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Applied Research in Statistics - Mathematics - Operations Research

TOLERANCE LIMITS AND VARIABLES SAMPLING PLANS: SOME POWER CALCULATIONS FOR THE NORMAL AND LOGNORMAL DISTRIBUTIONS

by

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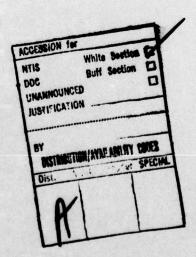
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#### I. INTRODUCTION

For product evaluation, life testing or reliability studies, a one-sided tolerance limit or a variables sampling plan is often required. Typical statements that may require these techniques are:

- (1) at least a desired proportion,  $p_0$ , of the product must meet or exceed a lower specification limit, L, with  $\gamma_0$  confidence
- or (2) at least a desired proportion,  $p_0$ , of the product must not exceed an upper specification limit, U, with  $\gamma_0$  confidence.

If  $p_0$  is taken to be 50% in a normal distribution, then the problem reduces to the familiar one of finding a one-sided confidence limit for  $\mu$ , or testing a statistical hypothesis concerning  $\mu$ . The problem under consideration here is the general problem where  $p_0$  is not restricted to be 50%.

Consider, for example, the U.S. Navy's requirement to have an oilwater separator capable of producing an effluent with less than 15 parts per million (ppm) of oil in the effluent water 85% of the time with 95% confidence. In this case,  $p_0 = 85\%$ , U = 15,  $\gamma_0 = 95\%$  and inferences related to the mean are not appropriate. As another example, suppose one gallon paint containers are filled by a machine. The manufacturer wishes to be 95% confident that at least 99% of the paint containers have one gallon or more in them. Here,  $p_0 = 99\%$ ,  $\gamma_0 = 95\%$  and L = 1.

These problems can be solved using either a parametric or a nonparametric procedure. In this report it has been assumed that a sample  $\mathbf{x}_1,\dots,\mathbf{x}_n$  is

available from a population which follows a normal distribution with mean  $\mu$  and variance  $\sigma^2$  (both  $\mu$  and  $\sigma^2$  unknown). Since the lognormal distribution can be transformed into a normal distribution, the results of power and sample size calculations will also apply to the lognormal distribution.

One approach that could be used in this situation is the construction of a one-sided tolerance limit. For example, in the case of a specification limit U that must not be exceeded, an upper tolerance limit could be constructed. An upper one-sided tolerance limit, A, is a quantity that can be calculated from the sample. This quantity is determined by

$$Pr[Pr(X \le A) \ge p_0] = \gamma_0. \tag{1.1}$$

In other words, after an observed value of A is calculated for a sample, there would be  $\gamma_0$  confidence that  $P(X \le A)$  is at least  $p_0$ . The proportion  $p_0$  is referred to as the coverage and  $\gamma_0$  as the confidence coefficient.

In the oil-water separator example, attention would be on the probability that the amount of oil in the effluent water is less than or equal to A. The value of A would be determined such that this probability is at least 85% with 95% confidence. The obvious change can be made if a lower one-sided tolerance limit is required. For example, in the paint container illustration, attention would be on the probability that the amount of paint in the container is at least A. The value of A would be determined such that this probability is greater than or equal to 99% with 95% confidence. In the case of a lower tolerance limit, p<sub>0</sub> is often referred to as the reliability of the product.

Based on a random sample, A could be calculated and then compared with U or L. The product would be accepted if U > A for an upper one-sided tolerance limit and rejected otherwise. Similarly, for a lower one-sided

tolerance limit, the product would be accepted if A > L and rejected otherwise. If the product just meets the specification, there is a probability of  $1-\gamma_0$  of accepting it. For values of  $\gamma_0$  that are generally used, this procedure places a large risk on a product being rejected if, in fact, the product just meets the specification.

Another approach to this problem is hypothesis testing by means of a one-sided variables sampling plan. This is a plan which guarantees that at least a proportion  $p_0$  of the population is less than a given value U with a probability  $\gamma_0$ . Specifically, if  $p = \Pr[X < U]$ , then it is desired to test  $H_0$ :  $p < p_0$  versus  $H_1$ :  $p \ge p_0$ . If a lower specification limit L is required, the problem can be described in similar statements where the hypotheses have been appropriately altered.

The tolerance limit approach and the variables sampling plan approach to the problem under consideration have been shown by Owens [6] to be equivalent. For brevity, the case of an upper specification limit will be assumed throughout the remainder of this report, although the results also apply to the case of a lower specification limit.

