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SCHUYLKILL RIVER BASIN
TUMBLING RUN, SCHUYLKILL COUNTY

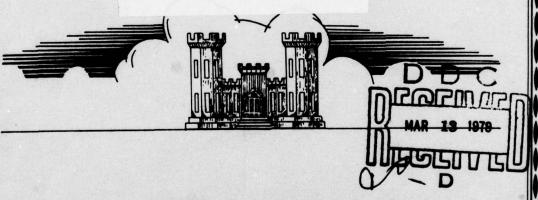
PENNSYLVANIA ID NO. PA.00688

LOWER TUMBLING BUN DAM

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM

Distribution Unlimited Approved for Public Release

Contract No. DACW31-78-C-0048



DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers Baltimore, Maryland 21203

AUGUST 1978

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SCHUYLKILL RIVER BASIN

LOWER TUMBLING RUN DAM SCHUYLKILL COUNTY, PENNSYLVANIA NATIONAL I.D. NO. PA 00688

National Dam Safety Program. Lower Tumbling Run Dam (National I.D. Number PA-00688), Schuylkill River Basin, Schuylkill County, Pennsylvania. Phase I Inspection Report.

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

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Prepared by:

WOODWARD-CLYDE CONSULTANTS 5120 Butler Pike

Plymouth Meeting, Pennsylvania 19462

Submitted to:

DEPARTMENT OF THE ARMY Baltimore District, Corps of Engineers Baltimore, Maryland 21203

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August 1978

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PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM

Name of Dam: Lower Tumbling Run Dam County Located: Schuylkill County

State Located: Pennsylvania Stream: Tumbling Run Creek

Coordinates: Latitude 40° 40.5' Longitude 76° 10.9'

Date of Inspection: 4 August 1978

Lower Tumbling Run Dam, is owned by the Schuyl-kill Haven Borough, and is used as a water supply structure for the town of Schuylkill Haven and surrounding areas. Limited records indicate that the dam was constructed in 1832 and was completed in 1833. The dam failed in 1850 as a result of overtopping and again in 1869, as a result of a leak through water supply pipes embedded in the embankment. The facility is judged to be in fair condition although the embankment slopes are considered to be steep. Furthermore, the condition of the outlet works is unknown.

Hydrologic and hydraulic calculations indicate that overtopping of the dam will occur at approximately 30% thirty percent of the probable maximum flood (PMF) of Therefore, the spillway is considered to be Seriously Inadequate.

The dam is classified as an Intermediate structure by virtue of its forty-nine foot height, It is classified as a High hazard dam consistent with a potential at failure for extensive property damage, and loss of life at the water treatment plant and further downstream at Mount Carbon, Pennsylvania.

A review of the records indicates that there is insufficient engineering and construction data to adequately evaluate the stability of the dam and condition of the outlet works. Specifically, there was no substantial data delineating the types of material used in the embankment nor were there sufficient details to determine foundation conditions. Furthermore, the outlet system could not be inspected.

The following recommended remedial work is considered critical and should be performed immediately.

- 1. The spillway system should be reconstructed to meet current hydrologic/hydraulic criteria.
- Prepare As-Built drawings in conjunction with a geotechnical investigation and stability analysis performed under the direction of a registered professional engineer. See Section 7 for details.
- 3. The outlet works sould be inspected and repaired as necessary.

The following items are considered important and should be performed as soon as practical.

- Clear underbrush from the abutments to facilitate visual inspections for seepage.
- Install seepage measuring devices. Monitor and record rates of flow and changes in turbidity.
- 3. Repair the riprap on the upstream slope.

A formal operation and maintenance procedure together with a warning procedure should be established and incorporated into the water treatment facilities operations manual. The warning procedure should include a method of warning downstream residents that high flows are to be expected. Evacuation procedures should also be developed.

The Owner should also develop an inspection checklist as an amendment to the maintenance procedure to insure that all items are inspected and maintained on a periodic basis. dohn H. Frederick, Jr., P.E.
Maryland Registration 7301
Woodward-Clyde Consultants

9/23/78 Date

WS bardner

William S. Gardner, P.E. Pennsylvania Registration 4302E Woodward-Clyde Consultants 9/22/78 Date

APPROVED BY:

G. WITHERS

Colonel, Corps of Engineers

District Engineer

Under the recently revised spillway evaluation guidelines, this dam is considered unsafe, non-emergency.



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OVERVIEW LOWER TUMBLING RUN, SCHUYLKILL COUNTY, PENNSYLVANIA

PHASE I INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM LOWER TUMBLING RUN DAM NATIONAL ID #PA 00688 DER ID #54-24

SECTION I PROJECT INFORMATION

1.1 General.

- a. <u>Authority</u>. The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. Purpose. The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 Description of Project.

a. Dam and Appurtenances. Lower Tumbling Run Dam is a 49 foot high earth dam across Tumbling Run Creek. The structure is 430 feet long with a 10 foot wide crest that impounds a 25.7 acre reservoir. The upstream slope from the crest to the waterline was observed to be approximately 0.5H:1V. The downstream slope measures approximately 1.5H:1V.

The outlet works consist of three 12-inch 1.D. cast iron pipes which extend through the dam. The pipes are located approximately 42 feet below the dam crest. Two of the pipes carry water directly into the water treatment plant located immediately downstream of the dam. The third pipe extends downstream and can be used to drain the reservoir. The water supply intake structure is located within the upstream embankment and contains a 20-foot high semi-circular masonry approach channel wall. An access bridge has been constructed from the dam to a riser structure which houses the valves controlling the discharge of the three pipes. A plan and profile of the outlet works is presented in Appendix E as Plate 3. A sketch of the intake structure is presented in this report as Plate 5. This data was obtained from the Owner's representative.

Excess water is stored in the reservoir to elevation 646.5 and thereafter is discharged over the spillway. This spillway is located at the left abutment of the dam, and it is 55 feet long.

b. <u>Location</u>. The dam is located on Tumbling Run Creek in North Manheim Township, Schuylkill County, Pennsylvania. The embankment is located 2,600 feet downstream of Upper Tumbling Run Dam. The dam site and reservoir are

shown on USGS Quandrangle entitled, "Pottsville, Pennsylvania", at coordinates N 40° 40.5' W 76° 10.9'. A Regional Location Plan is enclosed as Plate 1, Appendix E.

- e. Size Classification. The dam is classified as "Intermediate" by virtue of its 49-foot height.
- d. <u>Hazard Classification</u>. A "High" hazard classification is assigned consistent with the potential for extensive property damage and loss of life downstream at the water treatment plant and in the town of Mount Carbon, Pennsylvania.
- e. Ownership. The dam is owned by the Schuylkill Haven Borough located at 39 Dock Street, Schuylkill Haven, Pennsylvania.
- f. Purpose of Dam. The dam was initially constructed to augment water supply for the Schuylkill Navigation Company canal, but has been used since 1908 for water supply.
- g. Design and Construction History. Records concerning the design and construction of the dam could not be found and are no longer believed to exist. Limited post-construction documents report that the dam was constructed in 1832 for the Schuylkill Navigation Company. Records indicate that the construction began under the direction of Mr. George Duncan, but was completed in 1833 by an unknown contractor.

The dam failed in 1850. There was considerable damage and the reported loss of one life. The failure is reported to have been caused by a temporary weir constructed across the spillway weir in an attempt to store additional water. However, as a result of the dam being overtopped, a significant portion of the embankment was washed out. The dam was rebuilt in the same year by Colonel Knoderer.

Before 1869, the water supply pipes were always under full hydrostatic head. These pipes apparently cracked and the resulting leakage was large enough to cause piping and eventual embankment failure in 1869. As shown on Plate 4, the top of the dam dropped 10 feet. The pipes were repaired, encased in concrete for part of their length, and the valves moved to the upstream end of the pipes.

In 1909, the control valves were replaced, vertical riser pipes were added to the intakes, and an excavation was made in the embankment to investigate possible seepage along the outlet pipes. No evidence of seepage was found. The material excavated from the embankment was reported to be a mixture of yellow clay and gravel.

A tile drain system was installed in about 1961 and is located at the toe of the dam. Portions of the drain can be seen near the left abutment.

h. Normal Operating Procedures. Water is normally discharged through pipes extending through the dam into the water supply treatment facilities located

immediately downstream of the dam. The quantity discharged is dependent upon water supply demand. Excess water is discharged over the spillway into Tumbling Run Creek.

1.3 Pertinent Data.

A summary of pertinent data for Lower Tumbling Run Dam is presented as follows:

1.	Drainage Area (sq. miles)	6.0
2.	Discharge at Dam Site (cfs) Spillway Outlet Works	2,200 Not determined.
3.	Elevations (feet above MSL) ⁽¹⁾ Top of Dam Spillway Max. Pool of Record	653.0 646.5 651.3
4.	Reservoir (miles) Length at Normal Pool Fetch at Normal Pool	0.5 0.5
5.	Storage (acre-feet) Normal Pool Top of Dam	531 698
6.	Reservoir Surface (acres) Normal Pool	25.7
7.	Dam Data Type Length Maximum Height Top Width	Rolled earth with riprap covering the upper portion of upstream slope and completely covering downstream slope. 430 feet 49 feet 10 feet
	Side Slopes (approximate) Upstream Exposed Riprapped Portion Below Water Level Downstream	1.3H:1V, measured. Unknown 1.6H:1V, measured.

8. Spillway Type

Length (1)

Broad crested concrete and rock weir. 55 feet 646.5

(1) Estimated from USGS Mapping and available drawings.

