	1720	1725
140	1730	1735	1740	1745	1750	1755	1760	1765	1770	1730	1735
141	1740	1745	1750	1755	1760	1765	1770	1775	1780	1740	1745
142	1750	1755	1760	1765	1770	1775	1780	1785	1790	1750	1755
143	1760	1765	1770	1775	1780	1785	1790	1795	1800	1760	1765
144	1770	1775	1780	1785	1790	1795	1800	1805	1810	1770	1775
145	1780	1785	1790	1795	1800						

TABLE 16. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 1

WEIGHTED RANGE SOLUTION FOR RANS											
SL	TP	In	u	v	w	Up	22	V1	V2	V3	Tr
0.00	1	-6	25	1.00	30.00	5	0.0	0.00	0.00	0.00	10.00
-9	-674	-677	-929	-933	-933	-933	-933	-933	-933	-933	539
-8	-947	-947	-947	-947	-947	-947	-947	-947	-947	-947	470
-7	-945	-945	-945	-945	-945	-945	-945	-945	-945	-945	407
-6	-940	-940	-940	-940	-940	-940	-940	-940	-940	-940	345
-5	-939	-939	-939	-939	-939	-939	-939	-939	-939	-939	287
-4	-930	-930	-930	-930	-930	-930	-930	-930	-930	-930	229
-3	-922	-922	-922	-922	-922	-922	-922	-922	-922	-922	170
-2	-918	-918	-918	-918	-918	-918	-918	-918	-918	-918	110
-1	-910	-910	-910	-910	-910	-910	-910	-910	-910	-910	50
0	-900	-900	-900	-900	-900	-900	-900	-900	-900	-900	0
1	752	222	181	178	167	166	165	168	173	178	10
2	-179	-179	-179	-179	-179	-179	-179	-179	-179	-179	0
3	269	111	114	116	117	118	119	117	120	120	0
4	-76	-76	-76	-76	-76	-76	-76	-76	-76	-76	0
5	45	69	69	69	69	69	69	69	69	69	0
6	-92	-92	-92	-92	-92	-92	-92	-92	-92	-92	0
7	110	24	31	38	40	47	51	56	60	65	0
8	-17	-17	-17	-17	-17	-17	-17	-17	-17	-17	0
9	0	50	61	73	74	80	85	89	90	93	0
10	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	0
11	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0
44	0	0	0	0	0	0	0	0	0	0	0
45	0	0	0	0	0	0	0	0	0	0	0
46	0	0	0	0	0	0	0	0	0	0	0
47	0	0	0	0	0	0	0	0	0	0	0
48	0	0	0	0	0	0	0	0	0	0	0
49	0	0	0	0	0	0	0	0	0	0	0
50	0	0	0	0	0	0	0	0	0	0	0
51	0	0	0	0	0	0	0	0	0	0	0
52	0	0	0	0	0	0	0	0	0	0	0
53	0	0	0	0	0	0	0	0	0	0	0
