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CALCULATIONS PERTAINING TO THE ENERGY BALANCE AND PLASMA MOTIONS IN THE IONOSPHERE

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applications are required to produce definitive results.

Procedures for the calculation of the rate of energy deposition by solar EUV flux and of the rate of photoionization of the principal atmospheric constituents have been revised. The associated computer codes have been modified or rewritten. The atomic and molecular cross sections utilized by these codes have been updated. The total photoionization cross section of atomic oxygen was revised significantly. Branching ratios for the photoion-ization of N, and G are substantially different from those used previously. Future work undertaken under contract F19628-78-C-9047 will incorporate

electric fields into the transport equations. The study of the spectrum of secondary electrons produced by energetic precipitating particles will be continued under the new contract.

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SECTION I INTRODUCTION AND SUMMARY

Knowledge of the energy balance and plasma motions in the ionosphere is essential for the accurate prediction of atmospheric effects on radio communications under both normal and disturbed conditions. The major source of energy in the upper atmosphere is the extreme ultraviolet (EUV) solar flux. In addition, the EUV flux is the major source of ionization in the daytime at midlatitudes. At high latitudes, precipitating energetic particles contribute substantially to and at times dominate the energy budget and rate of ionization of the topside ionosphere. Charged particle motions, due primarily to diffusion, electric fields, and neutral winds, play a major role in determining local ion concentrations as well as the rate of energy transport.

A major part of the effort under the present contract was devoted to developing procedures and computer codes for the calculation of the diffusive transport of atomic oxygen ions. The pertinent equations are given in Appendix B, and the results are discussed in Section II. In general the calculations show that diffusive transport produces qualitative agreement between the observed and calculated profiles of atomic oxygen ions.

Procedures for the calculation of the rate of energy deposition by solar EUV flux and of the rate of photoionization of the principal

atmospheric constituents have been revised, and the associated computer codes have been modified or rewritten. The necessary atomic and molecular data have been updated and are given in detail in Appendix A.

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SECTION II

DIFFUSIVE TRANSPORT OF ATOMIC OXYGEN IONS

A part of the current study pertains to the study of plasma motions in the ionosphere. The agents of ionospheric transport are ambipolar diffusion, electric fields, neutral winds, and to some extent temperature gradients of the ionized components.

For the principal molecular ions, O_2^+ , N_2^+ . and NO^+ , transport processes are unimportant in the daytime. The short chemical reaction times of these ions cause them to be in photochemical equilibrium at all altitudes. This has been demonstrated in a theoretical study by Schunk and Walker (1973), and by a comparison of calculated and observed molecular ion profiles by Oppenheimer et al. (1977). A typical comparison is shown in Figure 1. The principal molecular ions are also insensitive to transport processes in the nighttime ionosphere above about 200 kilometers (cf. Schunk and Walker, 1973). Below this altitude, the time scales associated with transport due to neutral winds and electric fields are comparable to photochemical times, and photochemical equilibrium no longer prevails.

In contrast to the molecular ions, 0^+ ceases to be in photochemical equilibrium at altitudes above the F₂ peak (~250 km) even in daytime. The departure from photochemical equilibrium is clearly demonstrated by Figure 2. This departure is thought to be primarily due to the effects of ambipolar diffusion. Accordingly an effort

was undertaken to study these effects in situations where both the neutral and ionized ionospheric constituents are known.

The formulation of the equations for diffusive transport is outlined in Appendix B. Since the electric field is not among the observed quantities, the current formulation eliminates it from the transport equations. In future work, a modified version will study the effects of sample electric fields compatible with those observed by AFGL satellite measurements.

Since the diffusion equation is of second order, two boundary conditions are required for a solution. One of the boundary conditions is chosen to be the 0⁺ concentration of the lower boundary (200 km in the present calculations). For the second boundary condition two different choices were made. One was to fix the O' concentration at some upper boundary (chosen as 470 km in the present calculations), or to fix the 0⁺ flux at some upper boundary (chosen as 600 km in the present calculations). Figure 3 displays the results of two calculations with fixed concentrations at the upper boundary. Figure 4 displays the results of three calculations with fixed flux at the upper boundary. In both figures the observed O⁺ concentration has been plotted as well (in this instance data from orbit 594 of the AE-C satellite were used). For either type of upper boundary condition the altitude profiles are in marked contrast to the profile calculated under the assumption of local photochemical equilibrium. The latter calculation results in a profile which increases exponentially above the F2 peak. Calculations

including diffusion, on the other hand, result in profiles that qualitatively reproduce the observed decline of the concentration above the F_2 peak. The results obtained with fixed upper boundary concentration (Figure 3) are generally less satisfactory in the sense that a reasonable 0⁺ value at the top of the atmosphere forces very large values at the F_2 peak. The calculations with fixed-flux upper boundary condition are in better qualitative agreement with the observed profile (for the case where the flux is set to zero).

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Ideally, a truly vertical O⁺ concentration profile is needed for comparison with the calculations. In the absence of such data, however, the closest available approximation to a vertical profile is data from a highly elliptic satellite orbit. Even for such orbits, however, the satellite observations reflect horizontal variations, where such variations exist. The search for orbits which are known to be free from horizontal variations, and which, at the same time, contain all the necessary data has so far been unsuccessful. Diffusive transport calculations for other orbits will, however, serve as a criterion of whether the adopted procedures are valid.

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Fig. 1. The densities of the molecular ions plotted against altitude and latitude. Dots indicate measurements by the MIMS experiment for the upleg of orbit 594 of the AE-C satellite. Pluses indicate theoretical values (Oppenheimer et al., 1977).



Fig. 2. The density of 0^+ plotted against altitude. Dots indicate measurements by the MIMS experiment for four orbits of the AE-C satellite. Pluses indicate theoretical values calculated on the assumption of local photochemical equilibrium (Oppenheimer et al., 1977). The divergence of the theoretical and measured profiles above the F₂ peak demonstrates the breakdown of local photochemical equilibrium.





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Fig. 4. The density of 0^+ plotted against altitude. Filled circles indicate measurements by the BIMS experiment for orbit 594, upleg, of the AE-C satellite. Also shown are the results of three calculations based on a fixed flux boundary condition at 600 km: 000 $\phi = 5 \times 10^8$, +++ $\phi = 0, \Box \sqcup \sqcup \phi = 5 \times 10^8$. Flux is in units of cm⁻² sec⁻¹.

SECTION III

PROCEDURES AND COMPUTER CODES PERTAINING

TO ENERGY BALANCE CALCULATIONS

Previously existing procedures for the calculation of the rate of energy deposition by solar EUV flux and of the rate of photoionization of the principal atmospheric constituents have been modified in several respects, and the associated computer codes have been rewritten. The new procedures and codes allow the neutral atmosphere to be specified either in terms of a set of measurements or by a model. Further, the new codes keep track of the energy absorbed by each atmospheric species, and the chemical energy stored in each ionization channel. The energy spectrum of the photoelectrons produced is calculated with any specified resolution, as before. In addition, flexibility has been introduced into the computer codes to make possible a detailed investigation of specific processes.

It had been assumed previously that secondary photons emitted from the radiative decay of inner-shell atomic oxygen ions are absorbed locally. A more careful examination of optical depths for these photons indicates that this assumption is not valid. Hence, the contribution to ionization from these secondary photons has been eliminated. The effect of this change on the total ionization rate is less than five percent.

The atomic and molecular cross sections utilized by those codes have been revised significantly. A detailed description of the cross sections currently in use is given in Appendix A.

The code that calculates the equilibrium electron flux has been modified to some extent in order to make it suitable for execution on a CDC system. A listing and a punched-card copy of this code, together with the necessary input files, is being submitted separately. A sample execution on a CDC-6400 system is also being submitted.

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APPENDIX A

Atomic and Molecular Cross Sections

The extreme ultraviolet (EUV) solar flux supplies the major energy input in the upper atmosphere. In addition, the EUV flux is the major source of ionization in the daytime at midlatitudes. To account properly for the rates of energy deposition and ionization in the upper atmosphere accurate photoabsorption and photoionization cross sections are required. This appendix contains cross sections for the most important atmospheric constituents. These cross sections are based on critical reviews and evaluations of laboratory and theoretical data. A considerable body of new data has become available recently. The agreement among results reported by various investigators is good (generally within 10% or better). Consequently the present body of cross section data may be considered complete insofar as aeronomic calculations are concerned, at least at wavelengths longer than 300 A.

A.1 Atomic Oxygen Cross Sections

The photionization of atomic oxygen through the removal of the 2p valence shell electron leads to $0^+({}^4S^\circ)$, $0^+({}^2D^\circ)$, and $0^+({}^2P^\circ)$ with thresholds at 910.4 Å, 732 Å, and 665 Å respectively. The partial cross sections for these processes as calculated by Henry (1970) have been renormalized using

the total ionization cross section calculated by Taylor and Burke (1976). Ionization through the removal of a 2s inner shell electron gives rise to $0^+({}^4P^e)$ and $0^+({}^2P^e)$ with thresholds at 435 Å and 315 Å respectively. The partial cross sections for these processes were obtained from a calculation by Dalgarno, Henry and Stewart (1964) as modified by Henry (1967). The total ionization cross sections at wavelengths shorter than 435 Å were obtained by adding the partial cross sections for inner shell ionization to the total ionization cross sections of Taylor and Burke.

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Table A-1 displays the total and partial ionization cross sections at selected wavelengths between 14.25 Å and 910 Å. Cross sections at other wavelengths can be obtained by linear interpolation.

A. 2 Molecular Oxygen Cross Sections

Total absorption (and ionization) cross sections in the region 14 Å - 662 Å were derived from the data of Lee, Carlson, Judge and Ogawa (1973), Samson, Gardner and Haddad (1977), Mehlman, Ederer and Saloman (1978), and Huffman (1963). In the region 662 Å - 870 Å a least squares fit to the values of Cook and Metzger (1964) was used. The 870 Å - 1030 Å region is marked by wider, well separated peaks. Using data from Huffman (1963) a background cross section σ_b was obtained by drawing in a baseline, upon which the peak

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cross section σ_p was superimposed. Each peak area was approximated as a square wave over the same wavelength interval as the actual triangular line shape. Total abosrption and total ionization cross sections are displayed in Tables A-2 and A-3 respectively.

Branching ratios as a function of wavelength were assigned on the basis of the results of Samson, Gardner and Haddad (1977), and of Fryar and Browning (1973). Samson et al. detected nine photoionization channels, of which the last five are predissociating states. Fryar and Browning have measured the total cross section for dissociative ionization.

Between the threshold for photoionization at 1026 Å and the threshold for dissociative ionization at 662 Å, we have used the branching ratios of Samson et al. with the following exception: Samson et al. give combined values for the $a^4 \Pi_u$ and $A^2 \Pi_u$ states. We have assigned the (small) branching ratios for the $A^2 \Pi_u$ state on the basis of earlier work by Schoen (1969), and thus derived branching ratios for the $a^4 \Pi_u$ state from the combined values of Samson et al.

In the region between 303 Å and 662 Å, the total cross section for dissociative ionization of Fryar and Browning (1973) exceeds the sum of the partial cross sections for the predissociating states observed by Samson et al. To reconcile this difference we have postulated the existence

- A-3 -

of a single additional predissociating branch with threshold at 662 Å. A straightforward algorithm yields branching ratios for this (tenth) additional branch as well as renormalized branching ratios for the branches observed by Samson et al.

No measurements of the branching ratios have been reported at wavelengths shorter than 303 Å. We have arbitrarily assumed that branching ratios remain constant short of 303 Å. This assumption is of minor importance for most aeronomic applications.

Table A-4 displays branching ratios at selected wavelengths between 14 Å and 1026 Å for each of ten branches. At other wavlengths the branching ratios can be obtained by linear interpolation. It should be kept in mind that the last six branches represent dissociative ionization.

