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Coordinate Conversion Technique for OTH
Backscatter Radar,

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TERENCE J. / ELKINS
JOSEPH / GIBBS

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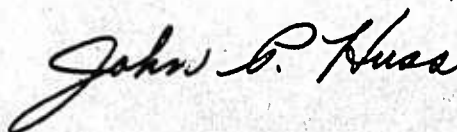
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A radio propagation simulation computer program, known as WIMP (World-Wide Ionospheric Modelling Program), has been studied and documented. The purpose of the program is to permit the transformation from Over-The-Horizon (OTH) Backscatter radar coordinates to geographic coordinates, given a vertical incidence and a backscatter ionogram measured at the radar site. The program consists of a three-dimensional ionospheric modelling algorithm, which contains a provision for updating on the basis of the ionograms, followed by a ray-tracing procedure. These algorithms have		

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been deduced from a program source deck and the program structure has been documented in terms of mathematical algorithms and flow charts, together with program listings.

The algorithms have been compared with others in use at RADC and quantitative results of this comparison are presented. These consist of ionospheric model comparisons for representative ranges of the model parameters. Finally, a measured backscatter ionogram is simulated, using the RADC program, and the ionospheric structure along the sounder boresight is deduced.

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Coordinate Conversion Technique for OTH Backscatter Radar

1. INTRODUCTION

The WIMP Program is a complex algorithm which purports to permit accurate conversion from radar target range coordinates to geographic target coordinates in OTH Backscatter HF radar applications; the complexity is fundamentally due to a deeply developed iterative and reiterative algorithm that ultimately involves the user. The program consists of three main components:

(a) A set of subprograms which construct a three-dimensional three-layer ionospheric model.

(b) A set of subprograms which simulate HF radio wave propagation in the ionosphere constructed in (a).

(c) One of three driving programs controlling the calling sequence to the radio wave propagation simulator in (b); these driving programs perform the following tasks: (1) From a given ionosphere, generate the leading edge of a simulated oblique ionogram including scale factors to the F_2 -layer parameters to force agreement with a given vertical ionogram; (2) from a comparison of the simulation in (1) to a given oblique ionogram generate range gradient factors to apply to $f_o F_2$ and $M(3000)F_2$ to force agreement; (3) from the final ionosphere generated in (1) and (2), simulate predicted radio frequency propagation paths, from which range vs group path functions may be tabulated.

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We first describe in some detail the WIMP three-dimensional three-layer ionospheric model, followed by a general description of the radio wave propagation simulation subprogram (ray-tracing algorithm). A functional description is given of the three driving programs; the operating instructions for their use are included next.

Program block diagrams, flow charts, and program listings are included in Appendixes A, B, and C.

Comparisons have been made of the results of the WIMP ray tracings with techniques developed at RADC. The description and results of these studies are reported in Sections 19 through 21.

2. THE WIMP 3-D IONOSPHERIC MODEL

A complete three-dimensional ionospheric model generally consists of three fundamental aspects: (1) How many distinct layers are to be included, (2) How shall the layer parameters be modelled, (3) How shall the electron density profile be erected from the modelled parameters? A collateral question, equally important is, what ray-tracing technique is to be used, that is, which aspect dominates the simulation of HF propagation? To put the following discussion in proper perspective the latter question will be considered here in general, reserving a more detailed treatment to a latter section.

The WIMP ray-tracing algorithm, SUBROUTINE TRISL, is a control point technique based on layer parameters as in the ITS-78 program¹ and the DEVAN program.^{2,3} The treatment of gradients of electron density, however, differs: ITS-78 does not consider gradients explicitly, DEVAN constructs an equivalent tilted reflecting surface from variations in virtual height, while WIMP constructs the tilt of the reflecting layer from the gradients of electron density. The predictions of the WIMP model are primarily sensitive to the layer parameter predictions, and only weakly sensitive to the electron density profile model. This latter dependence only enters the calculation at the reflection point (which generally is within the F_2 layer), and involves the horizontal gradients of the electron density which are determined primarily by the gradients of the F_2 -layer parameters.

The WIMP model ray tracing considers three distinct layers, E, F_1 , and F_2 ; an optional D-layer tail may be appended to the E layer. The E-layer critical

1. Barghausen, A. F., et al (1969) Predicting Long-Term Operational Parameters of High-Frequency Sky-Wave Telecommunication Systems, ESSA Technical Report FRL 110-ITS-78, Institute for Telecommunication Sciences, Boulder, CO.
2. Beckwith, R. I., Bailey, A. D., and Rao, N. N. (1972) An Investigation of Directional Propagation Effects in High-Frequency Radio Source Location, RRL Publication No. 409.
3. Beckwith, R. I. (1973) A Computer Program for the Rapid Prediction of Angles of Arrival of HF Radio Waves, RRL Publication No. 442.

frequency is determined from the local solar zenith angle. The model employed for the latter is sufficiently unique to describe in some detail below. The F_1 critical frequency is 25 percent larger than f_oE with an additional 0.5 MHz.

The ITS model provides predictions for the F_2 critical frequency and M(3000) factor. These parameters may be modified by ad hoc scale factors to force agreement with a given vertical ionogram, and ad hoc gradient factors to force agreement with a given oblique ionogram. The F_2 semithickness is determined from a linear sunspot model. All parameters thus far mentioned are used to generate the F_2 -layer height.

The F_1 layer is fitted between the E and F_2 layers such that the F_1 bottom coincides with the E-layer height and the F_1 -layer height coincides with the F_2 -layer bottom.

A more detailed description of the layer parameters and electron density model follows.

3. MODEL FOR SOLAR ZENITH ANGLE

The model for f_oE requires the solar zenith angle. From the law of cosines of a spherical triangle, this quantity is given by:

$$\cos Z = \sin \delta \sin \theta + \cos \delta \cos \theta \cos (\phi - \phi_s), \quad (1)$$

where

- Z is the solar zenith angle,
- δ is the solar declination (=latitude of the subsolar point),
- ϕ_s is the east longitude of the subsolar point,
- θ is the geographic latitude of the field point,
- ϕ is the east longitude of the subsolar point.

The field point (θ, ϕ) is given, and the subsolar point (δ, ϕ_s) is required.

The subsolar point may be determined from the solution of the Kepler problem using mean elements from the American Ephemeris and Nautical Almanac. Such a solution, to second order in the eccentricity of the earth's orbit and neglecting lunar perturbations, produces an ephemeris accurate to within a nautical mile.

Alternatively, a simplified model for the solar ephemeris may be constructed, accurate to one degree of arc, as follows:

$$\delta = E \sin \Lambda, \quad \Lambda = 2\pi(d-80)/365.25, \quad (2)$$

$$\phi_s = \pi - UT,$$

where, E is the obliquity of the earth's equator ($=23.45$), Λ is the mean longitude of the sun measured in the ecliptic counterclockwise from the first point of Aries, UT is the universal time, and d the day of year.

Clearly, models between these two may be constructed; in particular, the annual variation of the equation of time may be modelled as a correction to the subsolar longitude. (The equation of time is the correction to be added to "sundial time" to reduce it to local mean time.) Such an approach is used in the WIMP program, with the following algorithm implemented in subroutine PTHP each time it is called. The solar declination ("zenith correction angle for day of year") is approximated by:

$$\delta' = E \sin (2\pi(d-82.5)/364) . \quad (3)$$

The equation of time in hours is modelled by:

$$X_j = aY^* [A_1/(B_1 + X_1)] - [A_2/(B_2 + X_2)] , \quad (4)$$

where

$$\begin{aligned} a &= 0.0235 \text{ hours;} \\ Y &= +1. , X_2 = d + 21. , \quad 0.0 < d < 162.5 ; \\ Y &= -1. , X_2 = 344.5 - d, \quad 162.5 \leq d < 344.5 ; \\ Y &= +1. , X_2 = d - 344.5, \quad 344.5 \leq d < 366.5 ; \\ X_1 &= (X_2/45.)^3 ; \\ A_1 &= 64. , A_2 = 240. , B_1 = 4. , B_2 = 15. \end{aligned}$$

The following angle is defined, X_j being converted to radians:

$$D = \phi' + X_j - \phi , \quad (5)$$

where

$$\phi' = \pi - UT, \quad UT \geq \pi ,$$

$$\phi' = \pi + UT, \quad UT < \pi .$$

The following approximation to the solar zenith angle is constructed:

$$Z_a^2 = \left[(D \cdot \cos(0.6(\phi + \delta'))) \right]^2 + (\theta - \delta')^2 , \quad (6)$$

and the cosine of the solar zenith angle is approximated by:

$$\cos Z = \cos (0.932 Z_a) . \quad (7)$$

In the above description, angles are considered in radians, including UT; furthermore, longitudes are conventionally taken to be positive east. In the coding of PTHP, angles are conventionally in degrees, UT in hours, and longitudes are positive west.

4. MODEL FOR THE E-LAYER PARAMETERS

The E-layer critical frequency f_E , layer height h_E , semithickness y_E , and bottom altitude h_b are required. If the simple parabolic E-layer model is selected,

$$\begin{aligned} h_b &= 100 \text{ km}, \\ h_E &= 115 \text{ km}, \\ y_E &= 15 \text{ km}. \end{aligned} \quad (8a)$$

If, on the other hand, the "parabolic E- with D-layer tail" electron density model is selected,

$$\begin{aligned} h_b &= 100 - 4 \cdot F_1 F_2, \\ h_E &= 115 \text{ km}, \\ y_E &= h_E - h_b. \end{aligned} \quad (8b)$$

where

$$\begin{aligned} F_1 &= 1 - (1 - R/3000)^2 & R < 6000 \text{ km}; \\ F_1 &= 0 & R \geq 6000 \text{ km}; \\ F_2 &= \cos(A) & A < \pi/2; \\ F_2 &= 0 & A \geq \pi/2; \\ R &= \text{DIST} (\theta, \phi, 76.0^\circ \text{ N}, 102.0^\circ \text{ W}); \\ A &= \phi + \frac{1}{2} |t - \pi| - \frac{1}{2} \pi; \end{aligned}$$

and (θ, ϕ) is the geographic north latitude and east longitude of the field point; DIST is the great circle distance (in km) between the two points specified in the argument list.

The critical frequency f_E is modelled from the sunspot number N_S and the cosine of the solar zenith angle $\cos Z$ [as modelled by Eq. (7)]. Let

$$C_1 = \frac{1}{4} (1 + \cos Z)^2, \quad S_1 = (1 + 0.004 N_S)^{\frac{1}{2}},$$

$$f_n = 0.75 S_1 C_1, \quad f_x = 3.17 S_1 (\cos Z)^a, \quad (9a)$$

$$f_d = (f_x^2 + f_n^2)^{\frac{1}{2}}, \quad a = 1/3.775.$$

Then, at night ($\cos Z$ negative) f_E is given by f_n ; during the day ($\cos Z$ positive) f_E is given by f_d , unless f_d exceeds f_2 (f_oF_2 as modelled by the ITS-78 model) in which case f_n is taken. Furthermore, f_E is constrained not to exceed

$$f_{E \max} = (0.99 f_2 - 0.5)/1.26. \quad (9b)$$

5. MODEL FOR THE F_1 -LAYER CRITICAL FREQUENCY

The F_1 -layer critical frequency f_1 is given by

$$f_1 = 0.5 + 1.26 f_E, \quad (10)$$

(10)

and is constrained [Eq. (9b)] not to exceed $0.99 f_2$.

6. MODEL FOR f_oF_2 AND $M(3000)F_2$

These two parameters, f_2 and M_3 , are given by the ITS-78 parameter prediction model. This model is sufficiently well known that it will not be described in detail herein. Generally, the model consists in reducing a set of coefficients for each modelled parameter to a given phase of the solar cycle, season of the year, universal time, and geographic position. The solar cycle is represented by the sunspot number, and the parameters are fitted to a first or second order polynomial. The seasonal variation of the various parameters is represented by different sets of coefficients for each month, except for f_oF_2 . The latter is represented as a Fourier sum (9 terms) in the day of the year. The diurnal variation is represented by a Fourier expansion (up to 13 terms) and the global variation is represented by a (modified) spherical harmonic expansion. Parameters modelled are f_oF_2 , $M(3000)F_2$, $h'F_2$, f_oE , upper decile f_oE_s , median f_oE_s , and the lower decile f_oE_s . Only the first two parameters are used herein.

7. MODEL FOR THE F₂-LAYER SEMITHICKNESS

The F₂-layer semithickness y_2 is given by

$$y_2 = F_y (56 + 0.489 N_s). \quad (11)$$

The model allows for a correction scale factor F_y , which is initialized to unity; no provision is made for its redefinition.

8. MODEL FOR THE F₂-LAYER HEIGHT

The model employed for the construction of the F₂-layer height uses all of the parameters thus far described: f_E , f_1 , f_2 , M_2 , y_2 , h_b , h_m . The following frequencies are defined:

$$\begin{aligned} f'_q &= f_2 - \frac{1}{4} (f_2 - f_1), \\ f''_q &= f_2 - 0.01 f_2 y_2, \\ f_q &= \max (f'_q, f''_q), \\ f_3 &= f_2 M_3, \\ f_o &= 4 f_q - 3 f_2, \\ f_a &= f_o + 3.78 f_E + 1.5, \\ f_b &= 1.26 f_E + 0.5, \\ f_c &= f_o + 8.82 f_E + 3.5, \\ f_d &= f_o - 1.26 f_E - 0.5 = f_o = f_1, \\ f_e &= 8.00 f_E, \\ f_f &= f_o + 7.78 f_E + 1.5, \\ f_h &= f_o - 0.22 f_E + 1.5, \\ f_i &= f_2 + f_q, \\ f_j &= f_2 - f_q. \end{aligned} \quad (12)$$

The following parameters are defined (these are stored for later use in the construction of the M(3000)F₂ correction factor:

$$\begin{aligned} H_3 &= 70 + 3100 (f_q/f_3)^2, \\ F_q &= f_q/f_2, \end{aligned} \quad (13)$$

$$\begin{aligned}
P_3 &= (f_a/f_b) \log (f_c/f_d), \\
Z_1 &= y_E (f_a/f_e) \log (f_f/f_h), \\
Z_2 &= \frac{1}{2} y_2 (f_q/f_2) \log (f_i/f_j).
\end{aligned}$$

The F_2 -layer height is given by:

$$h_2 = 8.0 (H_3 - Z_1 - Z_2 - h_b) / P_3 + y_2 + h_E. \quad (14)$$

9. MODEL FOR THE F_1 -LAYER HEIGHT AND SEMITHICKNESS

The F_1 -layer height h_1 and semithickness y_1 are given by:

$$\begin{aligned}
h_1 &= h_2 - y_2, \\
y_1 &= h_1 - h_E.
\end{aligned} \quad (15)$$

10. MODEL FOR F_2 -LAYER CORRECTION FACTORS - VERTICAL IONOGRAM

The following information had been extracted from a vertical incidence ionogram as input to the program from which correction factors to the F_2 layer parameters are to be derived:

- t_r — universal time of ionogram,
- L_r — geographic north latitude of sounding station,
- W_r — geographic west longitude of sounding station,
- F_1 — $f_o F_1$ from ionogram,
- F_2 — $f_o F_2$ from ionogram,
- $F_q = F_1 + \frac{1}{4} (F_2 - F_1)$,
- $F'_q = F_2 - \frac{1}{4} (F_2 - F_1)$,
- H_v — F_2 virtual height at frequency F_q ,
- H'_v — F_2 virtual height at frequency F'_q ,
- N_s — sunspot number,
- D_y — day of year.

The ionospheric parameters at the given event are constructed from the parameter prediction model; let these parameters be represented by the following notation:

- f_E, f_1, f_2 — critical frequencies,
 h_E, h_1, h_2 — layer heights,
 y_E, y_1, y_2 — semithickness,
 h_b — bottom of ionosphere,
 M_3 — $M(3000)F_2$,
 f_q — "quarter point frequency", Eq. (14),
 Z_1, Z_2, P_3 — Eq. (15) parameters.

Define the following frequencies:

$$\begin{aligned}
 f'_q &= f_1 + \frac{1}{4}(f_2 - f_1), \\
 f'_a &= f_2 + 3.78 f_E + 1.5, \\
 f'_c &= f_2 + 8.82 f_E + 3.5, \\
 f'_d &= f_2 - f_1, \\
 f'_f &= f_2 + 7.78 f_E + 1.5, \\
 f'_h &= f_2 - 0.22 f_E + 1.5, \\
 f'_i &= f_2 + f'_q, \\
 f'_j &= f_2 - f'_q.
 \end{aligned}$$

Define the following quantities:

$$\begin{aligned}
 Z'_1 &= (y_E/8) * (f'_a/f_E) * \log(f_f/f_h), \\
 Z'_2 &= (y_2/2) * (f'_q/f_2) * \log(f_1/f_j), \\
 P'_3 &= (f'_a/f_1) * \log(f_c/f_d), \\
 H'_3 &= (P_3/P'_3) * (H_v - Z'_1 - Z'_2 - h_b) + Z_1 + Z_2 + h_b, \\
 M'_3 &= (f'_q/f_2) * (3100/H'_3 - 70)^2.
 \end{aligned}$$

Then the correction factors R_f and R_m purporting to correct predicted f_oF_2 and $M(3000)F_2$ parameters are given by:

$$\begin{aligned}
 R_f &= F_2/f_2, \\
 R_m &= M'_3/M_3.
 \end{aligned} \tag{16}$$

11. MODEL FOR F₂-LAYER CORRECTION FACTORS – OBLIQUE IONOGRAM

Factors FR and MR are calculated in one run of the OBLFACT program, and are used as input for the next run of OBLFACT to be stored in elements 3 and 5 of /PERTC/. The reference point is also input directly into elements 1 and 2 of /PERTC/; the remaining elements are established by DATA statements. In the following description, the elements of /PERTC/ are referenced by the elements of (C_i; i=1, 16). The field point north latitude and west longitude (N, W) are arguments of PERTC, the algorithm for the calculation of the oblique correction factors. The reference latitude and longitude, C₁ and C₂, are alternatively referenced as N_r and W_r, respectively.

The algorithm commences by computing the distance and azimuth to the field point (N, W) from the reference point (N_r, W_r); let these two quantities be D and Z_o, respectively.

Define the following quantities:

$$\begin{aligned}Z &= Z_o - C_{16}, \\Z_1 &= (\pi/180)*(C_{13} - C_{12} - 90), \\S &= \csc(Z_1), \\Y &= 3600 C_9 C_{11} S, \\W &= C_{10} S \\Z_2 &= (\pi/180)*((D + Y)/360 W), \\X &= \sin(Z_2).\end{aligned}$$

The following correction factors are then calculated:

$$R_a = (1 + C_i X) * (1 + C_j D / C_k) * (1 + C_m Z) \quad (17)$$

where the f_oF₂ and M(3000)F₂ corrections are specified by the index set (a; i, j, k, m) being assigned values (f; 7, 3, 4, 14) and (m; 8, 5, 6, 15), respectively. These factors are then applied to the appropriate F₂-level parameter.

12. ELEMENTS OF COMMON BLOCK/PERTC/

This common block is linked to the INPUT file via NAMELIST inputs in the main programs MAIN and FTDBLB; OBLFACT links elements of NAMELIST input (FRO and MRO) as arguments of subroutines SKIP and/or PEAK; the latter two routines

then define elements 3 and 5 of /PERTC/ equal to FRO and MRO, respectively. OBLFACT also links the first two elements NLREF and WLREF to the input NAMELIST. All elements are assigned default values in a BLOCK DATA program; presumably, these defaults may be assigned different values by replacing the BLOCK DATA program. The elements of /PERTC/ are used by SUBROUTINE PERTC which computes additional corrections to $f_o F_2$ and $M(3000)F_2$ based on information extracted from an oblique ionogram. The reference point (NLREF, WLREF) is the same reference point used in the construction of the updating correction factors to $f_o F_2$ and $M(3000)F_2$ effected in SUBROUTINE FACTO.

Table 1. The Elements of /PERTC/ with the Mnemonic Names Used in PERTC and the Default Values Assigned in the BLOCK DATA Program

Element	Mnemonic	Default	Element	Mnemonic	Default
1	NLREF		2	WLREF	
3	FR	0.0	4	FD	1000.0
5	MR	0.0	6	MD	1000.0
7	FZ	0.0	8	MZ	0.0
9	DUT	0.0792	10	DW	148.5
11	X	0.225	12	GAMMA	180.0
13	AZM	38.808	14	DFAC	0.0
15	DMAC	0.0	16	AZREF	0.0

13. ELECTRON DENSITY MODEL

A continuous electron density profile is constructed from the predicted ionospheric parameters. Slope discontinuities may occur in the model at the critical points of the profile. The model allows for either a parabolic model for the lower E-layer (below the critical altitude) or an E-layer with a D-layer tail; these two models will be described first.

In the parabolic E-layer model, the base altitude, layer height, and semi-thickness are modelled to be 100, 115, and 15 km, respectively. Below the E-layer height h_E , the electron density N_e is given by:

$$\begin{aligned}
 N_e &= 12400 f_E^2 (1 - Y^2), & h_b < h < h_E; \\
 N_e &= 0, & h < h_b,
 \end{aligned}
 \tag{18}$$

where

$Y = (h_E - h)/y_E$; h is the altitude; h_E , y_E , and f_E are the E-layer height, semithickness, and critical frequency.

In the E-layer/D-layer tail model the semithickness may increase by up to 4 km, h_p will lower correspondingly, and h_E remains at 115 km. First, an electron density N_{eo} is calculated by Eq. (20) with Y , however, constructed as follows:

$$\begin{aligned} Y' &= 2 (h_E - h)/y_E, \\ x &= 1.5 \left[1.7 / (1.7 + Y') \right]^{\frac{1}{2}}, \\ z &= \left[1 + 0.1 (Y' - 1) \left| Y' - 1 \right| \right] / \left[1 - 0.1 / (Y' + 1)^2 \right], \\ Y'' &= 2 - \log (1 + 1.72 (Y')^x), \\ Y &= 1, Y'' \text{ negative}, \\ Y &= 1 - \frac{1}{2} (Y'')^2, Y'' \text{ not negative}. \end{aligned}$$

Then

$$N_{eo} = 12400 f_E^2 (1 - Y^2). \quad (19)$$

Calculate the correction for the D-layer tail N_d as follows:

$C = \cos (0.85 X)$, where X is the solar zenith angle;

$$\begin{aligned} N_d &= 0, C \text{ negative}; \\ N_d &= (1 + 0.004 N_s) C^{\frac{1}{4}} / (1 + 81 W^4); \end{aligned} \quad (20)$$

where

$W = (65 - h)/y_E$, and N_s is the sunspot number.

The electron density is finally given by:

$$N_e = N_{eo} + N_d. \quad (21)$$

Between h_E and H_2 , the plasma frequency F_p is taken as the positive solution of a quadratic equation:

$$aF_p^2 + bF_p + c = 0 \quad (22)$$

and the electron density is taken as

$$N_e = 12400 (F_p)^2. \quad (23)$$

The coefficients a, b, and c are calculated as follows:

First, define three reference heights h_a , h_b , h_c :

$$h_a = h_1 - y_1 (1 - (f_E/f_1)^2)^{\frac{1}{2}},$$

$$h_b = h_2 - y_2 (1 - (f_1/f_2)^2)^{\frac{1}{2}},$$

$$h_c = \frac{1}{2} (h_1 + h_b).$$

For h between h_E and h_c , define coefficients B_1 , B_2 , B_3 , B_4 as follows:

$$B_1 = \frac{1}{2} (h_a - h_E + h_b - h_1) / (f_1 - f_E),$$

$$B_2 = (h_1) - \frac{1}{2} (f_1 (h_a - h_E) + f_E (h_b - h_1)) / (f_1 - f_E),$$

$$B_3 = y_1 / f_1,$$

$$B_4 = y_1.$$

For h between h_c and h_2 , the B_i 's are given by:

$$B_1 = \frac{1}{2} (h_b - h_1) / (f_2 - f_1), \quad B_2 = h_2 - f_2 B_1;$$

$$B_3 = y_2 / f_2, \quad B_4 = y_2.$$

The coefficients a, b, c of the quadratic Eq. (22) are defined as:

$$a = B_1^2 + B_3^2,$$

$$b = 2 B_1 (B_2 - h),$$

$$c = (B_2 - h)^2 - B_4^2.$$

The topside model (h greater than h_2) is a modified Chapman profile. Let $Y = 2 (h - h_2) / y_2$; then,

$$N_e = 12400 \left\{ (f_2)^2 \exp [1 - Y - \exp (-Y)] + (0.5 + 0.1 f_2) h_2 (h - h_2) / h^2 \right\}. \quad (24)$$

1.4. MODEL FOR THE GRADIENT OF THE ELECTRON DENSITY

Any ray-tracing technique will require the gradient of the electron density at a field point (r, θ, ϕ) . Clearly, the complications of the model described above for the electron density mitigate against any attempt to derive analytic expressions for the gradient, even neglecting variations in the ionospheric parameters. Furthermore, should one desire to replace the electron density model with some other, either more or less complicated, a general numerical algorithm for the gradient is desired.

The gradient model employed in the WIMP program places the field point at the center of a cubical volume, and computes the electron density at each of the nine points so defined. The coordinates of these nine points are listed in the following table.

Table 2. Coordinates of Points Used for Gradient Calculation

Point	Radial Coordinate	Theta	Phi
1	r	θ	ϕ
2	$r + D_r$	$\theta + D_\theta$	$\phi + D_\phi$
3	$r + D_r$	$\theta - D_\theta$	$\phi + D_\phi$
4	$r + D_r$	$\theta + D_\theta$	$\phi - D_\phi$
5	$r + D_r$	$\theta - D_\theta$	$\phi - D_\phi$
6	$r - D_r$	$\theta + D_\theta$	$\phi + D_\phi$
7	$r - D_r$	$\theta - D_\theta$	$\phi + D_\phi$
8	$r - D_r$	$\theta + D_\theta$	$\phi - D_\phi$
9	$r - D_r$	$\theta - D_\theta$	$\phi - D_\phi$

(r, θ, ϕ) are the coordinates of the field point,

(D_r, D_θ, D_ϕ) are the grid spacings,

$$D_\theta = D_r / r,$$

$$D_\phi = D_r / r \sin \theta.$$

Given a function $f(x)$ evaluated at three points, x_0 , $x_+ = x_0 + dx$, and $x_- = x_0 - dx$, then the best estimate of the derivative of f at x_0 is given numerically by:

$$f'_0 = \frac{1}{2} (f_+ - f_-) / dx \quad (25)$$

where f_- , f_0 , and f_+ represent $f(x_-)$, $f(x_0)$, and $f(x_+)$. The best estimate of the second derivative is given by:

$$f''_0 = \frac{1}{2} (f_+ - 2f_0 + f_-) / dx^2. \quad (26)$$

Unfortunately, the defined set of points does not contain quite the correct subset to implement the numerical model for the derivative specified by Eq. (25). However, appropriate partial derivatives may be evaluated at the center of each side of the defined cube. Each coordinate then has four approximations to the appropriate partial derivative of the electron density; for instance, the r partial derivative will use pairs (2, 6), (3, 7), (4, 8), and (5, 9).

The algorithm adopted to represent the partial derivatives is the average of the four approximate values.

The value chosen for the grid space is 1 / 3-1/2 km.

15. THE WIMP 3-D RAY-TRACING TECHNIQUE

The ray-tracing model employed in the WIMP program depends upon the application of Bouger's rule and parabolic electron density models in multiple layers; the gradient of the electron density at the reflection height is employed to determine the tilt of the reflecting layer.

The program allows for refraction and/or reflecting in the E, F₁, and F₂ layers. The F₁ layer is inserted between the E and F₂ such that the bottom of the F₁ layer is at the E-layer height and the F₁-layer height is at the bottom of the F₂ layer.

The ray tracing is accomplished in SUBROUTINE TRISL.

15.1 Bouger's Rule

Bouger's rule states that in a refracting medium with spherical symmetry electromagnetic radiation propagates in such a way that the quantity $\mu r \cos \beta$ remains constant where μ is the local index of refraction, r is the distance to the field point from the center of symmetry, and β is the local elevation angle.

15.2 Refraction Through a Layer

Refraction through a layer is depicted in Figure 1. The group path correction $\Delta P'$ phase path correction ΔP , and range correction Δ are given by

$$\begin{aligned} \Delta P' &= \left(\frac{y}{\sin \beta_c} \right) \left\{ \frac{1}{2} u \log \left(\frac{u+1}{u-1} \right) - 1 \right\}, \\ \Delta P &= \left\{ 1 - \frac{1}{2} \sin^2 \beta_c (1 + 1/u^2) \right\} \Delta P' - \frac{1}{2} y \sin \beta_c / u^2, \\ \Delta &= \Delta P' \cos \beta_c / (R_0 + h_m), \end{aligned} \quad (27)$$

where $u = f \sin \beta_c / f_c$ and f is the operating frequency, f_c the critical frequency, R_o the radius of the earth, h_m the layer height, y the layer semithickness, and β_c the local elevation angle of the unrefracted ray at the layer height.

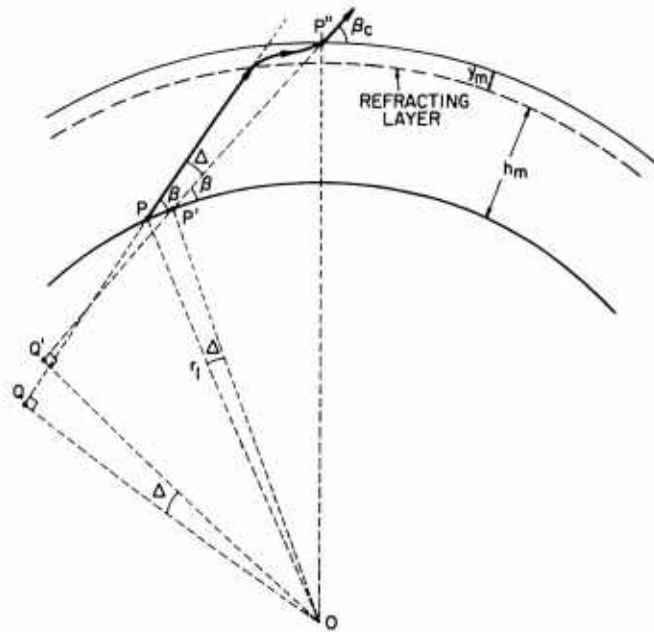


Figure 1. Refraction Through Layer

The group path length P' and phase path length P upon exiting the layer are given by

$$\begin{aligned} P' &= D_o + \Delta P', \\ P &= D_o + \Delta P, \end{aligned} \tag{28}$$

where D_o is the distance $P'P''$ in Figure 1.

15.3 Reflection from a Layer

Reflection from a layer is depicted in Figure 2. The group path corrections ΔP are given by

$$\Delta P' = \frac{y}{\sin \beta_r} \frac{1}{2} u \log \frac{u+1}{u-1},$$

$$\Delta P = \frac{1}{2} y \sin \beta_r + \left\{ 1 - \frac{1}{2} \sin^2 \beta_r (1 + 1/u^2) \right\} \Delta P',$$
(29)

where $u = f \sin \beta_r / f_c$, and β_r is the local elevation angle at the virtual height P'' . These corrections apply for the upward trace to the reflection point; equal corrections obtain for the downward trace.