54	0	0	0	0	0	0	0	0	0	0	0
55	0	0	0	0	0	0	0	0	0	0	0
56	0	0	0	0	0	0	0	0	0	0	0
57	0	0	0	0	0	0	0	0	0	0	0
58	0	0	0	0	0	0	0	0	0	0	0
59	0	0	0	0	0	0	0	0	0	0	0
60	0	0	0	0	0	0	0	0	0	0	0
61	0	0	0	0	0	0	0	0	0	0	0
62	0	0	0	0	0	0	0	0	0	0	0
63	0	0	0	0	0	0	0	0	0	0	0
64	0	0	0	0	0	0	0	0	0	0	0
65	0	0	0	0	0	0	0	0	0	0	0
66	0	0	0	0	0	0	0	0	0	0	0
67	0	0	0	0	0	0	0	0	0	0	0
68	0	0	0	0	0	0	0	0	0	0	0
69	0	0	0	0	0	0	0	0	0	0	0
70	0	0	0	0	0	0	0	0	0	0	0
71	0	0	0	0	0	0	0	0	0	0	0
72	0	0	0	0	0	0	0	0	0	0	0
73	0	0	0	0	0	0	0	0	0	0	0
74	0	0	0	0	0	0	0	0	0	0	0
75	0	0	0	0	0	0	0	0	0	0	0
76	0	0	0	0	0	0	0	0	0	0	0
77	0	0	0	0	0	0	0	0	0	0	0
78	0	0	0	0	0	0	0	0	0	0	0
79	0	0	0	0	0	0	0	0	0	0	0
80	0	0	0	0	0	0	0	0	0	0	0
81	0	0	0	0	0	0	0	0	0	0	0
82	0	0	0	0	0	0	0	0	0	0	0
83	0	0	0	0	0	0	0	0	0	0	0
84	0	0	0	0	0	0	0	0	0	0	0
85	0	0	0	0	0	0	0	0	0	0	0
86	0	0	0	0	0	0	0	0	0	0	0
87	0	0	0	0	0	0	0	0	0	0	0
88	0	0	0	0	0	0	0	0	0	0	0
89	0	0	0	0	0	0	0	0	0	0	0
90	0	0	0	0	0	0	0	0	0	0	0
91	0	0	0	0	0	0	0	0	0	0	0
92	0	0	0	0	0	0	0	0	0	0	0
93	0	0	0	0	0	0	0	0	0	0	0
94	0	0	0	0	0	0	0	0	0	0	0
95	0	0	0	0	0	0	0	0	0	0	0
96	0	0	0	0	0	0	0	0	0	0	0
97	0	0	0	0	0	0	0	0	0	0	0
98	0	0	0	0	0	0	0	0	0	0	0
99	0	0	0	0	0	0	0	0	0	0	0
100	0	0	0	0	0	0	0	0	0	0	0
101	0	0	0	0	0	0	0	0	0	0	0
102	0	0	0	0	0	0	0	0	0	0	0
103	0	0	0	0	0	0	0	0	0	0	0
104	0	0	0	0	0	0	0	0	0	0	0
105	0	0	0	0	0	0	0	0	0	0	0
106	0	0	0	0	0	0	0	0	0	0	0
107	0	0	0	0	0	0	0	0	0	0	0
108	0	0	0	0	0	0	0	0	0	0	0
109	0	0	0	0	0	0	0	0	0	0	0
110	0	0	0	0	0	0	0	0	0	0	0
111	0	0	0	0	0	0	0	0	0	0	0
112	0	0	0	0	0	0	0	0	0	0	0
113	0	0	0	0	0	0	0	0	0	0	0
114	0	0	0	0	0	0	0	0	0	0	0
115	0	0	0	0	0	0	0	0	0	0	0
116	0	0	0	0	0	0	0	0	0	0	0
117	0	0	0	0	0	0	0	0	0	0	0
118	0	0	0	0	0	0	0	0	0	0	0
119	0	0	0	0	0	0	0	0	0	0	0
120	0	0	0	0	0	0	0	0	0	0	0
121	0	0	0	0	0	0	0	0	0	0	0
122	0	0	0	0	0	0	0	0	0	0	0
123	0	0	0	0	0	0	0	0	0	0	0
124	0	0	0	0	0	0	0	0	0	0	0
125	0	0	0	0</							