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- A-5 -Table A-4

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Branching Ratios for the Photoionization of $\mathbf{0}_2$

brancn	-	7.	r	4	•	0	1	D	N (1)	2	
Deisgnation	x ² π _g	a ⁴ IIu	A ² IIu	ь ⁴ г ₉ -	Β²Σg ⁻	$2_{\Pi_{u}}$	$c^4 \Sigma_u^-$	2 _{2u} -	2,4 ₅ -	662 å	
λ (Å)		6 2010 - 1 1 1 2010 - 1 1 2010 - 1	63 8	123.3	Branc	ching Rat	ios	2 (0) 12 946	9923 9483 	1918 - 61 1913 - 61 1915 - 61	24.98
14	0.365	0.185	0.020	0.125	0.055	0.060	0.035	0.030	0.125	0.000	2413
303	0.365	0.185		0.125					0.125	0.000	
323								0.030	0.000	0.112	
454								0.000		0.055	
461	0.435	0.225		0.120	0.055	0.060	0.035			0.050	
504							0.000			0.115	
537	0.345	0.270		0.130		0.000				0.137	
556		0.210		0.225							
573	0.365	0.250								0.030	
584		0.310		0.210	0.125					0.030	
598	0 230	0.275		0.375						0.045	
610		0.365		0.305	0.000					0.075	1.1
637	0.245	0.330		0.370							
645	0.340	0.285		0.330							
662	0.270		0.020	0.345						0.000	
684		0.468	0.050	0.000					993 993		
704	0.675	0.275									
720	0.565	0.385	0.050								
737	0.565	0.435	0.000								
774	1.000	0.000									
1026	1.000										
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A.3 Molecular Nitrogen Cross Sections

Total absorption (and ionization) cross sections in the region 100 A - 650 A were derived from the data of Lee, Carlson, Judge and Ogawa (1973) and of Samson, Haddad and Gardner (1977). The data were extrapolated from 100 A to 14 A so that consistency was obtained with the cross section measurements by Huffman (1969) at 100 Å, 68 Å, 44.6 Å and 13.4 Å. From 650 Å to 734 Å total absorption cross sections were obtained from Huffman (1969) by superimposing peak values on a baseline representing the continuum, as for molecular oxygen. From 734 Å to 986 Å cross sections were derived from the tabulated oscillator strengths of Carter (1972). Ionization yields from 650 A to the photoionization threshold at 796 Å were obtained by a least squares fit to the data of Cook and Metzger (1964). Above 1000 Å no detectable absorption was observed by Huffman, Tanaka and Larrabee (1963). Thus from 986 Å to 1030 Å the absorption cross section has been set to zero. Total absorption and total ionization cross sections are displayed in Tables A-5 and A-6 respectively.

- A-6 -

Dissociative ionization of N_2 is assumed to occur through a single channel with threshold at 509 Å. The partial cross section for dissociative ionization is obtained by multiplying the total ionization cross section by the fractional yield for dissociative ionization. The remaining part of the total ionization cross section is apportioned among five branches of N_2^+ . Fractional yields for dissociative ionization are displayed in Table A-7 for wavelengths

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between 14 Å and 509 Å. At other wavelengths the yield can be obtained by linear interpolation, with one exception: between 387 Å and 477 Å the yield, Y, is given by

$$Y = 0.0329 + 8.13 \times 10^{-6} \times (\lambda - 442)^2$$

Values for the yield for dissociative ionization were derived from the data of Wight, Van der Wiel and Brion (1976), and of Fryar and Browning (1973).

Branching ratios as a function of wavelength for five N_2^{+} branches were derived from the data of Samson, Haddad and Gardner (1977), Plummer, Gustafson, Gudat and Eastman (1977), Hamnet, Stoll and Brion (1976), and Lee (1977). The agreement among the results published by these investigators is good (generally within 10%). No measurements have been reported at wavelengths shorter than 210 Å. We have arbitrarily assumed that branching ratios remain constant short of 210 Å. This assumption is of minor importance for most aeronomic calculations. Table A-8 displays branching ratios between 14 Å and 795 Å for each of five branches. At other wavelengths the branching ratios can be obtained by linear interpolation.

- A-7 -

Table A-7

Fractional Yield for Dissociative Ionization of N2

<u>λ (Å)</u>	Yield
14	0.360
210	0.360
240	0.346
302	0.202
387*	0.033
477*	0.041
496	0.024
509	0.000

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Table	A-	8
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Branch	1	2	3	4	5
Designation .	$x^2 \Sigma_{g}^{+}$	a ² II _u	^{β²Σ⁺_u}	F ² Σ _u	² Σ _g ⁺
λ(Å)			Branching	Ratios	
14	0.271	0.275	0.110	0.064	0.278
210		0.275			0.278
240		0.345	0.110	0.064	0.210
280		0.470	0.095	0.040	0.124
300	0.271	0.470	0.110	0.074	0.075
332	0.300	0.520	0.120	0.060	0.000
428	0.460	0.460	0.080	0.000	
500	0.404	0.506	0.090		
600	0.308	0.589	0.103		
660	0.308	0.589	0.103		
660.01		0.692	0.000		
720	0.420	0.580			
747	1.000	0.000			
795	1.000				

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Branching Ratios for the Photionization of N_2

A.4 Helium Cross Sections

For helium, with a photionization threshold at 504 Å, we have used the cross sections given by Jacobs (1971). These are displayed in Table A-9.

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TABLE A-1

TOTAL AND PARTIAL PHOTOIONIZATION CROSS SECTIONS

<u>λ(Å)</u>	Total	450	2 _D o	2 _p o	4 _p e	2 _p e
14.25	0.322	0.095	0.102	0.063	2.031	0.025
30.92	0.277	0.093	6°C.0	0.058	0.027	0.021
46.40	0.261	0.078	0.083	0.055	0.025	0.020
50.30	0.423	0.123	9.140	C.08P	.0.040	0.032
75.03	0.824	6.245	0.253	0.173	0.079	6.063
90.14	1.527	0.455	0.486	0.321	n.147	0.117
135.23	2.310	0.685	.0.736	0.496	3.222	0.176
127.65	3.714	1.108	1.194	0.782	0.357	0.284
150.10	4.789	1.372	1.562	1.025	0.460	0.370
130.40	5.923	1.611	1.931	1.293	0.571	0.465
200.00	5.633	1.759	2.253	1.465	0.657	0.510
\$50.08	7.345	1.905	2.531	1.640	0.725	0.544
243.03	3.0P7	2.064	2.344	1.836	0.763	0.561
25 5 . 37	3.43?	2.154		1.547	0.818	0.556
270.50	8.915	2.245	3.210	2.061	0.353	0.532
284 . 15	9.262	2.332	3.387	2.168	1.987	0 . 487
303.78	9.719	2.451	3.533	2.316	00914	6.405
315.02	9.573	2.5.07	3.755	2.398	0.923	0.000
335.39	10.127	2.636	4.014	2.540	9.938	
349.95	10.456	2.713	4.173	2.631	0.940	
368.07	10.837	2.811	4.371	2.743	0.915	
401070	110265	2.930	4.529	2.873	00035	
413.00	110435	2.535	4.740	2.925	0.785	
435.000	11.609	3.045	4.359	2.981	0.720	
4360 00	10.500	3.052	4.964	2.984	0.000	
450000	11.100	3.109	4.957	3.025		
454.00	110307	3.167	50360	3.081		
452020	11.853	2.331	5 . 234	3.240		
4= 2000	:10765	2.295	50245	7.0234		
457.00	11.603	3.252	5.196	3.150		
45.30 70	11.503	: 0222	30150	3.131		
45000	110425	3 0 2 0 1	-50116	2.108		
450.00	11.03/3	20150	20192			
+1.20 30	11.32 J	201/2	5.071	3.077		
424000	11.242	20105	5.179	20051		
453000	1.145	1.131	5.034	7. 234		
4-7000	11.077	3-104	4 6 (5	7.001		
405000	11.000	3.035	407:5	3.0.07		
4700 30	10.517	3.045	40522	20790		
472.00	10.767	7.026	U. 971	2.622		
173.00	10 . EL 3	2.941	40773	2.250		
471.20	5.901	2.807	4.450	2.7.94		
175.11	5.0172	2.631	4.777	2.543		
47 12	:1.447	3 . 212	5.136	2.096		

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FOR ATOMIC OXYGEN (IN MEGABARNS)

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TABLE A-2

MOLECULAR OXYGEN ABSORPTION CROSS SECTIONS σ_{T} (Mb)

λ	T		σ _T	λ	σ _T	λ	σT	λ	σ _T
14.75	.29	14.40	. 29	15.01	. ? ?	15.26	.29	16.71	•29
16.77	.29	17.05	. 29	17.11	.29	18.62	.25	16.97	.29
21.40	.29	21.50	.29	22.19	.29	28.47	.30	25.79	.30
29.54	.30	73.02	.30	30.43	.30	33.74	.30	40.95	.31
43.76	.21	44.02	.31	44.16	.31	45.66	.33	46.40	.35
45.67	.76	47.87	. 35	49.22	.42	50.36	.45	50.52	.45
56.69	.44	52.30	.50	52.91	.51	54.15	.54	34.42	.55
34.70	.54	5.06	•57	55.34	.57	56.09	.59	56.92	.61
57.76	.6?	\$7.56	.53	57.68	.64	54.95	.66	55.62	.68
-0.30	•71	63.65	71	51.07	.72	61.53	•73	61.90	.74
62.070	.75	62.35	•75	52.77	.76	62.92	.76	63.15	•77
62.020	•77	63.65	.78	53.72	.78	64.11	.79	64.60	.80
65.71	.82	65071	.83	65 .85	• 34	66.30	.85	67 .14	.67
67.035	• 87	68.35	.91	59.65	.95	70.00	.96	70.54	8
76075	• 93	71.00	.99	71.54	1.01	72.31	1.02	72.63	1.03
72000	1,004	72.95	1.04	73.55	1.05	74.21	1.08	74.044	1.05
74020	1.19	75.03	1.10	75029	1.11	75.46	1.11	75.73	1.12
76.01	1.13	75046	.1.14	76.03	1.15	76.72	1.15	77 .30	1.16
77.74	1.19	73.56	1.20	78.70	1.20	75.75	1.21	75.48	1.23
75.70	1.27	R3.00	1.24	30.21	1.25	£0.55	1.26	33.94	1.27
01.16	1.27	11056	1.28	51.94	1.29	82.43	1.31	32.47	1.31
8- 0.20	1.23	33.42	1.34	33.67	1.34	24.70	1.35	34.26	1.36
04.50	1.27	14072	1.37	50.85	1.38	35.16	1.38	35.50	1.29
35067	1.41	13067	1040	96.23	3.41	86.40	1.42	31 .77	.43
86.98	1.41	F7.3C	1044	37.61	1.45	85.10	1.47	Sc .11	1.47
82.014	1.4"	53042	1.48	95.69	2 . 48	83.90	1.49	57.14	1020
05.070	1051	5 30 14	1.52	90.45	3 . 5 3	90.71	1.54	91010	10:5
91.48	Iere	72035	1:5/	91.81	1.5/	92.19	1.56	72015	1.57
76081	1001	73961	1.02	94 . 07	1.000	74027	1054	94035	1.004
740-1	1.00-	4090	1.30	9:00/	1.71	77031	1.00/	73 en1	1.77
50000	1.004	- 3045	1.71	70.03	10/1	9/012	1.76	7/051	10/0
57.04	1.79	12.71	10/0	35.63	1.37	100-53	1.70	110-94	1.56
101-57	1.50	102.11	1.71	107.01	2.00	107.15	2.01	107.17	2.61
10:05	2.09	103.34	2.16	100.01	2.04	104.76	2.11	105-24	2.15
106020	2.21	1050-2	2. 23	104.93	2.26	108.25	2.33	108-45	2.36
105 .50	2.47	165.50	1.45	110.16	1.57	110.52	2.50	111.70	2.61
111.1010	2.54	111.25	2.54	113.87	2.71	114.39	2.73	114.24	2.74
11: . 35	2.8?	115.82	2.34	116.75	2.91	117.20	2.94	120.40	3.15
121010	3.20	1:1.75	3.24	122.70	3.20	123.50	3.35	127 . 65	3.62
125.57	3.77	137.35	3.92	131.02	3.06	12 1.0 21	3.97	124.21	4.26
131020	4.27	1: 3005	5027	136.45	4.023	136.42	4.29	144.21	4.79
14:	4.53	240050	5035	155010	5.21	152.15	5.33	152.34	13
154.20	5.44	157.75	3 . 36	154.39	5.77	159.74	5.30	1 54 . 13	6.03
167.50	6032	143.17	6.37	141.55	6.47	169.92	6.42	171.006	60F 3
17 12	6065.	172072	5e71	173.10	6.72	174.53	6.32	175 0 24	6.07
17: 047	6.80	177 . 22	7.31	178.62	7.05	175.70	7.13	190.40	7.22
156071	7 . 24	151014	1.27	132.16	70:5	132.39	7.34	133.91	7.44
104010	7.2=	1:4052	7 . 47	1 34 . 7 5	1 347	185021	7052	136.60	7019
136.87	7.12	11.302.	7.73	158073	7.72	190.77	7.90	191.29	7.87
14:030	7 . 97	152036	7095	192.000	10003	105014	9.05	196.063	2.13