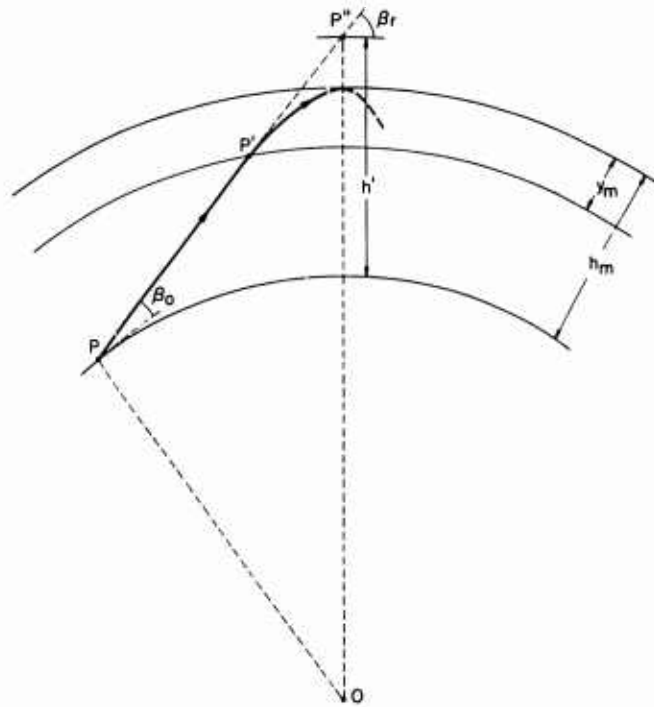


Figure 2. Reflection From Layer

15.4 Tilted Reflection Layer

The gradient of the electron density at the ray reflection point is evaluated and employed to construct an effective tilted reflecting layer. Underlying refracting layers are considered concentric with the earth; however, gradients in these layers are taken into account in that the upward and downward legs of the ray trace through the underlying layers are spatially separated.

The introduction of a tilted reflecting layer, of course, generates considerable complication in the ray trace in that the ray direction, layer normal, and radius vector are no longer coplanar. The program accounts for these bookkeeping complications by setting up orthonormal triads as the ray attacks successive layers.

The y axis is taken parallel to the ray direction. The yz plane contains the center of curvature of the tilted reflecting layer (or the center of the earth in a refracting layer).

15.5 Iteration Scheme

In each hop of the ray trace, the various calculations are iterated to refine the location of the profiles at which refraction through a layer and reflection from a layer occur. In the reflecting layer, the layer tilt is included within the iteration scheme.

At each stage of the ray-trace tests are made for pathological cases such as convergence failures in the allotted number of iterations, inconsistencies between stages, extremely tilted reflecting layers, ducting of the ray between layers, and so forth. Error diagnostic messages are printed prior to returning the main program should TRISL be required to abort the task.

16. FUNCTIONAL DESCRIPTION OF PROGRAM OBLFACT

16.1 Initialization (Block 1)

This part of the program clears the INPUT file (NAMELIST INPUT). The elements of the NAMELIST are listed in Table 3 including the mnemonic name used, definition, and default value. A call to RIIP clears the INPUT file of the ITS parameter prediction coefficients. A call to FACTO calculates the F_2 layer correction factors from f_oF_2 and $h'_{min}F_2$ scaled from the vertical ionogram and appearing in the NAMELIST input. Successive calls to PEAK and SKIP with the remote correction factors $FR\phi$ and $MR\phi$, calculated from a previous run of OBLFACT, check that the ray tracing proceeds as expected (ground-to-ground mode). If not, the mission is aborted and the next task is initiated.

Table 3. Elements of NAMELIST/INPUT/

Mnemonic	Definition	Unit	Notes
SN	Sunspot Number		UNDEF
YRMD	Year & Month, concatenated		UNDEF
DOY	Day of Year	day	UNDEF
ZT	Universal Time, Vertical Ionogram (VI)	hours	UNDEF
RI	Geocentric Distance, VI	km	6370.
NL1	North Latitude, VI	degrees	
WL1	West Longitude, VI	degrees	

Table 3. Elements of NAMELIST/INPUT/ (Cont)

Mnemonic	Definition	Unit	Notes
ZIREF	Universal Time, Oblique Ionogram (OI)	hours	UNDEF
RS	Geocentric Distance to ray end point	km	5370.
NLREF	North Latitude, OI Sounder	degrees	
WLREF	West Longitude, OI Sounder	degrees	
AZ	Bore sight azimuth	degrees	
ELSTEP	Elevation step for SKIP search	degrees	1.0
FCF2R	$f_o F_2$ from VI	MHz	UNDEF
HMINR	$h'_{min} F_2$ from VI	km	UNDEF
FP	Peak Frequency	MHz	*
DELP	Peak Group Path Error	km	*
FS	Skip Frequency	MHz	*
DELS	Skip Group Path Error	km	*
DCIK	Tolerance in Group Path Deviations		10.0
MR ϕ	Gradient Correction Factor, $M(3000)F_2$		\neq
FR ϕ	Gradient Correction Factor, $f_o F_2$	MHz	\neq
MODE	MODE = number of hops		?
IRSTRT	Termination Flag (STOP if ϕ)		1

Explanation of Terms Used in Table 3

- NOTES - A numerical value of this column is the default value set in OBLFACT.
- UNDEF - Implies that OBLFACT does not establish a default value.
- *
- These values are determined from a comparison between the observed oblique ionogram (OOI) and the predicted oblique ionogram (POI) generated from a previous run of the BLOBZ driving program. Refer to "Step 5" of the Operating Instructions. Default values of ϕ are assigned to FP and DELP.
- \neq
- For the first run of OBLFACT, these parameters are set to ϕ . Corrected values will be part of the output of OBLFACT to be used as inputs of a new run of OBLFACT at the user level of iteration. Refer to Steps 4 to 7 of the Operating Instructions.
- ?
- This parameter is an element of the argument list of the ray tracing program TRISL. Neither the operating instruction or the program flow chart illuminate the meaning of its sign. OBLFACT assigns a default value of -1.

16.2 Refinement of MR (Block II)

This part of the program iterates calls to PEAK in order to refine the M(3000) gradient correction factor MR. Since the peak frequency depends on antenna pattern and, thus upon elevation, it therefore depends primarily on the height of the layer. The Block II iteration maintains the $f_o F_2$ gradient correction factor fixed. The value of MR is adjusted initially by 0.001 and subsequently by a Newton iterative technique until the predicted peak group path agrees with that from the oblique ionogram to within the specified tolerance (DCIK, nominally 10 km), at which point transfer is made to Block III.

Block II is ultimately reentered from Block IV after refinement of the $f_o F_2$ gradient correction factor. A call to PEAK establishes whether further refinement is required. If the resultant group path is within tolerance, the task is terminated and the results printed.

Should the required information to effect this refinement be not available, the default values of 0 assigned to FP and DELP automatically cause this part of the program to be bypassed. Thus, only the $f_o F_2$ gradient correction is determined; the M(3000) F_2 gradient remains by default the same as that of the parameter model (ITS-78), which, presumably, is the best available in the absence of evidence to the contrary.

16.3 Refinement of FR (Block III and IV)

This part of the program iterates calls to SKIP in order to refine the $f_o F_2$ gradient correction factor FR. In SKIP, rays are traced at frequency FS from 0° to 20° in steps given by ELSTEP (nominally 1° and must not be less than 1/2°). The array of group paths is searched to locate the minimum. This is compared with the minimum group path extracted from the leading edge of the oblique ionogram at frequency FS. If the difference is within tolerance, the MR iteration is reentered. If not, FR is corrected for the next iteration.

Since OBLFACT is in a late user stage of simulation and a previous stage BLOB 2 produces the general ray-trace results, the user should have limiting information on the elevations between which the minimum group path should be located. The built-in 0° to 20° may not be sufficient to properly locate the minimum group path. The using facility might consider modifying the program to allow the user to specify the elevation domain to be searched. This may be accomplished as follows:

- (a) Link the initial elevation, ELBEG and number of elevations to be traced, NELM to NAMELIST/INPUT/ in OBLFACT.
- (b) Add ELBEG and NELM to COMMON/FIDDLE/ in OBLFACT, SKIP, and PEAK.

(c) Modify the elevation DO loop in SKIP as follows:

PRESENT VERSION	RECOMMENDED VERSION
NELM=20, D ϕ /ELSTEP + 1.D ϕ	(delete)
.	
.	EL=ELBEG
DO 10 IEL=1, NELM	DO 10 IEL=1, NELM
EL=(IEL-1)* ELSTEP	:
.	:
.	.
.	.
.	.
.	.
10 CONTINUE	10 EL=EL + ELSTEP

17. SUBROUTINE PEAK (FRR, MRR, GPP, IGOBAK)

17.1 Argument List

FRR - $f_o F_2$ correction quantity (INPUT)
MRR - $M(3000)F_2$ correction quantity (INPUT)
GPP - Predicted peak group path (OUTPUT)
IGOBAK - Error condition returned (OUTPUT)

17.2 Common Blocks

/PERT C/ linked to PERT F, the routine that calculates F_2 -layer correction factors from parameters scaled from the oblique ionogram.

/REMWEN/ linked from TRISL. Contains reflection layer information.

/FIDDLE/ linked from OBLFACT. Contains the "peak frequency" FP scaled from the oblique ionogram, transmitter location, and take-off azimuth.

17.3 Function

Computes the "predicted peak group path" corresponding to oblique ionogram correction factors FRR and MRR, and "peak frequency" FP.

17.4 Algorithm

The input parameters FRR and MRR are stored in elements 3 and 5 of /PERT C/ for use by PERT F for calculating correction factors to $f_o F_2$ and $M(3000)F_2$.

An elevation is selected from the following critical table according to the peak frequency, element 1 of /FIDDLE/:

Table 4. Elevation Determination

FP less than	Elevation	FP less than	Elevation
5.74	Undefined	16.74	5.2
6.74	11.9	17.74	4.8
7.74	10.3	18.74	4.5
8.74	8.9	19.74	4.2
9.74	7.7	20.74	4.0
10.74	6.7	21.74	3.8
11.74	5.9	23.74	3.7
12.74	5.2	25.74	3.6
13.74	4.6	28.74	3.5
14.74	4.1	30.74	3.4
15.74	3.9	≥ 30.74	Undefined

The calling program is required to insure that $5.74 < FP < 30.74$.

The ray-tracing program TRISL is called to compute the predicted peak group path GPP.

Elements of /REMWEN/ are checked to insure reflection consistency occurs in the F2 layer. Furthermore, the geocentric distance of the ray endpoint is checked that it is less than 6378.85 km. If these tests are passed, the error condition flag IGOBAK is set to zero; otherwise, an error condition is noted by setting IGOBAK to unity.

18. SUBROUTINE SKIP (FRR, MRR, GPS, IOPT, IGOBAK)

18.1 Argument List

- FRR - $f_o F_2$ correction quantity (INPUT)
- MRR - $M(3000)F_2$ correction quantity (INPUT)
- GPS - Predicted minimum group path (OUTPUT)
- IOPT - Correction control parameter (INPUT)
- IGOBAK - Error condition returned (OUTPUT)

18.2 Common Blocks

- /PERT C/ linked to PERT F
- /REMWEN/ linked from TRISL
- /FIDDLE/ linked from calling program (OBLFACT)

18.3 Function

Computes the predicted minimum group path corresponding to the oblique ionogram correction terms FRR and MRR, and "skip frequency" FS (element 2 of /FIDDLE/).

18.4 Algorithm

SKIP transfers FRR and MRR of the argument list to elements 3 and 5 of /PERT C/ respectively, to be used in PERT F to calculate F_2 correction factors.

A sequence of elevations between 0° and 20° is selected for ray tracing via calls to TRISL. The elevation step is contained in element 8 of /FIDDLE/ and a sufficient number of elevations are selected to include the entire domain (0° , $20^\circ+$). Provision is made for up to 41 ray traces; thus, the user must insure that the elevation step size is no greater than 0.5° . The elevation scan is terminated at the first occurrence of a penetration through the ionosphere if such occurs before the normal loop termination.

The rays traced in this elevation scan are partitioned into three sets:

- (a) Rays not reflecting from the F_2 layer. These are excluded from further consideration in (b) and (c).
- (b) Rays with end point at geocentric distance no greater than 6378.85 km.
- (c) Rays with end point at geocentric distance greater than 6378.85 km.

If set (b) is empty, the error flag IGOBAK is set to unity and control is returned to the calling program. Otherwise, the element of (b) with the smallest group path is determined. This least group path is established as the predicted minimum group path GPS unless the following conditions obtain:

- (a) SKIP had been called with IOPT not zero, and
- (b) The ray with next higher elevation belongs to set (c) and has a smaller group path length.

In the latter case, the minimum group path returned as GPS is given by:

$$GPS = G_b + \left\{ (G_c - G_b) / (R_c - R_b) \right\} (6378.85 - R_b),$$

where the G's and R's refer to group paths and end point geocentric distance, and the subscripts b and c refer to the above selected elements of set (b) and (c).

Should calls be issued to SKIP more than 100 times in any run of OBLFACT, the error flag is set to two and the task immediately aborted.

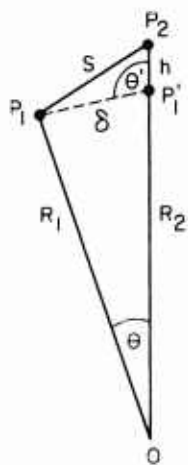
19. REMARKS ON THE USE OF DOUBLE PRECISION ARITHMETIC

The version of the program that the present author has studied has been modified from CDC 6600 machines for use on UNIVAC machines. The essence of this modification is to assign the double precision attribute to every real variable. In the opinion of the present author, wholesale use of double precision arithmetic is not justified, reduction notwithstanding.

In the first place, double precision arithmetic is expensive. Analysis of double precision arithmetic reveals that (1) twice the core storage is required for the variables involved in the calculation, (2) the coding requires, in general, three times the number of instructions, and (3) the execution time increases by approximately a factor of four.

In the second place, increasing the precision of a calculation does not increase the accuracy of the computed result. For example, the geomagnetic field employed in conjunction with the ITS parameter prediction model is a sixth order spherical harmonic expansion. The expansion coefficients are given to one part per million or less. An eight significant digit machine in single precision can calculate the geomagnetic field at a point to the accuracy of the model. The ionospheric parameter model is essentially a one percent model; double precision arithmetic will not improve this situation.

On the other hand, there are situations where single precision arithmetic may produce inaccurate results; for example, in the solution of plane triangles in certain situations.



Consider the situation depicted here. The distances R_1 and R_2 and the angle θ are known and the distance S between P_1 and P_2 is required. The law of cosines applies and

$$S_2 = R_1^2 + R_2^2 - 2R_1 R_2 \cos \theta . \quad (30)$$

Typically, the distances R_1 and R_2 are of the order of 6000 km, the arc $P_1P'_1$ might be 60 km ($\theta = 0.01$ rad), and the altitude difference P'_1P_2 might also be of the order of 60 km. Thus, take R_2 and $\cos \theta$ to be given exactly by

$$R_2 = R_1(1 + 0.01),$$

$$\cos \theta = 1 - \frac{1}{2} \times 10^{-4} .$$

With single precision of 8 significant digits,

$$S^2 = R_1^2 \{ 1 + (1 + 2 \times 10^{-2} + 10^{-4} \pm 10^{-9}) - (2 + 2 \times 10^{-2} - 10^{-4} - 10^{-6} \pm 10^{-8}) \}$$

$$S^2 + R_1^2 = 2 \times 10^{-4} + 10^{-6} \pm 10^{-8} .$$

In this case, the truncation error has resulted in reduction of precision to one part in 10^4 .

This loss of precision may or may not be tolerable; in either case it is not necessary, for the law of cosines may be reformulated to solve the triangle $P_1 P_2 P_1'$ for S , retaining full single precision results. The length of the cord of the angle θ is given by

$$\delta = 2R_1 \sin \frac{1}{2} \theta .$$

Furthermore,

$$\cos \theta' = - \sin \frac{1}{2} \theta = -\delta / 2R_1 ,$$

$$R_2 = R_1 + h .$$

Then,

$$S^2 = h^2 + \delta^2 + h\delta^2/R_1 . \quad (31)$$

This form of the law of cosines will retain single precision results, and should be used wherever possible. To implement this recommendation in SUBROUTINE TRISL, however, would require considerable effort and analysis; a totally new program may be required.

20. MODEL COMPARISON

For purposes of comparison, the WIMP program modelling subroutines were used to generate ionospheric models for various combinations of parameters (Sunspot Number, Season, Universal Time) for a midlatitude location. These were compared with similar models derived from a program in use at RADDC.⁴ These comparisons are shown in Figures 3 through 13.

4. Rush, C. M., Miller, D., and Gibbs, J. (1974) The relative daily variability of F_oF_2 and h_mF_2 and their implications for HF radio propagation, Radio Science, 9:749-756.
ww

Both models use the same formulation for f_oF_2 - the maximum plasma frequency of the F-layer (the ITS-78 model). Figures 3 through 5 show the Universal Time variation of the height of maximum electron density (h_mF_2) for three seasons and two sunspot numbers [W(XX) and R(XX) refer to the WIMP and RADC models for SSN = XX]. Similarly, Figures 6 through 8 show the comparison of parabolic semithickness (y_mF_2); WIMP uses a semithickness value which is time independent. The WIMP model contains a discontinuity at the lower side of the F layer, which results in the most significant departures from the RADC model in the vertical profile. In order to illustrate these departures, the difference between the plasma frequency was calculated by the two models at the altitude of the F_1 -layer maximum used in WIMP. These results are shown for four seasons in Figures 9 through 12, where the times of sunrise and sunset are also indicated. Figure 13 shows a comparison of the two models for given time (χ is the solar zenith angle). The relevant ionospheric model parameters are indicated in the figure.

The results of ray tracing obliquely through the 3-D ionosphere of which Figure 13 represents a single vertical profile are shown in Figure 14. The ray-trace program used was the standard RADC program, known as ARCON II, ITS. As expected, the greatest discrepancies between the oblique group path for the WIMP and RADC models are to be found corresponding to the profile discontinuity at the F_1 layer (compare Figures 9 through 12). In order to examine the differences in computed leading edge of a backscatter ionogram, due to the different models, a one-dimensional ionospheric model was generated, having the vertical profile given by the RADC and WIMP models in Figure 13, (that is, having no horizontal gradients). Leading edges were then computed for simulated backscatter ionograms, using the ARCON II ray-trace program, and the results shown in Figure 15.

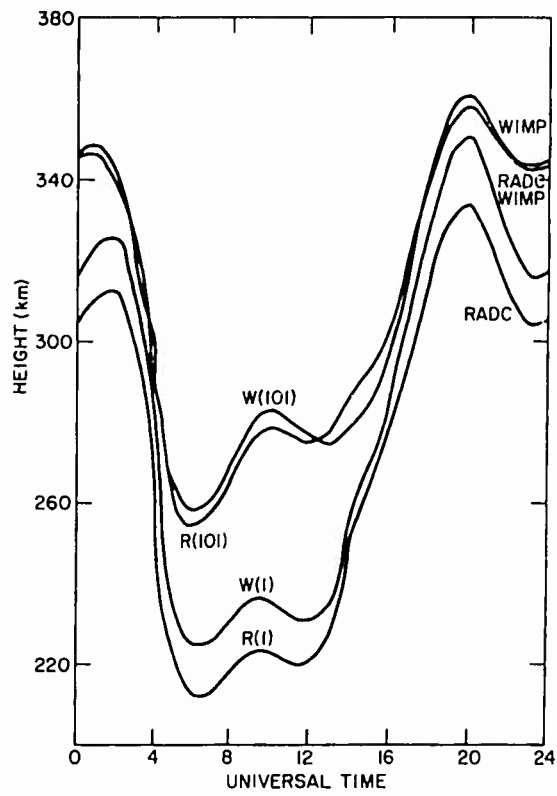


Figure 3. RADG and WIMP Model $h_m F_2$, Winter Solstice

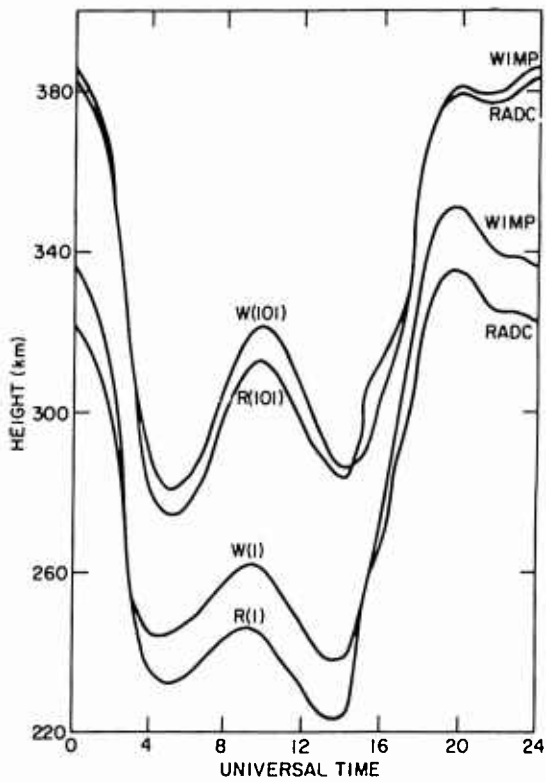


Figure 4. RADG and WIMP Model $h_m F_2$, Vernal Equinox

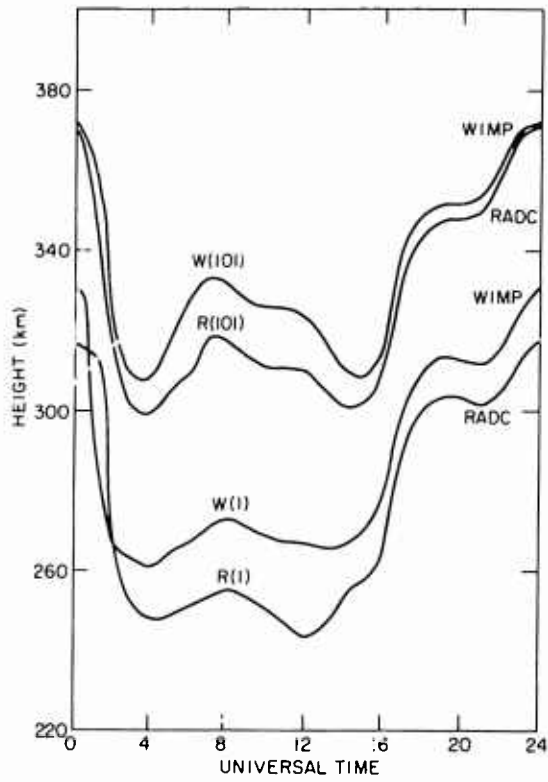


Figure 5. RADC and WIMP Model $h_m F_2$, Summer Solstice

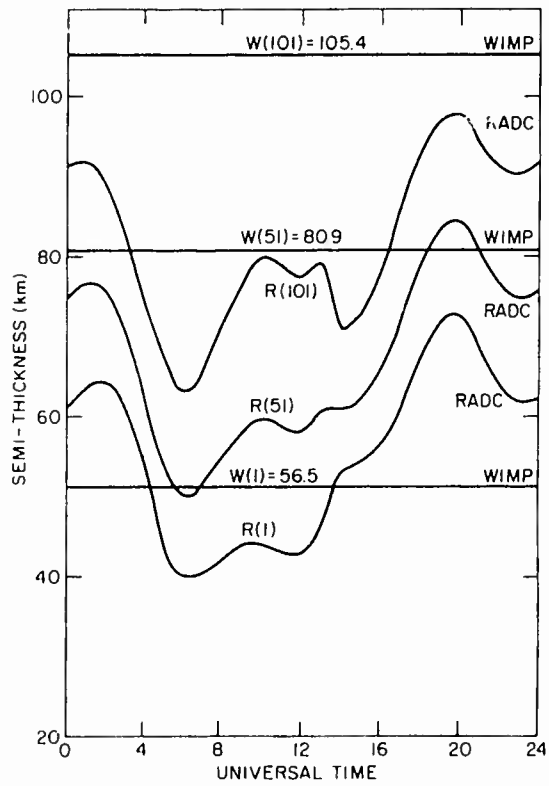


Figure 6. RADC and WIMP Model $y_m F_2$, Winter Solstice

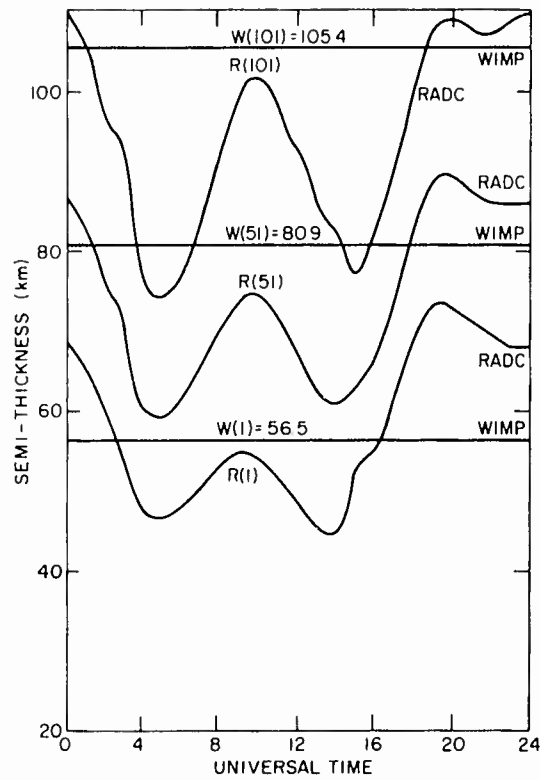


Figure 7. RADC and WIMP Model $y_m F_2$, Vernal Equation

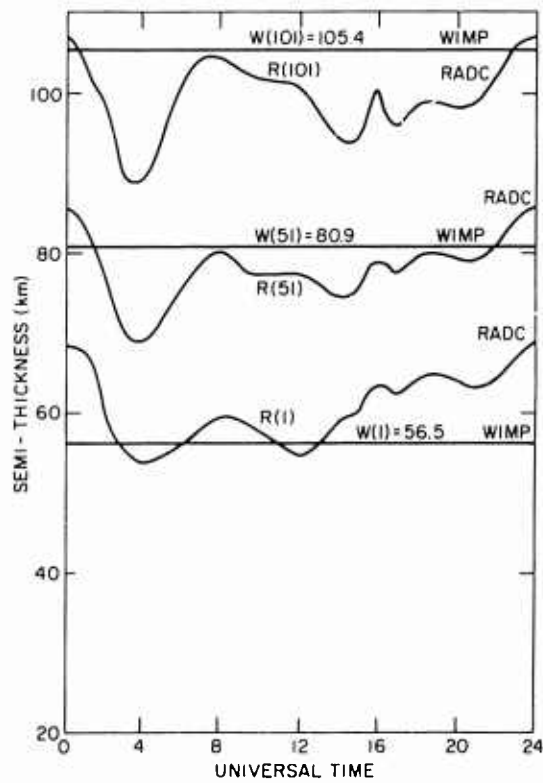


Figure 8. RADC and WIMP Model $y_m F_2$, Summer Solstice

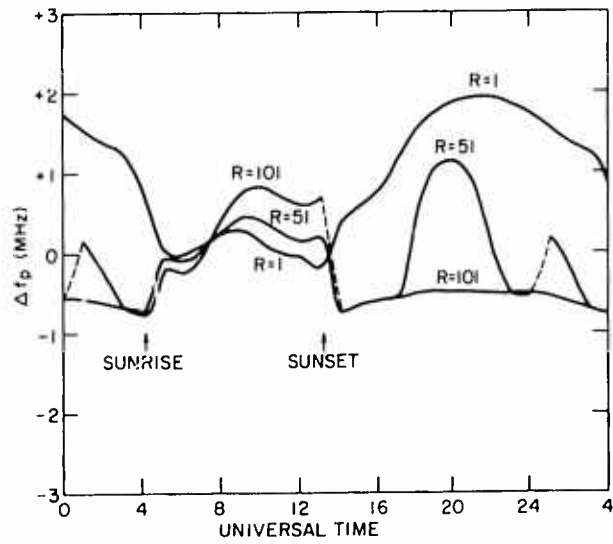


Figure 9. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Winter Solstice

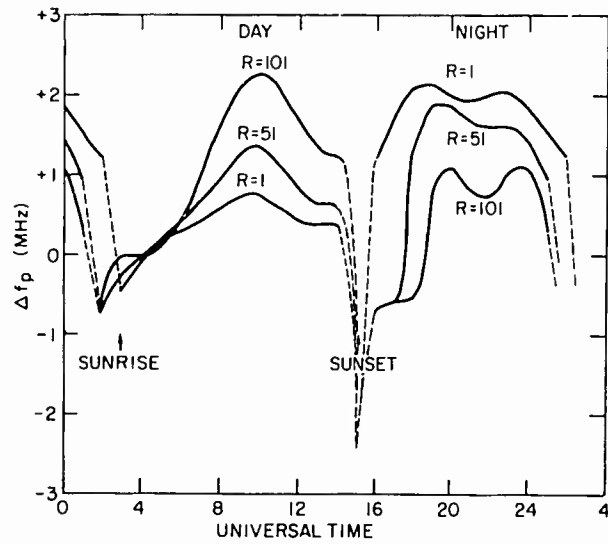


Figure 10. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Vernal Equinox

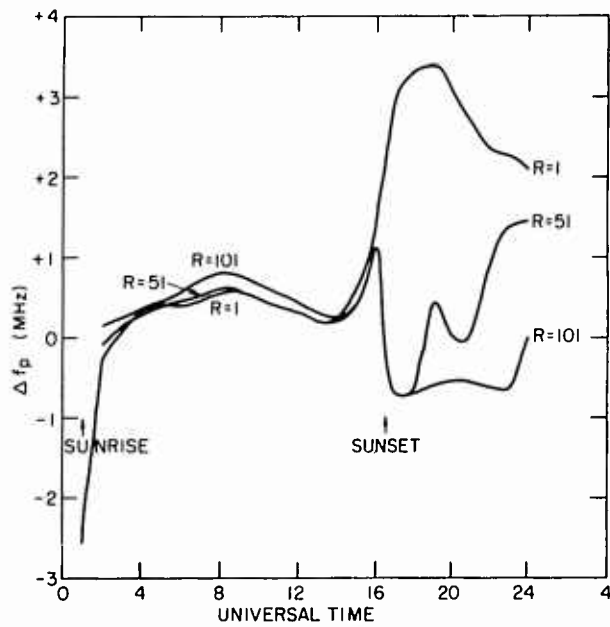


Figure 11. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Summer Solstice

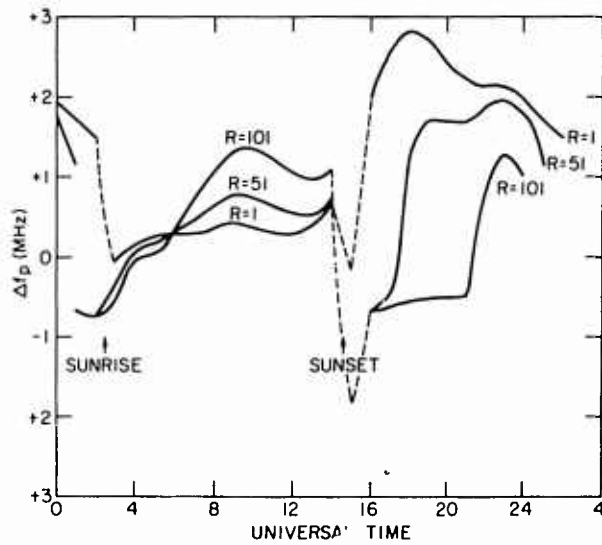


Figure 12. RADC Plasma Frequency at WIMP $h_m F_1$ Minus WIMP $f_o F_1$, Autumnal Equinox

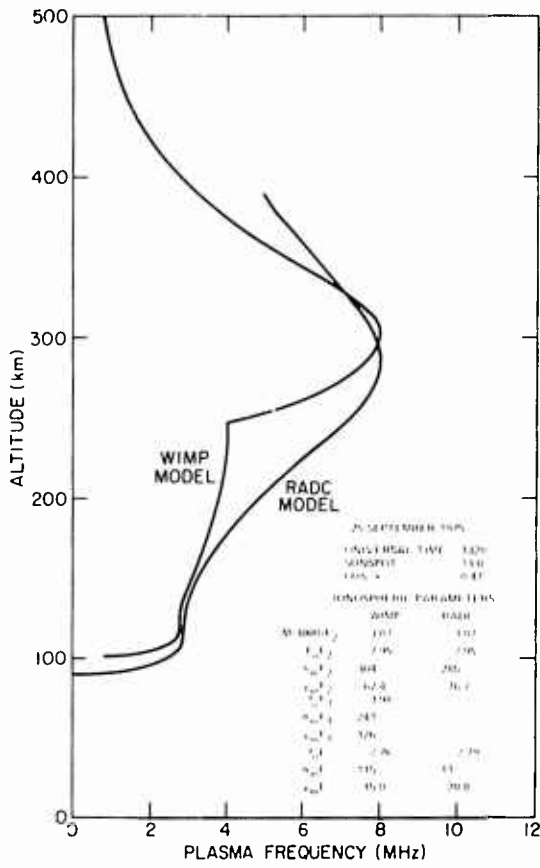


Figure 13. RADC and WIMP Plasma Frequency Profiles

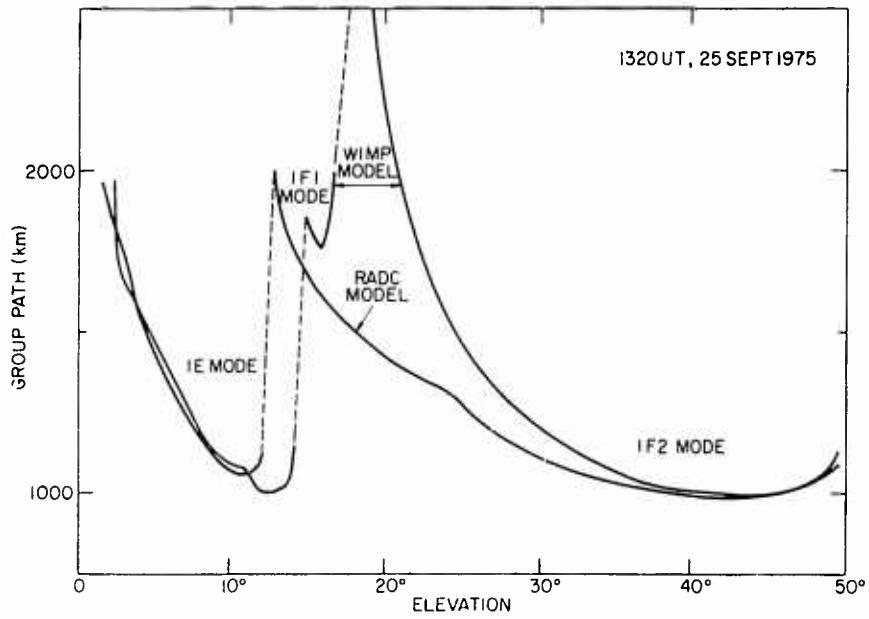


Figure 14. ALCON II 10-MHz Ray Traces, RADC and WIMP Profiles

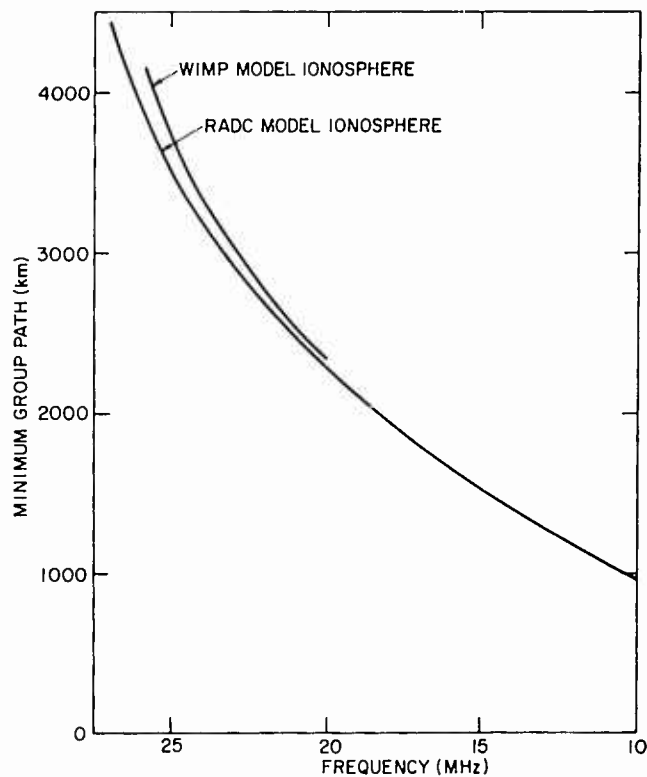


Figure 15. ARCON II
Predicted Leading Edges,
RADC and WIMP Profiles

21. COORDINATE CONVERSION

The conversion from apparent radar range (that is, group path (P) to true range (R) can be accomplished if the ionospheric structure is known, by using the procedures described earlier. The RADC model for 1320 UT on 25 September 1975 was used, together with the ARCON II ray-trace program, to compute (P-R) as a function of P for frequencies in the range 18 to 26 MHz, as shown in Figure 16. The locus of the backscatter leading edge is indicated by the curve labelled P_{\min} , corresponding to the minimum group path at each frequency.