TABLE 17. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 2

WEIGHTED MEAN CONTRIBUTION TO TOTAL ERROR XFER FCHS											
BL	IP	IN	U	N	UP	V1	V2	V3	V4	V5	V6
0.00	2	3	0	29	1.000	0.0	0.00	0.00	0.00	0.00	10.00
-0.000	72	814	732	627	543	501	463	434	413	396	374
0.000	702	713	615	524	472	424	366	326	306	300	291
-0.000	817	811	822	891	863	829	793	753	711	696	687
0.000	817	811	822	878	802	772	746	718	686	664	655
-0.000	817	811	822	878	802	772	746	718	686	664	655
0.000	182	482	375	130	300	278	242	251	248	239	230
-0.000	182	482	375	130	300	278	242	251	248	239	230
0.000	460	314	275	280	230	214	256	190	193	192	191
-0.000	547	527	524	195	181	180	180	180	180	180	180
0.000	130	114	114	131	122	114	111	110	111	110	110
-0.000	114	114	114	131	122	114	111	110	111	110	110
0.000	40	46	41	74	68	47	67	68	71	75	79
-0.000	11	17	26	29	27	34	30	44	46	55	61
0.000	0	0	0	46	46	46	70	70	90	100	100
-0.000	12	16	14	10	6	2	6	12	17	23	29
0.000	0	0	14	21	21	31	31	31	31	31	31
-0.000	1	-1	-6	-21	-21	-21	-21	-21	-21	-21	-21
0.000	0	0	0	0	0	0	0	0	0	0	0
-0.000	2	1	-3	-17	-21	-21	-21	-21	-21	-21	-21
0.000	0	0	0	0	0	0	0	0	0	0	0
-0.000	3	-4	-14	-26	-36	-42	-46	-46	-46	-46	-46
0.000	0	0	0	0	0	0	0	0	0	0	0
-0.000	2	-1	-19	-19	-19	-19	-19	-19	-19	-19	-19
0.000	0	0	0	0	0	0	0	0	0	0	0
-0.000	4	-13	-22	-22	-22	-22	-22	-22	-22	-22	-22
0.000	0	0	0	0	0	0	0	0	0	0	0
-0.000	20	172	141	141	141	141	141	141	141	141	141
0.000	559	560	562	562	562	562	562	562	562	562	562
-0.000	497	497	497	497	497	497	497	497	497	497	497
0.000	472	472	472	472	472	472	472	472	472	472	472
-0.000	397	397	397	397	397	397	397	397	397	397	397
0.000	397	397	397	397	397	397	397	397	397	397	397
-0.000	397	397	397	397	397	397	397	397	397	397	397

TABLE 18. X- AND Y-COMPONENT ERRORS DUE TO A 30-MILLISECOND ERROR IN ARRIVAL TIME AT MICROPHONE 3

TABLE 19. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 1 AND 2

RELATIVE RANGE SOLUTION TO EQL TGT LUCN ERROR XFM FNS											
SL	1 ^Y	10 ^W	W ^N	2 ^S	1,000 ^U	3,000 ^V	1W ^U	1L ^V	0,000 ^W	0,000 ^X	TE
0.000	1	6	-9	25	1,000	3,000	0.0	0.0	0.000	0.000	10.00
1.000	-132*	-53*	-23*	-59*	-0*	-56*	10*	13*	16*	10*	29*
2.000	44	28	18	12	6	1	-2	-7	-11	-12	-39*
3.000	-111*	-45*	-20*	-59*	-0*	-0*	4*	8*	11*	13*	27*
4.000	-34*	-82*	-34*	-15*	-6*	-3*	6*	9*	11*	14*	22*
5.000	11	35	23	15	10	5	-2	-6	-10	-14	-34*
6.000	-23*	-53*	-22*	-10*	-3*	-0*	3*	6*	9*	11*	17*
7.000	-22	25	18	13	8	4	0	-3	-6	-10	-22
8.000	-100*	-29*	-13*	-5*	-11*	-14*	5*	7*	6*	9*	19*
9.000	20	14	10	6	2	0	-4	-7	-11	-14	-22
10.000	-59*	-12*	-5*	-2*	-0*	-2*	3*	5*	6*	7*	12*
11.000	13	9	7	3	0	-2	-5	-8	-11	-12	-20
12.000	-3	2	0	-1	-3	-5	-8	-10	-13	-12	-23
13.000	1*	1*	1*	-2	-2*	-3*	4*	5*	6*	7*	10*
14.000	0	-1	-2	-3	-5	-7	-9	-12	-14	-17	-23
15.000	0	0*	0*	0*	1*	2*	3*	4*	5*	6*	7*
16.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
17.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
18.000	0	0	0	0	0*	1*	1*	1*	1*	1*	1*
19.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
20.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
21.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
22.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
23.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
24.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
25.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
26.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
27.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
28.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
29.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
30.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
31.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
32.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
33.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
34.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
35.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
36.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
37.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
38.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
39.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11
40.000	0	0	0	0	0*	0*	0*	0*	0*	0*	0*
41.000	-1	-2	-3	-4	-5	-6	-7	-8	-9	-10	-11

