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AUG 78 J P MCISAAC, R E MCINERNEY, D DELOREY

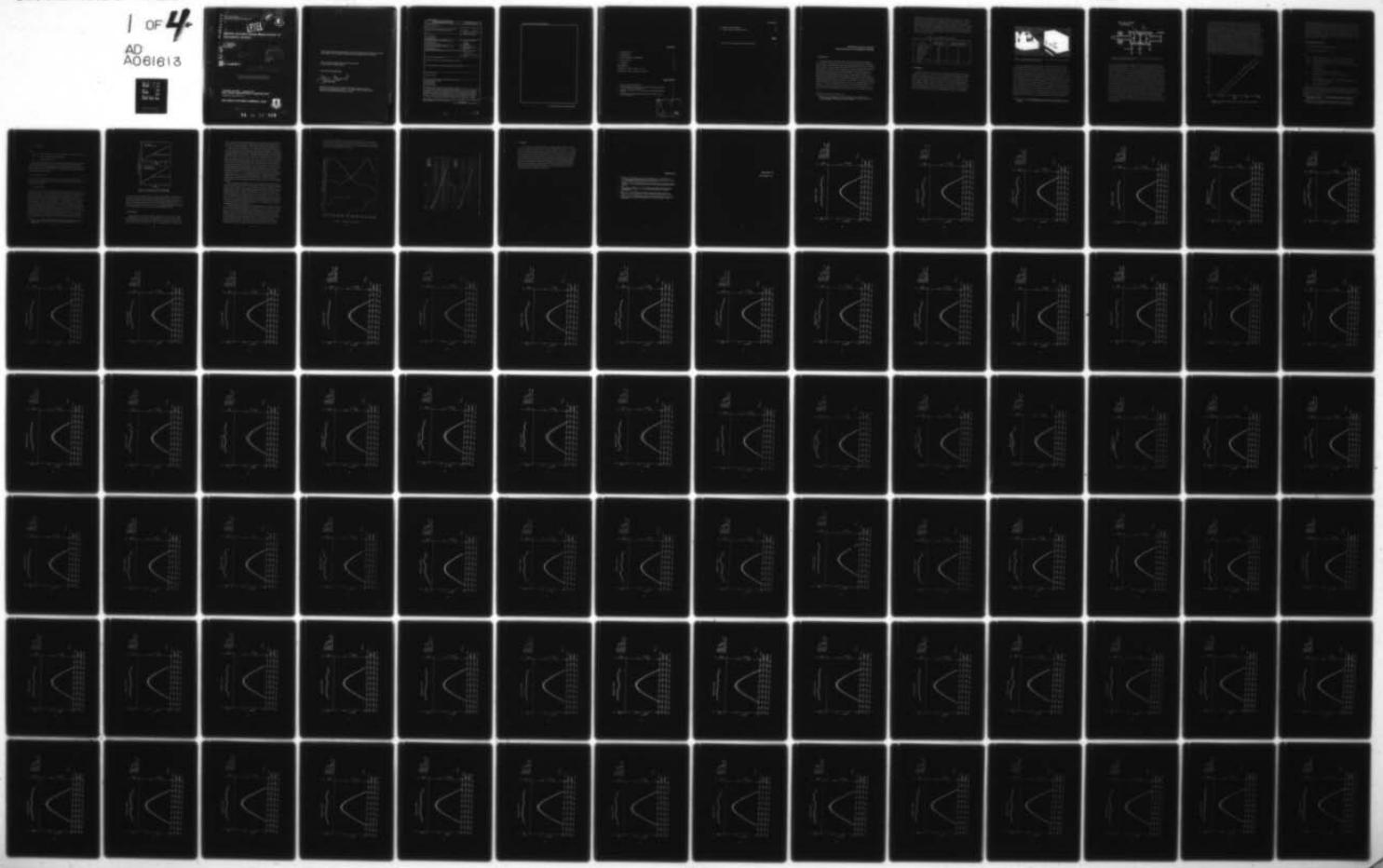
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Satellite Ionization Gauge Measurements of Atmospheric Density.

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J. P. McISAAC
R. E. McINERNEY
D. DELOREY

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HANSCOM AFB, MASSACHUSETTS 01731

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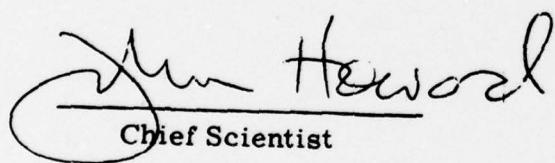
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This report has been reviewed by the ESD Information Office (OI) and is releasable to the National Technical Information Service (NTIS).

This technical report has been reviewed and is approved for publication.

FOR THE COMMANDER



John Howard
Chief Scientist

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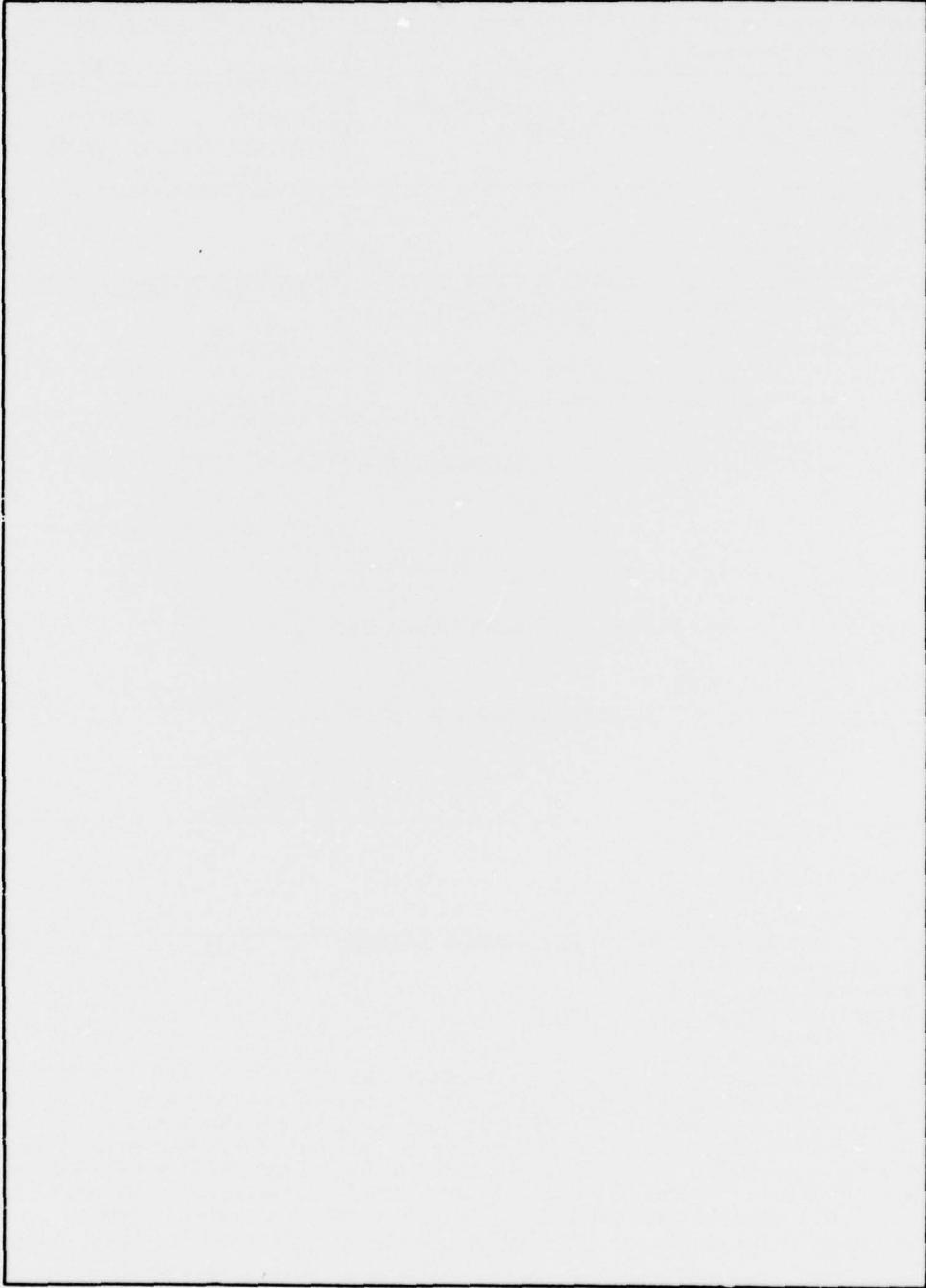
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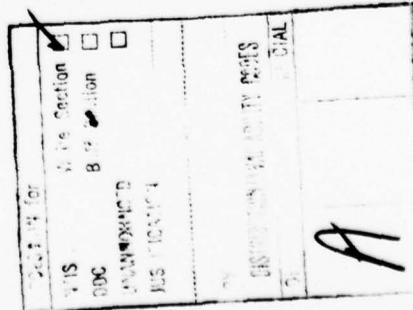
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Satellite Ionization Gauge Measurements of Atmospheric Density

I. INTRODUCTION

Ionization gauge measurements performed onboard the Air Force Satellite (S3-1) launched in October 1974 have been processed and reduced into atmospheric density results. Representative results obtained during the period from November 1974 to January 1975 covering the first 1000 revolutions, were previously reported¹ together with a description of the satellite and experiment operations as well as data reduction procedures and processing techniques. This report supplements the information given in reference 1 and serves to complete the compilation of flight results. Representative samples of flight results obtained after revolution 1000 and up to satellite reentry are included in the appendices. These results were acquired during the period from January 1975 to May 1975. A summary of the total number of processed revolutions provided in terms of a monthly breakdown is shown in Table 1. In order to make this report more comprehensive and complete, a certain amount of the material given in reference 1 has been repeated here. However, the reader would find this report to be more useful if taken together with that

(Received for publication 15 August 1978)

1. McIssac, J. P., Champion, K. S. W., McInerney, R. E., and Delorey, D.
(1976) Ionization Gauge Measurements of Atmospheric Density From a Low Altitude Satellite, AFGL Report No. TR-76-0113.

reference, as there is material contained in that report, which is not repeated here. All the data included in the appendices are new and unpublished. Upon the publication of these results, the compilation stage of the S3-1 ionization gauge flight data processing will be completed. With the completion of that task, compiled results along with model and geophysical parameters (magnetic indices, solar flux values, etc) are packed on magnetic tapes for use in later correlation and analysis studies, as well as statistical investigations useful in the development and improvement of atmospheric models.

Table 1. S3-1 Satellite Density Data Base

| Month | Total Number of Data Acquisitions | Number of Acquisitions in Appendix this report |
|---------------|-----------------------------------|--|
| November 1974 | 220 | 0 |
| December 1974 | 229 | 0 |
| January 1975 | 233 | 18 |
| February 1975 | 213 | 33 |
| March 1975 | 267 | 37 |
| April 1975 | 278 | 42 |
| May 1975 | 218 | 28 |
| Totals | 1658 | 158 |

2. EXPERIMENT

The flight apparatus consisted of two units referred to as the sensor and electronics units. The sensor unit housed a cold-cathode ionization gauge, its magnet and physical mechanism required to open the gauge once it was placed into orbit. Contained in the electronics unit were the operating circuits. Included were amplifiers, signal conditioners, filters, switches, timers, and high and low voltage power supplies. Figure 1 shows the experiment. On the left in the figure is the ionization gauge sensor with its cover removed. The cover also serves as a magnetic shield confining stray field lines within the box perimeter. To the right in Figure 1 is the auxiliary electronics box containing the circuits described above.

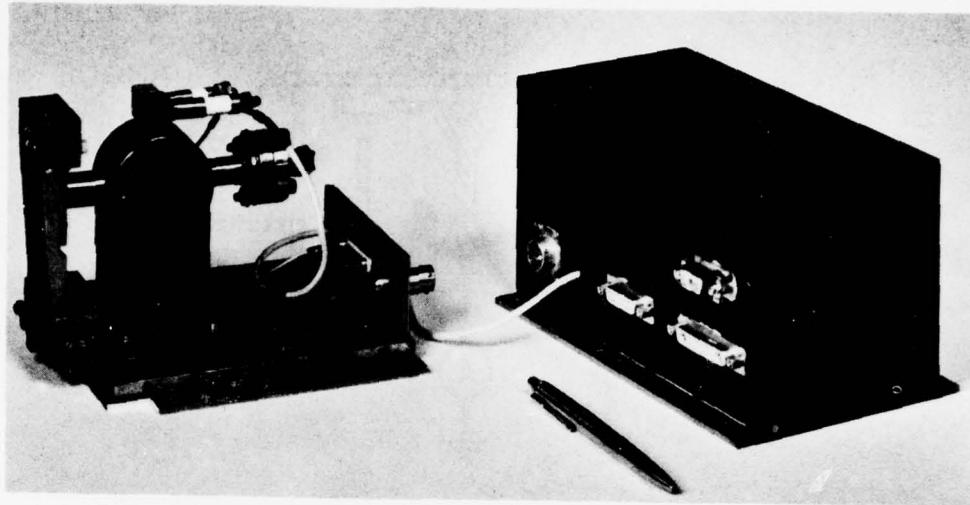


Figure 1. Ionization Gauge Flight System. Shown to the left is the sensor unit with its magnetic shield cover removed

A total of seven gauges were fabricated, tested and calibrated by GCA Corporation, Bedford, MA. The gauges are a modified version of the R-5 gauge, cold-cathode magnetron, developed for NASA by GCA.² The principal modification performed on the R-5 gauge was to restructure the gauge envelope in order to accommodate an additional second tubulation. Figure 2 shows a schematic view of the gauge and illustrates the internal arrangement of the gauge electrodes as well as the configuration of the two tubulations. The flight sampling tubulation is shown on the right in the figure, and the test tubulation is shown on the left. Each tubulation, or connection, serves a particular designed function. The test tubulation with its demountable flange fitting is used for test, calibration and evacuation purposes where by nature of the requirement a non-permanent, replaceable connection would be employed. With such a connection other functions, as well, can be performed. As the gauge has been evacuated and sealed before delivery to the space-craft contractor, the need for a vacuum pump station to evacuate the gauge during satellite payload operating tests has been eliminated. Here the test tubulation

2. Kreisman, W. (1964) Development of Cold Cathode Ionization Gauges for Space Vehicles, GCA Corporation Report No. 64-17-N, Part I and No. 64-19-N, Part II.

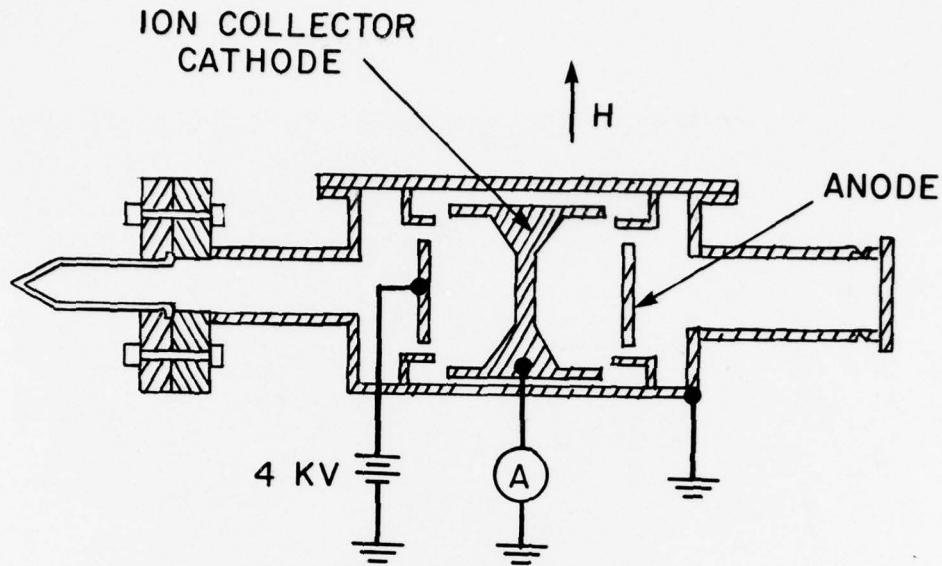


Figure 2. Simplified Schematic Diagram of Ionization Gauge Envelope and Internal Electrode Configuration

provides a backup capability by supplying the means for reconditioning the gauge in the event the gauge loses its vacuum, or, due to the long duration of satellite test and integration programs, increases to an unacceptable operating level. This buildup of internal gauge pressure can be attributed to a variety of causes individually or collectively, as, for example, outgassing, desorption, sputtering and accumulated leakage from long periods of non-operation and storage. In the case where internal pressure does reach a high unacceptable level, the test tubulation together with a simple portable vacuum system provides the capability for quick and efficient evacuation, test and resealing. On the other hand, the flight tubulation is a hard sealed (once broken cannot be resealed) connection that is installed during gauge fabrication and remains intact until the gauge is placed into orbit. When orbit is obtained, the head sealed connection is explosively ruptured thereby opening and exposing the gauge to the ambient atmosphere. The uncapping or opening process breaks the tubulation at a predetermined interface thus assuring that the in-orbit sampling geometry (length and radius) is precisely defined and known. This is accomplished by machining a "break-off" groove around the sampling tube's circumference reducing the tube wall thickness at the groove to 0.005 in. The break location, therefore, is confined to the groove. As elsewhere, the wall thickness is 0.1250 in.

Typical calibrations for nitrogen and helium gases are shown in Figure 3. Attempts to calibrate with oxygen proved to be troublesome and results for the most part were unsatisfactory. Some success, however, was obtained using a specially fabricated gauge containing gold coated electrodes and internal surfaces. Results obtained from this gauge produced calibrations for both N_2 and O_2 , each of which displayed hysteresis effects, although untreated gauges, those without gold surfaces, displayed insignificant hysteresis effects when calibrated with nitrogen gas. The hysteresis effect is defined as the differences in response that can occur in calibration depending upon in which direction the steady state, calibration, pressure levels are reached; that is, whether they are reached by increasing calibration system pressure as opposed to decreasing system pressure. It was noted that hysteresis effects were largest at the lowest system pressures suggesting that, at least, part of the effect was due to gas losses in the vacuum station. Differences in response between the two gases, nitrogen and oxygen, for the most part were within ± 15 percent of each other. If the hysteresis effect for each gas is removed, that is, each individual gas calibration is formed by averaging the

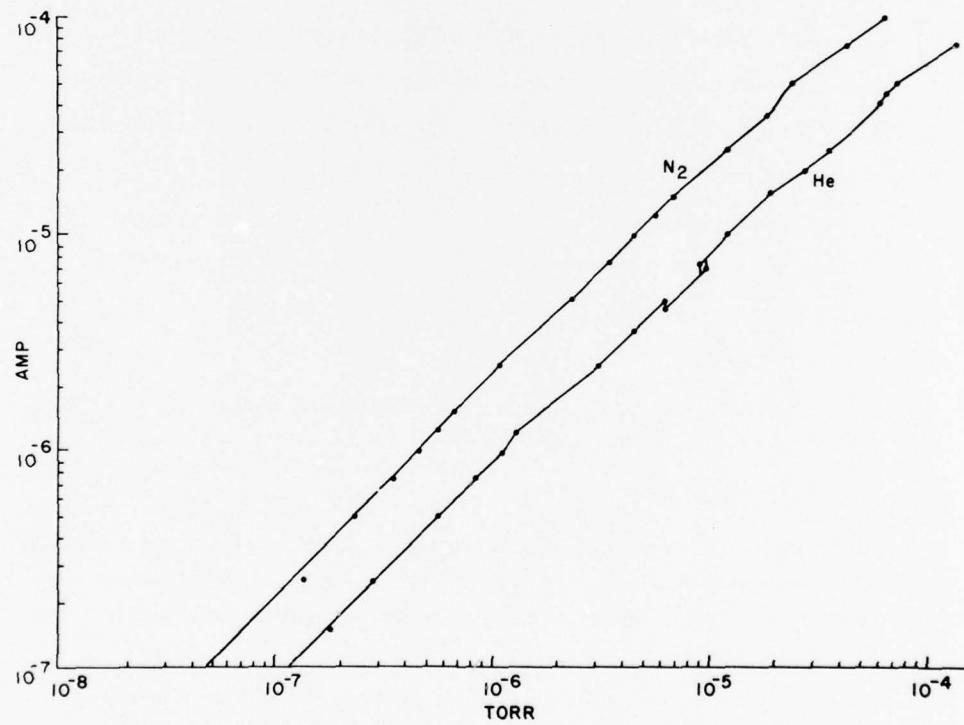


Figure 3. Laboratory Calibration Curves Obtained for Nitrogen and Helium Gases

responses obtained during the increasing system pressure cycles with those obtained during the decreasing pressure cycles, then the differences for the two gases, N_2 and O_2 , becomes less then 6 percent. The calibration for oxygen only covered the range from 1×10^{-6} to 1×10^{-5} torr so that the above discussion is relevant only to that range of values. The above does indicate that because of the small observed differences, serious errors are not introduced into the data reduction results if one assumes equal sensitivities for nitrogen and oxygen as has been done here and elsewhere, Ching.³

3. DATA REDUCTION TECHNIQUE

The relationship used for data reduction is:

$$p_g = (T_g/T_a)^{1/2} p_a R(S, D, \alpha) \delta + p_{out} \quad (1)$$

where

p_g , p_a = gauge internal pressure and ambient pressure respectively.

T_g , T_a = absolute gauge wall temperature and ambient gas respectively.

$R(S, D, \alpha)$ = gauge sampling tube factor, a function of transmission probabilities.

S = speed ratio U/v_m .

U = satellite velocity.

v_m = most probable velocity of the ambient gas.

D = diameter to length ratio of the gauge sampling tube.

α = attack angle.

δ = recombination factor, for no recombination δ equals unit and for total recombination equals $\sqrt{2}$.

p_{out} = residual gauge pressure.

Tabulated values and the theory for the $R(S, D, \alpha)$ function have been published by Hughes.⁴ A more detailed description and discussion of Eq. (1) above is contained in reference 1. Once ambient pressure has been determined, ambient density is obtained using the ideal gas law:

- 3. Ching, B.K., and Palmer, J. (1974) Upper Atmospheric Density Inferred From Magnetron Data, Aerospace Corporation Report No. TR-0074 (4260-10)-7.
- 4. Hughes, P.C. (1965) Theory for the Free Molecular Impact Probe at an Arbitrary Angle of Attack, University of Toronto UTIAS Report No. 103.

$$\rho_a = \frac{M}{R_m} \frac{1}{T_a} p_a \quad (2)$$

where

ρ_a , p_a , T_a = ambient density, pressure and absolute temperature respectively.

M = mean molecular mass of ambient gas.

R_m = Universal gas constant.

Data reduction involved the processing of the ionization gauge measurements to obtain internal gauge pressures (p_g) as a function of attack angle over each satellite spin cycle. The gauge dependence upon attack angles is contained in the R function; hence a linear least squares fit of the following form was performed over each half of the spin cycle:

$$p_g = a R(S, D, \alpha) + b \quad (3)$$

Figure 4 shows an example of the fit obtained in the manner described above. From such fits the value of a and b are obtained. The slope of the least squares fit involving p_g and R is:

$$a = (T_g/T_a)^{1/2} p_a \delta \quad . \quad (4)$$

As all the parameters in the above equation can be ascertained, one can solve for the ambient pressure. Some assumptions have to be made concerning T_a and δ and values for these parameters are obtained under the appropriate conditions from atmospheric models. For this data the Jacchia 1971 model⁵ has been used. It should be noted, however, that the dependence of p_a upon the above two parameters is at its greatest, a square root dependence. For each spin cycle two ambient pressure values are determined one from data obtained as the gauge approaches ram and the second as it moves away from ram. The two ambient pressure values are averaged producing a single value for each spin cycle which is assigned the altitude at which the minimum attack angle for that spin cycle occurs. The pressure is converted to density by application of the ideal gas law, Eq. (2). A complete orbital acquisition, is processed in the above manner so that the final output in terms of processed data per satellite acquisition is one density determination per

5. Jacchia, L. G. (1971) Revised Static Models of Thermosphere and Exosphere With Empirical Temperature Profiles, Smithsonian Astrophys. Obs. Report 332.

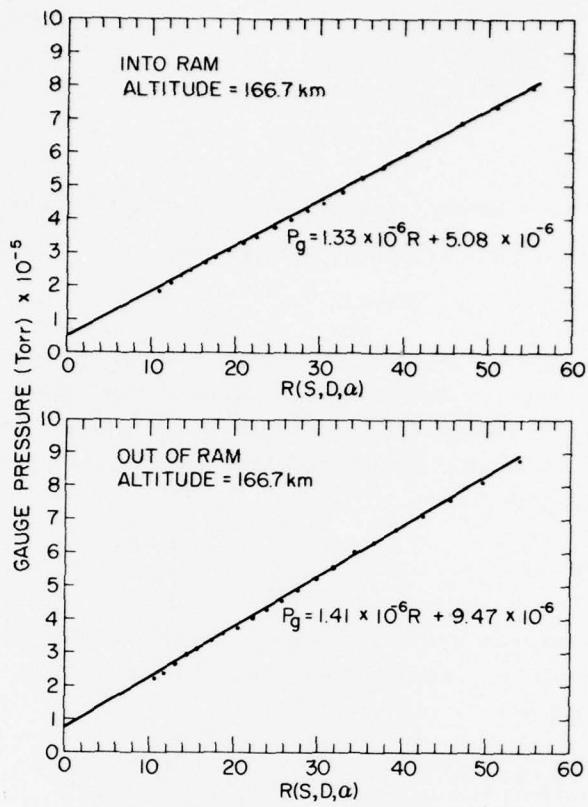


Figure 4. Least Squares Fit to Satellite Data Taken Over a Spin Cycle at 166.7 km Altitude

spin cycle. An orbital data acquisition, which for this flight was a nominal 20 min recording centered at perigee, would total about 100 spin cycles. Hence, 100 density determinations (one per spin cycle) with varying altitudinal resolution, less than 0.5 km around perigee and 10 km at 400 km altitude were obtained. The reader is again referred to reference 1 for a more detailed description and explanation of the parameters, theory of measurement and flight operations.

4. DATA RESULTS

Measurements are presented in the two appendices as altitude/density plots and altitude/universal time plots. The data given are not all inclusive but rather representative samples taken over the satellite's life during the four month period from 24 January 1975 to 24 May 1975. Although the appendices are lengthy, the

data shown in them represents slightly less than 10 percent of the total data base accrued from the satellite flight. Taken together with the data published in reference 1, their combined total still represents only 25 percent of the data base.

Table 1 provides a tabulation on a monthly basis of both the data obtained over the entire flight as well as the data given in the attached appendices. Figure 5 is a graph of satellite positional data. This figure defines satellite location in terms of perigee location, with local time, latitude and altitude of the satellite's perigee given as a function of date and revolution number. In Appendix A plots of density (gm/cc) vs universal time are shown. The circle values are values of atmospheric density obtained from gauge measurements, and the crosses are the appropriate Jacchia 71 model values computed for the same conditions of the measurements. In the upper portion of the same plots, the crosses now denote the ratios of the measured gauge determined densities to the J71 model values. It should be noted here that the scale on the upper portion ratio plots does not remain the same throughout the appendix. In some data the scale for the ratio plots was expanded to range from 0.25 to 1.75. The sunshade nomenclature shown in the right hand legend gives the time (U.T.) when the satellite was in sunlight and darkness, respectively. Other designations shown in ordinates, abscissa and legend are self-explanatory with the possible exception of "Geom. Lat." which is geomagnetic latitude.

In the altitude plots of Appendix B, both the circle and cross symbols denote gauge measurements; the circles are measurements performed during the downleg portion of the acquisition, that is, as the satellite descended in altitude towards perigee and the crosses are for upleg measurements when the satellite was ascending in altitude away from perigee. The solid lines shown are least squares fits through the data points. Some altitude plots as for example the one shown in Figure 6, required further processing in the form of noise editing. Figure 6 shows a "before" and "after" sample of the effect of noise data point deletion upon the least squares fit of the upleg and downleg profiles. As the least squares fit coefficients are incorporated into the computer data base files, it is especially important that meaningful and valid fits be performed.

At higher altitudes the downleg (circles) and upleg (crosses) profiles of a large number of the Appendix B plots exhibit a divergence. A major portion of this divergence is due to the spatial separation of the measurements. For example, initially perigee was located in the northern sunlit hemisphere and precessing northward towards the pole. In this case the downleg measurements are performed at high northern latitudes, whereas the upleg measurements are performed at middle and equatorial latitudes nearer to the sub-solar point. Continued precession of perigee produces downleg measurements at high northern latitudes during night, and upleg measurements at high northern latitudes during the day. In the first

case above, the divergence would reflect higher upleg densities that would be associated with the higher temperatures due to the proximity of the solar bulge. In the second case, downleg measurements reflect lower nighttime temperatures as opposed to upleg daylight measurements.

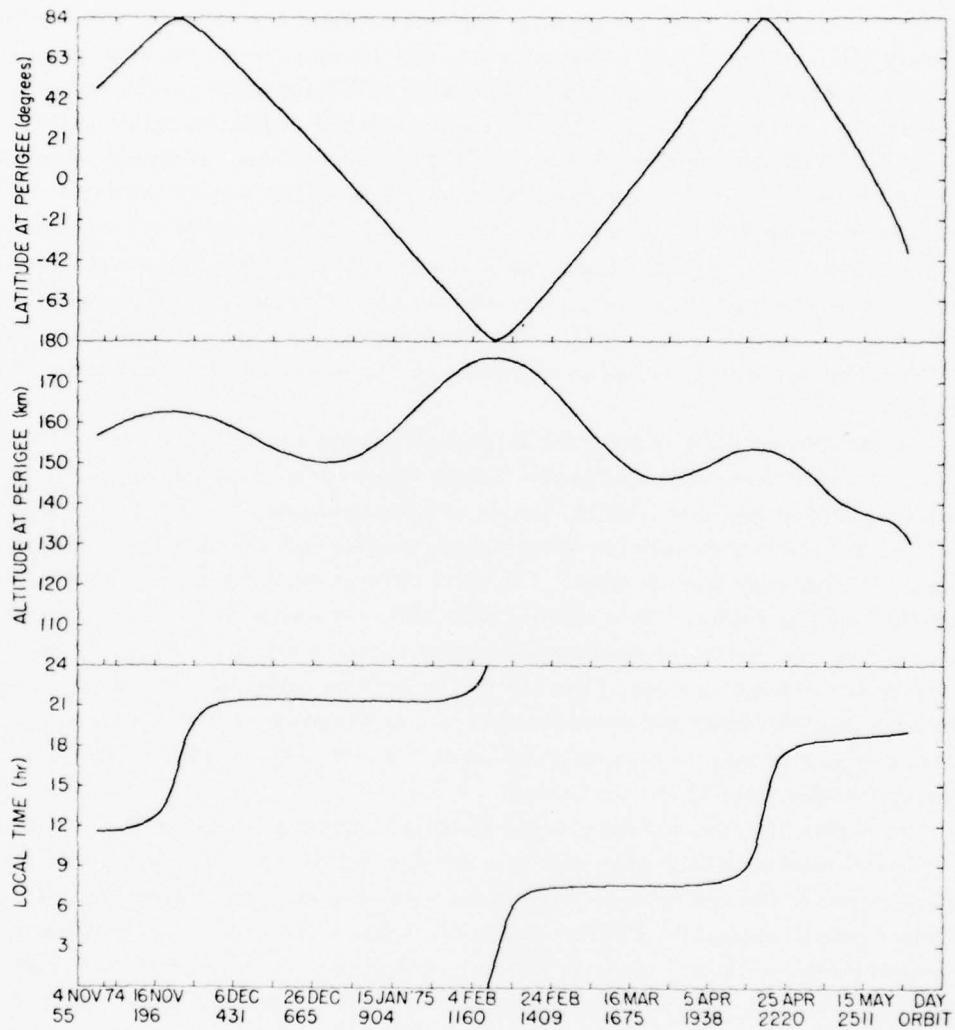


Figure 5. Satellite Location Diagram

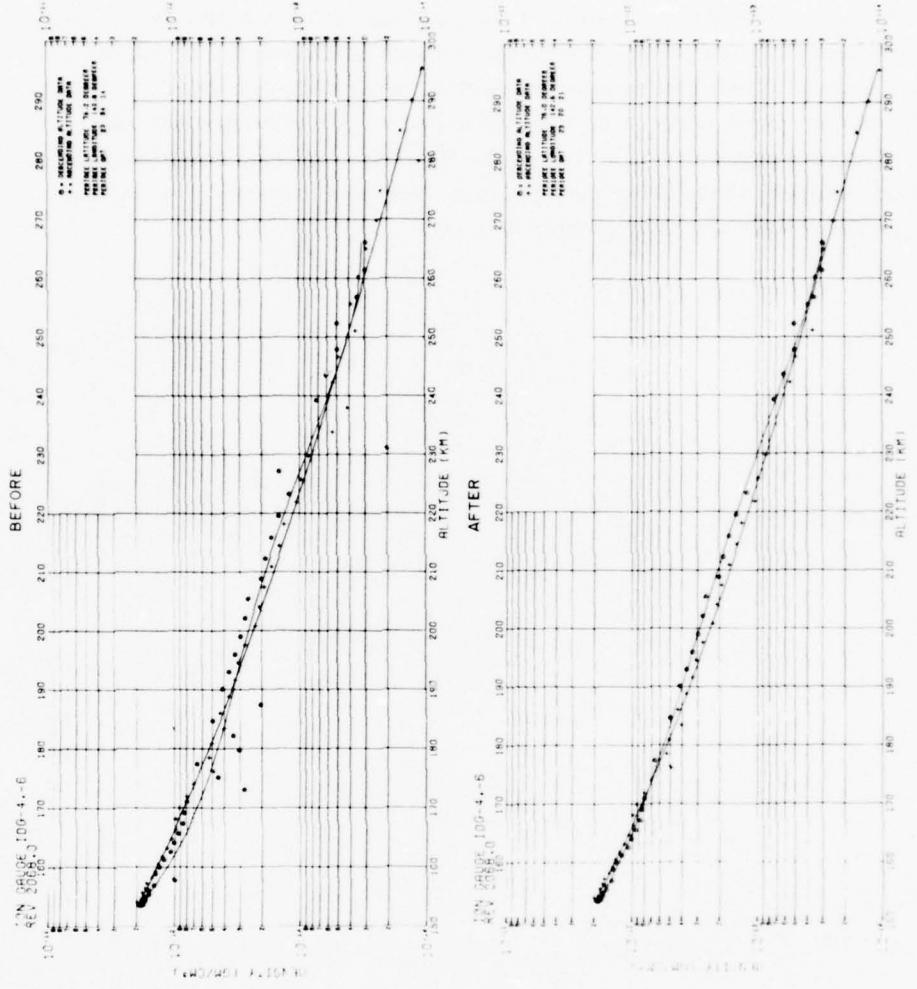


Figure 6. Ambient Density vs Altitude Profile, Before and After Noise Editing Procedure

5. SUMMARY

In this report the compilation of the S3-1 satellite ionization gauge measurements is completed. Representative samples, totalling 158 acquisitions, of neutral density measurements performed over an altitude range, in some cases, as low as 135 km up to 325 km are given in the appendices. The time period over which these measurements were obtained extended from January 1975 into May 1975. Results were obtained over both the southern and northern hemispheres; during the winter season in the southern hemisphere and during spring in the northern hemisphere. Details on the experiment, calibration procedures, measurement technique and data reduction method are described. The total data set generated as a result of this flight exceeds 1650 orbital acquisitions. The time duration of an average orbital acquisition was approximately 20 min.

References

1. McIsaac, J. P., Champion, K. S. W., McInerney, R. E., and Delorey, D. (1976) Ionization Gauge Measurements of Atmospheric Density From a Low Altitude Satellite, AFGL Report No. TR-76-0113.
2. Kreisman, W. (1964) Development of Cold Cathodes Ionization Gauges for Space Vehicles, GCA Corporation Report No. 64-17-N, Part I and No. 64-19-N, Part II.
3. Ching, B. K., and Palmer, J. (1974) Upper Atmospheric Density Inferred From Magnetron Data, Aerospace Corporation Report No. TR-0074 (4260-10)-7.
4. Hughes, P. C. (1965) Theory for the Free Molecular Impact Probe at an Arbitrary Angle of Attack, University of Toronto UTIAS Report No. 103.
5. Jacchia, L. G. (1971) Revised Static Models of Thermosphere and Exosphere With Empirical Temperature Profiles, Smithsonian Astrophys. Obs. Report 332.

Appendix A

Plots of Density vs U.T.

100-4.-6 REV. NO. 1001-0
DAY OF ORBIT 1/22/75

PERIOD

ALT (KM.) = 165.49
LONG (E) = 327.60
LAT (DEG.) = -44.57
DAT (SEC.) = 84345.0 (2325M)
LOCAL TIME 2118 (H)
IN SUN FROM 05565. TO 04297.
IN SHADE FROM 04297. TO 05095.

RATIO

1.00

1.25

0.25

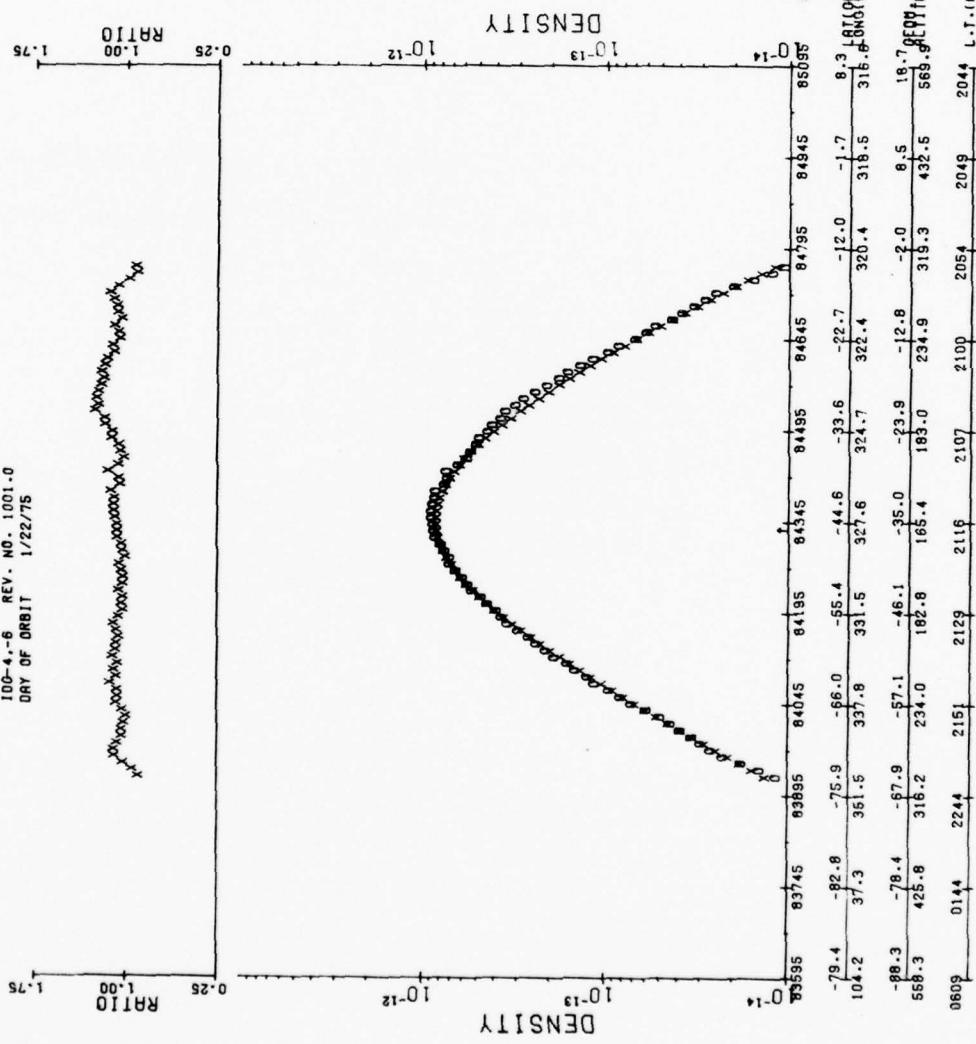
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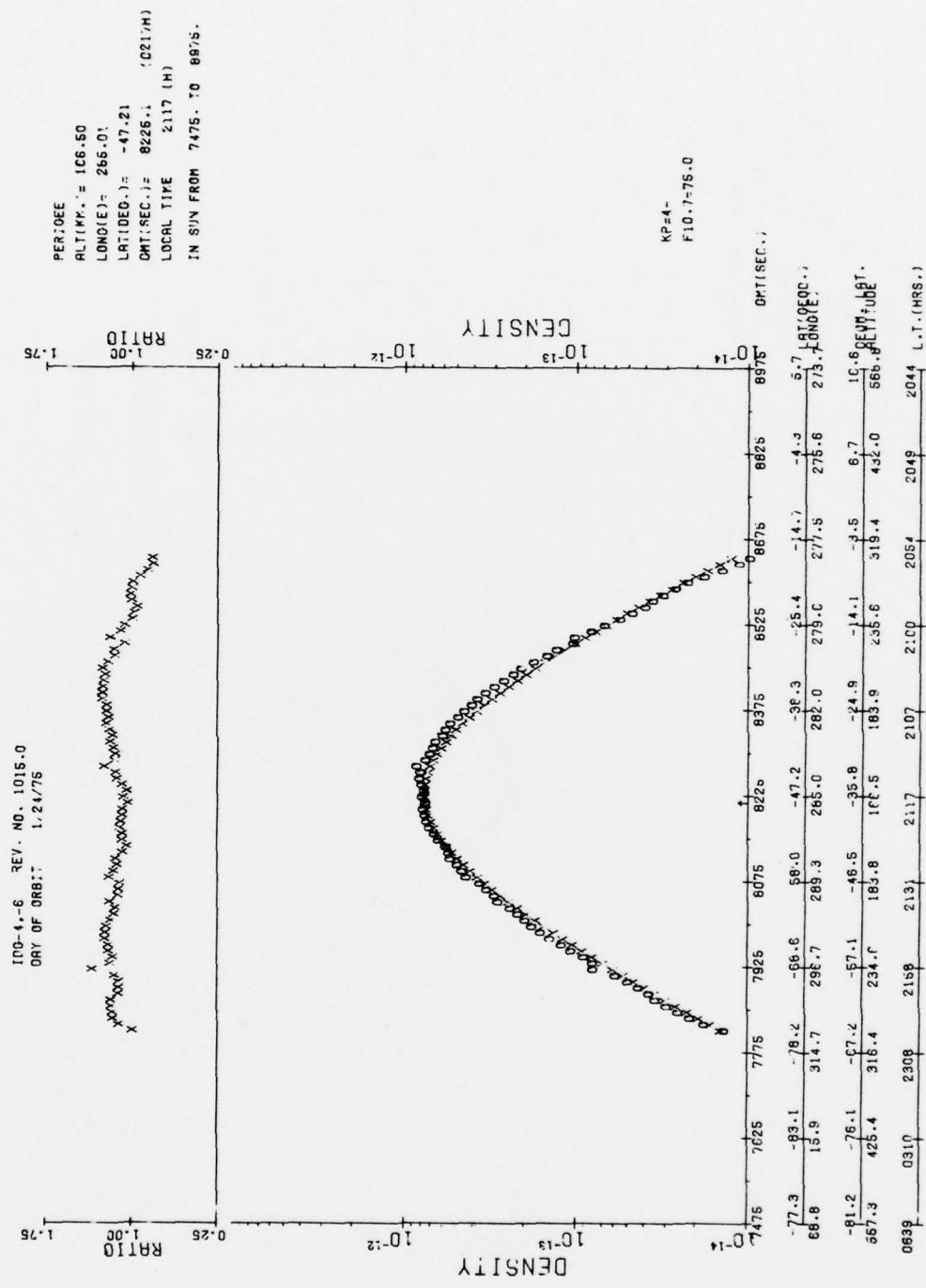
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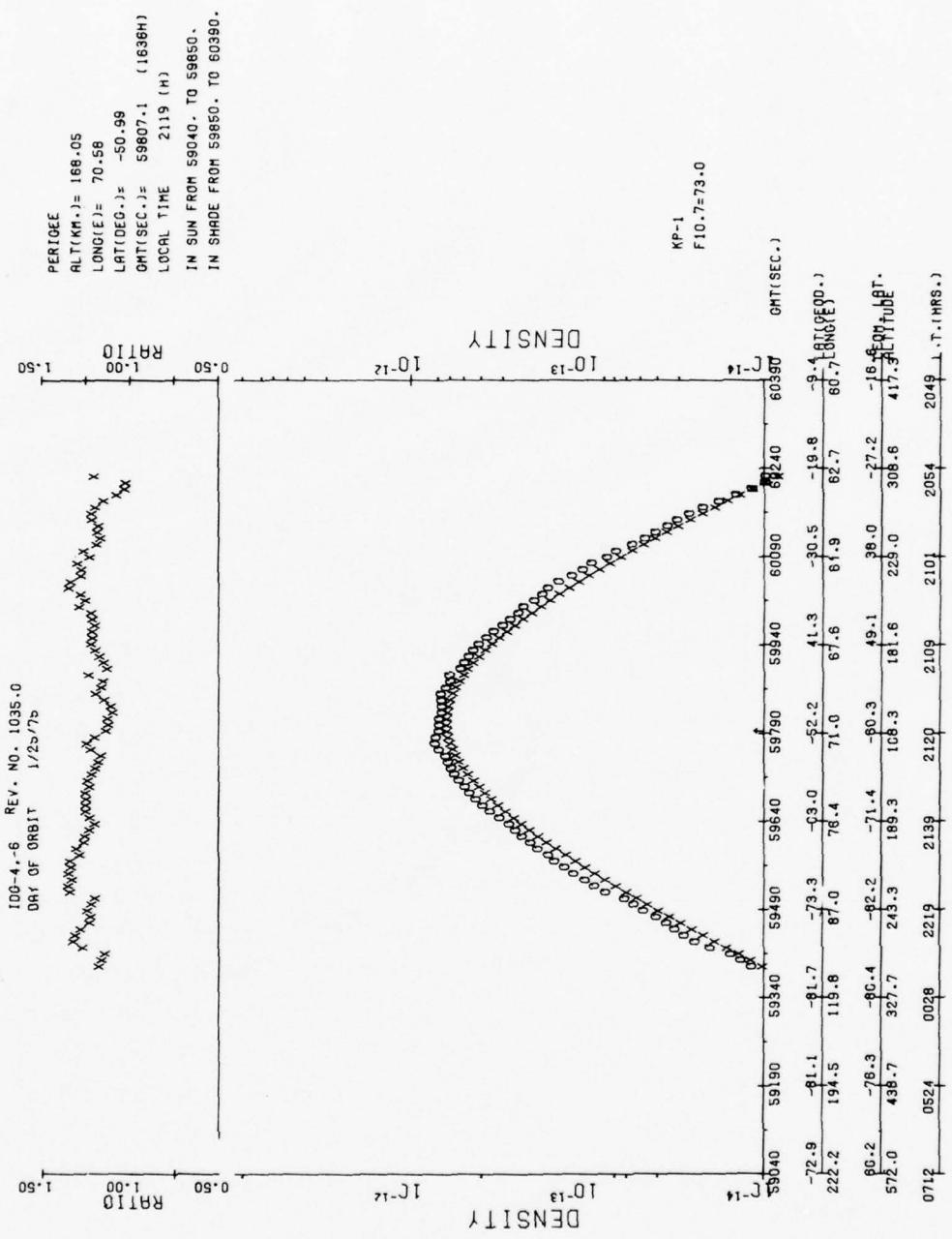
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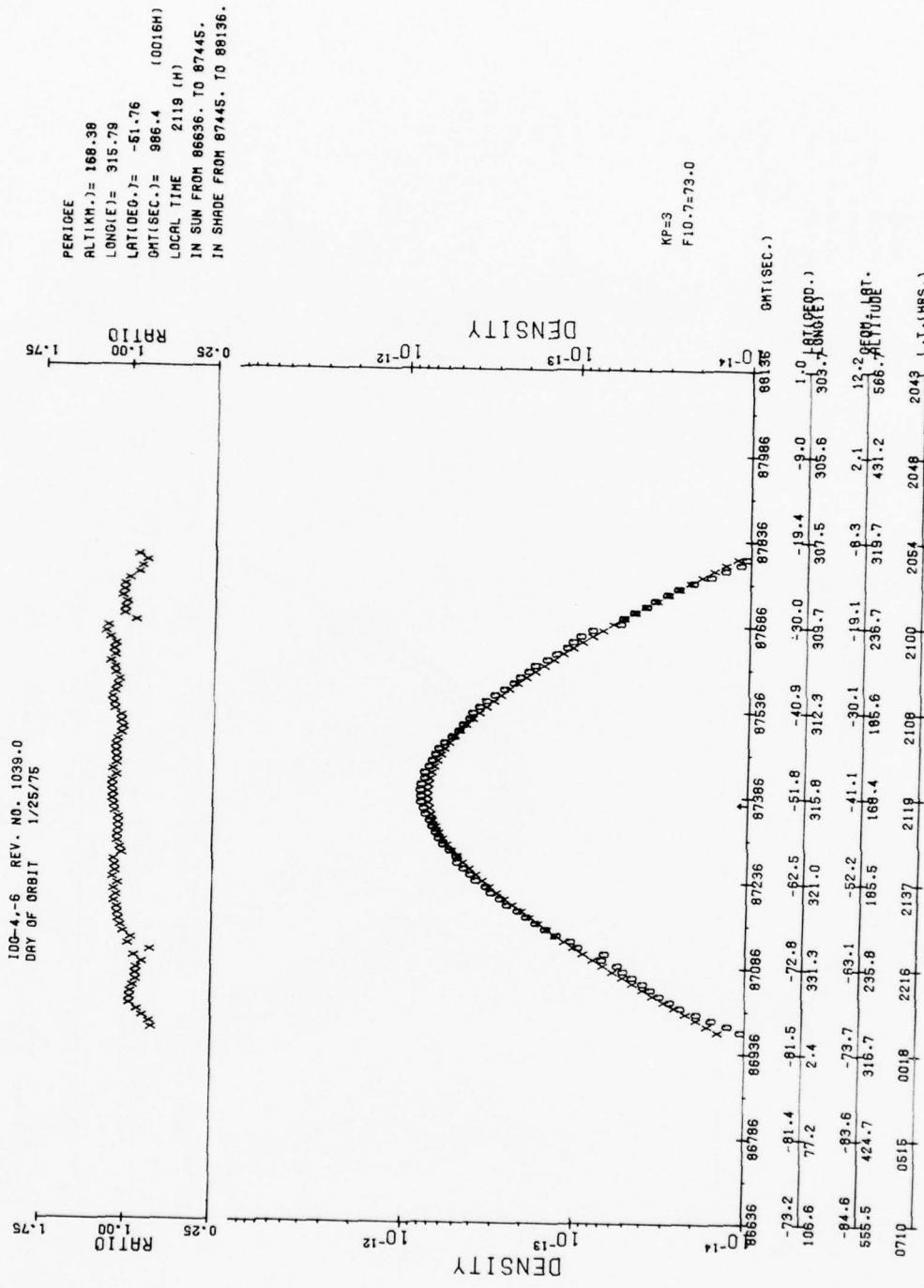
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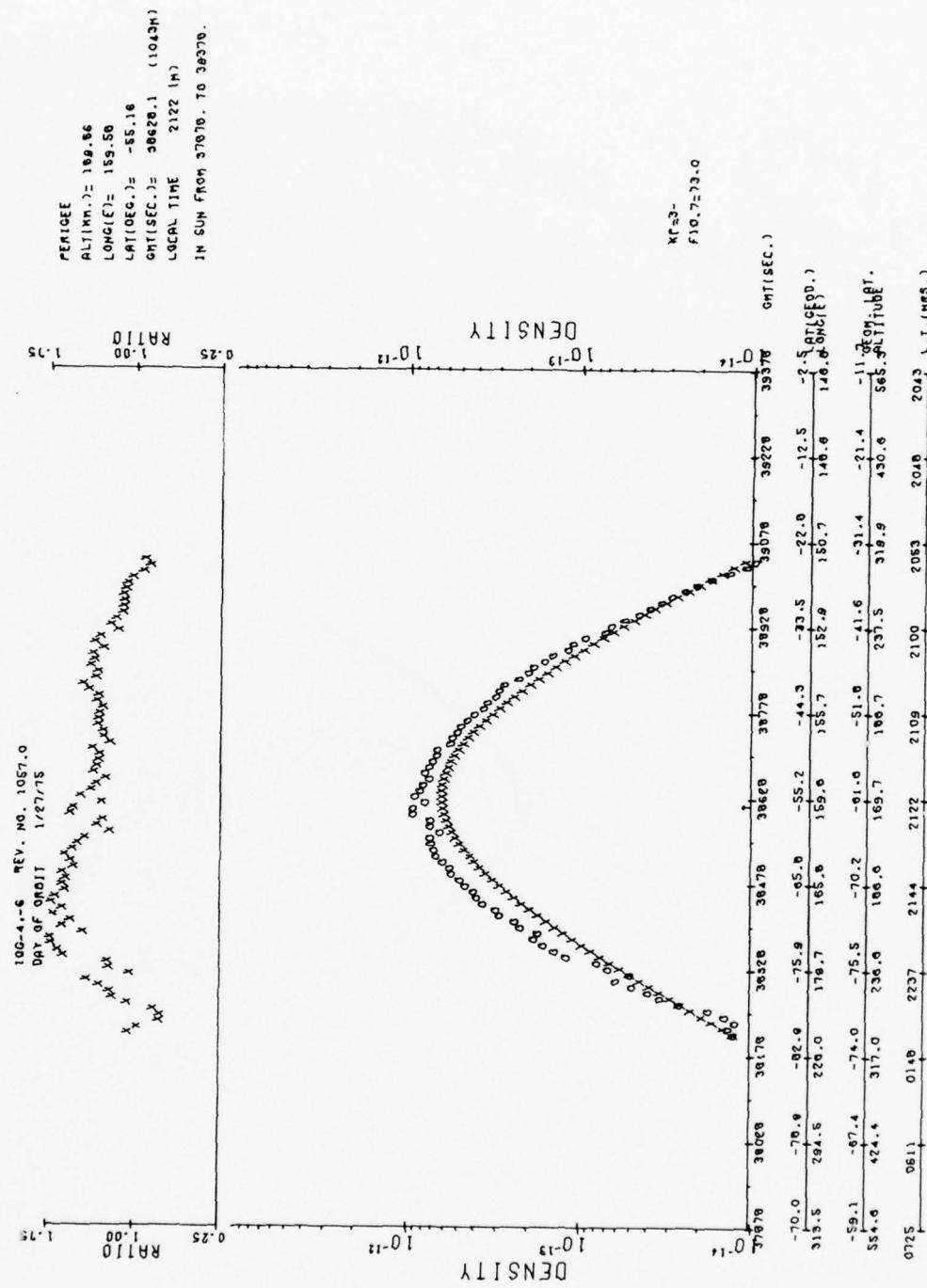
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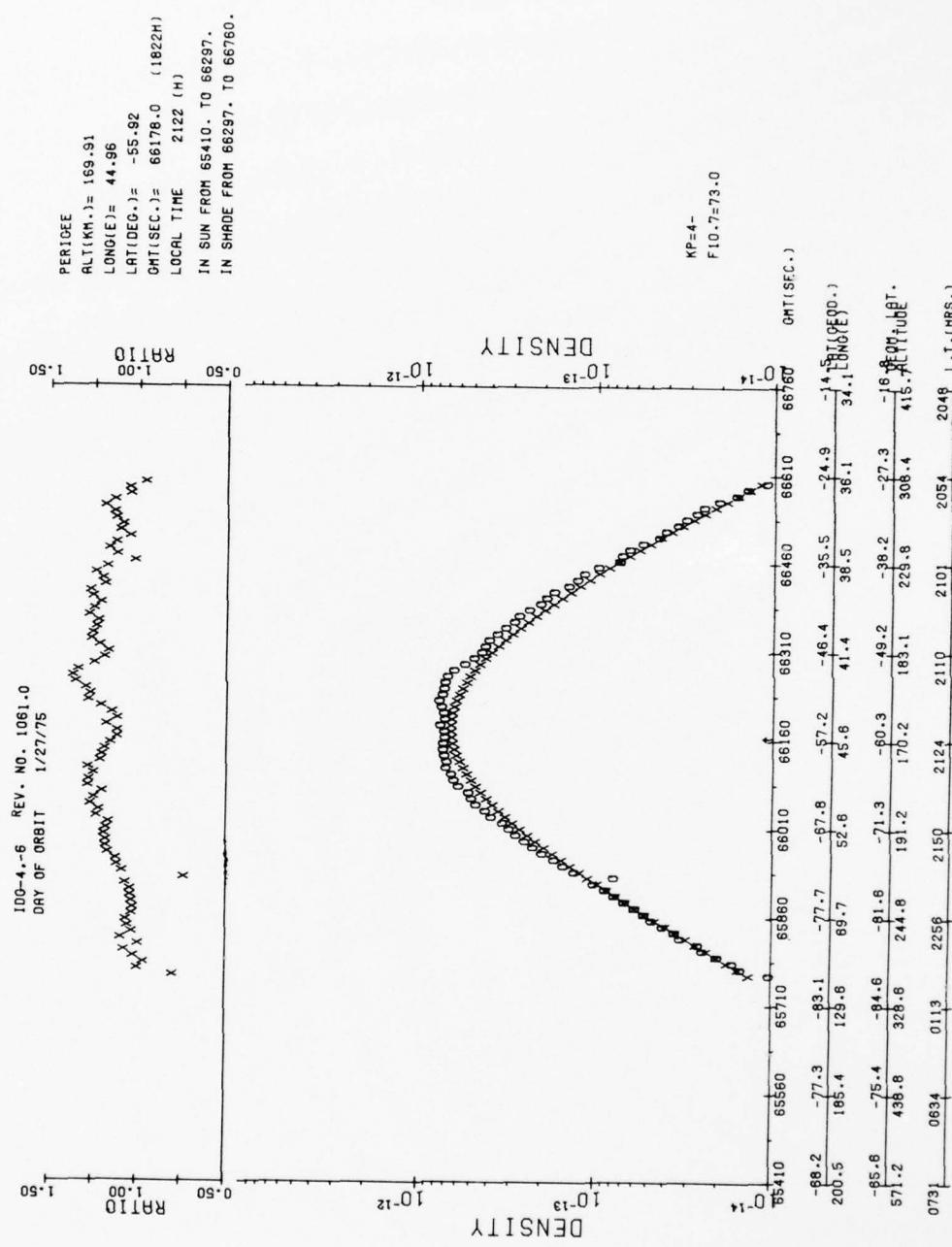




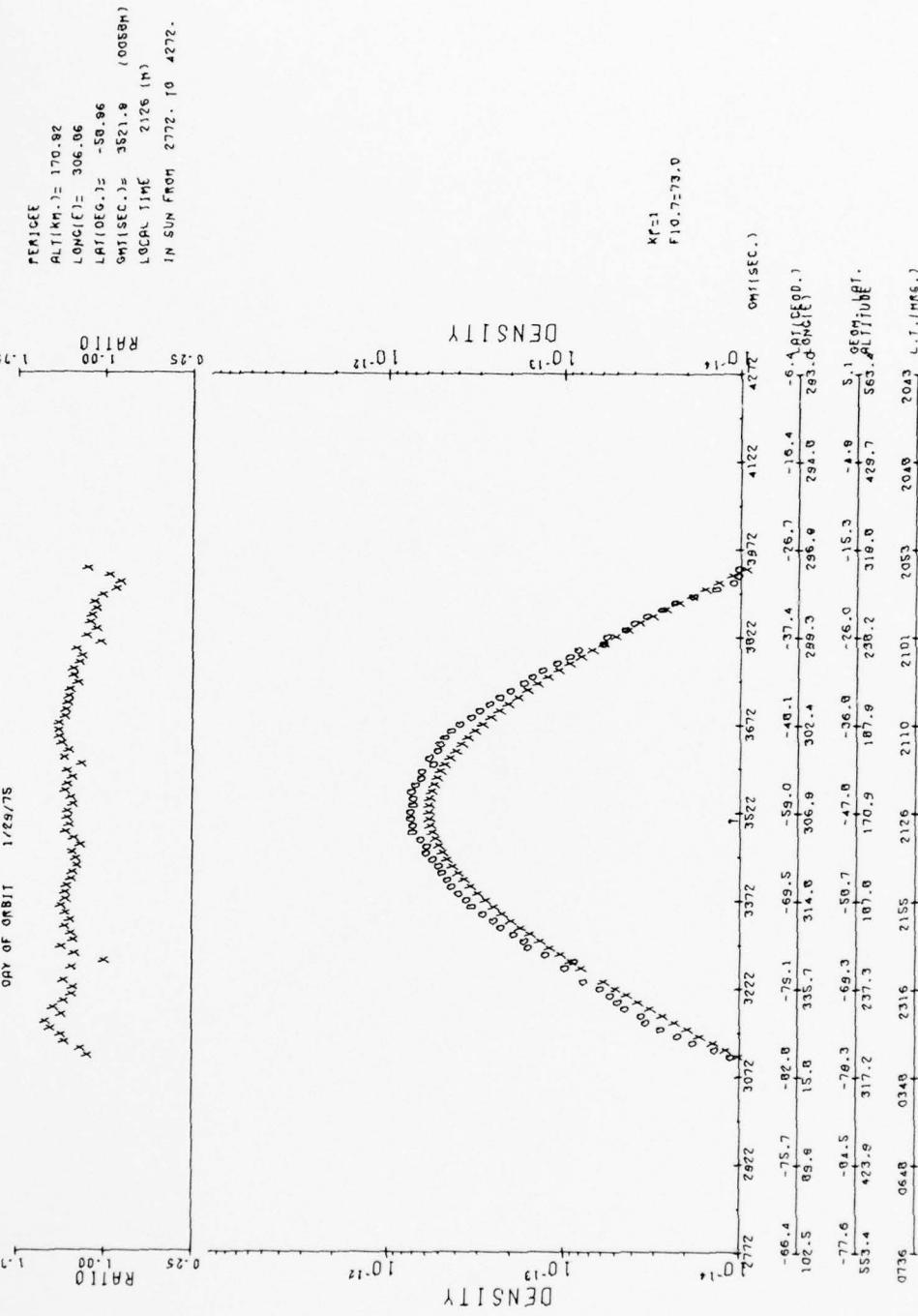


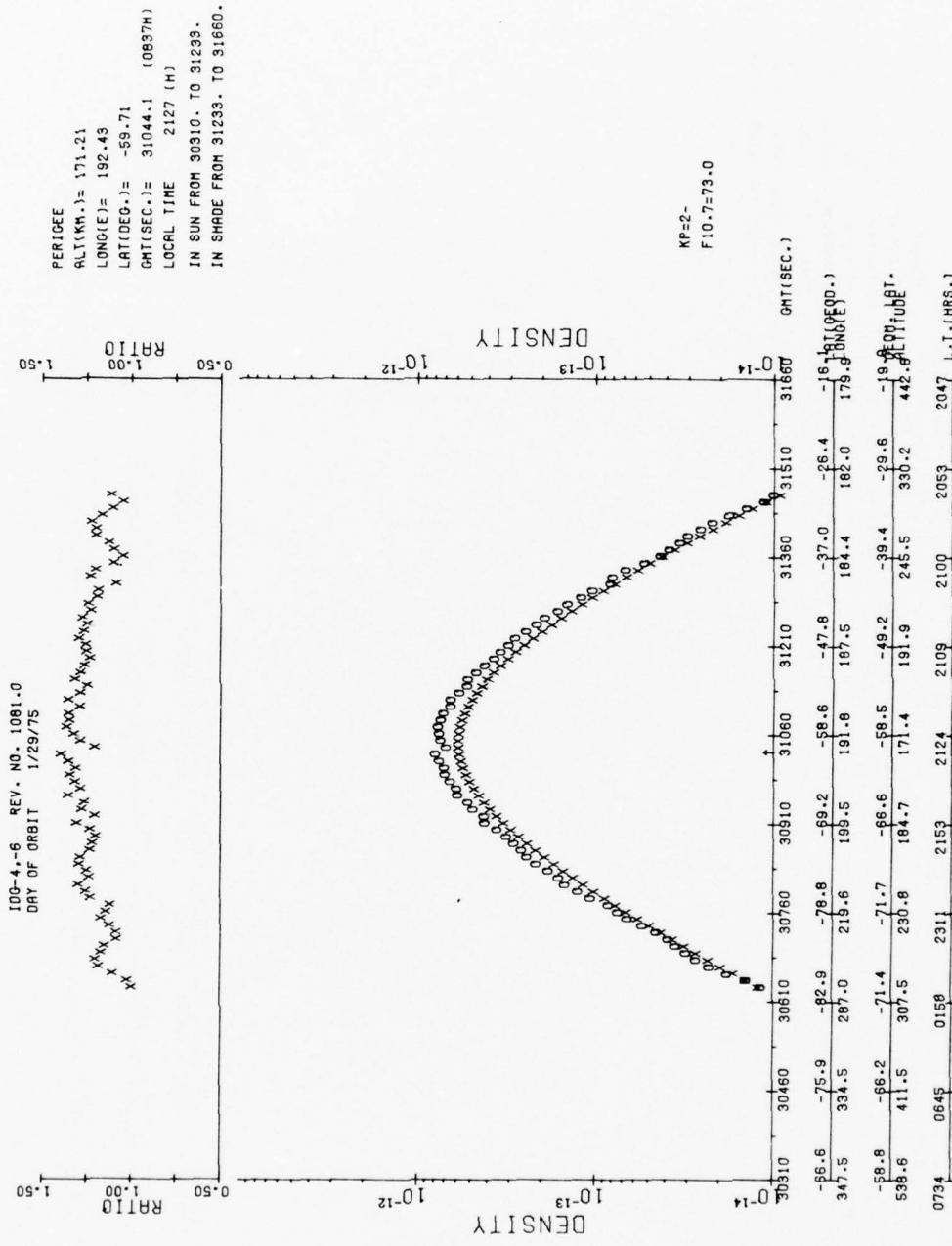


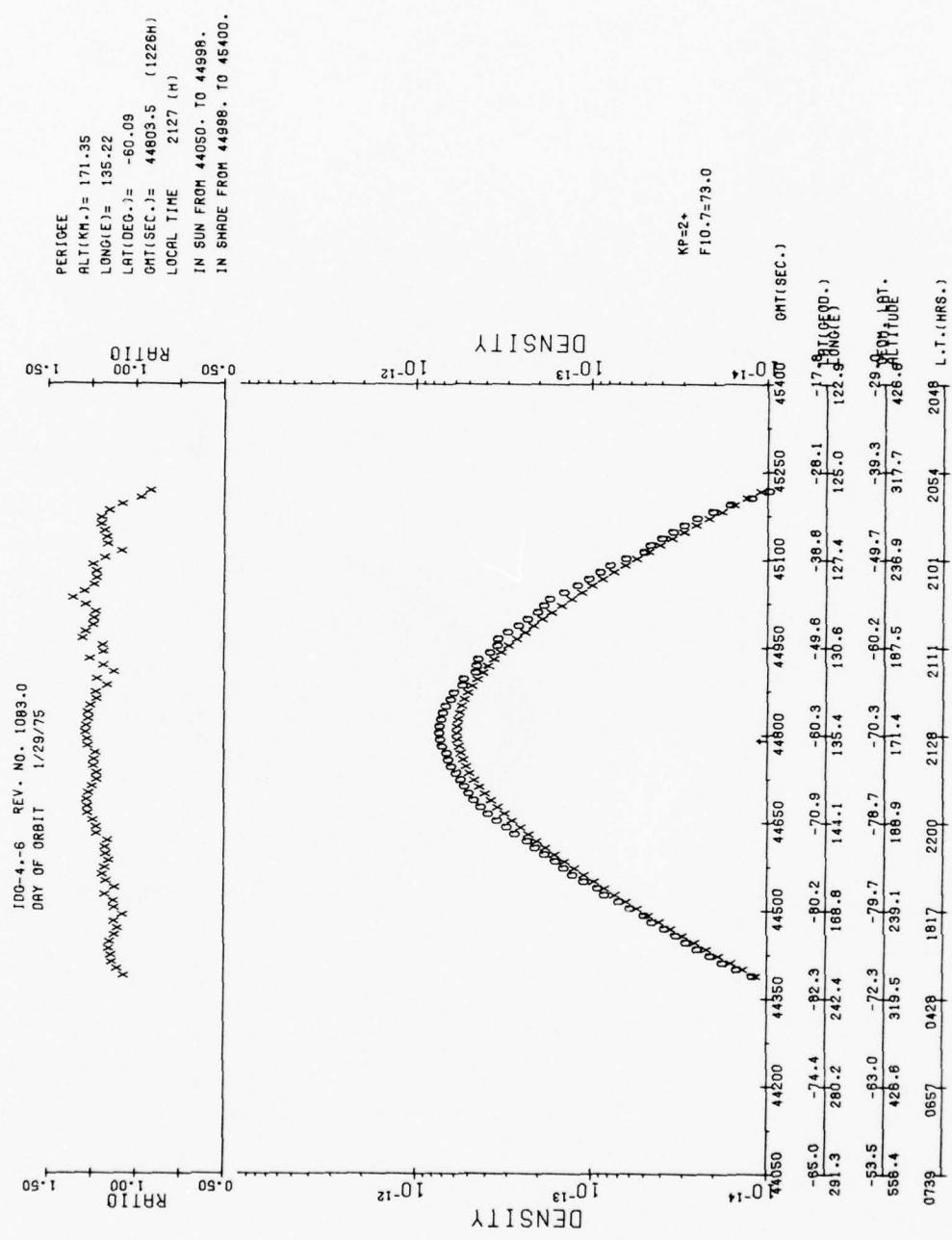


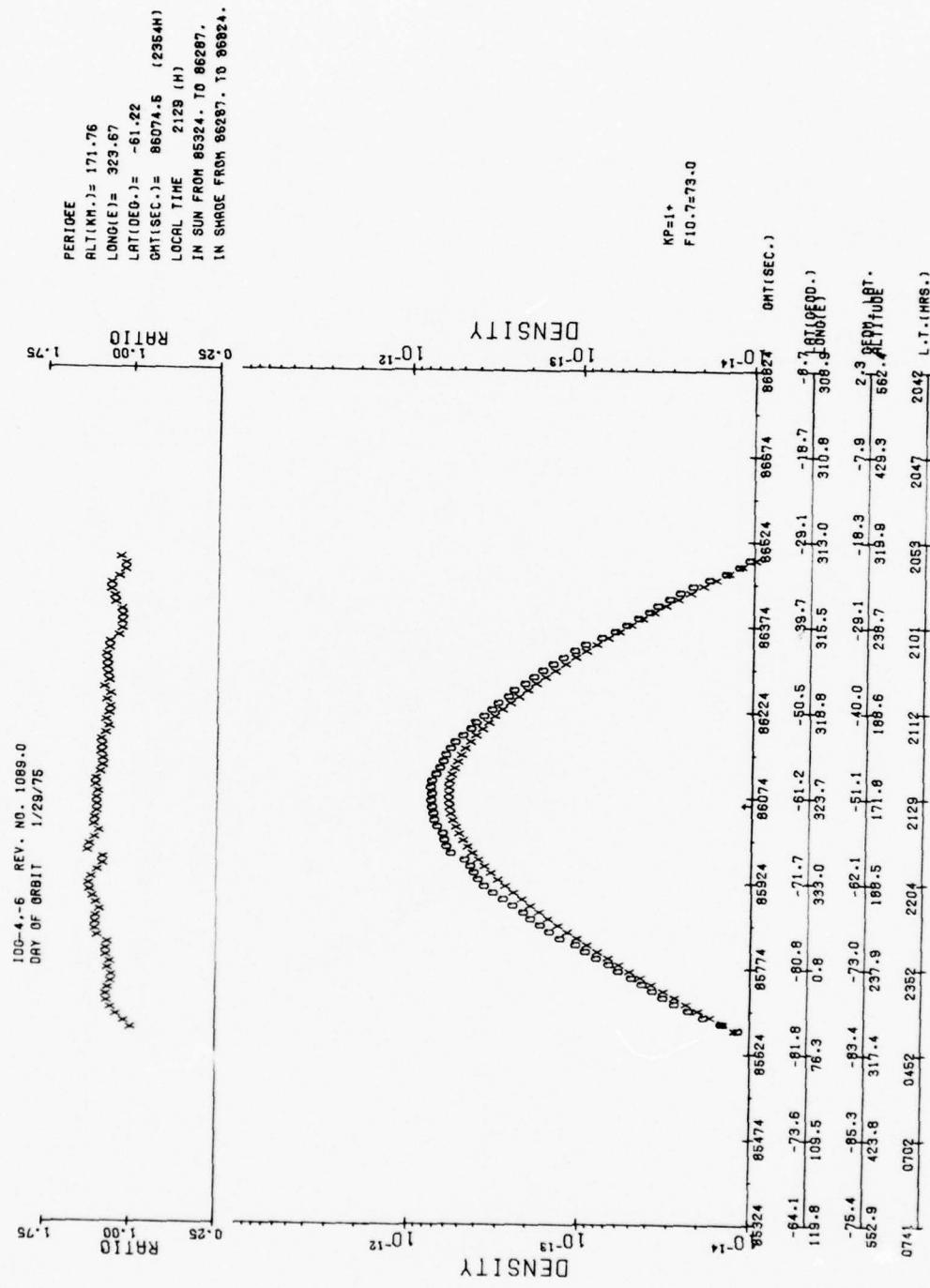


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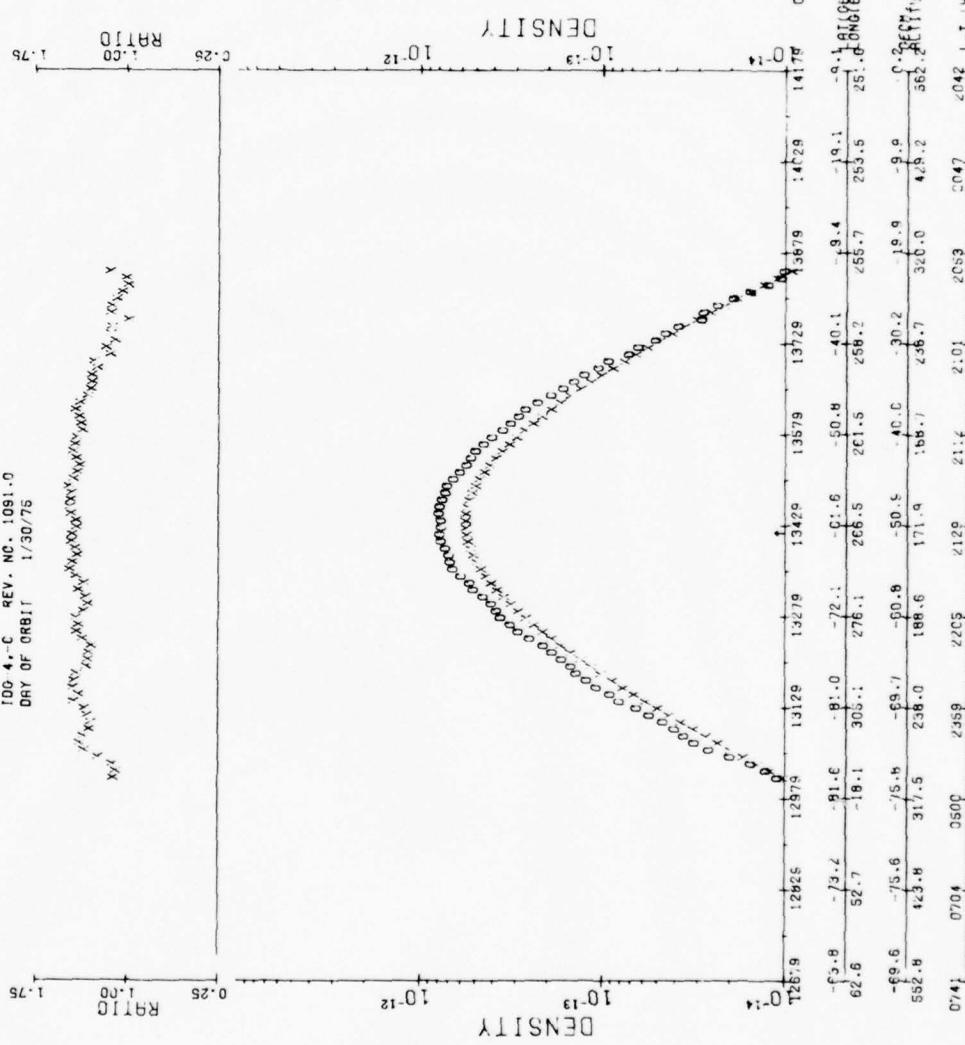


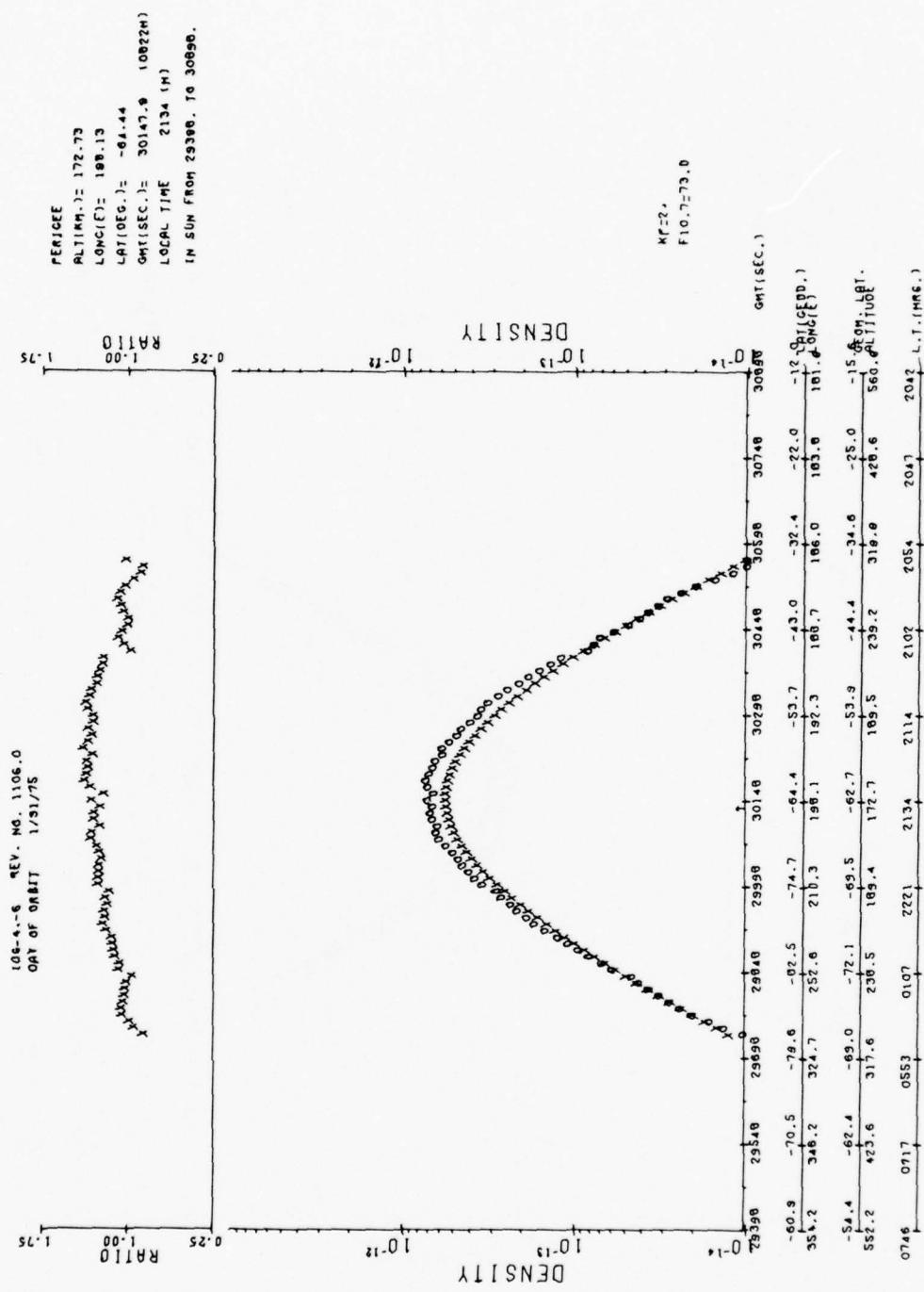


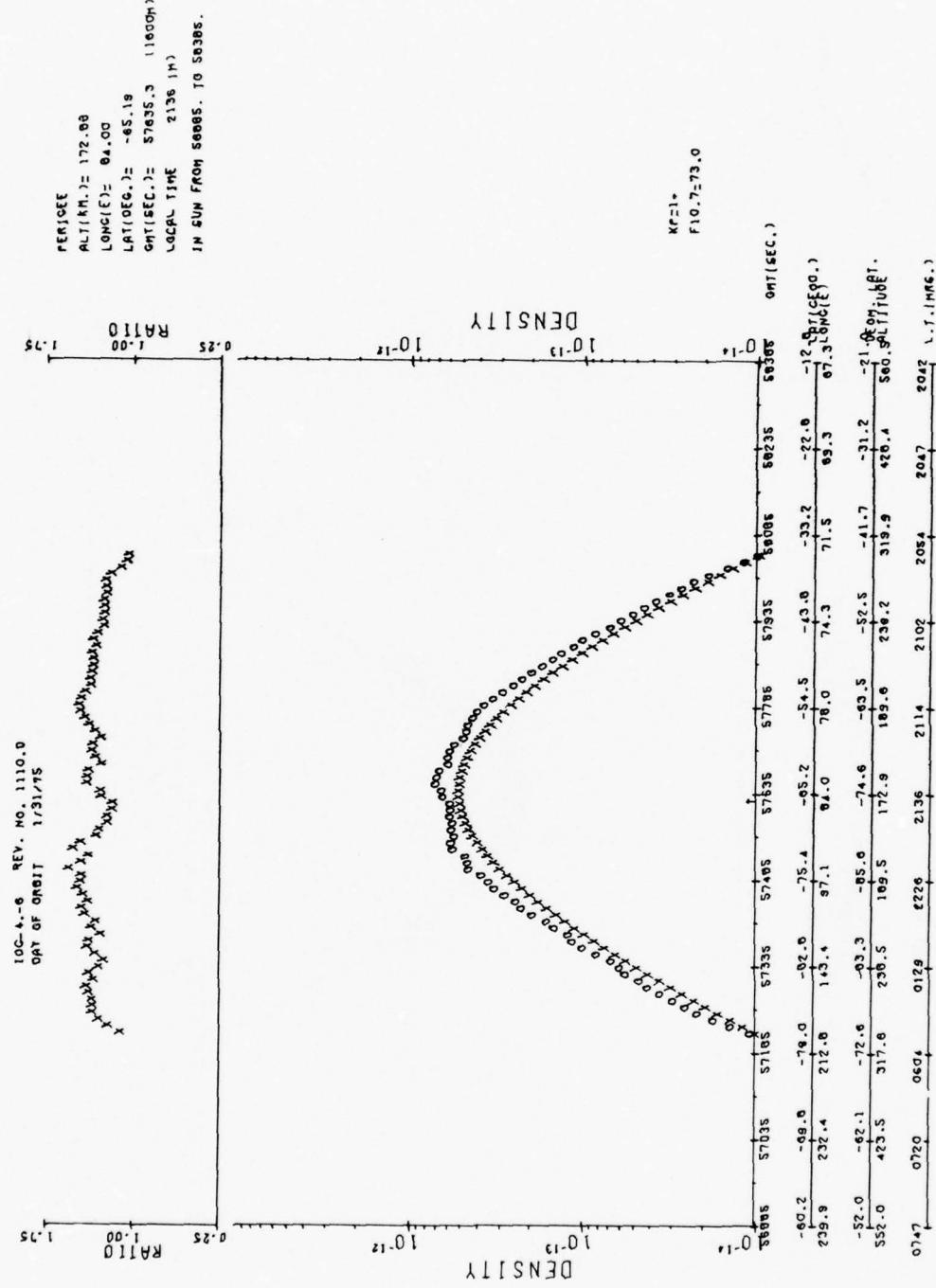


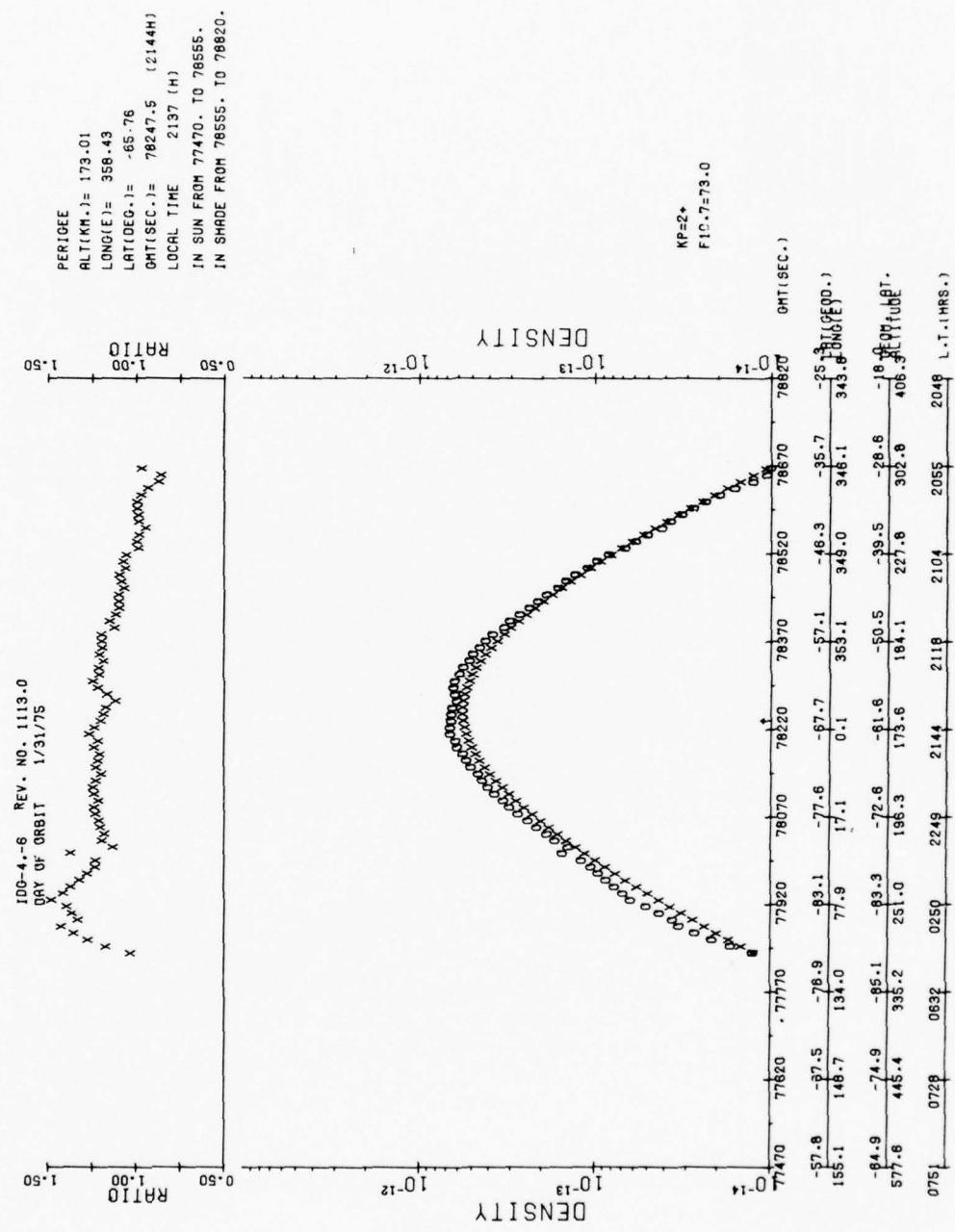
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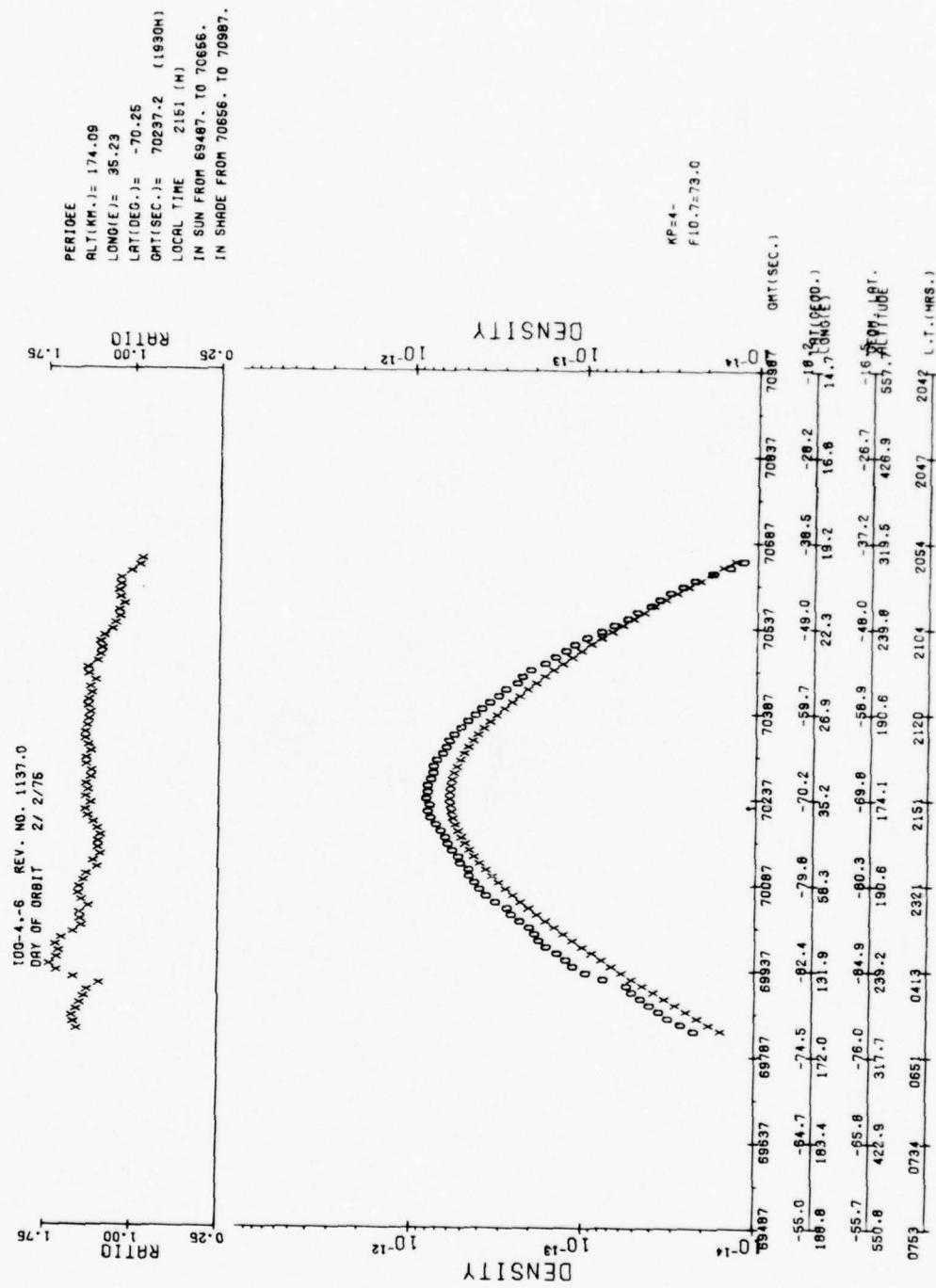
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|------------------------------|--------------------|
| PERIGEE | |
| ALTITUDE (M.) | 171.90 |
| LONGITUD. | 26°.50 |
| LATITUDE (S.) | -6°.10 |
| GMT (SEC.) | 1342.0 + 1 (0345M) |
| LOCAL TIME | 21.9 (H.) |
| IN SUN FROM 126°.9 TO 141°.9 | |

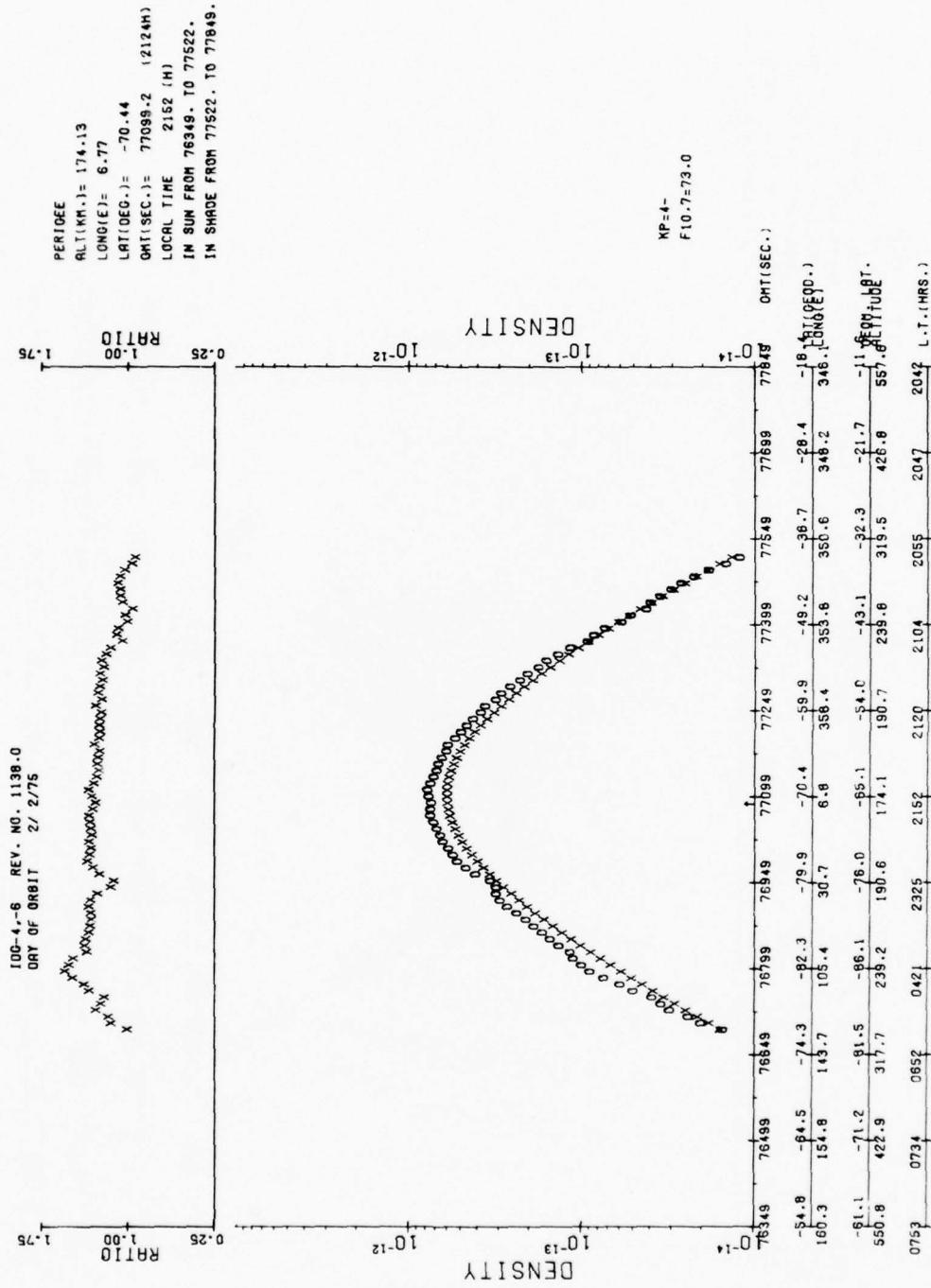


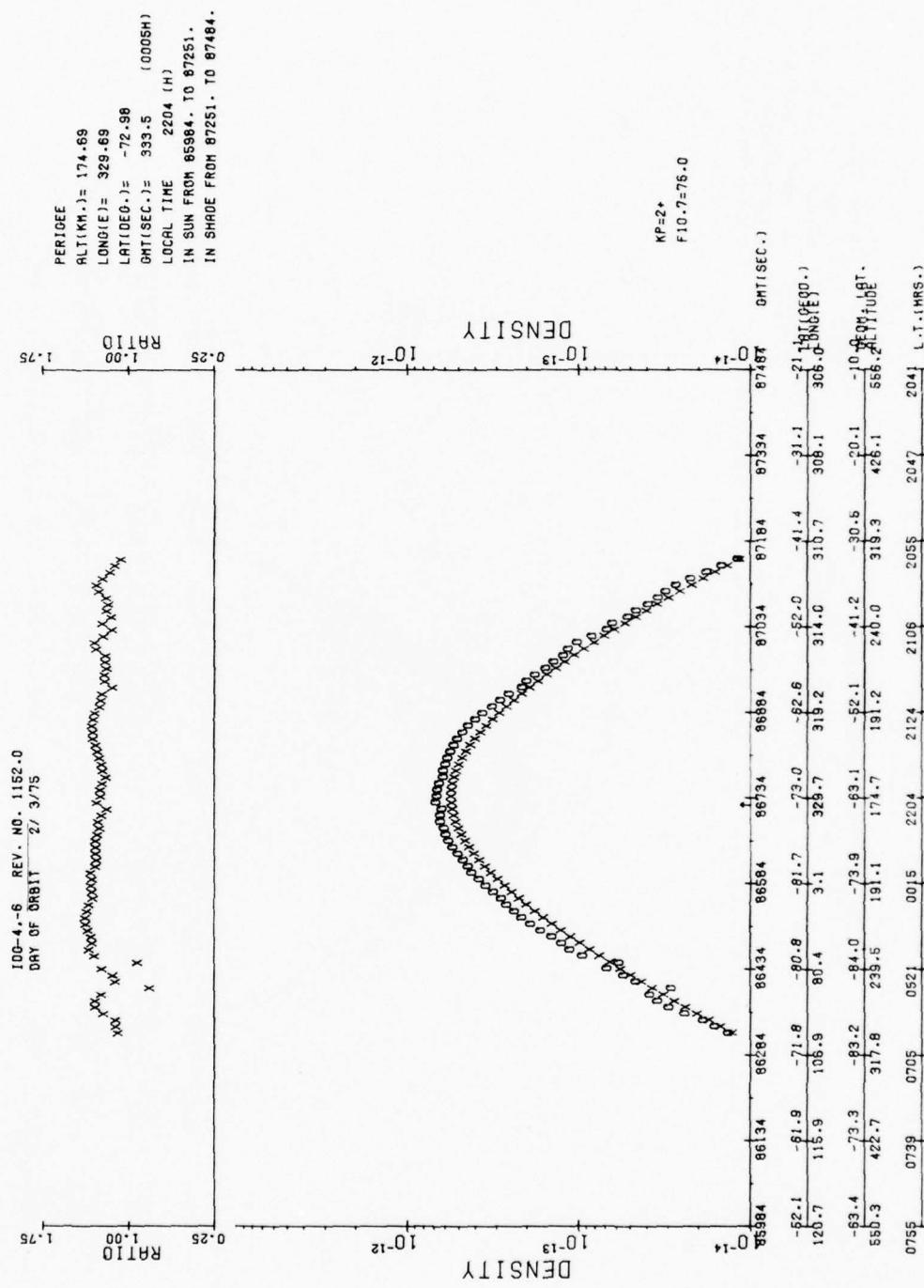




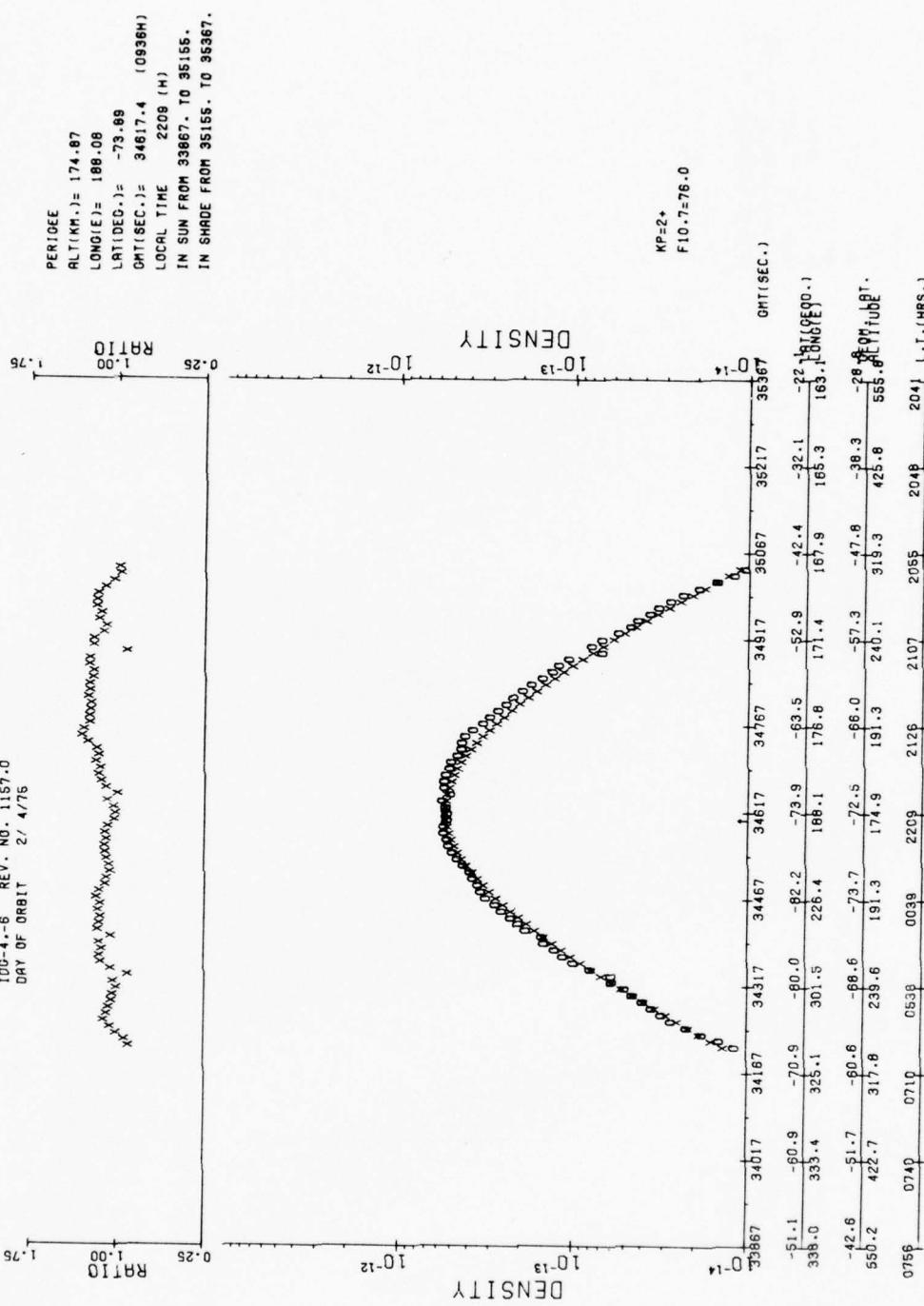


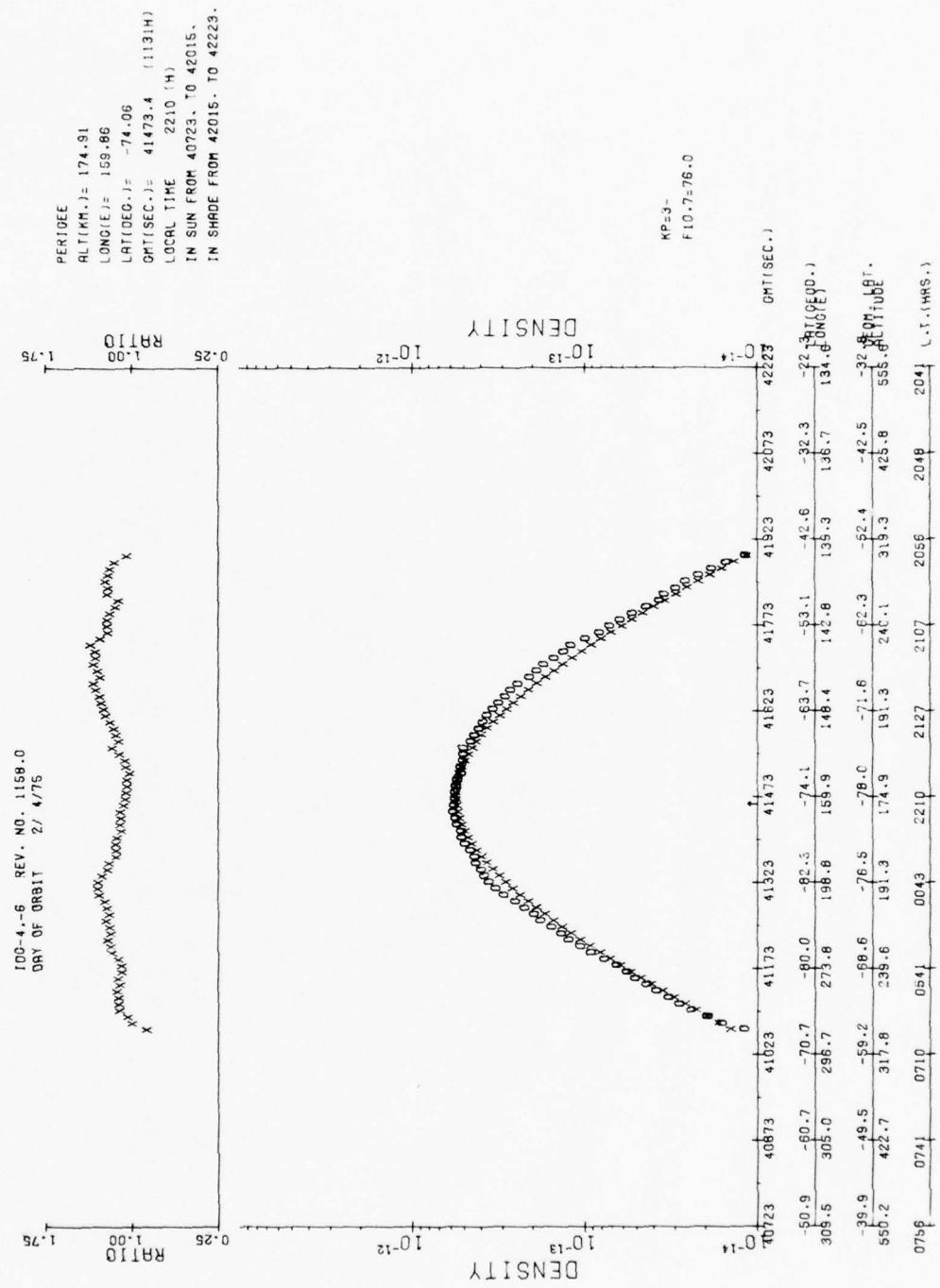




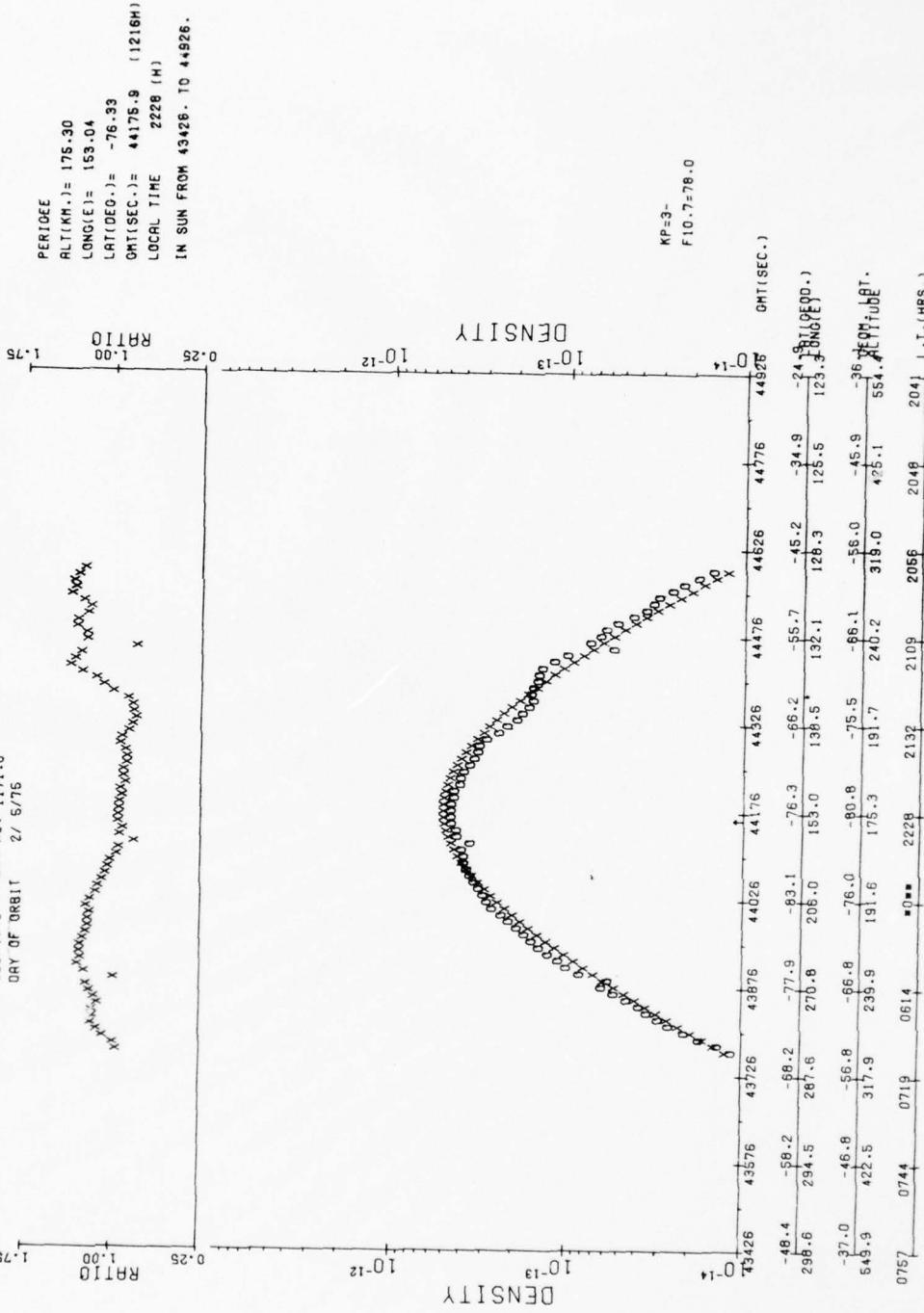


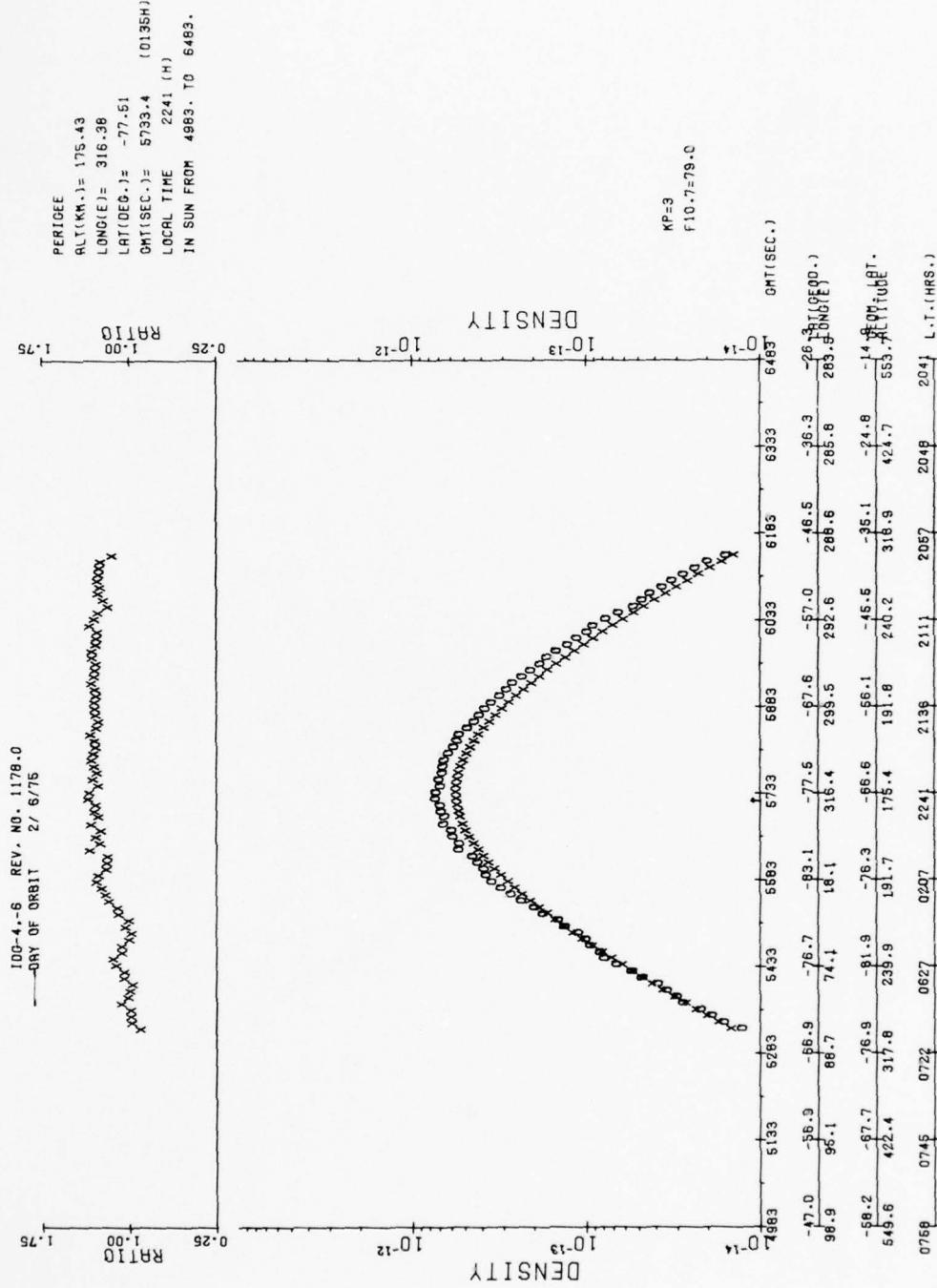
100-4,-6 REV. NO. 1157.0
DAY OF ORBIT 2 / 4/75

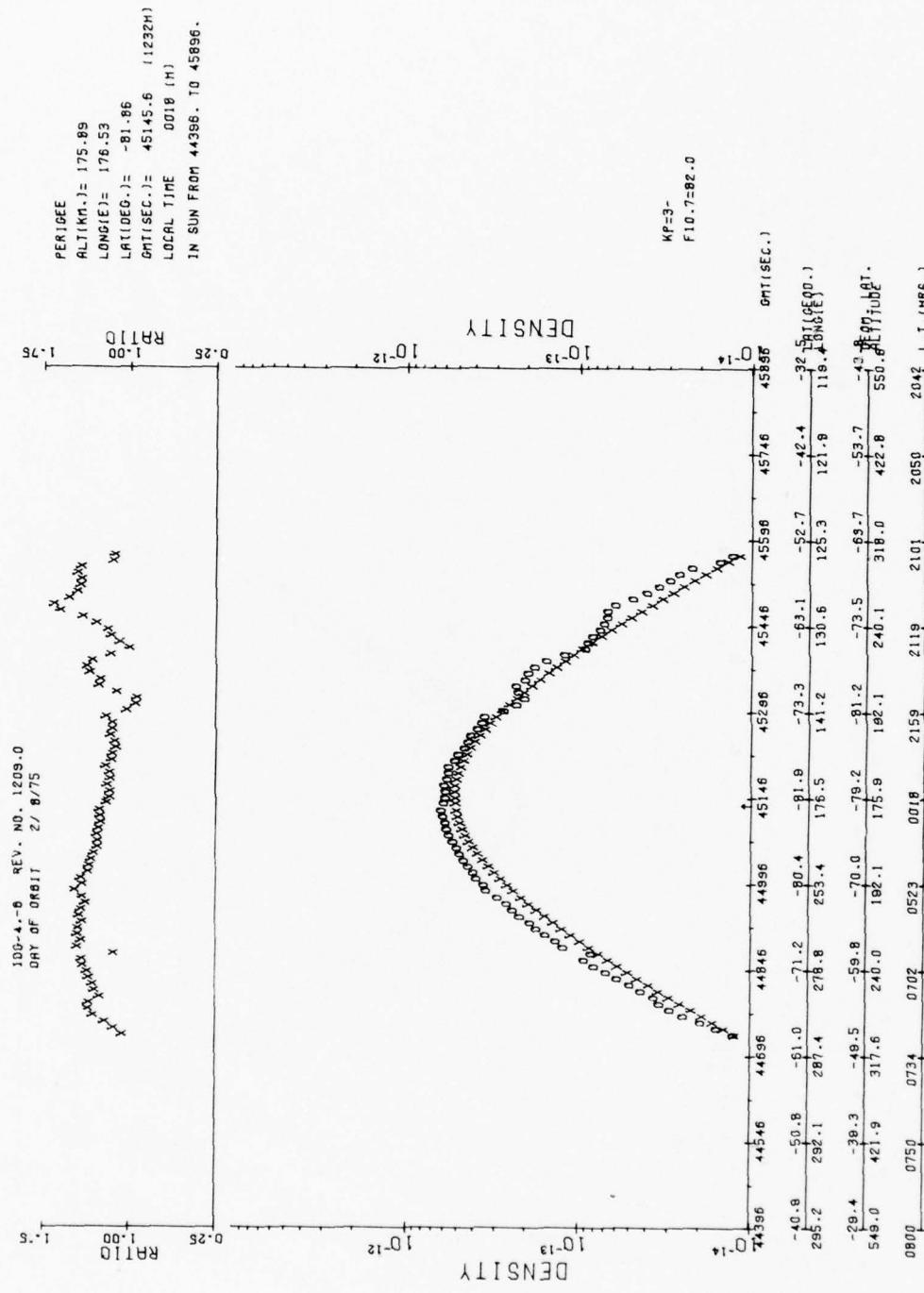


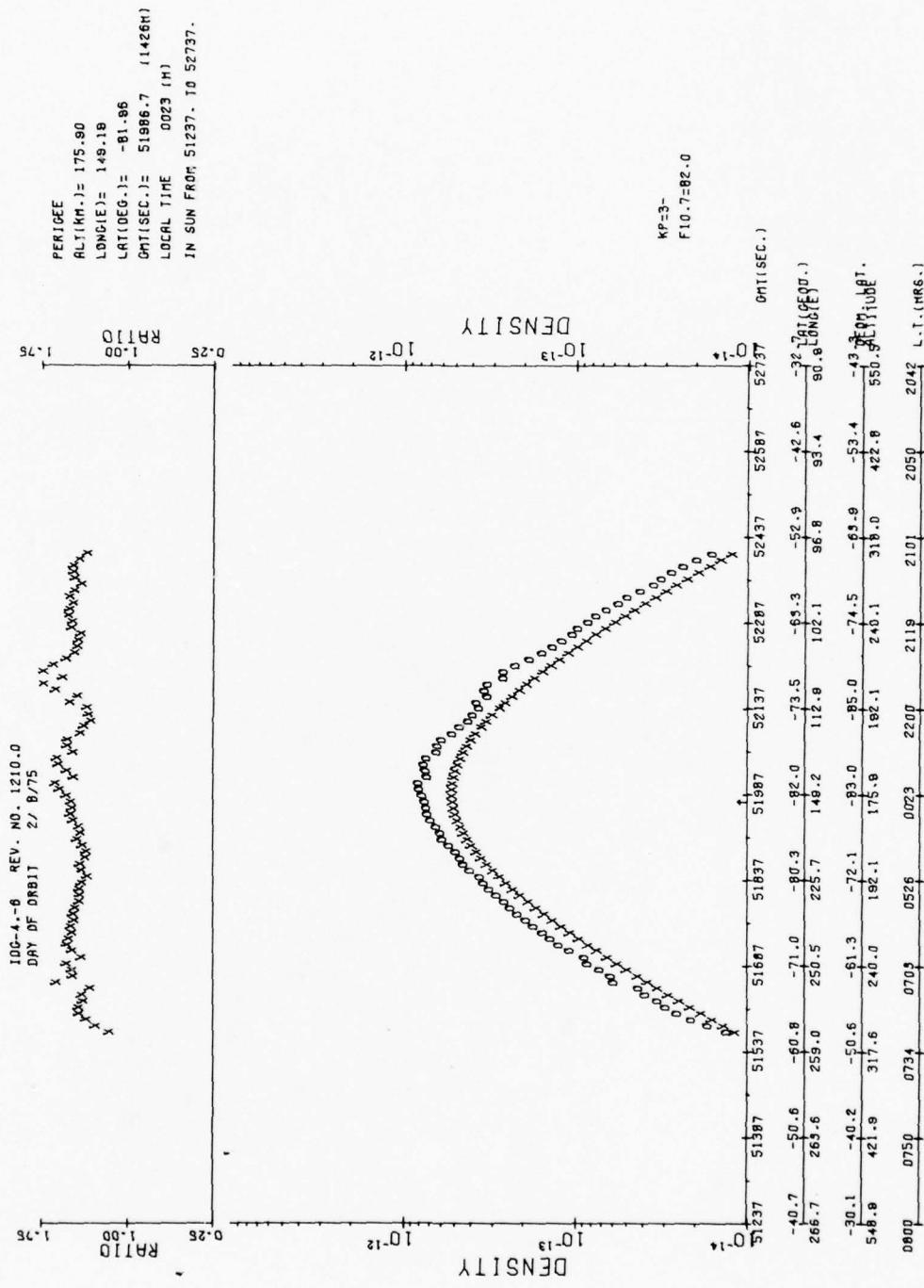


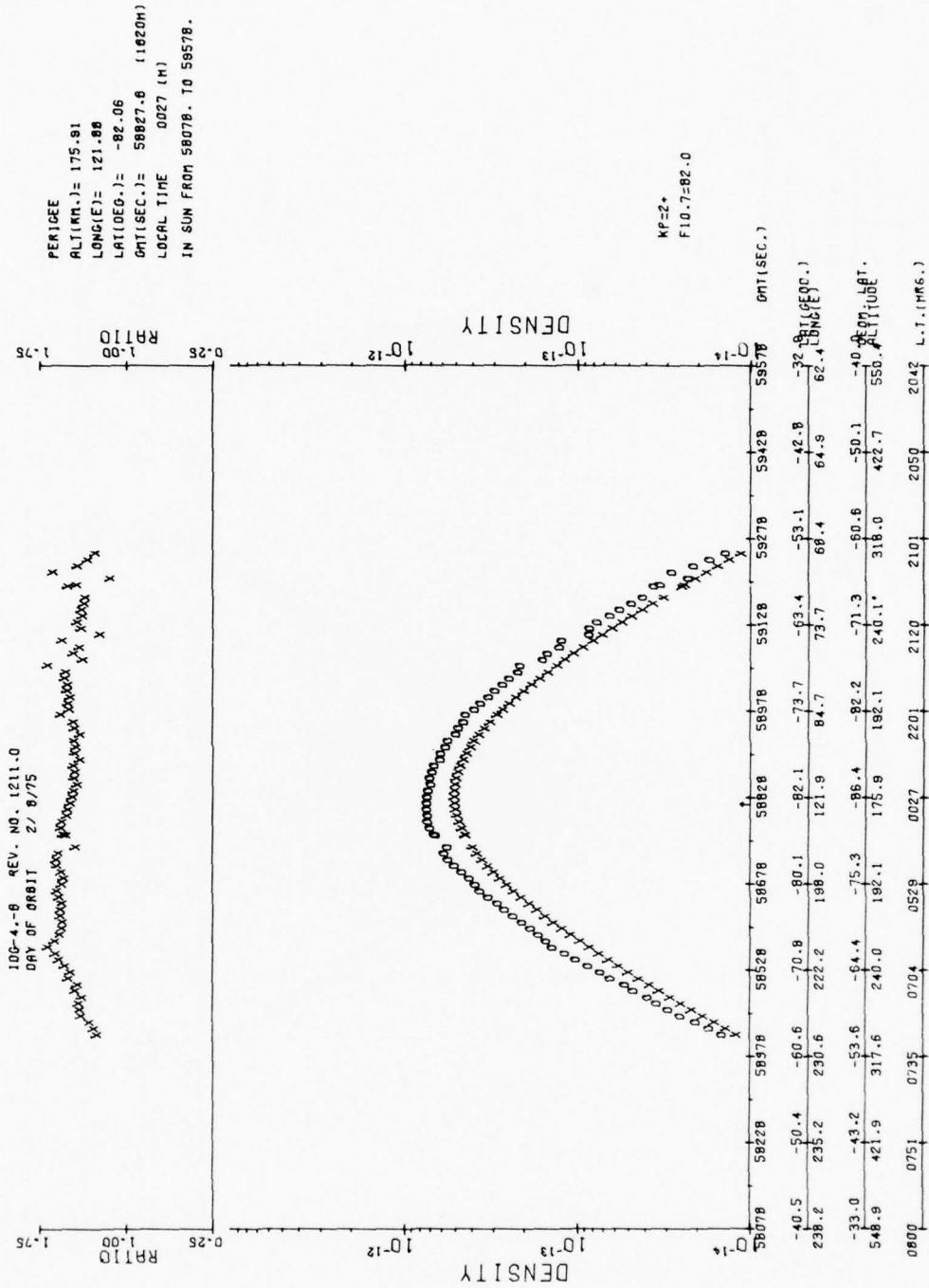
100-4-6 REV. NO. 1171-0
DAY OF ORBIT 2/ 5/76