Figure 17 shows the comparison of the actual leading edge of a backscatter ionogram measured at 1320 UT (Curve 2) with the simulated leading edge (Curve 6). Curve 1 shows a leading edge measured at 1340 UT, indicating that the ionosphere is moderately unstable, since Curves 1 and 2 are noticeably different. Curve 3 indicates a secondary leading edge appearing in the ionograms, perhaps a result of azimuthal gradients in the ionosphere. The ionospheric model was then updated by modifying it on the basis of the measured vertical ionogram and allowing for a linear gradient, such that

$$N_e = BN_{e0} (1 + A R_+),$$

where N_e is the modelled electron density at any location.

N_{e0} is the modelled electron density (from the RADC program)

$$B = \frac{(f_o F_2)_{\text{measured}}}{(f_o F_2)_{\text{model}}},$$

$A = \text{constant},$

$R_+ = \text{boresight range (in radians)}.$

It should be noted that the range is here measured in terms of the angle subtended at the earth's center by the arc on the earth's surface which is the ground range. Curve 5 in Figure 17 shows the computed leading edge for $A = 2.0$ and Curve 4 shows the best fit ($A = 1.61$) with the measured data. By repeating the procedure illustrated in Figure 16, the best estimated conversion from radar range to true range can be determined for any operating frequency. Although azimuthal radar information is not available, it is possible to ray trace at various azimuths to establish a locus on the ground of possible ranges for a target having any given radar range.

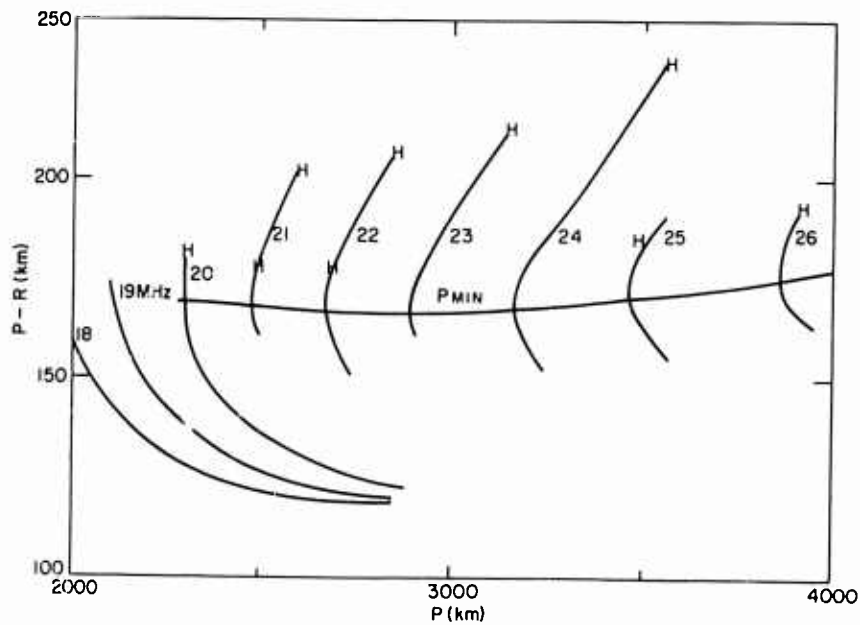


Figure 16. Illustrating Range Conversion

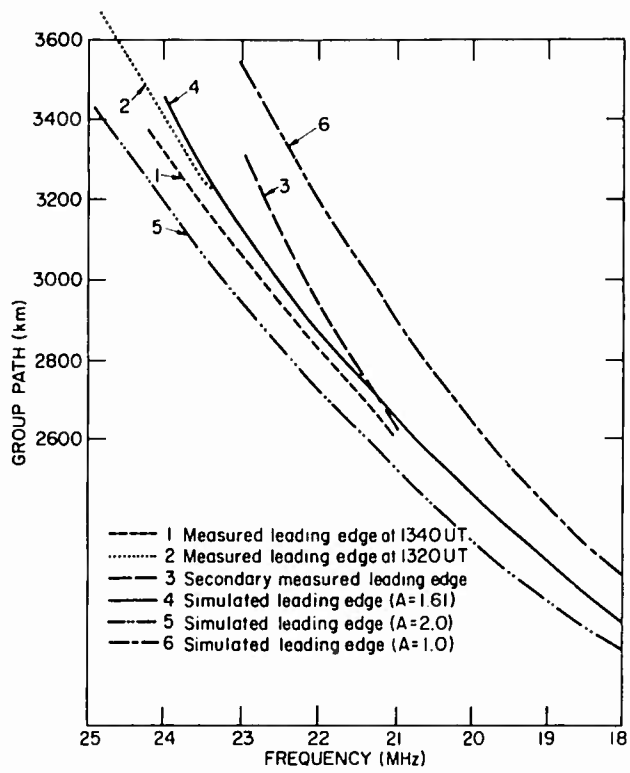


Figure 17. Backscatter Leading Edge Comparison

Appendix A

Program Listings for the WIMP Model Ionosphere

Program listings are included for the WIMP model ionosphere; each sub-routine is briefly described as follows:

1. RIIP - Calling control program for layer parameters and electron density.
2. CRPL2 - Generates f_oF_2 and $M(3000)F_2$.
3. MMDIP - Geomagnetic Field Model.
4. PERT F - f_oF_2 and $M(3000)F_2$ gradient factors.
5. DFP3 - Great Circle Range/Azimuth Calculations.
6. DFP - Great Circle Range Calculation.
7. PTHP - E, F_1 , $Y_m F_2$, and $h_m F_2$ calculations.
8. NFROMR - Electron Density Profile.

```
                SUBROUTINE RIIP(RFEC,BNLATA,BWLONGA,PLASD)
C
C             PROGRAMMED FOR D.ODOM BY COMPUTATIONS,INC. -OCTOBER,1967
C
C             IMPLICIT DOUBLE PRECISION (A-H,O-Z)
                DOUBLE PRECISION M3000,NLATA
                DOUBLE PRECISION MFAC
                LOGICAL SMOOTH,TILT,NIP,FAST
                COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2,
1SN,ZT,YR,D,HAESET,MFAC,F2FAC,F1FAC,EFAC,H2FAC,SNSQRT,QRAD,CQ,IDL,I
2A,SMOOTH
                COMMON/RPERT/RRFEC,ITIP/NIPRIP/NIP/TILTC/TILT,FAST
                COMMON/RIIFWA/IX(4)
                REAL IX

                DATA NLATA,WLONGA
                DATA SN,ZT,YR,D/13.00,13.00,7509.00,269.00/
                DATA M3000,FCF2,FCF1,FCE/3.0500,8.00,4.0800,2.7900/
                DATA HBE,HME,HMF1,HMF2/90.00,110.00,180.00,288.00/
                DATA HAE,HAF1,HAF2/20.00,70.00,108.00/
                DATA MFAC,F2FAC,F1FAC,EFAC,H2FAC/5*1.00/
                DATA HAESET/15.00/

                NLATA=BNLATA*57.2957795130823200
                WLONGA=BWLONGA *57.2957795130823200
                RRFEC=RFEC
                NLATA=DMOD(NLATA,90.00)
                WLONGA=DMOD(WLONGA,360.00)+180.00-DSIGN(180.00,WLONGA)
1004 CALL CRPL2(NLATA,WLONGA)
                M3000=M3000*MFAC
                FCF2 = FCF2*F2FAC
C   PREDICTED BOTTOM OF E LAYER
1005 BA=100.00
                AA=BA+HAESET
                IF(IDL*IA.EQ.0) GO TO 1006
                CALL DFP(NLATA,WLONGA,76.00,102.00,DIST)
                BA=100.00-4.00*DMAX1((1.00-DABS(DIST-3.03)/3.03)**2,0.000)*DMAX1(
1 DCOS((DABS(15.00*DABS(ZT-12.00)-WLONGA)-90.00)/(2.00*
2 57.2957795130823200)),0.000)
C   PREDICTED TRUE HEIGHT PROFILE
1006 CALL PTHP(NLATA,WLONGA,AA,BA)
C   GET ELECTRON DENSITY AT REF. POINT
C   GET N FROM R
                IF(RFEC.LE.6370.00) RETURN
                CALL NFROMR(RFEC,PLASD)
                RETURN
                END
```

```

SUBROUTINE CRPL2(NLAT,WLONG)
C   ...TO FIND CRITICAL FREQUENCY AS A FUNCTION OF THETA AND PHI
C   FROM NEW NBS IONOSPHERIC PREDICTIONS FOR A PARTICULAR TIME...
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DOUBLE PRECISION NLAT,M3000,MFAC
DIMENSION SINTO(11),COSTO(11),G(76),GAMMA(2),DKTO(76,2)
DIMENSION CT(8),ST(8)
COMMON/RIIPAR/M3000,FCF20,DUM(9),SN,ZT,YR,DAY,HAESSET,MFAC,FFAC,
1DUM1(6),ID(3)
*/LABCRP/NHARM(2),KI(2),KII(2),KIII(2),KIV(2),KV(2),KVI(2),KVII(2),
*KVIII(2),KIX(2),D(13,76,2)
DATA RAD/.0174532925199433D0/
G(1)=1.0D0
CALL MMDIP(NLAT,WLONG,SSMX)
THERAD=(360.D0-WLONG)*RAD
COSLAM=DCOS(NLAT*RAD)
CT(1)=COSLAM*DCOS(THERAD)
ST(1)=COSLAM*DSIN(THERAD)
DO 63047 IJK=2,8
CT(IJK)=CT(1)*CT(IJK-1)-ST(1)*ST(IJK-1)
63047 ST(IJK)=CT(1)*ST(IJK-1)+ST(1)*CT(IJK-1)
IF(DABS(ZT-ZTP).LT.1.D-3.AND.DABS(YR-YRP).LT.1.D-1)GO TO 20
ZTP=ZT
YRP=YR
T0=15.000*ZT-180.000
TORAD=T0*RAD
ARG=0.000
NHARML=MAX0(NHARM(1),NHARM(2))
DO 1 J=1,NHARML
ARG=TORAD+ARG
SINTO(J)=DSIN(ARG)
1 COSTO(J)=DCOS(ARG)
DO 2 L=1,2
NHARML=NHARM(L)
K9=KIX(L)+1
DO 2 K=1,K9
DKTO(K,L)=D(1,K,L)
DO 3 J=1,NHARML
3 DKTO(K,L)=DKTO(K,L)+D(2*J+1,K,L)*COSTO(J)+D(2*J,K,L)*SINTO(J)
2 CONTINUE
20 DO 100 L=1,2
NHARML=NHARM(L)
K1=KI(L)+1
K2=KII(L)+1
K3=KIII(L)+1
K4=KIV(L)+1
K5=KV(L)+1
K6=KVI(L)+1
K7=KVII(L)+1
K8=KVIII(L)+1
K9=KIX(L)+1
K1P1=K1+1
K1P2=K1+2
K1P3=K1+3
K2P1=K2+1
K2P2=K2+2
K2P3=K2+3

```

```

      K3P1=K3+1
      K3P2=K3+2
      K3P3=K3+3
      K4P1=K4+1
      K4P2=K4+2
      K4P3=K4+3
      K5P1=K5+1
      K6P1=K6+1
      K7P1=K7+1
      K8P1=K8+1
      DO 4 K=2,K1
4      G(K)=G(K-1)*SSMX
      IF(K1.EQ.K2) GO TO 9
      G(K1P1)=CT(1)
      G(K1P2)=ST(1)
      DO 5 K=K1P3,K2,2
      G(K)=G(K-2)*SSMX
5      G(K+1)=G(K-1)*SSMX
      IF(K2.EQ.K3) GO TO 9
      G(K2P1)=CT(2)
      G(K2P2)=ST(2)
      DO 6 K=K2P3,K3,2
      G(K)=G(K-2)*SSMX
6      G(K+1)=G(K-1)*SSMX
      IF(K3.EQ.K4) GO TO 9
      G(K3P1)=CT(3)
      G(K3P2)=ST(3)
      DO 7 K=K3P3,K4,2
      G(K)=G(K-2)*SSMX
7      G(K+1)=G(K-1)*SSMX
      IF(K4.EQ.K5) GO TO 9
      G(K4P1)=CT(4)
      G(K4P2)=ST(4)
      DO 8 K=K4P3,K5,2
      G(K)=G(K-2)*SSMX
8      G(K+1)=G(K-1)*SSMX
      IF(K5.EQ.K6) GO TO 9
      G(K5P1)=CT(5)
      G(K6)=ST(5)
      IF(K6.EQ.K7) GO TO 9
      G(K6P1)=CT(6)
      G(K7)=ST(6)
      IF(K7.EQ.K8) GO TO 9
      G(K7P1)=CT(7)
      G(K8)=ST(7)
      IF(K8.EQ.K9) GO TO 9
      G(K8P1)=CT(8)
      G(K9)=ST(8)
9      GAMMA(L)=0.000
      DO 10 K=1,K9
10     GAMMA(L)=GAMMA(L)+DKTO(K,L)*G(K)
100    CONTINUE
      FCF20=GAMMA(1)*DABS(FFAC)
      M3000=GAMMA(2)*DABS(MFAC)
      IF(FFAC.LT.0.000)CALL PERTF(ZT,NLAT,WLONG,FCF20)
      IF(MFAC.LT.0.000)CALL PERTM(ZT,NLAT,WLONG,M3000)
      RETURN

```

```

SUBROUTINE PTHP(NLAT,WLONG,A,B) PTH
C PREDICTED TRUE HEIGHT PROFILE PTH
C PROGRAMMED FOR D.ODOM BY I.STUHLER PTH
IMPLICIT DOUBLE PRECISION (A-H,O-Z) PTH
DOUBLE PRECISION NLAT,M3000,M,J,KK PTH
LOGICAL SMOOTH PTH
COMMON/FACCOM/FM,ZZ,KK,P3000 PTH
COMMON/RIIPAR/M3000,FCF20,FCF10,FCEO,HBEP,HPE,HMEP,F1,HMF1P,HPF2 PTH
1,HMF2P,SN,ZT,YR,D,DUM(3),F1FAC,EFAC,H2FAC, PTH
2 SNSQRT,QRAD,CQ,IO(2),SMOOTH PTH
DATA RAD/57.2957795130823200/ PTH
C SOLVE FOR ZENITH CORR. ANGLE FOR DAY OF YEAR PTH
M=23.4500*DSIN(180.00*(D-82.500)/(182.00*RAD)) PTH
C GET F3000 PROPAGATION FREQ FOR F2 LAYER PTH
F3000=FCF20*M3000 PTH
C CHECK FOR INCORRECT DAY (NEG) PTH
IF(D.LT.0.000) GO TO 2000 PTH
C IS DAY PAST SPRING PTH
IF(D.GE.162.500) GO TO 1000 PTH
X=D+365.500 PTH
Y=1.000 PTH
GO TO 1001 PTH
C IS DAY PAST FALL PTH
1000 IF(D.GE.344.500) GO TO 1002 PTH
X=D PTH
Y=-1.600 PTH
GO TO 1001 PTH
C CHECK FOR INCORRECT DAY (TOO LARGE) PTH
1002 IF(D.GE.366.500) GO TO 2001 PTH
X=D PTH
Y=1.00 PTH
C SOLVE FOR SOLAR ZENITH ANGLE IN RAD PTH
1001 J=Y*.023500*(64.00/(4.00+DABS((X-344.500)/45.00)**3)-240.00/(15.00 PTH
1 +DABS(X-344.500))) PTH
IF(ZT.LT.12.00)ZT=-ZT PTH
Z=DABS(15.00*DABS(ZT-12.00)-J*15.00-WLONG) PTH
IF(Z.GE.180.00)Z=360.00-Z PTH
ZSQ=Z*Z PTH
QSQ=ZSQ*(DCOS(0.600*(NLAT+M)/RAD)**2)+(NLAT-M)**2 PTH
1005 Q=DSQRT(QSQ) PTH
QRAD=Q/RAD PTH
CQ=DCOS(.93200*QRAD) PTH
C FUNCTION FOR E-LAYER NIGHT TIME FORMATION PTH
CCQ=((CQ+1.00)*.500)**2 PTH
SNSQRT=DSQRT(1.00+.00400*SN) PTH
IF(CQ.LE.0.00) GO TO 1101 PTH
C SOLVE FOR PRED E-LAYER CRITICAL FREQ PTH
10.0489=3.17*3.17, .5625=.75*.75 PTH
FCEO=SNSQRT*DSQRT(10.048900*CQ**(2.00/3.77500)+.562500*CCQ**2) PTH
IF(FCEO.GE.FCF20)FCEO=.7500*SNSQRT*CCQ PTH
GO TO 1102 PTH
1101 FCEO=.7500*SNSQRT*CCQ PTH
C SOLVE FOR PRED F1-LAYER CRITICAL FREQ PTH
1102 FCF10=1.2600*FCEO+0.500 PTH
IF(FCF10.LT.FCF20*.9900) GO TO 9982 PTH
FCF10=.9900*FCF20 PTH
FCEO=DMAX1((FCF10-.500)/1.2600,1.0-5) PTH

```

```

C SOLVE FOR REF. FREQ. NO. 1 PTH
9982 FK1=FCF20-(FCF20-FCF10)/4.00 PTH
C CALCULATE PRED. SEMITHICKNESS OF F2 LAYER PTH
HPF2=(0.48900*SN+56.000)*H2FAC PTH
C SOLVE FOR REF FREQ. NO. 2 PTH
FK2=FCF20*(1.00-(DSQRT(HPF2)/100.000)) PTH
C SET FM TO GREATER OF TWO REF. FREQ. PTH
IF(FK1.GT.FK2) GO TO 1003 PTH
FM=FK2 PTH
GO TO 1004 PTH
1003 FM=FK1 PTH
C SOLVE FOR VIRTUAL HT. OF F3000 PTH
1004 XX=FM/F3000 PTH
H3000=3100.00*XX**2+70.000 PTH
FC=4.00*FM-3.00*FCF10 PTH
P3000=((FC+3.7800*FCEO+1.500)/(1.2600*FCEO+.500))*DLOG((FC+8.8200
1 *FCEO+3.500)/(FC-1.2600*FCEO-0.500)) PTH
ZZ=(A-B)*(FC+3.7800*FCEO+1.500)/(8.00*FCEO)*DLOG((FC+7.7800
* *FCEO+1.500)/(FC-.2200*FCEO+1.500)) PTH
FF=FM/FCF20 PTH
KK=HPF2*FF*DLOG((1.00+FF)/(1.00-FF))/2.000 PTH
C CALCULATE PRED. HT. OF F2 LAYER MAX. PTH
HMF2P=8.00*(H3000-ZZ-B-KK)/P3000+HPF2+A PTH
C CALC. HTS. OF OTHER LAYERS PTH
HMF1P=HMF2P-HPF2 PTH
HMEP=A PTH
HBEP=B PTH
HPF1=HMF1P-HMEP PTH
HPE=A-B PTH
ZT=DABS(ZT) PTH
FCEO=DMIN1(FCEO*EFAC,(.9900*FCF20-.500)/1.2600) PTH
IF(F1FAC) 1014, 1014, 1015 PTH
1014 FCF10=1.2600*FCEO+.500 PTH
GO TO 1016 PTH
1015 FCF10=FCF10*F1FAC PTH
1016 IF(SMOOTH)FCF10=FCF10/.86602540378443900 PTH
FCF10=DMIN1(FCF10,.9900*FCF20) PTH
RETURN PTH
2000 WRITE(6,4)D PTH
4 FORMAT(4H D =D13.5,12H IS NEGATIVE) PTH
STOP PTH
2001 WRITE(6,5)D PTH
5 FORMAT(4H D =D13.5,22H IS GREATER THAN 366.5) PTH
STOP PTH
END PTH

```



```

SUBROUTINE NFROMR(RFEC,PLASD)
C
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DOUBLE PRECISION K,J,M3000
LOGICAL SMOOTH
COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAЕ,HME,HAF1,HMF1,HAF2,HMF2,
1DUM(10),SNSQRT,QRAD,CQ,ID,IA,SMOOTH
C HEIGHT ABOVE GROUND OF REF. PT.
OH=RFEC-6370.00
C NO - IS PCINT OF INTEREST ABOVE E LAYER MAX
IF(OH.GT.HME) GO TO 201
IF(ID.EQ.1) GO TO 2001
C IS PT. OF INTEREST BELOW E LAYER
IF((HME-OH).GE.HAE) GO TO 300
C NO - SOLVE FOR E LAYER PLASMA DENSITY
F02=FCE*FCE*(1.00-((HME-OH)/HAE)**2)
GO TO 202
C E LAYER WITH D LAYER TAIL
2001 ZP=2.00*(HME-OH)/HAE
K=1.500*DSQRT(1.700/(1.700+ZP))
J=1.00+(ZP-1.00)*DABS(ZP-1.00)/10.00
J=J/(1.00-.100/(1.00+ZP)**2)
ZPP=2.00
IF(ZP.GT.0.00)ZPP=2.00-0LOG(1.00+1.7200*ZP**K)
IF(ZPP.LE.0.00) GO TO 300
ZPP=2.00-ZPP**J
F02=FCE*FCE*(1.00-ZPP*ZPP/4.00)
GO TO 202
C SOLVE FOR REF. HTS. 1 THRU 3
201 HS2=HMF2-HAF2*DSQRT(1.00-(FCF1/FCF2)**2)
HS1=HMF1-HAF1*DSQRT(1.00-(FCE/FCF1)**2)
HT2=(HS2+HMF1)/2.00
C IS PT. OF INTEREST ABOVE REF PT 3
IF(OH.GT.HT2) GO TO 203
C NO- SOLVE FOR F1 LAYER PLASMA DENSITY
BIGK1=(HS1-HME+HS2-HMF1)/(2.00*(FCF1-FCE))
BIGK3=HAF1/FCF1
BIGK2=HMF1-(FCF1*(HS1-HME)+FCE*(HS2-HMF1))/(2.00*(FCF1-FCE))
BIGA=BIGK1**2+BIGK3**2
BIGB=2.00*BIGK1*(BIGK2-OH)
BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF1**2
FO=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA)
IF(FO.LT.FCE)FO=FCE
F02=FO*FO
GO TO 202
C SOLVE FOR DENSITY ABOVE F2 LAYER MAX
211 OHH=(OH-HMF2)/OH
Z=(OH-HMF2)/HAF2*2.00
F02=FCF2**2*DEXP(1.00-Z-DEXP(-Z))+(0.500+FCF2/10.000)*OHH*HMF2/OH
F02=DMIN1(F02,FCF2**2)
GO TO 202
C IS POINT OF INTEREST ABOVE F2-LAYER MAX
203 IF(OH.GT.HMF2) GO TO 211
C NO-SOLVE FOR F2-LAYER PLASMA DENSITY
BIGK1=(HS2-HMF1)/(2.00*(FCF2-FCF1))
BIGK3=HAF2/FCF2
BIGK2=HMF2-FCF2*BIGK1

```

	BIGA=BIGK1**2+BIGK3**2	NFR
	BIGB=2.00*BIGK1*(BIGK2-OH)	NFR
	BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF2**2	NFR
	F0=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA)	NFR
	F02=F0*F0	NFR
202	PLASD=F02*12400.00	NFR
	IF(ID.EQ.1) GO TO 301	NFR
	RETURN	NFR
300	PLASD=0.00	NFR
	IF(ID.EQ.0) RETURN	NFR
301	CQ=DCOS(QRAD*.8500)	NFR
	IF(CQ.GT.0.000) GO TO 302	NFR
	CQ=0.00	NFR
	RETURN	NFR
302	CQ=CQ** (0.2500)	NFR
303	PLASD=PLASD+SNSQRT*SNSQRT*CQ*1.02/(1.00+81.00*((65.00-OH)/HAE)**4)	NFR
	RETURN	NFR
	END	NFR

```

      SUBROUTINE DFP(NLATA,WLONGA,NLATB,WLONGB,DIST)
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DOUBLE PRECISION NLATA,NLATB
      DATA RAD/57.2957795130823200/
      DACOS(DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY),DUMMY)
C     SHIFT INPUT LAT. BY ONE QUADRANT
      PPA=90.000-NLATA
      PPB=90.000-NLATB
      GGH=WLONGA
      GGK=WLONGB
C     FIND SMALLEST ANGULAR DIFF. BETWEEN A AND B
      HHGK=GGH-GGK
      ABHHGK=DABS(HHGK)
      HHK=ABHHGK
      IF(HHK.GT.180.00) HHK=360.00-HHK
C     SOLVE FOR BEARING FROM A TO B
      RAAPB=HHK/RAD
      CSAAPB=DCOS(RAAPB)
      RPPA=PPA/RAD
      SINPPA=DSIN(RPPA)
      COSPPA=DCOS(RPPA)
      RPPB=PPB/RAD
      SINPPB=DSIN(RPPB)
      COSPPB=DCOS(RPPB)
      COSAAB=COSPPA*COSPPB+SINPPA*SINPPB*CSAAPB
      RAAB=DACOS(COSAAB)
C     SOLVE FOR GREAT CIRCLE DISTANCE BETWEEN A AND B
      DIST=6370.000*RAAB
      RETURN
      END

```

```

SUBROUTINE MMDIP(NLAT,WLONG,SSMX)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
C COMPUTE MAGNETIC FIELD COMPONENTS MAGNETIC DIP AND MODIFIED MAGNETIC
C DIP
DOUBLE PRECISION NLAT
DIMENSION P(7,7),DP(7,7),CP(7),AOR(7),SP(7)
DIMENSION CT(7,7),H(7,7),G(7,7)
DATA P,DP,SP/1.000,104*0.000/,CP/1.000,6*0.000/
DATA RD/57.2957795130823200 /,HC/6371.203/
DATA CT/2*0.00,.3333333300,.26666666700,.2571428600,
1 .2539682500,.2525252500,3*0.00,.200,.2285714200,.2380952300,
2 .2424242400,4*0.00,.1428571400,.1904761900,.2121212100,
3 5*0.00,.1111111100,.1616161600,6*0.00,.0909090900,14*0.00/
DATA G/0.00,.30411200,.02403500,-.03151800,-.04179400,
1 .01625600,-.01952300,0.00,.02147400,-.05125300,
2 .06213000,-.04529800,-.03440700,-.00485300,2*0.00,
3 -.01338100,-.02489800,-.02179500,-.01944700,.00321200,
4 3*0.00,-.00649600,.00700800,-.005060800,.02141300,
5 4*0.00,-.00204400,.00277500,.00105100,5*0.00,.00069700,
6 .00022700,6*0.00,.00111500/
DATA H/8*0.00,-.05798900,.03312400,.01487000,-.01182500,
1 -.00079600,-.00575800,2*0.00,-.00157900,-.00407500,
2 .01000600,-.002000,-.00873500,3*0.00,.0002100,.0004300,
3 .00459700,-.00340600,4*0.00,.00138500,.00242100,
4 -.00011800,5*0.00,-.00121800,-.00111600,6*0.00,
5 -.00032500/
P1=NLAT
P2=360.000-(WLONG)
IF(P1-89.900)2,4,1
1 P1=89.900
P2=0.00
GO TO 4
2 IF(P1+89.900)3,4,4
3 P1=-89.900
P2=0.00
4 PHI=P2/RD
AR=HC/(HC+3.D5)
C=DSIN(P1/RD)
S=DSQRT(1.-C**2)
SP(2)=DSIN(PHI)
CP(2)=DCOS(PHI)
AOR(1)=AR**2
AOR(2)=AR**3
DO 5 M=3,7
SP(M)=SP(2)*CP(M-1)+CP(2)*SP(M-1)
CP(M)=CP(2)*CP(M-1)-SP(2)*SP(M-1)
5 AOR(M)=AR*AOR(M-1)
BV=0.00
BN=0.00
BPHI=0.00
DO 6 N=2,7
FN=DBLE(FLOAT(N))
SUMR=0.00
SUMT=0.00
SUMP=0.00
DO 7 M=1,N
IF(N-M)8,9,8

