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EXTENDED OIL-CHANGE AND OIL-FILTER-CHANGE INTERVALS FOR DOD 5- --ETC(U)
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Report 2234

EXTENDED OIL-CHANGE AND OIL-FILTER-CHANGE
INTERVALS FOR DOD 5- TO 200-KILOWATT
DED GENERATOR SETS

By

Chester R. Gurski
Ernest Fitzgibbons
John W. Dreger

March 1978



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U.S. ARMY MOBILITY EQUIPMENT
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The in-house investigation described was to determine whether the industry- and military- standard oil-change interval of 100 hours could be extended for the DOD Family of Diesel Engine Driven Generator Sets using MIL-L-2104C specification lubricating oil. The investigation was conducted in two phases. In Phase I, the oil and filter were changed each 100 hours in accordance with the servicing and maintenance guide specified for the preproduction model 5,000-hour reliability and acceptance tests. In Phase II, the oil-change and filter-change inter- vals were established by the condition of the oil. The condition of the oil was monitored by		

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chemical and spectrometric analyses. Based on the test results and the urgency of the current energy crisis, the Project Manager, Mobile Electric Power, issued an oil-change policy for the 15-through 200-kW size generator sets directing that the oil and oil filters be changed each 300 hours of engine running (normal running conditions) or after 6 months whichever comes first. It is conservatively estimated that a savings in excess of \$1.7 million a year can be realized by the military with the implementation of this directive for generator sets alone.

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SUMMARY

Since July 1972, MERADCOM has been conducting an in-house, two-phase test program to determine whether the industry and military-standard, engine-oil-change interval of 100 hours could be extended for the DOD Family of Diesel Engine Driven (DED) Generator Sets using Specification MIL-L-2104C lubricating oil.

Under Phase I of the program, a total of 54,392 hours of engine running was accumulated on 13 *preproduction* model generator sets that included seven different models of diesel engines. Chemical and spectrometric data, obtained from analyses of oil samples that were taken at regular 100-hour intervals, were plotted for baseline reference.

Phase II of the program was initiated in February 1974 and included eight *production* model generator sets utilizing four different diesel engine models. The major difference between Phase I and II was in the oil-change and oil-filter-change intervals. Under Phase I, the oil and the oil filter were required to be changed each 100 hours in accordance with the servicing and maintenance guide applicable to the *preproduction* model, 5000-hour reliability and acceptance test. Under Phase II, the oil and the oil filter were changed only when required as indicated by the condition of the oil based on oil-sample analyses. A total of 22,138 hours of engine operations was accumulated. Repeatable oil-change and oil-filter-change intervals of 700 hours on each of the 15- and 30-kilowatt sets, 600 hours on each of the 60-kilowatt sets, and 1000 hours on each of the 100-kilowatt sets were obtained. Included also under Phase II were 1851 hours of "Extreme-Temperature" and "Stand-by, Low-Usage" operations on each of the 60- and 100-kilowatt sets. There was no variation in analyses data noted in oil samples taken during these operations as compared to the patterns previously established under normal, ambient conditions. Following completion of all engine running, several engines were disassembled, and critical parts were examined on a "one-to-one" basis, i.e., Phase I vs Phase II of like models. The examinations revealed no major differences in the wear patterns on parts.

Based on the test results and the urgency of the current energy crisis, the Project Manager, Mobile Electric Power, issued a new oil-change policy, effective date, 20 January 1976, directing that the oil and the oil filters be changed each 300 hours of engine running or after each 6 months, whichever occurs first, for all DOD Diesel Engine Driven Generator Sets in the 15- through 200-kilowatt range when operating under normal running conditions. It is conservatively estimated that a savings in excess of \$1.7 million a year can be realized by the military with the implementation of this directive. This does not include the man-hours that will be saved in servicing, stocking, and handling.

PREFACE

Chester R. Gurski and Ernest Fitzgibbons, Support Equipment Group, Engineering Division, Electrical Power Laboratory, MERADCOM, compiled this final report.

John W. Dreger, the Project Engineer, prepared the interim report, MERDC 2153, dated August 1975, and coordinated the findings with Colonel R. H. Sievers, Jr., DOD Project Manager, Mobile Electric Power, AMC (DARCOM).

The analysis and interpretation of the oil sample data were performed by Sidney Levine and Basil Zanedis. The chemical and wear-metal analyses were performed by SP4 R. T. Wood, J. Bennett, and N. H. Arshad, Material Technology Laboratory, MERADCOM.

The computer programing and printout graphs were compiled by Dorothine Murphy, Mathematical and Computer Science Division, MERADCOM.

The inspections and the evaluation of wear patterns on critical engine parts were made by Thomas C. Bowen, Energy and Water Resources Laboratory, Fuels and Lubricants Division, MERADCOM.

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EXTENDED OIL-CHANGE AND OIL-FILTER-CHANGE INTERVALS FOR DOD 5- TO 200-KILOWATT DED GENERATOR SETS

I. INTRODUCTION

1. **Statement of the Purpose.** The purpose of this controlled test program was to determine an optimum oil-change and oil-filter-change interval, using Military Specification MIL-C-2104C lubricating oil, that would not adversely affect the reliability or total life cycle of engines in the DOD Family of Diesel Engine Driven (DED) Generator Sets.

2. **Background.** At the request of the DOD Project Manager, Mobile Electric Power (PM-MEP), in May 1972, a two-phase test program was formulated and subsequently approved. The program included both preproduction- and production-model sets of the DOD, diesel engine driven generator family currently being procured. Phase I of the program was made a part of the scheduled 5000-hour reliability and acceptance tests required by contract for the preproduction-model generator sets and included 13 sets which used 7 different models of engines. A baseline of reference was developed from the oil analyses data based on the specified 100-hour oil-change and oil-filter-change intervals.

Initially, Phase II of the program was to include two production-model DOD sets of each size ranging from 5 through 200 kilowatts. Each set was to run 5000 hours at normal, ambient temperature with oil changes being dictated by the condition of the oil as determined by chemical and spectrometric analyses of oil samples taken at specified intervals during set operations. However, during the course of the program, changes were made in the schedule, i.e., the 5000 hours of operation was reduced to 3000 hours and "extreme temperature" and "stand-by, low-usage" operations were added for the 60- and 100-kilowatt sets. Also, no testing was accomplished on either the 5- or 10-kW sets because of the long leadtime for delivery, and the 200-kW sets were not tested because the engine manufacturer had proposed making major changes to this series of engines for all future production.

II. PROCEDURE

3. Approach.

a. **Phase I.** Phase I was conducted from July 1972 through December 1973. Thirteen preproduction-model DOD generator sets of varied sizes powered by seven different models of diesel engines were subjected to long-term endurance running

(2200/5278 hours) at normal, ambient temperatures. Tests were conducted by the U.S. Army Mobility Equipment Research and Development Command (MERADCOM), Fort Belvoir, Virginia, and by the Test and Evaluation Command (TECOM), Aberdeen Proving Ground, Aberdeen, Maryland.

b. **Phase II.** Phase II was conducted from February 1974 through December 1976. Eight production-model DOD generator sets of four sizes powered by four different models of diesel engines were subjected to long-term endurance running (1465/3578 hours) at normal, ambient temperatures. In addition, two different size sets were subjected to 300 hours operation at +125° F ambient temperature, and two other sets were subjected to "stand-by, low-usage" type operations that consisted of running at variable loads for 1 hour in every 8 hours for 350 hours. All of the testing was conducted at MERADCOM or at a commercial facility – General Environments Corporation, Hartwood, Virginia.

c. **Test Units and Test Time.** The types and sizes of the generator sets, the makes and models of the diesel engines powering each set, the type of running, and the accumulated number of hours for each set are included in Table 1 for Phase I and Table 2 for Phase II.

Table 1. Phase I – Preproduction-Model DOD Generator Sets

Power (kW)	Frequency (Hz)	Set Serial Number	Engine Model	Test Mode	Hours
5	60	359821	Onan DJE 99E	Norm Amb	5,048
10	60	359823	Onan DJF 99E	Norm Amb	4,984
15	60	RZ-00001	Hercules D198ER	Norm Amb	2,500
15	400	RZ-10012	Hercules D198ER	Norm Amb	2,917
30	60	RZ-30002	Hercules D298ER	Norm Amb	2,200
30	400	RZ-40002	Hercules D298ER	Norm Amb	2,824
60	60	2001	Allis Chalmers 3500	Norm Amb	5,118
60	60	2003	Allis Chalmers 3500	Norm Amb	5,115
60	400	6002	Allis Chalmers 3500	Norm Amb	5,101
100	60	4302-001	Caterpillar D-333T	Norm Amb	5,278
100	60	4302-002	Caterpillar D-333T	Norm Amb	5,200
200	60	4305-001	Caterpillar D-343T/A	Norm Amb	4,275
200	60	4305-004	Caterpillar D-343T/A	Norm Amb	3,832
Total Hours					54,392

Table 2. Phase II -- Production-Model DOD Generator Sets

Power (kW)	Frequency (Hz)	Set Serial Number	Engine Model	Test Mode	Hours
15*	60	RZ-00001	Hercules D198ER	Norm Amb	2,341
15**	400	RZ-10012	Hercules D198ER	Norm Amb	2,089
30*	60	TZ-30002	Hercules D298ER	Norm Amb	1,465
30**	400	RZ-40002	Hercules D298ER	Norm Amb	1,708
60	60	FZ-00455	Allis Chalmers 3500	Norm Amb	3,315
				+125°F Temp	302
60	400	FZ-06024	Allis Chalmers 3500	Norm Amb	3,348
				Stand-by,	
				Low-Usage	352
100	60	UZ-00001	Caterpillar D333T	Norm Amb	3,578
				+125° Temp	300
100	60	UZ-02008	Caterpillar D333T	Norm Amb	3,001
				Stand-by,	
				Low-Usage	339
				Total Hours	22,138

* Preproduction-model generator set with new engine installed.

** Original preproduction-model generator set.

4. Description of Test Program.

a. **Phase I.** Phase I consisted of performing both a chemical and a spectrometric analysis of oil samples taken at the regularly scheduled, 100-hour oil-change and oil-filter-change intervals during the entire reliability endurance test program for preproduction-model DOD generator sets. The endurance reliability test was a contractual requirement contingent on the release of each set for further production. All engine maintenance and servicing were performed as specified for the endurance reliability program.

b. **Phase II.** Phase II consisted of running new production model DOD generator sets, except as shown in Table 2, with the oil change and oil-filter change being performed only as the data from the chemical and spectrometric oil analyses required. The oil analyses were performed within 24 hours after the oil samples were taken from the engines; therefore, there were no delays that could possibly jeopardize the results of the program. There were over 520 chemical and 2080 spectrometric analyses made on oil samples taken during testing. All other engine and generator set maintenance and servicing were performed in accordance with the technical manuals applicable to each size set.

c. **Receiving Inspection.** A visual inspection of each production-model generator set was made, and the sets were found to be in satisfactory, "as new" condition with only a very few hours registered on the time meters. The oil, oil filters, and fuel filters were changed on each set. A logbook, initiated for each set, contained all the identification information, i.e., set type; size; serial number; manufacturer; engine make, model, and serial number; dates of manufacture; location of test site; and operating hours registered at time of delivery of the set. The logbooks include a continuing account of set operations, servicing, and maintenance performed; failures; and all other instances relative to successful operation. Notations were included regarding fuel type and sulfur content, lubricating oil specification including bulk batch-lot number, fuel and oil consumption, and when an oil sample was taken.

d. **Preparation of Sets for Test.** The generator sets were prepared for operation in accordance with the procedures contained in the applicable DOD generator technical manuals as listed in Table 3. An external fuel-supply line was connected to the set auxiliary fuel pump.

Table 3. Technical Manuals Used for Generator Preparation

Set	Model Number	TM Number
15 kW, 60 Hz	MEP-004A (T.U.) ¹	TM 5-6115-464-12
15 kW, 400 Hz	MEP-113A (T.P.) ²	TM 5-6115-464-12
30 kW, 60 Hz	MEP-005A (T.U.)	TM 5-6115-465-12
30 kW, 400 Hz	MEP-114A (T.P.)	TM 5-6115-465-12
60 kW, 60 Hz	MEP-006A (T.U.)	TM 5-6115-545-12
60 kW, 400 Hz	MEP-115A (T.P.)	TM 5-6115-545-12
100 kW, 60 Hz	MEP-007A (T.U.)	TM 5-6115-457-12
100 kW, 60 Hz	MEP-106A (T.P.)	TM 5-6115-457-12

1. T.U. - Tactical Utility

2. T.P. - Tactical Precise

An oil-sampling valve with the necessary plumbing was installed on each engine in the lube gallery to provide a means for taking oil samples as required during the course of the endurance test. The installation of the oil-sampling valve can be seen in Figure 1.

e. **Instrumentation.** Various temperature, pressure, and electrical parameters were measured.

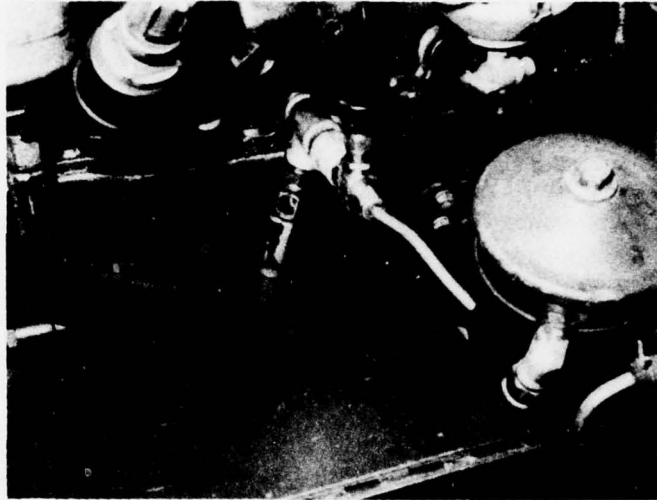


Figure 1. Oil sampling valve.

(1) **Temperature.** The following temperatures were measured:

- Engine coolant "in" and "out"
- Intake manifold
- Air inlet
- Engine exhaust
- Engine oil in sump and gallery
- Generator frame
- Ambient air
- Fuel oil

(2) **Pressure.** The following pressures were measured:

- Lube gallery
- Exhaust manifold
- Inlet manifold

(3) **Electrical.** The following electrical measurements were made:

- Terminal voltage
- Line current
- Power
- Frequency

All instruments were of laboratory grade and were maintained under a periodic calibration program to meet the requirements of MIL-C-45662.

f. **Fuel and Lubricants.** The diesel fuel used during testing was grade DF2 certified to meet the requirements of VV-F-800a.

The lubricating oil used during testing was SAE grade 30 certified to meet the requirements of MIL-L-2104C.

g. **Pre-endurance Operation.** All starting and operating procedures were in accordance with the appropriate technical manuals except as pertain to the scheduled oil-change and oil-filter-change intervals which were dictated by the condition of the oil based on the analysis of oil samples.

Set installation for tests was in such a manner as to minimize the ingestion of exhaust gases between engines.

h. **Endurance Tests.** All tests were conducted in accordance with MIL-STD-705B, Test Method 690.1C, except as noted.

The generators were connected, using the three-phase, 120-volt connection, to suitable load banks having a 1/4-load-step and 0.8 power-factor capability.

All temperature, pressure, and electrical data were observed and recorded hourly.

Smoke readings were taken during each rated-load step of the schedule.

Atmospheric conditions were noted on a daily basis and recorded on data sheets.

Normal, ambient operation was performed on a 24-hour, 7-day basis in accordance with the load-cycle schedule given in Table 4.

Plus 125°F operation was at the "full-load" condition with no oil change or oil-filter change.

Stand-by, low-usage operation included 1 hour of each 8 hours running in accordance with the load-cycle given in Table 5. This approximated a 5-month period with no oil change or oil-filter change.