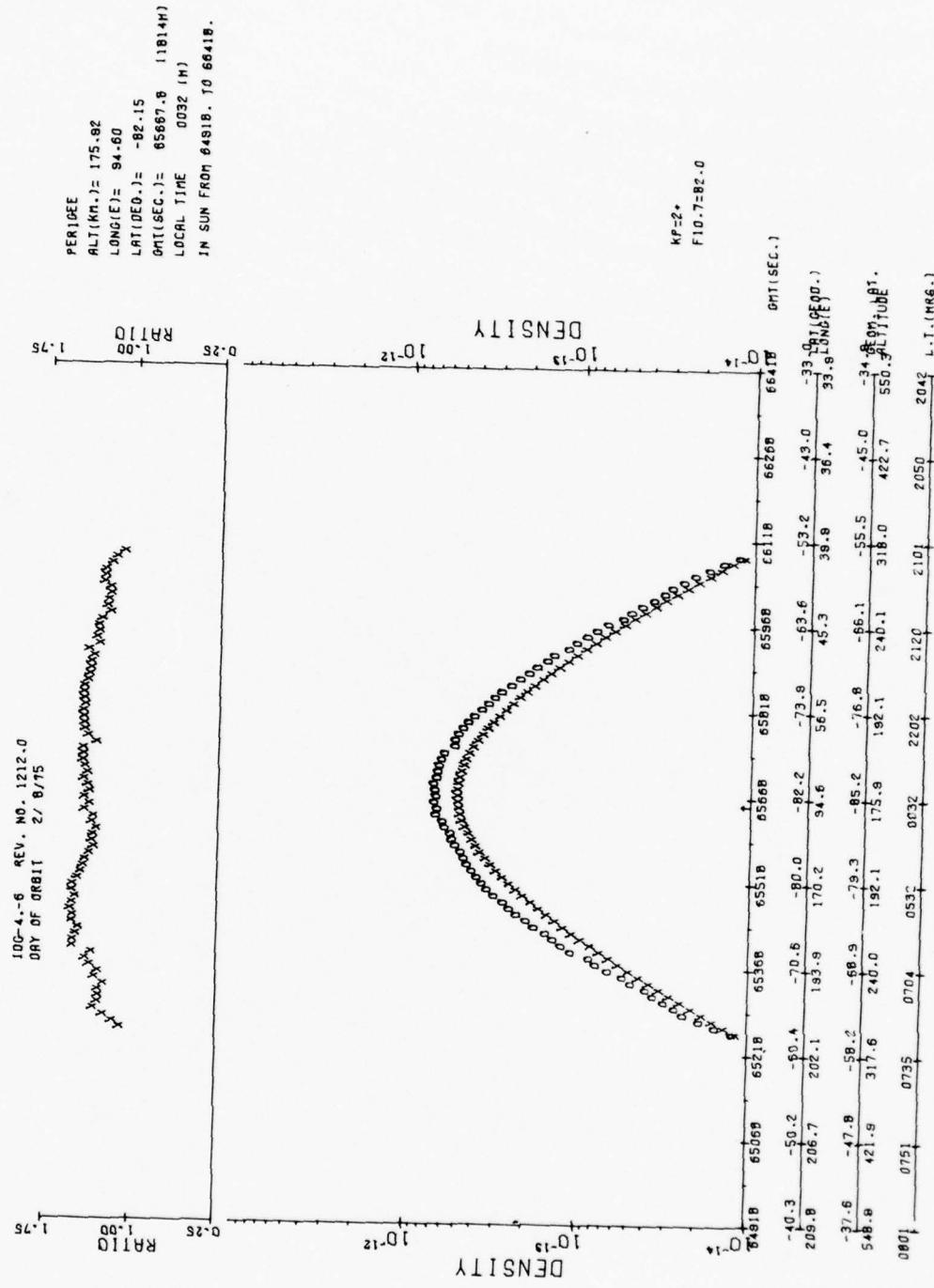


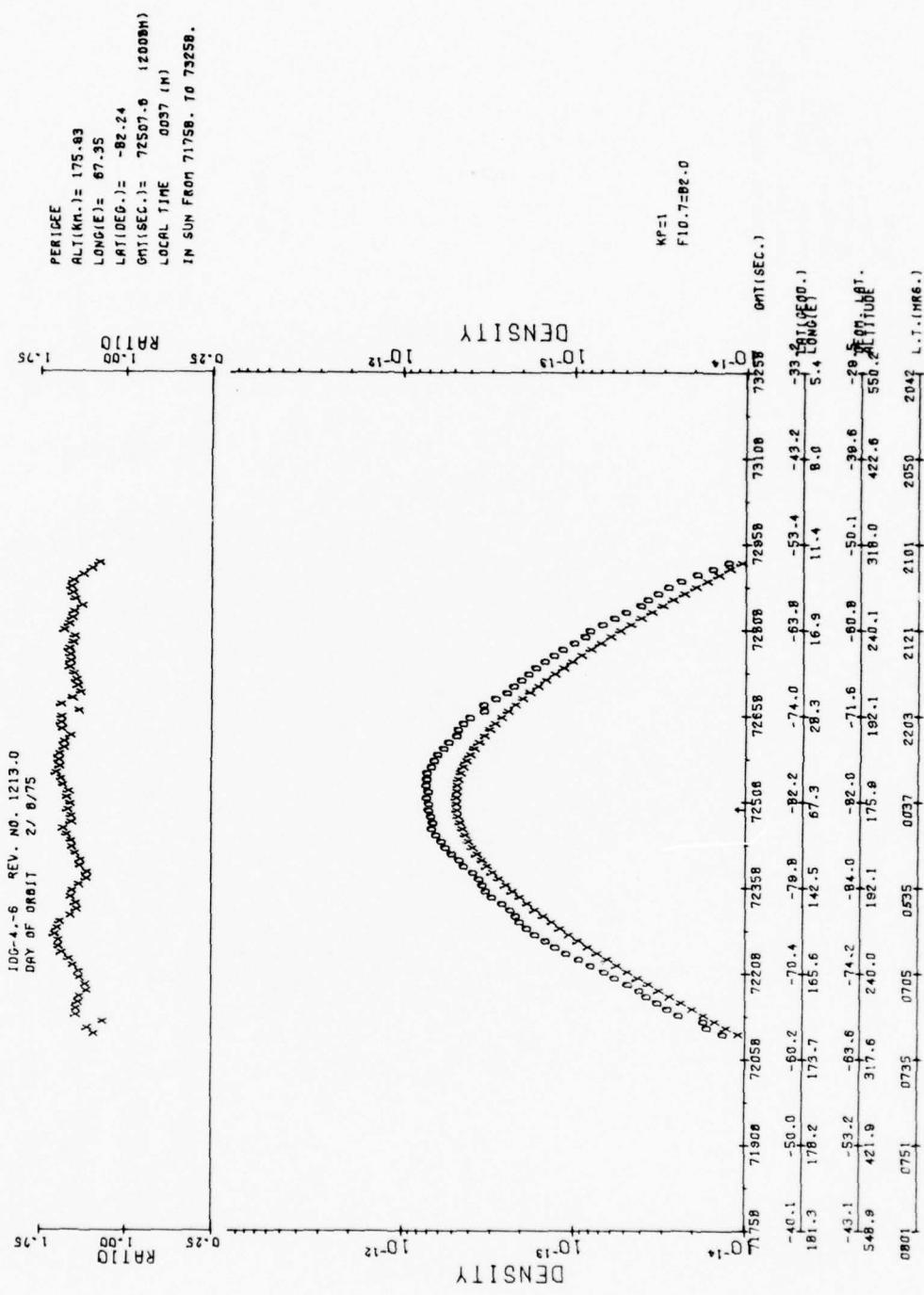


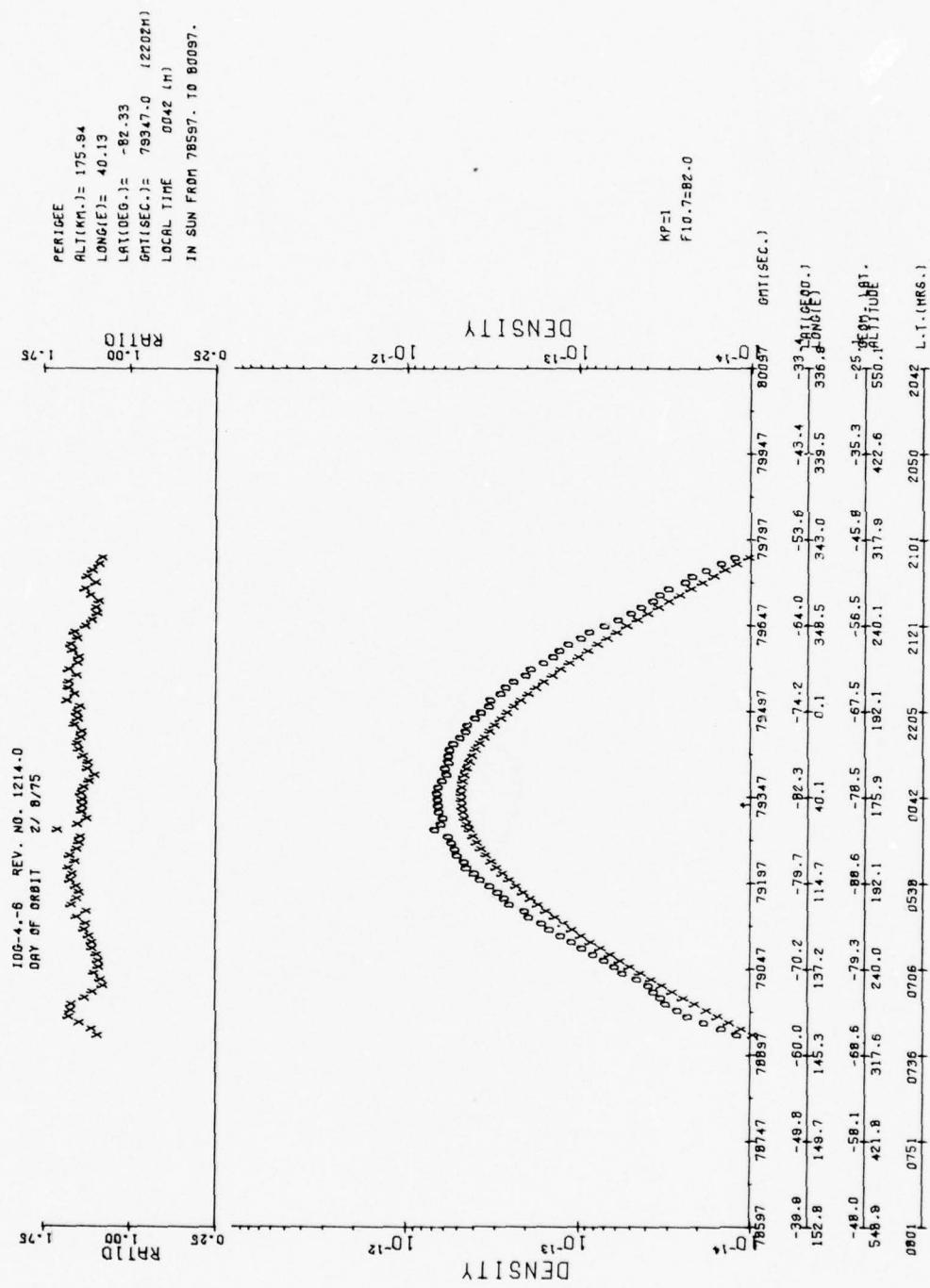


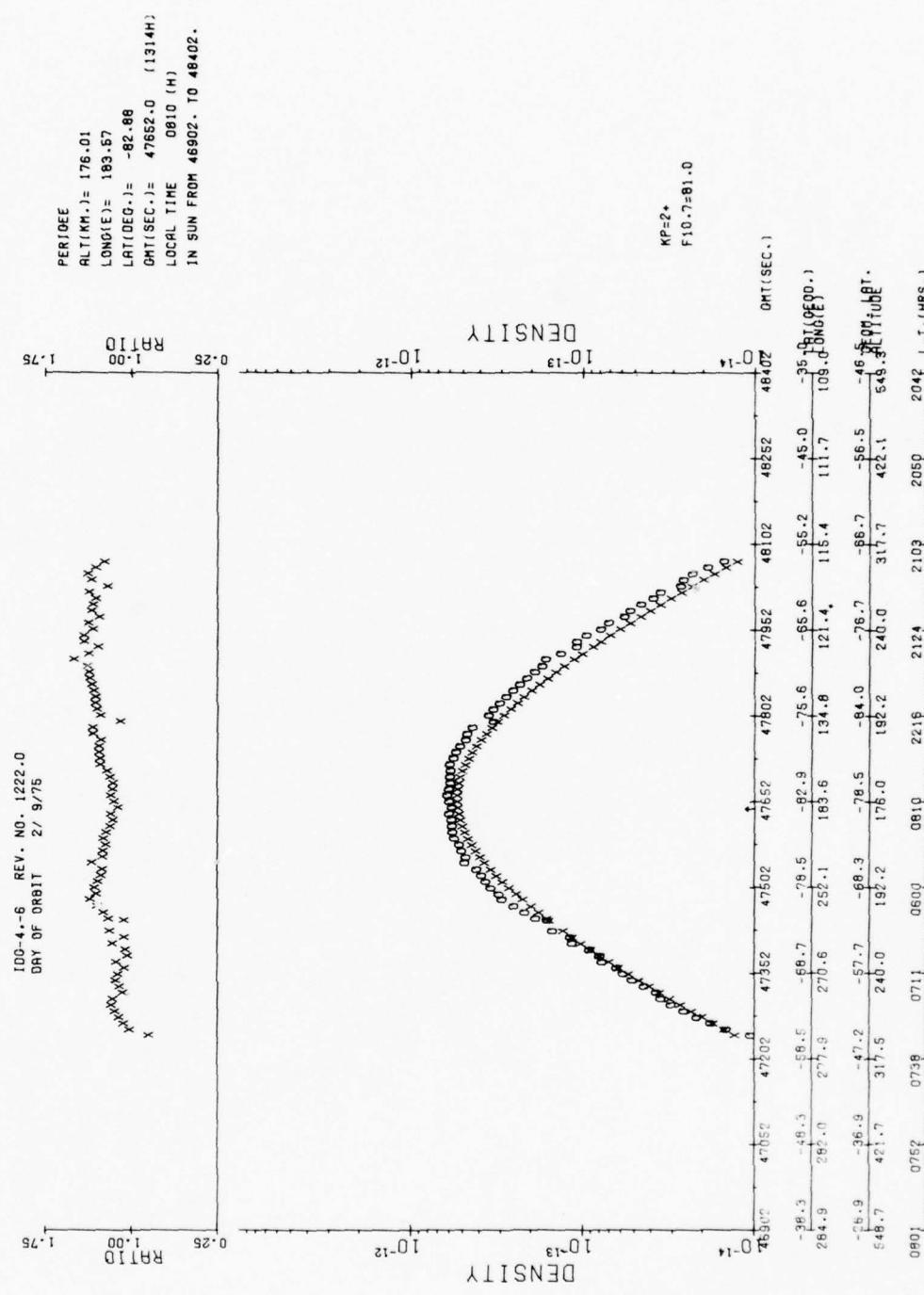


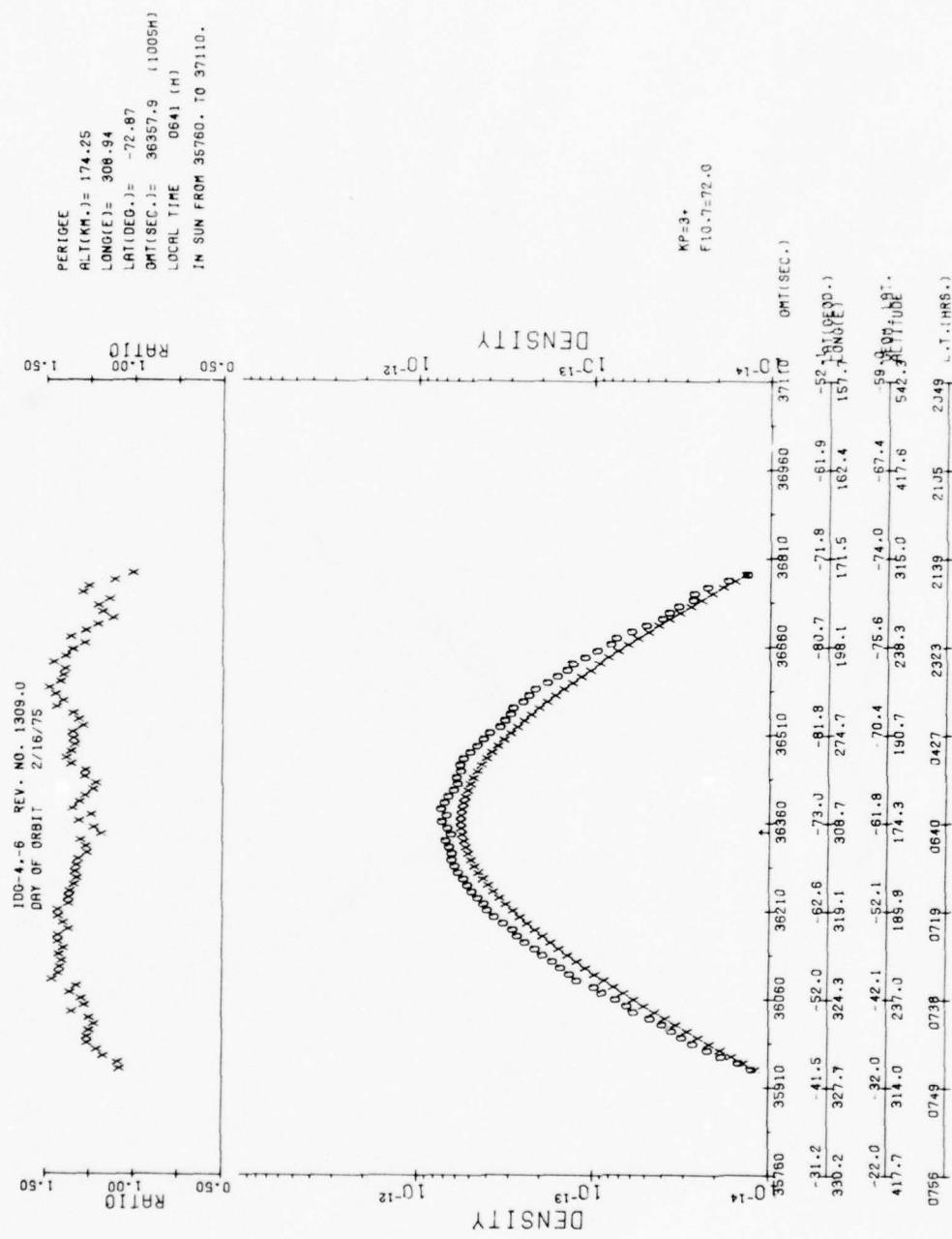


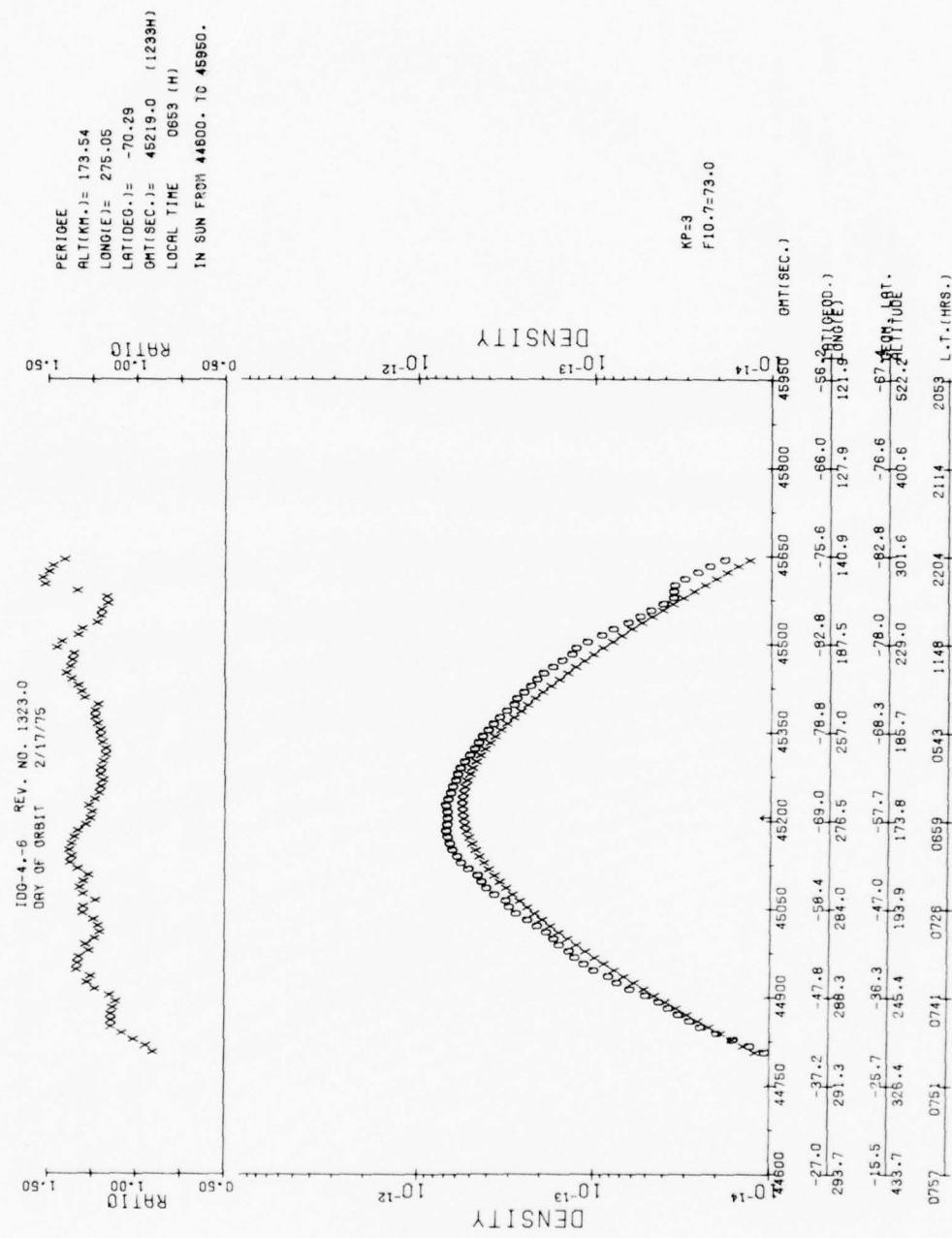


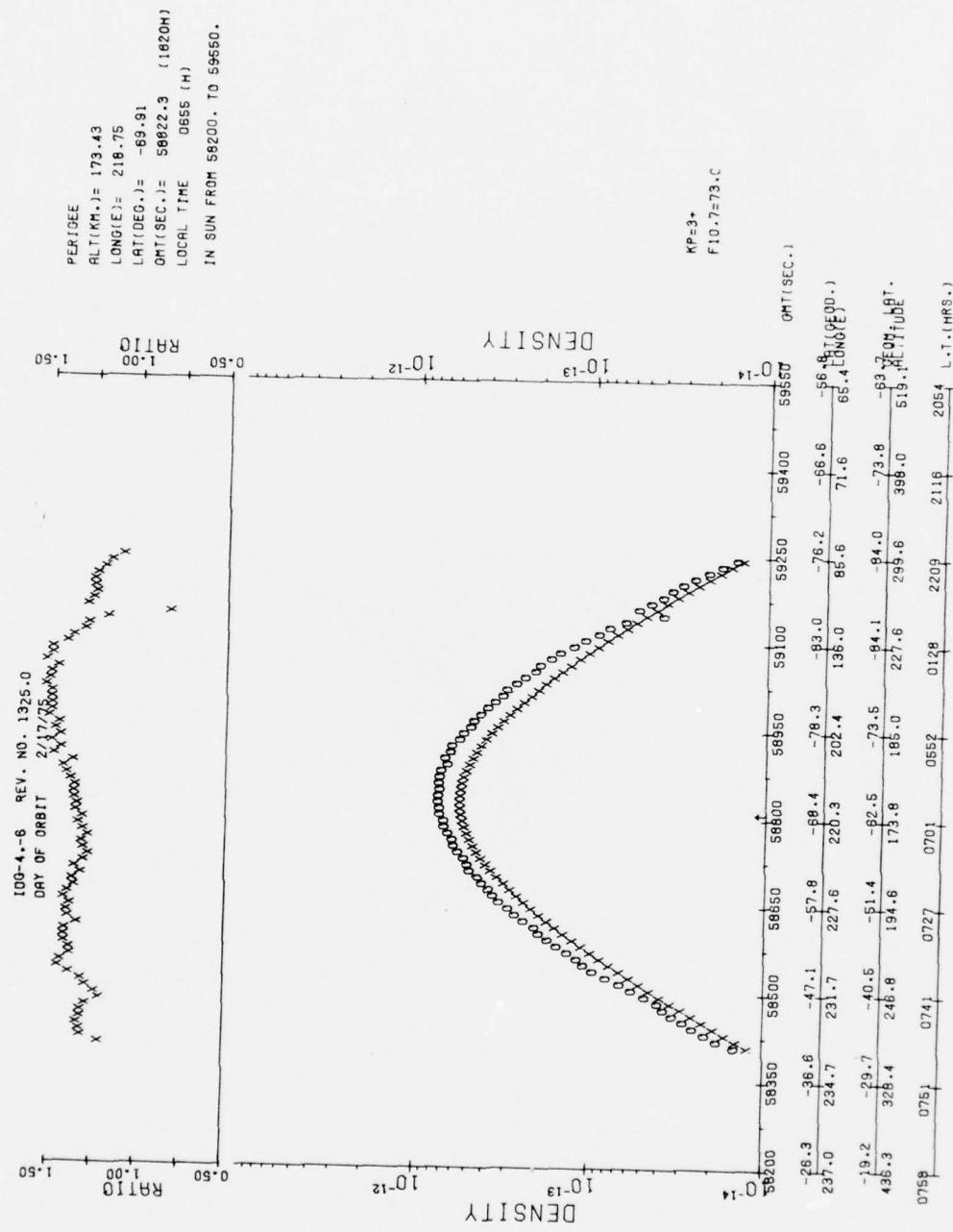


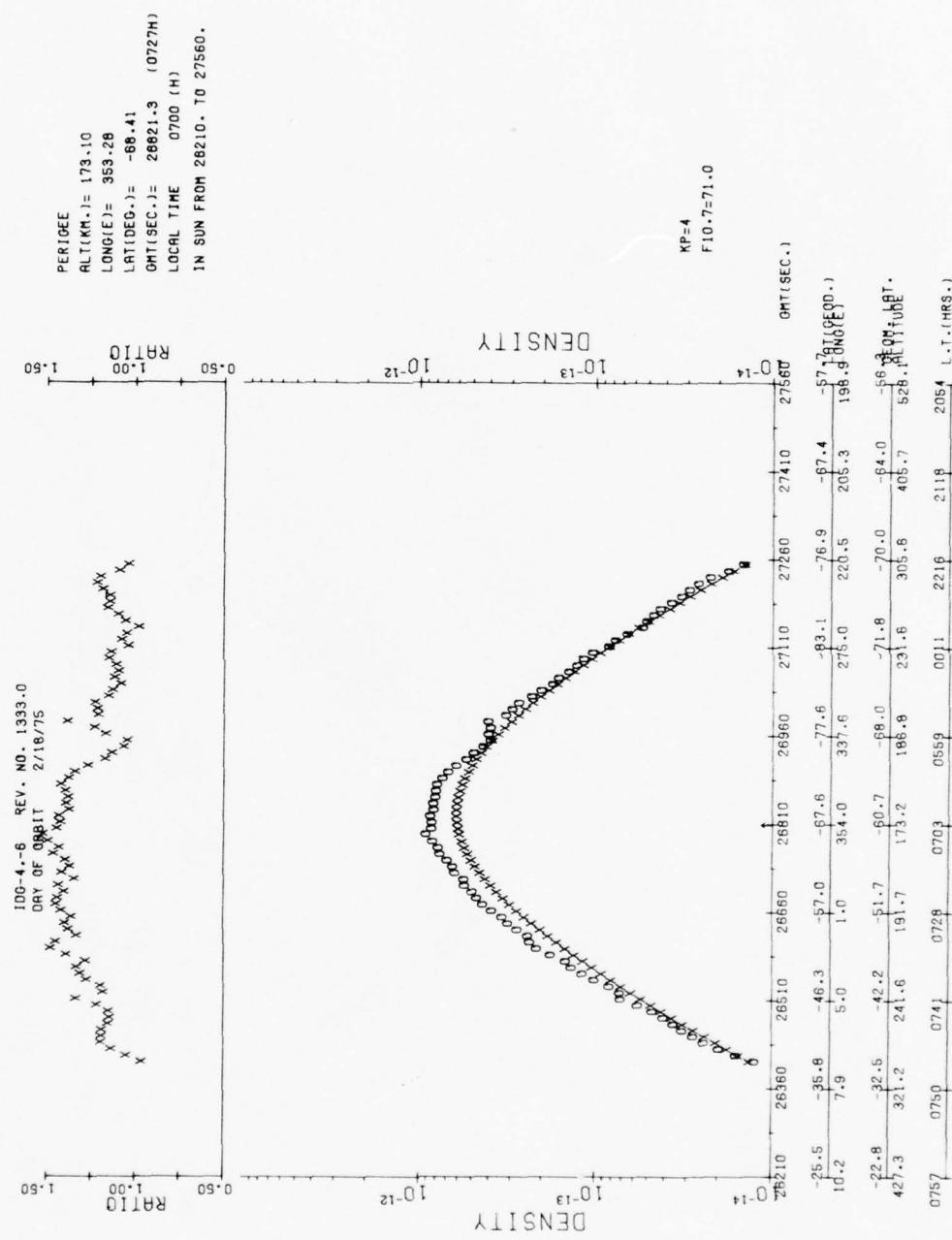


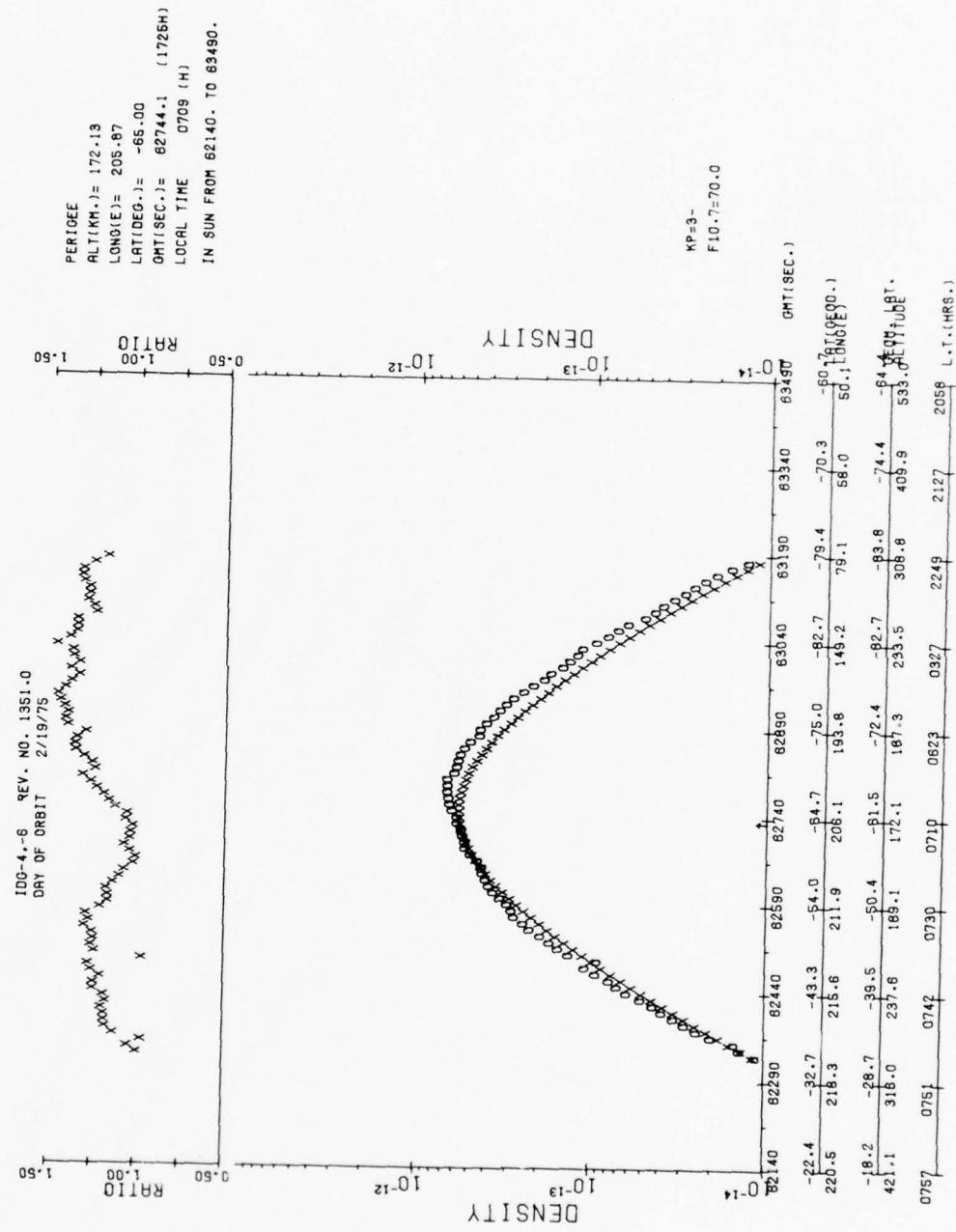


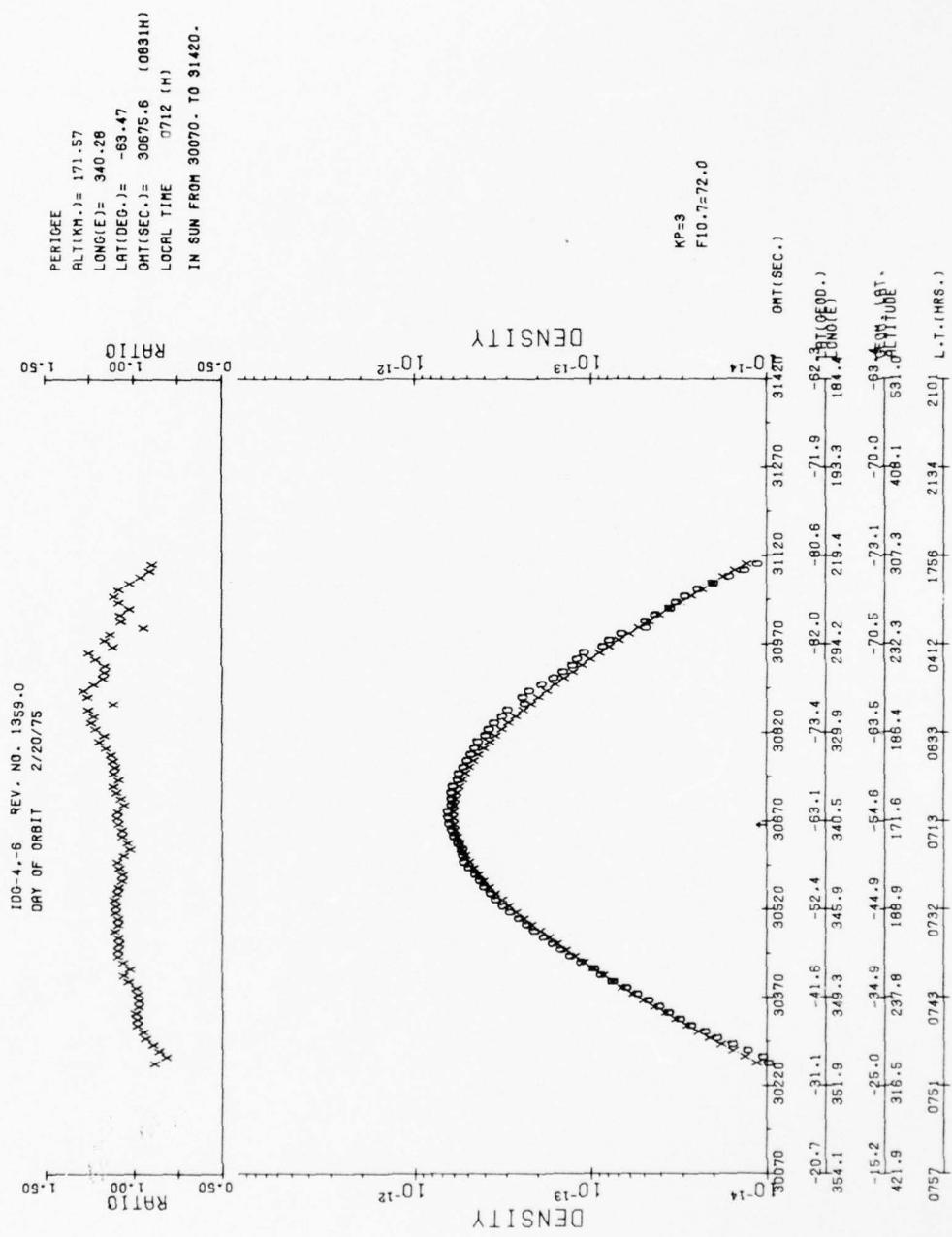


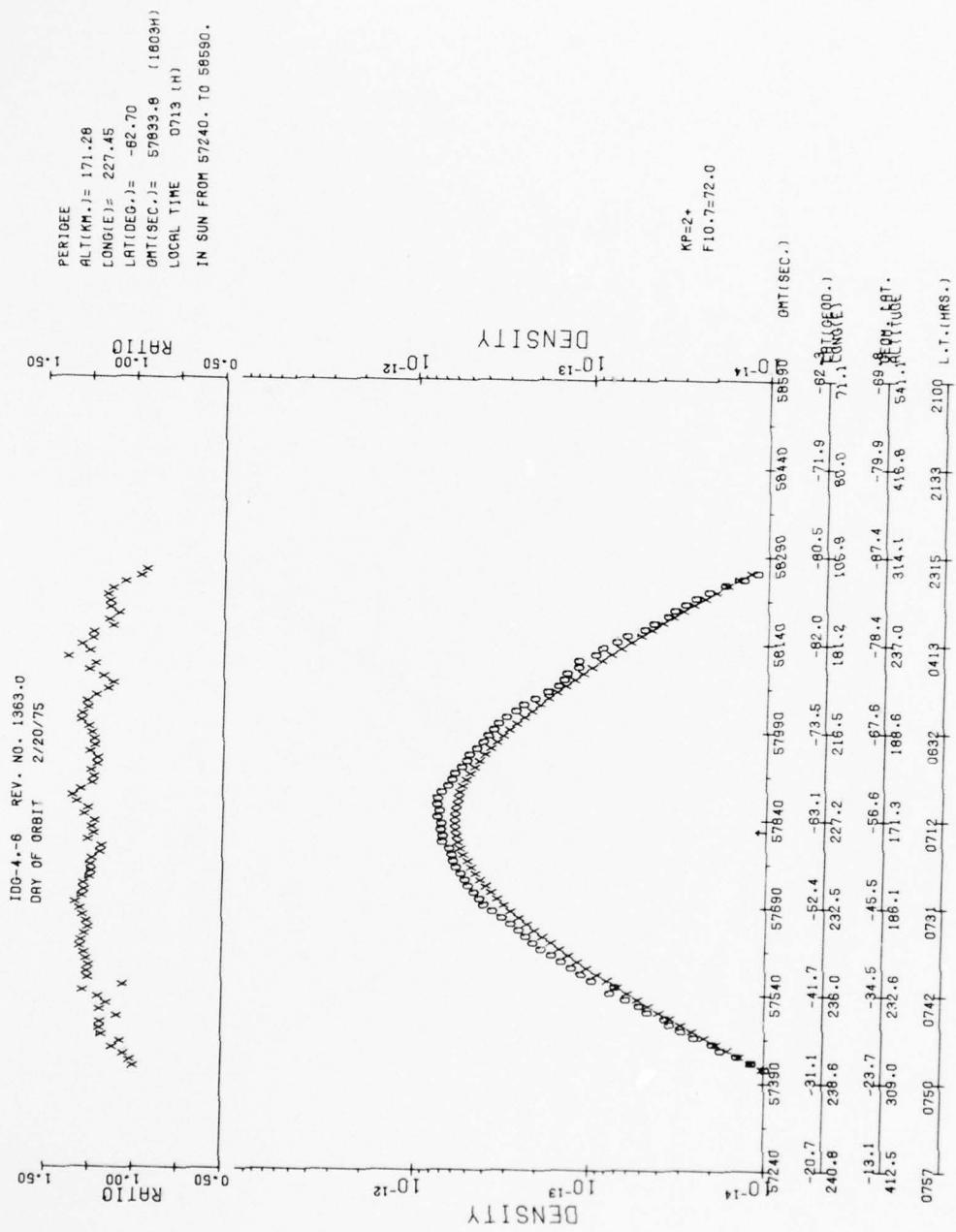






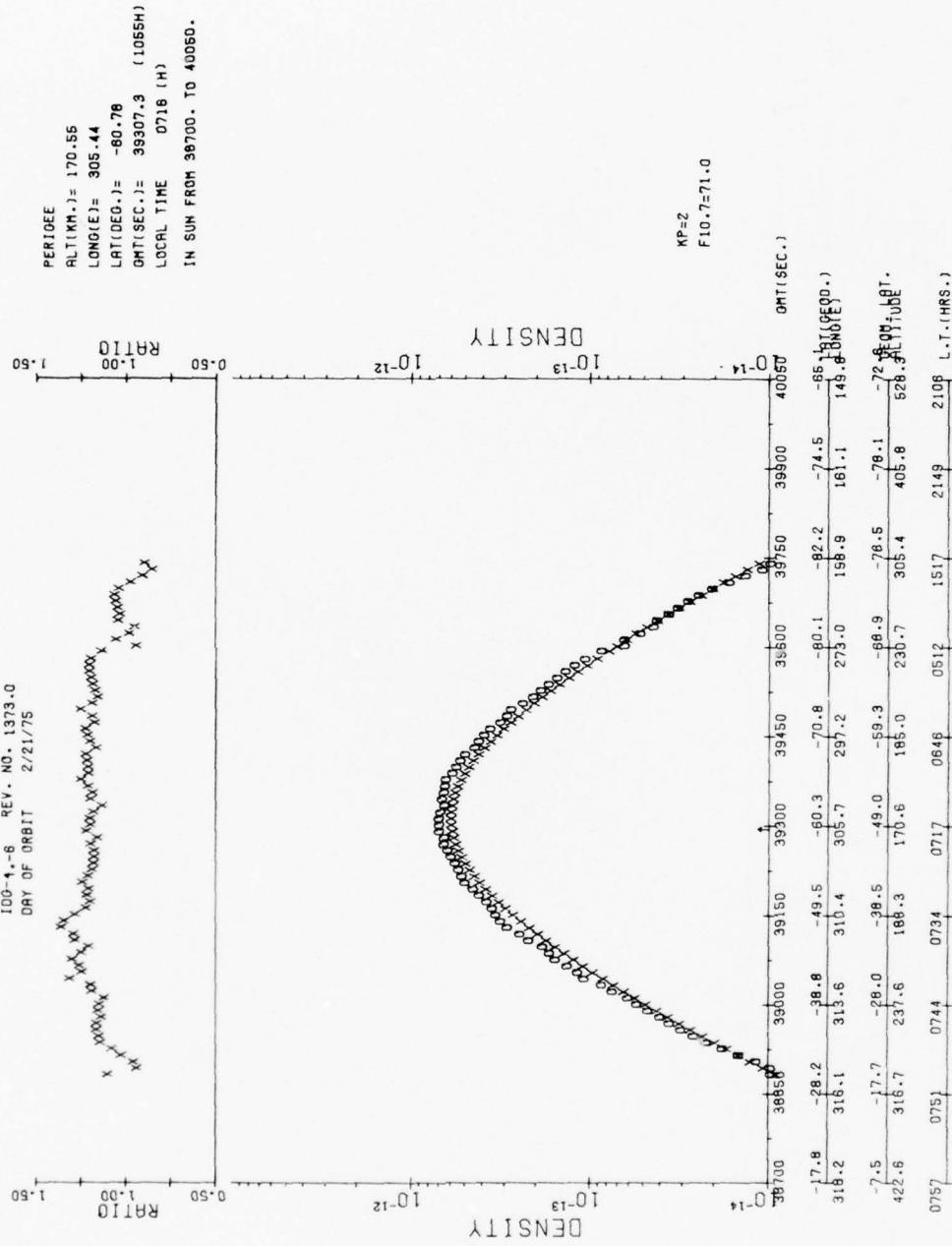


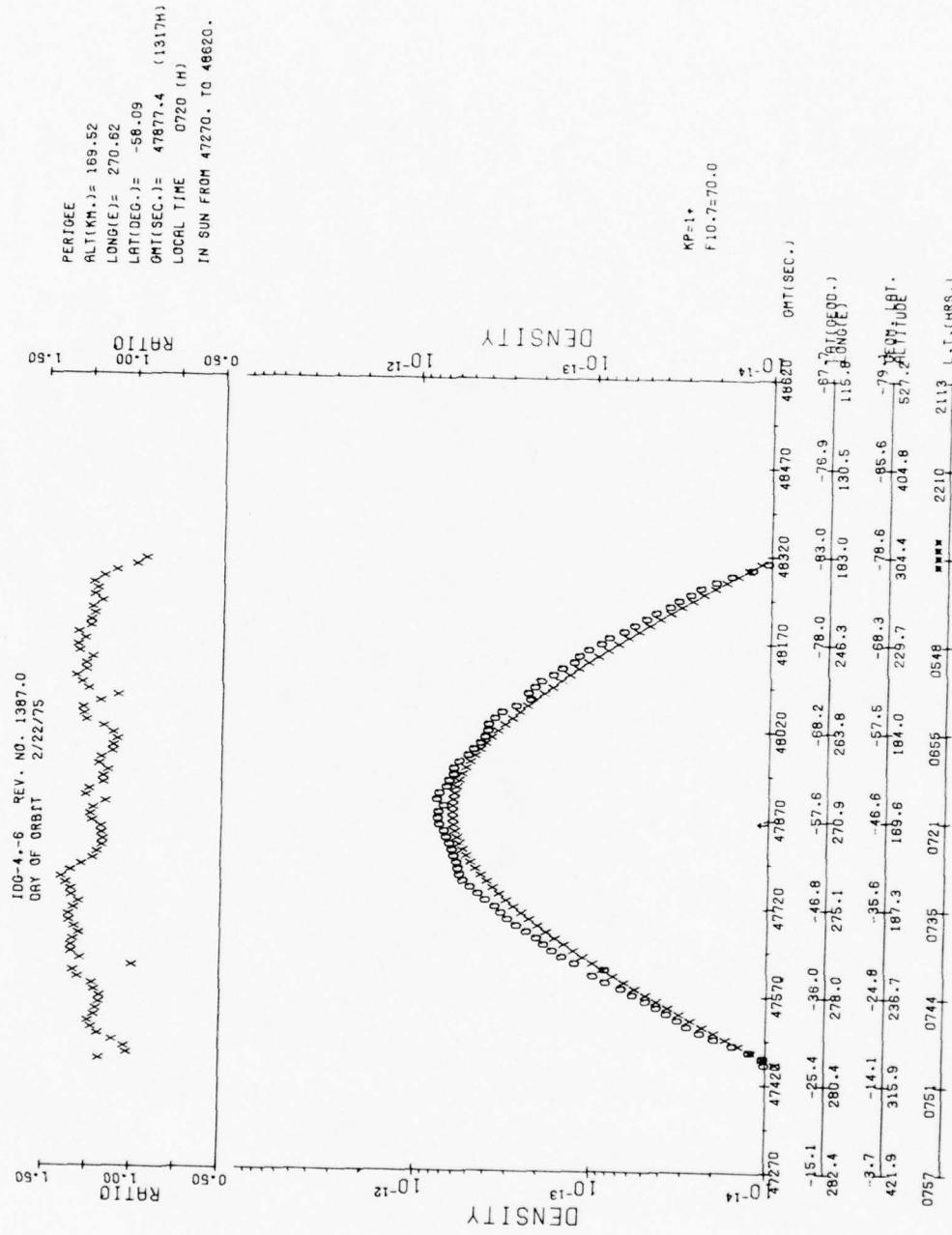


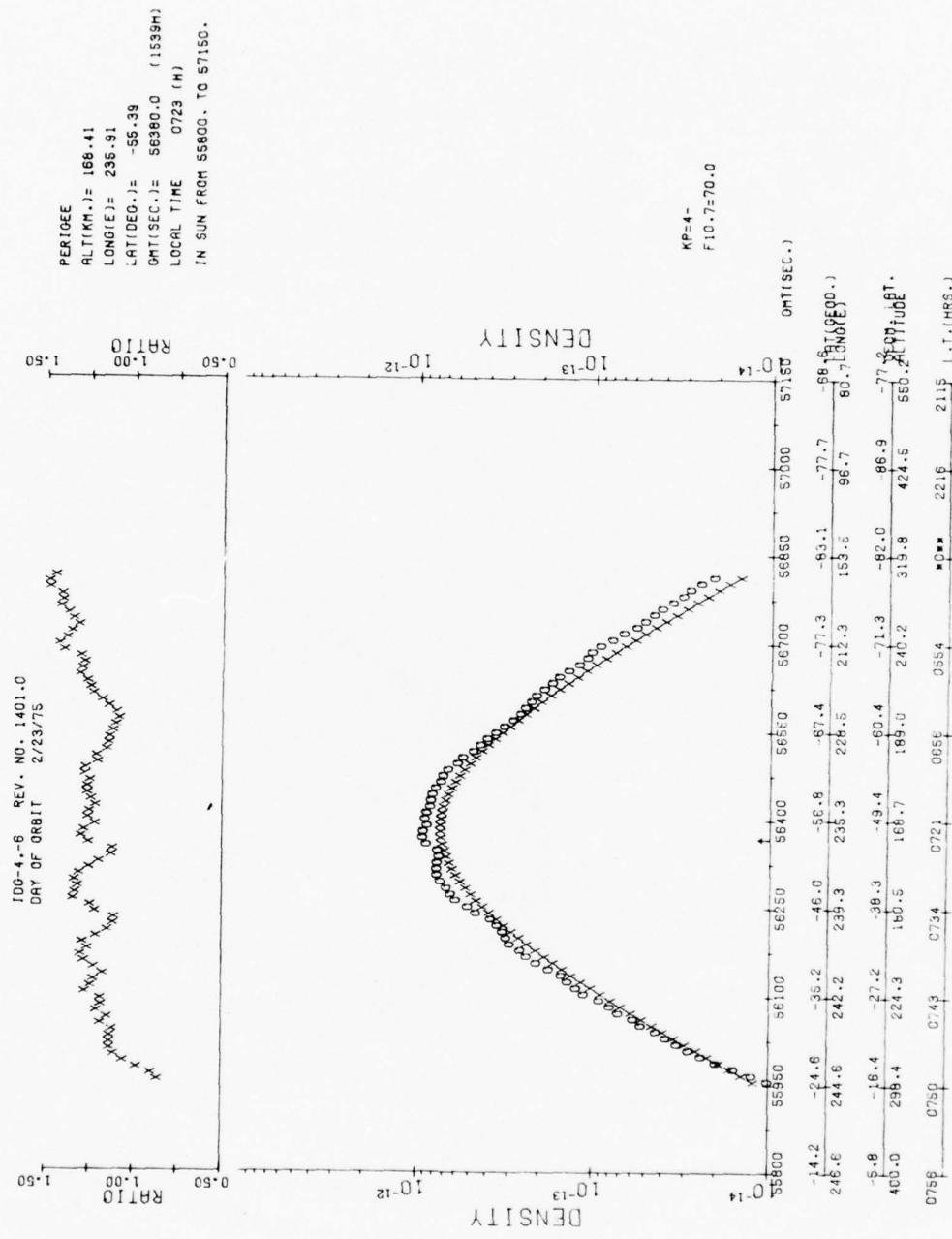


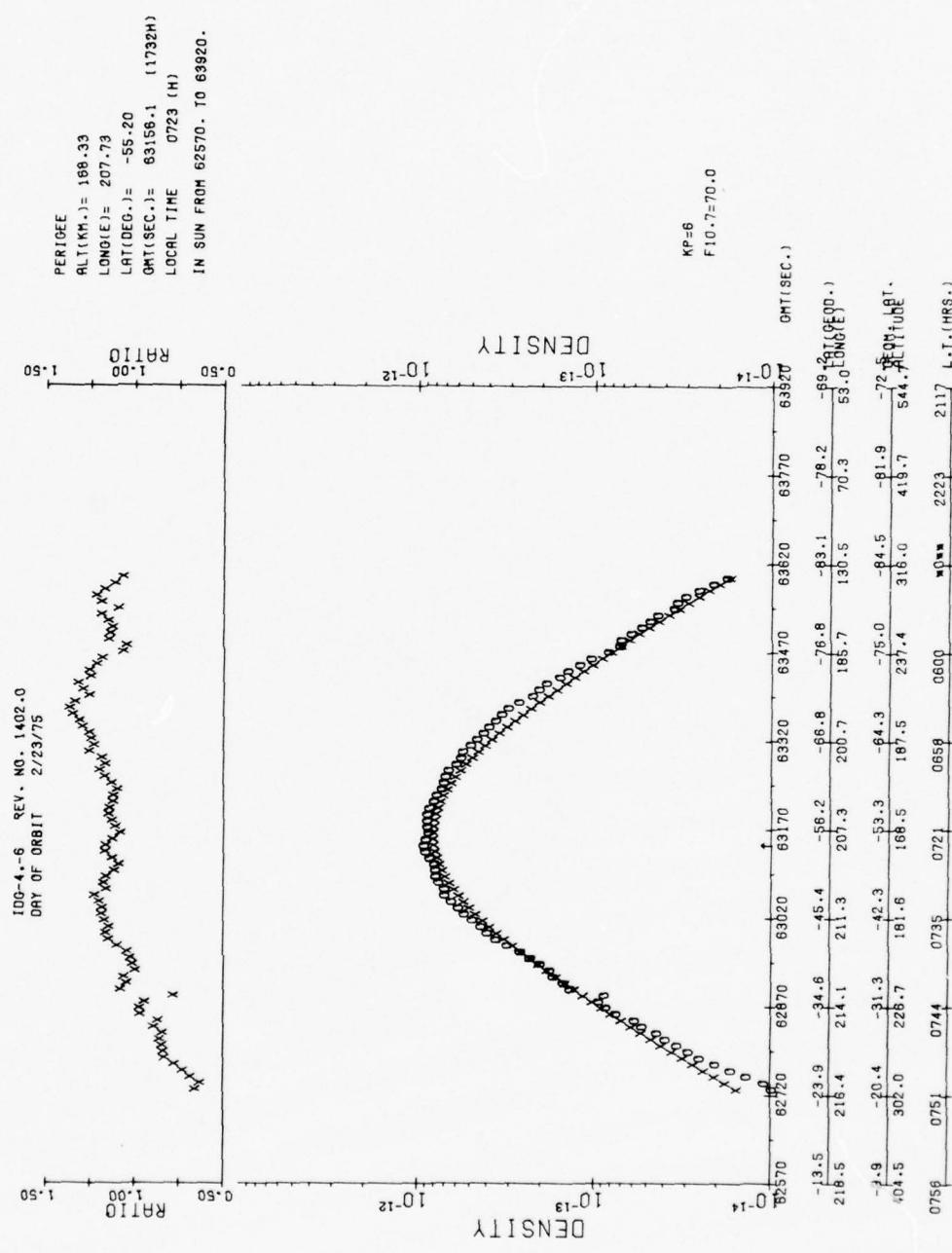
100-1.-6 REV. NO. 1373.0
DAY OF ORBIT 2/21/75

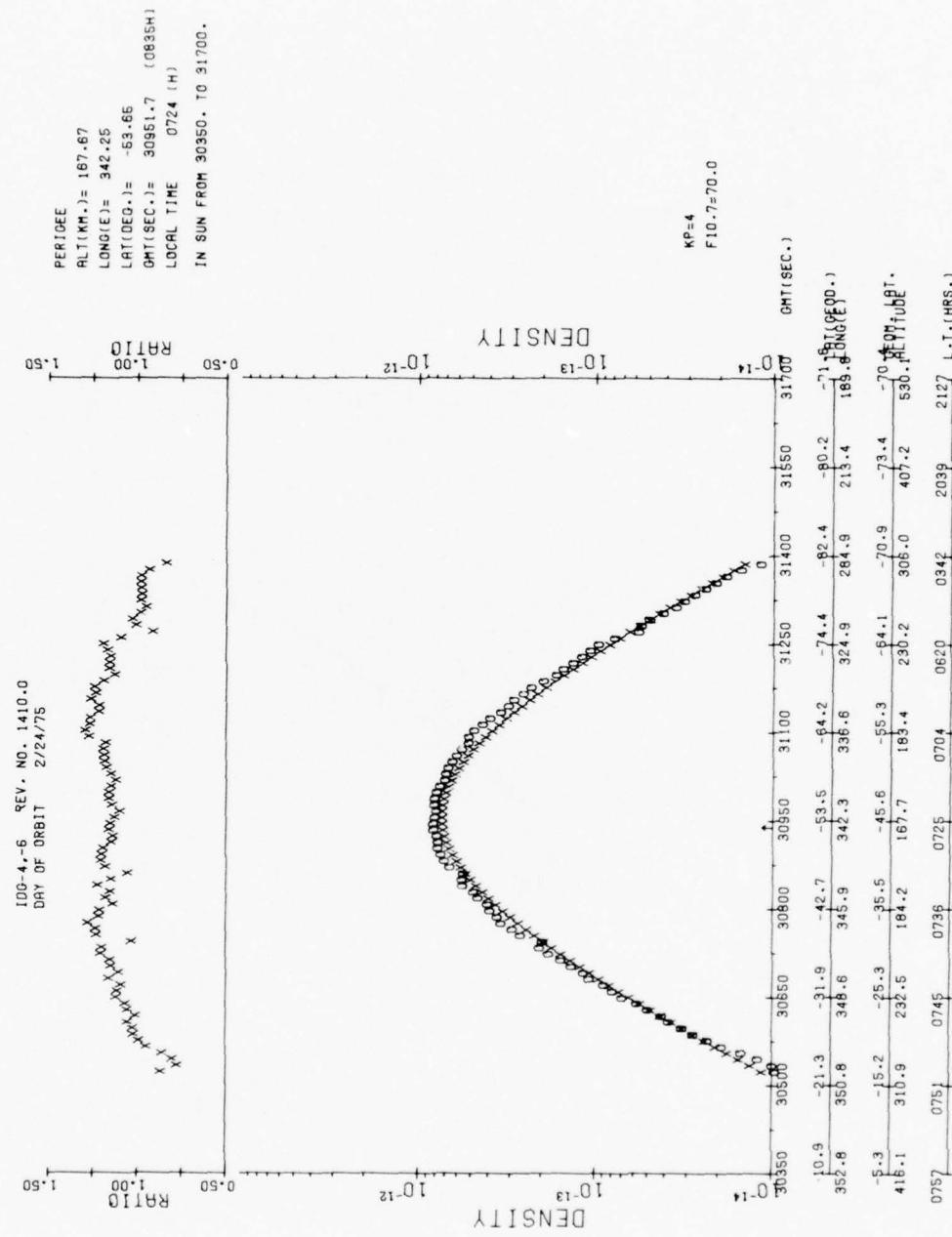
DAY OF ORBIT 2/21/75

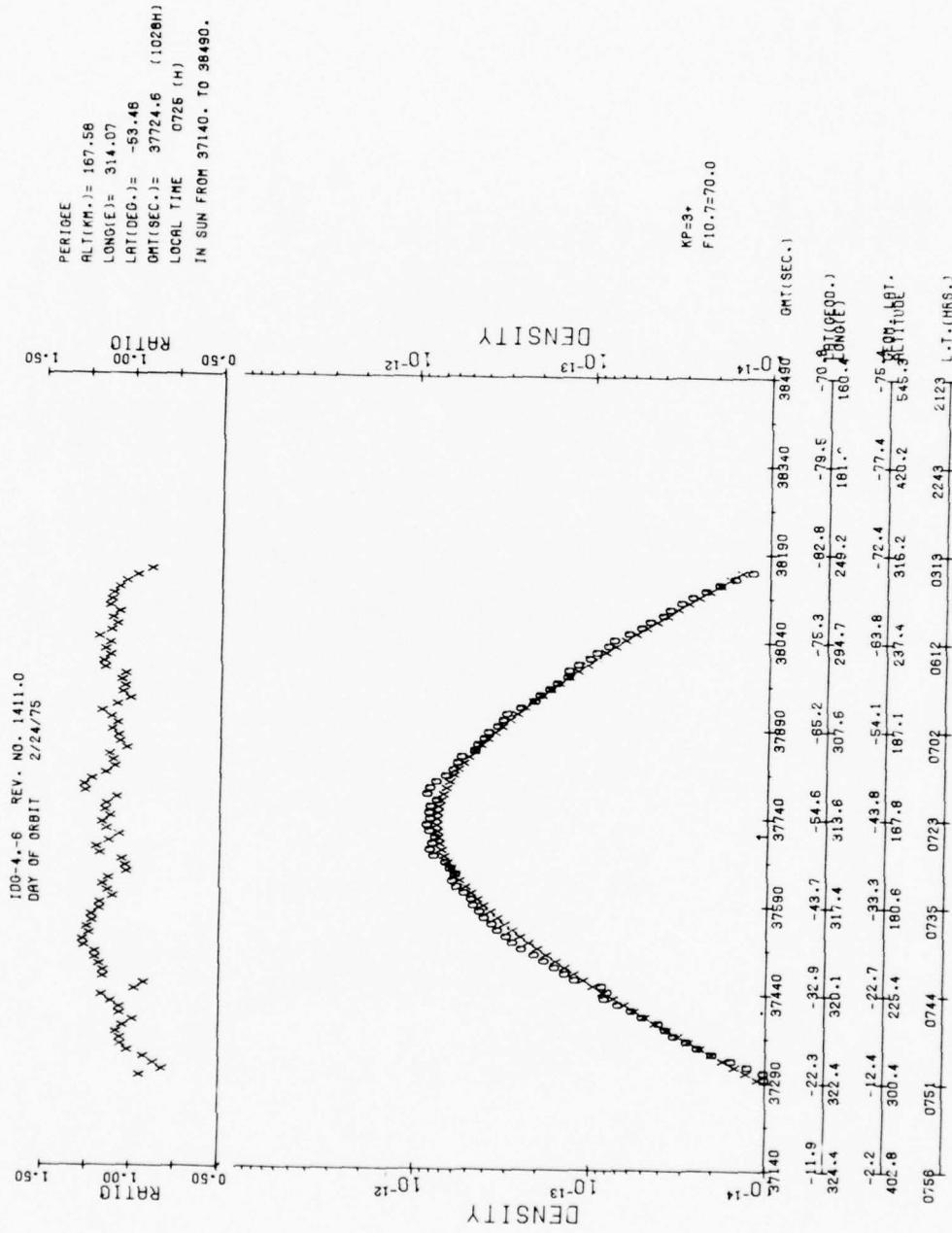


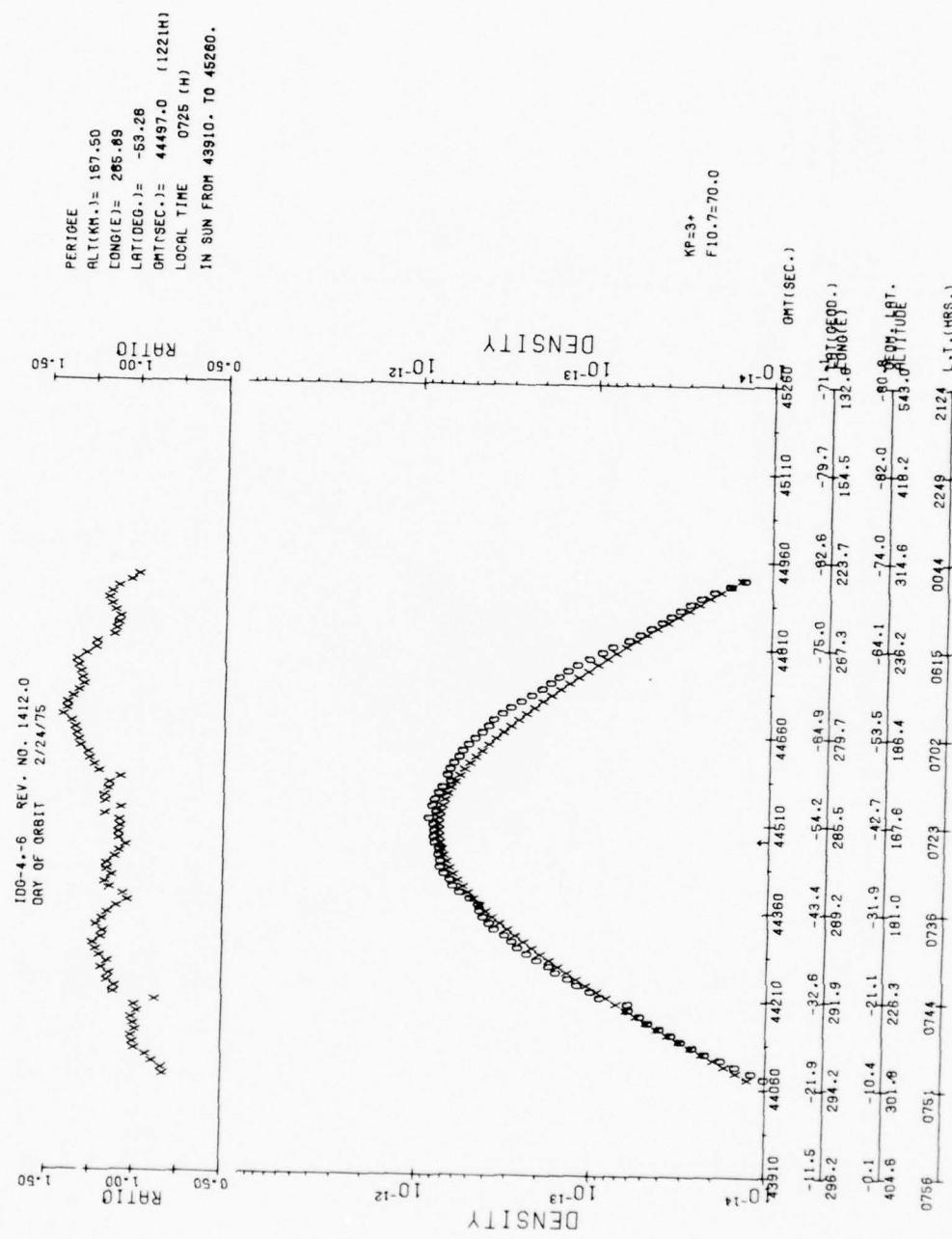




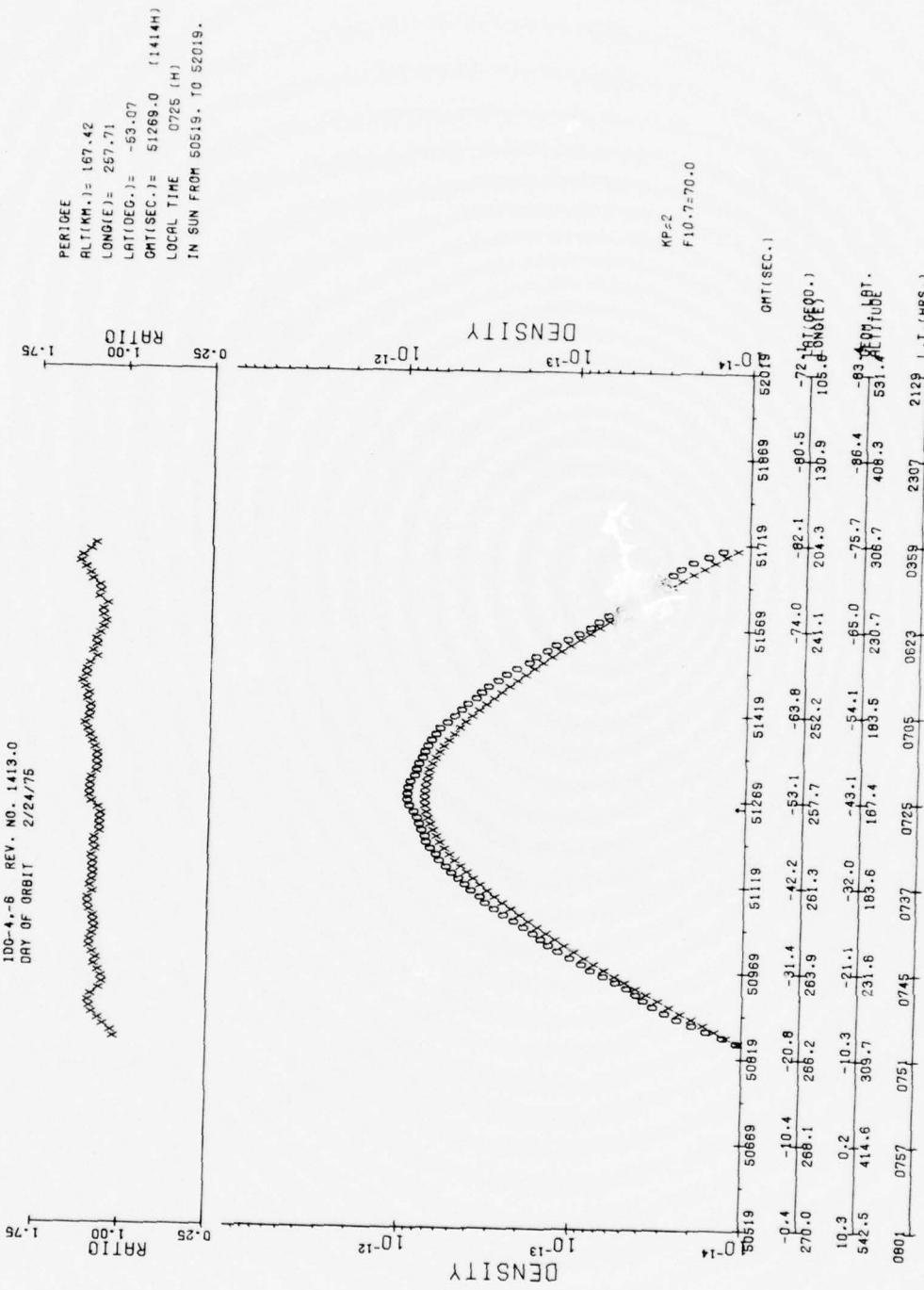


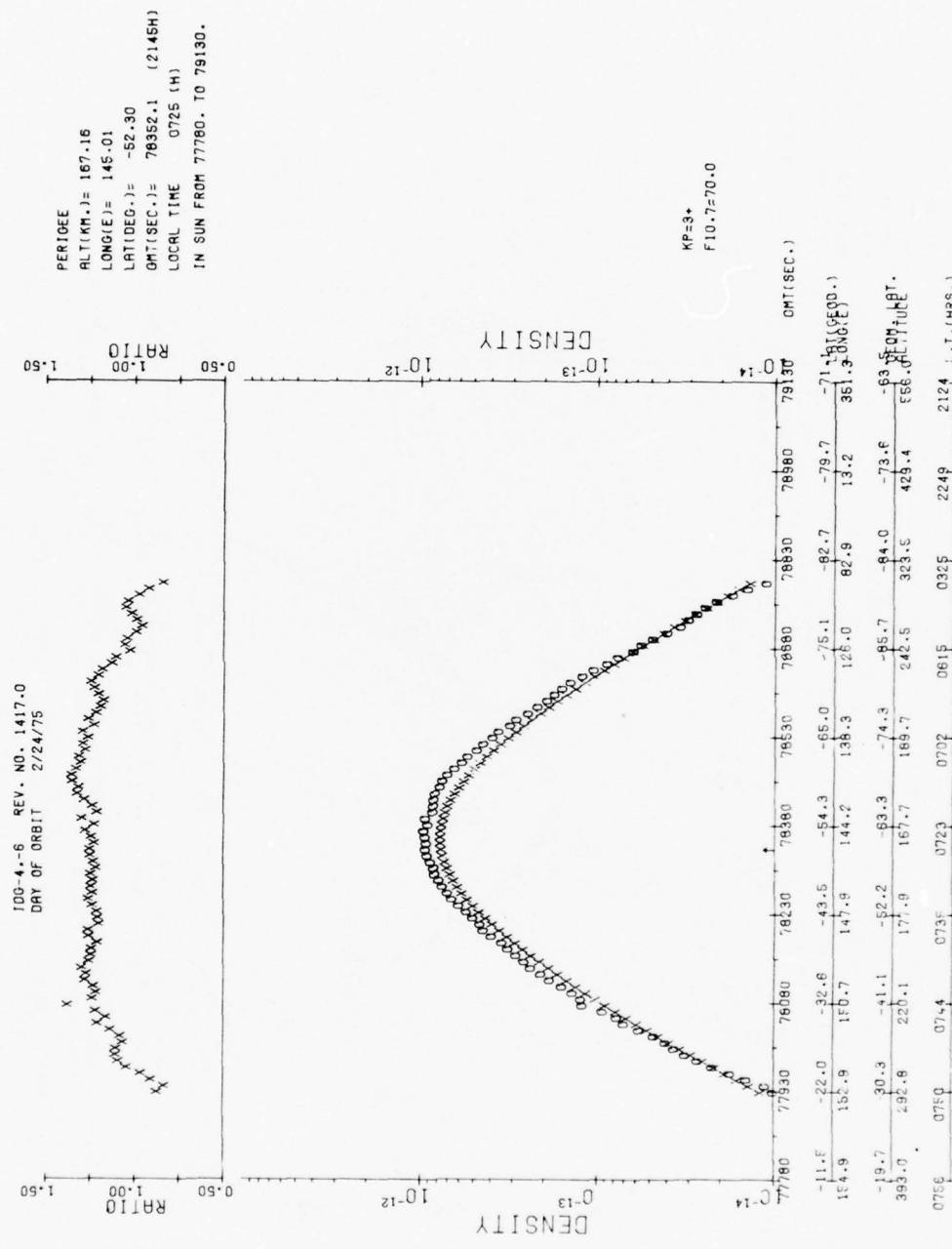


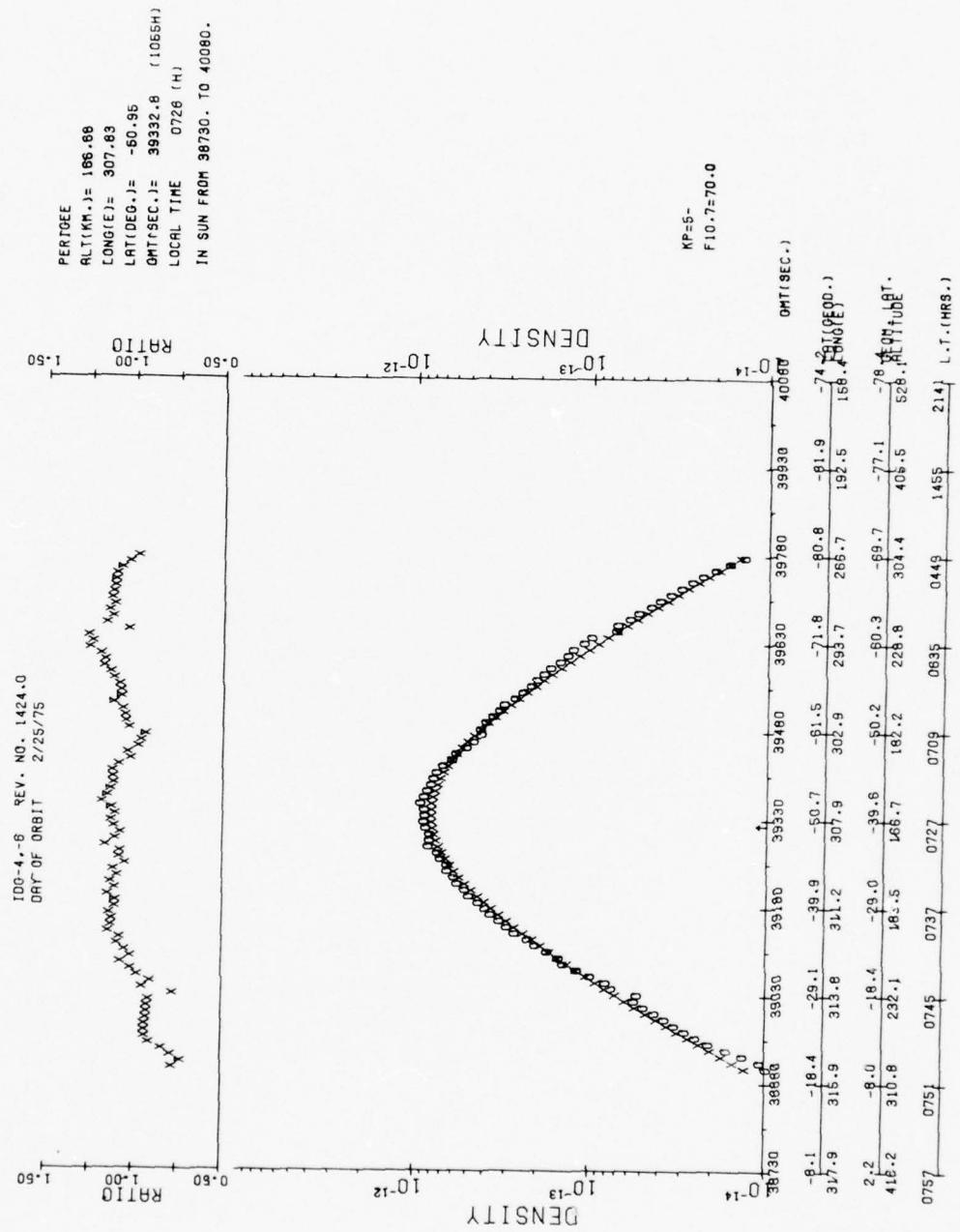


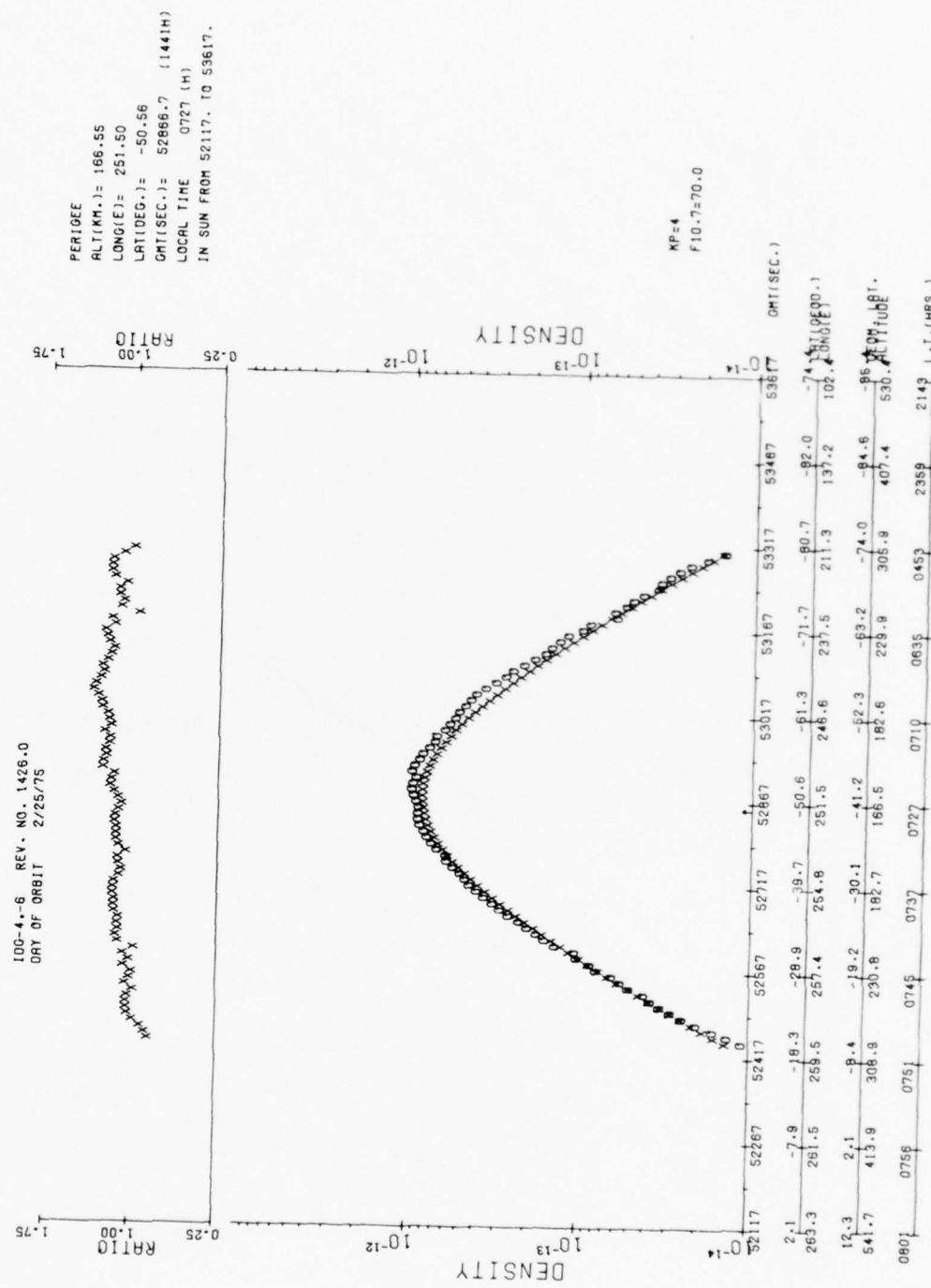


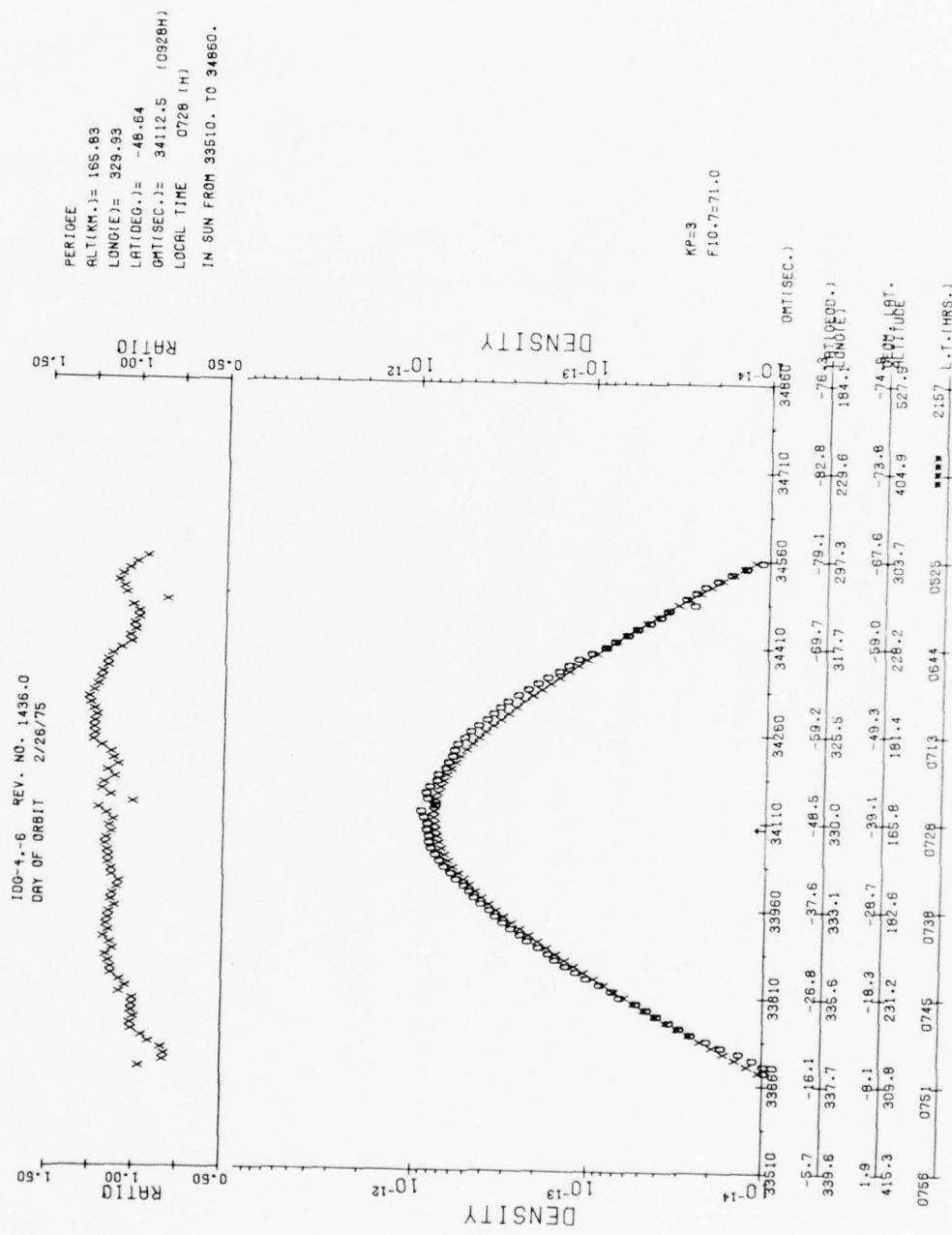
100-4-B REV. NO. 1413.0
DAY OF ORBIT 2/24/75

