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A COMPUTER SUBROUTINE FOR STRESS ANALYSIS OF ROTATING DISKS. II--ETC(U)

AUG 78 J E BROCK

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	by
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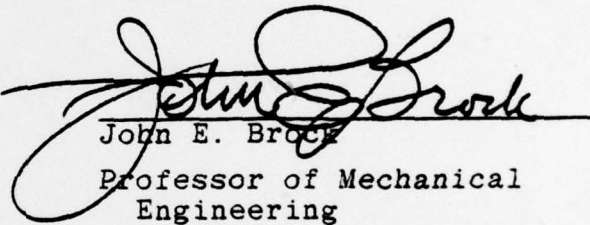
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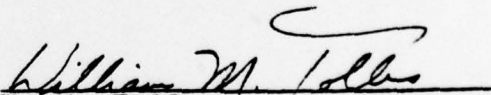
A COMPUTER SUBROUTINE FOR STRESS
ANALYSIS OF ROTATING DISKS - II

This report corrects errors in a previous report on the same subject and presents a listing of a revised and improved digital computer program for finding stress distribution in a thin rotating disk with nonuniform heating.


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A Computer Subroutine for Stress
Analysis of Rotating Disks - II.

by John E. Brock

Based upon theory developed by the writer, R. E. Brown developed a successful computer program for analysis of radial and circumferential stresses in rotating axisymmetric disks of variable thickness having an axisymmetrical thermal strain field. The writer revised Brown's program so as to invoke a group of ancillary subroutines which have been found useful in another application. In doing so, however, much unnecessary and confusing normalization was introduced. In particular, one of the normalizations would cause the analysis to fail in the quite common case of a disk with no radial loading at its outer boundary. All this material appears as Reference 1, hereof.

Referees evaluating a paper based upon Reference 1, called attention to these faults so that the program has been rewritten. A listing of the main subroutine, RODISK, as revised, as well as listings of the ancillary subroutines may be found in Appendix A hereof. The reader will note that other changes have also been made resulting in somewhat more flexibility of application. Employment of the revised program is described in the textual material which appears at the beginning of the listing.

Appendix B contains a revision of the second illustrative example problem of Reference 1. This problem was solved for various values of $M = N-1$, the number of equal subdivisions into which the annular radius $b-a$ is divided for purposes of numerical analysis by RODISK. Also, a

number of different values of KP(3) were used. If KP(3) > 0, its value is the number of iterations which will be performed by RODISK. If KP(3) < 0, iteration will continue until three successive values of the unknown parameter B determined in the course of the analysis, satisfy the relation

$$\frac{|B_1 - B_2| + |B_2 - B_3| + |B_3 - B_1|}{|B_1| + |B_2| + |B_3|} < 10^{KP(3)}$$

We also determined execution time by use of the library subroutine IXCLOK, executing under CP-cms on the IBM 360/67 at the W. R. Church Computer Center at the Naval Postgraduate School.

We found that execution time per iteration is

$$t_{\text{iter}} = 1.2 M + 5 \quad (\text{milliseconds})$$

for any problem.

Accuracy was evaluated by dealing with problems having available analytic solutions. It was found that the principal limitation on accuracy is determined by the choice of subdivisions, the integer $M = N-1$, so that there is a certain inherent error regardless of how many iterations are made. This error depends on M , of course, and upon the details of the problem. The error is greatest near the inner radius of an annular disk, and is large if the ratio a/b is small. Fortuitously, the error may be smaller for an early iteration than for a somewhat later iteration but this is not practically useful information. For the problem of Appendix B hereof, with $a/b = .165$, we find the results given in Table 1, (see next page).

Thus, for example, with $M = 20$, there is an inherent error of about 1% and the results are not significantly improved by iterating

M	approx. limiting % error	approx. iters. req'd.	total time, secs.
5	16	5	.055
10	5	7	.12
20	1	11	.32
40	.1	17	.90
100	.01	25	3.1

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Table 1. Percent error, required iterations, and execution time for problem of Appendix B.

more than eleven times. With eleven iterations, the solution is returned from RODISK in 0.32 seconds.