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TABLE A-2 (continued)

<u> </u>	σ _T	· . λ	σΤ	λ.	σT	· · · λ .	σT	λ	_ ^σ T_
197.41	P . 27	198.53	8.30	200.00	8.40	201.17	9.48	202.064	5.60
203.78	P .67	204.89	8.78	206.26	6003	206.39	3.91	207.40	°•00
208 . 35	9.07	209.63	9.17	209.75	9.18	205.93	7.19	211.22	9.30
212015	9.35	214.75	9.54	215.16	5.57	216.70	9.58	216.71	9.77
219 . 07	9.83	30.05	.9.91	221.26	9.99	221.51	10.01	223.26	10.15
223.72	10.10	274.81	10.27	225.12	10.30	227.01	10.45	227 . 47	10.49
223.74	10.69	230.65	10.75	231.55	10.83	232.50	10.91	232.34	11.01
234033	11.05	213.55	11.15	237.36	11.29	239.97	11.49	240.73	11.56
243.03	11.74	243.94	11.97	246.24	12.30	246.71	12.05	247 .13	12.07
245 023	12.24	251.10	12.39	251056	12.46	252.17	12.48	253.80	12.61
25 c . 37	12.82	255.69	12.34	257 • 48	12.91	258.40	12.98	259.50	13.06
261.08	13.19	252.95	13.32	264 .27	12 .41	264.90	13.44	270.50	13.63
271.59	13.94	272.70	13.079	274.24	14.07	275.35	14.17	275.76	14.20
270015	14.25	273.77	14.27	277.00	10.29	277027	14.51	276.40	14.29
281041	14063	274.15	14.30	235.655	11.072	288036	12.09	289 . 1	15.14
290072	15 025	251.60	15.31	292.03	15 02.5	292.3'	1.20,56	295071	12055
296.17	17.054	279050	15.//	3920/5	10.00	315002	15.51	215005	17.66
310070	17.69	317.42	17.77	2 35 0 05	17.00	3370.79	17.61	245013	17.93
360.73	18.12	364.00	13.25	7 58 . 07	10.75	421.70	17.14	UDE .00	15.21
404.00	10.27	407.00	19.21	438-00	16.27	409.30	13.26	#16.03	15.31
408000	19.31	612.60	1.9.32	E13.00	16.23	444.00	19.34	115.00	19.75
411000	19.35	417.00	14.34	417.24	15 .37	417.71	19.37	414.00	19.37
415.00	19.39	429.00	19.46	421.00	15-12	422. 10	19.44	423.03	19.45
424.00	15.49	425.00	19.50	426.03	15.53	427.000	19.55	U2F.00	19.57
425.00	10.51	420.00	15.60	430.50	15 . 61	471.00	19.51	432.00	15.0(2
122000	15.63	434000	19.54	435.00	19.54	425.77	19.55	436.19	14.65
457.000	19.65	433.00	19.57	139.00	15069	440. 00	19.70	441.00	15.72
442060	15.7=	443.00	19.78	444.00	19.31	445.00	19.84	446.000	19.88
447.000	19.51	443.00	11.74	449.00	15.07	420.00	27.00	451.00	20.02
452.00	20.04	453.00	20.35	434.000	20.03	455.00	20.10	456.00	20.11
457050	20.13	4: 9.00	20.15	4 55 . 00	21.017	450.00	20.20	451.60	20.23
402060	20.25	253.000	20030	454000	20.34	465.00	30.058	465.0%2	20039
460000	2.0.43	4(7.)0	20.47	458.00	20.31	469.10	23.56	465 . 8.0	20.59
470000	20.67	471.00	20.54	472.00	26 . 58	473.00	20.72	474.00	20.75
475000	20.00	476.00	20.34	477.00	20.33	473.20	20.92	479.03	20.55
480000	21.00	421.00	21.04	432.00	21.09	482.19	21009	485.90	21014
104.0	21.14	485000	21023	435.09	21.020	49/000	21.34	466.0J	21.029
439029	21044	444050	21.047	490000	21 .: 0	491.00	21056	492.00	21.61
472020	11007	454000	210/0	575 .00	210/9	4560 32	21055	49/000	21051
472000	21 057	4 /9 000	22014	4 79 021	20	5000.00	2011	FULSUJ	22.15
502000	22 . 6 2	505-10	22030	E 17 61	21 301	507090	22060	-100FJ	2005/
EnusE1	25.55	FE 1 . 00	20075	1 12.80	25020	542010	35.75	571.33	22040
546.1	23.03	F.P.H. 33	22.01	504.003	26 . 1. 2	408.10	24.56	606.03	26.30
605 .8.	25.1.	610.00	24.10	611.60	21 .33	512. 30	15.75	612.00	25.77
614 . 00	25 . 63	515.00	25.60	616-00	25.50	515.50	25.55	617-04	25.60
515 . 00	25 . 1.7	619.00	2- 56	636.00	25 .70	521.00	25.75	622.00	26.72
522 . 00	25 . 5 7	624.20	25.37	625.00	21 .39	625.23	25.90	12(. 0.)	25.51
621020	25 . 51	623.000	25.70	627.63	25 . 35	325.77	25.82	630.01	25.50
502000	25.72	5:2.00	2: . 51	633.000	25.050	\$34.73	23.37	135.00	25.24

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TABLE A-2 (continued)

	σ _T	λ	T	λ	σT	λ	°T_	λ	σT
366.00	11.52	6 69 . DC	11.94	£70.00	12.10	971.73	12.39	872.00	10.50
972.000	9.00	374.00	7.50	875.00	6.02	876.20	5.84	P77.00	5.65
378.00	9.49	879.00	9.31	£30.00	5.15	981.07	9.01	832.00	8.50
853.00	8.027	864.00	11.41	835.00	11.35	886.00	11.31	A87.00	11.29
694.60	11.28	889.00	11.27	890.00	11 .24	591.70	7.55	892.00	7.61
872010	7.64	904.00	7.58	875.00	7.71	396.00	7.74	A97.00	4.79
956.00	4.82	8:9.00	4.34	\$ 20.00	17.57	701.00	17.58	502.00	17.55
903.00	17 .59	904.00	17.57	504.10	17.57	935.00	17.55	906.00	4.82
907.00	17.75	503.00	17.72	9 09 . 00	17.59	910.72	17.55	\$11.00	17.60
\$12070	17.55	913.00	17.50	514.00	17.45	915.30	4.43	910.00	4.39
\$17.00	14.35	913.00	14.30	919.00	14.24	920.00	14.18	921.00	14.12
524000	14.05	923:00	3600	923.13	2.55	924.00	13.52	925.00	13.47
926.00	13.41	926.20	13.40	927.63	13.35	926.30	13.30	925.00	13.25
950.00	3.50	933.70	2.54	531.00	25 .74	932.00	25.54	933.00	25.64
932.040	25 . 62	924.00	25.60	935.00	21.5	736.30	25.51	937.00	3.27
937 .63	3.24	933.00	23.56	539.00	22.53	940.00	23.50	941.00	23.47
942030	23.44	943.00	23042	\$44.00	23 .40	940.50	23.35	945.00	39.16
:40000	30.14	94.7.00	33.13	544.00	30.11	949.00	30.10	949.74	30.09
556060	*0.0F	9-1.000	30. 37	952.00	2.55	753.00	2.54	954.00	2.53
955000	28.57	955000	2:.52	537.00	26.51	959.90	23.50	955.00	29.48
960.00	28.015	9/1.00	27 . 11	952.20	27 . 09	962.12	27.07	904.00	27.04
765.00	27 . 02	2=5.30	27.000	957.00	26 . 57	968.00	26.95	565.00	26.92
576000	26 . 8 "	971.00	25.36	\$72.60	21.46	472.50	21.75	973.000	21.53
774.CJ	21.57	\$75.00	21.37	576.20	21.34	977.00	21.50	977.03	21.83
570000	21.77	777.00	21.75	530.07	21 .71	731.03	21.67	= 32.00	21.64
922070	22.29	964.00	22.34	5 31 .00	22.31	586.00	27.78	987.00	22.74
202020	22.71	\$5.7.00	22.60	570.00	224	341.10	1.97	\$91.63	1.53
574002	1.50	593. UC	1.37	ccu.00	12.007	955.30	13.24	526.00	13.01
297.004	12.53	553040	1.72	579.00	1.67	100000	1.55	10 01 . 0	1064
1002.00	1.61	1263.06	1059	1034.03	2.13	1013.00	3.76	1006.00	3.74
1607.00	3.71	1019.00	1.47	0.05 .00	1.45	1310.30	1.42	1010.20	1.42
1011.00	1.40	1112.000	1.30	1017.00	1.5	014.00	1.24	111	1.32
1 01 6 . 70	1.20	1 217 240	1.27	018.00	1.2=	1719.00	1. 23	1020.001	1.21
1021.000	1.13	1021.000	1.18:	022.00	1.15	1123.00	1.14	1724.00	1.12
1025.000	1.00	1 025 .71	1.58	0 22.00	1.071	027.02	1.04	1020.00	1.02
12.5.00	1.001	1 0: 2.04	. 47		Sec. 1	100 2.72			
		10.000	1						

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TABLE A-3

MOLECULAR OXYGEN PHOTOIONIZATION CROSS SECTIONS σ_T (Mb)

λ	٥I	λ	σI	λ	σI	λ	۹I	λ	°I.
14.25		14.40	.29	15.01	.29	15.26	.29	16.01	.29
16.77	.29	17.05	. 29	17.11	.29	18.52	. 29	18.07	.29
21060	.29	21.30	.25	22.10	.29	28.47	.30	26 .79	.30
29.52	.30	30.02	30	30.43	.30	23.74	.20	40.95	.31
4 7 6	.31	44.62	.31	44.15	.31	45.56 .	.33	46.40	.35
40.67	.24	47.87	39	45.22	.42	50.36	.45	30.52	.45
50.69	.45	52.30	.30	52.91	.51	54.15	.54	54.42	.55
54.70	.55	53.06	· • 57	55.34	.57	56.98	.59	56.92	.61
57 . 76	.62	57.56	63	57.88	.64	58.76	.66	55.62	.68
60.30	.79	60.35	.71	61.07	.72	61.53	.73	51.90	.74
02.030	•75	62005	75	62.77	.76	62.92	.76	53.16	•77
02.30	.77	63.05	78	63.72	.7 9	54.11	.79	64.60	.80
65.21	.82	63.71	83	65 .85	.84	65.30	.85	67 . 14	.67
67 . 35	.87	63.35	•91	69.65	.75	73.39	.96	70.54	• ? 8
70.75	.99	71.00	.99	71.94	1.01	72.31	1.02	12.53	1.03
72.00	1.04	72.95	1.04	73 .5 5	1.06	74.21	1.05	74.44	1.08
74.95	1.19	75.03	1.10	75.29	1.11	75.46	1.11	75 .73	1.1?
76.01	1.13	75.48	1.14	76.63	1.15	76.94	1.15	77.30	1.16
11.74	1.19	73.56	1.20	79.70	1.20	75078	1.21	75.43	1.23
75.76	1.23	00.09	1.24	30.21	1.25	87.55	1.26	80.94	1.27
31.16	1 .27	81.56	1.28	81.94	1.29	#2.43	1.31	32.67	1.31
03.25	1.37	83.42	1.34	33 . 67	1.034	84.10	1.35	34.26	1.25
84.50	1.37	54072	1.37	84.86	1.38	65.16	1.30	62.28	1.39
85.69	1.40	1.3057	1.40	36.23	1.41	86.40	1.42	36.77	1.43
84.90	1.44	\$7.30	1044	67 .61	1 . 45	86.10	1.47	86.11	1.47
36 . 14	1. 47	83.42	1.46	88.64	1.48	85.70	1.49	39.14	1.50
85.70	1.51	~0.14	1.52	90.45	1.53	90.71	1.54	91.50	1.53
71040	1.056	51065	1.57	91.81	1.57	\$5.03	1.56	92.55	1059
92.051	1.69	53.61	1.62	74 . 07	1 . 53	94.25	1.64	94.27	1.64
94.81	1.65	\$4.90	1.56	95 .37	1 . 67	95.31	1.67	95.01	1069
56000	1060	\$ 5049	1.70	96 . 6 3	1 .7 1	97.12	1.72	97.51	1073
57057	1.74	53.12	1.75	75023	1 .73	98c50	1.76	6 20 36	1.77
77044	1079	47.71	1.79	79 . 57	1.050	107.74	1.84	100.55	1.56
101.57	1.57	102.15	1.94	173.01	2.00	103.15	2.01	102.17	2.01
102.55	2.04	103,94	2.06	104.23	2018	134.76	2.11	105.23	2015
101025	2.21	105057	2.23	106.93	2.26	108.75	2.32	106.45	2025
105.50	2043	107.95	2.46	110.55	2 . 20	11 9.52	2.50	110.76	2.51
111010	2.50	111025	2.54	113.80	2.71	114.79	2.73	114.24	2074
115.37	2.88	115.52	2.34	116.73	2091	117.20	2094	120.40	3.15
121015	3.020	121075	2.54	122.70	5.20	123.50	3.35	127 .63	2065
127 . 7	3077	137030	3.92	131.02	2026	111.21	3.57	136021	4.25
136020	4.27	125034	4 • 27	136.45	40?3	136.49	4.20	144.021	4.79
145.00	0.025	143000	5.09	150.10	5 . 21	152.13	5.33	152.024	5.33
154070	5005	15/073	70 56	1 35 . 2 3	5.70	155074	5.80	164.10	5008
10/050	5027	163017	0:37	1 58 .55	6.40	163.7?	5042	171.03	6.58
172012	6.65	177 35	3071	173019	6 .7 ?	174.53	5.32	175.24	5087
1/204/	2 004	101 1022	7.01	170.02	/035	1/90/2	7016	130.40	1.55
1000/1	7010	101014	7	1 52 01 5	1023	122039	1036	192051	7044
180-07	7.02	113.02	7.70	14:-70	7.77	100-00	7.80	156.060	7060
142 .7 .	7.01	162.95	7.36	1 33 3	5.20	106-10	7.00	146-6-	Pate
			1070		0000		20.02	1 1 6 0 0 0	