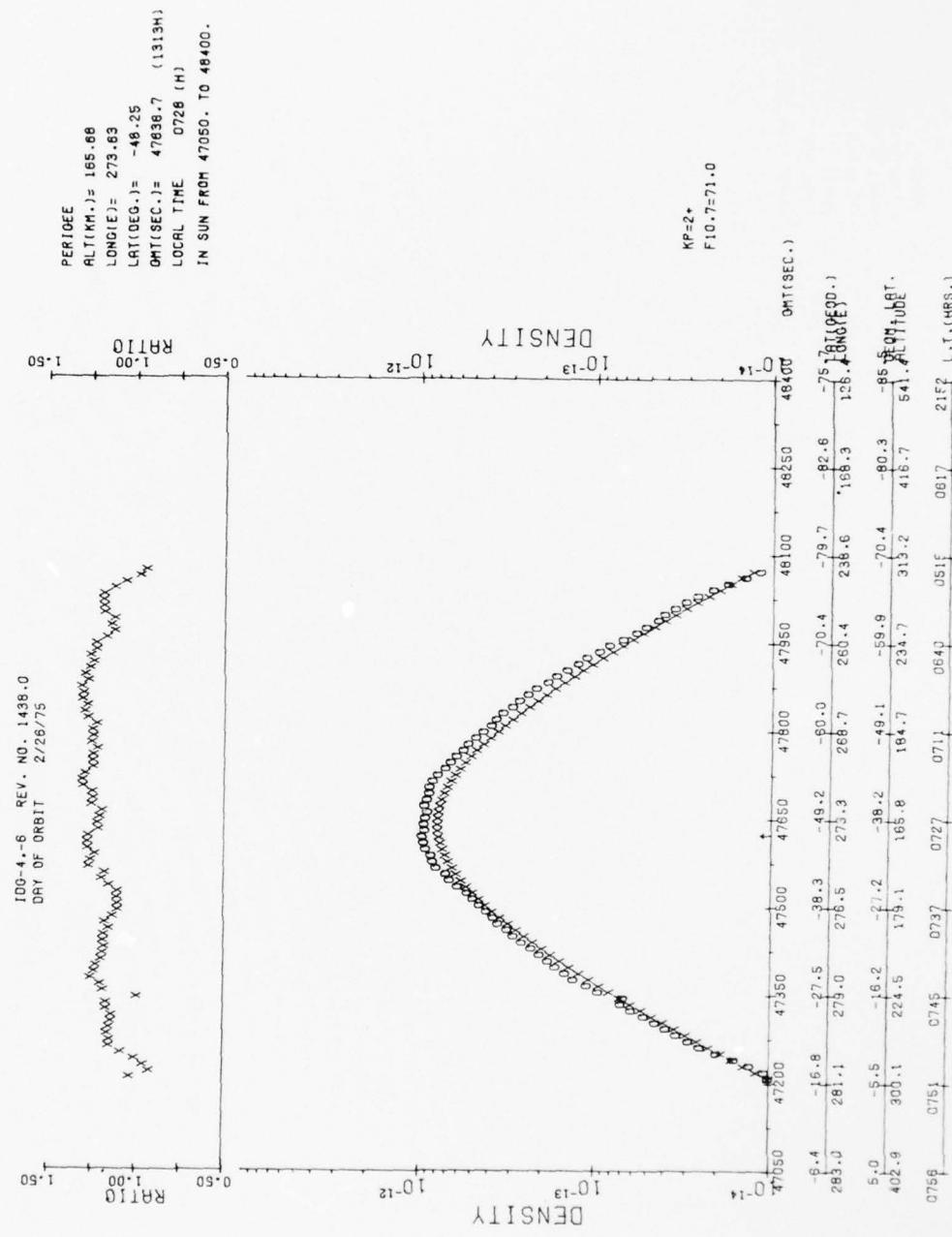


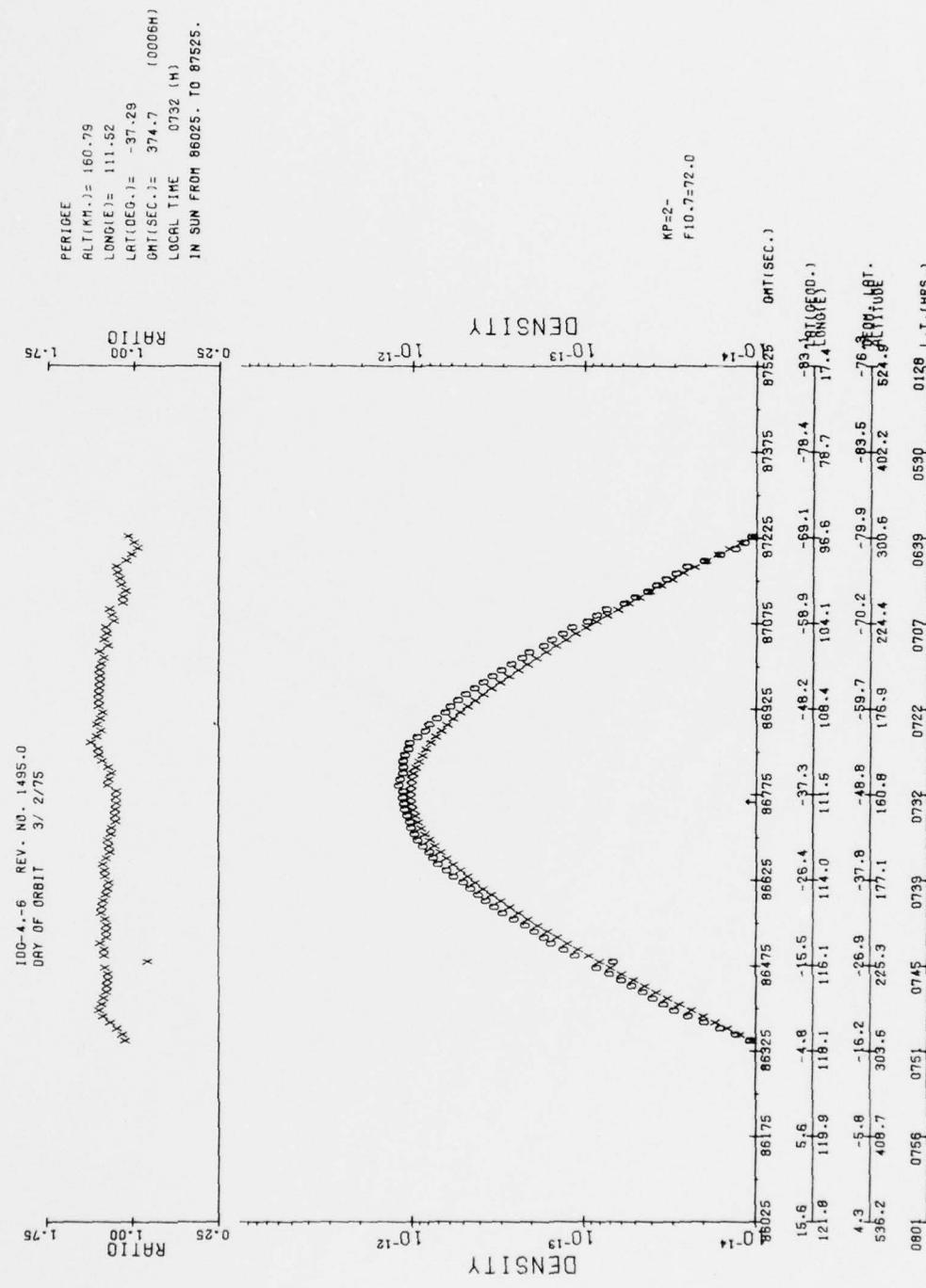


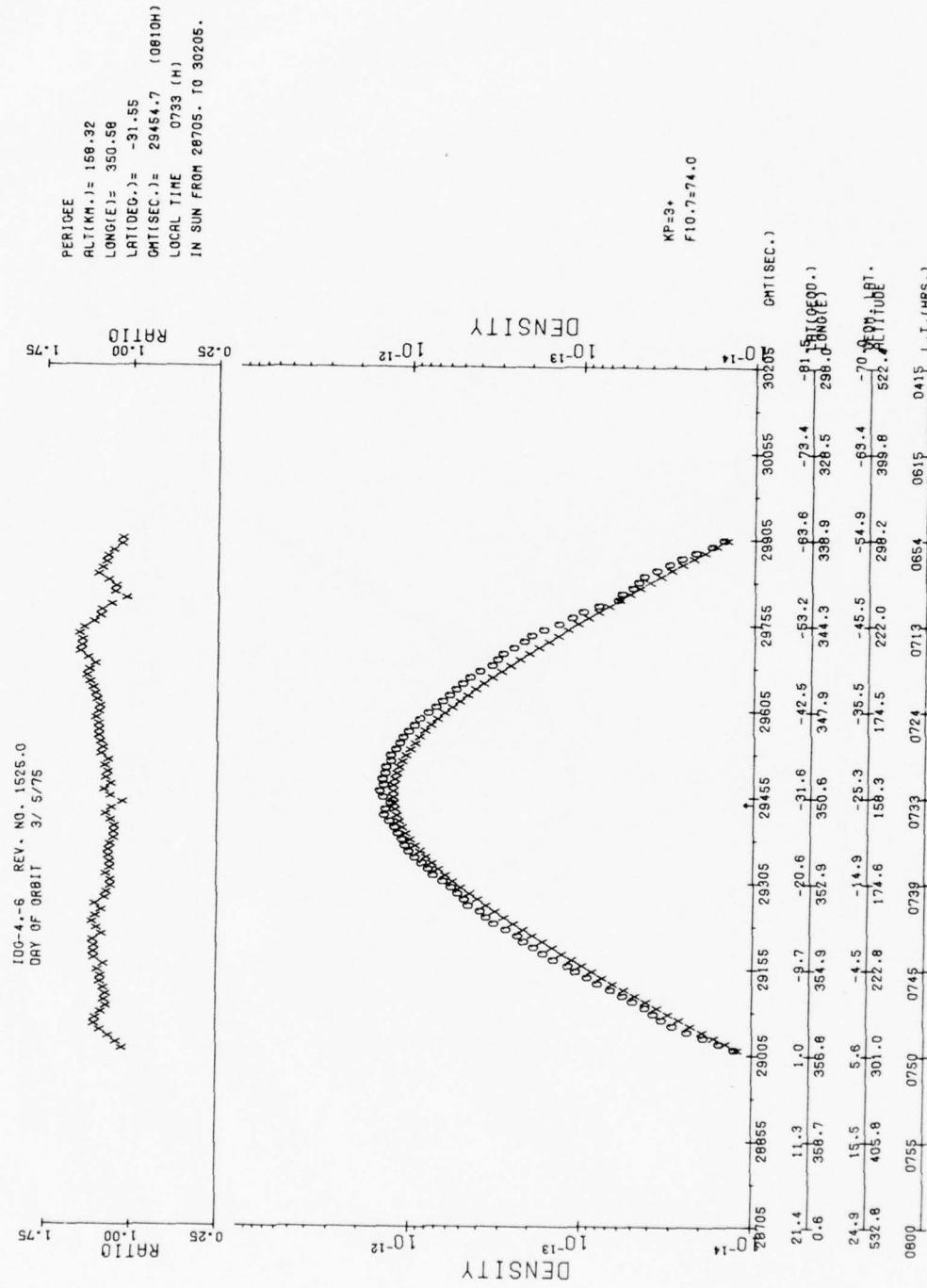


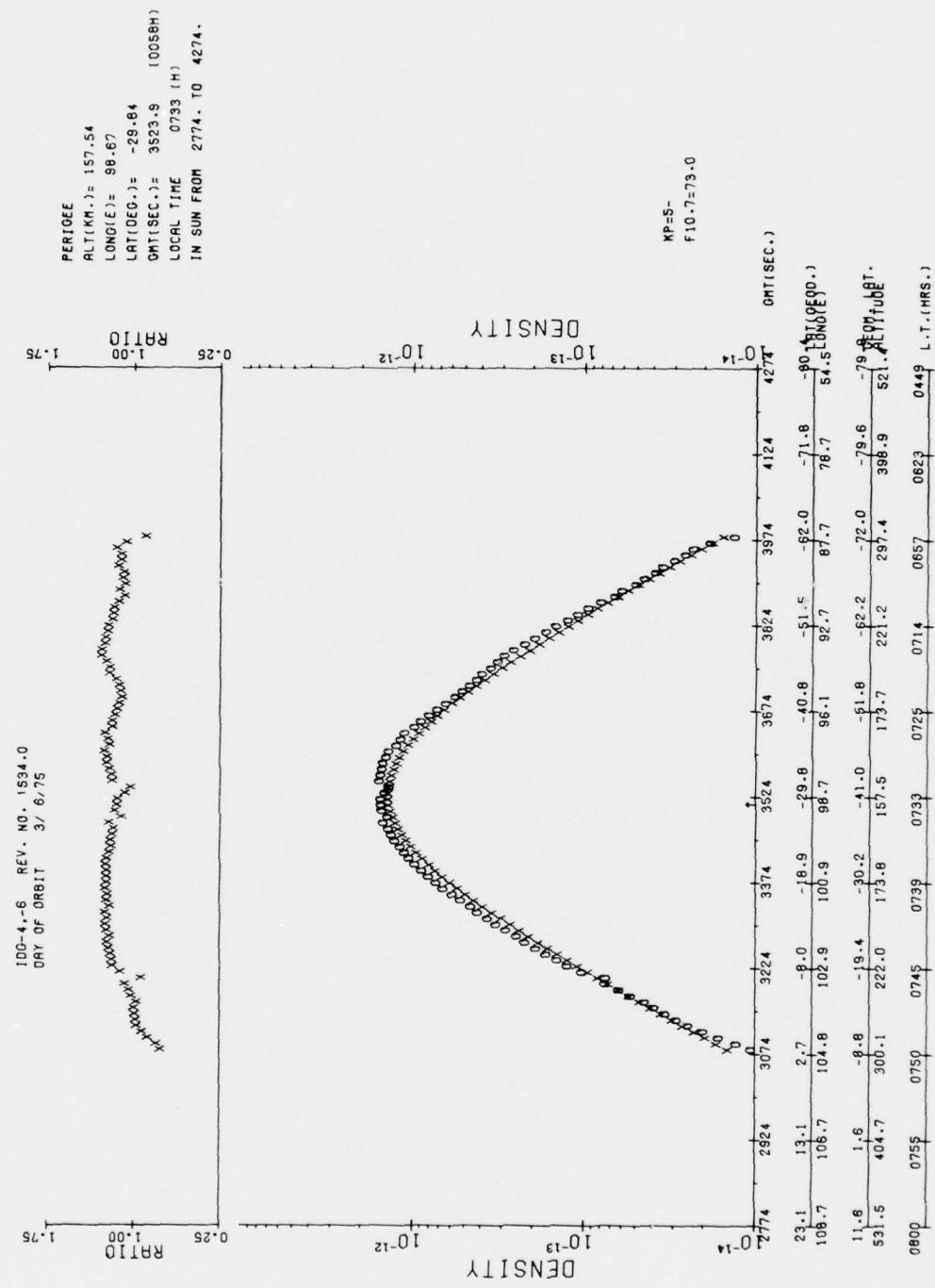


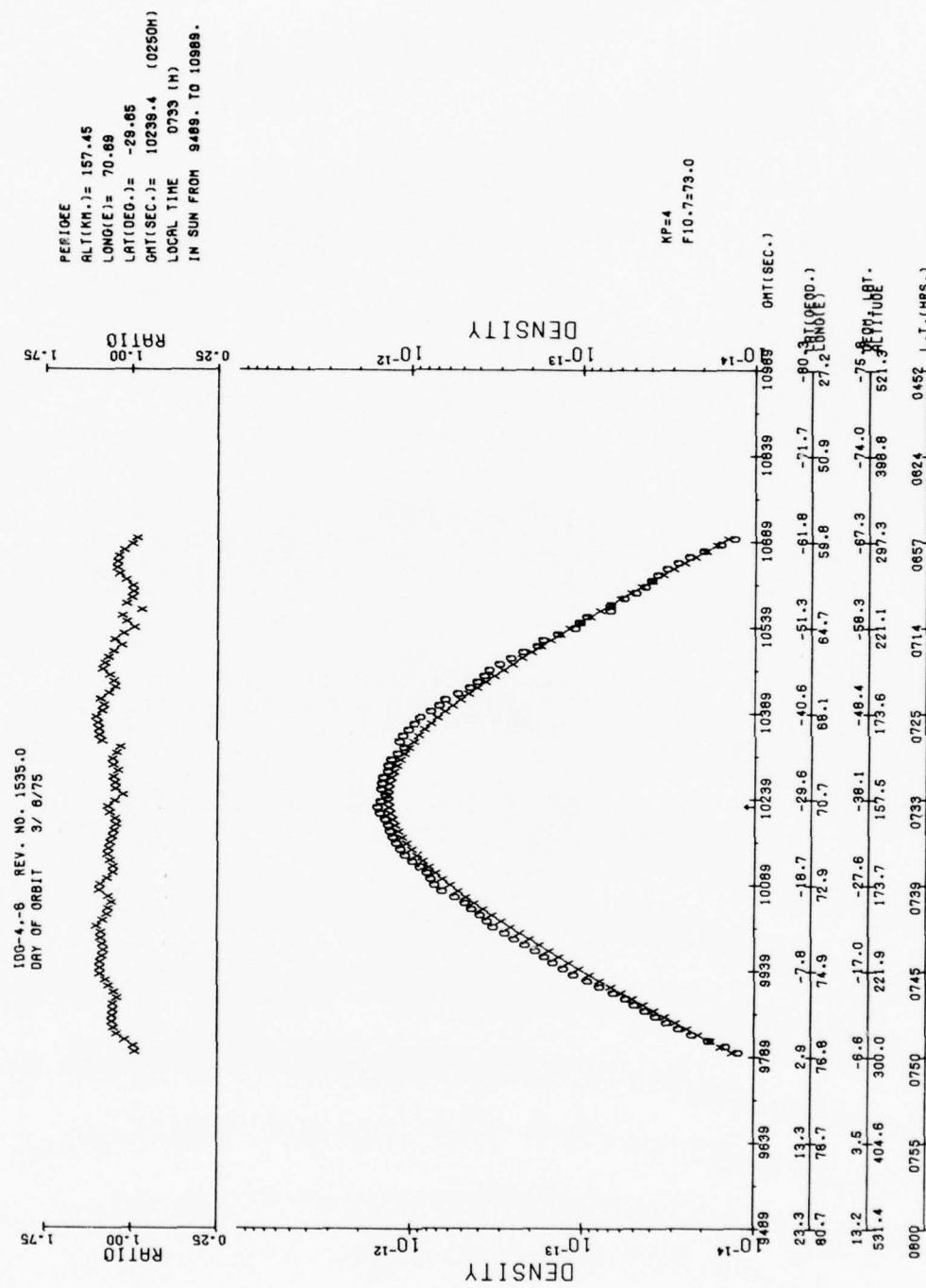


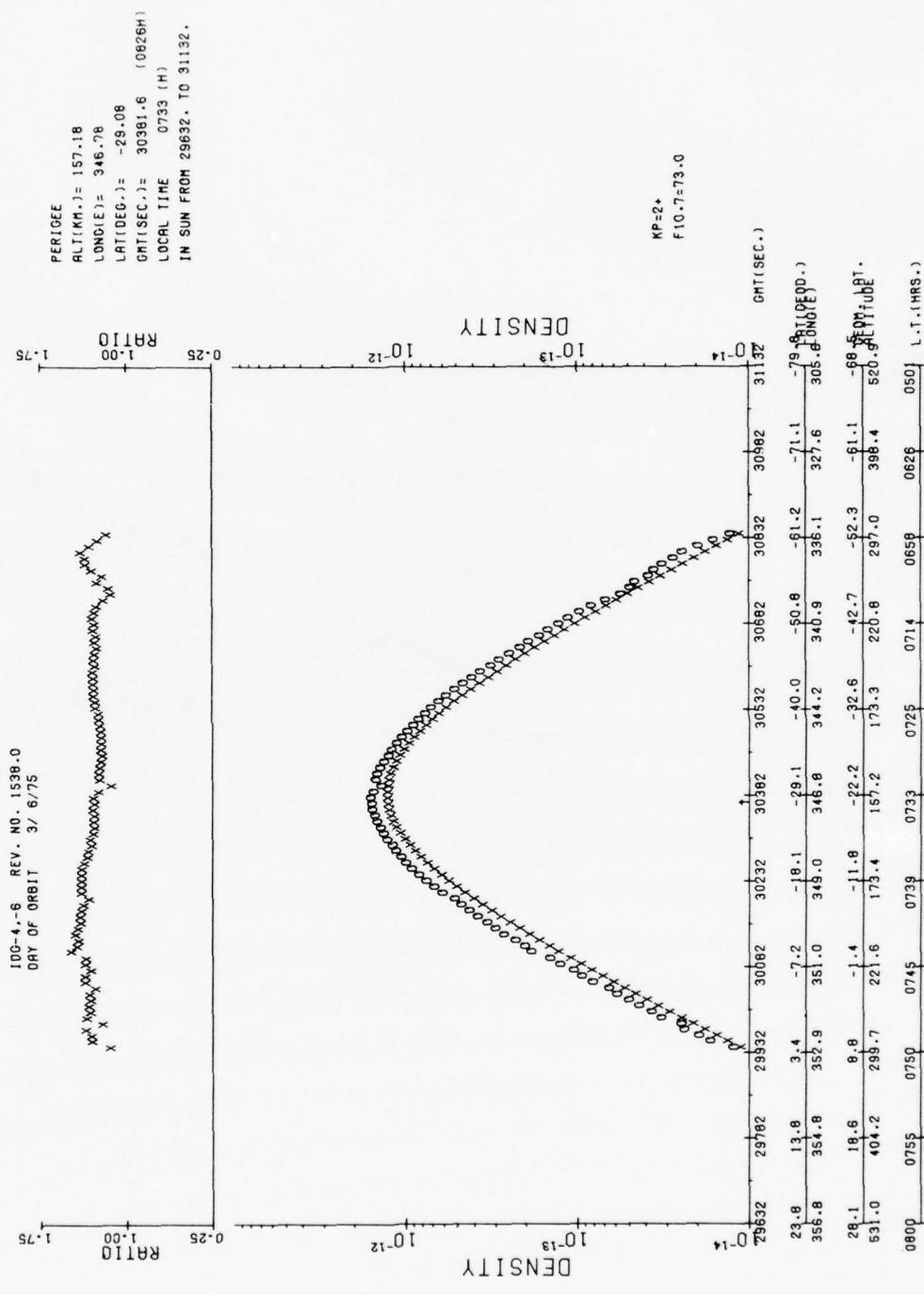


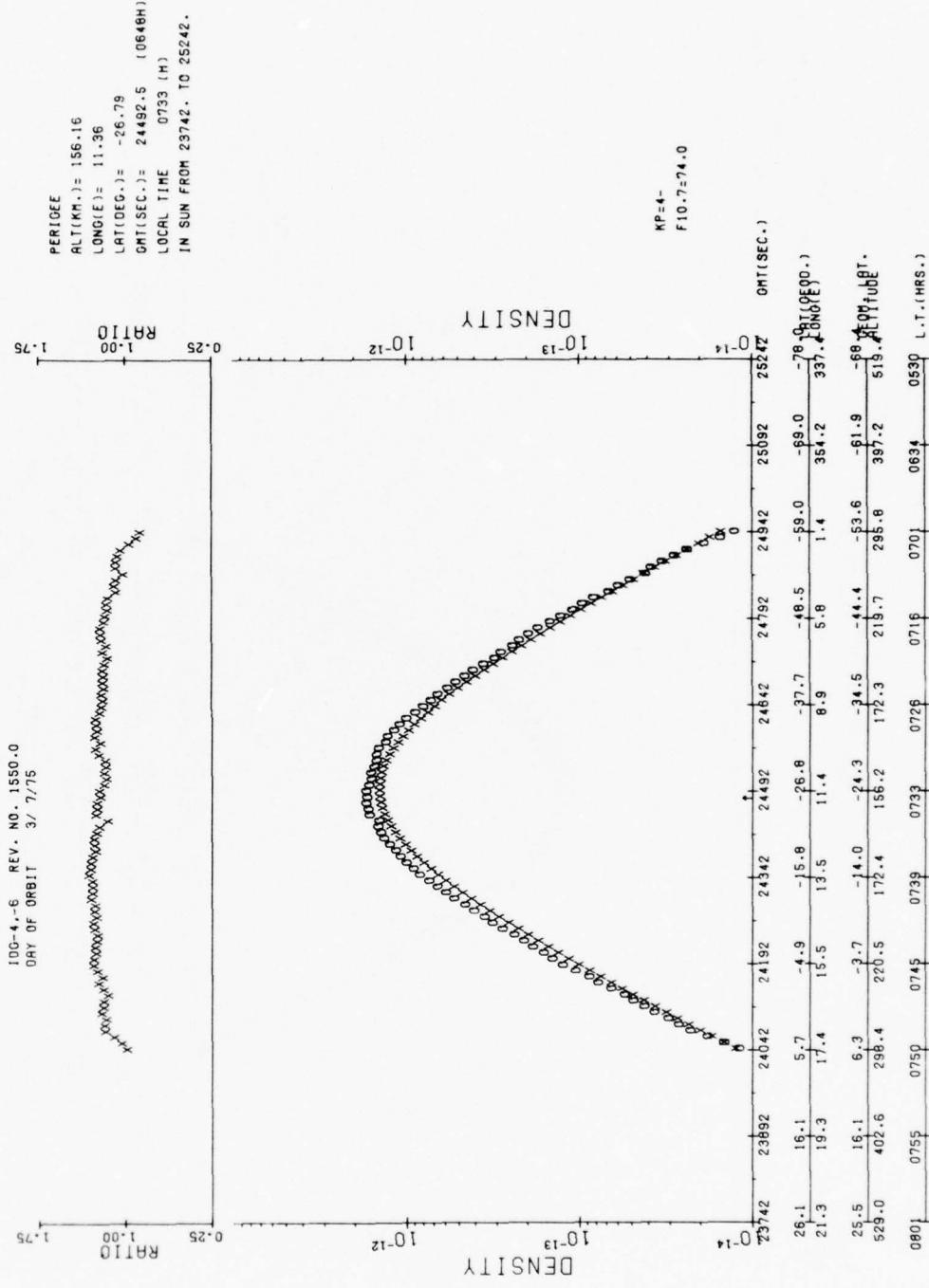


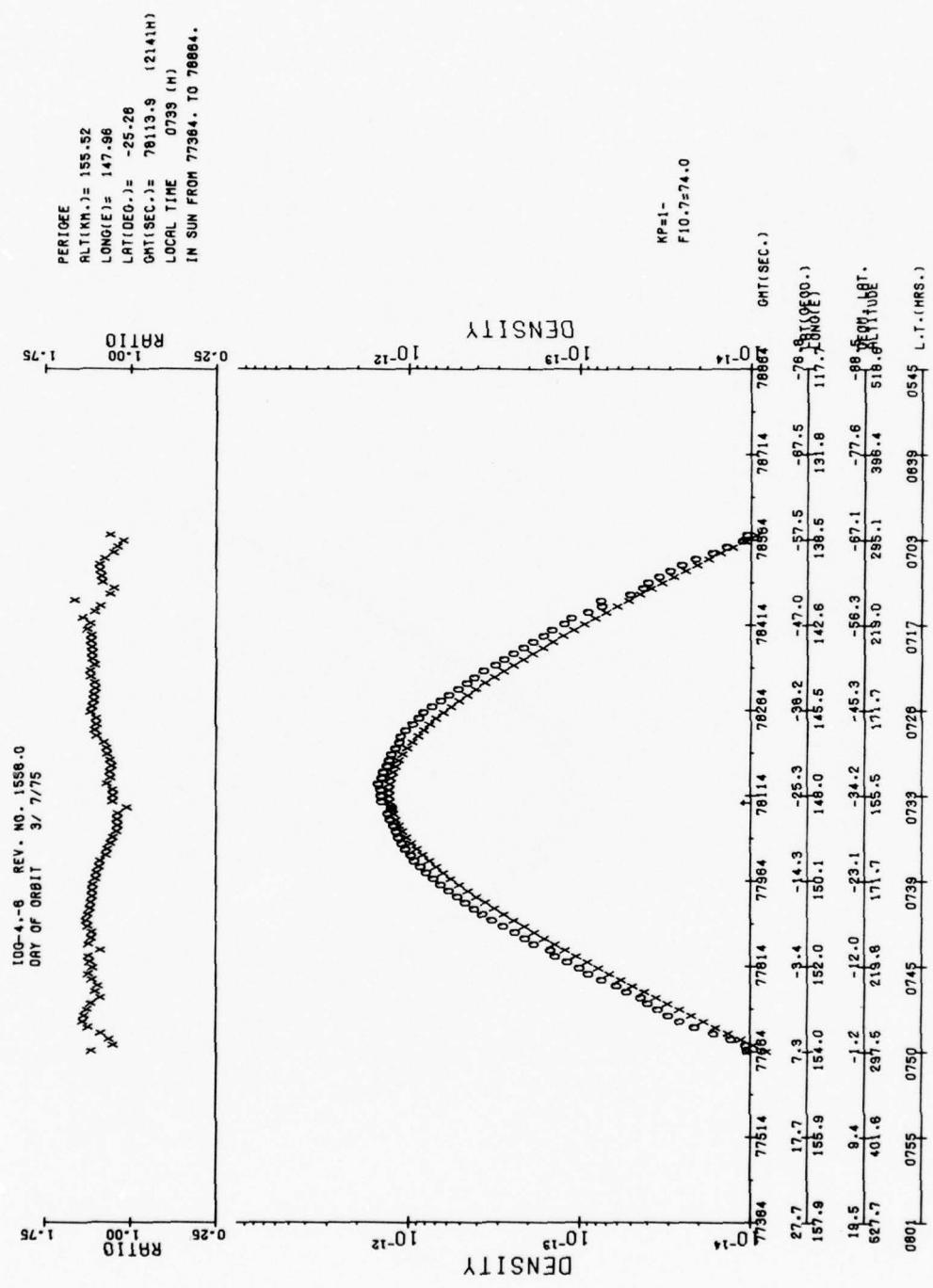


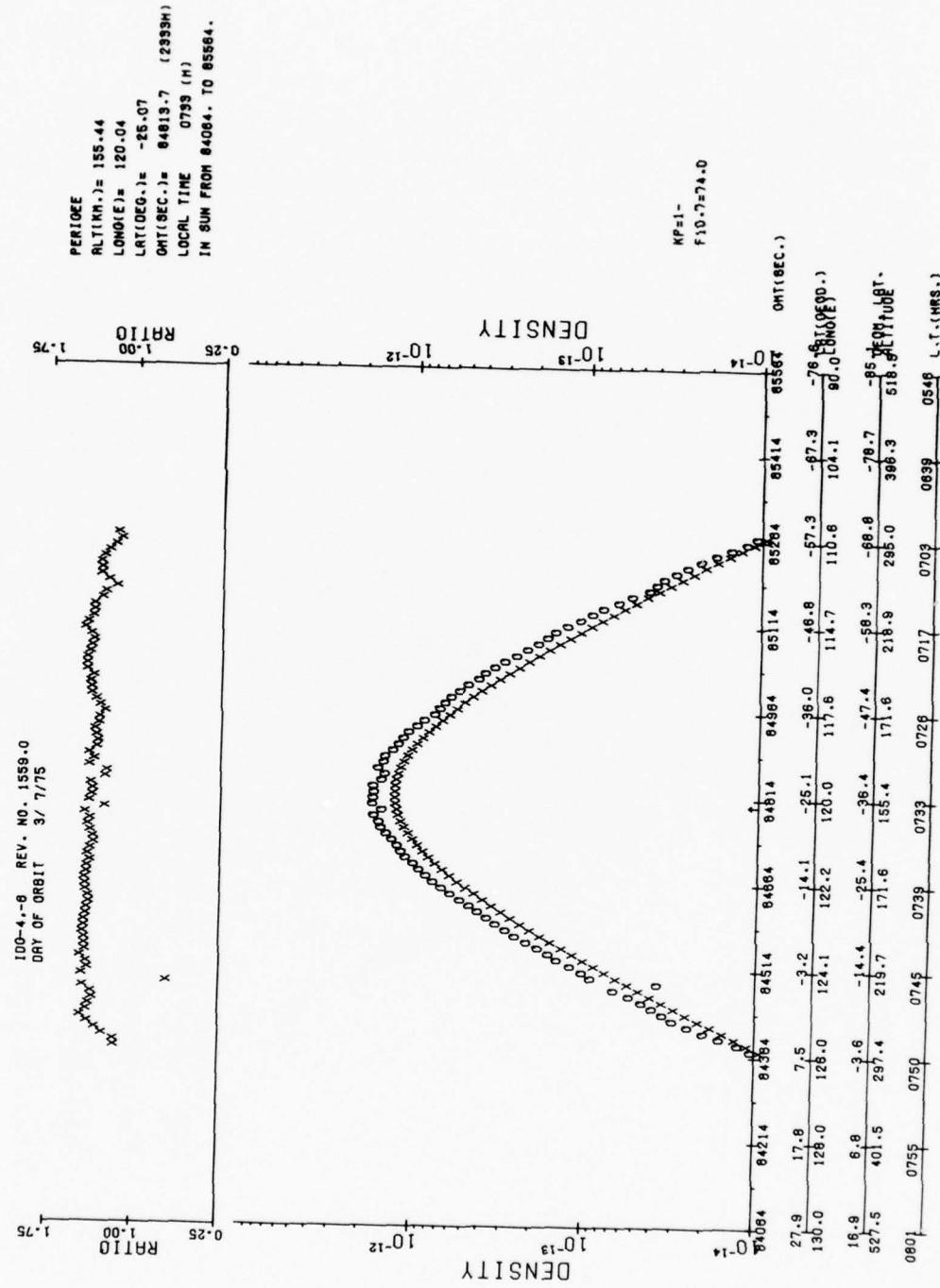


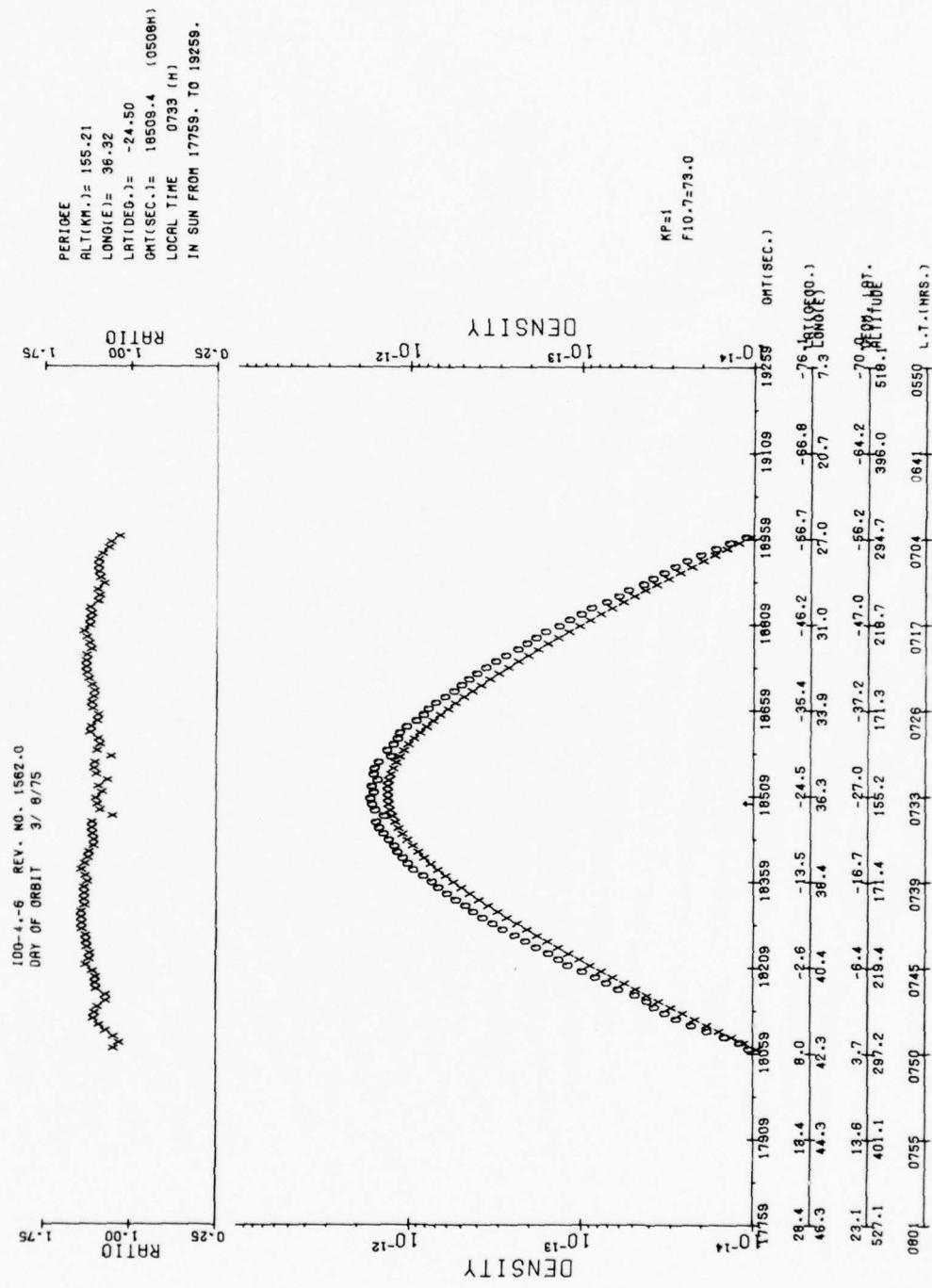




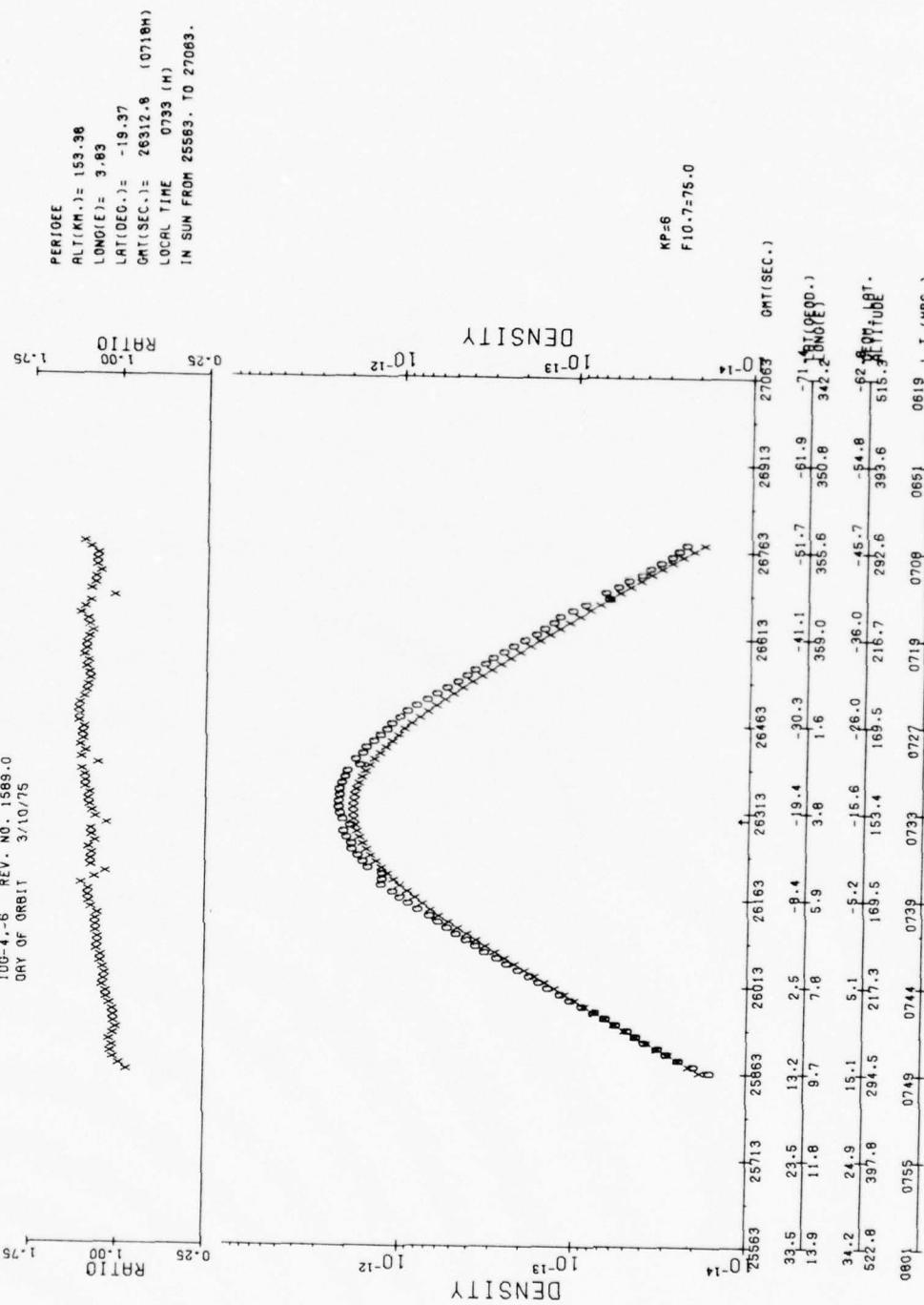


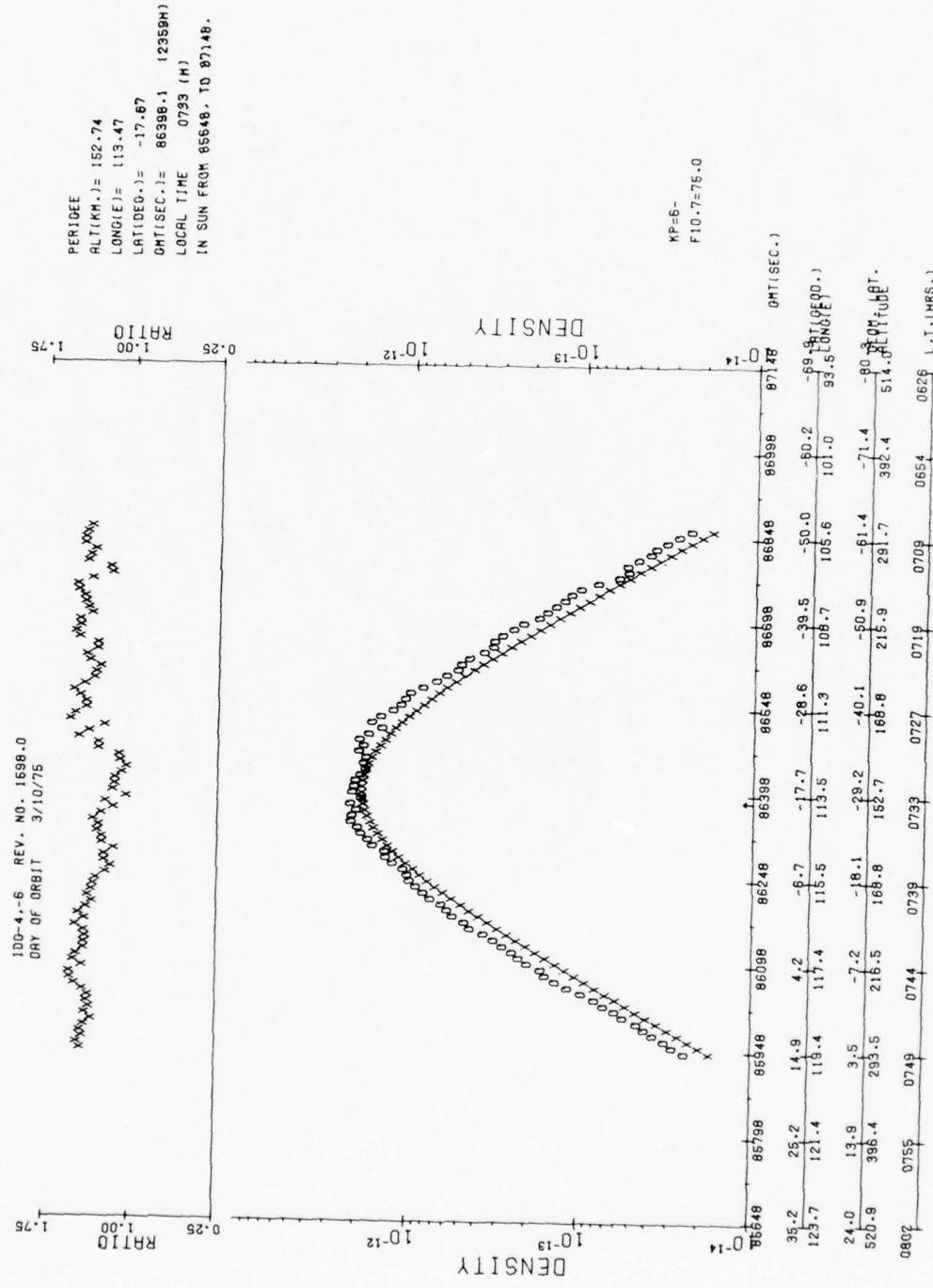


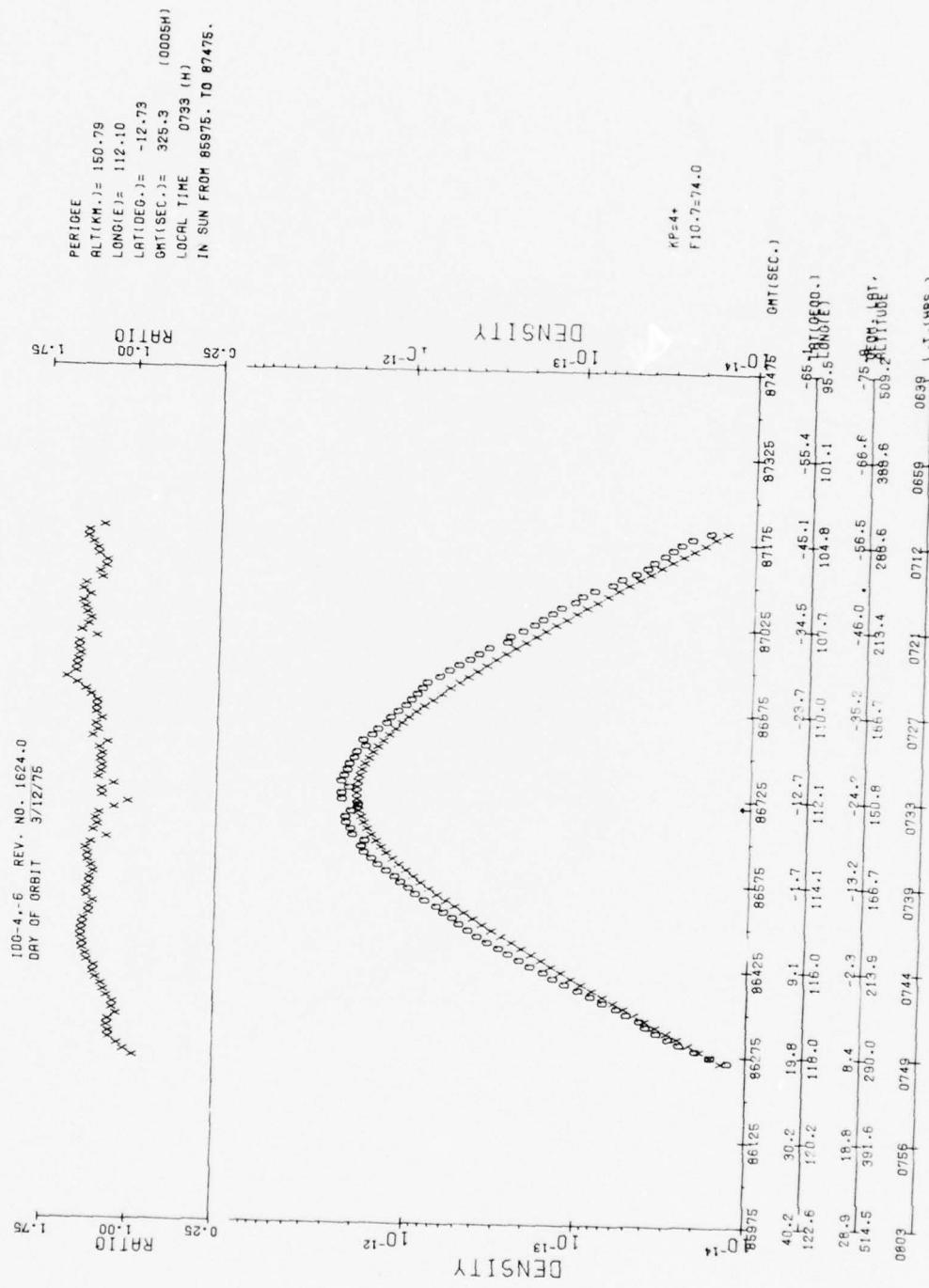


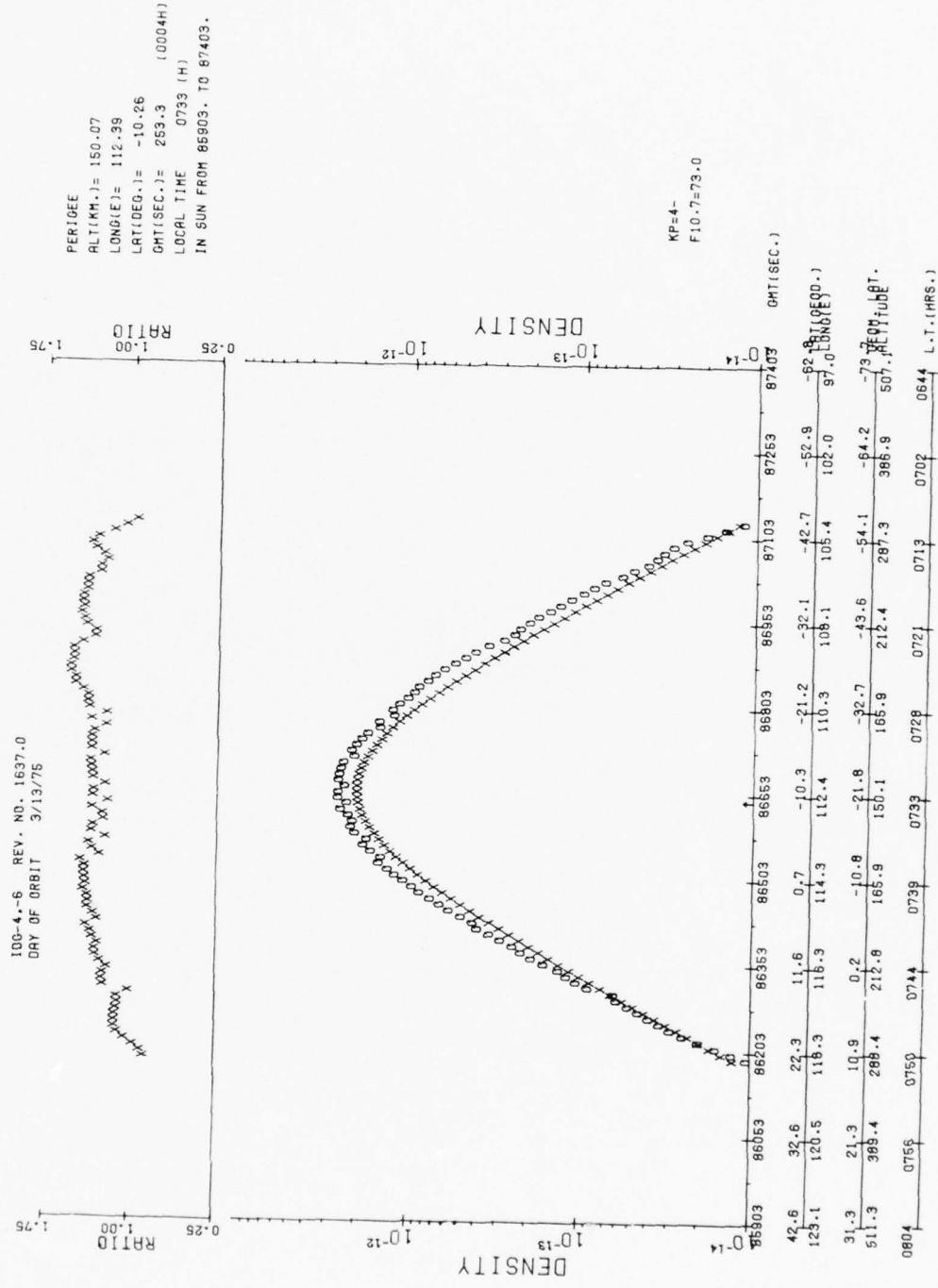


10G-4.-6 REV. NO. 1589.0
DAY OF ORBIT 3/10/75

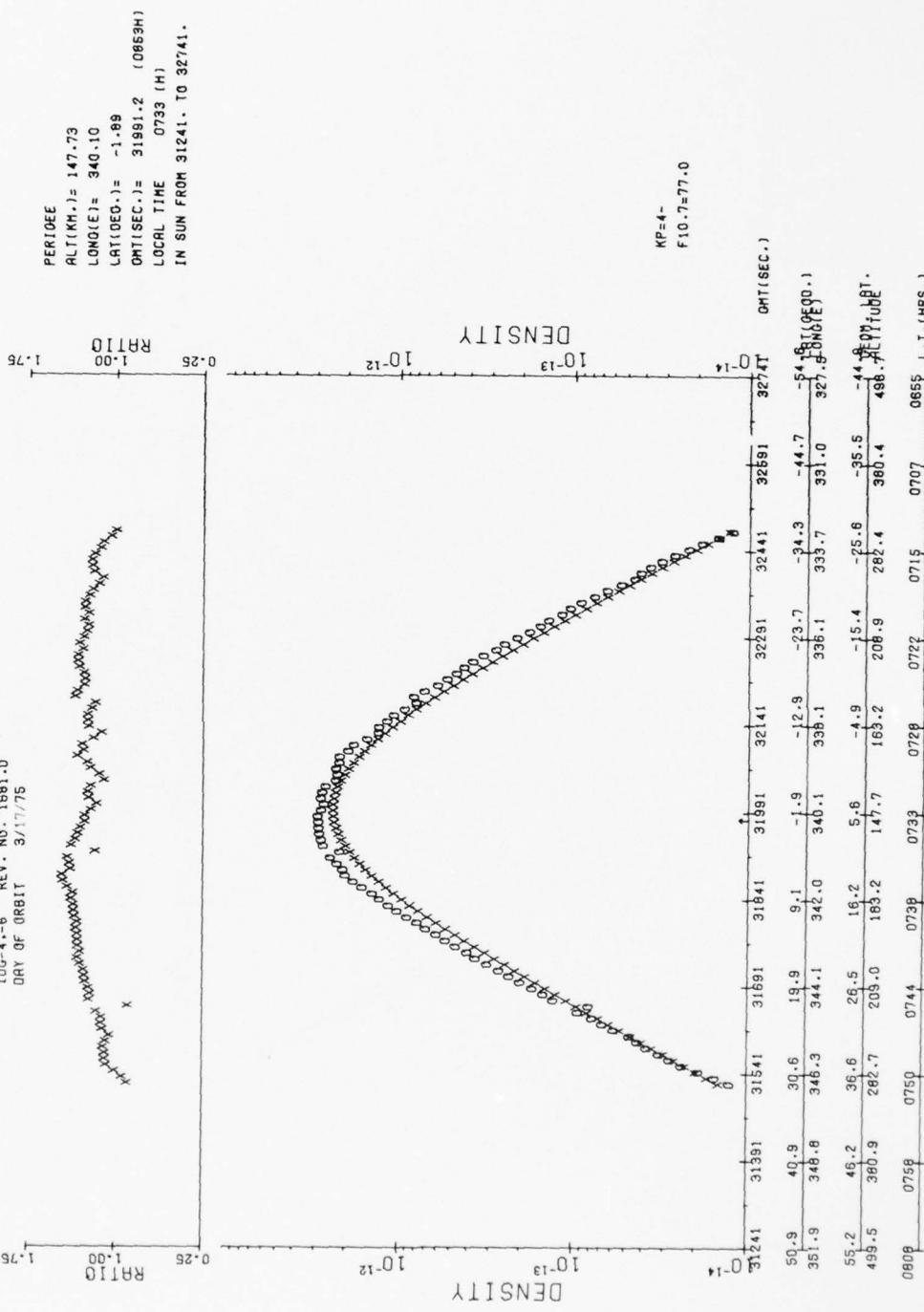




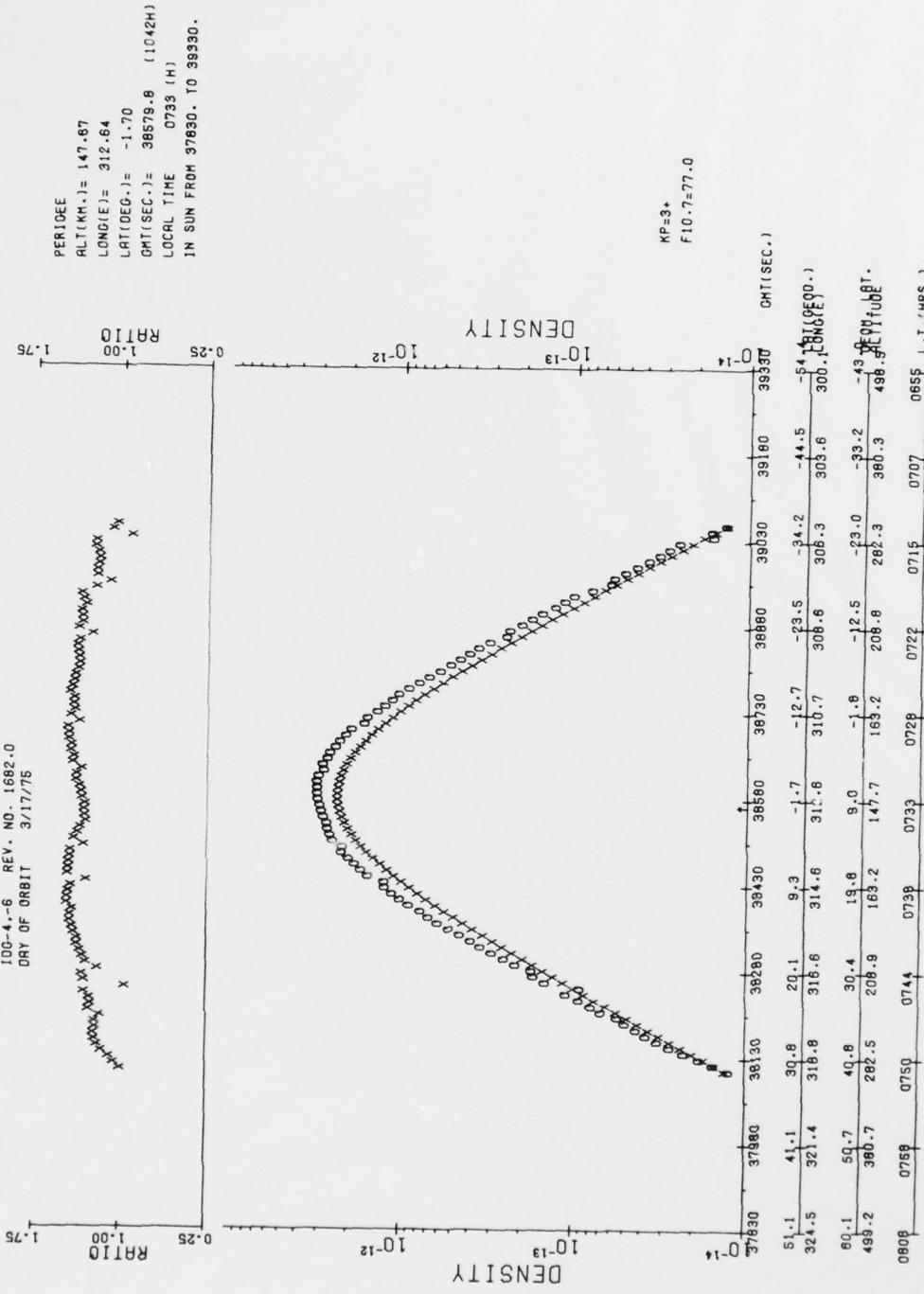


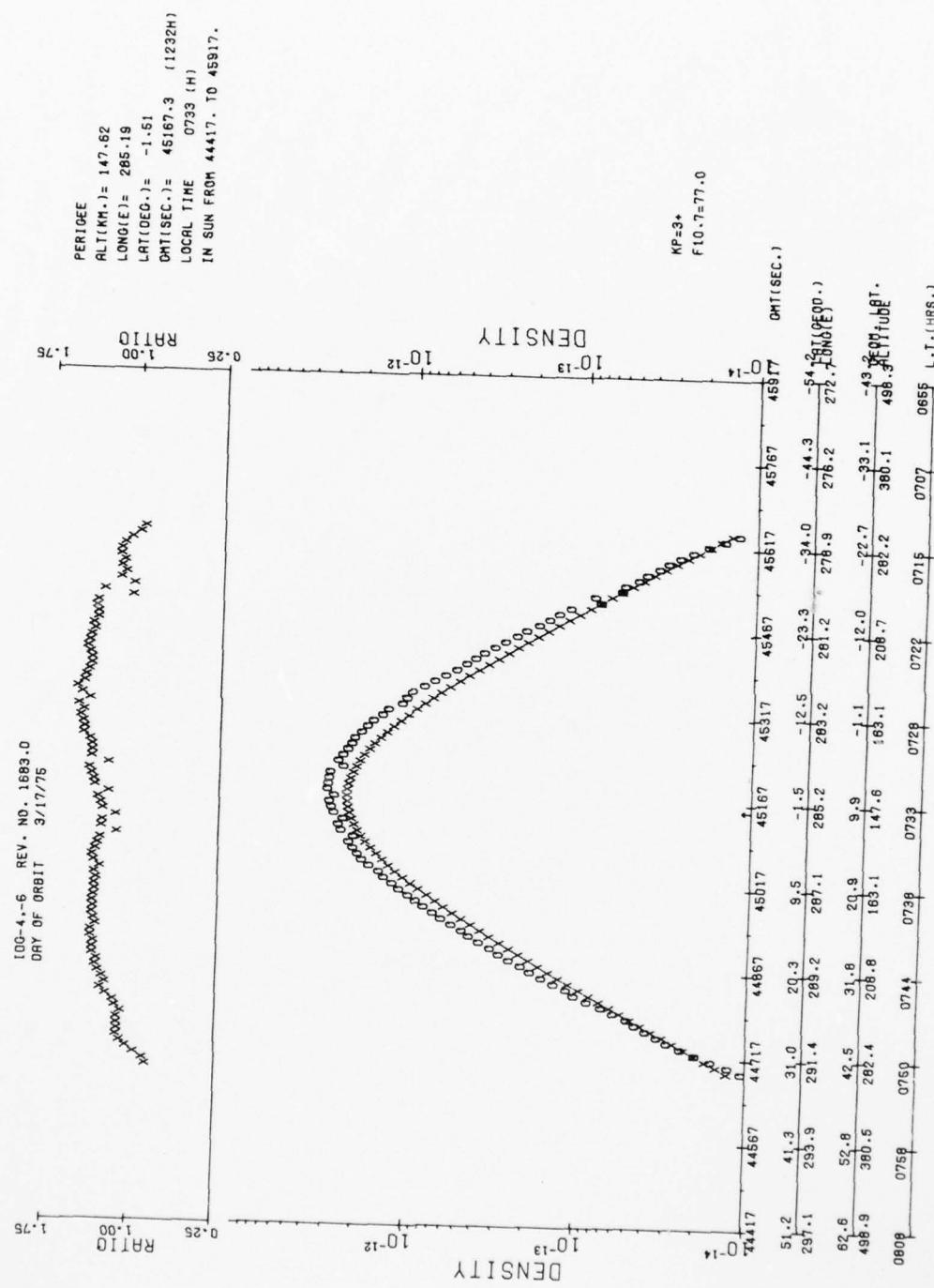


LOG-4,-6 REV. NO. 1601.0
DAY OF ORBIT 3/17/75

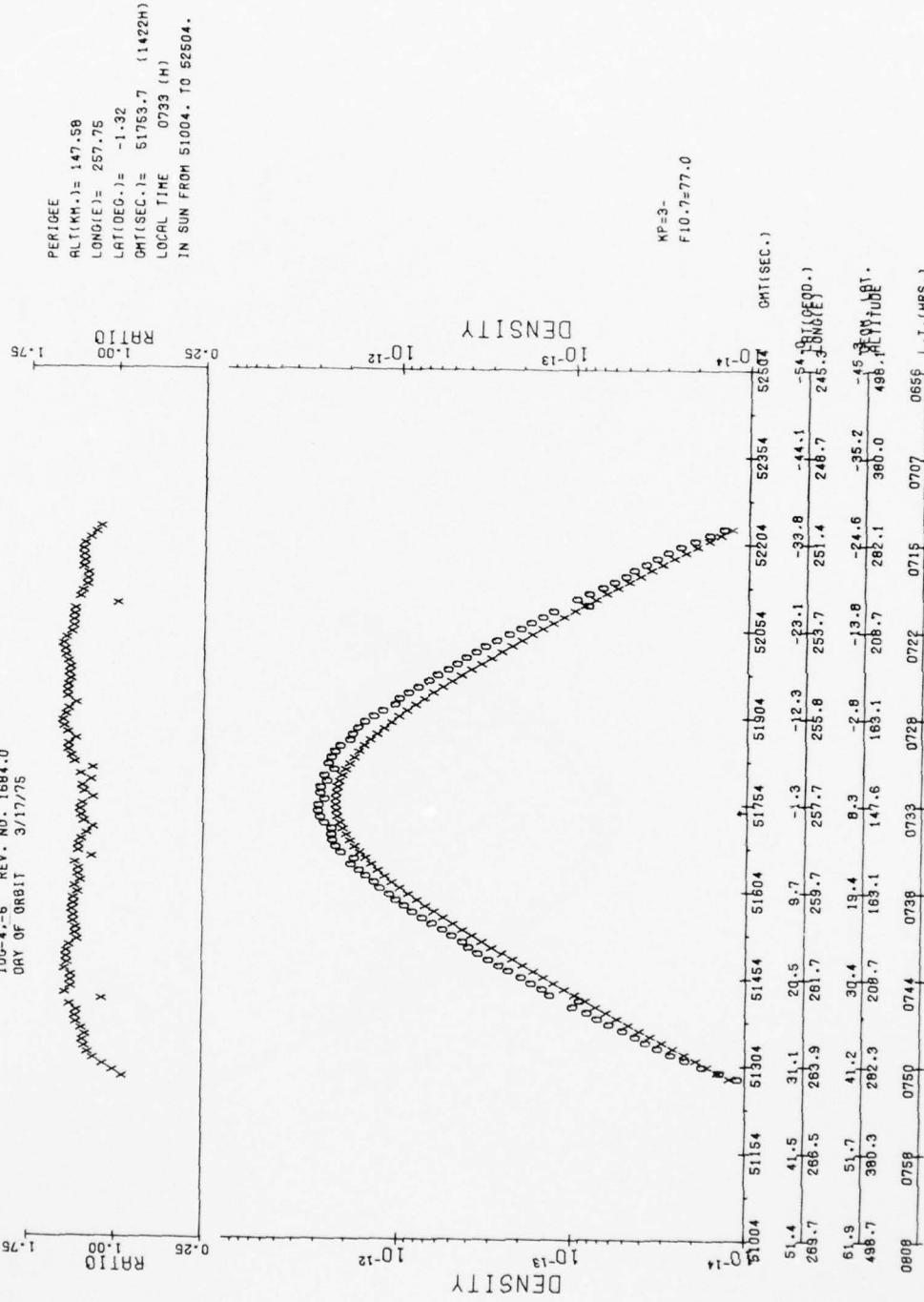


10G-4.-6 REV. NO. 1682.0
DAY OF ORBIT 3/17/75

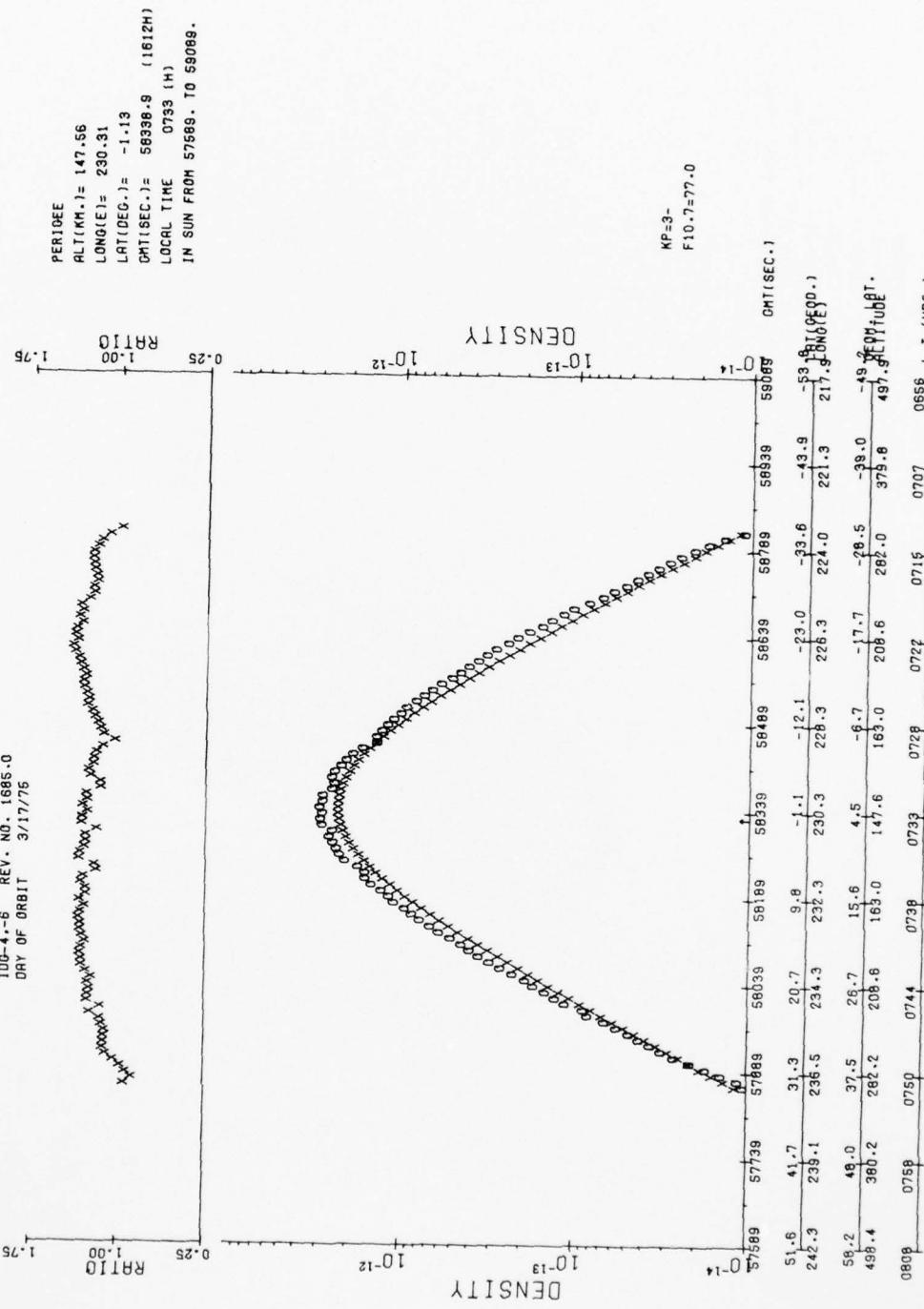


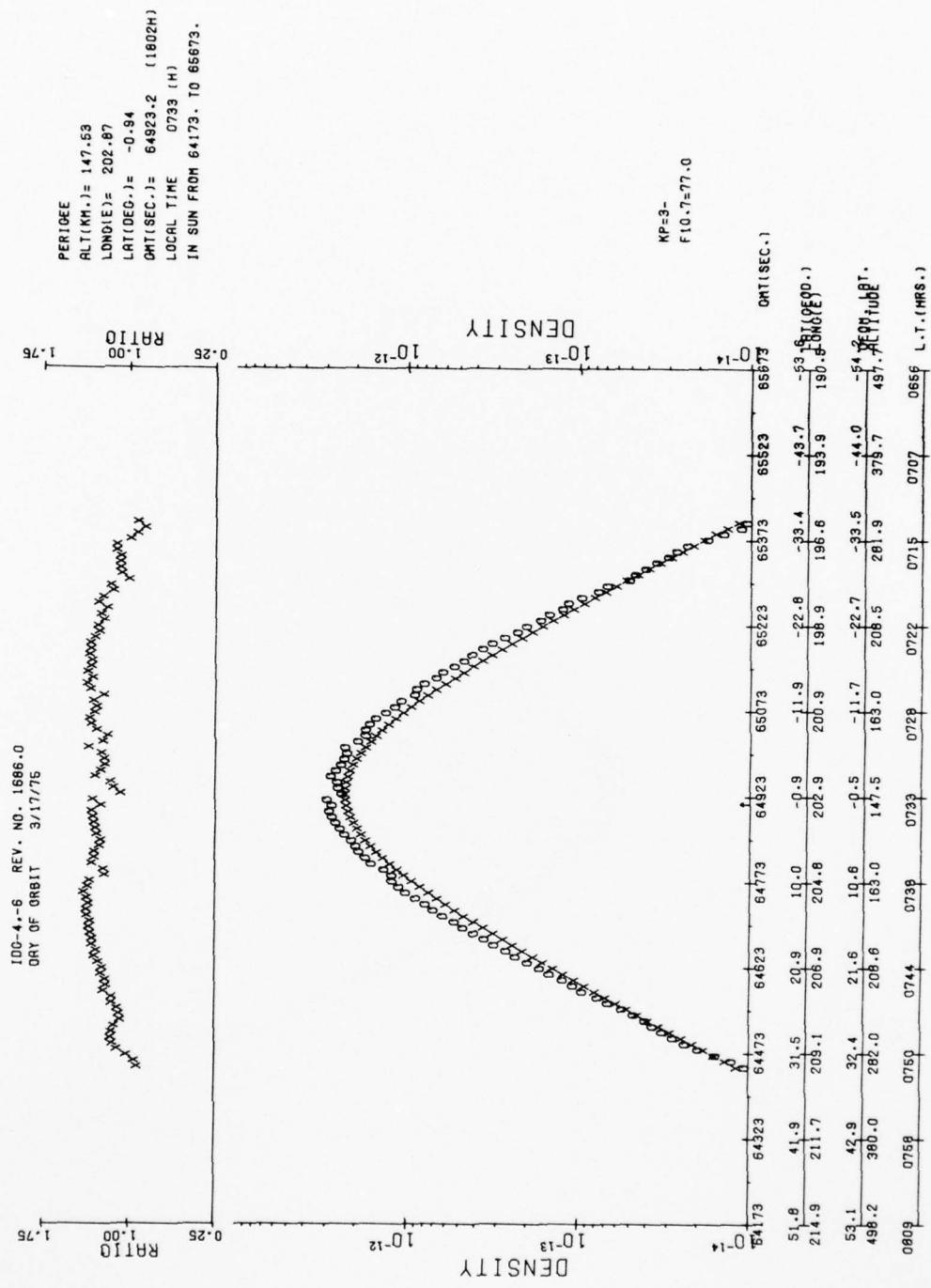


10G-4,-6 REV. NO. 1684.0
DAY OF ORBIT 3/17/75

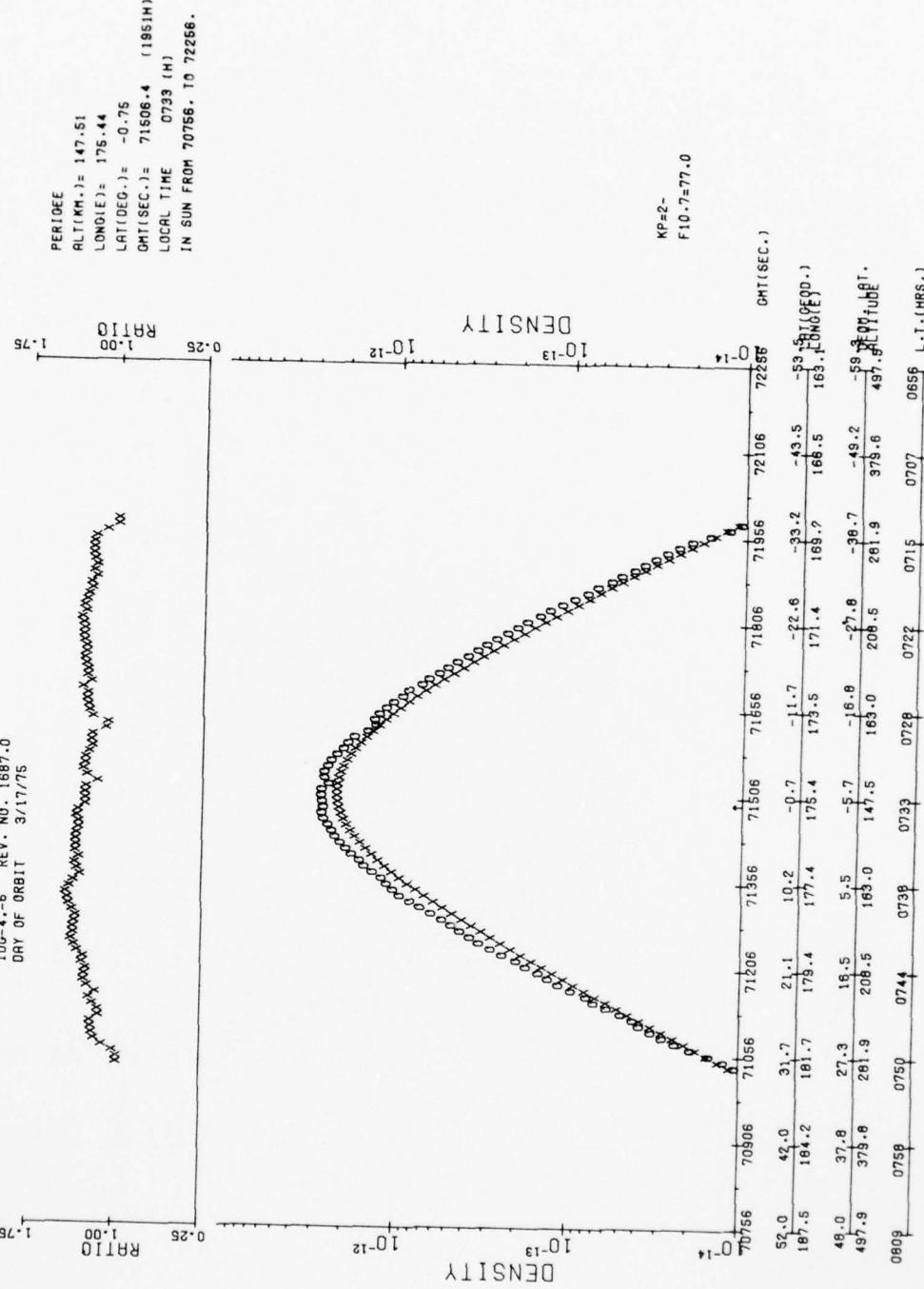


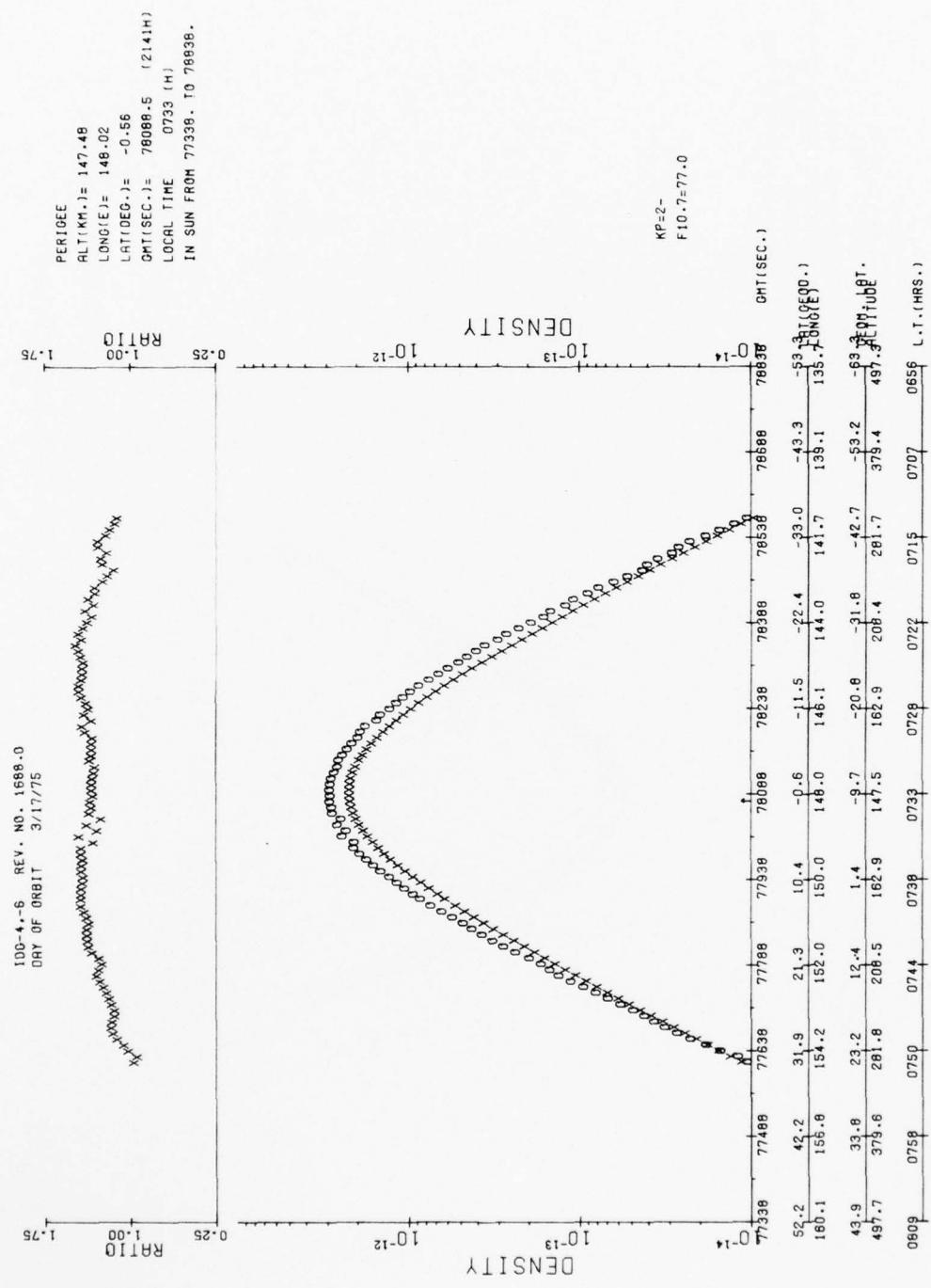
IDG-4-6 REV. NO. 1685-0
DAY OF ORBIT 3/17/75



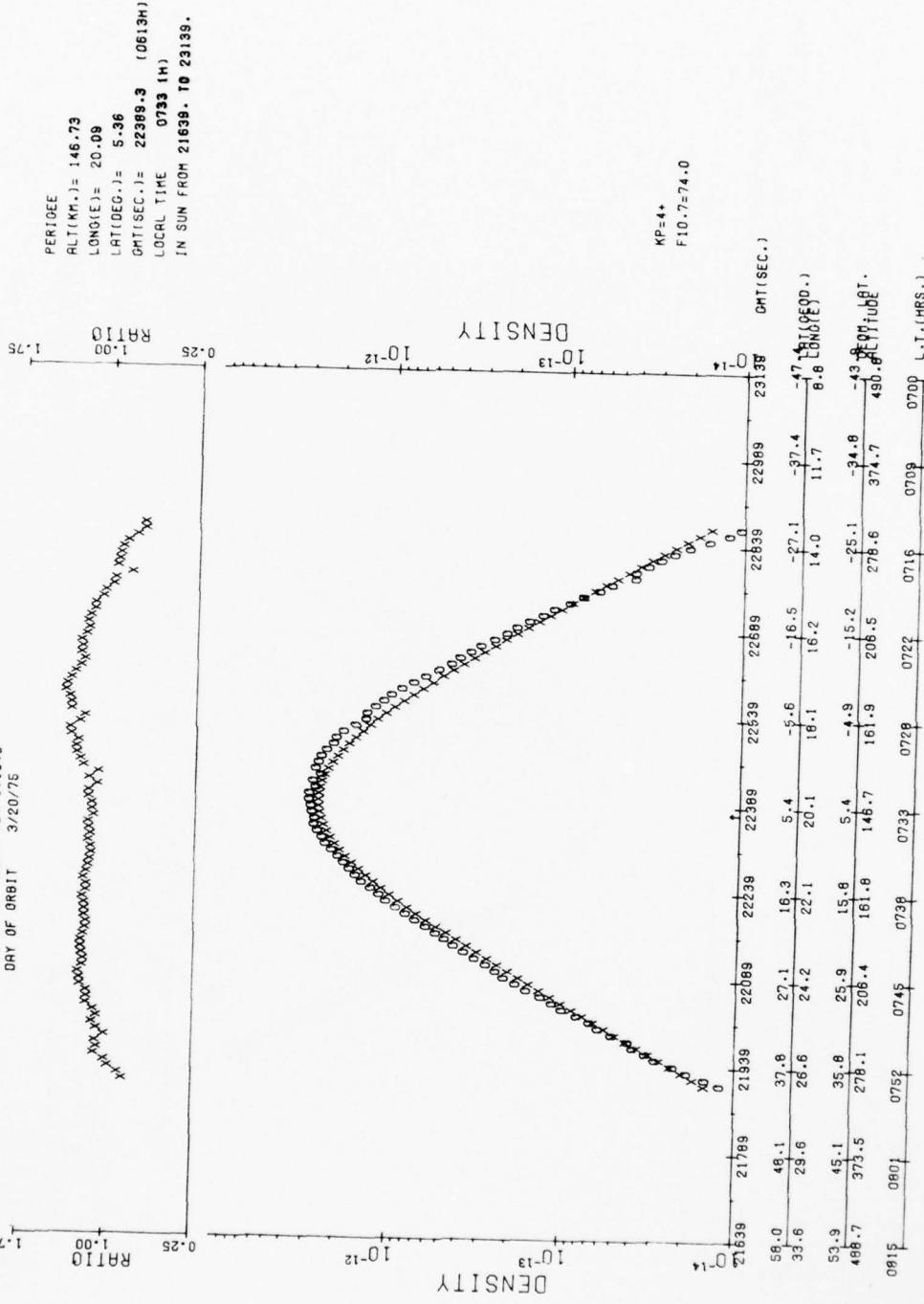


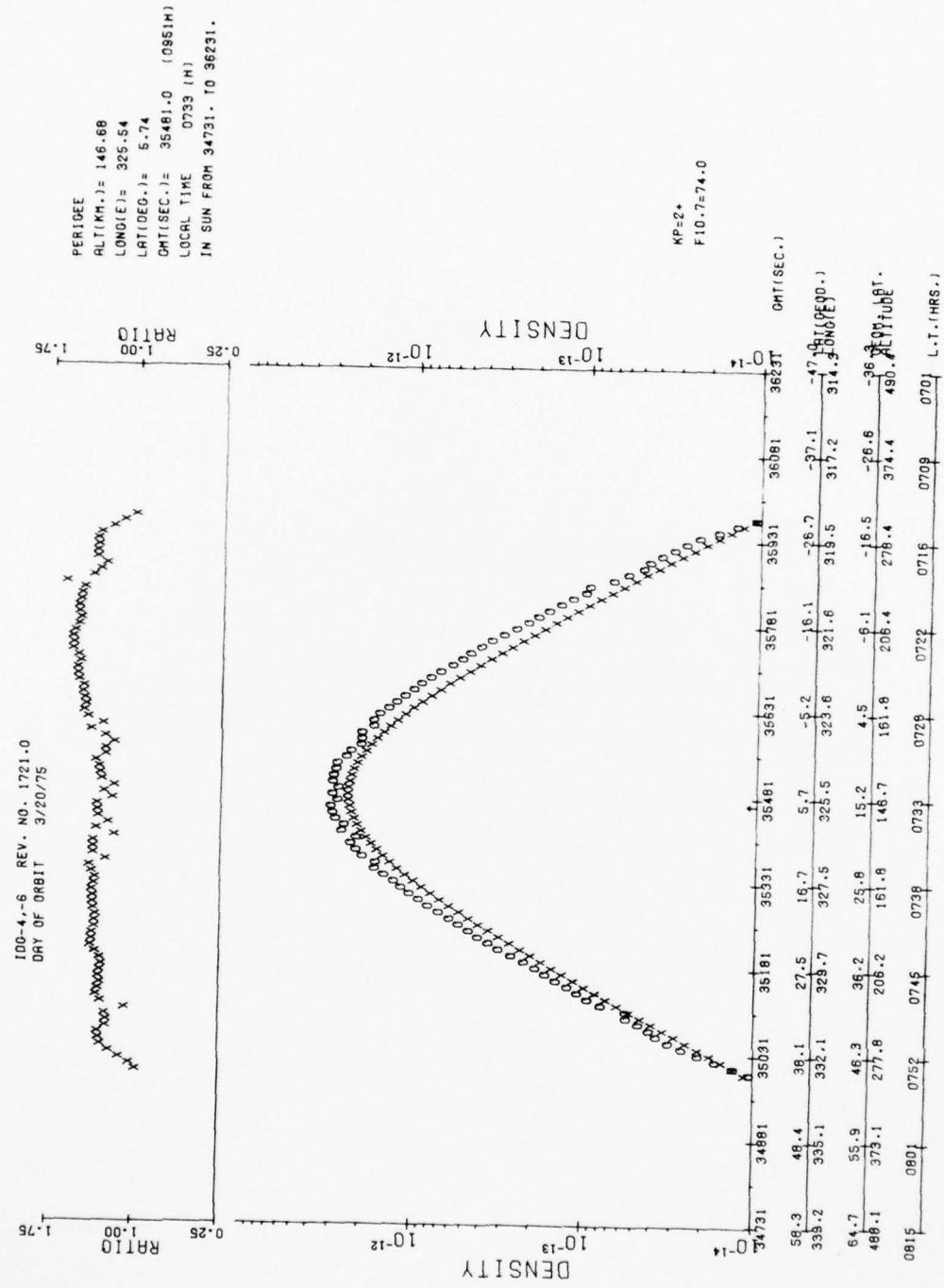
100-4-6 REV. NO. 1687.0
DAY OF ORBIT 3/17/76

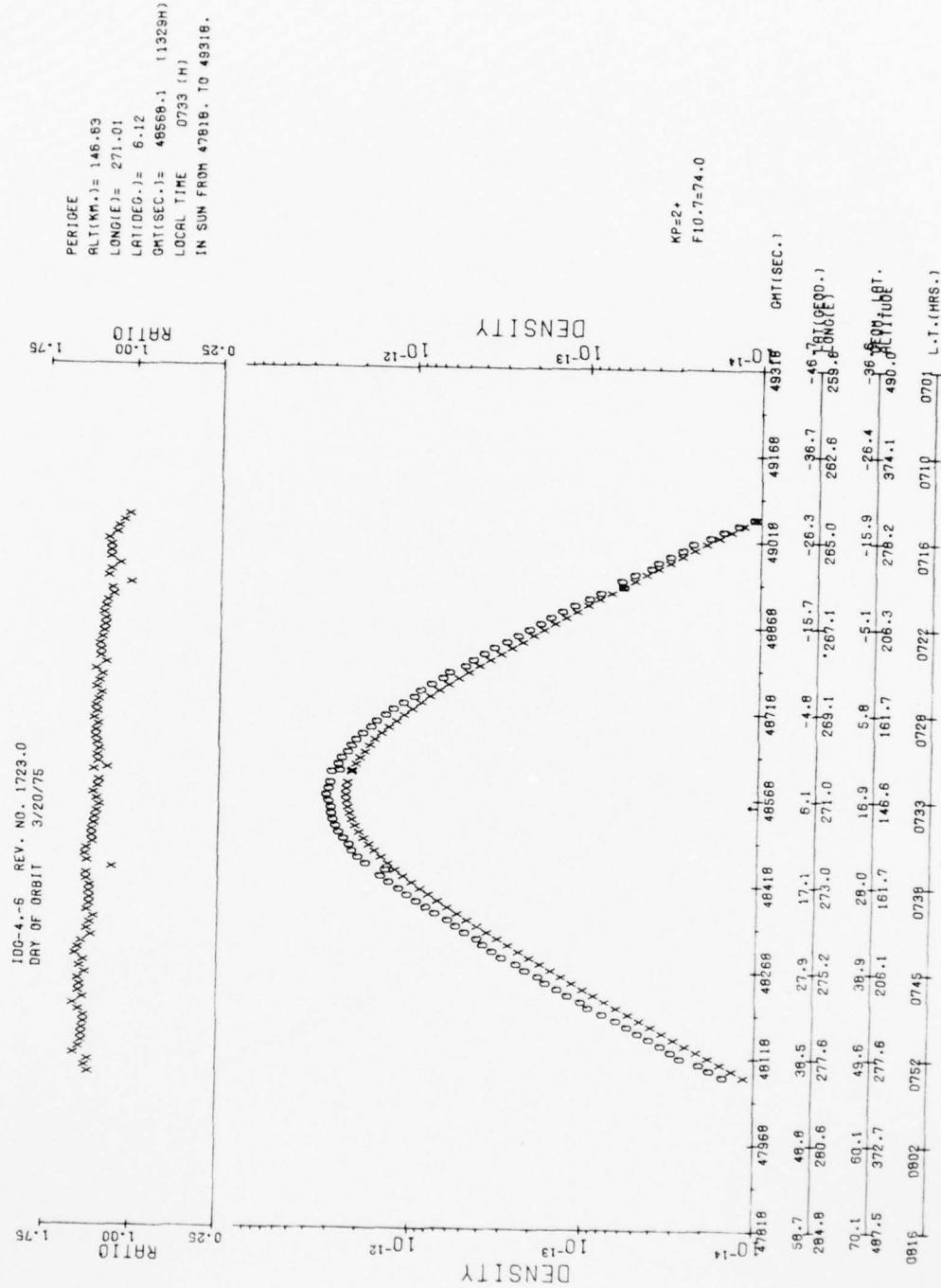


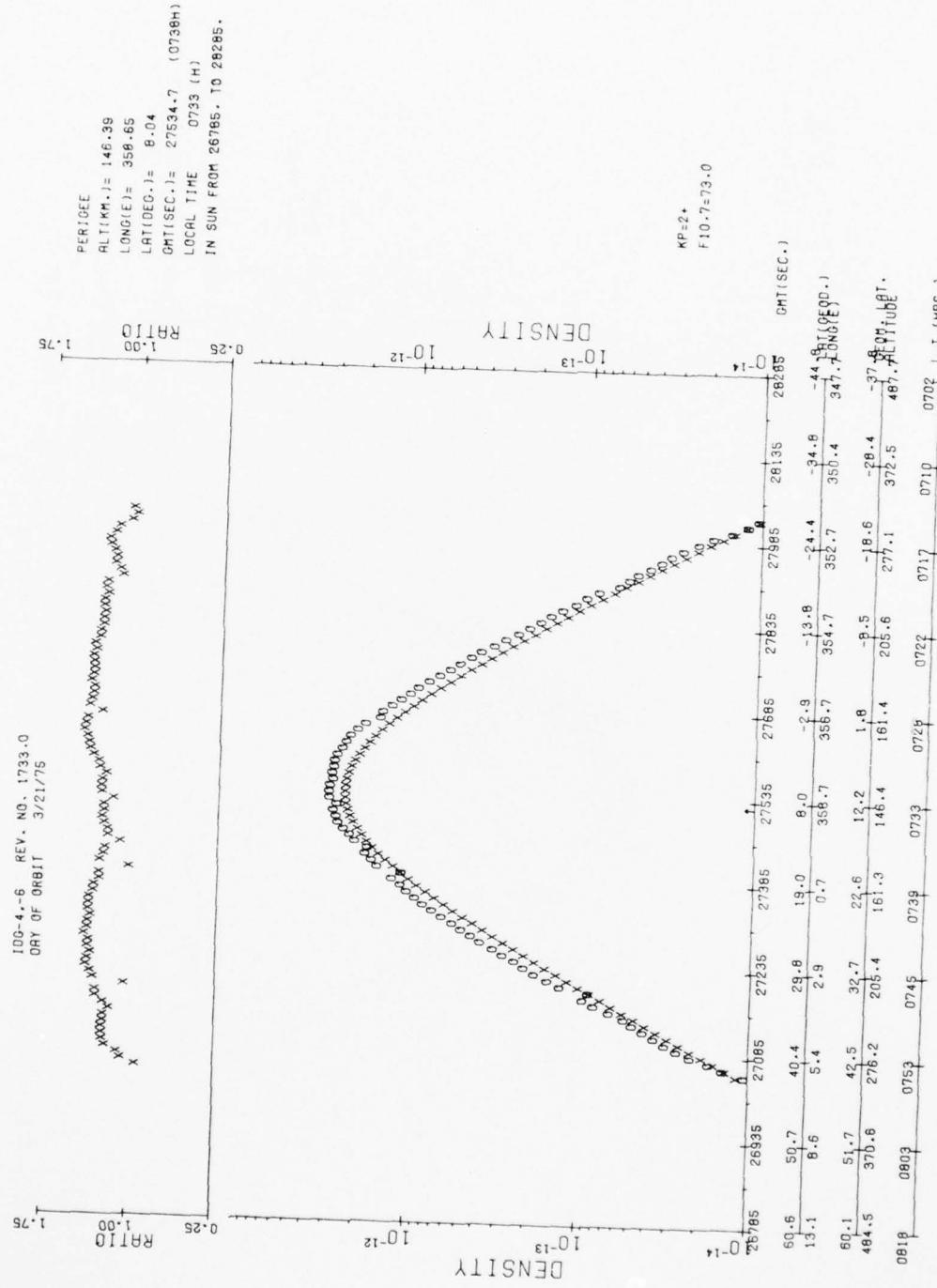


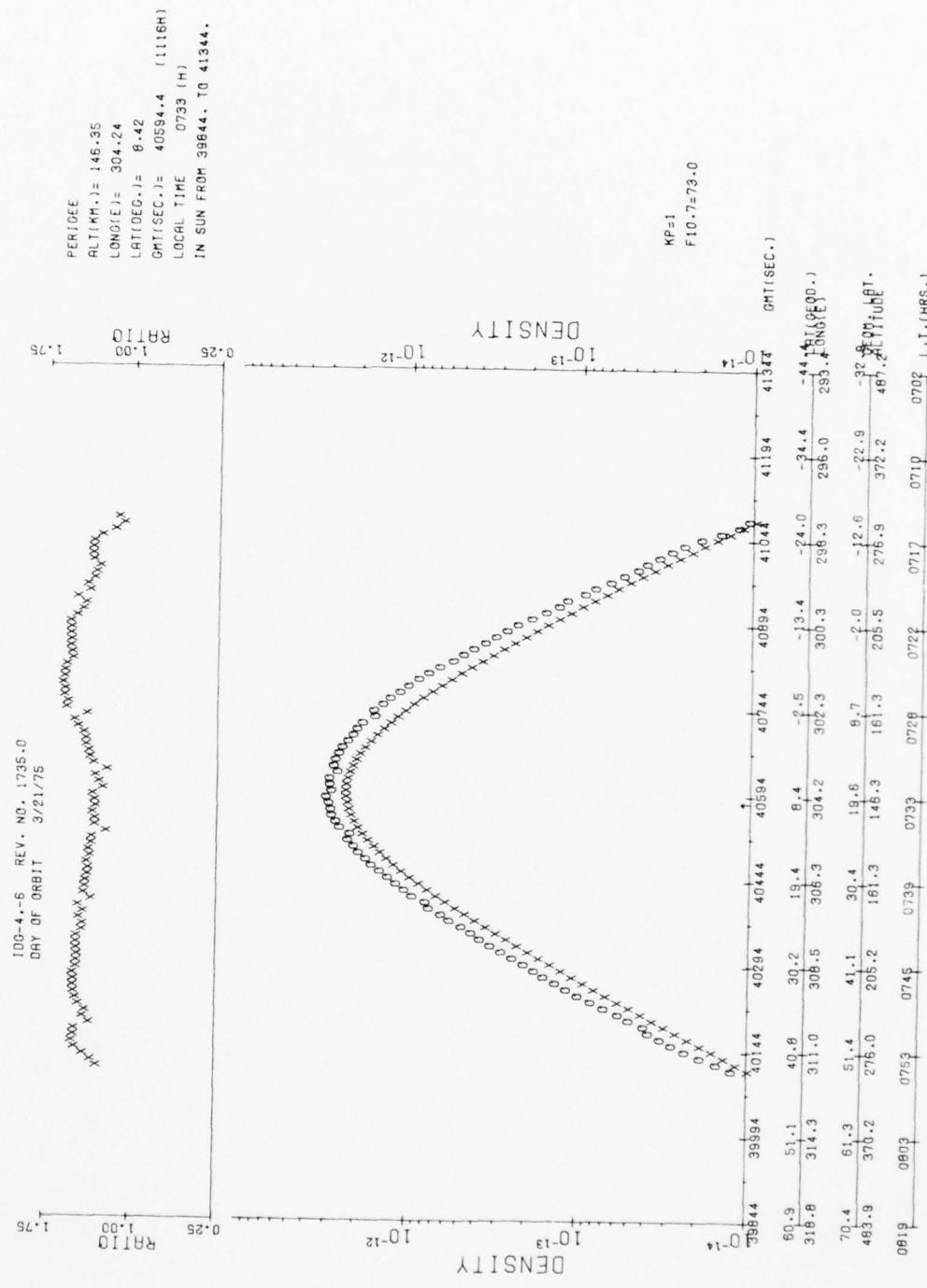
100-4,-6 REV. NO. 1719.0
DRY OF ORBIT 3/20/76

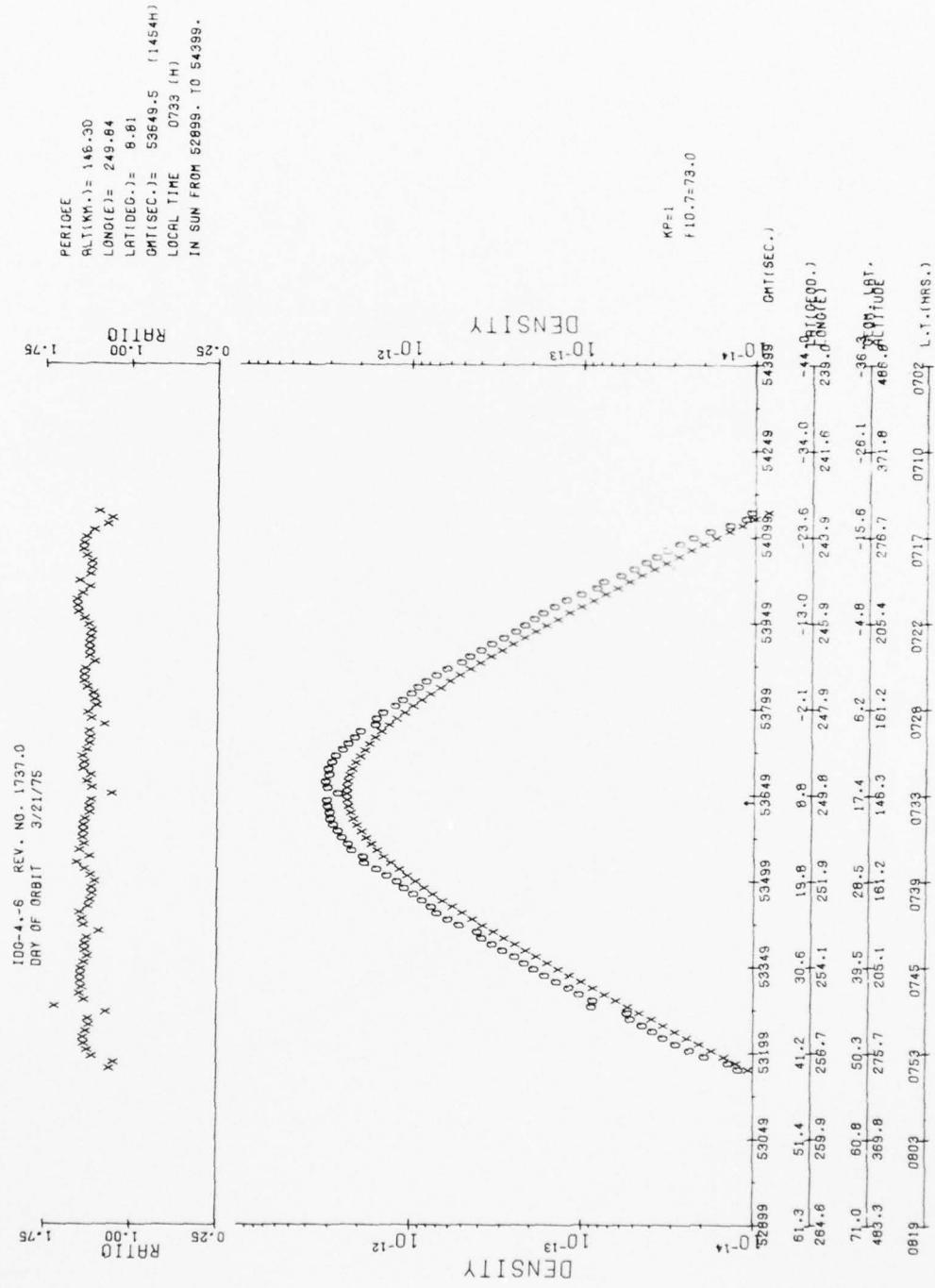


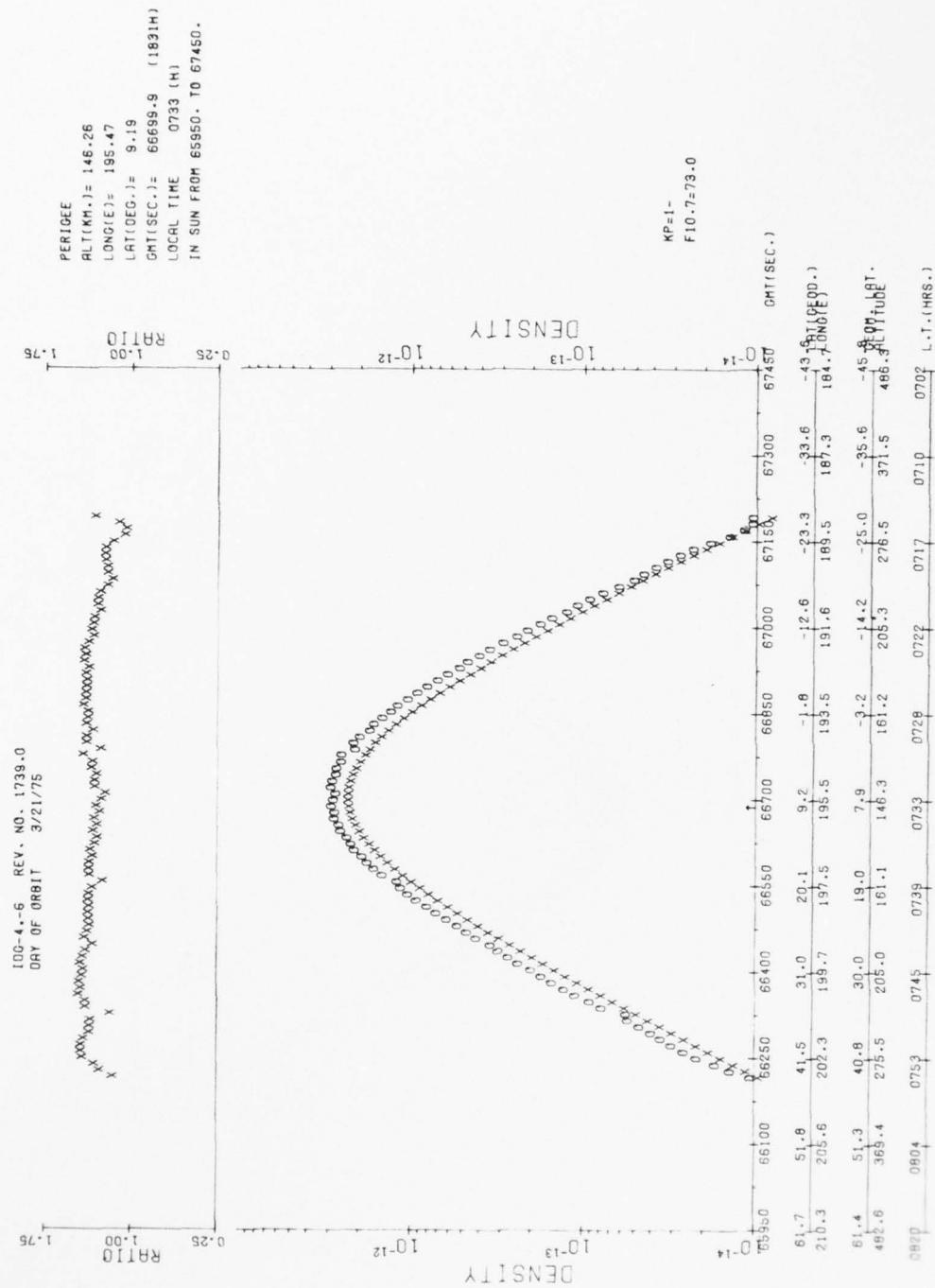












AD-A061 613

AIR FORCE GEOPHYSICS LAB HANSCOM AFB MASS
SATELLITE IONIZATION GAUGE MEASUREMENTS OF ATMOSPHERIC DENSITY. (U)

F/G 4/1

AUG 78 J P MCISAAC, R E MCINERNEY, D DELOREY

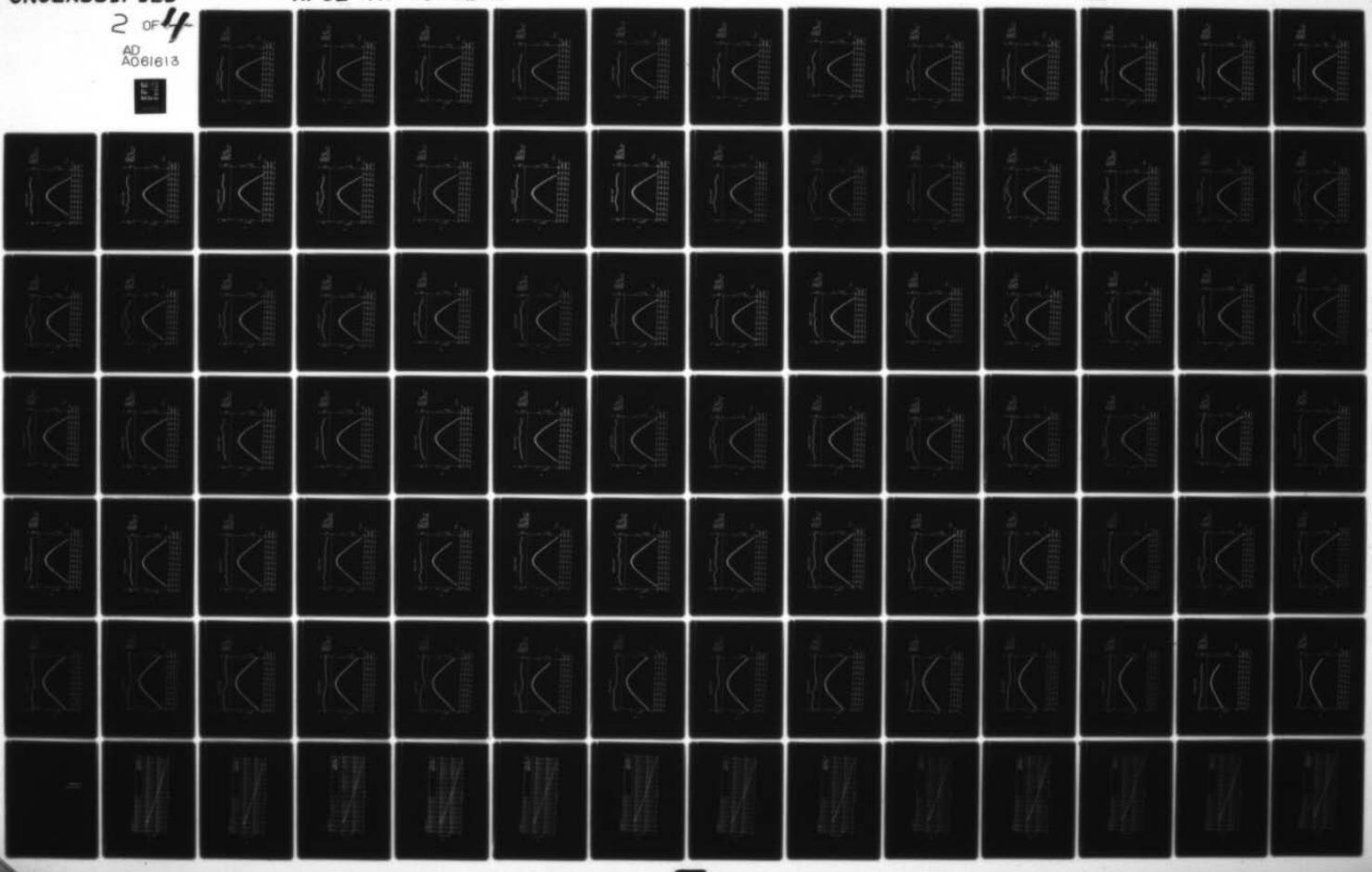
AFGL-TR-78-0201

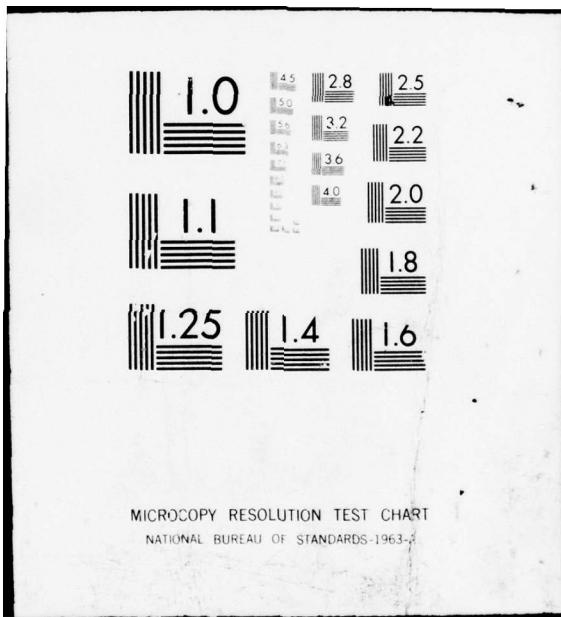
UNCLASSIFIED

NL

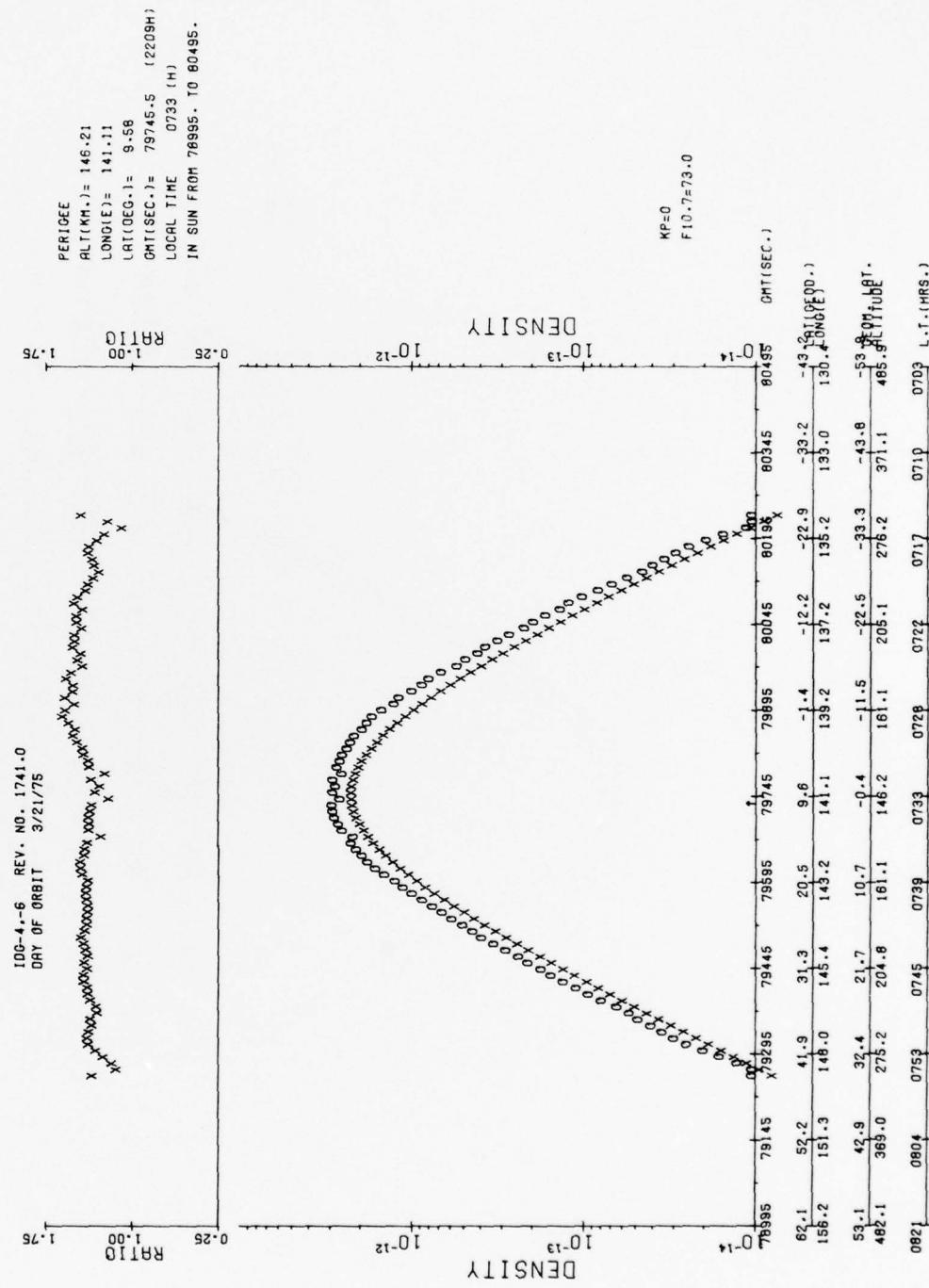
2 OF 4
AD A061613

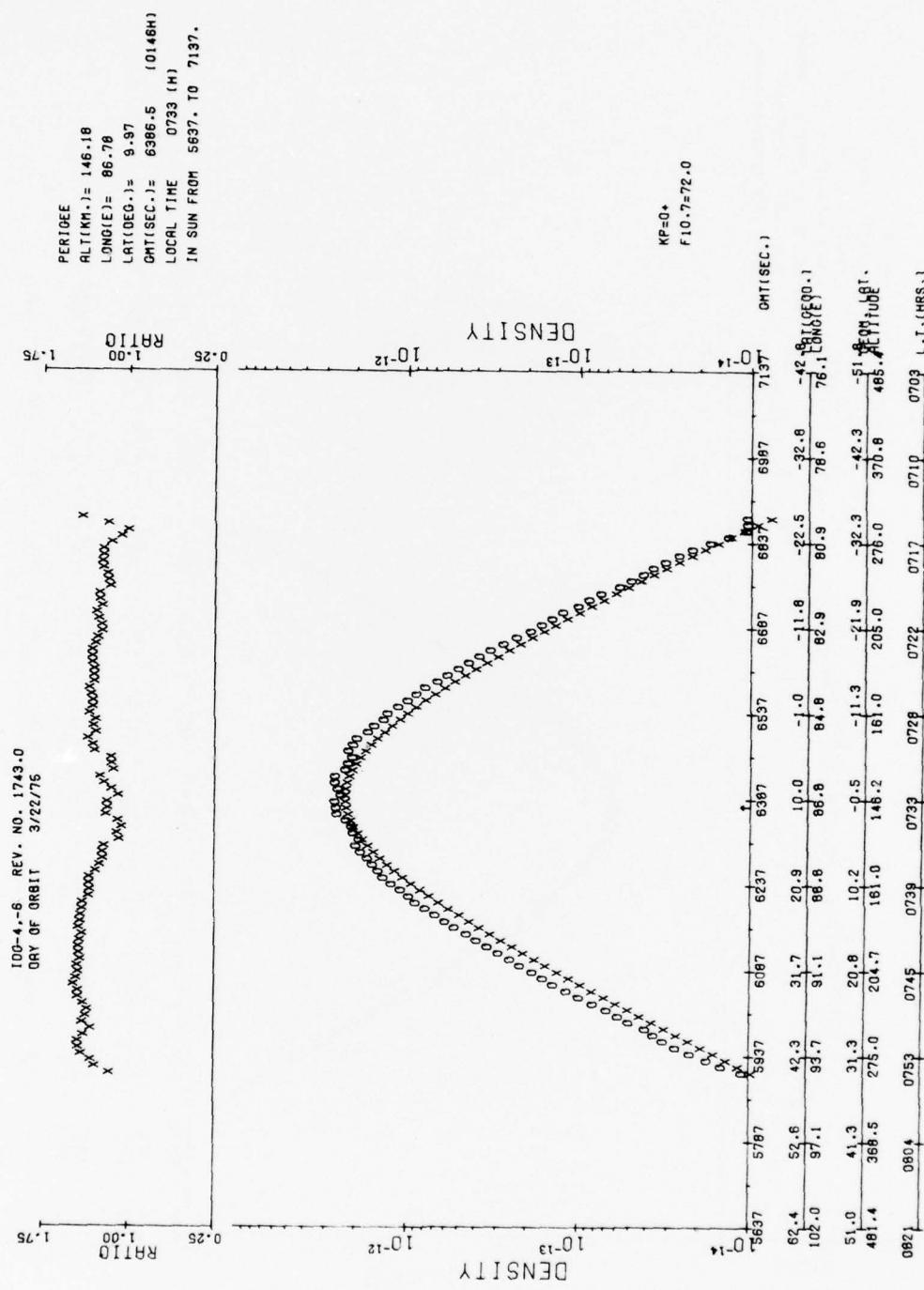
PER 40

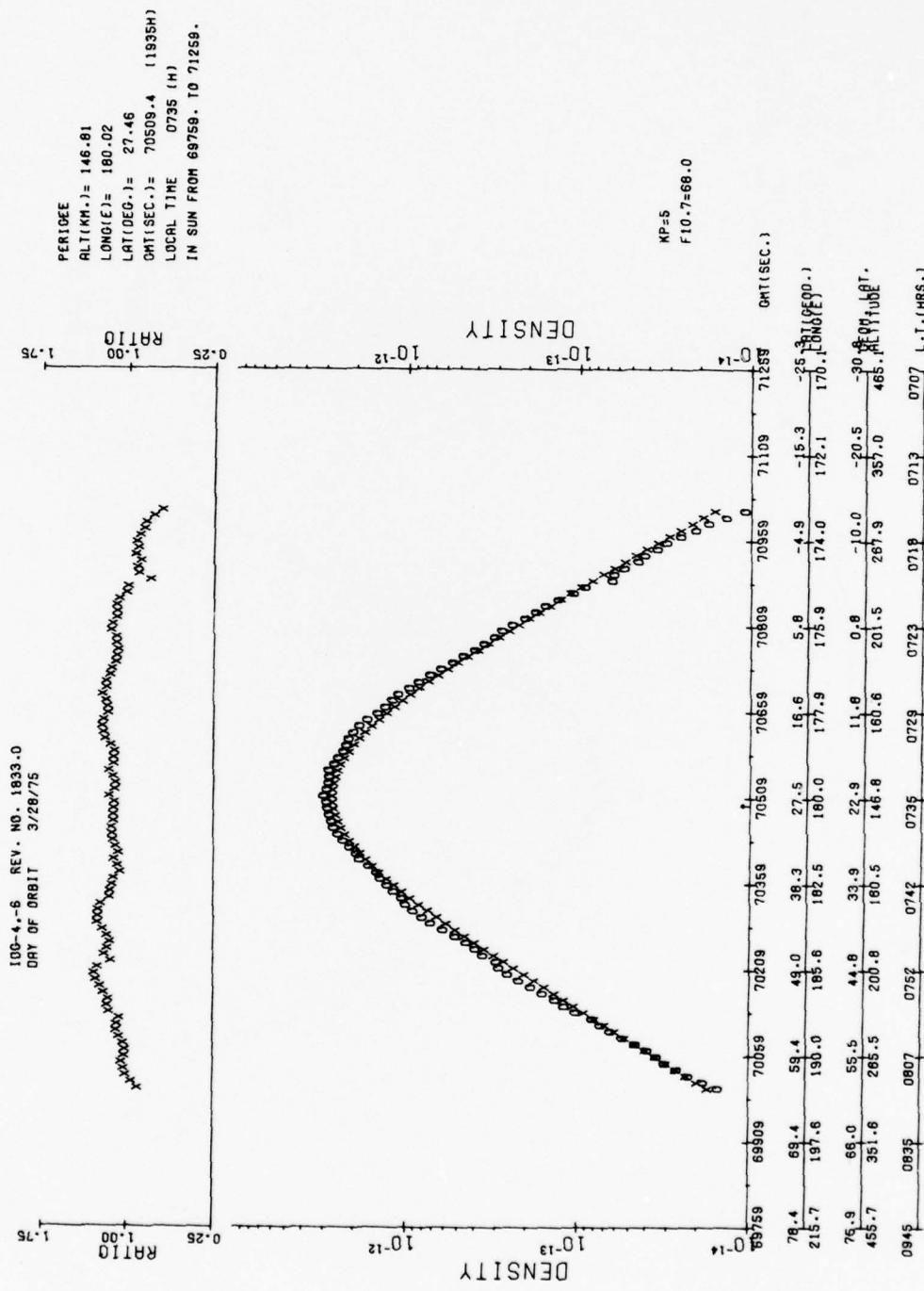




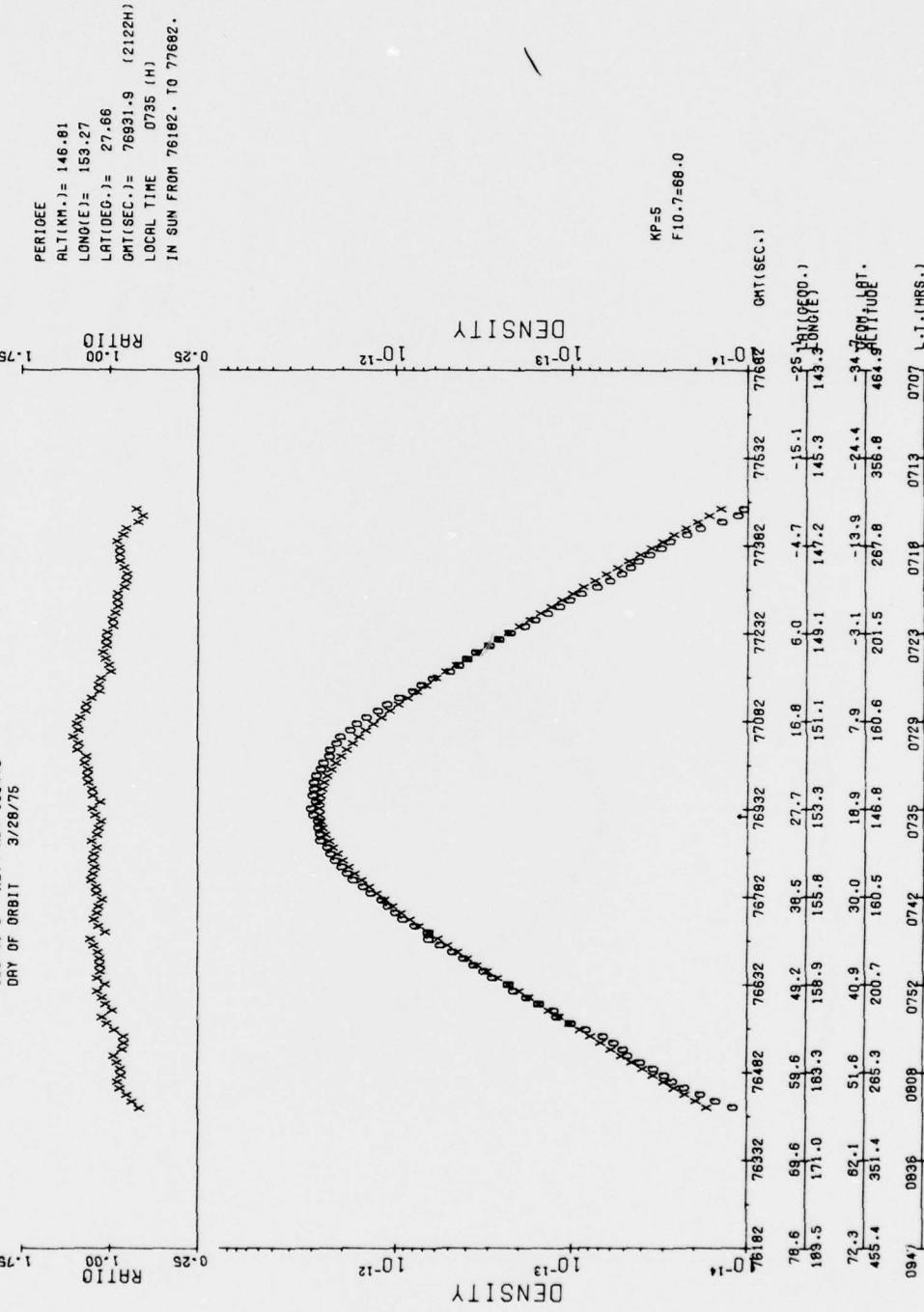
MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963

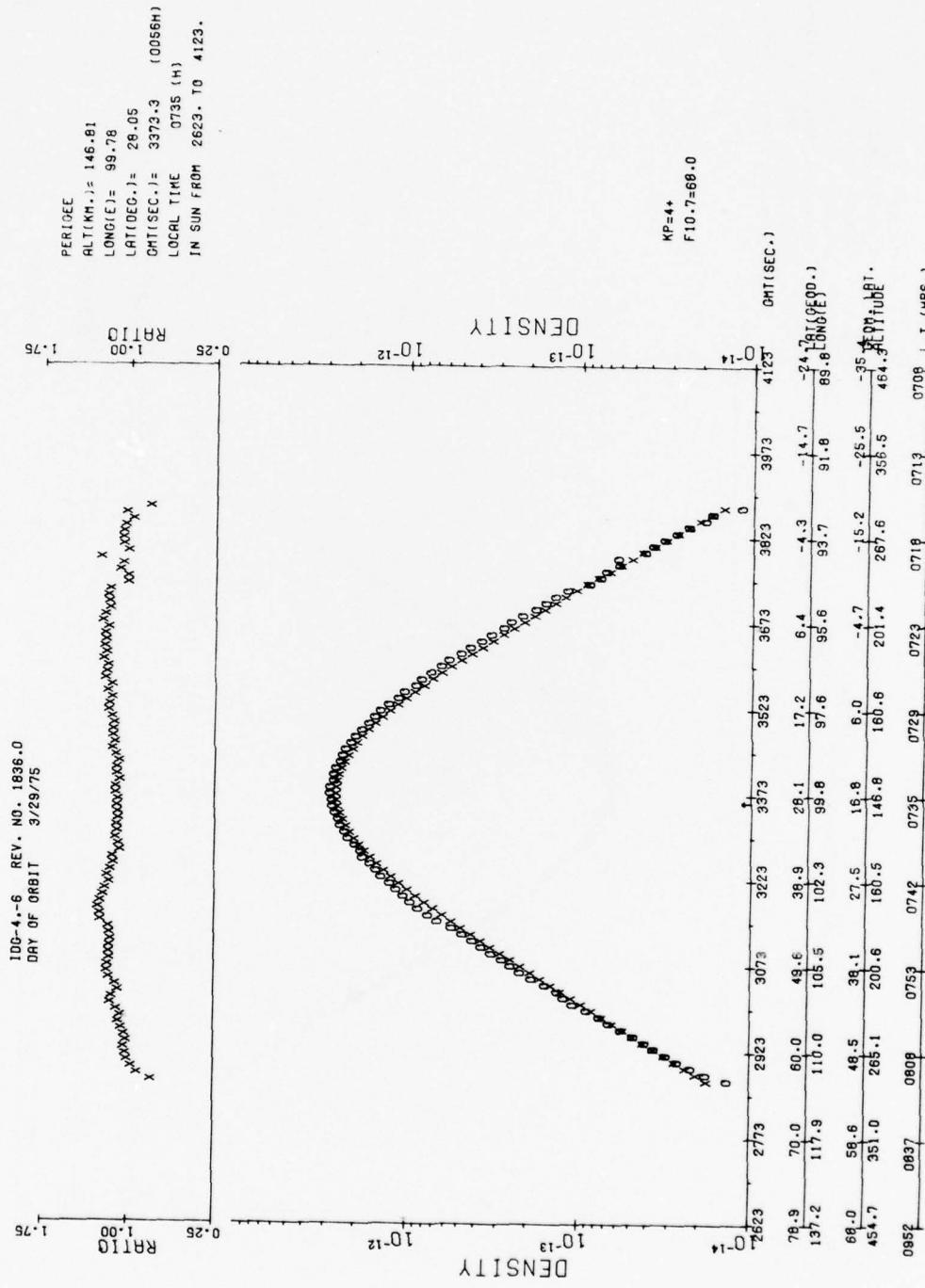


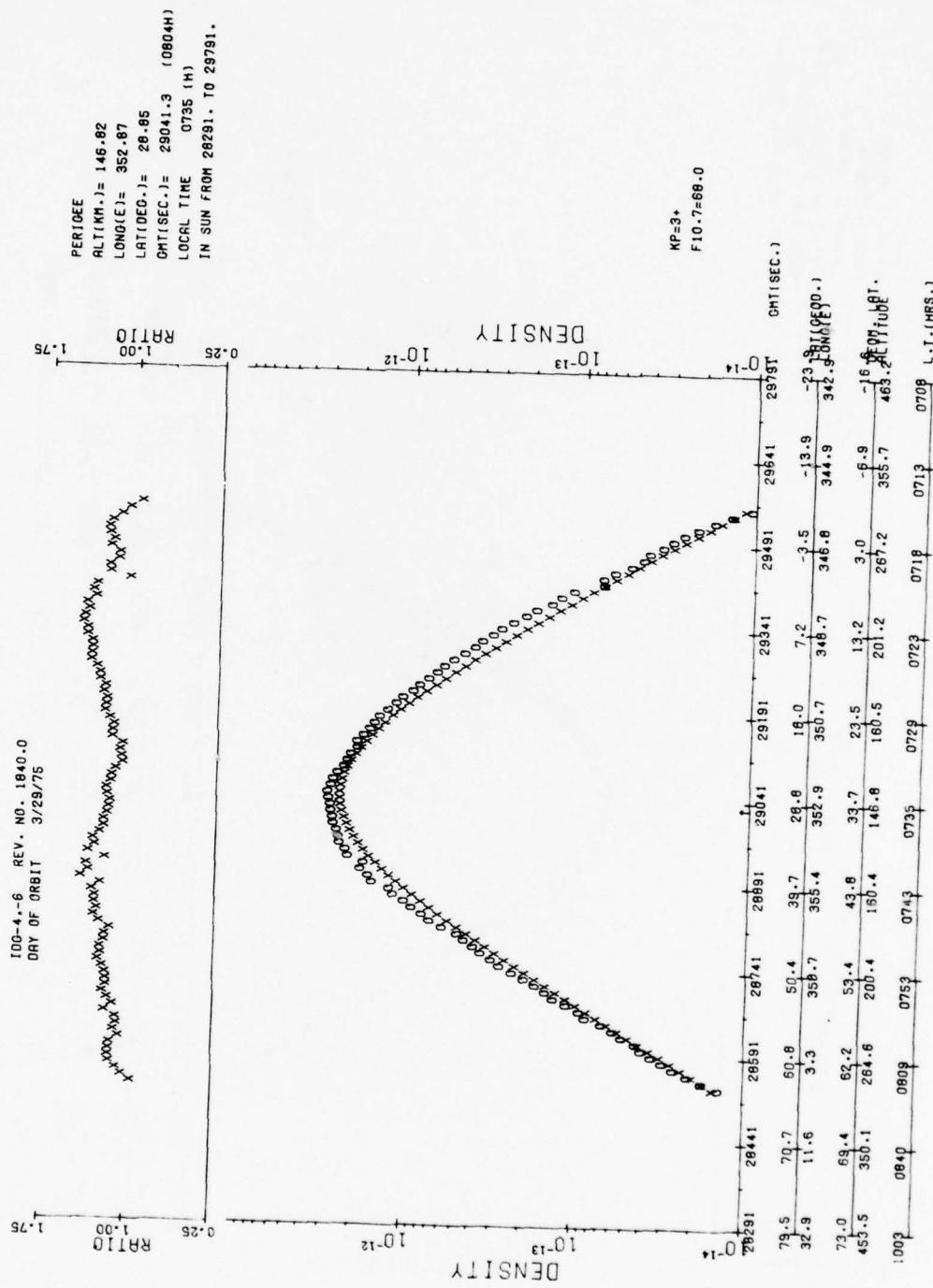




100-4-6 REV. NO. 1834.0
DAY OF ORBIT 3/28/75







IDC-4.-6 REV. NO. 1841-0
DAY OF ORBIT 3/29/75

PERIOD E

ALT (KM.) = 146.83
LONG (deg) = 326.15
LAT (DEG.) = 29.05
GHT (SEC.) = 35455.2 (0950H)
LOCAL TIME 0735 (H)
IN SUN FROM 34705. TO 36205.

