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PAFEC75 ON THE A.U.W.E. ICL 1904S\*. A USERS' GUIDE, (U)  
APR 78 W J BUTTERWORTH

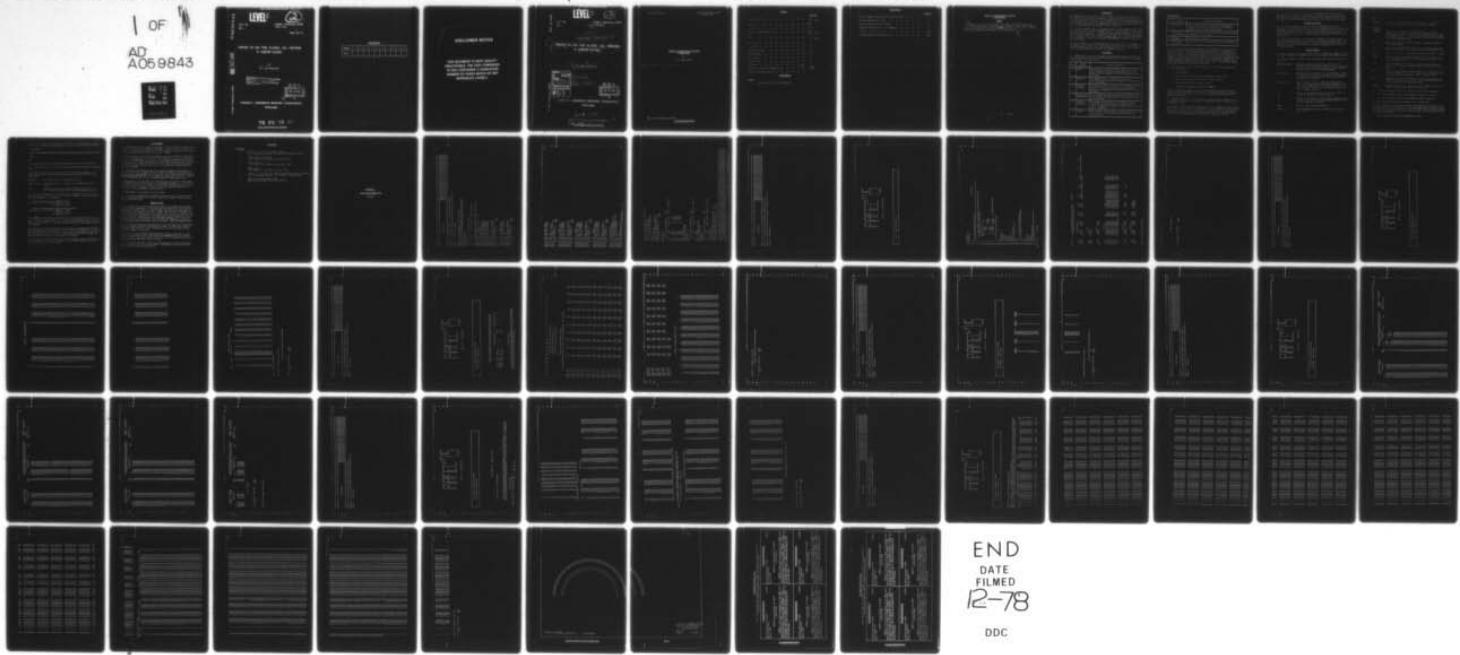
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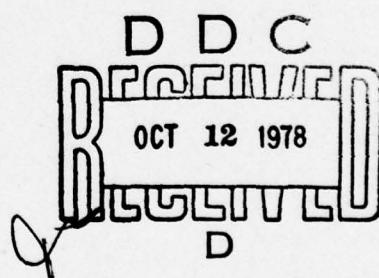
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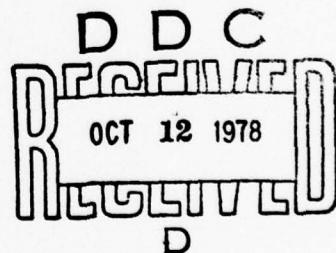
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PAFEC75 ON THE A.U.W.E. ICL 1904S\*  
A USERS GUIDE

by

W. J. Butterworth

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PAFEC75 ON THE A.U.W.E. ICL 1904S\*  
A USERS GUIDE

PRECIS

1. PAFEC75 is the latest development in the PAFEC suite which carries out stress or thermal analysis on any structure by means of finite element methods. A guide to the method of use on the 1904S at A.U.W.E. is given. It is intended that later a dedicated minicomputer will become available.

## INTRODUCTION

2. PAFEC (Program for Automatic Finite Element Calculations) is a suite of programs which is capable of carrying out a large range of engineering calculations on engineering structures. Its development started at Nottingham University in the middle 1960's and it was first issued commercially in 1970 as PAFEC70. In late 1972 this was superseded by PAFEC70\* and extensions were issued, when available. It was implemented at A.U.W.E. in 1976. (Ref. 1).

3. In 1976 the PAFEC group at Nottingham formed a company (PAFEC Ltd) to exploit the system. They then produced PAFEC75 based on a revised layout for input data, designed largely by users in 1974, together with internal changes to the scheme. This version was implemented at A.U.W.E. during 1977 and was finally made available to general users of the 1904S\* in January 1978. It is intended that PAFEC75 will eventually be mounted on a dedicated PAFEC/GRAPIICS computer, hopefully at the end of 1978.

4. Whilst PAFEC75 is well documented (Refs. 2, 3 and 4) it is the variation implemented on the 1904S\* that is described as far as the user is concerned. The method of implementation is described elsewhere (Ref. 5). It is also assumed that the user is already able to use the computer. (Ref. 6).

## THE SYSTEM

5. PAFEC75 uses a series of 10 phases each loading a program. The data is in modular form and if some parts are omitted default values are used. The phases are described in the table below.

Phase	Short description	Detailed description
1	Read	Data modules are read in, default values are inserted and the modules are placed onto backing store. The NODES module is expanded so that all mid-side nodes are included.
2	PAFBLOCKS	Any PAFBLOCK data is replaced by the full nodal co-ordinate and topological description of the complete mesh of elements.
3	IN.DRAW structure	The structure itself is drawn. At this stage it is not possible to show any results such as displacements, stresses or temperatures since these have not yet been evaluated.
4	Pre-solution housekeeping	In this PHASE the constraints on the problem are considered and a numbering system for the degrees of freedom is derived.
5	IN.DRAW constraints	This PHASE is very similar to the PHASE 3 except of course the constraints which have been applied are shown. Conversely the degrees of freedom can be indicated on a drawing.
6	Elements	The stiffness (or other such as conductivity, mass etc.) matrices of all the elements are found and put onto backing store.

Table (Cont'd)

Phase	Short description	Detailed description
7	Solution	The system equations are solved for displacements, temperatures or whatever happens to be the primary unknowns in the problem being tackled.
8	OUT.DRAW displacements	The primary unknowns in the problem (i.e. displacements or temperatures) are drawn.
9	STRESS	The stresses are found.
10	OUT.DRAW stresses	Stress contour, stress vector plate etc. are produced.

6. In the system at A.U.W.E., programs have been compiled in advance and use made of a facility for increasing the core requirement of a program whilst running in order to enlarge an array BASE (which is used by most routines and whose size depends on the problem). Due to the limitation of 150K core size, imposed by the installation manager, the greatest possible size of BASE (at its maximum in phase 7) is 55000. It is hoped that the dedicated computer will have a paged environment thus allowing larger sizes of BASE. This system of pre-compiled programs reduces the time taken for each job. It does however assume that certain element combinations are excluded.

7. The elements are taken from a library (Refs. 3, 4) and are mainly broken up into 5 categories:

- a. Beam elements.
- b. Plane stress, plane strain and axisymmetric elements (2D).
- c. Plate bending and flat faced shell elements (SHELL).
- d. Three dimensional solid elements (3D).
- e. Temperature or Laplacian elements (THERMAL).

The only combination assumed is between beam and shell elements which have a combined program. Any other combination will require a program to be specially written together with a macro to run it. This can be done by JCA1 staff at A.U.W.E. if required.

8. PAFBLOCKs (Phase 2) is a system whereby a mesh of finite elements can be created by specifying the topology of a block and the layout of the mesh in the block (Refs. 3, 4).

9. Using the series of phases enables the job to be stopped at certain stages. These usually coincide with a plotting phase so that the drawing can be inspected for any curious element distortions etc. It is also possible to run phases 6 and 7 on their own as they are those which involve the most computer time and core size in their execution and this enables the longer jobs to run.

10. At the time of writing this guide it is EASIDATA only (Ref. 3) which is implemented. This should be sufficient for most users but it is hoped that the full DATA system (Ref. 4) will be implemented later. Whether this will be on the 1904S\* or the dedicated computer will depend on the time scale and demand.

#### PREPARATION OF DATA

11. The written programs preclude the USE. and READ.FROM. facilities (Refs. 3, 4). The USE. facility would require a specially written program. The READ.FROM. facility is catered for in one of the parameters to the macro to run the system. Also the control of the phasing is done by parameters to the running macro and not by means of PHASE and SAVE commands in the CONTROL module (Refs. 3, 4).

12. Apart from these limitations the data is prepared in the same format as shown in the manuals (Refs. 3, 4). There are two points to make however. It is preferable that the CONTROL module is the first in the data and the FAST. READ facility does not give such a benefit in speed of reading and will not allow continuation lines.

#### RUNNING PAFEC75

13. Three macros are used in the system. These are RUN75 and CLEAR75 which are only used for PAFEC75 and PLOTMAC which is used in common with PAFEC70+ (Ref. 1).

14. RUN75, as might be expected, runs the system and has the following parameters:

- DATA <filename> : Where <filename> is the data file. Note that the absolute name is required if the file is not in <account> specified by DY below. This parameter is only required for Phase 1 and is ignored in other phases.
- OUT <ident> : Where <ident> is a string of up to 8 characters on which the output file names are to be based. If this parameter is absent the job identifier (or the first 8 characters if more than 8) is used.
- DY <account> : Where account is that in which the files are to be created. The account must exist and be available to the user. This parameter is not needed when running in the main account. It facilitates the erasure of files later (but see CLEAR75 below).
- STn : Where n is the phase at which the job is to start. If omitted the job tries to start at Phase 1.
- PLn : Where n is the number of the plot phase required. Such a parameter is required for each plot phase required unless STn above denotes a plot phase.
- ENDn : Where n is the last phase required.
- BLOCK : When PAFBLOCKS (Phase 2) are being used. Not needed if ST2 is used.

6.

2D        )  
3D        )  
BSH        )  
THERMAL):

One of these is required to indicate which type of element is being used in Phases 6 and 9. If omitted 2D is assumed.

DYNAMIC)  
STATIC )  
THERMAL):

One of these is required to indicate the type of solution (Phase 7). Of course for thermal work the parameter is the same as for Phases 6 and 9 so only one is required! If omitted STATIC is assumed. They can all be contracted to the first three characters. (i.e. DYN, STA, THE).

- JTn        : Where n is the total job time required. By default 10 minutes (the system default).
- TIn        : Where n is the program time required for each phase. By default 300 seconds (5 mins). This time is carried into PLOTMAC if used.
- BASEn      : Where n is the size of base required. By default 5000 is assumed.
- CLEAR      : This sets up a call to CLEAR75 (para. 17) which clears out the files created, except for those output for graph plotting. This can be shortened to CL.
- SAVE        : Saves the magnetic tape file(s) carrying information between Phases 6 and 7 which are normally erased. (Para. 24). SV can be used.
- LIST        : Causes the large number of output files to be listed on the line printer. Normally only those for Phases 7 and 9 (results) or the current file at any failure are listed. LI can be used.
- NEJ        : Suppresses the issuing of ENDJOB in a successful background job. Ignored in the event of any error. (It is assumed that the rest of the job depends on a successful run!!).
- RETAIN     : Retains the monitor file in the event of an ENDJOB issued by the macro. (See para. 26). RET or RT can be used.

15. There are only two restrictions in the order of the above parameters:

- a. The DY parameter should precede DYNAMIC (or DYN) (if present).
- b. The ST parameter should precede STATIC (or STA) (if present).

Apart from these restrictions the parameters can be in any order.

16. The formidable list of parameters should not frighten users! They are not all necessary at once. In fact for a static, 2D analysis run in the main account with BASE less than 5000, job time less than ten minutes (and presumably progtme less than five mimutes), no plotting, no pafblocks and no retained monitor file the command needs to be:

RJ <ident>, :<account>,RUN75,PARAM(DATA<filename>)

However if more than 5 or 6 parameters are needed it is preferable, when adding a job to the operators' background queue, to set up the call in a small file i.e.

IN FILENAME

RUN75 DATA PAFDAT,OUT PAFANS,BLOCK,PL3,END3,BASE 10000,RT,JT 900,DY<account>

\*\*\*\*

Then

RJ <ident>, <account>, FILENAME (where <account> here is the main account)

This facilitates the task of the operators when issuing jobs from their background queue.

17. CLEAR75 is responsible for dealing with the debris left by RUN75. It is able to cope with the remains of more than one job and requires the following parameters:

/<ident> : The identifier used in creating the files.

DY<account>: Causes the erasure to take place in the appropriate pseudo account.

PLOT : Causes the erasure of associated redundant plot files. These are not usually erased, in case of plotter/computer failure.

18. The first two parameters can be repeated as necessary. If all the files are in one pseudo account only one DY is needed. Otherwise one is needed paired with each /parameter. For example.

CLEAR75 /UBFSB01,DY:XYZA,DY:XYZB,/UBFSB02  
would clear all files based on UBFSB01 in :XYZA  
and UBFSB02 in :XYZB

CLEAR75 /UBFSB01,DY:XYZA,DY:XYZB,/UBFSB02,/UBFSB03  
would clear all files based on UBFSB01 in :XYZA  
UBFSB02 in :XYZB  
and UBFSB03 in :XYZB

19. PLOTMAC is called from inside RUN75 but can also be called by the user. Its use is described elsewhere (Ref. 1). There is one modification that has now been made, no real mag tapes are used and a series of pseudo mag tape files is set up. This has no direct effect on the user but makes the life of the computer staff a lot easier!!