No matter how one approaches the problem, one must, implicitly or explicitly, be concerned with testing the null hypothesis  $H_0$ :  $p < p_0$  against the alternative  $H_1$ :  $p \ge p_0$ .

Under the normality assumption, A can be taken in the form of  $\bar{x}$  + ks, where  $\bar{x}$  and  $s^2$  are the sample unbiased estimators of  $\mu$  and  $\sigma^2$ , respectively. To construct an upper one-sided tolerance limit, one must determine k such that

$$Pr[Pr(X \le \bar{x} + ks) \ge p_0] = \gamma_0. \tag{1.2}$$

For a given  $p_0$  and  $\gamma_0$ , only the sample size is needed to determine the

value of k and hence the tolerance limit. Values of k are given in many statistical tables, and approximation formulas are also available. See, for example, Natrella [5], Owens [6], Eisenhart, Hastay and Wallis [1].

Tolerance limits are usually used in estimation. That is, given  $p_0$  and  $\gamma_0$  it is desired to estimate  $\mu + \phi^{-1}(p_0)\sigma$  with  $\gamma_0$  confidence, where  $\phi$  is the standard normal cumulative distribution function. However, an upper one-sided tolerance limit may also be used to test a hypothesis in the situation where a specification limit U has been imposed on the product. The procedure is to conclude that the specification has been met if  $\bar{x} + ks \leq U$  and to conclude that it has not been met otherwise.

Guenther [3] linked certain one-sided tolerance limits to hypothesis testing. He showed that for the normal distribution, a test based on the tolerance limit  $\bar{x}$  + ks is the uniformly most powerful invariant test.

### II. STATISTICAL FRAMEWORK

As was mentioned previously, the problem may be considered as a test of the hypothesis  $H_0$ :  $p < p_0$  versus the alternative hypothesis  $H_1$ :  $p \ge p_0$  where p = Pr[X < U]. Equation (1.2) is equivalent to

$$\Pr[T(f,\delta) < k\sqrt{n} | \delta = \Phi^{-1}(p_0)\sqrt{n}, f = n-1] = \gamma_0$$
 (2.1)

where  $T(f,\delta)$  is a noncentral t random variable with f degrees of freedom and  $\delta$  as the noncentrality parameter. (For a derivation of this equivalence, see Owens [6].)

In hypothesis testing, it is customary to speak in terms of the level of significance  $\alpha = 1 - \gamma_0$  rather than the confidence. From the formulation of the problem in (2.1), it is clear that k is determined by  $p_0$ , n, and  $\alpha$  (or  $\gamma_0$ ); i.e., k is determined by  $H_0$ . Under the alternative hypothesis, only the noncentrality parameter  $\delta$  is changed.

Consider now the power of the test. It is a function of four parameters and can be written as

$$G(p_0, \gamma_0, p, n) = Pr[T(f, \delta) \ge k\sqrt{n} | \delta = \phi^{-1}(p)\sqrt{n}, f = n - 1]$$
 (2.2)

Since the alternative hypothesis is a one-sided alternative, it is only necessary to consider the power for values of  $p \ge p_0$ .

Before the power can be calculated, the value of k must be determined. This can be done by choosing the k which minimizes

$$(\Pr[T(f,\delta) < k\sqrt{n} | \delta = \Phi^{-1}(p_0) \sqrt{n}, f = n - 1] - \gamma_0)^2$$

With this value of k, the calculation of the power  $G(p_0, \gamma_0, p, n)$  for various values of p is an evaluation of the probability that a noncentral t random variable is greater than or equal to  $k\sqrt{n}$ . Tables 1 through 8 present the values of  $G(p_0, \gamma_0, p, n)$  for selected values of the parameters. All calculations were carried out in double precision using the IBM 370 computer.

Although the tables are given in terms of the confidence level  $(\gamma_0)$  and the power (G), some experimenters may find the tables easier to interpret in terms of consumer's and producer's risks. The consumer's risk in this problem is the probability of rejecting  $H_0$  and accepting the product when the specification limit has not been met. This is the level of significance of the test and is controlled at a maximum of  $\alpha$ . The producer's risk is the probability of rejecting the product when it does meet the standard. This can easily be calculated from the table, since this is the probability of a Type II error, and hence is equal to  $1 - G(p_0, \gamma_0, p, n)$ . For a given n and  $\gamma_0$ , as  $p - p_0$  becomes larger, the producer's risk becomes smaller.