```

```

9      P(N,N)=S*P(N-1,N-1)                                DMM
      DP(N,N)=S*DP(N-1,N-1)+C*P(N-1,N-1)                  DMM
      GO TO 10                                             DMM
8      P(N,M)=C*P(N-1,M)-CT(N,M)*P(N-2,M)                 DMM
      DP(N,M)=C*DP(N-1,M)-S*P(N-1,M)-CT(N,M)*DP(N-2,M)   DMM
10     FM=DOUBLE(FLOAT(M-1))                               DMM
      TS=G(N,M)*CP(M)+H(N,M)*SP(M)                        DMM
      SUMR=SUMP+P(N,M)*TS                                  DMM
      SUMT=SUMT+DP(N,M)*TS                                  DMM
7      SUMP=SUMP+FM*P(N,M)*(-G(N,M)*SP(M)+H(N,M)*CP(M))  DMM
      BV=BV+AOR(N)*FN*SUMR                                  DMM
      BN=BN-AOR(N)*SUMT                                     DMM
6      BPHI=BPHI-AOR(N)*SUMP                                DMM
      COSLAM=DCOS((NLAT)/RD)                               DMM
      COM1=-BV                                             DMM
      COM2=BN                                              DMM
      COM3=-BPHI/S                                         DMM
      TMP=COM2**2+COM3**2                                   DMM
      BIGI=DATAN(-COM1/DSQRT(TMP))                          DMM
      SSMX=(BIGI/DSQRT(BIGI**2+COSLAM))                     DMM
C     NEXT CARD DELETED DSINCE SMX NOT USED BY CRPL2      DMM
C     SMX=DASIN(SSMX)                                       DMM
      RETURN                                               DMM
      END                                                  DMM

```

```

SUBROUTINE PERTF(T,NL,WL,FCF20) PER
IMPLICIT DOUBLE PRECISION (A-H,O-Z) PER
DOUBLE PRECISION NLREF,MR,MZ,MD,NL PER
COMMON/PERTC/NLREF,WLREF,FR,FD,MR,MD,FZ,MZ,DUT,DW,X,GAMMA,AZM, PER
1 DFAC,DNAC,AZREF PER
RTD=57.2957795130823200 PER
CALL DFP3(NLREF,WLREF,NL,WL,DIST,AZ) PER
AZ=AZ-AZREF PER
STHINV=1.000/DABS(DSIN((AZM-(90.00+GAMMA))/RTD)) PER
Y=DUT*360.00*X*STHINV PER
W=DW*STHINV PER
SD=DSIN((DIST+Y)/W*360.00/RTD) PER
FCF20=FCF20*(1.00+FZ*SD)*(1.00+FR*DIST/MD)*(1.00+AZ*DFAC) PER
FCF20=AMAX1(.5100,FCF20) PER
RETURN PER
ENTRY PERTM(T,NL,WL,FCF20) PER
FCF20=FCF20*(1.00+MZ*SD)*(1.00+MR*DIST/MD)*(1.00+AZ*DNAC) PER
FCF20=AMAX1(1.00,FCF20) PER
RETURN PER
END PER

```

	SUBROUTINE FACTO(NLREF, WLREF, FCF2R, HMINR, ZTREF)	FAC
	IMPLICIT DOUBLE PRECISION(A-H, O-Z)	FAC
	DOUBLE PRECISION KK, M3000P, M3000R, MFAC, MM, NLREF, K1	FAC
	COMMON/FACCOM/F1, ZZ, KK, P3000	FAC
	COMMON/RIIPAR/M3000P, FCF2, FCF1, FCE, HBE, HAE, HME, HAF1, HMF1, HPF2,	FAC
	1 HMF2, SNS(5), MFAC, F2FAC, DUM(6), IDUM(3)	FAC
	DATA RTD/57.2957795130823200/	FAC
	F2FAC=1.00	FAC
	MFAC=1.00	FAC
	IF(FCF2R.EQ.0.00) RETURN	FAC
	ZTS=SNS(2)	FAC
	SNS(2)=ZTREF	FAC
	CALL CRPL2(NLREF, WLREF)	FAC
	F2FAC=DABS(FCF2R/FCF2)	FAC
	IF(HMINR.EQ.0.00) GO TO 10	FAC
	CALL RIIP(6370.00, NLREF/RTD, WLREF/RTD, PLASD)	FAC
	P1=(FCF2+3.7800*FCE+1.500)/FCF1*DLOG((FCF2+8.8200*FCE+3.500)/	FAC
	1 (FCF2-FCF1))	FAC
	MM=HAE/8.00	FAC
	Z1=MM*(FCF2+3.7800*FCE+1.500)/FCE*DLOG((FCF2+7.7800*FCE+1.500)/	FAC
	1 (FCF2-.2200*FCE+1.500))	FAC
	FFM=FCF1+(FCF2-FCF1)/4.00	FAC
	FF1=FFM/FCF2	FAC
	K1=50.00*FF1*DLOG((1.00+FF1)/(1.00-FF1))	FAC
	H3000=P3000/P1*(DABS(HMINR)-Z1-HBE-HPF2*K1/100.00)+ZZ+HBE+KK	FAC
	M3000R=(FM/FCF2)*DSQRT(3100.00/(H3000-70.00))	FAC
	MFAC=DSIGN(M3000R/M3000P, HMINR)	FAC
10	F2FAC=DSIGN(F2FAC, FCF2R)	FAC
	SNS(2)=ZTS	FAC
	RETURN	FAC
	END	FAC

Appendix B

Block Diagram and Flow Chart for WIMP Ray-Tracing Program TRISL

Explanation:

BI. TRISL BLOCK DIAGRAM

This presentation shows the general communication network among the various functional processes of TRISL, and illustrates the iterative complications inherent in the program. The function of the various blocks is generally described as follows:

- BLOCK I: Initialization Procedures.
- BLOCK II: E-layer refraction upwards.
- BLOCK III: F_1 -layer refraction upwards.
- BLOCK IV: Reflection layer initialization.
- BLOCK V: Tilt calculation and consistency checks.
- BLOCK VI: F_1 -layer refraction downwards.
- BLOCK VII: E-layer refraction downwards.
- BLOCK VIII: Error checks.
- BLOCK IX: Iterate reflection and tilt.
- BLOCK X: Traffic control.
- BLOCK XI: Normal Terminal calculations.
- BLOCK XII: ERROR exits.

B2. DETAILED FLOW CHARTS

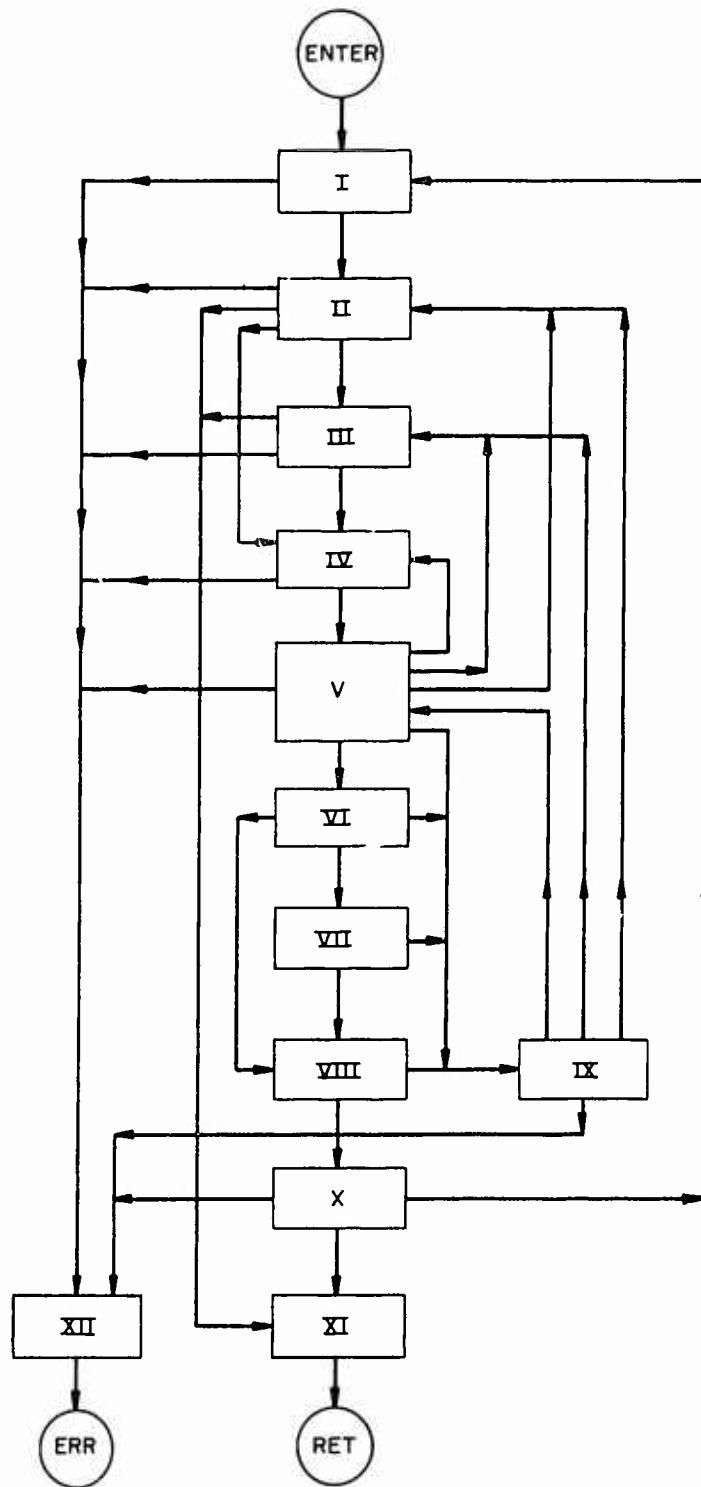
Detailed flow charts are presented for each block. Most line members of TRISL are accounted for except when so doing unduly complicates comprehension of the process.

B3. FLOW CHART SYMBOLS AND CONVENTIONS

- (a) Process entry/exit point.
- (b) Processing statements.
- (c) Decision trees, two or three way branches.
- (d) External procedures.
- (e) Numbers in the form Snnn refer to statement numbers in the program.
- (f) Numbers in the form nnn refer to line numbers of the program listing.
- (g) Entry points to a block are labelled generally with block designation state-number and line number specifying the source.
- (h) Exit points from a block are generally labelled by block designation, state-number, and line number specifying the destination.
- (i) Error exits are labelled by an error number and the error condition detected.
- (j) Exits from the bottom generally enter the next block at the top.
- (k) External call names and calling line numbers are contained within the external procedure symbols.

B4. PROGRAM LISTING

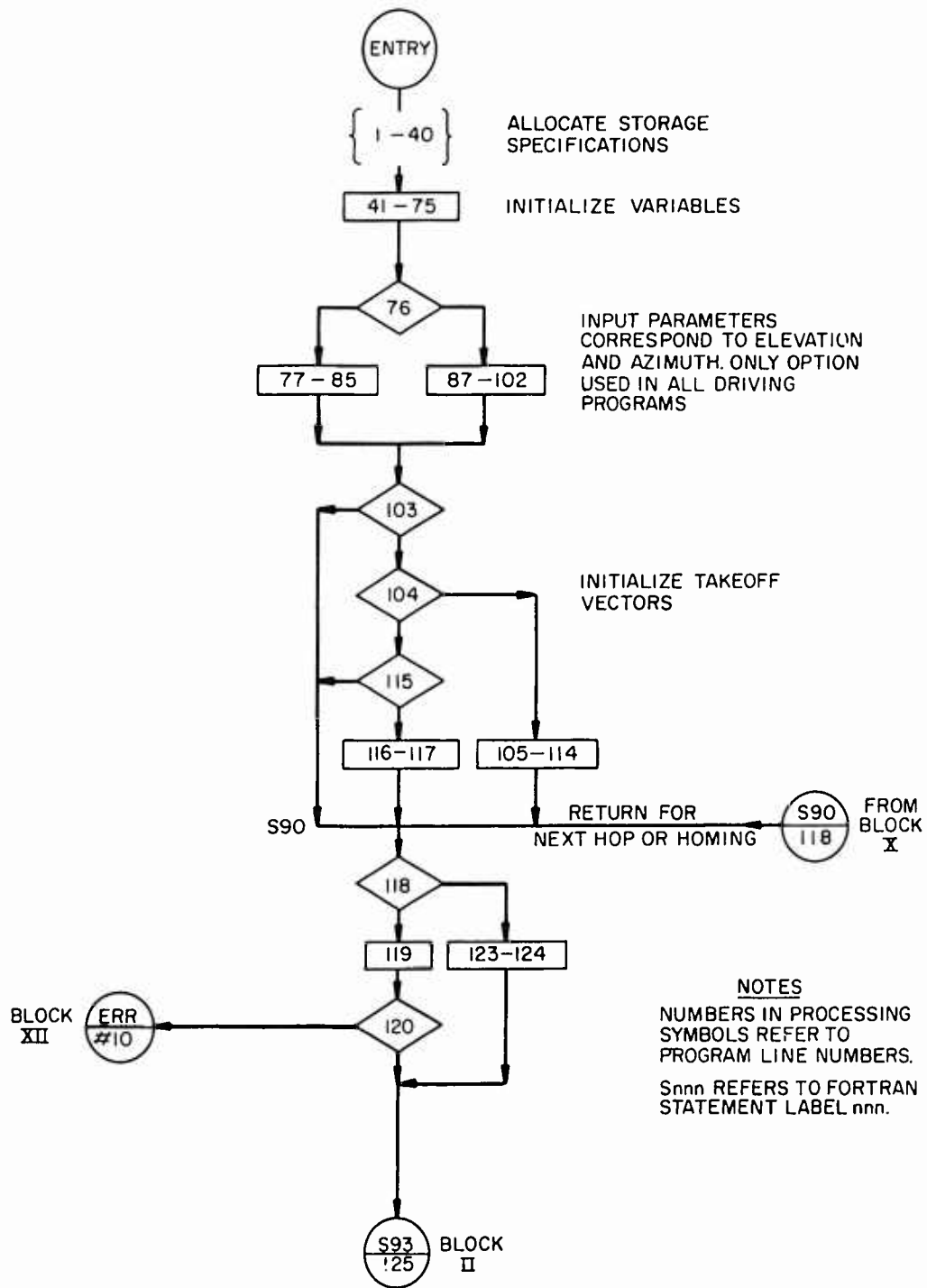
Listings are included for TRISL together with its externals.



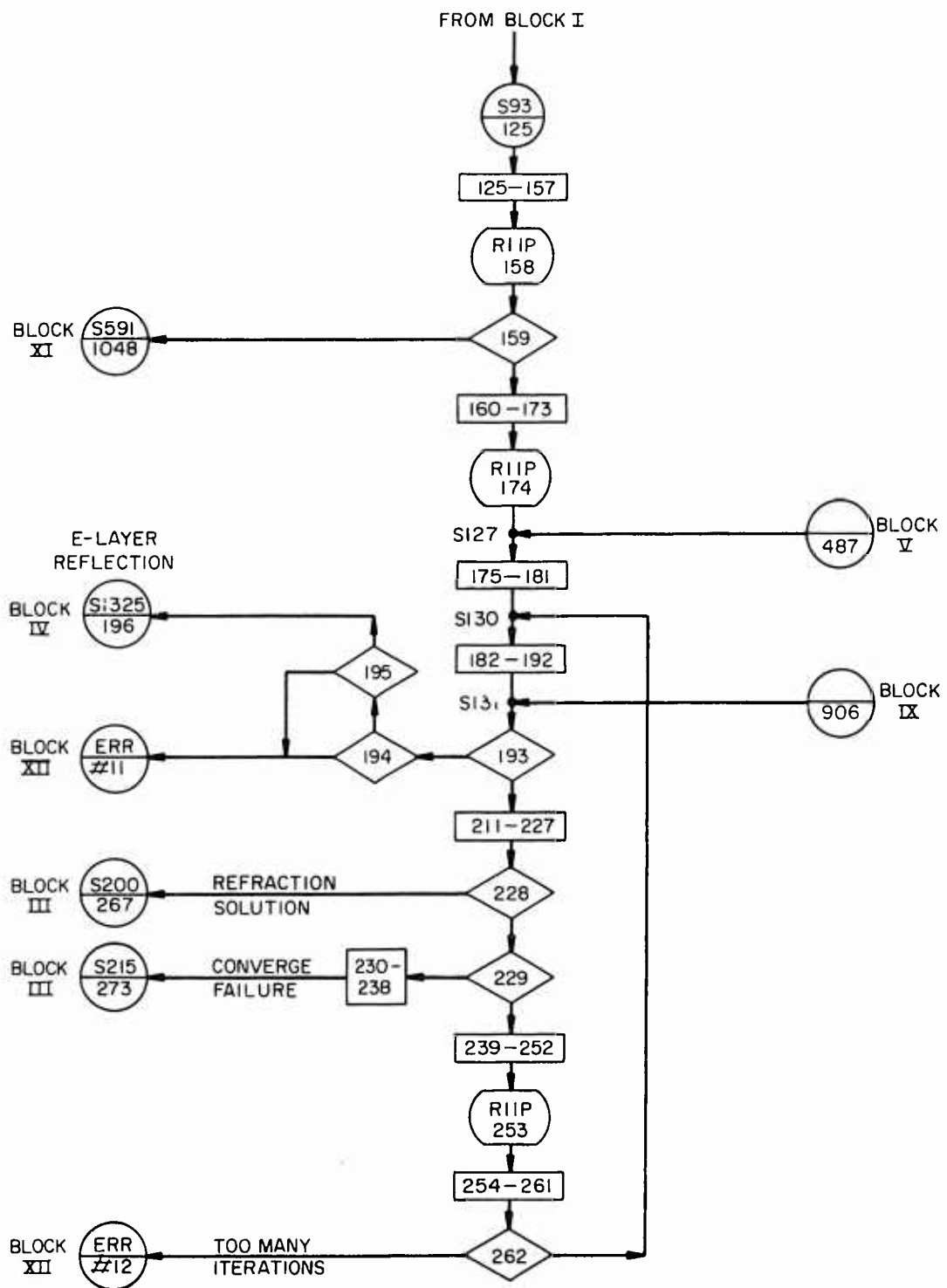
TRISL Block Diagram

TRISL: Block I, Argument List

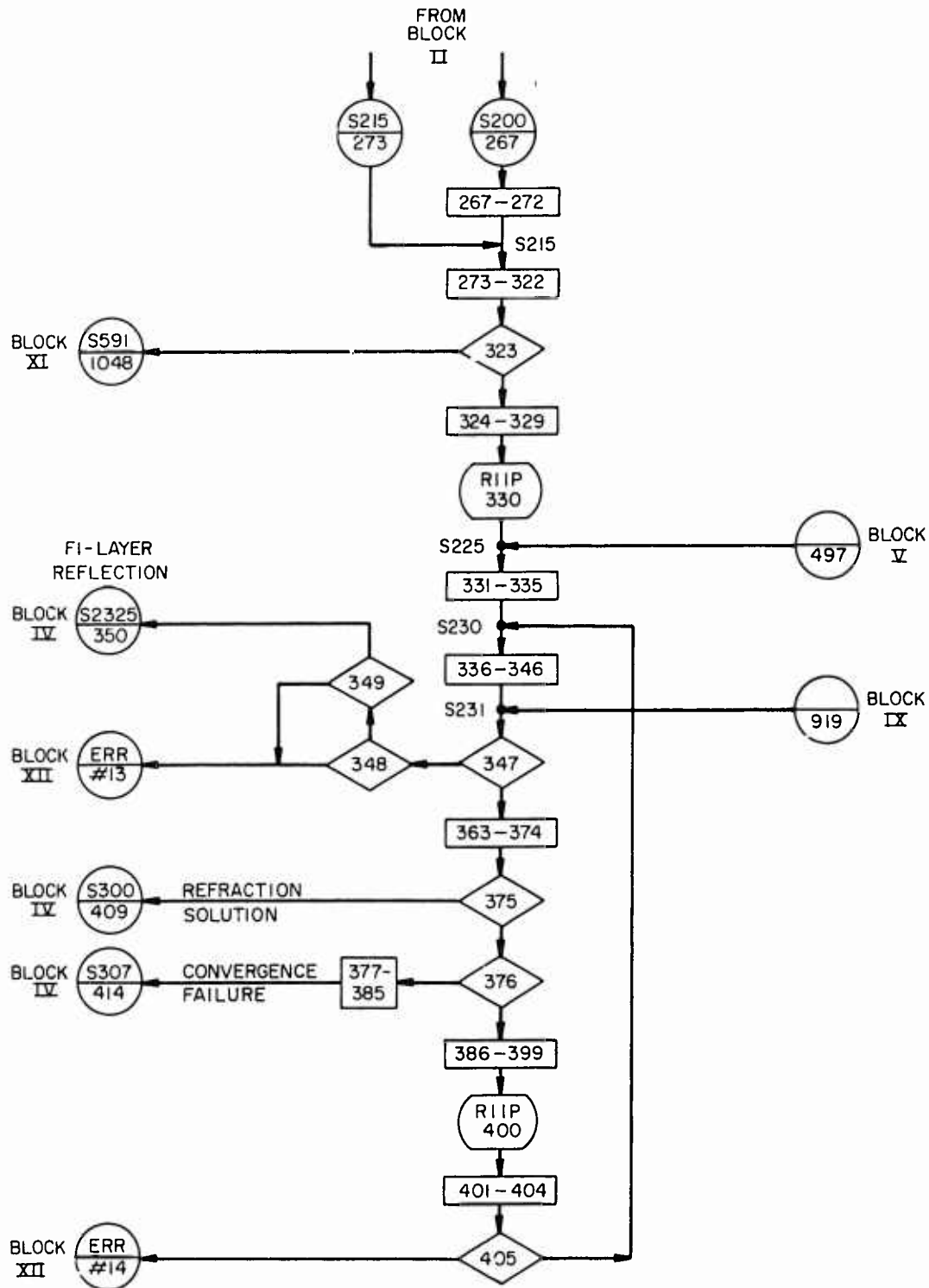
Element	I/D	Mnemonic	Type	Definition
1	I	MAI	Double	Geocentric Distance, Initial Point
2	I	NLAI	Double	North Latitude, Initial Point
3	I	WLAI	Double	West Longitude, Initial Point
4	I	NLAZ	Double	Takeoff Bearing (all calls) or Target North Latitude
5	I	WLAZ	Double	Takeoff Elevation (all calls) or Target West Longitude
6	I	MAZ	Double	Less than 6000 km (all calls) or Target Geocentric Distance
7	I	FREQ	Double	Frequency
8	I	MODE	Integer	MODE = Number of hops
9	I	RTARG	Double	= 6370 km, (all calls)
10	O	RS 2	Double	Geocentric Distance, End Point
11	O	NLTARG	Double	North Latitude, End Point
12	O	WLTARG	Double	West Longitude, End Point
13	O	PPTOT	Double	Phase Path Length
14	O	GPTOT	Double	Group Path Length
15	O	AZF	Double	Final to Initial Azimuth
16	O	ELF	Double	End Point Elevation
17	O	SRANGE	Double	Final-Initial Straight Line Distance
18	O	ELSR	Double	Takeoff Elevation
19	O	DIST	Double	Final-Initial Great Circle Ground Range
20	O	BEAR	Double	Initial to Final Azimuth
21	O	IGOBAK	Integer	Error Flag 8 = 0 No Error = 1 Fatal Error = 2 Penetrate



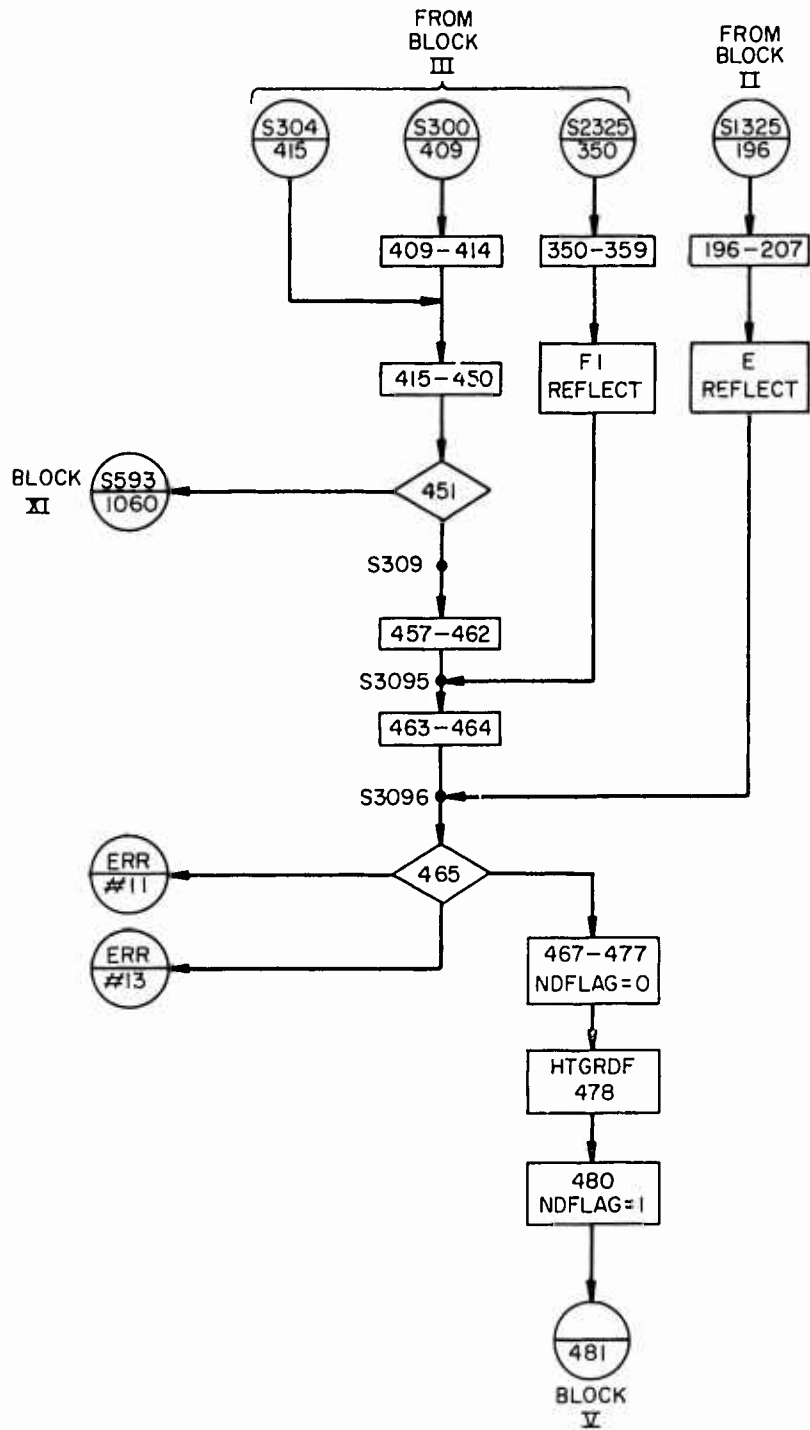
Block I, Initialization Procedures



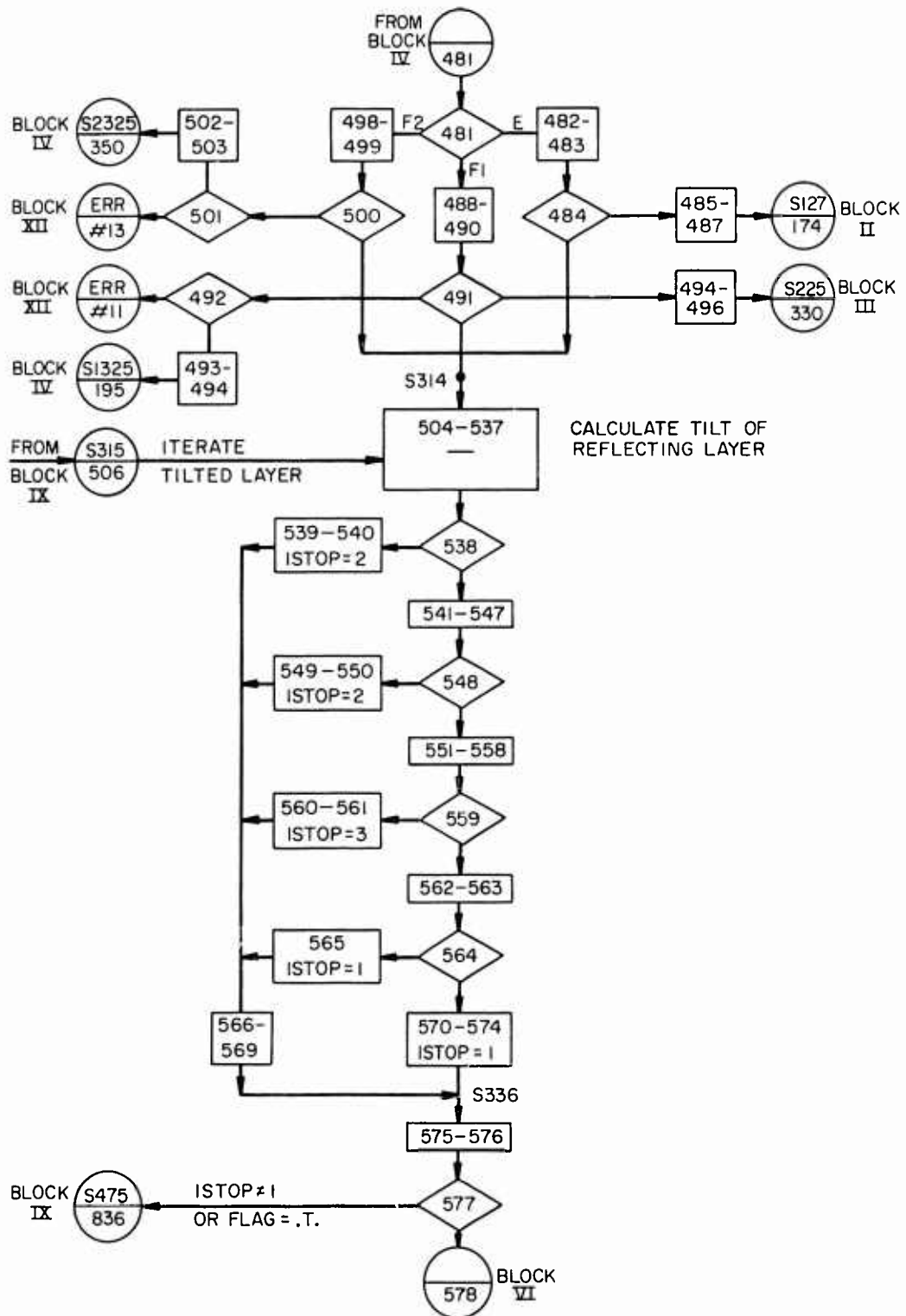
Block II, E-Layer Refraction Upwards



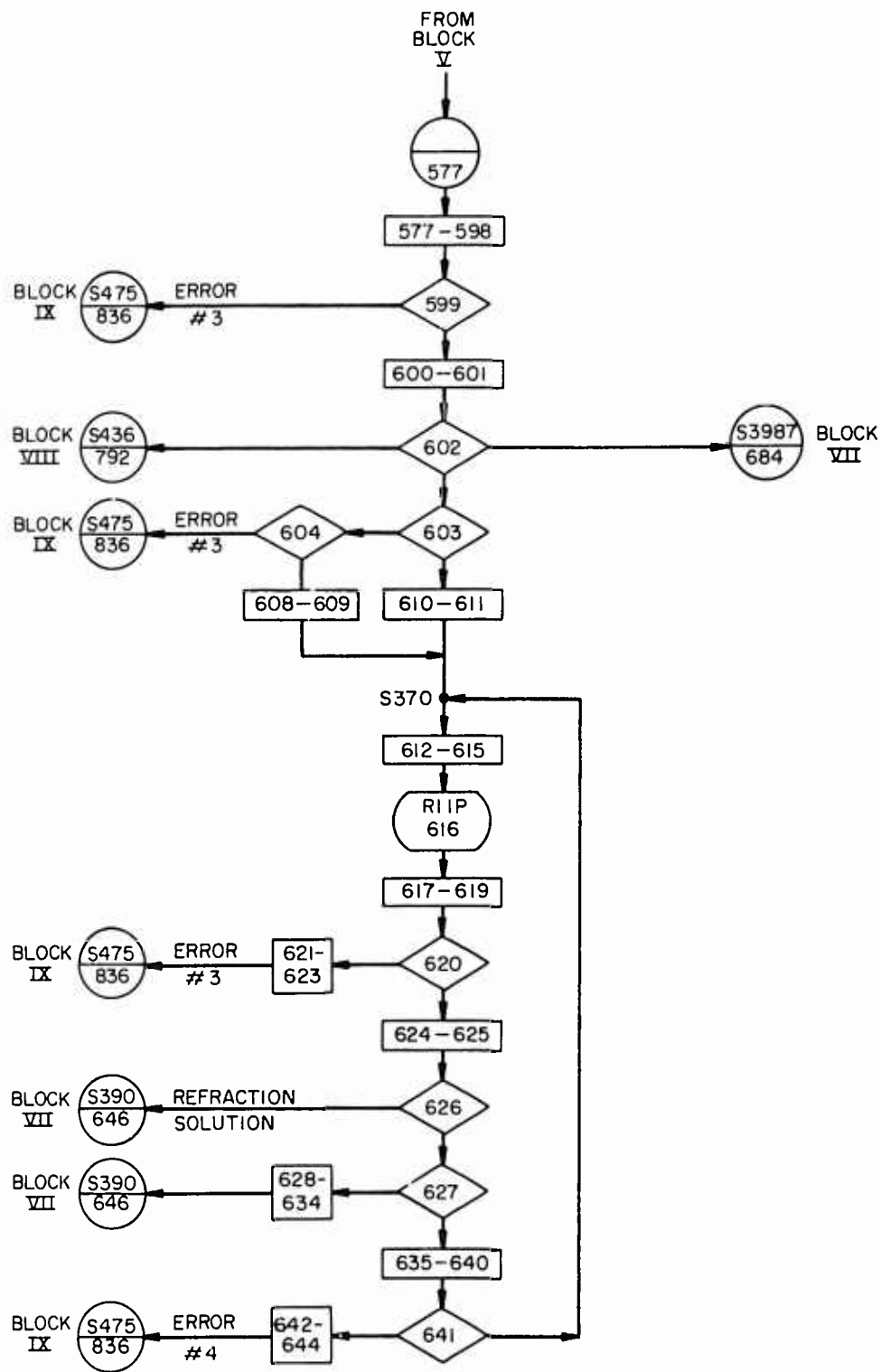
Block III, F_1 -Layer Refraction Upwards