TABLE 20. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 3

RELATIVE RANGE SOLUTION TO LOCAL TEST LUNCH ERROR AT LN FCHS		V1		V2		V3		V4		V5		V6		
SL	UP	IN	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT	IN	OUT	
4,000	3	17	N	25	1,000	3,000	0,00	0,00	0,00	0,00	0,00	0,00	10,00	
4,000	-3	6	-9	25	1,000	-89	-123	-124	-125	-88	-70	-73	-60	-64
4,025	100	127	105	94	89	86	85	86	87	90	92	96	100	103
4,050	-43	-217	-140	-140	-140	-140	-140	-140	-140	-140	-140	-140	-140	-140
4,075	127	93	79	73	71	70	71	73	75	78	81	85	89	94
4,100	-55	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36
4,125	29	28	30	32	35	37	40	43	46	50	52	54	58	63
4,150	-42	-20	-17	-16	-15	-14	-14	-14	-13	-13	-13	-13	-14	-14
4,175	1	5	9	12	14	16	18	21	25	30	33	36	39	43
4,200	-6	-6	-7	-7	-8	-8	-8	-8	-7	-7	-7	-7	-7	-7
4,225	4	7	12	16	19	21	24	27	30	33	37	41	45	50
4,250	-1	-2	-2	-2	-2	-3	-3	-3	-3	-3	-3	-3	-3	-3
4,275	2	4	6	9	11	13	16	19	22	26	30	35	40	45
4,300	-1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,325	0	0	1	3	4	6	9	11	15	18	21	24	27	31
4,350	-2	0	0	0	0	1	1	1	1	1	1	1	1	1
4,375	-1	-2	-2	-1	0	2	5	7	11	14	16	19	21	24
4,400	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,425	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,450	-1	-1	-3	-3	-3	-3	-3	-3	-3	-3	-3	-3	-3	-3
4,475	2	4	6	9	11	13	16	19	22	26	30	35	40	45
4,500	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,525	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,550	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,575	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,600	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,625	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,650	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,675	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,700	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,725	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,750	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,775	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,800	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,825	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,850	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,875	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,900	1	1	1	1	1	1	1	1	1	1	1	1	1	1
4,925	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4,950	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
4,975	1	1	1	1	1	1	1	1	1	1	1	1	1	1
5,000	0	0	0	0	0	0	0	0	0	0	0	0	0	0