20. One modification made at A.U.W.E. is to check on the maximum size of BASE used (as opposed to that asked for!). This is noted at the end of the output for each phase and listed to the monitor file (see para. 29 and Appendix A pp1 and 9) and also affords a check on the size of BASE obtained (which is not always the same as that asked for due to limitations on core size).

21. In the event of any program failure the macro RUN75 is ended (a background job is terminated even if NEJ is present) and the current output file (if one exists) is listed on the line printer.

#### FILES CREATED

22. TR<Ident> is the line printer output file. It has a generation number corresponding to the phase and a language code ANSA. If the first file for any phase becomes full (either due to the limit of 8192 transfers or physical size) a second file is assigned with code ANSB - and so on up to ANSZ.

23. B<Ident>S is the disc file containing backing store information (referred to as BS in literature). It is 240 kwords long. After each phase is run B<Ident>S is copied into H<Ident>S. In the event of a successful run H<Ident>S is erased but in the event of failure (usually due to BASE being too small or the time being insufficient) it is left in the filestore to be copied back by the macro before the phase is rerun. This has been found to be necessary as a restart may find B<Ident>S changed!!

24. M<Ident>T is a pseudo mag tape file to carry information between phases 6 and 7. If this file is nearly filled, a second is assigned from inside the program and so on. The language code of the first file is FIRS, subsequent codes are AAMT-AZMT-BAMT-BZMT-CAMT and so on to ZZMT thus catering for 677 files. Usually erased after Phase 7 is run but see SAVE parameter for RUN75 (para. 14).

25. Z<Ident>Qn is the card image file output by each plot phase to be presented to PLOTMAC where n denotes the phase i.e. Z<Ident>Q3 for Phase 3. It is the file from Phase 10 which sets the limit of 8 characters on <Ident> (from the limit of 12 characters for a filename). These files can have more than one generation number due to the card image file being filled.

26. M<Ident>N is the retained monitor file name.

27. It should be remembered that <Ident> is normally the job identifier unless OUT is being used and the files are all created in the pseudo account (if any) in which the job is run.

#### EXAMPLE OF RUN

28. The monitor file of the run and the listings of the output from the phases are to be found in Appendix A. The monitor file (pp A1-A3) shows the contents of :AAHC before the run (p A1), the effect of NEJ, the contents of :AAHC after the run (p A3) noting that the job is now in :AAHC. Then the effect of CLEAR75 can be seen when the LD command shows that the only files left are the data file and plotter output file. A further use of CLEAR75 with the PLOT parameter clears the plot file as well. RUN75 without any ST and DATA parameters gives rise to the DISPLAY and the job is terminated. Another RUN75 with DATAORB was included in the macro which would have given rise to the DISPLAY DATA FILE DOES NOT EXIST.

29. It can also be seen from the monitor file that the maximum size of BASE used was 2990 in Phase 9 (p A3) followed by 2022 in Phase 8 (p A2), 1851 in Phase 6 (p A2) and 1759 in Phase 7 (p A2). From page A1 it can be seen that the size required in Phase 1 is only 131.

30. The plot of the displaced shape from Phase 8 can be seen in Fig. 1. From the output from Phase 8 (p A31) the SCALE OF DISPLACEMENTS should be 0.994E-5 per cm. There is also some sorting of the layout of the labelling in the bottom right hand corner which will have to be done.

31. It should be noted that without the LI parameter the only listings (apart from the monitor file) would be from Phase 7 (pp A22-A27) and Phase 9 (pp A33 - A43) a total of 17 pages instead of 40.

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- 1 PAFEC on the A.U.W.E. ICL 1904S\* Computer.  
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- 2 PAFEC75 Theory and Results.  
R. D. Henshell (ed.), PAFEC Ltd., December 1975.
- 3 PAFEC75 EASIDATA.  
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- 4 PAFEC75 DATA.  
R. D. Henshell (ed.), PAFEC Ltd., April 1976.
- 5 PAFEC75 on the A.U.W.E. ICL 1904S\* - Implementation and its problems.  
W. J. Butterworth, A.U.W.E. To be issued. 1978 (C-in-C).
- 6 AUWE Computer Service User Guide.  
AUWE Publication 31904 3rd ed June 1976 (U).

APPENDIX A

OUTPUT FROM EXAMPLE RUN

(A1-A43)

\*\*\*\*\*  
 AAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA AAAAAA  
 \*\*\*\*\*

:AAAH.UJWCWHR0

LISTING OF :AAAH.UJWCWHR0(1/1818U) PRODUCED ON 21MARS AT 08.47.24

OUTPUT BY LISTFILE IN :AAAH.UJWCWHR0. ON 21MARS AT 08.47.25 USING U14

DOCUMENT :AAAH.UJWCWHR0(1/1818U)

STARTED :AAAH.UJWCWHR0,21MARS 08.47.47 TYPE:BULK  
 08.26.47+ M J UJWCWHR0,TESTAF  
 16/5/80 DUE TO CORROSION A GENERAL RESTORE HAS BEEN DONE FROM  
 DUMP TAKEN AT 16.27 ON 15/5/70. ALL WORK AFTER THIS TIME LOST.  
 08.26.47+ TESTAF  
 08.26.47+ LD :AAAH  
 08.26.48+ LF !

## LISTDIR LISTING OF DIRECTORY :AAAH

TYPE	NAME	GEN.NU.	LANG.	PEEL.NU.	SERIAL NU.
FILE	SMPRE	1			
08.26.49+	RUN/DYAAHC,DATASMPRE,OUTWRB,LINERJ,BLOCK,PLD				
08.26.49+	TA AB,CMRCT				
DISPLAY:	***** DATA FILE SMPRE				
08.26.52	0.01 USED URGENCY M				
08.26.52	0.04 CORE GIVEN 410RA				
08.26.45	FREE *DAZ *351 TRANSFERS				
08.27.45	FREE *CRI *35 TRANSFERS				
08.27.45	FREE *CRI *1 TRANSFERS				
08.27.45	FREE *DAI *21 TRANSFERS				
08.27.45	FREE *LPD *1/C 1-TRANSFERS				
DISPLAY:	11				
08.13	DELETED 1.00				
08.27.46	FREE *DAU *1/2 TRANSFERS				
08.27.46	0.14 DELETED CLOKED 0.05				
DISPLAY: END OF PHASE 1					
*****	MAX SIZE OF BASE USED 151				
	SET TO 5000				
DISPLAY:	***** PHASE 2				
08.25.46	0.17 CORE GIVEN 51930				
08.25.46	FREE *DAZ *24 TRANSFERS				
08.29.47	FREE *LPD *1/C TRANSFERS				
DISPLAY:	11				
0.25	DELETED 1.00				
08.29.48	FREE *DAU *74 TRANSFERS				
08.29.48	0.25 DELETED CLOKED 0.05				
DISPLAY: END OF PHASE 2					
*****	MAX SIZE OF BASE USED 1552				
	SFT TO 5000				
DISPDIR	*****				

A2 0 2  
 0 4  
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 0 8  
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DISPLAY: \*\*\* PHASE 0  
 08.30.38 0.27 CORE GIVEN 5619C  
 08.30.36 FREE \*DAZ \*31 TRANSFERS  
 08.30.37 FREE \*LPU 198 TRANSFERS  
 DISPLAY: 11  
 0.52 :DELETED : 00  
 08.30.2/ FREE \*DAZ 0 TRANSFERS  
 08.30.2/ 0.52 DELETED,CLUCKED 0.04  
 DISPLAY: END OF PHASE 4  
 \*\*\* MAX SIZE OF BASE USED 1066  
 SET TO 5000

DISPLAY: \*\*\* PHASE 0  
 08.31.4h 0.56 CORE GIVEN 5603C  
 08.31.44 FREE \*MTU \*13 TRANSFERS  
 08.31.44 FREE \*DAZ \*12 TRANSFERS  
 08.31.44 FREE \*LPU .89 TRANSFERS  
 DISPLAY: 11  
 1.40 :DELETED : 00  
 08.32.44 FREE \*DAU 1460 TRANSFERS  
 08.32.44 1.40 DELETED,CLUCKED 1.01  
 DISPLAY: END OF PHASE 6  
 \*\*\* MAX SIZE OF BASE USED 1651  
 SET TO 5000

DISPLAY: \*\*\* PHASE 7  
 08.30.46 1.45 CORE GIVEN 5/504  
 08.30.46 FREE \*MTU \*124 TRANSFERS  
 08.30.46 1.45 FREE \*DX1 \*51 TRANSFERS  
 08.30.46 1.45 FREE \*DAZ \*13 TRANSFERS  
 08.30.46 1.45 FREE \*LPU .223 TRANSFERS  
 DISPLAY: 11  
 2.17 :DELETED : 00  
 08.30.16 FREE \*DAU 64 TRANSFERS  
 08.30.16 2.17 DELETED,CLUCKED 0.32  
 DISPLAY: END OF PHASE 7  
 \*\*\* MAX SIZE OF BASE USED 1759  
 SET TO 5000

DISPLAY: \*\*\* PHASE 8  
 08.39.13 2.22 CORE GIVEN 41408  
 08.40.09 FREE \*CP3 \*215 TRANSFERS  
 08.40.09 FREE \*DAZ \*121 TRANSFERS  
 08.40.09 FREE \*LPU .429 TRANSFERS  
 DISPLAY: 11  
 2.55 :DELETED : 00  
 08.40.11 2.55 DELETED,CLUCKED 0.11  
 DISPLAY: END OF PHASE 8  
 \*\*\* MAX SIZE OF BASE USED 2022  
 SET TO 5000

DISPLAY: \*\*\* PHASE 9  
 08.40.2/ 2.57 USED URGENCY G  
 08.40.2/ 2.57 CORE GIVEN 7440  
 DISPLAY: OFFLINE PLOT FILE OPENED 08.40  
 08.40.4h FREE \*MT2 \*121 TRANSFERS  
 2.55 :SHALTED : END OF OFFLINING TAPE CLOSTED  
 08.40.42 FREE \*CRU \*2134 TRANSFERS  
 DISPLAY: 11  
 2.55 :DELETED : 00  
 08.42.45 2.55 DELETED CLOCKED 0.16  
 DISPLAY: ISSUING BACKGROUND PLOT JOB UJCWB/0AS  
 08.42.45 2.55 ISSUING BACKGROUND PLOT JOB UJCWB/0AS

DISPLAY: \*\*\* TURBOS PLUT FILE RETAINED \*\*\*

DISPLAY: \*\*\* PHASE Y

08.45.00 2.50 USED UNIVER.CY M

08.45.00 2.50 USED GIVEN CYCLOS

08.45.00 FREE \*DAZ \*GU TRANSFERS

08.45.05 FREE \*LPJ ,5/5 TRANSFERS

DISPLAY: 11

3.18 DELETED : GU

08.45.59 FREE \*DAU ,4/5 TRANSFERS

08.45.59 3.18 DELETED,LOCKED U,18

DISPLAY: END OF PHASE Y

\*\*\* MAX SIZE OF BASE USED 2990

SET TO SUUG

08.46.40+ LD

08.46.40+ LF 1

LISDIR LISTING OF DIRECTORY :AAMC

TYPE NAME GEN.NO. LANG. REEL.NO. SERIAL NO.

FILE DURBS 1

FILE TRURB 9 ANSA

FILE TRURB 3 ANSA

FILE TRURB 7 ANSA

FILE TRURB 6 ANSA

FILE TRURB 4 ANSA

FILE TRURB 2 ANSA

FILE SPHERE 1

FILE ZORG3 1

FILE 08.46.30+ CLEARS75 /ORB,PLUT

08.46.31+ TA AB,CM,CT

08.47.06+ LD

08.47.08+ LF 1

LISDIR LISTING OF DIRECTORY :AAMC

TYPE NAME GEN.NO. LANG. REEL.NO. SERIAL NO.

FILE SPHERE 1

FILE ZORG3 1

08.47.09+ CLEARS75 /ORB,PLUT

08.47.10+ TA AB,CM,CT

08.47.17+ LD

08.47.19+ LF 1

LISDIR LISTING OF DIRECTORY :AAMC

TYPE NAME GEN.NO. LANG. REEL.NO. SERIAL NO.

FILE SPHERE 1

08.47.19+ RUN75

08.47.19+ TA AB,CM,CT

DISPLAY: \*15\*\* DATA PARAMETER MISSING &\*\*15\*\*

MAXIMUM ONLINE RS USED 494 KWORDS

08.47.22 3.27 FINISHED :AAMCUJWB/0 : 6 LISTFILES

:AAH.UJCWB#U

#LISTING OF :AAH.C.IRUBC(1/ANSA) PRODUCED ON 21MARCH AT 08:27:40

#OUTPUT BY LISFILE IN 'IAAH.UJCWB#U' ON 21MARCH AT 08:27:49 USING U14

DOCUMENT

IRUBC(1/ANSA)

P	PPPPPP	A	AAAAAA	F	FFFFFF	E	EEEEEE	C	CCCCCC	/	/	/	/	555555
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55
P	P	A	A	F	F	E	E	C	C	/	/	/	/	55

LEVEL 1.3 -- OCTOBER 1977

PHASE NUMBER 1 STAKIS HERE

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1 CNDPOL
2 AXISMATERIAL
3 CONTROL-END
4 C
5 C
6 C
7 TITLE CHECK ON PAIRBLOCKS FOR SPHERE
8 C
9 C 20 - 56210 ELEMENTS IN AXISYMMETRIC REPRESENTATION OF SPHERE
10 C PRESSURE APPLIED TO OUTER SURFACE
11 C
12 C DISPLACEMENTS ARE :
13 C   NODE    UX      UY
14 C     1    1.9828    *
15 C     2    1.8934    *
16 C     5    *        -1.9801
17 C     4    *        -1.0876
18 C     3    -1.9828    *
19 C     6    -1.8934    *
20 C     7    1.8917    -0.0984 )SYMMETRICAL ABOUT X=0
21 C     64   -1.8917   -0.0984 )
22 C
23 C DIVISION FACTOR FOR ABOVE 0.1E6
24 C
25 C
26 NODES
27 NODE NUMBER,X,Y
28 1,-0.95,0
29 2,-1,0,0
30 3,0,0.95
31 4,0,1,0
32 5,0,0.95,0
33 6,1,0,0,U,V
34 PAIRBLOCKS
35 PROPS4
36 ELEMENT,N1,N2,TUPOL
37 56210,2,1,2,6,15,4,0,0,3
38 MESH
39 1,1
40 C
41 C THE FOLLOWING CAN BE CHANGED TO SET
42 C UP NODE ELEMENTS ROUND THE CIRCUMFERENCE
43 C,50
44 C
45 PLAT
46 4,4
47 RESTRAINTS
48 1,2,1,2
49 4,1,1,1
50 PRESSURE
51 1,202,0,03,0,04,1,2,4
52 C TWO ATMOSPHERES ON OUTSIDE SURFACE ???
53 END,OF,DATA
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END OF DATA 0 ERRORS

\*\*\*\*\*  
ALL INPUT DATA MODULES FOLLOW AS STORED  
ON BACKING STORE AT THE END OF PHASE 1.