It should also be emphasized that if the specifications are exactly met,  $(p=p_0)$ , and the test is conducted at  $\alpha=1-\gamma_0$  level of significance, then the producer's risk is  $\gamma_0$ . This means that the performance must indeed be better than the stated requirement to have much of a chance of being accepted. For example, if 80% confidence is required, then the producer's risk is 80% if his product meets, but is not better than, the stated requirement. In this case, the probability is 80% that the product will be rejected, even though it does meet the standard.

Sample	4			True Va	frue Value of P(X	( × U)		
		3.800	0.850	0.900	0.920	0.940	0.960	0.980
10	1 4741	100	198	378	0 482	609	0 75.5	906 0
20	1-24)4		0.267	6-579	6.729	0.865	0.950	0.997
36	1.1540	0.100	0.326	0.721	0.865	0.958	0.994	1.000
0 7	1.1901	100	0.380	0.818	0.535	0.988	0.999	1.000
50	1.0747	-	9-428	6.883	0.970	156.0	1.000	1.000
09	1.0522	0.5100	0.473	0.926	0.586	666.0	1.000	1.000
70	1.0351	30.90g	0.515	0.954	156.0	1.000	1.000	1.000
80	1.0215	7 10	0.553	0.571	1550	1.000	1.000	1.000
06	1.0103	2 30	0.589	0.982	666.0	1.000	1.000	1.000
100	1.3310	100	0.622	0.589	1.000	1.000	1.000	1.000
110	0.9930	4.500	0.653	0.993	1.000	1.000	1.000	1.000
120	0.7861	100	0.681	955 0	1.000	1.000	1.000	1.000
130	0.9801		0.708	0.958	1.000	1.000	1.000	1.000
07.	1.5747		6-732	0.599	1.000	1.000	1.000	1.000
150	0.5700	100	0.754	666.0	1.000	1.000	1.000	1.000
100	0.9656	188	6.775	1.000	1.000	1.000	1.000	1.000
170	0.9617		0.794	1.000	1.000	1.000	1.000	1.000
180	0.9582	100	0.512	1.000	1.000	1.000	1.000	1.000
190	0.9549		0.828	1.000	1.000	1.000	1.000	1.000
200	0.9519	200000	0.843	1-000	1.000	1.000	1.000	1.000

.90 Probability of Exhibiting  $P(X \le U) > p_0$  for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for  $p_0$  = .80 and  $\gamma_0$  = Table 1:

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<b>G</b>	0.940 0.960 0.980	0.581 (	0.896	0.980	0.997	1.000	1.000	1.090	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
frue Value of $P(X \le U)$	0-520																				
True /	006-0 0	E 0.233																			
		3.1CE																			
	0.800	32 3.050	0	C		7	0	C	_	^	7	0			C		•	0	0	î	?
<b>a</b>														1.0212				0			
Sample		-	20	36	7	5(	9	70	86	)6	100	11	120	130	140	150	160	170	180	190	200

Probability of Exhibiting P(X  $\leq$  U) >  $p_0$  for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for  $p_0$  = .80 and  $\gamma_0$  = .95 Table 2:

### THIS PAGE IS BEST QUALITY PRACTICABLE FROM COPY FARMISHED TO DDC

10         1.7332         0.10C         0.218         0.257         0.407         0.559         0.767           20         1.4710         0.10C         0.218         0.257         0.407         0.559         0.767           20         1.4710         0.10C         0.218         0.257         0.407         0.559         0.767           30         1.3754         0.10C         0.374         0.447         0.628         0.821         0.966           40         1.327         3.10C         0.443         0.644         0.656         0.977         1.000           50         1.2638         0.10C         0.555         0.802         0.955         0.992         1.000           70         1.2451         0.10C         0.636         0.914         0.992         1.000         1.000           80         1.2451         0.10C         0.686         0.914         0.992         1.000         1.000           100         1.293         0.10C         0.752         0.992         1.000         1.000           110         1.293         0.10C         0.752         0.992         1.000         1.000           110         1.1994         0.10C	Size	м		Ħ.	True Value of P(X	of P(X < U)	_		
0.10C 0.218 0.257 0.407 0.559 0.10C 0.377 0.568 0.774 0.934 0.10C 0.443 C.664 C.866 0.977 0.10C 0.443 C.664 C.866 0.977 0.10C 0.552 0.741 0.522 0.992 0.10C 0.603 0.849 0.975 0.999 0.10C 0.686 0.914 0.992 1.000 0.10C 0.721 0.935 C.996 1.000 0.10C C.78C 0.952 0.999 1.000 0.10C 0.82E C.989 1.000 0.10C 0.88E 0.973 0.999 1.000 0.10C 0.88E 0.973 1.00C 1.000 0.10C 0.88E 0.995 1.00C 1.00C 0.10C 0.89E 0.995 1.00C 1.00C			028-0	006-0	0-920	0.940	096.0	0.980	
0.10C 0.377 0.568 0.774 0.934 0.10C 0.377 0.568 0.774 0.934 0.10C 0.443 C.664 C.866 0.577 0.568 0.774 0.934 0.10C 0.502 0.741 0.522 0.992 0.10C 0.555 0.802 0.949 0.975 0.999 0.10C 0.686 0.914 0.992 1.000 0.10C 0.721 0.935 0.999 1.000 0.10C 0.721 0.935 0.999 1.000 0.10C 0.752 0.999 1.000 0.10C 0.828 0.999 1.000 0.828 0.999 1.000 0.828 0.999 1.000 0.828 0.999 1.000 0.828 0.995 1.000 0.828 0.995 1.000 0.828 0.995 1.000 0.828 0.995 1.000 0.000 0.828 0.995 1.000 0.000 0.828 0.995 1.000 0.000 0.806 0.995 1.000 0.000 0.806 0.995 1.000 0.000 0.806 0.995 1.000 0.000 0.806 0.995 1.000 0.000 0.806 0.995 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.996 0.000 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990 0.997 0.000 0.000 0.990		1.7332		0.218	0.297	0.407	0.559	0.767	
0.10C 0.377 0.568 0.774 0.934 0.10C 0.443 C.6E4 C.E66 0.977 0.10C 0.502 0.741 0.522 0.992 0.10C 0.555 0.802 0.955 0.999 0.10C 0.686 0.914 0.992 1.000 0.10C 0.751 0.935 0.998 1.000 0.10C 0.752 0.952 1.000 0.10C 0.752 0.999 1.000 0.10C 0.848 0.973 0.999 1.000 0.10C 0.866 0.973 0.999 1.000 0.10C 0.866 0.985 1.000 1.000 0.10C 0.862 0.992 1.000 1.000 0.10C 0.862 0.992 1.000 1.000 0.10C 0.896 0.994 1.000 1.000 0.10C 0.896 0.994 1.000 1.000		1.4710		0.304	0.447	0.628	0.821	996.0	
J.100 0.443 C.664 C.866 0.977 J.100 0.502 0.741 0.522 0.992 J.100 0.555 0.802 0.955 0.997 J.100 0.686 0.914 0.992 1.000 J.100 0.686 0.914 0.992 1.000 J.100 0.721 0.935 0.998 1.000 J.100 0.752 0.998 1.000 J.100 0.806 0.973 0.999 1.000 J.100 0.828 C.986 1.000 J.100 0.882 0.985 1.000 1.000 J.100 0.882 0.992 1.000 1.000 J.100 0.896 0.994 1.000 1.000 J.100 0.896 0.994 1.000 1.000 J.100 0.899 0.996 1.000 1.000		1,3754		0.377	0.568	0.774	0.934	966.0	
9.100 0.502 0.741 0.522 0.992 3.100 0.555 0.802 0.955 0.997 0.100 0.603 0.849 0.975 0.999 3.100 0.686 0.914 0.992 1.000 3.100 0.721 0.935 0.998 1.000 3.100 0.752 0.952 0.998 1.000 3.100 0.826 0.973 0.999 1.000 3.100 0.826 0.985 1.000 1.000 3.100 0.882 0.992 1.000 1.000 3.100 0.882 0.992 1.000 1.000 3.100 0.896 0.994 1.000 1.000 3.100 0.896 0.994 1.000 1.000		1.3227		0.443	C. EE4	0.866	0.977	1.000	