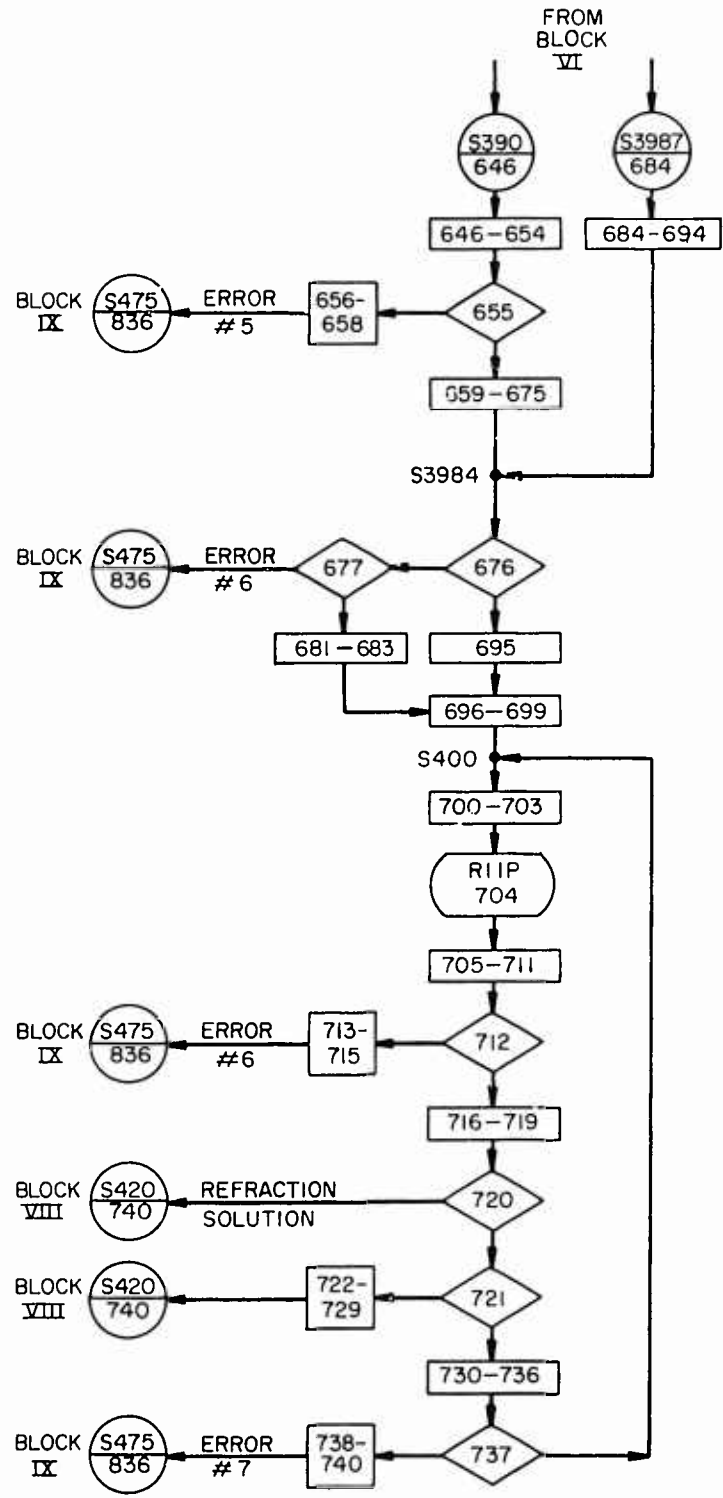
Block IV, Reflection Layer Initialization



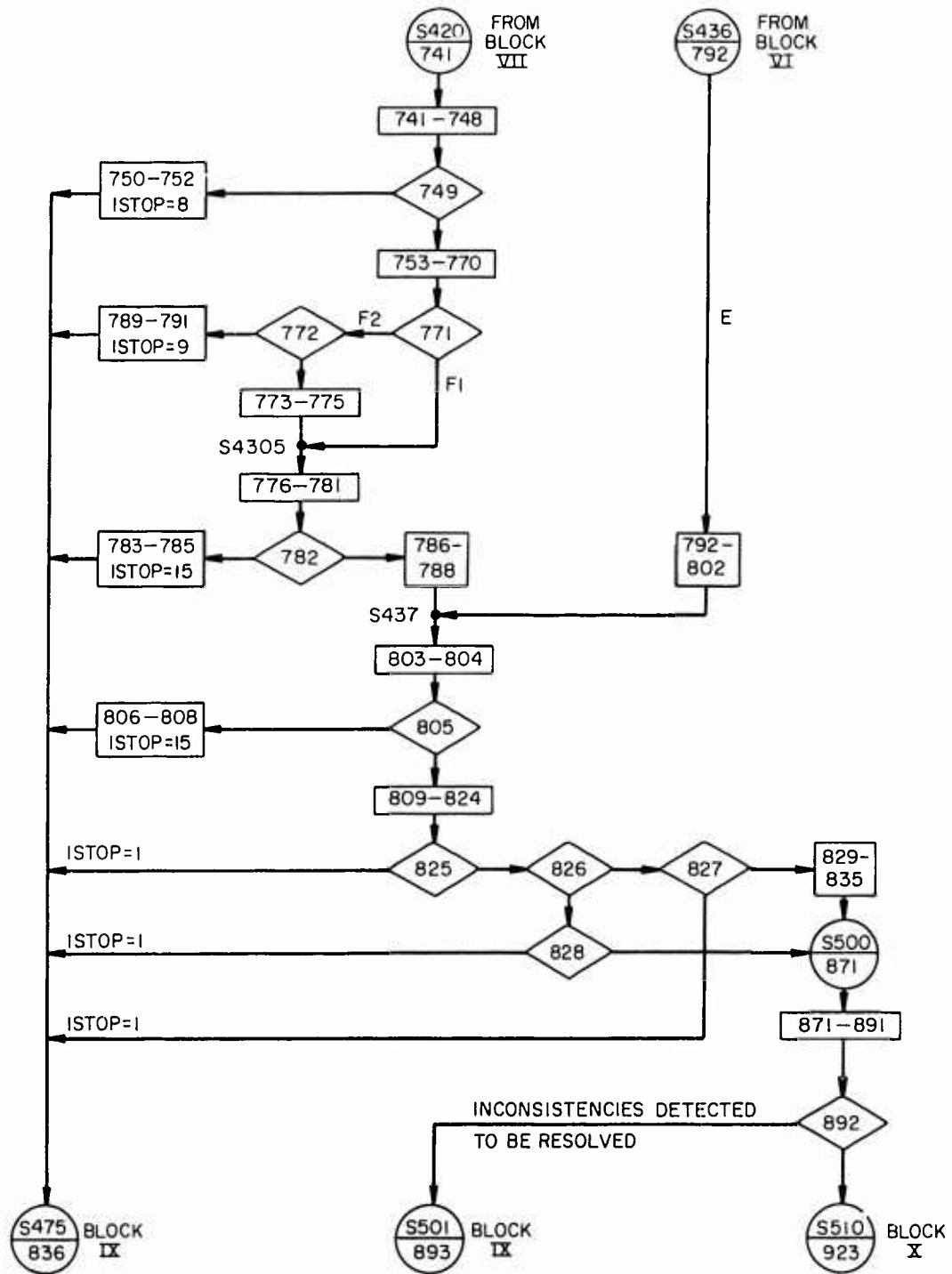
Block V, Tilt Calculation and Consistency Checks



Block VI, F₁-Layer Refraction Downwards

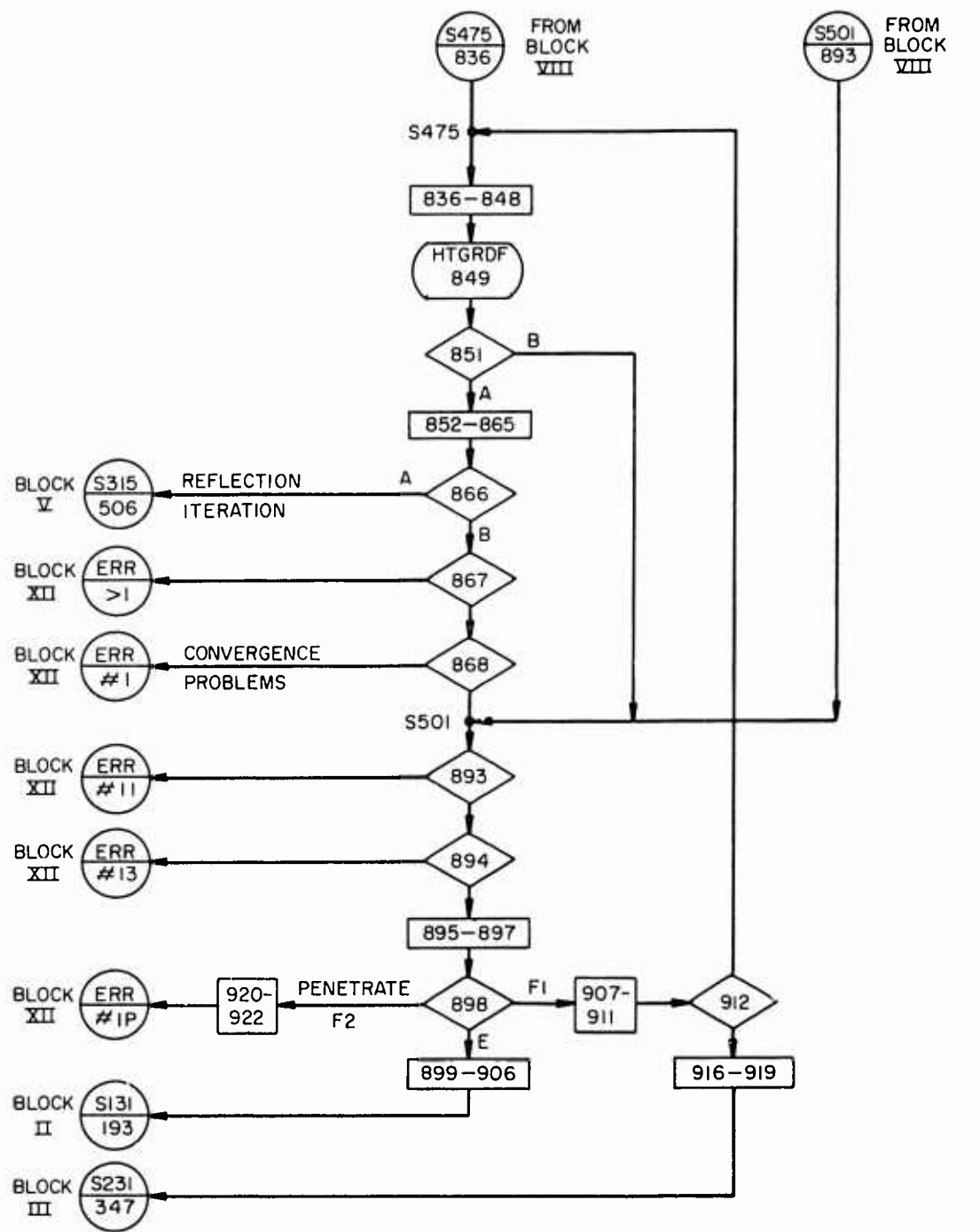


Block VII, E-Layer Refraction Downwards



NOTES
 BLOCK X EXIT IS DESIRED CONVERGENT SOLUTION TO
 TILTED LAYER ITERATION
 THE ISTOP=1 EXITS TO S475 ARE NORMAL. THE OTHER
 ERROR CONDITIONS MAY BE CORRECTED IN SUCCEEDING
 ITERATIONS

Block VIII, Error Checks

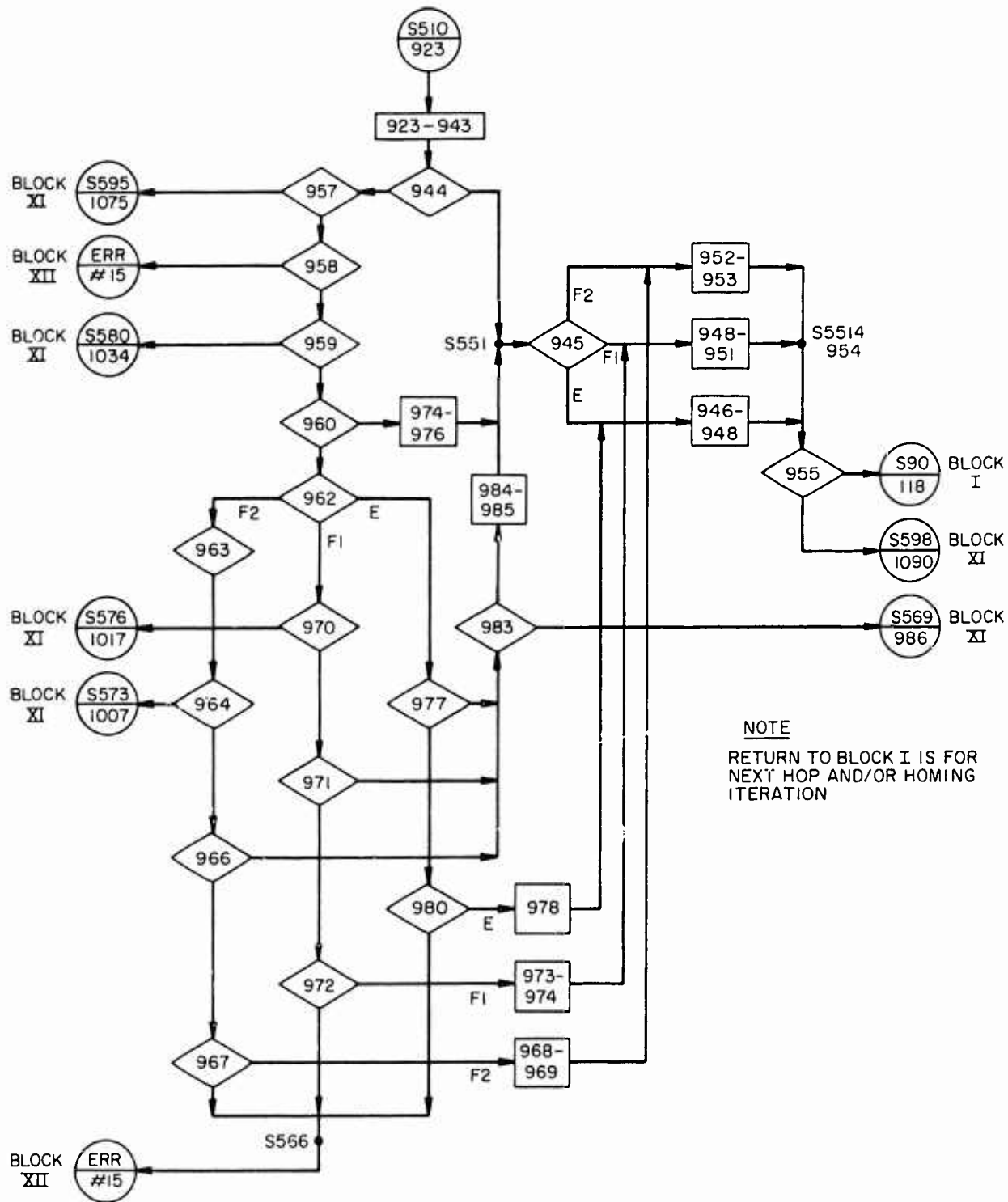


-851-
BRANCH B-INCONSISTENCY
BETWEEN HTGRDF AND
REST OF PROGRAM A PRO
PO REFLECTION LAYER

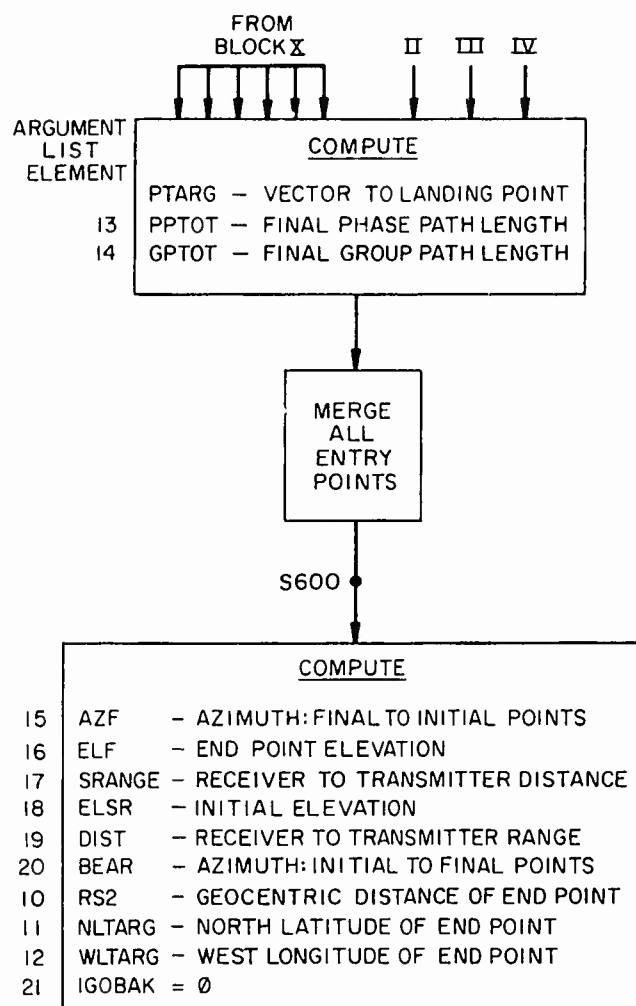
-866-
BRANCH B-
ITERATION LIMIT
EXCEEDED

-898-
E-E LAYER REFLECTION
F1-F1 LAYER REFLECTION
RETURNS TO BLOCK II OR
III TO RESOLVE INCON-
SISTENCIES DETECTED IN 851

Block IX, Iterate Reflection and Tilt



Block X, Traffic Control



Block XI, Normal Terminal Calculations

```

SUBROUTINE TRISL(MA1,NLA1,WLA1,NLA2,WLA2,MA2,FREQ,MODE,RTARG,RS2, TR2
*NLTARG,MLTARG,PPTOT,GPTOT,AZF,ELF,SRANGE,ELSR,DIST,BEAR,IGOBAK) TR2
IMPLICIT DOUBLE PRECISION (A-H,O-Z) TR2
LOGICAL HITS,FLAG,SEARCH,ASC,FLAG2,FLAG3,NOELAY,INCHOP,LP(6),NIP TR2
LOGICAL GPONLY TR2
DOUBLE PRECISION MESSPR TR2
DOUBLE PRECISION NLA1,MA1,NLA2,MA2,NLTARG,MAG,MA1B1,MB1,NLC1,NL4, TR2
1MRX1SQ,NLC2,MR3,NL8,NLC3,MN1,MA2C2,MC2,MA3C3,MC3,NLD,MRM1,MRM2, TR2
2MRY1SQ,MC4SQ,NLE,MRM3,MRM4,MC5SQ,NLW2,KP,L,N1,M,KPPP,LOC, TR2
3MAGVEC,NORTH(3),ME,MN,NORTH1(3),EAST1(3),MR2,MC1PSQ,M3000 TR2
REAL OUT2 TR2
DIMENSION S1(3),A1(3),B1(3),A11(3),EAST(3),MESSPR(15), TR2
* XI(3),KP(3),L(3,3),P1P(3),PC2(3),P8(3),R3(3),PC3(3),P10(3),C TR2
*2(3),PR1(3),N1(3),P0(3),A2(3),M(3,3),C3(3),A3(3),PHI(3),KPPP(3),P( TR2
*3,3),PD(3),PE(3),PQ(3),PW2(3),W2(3),PTARG(3), RN1(3),R2(3 TR2
*),PC1(3),P4(3) TR2
COMMON/FLIMSY/DIST1,ICNPRB /GPFLAG/GPONLY,IWRITE TR2
COMMON/CPREV/PQ,P,RT1,C52PPP,C53PPP,MRM1,CBETM1,MRM4,RY, TR2
2 DPP1P,MC5SQ,RM1,YY2PPP,ZY2PPP,H1,MC4SQ,MRY1SQ,YY1PPP, TR2
2 ZY1PPP,C42PPP,C43PPP,YS3PPP,ZS3PPP,C32PPP,RTM1,ONDR,DNDNL, TR2
3 DNDWL,D,GNU,PP2,PPEF1D,CBETM2,HE,PPF2,RV,HF1,PP2A,DPP2P, TR2
4 MB1,SBET1,GPF2,GPEF1D,DGP2P,DGP1P, TR2
5 F1,PREV(56),HITS,INCHOP,FLAG,FLAG2,FLAG3,NOELAY,LP TR2
COMMON/VECTRS/LOC(3,8),VEC(3,6),IREFL TR2
COMMON/NIPRIP/NIP TR2
*/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2,DUH(13 TR2
*),ID(3)/RTCOM/COS80,NUSE TR2
COMMON/REMHEN/INUSE,MNUSE(20),FCREF(20) TR2
DATA R,EPS1,EPS2,EPS3,EPS4,EPS5/6670.00,5*1.00/ TR2
DATA PI,RTD,OTR,R0/3.14159265358979300,57.2957795130823200, TR2
*.0174532925199433000,6370.00/ TR2
DATA LIMEA,LIMF1A,LIMF1D,LIMED,LIMF2/5*15/ TR2
DATA MESSPR/7HF2 ITER,8HBIG TILT,8HBIG TILT,9HF1-0 ITER, TR2
1 9HF1-D REFL,7HF1 MISS,8HE-D ITER,8HE-D REFL,6HE MISS, TR2
2 8HI-I REFL,9HE-F1 DUCT,8HE-A ITER,10HF1-F2 DUCT, TR2
3 9HF1-A ITER,9HMISS TARG/ TR2
WLN(ARG1,ARG2)=DSIGN(PI,ARG1)+PI-DATAN2(ARG1,ARG2) TR2
DACOS(ARG1)=DATAN2(DSQRT(1.00-ARG1**2),ARG1) TR2
DASIN(ARG1)=DATAN2(ARG1,DSQRT(1.00-ARG1**2)) TR2
INCHOP=.TRUE. TR2
HITS=.TRUE. TR2
ASC=MODE.EQ.0 TR2
SEARCH=ASC TR2
PP0=0.00 TR2
PPEF1A=0.00 TR2
DPP1=0.00 TR2
PP2A=0.00 TR2
PPF2=0.00 TR2
PP2=0.00 TR2
PPEF1D=0.00 TR2
DPP2P=0.00 TR2
PPP=0.00 TR2
PPTOT=0.00 TR2
GPTOT=0.00 TR2
GPEF1A=0.00 TR2
DGP1=0.00 TR2
DGP2=0.00 TR2

```

```

GPEF1A=0.00 TR2
GPF2=0.00 TR2
GPEF1D=0.00 TR2
DGP2P=0.00 TR2
DGP1F=0.00 TR2
ICNPRB=0 TR2
INISE=0 TR2
IGOBK=0 TR2
IHOPS=0 TR2
RS2=RTARG TR2
CN=DCOS(NLA1*DTR) TR2
SN=DSIN(NLA1*DTR) TR2
CW=DCOS(WLA1*DTR) TR2
SW=DSIN(WLA1*DTR) TR2
A1(1)=CN*CW TR2
A1(2)=-CN*SW TR2
A1(3)=SN TR2
IF(MA2.LT.6000.00) GO TO 50 TR2
CN=DCOS(NLA2*DTR) TR2
DO 45 I=1,3 TR2
A11(I)=MA1*A1(I) TR2
45 A1(I)=A11(I) TR2
B1(1)=MA2*DCOS(WLA2*DTR)*CN-A1(1) TR2
B1(2)=-MA2*DSIN(WLA2*DTR)*CN-A1(2) TR2
B1(3)=MA2*DSIN(WLA2*DTR)-A1(3) TR2
MB1=MAG(B1) TR2
DTA1B1=DOT(A1,B1) TR2
GO TO 60 TR2
C WHEN MA2 IS INPUTTED AS A NUMBER LESS THAN 6000, NLA2 IS ASSUMED TR2
C TO BE THE BEARING,AND WLA2 IS ASSUMED TO BE THE TAKE-OFF ANGLE TR2
50 EAST1(1)=SW TR2
EAST1(2)=CW TR2
EAST1(3)=0.00 TR2
CALL CROSS(A1,EAST1,NORTH1) TR2
CAZ=DCOS(NLA2*DTR) TR2
SAZ=DSIN(NLA2*DTR) TR2
CEL=DCOS(WLA2*DTR) TR2
SEL=DSIN(WLA2*DTR) TR2
DO 55 I=1,3 TR2
B1(I)=CEL*(CAZ*NORTH1(I)+SAZ*EAST1(I))+SEL*A1(I) TR2
A11(I)=MA1*A1(I) TR2
55 A1(I)=A11(I) TR2
MB1=1.00 TR2
DTA1B1=SEL*MA1 TR2
60 IF(DABS(MA1-R0).LE.1.0-5) GO TO 90 TR2
IF(DASIN(R0/MA1)-DACOS(-DTA1B1/(MA1*MB1)))88,88,80 TR2
80 T1=(-DTA1B1-DSQRT(DTA1B1**2-DOT(B1,B1)*(DOT(A1,A1)-R0**2))) TR2
*/DOT(B1,B1) TR2
DO 85 J=1,3 TR2
85 A1(J)=B1(J)*T1+A1(J) TR2
A=-2.00*DOT(A1,B1)/DOT(A1,A1) TR2
DO 87 J=1,3 TR2
87 B1(J)=B1(J)+A*A1(J) TR2
PPTOT=T1*MB1 TR2
GPTOT=PPTOT TR2
GO TO 90 TR2
88 IF(DTA1B1.GE.0.00)GO TO 90 TR2