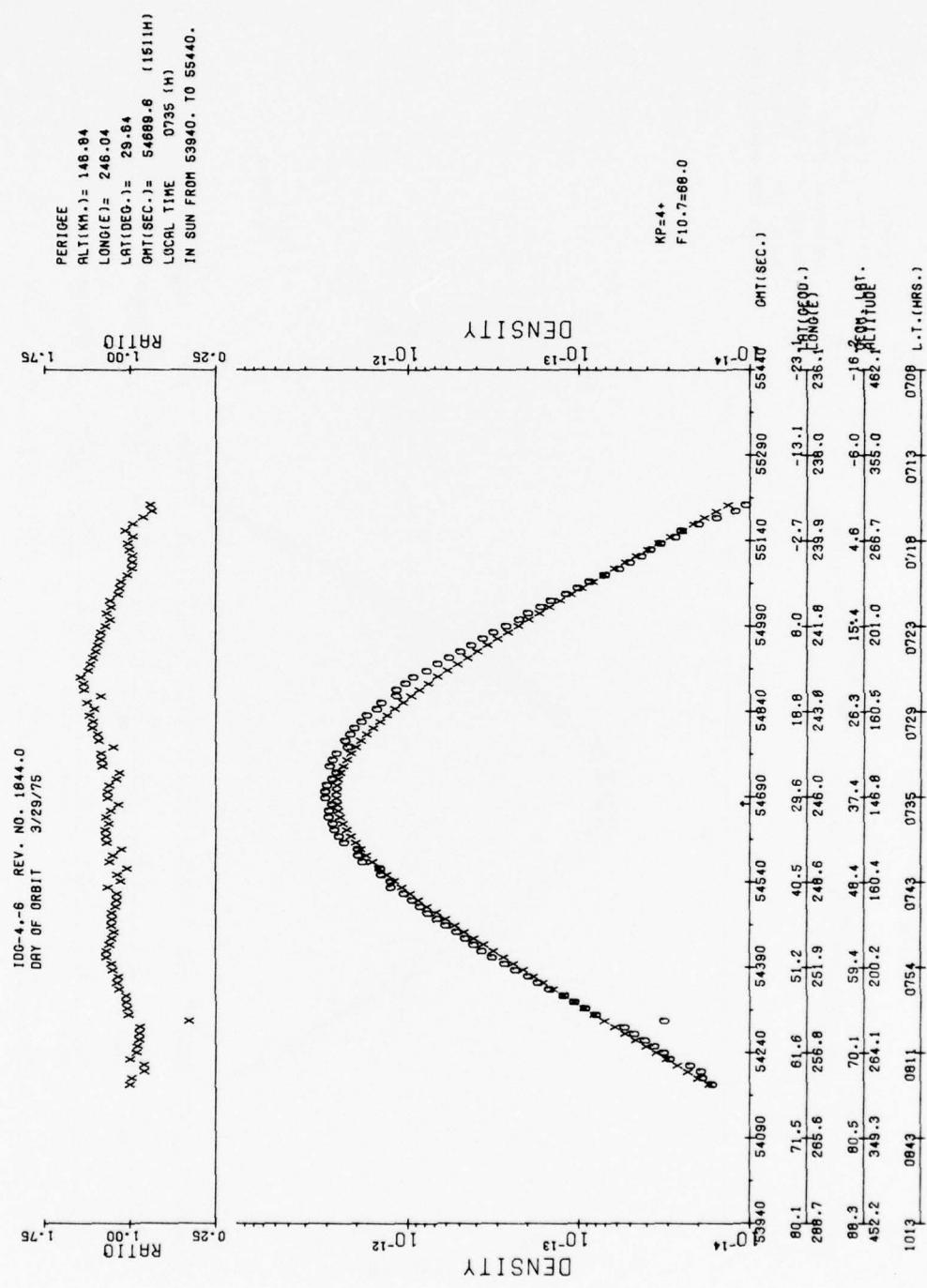
KP=3+
f10.7=68.0

DAY OF ORBIT 3/29/75

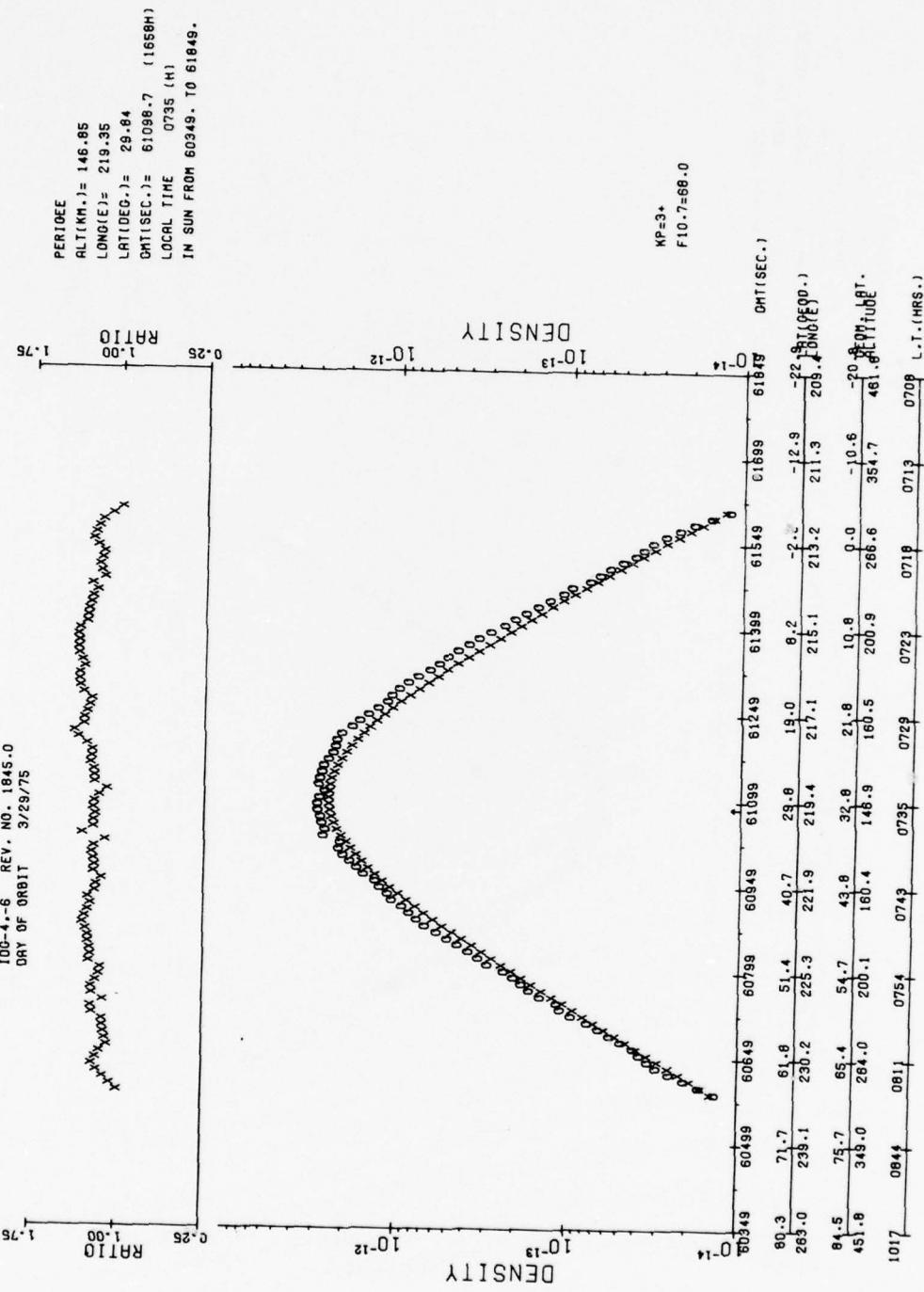
RBT10

DENSITY

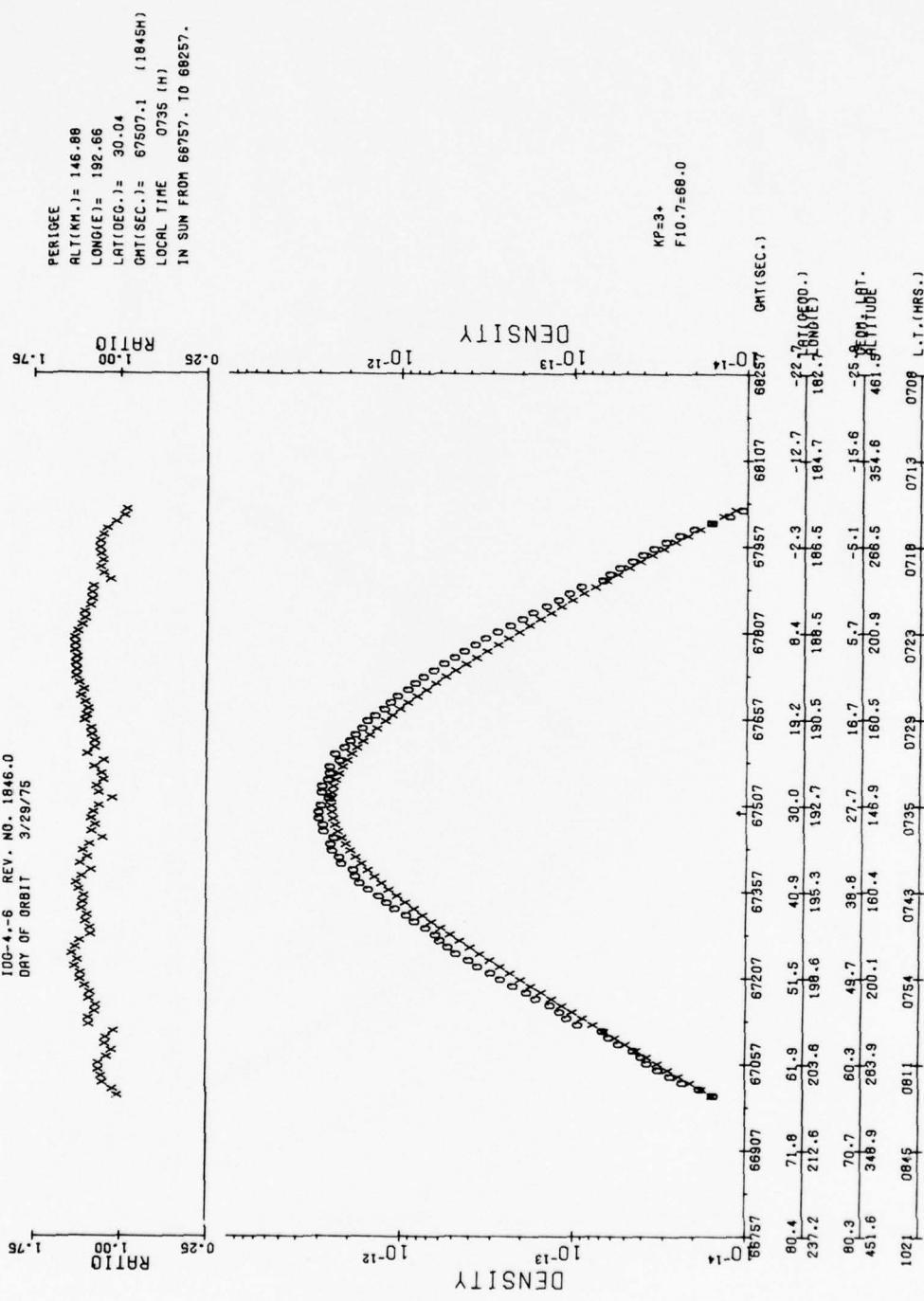
| Time (sec) | Open Circles (RBT10) | Solid Circles (RBT10) |
|------------|----------------------|-----------------------|
| 34705 | 0.25 | 0.25 |
| 34710 | 0.50 | 0.50 |
| 34715 | 1.00 | 1.00 |
| 34720 | 1.25 | 1.25 |
| 34725 | 1.50 | 1.50 |
| 34730 | 1.75 | 1.75 |
| 34735 | 1.75 | 1.75 |
| 34740 | 1.75 | 1.75 |
| 34745 | 1.75 | 1.75 |
| 34750 | 1.75 | 1.75 |
| 34755 | 1.75 | 1.75 |
| 34760 | 1.75 | 1.75 |
| 34765 | 1.75 | 1.75 |
| 34770 | 1.75 | 1.75 |
| 34775 | 1.75 | 1.75 |
| 34780 | 1.75 | 1.75 |
| 34785 | 1.75 | 1.75 |
| 34790 | 1.75 | 1.75 |
| 34795 | 1.75 | 1.75 |
| 34800 | 1.75 | 1.75 |
| 34805 | 1.75 | 1.75 |
| 34810 | 1.75 | 1.75 |
| 34815 | 1.75 | 1.75 |
| 34820 | 1.75 | 1.75 |
| 34825 | 1.75 | 1.75 |
| 34830 | 1.75 | 1.75 |
| 34835 | 1.75 | 1.75 |
| 34840 | 1.75 | 1.75 |
| 34845 | 1.75 | 1.75 |
| 34850 | 1.75 | 1.75 |
| 34855 | 1.75 | 1.75 |
| 34860 | 1.75 | 1.75 |
| 34865 | 1.75 | 1.75 |
| 34870 | 1.75 | 1.75 |
| 34875 | 1.75 | 1.75 |
| 34880 | 1.75 | 1.75 |
| 34885 | 1.75 | 1.75 |
| 34890 | 1.75 | 1.75 |
| 34895 | 1.75 | 1.75 |
| 34900 | 1.75 | 1.75 |
| 34905 | 1.75 | 1.75 |
| 34910 | 1.75 | 1.75 |
| 34915 | 1.75 | 1.75 |
| 34920 | 1.75 | 1.75 |
| 34925 | 1.75 | 1.75 |
| 34930 | 1.75 | 1.75 |
| 34935 | 1.75 | 1.75 |
| 34940 | 1.75 | 1.75 |
| 34945 | 1.75 | 1.75 |
| 34950 | 1.75 | 1.75 |
| 34955 | 1.75 | 1.75 |
| 34960 | 1.75 | 1.75 |
| 34965 | 1.75 | 1.75 |
| 34970 | 1.75 | 1.75 |
| 34975 | 1.75 | 1.75 |
| 34980 | 1.75 | 1.75 |
| 34985 | 1.75 | 1.75 |
| 34990 | 1.75 | 1.75 |
| 34995 | 1.75 | 1.75 |
| 35000 | 1.75 | 1.75 |
| 35005 | 1.75 | 1.75 |
| 35010 | 1.75 | 1.75 |
| 35015 | 1.75 | 1.75 |
| 35020 | 1.75 | 1.75 |
| 35025 | 1.75 | 1.75 |
| 35030 | 1.75 | 1.75 |
| 35035 | 1.75 | 1.75 |
| 35040 | 1.75 | 1.75 |
| 35045 | 1.75 | 1.75 |
| 35050 | 1.75 | 1.75 |
| 35055 | 1.75 | 1.75 |
| 35060 | 1.75 | 1.75 |
| 35065 | 1.75 | 1.75 |
| 35070 | 1.75 | 1.75 |
| 35075 | 1.75 | 1.75 |
| 35080 | 1.75 | 1.75 |
| 35085 | 1.75 | 1.75 |
| 35090 | 1.75 | 1.75 |
| 35095 | 1.75 | 1.75 |
| 35100 | 1.75 | 1.75 |
| 35105 | 1.75 | 1.75 |
| 35110 | 1.75 | 1.75 |
| 35115 | 1.75 | 1.75 |
| 35120 | 1.75 | 1.75 |
| 35125 | 1.75 | 1.75 |
| 35130 | 1.75 | 1.75 |
| 35135 | 1.75 | 1.75 |
| 35140 | 1.75 | 1.75 |
| 35145 | 1.75 | 1.75 |
| 35150 | 1.75 | 1.75 |
| 35155 | 1.75 | 1.75 |
| 35160 | 1.75 | 1.75 |
| 35165 | 1.75 | 1.75 |
| 35170 | 1.75 | 1.75 |
| 35175 | 1.75 | 1.75 |
| 35180 | 1.75 | 1.75 |
| 35185 | 1.75 | 1.75 |
| 35190 | 1.75 | 1.75 |
| 35195 | 1.75 | 1.75 |
| 35200 | 1.75 | 1.75 |
| 35205 | 1.75 | 1.75 |
| 35210 | 1.75 | 1.75 |
| 35215 | 1.75 | 1.75 |
| 35220 | 1.75 | 1.75 |
| 35225 | 1.75 | 1.75 |
| 35230 | 1.75 | 1.75 |
| 35235 | 1.75 | 1.75 |
| 35240 | 1.75 | 1.75 |
| 35245 | 1.75 | 1.75 |
| 35250 | 1.75 | 1.75 |
| 35255 | 1.75 | 1.75 |
| 35260 | 1.75 | 1.75 |
| 35265 | 1.75 | 1.75 |
| 35270 | 1.75 | 1.75 |
| 35275 | 1.75 | 1.75 |
| 35280 | 1.75 | 1.75 |
| 35285 | 1.75 | 1.75 |
| 35290 | 1.75 | 1.75 |
| 35295 | 1.75 | 1.75 |
| 35300 | 1.75 | 1.75 |
| 35305 | 1.75 | 1.75 |
| 35310 | 1.75 | 1.75 |
| 35315 | 1.75 | 1.75 |
| 35320 | 1.75 | 1.75 |
| 35325 | 1.75 | 1.75 |
| 35330 | 1.75 | 1.75 |
| 35335 | 1.75 | 1.75 |
| 35340 | 1.75 | 1.75 |
| 35345 | 1.75 | 1.75 |
| 35350 | 1.75 | 1.75 |
| 35355 | 1.75 | 1.75 |
| 35360 | 1.75 | 1.75 |
| 35365 | 1.75 | 1.75 |
| 35370 | 1.75 | 1.75 |
| 35375 | 1.75 | 1.75 |
| 35380 | 1.75 | 1.75 |
| 35385 | 1.75 | 1.75 |
| 35390 | 1.75 | 1.75 |
| 35395 | 1.75 | 1.75 |
| 35400 | 1.75 | 1.75 |
| 35405 | 1.75 | 1.75 |
| 35410 | 1.75 | 1.75 |
| 35415 | 1.75 | 1.75 |
| 35420 | 1.75 | 1.75 |
| 35425 | 1.75 | 1.75 |
| 35430 | 1.75 | 1.75 |
| 35435 | 1.75 | 1.75 |
| 35440 | 1.75 | 1.75 |
| 35445 | 1.75 | 1.75 |
| 35450 | 1.75 | 1.75 |
| 35455 | 1.75 | 1.75 |
| 35460 | 1.75 | 1.75 |
| 35465 | 1.75 | 1.75 |
| 35470 | 1.75 | 1.75 |
| 35475 | 1.75 | 1.75 |
| 35480 | 1.75 | 1.75 |
| 35485 | 1.75 | 1.75 |
| 35490 | 1.75 | 1.75 |
| 35495 | 1.75 | 1.75 |
| 35500 | 1.75 | 1.75 |
| 35505 | 1.75 | 1.75 |
| 35510 | 1.75 | 1.75 |
| 35515 | 1.75 | 1.75 |
| 35520 | 1.75 | 1.75 |
| 35525 | 1.75 | 1.75 |
| 35530 | 1.75 | 1.75 |
| 35535 | 1.75 | 1.75 |
| 35540 | 1.75 | 1.75 |
| 35545 | 1.75 | 1.75 |
| 35550 | 1.75 | 1.75 |
| 35555 | 1.75 | 1.75 |
| 35560 | 1.75 | 1.75 |
| 35565 | 1.75 | 1.75 |
| 35570 | 1.75 | 1.75 |
| 35575 | 1.75 | 1.75 |
| 35580 | 1.75 | 1.75 |
| 35585 | 1.75 | 1.75 |
| 35590 | 1.75 | 1.75 |
| 35595 | 1.75 | 1.75 |
| 35600 | 1.75 | 1.75 |
| 35605 | 1.75 | 1.75 |
| 35610 | 1.75 | 1.75 |
| 35615 | 1.75 | 1.75 |
| 35620 | 1.75 | 1.75 |
| 35625 | 1.75 | 1.75 |
| 35630 | 1.75 | 1.75 |
| 35635 | 1.75 | 1.75 |
| 35640 | 1.75 | 1.75 |
| 35645 | 1.75 | 1.75 |
| 35650 | 1.75 | 1.75 |
| 35655 | 1.75 | 1.75 |
| 35660 | 1.75 | 1.75 |
| 35665 | 1.75 | 1.75 |
| 35670 | 1.75 | 1.75 |
| 35675 | 1.75 | 1.75 |
| 35680 | 1.75 | 1.75 |
| 35685 | 1.75 | 1.75 |
| 35690 | 1.75 | 1.75 |
| 35695 | 1.75 | 1.75 |
| 35700 | 1.75 | 1.75 |
| 35705 | 1.75 | 1.75 |
| 35710 | 1.75 | 1.75 |
| 35715 | 1.75 | 1.75 |
| 35720 | 1.75 | 1.75 |
| 35725 | 1.75 | 1.75 |
| 35730 | 1.75 | 1.75 |
| 35735 | 1.75 | 1.75 |
| 35740 | 1.75 | 1.75 |
| 35745 | 1.75 | 1.75 |
| 35750 | 1.75 | 1.75 |
| 35755 | 1.75 | 1.75 |
| 35760 | 1.75 | 1.75 |
| 35765 | 1.75 | 1.75 |
| 35770 | 1.75 | 1.75 |
| 35775 | 1.75 | 1.75 |
| 35780 | 1.75 | 1.75 |
| 35785 | 1.75 | 1.75 |
| 35790 | 1.75 | 1.75 |
| 35795 | 1.75 | 1.75 |
| 35800 | 1.75 | 1.75 |
| 35805 | 1.75 | 1.75 |
| 35810 | 1.75 | 1.75 |
| 35815 | 1.75 | 1.75 |
| 35820 | 1.75 | 1.75 |
| 35825 | 1.75 | 1.75 |
| 35830 | 1.75 | 1.75 |
| 35835 | 1.75 | 1.75 |
| 35840 | 1.75 | 1.75 |
| 35845 | 1.75 | 1.75 |
| 35850 | 1.75 | 1.75 |
| 35855 | 1.75 | 1.75 |
| 35860 | 1.75 | 1.75 |
| 35865 | 1.75 | 1.75 |
| 35870 | 1.75 | 1.75 |
| 35875 | 1.75 | 1.75 |
| 35880 | 1.75 | 1.75 |
| 35885 | 1.75 | 1.75 |
| 35890 | 1.75 | 1.75 |
| 35895 | 1.75 | 1.75 |
| 35900 | 1.75 | 1.75 |
| 35905 | 1.75 | 1.75 |
| 35910 | 1.75 | 1.75 |
| 35915 | 1.75 | 1.75 |
| 35920 | 1.75 | 1.75 |
| 35925 | 1.75 | 1.75 |
| 35930 | 1.75 | 1.75 |
| 35935 | 1.75 | 1.75 |
| 35940 | 1.75 | 1.75 |
| 35945 | 1.75 | 1.75 |
| 35950 | 1.75 | 1.75 |
| 35955 | 1.75 | 1.75 |
| 35960 | 1.75 | 1.75 |
| 35965 | 1.75 | 1.75 |
| 35970 | 1.75 | 1.75 |
| 35975 | 1.75 | 1.75 |
| 35980 | 1.75 | 1.75 |
| 35985 | 1.75 | 1.75 |
| 35990 | 1.75 | 1.75 |
| 35995 | 1.75 | 1.75 |
| 36000 | 1.75 | 1.75 |



IOC-4.-6 REV. NO. 1845.0
DAY OF ORBIT 3/29/75

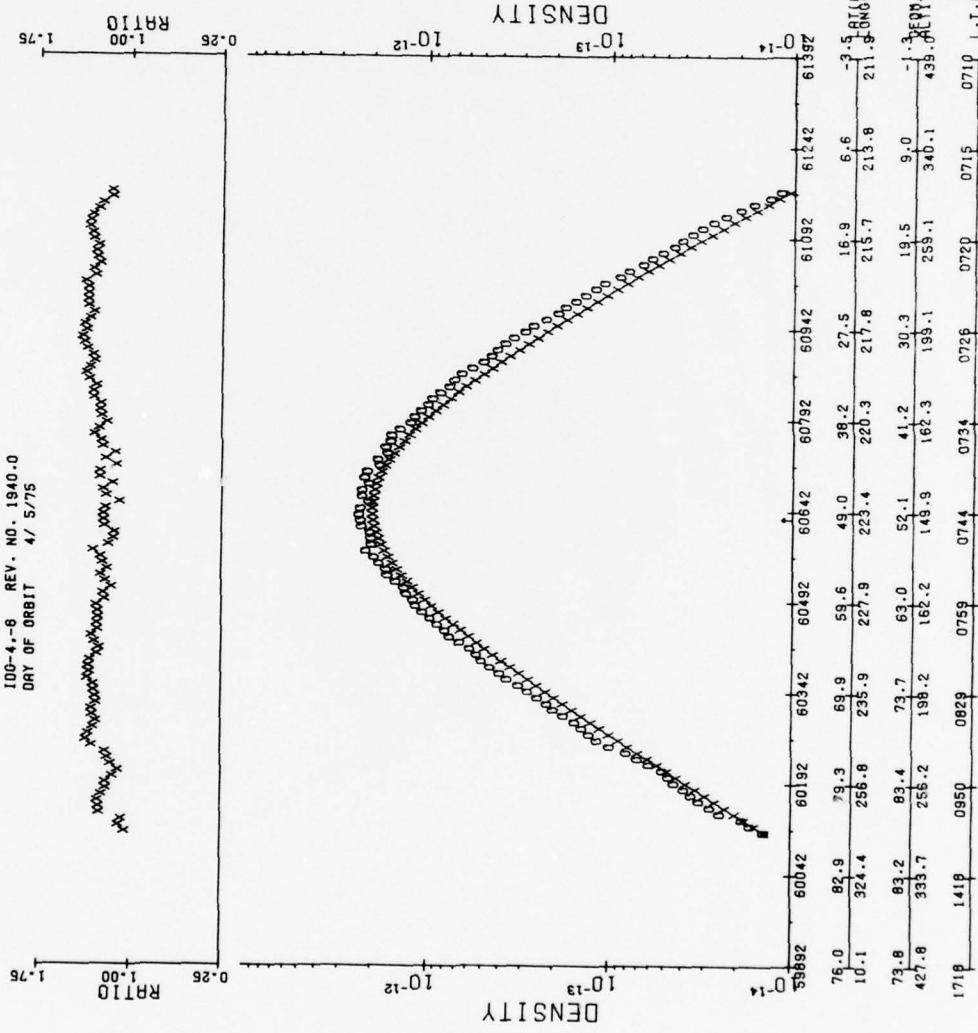


10G-4.-6 REV. NO. 1846.0
DAY OF ORBIT 3/29/75

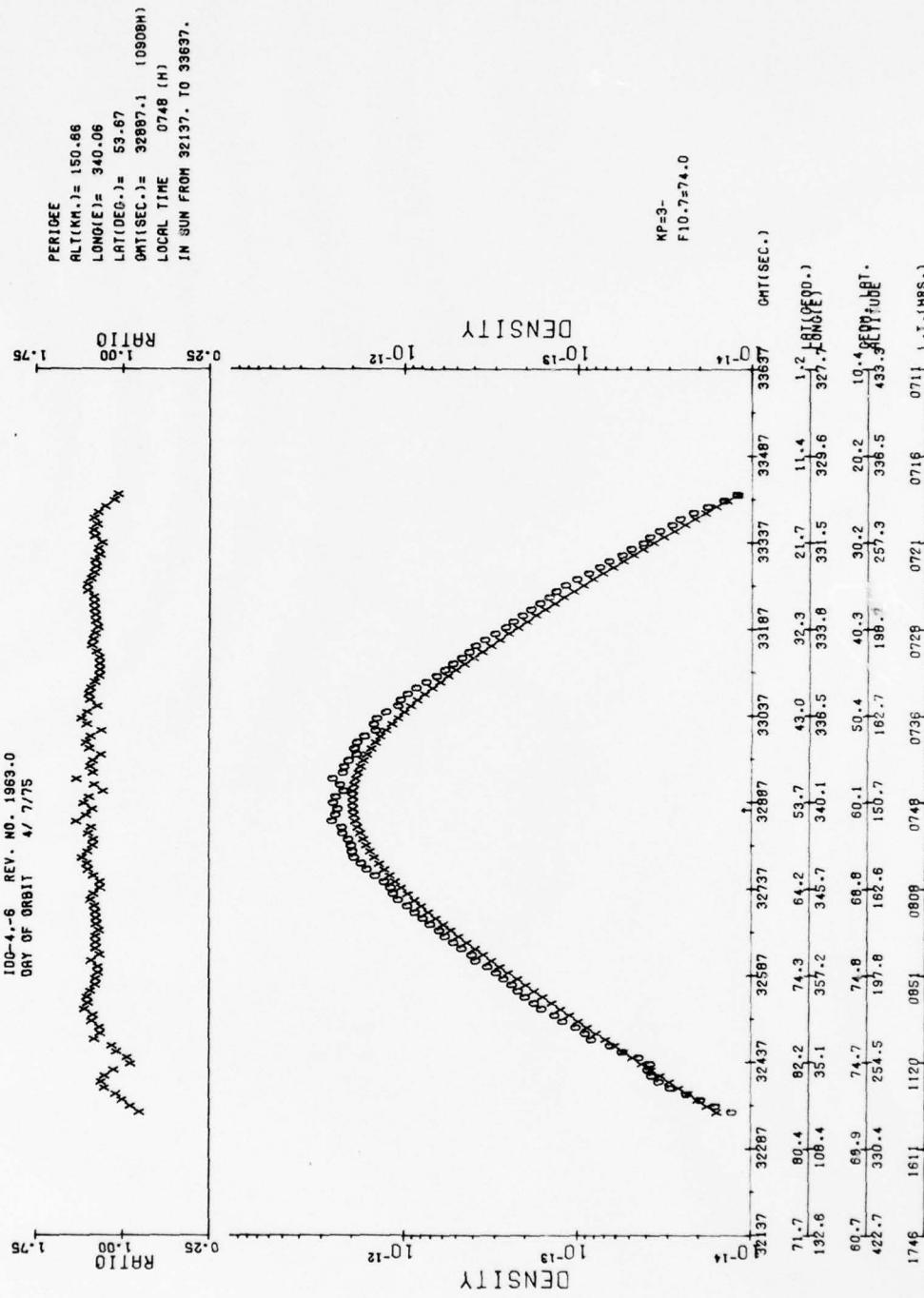


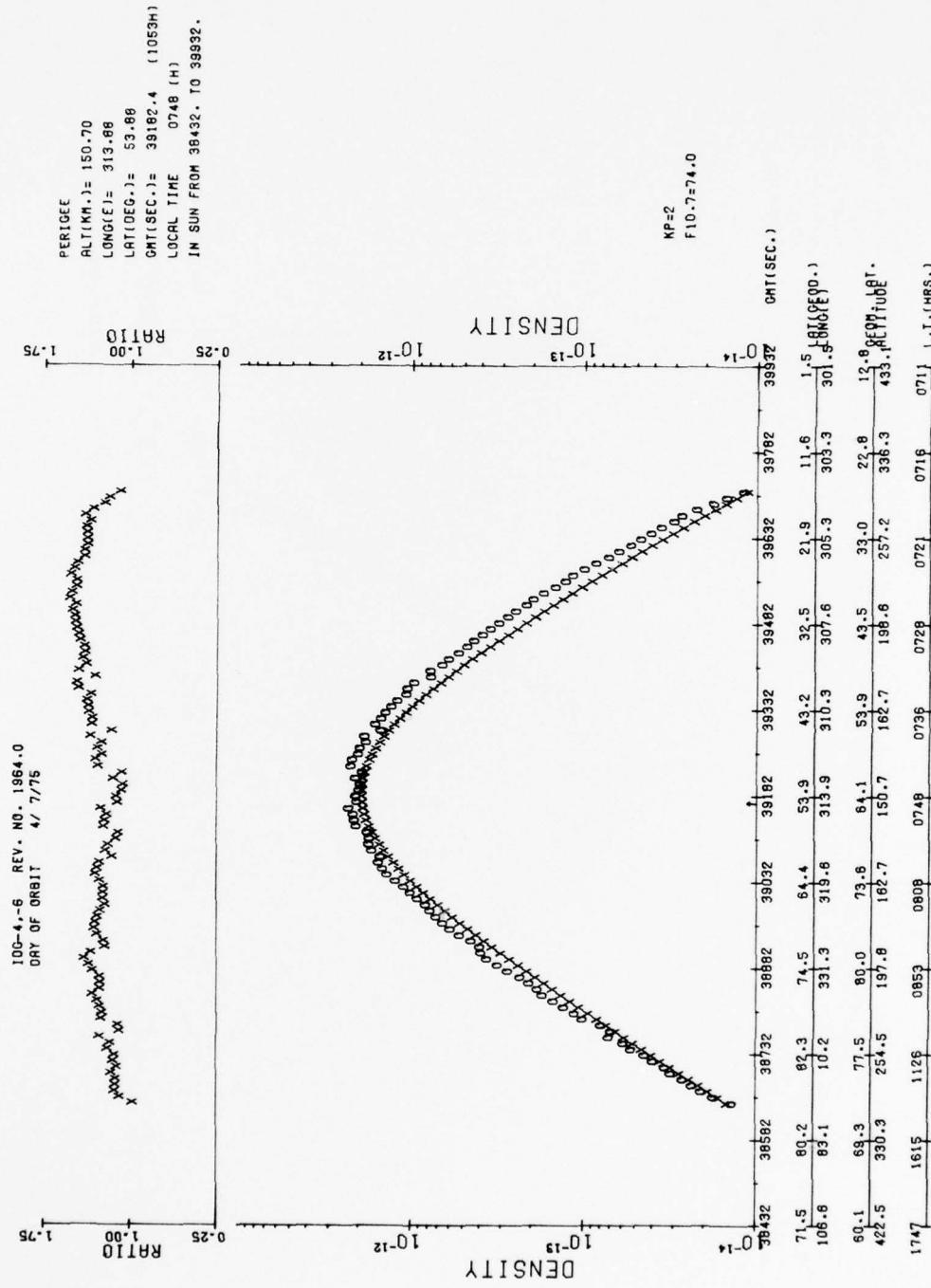
100-4-8 REV. NO. 1940-0
DAY OF ORBIT 4/ 5/75

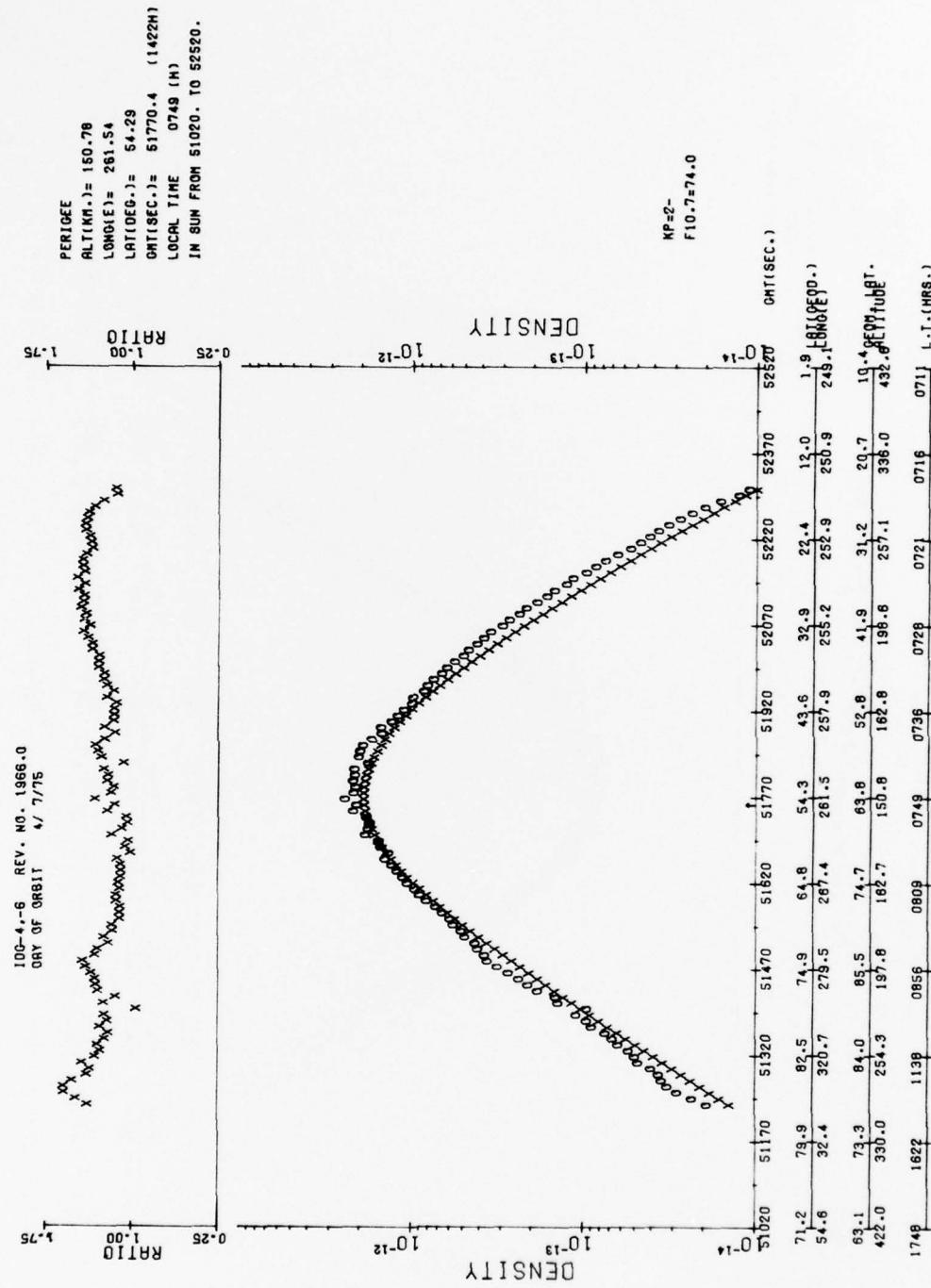
PERIGEE
ALT(MM)= 149.91
LONG(E)= 223.36
LAT(DEG.)= 48.99
GMT(SEC.)= 60642.0 (1650H)
LOCAL TIME 0744 (H)
IN SUN FROM 58892. TO 61392.

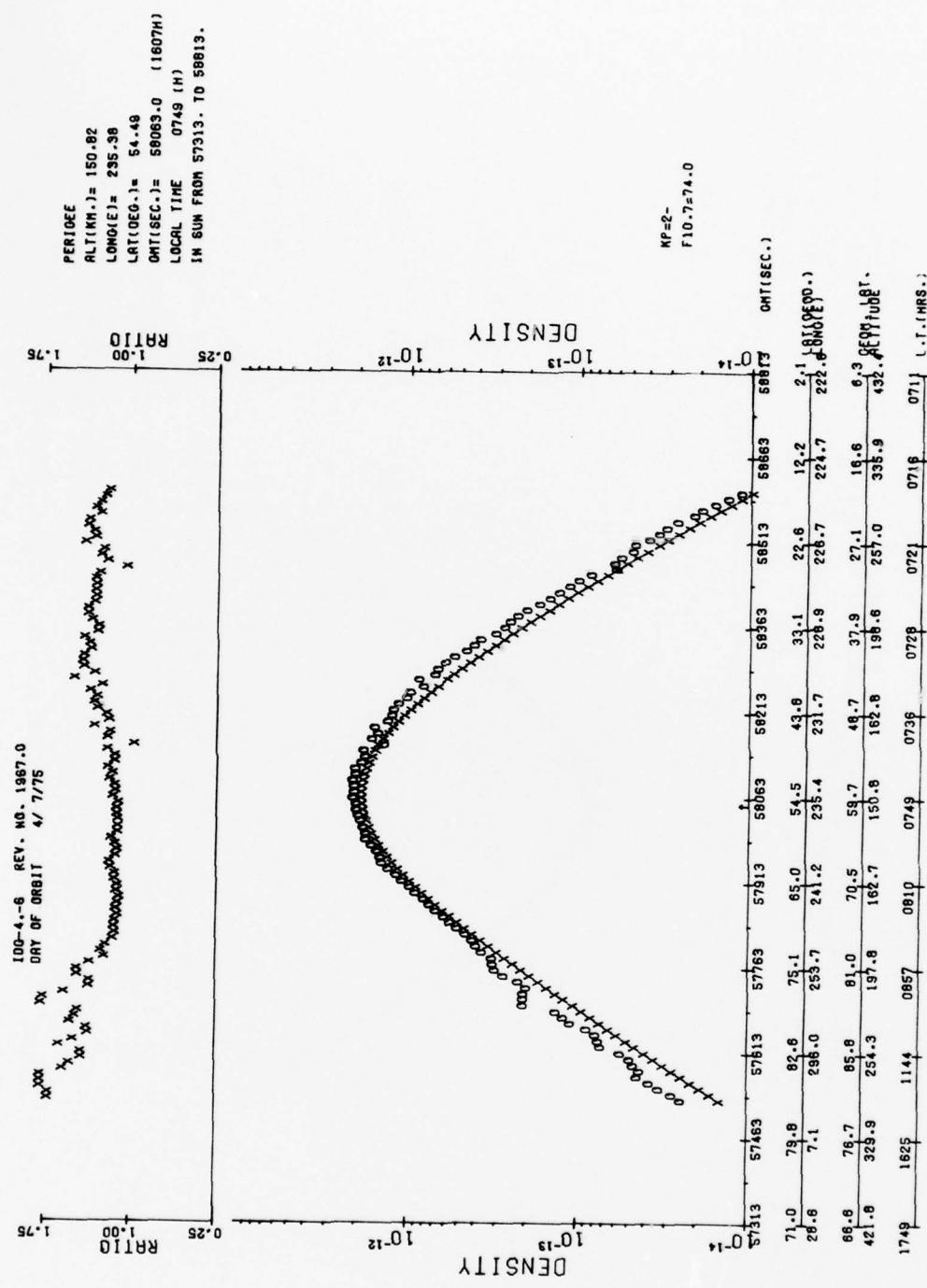


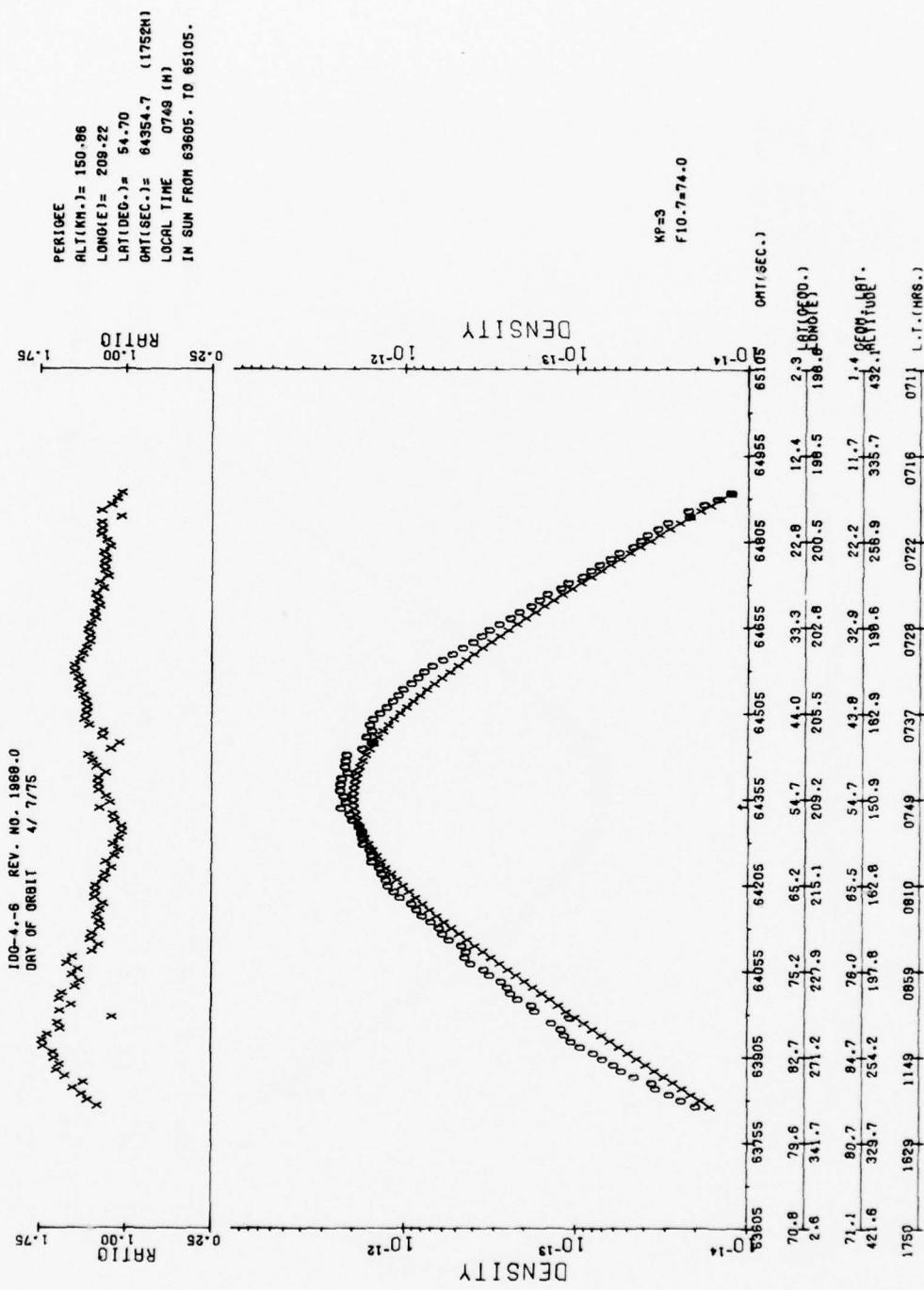
100-4,-6 REV. NO. 1963-0
DAY OF ORBIT 4 / 7/75

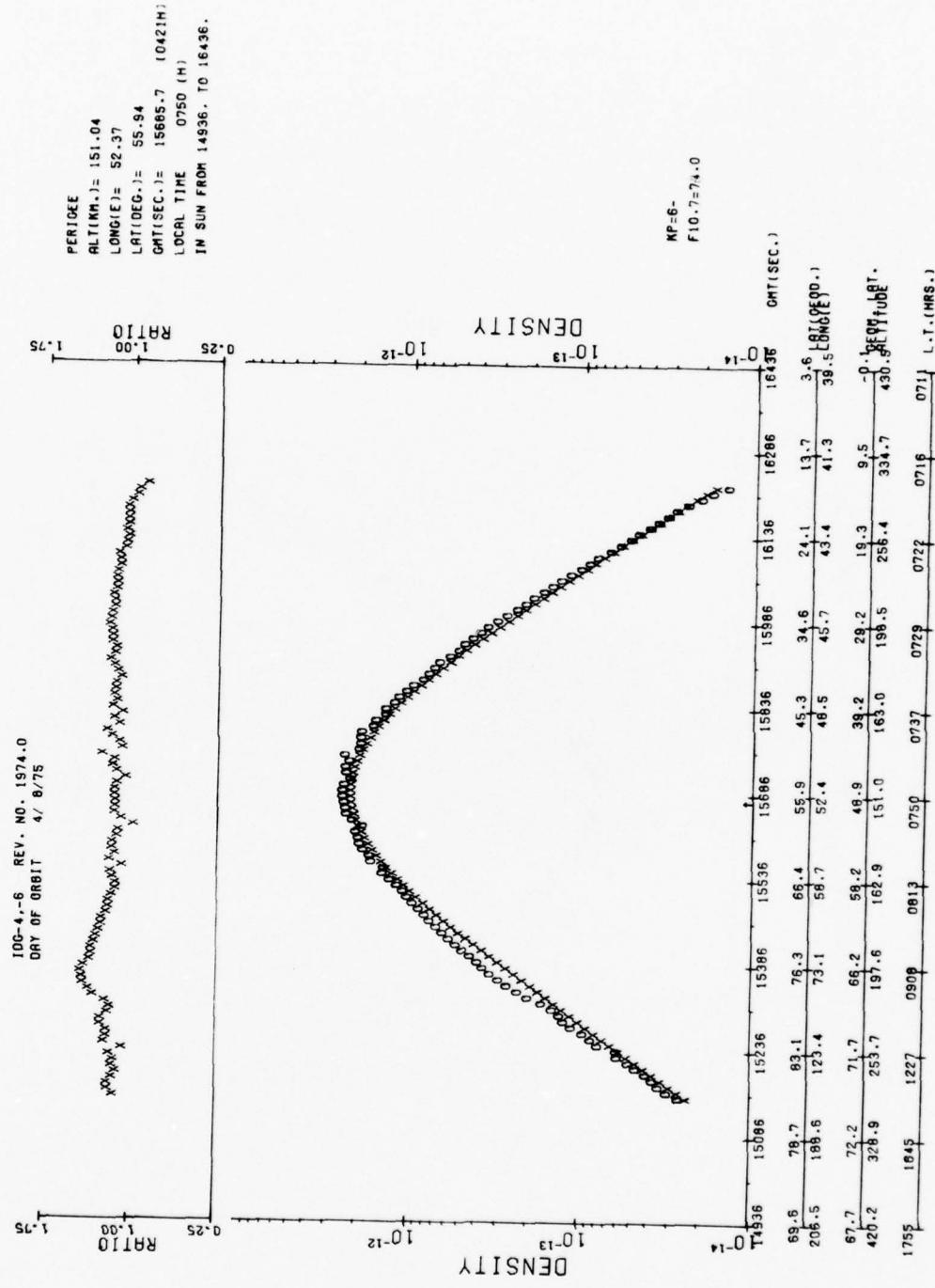


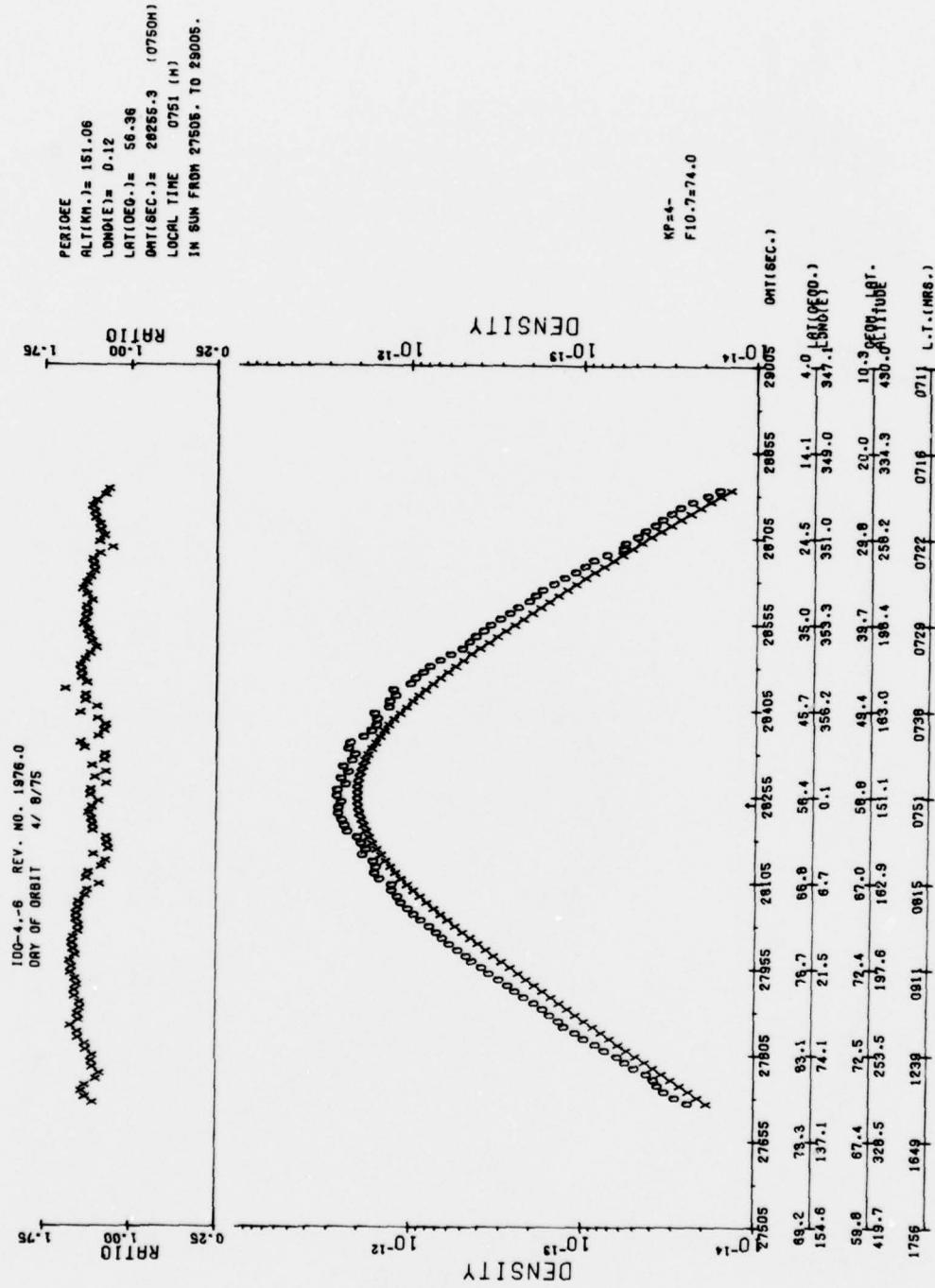


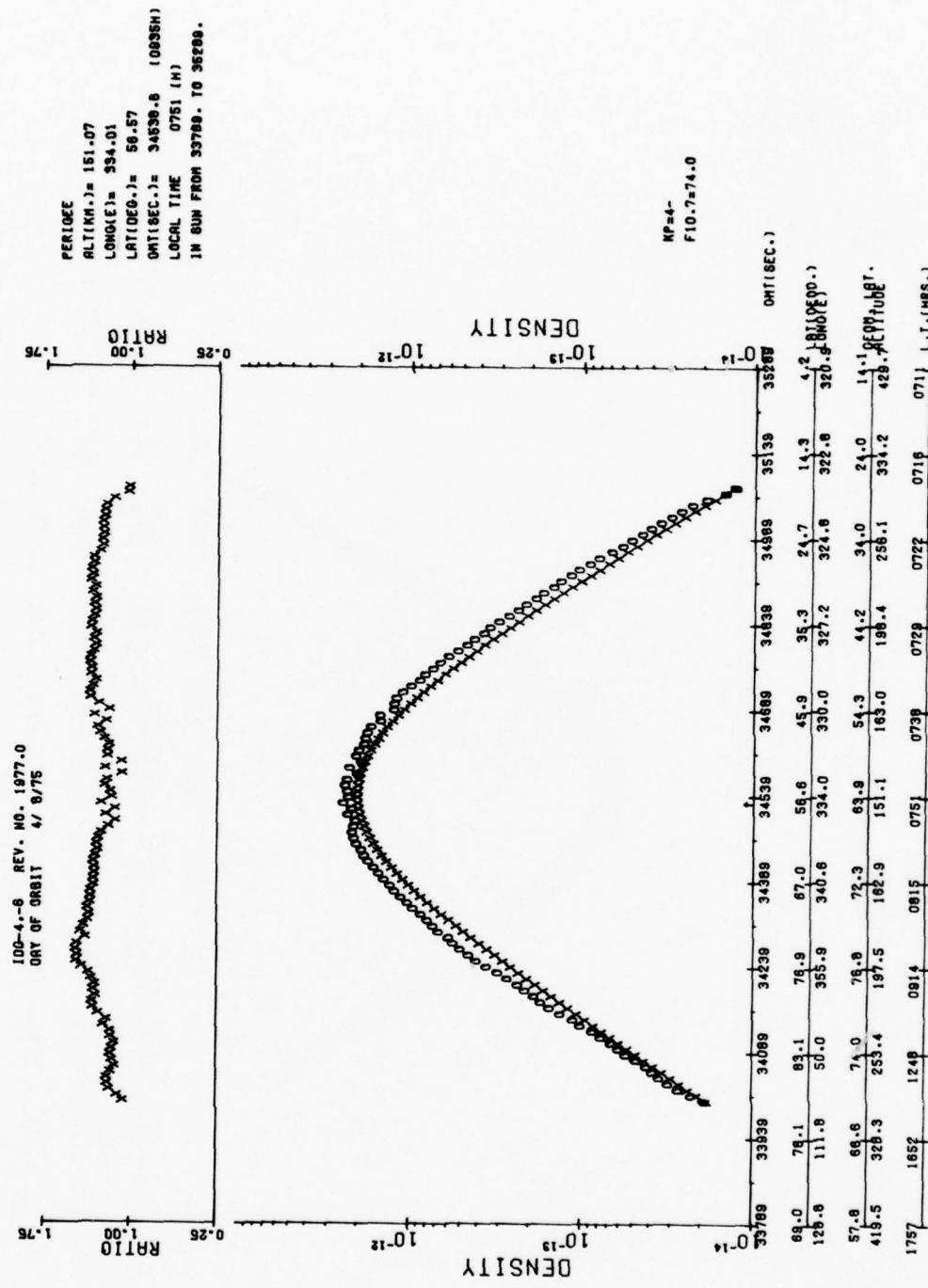


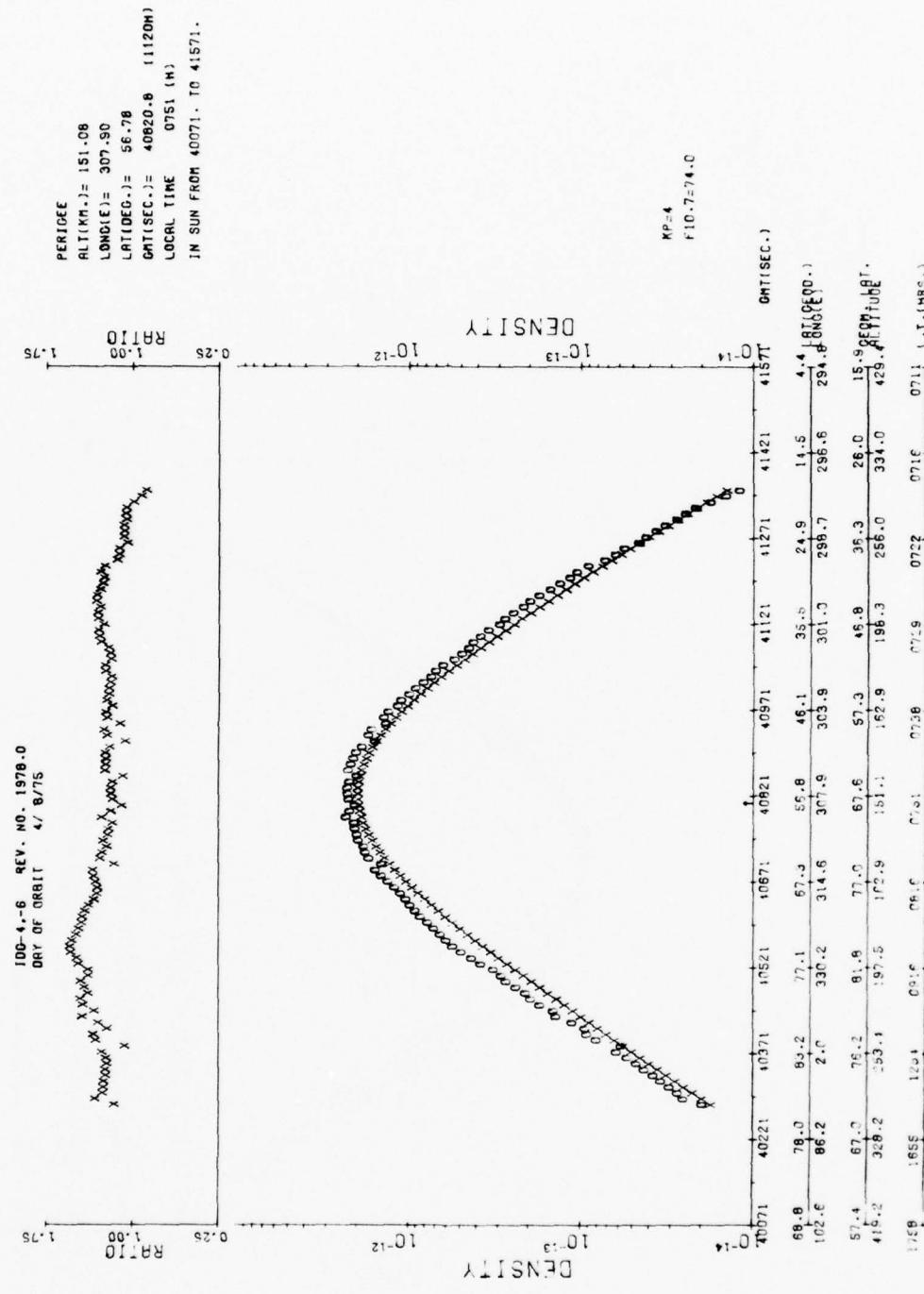


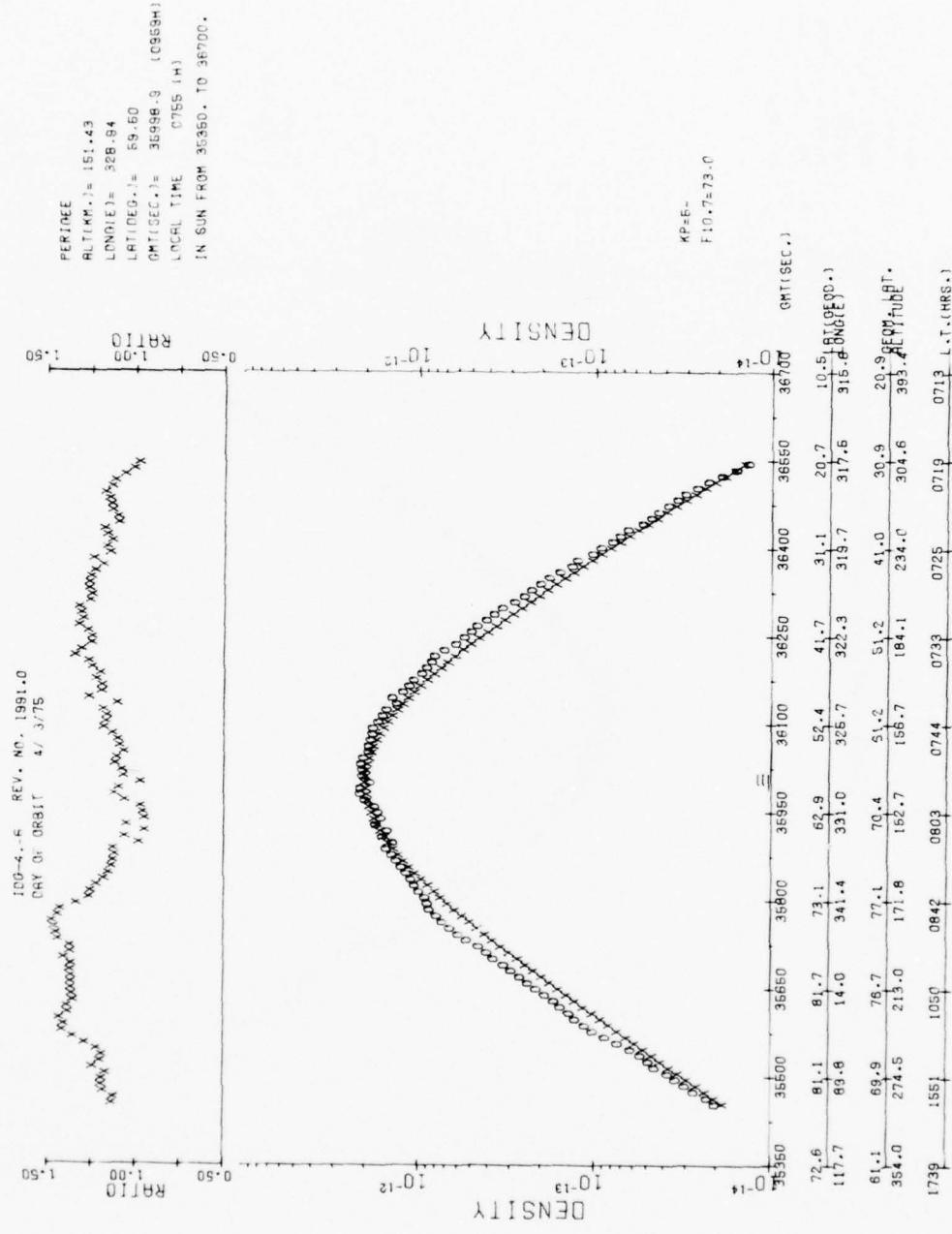






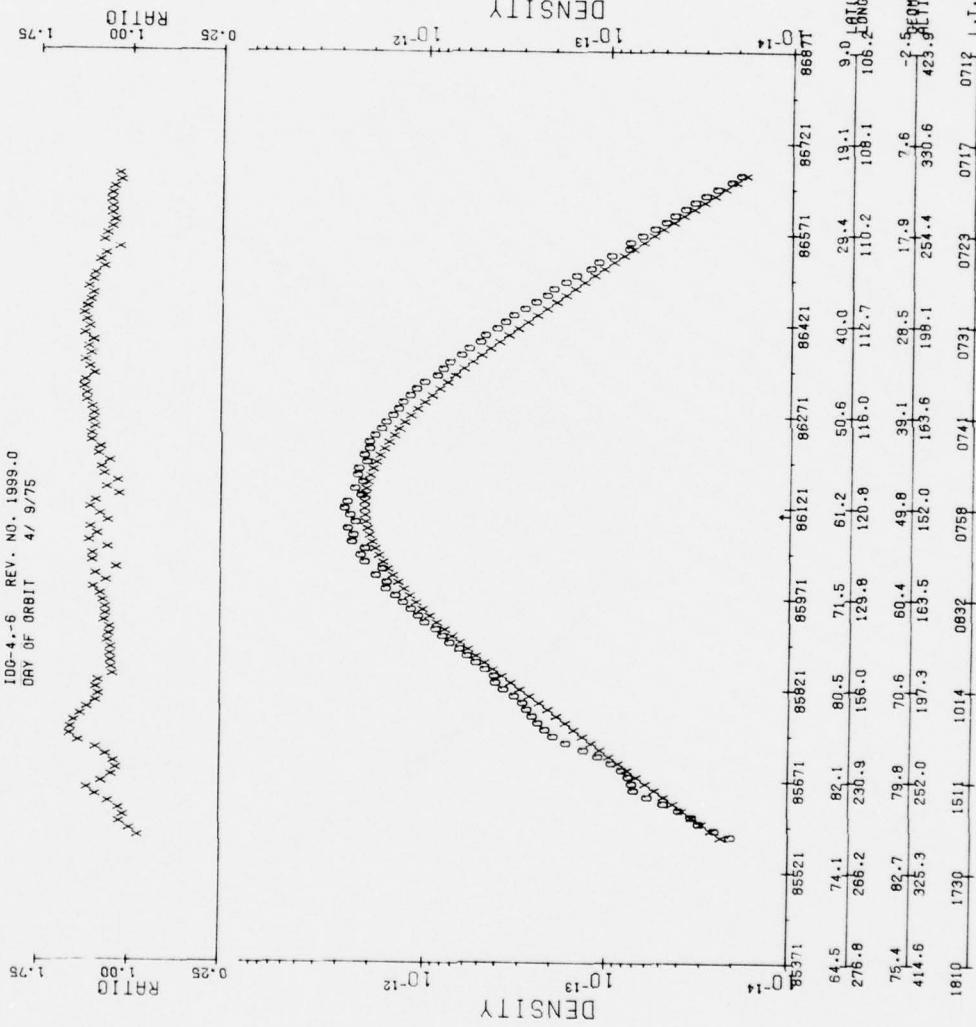


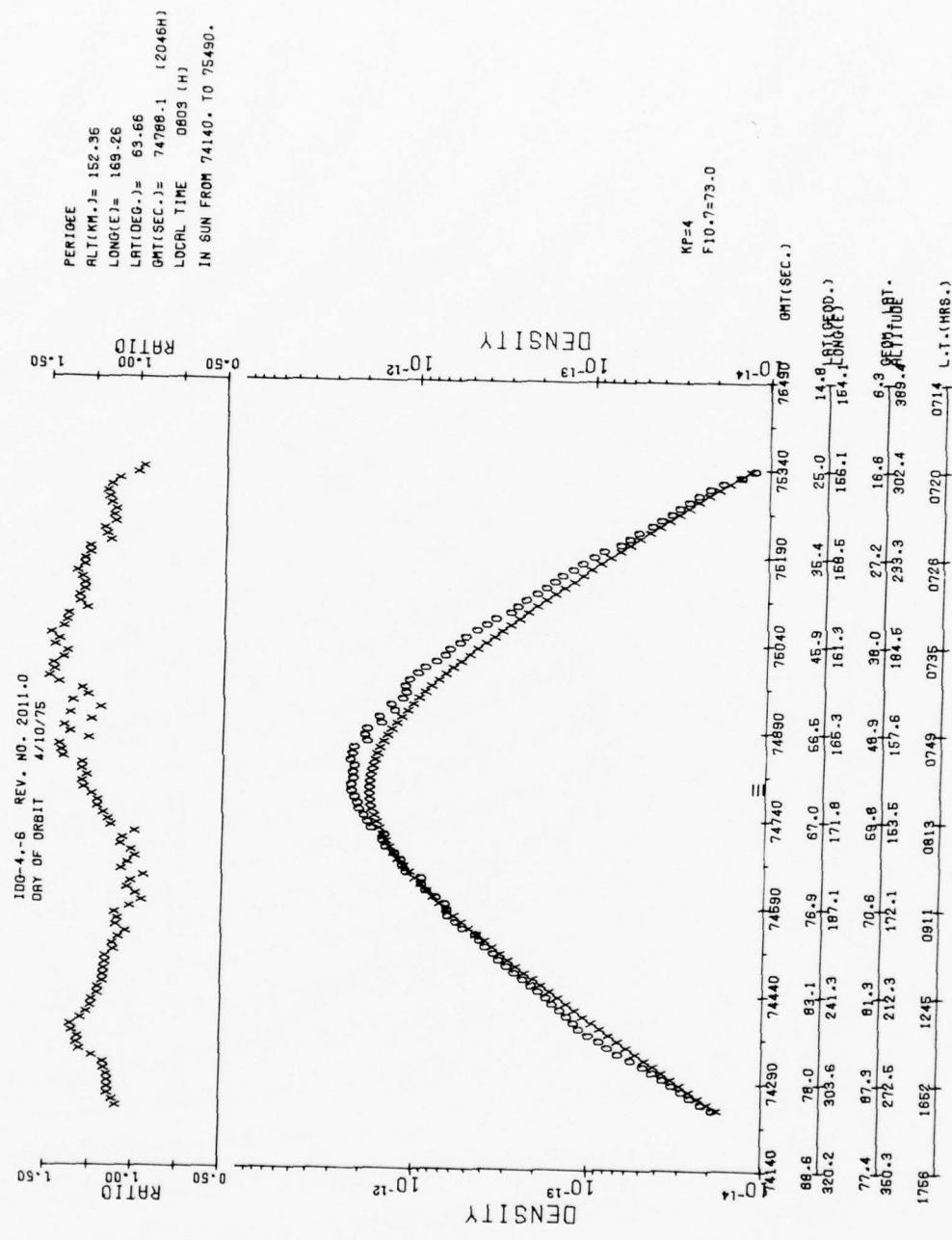


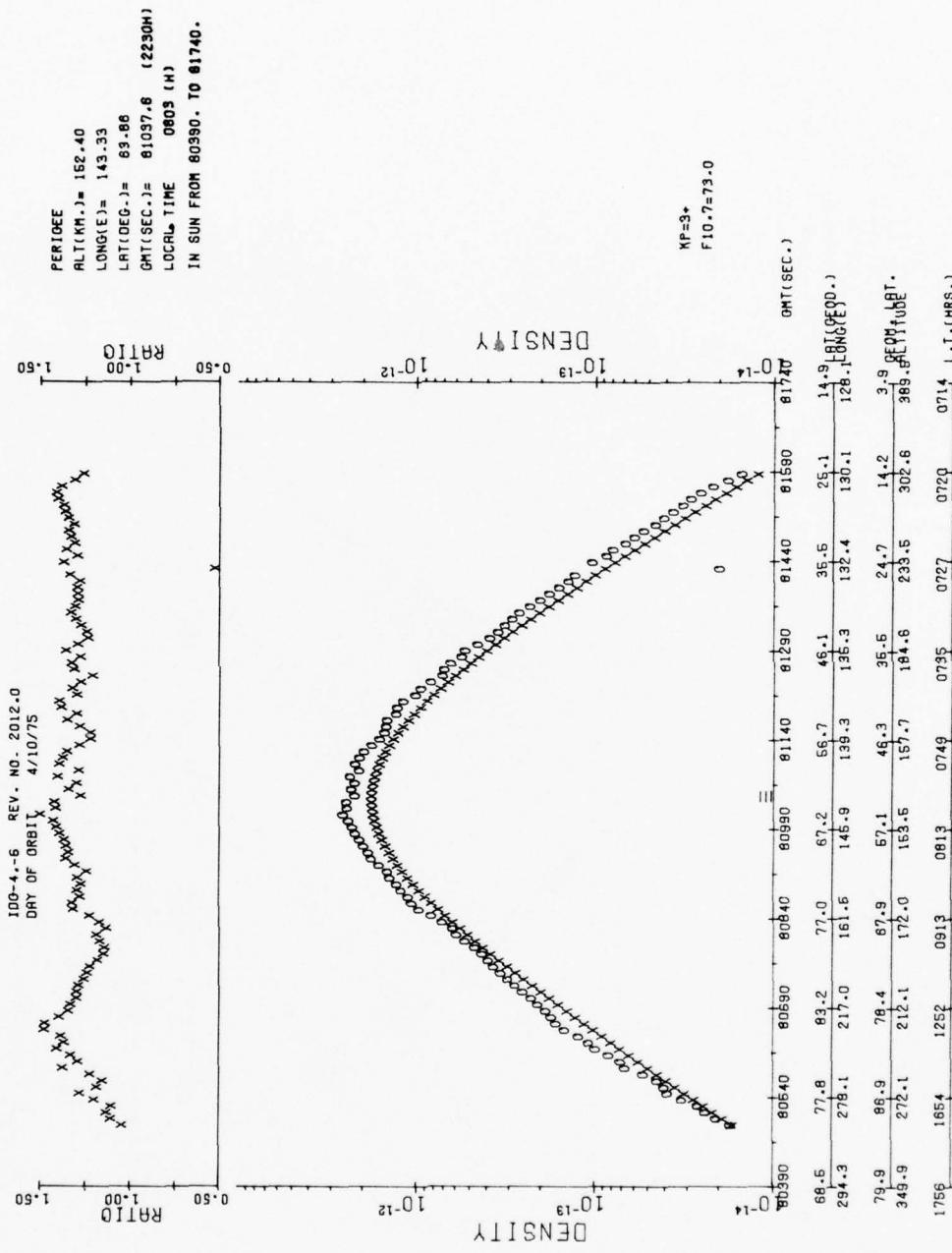


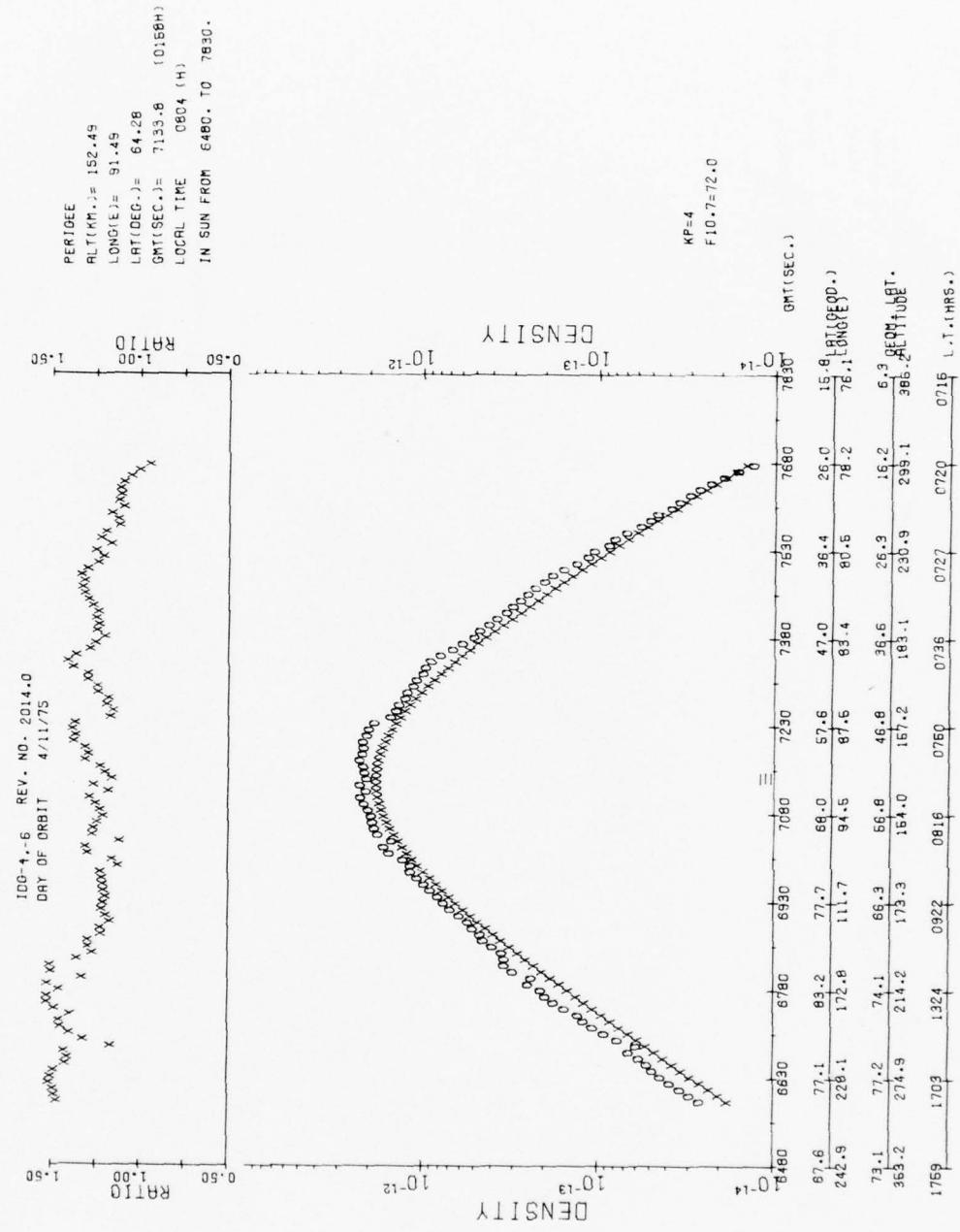
100-4-6 REV. NO. 1999-0
DAY OF ORBIT 4/ 9/75

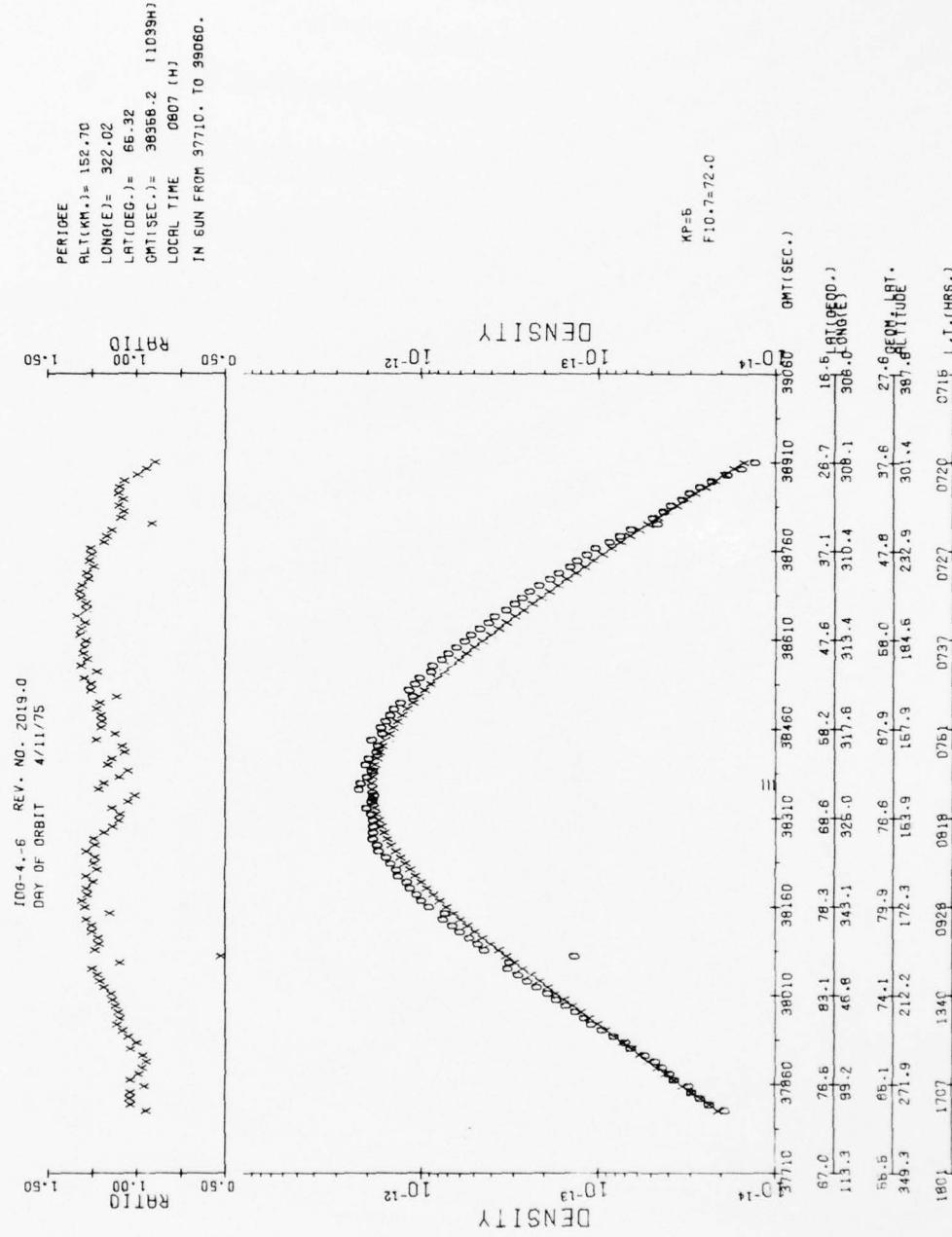
PER10EE
ALT(M.M.)= 151.98
LONG(E)= 120.81
LAT(DEG.)= 61.17
GHT(SEC.)= 86121.2 (2355H)
LOCAL TIME 0758 (H)
IN SUN FROM 86371 TO 86671.

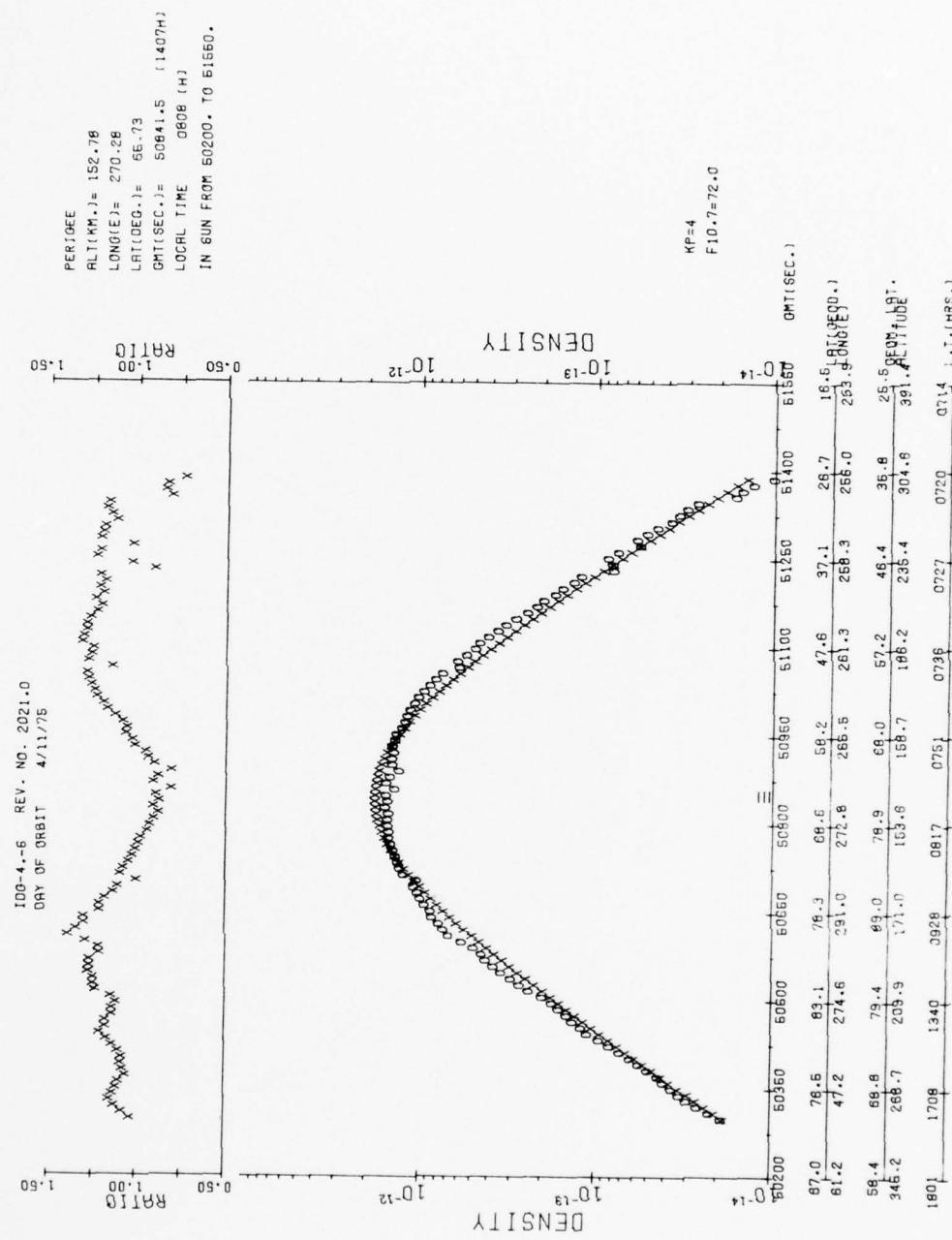


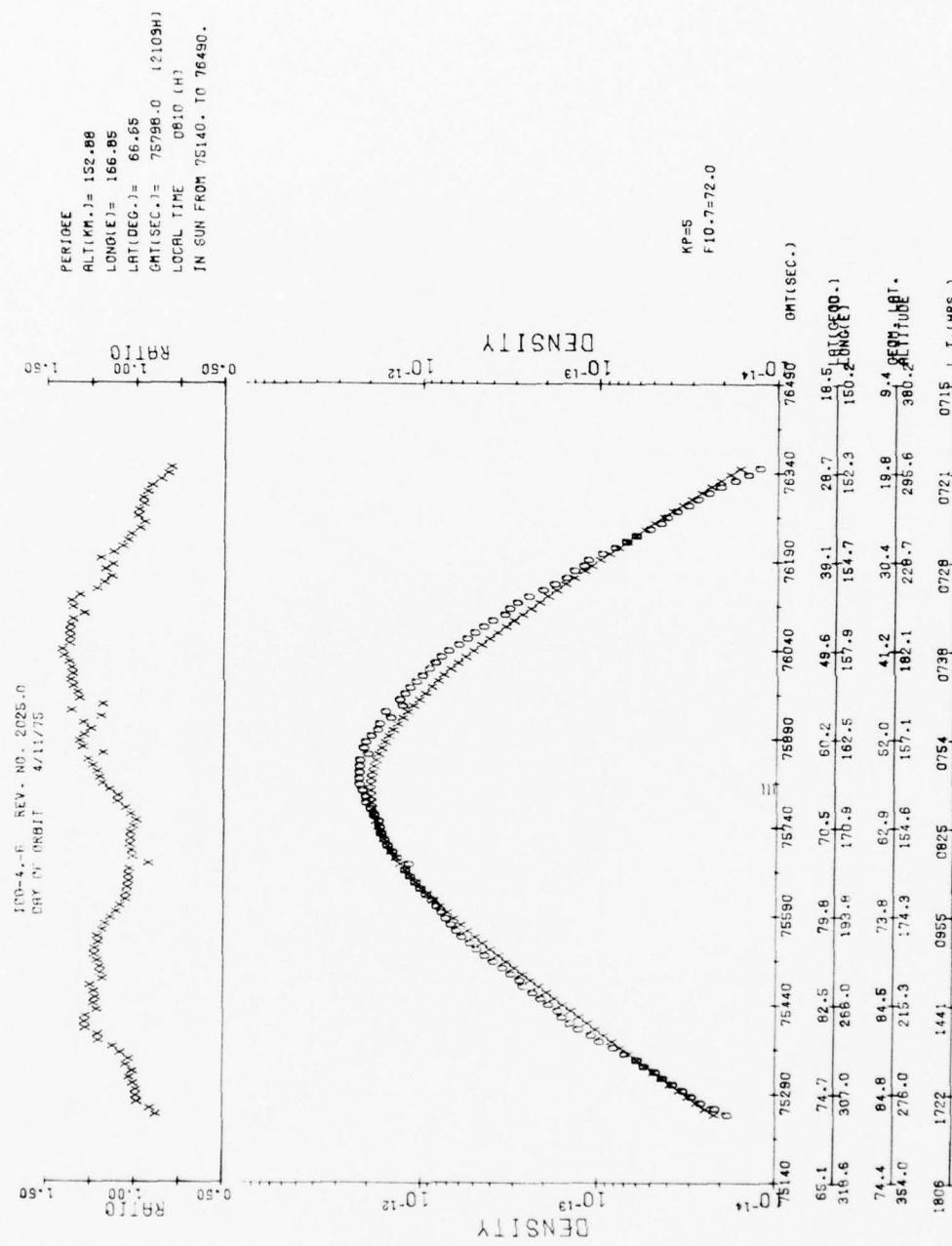


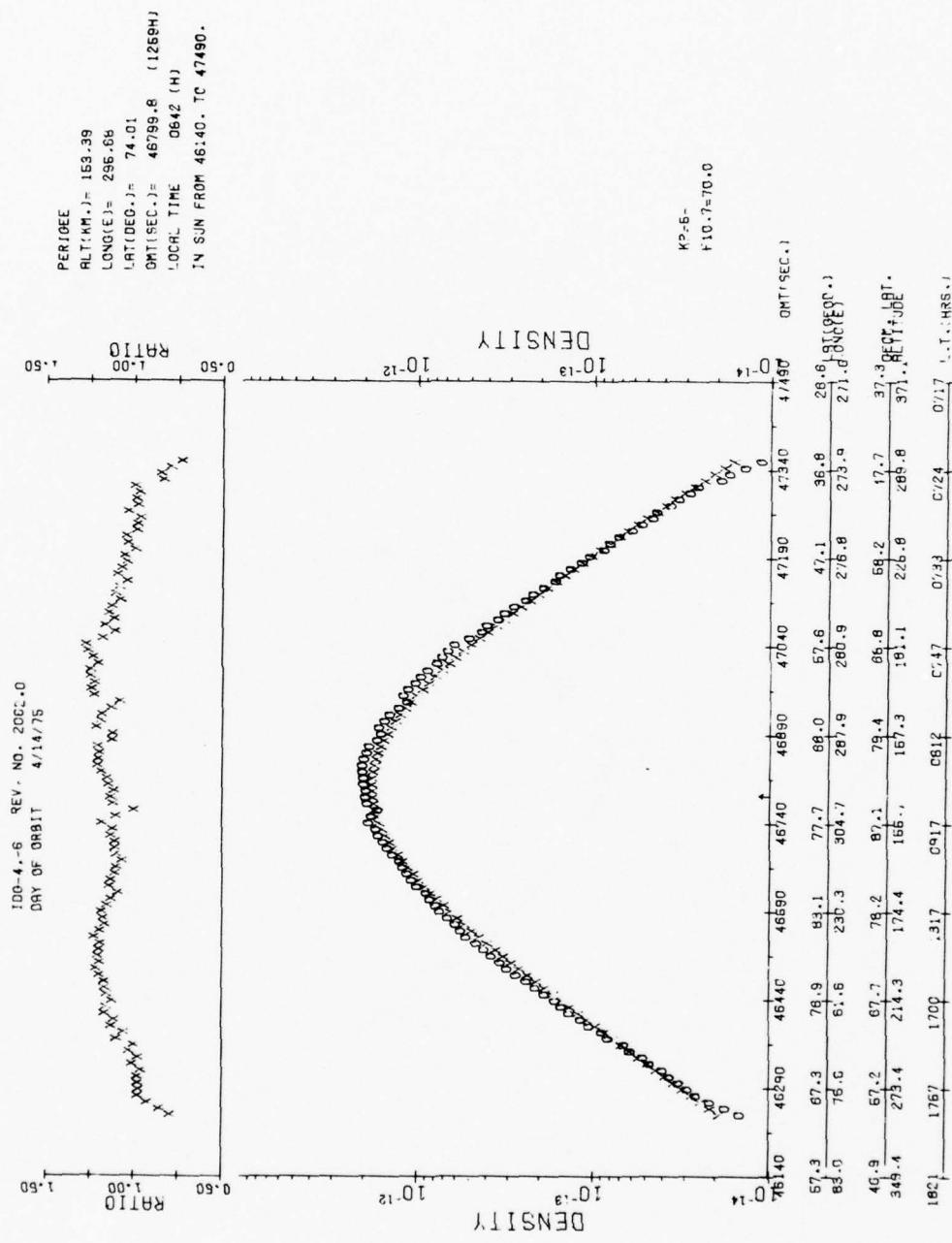


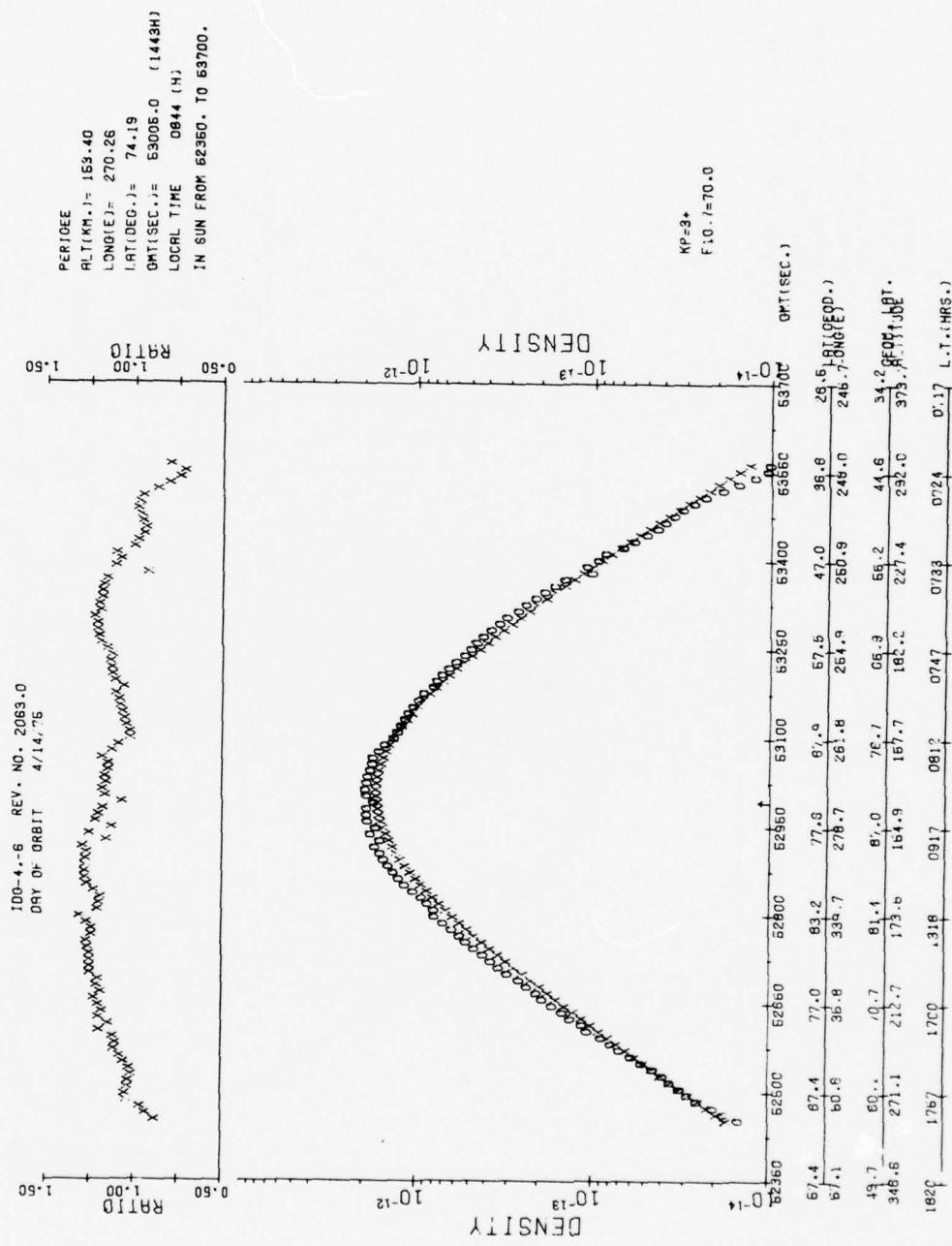






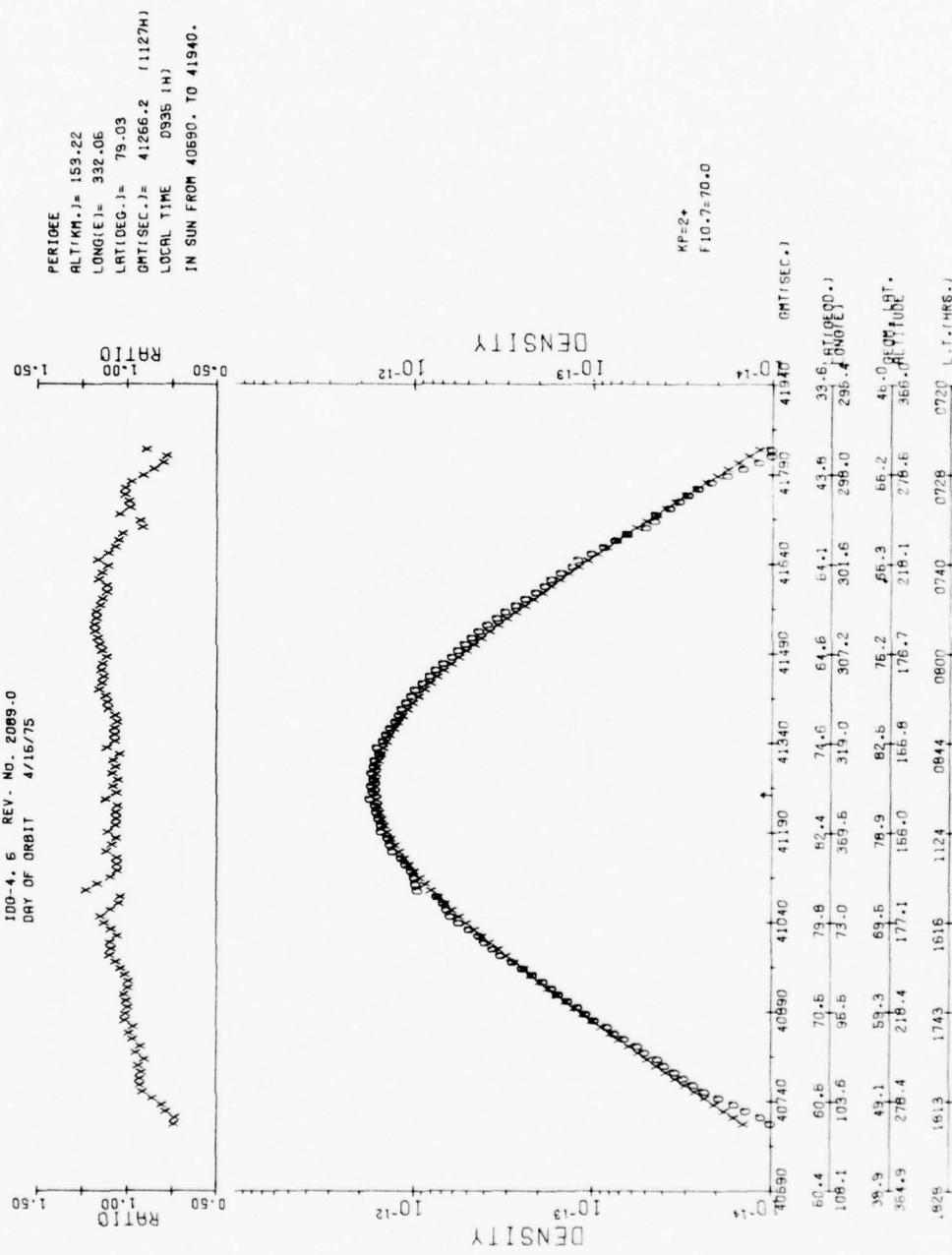


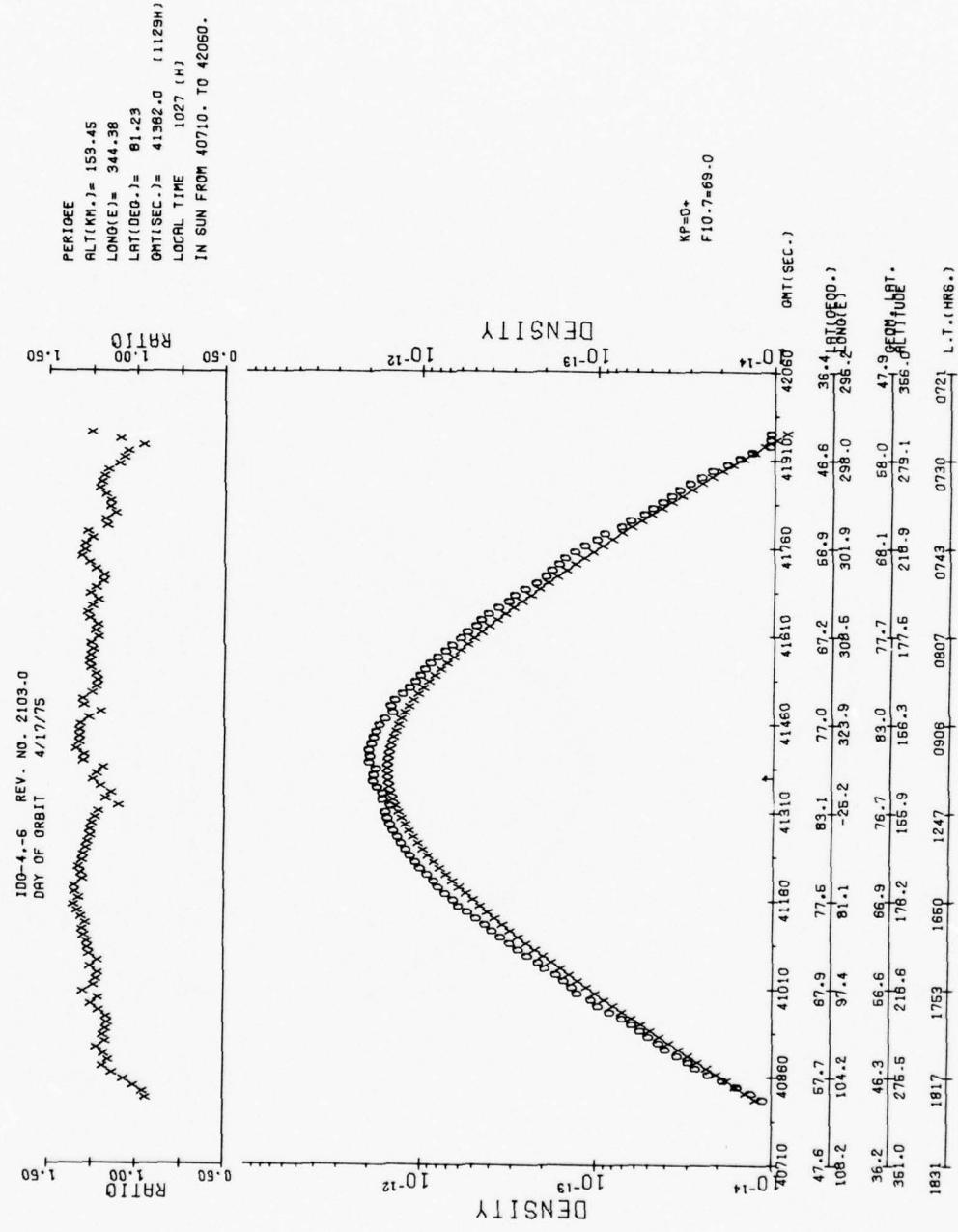




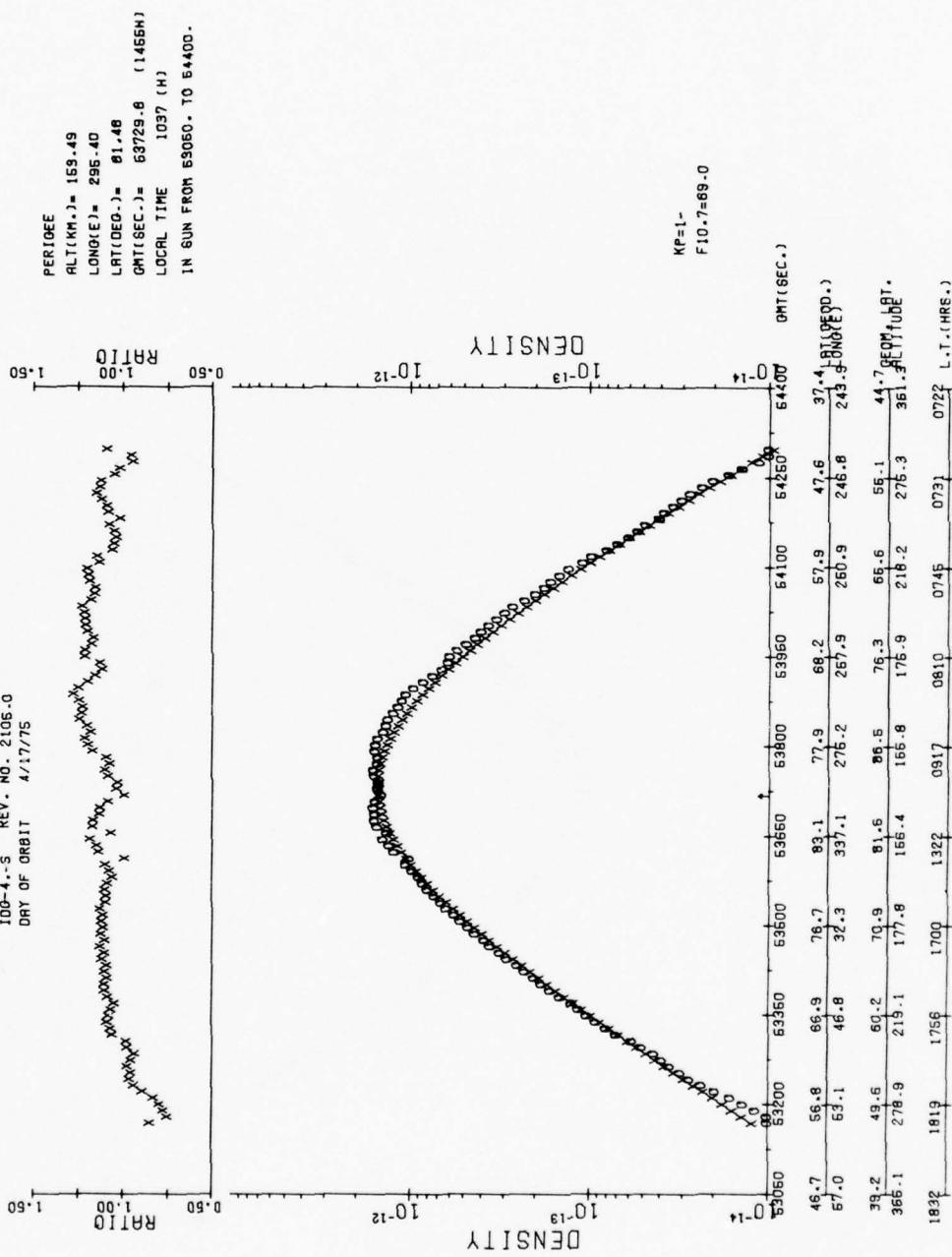
IDG-4.-6 REV. NO. 2071.0
DAY OF ORBIT 4/15/75

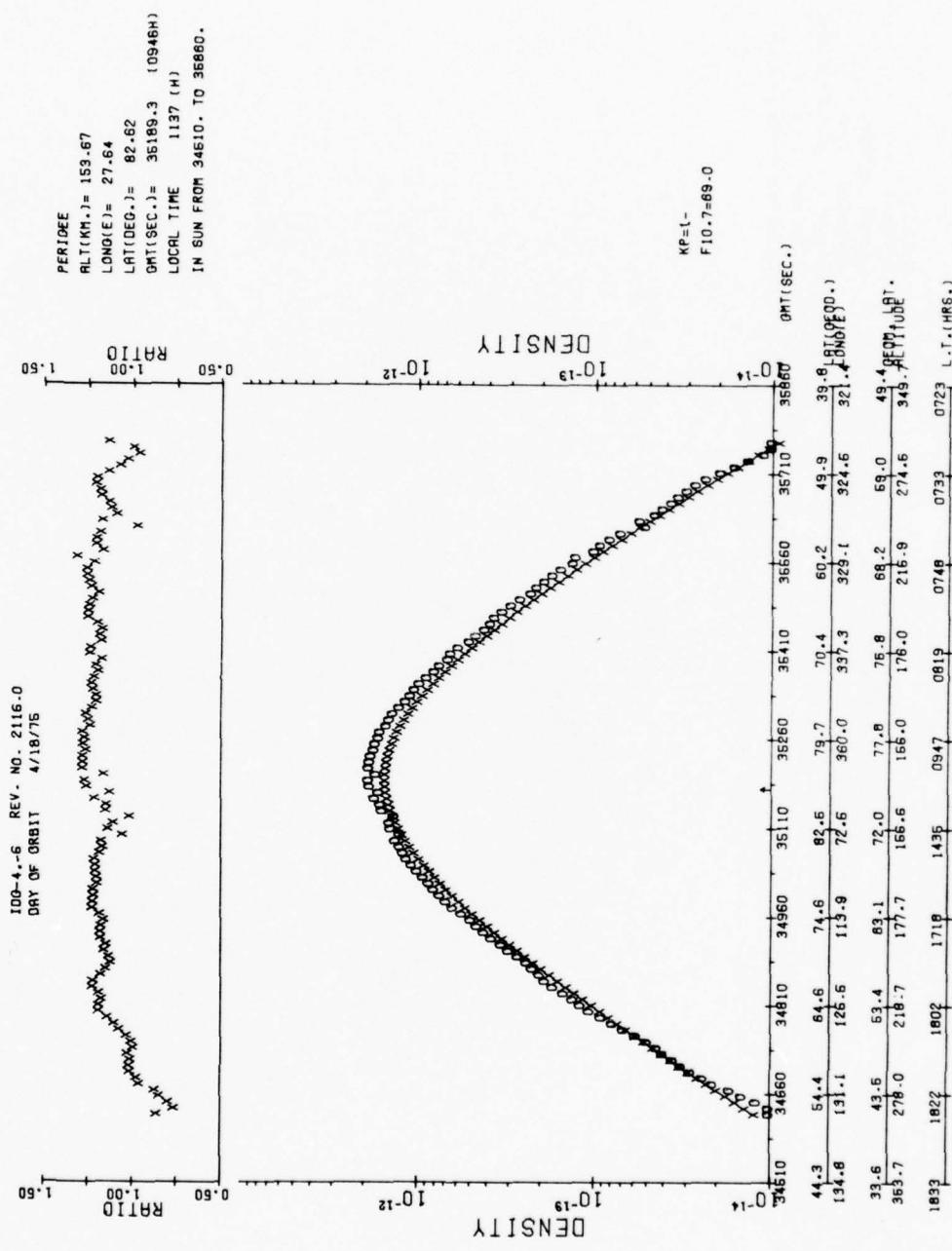
100-4. 6 REV. NO. 2009-0
DAY OF ORBIT 4/16/75

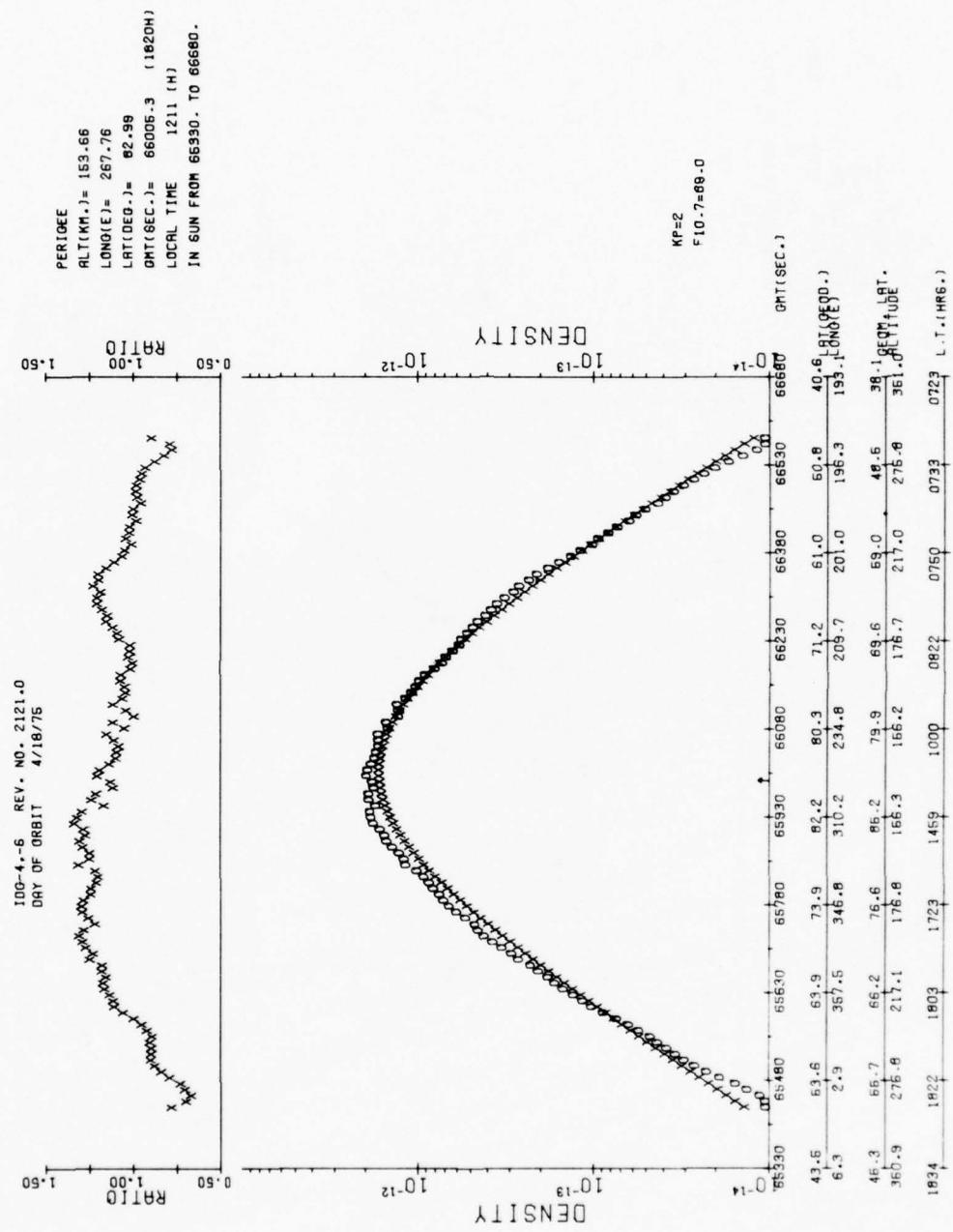


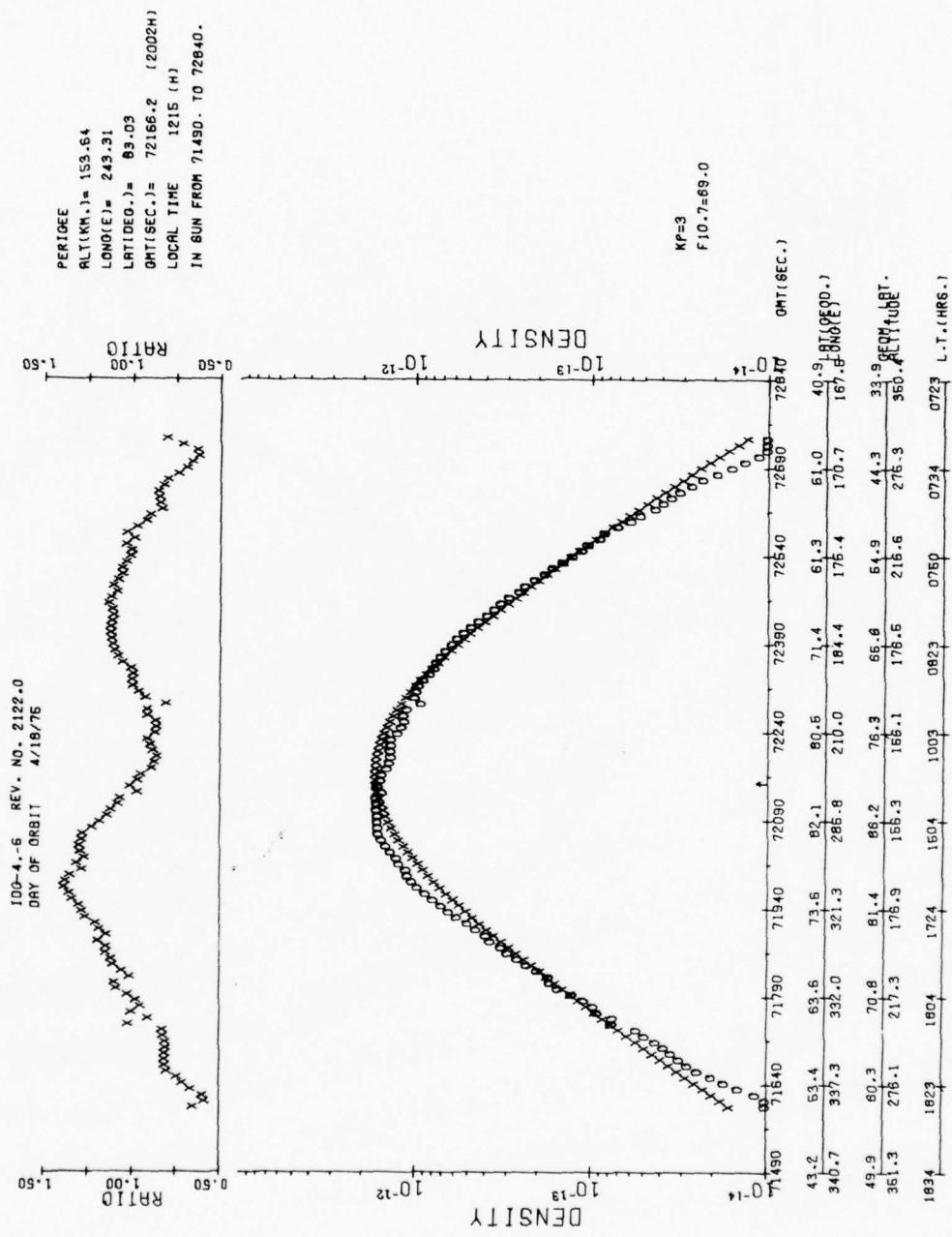


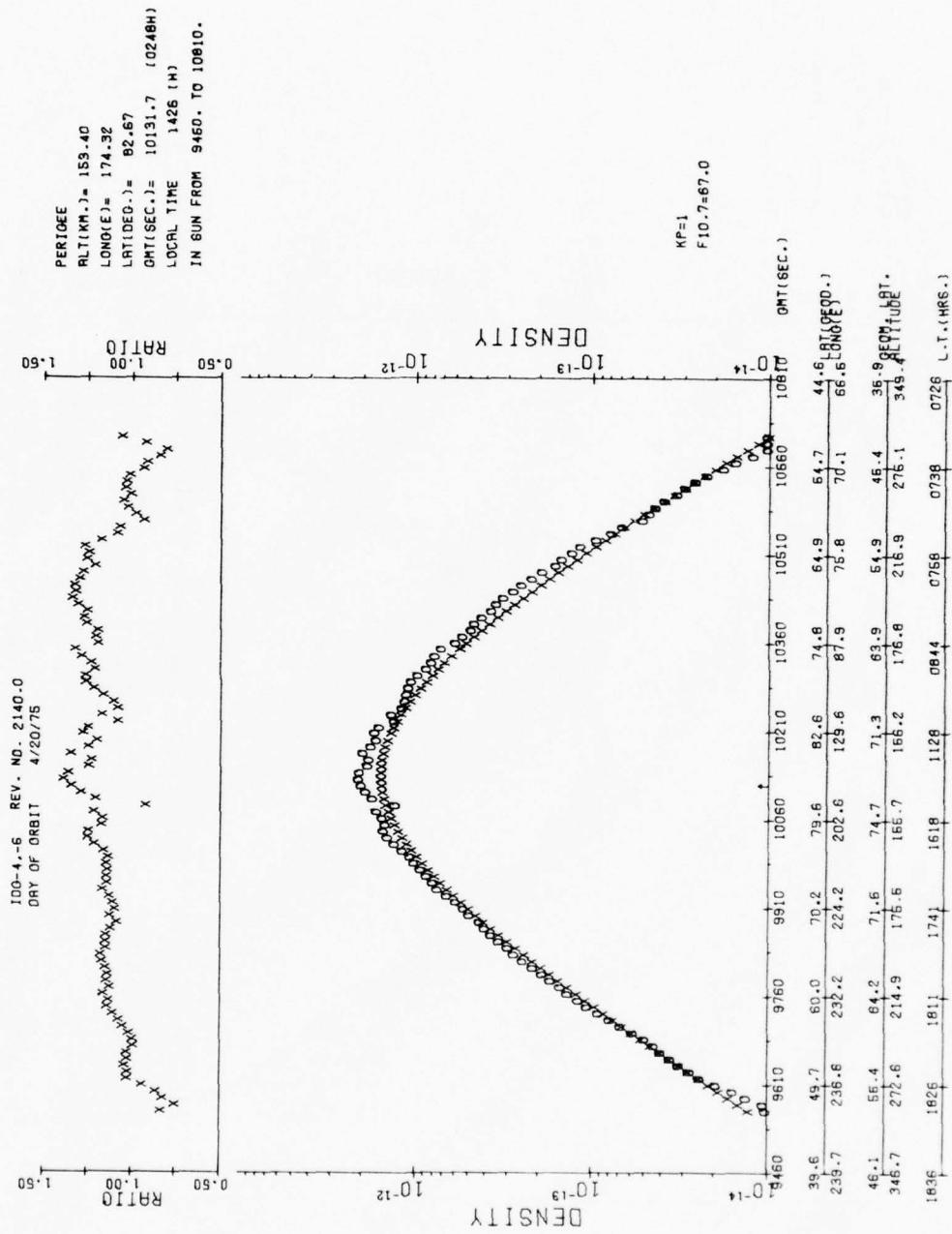
100-4-S REV. NO. 2106-0
DRY OF ORBIT 4/17/75



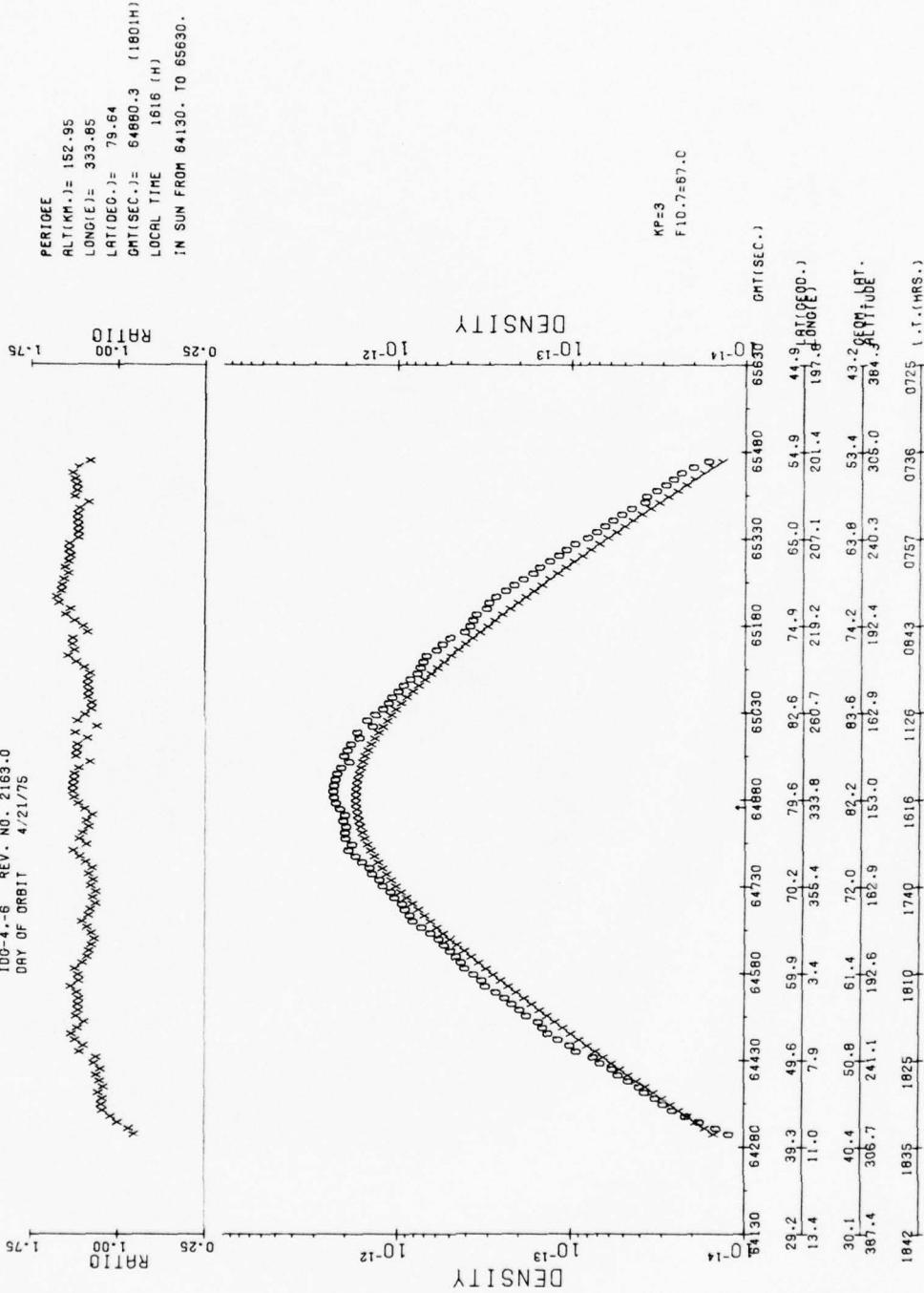


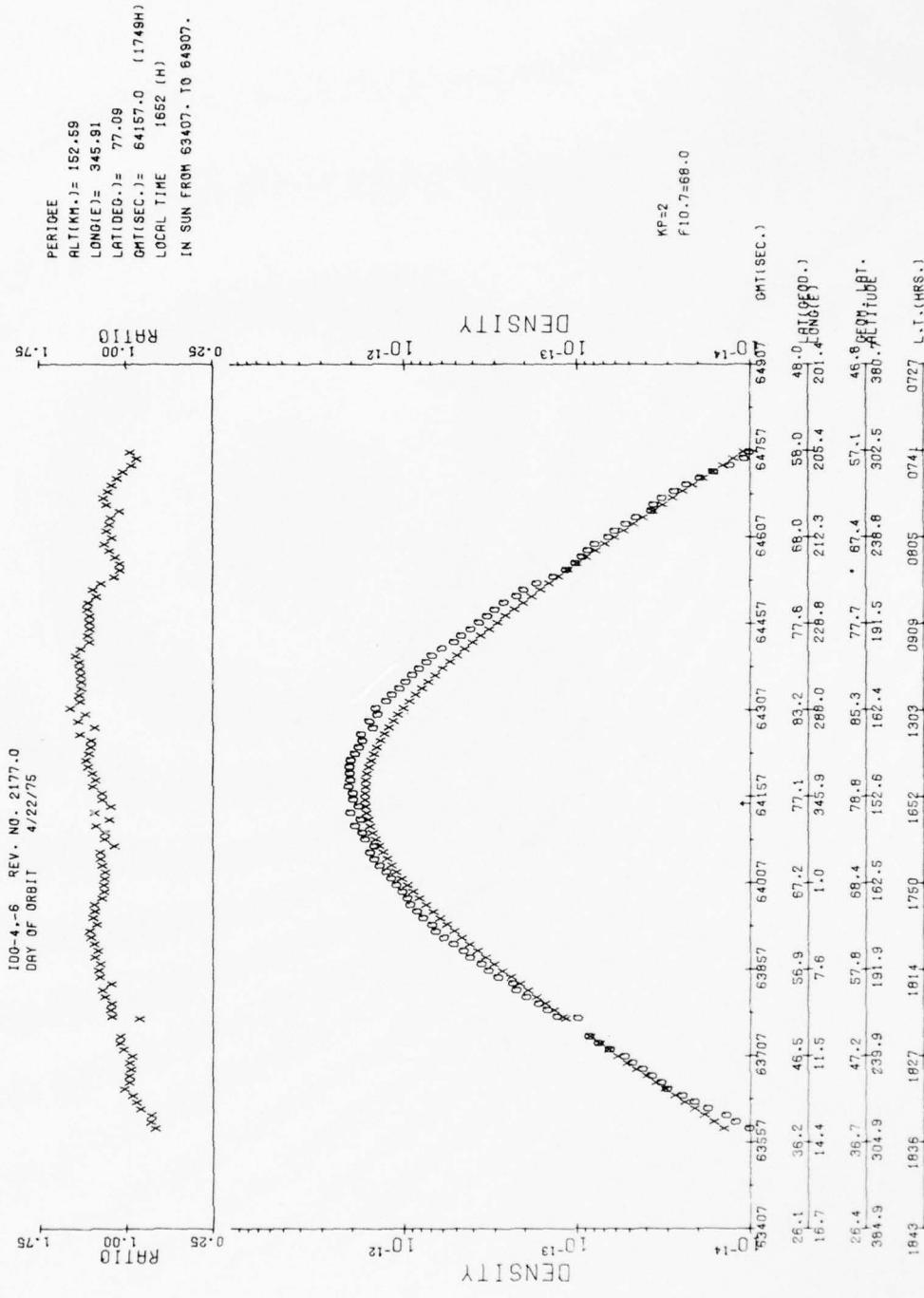


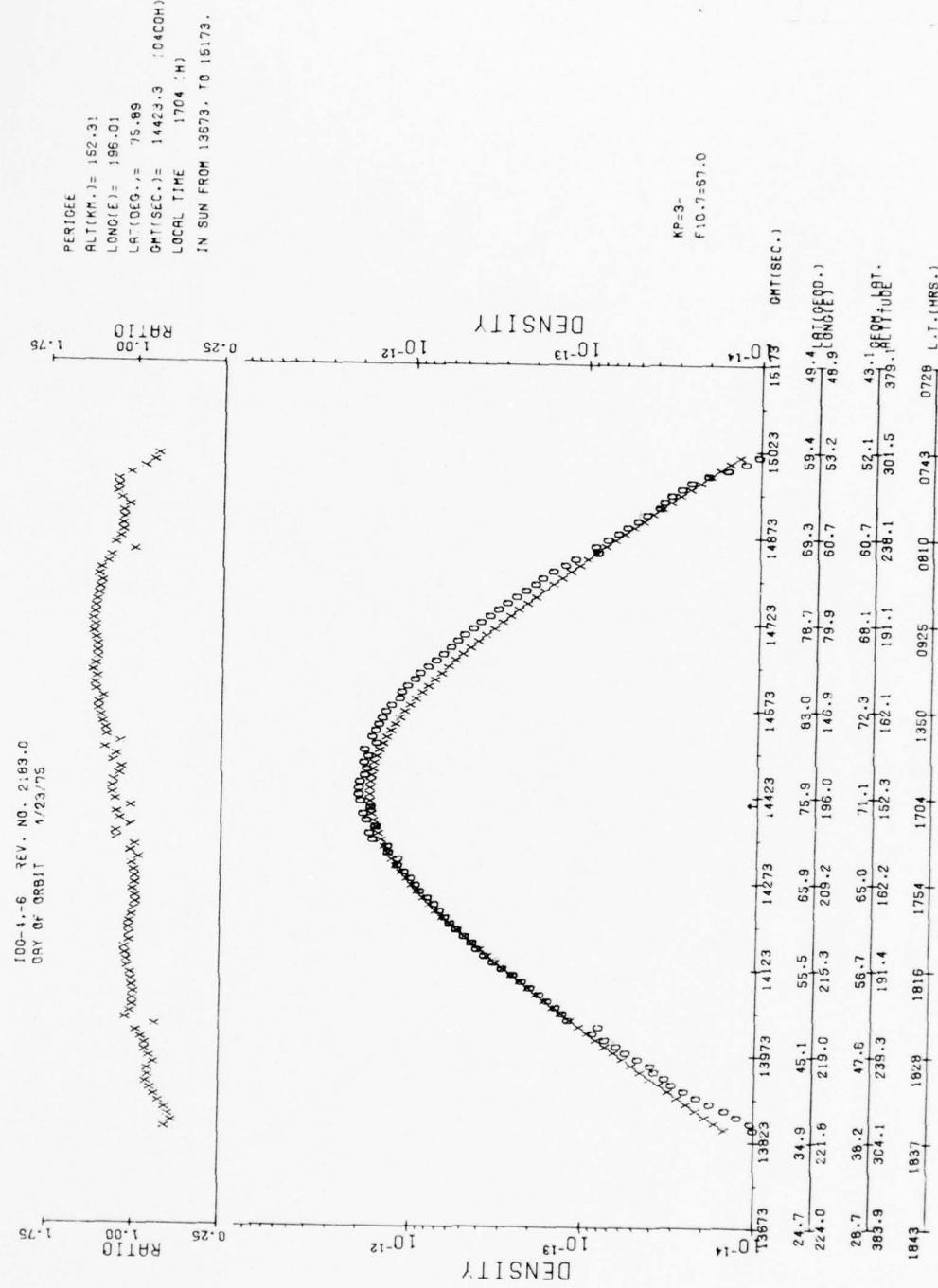


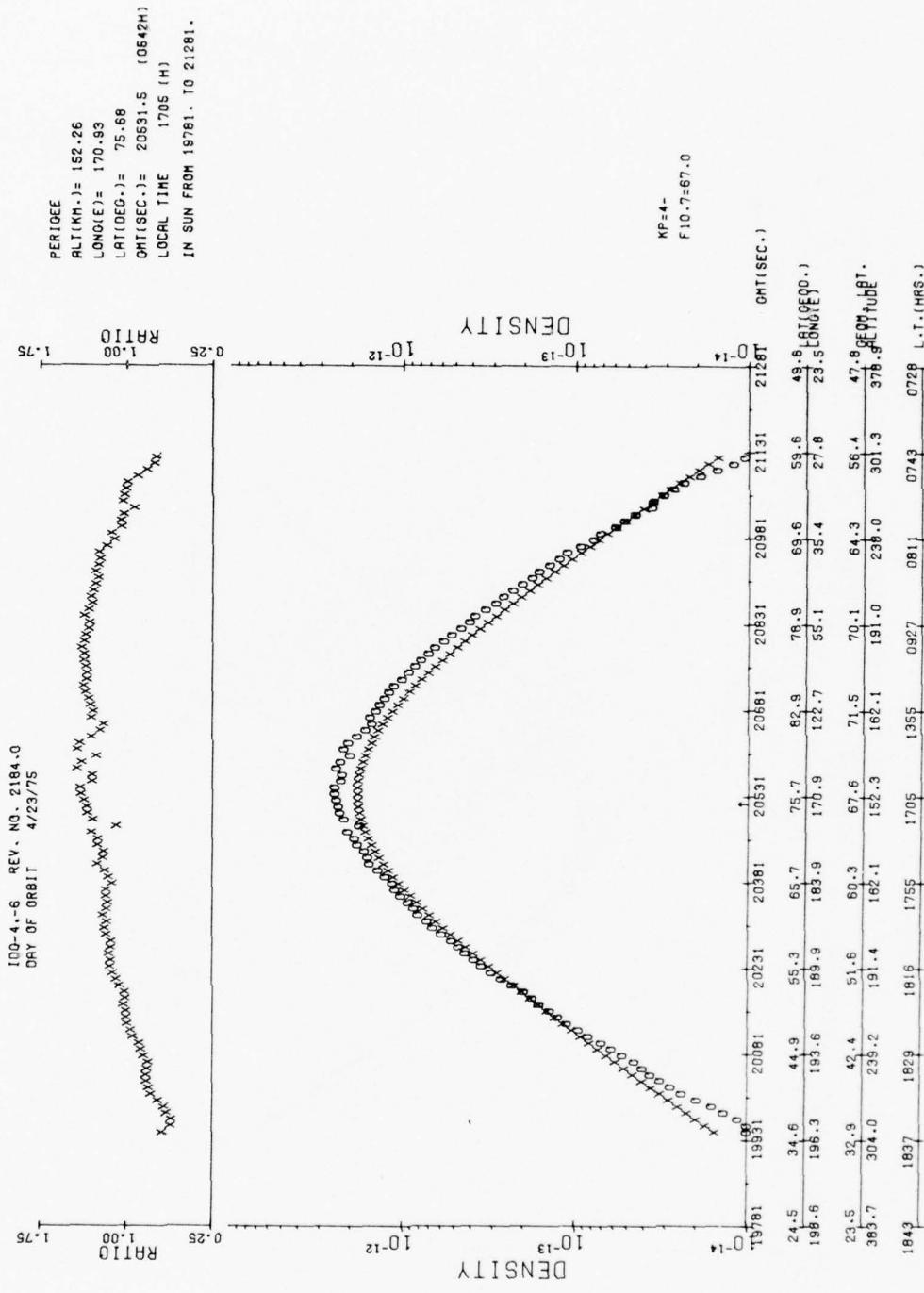


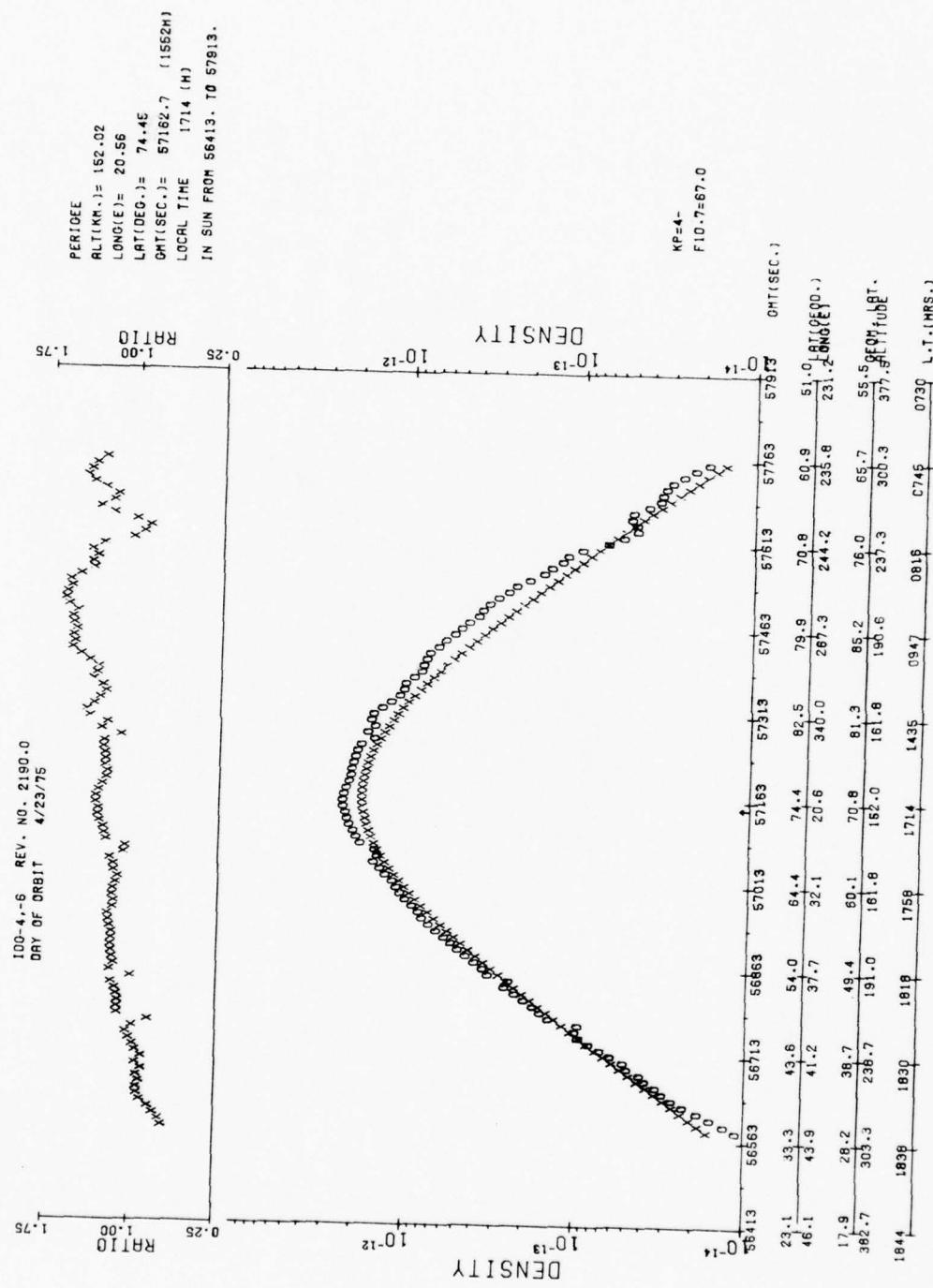
100-4-6 REV. NO. 2163-0
DAY OF ORBIT 4/21/75

