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CINCINNATI UNIV OH DEPT OF ENGINEERING SCIENCE
A CRITICAL EVALUATION OF COMPUTER SUBROUTINES FOR SOLVING STIFF--ETC(U)
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A CRITICAL EVALUATION OF
COMPUTER SUBROUTINES FOR
SOLVING STIFF DIFFERENTIAL EQUATIONS

Dennis C. Krinke
and
Ronald L. Huston

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I. INTRODUCTION

The integration of initial valued simultaneous differential equations commonly occurring in models of large, complex mechanical systems (for example, human body/crash victim models, finite-segment structural system models, and large vibrating system models) has been shown to be costly in both CPU time and "turn-around" time. Indeed, developers of such models have found the efficiency of the differential equation integrators to be the most critical aspect of a model's overall efficiency [1,2,3]. Hence the search for efficient integrating subroutines or "solvers" has been long standing and is continuing.

Shampine, Watts, and Davenport [4] have made an extensive evaluation of computer codes for "nonstiff" differential equations. They suggest, however, that there are special problems which arise in the solution of "stiff" differential equations.¹ It has been observed by Huston and Hessel [5] that the differential equations of large mechanical system models are frequently stiff. Hence, there is both academic as well as utilitarian interest in a critical, comparative evaluation of the commonly used and commonly available solvers as applied to stiff equations.

Solution time and accuracy are the primary concerns when solving the differential equations of large mechanical system models. Hence,

¹The following section of the report contains a definition of "stiffness" as associated with differential equations.

it was decided to test the available solvers on equation's where exact analytical solutions were available. However, the derivative functions (that is, "the right-hand side") of the equation for system models are generally significantly more complex than the corresponding functions for test equations for which exact solutions are known. Consequently, the subroutine which evaluates the derivative functions for system models consumes considerably more CPU time. Therefore, a measure of the efficiency of a differential equation solver is the number of function calls it needs to make to the derivative evaluating subroutine to integrate the equations while holding a given accuracy. Indeed, this is probably a better measure of the potential efficiency of a solver than the actual CPU time used to solve test equations. Thus, in the test cases considered herein, both CPU time and number of function calls are used for comparison of the solvers.¹

The balance of this report is divided into six sections with the next section providing definitions of "stiffness". This is followed in the next three sections by a description of the subroutines tested, the test systems, and the test procedures. The final two sections contain the results and conclusions of the tests. Recommendations for further study are presented in the final section. Finally, an outline of the analytical solution of one of the test systems, together with a listing of the subroutines of the solvers tested are given in the Appendices.

¹On one occasion, a program was run twice without modification and even though all other results were exactly the same, the CPU times differed by 6%. Apparently the time measurement is not as reproducible as other computer operations. Therefore when comparing these values, it is suggested that one should not expect them to be more than 5% accurate.

II. DEFINITION OF STIFFNESS

Two definitions of "stiffness" appear in literature. One defines a "stiff" linear system of differential equations as one which has widely separated eigenvalues or time constants [6,7,8,9,10]. The other associates "stiffness" with the presence of diverging exponential terms which exist in the general solution but happen to have zero coefficients in the actual solution due to the particular choice of initial conditions [11,12,13]. It is not clear that these definitions are equivalent; hence, systems which are best described by the first definition will be said to have "Type 1 stiffness" and systems which are best described by the second will be said to have "Type 2 stiffness".

Systems with Type 1 stiffness are expensive to integrate since a transient portion of the solution, which has long since decayed, prevents an increase in stepsize even though the solution at that point may be quite smooth [10,9].

Systems with Type 2 stiffness are difficult to integrate because algorithm approximation, roundoff and truncation error introduce non-zero coefficient values to the divergent exponential terms. Although these coefficients may be small, the exponential term can still grow to be large in the interval of integration [11,13]. This can, in turn, greatly reduce the accuracy of the solution.

III. SOLVER SUBROUTINE DESCRIPTIONS

Table 1. summarizes the subroutines tested and the numerical methods of each. The only subroutines tested were those that were believed to be generally available.

All of the subroutines are written in FORTRAN and are compatible with the AMDAHL 470 in use at the University of Cincinnati. DRKGS and DHPCG are interval oriented, while DVOGER, DREBS, and RK45 are step oriented. RK45 uses a constant stepsize, but all of the others use automatic stepsize adjustment. All of the routines were coded in double precision.¹

Subroutine Name	Source	Method
DRKGS	[14]	Fourth Order Runge-Kutta
DHPCG	[14]	Hamming Predictor-Corrector
DVOGER(ADAMS)	[15]	Adams Predictor-Corrector
DVOGER(GEAR)	[15]	Gear Predictor-Corrector
DREBS	[15]	Modification of Bulirsch-Stoer ALGOL Routine DESUB
RK45	[16]	Sixth Order Runge-Kutta

Table 1. Solver Subroutine Summary

DRKGS uses a fourth order Runge-Kutta method (as modified by Gill) [14]. Some pertinent characteristics of DRKGS are as follows:

¹RK45 was obtained in single precision, but was modified to use double precision for the test runs.

- (1) Local error estimation is accomplished by comparing the solution computed in two steps of stepsize h to the solution obtained in one step of stepsize $2h$;
 - (2) Separate error tolerances are required for each function in the system;
 - (3) The maximum stepsize is also used for the initial stepsize and the minimum stepsize is 2^{-10} of this value¹;
- and (4) An output subroutine which is called after every step is required and is expected to perform all output duties.

DHPCG and DRKGS have been written to be easily interchanged. (The parameter lists are all identical.) To change from one subroutine to the other requires only a change in the dimension of a work array. However, DHPCG uses a completely different algorithm, that is, a Hamming predictor-corrector method [14], with a fourth order Runge-Kutta technique is used to generate the starting values. Once again, local error estimation is accomplished by comparing the solution obtained in one step of stepsize h to that obtained in two steps of stepsize $h/2$ and the same limitations on minimum, initial, and maximum stepsize which exist for DRKGS, exist for DHPCG.

DVOGER [15] is a modification of the subroutine DIFSUB written by C.W. Gear [17]. This routine contains two methods:

¹For one of the tests, it was necessary to modify this in order to obtain a solution.

- (1) An Adam's predictor-corrector method of variable order and stepsize which is intended for use with nonstiff systems;
- and (2) Gear's modification of the Adam's method which is intended for use with stiff systems [18].

The pertinent characteristics of DVOGER are:

- (1) Gear's method seeks to have not only the usual derivatives, but also the gradient of these functions. However, if it is not convenient to supply coding to evaluate this gradient, an option is provided that numerically approximates the gradient when given only the standard derivatives;
- (2) Only a single error tolerance is permitted which is applied to all functions;
- (3) Separate specifications of minimum, initial, and maximum stepsize are permitted;
- and (4) Since DVOGER computes only a single step at each call, the user has the flexibility of utilizing either absolute or relative error control.

DREBS [15] is a modification of the Bulirsch-Stoer ALGOL routine DESUB. Like DVOGER, DREBS permits only one error tolerance which is applied to all functions and both absolute and relative error specifications are possible. However, although minimum and initial stepsizes may be specified, a maximum stepsize cannot be specified.

RK45 [16] computes both a fourth and a fifth order Runge-Kutta approximation to the solution at every step and then uses Richardson's

method to achieve sixth order accuracy.¹ RK45 does not estimate the local error or adjust stepsize. Furthermore, the derivative evaluating subroutine must be named XKOTEQ (although this would be simple to modify if it were inconvenient). RK45 is step oriented; however, without error control, this is no more flexible than interval orientation would be.

¹The coefficients of the Runge-Kutta formulae have been optimized for maximum numerical stability.

IV. TEST SYSTEMS

Five systems of stiff differential equations were chosen to evaluate the solvers. As much as possible, systems were chosen in which the stiffness could be varied and the trend in solver efficiency observed. Systems 1, 2, and 3 contain Type 1 stiffness and systems 4 and 5 contain Type 2.

System 1 is presented in Reference [6] and represents a very simple system of differential equations that contain Type 1 stiffness. The system is:

$$\dot{\underline{y}} = [A] \underline{y} \quad (1)$$

where

$$[A] = \begin{bmatrix} -a & b \\ b & -a \end{bmatrix} \quad (2)$$

and

$$\underline{y}(0) = \begin{bmatrix} 0 \\ 2 \end{bmatrix} \quad (3)$$

An analytical solution is:

$$\underline{y}(t) = \begin{bmatrix} e^{-\alpha_1 t} & - e^{-\alpha_2 t} \\ e^{-\alpha_1 t} & + e^{-\alpha_2 t} \end{bmatrix} \quad (4)$$

where $\alpha_1 (= a-b), \alpha_2 (= a+b)$ are the eigenvalues of A. If α_1 and α_2 are nearly equal, then the system is nonstiff, but if α_1 and α_2 have widely separated values, the system is stiff.¹ The test was conducted with the parameters shown in Table 2 and Figure 1 illustrates the solution with $\alpha_1 = 1$ and $\alpha_2 = 5$.

α_1	α_2	a	b	Period of Integration
1	2	1.5	0.5	5
1	5	3.0	2.0	5
1	10	5.5	4.5	5
1	20	10.5	9.5	5
1	50	25.5	24.5	5
1	100	50.5	49.5	5
1	200	100.5	99.5	5
1	500	200.5	249.5	5
1	1000	500.5	449.5	5

Table 2. System 1 Test Parameters.

¹Interestingly, in this simple system, one can perform the transformation:

$$\underline{\omega} = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix} \underline{y}$$

which couples the equations. That is, in terms of $\underline{\omega}$, the system

becomes:
$$\dot{\underline{\omega}} = \begin{bmatrix} -\alpha_1 & 0 \\ 0 & -\alpha_2 \end{bmatrix} \underline{\omega} .$$

With the equations decoupled, they can be solved separately and the stiffness is removed from the system,

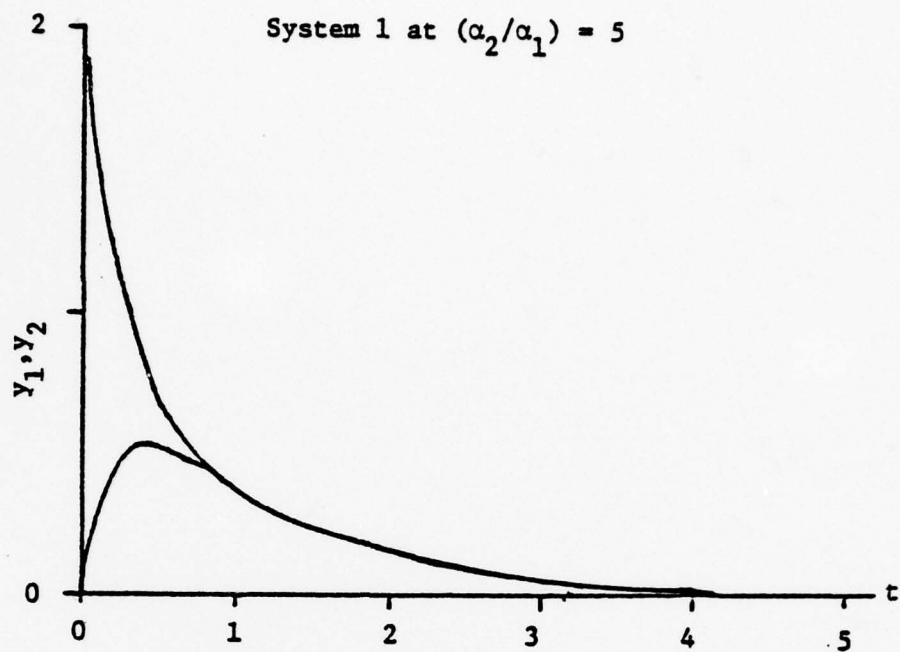


Figure 1. System 1 Exact Solution.

System 2 consists of the double mass-damper-spring system shown in Figure 2. Its governing equations are:

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \ddot{\mathbf{y}} + \begin{bmatrix} c_1+c_2 & -c_2 \\ -c_2 & c_2 \end{bmatrix} \dot{\mathbf{y}} + \begin{bmatrix} k_1+k_2 & -k_2 \\ -k_2 & k_2 \end{bmatrix} \mathbf{y} = \underline{\mathbf{0}} \quad (5)$$

Let the initial conditions be:

$$\mathbf{y}(0) = \begin{bmatrix} 1 \\ 1+k_1/k_2 \end{bmatrix} \quad (6)$$

$$\dot{\mathbf{y}}(0) = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad (7)$$

When the system is underdamped, the analytical solution¹ has the form:

$$y_1(t) = A_1 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_1) + A_2 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_2) \quad (8a)$$

and

$$y_2(t) = A_3 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_3) + A_4 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_4) \quad (8b)$$

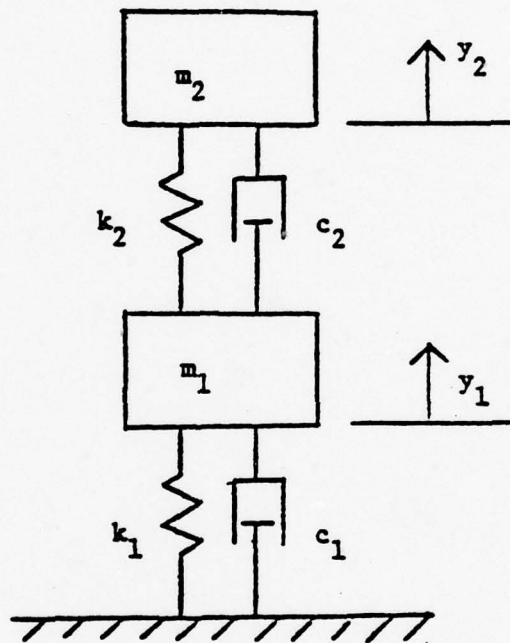


Figure 2. System 2. Model.

This solution contains damped exponential terms with time constants α_1 and α_2 . Hence, the problem is nonstiff if α_1 and α_2 are nearly equal, but has Type 1 stiffness if they have widely separated values. The system parameters m_1 , m_2 , c_1 , c_2 , k_1 , and k_2 were chosen to obtain the desired values of α_1 , α_2 , ω_1 , and ω_2 . The test was conducted with

¹The analytical solution to this system is derived in Appendix A.

the parameters shown in Table 3 and Figure 3 illustrates the solution with $\alpha_1 = 1$ and $\alpha_2 = 5$.

α_1	α_2	ω_1	ω_2	Period of Integration
1	2	2π	6π	5
1	5	2π	6π	5
1	10	2π	6π	5
1	20	2π	6π	5
1	50	2π	6π	5
1	100	2π	6π	5
1	200	2π	6π	5
1	500	2π	6π	5
1	1000	2π	6π	5

TABLE 3. System 2 Test Parameters.

System 2 at $(\alpha_2/\alpha_1) = 5$

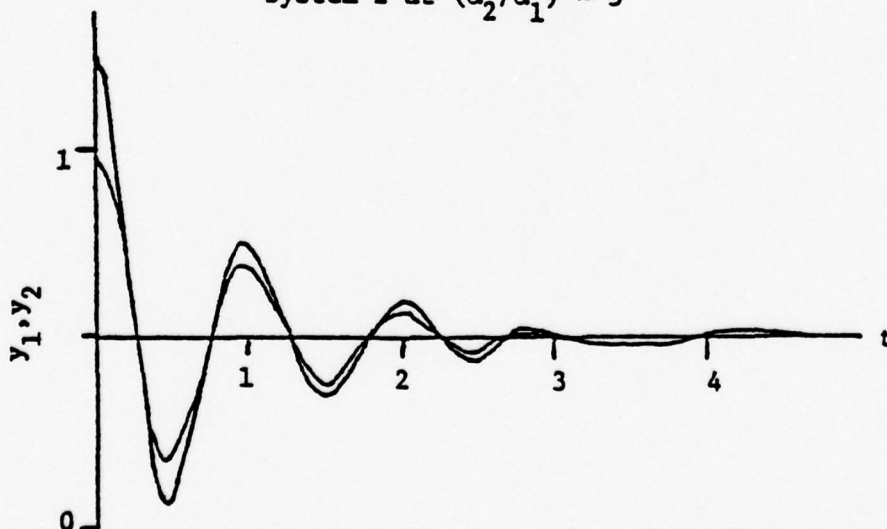


Figure 3. System 2 Exact Solution.

System 3 was obtained from References [6,17] and is attributed to F. T. Krogh. The equation

$$\dot{y} = -\beta y + y^2 \quad \text{with } y(0) = -1 \quad (9)$$

has the analytical solution:

$$y(t) = \frac{\beta}{1 - (1 + \beta)e^{\beta t}} \quad (10)$$

If one takes the system of four uncoupled equations:

$$\dot{y}_i = -\beta_i y_i + y_i^2, \quad (11)$$

$$y_i(0) = -1, \quad i = 1, 2, 3, 4 \quad (12)$$

and performs the transformation:

$$\underline{y} = [U] \underline{y} \quad (13)$$

where

$$[U] = \frac{1}{2} \begin{bmatrix} -1 & 1 & 1 & 1 \\ 1 & -1 & 1 & 1 \\ 1 & 1 & -1 & 1 \\ 1 & 1 & 1 & -1 \end{bmatrix} \quad (14)$$

then the system becomes

$$\dot{\underline{w}} = -[U] [B] [U] \underline{w} + [u] \underline{z} \quad (15)$$

with $w_i(0) = -1 \quad i = 1, 2, 3, 4 \quad (16)$

where $[B] = \begin{bmatrix} \beta_1 & 0 & 0 & 0 \\ 0 & \beta_2 & 0 & 0 \\ 0 & 0 & \beta_3 & 0 \\ 0 & 0 & 0 & \beta_4 \end{bmatrix} \quad (17)$

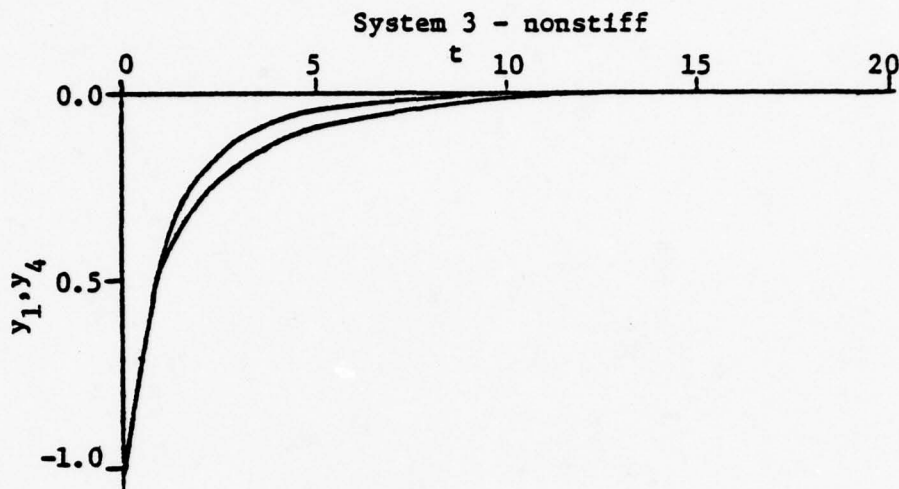
and $z_i = w_i^2 \quad (18)$

In this form, the equations are coupled and have Type 1 stiffness. Krogh suggests letting the values for the β_i 's be 0.1, 0.2, 0.3, and 0.4 for a nonstiff problem and 1000, 800, -10, and 0.001 for a stiff problem. The test was conducted with both sets of these values and Figure 4 illustrates the nonstiff solution. The period of integration was 20 for the nonstiff problem and was 1000 for the stiff problem.

System 4 is presented in Reference [11] and consists of the single equation:

$$\dot{y} = 5(y - t^2) \quad t \in (0, 5) \quad (19)$$

The general analytical solution is:



$$y(t) = C e^{5t} + t^2 + 0.4t + 0.08 \quad . \quad (20)$$

In the special cases where $y(0) = 0.08$, the value of C is exactly zero. However, algorithm approximation, roundoff and truncation errors cause the numerical solution to contain a ke^{5t} term. k must be very small indeed for ke^{5t} to be small in comparison to the exact solution, which is shown in Figure 5.

System 5 was a clear example of Type 2 stiffness but it lacked a means of varying that stiffness. System 5 does not obviously have Type 2 stiffness, but it behaves in sufficiently similar manner to suggest that it does.

System 5 models a central force orbit (two body problem with the mass of one body much larger than the other). Elliptical orbits

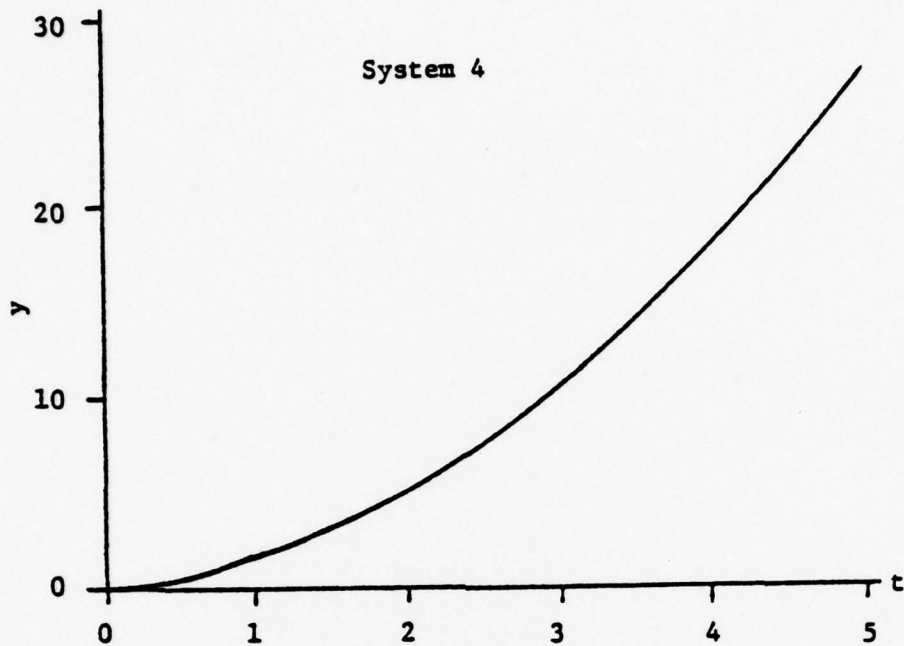


Figure 5. System 4 Exact Solution.

were chosen so that they would be periodic. The eccentricity of the ellipse was varied from moderately elliptical to highly "cigar-shaped" in order to change the amount of stiffness. The governing equations for this system are:

$$\ddot{r} = r\dot{\theta}^2 - \frac{GM}{r^2} \quad (21a)$$

$$\ddot{\theta} = -2\dot{r}\dot{\theta}/r \quad (21b)$$

where G and M are constants.