Table 4. Endurance Load-Cycle Schedule

Step No.	Total Time (hr)	Load Condition
1	20	1/2
2	4	0
3	24	Full
4	24	1/4
5	24	3/4

Table 5. Stand-by, Low-Usage, Load-Cycle Schedule

Step No.	Total Time (min)	Load Condition
1	5	Start – Full
2	15	$\frac{1}{4}$
3	10	Full
4	10	$\frac{1}{4}$
5	10	$\frac{1}{2}$
6	10	0

The following logbook entries were made during each shift as applicable:

Date, shift hours, and total elapsed test hours.
 All adjustments made.
 Information regarding scheduled maintenance performed.
 Title and test method number of all performance tests performed.
 Explanation of all shutdowns.
 Results of periodic, visual inspections.
 All failures which occurred and repair parts used.
 Oil added between oil changes.

i. **Oil Samples.** Samples of oil were taken as follows:

One quart of each certified lot of lubricating oil prior to start of test.

One ounce every 25 hours of engine operation.

Eight ounces every 100 hours of engine operation.

Each oil sample was identified with the following information on the label:

Generator set serial number.
 Total number of hours that oil was used.
 Total number of engine operating hours.
 Pertinent servicing, maintenance, failure, and parts replacement and/or adjustments since last oil sample was taken and amount of oil added if any since last sample.

j. **Scheduled Maintenance.** Scheduled maintenance was performed as required in accordance with Tables 6, 7, and 8.

Table 6. Maintenance Schedule for 15- and 30-Kilowatt Generator Sets

Every 8 Hours

- (1) Check for unusual noise and vibration
 - (2) Check oil sump level (do not shut engine down for oil level checks.)
 - (3) Service air cleaner as necessary
 - (4) Check fault indicator panel lights and control panel for proper operation
-

Every 40 Hours

- (1) Tighten loose and leaking connections
 - (2) Check condition of air filters
 - (3) Check condition of fan and alternator belts
 - (4) Check engine coolant level
 - (5) Check specific gravity of battery electrolyte
 - (6) Wipe the engine and generator of excessive oil and dirt
-

Every 100 Hours

- (1) Inspect lifting frame, skid base, shutter assembly, thermostat housing, intake exhaust manifolds, and belts for looseness or damage and replace as necessary
 - (2) Clean fuel strainer and fuel pump screens
 - (3) Check hydraulic-oil sump level
-

Every 500 Hours

- (1) Inspect radiator and grille for damage and obstructions to air flow
 - (2) Check valve tappet clearance and adjust if necessary
 - (3) Check compression pressure at cranking speed
 - (4) Clean or replace as necessary fuel injector nozzles
-

Table 7. Maintenance Schedule for 60-Kilowatt Generator Sets

Every 8 Hours

- (1) Check for unusual noise and vibration
 - (2) Check sump-oil level – do not shut down engine for oil-level checks
-

Every 40 Hours

- (1) Tighten loose and leaking connections
 - (2) Check condition of air filters
 - (3) Check condition of fan and alternator belts
 - (4) Check engine coolant level
 - (5) Check specific gravity of battery electrolyte
 - (6) Wipe the engine and generator of excessive oil and dirt
-

Every 100 Hours

- (1) Change fuel filters (2)
 - (2) Clean crankcase breather
 - (3) *Clean fuel strainer*
 - (4) Clean fuel-pump screens
 - (5) Check hydraulic-oil sump level on precise set
-

Every 250 Hours

- (1) Pressure test radiator cap and cooling system
 - (2) Clean governor actuator strainer
-

Every 500 Hours

- (1) Change hydraulic-oil filter on precise set
 - (2) Change hydraulic oil on precise set
 - (3) Check valve clearance – replace valve-cover gasket
 - (4) Clean fuel nozzles, check the popping pressure of the injectors, and leak test the injector nozzle valve
 - (5) Check compression
 - (6) Change engine coolant
 - (7) Adjust fan- and alternator-belt tension
-

Every 1,000 Hours

- Replace fuel nozzles
-

Table 8. Maintenance Schedule for 100-Kilowatt Generator Set

Every 8 Hours

- (1) Check for unusual noise and vibration
 - (2) Check sump-oil level – do not shut down engine for oil-level checks
-

Every 40 Hours

- (1) Tighten loose and leaking connections
 - (2) Clean the air filters
 - (3) Wipe excessive dirt and oil off the engine and generator
-

Every 100 Hours

- (1) Change fuel filters (2)
 - (2) Clean fuel strainer
 - (3) Clean crankcase breather
 - (4) Check fan- and alternator-belt tension
 - (5) Check hydraulic-oil sump level on precise set
 - (6) Check specific gravity of battery electrolyte
-

Every 250 Hours

- (1) Change hydraulic filter on precise set
 - (2) Check engine coolant level
 - (3) Drain water and sediment from fuel filters
 - (4) Drain water and sediment from day tank
 - (5) Pressure test radiator cap and cooling system
 - (6) Clean governor-actuator strainer
-

Every 500 Hours

Change hydraulic oil on precise set

Every 1,000 Hours

Check valve clearance (first check will be performed at 500 hours)

5. Description of Oil Analyses and Sampling Procedures.

a. Oil Analyses. A description of the chemical and spectrometric oil analyses performed during this program is included in Tables 9 and 10. The precautionary limits discussed in the chemical tests were established prior to initiation of Phase I through coordination with manufacturers and laboratory personnel. These limits reflect current research and field experience. The warning limits outlined for the spectrometric analysis were established through coordination with the respective engine manufacturers. The manufacturers cautioned that the wear-metal concentrations could vary between engines depending upon basic internal engine construction, type of service (i.e., duty cycle), and the regularity with which routine maintenance is performed. Consequently, these limits were used as a guide tempered with a certain degree of discretion. No information on wear-metal concentrations was available from the Hercules engine manufacturer.

b. Sampling Procedures.

(1) Chemical Analysis. Eight-ounce oil samples were taken from each generator set at established intervals and stored in plastic bottles for eventual analysis. The samples were analyzed in accordance with the designated ASTM method for determination of each property.

(2) Spectrometric Analysis. Samples taken from each generator set at established intervals were stored in unused 1-ounce polyethylene vials. The samples were analyzed utilizing a Jarrell-Ash Model 750 Atom-Counter, Atomic-Emission, Direct-Reading Spectrometer. The electrodes of the spectrometer were made by National: the solution disc electrode was a Type L4075 AGKSP, 1/2-inch-diameter, 1/8-inch thick; the counter electrode was a Type L3957 AGKSP, 1/4-inch rounded upper, 1/16-inch radius. The maximum impurity concentrations for these electrodes were as follows: Aluminum - 0.5 ppm, Copper - 0.5 ppm, Iron - 0.4 ppm, and Silicon - 2.4 ppm. The instrument was standardized with Continental Oil Company Conostan Type D-12 metallo-organic standards in the following concentrations: 0-, 10-, 30-, 50-, 100-, and 300-ppm ranges.

III. TEST RESULTS

6. Oil Analyses Test Data. During this program, the results of each chemical and spectrometric oil analysis were tabulated and plotted using a CalComp Plotter. This computer printout technique greatly simplified making decisions to change oil and oil filters on each generator set during Phase II and also provided a reference for comparison with Phase I data (Appendices A and B).

Table 9. Chemical Oil Analysis

Chemical Property	Test Methods	Significance	Precautionary Limits
Viscosity — 100°F and 210°F	ASTM-D445	(1) Establishes viscosity index. (2) An indication of oxidation can be summarized by observing successive differences between viscosity at 100°F and 210°F.	Limit has been reached when viscosity at 210°F either increases in value to the next higher SAE grade (maximum oxidation) or decreases in value to the next lower SAE grade (maximum fuel dilution).
Flashpoint	Cleveland Open Cup	This is a key physical property in determining fuel dilution into the oil.	Limit has been reached when the flashpoint reaches 300°F or lower (maximum fuel dilution).
Total Acid and Total Base	ASTM-D664 and D2896	The total acid number (TAN) to a degree defines the buildup of acidic materials in oil resulting from combustion and oil oxidation, while the total base number (TBN) relates to the oil alkaline reserve provided to combat acidic products. Decreasing TAN is indicative of additive depletion.	TAN limit has been reached when TAN increases two whole numbers from that value recorded for new oil (batch sample). TBN limit has been reached when TBN decreases to one-half original value of new oil (batch sample).
Insolubles — Percent Benzene and Pentane	ASTM-D-893, Procedure B	In principle, the arithmetic difference between the Pentane and Benzene insolubles is a measure of oxidation	Benzene: When percentage of Benzene insolubles reaches 1.00 percent. Pentane: When percentage of Pentane insolubles reaches 1.50 percent.

Table 10. Spectrometric Oil Analysis

Metal	Allis Chalmers Model No. 3500		Caterpillar Model No. D333T	
	Parts	Warning Limit (ppm)*	Parts	Warning Limit (ppm)*
Aluminum	Pistons	80	Pistons	18
	Blowers		Main Bearings	
	Bearings		Rod Bearings	
			Oil-Pump Bushing	
			Timing Gear Bushing	
			Crankshaft Thrust Bushing	
			Fuel-Pump Lifter	
Tin	Bearings	30	Bearings	40
Chromium	Piston Rings Shafts	50	Piston Rings	20
Lead	Bearings	60	Overlay on Main and Rod Bearings	75
Silicon	Air-Cleaner Element	30	Air-Cleaner Element	30
Iron	Piston Rings	125	Crankshafts	120
	Cylinders		Cylinder Liners	
	Shafts		Camshaft	
			Connecting Rod and Gears	
Copper	Bushings	60	Rocker-Arm Bushings	30
	Bearings		Wrist-Pin Bushings	
			Timing-Gear Thrust Washer	
			Governor Bushing	
			Fuel-Transfer-Pump Bushing	
			Oil-Pump-Drive Thrust Washer	

* Wear-metal concentrations are based on manufacturer's recommendation. This information was not available for the Hercules, Model D-198 and D-298, engines.

7. **Oil Consumption Data.** Oil consumption for Phase I (preproduction models) is given in Table 11 and for Phase II (production models), in Table 12.

Table 11. Oil Consumption – Phase I, Preproduction Models

Set Description				
Power (kW)	Frequency (Hz)	Serial No.	Total Accumulated Hours	Average Oil Consumption (qt/100 h)
5	60	359821	5,048	Not Available
10	60	359823	4,984	Not Available
15	60	RZ-00001	2,500	3.0
15	400	RZ-10002	2,917	1.75
30	60	RZ-30002	2,200	4.0
30	400	RZ-40002	2,824	4.25
60	400	6002	5,101	0.5
60	60	2001	5,118	0.75
60	60	2003	5,115	1.37
100	60	4302-001	5,278	1.0
100	60	4302-002	5,200	2.0
200	60	4305-001	4,275	30.0
200	60	4305-004	3,832	25.0

Note: A 100-hour, oil-change interval was maintained while the above generator sets were run at normal, ambient temperatures.

8. **Discussion of Oil Analyses Results.** Results are discussed as follows for Phase I and Phase II and are presented graphically in Appendices A and B.

a. **Phase I.** The chemical and spectrometric analyses for Phase I are reviewed as follows:

(1) **Chemical Data.**

(a) **Viscosity.** The viscosity-at-210°F data did not exceed the established precautionary limits. The mean values obtained from the smaller sets were slightly higher than those for the 100-kilowatt set. These values can be attributed to possibly three factors: engine design, sump capacity, and oil consumption and replenishment. The individual oil test samples from each engine never approached the upper precautionary viscosity limit; therefore, any adverse factors associated with changes in viscosity (i.e., oxidation or dilution) were not evident at the 100-hour, oil-change interval.

Table 12. Oil Consumption -- Phase II, Production Models

Set Description					Mode of Operation	Accumulated Hours	Oil-Change Interval (hr)	Oil Consumption (qt)	Average Oil Consumption (qt/100 h)
Power (kW)	Frequency (Hz)	Serial Number							
15*	60	RZ10001	Norm. Amb.	700	700	36.5	Avg 29.8	4.2	
			Norm. Amb.	1400	700	31.0			
			Norm. Amb.	2089	689	22.0			
					Avg 696				
15**	60	RZ00002	Norm. Amb.	778	778	42.5	Avg 52.5	6.7	
			Norm. Amb.	1500	722	52.0			
			Norm. Amb.	2341	841	63.0			
					Avg 780				
30*	60	RZ40002	Norm. Amb.	800	800	58.5	Avg 42.6	5.8	
			Norm. Amb.	1465	665	26.7			
									Avg 732
30**	60	RZ30002	Norm. Amb.	307	307	14.0	Avg 28.1	4.9	
			Norm. Amb.	1109	802	37.5			
			Norm. Amb.	1708	599	33.0			
					Avg 569				
60	60	FZ00455	Norm. Amb.	606	600	12.0	Avg 13.9	2.2	
			Norm. Amb.	1308	702	17.5			
			Norm. Amb.	1866	558	11.5			
						600	14.4		
						652	14.0		
					Avg 622				
						352	4.0	1.0	
					3470				
					Stand-by, Low Usage				

Table 12. Oil Consumption - Phase II, Production Models (Cont'd)

Set Description						
Power (kW)	Frequency (Hz)	Serial Number	Mode of Operation	Accumulated Hours	Oil-Change Interval (hr)	Average Oil Consumption (qt/100 h)
60	400	FZ06024	Norm. Amb.	606	597	15.5
			Norm. Amb.	1258	652	12.8
			Norm. Amb.	1857	599	9.0
			Norm. Amb.	2457	600	17.7
			Norm. Amb.	3013	556	10.5
				Avg	600	Avg 13.1
						2.2
			+125°F Temp.	3315	302	19.5
						6.5
100	60	UZ00001	Norm. Amb.	1112	1000	45.5
			Norm. Amb.	2112	1000	37.2
			Norm. Amb.	3112	1000	31.5
				Avg	1000	Avg 38.1
						3.8
			+125°F Temp.	3444	332	6.5
						2.0
100	60	UZ02008	Norm. Amb.	1018	1000	61.3
			Norm. Amb.	2018	1000	48.6
			Norm. Amb.	3018	1000	27.5
				Avg	1000	Avg 45.8
						4.6
			Stand-by, Low-Usage	3340	339	8.0
						2.3

* Preproduction-model generator set with new engine installed.

** Original, preproduction-model generator.

(b) **Flashpoints.** The mean flashpoint of the oil samples was within 20°F with a standard deviation of 10°F. It is evident from the data that diesel fuel was not present in any of the oil samples and that fuel dilution of the oil would not be a factor in affecting the hydrodynamic lubricating film during the Phase I program.

(c) **Pentane Insolubles.** The mean value for the pentane insolubles for oil samples from the smaller sets was higher than the value obtained for the 100-kilowatt sets. This indicated that more fuel soot was generated in the smaller sets. The typical patterns displayed on the CalComp plot were normal values for this test. In a few isolated cases, the higher values returned to a normal-trend pattern when successive, 100-hour samples were analyzed.

(d) **Benzene Insolubles.** The mean value for the benzene insolubles for oil samples from the smaller sets was again higher than the value obtained from the 100-kilowatt sets. The mean difference of pentane versus benzene, which is an indication of oil oxidation products, would signify that a lesser formation of oil-degradation products (i.e., varnish, lacquer, resins, and sludges) would be found in the 100-kilowatt sets. The overall results of these tests indicate that the oil-change interval was five times below established precautionary limits and that oil degradation would pose no serious problem to the internal engine components.

(e) **Total Acid Number.** The mean value of TAN for the smaller sets was lower than the value for the 100-kilowatt set. Some sporadic values were recorded above the precautionary limits; however, these data points returned to normal prior to the conclusion of the test interval. The acid component buildup, i.e., sulfuric acid or weak organic acids, did not materialize to a significant degree at the 100-hour samples.

(f) **Total Base Number.** The mean value of TBN for the smaller sets as compared to that for the 100-kilowatt set demonstrates a greater alkaline reserve for the smaller engines. These data in conjunction with the TAN data indicate sufficient alkaline reserve in the smaller sets. The 100-kilowatt set reveals a decreasing TBN trend during the latter 1,000 hours of testing; no similar pattern is demonstrated by the smaller sets. The observed TBN values for the 100-kilowatt set are still within tolerable limits and are considered satisfactory at the 100-hour level of testing.