SECTION 2 ENGINEERING DATA

2.1 Design.

- a. <u>Data Available</u>. A summary of engineering data is presented on the checklist attached as Appendix A. Principal documents containing data used for this report are as follows.
 - 1. "Report Upon the Investigation of the Philadelphia & Reading Coal & Iron Company Dams On Tumbling Run, Schuylkill County, Pennsylvania", by the Water Supply Commission of Pennsylvania, dated December 22, 1913.
 - 2. "Report Upon the Tumbling Run Supply of the Silver Creek Water Company", by the Water Supply Commission of Pennsylvania, dated November 12, 1920.
 - 3. Letter to Water and Power Resources Board, Department of Forests and Waters, Harrisburg, Pennsylvania, from the Silver Creek Water Company, by Mr. H. W. Weber, dated April 9, 1935.
 - 4. "Investigation of Tumbling Run Dams, W.O. 6338-00", by Gilbert Associ-ates, Inc., Reading, Pennsylvania, dated March 1, 1967.
 - 5. Miscellaneous letters, correspondence, memos, drawings and inspection reports located in the Department of Environmental Resources (DER) main office in Harrisburg, Pennsylvania.

The data consisted of post-construction reports and investigations of the dam. Documents regarding the design and construction could not be found and are no longer believed to exist.

b. Design Features. The principal design features are illustrated on the plan and cross-section plates enclosed in Appendix E as Plates 2 and 3. These plates were reproduced from drawings located in the DER files. A brief description of the design features is also presented in Section 1.2, "Description of Project".

The dam is an earth embankment with riprap on the downstream slope and the upper 15 feet of the upstream slope. There are various reports of the upstream and downstream slope inclinations. A summary of the reported slope inclinations is included in Table 1.

TABLE I SUMMARY OF REPORTED SLOPE INCLINATIONS

Upstream Slope	
Crest of dam to bottom of riprap	
Water Supply Commission, 1913	0.5H:1V
Silver Creek Water Company, 1935	IH:IV
Below riprap	
Cross Section of Embankment, 1869,	
Plate 4	2.25H: IV
Plan Showing Valves and Outlet, 1908,	
Plate 3	2.6H: IV
Water Supply Commission, 1913	2.6H: IV
Silver Creek Water Company, 1935	2.6H: IV
Gilbert Associates, Inc., 1967	2.25H: IV
Downstream Slope	
Cross Section of Embankment 1869	

Cross Section of Embankment, 1869,
Plate 4
Plan Showing Valves and Outlet, 1908,
Plate 3
Water Supply Commission, 1913
Silver Creek Water Company, 1935
Gilbert Associates, Inc., 1967
Visual Inspection, 1978
L625H:1V
1.5H:1V

Field measurements made during the visual inspection performed for this report indicate a downstream slope of 1.5H:1V and an upstream slope above the water level of 1.3H:1V, slope of grouted riprap. The crest of the dam was measured to be 430 feet long with a 10 foot wide crest. Seepage control is apparently minimal and consists of reported tile toe drains at the base of the dam.

2.2 Construction.

The earliest report of the construction history is documented in a Water Supply Commissions report dated December 22, 1913. This report states that the construction was performed for the Schuylkill Navigation Company. Construction began in 1832 by Mr. George Duncan, but was completed in 1833 by an unknown constructor. Materials used are reported to have been decomposed shale. Information about soil properties and construction techniques were not included in the files. All other records describing post-construction changes and investigations are described in Section 6.

2.3 Operation Data.

The only records currently being maintained are those related to the water supply treatment facilities. Discharge from the treatment facilities are recorded, but flows over the spillway are not.

2.4 Evaluation.

- a. Availability. All information presented herein was extracted from records located in the Department of Environmental Resources files in Harrisburg, Pennsylvania or from conversations with the Owner's representative. Design and construction data could not be located.
- b. Adequacy. The available data included in the State files and presented in this report are not adequate to evaluate the engineering aspects of the dam.
- c. <u>Validity</u>. There are several discrepancies in the post-construction reports which require verification. A significant amount of required data is nonexistent and must be determined to evaluate this dam.

SECTION 3 VISUAL INSPECTION

3.1 Findings.

- a. General. The observations and comments of the field inspection team are contained in the checklist enclosed herein as Appendix B and are summarized and evaluated as follows. In general, the appearance of the facility indicates that the dam is currently in good condition.
- b. <u>Dam.</u> During the visual survey, there were no indications or evidence of distortions in alignment. Minor grade differences were noted along the dam crest as the result of settlement. There were no surface cracks or sloughing observed. The upstream and downstream riprap was in good condition and stable. The upstream riprap has been grouted with pneumatically placed mortar. Some erosion was noted on the upstream slope below the riprap protection.

A slight quantity of seepage was observed through the valve chamber located at the downstream toe on the right side of the dam. Seepage was also noted through an observation well at the toe near the left abutment. This flow is probably the seepage through the French (tile) drain system reported by Gilbert Associates, Inc., in 1967. Location of the observed seepage is shown on Sheet 5a, Appendix B.

c. Appurtenant Structures.

1. Outlet Works. The intake structure and cast iron pipes were submerged during the visual inspection and could not be inspected. The access bridge to the intake valves consists of a steel frame structure with wood planking. The concrete supports of the bridge were noted to have a number of cracks, but appeared to be stable. It was reported by Mr. Charles Feindler, Borough Manager, that the intakes for the vertical riser pipes are approximately 7, 14 and 22 feet above the base of the intake structure. They are connected to three 12-inch diameter cast iron pipes. See Plate 5 for details.

A masonry arch valve chamber is located at the toe of the downstream slope. There are valves on each of the three pipes, but they are no longer used and are submerged. A small quantity of clear water was noted flowing from this area, which may be seepage and/or leakage from these valves. The two outer pipes are connected to the treatment plant and are currently used for water supply. The third pipe (center) discharges approximately 100 feet downstream through a valve. Leakage was observed at this valve.

2. Spillway. The spillway has been excavated into rock at the left abutment and was observed to be in good condition. The right side of the channel adjacent to the dam consists of a concrete retaining wall, which changes to a masonry wall beyond the dam. The left side of the channel has been excavated into

rock. Some rock spalling and broken rock was observed in the spillway. The spillway bottom is very irregular (See Photographs 6 and 7). Brush and some woody vegetation was noted to be growing in the spillway, but does not currently constitute an obstruction to flow.

- d. Reservoir. Reconnaissance of the reservoir disclosed no evidence of significant siltation, slope instability, or other features that would significantly affect the storage capacity of the reservoir. The reservoir side slopes are steep, well vegetated and stable.
- e. <u>Downstream Channel</u>. Flows from the spillway are directed into a 15 foot wide man-made channel. Portions of the channel are lined with hand-placed rock. Flows from the vicinity of the valve house are channeled into a narrow stream bed, and directed into a catch basin. Thereafter, the flow merges with the spillway channel. See Section 5 for more details of the downstream channel.

3.2 Evaluation.

In summary, the visual survey of the dam disclosed no evidence of existing instability of the dam. However, the steepness of the downstream slope and seepage, along with the age and leakage of the outlet works, are considered items of concern. Therefore, additional investigation and evaluation is recommended as described in Section 7.

SECTION 4 OPERATION PROCEDURES

4.1 Procedures.

Water is drawn from the reservoir on demand into the water treatment plant via two 12-inch pipes. Excess water discharges over the emergency spillway at elevation 646.5. The only records maintained are water supply discharges through the treatment facilities.

4.2 Maintenance of the Dam.

The dam is maintained by the Schuylkill Haven Borough and is periodically checked by the Department of Environmental Resources. There is no operational manual other than the operating procedures for the water treatment facility. Very little maintenance was performed in recent years. The upstream riprap was grouted in the early 1960's.

4.3 Maintenance of Operating Facilities.

Maintenance of the appurtenances is performed by the Schuylkill Haven Borough. However, valves outside of the treatment facility are not readily accessible and have received little maintenance over the years. The pipes downstream of the dam toe are being replaced as well as expansion of the treatment facilities. Woody vegetation is periodically removed from the spillway.

4.4 Warning Systems in Effect.

There are no formal warning systems or procedures established to be followed during periods of exceedingly heavy rainfall. The dam is checked almost daily for unusual conditions. It is understood that responsible people are always in the area and available if a potentially hazardous condition develops. In the event of an emergency, the local Civil Defense Authority would be notified. The Borough Manager stated that the city representatives are stationed at the dam during periods of heavy rainfall.

4.5 Evaluation.

No written operating procedures exist, but should be developed and integrated with the procedures of the treatment facilities. Maintenance procedures should be developed and incorporated into the operating procedures of the treatment facilities, and include a checklist of items to be observed during inspection of the dam and outlet works.

Since a formal warning procedure does not exist, a formal procedure should be developed and implemented during periods of extreme rainfall. This procedure should consist of a detailed method for notifying personnel working in the treatment plant and residents downstream.

SECTION 5 HYDROLOGY/HYDRAULICS

5.1 Evaluation of Features.

a. Design/Evaluation Data. There was no original design data available. Two inspection reports, one by C. E. Ryder of The Water Supply Commission of Pennsylvania, dated 22 December 1913, and one by H. T. Newton of Gilbert Associates, Inc., dated 1 March 1967, were in the State files. All other data was obtained from these reports, and from several drawings, many untitled and undated, supplemented with field observations. Upper Tumbling Run Dam is also the subject of inspection under the National Dam Inspection Program, and the results of the hydrologic/hydraulic analysis are incorporated in this section.

The watershed is small, approximately 6.0 square miles, and roughly rectangular, lying between parallel ridges 0.9 to 1.0 miles apart. The upper end is about 6.5 miles above the dam, at an elevation near 1,100 feet. The normal reservoir pool is at approximately elevation 646.5. The ridges run from elevation 1,200 to 1,400. The watershed is primarily owned by the Schuylkill Haven Borough. It is steep, rocky and densely wooded.

The earth fill dam extends across the valley and has a crest elevation of approximately 653.0 feet. Since there were no surveys since 1929, the datum relative to MSL could not be determined. Therefore, all elevations were estimated from USGS mapping.

