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HIGHLY SURVIVABLE TRUSS TYPE TAIL BOOM.(U)

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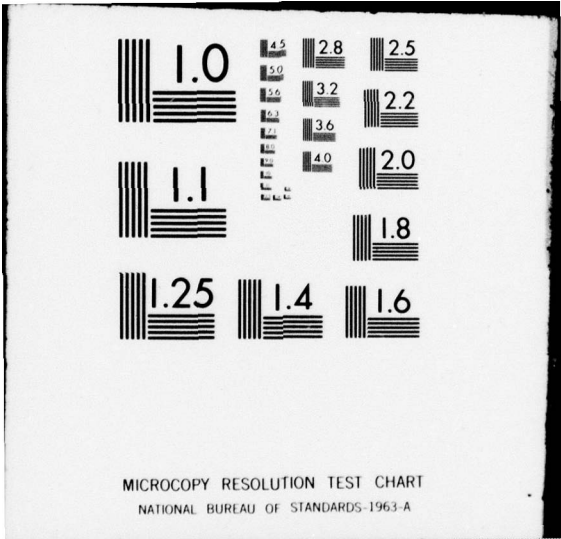
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TECHNICAL REPORT ARBRL-TR-02123

HIGHLY SURVIVABLE TRUSS TYPE
TAIL BOOM

Thomas F. Erline

November 1978

US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
BALLISTIC RESEARCH LABORATORY
ABERDEEN PROVING GROUND, MARYLAND

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Vulnerability Reduction	Semimonocoque	Anti-Aircraft
30mm HEI	23mm HEI	Threat
Structural Integrity	Highly Redundant	Substructured
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)		
<p>Highly redundant truss type structures, which are lightweight, have been analyzed by NASTRAN for replacement of the semimonocoque type tail boom. Analyses show that even with massive damage criterion imposed the structure retains its integrity with level flight loads up to 130 knots. The truss presents itself as a structural challenge to Soviet AA threat of the 23mm and 30mm HEI rounds.</p> <p>Comparing the vulnerable semimonocoque configuration with the truss structure: semimonocoque's vulnerable area is nearly 100% of the present area; the</p>		

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A truss has a greatly reduced vulnerable area (the joints are most vulnerable and their areas are small). The semimonocoque is blast sensitive to the AA threats mentioned because the detonation is confined and a large surface area is blown away; the truss does not confine the blast, thus is less sensitive. Since the thin skin structure of the semimonocoque carries a great deal of load it is sensitive to crack propagation; the truss is insensitive to crack propagation. Since the truss can be easily designed lightweight, the truss presents itself as a highly survivable competitive alternate for future Army helicopters.

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I. INTRODUCTION

Successful completion of Army helicopter missions in future battle scenarios may well depend upon survival of the structure after battle damage. Survivability of a helicopter will depend significantly upon the structure's ability to retain structural integrity. The principal purpose of this study is to develop a structural concept which assures a high degree of confidence in the integrity of a structure that has received combat damage. This study has been pursued because the Army needs to meet and provide a solution to the ever escalating high explosive anti-aircraft threat to the helicopter tail boom.

The highly lethal 23mm high explosive projectile represents an existing widely deployed threat to Army helicopters. The more lethal 30mm high explosive projectile appears on the horizon as the potential future threat. Because of this potentially severe 30mm threat and the possible inadequacy of present semimonocoque designs to survive hits by the 30mm, the present study was initiated to develop a structural challenge to the 30mm and to improve upon the present designs.

The tail boom of a helicopter (for example, the present AH-1 and UH-1 models) presents a significant amount of vulnerable area, and due to the flight loads of the tail rotor and elevators, the tail boom is constantly in some stressed condition. The semimonocoque tail boom construction configuration consists of skins, longerons, stringers, and bulkheads. Four longerons provide the main bending support for the tail boom. Shear loads are carried by the skin structure which is locally supported against buckling by the stringers. Presently the semimonocoque structure is configured to a minimum weight design. Ballistics tests using the 23mm high explosive against the minimum weight semimonocoque tail boom design have demonstrated its lack of damage tolerance¹. Structural modifications have been shown to increase the damage tolerance of the structure but the amount of damage is predictably a function of confined volume and detonation distance to the surface¹. Clearly the larger 30mm projectile reduces the survivability of the entire semimonocoque tail boom structure.

The solution for a structural challenge in this study took the form of a search for a highly redundant tail boom structure. A highly redundant structure is a structure that starts with a compact unit structure. The compact unit structure is interconnected within itself by comparatively small, relative to the entire structure, but stiff structural elements. The entire structure is then built up by a replication of the unit structure, scaling as desired or necessitated. The main reason for a high degree of redundancy is to build up damage tolerance by attempting to keep damage strictly localized.

¹D.F. Haskell, Damage Tolerance of Semimonocoque Aircraft, Paper at 41st Meeting of NATO-AGARD Impact Damage Tolerance of Structures Conference, Ankara, Turkey, October 1975.

A possible engineering solution that can easily be made highly redundant is the truss type structure. Use of modern technology and standard elements can make a truss both practical and economical. Because of its potential to fulfill such characteristics, the truss type structure was selected for this study in place of the semimonocoque structure. This study not only utilizes the truss concept but also introduces the concept of complete imbedded substructures. Complete imbedded substructures are easily generated within a truss structure that has a base figure equivalent to a quadrilateral by including the interior diagonals in a simple open truss structure. The intent is to develop a truss type tail boom with complete substructures that is highly redundant so that it can absorb massive damage and yet still hold the aerodynamic loads of flight. The truss tail boom can reduce vulnerability while lowering the weight of the tail boom. The observable surface area drops significantly reducing visibility and radar echo. A bonus would be the possibility of mounting a recoilless rifle on the helicopter because the openness of the truss allows the passage of back blast.

The development was performed throughout by computer modeling. The aerodynamic loads can be simulated and a damage criterion established very easily by this technique. A damage criterion should reflect a maximum amount of damage that can be sustained by the structure. The design objective is to retain structural integrity after imposition of the damage criterion.

Damage to a truss structure would not be in terms of confined volume or surface distance as it is in the semimonocoque structure, but damage would be in terms of loss of a member(s) or a loss of a joint. Not counting a completely destructive blast, the most catastrophic single event that could occur to a truss structure would be the destruction of a joint. The loss of a joint in a truss structure can be considered as massive damage because the loss of many members assembled at the joint is associated with loss of the joint. The demand that the truss sustain loss of a single joint and still retain structural integrity (not have other members buckle or fail) under flight loads is considered maximum survivability for the purpose of this study. Thus, loss of a joint is the damage criterion employed in this study.

Static and dynamic analyses of three truss design concepts were performed by the NASTRAN (NASA STRuctural ANalysis)² program. One of these truss concepts is a simple open truss design. The other two models incorporate the concept of complete substructures. The semimonocoque tail boom of AH-1 helicopter series is used as the basis for a replacement truss tail boom model. The AH-1 series helicopter presents a logical choice to develop a truss structure tail boom to

²Caleb, W. McCormick, Editor, The NASTRAN User's Manual, NASA SP 222(03), March 1976, Washington, D.C.

replace a semimonocoque structure. This helicopter has been in the Army's arsenal for a while and will continue in service for a number of years.

Selection of the design concept that is most likely to defeat the AA threat mentioned previously is dependent upon highest survivability and lowest weight. A selected design will be built, tested experimentally and reported on separately.

II. PROCEDURES

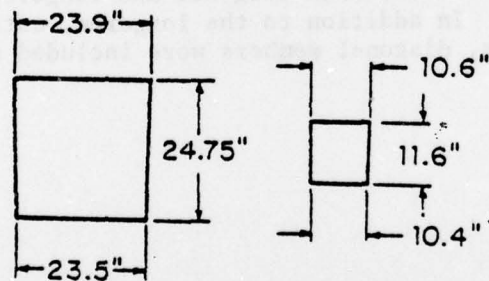
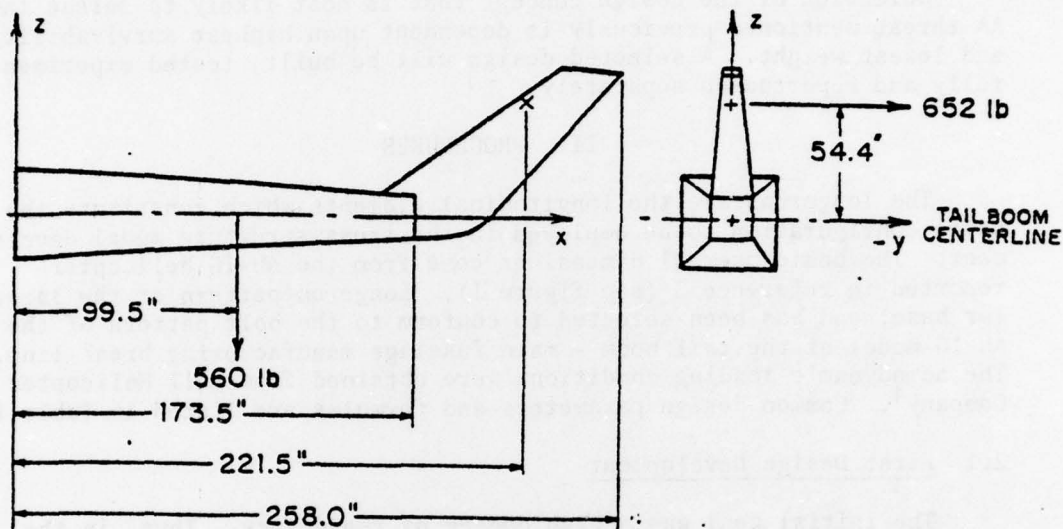
The longerons are the longitudinal elements which constitute the basic configuration to be employed in the truss structure model development. The basic overall dimensions come from the AH-1G helicopter reported in reference 3 (see figure 1). Longerons pattern at the larger (or base) end has been selected to conform to the bolt pattern of the AH-1G model at the tail boom - main fuselage manufacturing break line. The aerodynamic loading conditions were obtained from Bell Helicopter Company⁴. Common design parameters and formulas are listed in Table 1.

2.1 First Design Development

The initial goal was a high degree of redundancy. Thus, in the first iteration the structural member layout was generated by orienting the outside diagonals at 45° angles from the base. The vertical and transverse members were located at diagonal and longeron intersection points, see figure 2. In addition to the longeron, outside diagonal, and transverse members, diagonal members were included within the

³J.D. Cronkite, V.L. Berry, J.E. Brunlsen, A. NASTRAN Vibration Model of AH-1G Helicopter Airframe, June 1974, AD A009482.

⁴Private communication between D.F. Haskell of BRL and D. Reisdorfer, Bell Helicopter Company.



BASE OF TAILBOOM

END OF TAILBOOM

Figure 1. Geometry of Helicopter Tail Boom.

TABLE 1.

Common Design Parameters and Formulas

Material:	Aluminum Alloy	
Modulus of Elasticity:	$E = 7. \times 10^{10} \text{ n/m}^2 (10.5 \times 10^6 \text{ psi})$	(5)
Density ρ :	$\rho = 2.7 \times 10^3 \text{ kg/m}^3 (0.1 \text{ lbs/in}^3)$	(5)
Margin of Safety: of Individual Member	$M.S. = \frac{\text{stress limit}}{\text{applied stress}} - 1.$	(6)

Stress Limits per member

Compressive $CSL = .8 * \delta_{cr}$

Tensile $TSL = \delta_{cr}$

Euler Column Buckling (7)

$$\delta_{cr} = \frac{P_{cr}}{CSA}$$

Cross Sectional Area of Tube: $CSA = \pi(r_o^2 - r_i^2)$

Compressive Critical Load with Hinged Ends (7)

$$P_{cr} = \frac{\pi^2 EI}{l^2} \text{ where } l = \text{length of member}$$

⁵ALCOA STRUCTURAL HANDBOOK. A Design Manual for Aluminum Company of America, Pittsburg, PA, 1958.

⁶NASTRAN Programmer's Manual, NASA SP-221(03), July, 1976, Washington, D.C.

⁷S. Timoshenko, Strength of Materials, Part I. D. VanNostrand Company, Inc., New York, N.Y., 1940, pp 244-254.

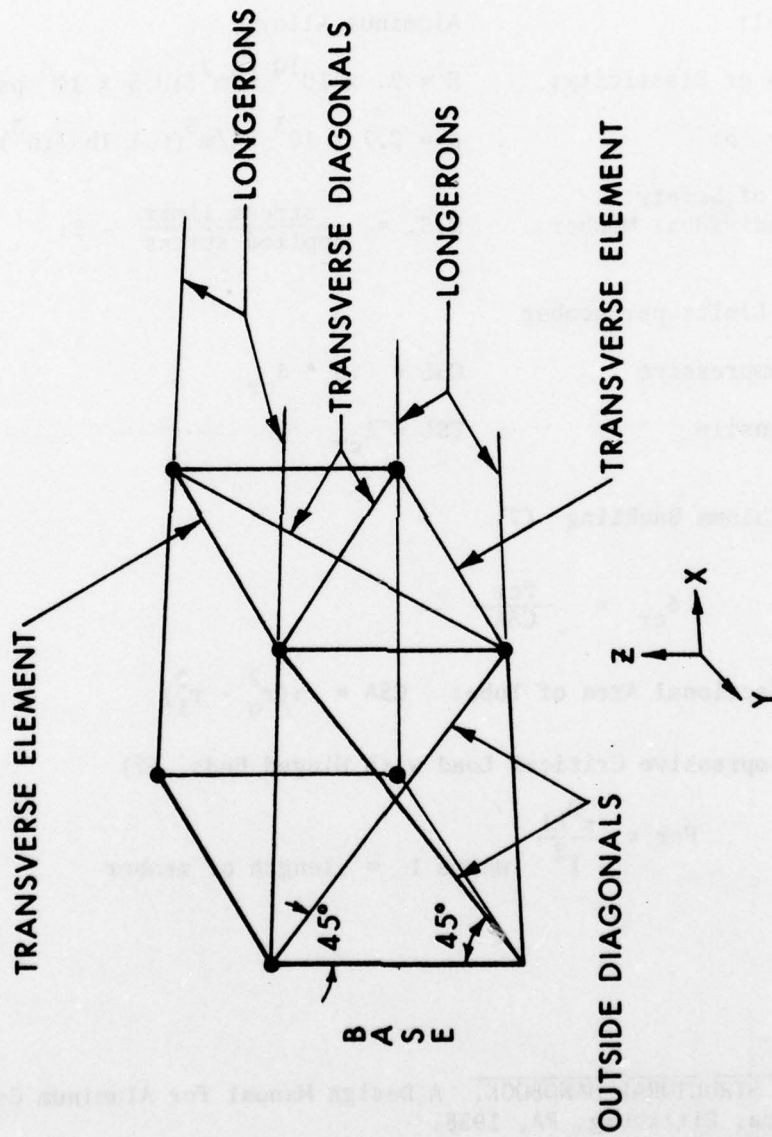


Figure 2. First Iteration Member Layout.

transverse sections defined by the transverse members, see figure 2. This layout was aided by geometry programs developed in-house⁸. The overall configuration consists of 44 joints, 120 degrees of freedom, with 186 members.

Analyses of this first design concept were started with the structural optimization program OPTBAR⁹. The OPTBAR program is an optimization procedure based on an energy criterion and a search procedure based on constraint gradient values. Constraint values of the geometric configuration, same material throughout, minimum element sizes and stress limit are input to OPTBAR and the indeterminate structure is optimized to lowest weight design. For this first simple open truss model the lowest weight was 44.45 kg (98 lbs). Initial damage criteria was loss of a member or members, and analyses of these cases produced higher weights. This was predictable because as the load path changes OPTBAR must strengthen the remaining members to take up the load. Of course, a critical event would be the loss of a joint and analyses simulating the loss of a joint using OPTBAR on the first iteration model indicated a geometrical instability.

Intuitively, one can observe the geometrical instability in a triangular cross section based truss (figure 3) if it would lose a joint. The structural integrity of a quadrilateral cross section based simple open truss that absorbed a loss of a joint has an uncertainty factor. This uncertainty in the simple open quad based truss led to the belief that it may be dependent on each and every joint. Dependence on a joint and the uncertainty of structural stability due to a geometric instability when a joint is lost reduces confidence in structural integrity.

This "simple" open truss structure was deemed unacceptable (simple is defined here as joint dependent). At this time the damage criterion was firmly established to be the loss of a single joint. A concept for independence of a joint was needed to reduce uncertainty of stability and increase confidence of structural integrity after damage. A number of ideas were passed over until the idea of complete substructures was conceived.

The concept that was used to generate complete substructures so as to obtain joint independence introduced the interior diagonals. The connection of all the interior diagonals from vertical station to vertical station generates forty additional elements in this first design. Because of the inclusion of these interior diagonals an increase in weight occurs, however, an increase in survivability is conceptually

⁸Keith Applin, Gary Kuehl; "Geometry Programs to Aid in Producing COM-GEOM Target Descriptions," BRL Memorandum Report No. 2712 Dec 1976.

⁹V.B. Venkayya, Design of Optimum Structures-Computers and Structures, Vol. 1, pp 285-309, Pergamon Press 1971.

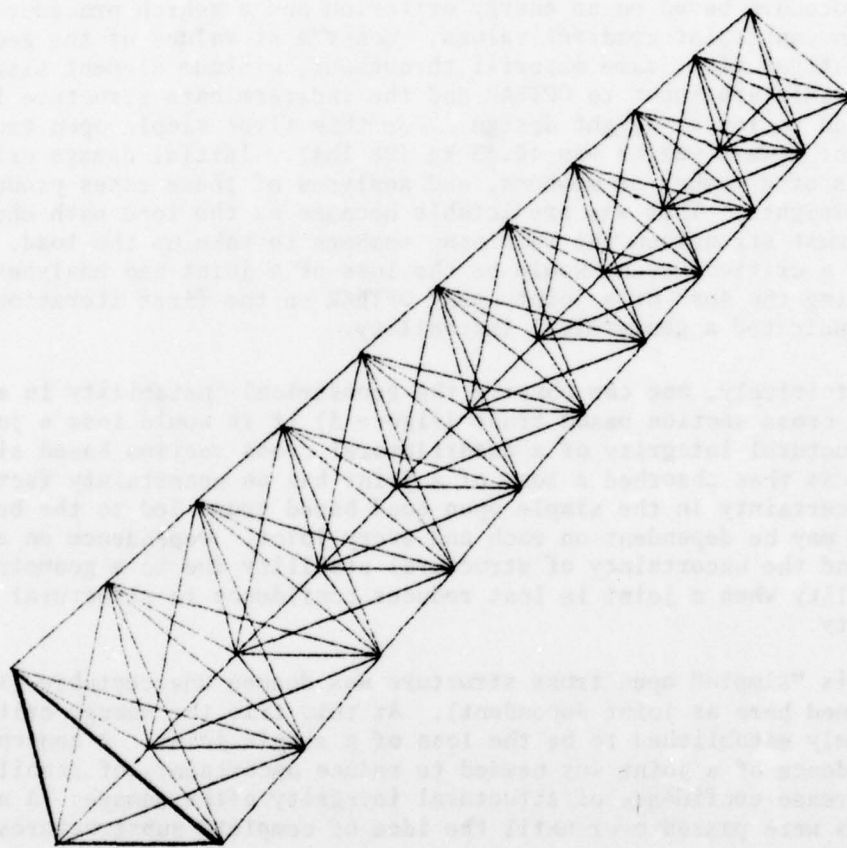


Figure 3. Computer Drawing of a Complete Triangular Substructure of Model 1.

assured because the structure's configuration has increased the ability to retain structural integrity after imposition of the loss of a joint. This method populates a joint with eleven members to be connected and generates a structure that has four complete triangular-based substructures (figure 3) within the entire quadrilateral cross section based structure (figure 4). This structure is highly redundant. The structure of figure 3 is a subset of that shown in figure 4. Figure 5 shows the fully connected composition of the addition of interior diagonals to the structure between the base and vertical station 1. The composition of this structure is truly shown in figure 6 which presents the base, vertical station 1 and vertical station 2. Note that the joints within the extremities are highly populated with eleven members per joint.

This new configuration has 226 members with 44 joints and 120 degrees of freedom. This complete, highly redundant truss when operated on by OPTBAR optimization analysis came to a weight of approximately 52.16 kg (115 lbs). The problem with the structural optimization scheme is that the optimization is for one and only one particular solution (weight optimization). The program results in a wide variety of cross sectional areas to the members so as to optimize the load path. Realistically there cannot be a universe of different size members; however, the weight output can be thought of as representative of an ideal lower bound. Being limited to this one area obviously does not account for a design-to-cost or a design-to-logistics solution.

A full accounting optimization could be defined as: design-to-cost, design-to-weight, design-to-logistics, and many other design-to-areas. For our purposes this study attempts to account for the three areas specifically mentioned. Considering cost and logistics, the ideal design would be to have all the truss members with the same cross sectional end dimensions. It costs less to buy a large quantity of structural elements all the same size than to buy small quantities of various sizes.

The standard tube structural element was chosen for this conceptual design study because of the tube's high inertia over rods of the same cross sectional area. Standard structural tube dimensions⁵ provide a wide range of possible designs (see Table 2). Analyses of the first design by changing standard dimensions allow a number of possible choices. Cases increment upward in weight by the different standard structural member dimensions. The structural element choice is 3.81 cm (1 1/2") outside diameter tubes with .159 cm (1/16") thickness. Using these element dimensions the first design weighs 63.73 kg (140.5 lbs) and meets our definition of full accounting.

Since these parameters are now set, the weight optimization program cannot be used for our analysis. Structural analyses from here on are performed by NASTRAN (NASA STRuctural ANalysis)². NASTRAN is a large, comprehensive, general purpose, finite element, displacement method,

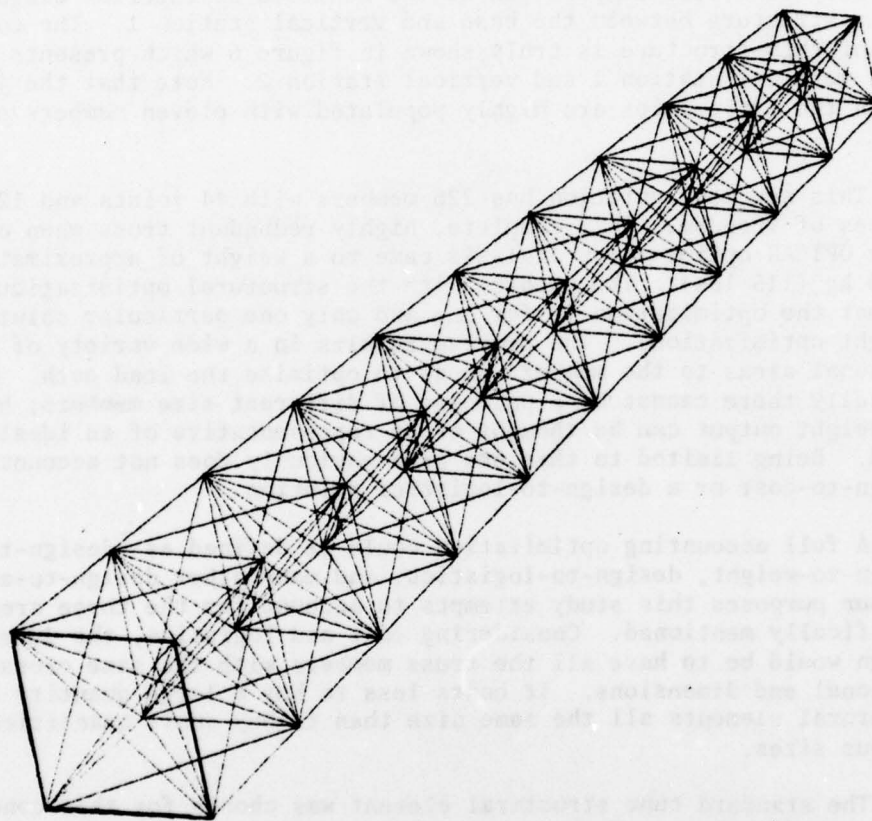


Figure 4. Computer Drawing of the Complete Quad Based Structure Model 1.

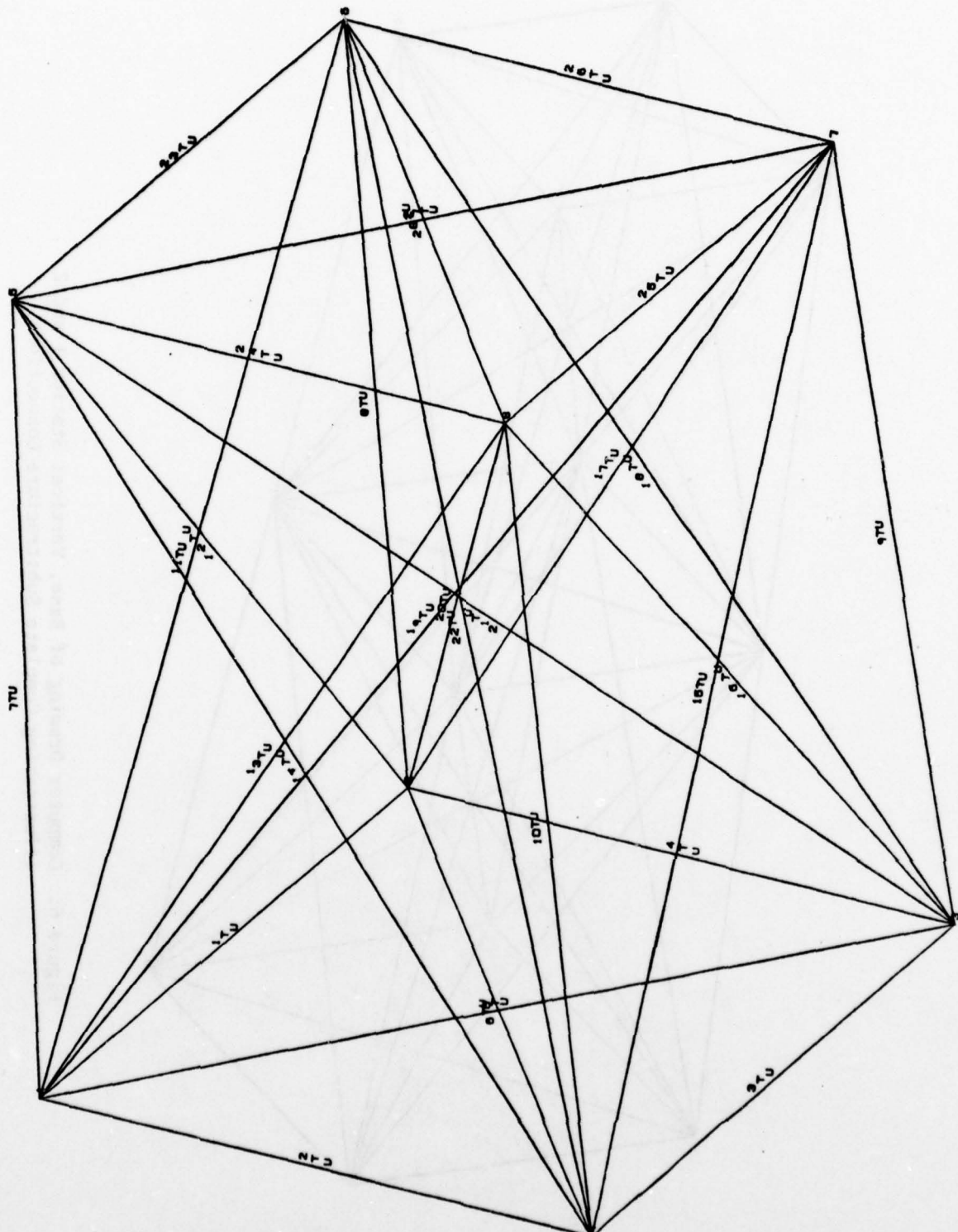


Figure 5. Computer Drawing of the Base and Vertical Station 1 Illustrating the Fully Connected Composition of the Structure.

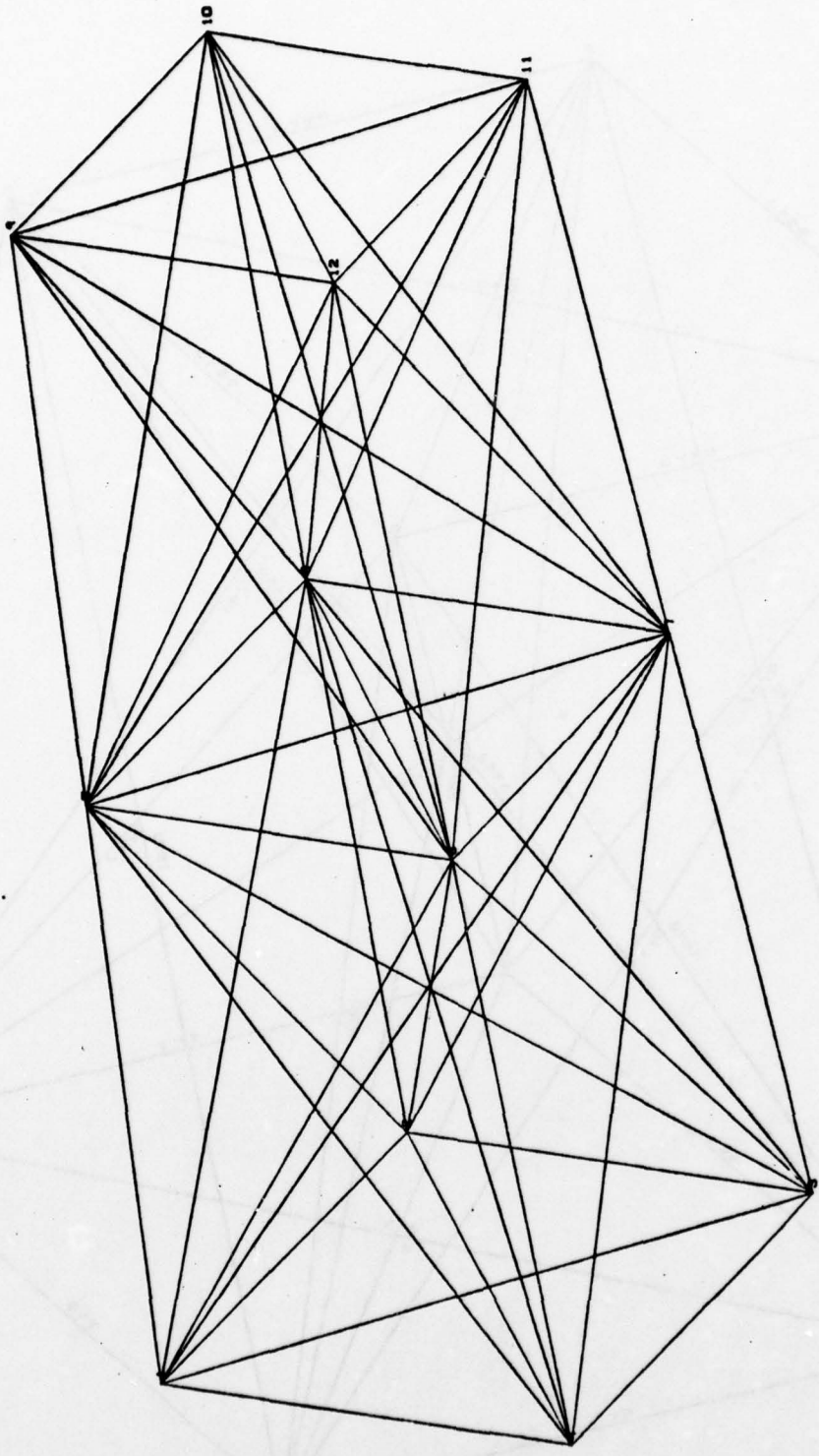


Figure 6. Computer Drawing of Base, Vertical Station 1 and 2
Illustrating Complete Substructure Connections.

TABLE 2

Different Weight Cases of First Design

<u>Design</u>	<u>O.D.</u>	<u>Thickness</u>	<u>Weight</u>
Interior Diagonals	3.81 cm (1 1/2")	.159 cm (1/16")	46.27 kg
Outer Members	3.81 cm (1 1/2")	.0795 cm (1/32")	(102 lbs)
All Members	3.81 cm (1 1/2")	.159 cm (1/16")	63.73 kg (140.5 lbs)
Interior Diagonals	4.45 cm (1 3/4")	.159 cm (1/16")	66.22 kg
Outer Members	3.81 cm (1 1/2")	.159 cm (1/16")	(146 lbs)
Interior Diagonals	4.45 cm (1 3/4")	.159 cm (1/16")	66.68 kg
Outer Members	4.45 cm (1 3/4")	.079 cm (1/32")	(147 lbs)
All Members	4.45 cm (1 3/4")	.159 cm (1/16")	74.66 kg (164.6 lbs)
All Members	5.04 (2")	.159 cm (1/16")	85.73 kg (189 lbs)

computer program. NASA, other government agencies, and aerospace industries have been using it for a number of years now for design and analysis of all forms of airframes.

The NASTRAN rigid format 3, Normal Modes and Frequencies, is a dynamic analysis providing the mode shapes and resonant frequencies of complete models. Analysis of flight loads on the models is performed by NASTRAN rigid format 4, Static Analysis with Differential Stiffness. This method was chosen over rigid format 1, Static Analysis, because design operating stresses are more accurately calculated for analysis of buckling failure of individual members¹⁰. The NASTRAN mathematical model in the design of the truss structure is straight forward. The joints are grid points and the connections made are with the standard line element CTUBE².

2.2 Weight Reduction by Changing Geometry Layout

The initial model truly achieves a high degree of redundancy and populates the structure with many members. This configuration, however, is not a low weight design. To obtain a geometric configuration conducive to a low weight design without doing a geometry optimization analysis, this study utilizes only the joint locations described in reference 11 for the second and third design cases.

2.3 Second Design Case

The second design is a "simple" open truss. The longeron elements are again following the longeron locations of the AH-1 series type helicopter. The configuration consists of 28 joints, 114 members, and 72 degrees of freedom. The same tube dimensions that are in the first design are used here. This configuration (see figure 7) weighs approximately 40.82 kg (90 lbs). This design case is included as a comparison to the third design case.

2.4 The Third Design Case

The third design has the same geometry as the second design except that the interior diagonals are introduced to generate complete sub-structures. This design has 138 members with 28 joints and 72 degrees of freedom. This highly redundant truss design weighs approximately 52.16 kg (115 lbs) (see figure 8), using the same 3.81 cm (1 1/2") outside diameter tubes with .159 cm (1/16") thickness.

¹⁰Robert B. Bennett, NASTRAN Differential Stiffness, Analysis of an Aircraft Canopy, NASA TMX 2378 p 85-105, September 1971.

¹¹J. S. Arora, E. J. Haug, A. K. Govil, Fail-Safe Design of an Open Truss Helicopter Tail Boom, Technical Report #32, April 1977, College of Engineering, University of Iowa.

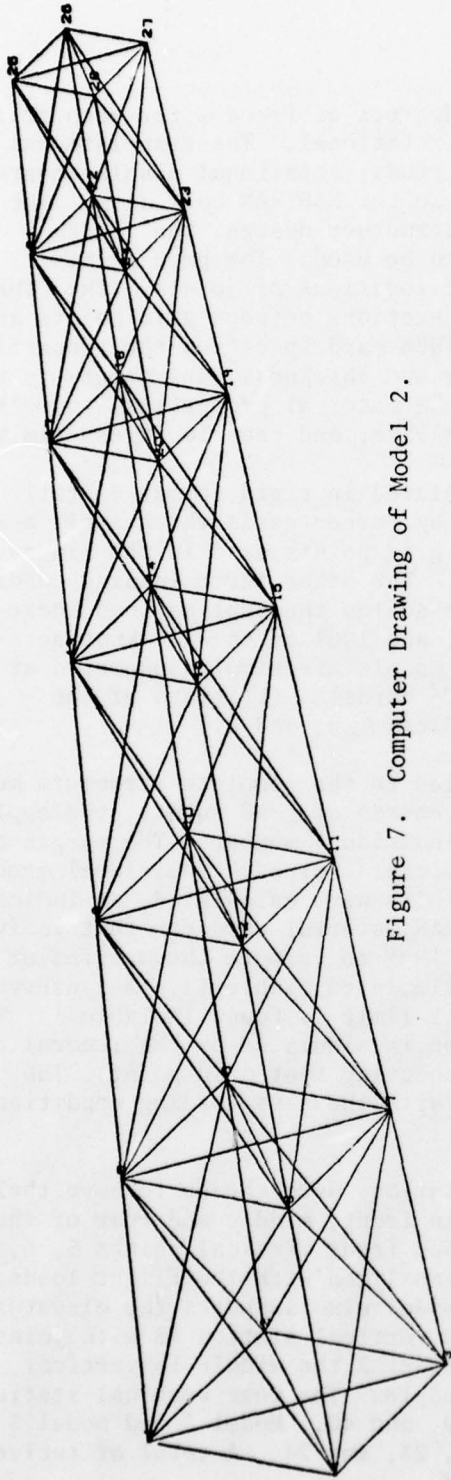


Figure 7. Computer Drawing of Model 2.

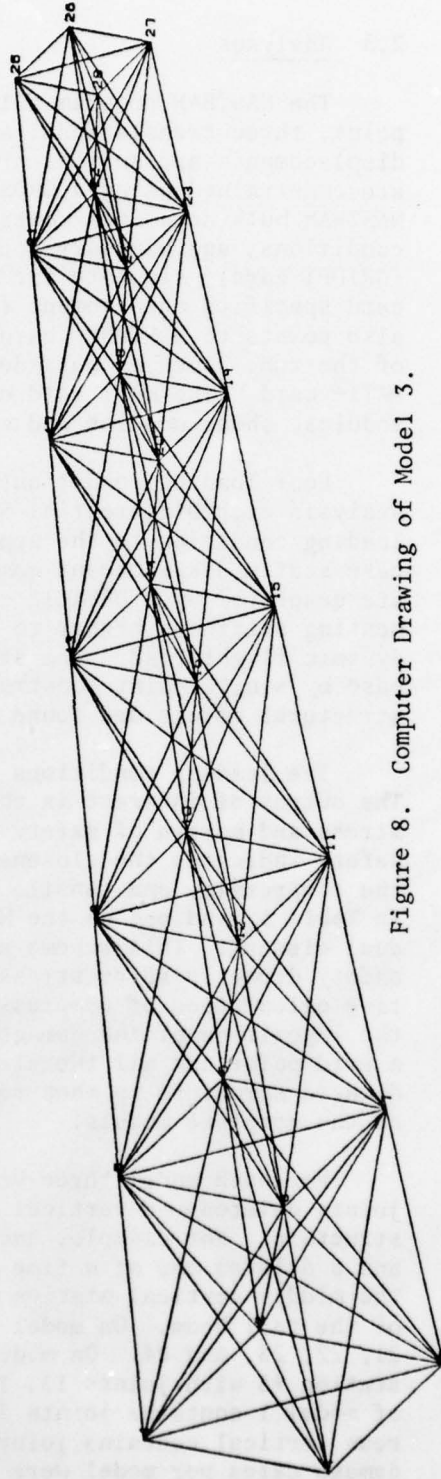


Figure 8. Computer Drawing of Model 3.

2.5 Analyses

The NASTRAN program allows six degrees of freedom for each grid point, three translational and three rotational. The translational displacements are sufficient in this study; rotational displacements are constrained using a GRDSET² card in the NASTRAN bulk data. The NASTRAN bulk data deck contains the structure design, the loading conditions, and boundary conditions to be used. The grid points (GRIDPT card)² simulate the geometric locations of joints. The CTUBE² card specifies the element (tube) connections between grid points and also points to a PTUBE² card. The PTUBE card specifies the properties of the tube, such as outside diameter and thickness, and points to the MAT1² card. The MAT1 card contains the material properties, Young's modulus, shear modulus and the compressive, and tensile stress limits.

Four loading conditions are simulated in rigid format 4 Static Analysis with Differential Stiffness by Force² cards which apply a 30% loading condition to the appropriate grid points used in the linear first case static displacement computation. The other three loading conditions are generated by a DSFACT² card which scales the applied load incrementing stiffness higher to 50%, 75%, and 100% of the 130 knot aerodynamic flight load. The structural models are simply supported at the base by single point constraints (SPC² cards). (Listings of the structural models are found in Appendices A, B, and C.)

The loading conditions are applied to the complete structure models. The output of interest is the displacements of grid points, the applied stress and margin of safety of each individual member. The margin of safety indicates the closeness of failure. For each individual member the compressive and tensile stress limits were calculated, as indicated in Table 1, and put on the MAT1 NASTRAN material card for that individual element. This scheme allows NASTRAN to compute the margins of safety directly after stresses are calculated (Table 1). A conservative calculation of compressive stress limit is found in Table 1. Then the imposition of the damage criterion is simulated by the removal of a grid point and all the elements connecting that grid point. The damaged structure is then reanalyzed with the same loading conditions as the complete models.

For each model three vertical stations were chosen to have their joints deleted -- a vertical station in front, middle and rear of the structure. For example, each model had front vertical joints 5, 6, 7, and 8 deleted one at a time and then analyzed with the flight loads. The middle vertical station of each model also supports the elevator of the tail boom. On model 1 this is vertical station #5 with joints 21, 22, 23, and 24. On model 2 and model 3 the middle is vertical station #3 with joints 13, 14, 15, and 16. The rear vertical station of model 1 contains joints 37, 38, 39, and 40. Model 2 and model 3 rear vertical contains joints 21, 22, 23, and 24. A total of twelve damage cases per model were simulated.

Extraction of a structure's natural frequencies can be performed by rigid format 3 of NASTRAN Normal Modes and Frequencies. These natural frequencies of structures are important in the analyses of aircraft structures. The natural frequencies are found only for the complete structures in this study.

2.6 Procedural Assumption

The existing semimonocoque tail boom at the base is canted at a small angle upward. Assuming a vertical base in our models is believed to be acceptable. Realistically, portions of members that enter a joint may remain affixed to the truss structure after loss of a joint. The effects of these members (or portions thereof) remaining are considered minor, and therefore are neglected in this study.

III. RESULTS

The appendices A, B, and C are listings of each complete model plus the results of displacements of each joint, stresses and margins of safety for each element for the applied loads. Resultant geometry framework is given in Appendices D, E, and F. Appendix D specifies the element connections between joints. The connection scheme is a replication and is valid for all the truss models. The only exceptions are: models 2 and 3 end at element number 138 and model 2 does not contain interior diagonals. Appendix E lists the joint locations of model 1 and Appendix F lists the joint locations of models 2 and 3.

3.1 Displacements

Maximum deflections at the end of the boom are limited because the maximum angle of the driveshaft couplings is 1° . Figure 9 shows where the couplings are located in reference to the end of the boom and provides the maximum deflection constraint to be 8.13 cm (3.2 in). Table 3 shows the maximum displacements of the truss models with and without damage imposed. These displacements lie comfortably within this maximum deflection constraint.

Table 4 lists the ratio of damage conditions displacements to the undamaged condition displacements of the complete longeron diagonally opposite a deleted node for damage to model 1. Each loading condition is presented. Translations of the X direction displacement are insignificant and not presented.

Table 5 lists the same results for model 2 and the results for model 3 are listed in Table 6.

3.2 Margins of Safety

The margin of safety of an individual element indicates its closeness to failure. Buckling failure determined by margin of safety

DRIVESHAFT COUPLINGS

$$\begin{aligned} \ell_1 &= 159.72\text{cm} \text{ (62.88 in.)} \\ \ell_2 &= 155.04\text{cm} \text{ (60.04 in.)} \end{aligned}$$

$$d_I = \ell_I \tan I^\circ \quad I=1,2$$

$$d_1 = \ell_1 \tan 1^\circ = 2.79\text{cm} \text{ (1.10 in.)}$$

$$d_2 = \ell_2 \tan 2^\circ = 5.33\text{cm} \text{ (2.10 in.)}$$

$$d_T = d_1 + d_2$$

$$d_T = 8.12\text{cm} \text{ (3.2 in.)}$$

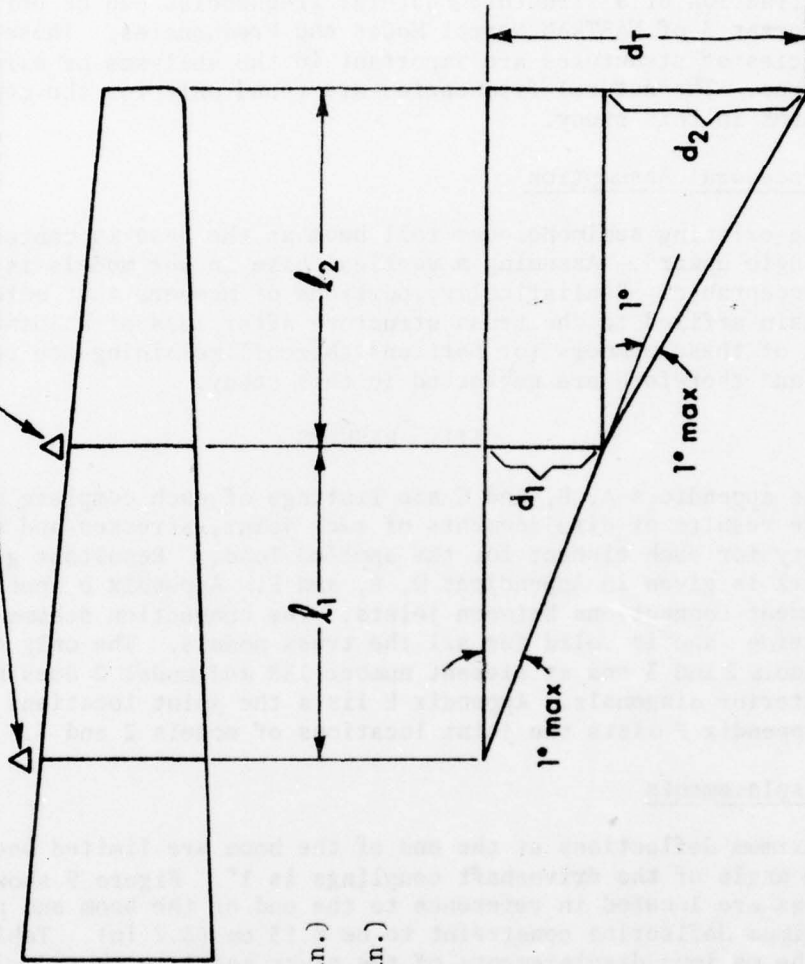


Figure 9. Maximum Deflection Constraint Due to Drive Shaft Couplings.