(2) **Spectrometric Data.** The spectrometric effort was directed toward seven key elements as follows: aluminum, chromium, copper, iron, lead, silicon, and tin. Since the 60- and 100-kilowatt units were of different manufactured design, the data were evaluated for those units only. The monitoring of these elements represented wear trends of major component parts in each engine. See Table 10 for a description of each component part and the element associated with its composition.

(a) **Sixty-Kilowatt Generator Set (Allis Chalmers (AC) Model 3500 Engine).** The internal engine condition was monitored through elemental analysis as follows:

Aluminum — The mean value of 14.7 ppm was five times below the established warning limit. There was an even pattern of wear from the 2,000- to 5,000-hour level. This would indicate a general wear pattern of attrition and indicate a satisfactory pattern for this engine.

Chromium — The mean value of 2.8 ppm was 25 times below the established warning limit. The two significant high values at 3,000 hours were attributed to ring seating. In general, the metallic contaminant levels were exceedingly low, and engine wear associated with this element was considered nil.

Copper — The mean value of 5.8 ppm was 10 times below the established warning limit. The high copper content at 400 hours is associated with the bushing and bearing break-in process. A stabilization pattern was established at about 500 hours into the test period.

Iron — The mean value of 15.5 ppm was eight times below the established warning limit. Iron content, however, is considered attrition rather than contamination.* The engines did not display any rapid rise after the initial break-in period at 400 hours; consequently, this mean wear pattern is indicative that oil meeting MIL-L-2104C is capable of providing satisfactory generator lubricating service.

Lead — The mean value of 15.5 ppm was eight times below the established warning limit. The element appeared to increase at the 3,000-hour level in conjunction with the two significant wear patterns of chromium. The pattern persisted to the 4,000-hour level. Since lead is associated with the overlay on the bearings, these surfaces were demonstrating component wear. However, the levels peaked at 20 ppm which is three times below the warning limit; consequently, these lead levels were considered normal.

Tin — The mean value, 7.8 ppm, was four times below the established warning limit. This metallic pattern followed a longer initial break-in period (700 hours) as compared to copper, lead, and iron and patterned itself more closely to aluminum. At 3,500 hours, the levels increased to points approaching the warning limit. This pattern could signify some excessive wear on the bearings. The pattern did not persist, and along with lead levels the spectrometric evaluation was

* Iron and copper displayed the same wear patterns.

considered normal. This element demonstrated the highest wear patterns associated with the Allis Chalmers Model 3500 engine.

Silicon — The mean value for silicon, 4 ppm, was about seven times less than the established warning limit. This element is primarily associated with dirt contamination and air cleaner efficiency. Aluminum also can signify this development; however, because its presence may be attributable to normal engine wear, aluminum is not considered a reliable indicator in this regard. These two elements in combination did not signify any apparent failure in the air-intake system, and associated indicators of wear through dirt contamination were regarded as being at a satisfactory performance level.

(b) One-Hundred-Kilowatt Generator Set (Caterpillar (CAT)) Model D-333T Engine). This engine was also subjected to elemental analysis as follows:

Aluminum — The mean value of 17 ppm was just 1 ppm below the warning limit for this engine design. From a period beyond 3,500 hours, all results were slightly above the warning limit. However, this engine has a 279-horsepower rating and a 638 inch³ displacement as compared to the AC Model 3500 engine which has a 184-horsepower rating and a 426 inch³ displacement and which has a warning limit four times above that of the Cat. engine. During the period of initial break-in, the warning limit was exceeded for the first 1,200 hours. The values when compared to those for the AC engine were about 2.3 ppm above the warning limit which is reasonable when taking into account the increased aluminum surface areas exposed in these engines. Therefore, the 17-ppm aluminum was considered a normal trend and a satisfactory level. Only by performing an engine teardown and surface evaluation of this engine design could a complete and effective lubrication performance be established to the contrary.

Chromium — The mean value of 9.3 ppm was two times below the established value. A significant wear pattern developed at 2,400 hours and peaked at 3,000 hours. This pattern also was shown in the AC engine and, although prolonged in the Cat. engine, is attributable to a piston ring break-in period. The value again decreased to 2 ppm levels throughout the remainder of the test period. This indicated a satisfactory performance and a normal wear pattern for this engine design.

Copper — The mean value of 1 ppm, a value 30 times below the warning limit, indicated satisfactory performance levels. An indication of slight bearing wear manifested itself at 4,500 hours. The level at this point is three times higher than the established trend; however, testing did not continue beyond 5,000 hours, and results are speculative. However, the level at 4,500 hours is exceedingly low when compared to an established 30-ppm warning limit.

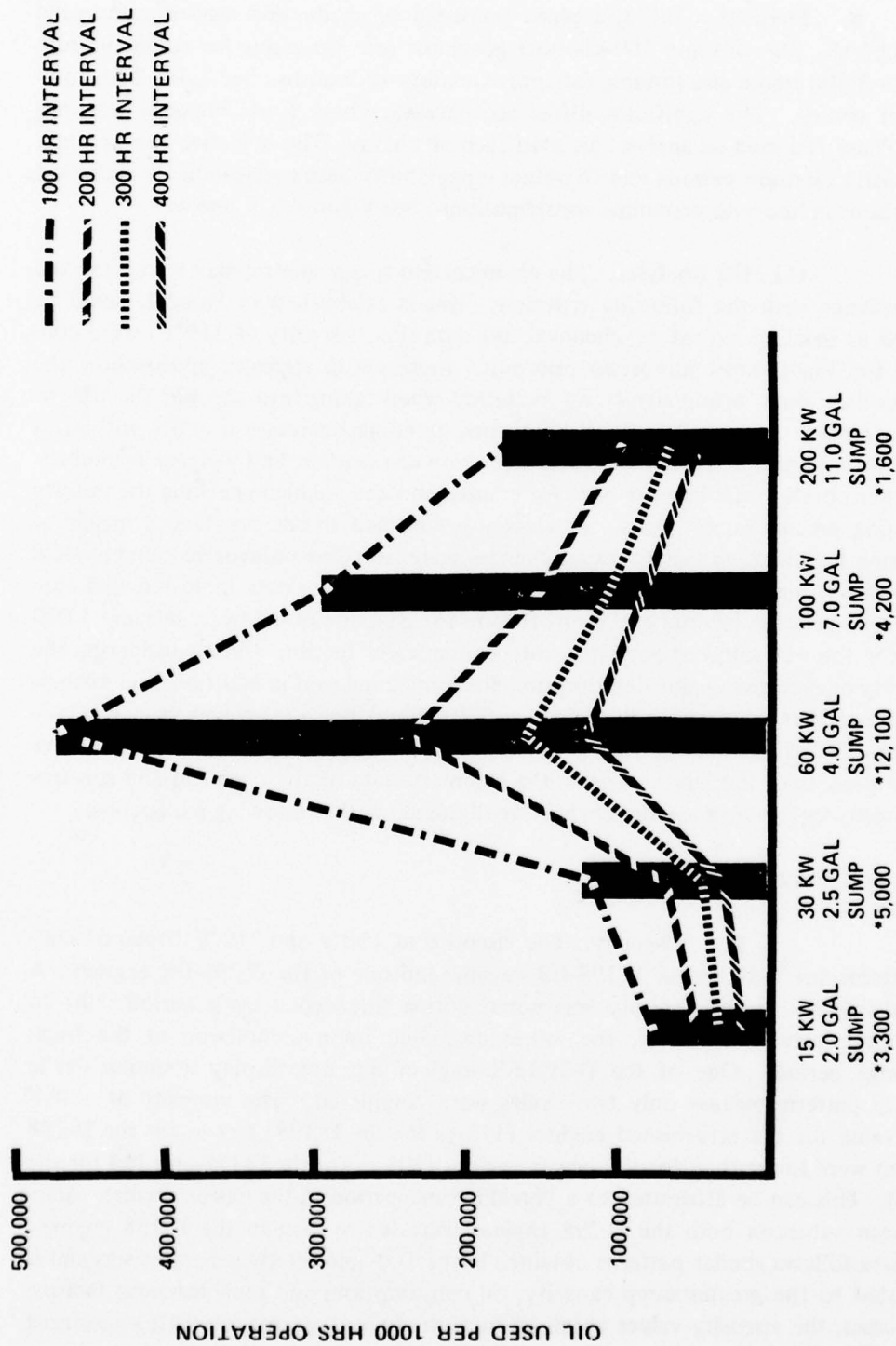
Iron — The mean value of 7 ppm was 17 times below the established warning limit. This pattern demonstrates a long-range level which is considered an attrition wear pattern. As previously discussed, iron values indicate general features; and these values are considered satisfactory.

Lead — The mean value of 6 ppm was 12 times below the established warning limit. This element increased from the 2,000-hour level and peaked at the 3,200-hour level following a similar wear pattern of chromium. This was also demonstrated in the AC engine, and a general repeatability of wear indicators can be loosely interpreted.

Tin — The mean value of 7.3 ppm was five times below the established warning limit. This metallic wear pattern had two significant peak areas: one at 2,000 hours and a second at 3,500 hours. The first wear pattern resembles the chromium and lead spectrometric analyses; however, tin indicators persisted to the 5,000-hour test interval at which time the peak levels of lead and chromium were observed and tin reverted to its baseline level. This low-level pattern was also repeated in the AC engine; however, there is no apparent explanation for these extremely low readings. In general, the values of tin were considered to be at a satisfactory wear level.

Silicon — The mean value for silicon, 3.7 ppm, was about eight times below the established warning limit. As discussed previously, it appears that no apparent problem has manifested itself because of dirt contamination. A general trend can be established which suggests that lower allowable levels of silicon are practical when the unit is operated under similar field conditions. This is important because of the direct relationship between increases in silicon and increases in iron and aluminum as overall indicators of internal component wear.

(3) **Summary of Test Data.** The Phase I wear patterns for both engines were appreciably below the established warning limits. The various used-oil analyses data accumulated on these engines demonstrated that the 100-hour, fixed-schedule drain was a conservative time interval. Monitoring these engines, test personnel found that abrupt increases in metallic elements suspended in the lubricating oil, indicative of internal component wear and possible indicators of pending engine failure, did not manifest themselves during the program. Therefore, successive 100-hour test sequences and mean wear patterns were used as indicators to the increased probability of a pending failure; the certainty of equipment degradation can be correlated only through a teardown inspection and dimensional checks in suspect wear areas.



* NOTE: Population data, Stratification Report Generator Sets Worldwide, July 1973

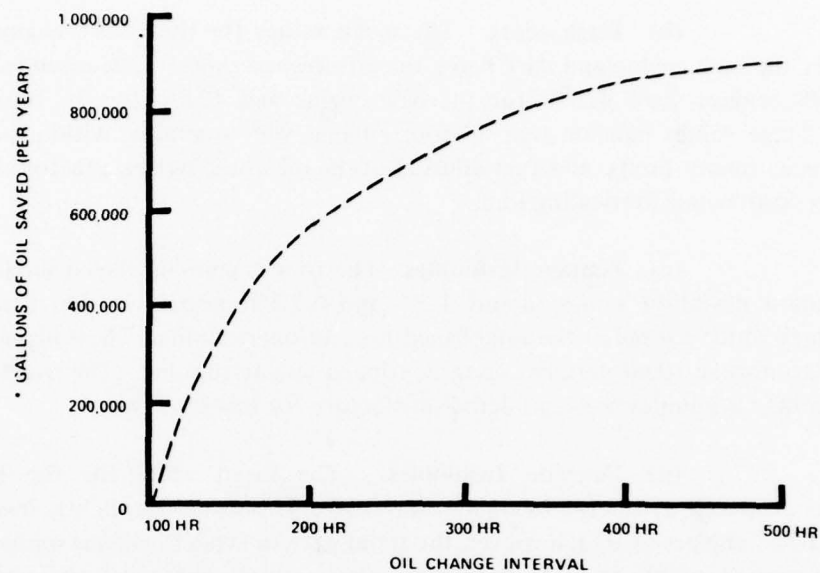
Figure 2. Oil consumption vs. oil-change interval.

b. **Phase II.** This test phase consisted of production models comprising two each, 15-, 30-, 60- and 100-kilowatt generator sets, operating for totals of from 1,600 to 3,800 hours and running for approximately 12 months. See Table 2 for total hours of testing. The significant difference between Phase I and Phase II was that during Phase II a used-oil analysis dictated each oil change. The objective was to establish realistic oil-drain periods and to obtain repeatability with cyclic data for statistical comparisons in line with economic considerations. See Figures 2, 3, and 4.

(1) **Oil Analyses.** The chemical and spectrometric data were analyzed in accordance with the following criterion: trends established in Phase I would be regarded as baseline indicators; chemical test data (i.e., viscosity at 210°F) were considered the single, most important criterion. Increases in viscosity approaching the precautionary limit would signify oil oxidation when taking into account the following test results: increases in TAN with corresponding decreases in TBN without a change in flashpoint and increased differences between pentane and benzene insolubles. This criterion also established a basis for comparison and enabled checking the validity of existing precautionary limits. Previously established trends provided a means of comparing test data; any sharp, rapid changes were noted as unfavorable, and gradual and upward slopes were considered normal. A review of the data indicated that continued set operation beyond 600 hours for the 15-, 30-, and 60-kilowatt sets and 1,000 hours for the 100-kilowatt sets was not economically feasible when considering the possibility of excessive engine deterioration and a marginal gain in additional oil savings. Since the smaller size engines in the 15- and 30-kilowatt sets (Hercules models D198-ER and D298-ER) could normally be expected to show more rapid and excessive deterioration than the larger engines, the summary data of the chemical and spectrometric analyses for these smaller engines are discussed in the following paragraphs.

(2) **Chemical Data.**

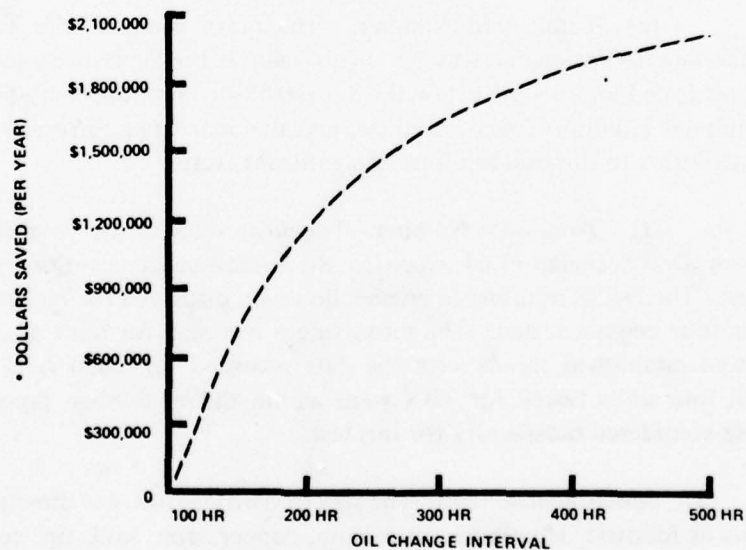
(a) **Viscosity.** The viscosity at 100°F and 210°F displayed similar patterns for both of the D-198-ER engines and one of the D-298-ER engines. A marked increase in the viscosity was noted during the second cycle period (700- to 1400-hour cycle). However, the values decreased upon completion of the final, oil-change period. One of the D-298-ER engines did not display a similar cyclic viscosity pattern because only two cycles were completed. The viscosity at 100°F mean value for the refurbished engines (175 cs for the D-198, 167 cs for the D-298 engines) were lower than for the newer engines (203 cs for the D-198 and 184 for the D-298). This can be attributed to a "breaking in" period in the newer engines. Also, the mean values in both the D-298 engines were lower than in the D-198 engines. This data follows similar patterns obtained in the 100- and 60-kW generator sets and is attributed to the greater sump capacity, oil consumption, and replenishment factors. In all cases, the viscosity values obtained from the four generator sets were considered to be satisfactory.