	NAME	TYPE	GRAD	ELEM	PROP	N1	N2	N3	N4	N5
1	BLOC	1.0000	1.0000	36210.	4.0000	4.0000	1.0000	0.0000E+00	0.0000E+00	0.0000E+00
2	TEPO	0.0000	0.0000	5.0000	4.0000	0.0000E+00	0.0000E+00	3.0000		

	REFE	MESH
1	1.0000	SPAC
2	2.0000	50.000

	PLAT	MATE	PLATES	THIC
1	4.0000	4.0000	1.0000	

#### MATERIAL

	E	MU	RO	ALPH	MU	K	SH
1	1.0000	0.2090E+12	0.50000	7800.0	0.11000E+04	0.50000E+02	48.000
2	2.0000	0.1930E+12	0.50000	7700.0	0.12000E+04	0.50000E+02	44.500
3	3.0000	0.1250E+12	0.50000	7100.0	0.12000E+04	0.50000E+02	54.000
4	4.0000	0.6850E+11	0.53000	2692.0	0.24000E+04	0.10000E+01	38.000
5	5.0000	0.7000E+11	0.53000	2800.0	0.22000E+04	0.10000E+01	38.000
6	6.0000	0.7500E+11	0.53000	3000.0	0.20000E+04	0.10000E+01	190.00
7	7.0000	0.11000E+12	0.50000	4532.0	0.85000E+05	0.50000E+02	582.00
8	8.0000	0.6100E+11	0.25000	2226.0	0.72000E+05	0.20000E+01	8400.0
9	9.0000	0.36200E+10	0.45000	1250.0	0.60000E+04	0.50000E+01	8100.0
10	10.0000	0.30000E+11	0.00000E+00	2400.0	0.10000E+04	0.50000E+01	653.00

	LOAD	PRES	SIAP	FINT	SITP	LIST
1	1.0000	0.20205E+06	0.0000	0.0000	1.0000	2.0000

	RESTRAINTS	PLAN	AXIS	DIME	VALU
1	4.00E	0.0000	1.0000	2.0000	0.0000E+00
2	1.0000	4.00E	1.0000	1.0000	0.0000E+00

NO ERRORS OR WARNINGS IN THIS PHASE

\*\* END OF PHASE 1 \*\*

\*\*\*\*\* MAX SIZE OF BCAST USED  
SET TO 151  
5000



\*AAH.UJCWB#0

\*LISTING OF :AAH.IRORB(Z/ANSAY PRODUCED ON 21MAR76 AT 08.29.ZF

#OUTPUT BY LISTFILE IN :AAH.UJCWB#0 ON 21MARCH AT 08.29.32 USING 014

DOCUMENT IRORB(Z/ANSAY)

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PPPPPP AAAAAA FFFFFF TTTTTE CCCCLC // / SSSSSS

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P P A A FF E CC // / SSS

P P A A FF E CC // / SSS

P P A A FF E CC // / SSSSSS

PPPPPP AAAAAA FFFF A EEE C // / SSS

PR PR AA A F EEE C // / SSS

PR PR AA A F EEE C // / SSS

PR PR AA A F EEE C // / SSS

PR PR AA A F EEE C // / SSS

PR PR AA A F EEE CCCCLC // / SSS

PR PR AA A F EEE CCCCLC // / SSS

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LEVEL 1.3 - OCTOBER 1977

\*\*\*\*\*TITLE CHECK ON PAPERBLOCKS FOR SPHERE

\*\*\*\*\*PHASE NUMBER 2 STAKIS HERE

**MODULE 1**      **GLOBAL COORDINATES**

NODE	X	Y	Z	NODE	X	Y	Z
1	-0.9200	0.0000	0.0000	51	0.1432	0.6691	0.0000
2	-1.0000	0.0000	0.0000	52	0.1772	0.6295	0.0000
3	0.0000	0.9200	0.0000	53	0.6191	0.2878	0.0000
4	0.0000	1.0000	0.0000	54	0.6387	0.3466	0.0000
5	0.0000	0.9200	0.0000	55	0.6660	0.2000	0.0000
6	0.0000	1.0000	0.0000	56	0.6910	0.4560	0.0000
7	0.0000	0.9200	0.0000	57	0.7135	0.4067	0.0000
8	0.0000	0.9200	0.0000	58	0.7335	0.5384	0.0000
9	0.0000	0.9200	0.0000	59	0.7504	0.5090	0.0000
10	0.0000	0.9200	0.0000	60	0.7658	0.5208	0.0000
11	0.0000	0.9200	0.0000	61	0.7780	0.4979	0.0000
12	0.0000	0.9200	0.0000	62	0.7875	0.1565	0.0000
13	0.0000	0.5564	0.0000	63	0.7944	0.1046	0.0000
14	0.0000	0.4067	0.0000	64	0.7985	0.5224	0.0000
15	0.0000	0.4540	0.0000	65	0.7950	-0.0000	0.0000
16	0.0000	0.5440	0.0000	66	0.7695	0.1019	0.0000
17	0.0000	0.6587	0.0000	67	0.7535	0.2027	0.0000
18	0.0000	0.8091	0.0000	68	0.7272	0.5013	0.0000
19	0.0000	0.6293	0.0000	69	0.7006	0.5906	0.0000
20	0.0000	0.6691	0.0000	70	0.6444	0.4875	0.0000
21	0.0000	0.7091	0.0000	71	0.7881	0.2751	0.0000
22	0.0000	0.7491	0.0000	72	0.7246	0.6524	0.0000
23	0.0000	0.7791	0.0000	73	0.6524	0.7246	0.0000
24	0.0000	0.8090	0.0000	74	-0.2731	0.7660	0.0000
25	0.0000	0.8597	0.0000	75	-0.4875	0.6444	0.0000
26	0.0000	0.8660	0.0000	76	-0.3966	0.6907	0.0000
27	0.0000	0.8710	0.0000	77	-0.5013	0.7275	0.0000
28	0.0000	0.9135	0.0000	78	-0.4027	0.7537	0.0000
29	0.0000	0.9356	0.0000	79	-0.1019	0.6497	0.0000
30	0.0000	0.9711	0.0000	80	0.0000	0.7570	0.0000
31	0.0000	0.9699	0.0000	81	0.1119	0.7697	0.0000
32	0.0000	0.9781	0.0000	82	0.2027	0.7537	0.0000
33	0.0000	0.9777	0.0000	83	0.5015	0.7275	0.0000
34	0.0000	0.9945	0.0000	84	0.5966	0.6907	0.0000
35	0.0000	0.9966	0.0000	85	0.4875	0.6444	0.0000
36	0.0000	0.9986	0.0000	86	0.2731	0.7660	0.0000
37	0.0000	0.9945	0.0000	87	0.0524	0.7246	0.0000
38	0.0000	0.9155	0.0000	88	0.1246	0.6524	0.0000
39	0.0000	0.8781	0.0000	89	0.7881	0.2751	0.0000
40	0.0000	0.8099	0.0000	90	0.0444	0.4875	0.0000
41	0.0000	0.9211	0.0000	91	0.0906	0.5906	0.0000
42	0.0000	0.9356	0.0000	92	0.7272	0.3013	0.0000
43	0.0000	0.9155	0.0000	93	0.7535	0.4027	0.0000
44	0.0000	0.8410	0.0000	94	0.7450	0.1019	0.0000
45	0.0000	0.2000	0.0000	95	0.7750	-0.0000	0.0000
46	0.0000	0.5587	0.0000	96	-0.4566	0.5457	0.0000
47	0.0000	0.5078	0.0000	97	-0.7440	0.5078	0.0000
48	0.0000	0.7711	0.0000	98	-0.3511	0.1486	0.0000
49	0.0000	0.6092	0.0000	99	-0.7291	0.1775	0.0000
50	0.0000	0.7711	0.0000	100	-0.1755	0.4459	0.0000

## A 12

NUDE	X	Y	Z	X	Y	Z
101	-u. 91154	v. 2y556	v. 00000	128	0. 1975	0. y292
102	-u. 80668	v. 5465	v. 00000	129	0. 2459	0. y176
103	-u. 007b	v. 5064	v. 00000	130	0. 2935	0. y053
104	-u. 84664	v. 4.513	v. 00000	131	0. 5404	0. 6169
105	-u. m227	v. 4.750	v. 00000	132	0. 5864	0. 6672
106	-u. 7y0b	v. 5114	v. 00000	133	0. 4313	0. 6465
107	-u. f60b	v. 5284	v. 00000	134	0. 4750	0. 6267
108	-u. 7	v. 5y18	v. 00000	135	0. 2174	0. 1967
109	-u. 7ub0	v. 0.537	v. 00000	136	0. 2584	0. 1606
110	-u. 0.716	v. 6f77	v. 00000	137	0. 2974	0. 1565
111	-u. 6557	v. 7060	v. 00000	138	0. 0357	0. 0600
112	-u. 3y79	v. 7.583	v. 00000	139	0. 0714	0. 0717
113	-u. 5284	v. 7086	v. 00000	140	0. 0760	0. 0537
114	-u. 5174	v. 7y07	v. 00000	141	0. 383	0. 2978
115	-u. 4.67u	v. 8c77	v. 00000	142	0. 666	0. 2564
116	-u. 4.513	v. 8465	v. 00000	143	0. 968	0. 2174
117	-u. 5004	v. 8079	v. 00000	144	0. 6227	0. 4750
118	-u. 5404	v. 8089	v. 00000	145	0. 664	0. 4315
119	-u. 2y35	v. 9y35	v. 00000	146	0. 6776	0. 3864
120	-u. 2429	v. 9176	v. 00000	147	0. 868	0. 3403
121	-u. 1y75	v. 9.42	v. 00000	148	0. y034	0. 2450
122	-u. 1466	v. 9.583	v. 00000	149	0. 1y75	0. 2429
123	-u. 0yy3	v. 9.448	v. 00000	150	0. y291	0. 1975
124	-u. 0yy7	v. 9.407	v. 00000	151	0. y381	0. 1486
125	-u. 0yy7	v. 9.467	v. 00000	152	0. y446	0. 0995
126	-u. 0yy5	v. 9.448	v. 00000	153	0. y486	0. 0497
127	-u. 1466	v. 9.583	v. 00000			

MODULE NUMBER 17 ELEMENTS

NUMBER	GROUP	TYPE	PROP	INT	TOPLOGY
1.		36210.	4.	6.	8.
2.	1.	36210.	4.	8.	10.
3.	1.	36210.	4.	8.	12.
4.	1.	36210.	4.	8.	14.
5.	1.	36210.	4.	8.	16.
6.	1.	36210.	4.	8.	18.
7.	1.	36210.	4.	8.	20.
8.	1.	36210.	4.	8.	22.
9.	1.	36210.	4.	8.	24.
10.	1.	36210.	4.	8.	26.
11.	1.	36210.	4.	8.	28.
12.	1.	36210.	4.	8.	30.
13.	1.	36210.	4.	8.	32.
14.	1.	36210.	4.	8.	34.
15.	1.	36210.	4.	8.	36.
16.	1.	36210.	4.	8.	38.
17.	1.	36210.	4.	8.	40.
18.	1.	36210.	4.	8.	42.
19.	1.	36210.	4.	8.	44.
20.	1.	36210.	4.	8.	46.
21.	1.	36210.	4.	8.	48.
22.	1.	36210.	4.	8.	50.
23.	1.	36210.	4.	8.	51.
24.	1.	36210.	4.	8.	52.
25.	1.	36210.	4.	8.	53.
26.	1.	36210.	4.	8.	55.
27.	1.	36210.	4.	8.	57.
28.	1.	36210.	4.	8.	59.
29.	1.	36210.	4.	8.	61.
30.	1.	36210.	4.	8.	63.
END OF PAFBLOCKS GENERATION					6.

7.	8.	9.	10.	11.	12.	13.	14.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.				
y7.	yy.																										
66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.	79.	80.	81.	82.	83.	84.	85.	86.	87.	88.	89.	90.	91.		
15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.	30.	31.	32.	33.	34.	35.	36.	37.	38.	39.	40.		
103.	104.	105.	106.	107.	108.	109.	110.	111.	112.	113.	114.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.	
102.	103.	104.	105.	106.	107.	108.	109.	110.	111.	112.	113.	114.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.