The operating outlet works consist of three 12-inch pipes, valved at the upper end, passing under the dam into the water treatment plant at the downstream toe. Their flows are hydrologically insignificant.

The spillway is an irregular channel cut through rock in the left abutment. A broad crested concrete control sill extends across all but about 10 feet of the crest. The crest length is 55 feet at an elevation of approximately 646.5. Below the crest, the rough rock channel slopes 6 to 8 percent and narrows, but not enough to impede flow over the crest. The spillway is capable of discharging approximately 2,200 cfs with the water level at the top of the dam (See Appendix C).

Upper Tumbling Run Dam is located 1/2 mile above Lower Tumbling Run Dam. Of the 6 square miles of watershed, 5.5 square miles contribute first to Upper Tumbling Run Dam, with only 0.5 square miles contributing directly to Lower Tumbling Run Reservoir. Consequently, the principal flood inflow is the discharge from the upper reservoir.

In accordance with the criteria established by the Federal (OCE) Guidelines, the recommended spillway design flood for this "Intermediate" size dam with a "High" hazard potential is the probable maximum flood (PMF).

- b. Experience Data. According to the Owner's representative, the worst flood of record occurred during Tropical Storm Agnes, on June 22 and 23, 1972. This rainfall produced a maximum water elevation in Lower Tumbling Run Reservoir of 651.3. This corresponds to 4.8 feet of flow over the spillway.
- c. <u>Visual Observations</u>. On the date of inspection, no conditions were observed to indicate reduction of spillway capacity during maximum discharge. Observations regarding the downstream channel, spillway conditions, and reservoir are located in Appendix B.
- d. Overtopping Potential. Maximum outflow without failure from Upper Tumbling Run is approximately 2,200 cfs (Sheet 5, Appendix C). This corresponds to an inflow into the upper dam of 30 percent of PMF (Sheet 9, Appendix C).

The spillway of this dam, while rated the same as the upper one, is both wider (55 feet as opposed to 52 feet) and a little deeper (6.5 feet below crest as opposed to 6.2 feet), and it is judged capable of handling the added local inflow from the 30 percent PMF without overtopping.

Inflows exceeding 30 percent of the PMF, however, will result in overtopping and failure of Upper Tumbling Run Dam (see Sheet 6, Appendix C).

- e. <u>Spillway Adequacy</u>. The spillway system is judged "Seriously Inadequate" as all of the following conditions exist (Engineering Technical Letter No. 1110-2-234, 10 May 1978):
 - "I. There is high hazard to loss of life from large flows downstream of the dam.
 - "2. Dam failure resulting from overtopping would significantly increase the hazard to loss of life downstream from the dam from that which would exist just before overtopping failure.
 - "3. The dam and spillway are not capable of passing one-half of the probable maximum flood without overtopping failure."

Item I is covered in the following subsection and item 3 is covered above. Overtopping of Upper Tumbling Run Dam would result in its failure, which would inevitably lead to the failure of Lower Tumbling Run Dam, 1/2 mile downstream. Failure of Lower Tumbling Run Dam will either cause the downstream railroad embankment to fail or massively overtop, increasing the damage downstream over what would occur from the maximum spillway discharge. Therefore, the spillway is "Seriously Inadequate".

f. <u>Downstream Conditions</u>. About 1,200 feet below Lower Tumbling Run Dam, the valley is blocked by an abandoned multi-track railroad earth embankment, and a multi-lane highway at a lower level on the downstream side. Tumbling Run,

below the dams, passes under the combined railroad and highway embankment through a culvert. The culvert is approximately 10 by 18 feet at its smallest section. The embankment is estimated to be 35 to 40 feet above the invert of the culvert on the upstream side. The creek joins the Schuylkill River in the town of Mount Carbon, Pennsylvania just below the tunnel outlet.

The capacity of the culvert, with 25 feet of water backed up behind the embankment, is about 5,800 cfs (Sheet 8, Appendix C). Storage behind the embankment appears to be about a quarter of the capacity of either dam. Consequently, while the culvert would most likely pass a PMF outflow through larger spillways, it would clearly massively overtop in a failure, which is likely with any inflow over 30 percent of PMF.

There are three buildings between Lower Tumbling Run Dam and the embankment that are possibly subject to damage in the event of large flows from the dam. These buildings would be destroyed, with possible loss of life, in the event of dam failure. In the event of dam failure and embankment failure, there are also several industrial buildings and houses in Mount Carbon and along the Schuylkill River which would be damaged or destroyed, justifying the "High" hazard classification.

SECTION 6 STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability.

- a. <u>Visual Observations</u>. The visual observations did not indicate any existing embankment stability problems. However, the downstream slope and observed portion of the upstream slope are unusually steep. Some slight erosion was noted upstream at the base of the riprap zone. Seepage was observed in the French drain system and valve leakage or embankment seepage was observed through the valve chamber. The seepage was clear and there were no indications of piping. The spillway was in good condition with stable channel sides, although some channel and wall spalling was noted. Woody vegetation was also noted.
- b. Design and Construction Data. No design or construction data is known to exist. All data concerning physical features of the dam have been determined by post-construction investigations, and judged to be inadequate for a detailed evaluation of the dam.
- c. Operating Procedures. The only procedures established have been for the operation of the water treatment facility.
- d. Post-Construction Changes. Major repairs to this dam were required in 1850 and 1869 as the result of failures, as described in Section 1. Normal maintenance and valve replacement was done in 1906. The dam was the subject of investigation by the State in 1913 and 1920. In 1913 the reservoir was emptied in order to inspect the outlet pipes, which were found to be in good condition. No repairs or alterations were recommended in either report. In 1967 Gilbert Associates, Inc., was hired to investigate both Upper and Lower Tumbling Run Dams. No repairs or modifications were recommended for Lower Tumbling Run (although further investigation was recommended for Upper Tumbling Run Dam).

Currently, the water treatment facility is being renovated and expanded. This work has been designed by Gilbert Associates, Inc.

e. Seismic Stability. This dam is located in Seismic Zone 1. Normally, it can be considered that if a dam in this zone is stable under static loading conditions, it can be assumed safe for any expected earthquake conditions. Since the static factor of safety for this dam is unknown, a seismic stability evaluation could not be made. Considering the steepness of the existing slopes, it is concluded that safety factors under both static and seismic loading should be evaluated.

SECTION 7 ASSESSMENT/REMEDIAL MEASURES

7.1 Dam Assessment.

a. Evaluation. The visual inspection indicates the dam is generally in fair condition. There is no engineering or construction data other than information obtained from post-construction investigations. The downstream slope is steep and would not meet current standards of practice. The outlet works are 109 years old and may be near the end of their service life. The spillway capacity is judged to be "Seriously Inadequate" using the Corps of Engineers criteria. A relatively small amount of seepage has been occurring over a significant period of time, and although it has not caused any problems since the failure of 1869, the flow should be monitored for changes in flow rates and turbidity.

Upper Tumbling Run Dam was also inspected under the National Dam Inspection Program. Results of that investigation indicate the spillway to be "Seriously Inadequate". The dam would fail in the event of overtopping, which is estimated to occur at approximately 30 percent PMF.

- b. Adequacy of Information. Insufficient engineering and construction data was found to adequately evaluate the stability of the dam and service life of the outlet works. Specifically, there is no substantial data delineating the types of materials and configuration of the embankment. Foundation preparation details are also unknown. Details of the outlet works were available only from photographs.
- c. Urgency. It is concluded that the recommendations considered to be critical in Section 7.2 be implemented immediately. All other items should be implemented as soon as practical.

7.2 Remedial Measures.

- a. <u>Facilities</u>. The following recommended remedial work is critical and should be performed immediately.
 - 1. The spillway system should be reconstructed to meet current hydrologic/hydraulic criteria.
 - 2. Prepare "As-Built" drawings in conjunction with a geotechnical investigation and stability analyses. Piezometers should be installed in the embankment to measure the phreatic surface.
 - 3. The outlet works should be inspected and repaired, if necessary.

The following items are considered important and should be performed as soon as practical.

- 1. Clear underbrush from abutments to facilitate visual observations for seepage.
- 2. Install seepage measuring devices/structures, and monitor and record rates of flow.
- 3. Repair the riprap on the upstream slope.
- b. Operation and Maintenance Procedures. Formal operations, maintenance, and warning procedures should be developed and incorporated into the water treatment facility's operation. The warning procedure should include a method of warning downstream residents that high flows are to be expected. Evacuation procedures should also be developed.

The Owner should also develop an inspection checklist as an amendment to the maintenance procedure to insure that all critical items are inspected and maintained on a periodic basis.

APPENDIX

DESIGN, CONSTRUCTION, OPERATION ENGINEERING DATA CHECK LIST PHASE I

NAME OF DAM Trumbling Run Dam Lower

00688

REMARKS

Sheet 1 of 4

AS-BUILT DRAWINGS

None. One drawing was made following the failure of 1869 and consisted of an embankment profile along with the outlet works. A plan and profile drawing prepared in 1908 was found in the files along with several plans of the reservoir but may not be As-Built plans.

REGIONAL VICINITY MAP

Unmarked plans of Lower and Upper Tumbling Run Reservoirs.

CONSTRUCTION HISTORY

Post-construction investigations included limited construction history which is presented in the text of this report.

TYPICAL SECTIONS OF DAM

"Cross-Section of Embankment", July 19, 1869. Plan Showing Valves and Outlet, dated August, 1908.

OUTLETS - PLAW

DETAILS

Limited and conflicting data included on drawings; "Cross-Section of Embankment", July 19, 1869. Plan Showing Valves and Outlet, August, 1908.

CONSTRAINTS

DISCHARGE RATINGS

None

RAINFALL/RESERVOIR RECORDS

None

Sheet 2 of 4 REMARKS None DESIGN REPORTS

ITEM

GEOLOGY REPORTS

None

DESIGN COMPUTATIONS
HYDROLOGY & HYDRAULICS
DAM STABILITY
SEEPAGE STUDIES

None found. Summaries presented in post-constrution investigations. None found. None found.