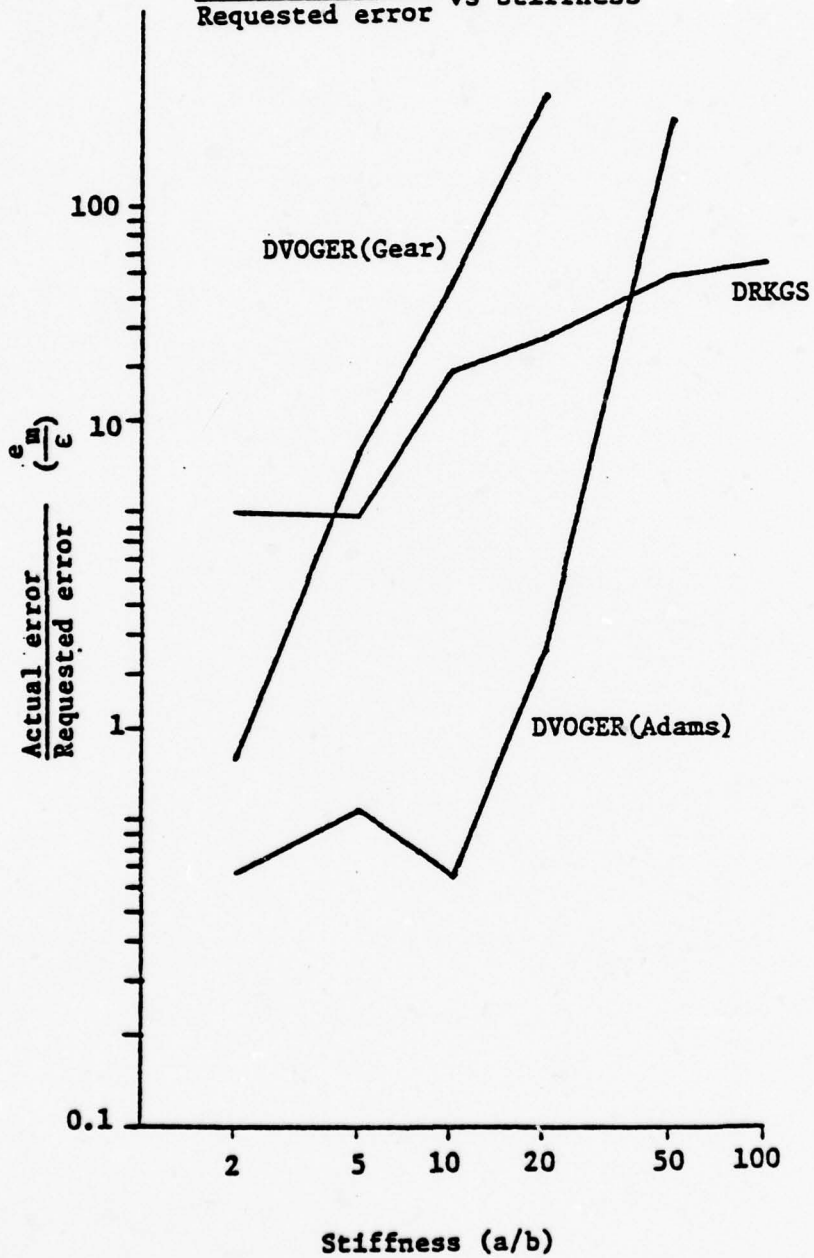
The initial conditions (which correspond to the apogee) are:

$$r(0) = a(1+e) \quad (22a)$$

$$\theta(0) = -\pi \quad (22b)$$

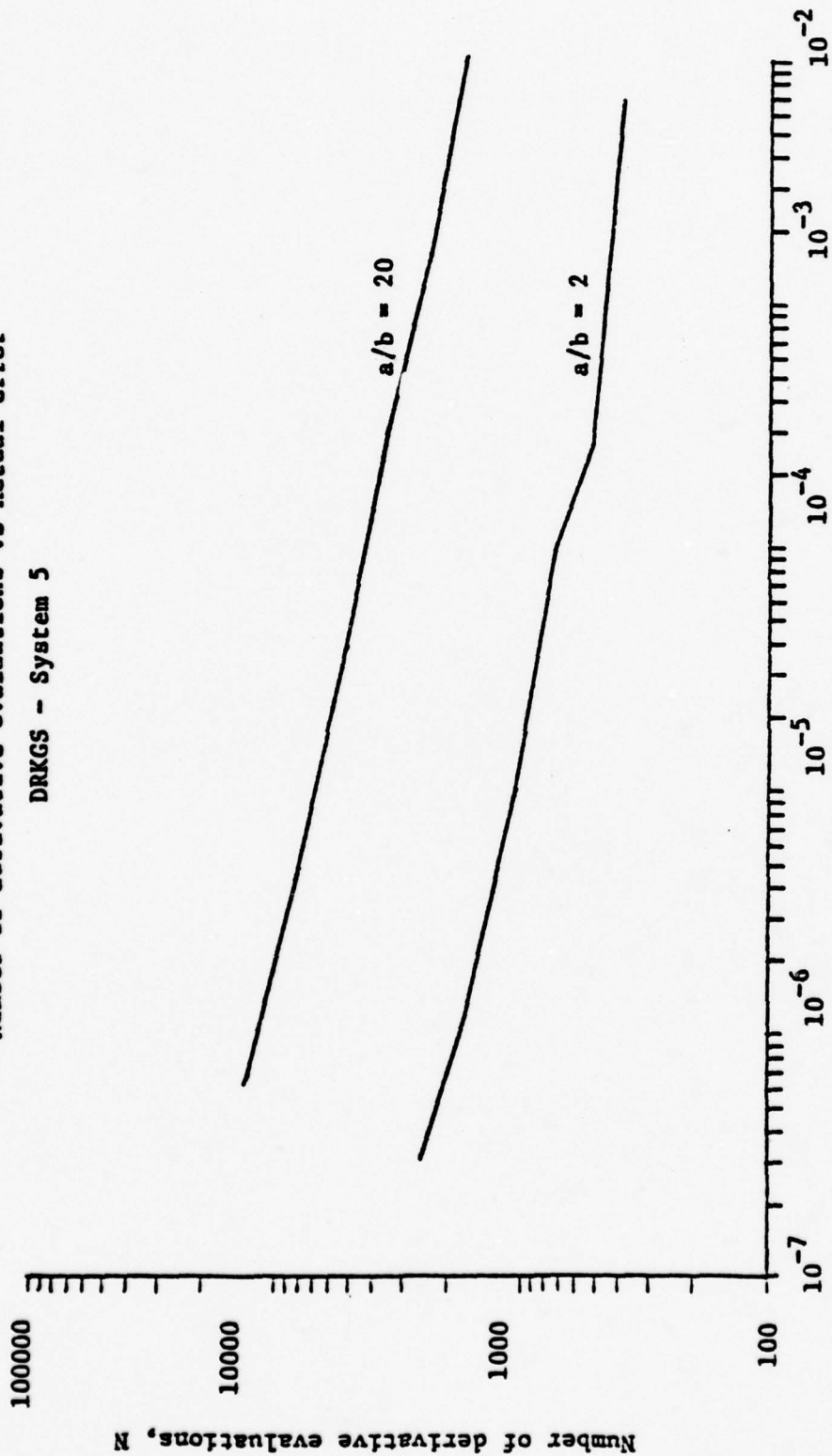
System 5

$\frac{\text{Actual error}}{\text{Requested error}}$ vs Stiffness



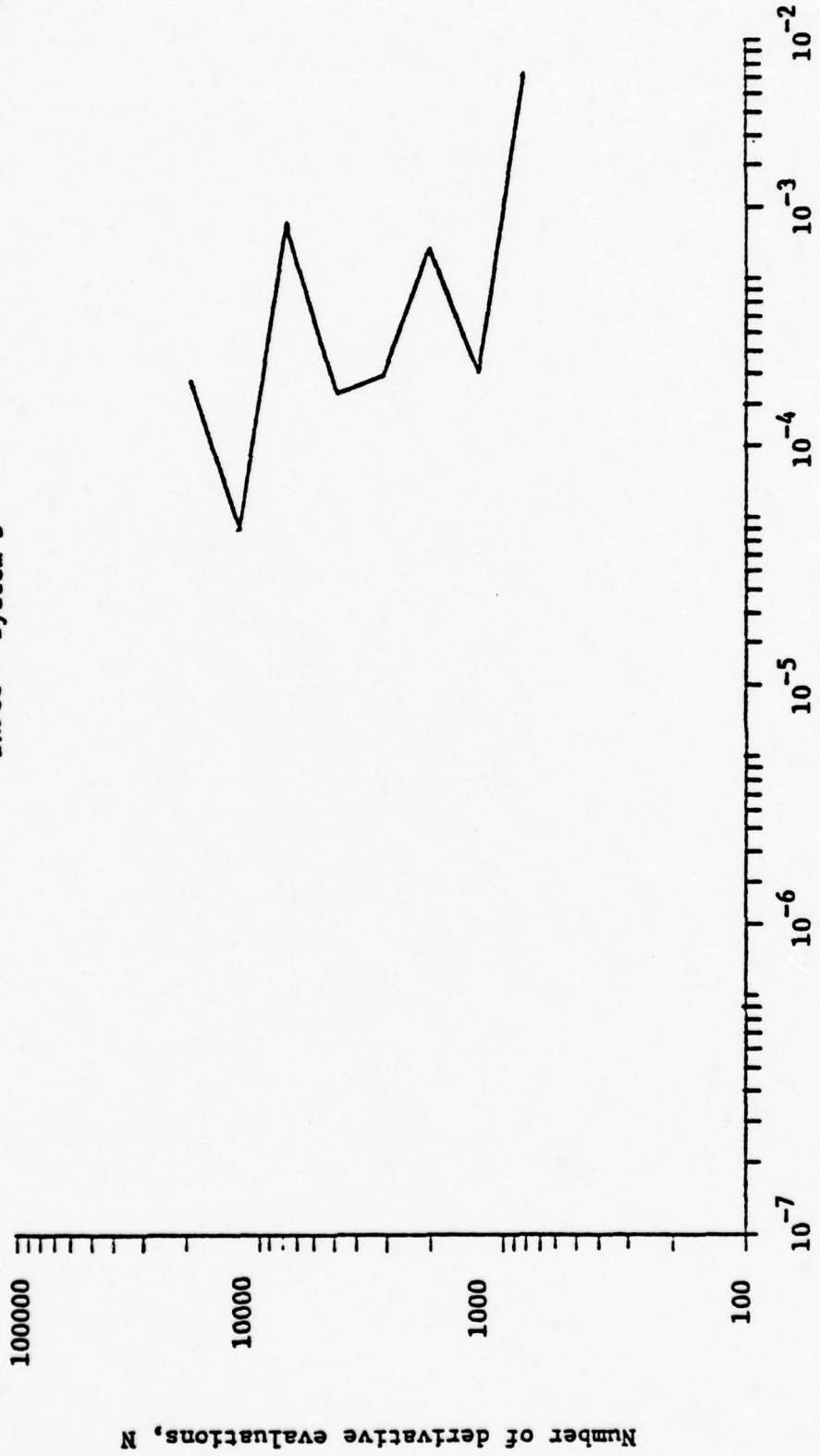
Graph 5. Accuracy vs. Stiffness - System 5.

Number of derivative evaluations vs Actual error
 DRKGS - System 5



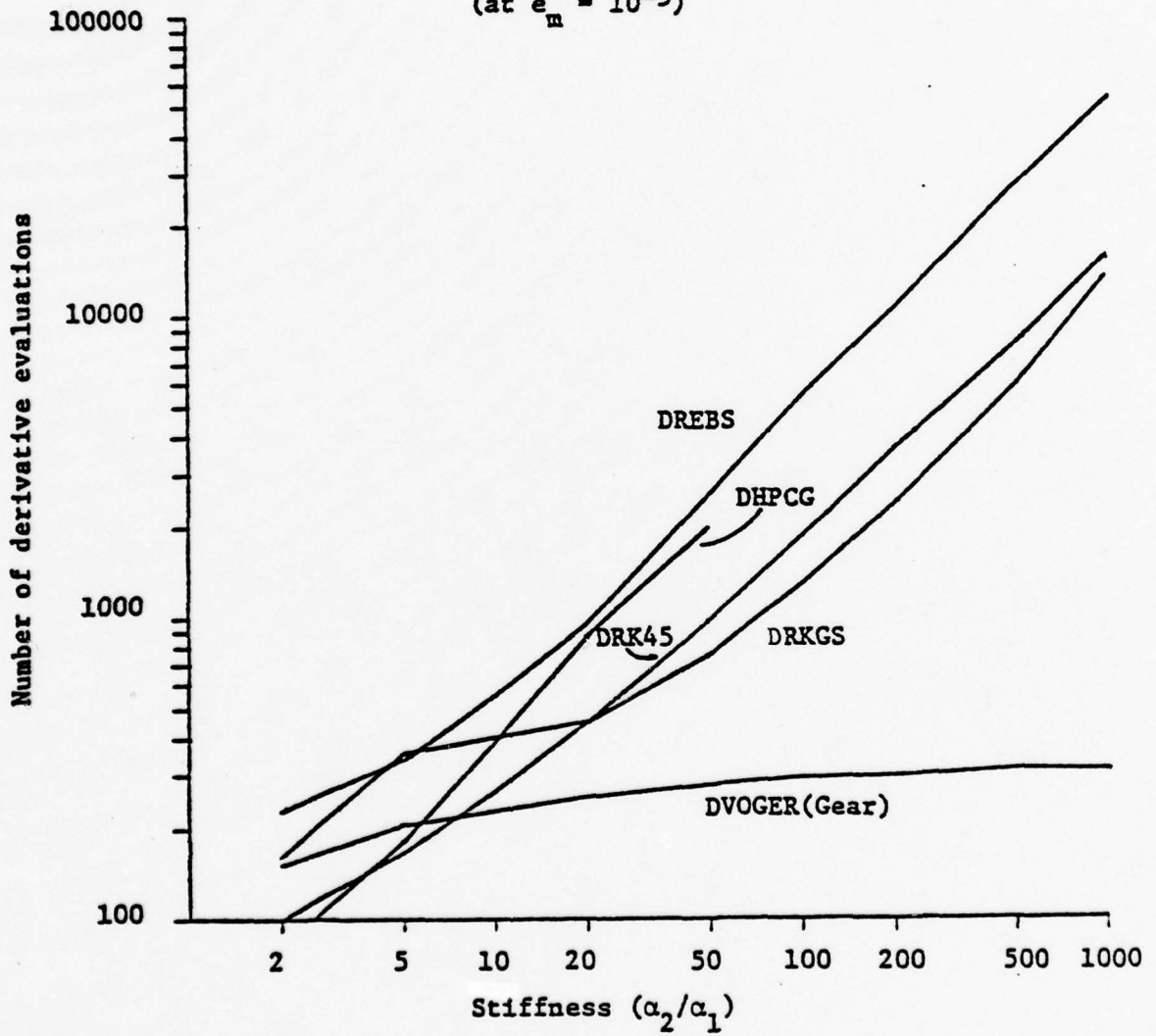
Graph 6. Effort vs. Accuracy - System 5 - DRKGS

Number of derivative evaluations vs Actual error
 DHPCC - System 5



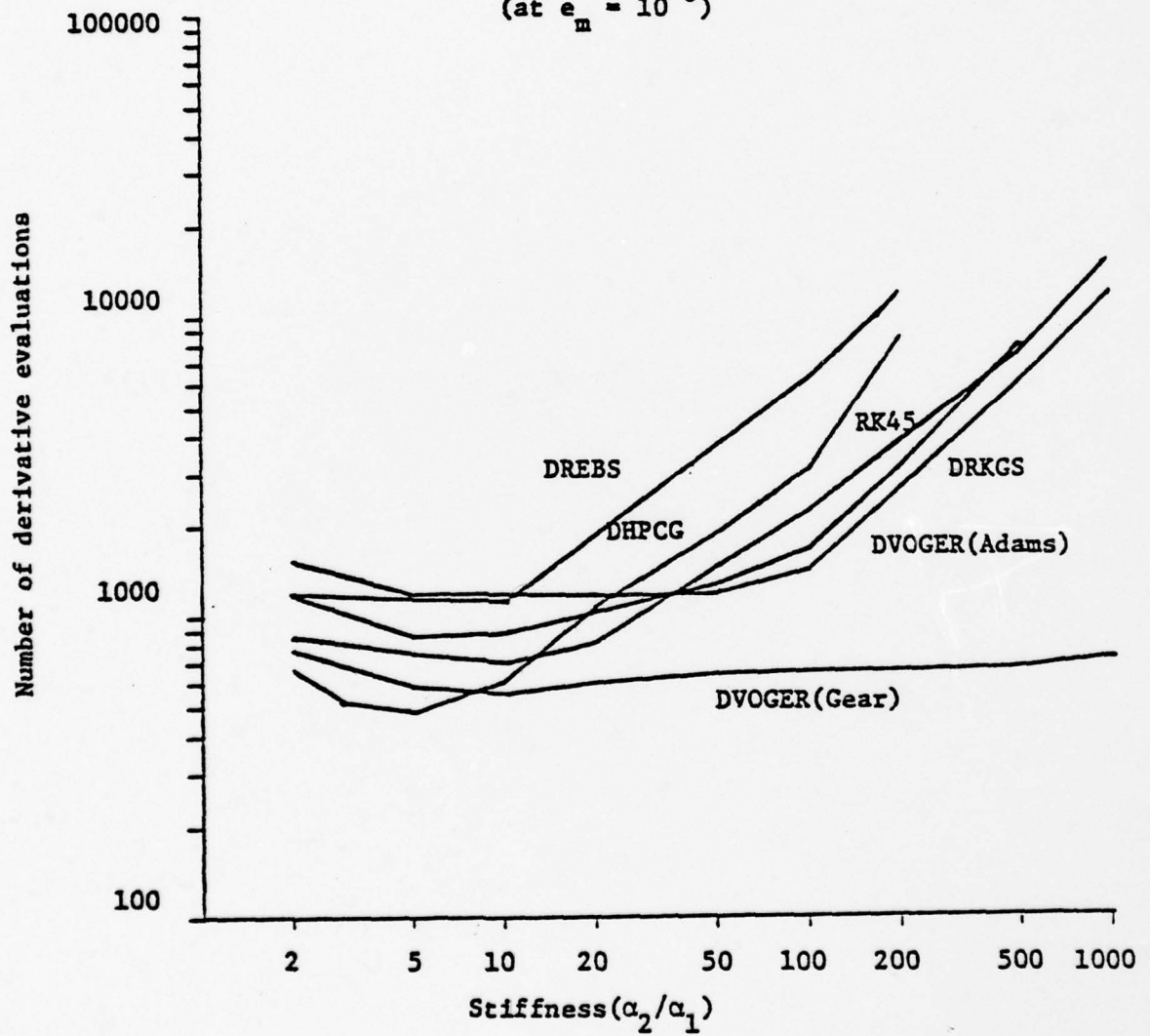
Graph 7. Effort vs. Accuracy - System 5 - EHPCC

System 1
Effort vs stiffness
(at $e_m = 10^{-5}$)



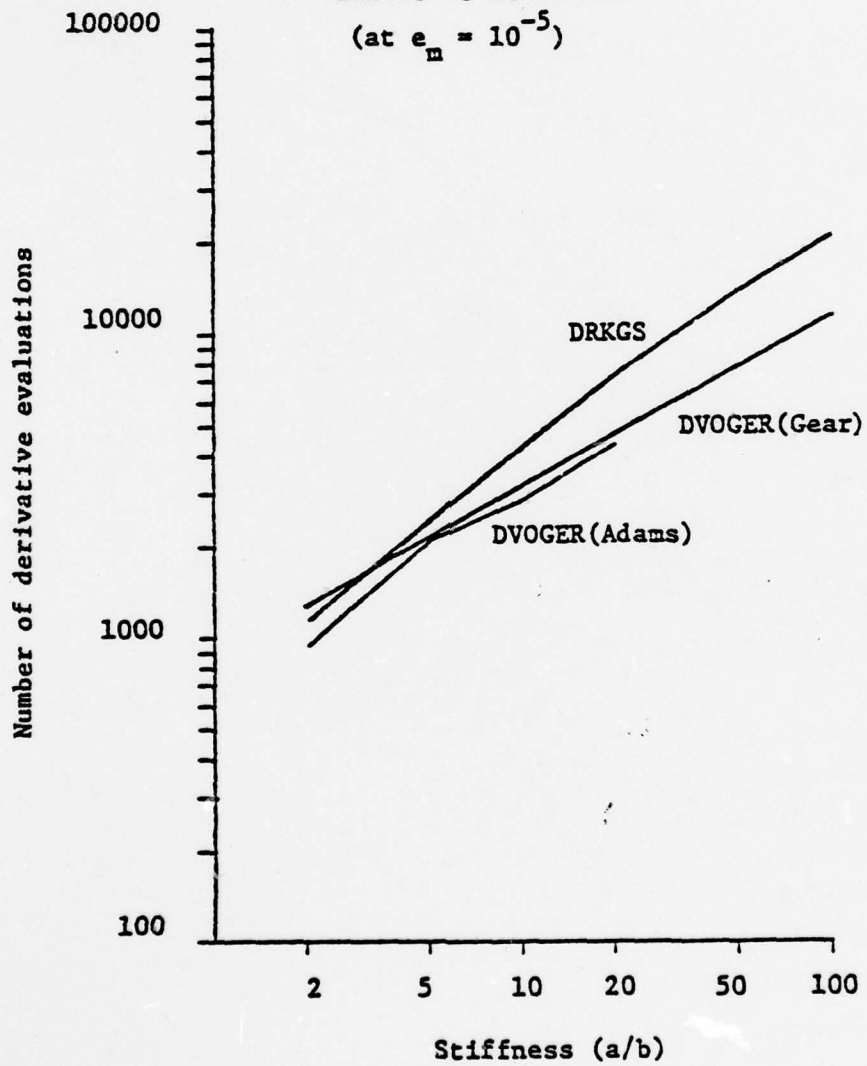
Graph 8. Effort vs. Stiffness - System 1.

System 2
 Effort vs Stiffness
 (at $e_m = 10^{-5}$)

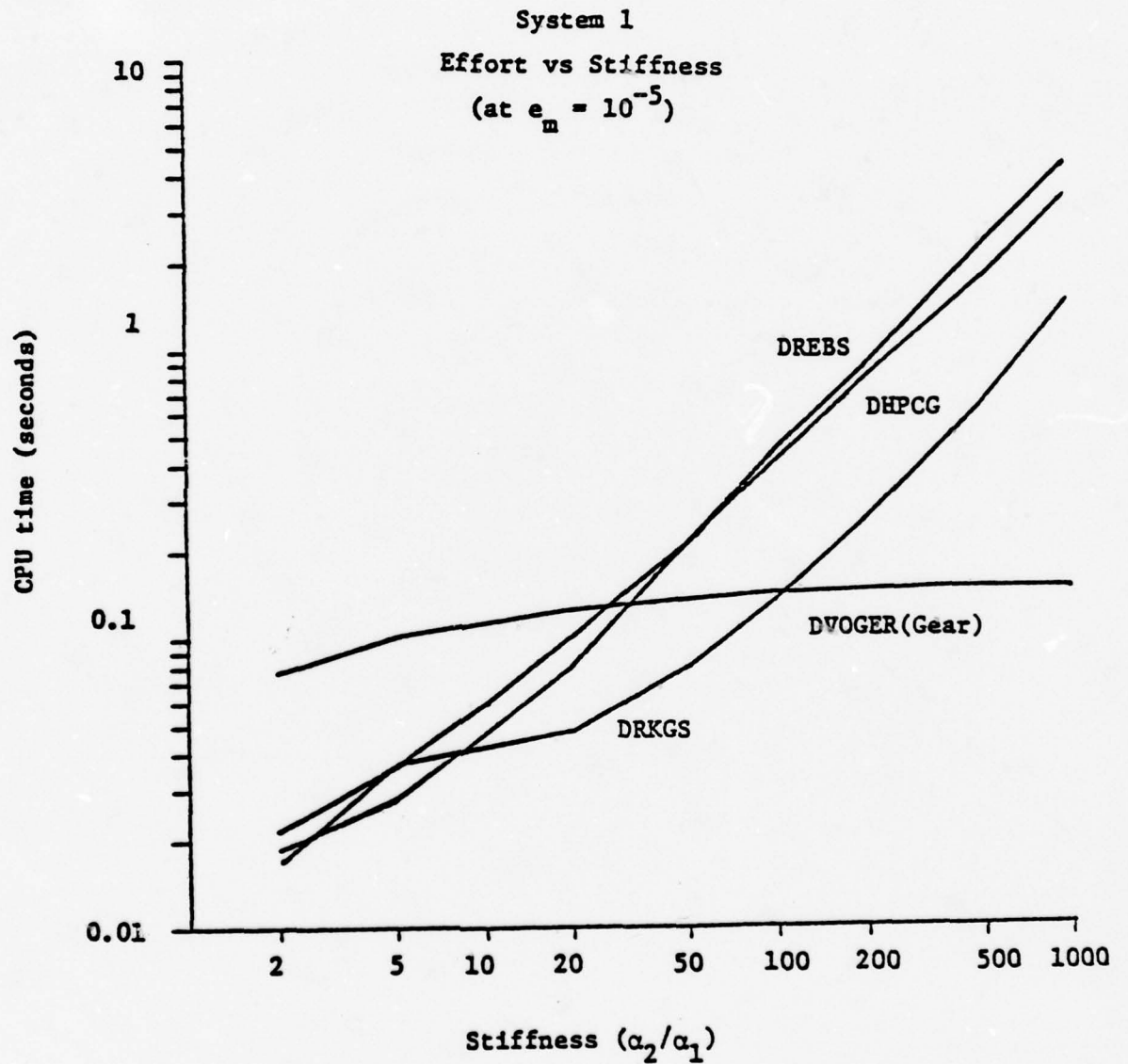


Graph 9. Effort vs. Stiffness - System 2.

System 5
Effort vs Stiffness
(at $e_m = 10^{-5}$)



Graph 10. Effort vs. Stiffness - System 5.



Graph 11. CPU Time vs. Stiffness - System 1.

VII. CONCLUSIONS AND RECOMMENDATIONS

Two significant and important conclusions can be drawn from this research effort. First, the solvers may not yield the requested accuracy when integrating a system with Type 2 stiffness. This suggests that the integration of such systems is not automatic at all. Rather, one must integrate every such system at least twice with different requested error tolerances (ϵ) and compare solutions. While such stiff systems are not as common as non-stiff systems, the user should be cautioned that they do exist.

Secondly, if a system has Type 1 stiffness and if the derivative evaluations are expensive, a routine using Gear's method (such as DVOGER) should be used. Gear's method was designed especially for stiff systems and it can be strikingly more efficient than the other solver routines.

Beyond this, experience with these subroutines prompts a few other remarks and opinions: First, even in system that were not stiff, the actual maximum error (e_m) frequently differed from that requested (ϵ) by factors of 20 or more. The subroutines would be more satisfying if their global error estimation could be improved.

Secondly, RK45 does not have automatic stepsize capability and was difficult to use. This emphasized the convenience of the automatic stepsize adjustment of the other subroutines. Even if one must solve every problem twice with them it is much better than making four or five runs to find the correct stepsize for RK45.¹

¹When the stepsize is too large for RK45, numerical instability occurs, leading to exponential overflow.

Third, the interval oriented format of DRKGS and DHPCG was convenient. Also, placing all of the output duties into a subroutine gives a modular property to the coding and further simplifies their use. However, the inability to separately specify the initial and maximum value of stepsize in these routines is disastrous to efficiency when looking for long time solutions in systems with decaying transients. Also, it is sometimes necessary to extend the permitted number of stepsize bisections to obtain solutions. Ten bisections may be a reasonable limit for single precision work, but forty or even fifty can be required for double precision integrations.

Finally, DVOGER and DREBS have no provision for the specification of separate error tolerances for the different functions in the system. While this presented no serious difficulty for this work, it could conceivably be important for a system with functions of greatly different magnitudes. The step oriented format of DVOGER and DREBS does however possess the potential for greater flexibility, particularly in error control. For example, if one suspected Type 2 stiffness, an exponential distribution of error per step would probably be better than a linear distribution.

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$$\dot{r}(0) = 0 \quad (22c)$$

$$\dot{\theta}(0) = 2\pi ab / (r^2(0)T) \quad (22d)$$

where a and b are respectively the major and minor semi-axes of the ellipse, e is the eccentricity ($\sqrt{1-(b/a)^2}$), and T is the period of the orbit. To achieve a period T, it is necessary to set $GM = a^3(2\pi/T)^2$.

The exact solution is simple only at $t = T$:

$$r(T) = r(0) \quad (23a)$$

$$\theta(T) = \pi \quad (24b)$$

The test was conducted with the parameters given in Table 4 and Figure 6 illustrates the solution for $a/b = 2$.

a	a/b	T
5	2	1
5	5	1
5	10	1
5	20	1
5	50	1
5	100	1

TABLE 4. System 5 Test Parameters.