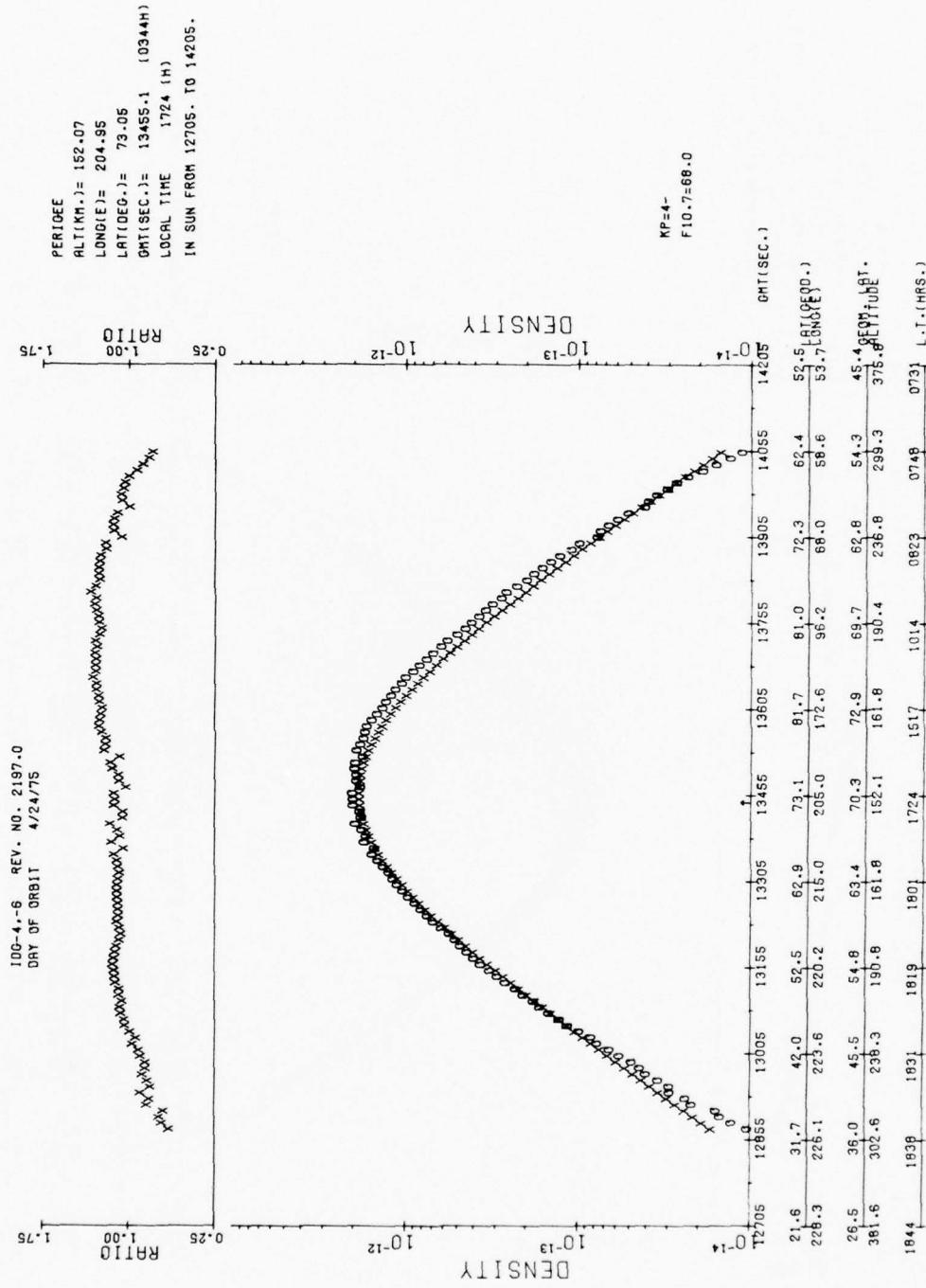




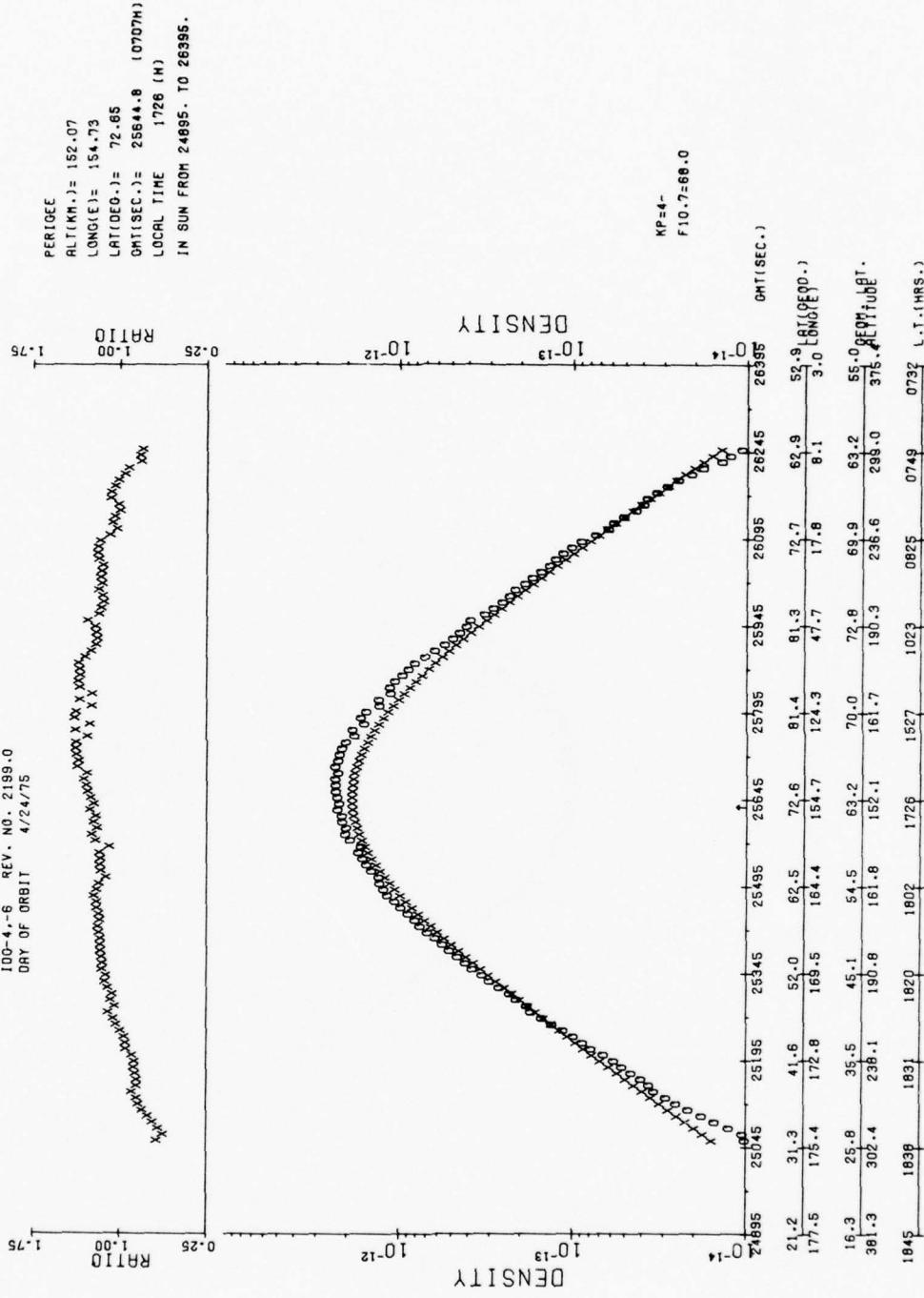


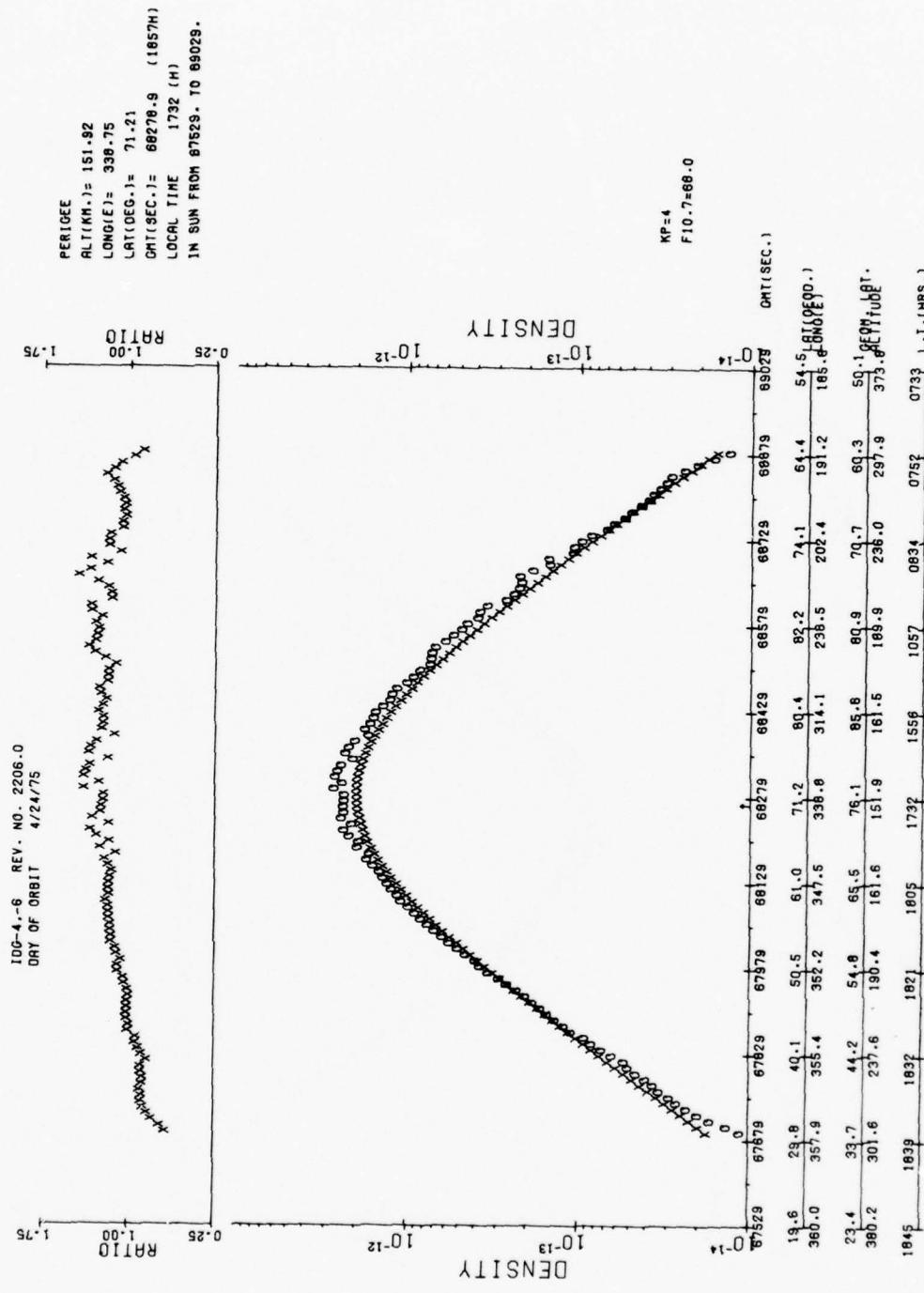


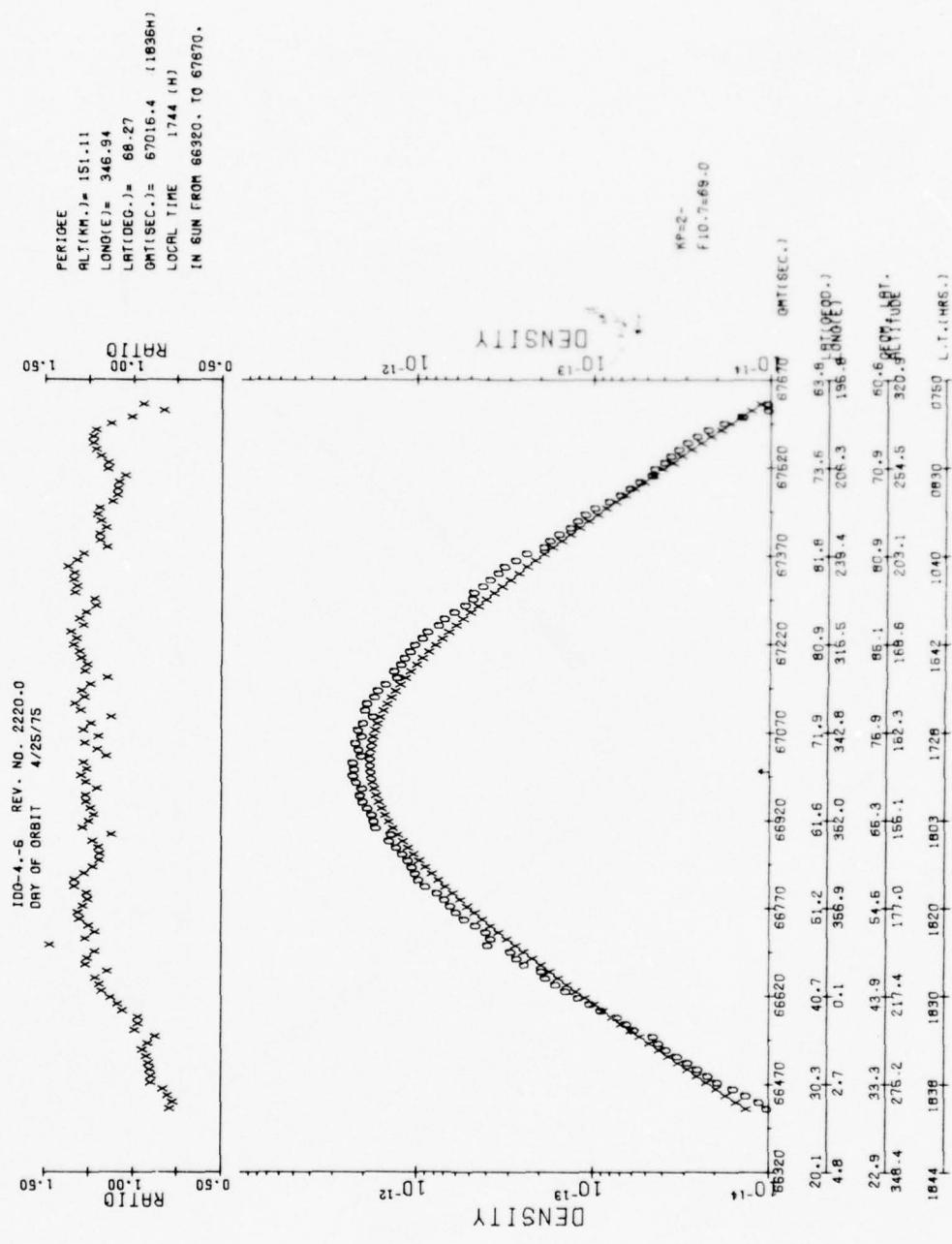


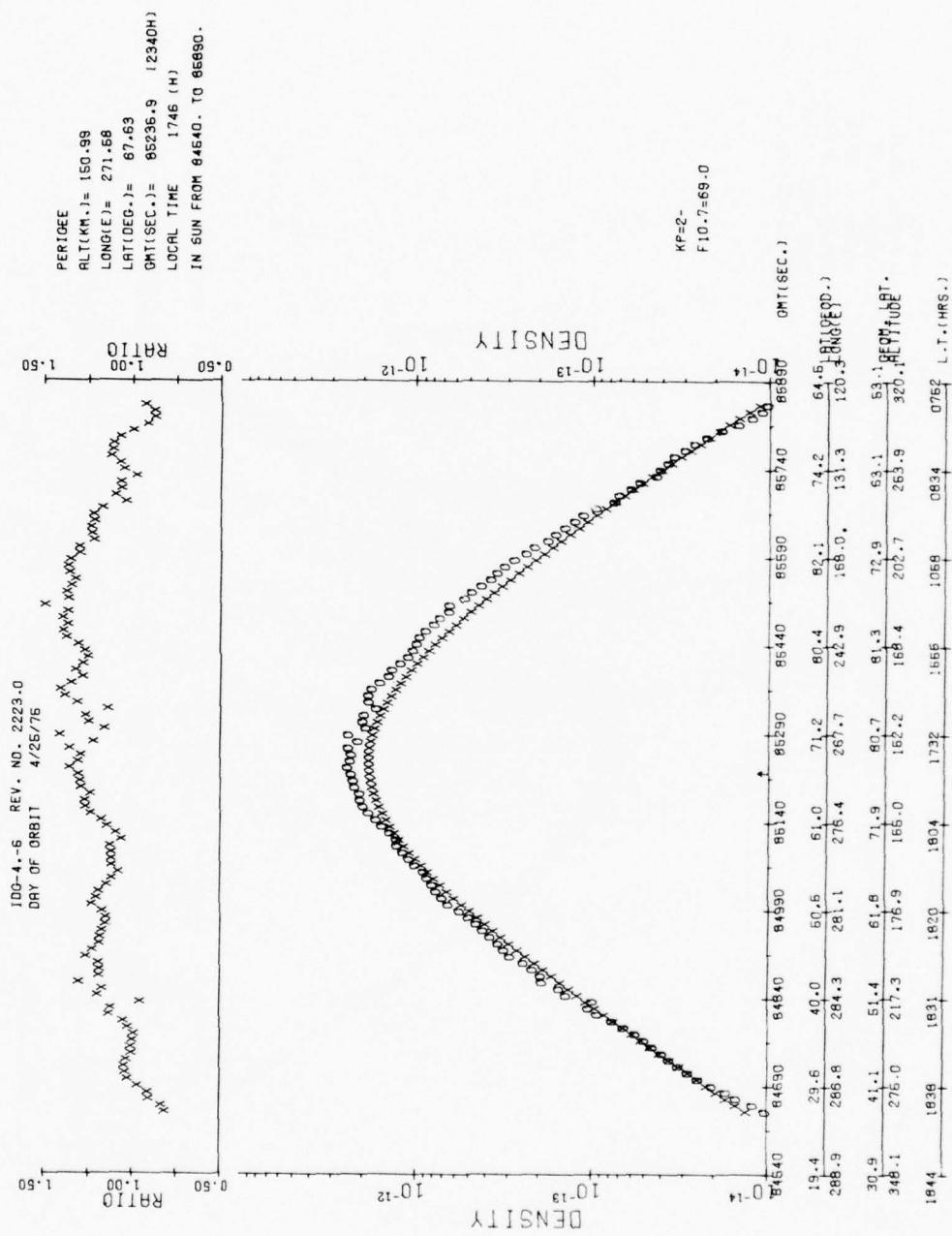


100-4.-6 REV. NO. 2199.0
DAY OF ORBIT 4/24/75

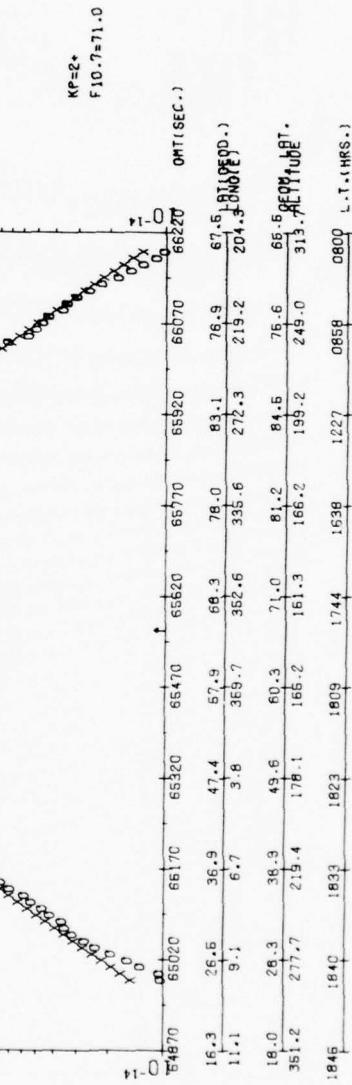
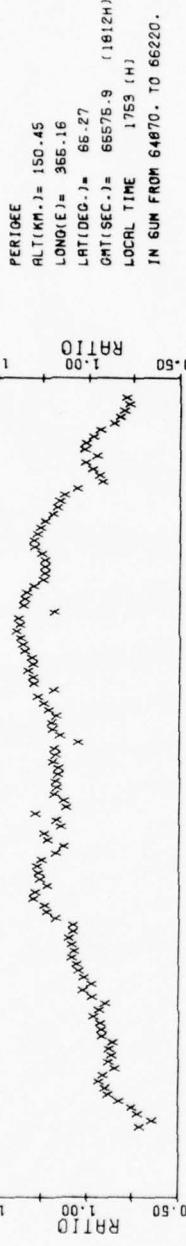


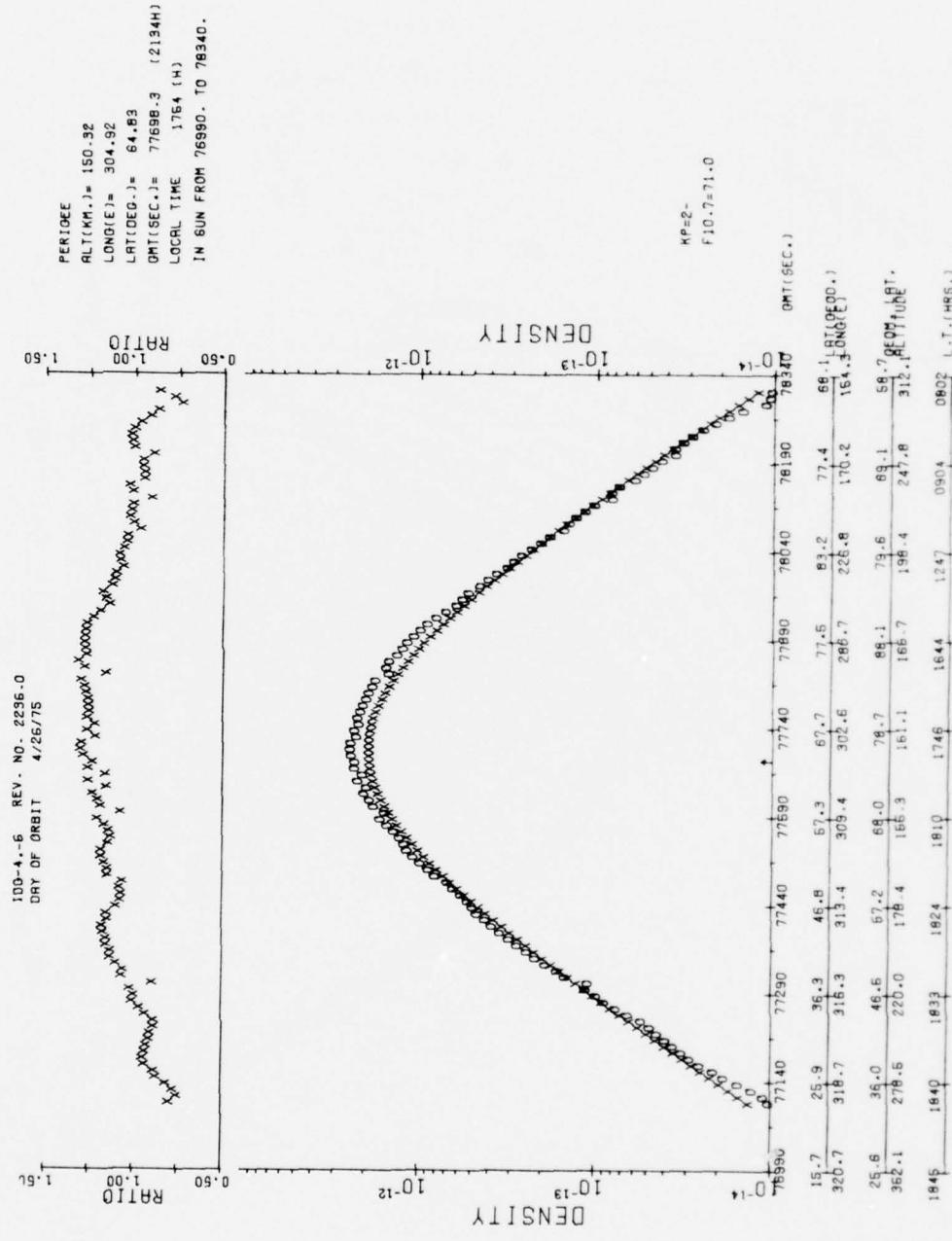


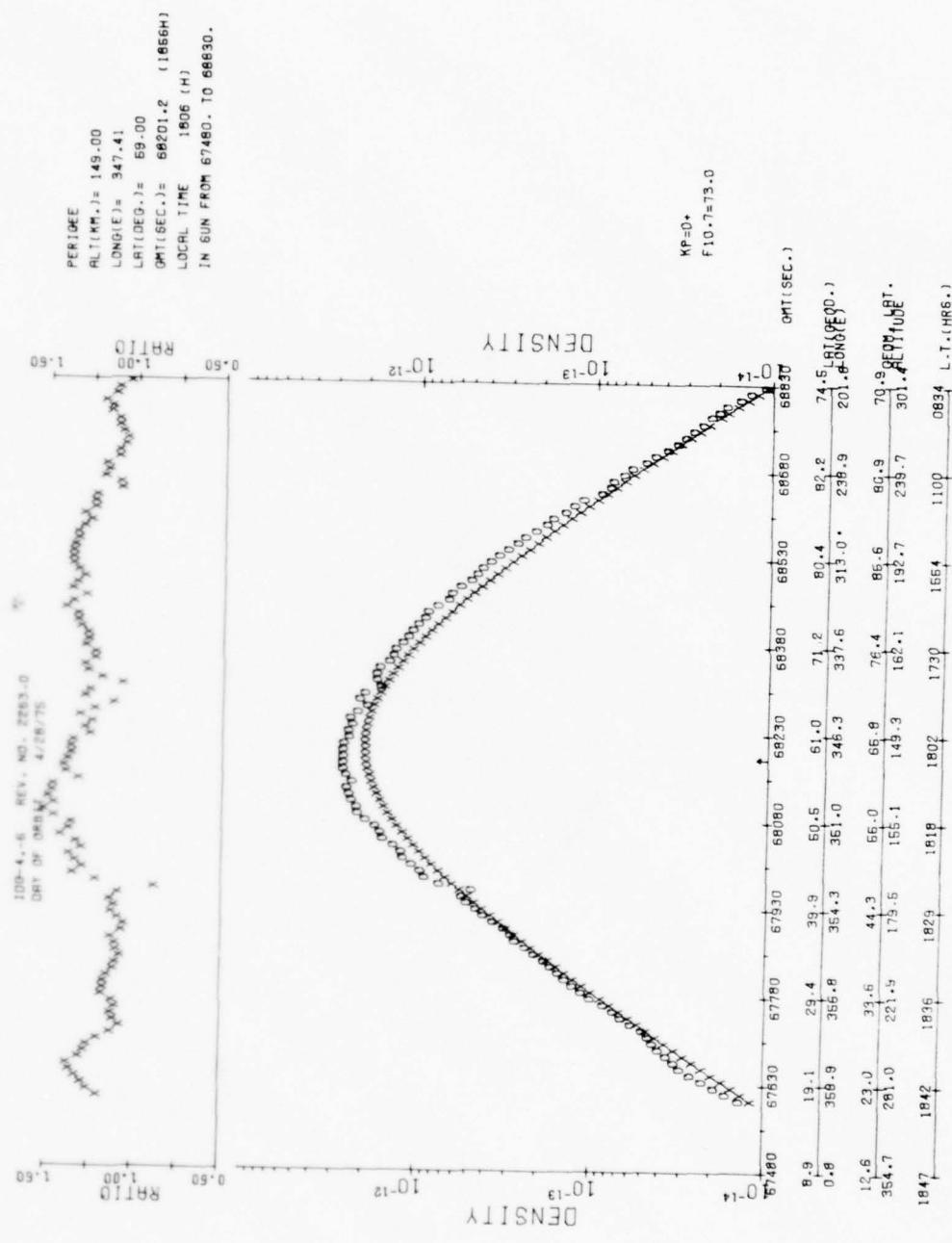


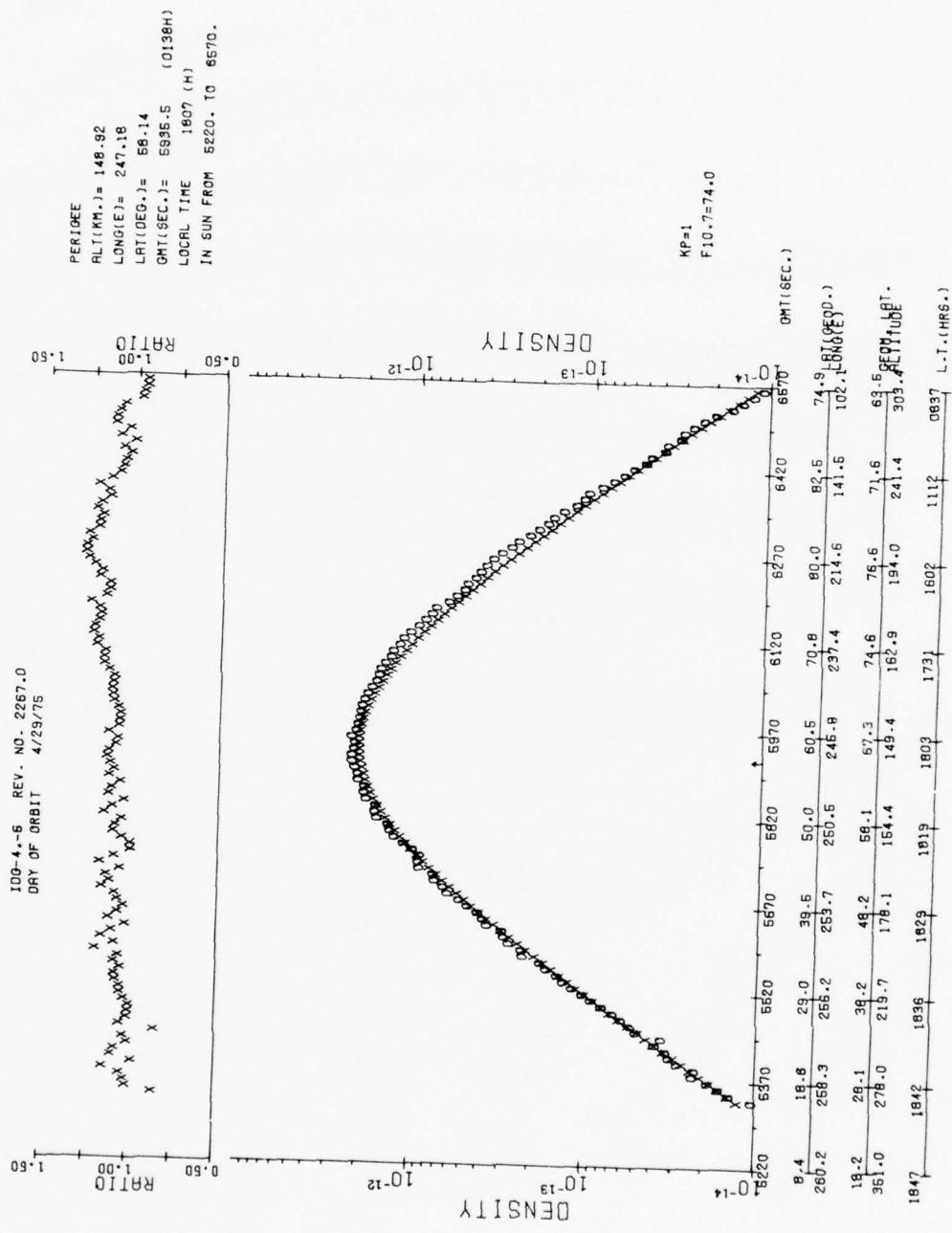


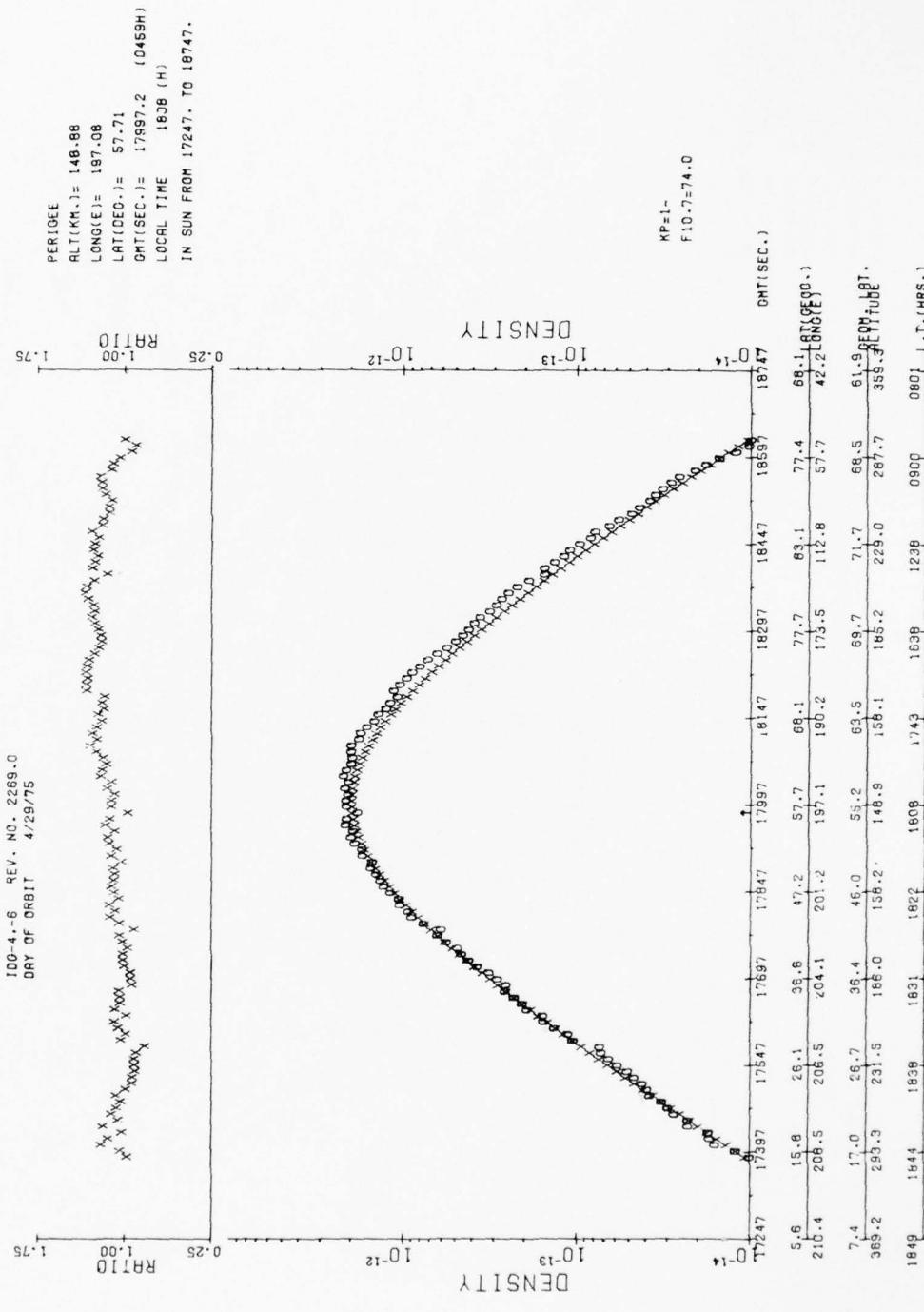
100-4-6 REV. NO. 2234.0
DAY OF ORBIT 4/26/75

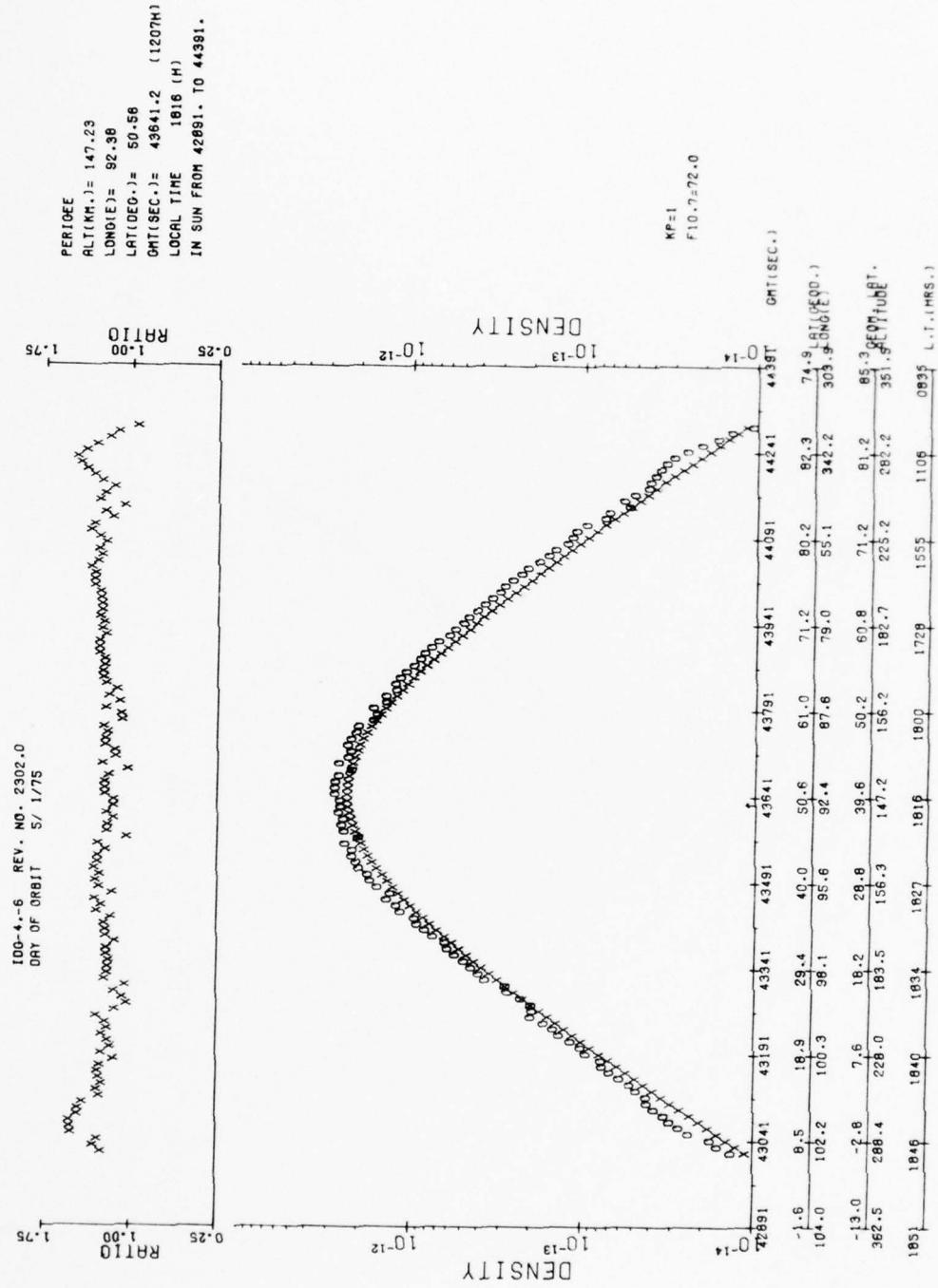


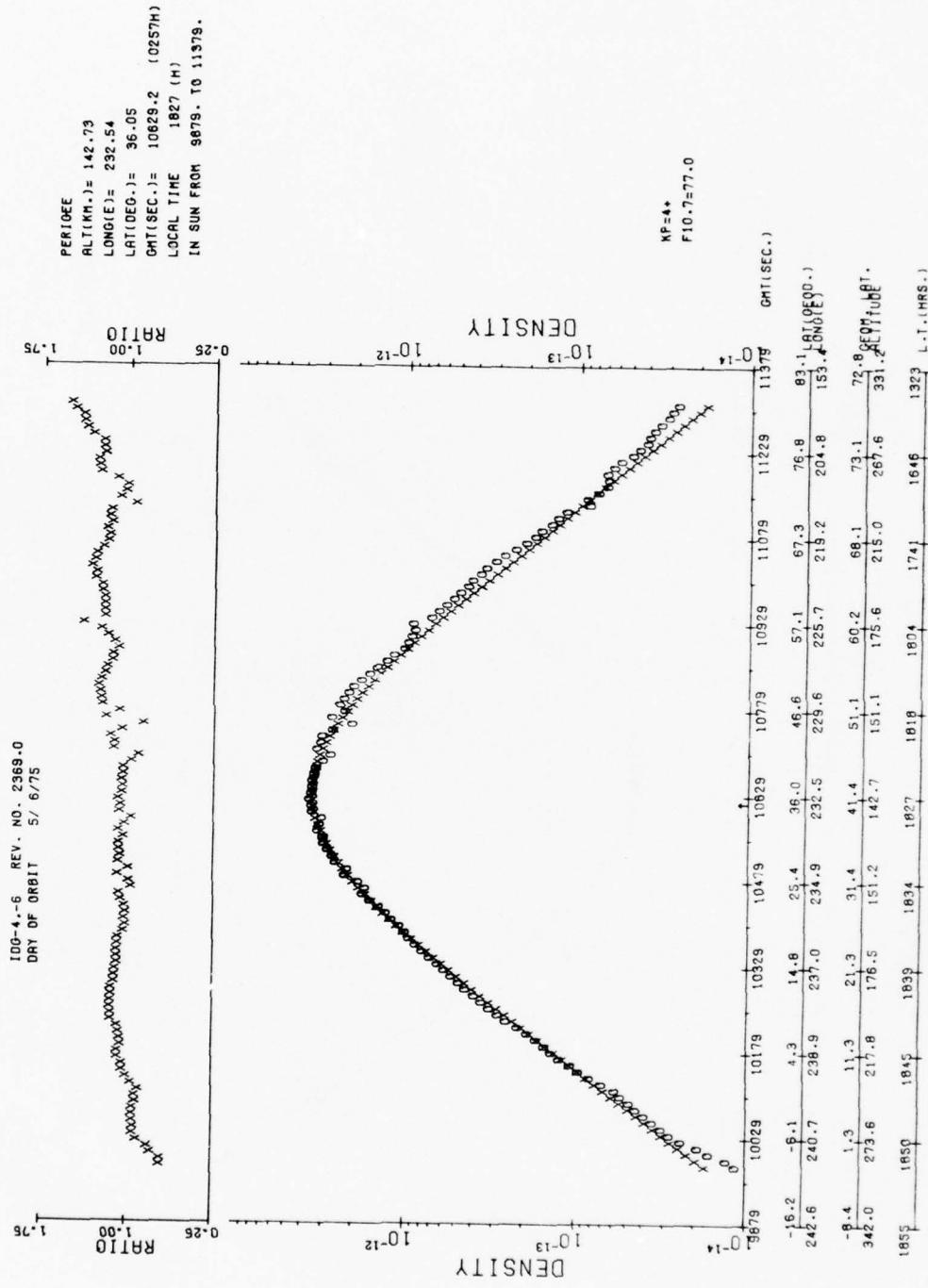


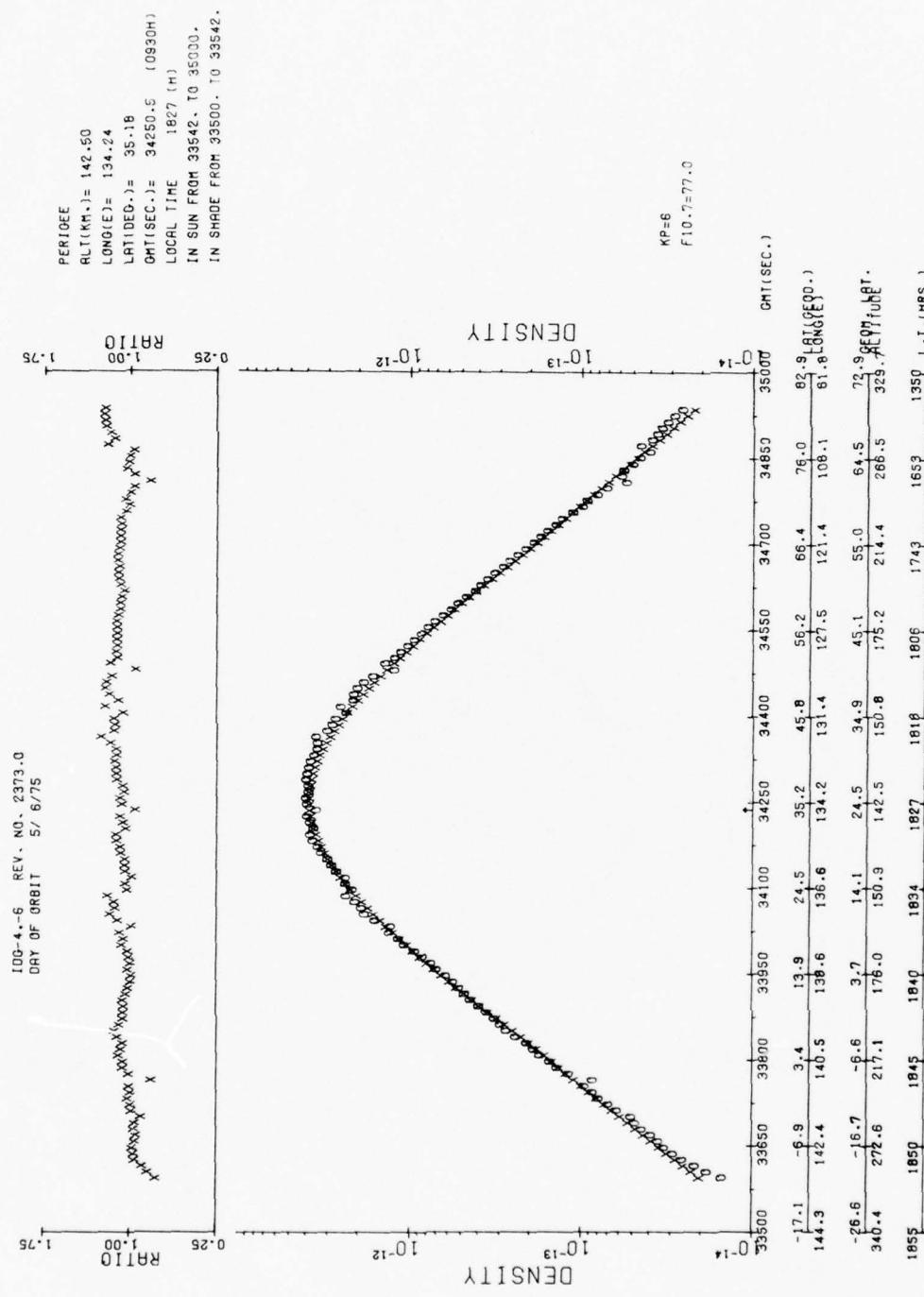


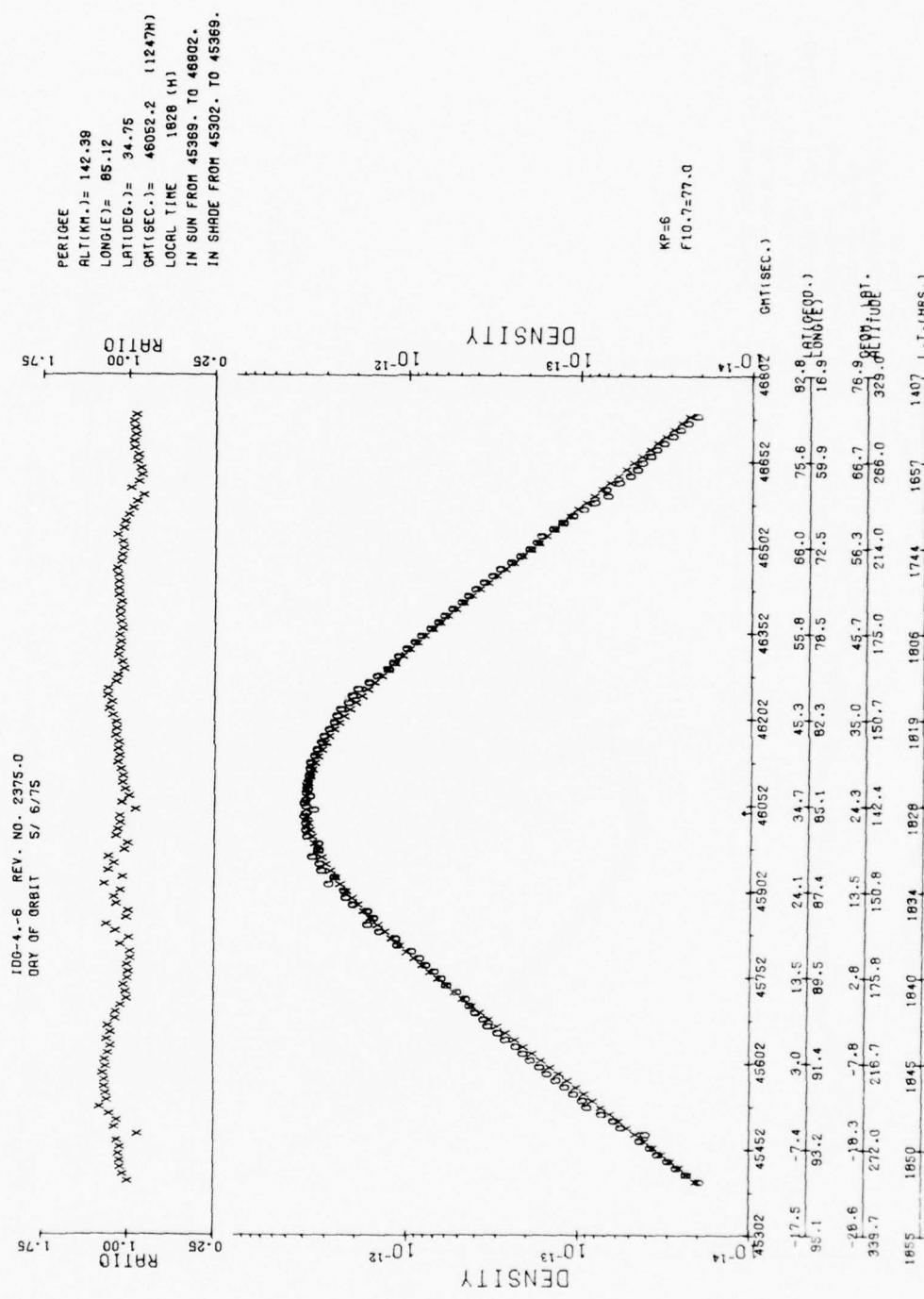




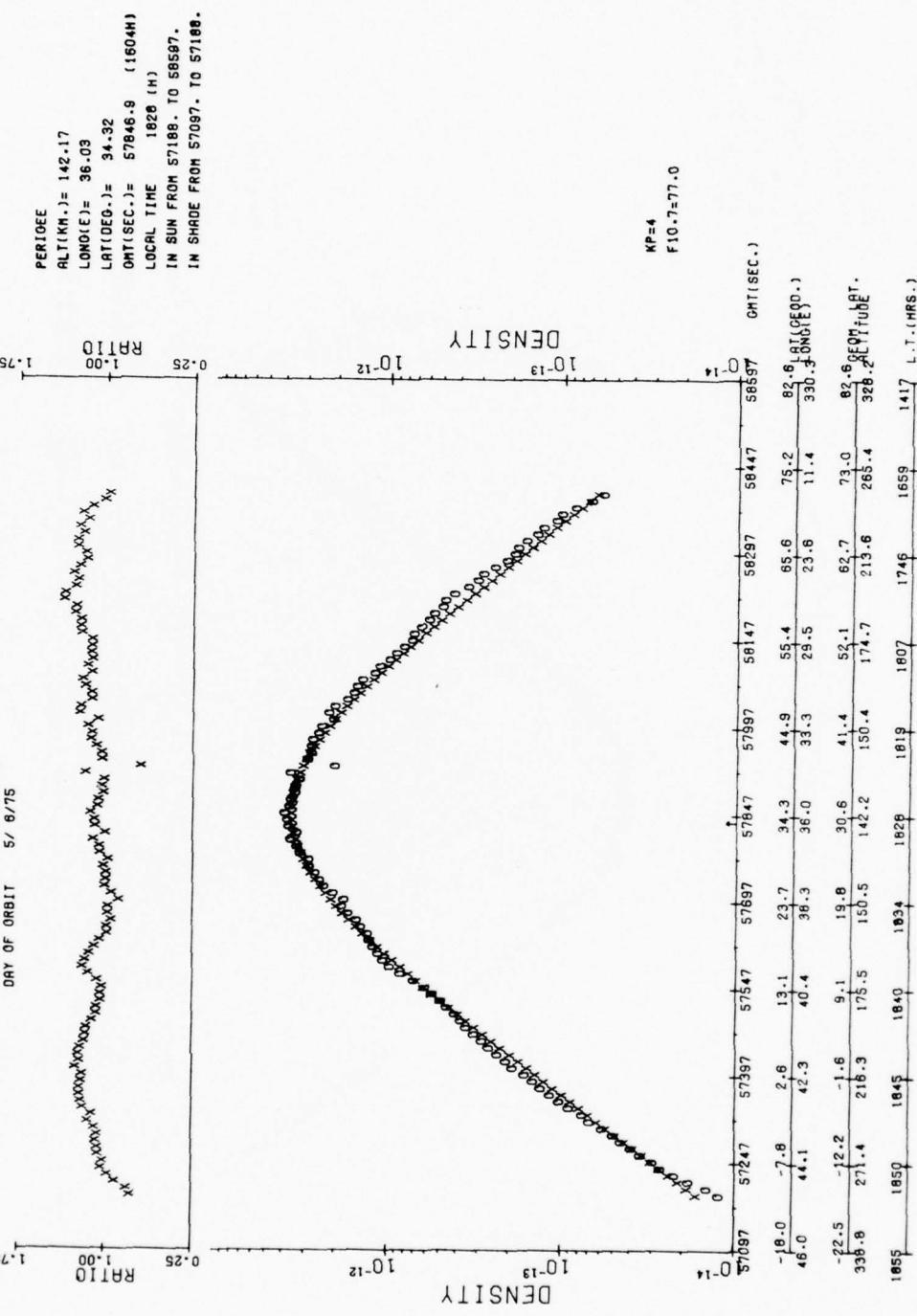


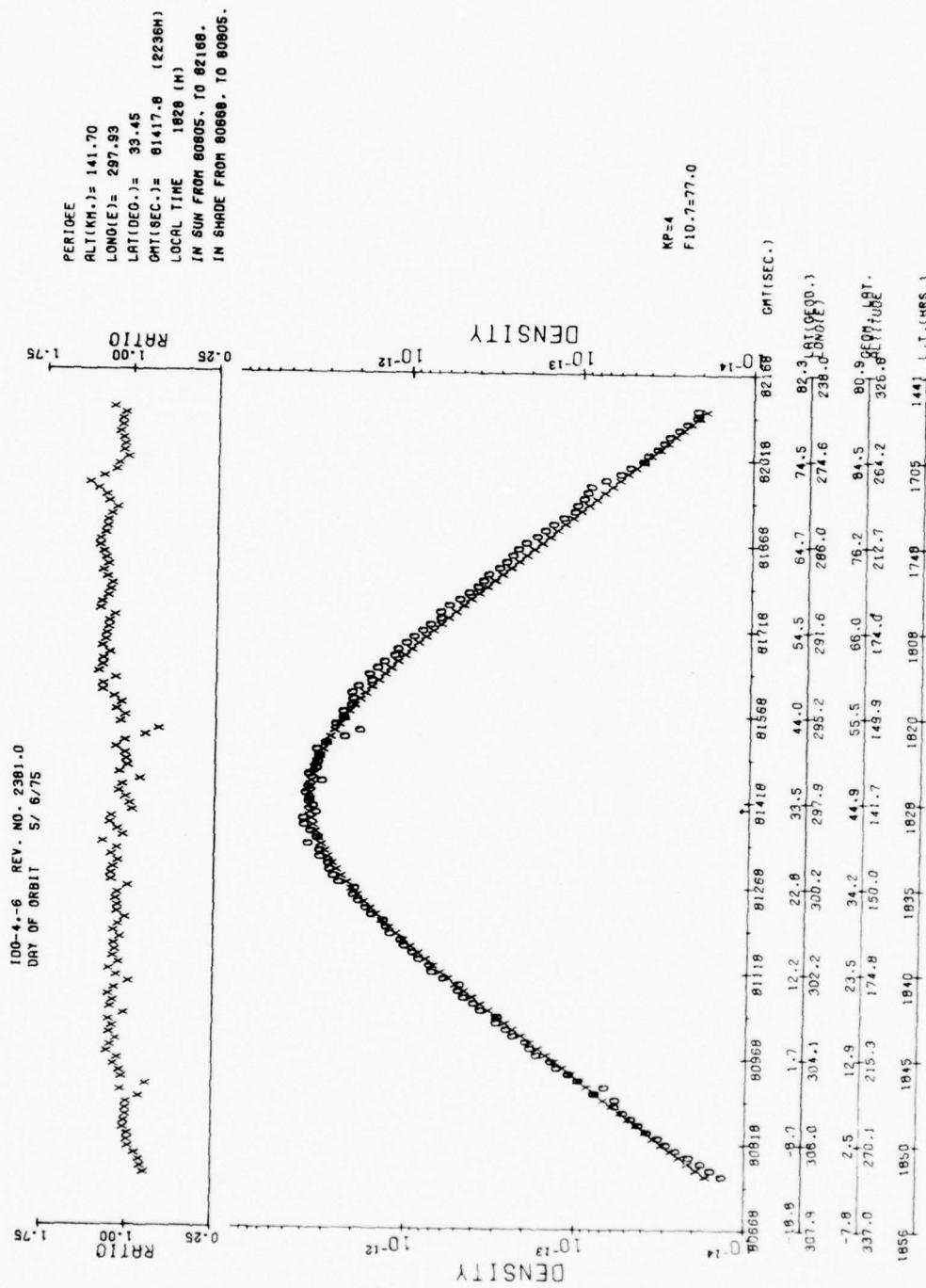


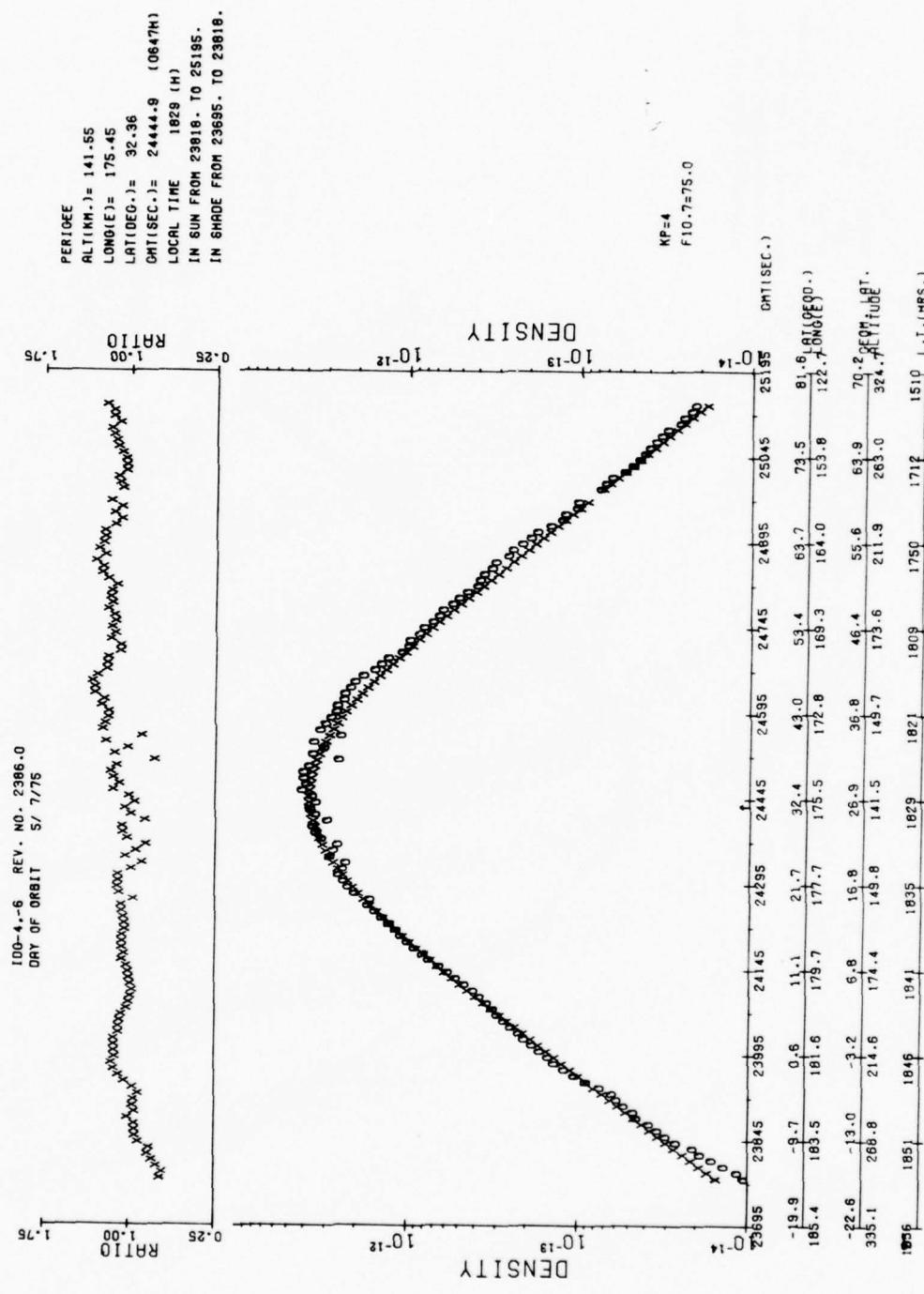


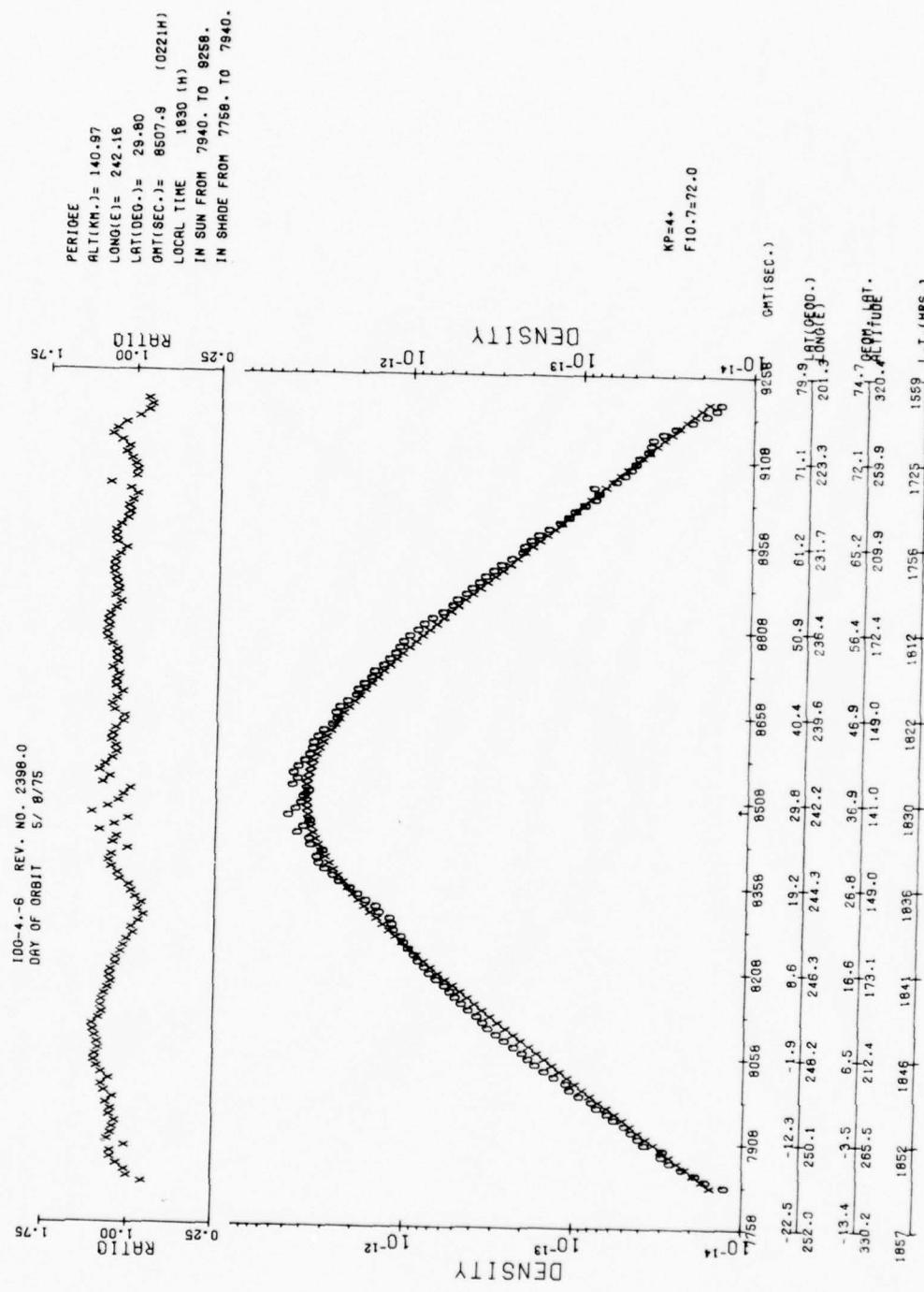


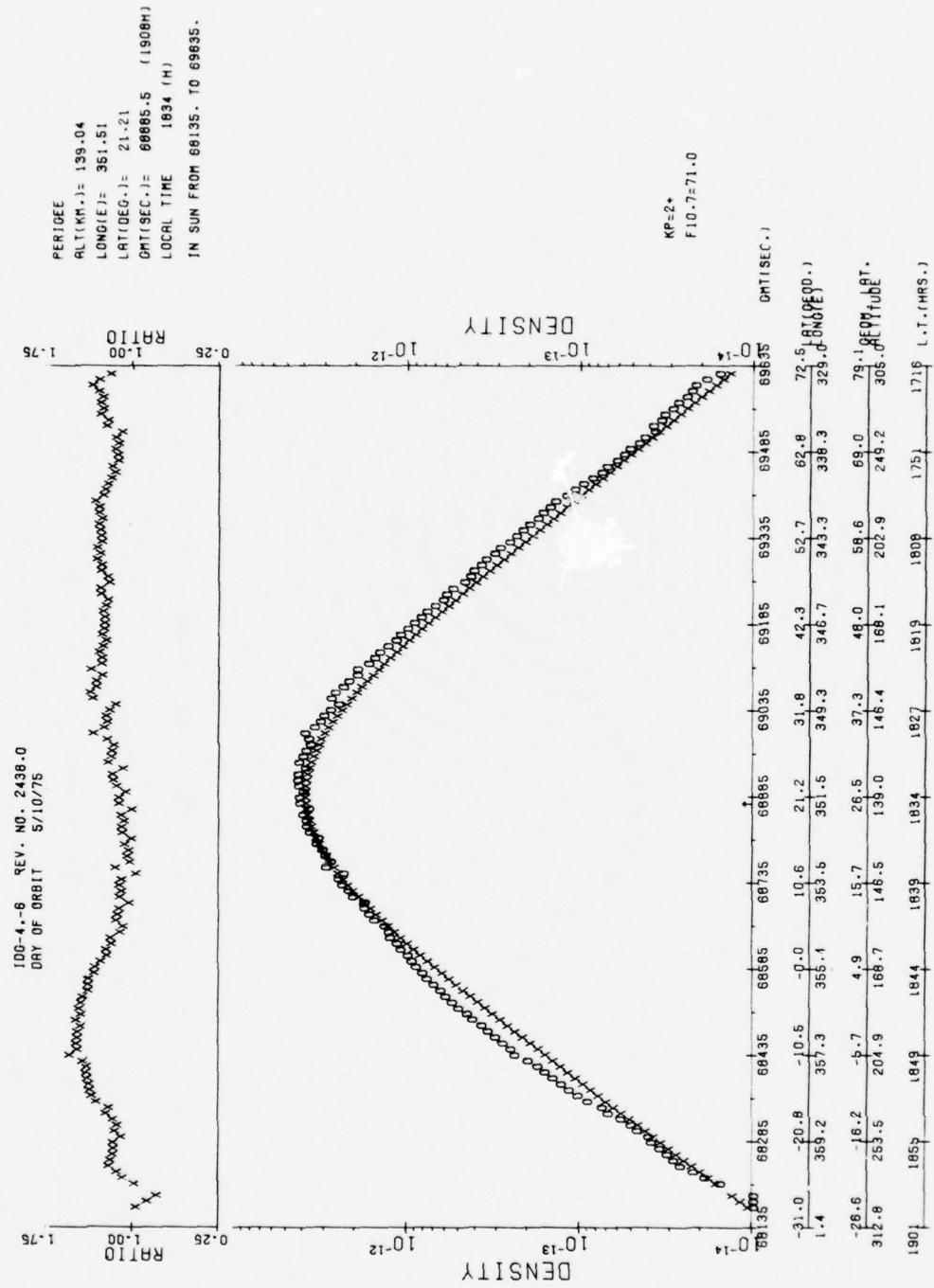
100-4-6 REV. NO. 2377.0
DAY OF ORBIT 5/ 8/75

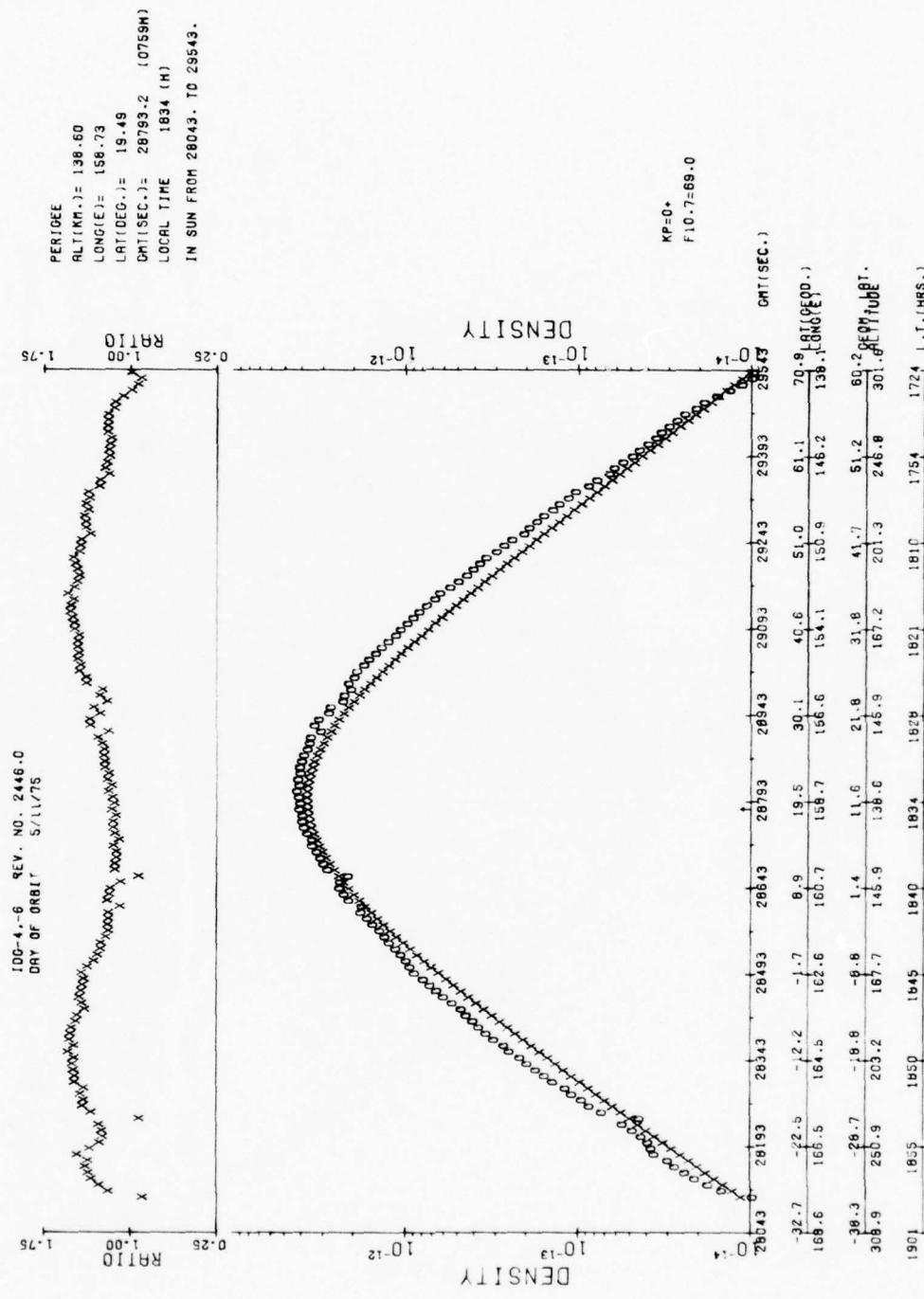












100-4.-6 REV. NO. 2448.0
DAY OF ORBIT 5/11/75

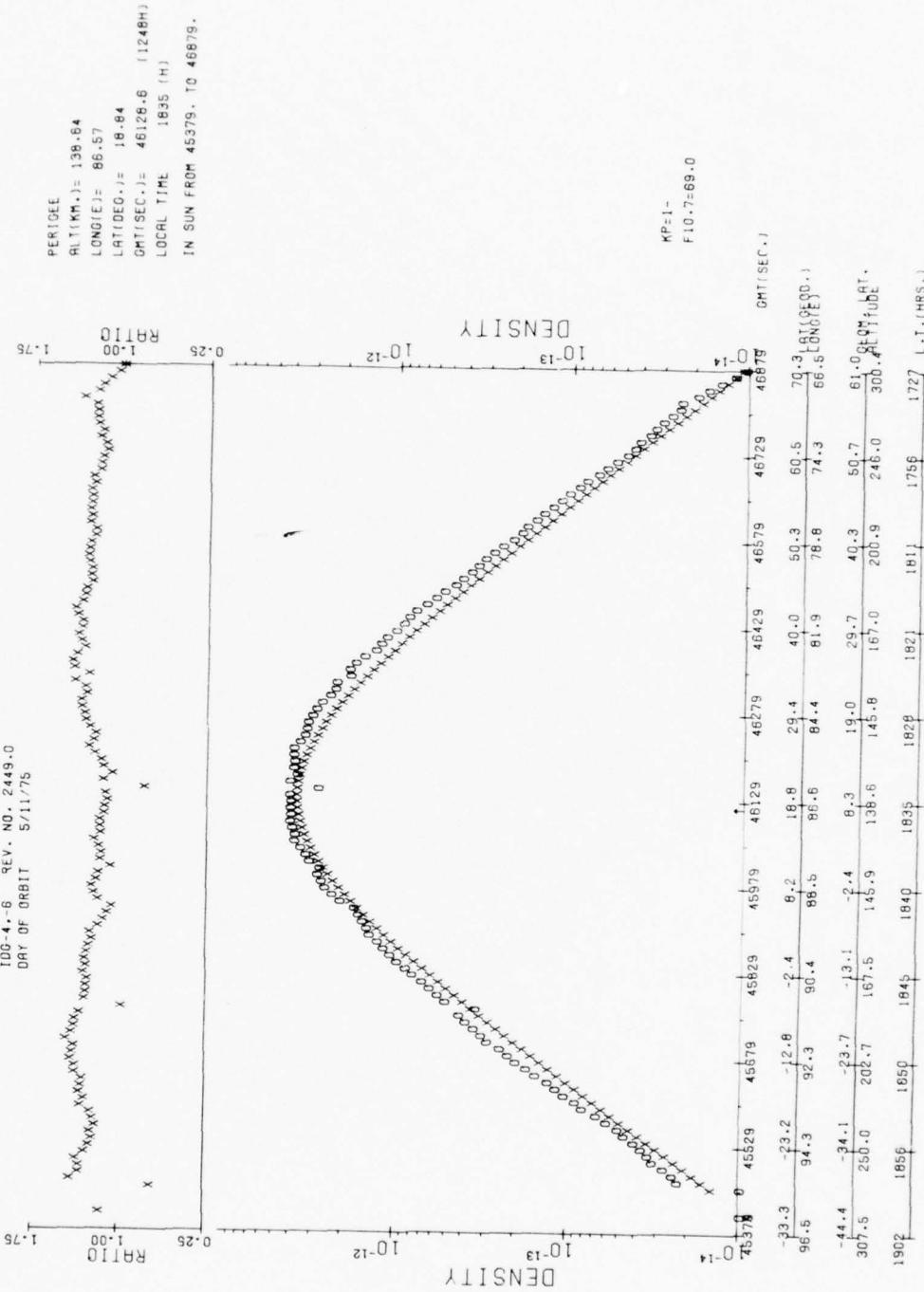
IDG-4,-6 QEV. NO. 2446-0
 DAY OF ORBIT - 5/11/75

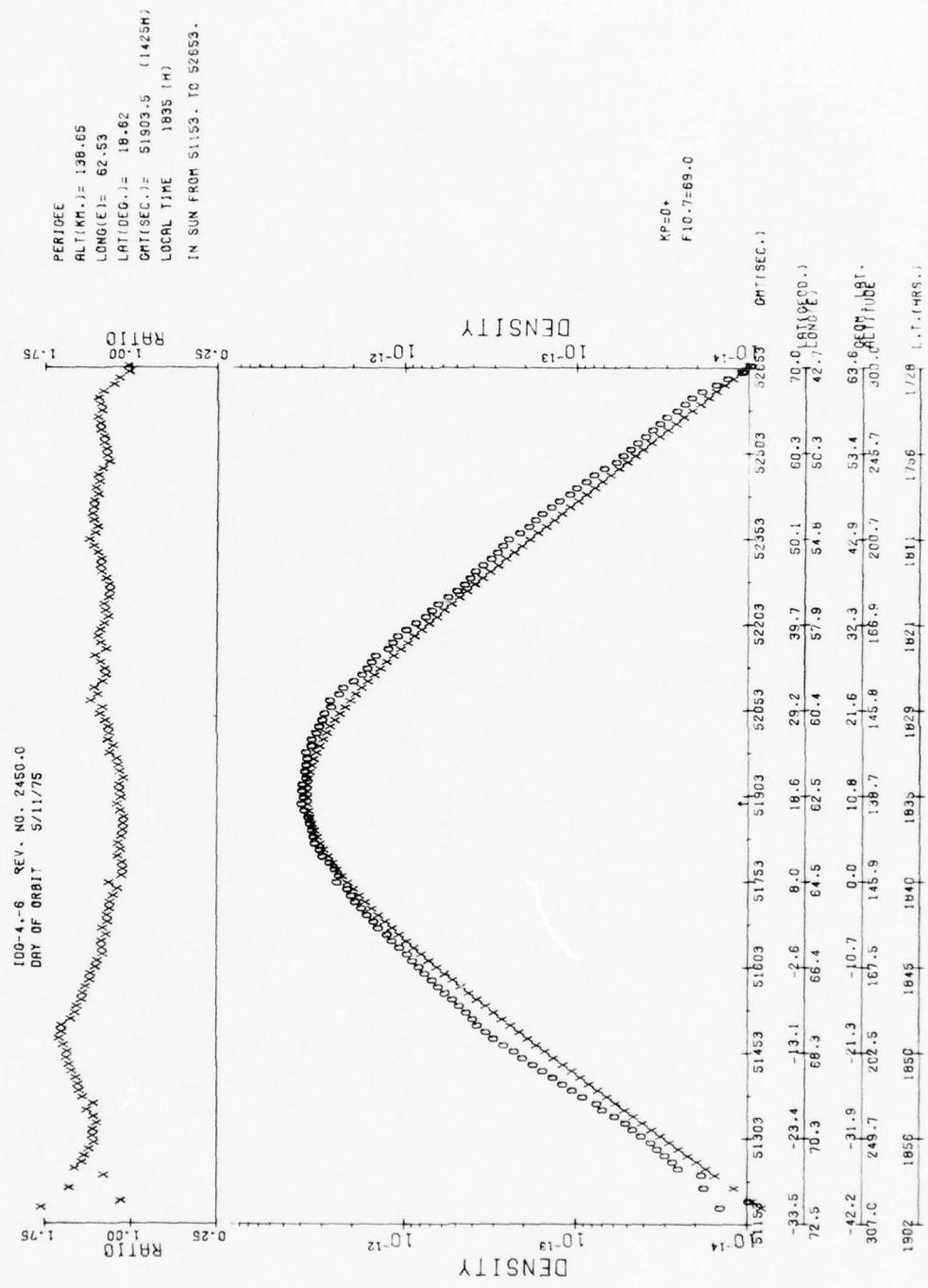
PERIGEE
 ALT (KM.) = 138.63
 LONG (E) = 110.62
 LAT (DEG.) = 19.06
 GMT (SEC.) = 40351.9 (11112H)
 LOCAL TIME = 1834 (H)
 IN SUN FROM 39602. TO 41102.

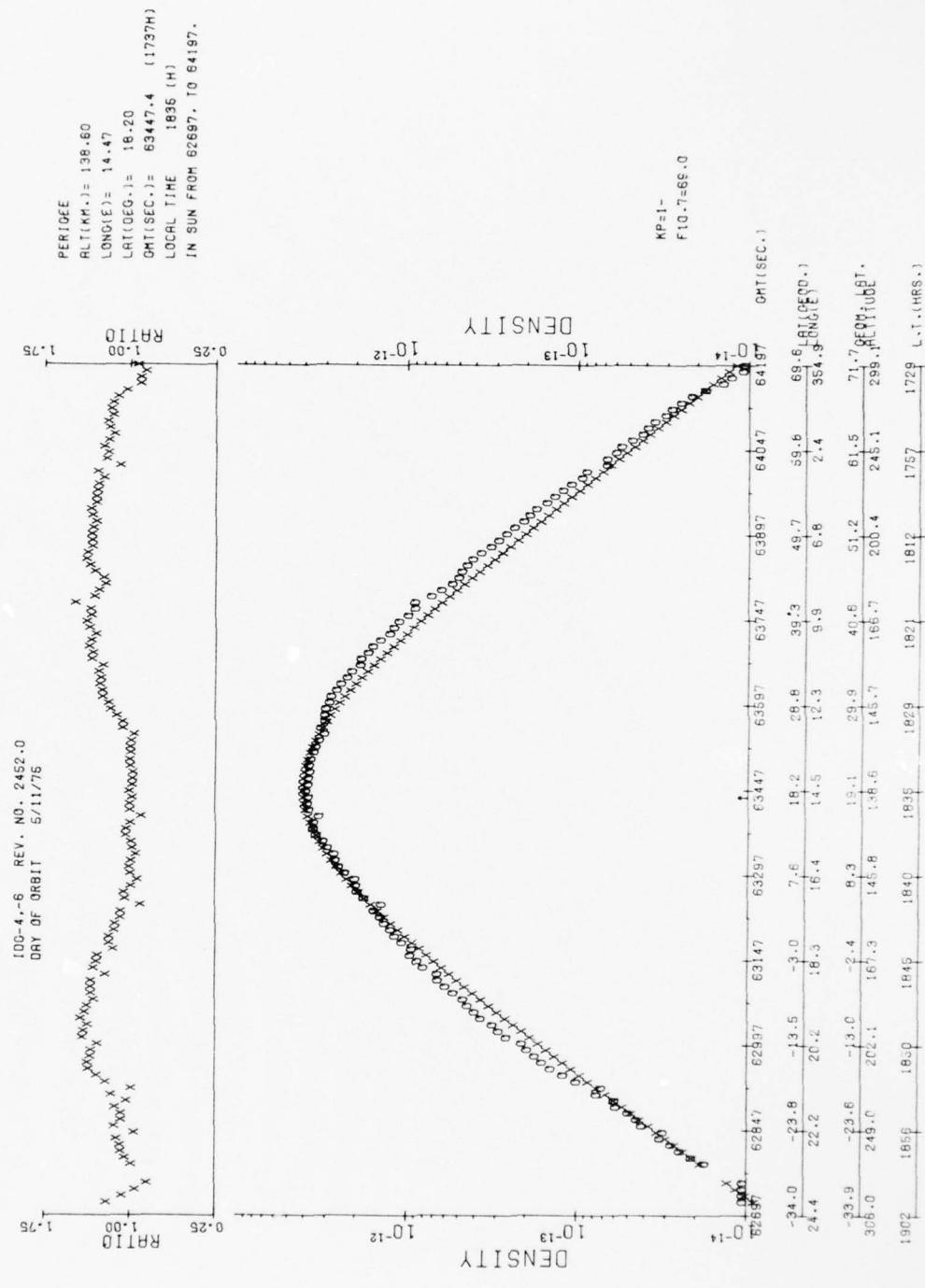
KF=1-
 F(10,7)=69.0

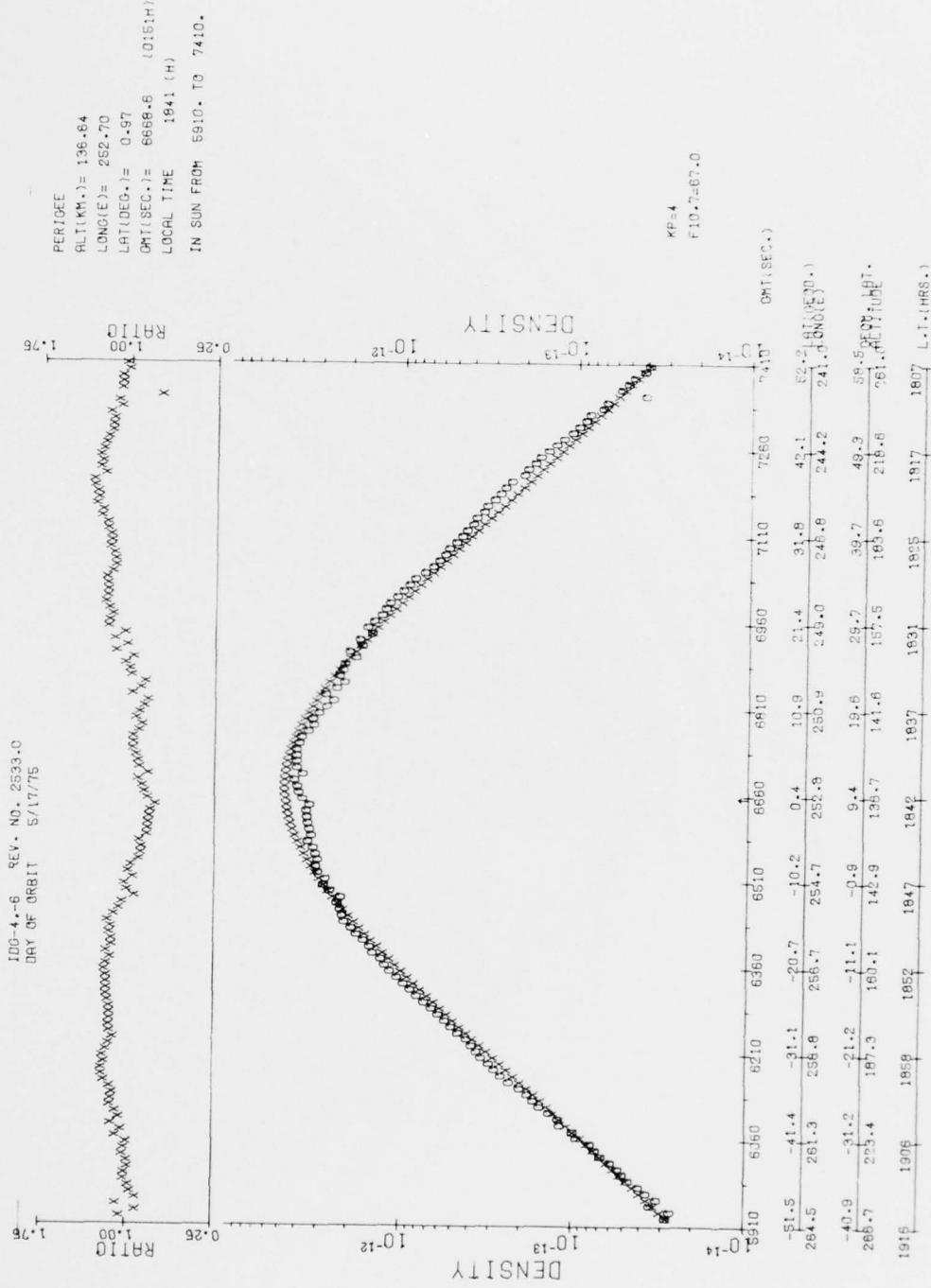
| RatiO | DENSITY (Open Circles) | DENSITY (Crosses) | GMT (SEC.) |
|-------|------------------------|----------------------|------------|
| 39602 | ~10 ^{-11.5} | ~10 ^{-11.5} | 40352 |
| 39752 | ~10 ^{-11.2} | ~10 ^{-11.2} | 40202 |
| 39902 | ~10 ^{-11.0} | ~10 ^{-11.0} | 40052 |
| 40052 | ~10 ^{-10.8} | ~10 ^{-10.8} | 39902 |
| 40202 | ~10 ^{-10.6} | ~10 ^{-10.6} | 39752 |
| 40352 | ~10 ^{-10.4} | ~10 ^{-10.4} | 39902 |
| 40502 | ~10 ^{-10.2} | ~10 ^{-10.2} | 40052 |
| 40652 | ~10 ^{-10.0} | ~10 ^{-10.0} | 40202 |
| 40802 | ~10 ^{-9.8} | ~10 ^{-9.8} | 40352 |
| 40952 | ~10 ^{-9.6} | ~10 ^{-9.6} | 40502 |
| 41102 | ~10 ^{-9.4} | ~10 ^{-9.4} | 40652 |

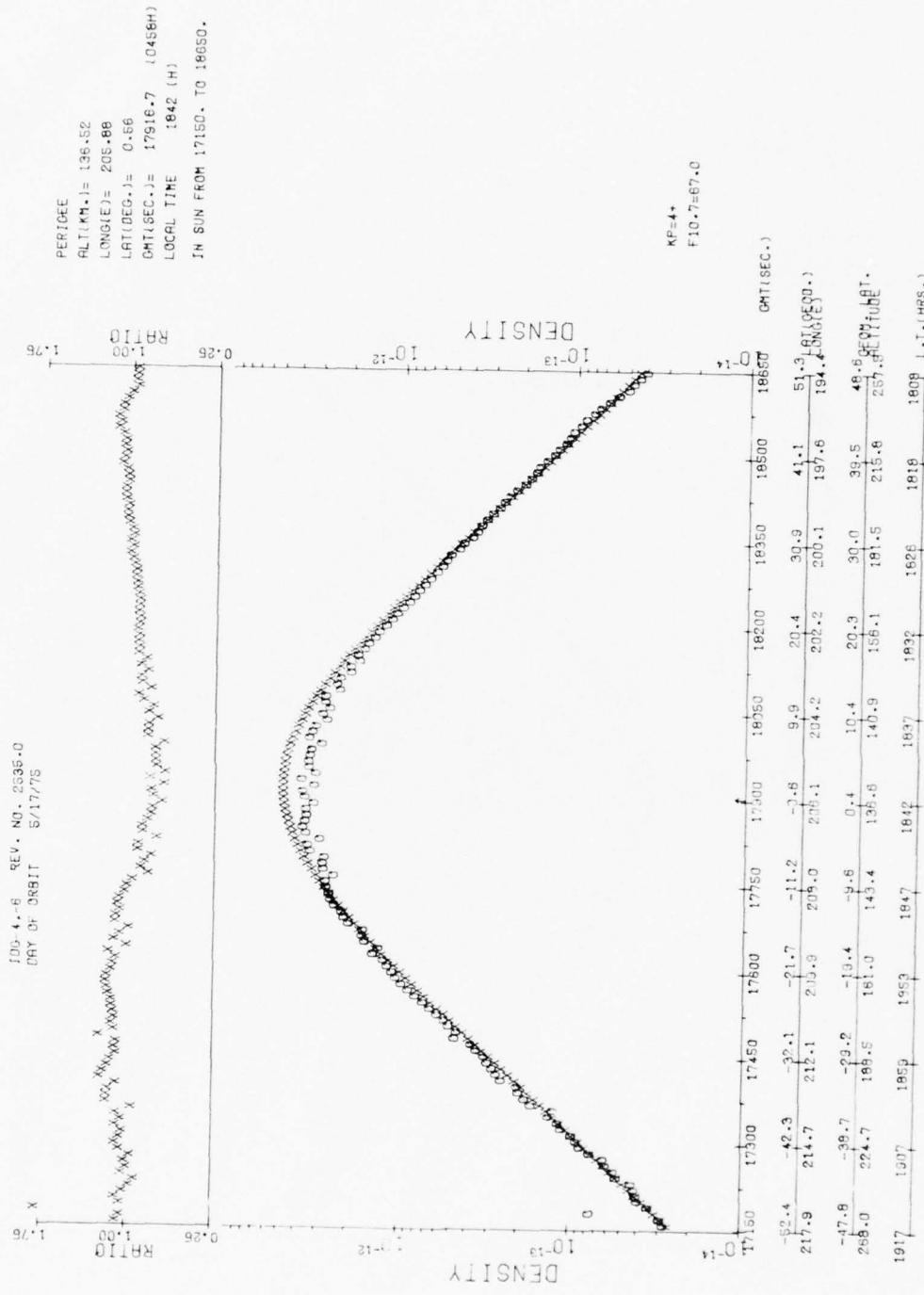
IDG-4,-6 REV. NO. 2449.0
DAY OF ORBIT 5/11/75

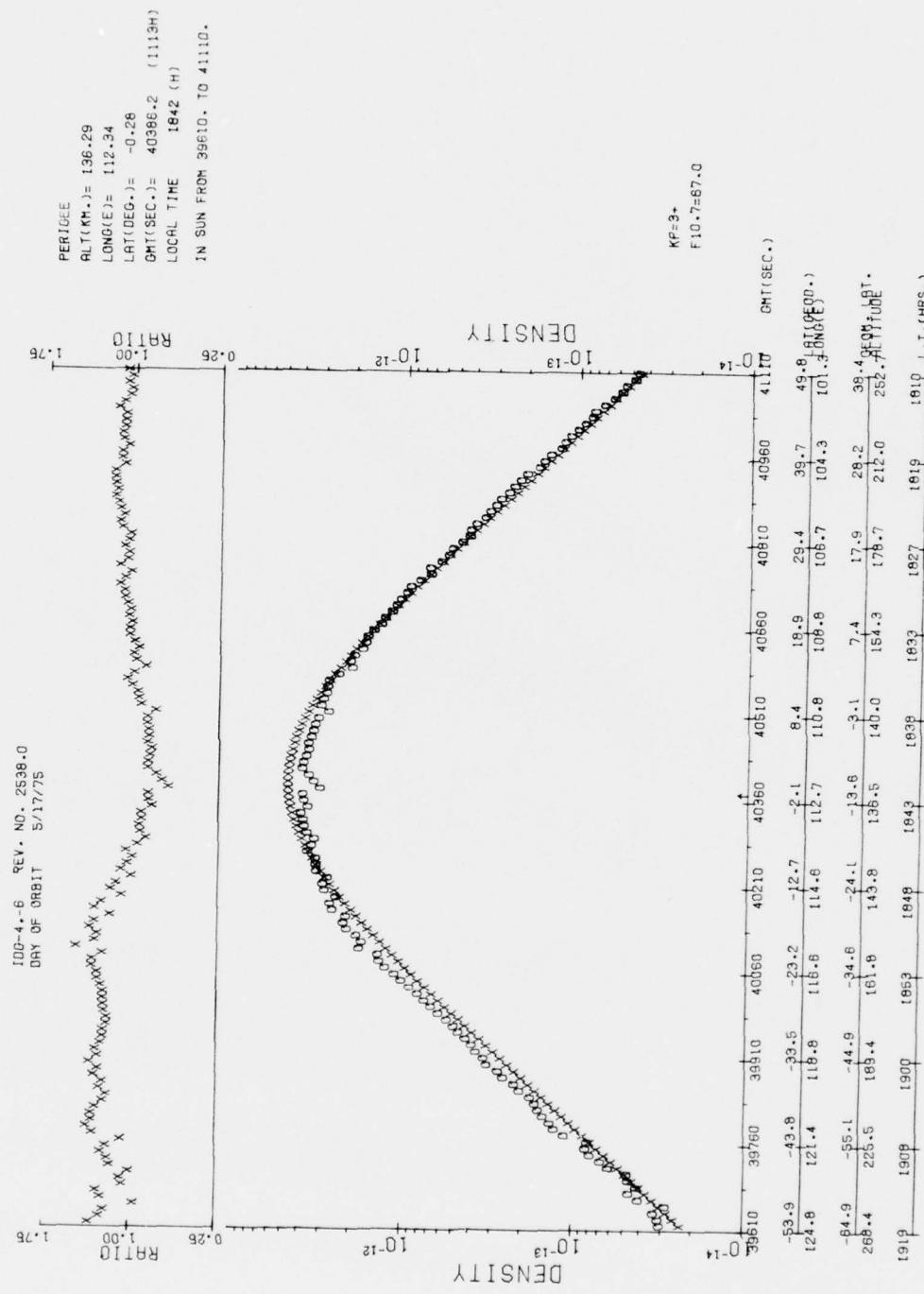


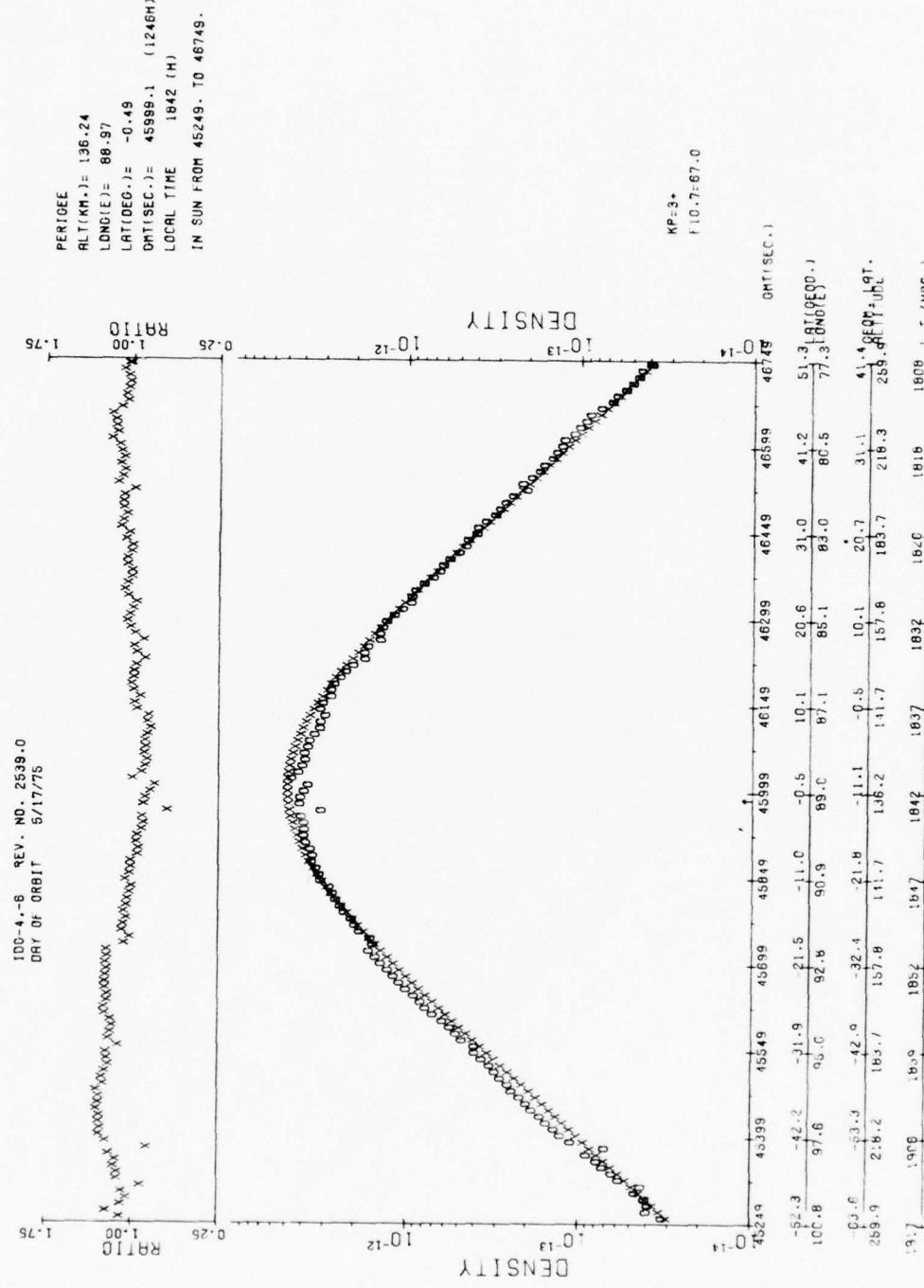


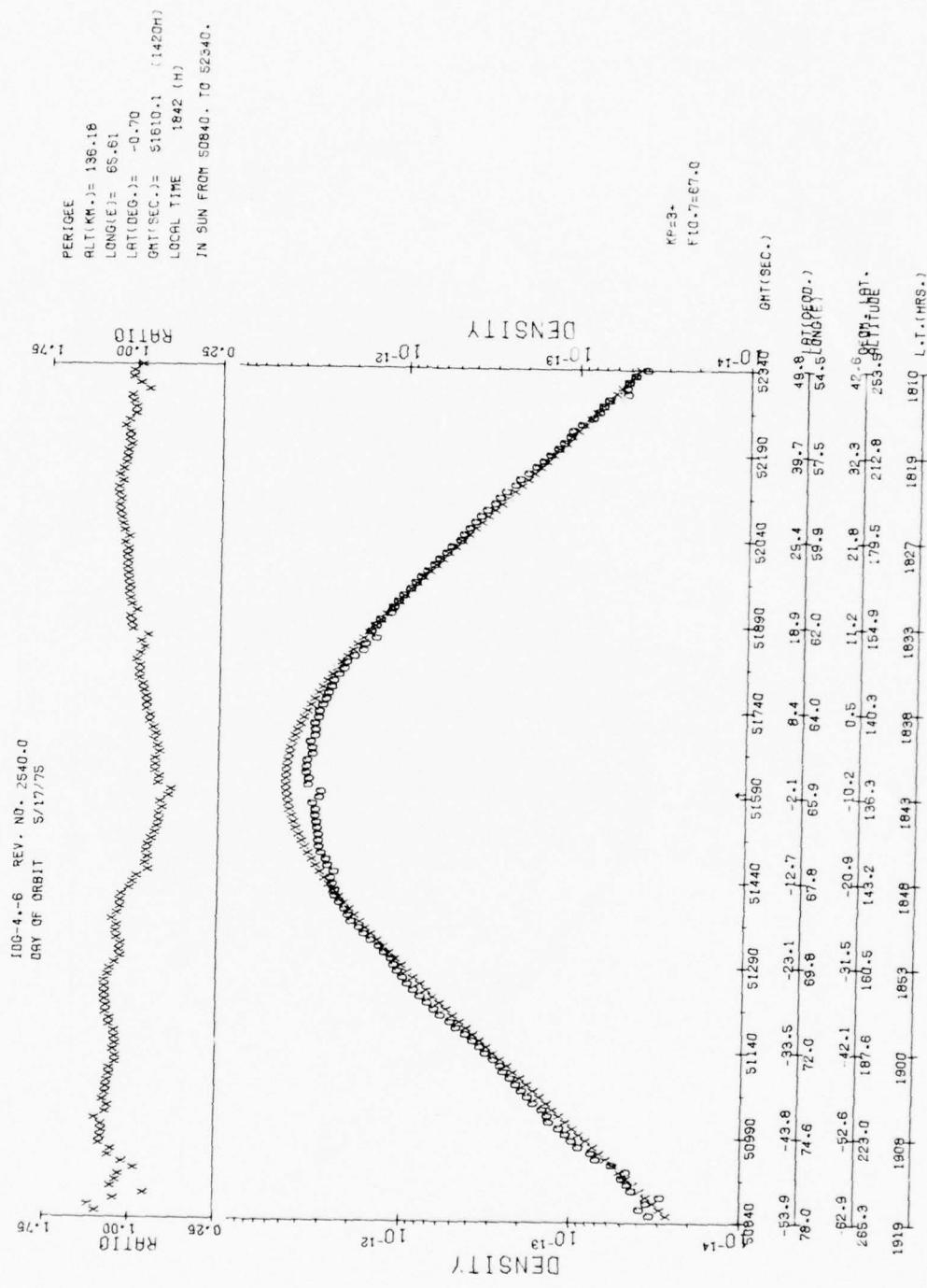


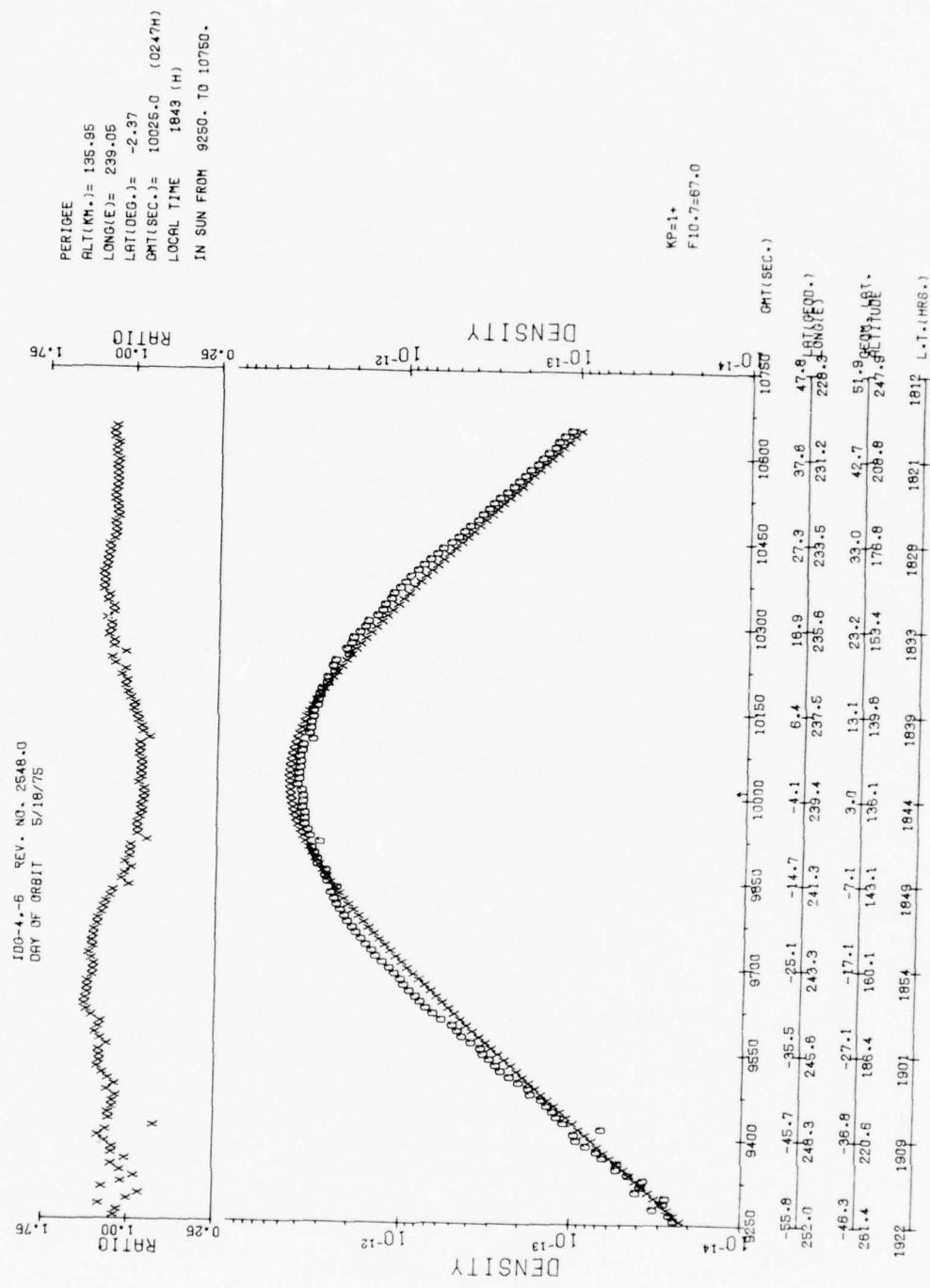


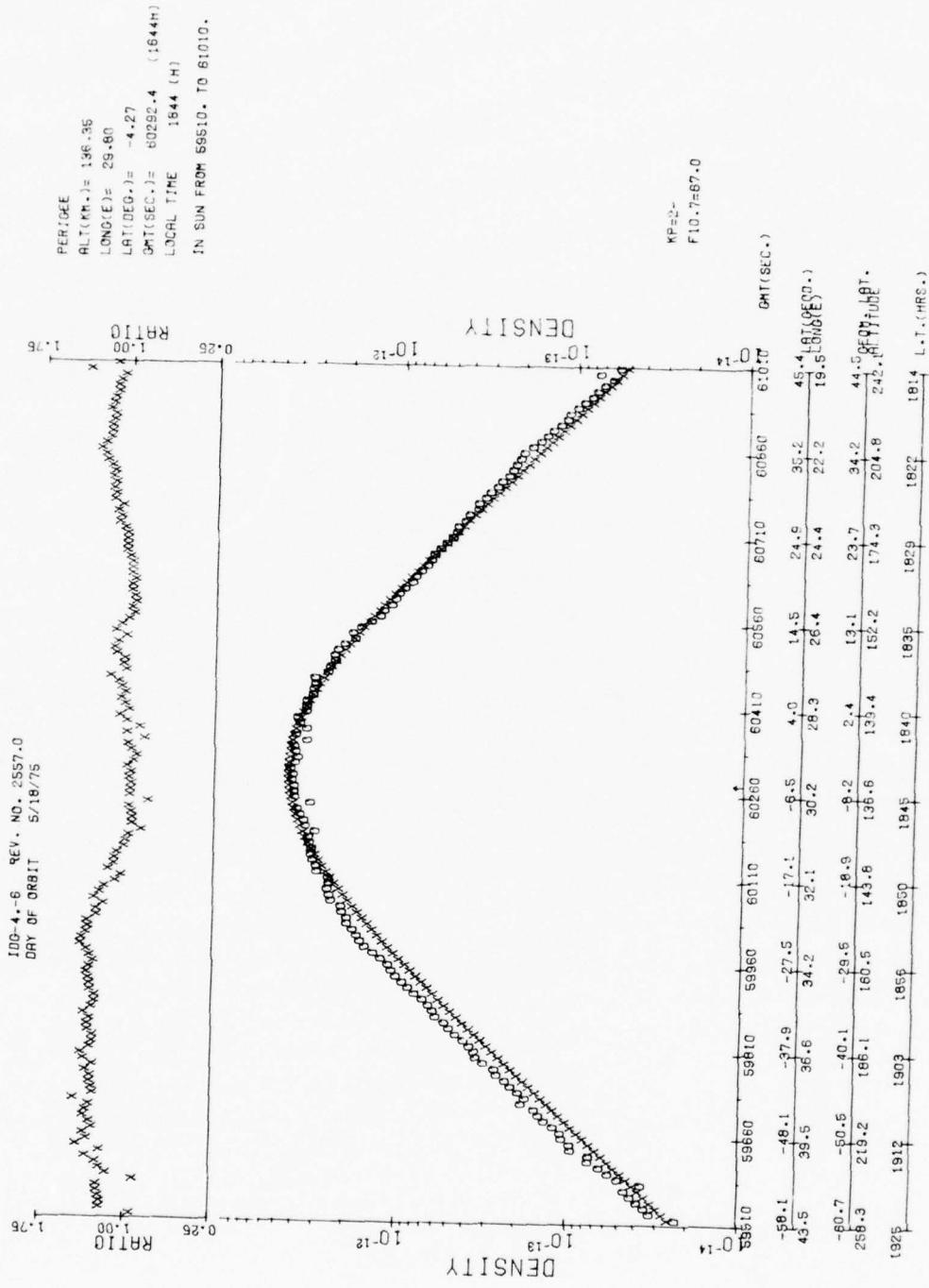




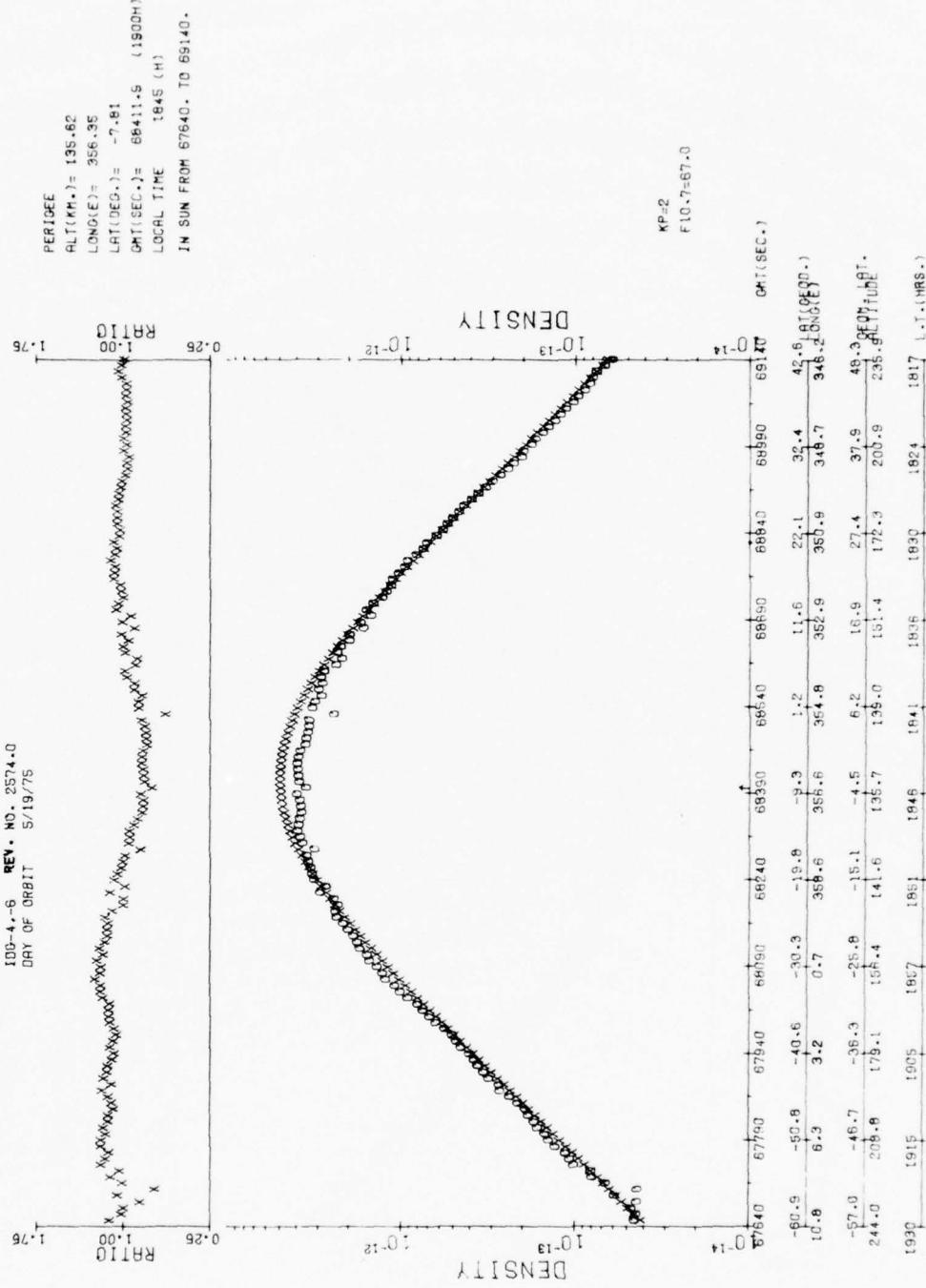


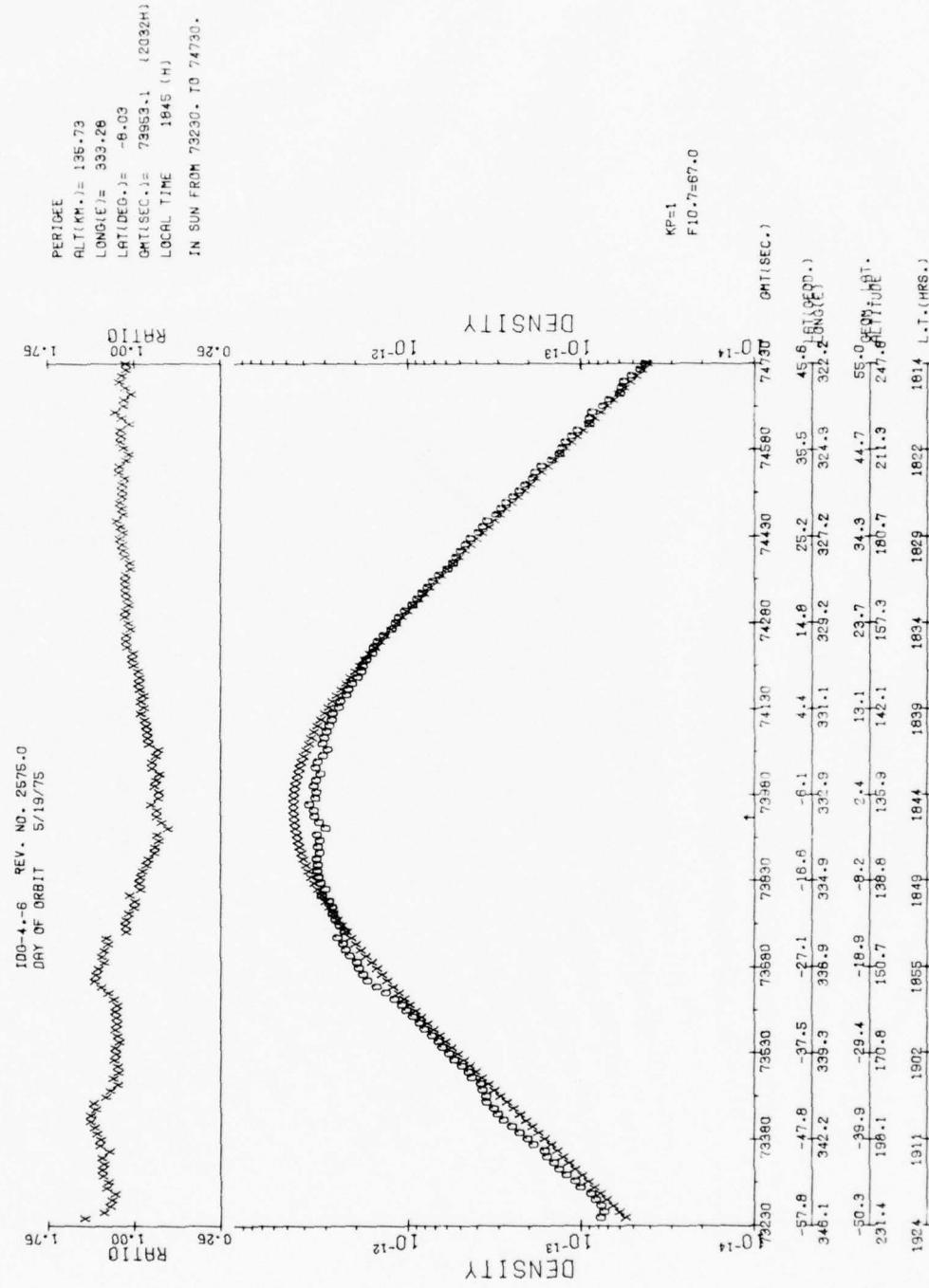


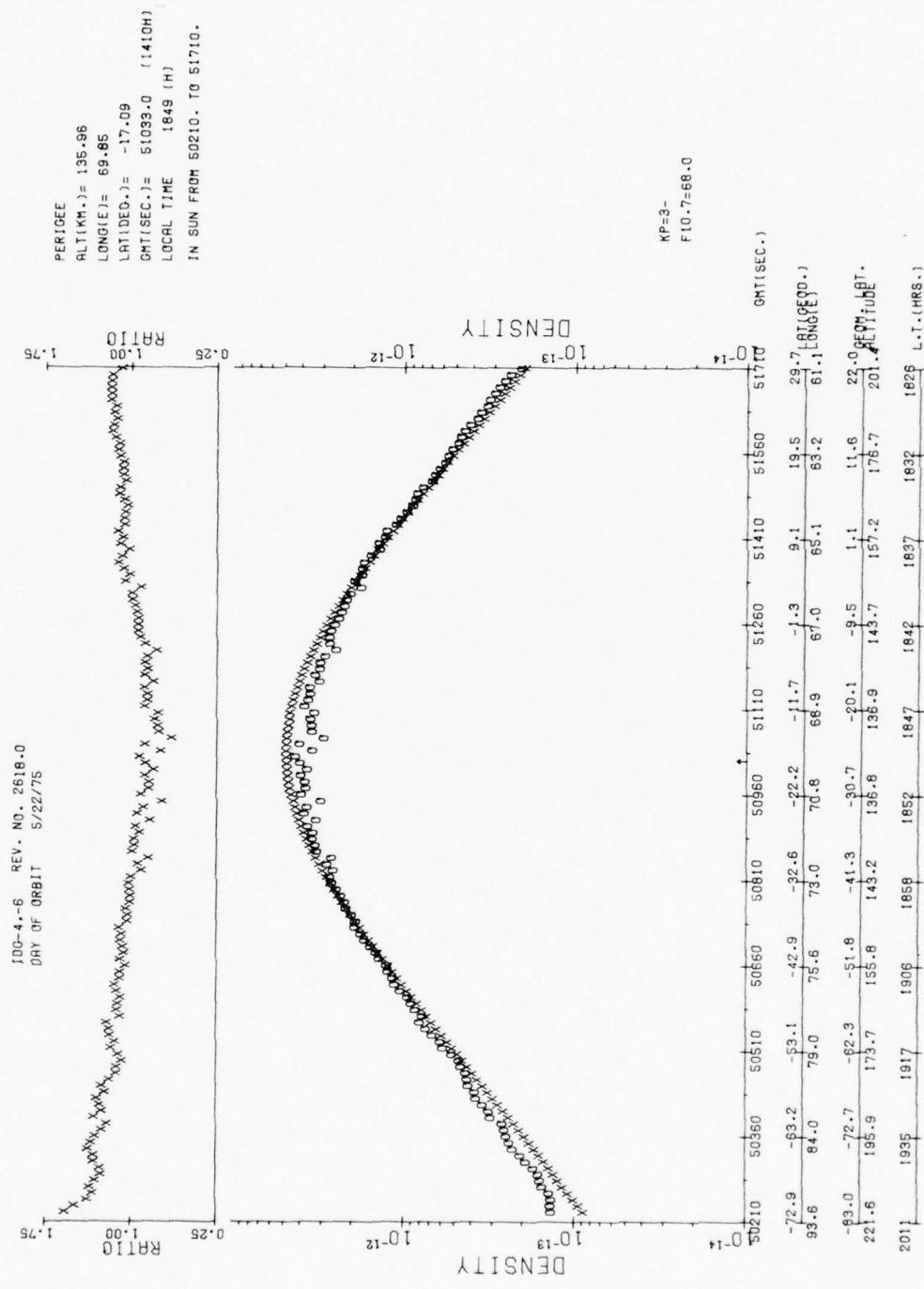




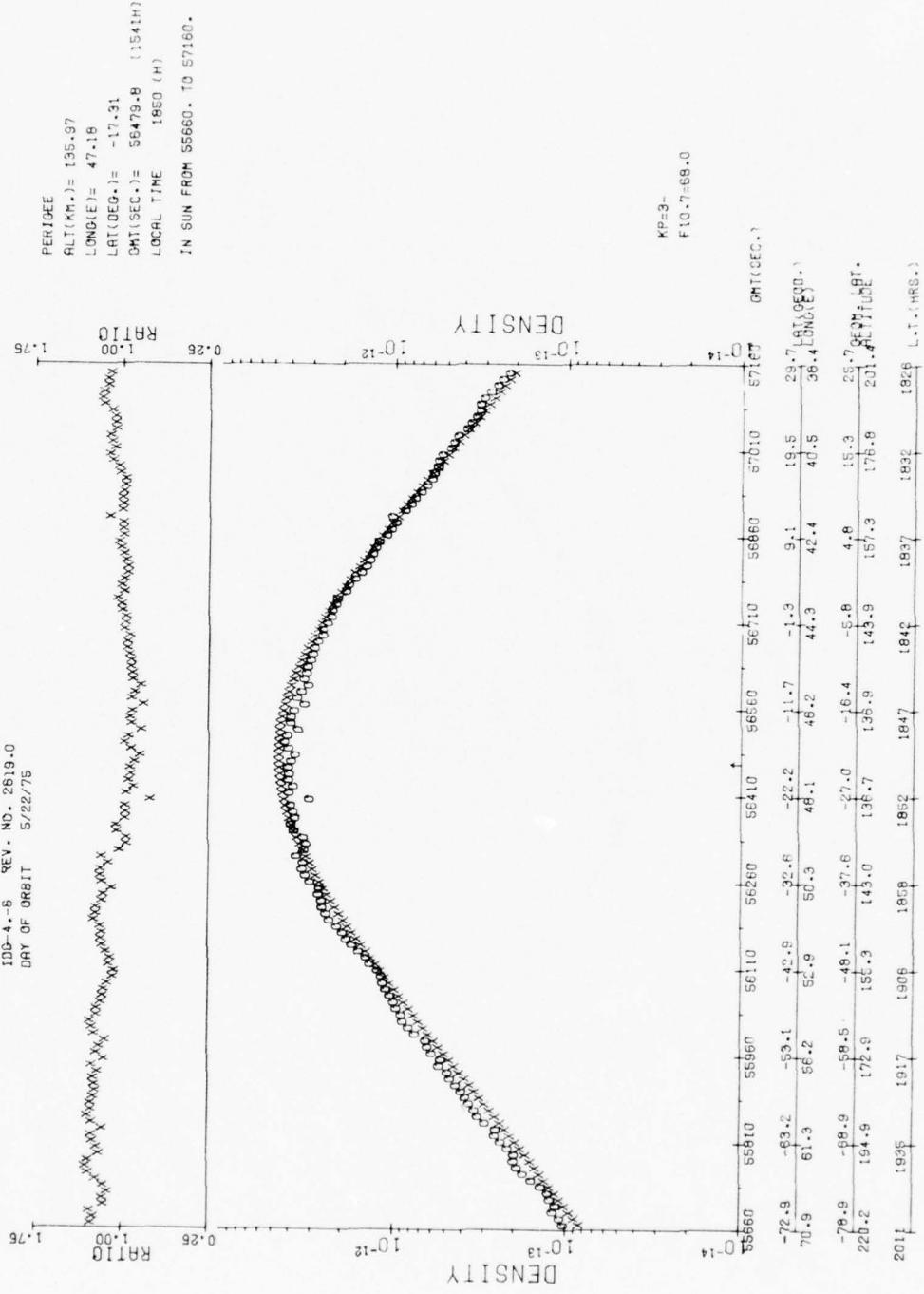
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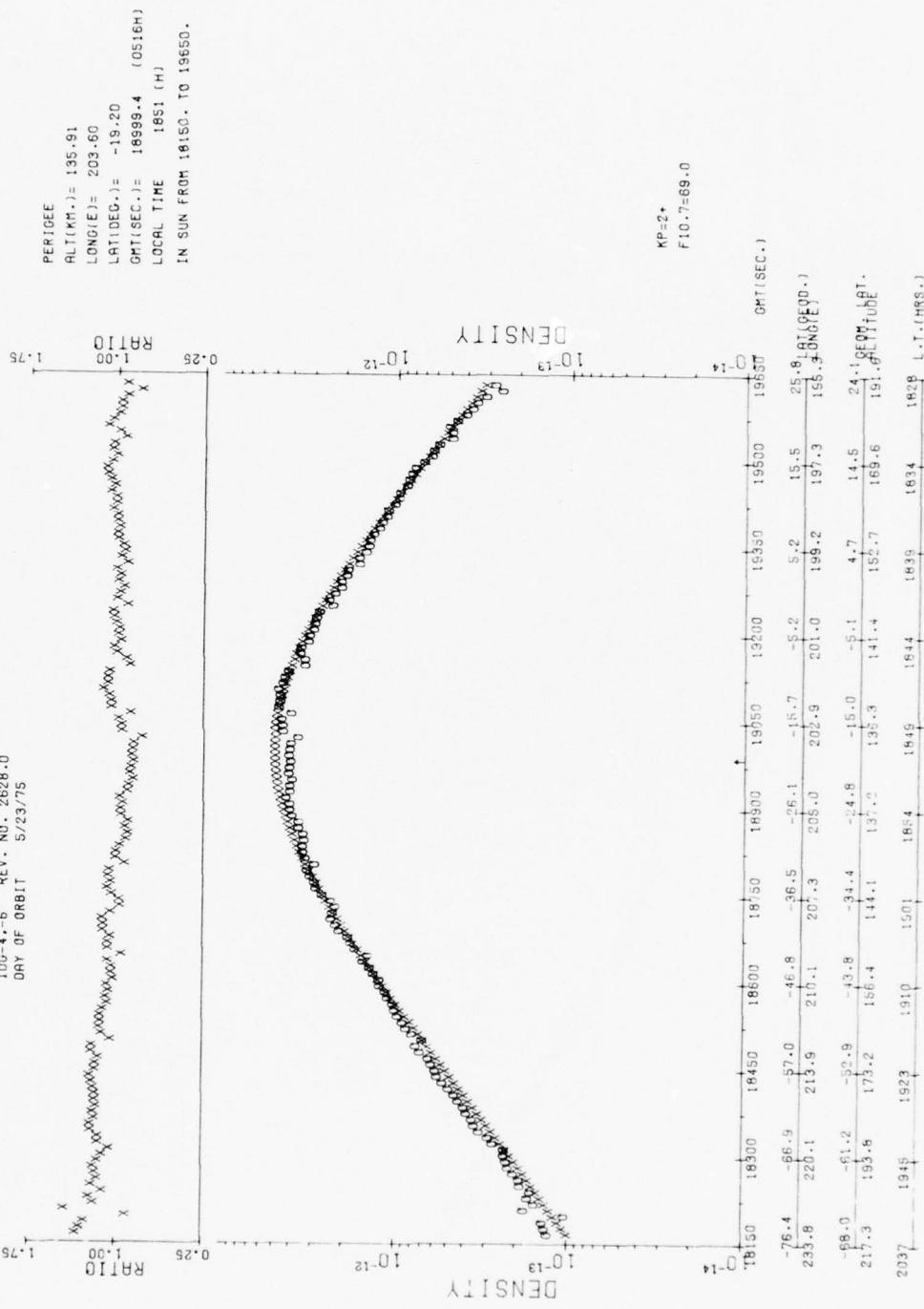