NO FRACTIONAL WARNINGS IN THIS PHASE

END OF PHASE 2 (PAFBLOCKS DATA GENERATION)

\*\*\*\*\* MAX SIZE OF BASE USED  
SET TO 5000



PPPPPP AAAAAA FFFFFF EEEEEE CCCCLC // //  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P A FF E C CC // / S S  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EE E / /  
 P P AA A F EEEEEE CCCCLC // / S S  
 P P AA A F EEEEEE CCCCLC // / S S  
 P P AA A F EEEEEE CCCCLC // / S S

LEVEL 1.3 - OCTOBER 1977

PROGRAM TO GENERATE EXTRA DATA FOR GAUSSIAN REDUCTION SOLUTION

\*\*\*\*\*  
 \* TITLE CHECK ON PARBLOCKS FOR SPHERE  
 \* PHASE NUMBER 4 STAKIS HERE  
 \*\*\*\*

	***RESTRAINTS***	NODE PLAN AXIS DIR
6	POINTS FOUND ON PLANE.	CASE 1 2 1 2
NODES	1. 2. 3. 6. 6.	CASE 4 1 1 1
NUDES	95.	CASE 51 52 53 54 55 56
3	POINTS FOUND ON PLANE.	56 57 58 59 60 61
NODES	5. 6.	62 63 64 65 66 67

\*\*\*\*FRONT SIZE\*\*\*\*  
 THE FOLLOWING LIST RUN BY ROW GIVES THE INSTANTANEOUS FRONT SIZE AS EACH ELEMENT  
 IS Merged. THE DIMENSION OF THE STIFFNESS MATRIX IS THE MAXIMUM VALUE (PLUS THE  
 NUMBER OF AUTOMATIC MASTERS IN A DYNAMIC ANALYSIS)

0	15	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16
0	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16	16

\*\*\*\*\*

DIMENSION OF STIFFNESS MATRIX = 16

\*\*\*\*\*

#### DEGREE OF FREEDOM NUMBERS AT NUDES

THE FOLLOWING INFORMATION MAY BE USED TO CHECK THAT CONSTRAINT DATA IS CORRECT

NODE NUMBER	1	2	3	4	5	6	7	8	9	10	11.	12.	13.	14.
D.O.F. N.U.	1.	2.	0.	0.	5.	6.	7.	9.	11.	13.	14.	15.	16.	17.
D.O.F. N.O.	0.	0.	3.	4.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
NODE NUMBER	11	12	13	14	15	16	17	18	19	20	21.	22.	23.	24.
D.O.F. N.U.	15.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.
D.O.F. N.O.	16.	17.	18.	19.	20.	21.	22.	23.	24.	25.	26.	27.	28.	29.
NODE NUMBER	21	22	23	24	25	26	27	28	29	30	31.	32.	33.	34.
D.O.F. N.U.	35.	36.	37.	38.	39.	40.	41.	42.	43.	44.	45.	46.	47.	48.
D.O.F. N.O.	36.	37.	38.	39.	40.	41.	42.	43.	44.	45.	46.	47.	48.	49.
NODE NUMBER	51	52	53	54	55	56	57	58	59	60	61.	62.	63.	64.
D.O.F. N.U.	55.	56.	57.	58.	59.	60.	61.	62.	63.	64.	65.	66.	67.	68.
D.O.F. N.O.	56.	57.	58.	59.	60.	61.	62.	63.	64.	65.	66.	67.	68.	69.
NODE NUMBER	61	62	63	64	65	66	67	68	69	70	71.	72.	73.	74.
D.O.F. N.U.	65.	66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.
D.O.F. N.O.	66.	67.	68.	69.	70.	71.	72.	73.	74.	75.	76.	77.	78.	79.
NODE NUMBER	91	92	93	94	95	96	97	98	99	100	101.	102.	103.	104.
D.O.F. N.U.	95.	96.	97.	98.	99.	100.	101.	102.	103.	104.	105.	106.	107.	108.
D.O.F. N.O.	96.	97.	98.	99.	100.	101.	102.	103.	104.	105.	106.	107.	108.	109.
NODE NUMBER	61	62	63	64	65	66	67	68	69	70.	71.	72.	73.	74.
D.O.F. N.U.	115.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.
D.O.F. N.O.	116.	117.	118.	119.	120.	121.	122.	123.	124.	125.	126.	127.	128.	129.
NODE NUMBER	71	72	73	74	75	76	77	78	79.	80	81.	82.	83.	84.
D.O.F. N.U.	134.	135.	136.	137.	138.	139.	140.	141.	142.	143.	144.	145.	146.	147.
D.O.F. N.O.	135.	136.	137.	138.	139.	140.	141.	142.	143.	144.	145.	146.	147.	148.
NODE NUMBER	81	82	83	84	85	86	87	88	89.	90	91.	92.	93.	94.
D.O.F. N.U.	153.	154.	155.	156.	157.	158.	159.	160.	161.	162.	163.	164.	165.	166.
D.O.F. N.O.	154.	155.	156.	157.	158.	159.	160.	161.	162.	163.	164.	165.	166.	167.
NODE NUMBER	91	92	93	94	95	96	97	98.	99	100	101.	102.	103.	104.
D.O.F. N.U.	192.	193.	194.	195.	196.	197.	198.	199.	200.	201.	202.	203.	204.	205.
D.O.F. N.O.	192.	193.	194.	195.	196.	197.	198.	199.	200.	201.	202.	203.	204.	205.

DEGREE OF FREEDOM ADDRESSES AND TAGS										A17										
O 2	NODE NUMBER	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	
O 2	D.O.F. NO.	212.	214.	216.	218.	220.	222.	224.	226.	228.	230.	231.	232.	234.	236.	238.	240.	242.	244.	246.
O 4	D.O.F. NO.	213.	215.	217.	219.	221.	223.	225.	227.	229.	231.	232.	234.	236.	238.	240.	242.	244.	246.	248.
O 6	NODE NUMBER	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
O 6	D.O.F. NO.	232.	234.	236.	238.	240.	242.	244.	246.	248.	250.	251.	233.	235.	237.	239.	241.	243.	245.	247.
O 8	D.O.F. NO.	233.	235.	237.	239.	241.	243.	245.	247.	249.	251.	252.	254.	256.	258.	260.	262.	264.	266.	268.
O 10	NODE NUMBER	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149
O 10	D.O.F. NO.	252.	254.	256.	258.	260.	262.	264.	266.	268.	270.	271.	253.	255.	257.	259.	261.	263.	265.	267.
O 12	D.O.F. NO.	253.	255.	257.	259.	261.	263.	265.	267.	269.	271.	272.	274.	276.	278.	280.	282.	284.	286.	288.
O 14	NODE NUMBER	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159
O 14	D.O.F. NO.	272.	274.	276.	278.	280.	282.	284.	286.	288.	290.	291.	273.	275.	277.	279.	281.	283.	285.	287.
O 16	D.O.F. NO.	292.	294.	296.	298.	299.	299.	299.	299.	299.	299.	299.	293.	295.	297.	299.	299.	299.	299.	299.
O 18	D.O.F. NO.	294.	296.	298.	299.	299.	299.	299.	299.	299.	299.	299.	295.	297.	299.	299.	299.	299.	299.	299.
O 20	D.O.F. NO.	295.	297.	299.	299.	299.	299.	299.	299.	299.	299.	299.	297.	299.	299.	299.	299.	299.	299.	299.
O 22	D.O.F. NO.	297.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 24	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 26	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 28	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 30	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 32	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 34	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 36	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 38	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 40	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 42	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 44	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 46	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 48	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 50	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 52	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 54	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 56	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 58	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 60	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.
O 62	D.O.F. NO.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.	299.

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62

NO ERRORS OR WARNINGS IN THIS PHASE

\*\*\*FREEDOM GENERATION FOR SOLUTION COMPLETED\*\*\*

\*\*\*\* MAX SIZE OF BASE USED 1066  
SET 10 5000

A18

119

IAAH.UJLRR8/U

LISTING OF :AANC.TKRB(6/ANS) PRODUCED ON 21MART8 AT 08:55:45  
AND INPUT BY LISTFILE IN :IAAH.UJLRR8/U ON 21MAY8 AT 08:35:47 USING U14  
DOCUMENT  
TKRB(6/ANS)

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62

PPP	AAA	FFF	EEE	CCC	UUU	SSS
P P	A A	A FF	E E	C CC	U U	S S
P P	P A	A FF	E E	C CC	U U	S S
P P	P A	A FF	E E	C CC	U U	S S
P P	AAA	FFF	EEE	C	UUU	SSS
P P	AA	A F	EE	C	UU	S S
P P	AA	A F	EE	C	UU	S S
P P	AA	A F	EE	C	UU	S S
P P	AA	A F	EE	C	UU	S S
P P	AA	A F	EE	C	UU	S S
P P	AA	A F	EE	CCC	UUU	S S
P P	AA	A F	EE	CCC	UUU	S S

LEVEL 1.5 \* OCTOBER 1977

TITLE CHECK ON PAFFBLOCKS FOR SPHERE  
PHASE NUMBER 6 STAKES HERE

ELEMENT NUMBER	GROUP NUMBER	ELEMENT TYPE	PROPERTY NUMBER	MATERIAL NUMBER
1	1	56210	4	4
2	1	56210	4	4
3	1	56210	4	4
4	1	56210	4	4
5	1	56210	4	4
6	1	56210	4	4
7	1	56210	4	4
8	1	56210	4	4
9	1	56210	4	4
10	1	56210	4	4
11	1	56210	4	4
12	1	56210	4	4
13	1	56210	4	4
14	1	56210	4	4
15	1	56210	4	4
16	1	56210	4	4
17	1	56210	4	4
18	1	56210	4	4

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62

A21 0 2  
0 4 0 6 0 8 0 10 0 12 0 14 0 16 0 18 0 20 0 22 0 24 0 26 0 28 0 30 0 32 0 34 0 36 0 38 0 40 0 42 0 44 0 46 0 48 0 50 0 52 0 54 0 56 0 58 0 60 0 62

19 1 36210  
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25 1 36210  
26 1 36210  
27 1 36210  
28 1 36210  
29 1 36210  
30 1 36210

NO ERRORS OR WARNINGS IN THIS PHASE

\*\*\*\*\* END OF ELEMENT MATRIX GENERATION \*\*\*\*\*

\*\*\*\*\* MAX SIZE OF BASE USED SET TO 1621 5UUV

1 A22 O 2  
2 O 4 O 4  
3 O 6 O 6  
4 O 8 O 8  
5 O 10 O 10  
6 :AAH.UJCMB/0  
7 :AAH.UJCMB/0  
8 :AAH.UJCMB/0  
9 :AAH.UJCMB/0  
10 :AAH.UJCMB/0  
11 :AAH.UJCMB/0  
12 :AAH.UJCMB/0  
13 :AAH.UJCMB/0  
14 :AAH.UJCMB/0  
15 :AAH.UJCMB/0  
16 :AAH.UJCMB/0  
17 :AAH.UJCMB/0  
18 :AAH.UJCMB/0  
19 :AAH.UJCMB/0  
20 :AAH.UJCMB/0  
21 :AAH.UJCMB/0  
22 :AAH.UJCMB/0  
23 :AAH.UJCMB/0  
24 :AAH.UJCMB/0  
25 :AAH.UJCMB/0  
26 :AAH.UJCMB/0  
27 :AAH.UJCMB/0  
28 :AAH.UJCMB/0  
29 :AAH.UJCMB/0  
30 :AAH.UJCMB/0  
31 :AAH.UJCMB/0  
32 :AAH.UJCMB/0  
33 :AAH.UJCMB/0  
34 :AAH.UJCMB/0  
35 :AAH.UJCMB/0  
36 :AAH.UJCMB/0  
37 :AAH.UJCMB/0  
38 :AAH.UJCMB/0  
39 :AAH.UJCMB/0  
40 :AAH.UJCMB/0  
41 :AAH.UJCMB/0  
42 :AAH.UJCMB/0  
43 :AAH.UJCMB/0  
44 :AAH.UJCMB/0  
45 :AAH.UJCMB/0  
46 :AAH.UJCMB/0  
47 :AAH.UJCMB/0  
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50 :AAH.UJCMB/0  
51 :AAH.UJCMB/0  
52 :AAH.UJCMB/0  
53 :AAH.UJCMB/0  
54 :AAH.UJCMB/0  
55 :AAH.UJCMB/0  
56 :AAH.UJCMB/0  
57 :AAH.UJCMB/0  
58 :AAH.UJCMB/0  
59 :AAH.UJCMB/0  
60 :AAH.UJCMB/0  
61 :AAH.UJCMB/0  
62 :AAH.UJCMB/0

#LISTING OF :AAH.UJCMB//ANSAL PRODUCED ON 21MAR/0 AT 08.38.10  
#OUTPUT BY LISTFILE IN :AAH.UJCMB/0 ON 21MAR/0 AT 08.38.20 USING U14  
DOCUMENT THURB//ANSAL

A23

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LEVEL 1.3 - OCTOBER 1977

TITLE CHECK ON PAFBLOCKS FOR SPHERE

PHASE NUMBER ? STAKIS HERE

2  
 SCALED COORDINATES DIVIDE BY 1.00000  
 \* INDICATES A CONSTRAIN HAS BEEN APPLIED

NODE NO.	COORDINATES		DISPLACEMENTS		ROTATIONS		1	
	X	Y	Z	UX	UY	PHIX	PHIY	PHIZ
1	-0.95000	0.00000		1	1.9038	*		
2	-1.00000	0.00000		2	1.8932	*		
3	0.00000	0.95000		3	*	-1.9801		
4	0.00000	1.00000		4	*	-1.6876		
5	0.95000	0.00000		5	-1.9858	*		
6	0.95000	0.00000		6	-1.8932	*		
7	1.00000	0.00000		7	1.8917	*		
8	0.00000	0.524		8	1.6852	*		
9	-0.944	0.1040		9	1.6750	*		
10	-0.9875	0.1565		10	1.6546	*		
11	-0.9780	0.2079		11	1.6350	*		
12	-0.9650	0.2586		12	1.6004	*		
13	-0.9509	0.3090		13	1.5655	*		
14	-0.9552	0.3594		14	1.4238	*		
15	-0.9135	0.4067		15	1.0617	*		
16	-0.8910	0.4540		16	1.0334	*		
17	-0.8660	0.2600		17	1.2012	*		
18	-0.8587	0.2646		18	1.2630	*		
19	-0.7772	0.6293		19	1.4049	*		
20	-0.7452	0.6691		20	1.4011	*		
21	-0.7072	0.7071		21	1.5333	*		
22	-0.6692	0.7431		22	1.2023	*		
23	-0.6294	0.7771		23	1.1073	*		
24	-0.3878	0.0090		24	1.1095	*		
25	-0.2446	0.6387		25	1.0483	*		
26	-0.2000	0.6661		26	0.9441	*		
27	-0.1540	0.6911		27	0.6273	*		
28	-0.4067	0.1353		28	0.1681	*		
29	-0.3283	0.3356		29	0.6767	*		
30	-0.5090	0.5511		30	0.2054	*		
31	-0.5988	0.6559		31	0.4086	*		
32	-0.2074	0.7781		32	0.5924	*		
33	-0.1504	0.8877		33	0.2952	*		
34	-0.1045	0.9445		34	0.1973	*		
35	-0.0525	0.986		35	0.0988	*		
36	0.0525	0.9986		36	-0.0986	*		
37	0.1045	0.9443		37	-0.1973	*		
38	0.1564	0.8877		38	-0.2952	*		
39	0.2074	0.781		39	-0.3924	*		
40	0.2586	0.6659		40	-0.4986	*		
41	0.3090	0.5511		41	-0.3934	*		
42	0.3585	0.3356		42	-0.6767	*		
43	0.4067	0.1353		43	-0.6081	*		
44	0.4540	0.0910		44	-0.8273	*		
45	0.5090	0.6661		45	-0.9441	*		
46	0.5546	0.6387		46	-1.0483	*		
47	0.5878	0.0900		47	-1.1095	*		
48	0.6294	0.1771		48	-1.1871	*		
49	0.6692	0.7431		49	-1.2023	*		