Central force orbit with $a/b = 2$

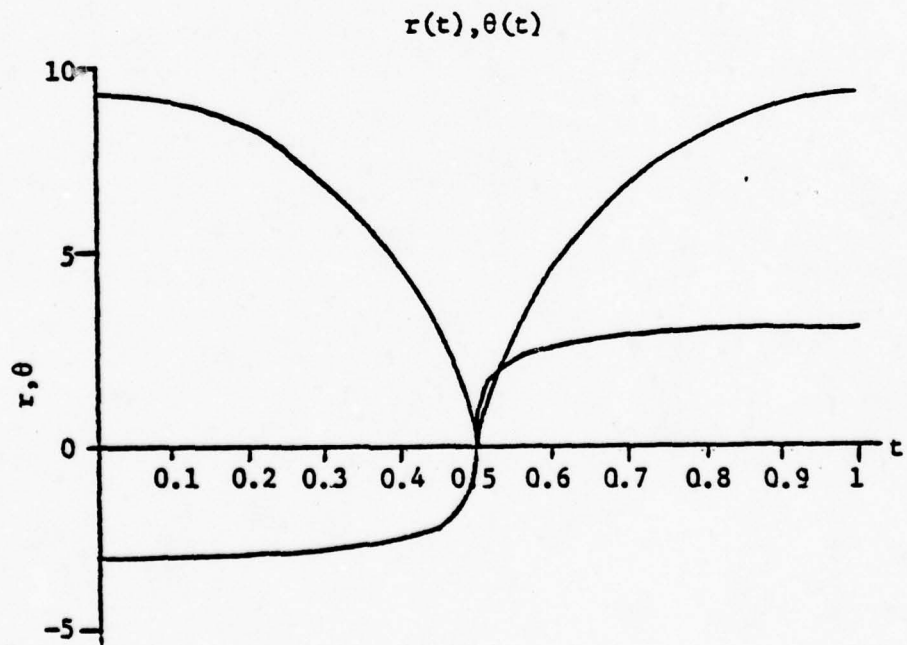
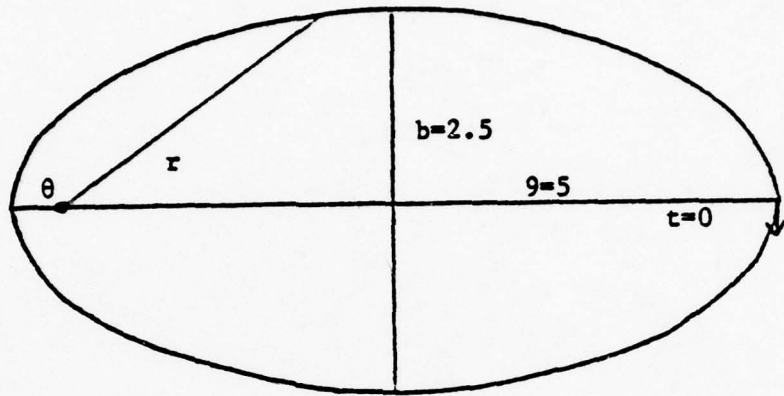


Figure 6. System 5 Exact Solution.

V. TEST PROCEDURE

In all of the tests, the number of derivative evaluating subroutine calls (N), the CPU time of integration, and the maximum occurring error (error_{\max}) were measured. (The solver DVOGER was used with both Adam's and Gear's methods and when it was used with Gear's method, the option was utilized in which the gradient of the derivative functions was evaluated numerically.)

All of the solvers, except RK45, require that an error tolerance (EPS) be given. For systems 1, 2, and 3, each integration was performed with $\text{EPS} = 10^{-3}, 10^{-4}, 10^{-5}, 10^{-6}$. For system 4, this was extended to 10^{-12} and for system 5 to 10^{-8} . RK45 was executed with a range of stepsizes which produced similar accuracy.

For the solvers which require a minimum stepsize, 10^{-15} of the interval value was used. This corresponds to about 140 units of round-off.

All tests were executed in double precision.

VI. RESULTS AND DISCUSSION

As mentioned previously, the primary interests are solver efficiency and accuracy. To discuss efficiency, it is desirable to consider the efficiency at a specified accuracy. Hence accuracy is discussed first.

The documentation of DRKGS and DHPCG state that the maximum global error, e_m , is usually of about the same magnitude as the specified error tolerance, ϵ , but the documentations of the other solvers do not state that. To assess the accuracy of the solvers e_m vs. ϵ was plotted for several cases. Graphs 1 and 2 are typical of these results and deal with systems 1 and 5 respectively. Error estimation is clearly not exact and it is somewhat disappointing that e_m differed by a factor of 20 or 50 from ϵ so frequently. From graph 1 alone, one might think that DHPCG is much superior to the other solvers in error estimation, but this is merely coincidence. There are other graphs where it appears to be poor and another appears to be good.

These graphs show only one value of stiffness and do not show if stiffness influences solver accuracy. Systems 1, 2 and 5 were specifically chosen because their stiffness could be varied in a desired manner. Graphs 3, 4 and 5 show explicitly how stiffness influences solver accuracy. These are graphs of (e_m/ϵ) vs. stiffness. Graphs 3 and 4 deal with systems 1 and 2 respectively and hence Type 1 stiffness. Graph 5 deals with System 5 and Type 2 stiffness. In Graph 3, it appears that DREBS and DRKGS lose accuracy with increasing stiffness,

but that behavior is not confirmed by Graph 4. The other routines are not clearly affected by Type 1 stiffness and DVOGER appears to be the least influenced. However, a look at Graph 5 clearly shows that Type 2 stiffness is different. As the stiffness of the problem increases, e_m grows much larger than ϵ .

Systems 3 and 4 contain Type 1 and Type 2 stiffness, respectively, and are even stiffer than the most stiff cases of systems 1, 2, and 5. Table 5 contains data pertinent to solver accuracy for systems 3 and 4. Note that e_m can be many orders of magnitude greater than ϵ .

(e_m/ϵ) for very stiff systems		
	SYSTEM 3 (Type 1)	SYSTEM 4 (Type 2)
DRKGS	-	1.2×10^{12}
DVOGER(GEAR)	4.6	3.1×10^{10}
DVOGER(ADAMS)	-	1.8×10^{10}
DREBS	-	1.3×10^8
DHPCG	-	2.3×10^8

Table 5. Error Ratio Data.

In every test integration, different solvers generated different accuracies, even when ϵ was constant and hence, it is probably misleading to compare solver effort at equal ϵ . Rather, it is probably more appropriate to compare solver effort at equal values of e_m . Graphs of N (the number of calls to the derivative evaluating subroutine) vs. e_m were prepared and estimates of N at a specific e_m were obtained. Usually these graphs were smooth and appeared to be hyperbolic (straight lines on log-log plots). Typical of these results is Graph 6 which pertains to System 5 and DRKGS. However, in some cases, these graphs were not smooth and Graph 7, concerning System 5 and DHPCG, shows such a result. In these cases, no attempt was made to estimate N .

In most of the tests, the solvers achieved 10^{-5} accuracy and this value of e_m was chosen to compare solver efficiencies. Graphs 8, 9, and 10 pertain to Systems 1, 2, and 5, respectively. They show how stiffness influences integration effort. The effect is quite striking. The systems in Graphs 8 and 9 both contain Type 1 stiffness. Almost every routine requires more effort for the integration as stiffness increases. However, DVOGER (Gear) was specifically designed for systems with this type of stiffness and it is relatively unaffected by Type 1 stiffness. System 5 in Graph 10 contains Type 2 stiffness and it is clear that this stiffness increases integration effort. No routine was much more efficient than another in this problem. Rather, the true test was whether they could integrate all of the cases. Only DRKGS and DVOGER (Gear) achieved solutions accurate to 10^{-5} for all stiffnesses.

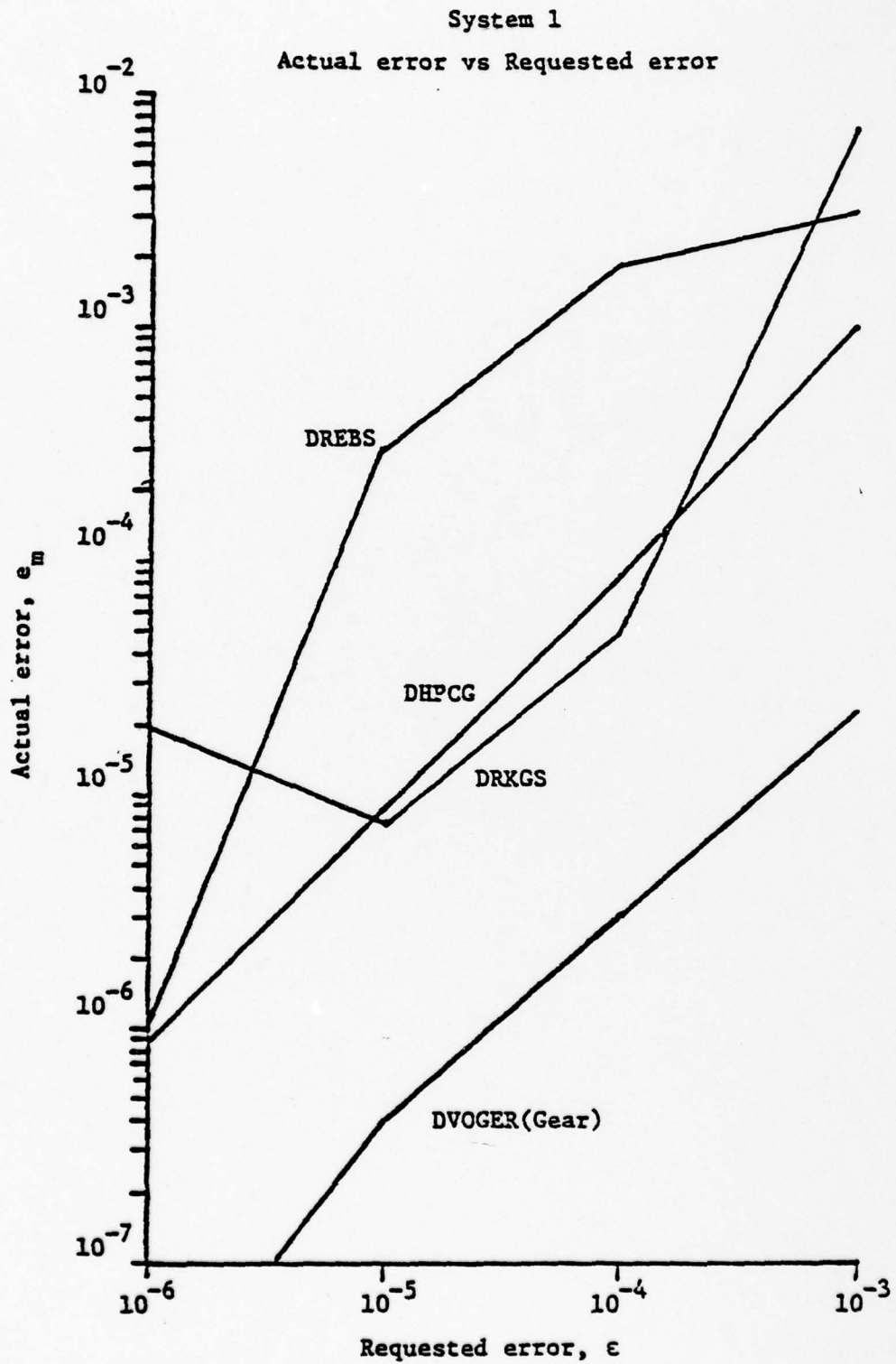
System 3, which had very much Type 1 stiffness could be solved to 10^{-5} accuracy only by DVOGER (Gear). The other routines took so many

function evaluations that apparently roundoff error limited their accuracy. System 4, which had very much type 2 stiffness, was solved by DRKGS, DRK45, DREBS and DHPCG to 10^{-3} relative error or better (10^{-2} was considered to be the minimum acceptable relative error). While DVOGER did not achieve this accuracy with absolute error control, it might perform better with relative error control. DHPCG achieved the best accuracy, about 10^{-6} .

The CPU times of integration, T, were measured but they primarily represent overhead (time spent in the solver subroutine rather than the derivative evaluating subroutine). The overhead per derivative evaluation was computed and these values are shown in Table 6. For systems where the derivative evaluations are simple, these values of (T/N) may be used to convert results from N to T
Graph 11 for the data from Graph 8 (System 1).

ROUTINE	CPU TIME PER DERIVATIVE SUBROUTINE CALL (μ-SEC)
DREBS	80
DRK45	103
DRKGS	106
DHPCG	220
DVOGER (ADAMS)	400
DVOGER (GEAR)	500

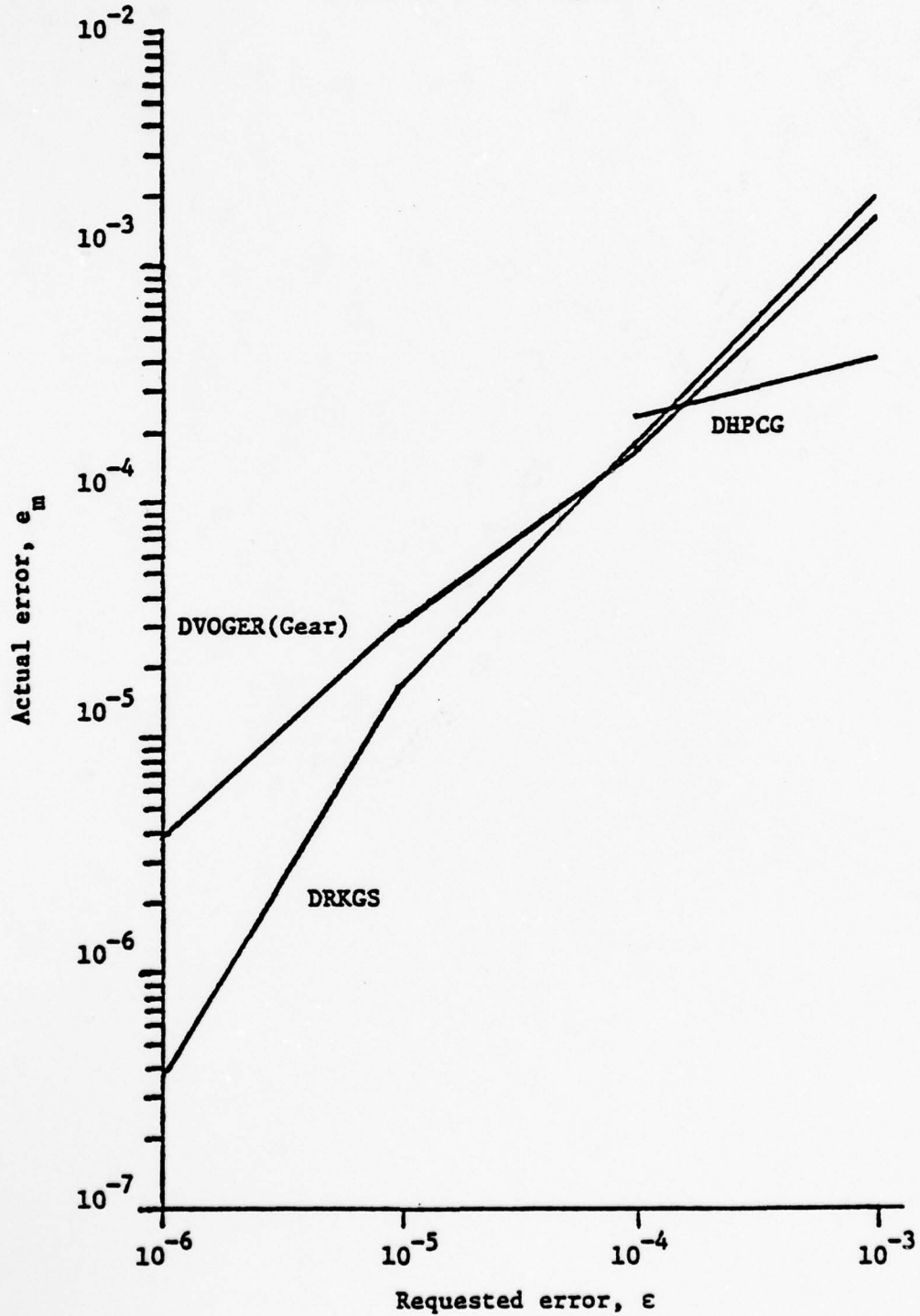
TABLE 6. CPU for Derivative Evaluation.



Graph 1. Actual Error vs. Requested Error - System 1.

System 5

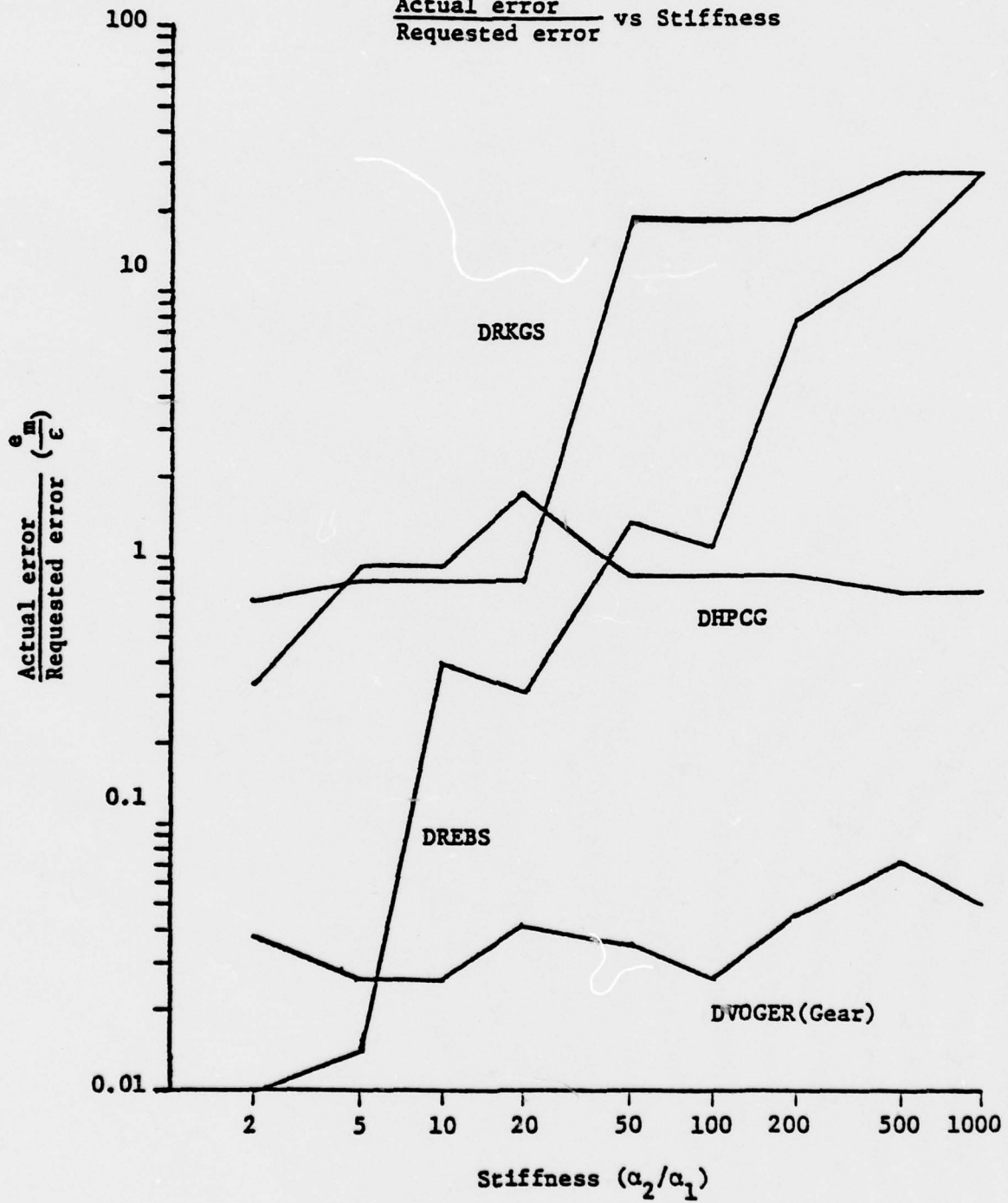
Actual error vs Requested error



Graph 2. Actual Error vs. Requested Error - System 5.

System 1

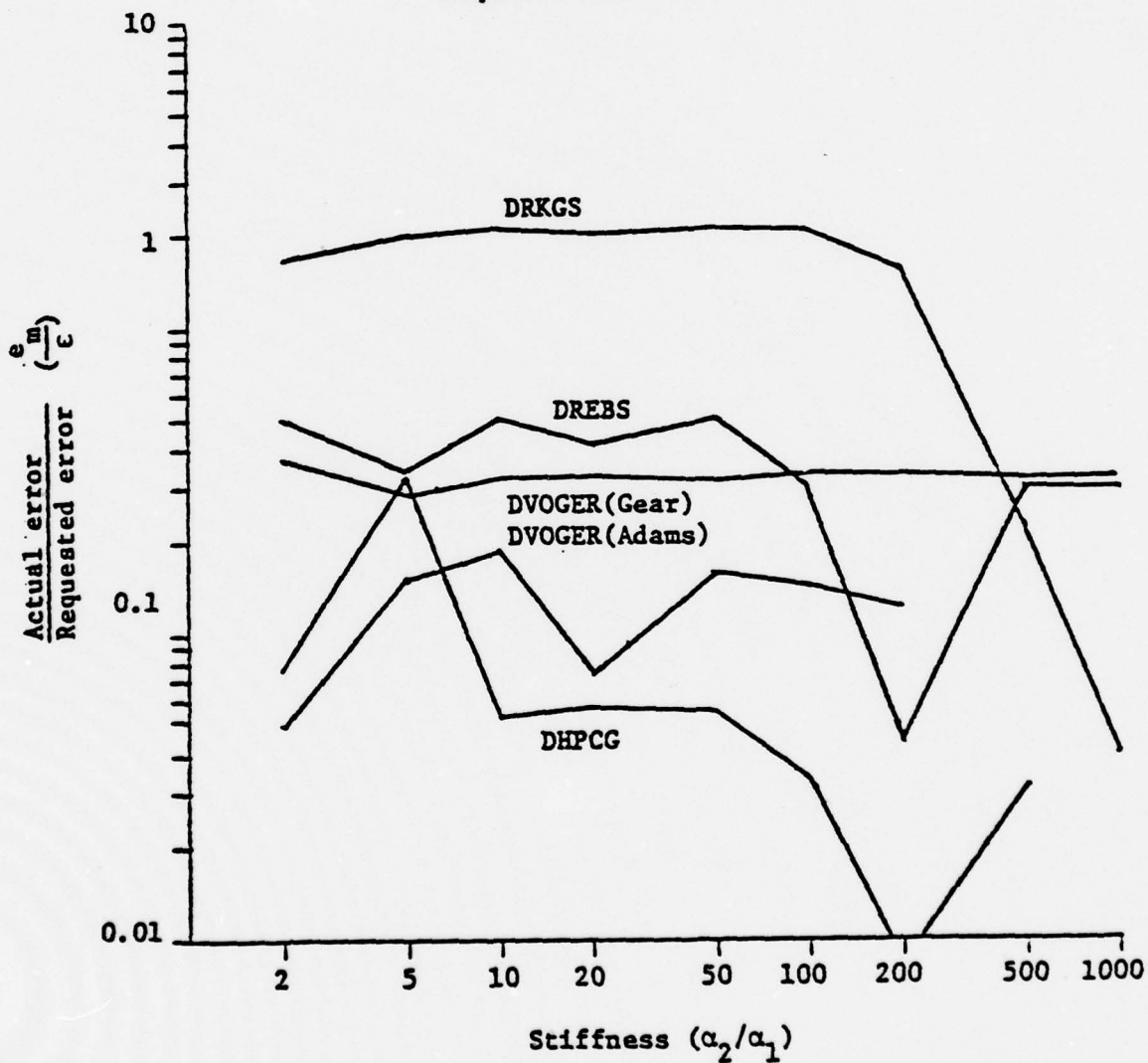
$\frac{\text{Actual error}}{\text{Requested error}}$ vs Stiffness



Graph 3. Accuracy vs. Stiffness - System 1.

System 2

$\frac{\text{Actual error}}{\text{Requested error}}$ vs Stiffness



Graph 4. Accuracy vs. Stiffness - System 2.