TABLE 3
 Maximum Displacement at End of Boom Due to 100% Flight Load
 With Joints Deleted

Damage	MODEL 1			Damage	MODEL 2			z	MODEL 3		
	y	z	y		y	z	y		z		
None	1.17cm	.797cm	None	1.09cm	.797cm	1.10cm	.784cm				
-5	1.97cm	1.55cm	-5	1.91cm	1.55cm	1.89cm	1.53cm				
-6	1.08cm	.9.50cm	-6	1.10cm	.955cm	1.10cm	.935cm				
-7	1.91cm	1.55cm	-7	1.83cm	1.60cm	1.84cm	1.53cm				
-8	1.11cm	.965cm	-8	1.17cm	1.01cm	1.13cm	.950cm				
-21	1.45cm	1.02cm	-13	1.55cm	1.04cm	1.50cm	1.04cm				
-22	1.37cm	.635cm	-14	1.32cm	.630cm	1.33cm	.635cm				
-23	1.35cm	1.04cm	-15	1.34cm	1.22cm	1.37cm	1.14cm				
-24	1.42cm	.650cm	-16	1.53cm	.81cm	1.46cm	.726cm				
-37	1.30cm	.866cm	-21	1.43cm	.889cm	1.36cm	.899cm				
-38	1.21cm	.772cm	-22	1.15cm	.726cm	1.19cm	.741cm				
-39	1.24cm	.901cm	-23	1.17cm	1.10cm	1.21cm	1.01cm				
-40	1.27cm	.795cm	-24	1.39cm	.924cm	1.33cm	.843cm				

TABLE 4a. Ratio of Damage Displacements to Undamage Displacements on Longeron Opposite Damage Criterion

MODEL 1 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 5

Lower Right Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	7	-.522	1.42	-.541	1.40	-.244	1.41	-.430	1.40
	11	-37.9	1.92	-40.1	1.91	-41.5	1.92	-43.1	1.93
	15	8.02	2.03	8.19	3.01	8.16	2.05	8.17	2.05
	19	4.73	2.00	4.81	2.09	4.74	2.03	4.77	2.04
	23	3.51	1.98	3.59	2.01	3.48	1.98	3.52	1.99
	27	2.90	1.97	2.90	1.98	2.92	1.96	2.93	1.97
	31	2.57	1.96	2.55	1.95	2.54	1.95	2.56	1.96
	35	2.24	1.95	2.23	1.94	2.21	1.94	2.23	1.94
	39	2.01	1.94	2.01	1.93	2.02	1.93	2.10	1.93
	43	1.97	1.93	1.98	1.92	1.96	1.91	1.97	1.92

Damage - Joint 21

	7	1.00	1.00	.99	1.00	.992	1.00	.989	1.00
	11	1.02	1.00	.94	1.00	.898	1.00	.857	1.00
	15	1.00	1.00	1.00	1.00	1.0	1.00	1.00	1.00
	19	.99	1.00	.990	1.00	.990	1.00	1.00	1.00
	23	1.05	1.02	1.06	1.02	1.07	1.02	1.08	1.02
	27	1.20	1.10	1.21	1.10	1.21	1.10	1.22	1.10
	31	1.27	1.17	1.28	1.18	1.28	1.18	1.29	1.19
	35	1.29	1.21	1.31	1.22	1.31	1.22	1.31	1.23
	39	1.30	1.25	1.31	1.25	1.31	1.26	1.32	1.27
	43	1.29	1.27	1.29	1.28	1.30	1.28	1.31	1.29

Damage - Joint 37

	7	1.00	1.00	.99	1.00	1.0	1.00	.985	1.00
	11	1.00	1.00	.87	1.00	.801	1.00	.722	1.00
	15	1.00	1.00	1.00	1.00	1.03	1.00	1.05	1.00
	19	1.00	1.00	1.01	1.00	1.02	1.00	1.03	1.00
	23	1.00	1.00	1.01	1.00	1.02	1.00	1.02	1.00
	27	1.00	1.00	1.01	1.00	1.02	1.00	1.02	1.00
	31	1.00	1.00	1.01	1.00	1.02	1.00	1.02	1.00
	35	1.00	1.00	1.01	1.00	1.02	1.00	1.02	1.00
	39	1.01	1.02	1.02	1.02	1.03	1.02	1.04	1.02
	43	1.07	1.07	1.08	1.07	1.09	1.07	1.09	1.08

TABLE 4b. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

MODEL 1 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 6

Upper Right Longeron (viewed from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	8	.899	1.11	.896	1.11	.892	1.12	.889	1.12
	12	.848	1.21	.843	1.21	.837	1.22	.831	1.22
	16	.857	1.22	.852	1.22	.848	1.23	.841	1.23
	20	.867	1.20	.860	1.21	.857	1.22	.854	1.22
	24	.880	1.19	.879	1.20	.879	1.20	.868	1.20
	28	.893	1.19	.889	1.20	.885	1.20	.883	1.20
	32	.903	1.19	.901	1.19	.895	1.19	.894	1.19
	36	.913	1.18	.908	1.18	.906	1.19	.905	1.19
	40	.915	1.18	.915	1.18	.915	1.19	.913	1.18
	44	.927	1.18	.925	1.18	.922	1.19	.919	1.19

Damage - Joint 22

	8	.999	.999	1.0	1.0	1.0	1.0	1.0	1.0
	12	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	16	.998	1.0	.998	1.0	.999	1.0	1.0	1.0
	20	1.0	1.0	1.0	1.0	.999	1.0	.998	1.0
	24	1.02	.986	1.02	.989	1.02	.991	1.02	.992
	28	1.10	.901	1.10	.916	1.09	.929	1.09	.932
	32	1.15	.858	1.15	.864	1.14	.875	1.13	.880
	36	1.17	.815	1.17	.826	1.16	.837	1.15	.843
	40	1.18	.785	1.18	.788	1.17	.810	1.16	.818
	44	1.18	.758	1.18	.773	1.17	.788	1.17	.797

Damage - Joint 38

	8	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	12	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	16	1.0	1.0	1.0	1.0	.996	1.0	1.0	1.0
	20	1.0	1.0	1.0	1.0	.995	1.0	.995	1.0
	24	1.0	1.0	1.0	1.0	.995	1.0	.994	1.0
	28	1.0	1.0	1.0	1.0	.995	1.0	.993	1.0
	32	1.0	1.0	1.0	1.0	.994	1.01	.992	1.0
	36	1.0	1.0	1.0	1.01	.995	1.01	.994	1.01
	40	1.01	.991	1.01	.997	1.0	1.0	1.0	1.0
	44	1.04	.947	1.04	.954	1.04	.960	1.03	.964

TABLE 4c. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 1 $r_i = \frac{DD}{UD}$, $i = y, z$

Damage - Joint 7

Upper Left Longeron (viewed from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	5	1.5	-5.63	1.51	-6.56	1.53	-7.13	1.54	-7.77
	9	2.13	5.05	2.14	4.99	2.16	4.94	2.17	4.89
	13	2.20	3.69	2.22	3.68	2.24	3.66	2.26	3.64
	17	2.11	3.18	2.13	3.16	2.15	3.15	2.16	3.14
	21	2.0	2.90	2.01	2.89	2.03	2.88	2.04	2.87
	25	1.89	2.79	1.9	2.78	1.92	2.77	1.93	2.75
	29	1.80	2.72	1.82	2.70	1.83	2.68	1.84	2.67
	33	1.72	2.67	1.73	2.65	1.75	2.64	1.76	2.62
	37	1.66	2.69	1.67	2.66	1.68	2.62	1.69	2.58
	41	1.60	2.60	1.61	2.58	1.62	2.55	1.63	2.53

Damage - Joint 23

	5	1.0	1.0	1.0	1.0	1.0	.992	1.0	.983
	9	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	13	1.0	1.0	1.0	1.0	1.0	1.01	1.0	1.01
	17	1.0	.987	1.0	.990	1.01	.973	1.01	.995
	21	1.03	1.03	1.03	1.03	1.04	1.04	1.04	1.04
	25	1.10	1.17	1.10	1.17	1.11	1.18	1.12	1.18
	29	1.15	1.28	1.15	1.29	1.16	1.30	1.17	1.30
	33	1.17	1.36	1.17	1.36	1.18	1.36	1.19	1.36
	37	1.18	1.41	1.18	1.41	1.19	1.41	1.20	1.41
	41	1.18	1.44	1.19	1.44	1.19	1.44	1.20	1.44

Damage - Joint 39

	5	1.0	1.0	1.0	1.0	1.0	.990	1.0	.928
	9	1.0	1.0	1.0	1.0	1.0	1.01	1.0	1.02
	13	1.0	1.0	1.0	1.01	1.0	1.01	1.01	1.01
	17	1.0	1.0	1.0	1.01	1.0	1.01	1.01	1.01
	21	1.0	1.0	1.0	1.0	1.01	1.0	1.01	1.01
	25	1.0	1.0	1.01	1.0	1.01	1.01	1.01	1.01
	29	1.0	1.0	1.01	1.01	1.01	1.01	1.01	1.01
	33	1.0	1.0	1.01	1.01	1.01	1.01	1.01	1.01
	37	1.01	1.02	1.02	1.02	1.02	1.03	1.02	1.03
	41	1.04	1.10	1.04	1.10	1.05	1.11	1.05	1.11

TABLE 4d. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 1 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 8

Lower Left Longeron (viewed from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
		6	1.29	.670	1.30	.651	1.31	.627	1.31
10	3.06	1.0	3.14	1.33	3.24	1.72	3.32	1.98	
14	.013	1.54	-.040	1.55	-.064	1.56	-.087	1.56	
18	.567	1.42	.555	1.43	.538	1.44	.519	1.44	
22	.722	1.36	.710	1.36	.701	1.37	.689	1.38	
26	.795	1.34	.787	1.34	.779	1.35	.771	1.35	
30	.838	1.32	.830	1.32	.824	1.33	.818	1.33	
34	.865	1.31	.859	1.31	.853	1.32	.848	1.32	
38	.887	1.31	.882	1.31	.877	1.31	.872	1.31	
42	.901	1.30	.90	1.30	.889	1.30	.888	1.30	

Damage - Joint 24

6	1.0	.996	1.0	.991	1.0	.985	1.0	.981
10	.998	1.0	1.04	1.01	1.07	1.01	1.09	1.01
14	1.0	1.0	.995	1.0	.989	1.01	.985	1.01
18	.981	.996	.977	.998	.973	1.0	.969	1.0
22	1.03	.952	1.03	.956	1.02	.960	1.02	.965
26	1.19	.810	1.18	.822	1.17	.834	1.17	.844
30	1.27	.690	1.26	.707	1.25	.725	1.24	.743
34	1.29	.617	1.28	.639	1.27	.660	1.27	.683
38	1.29	.563	1.29	.594	1.28	.623	1.27	.641
42	1.29	.532	1.28	.560	1.27	.691	1.26	.618

Damage - Joint 40

6	1.0	1.0	1.0	.994	1.0	.990	1.0	.986
10	1.0	1.0	1.02	1.01	1.06	1.01	1.08	1.01
14	1.0	1.0	.983	1.01	.967	1.01	.950	1.01
18	1.0	1.0	.989	1.0	.982	1.01	.971	1.01
22	1.0	1.0	.993	1.0	.985	1.01	.977	1.01
26	1.0	1.0	.994	1.0	.987	1.01	.979	1.01
30	1.0	.991	.996	.997	.988	1.0	.981	1.01
34	.996	.999	.990	1.0	.984	1.0	.978	1.01
38	1.01	.970	1.0	.976	1.0	.981	.996	.987
42	1.07	.868	1.06	.879	1.05	.891	1.05	.902

TABLE 5a. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 2 $r_k = \frac{DD}{UD}$, i - y,z.

Damage - Joint 5

Lower Right Longeron (viewed from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	7	-.144	1.15	-.150	1.16	-.153	1.17	-.158	1.17
	11	-9.47	1.69	-9.83	1.70	-10.02	1.71	-10.21	1.71
	15	10.80	1.82	10.82	1.83	10.77	1.84	10.76	1.84
	19	4.47	1.89	4.53	1.90	4.55	1.90	4.59	1.90
	23	3.11	1.92	3.15	1.91	3.18	1.92	3.20	1.92
	27	2.52	1.95	2.56	1.94	2.57	1.94	2.59	1.94

Damage - Joint 13

	7	1.0	1.0	.998	1.0	.997	1.0	.996	1.0
	11	1.14	1.0	1.11	1.0	1.10	1.0	1.09	1.0
	15	1.82	.988	1.84	.995	1.87	1.0	1.88	1.0
	19	1.94	1.10	1.97	1.12	2.00	1.12	2.02	1.13
	23	1.76	1.21	1.79	1.22	1.80	1.23	1.82	1.24
	27	1.63	1.27	1.66	1.29	1.68	1.31	1.69	1.31

Damage - Joint 21

	7	1.0	1.0	.994	1.0	.990	1.0	.985	1.0
	11	.998	1.0	.960	1.0	.940	1.0	.918	1.01
	15	.998	1.0	1.04	1.0	1.06	1.0	1.08	1.01
	19	.977	1.0	.996	1.0	1.0	1.01	1.01	1.01
	23	1.09	.988	1.11	1.0	1.11	1.0	1.12	1.01
	27	1.30	1.07	1.32	1.09	1.33	1.10	1.34	1.11

TABLE 5b. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 2

$$r_i = \frac{DD}{UD}, \quad i = y, z.$$

Upper Right Longeron (view from rear)	Load Joint	Damage - Joint 6							
		30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	8	.860	.973	.855	.977	.852	.981	.849	.986
	12	.919	1.07	.906	1.08	.899	1.09	.893	1.10
	16	1.0	1.13	.989	1.14	.980	1.15	.978	1.16
	20	1.02	1.15	1.01	1.16	1.0	1.17	1.0	1.18
	24	1.02	1.16	1.01	1.17	1.01	1.18	1.0	1.19
	28	1.02	1.17	1.02	1.18	1.01	1.19	1.01	1.19
		Damage - Joint 14							
	8	.996	1.0	.996	1.0	.995	1.0	.995	1.0
	12	.997	1.01	.997	1.01	.996	1.01	.996	1.01
	16	.984	.950	.982	.959	.981	.964	.980	.967
	20	1.12	.814	1.11	.834	1.11	.842	1.10	.853
	24	1.20	.760	1.19	.788	1.18	.799	1.18	.814
	28	1.23	.724	1.22	.757	1.21	.769	1.21	.788
		Damage - Joint 22							
	8	1.0	1.0	1.0	1.0	.997	1.0	.997	1.0
	12	1.0	1.0	.998	1.0	.997	1.01	.997	1.01
	16	1.0	1.0	.997	1.0	.996	1.01	.996	1.01
	20	1.0	1.0	1.0	1.01	.997	1.02	.997	1.02
	24	.996	.963	.994	.978	.993	.985	.992	.992
	28	1.06	.866	1.05	.890	1.05	.901	1.05	.912

TABLE 5c. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 2 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 7

Upper Left Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	5	1.13	-5.89	1.12	-7.54	1.15	-8.66	1.15	-10.0
	9	1.77	6.73	1.80	6.32	1.81	6.16	1.83	5.99
	13	1.86	4.75	1.89	4.54	1.91	4.46	1.93	4.38
	17	1.80	4.50	1.82	4.29	1.84	4.20	1.85	4.10
	21	1.71	4.38	1.74	4.11	1.75	4.01	1.76	3.91
	25	1.63	4.24	1.65	4.00	1.66	3.92	1.67	3.78

Damage - Joint 15

5	.994	1.03	.996	.987	.997	.952	.998	.918
9	1.0	.925	1.0	.959	1.0	.968	1.0	.987
13	.986	1.34	.988	1.34	.990	1.34	.992	1.34
17	1.10	1.93	1.11	1.90	1.12	1.88	1.12	1.86
21	1.18	2.11	1.19	2.05	1.20	2.03	1.20	2.00
25	1.21	2.23	1.21	2.15	1.22	2.12	1.22	2.09

Damage - Joint 23

5	1.0	1.0	1.0	.960	1.0	.888	1.0	.800
9	1.0	1.0	1.0	1.03	1.0	1.05	1.0	1.06
13	1.0	1.0	1.0	1.04	1.0	1.06	1.0	1.06
17	1.0	.982	1.0	1.01	1.0	1.03	1.0	1.05
21	.996	1.13	1.0	1.15	1.0	1.17	1.0	1.19
25	1.06	1.49	1.06	1.49	1.07	1.49	1.07	1.49

TABLE 5d. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criterion

Model 2 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 8

Lower Left Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	6	.637	-.760	.656	-.978	.666	-1.09	.675	-1.23
	10	-.136	2.86	.011	2.79	.082	2.77	.153	2.74
	14	1.66	1.81	1.48	1.82	1.40	1.83	1.31	1.84
	18	1.17	1.66	1.11	1.67	1.09	1.69	1.06	1.69
	22	1.09	1.59	1.06	1.60	1.04	1.60	1.02	1.61
	26	1.05	1.54	1.03	1.54	1.02	1.55	1.0	1.55

Damage - Joint 16

	6	.996	.978	.997	.954	.998	.941	1.0	.927
	10	1.16	.995	1.18	1.02	1.18	1.03	1.19	1.04
	14	1.81	1.18	1.75	1.20	1.72	1.21	1.70	1.21
	18	2.00	.735	1.95	.833	1.93	.875	1.91	.911
	22	1.82	.381	1.78	.541	1.76	.602	1.74	.666
	26	1.68	.200	1.65	.397	1.63	.474	1.62	.549

Damage - Joint 24

	6	1.0	1.0	1.0	.950	1.0	.960	1.01	.945
	10	1.0	.998	1.02	1.02	1.04	1.04	1.05	1.06
	14	.998	1.0	.960	1.02	.943	1.04	.928	1.05
	18	.977	1.0	.960	1.03	.953	1.04	.946	1.05
	22	1.09	1.04	1.07	1.08	1.07	1.09	1.06	1.11
	26	1.30	.713	1.28	.815	1.27	.857	1.26	.895

TABLE 6a. Ratio of Damage Displacements to Undamaged Displacements on Longeron Opposite Damage Criteria

MODEL 3 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 5

Lower Right Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	7	.129	1.29	.118	1.30	.112	1.30	.106	1.30
	11	-9.28	1.80	-9.67	1.81	-9.90	1.82	-10.13	1.82
	15	9.53	1.89	9.55	1.89	9.57	1.90	9.58	1.90
	19	4.22	1.92	4.27	1.92	4.30	1.93	4.33	1.93
	23	3.00	1.94	3.03	1.94	3.05	1.94	3.07	1.94
	27	2.45	1.96	2.48	1.95	2.50	1.95	2.51	1.95

Damage - Joint 13

	7	.996	.998	.991	1.0	.988	1.0	.985	1.0
	11	1.14	1.0	1.12	1.02	1.10	1.01	1.09	1.0
	15	1.34	1.04	1.38	1.04	1.40	1.04	1.41	1.04
	19	1.70	1.16	1.73	1.17	1.75	1.18	1.76	1.18
	23	1.64	1.25	1.67	1.26	1.68	1.27	1.70	1.27
	27	1.56	1.30	1.59	1.31	1.60	1.32	1.61	1.32

Damage - Joint 21

	7	1.0	1.0	.993	1.0	.990	1.0	.987	1.0
	11	1.0	1.0	.962	1.0	.941	1.0	.920	1.0
	15	1.0	1.0	1.03	1.0	1.05	1.01	1.07	1.01
	19	.983	1.0	1.0	1.01	1.01	1.01	1.01	1.01
	23	1.03	1.02	1.05	1.02	1.06	1.03	1.06	1.03
	27	1.22	1.11	1.23	1.12	1.24	1.13	1.25	1.14

TABLE 6b. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criteria

MODEL 3 $r_i = \frac{DD}{UD}$, $i = y, z$.

Damage - Joint 6

Upper Right Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	8	.945	1.06	.937	1.06	.934	1.07	.930	1.07
	12	1.0	1.16	.990	1.17	.983	1.18	.976	1.18
	16	1.02	1.16	1.01	1.17	1.0	1.18	1.0	1.19
	20	1.02	1.16	1.01	1.17	1.01	1.18	1.0	1.19
	24	1.02	1.16	1.01	1.17	1.01	1.18	1.0	1.19
	28	1.02	1.16	1.01	1.17	1.0	1.18	1.0	1.19

Damage - Joint 14

	8	.997	.933	.997	1.0	.997	1.0	.997	1.0
	12	1.0	1.0	1.0	1.01	1.0	1.01	1.0	1.01
	16	1.02	.980	1.02	.987	1.02	.990	1.02	.994
	20	1.16	.869	1.15	.887	1.15	.895	1.14	.903
	24	1.22	.797	1.21	.822	1.21	.834	1.20	.846
	28	1.23	.749	1.22	.780	1.22	.795	1.21	.810

Damage - Joint 22

	8	1.0	1.0	.998	1.0	.997	1.0	.997	1.0
	12	1.0	1.0	.998	1.0	.997	1.0	.997	1.0
	16	1.0	1.0	.997	1.0	.996	1.01	.996	1.01
	20	1.0	1.0	1.0	1.01	1.0	1.01	1.0	1.02
	24	1.01	.985	1.01	.996	1.01	1.0	1.01	1.0
	28	1.09	.905	1.08	.925	1.08	.934	1.07	.943

TABLE 6c. Ratio of Damaged Displacements to Undamaged Displacements on Longeron Opposite Damage Criteria

MODEL 3 $r_i = \frac{DD}{UD}$, $i = y, z.$

Damage - Joint 7

Upper Left Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	5	1.35	-.971	1.37	-1.20	1.38	-1.34	1.38	-1.49
	9	1.90	8.10	1.93	7.31	1.95	7.01	1.97	6.72
	13	1.91	5.19	1.93	4.89	1.95	4.77	1.97	4.65
	17	1.81	4.74	1.84	4.44	1.86	4.33	1.87	4.22
	21	1.72	4.51	1.74	4.20	1.76	4.09	1.77	3.96
	25	1.62	4.37	1.65	4.05	1.66	3.92	1.67	3.80

Damage - Joint 15

	5	.998	.991	1.0	.977	1.0	.969	1.0	.961
	9	1.0	.890	1.0	.933	1.0	.949	1.01	.965
	13	1.04	1.16	1.04	1.17	1.04	1.18	1.05	1.18
	17	1.16	1.42	1.17	1.67	1.18	1.66	1.18	1.65
	21	1.21	1.96	1.22	1.91	1.23	1.89	1.24	1.87
	25	1.22	2.11	1.23	2.04	1.24	2.01	1.24	1.98

Damage - Joint 23

	5	1.0	1.0	1.0	.976	1.0	.961	1.0	.946
	9	1.0	1.0	1.0	1.03	1.0	1.05	1.0	1.07
	13	1.0	1.0	1.0	1.03	1.0	1.04	1.0	1.05
	17	1.0	.982	1.0	1.01	1.0	1.02	1.0	1.04
	21	1.01	1.06	1.01	1.09	1.02	1.10	1.02	1.11
	25	1.09	1.36	1.09	1.37	1.10	1.37	1.10	1.37

TABLE 6d. Ratio of Damaged Displacement to Undamaged Displacements on Longeron Opposite Damage Criteria

MODEL 3 $r_i = \frac{DD}{UD}$, $i = y, z.$

Damage - Joint 8

Lower Left Longeron (view from rear)	Load Joint	30%		50%		75%		100%	
		Y	Z	Y	Z	Y	Z	Y	Z
	6	1.15	.847	1.17	.806	1.18	.785	1.18	.761
	10	1.30	2.32	1.46	2.29	1.53	2.27	1.62	2.26
	14	.865	1.57	.724	1.60	.659	1.61	.594	1.63
	18	.975	1.48	.921	1.51	.895	1.52	.869	1.53
	22	.991	1.44	.958	1.46	.941	1.47	.925	1.48
	26	.997	1.41	.973	1.43	.962	1.44	.949	1.44

Damage - Joint 16

	6	.994	.987	.996	.973	.997	.966	.997	.958
	10	1.12	.914	1.13	.961	1.14	.977	1.14	.994
	14	1.19	.857	1.16	.904	1.14	.929	1.12	.941
	18	1.68	.374	1.64	.508	1.62	.561	1.60	.614
	22	1.65	.100	1.61	.289	1.59	.362	1.58	.435
	26	1.57	.017	1.55	.201	1.53	.284	1.52	.367

Damage - Joint 24

	6	1.0	1.0	1.0	.987	1.0	.980	1.0	.973
	10	1.0	1.0	1.02	1.04	1.04	1.06	1.05	1.07
	14	1.0	1.0	.970	1.02	.956	1.04	.942	1.05
	18	.983	.989	.968	1.02	.961	1.03	.955	1.04
	22	1.03	.916	1.02	.963	1.01	.981	1.01	1.0
	26	1.21	.549	1.20	.665	1.19	.797	1.18	.753

for each individual element is calculated in NASTRAN according to the relations given in Table 1. Buckling due to compressive stress occurs before failure of an element due to tension. An additional 20% safety factor is included for compressive stress limits. A margin of safety less than zero indicates failure. A margin of safety between zero and one indicates structural integrity and is acceptable. Margin of safety greater than one is preferred for the purposes of this study.

Members in tension have been found to have margins of safety (M.S.) greater than one for all the models. Since the major changes in M.S. only occur locally, only the neighborhood of the damage criterion joint in question is presented in the tables for the models.

Key for Tables 7 through 12

I.D. = interior diagonal; O.D. = outside diagonal
T.H. = transverse horizontal; T.V. = transverse vertical
T.D. = transverse diagonal; Long. = longeron
J-J = joint-to-joint connection
D = deleted member; T = member in tension
- = Nonexistent member; Blank space = compressive

Margin of Safety greater than 10.0.

The highly redundant and densely populated model 1 results give the highest margins of safety. The number of elements that have M.S. under ten are few. Tables 7, 8, and 9 present a list of compressive margins of safety under 10.0 for model 1 with damage conditions giving member number, type, and damage condition for the 100% loading condition. Model 1 does not have any margin of safety of less than 1.0.

Models 2 and 3, as explained before, are identical except model 3 has the interior diagonals included. In modeling these structures, elements have a one to one correspondence for ease in comparison (see Appendix D). Therefore, results of models 2 and 3 will be shown together for their margins of safety under 10.0 in Tables 10 through 12. Model 2 produces four cases where the margin of safety drops under 1.0 when damage is imposed. Model 3 has two cases where margin of safety is under 1.0. These cases are displayed in Table 13 where the two structures are presented together with their respective M.S. for different loading conditions. Figures 10 through 15 locate the members in the truss models whose M.S. falls under 1.0

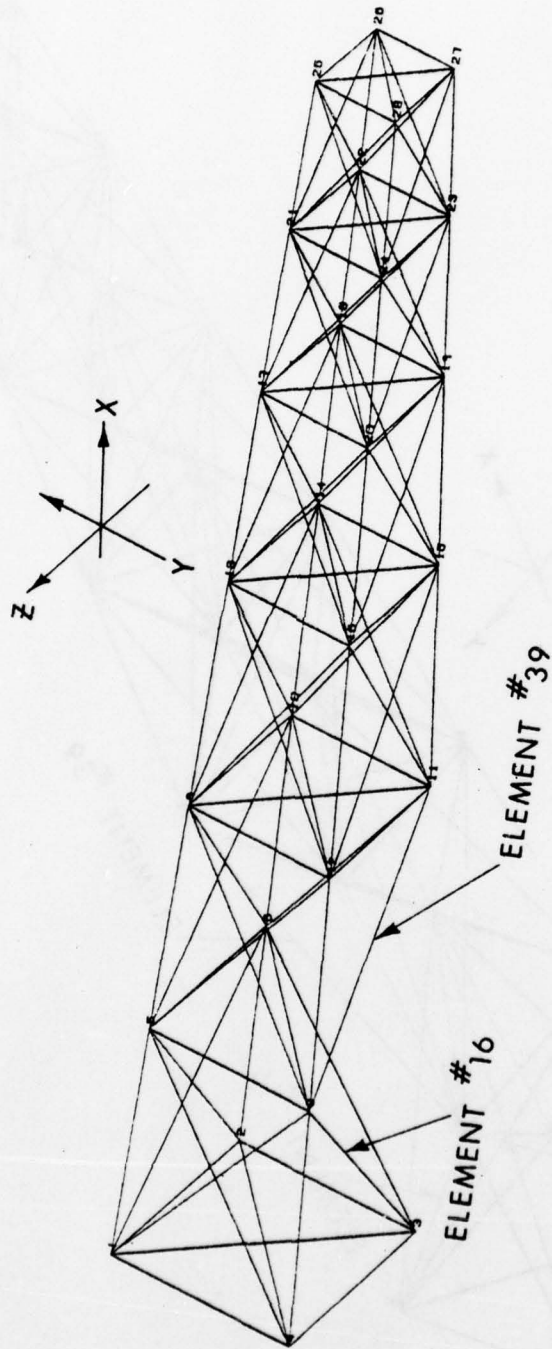


Figure 10. Computer Drawing of Model 2 with Damage of - Joint 7

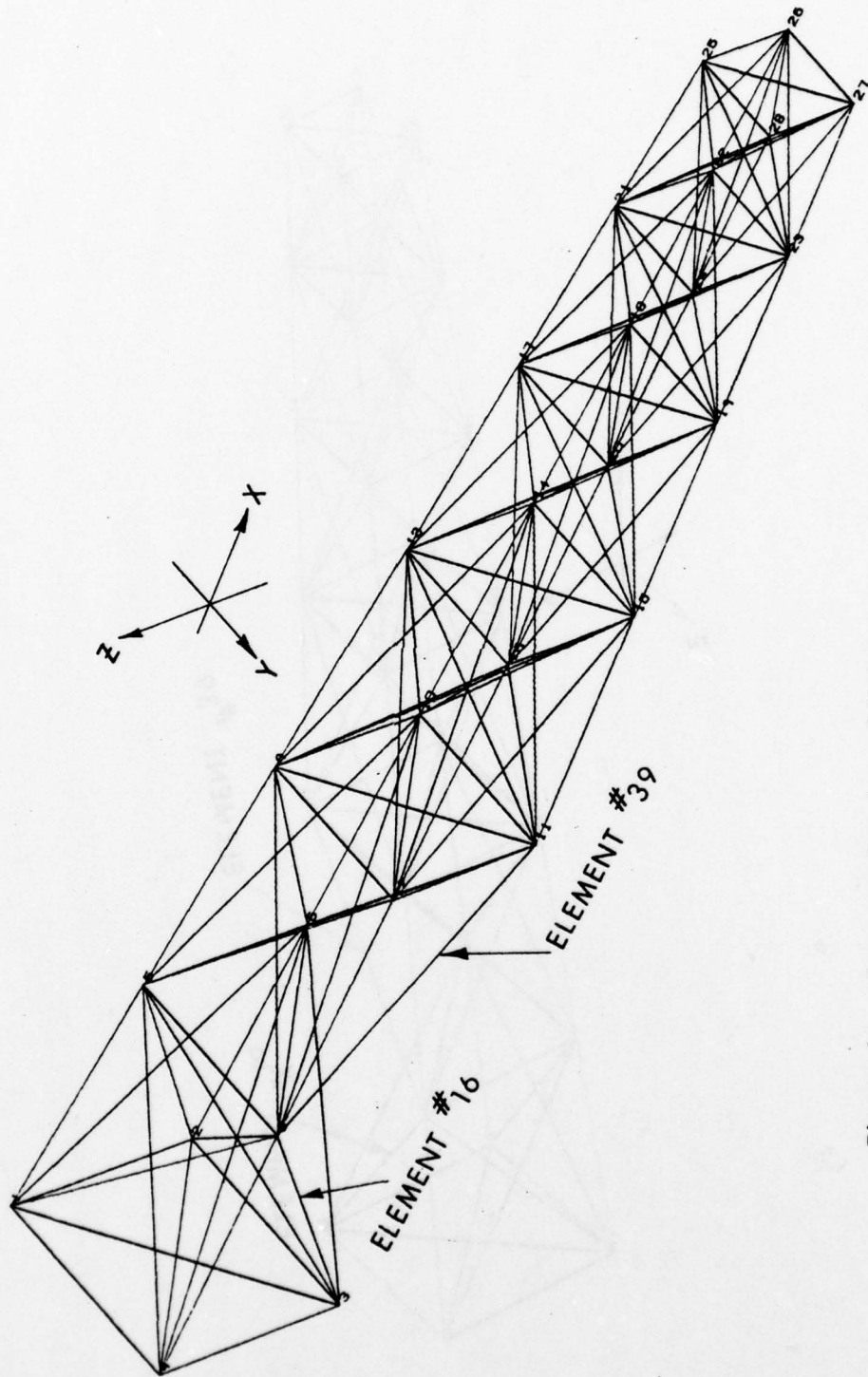


Figure 11. Computer Drawing of Model 3 with Damage of - Joint 7

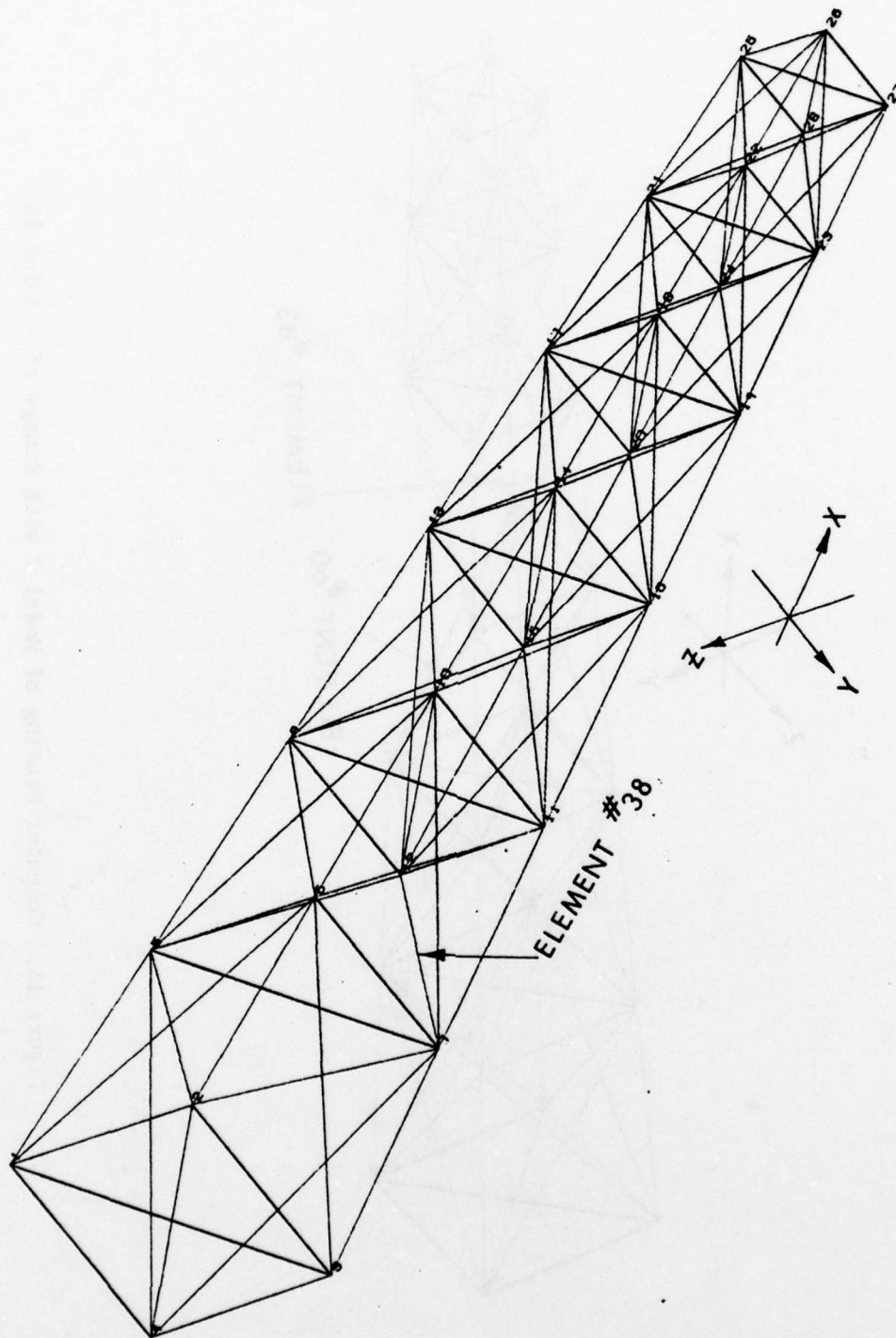


Figure 12. Computer Drawing of Model 2 with Damage of - Joint 8

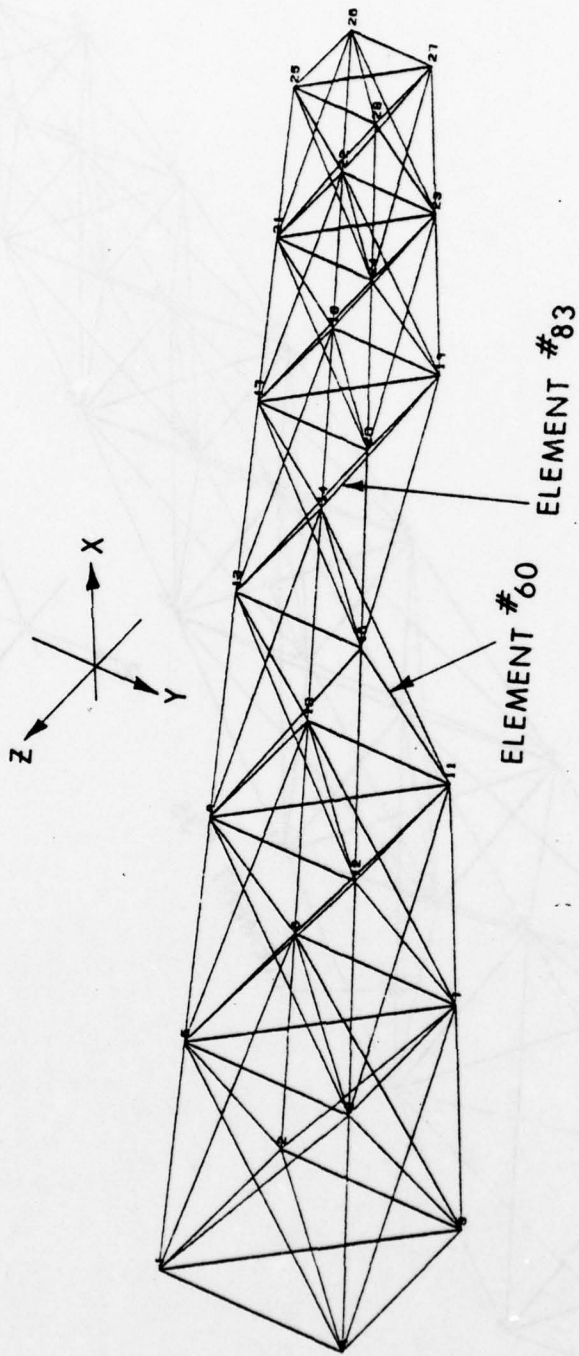


Figure 13. Computer Drawing of Model 2 with Damage of - Joint 15

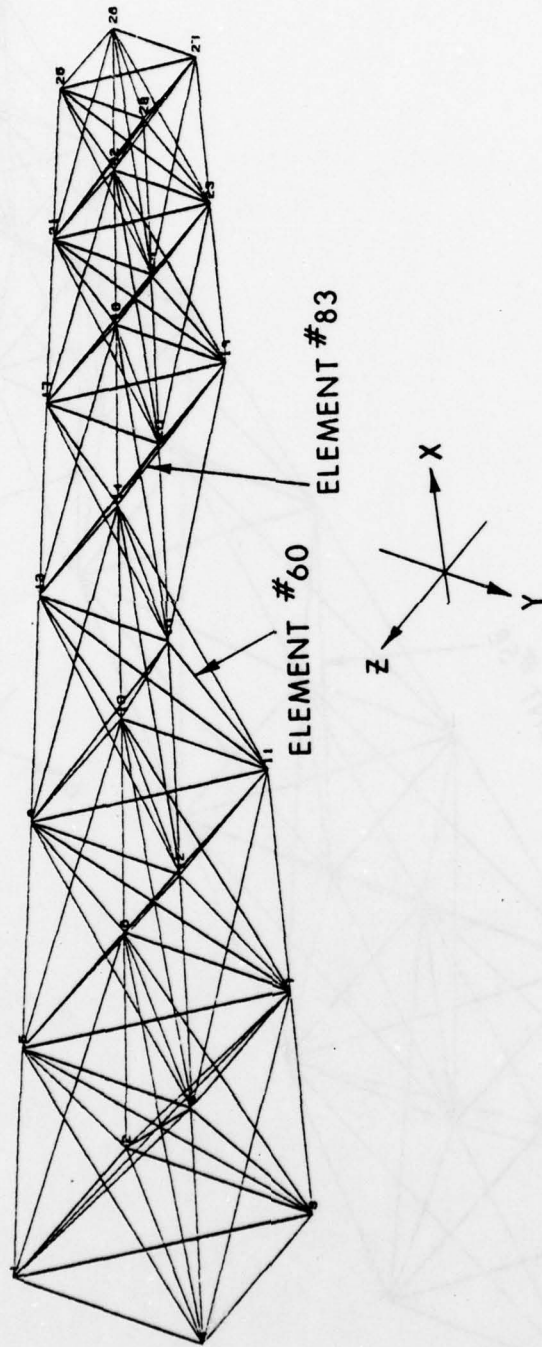


Figure 14. Computer Drawing of Model 3 with Damage of - Joint 15

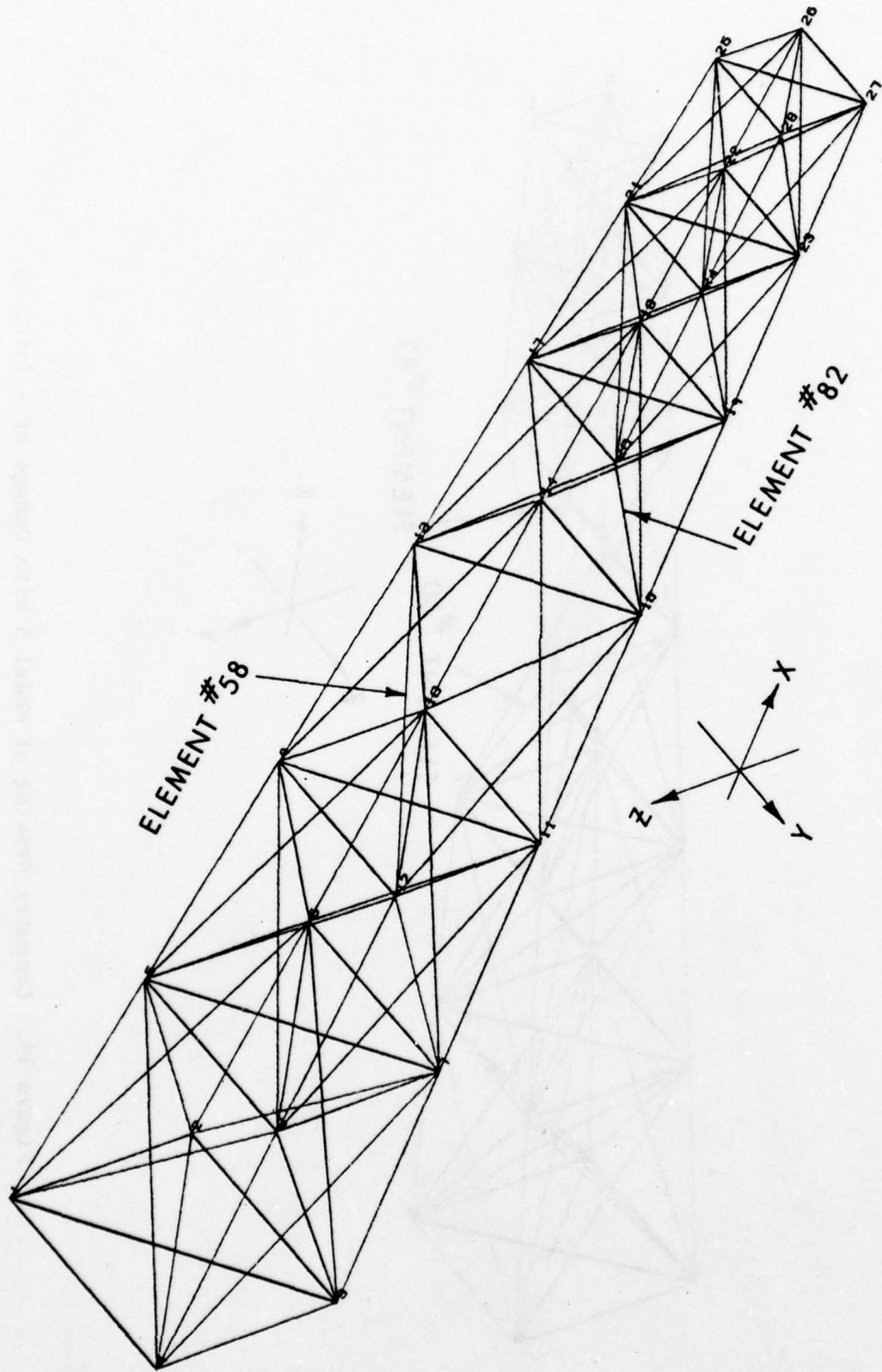


Figure 15. Computer Drawing of Model 2 with Damage of - Joint 16

TABLE 7
Compressive Margins of Safety Under 10.0 Due to 130 knot
Flight Load on Forward Vertical Sta with 100% Loading

DAMAGE MODEL 1 MEMBER	J-J	No#	None	Joint 5	Joint 6	Joint 7	Joint 8
Long.	1-5	7	T	D	T	T	T
"	2-6	8		T	D	4.3	
"	3-7	9	6.7	2.7	6.4	D	5.5
"	4-8	10	T	T	T		D
O.D.	1-6	11			D	4.8	
"	2-5	12	T	D	T	T	T
"	1-8	13	T	T	T	T	D
"	4-5	14		D		T	6.6
"	4-7	15	T	T	T	D	T
"	3-8	16	5.1	6.9	5.]	2.2	D
"	2-7	17	4.5	3.2	3.3	D	3.4
"	3-6	18	T	T	D	T	T
I.D.	1-7	19	T	T		D	T
"	2-8	20		T		7.6	D
"	3-5	21		D	T		6.9
"	4-6	22	T		T	T	T
T.V.	5-6	23		D	D		
T.H.	5-8	24		D			D
T.V.	7-8	25	T	T	T	D	D
T.H.	6-7	26	T	T	D	D	T
T.D.	5-7	27		D	T	D	
"	6-8	28		3.7	D	T	D
Long.	5-9	29	T	D	T	T	T
"	6-10	30	T	T	D		
"	7-11	31	8.1	3.7	5.3	D	
"	8-12	32	T	T	T	8.4	D
O.D.	5-10	33		D	5.6		
"	6-9	34	T	T	D	T	T
"	5-12	35	T	D	T	T	T
"	8-9	36				5.1	D
"	8-11	37	T	T	T	T	D
"	7-12	38	5.3	3.3	3.8	D	4.1
"	6-11	39	6.2	9.3	D	2.6	5.4
"	7-10	40	T	T	T	D	T
I.D.	5-11	41	T	D	10.		T
"	6-12	42		T	D	9.7	
"	8-10	44	T		T	T	D

TABLE 8
Compressive Margins of Safety Under 10.0 Due to 130 knot
Flight Load on Middle Vertical Sta with 100% Loading

DAMAGE MODEL 1 MEMBER			None	Joint 21	Joint 22	Joint 23	Joint 24
J-J	No#						
Long.	17-21	95	T	D	T	T	T
"	18-22	96	T	T	D		T
"	19-23	97		10.		D	8.6
"	20-24	98					D
O.D.	17-22	99			D	8.9	
"	18-21	100	T	D	T	T	T
"	17-24	101	T	T	T	T	D
"	20-21	102		D			5.5
"	20-23	103	T	T	T	D	T
"	19-24	104	7.1	7.3	5.6	3.8	D
"	18-23	105		7.5	8.6	D	6.0
"	19-22	106	T	T	D	T	T
I.D.	17-23	107	T			D	T
"	18-24	108		T			D
"	19-21	109	T	D	T	T	
"	20-22	110	T		D	T	T
T.V.	21-22	111		D	D		
T.H.	21-24	112		D	T		D
T.V.	23-24	113	T	T	T	D	D
T.H.	22-23	114		T	D	D	
T.D.	21-23	115		D		D	T
"	22-24	116			D	T	D
Long.	21-25	117	T	D	T	T	
"	22-26	118	T	T	D	T	T
"	23-27	119				D	
"	24-28	120		T			D
O.D.	21-26	121		D	9.9		9.2
"	22-25	122	T	T	D	T	T
"	21-28	123	T	D	T	T	T
"	24-25	124			9.6	7.7	D
"	24-27	125	T	T	T	T	D
"	23-28	126	8.8	6.6	8.3	D	5.0
"	22-27	127			D	5.5	
"	23-26	128	T	T	T	D	T
I.D.	21-27	129		D			T
"	22-28	1-0	T	T	D		
"	23-25	131		T	T	D	
"	24-26	132	T		T	T	D

TABLE 9
 Compressive Margins of Safety Under 10.0 Due to 130 knot
 Flight Load on End Vertical Sta with 100% Loading

DAMAGE MODEL 1 MEMBER	J-J	No#	None	Joint 37	Joint 38	Joint 39	Joint 40
Long.	33-37	183	T	D	T	T	T
"		184	T	T	D		T
"		185			T	D	
"		186					D
O.D.		187			D		
"		188	T	D	T	T	T
"		189	T	T	T	T	D
"		190		D			8.0
"		191	T	T	T	D	T
"		192	7.2	7.8	5.6	4.0	D
"		193				D	8.9
"		194	T	T	D	T	T
I.D.		195		T		D	T
"		196		T	T		D
"		197	T	D	T		
"		198	T		D	T	
T.V.		199		D	D		
T.H.		200		D	T		D
T.V.		201	T	T	T	D	D
T.H.		202	T	T	D	D	T
T.V.		203	T	D		D	T
T.H.		204			D	T	D
Long.		205	T	D	T	T	T
"		206	T	T	D	T	T
"		207				D	
"		208		T			D
O.D.		209		D			
"		210	T	T	D	T	T
"		211	T	D	T	T	T
"		212				9.4	D
"		213	T	T	T	T	D
"		214		8.1		D	5.9
"		215			D	7.3	
"		216	T	T	T	D	T
I.D.		217		D			T
"		218	T	T	D		
"		219		T	T	D	
"		220	T		T	T	D

TABLE 10
Compressive Margins of Safety Under 10.0 Due to 130 knot
Flight Load on Forward Vertical Sta with 100% Loading
for Models 2 and 3

DAMAGE MODEL MEMBER	J-J	No.#	None		Joint 5		Joint 6		Joint 7		Joint 8	
			2	3	2	3	2	3	2	3	2	3
Long.	1-5	7	T	T	D	D	T	T	T	T	T	T
"	2-6	8			T	T	D	D	2.0	2.3		
"	3-7	9	3.6	3.6	1.4	1.3	4.1	4.1	D	D	1.9	2.2
"	4-8	10	T	T	T	T	T	T			D	D
O.D.	1-6	11		8.0	8.4	10.	D	D	2.8	2.2		7.1
"	2-5	12	T	T	D	D	T	T	T	T	T	T
"	1-8	13	T	T	T	T	T	T	T	T	D	D
"	4-5	14			D	D	8.7	7.6	T	T	1.6	3.0
"	4-7	15	T	T	T	T	T	T	D	D	T	T
"	3-8	16	2.0	2.2	2.8	2.6	2.3	2.3	.36	.71	D	D
"	2-7	17	2.0	2.0	1.5	1.3	1.2	1.4	D	D	1.5	1.2
"	3-6	18	T	T	T	T	D	D	T	T	T	T
I.D.	1-7	19	-	T	-	T	-	-	-	D	-	T
"	2-8	20	-	-	-	T	-	-	-	3.2	-	D
"	3-5	21	-	-	-	D	-	T	-	-	-	3.7
"	4-6	22	-	T	-	-	-	D	-	T	-	T
T.V.	5-6	23			D	D	D	D				
T.H.	5-8	24			D	D					D	D
T.V.	7-8	25	T	T	T	T	T	T	D	D	D	D
T.H.	6-7	26	T	T	T	T	D	D	D	D	T	T
T.D.	5-7	27	T		D	D	T	T	D	D		
"	6-8	28			4.0	3.5	D	D	T	T	D	D
Long.	5-9	29	T	T	D	D	T	T	T	T	T	T
"	6-10	30	T	T	T	T	D	D				
"	7-11	31	4.4	4.4	1.8	1.8	1.9	2.2	D	D		8.5
"	8-12	32			T	T	T		2.5	3.1	D	D
O.D.	5-10	33	8.6	7.0	D	D	1.6	2.4	T		6.9	4.9
"	6-9	34	T	T	T	T	D	D	T	T		T
"	5-12	35	T	T	D	D	T	T	T	T	T	T
"	8-9	36	6.0	5.7	3.7	5.6		5.7	2.2	1.9	D	D
"	8-11	37	T	T	T	T	T	T	T	T	D	D
"	7-12	38	1.7	1.9	1.3	1.1	1.2	1.1	D	D	.81	1.2
"	6-11	39	2.3	2.3	3.1	2.6	D	D	.44	.79	2.6	2.1
"	7-10	40	T	T	T	T	T	T	D	D	T	T
I.D.	5-11	41	-	T	-	D	-	5.1	-	T	-	T
"	6-12	42	-	-	-	T	-	D	-	3.0	-	-
"	7-9	43	-	-	-	-	-	T	-	D	-	7.5
"	8-10	44	-	T	-	-	-	T	-	T	-	D

TABLE 11
Compressive Margins of Safety Under 10.0 Due to 130 knot
Flight Load on Middle Vertical Sta with 100% Loading
for Models 2 and 3

DAMAGE MODEL MEMBER	J-J	No.#	None		Joint 13		Joint 14		Joint 15		Joint 16	
			2	3	2	3	2	3	2	3	2	3
Long.	9-13	51	T	T	D	D	T	T	T	T	T	T
"	10-14	52	T	T	T	T	D	D	5.1	7.5	T	T
"	11-15	53	6.2	6.2	3.0	3.0	T	T	D	D	1.5	1.9
"	12-16	54			7.6	8.5	5.6	6.1			D	D
O.D.	9-14	55	7.0	5.6	2.5	3.7	D	D	2.9	2.2	T	8.4
"	10-13	56	T	T	D	D	T	T	T	T	T	T
"	9-16	57	T	T	T	T	T	T	T	T	D	D
"	12-13	58	3.5	3.4	D	D	3.8	3.0	10.	4.7	.62	1.1
"	12-15	59	T	T	T	T	T	T	D	D	T	T
"	11-16	60	1.3	1.5	1.3	1.2	1.3	1.2	.24	.56	D	D
"	10-15	61	2.3	2.3	2.2	1.7	1.2	1.7	D	D	1.2	1.0
"	11-14	62	T	T	T	T	D	D	T	T	T	T
I.D.	9-15	63	-	T	-	T	-	-	-	D	-	T
"	10-16	64	-	-	-	T	-	-	-	3.2	-	D
"	11-13	65	-	-	-	D	-	T	-	-	-	2.9
"	12-14	66	-	T	-	-	-	D	-	T	-	T
T.V.	13-14	67			D	D	D	D				
T.H.	13-16	68			D	D	T	T			D	D
T.V.	15-16	69	T	T	T	T	T	T	D	D	D	D
T.H.	14-15	70	T	T	T	T	D	D	D	D		
T.D.	13-15	71			D	D			D	D	T	T
"	14-16	72					D	D	T	T	D	D
Long.	13-17	73	T	T	D	D	T	T	T	T		
"	14-18	74	T	T	T	T	D	D	T	T	T	T
"	15-19	75	9.8	9.9	4.8	4.9	4.7	5.7	D	D		
"	16-20	76			T	T	5.9	5.8	2.6	3.1	D	D
O.D.	13-18	77	5.4	5.4	D	D	1.7	2.9		7.2	3.2	2.8
"	14-17	78	T	T	T	T	D	D	T	T	T	T
"	13-20	79	T	T	D	D	T	T	T	T	T	T
"	16-17	80	4.0	3.9	2.1	2.9	4.8	3.0	2.2	1.9	D	D
"	16-19	81	T	T	T	T	T	T	T	T	D	D
"	15-20	82	2.3	2.3	2.3	1.8	2.1	1.7	D	D	.87	1.2
"	14-19	83	3.3	3.4	3.3	2.8	D	D	.82	1.3	5.5	4.1
"	15-18	84	T	T	T	T	T	T	D	D	T	T
T.D.	13-19	85	-	-	-	D	-	5.9	-	-	-	T
"	14-20	86	-	-	-	T	-	D	-	4.2	-	
"	15-17	87	-	T	-	T	-	T	-	D	-	7.3
"	16-18	88	-	T	-	-	-	T	-	T	-	D

TABLE 12
Compressive Margins of Safety Under 10.0 Due to 130 knot
Flight Load on End Vertical Sta with 100% Loading for Models 2 and 3

DAMAGE MODEL MEMBER	J-J	No#	None		Joint 21		Joint 22		Joint 23		Joint 24	
			2	3	2	3	2	3	2	3	2	3
Long.	17-21	95	T	T	D	D	T	T	T	T	T	T
"	18-22	96	T	T	T	T	D	D			T	T
"	19-23	97			5.4	5.6	T	T	D	D	3.2	3.7
"	20-24	98			7.8	9.1	6.6	6.8			D	D
O.D.	17-22	99	6.5	6.5	2.6	4.1	D	D	3.6	3.2		9.1
"	18-21	100	T	T	D	D	T	T	T	T	T	T
"	17-24	101	T	T	T	T	T	T	T	T	D	D
"	20-21	102	5.1	4.9	D	D	5.0	4.1	6.5	6.5	1.4	2.0
"	20-23	103	T	T	T	T	T	T	D	D	T	T
"	19-24	104	2.9	2.9	2.9	2.4	3.0	2.4	1.1	1.5	D	D
"	18-23	105	4.2	4.3	4.1	3.1	2.3	3.3	D	D	2.5	2.2
"	19-22	106	T	T	T	T	D	D	T	T	T	T
I.D.	17-23	107	-	-	-	-	-	10.	-	D	-	T
"	18-24	108	-	-	-	T	-	-	-	6.7	-	D
"	19-21	109	-	T	-	D	-	T	-	T	-	6.1
"	20-22	110	-	T	-	9.6	-	D	-	T	-	T
T.V.	21-22	111			D	D	D	D				
T.H.	21-24	112			D	D	T	T			D	D
T.V.	23-24	113	T	T	T	T	T	T	D	D	D	D
T.H.	22-23	114			T	T	D	D	D	D		
T.D.	21-23	115		T	D	D			D	D	T	T
T.D.	22-24	116	T				D	D	T	T	D	D
Long.	21-25	117	T	T	D	D	T	T	T	T		
"	22-26	118	T	T	T	T	D	D	T	T	T	T
"	23-27	119			6.7	7.1	5.6	7.4	D	D		
"	24-28	120			T	T	7.8	7.3	3.4	3.9	D	D
O.D.	21-26	121	7.3	7.2	D	D	2.4	4.0			4.1	3.7
"	22-25	122	T	T	T	T	D	D	T	T	T	T
"	21-28	123	T	T	D	D	T	T	T	T	T	T
"	24-25	124	5.0	4.8	2.9	4.0	6.0	3.7	2.9	2.4	D	D
"	24-27	125	T	T	T	T	T	T	T	T	D	D
"	23-28	126	3.1	3.1	2.9	2.3	2.8	2.3	D	D	1.2	1.6
"	22-27	127	4.2	4.4	4.3	3.7	D	D	1.2	1.9	7.4	5.6
"	23-26	128	T	T	T	T	T	T	D	D	T	T
I.D.	21-27	129	-	-	-	D	-	6.2	-	-	-	T
"	22-28	130	-	T	-	T	-	D	-	6.3	-	-
"	23-25	131	-	-	-	T	-	T	-	D	-	8.0
"	24-26	132	-	T	-	-	-	T	-	T	-	D

TABLE 13

Cases of Models 2 and 3 Where M.S. Less Than 1.0

<u>Case Where Damage is - Joint 7</u>				
Loading	Element #	J-J	Model 2 M.S.	Model 3 M.S.
100%	16	3-8	.36	.71
	39	6-11	.44	.79
75%	16	3-8	.82	1.3
	39	6-11	.94	1.4
<u>Case Where Damage is - Joint 8</u>				
100%	38	7-12	.81	1.2
<u>Case Where Damage is - Joint 15</u>				
100%	60	11-16	.24	.56
	83	14-19	.82	1.3
75%	60	11-16	.66	1.1
<u>Case Where Damage is - Joint 16</u>				
100%	58	12-13	.62	1.1
	82	15-20	.87	1.2

3.3 Natural Frequencies

All structures have resonant frequencies. It is important to know these natural frequencies. To find these frequencies NASTRAN has an eigenvalue method, known as rigid format 3 Normal Modes and Frequencies, for extracting a model's natural frequencies. The first three natural frequencies of each complete structure are found with direction. Table 14 lists the frequencies of each model plus the figure that shows the mode shape.