NOTE: Composite quantity of DOD generator sets 26,200 units based on Stratification Report, Generator Sets Worldwide July 1973

* Quantity of oil saved, based on sets being operated 1000 hr per year.

Figure 3. Composite of oil saved vs oil-change interval.



NOTE: Composite quantity of DOD generator sets 26,200 units based on Stratification Report, Generator Sets Worldwide July 1973

Price of oil based on \$80.00/55 gal. drum, and \$2.00/oil filter element.

* Dollar savings, based on sets being operated 1000 hr per year.

Figure 4. Composite of dollars saved vs oil-change interval.

(b) **Flashpoints.** The mean values for the D-198 engines were 434°F for the new engine and 414°F for the refurbished engine. The mean values for the D-298 engines were 426°F for the new engine and 421°F for the refurbished engine. These values indicate that all four engines were operating within the established precautionary limits, and fuel dilution of the oil would not be a factor in affecting the hydrodynamic lubricating film.

(c) **Pentane Insolubles.** The four engines displayed similar mean and standard deviation values (about 1.3% and 0.7% respectively), and there were some values which exceeded the established precautionary limits. These higher values returned to normal trend patterns upon continued engine running. The overall result of the pentane insolubles was considered satisfactory for this test.

(d) **Benzene Insolubles.** The mean value for the benzene insolubles produced by the D-198 engines was 0.9%. This value was slightly lower than for the D-298 engines (1.0%); however, the trend pattern established was similar to the above pentane insoluble test. In both cases, these values approached the established precautionary limit of 1%. This would indicate that the oil degradation products (i.e., varnish, lacquers, resins, and sludges) produced could be a contributing factor to engine wear if the oil-change interval exceeded 700 hours. The benzene insolubles approached the upper precautionary limit established for this test.

(e) **Total Acid Number.** The mean value of the Total Acid Number for the new D-198 engine was 2.3. This value is the highest recorded among the four engines tested and is well below the 3.5 established precautionary limit. This indicates a minimal buildup of acid products, and the associated corrosion and wear degradation attributed to this buildup is not a significant factor.

(f) **Total Base Number.** The mean value of the Total Base Number for the new D-298 engine (1.6) exceeded the established precautionary limit of 1.5 for this test. The D-298 refurbished engine, however, displayed the highest alkaline reserve of the four engines tested. The mean values recorded for both of the D-198 engines followed established trends with the data recorded for Total Acid Number. In general, all four units tested for TBN were within the established precautionary limits and were considered satisfactory for this test.

(3) **Spectrometric Data.** The spectrometric effort was directed toward seven elements as follows: aluminum, chromium, copper, iron, lead, tin, and silicon. The monitoring of these elements represented wear trends of major component parts in each engine. The D-198 and D-298 engines were designed by the same manufacturer (Hercules). The main difference between each engine was the horsepower rating (61 vs 90 hp, 4-cylinder vs 6-cylinder) and the sump size (8 vs 10 qt). These units were

evaluated on a comparison basis for each respective element as follows: obvious abnormal peaks, statistical values using mean and standard deviation, and general wear-pattern trends established for metallic element.

Aluminum. The mean values for the D-198 and the D-298 engines were $30 \text{ ppm} \pm 2 \text{ ppm}$ from each other. The wear metal content was found to be lowest at each oil-change interval; however, this pattern would normalize after a period of about 300 hours. There were no abnormal peaks or spikes, and the overall trend was similar in each of the four engines. This indicates a general wear pattern of attrition and a satisfactory performance for these engines.

Chromium. The mean value was less than 1 ppm for the D-198 and the D-298 engines. This element displays a "double spike" pattern which is attributed to ring seating. This pattern was similar to that found in the 60-kW and 100-kW engine designs. The general wear pattern for this element is within normal limits and is considered satisfactory for this engine design.

Copper. The mean value for the D-198 and the D-298 engines was about 2 ppm. The low values are displayed throughout the test period and conform to the wear patterns associated with this element. This element, like chromium, also displays a typical break-in pattern for bushings, bearings, and thrust washers. This pattern is formed at the beginning of the test period near the 700-hour mark and to a lesser degree than that displayed for chromium. After a period of 1000 hours running time, the values approach the 1- to 2-ppm range and remain there throughout the completion of the test. The overall wear pattern for this element was considered to be satisfactory.

Iron. The mean value for the new D-298 engine (60 ppm) was the highest value in this series. The two D-298 engines displayed increased concentrations of iron when compared to the two D-198 engines tested. Also, the refurbished engines were significantly lower (15 ppm) than their new counterparts. Iron is considered an overall, general wear index indicator in these designs, and these patterns display a gradual elemental increase prior to each oil-change period. Such trends are of a typical engine performance cycle and do not indicate any abnormalities resulting from wear or breakdown. It is further indicative that the oil (MIL-L-2104C) is capable of providing satisfactory engine lubrication.

Lead. The mean value for both the D-198 and the D-298 engines was established at $31 \text{ ppm} \pm 2 \text{ ppm}$. The D-298 engine displayed two significant peaks which were attributed to wear patterns. Upon continued running, however, these values experienced marked decreases and approached the typical patterns associated with this element. Since lead is associated with bearings surfaces, some abnormal

wear may have occurred at various points in the cycle; but these periods are not definite and cannot be explained as was the chromium pattern. In general, the lead values are low (20 ppm) at the initial periods and cycle (60 ppm) prior to oil-change periods. The values for this element are considered normal. Actual wear abnormalities can only be ascertained by teardown and surface examination of pertinent parts.

Tin. The mean value for the D-198 and the D-298 engines was 33 ± 1 ppm. This value is the most consistent of the seven elements tested and is also present in the second highest concentration (iron being first) for this design. In general, this element follows a pattern which is similar to the established lead pattern; but unlike lead it does not display abnormal peaks. The presence of this element is lowest at the oil-change period, increases within the next 200-hour interval, and subsequently stabilizes at the 40 ppm vicinity until the next cycle period. The tin patterns displayed by this engine design are considered to be at a satisfactory performance level.

Silicon. The mean value of 12 ppm for the new D-298 engine was the highest recorded value for this series. Also, the high silicon established by this engine coincided with the highest values in iron and, to a lesser degree, copper, chromium, and tin. This element characterizes engine air filtration efficiency, and these high values denote external particulate contamination of the system and may account for some increased wear. The initial silicon values are in excess of 40 ppm but decrease to near normal values by 1000 hours running time. After the 1000-hour period, the silicon stabilized to about 10 ppm which is considered a satisfactory level for this engine design. The two D-198 engines and the one D-298 refurbished engine displayed similar patterns to the new D-298 engine but at consistently lower levels throughout the test period. The mean value for these three test engines was 4 ppm, and the engines were also considered to be performing at a satisfactory level.

(4) Extreme-Temperature Testing. High-temperature tests (125°F) were conducted on two generator sets, i.e., the 60 kW, #06024 (AC Model 3500 engine), and the 100-kW #UZ00001 (Cat. Model D333T engine) for one cycle period of 300 hours to determine any deleterious effects of elevated, ambient temperatures on lubrication performance, wear-pattern levels, and engine operation in general.

(a) Chemical Oil Analysis. The AC Model 3500 engine demonstrated a marked increase in the viscosity level at 100°F (250 cs) and 210°F (20 cs) as compared to the ambient operating test temperatures. The Cat. Model D333T engine operated at a level of performance equal to the ambient range. This level reached a viscosity plateau of 190 cs at 100°F; however, data for 210°F were inconsistent. The range varied from 13 to 17 cs but in general did not exceed the established upper precautionary limit for this test. The flash points for both engines were at the

same level recorded for new oil (440°F) with no apparent oil dilution in the system. The pentane and benzene insolubles for the AC Model 3500 engine were below the established precautionary limits. The general trend showed a slightly increasing slope prior to an oil-change period which is a normal pattern for this engine. The Cat. Model D333T engine demonstrated the same general trend and relationship with the exception of one abnormal peak at the 150-hour interval. This value immediately returned to the trend pattern in the next analysis period. It is considered an unexplained abnormality which could have developed through faulty analytical or sampling procedures. The total acid and total base levels for the AC Model 3500 engine were within the established precautionary limits. The general trend in pattern development demonstrated satisfactory performance levels for these tests. The Cat. Model D333T engine demonstrated moderate increases during the high-temperature test period when compared to the ambient range; however, it did not exceed the precautionary levels. The total base showed a normal decreasing slope which did exceed the precautionary limit after 125 hours of testing. At the conclusion of the test period, the alkaline reserve level reached 0.5 TBN which is a similar pattern developed under the ambient test program.

(b) Spectrometric Analysis. The AC Model 3500 engine displayed similar patterns for aluminum, chromium, copper, and silicon. The iron pattern in general was lower in value but displayed the same slope characteristics. The value for lead (50 ppm) peaked at the 100-hour period but remained below the established warning limit. The values for tin (40 ppm) exceeded the established limits; this element was the only pattern which increased in the high-temperature test. Continued testing after the high-temperature test period displayed a similar wear pattern in excess of the 30 ppm warning limit. The overall wear pattern (from initial to end of cycle) in the high-temperature test was doubled in comparison to the following 300-hour cycle. The tin wear was considered the most severe in the AC Model 3500 engine. The Cat. Model D333T engine displayed similar patterns for chromium and copper. The iron pattern followed the same general-trend relationship shown in the ambient cycles with about ½ the wear metal content. The aluminum pattern indicated an upward slope, and the values exceeded the warning limits by 50 ppm. The wear-metal levels, after the high-temperature cycle, returned to the warning limit; however, the cycle prior to the high-temperature cycle exceeded all values in wear-metal content. The lead and tin analyses had similar wear patterns with the peak being reached at 150 hours into the high-temperature test cycle. Both values (lead and tin) demonstrated the same concentration levels, 40 ppm at the peak, and then decreased to 25 ppm at the end of the test cycle. These patterns did not follow any general trend established by the previous ambient test cycles.

(5) **Stand-by Low-Usage Duty Cycle.** These tests were conducted on two other generator sets; i.e., the 60 kW, #F200455 (AC Model 3500 engine); and the 100 kW, #UZ02008 (Cat. Model D333T engine) for one cycle period of 300 hours at ambient temperature.

(a) **Chemical Oil Analysis.** Both of the engines displayed normal viscosity patterns with the exception of an isolated peak value exceeding the established precautionary limit. The flash points for both engines were at 425°F. These values were slightly lower than the standard, duty-cycle pattern, 440°F, but with no apparent oil dilution in this cycle. The pentane and benzene insolubles for the AC Model 3500 engine were the lowest recorded value for the entire 3600-hour test period. The Cat. Model D333T engine displayed similar patterns with the exception of the initial value. This is considered insignificant when the total cycle is evaluated. The total acid and the total base values for the AC Model 3500 engine displayed a slight improvement in the overall pattern. The Cat. Model D333T engine also demonstrated an improvement in the total acid performance and a significant increase in total base number performance. In the previous cycle, the data had indicated that the oil exceeded the established precautionary limit of 1.5; however, in the low duty cycle, the values for total base were below the precautionary limit.

(b) **Spectrometric Analysis.** The AC Model 3500 engine displayed similar wear patterns for aluminum, chromium, and copper. The iron pattern was lower in wear-metal content but had the same general slope characteristics. The lead content displayed one abnormal peak at the mid-cycle point but returned to near-normal levels at the conclusion of the cycle period. The tin analysis indicated a generally higher wear pattern than the standard duty cycle. This increase exceeded the established warning limit by 10 ppm throughout most of the test cycle but decreased during the last 50 hours of the cycle period to 20 ppm — a value below the warning limit. The silicon content (3 ppm) was lower in this cycle period but did not display any similar slope patterns to the previous standard cycle. The Cat. D333T engine displayed a similar pattern for chromium. The iron pattern was lower in wear-metal content but had the same general slope characteristics. The aluminum varied from previous patterns. It was lower in wear-metal content than the previous cycles, but it also exceeded the warning limits. The copper analysis was lowest in this cycle period with values three times lower than the established warning limit. The lead content displayed two major peaks at mid-cycle point, but these values returned to normal at the conclusion of the cycle period. The tin analysis indicated moderate increases in the wear-metal content. In one case, the value exceeded the warning limit but returned to the mean value at the end of the cycle period. The silicon content increased to 8 ppm at mid cycle; then, it decreased to a level of 2 ppm until the conclusion of the test period. This level was the lowest recorded for this element.

9. Oil-Change Intervals. Based on the results of the chemical and spectrometric analyses of oil samples and engine inspections under Phase II as described herein, the following repeatable, oil-change intervals were established:

- a. 15 kW (Hercules Model D198 engine) – 700 hours.
- b. 30 kW (Hercules Model D298 engine) – 700 hours.
- c. 60 kW (Allis Chalmers Model 3500 engine) – 600 hours.
- d. 100 kW (Caterpillar Model D333T engine) – 1000 hours.

10. Engine Teardown Inspections.

a. Units Inspected. Inspections were conducted on the following units at the General Environments Corporation facility, Hartwood, Virginia:

<u>Unit</u>	<u>S/N</u>	<u>Engine</u>	<u>Time (Hr)</u>	<u>Oil Change (Hr)</u>
60 kW	FZ2001	AC-3500	5118	100
60 kW	FZ6024	AC-3500	3700	600
100 kW	VZ00001	Cat. D333T	3878	1000
100 kW	VZ02008	Cat. D333T	3340	1000

b. Wear Ratings. The inspection wear ratings were made in accordance with CRC Rating Manual No. 5 and included the following:

- Pistons
- Liners
- Rings
- Rockers, Shaft, and Tappets
- Valves
- Main and Connecting-Rod Bearings
- Camshaft and Crankshaft
- Head, Oil Pans, Oil Pump, Timing Gears

c. Inspection Data. The inspection data, including photographs, are too voluminous to be included in this report; therefore, they will be part of the project record file.

d. Summary. In regard to oil performance, all engines had been adequately lubricated under the service conditions by which they were operated. It is possible only to draw general comparisons relative to lubricant performance under standard or extended-oil-drain intervals because of the effects of lubricant quality and differences in engine operations.

(1) **Allis Chalmers Model 3500 Engines.** Only one major problem was observed during the inspection. Both engines showed distress (abrasive wear/galling) between the rocker arms and the rocker shaft and fretting corrosion between the rocker shaft and shaft support mounts. Continued wear in this area could cause engine malfunction. In addition, the connecting-rod bearings appeared to have somewhat higher wear with one bearing from generator FZ06024 showing severe fatigue and metal removal. Although this wear was noted, ratings were visual; and it did not appear that the wear had reached a point of critical concern. Since the two units operated on different oil-drain intervals, the following comments are made relative to lubricant performance. From a deposit standpoint, the engine using the extended-drain intervals exhibited lower piston deposits and less port restriction than the engine operated under the standard, 100-hour-change period. The reverse was true in the area of valve operation and stem deposits. Here, the engine using the extended-drain interval exhibited sluggish valves which was likely the result of the carbon and lacquer noted on the valve stem in the guide travel area. This condition was not observed in the engine operated on standard drains where the valves were free and the stems clean in the guide area. With the exception of the above, lubricant performance was essentially equal under both the extended and standard oil-drain conditions.

(2) **Caterpillar, Model D333T Engines.** Both engines showed severe pitting of the cylinder liners on the coolant side. In addition, wear in the rocker-camshaft area was noted for the engine from unit UZ00001. Continued deterioration of these conditions would result in engine malfunctions/failures.

Although the major portions of the engines were in satisfactory condition, the excessive wear in the rocker-camshaft areas and the severe liner pitting (coolant side) are of critical concern. It should be noted that wear ratings are visual, and no numerical values are available to determine the true extent of the damage. For example, rocker shaft wear could be felt by touch on the front portions of the shaft but becomes only visible moving toward the rear portion. It is not possible to determine if the wear were lubricant related, a lubricant-mechanical problem, or strictly from a mechanical source. No matter what the source, the wear will eventually result in an engine malfunction. Likewise, the liner pitting could result in an engine failure. The most severe pitting (estimated 1/8 to 1/4 depth) occurred in the lower section of all liners. Again, the cause of pitting could not be determined directly.