The significant conclusion is that the execution is so fast that one may as well take $M = 100$ (corresponding to $N = 101$, the maximum available under present dimensioning) and iterate many more times than is strictly necessary. Taking $N = 101$ and $KP(3) = -8$ gave execution in 3.7 seconds with 31 iterations and with an accuracy of 0.004% (In the problem at hand, $\sigma_p(a)$ was specified as zero and the program gets $-1.14E-11$ so that the error here is "infinite". Our evaluation of 0.004% is for the first position rather than for the zeroeth.)

This concludes the text proper of the present report. However, we take advantage of this opportunity to correct errors in Reference 1, viz.:

(1) Page 3, equation 12 should read

$$m = \pm\sqrt{(n^2 - 4vn + 4)} = \pm\sqrt{[(n-2)^2 + 4(1-v)n]}$$

- (2) Page 6, line 2. In place of T read αT .
- (3) Page 6, equation 33. Lower limit of integration should be a rather than 0.
- (4) Page 7, line following equation 40. Reference should be to equation 37 rather than equation 38.

Acknowledgment is gratefully made for assistance by the Naval Postgraduate School Research Foundation. Appreciation is also expressed to the referees of the ASME Journal of Applied Mechanics for directing attention to the flaws in the earlier version of RODISK.

REFERENCE

1. Brock, J. E., and Brown, R. E., A computer subroutine for stress analysis of rotating, heated disks. NPS-69-78-012, Naval Postgraduate School, Monterey, California, May 1978