TABLE 14

NATURAL FREQUENCIES

Model 1		
15.67 Hz	FUNDAMENTAL Y	Figure 16 First Mode Shape
16.63 Hz	FUNDAMENTAL Z	Figure 17 Second Mode Shape
76.41 Hz	1st HARMONIC Y	Figure 18 Third Mode Shape
Model 2		
21.62 Hz	FUNDAMENTAL Y	Figure 19 First Mode Shape
22.92 Hz	FUNDAMENTAL Z	Figure 20 Second Mode Shape
88.44 Hz	1st HARMONIC Y	Figure 21 Third Mode Shape
Model 3		
19.30 Hz	FUNDAMENTAL Y	Figure 22 First Mode Shape
20.48 Hz	FUNDAMENTAL Z	Figure 23 Second Mode Shape
77.70 Hz	1st HARMONIC Y	Figure 24 Third Mode Shape

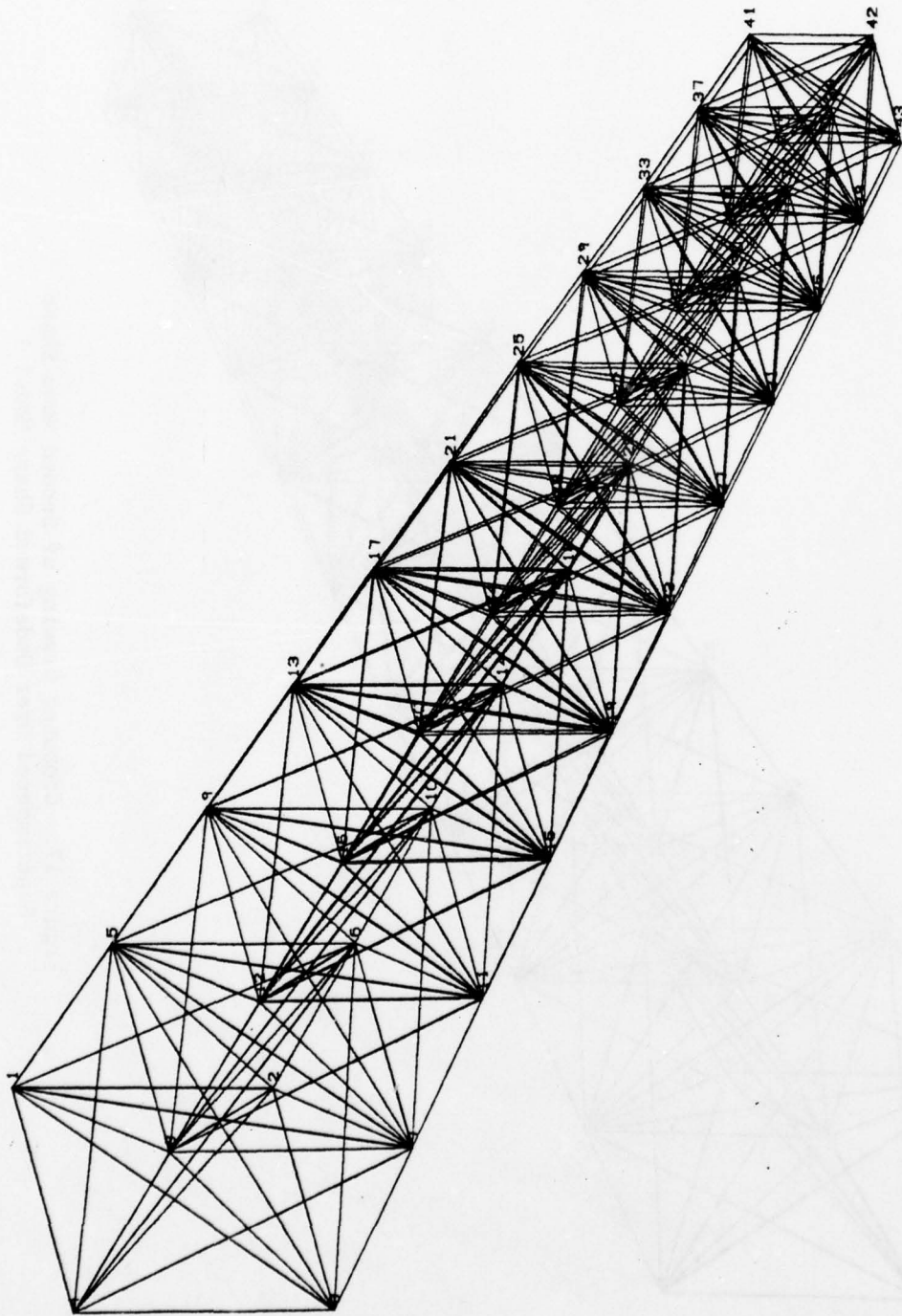


Figure 16. Computer Drawing of First Mode Shape
Superimposed Over Undeformed Shape Model 1

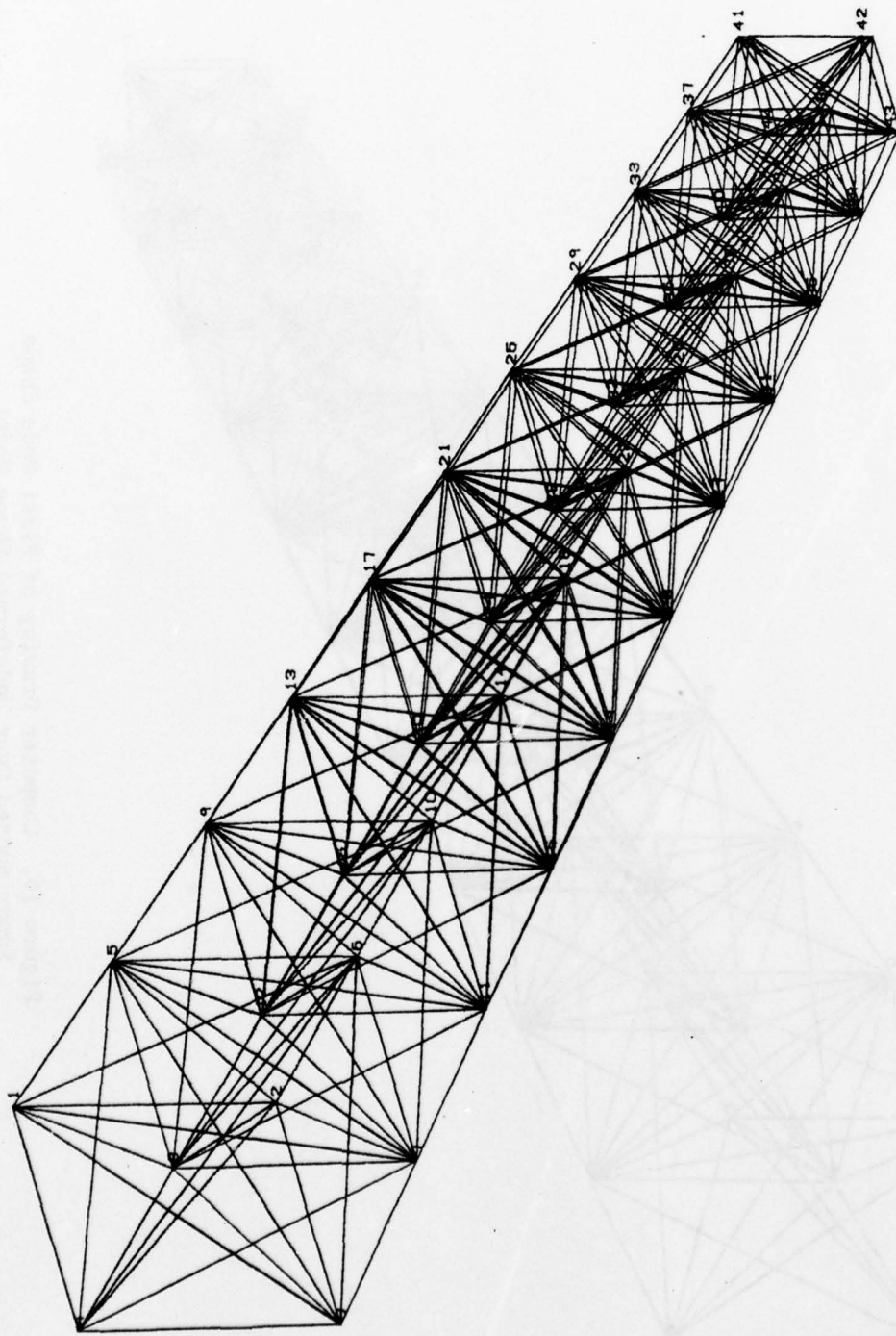


Figure 17. Computer Drawing of Second Mode Shape
Superimposed Over Undeformed Shape Model 1

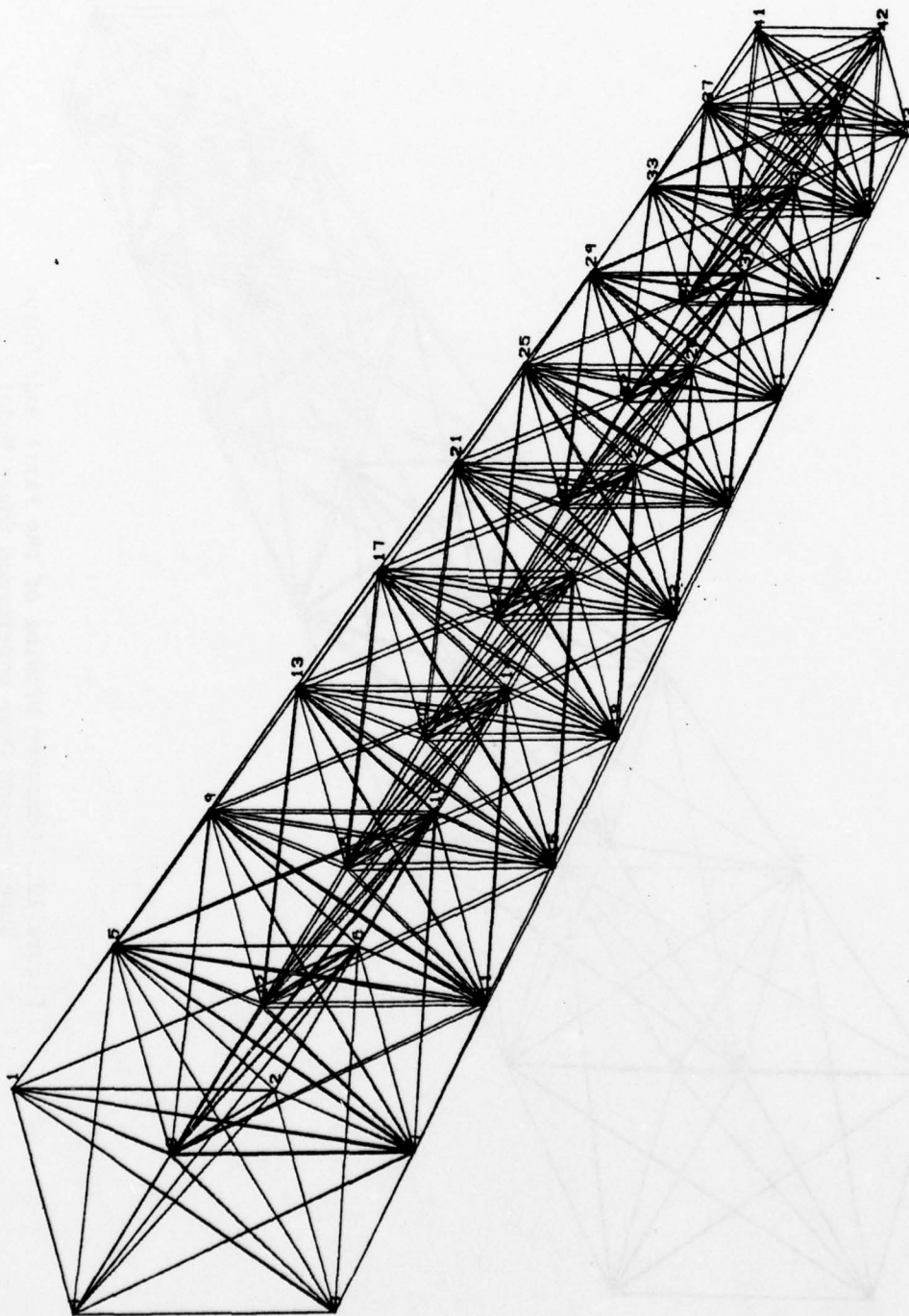


Figure 18. Computer Drawing of Third Mode Shape
Superimposed Over Undeformed Shape Model 1

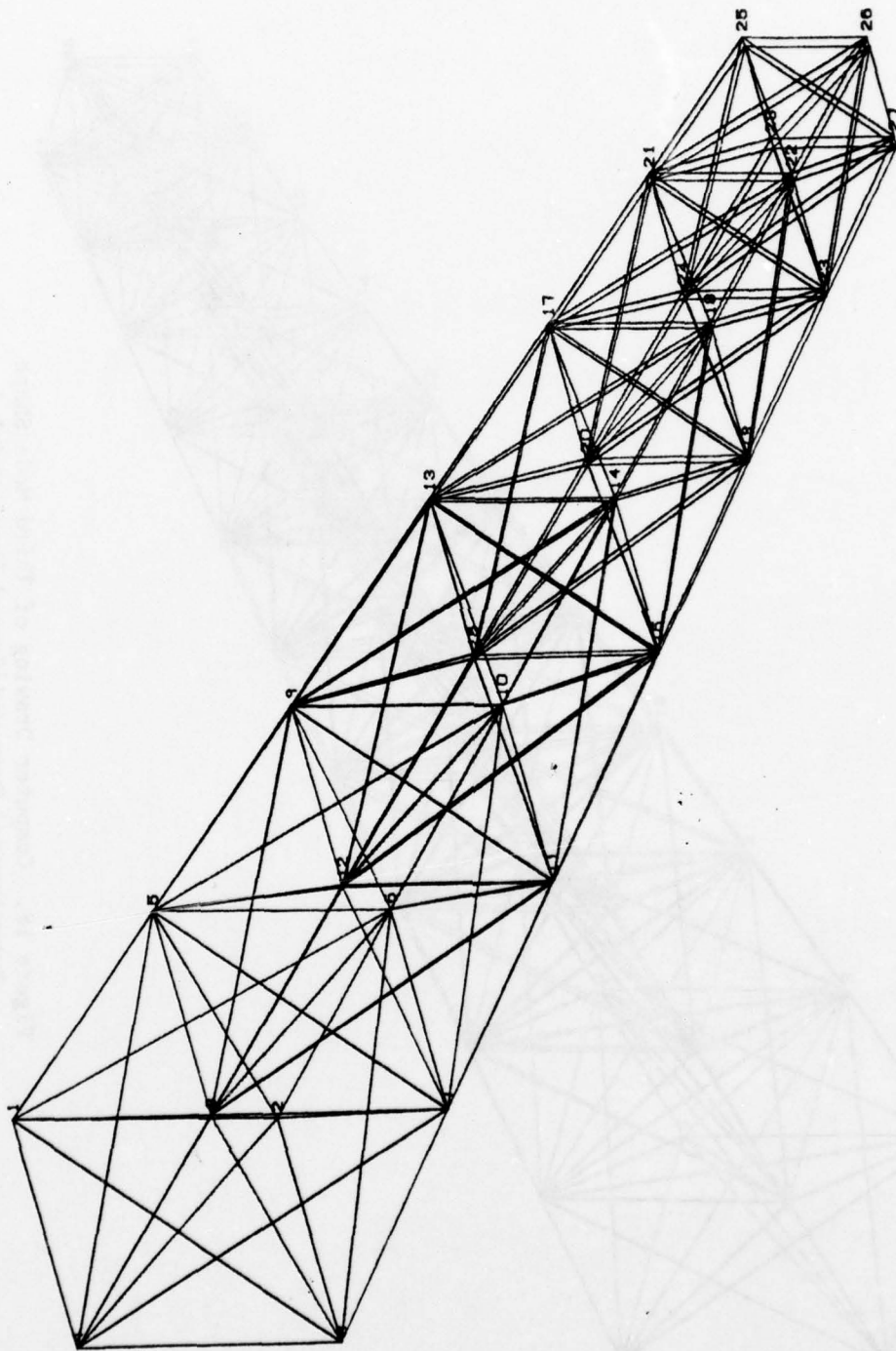


Figure 19. Computer Drawing of the First Mode Shape
Superimposed Over Undeformed Shape Model 2

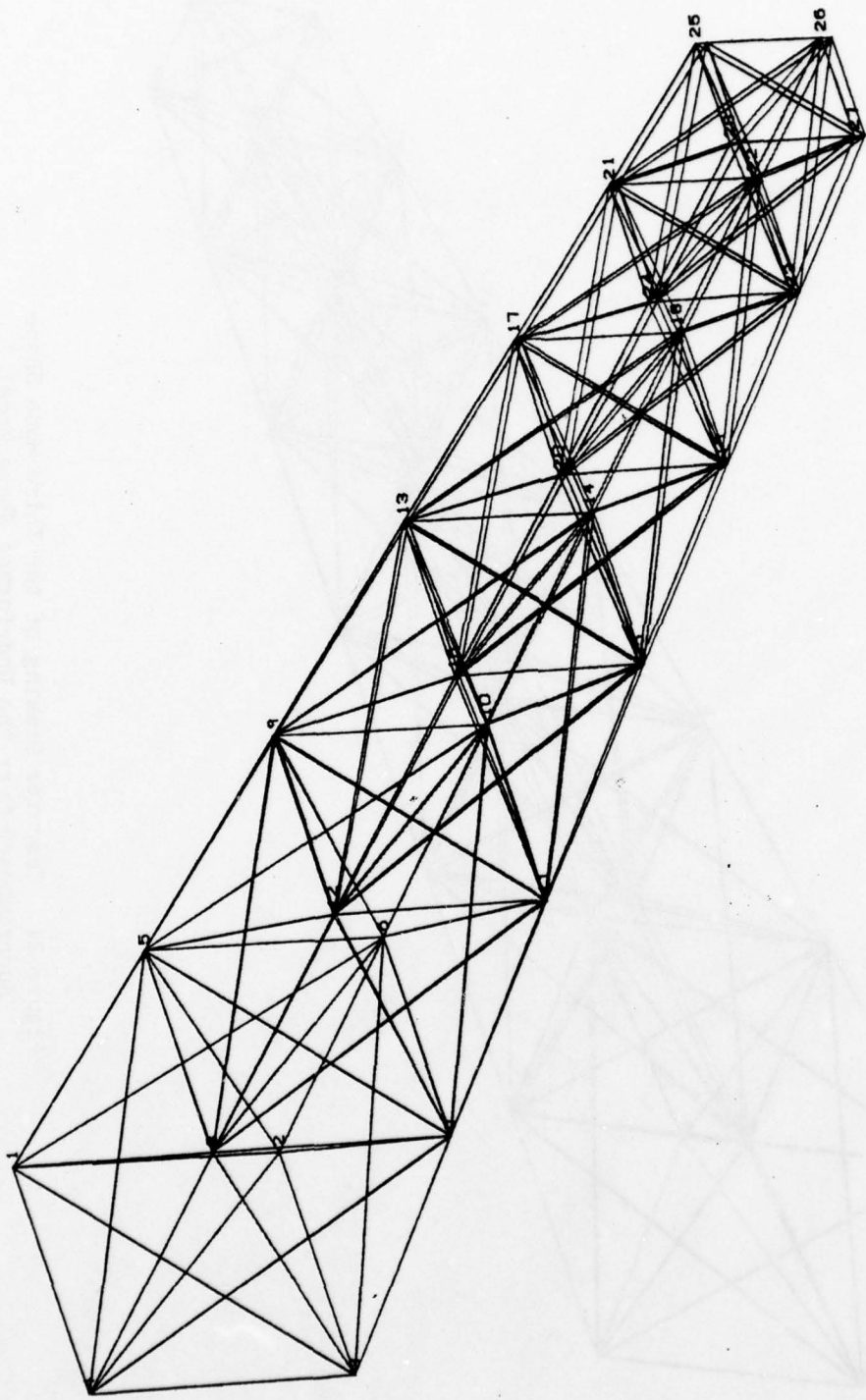


Figure 20. Computer Drawing of Second Mode Shape
Superimposed Over Undeformed Shape Model 2

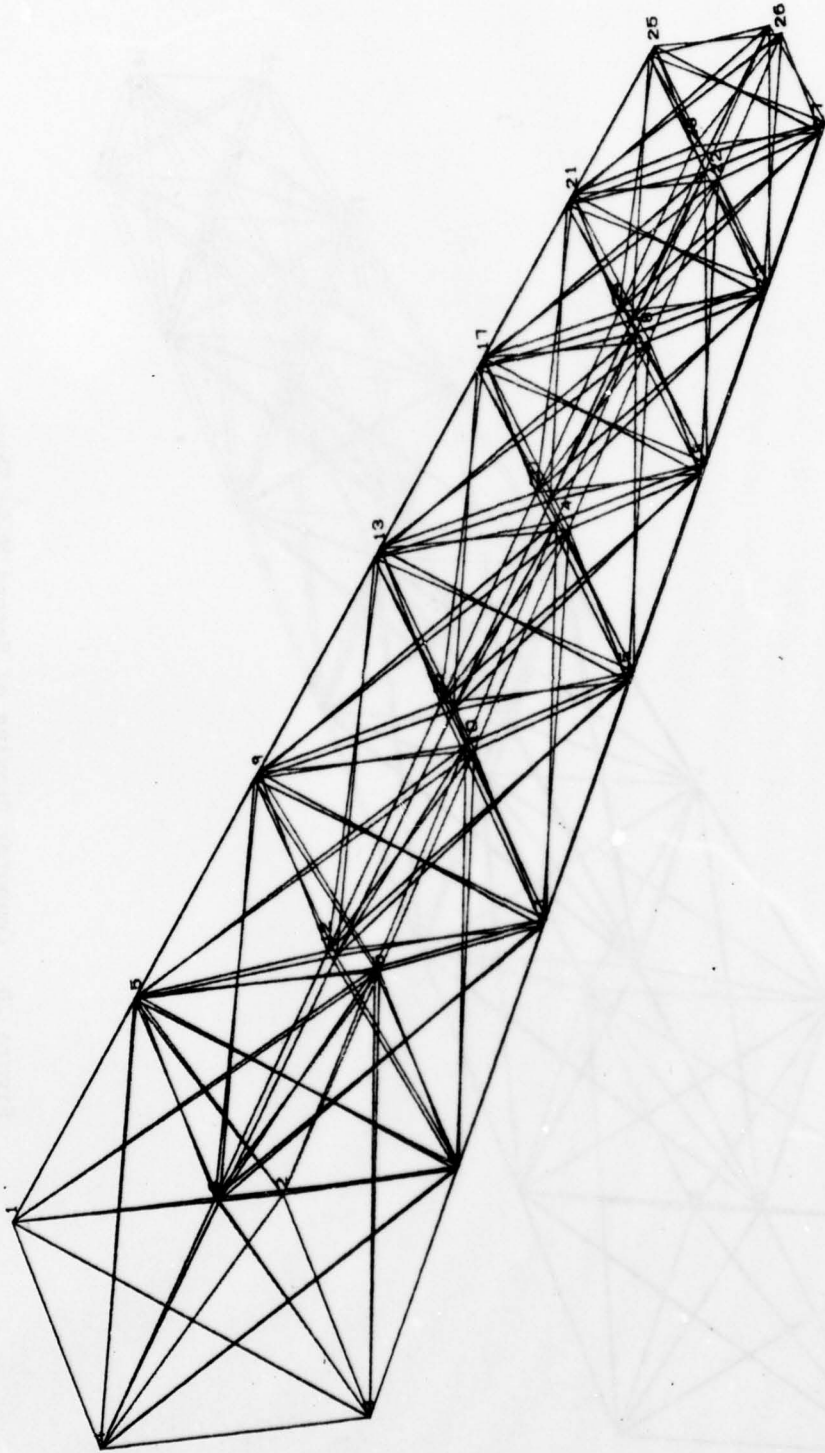


Figure 21. Computer Drawing of the Third Mode Shape
Superimposed Over the Undeformed Shape Model 2

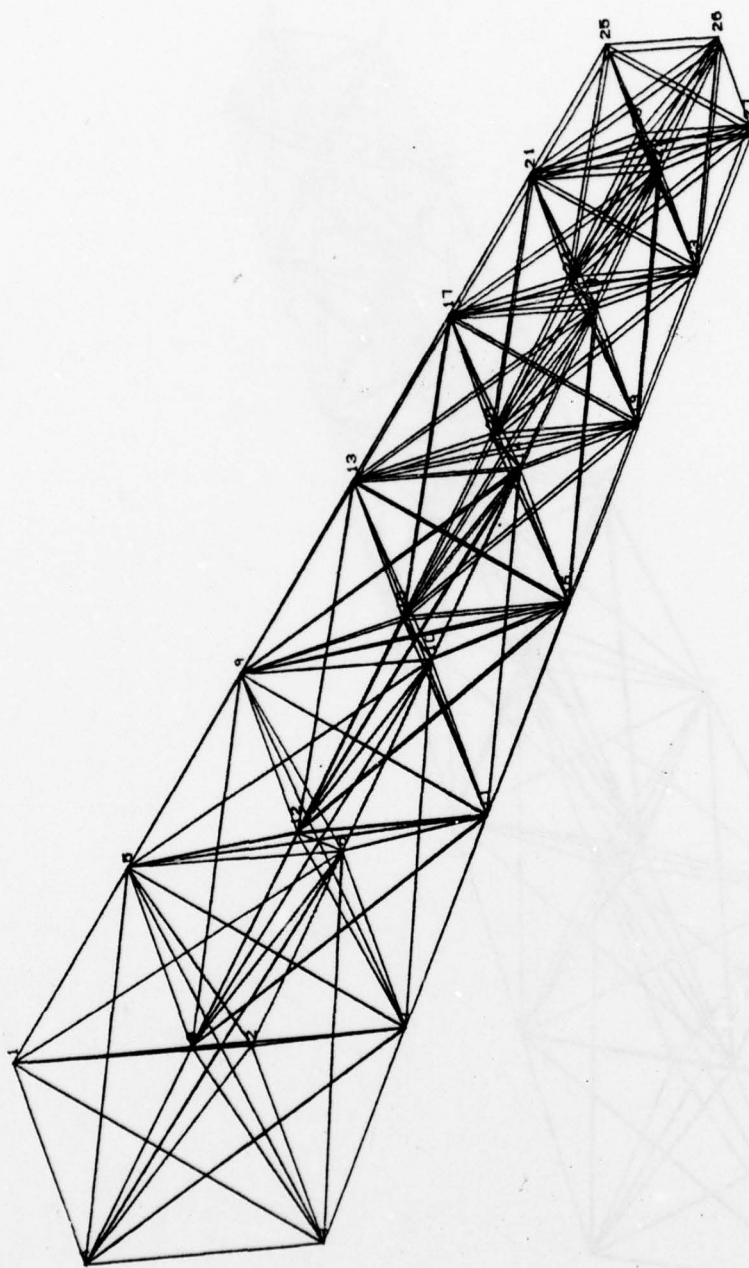


Figure 22. Computer Drawing of the First Mode Shape
Superimposed Over Undeformed Shape Model 3

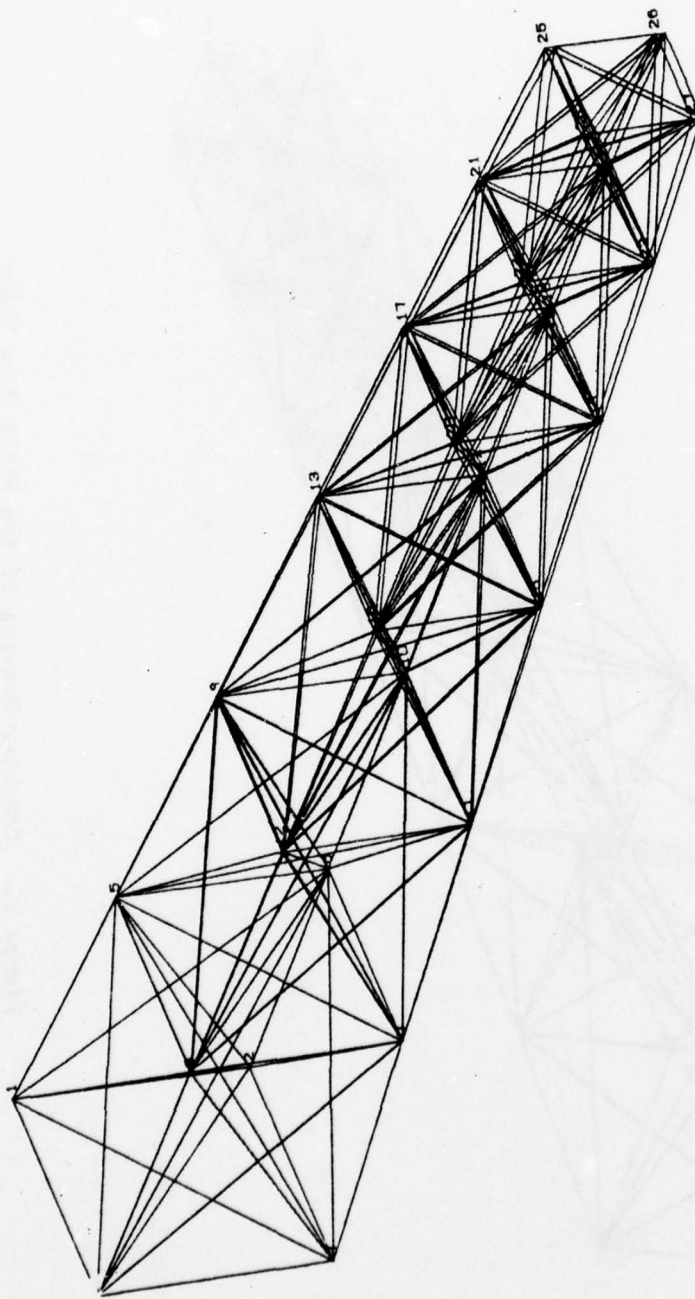


Figure 23. Computer Drawing of Second Mode Shape
Superimposed Over Undeformed Shape Model 3

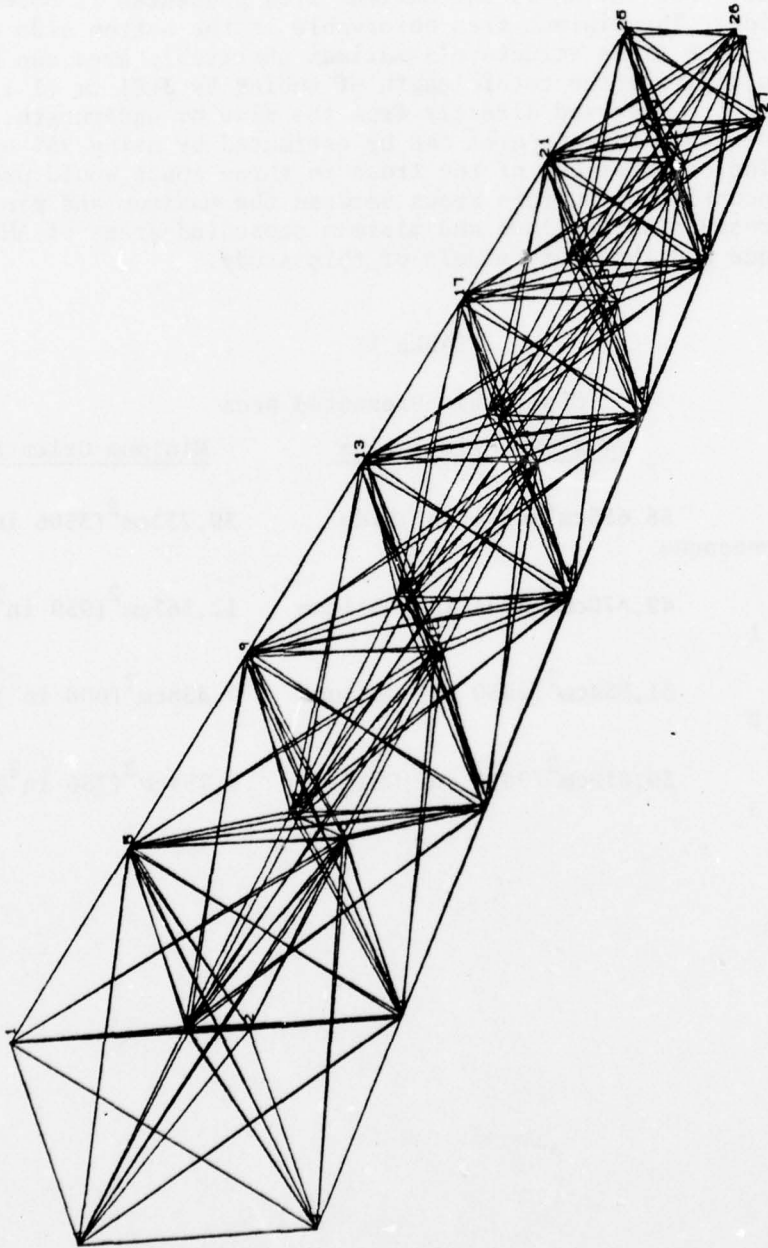


Figure 24. Computer Drawing of the Third Mode Shape
Superimposed Over Undeformed Shape Model 3

3.4 Observable Surface Area

The semimonocoque surface area observed can be considered flat and can be easily calculated by the area of the quadrilateral that presents itself. For the AH-1G the maximum area presented is observed from the side. The minimum area observable is the bottom side directly underneath. The truss structure's maximum observable area can be estimated by multiplying the total length of tubing by 3.81 cm (1 1/2 in). The minimums are observed directly from the side or underneath. The minimum observable surface area can be estimated by using 25% of the maximum. The orientations of the truss in three space would present varying noncontinuous surface areas between the maximum and minimum. Table 15 presents the maximum and minimum presented areas of AH-1G semimonocoque and the truss models of this study.

TABLE 15

	Observable Presented Area	
	<u>Maximum Orientation</u>	<u>Minimum Orientation</u>
AH-1G Semimonocoque	58,655cm ² (4546 in ²)Side	39,233cm ² (3506 in ²)Bottom
Truss Model 1	49,470cm ² (3834 in ²)Oblique	12,367cm ² (959 in ²)Side
Truss Model 2	31,354cm ² (2430 in ²)Oblique	7,838cm ² (608 in ²)Side
Truss Model 3	39,019cm ² (3024 in ²)Oblique	9,754cm ² (756 in ²)Side

IV. DISCUSSION

The complete semimonocoque tail boom structure weighs approximately 90.72 kg (200 lbs), reference 4, and its deflections due to 130 knot level flight load are 1.37 cm (.539 in) in y direction and .37 cm (.146 in) in the z direction, reference 12. As indicated in Table 3, the maximum displacements for each maximum loading case of the truss models show only a slight difference between the models. Comparing the complete truss models with the complete semimonocoque structure shows the stiffness of the truss models to be 12% greater in the y direction, and 46% less in the z direction. Considering the weight difference between the truss models and the semimonocoque structure, the stiffness of the truss models is reasonably competitive. Table 3 shows that the maximum increase in displacement for the y direction is .82 cm which occurs for unstructured model 2 when joint 5 is deleted. Table 3 also shows the maximum increase in z direction displacement to be .803 cm more than the undamaged case occurring when joint 7 is deleted in model 2. Damage criteria imposed on the models show model 2 to be the least stiff of the three models.

The displacement results of the three truss models show a truss design to be particularly stiff even when damage conditions are imposed. The "simple" open truss of model 2 shows itself to be light and strong in the undamaged condition. Model 3 with inclusion of interior structural diagonals is more massive, and more stiff than model 2. Model 1 is obviously very dense and stiffer than either model 2 or model 3. Table 14 reveals the stiffness of the undamaged three models. The lower the fundamental frequencies the closer the model approximates a stiff bar.

The goal of retaining structural integrity after imposition of a massive damage criterion is conceptually assured by the incorporation of complete substructures. The "simple" open truss exhibits the response of a geometrical instability when a joint is deleted. The weight optimizing program does not find supporting structure to transfer the loads that were carried by the missing members of the deleted joint. With the substructure models there is additional structural support for transfer of the load that the missing members carried. The interior diagonals carry bigger loads and redistribute the load path to the remaining structure. The distribution of loads into the interior diagonals raises the confidence of stability of the structure. The structural integrity can be assured in the design stage.

¹²D. A. Reisdorfer, Tail Boom Vulnerability Reduction Test Program, Report No. 699-099-004, August 1975, Bell Helicopter Company, Fort Worth, Texas 76101.

Application of the flight loads to damage simulated models results in margins of safety that indicate no failure of individual elements. Our assumption of an inherently strong truss structure simulated by model 1 is borne out by Tables 7, 8, and 9 which show not a single margin of safety (M.S.) under 1.0 for model 1 and very few M.S. under 10.0. Since models 2 and 3 are similar except that model 3 is substructured, a direct comparison is made. Note in Tables 10, 11, and 12 the substructured model 3 consistently has the interior diagonals taking on tensile and compressive loads. This shows that the interior diagonals are working. Tables 10, 11, and 12 also indicate how the interior diagonals are redistributing the load path and how much of the load they share. Though no members of model 2 or model 3 failed, Table 13 shows that model 2 has four cases where the M.S. falls under 1.0 and model 3 has 2 cases. To show bending a complete longeron diagonally opposite the damage criteria is chosen. The amount of bending is compared by a ratio of the damage displacements to the displacement of the undamaged model in Tables 6, 7, and 8. From Tables 6, 7, and 8 noted is the response of a large amount of displacement to all models where the loss of joint 5 is encountered, yet from the stress analysis of this damage criterion all the models have M.S. greater than 1.0.

Table 15 shows the maximum and minimum presented areas and orientations. The semimonocoque presents a continuous surface whereas the truss models present noncontinuous surface area. For the maximum, model 1 shows a 16% reduction, model 2 shows a 47% reduction, and model 3 shows a 33% reduction in presented area compared to the semimonocoque. Comparison of the minimum present areas shows model 1 with a 69% reduction, model 2 with a 80% reduction, and model 3 with a 75% reduction. These reductions show a clear reduction in visibility of the truss tail boom relative to the semimonocoque type tail boom.

V. CONCLUSIONS

This study presents two ideas for alternative construction of Army helicopter tail booms. The idea of truss structures for tail booms is not new but conceptualizing a high degree of redundancy for greater damage tolerance is preferable for design of combat aircraft. The idea of imbedded substructures is specifically included for increased confidence in the capability to absorb damage and yet retain structural integrity.

The truss type tail boom models of this study provide a reduction in weight over the present semimonocoque tail boom structure of the AH-1G. The truss models are reasonably stiff structures compared to the semimonocoque structure.

Analyses of the highly redundant truss models under the aerodynamic loads of flight and with imposition of a massive damage

criterion show:

- o Substantial retention of stiffness
- o Change of load path that is localized to the neighborhood of damage
- o No failure of elements due to tension or compression
- o Retention of structural integrity

The substructured truss models have more supporting structural elements to redistribute the load and consistently have margins of safety higher than the non-substructured truss model. The substructuring concept has vulnerability reduction built-in. The substructure concept assures a higher degree of confidence in the truss concept to retain structural integrity after imposition of the loss of a joint. The substructured truss models have at least a 16% reduction in presented area compared to the semimonocoque structure. The highly redundant substructured truss type tail boom is a highly survivable structure.

ACKNOWLEDGEMENT

I wish to gratefully acknowledge Dr. Donald F. Haskell for initiating the idea of a truss structure for helicopter tail booms and for his continuing confidence shown and demonstrated in my carrying on the analysis.

A note of appreciation is also extended to Dr. V. B. Venkayya and Dr. Harry S. Schaeffer for my recent instruction in use and understanding of the complex NASTRAN program.

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APPENDIX A

NASTRAN MATHEMATICAL MODEL OF THE UNDATED
TRUSS MODEL 1 PLUS OUTPUT OF DISPLACEMENTS, STRESSES
AND MARGINS OF SAFETY DUE TO FLIGHT LOADS.