TABLE 21. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 4

MEASURED RANGE SOLUTION TO EQUATION FOR FCNS											
SL.	1'	10'	10"	N	DAY	UP	IN	22	V1	V2	V3
	4	5	6	-9	25	1,000	3,000	5	0,00	0,00	10,00
9+ 159	91	96	54	45	46	45	47	49	52	55	57
9+ 157+ 196+	97+	63+	45+	38+	33+	30+	28+	27+	26+	25+	24+
9+ 175+	53+	30+	22+	15+	15+	14+	14+	15+	15+	16+	17+
9+ 45	30	49	26	29	31	33	34	43	48	52	57
9+ 29	22	21	22	23	25	28	31	32	39	43	46
9+ 27+	22+	15+	11+	10+	9+	9+	9+	10+	10+	11+	11+
9+ 24	16	15	15	16	18	21	23	27	31	35	39
9+ 3	6	6	7	9	12	14	17	21	23	26	30
9+ 1	0	0	0	0	0	0	0	0	0	0	0
9+ 2	0	0	0	0	0	0	0	0	0	0	0
9+ 3	0	0	0	0	0	0	0	0	0	0	0
9+ 4	0	0	0	0	0	0	0	0	0	0	0
9+ 5	0	0	0	0	0	0	0	0	0	0	0
9+ 6	0	0	0	0	0	0	0	0	0	0	0
9+ 7	0	0	0	0	0	0	0	0	0	0	0
9+ 8	0	0	0	0	0	0	0	0	0	0	0
9+ 9	0	0	0	0	0	0	0	0	0	0	0
9+ 10	0	0	0	0	0	0	0	0	0	0	0
9+ 11	0	0	0	0	0	0	0	0	0	0	0
9+ 12	0	0	0	0	0	0	0	0	0	0	0
9+ 13	0	0	0	0	0	0	0	0	0	0	0
9+ 14	0	0	0	0	0	0	0	0	0	0	0
9+ 15	0	0	0	0	0	0	0	0	0	0	0
9+ 16	0	0	0	0	0	0	0	0	0	0	0
9+ 17	0	0	0	0	0	0	0	0	0	0	0
9+ 18	0	0	0	0	0	0	0	0	0	0	0
9+ 19	0	0	0	0	0	0	0	0	0	0	0
9+ 20	0	0	0	0	0	0	0	0	0	0	0
9+ 21	0	0	0	0	0	0	0	0	0	0	0
9+ 22	0	0	0	0	0	0	0	0	0	0	0
9+ 23	0	0	0	0	0	0	0	0	0	0	0
9+ 24	0	0	0	0	0	0	0	0	0	0	0
9+ 25	0	0	0	0	0	0	0	0	0	0	0
9+ 26	0	0	0	0	0	0	0	0	0	0	0
9+ 27	0	0	0	0	0	0	0	0	0	0	0
9+ 28	0	0	0	0	0	0	0	0	0	0	0
9+ 29	0	0	0	0	0	0	0	0	0	0	0
9+ 30	0	0	0	0	0	0	0	0	0	0	0
9+ 31	0	0	0	0	0	0	0	0	0	0	0
9+ 32	0	0	0	0	0	0	0	0	0	0	0
9+ 33	0	0	0	0	0	0	0	0	0	0	0
9+ 34	0	0	0	0	0	0	0	0	0	0	0
9+ 35	0	0	0	0	0	0	0	0	0	0	0
9+ 36	0	0	0	0	0	0	0	0	0	0	0
9+ 37	0	0	0	0	0	0	0	0	0	0	0
9+ 38	0	0	0	0	0	0	0	0	0	0	0
9+ 39	0	0	0	0	0	0	0	0	0	0	0
9+ 40	0	0	0	0	0	0	0	0	0	0	0
9+ 41	0	0	0	0	0	0	0	0	0	0	0

TABLE 22. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 5

RELATIVE RANGE	SOLUTION	RELATIVE DAY	TGT	LURE	ERORN	RFLN	ICNS	IN	V1	V2	V3	TE
SL	1*	2*	3*	4*	5*	6*	7*	8*	0.00	0.00	0.00	10.00
4.000	2	9	-4	25	1,000	3,000	5	0.00	0.00	0.00	0.00	0.00
5.000	5.000	5.000	5.000	5.000	5.000	5.000	5.000	5.000	0.00	0.00	0.00	0.00
6.000	102	110	76	59	49	42	35	32	11	30	31	30
7.000	49	49	42	35	32	31	30	31	32	34	35	37
8.000	166	89	62	48	40	35	31	29	27	26	27	29
9.000	5.000	200*	450*	560*	440*	290*	190*	130*	110*	110*	110*	110*
10.000	132	68	38	32	28	25	23	22	21	21	22	23
11.000	5.000	200*	316*	556*	326*	433*	333*	273*	173*	163*	143*	173*
12.000	92	49	36	29	45	22	20	18	17	16	19	20
13.000	5.000	193*	556*	326*	21*	15*	12*	9*	7*	6*	6*	6*
14.000	32	32	65	55	22	19	16	15	14	14	15	16
15.000	5.	24*	15*	11*	5*	6*	5*	4*	4*	4*	4*	4*
16.000	47	19	17	15	13	12	10	10	11	12	14	15
17.000	5.	11*	6*	5*	3*	3*	2*	2*	2*	2*	2*	2*
18.000	14	11	11	10	9	7	7	6	5	5	5	5
19.000	5.	1*	1*	1*	1*	0*	0*	0*	1*	1*	1*	1*
20.000	2	6	5	4	3	3	4	5	6	7	9	10
21.000	5.	1*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
22.000	1	1	0	0	0	0	1	2	3	5	6	8
23.000	5.	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
24.000	9	-3	-2	-1	0	0	2	3	4	5	6	7
25.000	5.	-1*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
26.000	1	1	0	0	0	0	1	2	3	5	6	8
27.000	5.	1*	1*	1*	1*	0*	0*	0*	1*	1*	1*	1*
28.000	2	5	6	5	4	3	3	4	5	6	7	8
29.000	5.	11*	9*	6*	5*	3*	3*	2*	2*	2*	2*	2*
30.000	5.	52	19	16	15	14	13	14	15	16	17	18
31.000	5.	24*	15*	11*	5*	6*	5*	4*	4*	4*	4*	4*
32.000	6	92	36	29	25	22	20	18	17	16	15	14
33.000	5.	rob*	c00*	45*	86*	25*	43*	33*	19*	16*	15*	14*
34.000	7	132	68	38	32	28	25	23	22	21	22	23
35.000	5.	111*	145*	86*	25*	43*	33*	19*	16*	15*	14*	14*
36.000	6	166	89	62	48	40	35	31	29	27	26	27
37.000	5.	49/	207*	122*	91*	59*	65*	37*	31*	26*	21*	19*
38.000	6	102	110	76	59	49	42	35	32	31	30	31