With the exception of the severe liner pitting (coolant side), the engine was in satisfactory condition and had been adequately lubricated. Also, it should be noted that coolant had leaked into the crankcase. The source and time of this leakage could not be determined; therefore, it was not possible to evaluate the overall effect of the leak on the observations made during the inspection.

IV. CONCLUSIONS

11. **Conclusions.** Based on the work reported herein, it is concluded that:

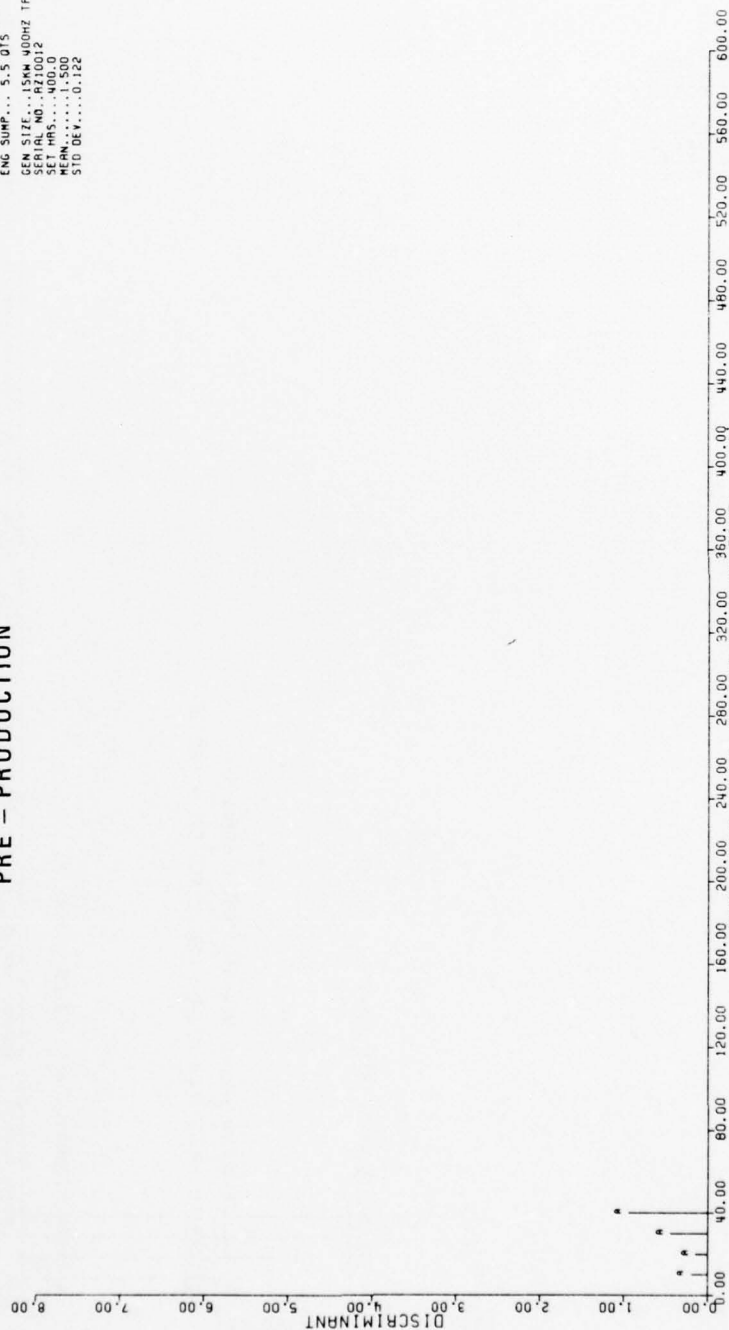
- a. The initial precautionary limits established in the Phase I testing were conservative except for a few isolated instances during which some engines operated beyond these limits.
- b. There were no engine failures or signs of pending trouble areas attributable to the lubricating oil under Phase I testing.
- c. The chemical and spectrometric analyses under Phase I indicated that the oil was performing in a satisfactory manner and that the standard, 100-hour, oil-change interval was conservative and could be safely extended.
- d. Under Phase II testing, there were no engine failures or any deleterious effects directly attributable to the extended-oil-change intervals established, i.e., 600, 700, and 1000 hours for the engines being tested.
- e. The test results indicate that generator sets ranging in size from 15 kW through 100 kW using MIL-L-2104C lubricating oil and operating under normal, ambient conditions or extreme temperatures up to 125°F or under stand-by, low-duty service could operate satisfactorily with a 300-hour/6-month oil-change interval without engine performance, reliability, or total life cycle being adversely affected.
- f. A 300-hour/6-month oil-change interval offers the maximum benefit and cost-saving compromise to the military while maintaining a minimum 100 percent safety factor with respect to risks of engine malfunctions or failures attributable to extended, lubricating-oil-change intervals.

APPENDIX A

PHASE I PRE-PRODUCTION MODELS

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE NO. 8 H.P.
ENG MAKE...HERC D-198ER
ENG SUMP...5.5 QTS
GEN SIZE...15MM 400HZ TP
SERIAL NO. A710012
SET HRS...400.0
MEAN...1.500
STD DEV...0.122

TOTAL ACID .VS. TOTAL BASE PRE - PRODUCTION



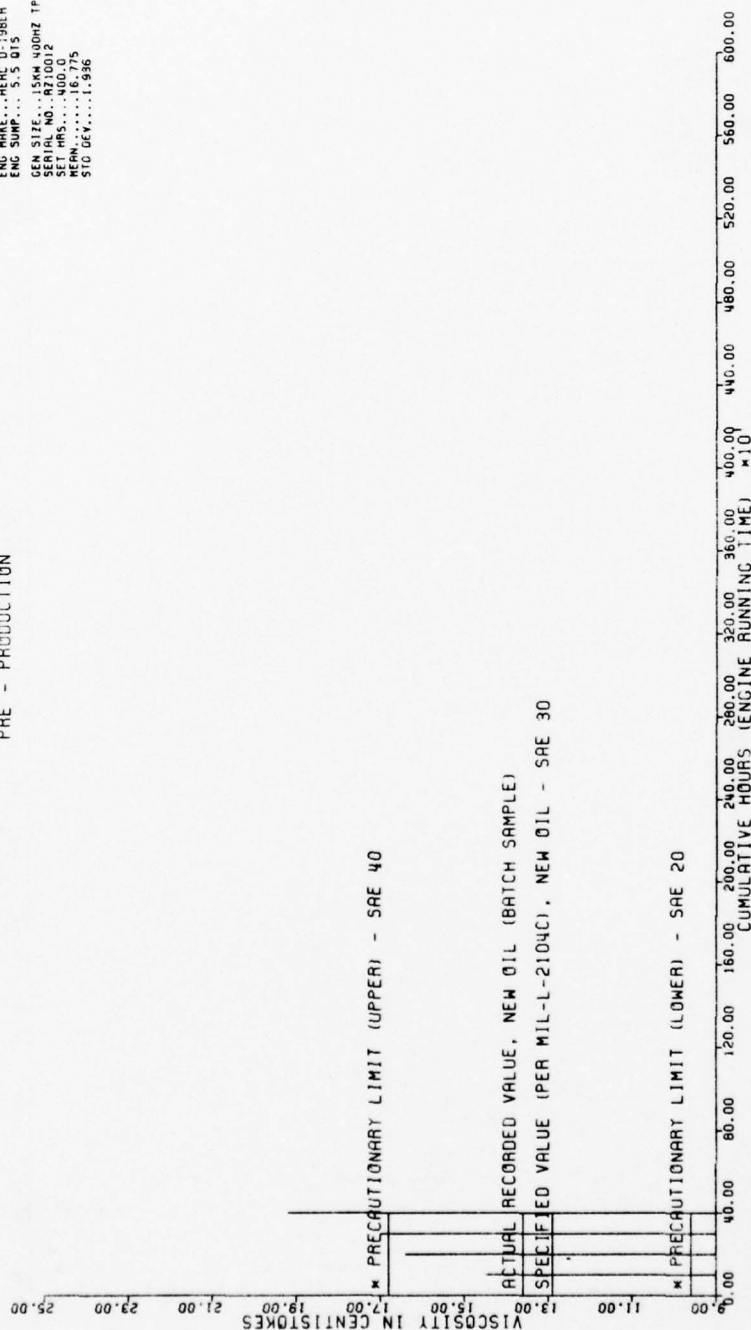
A SPECIFIES THAT THE TOTAL ACID READING IS GREATER THAN THE TOTAL BASE READING
B SPECIFIES THAT THE TOTAL BASE READING IS GREATER THAN THE TOTAL ACID READING

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREE

INCLUSIVE DATES
 22 JUN 76 13 JULY 76
 ENG SIZE... 1500 B.H.P.
 ENG MAKE... MERC D-198ER
 ENG SUMP... 5.5 QTS
 GEN SIZE... 1500 4000HZ 1P
 SERIAL NO... A710012
 SET HAS... 400.0
 MEAN... 16.775
 STD DEV... 1.956

VISCOSITY OF USED OIL AT 210 F

PRE - PRODUCTION

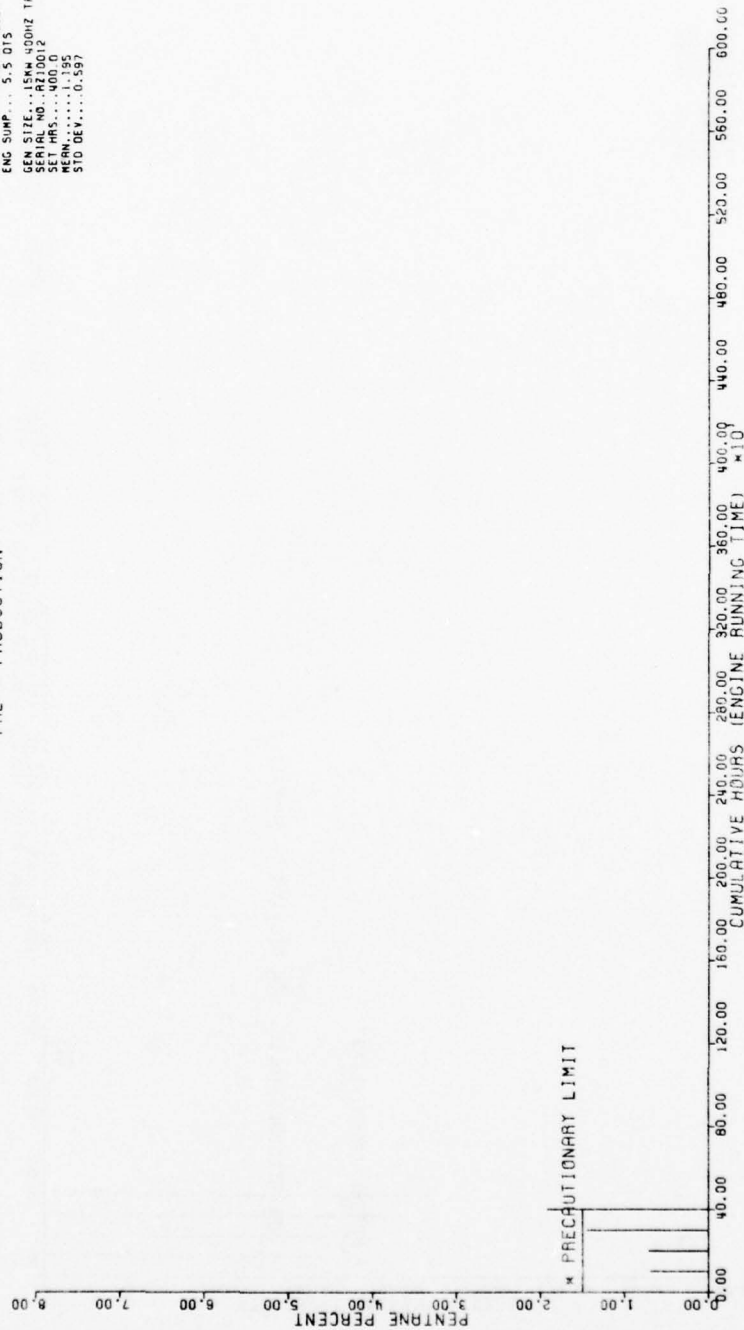


*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210F
 EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION
 LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MINIMUM FUEL
 DILUTION LIMIT).
 *REPRESENTS THE END OF 1 CYCLE. C REPRESENTS AN OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

PERCENTAGE INSOLUBLES (PENTANE) PRE - PRODUCTION

INCLUSIVE DATES
22 JUN 76 13 JUL 76
ENG SIZE... NO. 8 M.P.
ENG NAME... HMC 0-1968
ENG SNR... 3-5 Q13
GEN SIZE... 15MM 400HZ TP
SERIAL NO... 40012
SET HRS... 400.0
MEAN... 1.195
STD DEV... 0.597



* NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF PENTANE INSOLUBLES REACHES 1.50 PERCENT.

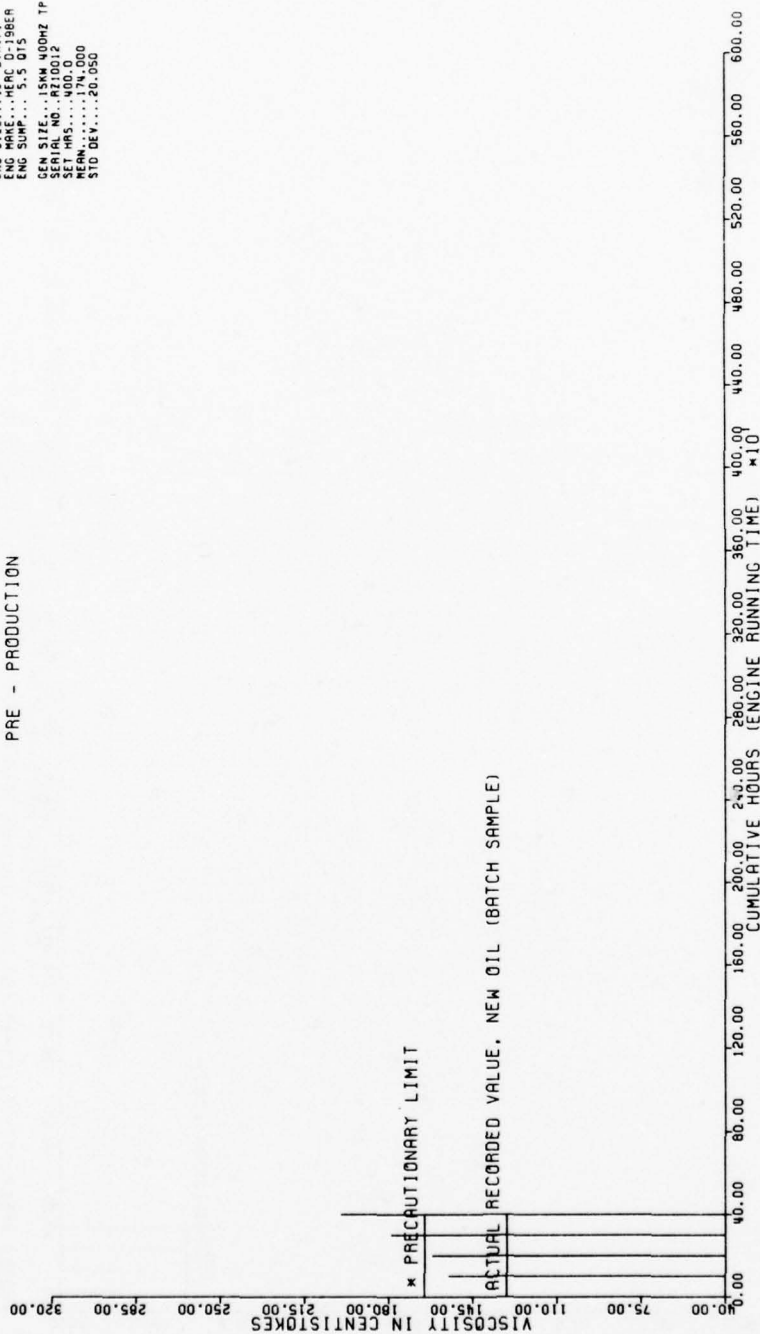
100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

VISCOSITY OF USED OIL AT 100 F

PRE - PRODUCTION

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE...NO. 8 M.P.
ENG SERIAL NO. 1000000000
ENG SUMP...5.5 QTS
CEN SITE...15KM 400HZ TP
SERIAL NO. A210012
SET HRS...400.0
MEAN...174.000
STD DEV...20.050



* NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 100F INCREASES 25 PER CENT FROM VISCOSITY VALUE RECORDED FOR NEW OIL (BATCH SAMPLE).

X REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE...40 B.H.P.
ENG MAKE...MERC D-198ER
ENG SUMP...5.5 QTS
GEN SIZE...15MM 400HZ TP
SERIAL NO. A210012
SERVARS...4000
WEAR...0.000
STD DEV...0.491

PERCENTAGE INSOLUBLES (BENZENE) PRE - PRODUCTION



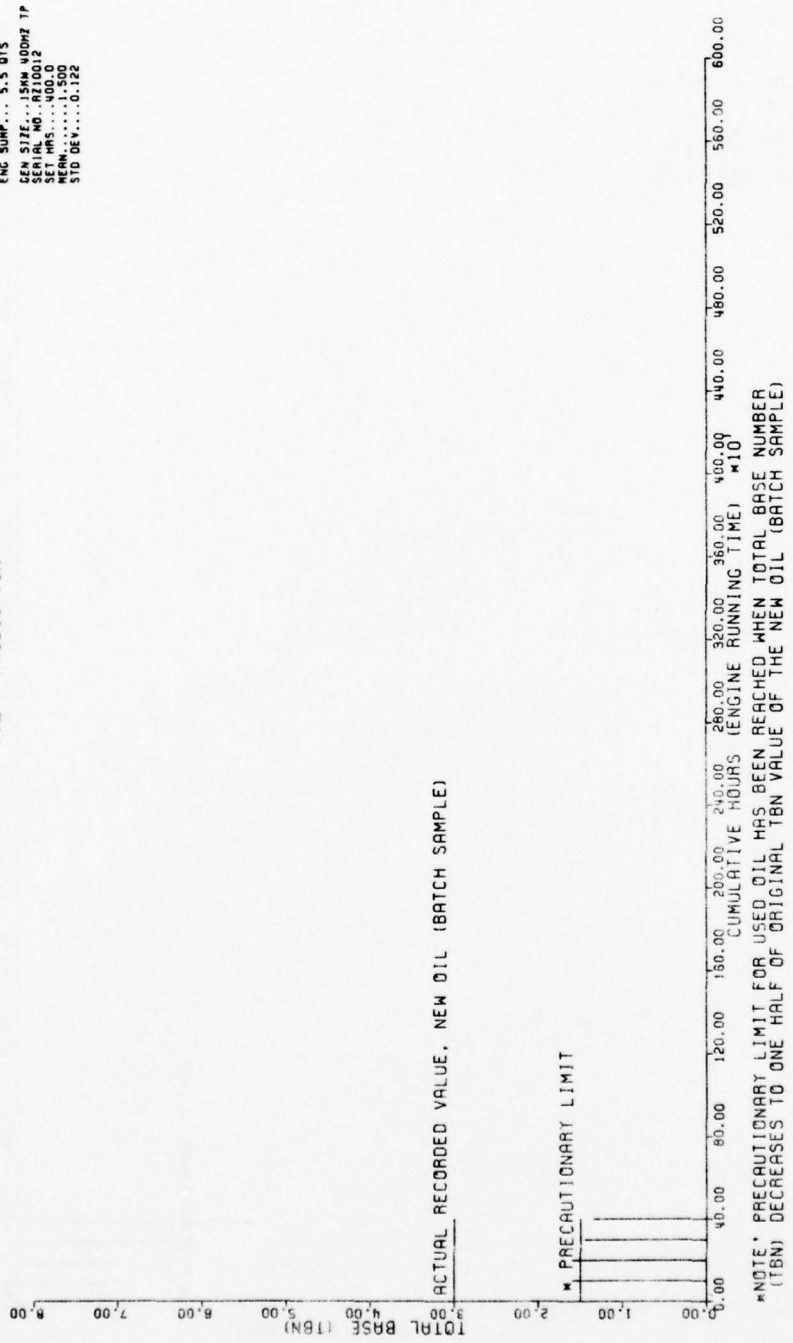
*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF BENZENE INSOLUBLES REACHES 1.00 PER CENT.

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

■ REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE... 1500 B.H.P.
ENG MAKE... MRC D-188R
ENG SUMP... 5.5 QTS
GEN SIZE... 1500 WODH 7P
SERIAL NO... A210012
SET MRS... 400.0
MEAN... 1.500
STD DEV... 0.122

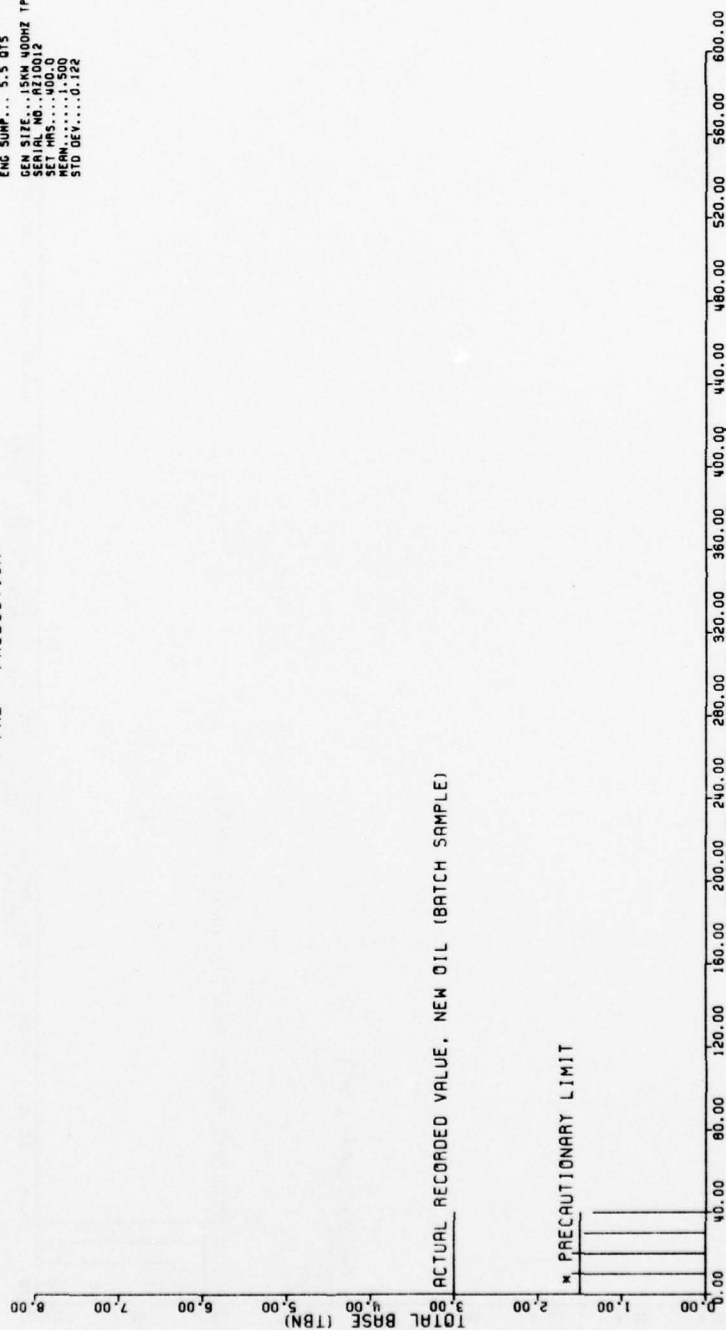
TOTAL BASE IN USED OIL PRE - PRODUCTION



X REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE
100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE...400 B.M.P.
ENG WIND...1000
ENG WIND...5.5 QTS
GEN SLIP...1500 4000Z 1P
SET HRS...070012
MEAN...1.500
STD DEV...0.122

TOTAL BASE IN USED OIL PRE - PRODUCTION



NOTE PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL BASE NUMBER (TBN) DECREASES TO ONE HALF OF ORIGINAL TBN VALUE OF THE NEW OIL (BATCH SAMPLE)

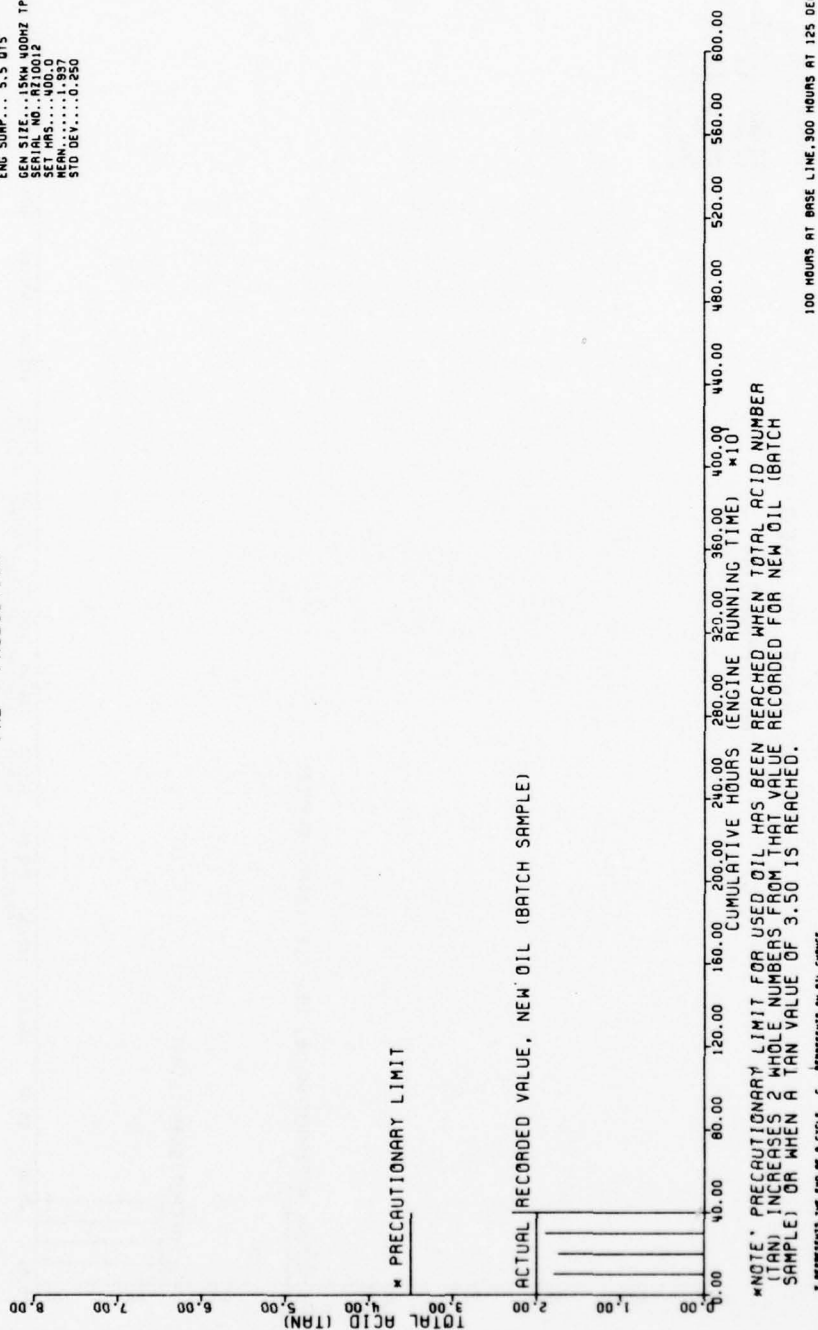
Z REPRESENTS THE END OF A CYCLE C REPRESENTS NEW OIL CHANGE

100 HOURS AT BASE LINE 300 HOURS AT 125 DEGREE

INCLUSIVE DATES
 22 JUN 76 15 JULY 76
 ENG SIZE...40 B.H.P.
 ENG MAKE...MERC D-198A
 ENG SUMP... 5.5 QTS
 GEN SIZE...15KW 400HZ TP
 SERIAL NO...A10012
 TEST NO...1052
 YEAR...1987
 STD DEV...0.250

TOTAL ACID IN USED OIL

PRE - PRODUCTION



NOTE PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

X REPRESENTS THE END OF A CYCLE C REPRESENTS THE OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
 22 JUN 76 13 JULY 76
 ENG SIZE... NC B H P
 ENG NAME... MERC D-108ER
 ENG SUMP... 5.5 Q15
 GEN SIZE... 15MM 400HZ TP
 SERIAL NO... RZ10012
 SET MRS... 400.0
 MEAN... 1.500
 STD DEV... 0.122

PENTANE .VS. BENZENE PRE - PRODUCTION



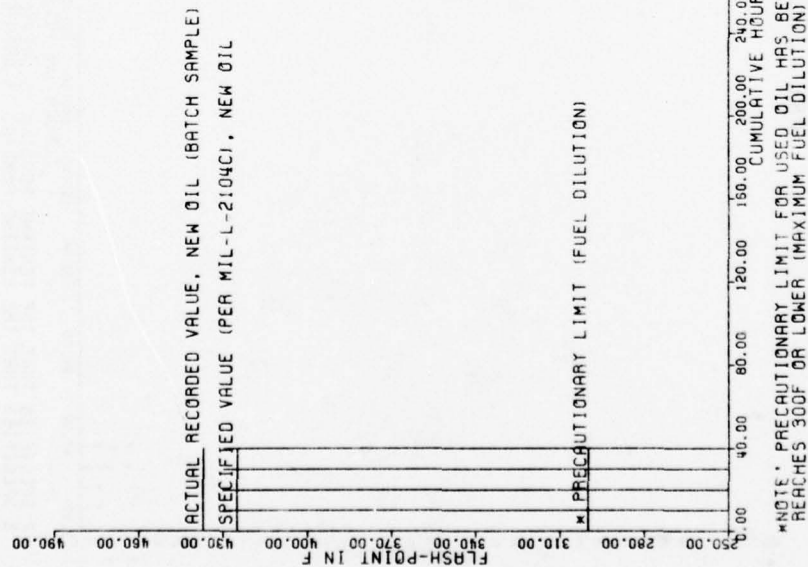
P SPECIFIES THAT THE PENTANE READING IS GREATER THAN THE BENZENE READING
 B SPECIFIES THAT THE BENZENE READING IS GREATER THAN THE PENTANE READING

100 HOURS AT BASE LINE. 300 HOURS AT 125 DEGREES

FLASH-POINT OF USED OIL (F)

PRE - PRODUCTION

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE...40 B.M.
ENG SUPP...5.5 DTS
SERIAL NO...1584-1000Z TP
SET MRS...400.0
MEAN...430.000
STD DEV...0.000