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NASTRAN EXECUTIVE CONTROL DECK ECHO

ID ERLINE,MODEL1
APP DISP
\$ STATIC ANALYSIS WITH DIFFERENTIAL STIFFNESS RF 4
SOL 4.0
TIME 10
CEMU

TRUSS TAIL BOOM MODEL1 **A 226 ELEMENT VERSION
DAMAGE CRITERION = NONE

CASE CONTROL DECK ECHO

CARD
COUNT

1 TITLE = TRUSS TAIL BOOM MODEL1 **A 226 ELEMENT VERSION
2 SUBTITLE = DAMAGE CRITERION = NONE
3 CLOAD = ALL
4 SPC = 10
5 DISP = ALL
6 SPFORCES = ALL
7 SET 5 = 1 THRU 226
8 SUBCASE 1
9 LABEL = LINEAR CASE
10 LOAD = 11
11 SUBCASE 2
12 LABEL = INCREMENTAL STIFFNESS
13 DSCOEFFICIENT = 200
14 STRESS = 5
15 \$ METHOD = 15
16 MAXLINES = 10000
17 BEGIN BULK

*** USE INFORMATION MESSAGE 207, BULK DATA NOT SORTED, XSORT WILL RE-ORDER DECK.

CARD COUNT	1	2	3	4	5	6	7	8	9	10	SORTED BULK DATA ECHO
1-	1	1	1	2	..	4	..	2	..	10	.
2-	2	2	1	4	..	4	..	4
3-	3	3	3	4	..	4	..	4
4-	4	4	2	3	..	3	..	3
5-	5	5	1	3	..	3	..	3
6-	6	6	2	4	..	4	..	4
7-	7	7	1	5	..	5	..	5
8-	8	8	2	6	..	6	..	6
9-	9	9	3	7	..	7	..	7
10-	10	10	4	8	..	8	..	8
11-	11	11	1	6	..	6	..	6
12-	12	12	2	5	..	5	..	5
13-	13	13	1	8	..	8	..	8
14-	14	14	4	5	..	5	..	5
15-	15	15	4	7	..	7	..	7
16-	16	16	3	8	..	8	..	8
17-	17	17	2	7	..	7	..	7
18-	18	18	3	6	..	6	..	6
19-	19	19	1	7	..	7	..	7
20-	20	20	2	8	..	8	..	8
21-	21	21	3	5	..	5	..	5
22-	22	22	4	6	..	6	..	6
23-	23	23	5	6	..	6	..	6
24-	24	24	5	8	..	8	..	8
25-	25	25	7	7	..	7	..	7
26-	26	26	6	7	..	7	..	7
27-	27	27	5	7	..	7	..	7
28-	28	28	6	8	..	8	..	8
29-	29	29	5	9	..	9	..	9
30-	30	30	6	10	..	10	..	10
31-	31	31	7	11	..	11	..	11
32-	32	32	8	12	..	12	..	12
33-	33	33	5	10	..	10	..	10
34-	34	34	6	9	..	9	..	9
35-	35	35	5	12	..	12	..	12
36-	36	36	8	9	..	9	..	9
37-	37	37	6	11	..	11	..	11
38-	38	38	7	12	..	12	..	12
39-	39	39	6	11	..	11	..	11
40-	40	40	7	10	..	10	..	10
41-	41	41	5	11	..	11	..	11
42-	42	42	6	12	..	12	..	12
43-	43	43	7	9	..	9	..	9
44-	44	44	8	10	..	10	..	10
45-	45	45	9	10	..	10	..	10

SORTED BULK DATA ECHO

CARU COUNT	1	2	3	4	5	6	7	8	9	10
46-	CTUBE 46	46	9	12						
47-	CTUBE 47	47	11	12						
48-	CTUBE 48	48	10	11						
49-	CTUBE 49	49	9	11						
50-	CTUBE 50	50	10	12						
51-	CTUBE 51	51	9	13						
52-	CTUBE 52	52	10	14						
53-	CTUBE 53	53	11	15						
54-	CTUBE 54	54	12	16						
55-	CTUBE 55	55	9	14						
56-	CTUBE 56	56	10	13						
57-	CTUBE 57	57	9	16						
58-	CTUBE 58	58	12	13						
59-	CTUBE 59	59	12	15						
60-	CTUBE 60	60	11	16						
61-	CTUBE 61	61	10	15						
62-	CTUBE 62	62	11	14						
63-	CTUBE 63	63	9	15						
64-	CTUBE 64	64	10	16						
65-	CTUBE 65	65	11	13						
66-	CTUBE 66	66	12	14						
67-	CTUBE 67	67	13	14						
68-	CTUBE 68	68	13	16						
69-	CTUBE 69	69	15	16						
70-	CTUBE 70	70	14	15						
71-	CTUBE 71	71	13	15						
72-	CTUBE 72	72	14	16						
73-	CTUBE 73	73	13	17						
74-	CTUBE 74	74	14	18						
75-	CTUBE 75	75	15	19						
76-	CTUBE 76	76	16	20						
77-	CTUBE 77	77	13	18						
78-	CTUBE 78	78	14	17						
79-	CTUBE 79	79	13	20						
80-	CTUBE 80	80	16	17						
81-	CTUBE 81	81	16	19						
82-	CTUBE 82	82	15	20						
83-	CTUBE 83	83	14	19						
84-	CTUBE 84	84	15	18						
85-	CTUBE 85	85	13	19						
86-	CTUBE 86	86	14	20						
87-	CTUBE 87	87	15	17						
88-	CTUBE 88	88	16	18						
89-	CTUBE 89	89	17	18						
90-	CTUBE 90	90	17	20						

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
91-	CTUSE	91	91	19	20						
92-	CTUSE	92	92	18	19						
93-	CTOFL	93	93	17	19						
94-	CTOBE	94	94	18	20						
95-	CTOBE	95	95	17	21						
96-	CTOBE	96	96	18	22						
97-	CTOBE	97	97	19	23						
98-	CTOBE	98	98	20	24						
99-	CTOBE	99	99	17	22						
100-	CTOBE	100	100	18	21						
101-	CTOBE	101	101	17	24						
102-	CTOBE	102	102	20	21						
103-	CTOBE	103	103	20	23						
104-	CTOBE	104	104	19	24						
105-	CTOBE	105	105	18	23						
106-	CTOBE	106	106	19	22						
107-	CTOBE	107	107	17	23						
108-	CTOBE	108	108	18	24						
109-	CTOBE	109	109	19	21						
110-	CTOBE	110	110	20	22						
111-	CTOBE	111	111	21	22						
112-	CTOBE	112	112	21	24						
113-	CTOBE	113	113	23	24						
114-	CTOBE	114	114	22	23						
115-	CTOBE	115	115	21	23						
116-	CTOBE	116	116	22	24						
117-	CTOBE	117	117	21	25						
118-	CTOBE	118	118	22	26						
119-	CTOBE	119	119	23	27						
120-	CTOBE	120	120	24	28						
121-	CTOBE	121	121	21	26						
122-	CTOBE	122	122	22	25						
123-	CTOBE	123	123	21	24						
124-	CTOBE	124	124	24	25						
125-	CTOBE	125	125	24	27						
126-	CTOBE	126	126	23	28						
127-	CTOBE	127	127	22	27						
128-	CTOBE	128	128	23	26						
129-	CTOBE	129	129	21	27						
130-	CTOBE	130	130	22	28						
131-	CTOBE	131	131	23	25						
132-	CTOBE	132	132	24	26						
133-	CTOBE	133	133	25	26						
134-	CTOBE	134	134	25	29						
135-	CTOBE	135	135	27	28						

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
136-	CTUBE	136	136	136	26	27					
137-	CTUBE	137	137	137	25	27					
138-	CTUBE	138	138	138	26	28					
139-	CTUBE	139	139	139	25	29					
140-	CTUBE	140	140	140	26	30					
141-	CTUBE	141	141	141	27	31					
142-	CTUBE	142	142	142	28	32					
143-	CTUBE	143	143	143	25	30					
144-	CTUBE	144	144	144	26	29					
145-	CTUBE	145	145	145	25	32					
146-	CTUBE	146	146	146	28	29					
147-	CTUBE	147	147	147	28	31					
148-	CTUBE	148	148	148	27	32					
149-	CTUBE	149	149	149	26	31					
150-	CTUBE	150	150	150	27	30					
151-	CTUBE	151	151	151	25	31					
152-	CTUBE	152	152	152	26	32					
153-	CTUBE	153	153	153	27	29					
154-	CTUBE	154	154	154	28	30					
155-	CTUBE	155	155	155	29	30					
156-	CTUBE	156	156	156	29	32					
157-	CTUBE	157	157	157	31	32					
158-	CTUBE	158	158	158	30	31					
159-	CTUBE	159	159	159	29	31					
160-	CTUBE	160	160	160	30	32					
161-	CTUBE	161	161	161	29	33					
162-	CTUBE	162	162	162	30	34					
163-	CTUBE	163	163	163	31	35					
164-	CTUBE	164	164	164	32	36					
165-	CTUBE	165	165	165	29	34					
166-	CTUBE	166	166	166	30	33					
167-	CTUBE	167	167	167	29	36					
168-	CTUBE	168	168	168	32	33					
169-	CTUBE	169	169	169	32	35					
170-	CTUBE	170	170	170	31	36					
171-	CTUBE	171	171	171	30	35					
172-	CTUBE	172	172	172	31	34					
173-	CTUBE	173	173	173	29	35					
174-	CTUBE	174	174	174	30	36					
175-	CTUBE	175	175	175	31	33					
176-	CTUBE	176	176	176	32	34					
177-	CTUBE	177	177	177	33	34					
178-	CTUBE	178	178	178	33	36					
179-	CTUBE	179	179	179	35	36					
180-	CTUBE	180	180	180	34	35					

SORTED BULK DATA ECHO

CARD	1	2	3	4	5	6	7	8	9	10
181-	CTUBE	181	161	33	35					
182-	CTUBE	182	162	34	36					
183-	CTUBE	183	163	33	37					
184-	CTUBE	184	184	34	38					
185-	CTUBE	185	185	35	39					
186-	CTUBE	186	186	36	40					
187-	CTUBE	187	187	33	38					
188-	CTUBE	188	188	34	37					
189-	CTUBE	189	189	33	40					
190-	CTUBE	190	190	36	37					
191-	CTUBE	191	191	36	39					
192-	CTUBE	192	192	35	40					
193-	CTUBE	193	193	34	39					
194-	CTUBE	194	194	35	38					
195-	CTUBE	195	195	33	39					
196-	CTUBE	196	196	34	40					
197-	CTUBE	197	197	35	37					
198-	CTUBE	198	198	36	38					
199-	CTUBE	199	199	37	38					
200-	CTUBE	200	200	37	40					
201-	CTUBE	201	201	39	40					
202-	CTUBE	202	202	38	39					
203-	CTUBE	203	203	37	39					
204-	CTUBE	204	204	38	40					
205-	CTUBE	205	205	37	41					
206-	CTUBE	206	206	38	42					
207-	CTUBE	207	207	39	43					
208-	CTUBE	208	208	40	44					
209-	CTUBE	209	209	37	42					
210-	CTUBE	210	210	38	41					
211-	CTUBE	211	211	37	44					
212-	CTUBE	212	212	40	41					
213-	CTUBE	213	213	40	43					
214-	CTUBE	214	214	39	44					
215-	CTUBE	215	215	38	43					
216-	CTUBE	216	216	39	42					
217-	CTUBE	217	217	37	43					
218-	CTUBE	218	218	38	44					
219-	CTUBE	219	219	39	41					
220-	CTUBE	220	220	40	42					
221-	CTUBE	221	221	41	42					
222-	CTUBE	222	222	41	44					
223-	CTUBE	223	223	43	44					
224-	CTUBE	224	224	42	43					
225-	CTUBE	225	225	41	43					

SORTED BULK DATA ECHO

CARD COUNT	1	2	3	4	5	6	7	8	9	10
226-	CTUBE	226	226	42	44					
227-	USFACT	200	1.60422	2.40632	3.20843					
228-	FORCE	11	21	0	44.2200	0	0.0	-1.		
229-	FORCE	11	22	0	44.2200	0	0.0	-1.		
230-	FORCE	11	23	0	44.2200	0	0.0	-1.		
231-	FORCE	11	24	0	44.2200	0	0.0	-1.		
232-	FORCE	11	41	0	464.5	1.	0.0	0.0		
233-	FORCE	11	41	0	527.3	0	-1.0	0.0		
234-	FORCE	11	42	0	464.5	1.0	0.0	0.0		
235-	FORCE	11	42	0	527.3	0	1.	0.0		
236-	FORCE	11	43	0	464.5	-1.	0.0	0.0		
237-	FORCE	11	43	0	527.5	0	1.	0.0		
238-	FORCE	11	44	0	464.5	-1.	0.0	0.0		
239-	FORCE	11	44	0	527.3	0	-1.	0.0		
240-	GRUSET									456
241-	GRID	1	.000	12.300	13.300					
242-	GRID	2	.000	12.100	-11.500					
243-	GRID	3	.000	-11.400	-11.500					
244-	GRID	4	.000	-11.600	13.300					
245-	GRID	5	23.700	11.300	12.300					
246-	GRID	6	23.900	11.100	-10.700					
247-	GRID	7	23.900	-10.600	-10.700					
248-	GRID	8	23.750	-10.800	12.300					
249-	GRID	9	45.950	10.400	11.300					
250-	GRID	10	45.950	10.200	-9.900					
251-	GRID	11	45.950	-9.800	-9.900					
252-	GRID	12	45.950	-10.000	11.300					
253-	GRID	13	66.400	9.500	10.500					
254-	GRID	14	66.500	9.300	-9.200					
255-	GRID	15	66.500	-9.100	-9.200					
256-	GRID	16	66.400	-9.300	10.500					
257-	GRID	17	85.400	8.800	9.700					
258-	GRID	18	85.400	8.600	-8.600					
259-	GRID	19	85.400	-8.400	-8.600					
260-	GRID	20	85.400	-8.600	9.700					
261-	GRID	21	103.000	8.000	8.900					
262-	GRID	22	103.000	7.900	-8.900					
263-	GRID	23	103.000	-7.800	-8.000					
264-	GRID	24	103.000	-8.000	8.900					
265-	GRID	25	119.300	7.400	8.200					
266-	GRID	26	119.300	7.200	-7.400					
267-	GRID	27	119.300	-7.300	-7.400					
268-	GRID	28	119.300	-7.500	8.200					
269-	GRID	29	134.400	6.700	7.400					
270-	GRID	30	134.400	6.600	-6.700					

S O R T E D B U L K D A T A E C H O

CARD	1	2	3	4	5	6	7	8	9	10
271-	GRID 31	134.500	-6.800	-6.900						
272-	GRID 32	134.400	-6.900	7.600						
273-	GRID 33	148.500	6.100	7.000						
274-	GRID 34	148.500	6.000	-6.500						
275-	GRID 35	148.500	-6.300	-6.500						
276-	GRID 36	148.500	-6.400	7.000						
277-	GRID 37	161.400	5.600	6.500						
278-	GRID 38	161.500	5.500	-6.000						
279-	GRID 39	161.500	-5.800	-6.000						
280-	GRID 40	161.400	-6.000	6.500						
281-	GRID 41	173.500	5.100	6.000						
282-	GRID 42	173.500	5.000	-5.600						
283-	GRID 43	173.500	-5.400	-5.600						
284-	GRID 44	173.500	-5.500	6.000						
285-	MAT1 1	10.5E6	.33	.1						+MAT001
286-	+MAT001	4.36+04	3.49+04							
287-	MAT1 2	10.5E6	3.8E6	.33	.1					+MAT002
288-	+MAT002	4.70+04	3.76+04							
289-	MAT1 3	10.5E6	3.8E6	.33	.1					+MAT003
290-	+MAT003	4.36+04	3.49+04							
291-	MAT1 4	10.5E6	3.8E6	.33	.1					+MAT004
292-	+MAT004	4.86+04	3.89+04							
293-	MAT1 5	10.5E6	3.8E6	.33	.1					+MAT005
294-	+MAT005	2.28+04	1.83+04							
295-	MAT1 6	10.5E6	3.8E6	.33	.1					+MAT006
296-	+MAT006	2.28+04	1.83+04							
297-	MAT1 7	10.5E6	3.8E6	.33	.1					+MAT007
298-	+MAT007	4.76+04	3.81+04							
299-	MAT1 8	10.5E6	3.8E6	.33	.1					+MAT008
300-	+MAT008	4.69+04	3.75+04							
301-	MAT1 9	10.5E6	3.8E6	.33	.1					+MAT009
302-	+MAT009	4.69+04	3.75+04							
303-	MAT1 10	10.5E6	3.8E6	.33	.1					+MAT010
304-	+MAT010	4.75+04	3.80+04							
305-	MAT1 11	10.5E6	3.8E6	.33	.1					+MAT011
306-	+MAT011	2.34+04	1.87+04							
307-	MAT1 12	10.5E6	3.8E6	.33	.1					+MAT012
308-	+MAT012	2.38+04	1.90+04							
309-	MAT1 13	10.5E6	3.8E6	.33	.1					+MAT013
310-	+MAT013	2.44+04	1.95+04							
311-	MAT1 14	10.5E6	3.8E6	.33	.1					+MAT014
312-	+MAT014	2.47+04	1.98+04							
313-	MAT1 15	10.5E6	3.8E6	.33	.1					+MAT015
314-	+MAT015	2.34+04	1.87+04							
315-	MAT1 16	10.5E6	3.8E6	.33	.1					+MAT016

TRUSS TAIL BOOM MODEL1 **A 226 ELEMENT VERSION
DAMAGE CRITERION = NONE

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
316-		+MAT016	2.37+04	1.90+04							
317-		MAT1	17	10.5E6	3.8E6	.33	.1				+MAT017
318-		+MAT017	2.47+04	1.98+04							
319-		MAT1	18	10.5E6	3.8E6	.33	.1				+MAT018
320-		+MAT018	2.49+04	1.99+04							
321-		MAT1	19	10.5E6	3.8E6	.33	.1				+MAT019
322-		+MAT019	1.61+04	1.28+04							
323-		MAT1	20	10.5E6	3.8E6	.33	.1				+MAT020
324-		+MAT020	1.62+04	1.30+04							
325-		MAT1	21	10.5E6	3.8E6	.33	.1				+MAT021
326-		+MAT021	1.63+04	1.31+04							
327-		MAT1	22	10.5E6	3.8E6	.33	.1				+MAT022
328-		+MAT022	1.61+04	1.29+04							
329-		MAT1	23	10.5E6	3.8E6	.33	.1				+MAT023
330-		+MAT023	5.07+04	4.06+04							
331-		MAT1	24	10.5E6	3.8E6	.33	.1				+MAT024
332-		+MAT024	5.30+04	4.40+04							
333-		MAT1	25	10.5E6	3.8E6	.33	.1				+MAT025
334-		+MAT025	5.07+04	4.06+04							
335-		MAT1	26	10.5E6	3.8E6	.33	.1				+MAT026
336-		+MAT026	5.70+04	4.56+04							
337-		MAT1	27	10.5E6	3.8E6	.33	.1				+MAT027
338-		+MAT027	2.66+04	2.13+04							
339-		MAT1	28	10.5E6	3.8E6	.33	.1				+MAT028
340-		+MAT028	2.66+04	2.13+04							
341-		MAT1	29	10.5E6	3.8E6	.33	.1				+MAT029
342-		+MAT029	5.40+04	4.32+04							
343-		MAT1	30	10.5E6	3.8E6	.33	.1				+MAT030
344-		+MAT030	5.21+04	4.0+04							
345-		MAT1	31	10.5E6	3.8E6	.33	.1				+MAT031
346-		+MAT031	5.51+04	4.40+04							
347-		MAT1	32	10.5E6	3.8E6	.33	.1				+MAT032
348-		+MAT032	5.43+04	4.34+04							
349-		MAT1	33	10.5E6	3.8E6	.33	.1				+MAT033
350-		+MAT033	2.71+04	2.17+04							
351-		MAT1	34	10.5E6	3.8E6	.33	.1				+MAT034
352-		+MAT034	2.76+04	2.21+04							
353-		MAT1	35	10.5E6	3.8E6	.33	.1				+MAT035
354-		+MAT035	2.63+04	2.25+04							
355-		MAT1	36	10.5E6	3.8E6	.33	.1				+MAT036
356-		+MAT036	2.85+04	2.28+04							
357-		MAT1	37	10.5E6	3.8E6	.33	.1				+MAT037
358-		+MAT037	2.72+04	2.18+04							
359-		MAT1	38	10.5E6	3.8E6	.33	.1				+MAT038
360-		+MAT038	2.77+04	2.21+04							

S O R T E D B U L K D A T A E C H O

CARD COUNT	1	2	3	4	5	6	7	8	9	10
361-	MAT1 39	10.5E6	3.8E6	.33	.1					+MAT039
362-	+MAT039	2.91+04	2.33+04	.33	.1					+MAT040
363-	MAT1 40	10.5E6	3.8E6	.33	.1					+MAT041
364-	+MAT040	2.92+04	2.34+04	.33	.1					+MAT042
365-	MAT1 41	10.5E6	3.8E6	.33	.1					+MAT043
366-	+MAT041	1.67+04	1.50+04	.33	.1					+MAT044
367-	MAT1 42	10.5E6	3.8E6	.33	.1					+MAT045
368-	+MAT042	1.90+04	1.52+04	.33	.1					+MAT046
369-	MAT1 43	10.5E6	3.8E6	.33	.1					+MAT047
370-	+MAT043	1.90+04	1.52+04	.33	.1					+MAT048
371-	MAT1 44	10.5E6	3.8E6	.33	.1					+MAT049
372-	+MAT044	1.88+04	1.51+04	.33	.1					+MAT050
373-	MAT1 45	10.5E6	3.8E6	.33	.1					+MAT051
374-	+MAT045	5.97+04	4.78+04	.33	.1					+MAT052
375-	MAT1 46	10.5E6	3.8E6	.33	.1					+MAT053
376-	+MAT046	0.45+04	5.16+04	.33	.1					+MAT054
377-	MAT1 47	10.5E6	3.8E6	.33	.1					+MAT055
378-	+MAT047	5.97+04	4.78+04	.33	.1					+MAT056
379-	MAT1 48	10.5E6	3.8E6	.33	.1					+MAT057
380-	+MAT048	6.71+04	5.37+04	.33	.1					+MAT058
381-	MAT1 49	10.5E6	3.8E6	.33	.1					+MAT059
382-	+MAT049	3.13+04	2.50+04	.33	.1					+MAT060
383-	MAT1 50	10.5E6	3.8E6	.33	.1					+MAT061
384-	+MAT050	3.13+04	2.50+04	.33	.1					
385-	MAT1 51	10.5E6	3.8E6	.33	.1					
386-	+MAT051	6.39+04	5.11+04	.33	.1					
387-	MAT1 52	10.5E6	3.8E6	.33	.1					
388-	+MAT052	6.34+04	5.07+04	.33	.1					
389-	MAT1 53	10.5E6	3.8E6	.33	.1					
390-	+MAT053	6.34+04	5.08+04	.33	.1					
391-	MAT1 54	10.5E6	3.8E6	.33	.1					
392-	+MAT054	6.40+04	5.12+04	.33	.1					
393-	MAT1 55	10.5E6	3.8E6	.33	.1					
394-	+MAT055	3.18+04	2.54+04	.33	.1					
395-	MAT1 56	10.5E6	3.8E6	.33	.1					
396-	+MAT056	3.22+04	2.57+04	.33	.1					
397-	MAT1 57	10.5E6	3.8E6	.33	.1					
398-	+MAT057	3.33+04	2.66+04	.33	.1					
399-	MAT1 58	10.5E6	3.8E6	.33	.1					
400-	+MAT058	3.36+04	2.69+04	.33	.1					
401-	MAT1 59	10.5E6	3.8E6	.33	.1					
402-	+MAT059	3.18+04	2.55+04	.33	.1					
403-	MAT1 60	10.5E6	3.8E6	.33	.1					
404-	+MAT060	3.22+04	2.57+04	.33	.1					
405-	MAT1 61	10.5E6	3.8E6	.33	.1					

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
406-		+MAT061	3.38+04	2.70+04							+MAT062
407-		MAT1	62	10.5E6	3.8E6	.33	.1				+MAT063
408-		+MAT062	3.41+04	2.73+04							+MAT064
409-		MAT1	63	10.5E6	3.8E6	.33	.1				+MAT065
410-		+MAT063	2.19+04	1.76+04							+MAT066
411-		MAT1	64	10.5E6	3.8E6	.33	.1				+MAT067
412-		+MAT064	2.21+04	1.77+04							+MAT068
413-		MAT1	65	10.5E6	3.8E6	.33	.1				+MAT069
414-		+MAT065	2.22+04	1.78+04							+MAT070
415-		MAT1	66	10.5E6	3.8E6	.33	.1				+MAT071
416-		+MAT066	2.21+04	1.77+04							+MAT072
417-		MAT1	67	10.5E6	3.8E6	.33	.1				+MAT073
418-		+MAT067	6.92+04	5.53+04							+MAT074
419-		MAT1	68	10.5E6	3.8E6	.33	.1				+MAT075
420-		+MAT068	7.59+04	6.08+04							+MAT076
421-		MAT1	69	10.5E6	3.8E6	.33	.1				+MAT077
422-		+MAT069	6.92+04	5.53+04							+MAT078
423-		MAT1	70	10.5E6	3.8E6	.33	.1				+MAT079
424-		+MAT070	7.93+04	6.34+04							+MAT080
425-		MAT1	71	10.5E6	3.8E6	.33	.1				+MAT081
426-		+MAT071	3.66+04	2.93+04							+MAT082
427-		MAT1	72	10.5E6	3.8E6	.33	.1				+MAT083
428-		+MAT072	3.66+04	2.93+04							
429-		MAT1	73	10.5E6	3.8E6	.33	.1				
430-		+MAT073	7.41+04	5.93+04							
431-		MAT1	74	10.5E6	3.8E6	.33	.1				
432-		+MAT074	7.50+04	6.00+04							
433-		MAT1	75	10.5E6	3.8E6	.33	.1				
434-		+MAT075	7.50+04	6.00+04							
435-		MAT1	76	10.5E6	3.8E6	.33	.1				
436-		+MAT076	7.41+04	5.93+04							
437-		MAT1	77	10.5E6	3.8E6	.33	.1				
438-		+MAT077	3.69+04	2.95+04							
439-		MAT1	78	10.5E6	3.8E6	.33	.1				
440-		+MAT078	3.76+04	3.01+04							
441-		MAT1	79	10.5E6	3.8E6	.33	.1				
442-		+MAT079	3.90+04	3.12+04							
443-		MAT1	80	10.5E6	3.8E6	.33	.1				
444-		+MAT080	3.90+04	3.12+04							
445-		MAT1	81	10.5E6	3.8E6	.33	.1				
446-		+MAT081	3.65+04	2.95+04							
447-		MAT1	82	10.5E6	3.8E6	.33	.1				
448-		+MAT082	3.76+04	3.01+04							
449-		MAT1	83	10.5E6	3.8E6	.33	.1				
450-		+MAT083	4.00+04	3.20+04							

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
451-		MAT1	84	10.5E6	3.8E6	.33	.1				+MAT084
452-		+MAT084	4.00+04	3.20+04							
453-		MAT1	85	10.5E6	3.8E6	.33	.1				+MAT085
454-		+MAT085	2.56+04	2.05+04							
455-		MAT1	86	10.5E6	3.8E6	.33	.1				+MAT086
456-		+MAT086	2.59+04	2.07+04							
457-		MAT1	87	10.5E6	3.8E6	.33	.1				+MAT087
458-		+MAT087	2.59+04	2.07+04							
459-		MAT1	88	10.5E6	3.8E6	.33	.1				+MAT088
460-		+MAT088	2.56+04	2.05+04							
461-		MAT1	89	10.5E6	3.8E6	.33	.1				+MAT089
462-		+MAT089	8.02+04	6.41+04							
463-		MAT1	90	10.5E6	3.8E6	.33	.1				+MAT090
464-		+MAT090	8.87+04	7.09+04							
465-		MAT1	91	10.5E6	3.8E6	.33	.1				+MAT091
466-		+MAT091	8.02+04	6.41+04							
467-		MAT1	92	10.5E6	3.8E6	.33	.1				+MAT092
468-		+MAT092	9.29+04	7.43+04							
469-		MAT1	93	10.5E6	3.8E6	.33	.1				+MAT093
470-		+MAT093	4.26+04	3.41+04							
471-		MAT1	94	10.5E6	3.8E6	.33	.1				+MAT094
472-		+MAT094	4.26+04	3.41+04							
473-		MAT1	95	10.5E6	3.8E6	.33	.1				+MAT095
474-		+MAT095	8.63+04	6.90+04							
475-		MAT1	96	10.5E6	3.8E6	.33	.1				+MAT096
476-		+MAT096	8.65+04	6.92+04							
477-		MAT1	97	10.5E6	3.8E6	.33	.1				+MAT097
478-		+MAT097	8.65+04	6.92+04							
479-		MAT1	98	10.5E6	3.8E6	.33	.1				+MAT098
480-		+MAT098	8.64+04	6.91+04							
481-		MAT1	99	10.5E6	3.8E6	.33	.1				+MAT099
482-		+MAT099	4.30+04	3.44+04							
483-		MAT1	100	10.5E6	3.8E6	.33	.1				+MAT100
484-		+MAT100	4.35+04	3.48+04							
485-		MAT1	101	10.5E6	3.8E6	.33	.1				+MAT101
486-		+MAT101	4.53+04	3.62+04							
487-		MAT1	102	10.5E6	3.8E6	.33	.1				+MAT102
488-		+MAT102	4.58+04	3.66+04							
489-		MAT1	103	10.5E6	3.8E6	.33	.1				+MAT103
490-		+MAT103	4.31+04	3.44+04							
491-		MAT1	104	10.5E6	3.8E6	.33	.1				+MAT104
492-		+MAT104	4.36+04	3.49+04							
493-		MAT1	105	10.5E6	3.8E6	.33	.1				+MAT105
494-		+MAT105	4.64+04	3.71+04							
495-		MAT1	106	10.5E6	3.8E6	.33	.1				+MAT106

S O R T E D B U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
496-	+MAT106	107	4.66+04	3.73+04							+MAT107
497-	MAT1	107	10.5E6	3.8E6	.33	.1					
498-	+MAT107	108	2.99+04	2.39+04							+MAT108
499-	MAT1	108	10.5E6	3.8E6	.33	.1					
500-	+MAT108	109	3.01+04	2.41+04							+MAT109
501-	MAT1	109	10.5E6	3.8E6	.33	.1					
502-	+MAT109	110	3.03+04	2.43+04							+MAT110
503-	MAT1	110	10.5E6	3.8E6	.33	.1					
504-	+MAT110	111	3.00+04	2.40+04							+MAT111
505-	MAT1	111	10.5E6	3.8E6	.33	.1					
506-	+MAT111	112	9.40+04	7.52+04							+MAT112
507-	MAT1	112	10.5E6	3.8E6	.33	.1					
508-	+MAT112	113	1.05+05	8.59+04							+MAT113
509-	MAT1	113	10.5E6	3.8E6	.33	.1					
510-	+MAT113	114	9.40+04	7.52+04							+MAT114
511-	MAT1	114	10.5E6	3.8E6	.33	.1					
512-	+MAT114	115	1.09+05	8.71+04							+MAT115
513-	MAT1	115	10.5E6	3.8E6	.33	.1					
514-	+MAT115	116	5.01+04	4.01+04							+MAT116
515-	MAT1	116	10.5E6	3.8E6	.33	.1					
516-	+MAT116	117	4.99+04	3.99+04							+MAT117
517-	MAT1	117	10.5E6	3.8E6	.33	.1					
518-	+MAT117	118	1.01+05	8.06+04							+MAT118
519-	MAT1	118	10.5E6	3.8E6	.33	.1					
520-	+MAT118	119	1.01+05	8.05+04							+MAT119
521-	MAT1	119	10.5E6	3.8E6	.33	.1					
522-	+MAT119	120	1.01+05	8.06+04							+MAT120
523-	MAT1	120	10.5E6	3.8E6	.33	.1					
524-	+MAT120	121	1.01+05	8.06+04							+MAT121
525-	MAT1	121	10.5E6	3.8E6	.33	.1					
526-	+MAT121	122	5.04+04	4.03+04							+MAT122
527-	MAT1	122	10.5E6	3.8E6	.33	.1					
528-	+MAT122	123	5.05+04	4.04+04							+MAT123
529-	MAT1	123	10.5E6	3.8E6	.33	.1					
530-	+MAT123	124	5.56+04	4.24+04							+MAT124
531-	MAT1	124	10.5E6	3.8E6	.33	.1					
532-	+MAT124	125	5.54+04	4.27+04							+MAT125
533-	MAT1	125	10.5E6	3.8E6	.33	.1					
534-	+MAT125	126	5.05+04	4.04+04							+MAT126
535-	MAT1	126	10.5E6	3.8E6	.33	.1					
536-	+MAT126	127	5.05+04	4.04+04							+MAT127
537-	MAT1	127	10.5E6	3.8E6	.33	.1					
538-	+MAT127	128	5.46+04	4.32+04							+MAT128
539-	MAT1	128	10.5E6	3.8E6	.33	.1					
540-	+MAT128	129	5.47+04	4.37+04							

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
541-		MAT1	129	10.5E6	3.8E6	.33	.1				+MAT129
542-		+MAT129	3.51+04	2.80+04							+MAT130
543-		MAT1	130	10.5E6	3.8E6	.33	.1				+MAT131
544-		+MAT130	3.49+04	2.79+04							+MAT132
545-		MAT1	131	10.5E6	3.8E6	.33	.1				+MAT133
546-		+MAT131	3.52+04	2.82+04							+MAT134
547-		MAT1	132	10.5E6	3.8E6	.33	.1				+MAT135
548-		+MAT132	3.52+04	2.82+04							+MAT136
549-		MAT1	133	10.5E6	3.8E6	.33	.1				+MAT137
550-		+MAT133	1.09+05	8.71+04							+MAT138
551-		MAT1	134	10.5E6	3.8E6	.33	.1				+MAT139
552-		+MAT134	1.21+05	9.67+04							+MAT140
553-		MAT1	135	10.5E6	3.8E6	.33	.1				+MAT141
554-		+MAT135	1.09+05	8.71+04							+MAT142
555-		MAT1	136	10.5E6	3.8E6	.33	.1				+MAT143
556-		+MAT136	1.28+05	1.02+05							+MAT144
557-		MAT1	137	10.5E6	3.8E6	.33	.1				+MAT145
558-		+MAT137	5.80+04	4.64+04							+MAT146
559-		MAT1	138	10.5E6	3.8E6	.33	.1				+MAT147
560-		+MAT138	5.80+04	4.64+04							+MAT148
561-		MAT1	139	10.5E6	3.8E6	.33	.1				+MAT149
562-		+MAT139	1.17+05	9.38+04							+MAT150
563-		MAT1	140	10.5E6	3.8E6	.33	.1				+MAT151
564-		+MAT140	1.16+05	9.27+04							
565-		MAT1	141	10.5E6	3.8E6	.33	.1				
566-		+MAT141	1.16+05	9.27+04							
567-		MAT1	142	10.5E6	3.8E6	.33	.1				
568-		+MAT142	1.17+05	9.38+04							
569-		MAT1	143	10.5E6	3.8E6	.33	.1				
570-		+MAT143	5.80+04	4.64+04							
571-		MAT1	144	10.5E6	3.8E6	.33	.1				
572-		+MAT144	5.92+04	4.74+04							
573-		MAT1	145	10.5E6	3.8E6	.33	.1				
574-		+MAT145	6.20+04	4.96+04							
575-		MAT1	146	10.5E6	3.8E6	.33	.1				
576-		+MAT146	6.24+04	4.99+04							
577-		MAT1	147	10.5E6	3.8E6	.33	.1				
578-		+MAT147	5.80+04	4.64+04							
579-		MAT1	148	10.5E6	3.8E6	.33	.1				
580-		+MAT148	5.92+04	4.74+04							
581-		MAT1	149	10.5E6	3.8E6	.33	.1				
582-		+MAT149	6.28+04	5.03+04							
583-		MAT1	150	10.5E6	3.8E6	.33	.1				
584-		+MAT150	6.33+04	5.06+04							
585-		MAT1	151	10.5E6	3.8E6	.33	.1				

DAMAGE CRITERION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
586-	+MAT151	4.05+04	3.24+04							+MAT152
587-	MAT1 152	10.5E6	3.8E6	.33	.1					+MAT153
588-	+MAT152	4.12+04	3.29+04							+MAT154
589-	MAT1 153	10.5E6	3.8E6	.33	.1					+MAT155
590-	+MAT153	4.13+04	3.31+04							+MAT156
591-	MAT1 154	10.5E6	3.8E6	.33	.1					+MAT157
592-	+MAT154	4.06+04	3.25+04							+MAT158
593-	MAT1 155	10.5E6	3.8E6	.33	.1					+MAT159
594-	+MAT155	1.28+05	1.02+05							+MAT160
595-	MAT1 156	10.5E6	3.8E6	.33	.1					+MAT161
596-	+MAT156	1.45+05	1.16+05							+MAT162
597-	MAT1 157	10.5E6	3.8E6	.33	.1					+MAT163
598-	+MAT157	1.28+05	1.02+05							+MAT164
599-	MAT1 158	10.5E6	3.8E6	.33	.1					+MAT165
600-	+MAT158	1.49+05	1.20+05							+MAT166
601-	MAT1 159	10.5E6	3.8E6	.33	.1					+MAT167
602-	+MAT159	6.84+04	5.47+04							+MAT168
603-	MAT1 160	10.5E6	3.8E6	.33	.1					+MAT169
604-	+MAT160	6.84+04	5.47+04							+MAT170
605-	MAT1 161	10.5E6	3.8E6	.33	.1					+MAT171
606-	+MAT161	1.34+05	1.08+05							+MAT172
607-	MAT1 162	10.5E6	3.8E6	.33	.1					+MAT173
608-	+MAT162	1.37+05	1.09+05							
609-	MAT1 163	10.5E6	3.8E6	.33	.1					
610-	+MAT163	1.37+05	1.09+05							
611-	MAT1 164	10.5E6	3.8E6	.33	.1					
612-	+MAT164	1.35+05	1.08+05							
613-	MAT1 165	10.5E6	3.8E6	.33	.1					
614-	+MAT165	6.74+04	5.40+04							
615-	MAT1 166	10.5E6	3.8E6	.33	.1					
616-	+MAT166	6.90+04	5.22+04							
617-	MAT1 167	10.5E6	3.8E6	.33	.1					
618-	+MAT167	7.24+04	5.79+04							
619-	MAT1 168	10.5E6	3.8E6	.33	.1					
620-	+MAT168	7.29+04	5.83+04							
621-	MAT1 169	10.5E6	3.8E6	.33	.1					
622-	+MAT169	6.74+04	5.40+04							
623-	MAT1 170	10.5E6	3.8E6	.33	.1					
624-	+MAT170	6.90+04	5.22+04							
625-	MAT1 171	10.5E6	3.8E6	.33	.1					
626-	+MAT171	7.40+04	5.92+04							
627-	MAT1 172	10.5E6	3.8E6	.33	.1					
628-	+MAT172	7.46+04	5.97+04							
629-	MAT1 173	10.5E6	3.8E6	.33	.1					
630-	+MAT173	4.74+04	3.79+04							

S C R T E D B U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
631-	MAT1	174	10.5E6	3.8E6	.33	.1					+MAT174
632-	+MAT174	4.81+04	3.85+04								
633-	MAT1	175	10.5E6	3.8E6	.33	.1					+MAT175
634-	+MAT175	4.83+04	3.87+04								
635-	MAT1	176	10.5E6	3.8E6	.33	.1					+MAT176
636-	+MAT176	4.76+04	3.81+04								
637-	MAT1	177	10.5E6	3.8E6	.33	.1					+MAT177
638-	+MAT177	1.47+05	1.18+05								
639-	MAT1	178	10.5E6	3.8E6	.33	.1					+MAT178
640-	+MAT178	1.72+05	1.37+05								
641-	MAT1	179	10.5E6	3.8E6	.33	.1					+MAT179
642-	+MAT179	1.47+05	1.18+05								
643-	MAT1	180	10.5E6	3.8E6	.33	.1					+MAT180
644-	+MAT180	1.77+05	1.42+05								
645-	MAT1	181	10.5E6	3.8E6	.33	.1					+MAT181
646-	+MAT181	7.99+04	6.39+04								
647-	MAT1	182	10.5E6	3.8E6	.33	.1					+MAT182
648-	+MAT182	7.99+04	6.39+04								
649-	MAT1	183	10.5E6	3.8E6	.33	.1					+MAT183
650-	+MAT183	1.61+05	1.29+05								
651-	MAT1	184	10.5E6	3.8E6	.33	.1					+MAT184
652-	+MAT184	1.58+05	1.27+05								
653-	MAT1	185	10.5E6	3.8E6	.33	.1					+MAT185
654-	+MAT185	1.58+05	1.27+05								
655-	MAT1	186	10.5E6	3.8E6	.33	.1					+MAT186
656-	+MAT186	1.61+05	1.29+05								
657-	MAT1	187	10.5E6	3.8E6	.33	.1					+MAT187
658-	+MAT187	7.94+04	6.35+04								
659-	MAT1	188	10.5E6	3.6E6	.33	.1					+MAT188
660-	+MAT188	8.00+04	6.40+04								
661-	MAT1	189	10.5E6	3.8E6	.33	.1					+MAT189
662-	+MAT189	8.58+04	6.86+04								
663-	MAT1	190	10.5E6	3.8E6	.33	.1					+MAT190
664-	+MAT190	8.64+04	6.91+04								
665-	MAT1	191	10.5E6	3.8E6	.33	.1					+MAT191
666-	+MAT191	7.94+04	6.35+04								
667-	MAT1	192	10.5E6	3.8E6	.33	.1					+MAT192
668-	+MAT192	5.60+04	4.48+04								
669-	MAT1	193	10.5E6	3.8E6	.33	.1					+MAT193
670-	+MAT193	8.71+04	6.96+04								
671-	MAT1	194	10.5E6	3.8E6	.33	.1					+MAT194
672-	+MAT194	8.71+04	6.96+04								
673-	MAT1	195	10.5E6	3.8E6	.33	.1					+MAT195
674-	+MAT195	5.60+04	4.48+04								
675-	MAT1	196	10.5E6	3.8E6	.33	.1					+MAT196

TRUSS TAIL BOOM MODELL **A.220 ELEMENT VERSION
DAMAGE CRITERION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
676-	+MAT196	5.60+04	4.48+04							
677-	MAT11	197	10.5E6	3.8E6	.33	.1				+MAT197
678-	+MAT197	5.63+04	4.50+04							+MAT198
679-	MAT11	198	10.5E6	3.8E6	.33	.1				+MAT199
680-	+MAT198	5.60+04	4.48+04							+MAT200
681-	MAT11	199	10.5E6	3.8E6	.33	.1				+MAT201
682-	+MAT199	1.72+05	1.37+05							+MAT202
683-	MAT11	200	10.5E6	3.8E6	.33	.1				+MAT203
684-	+MAT200	1.99+05	1.60+05							+MAT204
685-	MAT11	201	10.5E6	3.8E6	.33	.1				+MAT205
686-	+MAT201	1.72+05	1.37+05							+MAT206
687-	MAT11	202	10.5E6	3.8E6	.33	.1				+MAT207
688-	+MAT202	2.10+05	1.68+05							+MAT208
689-	MAT11	203	10.5E6	3.8E6	.33	.1				+MAT209
690-	+MAT203	9.38+04	7.50+04							+MAT210
691-	MAT11	204	10.5E6	3.8E6	.33	.1				+MAT211
692-	+MAT204	9.30+04	7.44+04							+MAT212
693-	MAT11	205	10.5E6	3.8E6	.33	.1				+MAT213
694-	+MAT205	1.63+05	1.46+05							+MAT214
695-	MAT11	206	10.5E6	3.8E6	.33	.1				+MAT215
696-	+MAT206	1.86+05	1.49+05							+MAT216
697-	MAT11	207	10.5E6	3.8E6	.33	.1				+MAT217
698-	+MAT207	1.86+05	1.49+05							+MAT218
699-	MAT11	208	10.5E6	3.8E6	.33	.1				+MAT219
700-	+MAT208	1.83+05	1.46+05							+MAT220
701-	MAT11	209	10.5E6	3.8E6	.33	.1				+MAT221
702-	+MAT209	9.16+04	7.33+04							+MAT222
703-	MAT11	210	10.5E6	3.8E6	.33	.1				+MAT223
704-	+MAT210	9.31+04	7.45+04							+MAT224
705-	MAT11	211	10.5E6	3.8E6	.33	.1				+MAT225
706-	+MAT211	9.94+04	7.95+04							+MAT226
707-	MAT11	212	10.5E6	3.8E6	.33	.1				+MAT227
708-	+MAT212	9.94+04	7.95+04							+MAT228
709-	MAT11	213	10.5E6	3.8E6	.33	.1				+MAT229
710-	+MAT213	9.16+04	7.33+04							+MAT230
711-	MAT11	214	10.5E6	3.8E6	.33	.1				+MAT231
712-	+MAT214	9.32+04	7.46+04							+MAT232
713-	MAT11	215	10.5E6	3.8E6	.33	.1				+MAT233
714-	+MAT215	1.02+05	8.16+04							+MAT234
715-	MAT11	216	10.5E6	3.8E6	.33	.1				+MAT235
716-	+MAT216	1.63+05	8.23+04							+MAT236
717-	MAT11	217	10.5E6	3.8E6	.33	.1				+MAT237
718-	+MAT217	6.49+04	5.15+04							+MAT238
719-	MAT11	218	10.5E6	3.8E6	.33	.1				+MAT239
720-	+MAT218	6.57+04	5.20+04							+MAT240

SORTED BULK DATA ECHO

CARD	1	2	3	4	5	6	7	8	9	10
COUNT										
721-	MAT1	219	10.5E6	3.8E6	.33	.1				+MAT219
722-	+MAT219	6.60+04	5.28+04							
723-	MAT1	220	10.5E6	3.8E6	.33	.1				+MAT220
724-	+MAT220	6.49+04	5.19+04							
725-	MAT1	221	10.5E6	3.8E6	.33	.1				+MAT221
726-	+MAT221	1.99+05	1.60+05							
727-	MAT1	222	10.5E6	3.8E6	.33	.1				+MAT222
728-	+MAT222	2.39+05	1.91+05							
729-	MAT1	223	10.5E6	3.8E6	.33	.1				+MAT223
730-	+MAT223	1.99+05	1.60+05							
731-	MAT1	224	10.5E6	3.8E6	.33	.1				+MAT224
732-	+MAT224	2.48+05	1.99+05							
733-	MAT1	225	10.5E6	3.8E6	.33	.1				+MAT225
734-	+MAT225	1.10+05	8.77+04							
735-	MAT1	226	10.5E6	3.8E6	.33	.1				+MAT226
736-	+MAT226	1.10+05	6.77+04							
737-	PARAM	GRUPNT	0							
738-	PTUBE	1	1	1.5	.0625					
739-	PTUBE	2	2	1.5	.0625					
740-	PTUBE	3	3	1.5	.0625					
741-	PTUBE	4	4	1.5	.0625					
742-	PTUBE	5	5	1.5	.0625					
743-	PTUBE	6	6	1.5	.0625					
744-	PTUBE	7	7	1.5	.0625					
745-	PTUBE	8	8	1.5	.0625					
746-	PTUBE	9	9	1.5	.0625					
747-	PTUBE	10	10	1.5	.0625					
748-	PTUBE	11	11	1.5	.0625					
749-	PTUBE	12	12	1.5	.0625					
750-	PTUBE	13	13	1.5	.0625					
751-	PTUBE	14	14	1.5	.0625					
752-	PTUBE	15	15	1.5	.0625					
753-	PTUBE	16	16	1.5	.0625					
754-	PTUBE	17	17	1.5	.0625					
755-	PTUBE	18	18	1.5	.0625					
756-	PTUBE	19	19	1.5	.0625					
757-	PTUBE	20	20	1.5	.0625					
758-	PTUBE	21	21	1.5	.0625					
759-	PTUBE	22	22	1.5	.0625					
760-	PTUBE	23	23	1.5	.0625					
761-	PTUBE	24	24	1.5	.0625					
762-	PTUBE	25	25	1.5	.0625					
763-	PTUBE	26	26	1.5	.0625					
764-	PTUBE	27	27	1.5	.0625					
765-	PTUBE	28	28	1.5	.0625					

S O R T E D B U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
766-	PTUBE	29	29	3	1.5	.0625					
767-	PTUBE	30	30	3	1.5	.0625					
768-	PTUBE	31	31	3	1.5	.0625					
769-	PTUBE	32	32	3	1.5	.0625					
770-	PTUBE	33	33	3	1.5	.0625					
771-	PTUBE	34	34	3	1.5	.0625					
772-	PTUBE	35	35	3	1.5	.0625					
773-	PTUBE	36	36	3	1.5	.0625					
774-	PTUBE	37	37	3	1.5	.0625					
775-	PTUBE	38	38	3	1.5	.0625					
776-	PTUBE	39	39	3	1.5	.0625					
777-	PTUBE	40	40	3	1.5	.0625					
778-	PTUBE	41	41	3	1.5	.0625					
779-	PTUBE	42	42	3	1.5	.0625					
780-	PTUBE	43	43	3	1.5	.0625					
781-	PTUBE	44	44	3	1.5	.0625					
782-	PTUBE	45	45	3	1.5	.0625					
783-	PTUBE	46	46	3	1.5	.0625					
784-	PTUBE	47	47	3	1.5	.0625					
785-	PTUBE	48	48	3	1.5	.0625					
786-	PTUBE	49	49	3	1.5	.0625					
787-	PTUBE	50	50	3	1.5	.0625					
788-	PTUBE	51	51	3	1.5	.0625					
789-	PTUBE	52	52	3	1.5	.0625					
790-	PTUBE	53	53	3	1.5	.0625					
791-	PTUBE	54	54	3	1.5	.0625					
792-	PTUBE	55	55	3	1.5	.0625					
793-	PTUBE	56	56	3	1.5	.0625					
794-	PTUBE	57	57	3	1.5	.0625					
795-	PTUBE	58	58	3	1.5	.0625					
796-	PTUBE	59	59	3	1.5	.0625					
797-	PTUBE	60	60	3	1.5	.0625					
798-	PTUBE	61	61	3	1.5	.0625					
799-	PTUBE	62	62	3	1.5	.0625					
800-	PTUBE	63	63	3	1.5	.0625					
801-	PTUBE	64	64	3	1.5	.0625					
802-	PTUBE	65	65	3	1.5	.0625					
803-	PTUBE	66	66	3	1.5	.0625					
804-	PTUBE	67	67	3	1.5	.0625					
805-	PTUBE	68	68	3	1.5	.0625					
806-	PTUBE	69	69	3	1.5	.0625					
807-	PTUBE	70	70	3	1.5	.0625					
808-	PTUBE	71	71	3	1.5	.0625					
809-	PTUBE	72	72	3	1.5	.0625					
810-	PTUBE	73	73	3	1.5	.0625					

TRUSS TAIL BOOM MODEL 1 ***A 226 ELEMENT VERSION
DAMAGE CRITERION = NONE

SORTED BULK DATA ECHO

CAKU	CUUNT	1	2	3	4	5	6	7	8	9	10
811-	PTUBE	74	74
812-	PTUBE	75	75	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
813-	PTUBE	76	76	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
814-	PTUBE	77	77	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
815-	PTUBE	78	78	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
816-	PTUBE	79	79	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
817-	PTUBE	80	80	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
818-	PTUBE	81	81	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
819-	PTUBE	82	82	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
820-	PTUBE	83	83	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
821-	PTUBE	84	84	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
822-	PTUBE	85	85	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
823-	PTUBE	86	86	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
824-	PTUBE	87	87	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
825-	PTUBE	88	88	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
826-	PTUBE	89	89	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
827-	PTUBE	90	90	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
828-	PTUBE	91	91	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
829-	PTUBE	92	92	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
830-	PTUBE	93	93	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
831-	PTUBE	94	94	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
832-	PTUBE	95	95	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
833-	PTUBE	96	96	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
834-	PTUBE	97	97	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
835-	PTUBE	98	98	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
836-	PTUBE	99	99	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
837-	PTUBE	100	100	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
838-	PTUBE	101	101	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
839-	PTUBE	102	102	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
840-	PTUBE	103	103	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
841-	PTUBE	104	104	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
842-	PTUBE	105	105	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
843-	PTUBE	106	106	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
844-	PTUBE	107	107	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
845-	PTUBE	108	108	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
846-	PTUBE	109	109	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
847-	PTUBE	110	110	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
848-	PTUBE	111	111	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
849-	PTUBE	112	112	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
850-	PTUBE	113	113	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
851-	PTUBE	114	114	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
852-	PTUBE	115	115	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
853-	PTUBE	116	116	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
854-	PTUBE	117	117	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625
855-	PTUBE	118	118	1.5	1.5	.0625	.0625	.0625	.0625	.0625	.0625

CARD COUNT	1	2	3	4	5	6	7	8	9	10
856-	PTUBE 119	119	119	1.5	.0625					
857-	PTUBE 120	120	120	1.5	.0625					
858-	PTUBE 121	121	121	1.5	.0625					
859-	PTUBE 122	122	122	1.5	.0625					
860-	PTUBE 123	123	123	1.5	.0625					
861-	PTUBE 124	124	124	1.5	.0625					
862-	PTUBE 125	125	125	1.5	.0625					
863-	PTUBE 126	126	126	1.5	.0625					
864-	PTUBE 127	127	127	1.5	.0625					
865-	PTUBE 128	128	128	1.5	.0625					
866-	PTUBE 129	129	129	1.5	.0625					
867-	PTUBE 130	130	130	1.5	.0625					
868-	PTUBE 131	131	131	1.5	.0625					
869-	PTUBE 132	132	132	1.5	.0625					
870-	PTUBE 133	133	133	1.5	.0625					
871-	PTUBE 134	134	134	1.5	.0625					
872-	PTUBE 135	135	135	1.5	.0625					
873-	PTUBE 136	136	136	1.5	.0625					
874-	PTUBE 137	137	137	1.5	.0625					
875-	PTUBE 138	138	138	1.5	.0625					
876-	PTUBE 139	139	139	1.5	.0625					
877-	PTUBE 140	140	140	1.5	.0625					
878-	PTUBE 141	141	141	1.5	.0625					
879-	PTUBE 142	142	142	1.5	.0625					
880-	PTUBE 143	143	143	1.5	.0625					
881-	PTUBE 144	144	144	1.5	.0625					
882-	PTUBE 145	145	145	1.5	.0625					
883-	PTUBE 146	146	146	1.5	.0625					
884-	PTUBE 147	147	147	1.5	.0625					
885-	PTUBE 148	148	148	1.5	.0625					
886-	PTUBE 149	149	149	1.5	.0625					
887-	PTUBE 150	150	150	1.5	.0625					
888-	PTUBE 151	151	151	1.5	.0625					
889-	PTUBE 152	152	152	1.5	.0625					
890-	PTUBE 153	153	153	1.5	.0625					
891-	PTUBE 154	154	154	1.5	.0625					
892-	PTUBE 155	155	155	1.5	.0625					
893-	PTUBE 156	156	156	1.5	.0625					
894-	PTUBE 157	157	157	1.5	.0625					
895-	PTUBE 158	158	158	1.5	.0625					
896-	PTUBE 159	159	159	1.5	.0625					
897-	PTUBE 160	160	160	1.5	.0625					
898-	PTUBE 161	161	161	1.5	.0625					
899-	PTUBE 162	162	162	1.5	.0625					
900-	PTUBE 163	163	163	1.5	.0625					