TABLE 23. X- AND Y-COMPONENT ERRORS DUE TO 3-MILLISECOND ERRORS IN ARRIVAL TIME AT MICROPHONES 2 AND 6

RELATIVE RANGE SOLUTION TO LEVEL TGT LUCN ERROR XFTH FCNS											
q, uv	1r	1d	M	N	Day	Up	3.00	5	0.0	V1	V2
									0.00	V3	TE
0.00	-61*	*211*	*121*	-151*	-151*	-38*	-27*	-19*	-13*	-8*	-2*
0.1	192	115	18	59	48	39	32	26	20	15	5
0.2	-326*	*150*	-86*	-37*	-30*	-26*	-20*	-14*	-9*	-5*	-2*
0.3	100	94	50	40	33	37	22	17	12	7	2
0.4	-621*	*211*	*100*	-40*	-28*	-26*	-14*	-9*	-6*	-3*	0*
0.5	144	72	31	40	33	27	22	17	13	9	4
0.6	-634*	*122*	-61*	-36*	-25*	-18*	-13*	-9*	-6*	-3*	-1*
0.7	98	52	38	31	26	21	17	13	9	5	1
0.8	-624*	*51*	-34*	-22*	-16*	-11*	-9*	-5*	-3*	-1*	-1*
0.9	20	34	27	23	20	16	13	9	5	2	-1
1.0	-63*	*25*	-16*	-12*	-8*	-6*	-4*	-2*	-1*	-1*	-1*
1.1	20	18	17	16	11	8	5	2	-1	-4	-4
1.2	-8*	*7*	*5*	*3*	-2*	-1*	0*	1*	1*	2*	2*
1.3	11	12	11	9	6	3	1	-1	-5	-11	-15
1.4	-1*	*1*	-1*	0*	0*	0*	0*	1*	1*	2*	3*
1.5	2	7	5	3	1	0	-3	-5	-8	-11	-15
1.6	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
1.7	1	1	1	0	-1	-2	-4	-7	-9	-12	-15
1.8	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
1.9	-2	-3	-4	-5	-6	-8	-10	-13	-16	-19	-23
2.0	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
2.1	-3	-5	-6	-7	-8	-10	-12	-14	-16	-18	-21
2.2	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
2.3	-1	-3	-6	-9	-11	-13	-16	-18	-21	-24	-27
2.4	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*	0*
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12.0	-142	-65	-6								