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TABLE A-3 (continued)

	<u>à</u>	٥I	λ	σI	λ	σI	λ	σI	λ	I
	157 .41		153.53	3.30	200.00	· .40	.201.10	9.46	202.64	8.60
	20:078	3.60	204.69	8.78	236.25	3.90	206.38	3.91	207.46	9.00
	206.35	5.07	207.63	9.17	239.73	5.13	209.93	9.19	211.32	. 9.30
	212.10	9.35	214.75	5.54	215.15	5.57	216.90	9.68	218.21	9.77
	215.09	7.8.9	220.08	.9.91	221.25	5.79	221.51	10.01	223.26	10.15
	222.72	10.19	224.31	10.27	225.12	11.30	227.01	10.45	227 . 47	10.49
	220.79	10.67	230.05	10.75	231.55	10.23	232.60	10.91	233.84	11.01
	234.38	11.05	235.55	11.15	237 .: 6	1: .29	239.87	11.45	240.73	11.56
	240.00	11.74	245.94	11.77	246.24	12.00	246.91	12.05	247 .13	12.07
	245.23	12.24	251.10	12.39	251.96	12.45	252.17	12.48	253.80	12.61
	256.37	12.8?	256.65	12.94	257 .48	12.51	258.40	12.98	255 .50	13.06
	261.08	13.19	262.99	13.32	264.27	12.41	264.30	13.44	270.50	13.83
	271.99	12.54	272.70	13.99	274024	14 . 39	275.35	14.17	275.75	14.20
	270015	14.23	275.77	14.27	277.00	1 - 0 ? 5	277.27	14.31	278.40	14.39
	281.41	14.67	284.15	14.30	295.85	14.92	288.34	15.09	205.17	15.14
	256.72	15.025	251.63	15.31	292.00	15 . 33	292.33	15.39	295.57	15.55
	276.17	15.59	297.50	15.77	303.78	16.00	315.02	16.51	215.03	16.51
	316020	16.55	317.93	16.59	335.05	17 . 7.1	335.39	17.32	345 .13	17.66
	345.74	17.69	347.42	17.73	345 .85	17.80	353.85	17.91	356.07	17.59
	366.76	18.17	364.80	19.25	3 52 . 07	15.35	401.70	19.14	405.00	15.021
	406.00	19.23	497.00	19.25	403.00	19.27	409.00	19.29	410.00	19.33
	411.000	19.31	412.00	19.32	413.00	19.23	414.70	17.34	415.00	19.35
	410000	19.34	417.00	17.36	417 .24	15.37	417.71	19.37	418.00	19.37
	415.00	15.39	423.00	19041	421.00	1 . 042	422.00	19.44	423.00	19.046
	424001	15.043	425.00	19.50	426000	19.53	427.00	19.55	428.00	19.57
	425.00	19.50	430.00	19.53	430.50	19 051	431.00	19.61	432.00	19.62
	455000	15063	424.00	19034	435.000	15.64	435.00	19.55	435010	15.65
	437.00	19.65	423.00	19057	435.00	1: .50	440.00	19.70	441.000	19.72
	442000	15 .75	443.00	19078	444060	15.61	445.00	19.54	445.00	19.28
•	447.000	15.91	443.00	19094	449.00	1:097	450.15	20.00	451.000	20.02
	452.00	20.04	453.00	20.06	434.00	20.00	455.03	20.10	456.00	20.11
	457013	20.11	45.3000	23015	459.00	2 017	460.00	20.20	451.00	20.23
	452000	20.25	463000	23.30	464.00	21034	465.00	20.38	465022	20.29
	466000	20041	4 0 / 0 0 0	20.4/	459.09	21 051	459010	20056	465	200:9
	4/0.00	20060	4/1000	20.54	4/2.00	20.968	4/2. 30	29.72	474.00	200/5
	4/5000	20.00	4/3000	20054	2//000	2.000	4/3010	21092	4/5.00	20035
	400000	21.40	401000	210 34	432000	21007	452019	21.004	403000	21014
	424000	21 01-	403.50	21.17	430.00	21.50	407010	21.54	488.00	21007
	403000	21.44	464.00	21.73	492000	2. 000	4710 11	21.050	492000	24.61
	4200.0	21.007	44000	22.74	473003	2. 0/ :	500.30	21033	E01.03	22.16
	190000	22.07	503-00	22.034	5 18 -00	22 800	507-53	22.68	515.6)	22.010
	5/1.14	23.57	523020	22.000	5 37 .03	2: .20	542.30	25.65	F56.00	25.40
	554 .51	25.56	553.60	25.73	5 50	24 .71	568.50	25.35	572.30	25.24
	Suleda	24.63	55 4.32	22.11	F 29.60	26 . 62	503.00	26.56	605.00	26.32
	6 05 . 5 .	26.13	61 1.00	26.10	(11.0)	25.03	612.13	25.75	613-01	25.70
	614-00	25 . 63	615.00	25440	616.00	25 .5.9	613-60	25.55	617-00	25.60
	51 00	25 . 62	613.00	25.66	620-63	21.70	521.01	23.73	622.0.1	25.79
	020050	25.63	624.30	25.97	625.00	25.49	525.29	25.50	126.00	25.51
	527 .00	25 .51	523.00	25.70	629.00	2: . 56	\$29.73	25.32	630.00	25.60
	601.00	25 .72	0:2.00	25.51	633.00	21 .50	624.00	25.37	435.00	25.24

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THUS FACE IS BEST QUALITY PRACTICABLE

TABLE A-3 (continued)

<u> </u>	I	λ	<u>σ</u> 1	λ	• <u>1</u>	λ	σI	λ	σI
536.00	25 .11	637.30	24.98	638.00	24.57	\$39.00	24.77	640.00	24.79
541:00	24.65	642.00	24.63	£43.00	24 . 53	644.30	24.64	644.13	24.64
645.00	24.66	646.00	24.69	647.00	24.73	648.00	24.76	649.00	24.78
550000	23.00	551.00	23.06	652.03	23.11	653. 10	23.14	654.00	23.16
655.00	23.14	656.00	23.15	657 . 69	23.13	657.30	23.12	658.00	23.10
659.00	23.05	663.00	22.94	651.00	22.92	661.40	22.88	602.00	22.83
665.00	22 .77	564.00	22.61	655.00	22.49	666.73	22.35	667.00	22.19
660.00	22.07	569.00	21.35	670.00	21 . 65	571.90	21.45	671.50	21.34
672073	21.27	673.00	21.30	674.00	20.75	575.00	20.49	676.00	20.22
677.00	19.53	673.00	19.54	679.00	19.32	53C. 90	19.00	630.94	18.23
641.00	18.23	631.70	13024	632.00	16.25	683.00	19.28	634.00	18.22
685.00	18.39	685.70	18.43	636.00	14.45	687.10	14.54	635.000	14.65
645.00	14.77	650.00	14.90	671.03	15.35	692.03	15.21	693.00	15.39
694.00	15.58	654.30	15 . 54	695.00	15 .79	696.70	15.01	697.00	16.25
690000	16.50	599.00	16.17	700.00	17.05	701.00	17.39	7 32 . 0 9	17.69
700.00	17 .93	703.40	10.02	7 34 . 6 3	18.15	705.00	19.32	700000	18.46
70% .00	18 .5	703.00	18.62	7 39 . 00	18.55	710.30	18.63	711.00	15.53
712.00	19.49	712.70	18.40	713.00	18.006	714.00	13.15	715.00	17.59
710000	17.74	717.00	17.45	718.00	17.14	719.50	16.96	715.00	16.78
726.00	16.20	721.00	13.14	722.03	18.71	723.00	19.21	724.03	19.64
725050	20.00	726.00	20.29	7 27 .00	20.51	728.10	29.66	725.03	20.74
7.0.00	20.75	731.00	20.70	732.07	20.57	733.00	23.38	734.03	20.11
735.00	19.79	725.00	19.37	737.00	18.70	738.00	19.36	735.000	17.74
746.00	17.04	741.00	15.31	742.00	15 .49	743.33	14066	740.00	13.64
745.00	12.61	746006	11001	747.00	10.34	740030	7.10	745.00	7.30
750.00	6.4?	7:1.00	.3.52	752.03	8.55	753.000	3.50	754.00	2.46
75:003	8.4?	7: 5.00	8.39	757.60	8.37	758.00	3.56	732.70	R.035
754000	8.34	759040	8.36	750.03	8.37	760.40	8.37	751.00	8.33
70000	2041	762.00	8 . 41	7 63 . 00	2.044	764.30	3.48	764.60	8.51
755.00	P .54	766.00	.8.50	757.00	8056	769.00	A.74	769.00	8.83
770.00	8 . 5 ?	773.40	3.62	771.00	4068	772.30	5.77	77:000	9.84
774000	2021	775000	9095	776.00	5057	776.00	9.95	777.03	10.01
776.90	10.02	779.00	10002	730.00	10.01	780.30	10.00	731003	5.58
702070	9094	783.00	7.37	734.00	5 . 6 3	785.00	7075	736.00	4046
706.40	90ć1	757.00	9.55	737.71	5040	788.00	9.45	735.00	5.32
790.00	5.69	793.21	5055	791.00	5.52	792.00	0.39	753.00	9.26
774000	.9.15	793030	9.13	796003	5.03	797.00	3045	798.00	8.99
775.000	5.50	500.00	9002	£01 .0 0	5.037	803000	9.15	.02.00	9.24
504.00	5.24	505.00	9.50	306.00	5065	307.000	9.35	200.00	10.05
805.00	10.29	817.06	10.52	811.000	11.85	912.00	11.50	913.00	11.11
514070	10.72	315.00	10035	£16.00	5.078	417030	9.67	816.00	5.027
315.00	5.9?	320.00	5059	£ 21 . 0 0	5.025	922033	7.93	455.00	7.62
524.30	7.21	925.00	7.011	636.00	6072	327 . 30	5043	N51.03	5017
925000	2.64	6:0.30	5.52	631.03	6003	3.2.11	5.71	, 30.000	6.54
834000	50.77	334020	6.34	630.00	E . 21	33 60 70	6075	837.00	5.0
431.000	5.75	529.00	5.50	540.00	5.46	341070	5.32	#42.00	5019
842.010	5.05	844000	4075	845.00	1.031	546070	40.65	P47.0C0	40:3
546000	4.47	447030	4.36	F3C.00	1.026	9:1.00	4.16	5200J	4.07
250070	2057	5: 4.30	3.39	255.000	(° e ;	356000	30/2	57023	3065
100.00	2019	0. 2000	÷=51	650.00	2.45	561075	2.00	162.00	3.03
A	1.1	864.01	3- 37	945-00	3-12	266.17	1.1.	35-00	7-12