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
901-	PTUBE	164	164	164	164	164	164	164	164	164	164
902-	PTUBE	165	165	165	165	165	165	165	165	165	165
903-	PTUBE	166	166	166	166	166	166	166	166	166	166
904-	PTUBE	167	167	167	167	167	167	167	167	167	167
905-	PTUBE	168	168	168	168	168	168	168	168	168	168
906-	PTUBE	169	169	169	169	169	169	169	169	169	169
907-	PTUBE	170	170	170	170	170	170	170	170	170	170
908-	PTUBE	171	171	171	171	171	171	171	171	171	171
909-	PTUBE	172	172	172	172	172	172	172	172	172	172
910-	PTUBE	173	173	173	173	173	173	173	173	173	173
911-	PTUBE	174	174	174	174	174	174	174	174	174	174
912-	PTUBE	175	175	175	175	175	175	175	175	175	175
913-	PTUBE	176	176	176	176	176	176	176	176	176	176
914-	PTUBE	177	177	177	177	177	177	177	177	177	177
915-	PTUBE	178	178	178	178	178	178	178	178	178	178
916-	PTUBE	179	179	179	179	179	179	179	179	179	179
917-	PTUBE	180	180	180	180	180	180	180	180	180	180
918-	PTUBE	181	181	181	181	181	181	181	181	181	181
919-	PTUBE	182	182	182	182	182	182	182	182	182	182
920-	PTUBE	183	183	183	183	183	183	183	183	183	183
921-	PTUBE	184	184	184	184	184	184	184	184	184	184
922-	PTUBE	185	185	185	185	185	185	185	185	185	185
923-	PTUBE	186	186	186	186	186	186	186	186	186	186
924-	PTUBE	187	187	187	187	187	187	187	187	187	187
925-	PTUBE	188	188	188	188	188	188	188	188	188	188
926-	PTUBE	189	189	189	189	189	189	189	189	189	189
927-	PTUBE	190	190	190	190	190	190	190	190	190	190
928-	PTUBE	191	191	191	191	191	191	191	191	191	191
929-	PTUBE	192	192	192	192	192	192	192	192	192	192
930-	PTUBE	193	193	193	193	193	193	193	193	193	193
931-	PTUBE	194	194	194	194	194	194	194	194	194	194
932-	PTUBE	195	195	195	195	195	195	195	195	195	195
933-	PTUBE	196	196	196	196	196	196	196	196	196	196
934-	PTUBE	197	197	197	197	197	197	197	197	197	197
935-	PTUBE	198	198	198	198	198	198	198	198	198	198
936-	PTUBE	199	199	199	199	199	199	199	199	199	199
937-	PTUBE	200	200	200	200	200	200	200	200	200	200
938-	PTUBE	201	201	201	201	201	201	201	201	201	201
939-	PTUBE	202	202	202	202	202	202	202	202	202	202
940-	PTUBE	203	203	203	203	203	203	203	203	203	203
941-	PTUBE	204	204	204	204	204	204	204	204	204	204
942-	PTUBE	205	205	205	205	205	205	205	205	205	205
943-	PTUBE	206	206	206	206	206	206	206	206	206	206
944-	PTUBE	207	207	207	207	207	207	207	207	207	207
945-	PTUBE	208	208	208	208	208	208	208	208	208	208

S O R T E D B U L K D A T A E C H O

CARD	1	2	3	4	5	6	7	8	9	10
COUNT	209	210	211	212	213	214	215	216	217	218
946-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
947-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
948-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
949-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
950-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
951-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
952-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
953-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
954-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
955-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
956-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
957-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
958-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
959-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
960-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
961-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
962-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
963-	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE	PTUBE
964-	SPC	10	1	123456	2	123456	4	123456		
965-	SPC	10	3	123456	4	123456				

* 19.6 CPU-S 71.0 COR-S 11.7 ELP-S. XGPI
 NO ERRORS FOUND - EXECUTE NASTRAN PROGRAM
 * 23.1 CPU-S 75.3 COR-S 13.1 ELP-S. SEMI END
 * 23.1 CPU-S 75.3 COR-S 13.1 ELP-S. ---- LINK END ---

AD-A064 181

ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND ABERD--ETC F/6 1/3
HIGHLY SURVIVABLE TRUSS TYPE TAIL BOOM.(U)
NOV 78 T F ERLINE

UNCLASSIFIED

ARBRL-TR-02123

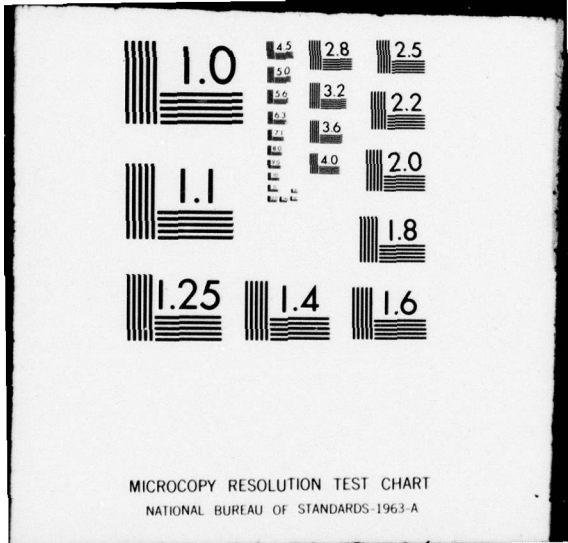
SBIE-AD-E430 172

NL

2 OF 2
AD
A064181



END
DATE
FILMED
4-79
DDC



TRUSS TAIL BOOM MODEL 1 *** 226 ELEMENT VERSION
DAMAGE CRITERION = NONE

SORTED BULK DATA ECHO

CARD	1	2	3	4	5	6	7	8	9	10
946-	PTUBE	209	1.5	.0625						
947-	PTUBE	210	1.5	.0625						
948-	PTUBE	211	1.5	.0625						
949-	PTUBE	212	1.5	.0625						
950-	PTUBE	213	1.5	.0625						
951-	PTUBE	214	1.5	.0625						
952-	PTUBE	215	1.5	.0625						
953-	PTUBE	216	1.5	.0625						
954-	PTUBE	217	1.5	.0625						
955-	PTUBE	218	1.5	.0625						
956-	PTUBE	219	1.5	.0625						
957-	PTUBE	220	1.5	.0625						
958-	PTUBE	221	1.5	.0625						
959-	PTUBE	222	1.5	.0625						
960-	PTUBE	223	1.5	.0625						
961-	PTUBE	224	1.5	.0625						
962-	PTUBE	225	1.5	.0625						
963-	PTUBE	226	1.5	.0625						
964-	SPC	10	1	123456	2					123456
965-	SPC	10	3	123456	4					123456

ENDDATA

- * 19.6 CPU-S 71.0 COR-S 117 ELP-S. XGPI -
- **NO ERRORS FOUND - EXECUTE NASTRAN PROGRAM**
- * 23.1 CPU-S 75.3 COR-S 131 ELP-S. SEM1 END
- * 23.1 CPU-S 75.3 COR-S 131 ELP-S. ---- LINK END ----

TRUSS TAIL BOOM MODEL **A 226 ELEMENT VERSION
DAMAGE CRITERION = NONE

LINEAR CASE 30 X LOADING

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	3.317435-03	-4.525320-03	2.740695-04	.0	.0	.0
6	6	-7.17699-04	2.263182-03	8.276372-04	.0	.0	.0
7	6	-3.250243-03	1.422724-03	-5.456768-03	.0	.0	.0
8	6	5.965247-04	-3.688462-03	-4.836820-03	.0	.0	.0
9	6	6.047826-03	-1.120983-02	-2.942591-03	.0	.0	.0
10	6	-8.974057-04	9.010426-04	-2.458876-03	.0	.0	.0
11	6	-5.959460-03	3.353342-04	-1.394383-02	.0	.0	.0
12	6	6.588768-04	-1.062861-02	-1.344618-02	.0	.0	.0
13	6	8.030114-03	-2.034682-02	-8.673496-03	.0	.0	.0
14	6	-5.977564-04	-3.228083-03	-8.271170-03	.0	.0	.0
15	6	-8.014410-05	-3.596386-03	-2.457499-02	.0	.0	.0
16	6	2.322426-04	-1.998783-02	-2.408844-02	.0	.0	.0
17	6	9.446027-03	-3.179371-02	-1.560709-02	.0	.0	.0
18	6	1.477403-04	-9.917407-03	-1.523586-02	.0	.0	.0
19	6	-9.460349-05	-1.008557-02	-3.600965-02	.0	.0	.0
20	6	-6.510956-04	-3.161392-02	-3.562558-02	.0	.0	.0
21	6	1.018451-02	-4.528521-02	-2.304737-02	.0	.0	.0
22	6	1.261433-03	-1.915144-02	-2.259622-02	.0	.0	.0
23	6	-1.039438-02	-1.912108-02	-4.751317-02	.0	.0	.0
24	6	-1.976220-03	-4.531758-02	-4.721712-02	.0	.0	.0
25	6	1.084307-02	-6.111844-02	-2.947164-02	.0	.0	.0
26	6	2.441486-03	-3.066077-02	-2.924202-02	.0	.0	.0
27	6	-1.109875-02	-3.065947-02	-5.797527-02	.0	.0	.0
28	6	-3.362920-03	-6.112394-02	-5.775036-02	.0	.0	.0
29	6	1.124946-02	-7.849591-02	-3.567908-02	.0	.0	.0
30	6	3.547208-03	-4.429195-02	-3.534126-02	.0	.0	.0
31	6	-1.177890-02	-4.428613-02	-6.770101-02	.0	.0	.0
32	6	-4.606679-03	-7.850019-02	-6.726075-02	.0	.0	.0
33	6	1.171436-02	-9.796644-02	-4.140473-02	.0	.0	.0
34	6	4.472547-03	-5.969817-02	-4.105748-02	.0	.0	.0
35	6	-1.240374-02	-5.969571-02	-7.659027-02	.0	.0	.0
36	6	-5.828729-03	-9.796801-02	-7.623815-02	.0	.0	.0
37	6	1.230858-02	-1.190330-01	-4.650517-02	.0	.0	.0
38	6	5.372251-03	-7.750216-02	-4.624579-02	.0	.0	.0
39	6	-1.278492-02	-7.749596-02	-8.468287-02	.0	.0	.0
40	6	-7.096980-03	-1.190386-01	-8.465548-02	.0	.0	.0
41	6	1.287949-02	-1.425276-01	-5.188111-02	.0	.0	.0
42	6	5.943539-03	-9.621248-02	-5.194198-02	.0	.0	.0
43	6	-1.310563-02	-9.621593-02	-9.160534-02	.0	.0	.0
44	6	-8.148774-03	-1.425316-01	-9.167417-02	.0	.0	.0

TRUSS TAIL BOOM MODEL 1 **A 226 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 75 % LOADING SUBCASE 2

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	8.161912-03	-1.098737-02	5.579749-04	.0	.0	.0
6	6	-1.531652-03	5.506288-03	1.917068-03	.0	.0	.0
7	6	-7.994130-03	3.424577-03	-1.329790-02	.0	.0	.0
8	6	1.547047-03	-8.698459-03	-1.179971-02	.0	.0	.0
9	6	1.494925-02	-2.720790-02	-7.559873-03	.0	.0	.0
10	6	-2.355201-03	2.166273-03	-6.371371-03	.0	.0	.0
11	6	-1.467079-02	7.538492-04	-3.417505-02	.0	.0	.0
12	6	1.805218-03	-2.573578-02	-3.296987-02	.0	.0	.0
13	6	1.963715-02	-4.940244-02	-2.198809-02	.0	.0	.0
14	6	-1.719038-03	-7.911682-03	-2.100304-02	.0	.0	.0
15	6	-1.975753-02	-8.845319-03	-6.046708-02	.0	.0	.0
16	6	8.759450-04	-4.846662-02	-5.928702-02	.0	.0	.0
17	6	-2.537899-02	-7.722830-02	-3.953872-02	.0	.0	.0
18	6	-7.862373-06	-2.421004-02	-3.863130-02	.0	.0	.0
19	6	-2.337501-02	-2.465797-02	-8.890931-02	.0	.0	.0
20	6	-1.154399-03	-7.670873-02	-8.798461-02	.0	.0	.0
21	6	2.524840-02	1.099700-01	-5.851043-02	.0	.0	.0
22	6	2.586679-03	-4.666657-02	-5.742018-02	.0	.0	.0
23	6	-2.509353-02	-4.663386-02	-1.177156-01	.0	.0	.0
24	6	-4.249045-03	-1.099780-01	-1.170125-01	.0	.0	.0
25	6	2.691707-02	-1.483379-01	-7.521807-02	.0	.0	.0
26	6	5.342885-03	-7.457530-02	-7.466317-02	.0	.0	.0
27	6	-2.744954-02	-7.460943-02	-1.441914-01	.0	.0	.0
28	6	-7.489395-03	-1.482817-01	-1.436619-01	.0	.0	.0
29	6	2.705240-02	-1.904010-01	-9.155695-02	.0	.0	.0
30	6	7.934466-03	-1.075763-01	-9.074915-02	.0	.0	.0
31	6	-2.914447-02	-1.075954-01	-1.690522-01	.0	.0	.0
32	6	-1.040860-02	-1.903437-01	-1.679927-01	.0	.0	.0
33	6	2.912243-02	-2.374892-01	-1.068757-01	.0	.0	.0
34	6	1.009445-02	-1.446328-01	-1.060361-01	.0	.0	.0
35	6	-4.070355-02	-1.448545-01	-1.920171-01	.0	.0	.0
36	6	-1.526580-02	-2.374274-01	-1.911783-01	.0	.0	.0
37	6	3.064175-02	-2.084089-01	-1.207733-01	.0	.0	.0
38	6	1.222305-02	-1.874536-01	-1.201455-01	.0	.0	.0
39	6	-3.164104-02	-1.878572-01	-2.131544-01	.0	.0	.0
40	6	-1.627243-02	-2.693468-01	-2.131045-01	.0	.0	.0
41	6	3.190193-02	-3.451012-01	-1.655408-01	.0	.0	.0
42	6	1.954032-02	-2.330576-01	-1.356319-01	.0	.0	.0
43	6	-3.246167-02	-2.330799-01	-2.316474-01	.0	.0	.0
44	6	-1.687229-02	-3.451223-01	-2.516757-01	.0	.0	.0

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	5.401103-03	-7.302572-03	3.2946496-04	.0	.0	.0
6	6	-1.198328-03	3.657666-03	1.294459-03	.0	.0	.0
7	6	-5.288627-03	2.283098-03	-8.827812-03	.0	.0	.0
8	6	1.006949-03	-5.926726-03	-7.830610-03	.0	.0	.0
9	6	9.659174-03	-1.808461-02	-4.933166-03	.0	.0	.0
10	6	-1.527266-03	1.446033-03	-4.146489-03	.0	.0	.0
11	6	-9.706000-03	5.158317-04	-2.264438-02	.0	.0	.0
12	6	1.154378-03	-1.711960-02	-2.184279-02	.0	.0	.0
13	6	1.310690-02	-3.283236-02	-1.440982-02	.0	.0	.0
14	6	-1.084515-03	-5.239063-03	-1.375706-02	.0	.0	.0
15	6	-1.306519-02	-5.850910-03	-4.001381-02	.0	.0	.0
16	6	5.143350-04	-3.222438-02	-3.922930-02	.0	.0	.0
17	6	1.543848-02	-5.132059-02	-2.591715-02	.0	.0	.0
18	6	7.447933-05	-1.605720-02	-2.531549-02	.0	.0	.0
19	6	-1.545040-02	-1.634617-02	-5.876828-02	.0	.0	.0
20	6	-8.602542-04	-5.099040-12	-5.815204-02	.0	.0	.0
21	6	1.666514-02	-7.308003-02	-3.832684-02	.0	.0	.0
22	6	1.823047-03	-3.097260-02	-3.760114-02	.0	.0	.0
23	6	-1.697971-02	-3.094178-02	-7.772112-02	.0	.0	.0
24	6	-2.5944162-03	-7.310096-02	-7.725040-02	.0	.0	.0
25	6	1.775880-02	-9.859499-02	-4.918683-02	.0	.0	.0
26	6	3.680367-03	-4.952760-02	-4.881749-02	.0	.0	.0
27	6	-1.813233-02	-4.954203-02	-9.508106-02	.0	.0	.0
28	6	-5.125788-03	-9.857303-02	-9.472551-02	.0	.0	.0
29	6	1.843620-02	-1.265778-01	-5.976685-02	.0	.0	.0
30	6	5.422151-03	-7.148031-02	-5.922723-02	.0	.0	.0
31	6	-1.924920-02	-7.148564-02	-1.113292-01	.0	.0	.0
32	6	-7.088307-03	-1.265547-01	-1.106230-01	.0	.0	.0
33	6	1.920476-02	-1.579131-01	-6.963489-02	.0	.0	.0
34	6	6.877025-03	-9.627356-02	-6.907696-02	.0	.0	.0
35	6	-2.027487-02	-9.628187-02	-1.262873-01	.0	.0	.0
36	6	-9.019688-03	-1.578865-01	-1.257263-01	.0	.0	.0
37	6	2.018002-02	-1.918048-01	-7.853878-02	.0	.0	.0
38	6	8.305113-03	-1.249110-01	-7.812101-02	.0	.0	.0
39	6	-2.089675-02	-1.249092-01	-1.400071-01	.0	.0	.0
40	6	-1.102624-02	-1.917804-01	-1.399702-01	.0	.0	.0
41	6	2.109892-02	-2.295506-01	-8.788693-02	.0	.0	.0
42	6	9.198828-03	-1.549945-01	-8.804872-02	.0	.0	.0
43	6	-2.143307-02	-1.550151-01	-1.519258-01	.0	.0	.0
44	6	-1.276571-02	-2.295722-01	-1.519764-01	.0	.0	.0

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	1.076420-02	-1.469579-02	6.984184-04	.0	.0	.0
6	6	-2.467121-03	7.367751-03	2.523562-03	.0	.0	.0
7	6	1.075104-02	4.565494-03	-1.780627-02	.0	.0	.0
8	6	-2.110931-03	-1.187691-02	1.580512-02	.0	.0	.0
9	6	2.004217-02	-3.636891-02	-1.029409-02	.0	.0	.0
10	6	-3.224803-03	2.881837-03	-9.697676-03	.0	.0	.0
11	6	-1.571255-02	9.756505-04	-4.584691-02	.0	.0	.0
12	6	2.496644-03	-3.439300-02	4.423597-02	.0	.0	.0
13	6	2.668493-02	-6.608486-02	-2.981716-02	.0	.0	.0
14	6	-2.413424-03	-1.062667-02	-2.849552-02	.0	.0	.0
15	6	-2.055981-02	-1.189240-02	-8.122218-02	.0	.0	.0
16	6	1.305562-03	-6.480412-02	-7.964410-02	.0	.0	.0
17	6	3.146380-02	-1.033173-01	-5.360582-02	.0	.0	.0
18	6	-1.679463-04	-3.245814-02	-5.236903-02	.0	.0	.0
19	6	-5.145681-02	-3.307480-02	-1.195619-01	.0	.0	.0
20	6	-1.359779-03	-1.025920-01	-1.185283-01	.0	.0	.0
21	6	3.400541-02	-1.471174-01	-7.937973-02	.0	.0	.0
22	6	3.253897-03	-6.251793-02	-7.792355-02	.0	.0	.0
23	6	-3.457429-02	-6.249245-02	-1.584763-01	.0	.0	.0
24	6	-5.444533-03	-1.470968-01	-1.575426-01	.0	.0	.0
25	6	3.620689-02	-1.984105-01	-1.022158-01	.0	.0	.0
26	6	6.097176-03	-9.983833-02	-1.014746-01	.0	.0	.0
27	6	-3.695942-02	-9.990059-02	-1.943624-01	.0	.0	.0
28	6	-9.722336-03	-1.983045-01	-1.936614-01	.0	.0	.0
29	6	3.767535-02	-2.546222-01	-1.246287-01	.0	.0	.0
30	6	1.031651-02	-1.439830-01	-1.235538-01	.0	.0	.0
31	6	-3.922578-02	-1.439834-01	-2.281658-01	.0	.0	.0
32	6	-1.358183-02	-2.545136-01	-2.267529-01	.0	.0	.0
33	6	3.925623-02	-5.175297-01	-1.457402-01	.0	.0	.0
34	6	1.516653-02	-1.937147-01	1.446224-01	.0	.0	.0
35	6	-4.132415-02	-1.937361-01	1.594935-01	.0	.0	.0
36	6	-1.730620-02	-3.174180-01	-2.583791-01	.0	.0	.0
37	6	4.125044-02	-3.855419-01	-1.650010-01	.0	.0	.0
38	6	1.599103-02	-2.511697-01	-1.641622-01	.0	.0	.0
39	6	-4.250644-02	-2.511627-01	-2.654251-01	.0	.0	.0
40	6	-2.139271-02	-3.854251-01	-2.683668-01	.0	.0	.0
41	6	4.382287-02	-4.612166-01	-1.611539-01	.0	.0	.0
42	6	1.775295-02	-3.115010-01	-1.615670-01	.0	.0	.0
43	6	-9.579124-02	-5.115723-01	-3.139087-01	.0	.0	.0
44	6	-2.447903-02	-4.612120-01	-3.138096-01	.0	.0	.0

INCREMENTAL STIFFNESS 50% LOADING SUBCASE 2

ELEMENT ID.	AXIAL STRESS	S T K E S S E S IN R O D SAFETY MARGIN	TORSIONAL STRESS	E L E M E N T S E S S E S IN R O D SAFETY MARGIN	E L E M E N T S ID.	AXIAL STRESS	S A F E T Y M A R G I N	T O R S I O N A L S T R E S S	S A F E T Y M A R G I N	(C T U B E) (L B S / S Q . I N .) T O R S I O N A L S T R E S S	S A F E T Y M A R G I N
1	.0		.0		2	.0		.0		.0	
3	.0		.0		4	.0		.0		.0	
5	.0		.0		6	.0		.0		.0	
7	2.513079+03	1.8+01	.0		8	-5.730164+02			6.4+01		
9	-2.414269+03	1.5+01	.0		10	5.012258+02			9.4+01		
11	-5.859145+02	3.1+01	.0		12	1.332443+03			1.7+01		
13	1.611815+03	1.4+01	.0		14	-3.826537+02			5.4+01		
15	8.024666+02	2.8+01	.0		16	-1.541390+03			1.1+01		
17	-1.789568+03	1.0+01	.0		18	5.326748+02			4.6+01		
19	2.084545+02	7.6+01	.0		20	-1.696044+02			7.6+01		
21	-1.812566+02	7.1+01	.0		22	1.472966+02			1.1+02		
23	-4.808175+02	8.4+01	.0		24	-6.584026+02			6.6+01		
25	4.690359+02	1.1+02	.0		26	6.651136+02			8.5+01		
27	5.463867-01	4.9+04	.0		28	-3.218697+00			6.6+03		
29	2.413797+03	2.1+01	.0		30	-2.070356+02			2.1+02		
31	-2.366522+03	1.8+01	.0		32	1.769000+02			3.1+02		
33	-6.684247+02	3.1+01	.0		34	1.319998+03			2.0+01		
35	1.512953+03	1.8+01	.0		36	-7.138811+02			3.1+01		
37	1.037365+03	2.5+01	.0		38	-1.686630+03			1.2+01		
39	-1.603797+03	1.4+01	.0		40	7.910505+02			3.6+01		
41	7.598144+01	2.5+02	.0		42	-1.390335+02			1.1+02		
43	-5.975171+01	2.5+02	.0		44	1.235029+02			1.5+02		
45	-4.608416+02	9.8+01	.0		46	-4.966935+02			1.0+02		
47	4.793735+02	1.2+02	.0		48	4.883556+02			1.4+02		
49	-3.075134+00	8.1+03	.0		50	-1.661591+00			1.5+04		
51	2.184587+03	2.8+01	.0		52	2.079078+02			3.0+02		
53	-2.124558+03	2.3+01	.0		54	-2.442134+02			2.1+02		
55	-7.234236+02	3.4+01	.0		56	1.432937+03			2.1+01		
57	1.494955+03	2.1+01	.0		58	-8.918735+02			2.9+01		
59	1.129940+03	2.7+01	.0		60	-1.832963+03			1.3+01		
61	-1.602566+03	1.6+01	.0		62	9.795283+02			3.4+01		
63	8.157941+01	2.7+02	.0		64	-1.501217+02			1.2+02		
65	-7.891406+01	2.2+02	.0		66	1.514687+02			1.4+02		
67	-5.353593+02	1.0+02	.0		68	-3.395662+02			1.8+02		
69	5.243415+02	1.3+02	.0		70	3.491517+02			2.3+02		
71	-1.054932+00	2.8+04	.0		72	-5.177612-01			5.7+04		
73	1.925554+03	3.7+01	.0		74	6.610580+02			1.1+02		
75	-1.867392+03	3.1+01	.0		76	-6.992236+02			8.4+01		
77	-7.868762+02	3.6+01	.0		78	1.550012+03			2.3+01		
79	1.496589+03	2.5+01	.0		80	-1.108003+03			2.7+01		
81	1.216079+03	2.9+01	.0		82	-1.979198+03			1.4+01		
83	-1.593301+03	1.9+01	.0		84	1.197457+03			3.2+01		
85	9.551375+01	2.7+02	.0		86	-1.611028+02			1.3+02		
87	-8.889575+01	2.3+02	.0		88	1.533651+02			1.7+02		
89	-5.662751+02	1.1+02	.0		90	-1.992517+02			3.5+02		

BRUSS FAIL GOOD ADULT1 **A 226 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 50 X LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ROU SAFETY MARGIN	E L E M E N T S E L E M E N T I D.	A X I A L S T R E S S		(C T U B E) (L B S / S Q . I N .)		S A F E T Y M A R G I N	
	AXIAL STRESS	MARGIN	TORSIONAL STRESS	MARGIN			AXIAL STRESS	MARGIN	TORSIONAL STRESS	MARGIN		
91	5.707593+02	1.4+02	.0	.0	92	1.784789+02	5.2+02	.0	.0	94	1.784789+02	5.2+02
93	-6.337794+00	3.3+03	.0	.0	94	-9.831348-01	3.5+04	.0	.0	96	-9.831348-01	3.5+04
95	1.851550+05	3.1+01	.0	.0	96	1.144083+03	7.5+01	.0	.0	98	1.144083+03	7.5+01
97	-1.590996+03	4.2+01	.0	.0	98	-1.171246+03	5.8+01	.0	.0	100	-1.171246+03	5.8+01
99	-8.686906+02	3.9+01	.0	.0	100	1.678153+03	2.5+01	.0	.0	102	1.678153+03	2.5+01
101	1.479375+03	3.0+01	.0	.0	102	-1.327839+03	2.7+01	.0	.0	104	-1.327839+03	2.7+01
103	1.325091+05	3.2+01	.0	.0	104	-2.147634+03	1.5+01	.0	.0	106	-2.147634+03	1.5+01
105	-1.586368+03	2.2+01	.0	.0	106	1.427854+03	3.2+01	.0	.0	108	1.427854+03	3.2+01
107	9.443364+01	3.2+02	.0	.0	108	-1.773944+02	1.3+02	.0	.0	110	-1.773944+02	1.3+02
109	-8.870654+01	2.7+02	.0	.0	110	1.614818+02	1.8+02	.0	.0	112	1.614818+02	1.8+02
111	-6.056536+02	1.2+02	.0	.0	112	1.373535+01	7.6+03	.0	.0	114	1.373535+01	7.6+03
113	6.023530+02	1.6+02	.0	.0	114	-2.060889+01	4.2+03	.0	.0	116	-2.060889+01	4.2+03
115	-4.101563-01	9.8+04	.0	.0	116	-4.515991+00	8.8+03	.0	.0	118	-4.515991+00	8.8+03
117	1.562786+05	6.4+01	.0	.0	118	1.439171+03	6.9+01	.0	.0	120	1.439171+03	6.9+01
119	-1.518171+05	5.2+01	.0	.0	120	-1.490877+03	5.3+01	.0	.0	122	-1.490877+03	5.3+01
121	-1.174221+05	3.3+01	.0	.0	122	2.068227+03	2.3+01	.0	.0	124	2.068227+03	2.3+01
123	1.530281+05	3.4+01	.0	.0	124	-1.502105+03	2.7+01	.0	.0	126	-1.502105+03	2.7+01
125	1.175899+03	4.2+01	.0	.0	126	-2.059461+03	1.9+01	.0	.0	128	-2.059461+03	1.9+01
127	-1.637135+03	2.5+01	.0	.0	128	1.610426+03	3.3+01	.0	.0	130	1.610426+03	3.3+01
129	-3.067359+01	9.1+02	.0	.0	130	-4.572046+01	6.1+02	.0	.0	132	-4.572046+01	6.1+02
131	4.156123+01	8.5+02	.0	.0	132	3.908972+01	9.0+02	.0	.0	134	3.908972+01	9.0+02
133	-6.649360+02	1.3+02	.0	.0	134	-1.547363+01	6.2+03	.0	.0	136	-1.547363+01	6.2+03
135	6.554028+02	1.7+02	.0	.0	136	1.045361+01	1.2+04	.0	.0	138	1.045361+01	1.2+04
137	-1.225633+01	3.9+03	.0	.0	138	4.610547+00	1.2+04	.0	.0	140	4.610547+00	1.2+04
139	1.706793+05	8.8+01	.0	.0	140	1.561146+03	7.3+01	.0	.0	142	1.561146+03	7.3+01
141	-1.635831+05	5.6+01	.0	.0	142	-1.619312+03	5.7+01	.0	.0	144	-1.619312+03	5.7+01
143	-1.829424+05	3.5+01	.0	.0	144	2.249318+03	2.5+01	.0	.0	146	2.249318+03	2.5+01
145	1.640231+03	3.7+01	.0	.0	146	-1.619726+03	3.0+01	.0	.0	148	-1.619726+03	3.0+01
147	1.286183+03	4.4+01	.0	.0	148	-2.251420+03	2.0+01	.0	.0	150	-2.251420+03	2.0+01
149	-1.778448+05	2.7+01	.0	.0	150	1.756503+03	3.5+01	.0	.0	152	1.756503+03	3.5+01
151	-4.603125+01	7.0+02	.0	.0	152	-5.609705+01	5.7+02	.0	.0	154	-5.609705+01	5.7+02
153	5.495215+04	7.5+02	.0	.0	154	4.388464+01	9.2+02	.0	.0	156	4.388464+01	9.2+02
155	-7.303437+02	1.4+02	.0	.0	156	-1.782715+01	6.5+03	.0	.0	158	-1.782715+01	6.5+03
157	7.255484+02	1.8+02	.0	.0	158	4.179199+00	3.6+04	.0	.0	160	4.179199+00	3.6+04
159	3.785156+00	1.3+04	.0	.0	160	-1.290527+01	4.2+03	.0	.0	162	-1.290527+01	4.2+03
161	1.971223+05	7.1+01	.0	.0	162	1.672579+03	8.1+01	.0	.0	164	1.672579+03	8.1+01
163	-1.750305+05	6.1+01	.0	.0	164	-1.781577+03	6.0+01	.0	.0	166	-1.781577+03	6.0+01
165	1.895871+05	3.8+01	.0	.0	166	2.467049+03	2.7+01	.0	.0	168	2.467049+03	2.7+01
167	-1.722514+05	4.0+01	.0	.0	168	-1.754500+03	3.2+01	.0	.0	170	-1.754500+03	3.2+01
169	1.400972+05	4.7+01	.0	.0	170	-2.466527+03	2.1+01	.0	.0	172	-2.466527+03	2.1+01
171	-1.829952+05	3.0+01	.0	.0	172	1.906596+03	3.8+01	.0	.0	174	1.906596+03	3.8+01
173	3.214169+01	1.2+03	.0	.0	174	-6.097119+01	6.3+02	.0	.0	176	-6.097119+01	6.3+02
175	5.655127+01	6.5+02	.0	.0	176	5.238524+01	1.5+03	.0	.0	178	5.238524+01	1.5+03
177	-7.390285+02	1.0+02	.0	.0	178	-2.232422+01	4.1+03	.0	.0	180	-2.232422+01	4.1+03
179	7.912764+02	1.0+02	.0	.0	180	7.098635+00	2.5+04	.0	.0			

DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 50 X LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	IN SAFETY MARGIN	K U D SAFETY MARGIN	E L E M E N T S	E L E M E N T S	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SUBCASE 2
181	1.81499414J1	4.4+03	.0	162	182	AXIAL STRESS	AXIAL STRESS	-2.389746+01	2.7+03	.0	
183	2.137536+03	7.4+01	.0	184	184	TORSIONAL STRESS	TORSIONAL STRESS	1.756927+03	8.9+01	.0	
185	-1.812439+03	6.9+01	.0	186	186	AXIAL STRESS	AXIAL STRESS	-2.034296+03	6.2+01	.0	
187	-1.584130+03	3.3+01	.0	188	188	TORSIONAL STRESS	TORSIONAL STRESS	2.716524+03	2.8+01	.0	
189	1.484613+03	4.5+01	.0	190	190	AXIAL STRESS	AXIAL STRESS	-1.823012+03	3.7+01	.0	
191	1.583730+03	4.9+01	.0	192	192	TORSIONAL STRESS	TORSIONAL STRESS	-2.729661+03	1.5+01	.0	
193	-1.795350+03	3.4+01	.0	194	194	AXIAL STRESS	AXIAL STRESS	1.967314+03	4.3+01	.0	
195	1.671672+01	3.3+03	.0	196	196	TORSIONAL STRESS	TORSIONAL STRESS	-1.419800+02	3.1+02	.0	
197	1.233525+02	4.3+02	.0	198	198	AXIAL STRESS	AXIAL STRESS	-2.707178+01	1.7+03	.0	
199	-8.801348+02	1.5+02	.0	200	200	TORSIONAL STRESS	TORSIONAL STRESS	-2.213672+01	7.2+03	.0	
201	8.631416+02	2.0+02	.0	202	202	AXIAL STRESS	AXIAL STRESS	-1.625000+00	1.0+05	.0	
203	6.003320+01	1.6+03	.0	204	204	TORSIONAL STRESS	TORSIONAL STRESS	-7.946729+01	9.4+02	.0	
205	2.477946+03	7.3+01	.0	206	206	AXIAL STRESS	AXIAL STRESS	1.584727+03	1.2+02	.0	
207	-1.691239+03	8.7+01	.0	208	208	TORSIONAL STRESS	TORSIONAL STRESS	-2.425800+03	5.9+01	.0	
209	-1.428569+03	5.0+01	.0	210	210	AXIAL STRESS	AXIAL STRESS	-2.849251+03	3.2+01	.0	
211	2.229136+03	4.4+01	.0	212	212	TORSIONAL STRESS	TORSIONAL STRESS	-2.205611+03	5.5+01	.0	
213	1.481186+03	5.2+01	.0	214	214	AXIAL STRESS	AXIAL STRESS	-2.823113+03	2.5+01	.0	
215	-2.525636+03	3.4+01	.0	216	216	TORSIONAL STRESS	TORSIONAL STRESS	2.295219+03	4.4+01	.0	
217	-5.131152+02	1.0+02	.0	218	218	AXIAL STRESS	AXIAL STRESS	3.121401+02	2.1+02	.0	
219	-2.919414+02	1.0+02	.0	220	220	TORSIONAL STRESS	TORSIONAL STRESS	5.358247+02	1.2+02	.0	
221	-4.353975+02	3.7+02	.0	222	222	AXIAL STRESS	AXIAL STRESS	1.140039+01	2.1+04	.0	
223	5.359141+02	3.7+02	.0	224	224	TORSIONAL STRESS	TORSIONAL STRESS	2.076758+01	1.2+04	.0	
225	-1.710363+03	5.0+01	.0	226	226	AXIAL STRESS	AXIAL STRESS	1.780122+03	6.1+01	.0	

TRUSS TAIL BOOM MODEL 1 ***A 226 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 75 % LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	IN R O J SAFETY MARGIN	E L E M E N T S E S I N R O J SAFETY MARGIN	E L E M E N T S ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	(C T U B E) (L B S / S Q . I N .) SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
91	8.563584+02	9.3+01	.0			92	2.766646+02	3.3+02	.0			
93	-1.211914+01	2.6+03	.0			94	-3.129639+00	1.1+04	.0			
95	2.508874+03	5.3+01	.0			96	1.6539946+03	5.0+01	.0			
97	-2.413285+03	2.8+01	.0			98	-1.730121+03	3.9+01	.0			
99	-1.294235+03	2.6+01	.0			100	2.522539+03	1.6+01	.0			
101	2.231884+03	1.9+01	.0			102	-1.989594+03	1.7+01	.0			
103	1.992042+03	2.1+01	.0			104	-3.226106+03	9.8+00	.0			
105	-2.390769+03	1.5+01	.0			106	2.134958+03	2.1+01	.0			
107	1.420098+02	2.1+02	.0			108	-2.657906+02	9.0+01	.0			
109	-1.348865+02	1.6+02	.0			110	2.409902+02	1.2+02	.0			
111	-9.100669+02	6.2+01	.0			112	5.246094+00	2.0+04	.0			
113	9.024551+02	1.0+02	.0			114	-2.187427+01	4.0+03	.0			
115	-2.819824+00	1.4+04	.0			116	-8.940918+00	4.5+03	.0			
117	2.374544+03	4.2+01	.0			118	2.133775+03	4.6+01	.0			
119	-2.303337+03	3.4+01	.0			120	-2.207244+03	3.6+01	.0			
121	-1.765076+03	2.2+01	.0			122	3.107073+03	1.5+01	.0			
123	2.308205+03	2.2+01	.0			124	-2.249587+03	1.8+01	.0			
125	1.768982+03	2.8+01	.0			126	-3.094152+03	1.2+01	.0			
127	-2.469725+03	1.6+01	.0			128	2.410490+03	2.2+01	.0			
129	-4.649414+01	6.0+02	.0			130	-6.978052+01	4.0+02	.0			
131	6.114600+01	5.7+02	.0			132	5.817676+01	6.0+02	.0			
133	-9.393750+02	8.6+01	.0			134	-3.957324+01	2.4+03	.0			
135	9.816182+02	1.1+02	.0			136	2.472119+01	5.2+03	.0			
137	-2.102051+01	2.2+03	.0			138	4.619629+00	1.3+04	.0			
139	2.591447+03	4.4+01	.0			140	2.316407+03	4.9+01	.0			
141	-2.879947+03	3.6+01	.0			142	-2.398841+03	3.8+01	.0			
143	-1.930448+03	2.3+01	.0			144	3.379048+03	1.7+01	.0			
145	2.473710+03	2.4+01	.0			146	-2.426299+03	2.0+01	.0			
147	1.935244+03	2.9+01	.0			148	-3.362723+03	1.3+01	.0			
149	-2.682609+03	1.6+01	.0			150	2.629799+03	2.3+01	.0			
151	-6.953961+01	4.6+02	.0			152	-8.861548+01	3.7+02	.0			
153	8.039730+01	5.1+02	.0			154	6.537671+01	6.2+02	.0			
155	-1.099455+03	9.2+01	.0			156	-4.418750+01	2.6+03	.0			
157	1.086801+03	1.2+02	.0			158	1.495410+01	1.0+04	.0			
159	2.578125+00	2.7+04	.0			160	-2.239502+01	2.4+03	.0			
161	2.839501+03	4.8+01	.0			162	2.483339+03	5.4+01	.0			
163	-2.651632+03	4.0+01	.0			164	-2.641626+03	4.0+01	.0			
165	-2.097823+03	2.5+01	.0			166	3.705879+03	1.8+01	.0			
167	2.672932+03	2.6+01	.0			168	-2.628769+03	2.1+01	.0			
169	1.945747+03	3.1+01	.0			170	-3.706188+03	1.4+01	.0			
171	-2.310716+03	1.9+01	.0			172	2.855780+03	2.5+01	.0			
173	-4.852865+01	7.7+02	.0			174	-9.324605+01	4.1+02	.0			
175	8.232444+01	9.7+02	.0			176	4.832275+01	9.4+02	.0			
177	-1.133227+03	4.1+01	.0			178	-5.191465+01	2.6+03	.0			
179	1.135654+03	1.6+02	.0			180	1.855664+01	9.5+03	.0			

INCREMENTAL STIFFNESS 75 X LOADING SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ROD SAFETY MARGIN	ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
	STRESS	SAFETY MARGIN	STRESS	SAFETY MARGIN			STRESS	SAFETY MARGIN	STRESS	SAFETY MARGIN			
1	.0		.0			2	.0		.0			.0	
3	.0		.0			4	.0		.0			.0	
5	.0		.0			6	.0		.0			.0	
7	3.797476+05	1.2+01	.0			8	-8.752129+02	4.2+01	.0			.0	
9	-3.647329+05	4.5+00	.0			10	7.688577+02	6.1+01	.0			.0	
11	-8.811505+02	2.0+01	.0			12	2.004681+03	1.1+01	.0			.0	
13	2.424357+05	9.0+00	.0			14	-5.672701+02	3.4+01	.0			.0	
15	1.203531+05	1.0+01	.0			16	-2.315942+03	7.2+00	.0			.0	
17	-2.697972+05	6.3+00	.0			18	7.952058+02	3.0+01	.0			.0	
19	3.125762+02	5.1+01	.0			20	-2.557945+02	5.0+01	.0			.0	
21	-2.727964+02	4.7+01	.0			22	2.223576+02	7.1+01	.0			.0	
23	-7.254938+02	5.5+01	.0			24	-9.995728+02	4.3+01	.0			.0	
25	7.043995+02	7.1+01	.0			26	1.007280+03	5.6+01	.0			.0	
27	-1.736420+00	1.2+04	.0			28	-5.503544+00	3.9+03	.0			.0	
29	3.652574+03	1.4+01	.0			30	-3.266145+02	1.3+02	.0			.0	
31	-3.573677+05	1.1+01	.0			32	2.842719+02	1.9+02	.0			.0	
33	-1.004693+05	2.1+01	.0			34	1.985396+03	1.3+01	.0			.0	
35	2.279516+03	1.1+01	.0			36	-1.065935+03	2.0+01	.0			.0	
37	1.557409+05	1.6+01	.0			38	-2.535160+03	7.7+00	.0			.0	
39	-2.417395+05	0.6+00	.0			40	1.183270+03	2.4+01	.0			.0	
41	1.121420+02	1.7+02	.0			42	-2.088716+02	7.2+01	.0			.0	
43	-9.013721+01	1.7+02	.0			44	1.856157+02	1.0+02	.0			.0	
45	-7.258307+02	6.5+01	.0			46	-7.577074+02	6.7+01	.0			.0	
47	7.206125+02	8.2+01	.0			48	7.415224+02	8.9+01	.0			.0	
49	-7.169678+00	3.5+03	.0			50	-3.266418+00	7.7+03	.0			.0	
51	3.310092+05	1.8+01	.0			52	2.949982+02	2.1+02	.0			.0	
53	-3.216269+05	1.5+01	.0			54	-3.460582+02	1.5+02	.0			.0	
55	-1.087029+05	2.2+01	.0			56	2.155097+03	1.4+01	.0			.0	
57	2.253595+05	1.4+01	.0			58	-1.333581+03	1.9+01	.0			.0	
59	1.690990+05	1.8+01	.0			60	-2.754711+03	8.3+00	.0			.0	
61	-2.415609+05	1.0+01	.0			62	1.464707+03	2.2+01	.0			.0	
63	1.212932+02	1.8+02	.0			64	-2.253537+02	7.8+01	.0			.0	
65	-1.193195+02	1.5+02	.0			66	2.272993+02	9.6+01	.0			.0	
67	-8.077521+02	6.7+01	.0			68	-5.228784+02	1.2+02	.0			.0	
69	7.874292+02	8.7+01	.0			70	5.327816+02	1.5+02	.0			.0	
71	-4.089111+00	7.2+03	.0			72	-1.989929+00	1.5+04	.0			.0	
73	2.921486+05	2.4+01	.0			74	9.727913+02	7.6+01	.0			.0	
75	-2.829970+05	2.0+01	.0			76	-1.026086+03	5.7+01	.0			.0	
77	-1.182678+03	2.4+01	.0			78	2.330633+03	1.5+01	.0			.0	
79	2.257688+05	1.6+01	.0			80	-1.658812+03	1.8+01	.0			.0	
81	1.827187+05	1.9+01	.0			82	-2.973885+03	9.1+00	.0			.0	
83	-2.404586+05	1.2+01	.0			84	1.790767+03	2.1+01	.0			.0	
85	1.428909+02	1.8+02	.0			86	-2.416179+02	8.5+01	.0			.0	
87	-1.347888+02	1.5+02	.0			88	-2.295203+02	1.1+02	.0			.0	
89	-8.530154+02	7.4+01	.0			90	-3.135308+02	2.3+02	.0			.0	

TRUSS TAIL BOOM MODEL 1 **A 226 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 100% LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		R U D SAFETY MARGIN	E L E M E N T S ELEMENT ID.	A X I A L S T R E S S		S A F E T Y M A R G I N		S A F E T Y M A R G I N
	STRESS	MARGIN	STRESS	MARGIN			STRESS	MARGIN	STRESS	MARGIN	
1	.0		.0			2	.0				
3	.0		.0			4	.0				
5	.0		.0			6	.0				
7	5.101056+03	3.3+00	.0			8	-1.187582+03	3.1+01			
9	-4.898210+03	6.7+00	.0			10	1.047549+03	4.4+01			
11	-1.177830+03	1.5+01	.0			12	2.681167+03	7.9+00			
13	3.252208+03	6.5+00	.0			14	-7.473961+02	2.5+01			
15	1.604378+03	1.4+01	.0			16	-3.093311+03	5.1+00			
17	-3.515645+03	4.5+00	.0			18	1.055270+03	2.3+01			
19	4.166331+02	3.5+01	.0			20	-3.429081+02	3.7+01			
21	-3.649494+02	3.5+01	.0			22	2.983596+02	5.3+01			
23	-9.740558+02	4.1+01	.0			24	-1.348798+03	3.2+01			
25	9.404948+02	5.3+01	.0			26	1.355931+03	4.1+01			
27	-5.761383+00	3.7+03	.0			28	-8.237411+00	2.6+03			
29	4.913271+03	1.0+01	.0			30	-4.565922+02	9.5+01			
31	-4.810716+03	8.1+00	.0			32	4.039727+02	1.3+02			
33	-1.342313+03	1.5+01	.0			34	2.654633+03	9.4+00			
35	3.952952+03	8.3+00	.0			36	-1.414921+03	1.5+01			
37	2.073325+03	1.2+01	.0			38	-3.387421+03	5.5+00			
39	-3.233969+03	6.2+00	.0			40	1.573366+03	1.6+01			
41	1.471295+02	1.3+02	.0			42	-2.789336+02	5.3+01			
43	-1.208662+02	1.2+02	.0			44	2.479878+02	7.5+01			
45	-9.740884+02	4.6+01	.0			46	-1.027256+03	4.9+01			
47	9.630522+02	6.1+01	.0			48	1.000748+03	6.6+01			
49	-1.301125+01	1.9+03	.0			50	-5.386261+00	4.6+03			
51	4.459414+03	1.3+01	.0			52	3.711416+02	1.7+02			
53	-4.323220+03	1.1+01	.0			54	-4.346582+02	1.2+02			
55	-1.451903+03	1.6+01	.0			56	2.881327+03	1.0+01			
57	3.019464+03	1.0+01	.0			58	-1.772530+03	1.4+01			
59	2.257431+03	1.3+01	.0			60	-3.680252+03	6.0+00			
61	-3.235694+03	7.0+00	.0			62	1.946927+03	1.7+01			
63	1.602610+02	1.4+02	.0			64	-3.007039+02	5.8+01			
65	-1.603645+02	1.1+02	.0			66	3.032131+02	7.2+01			
67	-1.093105+03	3.0+01	.0			68	-7.153066+02	8.4+01			
69	1.051694+03	6.5+01	.0			70	7.225172+02	1.1+02			
71	-8.635670+00	3.0+03	.0			72	-4.268860+00	6.9+03			
73	3.940152+03	1.3+01	.0			74	1.272265+03	5.8+01			
75	-3.123399+03	1.5+01	.0			76	-1.336010+03	4.3+01			
77	-1.580104+03	1.3+01	.0			78	3.115316+03	1.1+01			
79	3.027587+03	1.2+01	.0			80	-2.027601+03	1.3+01			
81	2.440401+03	1.4+01	.0			82	-3.972358+03	6.6+00			
83	-3.221572+03	1.3+01	.0			84	2.340555+03	1.6+01			
85	1.499873+02	1.3+02	.0			86	-3.221087+02	8.3+01			
87	-1.315553+02	1.1+02	.0			88	0.050400+02	8.3+01			
89	-1.142335+03	3.0+01	.0			90	-0.376880+02	1.6+02			

SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS	
	SAFETY MARGIN	STRESS	SAFETY MARGIN	STRESS		SAFETY MARGIN	STRESS	SAFETY MARGIN	STRESS		SAFETY MARGIN	STRESS	SAFETY MARGIN	STRESS
181	3.3+03	2.335504+J1	3.3+03	-3.897070+01	182	3.3+03	-3.897070+01	3.3+03	2.611281+03	184	3.3+03	2.611281+03	3.3+03	2.611281+03
183	4.5+01	3.253317+03	4.5+01	2.611281+03	184	4.5+01	2.611281+03	4.5+01	-3.018602+03	186	4.5+01	-3.018602+03	4.5+01	-3.018602+03
185	4.5+01	-2.744052+03	4.5+01	4.079821+03	186	4.5+01	4.079821+03	4.5+01	4.079821+03	188	4.5+01	4.079821+03	4.5+01	4.079821+03
187	2.6+01	-2.388807+03	2.6+01	-2.732912+03	188	2.6+01	-2.732912+03	2.6+01	-4.101758+03	190	2.6+01	-4.101758+03	2.6+01	-4.101758+03
189	3.0+01	2.780331+03	3.0+01	2.946871+03	190	3.0+01	2.946871+03	3.0+01	2.946871+03	194	3.0+01	2.946871+03	3.0+01	2.946871+03
191	3.2+01	2.382835+03	3.2+01	-2.158149+02	194	3.2+01	-2.158149+02	3.2+01	-4.125977+01	196	3.2+01	-4.125977+01	3.2+01	-4.125977+01
193	2.2+01	-3.009968+03	2.2+01	-5.622070+01	196	2.2+01	-5.622070+01	2.2+01	3.316406+00	198	2.2+01	3.316406+00	2.2+01	3.316406+00
195	2.3+03	2.414355+01	2.3+03	-1.261562+02	198	2.3+03	-1.261562+02	2.3+03	2.346828+03	200	2.3+03	2.346828+03	2.3+03	2.346828+03
197	2.9+02	1.903701+02	2.9+02	3.164060+00	200	2.9+02	3.164060+00	2.9+02	-3.613542+03	202	2.9+02	-3.613542+03	2.9+02	-3.613542+03
199	1.0+02	-1.326468+03	1.0+02	4.286477+03	202	1.0+02	4.286477+03	1.0+02	4.286477+03	204	1.0+02	4.286477+03	1.0+02	4.286477+03
201	1.3+02	1.253867+03	1.3+02	-3.3066238+03	204	1.3+02	-3.3066238+03	1.3+02	-4.236790+03	206	1.3+02	-4.236790+03	1.3+02	-4.236790+03
203	1.1+03	8.250741+01	1.1+03	3.435506+03	206	1.1+03	3.435506+03	1.1+03	4.720903+02	208	1.1+03	4.720903+02	1.1+03	4.720903+02
205	4.8+01	3.740170+03	4.8+01	8.071997+02	208	4.8+01	8.071997+02	4.8+01	2.096875+01	210	4.8+01	2.096875+01	4.8+01	2.096875+01
207	5.7+01	-2.559798+03	5.7+01	2.453906+01	210	5.7+01	2.453906+01	5.7+01	4.253906+01	212	5.7+01	4.253906+01	5.7+01	4.253906+01
209	5.5+01	-2.140976+03	5.5+01	2.691182+03	212	5.5+01	2.691182+03	5.5+01	2.691182+03	214	5.5+01	2.691182+03	5.5+01	2.691182+03
211	2.9+01	3.559104+03	2.9+01	2.691182+03	214	2.9+01	2.691182+03	2.9+01	2.691182+03	216	2.9+01	2.691182+03	2.9+01	2.691182+03
213	4.0+01	2.209187+03	4.0+01	2.691182+03	216	4.0+01	2.691182+03	4.0+01	2.691182+03	218	4.0+01	2.691182+03	4.0+01	2.691182+03
215	2.2+01	-3.503229+03	2.2+01	2.691182+03	218	2.2+01	2.691182+03	2.2+01	2.691182+03	220	2.2+01	2.691182+03	2.2+01	2.691182+03
217	6.7+01	-7.655715+02	6.7+01	2.691182+03	220	6.7+01	2.691182+03	6.7+01	2.691182+03	222	6.7+01	2.691182+03	6.7+01	2.691182+03
219	1.2+02	-4.315557+02	1.2+02	2.691182+03	222	1.2+02	2.691182+03	1.2+02	2.691182+03	224	1.2+02	2.691182+03	1.2+02	2.691182+03
221	2.6+02	-6.109180+02	2.6+02	2.691182+03	224	2.6+02	2.691182+03	2.6+02	2.691182+03	226	2.6+02	2.691182+03	2.6+02	2.691182+03
223	2.3+02	8.452617+02	2.3+02	2.691182+03	226	2.3+02	2.691182+03	2.3+02	2.691182+03					
225	3.4+01	-2.533213+03	3.4+01	2.691182+03										

TRUSS TAIL BOOM MODEL **A 226 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 10

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	STRESSES IN ROD SAFETY MARGIN	ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	(C T U B E) (L B S / S Q . I N .)	TORSIONAL STRESS	SAFETY MARGIN
181	2.753320+J1	2.9+03	.0	182	-5.611230+01	1.1+03		.0	
183	4.363463+03	3.6+01	.0	184	3.449622+03	4.5+01		.0	
185	-3.692930+03	3.3+01	.0	186	-3.980987+03	3.1+01		.0	
187	-3.189072+03	1.9+01	.0	188	5.447357+03	1.4+01		.0	
189	3.726840+03	2.2+01	.0	190	-3.642287+03	1.8+01		.0	
191	3.187260+03	2.4+01	.0	192	-5.479344+03	7.2+00		.0	
193	-4.036521+03	1.6+01	.0	194	3.924226+03	2.1+01		.0	
195	3.050977+01	1.8+03	.0	196	-2.915430+02	1.5+02		.0	
197	2.502441+02	2.2+02	.0	198	-5.584814+01	8.0+02		.0	
199	-1.777078+03	7.6+01	.0	200	-1.057500+02	1.5+03		.0	
201	1.710539+03	1.0+02	.0	202	1.213281+01	1.7+04		.0	
203	9.987693+01	9.4+02	.0	204	-1.774834+02	4.2+02		.0	
205	5.017898+03	3.5+01	.0	206	3.088778+03	5.9+01		.0	
207	-3.470639+03	4.2+01	.0	208	-4.784399+03	3.0+01		.0	
209	-2.852751+03	2.5+01	.0	210	5.732853+03	1.5+01		.0	
211	4.500035+03	2.1+01	.0	212	-4.406020+03	1.7+01		.0	
213	2.966884+03	3.0+01	.0	214	-5.652594+03	1.2+01		.0	
215	-4.704664+03	1.5+01	.0	216	4.571439+03	2.2+01		.0	
217	-1.009607+03	3.0+01	.0	218	6.345557+02	1.0+02		.0	
219	-5.663241+02	7.2+01	.0	220	1.080805+03	5.9+01		.0	
221	-7.591074+02	4.1+02	.0	222	3.311719+01	7.2+03		.0	
223	1.185168+03	1.7+02	.0	224	7.192578+01	3.4+03		.0	
225	-3.333855+03	2.5+01	.0	226	3.615910+03	2.9+01		.0	

* 85.1 CPU-S 320.6 COR-S 577 ELP-S. 158. OFF END
 * 65.2 CPU-S 320.6 COR-S 577 ELP-S. 179. EXIT BEGN

*** END OF JOB ***

SUBCASE 2

INCREMENTAL STIFFNESS 100% LOADING

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	IN TORSIONAL STRESS	R O O D SAFETY MARGIN	E L E M E N T S (C T U B E) (L B S / S Q . I N .)	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	S A F E T Y M A R G I N
91	1.143596E+03	6.9+01	.0	.0	92	3.808765E+02	2.4+02	.0	.0	
93	-1.956750E+01	1.7+03	.0	.0	94	-6.420288E+00	5.3+03	.0	.0	
95	3.587807E+03	2.4+01	.0	.0	96	2.229254E+03	3.8+01	.0	.0	
97	-3.253991E+03	2.0+01	.0	.0	98	-2.271342E+03	2.9+01	.0	.0	
99	-1.730027E+03	1.9+01	.0	.0	100	3.370831E+03	1.2+01	.0	.0	
101	2.995250E+03	1.4+01	.0	.0	102	-2.650071E+03	1.5+01	.0	.0	
103	2.662065E+03	1.3+01	.0	.0	104	-4.308036E+03	7.1+00	.0	.0	
105	-3.202899E+03	1.1+01	.0	.0	106	2.837690E+03	1.5+01	.0	.0	
107	1.693091E+02	1.6+02	.0	.0	108	-3.539541E+02	6.7+01	.0	.0	
109	-1.822925E+02	1.3+02	.0	.0	110	3.196942E+02	9.3+01	.0	.0	
111	-1.215705E+03	6.1+01	.0	.0	112	-1.357617E+01	6.2+03	.0	.0	
113	1.201986E+03	7.7+01	.0	.0	114	-1.704443E+01	5.1+03	.0	.0	
115	-6.734375E+00	6.6+03	.0	.0	116	-1.480127E+01	2.7+03	.0	.0	
117	3.207114E+03	3.6+01	.0	.0	118	2.811887E+03	3.5+01	.0	.0	
119	-3.106521E+03	2.5+01	.0	.0	120	-2.904386E+03	2.7+01	.0	.0	
121	-2.538629E+03	1.6+01	.0	.0	122	4.149485E+03	1.1+01	.0	.0	
123	3.095008E+03	1.6+01	.0	.0	124	-2.994922E+03	1.3+01	.0	.0	
125	2.565713E+03	2.0+01	.0	.0	126	-4.132564E+03	8.8+00	.0	.0	
127	-3.512031E+03	1.2+01	.0	.0	128	3.207362E+03	1.6+01	.0	.0	
129	-6.266064E+01	4.5+02	.0	.0	130	-9.464111E+01	2.9+02	.0	.0	
131	7.992236E+01	4.4+02	.0	.0	132	7.697778E+01	4.6+02	.0	.0	
133	-1.535275E+03	6.4+01	.0	.0	134	-7.468359E+01	1.3+03	.0	.0	
135	1.305969E+03	8.2+01	.0	.0	136	4.508789E+01	2.8+03	.0	.0	
137	-3.162012E+01	1.5+03	.0	.0	138	2.710937E+00	2.1+04	.0	.0	
139	3.497457E+03	3.2+01	.0	.0	140	3.054913E+03	3.7+01	.0	.0	
141	-3.342004E+03	2.7+01	.0	.0	142	-3.158396E+03	2.9+01	.0	.0	
143	-2.579676E+03	1.7+01	.0	.0	144	4.512638E+03	1.2+01	.0	.0	
145	3.316531E+03	1.9+01	.0	.0	146	-3.230994E+03	1.4+01	.0	.0	
147	2.589586E+03	2.1+01	.0	.0	148	-4.518240E+03	9.5+00	.0	.0	
149	-3.597171E+03	1.3+01	.0	.0	150	3.500107E+03	1.7+01	.0	.0	
151	-9.355957E+01	3.5+02	.0	.0	152	-1.201167E+02	2.7+02	.0	.0	
153	1.060498E+02	3.9+02	.0	.0	154	8.658984E+01	4.7+02	.0	.0	
155	-1.467650E+03	6.8+01	.0	.0	156	-8.228125E+01	1.4+03	.0	.0	
157	1.446943E+03	8.7+01	.0	.0	158	3.158301E+01	4.7+03	.0	.0	
159	-7.363281E-01	7.4+04	.0	.0	160	-3.389844E+01	1.6+03	.0	.0	
161	3.827334E+03	3.4+01	.0	.0	162	3.277151E+03	4.1+01	.0	.0	
163	-3.570811E+03	3.0+01	.0	.0	164	-3.461243E+03	3.0+01	.0	.0	
165	-2.802858E+03	1.3+01	.0	.0	166	4.948802E+03	1.3+01	.0	.0	
167	3.583319E+03	1.9+01	.0	.0	168	-3.501463E+03	1.6+01	.0	.0	
169	2.821336E+03	2.3+01	.0	.0	170	-4.950678E+03	1.0+01	.0	.0	
171	-3.902544E+03	1.4+01	.0	.0	172	3.801829E+03	1.9+01	.0	.0	
173	-6.533867E+01	5.8+02	.0	.0	174	-1.267148E+02	3.0+02	.0	.0	
175	1.090088E+02	4.5+02	.0	.0	176	6.411182E+01	7.4+02	.0	.0	
177	-1.582652E+03	7.4+01	.0	.0	178	-9.389062E+01	1.5+03	.0	.0	
179	1.579355E+03	9.2+01	.0	.0	180	3.534180E+01	5.0+03	.0	.0	

APPENDIX B

NASTRAN MATHEMATICAL MODEL OF THE UNDAMAGED
TRUSS MODEL 2 PLUS OUTPUT OF DISPLACEMENTS, STRESSES
AND MARGINS OF SAFETY DUE TO FLIGHT LOADS.

NASTRAN EXECUTIVE CONTROL DECK ECHO

ID ERLINE,MODEL2
APP DISP
\$ STATIC ANALYSIS WITH DIFFERENTIAL STIFFNESS RF 4
SOL 4.0
TIME 10
CEND

TRUSS TAIL BOOM MODEL2 **A 114 ELEMENT VERSION
DAMAGE CRITRION = NONE

OCTOBER 26. 1977 NASTRAN 7/15/77

PAGE 2

C A S E C O N T R O L D E C K E C H O

CARD
COUNT

1 TITLE = TRUSS TAIL BOOM MODEL2 **A 114 ELEMENT VERSION
2 SUBTITLE = DAMAGE CRITRION = NONE
3 OLOAD = ALL
4 SPL = 10
5 SPCFORCLS = ALL
6 DISP = ALL
7 SET 5 = 1 THRU 138
8 SUBCASE 1
9 LABEL = LINEAR CASE
10 LOAD = 11
11 SUBCASE 2
12 LABEL = INCREMENTAL STIFFNESS
13 DSCOEFFICIENT = 200
14 STRESS = 5
15 MAXLINES = 100000
16 BEGIN BULK

114

*** USER INFORMATION MESSAGE 207: BULK DATA NOT SORTED, X SORT WILL RE-ORDER DECK.

TRUSS TAIL BOOM MODEL2 **A 114 ELEMENT VERSION
DAMAGE CRITION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
1-	1	1	3	4
2-	CTUBE	2	1	4
3-	CTUBE	3	1	4
4-	CTUBE	4	3	4
5-	CTUBE	5	2	3
6-	CTUBE	6	1	3
7-	CTUBE	7	2	4
8-	CTUBE	8	1	5
9-	CTUBE	9	2	6
10-	CTUBE	10	3	7
11-	CTUBE	11	4	8
12-	CTUBE	12	5	9
13-	CTUBE	13	6	10
14-	CTUBE	14	7	11
15-	CTUBE	15	8	12
16-	CTUBE	16	9	13
17-	CTUBE	17	10	14
18-	CTUBE	18	11	15
19-	CTUBE	19	12	16
20-	CTUBE	20	13	17
21-	CTUBE	21	14	18
22-	CTUBE	22	15	19
23-	CTUBE	23	16	20
24-	CTUBE	24	17	21
25-	CTUBE	25	18	22
26-	CTUBE	26	19	23
27-	CTUBE	27	20	24
28-	CTUBE	28	21	25
29-	CTUBE	29	22	26
30-	CTUBE	30	23	27
31-	CTUBE	31	24	28
32-	CTUBE	32	25	29
33-	CTUBE	33	26	30
34-	CTUBE	34	27	31
35-	CTUBE	35	28	32
36-	CTUBE	36	29	33
37-	CTUBE	37	30	34
38-	CTUBE	38	31	35
39-	CTUBE	39	32	36
40-	CTUBE	40	33	37
41-	CTUBE	41	34	38
42-	CTUBE	42	35	39
43-	CTUBE	43	36	40
44-	CTUBE	44	37	41
45-	CTUBE	45	38	42
			39	43
			40	44
			41	45
			42	46
			43	47
			44	48
			45	49
			50	50
			51	51
			52	52
			53	53

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
46-	CTUBE	54	54	12	16						
47-	CTUBE	55	55	9	14						
48-	CTUBE	56	56	10	13						
49-	CTUBE	57	57	9	16						
50-	CTUBE	58	58	12	13						
51-	CTUBE	59	59	12	15						
52-	CTUBE	60	60	11	16						
53-	CTUBE	61	61	10	15						
54-	CTUBE	62	62	11	14						
55-	CTUBE	67	67	13	14						
56-	CTUBE	68	68	13	16						
57-	CTUBE	69	69	15	16						
58-	CTUBE	70	70	14	15						
59-	CTUBE	71	71	13	15						
60-	CTUBE	72	72	14	16						
61-	CTUBE	73	73	13	17						
62-	CTUBE	74	74	14	18						
63-	CTUBE	75	75	15	19						
64-	CTUBE	76	76	16	20						
65-	CTUBE	77	77	13	18						
66-	CTUBE	78	78	14	17						
67-	CTUBE	79	79	13	20						
68-	CTUBE	80	80	16	17						
69-	CTUBE	81	81	16	19						
70-	CTUBE	82	82	15	20						
71-	CTUBE	83	83	14	19						
72-	CTUBE	84	84	15	18						
73-	CTUBE	89	89	17	18						
74-	CTUBE	90	90	17	20						
75-	CTUBE	91	91	19	20						
76-	CTUBE	92	92	18	19						
77-	CTUBE	93	93	17	19						
78-	CTUBE	94	94	18	20						
79-	CTUBE	95	95	17	21						
80-	CTUBE	96	96	18	22						
81-	CTUBE	97	97	19	23						
82-	CTUBE	98	98	20	24						
83-	CTUBE	99	99	17	22						
84-	CTUBE	100	100	18	21						
85-	CTUBE	101	101	17	24						
86-	CTUBE	102	102	20	21						
87-	CTUBE	103	103	20	23						
88-	CTUBE	104	104	19	24						
89-	CTUBE	105	105	18	23						
90-	CTUBE	106	106	19	22						

CARD COUNT	1	2	3	4	5	6	7	8	9	10
91-	CTUBE	111	111	21	22					
92-	CTUBE	112	112	21	24					
93-	CTUBE	113	113	23	23					
94-	CTUBE	114	114	22	23					
95-	CTUBE	115	115	21	23					
96-	CTUBE	116	116	22	24					
97-	CTUBE	117	117	21	25					
98-	CTUBE	118	118	22	26					
99-	CTUBE	119	119	23	27					
100-	CTUBE	120	120	24	28					
101-	CTUBE	121	121	21	26					
102-	CTUBE	122	122	22	25					
103-	CTUBE	123	123	21	28					
104-	CTUBE	124	124	24	25					
105-	CTUBE	125	125	24	27					
106-	CTUBE	126	126	23	28					
107-	CTUBE	127	127	22	27					
108-	CTUBE	128	128	23	26					
109-	CTUBE	133	133	25	26					
110-	CTUBE	134	134	25	28					
111-	CTUBE	135	135	27	28					
112-	CTUBE	136	136	26	27					
113-	CTUBE	137	137	25	27					
114-	CTUBE	138	138	26	28					
115-	USFACT	200	1.60422	2.40632	3.20843					
116-	FORCE	11	13	0	44.2200	.0	0.0			-1.
117-	FORCE	11	14	0	44.2200	.0	0.0			-1.
118-	FORCE	11	15	0	44.2200	.0	0.0			-1.
119-	FORCE	11	16	0	44.2200	.0	0.0			-1.
120-	FORCE	11	25	0	464.5	1.	.0			.0
121-	FORCE	11	25	0	527.3	.0	-1.0			.0
122-	FORCE	11	26	0	464.5	1.0	0.0			.0
123-	FORCE	11	26	0	527.3	.0	1.0			.0
124-	FORCE	11	27	0	464.5	-1.	0.0			.0
125-	FORCE	11	27	0	527.5	.0	1.0			.0
126-	FORCE	11	28	0	464.5	-1.	.0			.0
127-	FORCE	11	28	0	527.5	.0	-1.			.0
128-	GRUSET									456
129-	GRID	1	.000	.000	11.95	12.375				
130-	GRID	2	.000	.000	11.75	-12.375				
131-	GRID	3	.000	.000	-11.75	-12.375				
132-	GRID	4	.000	.000	-11.95	12.375				
133-	GRID	5	33.5	33.5	10.656	11.105				
134-	GRID	6	33.5	33.5	10.495	-11.105				
135-	GRID	7	33.5	33.5	-10.485	-11.105				

TRUSS TAIL BUOM MODEL2 *** 114 ELEMENT VERSION
DAMAGE CRITION = VONE

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
136-	GRID	8		33.5		-10.666	11.105				
137-	GRID	9		66.5		9.401	9.855				
138-	GRID	10		66.5		9.239	-9.855				
139-	GRID	11		66.5		-9.239	-9.855				
140-	GRID	12		66.5		-9.401	9.855				
141-	GRID	13		99.5		8.136	8.604				
142-	GRID	14		99.5		7.994	-8.604				
143-	GRID	15		99.5		-7.994	-8.604				
144-	GRID	16		99.5		-8.136	8.604				
145-	GRID	17		127.5		7.063	7.543				
146-	GRID	18		127.5		6.937	-7.543				
147-	GRID	19		127.5		-6.937	-7.543				
148-	GRID	20		127.5		-7.063	7.543				
149-	GRID	21		151.5		6.143	6.634				
150-	GRID	22		151.5		151.5	-6.634				
151-	GRID	23		151.5		-6.031	-6.634				
152-	GRID	24		151.5		-6.143	6.634				
153-	GRID	25		173.5		5.3	5.8				
154-	GRID	26		173.5		5.2	-5.8				
155-	GRID	27		173.5		-5.2	-5.8				
156-	GRID	28		173.5		-5.3	5.800				
157-	MAT1	1	10.5E6	3.8E6	.33	.33	.1				+MAT001
158-	MAT1	2	4.38+04	3.51+04							+MAT002
159-	MAT1	3	10.5E6	3.8E6	.33	.33	.1				+MAT003
160-	MAT1	4	4.70+04	3.76+04							+MAT004
161-	MAT1	5	10.5E6	3.8E6	.33	.33	.1				+MAT005
162-	MAT1	6	4.38+04	3.51+04							+MAT006
163-	MAT1	7	10.5E6	3.8E6	.33	.33	.1				+MAT007
164-	MAT1	8	4.86+04	3.89+04							+MAT008
165-	MAT1	9	10.5E6	3.8E6	.33	.33	.1				+MAT009
166-	MAT1	10	2.29+04	1.83+04							+MAT010
167-	MAT1	11	10.5E6	3.8E6	.33	.33	.1				+MAT011
168-	MAT1	12	2.29+04	1.83+04							+MAT012
169-	MAT1	13	10.5E6	3.8E6	.33	.33	.1				
170-	MAT1	14	2.38+04	1.91+04							
171-	MAT1	15	10.5E6	3.8E6	.33	.33	.1				
172-	MAT1	16	2.38+04	1.91+04							
173-	MAT1	17	10.5E6	3.8E6	.33	.33	.1				
174-	MAT1	18	2.38+04	1.91+04							
175-	MAT1	19	10.5E6	3.8E6	.33	.33	.1				
176-	MAT1	20	2.38+04	1.91+04							
177-	MAT1	21	10.5E6	3.8E6	.33	.33	.1				
178-	MAT1	22	1.60+04	1.28+04							
179-	MAT1	23	10.5E6	3.8E6	.33	.33	.1				
180-	MAT1	24	1.60+04	1.28+04							

TRUSS TAIL BOOM MODEL2 ***A 114 ELEMENT VERSION
 DAMAGE CRITERION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
181-	MAT1	13	10.5E6	3.8E6	.33	.1				+MAT013
182-	+MAT013	1.64+04	1.31+04							+MAT014
183-	MAT1	14	10.5E6	3.8E6	.33	.1				+MAT015
184-	+MAT014	1.64+04	1.31+04							+MAT016
185-	MAT1	15	10.5E6	3.8E6	.33	.1				+MAT017
186-	MAT015	1.60+04	1.28+04							+MAT018
187-	MAT1	16	10.5E6	3.8E6	.33	.1				+MAT019
188-	+MAT016	1.60+04	1.28+04							+MAT020
189-	MAT1	17	10.5E6	3.8E6	.33	.1				+MAT021
190-	+MAT017	1.66+04	1.33+04							+MAT022
191-	MAT1	18	10.5E6	3.8E6	.33	.1				+MAT023
192-	+MAT018	1.66+04	1.33+04							+MAT024
193-	MAT1	19	10.5E6	3.8E6	.33	.1				+MAT025
194-	+MAT019	1.23+04	9.86+03							+MAT026
195-	MAT1	20	10.5E6	3.8E6	.33	.1				+MAT027
196-	+MAT020	1.23+04	9.87+03							+MAT028
197-	MAT1	21	10.5E6	3.8E6	.33	.1				+MAT029
198-	+MAT021	1.23+04	9.87+03							+MAT030
199-	MAT1	22	10.5E6	3.8E6	.33	.1				+MAT031
200-	+MAT022	1.23+04	9.86+03							+MAT032
201-	MAT1	23	10.5E6	3.8E6	.33	.1				+MAT033
202-	+MAT023	5.44+04	4.35+04							+MAT034
203-	MAT1	24	10.5E6	3.8E6	.33	.1				+MAT035
204-	+MAT024	5.90+04	4.72+04							
205-	MAT1	25	10.5E6	3.8E6	.33	.1				
206-	+MAT025	5.44+04	4.35+04							
207-	MAT1	26	10.5E6	3.8E6	.33	.1				
208-	+MAT026	6.10+04	4.88+04							
209-	MAT1	27	10.5E6	3.8E6	.33	.1				
210-	+MAT027	2.85+04	2.28+04							
211-	MAT1	28	10.5E6	3.8E6	.33	.1				
212-	+MAT028	2.85+04	2.28+04							
213-	MAT1	29	10.5E6	3.8E6	.33	.1				
214-	+MAT029	2.46+04	1.97+04							
215-	MAT1	30	10.5E6	3.8E6	.33	.1				
216-	+MAT030	2.46+04	1.97+04							
217-	MAT1	31	10.5E6	3.8E6	.33	.1				
218-	+MAT031	2.46+04	1.97+04							
219-	MAT1	32	10.5E6	3.8E6	.33	.1				
220-	+MAT032	2.46+04	1.97+04							
221-	MAT1	33	10.5E6	3.8E6	.33	.1				
222-	+MAT033	1.75+04	1.40+04							
223-	MAT1	34	10.5E6	3.8E6	.33	.1				
224-	+MAT034	1.75+04	1.40+04							
225-	MAT1	35	10.5E6	3.8E6	.33	.1				

TRUSS TAIL BOOM MODEL 2 **A 114 ELEMENT VERSION
DAMAGE CRITERION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
226-	+MAT035	1.80+04	1.44+04							
227-	MAT1	36	10.5E6	3.8E6	.33	.1				+MAT036
228-	+MAT036	1.80+04	1.44+04							
229-	MAT1	37	10.5E6	3.8E6	.33	.1				+MAT037
230-	+MAT037	1.75+04	1.40+04							
231-	MAT1	38	10.5E6	3.8E6	.33	.1				+MAT038
232-	+MAT038	1.75+04	1.40+04							
233-	MAT1	39	10.5E6	3.8E6	.33	.1				+MAT039
234-	+MAT039	1.81+04	1.45+04							
235-	MAT1	40	10.5E6	3.8E6	.33	.1				+MAT040
236-	+MAT040	1.81+04	1.45+04							
237-	MAT1	41	10.5E6	3.8E6	.33	.1				+MAT041
238-	+MAT041	1.39+04	1.12+04							
239-	MAT1	42	10.5E6	3.8E6	.33	.1				+MAT042
240-	+MAT042	1.40+04	1.12+04							
241-	MAT1	43	10.5E6	3.8E6	.33	.1				+MAT043
242-	+MAT043	1.40+04	1.12+04							
243-	MAT1	44	10.5E6	3.8E6	.33	.1				+MAT044
244-	+MAT044	1.39+04	1.12+04							
245-	MAT1	45	10.5E6	3.8E6	.33	.1				+MAT045
246-	+MAT045	6.91+04	5.53+04							
247-	MAT1	46	10.5E6	3.8E6	.33	.1				+MAT046
248-	+MAT046	7.59+04	6.08+04							
249-	MAT1	47	10.5E6	3.8E6	.33	.1				+MAT047
250-	+MAT047	6.91+04	5.53+04							
251-	MAT1	48	10.5E6	3.8E6	.33	.1				+MAT048
252-	+MAT048	7.86+04	6.29+04							
253-	MAT1	49	10.5E6	3.8E6	.33	.1				+MAT049
254-	+MAT049	3.65+04	2.92+04							
255-	MAT1	50	10.5E6	3.8E6	.33	.1				+MAT050
256-	+MAT050	3.65+04	2.92+04							
257-	MAT1	51	10.5E6	3.8E6	.33	.1				+MAT051
258-	+MAT051	2.46+04	1.97+04							
259-	MAT1	52	10.5E6	3.8E6	.33	.1				+MAT052
260-	+MAT052	2.46+04	1.97+04							
261-	MAT1	53	10.5E6	3.8E6	.33	.1				+MAT053
262-	+MAT053	2.46+04	1.97+04							
263-	MAT1	54	10.5E6	3.8E6	.33	.1				+MAT054
264-	+MAT054	2.46+04	1.97+04							
265-	MAT1	55	10.5E6	3.8E6	.33	.1				+MAT055
266-	+MAT055	1.87+04	1.50+04							
267-	MAT1	56	10.5E6	3.8E6	.33	.1				+MAT056
268-	+MAT056	1.88+04	1.50+04							
269-	MAT1	57	10.5E6	3.8E6	.33	.1				+MAT057
270-	+MAT057	1.92+04	1.54+04							

S O R T E D B U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
271-	MAT1	58	10.5E6	3.8E6	.33	.1					+MAT058
272-	+MAT058	1.92+04	1.54+04								+MAT059
273-	MAT1	59	10.5E6	3.8E6	.33	.1					+MAT060
274-	+MAT059	1.87+04	1.50+04								+MAT061
275-	MAT1	60	10.5E6	3.8E6	.33	.1					+MAT062
276-	+MAT060	1.88+04	1.50+04								+MAT063
277-	MAT1	61	10.5E6	3.8E6	.33	.1					+MAT064
278-	+MAT061	1.93+04	1.55+04								+MAT065
279-	MAT1	62	10.5E6	3.8E6	.33	.1					+MAT066
280-	+MAT062	1.93+04	1.55+04								+MAT067
281-	MAT1	63	10.5E6	3.8E6	.33	.1					+MAT068
282-	+MAT063	1.55+04	1.24+04								+MAT069
283-	MAT1	64	10.5E6	3.8E6	.33	.1					+MAT070
284-	+MAT064	1.55+04	1.24+04								+MAT071
285-	MAT1	65	10.5E6	3.8E6	.33	.1					+MAT072
286-	+MAT065	1.55+04	1.24+04								+MAT073
287-	MAT1	66	10.5E6	3.8E6	.33	.1					+MAT074
288-	+MAT066	1.55+04	1.24+04								+MAT075
289-	MAT1	67	10.5E6	3.8E6	.33	.1					+MAT076
290-	+MAT067	9.06+04	7.25+04								+MAT077
291-	MAT1	68	10.5E6	3.8E6	.33	.1					+MAT078
292-	+MAT068	1.01+05	8.11+04								+MAT079
293-	MAT1	69	10.5E6	3.8E6	.33	.1					+MAT080
294-	+MAT069	9.06+04	7.25+04								
295-	MAT1	70	10.5E6	3.8E6	.33	.1					
296-	+MAT070	1.05+05	8.40+04								
297-	MAT1	71	10.5E6	3.8E6	.33	.1					
298-	+MAT071	4.82+04	3.86+04								
299-	MAT1	72	10.5E6	3.8E6	.33	.1					
300-	+MAT072	4.82+04	3.86+04								
301-	MAT1	73	10.5E6	3.8E6	.33	.1					
302-	+MAT073	3.41+04	2.73+04								
303-	MAT1	74	10.5E6	3.8E6	.33	.1					
304-	+MAT074	3.41+04	2.73+04								
305-	MAT1	75	10.5E6	3.8E6	.33	.1					
306-	+MAT075	3.41+04	2.73+04								
307-	MAT1	76	10.5E6	3.8E6	.33	.1					
308-	+MAT076	3.41+04	2.73+04								
309-	MAT1	77	10.5E6	3.8E6	.33	.1					
310-	+MAT077	2.57+04	2.05+04								
311-	MAT1	78	10.5E6	3.8E6	.33	.1					
312-	+MAT078	2.57+04	2.05+04								
313-	MAT1	79	10.5E6	3.8E6	.33	.1					
314-	+MAT079	2.64+04	2.11+04								
315-	MAT1	80	10.5E6	3.8E6	.33	.1					

S O K E T E D B U L K D A T A E C H O

CARD	1	2	3	4	5	6	7	8	9	10
316-	+MAT080	2.64+04	2.11+04							+MAT081
317-	MAT1	81	10.5E6	3.8E6	.33					
318-	+MAT081	2.57+04	2.05+04							+MAT082
319-	MAT1	82	10.5E6	3.8E6	.33					
320-	+MAT082	2.57+04	2.05+04							+MAT083
321-	MAT1	83	10.5E6	3.8E6	.33					
322-	+MAT083	2.66+04	2.13+04							+MAT084
323-	MAT1	84	10.5E6	3.8E6	.33					
324-	+MAT084	2.66+04	2.13+04							+MAT085
325-	MAT1	85	10.5E6	3.8E6	.33					
326-	+MAT085	2.11+04	1.69+04							+MAT086
327-	MAT1	86	10.5E6	3.8E6	.33					
328-	+MAT086	2.11+04	1.09+04							+MAT087
329-	MAT1	87	10.5E6	3.8E6	.33					
330-	+MAT087	2.11+04	1.69+04							+MAT088
331-	MAT1	88	10.5E6	3.8E6	.33					
332-	+MAT088	2.11+04	1.69+04							+MAT089
333-	MAT1	89	10.5E6	3.8E6	.33					
334-	+MAT089	1.18+05	9.43+04							+MAT090
335-	MAT1	90	10.5E6	3.8E6	.33					
336-	+MAT090	1.34+05	1.08+05							+MAT091
337-	MAT1	91	10.5E6	3.8E6	.33					
338-	+MAT091	1.18+05	9.43+04							+MAT092
339-	MAT1	92	10.5E6	3.8E6	.33					
340-	+MAT092	1.40+05	1.12+05							+MAT093
341-	MAT1	93	10.5E6	3.8E6	.33					
342-	+MAT093	6.34+04	5.07+04							+MAT094
343-	MAT1	94	10.5E6	3.8E6	.33					
344-	+MAT094	6.34+04	5.07+04							+MAT095
345-	MAT1	95	10.5E6	3.8E6	.33					
346-	+MAT095	4.65+04	3.72+04							+MAT096
347-	MAT1	96	10.5E6	3.8E6	.33					
348-	+MAT096	4.65+04	3.72+04							+MAT097
349-	MAT1	97	10.5E6	3.8E6	.33					
350-	+MAT097	4.65+04	3.72+04							+MAT098
351-	MAT1	98	10.5E6	3.8E6	.33					
352-	+MAT098	4.65+04	3.72+04							+MAT099
353-	MAT1	99	10.5E6	3.8E6	.33					
354-	+MAT099	3.45+04	2.76+04							+MAT100
355-	MAT1	100	10.5E6	3.8E6	.33					
356-	+MAT100	3.45+04	2.76+04							+MAT101
357-	MAT1	101	10.5E6	3.8E6	.33					
358-	+MAT101	3.57+04	2.86+04							+MAT102
359-	MAT1	102	10.5E6	3.8E6	.33					
360-	+MAT102	3.57+04	2.86+04							

S O R T E D B U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
361-	MAT1	103	10.5E6	3.8E6	.33	.1					+MAT103
362-	+MAT103	3.45+04	2.76+04								+MAT104
363-	MAT1	104	10.5E6	3.8E6	.33	.1					+MAT105
364-	+MAT104	3.45+04	2.76+04								+MAT106
365-	MAT1	105	10.5E6	3.8E6	.33	.1					+MAT107
366-	+MAT105	3.60+04	2.88+04								+MAT108
367-	MAT1	106	10.5E6	3.8E6	.33	.1					+MAT109
368-	+MAT106	3.60+04	2.88+04								+MAT110
369-	MAT1	107	10.5E6	3.8E6	.33	.1					+MAT111
370-	+MAT107	2.83+04	2.26+04								+MAT112
371-	MAT1	108	10.5E6	3.8E6	.33	.1					+MAT113
372-	+MAT108	2.83+04	2.27+04								+MAT114
373-	MAT1	109	10.5E6	3.8E6	.33	.1					+MAT115
374-	+MAT109	2.83+04	2.27+04								+MAT116
375-	MAT1	110	10.5E6	3.8E6	.33	.1					+MAT117
376-	+MAT110	2.83+04	2.26+04								+MAT118
377-	MAT1	111	10.5E6	3.8E6	.33	.1					+MAT119
378-	+MAT111	1.52+05	1.42+05								+MAT120
379-	MAT1	112	10.5E6	3.8E6	.33	.1					+MAT121
380-	+MAT112	1.78+05	1.42+05								+MAT122
381-	MAT1	113	10.5E6	3.8E6	.33	.1					+MAT123
382-	+MAT113	1.52+05	1.22+05								+MAT124
383-	MAT1	114	10.5E6	3.8E6	.33	.1					+MAT125
384-	+MAT114	1.85+05	1.48+05								
385-	MAT1	115	10.5E6	3.8E6	.33	.1					
386-	+MAT115	8.28+04	6.62+04								
387-	MAT1	116	10.5E6	3.8E6	.33	.1					
388-	+MAT116	8.28+04	6.62+04								
389-	MAT1	117	10.5E6	3.8E6	.33	.1					
390-	+MAT117	5.53+04	4.42+04								
391-	MAT1	118	10.5E6	3.8E6	.33	.1					
392-	+MAT118	5.53+04	4.42+04								
393-	MAT1	119	10.5E6	3.8E6	.33	.1					
394-	+MAT119	5.53+04	4.42+04								
395-	MAT1	120	10.5E6	3.8E6	.33	.1					
396-	+MAT120	5.53+04	4.42+04								
397-	MAT1	121	10.5E6	3.8E6	.33	.1					
398-	+MAT121	4.20+04	3.56+04								
399-	MAT1	122	10.5E6	3.8E6	.33	.1					
400-	+MAT122	4.20+04	3.56+04								
401-	MAT1	123	10.5E6	3.8E6	.33	.1					
402-	+MAT123	4.36+04	3.49+04								
403-	MAT1	124	10.5E6	3.8E6	.33	.1					
404-	+MAT124	4.56+04	3.49+04								
405-	MAT1	125	10.5E6	3.8E6	.33	.1					

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
406-	+MAT125	4.20+04	3.36+04								
407-	MAT1	126	10.5E6	3.8E6	.33	.1					+MAT126
408-	+MAT126	4.20+04	3.36+04								
409-	MAT1	127	10.5E6	3.8E6	.33	.1					+MAT127
410-	+MAT127	4.40+04	3.52+04								
411-	MAT1	128	10.5E6	3.8E6	.33	.1					+MAT128
412-	+MAT128	4.40+04	3.52+04								
413-	MAT1	129	10.5E6	3.8E6	.33	.1					+MAT129
414-	+MAT129	3.50+04	2.80+04								
415-	MAT1	130	10.5E6	3.8E6	.33	.1					+MAT130
416-	+MAT130	3.50+04	2.80+04								
417-	MAT1	131	10.5E6	3.8E6	.33	.1					+MAT131
418-	+MAT131	3.50+04	2.80+04								
419-	MAT1	132	10.5E6	3.8E6	.33	.1					+MAT132
420-	+MAT132	3.50+04	2.80+04								
421-	MAT1	133	10.5E6	3.8E6	.33	.1					+MAT133
422-	+MAT133	1.99+05	1.60+05								
423-	MAT1	134	10.5E6	3.8E6	.33	.1					+MAT134
424-	+MAT134	2.39+05	1.91+05								
425-	MAT1	135	10.5E6	3.8E6	.33	.1					+MAT135
426-	+MAT135	1.99+05	1.60+05								
427-	MAT1	136	10.5E6	3.8E6	.33	.1					+MAT136
428-	+MAT136	2.48+05	1.99+05								
429-	MAT1	137	10.5E6	3.8E6	.33	.1					+MAT137
430-	+MAT137	1.10+05	8.77+04								
431-	MAT1	138	10.5E6	3.8E6	.33	.1					+MAT138
432-	+MAT138	1.10+05	8.77+04								
433-	PAKAM	GRDPNT	0								
434-	PTUBE	1	1.5			.0625					
435-	PTUBE	2	1.5			.0625					
436-	PTUBE	3	1.5			.0625					
437-	PTUBE	4	1.5			.0625					
438-	PTUBE	5	1.5			.0625					
439-	PTUBE	6	1.5			.0625					
440-	PTUBE	7	1.5			.0625					
441-	PTUBE	8	1.5			.0625					
442-	PTUBE	9	1.5			.0625					
443-	PTUBE	10	1.5			.0625					
444-	PTUBE	11	1.5			.0625					
445-	PTUBE	12	1.5			.0625					
446-	PTUBE	13	1.5			.0625					
447-	PTUBE	14	1.5			.0625					
448-	PTUBE	15	1.5			.0625					
449-	PTUBE	16	1.5			.0625					
450-	PTUBE	17	1.5			.0625					

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
496-	PTUBE	63	63
497-	PTUBE	64	64	1.5	1.5	.0625					
498-	PTUBE	65	65	1.5	1.5	.0625					
499-	PTUBE	66	66	1.5	1.5	.0625					
500-	PTUBE	67	67	1.5	1.5	.0625					
501-	PTUBE	68	68	1.5	1.5	.0625					
502-	PTUBE	69	69	1.5	1.5	.0625					
503-	PTUBE	70	70	1.5	1.5	.0625					
504-	PTUBE	71	71	1.5	1.5	.0625					
505-	PTUBE	72	72	1.5	1.5	.0625					
506-	PTUBE	73	73	1.5	1.5	.0625					
507-	PTUBE	74	74	1.5	1.5	.0625					
508-	PTUBE	75	75	1.5	1.5	.0625					
509-	PTUBE	76	76	1.5	1.5	.0625					
510-	PTUBE	77	77	1.5	1.5	.0625					
511-	PTUBE	78	78	1.5	1.5	.0625					
512-	PTUBE	79	79	1.5	1.5	.0625					
513-	PTUBE	80	80	1.5	1.5	.0625					
514-	PTUBE	81	81	1.5	1.5	.0625					
515-	PTUBE	82	82	1.5	1.5	.0625					
516-	PTUBE	83	83	1.5	1.5	.0625					
517-	PTUBE	84	84	1.5	1.5	.0625					
518-	PTUBE	85	85	1.5	1.5	.0625					
519-	PTUBE	86	86	1.5	1.5	.0625					
520-	PTUBE	87	87	1.5	1.5	.0625					
521-	PTUBE	88	88	1.5	1.5	.0625					
522-	PTUBE	89	89	1.5	1.5	.0625					
523-	PTUBE	90	90	1.5	1.5	.0625					
524-	PTUBE	91	91	1.5	1.5	.0625					
525-	PTUBE	92	92	1.5	1.5	.0625					
526-	PTUBE	93	93	1.5	1.5	.0625					
527-	PTUBE	94	94	1.5	1.5	.0625					
528-	PTUBE	95	95	1.5	1.5	.0625					
529-	PTUBE	96	96	1.5	1.5	.0625					
530-	PTUBE	97	97	1.5	1.5	.0625					
531-	PTUBE	98	98	1.5	1.5	.0625					
532-	PTUBE	99	99	1.5	1.5	.0625					
533-	PTUBE	100	100	1.5	1.5	.0625					
534-	PTUBE	101	101	1.5	1.5	.0625					
535-	PTUBE	102	102	1.5	1.5	.0625					
536-	PTUBE	103	103	1.5	1.5	.0625					
537-	PTUBE	104	104	1.5	1.5	.0625					
538-	PTUBE	105	105	1.5	1.5	.0625					
539-	PTUBE	106	106	1.5	1.5	.0625					
540-	PTUBE	107	107	1.5	1.5	.0625					

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
541-	PTUBE	108	108	1.5	1.5	.0625					
542-	PTUBE	109	109	1.5	1.5	.0625					
543-	PTUBE	110	110	1.5	1.5	.0625					
544-	PTUBE	111	111	1.5	1.5	.0625					
545-	PTUBE	112	112	1.5	1.5	.0625					
546-	PTUBE	113	113	1.5	1.5	.0625					
547-	PTUBE	114	114	1.5	1.5	.0625					
548-	PTUBE	115	115	1.5	1.5	.0625					
549-	PTUBE	116	116	1.5	1.5	.0625					
550-	PTUBE	117	117	1.5	1.5	.0625					
551-	PTUBE	118	118	1.5	1.5	.0625					
552-	PTUBE	119	119	1.5	1.5	.0625					
553-	PTUBE	120	120	1.5	1.5	.0625					
554-	PTUBE	121	121	1.5	1.5	.0625					
555-	PTUBE	122	122	1.5	1.5	.0625					
556-	PTUBE	123	123	1.5	1.5	.0625					
557-	PTUBE	124	124	1.5	1.5	.0625					
558-	PTUBE	125	125	1.5	1.5	.0625					
559-	PTUBE	126	126	1.5	1.5	.0625					
560-	PTUBE	127	127	1.5	1.5	.0625					
561-	PTUBE	128	128	1.5	1.5	.0625					
562-	PTUBE	129	129	1.5	1.5	.0625					
563-	PTUBE	130	130	1.5	1.5	.0625					
564-	PTUBE	131	131	1.5	1.5	.0625					
565-	PTUBE	132	132	1.5	1.5	.0625					
566-	PTUBE	133	133	1.5	1.5	.0625					
567-	PTUBE	134	134	1.5	1.5	.0625					
568-	PTUBE	135	135	1.5	1.5	.0625					
569-	PTUBE	136	136	1.5	1.5	.0625					
570-	PTUBE	137	137	1.5	1.5	.0625					
571-	PTUBE	138	138	1.5	1.5	.0625					
572-	SPC	10	1	123456	2	123456					
573-	SPC	10	3	123456	4	123456					
	ENDDATA										

* 11.4 CPU-S 60.4 COR-S 20 LLP-S. XGPI
 NO ERRORS FOUND - EXECUTE NASTRAN PROGRAM
 * 14.6 CPU-S 64.6 COR-S 25 LLP-S. SEMI END
 * 14.6 CPU-S 64.6 COR-S 25 LLP-S. ---- LINK END ---

TRUSS TAIL BOOM MODEL? **A 114 ELEMENT VERSION
DAMAGE CRITERIUM = NONE

LINEAR CASE 30 X LOADING

SUBCASE 1

POINT ID,	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	3.408960-03	-8.003385-03	5.592414-04	.0	.0	.0
6	6	-6.060912-04	3.930867-03	1.190927-03	.0	.0	.0
7	6	-3.676434-03	3.140641-03	-1.009343-02	.0	.0	.0
8	6	4.968148-04	-7.199159-03	-9.451740-03	.0	.0	.0
9	6	6.567249-03	-2.157185-02	-3.772064-03	.0	.0	.0
10	6	-1.843186-04	2.479580-03	-3.280151-03	.0	.0	.0
11	6	-6.407310-03	2.128899-03	-2.620921-02	.0	.0	.0
12	6	4.528371-05	-2.121480-02	-2.571272-02	.0	.0	.0
13	6	9.108101-03	-4.351939-02	-1.062160-02	.0	.0	.0
14	6	1.290961-03	-4.270602-03	-1.025311-02	.0	.0	.0
15	6	-7.890126-03	-4.350141-03	-4.736535-02	.0	.0	.0
16	6	-1.462164-03	-4.344037-02	-4.699647-02	.0	.0	.0
17	6	9.022580-03	-6.905972-02	-1.564162-02	.0	.0	.0
18	6	2.969545-03	-1.722768-02	-1.537139-02	.0	.0	.0
19	6	-8.760307-03	-1.722553-02	-6.383362-02	.0	.0	.0
20	6	-3.176044-03	-6.907189-02	-6.356338-02	.0	.0	.0
21	6	9.934891-03	-9.789615-02	-2.028055-02	.0	.0	.0
22	6	4.301572-03	-3.529501-02	-2.008361-02	.0	.0	.0
23	6	-9.399123-03	-3.529508-02	-7.764830-02	.0	.0	.0
24	6	-4.790581-03	-9.789609-02	-7.745137-02	.0	.0	.0
25	6	1.061690-02	-1.330094-01	-2.448695-02	.0	.0	.0
26	6	5.548152-03	-5.775276-02	-2.483351-02	.0	.0	.0
27	6	-1.000189-02	-5.775245-02	-8.988068-02	.0	.0	.0
28	6	-6.116372-03	-1.330094-01	-9.022717-02	.0	.0	.0

SUBCASE 2

TRUSS TAIL BOOM MODEL2 *** 114 ELEMENT VERSION

DAMAGE CRITERION = NCHE

INCREMENTAL STIFFNESS 50 X LOADING

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	6.255592-03	-1.290247-02	7.447220-04	.0	.0	.0
6	6	-1.076665-03	6.356675-03	1.775518-03	.0	.0	.0
7	6	-6.033014-03	5.046518-03	-1.638145-02	.0	.0	.0
8	6	9.087669-04	-1.154819-02	-1.535603-02	.0	.0	.0
9	6	1.085260-02	-3.477493-02	-6.742868-03	.0	.0	.0
10	6	-4.873443-04	3.973119-03	-5.937379-03	.0	.0	.0
11	6	-1.053797-02	3.383438-03	-4.283017-02	.0	.0	.0
12	6	2.900520-04	-3.413987-02	-4.204186-02	.0	.0	.0
13	6	1.339756-02	-7.019109-02	-1.872231-02	.0	.0	.0
14	6	1.802321-03	-7.002152-03	-1.811730-02	.0	.0	.0
15	6	-1.299832-02	-7.145423-03	-7.783044-02	.0	.0	.0
16	6	-2.029264-03	-7.000571-02	-7.725334-02	.0	.0	.0
17	6	1.493055-02	-1.113359-01	-2.801512-02	.0	.0	.0
18	6	4.429339-03	-2.789172-02	-2.756683-02	.0	.0	.0
19	6	-1.443700-02	-2.789467-02	-1.055399-01	.0	.0	.0
20	6	-4.704782-03	-1.112835-01	-1.051230-01	.0	.0	.0
21	6	1.643511-02	-1.577144-01	-3.683409-02	.0	.0	.0
22	6	5.596255-03	-5.696797-02	-3.649950-02	.0	.0	.0
23	6	-1.547599-02	-5.696326-02	-1.291162-01	.0	.0	.0
24	6	-7.246980-03	-1.576620-01	-1.286238-01	.0	.0	.0
25	6	1.753051-02	-2.141573-01	-4.502065-02	.0	.0	.0
26	6	8.560392-03	-9.308011-02	-4.569347-02	.0	.0	.0
27	6	-1.643499-02	-9.306449-02	-1.503643-01	.0	.0	.0
28	6	-9.362262-03	-2.141306-01	-1.508090-01	.0	.0	.0