Appendix A
Listing of
Subroutine
RODISK
and ancillary
subroutines

```

C SUBROUTINE RODISK. JOHN E. BROCK, 1 MAY 1978, REVISED 1 AUGUST 1978. R00000000000000000
C THIS IS A SUBROUTINE FOR DETERMINING RADIAL AND CIRCUMFERENTIAL STRESS R00000000000000000
C IN AN AXISYMMETRIC THIN ELASTIC DISK HAVING AN AXISYMMETRIC THERMAL R00000000000000000
C STRAIN FIELD AND ROTATING AT ANGULAR VELOCITY OMEGA (RADIANS/SECOND) R00000000000000000
C ABOUT THE AXIS OF SYMMETRY. TWO TYPES OF PROBLEM MAY BE TREATED: R00000000000000000
C TYPE 1: ANNULAR DISK OF INSIDE RADIUS ARAC AND OUTSIDE RADIUS R00000000000000000
C BRAD. THE RADIAL STRESS IS SRA AT THE INNER RADIUS AND R00000000000000000
C SRB AT THE OUTER RADIUS. THE INSIDE RADIUS MUST BE R00000000000000000
C GREATER THAN ZERO. R00000000000000000
C TYPE 2: SOLID DISK HAVING RADIAL STRESS SRB AT OUTSIDE RADIUS BRAD. R00000000000000000
C THE USER MUST PROVIDE A MAIN PROGRAM WHICH CALLS SUBROUTINE RODISK R00000000000000000
C AFTER IT HAS SUPPLIED THE FOLLOWING INFORMATION. R00000000000000000
C (1) N, INTEGER. (N-1) IS THE NUMBER OF EQUAL SUBDIVISIONS INTO WHICH R00000000000000000
C THE ANNULAR RADIUS (BRAD MINUS ARAC) IS DIVIDED FOR COMPUTATIONAL PURPOSES. THE PRESENT DIMENSIONING CAN ACCOMMODATE N R00000000000000000
C NOT GREATER THAN 101. R00000000000000000
C (2) BRAD R00000000000000000
C (3) ARAC (NOT NECESSARY FOR PROBLEMS OF TYPE 2.) R00000000000000000
C (4) SRB R00000000000000000
C (5) SRA (NOT NECESSARY FOR PROBLEMS OF TYPE 2.) R00000000000000000
C (6) POIS, POISSON'S RATIO R00000000000000000
C (7) KP(1)=1,2. INTEGERS TO DENOTE PROBLEM OF TYPE 1,2. R00000000000000000
C (8) KP(2), INTEGER TO PROVIDE FOR SKIPPING WHILE PRINTING R00000000000000000
C OUTPUT. FOR EXAMPLE, IF N=101 AND KP(2)=5, ONLY EVERY R00000000000000000
C FIFTH SET OF VALUES WILL BE PRINTED: 1ST,6TH,...., 96TH, R00000000000000000
C AND 101ST. R00000000000000000
C (9) KP(3), INTEGER SPECIFYING NUMBER OF ITERATIONS TO BE R00000000000000000
C PERFORMED. USUALLY KP(3)=10 IS SUFFICIENT FOR ENGINEERING ACCURACY. ALTERNATELY, IF KP(3) IS A NEGATIVE R00000000000000000
C INTEGER, ITERATION WILL CONTINUE UNTIL THREE SUCCESSIVE R00000000000000000
C VALUES OF A PARAMETER ARE DETERMINED INTERNALLY, ARE R00000000000000000
C SUFFICIENTLY CLOSE AS COMPARED TO AN EPSILON EQUAL TO R00000000000000000
C TEN RAISED TO THE KP(3) POWER. R00000000000000000
C (10) KP(4). IF KP(4)=0, ONLY FINAL ANSWERS WILL BE PRINTED. R00000000000000000
C IF KP(4)=1, A SEQUENCE OF ITERANT VALUES OF F WILL BE R00000000000000000
C PRINTED TO INDICATE ORIGIN OF CONVERGENCE. IF KP(4)>1, R00000000000000000