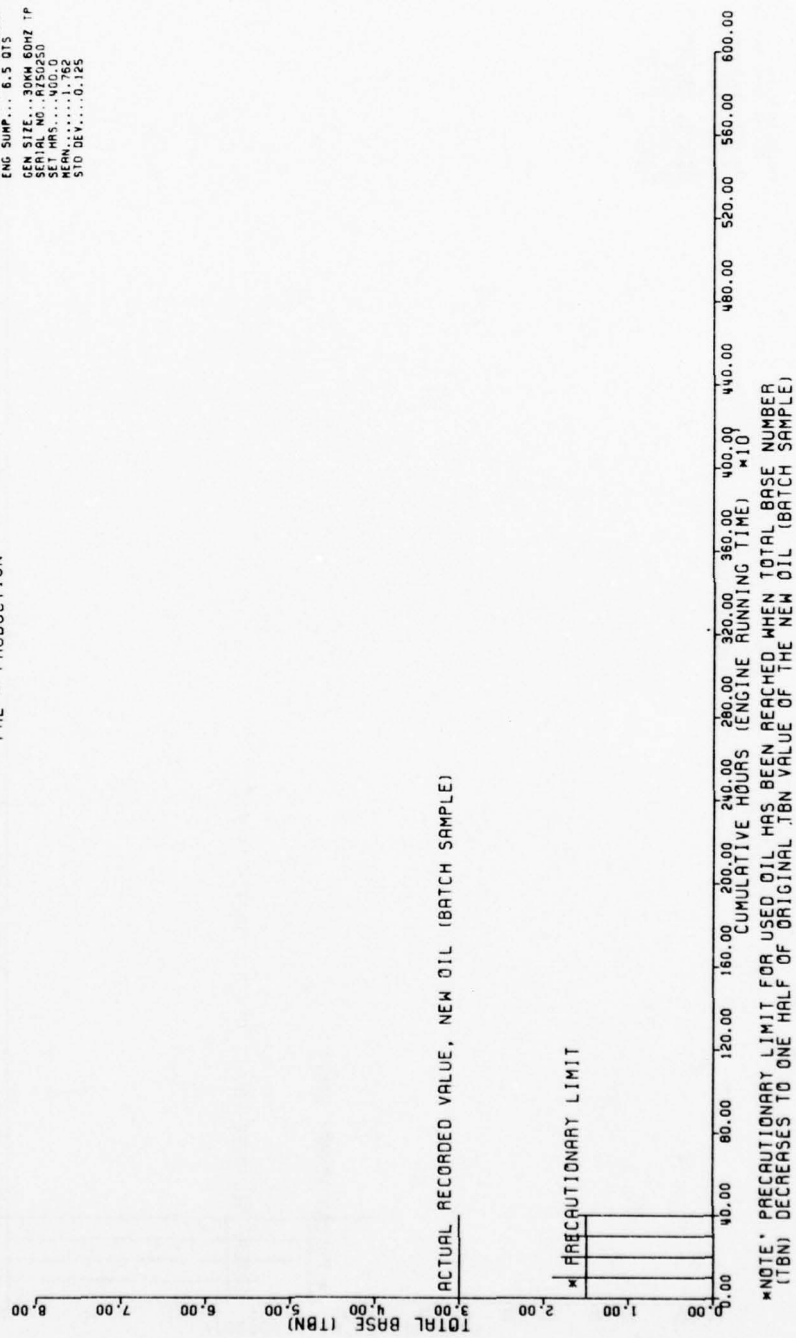
X REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREE

INCLUSIVE DATES
22 JUN 76 13 JUL 76
ENG SIZE... 50 B H P
ENG MAKE... PERC
ENG SUMP... 6.5 QTS
CEN SIZE... 30XW 50HZ 1P
SERIAL NO... A750250
SET HRS... 400.0
MEAN... 1.762
STD DEV... 0.125

TOTAL BASE IN USED OIL

PRE - PRODUCTION

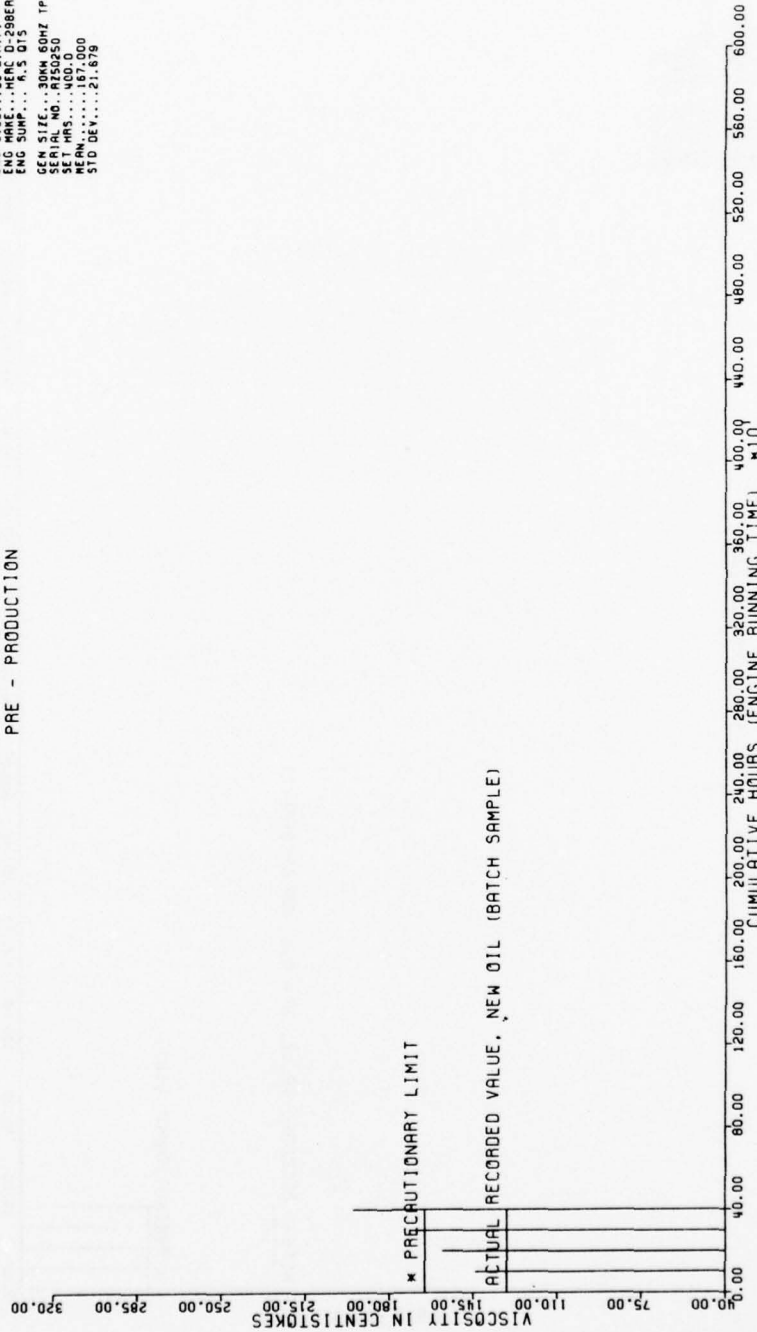


100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

Z REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
22 JUN 76 13 JULY 76
ENG SIZE... 50 P. P.
ENG MAKE... D-208ER
ENG SUMP... 6.5 QTS
GEN SIZE... 30W 50HZ 1P
SERIAL NO... R750250
SET HRS... 400.0
MEAN... 187.000
STD DEV... 21.879

VISCOSITY OF USED OIL AT 100 F PRE - PRODUCTION



* NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 100F INCREASES 25 PER CENT FROM VISCOSITY VALUE RECORDED FOR NEW OIL (BATCH SAMPLE).

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

Z REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
22 JUN 78 13 JUL 78
ENG SIZE...60 B.H.P.
ENG MAKE...HERC D-298ER
ENG SUMP...6.5 QTS
GEN SIZE...30KW 60HZ TP
SERIAL NO...R250250
SET MRS...400.0
STD DEV...1.128

PERCENTAGE INSOLUBLES (PENTANE) PRE - PRODUCTION



*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF PENTANE INSOLUBLES REACHES 1.50 PERCENT.

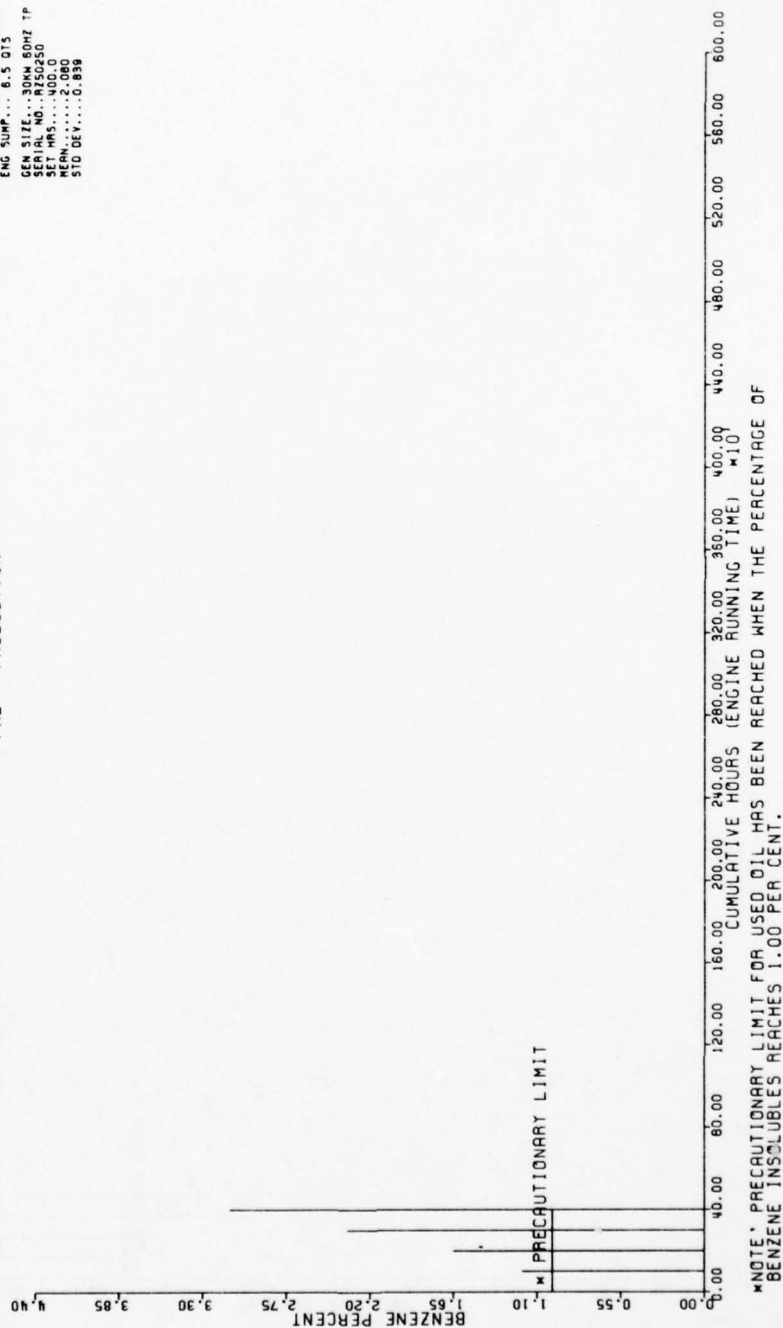
Z REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE 100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

PRE - PRODUCTION

INCLUSIVE DATES
22 JUN 78 13 JULY 78

ENG SIZE... 60 B.M.P.
ENG MAKE... HEC D-290EA
ENG SUMP... 6.5 Q15

GEN SIZE... 30KW 60HZ TP
SERIAL NO. A750250
SET HAS... 400.0
MEAN... 2.080
STD DEV... 0.839

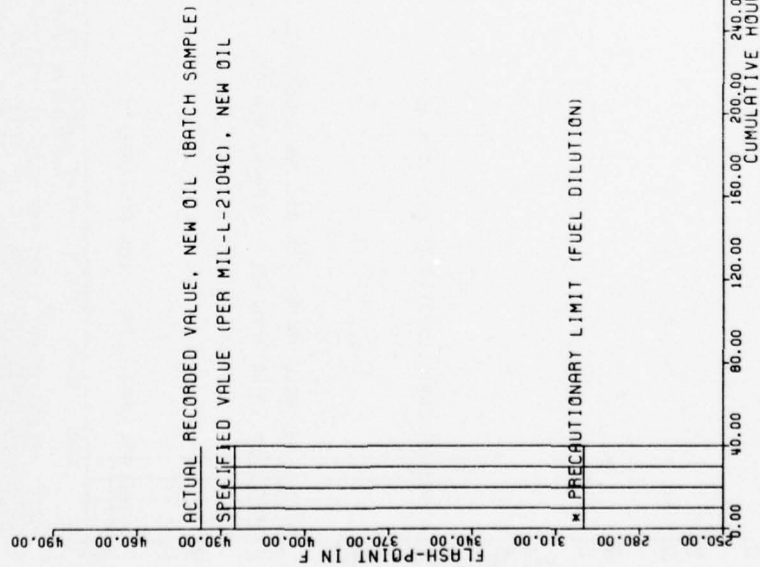


P REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CRUISE

INCLUSIVE DATES
 22 JUN 78 13 JUL 78
 ENG SIZE...60 B.H.P.
 ENG MAKE...MERC D-288EA
 ENG SUMP... 6.5 DTS
 GEN SIZE...30KW 50HZ 1P
 SERIAL NO...R750250
 SET HPS...400.0
 RPM...1500.0
 STD DEV...0.000

FLASH-POINT OF USED OIL (F)

PRE - PRODUCTION



*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

T REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE 100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

VISCOSITY OF USED OIL AT 210 F

PRE - PRODUCTION

INCLUSIVE DATES
28 JUN 76 13 JULY 76
ENG SIZE...60 B. H. P. 5.0
ENG SPEED...1800 RPM
ENG SUMP...16.5 OLS
SEN SIZE...30MM 60HZ TP
SERIAL NO...R502630
SET HRS...400.0
MEAN...16.200
STD DEV...2.093

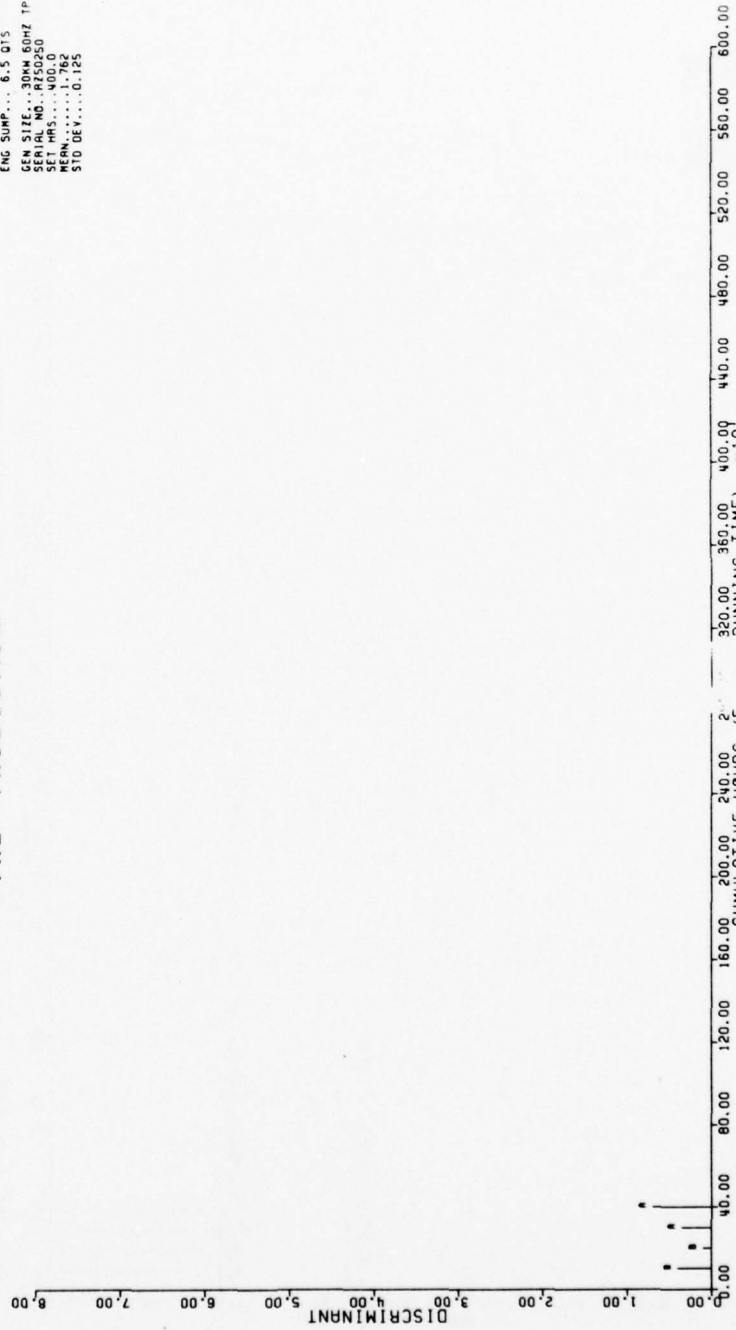


* PRECAUTIONARY LIMIT (UPPER) - SAE 40
* PRECAUTIONARY LIMIT (LOWER) - SAE 20
* NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).
* REPRESENTS THE END OF A CYCLE. C REPRESENTS AN OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
22 JUN 76 13 JUL 76
ENG SIZE...50 B.H.P.
ENG MAKE...MERC D-298ER
ENG SUMP...6.5 DTS
GEN SIZE...30MM 60HZ TP
SERIAL NO...R250250
SET RMS...400.0
SERIAL...125
STD DEV...0.125