SCALED COORDINATES  
DIVIDE BY 1.0000

SCALED DISPLACEMENTS/ROTATIONS FOR LOAD CASE 1  
\* INDICATES A CONSTRAINT HAS BEEN APPLIED

DIVIDE BY 0.10000000  
NODES 50= 59

		X	Y	Z	COORDINATES	NUDE NO.	DISPLACEMENTS UX	DISPLACEMENTS UY	DISPLACEMENTS UZ	PHIX	PHIY	PHI Z
1	10	0.7072	0.7071	0	0	50	-1.5335	-1.5330	-1.5330	-1.4011	-1.2610	-1.1056
	10	0.7434	0.6691	0	0	51	-1.4049	-1.4049	-1.4049	-1.3250	-1.1072	-1.0661
	12	0.7772	0.6293	0	0	52	-1.3250	-1.3250	-1.3250	-1.2812	-1.0534	-0.9223
	12	0.8071	0.5876	0	0	53	-1.2812	-1.2812	-1.2812	-1.0017	-0.8262	-0.7678
	14	0.8387	0.5446	0	0	54	-1.2503	-1.2503	-1.2503	-1.0045	-0.6845	-0.6199
	14	0.8660	0.5000	0	0	55	-1.2503	-1.2503	-1.2503	-1.0046	-0.3956	-0.2959
	15	0.8910	0.4544	0	0	56	-1.0017	-1.0017	-1.0017	-0.7650	-0.1972	-0.0984
	15	0.9153	0.4067	0	0	57	-1.1258	-1.1258	-1.1258	-1.0555	-0.6772	-0.5645
	18	0.9352	0.3584	0	0	58	-1.0555	-1.0555	-1.0555	-1.0004	-0.4699	-0.3956
	18	0.9509	0.3090	0	0	59	-1.0004	-1.0004	-1.0004	-1.0503	-0.2956	-0.2299
	20	0.9658	0.2586	0	0	60	-1.0503	-1.0503	-1.0503	-1.0546	-0.1972	-0.1200
	20	0.9780	0.2079	0	0	61	-1.0546	-1.0546	-1.0546	-1.0550	-0.1972	-0.1200
	22	0.9815	0.1563	0	0	62	-1.0550	-1.0550	-1.0550	-1.0552	-0.1972	-0.1200
	22	0.9944	0.1046	0	0	63	-1.0552	-1.0552	-1.0552	-1.0517	-0.1972	-0.1200
	24	0.9985	0.0524	0	0	64	-1.0917	-1.0917	-1.0917	-1.0917	-0.1972	-0.1200
	24	-0.9750	-0.0000	0	0	65	-1.3568	-1.3568	-1.3568	-1.2608	-0.2023	-0.1200
	26	-0.9695	0.1019	0	0	66	-1.4268	-1.4268	-1.4268	-1.0977	-0.4023	-0.2299
	26	-0.9555	0.2027	0	0	67	-1.0977	-1.0977	-1.0977	-1.0425	-0.5971	-0.4299
	28	-0.9212	0.3015	0	0	68	-1.0425	-1.0425	-1.0425	-1.0662	-0.7867	-0.6135
	28	-0.8900	0.3966	0	0	69	-1.0662	-1.0662	-1.0662	-1.0516	-0.9037	-0.7299
	30	-0.8444	0.4873	0	0	70	-1.0516	-1.0516	-1.0516	-1.2504	-1.1329	-0.9223
	30	-0.7969	0.5731	0	0	71	-1.2504	-1.2504	-1.2504	-1.4534	-1.2404	-1.0534
	32	-0.7446	0.6524	0	0	72	-1.4534	-1.4534	-1.4534	-1.2915	-1.4343	-1.2404
	32	-0.6524	0.7446	0	0	73	-1.2915	-1.2915	-1.2915	-1.1550	-1.2027	-1.0534
	34	-0.5751	0.8888	0	0	74	-1.1550	-1.1550	-1.1550	-1.0659	-0.8597	-0.7056
	34	-0.4875	0.6444	0	0	75	-0.9659	-0.9659	-0.9659	-0.9659	-0.9697	-0.8378
	36	-0.5960	0.6907	0	0	76	-0.7659	-0.7659	-0.7659	-0.9711	-0.8097	-0.6559
	36	-0.5013	0.7275	0	0	77	-0.5971	-0.5971	-0.5971	-0.4017	-0.2019	-0.1920
	38	-0.2047	0.9537	0	0	78	-0.4017	-0.4017	-0.4017	-0.2019	-0.1920	-0.1921
	38	-0.1019	0.6977	0	0	79	-0.2019	-0.2019	-0.2019	-0.1921	-0.1921	-0.1921
	40	0.0610	0.7575	0	0	80	*	*	*	-0.2019	-0.1921	-0.1921
	40	0.1019	0.6697	0	0	81	-0.2019	-0.2019	-0.2019	-0.1921	-0.1921	-0.1921
	42	0.2047	0.5357	0	0	82	-0.4017	-0.4017	-0.4017	-0.2019	-0.1921	-0.1921
	42	0.3015	0.2775	0	0	83	-0.3071	-0.3071	-0.3071	-0.1921	-0.1921	-0.1921
	44	0.2466	0.0524	0	0	84	-0.6559	-0.6559	-0.6559	-0.5971	-0.5971	-0.5971
	44	0.3966	0.0907	0	0	85	-0.9659	-0.9659	-0.9659	-0.8597	-0.8597	-0.8597
	46	0.4875	0.0444	0	0	86	-1.1550	-1.1550	-1.1550	-1.0659	-0.7647	-0.6135
	46	0.5751	0.1888	0	0	87	-1.2504	-1.2504	-1.2504	-1.2404	-1.2404	-1.2404
	48	0.6524	0.2446	0	0	88	-1.4534	-1.4534	-1.4534	-1.3004	-1.2404	-1.1299
	48	0.7668	0.2751	0	0	89	-1.3004	-1.3004	-1.3004	-1.2404	-1.2404	-1.1299
	50	0.8444	0.4875	0	0	90	-1.0659	-1.0659	-1.0659	-0.9659	-0.9659	-0.9659
	50	0.8906	0.5466	0	0	91	-1.0659	-1.0659	-1.0659	-0.9659	-0.9659	-0.9659
	52	0.9662	0.5013	0	0	92	-1.0423	-1.0423	-1.0423	-0.9423	-0.9423	-0.9423
	52	0.9535	0.4027	0	0	93	-1.0423	-1.0423	-1.0423	-0.9423	-0.9423	-0.9423
	54	0.9695	0.1019	0	0	94	-1.0423	-1.0423	-1.0423	-0.9423	-0.9423	-0.9423
	54	0.9750	0.0000	0	0	95	-1.0423	-1.0423	-1.0423	-0.9423	-0.9423	-0.9423
	56	-0.9456	0.4977	0	0	96	-1.0423	-1.0423	-1.0423	-0.9423	-0.9423	-0.9423
	56	-0.9446	0.0995	0	0	97	-1.0772	-1.0772	-1.0772	-0.9772	-0.9772	-0.9772
	58	-0.9561	0.1486	0	0	98	-1.0645	-1.0645	-1.0645	-0.9645	-0.9645	-0.9645

SCALING COORDINATES  
DIVIDE BY 1.00000

SCALING DISPLACEMENTS/ROTATIONS FOR LOAD CASE 1  
\* INDICATES A CONSTRAINT HAS BEEN APPLIED

NODE	COORDINATES		L	NODE	DISPLACEMENTS		PHIX	PHIY	PHIZ
	X	Y			UX	UY			
1	-0.9491	0.1975	99		1.9454	-0.4121			
2	-0.9175	0.2459	100		1.9202	-0.5124			
3	-0.9354	0.2936	101		1.8911	-0.6112			
4	-0.8868	0.3403	102		1.8226	-0.7084			
5	-0.8618	0.3864	103		1.8111	-0.8036			
6	-0.8464	0.4315	104		1.7648	-0.8968			
7	-0.8227	0.4750	105		1.7141	-0.9875			
8	-0.7968	0.5174	106		1.6591	-1.0759			
9	-0.7686	0.5584	107		1.5999	-1.1614			
10	-0.7385	0.2978	108		1.5260	-1.2439			
11	-0.7060	0.0357	109		1.4695	-1.3232			
12	-0.6710	0.0717	110		1.3984	-1.3989			
13	-0.6357	0.1060	111		1.3236	-1.4708			
14	-0.5979	0.1385	112		1.2422	-1.5386			
15	-0.5584	0.1686	113		1.1654	-1.6022			
16	-0.5174	0.1967	114		1.0882	-1.6613			
17	-0.4750	0.0227	115		0.9901	-1.7158			
18	-0.4315	0.0465	116		0.8992	-1.7654			
19	-0.3864	0.0679	117		0.8057	-1.8101			
20	-0.3464	0.0869	118		0.7099	-1.8497			
21	-0.2953	0.0352	119		0.6122	-1.8841			
22	-0.2459	0.176	120		0.5126	-1.9134			
23	-0.1975	0.292	121		0.4119	-1.9373			
24	-0.1480	0.383	122		0.3099	-1.9560			
25	-0.0995	0.4668	123		0.2071	-1.9694			
26	-0.0497	0.4487	124		0.1057	-1.9774			
27	0.0497	0.4487	125		0.1057	-1.9774			
28	0.0995	0.4487	126		0.2071	-1.9094			
29	0.1480	0.383	127		0.3099	-1.9260			
30	0.1975	0.292	128		0.4119	-1.9373			
31	0.2459	0.176	129		0.5126	-1.9494			
32	0.2953	0.0352	130		0.6122	-1.8841			
33	0.3464	0.0869	131		0.7099	-1.8497			
34	0.3864	0.0679	132		0.8057	-1.8101			
35	0.4315	0.0465	133		0.8992	-1.7654			
36	0.4750	0.0227	134		0.9901	-1.7158			
37	0.5174	0.0557	135		1.0882	-1.6613			
38	0.5584	0.1686	136		1.1654	-1.6022			
39	0.5979	0.3585	137		1.2422	-1.5386			
40	0.6357	0.0600	138		1.3236	-1.4708			
41	0.6710	0.0717	139		1.3984	-1.3989			
42	0.7060	0.2978	140		1.4695	-1.3232			
43	0.7385	0.2978	141		1.5260	-1.2339			
44	0.7686	0.5584	142		1.5999	-1.1614			
45	0.8064	0.2174	143		1.6591	-1.0759			
46	0.8227	0.4750	144		1.7141	-0.9875			
47	0.8464	0.5135	145		1.7648	-0.8968			
48	0.8618	0.5864	146		1.8111	-0.8036			
49	0.8779	0.5864	147		1.8526	-0.7084			

SCALING DISPLACEMENTS/ROTATIONS FOR LOAD CASE 1  
\* INDICATES A CONSTRAINT HAS BEEN APPLIED

DIVIDE BY 0.10000  
NODES 99-148

SCALED COORDINATES  
 DIVIDE BY 1.00000

\* INDICATES A CONSTRAINT HAS BEEN APPLIED

NODE NO.	COORDINATES			DISPLACEMENTS			ROTATIONS		
	X	Y	Z	UX	UY	UZ	PHIX	PHIY	PHIZ
10	0.9034	0.4936		148	-1.6891	-0.6112			
10	0.9175	0.4459		149	-1.9202	-0.5124			
12	0.9291	0.1973		150	-1.9454	-0.4121			
12	0.9381	0.1480		151	-1.9645	-0.5105			
14	0.9446	0.0995		152	-1.9772	-0.2080			
14	0.9486	0.0497		153	-1.9841	-0.1044			
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END OF PHASE /  
 \*\*\*\* MAX SIZE OF BASE USED  
 SET TO 10000

NO ERRORS OR WARNINGS IN THIS PHASE

A27

A28

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:AAM.UJCHM/HU

#LISTING OF :AARC.IR0108/ANS1 PRODUCED ON 21MAR78 AT 08:40:11

#OUTPUT BY LISTFILE IN :AAM.UJCHM/HU ON 21MAR78 AT 08:40:16 USING U14

DOCUMENT THURB(O/ANSA)

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PPPPPP AAAAAA FFFF FF EEEE CCCLC // / 555555  
P P A A FF E C CC // / 55  
P P A A FF E C CC // / 55  
P P A A FF E C CC // / 55  
P P P P AAAAAA FFFF EEEE C // / 555555  
Pr AA A F EE C // / 55  
Pr AA A F EE C // / 55  
Pr AA A F EE C // / 55  
Pr AA A F EE C // / 55  
Pr AA A F EE C // / 55  
Pr AA A F EEEEEE CCCCCC // / 555555

LEVEL 1.3 - OCTOBER 1977

\*\*\*\*\* TITLE CHECK ON PAIBLOCKS FOR SPHERE  
\*\*\*\*\* PHASE NUMBER 8 STARTS HERE

\*\*\*\*\* PAIFEC DRAW (PHASE 8) \*\*\*\*\*

THIS IS A PHASE 8 DEFAULT DRAWING

AUTOMATIC VIEWING ROUTINE ENTERED - VIEWING NODE NUMBER IS NOT IN THE NODS MODULE.  
THIS IS A TWO-DIMENSIONAL STRUCTURE, SELECTED VIEW WILL BE PERPENDICULAR TO THE PLANE OF THE STRUCTURE.  
SELECTED VIEW IS ALONG THE LINE JOINING THE POINT X= 0.00 , Y= 0.00 , Z= 1.00 , TO THE ORIGIN.