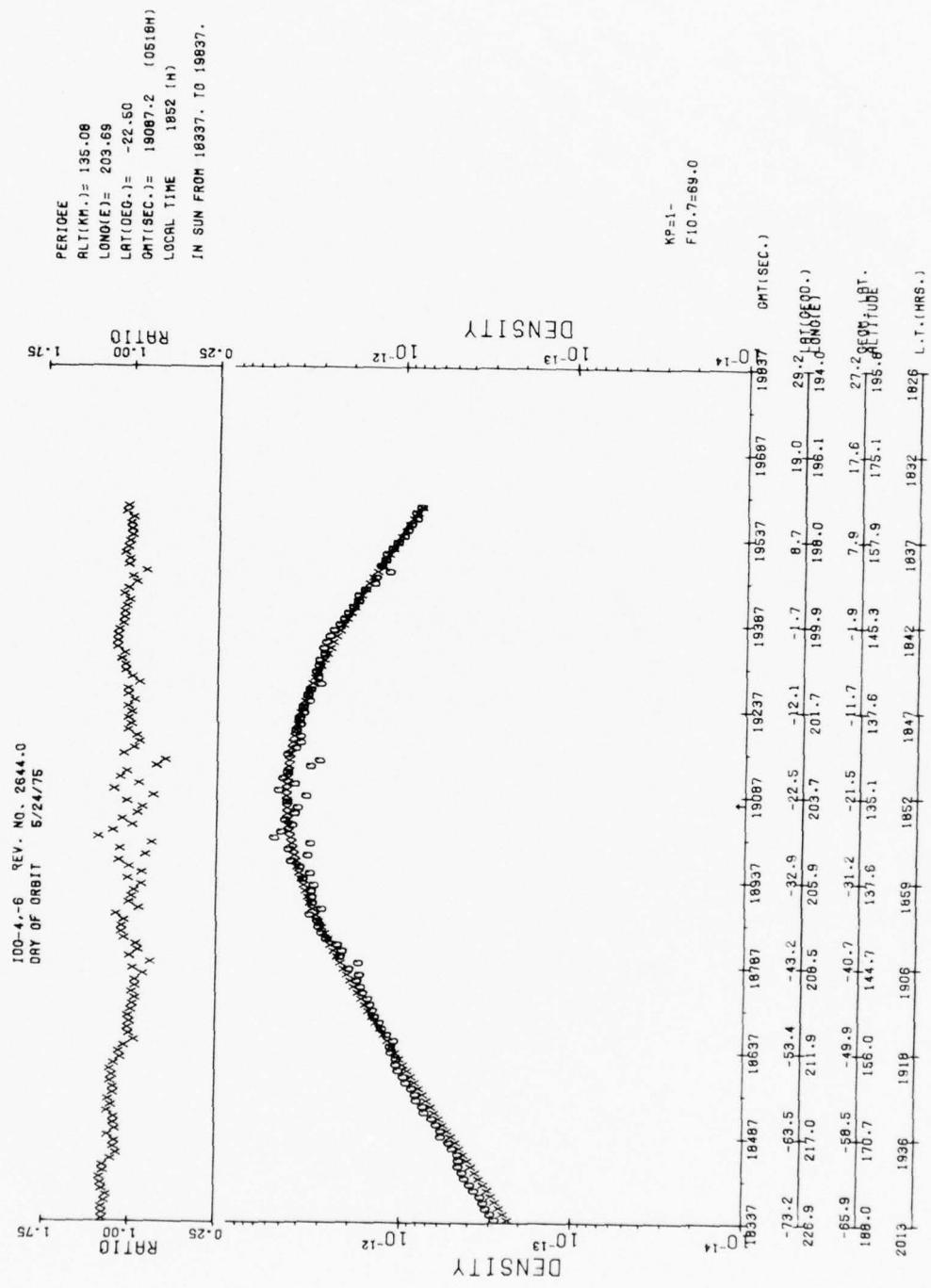


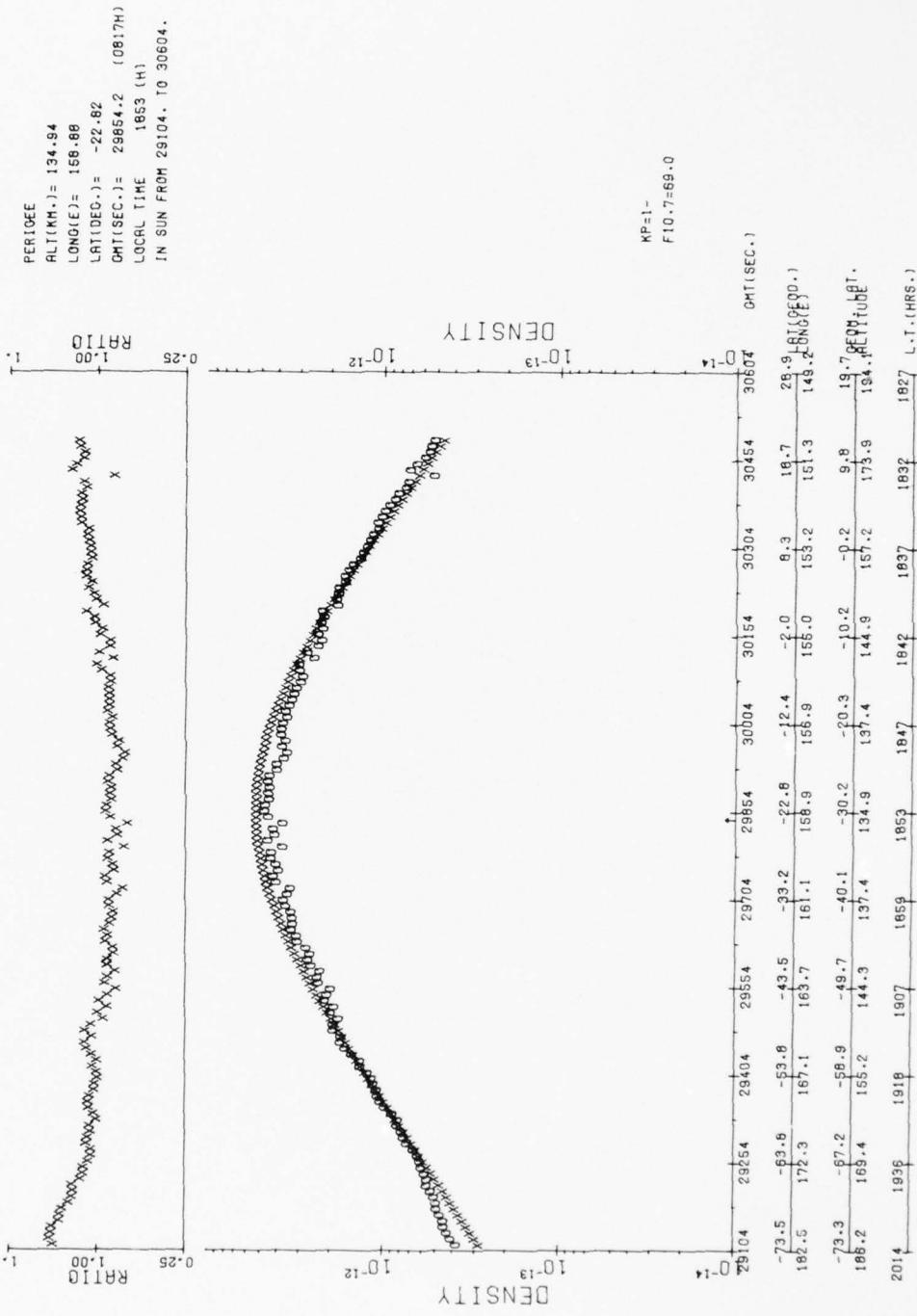
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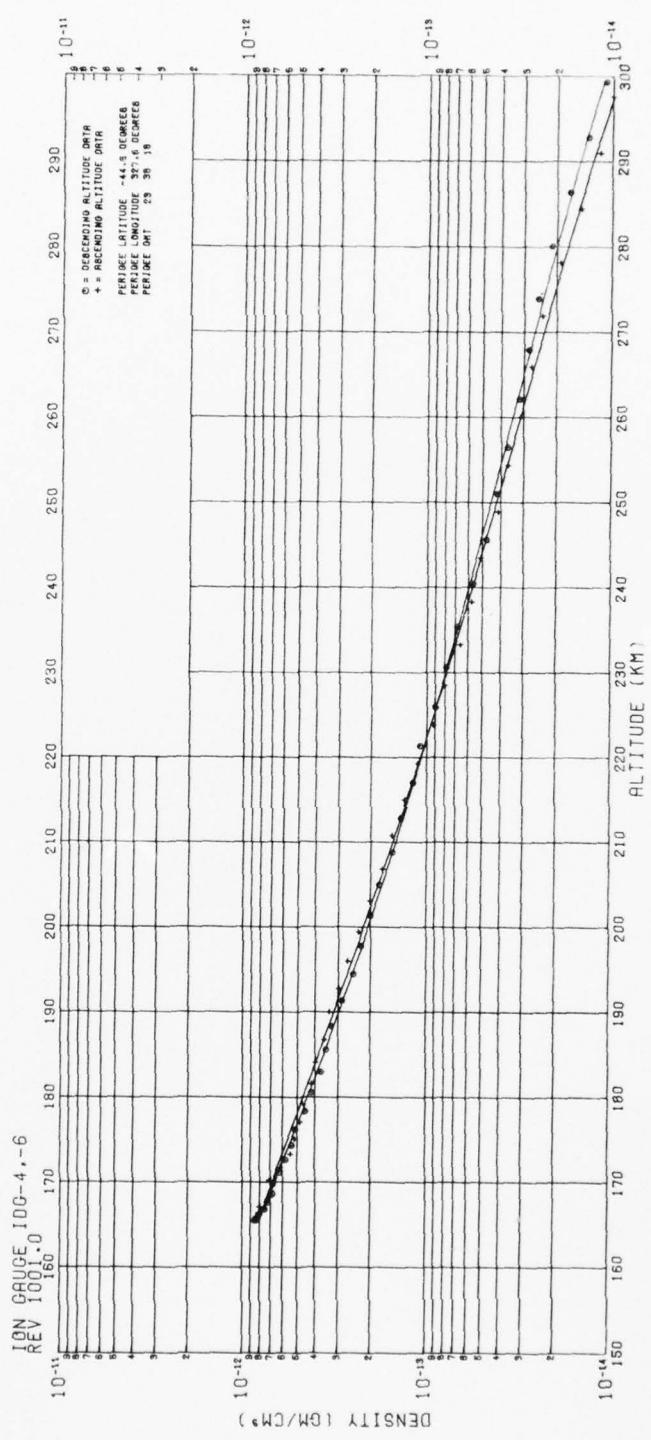


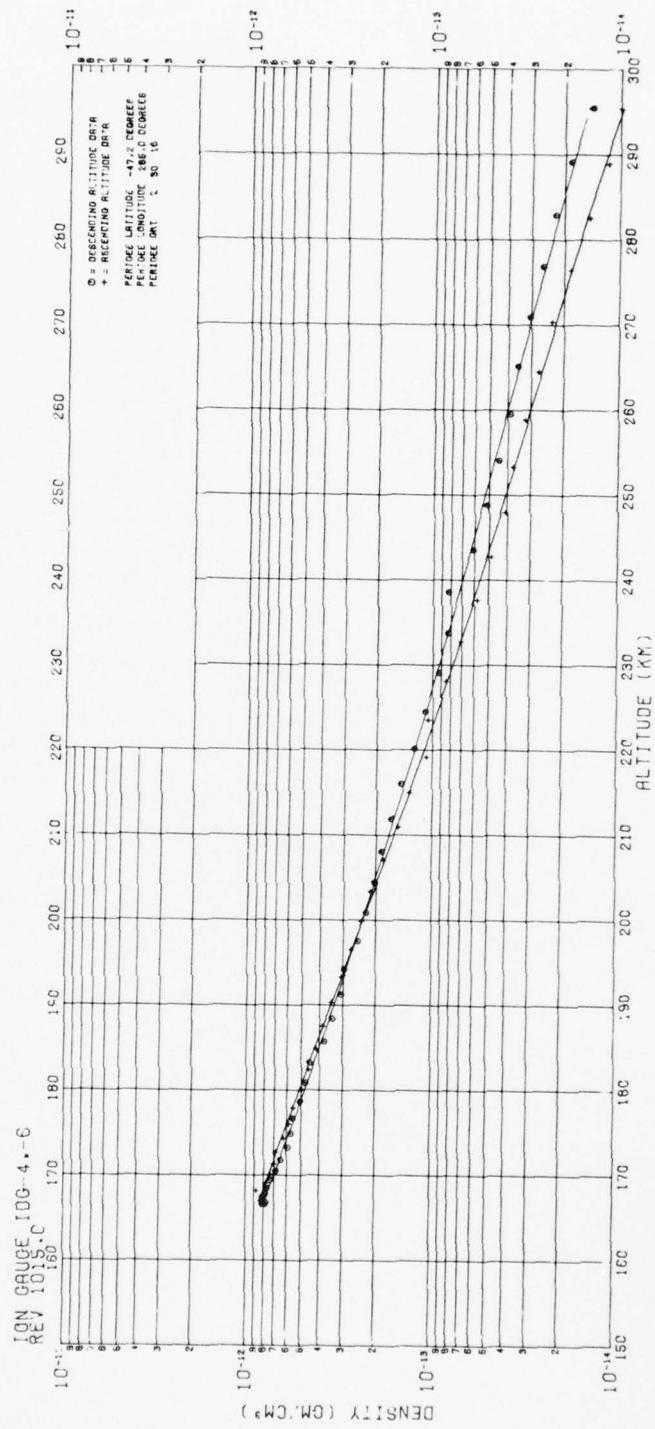


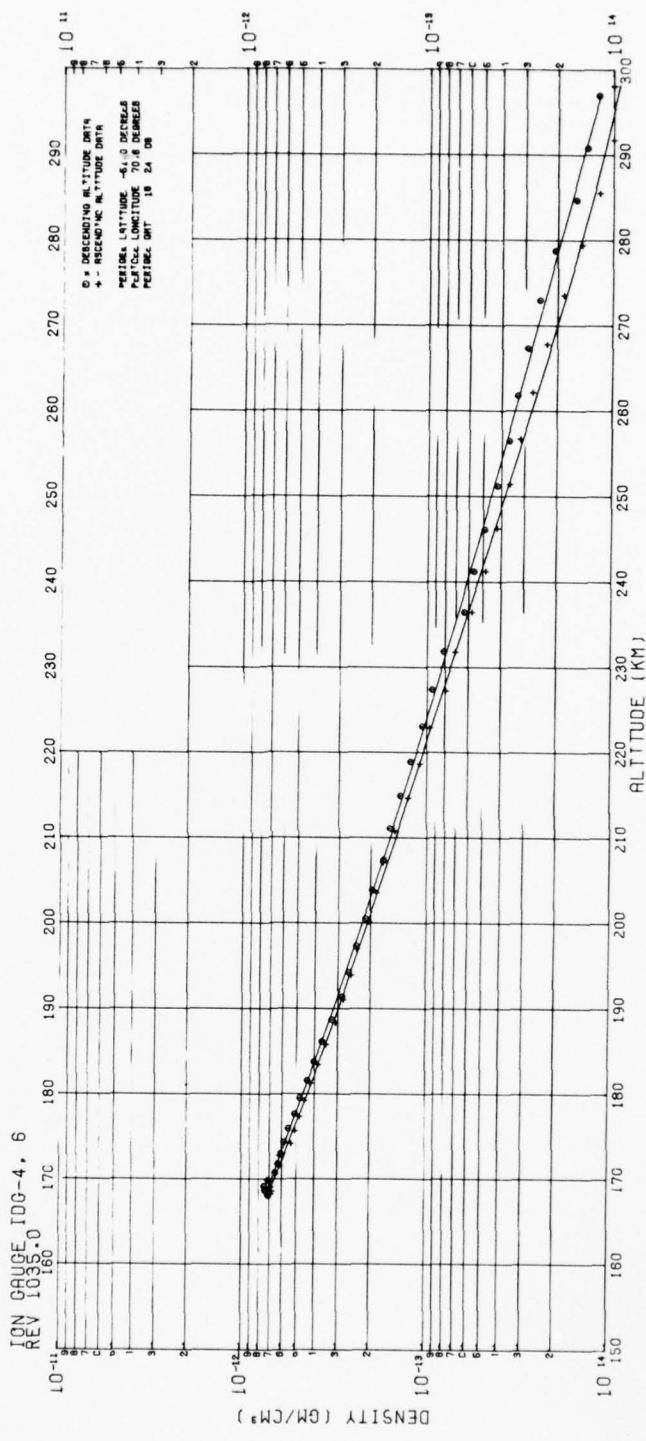


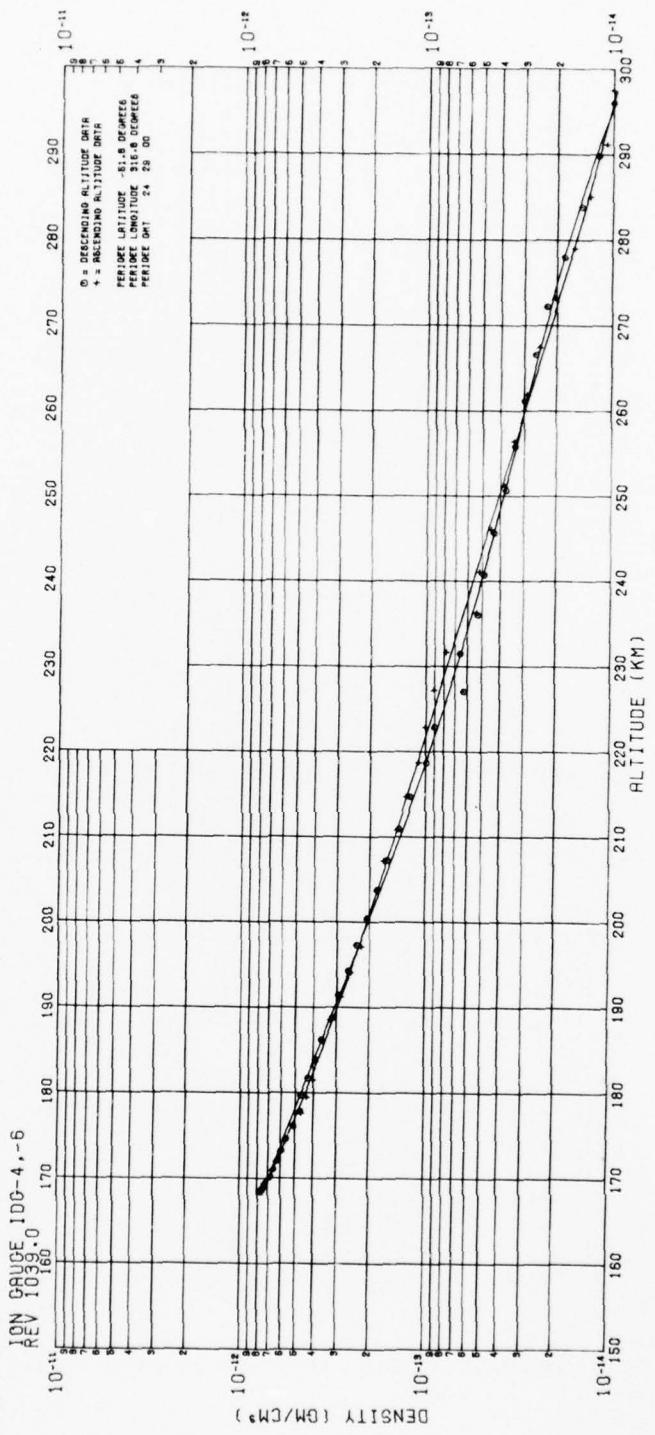
Appendix B

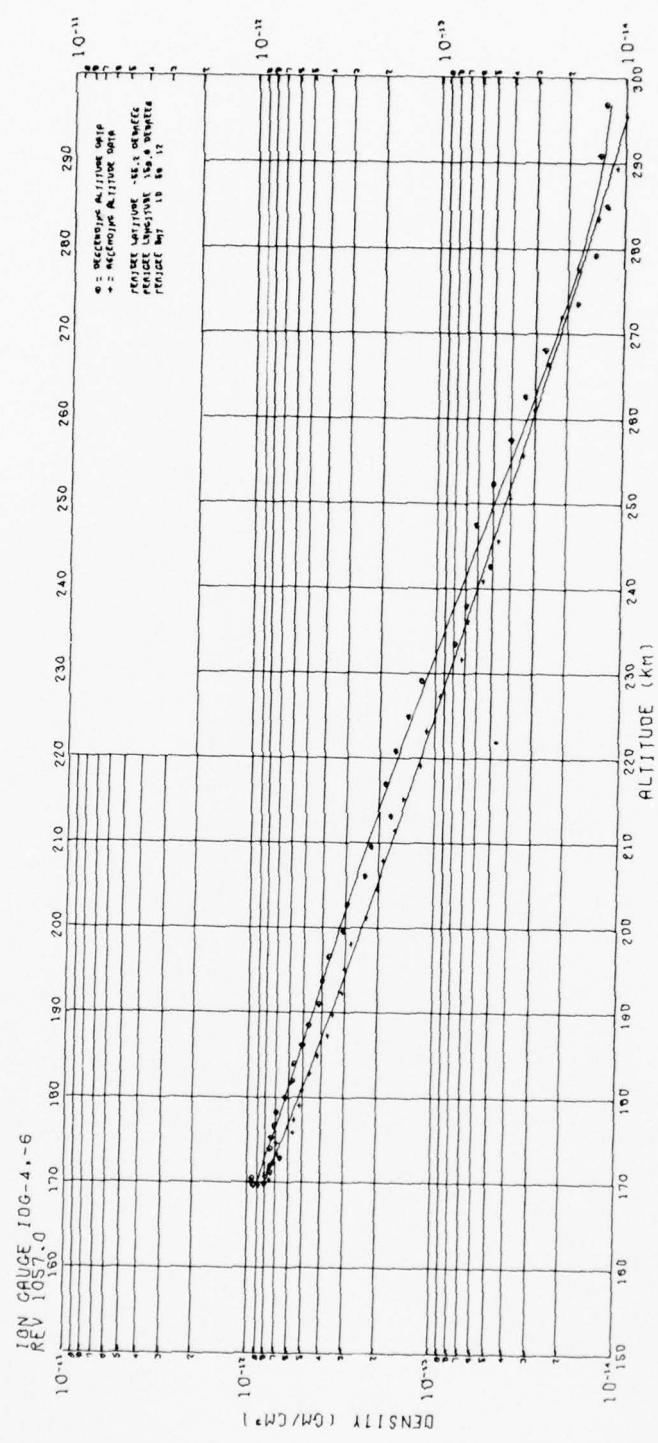
Plots of Density vs Altitude

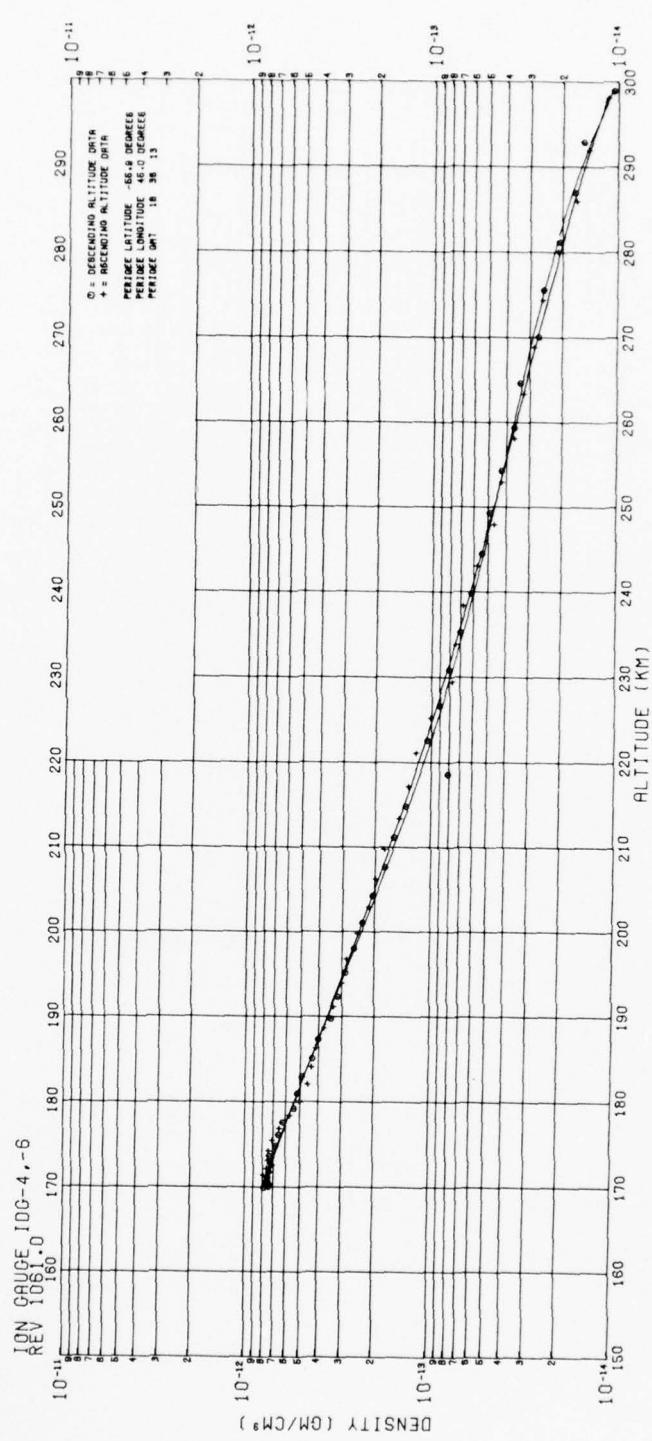


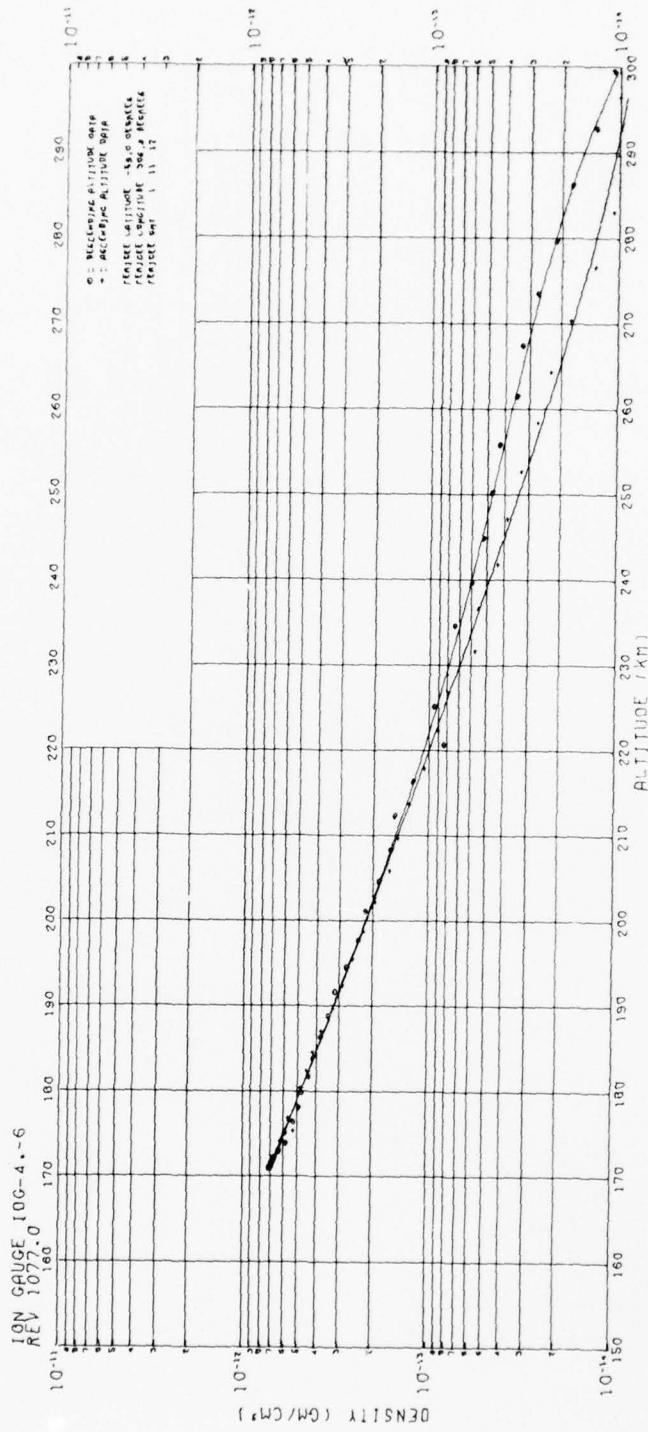


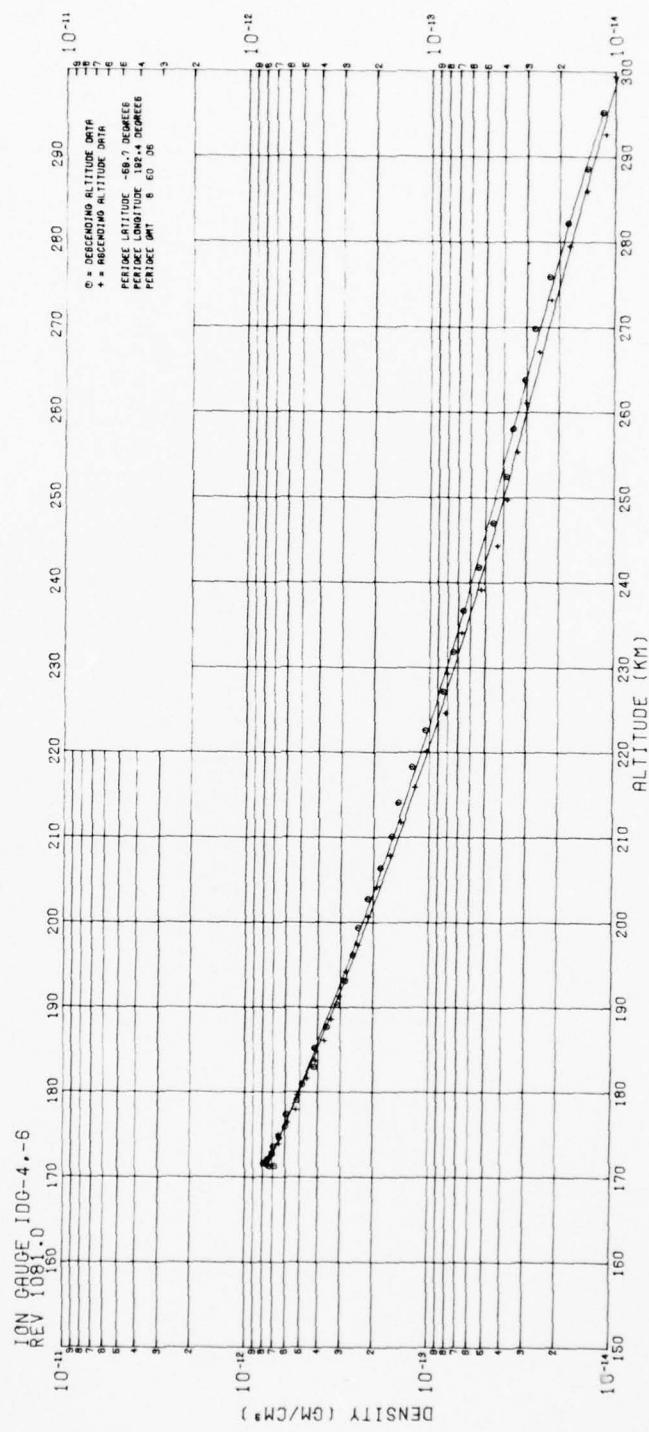


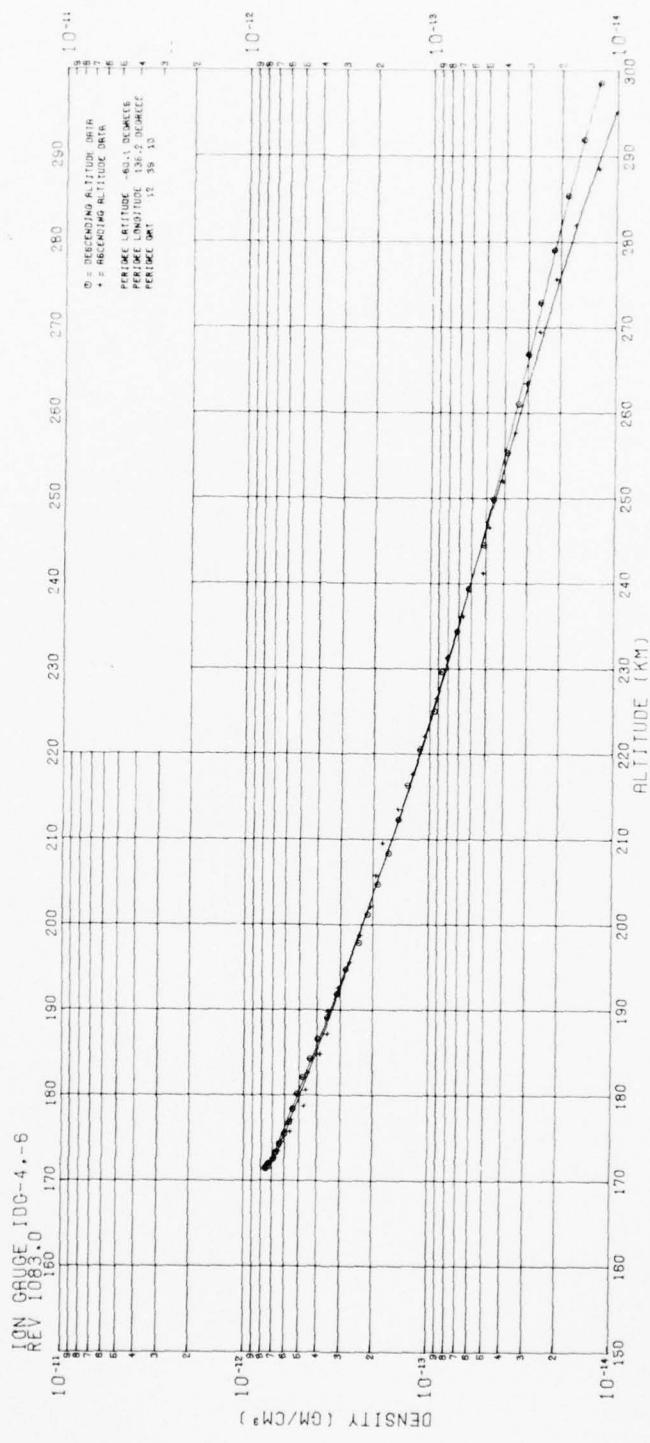


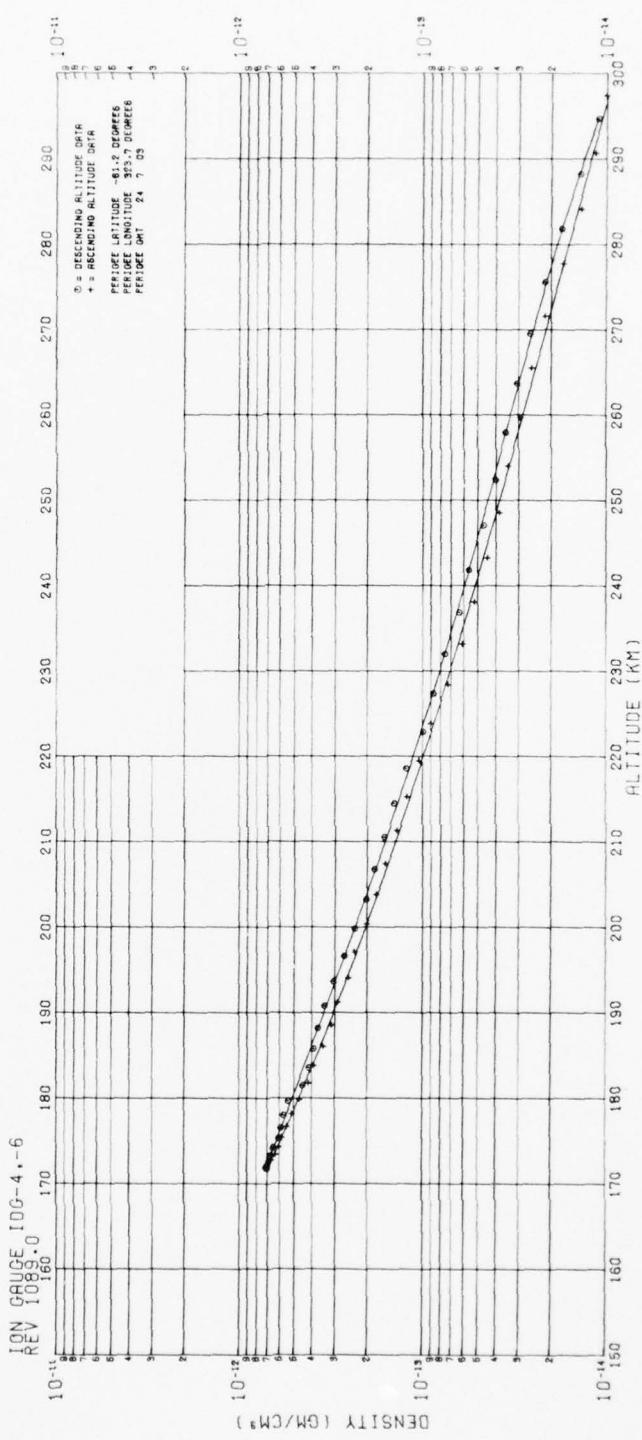


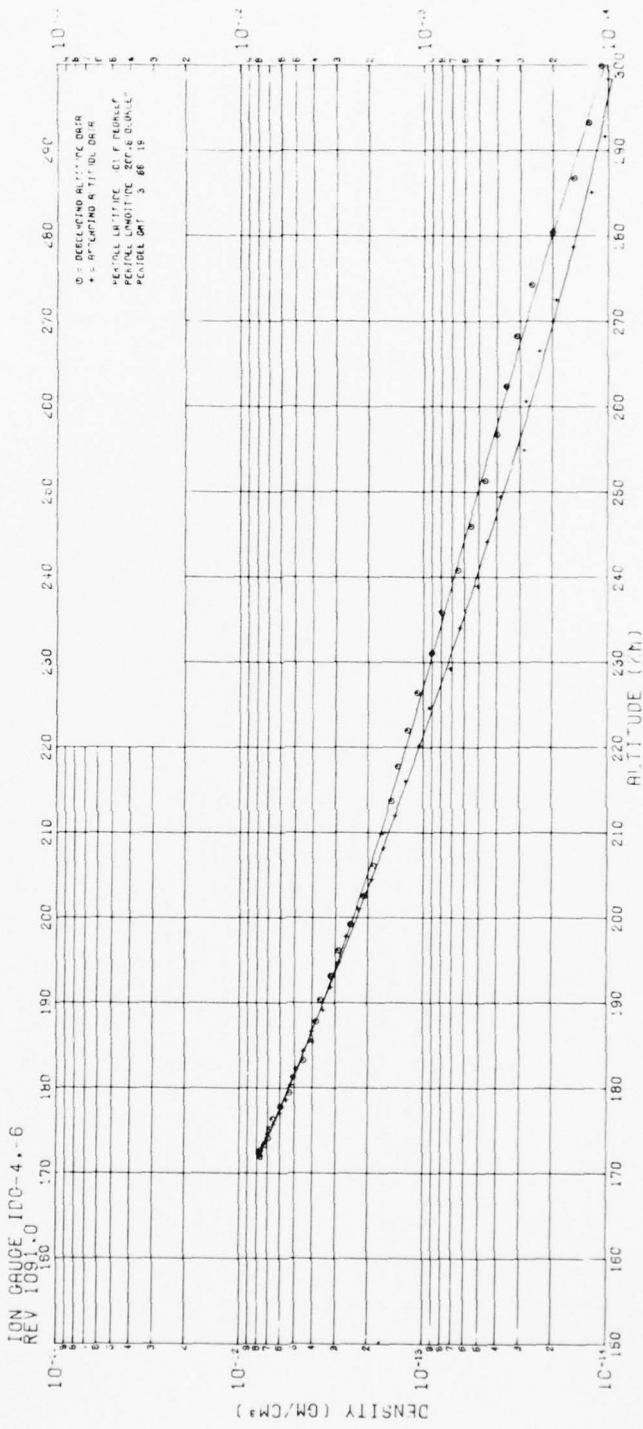


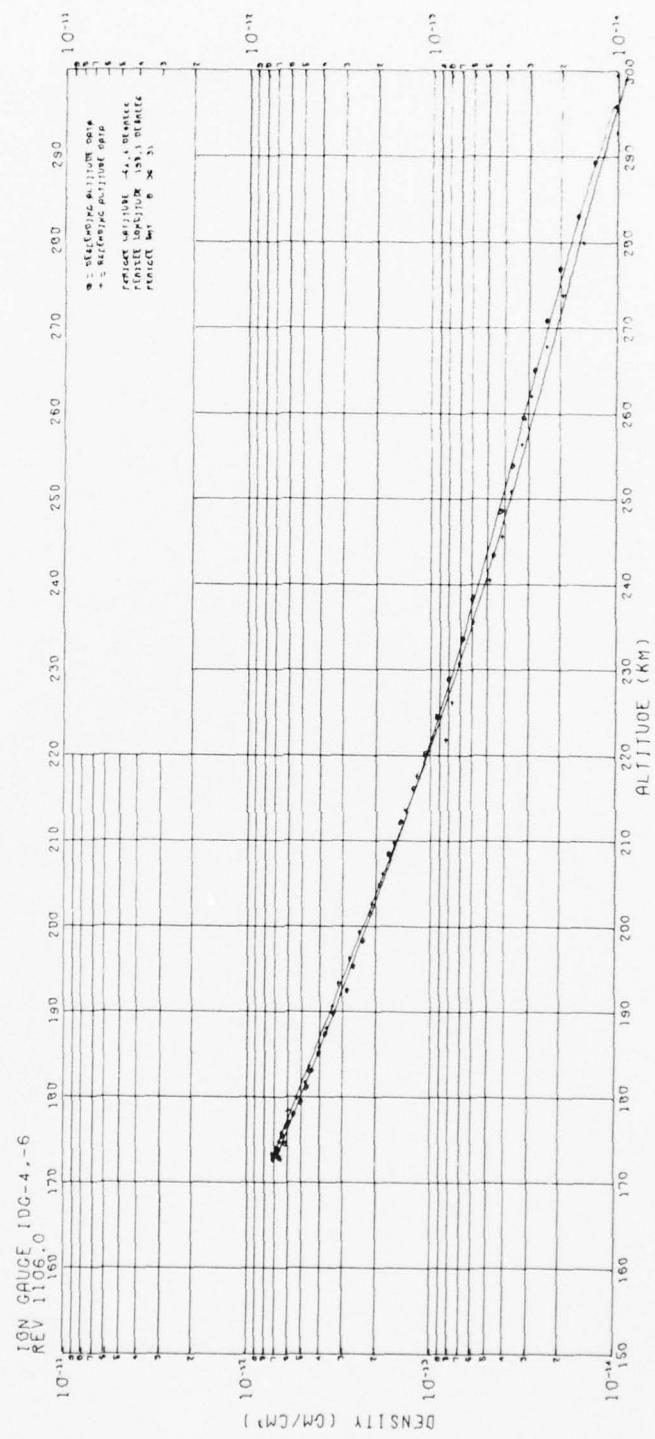


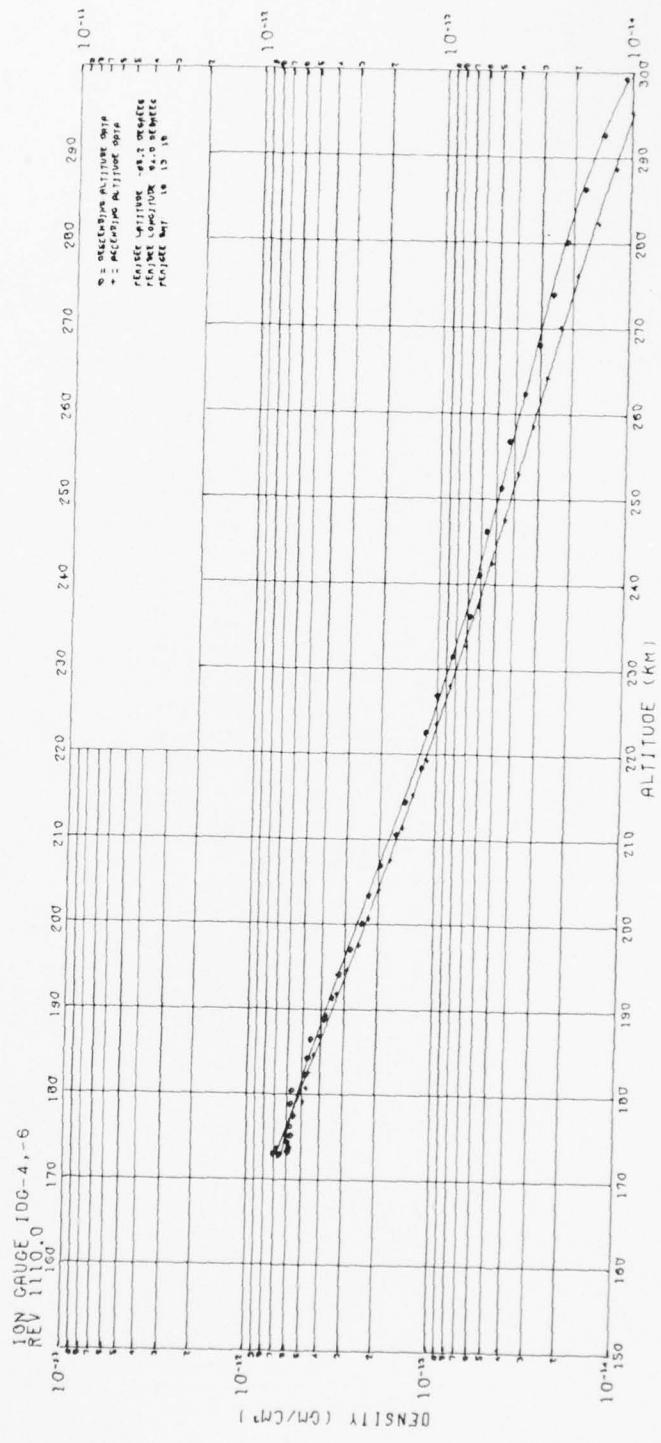












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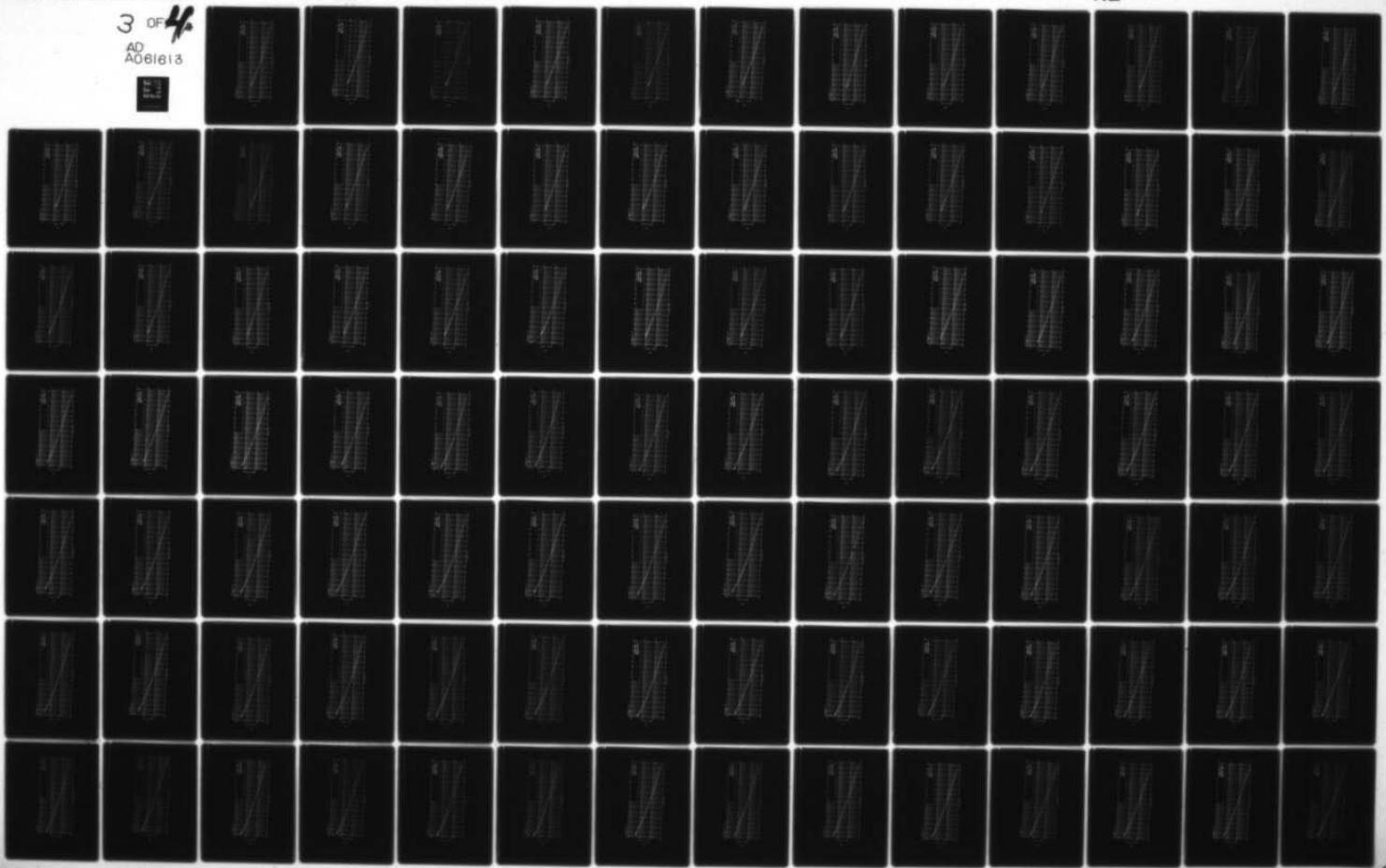
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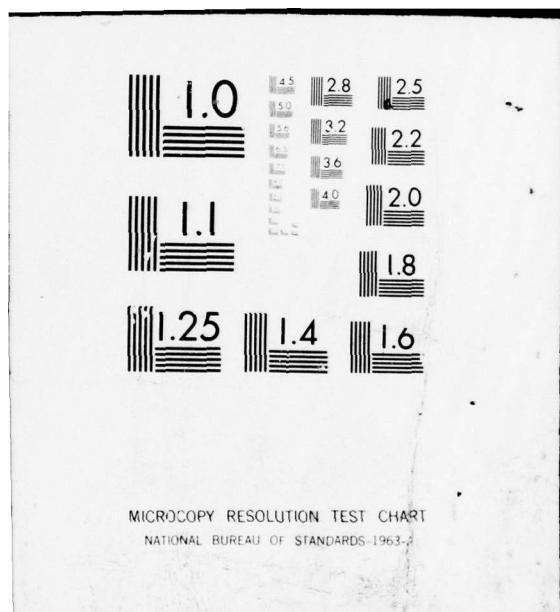
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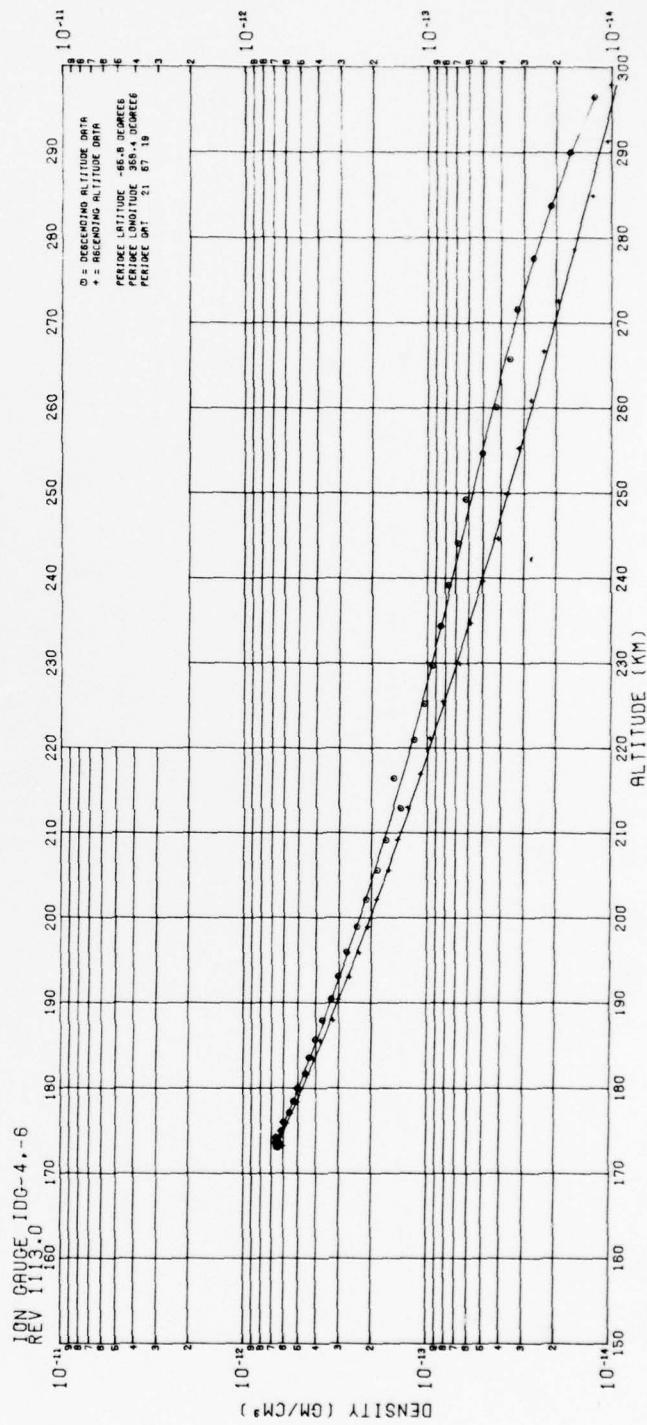
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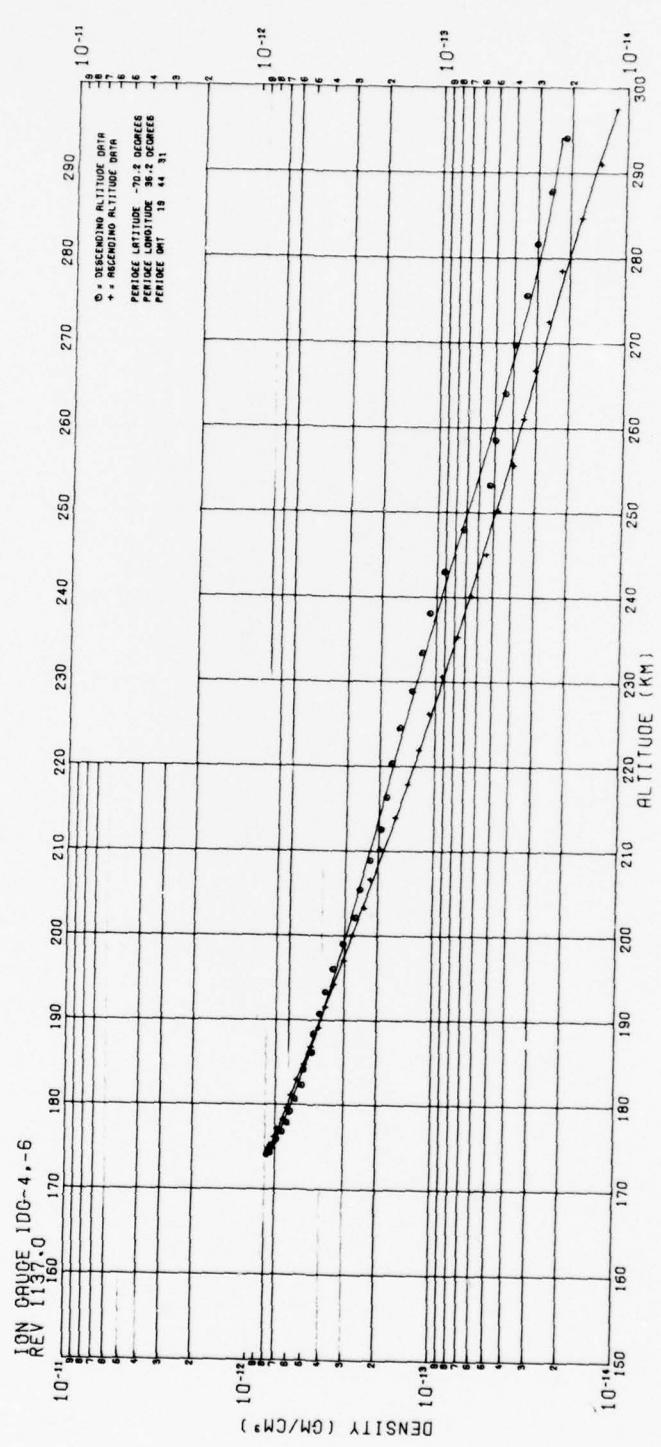
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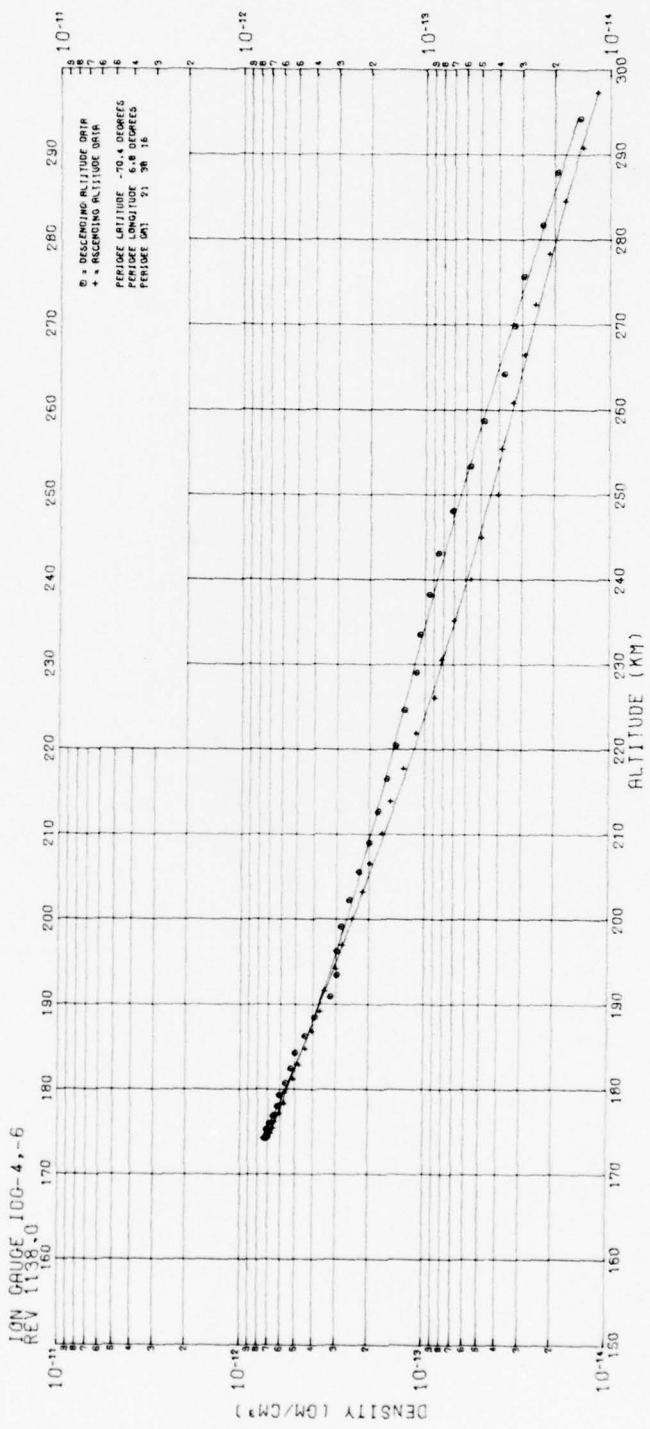


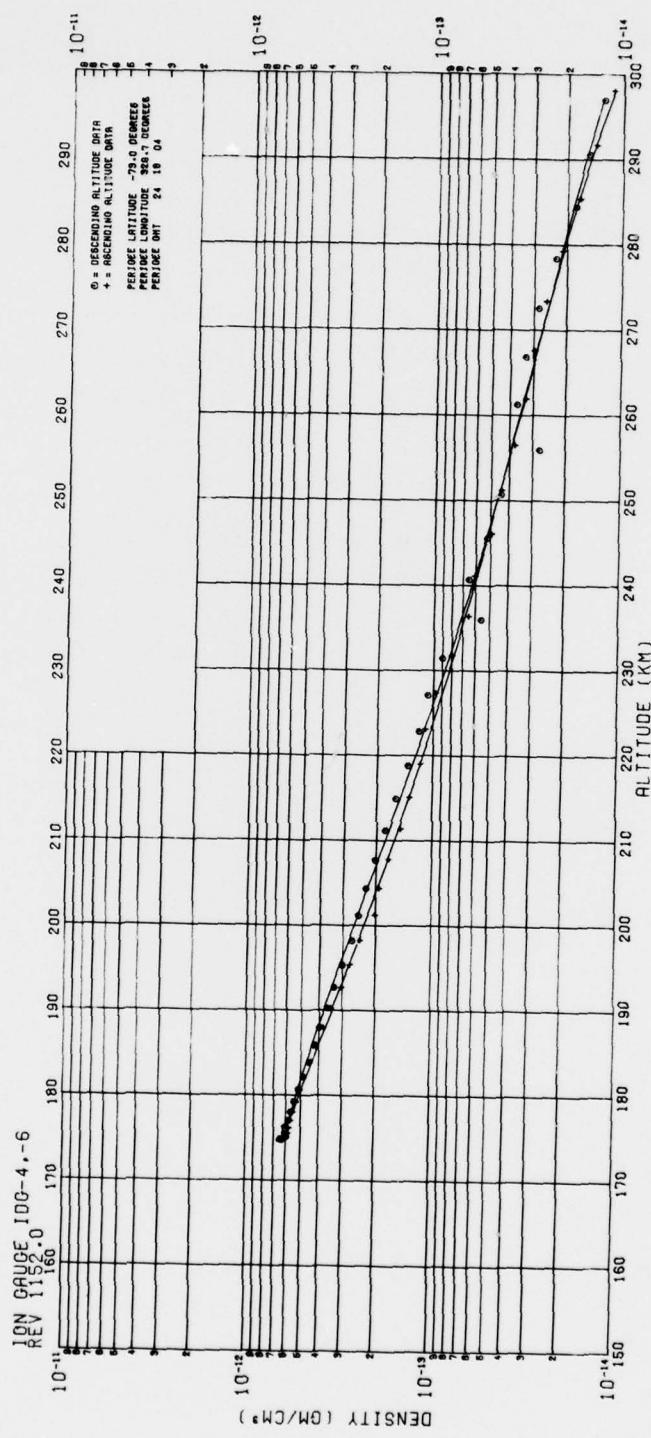


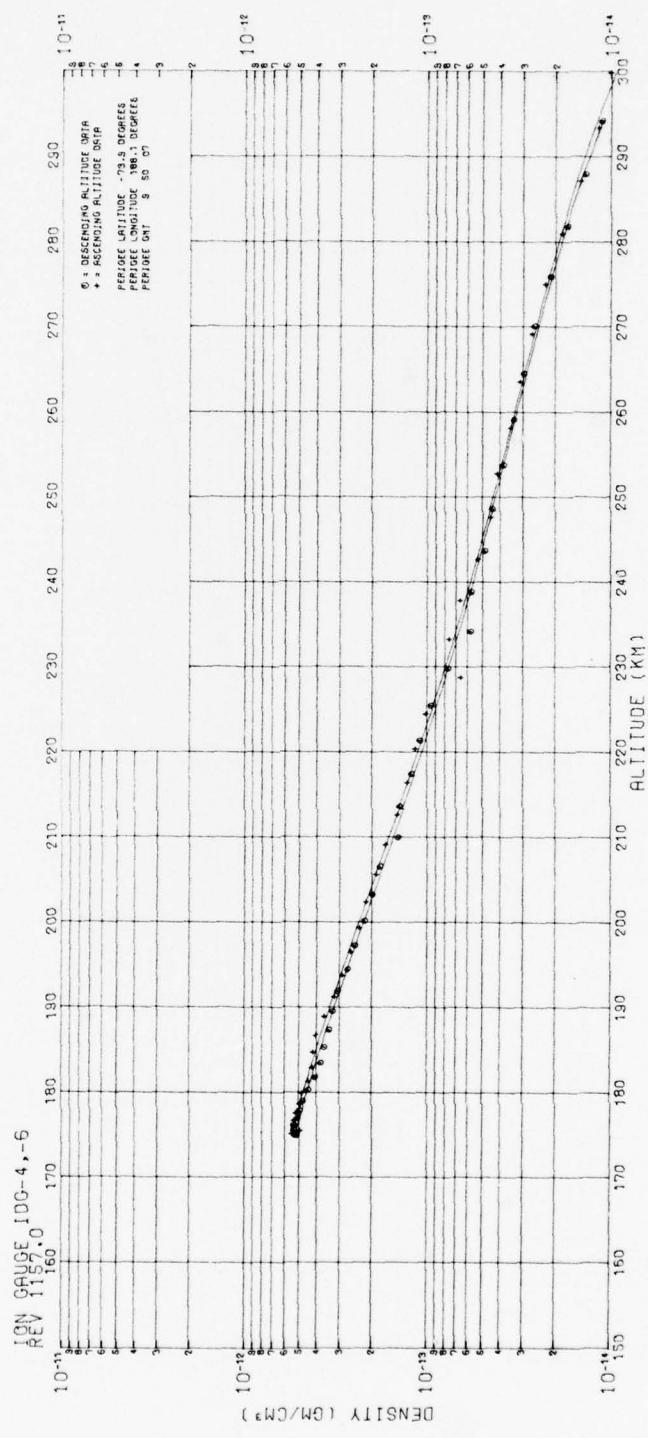
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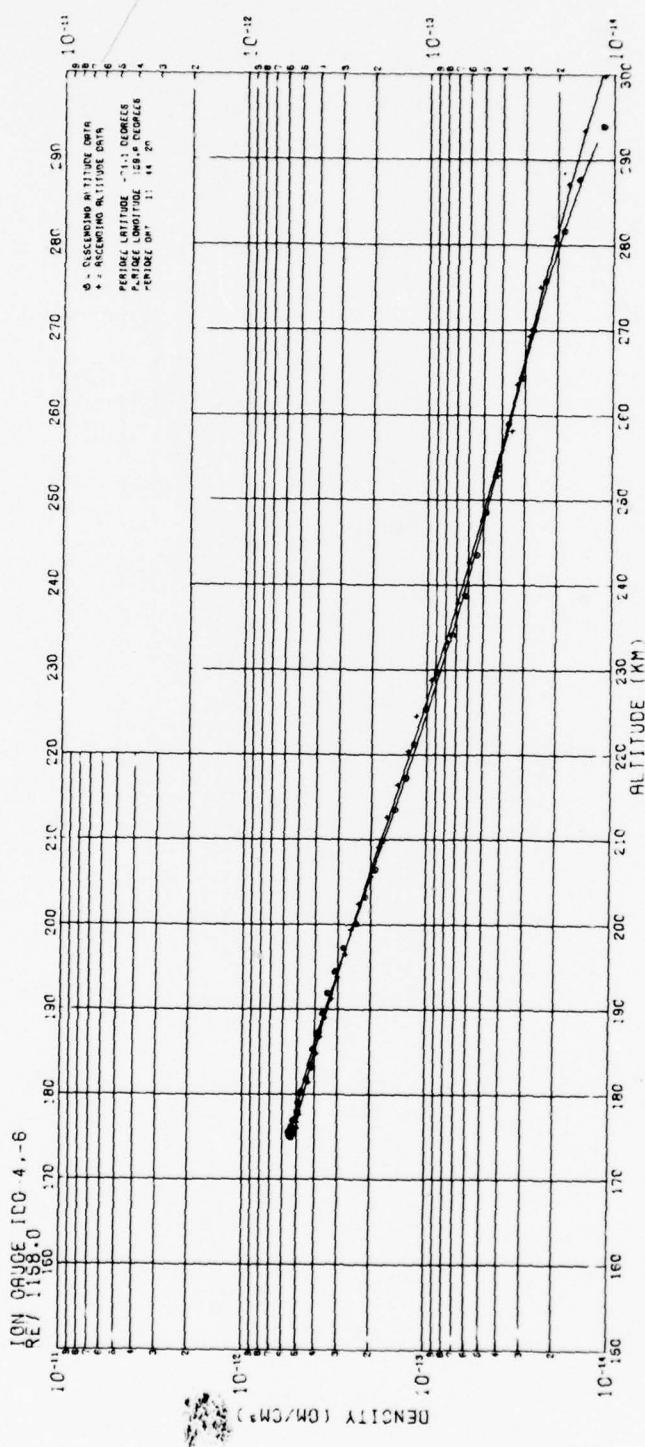