```



```

          PPTOT=-2.00*DTA1B1/MB1
          GPTOT=PPTOT
90      IF(INCHOP) GO TO 92
          IONREF=IONREF+1
          IF(IONREF.LT.40) GO TO 93
          ISTOP=10
          GO TO 7310
92      IONREF=0
          IHOPS=IHOPS+1
93      PREV(13)=0.00
C      START OF E LAYER REFRACTION
          NIP=.FALSE.
          INT=0
          INUSE=INUSE+1
          FLAG=.FALSE.
          FLAG2=.FALSE.
          CALL CROSS(A1,B1,XI)
          CALL CROSS(XI,B1,KP)
          MA1B1=MAG(XI)
          MB1=MAG(B1)
          A1MAG=MAG(A1)
C      EQN(2)
          DO 100 J=1,3
          L(1,J)=XI(J)/MA1B1
          L(2,J)=B1(J)/MB1
100     L(3,J)=KP(J)/(4*A1B1*MB1)
          Y5P=0.00
          Z5P=0.00
C      EQN(9)
          P1P(1)=0.00
          DO 110 I=2,3
110     P1P(I)=L(I,1)*A1(1)+L(I,2)*A1(2)+L(I,3)*A1(3)
          YC1P=DSQRT(B**2-P1P(3)**2)
C      EQN(12)
          DO 120 J=1,3
120     PC1(J)=L(2,J)*YC1P+L(3,J)*P1P(3)
C      EQN(14,15)
          NLC1=DASIN(PC1(3)/B)
          WLC1=WLCN(PC1(2),PC1(1))
C      EQN(17)
          BETAC1=DASIN(DOT(PC1,B1)/(MB1*B))
          BCBC1=B*DCOS(BETAC1)
125     CALL RIIP(R0,NLC1,WLC1,PLASD)
          IF(SEARCH.AND.ASC.AND.RTARG.GT.BCBC1.AND.RTARG.LE.R0+HBE) GOTO 591
          NIP=.TRUE.
          NOELAY=.FALSE.
          IF(FCE.GT.0.00) GO TO 126
          FCE=1.D-2
          NOELAY=.TRUE.
126     RM=R0+HBE+HAE
          H=HAE
          F=FREQ/FCE
          Y3P=DSQRT(RM**2-P1P(3)**2)
          YBEP=DSQRT((R0+HBE)**2-P1P(3)**2)
1265    PC1(J)=L(2,J)*Y3P+L(3,J)*P1P(3)
          NLC1= DASIN(PC1(3)/RM)

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      WLC1=WLON(PC1(2),PC1(1))
      CALL RIIP(R0,WLC1,WLC1,PLASD)
127  RM=HBE+HAE+R0
      H=HAE
      NOELAY=.FALSE.
      IF(FCE.GT.0.00)GO TO 129
      FCE=1.0-2
      NOELAY=.TRUE.
129  F=FREQ/FCE
130  IF(.NOT.FLAG)GO TO 1305
      CBET1= DABS(Z10PP)/RM
      SBET1=DSQRT(1.00-CBET1**2)
      Y3P=RM*SBET1
      YBEP=(R0+HBE)*SBET1
      GO TO 131
1305 Y3P=DSQRT(RM**2-P1P(3)**2)
      YBEP=DSQRT((R0+HBE)**2-P1P(3)**2)
C   EQN(18)
      CBET1=BCBC1/RM
      SBET1=DSQRT(1.00-CBET1*CBET1)
131  IF(F*SBET1.GT.1.00) GO TO 135
      IF(FLAG) GO TO 134
132  IF(FLAG2) GO TO 134
1325 IREFL=1
      RM=R0+HBE+HAE
      MR3=A1MAG
      SIN02=DOT(A1,B1)/(MB1*A1MAG)
      COS02=DSQRT(1.00-SIN02**2)
      Y9P=P1P(2)
      Z9P=P1P(3)
      C22P=L(2,1)*B1(1)+L(2,2)*B1(2)+L(2,3)*B1(3)
      C23P=L(3,1)*B1(1)+L(3,2)*B1(2)+L(3,3)*B1(3)
      Y10P=COS02*(Y9P*COS02+Z9P*SIN02)
      Z10P=COS02*(Z9P*COS02-Y9P*SIN02)
      GO TO 3096
134  FLAG=.FALSE.
      ISTOP=11
      GO TO 7310
135  IF(.NOT.NOELAY) GO TO 137
      Y4P=Y3P
      DGP1=0.00
      Z4P=P1P(3)
      GO TO 139
137  DGP1=-H/SBET1+H*F/2.00*DLOG((F*SBET1+1.00)/(F*SBET1-1.00))
      GAM1=CBET1*DGP1/RM
      Y4P=Y3P*DCOS(GAM1)-P1P(3)*DSIN(GAM1)
      Z4P=P1P(3)*DCOS(GAM1)+Y3P*DSIN(GAM1)
C   DIST BETWEEN SUCCESSIVE R<S
139  DISTB=DSQRT((Y4P-Y5P)**2+(Z4P-Z5P)**2)
      IF(FLAG) GO TO 141
      DO 140 J=1,3
140  P4(J)=L(2,J)*Y4P+L(3,J)*Z4P
      GO TO 1418
141  DO 1413 J=1,3
1413 P4(J)=M(2,J)*Y4P+M(3,J)*Z4P+P0(J)
1418 IF(DISTB.LE.EPS1) GO TO 200
      IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 145

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      OUT2=DISTA
      IF(IWRITE.EQ.1) WRITE(6,142) OUT2,IHOPS
142  FORMAT(24H E-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3)
      H=HP
      Y3P=Y3PP
      RM=RMP
      DGP1=GPP
      F=FP
      GO TO 215
145  NL4=DASIN(P4(3)/MAG(P4))
      WL4=WLON(P4(2),P4(1))
      DISTA=DISTB
      GPP=DGP1
      Y5P=Y4P
      Z5P=Z4P
      HP=H
      FP=F
      Y3PP=Y3P
      RMP=RM
      SIN01=SBET1
      COS01=CBET1
      DO 148 J=1,3
148  R2(J)=P4(J)
      CALL RIIP(R0,NL4,WL4,PLASD)
      NOELAY=.FALSE.
      IF(FCE.GT.0.00) GO TO 149
      FCE=1.0-2
      NOELAY=.TRUE.
149  RM=HBE+HAE*R0
      H=HAE
      F=FREQ/FCE
      INT=INT+1
      IF(INT.LE.LIMEA) GO TO 130
      ISTOP=12
      GO TO 7310
C     END OF E LAYER REFRACTION
C     START OF F1 LAYER REFRACTION
200  Y5P=Y4P
      Z5P=Z4P
      SIN01=SBET1
      COS01=CBET1
      DO 210 J=1,3
210  R2(J)=P4(J)
215  MR2=RM
      RR1=MR2-H
      SIN01P=SIN01
      COS01P=COS01
      Y6P=COS01*(Y5P*COS01+Z5P*SIN01)
      Z6P=COS01*(Z5P*COS01-Y5P*SIN01)
      IF(.NOT.FLAG) GO TO 2155
      DO 2151 J=1,3
2151 P4(J)=H(2,J)*Y3P+H(3,J)*Z10PP
      RR1=-H/MAG(P4)
      DO 2152 J=1,3
2152 P4(J)=R2(J)+RR1*P4(J)
      RR1=MAG(P4)
      MR2=MAG(R2)

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COS01P=BCBC1/MR2
SIN01P=DSQRT(1.00-COS01P**2)
DO 2153 J=1,3
P4(J)=M(2,J)*Y6P+M(3,J)*Z6P+P0(J)
2153 P8(J)=R2(J)-P4(J)
CALL CROSS(R2,P8,XI)
CALL CROSS(XI,P8,KP)
CNST=MAG(XI)
FLOG=MAG(P8)
DO 2154 J=1,3
L(1,J)=XI(J)/CNST
L(2,J)=P8(J)/FLOG
2154 L(3,J)=KP(J)/(CNST*FLOG)
Y5P=L(2,1)*R2(1)+L(2,2)*R2(2)+L(2,3)*R2(3)
Z5P=L(3,1)*R2(1)+L(3,2)*R2(2)+L(3,3)*R2(3)
Y6P=L(2,1)*P4(1)+L(2,2)*P4(2)+L(2,3)*P4(3)
Z6P=L(3,1)*P4(1)+L(3,2)*P4(2)+L(3,3)*P4(3)
FLAG=.FALSE.
2155 INT=0
FLAG3=.FALSE.
HEA=H
HE=H
PPEF1A=0.00
IF(.NOT.NOELAY)PPEF1A=H*(.500*SIN01-1.00/SIN01+F/4.00*(1.00-F**(-2
)+COS01**2)*DLOG((F*SIN01+1.00)/(F*SIN01-1.00)))
JPP1=PPEF1A
PP0=RR1*DSQRT(1.00-(COS01P*MR2/RR1)**2)
1AU1EA=MR2*SIN01P-PP0
IF(.NOT.HITS.OR.COS01P*MR2/A1MAG.GE.1.00) GO TO 217
PP0=PP0-A1MAG*DSQRT(1.00-(COS01P*MR2/A1MAG)**2)
217 C12P=Y5P-Y6P
C13P=Z5P-Z6P
MC1PSQ=C12P**2+C13P**2
MRX1SQ=BCBC1**2
218 RM=R0+HBE+HAE+HAF1
TC2=DSQRT((RM**2-MRX1SQ)/MC1PSQ)
IF(SEARCH.AND.RTARG.GT.DSQRT(MRX1SQ).AND.RTARG.LE.RR1) GO TO 591
YC2P=C12P*TC2+Y6P
ZC2P=C13P*TC2+Z6P
DO 220 J=1,3
220 PC2(J)=L(2,J)*YC2P+L(3,J)*ZC2P
NLC2= DABS(PC2(3)/RM)
WLC2=WLON(PC2(2),PC2(1))
CALL PIIF(R0,NLC2,WLC2,PLASD)
225 RM=R0+HBE+HAE+HAF1
H=HAF1
F=FREQ/FCF1
Y9P=0.00
Z9P=0.00
230 IF(.NOT.FLAG) GO TO 2305
CBET4= DABS(Z10PP)/RM
SBET4=DSQRT(1.00-CBET4**2)
Y7P=RM*SBET4
GO TO 231
2305 TDEL3=DSQRT((RM**2-MRX1SQ)/MC1PSQ)
Y7P=C12P*TDEL3+Y6P
Z7P=C13P*TDEL3+Z6P

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      MR3=RM
      CBET4=BCBC1/MR3
      SBET4=DSQRT(1.00-CBET4*CBET4)
231  IF(F*SBET4.GT.1.00) GO TO 235
      IF(FLAG) GO TO 234
232  IF(FLAG3) GO TO 234
2325  IREFL=2
      RM=R0+H9E+HAE+HAF1
      Y9P=Y5P
      Z9P=Z5P
      MR3=MR2
      COS02=COS01
      SIN02=SIN01
      Y10P=COS02*(Y9P*COS02+Z9P*SIN02)
      Z10P=COS02*(Z9P*COS02-Y9P*SIN02)
      GO TO 3095
234  FLAG=.FALSE.
      ISTOP=13
      GO TO 7310
235  DGP2=H*(F/2.00*DLOG((F*SBET4+1.00)/(F*SBET4-1.00))-1.00/SBET4)
      GAM2=CBET4*DGP2/RM
      Y8P=Y7P*DCOS(GAM2)-Z7P*DSIN(GAM2)
      Z8P=Z7P*DCOS(GAM2)+Y7P*DSIN(GAM2)
C   DIST BETWEEN SUCCESSIVE R<S
      DISTB=DSQRT((Y8P-Y9P)**2+(Z8P-Z9P)**2)
      IF(FLAG) GO TO 241
      DO 240 J=1,3
240  P8(J)=L(2,J)*Y8P+L(3,J)*Z8P
      GO TO 2425
241  DO 242 J=1,3
242  P8(J)=M(2,J)*Y8P+M(3,J)*Z8P+P0(J)
2425  IF(OISTB.LE.EPS2) GO TO 300
      IF(INT.LE.1.OR.DISTB.LT.OISTA)GO TO 245
      OUT2=OISTA
243  IF(IWRITE.EQ.1)WRITE(6,243)OUT2,IHOPS
      FORMAT(25H F1-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3)
      H=HP
      F=FP
      Y7P=Y7PP
      RM=RMP
      DGP2=GPP
      GO TO 307
245  NL8= DASIN(P8(3)/MAG(P8))
      WL8=WLON(P8(2),P8(1))
      Y9P=Y8P
      Z9P=Z8P
      HP=H
      FP=F
      Y7PP=Y7P
      RMP=RM
      GPP=DGP2
      COS02=CBET4
      SIN02=SBET4
      DO 247 J=1,3
247  R3(J)=P8(J)
      OISTA=DISTB
      CALL RIIP(R0,NL8,WL8,PLASD)

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      RM=R0+H0E+HAE+HAF1
      H=HAF1
      F=FREQ/FCF1
      INT=INT+1
      IF(INT.LE.LIMF1A) GO TO 230
      ISTOP=14
      GO TO 7310
C   END OF F1 LAYER REFRACTION
300  Y9P=Y8P
      Z9P=Z8P
      SIN02=SBET4
      COS02=CBET4
      DO 305 J=1,3
305  R3(J)=P8(J)
307  MR3=RM
      IREFL=3
      RM=R0+HMF2
      RR2=MR3-H
      Y10P=COS02*(Y9P*COS02+Z9P*SIN02)
      Z10P=COS02*(Z9P*COS02-Y9P*SIN02)
      COS02P=COS02
      SIN02P=SIN02
      IF(.NOT.FLAG) GO TO 3075
      DO 3071 J=1,3
3071 P8(J)=M(2,J)*Y7P+M(3,J)*Z10P+P0(J)
      RR2=-H/MAG(P8)
      DO 3072 J=1,3
3072 P8(J)=R3(J)+RR2*P8(J)
      RR2=MAG(P8)
      MR3=MAG(R3)
      COS02P=BCRC1/MR3
      SIN02P=DSQRT(1.00-COS02P**2)
      DO 3073 J=1,3
3073 P4(J)=R3(J)-P8(J)
      CALL CROSS(R3,P4,XI)
      CALL CROSS(XI,P4,KP)
      CNST=MAG(XI)
      FLOG=MAG(P4)
      DO 3074 J=1,3
3074 L(1,J)=XI(J)/CNST
      L(2,J)=P4(J)/FLOG
      L(3,J)=KP(J)/(CNST*FLOG)
      Y9P=L(2,1)*R3(1)+L(2,2)*R3(2)+L(2,3)*R3(3)
      Z9P=L(3,1)*R3(1)+L(3,2)*R3(2)+L(3,3)*R3(3)
      Y10P=L(2,1)*P8(1)+L(2,2)*P8(2)+L(2,3)*P8(3)
      Z10P=L(3,1)*P8(1)+L(3,2)*P8(2)+L(3,3)*P8(3)
      FLAG=.FALSE.
3075 DO 308 J=1,3
308  PREV(J)=0.00
      IF(.NOT.SEARCH) GO TO 309
      IF(RTARG.GT.RR1.AND.RTARG.LE.MR2) GO TO 593
      IF(IREFL.EQ.1) GO TO 309
      IF(MR2.LE.RR2.AND.RTARG.LE.RR2.AND.RTARG.GT.MR2) GO TO 593
      IF(RR1.GT.MR3.AND.RTARG.LE.RR1.AND.RTARG.GT.MR3) GO TO 593
C   TILTED F2 LAYER
309  HF1A=H

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      HF1=H
      TAU=MR3*SINO2P-RR2*DSQRT(1.00-(MR3/RR2*COS02P)**2)+TAU1EA
      PPEF1A=PPEF1A+H*(.500*SINO2+F/4.00*(1.00-F**(-2)+COS02**2)*DLOG((F
      **SINO2+1.00)/(F*SINO2-1.00))-1.00/SINO2)+TAU
      GPEF1A=OGP1+OGP2+TAU
3095  C22P=Y9P-Y10P
      C23P=Z9P-Z10P
3096  TC3=(RM**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2)
      IF(TC3.LT.0.00)GO TO (134,134,234),IREFL
      TC3=DSQRT(TC3)
      YC3P=C22P*TC3+Y10P
      ZC3P=C23P*TC3+Z10P
      DO 310 J=1,3
      PC3(J)=L(2,J)*YC3P+L(3,J)*ZC3P
      P10(J)=L(2,J)*Y10P+L(3,J)*Z10P
310   C2(J)=L(2,J)*C22P+L(3,J)*C23P
      BETA22=0.00
      NLC3=DASIN(PC3(3)/RM)
      WLC3=WLON(PC3(2),PC3(1))
      NOFLAG=0
      CALL HTGRDF(NDFLAG,FREQ,RTD*NLC3,RTD*WLC3,RTD*DACOS(BCBC1/RM),0.
      *00,RM,RM1,RT1,RTM1,ONDR,DNDNL,DNDWL,PNTFLG)
      NOFLAG=1
      GO TO (311,312,313),IREFL
311   F1=FREQ/FCE
      H1=HAE
      IF(NUSE.EQ.1)GO TO 314
      FLAG2=.TRUE.
      INT=0
      GO TO 127
312   F1=FREQ/FCF1*.86602540378443900
      RM1=RM1+HAF1
      H1=HAF1*2.00
      GO TO (3123,314,3125),NUSE
3123  IF(FLAG2)GO TO 134
      FLAG2=.TRUE.
      GO TO 1325
3125  FLAG3=.TRUE.
      INT=0
      GO TO 225
313   F1=FREQ/FCF2
      H1=HAF2
      IF(NUSE.EQ.3)GO TO 314
      IF(FLAG3)GO TO 234
      FLAG3=.TRUE.
      GO TO 2325
314   INTF2=0
      IRCYCL=0
315   COPHC3=PC3(3)/RM
      SIPHC3=DSQRT(1.00-COPHC3**2)
      NNUSE(INUSE)=NUSE
      FCREP(INUSE)=FREQ/F1
C     CORRECTION IN F1 CRITICAL PRINT OUT
      IF(NUSE.EQ.2)FCREP(INUSE)=FCF1
      COTH3=PC3(1)/DSQRT(PC3(1)**2+PC3(2)**2)
      SITH3=PC3(2)/DSQRT(PC3(1)**2+PC3(2)**2)
      PR1(1)=RTM1*COTH3*SIPHC3

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PR1(2)=RTM1*SITHC3*SIPHC3 TR2
PR1(3)=RTM1*COPHC3 TR2
N1(1)=COTH3*SIPHC3*DNDR-COTH3*COPHC3*DNONL/RTM1+SITHC3*DNONL/(RT TR2
*M1*SIPHC3) TR2
N1(2)=SITHC3*SIPHC3*DNDR-SITHC3*COPHC3*DNONL/RTM1-COTH3*DNONL/(RT TR2
*M1*SIPHC3) TR2
N1(3)=COPHC3*DNDR+SIPHC3*DNONL/RTM1 TR2
MN1=MAG(N1) TR2
T0=-RTM1/MN1 TR2
ISTOP=1 TR2
DO 320 J=1,3 TR2
P0(J)=N1(J)*T0+PR1(J) TR2
320 A2(J)=P10(J)-P0(J) TR2
CALL CROSS(A2,C2,XI) TR2
CALL CROSS(XI,C2,KP) TR2
MA2C2=MAG(XI) TR2
MC2=MAG(C2) TR2
DO 330 J=1,3 TR2
M(1,J)=XI(J)/MA2C2 TR2
M(2,J)=C2(J)/MC2 TR2
330 M(3,J)=KP(J)/(MA2C2*MC2) TR2
Z10PP=M(3,1)*A2(1)+M(3,2)*A2(2)+M(3,3)*A2(3) TR2
RB=RM1-H1 TR2
IF(PB.GE.DABS(Z10PP))GO TO 332 TR2
ISTOP=2 TR2
GO TO 3345 TR2
332 COBETB= NABS(Z10PP)/RB TR2
SIBETB=DSQRT(1.00-COBETB**2) TR2
YS1PP=RB*SIBETB TR2
DO 333 J=1,3 TR2
333 S1(J)=M(2,J)*YS1PP+M(3,J)*Z10PP+P0(J) TR2
R4=MAG(S1) TR2
PP2=1.00-(MR3/R4*COS02)**2 TR2
IF(PP2.GE.0.00) GO TO 3331 TR2
ISTOP=2 TR2
GO TO 3345 TR2
3331 PP2=R4*DSQRT(PP2)-MR3*SIN02 TR2
PP2A=PP2 TR2
IF(IREFL.GT.1) GO TO 3336 TR2
IF(HITS) GO TO 3334 TR2
PP0=R4*DSQRT(1.00-(MR3/R4*COS02)**2) TR2
GO TO 3336 TR2
3334 PP0=PP2 TR2
3336 CBTTM1=RB*COBETB/RTM1 TR2
IF(CBTTM1.LE.1.00)GO TO 334 TR2
ISTOP=3 TR2
GO TO 3345 TR2
334 SBTTM1=DSQRT(1.00-CBTTM1**2) TR2
FLAG=.FALSE. TR2
IF(1.00-F1*SBTTM1.GT.0.00) GO TO 335 TR2
FLAG=.TRUE. TR2
3345 THETA=1.00/RTM1 TR2
DIST1=1.010 TR2
IRCYCL=0 TR2
GO TO 336 TR2
335 FLOG=H1*F1*DLOG((1.00+F1*SBTTM1)/(1.00-F1*SBTTM1))/2.00 TR2
GPF2=FLOG*2.00 TR2

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      THETA=CBTTH1*FLOG/RTM1
      PPF2=M1*SBTTH1+(1.00-F1**(-2)+CBTTH1**2)*FLOG
      IRCYCL=IRCYCL+1
336  YS2PP=YS1PP*DCOS(THETA)-Z10PP*DSIN(THETA)
      ZS2PP=Z10PP*DCOS(THETA)+YS1PP*DSIN(THETA)
      IF(FLAG.OR.ISTOP.GT.1) GO TO 475
      YS3PP=YS1PP*DCOS(2.00*THETA)-Z10PP*DSIN(2.00*THETA)
      ZS3PP=Z10PP*DCOS(2.00*THETA)+YS1PP*DSIN(2.00*THETA)
      ALPHAV=PI/2.00-THETA-DASIN(SIBETB)
      RV=RB*COBETB/OSIN(ALPHAV)
      YVPP=YS2PP*RV/RB
      C32PP=YS3PP-YVPP
      C33PP=ZS3PP-Z10PP
      DO 340 J=1,3
      C3(J)=M(2,J)*C32PP+M(3,J)*C33PP
340  A3(J)=M(2,J)*YS3PP+M(3,J)*ZS3PP+P0(J)
      CALL CROSS(A3,C3,PHI)
      CALL CROSS(PHI,C3,KPPP)
      MA3C3=MAG(PHI)
      MC3=MAG(C3)
      C32PPP=MC3
      DO 350 J=1,3
      P(1,J)=PHI(J)/MA3C3
      P(2,J)=C3(J)/MC3
350  P(3,J)=KPPP(J)/(MA3C3*MC3)
C    F1 LAYER DOWNWARD
      YS3PPP=P(2,1)*A3(1)+P(2,2)*A3(2)+P(2,3)*A3(3)
      IF(YS3PPP.GE.0.D0) GO TO 3555
      ZS3PPP=P(3,1)*A3(1)+P(3,2)*A3(2)+P(3,3)*A3(3)
      INT=0
      GO TO(436,3987,353),IREFL
353  IF(MR3.GE.DABS(ZS3PPP)) GO TO 360
      IF(B.GE.DABS(ZS3PPP)) GO TO 356
3555  ISTOP=3
      IRCYCL=0
      GO TO 475
356  YDPPP=-DSQRT(B**2-ZS3PPP**2)
      GO TO 370
360  YDPPP=-DSQRT(MR3**2-ZS3PPP**2)
C    F1 LAYER ITERATION 370 TO 390
370  DO 380 J=1,3
380  PD(J)=P(2,J)*YDPPP+P(3,J)*ZS3PPP
      NLD=DASIN(PD(3)/MAG(PD))
      WLD=WLON(PD(2),PD(1))
      CALL RIIP(R0,NLD,WLD,PLASD)
      RM=HBE+HAE+HAF1+R0
      H=HAF1
      F=FREQ/FCF1
      IF(RM.GE.DABS(ZS3PPP)) GO TO 382
      ISTOP=3
      IRCYCL=0
      GO TO 475
382  YDPPP2=-DSQRT(RM**2-ZS3PPP**2)
      DISTB=DABS(YDPPP2-YDPPP)
      IF(DISTB.LE.EPS3) GO TO 390
      IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 384
      H=HP

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      F=FP
      RM=RMP
      YOPPP2=YOPPP
      OUT2=DISTA
      IF(IWRITE.EQ.1)WRITE(6,243)OUT2,IHOPS
      GO TO 390
384  YOPPP=YOPPP2
      DISTA=DISTB
      RMP=RM
      FP=F
      HP=H
      INT=INT+1
      IF(INT.LE.LIMF1D) GO TO 370
      ISTOP=4
      IRCYCL=0
      GO TO 475
C   E LAYER DOWNWARD
390  YM1PPP=YOPPP2
      HF1=H
      MRM1=DSQRT(YM1PPP**2+ZS3PPP**2)
      DO 395 J=1,3
395  RN1(J)=P(2,J)*YM1PPP+P(3,J)*ZS3PPP
      SBETM1=OABS(DOT(RN1,C3)/(MRM1*MC3))
      CBETM1=DSQRT(1.00-SBETM1*SBETM1)
      R4=MAG(A3)
      PP2=PP2+R4*DSQRT(1.00-(MRM1/R4*CBETM1)**2)-MRM1*SBETM1
      IF(F*SBETM1.GT.1.00)GO TO 398
      ISTOP=5
      IRCYCL=0
      GO TO 475
398  FLOG=DLG((F*SBETM1+1.00)/(F*SBETM1-1.00))
      DGP2P=H*(F/2.00*FLOG-1.00/SBETM1)
      TH12=CBETM1*DGP2P/RM
      PPEF1D=H*(.5D0*SBETM1+F/4.00*(1.00-F**(-2)+CBETM1**2)*FLOG-1.00/SB
*ETM1)
      DPP2P=PPEF1D
      RR2=MRM1*SBETM1
      RR2C=MRM1*CBETM1
      YM2PPP=YM1PPP*DCOS(TH12)-ZS3PPP*DSIN(TH12)
      ZM2PPP=ZS3PPP*DCOS(TH12)+YM1PPP*DSIN(TH12)
      MRM2=DSQRT(YM2PPP**2+ZM2PPP**2)
      YY1PPP=CBETM1*(YM2PPP*CBETM1-ZM2PPP*SBETM1)
      ZY1PPP=CBETM1*(ZM2PPP*CBETM1+YM2PPP*SBETM1)
      C42PPP=YY1PPP-YM2PPP
      C43PPP=ZY1PPP-ZM2PPP
      MRY1SQ=YY1PPP**2+ZY1PPP**2
      MC4SQ=C42PPP**2+C43PPP**2
3984 IF(MR2**2.GE.MRY1SQ)GO TO 399
      IF(B**2.GE.MRY1SQ) GO TO 3986
      ISTOP=6
      IRCYCL=0
      GO TO 475
3986 TE=-DSQRT((B**2-MRY1SQ)/MC4SQ)
      RM=B
      GO TO 3995
3987 CNST=-DOT(A3,C3)/MC3**2
      C42PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3)

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```
C43PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3) TR2
YY1PPP=YS3PPP+CNST*C42PPP TR2
ZY1PPP=ZS3PPP+CNST*C43PPP TR2
MRY1SQ=YY1PPP**2+ZY1PPP**2 TR2
MC4SQ=MC3**2 TR2
MRM1=DSQRT(YS3PPP**2+ZS3PPP**2) TR2
CBETH1=DSQRT(MRY1SQ)/MRM1 TR2
SBETH1=DSQRT(1.00-CBETH1**2) TR2
GO TO 3984 TR2
399 TE=-DSQRT((MR2**2-MRY1SQ)/MC4SQ) TR2
3995 YEPPP=C42PPP*TE+YY1PPP TR2
ZEPPP=C43PPP*TE+ZY1PPP TR2
C E LAYER ITERATION 400 TO 420 TR2
INT=0 TR2
400 DO 410 J=1,3 TR2
410 PE(J)=P(2,J)*YEPPP+P(3,J)*ZEPPP TR2
NLE=DASIN(PE(3)/MAG(PE)) TR2
WLE=WLN(PE(2),PE(1)) TR2
CALL RIIP(R0,NLE,WLE,PLASD) TR2
NOELAY=.FALSE. TR2
IF(FCE.GT.0.00) GO TO 4105 TR2
FCE=1.0-2 TR2
NOELAY=.TRUE. TR2
4105 RM=HBE+HAE+R0 TR2
H=HAE TR2
F=FREQ/FCE TR2
IF(RM**2.GE.MRY1SQ) GO TO 411 TR2
ISTOP=6 TR2
IRCYCL=0 TR2
GO TO 475 TR2
411 TE=-DSQRT((RM**2-MRY1SQ)/MC4SQ) TR2
YEPPP2=C42PPP*TE+YY1PPP TR2
ZEPPP2=C43PPP*TE+ZY1PPP TR2
DISTB=DSQRT((YEPPP-YEPPP2)**2+(ZEPPP-ZEPPP2)**2) TR2
IF(DISTB.LE.EPS4) GO TO 420 TR2
IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 414 TR2
H=HP TR2
F=FP TR2
RM=RMP TR2
YEPPP2=YEPPP TR2
ZEPPP2=ZEPPP TR2
OUT2=DISTA TR2
IF(IWRITE.EQ.1)WRITE(6,142)OUT2,IHOPS TR2
GO TO 420 TR2
414 YEPPP=YEPPP2 TR2
ZEPPP=ZEPPP2 TR2
RMP=RM TR2
FP=F TR2
HP=H TR2
DISTA=DISTB TR2
INT=INT+1 TR2
IF(INT.LE.LIMED) GO TO 400 TR2
ISTOP=7 TR2
IRCYCL=0 TR2
GO TO 475 TR2
420 YM3PPP=YEPPP2 TR2
ZM3PPP=ZEPPP2 TR2
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HE=H
C   END OF E LAYER
MRM3=DSQRT(YM3PPP**2+ZM3PPP**2)
CBETM2=MRM1*CBETM1/MRM3
SBETM2=DSQRT(1.00-CBETM2*CBETM2)
IF(IREFL.EQ.2) PP2=PP2+MRM1*SBETM1-MRM3*SBETM2
IF(F*SBETM2.GT.1.00) GO TO 430
ISTOP=8
IRCYCL=0
GO TO 475
430  IF(.NOT.NOELAY) GO TO 4302
FLOG=0.00
DPP1P=0.00
TH34=0.00
DGP1P=0.00
YM4PPP=YM3PPP
ZM4PPP=ZM3PPP
MRM4=MRM3
GO TO 4304
4302 FLOG=DLG((F*SBETM2+1.00)/(F*SBETM2-1.00))
DGP1P=H*(F/2.00*FLOG-1.00/SBETM2)
TH34=CBETM2*DGP1P/RM
YM4PPP=YM3PPP*DCOS(TH34)-ZM3PPP*DSIN(TH34)
ZM4PPP=ZM3PPP*DCOS(TH34)+YM3PPP*DSIN(TH34)
MRM4=DSQRT(YM4PPP**2+ZM4PPP**2)
DPP1P=H*(.500*SBETM2+F/4.00*(1.00-F**(-2)+CBETM2**2)*FLOG-1.00/SBE
*TH2)
4304 RR1=MRM4-H
IF(IREFL.LT.3) GO TO 4305
IF(DABS(RR2C).GT.RR1) GO TO 431
TAU=RR2-RR1*DSQRT(1.00-(RR2C/RR1)**2)
PPEF1D=PPEF1D+DPP1P+TAU
GPEF1D=GPEF1D+DGP1P+TAU
4305 YY2PPP=CBETM2*(YM4PPP*CBETM2-ZM4PPP*SBETM2)
ZY2PPP=CBETM2*(ZM4PPP*CBETM2+YM4PPP*SBETM2)
C52PPP=YY2PPP-YM4PPP
C53PPP=ZY2PPP-ZM4PPP
MC5SQ=C52PPP**2+C53PPP**2
SBM4H2=1.00-(CBETM2/(1.00-HE/MRM4))**2
IF(SBM4H2.GT.0.00) GO TO 4307
ISTOP=15
IRCYCL=0
GO TO 475
4307 TAU1ED=MRM4*SBETM2-(MRM4-HE)*DSQRT(SBM4H2)
RY=DSQRT(MRY1SQ)
GO TO 437
431  ISTOP=9
IRCYCL=0
GO TO 475
436  MB1=MAG(A3)
SBET1=-DOT(A3,C3)/(MB1*MC3)
CBET1=DSQRT(1.00-SBET1**2)
RY=MB1*CBET1
MRY1SQ=RY**2
CNST=MB1/MC3*SBET1
C52PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3)
C53PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3)

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YY2PPP=YS3PPP+CNST*C52PPP
ZY2PPP=ZS3PPP+CNST*C53PPP
MC5SQ=MC3**2
437 HITS=R0.GT.RY
INCHOP=(R0+50.00).GE.RY
IF(R0+HBE.GT.RY) GO TO 438
ISTOP=15
IRCYCL=0
GO TO 475
438 TQ=-DSQRT(((R0+HBE)**2-MRY1SQ)/MC5SQ)
YBEP= C52PPP*TQ+YY2PPP
ZBEP= C53PPP*TQ+ZY2PPP
IF(.NOT.HITS) GO TO 450
TQ=-DSQRT((R0**2-MRY1SQ)/MC5SQ)
YQPPP=C52PPP*TQ+YY2PPP
ZQPPP=C53PPP*TQ+ZY2PPP
DO 440 J=1,3
440 PQ(J)=P(2,J)*YQPPP+P(3,J)*ZQPPP
GO TO 461
450 DO 460 J=1,3
460 PQ(J)=P(2,J)*YY2PPP+P(3,J)*ZY2PPP
C STARTS TO ITERATE TILTED F2
461 DIST2=DSQRT((PQ(1)-PREV(1))**2+(PQ(2)-PREV(2))**2+(PQ(3)-PREV
*(3))**2)
RTDIF=DABS(RT1-PREV(13))
IF(IRCYCL.LE.2) GO TO 475
IF(DIST2-EPS5)463,463,462
462 IF(DIST1-DIST2)470,475,475
463 IF(RTDIF-EPS5)500,500,475
470 CALL PRVGET
ICNPRB=1
IF(IWRITE.EQ.1)WRITE(6,473) IHOPS,EPS5,DIST1,RTDIF
473 FORMAT(48H TILTED LAYER CONVERGENCE PROBLEMS ON HOP NUMBER,I3,
1 1H,,F6.1,29H KM. CRITERIA NOT MET, DIST1=,F8.2,8H, RTDIF=,
2 F8.2)
GO TO 500
475 YW2PP=RTM1*YS2PP/RB
ZW2PP=RTM1*ZS2PP/RB
DO 480 J=1,3
480 PW2(J)=M(2,J)*YW2PP+M(3,J)*ZW2PP+P0(J)
NLW2=DASIN(PW2(3)/MAG(PW2))
HLW2=WLON(PW2(2),PW2(1))
DO 490 J=1,3
490 W2(J)=PW2(J)-P0(J)
BETA22=DACOS(DOT(PW2,W2)/(MAG(W2)*MAG(PW2)))
BETTM1=DASIN(SBTM1)
CALL PRVSTO
DIST1=DIST2
BP=RTM1
CALL HTGROF(NDFLAG,FREQ,RTD*NLW2,RTD*HLW2,RTD*BETTM1,RTD*BETA22,B
*P,RTM1,RT1,RTM1,DNDR,DONL,DONL,INTFLG)
IF(IREFL.NE.NUSE) GO TO 501
GO TO(4916,4917,4918),IREFL
4916 F1=FREQ/FCF
H1=HAE
GO TO 4919
4917 F1=FREQ/FCF1*.86602540378443900

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      RM1=RM1+HAF1
      H1=HAF1*2.00
      GO TO 4919
4918  F1=FREQ/FCF2
      H1=HAF2
4919  INTF2=INTF2+1
      RM=MAG(PW2)
      DO 492 J=1,3
492   PC3(J)=PW2(J)
      IF(INTF2.LE.LIMF2) GO TO 315
      IF(ISTOP.GT.1) GO TO 7310
494   IF(FLAG.OR.PNTFLG.GT.500) GO TO 501
      GO TO 7310
C     ITERATION FINISHED
500   DO 5003 J=1,3
      VEC(J,1)=L(2,J)
      LOC(J,1)=L(2,J)*YBEP+L(3,J)*P1P(3)
      VEC(J,2)=L(2,J)*C12P+L(3,J)*C13P
      LOC(J,2)=R2(J)
      VEC(J,3)=M(2,J)
      LOC(J,3)=L(2,J)*Y9P+L(3,J)*Z9P
      VEC(J,4)=P(2,J)
      LOC(J,4)=M(2,J)*YS1PP+M(3,J)*Z10PP+P0(J)
      LOC(J,5)=A3(J)
      LOC(J,6)=P(2,J)*YH1PPP+P(3,J)*ZS3PPP
      VEC(J,5)=P(2,J)*C42PPP+P(3,J)*C43PPP
      LOC(J,7)=P(2,J)*YH3PPP+P(3,J)*ZM3PPP
      VEC(J,6)=P(2,J)*C52PPP+P(3,J)*C53PPP
5003  LOC(J,8)=P(2,J)*YBEP+P(3,J)*ZBEP
      DO 5008 K=1,6
      MAGVEC=MAG(VEC(1,K))
      IF(MAGVEC.EQ.0.00) GO TO 5008
      DO 5007 J=1,3
5007  VEC(J,K)=VEC(J,K)/MAGVEC
5008  CONTINUE
      IF(PNTFLG.LT..5) GO TO 510
501   IF(FLAG2) GO TO 134
      IF(FLAG3) GO TO 234
      RM=RM1
      INT=0
      FLAG=.TRUE.
      GO TO(502,503,504),IREFL
502   CBET1=COBETB*RB/RM
      FLAG2=.TRUE.
      SBET1=DSQRT(1.00-CBET1**2)
      Y3P=DSQRT(RM**2-Z10PP**2)
      P1P(3)=Z10PP
      F=FREQ/FCF
      H=HAE
      GO TO 131
503   F=FREQ/FCF1
      FLAG3=.TRUE.
      H=HAF1
      MR3=RM
      CBET4=COBETB*RB/RM
      IF(DABS(CBET4).LT.1.00.AND.DABS(RM).GT.DABS(Z10PP)) GO TO 5035
      ISTOP=6

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      IRCYCL=0
      GO TO 475
5035 SBET4=DSQRT(1.00-CBET4**2)
      Y7P=DSQRT(RM**2-Z10PP**2)
      Z7P=Z10PP
      GO TO 231
504  IF(IWRITE.EQ.1)WRITE(6,505)IHOPS
505  FORMAT(23H PENETRATION ON HOP NO.,I3,1H.)
      GO TO 7311
510  IF(HITS) GO TO 530
      GO TO (512,514,514),IREFL
512  PP0P=MB1*SBET1
      GO TO 516
514  PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)
516  DO 520 J=1,3
      B1(J)=P(2,J)*C52PPP+P(3,J)*C53PPP
520  A1(J)=PQ(J)
      GO TO 550
530  GO TO (531,532,532),IREFL
531  ALPHAQ=DASIN(MB1/R0*CBET1)
      PP0P=MB1*SBET1-R0*DSQRT(1.00-(RY/R0)**2)
      GO TO 533
532  ALPHAQ=DASIN(MRM1*CBETM1/R0)
      PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)-R0*DSQRT(1.00-
*0-(MRM4/R0*CBETM2)**2)
533  B22PPP=-C52PPP*DCOS(2.00*ALPHAQ)+C53PPP*DSIN(2.00*ALPHAQ)
      B23PPP=-C53PPP*DCOS(2.00*ALPHAQ)-C52PPP*DSIN(2.00*ALPHAQ)
      DO 540 J=1,3
      A1(J)=PQ(J)
540  B1(J)=P(2,J)*B22PPP+P(3,J)*B23PPP
550  IF(IHOPS.GE.IABS(MODE))GO TO 552
551  GO TO (5511,5512,5513),IREFL
5511 PPTOT=PPTOT+PP0+PPF2+PP0P
      GPTOT=GPTOT+PP0+GPF2+PP0P
      GO TO 5514
5512 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED
      GO TO 5514
5513 PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P
      GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P
5514 MB1=MAG(A1)
      IF(.NOT.HITS.AND.IHOPS.GE.IABS(MODE).AND.MB1.GE.RTARG) GO TO 598
      GO TO 90
552  IF(SEARCH.AND.RTARG.GT.MR3-HF1A.AND.RTARG.LE.DMAX1(RV,MR3))GOTO595
      IF(ASC) GO TO 566
      IF(DABS(RTARG-R0).LE.1.0-5.AND.HITS) GO TO 580
      IF(MODE.GT.0) GO TO 563
C  DESCENDING MODE
      GO TO(564,562,560),IREFL
560  IF(RTARG.LE.DMAX1(RV,MRM1).AND.RTARG.GT.MRM1-HF1) GO TO 576
      IF(DMIN1(MRM4-4E,MRM1).LT.RTARG.AND.RTARG.LE.DMAX1(MRM4,MRM1-HF1))
* GO TO 573
      IF(RTARG.LE.MRM4-HE) GO TO 568
      IF(INCHOP) GO TO 566
      SEARCH=.TRUE.
      GO TO 5513
562  IF(RTARG.LE.RV.AND.RTARG.GT.MRM4) GO TO 576

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IF(RTARG.LE.MRM4) GO TO 568
IF(INCHOP) GO TO 566
SEARCH=.TRUE.
GO TO 5512
563 SEARCH=.TRUE.
ASC=.TRUE.
GO TO 551
564 IF(RTARG.LE.RV) GO TO 568
SEARCH=.TRUE.
IF(.NOT.INCHOP) GO TO 5511
566 ISTOP=15
GO TO 7310
568 IF(RTARG.GE.RY.OR.INCHOP) GO TO 569
SEARCH=.TRUE.
GO TO 551
569 TTARG=0.00
IF(RTARG.GT.RY) TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC5SQ)
YTARGP=C52PPP*TTARG+YY2PPP
ZTARGP=C53PPP*TTARG+ZY2PPP
DO 570 J=1,3
B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J)
570 PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
PP0P=0.00
IF(RTARG.GT.RY) PP0P=-RTARG*DSQRT(1.00-(RY/RTARG)**2)
GO TO (571,5715,5715),IREFL
571 PP0P=MB1*SBET1+PP0P
PPTOT=PPTOT+PP0+PPF2+PP0P
GPTOT=GPTOT+PP0+GPF2+PP0P
GO TO 600
5715 PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+PP0P
GO TO (5720,5720,5725),IREFL
5720 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED
GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED
GO TO 600
5725 PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P
GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P
GO TO 600
573 TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC4SQ)
YTARGP=C42PPP*TTARG+YY1PPP
ZTARGP=C43PPP*TTARG+ZY1PPP
DO 575 J=1,3
B1(J)=C42PPP*P(2,J)+C43PPP*P(3,J)
575 PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
PPTOT=PPTOT+PPEF1A+PPF2+PP2+PP0+PPEF1D
GPTOT=GPTOT+GPEF1A+GPF2+PP2+PP0+GPEF1D
GO TO 600
576 YTARGP=-DSQRT(RTARG**2-ZS3PPP**2)
ZTARGP=ZS3PPP
DO 579 J=1,3
B1(J)=C32PPP*P(2,J)
579 PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
GO TO (5793,5793,5797),IREFL
5793 TAU=MRM4*SBETH2-(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+P
*P0+PP2
PPTOT=PPTOT+TAU+DPP1+PPF2+TAU1EA
GPTOT=GPTOT+TAU+DGP1+GPF2+TAU1EA
GO TO 600

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5797 TAU=MRM1*SBETH1-(MRM1-HF1)*DSQRT(1.00-(CBETH1/(1.00-HF1/MRM4))**2) TF
      *+PP0+PP2 TR
      PPTOT=PPTOT+TAU+PPEF1A+PPF2+DPP2P TF
      GPTOT=GPTOT+TAU+GPEF1A+GPF2+DGP2P TF
      GO TO 600 TR
C TARGET ON GROUND TR
580 DO 590 J=1,3 TR
      B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J) TR
590 PTARG(J)=A1(J) TR
      GO TO(5902,5904,5906),IREFL TR
5902 PPTOT=PPTOT+PP0+PPF2+PP0P TR
      GPTOT=GPTOT+PP0+GPF2+PP0P TR
      GO TO 600 TR
5904 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED TR
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED TR
      GO TO 600 TR
5906 PPTOT=PPTOT+PP0+PPEF1A+PP2+PPF2+PPEF1D+PP0P TR
      GPTOT=GPTOT+PP0+GPEF1A+PP2+GPF2+GPEF1D+PP0P TR
      GO TO 600 TR
C ASCENDING MODE TR
591 YTARGP=DSQRT(RTARG**2-P1P(3)**2) TR
      DO 592 J=1,3 TR
592 PTARG(J)=L(2,J)*YTARGP+L(3,J)*P1P(3) TR
      TAU=RTARG*DSQRT(1.00-(RY/RTARG)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      INUSE=INUSE-1 TR
      IF(.NOT.HITS) GO TO 600 TR
      TAU=-R0*DSQRT(1.00-(RY/R0)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      GO TO 600 TR
593 TTARG=DSQRT((RTARG**2-MRX1SQ)/MC1PSQ) TR
      YTARGP=C12P*TTARG+Y6P TR
      ZTARGP=C13P*TTARG+Z6P TR
      DO 594 J=1,3 TR
      PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
594 B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
      TAU=(MR3-HF1A)*DSQRT(1.00-(COS02/(1.00-HF1A/MR3))**2) TR
      PPTOT=PPTOT+DPP1+TAU TR
      GPTOT=GPTOT+DGP1+TAU TR
      INUSE=INUSE-1 TR
      IF(.NOT.HITS) GO TO 600 TR
      TAU=-R0*DSQRT(1.00-((MR2-HEA)/R0*COS01)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      GO TO 600 TR
595 TTARG=DSQRT((RTARG**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2)) TR
      YTARGP=C22P*TTARG+Y10P TR
      ZTARGP=C23P*TTARG+Z10P TR
      DO 596 J=1,3 TR
      PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
596 B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
      TAU=(MR2-HEA)*DSQRT(1.00-(COS01/(1.00-HEA/MR2))**2)+PP2A TR
      PPTOT=PPTOT+PPEF1A+PPF2/2.00+TAU TR
      GPTOT=GPTOT+GPEF1A+GPF2/2.00+TAU TR
      IF(.NOT.ASC) GO TO 600 TR