APPENDIX A

EXACT SOLUTION TO THE DOUBLE-MASS-SPRING DASHPOT SYSTEM (SYSTEM 2)

The governing differential equations of motion for the system are:

$$m_1 \ddot{y}_1 + (c_1 + c_2) \dot{y}_1 - c_2 \dot{y}_2 + (k_1 + k_2) y_1 - k_2 y_2 = 0 \quad (A1)$$

and

$$m_2 \ddot{y}_2 - c_2 \dot{y}_1 + c_2 \dot{y}_2 - k_1 y_1 + k_2 y_2 = 0 \quad (A2)$$

Taking the Laplace transform of these equations and solving for $y_1(s)$ and $y_2(s)$ leads to:

$$y_1(s) = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{d_4 (s^4 + d_3 s^3 + d_2 s^2 + d_1 s + d_0)} \quad (A3)$$

$$y_2(s) = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{d_4 (s^4 + d_3 s^3 + d_2 s^2 + d_1 s + d_0)} \quad (A4)$$

where:

$$a_0 = c_1 k_2 y_1(0) + m_1 k_2 \dot{y}_1(0) + m_2 k_2 \dot{y}_2(0) \quad (A5)$$

$$a_1 = (m_1 k_2 + c_1 c_2) y_1(0) + m_2 k_2 y_2(0) + m_1 c_2 \dot{y}_1(0) + m_2 c_2 \dot{y}_2(0) \quad (A6)$$

$$a_2 = [m_1 c_2 + m_2 (c_1 + c_2)] y_1(0) + m_1 m_2 \dot{y}_1(0) \quad (A7)$$

$$a_3 = m_1 m_2 y_1(0) \quad (A8)$$

$$b_0 = (c_1 k_2 - c_2 k_1) y_1(0) + c_2 k_2 y_2(0) + m_1 k_2 \dot{y}_1(0) + m_2 (k_1 + k_2) \dot{y}_2(0) \quad (A9)$$

$$b_1 = m_1 k_2 y_1(0) + [m_2 (k_1 + k_2) + c_1 c_2] y_2(0) + m_1 c_2 \dot{y}_1(0) + m_2 (c_1 + c_2) \dot{y}_2(0) \quad (A10)$$

$$b_2 = -m_1 c_2 y_1(0) + [m_1 c_2 + m_2 (c_1 + c_2)] y_2(0) + m_1 m_2 \dot{y}_2(0) \quad (A11)$$

$$b_3 = m_1 m_2 y_2(0) \quad (A12)$$

$$d_0 = k_1 k_2 / d_4 \quad (A13)$$

$$d_1 = (c_1 k_2 + c_2 k_1) / d_4 \quad (A14)$$

$$d_2 = [m_1 k_2 + m_2 (k_1 + k_2) + c_1 c_2] / d_4 \quad (A15)$$

$$d_3 = [m_1 c_2 + m_2 (c_1 + c_2)] / d_4 \quad (A16)$$

$$d_4 = m_1 m_2 \quad (A17)$$

To "invert" the Laplace transform, it is convenient to break the expressions for $y_1(s)$ and $y_2(s)$ into partial fractions. If the mass-damper-spring system is underdamped, then solutions of the form $e^{-\alpha t} \cos \omega t$ and $e^{-\alpha t} \sin \omega t$ will exist. The inverse Laplace transforms of these functions are:

$$e^{-\alpha t} \cos \omega t \Leftrightarrow \frac{s + \alpha}{(s + \alpha)^2 + \omega^2} \quad (A18)$$

$$\frac{e^{-\alpha t} \sin \omega t}{\omega} \Leftrightarrow \frac{1}{(s + \alpha)^2 + \omega^2} \quad (A19)$$

Hence, it is necessary to factor the fourth order denominator into two quadratic terms. This was performed numerically with a computer routine for every case. Since all cases are underdamped the roots consist of two complex conjugate pairs:

$$-\alpha_1 \pm \omega_1 i \Leftrightarrow (s + \alpha_1 - \omega_1 i)(s + \alpha_1 + \omega_1 i) = (s + \alpha_1)^2 + \omega_1^2 \quad (A20)$$

and

$$-\alpha_2 \pm \omega_2 \Leftrightarrow (s + \alpha_2 - \omega_2)(s + \alpha_2 + \omega_2) = (s + \alpha_2)^2 + \omega_2^2 \quad (\text{A21})$$

Hence:

$$d_4 y_1(s) = \frac{e_1(st\alpha_1) + e_2}{(st\alpha_1)^2 + \omega_1^2} + \frac{e_3(st\alpha_2) + e_4}{(st\alpha_2)^2 + \omega_2^2} \quad (\text{A22})$$

$$d_4 y_2(s) = \frac{f_1(st\alpha_1) + f_2}{(st\alpha_1)^2 + \omega_1^2} + \frac{f_3(st\alpha_2) + f_4}{(st\alpha_2)^2 + \omega_2^2} \quad (\text{A23})$$

where $e_1, e_2, e_3, e_4, f_1, f_2, f_3, f_4$ are determined by letting s approach $-\alpha_1 \pm \omega_1 i$ and $-\alpha_2 \pm \omega_2 i$. This is equivalent to defining Z_1, Z_2, Z_3 and Z_4 as:

$$Z_1 = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{(st\alpha_2)^2 + \omega_2^2} \quad \text{with } s = -\alpha_1 + \omega_1 i \quad (\text{A24})$$

$$Z_2 = \frac{a_3 s^3 + a_2 s^2 + a_1 s + a_0}{(st\alpha_1)^2 + \omega_1^2} \quad \text{with } s = \alpha_2 \pm \omega_2 i \quad (\text{A25})$$

$$Z_3 = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{(st\alpha_2)^2 + \omega_2^2} \quad \text{with } s = \alpha_1 \pm \omega_1 i \quad (\text{A26})$$

$$Z_4 = \frac{b_3 s^3 + b_2 s^2 + b_1 s + b_0}{(s + \alpha_1)^2 + \frac{1}{1}} \quad \text{with } s = \alpha_2 \pm \omega_s i \quad (\text{A27})$$

and then:

$$e_1 = \text{imag } Z_1 / \omega_1 \quad e_2 = \text{real } Z_1 \quad (\text{A28})$$

$$e_3 = \text{imag } Z_2 / \omega_2 \quad e_4 = \text{real } Z_2 \quad (\text{A29})$$

$$f_1 = \text{imag } Z_3 / \omega_1 \quad f_2 = \text{real } Z_3 \quad (\text{A30})$$

$$f_3 = \text{imag } Z_4 / \omega_2 \quad f_4 = \text{real } Z_4 \quad (\text{A31})$$

Finally, $y_1(s)$ and $y_2(s)$ can be "inverted", leading to the expressions:

$$y_1(t) = e^{-\alpha_1 t} \left[\frac{e_1}{d_4} \cos \omega_1 t + \frac{e_2}{d_4 1} \sin \omega_1 t \right] + e^{-\alpha_2 t} \left[\frac{e_3}{d_4} \cos \omega_2 t + \frac{e_4}{d_4 1} \sin \omega_2 t \right] \quad (\text{A32})$$

and

$$y_2(t) = e^{-\alpha_1 t} \left[\frac{f_1}{d_4} \cos \omega_1 t + \frac{f_2}{d_4 \omega_1} \sin \omega_1 t \right] \\ + e^{-\alpha_2 t} \left[\frac{f_3}{d_4} \cos \omega_2 t + \frac{f_4}{d_4 \omega_2} \sin \omega_2 t \right] \quad (\text{A33})$$

These expressions can be written in the more convenient form:

$$y_1(t) = A_1 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_1) + A_2 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_2) \quad (\text{A34})$$

$$y_2(t) = A_3 e^{-\alpha_1 t} \cos(\omega_1 t + \phi_3) + A_4 e^{-\alpha_2 t} \cos(\omega_2 t + \phi_4) \quad (\text{A35})$$

where :

$$A_1 = [e_1^2 + (e_2/\omega_1)^2]^{1/2}/d_4 \quad (\text{A36})$$

$$A_2 = [e_3^2 + (e_4/\omega_2)^2]^{1/2}/d_4 \quad (\text{A37})$$

$$A_3 = [f_1^2 + (f_2/\omega_1)^2]^{1/2}/d_4 \quad (\text{A38})$$

$$A_4 = [f_3^2 + (f_4/\omega_2)^2]^{1/2}/d_4 \quad (\text{A39})$$

$$\phi_1 = -\tan^{-1} (e_2/e_1\omega_2) \quad (\text{A40})$$

$$\phi_2 = -\tan^{-1} (e_4/e_3\omega_2) \quad (\text{A41})$$

$$\phi_3 = -\tan^{-1} (f_2/f_1\omega_1) \quad (\text{A42})$$

$$\phi_4 = -\tan^{-1} (f_4/f_3\omega_2) \quad (\text{A43})$$

It is possible to choose m_1 , c_1 , k_1 , m_2 , c_2 and k_2 to obtain various desired values of α_1 , α_2 , ω_1 and ω_2 . The required relationships are simplified if the product m_1m_2 is arbitrarily set to 1. Then the following four simultaneous nonlinear equations are obtained:

$$c_1 + 2c_2 = 2(\alpha_1 + \alpha_2) \quad (\text{A44})$$

$$k_1 + 2k_2 + c_1c_2 = \alpha_1^2 + \omega_1^2 + 4\alpha_1\alpha_2 + \alpha_2^2 + \omega_2^2 \quad (\text{A45})$$

$$c_1k_2 + c_2k_1 = 2[\alpha_1(\alpha_2^2 + \omega_2^2) + \alpha_2(\alpha_1^2 + \omega_1^2)] \quad (\text{A46})$$

$$k_1k_2 = (\alpha_1^2 + \omega_1^2)(\alpha_2^2 + \omega_2^2) \quad (\text{A47})$$

It is possible to solve these numerically for c_1 , c_2 , k_1 and k_2 (see Reference [19]). That is, let $\underline{y}(\tau)$ be functions such that:

$$\underline{y}(\tau) = \begin{bmatrix} y_1(\tau) \\ y_2(\tau) \\ y_3(\tau) \\ y_4(\tau) \end{bmatrix} \quad (\text{A48})$$

and let

$$\underline{y}(0) = \begin{bmatrix} 2\alpha_1 \\ \alpha_1^2 + \omega_1^2 \\ 2\alpha_2 \\ \alpha_2^2 + \omega_2^2 \end{bmatrix} \quad (\text{A49})$$

Further, let

$$\underline{F}(\underline{y}) = \begin{bmatrix} y_1 + 2y_3 \\ y_2 + 2y_4 + y_1y_3 \\ y_1y_4 + y_3y_2 \\ y_2y_4 \end{bmatrix} - \begin{bmatrix} y_1(0) + y_3(0) \\ y_2(0) + y_1(0)y_3(0) + y_4(0) \\ y_1(0)y_4(0) + y_3(0)y_2(0) \\ y_2(0)y_4(0) \end{bmatrix} \quad (\text{A50})$$

Thus

$$\underline{F}(0) = \begin{bmatrix} y_3(0) \\ y_4(0) \\ 0 \\ 0 \end{bmatrix} \quad (\text{A51})$$

and

$$\underline{\nabla F} = \begin{bmatrix} 1 & 0 & 2 & 0 \\ y_3 & 1 & y_1 & 2 \\ y_4 & y_3 & y_2 & y_1 \\ 0 & y_4 & 0 & y_2 \end{bmatrix} \quad (\text{A52})$$

Finally, let

$$\underline{F}(\tau) = (1 - \tau)\underline{F}(0) \quad (\text{A53})$$

Then

$$\underline{F}(1) = 0 \quad (\text{A54})$$

and

$$\dot{\underline{F}}(\tau) = \underline{\nabla F} \dot{\underline{Y}} = -\underline{F}(0) \quad (\text{A55})$$

Hence,

$$\dot{\underline{Y}} = -[\underline{\nabla F}]^{-1}\underline{F}(0) \quad (\text{A56})$$

Equations (A56) form a system of four first order differential equations whose solution $y(\tau)$ evaluated at $\tau = 1$, provide the desired values of c_1 , k_1 , c_2 , and k_2 .

APPENDIX B

Solver Subroutine Listings

```

1  SUBROUTINE DRK45(X,XDOT,I,H,M)
2  IMPLICIT REAL*8 (A-H,O-Z)
3  RUNGE-KUTTA OPTIMAL COEFFS ROUTINE. TRUNCATION ERROR = H**6.
4  H = STEP SIZE
5  M = NUMBER OF FIRST ORDER DIFFERENTIAL EQUATIONS
6  I = INDEPENDENT VARIABLE
7  X IS THE STATE VECTOR AND XDOT(T+H) ARE RETURNED
8  THE STATE DERIVATIVE AND XDOT(T) WHICH IS THE SUBROUTINE IN
9  RK45 CALLS XDOTEQ(X,XDOT,T) WHICH IS THE SUBROUTINE IN
10 WHICH THE M FIRST ORDER EQUATIONS ARE INPUT..
11 XDOTEQ INPUT IS AS FOLLOWS
12 XDOT(1) = F(X,T)
13 XDOT(2) = G(X,T)
14 ETC.
15
16 DIMENSION X(M),XDOT(M),XNEW(20),A(6),F(6,20),SAVE(20),B(6,5)
17 DATA XSAVE(20)
18 IF(KOUNT.GT.0) GO TO 5
19 KOUNT=1
20 A(1)=0.2D0
21 A(2)=.3D0
22 A(3)=.5D0
23 A(4)=.6D0
24 A(5)=1.0D0
25 A(6)=1.0D0/12.D0
26 C1=59.5D0/594.D0
27 C3=275D0/693.D0
28 C4=125D0/513.D0
29 C5=-1.8D0/14.D0
30 C6=2592.D0/7733.D0
31 H(2,1)=.2D0
32 H(3,1)=3.D0/40.D0
33 H(3,2)=9.D0/40.D0
34 B(4,1)=.3D0
35 B(4,2)=.9D0
36 B(4,3)=1.2D0
37 B(4,4)=1.D0/54.D0
38 H(5,1)=2.5D0
39 H(5,2)=7D0/27.D0
40 H(5,3)=35D0/27.D0
41 B(6,1)=-473.D0/10368.D0
42 B(6,2)=-1595.D0/1728.D0
43 B(6,3)=-34595.D0/54432.D0
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B(6,4)=38665, D0/62208, D0
H(6,5)=7733, D0/145152, D0
5 DO 4 J=1, M
4 XSAVE(J)=X(J)
  IF(K, EQ, 1) GO TO 30
  N=K-J
  DO 20 J=1, M
  SAVE(J)=0, 0D0
  DO 40 LAM=1, L
  SAVE(J)=SAVE(J)+B(K, LAM)*F(LAM, J)
  40 SAVE(J)=H*SAVE(J)
  20 DJ 50 N=1, M
  50 XNEW(N)=XSAVE(N)+SAVE(N)
  TNEW=T+A(K)*H
  CALL XDOTEQ(XNEW, XDOT, TNEW)
  DO 60 J=1, M
  F(K, J)=XDOT(J)
  60 CONFJUE
  10 DU 70 J=1, M
  70 X(J)=XSAVE(J)+H*(C1*F(1, J)+C3*F(3, J)+C4*F(4, J)+C5*F(5, J)+
  C6*F(6, J))
  I=I+H
  RETURN
END

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CC
SUBROUTINE DRKGS(PRMT, Y, DERY, NDIM, IHLF, FCT, OUTP, AUX)
PURPOSE
TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY DIFFERENTIAL
EQUATIONS WITH GIVEN INITIAL VALUES.
USAGE
CALL DRKGS (PRMT, Y, DERY, NDIM, IHLF, FCT, OUTP, AUX)
PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.
DESCRIPTION OF PARAMETERS
PRMT - DIMENSION INPJT AND OUTPUT VECTOR WITH
DOUBLE PRECISION INPUT OR EQUAL TO 5, WHICH
DIMENSION GREATER THAN OR EQUAL TO 5, WHICH
SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF
ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN
OUTPUT SUBROUTINE (FORNISHED BY THE USER) AND
SUBROUTINE DRKGS. EXCEPT PRMT(5) THE COMPONENTS
ARE NOT DESTROYED BY SUBROUTINE DRKGS AND THEY ARE
PRMT(1) - LOWER BOUND OF THE INTERVAL (INPUT),
PRMT(2) - UPPER BOUND OF THE INTERVAL (INPUT),
PRMT(3) - INITIAL INCREMENT OF THE INDEPENDENT VARIABLE
(INPJT),
PRMT(4) - UPPER ERROR BOUND (INPUT), IF ABSOLUTE ERROR IS
GREATER THAN PRMT(4), INCREMENT GETS HALVED.
IF INCREMENT IS LESS THAN PRMT(3) AND ABSOLUTE
ERROR LESS THAN PRMT(4)/50 INCREMENT GETS DOUBLED.
THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS
OUTPUT SUBROUTINE.
PRMT(5) - NO INPUT PARAMETER. SUBROUTINE DRKGS INITIALIZES
PRMT(5)=0. IF THE USER WANTS TO TERMINATE
SUBROUTINE DRKGS AT ANY POINT, HE HAS TO
CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE
OUTPUT. FURTHER DIMENSIONS OF VECTOR PRMT ARE
FEASIBLE IF ITS DIMENSION IS DEFINED GREATER
THAN 5. HOWEVER SUBROUTINE DRKGS DOES NOT REQUIRE
AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL
FOR HANDLING RESULTS WHICH ARE OBTAINED IN PROGRAM
(CALLING DRKGS) WHICH ARE OBTAINED IN SPECIAL
MANIPULATIONS WITH INPJT VECTOR IN SUBROUTINE
DOUBLE PRECISION WITH INPJT VECTOR OF INITIAL VALUES
(DESTROYED). LATERON Y IS THE RESULTING VECTOR OF
DEPENDENT VARIABLES COMPILED AT INTERMEDIATE
POINTS X.
DERY - DIMENSION INPJT VECTOR OF ERROR WEIGHTS
DOUBLE PRECISION). THE SUM OF ITS COMPONENTS MUST BE
(DESTROYED).

DRKGS 50
DRKGS 60
DRKGS 70
DRKGS 80
DRKGS 90
DRKGS 100
DRKGS 110
DRKGS 120
DRKGS 130
DRKGS 140
DRKGS 150
DRKGS 160
DRKGS 170
DRKGS 180
DRKGS 190
DRKGS 200
DRKGS 210
DRKGS 220
DRKGS 230
DRKGS 240
DRKGS 250
DRKGS 260
DRKGS 270
DRKGS 280
DRKGS 290
DRKGS 300
DRKGS 310
DRKGS 320
DRKGS 330
DRKGS 340
DRKGS 350
DRKGS 360
DRKGS 370
DRKGS 380
DRKGS 390
DRKGS 400
DRKGS 410
DRKGS 420
DRKGS 430
DRKGS 440
DRKGS 450
DRKGS 460
DRKGS 470
DRKGS 480

46 C C C C C
47 C C C C C
48 C C C C C
49 C C C C C
50 C C C C C
51 C C C C C
52 C C C C C
53 C C C C C
54 C C C C C
55 C C C C C
56 C C C C C
57 C C C C C
58 C C C C C
59 C C C C C
60 C C C C C
61 C C C C C
62 C C C C C
63 C C C C C
64 C C C C C
65 C C C C C
66 C C C C C
67 C C C C C
68 C C C C C
69 C C C C C
70 C C C C C
71 C C C C C
72 C C C C C
73 C C C C C
74 C C C C C
75 C C C C C
76 C C C C C
77 C C C C C
78 C C C C C
79 C C C C C
80 C C C C C
81 C C C C C
82 C C C C C
83 C C C C C
84 C C C C C
85 C C C C C
86 C C C C C
87 C C C C C
88 C C C C C
89 C C C C C
90 C

NDIM - EQUAL TO 1, LATERON DERY IS THE VECTOR OF DERIVATIVES, WHICH BELONG TO FUNCTION VALUES Y AT INTERMEDIATE POINTS X.

IHLF - AN INPUT VALUE, WHICH SPECIFIES THE NUMBER OF EQUATIONS IN THE SYSTEM. SPECIFIES THE NUMBER OF BISECTION VALUE, WHICH SPECIFIES THE NUMBER OF GREATER THAN 10, SUBROUTINE RETURNS WITH ERROR MESSAGE IHLF=1 INTO MAIN PROGRAM, ERROR MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE PRMT(3) IS 0 OR IN CASE.

FCT - THE NAME OF AN EXTERNAL SUBROUTINE USED. THIS SUBROUTINE COMPUTES THE RIGHT HAND SIDES DERY OF THE SYSTEM TO GIVEN VALUES X AND Y. ITS PARAMETER LIST MUST BE X, Y, DERY. SUBROUTINE FCT SHOULD LIST DESTROY BE X, Y, AND Y.

OUTP - THE NAME OF AN INTERVAL OUTPUT SUBROUTINE USED. ITS PARAMETER LIST MUST BE X, Y, IHLF, NDIM, PRMT.

AUX - MOVE OF THESE PARAMETERS (EXCEPT, IF NECESSARY, PRMT(4), PRMT(5)). IF PRMT(5) IS CHANGED TO NON-ZERO, SUBROUTINE OUTPUT IS TERMINATED.

REMARKS - DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 8 RUNS AND NDIM COLUMNS.

PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE IHLF=11), INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN (ERROR MESSAGE IHLF=12 OR IHLF=13), THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH, SUBROUTINE OUTPUT HAS CHANGED PRMT(5) TO NON-ZERO.

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED THE EXTERNAL SUBROUTINES FCT(X, Y, DERY) AND OUTP(X, Y, DERY, IHLF, NDIM, PRMT) MUST BE FURNISHED BY THE USER.

METHOD EVALUATION IS DONE BY MEANS OF FOURTH ORDER RUNGE-KUNTA FORMULAE IN THE MODIFICATION OF GILL. ACCURACY IS TESTED COMPARING THE RESULTS OF THE PROCEDURE WITH SINGLE AND DOUBLE INCREMENT.

DRKG 490
DRKG 500
DRKG 510
DRKG 520
DRKG 530
DRKG 540
DRKG 550
DRKG 560
DRKG 570
DRKG 580
DRKG 590
DRKG 600
DRKG 610
DRKG 620
DRKG 630
DRKG 640
DRKG 650
DRKG 660
DRKG 670
DRKG 680
DRKG 690
DRKG 700
DRKG 710
DRKG 720
DRKG 730
DRKG 740
DRKG 750
DRKG 760
DRKG 770
DRKG 780
DRKG 790
DRKG 800
DRKG 810
DRKG 820
DRKG 830
DRKG 840
DRKG 850
DRKG 860
DRKG 870
DRKG 880
DRKG 890
DRKG 900
DRKG 910
DRKG 920
DRKG 930

940 DRKG
950 DRKG
960 DRKG
970 DRKG
980 DRKG
990 DRKG
1000 DRKG
1010 DRKG
1020 DRKG
1030 DRKG
1040 DRKG
1050 DRKG
1060 DRKG
1070 DRKG
1080 DRKG
1090 DRKG
1100 DRKG
1110 DRKG
1120 DRKG
1130 DRKG
1140 DRKG
1150 DRKG
1160 DRKG
1170 DRKG
1180 DRKG
1190 DRKG
1200 DRKG
1210 DRKG
1220 DRKG
1230 DRKG
1240 DRKG
1250 DRKG
1260 DRKG
1270 DRKG
1280 DRKG
1290 DRKG
1300 DRKG
1310 DRKG
1320 DRKG
1330 DRKG
1340 DRKG
1350 DRKG
1360 DRKG
1370 DRKG
1380 DRKG
1390 DRKG

SUBROUTINE DRKGS AUTOMATICALLY ADJUSTS THE INCREMENT DURING THE WHOLE COMPUTATION BY HALVING OR DOUBLING. IF MORE THAN 10 BISECTIONS OF THE INCREMENT ARE NECESSARY TO GET SATISFACTORY ACCURACY, THE SUBROUTINE RETURNS WITH ERROR MESSAGE IHLF=11 IN MAIN PROGRAM. TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE MUST BE FURNISHED BY THE USER. FOR REFERENCE, SEE RALSTON/WILF, MATHEMATICAL METHODS FOR DIGITAL COMPUTERS, WILEY, NEW YORK/LONDON, 1960, PP.110-120.

.....

DIMENSION Y(NDIM), DERY(NDIM), AUX(8, NDIM), A(4), B(4), C(4), PRMT(5)
DOUBLE PRECISION PRMT, Y, DERY, AUX, A, B, C, X, XEND, H, AJ, BJ, CJ, RI, K2,
IDELT, DABS

```
1 DO I=1, NDIM
  AUX(B,I)=.0666666666666667 D0*DERY(I)
  X=PRMT(1)
  XEND=PRMT(2)
  H=PRMT(3)
  PRMT(5)=0. D0
  CALL FCT(X, Y, DERY)
```

```
ERROR TEST
IF(H*(XEND-X)) 38, 37, 2
```

PREPARATIONS FOR RUNGE-KUTTA METHOD

```
2 A(1)=.5D0
  A(2)=.2928932188134525 D0
  A(3)=1.707106781186548 D0
  A(4)=1.6666666666666667 D0
  B(1)=2. D0
  B(2)=1. D0
  B(3)=1. D0
  B(4)=2. D0
  C(1)=.5D0
  C(2)=.2928932188134525 D0
  C(3)=1.707106781186548 D0
  C(4)=.5D0
```

PREPARATIONS OF FIRST RUNGE-KUTTA STEP
DO 3 I=1, NDIM

91 C
92 C
93 C
94 C
95 C
96 C
97 C
98 C
99 C
100 C
101 C
102 C
103 C
104 C
105 C
106 C
107 C
108 C
109 C
110 C
111 C
112 C
113 C
114 C
115 C
116 C
117 C
118 C
119 C
120 C
121 C
122 C
123 C
124 C
125 C
126 C
127 C
128 C
129 C
130 C
131 C
132 C
133 C
134 C
135 C

DKKG1400
 DKKG1410
 DKKG1420
 DKKG1430
 DKKG1440
 DKKG1450
 DKKG1460
 DKKG1470
 DKKG1480
 DKKG1490
 DKKG1500
 DKKG1510
 DKKG1520
 DKKG1530
 DKKG1540
 DKKG1550
 DKKG1560
 DKKG1570
 DKKG1580
 DKKG1590
 DKKG1600
 DKKG1610
 DKKG1620
 DKKG1630
 DKKG1640
 DKKG1650
 DKKG1660
 DKKG1670
 DKKG1680
 DKKG1690
 DKKG1700
 DKKG1710
 DKKG1720
 DKKG1730
 DKKG1740
 DKKG1750
 DKKG1760
 DKKG1770
 DKKG1780
 DKKG1790
 DKKG1800
 DKKG1810
 DKKG1820
 DKKG1830
 DKKG1840

```

136 AUX(1,1)=Y(I)
137 AUX(2,1)=DERY(I)
138 AUX(3,1)=0.00
139 AUX(6,1)=0.00
140 IREC=0
141 H=H+H
142 IHLEF=-1
143 ISTEP=0
144 IEND=0
145 C C C
146 C C C
147 C C C
148 C C C
149 C C C
150 C C C
151 C C C
152 C C C
153 C C C
154 C C C
155 C C C
156 C C C
157 C C C
158 C C C
159 C C C
160 C C C
161 C C C
162 C C C
163 C C C
164 C C C
165 C C C
166 C C C
167 C C C
168 C C C
169 C C C
170 C C C
171 C C C
172 C C C
173 C C C
174 C C C
175 C C C
176 C C C
177 C C C
178 C C C
179 C C C
180 C C C