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TABLE A-3 (continued)

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λ	σI	λ	σI	<u>λ</u>	σI	· .	. oI	λ	σI
860.00	3.13	367.00	3.15	870.00	3.17	371.00	3.18	872.00	3.20
873.00	3.22	874.00	3.24	\$75.00	3.25	976.00	3.27	\$77.0U	3.29
876.00	3.20	979.00	3.32	830.00	3.34	891.000	3.36	892.00	3.33
882.00	3.29	984.00	3.41	835.00	3.43	386. 90	3.45	• 37 . DJ	3.46
A81.00	3.49	829.00	3.49	690.00	3.50	991.00	3.51	292.00	3.52
892.00	3.53	8:4.00	3.54	P95.00	3.54	896.00	3.54	897.00	3.54
998.00	3.54	897.00	3.53	c00.00	2052	901.00	3.51	902.00	3.50
900000	3.4.0	904.00	3.46	\$ 04 .10	3.46	905.00	3.44	506.00	3.42
907.00	3.20	903.00	3.36	\$ 99 . 0 3	3 . 34	910.00	3.31	\$11.00	3.23
912.00	3.25	913.30	3.21	514.00	2.12	915.10	3.15	\$16000	3.12
917.00	3.09	918.00	3.36	\$19.00	2.03	923.90	3.00	921.00	2.97
\$22.00	2.95	923.00	2092	\$ 23 .10	2.092	924.00	2.90	925.00	2.83
926.00	2.005	926.20	2.95	927 .00	2.23	928.00	2.81	\$25.00	2.79
936.00	2.77	930.70	2.75	931.000	2.75	932.00	2.73	932.000	2071
952.40	2.077	934.00	2.69	\$35.00	2 .67	936.00	2.65	\$27.000	2.62
937 . 50	2061	939.00	2.60	°39.00	2.55	740.00	2.56	941.03	2.53
544000	2.51	943.00	2.43	\$44.00	2 .45	944.53	2.44	945.00	2.43
946.00	2.40	947.00	2037	948.00	2.34	949.00	2032	949074	2.30
\$50.00	2.29	551.00	2026	552.00	2024	953000	2.21	954.000	2019
955.000	2.15	956.00	2.14	957.00	2.12	958.00	2.10	959.00	2.03
706030	5105	\$ 1.00	2.05	\$62.00	2.033	963.00	2.02	5 511 0 0 0	2.01
505000	5.00	765000	1.39	557.000	1093	369.00	1.97	965 000	10:5
576.00	1.55	971.000	1.75	\$72.03	1.094	972.30	1.92	\$72.00	1.53
5740 PU	105?	975.00	1.91	976.00	1,99	977.00	1.85	-77.03	1.69
776 . PU	1.2.9	977.00	1097	530.00	1.35	981e70	1.30	00.205	1.62
983.00	1.89	984.30	1.78	935.00	1.76	786.10	1.74	937000	1072
936.00	1.69	919.000	1.57	\$ 70.07	1.55	991.00	1052	\$91.00	1.12
992000	1.67	993.00	1.58	594.00	1.55	993.00	1.53	972003	1.50
997	1.49	09.5.00	1.45	559.60	1044:	1000000	1.421	001000	1.40
1002.00	1.204	003.06	1.36	10 34 . 60	1.35	1005.02	1.321	006.00	1.32
1007.00	1.27:	00.600	1.25	10 99 .00	1.27:	1010.00	1.261	916.20	1.26
1011.10	1.25	1 312.30	1.24	1013.00	1.23:	1014.00	1.211	015.00	1.2 ?
1016.00	1 . 1 .	1 117.00	1.18:	1013.00	1 . 17:	1019.70	1.161	020.00	1.15
1021.00	1 .1 "	071.000	1.12	1022.00	1.12:	1023.70	1.111	.024.00	1.10
192: . 00	1 . 6 91	1 323072	. 98	10 26 . 00	1.07:	1027.00	1.061	026.00	.00
1024.00	.0.04	177.7.70	- 02						

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TABLE A-5

MOLECULAR NITROGEN ABSORPTION CROSS SECTIONS $\sigma_{\rm T}$ (Mb)

	λ	T	λ	T	λ	°T_	λ	σ _T	λ	σ _T
0	14.75	.04	14.40	. 03	15.01	.03	15.76	. 03	16.01	•04
·	11077	.04	17.05	. 94	17.11	. 34	15.52	. 05	16.97	.05
	21.60	.0%	21.80	. 26	22.10	.06	28.47	.09	28.79	•09
	29.52	.10	:0.02	.10	30.43	.10	33.74	.11	40.95	•14
	42.76	.16	44.02	.16	44.15	.16	45.65	.20	46.40	.21
	41.057	.21	47.57	•23	45.22	.24	50.35	. ?6	50.52	.25
	56059	.25	52.30	. 29	52.91	.29	54.15	.31	54.42	.32
	34070	.32	55.06	.32	35.24	.33	56.79	.34	56.92	.35
	57036	.26	57.56	36	57.68	.36	58.76	.38	59.62	.39
	40.034	.47	63.85	4 C	51.07	.41	61.57	.41	61.90	.42
	62.30	. 12	62.35	.42	62.77	.47	62.72	.43	63.10	.44
	02.30	.41	63.65	44	53.72	.44	64.11	.45	64.60	.46
	01 . 21	.45	63.71	47	65.65	.17	66.30	.48	67 .14	.49
	67.35	.49	69.35	50	65 . 65	.= 2	7.0.00	.52	70.54	.53
	70.73	.53	71.00	53	71.94	.54	72.31	.55	72.53	.55
	72.00		72.95	.35	73.55	.56	74=21	.57	74.44	.57
	74.83	.17	75.03	52	75.29		75.46	.58	75.73	.58
	10.01		75045	.59	76	.55	76.94	. 60	77.70	.60
	77.74	.67	73.50	. 61	7579		79.18	.62	75.48	.62
	15.70	. 63	52.00		90.21		81.55	.67	80.94	-64
	61.1.3	. 64	F1.55	.64	31.94	-65	\$ 2.43	.65	92.47	.6.6
		. 6.5	53.42	-54	17.67	-67	84.10	.67	84.26	.67
	44.05.4	. 69	14075	.66	34.66	.6.5	55.16	.65	85.50	.69
		- 19		- 59	26.23	- 4.9	36.40	.70	46.77	.70
	54 . 5 d	.77	57030	.71	27.61		BBATO	.71	85.11	.71
	35.412	.71	53.42	.72	96.64	.72	86.90	.72	RC.14	.72
		.77	1114	7 .1	10.45	.74	\$ 3. 71	.74	91.00	.74
	41.UE		-1-65	.75	91.41	75	92.05	.76	92.55	.76
	120-B1		53.61	.77	94.07	.73	C 4. 7E	.78	94.39	.79
	54.01	.78	14.90	.70	35.77	.7 5	45.51	.75	05.01	. 90
	- 1 Pi,		56.445		26.53	.01	97.12	. 31	97.54	
	47.57	.52	(1.12	.92	78.23	. 72	95.50	. 12	3 . 8 .	
	55.64	. 23.	59.71	. 34	96		100.54	. 87	100.053	620
	1115.5.		102.15	. 76	102.01	1.01	173.45	1.02	1 32 .17	1.62
	103.58	1.04	113.94	1. 76	1 74 . 23	4.00	104.76	1.10	164.23	1.13
	106.23	1.10	106.57	1.21	106-53	1.73	108.05	1.20	102.44	1.21
	105-50	4.37	103-44	1.30	110.54	1.13	11 3.62	1.47	115.7.5	1-44
	111.1	1 - 8 6	111.21	1.17	113-63	1.64	114.30	1.40	114.24	1.43
	115.5	1.77	143.12	1.70	114.75	1.77	117.20	1.30	120.41	1.67
	1.1.1.1.	2.02	1 21 . 75	2. 35	122.32	3-43	1270	2.16	121 045	3.70
	12.0.5	2.12	1711-15	2005	1220/0	6.54	1200 70	2.50	146.31	2.20
	123 0.7	2.70	476.24	2.10	1 31 002	2021	136.031	2.40	112.21	1.25
	441 - 04	1.00	111.14	1	100043	2 8 7 3	45.5.45	1.7	440.01	
	1450 0	7.61	457 77	2000	150011	COUL	102003	3070	132004	00/0
	1/1-0/0	4 . 6 4	167.17	40 37	100003		140.30	4029	154012	4042
	472-44	1.62	179.14	4034	172.40	- 00/	100042	5.00	175-53	4061
	172012	1000	177.70	4073	110010	4074	174070	5004	4 10 10	2013
	1/204/	5.30	464 40	5.10	171.002	1001	179074	2030	100.40	2027
	1010.1	5.57	411 -1	2040	1 38 61 5	2045	1-2037	2046	132001	2012
	184010		1. 4	2025	1440/5	5.056	152.021	Debb	126669	2064
	150.41/	1.665	1. 3020	50/1	1 50 670	5.074	150010	3690	191029	5087
	AC			7.44	7 4. 4. 1		1	0.010	TYPET	

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TABLE A-5 (continued)

λ	°T_	λ	σΤ	λ	σT	λ	σ _T	λ	σT
197.41	6 . 27	143.53	6.30	200.00	F . 4 0.	201.17	6.45	202064	é • 5 9
202.70	6.67	264.85	6.75	206.25	6.85	206.38	5.95	2 37 .46	6 . 4 3
201 .33	6.50	209.53	7.08	209.73	7.07	209.93	7.10	211.32	7.13
21.015	7 . 27	214.75	7.39	215.15	7.41	216.90	7.51	?16.21	7.59
215.09	7.64	220.08	7.71	221026	7.78	221.51	7.90	223.76	7.52
22:072	7.55	224.81	0.03	225.12	£ .03	227 . 11	8.15	227.47	9.22
262.79	8.27	230.55	8.44	231.55	3.51	232.57	9.58	232.084	+ + e 5
234.30	8.69	235.55	3.75	237.36		239.97	8.75	240.73	9.03
242013	5.14	243.94	5.25	246.24	5.26	2460 71	9.79	247 .13	7.20
247.20	9.37	2:1.10	9044	251.96	5027	252017	9.48	-2:	90:4
256.77	9.6F	255.59	9.56	2 57 .48	5.69	258.40	9.73	259.50	5.73
201.00	P . 85	242.99	5073	2 54 . 27	= 9	244050	10.01	270050	10.21
271099	10.24	272.70	10.26	274024	1 . 023	27 5 . 35	10.30	275076	10.30
276.15	10.31	275.77	10.32	277.00)	10.33	277027	10.33	274.40	10.35
281.41	10.45	264.15	10.50	235.23	1007	288.36	10.51	205017	10065
290.72	10.94	291.03	10.75	292.00	1:.00	252083	11.05	295 .57	11.13
276.17	11.21	259.50	11.37	303.78	1: 061	315072	12.006	315.05	12.26
316.20	12.45	319.83	12.73	235.05	1-007	335.39	14071	245015	15009
345074	15 .95	347.42	16.14	:49.63	16 .39	353055	15.77	252017	16055
366.76	17.26	364.30	17.69	3 56 . 07	17 0 95	401.70	20.11	435.00	20.32
406.00	20.23	407.00	20.44	405.00	20.49	429.00	20.55	410.00	20.60
411.00	22065	412.00	20.69	413.00	2 074	414.00	20.78	415.00	20.83
416000	20.10	417.00	20.93	4.17 . 24	2: •94	417071	20.96	410.00	20 . 5 9
415000	21.004	4: 0.00	21.10	421.00	21.17	422.00	21.24	423.00	21 03 2
424020	21 .4 0	425.00	21.43	425.00	21.56	427.00	21.63	425.00)	21069
425.000	21.75	420.00	21.30	430.50	21002	431.00	21034	132.00	21.57
432.00	21083	424000	21,70	135.000	2: 250	436.00	21050	436010	21093
437.00	21 . 5 7	423000	21.90	435.07	2: 0 5 0	440.00	21.90	441.03	21090
442000	21051	413000	21.92	44.00	2: 0?2	445.00	21.94	146000	21095
447.00	21 . 95	443.00	21077	449.00	21.059	450.07	22.00	451000	22.01
432000	22.05	453.00	22033	434.00	22 0 74	455.000	22.04	136.00	22.04
497.00	25.04	453.00	22033	435.00	21 203	440000	22.00	061020	21099
402010	?1.000	463.05	21071	450.07	21.015	4650 90	21.24	" 25 0 7 2	21.024
401.000	21.081	447000	21073	450.00	2: 075	449070	21072	235050	21070
476.00	21 07 7	471.00	21055	477.03	2:069	473054	21057	474.03	21067
4/5000	21	4/5000	21003	477.000	21 0 5 9	4/3010	21055	0/5000	210/9
400.00	27 07 7	45 1. 96	21075	4 42 000	21.070	482.10	21.70	40:000	21059
464.00	21.020	4	21050	436.00	2: 055	487.072	2105F	012020	21063
437010	21 024	101 00	21057	435.00	2:0/0	491000	11012	29.000	210/4
47200	1.0/	4-1000	21000	093000	4- 0:0	45 66 11	2108/	09/000	22 0 5 9
492.000	21054	457000	1109/	495021	21.099	500010	22035		22003
	22 . 4 9	503030	220 15		2. 012	507043	2 2041	-15069	20059
521010	12017		22079	23/003	22 020	542012	23014		25019
554071	23 . 13	5. 5000	23. 2.	1 20 20	2-001	206020	22011	: / 2020	2.0:1
405-9-	27.17	611.10	23011	411.00	2-011	612.20	23030	535030	2:001
6:6-00	23.15	615-20	24-14	616-00	23 47	5120 10	22012	(15 00	23014
515-00	27.10	619.30	24.20	620.00	2 30	1010050	23010	420.00J	20013
625-00	23.20	624-06	23.20	625-03	27 . 20	625-20	23.20	626.00	20020
627 - 04	27.17	623-00	23.10	625-00	27.20	\$25.73	23.20	630-03	23.20
0-1-00	23.51	6:2.00	23.21	(33 - 42	224	6-4-22	23.24	(75-00	23.25