C THERE WILL BE NO PRINTING AT ALL WITHIN RODISK, BUT UPON R00000000000000000
C RETURN KP(5) WILL CONTAIN THE NUMBER OF ITERATIONS WHICH R00000000000000000
C WERE PERFORMED SO THAT KP(5) MUST BE RESET BEFORE RODISK R00000000000000000
C IS CALLED AGAIN. R00000000000000000
C (11) KP(5). KP(5)=0 CALLS MILES CUBIC SPLINE INTEGRATION R00000000000000000
C TO BE USED. OTHERWISE TRAPEZOIDAL INTEGRATION IS USED. R00000000000000000
C (12) VECTOR X(1,J), J=1,2,....,N, CONTAINING VALUES OF DISK R00000000000000000
C THICKNESS AT EQUALLY SPACED RADII FROM INSIDE TO OUTSIDE. R00000000000000000
C (13) VECTOR X(2,J) CONTAINS VALUES OF GAMMA TIMES OMEGA R00000000000000000
C SQUARED WITH J GAMMA IS MASSIVE DENSITY OF THE MATERIAL. R00000000000000000
C FOR MOST PROBLEMS GAMMA OCCURS NOT VARY WITH RADIUS AND R00000000000000000
C ALL ELEMENTS OF THE VECTOR WILL BE THE SAME. R00000000000000000
C (14) VECTOR X(3,J) CONTAINS VALUES OF (E/E) (ALPHA) (TEE) WHERE R00000000000000000
C E IS YOUNG'S MODULUS, ALPHA IS THE COEFFICIENT OF LINEAR R00000000000000000
C THERMAL EXPANSION, AND TEE IS THE TEMPERATURE CHANGE. R00000000000000000
C THE MAIN PROGRAM MUST CONTAIN THE STATEMENTS: R00000000000000000
C IMPLICIT REAL*8 (A-H,C-Z) R00000000000000000
  
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```
FEAL=8 X(20,101)
INTEGER X,N,P(S)
COMMON X,N,P,ARAC,BRAD,SRA,SRB,POIS
SUBROUTINE FOLLOWS THE SUBROUTINE RODISK, THERE ARE SEVERAL ANCILLARY
THEY MAY BE USED TO PERFORM VARIOUS OPERATIONS ON THE VECTORS
COPY, WHICH COPIES IN THE MAIN PROGRAM. SUBROUTINE
IN THE USE OF THE PROGRAM.
SUBROUTINE RODISK
IMPLICIT REAL*8 (A-H,O-Z)
REAL*8 X(20,101)
INTEGER X,N,P
COMMON X,N,P,ARAC,BRAD,SRA,SRB,POIS
ONE=1.D+0
ZERO=0.D+0
BI=1.D+8
BLANK=1.D+10
IT=1.D+12
IF (KP(3).LT.0) EPS=(1.D+11)*(KP(3))
IF (KP(1).EQ.2) ARAC=ZERO
X(4,1)=ARAC+(BRAD-ARAC)*Y
X(5,1)=Y
5 X(6,1)=Y
ITER=1
IF (KP(1).EQ.2) GO TO 1CC
C THE PROBLEM IS OF TYPE 1: ANNULAR DISK
C1=(2.D+0+POIS)*(BRAD-ARAC)
CALL INTV(1,7,8MA)
C2=X(7,N)
C3=X(3,N)-X(3,N)+(CNE-FOISI)*(SRA-SRB)
CALL MULV(1,2,8)
CALL MULV(4,8,5)
CALL INTV(9,10,8MA)
C4=X(10,N)+X(10,N)*SRB-X(1,1)*SRA
20 CALL INTV(5,11,8MA)
C5=BRAD+(CNE+POIS)*X(11,N)
CALL MULV(1,6,12)
CALL INTV(12,13,8MA)
C6=X(13,N)
D=C1*C4-C2*C3
A=(C5*C4-C6*C3)/D
B=(C1*C6-C2*C5)/D
30 CONTINUE
7 IF (KP(1).EQ.1) WRITE(6,1) ITER,A,B
FORMAT(5X,10.1F2E10.5)
CALL MULS(7,14,4)
CALL MULS(13,15,8)
CALL ADDV(14,15,15)
CALL SUBV(15,15,16)
S=SRB*X(1,N)-X(16,N)
CALL ADDS(16,16,5)
CALL DIVV(16,1,10)
ZA=X(3,1)+ARAC+(CNE-POIS)*X(16,1)
CALL MULS(11,17,8)
CALL SUBV(17,18,ARAC)
CALL MULS(13,18,4)
CALL ADDV(17,18,17)
S=-(CNE+POIS)
CALL MULS(17,17,5)
CALL ADDS(17,17,2A)
S=CNE
CALL MULS(16,18,5)
CALL SUBV(17,3,17)
```