3 AUX(1,1)=Y(I)
  AUX(2,1)=DERY(I)
  AUX(3,1)=0.00
  AUX(6,1)=0.00
  IREC=0
  H=H+H
  IHLEF=-1
  ISTEP=0
  IEND=0

  START OF A RUNGE-KUTTA STEP
  4 IF((X+H-XEND)*H)7,6,5
  5 H=XEND-X
  6 IEND=1

  RECORDING OF INITIAL VALUES OF THIS STEP
  7 CALL CJTP(X,Y,DERY,IREC,NDIM,PRMT)
  8 IF(PRMT(5))40,8,40
  9 ISTEP=ISTEP+1

  START OF INNERMOST RUNGE-KUTTA LOOP
  10 J=1
  11 AJ=A(J)
  12 BJ=B(J)
  13 CJ=C(J)
  14 DO 11 I=1,NDIM
  15 RI=H*DERY(I)
  16 K2=AJ*(RI-HJ)*AUX(6,I)
  17 Y(I)=Y(I)+R2
  18 R2=R2+R2+R2
  19 AUX(6,I)=AUX(6,I)+R2-CJ*RI
  20 IF(J-4)12,15,15
  21 J=J+1
  22 IF(J-3)13,14,13
  23 X=X+H*SDO*H
  24 CALL FCI(X,Y,DERY)
  25 GOTO 10

  END OF INNERMOST RUNGE-KUTTA LOOP

  TEST OF ACCURACY
  15 IF(ITEST)16,16,20
  
```

```

181 C
182
183
184
185
186
187
188
189
190
191
192
193
194
195 C
196 C
197
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201
202
203
204 C
205 C
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208
209 C
210 C
211
212
213
214
215
216
217
218 C
219 C
220
221
222
223
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225

IN CASE ITEST=0 THERE IS NO POSSIBILITY FOR TESTING OF ACCURACY
16 DO 17 I=1,NDIM
17 AUX(4,I)=Y(I)
18 ITEST=1
19 ISTEP=ISTEP+1STEP-2
19 IHLF=IHLF+1
19 X=X-H
19 H=.5D0*H
19 DO 19 I=1,NDIM
19 Y(I)=AJX(I,1)
19 DERY(I)=AUX(2,I)
19 AUX(6,I)=AUX(3,I)
19 GO TO 9

IN CASE ITEST=1 TESTING OF ACCURACY IS POSSIBLE
20 IMOD=ISTEP/2
21 IF(ISTEP-IMOD-IMOD)21,23,21
21 CALL FCT(X,Y,DERY)
21 DO 22 I=1,NDIM
21 AUX(5,I)=Y(I)
22 AUX(7,I)=DERY(I)
22 GO TO 9

COMPUTATION OF TEST VALUE DELT
23 DELT=0.00
24 DO 24 I=1,NDIM
24 DELT=DELT+AUX(8,I)*DABS(AUX(4,I)-Y(I))
24 IF(DELT-PRMT(4))28,26,25

ERROR IS TOO GREAT
25 IF(IHLF-30)26,56,56
26 DO 27 I=1,NDIM
27 AUX(4,I)=AUX(5,I)
27 ISTEP=ISTEP+1STEP-4
27 X=X-H
27 IEND=0
27 GO TO 18

RESULT VALUES ARE GOOD
28 CALL FCT(X,Y,DERY)
28 DO 29 I=1,NDIM
28 AUX(1,I)=Y(I)
28 AUX(2,I)=DERY(I)
28 AUX(3,I)=AUX(6,I)

```

```

DRKG1850
DRKG1860
DRKG1870
DRKG1880
DRKG1890
DRKG1900
DRKG1910
DRKG1920
DRKG1930
DRKG1940
DRKG1950
DRKG1960
DRKG1970
DRKG1980
DRKG1990
DRKG2000
DRKG2010
DRKG2020
DRKG2030
DRKG2040
DRKG2050
DRKG2060
DRKG2070
DRKG2080
DRKG2090
DRKG2100
DRKG2110
DRKG2120
DRKG2130
DRKG2140
DRKG2150
DRKG2160
DRKG2170
DRKG2180
DRKG2190
DRKG2200
DRKG2210
DRKG2220
DRKG2230
DRKG2240
DRKG2250
DRKG2260
DRKG2270
DRKG2280
DRKG2290

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DRKG2300
 DRKG2310
 DRKG2320
 DRKG2330
 DRKG2340
 DRKG2350
 DRKG2360
 DRKG2370
 DRKG2380
 DRKG2390
 DRKG2400
 DRKG2410
 DRKG2420
 DRKG2430
 DRKG2440
 DRKG2450
 DRKG2460
 DRKG2470
 DRKG2480
 DRKG2490
 DRKG2500
 DRKG2510
 DRKG2520
 DRKG2530
 DRKG2540
 DRKG2550
 DRKG2560
 DRKG2570
 DRKG2580
 DRKG2590
 DRKG2600
 DRKG2610
 DRKG2620
 DRKG2630

```

29 Y(I)=AUX(5,I)
   DERY(I)=AUX(7,I)
   CALL JUIP(X,H,Y,DERY,IHLF,NDIM,PRMT)
   IF (PRMT(5)) 40,30,40
30 DO 31 I=1,NDIM
   Y(I)=AUX(1,I)
31 DERY(I)=AUX(2,I)
   IREC=IHLF
   IF (IEVD) 32,32,39
32 INCREMENT GETS DOUBLED
   IHLF=IHLF-1
   ISTEP=ISTEP/2
   H=H+H
   IF (IHLF) 4,33,33
33 IMOD=ISTEP/2
   IF (ISTEP-IMOD-IMOD) 4,34,4
34 IF (DELT-0.200*PRMT(4)) 35,35,4
35 IHLF=IHLF-1
   ISTEP=ISTEP/2
   H=H+H
   GO TO 4

36 RETURN TO CALLING PROGRAM
   IHLF=31
   CALL FCT(X,Y,DERY)
37 GO TO 39
   IHLF=32
   GO TO 39
38 IHLF=33
39 CALL JUIP(X,Y,DERY,IHLF,NDIM,PRMT)
40 RETURN
   END
  
```

227
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 254
 255
 256
 257
 258
 259

```

1  CC
2  CC
3  CC
4  CC
5  CC
6  CC
7  CC
8  CC
9  CC
10 CC
11 CC
12 CC
13 CC
14 CC
15 CC
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37 CC
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41 CC
42 CC
43 CC
44 CC
45 CC

```

SUBROUTINE DHPGG(PRMT, Y, DERY, NDIM, IMLF, FCI, UUIP, AUX)
PURPOSE
TO SOLVE A SYSTEM OF FIRST ORDER ORDINARY GENERAL
DIFFERENTIAL EQUATIONS WITH GIVEN INITIAL VALUES.
USAGE
CALL DHPGG (PRMT, Y, DERY, NDIM, IMLF, FCI, UUIP, AUX)
PARAMETERS FCT AND OUTP REQUIRE AN EXTERNAL STATEMENT.
DESCRIPTION OF PARAMETERS
PRMT - DOUBLE PRECISION INPUT AND OUTPUT VECTOR WITH
DIMENSION GREATER THAN OR EQUAL TO 5, WHICH
SPECIFIES THE PARAMETERS OF THE INTERVAL AND OF
ACCURACY AND WHICH SERVES FOR COMMUNICATION BETWEEN
OUTPUT SUBROUTINE (EXCEPT PRMT(5) THE COMPONENTS
SUBROUTINE DHPGG, EXCEPT PRMT(5) THE COMPONENTS
ARE NOT DESTROYED BY SUBROUTINE DHPGG AND THEY ARE
LOWER BOUND OF THE INTERVAL (INPUT),
PRMT(1) - INITIAL INCREMENT OF THE INDEPENDENT VARIABLE
PRMT(2) - UPPER ERROR BOUND (INPUT). IF ABSOLUTE ERROR IS
PRMT(3) - GREATER THAN PRMT(4), INCREMENT GETS HALVED.
IF INCREMENT IS LESS, THAN PRMT(3) AND ABSOLUTE
ERROR LESS THAN PRMT(4)/50, INCREMENT GETS DOUBLED.
THE USER MAY CHANGE PRMT(4) BY MEANS OF HIS
OUTPUT SUBROUTINE.
PRMT(5) - NO INPUT PARAMETER. SUBROUTINE DHPGG INITIALIZES
PRMT(5)=0. IF THE USER WANTS TO TERMINATE
SUBROUTINE DHPGG AT ANY OUTPUT POINT, HE HAS TO
CHANGE PRMT(5) TO NON-ZERO BY MEANS OF SUBROUTINE
OUTP. FURTHER COMPONENTS OF VECTOR PRMT ARE
FEASIBLE IF ITS DIMENSION IS DEFINED GREATER
THAN 5. HOWEVER SUBROUTINE DHPGG DOES NOT REQUIRE
AND CHANGE THEM. NEVERTHELESS THEY MAY BE USEFUL
FOR HANDLING RESULT VALUES TO THE MAIN PROGRAM
(CALLING DHPGG) WHICH ARE OBTAINED BY SPECIAL
MANIPULATIONS WITH OUTPUT DATA IN SUBROUTINE UUIP.
Y - DOUBLE PRECISION INPUT VECTOR OF INITIAL VALUES
(DESTROYED). LATERON Y IS THE RESULTING VECTOR OF
DEPENDENT VARIABLES COMPUTED AT IMMEDIATE
POINTS X
DERY - DOUBLE PRECISION INPUT VECTOR OF ERROR WEIGHTS
(DESTROYED). THE SUM OF ITS COMPONENTS MUST BE

50 DHPGG
60 DHPGG
70 DHPGG
80 DHPGG
90 DHPGG
100 DHPGG
110 DHPGG
120 DHPGG
130 DHPGG
140 DHPGG
150 DHPGG
160 DHPGG
170 DHPGG
180 DHPGG
190 DHPGG
200 DHPGG
210 DHPGG
220 DHPGG
230 DHPGG
240 DHPGG
250 DHPGG
260 DHPGG
270 DHPGG
280 DHPGG
290 DHPGG
300 DHPGG
310 DHPGG
320 DHPGG
330 DHPGG
340 DHPGG
350 DHPGG
360 DHPGG
370 DHPGG
380 DHPGG
390 DHPGG
400 DHPGG
410 DHPGG
420 DHPGG
430 DHPGG
440 DHPGG
450 DHPGG
460 DHPGG
470 DHPGG
480 DHPGG

490 DMCG
 500 DMCG
 510 DMCG
 520 DMCG
 530 DMCG
 540 DMCG
 550 DMCG
 560 DMCG
 570 DMCG
 580 DMCG
 590 DMCG
 600 DMCG
 610 DMCG
 620 DMCG
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 650 DMCG
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 670 DMCG
 680 DMCG
 690 DMCG
 700 DMCG
 710 DMCG
 720 DMCG
 730 DMCG
 740 DMCG
 750 DMCG
 760 DMCG
 770 DMCG
 780 DMCG
 790 DMCG
 800 DMCG
 810 DMCG
 820 DMCG
 830 DMCG
 840 DMCG
 850 DMCG
 860 DMCG
 870 DMCG
 880 DMCG
 890 DMCG
 900 DMCG
 910 DMCG
 920 DMCG
 930 DMCG

EQUAL TO 1, LATERON DERY IS THE VECTOR OF
 DERIVATIVE, WHICH BELONG TO FUNCTION VALUES Y AT
 INTERMEDIATE POINTS X, WHICH X, SPECIFIES THE NUMBER OF
 AN INPUT VALUE, WHICH SYSTEM, SPECIFIES THE NUMBER OF
 EQUATIONS IN THE SYSTEM, SPECIFIES THE NUMBER OF
 IHLF IN THE SYSTEM, WHICH IHLF GETS
 BISECTION OF THE INITIAL INCREMENT, IF IHLF=1
 GREATER THAN 10, SUBROUTINE DHPG RETURNS WITH
 ERROR MESSAGE IHLF=11 INTO MAIN PROGRAM
 ERVT MESSAGE IHLF=12 OR IHLF=13 APPEARS IN CASE
 PRMT(3)=0 OR IN CASE SIGN(PRMT(3)).NE.SIGN(PRMT(2))
 PRMT(1)) RESPECTIVELY
 - THE NAME OF AN EXTERNAL SUBROUTINE USED. IF
 COMPUTES THE RIGHT HAND SIDES DERY OF THE SYSTEM
 TO GIVEN VALUES OF X AND Y. ITS PARAMETER LIST
 MUST BE X, Y, DERY. THE SUBROUTINE SHOULD NOT
 DESTROY X AND Y
 - THE NAME OF AN EXTERNAL SUBROUTINE USED. IF
 ITS PARAMETER LIST MUST BE X, Y, DERY, IHLF, NDIM, PRMT.
 NONE OF THESE PARAMETERS (EXCEPT, IF NECESSARY,
 PRMT(4), PRMT(5), ..) SHOULD BE CHANGED BY
 SUBROUTINE OUTP. IF PRMT(5) IS CHANGED TO NON-ZERO,
 SUBROUTINE DHPG IS TERMINATED.
 - DOUBLE PRECISION AUXILIARY STORAGE ARRAY WITH 10
 RUNS AND NDIM COLUMNS.

REMARKS
 THE PROCEDURE TERMINATES AND RETURNS TO CALLING PROGRAM, IF
 MORE THAN 10 BISECTIONS OF THE INITIAL INCREMENT ARE
 NECESSARY TO GET SATISFACTORY ACCURACY (ERROR MESSAGE
 IHLF=11), INCREMENT IS EQUAL TO 0 OR HAS WRONG SIGN
 (2) INITIAL MESSAGE IHLF=12 OR IHLF=13,
 (3) THE WHOLE INTEGRATION INTERVAL IS WORKED THROUGH,
 (4) SUBROUTINE OUTP HAS CHANGED PRMT(5) TO NON-ZERO.

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
 THE EXTERNAL SUBROUTINES FCT(X, Y, DERY) AND
 OUTP(X, Y, DERY, IHLF, NDIM, PRMT) MUST BE FURNISHED BY THE USER.
 METHOD
 EVALUATION IS DONE BY MEANS OF HAMMING'S MODIFIED PREDICTOR-
 CORRECTOR METHOD. IT IS A FOURTH ORDER METHOD, USING 4
 PRECEDING POINTS FOR COMPUTATION OF A NEW VECTOR Y OF THE
 DEPENDENT VARIABLES.

46 C
 47 C
 48 C
 49 C
 50 C
 51 C
 52 C
 53 C
 54 C
 55 C
 56 C
 57 C
 58 C
 59 C
 60 C
 61 C
 62 C
 63 C
 64 C
 65 C
 66 C
 67 C
 68 C
 69 C
 70 C
 71 C
 72 C
 73 C
 74 C
 75 C
 76 C
 77 C
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 79 C
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 81 C
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135

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

DHCG 940
 DHCG 950
 DHCG 960
 DHCG 970
 DHCG 980
 DHCG 990
 DHCG1000
 DHCG1010
 DHCG1020
 DHCG1030
 DHCG1040
 DHCG1050
 DHCG1060
 DHCG1070
 DHCG1080
 DHCG1100
 DHCG1110
 DHCG1140
 DHCG1150
 DHCG1160
 DHCG1170
 DHCG1180
 DHCG1190
 DHCG1200
 DHCG1210
 DHCG1220
 DHCG1230
 DHCG1240
 DHCG1250
 DHCG1260
 DHCG1270
 DHCG1280
 DHCG1290
 DHCG1300
 DHCG1310
 DHCG1320
 DHCG1330
 DHCG1340
 DHCG1350
 DHCG1360
 DHCG1370
 DHCG1380
 DHCG1390

FOURTH ORDER RUNGE-KUITA METHOD SUGGESTED BY KALSTON IS
 USED FOR ADJUSTMENT OF THE INITIAL INCREMENT AND FOR
 COMPUTATION OF STARTING VALUES.
 SUBROUTINE DHPCG AUTOMATICALLY ADJUSTS THE INCREMENT DURING
 THE WHOLE COMPUTATION BY HALVING OR DOUBLING.
 TO GET FULL FLEXIBILITY IN OUTPUT, AN OUTPUT SUBROUTINE
 MUST BE CODED BY THE USER.
 FOR REFERENCE, SEE MATHEMATICAL METHODS FOR DIGITAL
 COMPUTERS, WILEY, NEW YORK/LONDON, 1960, PP. 95-109.
 (1) KALSTON, RUNGE-KUITA METHODS WITH MINIMUM ERROR BOUNDS,
 (2) MIAC, VOL. 16, ISS. 80 (1962), PP. 431-437.

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

.....
 DIMENSION PRMT(5), Y(NDIM), DERY(NDIM), AUX(16, NDIM),
 DOUBLE PRECISION Y, DERY, AUX, PRMT, X, H, Z, DELT, DABS
 N=1
 IHLF=0
 X=PRMT(1)
 H=PRMT(3)
 PRMT(5)=0.0, D0
 DO 1 I=1, NDIM
 AUX(16, I)=0.0, D0
 AUX(15, I)=DERY(I)
 AUX(1, I)=Y(I)
 IF (H*(PRMT(2)-X)) 3, 2, 4
 1
 2
 3
 4
 5
 6
 7
 8

```

136 C      COMPUTATION OF AUX(2,1)
137 C      ISW=1
138 C      GUID 100
139 C
140 C      9 X=X+H
141 C      DO 10 I=1,NDIM
142 C      10 AUX(2,I)=Y(I)
143 C
144 C      INCREMENT H IS TESTED BY MEANS OF BISECTION
145 C      11 IHLF=IHLF+1
146 C      X=X-H
147 C      DO 12 I=1,NDIM
148 C      12 AUX(4,I)=AUX(2,I)
149 C      H=.5DU*H
150 C      N=1
151 C      ISW=2
152 C      GUID 100
153 C
154 C      13 X=X+H
155 C      CALL FCI(X,Y,DERY)
156 C      N=N+2
157 C      DO 14 I=1,NDIM
158 C      14 AUX(2,I)=Y(I)
159 C      AUX(9,I)=DERY(I)
160 C      ISW=3
161 C      GUID 100
162 C
163 C      COMPUTATION OF TEST VALUE DELT
164 C      DELT=0,DU
165 C      DO 16 I=1,NDIM
166 C      16 DELT=DELT+AUX(15,I)*DABS(Y(I))-AUX(4,I))
167 C      DELT=.066666666666666667DU*DELT
168 C      IF(DELT-PRM1(4))19,19,17
169 C      17 IF(IHLF-20)11,16,18
170 C
171 C      NO SATISFACTORY ACCURACY AFTER 10 BISECTIONS. ERROR MESSAGE.
172 C      18 IHLF=21
173 C      X=X+H
174 C      GUID 4
175 C
176 C      THERE IS SATISFACTORY ACCURACY AFTER LESS THAN 11 BISECTIONS.
177 C      19 X=X+H
178 C      CALL FCI(X,Y,DERY)
179 C      DO 20 I=1,NDIM
180 C

```

```

DHC61400
DHC61410
DHC61420
DHC61430
DHC61440
DHC61450
DHC61460
DHC61470
DHC61480
DHC61490
DHC61500
DHC61510
DHC61520
DHC61530
DHC61540
DHC61550
DHC61560
DHC61570
DHC61580
DHC61590
DHC61600
DHC61610
DHC61620
DHC61630
DHC61640
DHC61650
DHC61660
DHC61670
DHC61680
DHC61690
DHC61700
DHC61710
DHC61720
DHC61730
DHC61740
DHC61750
DHC61760
DHC61770
DHC61780
DHC61790
DHC61800
DHC61810
DHC61820
DHC61830
DHC61840

```

DHCG1850
 DHCG1860
 DHCG1870
 DHCG1880
 DHCG1890
 DHCG1900
 DHCG1910
 DHCG1920
 DHCG1930
 DHCG1940
 DHCG1950
 DHCG1960
 DHCG1970
 DHCG1980
 DHCG1990
 DHCG2000
 DHCG2010
 DHCG2020
 DHCG2030
 DHCG2040
 DHCG2050
 DHCG2060
 DHCG2070
 DHCG2080
 DHCG2090
 DHCG2100
 DHCG2110
 DHCG2120
 DHCG2130
 DHCG2140
 DHCG2150
 DHCG2160
 DHCG2170
 DHCG2180
 DHCG2190
 DHCG2200
 DHCG2210
 DHCG2220
 DHCG2230
 DHCG2240
 DHCG2250
 DHCG2260
 DHCG2270
 DHCG2280
 DHCG2290

```

181 AUX(3,I)=Y(I)
182 AUX(10,I)=DERY(I)
183 N=3
184 ISW=4
185 GUD=100
186
187
188
189
190
191
192
193
194
195
196
197
198
199
200
201
202
203
204
205
206
207
208
209
210
211
212
213
214
215
216
217
218
219
220
221
222
223
224
225
  
```

```

20 AUX(3,I)=Y(I)
   AUX(10,I)=DERY(I)
   N=3
   ISW=4
   GUD=100
21 N=X+H
   CALL FCT(X,Y,DERY)
   X=PRMT(I)
   DO 22 I=1,NDIM
     AUX(I)=AJX(I,I)+H*(.375D0*AUX(8,I)+.7916666666666667D0*AUX(9,I)
     1-.2083333333333333D0*AUX(10,I))+.0416666666666666666667D0*DERY(I))
23 X=X+H
   W=N+1
   CALL FCT(X,Y,DERY)
   CALL QJIP(X,Y,DERY,IHLF,NDIM,PRMT)
   IF(PHMT(5))6,24,6
24 IF(N=4)25,200,200
25 DO 26 I=1,NDIM
   AUX(N,I)=Y(I)
26 AUX(N+1,I)=DERY(I)
   IF(N=5)27,29,200
27 DO 28 I=1,NDIM
   DELT=AUX(9,I)+AUX(9,I)
   DELI=DELT+DELT
28 Y(I)=AUX(1,I)+.3555333333333333D0*H*(AUX(8,I)+DELT+AUX(10,I))
   GUD=25
29 DO 30 I=1,NDIM
   DELT=AUX(9,I)+AUX(10,I)
   DELI=DELT+DELT+DELT
30 Y(I)=AUX(1,I)+.575D0*H*(AUX(8,I)+DELT+AUX(11,I))
   GUD=25
100 THE FOLLOWING PART OF SUBROUTINE DHPCG COMPUTES BY MEANS OF
   RUNGE-KUTTA METHOD STARTING VALUES FOR THE NOT SELF-STARTING
   PREDICTOR-CORRECTOR METHOD.
   DO 101 I=1,NDIM
     Z=H*AUX(N+7,I)
     AUX(5,I)=Z
101 Y(I)=AUX(N,I)+4D0*Z
   Z IS AN AUXILIARY STORAGE LOCATION
  
```

```

226 C      Z=X+.4D0*M
227      CALL FCI(Z, Y, DERY)
228      DO 102 I=1, NDIM
229      Z=H*DERY(I)
230      AUX(6, I)=Z
231      102 Y(I)=AUX(N, I)+.29697760924775360D0*AUX(5, I)+.15875964497103583D0*Z
232 C
233      Z=X+.45573725421878943D0*M
234      CALL FCI(Z, Y, DERY)
235      DO 103 I=1, NDIM
236      Z=H*DERY(I)
237      AUX(7, I)=Z
238      103 Y(I)=AUX(N, I)+.21810038822592047D0*AUX(5, I)-3.0509651486929308D0*
239      1AUX(6, I)+3.8328647604670103D0*Z
240 C
241      Z=X+H
242      CALL FCI(Z, Y, DERY)
243      DO 104 I=1, NDIM
244      Y(I)=AUX(N, I)+.17476028226269037D0*AUX(5, I)-55148066287873294D0*
245      1AUX(6, I)+1.20553559939652350D0*AUX(7, I)+.17118478121951903D0*
246      2H*DERY(I)
247      2GOTO(9, 13, 15, 21), ISW
248 C
249 C      POSSIBLE BREAK-POINT FOR LINKAGE
250 C
251 C      STARTING VALUES ARE COMPUTED.
252 C      NOW START HAMMING'S MODIFIED PREDICTOR-CORRECTOR METHOD.
253 C      ISTEP=5
254      200 IF(N=8)204,202,204
255 C
256 C      N=H CAUSES THE ROWS OF AUX TO CHANGE THEIR STORAGE LOCATIONS
257 C      DO 203 N=2, 7
258      DO 203 I=1, NDIM
259      AUX(N-1, I)=AUX(N, I)
260      AUX(N+1, I)=AUX(N+7, I)
261      N=7
262 C
263 C      N LESS THAN 8 CAUSES N+1 TO GET N
264      N=N+1
265 C
266 C      COMPUTATION OF NEXT VECTOR Y
267 C      DO 205 I=1, NDIM
268      AUX(N-1, I)=Y(I)
269      AUX(N+6, I)=DERY(I)
270

```

```

DHC62300
DHC62310
DHC62320
DHC62330
DHC62340
DHC62350
DHC62360
DHC62370
DHC62380
DHC62390
DHC62400
DHC62410
DHC62420
DHC62430
DHC62440
DHC62450
DHC62460
DHC62470
DHC62480
DHC62490
DHC62500
DHC62510
DHC62520
DHC62530
DHC62540
DHC62550
DHC62560
DHC62570
DHC62580
DHC62590
DHC62600
DHC62610
DHC62620
DHC62630
DHC62640
DHC62650
DHC62660
DHC62670
DHC62680
DHC62690
DHC62700
DHC62710
DHC62720
DHC62730
DHC62740