ELEMENT LISTING.

GROUPS LIST EMPIY - ALL ELEMENTS DRAWN  
1. 2 8 1 47 7 65 66 96  
1. 10 97 99 97 99 97 99  
2. 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62

NOTE:

1	3.429	26.540	2	3.000	26.540	3	11.586	34.696
4	11.286	35.126	5	19.742	26.540	6	20.171	40.340
7	5.013	26.990	8	3.048	27.438	9	5.107	47.685
10	3.189	26.525	11	3.294	28.762	12	3.421	47.193
13	3.571	29.617	14	3.743	50.032	15	3.930	50.438
16	4.150	30.833	17	4.585	51.216	18	4.639	51.260
19	4.715	31.943	20	5.205	52.205	21	5.514	52.611
22	5.640	32.920	23	6.182	53.212	24	6.539	53.400
25	6.909	33.740	26	7.293	53.975	27	7.616	54.790
28	8.094	34.583	29	8.209	54.555	30	8.935	54.702
31	9.364	34.833	32	9.801	54.938	33	10.243	55.020
34	10.688	35.078	35	11.136	55.114	36	12.052	55.114
37	12.485	35.078	38	12.928	55.020	39	15.370	54.758
40	13.807	34.833	41	14.238	54.705	42	14.662	54.222
43	15.077	34.583	44	15.483	54.190	45	15.878	53.472
46	16.262	33.740	47	16.652	53.466	48	16.989	53.612
49	17.531	32.920	50	17.637	52.611	51	17.966	52.285
52	18.258	31.943	53	18.532	51.586	54	18.786	51.616
55	19.021	30.833	56	19.235	50.458	57	19.428	50.032
58	19.600	29.617	59	19.750	29.193	60	19.877	28.762
61	19.982	28.525	62	20.064	27.863	63	20.125	27.438
64	20.158	26.989	65	21.540	26.540	66	21.215	26.113
67	23.599	26.281	68	3.025	29.127	69	3.939	29.743
70	4.536	30.723	71	4.613	51.460	72	5.364	52.141
73	5.984	32.761	74	6.065	53.512	75	7.400	53.787
76	8.181	34.187	77	8.499	54.501	78	9.843	54.728
79	10.711	34.862	80	11.296	54.911	81	12.660	56.065
82	13.326	34.728	83	13.789	34.501	84	14.940	34.187

SCALE OF DRAWING IS 0.0859 TO 1

## PUTNIS ARRAY

PAPER COORDINATES	26.540	2	3.000	26.540	3	11.586	34.696	
1	3.429	26.540	5	19.742	26.540	6	20.171	40.340
4	11.286	35.126	8	3.048	27.438	9	5.107	47.685
7	5.013	26.990	11	3.294	28.762	12	3.421	47.193
10	3.189	26.525	14	3.743	50.032	15	3.930	50.438
13	3.571	29.617	17	4.585	51.216	18	4.639	51.260
16	4.150	30.833	20	5.205	52.205	21	5.514	52.611
19	4.715	31.943	23	6.182	53.212	24	6.539	53.400
22	5.640	32.920	26	7.293	53.975	27	7.616	54.790
25	6.909	33.740	29	8.209	54.555	30	8.935	54.702
28	8.094	34.583	32	9.801	54.938	33	10.243	55.020
31	9.364	34.833	35	11.136	55.114	36	12.052	55.114
34	10.688	35.078	38	12.928	55.020	39	15.370	54.758
37	12.485	35.078	41	14.238	54.705	42	14.662	54.222
40	13.807	34.833	44	15.483	54.190	45	15.878	53.472
43	15.077	34.583	47	16.652	53.466	48	16.989	53.612
46	16.262	33.740	50	17.637	52.611	51	17.966	52.285
49	17.531	32.920	53	18.532	51.586	54	18.786	51.616
52	18.258	31.943	56	19.235	50.458	57	19.428	50.032
55	19.021	30.833	59	19.750	29.193	60	19.877	28.762
58	19.600	29.617	62	20.064	27.863	63	20.125	27.438
61	19.982	28.525	65	21.540	26.540	66	21.215	26.113
64	20.158	26.989	68	3.025	29.127	69	3.939	29.743
67	23.599	26.281	71	4.613	51.460	72	5.364	52.141
70	4.536	30.723	74	6.065	53.512	75	7.400	53.787
73	5.984	32.761	77	8.499	54.501	78	9.843	54.728
76	8.181	34.187	80	11.296	54.911	81	12.660	56.065
79	10.711	34.862	83	13.789	34.501	84	14.940	34.187

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A1965U ENITED - DETERMINES POINTS ARRAY FOR DISPLACED SHAPE PLOT.  
 LARGEST DISPLACEMENT IN STRUCTURE = 0.1980E-04 AT NUDE NUMBER 151  
 SCALE OF DISPLACEMENT IS 0.994E-05 X 1

POINTS ARRAY FOR DISPLACED STRUCTURE  
 PAPER COORDINATES  
 NODE 1 5.426 26.540 2 4.904 26.540 3 11.585 26.540  
 4 11.285 35.227 5 17.745 26.540 6 18.267 26.540  
 7 4.915 26.891 8 4.944 27.259 9 4.991 27.259  
 10 5.054 27.930 11 5.154 28.270 12 2.232 28.006  
 13 5.346 28.936 14 5.478 29.260 15 2.627 29.277  
 16 5.793 29.885 17 5.975 30.184 18 6.175 30.475  
 19 6.586 30.751 20 6.614 31.017 21 6.857 31.267  
 22 7.110 31.211 23 7.576 31.758 24 7.654 32.000  
 25 7.943 32.148 26 8.242 32.531 27 8.520 32.847  
 26 8.060 32.648 29 9.189 32.762 30 9.519 32.979  
 31 9.855 32.999 32 10.195 33.061 33 10.539 33.143  
 34 10.086 33.191 35 11.435 33.218 36 11.952 33.218  
 37 12.284 33.191 38 12.631 33.145 39 12.910 33.145  
 40 13.516 32.999 41 13.651 32.899 42 13.911 32.882  
 43 14.315 32.048 44 14.621 32.497 45 14.929 32.551  
 46 15.227 32.168 47 15.516 31.950 48 12.794 31.758  
 49 16.061 31.211 50 16.316 31.270 51 16.557 31.017  
 52 16.785 30.751 53 16.998 30.473 54 17.196 30.184  
 55 17.378 29.885 56 17.544 29.577 57 17.693 29.260  
 58 17.625 28.936 59 17.739 28.605 60 18.056 28.277  
 61 18.117 27.930 62 18.180 27.566 63 18.227 27.259  
 64 18.456 26.891 65 18.162 26.540 66 22.202 26.540  
 67 5.307 27.876 68 5.478 28.526 69 2.715 28.156  
 70 6.017 29.756 71 6.362 30.321 72 8.186 30.844  
 73 7.282 31.518 74 7.606 31.741 75 8.371 32.106  
 76 8.971 32.412 77 9.599 32.653 78 10.244 32.828  
 79 10.416 32.935 80 10.416 32.935

A32

12.422	80	11.385	52.969	14.257	56.955
82	83	13.271	52.653	14.200	56.412
85	14.149	15.364	51.741	15.848	51.516
88	32.106	89	16.789	17.124	24.756
91	30.064	91	28.526	17.664	24.076
94	17.456	92	17.693	26.457	24.062
97	17.469	95	18.009	26.540	24.062
100	5.464	97	9.507	27.594	24.062
103	5.039	98	5.729	28.446	24.062
105	5.750	101	6.093	29.541	24.062
108	6.613	104	6.595	30.166	24.062
110	29.900	107	6.595	30.742	24.062
114	7.001	110	7.224	30.911	24.062
116	7.704	113	7.461	31.527	24.062
118	8.203	116	8.67	32.052	24.062
121	9.577	119	9.681	32.492	24.062
124	10.204	122	10.621	32.679	24.062
126	32.570	125	11.708	32.677	24.062
127	32.697	128	12.067	32.570	24.062
130	12.349	131	13.794	32.294	24.062
133	13.490	134	14.668	31.678	24.062
135	14.384	137	15.466	31.531	24.062
136	15.410	140	16.169	30.677	24.062
139	15.447	143	16.758	29.900	24.062
142	16.275	146	17.415	29.049	24.062
143	17.076	149	17.552	28.156	24.062
148	17.442	152	17.707	27.104	24.062
151	17.664				

\*\* END OF PAPEC DRAW PRINT OUT FOR PHASE 8 \*\*

NO ERRORS OR WARNINGS IN THIS PHASE

\*\*\* MAX SIZE OF BASE USED  
SFT 10 2022 5000

A33

LISTING OF :AAMC-TRUNKS(4/ANS) PRODUCED ON 21MAY80 AT 08:45:06  
OUTPUT BY LISFILE IN :AAH.UJCWB/S0\* ON 21MAY80 AT 08:45:46 USING U14  
DOCUMENT: TRUNKS(4/ANS)

PUPPPR	AAAAAA	FFFFF	EEEEE	CCCCC	///	555555
P	P	A	FF	E	C	CC
P	P	A	FF	E	C	CC
P	P	A	FF	E	C	CC
PUPPPR	AAAAAA	FFFFF	EEEEE	CCCCC	///	555555
P	P	A	EE	E	C	CC
P	P	A	EE	E	C	CC
P	P	AA	EE	E	C	CC
P	P	AA	EE	E	C	CC
P	P	AA	EE	E	C	CC
P	P	AA	EE	E	C	CC

LEVEL 1.3 - OCTOBER 1977

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***** TITTLE CHECK ON PAFBLOCKS FOR SPHERE
***** PHASE NUMBER 9 STARTS HERE
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#### DEFAULT STRESSES ELEMENTS MODULE CREATED IN R09150

SUBROUTINE R09150 IS NUDT ISOPARAMETRIC STRESSING ROUTINE.  
SIGMA1 IS THE MAXIMUM VALUE OF STRESS IN THE PLANE, SIGMA2 IS THE MINIMUM IN THE PLANE, SIGMA3 IS PERPENDICULAR TO THE  
PLANE (I.E. HING STRESS IN AXISYMETRIC CASES), ALPHAS IS THE ANGLE OF SIGMA1 MEASURED + TO THE Y-AXIS FROM THE ELEMENT  
X-AXIS, BETA IS THE ANGLE OF SIGMA1 TO THE GLOBAL X-AXIS, N/A INDICATES THE ELEMENT IS NOT IN THE GLOBAL XY PLANE.

ELE LOAD IN PLANE OF ELEMENT OUT OF PLANE						MAX SHEAR STRESS OF SIGMA1		ANGLE OF SIGMA1		NODE
NU CASE	SIGMA 1	SIGMA 2	SIGMA 3	STRESS	ALPHA	BETA	GLOBAL COORDINATES OF POSITION	POSITION NO		
1 1	0.757E 06	-0.108E 06	-0.117E 06	0.932E 06	06.78	0.13	-1.0000	0.0000	2	
1 1	0.368E 06	-0.108E 06	-0.626E 03	0.967E 06	06.78	0.13	-0.9750	-0.0000	65	
1 1	0.166E 07	-0.110E 07	-0.180E 03	0.107E 07	06.82	0.09	-0.9500	0.0000	1	
1 1	-0.295E 06	-0.202E 06	-0.202E 06	0.945E 06	09.45	-5.04	-0.9465	0.0524	7	
1 1	0.165E 06	-0.207E 06	-0.207E 06	0.967E 06	09.42	-5.01	-0.9356	0.0510	-1	
1 1	0.755E 04	-0.214E 07	-0.216E 07	0.107E 07	09.34	-5.03	-0.9406	0.0477	96	
1 1	-0.208E 06	-0.204E 06	-0.205E 06	0.958E 06	-87.15	-25.96	-0.9444	0.1046	8	
1 1	0.164E 06	-0.207E 07	-0.205E 07	0.982E 07	09.37	-5.05	-0.9395	0.1019	66	
1 1	-0.459E 04	-0.213E 07	-0.214E 07	0.106E 07	-87.12	-5.97	-0.9446	0.0993	97	
2 1	-0.209E 06	-0.604E 07	-0.205E 07	0.916E 07	86.98	-5.99	-0.9944	0.1046	8	
2 1	-0.754E 06	-0.214E 07	-0.205E 07	0.942E 07	86.98	-5.99	-0.9495	0.1019	66	