MATERIALS INVESTIGATIONS
BORING RECORDS
LABORATORY
FIELD

None found.

POST-CONSTRUCTION SURVEYS OF DAM

"Cross-Section of Embankment", July 19, 1869.

BORROW SOURCES

Unknown

Sheet 3 of 4

REMARKS

MONITORING SYSTEMS

TEM

None

MODIFICATIONS

Section containing outlet works Dam essentially rebuilt following failure in 1850. Section containing outlet we rehabilitated after failure in 1869. New valves installed at intake of 12 inch I.D. pipes, 1909. Riser pipes added, unknown date.

HIGH POOL RECORDS None

POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS

The following post-construction studies are known to have been made and included in the DER files:

"Report Upon the Investigation of the Philadelphia & Reading Coal & Iron Company Dams on Tumbling Run, Schuylkill County, Pennsylvania", by the Water Supply Commission of Pennsylvania, dated December 22, 1913, and supplementary reports of 1914.----(Continued on Sheet 4 of 4).

PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS

Yes, two failures have occurred. Included in post-construction reports. No specific reports.

> MAINTENANCE OPERATION RECORDS

None

Sheet 4 of 4

REMARKS None None **SECTIONS** SPILLWAY PLAN ITEM

DETAILS

OPERATING EQUIPMENT PLANS & DETAILS

"Plan Showing Valves and Outlet", August, 1908.

POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS--CONTINUED FROM SHEET 3 of 4

"Report Upon the Tumbling Run Supply of the Silver Creek Water Company", by the Water Commission of Pennsylvania, dated November 12, 1920.

Letters to Water and Power Resources Board, Department of Forest and Waters, Harrisburg, Pennsylvania from the Silver Creek Water Company by Mr. H.W. Weber, dated April 9, 1935. "Investigation of Tumbling Run Dams, W.O. 6338-00", by Gilbert Associates, Inc., Reading, Pennsylvania. 3

O PPENDIX CHECK LIST VISUAL INSPECTION PHASE I

Sheet 1 of 11

3	Z	Lower	ame Dam Lower Tumbling Dam	County	County Schuylkill	State Pennsylvania ID # PA 00688	National ID #	PA	00688
8	of	ype of Dam	Rolled Earth	1	Hazard Category I (High)	I (High)			
ate	3	ate(s) Inspection	n 4 Aug. 1928	Weather Rain	Cloudy Ten	4 Aug. 1928 Weather Rain, Cloudy Temperature 70's	1		

M.S.L. Tailwater at Time of Inspection None Pool Elevation at Time of Inspection 644.3 M.S.L.

John H. Fredrick, Jr. (Geotechnical) (1 Aug. 1978) John Boschuk, Jr. nical/Civil) Vince McKeever (Hydrologist) Ralph H. Cross (Hydrologist) John Boschuk, Jr. Brady Bisson (Geotechnical) Inspection Personnel:

Recorder

Remarks:

Mr. Dick Nagle, Chief Operator and Mr. Kenny Frehafer, Borough Manager were onsite and provided information during the inspection.

CONCRETE/MASONRY DAMS

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 2 of 11 REMARKS OR RECOMMENDATIONS
ANY NOTICEABLE SEEPAGE	N/A	
STRUCTURE TO ABUTHENT/EMBANCHENT JUNCTIONS	N/A	
DRAINS	N/A	
WATER PASSAGES	N/A	
FOUNDATION	N/A	

CONCRETE/MASONRY DAMS

0

VISUAL EXAMINATION OF	OBSERVATIONS	Sheet 3 of 11 REMARKS OR RECOMMENDATIONS
SURFACE CIRCLES		
CONCRETE SURFACES "V"		

VERTICAL AND HORIZONTAL N/A ALIGNMENT

STRUCTURAL CRACKING N/A

MONOLITH JOINTS N/A

CONSTRUCTION JOINTS N/A

EMBANKMENT

Sheet 4 of 11

0

VISUAL EXAMINATION OF

SURFACE CRACKS None observed.

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE

None observed.

SLOUGHING OR EROSION OF EMBANIMENT AND ABUTMENT SLOPES

Some slight slope discontinuities were observed on the downstream slope but were assessed to be associated with adjustment of the riprap protection and not slope failure.

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST

The vertical and horizontal alignment is good with no misalignments observed.

The crest was noted to be slightly irregular as a result of settlements.

RIPRAP FAILURES

None observed but some slight slope adjustments were observed. The upstream riprap was covered with grout. Wave action is washing out soil and/or rock along sections at the base of the rock. See Photograph No. 9.

EMBANKMENT

Sheet 5 of 11

VISUAL EXAMINATION OF

OBSERVATIONS

REMARKS OR RECOMMENDATIONS

JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLMAY AND DAM

. All junctions were in good condition.

ANY NOTICEABLE SEEPAGE

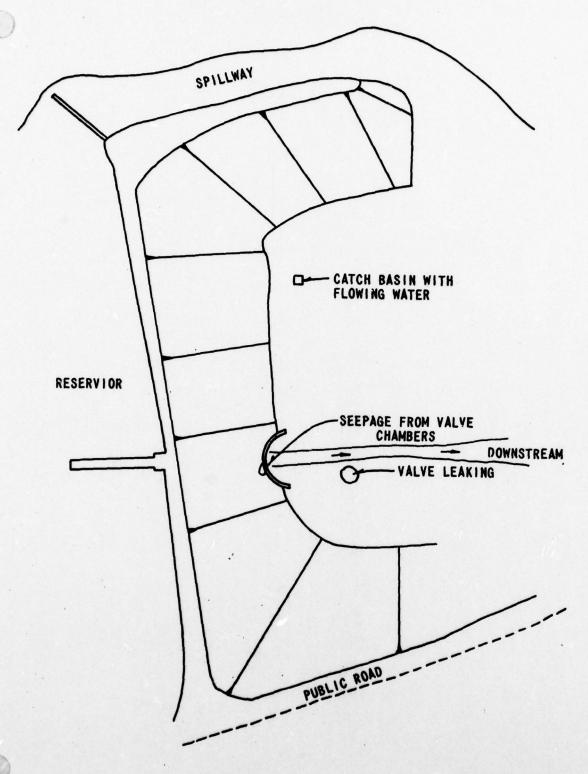
Yes. See sheet 5a of 11 for details. A slight amount of seepage was noted at the valve chamber. A catch basin was also observed near the downstream toe which contained water and appears to be connected to a french drain system.

STAFF GAGE AND RECORDER

None

DRAINS

Yes. The french drain below the dam toe is presently covered and serves as a parking area but there are two existing brick access boxes, catchbasins, where the seepage can be observed. The flow was clear.



SEEPAGE LOCATION PLAN LOWER TUMBLING RUN DAM SHEET 5a OF 11

OUTLET WORKS

	Sheet 6 of 11
VISUAL EXAMINATION OF	OBSEAVATIONS REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	Cast iron pipes lead from the upstream toe through the embankment and are underground below the downstream toe. These pipes could not be inspected.
ACCESS BRIDGE SUPPORT	The portions of the concrete bridge supports the water surface were observed to contain a number of cracks and should be replaced. See Photo. No. 10
IMTAKE STRUCTURE	
OUTLET STRUCTURE	N/A
OUTLET CHANNEL	None

Pond drain valve was closed at three locations along the line. It was not exercised. Leakage was noted at the downstream outlet

value.

EMERGENCY GATE

UNGATED SPILLMAY

Sheet 7 of 11

VISUAL EXAMINATION	I OF OBSERVATIONS	REMARKS	REMARKS OR RECOMMENDATIONS
ONCRETE WEIR	The broad crested concrete weir was poured directly onto the rock foundation and is in generally good condition. See Photograph 5.	the rock 5.	founda-

The approach channel is cut through natural material as shown on Photograph 4. It is stable and in generally good condition. APPROACH CHANNEL

The channel is cut into natural rock and is extremely rough as can be seen on Photographs 6 and 7. DISCHARGE CHA:WEL

BRIDGE AND PIERS

None

GATED SPILLWAY

0

		Sheet 8 of 11
VISUAL EXAMINATION OF	F OBSERVATIONS	IS RECOMMENDATIONS
CONCRETE SILL	None	
APPROACH CHAMNEL	None	
DISCHARGE CHANNEL	None	
BRIDGE AND PIERS	None	
GATES AND OPERATION EQUIPMENT	None	

INSTRUMENTATION

VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None	
OBSERVATION WELLS	None	
METRS	None	
PIEZOMETERS	None	

None

OTHER

RESERVOIR

VISUAL EXAMINATION OF

OBSERVATIONS

Sheet 10 of 11 REMARKS OR RECOMMENDATIONS

SLOPES ROS

Reservoir slopes are steep, densely vegetated and stable.

SEDIMENTATION

As reported by the Chief Operator and Borough Manager, there is no significant sedimentation in the reservoir. An inspection around the reservoir edge did not disclose significant accumulation of sediment.

DOWNSTREAM CHANNEL

Sheet 11 of 11

Mount Carbon, Pennsylvania. In the event of dam failure the flood wave would be attenuated by the embankment and the tunnel would control flow. See Photograph 13. This tunnel could be clogged by debris from the woods. The tunnel is 18 feet wide, 18 feet high with a nine foot radius roof passing beneath a four track railroad and multilame highway fill. It is conservatively assumed the railroad/highway embankment would fail if the dam failed. The downstream channel is rocky and passes through dense woods to a tunnel approximately 1200 feet downstream. Beyond the tunnel the stream passes into the town of REMARKS OR RECOMMENDATIONS **OBSERVATIONS** VISUAL EXAMINATION OF (OBSTRUCTIONS, DEBRIS, ETC.) CONDITION

SLOPES

Side slopes are steep, well vegetated and stable.