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TABLE A-5 (continued)

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<u>}</u>	^о т	λ	σ _T	λ.	σ _T	λ	σ _T	λ	σ _T
530.00	23 .24	677.00	23.27	639.63	27 . 28	639.77	23.29	146.00	23.30
441000	22.031	54 2. 00	23.31	643.00	22.031	544. 30	23.31	644.10	27 .21
645.00	23 . 2 1	646.00	23.31	647.000	22.20	643.00	23.30	645.00	23.30
655020	23.020	651.00	23.69	652.00	24.10	653.00	24.52	654.00	24.94
55: 000	25 . 25	615000	25077	657.00	26.14	657.30	26.25	658.00	26.49
6550 0	27.53	553000	27 . 54	to1009	2/ 01/	561040	27.21	F62000	27.20
fob alli	27.14	661.00	31.72	670.01	30.69	671.00	33.96	671.51	33.84
6/	32 . 87	673.0C	23.39	674.00	27.14	575.10	35.14	476.00	35.15
577 . 20	35.17	673.00	27 . 19	679.50	27 .15	630.10	23.91	631.094	23.82
501.00	23 .82	681.70	30007	652.07	38.03	553.70	37.36	62-000	37.71
605 . PO	26 . 3 9	645076	26.25	63000	26.020	557 . 32	25.01	68:000	25 . 5 3
637000	25 064	353000	22001	691.000	22 .1 9	692.000	22.07	690000	43.49
694000	42004	663.00	43043	7 30 .03	42 041	596.00	43042	59/ 099	43045
742.00	26.52	703-40	25034	7 74 .67	22 020	715.10	16.8F	702000	22.034
767 .00	27 .56	793.00	27 . 74	739.03	25.32	710.10	23.70	711.00	29.03
712.000	25 .45	712070	29.05	713.00	25.000	714022	20.12	715.00	36 . 7 9
710.000	37 . 67	717000	37 . 23	718.00	31	713.30	71.06	715.000	11.09
726.00	31.17	7:1:00	31.03	722.00	57.17	723.70	56.92	724.00	56.57
723070	56.10	725000	55.05?	7.27 .00	54.000	725010	27 . 56	725.00	20066
730.00	25.05.0	721000	24.19	732.00	22 .73	733.00	21.32	734.000	27 . 07
785000	25.56	7:3000	20.77	737000	26032	738019	33.32	735 0 1	23071
740000	20 .115	74 3.00	27020	742000	27 025	742030	23.63	744000	22.040
756004	28.84	7:1.00	24670	252.60	21 . 7 0	753.00	17.73	754.00	17.73
755 . 20	31.59	75 5000	31.76	757.00	31 893	753.00	32.16	758 .70	32.16
755.00	25.09	7 9.40	26.09	750.000	26 . 59	769.40	30.27	761.000	30.027
702000	30.27	76.2000	30027	753.00	30.27	764.00	19.54	764060	12.64
765 800	35 6 47	765000	35647	757.00	31.047	763.00	9.72	755020	5.7?
776000	5012	773.00	56012	771000		772000	75055	772000	20089
77 - 7.1	47.40	779.00	-7-10	725-03	26.017	790-30	24.67	794-01	4/019
75:010	49.75	793.000	1.7.79	754.00	54 .P3	755.00	64.43	706000	54.83
70604c	16.25	707.00	10026	797.71	14 .26	793.70	15026	787.00	16.25
790000	20 . 21	797021	23021	771000	25.21	752.31	59.36	79:000	55.85
124075	59015	743000	25.77	796030	26097	797.77	25057	790.00	2.25
795000	7629	300000	5092	10100	5.03	302610	43.00	°0.,00	45.005
204050	117 53	JU	27075	E 05 0 C J	6.26	-17.11	21680	552000	25054
51592U	35.51	513420	3: 1	116403	75.01	517.11	• 00	810.001	•00
315074	10.	313.00	45.33	F21.07	45	322.011	.00	222.00	16.00
924070	16.00	223000	7032	8 26 . 00	6 423	327.070	15.73	P22000	15.73
91500J	15 .73	37 0. 00	. 00	831.00		332.10	10.	00.0553	
03407J		R24020	• 2 3	635.000		934070	: ?. 30		22.00
808.00	32.00	9: 9.00	3.31	846.00	F 821	541077	8031	P42000	21 .5 3
342070	2105	24000	21033	845 80 9	21.153	4450 70	1 96 97	847.00	10.57
2-2-6	13.052	5-4000	1	FSF-00	36. 12	351039	10002	057.03	1.083
535.000	53.001	150000	21064	560.00	27.444	3.1.1.7.3	26.542	565.600	9.30
360 . 10	5085	\$34.00	9036	555060	16.01	355070	16.01	Po7 . CO	54.t 3
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TABLE A-5 (continued)

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λ.	σ _T	λ	σ _T	λ	σT	·····	σ _T	. λ	σ _T
866.00	41.97	869.00	41.97	670.00	41 . 97	371.07	41.97	872.00	16.50
870.00	37 . 54	874.00	37.76	875.00	37 . 96	376.90	37.56	£77 . CU	47.87
978 . 90 4	17 . 87	879.00	47 . 37	830.00	47 . 37	381.70	47.87	832.000	63.18
9300	52.19	AF4.00	63016	CC. 263	63.13	326. 10	.00	. 37 . 0 0	45.65
300.001	76.16	287.001	76.16	870.00	5.37	351.00	9.37	892.00	45.71
893.00	45.71	894000	43.71	875.00	15.26	996000	10.26	497.00	10.25
091.000	5105?	857.001	Céedó	\$ 30.031	06.05	901000	19.11	502.00	18.11
90: . 00 :	22 .77	964.00	19.25	\$ 04 . 102	03.73	705.002	23.78	C 36 . C 3	18.04
907.00	18.1.4	903.00	10:04	505000	11.52	710.00	11.62	511000	11062
912.000	14.57	\$13.00	14.50	514.007	40.92	915.10	40.92	\$16000	40.52
517000	40.92	913.00	10.04	519.00	10.014	920.00	10.00	\$21.000	95.77
542.00 4	75.77	523.00	55.55	523.10	31.92	924.000	31.92	\$25.00	31.52
920.00	1 . 5 ?	925.20	15.03	927.000	15.03	929.00	19.03	525.00	19.03
936.00 0	54 .51	930.70	64031	\$31.00	60 051	932.00	64.51	532.000	3.13
723.40	3017	9:4.00	3.13	\$35.00	3.13	936.22	3.12	\$37.00	2094
937 .90	3.15	933000	3015	939.00	2.15	940.00:	20.77	\$ 11.0001	20.77
942.001	20.77	543.001	20.77	544.00	34.73	\$44.50	79.07E	545.00	39.73
546.00 :	19.73	947.00	39.78	548.00	.00	949.10	.00	\$49.74	
\$50.00	7.15	951.00	7.16	552.00	7.16	753.00	7.16	\$54.00	7015
155050	7.14	956.00	7.16	957.00	15 . 99	953.11	15.85	55000	15.089
966.0024	50.79	9(1.002	60.78	\$ 52.00	56.037	763.00	5 5 . 37	c 6 4 . n g	56.87
901 00 B	5.5.67	965000	56.37	957.00	62 7	768.20	53.37	559.00	53.37
972050 4	52.27	971.000	63.37	\$72.003	62.37	772.30	63.11	973.03	55.011
974000 4	55.11	975.04	50.11	576.00	61 . 11	577.00	66.11	577.003	68.11
578.00 4	50 . 11	57900L	68.11	950.00	44.22	981.00	44.22	\$92.00	44.22
CA:	14.52	004.00	44.22	085.00	41.22	386.11	14.22		

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TABLE A-6

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MOLECULAR NITROGEN PHOTOIONIZATION CROSS SECTIONS σ_{I} (Mb)

<u>}</u>	σI	λ	۰I	λ	۹I	λ	σI	λ.	σI
14.25	.03	14.40	.03	15.01	• 33	15.26	.03	16.01	.04
16.77	.04	17.05	.04	17.11	.04	18.52	. 05	18.97	.05
21.60	. 05	21.60	06	22.10	. 36	25.47	. 35	28.79	.09
25.52	.19	20.02	10	30.43	.10	33.74	•11	40.95	•14
43.76	.15	44.04	.16	40.15	.16	45.56	•20	46.40	•21
46061	.21	47.37	.23	49.22	•24	50.36	•26	50.52	.26
50.64	.24	52.30	.29	52.91	.29	54.15	• 31	54.42	.32
54.70	.32	55.00	•32	55.34	.33	56.09	.34	56.52	.35
57 .76	.35	\$7.56		57.83	.36	58.96	• 3 8	59.62	.39
60.70	•40	6).85	•40	61.07	•41	61.63	•41	61.90	•42
62.030	• 4?	42.35	. 042	62.77	•43	6 ?. 92	•43	53.16	.44
53.70	• 44	63.65	044	63.72	•44	64.11	•45	64.60	•46
05.71	.46	63.71	•47	65.85	• 47	66.30	.46	67.14	•49
67 . 30	• 49	63.05	• • 50	59.65	•52	70.00	• 52	70.54	•53
70.75	0: 3	71.000	53	71.94	054	72031	•55	72.65	055
72.90	•55	72.95	• • 55	73.55	•55	74.21	•57	74.44	•57
74.83	0.57	75.03	•58	75029	•53	75046	056	75.73	•58
73.01		76.48	59	76023	•59	76.94	•60	77.30	•60
77 .74	•67	75.56	. 001	76.20	>01	79018	•62	75.48	062
75070	•63	20.00	•63	80.21	050	80.55	•6:	80.54	•64
d1.10	• 64	1058	•64	31054	•55	82.43		82061	065
03.25	0 55	13042	.50	50.00/	100	84000	•6/	84025	00/
54050	200	40/2		34035	020	85016	060	32010	004
32067	• 6 7	1308/	607	30023	057	66.41	0/0	520/1	0/0
96.95	0/9	5/030	0/1	8/061	•/1	88019	•/1	36.11	•/1
02014	•/1	53042	0/2	48.04	0/2	55040	0/2	57014	0/2
070.5	•/ 	50014	0/4	70045	3/4	90071	.74	91010	.74
91 . 91	.76	51007	.77	94.07	-7.8	92039	.78	94.74	.79
54.81	-79	54.91	.79	35.17	.73	95.51	.75	05.51	. 5 0
54.0.2		56.44	- 50	96.53	. 31	97.12	. 31	97.51	.81
57 . 67	.87	58012	.82	38.23	.22	58.50	.8:	91.088	.63
55.44	130	59071	.R4	99.59	254	100.54	• 37	100.56	7
141051		10 2015	76	103.01	1.01	103.15	1.92	103.17	1.02
102.50	1.04	103.54	1.36	194.23	1.08	195076	1.10	135.23	1.13
106.20	1.19	105.57	.1.21	196.93	1 . 23	105.05	1.29	102.46	1.31
105.53	1.37	107090	1.39	110.50	1,43	110.62	1.42	110076	1.44
111010	1.45	111.25	1.47	113.80	1.61	114.07	1.62	114 024	1063
11:039	1.77	115.82	1.72	116.75	1.77	117020	1.50	122.40	1.97
121010	2.052	171.75	2.05	122.70	2.10	123050	2015	127 .65	2.38
125 .97	20:0	170.20	2047	131.02	2011	1-1.21	2.52	136.21	2.79
102020	2077	175034	2.30	136943	2.50	136.48	2.30	144.21	3.25
145.00	3.27	1130-5	2.50	150.10	3.51	132.15	3.7:	152.0 %	2.78
154.20	3 . 5 4	1.7.73	4.07	158 .33	11	155.74	4.20	154.13	4.42
167.50	4061	1:3017	4054	168.055	- 207	150.72	4.65	171.06	4.81
172012	4.59	172092	4.93	173.10	1.94	174033	5004	175024	5.03
175.047	5.17	177022	5.22	170.02	5 3 27	179074	5.30	180.40	5.37
126071	502R	11.1014	5.40	192015	5.45	182.39	5.46	182.051	5.52
104010	5053	114052	5053	134076	1 335	185.21	5.58	136.60	5.64
100057	5045	109020	5.71	131.0/0	5 . 74	150.00	5.30	191023	5.87