SUBCASE 2

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	9.494084-03	-1.940388-02	1.002610-03	.0	.0	.0
6	6	-1.692481-03	4.572472-03	2.562577-03	.0	.0	.0
7	6	-9.152618-03	7.575185-03	-2.471574-02	.0	.0	.0
8	6	1.446179-03	-1.732417-02	-2.318028-02	.0	.0	.0
9	6	1.649621-02	-5.229225-02	-1.063383-02	.0	.0	.0
10	6	-8.737777-04	5.951338-03	-9.412849-03	.0	.0	.0
11	6	-1.600451-02	5.046369-03	-6.483904-02	.0	.0	.0
12	6	5.968494-04	-5.129968-02	-6.366249-02	.0	.0	.0
13	6	2.039370-02	-1.055932-01	-2.934786-02	.0	.0	.0
14	6	2.503719-03	-1.062868-02	-2.842971-02	.0	.0	.0
15	6	-1.975715-02	-1.085544-02	-1.181421-01	.0	.0	.0
16	6	-2.808020-03	-1.052697-01	-1.172873-01	.0	.0	.0
17	6	2.274316-02	-1.674411-01	-4.421894-02	.0	.0	.0
18	6	6.405707-03	-4.204874-02	-4.353985-02	.0	.0	.0
19	6	-2.194762-02	-4.205800-02	-1.606927-01	.0	.0	.0
20	6	-6.765771-03	-1.673204-01	-1.600697-01	.0	.0	.0
21	6	2.502630-02	-2.371250-01	-5.848265-02	.0	.0	.0
22	6	9.585249-03	-8.574011-02	-5.796680-02	.0	.0	.0
23	6	-2.351677-02	-4.572942-02	-1.971170-01	.0	.0	.0
24	6	-1.054286-02	-2.370068-01	-1.966563-01	.0	.0	.0
25	6	2.667450-02	-3.218895-01	-7.184347-02	.0	.0	.0
26	6	1.258687-02	-1.399797-01	-7.294101-02	.0	.0	.0
27	6	-2.434869-02	-1.399448-01	-2.302184-01	.0	.0	.0
28	6	-1.370677-02	-3.218294-01	-2.308019-01	.0	.0	.0

INCREMENTAL STIFFNESS 100% LOADING

SUBCASE 2

D I S P L A C E M E N T V E C T O R

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	1.280617-02	-2.594144-02	1.183984-03	.0	.0	.0
6	6	-2.359331-03	1.281287-02	3.282948-03	.0	.0	.0
7	6	-1.234264-02	1.010685-02	-3.314748-02	.0	.0	.0
8	6	2.038312-03	-2.310383-02	-3.110345-02	.0	.0	.0
9	6	2.228407-02	-6.992449-02	-1.487235-02	.0	.0	.0
10	6	-1.353839-03	7.919747-03	-1.322693-02	.0	.0	.0
11	6	-2.160590-02	6.685727-03	-8.724951-02	.0	.0	.0
12	6	1.010485-03	-6.852884-02	-8.568846-02	.0	.0	.0
13	6	2.752259-02	-1.412214-01	-4.081963-02	.0	.0	.0
14	6	3.073342-03	-1.434981-02	-3.958100-02	.0	.0	.0
15	6	-2.669315-02	-1.466805-02	-1.593978-01	.0	.0	.0
16	6	-3.430614-03	-1.407294-01	-1.582725-01	.0	.0	.0
17	6	3.079236-02	-2.238735-01	-6.189306-02	.0	.0	.0
18	6	8.224595-03	-5.636504-02	-6.097465-02	.0	.0	.0
19	6	-2.965747-02	-5.638369-02	-2.174290-01	.0	.0	.0
20	6	-8.633497-03	-2.236561-01	-2.166283-01	.0	.0	.0
21	6	3.587570-02	-3.169543-01	-8.229487-02	.0	.0	.0
22	6	1.244271-02	-1.147303-01	-8.158848-02	.0	.0	.0
23	6	-3.176392-02	-1.147113-01	-2.674441-01	.0	.0	.0
24	6	-1.362108-02	-3.167440-01	-2.669072-01	.0	.0	.0
25	6	3.607561-02	-4.301218-01	-1.015335-01	.0	.0	.0
26	6	1.644532-02	-1.871523-01	-1.031353-01	.0	.0	.0
27	6	-3.366455-02	-1.870905-01	-3.132290-01	.0	.0	.0
28	6	-1.782735-02	-4.300146-01	-3.138955-01	.0	.0	.0

TRUSS TAIL BOOM MODEL2 **A 114 ELEMENT VERSION
DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 50 X LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	S T K E S S E S TORSIONAL STRESS	S A F E T Y M A R G I N	E L E M E N T S E L E S I N R O D E L E M E N T S E L E M E N T S	A X I A L S T R E S S	S A F E T Y M A R G I N	(C T U B E) (L B S / S Q . I N .)	T O R S I O N A L S T R E S S	S A F E T Y M A R G I N
1	.0	.0	.0	2	.0	.0	.0	.0	.0
3	.0	.0	.0	4	.0	.0	.0	.0	.0
5	.0	.0	.0	6	.0	.0	.0	.0	.0
7	2.1100756+03	1.0+01	1.0+01	8	-3.904817+02	4.8+01	4.8+01	.0	.0
9	-2.020083+03	8.5+00	8.5+00	10	3.276187+02	7.2+01	7.2+01	.0	.0
11	-5.455813+02	2.2+01	2.2+01	12	1.511202+03	9.6+00	9.6+00	.0	.0
13	1.997594+03	7.2+00	7.2+00	14	-5.341067+02	2.4+01	2.4+01	.0	.0
15	1.190064+03	1.2+01	1.2+01	16	-2.148195+03	5.0+00	5.0+00	.0	.0
17	-2.174410+03	5.1+00	5.1+00	18	6.976864+02	2.3+01	2.3+01	.0	.0
23	-5.614824+02	7.6+01	7.6+01	24	-6.665977+02	7.0+01	7.0+01	.0	.0
25	5.486782+02	9.8+01	9.8+01	26	6.560154+02	9.2+01	9.2+01	.0	.0
27	8.185547+00	3.5+03	3.5+03	28	-1.993307+01	1.1+03	1.1+03	.0	.0
29	1.814436+03	1.3+01	1.3+01	30	1.227732+02	2.0+02	2.0+02	.0	.0
31	-1.767088+03	1.0+01	1.0+01	32	-1.503503+02	1.3+02	1.3+02	.0	.0
33	-7.310417+02	1.5+01	1.5+01	34	1.782890+03	8.8+00	8.8+00	.0	.0
35	1.988491+03	8.1+00	8.1+00	36	-1.045684+03	1.3+01	1.3+01	.0	.0
37	1.505494+03	1.1+01	1.1+01	38	-2.551441+03	4.5+00	4.5+00	.0	.0
39	-2.195208+03	5.6+00	5.6+00	40	1.241067+03	1.4+01	1.4+01	.0	.0
45	-5.987239+02	9.1+01	9.1+01	46	-3.546543+02	1.7+02	1.7+02	.0	.0
47	5.842102+02	1.2+02	1.2+02	48	3.550825+02	2.3+02	2.3+02	.0	.0
49	1.237793-01	2.9+05	2.9+05	50	-1.702484+01	1.7+03	1.7+03	.0	.0
51	1.382209+03	1.7+01	1.7+01	52	7.113932+02	3.4+01	3.4+01	.0	.0
53	-1.527605+03	1.4+01	1.4+01	54	-7.485229+02	2.5+01	2.5+01	.0	.0
55	-9.370841+02	1.5+01	1.5+01	56	2.230792+03	7.4+00	7.4+00	.0	.0
57	2.109965+03	6.1+00	6.1+00	58	-1.718732+03	8.0+00	8.0+00	.0	.0
59	1.507438+03	8.8+00	8.8+00	60	-3.196176+03	3.7+00	3.7+00	.0	.0
61	-2.354866+03	5.6+00	5.6+00	62	1.961231+03	8.8+00	8.8+00	.0	.0
67	-6.872863+02	1.0+02	1.0+02	68	-1.196187+02	6.8+02	6.8+02	.0	.0
69	6.686064+02	1.3+02	1.3+02	70	9.409235+01	1.1+03	1.1+03	.0	.0
71	3.891846+00	1.2+04	1.2+04	72	-2.577368+01	1.5+03	1.5+03	.0	.0
73	1.294431+03	2.5+01	2.5+01	74	1.143274+03	2.9+01	2.9+01	.0	.0
75	-1.223482+03	2.1+01	2.1+01	76	-1.197003+03	2.2+01	2.2+01	.0	.0
77	-1.595655+03	1.2+01	1.2+01	78	3.061902+03	7.4+00	7.4+00	.0	.0
79	2.163459+03	1.1+01	1.1+01	80	-2.123941+03	8.9+00	8.9+00	.0	.0
81	1.604046+03	1.5+01	1.5+01	82	-3.067136+03	5.7+00	5.7+00	.0	.0
83	-2.453084+03	7.7+00	7.7+00	84	2.411720+03	1.0+01	1.0+01	.0	.0
89	-7.956382+02	1.2+02	1.2+02	90	-3.895215+01	2.8+03	2.8+03	.0	.0
91	7.749082+02	1.5+02	1.5+02	92	2.227783+00	6.3+04	6.3+04	.0	.0
93	3.378076+01	1.9+03	1.9+03	94	-6.191101+01	8.2+02	8.2+02	.0	.0
95	1.576733+03	2.8+01	2.8+01	96	1.260624+03	3.6+01	3.6+01	.0	.0
97	-1.321531+03	2.7+01	2.7+01	98	-1.492953+03	2.4+01	2.4+01	.0	.0
99	-1.845161+03	1.4+01	1.4+01	100	3.508241+03	8.8+00	8.8+00	.0	.0
101	2.392293+03	1.4+01	1.4+01	102	-2.347227+03	1.1+01	1.1+01	.0	.0
103	1.858308+03	1.6+01	1.6+01	104	-3.518415+03	6.8+00	6.8+00	.0	.0
105	-2.720641+03	9.6+00	9.6+00	106	2.672993+03	1.2+01	1.2+01	.0	.0

SUBCASE 2

INCREMENTAL STIFFNESS 50 & LOADING		STRESSES IN ROD		ELEMENTS (CTUBE) (LBS/SQ.IN.)		SAFETY MARGIN	
ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS
111	-9.377385+02	1.3+02	.0	112	-4.484180+01	3.2+03	.0
113	9.040322+02	1.7+02	.0	114	-4.105469+00	3.6+04	.0
115	-6.950195+01	9.5+02	.0	116	2.883008+01	2.9+03	.0
117	1.693178+03	3.2+01	.0	118	1.935480+03	5.8+01	.0
119	-1.488711+03	2.9+01	.0	120	-1.639735+03	2.6+01	.0
121	-2.035861+03	1.6+01	.0	122	4.112227+03	9.2+00	.0
123	2.952771+03	1.4+01	.0	124	-2.920976+03	1.1+01	.0
125	2.079911+03	1.9+01	.0	126	-4.109003+03	7.2+00	.0
127	-3.359635+03	9.5+00	.0	128	3.313254+03	1.2+01	.0
133	-3.357437+02	4.8+02	.0	134	-2.641211+01	7.2+03	.0
135	5.421074+02	3.7+02	.0	136	-1.577051+01	1.3+04	.0
137	-2.122560+03	4.0+01	.0	138	2.217000+03	4.9+01	.0

ELEMENT ID.	INCREMENTAL STIFFNESS 75 * LOADING		S T R E S S E S I N		R O D		E L E M E N T S		(C T U B E) (L B S / S Q . I N .)	
	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN	AXIAL STRESS	SAFETY MARGIN	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
1	.0		.0		.0		.0		.0	
3	.0		.0		.0		.0		.0	
5	.0		.0		.0		.0		.0	
7	3.187686+03	6.5+00	.0		-6.115744+02	3.0+01	-6.115744+02	3.0+01	.0	
9	-3.0639+03	5.2+00	.0		5.190866+02	4.5+01	5.190866+02	4.5+01	.0	
11	-8.201653+02	1.5+01	.0		2.2735+03	6.0+00	2.2735+03	6.0+00	.0	
13	3.013715+03	4.4+00	.0		-7.837040+02	1.6+01	-7.837040+02	1.6+01	.0	
15	1.734626+03	8.0+00	.0		-3.226393+03	3.0+00	-3.226393+03	3.0+00	.0	
17	-3.283988+03	3.0+00	.0		1.034262+03	1.5+01	1.034262+03	1.5+01	.0	
23	-8.490722+02	5.0+01	.0		-1.023673+03	4.5+01	-1.023673+03	4.5+01	.0	
25	8.217820+02	6.5+01	.0		1.000072+03	6.0+01	1.000072+03	6.0+01	.0	
27	6.363417+00	4.5+03	.0		-3.190088+01	7.1+02	-3.190088+01	7.1+02	.0	
29	2.761400+03	7.9+00	.0		1.592125+02	1.5+02	1.592125+02	1.5+02	.0	
31	-2.686425+03	6.3+00	.0		-1.961643+02	9.9+01	-1.961643+02	9.9+01	.0	
33	-1.097874+03	1.2+01	.0		2.682151+03	5.5+00	2.682151+03	5.5+00	.0	
35	3.004455+03	5.0+00	.0		-1.553130+03	8.3+00	-1.553130+03	8.3+00	.0	
37	2.258808+03	6.7+00	.0		-3.833500+03	2.7+00	-3.833500+03	2.7+00	.0	
39	-3.316035+03	3.4+00	.0		1.847235+03	8.8+00	1.847235+03	8.8+00	.0	
45	-9.054391+02	6.0+01	.0		-5.582087+02	1.1+02	-5.582087+02	1.1+02	.0	
47	8.734326+02	7.8+01	.0		5.142428+02	1.5+02	5.142428+02	1.5+02	.0	
49	-7.670166+00	3.8+03	.0		-2.998175+01	9.7+02	-2.998175+01	9.7+02	.0	
51	2.109731+03	1.1+01	.0		1.041327+03	2.3+01	1.041327+03	2.3+01	.0	
53	-2.022066+03	6.7+00	.0		-1.091643+03	1.7+01	-1.091643+03	1.7+01	.0	
55	-1.407286+03	9.7+00	.0		3.352483+03	4.6+00	3.352483+03	4.6+00	.0	
57	3.194263+03	5.0+00	.0		-2.566785+03	5.0+00	-2.566785+03	5.0+00	.0	
59	2.866532+03	5.5+00	.0		-4.801383+03	2.1+00	-4.801383+03	2.1+00	.0	
61	-3.553174+03	3.4+00	.0		2.922444+03	5.6+00	2.922444+03	5.6+00	.0	
67	-1.038335+03	6.9+01	.0		-2.087119+02	3.9+02	-2.087119+02	3.9+02	.0	
69	9.968916+02	9.0+01	.0		1.489202+02	7.0+02	1.489202+02	7.0+02	.0	
71	-2.793945+00	1.4+04	.0		-4.722998+01	8.2+02	-4.722998+01	8.2+02	.0	
73	1.975413+03	1.6+01	.0		1.688493+03	1.9+01	1.688493+03	1.9+01	.0	
75	-1.862303+03	1.4+01	.0		-1.762807+03	1.8+01	-1.762807+03	1.8+01	.0	
77	-2.395710+03	7.6+00	.0		4.596776+03	4.6+00	4.596776+03	4.6+00	.0	
79	3.269676+03	7.1+00	.0		-3.172676+03	5.7+00	-3.172676+03	5.7+00	.0	
81	2.414694+03	9.6+00	.0		-4.608497+03	3.8+00	-4.608497+03	3.8+00	.0	
83	-3.704849+03	4.7+00	.0		3.603595+03	6.4+00	3.603595+03	6.4+00	.0	
89	-1.201492+03	7.7+01	.0		-8.974121+01	1.2+03	-8.974121+01	1.2+03	.0	
91	1.154734+03	1.0+02	.0		7.005859+00	2.0+04	7.005859+00	2.0+04	.0	
93	3.989160+01	1.6+03	.0		-1.032948+02	4.9+02	-1.032948+02	4.9+02	.0	
95	2.396922+03	1.8+01	.0		1.868239+03	2.4+01	1.868239+03	2.4+01	.0	
97	-2.003754+03	1.8+01	.0		-2.207851+03	1.6+01	-2.207851+03	1.6+01	.0	
99	-2.765247+03	9.0+00	.0		5.265283+03	5.6+00	5.265283+03	5.6+00	.0	
101	3.612022+03	8.9+00	.0		-3.510689+03	7.1+00	-3.510689+03	7.1+00	.0	
103	2.796879+03	1.1+01	.0		-5.288227+03	4.2+00	-5.288227+03	4.2+00	.0	
105	-4.105455+03	6.0+00	.0		3.998314+03	8.0+00	3.998314+03	8.0+00	.0	

INCREMENTAL STIFFNESS 75 % LOADING

SUBCASE 2

ELEMENT ID.	STRESSES IN ROD		ELEMENTS		(C T U B E)		SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
	AXIAL STRESS	TORSIONAL STRESS	AXIAL STRESS	TORSIONAL STRESS	AXIAL STRESS	TORSIONAL STRESS			
111	-1.41942+03	0	112	-1.009668+02	1.4+03	0	1.4+03	0	
113	1.343428+03	0	114	-9.303711+00	1.6+04	0	1.6+04	0	
115	-1.194492+02	0	116	2.778809+01	3.0+03	0	3.0+03	0	
117	2.571103+03	0	118	2.133381+03	2.5+01	0	2.5+01	0	
119	-2.253350+03	0	120	-2.437149+03	1.7+01	0	1.7+01	0	
121	-3.045770+03	0	122	6.177823+03	5.8+00	0	5.8+00	0	
123	4.449080+03	0	124	-4.377426+03	7.0+00	0	7.0+00	0	
125	3.142815+03	0	126	-6.170614+03	4.4+00	0	4.4+00	0	
127	-5.064699+03	0	128	4.960231+03	7.9+00	0	7.9+00	0	
133	-4.259883+02	0	134	-5.958594+01	3.2+03	0	3.2+03	0	
135	8.910059+02	0	136	-3.518750+01	5.7+03	0	5.7+03	0	
137	-3.142594+03	0	138	3.355533+03	3.2+01	0	3.2+01	0	

DAMAGE CRITERION = NONE

ELEMENT ID.	AXIAL STRESS		SAFETY MARGIN		TORSIONAL STRESS		SAFETY MARGIN		E L E M E N T S (C T U B E) (L B S / S Q . I N .)		SUBCASE 2	
	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
1	.0		.0		.0		.0		.0		.0	
3	.0		.0		.0		.0		.0		.0	
5	.0		.0		.0		.0		.0		.0	
7	4.299580+03	4.5+00	.0		-8.496977+02	2.1+01	.0		7.287840+02	3.2+01	.0	
9	-4.131011+03	3.6+00	.0		3.04742+03	4.3+00	.0		1.2+01	.0		
11	-1.095876+03	1.1+01	.0		-1.021666+03	1.2+01	.0		2.0+00	.0		
13	4.046948+03	3.1+00	.0		-4.307687+03	2.0+00	.0		1.1+01	.0		
15	2.379773+03	5.7+00	.0		1.362744+03	1.1+01	.0		3.3+01	.0		
17	-4.414104+03	2.0+00	.0		-1.396721+03	3.3+01	.0		4.4+01	.0		
23	-1.141541+03	3.7+01	.0		1.354944+03	4.4+01	.0		5.0+02	.0		
25	1.094213+03	4.9+01	.0		-4.518335+01	5.0+02	.0		1.4+02	.0		
27	4.954224+01	5.8+04	.0		1.792187+02	1.4+02	.0		8.8+01	.0		
29	3.735461+03	5.6+00	.0		-2.225599+02	8.8+01	.0		3.9+00	.0		
31	-3.630174+03	4.4+00	.0		3.587078+03	3.9+00	.0		6.0+00	.0		
33	-1.465632+03	8.6+00	.0		-2.050409+03	6.0+00	.0		1.7+00	.0		
35	4.035245+03	3.5+00	.0		-5.120242+03	1.7+00	.0		6.4+00	.0		
37	3.012535+03	4.8+00	.0		2.443989+03	6.4+00	.0		7.7+01	.0		
39	-4.452714+03	2.3+00	.0		-7.794019+02	7.7+01	.0		1.1+02	.0		
45	-1.217323+03	4.4+01	.0		7.012236+02	1.1+02	.0		6.4+02	.0		
47	1.150861+03	5.9+01	.0		-4.587115+01	6.4+02	.0		1.7+01	.0		
49	-2.084058+01	1.4+03	.0		1.354219+03	1.7+01	.0		1.3+01	.0		
51	2.862065+03	7.6+00	.0		-1.414088+03	3.2+00	.0		3.5+00	.0		
53	-2.737424+03	6.2+00	.0		4.478988+03	3.2+00	.0		1.3+00	.0		
55	-1.878810+03	7.0+00	.0		-3.407583+03	3.5+00	.0		4.0+00	.0		
57	4.298674+03	3.5+00	.0		-6.411950+03	1.3+00	.0		2.5+02	.0		
59	3.829468+03	3.9+00	.0		3.871020+03	4.0+00	.0		5.0+02	.0		
61	-4.765922+03	2.3+00	.0		-3.174795+02	2.5+02	.0		5.2+02	.0		
67	-1.394514+03	5.1+01	.0		-7.435474+01	5.2+02	.0		1.4+01	.0		
69	1.521283+03	6.8+01	.0		2.216158+03	1.4+01	.0		3.2+00	.0		
71	-1.536084+01	2.5+03	.0		6.135022+03	3.2+00	.0		4.0+00	.0		
73	2.673344+03	1.2+01	.0		-4.213091+03	4.0+00	.0		4.6+00	.0		
75	-2.319567+03	9.8+00	.0		-1.615684+02	6.7+02	.0		3.3+02	.0		
77	-3.197721+03	5.4+00	.0		1.426807+01	9.8+03	.0		1.8+01	.0		
79	4.392954+03	5.0+00	.0		-1.515894+02	3.3+02	.0		2.9+00	.0		
81	3.231589+03	7.0+00	.0		2.460750+03	1.8+01	.0		5.1+00	.0		
83	-4.974166+03	3.3+00	.0		-2.901663+03	1.2+01	.0		5.1+00	.0		
89	-1.612864+03	5.7+01	.0		7.025193+03	3.9+00	.0		2.9+00	.0		
91	1.529549+03	7.6+01	.0		-4.668152+03	5.1+00	.0		5.8+00	.0		
93	3.857090+01	1.6+03	.0		-7.066084+03	5.8+00	.0		5.8+00	.0		
95	3.238653+03	1.3+01	.0		5.316936+03	5.8+00	.0					
97	-2.705912+03	1.3+01	.0									
99	-3.695076+03	6.5+00	.0									
101	4.848444+03	8.2+00	.0									
103	3.747856+03	6.4+00	.0									
105	-5.507550+03	4.2+00	.0									

TRUSS TAIL BOOM MODEL2 **A 114 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 100% LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ROD SAFETY MARGIN		ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		TUBE SAFETY MARGIN		SAFETY MARGIN																						
	111	113	115	117	119	121		123	125	127	133	135	137		112	114	116	118	120	122	124	126	128	134	136	138										
111	-1.909799+03	1.774391+03	-1.796172+02	3.458084+03	-3.031671+03	-4.051315+03	5.959820+03	4.224214+03	-6.787707+03	-4.641445+02	1.292254+03	-4.134330+03	-1.797109+02	-1.659277+01	1.637744+01	2.818036+03	-3.219545+03	8.250880+03	-5.832223+03	-8.238140+03	6.601729+03	-1.061953+02	-6.237305+01	4.513631+03	7.9+02	8.9+03	5.1+03	1.9+01	1.3+01	4.1+00	5.0+00	3.1+00	5.7+00	1.8+03	3.2+03	2.3+01

* 53.2 CPU-S 262.5 COR-S 182 ELP-S. 158 OFF END

* 53.2 CPU-S 263.4 COR-S 182 ELP-S. 179 EXIT BEGIN

APPENDIX C

NASTRAN MATHEMATICAL MODEL OF THE UNDAMAGED
TRUSS MODEL 3 PLUS OUTPUT OF DISPLACEMENTS, STRESSES
AND MARGINS OF SAFETY DUE TO FLIGHT LOADS

PRECEDING PAGE NOT FILMED
BLANK

N A S T R A N E X E C U T I V E C O N T R O L D E C K E C H O

ID ERLINE,MODEL3
APP DISP
\$ STATIC ANALYSIS WITH DIFFERENTIAL STIFFNESS RF 4
SOL 4.0
TIME 10
CEND

DAMAGE CRITICN = NONE

C A S E C O N T R O L D E C K E C H O

CARD
COUNT

1 TITLE = TRUSS TAIL BOOM MODEL3 *** 138 ELEMENT VERSION

2 SUBTITLE = DAMAGE CRITICN = NONE

3 ULDAD = ALL

4 SPC = 10

5 DISP = ALL

6 SPCFORCES = ALL

7 SET 5 = 1 THRU 138

8 SUBCASE 1

9 LABEL = LINEAK CASE

10 LOAD = 11

11 SUBCASE 2

12 LABEL = INCREMENTAL STIFFNESS

13 USCOEFFICIENT = 200

14 STRESS = 5

15 MAXLINES = 100000

16 BEGIN BULK

*** USER INFORMATION MESSAGE 207, BULK DATA NOT SORTED, X SORT WILL RE-ORDER DECK.

SORTED BULK DATA ECHO

CARD COUNT	1	2	3	4	5	6	7	8	9	10
1-	CTUBE	1	1	1	2					
2-	CTUBE	2	2	1	4					
3-	CTUBE	3	3	3	4					
4-	CTUBE	4	4	2	3					
5-	CTUBE	5	5	1	3					
6-	CTUBE	6	6	2	4					
7-	CTUBE	7	7	1	5					
8-	CTUBE	8	8	2	6					
9-	CTUBE	9	9	3	7					
10-	CTUBE	10	10	4	8					
11-	CTUBE	11	11	1	6					
12-	CTUBE	12	12	2	5					
13-	CTUBE	13	13	1	8					
14-	CTUBE	14	14	4	5					
15-	CTUBE	15	15	4	7					
16-	CTUBE	16	16	3	8					
17-	CTUBE	17	17	2	7					
18-	CTUBE	18	18	3	6					
19-	CTUBE	19	19	1	7					
20-	CTUBE	20	20	2	8					
21-	CTUBE	21	21	3	5					
22-	CTUBE	22	22	4	6					
23-	CTUBE	23	23	5	6					
24-	CTUBE	24	24	5	8					
25-	CTUBE	25	25	7	8					
26-	CTUBE	26	26	6	7					
27-	CTUBE	27	27	5	7					
28-	CTUBE	28	28	6	8					
29-	CTUBE	29	29	5	9					
30-	CTUBE	30	30	6	10					
31-	CTUBE	31	31	7	11					
32-	CTUBE	32	32	8	12					
33-	CTUBE	33	33	5	10					
34-	CTUBE	34	34	6	9					
35-	CTUBE	35	35	5	12					
36-	CTUBE	36	36	8	9					
37-	CTUBE	37	37	8	11					
38-	CTUBE	38	38	7	12					
39-	CTUBE	39	39	6	11					
40-	CTUBE	40	40	7	10					
41-	CTUBE	41	41	5	11					
42-	CTUBE	42	42	6	12					
43-	CTUBE	43	43	7	9					
44-	CTUBE	44	44	8	10					
45-	CTUBE	45	45	9	10					

TRUSS TAIL BOOM MODEL3 **A 138 ELEMENT VERSION
DAMAGE CRITITION = NONE

S O R T E D B U L K D A T A E C H O

CARD COUNT	1	2	3	4	5	6	7	8	9	10
46-	CTUBE 46	46	9	12						
47-	CTUBE 47	47	11	12						
48-	CTUBE 48	48	10	11						
49-	CTUBE 49	49	9	11						
50-	CTUBE 50	50	10	12						
51-	CTUBE 51	51	9	13						
52-	CTUBE 52	52	10	14						
53-	CTUBE 53	53	11	15						
54-	CTUBE 54	54	12	16						
55-	CTUBE 55	55	9	14						
56-	CTUBE 56	56	10	13						
57-	CTUBE 57	57	9	16						
58-	CTUBE 58	58	12	13						
59-	CTUBE 59	59	12	15						
60-	CTUBE 60	60	11	16						
61-	CTUBE 61	61	10	15						
62-	CTUBE 62	62	11	14						
63-	CTUBE 63	63	9	15						
64-	CTUBE 64	64	10	16						
65-	CTUBE 65	65	11	13						
66-	CTUBE 66	66	12	14						
67-	CTUBE 67	67	13	14						
68-	CTUBE 68	68	13	16						
69-	CTUBE 69	69	15	16						
70-	CTUBE 70	70	14	15						
71-	CTUBE 71	71	13	15						
72-	CTUBE 72	72	14	16						
73-	CTUBE 73	73	13	17						
74-	CTUBE 74	74	14	18						
75-	CTUBE 75	75	15	19						
76-	CTUBE 76	76	16	20						
77-	CTUBE 77	77	13	18						
78-	CTUBE 78	78	14	17						
79-	CTUBE 79	79	13	20						
80-	CTUBE 80	80	16	17						
81-	CTUBE 81	81	16	19						
82-	CTUBE 82	82	15	20						
83-	CTUBE 83	83	14	19						
84-	CTUBE 84	84	15	18						
85-	CTUBE 85	85	13	19						
86-	CTUBE 86	86	14	20						
87-	CTUBE 87	87	15	17						
88-	CTUBE 88	88	16	18						
89-	CTUBE 89	89	17	18						
90-	CTUBE 90	90	17	20						

SORTED BULK DATA ECHO

CARD COUNT	1 ..	2 ..	3 ..	4 ..	5 ..	6 ..	7 ..	8 ..	9 ..	10 ..
91-	CTUBE 91	91	19	20						
92-	CTUBE 92	92	18	19						
93-	CTUBE 93	93	17	19						
94-	CTUBE 94	94	18	20						
95-	CTUBE 95	95	17	21						
96-	CTUBE 96	96	18	22						
97-	CTUBE 97	97	19	23						
98-	CTUBE 98	98	20	24						
99-	CTUBE 99	99	17	22						
100-	CTUBE 100	100	18	21						
101-	CTUBE 101	101	17	24						
102-	CTUBE 102	102	20	21						
103-	CTUBE 103	103	20	23						
104-	CTUBE 104	104	19	24						
105-	CTUBE 105	105	18	23						
106-	CTUBE 106	106	19	22						
107-	CTUBE 107	107	17	23						
108-	CTUBE 108	108	18	24						
109-	CTUBE 109	109	19	21						
110-	CTUBE 110	110	20	22						
111-	CTUBE 111	111	21	22						
112-	CTUBE 112	112	21	24						
113-	CTUBE 113	113	23	24						
114-	CTUBE 114	114	22	23						
115-	CTUBE 115	115	21	23						
116-	CTUBE 116	116	22	24						
117-	CTUBE 117	117	21	25						
118-	CTUBE 118	118	22	26						
119-	CTUBE 119	119	23	27						
120-	CTUBE 120	120	24	28						
121-	CTUBE 121	121	21	26						
122-	CTUBE 122	122	22	25						
123-	CTUBE 123	123	21	28						
124-	CTUBE 124	124	24	25						
125-	CTUBE 125	125	24	27						
126-	CTUBE 126	126	23	28						
127-	CTUBE 127	127	22	27						
128-	CTUBE 128	128	23	26						
129-	CTUBE 129	129	21	27						
130-	CTUBE 130	130	22	28						
131-	CTUBE 131	131	23	25						
132-	CTUBE 132	132	24	26						
133-	CTUBE 133	133	25	26						
134-	CTUBE 134	134	25	28						
135-	CTUBE 135	135	27	24						

CARD	1	2	3	4	5	6	7	8	9	10
136-	CTUBE	136	136	26	27					
137-	CTUBE	137	137	25	27					
138-	CTUBE	138	138	26	28					
139-	DSFACT	200	1.60422	2.40632	3.20843					
140-	FORCE	11	13	0	44.2200	0	0.0			-1.
141-	FORCE	11	14	0	44.2200	0	0.0			-1.
142-	FORCE	11	15	0	44.2200	0	0.0			-1.
143-	FORCE	11	16	0	44.2200	0	0.0			-1.
144-	FORCE	11	25	0	464.5	1.	0.0			0.0
145-	FORCE	11	25	0	527.3	0	-1.0			0.0
146-	FORCE	11	26	0	464.5	1.0	0.0			0.0
147-	FORCE	11	26	0	527.3	0	1.			0.0
148-	FORCE	11	27	0	464.5	-1.	0.0			0.0
149-	FORCE	11	27	0	527.5	0	1.			0.0
150-	FORCE	11	28	0	464.5	-1.	0.0			0.0
151-	FORCE	11	28	0	527.3	0	-1.			0.0
152-	GRUSET									456
153-	GRID	1	.000	11.95	12.375					
154-	GRID	2	.000	11.75	-12.375					
155-	GRID	3	.000	-11.75	-12.375					
156-	GRID	4	.000	-11.95	12.375					
157-	GRID	5	33.5	10.666	11.105					
158-	GRID	6	33.5	10.485	-11.105					
159-	GRID	7	33.5	-10.485	-11.105					
160-	GRID	8	33.5	-10.666	11.105					
161-	GRID	9	66.5	9.401	9.855					
162-	GRID	10	66.5	9.239	-9.855					
163-	GRID	11	66.5	-9.239	-9.855					
164-	GRID	12	66.5	-9.401	9.855					
165-	GRID	13	99.5	8.136	8.604					
166-	GRID	14	99.5	7.994	-8.604					
167-	GRID	15	99.5	-7.994	-8.604					
168-	GRID	16	99.5	-8.136	8.604					
169-	GRID	17	127.5	7.063	7.543					
170-	GRID	18	127.5	6.937	-7.543					
171-	GRID	19	127.5	-6.937	-7.543					
172-	GRID	20	127.5	-7.063	7.543					
173-	GRID	21	151.5	6.143	6.634					
174-	GRID	22	151.5	6.031	-6.634					
175-	GRID	23	151.5	-6.031	-6.634					
176-	GRID	24	151.5	-6.143	6.634					
177-	GRID	25	173.5	5.3	5.8					
178-	GRID	26	173.5	5.2	-5.8					
179-	GRID	27	173.5	-5.2	-5.8					
180-	GRID	28	173.5	-5.3	5.800					

DAMAGE CRITICON = NONE

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
181-	MAT1	1	10.5E6	3.8E6	.33	.1					+MAT001
182-	+MAT001	4.38+04	3.51+04								+MAT002
183-	MAT1	2	10.5E6	3.8E6	.33	.1					+MAT003
184-	+MAT002	4.70+04	3.76+04								+MAT004
185-	MAT1	3	10.5E6	3.8E6	.33	.1					+MAT005
186-	+MAT003	4.38+04	3.51+04								+MAT006
187-	MAT1	4	10.5E6	3.8E6	.33	.1					+MAT007
188-	+MAT004	4.86+04	3.89+04								+MAT008
189-	MAT1	5	10.5E6	3.8E6	.33	.1					+MAT009
190-	+MAT005	2.29+04	1.83+04								+MAT010
191-	MAT1	6	10.5E6	3.8E6	.33	.1					+MAT011
192-	+MAT006	2.29+04	1.83+04								+MAT012
193-	MAT1	7	10.5E6	3.8E6	.33	.1					+MAT013
194-	+MAT007	2.38+04	1.91+04								+MAT014
195-	MAT1	8	10.5E6	3.8E6	.33	.1					+MAT015
196-	+MAT008	2.38+04	1.91+04								+MAT016
197-	MAT1	9	10.5E6	3.8E6	.33	.1					+MAT017
198-	+MAT009	2.38+04	1.91+04								+MAT018
199-	MAT1	10	10.5E6	3.8E6	.33	.1					+MAT019
200-	+MAT010	2.38+04	1.91+04								+MAT020
201-	MAT1	11	10.5E6	3.8E6	.33	.1					+MAT021
202-	+MAT011	1.60+04	1.28+04								+MAT022
203-	MAT1	12	10.5E6	3.8E6	.33	.1					+MAT023
204-	+MAT012	1.60+04	1.28+04								
205-	MAT1	13	10.5E6	3.8E6	.33	.1					
206-	+MAT013	1.64+04	1.31+04								
207-	MAT1	14	10.5E6	3.8E6	.33	.1					
208-	+MAT014	1.64+04	1.31+04								
209-	MAT1	15	10.5E6	3.8E6	.33	.1					
210-	+MAT015	1.60+04	1.28+04								
211-	MAT1	16	10.5E6	3.8E6	.33	.1					
212-	+MAT016	1.60+04	1.28+04								
213-	MAT1	17	10.5E6	3.8E6	.33	.1					
214-	+MAT017	1.06+04	1.03+04								
215-	MAT1	18	10.5E6	3.8E6	.33	.1					
216-	+MAT018	1.66+04	1.33+04								
217-	MAT1	19	10.5E6	3.8E6	.33	.1					
218-	+MAT019	1.23+04	9.86+03								
219-	MAT1	20	10.5E6	3.8E6	.33	.1					
220-	+MAT020	1.23+04	9.87+03								
221-	MAT1	21	10.5E6	3.8E6	.33	.1					
222-	+MAT021	1.23+04	9.87+03								
223-	MAT1	22	10.5E6	3.8E6	.33	.1					
224-	+MAT022	1.23+04	9.86+03								
225-	MAT1	23	10.5E6	3.8E6	.33	.1					

S C R T E D B U L K D A T A E C H O

CARD COUNT	1 ..	2 ..	3 ..	4 ..	5 ..	6 ..	7 ..	8 ..	9 ..	10 ..
226-	+MAT023	5.44+04	4.35+04							+MAT024
227-	MAT1	24	10.5E6	3.8E6	.33					
228-	+MAT024	5.90+04	4.72+04							+MAT025
229-	MAT1	25	10.5E6	3.8E6	.33					
230-	+MAT025	5.44+04	4.35+04							+MAT026
231-	MAT1	26	10.5E6	3.8E6	.33					
232-	+MAT026	6.10+04	4.88+04							+MAT027
233-	MAT1	27	10.5E6	3.8E6	.33					
234-	+MAT027	2.85+04	2.28+04							+MAT028
235-	MAT1	28	10.5E6	3.8E6	.33					
236-	+MAT028	2.85+04	2.28+04							+MAT029
237-	MAT1	29	10.5E6	3.8E6	.33					
238-	+MAT029	2.46+04	1.97+04							+MAT030
239-	MAT1	30	10.5E6	3.8E6	.33					
240-	+MAT030	2.46+04	1.97+04							+MAT031
241-	MAT1	31	10.5E6	3.8E6	.33					
242-	+MAT031	2.46+04	1.97+04							+MAT032
243-	MAT1	32	10.5E6	3.8E6	.33					
244-	+MAT032	2.46+04	1.97+04							+MAT033
245-	MAT1	33	10.5E6	3.8E6	.33					
246-	+MAT033	1.75+04	1.40+04							+MAT034
247-	MAT1	34	10.5E6	3.8E6	.33					
248-	+MAT034	1.75+04	1.40+04							+MAT035
249-	MAT1	35	10.5E6	3.8E6	.33					
250-	+MAT035	1.80+04	1.44+04							+MAT036
251-	MAT1	36	10.5E6	3.8E6	.33					
252-	+MAT036	1.80+04	1.44+04							+MAT037
253-	MAT1	37	10.5E6	3.8E6	.33					
254-	+MAT037	1.75+04	1.40+04							+MAT038
255-	MAT1	38	10.5E6	3.8E6	.33					
256-	+MAT038	1.75+04	1.40+04							+MAT039
257-	MAT1	39	10.5E6	3.8E6	.33					
258-	+MAT039	1.81+04	1.45+04							+MAT040
259-	MAT1	40	10.5E6	3.8E6	.33					
260-	+MAT040	1.81+04	1.45+04							+MAT041
261-	MAT1	41	10.5E6	3.8E6	.33					
262-	+MAT041	1.39+04	1.12+04							+MAT042
263-	MAT1	42	10.5E6	3.8E6	.33					
264-	+MAT042	1.4C+04	1.12+04							+MAT043
265-	MAT1	43	10.5E6	3.8E6	.33					
266-	+MAT043	1.40+04	1.12+04							+MAT044
267-	MAT1	44	10.5E6	3.8E6	.33					
268-	+MAT044	1.39+04	1.12+04							+MAT045
269-	MAT1	45	10.5E6	3.8E6	.33					
270-	+MAT045	6.91+04	5.53+04							

TRUSS TAIL BOOM MODEL3 **A 138 ELEMENT VERSION
DAMAGE CRITERION = NONE

CARD	1	2	3	4	5	6	7	8	9
271-	MAT1	46	10.5E6	3.8E6	.33	.1			
272-	+MAT046	7.59+04	6.08+04						+MAT046
273-	MAT1	47	10.5E6	3.8E6	.33	.1			+MAT047
274-	+MAT047	6.91+04	5.53+04						+MAT048
275-	MAT1	48	10.5E6	3.8E6	.33	.1			+MAT049
276-	+MAT048	7.86+04	6.29+04						+MAT050
277-	MAT1	49	10.5E6	3.8E6	.33	.1			+MAT051
278-	+MAT049	3.65+04	2.92+04						+MAT052
279-	MAT1	50	10.5E6	3.8E6	.33	.1			+MAT053
280-	+MAT050	3.65+04	2.92+04						+MAT054
281-	MAT1	51	10.5E6	3.8E6	.33	.1			+MAT055
282-	+MAT051	2.46+04	1.97+04						+MAT056
283-	MAT1	52	10.5E6	3.8E6	.33	.1			+MAT057
284-	+MAT052	2.46+04	1.97+04						+MAT058
285-	MAT1	53	10.5E6	3.8E6	.33	.1			+MAT059
286-	+MAT053	2.46+04	1.97+04						+MAT060
287-	MAT1	54	10.5E6	3.8E6	.33	.1			+MAT061
288-	+MAT054	2.46+04	1.97+04						+MAT062
289-	MAT1	55	10.5E6	3.8E6	.33	.1			+MAT063
290-	+MAT055	1.87+04	1.50+04						+MAT064
291-	MAT1	56	10.5E6	3.8E6	.33	.1			+MAT065
292-	+MAT056	1.88+04	1.50+04						+MAT066
293-	MAT1	57	10.5E6	3.8E6	.33	.1			+MAT067
294-	+MAT057	1.92+04	1.54+04						+MAT068
295-	MAT1	58	10.5E6	3.8E6	.33	.1			
296-	+MAT058	1.92+04	1.54+04						
297-	MAT1	59	10.5E6	3.8E6	.33	.1			
298-	+MAT059	1.87+04	1.50+04						
299-	MAT1	60	10.5E6	3.8E6	.33	.1			
300-	+MAT060	1.88+04	1.50+04						
301-	MAT1	61	10.5E6	3.8E6	.33	.1			
302-	+MAT061	1.93+04	1.55+04						
303-	MAT1	62	10.5E6	3.8E6	.33	.1			
304-	+MAT062	1.93+04	1.55+04						
305-	MAT1	63	10.5E6	3.8E6	.33	.1			
306-	+MAT063	1.55+04	1.24+04						
307-	MAT1	64	10.5E6	3.8E6	.33	.1			
308-	+MAT064	1.55+04	1.24+04						
309-	MAT1	65	10.5E6	3.8E6	.33	.1			
310-	+MAT065	1.55+04	1.24+04						
311-	MAT1	66	10.5E6	3.8E6	.33	.1			
312-	+MAT066	1.55+04	1.24+04						
313-	MAT1	67	10.5E6	3.8E6	.33	.1			
314-	+MAT067	9.66+04	7.25+04						
315-	MAT1	68	10.5E6	3.8E6	.33	.1			

DAMAGE CRITERION = NONE

SCRTE D BULK DATA ECHO

CARD COUNT	1	2	3	4	5	6	7	8	9	10
316-	+MAT068	1.01+05	8.11+04							
317-	MAT1	69	10.5E6	3.8E6	.33	.1				+MAT069
318-	+MAT069	9.06+04	7.25+04							+MAT070
319-	MAT1	70	10.5E6	3.8E6	.33	.1				+MAT071
320-	+MAT070	1.05+05	8.40+04							+MAT072
321-	MAT1	71	10.5E6	3.8E6	.33	.1				+MAT073
322-	+MAT071	4.82+04	3.86+04							+MAT074
323-	MAT1	72	10.5E6	3.8E6	.33	.1				+MAT075
324-	+MAT072	4.82+04	3.86+04							+MAT076
325-	MAT1	73	10.5E6	3.8E6	.33	.1				+MAT077
326-	+MAT073	3.41+04	2.73+04							+MAT078
327-	MAT1	74	10.5E6	3.8E6	.33	.1				+MAT079
328-	+MAT074	3.41+04	2.73+04							+MAT080
329-	MAT1	75	10.5E6	3.8E6	.33	.1				+MAT081
330-	+MAT075	3.41+04	2.73+04							+MAT082
331-	MAT1	76	10.5E6	3.8E6	.33	.1				+MAT083
332-	+MAT076	3.41+04	2.73+04							+MAT084
333-	MAT1	77	10.5E6	3.8E6	.33	.1				+MAT085
334-	+MAT077	2.57+04	2.05+04							+MAT086
335-	MAT1	78	10.5E6	3.8E6	.33	.1				+MAT087
336-	+MAT078	2.57+04	2.05+04							+MAT088
337-	MAT1	79	10.5E6	3.8E6	.33	.1				+MAT089
338-	+MAT079	2.64+04	2.11+04							+MAT090
339-	MAT1	80	10.5E6	3.8E6	.33	.1				
340-	+MAT080	2.64+04	2.11+04							
341-	MAT1	81	10.5E6	3.8E6	.33	.1				
342-	+MAT081	2.57+04	2.05+04							
343-	MAT1	82	10.5E6	3.8E6	.33	.1				
344-	+MAT082	2.57+04	2.05+04							
345-	MAT1	83	10.5E6	3.8E6	.33	.1				
346-	+MAT083	2.66+04	2.13+04							
347-	MAT1	84	10.5E6	3.8E6	.33	.1				
348-	+MAT084	2.66+04	2.13+04							
349-	MAT1	85	10.5E6	3.8E6	.33	.1				
350-	+MAT085	2.11+04	1.69+04							
351-	MAT1	86	10.5E6	3.8E6	.33	.1				
352-	+MAT086	2.11+04	1.69+04							
353-	MAT1	87	10.5E6	3.8E6	.33	.1				
354-	+MAT087	2.11+04	1.69+04							
355-	MAT1	88	10.5E6	3.8E6	.33	.1				
356-	+MAT088	2.11+04	1.69+04							
357-	MAT1	89	10.5E6	3.8E6	.33	.1				
358-	+MAT089	1.18+05	9.43+04							
359-	MAT1	90	10.5E6	3.8E6	.33	.1				
360-	+MAT090	1.34+05	1.08+05							

TRUSS TAIL BOOM MODEL3 ***A 138 LLEMENT VERSION
DAMAGE CRITION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
361-	MAT1 91	10.5E6	3.8E6	.33	.1					+MAT091
362-	+MAT091	1.18+05	9.43+04							+MAT092
363-	MAT1 92	10.5E6	3.8E6	.33	.1					+MAT093
364-	+MAT092	1.40+05	1.12+05							+MAT094
365-	MAT1 93	10.5E6	3.8E6	.33	.1					+MAT095
366-	+MAT093	6.34+04	5.07+04							+MAT096
367-	MAT1 94	10.5E6	3.8E6	.33	.1					+MAT097
368-	+MAT094	6.34+04	5.07+04							+MAT098
369-	MAT1 95	10.5E6	3.8E6	.33	.1					+MAT099
370-	+MAT095	4.65+04	3.72+04							+MAT100
371-	MAT1 96	10.5E6	3.8E6	.33	.1					+MAT101
372-	+MAT096	4.65+04	3.72+04							+MAT102
373-	MAT1 97	10.5E6	3.8E6	.33	.1					+MAT103
374-	+MAT097	4.65+04	3.72+04							+MAT104
375-	MAT1 98	10.5E6	3.8E6	.33	.1					+MAT105
376-	+MAT098	4.65+04	3.72+04							+MAT106
377-	MAT1 99	10.5E6	3.8E6	.33	.1					+MAT107
378-	+MAT099	3.45+04	2.76+04							+MAT108
379-	MAT1 100	10.5E6	3.8E6	.33	.1					+MAT109
380-	+MAT100	3.45+04	2.76+04							+MAT110
381-	MAT1 101	10.5E6	3.8E6	.33	.1					+MAT111
382-	+MAT101	3.57+04	2.86+04							+MAT112
383-	MAT1 102	10.5E6	3.8E6	.33	.1					+MAT113
384-	+MAT102	3.57+04	2.86+04							
385-	MAT1 103	10.5E6	3.8E6	.33	.1					
386-	+MAT103	3.45+04	2.76+04							
387-	MAT1 104	10.5E6	3.8E6	.33	.1					
388-	+MAT104	3.45+04	2.76+04							
389-	MAT1 105	10.5E6	3.8E6	.33	.1					
390-	+MAT105	3.45+04	2.76+04							
391-	MAT1 106	10.5E6	3.8E6	.33	.1					
392-	+MAT106	3.45+04	2.76+04							
393-	MAT1 107	10.5E6	3.8E6	.33	.1					
394-	+MAT107	2.83+04	2.26+04							
395-	MAT1 108	10.5E6	3.8E6	.33	.1					
396-	+MAT108	2.83+04	2.27+04							
397-	MAT1 109	10.5E6	3.8E6	.33	.1					
398-	+MAT109	2.83+04	2.27+04							
399-	MAT1 110	10.5E6	3.8E6	.33	.1					
400-	+MAT110	2.83+04	2.26+04							
401-	MAT1 111	10.5E6	3.8E6	.33	.1					
402-	+MAT111	1.32+05	1.22+05							
403-	MAT1 112	10.5E6	3.8E6	.33	.1					
404-	+MAT112	1.78+05	1.42+05							
405-	MAT1 113	10.5E6	3.8E6	.33	.1					