APPROXIMATE NO. OF HOMES AND POPULATION

There are no homes along the channel until the stream passes through Mount Carbon, Pennsylvania. APPENDIX C

LOWER TUMBLING RUN DAM CHECK LIST HYDROLOGIC AND HYDRAULIC ENGINEERING DATA 1

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DRAINAGE AREA CHARACTERISTICS: Steep, rocky, 100% wooded.
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 646.5 (502 Acre-Feet).
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 653.0 feet (668 Acre-Feet).
ELEVATION MAXIMUM DESIGN POOL: 653.0 feet.
ELEVATION TOP DAM: 653.0 feet.
SPILLWAY
a. Elevation 646.5 feet.
b. Type Rectangular concrete slab in channel cut through rock.
c. Width 55 feet.
d. Length 150 feet to drop down hill.
e. Location Spillover Left (South) abutment.
f. Number and Type of GatesNone.
OUTLET WORKS:
a. Type Three 12" dia cast iron pipes.
b. Location Under center of dam.
c. Entrance inverts Approximately 605 feet.
d. Exit inverts Approximately 603 feet.
e. Emergency draindown facilities
HYDROMETEOROLOGICAL GAGES:
a. Type Recording Rain Gage Station.
b. Location Joe Zerbey Airport, 15 miles from dam.
c. Records Sent to National Weather Service.
MAXIMUM NON-DAMAGING DISCHARGE: 5780 cfs. (Capacity of culvert under R.R. tracks with 25 foot head)

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DAM SAFETY ANALYSIS
HYDROLOGIC/HYDRAULIC DATA

Date: 21 Aug. 1978

By: 2. U. Cross

Sheet: 2 Of 9

DAM Lower Tumbling Run Nat. ID No. PA 00688 DER No. 54-24

	ITEM/UNITS	Permit/Design Files (A)	Calc. from Files/Other . (B)	Calc. from Observations (C)
1.	Min. Crest Elev., ft.	652.6		653.0
2.	Freeboard, ft.			
3.	Spillway ⁽¹⁾ Crest Elev, ft.	646.5		
3a.	Secondary ⁽²⁾ Crest Elev, ft.			
4.	Max. Pool Elev., ft.			653.0
5.	Max. Outflow ⁽³⁾ , cfs	2200		
6.	Drainage Area, mi²	6.5		6.0
7.	Max Inflow (4), cfs	Failure of Upp	er Tumb. Run from	n inflow > 0.3 PMF
8.	Reservoir Surf. Area, Acre	25.5		25.7
9.	Flood Storage (5), ft ³ Ac-Ft			166
10.	Inflow Volume, ft ³			

Reference all figures by number or calculation on attached sheets:

Example: 3A - Drawing No. xxx by J. Doe, Engr., in State File No. yyyy.

NOTES:

- (1) Main emergency spillway.
- (2) Secondary ungated spillway.
- (3) At maximum pool, with freeboard, ungated spillways only.
- (4) For columns B, C, use PMF.
- (5) Between lowest ungated spillway and maximum poul.

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PMF for Upper Tumb PMF for Upper Tumb PMF for Upper Timb PMF for Upper Timb West T. Spillway Capaci	Spillway with Max Spillway Way Spillway Using @ = C L H 1/2 From the V.S.G.S. G = Z.S × 555 × 6 We way a levation The Depart was a elevation for elev. Difference field (Shaets 2 Effect of Upper Tumble PMF for Upper Tumble PMF for Upper Tomble PMF for Upper Tomble West Bo PMF = 7200 Spillway Capacity PMP 25.5 inche (U.S. W. B TP- Use 90% ru Tumble val. Vz = Z Storage = 35.55 Ac	Spillway with Max Spillway Using Q = C L H3/2 or rough I irregular Q = 2.5 × 5.5 × 6.5 USE From the V.S.C.S. To drainage area 6.0 mit with to Doper T. Z. Spillway elevation report was acce elevation from elev. Difference fiel Q (Sheets 2. Effect of Upper Tomblin PMF for Upper T. R. the Comps of En with West Br. PMF = 7200(Spillway Capacity = One 90% rune Tuflow val. Vz = 22.5 Tuflow val. Vz = 22.5 Storage = 35.55 Ac ×	Spillway width: Max Spillway can Using Q = C = H with From the V.S.C.S. Top drainage area 6.0 mil with Sis to Upper T. R. D Spillway elevation P ve port was acces elevation found clev. Difference in field (Sheets 14) 2. Effect of Upper Tumbling PMF for Upper T.R. of the Corps of Engin with West Br. Sc PHF: 7200(A Spillway Cagazity = 2: PMP 25.5 inches fi (U.S. W. B TP-40 Use 90% run of S Tutlow val. Vz = 22.95 Tutlow val. Vz = 22.95 Storage = 35.55 Ac × 6.	Spillway with: S Max Spillway capa Using Q = C L H 2 with rough 1 irregular spi Q = 2.5 × 55 × 6.5 ½ = USE 2 From the V.S.G.S. Topose divariant area is 6.0 with with \$.5 to Upper T. R. Das Spillway alevation from & Irre report was accept elevation found if elevation fou	Spillway elev. 646.5 Spillway width: 56 Max Spillway capaci Using Q = C = H3/2 with C rough 1 irrecular spillw Q = 2.5 = 5.5 = 6.5 = 2 USE 22c From the V.S.G.S. Topogra diamage area was 6.0 mil, with S.S m to Upper T. R. Dam. Spillway elevation from capacity sport was accepted elevation from be clev. Difference meas field (Sheets 1911) 2. Effect of Upper Tumbling Run PMF for Upper T.R. as in the Corps of Engineer with West Br. Schuy PMF = 7200 (A.V) Spillway Capacity = 2200 PMP 25.5 inches for (Us. w. B. TP-40) Use 90% run aff = Inflow vol. Vz = 22.95/12 Storage = 35.55 Ac × 6.2 file	Spillway with: 56 ft Mark Spillway with: 56 ft Mark Spillway capacity Using Q = C L H* with C = Trough I irregular spillway Q = 2.5 × 55 × 6.5 × = 220 From the V.S.C.S. Topograph drainage area was 6.0 mill with S.S mill to Upper T. D. Dam Spillway elevation from report was accepted, elevation found by elev. Difference weason field (Sharts 14 II) 2. Effect of Upper T. Winding Run The Corps of Engineeric with West Br. Schwylk PMF = 7200 (S.S. as PMP 25.5 inches for 10 (U.S. w. B. TP-40) Use 90% run aff = 22 Tufflaw vol. V= 22.95/12 * S. Storage = 35.55 Ac × 6.2 ft =	Sp. Mary elev. 646. S. Ft Sp. Mary with: 56 ft Mark Sp. Mary capacity. Using Q = C. 11 way capacity. Prough I revealer sp. Mary capacity. Q = 2.5 × 55 × 6.5 × 2 = 2278. USE 2200 c From the V.S.G. S. Topographic distance area was for 6.0 mit with s. S. mit to Upper T. R. Dam. Sp. Mary elevation from the report was accepted, as elevation from the report was accepted, as elevation from the capacity. Special (Sweets 1911) 2. Effect of Upper Tombling Zim De. PMF for Upper T.R., as instruct we with west Br. Schwyllick with west Br. Schwyllick with west Br. Schwyllick with west Br. Schwyllick Tr. Schwyllick with west Br. Schwyllick Tr. Schw	Spillway width: 56 ft Max Spillway capacity: 210 Using & = C. 14 2 with C=2.5 1 Tough I receiver spillway give Q=2.5 = 5.5 = 6.5 2 = 2278.6 c USE 2200 cfs From the V.S.G.S. Toppgraphic w drawage area was found 6.0 mil with \$.5 mil trub. to Upper T. R. Dam Spillway alevation from the m report was accepted, and elevation found by address elev. Difference weasured full (Sheets 1915) 2 Effect of Upper Tumbling Run Dam: PMF for Upper T.R. as instructed the Copps of Engineers by a with West Br. Schwyllkill Ru PMF = 7200 (Ax) = 80 Spillway Capacity = 2200 cfs (19 PMP 25.5 inches for 10 mil Use 90% run off = 22.95. Tuffow val. Vz = 22.95/12 = 5.5 x = 6732 Acre-ft Storage = 35.55 Ac = 6.2 ft = 220	Spillway with: 56 ft Max Spillway capacity: 2100 c Using @ = C = H# with C = 2.5 for rough 1 irregular spillway gives @ = 2.5 * 55 * 6.5 % = 2278.6 cts USE 2200 cts From the V.S.G.S. Topographic may distinate area was found 6.0 mil, with S.S mil tribute to Doper T. Z. Dam Spillway elevation from the mos report was accepted, and co elevation from by adding elev. Difference measured in full (Shoets 14T) 2. Effect of Upper Tombling Zun Dam: PMF for Upper T.R., as instructed the Corps of Engineers to be con with west Br. Schwill kill Rour PHF = 7200 (AV) = 8028 Spillway Capacity = 2200 cfs (1913 PMP 25.5 inches for 10 mil, 6-1 (Using B, TP-40) Use 90% runaff = 22.95 in Tuffaw val. V= 22.95/12 * 5.5 * 66	Spillway width: 56 st Spillway width: 56 st Max Spillway capacity: 2100 c\$3 Using Q = C L H* with C = 2.5 for th rough 1 irregular spillway gives Q = 2.5 × 55 × 6.5 × 2 = 2278. G cts = 2 USE 2200 cfs From the V.S.G.S. Topographic map, drainage area was found to 6:0 mit, with 5.5 mil tributary to laper T. R. Dam Spillway elevation from the most report was accepted, and cross elevation found by adding t elev. Departion from the most report was accepted, and cross elevation found by adding t elev. Depart was instructed to The Corps of Engineers to composite the Corps of Engineers to c	Spillway cleve 646.5 ft Spillway with 56 ft Max Spillway capacity 2100 css Using Q = C = 11 with C = 2.5 for the rough 1 irregular spillway gives Q = 2.5 × 5.5 × 6.5 × = 2278.6 cts 2200 Cs = 22.5 × 5.5 × 6.5 × = 2278.6 cts 2200 The USG = 2200 cfs From the V.S.G.S. Topographic map, the disamage area was found to be 6.0 mil with S.S mil tributary a to Upper T. R. Dam Spillway elevation from the most re- report was accepted, and crest elevation found by adding the elevation found by adding the elevation found by adding the fell (Sheets 14 II) 2. Effect of Upper Tumbling izm Dam The Corps of Engineers by compani- with West Br. Schwyllia River is PMF = 7200 (Ax) = 8028 cfs Spillway Capacity = 2200 cfs (1913 Zepo PMP 25.5 inches for 10 mil, 6-hr du (U.S. W. B. TP 40) Use 90% runaff = 22.95 im Tutlow val. Vz = 22.95/12 × 5.5 × 640 = 6732 Acre-ft Storage = 35.55 Ac × 6.2 ft = 220 Acre-f