0.100		1.2884		0.502	0.741	0.522	0.992	1.000	
0.100		1.2638		0.555	0.802	0.955	0.997	1.000	
1.10C		1.2451		0.603	0.849	0.975	0.999	1.000	
C.10C 0.686 0.914 0.992 1.000 0.10C C.721 0.935 C.996 1.000 0.100 C.752 0.952 0.998 1.000 0.100 C.78C C.944 C.999 1.000 0.10C C.78C C.989 1.000 0.10C C.848 0.973 C.999 1.000 0.10C C.848 0.985 1.00C 1.000 0.10C C.882 0.992 1.00C 1.000 0.10C C.896 0.994 1.00C 1.000 0.10C C.896 0.994 1.000 1.000 0.10C C.896 0.997 1.000 1.000		1.2303		9.647	0.886	0.586	1.000	1.000	
3.10c       0.721       0.935       0.996       1.000         3.100       0.752       0.952       0.998       1.000         0.100       0.806       0.973       0.999       1.000         3.10c       0.826       0.973       0.999       1.000         3.10c       0.826       0.983       1.000       1.000         0.10c       0.866       0.985       1.000       1.000         0.10c       0.862       0.992       1.000       1.000         0.10c       0.896       0.992       1.000       1.000         0.10c       0.896       0.996       1.000       1.000         0.100       0.909       1.000       1.000		1.2131		0.686	0.914	0.992	1.000	1.000	
3.100       C.752       0.952       0.998       1.000         0.100       C.78C       C.944       C.999       1.000         0.100       0.82E       C.980       1.000       1.000         1.100       C.84E       0.985       1.000       1.000         0.100       C.6E       0.985       1.000       1.000         0.100       C.8E       0.992       1.000       1.000         0.100       C.89E       0.992       1.000       1.000         0.100       C.909       0.996       1.000       1.000         0.100       C.920       0.997       1.000       1.000		1.2030		0.721	0.935	965.0	1.000	1.000	
0.100 C.78C C.544 C.999 1.000 0.100 0.826 0.973 C.999 1.000 3.10C C.846 0.985 1.000 1.000 0.10C C.846 0.985 1.00C 1.000 0.10C C.862 0.992 1.00C 1.000 0.10C C.882 0.992 1.00C 1.000 0.10C C.896 0.994 1.00C 1.000 0.10C C.896 0.996 1.000 1.000		1.1994		0.752	0.952	966-0	1.000	1.000	
0.100 0.806 0.973 0.999 1.000 3.100 0.828 0.985 1.000 1.000 7.100 0.848 0.985 1.000 1.000 0.100 0.866 0.989 1.000 1.000 0.100 0.886 0.992 1.000 1.000 0.100 0.809 0.996 1.000 1.000 0.100 0.809 0.996 1.000 1.000		1.1917		081.3	C. 9t4	566.0	1.000	1.000	
3.100 0.82E C.580 1.000 1.000 7.100 C.84E 0.9E5 1.000 1.000 0.10C C.EE 0.992 1.00C 1.000 0.10C C.8E 0.992 1.00C 1.000 0.10C C.89E 0.992 1.00C 1.000 0.10C C.89E 0.99E 1.00C 1.000 0.10C C.92C 0.99F 1.00C 1.000		1.1854		0.806	0.973	0.999	1.000	1.000	
7.100 C.848 0.985 1.000 1.000 0.100 C.866 0.589 1.00C 1.000 0.10C C.882 0.992 1.00C 1.000 0.10C C.896 0.994 1.000 1.000 0.100 0.509 0.996 1.000 1.000 0.100 C.920 0.957 1.000 1.000		1.1796		0.826	085.0	1.000	1.000	1.000	
0.100 6.862 0.992 1.000 1.000 0.100 0.862 0.992 1.000 1.000 0.100 0.509 0.954 1.000 1.000 0.100 0.509 0.996 1.000 1.000 0.100 0.520 0.957 1.000 1.000		1.1744		848.0	0.985	1.000	1.000	1.000	
0.10C 0.882 0.992 1.00C 1.000 0.10C 0.896 0.954 1.000 1.000 0.100 0.509 0.996 1.000 1.000 0.100 0.520 0.957 1.000 1.000		1.1697		0.866	0.589	1.000	1.000	1.000	
0.100 0.896 0.954 1.000 1.000 0.100 0.909 0.996 1.000 1.000 0.100 0.920 0.997 1.000 1.000		1, 1655		0.882	0.992	1.000	1.000	1.000	
0.100 0.509 0.996 1.000 1.000 0.100 0.520 0.957 1.000 1.000		1. 16 16		0.896	176.0	1.000	1,000	1.000	
J. 100 C. 920 0.957 1.000 1.000		1.1531		505.0	966.0	1.000	1.000	1.000	
		1.1548		C- 520	156.0	1.000	1.000	1.000	