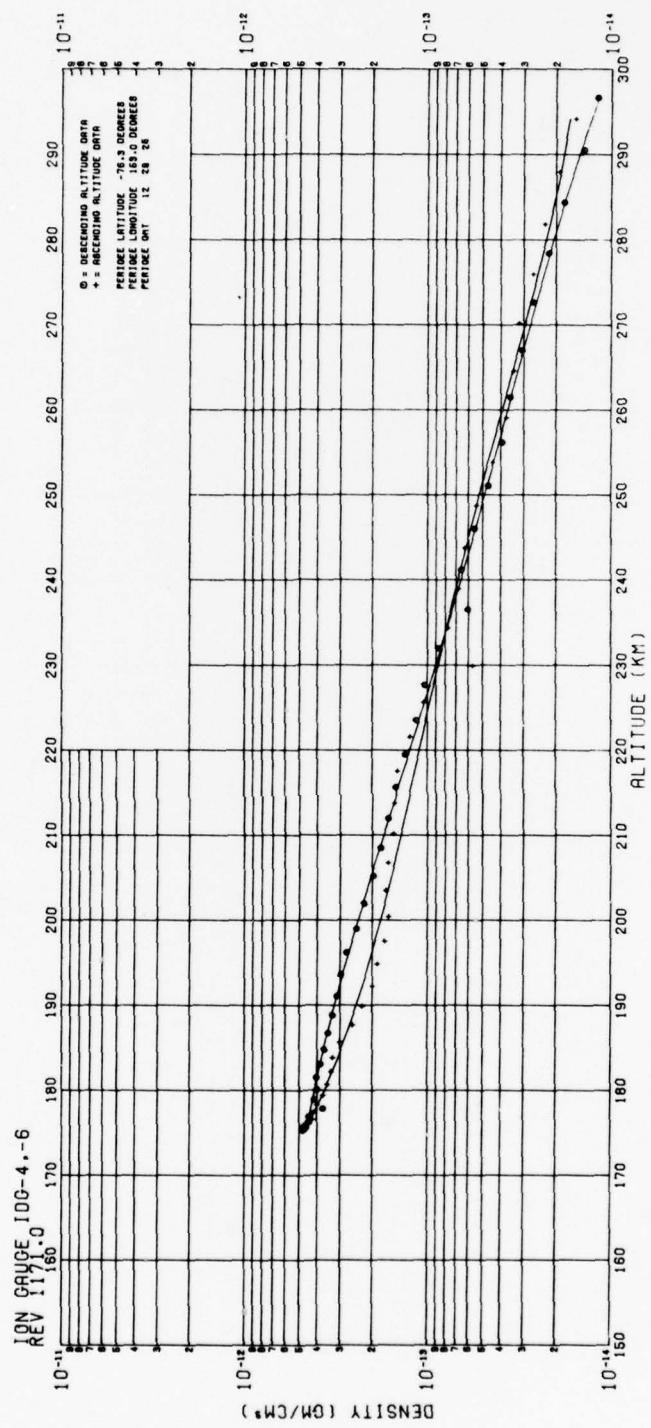


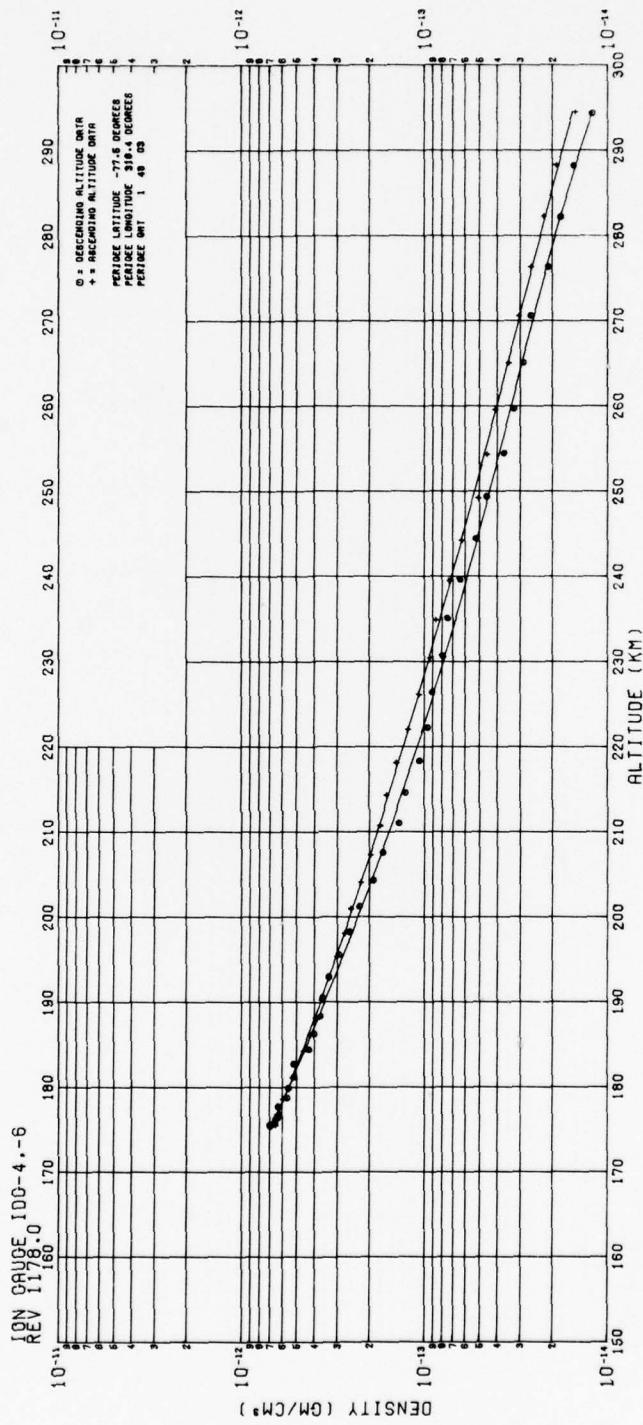


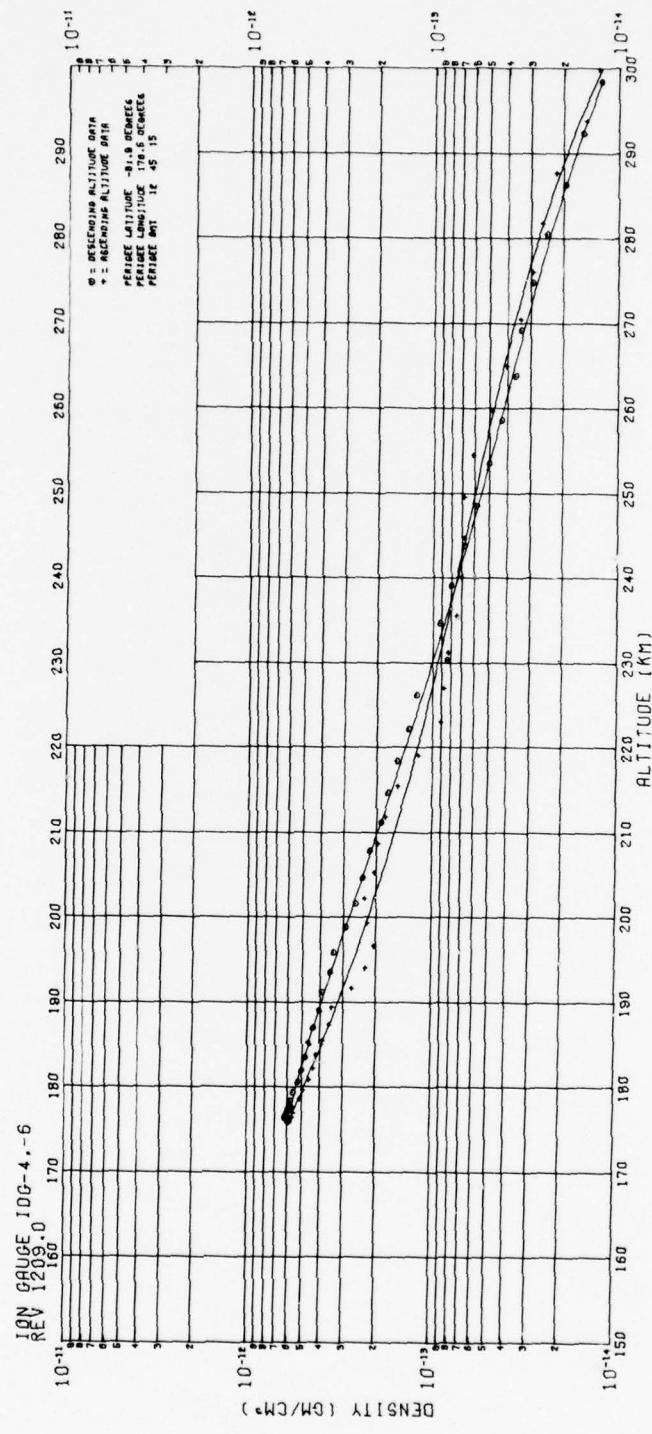


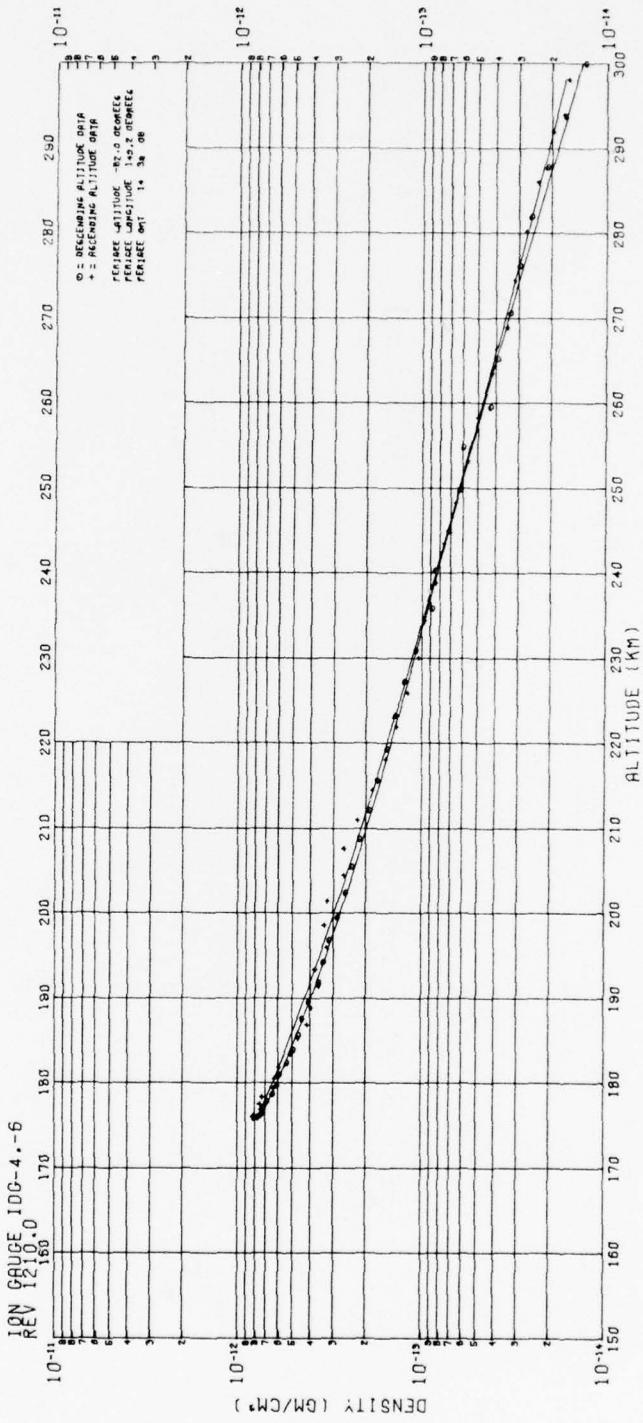


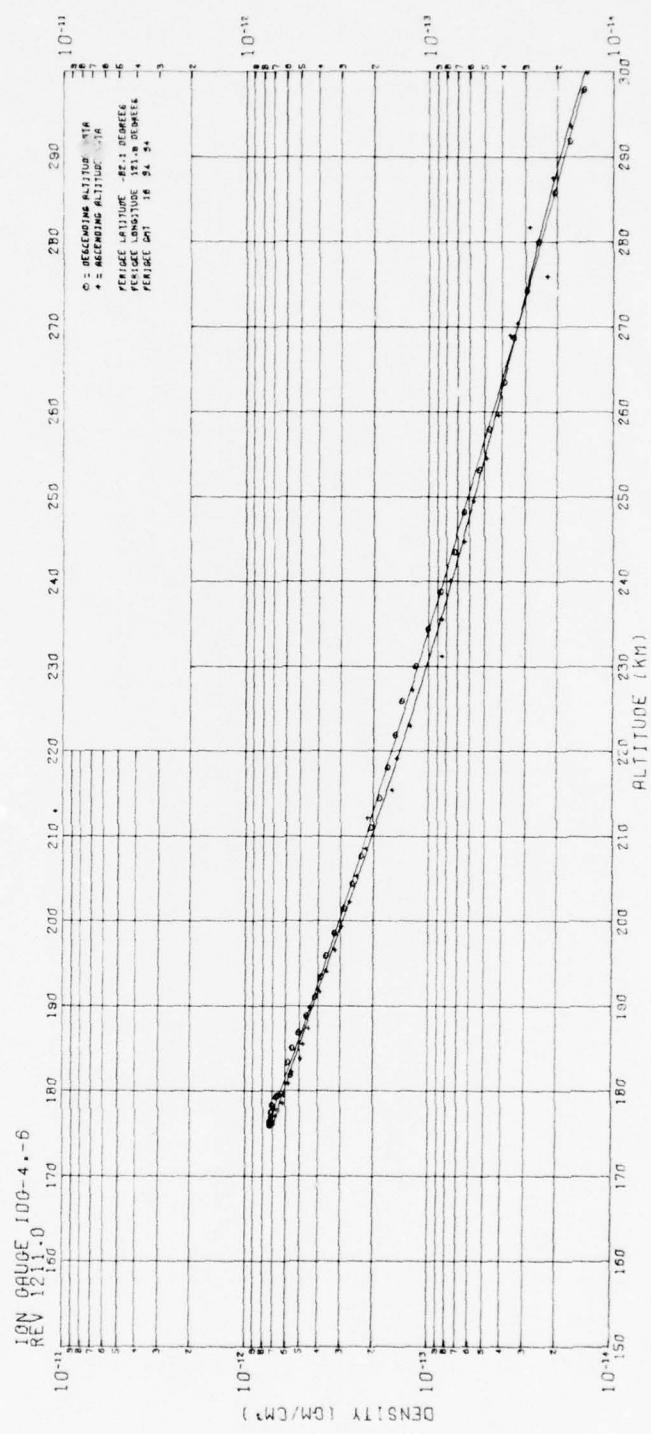


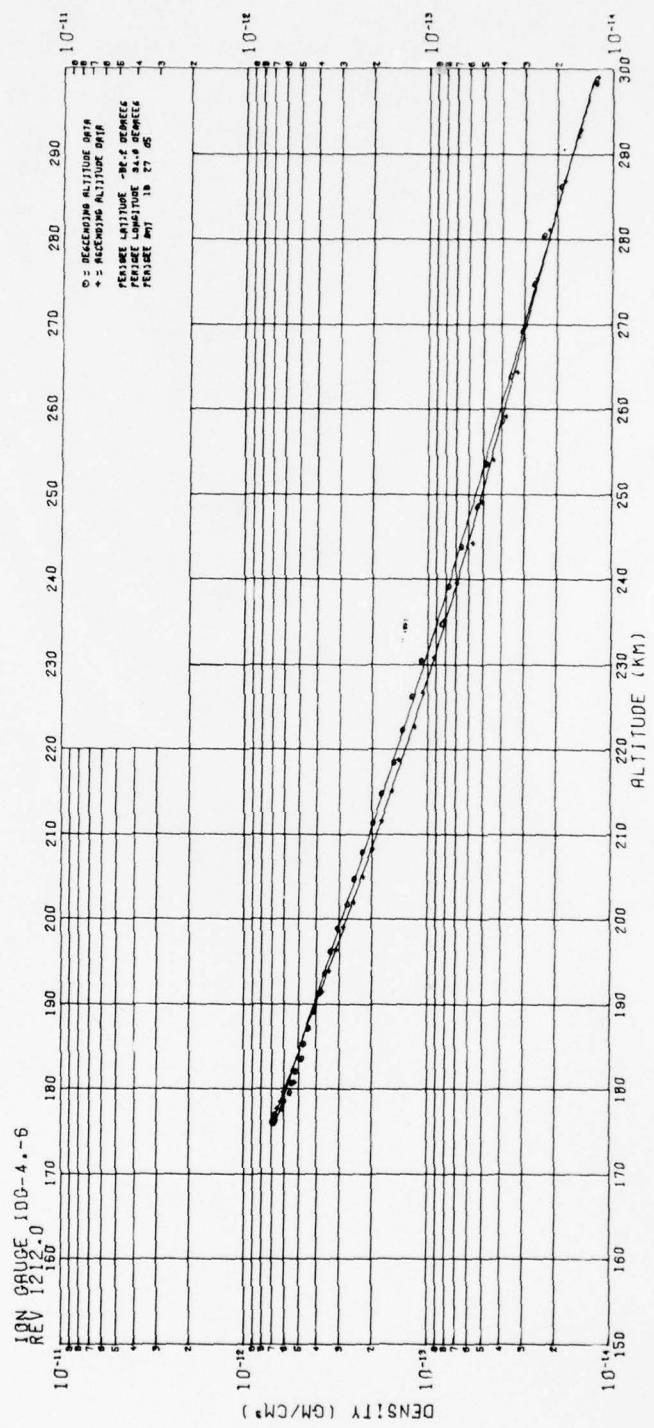


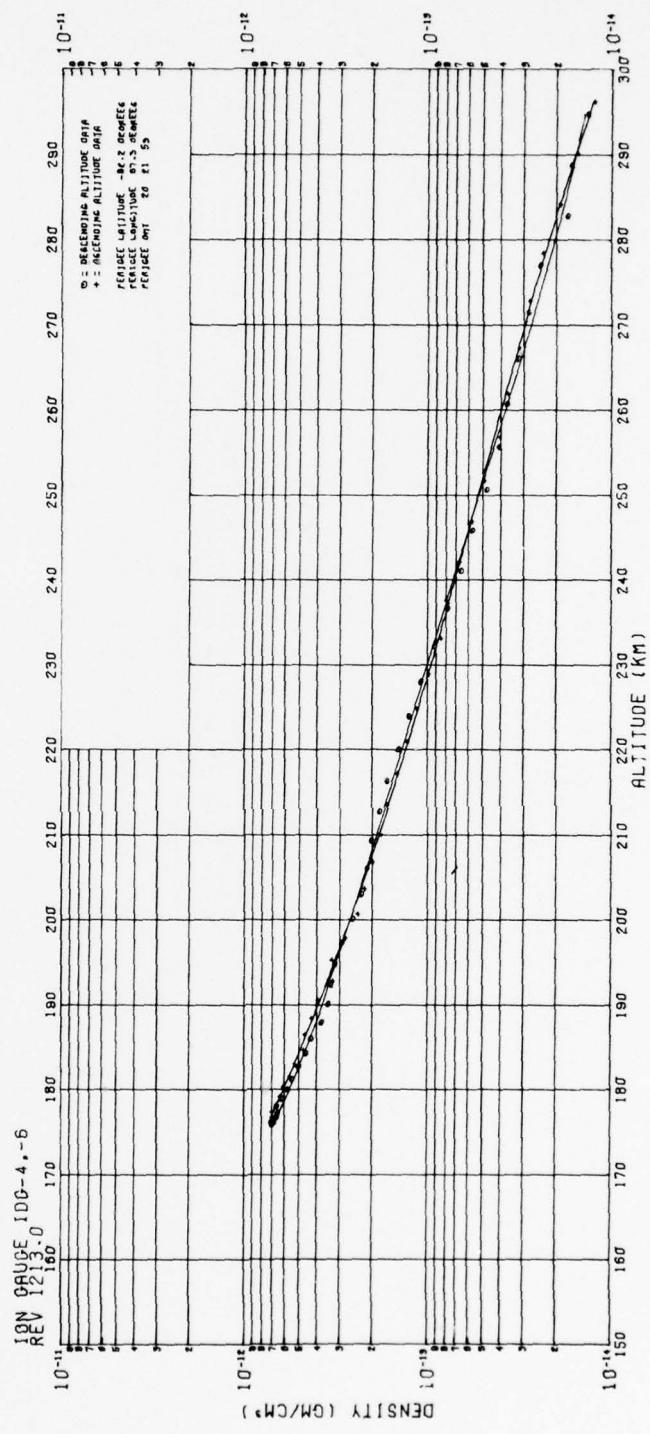


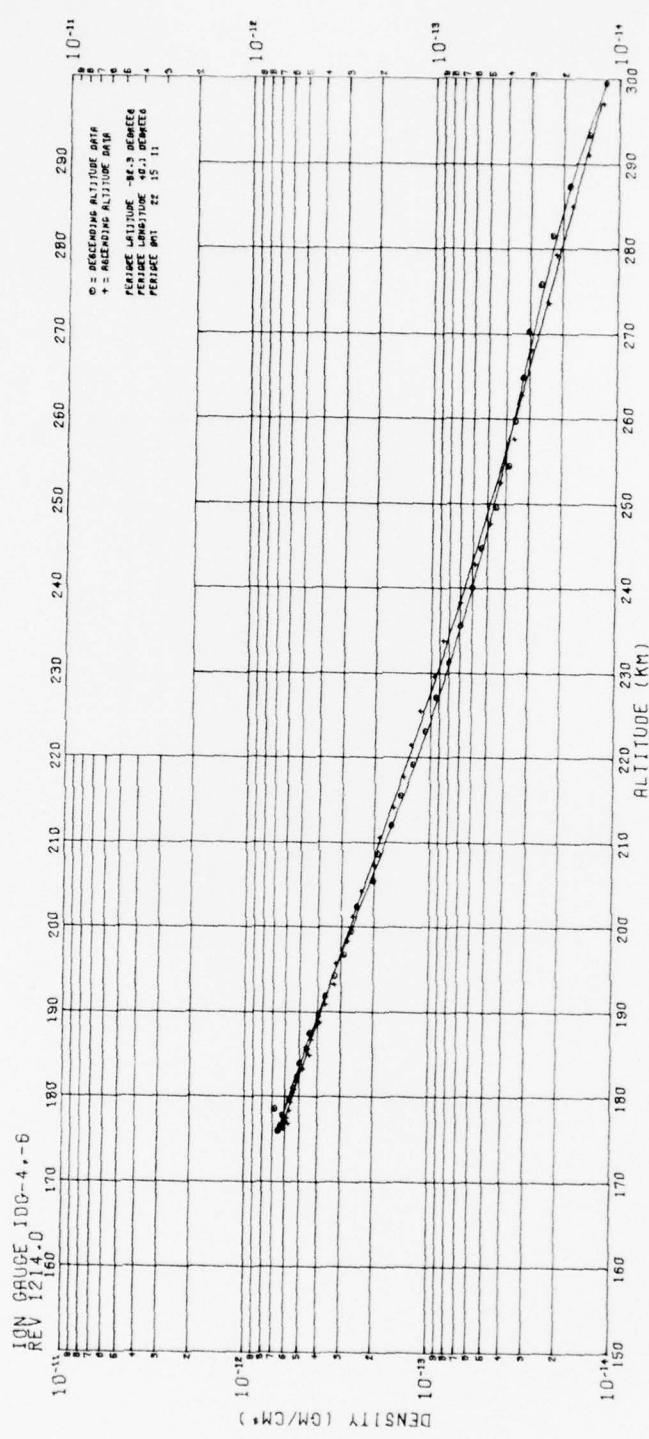


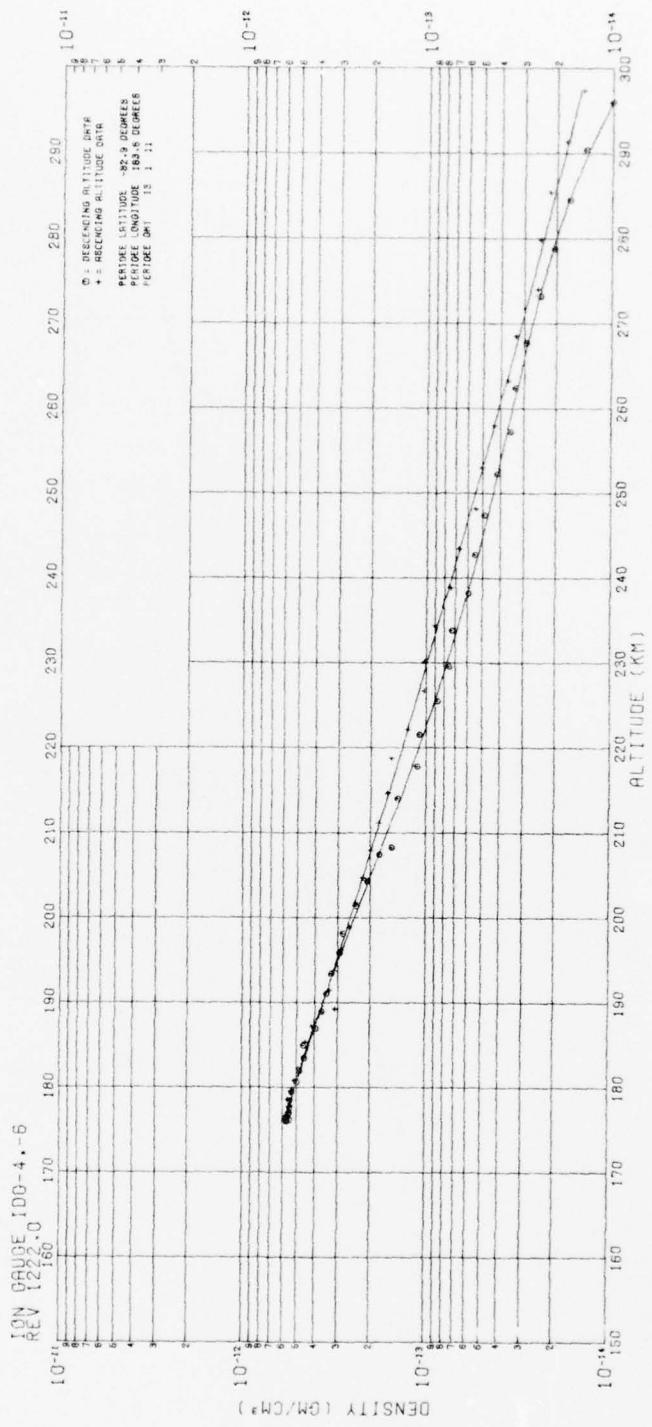


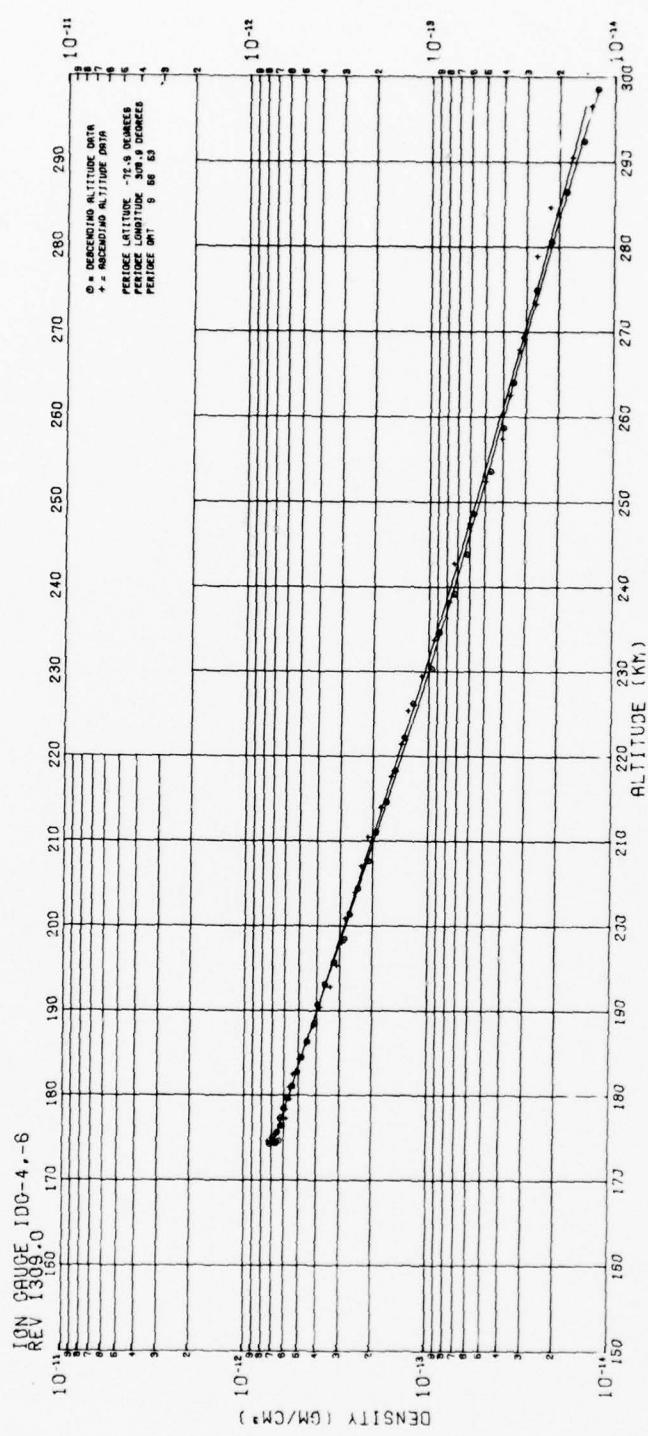


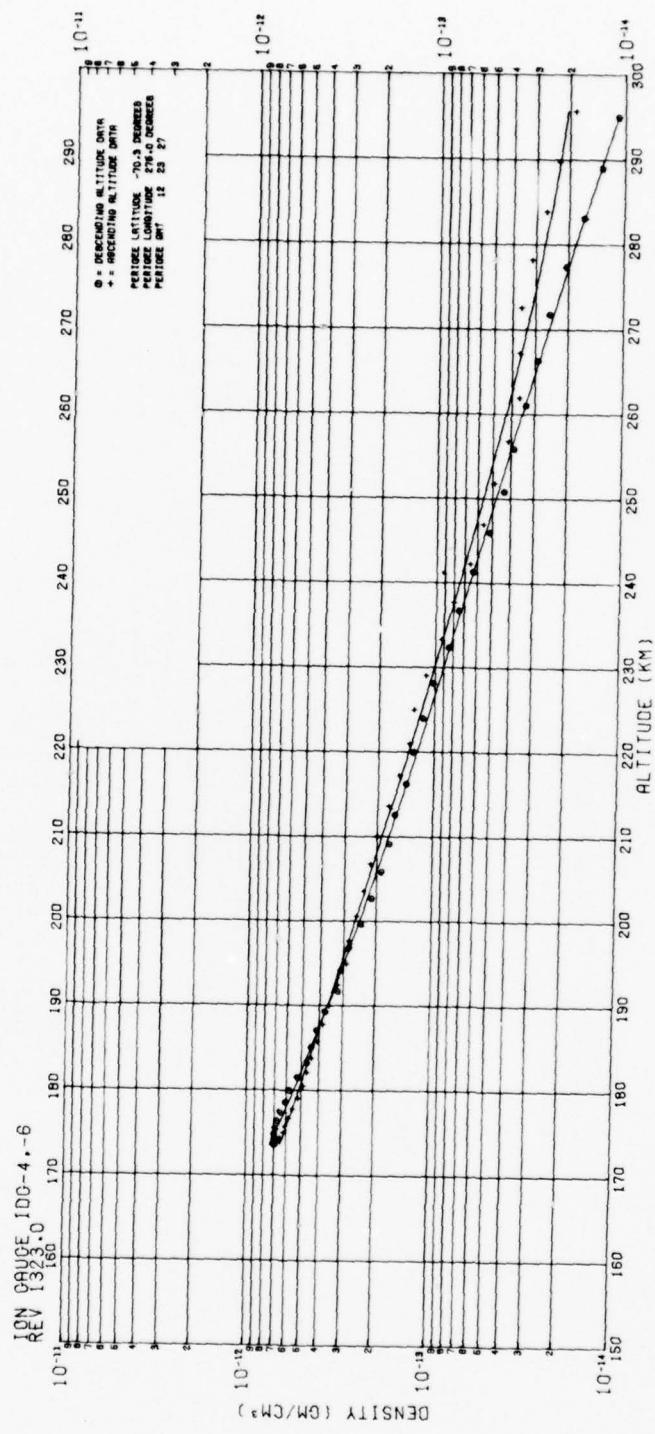


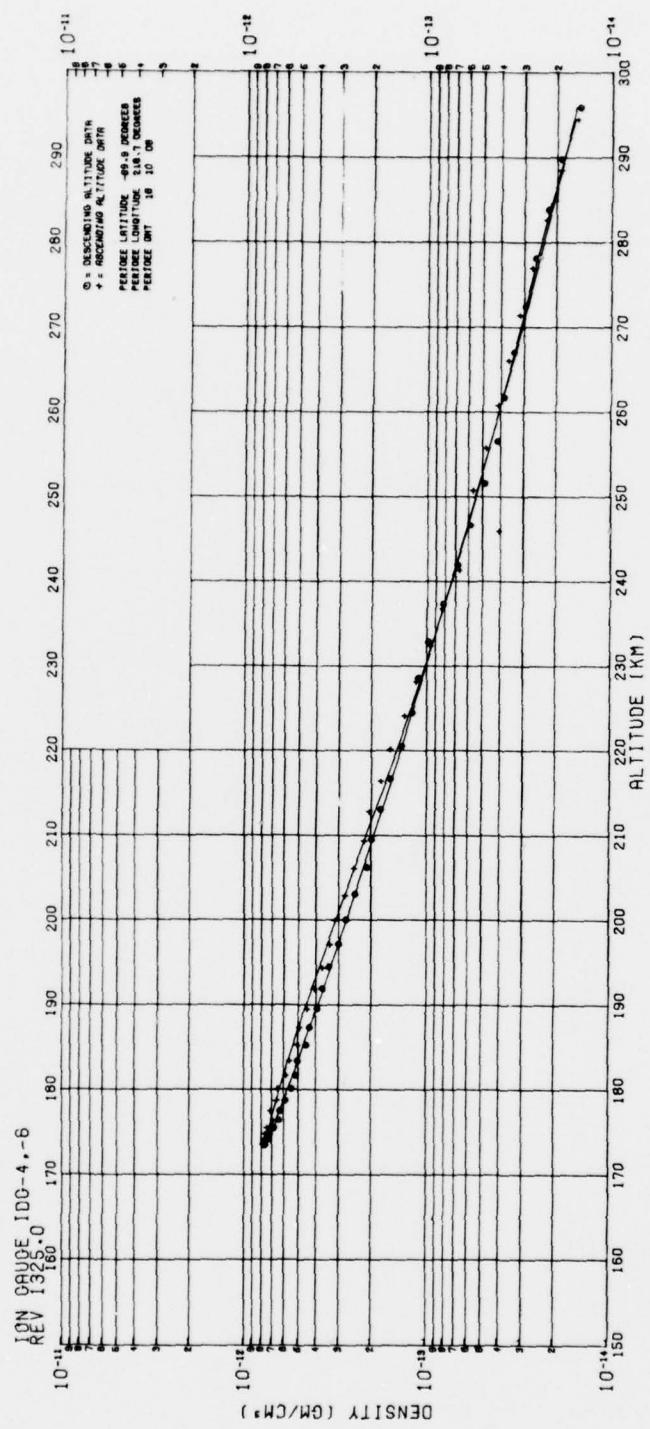


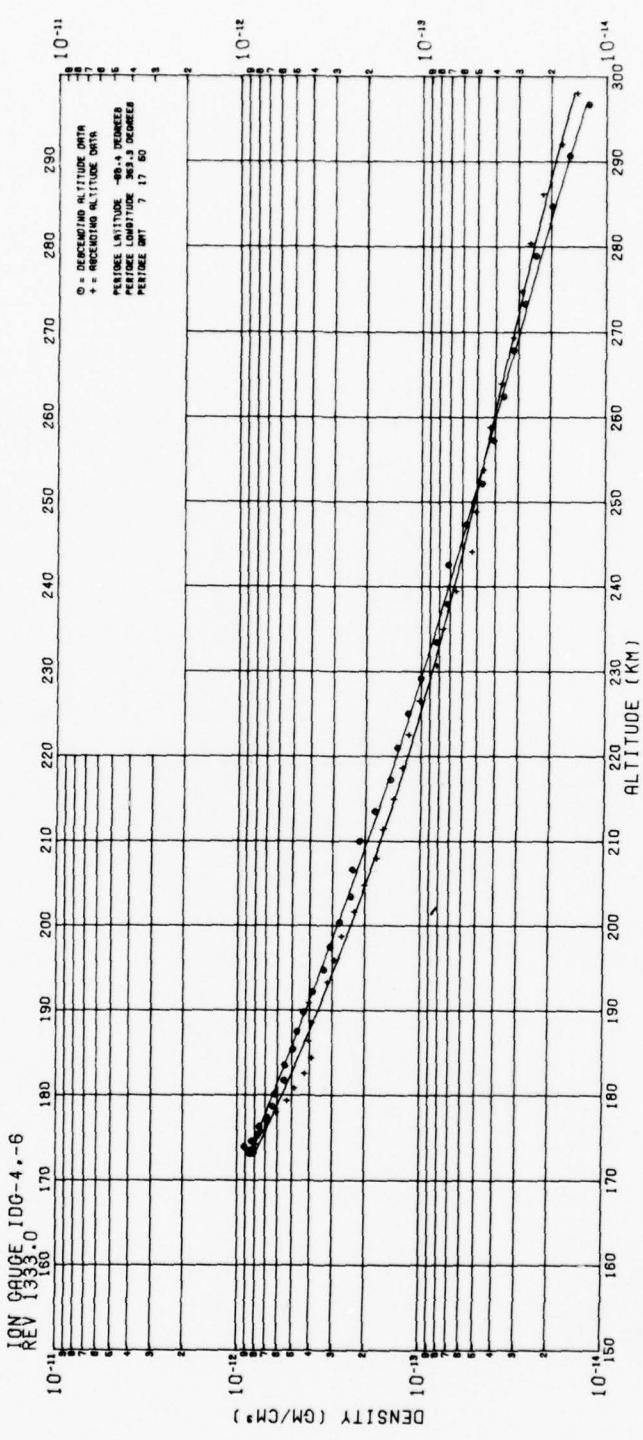


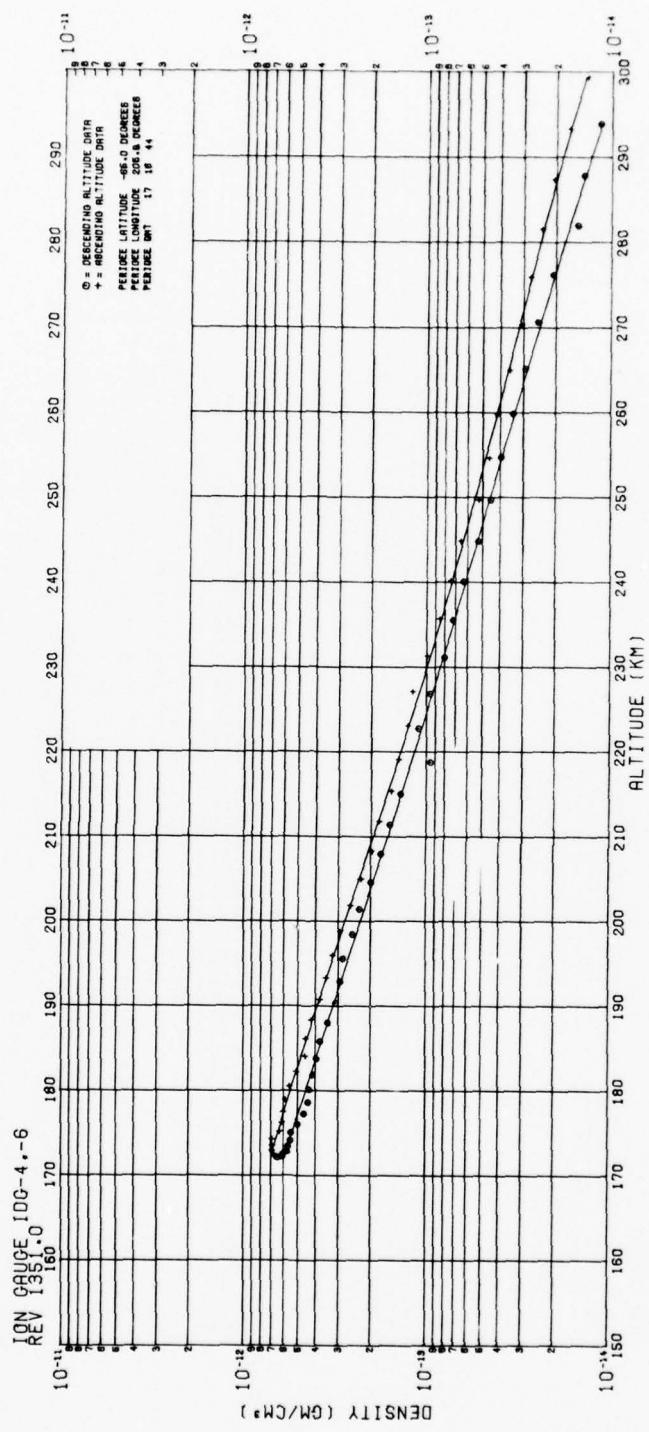


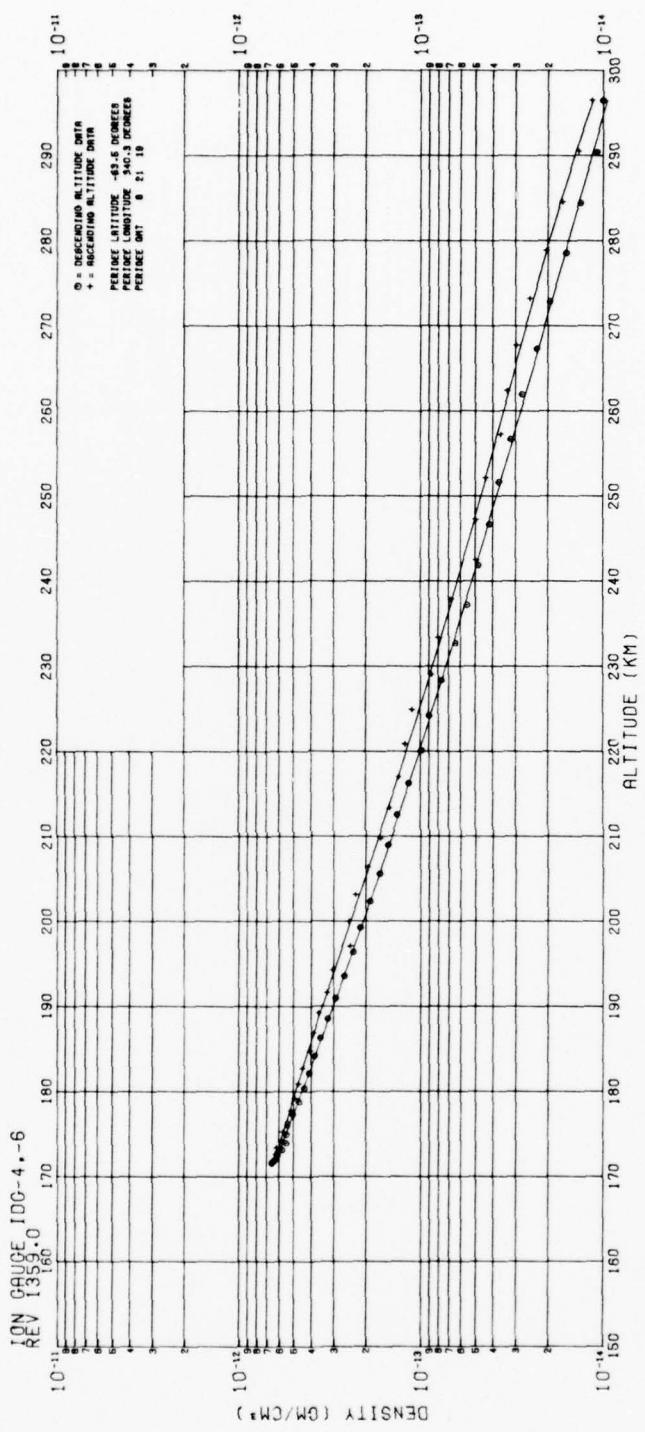


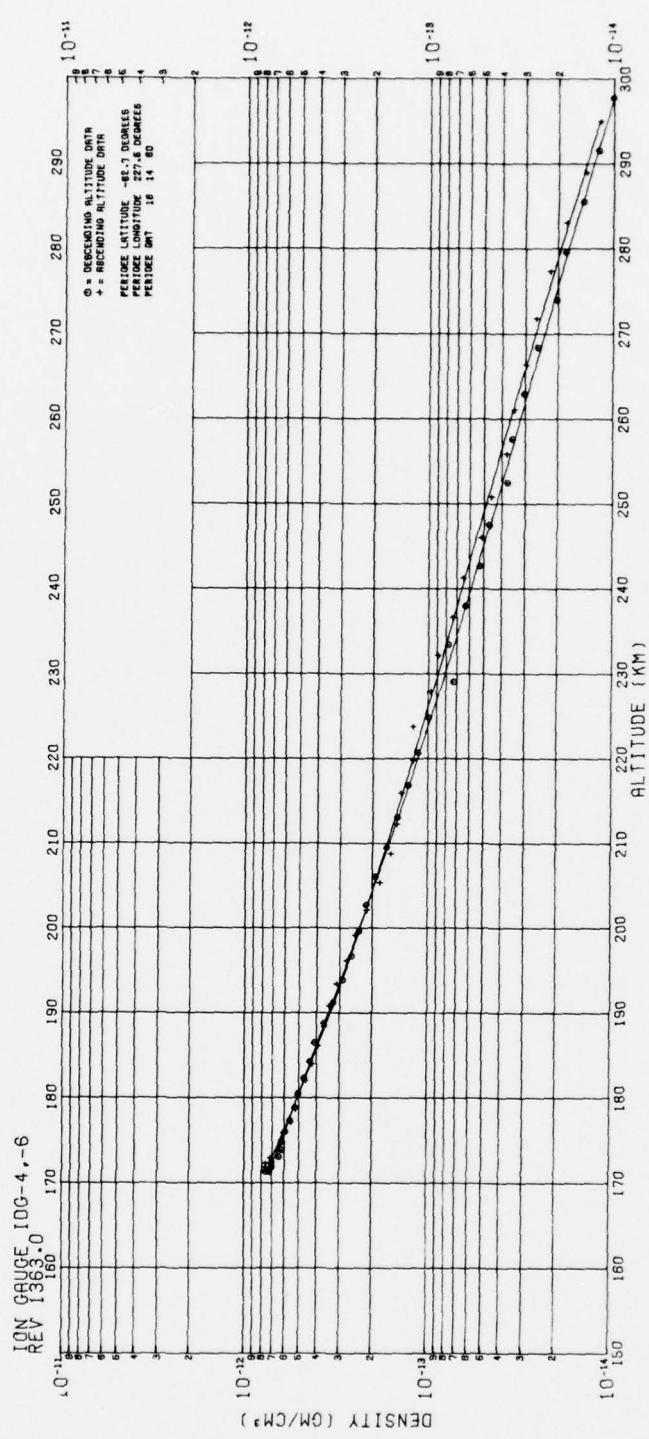


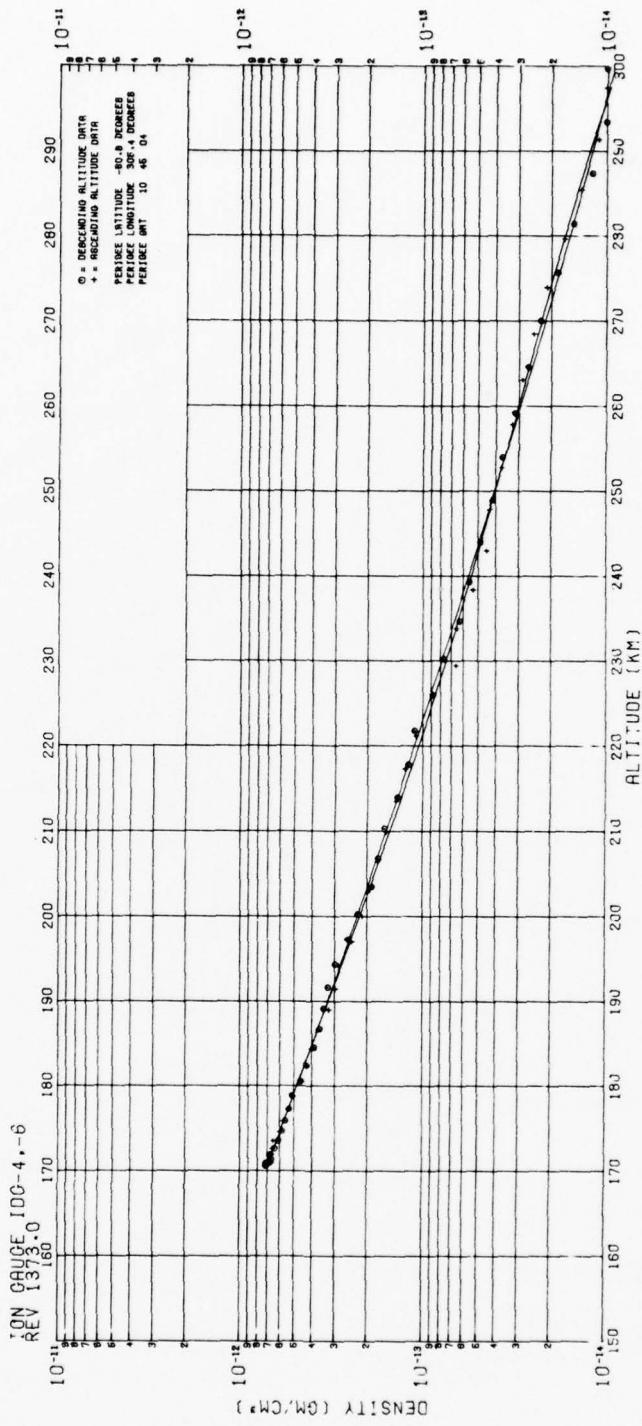


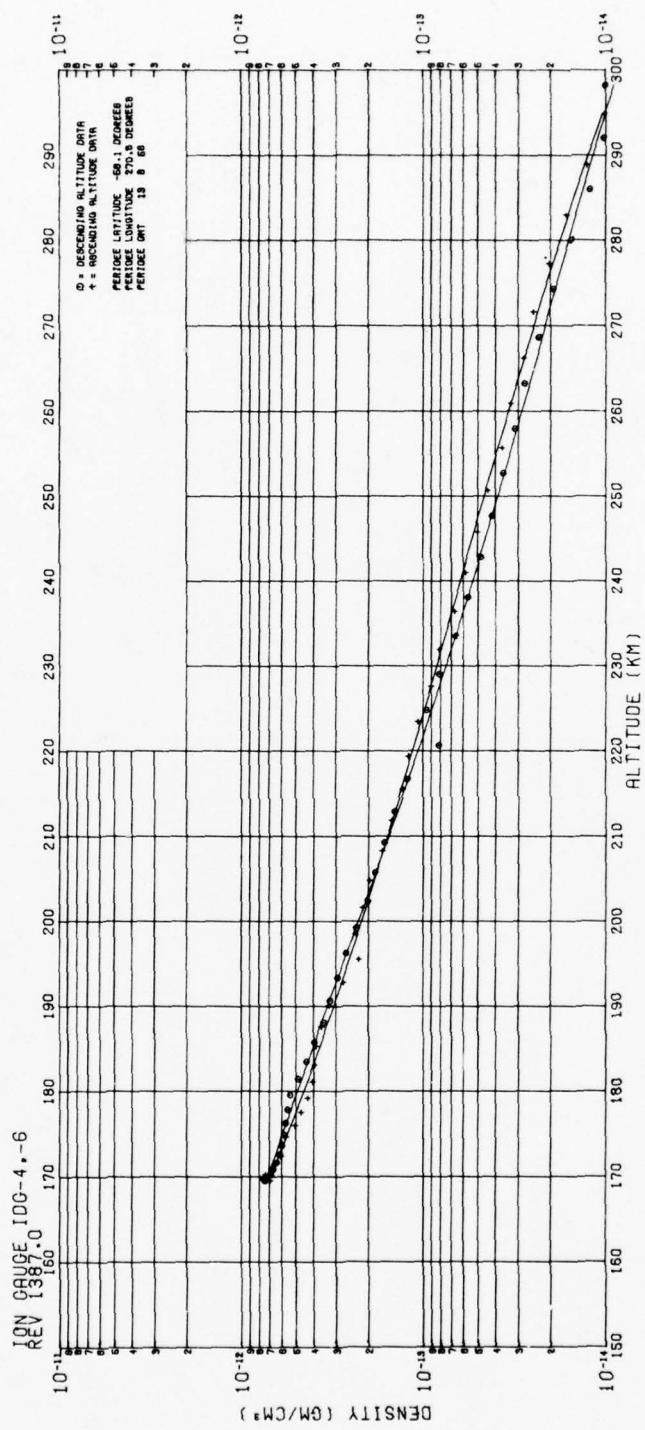


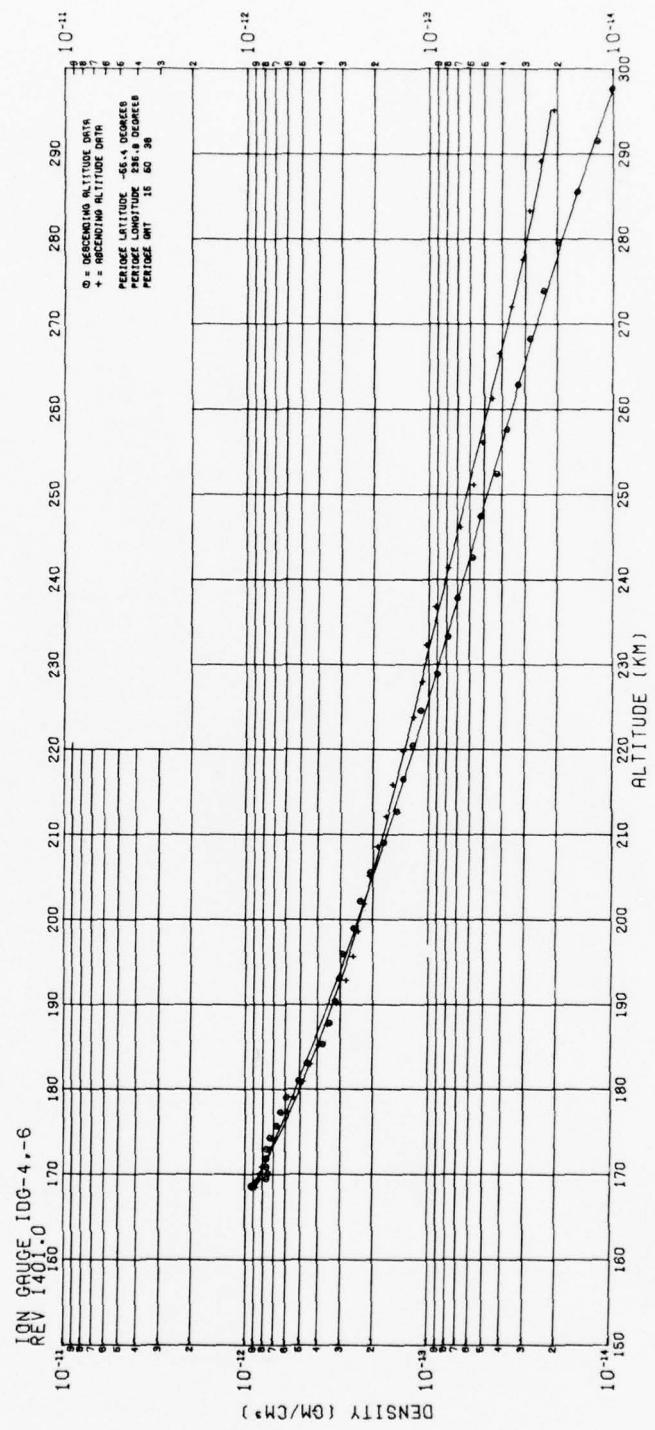


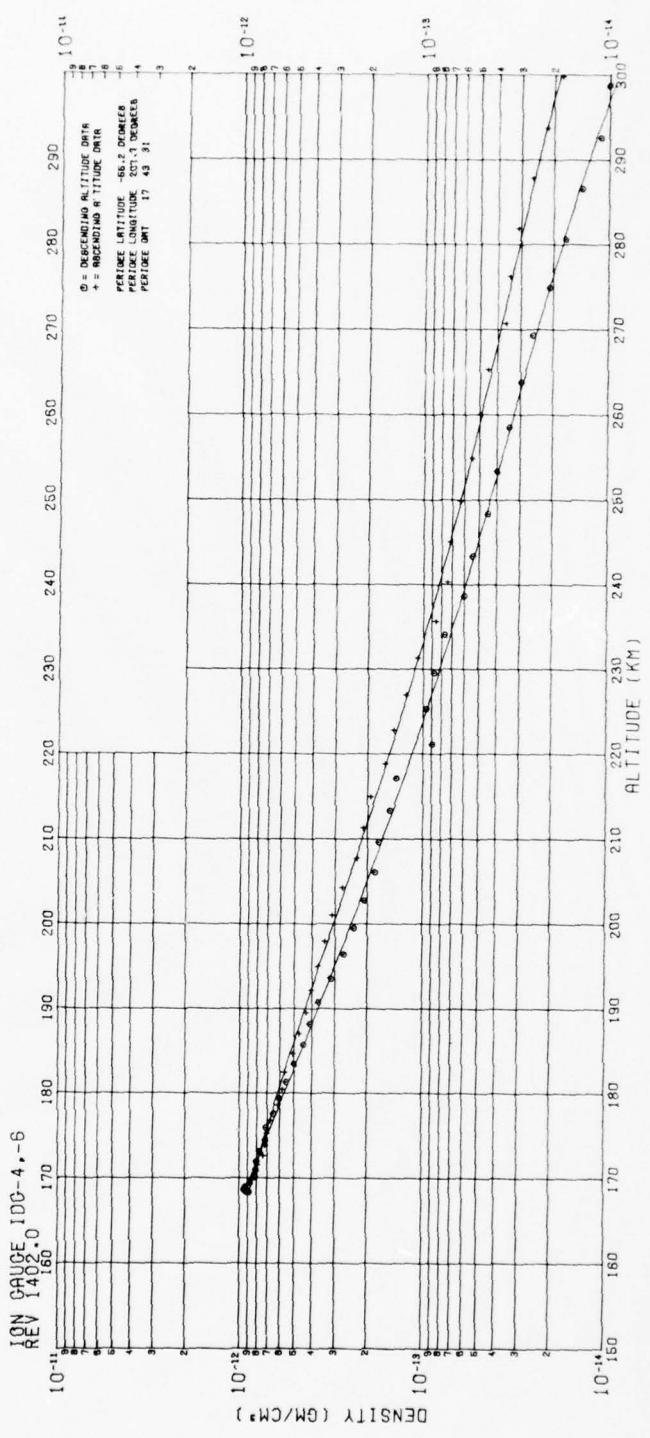


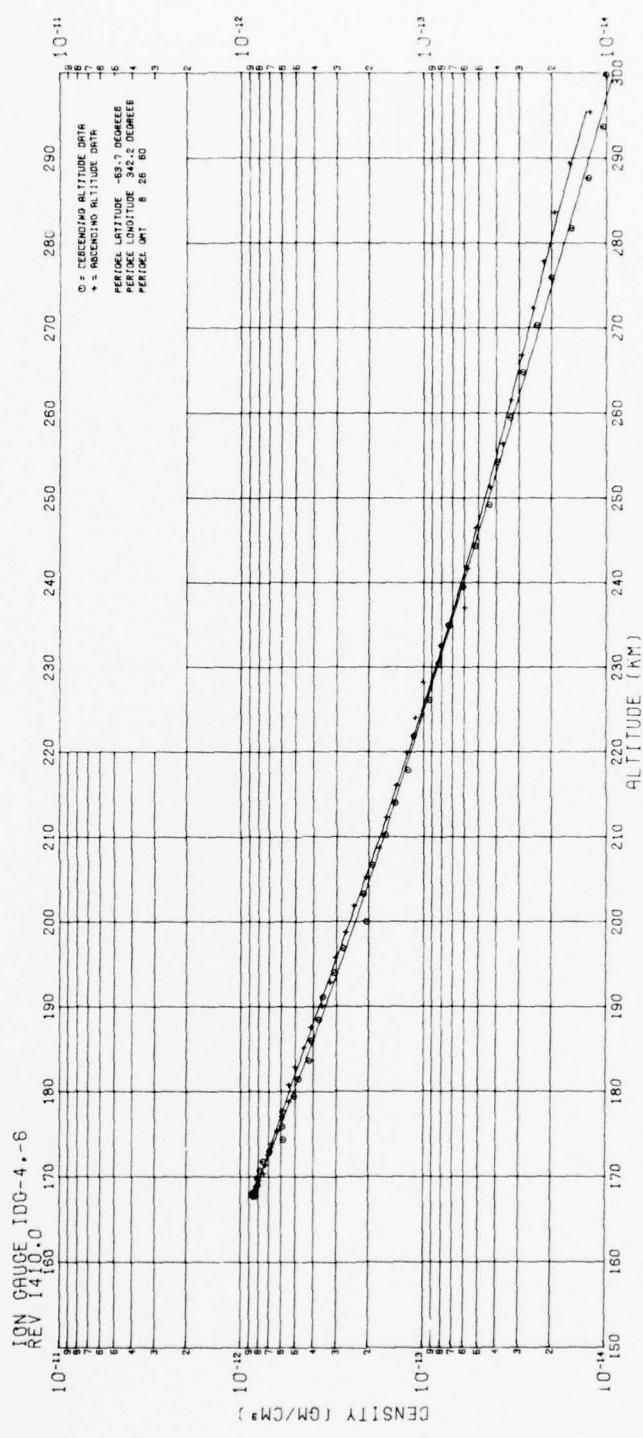


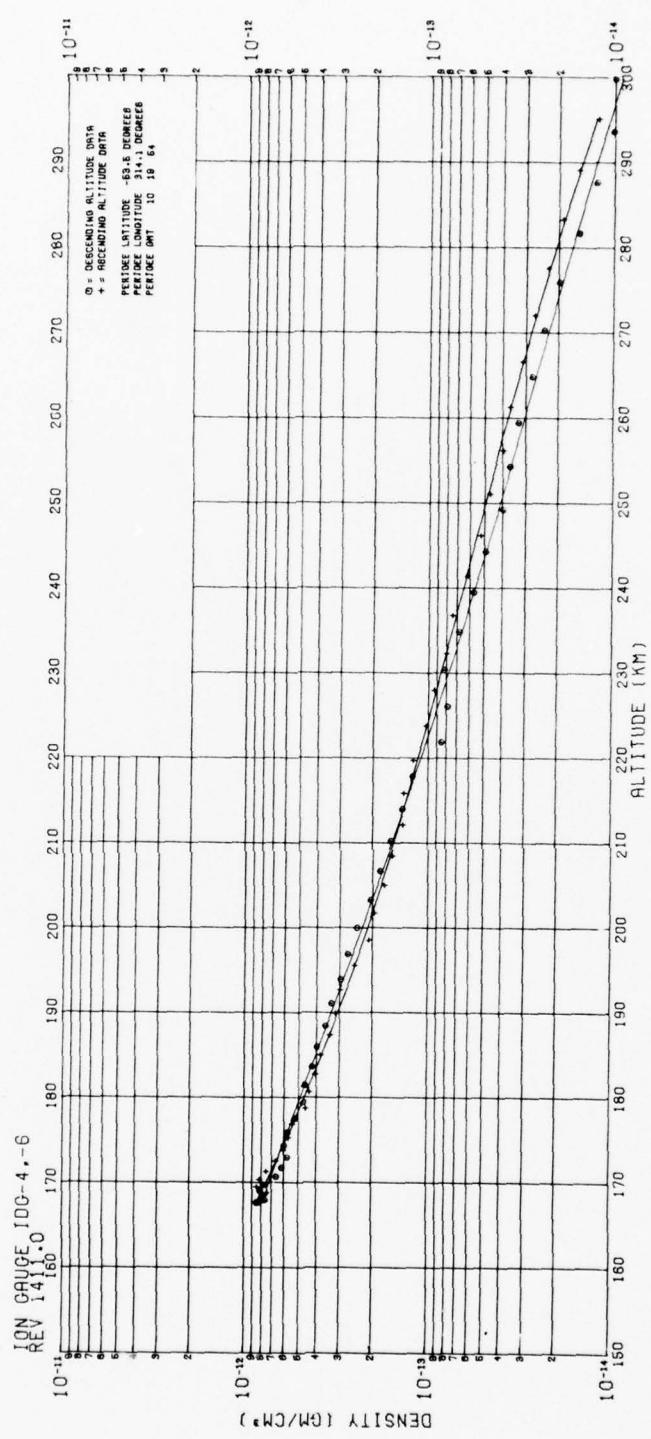


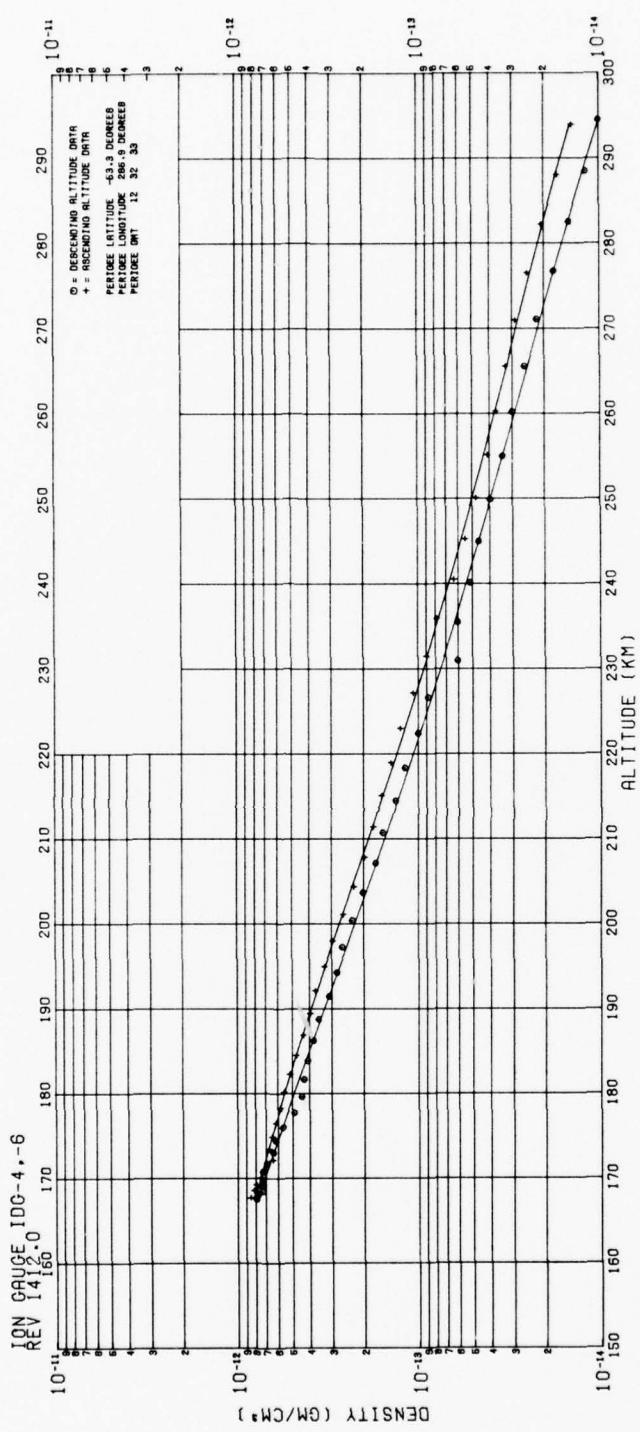


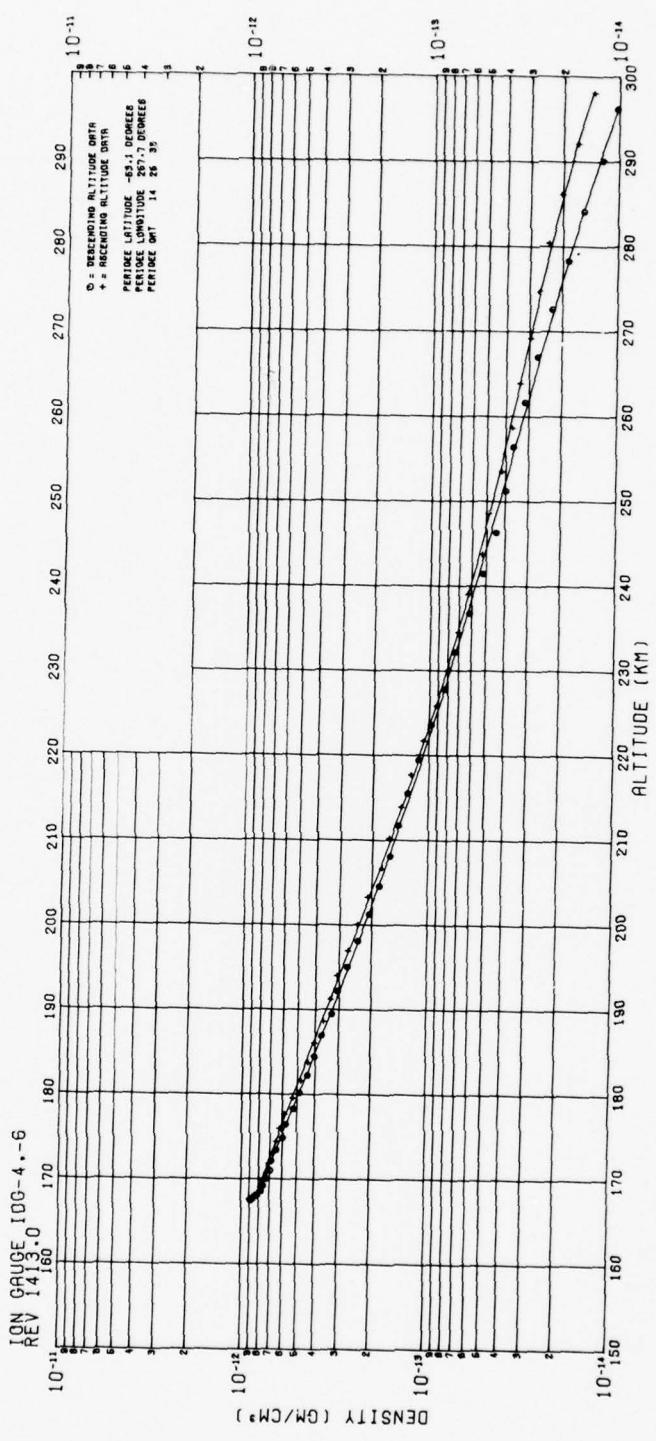


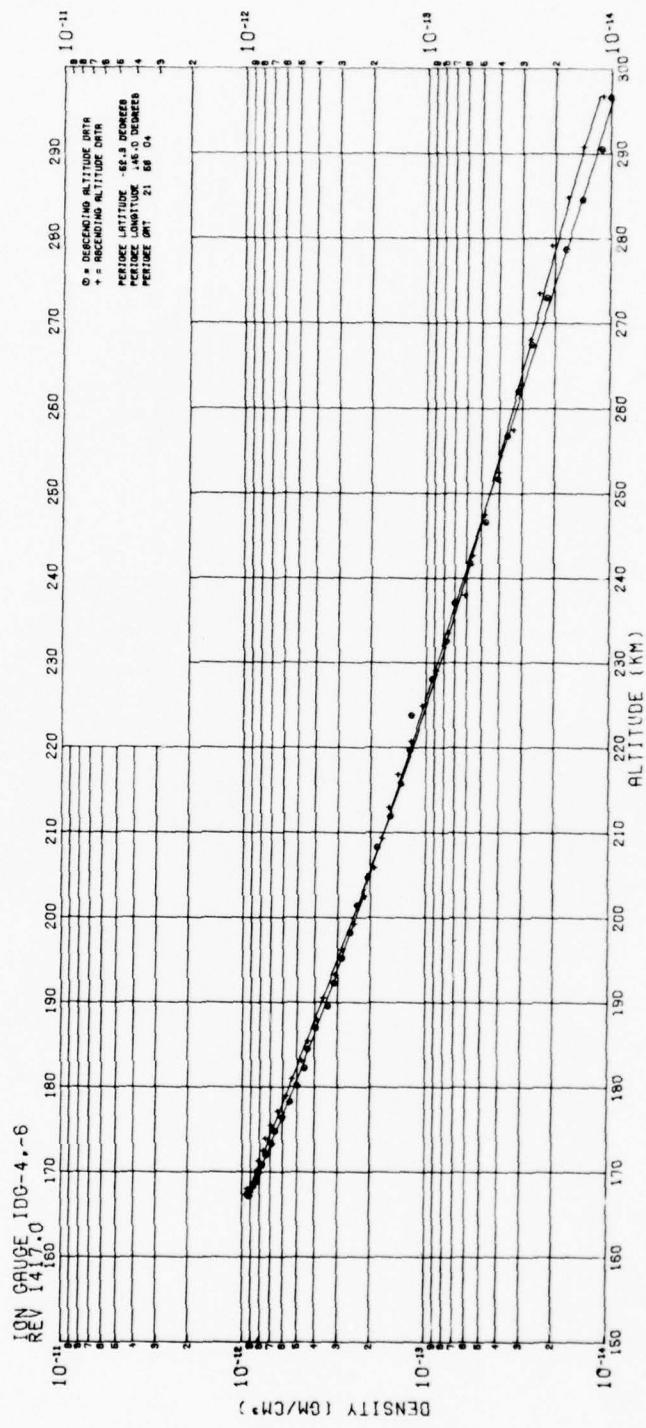


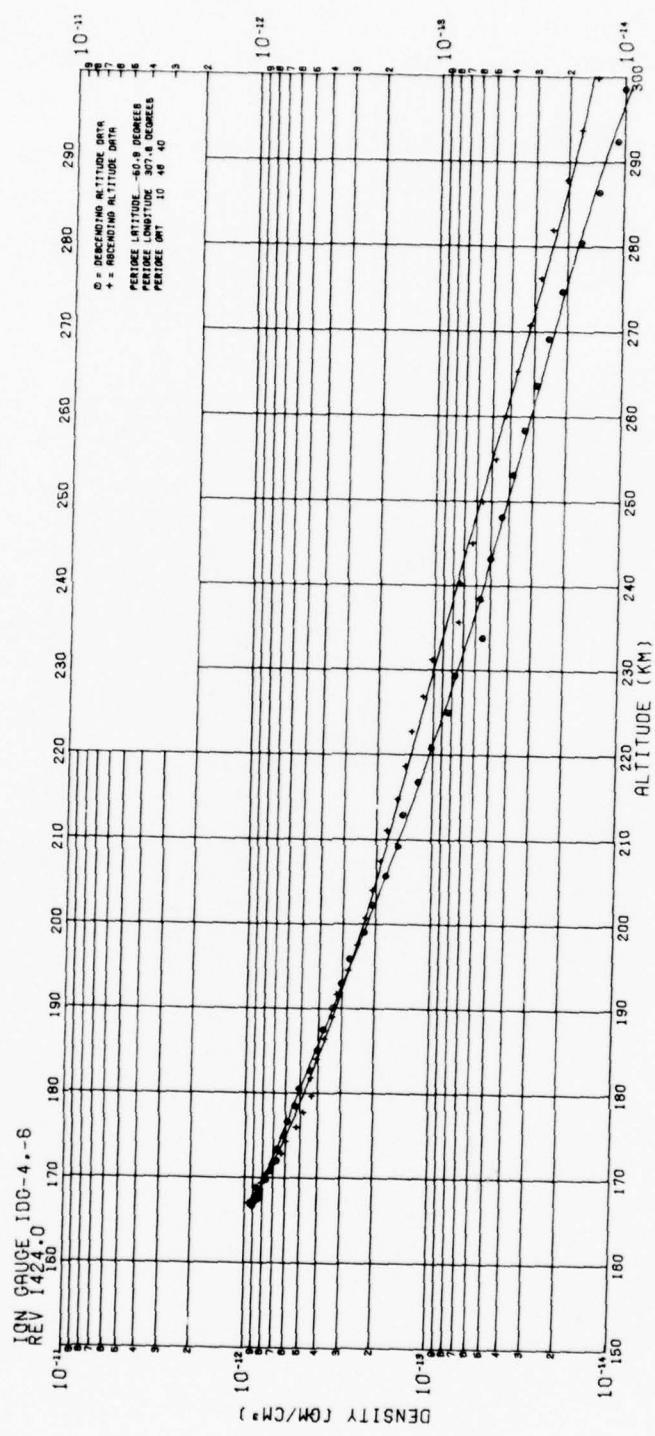


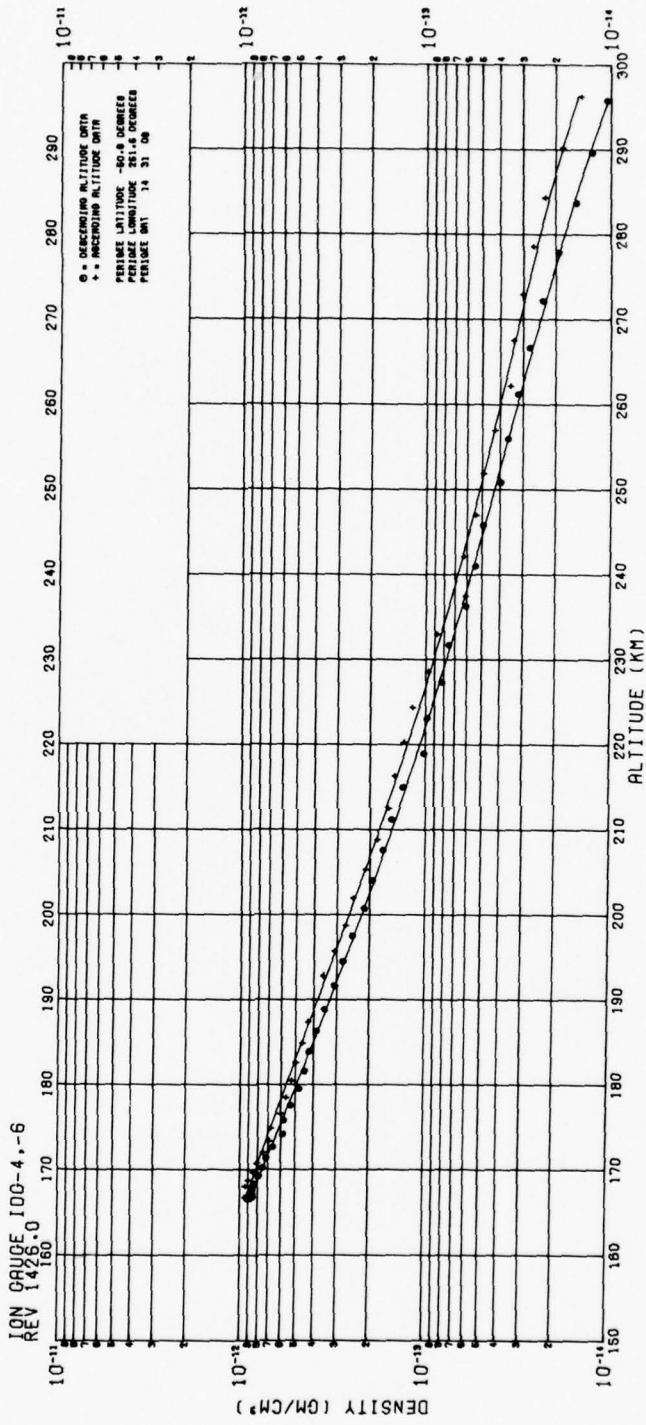


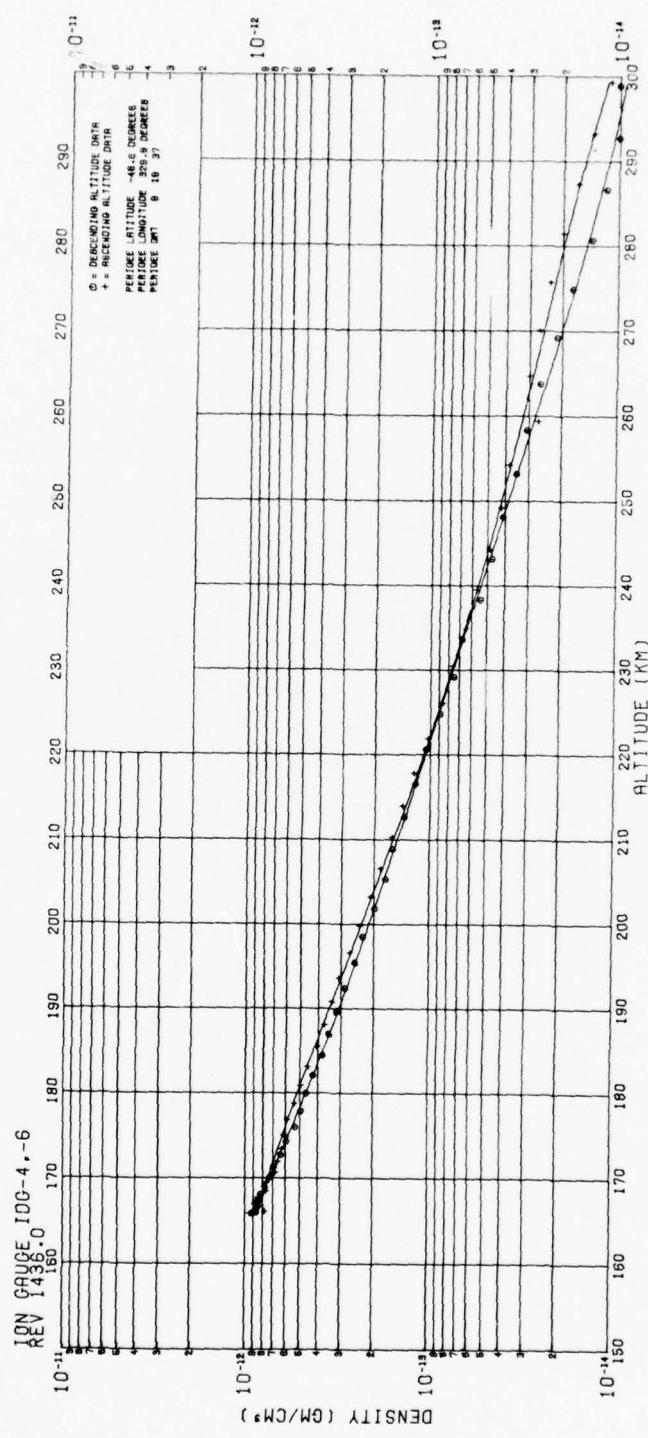


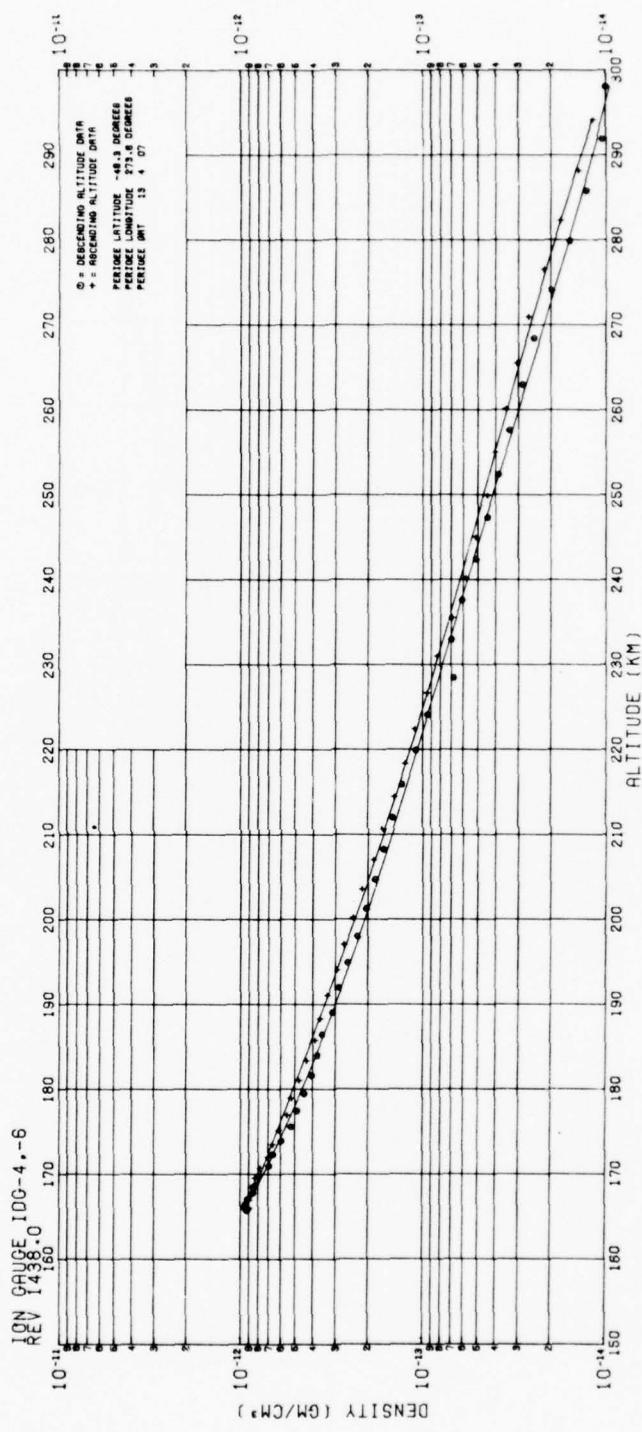


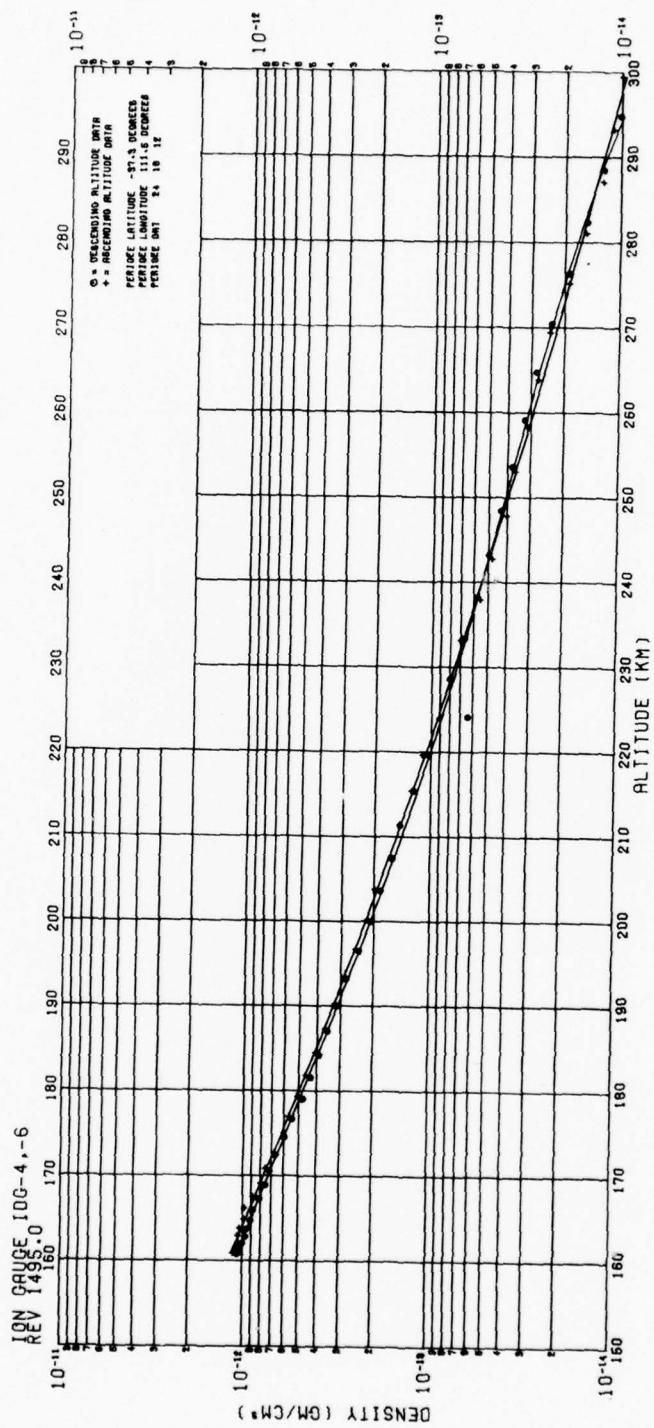


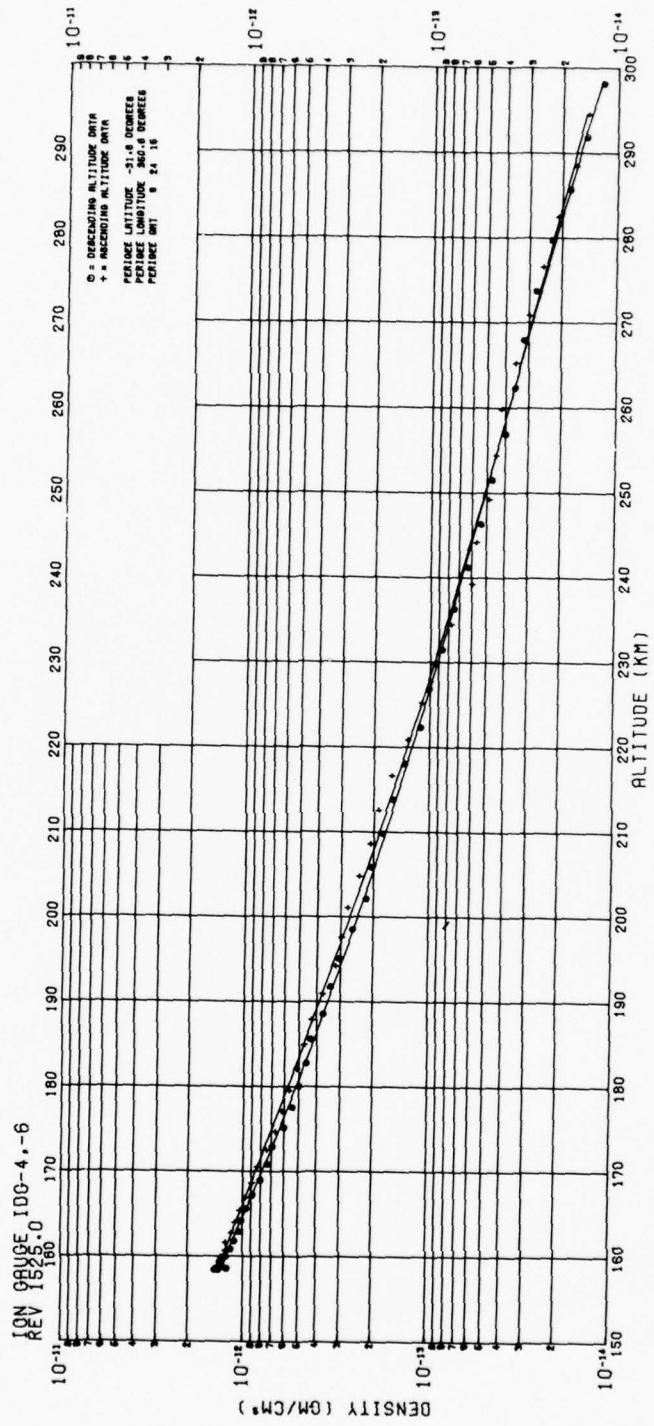


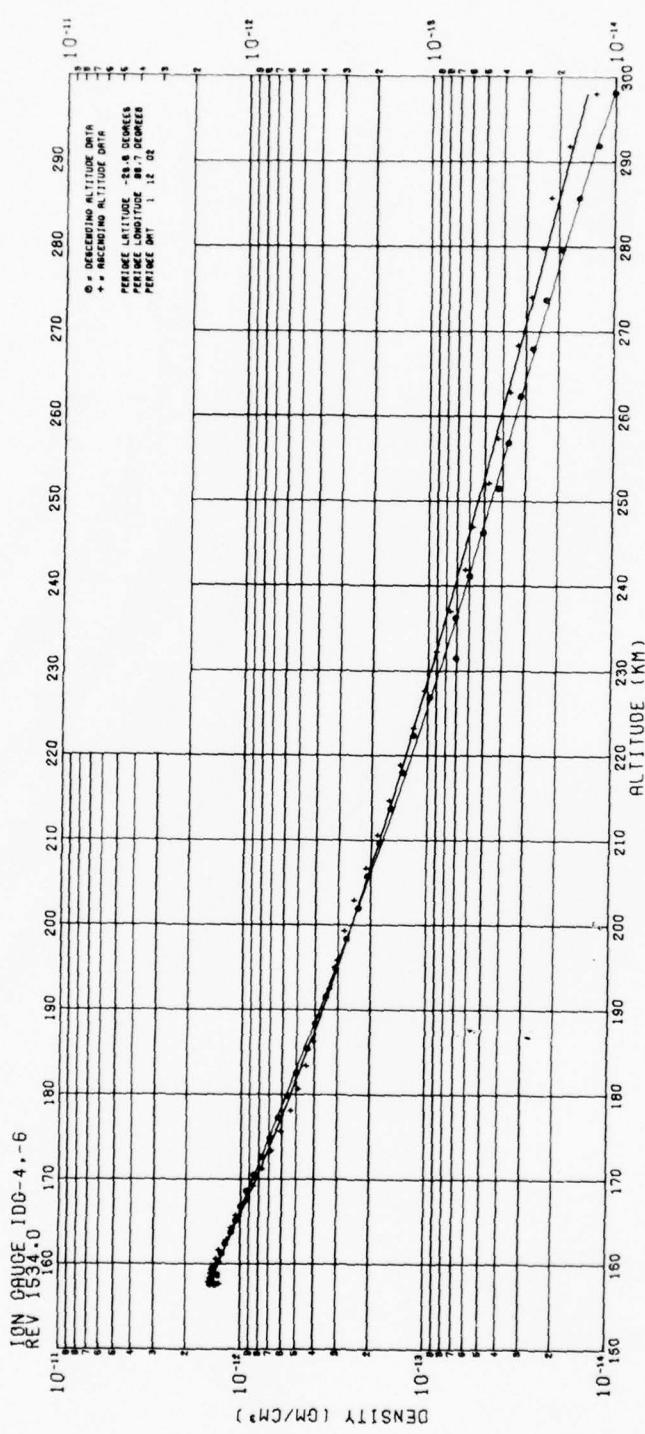


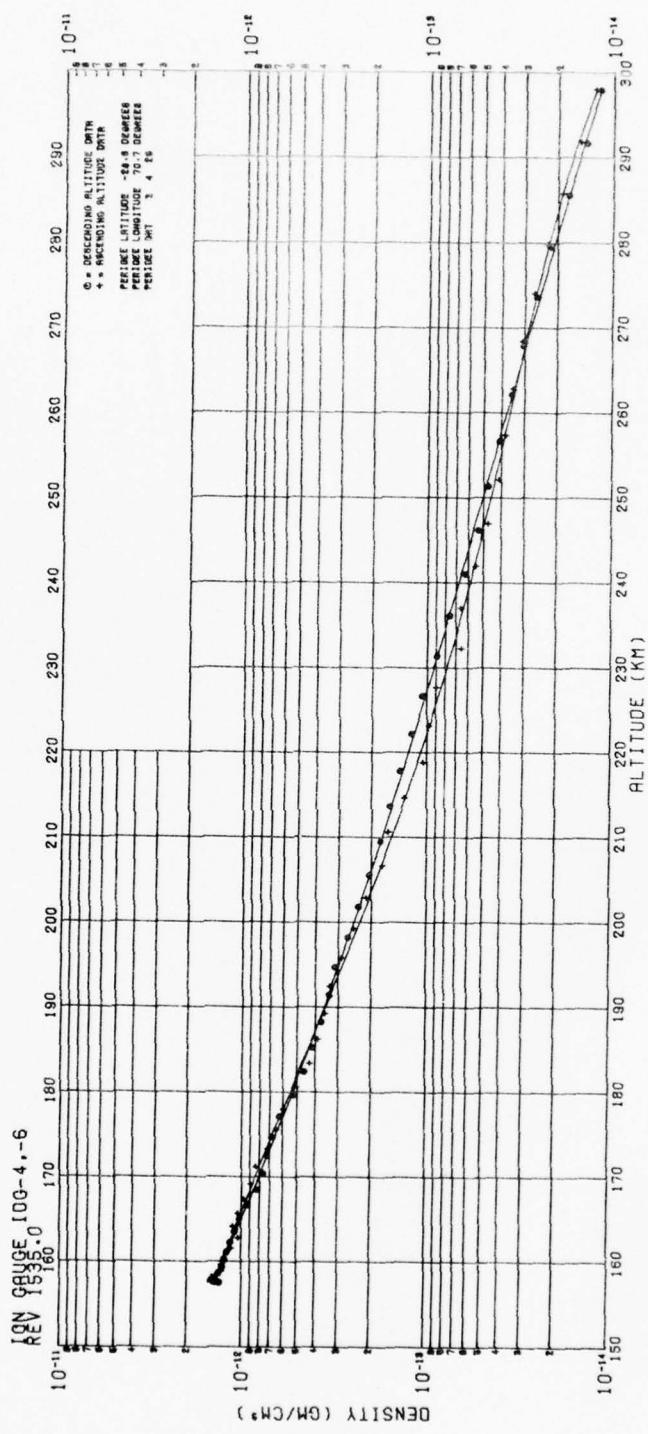


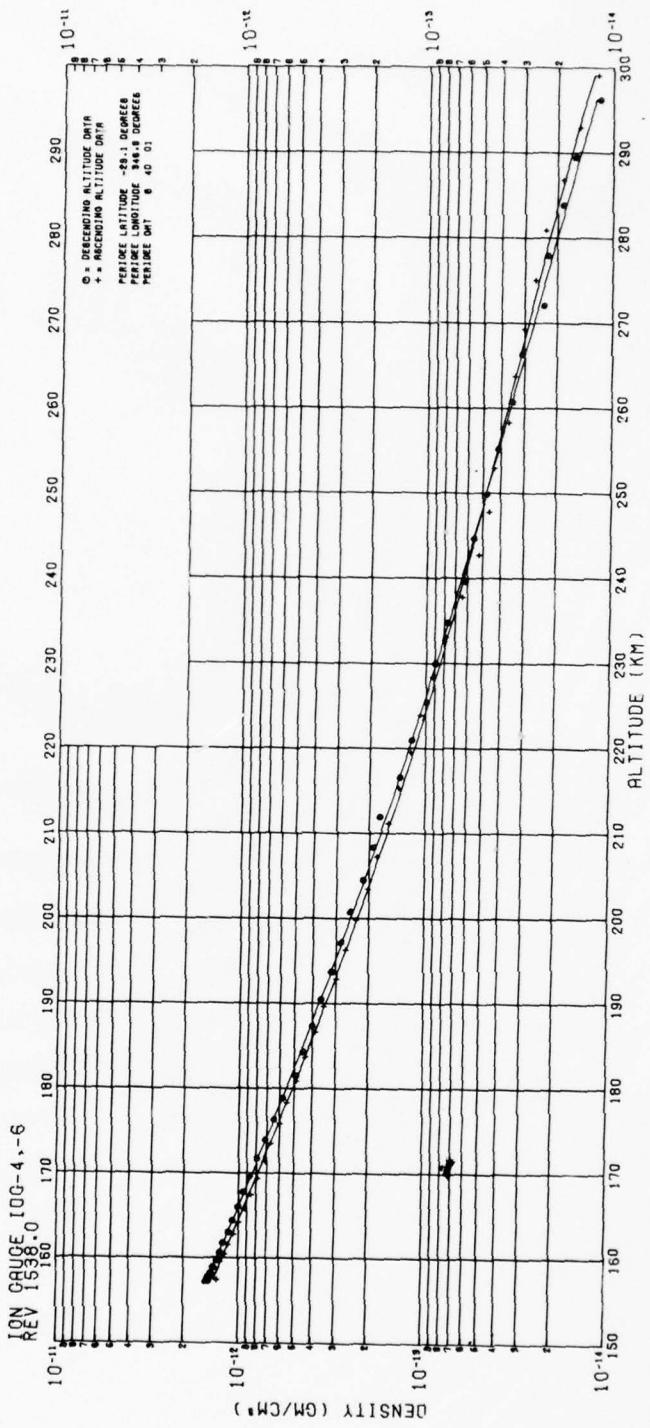


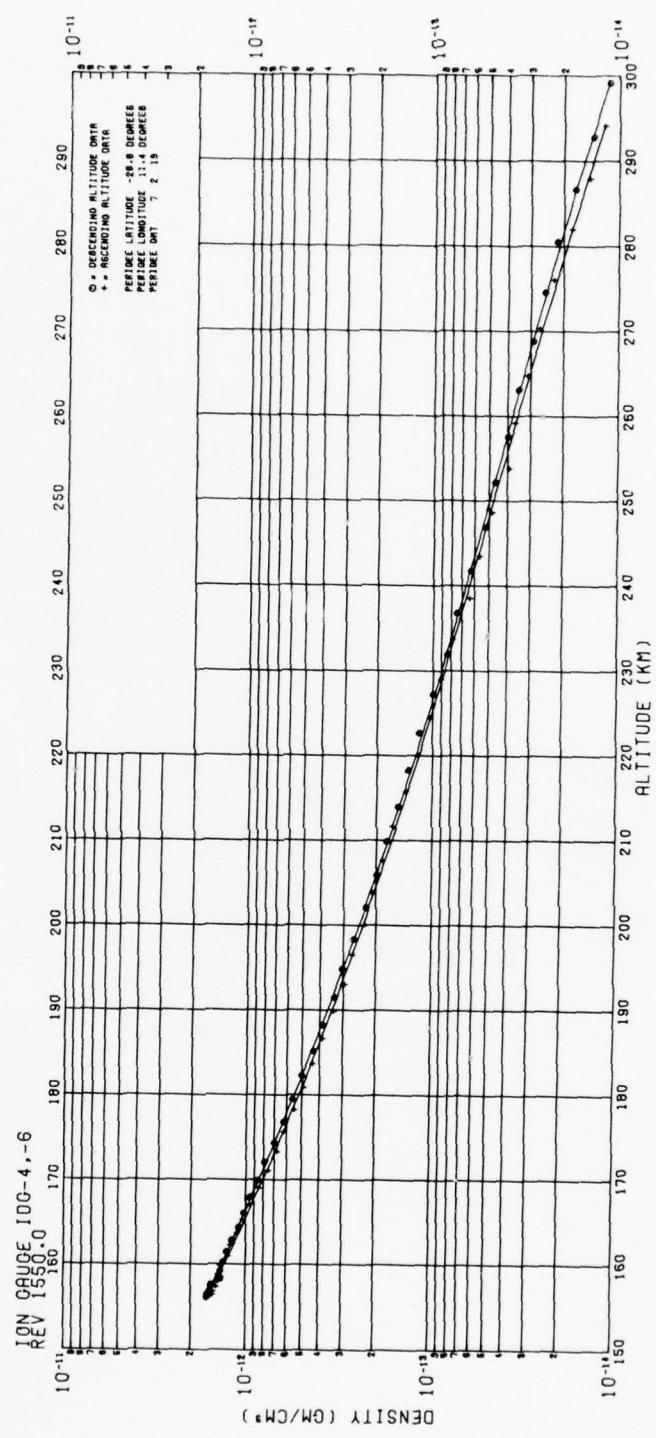


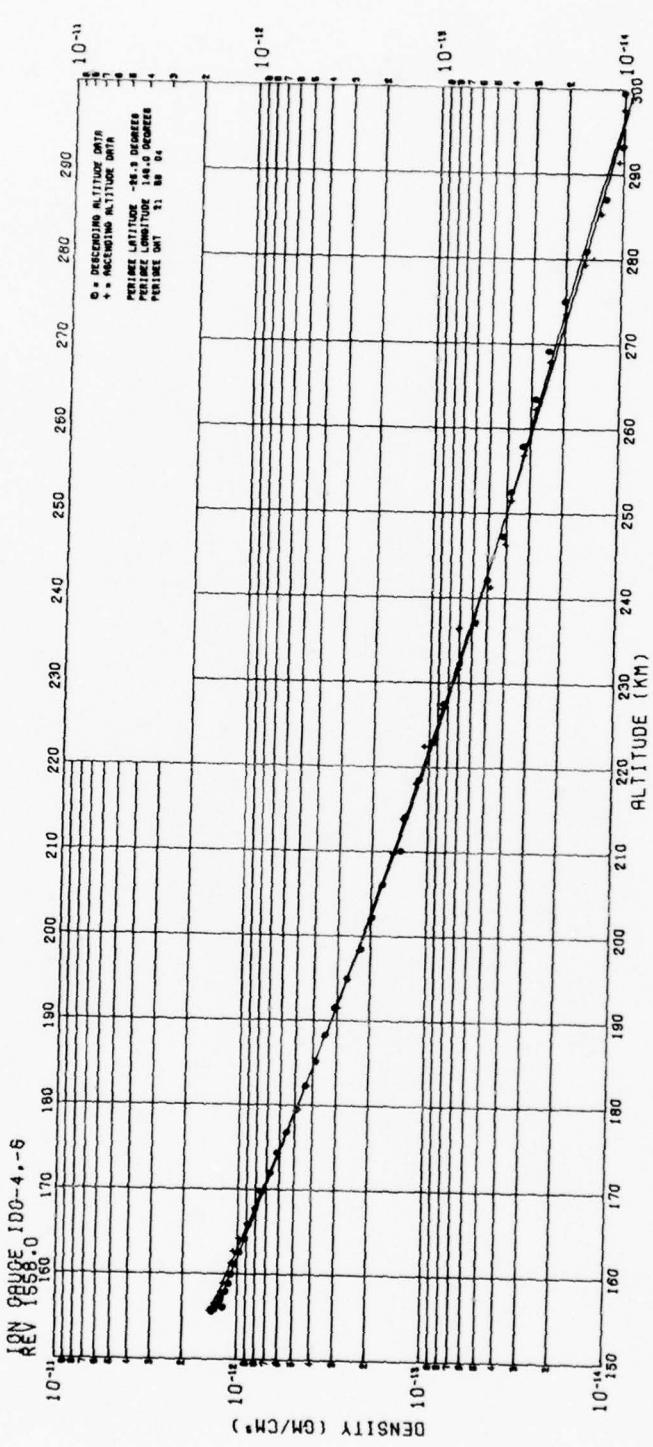


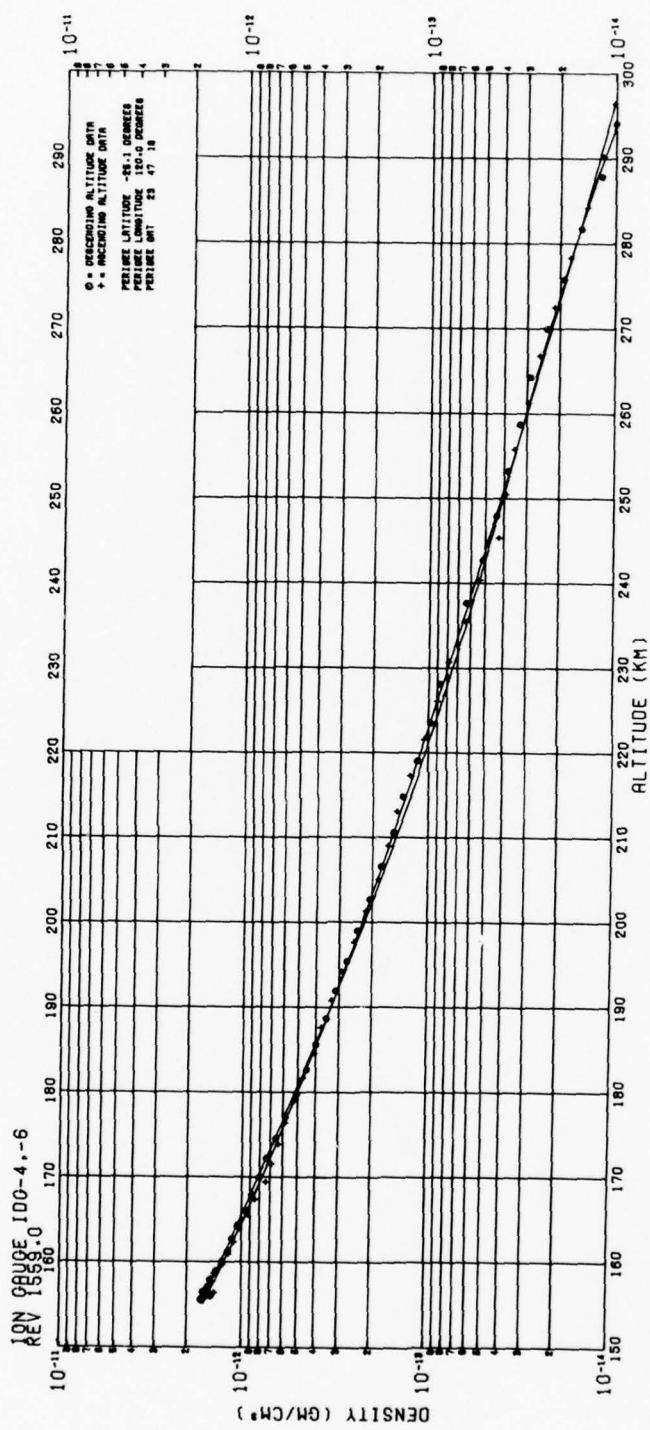


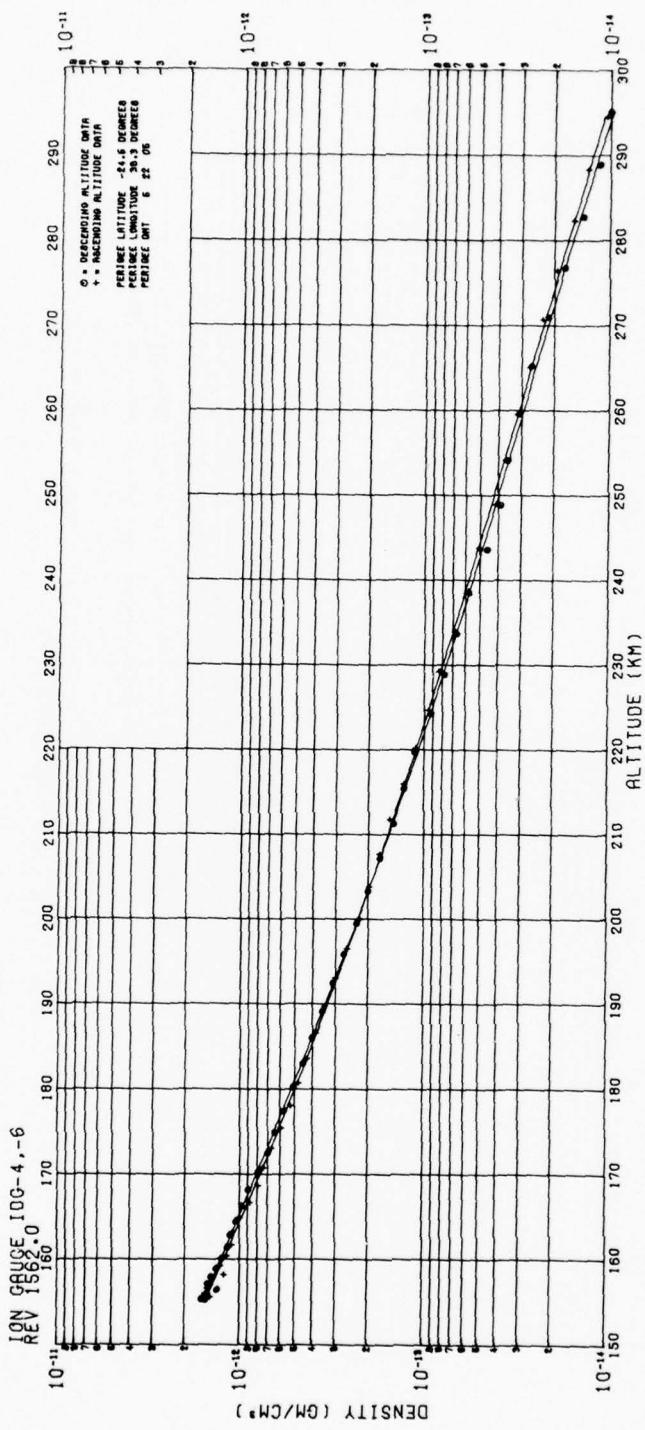


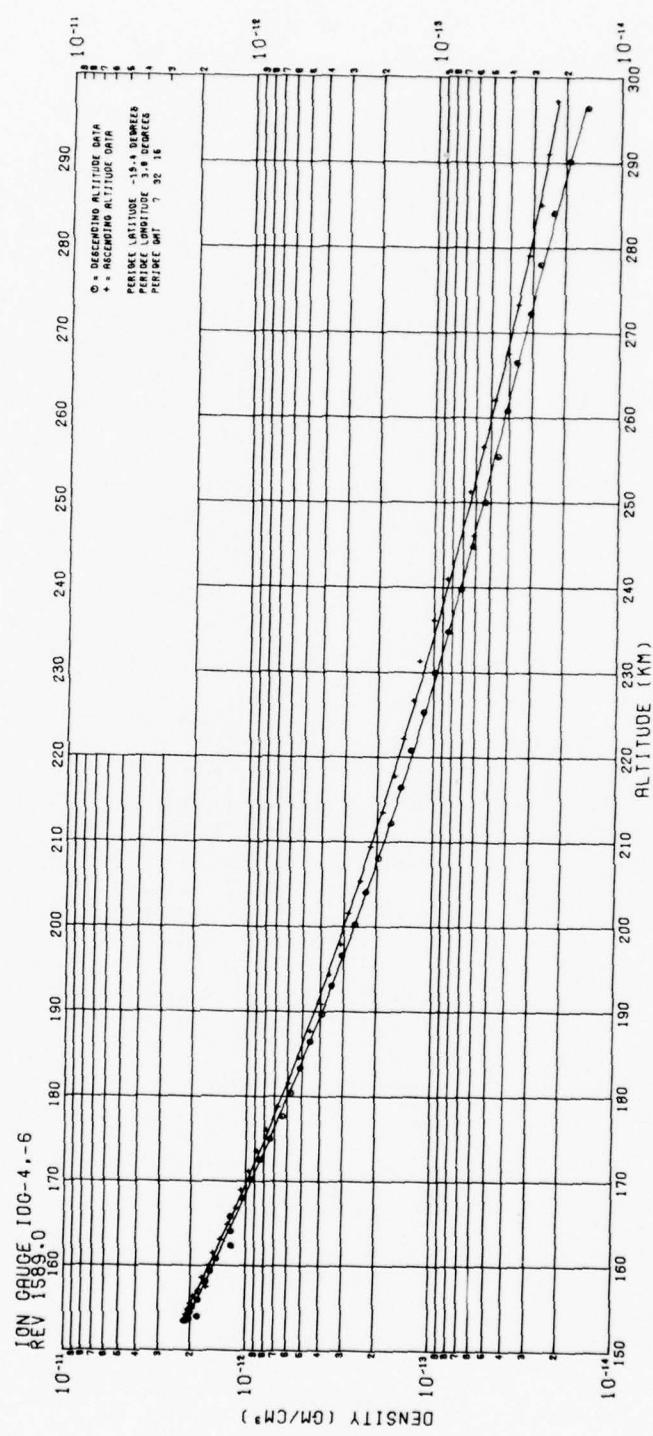


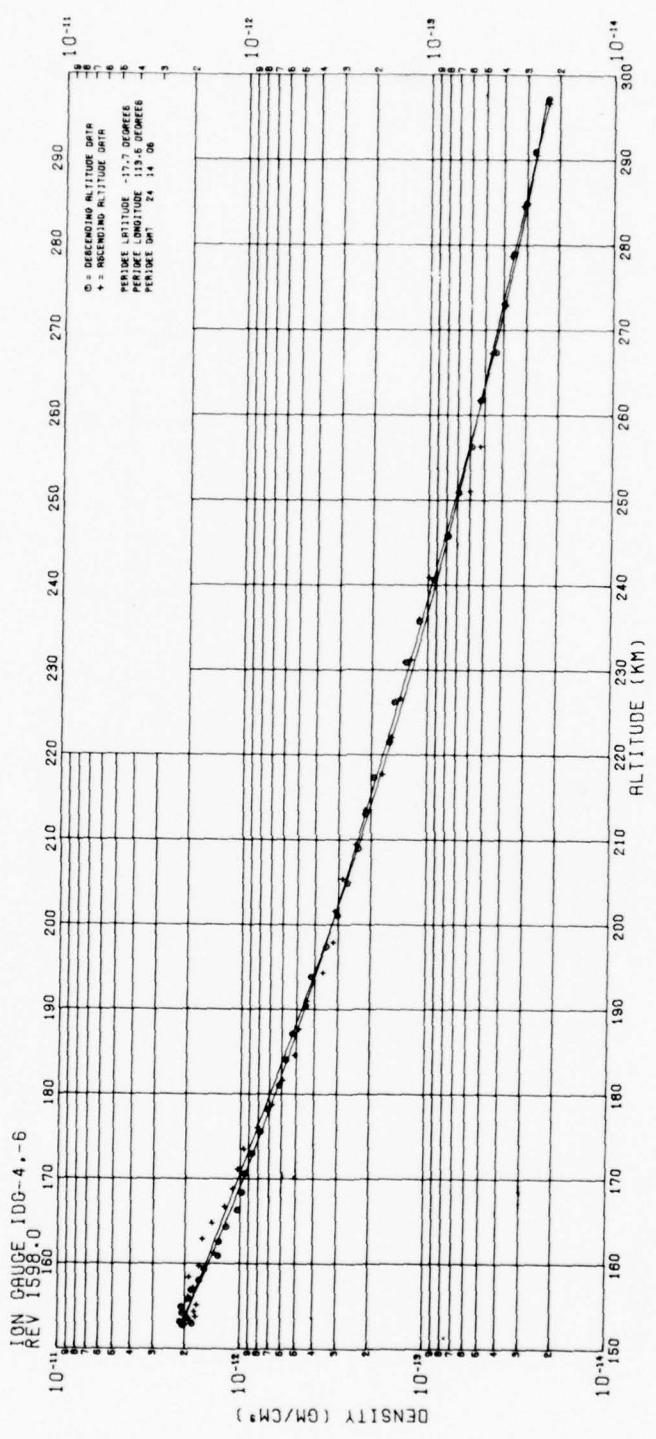


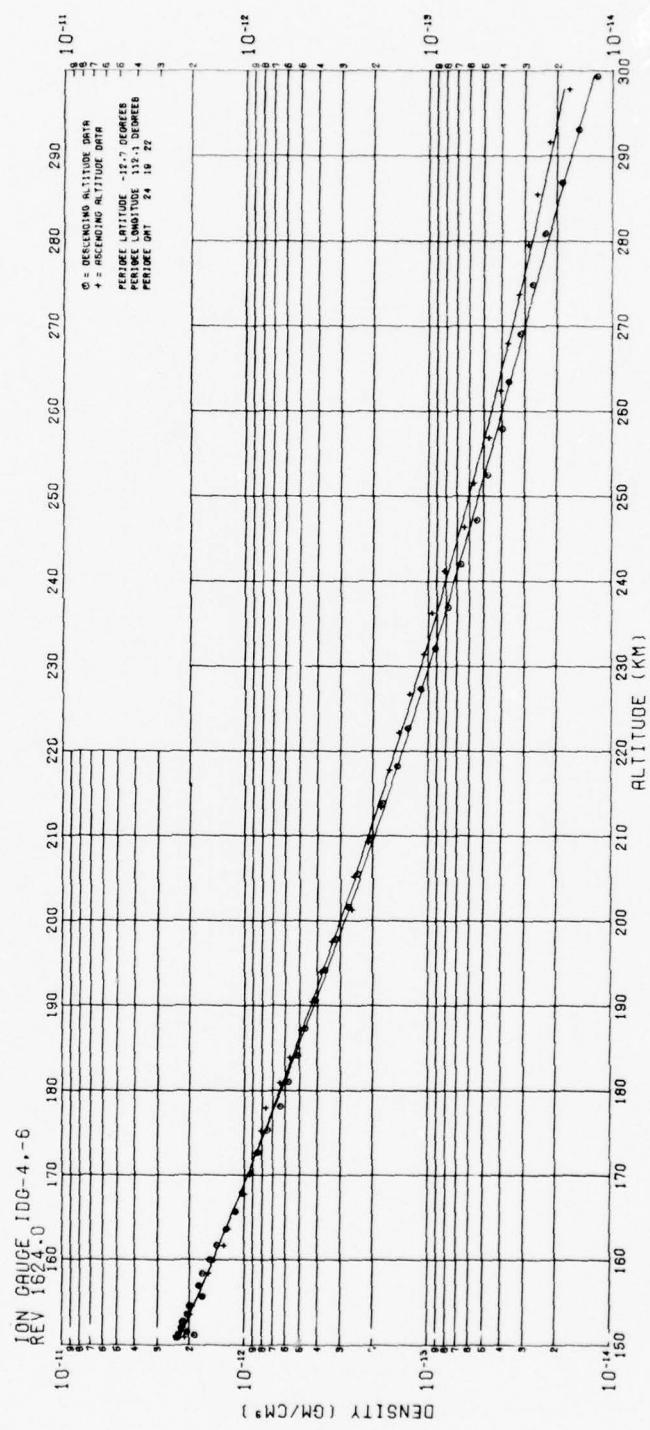


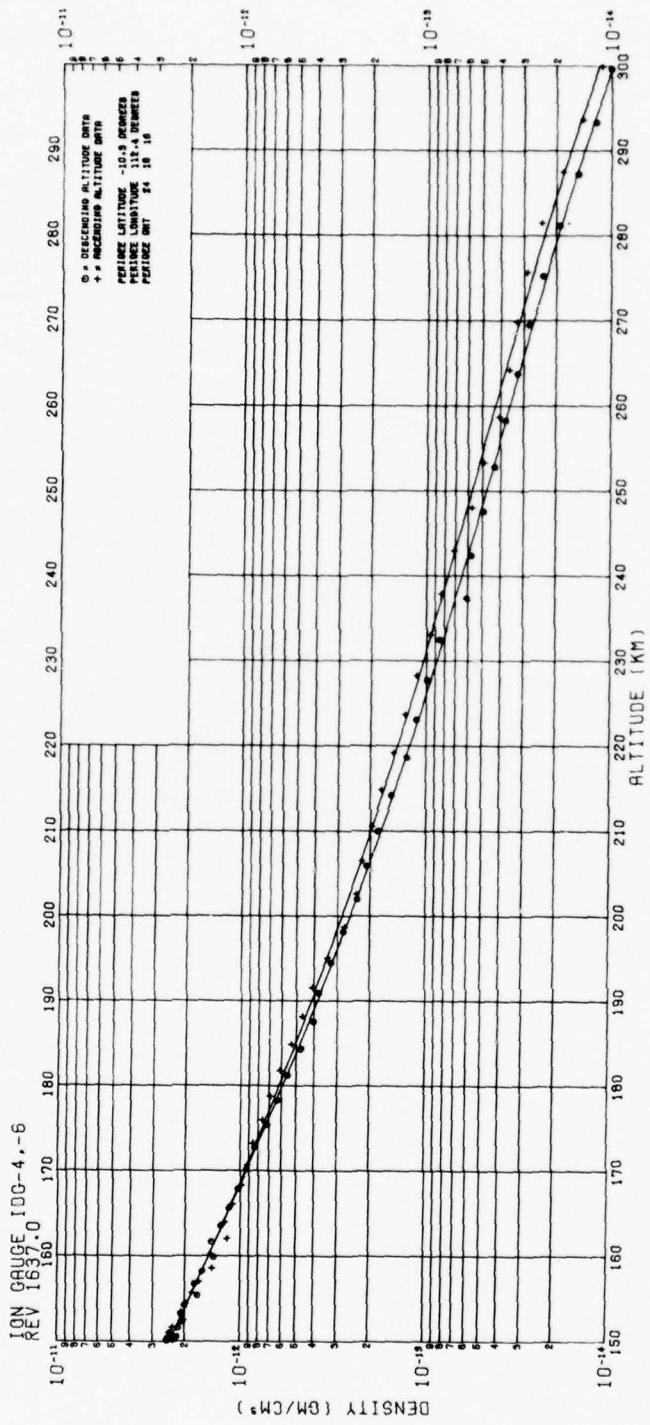


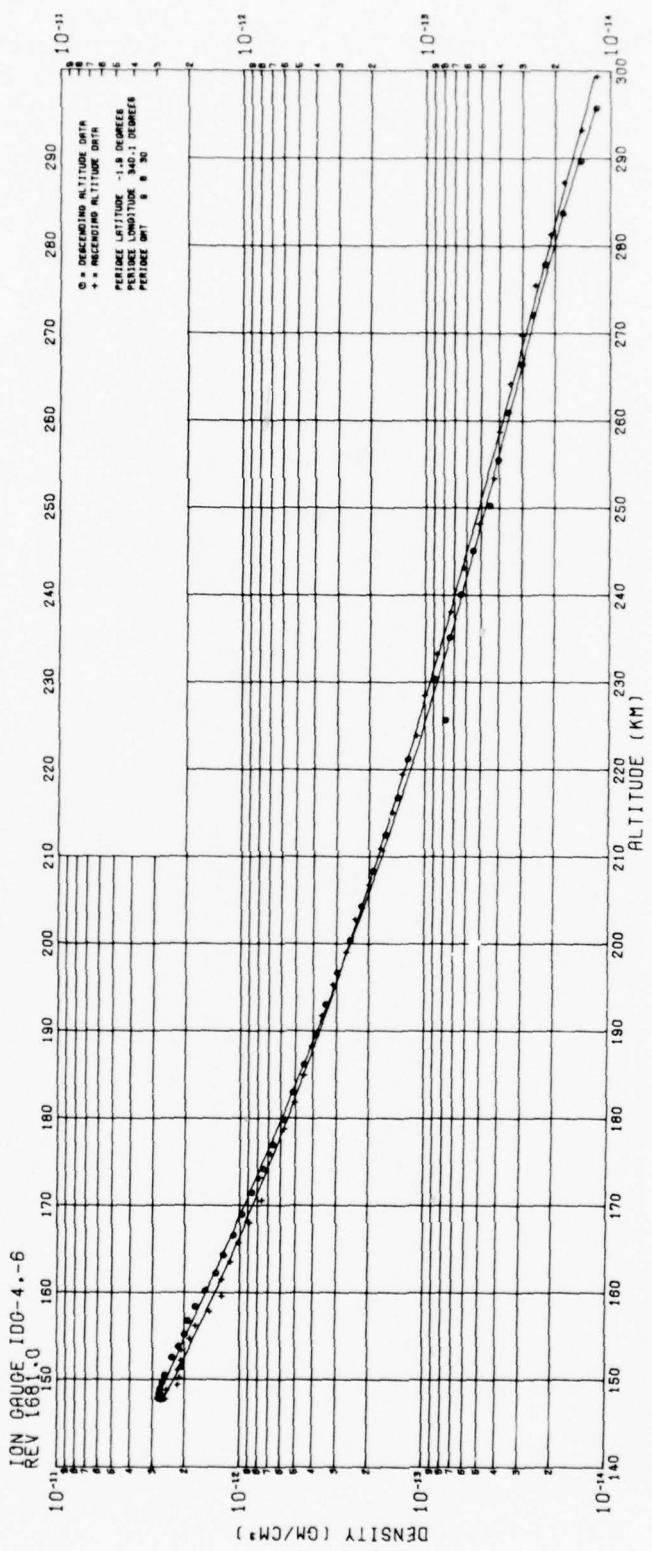


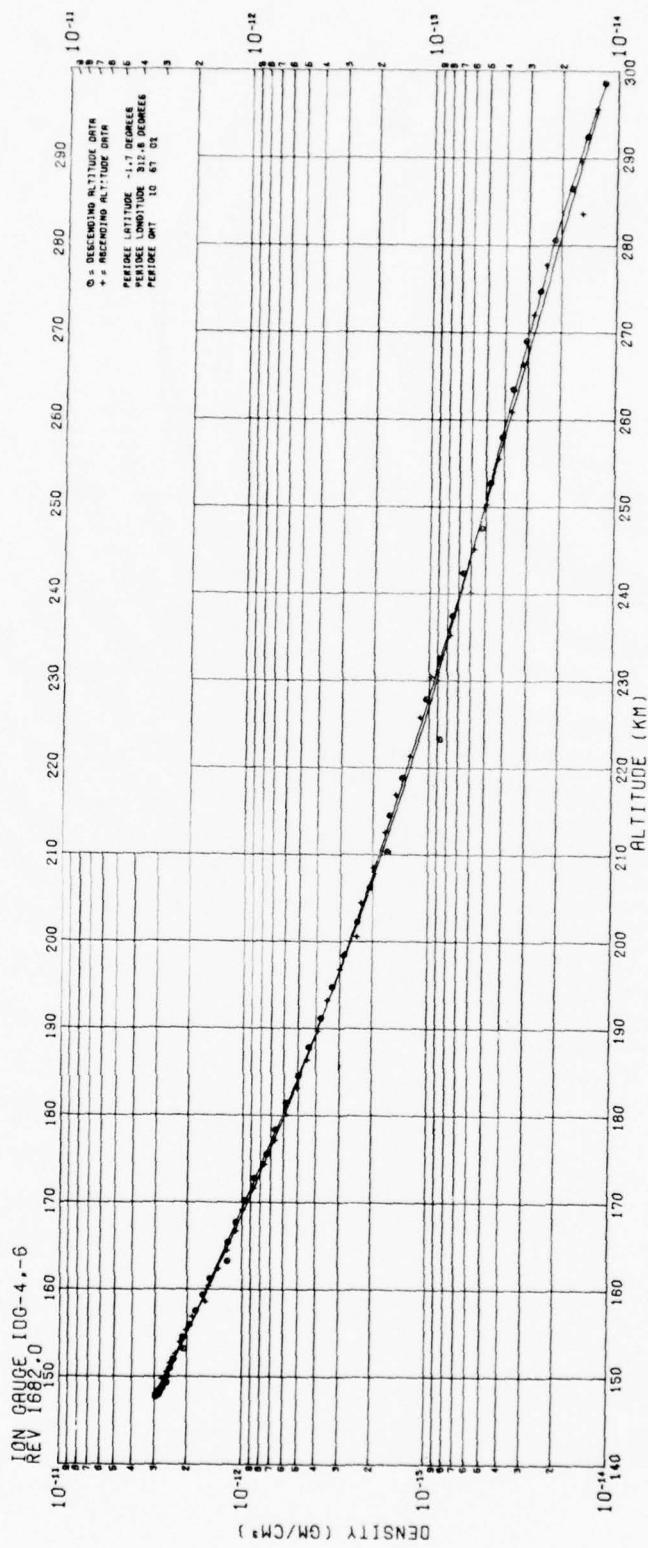


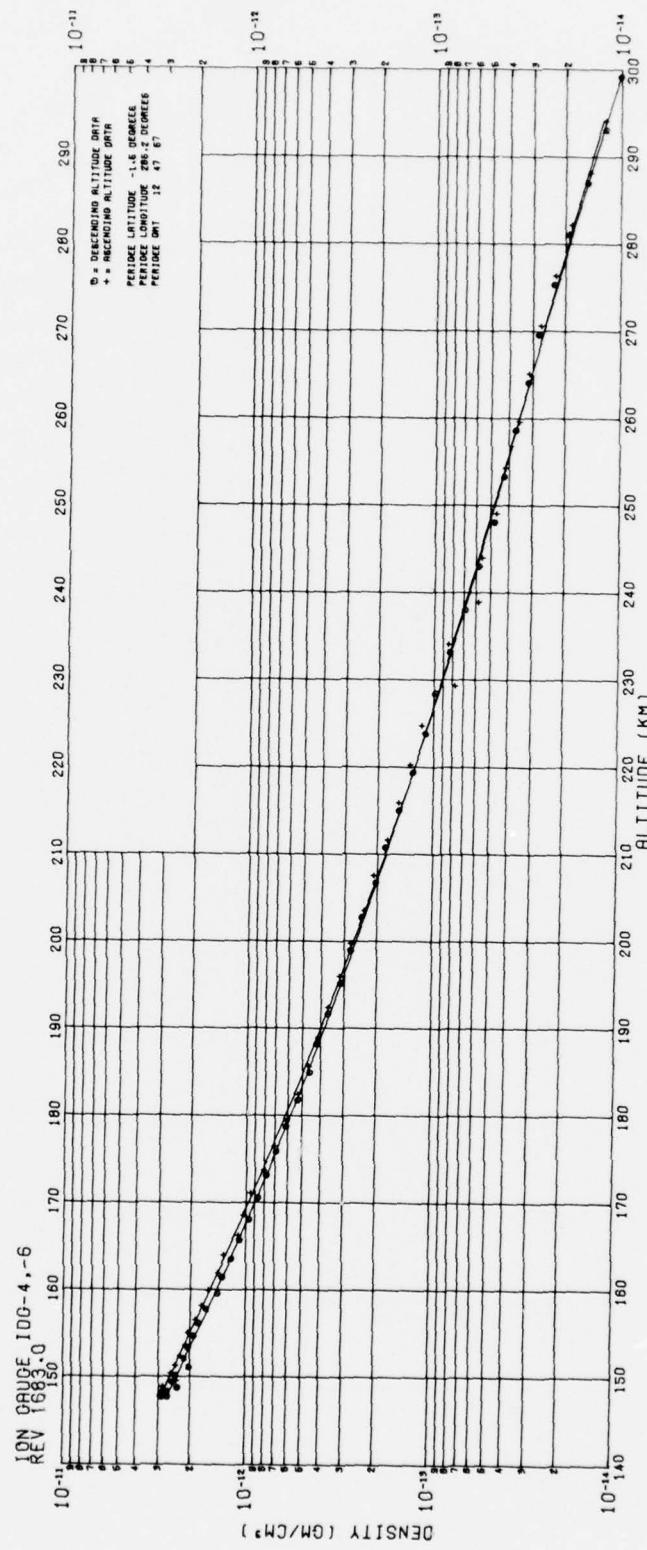


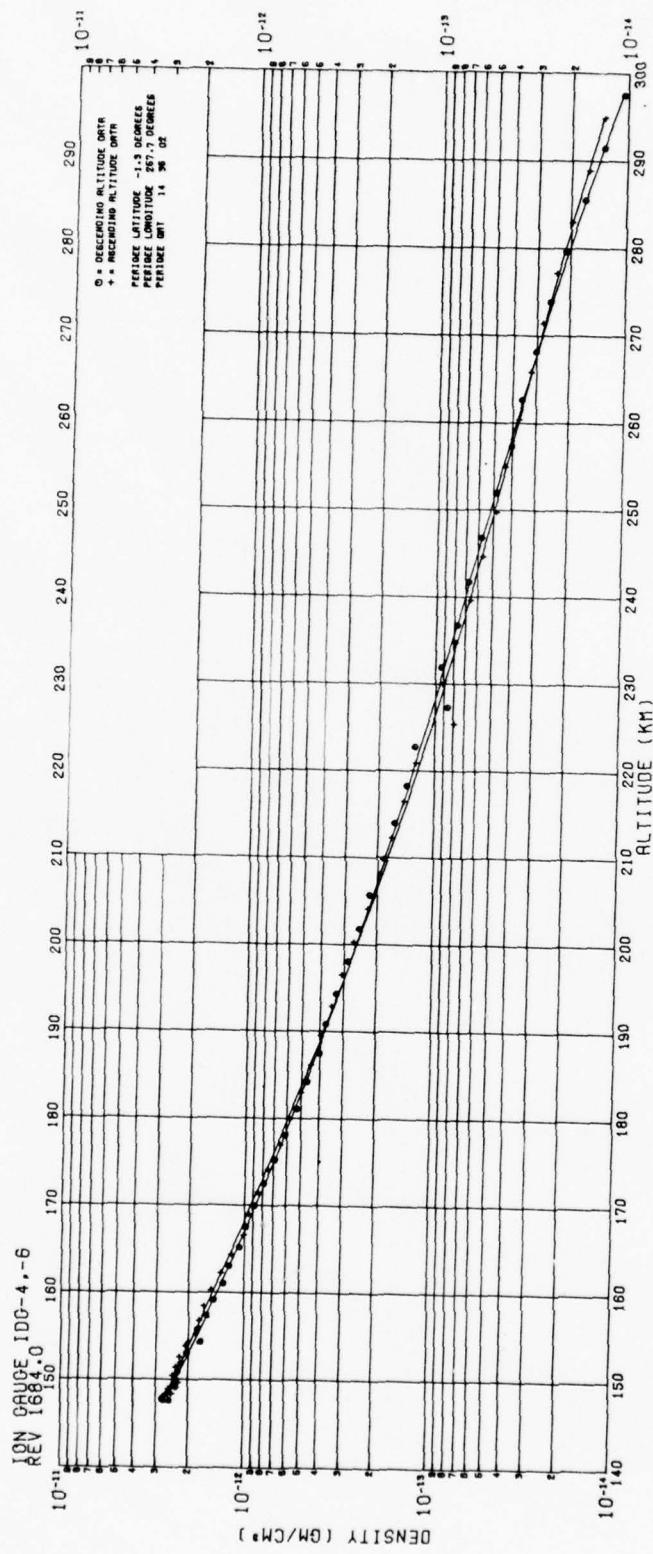


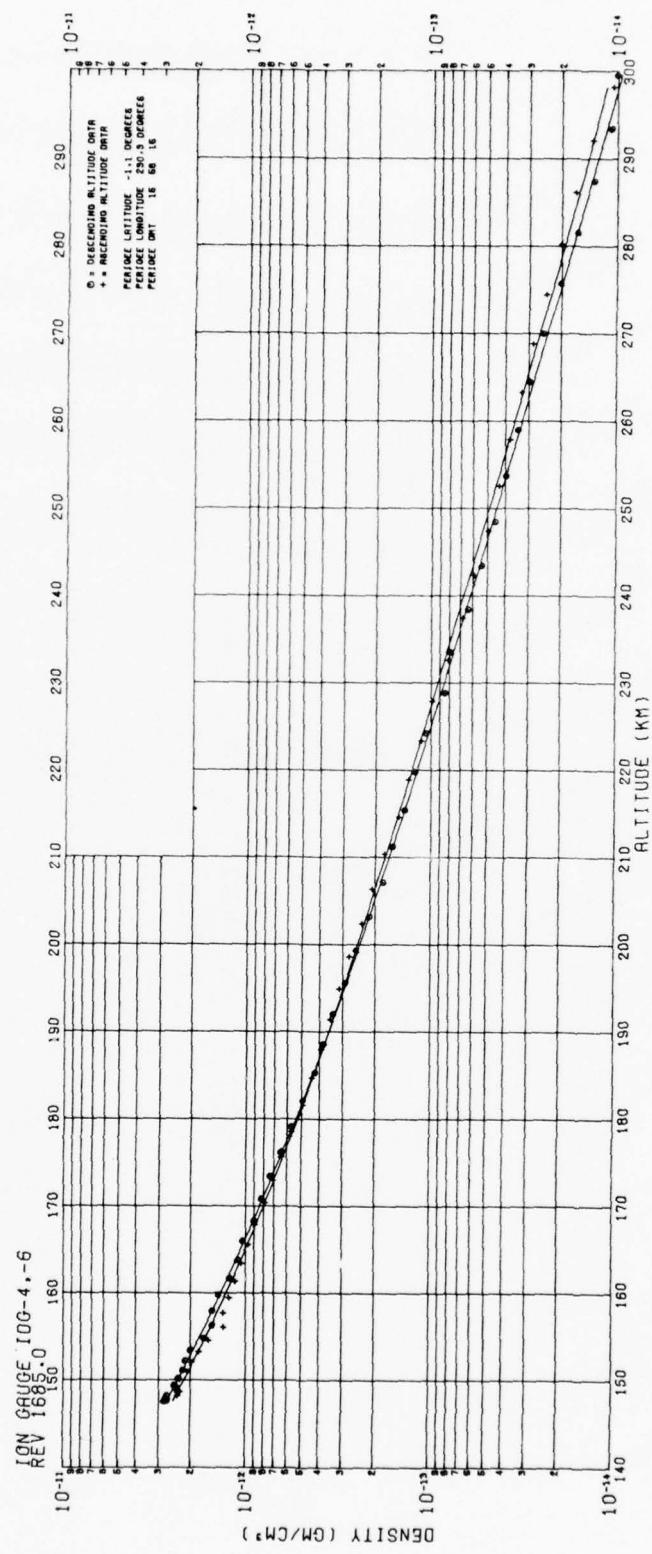