100

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	DATE	2978 SUBJECT LOWER TUMB. Pun Dam SHEET 6 OF 9
)		<u> </u>
		FOR PMF: [Ref: Sheets 8 , 9]
		Q = 2200 = 0.274 = P
		Storage Reg. = Ve
+++		Ve = (1-p) Vs : (1274)-6732
+++-	+-+-+-+	= 4887 Ac-A >> 220 Ac-ft.
+++-		-4081 Ac- # >7 200 Ac- 11.
		For SO% PMF
1		
		Q 2200 = 0.54B
		V-= (1-0.548) + 3366
1		* 1521 Ac - ft >> 220 Ac - ft
1		
		For 30 % PMF
		Qo . 200 = 0,913
+++		Ch 2408 0,913
+++-		V-+ (1913) +(-3+6732)
+++		VET UF (3, 3) (3, 6)
		= 176 Ac st = 220 Ac st OK
		: INFLOW OVER 30% OF PMF WILL
		CAUSE UPPER TURBLING ZUN TO OVERTOP.
	++++	AUD PRESUMABLY FAIL
	++++	+++++++++++++++++++++++++++++++++++++++
+		Capacity of Doper T.R. with water at com
+++	++++	crest is lous Ac-At
		With Lower T.T. reservoir at spillway
		crest remaining storage is 668-502= 166 ke hassuming failure is rapid; the available
		storage is only about 16 the inflow
		volume, and thus Lower T.E. Dam is
		THE CHICALITY
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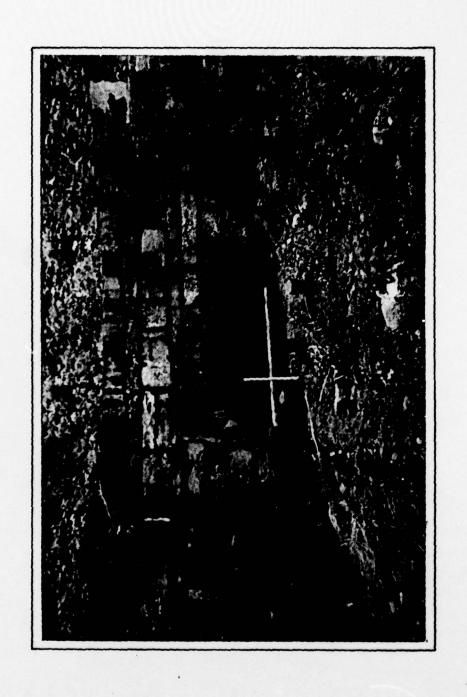
		478 SUBJECT LOWER TUMB DUN Dem SHEET 7 OF 9
KD. 8Y	DATE	108 No.
)		
/		
	3.	DOWDSTREAM
		Appropriately 1200 ft days trans
		the valley is blocked by an abandoned
		the value is blocked by an abandance
		multiple - track railroad embantement.
	-+-+-+	At the embankment, the stream passes
++++	\rightarrow	through a culvert; the downstream
1		portion of the edvert is 18 fit wide by 10 ft high and the top of the embandament is about 35-40 ft above
		by 10 ft high and the top of the
		embankment is about 35-40 ft about
		the channel invest
		= 4 12500 7
++++		"Tou me U.S. G.S. Topograpue map
+	++++	rottsville, Pa, The storage upstream
	-+	From the U.S.G.S. Topographic map "Pottsville, Pa", the storage upstream from the embandment is less than
		a avarter of the capacity of
		Lower Tumbling Run.
		THUS FAILURE OF LOWER TUNBLING
		EVIZZAM EZUAS OLUON MAC. UUS
		FLOODING OF MOUNT CARBON.
		TOO IN TOO CONSTRUCT
		++,+++,++++++++++++++++++++++++++++++++
	++++	Nou-acuaqua downstream discharge:
1-1-1		Nou-demaging domustream discharge:
		can take flooding to 25 ft over
		culvert center, with a no damage
		Smallest X-section is downstream.
		under highway, approx. 10 x 18 ft
		Area ~ 18=10= 180 54
		+ + + RIEQ T IDROF IBO III
		Head - 25 ft (neglecting tailwater effect
		Cc est. at 0.8 es ent. is from larger Culver
		Q= Cc4 /29 H = 0.8 × 180 1/2×37.2×25
		= 5778 cfs
1		THE OWNER OF THE PROPERTY PROCESSION
		MITS PAGE TS BEST QUALITY PRACTICALIS
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1	Sheet 8 of 9.
Q	
	Qr mav.
	3700 0 90 CO COC
3	
,	Qo mar. (PQI max)
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	
1-4	T B
	Time
PURPOSE: E	stablish relationship between
	coximum Spillway discharge and
	torage required to pass flood
	ydrograph Without exceeding
manufacture /m	paximum pool level.
A-400	_ AOB - A COB A COB
A AOB	
BAUD	AAOB AAOB
AAOC	$T \rho Q_{\rm r} m v / 2$
AACB	-1
	T. QI max /2
	400
^ /	40C = (1-p) AOB where 0 = p = 1.0
	A AOC
REFERENCE	100 0
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LETTER NO. 111 25 January 197	8-2 0.50 0.50 A ACB
	0.25 0.75 AAOB
	0 1.00 A AOB
	psge 1.05.2

APPENDIX

D

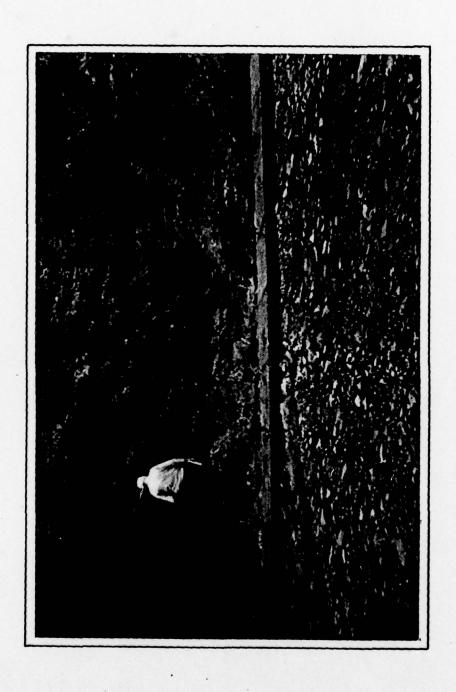
OUTLET SUPPLY CONTROL TOWER AND ACCESS BRIDGE.



VIEW OF TUNNEL AT DOWNSTREAM TOE THROUGH WHICH THREE WATER SUPPPLY PIPES PASS. VALVE HOUSINGS CAN BE SEEN IN FOREGROUND.

CONTROL VALVES FOR WATER SUPPLY PIPES.

VIEW OF SPILLWAY APPROACH CHANNEL AND BROAD CRESTED WEIR.



VIEW LOOKING DOWNSTREAM THROUGH SPILLWAY. NOTE BROAD CRESTED WEIR.



VIEW LOOKING UPSTREAM TOWARDS SPILLWAY CONTROL SECTION.

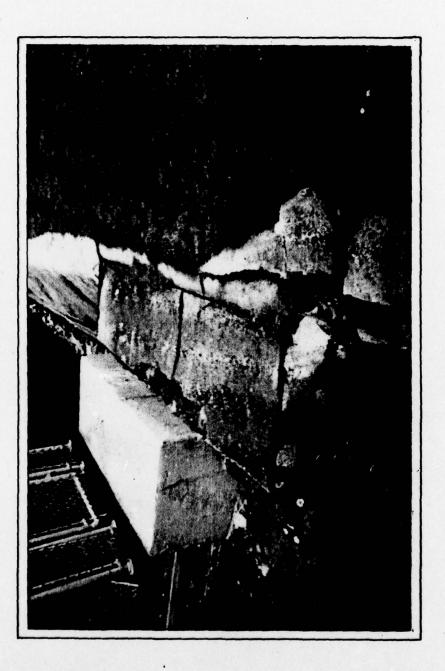
VIEW LOOKING UPSTREAM TOWARDS END OF SPILLWAY CHANNEL. NOTE CHANNEL DETERIORATION.

œ



END OF SPILLWAY CHANNEL LOOKING DOWNSTREAM INTO THE NATURAL STREAMBED.

VIEW OF UPSTREAM RIPRAP SPRAYED WITH GUNITE. NOTE EROSION AT BASE OF RIPRAP.