S O R T E D H U L K D A T A E C H O

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
406-		+MAT113	1.52+05	1.22+05							+MAT114
407-		MAT1	114	10.5E6	3.8E6	.33	.1				+MAT115
408-		+MAT114	1.85+05	1.48+05							+MAT116
409-		MAT1	115	10.5E6	3.8E6	.33	.1				+MAT117
410-		+MAT115	8.28+04	6.62+04							+MAT118
411-		MAT1	116	10.5E6	3.8E6	.33	.1				+MAT119
412-		+MAT116	8.28+04	6.62+04							+MAT120
413-		MAT1	117	10.5E6	3.8E6	.33	.1				+MAT121
414-		+MAT117	5.53+04	4.42+04							+MAT122
415-		MAT1	118	10.5E6	3.8E6	.33	.1				+MAT123
416-		+MAT118	5.53+04	4.42+04							+MAT124
417-		MAT1	119	10.5E6	3.8E6	.33	.1				+MAT125
418-		+MAT119	5.53+04	4.42+04							+MAT126
419-		MAT1	120	10.5E6	3.8E6	.33	.1				+MAT127
420-		+MAT120	5.53+04	4.42+04							+MAT128
421-		MAT1	121	10.5E6	3.8E6	.33	.1				+MAT129
422-		+MAT121	4.20+04	3.36+04							+MAT130
423-		MAT1	122	10.5E6	3.8E6	.33	.1				+MAT131
424-		+MAT122	4.20+04	3.36+04							+MAT132
425-		MAT1	123	10.5E6	3.8E6	.33	.1				+MAT133
426-		+MAT123	4.36+04	3.49+04							+MAT134
427-		MAT1	124	10.5E6	3.8E6	.33	.1				+MAT135
428-		+MAT124	4.36+04	3.49+04							
429-		MAT1	125	10.5E6	3.8E6	.33	.1				
430-		+MAT125	4.20+04	3.36+04							
431-		MAT1	126	10.5E6	3.8E6	.33	.1				
432-		+MAT126	4.20+04	3.36+04							
433-		MAT1	127	10.5E6	3.8E6	.33	.1				
434-		+MAT127	4.40+04	3.52+04							
435-		MAT1	128	10.5E6	3.8E6	.33	.1				
436-		+MAT128	4.40+04	3.52+04							
437-		MAT1	129	10.5E6	3.8E6	.33	.1				
438-		+MAT129	3.50+04	2.80+04							
439-		MAT1	130	10.5E6	3.8E6	.33	.1				
440-		+MAT130	3.50+04	2.80+04							
441-		MAT1	131	10.5E6	3.8E6	.33	.1				
442-		+MAT131	3.50+04	2.80+04							
443-		MAT1	132	10.5E6	3.8E6	.33	.1				
444-		+MAT132	3.50+04	2.80+04							
445-		MAT1	133	10.5E6	3.8E6	.33	.1				
446-		+MAT133	1.99+05	1.60+05							
447-		MAT1	134	10.5E6	3.8E6	.33	.1				
448-		+MAT134	2.39+05	1.91+05							
449-		MAT1	135	10.5E6	3.8E6	.33	.1				
450-		+MAT135	1.99+05	1.60+05							

SORTED BULK DATA ECHO

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
451-	MAT1	136	10.5E6	3.8E6	.33	.1					+MAT136
452-	+MAT136	2.48+05	1.99+05								
453-	MAT1	137	10.5E6	3.8E6	.33	.1					+MAT137
454-	+MAT137	1.10+05	8.77+04								
455-	MAT1	138	10.5E6	3.8E6	.33	.1					+MAT138
456-	+MAT138	1.10+05	8.77+04								
457-	PARAM	GRDPNT	0								
458-	PTUBE	1	1	1.5	.0625						
459-	PTUBE	2	2	1.5	.0625						
460-	PTUBE	3	3	1.5	.0625						
461-	PTUBE	4	4	1.5	.0625						
462-	PTUBE	5	5	1.5	.0625						
463-	PTUBE	6	6	1.5	.0625						
464-	PTUBE	7	7	1.5	.0625						
465-	PTUBE	8	8	1.5	.0625						
466-	PTUBE	9	9	1.5	.0625						
467-	PTUBE	10	10	1.5	.0625						
468-	PTUBE	11	11	1.5	.0625						
469-	PTUBE	12	12	1.5	.0625						
470-	PTUBE	13	13	1.5	.0625						
471-	PTUBE	14	14	1.5	.0625						
472-	PTUBE	15	15	1.5	.0625						
473-	PTUBE	16	16	1.5	.0625						
474-	PTUBE	17	17	1.5	.0625						
475-	PTUBE	18	18	1.5	.0625						
476-	PTUBE	19	19	1.5	.0625						
477-	PTUBE	20	20	1.5	.0625						
478-	PTUBE	21	21	1.5	.0625						
479-	PTUBE	22	22	1.5	.0625						
480-	PTUBE	23	23	1.5	.0625						
481-	PTUBE	24	24	1.5	.0625						
482-	PTUBE	25	25	1.5	.0625						
483-	PTUBE	26	26	1.5	.0625						
484-	PTUBE	27	27	1.5	.0625						
485-	PTUBE	28	28	1.5	.0625						
486-	PTUBE	29	29	1.5	.0625						
487-	PTUBE	30	30	1.5	.0625						
488-	PTUBE	31	31	1.5	.0625						
489-	PTUBE	32	32	1.5	.0625						
490-	PTUBE	33	33	1.5	.0625						
491-	PTUBE	34	34	1.5	.0625						
492-	PTUBE	35	35	1.5	.0625						
493-	PTUBE	36	36	1.5	.0625						
494-	PTUBE	37	37	1.5	.0625						
495-	PTUBE	38	38	1.5	.0625						

SORTED BULK DATA ECHO

CARD	1	2	3	4	5	6	7	8	9	10
496-	PTUBE 39	39	39	1.5	.0625					
497-	PTUBE 40	40	40	1.5	.0625					
498-	PTUBE 41	41	41	1.5	.0625					
499-	PTUBE 42	42	42	1.5	.0625					
500-	PTUBE 43	43	43	1.5	.0625					
501-	PTUBE 44	44	44	1.5	.0625					
502-	PTUBE 45	45	45	1.5	.0625					
503-	PTUBE 46	46	46	1.5	.0625					
504-	PTUBE 47	47	47	1.5	.0625					
505-	PTUBE 48	48	48	1.5	.0625					
506-	PTUBE 49	49	49	1.5	.0625					
507-	PTUBE 50	50	50	1.5	.0625					
508-	PTUBE 51	51	51	1.5	.0625					
509-	PTUBE 52	52	52	1.5	.0625					
510-	PTUBE 53	53	53	1.5	.0625					
511-	PTUBE 54	54	54	1.5	.0625					
512-	PTUBE 55	55	55	1.5	.0625					
513-	PTUBE 56	56	56	1.5	.0625					
514-	PTUBE 57	57	57	1.5	.0625					
515-	PTUBE 58	58	58	1.5	.0625					
516-	PTUBE 59	59	59	1.5	.0625					
517-	PTUBE 60	60	60	1.5	.0625					
518-	PTUBE 61	61	61	1.5	.0625					
519-	PTUBE 62	62	62	1.5	.0625					
520-	PTUBE 63	63	63	1.5	.0625					
521-	PTUBE 64	64	64	1.5	.0625					
522-	PTUBE 65	65	65	1.5	.0625					
523-	PTUBE 66	66	66	1.5	.0625					
524-	PTUBE 67	67	67	1.5	.0625					
525-	PTUBE 68	68	68	1.5	.0625					
526-	PTUBE 69	69	69	1.5	.0625					
527-	PTUBE 70	70	70	1.5	.0625					
528-	PTUBE 71	71	71	1.5	.0625					
529-	PTUBE 72	72	72	1.5	.0625					
530-	PTUBE 73	73	73	1.5	.0625					
531-	PTUBE 74	74	74	1.5	.0625					
532-	PTUBE 75	75	75	1.5	.0625					
533-	PTUBE 76	76	76	1.5	.0625					
534-	PTUBE 77	77	77	1.5	.0625					
535-	PTUBE 78	78	78	1.5	.0625					
536-	PTUBE 79	79	79	1.5	.0625					
537-	PTUBE 80	80	80	1.5	.0625					
538-	PTUBE 81	81	81	1.5	.0625					
539-	PTUBE 82	82	82	1.5	.0625					
540-	PTUBE 83	83	83	1.5	.0625					

TRUSS TAIL BOOM MODEL3 ***A 138 ELEMENT VERSION
DAMAGE CRITTIION = NONE

CARD COUNT	1	2	3	4	5	6	7	8	9	10
541-	PTUBE 84	84	1.5	.0625						
542-	PTUBE 85	85	1.5	.0625						
543-	PTUBE 86	86	1.5	.0625						
544-	PTUBE 87	87	1.5	.0625						
545-	PTUBE 88	88	1.5	.0625						
546-	PTUBE 89	89	1.5	.0625						
547-	PTUBE 90	90	1.5	.0625						
548-	PTUBE 91	91	1.5	.0625						
549-	PTUBE 92	92	1.5	.0625						
550-	PTUBE 93	93	1.5	.0625						
551-	PTUBE 94	94	1.5	.0625						
552-	PTUBE 95	95	1.5	.0625						
553-	PTUBE 96	96	1.5	.0625						
554-	PTUBE 97	97	1.5	.0625						
555-	PTUBE 98	98	1.5	.0625						
556-	PTUBE 99	99	1.5	.0625						
557-	PTUBE 100	100	1.5	.0625						
558-	PTUBE 101	101	1.5	.0625						
559-	PTUBE 102	102	1.5	.0625						
560-	PTUBE 103	103	1.5	.0625						
561-	PTUBE 104	104	1.5	.0625						
562-	PTUBE 105	105	1.5	.0625						
563-	PTUBE 106	106	1.5	.0625						
564-	PTUBE 107	107	1.5	.0625						
565-	PTUBE 108	108	1.5	.0625						
566-	PTUBE 109	109	1.5	.0625						
567-	PTUBE 110	110	1.5	.0625						
568-	PTUBE 111	111	1.5	.0625						
569-	PTUBE 112	112	1.5	.0625						
570-	PTUBE 113	113	1.5	.0625						
571-	PTUBE 114	114	1.5	.0625						
572-	PTUBE 115	115	1.5	.0625						
573-	PTUBE 116	116	1.5	.0625						
574-	PTUBE 117	117	1.5	.0625						
575-	PTUBE 118	118	1.5	.0625						
576-	PTUBE 119	119	1.5	.0625						
577-	PTUBE 120	120	1.5	.0625						
578-	PTUBE 121	121	1.5	.0625						
579-	PTUBE 122	122	1.5	.0625						
580-	PTUBE 123	123	1.5	.0625						
581-	PTUBE 124	124	1.5	.0625						
582-	PTUBE 125	125	1.5	.0625						
583-	PTUBE 126	126	1.5	.0625						
584-	PTUBE 127	127	1.5	.0625						
585-	PTUBE 128	128	1.5	.0625						

CARD	COUNT	1	2	3	4	5	6	7	8	9	10
585-	PTUBE	129	129	1.5	0.625						
587-	PTUBE	130	130	1.5	0.625						
588-	PTUBE	131	131	1.5	0.625						
589-	PTUBL	132	132	1.5	0.625						
590-	PTUBE	133	133	1.5	0.625						
591-	PTUBE	134	134	1.5	0.625						
592-	PTUBE	135	135	1.5	0.625						
593-	PTUBE	136	136	1.5	0.625						
594-	PTUBL	137	137	1.5	0.625						
595-	PTUBE	138	138	1.5	0.625						
596-	SPC	10	1	123456		2	123456				
597-	SPC	10	3	123456		4	123456				
	ENDDATA										

* 12.0 CPU-S 61.0 COR-S 83 ELP-S. XGPI
 NO ERRORS FOUND - EXECUTE NASTRAN PROGRAM
 * 15.3 CPU-S 65.3 COR-S 87 ELP-S. SEM1 END
 * 15.3 CPU-S 65.6 COR-S 87 ELP-S. ---- LINK END ---

SUBCASE 1

LINEAR CASE 30 * LOADING

D I S P L A C E M E N T V E C T O R

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	3.824586-03	-8.002697-03	1.239147-03	.0	.0	.0
6	6	-6.296042-04	3.914426-03	1.846044-03	.0	.0	.0
7	6	-3.686554-03	3.156076-03	-9.398228-03	.0	.0	.0
8	6	5.239937-04	-7.229598-03	-8.782766-03	.0	.0	.0
9	6	6.610921-03	-2.175839-02	-2.567162-03	.0	.0	.0
10	6	-2.368843-04	2.303234-03	-2.075979-03	.0	.0	.0
11	6	-6.435060-03	1.945657-03	-2.499642-02	.0	.0	.0
12	6	9.741511-05	-2.139398-02	-2.450107-02	.0	.0	.0
13	6	9.146073-03	-4.387943-02	-8.707179-03	.0	.0	.0
14	6	1.206440-03	-4.716482-03	-8.338110-03	.0	.0	.0
15	6	-7.922483-03	-4.710570-03	-4.543954-02	.0	.0	.0
16	6	-1.385646-03	-4.388671-02	-4.507126-02	.0	.0	.0
17	6	9.036464-03	-6.966224-02	-1.391069-02	.0	.0	.0
18	6	2.886190-03	-1.779398-02	-1.364049-02	.0	.0	.0
19	6	-8.772825-03	-1.779401-02	-6.206533-02	.0	.0	.0
20	6	-3.109049-03	-6.966215-02	-6.179508-02	.0	.0	.0
21	6	9.857841-03	-9.855769-02	-1.861497-02	.0	.0	.0
22	6	4.305520-03	-3.607603-02	-1.843069-02	.0	.0	.0
23	6	-9.480291-03	-3.607603-02	-7.607050-02	.0	.0	.0
24	6	-4.641686-03	-9.855770-02	-7.588623-02	.0	.0	.0
25	6	1.072468-02	-1.339295-01	-2.298322-02	.0	.0	.0
26	6	5.354045-03	-5.878662-02	-2.328369-02	.0	.0	.0
27	6	-9.875625-03	-5.878632-02	-8.844667-02	.0	.0	.0
28	6	-6.161680-03	-1.339296-01	-8.874706-02	.0	.0	.0

TRUSS TAIL BOOM MODEL3 **A 138 ELEMENT VERSION
DAMAGE CRITERION = NONE

SUBCASE 2

INCREMENTAL STIFFNESS 50 % LOADING

DISPLACEMENT VECTOR

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	6.281367-03	-1.290758-02	1.840769-03	.0	.0	.0
6	6	-1.113541-03	6.320952-03	2.833394-03	.0	.0	.0
7	6	-6.069280-03	5.062479-03	-1.526184-02	.0	.0	.0
8	6	9.520196-04	-1.160466-02	-1.427592-02	.0	.0	.0
9	6	1.093392-02	-3.508677-02	-4.808997-03	.0	.0	.0
10	6	-5.700293-04	3.676014-03	-4.001624-03	.0	.0	.0
11	6	-1.058286-02	3.073215-03	-4.088399-02	.0	.0	.0
12	6	3.735691-04	-3.443918-02	-4.009303-02	.0	.0	.0
13	6	1.346446-02	-7.077503-02	-1.564776-02	.0	.0	.0
14	6	1.670186-03	-7.724496-03	-1.504323-02	.0	.0	.0
15	6	-1.305685-02	-7.732561-03	-7.473497-02	.0	.0	.0
16	6	-1.908340-03	-7.072629-02	-7.415868-02	.0	.0	.0
17	6	1.496082-02	-1.123012-01	-2.523106-02	.0	.0	.0
18	6	4.313699-03	-2.881596-02	-2.478346-02	.0	.0	.0
19	6	-1.445805-02	-2.882510-02	-1.026548-01	.0	.0	.0
20	6	-4.594557-03	-1.122454-01	-1.022772-01	.0	.0	.0
21	6	1.631946-02	-1.588013-01	-3.414978-02	.0	.0	.0
22	6	6.570183-03	-5.824551-02	-3.383663-02	.0	.0	.0
23	6	-1.560526-02	-5.824007-02	-1.265726-01	.0	.0	.0
24	6	-7.003218-03	-1.587456-01	-1.262994-01	.0	.0	.0
25	6	1.770963-02	-2.156645-01	-4.258951-02	.0	.0	.0
26	6	8.250180-03	-9.476994-02	-4.318600-02	.0	.0	.0
27	6	-1.623571-02	-9.475413-02	-1.480426-01	.0	.0	.0
28	6	-9.431505-03	-2.156395-01	-1.484158-01	.0	.0	.0

INCREMENTAL STIFFNESS 75 * LOADING

SUBCASE 2

D I S P L A C E M E N T V E C T O R

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	9.533282-03	-1.941616-02	2.650673-03	.0	.0	.0
6	6	-1.747135-03	9.511817-03	4.154578-03	.0	.0	.0
7	6	-9.207624-03	7.592465-03	-2.303305-02	.0	.0	.0
8	6	1.512604-03	-1.741457-02	-2.155492-02	.0	.0	.0
9	6	1.656074-02	-5.277652-02	-7.732364-03	.0	.0	.0
10	6	-9.960997-04	5.494815-03	-6.506245-03	.0	.0	.0
11	6	-1.607215-02	4.568615-03	-6.191937-02	.0	.0	.0
12	6	7.220533-04	-5.175763-02	-6.073546-02	.0	.0	.0
13	6	2.049857-02	-1.064728-01	-2.473355-02	.0	.0	.0
14	6	2.308141-03	-1.171781-02	-2.381716-02	.0	.0	.0
15	6	-1.984633-02	-1.174316-02	-1.134944-01	.0	.0	.0
16	6	-2.623525-03	-1.063539-01	-1.126407-01	.0	.0	.0
17	6	2.279416-02	-1.689005-01	-4.003750-02	.0	.0	.0
18	6	6.235000-03	-4.344740-02	-3.935992-02	.0	.0	.0
19	6	-2.197997-02	-4.346799-02	-1.564087-01	.0	.0	.0
20	6	-6.598385-03	-1.687749-01	-1.557942-01	.0	.0	.0
21	6	2.486342-02	-2.387751-01	-5.444707-02	.0	.0	.0
22	6	9.604355-03	-8.767548-02	-5.396424-02	.0	.0	.0
23	6	-2.370997-02	-8.766325-02	-1.932925-01	.0	.0	.0
24	6	-1.017334-02	-2.3866495-01	-1.928997-01	.0	.0	.0
25	6	2.694789-02	-3.241742-01	-6.816286-02	.0	.0	.0
26	6	1.212250-02	-1.425366-01	-6.916410-02	.0	.0	.0
27	6	-2.465255-02	-1.425034-01	-2.267200-01	.0	.0	.0
28	6	-1.380776-02	-3.241178-01	-2.271980-01	.0	.0	.0

SUBCASE 2

DISPLACEMENT VECTOR

X (IN)

Y (IN)

Z (IN)

R1

R2

R3

POINT ID.	TYPE	X (IN)	Y (IN)	Z (IN)	R1	R2	R3
1	6	.0	.0	.0	.0	.0	.0
2	6	.0	.0	.0	.0	.0	.0
3	6	.0	.0	.0	.0	.0	.0
4	6	.0	.0	.0	.0	.0	.0
5	6	1.286115-02	-2.596397-02	3.386742-03	.0	.0	.0
6	6	-2.431297-03	1.272251-02	5.412542-03	.0	.0	.0
7	6	-1.241481-02	1.012095-02	-3.089950-02	.0	.0	.0
8	6	2.127547-05	-2.323194-02	-2.892935-02	.0	.0	.0
9	6	2.237754-02	-7.057362-02	-1.100286-02	.0	.0	.0
10	6	-1.515039-03	7.296367-03	-9.347485-03	.0	.0	.0
11	6	-2.162648-02	6.031951-03	-8.335608-02	.0	.0	.0
12	6	1.177266-03	-6.915148-02	-8.178067-02	.0	.0	.0
13	6	2.773050-02	-1.423995-01	-3.466389-02	.0	.0	.0
14	6	2.816091-03	-1.580974-02	-3.342902-02	.0	.0	.0
15	6	-2.681393-02	-1.586134-02	-1.531947-01	.0	.0	.0
16	6	-3.144492-03	-1.421796-01	-1.520707-01	.0	.0	.0
17	6	3.086790-02	-2.258348-01	-5.631068-02	.0	.0	.0
18	6	8.000676-03	-5.824678-02	-5.539491-02	.0	.0	.0
19	6	-2.970165-02	-5.828346-02	-2.117218-01	.0	.0	.0
20	6	-8.407594-03	-2.256113-01	-2.109185-01	.0	.0	.0
21	6	3.366880-02	-3.191812-01	-7.690203-02	.0	.0	.0
22	6	1.247221-02	-1.173368-01	-7.624082-02	.0	.0	.0
23	6	-3.202059-02	-1.173151-01	-2.623322-01	.0	.0	.0
24	6	-1.512326-02	-3.189575-01	-2.618314-01	.0	.0	.0
25	6	3.644662-02	-4.332005-01	-9.665431-02	.0	.0	.0
26	6	1.582748-02	-1.905973-01	-9.807861-02	.0	.0	.0
27	6	-3.327300-02	-1.905348-01	-3.085431-01	.0	.0	.0
28	6	-1.795811-02	-4.330399-01	-3.090712-01	.0	.0	.0

TRUSS TAIL 500M MODEL3
 DAMAGE CRITERION = NONE

OCTOBER 26, 1977

NASTRAN 7/15/77

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INCREMENTAL STIFFNESS 50 * LOAD1J6

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	S T R E S S E S IN R O D SAFETY MARGIN	E L E M E N T S E L E M E N T ID.	AXIAL STRESS	(C T U B E) (L B S / S Q . I N .) SAFETY MARGIN	T O R S I O N A L STRESS	S A F E T Y M A R G I N
1	.0		2	.0		.0	
3	.0		4	.0		.0	
5	.0		6	.0		.0	
7	-2.095866+03	1.0+01	8	-3.890512+02	4.8+01	.0	
9	-2.017964+03	8.5+00	10	3.279128+02	7.2+01	.0	
11	-7.086355+02	1.7+01	12	1.678001+03	8.5+00	.0	
13	2.006461+03	7.2+00	14	-5.382429+02	2.5+01	.0	
15	1.017874+03	1.5+01	16	-1.980322+03	5.5+00	.0	
17	-2.175370+03	5.1+00	18	6.932344+02	2.3+01	.0	
19	1.999312+02	6.1+01	20	-2.082070+02	4.6+01	.0	
21	-1.722111+02	5.6+01	22	1.831870+02	6.6+01	.0	
23	-5.433204+02	7.9+01	24	-6.413224+02	7.3+01	.0	
25	5.302805+02	1.0+02	26	6.301366+02	9.6+01	.0	
27	-2.633026+00	8.7+03	28	-9.525177+00	2.4+03	.0	
29	1.813031+03	1.3+01	30	1.219843+02	2.0+02	.0	
31	-1.763800+03	1.0+01	32	-1.512231+02	1.3+02	.0	
33	-8.734526+02	1.5+01	34	1.928708+03	8.1+00	.0	
35	2.035907+03	7.8+00	36	-1.089855+03	1.2+01	.0	
37	1.358321+03	1.2+01	38	-2.407334+03	4.8+00	.0	
39	-2.150784+03	5.7+00	40	1.193662+03	1.4+01	.0	
41	1.139936+02	1.2+02	42	-2.189064+02	5.0+01	.0	
43	-1.065987+02	1.0+02	44	2.103704+02	6.5+01	.0	
45	-5.997918+02	9.1+01	46	-3.616479+02	1.7+02	.0	
47	5.855759+02	1.2+02	48	3.425364+02	2.5+02	.0	
49	-3.765503+00	7.8+03	50	-1.276120+01	2.3+03	.0	
51	1.379911+03	1.7+01	52	7.144226+02	3.3+01	.0	
53	-1.321422+03	1.4+01	54	-7.549249+02	2.5+01	.0	
55	-1.129183+03	1.2+01	56	2.423532+03	6.8+00	.0	
57	2.173116+03	7.8+00	58	-1.770916+03	7.7+00	.0	
59	1.714863+03	9.4+00	60	-3.003300+03	4.0+00	.0	
61	-2.300082+03	5.7+00	62	1.896380+03	9.2+00	.0	
63	1.488735+02	1.0+02	64	-2.812774+02	4.3+01	.0	
65	-1.438065+02	8.5+01	66	2.733373+02	5.6+01	.0	
67	-6.862996+02	1.0+02	68	-3.145312+01	2.6+03	.0	
69	6.687827+02	1.3+02	70	5.296387+00	2.0+04	.0	
71	-1.930908+00	2.0+04	72	-1.962646+01	2.0+03	.0	
73	1.290318+03	2.5+01	74	1.148172+03	2.9+01	.0	
75	-1.217862+03	2.1+01	76	-1.201685+03	2.2+01	.0	
77	-1.595667+03	1.2+01	78	3.062812+03	7.4+00	.0	
79	2.237876+03	1.1+01	80	-2.185781+03	8.7+00	.0	
81	1.601493+03	1.5+01	82	-3.063670+03	5.7+00	.0	
83	-2.390856+03	7.9+00	84	2.339188+03	1.0+01	.0	
85	-7.993945+01	2.4+02	86	-6.429602+01	2.0+02	.0	
87	7.717090+01	2.7+02	88	7.137585+01	2.9+02	.0	
89	-7.953979+02	1.2+02	90	-4.143457+01	2.6+03	.0	

DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 50 % LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ROD SAFETY MARGIN		ELEMENT ID.	AXIAL STRESS		TORSIONAL STRESS		ROD SAFETY MARGIN	
	STRESS	MARGIN	STRESS	MARGIN	STRESS	MARGIN		STRESS	MARGIN	STRESS	MARGIN	STRESS	MARGIN
91	7.755576+02	1.5+02	.0	.0	91	6.912109+00	2.0+04	.0	.0	91	6.912109+00	2.0+04	.0
93	-1.174805+00	4.3+04	.0	.0	93	-2.545911+01	2.0+03	.0	.0	93	-2.545911+01	2.0+03	.0
95	1.517651+03	3.0+01	.0	.0	95	1.319505+03	3.4+01	.0	.0	95	1.319505+03	3.4+01	.0
97	-1.379430+03	2.6+01	.0	.0	97	-1.431422+03	2.5+01	.0	.0	97	-1.431422+03	2.5+01	.0
99	-1.824011+03	1.4+01	.0	.0	99	3.491667+03	8.9+00	.0	.0	99	3.491667+03	8.9+00	.0
101	2.489045+03	1.3+01	.0	.0	101	-2.443332+03	1.1+01	.0	.0	101	-2.443332+03	1.1+01	.0
103	1.834190+03	1.6+01	.0	.0	103	-3.495652+03	6.9+00	.0	.0	103	-3.495652+03	6.9+00	.0
105	-2.663855+03	9.6+00	.0	.0	105	2.617911+03	1.3+01	.0	.0	105	2.617911+03	1.3+01	.0
107	-5.250098+01	4.3+02	.0	.0	107	-1.250378+02	1.6+02	.0	.0	107	-1.250378+02	1.6+02	.0
109	1.144460+02	2.5+02	.0	.0	109	5.255762+01	5.4+02	.0	.0	109	5.255762+01	5.4+02	.0
111	-9.194983+02	1.3+02	.0	.0	111	-4.764453+01	3.0+03	.0	.0	111	-4.764453+01	3.0+03	.0
113	8.875625+02	1.7+02	.0	.0	113	-4.732910+00	3.1+04	.0	.0	113	-4.732910+00	3.1+04	.0
115	6.586035+01	1.3+03	.0	.0	115	-1.071396+02	6.2+02	.0	.0	115	-1.071396+02	6.2+02	.0
117	1.850741+03	2.9+01	.0	.0	117	1.287430+03	4.2+01	.0	.0	117	1.287430+03	4.2+01	.0
119	-1.343775+03	3.2+01	.0	.0	119	-1.794080+03	2.4+01	.0	.0	119	-1.794080+03	2.4+01	.0
121	-2.061425+03	1.5+01	.0	.0	121	4.128576+03	9.2+00	.0	.0	121	4.128576+03	9.2+00	.0
123	3.055926+03	1.3+01	.0	.0	123	-3.026574+03	1.1+01	.0	.0	123	-3.026574+03	1.1+01	.0
125	2.094837+03	1.9+01	.0	.0	125	-4.120793+03	7.2+00	.0	.0	125	-4.120793+03	7.2+00	.0
127	-3.213598+03	1.0+01	.0	.0	127	3.164576+03	1.3+01	.0	.0	127	3.164576+03	1.3+01	.0
129	-3.634321+02	7.6+01	.0	.0	129	9.194763+01	3.8+02	.0	.0	129	9.194763+01	3.8+02	.0
131	-9.038428+01	3.1+02	.0	.0	131	3.806885+02	9.1+01	.0	.0	131	3.806885+02	9.1+01	.0
133	-4.034072+02	4.0+02	.0	.0	133	-2.479297+01	7.7+03	.0	.0	133	-2.479297+01	7.7+03	.0
135	6.054766+02	3.3+02	.0	.0	135	-1.595508+01	1.2+04	.0	.0	135	-1.595508+01	1.2+04	.0
137	-1.985955+03	4.3+01	.0	.0	137	2.078661+03	5.2+01	.0	.0	137	2.078661+03	5.2+01	.0

INCREMENTAL STIFFNESS 75 % LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	STRESSES IN TORSIONAL STRESS	R O D SAFETY MARGIN	E L E M E N T S E S I N R O D SAFETY MARGIN	E L E M E N T S E S I N TORSIONAL STRESS	A X I A L STRESS	(C T U B E) SAFETY MARGIN	(L B S / S Q . I N .) TORSIONAL STRESS	SAFETY MARGIN
1	.0						.0		.0	
3	.0						.0		.0	
5	.0						.0		.0	
7	3.180557+03	6.5+00					-6.090774+02	3.0+01	.0	
9	-3.061034+03	5.2+00					5.195061+02	4.5+01	.0	
11	-1.065306+03	1.1+01					-2.524473+03	5.3+00	.0	
13	3.029875+03	4.4+00					-7.904973+02	1.6+01	.0	
15	1.525671+03	9.5+00					-2.973785+03	3.3+00	.0	
17	-3.286572+03	3.0+00					-1.026750+03	1.5+01	.0	
19	2.991644+02	4.4+01					-3.139926+02	3.0+01	.0	
21	-2.587820+02	3.7+01					2.764727+02	4.3+01	.0	
23	-8.223837+02	5.2+01					-9.852325+02	4.7+01	.0	
25	7.950940+02	6.7+01					9.610486+02	6.2+01	.0	
27	-9.202881+00	2.5+03					-1.660980+01	1.4+03	.0	
29	2.760029+03	7.3+00					1.582844+02	1.5+02	.0	
31	-2.681496+03	6.3+00					-1.976353+02	9.9+01	.0	
33	-1.311085+03	9.7+00					2.900671+03	5.0+00	.0	
35	3.076049+03	4.9+00					-1.619376+03	7.9+00	.0	
37	2.039528+03	7.6+00					-3.617165+03	2.9+00	.0	
39	-3.248916+03	3.5+00					1.776009+03	9.2+00	.0	
41	1.690861+02	8.1+01					-3.286189+02	3.3+01	.0	
43	-1.606795+02	6.3+01					3.153703+02	4.3+01	.0	
45	-9.082664+02	6.0+01					-5.690024+02	1.1+02	.0	
47	8.772700+02	7.8+01					5.263073+02	1.5+02	.0	
49	-1.266028+01	2.3+03					-2.385867+01	1.2+03	.0	
51	2.106822+03	1.1+01					1.046175+03	2.3+01	.0	
53	-2.013024+03	6.8+00					-1.101124+03	1.7+01	.0	
55	-1.695562+03	7.8+00					3.642226+03	4.2+00	.0	
57	3.287532+03	4.8+00					-2.643214+03	4.8+00	.0	
59	2.577278+03	6.3+00					-4.511325+03	2.3+00	.0	
61	-3.472183+03	3.5+00					2.826793+03	5.8+00	.0	
63	2.245847+02	6.8+01					-4.212401+02	2.8+01	.0	
65	-2.189875+02	5.6+01					4.082813+02	3.7+01	.0	
67	-1.036204+03	6.9+01					-7.672949+01	1.1+03	.0	
69	9.972158+02	9.0+01					1.665448+01	6.3+03	.0	
71	-1.119945+01	3.4+03					-3.766003+01	1.0+03	.0	
73	1.969708+03	1.6+01					1.696032+03	1.9+01	.0	
75	-1.853718+03	1.4+01					-1.769254+03	1.4+01	.0	
77	-2.396512+03	7.6+00					4.599665+03	4.6+00	.0	
79	3.581771+03	6.3+00					-3.265125+03	5.5+00	.0	
81	2.410217+03	9.7+00					-4.602005+03	3.5+00	.0	
83	-3.611081+03	4.9+00					3.495187+03	6.6+00	.0	
85	-1.065982+02	1.6+02					-1.284851+02	1.3+02	.0	
87	1.133459+02	1.5+02					1.070165+02	2.0+02	.0	
89	-1.200795+03	7.8+01					-9.330469+01	1.2+03	.0	

SUBCASE 2

ELEMNT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN	ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN	ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	SAFETY MARGIN
91	1.156034+03	1.0+02	.0	9.0+03	92	1.558154+01	9.0+03	.0	.0	94	-4.814172+01	1.1+03	.0	.0
93	-1.186914+01	4.3+03	.0	2.3+01	96	1.956901+03	1.7+01	.0	5.6+00	100	5.242883+03	6.8+00	.0	.0
95	2.309225+03	1.9+01	.0	1.7+01	102	-3.654515+03	8.5+00	.0	6.8+00	104	-5.251874+03	4.3+00	.0	.0
97	-2.091982+03	9.1+00	.0	8.5+00	106	3.916175+03	1.1+01	.0	8.2+00	108	-1.914911+02	1.2+02	.0	.0
99	-2.733761+03	9.1+00	.0	1.1+01	110	7.899951+01	1.7+02	.0	1.3+03	112	-1.073594+02	1.3+03	.0	.0
101	3.757562+03	8.5+00	.0	6.2+00	114	-1.064844+01	1.1+02	.0	1.4+04	116	-1.760957+02	3.7+02	.0	.0
103	2.761693+03	1.1+01	.0	2.9+02	118	1.910486+03	1.9+01	.0	2.8+01	120	-2.669357+03	1.6+01	.0	.0
105	-4.019805+03	6.2+00	.0	8.7+01	122	6.204114+03	9.9+00	.0	5.8+00	124	-4.536874+03	6.7+00	.0	.0
107	-7.896230+01	2.9+02	.0	1.1+02	126	-6.186660+03	8.5+00	.0	6.7+00	128	4.736312+03	4.4+00	.0	.0
109	1.676157+02	1.7+02	.0	1.1+02	130	1.379353+02	5.1+01	.0	2.5+02	132	5.770344+02	6.0+01	.0	.0
111	-1.391391+03	8.7+01	.0	8.7+01	134	-5.592969+01	3.0+02	.0	3.4+03	136	-3.560937+01	5.6+03	.0	.0
113	1.319391+03	1.1+02	.0	1.1+02	138	3.147651+03	2.9+01	.0	3.4+03					
115	8.306836+01	1.0+03	.0	1.1+02										
117	2.797051+03	1.9+01	.0	1.9+01										
119	-2.037488+03	2.1+01	.0	2.1+01										
121	-3.087795+03	9.9+00	.0	8.5+00										
123	4.603016+03	8.5+00	.0	1.2+01										
125	3.163083+03	1.2+01	.0	6.3+00										
127	-4.846732+03	6.3+00	.0	5.1+01										
129	-5.380937+02	5.1+01	.0	2.1+02										
131	-1.344390+02	2.1+02	.0	3.0+02										
133	-5.291074+02	3.0+02	.0	2.0+02										
135	9.844414+02	2.0+02	.0	2.9+01										
137	-2.939574+03	2.9+01	.0											

INCREMENTAL STIFFNESS 100% LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	STRESSES IN R O D	E L E M E N T S	AXIAL STRESS	SAFETY MARGIN	(C T U B E) (L B S / S Q . I N .)	TORSIONAL STRESS	SAFETY MARGIN
1	.0			2	.0			.0	
3	.0			4	.0			.0	
5	.0			6	.0			.0	
7	4.293310+03	4.5+00		8	-8.458912+02	2.2+01		.0	
9	-4.127390+03	3.6+00		10	7.293166+02	3.2+01		.0	
11	-1.423472+03	9.0+00		12	3.376294+03	3.7+00		.0	
13	4.056972+03	5.0+00		14	-1.031504+03	1.2+01		.0	
15	2.032590+03	6.9+00		16	-3.969805+03	2.2+00		.0	
17	-4.413740+03	2.1+00		18	1.351614+03	1.1+01		.0	
19	3.979033+02	5.3+01		20	-4.208998+02	2.2+01		.0	
21	-3.456797+02	2.8+01		22	3.708930+02	3.2+01		.0	
23	-1.105693+03	5.8+01		24	-1.344760+03	3.4+01		.0	
25	1.059840+03	5.0+01		26	1.302639+03	4.6+01		.0	
27	-1.935426+01	1.2+03		28	-2.523804+01	9.0+02		.0	
29	3.734625+03	5.6+00		30	1.783222+02	1.4+02		.0	
31	-3.623605+03	4.4+00		32	-2.247424+02	8.7+01		.0	
33	-1.749367+03	7.9+00		34	3.878163+03	3.5+00		.0	
35	4.131343+03	3.4+00		36	-2.138730+03	5.7+00		.0	
37	2.713465+03	5.4+00		38	-4.831562+03	1.9+00		.0	
39	-4.362564+03	2.3+00		40	2.348850+03	6.7+00		.0	
41	2.824667+02	6.1+01		42	-4.385020+02	2.5+01		.0	
43	-2.132924+02	5.1+01		44	4.202727+02	3.2+01		.0	
45	-1.222733+03	4.4+01		46	-7.941973+02	7.6+01		.0	
47	1.168376+03	5.8+01		48	7.184955+02	1.1+02		.0	
49	-2.633715+01	1.1+03		50	-3.809613+01	7.7+02		.0	
51	2.854908+03	7.6+00		52	1.361091+03	1.7+01		.0	
53	-2.725606+03	6.2+00		54	-1.426571+03	1.3+01		.0	
55	-2.263343+03	5.8+00		56	4.866162+03	2.9+00		.0	
57	4.421090+03	3.5+00		58	-3.507026+03	3.4+00		.0	
59	3.443265+03	4.9+00		60	-6.024208+03	1.5+00		.0	
61	-4.659512+03	2.5+00		62	3.745650+03	4.2+00		.0	
63	3.011294+02	5.0+01		64	-5.607360+02	2.1+01		.0	
65	-2.961052+02	4.1+01		66	5.421022+02	2.8+01		.0	
67	-1.391804+03	5.1+01		68	-1.418672+02	5.7+02		.0	
69	1.321790+03	6.0+01		70	3.388843+01	3.1+03		.0	
71	-2.607665+01	1.3+03		72	-6.115771+01	6.3+02		.0	
73	2.672570+03	1.2+01		74	2.224668+03	1.4+01		.0	
75	-2.507918+03	9.9+00		76	-2.314683+03	1.1+01		.0	
77	-3.199857+03	5.4+00		78	6.140916+03	3.2+00		.0	
79	4.545040+03	4.8+00		80	-4.335938+03	3.9+00		.0	
81	3.224751+03	7.8+00		82	-6.145446+03	2.3+00		.0	
83	-4.043562+03	5.9+00		84	4.642612+03	4.7+00		.0	
85	-1.492115+02	1.2+02		86	-1.750961+02	9.6+01		.0	
87	1.474670+03	1.9+02		88	1.426525+02	1.5+02		.0	
89	-1.621440+03	5.3+01		90	-1.661094+02	6.5+02		.0	

TRUSS TAIL ROOM MODELS **A 138 ELEMENT VERSION
 DAMAGE CRITERION = NONE

INCREMENTAL STIFFNESS 100% LOADING

SUBCASE 2

ELEMENT ID.	AXIAL STRESS	SAFETY MARGIN	TORSIONAL STRESS	IN TORSIONAL STRESS	R O D SAFETY MARGIN	E L E M E N T S ID.	AXIAL STRESS	SAFETY MARGIN	(C T U B E) SAFETY MARGIN	(L B S / S Q . I N .) TORSIONAL STRESS	SAFETY MARGIN
91	1.531721+03	7.6+01	.0	.0	7.6+01	92	2.777783+01	5.0+03	.0	.0	.0
93	-2.941113+01	1.7+03	.0	.0	1.7+03	94	-7.744897+01	6.5+02	.0	.0	.0
95	3.123028+03	1.4+01	.0	.0	1.4+01	96	2.579405+03	1.7+01	.0	.0	.0
97	-2.820045+03	1.2+01	.0	.0	1.2+01	98	-2.776889+03	1.2+01	.0	.0	.0
99	-3.658008+03	6.5+00	.0	.0	6.5+00	100	6.998632+03	3.9+00	.0	.0	.0
101	5.043096+03	6.1+00	.0	.0	6.1+00	102	-4.859465+03	4.9+00	.0	.0	.0
103	3.696921+03	8.3+00	.0	.0	8.3+00	104	-7.014665+03	2.9+00	.0	.0	.0
105	-5.392645+03	4.3+00	.0	.0	4.3+00	106	5.208050+03	5.9+00	.0	.0	.0
107	-1.053232+02	2.1+02	.0	.0	2.1+02	108	-2.605734+02	8.6+01	.0	.0	.0
109	2.180469+02	1.3+02	.0	.0	1.3+02	110	1.055802+02	2.7+02	.0	.0	.0
111	-1.871523+03	6.4+01	.0	.0	6.4+01	112	-1.911719+02	7.4+02	.0	.0	.0
113	1.743232+03	8.6+01	.0	.0	8.6+01	114	-1.892187+01	7.8+03	.0	.0	.0
115	8.967363+01	9.2+02	.0	.0	9.2+02	116	-2.553506+02	2.6+02	.0	.0	.0
117	3.757447+03	1.4+01	.0	.0	1.4+01	118	2.519782+03	2.1+01	.0	.0	.0
119	-2.743965+03	1.5+01	.0	.0	1.5+01	120	-3.530040+03	1.2+01	.0	.0	.0
121	-4.112268+03	7.2+00	.0	.0	7.2+00	122	8.288303+03	4.1+00	.0	.0	.0
123	6.163988+03	6.1+00	.0	.0	6.1+00	124	-6.046208+03	4.8+00	.0	.0	.0
125	4.246366+03	8.9+00	.0	.0	8.9+00	126	-8.257161+03	3.1+00	.0	.0	.0
127	-6.498541+03	4.4+00	.0	.0	4.4+00	128	6.301957+03	6.0+00	.0	.0	.0
129	-7.079434+02	3.9+01	.0	.0	3.9+01	130	1.838745+02	1.9+02	.0	.0	.0
131	-1.776914+02	1.6+02	.0	.0	1.6+02	132	7.773601+02	4.4+01	.0	.0	.0
133	-6.038027+02	2.6+02	.0	.0	2.6+02	134	-9.966016+01	1.9+03	.0	.0	.0
135	1.414676+03	1.4+02	.0	.0	1.4+02	136	-6.313672+01	3.2+03	.0	.0	.0
137	-3.863580+03	2.2+01	.0	.0	2.2+01	138	4.235999+03	2.5+01	.0	.0	.0

* 57.8 CPU-S 266.3 COR-S 1345 ELP-S. 158 OFP END

* 57.9 CPU-S 266.3 COR-S 1345 ELP-S. 179 EXIT BEGN

APPENDIX D

Element Identification Table for All Models

<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>	<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>
Vertical	1	1-2	Vertical	25	7-8
Horizontal	2	1-4	Horizontal	26	6-7
Vertical	3	3-4	Transverse	27	5-7
Horizontal	4	2-3	Diagonals	28	6-8
Transverse	5	1-3	Longerons	29	5-9
Diagonals	6	2-4	"	30	6-10
Longerons	7	1-5	"	31	7-11
"	8	2-6	"	32	8-12
"	9	3-7	Outside	33	5-10
"	10	4-8	Diagonals	34	6-9
Outside	11	1-6	"	35	5-12
Diagonals	12	2-5	"	36	8-9
"	13	1-8	"	37	8-11
"	14	4-5	"	38	7-12
"	15	4-7	"	39	6-11
"	16	3-8	"	40	7-10
"	17	2-7	Interior	41	5-11
"	18	3-6	Diagonals	42	6-12
Interior	19	1-7	"	43	7-9
Diagonals	20	2-8	"	44	8-10
"	21	3-5	Vertical	45	9-10
"	22	4-6	Horizontal	46	9-12
Vertical	23	5-6	Vertical	47	11-12
Horizontal	24	5-8	Horizontal	48	10-11

<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>	<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>
Transverse	49	9-11	Diagonals	80	16-17
Diagonals	50	10-12	"	81	16-19
Longerons	51	9-13	"	82	15-20
"	52	10-14	"	83	14-19
"	53	11-13	"	84	15-18
"	54	12-16	Interior	85	13-19
Outside	55	9-14	Diagonals	86	14-20
Diagonals	56	10-13	"	87	15-17
"	57	9-16	"	88	16-18
"	58	12-13	Vertical	89	17-18
"	59	12-15	Horizontal	90	17-20
"	60	11-16	Vertical	91	19-20
"	61	10-15	Horizontal	92	18-19
"	62	11-14	Transverse	93	17-19
Interior	63	9-15	Diagonals	94	18-20
Diagonals	64	10-16	Longerons	95	17-21
"	65	11-13	"	96	18-22
"	66	12-14	"	97	19-23
Vertical	67	13-14	"	98	20-24
Horizontal	68	13-16	Outside	99	17-22
Vertical	69	15-16	Diagonals	100	18-21
Horizontal	70	14-15	"	101	17-24
Transverse	71	13-15	"	102	20-21
Diagonals	72	14-16	"	103	20-23
Longerons	73	13-17	"	104	19-24
Longerons	74	14-18	"	105	18-23
"	75	15-19	"	106	19-22
"	76	16-20	Interior	107	17-23
Outside	77	13-18	Diagonals	108	18-24
Diagonals	78	14-17	"	109	19-21
"	79	13-20	"	110	20-22

<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>	<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>
Vertical	111	21-22	Longerons	142	28-32
Horizontal	112	21-24	Outside	143	25-30
Vertical	113	23-24	Diagonals	144	26-29
Horizontal	114	22-23	"	145	25-32
Transverse	115	21-23	"	146	28-29
Diagonals	116	22-24	"	147	28-31
Longerons	117	21-25	"	148	27-32
"	118	22-26	"	149	26-31
"	119	23-27	"	150	27-30
"	120	24-28	Interior	151	25-31
Outside	121	21-26	Diagonals	152	26-32
Diagonals	122	22-25	"	153	27-29
"	123	21-28	"	154	28-30
Diagonals	124	24-25	Vertical	155	29-30
"	125	24-27	Horizontal	156	29-32
"	126	23-28	Vertical	157	31-32
"	127	22-27	Horizontal	158	30-31
"	128	23-26	Transverse	159	29-31
Interior	129	21-27	Diagonals	160	30-32
Diagonals	130	22-28	Longerons	161	29-33
"	131	23-25	"	162	30-34
"	132	24-26	"	163	31-35
Vertical	133	25-26	"	164	32-36
Horizontal	134	25-28	Outside	165	29-34
Vertical	135	27-28	Diagonals	166	30-33
Horizontal	136	26-27	"	167	29-36
Transverse	137	25-27	"	168	32-33
Diagonals	138	26-28*	"	169	32-35
*Note models 2 & 3 end 138			"	170	31-36
Longerons	139	25-29	"	171	3-35
"	140	26-30	"	172	31-34
"	141	27-31	Interior	173	29-35

<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>	<u>Type</u>	<u>Element ID</u>	<u>Node-Node</u>
Diagonals	174	30-36	Longerons	206	38-42
"	175	31-33	"	207	39-43
"	176	32-34	"	208	40-44
Vertical	177	33-34	Outside	209	37-42
Horizontal	178	33-36	Diagonals	210	38-41
Vertical	179	35-36	"	211	37-44
Horizontal	180	34-35	"	212	40-41
Transverse	181	33-35	"	213	40-43
Diagonals	182	34-36	"	214	39-44
Longerons	183	33-37	"	215	38-43
"	184	34-38	"	216	39-42
"	185	35-39	Interior	217	37-43
"	186	36-40	Diagonals	218	38-44
Outside	187	33-38	"	219	39-41
Diagonals	188	34-37	"	220	40-42
"	189	33-40	Vertical	221	41-42
"	190	36-37	Horizontal	222	41-44
"	191	36-39	Vertical	223	43-44
"	192	35-40	Horizontal	225	42-43
"	193	34-39	Transverse	225	41-43
"	194	35-38	Diagonals	226	42-44
Interior	195	33-39			
Diagonals	196	34-40			
"	197	35-37			
"	198	36-38			
Vertical	199	37-38			
Horizontal	200	37-40			
Vertical	201	39-40			
Horizontal	202	38-39			
Transverse	203	37-39			
Diagonals	204	38-40			
Longerons	205	37-41			

Appendix E

Grid Point Locations Model 1

<u>Point #</u>	<u>X</u>	<u>Y</u>	<u>Z</u>
1	.000	12.300	13.300
2	.000	12.100	-11.500
3	.000	-11.400	-11.500
4	.000	-11.600	13.300
5	23.700	11.300	12.300
6	23.900	11.100	-10.700
7	23.900	-10.600	-10.700
8	23.750	-10.800	12.300
9	45.950	10.400	11.300
10	45.950	10.200	-9.900
11	45.950	-9.800	-9.900
12	45.950	-10.000	11.300
13	66.400	9.500	10.500
14	66.500	9.300	-9.200
15	66.500	-9.100	-9.200
16	66.400	-9.300	10.500
17	85.400	8.800	9.700
18	85.400	8.600	-8.600
19	85.400	-8.400	-8.600
20	85.400	-8.600	9.700
21	103.000	8.000	8.900
22	103.000	7.900	-8.000
23	103.000	-7.800	-8.000
24	103.000	-8.000	8.900
25	119.300	7.400	8.300
26	119.300	7.200	-7.400
27	119.300	-7.300	-7.400
28	119.300	-7.500	8.300
29	134.400	6.700	7.600

Appendix E (continued)

<u>Point #</u>	<u>X</u>	<u>Y</u>	<u>Z</u>
30	134.500	6.600	-6.900
31	134.500	-6.800	-6.900
32	134.400	-6.900	7.600
33	148.500	6.100	7.000
34	148.500	6.000	-6.500
35	148.500	-6.300	-6.500
36	148.500	-6.400	7.000
37	161.400	5.600	6.500
38	161.500	5.500	-6.000
39	161.500	-5.800	-6.000
40	161.400	-6.000	6.500
41	173.500	5.100	6.000
42	173.500	5.000	-5.600
43	173.500	-5.400	-5.600
44	173.500	-5.500	6.000

Appendix F

Grid Point Locations Models 2 and 3

<u>Point #</u>	<u>X</u>	<u>Y</u>	<u>Z</u>
1	.000	11.95	12.375
2	.000	11.75	-12.375
3	.000	-11.75	-12.375
4	.000	-11.95	12.375
5	33.5	10.666	11.105
6	33.5	10.485	-11.105
7	33.5	-10.485	-11.105
8	33.5	-10.666	11.105
9	66.5	9.401	9.855
10	66.5	9.239	-9.855
11	66.5	-9.239	-9.855
12	66.5	-9.401	9.855
13	99.5	8.136	8.604
14	99.5	7.994	-8.604
15	99.5	-7.994	-8.604
16	99.5	-8.136	8.604
17	127.5	7.063	7.543
18	127.5	6.937	-7.543
19	127.5	-6.937	-7.543
20	127.5	-7.063	7.543
21	151.5	6.143	6.634
22	151.5	6.031	-6.634
23	151.5	-6.031	-6.634
24	151.5	-6.143	6.634
25	173.5	5.3	5.8
26	173.5	5.2	-5.8
27	173.5	-5.2	-5.8
28	173.5	-5.3	5.800

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