```

```

271 X=X+H
272 I=STEP+1
273 DO 207 I=1,NDIM
274 ODELTA=AUX(N-4,I)+1.3333333333333333D0*H*(AUX(N+6,I)+AUX(N+6,I))-
275 1AUX(N+5,I)+AUX(N+4,I)+AUX(N+4,I))
276 Y(I)=DELT+DELTA
277 AUX(16,I)=DELT
278 PREDICTOR IS NOW GENERATED IN ROW 16 OF AUX, MODIFIED PREDICTOR
279 IS GENERATED IN Y. DELT MEANS AN AUXILIARY STORAGE.
280 CALL FCT(X,Y,DERY)
281 DERIVATIVE OF MODIFIED PREDICTOR IS GENERATED IN DERY
282
283 DO 208 I=1,NDIM
284 ODELTA=.125D0*(9.D0*AUX(N-1,I)-AUX(N-3,I))+3.D0*H*(DERY(I)+AUX(N+6,I))
285 1+AUX(N+6,I)-AUX(N+5,I))
286 AUX(16,I)=AUX(16,I)-DELT
287 Y(I)=DELT+.07438016528925620D0*AUX(16,I)
288
289 C
290 TEST WHETHER H MUST BE HALVED OR DOUBLED
291 DELT=0.D0
292 DO 209 I=1,NDIM
293 DELT=DELT+AUX(15,I)*DABS(AUX(16,I))
294 IF (DELT-PRMT(4))210,222,222
295
296 C
297 H MUST NOT BE HALVED. THAT MEANS Y(I) ARE GOOD.
298 CALL FCT(X,Y,DERY)
299 CALL JUIP(X,Y,DERY,IHLF,NDIM,PRMT)
300 IF (PRMT(5))212,211,212
301 IF (IHLF-21)213,212,212
302 RETURN
303 IF (H*(X-PRMT(2)))214,212,212
304 IF (DABS(X-PRMT(2))-.1D0*DABS(H))212,215,215
305 IF (DELT-.02D0*PRMT(4))216,216,201
306
307 C
308 H COULD BE DOUBLED IF ALL NECESSARY PRECEDING VALUES ARE
309 AVAILABLE
310 IF (IHLF)201,201,217
311 IF (N-7)201,218,218
312 IF (ISTEP-4)201,219,219
313 IF (MOD=ISTEP/2)
314 IF (ISTEP-IMOD-1MOD)201,220,201
315 H=H+H
316 IHLF=IHLF-1

```

```

DHC62750
DHC62760
DHC62770
DHC62780
DHC62790
DHC62800
DHC62810
DHC62820
DHC62830
DHC62840
DHC62850
DHC62860
DHC62870
DHC62880
DHC62890
DHC62900
DHC62910
DHC62920
DHC62930
DHC62940
DHC62950
DHC62960
DHC62970
DHC62980
DHC62990
DHC63000
DHC63010
DHC63020
DHC63030
DHC63040
DHC63050
DHC63060
DHC63070
DHC63080
DHC63090
DHC63100
DHC63110
DHC63120
DHC63130
DHC63140
DHC63150
DHC63160
DHC63170
DHC63180
DHC63190

```

```

316 18STEP=0
317 DO 221 I=1,NDIM
318 AUX(N-1,I)=AUX(N-2,I)
319 AUX(N-2,I)=AUX(N-4,I)
320 AUX(N-3,I)=AUX(N-6,I)
321 AUX(N+6,I)=AUX(N+5,I)
322 AUX(N+5,I)=AUX(N+3,I)
323 AUX(N+4,I)=AUX(N+1,I)
324 DELI=AUX(N+6,I)+AUX(N+5,I)
325 DELI=DELI+DELI
326 AUX(16,I)=H.962962962962963D0*(Y(I)-AUX(N-3,I))
327 I-3.3611111111111111D0*H*(DERY(I)+DELI+AUX(N+4,I))
328 GO TO 201
329
330
331 H MUST BE HALVED
332 IF(IHLF-20)223,223,210
333
334 H=.5D0*H
335
336 18STEP=0
337 DO 224 I=1,NDIM
338 0Y(I)=390625D-2*(8.D1*AUX(N-1,I)+135.D0*AUX(N-2,I)+4.D1*AUX(N-3,I)
339 I+AUX(N-4,I))-1171875D0*(AUX(N+6,I)-6.D0*AUX(N+5,I)-AUX(N+4,I))*H
340 0AUX(N-4,I)=.390625D-2*(12.D0*AUX(N-1,I)+135.D0*AUX(N-2,I)+
341 218.D0*AUX(N+5,I))-9.D0*AUX(N+4,I))*H
342 AUX(N-3,I)=AUX(N-2,I)
343 AUX(N+4,I)=AUX(N+5,I)
344
345 DELI=X-(H+H)
346 CALL FC(DELI,Y,DERY)
347 DO 225 I=1,NDIM
348 AUX(N-2,I)=Y(I)
349 AUX(N+5,I)=DERY(I)
350 Y(I)=AUX(N-4,I)
351 DELI=DELI-(H+H)
352 CALL FC(DELI,Y,DERY)
353 DO 226 I=1,NDIM
354 DELI=AUX(N+5,I)+AUX(N+4,I)
355 DELI=DELI+DELI+DELI
356 AUX(16,I)=H.962962962962963D0*(AUX(N-1,I)-Y(I))
357 I-3.3611111111111111D0*H*(AUX(N+6,I)+DELI+DERY(I))
358 AUX(N+5,I)=DERY(I)
359 GO TO 206
360 END

```

```

DMCG3200
DMCG3210
DMCG3220
DMCG3230
DMCG3240
DMCG3250
DMCG3260
DMCG3270
DMCG3280
DMCG3290
DMCG3300
DMCG3310
DMCG3320
DMCG3330
DMCG3340
DMCG3350
DMCG3360
DMCG3370
DMCG3380
DMCG3390
DMCG3400
DMCG3410
DMCG3420
DMCG3430
DMCG3440
DMCG3450
DMCG3460
DMCG3470
DMCG3480
DMCG3490
DMCG3500
DMCG3510
DMCG3520
DMCG3530
DMCG3540
DMCG3550
DMCG3560
DMCG3570
DMCG3580
DMCG3590
DMCG3600
DMCG3610
DMCG3620
DMCG3630
DMCG3640

```

```

SUBROUTINE DREBS(DFN,Y,T,N,JM,IND,JSTART,H,HMIN,EPS,R,S,MK,IER)
-----LIBRARY 1-----
FUNCTION
  - FIRST ORDER DIFFERENTIAL EQUATION SOLVER -
  THE METHOD OF BULIRSCH - STOER FOR
  DY/DX = F(Y,T)
USAGE
  - CALL DREBS(DFN,Y,T,N,JM,IND,JSTART,H,HMIN,
  EPS,R,S,MK,IER)
PARAMETERS
  DFN      DFN      INTERNAL SUBROUTINE,
  Y        Y(1),Y(2),...Y(N) ARE INITIAL VALUES
  T        T        DFN MUST CALCULATE DY(1) =
  N        ON INPUT Y(1),Y(2),...Y(N) CONTAIN AN
  JM       ON APPROXIMATE SOLUTION TO Y AT T (AS SET ON
  IND      OUTPUT)
  JSTART   INDEPENDENT VARIABLE. ON INPUT, T
  H        SHOULD CONTAIN THE INITIAL VALUE OF THE
  HMIN     INDEPENDENT VARIABLE. ON OUTPUT, T
  EPS      CONTAINS THE UPDATED VALUE OF THE INDEPEN-
  R        DENT VARIABLE.
  S        THE NUMBER OF EQUATIONS IN THE SYSTEM
  MK       THE MAXIMUM ORDER OF THE RATIONAL APPROX-
  IER      IMATION. JM MUST BE LESS THAN 7.
  I        CONVERGENCE TYPE INDICATOR (INPUT)
  IND = 1 SPECIFIES THE STANDARD ERROR TEST
  IND = 2 SPECIFIES THE RELATIVE ERROR TEST
  IND = 3 SPECIFIES THE ABSOLUTE ERROR TEST
  JSTART = AN INPUT INDICATOR WITH THE FOLLOWING MEANINGS
  H        0 - PERFORM A STEP WITH THE FIRST VALUE OF JSTART SO
  H        1 - MUST BE DONE WITH THIS VALUE OF JSTART SO
  H        THAT THE SUBROUTINE CAN INITIALIZE ITSELF.
  H        -1 - REPEAT THE LAST STEP WITH A NEW VALUE
  H        OF H OR JM, SET TO THE INITIAL VALUES OF Y,
  H        DREBS AND TAKE FROM THE MOST RECENT CALL TO
  H        DREBS WITH JSTART = 0.
  H        ON INPUT, H IS AN INITIAL GUESS FOR THE STEP
  H        SIZE.
  H        ON OUTPUT, H CONTAINS A SUGGESTED STEP SIZE
  H        FOR THE NEXT STEP. THE SUGGESTED VALUE MAY
  H        BE LARGER OR SMALLER THAN THE ORIGINAL
  H        STEP SIZE.
  HMIN     HMIN IS THE SMALLEST PERMISSIBLE STEP SIZE.
  DREBS   DREBS WILL DECREASE THE STEP SIZE.

```

```

1 C
2 C
3 C
4 C
5 C
6 C
7 C
8 C
9 C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
18 C
19 C
20 C
21 C
22 C
23 C
24 C
25 C
26 C
27 C
28 C
29 C
30 C
31 C
32 C
33 C
34 C
35 C
36 C
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C

```



```

91  N7=N6+N5+N3
92  N8=N7+N5+N3
93  N2P1=V2+1
94  N3P1=V3+1
95  N8P1=V8+1
96  IF(JM.GT.0.AND.JM.LE.6) GO TO 5
97  IER = 66
98  JM=6
99
100 C C C
101 C C C
102 C C C
103 C C C
104 C C C
105 C C C
106 C C C
107 C C C
108 C C C
109 C C C
110 C C C
111 C C C
112 C C C
113 C C C
114 C C C
115 C C C
116 C C C
117 C C C
118 C C C
119 C C C
120 C C C
121 C C C
122 C C C
123 C C C
124 C C C
125 C C C
126 C C C
127 C C C
128 C C C
129 C C C
130 C C C
131 C C C
132 C C C
133 C C C
134 C C C
135 C C C

N7=N6+N5+N3
N8=N7+N5+N3
N2P1=V2+1
N3P1=V3+1
N8P1=V8+1
IF(JM.GT.0.AND.JM.LE.6) GO TO 5
IER = 66
JM=6

5  JMAX = JM+4
   JF(JSTART.NE.0) GO TO 135

   YOLD = T
   IJK4=V4
   DO 10 I = 1,N
     AK(I) = Y(I)
     IJK4=IJK4+1
     WK(IJK4) = S(I)
10  CONTINUE

   CALL OFN(Y,I,N,WK(N3P1))

15  BH = .FALSE.
    KUNVF = .TRUE.

20  A = H+T
    HU = .FALSE.

FOR AN EXTRAPOLATION OF ORDER JM,
JM+1 APPROXIMATIONS ARE REQUIRED.
THREE MORE ARE ALLOWED IN ATTEMPTING
TO ACHIEVE CONVERGENCE.

INITIALIZATION
SAVE THE INITIAL VALUES FOR THE DEP-
ENDENT VARIABLES AND THE ERROR TEST
VECTOR FOR THE STEP

USE THE FUNCTION ROUTINE TO OBTAIN
THE INITIAL SLOPES
DZ = DY/DX

THE LOGICAL VARIABLE, BH, DETERMINES
WHETHER THE STEP SIZE HAS BEEN
HALVED. INITIALLY FALSE.
LATER, BH IS FALSE IF THE STEP SIZE IS
CUT BY A FACTOR NUT 2

PRESET THE CONVERGENCE SUCCESS FLAG
TRUE

ADVANCE THE INDEPENDENT VARIABLE BY
THE STEP SIZE, H

SET THE SWITCH NO FOR THE FIRST SET
OF COEFFICIENTS, D

INITIALIZE THE H SEQUENCE...

```

```

136 C H/M,H/JR,H/JS
137 M = 1
138 JR = 2
139 JS = 3
140 CC
141 CC
142 CC
143 J = 0
144 CC
145
146 IJ6=N6-N
147 IJ7=N7-N
148 I6=IJ6
149 I7=IJ7
150 DO 125 J = 1,JMAX
151 CC
152 CC
153
154 IJ6=IJ6+N
155 IJ7=IJ7+N
156 IF (.NOT. BO) GO TO 25
157 D(2)=1.777777777778D0
158 D(4)=7.111111111111D0
159 D(6)=28.444444444444D0
160 GO TO 30
161 D(2)=2.25D0
162 D(4)=9.0D0
163 D(6)=36.0D0
164 CC
165 CC
166
167 K0VV = .TRUE.
168 IF (J.LE.(JM/2)) K0NV = .FALSE.
169 IF (J.LE.(JM+1)) GO TO 35
170 CC
171 CC
172 CC
173 L = JM+1
174 D(L) = 4.0D0*(L-2)
175 CC
176 CC
177 CC
178 FC = .7071068*FC
179 GO TO 40
180

```

H/M,H/JR,H/JS

JJ IS THE INDEX FOR THE ARRAY OF VALUES SAVED IN CASE THE INTERVAL MUST BE HALVED

INTEGRATION STEP
MIDPOINT + EXTRAPOLATION

SET THE VALUES OF THE EXTRAPOLATION COEFFICIENTS TO THEIR CORRECT VALUES FOR THIS EXTRAPOLATION STEP

IF THE ORDER OF THE EXTRAPOLATION STEP BEING COMPUTED IS LESS THAN JM/2 SET K0NV FALSE

RESTRICT THE ORDER OF THE EXTRAPOLATION TO JM

ADJUST THE EXTRAPOLATION COEFFICIENT

DISCOURAGE THE STEP-INCREASING FACTOR FC, BY A FACTOR OF SQRT(2) SINCE CONVERGENCE WAS NOT OBTAINED IN JM EXTRAPOLATIONS

```

181 C C C C C C C
182
183
184
185
186
187
188
189
190 C C C
191
192
193
194
195
196 C C C C C
197
198
199
200
201
202 C C
203
204
205
206
207
208
209
210
211
212
213
214
215
216
217 C
218
219
220
221
222
223
224
225

```

THE NUMBER, J, OF EXTRAPOLATIONS HAS
 NOT EXCEEDED JM
 FIND U(J) = ((H DIVIDED BY H/M)**2
 ADJUST THE FACTOR, FC, USED TO ADJUST
 THE STEPSIZE FOR THE NEXT STEP TO BE
 TAKEN

```

35 L = J
   U(L) = DFLOAT(M*M)
   FC = 1.0+FLOAT(JM+1-J)*.1666667

```

MODIFIED MIDPOINT RULE USED TO FIND
 FIRST VALUE FOR THIS EXTRAPOLATION
 STEP

```

40 M = M+M
   G = H/FLOAT(M)
   B = G+G

```

IF THE STEPSIZE HAS NOT BEEN HALVED
 OR IF THE ORDER OF THE EXTRAPOLATION
 STEP EXCEEDS THAT FOR WHICH PREVIOUS-
 LY COMPUTED VALUES WERE SAVED, THEY
 MUST BE COMPUTED

```

45 IF ((.NOT. BH) .OR. (J .GE. (JMAX-1))) GO TO 50

```

OTHERWISE THE VALUES HAVE BEEN SAVED
 AND CAN BE RESTORED

```

50 IJK1=N
   IJK2=N2
   IJK6=IJK6
   IJK7=IJK7
   DO 45 I = 1, N
     IJK2=IJK2+1
     IJK7=IJK7+1
     MK(IJK2) = MK(IJK7)
     IJK1=IJK1+1
     IJK6=IJK6+1
     MK(IJK1) = MK(IJK6)
   CONTINUE
   GO TO 75

```

COMPUTE STARTING VALUES FOR THE MODI-
 FIED MIDPOINT RULE

```

50 IJK1=N
   IJK2=N2
   IJK3=N3
   DO 55 I = 1, N
     IJK1=IJK1+1
     MK(IJK1) = MK(I)
     IJK2=IJK2+1

```

226 D1KB2350
 227 D1KB2360
 228 D1KB2370
 229 D1KB2380
 230 D1KB2390
 231 D1KB2400
 232 D1KB2410
 233 D1KB2420
 234 D1KB2430
 235 D1KB2440
 236 D1KB2450
 237 D1KB2460
 238 D1KB2470
 239 D1KB2480
 240 D1KB2490
 241 D1KB2500
 242 D1KB2510
 243 D1KB2520
 244 D1KB2530
 245 D1KB2540
 246 D1KB2550
 247 D1KB2560
 248 D1KB2570
 249 D1KB2580
 250 D1KB2590
 251 D1KB2600
 252 D1KB2610
 253 D1KB2620
 254 D1KB2630
 255 D1KB2640
 256 D1KB2650
 257 D1KB2660
 258 D1KB2670
 259 D1KB2680
 260 D1KB2690
 261 D1KB2700
 262 D1KB2710
 263 D1KB2720
 264 D1KB2730
 265 D1KB2740
 266 D1KB2750
 267 D1KB2760
 268 D1KB2770
 269 D1KB2780
 270 D1KB2790

IJK3=IJK3+1
 WK(IJK2) = WK(I)+G*WK(IJK3)
 CONTINUE
 KH = W/2
 XU=1

THE MEMBER OF THE H SEQUENCE
 BEING USED BY THE MIDPOINT INTEGRA-
 TION RULE IS H/M. COMPUTE THE END
 OF THE STEP FOR EACH DEPENDENT VARI-
 ABLE

55 DO 70 K = 2,M
 XU = XU + G
 CALL OFN(WK(N2P1),XU,N,WK(N6P1))
 IJK1=N
 IJK2=N2
 IJK8=N8
 DU 60 I = 1,N
 IJK1=IJK1+1
 IJK8=IJK8+1
 U = WK(IJK1) + B*WK(IJK8)
 IJK2=IJK2+1
 WK(IJK1) = WK(IJK2)
 WK(IJK2) = U
 CONTINUE

60 IF ((K .NE. KH) .OR. (K .EQ. 3)) GO TO 70
 JJ = 1+JJ
 I6=I6+N
 I7=I7+N
 IJK1=N
 IJK2=N2
 IJK6=I6
 IJK7=I7
 DU 65 I = 1,N
 IJK2=IJK2+1
 IJK7=IJK7+1
 WK(IJK7) = WK(IJK2)
 IJK6=IJK6+1
 IJK1=IJK1+1
 WK(IJK6) = WK(IJK1)
 CONTINUE
 65 CONTINUE
 70 CALL OFN(WK(N2P1),A,N,WK(N6P1))
 75

IN CASE THE INTERVAL MUST BE HALVED
 NEXT TIME, SAVE THE VALUES AT HALFWAY
 ALONG (KH=N/2) THE STEP UNLESS KE3
 GO TO 70

226 CCCCC
 227 CCCCC
 228 CCCCC
 229 CCCCC
 230 CCCCC
 231 CCCCC
 232 CCCCC
 233 CCCCC
 234 CCCCC
 235 CCCCC
 236 CCCCC
 237 CCCCC
 238 CCCCC
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 262 CCCCC
 263 CCCCC
 264 CCCCC
 265 CCCCC
 266 CCCCC
 267 CCCCC
 268 CCCCC
 269 CCCCC
 270 CCCCC

DFR2800
 DFR2810
 DFR2820
 DFR2830
 DFR2840
 DFR2850
 DFR2860
 DFR2870
 DFR2880
 DFR2890
 DFR2900
 DFR2910
 DFR2920
 DFR2930
 DFR2940
 DFR2950
 DFR2960
 DFR2970
 DFR2980
 DFR2990
 DFR3000
 DFR3010
 DFR3020
 DFR3030
 DFR3040
 DFR3050
 DFR3060
 DFR3070
 DFR3080
 DFR3090
 DFR3100
 DFR3120
 DFR3130
 DFR3140
 DFR3150
 DFR3160
 DFR3170
 DFR3180
 DFR3190
 DFR3200
 DFR3210
 DFR3220
 DFR3230
 DFR3240
 DFR3250

V IS USED TO SAVE THE VALUE OBTAINED
 BY THE MIDPOINT RULE USING THE PREVIOUS
 MEMBER OF THE H SEQUENCE
 (THE FIRST TIME THROUGH THIS VALUE IS
 MEANINGLESS, BUT IT IS NOT USED SINCE
 L IS LESS THAN 2)
 COMPUTE THE FINAL VALUE OBTAINED FOR
 THIS MEMBER OF THE H SEQUENCE BY THE
 MODIFIED MIDPOINT RULE
 IF (L .GE. 2) V = WK(IJK5)
 IJK1=IJK1+1
 IJK2=IJK2+1
 IJK5=IJK5+1
 IK5=IK5+1
 IF (L .GE. 2) V = WK(IJK5)
 IJK8=IJK8+1
 WK(IJK5) = (WK(IJK2) + WK(IJK8)) * HALF
 C = WK(IJK5)
 IA = C
 IF (L .LT. 2) GO TO 90
 AT LEAST TWO VALUES ARE NEEDED TO
 START EXTRAPOLATION
 IF THE VALUE JUST COMPUTED BY THE
 MIDPOINT RULE SHOWS A LARGE JUMP FROM
 THE PREVIOUS, HALVE THE INTERVAL
 DABS(C) .AND. (H .NE. HMIN) .AND.
 (J.GT.JM/2+1) .GO
 IF ((DABS(V)*ZDUP) .LT.
 (J.GT.JM/2+1)) .GO
 PERFORM THE L STEPS FOR THE CURRENT
 ORDER EXTRAPOLATION STEP IF THE
 DENOMINATOR OF THE RATIONAL FUNCTION
 GOES TO ZERO AT ANY STEP, SET AT
 THAT STEP TO ITS VALUE JUST BEFORE

IJK1=N
 IJK2=N2
 IJK5=N5
 IK5=N5
 IJK8=N8
 DO 115 I = 1,N
 IJK1=IJK1+1
 IJK2=IJK2+1
 IJK5=IJK5+1
 IK5=IK5+1
 IF (L .GE. 2) V = WK(IJK5)
 IJK8=IJK8+1
 WK(IJK5) = (WK(IJK2) + WK(IJK8)) * HALF
 C = WK(IJK5)
 IA = C
 IF (L .LT. 2) GO TO 90
 AT LEAST TWO VALUES ARE NEEDED TO
 START EXTRAPOLATION
 IF THE VALUE JUST COMPUTED BY THE
 MIDPOINT RULE SHOWS A LARGE JUMP FROM
 THE PREVIOUS, HALVE THE INTERVAL
 DABS(C) .AND. (H .NE. HMIN) .AND.
 (J.GT.JM/2+1) .GO
 IF ((DABS(V)*ZDUP) .LT.
 (J.GT.JM/2+1)) .GO
 PERFORM THE L STEPS FOR THE CURRENT
 ORDER EXTRAPOLATION STEP IF THE
 DENOMINATOR OF THE RATIONAL FUNCTION
 GOES TO ZERO AT ANY STEP, SET AT
 THAT STEP TO ITS VALUE JUST BEFORE

271 C C C C C
 272
 273
 274
 275
 276
 277 C C C C C
 278
 279
 280 C C C C C
 281
 282
 283
 284
 285
 286
 287
 288 C C C
 289
 290 C
 291
 292 C
 293
 294 C
 295 C
 296
 297 C C C
 298
 299 C C C
 300
 301
 302 C C C C C
 303
 304
 305 C C C C C
 306
 307
 308
 309
 310
 311
 312
 313
 314
 315

```

316 U = C*H
317 C = H1*H
318 IF(K-LI.L) V=WK(IP5)
319 WK(IP5) = U
320 HA = U + 1A
321 CONTINUE
322 C
323 C
324 C
325 GO TO (95,100,105),IND
326 UST=DABS(IA)
327 IF(UST.GT.S(I)) S(I)=UST
328 GO TO 110
329 S(I)=DABS(Y(I))
330 GO TO 110
331 S(I)=1
332 R(I)=DABS(Y(I)-IA)
333 Y(I)=IA
334 IF(S(I).LT.EPS) S(I)=EPS
335 IF(R(I).GT.EPS*S(I)) KONV=.FALSE.
336 CONTINUE
337 IF(KONV) GO TO 155
338 C
339 D(3) = 4.
340 D(5) = 16.
341 C
342 C
343 C
344 C
345 BU = (.NOT.BU)
346 IJK4=N4
347 DO 120 J=1,N
348 IJK4=IJK4+1
349 S(I)=WK(IJK4)
350 CONTINUE
351 C
352 C
353 M = JK
354 JR = JS
355 JS = M+M
356 C
357 C
358 C
359 C
360 125 CONTINUE