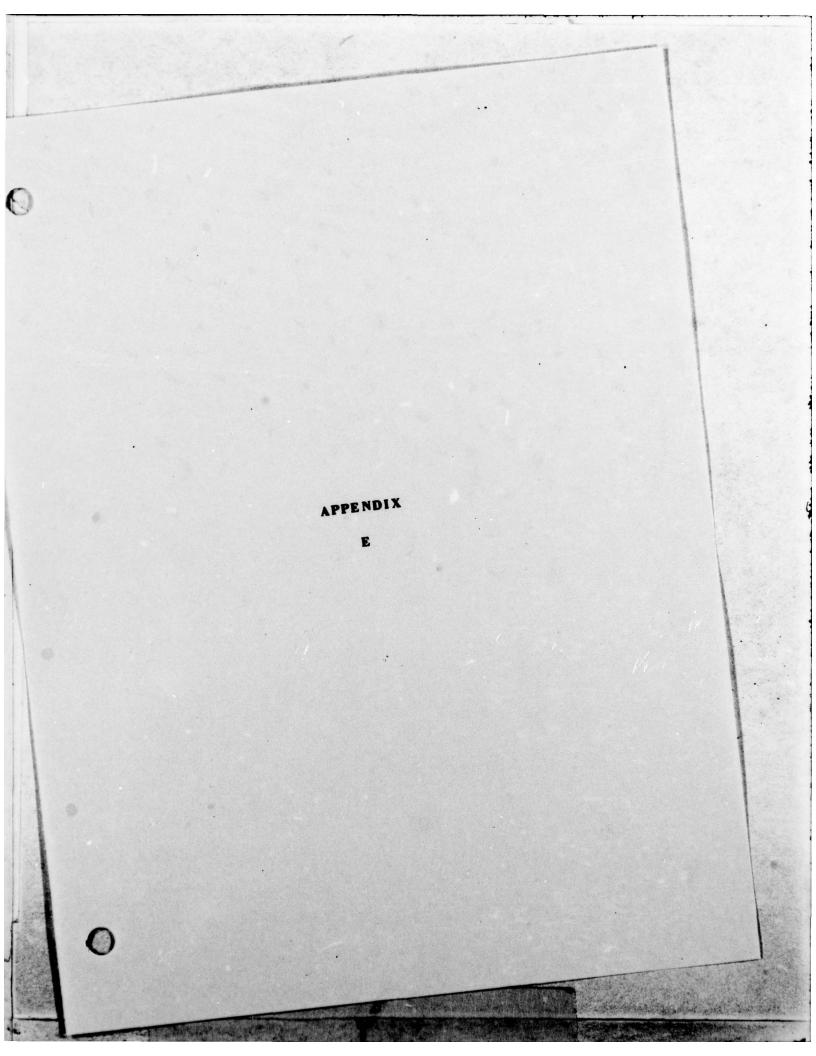
PHOTOGRAPH NO. 10

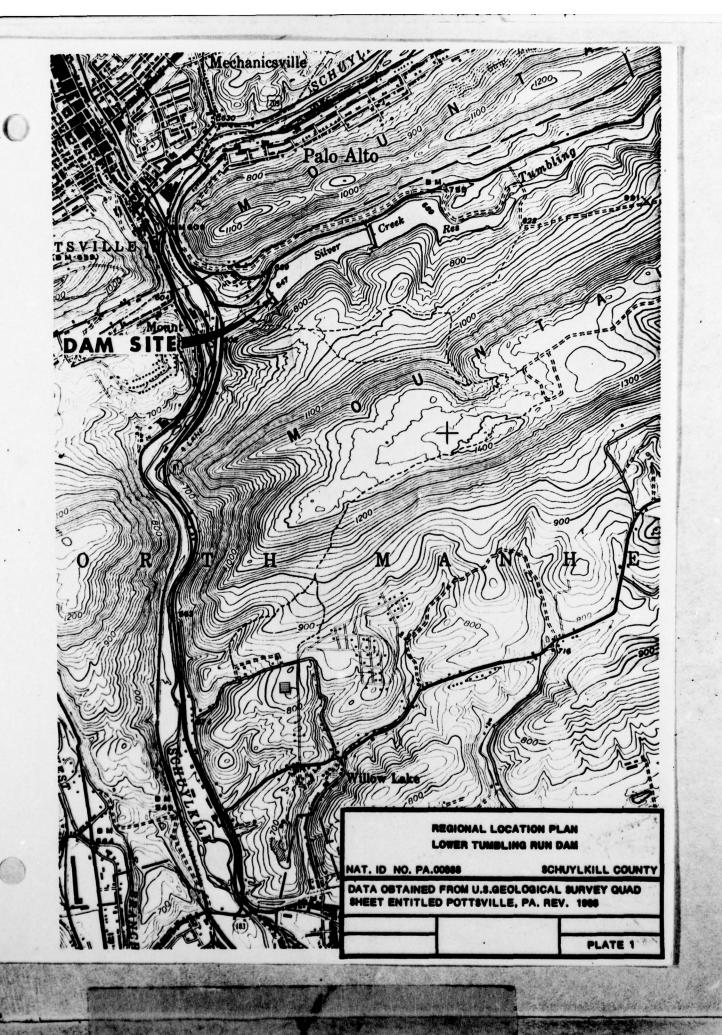
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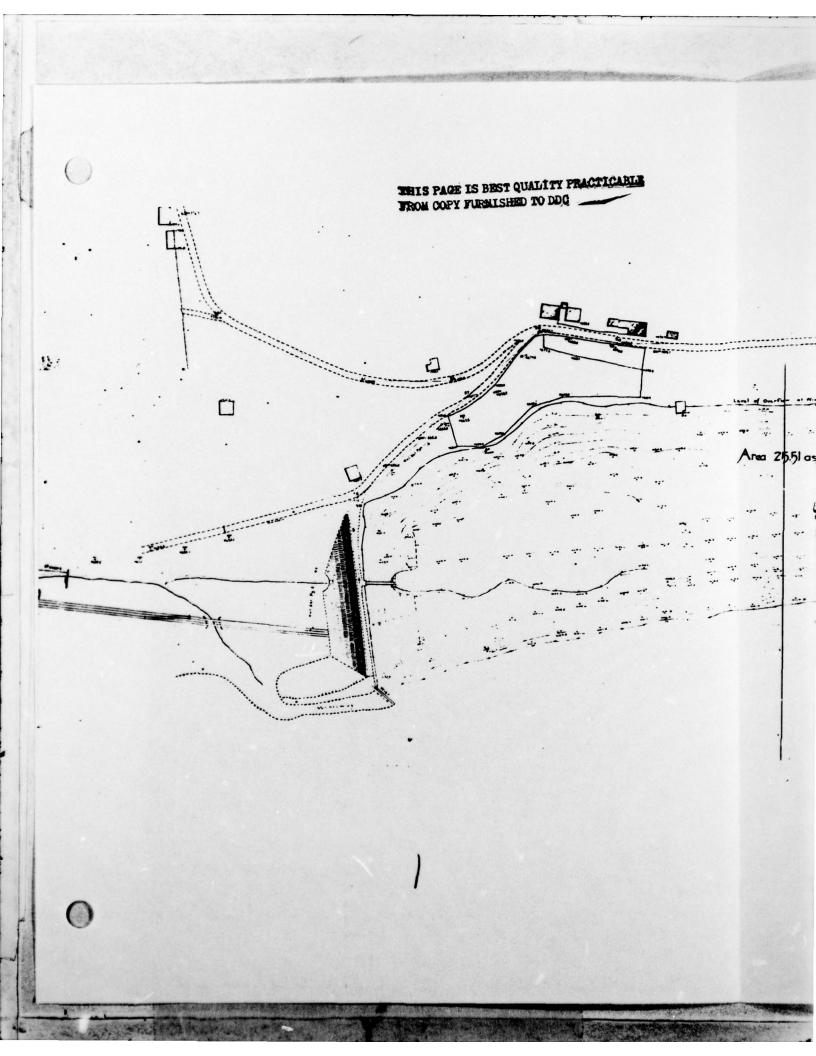
OVERVIEW OF DOWNSTREAM EMBANKMENT SLOPE. NOTE VEGETATION AND STEEP-NESS OF SLOPE.

ACCESS BOX TO TOE DRAIN SEEPAGE.
THE EMBNAKMENT IS ON THE LEFT
OF THE PHOTOGRAPH.

TUMBLING RUN CREEK PASSES THROUGH A TUNNEL UNDER A COMBINED 4-TRACK RAILROAD SIDING AND MULTILANE HIGHWAY DOWNSTREAM OF THE DAMS.