Probability of Exhibiting P(X  $\le$  U)  $^>$  p<sub>0</sub> for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for p<sub>0</sub> = .85 and  $\gamma_0$  = .90 Table 3:

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Sample	4		F	True Value of P(X <	of P(X < 1	n)	
		0-850	006-5	0-920	0 75 - 3	096-0	0-980
01	1,5881	0.050	0.120	0.174	0.254	0.381	0.594
50	1.6145	0.050	0.182	0.295	0.400	0.680	606.0
30	1,4833	050-0	0.241	0-466	6.627	0.854	0.985
0,	1.4121	0.050	967-0	0.507	0.752	0.938	0.998
20	1. 3660	3.050	6.349	0.555	C. E40	0.576	1.000
09	1, 1332	0.050	004.0	0.670	669.0	0.991	1.000
7.0	1,3084	0.050	344.0	6-734	0.538	156.0	1.000
90	1.2889	0.050	161-0	0.787	0.962	0.999	1.000
06	1.2728	0.050	0.537	0.831	0.977	1.000	1.000
100	1.2594	0.050	0.577	0.867	0.987	1.000	1.000
110	1.2480	0.050	0.614	0.855	C. 592	1.000	1.000
120	1.2382	3.050	649-0	0.918	0.555	1.000	1.000
130	1.2236	3.050	0.661	0.537	0.967	1.000	1.000
140	1.2220	0.050	0.711	0.951	665.0	1.000	1.000
150	1.2152	0.050	0.736	0.562	665.0	1.000	1.000
160	1.2091	0.050	C.763	0.971	1.000	1.000	1.000
170	1,2936	0.050	6.786	872.0	1.000	1.000	1.000
180	1.1985	0.050	C.8C7	0.583	1.000	1.000	1.000
190	1.1939	0.050	0.827	C. 587	1.000	1.000	1.000
200	1.1897	0.050	0.844	066-0	1.000	1.000	1.000

Probability of Exhibiting  $P(X \le U) > p_0$  for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for  $p_0$  = .85 and  $\gamma_0$  = .95 Table 4:

		006-00	0.910	0- 320	0.930	0-640	0-950	0-360	0-970	0.980	9
2	2.0659	0.100	0.121	0.146	0.178	0.218	0.269	0.334	0.421	0.541	0.7
20	1.7054	0.100	0.133	0.176	0.233	0.306	0.399	0.515	0.654	0.806	0.9
30	1.6573	3.100	0.143	0-202	0.280	0.382	0.507	0.652	0.800	0.925	6.0
01	1.5981	0.100	0.152	0.224	0.323	644.0	0.597	0.753	0.889	0.973	0.9
20	1.5597	0.100	0.159	0-245	0.363	6.509	0.673	0.827	0.939	0.991	1.000
09	1.5322	0.100	0.167	0.265	004.0	0.563	0.735	0.880	0.968	0.997	1.0
20	1.5114	c. 10c	0.174	0.284	C-435	0.612	0.767	0.918	0.983	0.999	1.0
80	1.4949	3.100	0.130	0.303	0.468	0.656	0.829	0.944	0.991	1.000	1.0
06	1, 4,815	3.100	0.187	6.320	0.499	9690	0.864	0.962	966.0	1.000	1.0
00	1.4702	9.100	0.193	0.337	0.528	0.731	0.891	0.975	0.998	1.000	1.000
10	1.4607	3.100	0.199	0.354	6.556	0.762	0.914	0.983	666.0	1.000	1.0
150	1.4524	3.100	0.204	0.370	0.582	0.790	0.932	0.989	0.999	1.000	1.0
30	1.4452	3-100	C-210	0.365	C.6C7	0.815	946.0	0.993	1.000	1.000	1.0
04	1.4388	c. 10c	0.216	004.0	0.631	0.838	0.958	0.995	1.000	1.000	1.0
. 05	1.4330	0.100	0.221	0.415	C-653	0.357	0.967	0.997	1.000	1.000	1.0
09	1.4279	0.100	0.226	0.430	0.674	0.875	0.974	0.998	1.000	1.000	1.0
10	1.4232	3.100	0.231	111-0	£59°3	0-890	0.980	0.999	1.000	1.000	1.0
80	1.4190	0.100	0.237	0.457	0.713	106.0	0.984	0.999	1.000	1.000	1.0
06	1.4150	0-100	0.242	0-471	C.730	0.916	0.988	0.999	1.000	1.000	1.0
00	1.4115	0.100	0.246	0.484	0.747	0.927	0.830	1.000	1.000	1.000	1.0