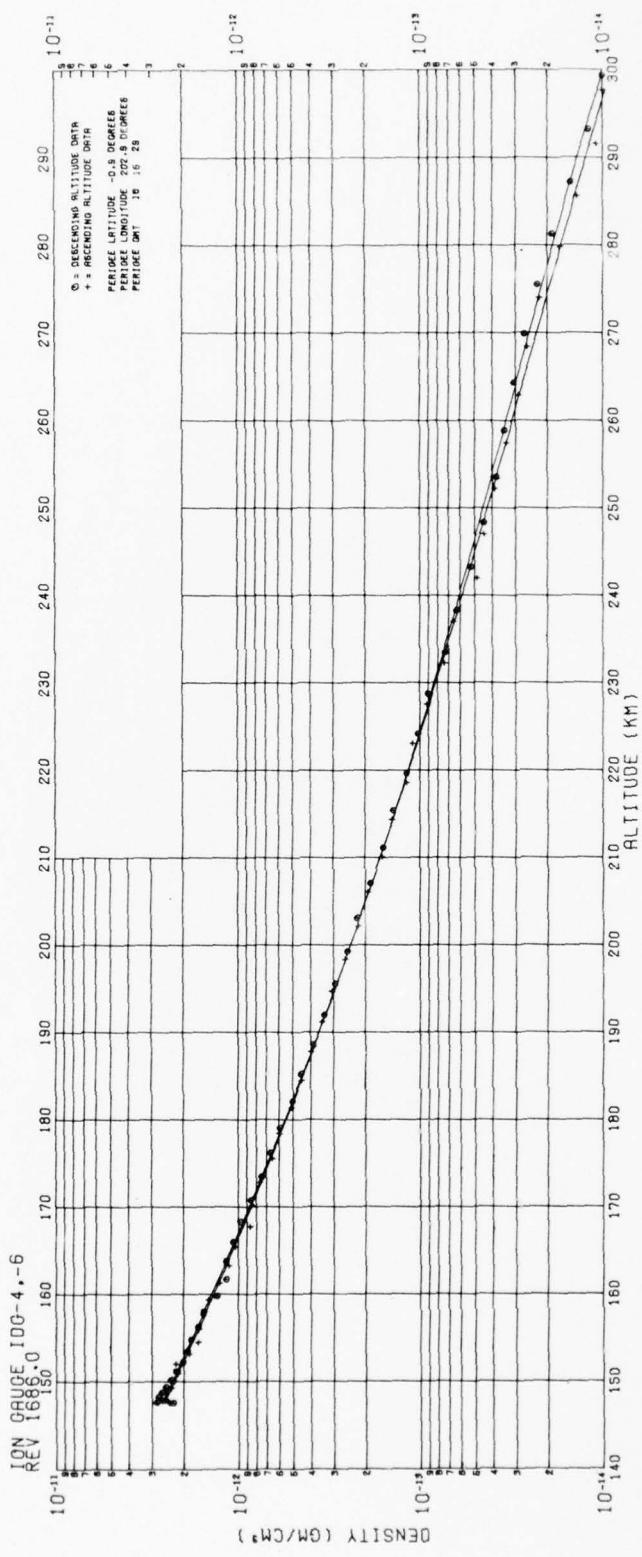


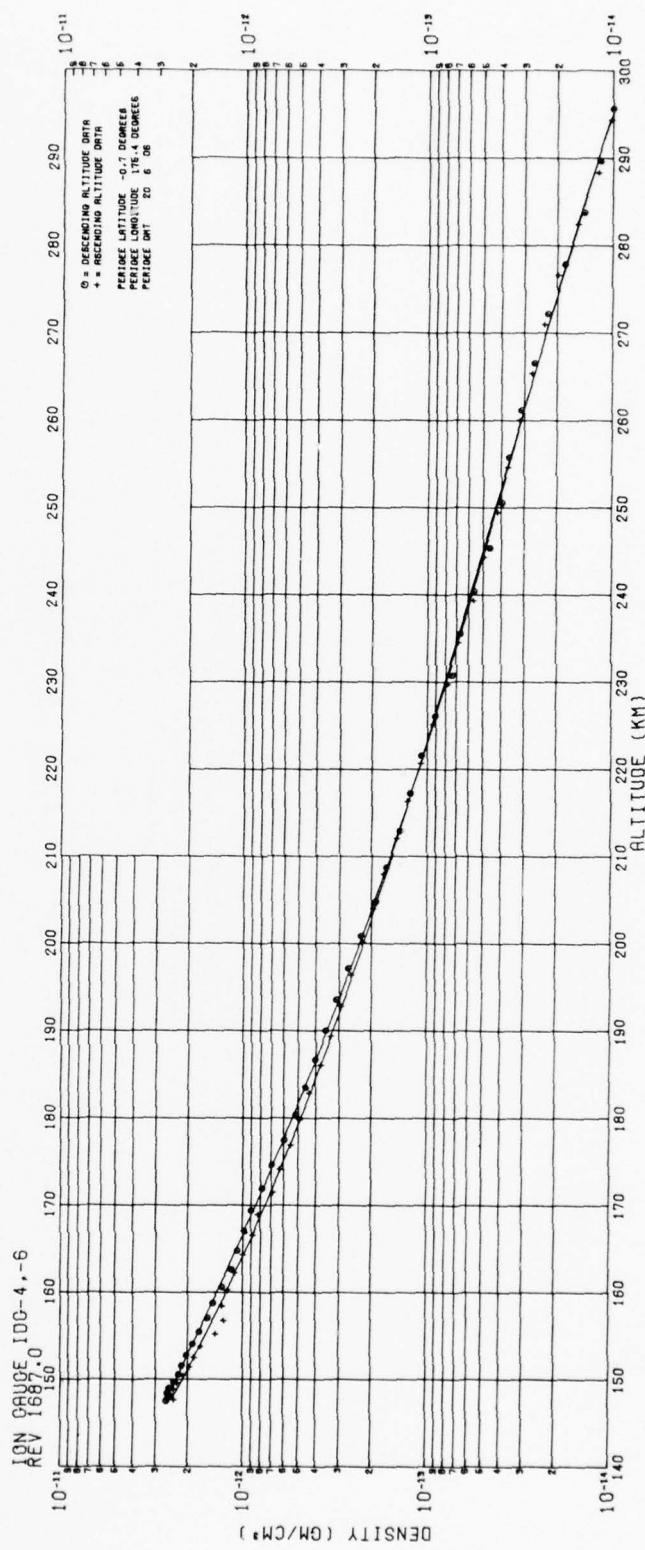


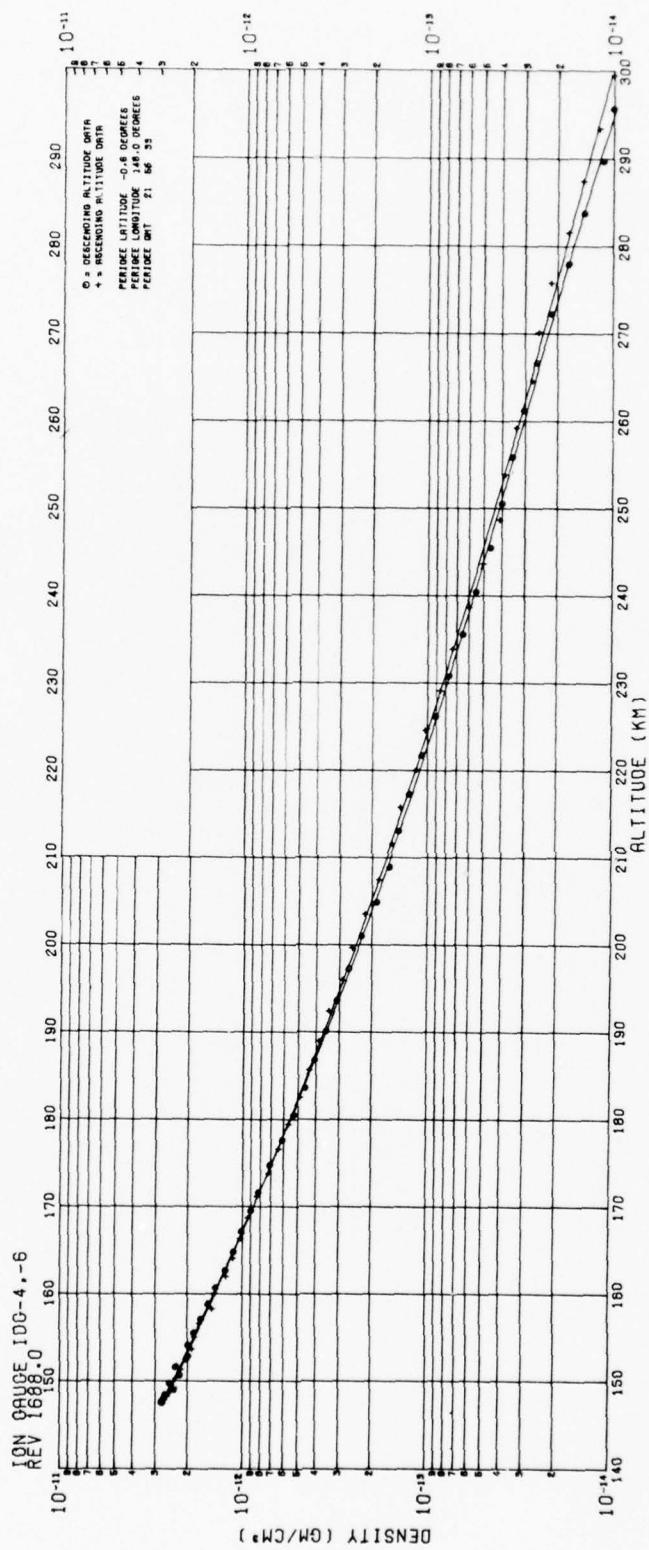


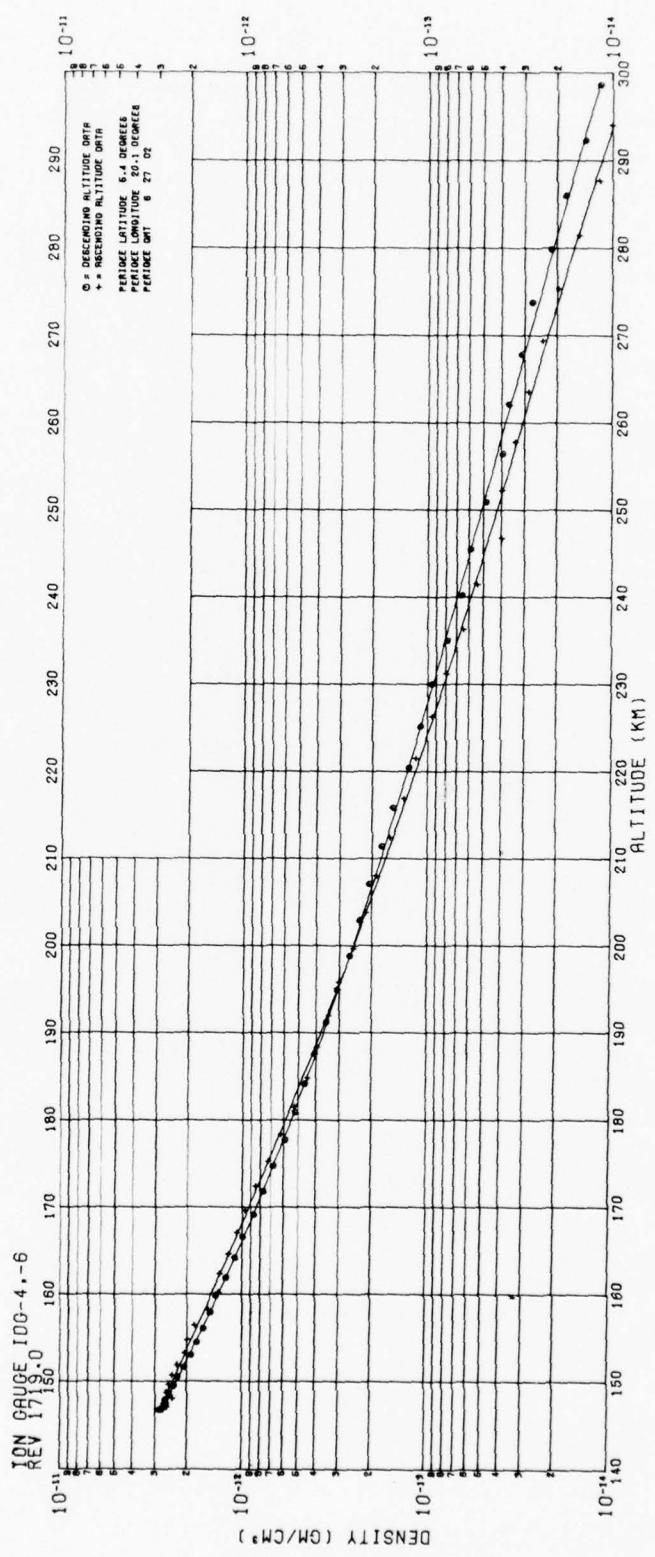


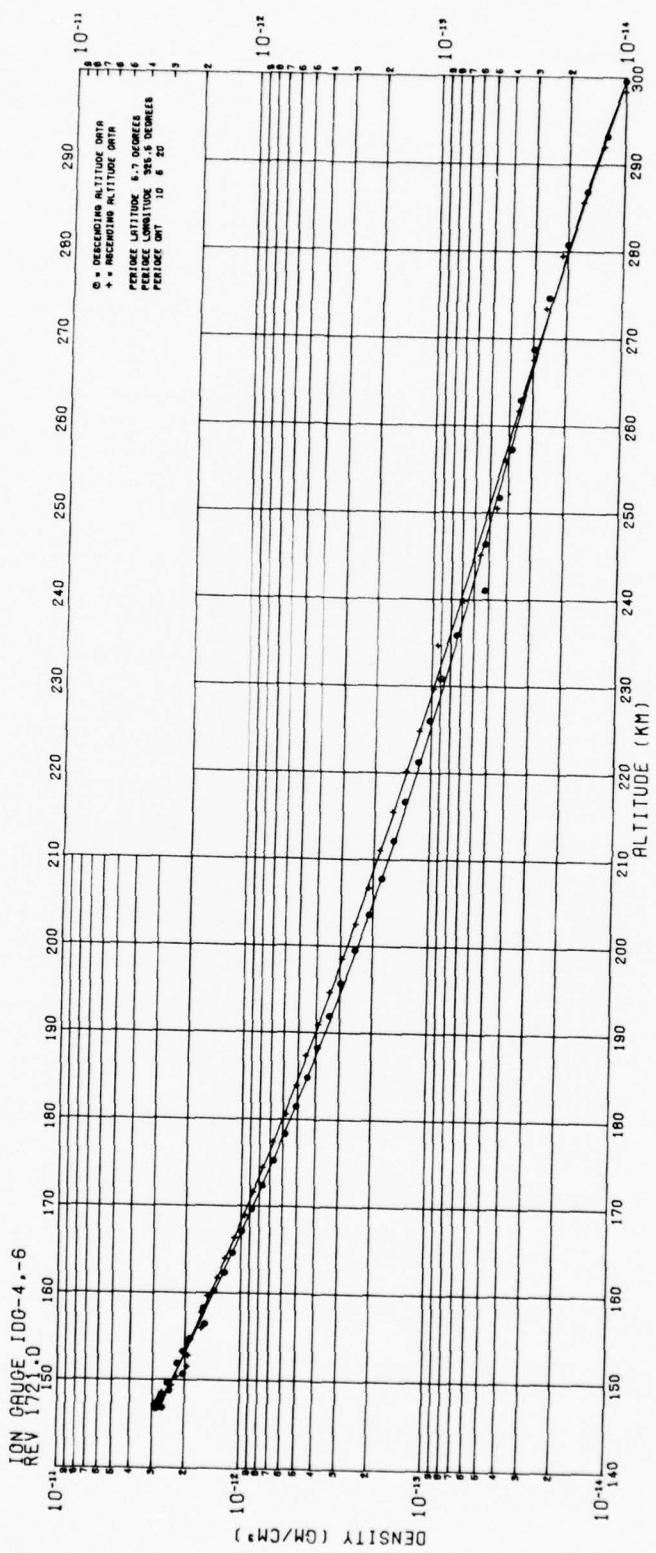


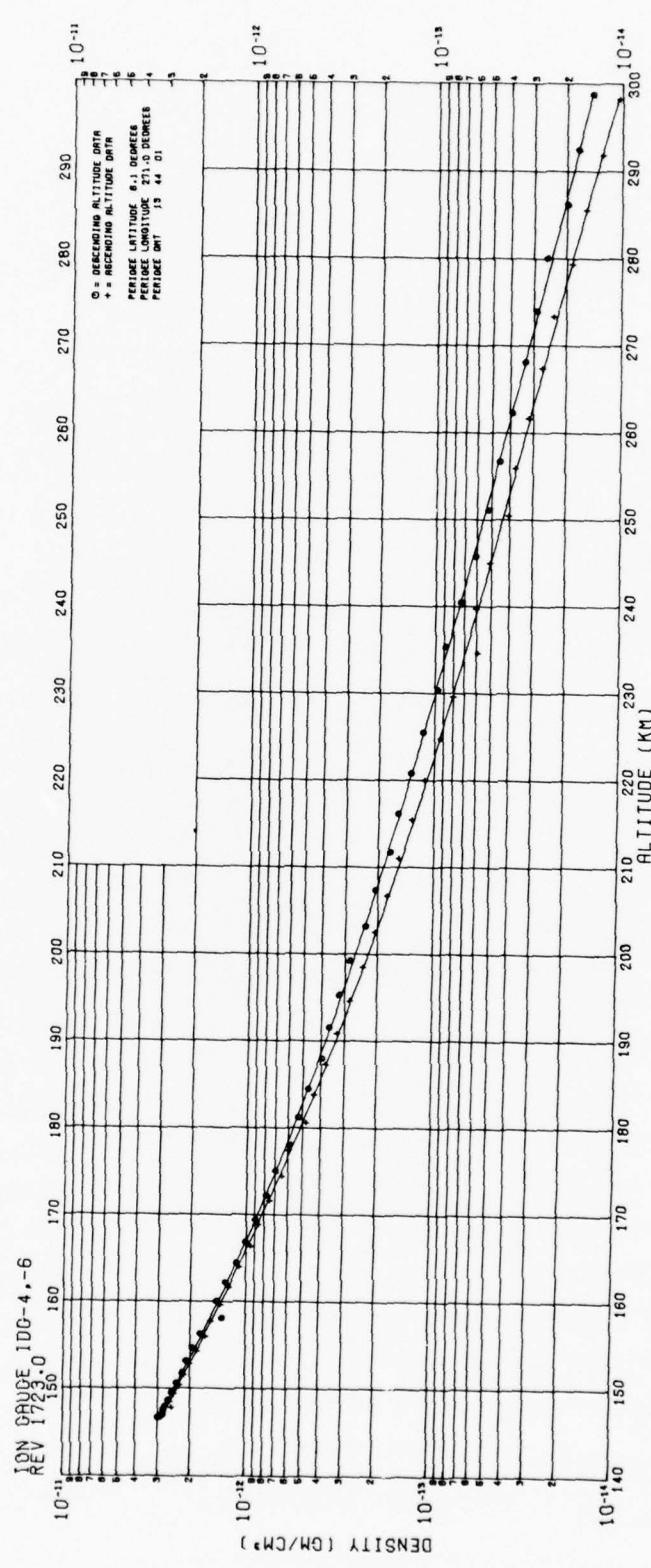


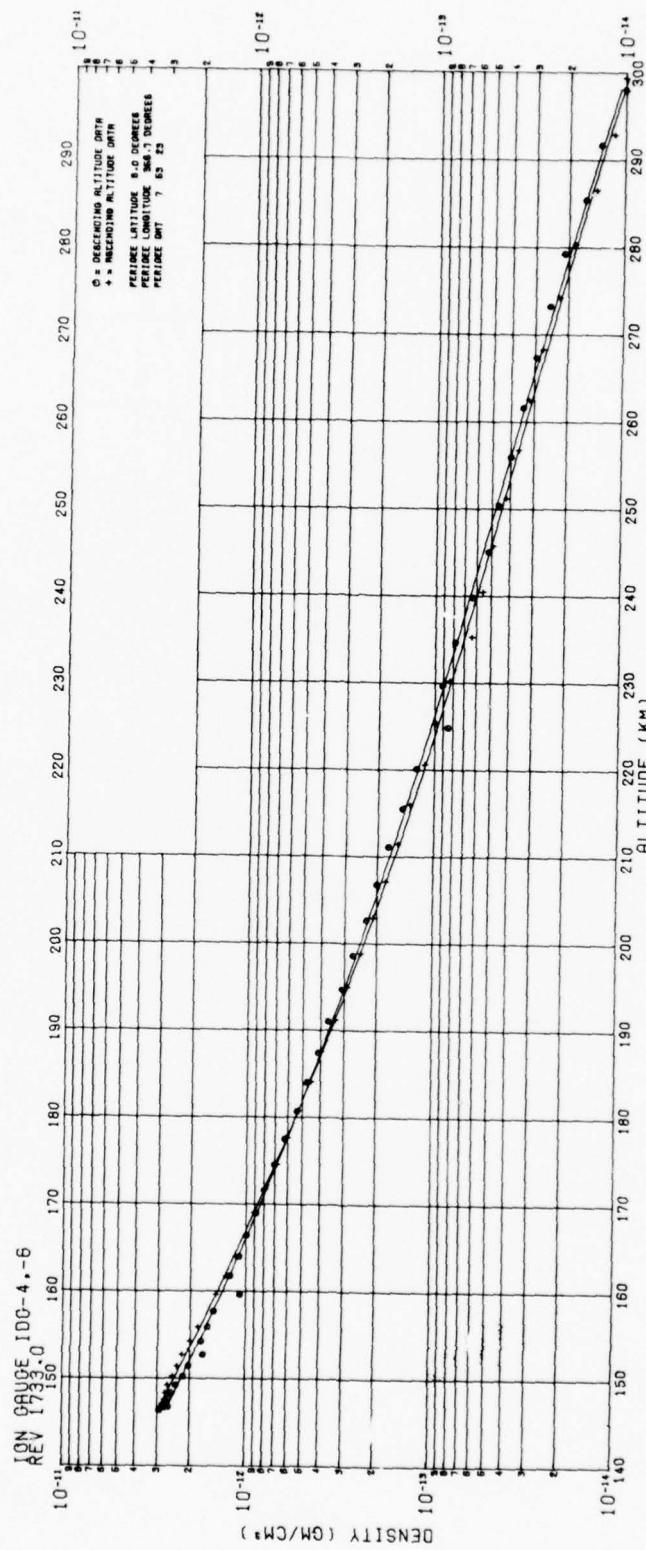


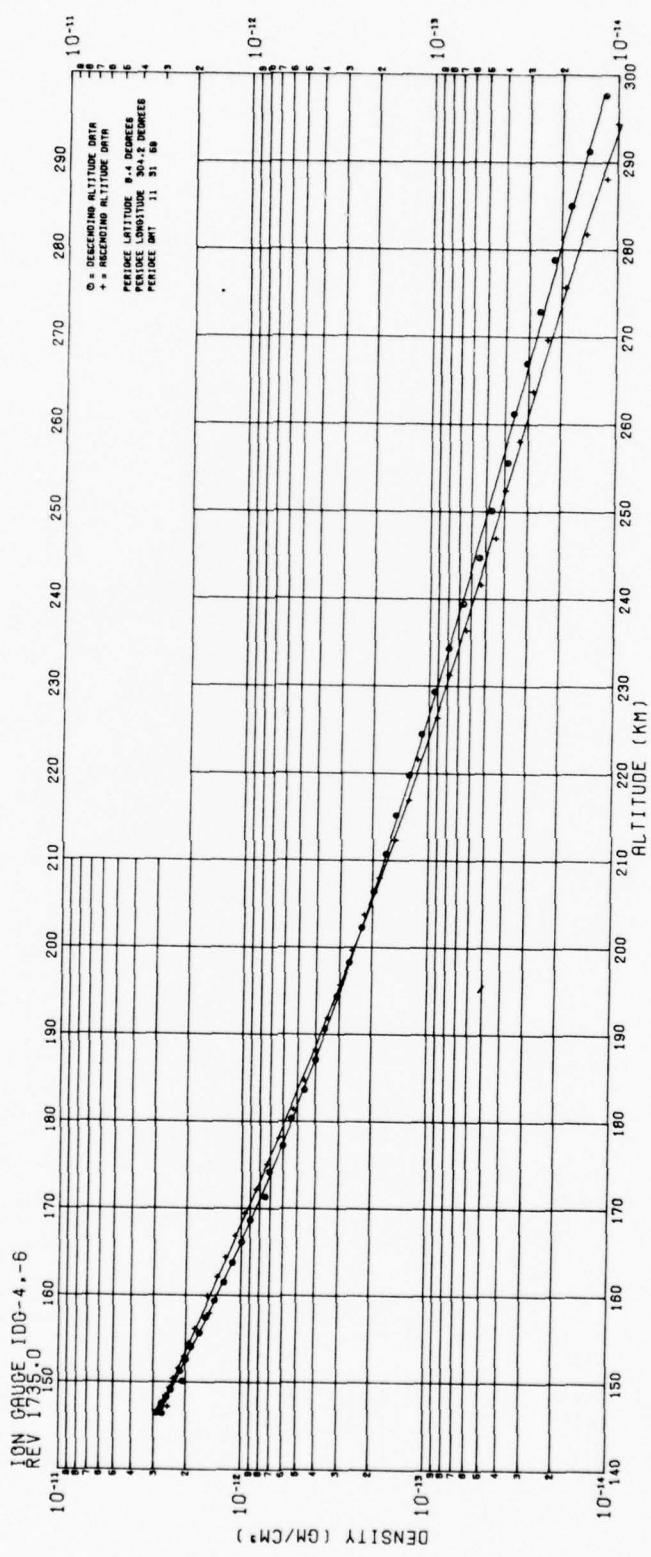


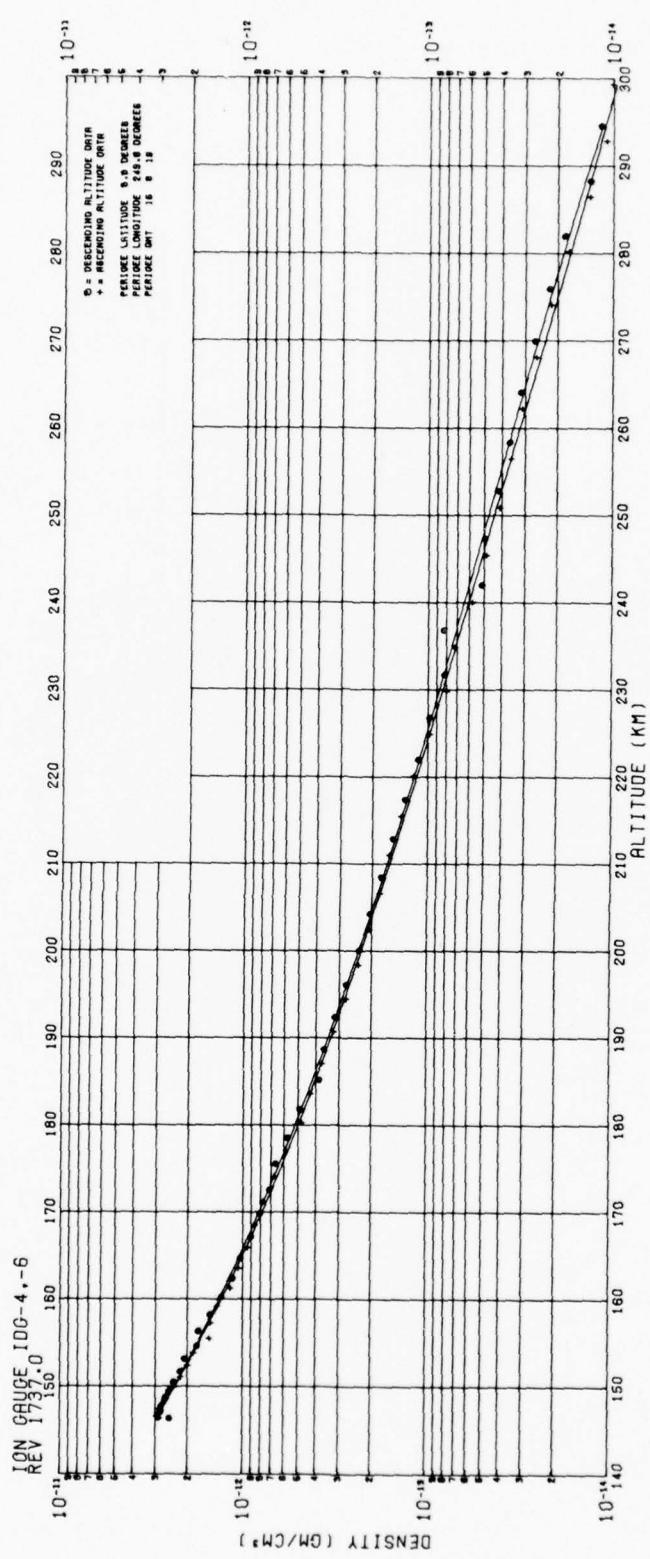


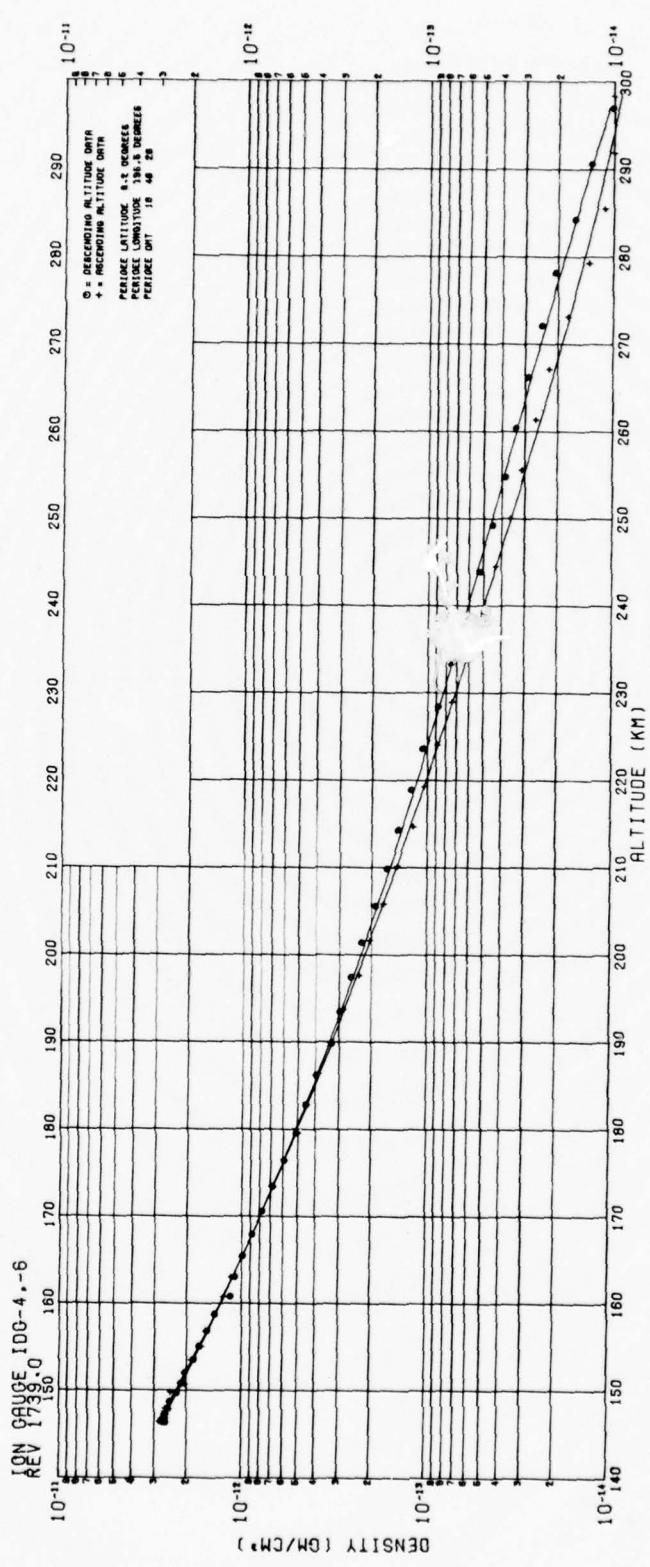


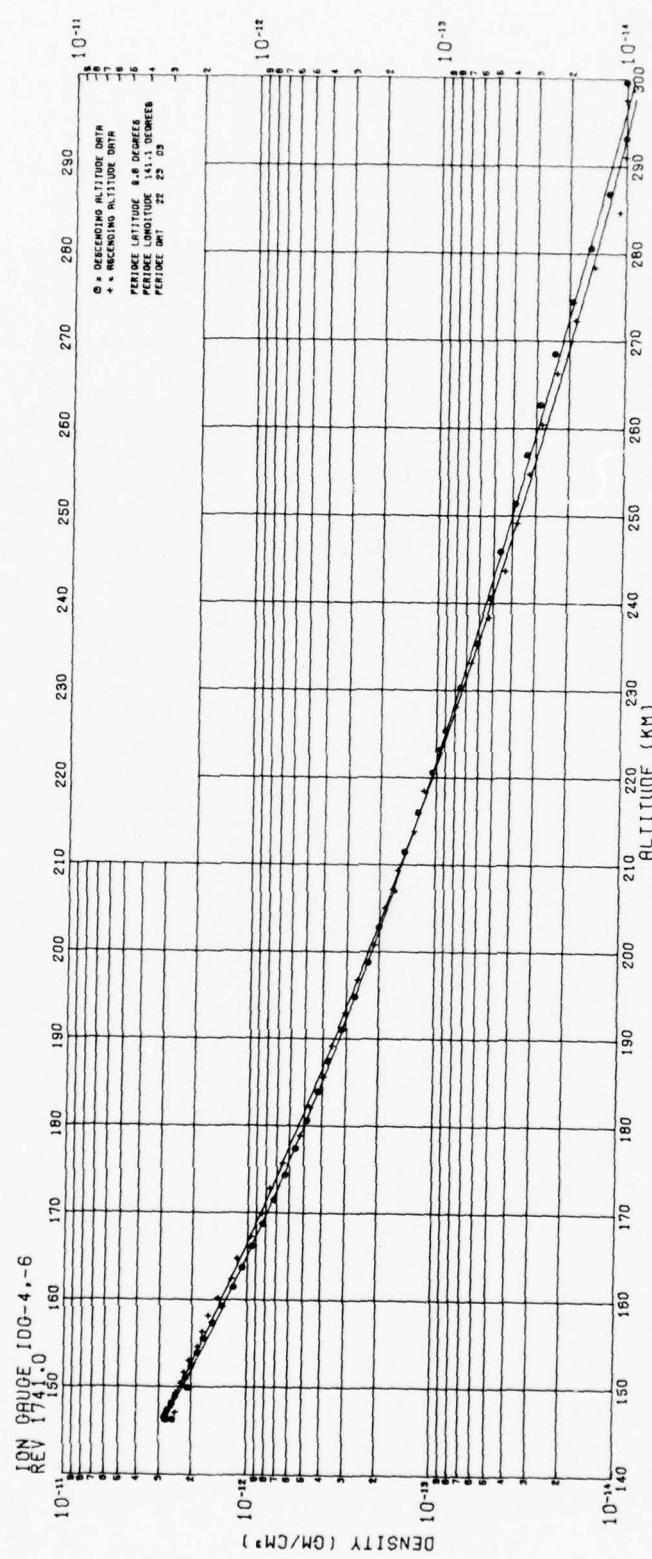


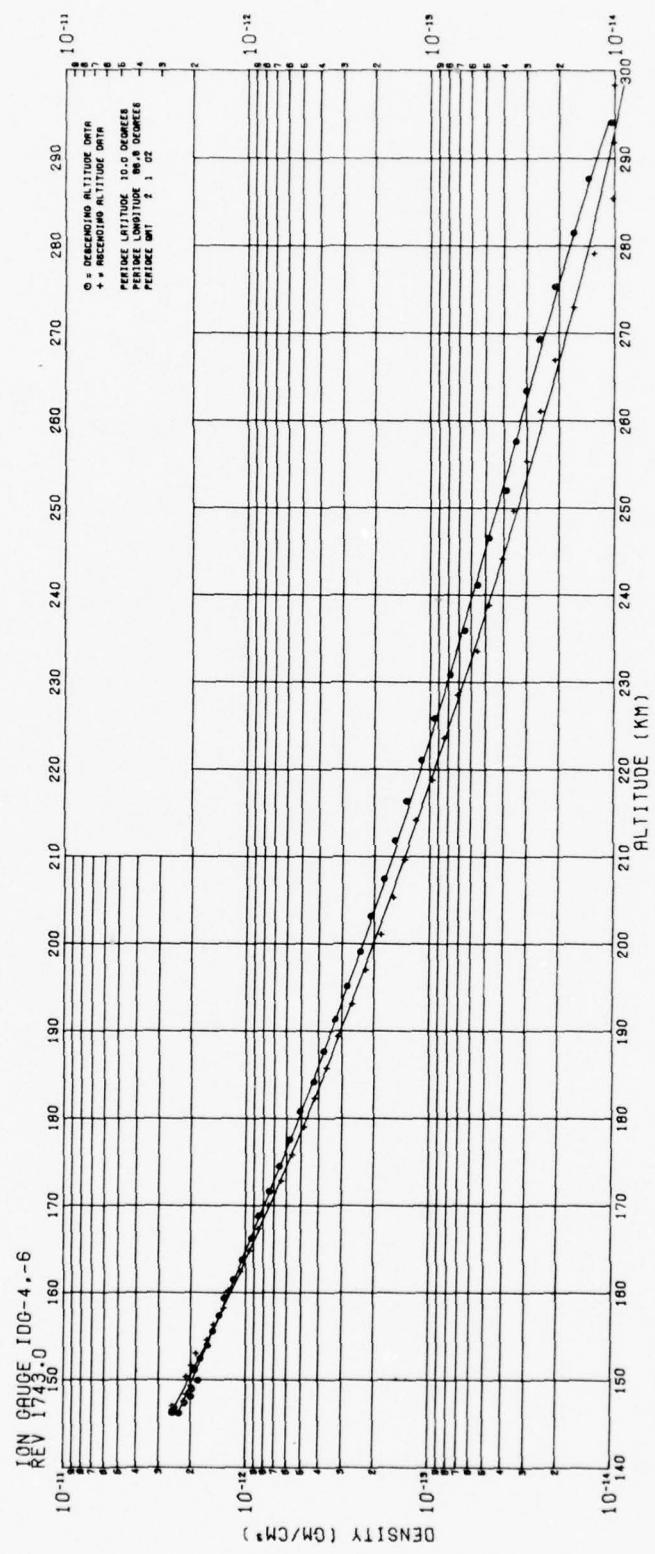


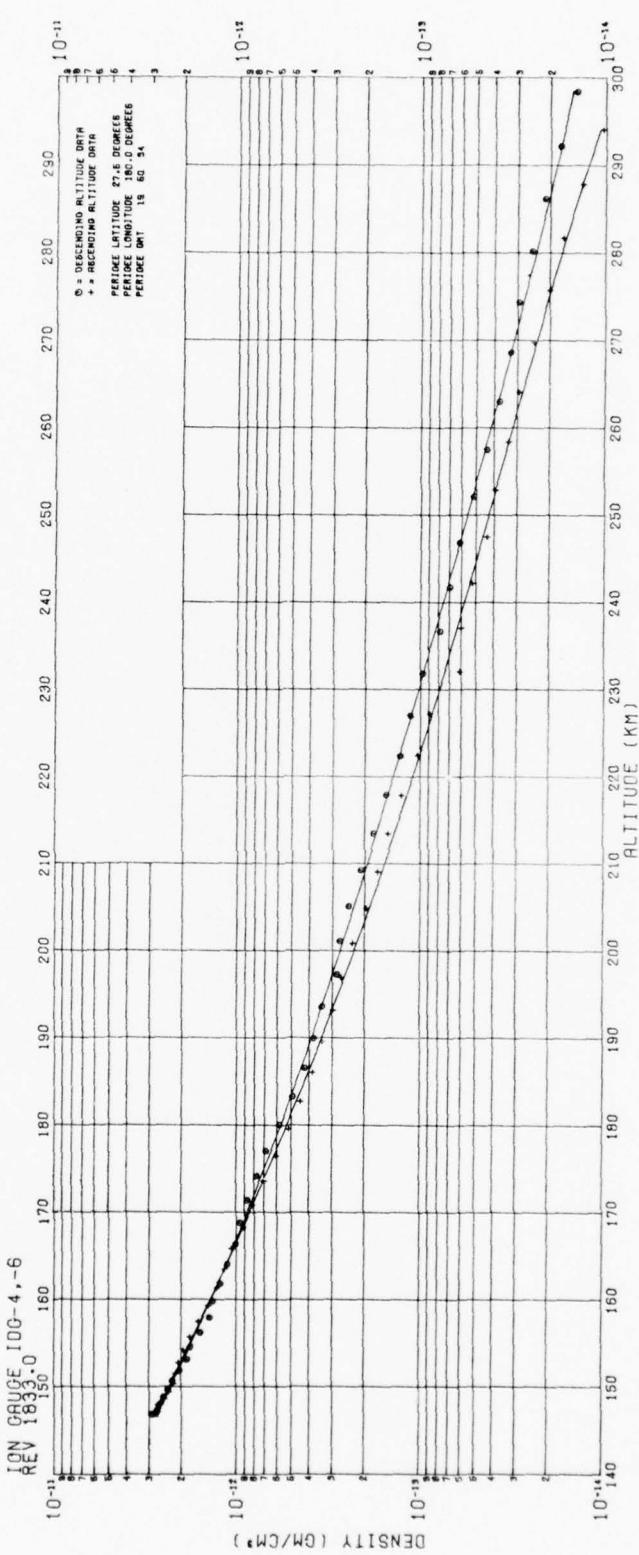


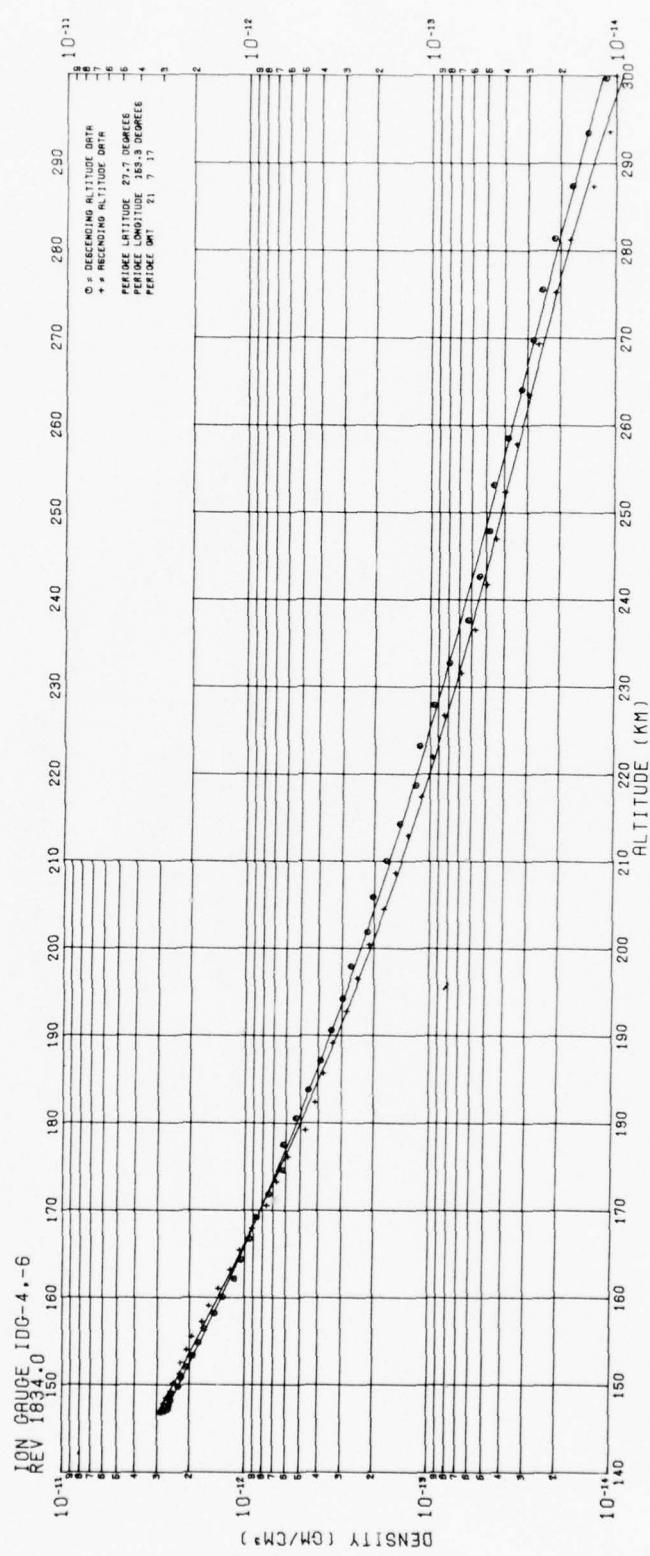


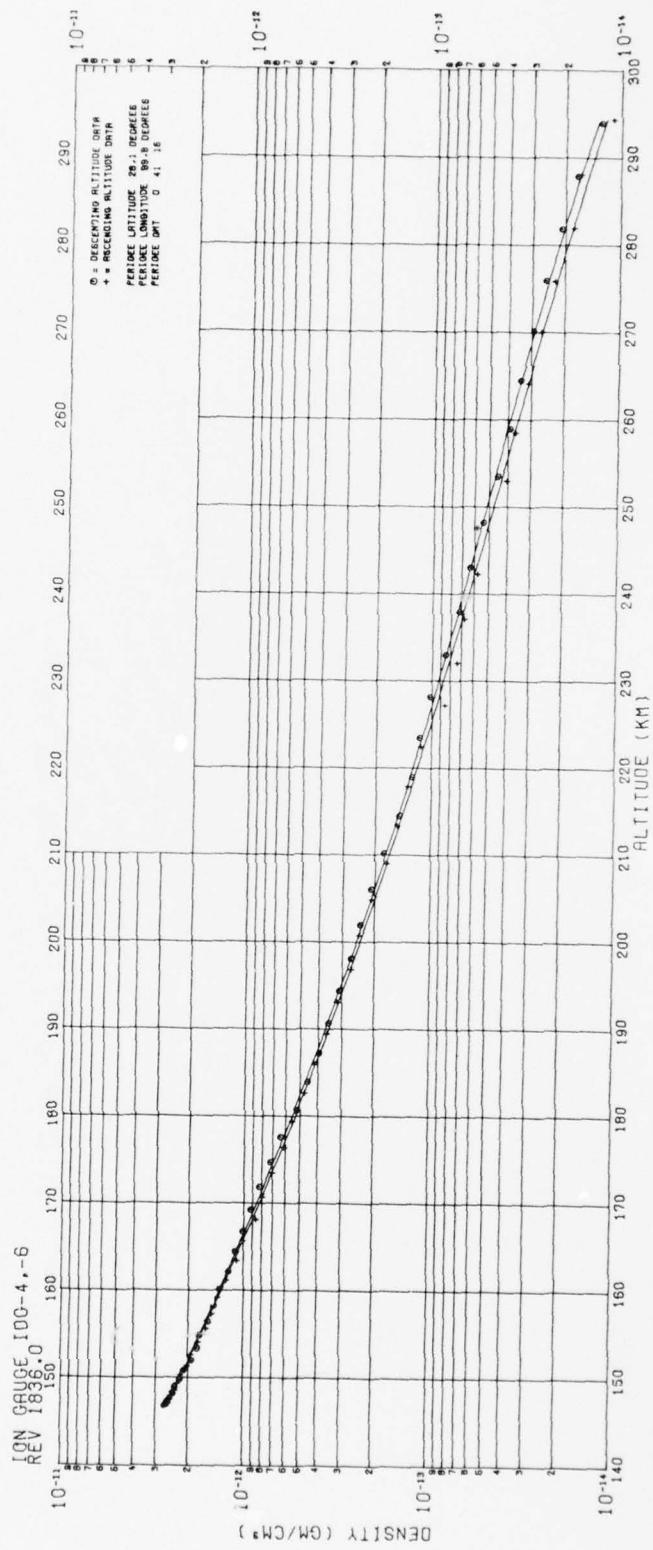


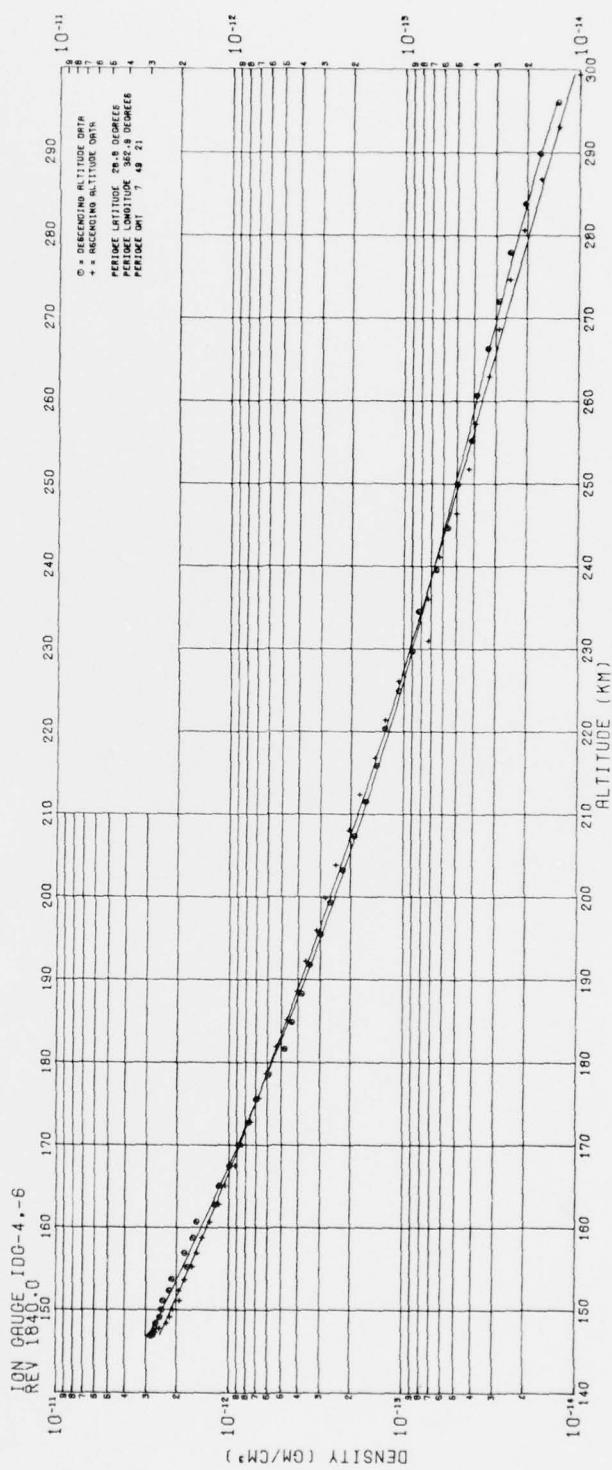


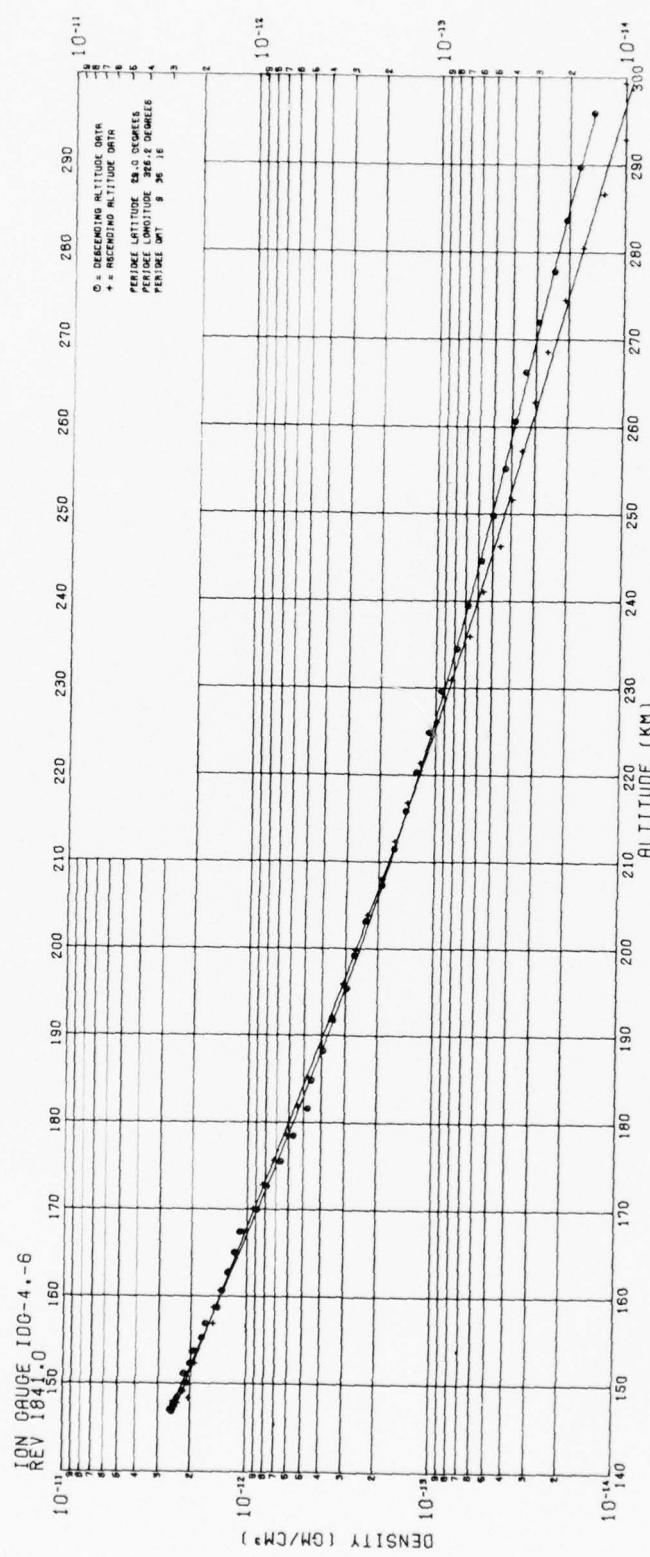


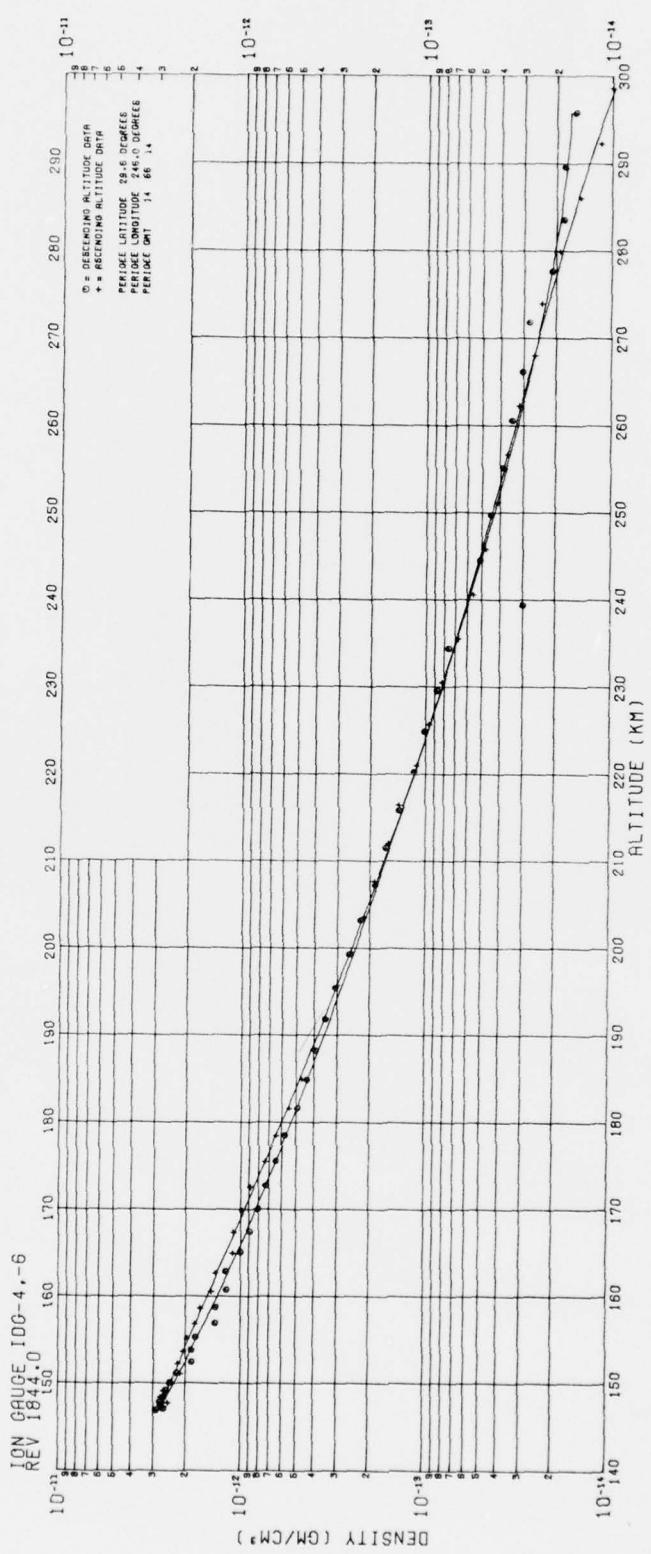


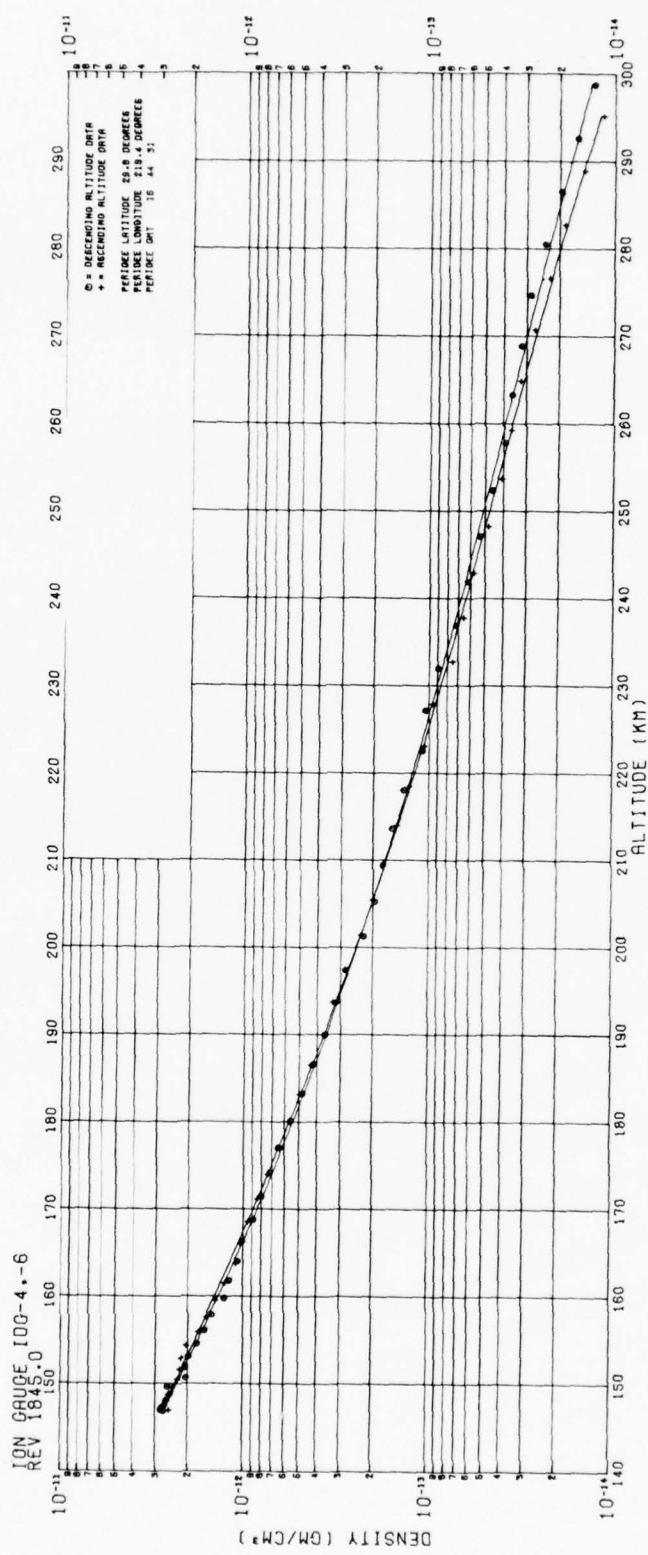


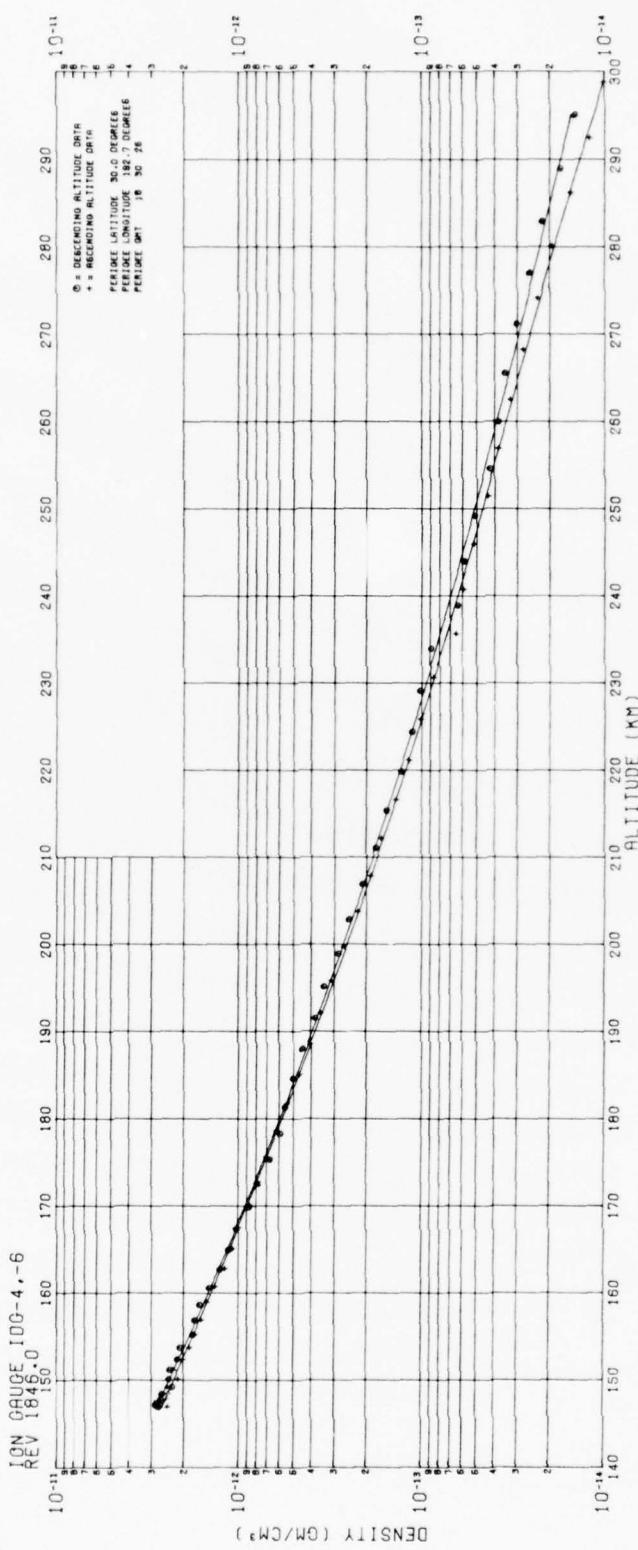


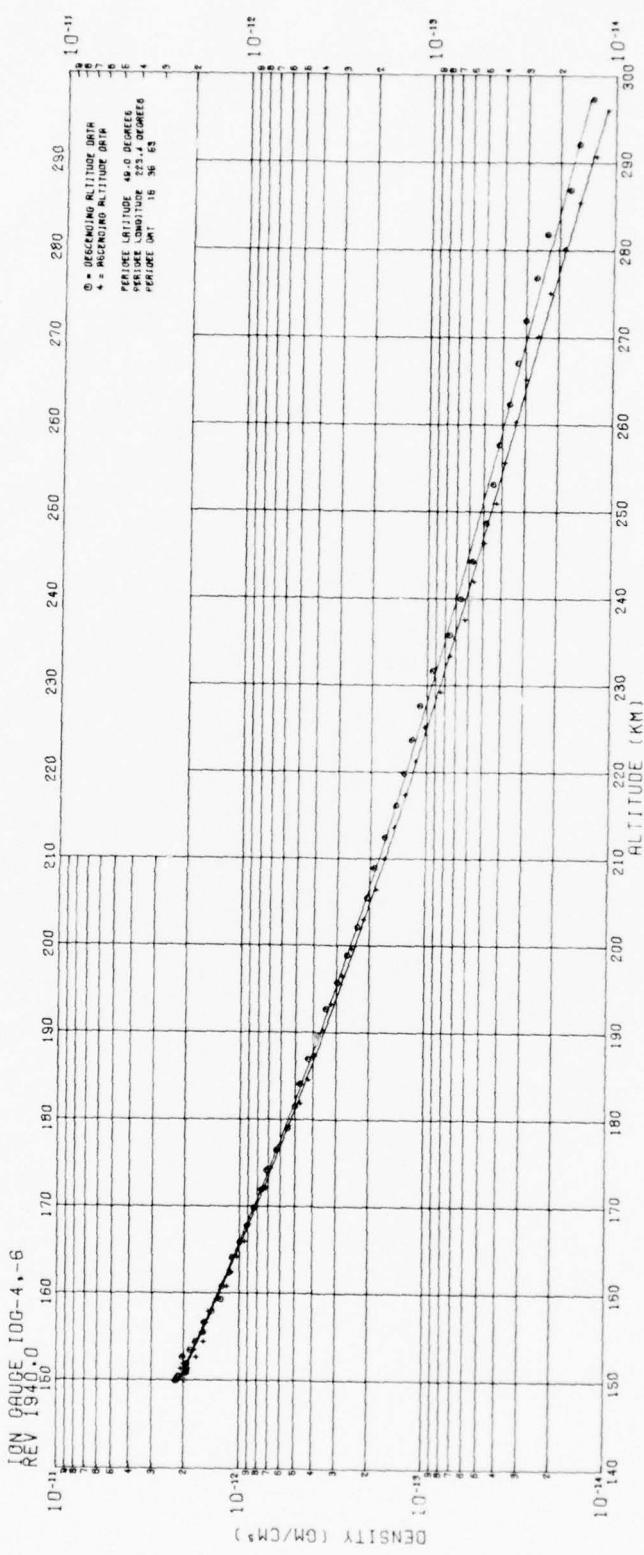


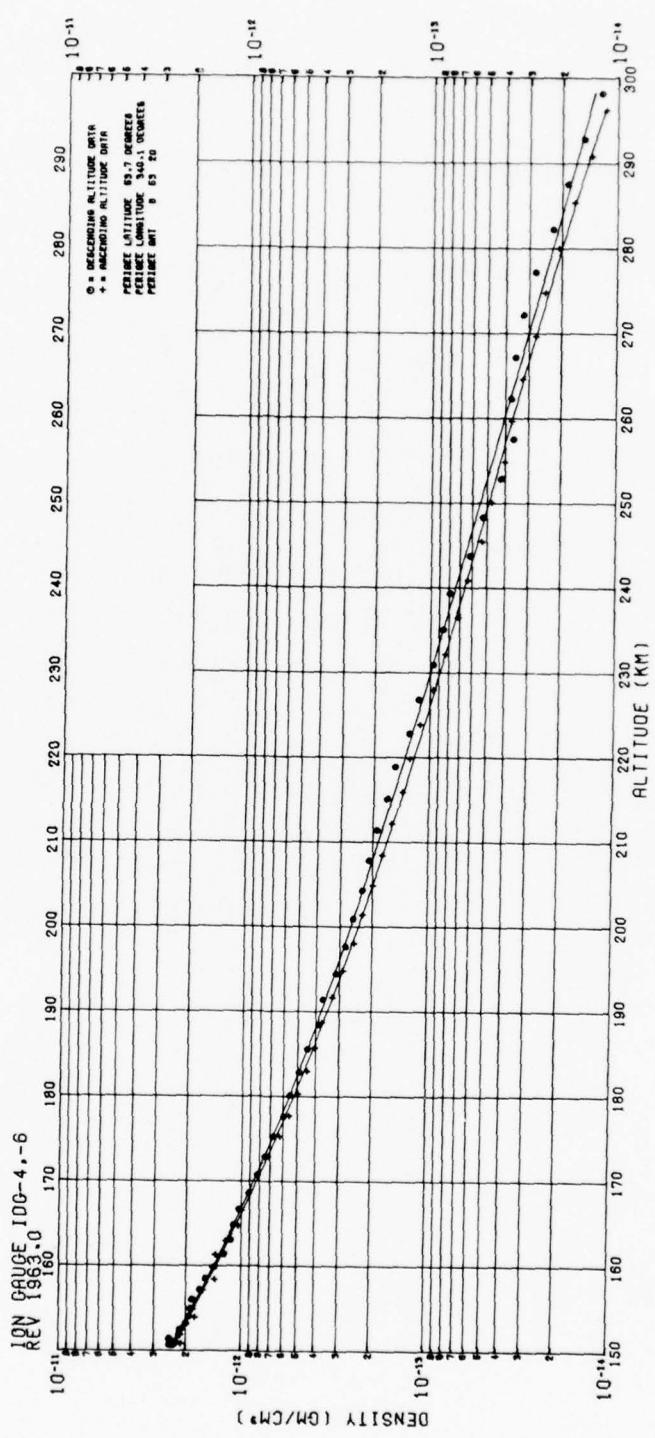


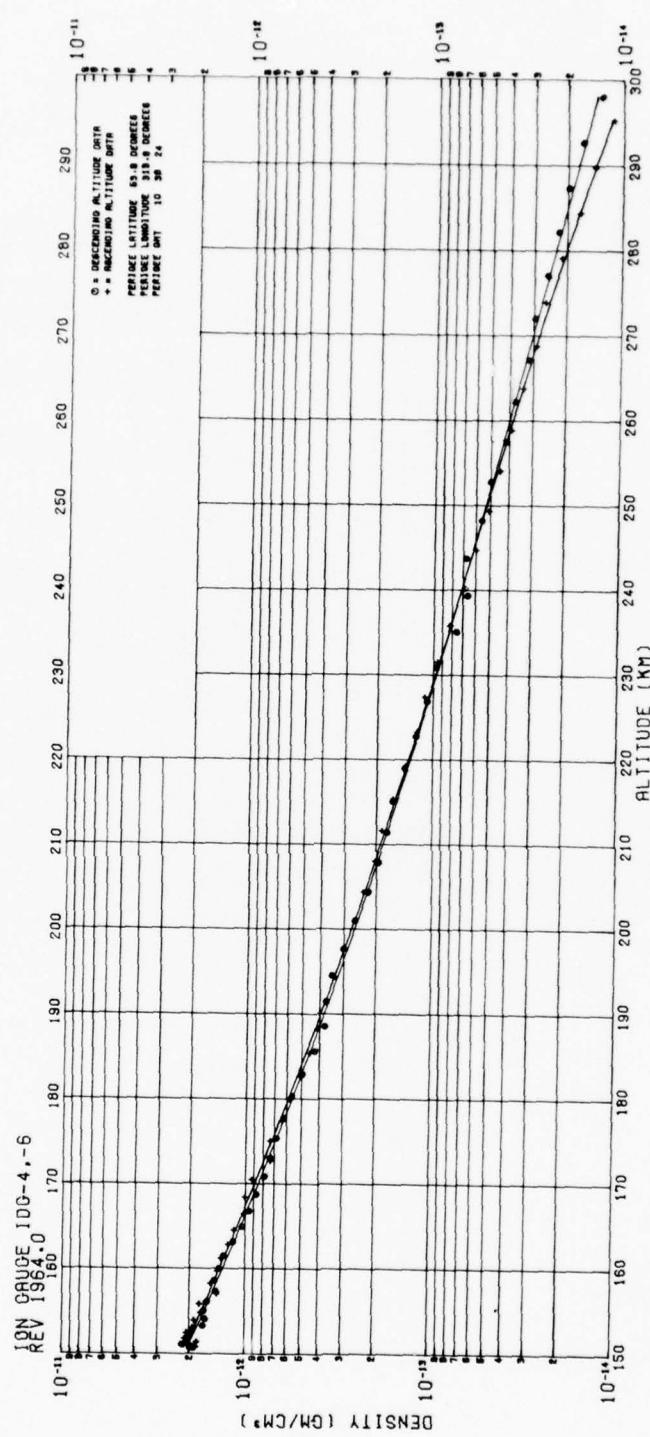


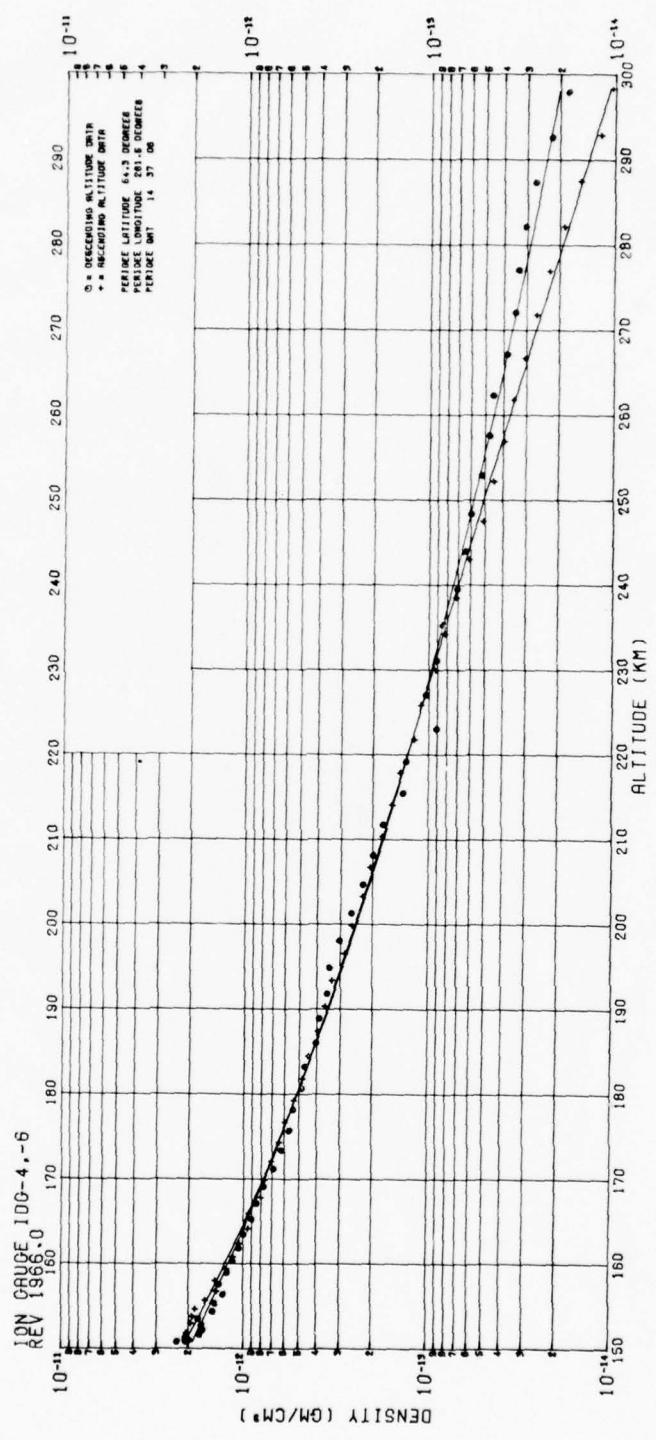


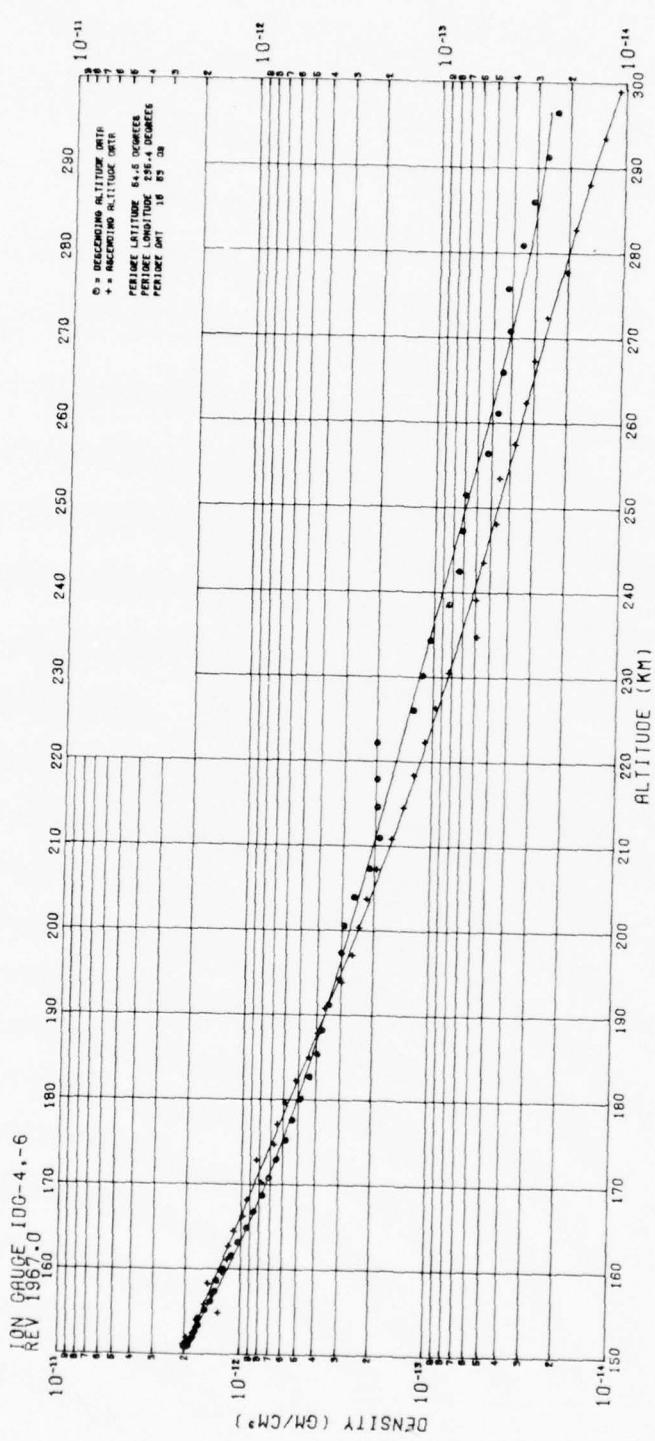


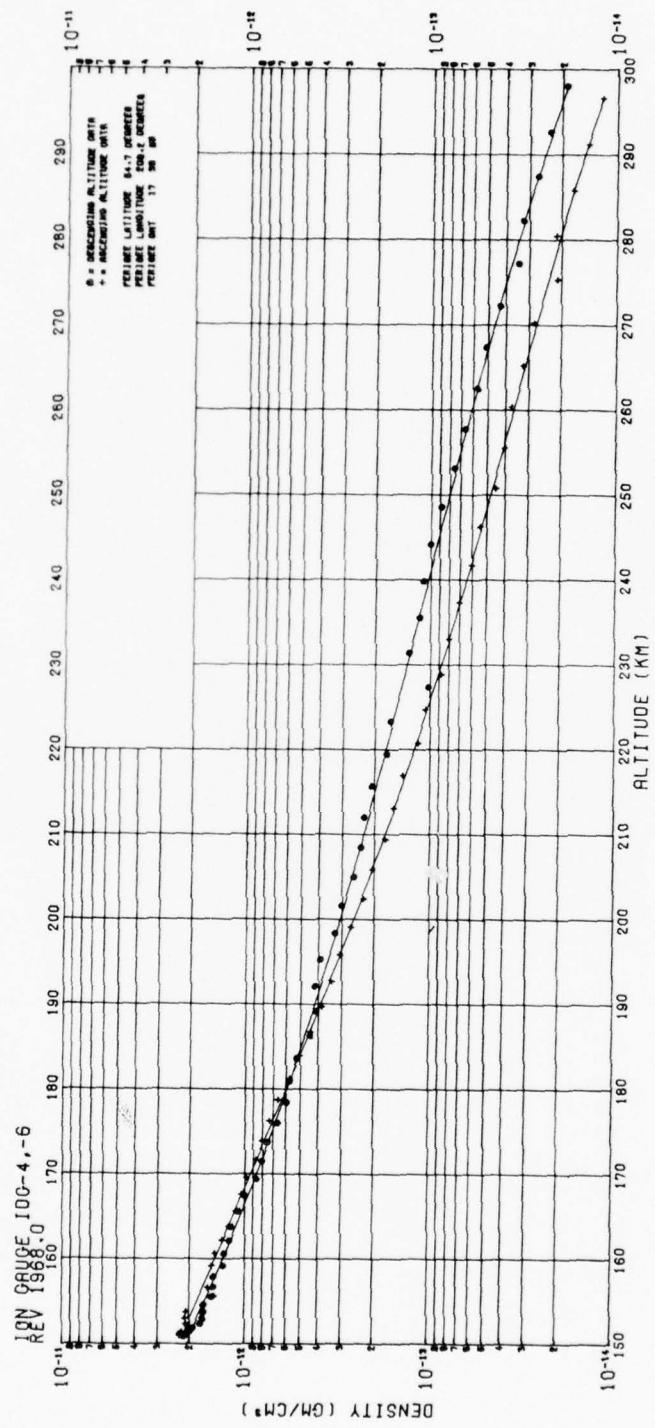


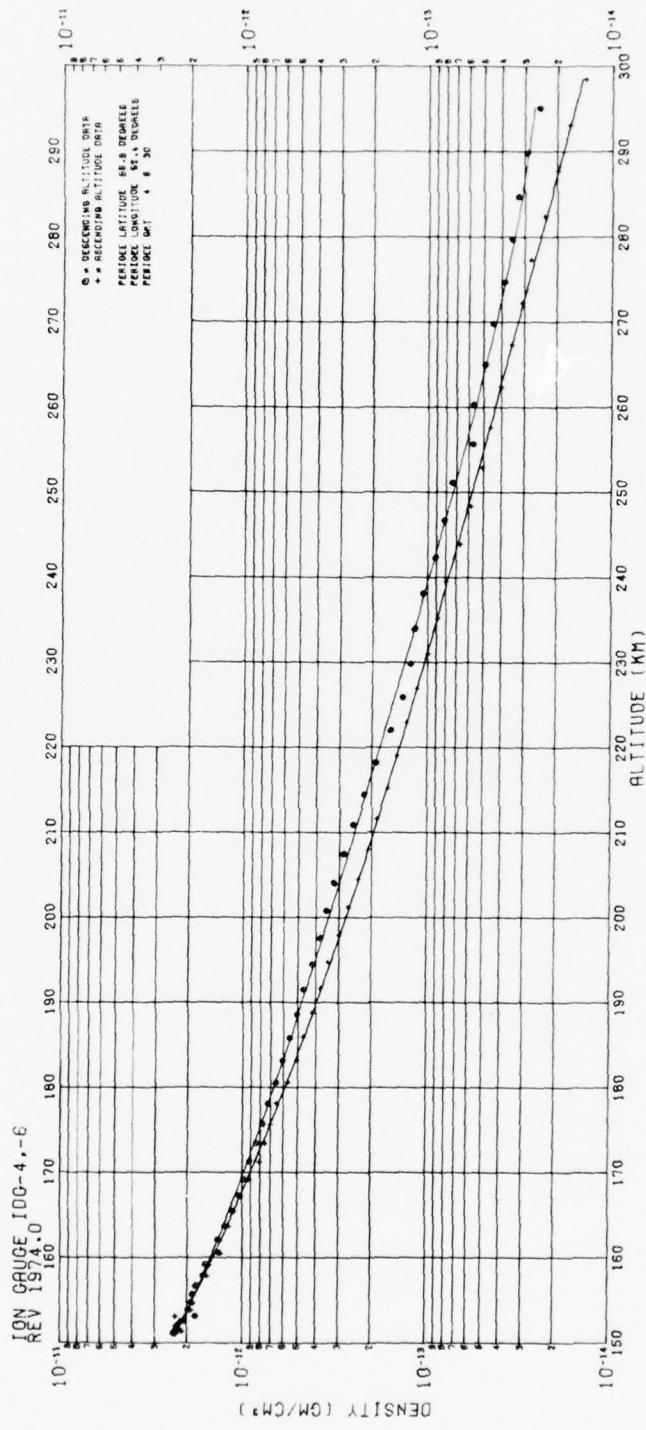


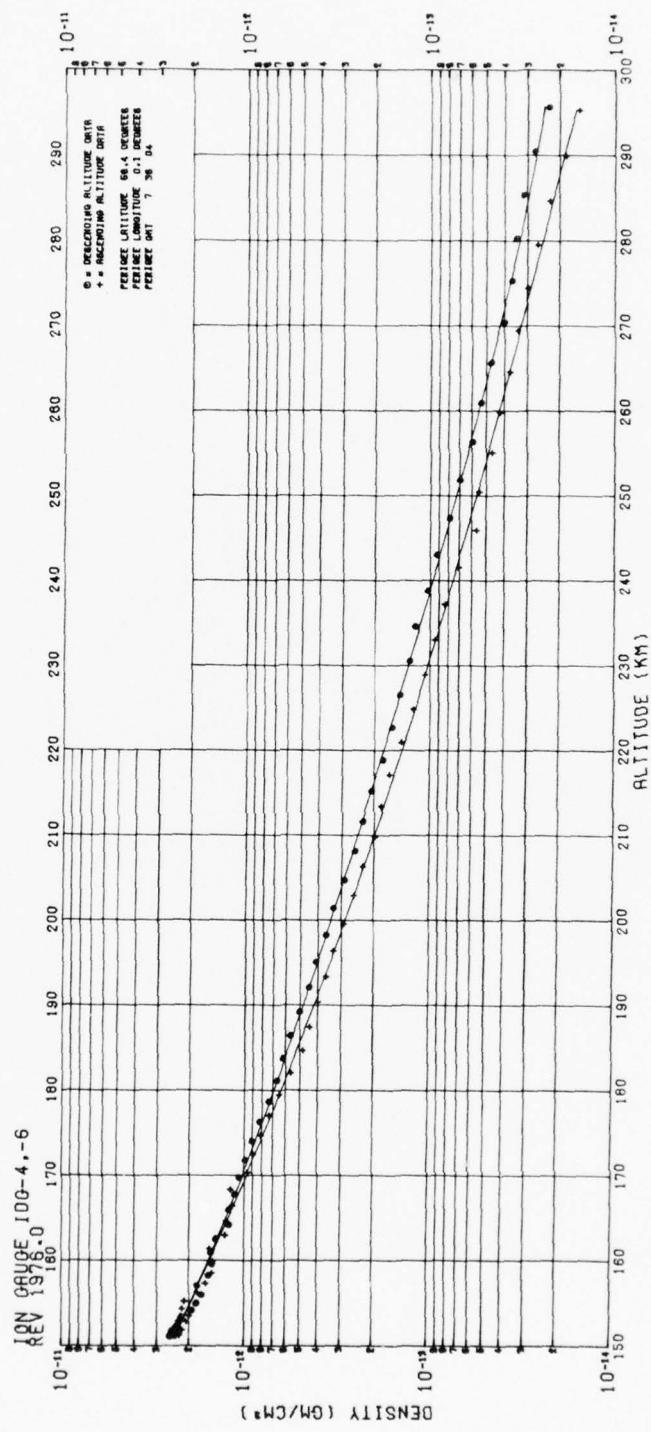


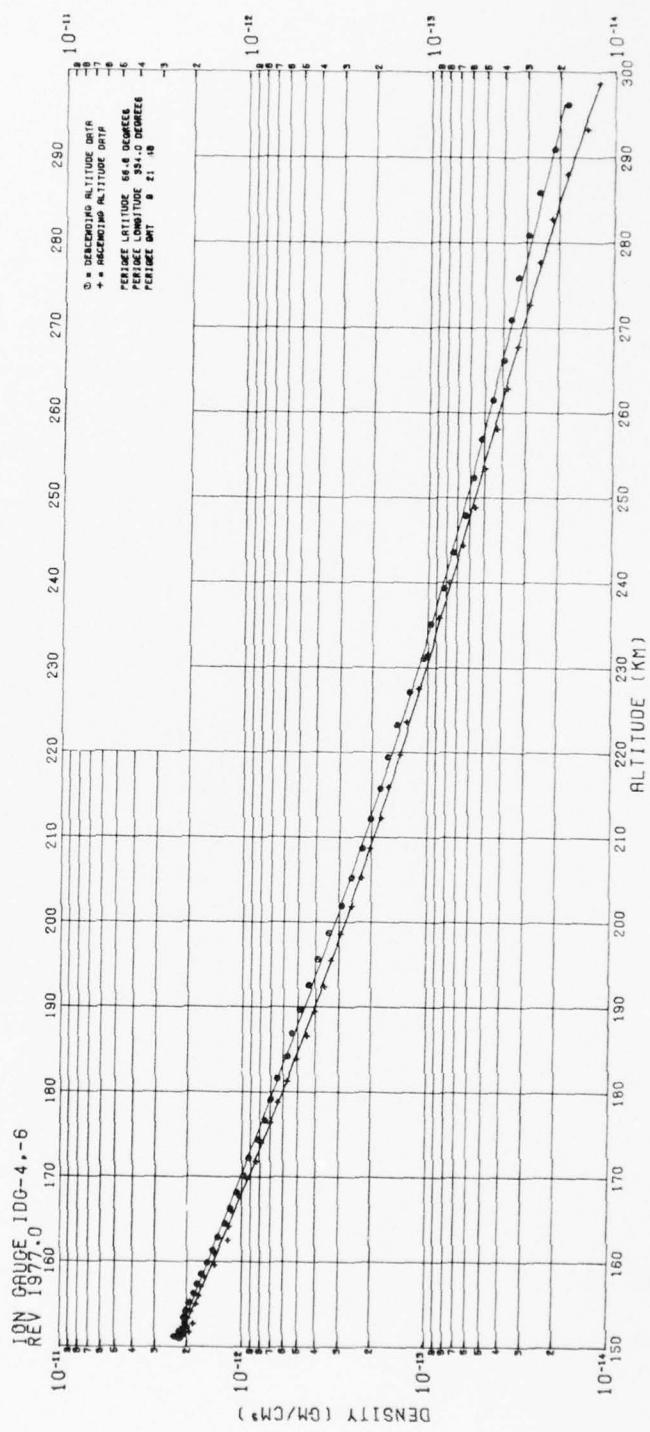


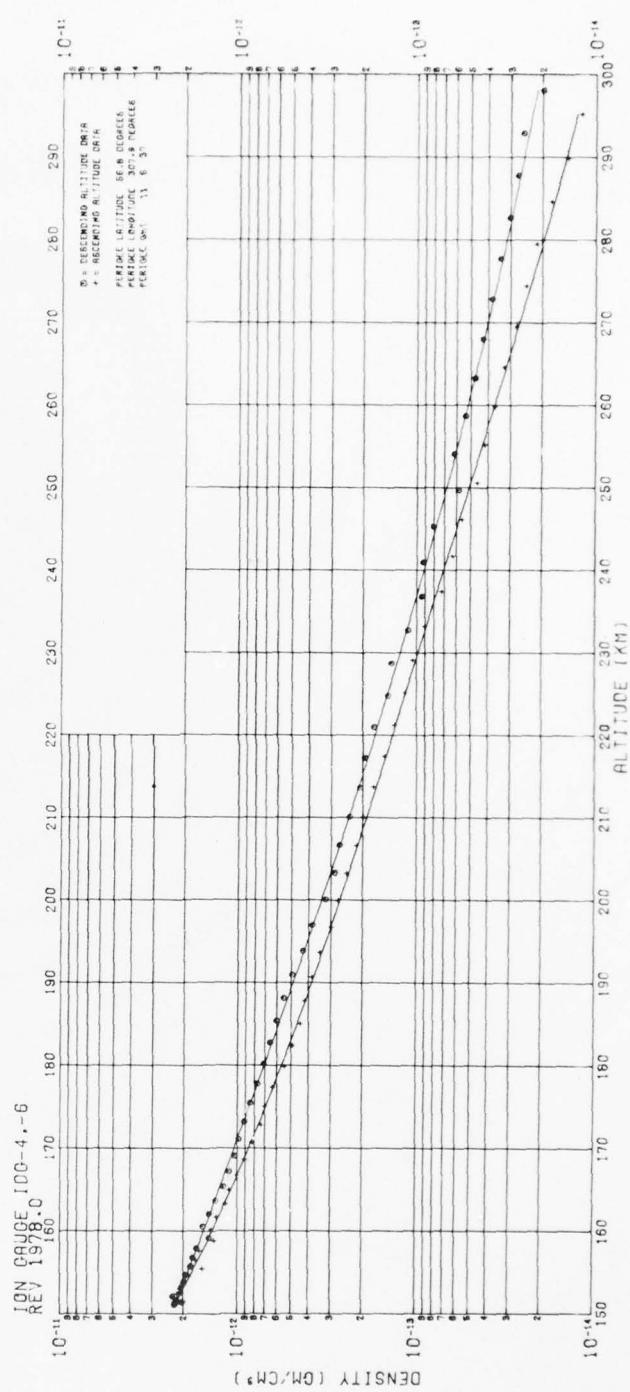


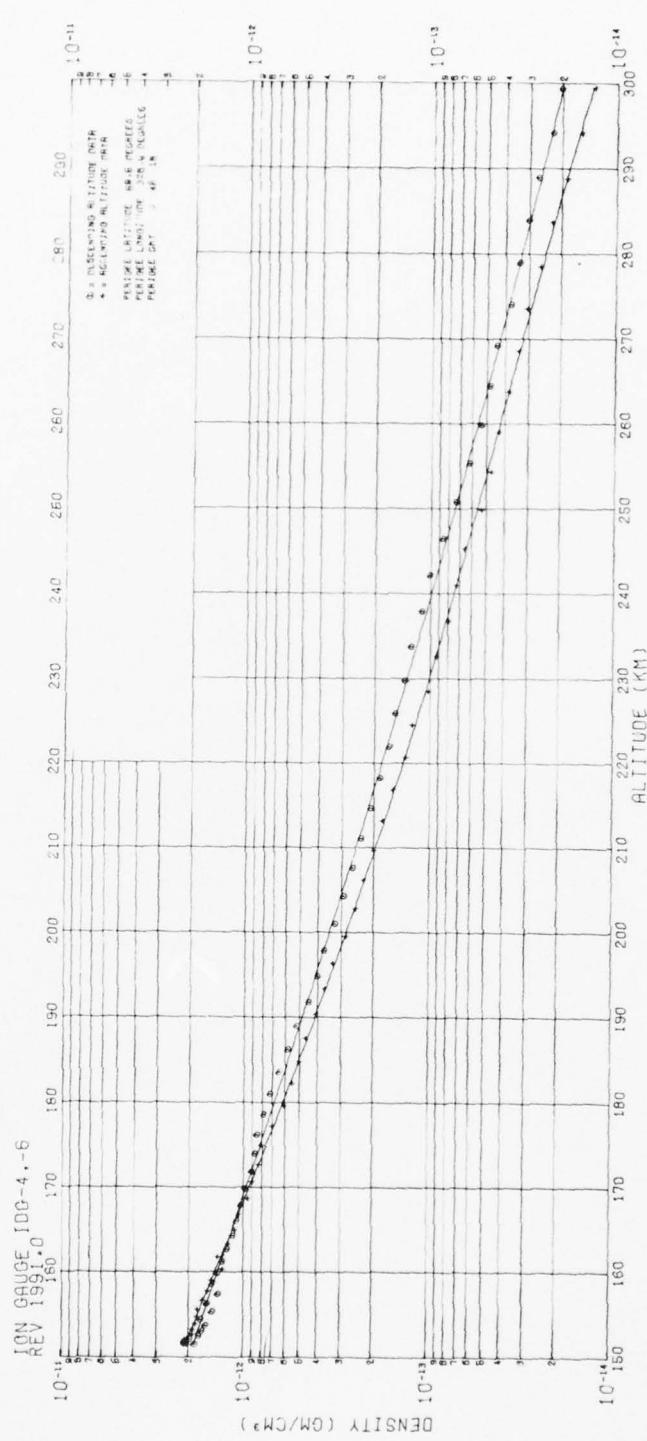


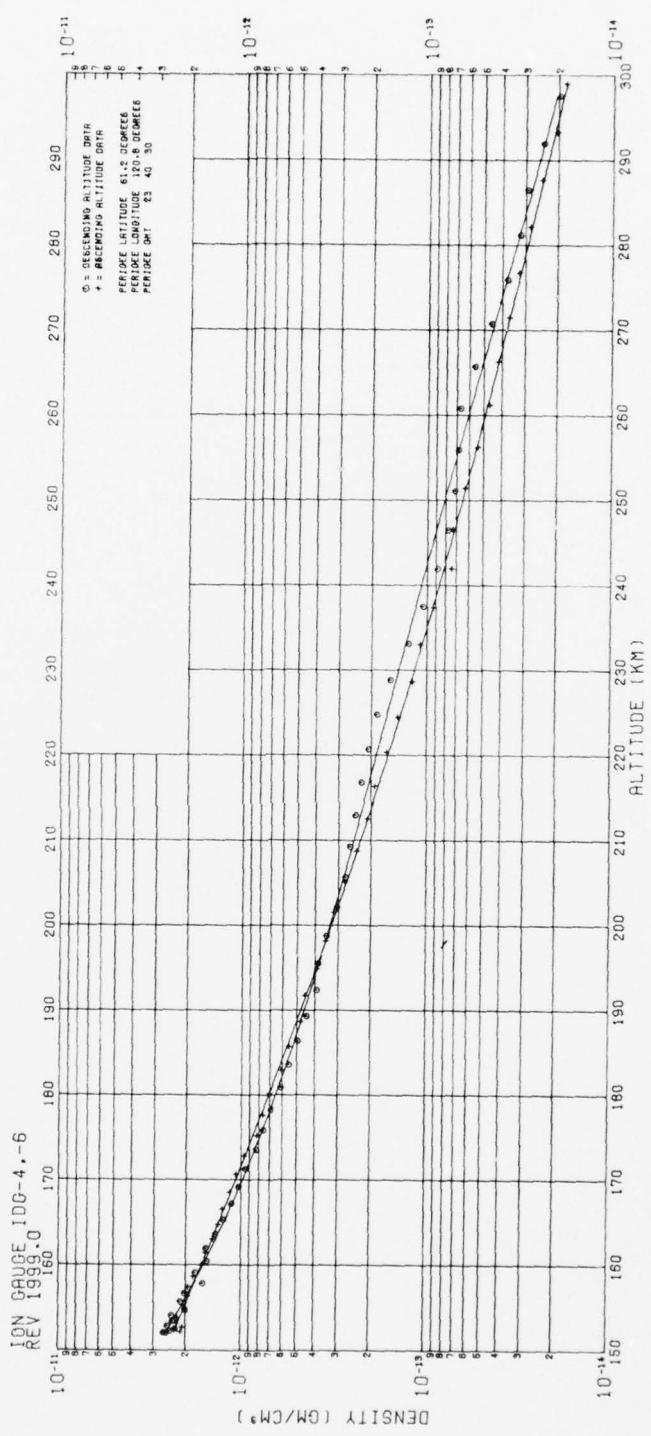


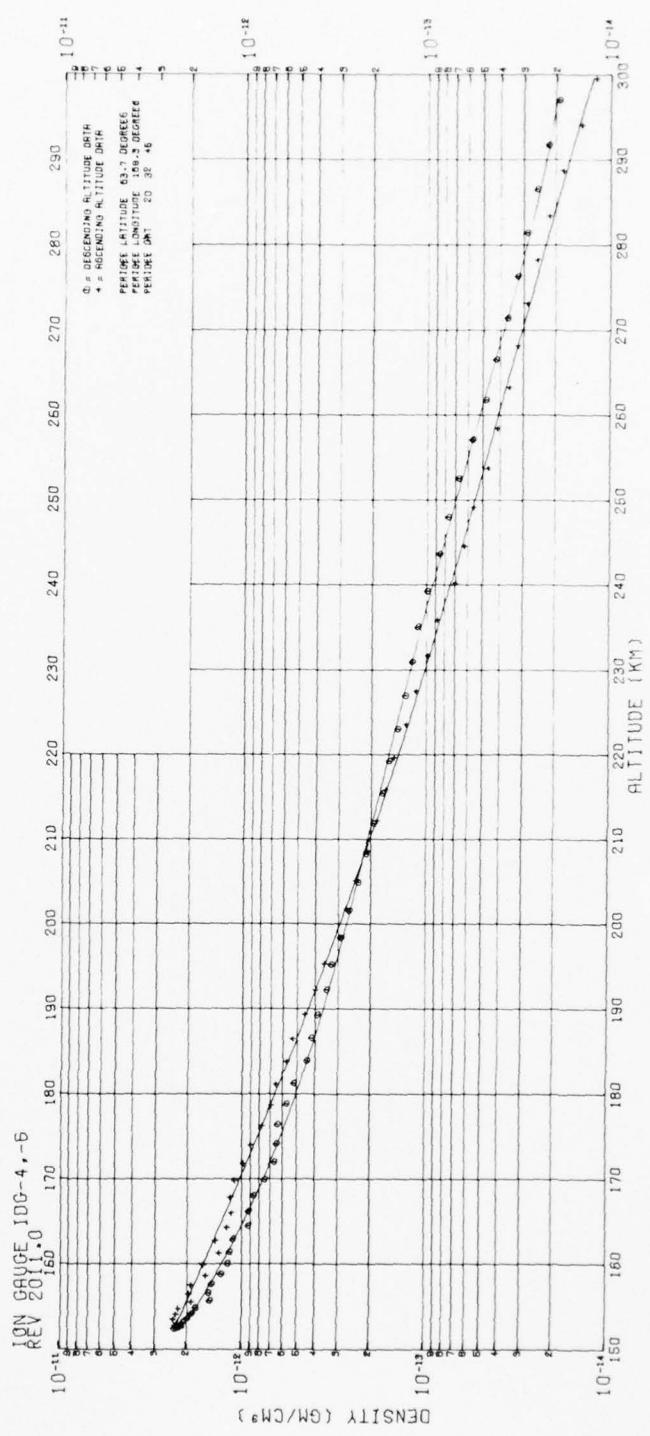


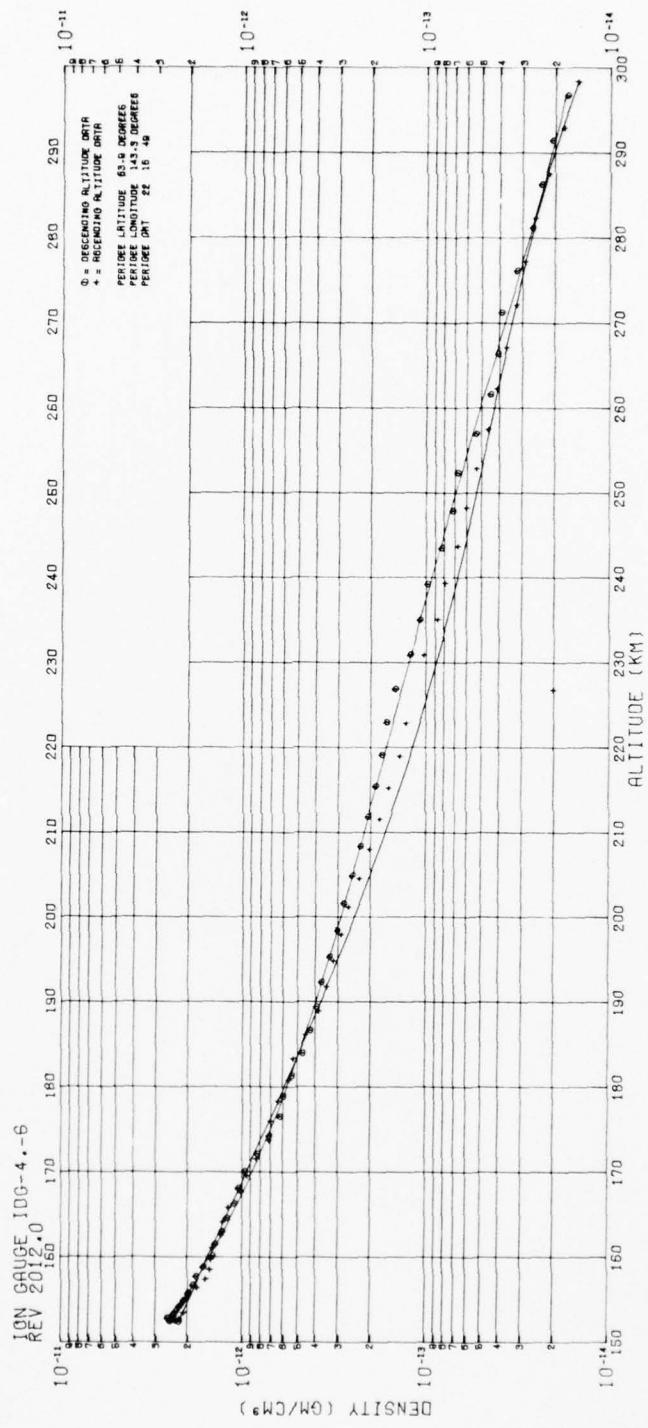


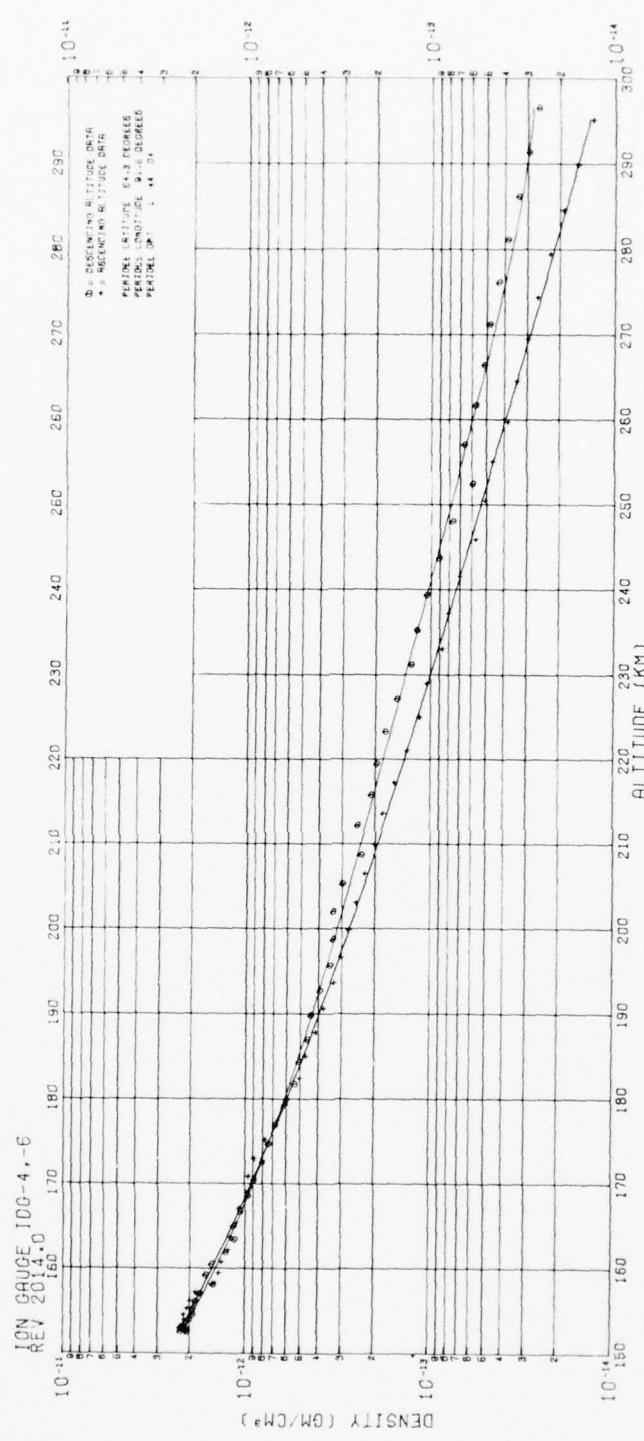


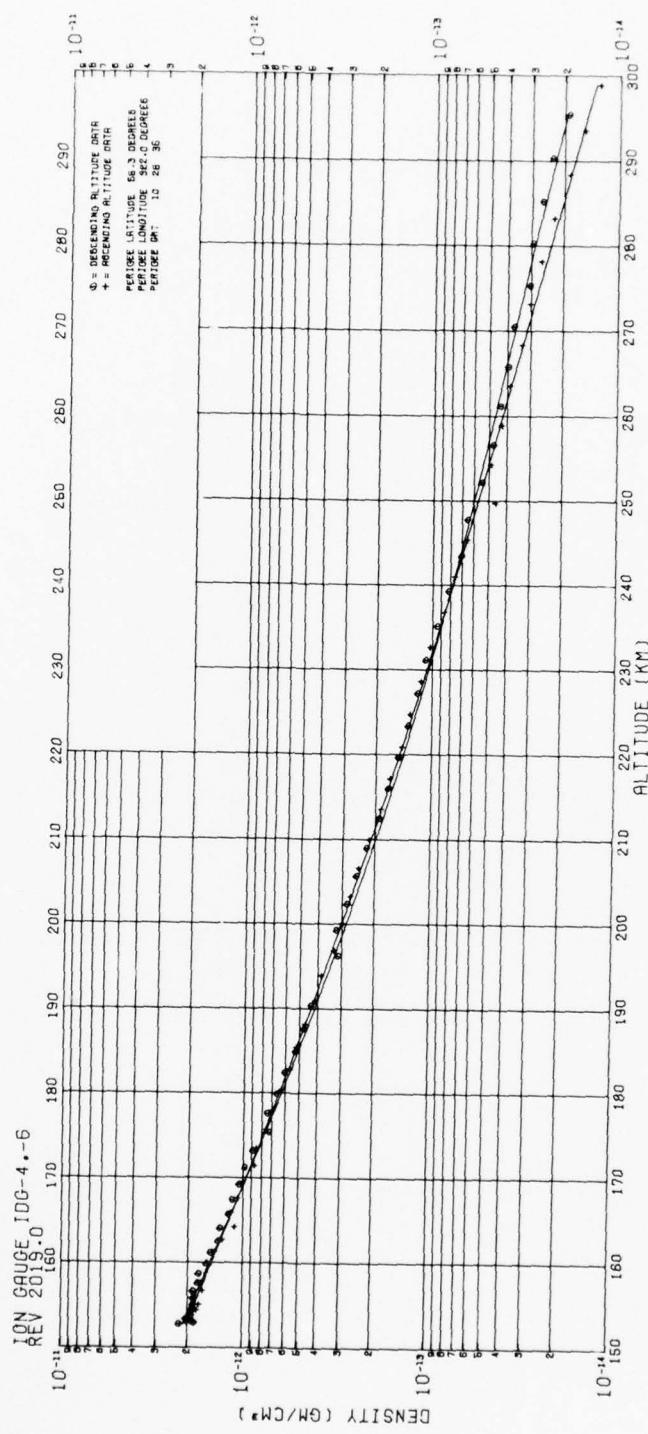


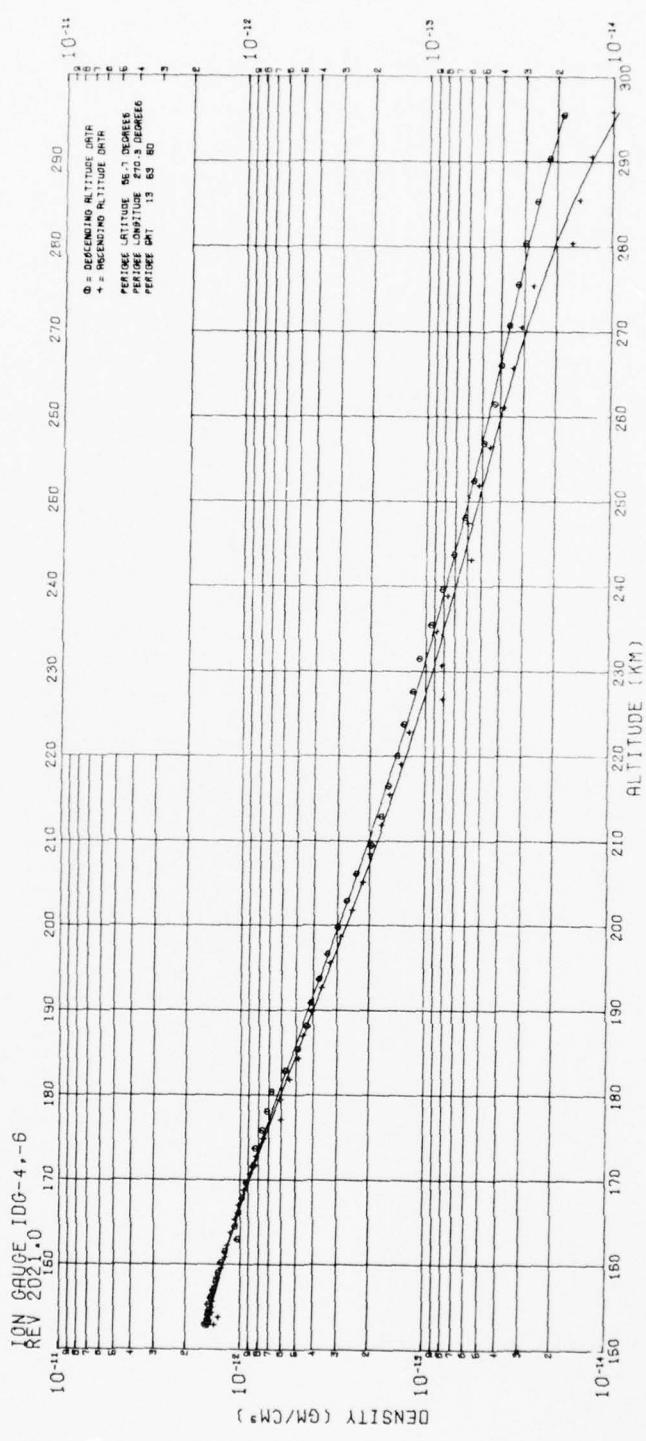


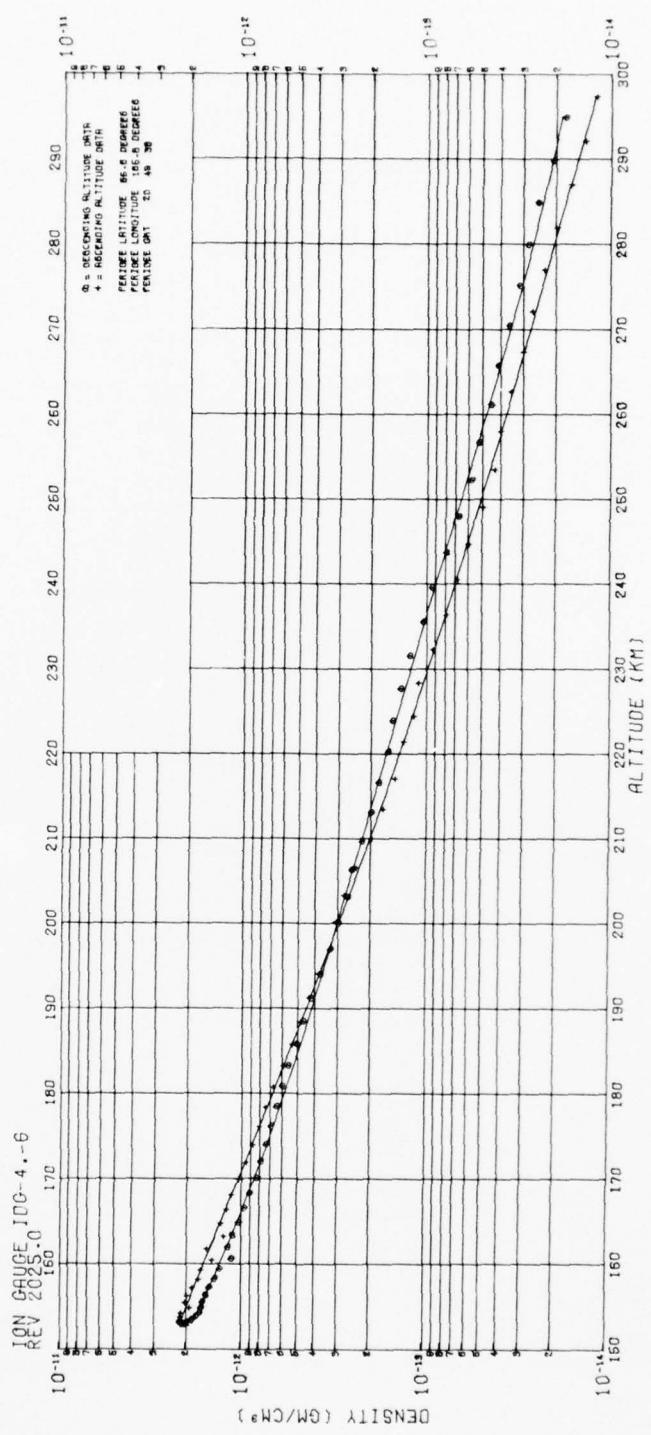


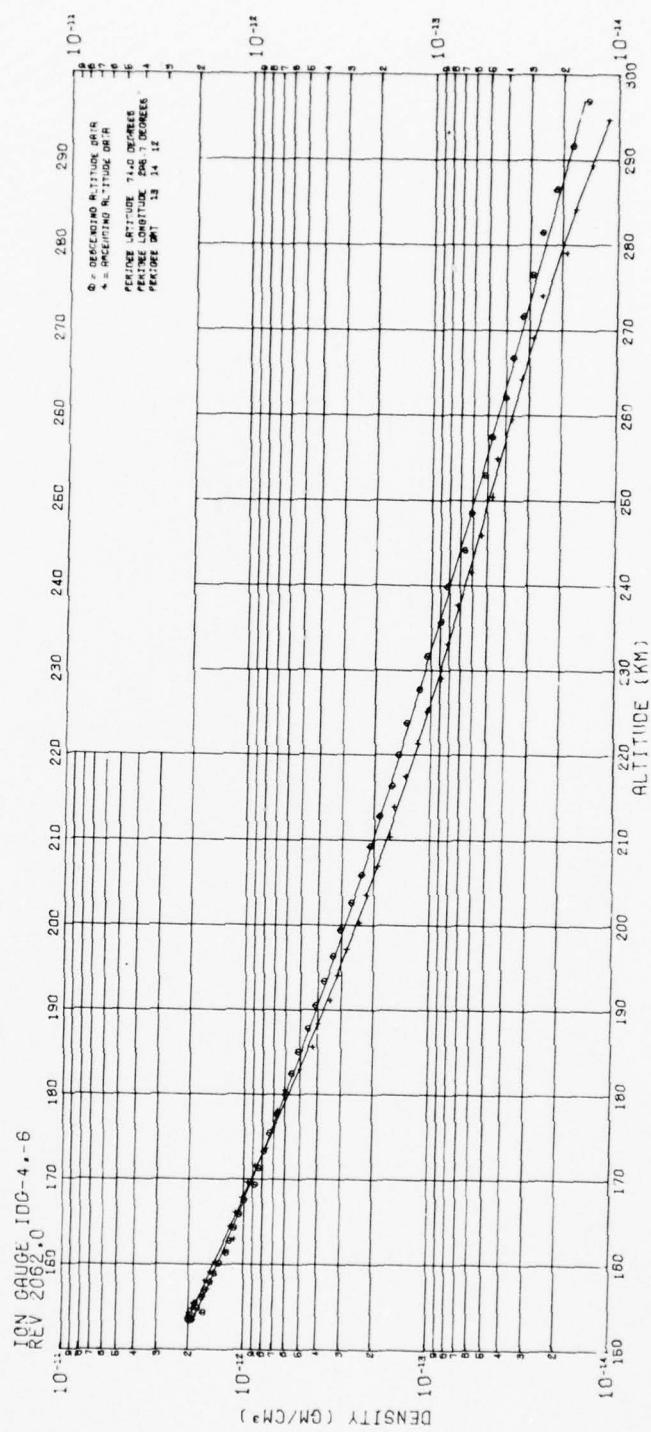


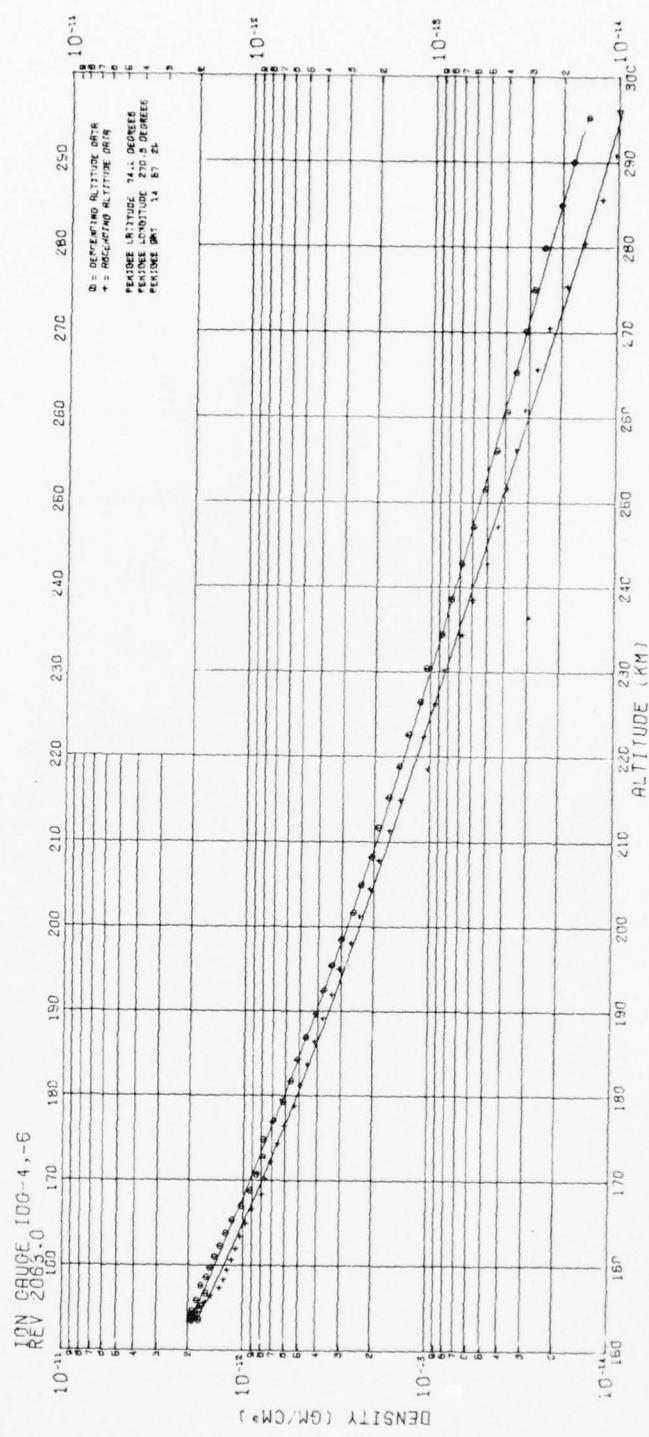


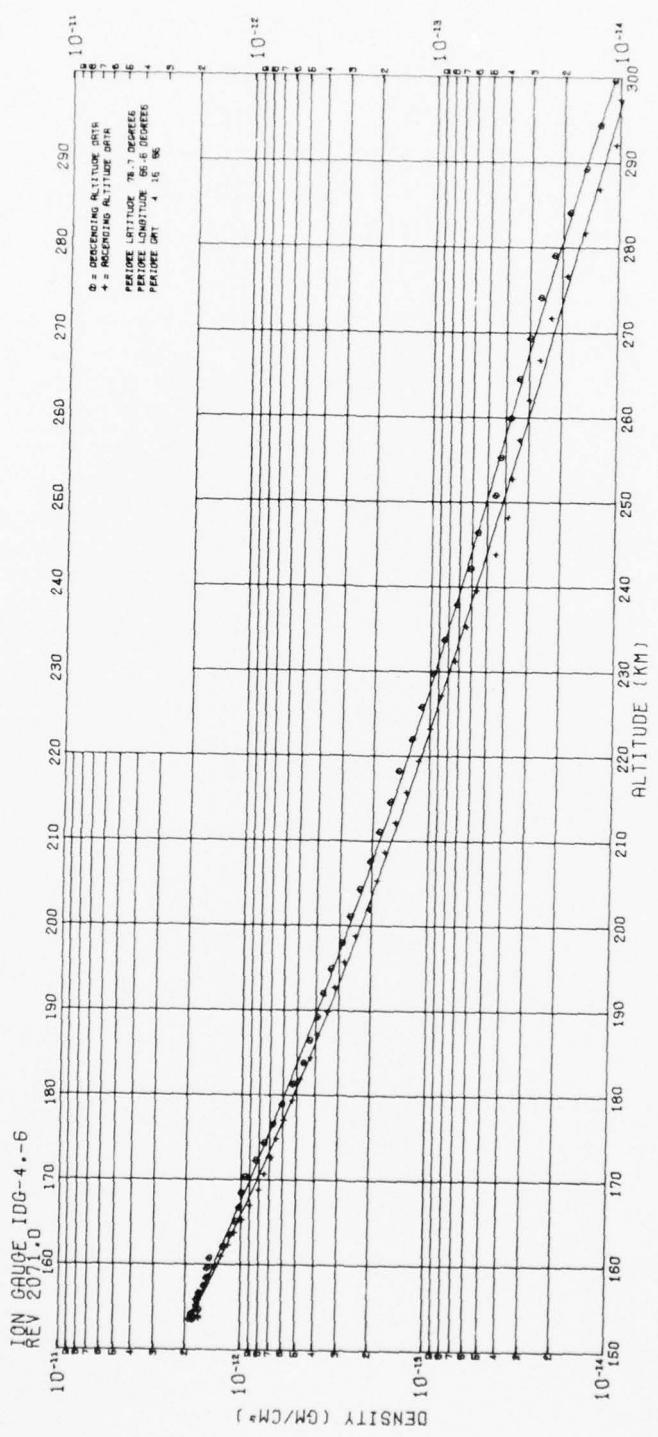


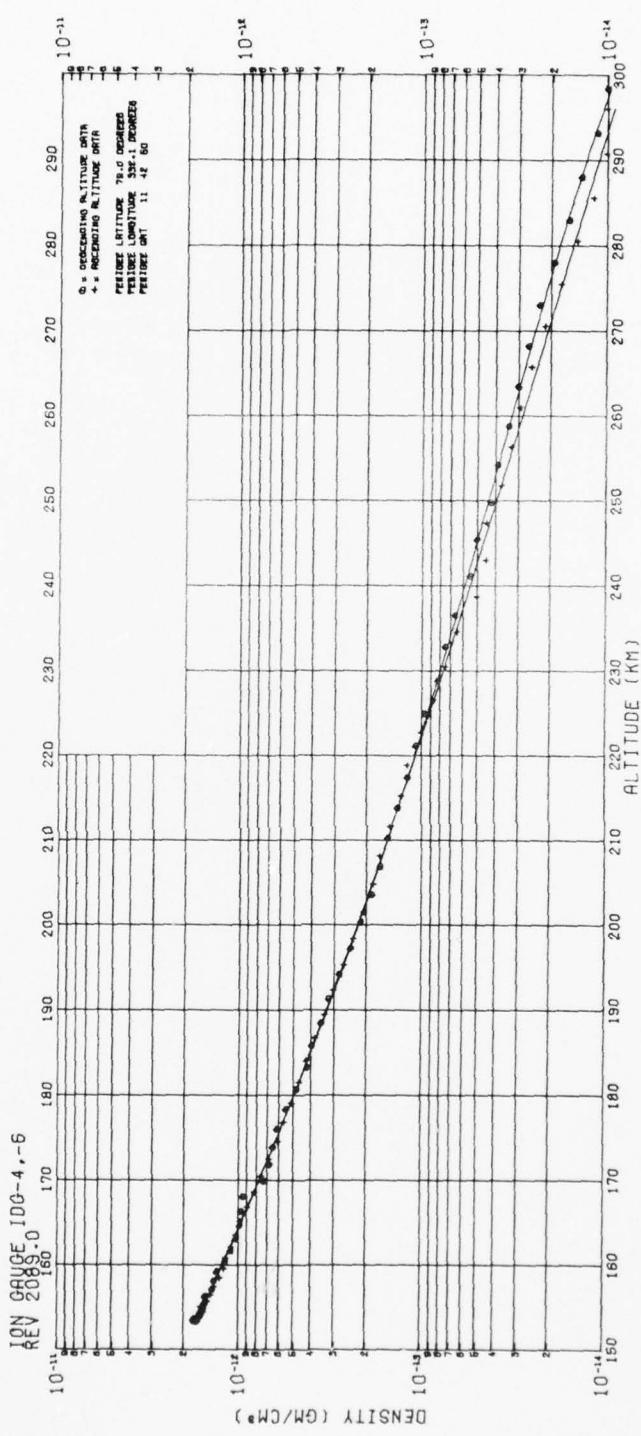


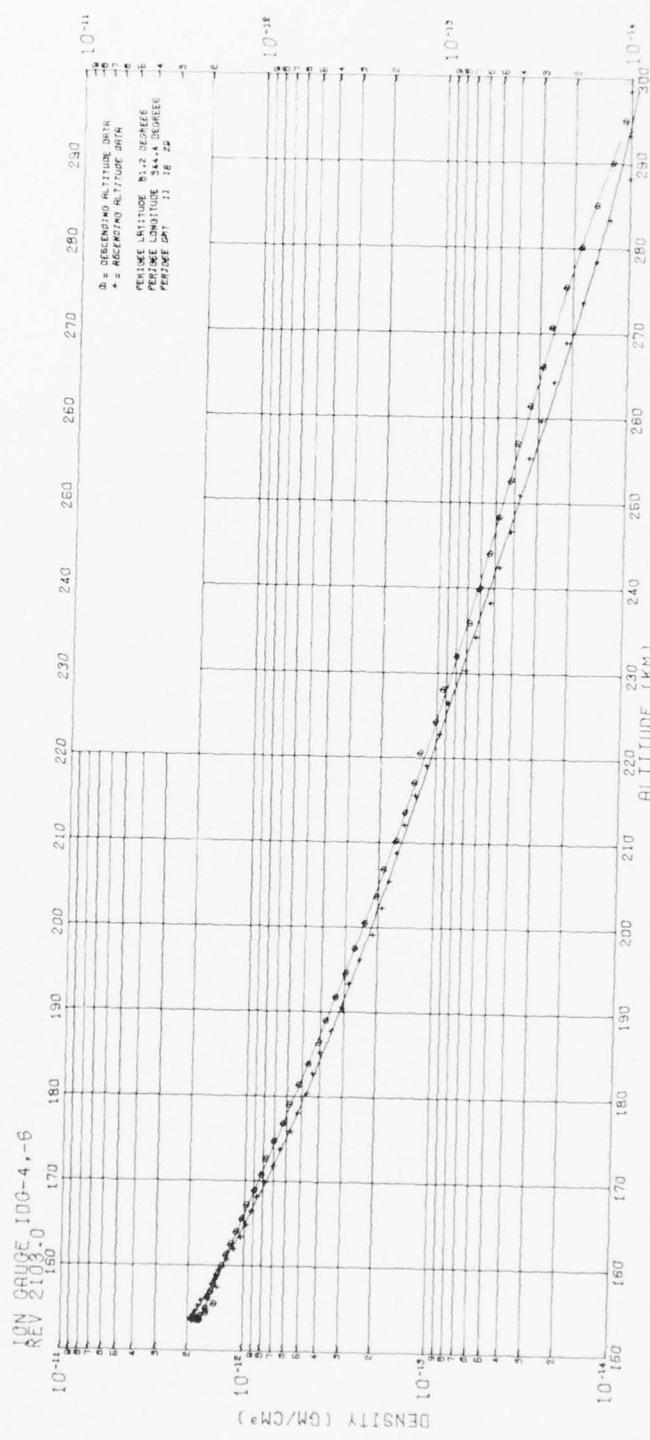












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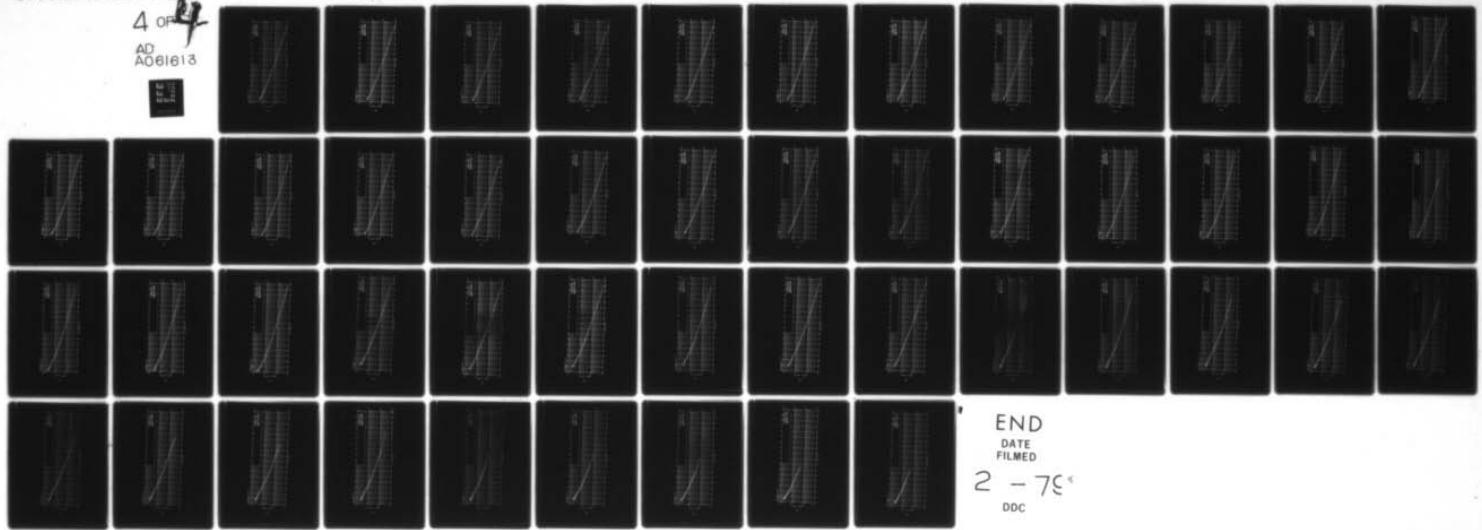
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