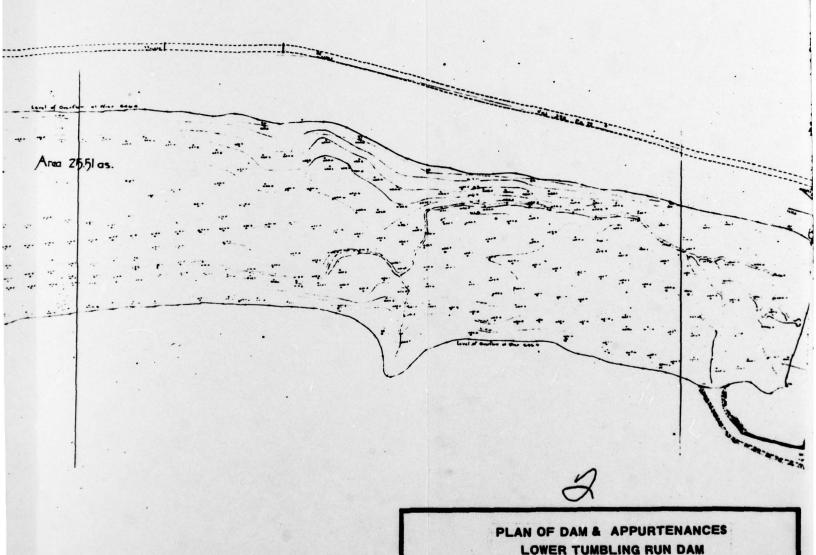


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SCHUYLKILL COUNTY

PLATE 2

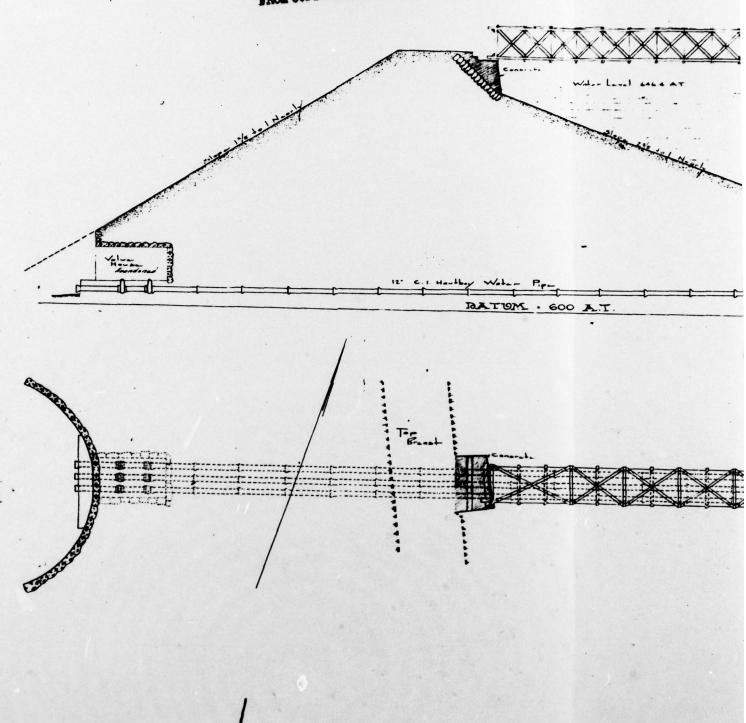
DATA OBTAINED FROM DEPARTMENT OF ENVIROMENTAL

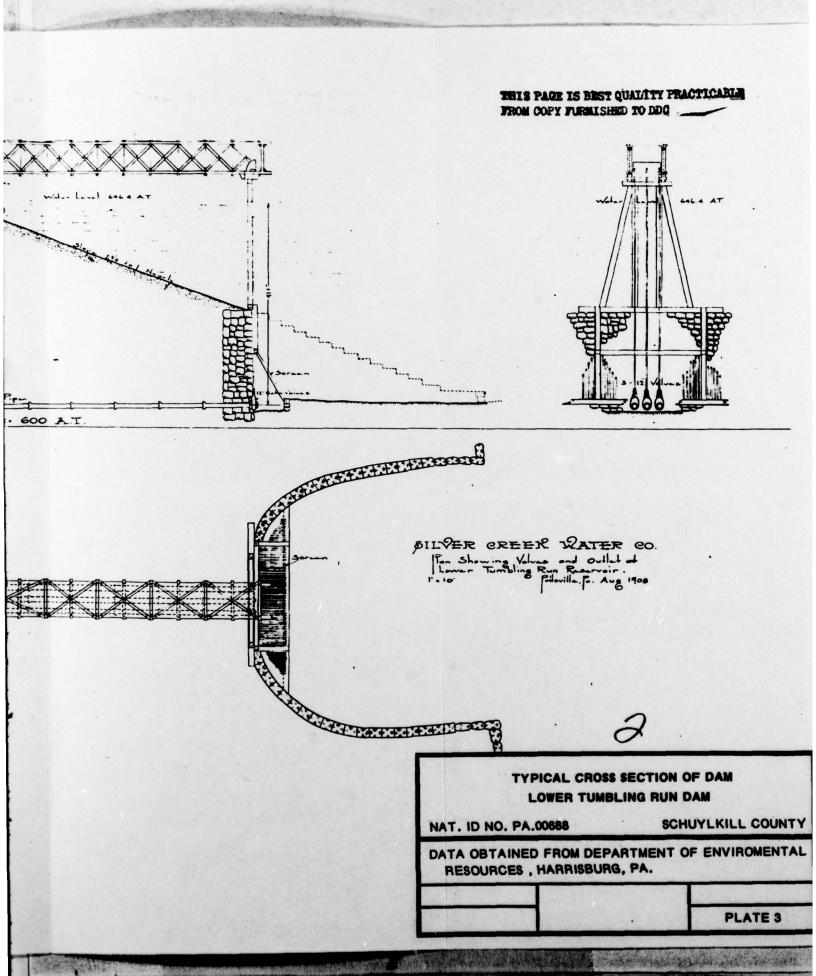


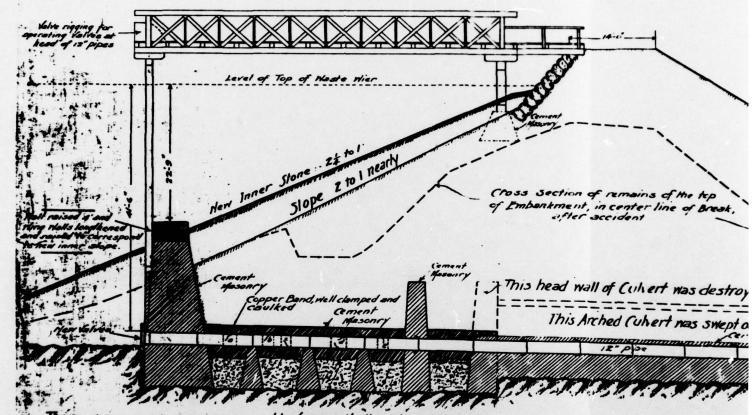
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RESOURCES, HARRISBURG, PA.

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There were a number of cracks in the pipe (a, b, c, d, e) which were banded, clamped and caulked in the very best manner before building the cement wall around the pipes.

Underneath the pipe Was soft Clay puddles — this is now dug out 2ft. below pipes and under this for 5ft. more in depth the Clay has been consolidated to a good building foundation by ramming pebbles and broken stone and working it down with an iron puddle bar. Pipes are now covered with cement wall shown in Red.

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TUMBLING RUN RESERVOIR CROSS SECTION OF EMBANKMENT

SURVEY made after Accident.

which happened July 19th, 1869.

New Colvert.

Resident Engineer,
Schuylkill Navigation Co.

Scale: - 10ft. = 1 in.

ead wall of Culvert was destroyed.

tection of remains of the tep tement, in center line of Break, after accident

ABLE

This Arched (uhert was swept out before the bank cased in.

the upper end of the pipes suther the are new net under pressure, as her tefere, when valves are dased.

Bottom of Slope.

2

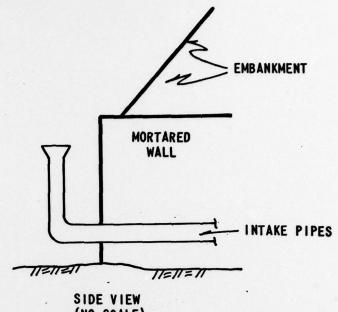
TYPICAL CROSS SECTION OF EMBANKMENT
LOWER TUMBLING RUN DAM

NAT. ID NO. PA.00688

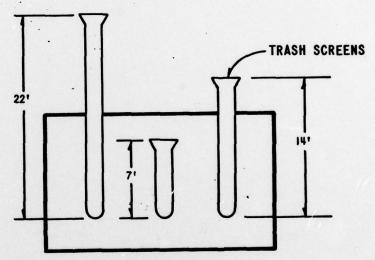
SCHUYLKILL COUNTY

DATA OBTAINED FROM DEPARTMENT OF ENVIROMENTAL RESOURCES, HARRISBURG, PA.

PLATE 4



SIDE VIEW (NO SCALE)



FRONT VIEW
LOOKING DOWNSTREAM
(NO SCALE)

SECTION OF WATER SUPPLY LOWER TUMBLING	
NAT. ID NO. PA.00688	SCHUYLKILL COUNTY
DATA OBTAINED FROM VER	BAL REPORTS FROM

APPENDIX

SITE GEOLOGY LOWER TUMBLING RUN DAM

Lower Tumbling Run Dam is located in the Appalachian Mountain Section of the Valley and Ridge Physiographic Province. The bedrock at the dam site is reported to consist of the red and brown sandstones, siltstones, and shales of the Mauch Chunk Formation (see Plate F-1). To the north, the Mauch Chunk Formation is bounded by the sandstones, shales and coal of the Pennsylvanian Pottsville and Llewellyn Formations, and to the south the Mauch Chunk Formation is bounded by the sandstones, siltstones, and shales of the Mississippian, Pocono and the Devonian Catskill Formation (Wood, 1973). Bedding is overturned, striking to the east-northeast and dipping steeply to the south-southwest (Wood, 1973). Two dominant sets of open, variably spaced joints have been observed: one set oriented along the strike of bedding, dipping gently to the northwest, and a second set striking north-northwest, and dipping steeply to the west (Wood, 1973; Sevon, 1975). No faults have been mapped beneath the dam, although two faults, one on either side of the reservoir, have been reported striking parallel to the reservoir.

Pleistocene age deposits are very limited in the dam site area, and are reported to mainly consist of periglacial talus deposits that cover much of the Tumbling Run stream valley (Wood, 1973).

Downstream seepage should not be a major problem unless the major east-northeast joint set is well developed, and is a zone of groundwater transport, beneath the dam due to the dam being constructed perpendicular to these features.

References:

1. Sevon, W.D., 1975, Geology and Mineral Resources of the Christmans and Pohopoco Mountain Quadrangle Carbon and Monroe Counties, Pennsylvania: Pa. Geol. Survey Atlas 195 ab, Plate 1, 1:24,000.

- 2. Willard, Bradford, 1939, Guide to the Geology of the Upper Schuylkill Valley: Pa. Geol. Survey, 4th Series, Bull. 1939, 24 p.
- 3. Wood, G.H., 1973, Geologic Map of the Pottsville Quadrangle, Schuylkill County, Pennsylvania: USGS Geologic Map GQ1028, 1:24,000.