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TABLE A-6 (continued)

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	λ	I	<u>}</u>	σI	λ	σI	. λ	σI	λ	٥I
	197.41	6.23	198.53	6.30	200.00	6.40	201.19	6.48	2 32 .64	6.59
•	202.76	6.67	204.35	5075	206.26	6.85	206.3A	5.45	207 .45	6.53
	206.33	6.99	209.62	7.38	205.73	7.09	209.73	7.10	211.32	7.19
	212.15	7.23	214.75	7.39	215.16	7.41	216.00	7.51	216.21	7.59
	215.09	7.64	30.055	7.71	221.25	7.78	221.51	7.30	?22.26	7.92
	220072	7.55	224001	0.03	225 .12	8.05	227 . 01	8.19	227 . 47	E 2 2
	220 075	5.2.3	2:0.65	3.44	231.55	8.51	232.50	8.50	233.84	8.65
	234030	P.6c	233055	8.76	237 .36	5.006	235.97	8.99	246.73	9.03
	242000	9014	245.94	7.25	246024	c.56	24 60 71	9.29	247 . 18	9.30
	245023	0.37	2:1.10	5.44	231.96	ç.47	25 2 • 17	9.48	752.00	4.54
	256.37	9.65	25 5 . 69	7.56	257 .49	5069	258.47	7.73	255.50	9.73
	261.08	5.85	242.55	5.93	234.27	9.57	264.90	10.01	275.FD	10.21
	271.99	10.24	272.70	10.26	274.24	10.25	275.35	10.30	275.76	10.20
	2/0015	19.21	2/30//	10.32	211.003	11.000	277027	10.33	278.40	10.25
	281.01	10.45	284.15	10.58	235.85	10.5/	29 50 26	10.81	239.17	10.55
	290012	11.21	253.50	11.37	303.78	11.61	315.02	12.36	315.05	12.76
	716.20	12-115	319.83	12.78	335.05	16.67	335.35	14.71	346.13	15.89
	345.74	15.04	747.42	16.14	345 .85	16.39	35 3. 36	14.77	356.07	16.46
	3.0.70	17.36	364.30	17.59	2 49 003	17.55	401.70	20.11	425.00	20.32
	406.00	20.079	407.00	21.44	436.09	23.49	409.00	20.55	410.00	20.60
	411.00	20.01=	412.00	27.64	413.00	20.74	414.00	20.75	415.00	20.23
	410000	20.089	417.00	20.93	417.24	20.94	417.71	20.56	415.00	26.93
	415.00	21.004	423.00	21.10	421.00	21 . 17	422.00	21.24	#23.00	21.22
	424.00	21060	425.00	21.45	425003	21 .55	427.00	21.53	#22.CJ	21.69
	425.000	21.75	4:0.00	21.030	430.50	21 .62	431.00	21.54	432.000	21.027
	403.00	21 .E.A.	474.00	21090	425.00	21 . 50	476.00	21.90	236.10	21.50
	437.00	21 . 5 "	423.00	21.90	439.00	21.90	440.00	21.50	041.00	21.57
	442000	21 . 51	443.00	21.72	444.00	21092	445.00	21.94	446.00	21095
	447 .00	21 . 55	443.00	21.97	449.00	21.079	450.00	22.00	001.00	22.01
	452.000	35 ° 6 5	453.00	22.03	034.00	22004	435.00	22.04	436.00	22004
	437.00	22 . 64	453030	22.03	455.00	22 . 32	460.73	55.00	461.00	21.93
	452.00	21 . 95	467.000	21071	4 51 . 00	21	465.00	21.34	465.22	21.64
	460.00	21.81	467.00	21.70	458.00	21 075	469.73	71.72	065.80	21.070
	4/0.00	210/"	4/1000	21057	4/2003	21053	4/3000	2105/	074.20	2100/
	4/2.00	21 . 2	4/5000	21 668	477003	21 009	4/0000	21.00:	427 03	210/0
	430000	21.40	471000	11.28	452 000	21.44	432010	21.0/0	451.000	21.63
	145.60	21.67	4	21.26	199.00	21.70	467 0 10	21.70	195-00	21.34
	407000	21.77	4.7050	21.30	454.00	21 . 43	4910 33	21.32	452.00	21.60
	445.000	21.54	459.00	21.37	4 19 .27	24 .63	500.00	22.000	501.00	22.03
	562.000	22.55	503.000	22.38	504.00	22 . 12	507.90	22.46	515.60	22.459
	521014	25.013	523030	2: . 34	537.063	25 .30	512.80	25.13	530.04	25. 10
	5:4.51	24 .7 11	55 3000	24052	552.80	24.02	543.50	23.77	572.030	23.57
	580.40	23 . 19	524032	22021	599.60	23.11	563.20	19.65	605.00	18.64
	505.85	18064	617.000	15.54	611.00	15064	612.000	13.64	613.00	13.64
	614 . 10	18.65	6:5.00	18.55	616.00	15.000	515050	18.66	617.000	19.67
	510000	15 . 67	6: 3000	10068	620.00	1-169	521.10	18055	1:2.10	18.70
	523050	13.77	654.00	15.71	62= .00	18 372	525 . 25	13.72	52: . 00	11.073
	621050	15.74	623000	18.75	629.00	10 .77	625 .73	18.78	07.253	18 .79
	53: . 00	15.11	6:2000	15034	632 . 49	1	6340 30	13.30	135.00	16.53

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TABLE A-6 (continued)

	I	*		<u> </u>	I	λ	σI	λ	σI
600000	13.57	637.00	19.00	£38.00	15.04	639.00	19.05	646.00	19.11
641.00	19.15	642.00	19.19	643.00	15.22	644.00	19.26	644.10	19.26
645000	10.79	646.00	19.33	647.00	19.37	548.70.	17.41	£45.00	19.45
650.00	19.52	651.00	19.99	652.00	20.47	653.00	20.96	654.00	21.43
655.00	21.89	655.00	22.31	657.00	22.70	637.30	22.81	659.00	23.05
655.000	23.23	669.01	23.55	651.00	23.69	561.40	23.73	662.00	22.75
552.00	22.79	664.00	20074	665.00	23.65	666.00	23.53	667.00	22.33
660.00	23.21	669.00	26. 30	670.00	25 .37	571.00	28.32	\$71.50	29.021
672.00	21.09	673.00	27.85	674.00	22.03	675.00	23.27	676.00	22.23
571070	28.40	673.00	22.05	679.00	22.011	530.00	19.53	620.94	19.50
661.00	19.57	611.70	31.22	692.00	31.21	683. 22	31.13	534.000	31.03
685.70	21.73	6.85.70	21.62	636.09	21 . 53	537.00	21.42	632.00	21.26
685.60	21.10	690.00	15.32	691.00	16 . 19	592.00	13.06	693.00	35.52
694.00	35.39	6-4.30	35.35	675.00	35.23	595.77	35.18	697 . 0 3	35.11
556.00	20.31	699.00	20.33	790.00	20.33	701.90	27.47	792.00	20.58
700.00	20.71	703.40	23.77	734.00	20.87	705.00	21.04	796.00	21.25
707.00	2104?	709.00	21.62	799.07	21 . 23	710.00	21.98	711.00	22.23
71:000	22.43	712.70	22.36	713.00	22 . 61	714.00	22.77	715.00	27.71
716.00	27 . 11	717.00	27 . SR	718.00	23 . 16	718.50	23.16	715.00	23016
726.00	23 .12	721.00	23.03	722.00	42.035	723.00	42.12	721.000	41.053
725.00	41.47	720000	41.05	727.03	40.54	718.00	20.48	725.000	15.77
730090	12056	721.00	18.03	732.00	17.034	7:3.30	16.01	734.00	20.41
70:000	5.75	725000	25 .17	737.09	23.79	738.13	20.12	735.03	25.25
740.00	26.43	741.000	25.73	742.09	24 . 59	743.00	17.74	744.00	22.76
745 .00	21.51	745000	20.29	747.00	1:016	718.90	13.50	745.00	16.78
700.00	16060	751000	14.23	732.00	14055	7: 3. 70	39.00	754.00	11.87
735000	19.55	755.00	17.72	737.000	15.030	753.00	20.16	738.70	20.28
755.00	16.49	759040	16.55	760.00	16.03	760.40	19.3t	761.00	15.045
7.62.03	15.62	762.000	17062	753.03	15 .73	764.00	12.27	764060	12.33
105000	23 . 5 ?	755000	23057	7 57 .00	22 . 91	768.10	6.55	755.00	6.59
770.00	1.061	770.40	6.52	771.00	6.63	772.73	18.35	773.00	12036
774070	12.34	775.06	13.30	776.03	24.58	77 6. 39	31.55	777 . 03	31078
770000	29047	779.00	29.19	730.00	15 . 17	780.30	15.14	781.00	15.03
782070	20.83	753.00	24.77	794.00	39.31	785.30	29.28	736.00	35.27
765000	9.65	707000	9.35	737.71	9.35	708.10	9.85	735.00	5.85
790.00	17.79	750021	17.70	791.03	18.12	792.00	23.25	792.00	26.59
7	47.04	765 30	7 14						

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TABLE A-9

HELIUM PHOTOIONIZATION CROSS SECTIONS σ_{T} (Mb)