4	1	-0.1606E+04	-0.2133E+04	-0.2140E+04	-0.1066E+07	66.44	-6.00	-0.9446	0.0943	0.0000	97
2	1	-0.2091E+06	-0.2442E+06	-0.2058E+06	-0.2000E+06	69.44	-9.00	-0.9875	0.1563	0.0000	9
2	1	-0.1630E+06	-0.2407E+06	-0.2008E+06	-0.1983E+06	69.44	-8.99	-0.9648	0.1526	0.0000	42
2	1	-0.2029E+06	-0.2430E+06	-0.2120E+06	-0.1963E+06	69.44	-8.99	-0.9561	0.1466	0.0000	48
2	1	-0.1693E+06	-0.2464E+06	-0.2046E+06	-0.1917E+06	67.02	-11.44	-0.9760	0.2047	0.0000	10
2	1	-0.1935E+06	-0.2480E+06	-0.2006E+06	-0.1963E+06	67.02	-11.43	-0.9555	0.2027	0.0000	67
2	1	-0.6083E+04	-0.2135E+04	-0.2134E+04	-0.1064E+07	67.02	-11.44	-0.9241	0.1975	0.0000	99
3	1	-0.2086E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9740	0.2047	0.0000	10
3	1	-0.1615E+06	-0.2489E+06	-0.2008E+06	-0.9822E+06	67.03	-12.00	-0.9555	0.2027	0.0000	67
3	1	-0.1748E+06	-0.2131E+06	-0.2132E+06	-0.1044E+07	67.03	-12.00	-0.9241	0.1975	0.0000	99
3	1	-0.2089E+06	-0.2464E+06	-0.2029E+06	-0.9192E+06	67.03	-12.00	-0.9658	0.2506	0.0000	11
3	1	-0.1615E+06	-0.2472E+06	-0.2074E+06	-0.9660E+06	67.03	-14.97	-0.9416	0.2524	0.0000	-3
3	1	-0.6071E+04	-0.2134E+04	-0.2135E+04	-0.1063E+07	67.03	-14.97	-0.9175	0.2454	0.0000	100
3	1	-0.2096E+06	-0.2459E+06	-0.2058E+06	-0.9149E+06	66.94	-17.49	-0.9509	0.5090	0.0000	12
3	1	-0.1932E+06	-0.2477E+06	-0.2070E+06	-0.9817E+06	66.94	-17.49	-0.9712	0.5013	0.0000	68
3	1	-0.6061E+04	-0.2134E+04	-0.2134E+04	-0.1044E+07	66.94	-17.49	-0.9354	0.2950	0.0000	101
3	1	-0.2088E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9555	0.2027	0.0000	12
4	1	-0.1615E+06	-0.2489E+06	-0.2008E+06	-0.9822E+06	67.03	-12.00	-0.9740	0.2047	0.0000	67
4	1	-0.1748E+06	-0.2131E+06	-0.2132E+06	-0.1044E+07	67.03	-12.00	-0.9555	0.2027	0.0000	99
4	1	-0.2089E+06	-0.2464E+06	-0.2029E+06	-0.9192E+06	67.03	-12.00	-0.9241	0.1975	0.0000	101
4	1	-0.1615E+06	-0.2472E+06	-0.2074E+06	-0.9660E+06	67.03	-12.00	-0.9658	0.2506	0.0000	13
4	1	-0.6071E+04	-0.2134E+04	-0.2135E+04	-0.1063E+07	67.03	-14.97	-0.9416	0.2524	0.0000	-4
4	1	-0.2096E+06	-0.2459E+06	-0.2058E+06	-0.9149E+06	66.94	-17.49	-0.9509	0.5090	0.0000	100
4	1	-0.1932E+06	-0.2477E+06	-0.2070E+06	-0.9817E+06	66.94	-17.49	-0.9712	0.5013	0.0000	68
4	1	-0.6061E+04	-0.2134E+04	-0.2134E+04	-0.1044E+07	66.94	-17.49	-0.9354	0.2950	0.0000	101
4	1	-0.2088E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9555	0.2027	0.0000	12
5	1	-0.1615E+06	-0.2489E+06	-0.2008E+06	-0.9822E+06	67.03	-12.00	-0.9740	0.2047	0.0000	67
5	1	-0.1748E+06	-0.2131E+06	-0.2132E+06	-0.1044E+07	67.03	-12.00	-0.9555	0.2027	0.0000	99
5	1	-0.2089E+06	-0.2464E+06	-0.2029E+06	-0.9192E+06	67.03	-12.00	-0.9241	0.1975	0.0000	101
5	1	-0.1615E+06	-0.2472E+06	-0.2074E+06	-0.9660E+06	67.03	-12.00	-0.9658	0.2506	0.0000	13
5	1	-0.6071E+04	-0.2134E+04	-0.2135E+04	-0.1063E+07	67.03	-14.97	-0.9416	0.2524	0.0000	-5
5	1	-0.2096E+06	-0.2459E+06	-0.2058E+06	-0.9149E+06	66.94	-17.49	-0.9509	0.5090	0.0000	100
5	1	-0.1932E+06	-0.2477E+06	-0.2070E+06	-0.9817E+06	66.94	-17.49	-0.9712	0.5013	0.0000	68
5	1	-0.6061E+04	-0.2134E+04	-0.2134E+04	-0.1044E+07	66.94	-17.49	-0.9354	0.2950	0.0000	101
5	1	-0.2088E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9555	0.2027	0.0000	12
6	1	-0.1615E+06	-0.2489E+06	-0.2008E+06	-0.9822E+06	67.03	-12.00	-0.9740	0.2047	0.0000	67
6	1	-0.1748E+06	-0.2131E+06	-0.2132E+06	-0.1044E+07	67.03	-12.00	-0.9555	0.2027	0.0000	99
6	1	-0.2089E+06	-0.2464E+06	-0.2029E+06	-0.9192E+06	67.03	-12.00	-0.9241	0.1975	0.0000	101
6	1	-0.1615E+06	-0.2472E+06	-0.2074E+06	-0.9660E+06	67.03	-12.00	-0.9658	0.2506	0.0000	13
6	1	-0.6071E+04	-0.2134E+04	-0.2135E+04	-0.1063E+07	67.03	-14.97	-0.9416	0.2524	0.0000	-5
6	1	-0.2096E+06	-0.2459E+06	-0.2058E+06	-0.9149E+06	66.94	-17.49	-0.9509	0.5090	0.0000	100
6	1	-0.1932E+06	-0.2477E+06	-0.2070E+06	-0.9817E+06	66.94	-17.49	-0.9712	0.5013	0.0000	68
6	1	-0.6061E+04	-0.2134E+04	-0.2134E+04	-0.1044E+07	66.94	-17.49	-0.9354	0.2950	0.0000	101
6	1	-0.2088E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9555	0.2027	0.0000	12
7	1	-0.1615E+06	-0.2489E+06	-0.2008E+06	-0.9822E+06	67.03	-12.00	-0.9740	0.2047	0.0000	67
7	1	-0.1748E+06	-0.2131E+06	-0.2132E+06	-0.1044E+07	67.03	-12.00	-0.9555	0.2027	0.0000	99
7	1	-0.2089E+06	-0.2464E+06	-0.2029E+06	-0.9192E+06	67.03	-12.00	-0.9241	0.1975	0.0000	101
7	1	-0.1615E+06	-0.2472E+06	-0.2074E+06	-0.9660E+06	67.03	-12.00	-0.9658	0.2506	0.0000	13
7	1	-0.6071E+04	-0.2134E+04	-0.2135E+04	-0.1063E+07	67.03	-14.97	-0.9416	0.2524	0.0000	-5
7	1	-0.2096E+06	-0.2459E+06	-0.2058E+06	-0.9149E+06	66.94	-17.49	-0.9509	0.5090	0.0000	100
7	1	-0.1932E+06	-0.2477E+06	-0.2070E+06	-0.9817E+06	66.94	-17.49	-0.9712	0.5013	0.0000	68
7	1	-0.6061E+04	-0.2134E+04	-0.2134E+04	-0.1044E+07	66.94	-17.49	-0.9354	0.2950	0.0000	101
7	1	-0.2088E+06	-0.2463E+06	-0.2040E+06	-0.9722E+06	67.03	-12.00	-0.9555	0.2027	0.0000	12

8	1	-0.2093E+06	-0.4033E+06	-0.2051E+06	-0.9112E+06	86.99	-41.99	-0.7452	0.6691	0.0000	50
8	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	86.99	-41.99	-0.7246	0.6524	0.0000	72
8	1	-0.6096E+04	-0.1305E+06	-0.2155E+06	-0.1062E+07	86.99	-41.99	-0.7050	0.6327	0.0000	109
8	1	-0.2091E+06	-0.4034E+06	-0.2051E+06	-0.9116E+06	86.99	-41.99	-0.7072	0.6071	0.0000	6
8	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	86.99	-41.99	-0.6894	0.6094	0.0000	58
8	1	-0.7275E+04	-0.1305E+06	-0.2155E+06	-0.1062E+07	86.99	-41.99	-0.6718	0.6117	0.0000	110
8	1	-0.2093E+06	-0.4033E+06	-0.2051E+06	-0.9118E+06	87.01	-46.00	-0.6692	0.7451	0.0000	62
8	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-46.00	-0.6524	0.7240	0.0000	73
8	1	-0.7240E+04	-0.1305E+06	-0.2155E+06	-0.1062E+07	87.01	-46.00	-0.6357	0.7060	0.0000	111
9	1	-0.2094E+06	-0.4033E+06	-0.2052E+06	-0.9118E+06	86.99	-46.00	-0.6692	0.7451	0.0000	22
9	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	86.99	-46.00	-0.6524	0.7246	0.0000	73
9	1	-0.6415E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	86.99	-46.00	-0.6357	0.7070	0.0000	111
9	1	-0.2091E+06	-0.4033E+06	-0.2052E+06	-0.9116E+06	86.99	-46.00	-0.6244	0.7771	0.0000	23
9	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	86.99	-46.00	-0.6156	0.7577	0.0000	59
9	1	-0.7149E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	86.99	-46.00	-0.5970	0.7335	0.0000	112
9	1	-0.2093E+06	-0.4033E+06	-0.2053E+06	-0.9118E+06	87.01	-54.00	-0.5874	0.8080	0.0000	24
9	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-54.00	-0.5751	0.7768	0.0000	74
9	1	-0.6404E+04	-0.1303E+06	-0.2153E+06	-0.1064E+07	87.01	-54.00	-0.5584	0.7686	0.0000	113
10	1	-0.2094E+06	-0.4033E+06	-0.2053E+06	-0.9118E+06	87.01	-54.00	-0.5494	0.8180	0.0000	24
10	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-54.00	-0.5310	0.8177	0.0000	114
10	1	-0.6416E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.01	-54.00	-0.5176	0.7676	0.0000	115
10	1	-0.2091E+06	-0.4033E+06	-0.2052E+06	-0.9116E+06	87.01	-54.00	-0.5000	0.8680	0.0000	26
10	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-54.00	-0.4875	0.8444	0.0000	75
10	1	-0.6405E+04	-0.1303E+06	-0.2153E+06	-0.1064E+07	87.01	-54.00	-0.4750	0.8227	0.0000	115
11	1	-0.2094E+06	-0.4034E+06	-0.2053E+06	-0.9113E+06	87.00	-54.00	-0.5494	0.8501	0.0000	26
11	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.00	-54.00	-0.5357	0.8886	0.0000	75
11	1	-0.6433E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.00	-54.00	-0.5227	0.8227	0.0000	115
11	1	-0.2091E+06	-0.4033E+06	-0.2052E+06	-0.9115E+06	87.00	-54.00	-0.5046	0.8686	0.0000	113
11	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.00	-54.00	-0.4910	0.8557	0.0000	27
11	1	-0.6417E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.00	-54.00	-0.4767	0.8677	0.0000	111
11	1	-0.2093E+06	-0.4033E+06	-0.2052E+06	-0.9118E+06	87.01	-60.00	-0.5000	0.8680	0.0000	114
11	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-60.00	-0.4875	0.8444	0.0000	76
11	1	-0.6405E+04	-0.1303E+06	-0.2153E+06	-0.1064E+07	87.01	-60.00	-0.4750	0.8227	0.0000	115
11	1	-0.2094E+06	-0.4034E+06	-0.2053E+06	-0.9112E+06	87.01	-60.00	-0.5494	0.8501	0.0000	26
11	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-60.00	-0.5357	0.8886	0.0000	75
11	1	-0.6406E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.01	-60.00	-0.5227	0.8227	0.0000	115
12	1	-0.2093E+06	-0.4034E+06	-0.2053E+06	-0.9112E+06	87.01	-66.01	-0.4667	0.9155	0.0000	28
12	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-66.01	-0.4505	0.8686	0.0000	76
12	1	-0.6418E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.01	-66.01	-0.4227	0.8686	0.0000	117
12	1	-0.2091E+06	-0.4033E+06	-0.2052E+06	-0.9116E+06	87.01	-66.01	-0.4067	0.9155	0.0000	50
12	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-66.01	-0.3905	0.9155	0.0000	77
12	1	-0.6420E+04	-0.1304E+06	-0.2154E+06	-0.1064E+07	87.01	-66.01	-0.3643	0.9155	0.0000	119
12	1	-0.2092E+06	-0.4033E+06	-0.2051E+06	-0.9115E+06	87.01	-66.01	-0.3481	0.9155	0.0000	51
12	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-66.01	-0.3319	0.9155	0.0000	78
12	1	-0.6421E+04	-0.1303E+06	-0.2153E+06	-0.1064E+07	87.01	-66.01	-0.3157	0.9155	0.0000	119
12	1	-0.2093E+06	-0.4034E+06	-0.2052E+06	-0.9118E+06	87.01	-66.01	-0.2995	0.9155	0.0000	52
12	1	-0.1031E+06	-0.2070E+06	-0.2070E+06	-0.9066E+06	87.01	-66.01	-0.2833	0.9155	0.0000	79





A39			
24	1	-0.1031E 06	-0.2071E 07
24	1	-0.6063E 04	-0.2136E 07
25	1	-0.2093E 06	-0.2030E 07
25	1	-0.1031E 06	-0.2135E 07
25	1	-0.6057E 04	-0.2131E 07
25	1	-0.2092E 06	-0.2031E 07
25	1	-0.1031E 06	-0.2130E 07
25	1	-0.6059E 04	-0.2134E 07
25	1	-0.2094E 06	-0.2031E 07
25	1	-0.1030E 06	-0.2071E 07
25	1	-0.6010E 04	-0.2139E 07
26	1	-0.2094E 06	-0.2031E 07
26	1	-0.1031E 06	-0.2071E 07
26	1	-0.6022E 04	-0.2137E 07
26	1	-0.2094E 06	-0.2031E 07
26	1	-0.1031E 06	-0.2070E 07
26	1	-0.6033E 04	-0.2139E 07
26	1	-0.2094E 06	-0.2033E 07
26	1	-0.1030E 06	-0.2071E 07
26	1	-0.6002E 04	-0.2139E 07
27	1	-0.2096E 06	-0.2034E 07
27	1	-0.1031E 06	-0.2070E 07
27	1	-0.6056E 04	-0.2136E 07
27	1	-0.2095E 06	-0.2030E 07
27	1	-0.1031E 06	-0.2071E 07
27	1	-0.6019E 04	-0.2139E 07
27	1	-0.2098E 06	-0.2035E 07
27	1	-0.1031E 06	-0.2071E 07
27	1	-0.6017E 04	-0.2139E 07
28	1	-0.2096E 06	-0.2034E 07
28	1	-0.1032E 06	-0.2071E 07
28	1	-0.6061E 04	-0.2134E 07
28	1	-0.2089E 06	-0.2041E 07
28	1	-0.1030E 06	-0.2071E 07
28	1	-0.6011E 04	-0.2132E 07
28	1	-0.2086E 06	-0.2063E 07
28	1	-0.1031E 06	-0.2071E 07
28	1	-0.6017E 04	-0.2139E 07
29	1	-0.2095E 06	-0.2044E 07
29	1	-0.1032E 06	-0.2080E 07
29	1	-0.6083E 04	-0.2130E 07
29	1	-0.2091E 06	-0.2044E 07
29	1	-0.1031E 06	-0.2071E 07
29	1	-0.6059E 04	-0.2130E 07
29	1	-0.2091E 06	-0.2041E 07
29	1	-0.1032E 06	-0.2080E 07
29	1	-0.6042E 04	-0.2131E 07
30	1	-0.2088E 06	-0.2040E 07
30	1	-0.1030E 06	-0.2079E 07
30	1	-0.6006E 04	-0.2133E 07
30	1	-0.2076E 06	-0.2041E 07
30	1	-0.1031E 06	-0.2080E 07
30	1	-0.6042E 04	-0.2139E 07
30	1	-0.2086E 06	-0.2041E 07
30	1	-0.1031E 06	-0.2080E 07
30	1	-0.6042E 04	-0.2131E 07