```

	INUSE=INUSE-1	TR2
	TAU=-R0*DSQRT(1.00-((HR2-HEA)/R0*COS01)**2)	TR2
	PPTOT=PPTOT+TAU	TR2
	GPTOT=GPTOT+TAU	TR2
	GO TO 600	TR2
598	RS2=MAG(A1)	TR2
	DO 599 I=1,3	TR2
599	PTARG(I)=A1(I)	TR2
	GO TO 601	TR2
600	IF(.NOT.HITS) RS2=MAG(PTARG)	TR2
601	IF(GPONLY) RETURN	TR2
	NLTARG=RTD*DASIN(PTARG(3)/RS2)	TR2
	WLTARG=RTD*WLN(PTARG(2),PTARG(1))	TR2
	EAST(1)=-PTARG(2)	TR2
	EAST(2)=PTARG(1)	TR2
	EAST(3)=0.00	TR2
	CALL CROSS(PTARG,EAST,NORTH)	TR2
	CNST1=DOT(PTARG,B1)/RS2	TR2
	ELF=RTD*DASIN(CNST1/MAG(B1))	TR2
	ME=MAG(EAST)	TR2
	MN=MAG(NORTH)	TR2
	CNST=DOT(EAST,B1)/ME	TR2
	AZF=RTD*DATAN2(CNST,DOT(NORTH,B1)/MN)+180.00-DSIGN(180.00,CNST)	TR2
	B1(1)=PTARG(1)-A11(1)	TR2
	B1(2)=PTARG(2)-A11(2)	TR2
	B1(3)=PTARG(3)-A11(3)	TR2
	SRANGE=MAG(B1)	TR2
	ELSR=RTD*DASIN(DOT(A11,B1)/(SRANGE*MA1))	TR2
	DIST=R0*DACOS(DOT(A11,PTARG)/(RS2*MA1))	TR2
	CNST=DOT(EAST1,B1)	TR2
	BEAR=RTD*DATAN2(CNST,DOT(NORTH1,B1))+180.00-DSIGN(180.00,CNST)	TR2
	RETURN	TR2
7310	IGOBAK=1	TR2
	IF(IWRITE.EQ.1)WRITE(6,7309) MESSPR(ISTOP)	TR2
7309	FORMAT(11H MESSUP---,A10)	TR2
	RETURN	TR2
7311	IGOBAK=2	TR2
	RETURN	TR2
	END	TR2

FUNCTION MAG 74/74 OPT=1 FTN 4.5+414 04/27/

```
DOUBLE PRECISION FUNCTION MAG(A)
IMPLICIT DOUBLE PRECISION(A-Z)
DIMENSION A(3)
MAG=DSORT(A(1)*A(1)+A(2)*A(2)+A(3)*A(3))
RETURN
END
```

MAG
MAG
MAG
MAG
MAG
MAG

FUNCTION DOT 74/74 OPT=1 FTN 4.5+414 04/27/

```
DOUBLE PRECISION FUNCTION DOT(A,B)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3)
DOT=A(1)*B(1)+A(2)*B(2)+A(3)*B(3)
RETURN
END
```

DOT
DOT
DOT
DOT
DOT
DOT

SUBROUTINE CROSS 74/74 OPT=1 FTN 4.5+414 04/27/

```
SUBROUTINE CROSS(A,B,C)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3),C(3)
C(1)=A(2)*B(3)-A(3)*B(2)
C(2)=A(3)*B(1)-A(1)*B(3)
C(3)=A(1)*B(2)-A(2)*B(1)
RETURN
END
```

VEC
VEC
VEC
VEC
VEC
VEC
VEC
VEC

ROUTINE PRVSTO 74/74 OPT=1

FTN 4.5+414

04/27/

```
      SUBROUTINE PRVSTO
      DOUBLE PRECISION P1,P2
      LOGICAL LP1,LP2
      COMMON/CPREV/P1(56),P2(56),LP1(6),LP2(6)
      DO 1 I=1,56
1      P2(I)=P1(I)
      DO 2 I=1,6
2      LP2(I)=LP1(I)
      RETURN
      ENTRY PRVGET
      DO 3 I=1,56
3      P1(I)=P2(I)
      DO 4 I=1,6
4      LP1(I)=LP2(I)
      RETURN
      END
```

ROUTINE HTGRDF 74/74 OPT=1

FTN 4.5+414

04/27/

```
      SUBROUTINE HTGRDF(NDFLAG,FREQ,NLAT,WLONG,ANGLE1,ANGLE2,RANG12,RMU HTG
*,RTU,RTMU,DNDR,DNDT,DNDP,PNTFLG) HTG
      IMPLICIT DOUBLE PRECISION (A-H,O-Z) HTG
      DOUBLE PRECISION NLAT,NLATR HTG
      LOGICAL TILT,FAST HTG
      COMMON/TILTC/TILT,FAST HTG
      NLATR=NLAT/57.2957795130823200 HTG
      WLONGR=WLONG/57.2957795130823200 HTG
      CALL RIIP(6370.00,NLATR,WLONGR,EN) HTG
      CALL RTFIND(NDFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RMU,RTMU,PNTFLG) HTG
      IF(TILT) GO TO 1 HTG
      DNDR=1.000 HTG
      DNDP=0.000 HTG
      DNDT=0.000 HTG
      RETURN HTG
1      CALL DENSE(RTU,NLAT,WLONG,EN,DNDR,DNDT,DNDP) HTG
      RETURN HTG
      END HTG
```

```

      SUBROUTINE RTFIND(NDFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RMU,RTMU,P RTF
      *NTFLG) RTF
C   NDFLAG FLAG TO INDICATE WHICH PASS RTF
C   =0 FIRST PASS RTF
C   =1 SUBSEQUENT PASSES RTF
C   NOTE - THIS ROUTINE REQUIRES INITIALIZATION . RTF
C           ON FIRST PASS, ANGLE1 MUST = THE INITIAL TAKE OFF ANGLE ON RTF
C           GROUND, ANGLE2 MUST =0, RANG12 MUST = RADIUS OF EARTH RTF
C   FREQ-OPERATING FREQUENCY IN MHZ. RTF
C   ANGLE1 - ANGLE (DEG) BETWEEN TILTED LAYER AND RAY INCIDENT ON THE LAY RTF
C   ANGLE2 - TILT ANGLE (DEG) - THAT IS, ANGLE BETWEEN TILTED LAYER AND A RTF
C           EXACTLY HORIZONTAL LAYER AT THE REFLECTION POINT RTF
C   RANG12 - DISTANCE FROM CENTER OF EARTH (KM) OF REFLECTION POINT USED RTF
C           COMPUTE ANGLE1+2 RTF
C   RTU-COMPUTED DISTANCE FROM CENTER OF EARTH IN KM. OF POINT OF INTERES RTF
C   RMU-DISTANCE FROM CENTER OF EARTH TO LAYER IN KM. RTF
C   PNTFLG-PENETRATION FLAG RTF
C           =0. REFLECTION RTF
C           =1. PENETRATION RTF
      IMPLICIT DOUBLE PRECISION (A-H,O-Z) RTF
      DOUBLE PRECISION M3000 RTF
      DIMENSION RM(3),H(3),FC(3),RTM(3) RTF
      COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2, RTF
      IDUM(13),ID(3) RTF
      COMMON/RTCOM/COSBO,NUSE RTF
      DATA R1D/0.1745329251994330D-01/ RTF
      DACOS((DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY),DUMMY) RTF
      PNTFLG=0.000 RTF
      IF(NDFLAG)4,4,44 RTF
4   IF(ANGLE2.EQ.0.000)GO TO 44 RTF
      WRITE(5,100) ANGLE2 RTF
100  FORMAT(22H THE VALUE OF ANGLE2 =,D15.8,13H IS IN ERROR.) RTF
      PNTFLG=1.000 RTF
44   FC(1)=FCE RTF
      FC(2)=FCF1 RTF
      FC(3)=FCF2 RTF
      H(1)=HAE RTF
      H(2)=HAF1 RTF
      H(3)=HAF2 RTF
      RM(3)=6370.00+HMF2 RTF
      RM(2)=RM(3)-H(3) RTF
      RM(1)=RM(2)-H(2) RTF
      IF(NDFLAG.GT.0) GO TO 45 RTF
      COSBO=(DCOS(ANGLE1*RAD)*RANG12/6370.00) RTF
45   DO 10 N=1,3 RTF
C   COMPUTE RTM FOR EACH LAYER RTF
      IF(FC(N).EQ.0.000)GO TO 6 RTF
      FAC=(RM(N)**2)/16.00-(H(N)**2/2.00)*((FREQ/FC(N))**2-1.00) RTF
      IF(FAC)6,5,5 RTF
5     RTM(N)=0.7500*RM(N)+DSQRT(FAC) RTF
      GO TO 10 RTF
6     RTM(N)=RM(3) RTF
10   CONTINUE RTF
C   FIND MAX RTM RTF
      RMM=RTM(3) RTF
      IF(RTM(3).EQ.RM(3))RMM=RM(3)/2.000 RTF
3000 IF(NDFLAG.GT.0) GO TO 14 RTF

```

```

C   IF ALL RTM ARE EQUAL, USE F2 LAYER                                RTF
      IF(RTM(2).NE.RTM(3).OR.RTM(1).NE.RTM(3))GO TO 12              RTF
      NUSE=3                                                         RTF
      RTMUSE=RTM(3)                                                 RTF
      GO TO 14                                                       RTF
C   FIND MINIMUM RTM                                               RTF
12   RTMUSE=RTM(1)                                                 RTF
      NUSE=1                                                         RTF
      DO 13 I=2,3                                                  RTF
      IF(RTMUSE.LT.RTM(I))GO TO 13                                  RTF
      RTMUSE=RTM(I)                                               RTF
      NUSE=I                                                         RTF
13   CONTINUE                                                       RTF
      IF(NDFLAG.GT.0) GO TO 14                                       RTF
123  ANGLE1=(DACOS(COSB0*6370.00/RANG12))/RAD                       RTF
C   USE PARAMETERS ASSOC. WITH MIN RTM                             RTF
14   RTMUSE=RTM(NUSE)                                             RTF
      RMUSE=RM(NUSE)                                               RTF
      HUSE=H(NUSE)                                                 RTF
      FCUSE=FC(NUSE)                                              RTF
144  CBTM=DCOS(ANGLE1*RAD) *RANG12/RTMUSE                          RTF
      IF(CBTM-1.000)15,15,16                                       RTF
15   BTM=DACOS(CBTM)                                              RTF
17   X=1.000-((FREQ/FCUSE)**2)*((DSIN(BTM))**2)                  RTF
      IF(X.GE.0.000)GO TO 20                                       RTF
16   IF(RTMUSE.NE.RM(3))GO TO 18                                  RTF
C   PENETRATION                                                    RTF
185  RTU=RMM                                                       RTF
      PNTFLG=1.000                                                 RTF
      RMU=RM(3)                                                     RTF
      RTMU=RTMUSE                                                  RTF
2000 RETURN                                                         RTF
18   IF(NUSE-3)19,185,185                                         RTF
C   ELIMINATE RTM USED AND FIND NEXT SMALLEST RTM                RTF
19   NUSE=NUSE+1                                                  RTF
      GO TO 123                                                    RTF
C   REFLECTION                                                      RTF
20   RT=RTMUSE-HUSE*DSQRT(X)                                       RTF
      RMU=RMUSE                                                    RTF
      RTMU=RTMUSE                                                  RTF
      A=RMU-PT                                                     RTF
      B=A/DCOS(ANGLE2*RAD)                                         RTF
      IF(B.GE.HUSE)B=HUSE                                          RTF
      RTU=RMU-B                                                    RTF
      END                                                           RTF

```

```

      SUBROUTINE DENSE(R,THETA,PHI,EN,DNDR,DNDT,DNDP)
C R-DISTANCE FROM CENTER OF EARTH IN KM.
C THETA-NORTH LATITUDE IN DEGREES
C PHI-WEST LONGITUDE IN DEGREES
C EN-VALUE OF ELECTRON DENSITY AT GIVEN POINT
C DNDR-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO R
C DNDT-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO THETA
C DNDP-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO PHI
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DIMENSION RX(9),RY(9),ALPHA(9),FN(9)
      COMMON/PERT/RRIIP,ITIP
      DATA RAD/.017453292519943300/
10    RY(1)=R
      RX(1)=THETA*RAD
      ALPHA(1)=PHI*RAD
      NSIG=1
20    CALL DERV(NSIG,FN,RY,RX,ALPHA,DNDR,DNDT,DNDP)
      IF(NSIG.EQ.3) GO TO 30
      DO 25 I=2,5
      CALL RIIP(RY(I),RX(I),ALPHA(I),FN(I))
      GO TO (22,23),ITIP
22    CALL NFROMR(RY(I+4),FN(I+4))
      GO TO 25
23    CALL RIIP(RY(I+4),RX(I+4),ALPHA(I+4),FN(I+4))
25    CONTINUE
      CALL RIIP(RY(1),RX(1),ALPHA(1),FN(1))
      NSIG=2
      GO TO 20
30    EN=FN(1)
      RETURN
      END

```

```

      SUBROUTINE DERV(NSIG,FN,RY,RX,ALPHA,DNDR,DNDT,DNDP)
C   NSIG-SWITCH TO INDICATE WHETHER POINTS OR DERIVATIVES ARE REQUIRED
C   FN-ARRAY OF 9 VALUES OF ELEC. DEN.
C   RY-ARRAY OF 9 VALUES OF R IN KM.
C   RX-ARRAY OF 9 VALUES OF THETA IN RAD.
C   ALPHA-ARRAY OF 9 VALUES OF PHI IN RAD.
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DIMENSION FN(9),RY(9),RX(9),ALPHA(9),DF(3)
      DATA S/1.000/
      IF(NSIG-2)100,200,200
C   FIND 8 POINTS ON CUBIC SURROUNDING RY(1),RX(1),ALPHA(1)
100  X1=S/(0.173205080+01)
      X2=X1/RY(1)
      C=RY(1)*DCOS(RX(1))
      IF(C.EQ.0.000)C=100.000
      X3=X1/C
      DO 10 I=2,5
      RY(I)=RY(1)+X1
      RY(I+4)=RY(1)-X1
10   CONTINUE
      DO 20 I=2,8,2
      RX(I)=RX(1)+X2
      RX(I+1)=RX(1)-X2
20   CONTINUE
      DO 30 I=2,6,4
      ALPHA(I)=ALPHA(1)+X3
      ALPHA(I+1)=ALPHA(I)
      ALPHA(I+2)=ALPHA(1)-X3
      ALPHA(I+3)=ALPHA(I+2)
30   CONTINUE
      RETURN
C   FIND PARTIALS
200  AM=0.125000
      DF(1)=AM*(FN(2)-FN(6)+FN(3)-FN(7)+FN(4)-FN(8)+FN(5)-FN(9))
      DF(2)=AM*(FN(2)-FN(3)+FN(4)-FN(5)+FN(6)-FN(7)+FN(8)-FN(9))
      DF(3)=AM*(FN(2)-FN(4)+FN(3)-FN(5)+FN(6)-FN(8)+FN(7)-FN(9))
240  DNDR=DF(1)/X1
      DNDT=DF(2)/X2
      DNDP=DF(3)/X3
      NSIG=3
      RETURN
      END

```


Appendix C

Block Diagram, Flow Chart, and Program Listing for WIMP Driving Program OBLFACT

Explanation:

C1. OBLFACT BLOCK DIAGRAM

This presentation illustrates the communication and iteration network employed to generate the $M(3000)F_2$ and $f_o F_2$ gradient correction factors required to match the predicted leading edge to the given oblique ionogram. The function of the various blocks is generally described as follows:

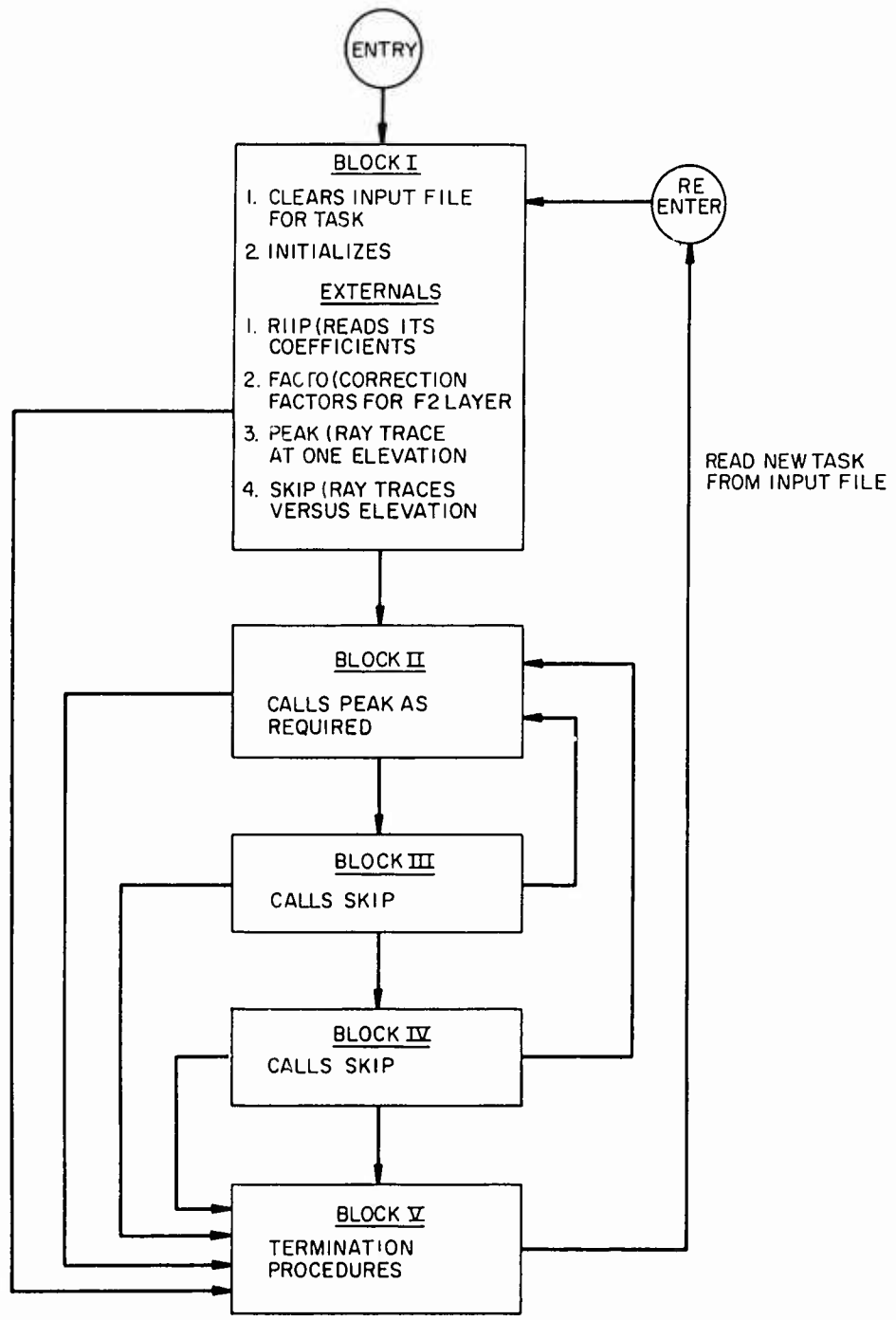
- BLOCK I: Initialization and Input Procedures.
- BLOCK II: Refinement of $M(3000)F_2$ Gradient Correction Factor.
- BLOCKS III and IV: Refinement of $f_o F_2$ Gradient Correction Factor.
- BLOCK V: Termination and Output Procedures.