RCCCCC 40
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RCCCCC 60
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RCCCCC 950
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RCCCCC 970
RCCCCC 980
RCCCCC 990
RCCCCC 1000

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CALL SUBV(17,18,17)
ITER=ITER+1
IF(KP(3).LT.0) GO TO 215
IF(ITER.GT.KP(3)) GO TO 200
40 CCNTINUE
CALL DUPV(4,14)
IF(KP(1).EQ.2) X(14,1)=CAE
CALL DIVV(17,14,13)
CALL SUBS(18,18,A)
CALL DIVS(19,8,B)
IF(KP(1).EQ.2) GO TO 150
GC TO 20
100 A=ZSRC
C=(ONE-POIS)/X(1,1)
CALL MULV(1,2,7)
CALL MULV(4,7,8)
CALL INTV(8,10,2MA)
SUM=X(10,A)+SR6*(X(1,N)-X(1,1))
SUM=C*SUM+X(3,1)-X(3,N)
150 CALL INTV(6,11,8MA)
DEN=BRAC+(ONE+POIS)*X(11,N)
CALL MULV(1,6,11)
CALL INTV(11,13,8MA)
DEN=DEN+C*X(13,N)
B=SUM/DEN
CALL INTV(1,7,8MA)
CALL INTV(6,11,8MA)
GC TO 30
215 B3=B2
B2=B1
B1=B
ZUM=OABS(B1-B2)+OABS(E2-E3)+CABS(B3-B1)
DIV=OABS(B1)+OABS(B2)+CABS(B3)
CRIT=ZUM/DIV
IF(CRIT.LT.SPS) GO TO 200
GO TO 40
200 CALL ACEV(17,16,19)
IF(AP(3).LT.0.AND.KP(4).EQ.0) WRITE(6,201) ITER, EPS
201 FORMAT(//,20X,'ITERATIONS REQUIRED WITH EPSILON = ',1PE8.1)
IF(KP(4).LE.1) WRITE(6,204)
204 FORMAT(//)
IF(KP(4).LE.1) WRITE(6,205)
205 FORMAT(23X,'RADIUS',10X,'THICKNESS',5X,'GAMMA OMEGA SQ',7X,
1'EE ALPHA TEE',7X,'SIGMA RADIAL',6X,'SIGMA CIRCUMF')
NSKIP=KP(2)
DO 210 I=1,N,NSKIP
J=1/NSKIP
IF(KP(4).LE.1) WRITE(6,211) J, X(4, J), X(1, J), X(2, J),
X(3, J), X(16, J), X(19, J)
210 CCNTINUE
IF(KP(4).GT.1) KP(5)=ITER
211 FORMAT(110,1P6E19.5)
RETURN
END
C THIS IS THE START OF THE ANCILLARIES
SUBROUTINE ADCV(N1,N2,N3)
REAL*8 X(20,101),S
INTEGER KP(5)
COMMON X,N,KP
DO 1 I=1,N
1 X(N3, I)=X(N1, I)+X(N2, I)
RETURN
END
SUBROUTINE SUBV(N1,N2,N3)
REAL*8 X(20,101),S
INTEGER KP(5)
COMMON X,N,KP
DO 1 I=1,N
1 X(N3, I)=X(N1, I)-X(N2, I)
RETURN
END
SUBROUTINE MULV(N1,N2,N3)
REAL*8 X(20,101),S
INTEGER KP(5)

```