λ	۰I	<u>}</u>	٥I	λ	۹I	٦	σI	\$	۹I
14.25	.05	14.40	. 05	15.01	.05	15.26	• 05	16.01	.05
10.77	.05	17.05	. 96	17.11	. 25	18.5?	.06	16.97	.06
.21.60	.07	71.80	.07	22.10	.07	28.47	.08	28.79	.09
25.52	.09	20.02	.05	30.43	.09	33.74	.10	40.95	.12
42.70	.1?	44.02	13	44.16	.13	45.66	.13	46.40	.13
46.47	.13	47.37	.13	49.22	.14	50.36	14	50.52	.14
50.65	014	52.30	.15	52.91	.15	54.15	.15	54.42	.15
54.70	.15	55.06	.15	35 . 34	.15	5 . 38	.16	56.92	.16
57.36	.16	57.56	•16	37 . 68	.15	58.95	.16	55.62	.17
65030	•17	60.05	.17	51.07	•17	61.53	•17	61.90	.17
62.30	• 17	62.35	• 17	52.77	.17	52.92	•17	53.16	•17
63.30	•17	63.65	•18	63 . 7 2	•18	64.11	.18	54.60	.19
05.21	.19	65.71	.18	65 . 25	•13	66.73	.18	67.14	.18
67 .25	•19	62.35	.19	59.65	.19	70.00	.19	70.54	•19
70.75	.19	71.00	• 19	71.94	•27	72.31	•20	72.63	.20
.72.80	.20	72.95	• • 20	73.55	•20	74.21	• 20	74.44	•20
74085	20	75.02	• •21	75.29	•71	75.46	•21	75.73	•21
70.01	21	75046	•21	76.83	•21	76.74	•21	77.30	•21
77074	•21	73.53	•21	78.70	•21	75.74	• 22	79.40	•22
79076	•23	60.00	• 22	30.21	•22	80.35	• 2?	£0.04	•22
81010		81.58	• 22	31.54	• 22	82.43	• 22	32.67	•23
82.25	•23	13042	• 23	93 . 67	•23	£4000	•23	84.26	•23
84.50	.23	64072	• 23	34.86	•23	35.16	• 22	85.50	•23
35.64	.23	85.97	•23	36.23	•23	96.40	•23	86.77	•24
06.50	•20	87.30	•24	37.61	024	88.10	•24	86.11	•24
00014	•24	83042	•24	88.64	\$24	35.70	•24	09.14	•24
85.70	•24	50014	• 24	70.45	•25	\$0.71	• 25	51.00	025
91.006	•25	\$1055	•25	91.c1	•25	92.39	• 25	92.55	•25
92081	• 25	\$3.51	• 25	74.07	•25	\$ 4 . 25	• 26	94.39	026
54031	024	54095	• 26	95037	•26	25.51	• 26	55081	•25
76 350	025	20045	• 26	76 . 6 3	• 25	57.12	•26	57.51	•26
9/0:/	015	93012	e 21	75023	121	93059	021	75.83	021
25044	027	59071	• 27	99.059	027	100.54	• 25	100.55	•25
102.0-7	079	102010	• 29	200011	20	103015	• 30	102.01/	0:0
102050	021	103094		1 16023	0.21	104075	0.52	105.23	022
106025	000	1.3503/		1 36 053	• 34	138035	0 32	102.40	0:5
1050-0	024	11.9070	e 5/	1110:5	027	110.52	0.37	110/6	0.67
1.1.016	•24	111021	• • • •	113.50	047	114.79	.41	114.24	041
115039		115032	. 44	116 075	040	11/620	044	120.49	•47
121015	041	1/10/9	• + 6	1220/0	043	123057	• • • •	127.65	0.4
129 0 3/	0:5	1:0030	020	131.02	0:1	131021	• 5/	136.21	.62
100020		10 50 34	.54	132045	062	106045	• 62	144 021	0/0
145070	0/1	467.75	6/3	1.50020	0/5	152017	0/0	1:20:4	0/9
141-50	1.30	1/3.13		1 50.003	054	1/0 30	• 35	174 013	0 7 5
173-1	070	173.01/	071	1 32 0 3 5	• • 1	150072	0.1	171005	053
175-47	.44	177.30		176-02		179-74		130-10	1.00
100-71	1.00	181-14	1 - 10	1 12 - 1 /	1.04	197.70	1.04	497.01	1.07
184-10	1.07	116-35	1.032	1 20 - 74	1.001	165-24	1.001	126-63	1.06
125-97	1.05	189	1. 17	138.70	1.14	190-22	1.004	131-24	1.11
142.33	1.12	112-40	1.13	123.50	1.14	154-10	1.1/	106-63	1.10

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TABLE A-9 (continued)

λ	σI	λ	σI	λ	σI	. λ	۹I	λ	σI
197.41	1.20	103.53	1.22	200.00	1.24	201.19	1.26	202.64	1.29
202.70	1.31	204.29	1.34	206 26	1.36	206.38	1.37	207.46	1.39
200.33	1.41	207.62	1.44	235.78	1.44	209.93	1.45	211.32	1.48
212015	1.50	214.75	1.55	215.15	1.15	216.93	1.59	218.21	1.61
215.95	1.6?	223.000	1.53	221.25	: . 64	221.51	1.55	222 .26	1.66
223072	1.67	224.31	1.64	225.12	5	227.01	1.70	227.47	1.70
220079	1.72	273.55	1.75	231.55	1.75	232.60	1.78	203.84	1.087
234075	1.81	235.55	1.63	237.35	:. 95	239.37	1.50	246.75	1.52
240.000	1.55	245074	2.00	246.24	2.01	245.91	2.02	:47 .1 à	2.02
245.23	2.05	251.10	2. 38	25: .96	2.19	25 2.17	2.10	253.80	2.12
256 .37	2.15	256.65	2.17	257.48	2018	258.40	2.25	255.50	2.22
261.08	2.25	262055	2020	264.27	20:3	264.90	2.31	270.50	2.42
271.59	2.44	272.70	2.46	274 .24	2.49	275.35	2.51	275.76	2.51
276.15	2.52	275.77	2.33	277.00	2.54	277.27	2.34	276.40	2.56
281.41	2.6?	214.15	2.57	285.65	2.71	288.36	2.75	289 . 17	2.77
290.72	2.60	291.63	2.91	292.00	: .22	292.83	2.84	295.57	2.89
296.17	2.90	257.50	2.96	203.78	3.04	315.72	3.24	715.03	3.26
316.20	3.28	319.53	3.35	235.05	3067	335.39	3.58	345.13	3.88
345 .74	3.89	347042	3.72	249.85	2057	353.96	4.03	356.07	4.07
360.7é	4.15	3 5 4 • 30	4.55	3 68 . 97	= .2R	401.70	5.55	405.00	5.87
406000	5.6?	427.00	5.37	403.00	£ . [?	439.30	6.07	410.00	6.11
413.00	6.015	4:2000	6.21	413.60	6.25	414.00	5.25	415.00	6.33
416000	6.27	417.00	0.41	417 .24	6.42	417.71	6.44	412.00	6.45
415.00	5.4.7	423.30	6.52	421.00	6055	422.00	6.35	423.00	6.62
424.00	C . 65	423000	6.60	426.00	c .71	427.000	6.74	226.00	5.76
425.000	6.79	43 7. 30	6.91	430.50	6 : 53	431.00	6.94	432.00	6.85
43:000	4.83	424000	6.90	435.00	6033	436010	6.94	436 • 10	5.94
407010	5.55	423.33	6.76	434.000	f . c .	440.00	7 . 01	"41.00	7.02
442.00	7.04	445.00	7.05	444.00	7.05	445000	7.07	442.00	7.09
447000	7.17	403000	7.11	449.00	7 012	45 0. 30	7.12	451.00	7.13
452000	7.14	4:3.00	7.15	454.00	7 . 15	455.70	7.16	456.00	7017
457000	7019	453.00	1.13	224000	7019	460.00	7.19	451070	7.20
462.00	7020	453000	7.20	464.00	7.021	465.70	7 . 21	465.022	7.21
466.00	7 .22	467.00	7022	458.00	7 .22	469000	7.022	465023	7.23
470000	7024	471.00	7.23	472.00	7.025	173070	7.24	474.03	7.24
475.00	7.024	475030	7024	477.60	7 .25	473.00	7.25	475.00	7.25
450.00	7025	41.1011	7 16	432.00	1 325	452010	1016	432000	1025
434000	7 00	4-3000	1027	436.00	1 323	437030	7 7 7 7	136010	1029
4070.00	7.34	46 1 30	7.20	479.09	10.0	491000	7 30	492000	7.35
4500.00	7.35	4	7.34	435-27	7 333	330-30	7.37	F 01 - C -	7.30
50% -00	7.00	503.00	7.14	5 34 .00	- 10		/ 80/		
	λ 197.41 202.7d 212.15 215.75 222.075 222.075 243.25 243.25 243.25 256.75 256.75 256.75 256.25 257.55	λ σ_I 197.411.20202.731.31202.331.41212.151.50215.051.62225.721.67225.721.67225.721.67234.751.81245.751.55245.232.05256.372.15261.082.25271.592.44276.152.52281.412.62296.722.60296.742.90316.203.28345.743.69366.764.15406.015.52411.606.15425.705.47424.006.65425.007.64452.007.619452.007.20464.007.22475.007.27435.707.27435.707.27435.707.27435.707.27435.707.255.52.717.27455.707.25	λ σ_I λ 197.411.201.63.53202.731.31204.89202.331.41207.62212.151.50214.75215.051.62223.02223.721.67274.31225.721.67274.31225.721.67274.31225.721.67274.31225.721.67274.31225.721.67274.31225.721.55245.55245.731.81235.55245.732.15256.65261.062.25262.55271.592.44272.70276.152.57257.677281.412.62274.15296.722.60291.63296.742.90257.50316.203.28319.53345.743.69247.42366.764.17364.30406.005.52407.00415.006.37417.00415.006.5442.50424.006.6542.500425.007.6445.00447.007.61945.00447.007.61945.00447.007.22467.00452.007.25461.00452.007.25461.00452.007.25461.00452.007.25461.00452.007.25451.00452.007.25451.00453.007.25451.00453.00	λ σ_I λ σ_I 197.411.201.3.531.22202.731.31204.891.34204.331.41207.621.44212.151.50214.751.55215.051.62223.061.63225.721.67274.311.66226.751.81235.551.63245.751.81235.551.63245.751.81235.551.63245.751.55245.742.00245.252.05251.162.98256.372.15256.652.17261.082.25262.552.26271.592.44272.702.46276.152.57255.502.62271.592.44272.702.46276.152.57257.6772.33281.412.622.74.152.67296.722.60291.632.96316.203.29319.533.35345.743.69347.423.72366.764.153.64.804.22406.015.52407.005.57411.606.16412.6006.52424.006.65425.006.61425.006.79427.005.57416.006.79427.006.52424.006.65425.006.61425.006.79425.007.05424.006.65425.007.05424.00 <td< td=""><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td></td<>	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

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APPENDIX B

B-1

THE DIFFUSIVE TRANSPORT MODEL

The model used for the diffusive transport of atomic oxygen ions is essentially that of Schunk and Walker (1973). There are two relevant equations, the first of which is the equation of continuity

$$\frac{\partial n_{j}}{\partial t} + \nabla \cdot (n_{j} \underline{v}_{i}) = P_{j} - L_{j}$$
(B-1)

where n_j is the number density of species j, \underline{v}_j is the drift velocity, P_j is the production rate, and L_j is the loss rate. The second relevant equation is the equation of motion. If thermal diffusion, viscosity, and non-linear acceleration terms are neglected, the particle drift velocities may be obtained by solving the equations

$$\nabla p_i - n_j m_j \underline{G} - n_j \underline{e}_j \underline{E} = n_j m_j \underline{\Sigma} r_{jk} (\underline{v_k} - \underline{v_j})$$
 (B-2)

where $P_j = n_j kT_j$ is the partial pressure for species j, T_j is its temperature, m_j its mass, e_j its charge, <u>G</u> is the acceleration due to gravity, <u>E</u> is the electric field, k is Boltzmann's constant, and r_{jk} is the momentum transfer collision frequency of species j with species k. Equation (B-2) is valid for both electrons and ions. Using the subscripts i and j to denote ions, n and m to denote neutrals, e to denote electrons, and the convention that a sum over subscript k is over all particles, equation (B-2) takes the following explicit form for electrons:

This equation determines the electric field:

$$e = \frac{1}{ne} \left[-\nabla pe + neme G + neme \Sigma rek (v_e - v_e) \right] \quad (B-4)$$

B-2

where $e_{\Xi^-|e_e|}$. The electric field can be eliminated from (B-2) with the help of (B-4). If the neutral atmosphere is assumed stationary terms of order m_e/m_j are neglected, and ion-ion and ion-electron collision frequencies are neglected (compared to ion-neutral collision frequencies), the equation for a single ion (0⁺ in this instance) reduces to

$$\underline{v}_{i} = -\frac{kT_{i}}{m_{i}r_{i}n^{*}} \left[\frac{1}{n_{i}} \nabla n_{i} + \frac{1}{T_{i}} \nabla T_{i} - \frac{m_{i}}{kT_{i}} \frac{G}{G} + \frac{T_{e}}{n_{e}T_{i}} \nabla n_{e} + \frac{1}{T_{i}} \nabla T_{e} \right]_{(B-5)}$$

where $r_{in} = r_{in} r_{in}$ is the effective ion-neutral collision frequency. For the vertical component, the equation for the drift velocity becomes

$$V_{3} = -\frac{1}{n} D \left[\frac{dn}{d3} + n \left[\frac{1}{T} \frac{d(T_{e}+T)}{d3} + \frac{mq}{kT} \right] + \frac{n}{ne} \frac{T_{e}}{T} \frac{dn_{e}}{d3} \right]$$
(B-6)

where $D=\frac{kT}{mT^*}$, and the subscripts have been dropped from quantities that refer to the ion. It can be shown that, in the presence of a magnetic field, the diffusion coefficient D is reduced by the factor $\sin^2 I$, where I is the dip angle. If (B-6) is substituted in (B-1), and the time derivative is set to zero, the resulting diffusion equation is one of second order in the ion density n.