C2. DETAILED FLOW CHARTS

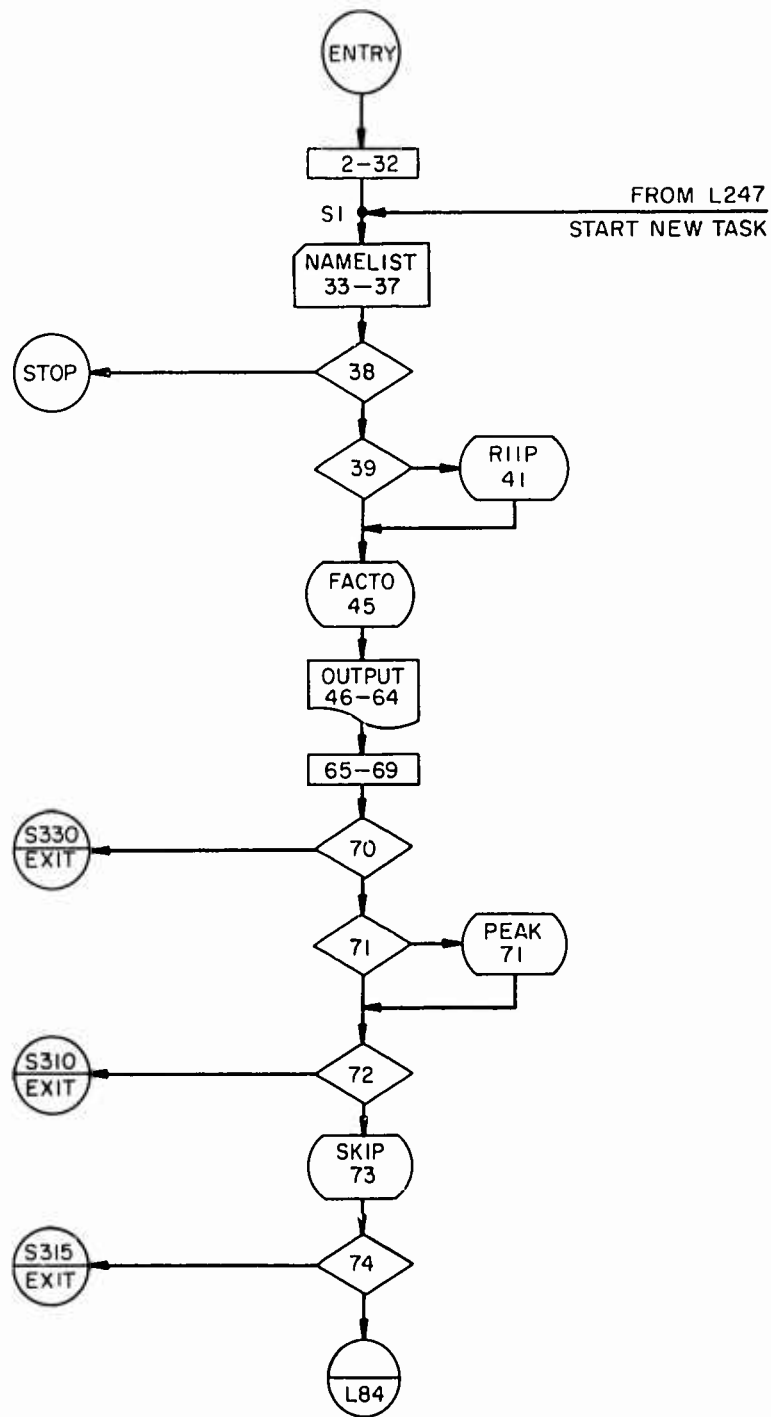
Detailed flow charts are presented for each block. Symbols and conventions are the same as described in Appendix A.

C3. PROGRAM LISTING

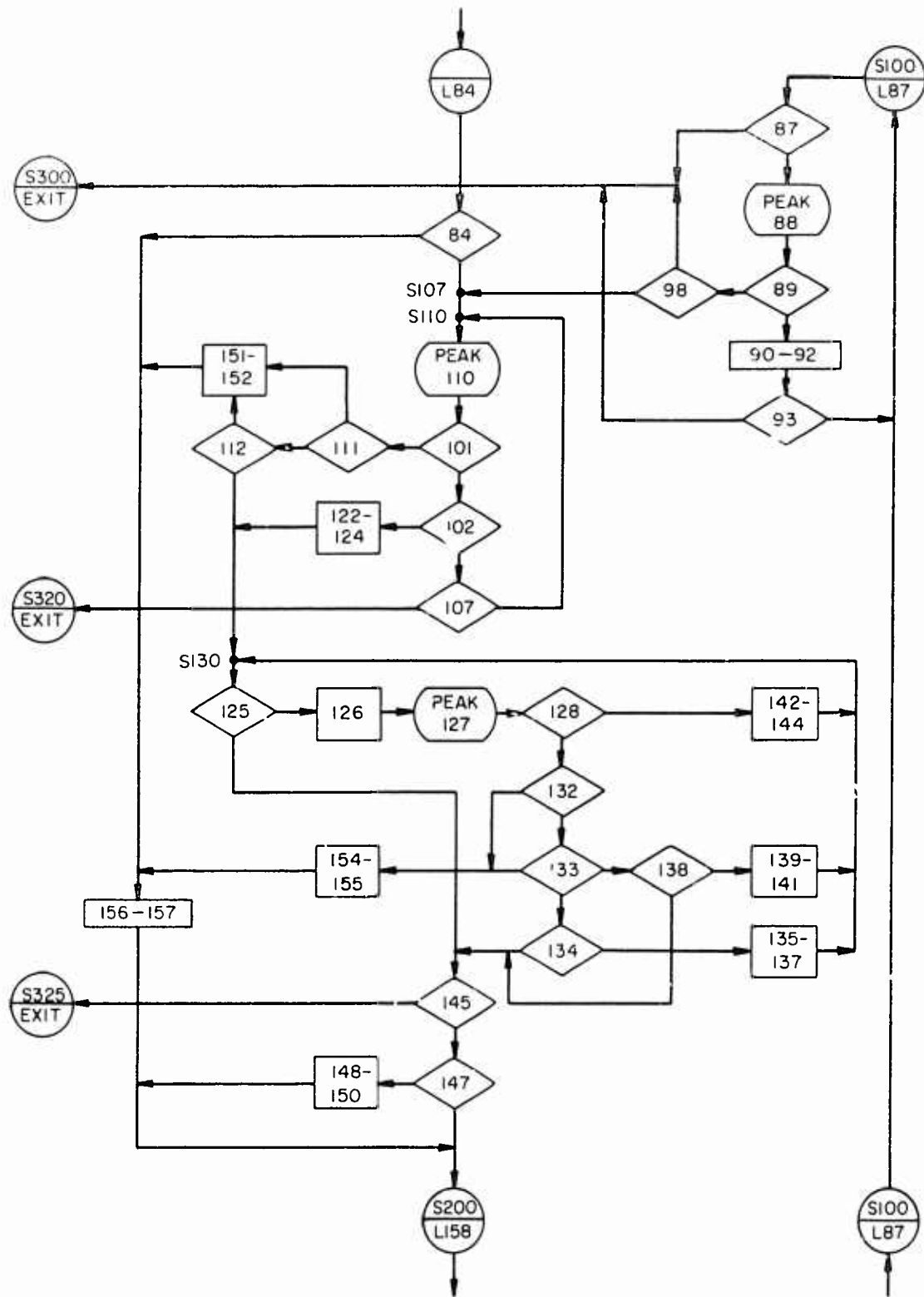
Listings are included for OBLFACT, PEAK, and SKIP.



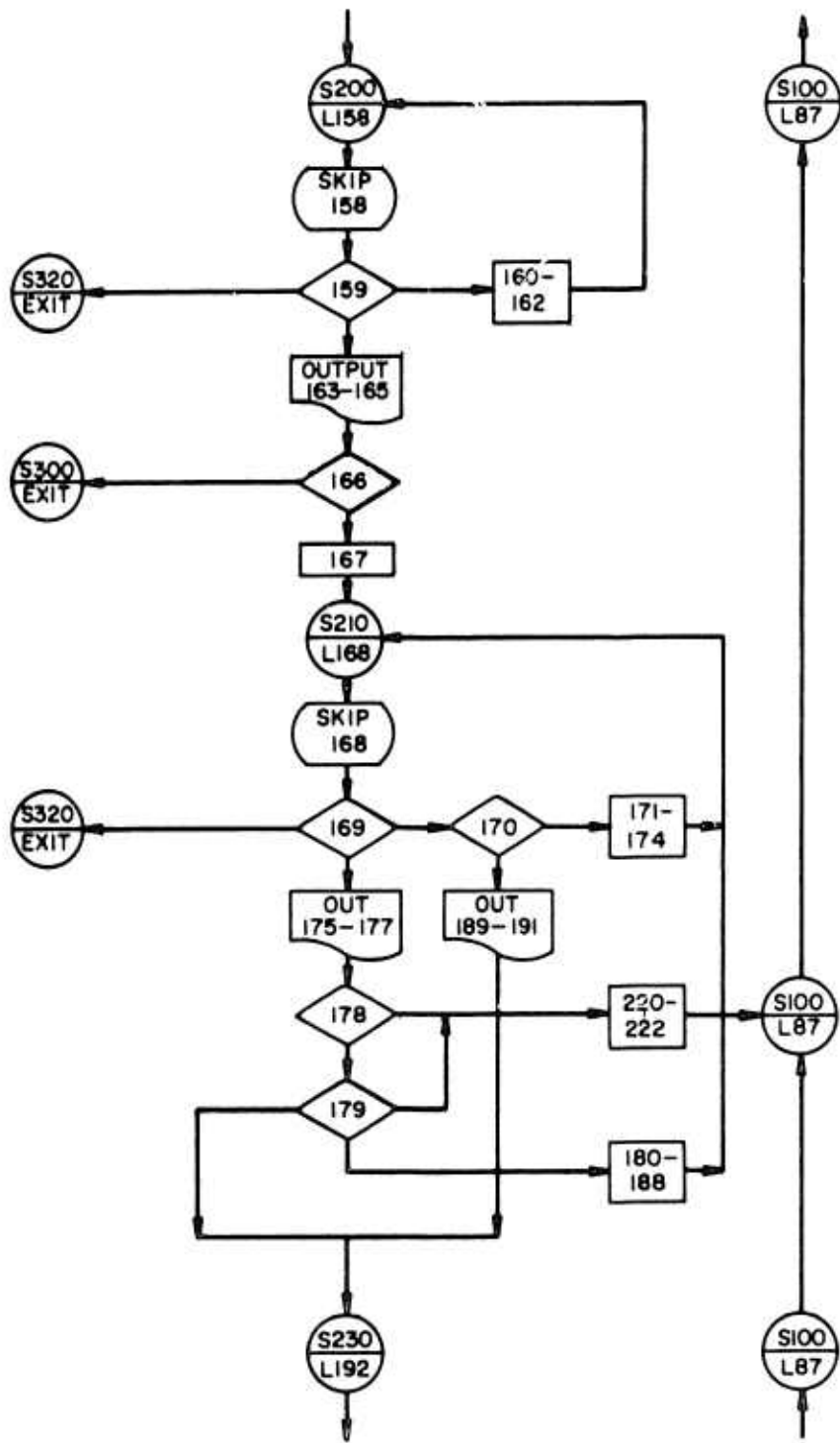
OBLFACT Block Diagram



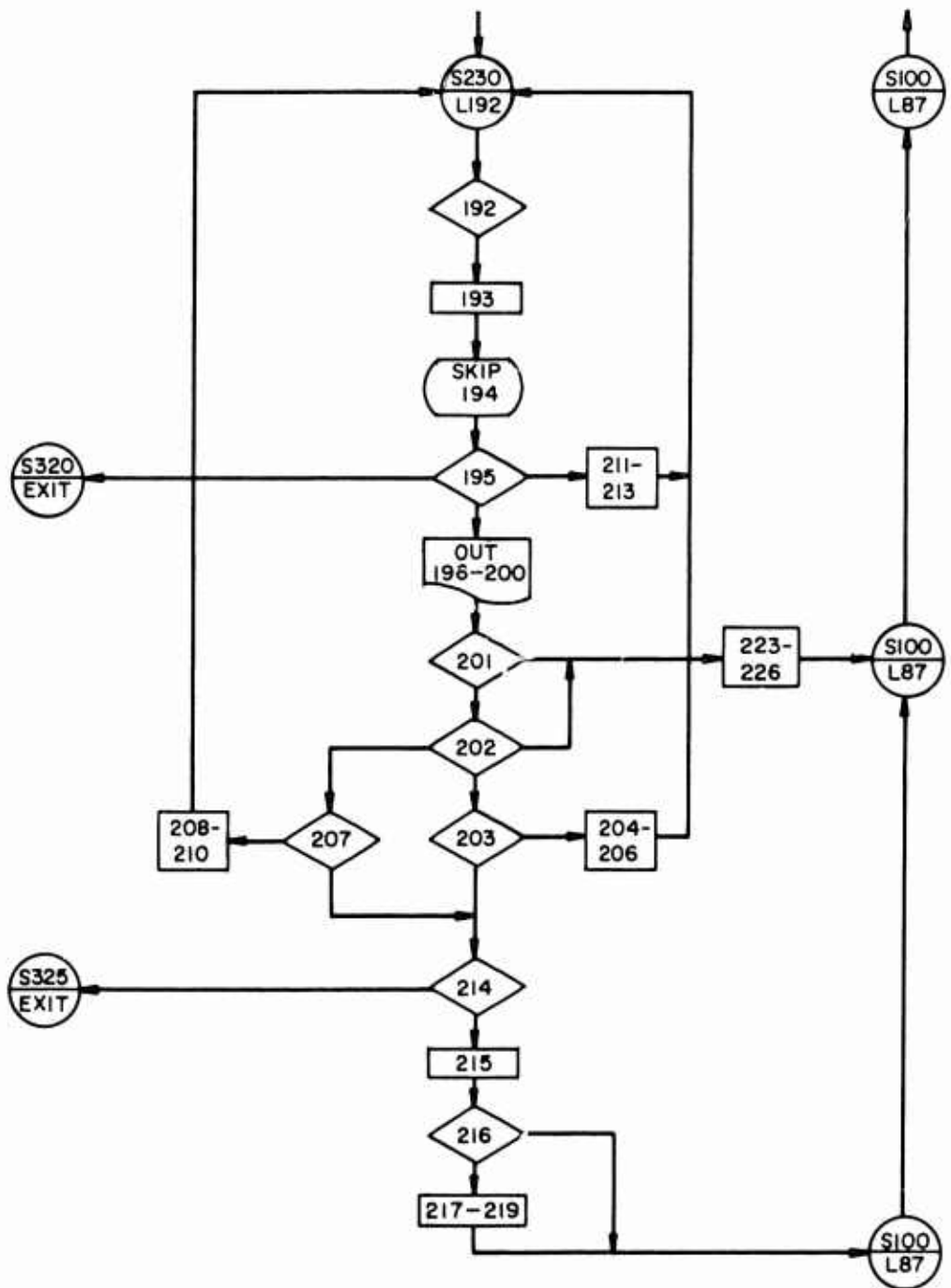
Block I, Detailed Flowchart



Block II, Detailed Flowchart



Block III, Detailed Flowchart



Block IV, Detailed Flowchart

```

SUBROUTINE OBL
PROGRAM OBLFACT (INPUT, OUTPUT, TAPE5=INPUT, TAPE6=OUTPUT)
IMPLICIT DOUBLE PRECISION (A-H, M, O-Z)
INTEGER MODE
DOUBLE PRECISION NL1, NLREF
LOGICAL SMOOTH, GPONLY
COMMON/ GPFLAG/ GPONLY, IWRITE
COMMON/ FIDDLE/ FP, FS, R1, NL1, WL1, AZ, RS, ELSTEP, MODE, NSKPCL
COMMON/ PERTC/ NLREF, WLREF, PERTP(14)
COMMON/ RIIPAR/ DUM1(11), SN, ZT, YRMO, DOY, HAESSET, MFAC, F2FAC, F1FAC,
1 EFAC, H2FAC, DUM2(3), ID, IA, SMOOTH
NAMFLIST/ INPUT/ SN, ZT, YRMO, DOY, MFAC, F2FAC,
1 NL1, WL1, R1, NLREF, WLREF, RS, AZ, ELSTEP, MODE,
1 FCF2R, HMINR, OCHK, FP, DELP, FS, DELS, MR0, FR0
3, IRSTRT, ZTREF
IRSTRT=1
GPONLY=.TRUE.
IWRITE=0
IO=1
IA=0
R1=6370.D0
RS=6370.D0
MODE=-1
NL1=
WL1=
OCHK=10.D0
SN30=0.D0
NLREF=NL1
WLREF=WL1
AZ=
ELSTEP=1.00
1 FR0=0.D0
MR0=0.D0
FP= 0.D0
DELP=0.D0
READ(5, INPUT)
IF (IRSTRT.EQ.0) STOP
IF (SN30.EQ.YRMO) GO TO 4
SN30=YRMO
CALL RIIP(0.D0, 0.D0, 0.D0, 0.D0)
4 IPKCNT=0
FCF2R=- DABS (FCF2R)
HMINR=- DABS (HMINR)
CALL FACTO (NLREF, WLREF, FCF2R, HMINR, ZTREF)
CCCC WRITE (6, INPUT)
WRITE (6, 900) SN, ZT, YRMO, DOY, MFAC, F2FAC
900 FORMAT (1X, (SN =[, 11X, D24.18/1X, (ZT =[, 11X, D24.18/
* 1X, (YRMO =[, 11X, D24.18/1X, (DOY =[, 11X, D24.18/
* 1X, (MFAC =[, 11X, D24.18/1X, (F2FAC =[, 11X, D24.18)
WRITE (6, 901) NL1, WL1, R1, NLREF, WLREF, RS
901 FORMAT (1X, (NL1 =[, 11X, D24.18/1X, (WL1 =[, 11X, D24.18/
* 1X, (R1 =[, 11X, D24.18/1X, (NLREF =[, 11X, D24.18/
* 1X, (WLREF =[, 11X, D24.18/1X, (RS =[, 11X, D24.18)
WRITE (6, 902) AZ, ELSTEP, MODE, FCF2R, HMINR, OCHK
902 FORMAT (1X, (AZ =[, 11X, D24.18/1X, (ELSTEP =[, 11X, D24.18/
* 1X, (MODE =[, 16X, I3 /1X, (FCF2R =[, 11X, D24.18/
* 1X, (HMINR =[, 11X, D24.18/1X, (OCHK =[, 11X, D24.18)

```

```

WRITE(6,903)FP,DELP,FS,DELS,MRO,FRO
903 FORMAT(1X,(FP=[,11X,024.18/1X,(DELP=[,11X,024.18/
* 1X,(FS=[,11X,024.18/1X,(DELS=[,11X,024.18/
* 1X,(MRO=[,11X,024.18/1X,(FRO=[,11X,024.18)
WRITE(6,904)IRSTRT,ZTREF
904 FORMAT(1X,(IRSTRT=[,16X,I3 /1X,(ZTREF=[,11X,024.18)
IM01=0
IF01=0
NSKPCL=0
IGOBAK=0
GPP0=0.00
IF(DABS(DELP).LT.DCHK.AND.DABS(DELS).LT.DCHK) GO TO 330
IF(FP.GE.5.7400) CALL PEAK(FRO,MRO,GPP0,IGOBAK)
IF(IGOBAK.GT.0) GO TO 310
CALL SKIP(FRO,MRO,GPS0,0,IGOBAK)
IF(IGOBAK.GT.0) GO TO 315
GPPDES=GPP0+DELP
GPSDES=GPS0+DELS
WRITE(6,111) GPPDES,GPSDES
111 FORMAT(1 DESIRED GPP=[,4P015.2,(, GPS=[,015.2)
DELP1=DELP
DELS1=DELS
DELP0=DELP
DELS0=DELS
MRO=MRO
IF(DABS(DELP).LT.DCHK) GO TO 197
GO TO 107
C MR FIDDLING
100 IF(FP.LT.5.7400) GO TO 300
CALL PEAK(FRO,MRO,GPP0,IGOBAK)
IF(IGOBAK.EQ.0) GO TO 105
MRO=MRO
MRO=MRO+.00100
IPKCNT=IPKCNT+1
IF(IPKCNT-100) 100,320,320
105 DELP0=GPPDES-GPP0
NSTMT=105
WRITE(6,1111) NSTMT,FRO,MRO,DELP0
1111 FORMAT(I10,1P3015.7)
IF(DABS(DELP0).LT.DCHK) GO TO 300
107 MRO=MRO-DSIGN(.00100,DELP0)
110 CALL PEAK(FRO,MRO,GPP1,IGOBAK)
IF(IGOBAK.EQ.0) GO TO 115
IF(DELP0.GT.0.00) GO TO 128
MRO=MRO
MRO=MRO-DSIGN(.00100,DELP0)
DELP0=-10000.00
IPKCNT=IPKCNT+1
IF(IPKCNT-100) 110,320,320
115 DELP1=GPPDES-GPP1
NSTMT=115
WRITE(6,1111) NSTMT,FRO,MRO,DELP1
IF(DABS(DELP1).LT.DCHK) GO TO 190
IF(DELP1*DELP0) 130,190,120
120 MRR=DELP1*(MRO-MRO)/(DELP0-DELP1)
IF(DABS(MRR).GT.0.100) MRR=DSIGN(0.100,MRR)
MRR=MRO+MRR

```



```

      IF(-DELP0.EQ.10000.000.OR.(MR1-MRR)*DELP0.LE.0.00) OBL
1  MRR=MR1-DSIGN(.00100,DELP1) OBL
      MR0=MR1 OBL
      MR1=MRR OBL
      DELP0=DELP1 OBL
      GO TO 110 OBL
128  DELP1=-10000.00 OBL
      NSTMT=128 OBL
      WRITE(6,1111) NSTMT,FR0,MR1,DELP1 OBL
130  IF(DABS(MR1-MR0).LT..000100) GO TO 180 OBL
      MRR=(MR1+MR0)*.500 OBL
      CALL PEAK(FR0,MRR,GPPR,IGOBAK) OBL
      IF(IGOBAK.GT.0) GO TO 160 OBL
      DELPR=GPPDES-GPPR OBL
      NSTMT=130 OBL
      WRITE(6,1111) NSTMT,FR0,MRR,DELPR OBL
      IF(DABS(DELPR).LT.DCHK) GO TO 195 OBL
      IF(DELPR*DELP0) 150,195,140 OBL
140  IF(DABS(DELPR).GT.DABS(DELP0)) GO TO 180 OBL
      DELP0=DELPR OBL
      MR0=MRR OBL
      GOTO 130 OBL
150  IF(DABS(DELPR).GT.DABS(DELP1)) GO TO 180 OBL
      DELP1=DELPR OBL
      MR1=MRR OBL
      GOTO 130 OBL
160  DELP1=-10000.00 OBL
      MR1=MRR OBL
      GO TO 130 OBL
180  IF(IM01*IF01.EQ.1) GOTO 325 OBL
      IM01=1 OBL
      IF(DABS(DELP1).GE.DABS(DELP0)) GO TO 200 OBL
      DELP0=DELP1 OBL
      MR0=MR1 OBL
      GOTO 200 OBL
190  MR0=MR1 OBL
      DELP0=DELP1 OBL
      GOTO 197 OBL
195  MR0=MRR OBL
      DELP0=DELPR OBL
197  IM01=0 OBL
C  FR FIDDLE OBL
200  CALL SKIP(FR0,MR0,GPS0,1,IGOBAK) OBL
      IF(IGOBAK-1) 205,201,320 OBL
201  FR1=FR0 OBL
      FR0=FR1+.00100 OBL
      GO TO 200 OBL
205  DELS0=GPPDES-GPS0 OBL
      NSTMT=205 OBL
      WRITE(6,1111) NSTMT,FR0,MR0,DELS0 OBL
      IF(DABS(DELS0).LT.DCHK) GO TO 300 OBL
      FR1=FR0-DSIGN(.00100,DELS0) OBL
210  CALL SKIP(FR1,MR0,GPS1,1,IGOBAK) OBL
      IF(IGOBAK-1) 215,211,320 OBL
211  IF(DELS0.GT.0.00) GO TO 228 OBL
      FR0=FR1 OBL
      FR1=FR0-DSIGN(.00100,DELS0) OBL

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```

DELS0=-10000.00 OBL
GO TO 210 OBL
215 DELS1=GPSDES-GPS1 OBL
NSTMT=215 OBL
WRITE(6,1111) NSTMT,FR1,MRO,DELS1 OBL
IF(DABS(DELS1).LT.DCHK) GO TO 290 OBL
IF(DELS1*DELS0) 230,290,220 OBL
220 FRR=DELS1*(FR1-FR0)/(DELS0-DELS1) OBL
IF(DABS(FRR).GT.0.1D0) FRR=DSIGN(0.1D0,FRR) OBL
FRR=FR1+FRR OBL
IF(-DELS0.EQ.10000.0D0.OR.(FR1-FRR)*DELS0.LE.0.0D0) OBL
1 FRR=FR1-DSIGN(.001D0,DELS1) OBL
FR0=FR1 OBL
FR1=FRR OBL
DELS0=DELS1 OBL
GOTO 210 OBL
228 DELS1=-10000.00 OBL
NSTMT=228 OBL
WRITE(6,1111) NSTMT,FR1,MRO,DELS1 OBL
230 IF(DABS(FR1-FR0).LT..0001D0) GO TO 280 OBL
FRR=(FR1+FR0)*.5D0 OBL
CALL SKIP(FRR,MRO,GPSR,1,IGOBAK) OBL
IF(IGOBAK-1) 235,260,320 OBL
235 DELSR=GPSDES-GPSR OBL
NSTMT=235 OBL
WRITE(6,1111) NSTMT,FRR,MRO,DELSR OBL
OBL
OBL
IF(DABS(DELSR).LT.DCHK) GO TO 295 OBL
IF(DELSR*DELS0) 250,295,240 OBL
240 IF(DABS(DELSR).GT.DABS(DELS0)) GO TO 280 OBL
DELS0=DELSR OBL
FR0=FRR OBL
GOTO 230 OBL
250 IF(DABS(DELSR).GT.DABS(DELS1)) GO TO 280 OBL
DELS1=DELSR OBL
FR1=FRR OBL
GOTO 230 OBL
260 DELS1=-10000.00 OBL
FR1=FRR OBL
GO TO 230 OBL
280 IF(IM01*IF01.EQ.1) GO TO 325 OBL
IF01=1 OBL
IF(DABS(DELS1).GE.DABS(DELS0)) GO TO 100 OBL
DELS0=DELS1 OBL
FR0=FR1 OBL
GOTO 100 OBL
290 FR0=FR1 OBL
DELS0=DELS1 OBL
GOTO 297 OBL
295 FR0=FRR OBL
DELS0=DELSR OBL
297 IF01=0 OBL
GOTO 100 OBL
300 WRITE(6,305) MRO,FR0,DELP0,DELS0 OBL
305 FORMAT((0 CONVERGENT VALUES\ MR=[,1PD15.7,[, FR=[,D15.7/ OBL
1 10X,[ MISS DIST. PEAK=[,D10.3,[, SKIP=[,D10.3) OBL

```

```
GOTO 1 OBL
310 WRITE(6,312) OBL
312 FORMAT((0 PEAK RAYTRACE FAILS ON INPUT CASE, TRY DIFFERENT INPUT()) OBL
GOTO 1 OBL
315 WRITE(6,317) OBL
317 FORMAT((0 SKIP RAYTRACES FAIL ON INPUT CASE, TRY DIFFERENT INPUT()) OBL
GOTO 1 OBL
320 WRITE(6,322) OBL
322 FORMAT((0 100 ITERATIONS DONE BUT DOESN'T CONVERGE, [
1[ TRY DIFFERENT INPUT() OBL
GOTO 300 OBL
325 WRITE(6,327) OBL
327 FORMAT((0 CONVERGENCE PROBLEMS, TRY DIFFERENT INPUT()) OBL
GOTO 300 OBL
330 WRITE(6,332) OBL
332 FORMAT([ YOUR ORIGINAL INPUT CONVERGES() OBL
GOTO 1 OBL
END OBL
```

```

SUBROUTINE SKIP(FRR,MRR,GPS,IOPT,IGOBAK) SKI
IMPLICIT DOUBLE PRECISION (A-H,O-Z) SKI
REAL OUT(3) SKI
DOUBLE PRECISION MRR,MR,NL1,NLT,NLREF,GP(42),RS2(42) SKI
COMMON/PERTC/NLREF,WLREF,FR,FD,MR,DUM(11) SKI
COMMON/FIDDLE/FP,FS,R1,NL1,WL1,AZ,RS,ELSTEP,MODE,NSKPCL SKI
COMMON/REMVEN/INUSE,NNUSE(20),FCREF(20) SKI
NSKPCL=NSKPCL+1 SKI
IF(NSKPCL.GT.100) GO TO 120 SKI
IGOBAK=0 SKI
NELM=20.00/ELSTEP+1.00 SKI
FR=FRR SKI
MR=MRR SKI
DO 10 IEL=1,NELM SKI
EL=(IEL-1)*ELSTEP SKI
CALL TRISL(R1,NL1,WL1,AZ,EL,0.00,FS,MODE,RS,RS2(IEL),NLT,HLT, SKI
1PP,GP(IEL),AZF,ELF,SRANGE,ELSR,DIST,BEAR,IRETRN) SKI
IF(IRETRN-1) 6,8,12 SKI
6 DO 7 I=1,INUSE SKI
IF(NNUSE(I).NE.3) GO TO 8 SKI
7 CONTINUE SKI
GO TO 10 SKI
8 RS2(IEL)=1.020 SKI
GP(IEL)=1.020 SKI
10 CONTINUE SKI
IEL=NELM+1 SKI
12 IF(IEL.EQ.1) GO TO 110 SKI
RS2(IEL)=1.020 SKI
NELM=IEL-1 SKI
IMIN=1 SKI
IF=0 SKI
DO 20 IEL=1,NELM SKI
IF(RS2(IEL).GT.6378.8500) GO TO 20 SKI
IF=1 SKI
IF(GP(IEL).LT.GP(IMIN)) IMIN=IEL SKI
20 CONTINUE SKI
IF(IF.EQ.0) GO TO 110 SKI
GPS=GP(IMIN) SKI
IF(IOPT.EQ.0) GO TO 130 SKI
IF(RS2(IMIN+1).LT.6378.8500) GO TO 130 SKI
IF(RS2(IMIN+1).GE.0.9020) GO TO 130 SKI
IF(GP(IMIN+1).GT.GP(IMIN)) GO TO 130 SKI
GPS=GP(IMIN)+(GP(IMIN+1)-GP(IMIN))*(6378.8500-RS2(IMIN))/ SKI
1(RS2(IMIN+1)-RS2(IMIN)) SKI
GO TO 130 SKI
110 IGOBAK=1 SKI
GO TO 130 SKI
120 IGOBAK=2 SKI
130 OUT(1)=FR SKI
OUT(2)=MR SKI
OUT(3)=GPS SKI
WRITE(6-140) OUT,IGOBAK SKI
140 FORMAT(1 SKIP(,2F10.6,F10.2,I5) SKI
RETURN SKI
END SKI

```

ROUTINE PEAK

74/74 OPT=1

FTN 4.5+414

04/27

```
SUBROUTINE PEAK(FRR,MRR,GPP,IGOBAK) PEA
IMPLICIT DOUBLE PRECISION(A-H,O-Z) PEA
REAL OUT(3) PEA
DOUBLE PRECISION MRR,NL1,NLT,ELP(25),NLREF,MR PEA
COMMON/PERTC/NLREF,MLREF,FR,FD,MR,DUM(11) PEA
COMMON/FIDDLE/FP,FS,R1,NL1,HL1,AZ,RS,ELSTEP,MODE,NSKPCL PEA
COMMON/REMWEN/INUSE,NNUSE(20),FCREF(20) PEA
DATA ELP/11.900,10.300,8.900,7.700,6.700,5.900,5.200,4.600, PEA
1 4.100,3.900,5.200,4.800,4.500,4.200,4.00,3.800,2*3.700, PEA
2 2*3.600,3*3.500,2*3.400/ PEA
FR=FRR PEA
MR=MRR PEA
IF=FP-4.7400 PEA
CALL TRISL(R1,NL1,HL1,AZ,ELP(IF),0.00,FP,MODE,RS, PEA
1RS2,NLT,HLT,PP,GPP,AZF,ELF,SRANGE,ELSR,OST,BEAR,IGOBAK) PEA
IF(RS2.GT.6378.8500) IGOBAK=1 PEA
DO 1 I=1,INUSE PEA
IF(NNUSE(I).NE.3) IGOBAK=1 PEA
1 CONTINUE PEA
OUT(1)=FR PEA
OUT(2)=MR PEA
OUT(3)=GPP PEA
WRITE(6,11) OUT,IGOBAK PEA
11 FORMAT(1 PEAK(,2F10.6,F10.2,I5) PEA
RETURN PEA
END PEA
```