Probability of Exhibiting  $P(X \le U) > p_0$  for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for  $p_0$  = .90 and  $\gamma_0$  = .90 Table 5:

Size

True Value of P(X < U)

	0-990	0.534	0.866	0-970	0.994	0.999	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
	0.980	0.364	0.660	0.838	0.929	0.971	0.989	966.0	0.998	0.999	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	
	0.970	0.264	0.485	099.0	0.784	0.868	0.921	0.954	476.0.	0.985	0.992	966 0	0.998	0.999	0.999	1.000	1.000	1-000	1.000	1.000	
	096-0	0.199	0.352	0.489	909.0	0.701	0.777	0.835	0.880	0.913	0.938	0.956	696 0	0.978	0.985	0.990	0.993	0.995	0.997	0.998	000
	0.950	0.154	0.255	0.349	0.437	0.517	0.589	0.652	0.708	0.756	0.797	0.832	0.861	0.886	0.907	0.924	0.938	0.950	0.959	0.967	
	0+6-0	0.120	0.184	0.243	0.301	0.355	0.407	0.457	0.503	0.547	0.588	0.626	0.661	0.693	0.723	0.750	0.775	0.798	0.819	0.838	1100
	0.930	0.095	6.133	0.167	0.199	0.231	0.261	162.0	0.320	6.349	0.377	C.403	0.430	0.455	0.480	0.503	0.526	6.549	0.570	0.591	000
	0-920	0.076	960-0	0.113	0.128	0.143	0.158	0.172	0.186	0.199	0.213	0.226	0.239	0.252	0.265	0.277	0.290	0.302	0.314	0.326	000
	0-910	0.062	690-0	6.075	0.081	0.086	0.091	6.055	C. 100	3.104	0.108	0.112	0.116	0-120	0.124	6-127	0.131	0.135	0.138	0.142	7:10
	006-0	0.050	0.350	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050	3.056	0.050	3.050	0.050	0.050	0.050	0.050	0.050	0.050	000
		2,3549	1.9262	1.1775	1.6974	1.0458	1.6091	1,5914	1,5596	1.5418	1,5269	1,5143	1.5034	1.4939	1.4855	1.4730	1.4712	1,4651	1.4595	1. 4544	
S1 <b>z</b> e		10	20	36	0,	50	09	0,	90	06	100	110	120	130	140	150	160	170	180	190	2.10

Probability of Exhibiting P(X  $\le$  U) > p<sub>0</sub> for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for p<sub>0</sub> = .90 and  $\gamma_0$  = .95 Table 6:

Sample

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Sample Size	ч		True Value	alue of P(X	K (4)	
		0-950	095-2	0-970	086.0	056-0
92	ഗ		.13	18	26	7
20	N		5	24	33	
30	$\circ$		.17	53	64	. 7
04	2.3107	9-100	C. 187	0.340	C.585	0.882
50	C		.20	38	99	6.
09	cn.		.21	42	72	5.
0,	o		.22	94	17	6.
80	Œ		. 23	6 4	13	6.
30	$\mathbf{x}$		. 25	52	85	6.
100	0.00		. 26	56	88	6.
110	200		.27	59	90	6.
120	$\mathbf{a}$		8 Z .	19	52	6.
130			. 29	19	45	0
140	1.3252		.36	99	55	0
150			.31	69	96	0.
160	33		32	71	57	0
170	(2)		.33	73	67	0.
130	1, 90?3		.34	75	CB	0.
190	1.7978		.35	16	98	0
200	1.7937		. 36	18	98	0

Probability of Exhibiting P(X  $\leq$  U) > p<sub>0</sub> for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for p<sub>0</sub> = .95 and  $\gamma_0$  = .90 Table 7:

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Size			True Va	True Value of $P(X \le U)$	(a > I	
		0-950	595.5	026-5	095 - 0	066-5
10	116	. 05	.ct		0.149	0.256
70	.396	.05	82.		24	0.473
30	.220	.05	60.		33	0-647
0,7	2.1259	0.050	0.103	0.212	0.424	0.774
50	.065	.05			50	0.860
90	.022	.05	.12		57	0.915
20	696.	.05	. 13		£ 3	C.550
9	.964	. 05	114		69	0.971
90	116.	. 35	14		74	0.584
100	976.	. 05	.15		78	0.941
110	.912	.05	. 16		13	0.995
126	.839	.05	.17		13	0.997
130	989	.05	. 13		13	656.0
140	.873	. 05	.18		80	0.000
150	.R73	.05	.13		5	1.000
160	.862	.05	.20		93	1.000
170	.355	.05	.21		45	1.000
180	. 348	. 05	.22		55	1.000
190	~	- 05	.22.		95	1.000
200	-	.05	.23		67	1.000