AVERAGING ROUTINE ENTERED

LOAD GLOBAL COORDINATES ANGLE

NODE NU	LOAD CASE	X	Y	Z	BETA	1	2	3
50	1	-0.7439E-04	-0.1133E-04	0.2149E-04	0.1133E-04	-0.1666E-07	0.97	0.9446
51	1	-0.4693E-06	-0.2022E-06	0.2022E-06	0.4693E-06	-0.95	0.9905	0.9954
52	1	-0.1033E-06	-0.4570E-06	0.2074E-06	0.4570E-06	-0.95	0.9756	0.9510
53	1	-0.7753E-04	-0.1212E-04	0.2149E-04	0.1212E-04	-0.94	0.9466	0.9477
54	1	-0.7257E-06	-0.1172E-06	0.1172E-06	0.7257E-06	-0.13	1.0000	0.0000
55	1	0.4687E-06	-0.1090E-06	0.6250E-06	0.1090E-06	-0.13	0.7500	0.0000
56	1	0.1046E-07	-0.1103E-07	0.1802E-07	0.1103E-07	-0.09	0.9500	0.0000

STRESSES

ELT.	NU	SIGMA 1	SIGMA 2	SIGMA 3	SIGMA 1 2	SIGMA 1 3	SIGMA 2 3	TAU MAX
1	1	-0.105E-07	-0.111E-07	-0.111E-07	0.000E-09	0.000E-09	0.000E-09	0.107E-07
2	1	-0.126E-06	-0.108E-07	-0.000E-07	0.000E-09	0.000E-09	0.000E-09	0.903E-06
3	1	-0.695E-04	-0.214E-07	-0.214E-07	0.106E-07	0.106E-07	0.106E-07	0.106E-07
4	1	-0.202E-06	-0.205E-07	-0.205E-07	0.127E-07	0.127E-07	0.127E-07	0.912E-06
5	1	-0.105E-07	-0.110E-07	-0.110E-07	0.009E-09	0.009E-09	0.009E-09	0.107E-07
6	1	-0.146E-06	-0.108E-07	-0.000E-07	0.000E-09	0.000E-09	0.000E-09	0.935E-06
7	1	-0.409E-06	-0.203E-07	-0.203E-07	0.099E-06	0.099E-06	0.099E-06	0.107E-07
8	1	-0.419E-06	-0.204E-07	-0.204E-07	0.116E-06	0.116E-06	0.116E-06	0.116E-06
9	1	-0.409E-06	-0.204E-07	-0.204E-07	0.117E-06	0.117E-06	0.117E-06	0.117E-06
10	1	-0.209E-06	-0.204E-07	-0.204E-07	0.117E-06	0.117E-06	0.117E-06	0.117E-06
11	1	-0.105E-07	-0.110E-07	-0.110E-07	0.009E-09	0.009E-09	0.009E-09	0.107E-07
12	1	-0.105E-07	-0.109E-07	-0.109E-07	0.009E-09	0.009E-09	0.009E-09	0.107E-07
13	1	-0.419E-06	-0.204E-07	-0.204E-07	0.116E-06	0.116E-06	0.116E-06	0.116E-06
14	1	-0.419E-06	-0.204E-07	-0.204E-07	0.117E-06	0.117E-06	0.117E-06	0.117E-06
15	1	-0.491E-06	-0.215E-07	-0.215E-07	0.117E-06	0.117E-06	0.117E-06	0.117E-06
16	1	-0.8660	-0.2288	-0.2288	-0.491E-06	-0.491E-06	-0.491E-06	-0.491E-06
17	1	-0.9509	-0.3090	-0.3090	-0.55	-0.55	-0.55	-0.55
18	1	-0.6071	-0.2078	-0.2078	-0.56	-0.56	-0.56	-0.56
19	1	-0.7776	-0.0293	-0.0293	-59	-59	-59	-59
20	1	-0.9132	-0.4067	-0.4067	-24	-24	-24	-24
21	1	-0.8910	-0.4240	-0.4240	-27	-27	-27	-27
22	1	-0.8660	-0.2000	-0.2000	-30	-30	-30	-30
23	1	-0.8367	-0.2446	-0.2446	-33	-33	-33	-33
24	1	-0.6071	-0.2078	-0.2078	-36	-36	-36	-36
25	1	-0.7776	-0.0293	-0.0293	-39	-39	-39	-39
26	1	-0.9132	-0.4067	-0.4067	-42	-42	-42	-42
27	1	-0.8910	-0.4240	-0.4240	-45	-45	-45	-45
28	1	-0.8660	-0.4351	-0.4351	-48	-48	-48	-48
29	1	-0.6224	-0.1771	-0.1771	-51	-51	-51	-51
30	1	-0.5816	-0.0690	-0.0690	-54	-54	-54	-54
31	1	-0.5446	-0.3587	-0.3587	-57	-57	-57	-57
32	1	-0.7432	-0.0693	-0.0693	-60	-60	-60	-60
33	1	-0.7072	-0.7071	-0.7071	-63	-63	-63	-63
34	1	-0.6664	-0.7431	-0.7431	-66	-66	-66	-66
35	1	-0.6224	-0.2711	-0.2711	-69	-69	-69	-69
36	1	-0.5816	-0.0690	-0.0690	-72	-72	-72	-72
37	1	-0.5446	-0.3587	-0.3587	-75	-75	-75	-75
38	1	-0.5050	-0.0660	-0.0660	-78	-78	-78	-78
39	1	-0.4684	-0.6910	-0.6910	-81	-81	-81	-81
40	1	-0.4335	-0.1771	-0.1771	-84	-84	-84	-84
41	1	-0.4043	-0.7445	-0.7445	-87	-87	-87	-87
42	1	-0.3625	-0.9986	-0.9986	-90	-90	-90	-90
43	1	-0.2560	-0.6659	-0.6659	-93	-93	-93	-93
44	1	-0.2079	-0.7811	-0.7811	-96	-96	-96	-96
45	1	-0.1564	-0.7877	-0.7877	-99	-99	-99	-99
46	1	-0.1043	-0.7881	-0.7881	-102	-102	-102	-102
47	1	-0.0625	-0.9986	-0.9986	-105	-105	-105	-105
48	1	-0.5309	-0.9211	-0.9211	-108	-108	-108	-108
49	1	-0.5593	-0.9536	-0.9536	-111	-111	-111	-111
50	1	-0.1942	-0.7811	-0.7811	-114	-114	-114	-114
51	1	-0.1564	-0.7877	-0.7877	-117	-117	-117	-117
52	1	-0.2079	-0.7881	-0.7881	-120	-120	-120	-120
53	1	-0.1043	-0.7881	-0.7881	-123	-123	-123	-123
54	1	-0.5309	-0.9986	-0.9986	-126	-126	-126	-126
55	1	-0.5593	-0.9986	-0.9986	-129	-129	-129	-129
56	1	-0.1942	-0.7811	-0.7811	-132	-132	-132	-132
57	1	-0.1564	-0.7877	-0.7877	-135	-135	-135	-135
58	1	-0.2079	-0.7881	-0.7881	-138	-138	-138	-138
59	1	-0.1043	-0.7881	-0.7881	-141	-141	-141	-141
60	1	-0.5309	-0.9986	-0.9986	-144	-144	-144	-144
61	1	-0.5593	-0.9986	-0.9986	-147	-147	-147	-147
62	1	-0.1942	-0.7811	-0.7811	-150	-150	-150	-150
63	1	-0.1564	-0.7877	-0.7877	-153	-153	-153	-153
64	1	-0.2079	-0.7881	-0.7881	-156	-156	-156	-156
65	1	-0.1043	-0.7881	-0.7881	-159	-159	-159	-159
66	1	-0.5309	-0.9986	-0.9986	-162	-162	-162	-162
67	1	-0.5593	-0.9986	-0.9986	-165	-165	-165	-165
68	1	-0.1942	-0.7811	-0.7811	-168	-168	-168	-168
69	1	-0.1564	-0.7877	-0.7877	-171	-171	-171	-171
70	1	-0.2079	-0.7881	-0.7881	-174	-174	-174	-174
71	1	-0.1043	-0.7881	-0.7881	-177	-177	-177	-177
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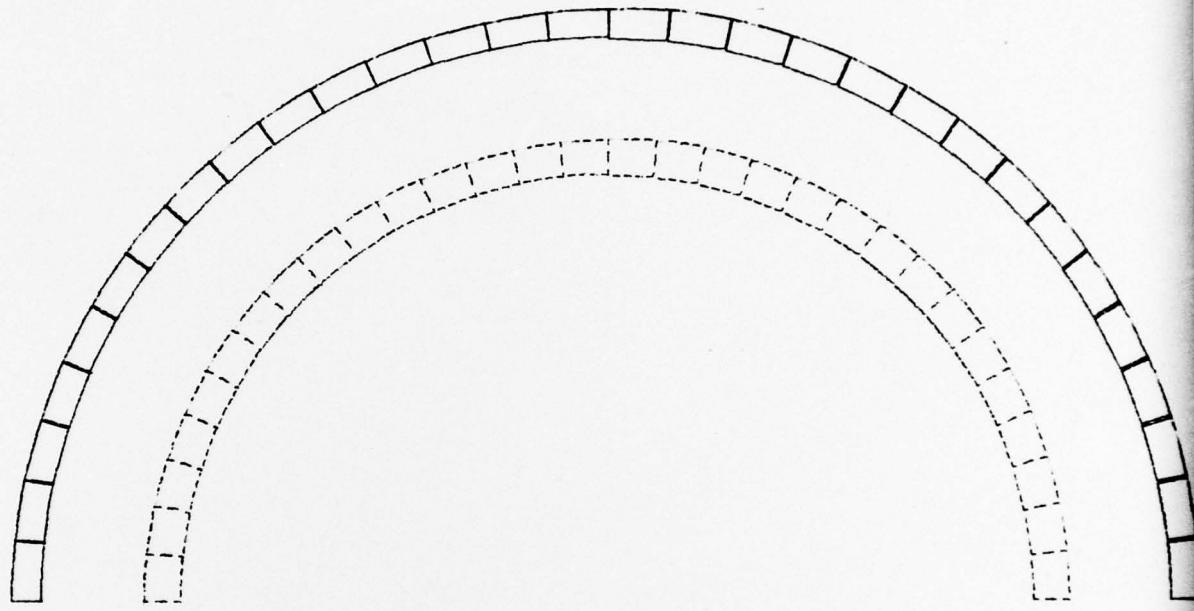
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0	1	U.4460	0.4087	65.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.5310	0.6177	57.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.6150	0.7377	51.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.6892	0.6894	45.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.7510	0.9136	39.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.7510	0.5136	35.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06	
0	1	U.8111	0.5510	0.0000	47.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06
0	1	U.9081	0.4420	0.0000	21.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06
0	1	U.9101	0.5494	0.0000	15.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06
0	1	U.9410	0.6244	0.0000	9.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06
0	1	U.9620	0.1526	0.0000	5.0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06
0	1	U.9730	0.0210	0.0000	0	-0.103E 06	-U.208E 07	-U.208E 07	0.987E 06	0.987E 06

NO ERRORS OR WARNINGS IN THIS PHASE

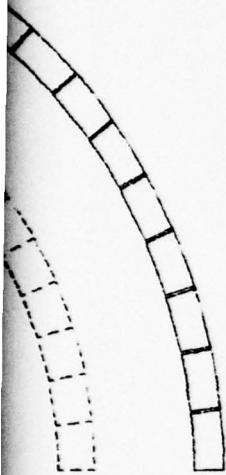
*****	MAX SIZE OF BASE USED Set To	2990
18	20	5000



PAFEC/DRAW ON 22/03/78 AT 09/29/49

DISPLACED SHAPE PLOT FROM EXAMPLE RUN

X



DISPLACED SHOWN DOTTED  
SCALE OF DISPLACEMENTS =  
0.0000000NITS/CM  
DRG. NO. 1  
SCALE = 0.0859:1

FIG. 1

2

Detachable Abstract Cards

These abstract cards are inserted in A.U.W.E. reports and notes for the convenience of librarians and others who need to maintain an information index

<u>UNCLASSIFIED/UNLIMITED</u>	<u>UNCLASSIFIED/UNLIMITED</u>	<u>UNCLASSIFIED/UNLIMITED</u>
A.U.W.E. Publication 45685 W. J. Butterworth April, 1978	62:681.3  PAFEC75 on the A.U.W.E. ICL 1904S* A Users Guide	62:681.3  PAFEC75 is the latest development in the PAFEC suite which carries out stress or thermal analysis on any structure by means of finite element methods. A guide to the method of use on the 1904S* at A.U.W.E. is given. It is intended that later a dedicated minicomputer will become available.
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