REFERENCES

1. Swingle, Donald M., Craig M. Crenshaw, and Raymond Bellucci, 1972, "Improved Sound Ranging Location of Enemy Artillery," Army Science Conference, US Military Academy, West Point, NJ.
2. Swingle, Donald M., and Raymond Bellucci, 1973, "Improved Sound Ranging Location of Enemy Artillery," R&D Technical Report ECOM-5486, US Army Electronics Command, Fort Monmouth, NJ.
3. Personal communications between Dr. Craig M. Crenshaw and Dr. Donald M. Swingle, June 1972-December 1973.
4. Crenshaw, Craig M., 1972, "Sound Ranging Calculations," AMC Chief Scientist Technical Note Number 1, US Army Materiel Command, Alexandria, VA.
5. Arnold, A., and R. Bellucci, 1957, "Variability of Ballistic Meteorological Parameters," Technical Memorandum M-1913, US Army Signal Engineering Laboratories, Fort Monmouth, NJ.
6. Lowenthal, Marvin J., and Raymond Bellucci, 1970, "Variability of Ballistic Winds, R&D Technical Report ECOM-3259, US Army Electronics Command, Fort Monmouth, NJ.
7. Fox, H. L., 1968, "Meteorological Techniques for Sound Ranging; Theory of Errors," Technical Report ECOM-0233-2, US Army Electronics Command, Fort Monmouth, NJ.
8. Lee, Robert P., 1972, "Artillery Sound Ranging Computer Simulations," R&D Technical Report ECOM-5441, US Army Electronics Command, White Sands Missile Range, NM.
9. Bellucci, Raymond, 1966, "Studies of Meteorological Techniques for Sound Ranging: Report II, Error Analysis," Technical Report ECOM-2703, US Army Electronics Command, Fort Monmouth, NJ.
10. Personal communications between Raymond Bellucci and Dr. Donald M. Swingle, June 1966-June 1972.

APPENDIX
THE WEIGHTED RANGE EQUATION SOLUTION

Given microphone positions $(x, y, z)_i$, arrival time t_i , target position (X, Y, Z) , shot time T , effective mean air velocity components $(u, v, w)_i$ and sound speed c_i , we can write the equation connecting these as follows:

$$\begin{aligned} & \left[(x - x_i) + u_i(t_i - T) \right]^2 + \left[(y - y_i) + v_i(t_i - T) \right]^2 \\ & + \left[(z - z_i) + w_i(t_i - T) \right]^2 - c_i^2(t_i - T)^2 = e_i . \end{aligned} \quad (A1)$$

With real data, there may be errors in our determination of any of the subscripted variables in the left-hand member, so that the e_i are generally nonzero. Expansion and rearrangement yield

$$R_i^2 - P_i^2 = e_i , \quad (A2)$$

where, denoting the effective speed of sound travel toward each microphone by s_i ,

$$R_i^2 = (X - x_i)^2 + (Y - y_i)^2 + (Z - z_i)^2 , \quad (A3)$$

$$P_i^2 = s_i^2(t_i - T)^2 , \quad (A4)$$

$$\begin{aligned} s_i^2 &= (c_i^2 - u_i^2 - v_i^2 - w_i^2) - \left[2/(t_i - T) \right] \\ &\times \left[u_i(X - x_i) + v_i(Y - y_i) + w_i(Z - z_i) \right] . \end{aligned} \quad (A5)$$

Thus defined, the weighted range equation solution seeks those values of the unknown target coordinates and shot time (X , Y , Z , T) for which

$$\sum_{i=1}^N w_i e_i^2 = \text{minimum} . \quad (A6)$$

For the purposes of this study, y_i , z_i , u_i , v_i , w_i , and Z are taken to be zero, all c_i are assumed equal to a single value (the speed of sound at an effective temperature of 10°C), and $x_{i+1} - x_i$ is assumed to be a constant, 1350 meters. Based on prior experimentation with real sound ranging data to determine the best exponent n , w_i is defined as follows:

$$w_i = R_i^n / \sqrt{\sum_{i=1}^N R_i^n} , \quad (A7)$$

$$n = -5 . \quad (A8)$$

The solution to (A6) is obtained by an iterative computation, using conventional least squares methods and treating the w_i as constants during each approximation.

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