Probability of Exhibiting  $P(X \le U) > p_0$  for a Normal Distribution When the One-sided Tolerance Limit  $\bar{x}$  + ks is Calculated for  $p_0$  = .95 and  $\gamma_0$  = .95 Table 8:

### III. APPLICATIONS

These results can be used in a variety of situations. In general, the tables will be useful to any experimenter in a situation in which the test statistic follows a noncentral t distribution under both the null and the alternative hypothesis, with the difference in the distribution being only a change in the noncentrality parameter  $\delta$ . Specifically, the problems that have been considered by the authors are related to tolerance limits and variables sampling plans. The following examples illustrate some of these situations.

Example 1: Suppose a consumer, for example, the U.S. Navy, requires an oil-water separator system capable of separation such that not more than 20 parts per million (ppm) of oil is contained in the water effluent 85% of the time with 95% confidence. Previous experience indicates that the distribution of the amount of oil in the effluent water follows a lognormal distribution. A separator system is put on test, 170 samples are collected and analyzed. The natural logarithms of the observations were found, and the mean and standard deviations of the transformed scores were 1.7542 and 0.8262 respectively, With k = 1.2036 taken from Table 4 with  $p_0 = .85$  and  $\gamma_0 = .95$ , it is found that  $\bar{x} + ks = 2.7487$  which is less than  $\ln(20)$ . It is therefore concluded that the system does meet the requirement.

Example 2: If, in example 1, the requirement had been that the effluent contain not more than 15 ppm of oil 85% of the time with 95%

confidence, the system would have been judged unsatisfactory since 2.7487 > ln(15). After examining the tables, the manufacturer may in return have argued that his risk in this situation was too high. If his system meets, but does not exceed the requirement, he faces a 95% chance of having his system rejected. In fact, his system must produce less than 15 ppm of oil 90% of the time in order to have a probability of 76% of being accepted.

Example 3: Suppose a lower 95% tolerance limit is required for  $p_0$  = 85%. It is, of course, desirable to have this quantity close to the point it is estimating,  $\mu + \Phi^{-1}(1 - p_0)\sigma$ . A method of measuring this closeness and determining sample size was presented by Faulkenberry and Weeks [2]. Using this method, a  $p > p_0$  and a small  $\epsilon > 0$  would be chosen. Then the sample size would be determined to satisfy

$$Pr[Pr(X > \bar{x} + ks) \ge p] \le \varepsilon.$$

In other words, the probability of a Type II error is no larger than & at p.

If p = 96% and  $\epsilon = 5\%$  are chosen, the power at 96% must be at least 95%. In Table 4, it is seen that the required sample size is between 40 and 50. Therefore, a sample size 50 is adequate. (Exact calculation can be performed using the techniques of the previous section.)

It should be noted that the choice of p need not be made independently of n. A more useful procedure would be for the experimenter to consult the tables and choose n by examining the effect that an increased sample size has on the power (or Type II error). In this way, the sample size could be determined with the knowledge of how much power the sample size

"buys" as compared to a different sample size.

Another example was suggested by Guenther [4]. He considered several hypothesis testing situations in which the statistic is distributed as a (central) t random variable under the null hypothesis, and as a noncentral t under the alternative hypothesis. One of the situations considered is where inferences are being made about the mean of a normal distribution. He determined the sample size by specifying the power when the difference between the mean under the null hypothesis and the mean under the alternative is expressed in quantiles. This result has been extended in this report to include the case where the inference is to be made about any given quantile, not necessarily the mean, of a normal distribution.

### IV. SUMMARY

In this technical report, tables for the power of a one-sided statistical hypothesis test are presented for the situation in which the statistic is distributed as a noncentral t under both the null and alternative hypothesis. Specifically, power and sample size problems are considered for a one-sided tolerance limit and for a variables sampling plan. Examples are also included to illustrate how these tables can be used in hypothesis testing situations and for determining sample size requirements in some estimation procedures.

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