```

ROCC1280
ROCC1290
ROCC1300
ROCC1310
ROCC1320
ROCC1330
ROCC1340
ROCC1350
ROCC1360
ROCC1370
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ROCC1780
ROCC1790
ROCC1800
ROCC1810
ROCC1820
ROCC1830
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ROCC1850
ROCC1860
ROCC1870
ROCC1880
ROCC1890
ROCC1900
ROCC1910
ROCC1920
ROCC1930
ROCC1940
ROCC1950
ROCC1960
ROCC1970
ROCC1980
ROCC1990
ROCC2000
ROCC2010

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```
5 WRITE(6,51) J
51 FORMAT(//,30X,'VECTOR WITH IDENTITY ',15,' HAS BEEN GENERATED.')
GO TO 10
END
SUBROUTINE DUPV(N1,N2)
REAL*8 X(20,101),J
INTEGER KP(5)
COMMON X,N,KP
DO 1 I=1,N
1 X(N2,I)=X(N1,I)
RETURN
END
SUBROUTINE INTV(N1,N2,S)
C KP(5)=0 CAUSES MILNE INTEGRATION TO BE USED.
  OTHERWISE TRAPEZOIDAL INTEGRATION IS USED.
REAL*8 X(20,101),S,ADC,NINO,NTNO,FIVO,THTC,EN,R,F
INTEGER KP(5)
COMMON X,N,KP
IF(KP(5).NE.0) GO TO 10
EN=N-1
EN=1.0+0/EN
NINO=EN*9.0+0/2.40+1
NTNO=EN*1.90+1/2.40+1
FIVO=EN*5.0+0/2.40+1
THTC=EN*1.30+1/2.40+1
R=EN/2.40+1
X(N2,1)=0.0+0
X(N2,2)=NINO*X(N1,1)+NTNO*X(N1,2)-FIVO*X(N1,3)+X(N1,4)*R
NM3=N-3
DO 1 K=1,NM3
  KP1=K+1
  KP2=K+2
  KP3=K+3
  ACC=THTC*(X(N1,KP1)+X(N1,KP2))-R*(X(N1,K)+X(N1,KP3))
1 X(N2,KP2)=X(N2,KP1)+ACC
X(N2,N)=X(N2,N-1)+NINO*X(N1,N)+NTNO*X(N1,N-1)-FIVO*X(N1,N-2)
1+X(N1,N-3)*R
CALL MULS(N2,N2,S)
RETURN
10 CONTINUE
X(N2,1)=0.0+0
P=2*(N-1)
DO 1 I=2,N
  J=I-1
11 X(N2,I)=X(N2,J)+X(N1,I)/F+X(N1,J)/F
CALL MULS(N2,N2,S)
RETURN
END
```

RDC C 2760
RDC C 2770
RDC C 2780
RDC C 2790
RDC C 2800
RDC C 2810
RDC C 2820
RDC C 2830
RDC C 2840
RDC C 2850
RDC C 2860
RDC C 2870
RDC C 2880
RDC C 2890
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RDC C 3100
RDC C 3110
RDC C 3120
RDC C 3130
RDC C 3140
RDC C 3150
RDC C 3160
RDC C 3170
RDC C 3180
RDC C 3190
RDC C 3200
RDC C 3210
RDC C 3220
RDC C 3230

Appendix B

Sample Problem

A disk rotating at 7200 rpm and composed of a metal having a specific weight of 0.283 pounds per cubic inch, is 0.85 inches inside diameter and 5.15 inches outside diameter. The radial stress at the inside radius is zero and that at the outside radius is 22,000 psi. The thickness varies with radius according to the law

$$t = 0.1493 r^{-0.42} \quad (\text{all dimensions in inches})$$

and the temperature change (from the zero stress condition) is given by

$$T = 60 - 1.6 r^2.$$

Take $E = 29,000,000$ psi and $\alpha = 6.7 \cdot 10^{-6}$ /°F and determine radial stress (σ_r) and circumferential stress (σ_θ) as functions of r .

This problem illustrates most of the capabilities of RODISK. Because of the special nature of the thickness variation, i.e., a power relation, an analytic solution may be established so that the accuracy of the RODISK solution may be evaluated. Results of such evaluations are given in Table 1 of the body of this report. There it may be seen that accuracy far better than engineering considerations require or justify may be obtained by taking, say, $N = 101$ and $KP(3) = 25$, so that in 3.1 seconds RODISK returns to the calling (i.e., input) program results with a maximum error of 0.01 % or less. The tabulation which follows shows output with $N = 101$ and $KP(3) = -6$, resulting in 27 iterations and taking 3.3 seconds. Accuracy is better than .006%.

RODISK PROBLEM OF TYPE I

27 ITERATIONS REQUIRED WITH EPSILON = 1.00-6

	RADIUS	THICKNESS	GAMMA	OMEGA	SO	EE	ALPHA	TEE	SIGMA	RADIAL	SIGMA	CIRCUMF
0	8.500000-01	1.59847D 00	4.168800	02	1.14334D 04	-2.27592D-12	3.26495D 04					
1	1.280000 00	1.34596D 00	4.168800	02	1.11487D 04	9.84878D 03	2.40489D 04					
2	1.710000 00	1.19179D 00	4.168800	02	1.07490D 04	1.41231D 04	2.17416D 04					
3	2.140000 00	1.08464D 00	4.168800	02	1.02343D 04	1.65779D 04	2.12388D 04					
4	2.570000 00	1.00436D 00	4.168800	02	9.60467D 03	1.82055D 04	2.14332D 04					
5	3.000000 00	9.41172D-01	4.168800	02	8.86008D 03	1.93710D 04	2.19515D 04					
6	3.430000 00	8.89685D-01	4.168800	02	8.00053D 03	2.02394D 04	2.26427D 04					
7	3.860000 00	8.46629D-01	4.168800	02	7.02601D 03	2.08959D 04	2.34382D 04					
8	4.290000 00	8.09893D-01	4.169900	02	5.93653D 03	2.13897D 04	2.43040D 04					
9	4.720000 00	7.78044D-01	4.168800	02	4.73209D 03	2.17511D 04	2.52226D 04					
10	5.150000 00	7.50068D-01	4.168800	02	3.41269D 03	2.20000D 04	2.61848D 04					

Figure 1. Typical output (for sample problem). The main program supplied information about inner and outer radii and the radial stress thereat, angular velocity and density, and "EE ALPHA TEE." These data reappear in the output above. The main program also supplied $N = 101$, $\nu = 0.3$, $KP(1) = 1$, $KP(2) = 10$, $KP(3) = -6$, $KP(4) = 0$, and $KP(5) = 0$. Then it called subroutine RODISK which produced the output shown here. Execution time was 3.3 seconds.

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