```

USE THE ERROR ROUTINE FOR EACH
DEPENDENT VARIABLE TO CHECK WHETHER
CONVERGENCE HAS BEEN ACHIEVED

RESET THE EXTRAPOLATION COEFFICIENTS

FLIP THE BU SWITCH FOR THE NEXT SET
OF COEFFICIENTS

RESET S

TAKE THE NEXT MEMBER
OF THE H SEQUENCE

AND GO BACK FOR THE
NEXT EXTRAPOLATION

IF, AFTER ALL THE EXTRAPOLATIONS
ALLOWED, CONVERGENCE HAS NOT BEEN
ACHIEVED, ATTEMPT TO HALVE H SO THAT

DIRB3260
DIRB3270
DIRB3280
DIRB3290
DIRB3300
DIRB3310
DIRB3320
DIRB3330
DIRB3340
DIRB3350
DIRB3360
DIRB3370
DIRB3380
DIRB3390
DIRB3400
DIRB3410
DIRB3420
DIRB3430
DIRB3440
DIRB3450
DIRB3460
DIRB3470
DIRB3480
DIRB3490
DIRB3500
DIRB3510
DIRB3520
DIRB3530
DIRB3540
DIRB3550
DIRB3560
DIRB3570
DIRB3580
DIRB3590
DIRB3600
DIRB3610
DIRB3620
DIRB3630
DIRB3640
DIRB3650
DIRB3660
DIRB3670
DIRB3680
DIRB3690
DIRB3700
DIRB3710
DIRB3720
DIRB3730

```

361 C
362 C
363 C
364 C
365 C
366 C
367 C
368 C
369 C
370 C
371 C
372 C
373 C
374 C
375 C
376 C
377 C
378 C
379 C
380 C
381 C
382 C
383 C
384 C
385 C
386 C
387 C
388 C
389 C
390 C
391 C
392 C
393 C
394 C
395 C
396 C
397 C
398 C
399 C
400 C
401 C

THE SAVED VALUES CAN BE USED (SET BH
TRUE FJR THIS PURPOSE)
IF HALVING H MAKES IT LESS THAN HMIN,
SET H = HMIN
IN THIS CASE THE SAVED VALUES CANNOT
BE USED
IF H HAD ALREADY BEEN AT HMIN,
CONVERGENCE CANNOT BE ACHIEVED FOR
THIS HMIN AND THIS EPS CRITERION.
SET KUNV FALSE

HH = (.NOT. BH)
IF (DABS(H) .LE. DABS(HMIN)) GO TO 150
H = H * HALF
IF (DABS(H) .GE. DABS(HMIN)) GO TO 20
H = DSIGN(HMIN,H)
GO TO 15
DO 140 I = 1,N
Y(I) = WK(I)
CONTINUE
IJK4=V4
DO 145 I=1,N
IJK4=IJK4+1
S(I)=WK(IJK4)
CONTINUE
I = IJLD
GO TO 15
KUNV = .FALSE.

H = FC*H
IF(KUNV) GO TO 160
IER=129
IF(IER.EQ.0) GO TO 9005
CONTINUE
CALL JERIST (IER,6HDREIS )
RETURN
END

WHEATHER OR NOT CONVERGENCE HAS BEEN
ACHIEVED SET A NEW SUGGESTED STEPSIZE
FOR THE NEXT STEP
ASSIGN THE END OF STEP VALUE TO THE
INDEPENDENT VARIABLE

```

```

1  C
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
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27
28
29
30
31
32
33
34
35

SUBROUTINE UERTST(IER,NAME)
  DIMENSION IYYP(5,4),IBIT(4)
  INTEGER*2 IER2=IER
  EQUIVALENCE IYYP,IBIT
  DATA IYYP / 32,04,128,0 /
  * * * *
  * IER1=4
  * GO TO 20
  * IF (IER2 .LT. IER1) GO TO 10
  * IER1=3
  * GO TO 20
  * IF (IER2 .LT. IER1) GO TO 15
  * IER1=2
  * GO TO 20
  * IER1=1
  * IER2=IER2-IBIT(IER1)
  * WRITE (PRINTK,25) (IYYP(I,IER1),I=1,5),NAME,IER2,IER
  * FORMAT('*** I M S L(UERTST) ***',5A4,4X,3A2,4X,12,
  * * * *
  * RETURN
  * END

  IYYP(5,4),IBIT(4)
  NAME(3)
  WARN,WARF,TERM,PRINTR
  (IBIT(1),WARN),(IBIT(2),WARF),(IBIT(3),TERM)
  (IBIT(4),PRINTR)
  (WARN,ING),(WITH,FI)
  (TERM,INAL),(NON-DEFI,NED)
  (NON-DEFI,NED)
  / 32,04,128,0 /
  / 6 /
  DATA IER1=4
  IER2=IER
  IF (IER2 .GE. WARN) GO TO 5
  IER1=4
  GO TO 20
  IF (IER2 .LT. IER1) GO TO 10
  IER1=3
  GO TO 20
  IF (IER2 .LT. IER1) GO TO 15
  IER1=2
  GO TO 20
  IER1=1
  IER2=IER2-IBIT(IER1)
  WRITE (PRINTK,25) (IYYP(I,IER1),I=1,5),NAME,IER2,IER
  FORMAT('*** I M S L(UERTST) ***',5A4,4X,3A2,4X,12,
  RETURN
  END

  NON-DEFINED
  TERMINAL
  WARNING(WITH FIX)
  WARNING
  EXTRACT 'M'
  PRINT ERROR MESSAGE
  I=1,5),NAME,IER2,IER
  ,5A4,4X,3A2,4X,12,

```



```

1 C
2 C
3 C
4 C
5 C
6 C
7 C
8 C
9 C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
18 C
19 C
20 C
21 C
22 C
23 C
24 C
25 C
26 C
27 C
28 C
29 C
30 C
31 C
32 C
33 C
34 C
35 C
36 C
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C

SUBROUTINE DVOGER(Y, I, N, MTH, MAXDER, JSTART, H, HMIN, HMAX, EPS,
YMAX, EKOR, WK, IER)
LIBRARY 1-----D-----LHRRARY 1-----D-----
FUNCTION
USAGE
PARAMETERS DFUN

- FIRST ORDER DIFFERENTIAL EQUATION SOLVER-
GEAR'S METHOD FOR  $DX/DT = F(X, T)$ 
CALL DVOGER(DFUN, Y, I, N, MTH, MAXDER, JSTART, H,
HMIN, HMAX, EPS, WK, IER)
USER SUPPLIED EXTERNAL SUBROUTINE, DFUN(Y, TP,
M, DY, PW, IND), WHERE
M, YP CONTAINS THE PRESENT (I.E. AT TP)
SOLUTION VECTOR AS  $X(1) = YP(1, 1)$ ,
 $X(2) = YP(1, 2)$ , ...,  $X(N) = YP(1, N)$ ,
TP IS THE ORDER OF THE JACOBIAN.
M IS THE ORDER OF THE JACOBIAN.
IF IND=0, DFUN MUST COMPUTE THE N-VECTOR
F(Y, TP) AND STORE THE VALUES IN DY.
IF IND=1, DFUN MUST COMPUTE THE JACOBIAN OF
F EVALUATED AT (Y, TP) AND STORE THE
RESULT IN THE M BY M MATRIX PW.
THE JACOBIAN IS COMPUTED ONLY FOR CALLS WITH
MTH=1.
YP IS AN 8 BY N ARRAY. THE SOLUTION COMPONENTS
ARE  $Y(1, 1), Y(1, 2), \dots, Y(1, N)$ 
IS A TWO DIMENSIONAL ARRAY (8 BY N)
CONTAINING THE DEPENDENT VARIABLES AND THEIR
SCALED DERIVATIVES. THE SOLUTION COMPONENTS
ARE  $X(1) = Y(1, 1), X(2) = Y(1, 2), \dots$ 
 $X(N) = Y(1, N)$  AND  $Y(J+1, I)$  CONTAINS THE J-TH
DERIVATIVE OF  $X(I)$  SCALED BY  $H**J/FACTORIAL$ 
(J). HERE H IS THE CURRENT STEP SIZE.
ONLY  $Y(1, 1), I=1, 2, \dots, N$  NEED BE PROVIDED BY
THE CALLING PROGRAM IN THE FIRST CALL TO
DVOGER, WITH  $JSTART = 0$ .
IS THE INDEPENDENT VARIABLE. ON INPUT, I
SHOULD CONTAIN THE INITIAL VALUE OF THE
INDEPENDENT VARIABLE. ON OUTPUT, I
CONTAINS THE UPDATED VALUE OF THE INDEPEN-
DENT VARIABLE.
N IS THE NUMBER OF FIRST ORDER DIFFERENTIAL
EQUATIONS.
MTH IS THE METHOD INDICATOR. THE USER MAY
SELECT ONE OF THE FOLLOWING.
METHOD INDICATES A PREDICTOR-CORRECTOR
(ADAMS) METHOD

```

```

DVOG1300
DVOG0020
DVOG0030
DVOG0040
DVOG0050
DVOG0060
DVOG0070
DVOG0080
DVOG0090
DVOG0100
DVOG0110
DVOG0120
DVOG0130
DVOG0140
DVOG0150
DVOG0160
DVOG0170
DVOG0180
DVOG0190
DVOG0200
DVOG0210
DVOG0220
DVOG0230
DVOG0240
DVOG0250
DVOG0260
DVOG0270
DVOG0280
DVOG0290
DVOG0300
DVOG0310
DVOG0320
DVOG0330
DVOG0340
DVOG0350
DVOG0360
DVOG0370
DVOG0380
DVOG0390
DVOG0400
DVOG0410
DVOG0420
DVOG0430
DVOG0440
DVOG0450

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46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C
58 C
59 C
60 C
61 C
62 C
63 C
64 C
65 C
66 C
67 C
68 C
69 C
70 C
71 C
72 C
73 C
74 C
75 C
76 C
77 C
78 C
79 C
80 C
81 C
82 C
83 C
84 C
85 C
86 C
87 C
88 C
89 C
90 C

DV060460
DV060470
DV060480
DV060490
DV060500
DV060510
DV060520
DV060530
DV060540
DV060550
LV060560
DV060570
DV060580
DV060590
DV060600
DV060610
DV060620
DV060630
DV060640
DV060650
DV060660
DV060670
DV060680
DV060690
DV060700
DV060710
DV060720
DV060730
DV060740
DV060750
DV060760
DV060770
DV060780
DV060790
DV060800
DV060810
DV060820
DV060830
DV060840
DV060850
DV060860
DV060870
DV060880
DV060890
DV060900

MH=1 INDICATES A VARIABLE-ORDER METHOD
 SUITABLE FOR SYSTEMS OF STIFF DIFFER-
 ENTIAL EQUATIONS. HERE THE USER MUST
 PROVIDE THE PARTIAL DERIVATIVES OF THE
 DIFFERENTIAL EQUATIONS WITH RESPECT TO
 THE X'S, THE JACOBIAN. THIS IS
 DONE IN THE CALL TO DFUN(Y,P,4,DY,PW,
 IND) WITH IND=1. ON OUTPUT, PNI(J,
 I) IS THE DERIVATIVE OF THE I-TH EQUATION
 WITH RESPECT TO X(J).
 MTH=2 INDICATES A VARIABLE-ORDER METHOD,
 BUT DVOGER COMPUTES THE PARTIAL DERIVA-
 TIVES BY NUMERICAL DIFFERENCING. HENCE,
 DFUN IS CALLED WITH INDEX=0 ONLY.
 MAXDER - MAXDER MUST BE USED BY THE MAXIMUM
 ORDER TO BE USED IN THE APPROXIMATION.
 IT MUST BE LESS THAN R FOR THE ADAMS METHOD
 AND LESS THAN 7 FOR THE STIFF METHODS.
 JSTART - ON INPUT, JSTART HAS THE FOLLOWING MEANINGS...
 -1 -- REPEAT THE LAST STEP WITH A NEW VALUE
 0 -- INITIALIZE THE INTEGRATION. THE FIRST
 CALL TO DVOGER MUST BE DONE WITH THIS
 VALUE OF JSTART
 +1 -- TAKE A NEW STEP CONTINUING FROM THE
 ON OUTPUT, JSTART IS SET TO 0, THE CURRENT
 ORDER OF THE METHOD. JSTART IS ALSO THE
 ORDER OF THE MAXIMUM DERIVATIVE AVAILABLE IN
 Y
 H - ON INPUT, H CONTAINS THE STEP SIZE TO BE
 ATTEMPTED ON THE NEXT STEP. IF THIS STEP
 SIZE DOES NOT CAUSE A LARGER ERROR THAN
 REQUESTED, IT WILL BE USED. OTHERWISE, SEE
 PARAMETER TOL. THE USER IS ADVISED TO USE
 A FAIRLY SMALL STEP IN THE FIRST CALL TO
 DVOGER.
 ON OUTPUT, H CONTAINS A SUGGESTED STEP SIZE
 FOR THE NEXT STEP IN ORDER TO ACHIEVE AN
 ECONOMICAL INTEGRATION.
 HMIN - ON INPUT, HMIN MUST BE THE SMALLEST STEP SIZE
 ALLOWABLE IN THIS INTEGRATION. HMIN SHOULD
 BE MUCH SMALLER THAN THE EXPECTED AVERAGE
 STEP SIZE FOR THE FIRST CALL SINCE A FIRST

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91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135
ORDER METHOD IS USED INITIALLY. STEP SIZE
HMAX MUST BE SET TO THE LARGEST STEP SIZE
HMAX ALLOWABLE IN THIS INTEGRATION.
EPS IS USED TO SPECIFY THE MAXIMUM ERROR
CRITERION, THE STEP SIZE AND/OR THE ORDER IS
ADJUSTED SO THAT THE SINGLE STEP ERROR ESTI-
MATES DIVIDED BY YMAX(I) ARE LESS THAN
EPS IN THE EUCLIDEAN NORM.
YMAX IS AN N-VECTOR WHICH CONTAINS THE MAXIMUM
ABSOLUTE VALUE OF EACH COMPONENT OF X CAL-
CULATED SO FAR. THE COMPONENTS OF YMAX
SHOULD NORMALLY BE SET TO 1. BEFORE THE
FIRST CALL TO DVGGR, WHICH CONTAINS THE ESTI-
MATED ONE STEP ERROR IN EACH COMPONENT.
WK (N*(17) IF MTH = 0
  (N*(17) OTHERWISE
  N*(N+17) OTHERWISE
  N*(N+17) OTHERWISE
IER ERROR METER
  WARNING ERROR = 32 + N STEP WAS TAKEN WITH
  N = 1 MIN, BUT THE REQUESTED ERROR WAS NOT
  ACHIEVED
  N = 2 INDICATES CONVERGENCE COULD
  NOT BE ACHIEVED FOR H GREATER THAN HMIN
  N = 3 INDICATES THE REQUESTED ERROR IS
  SMALLER THAN CAN BE HANDLED FOR THIS
  PROBLEM
  WAKN = 4 INDICATES (WITH FIX J) = 64 + N
  ORDER SPECIFIED
  N = 4 INDICATES THE MAXIMUM ORDER
  WAS TOO LARGE. THE MAXIMUM
  ORDER WAS SET TO 7 FOR MTH = 0 AND
  TO 6 OTHERWISE.
PRECISION SINGLE/DOUBLE
REGD. LUDATF, LUELMF, UERTST
LANGUAGE FORTRAN
LATEST REVISION - MARCH 18, 1975
*
DIMENSION YMAX, ERROR, WK, IER
Y(8, N), YMAX(N), ERROR(N), WK(84, 4),
C(8), COEF(7, 2, 3)
C, D, E, H, I, Y, R1, BND, EPS, EUP, EOWN, ENGI, D1, D2,
ENU2, ENU3, HMAX, HMIN, HNEW, HOLD, TOLD, YMAX,

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181 C
182 C
183 C
184 C
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197 C
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200 C
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221 C
222 C
223 C
224 C
225 C

10 IF (JSTART .LE. 0) GO TO 35
15 DO 20 I = 1,N
    DO 20 J = 1,K
        WK(N4+J,I)=Y(J,I)
20 CONTINUE
    HNEW = HNEW HOLD) GO TO 30
    IF (H .EQ. HOLD) GO TO 30
25 RACUM = H/HOLD
    IRETA = 1
    GO TO 375
30 IOLD = IO
    TOLD = T
    RACUM = ONE
    IF (JSTART .GT. 0) GO TO 135
    GO TO 50
35 JF (JSTART .EQ. -1) GO TO .45
    IO = 1
    CALL DFUN(Y,T,N,WK(N2,1),WK,0)
    DO 40 I = 1,N
        N1 = N1 + I
        Y(2,I)=WK(N11,1)*H
40 CONTINUE
    HNEW = H
    K = 2
    GO TO 15
45 IF (IO .EQ. IOOLD) JSTART = 1
    I = IOOLD
    IO = IOOLD
    K = IJ + 1
    GO TO 25
50 IF (MTH .EQ. 0) GO TO 55
    GO TO (95,100,105,110,115,120),IO
55 GO TO (60,65,70,75,80,85,90),IO
60 C(1) = -ONE

```

TAKE A STEP CONTINUING FROM THE LAST
STEP SAVE INFORMATION FOR A POSSIBLE
RESTART AND CHECK H FOR A POSSIBLE
USER CHANGE. HNEW IS THE PREVIOUS
STEP SIZE AND IO IS THE CURRENT ORDER

FIRST CALL. THE ORDER IS SET TO 1 AND
THE INITIAL DERIVATIVES CALCULATED.

REPEAT LAST STEP. RESTORE THE SAVED
INFORMATION.

SET ALL COEFFICIENTS DETERMINED BY
THE ORDER AND THE METHOD TYPE.

DVUG22H0
DVUG2290
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DVUG2470
DVUG2480
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DVUG2500
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DVUG2940
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DVUG2970
DVUG2990
DVUG3000
DVUG3010

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2265
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2270

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90
95
100
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110

GO TO 125
C(1)=-HALF
C(3)=-HALF
GO TO 125
C(1)=-0.4166666666666667D0
C(3)=-0.75D0
C(4)=-0.1666666666666667D0
GO TO 125
C(1)=-0.375D0
C(3)=-0.9166666666666667D0
C(4)=-0.3333333333333333D0
C(5)=-0.0416666666666667D0
GO TO 125
C(1)=-0.3486111111111111D0
C(3)=-1.0416666666666667D0
C(4)=-0.4861111111111111D0
C(5)=-0.1041666666666667D0
C(6)=-0.0083333333333333D0
GO TO 125
C(1)=-0.3298611111111111D0
C(3)=-1.1416666666666667D0
C(4)=-0.625D0
C(5)=-0.1770833333333333D0
C(6)=-0.025D0
C(7)=-0.0013888888888889D0
GO TO 125
C(1)=-0.3155919312169312D0
C(3)=-1.225D0
C(4)=-0.7518518518518519D0
C(5)=-0.2552083333333333D0
C(6)=-0.0486111111111111D0
C(7)=-0.4861111111111111D0-2
C(8)=-1.1984126984126984D0-3
GO TO 125
C(1)=-ONE
GO TO 125
C(1)=-0.6666666666666667D0
C(3)=-0.3333333333333333D0
GO TO 125
C(1)=-0.5454545454545455D0
C(3)=-0.090909090909091D0
GO TO 125
C(1)=-0.48D0
C(3)=-0.7D0

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C(4) = -0.200
C(5) = -0.0200
GO TO 125
C(1) = -0.43795620437956200
C(3) = -0.821167883211678800
C(4) = -0.310218978102189800
C(5) = -0.05474452555474452600
C(6) = -0.003649635036496350400
GO TO 125
C(1) = -0.408163265306122500
C(3) = -0.920634920634920600
C(4) = -0.41666666666666700
C(5) = -0.099206349206349200
C(6) = -0.011904761904761900
C(7) = -0.00056689342403628200
    IF THE JACOBIAN MUST BE RE-CALCULATED
    BECAUSE OF AN ORDER CHANGE, SET
    IWEVAL POSITIVE IF IT HAS NOT YET BEEN
    DONE (IREF=1) OR SKIP TO A FINAL SCALING
    (IREF=2). DVOG3370
    IF IT HAS BEEN COMPLETED (IREF=2),
    IWEVAL IS USED FOR COMPARISON OF ERRORS
    IN THE CURRENT ORDER, EDWN IS USED TO
    INCREASE THE ORDER, EDWN IS USED TO
    DECREASE THE ORDER.
    K = IO+1
    IDOUB = (4 - MTH)/2
    MTYP = HALF/(IO + 1)
    ENQ2 = HALF/(IO + 2)
    ENQ3 = HALF/(IO)
    PEP SH = EPS
    EUP = (COEF(IO,MTYP,2)*PEPSH)**2
    EDWN = (COEF(IO,MTYP,1)*PEPSH)**2
    IF (EDWN.EQ.0) GO TO 390
    BND = EPS*ENQ3/N
    IWEVAL = MTH
    GO TO (135,340), IRET
  
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IF THE JACOBIAN MUST BE RE-CALCULATED
 BECAUSE OF AN ORDER CHANGE, SET
 IWEVAL POSITIVE IF IT HAS NOT YET BEEN
 DONE (IREF=1) OR SKIP TO A FINAL SCALING
 (IREF=2). DVOG3370
 IF IT HAS BEEN COMPLETED (IREF=2),
 IWEVAL IS USED FOR COMPARISON OF ERRORS
 IN THE CURRENT ORDER, EDWN IS USED TO
 INCREASE THE ORDER, EDWN IS USED TO
 DECREASE THE ORDER.

COMPUTE THE PREDICTED Y VALUES BY
 EFFECTIVELY MULTIPLYING THE SAVED
 INFORMATION BY THE PASCAL TRIANGLE
 MATRIX.

```

316 DO 140 J1 = J1,K + J1 + J - 1
317 J2 = K - J1 + J - 1
318 DO 140 I = 1,N
319 Y(J2,I) = Y(J2,I) + Y(J2+1,I)
320
321 140 CONTINUE
322
323 CCCCCCCCCC
324
325 TAKE UP TO 3 CORRECTOR ITERATIONS.
326 CONVERGENCE IS TESTED BY REQUIRING
327 CHANGES TO BE LESS THAN BND.
328 THE SUMS OF THE CORRECTIONS ARE
329 ACCUMULATED IN THE ARRAY ERKOK(I).
330 IS EQUAL TO THE K-TH DERIVATIVE OF
331 MULTIPLIED BY H**K/(FACTORIAL(K-1)
332 (C(K))). ERROR(I) IS THE REFERENCE PRO-
333 PORTIONAL TO THE ACTUAL ERRORS IN THE
334 LOWEST POWER OF H PRESENT. (H**K)
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DVUG4010
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DO 145 I = 1,N
ERROR(I) = ZERO
CONTINUE
DO 220 L = 1,3
CALL DFUN(Y,T,N,WK(N2,1),WK 0)
IF THERE HAS BEEN A CHANGE OF ORDER
OR THERE HAS BEEN TROUBLE WITH CON-
VERGENCE THE JACOBIAN IS RE-EVALU-
ATED PRIOR TO STARTING THE CORRECTOR
ITERATION IN THE CASE OF STIFF
METHODS. IMEVAL IS THEN SET TO -1 AS
AN INDICATOR THAT IT HAS BEEN DONE.
IF (IMEVAL .LT. 1) GO TO 185
IF (MTH .EQ. 2) GO TO 165
CALL DFUN(Y,T,N3,WK,WK,1)
R = C(1)*H
DO 150 I = 1,N4
WK(I,1) = WK(I,1)*R
CONTINUE
N11 = N3 + 1
N12 = N*N11 - N3
DO 160 I = 1,N12,N11
WK(I,1) = WK(I,1)+ONE
CONTINUE
IMEVAL = -1
IF(N.EQ.1) GO TO 185
CALL LUDAIF(WK,WK,N,N3,NDIG,D1,D2,WK(N7,1),WK(N8,1),WK(N9,1),
KER)
IF (KER) 185,185,225

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CCCCCCCCC
CCCCCCCCC
C

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361 DO 170 I = 1,N
362 WK(IND9,I)=Y(1,I)
363 CONTINUE
364 DO 180 J = 1,N
365 K=EPS*DMAX1(EPS,DABS(WK(IND9,J)))
366 Y(1,J) = Y(1,J) + R
367 D = C(1)*H/R
368 CALL DFUN(Y,I,N,WK(N6,1),WK,0)
369 DO 175 I = 1,N
370 N11 = N5 + I
371 N12 = N1 + I
372 N13 = N1 + I
373 WK(N11,1)=(WK(N12,1)-WK(N13,1))*D
374 CONTINUE
375 Y(1,J)=WK(IND9,J)
376 CONTINUE
377 GO TO 155
378 IF (MTH .NE. 0) GO TO 195
379 DO 190 I = 1,N
380 N11 = N1 + I
381 WK(IND9,I)=Y(2,I)-WK(N11,1)*H
382 CONTINUE
383 GO TO 210
384 DO 200 I = 1,N
385 N11 = N5 + I
386 N12 = N1 + I
387 WK(N11,1)=Y(2,I)-WK(N12,1)*H
388 CONTINUE
389 GO TO 202
390 IF(N.GT.1) GO TO 202
391 WK(N8,1) = WK(N6,1) / WK(1,1)
392 CALL LUFLMF(WK,WK(N6,1),WK(N7,1),N,N3,WK(N8,1))
393 GO TO 203
394 DO 205 I=1,N
395 WK(IND9,I)=WK(N10+I,1)
396 CONTINUE
397 NT = N
398 DO 215 I = 1,N
399 I) = Y(1,I)+C(1)*WK(IND9,I)
400 Y(2,I) = Y(2,I)-WK(IND9,I)
401 ERROR(I)=ERROR(I)+WK(IND9,I)
402 IF (DABS(WK(IND9,I)).LE. (BND*YMAX(I))) NT=NT-1
403 CONTINUE
404 IF (NT .LE. 0) GO TO 245
405 THE CORRECTOR FAILED TO CONVERGE IN 3

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DV0G4070
DV0G4080
DV0G4090
DV0G4100
DV0G4110
DV0G4130
DV0G4140
DV0G4150
DV0G4160
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DV0G4190
DV0G4200
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DV0G4240
DV0G4250
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DV0G4330
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DV0G4370
DV0G4380
DV0G4390
DV0G4400
DV0G4410
DV0G4420
DV0G4430
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DV0G4460
DV0G4470
DV0G4480
DV0G4500
DV0G4510
DV0G4520
DV0G4530

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ITERATIONS, VARIOUS POSSIBILITIES ARE
 CHECKED. IF H IS EQUAL TO HMIN AND
 THIS IS THE ADAMS METHOD OR A STIFF
 METHOD IN WHICH THE JACOBIAN HAS
 ALREADY BEEN RE-EVALUATED, A NO CON-
 VERGENCE EXIT IS TAKEN, OTHERWISE THE
 JACOBIAN IS RE-EVALUATED AND/OR THE
 STEP IS REDUCED TO TRY TO OBTAIN
 CONVERGENCE.

406 C
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 450 C

```

225 I = I - H
    IF ((DABS(H) .LE. (DABS(HMIN)*ONEP)) .AND. ((IMEVAL - M1YP) .LT.
    * IF ((MTH .EQ. 0) .OR. (IMEVAL .NE. 0)) RACUM = RACUM*0.25
    IMEVAL = MTH
    GO TO 375
    IMEVAL = 2
    KFLAG = -3
    DO 240 I = 1, N
    DO 240 J = 1, K
    Y(J, I) = WK(N4+J, I)
240 CONTINUE
    H = HOLD
    IO = IOOLD
    JSTART = IO
    GO TO 395
  
```

THE CORRECTOR CONVERGED AND CONTROL
 IS PASSED TO STATEMENT 260 IF THE
 ERROR TEST IS PASSED, AND TO 270
 OTHERWISE. STEP IS O.K. IT IS ACCEPTED.
 IF IDOUB HAS BEEN REDUCED TO ONE,
 A TEST IS MADE TO SEE IF THE STEP CAN
 BE INCREASED AT ONE LOWER, THE A STEP
 CURRENT, IS ONLY MADE IF THE STEP CAN
 BE INCREASED BY AT LEAST 1.1*M. IF
 CHANGE IS POSSIBLE, IDOUB IS SET TO
 IO TO PREVENT FURTHER TESTING FOR THE
 NEXT TEN STEPS. POSSIBLE, IT IS MADE
 AND IDOUB IS SET TO IO + 1 TO PREVENT
 FURTHER TESTING FOR THAT NUMBER OF
 STEPS. IF THE ERROR WAS TOO LARGE,
 THE OPTIMUM STEP SIZE FOR THIS OR
 SOME LOWER ORDER IS COMPUTED, AND THE

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451 C
452 C
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467 C
468 C
469 C
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482 C
483 C
484 C
485 C
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494 C
495 C

STEP RETRIED. IF IT SHOULD FAIL TWICE
MORE IT IS AN INDICATION THAT THE
DERIVATIVES THAT HAVE ACCUMULATED IN
THE Y ARRAY HAVE ERRORS OF THE WRONG
ORDER, SO THE FIRST DERIVATIVES ARE
RECOMPUTED AND THE ORDER IS SET TO 1.
D = ZERO
DO 250 I = 1,N
  D = D + (ERROR(I)/YMAX(I))**2
CONTINUE
IWEVAL = 0
IF (D.GT. 3) GO TO 270
IF (K.LT. 3) GO TO 260
DO 255 J = 3,K
  I = 1,N
  Y(J,I) = Y(J,I) + C(J)*ERROR(I)
CONTINUE
KFLAG = +1
HNEA = H
IF (IDJUB.LE. 1) GO TO 275
IDJUB = IDJUB - 1
IF (IDJUB.GT. 1) GO TO 350
DO 265 I = 1,N
  WK(IND10,I) = ERROR(I)
CONTINUE
GO TO 350
KFLAG = KFLAG - 2 (DABS(HMIN)*DNEP) GO TO 370
I = TJLD
IF (KFLAG.LE. -5) GO TO 360
PR2 = (D/E)**ENQ2*1.2
PR3 = 1.E+20
IF ((I).GE. MXDER) .OR. (KFLAG .LE. -1) GO TO 285
D = ZERO
DO 280 I = 1,N
  D = D + ((ERROR(I) - WK(IND10,I))/YMAX(I))**2
CONTINUE
PR3 = (D/EUP)**ENQ3*1.4
PR1 = 1.E+20
IF (I).LE. 1) GO TO 295
D = ZERO
DO 290 I = 1,N
  D = D + (Y(K,I)/YMAX(I))**2
CONTINUE
PR1 = (D/EDWN)**ENQ1*1.3

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451 C
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295 CONTINUE
   IF (PR2 .LE. PR3) GO TO 325
   IF (PR1 .LT. PR1) GO TO 330
   R = 1.0/AMAX1(PRI,1.E-4)
300 NEWI = IO
305 IDOUB = IO
   IF ((KFLAG.EQ.1) .AND. (R.LT. (1.1))) GO TO 350
   IF (NEWI .LE. IO) GO TO 315
   XK = JNE / K
   DO 310 I = 1,N
     Y(NEWI+1,I) = ERROR(I)*C(K)*XK
310 CONTINUE
315 K = NEWI + 1
   IF (KFLAG.EQ.1) GO TO 335
   RACUM = RACUM*R
   IRET = 3
   GO TO 375
320 IF (NEWI.EQ. IO) GO TO 135
325 IO = NEWI
   GO TO 30
   IF (PR2 .GT. PR1) GO TO 300
   NEWI = IO
   K = 1.0/AMAX1(PR2,1.E-4)
   GO TO 305
330 NEWI = IO + 1
   GO TO 305
335 IRET = 2
   R = DMIN1(R,DABS(HMAX/H))
   H = HAR
   HNEW = H
   IF (IJEVNI) GO TO 340
   IO = VEVI
340 KI = JNE
   DO RI = 345 J = 2,K
     RI = R1*R
     DO 345 I = 1,N
       Y(J,I) = Y(J,1)*RI
345 CONTINUE
   IDOUB = K
350 DO 355 I = 1,N
     YMAX(I) = DMAX1(YMAX(1),DABS(Y(1,I)))
355 CONTINUE
   JSTART = IO
  
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 DVUG6070
 DVUG6080
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 DVUG6100
 DVUG6110
 DVUG6120
 DVUG6130
 DVUG6140
 DVUG6170
 DVUG6180
 DVUG6190
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 DVUG6240
 DVUG6250
 DVUG6260
 DVUG6270
 DVUG6280
 DVUG6290
 DVUG6300
 DVUG6310
 DVUG6320
 DVUG6330
 DVUG6340
 DVUG6350
 DVUG6360
 DVUG6370
 DVUG6380

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360 GO TO 395
    IF (ID.EQ.1) GO TO 390
    CALL DFUN(Y,I,N,WK(N2,I),WK,0)
    R = H/HOLD
    DO 365 I = 1,N
      Y(I,I) = WK(IND1,I)
      NI1 = NI + I
      WK(IND2,I) = HOLD*WK(NI1,I)
      Y(2,I) = WK(IND2,I)*R
365 CONTINUE
    IO = I
    KFLAG = 1
    GO TO 50
370 KFLAG = -1
    HNEW = H
    JSTART = IO
    GO TO 400

375 RACUM = DMAXI(DABS(HMIN/HOLD),RACUM)
    RACUM = DMINI(RACUM,DABS(HMAX/HOLD))
    RI = ONE
    DO 380 J = 2,KUM
      RI = RI*RACUM
      DO 380 I = 1,N
        Y(J,I) = WK(N4+J,I)*RI
380 CONTINUE
    H = HJLD*RACUM
    DO 385 I = 1,N
      Y(I,I) = WK(IND1,I)
385 CONTINUE
    IDUUB = K
    GO TO (30,135,320),IRET1
390 KFLAG = -4
    GO TO 235
395 IF(KFLAG.EQ.1) GO TO 9000
400 IER = 32-KFLAG
9000 CONTINUE
    IF(JER.NE.0) CALL UERTST(JER,6HDVDGER)
    IF(IER.GT.33) IER = IER - 1
    IF(IER.LE.0) CALL UERTST(IER,6HDVDGER)
9005 RETURN
    END
  
```

SCALE ALL VARIABLES CONNECTED WITH
 H AND RETURN TO THE CALLING SECTION

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1  SUBROUTINE LUDATF (A,LU,N,IA,IDGT,D1,D2,IPVT,EQUIL,WA,IER)
2  C-----LIBRARY 1-----
3  C
4  C
5  C
6  C
7  C
8  C
9  C
10 C
11 C
12 C
13 C
14 C
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45 C

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FUNCTION
 USAGE
 PARAMETERS

A
 LU
 N
 IA
 IDGT

D1
 D2
 IPVT
 EQUIL
 WA

L-U DECOMPOSITION BY THE CROUT ALGORITHM WITH OPTIONAL ACCURACY TEST.
 CALL LUDATF(A,LU,N,IA,IOGT,D1,D2,IPVT,EQUIL,WA,IER)
 INPUT MATRIX OF DIMENSION N BY N CONTAINING THE MATRIX TO BE DECOMPOSED
 REAL OUTPUT MATRIX OF DIMENSION N BY N CONTAINING THE L-U DECOMPOSITION OF A
 ROWWISE PERMUTATION OF THE INPUT MATRIX FOR A DESCRIPTION OF THE FORMAT OF LU, SEE EXAMPLE.
 INPUT SCALAR CONTAINING THE ORDER OF THE MATRIX A.
 INPUT SCALAR CONTAINING THE ROW DIMENSION OF MATRICES A AND LU IN THE CALLING PROGRAM.
 INPUT OPTION.
 IF IOGT IS GREATER THAN ZERO, THE NON-ZERO ELEMENTS OF A ARE ASSUMED TO BE CORRECT TO IOGT DECIMAL PLACES. LUDATF PERFORMS AN ACCURACY TEST TO DETERMINE IF THE COMPUTED DECOMPOSITION IS THE EXACT DECOMPOSITION OF A MATRIX WHICH DIFFERS FROM THE GIVEN ONE BY LESS THAN ITS UNCERTAINTY.
 IF IOGT IS EQUAL TO ZERO, THE ACCURACY TEST IS BYPASSED.
 OUTPUT SCALAR CONTAINING ONE OF THE IWD COMPONENTS OF THE DETERMINANT. SEE DESCRIPTION OF PARAMETER D2, BELOW.
 OUTPUT SCALAR CONTAINING ONE OF THE IWD COMPONENTS OF THE DETERMINANT. THE DETERMINANT MAY BE EVALUATED AS (01)(2*N D2) PERMUTATION INDICES. SEE DOCUMENT (ALGORTIHM).
 OUTPUT VECTOR OF LENGTH N CONTAINING THE RECIPROCALS OF THE ABSOLUTE VALUES OF THE LARGEST (IN ABSOLUTE VALUE) ELEMENT IN EACH ROW.
 ACCURACY TEST PARAMETER, OUTPUT ONLY IF IOGT IS GREATER THAN ZERO.
 SEE ELEMENT DOCUMENTATION FOR DETAILS.

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LUDA0930

IER - ERROR PARAMETER = 128 + N
TERMINAL ERROR INDICATES THAT MATRIX A IS
N = 1 ALGORITHMICALLY SINGULAR. (SEE THE
CHAPTER L PRELUDE).
WARNING ERROR = 32 + N
N = 2 INDICATES THAT THE ACCURACY TEST
FAILED.
THE COMPUTED SOLUTION MAY BE IN ERROR
BY MORE THAN CAN BE ACCOUNTED FOR BY
THE UNCERTAINTY OF THE DATA.
THIS WARNING CAN BE PRODUCED ONLY IF
IDGT IS GREATER THAN U ON INPUT.
SEE CHAPTER L PRELUDE FOR FURTHER
DISCUSSION.

PRECISION - SINGLE/DOUBLE
REQD. IMSL ROUTINES - UERTST
LANGUAGE - FORTRAN
LATEST REVISION - AUGUST 15, 1973

DIMENSION A(IA,N), LU(IA,N), IPVT(N), EQUIL(N)
DOUBLE PRECISION A, LU, DL, D2, EQUIL, WA, ZERU, ONE, FOUR, SIXTN, SIXTH,
RN, WRRL, BIGA, BIG, P, SUV, AI, WI, T, TEST, Q
, DABS
, ZERU, ONE, FOUR, SIXTN, SIXTH/0.00, 1.00, 4.00,
16.00, .062500/
INITIALIZATION

* 2 DATA
*
IER = 0
RN = V ZERO
WRRL = ONE
DL = ZERO
D2 = ZERO
BIGA = ONE
DO 10 I = 1, N
BIG = I
DO 5 J = 1, N
P = A(I, J)
LJ(I, J) = P
P = DABS(P)
IF (P .GT. BIG) BIG = P
CONTINUE
IF (BIG .GT. BIGA) BIGA = BIG
IF (BIG .EQ. ZERU) GO TO 110

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91 EQUJL(I) = ONE/BIG
92 CONTINUE
93 DO 105 J=1,N
94 JMI = J-1
95 IF (JMI .LT. 1) GO TO 40
96 DO 35 I=1,JMI
97 SUM = LU(I,J)
98 IMI = I-1
99 IF (IDGT .EQ. 0) GO TO 25
100 C
101 COMPUTE U(I,J), I=1,.....,J-1
102 WITH ACCURACY TEST
103 AI = DABS(SUM)
104 NI = ZERO
105 IF (IMI .LT. 1) GO TO 20
106 DO 15 K=1,IMI
107 T = LU(I,K)*LU(K,J)
108 SUM = SUM-T
109 NI = NI+DABS(T)
110 CONTINUE
111 LU(I,J) = SUM
112 IF (AI .EQ. ZERO) AI = BIGA
113 TEST = NI/AI
114 IF (TEST .GT. WREL) WREL = TEST
115 GO TO 35
116 C
117 WITHOUT ACCURACY
118 IF (IMI .LT. 1) GO TO 35
119 DO 30 K=1,IMI
120 SUM = SUM-LU(I,K)*LU(K,J)
121 CONTINUE
122 LU(I,J) = SUM
123 P = ZERO
124 C
125 DO 70 I=J,N
126 SUM = LU(I,J)
127 IF (IDGT .EQ. 0) GO TO 55
128 C
129 WITH ACCURACY TEST
130 AI = DABS(SUM)
131 NI = ZERO
132 IF (JMI .LT. 1) GO TO 50
133 DO 45 K=1,JMI
134 T = LU(I,K)*LU(K,J)
135 SUM = SUM-T
136 NI = NI+DABS(T)

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```

136 CONTINUE
137 LU(I,J) = SUM
138 MI = MI + DABS(SUM)
139 IF (AI .EQ. ZERO) AI = BIGA
140 IF EST = MI/AI
141 IF (TEST .GT. WREL) WREL = TEST
142 GO TO 65
143 C
144 IF (JMI .LI. 1) GO TO 65
145 DJ 60 K=1,JMI
146 SUM = SUM - LU(I,K)*LU(K,J)
147 CONTINUE
148 LU(I,J) = SUM
149 Q = EQUIL(I)*DABS(SUM)
150 IF (P .GE. Q) GO TO 70
151 P = Q
152 IMAX = I
153 CONTINUE
154 C
155 IF (RN+P .EQ. RN) GO TO 110
156 IF (J .EQ. IMAX) GO TO 80
157 C
158 D1 = -D1
159 DO 75 K=1,N
160 P = LU(IMAX,K)
161 LU(IMAX,K) = LU(J,K)
162 LU(J,K) = P
163 CONTINUE
164 EQUIL(IMAX) = EQUIL(J)
165 IPVT(J) = IMAX
166 D1 = D1*LU(J,J)
167 IF (DABS(D1) .LE. ONE) GO TO 90
168 D2 = D2*FOUR
169 GO TO 85
170 IF (DABS(D1) .GE. SIXTH) GO TO 95
171 D1 = D1*SIXTN
172 D2 = D2-FOUR
173 GO TO 90
174 CONTINUE
175 JPI = J+1
176 IF (JPI .GT. N) GO TO 105
177 C
178 P = LU(J,J)
179 DO 100 I=JPI,N
180

```

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LUDA1440
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TEST FOR ALGRITHMIC SINGULARITY
INTERCHANGE ROWS J AND I MAX

```

```

DIVIDE BY PIVOT ELEMENT U(J,J)

```

AD-A064 545

CINCINNATI UNIV OH DEPT OF ENGINEERING SCIENCE
A CRITICAL EVALUATION OF COMPUTER SUBROUTINES FOR SOLVING STIFF--ETC(U)
OCT 78 D C KRINKE, R L HUSTON
UC-ES-101578-8-0NR

F/6 12/1

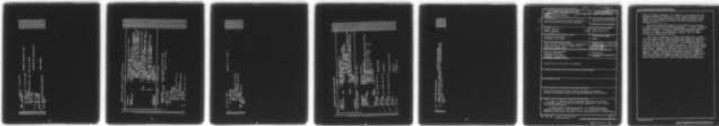
N00014-76-C-0139

NL

UNCLASSIFIED

2 of 2

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A064545



END

DATE
FILMED

4-79

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 LUDA1960
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 LUDA1980
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 LUDA2050
 LUDA2060
 LUDA2070
 LUDA2080
 LUDA2090
 LUDA2100
 LUDA2110
 LUDA2120

```

181 LU(I,J) = LU(I,J)/P
182 CONTINUE
183 CONTINUE
184 C
185 IF (IDGT .EQ. 0) GO TO 9005
186 P = 3**I+3
187 WA = SPANREL
188 IF (WA+10.D0**(-IDGT)) .NE. WA) GO TO 9005
189 IER = 34
190 GO TO 9000
191 C
192 IER = 129
193 D1 = ZERO
194 D2 = ZERO
195 C
196 CONTINUE
197 CALL JERTST(IER,6HLUDATF)
198 RETURN
199 END
  
```

PERFORM ACCURACY TEST

ALGORITHMIC SINGULARITY

PRINT ERROR

LUEF0280
 LUEF0020
 LUEF0030
 LUEF0040
 LUEF0050
 LUEF0060
 LUEF0070
 LUEF0080
 LUEF0090
 LUEF0100
 LUEF0110
 LUEF0120
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 LUEF0240
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 LUEF0270
 LUEF0290
 LUEF0300
 LUEF0310
 LUEF0320
 LUEF0330
 LUEF0340
 LUEF0350
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 LUEF0370
 LUEF0380
 LUEF0390
 LUEF0400
 LUEF0410
 LUEF0420
 LUEF0430
 LUEF0440
 LUEF0450
 LUEF0460

```

SUBROUTINE LUELMF (A,B,IPVT,N,IA,X)
C-----D-----LIBRARY I-----
FUNCTION
USAGE
PARAMETERS A
B
IPVT
N
IA
X
PRECISION
LANGUAGE
LATEST REVISION
DIMENSION
DOUBLE PRECISION
DO 5 I=1,N
X(I) = B(I)
IW = 0
DO 20 I=1,N
IP = IPVT(I)
SUM = X(IP)
IF (IW.EQ. 0) GO TO 15
IM1 = I-1
DO 10 J=IW,IM1
SUM = SUM-A(I,J)*X(J)
CONTINUE
GO TO 20
IF (SUM.NE. 0.) IW = I

```

C-----D-----LIBRARY I-----
 FUNCTION
 USAGE
 PARAMETERS A
 B
 IPVT
 N
 IA
 X
 PRECISION
 LANGUAGE
 LATEST REVISION
 DIMENSION
 DOUBLE PRECISION
 DO 5 I=1,N
 X(I) = B(I)
 IW = 0
 DO 20 I=1,N
 IP = IPVT(I)
 SUM = X(IP)
 IF (IW.EQ. 0) GO TO 15
 IM1 = I-1
 DO 10 J=IW,IM1
 SUM = SUM-A(I,J)*X(J)
 CONTINUE
 GO TO 20
 IF (SUM.NE. 0.) IW = I

LUEF0470
 LUEF0480
 LUEF0490
 LUEF0500
 LUEF0510
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 LUEF0540
 LUEF0550
 LUEF0560
 LUEF0570
 LUEF0580
 LUEF0590

SOLVE JX = Y FOR X

```

46 C
47 20 X(I) = SUM
48 DO 30 IB=1,N
49 IPI = N+1-IB
50 SUM = X(I)
51 IF (IPI > N) GO TO 30
52 DO 25 J=IPI,N
53 SUM = SUM-A(I,J)*X(J)
54 CONTINUE
55 25 X(I) = SUM/A(I,I)
56 RETURN
57 END
58

```

```

12 SUBROUTINE UERTST(IER,NAME)
13 -----LIBRARY 1-----
14 FUNCTION
15 USAGE
16 PARAMETERS IER
17
18 NAME
19
20 -----
21 LANGUAGE
22 -----
23 LATEST REVISION
24 -----
25
26 DIMENSION
27 ITP(5),IBIT(4)
28 NAME(3)
29 WARN(WARF,TERM,PRINTR
30 (IBIT(1),WARN),(IBIT(2),WARF),(IBIT(3),TERM)
31 /IBIT(1),IBIT(2),IBIT(3)
32 /IBIT(1),IBIT(2),IBIT(3)
33 /IBIT(1),IBIT(2),IBIT(3)
34 /IBIT(1),IBIT(2),IBIT(3)
35 /IBIT(1),IBIT(2),IBIT(3)
36 /IBIT(1),IBIT(2),IBIT(3)
37 /IBIT(1),IBIT(2),IBIT(3)
38 /IBIT(1),IBIT(2),IBIT(3)
39 /IBIT(1),IBIT(2),IBIT(3)
40 /IBIT(1),IBIT(2),IBIT(3)
41 /IBIT(1),IBIT(2),IBIT(3)
42 /IBIT(1),IBIT(2),IBIT(3)
43 /IBIT(1),IBIT(2),IBIT(3)
44 /IBIT(1),IBIT(2),IBIT(3)
45 /IBIT(1),IBIT(2),IBIT(3)

```

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UERT0190
UERT0200
UERT0210
UERT0220
UERT0230
UERT0240
UERT0250
UERT0260
UERT0270
UERT0280
UERT0290
UERT0300
UERT0310
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UERT0350
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UERT0400
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```

-----
-- UERTST
-----
FUNCTION
USAGE
PARAMETERS IER
NAME
LANGUAGE
LATEST REVISION
DIMENSION
INTEGER*2
EQUIVALENCE
DATA
* * *
DATA IER2=IER
IF (IER2 .GE. WARF) GO TO 5
IER1=4
GO TO 20
IF (IER2 .LT. TERM) GO TO 10
IER1=3
GO TO 20
IF (IER2 .LT. WARF) GO TO 15
IER1=2
GO TO 20
IER1=1

```

```

-----
-- ERROR MESSAGE GENERATION
-- CALL UERTST(IER,NAME)
-- ERROR PARAMETER TYPE + N WHERE
TYPE= 128 IMPLIES TERMINAL ERROR
64 IMPLIES WARNING WITH FIX
32 IMPLIES WARNING TO CALLING ROUTINE
N = INPUT VECTOR CONTAINING THE CHARACTER LITERAL
CALLING ROUTINE AS A SIX CHARACTER LITERAL
STRING.
FORTRAN
-- JANUARY 18, 1974

```

```

-----
-- ERROR MESSAGE GENERATION
-- CALL UERTST(IER,NAME)
-- ERROR PARAMETER TYPE + N WHERE
TYPE= 128 IMPLIES TERMINAL ERROR
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FORTRAN
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CALLING ROUTINE AS A SIX CHARACTER LITERAL
STRING.
FORTRAN
-- JANUARY 18, 1974

```

```

-----
-- ERROR MESSAGE GENERATION
-- CALL UERTST(IER,NAME)
-- ERROR PARAMETER TYPE + N WHERE
TYPE= 128 IMPLIES TERMINAL ERROR
64 IMPLIES WARNING WITH FIX
32 IMPLIES WARNING TO CALLING ROUTINE
N = INPUT VECTOR CONTAINING THE CHARACTER LITERAL
CALLING ROUTINE AS A SIX CHARACTER LITERAL
STRING.
FORTRAN
-- JANUARY 18, 1974

```

UERT0470
UERT0480
UERT0490
UERT0500
UERT0510
UERT0520
UERT0530

```
46 C  
47 IER2=IER2-IBIT(IER1)  
48 WRITE (PRINTR,25) (ITYP(I,IER1),I=1,5),NAME,IER2,IER  
49 FORMAT('*** I M $ L(UERTIST) ***',5A4,4X,3A2,4X,I2,  
50 * RETURN  
51 *  
52 END
```

PRINT ERROR MESSAGE

9 Technical rept. 2 Sep 77-
15 Oct 78

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER UC-ES-101578-8-ONR	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) A Critical Evaluation of Computer Subroutines for Solving Stiff Differential Equations.	5. TYPE OF REPORT & PERIOD COVERED Technical 9/1/77-10/15/78	
	6. PERFORMING ORG. REPORT NUMBER	
7. AUTHOR(s) Dennis C./Krinke Ronald L./Huston	8. CONTRACT OR GRANT NUMBER(s) N00014-76-C-0139	
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9. PERFORMING ORGANIZATION NAME AND ADDRESS University of Cincinnati Cincinnati, Ohio 45221	11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research Resident Representative Purdue University, Room 84 Graduate House Lafayette, Indiana 47907	
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16. DISTRIBUTION STATEMENT (of this Report) Distribution of this report is unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Differential Equation Solvers, Computer Integrator Subroutines, Systems of Differential Equations, Computer Modelling, Miff Systems		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A number of commonly available computer subroutines for solving differential equation systems are tested and compared for their ability to solve "stiff" systems. A "stiff" system is defined as either: 1) a system with widely separated eigenvalues or time constants or 2) a system with diverging exponential terms which have small or zero coefficients due to a particular		

410649 B

choice of initial conditions. For example, it is believed that the governing differential equations of large complex mechanical system models (such as, human-body/crash-victim simulation models, finite segment structural models, and large vibrating system models) are frequently stiff. ←

The solver subroutines tested on such systems are as follows: 1) DRKGS (a fourth-order Runge-Kutta routine); 2) DHPCG (a Hamming predictor-corrector routine); 3) DVOGER-ADAMS (an Adams predictor-corrector routine); 4) DVOGER-GEAR (a Gear predictor-corrector routine) 5) DREBS (a Bulirsch-Stoer routine); and 6) RK45 (a sixth-order Runge-Kutta routine).

These solver subroutines are tested and compared for a number of stiff systems of both types described above where the exact analytical solution is known. The subroutines are compared in terms of run time, accuracy, and function calls. It is found that the subroutines vary considerably in terms of accuracy. Also, their overall individual effectiveness is highly dependent upon the specific system being solved. However, for systems of the first type of stiffness, Gear's method (DVOGER-GEAR) and DRKGS appear to be the preferred routines. Finally, the automatic stepsize capability of DRKGS and DHPCG is a definite advantage over the other routines. However, the step oriented format of DVOGER and DREBS provides a potential for similar flexibility in error control through coding modifications.