TOTAL ACID .VS. TOTAL BASE PRE - PRODUCTION

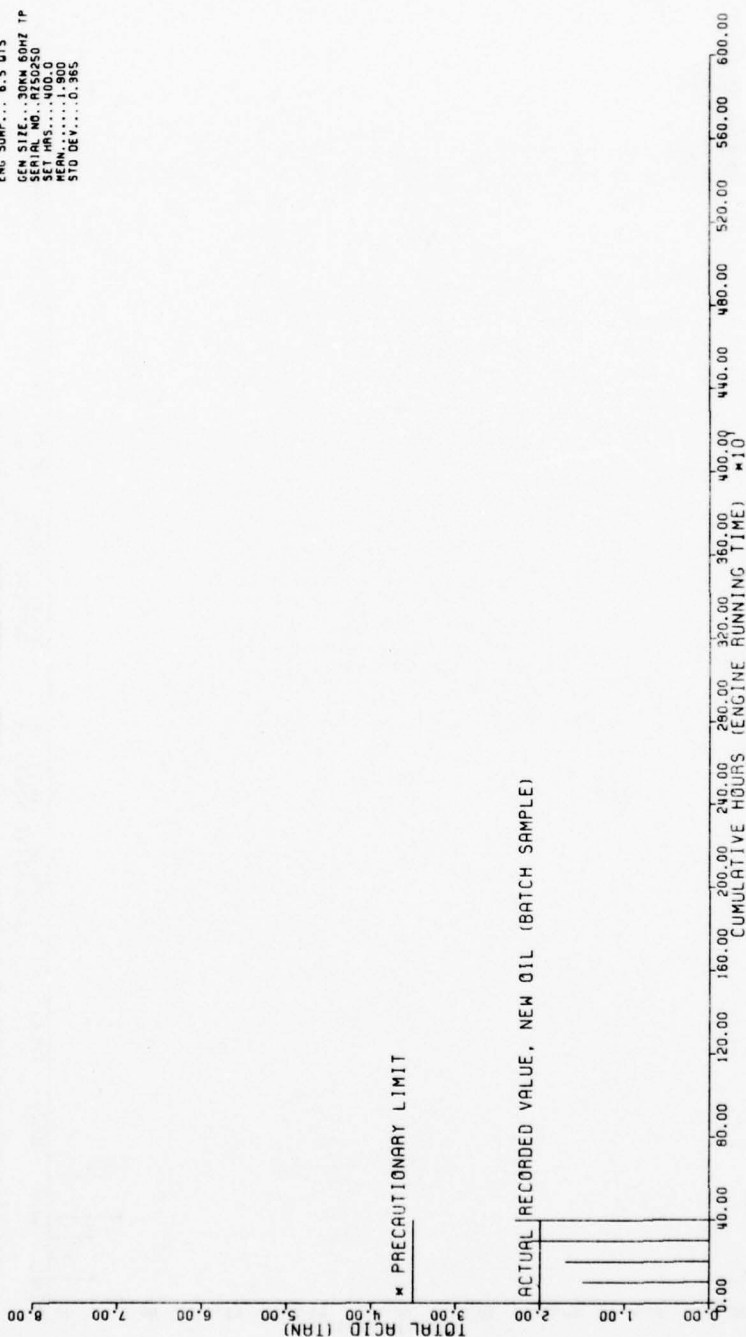


A SPECIES THAT THE TOTAL ACID READING IS GREATER THAN THE TOTAL BASE READING
B SPECIES THAT THE TOTAL BASE READING IS GREATER THAN THE TOTAL ACID READING

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
22 JUN 78 13 JULY 78
ENG SIZE...60 B H-P-808R
ENG MAN...1000000000
ENG SUPP...1000000000
ENG SIZE...3000 60HZ TP
SET HRS...400.0
MEAN...1.800
STD DEV...0.365

TOTAL ACID IN USED OIL PRE - PRODUCTION



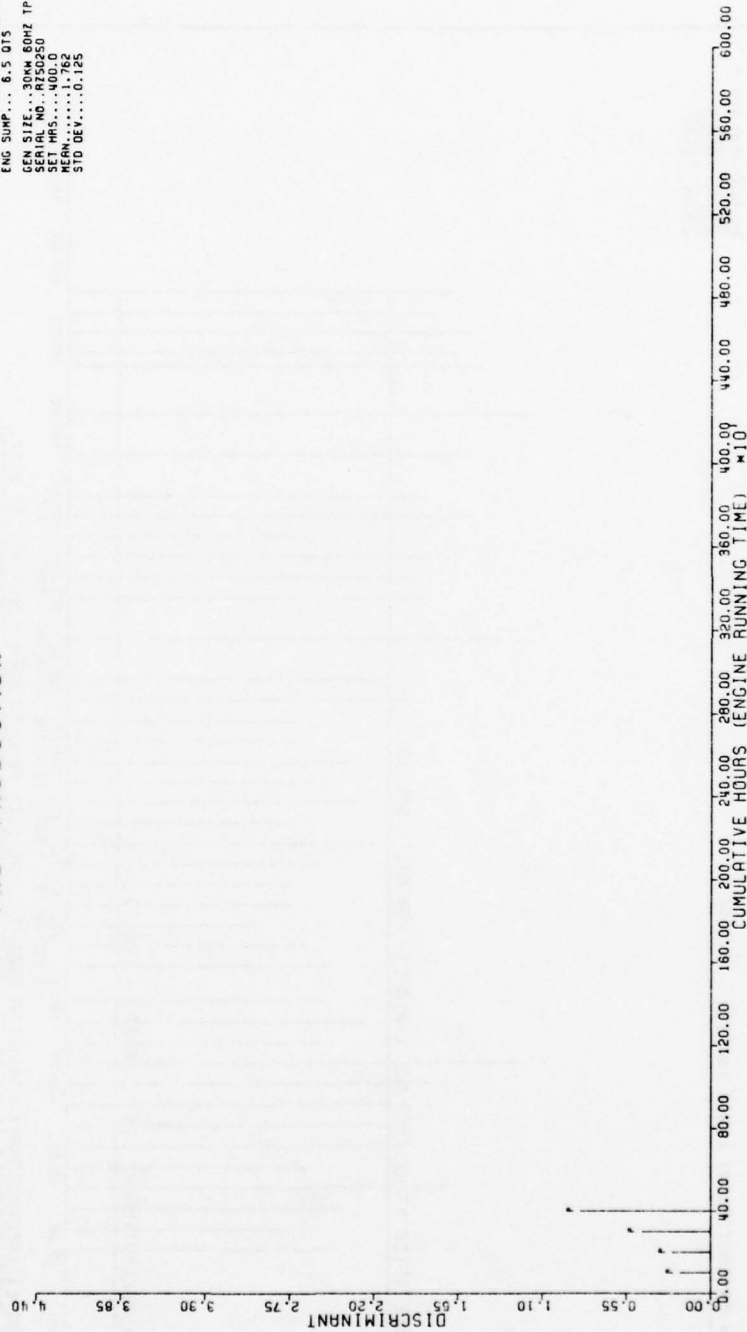
NOTE PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

INCLUSIVE DATES
22 JUN 76 19 JULY 76
ENG SIZE... 60.0 H.P.
ENG NO... 288R
ENG SUMP... 6.5 QTS
GEN SIZE... 3004 60HZ TP
SERIAL NO... R750250
SET HRS... 400.0
MEAN... 1.762
STD DEV... 0.125

PENTANE .VS. BENZENE PRE - PRODUCTION



P SPECIFIES THAT THE PENTANE READING IS GREATER THAN THE BENZENE READING
B SPECIFIES THAT THE BENZENE READING IS GREATER THAN THE PENTANE READING

100 HOURS AT BASE LINE, 300 HOURS AT 125 DEGREES

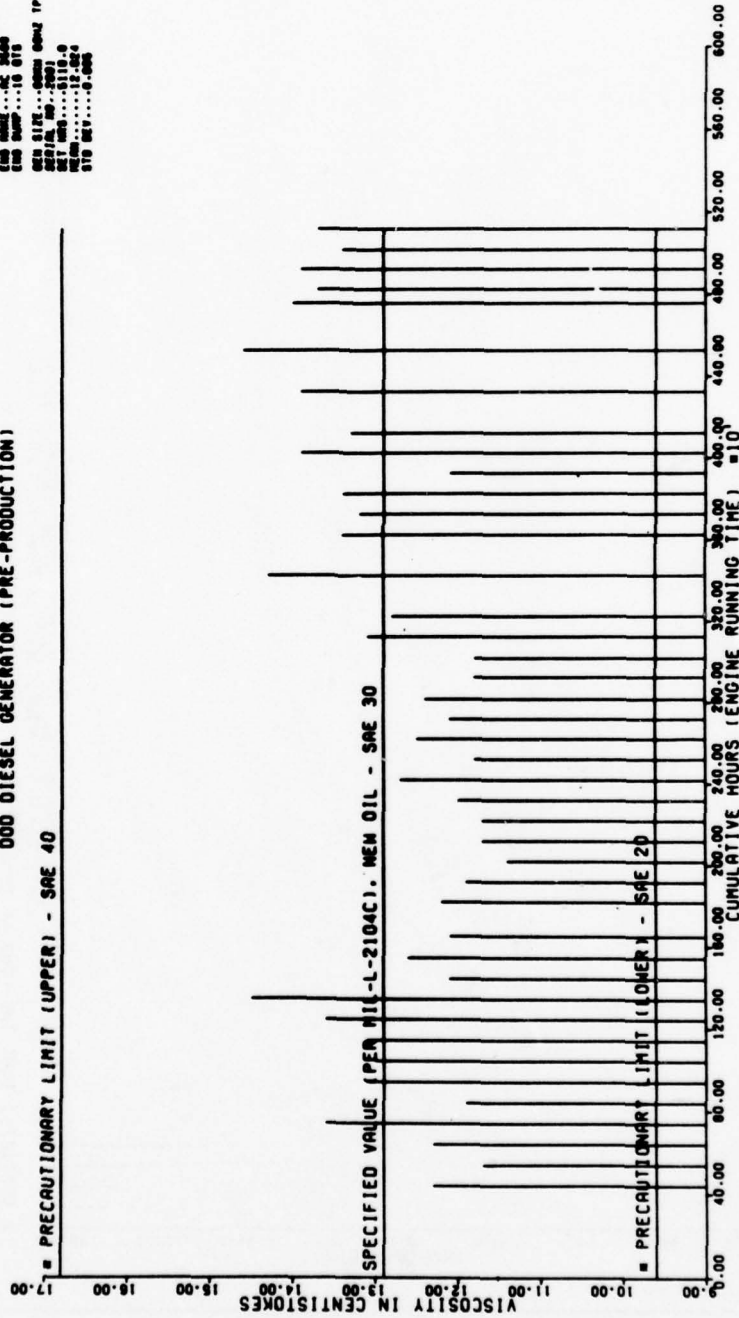
INCLUSIVE DATES
15 MAY 72 14 SEP 73
END DATE 104 0-0-0
END NAME MC 2000
END SAE 10 010
END DATE 0000 00-0-0
END NAME 00-0-0
END SAE 11 010-0
END DATE 12-000
END NAME 0-000

VISCOSITY OF USED OIL AT 210 F 000 DIESEL GENERATOR (PRE-PRODUCTION)

PRECAUTIONARY LIMIT (UPPER) - SAE 40

SPECIFIED VALUE (PER MIL-L-2104C). NEW OIL - SAE 30

PRECAUTIONARY LIMIT (LOWER) - SAE 20



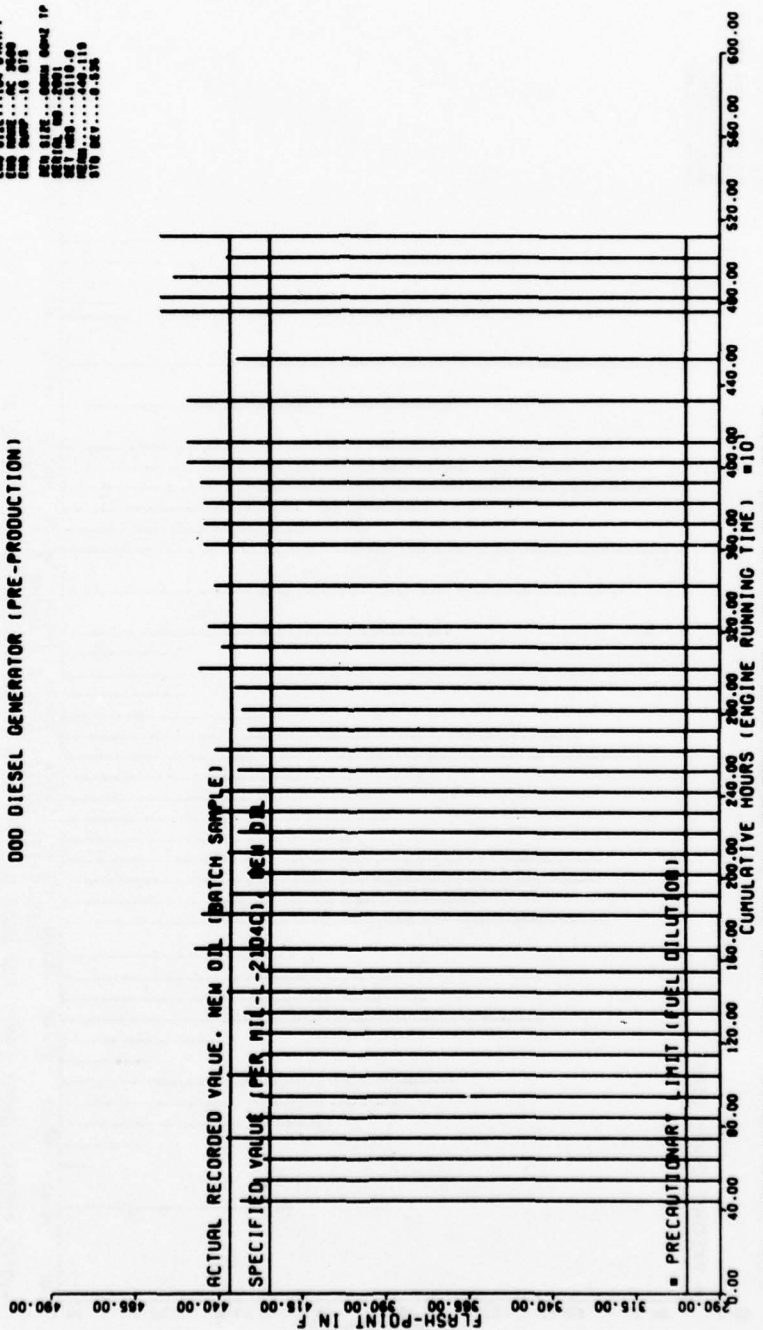
NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210 F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).

000 DIESEL GENERATOR (PRE-PRODUCTION)

INCLUSIVE DATES
13 MAY 72 14 SEP 73

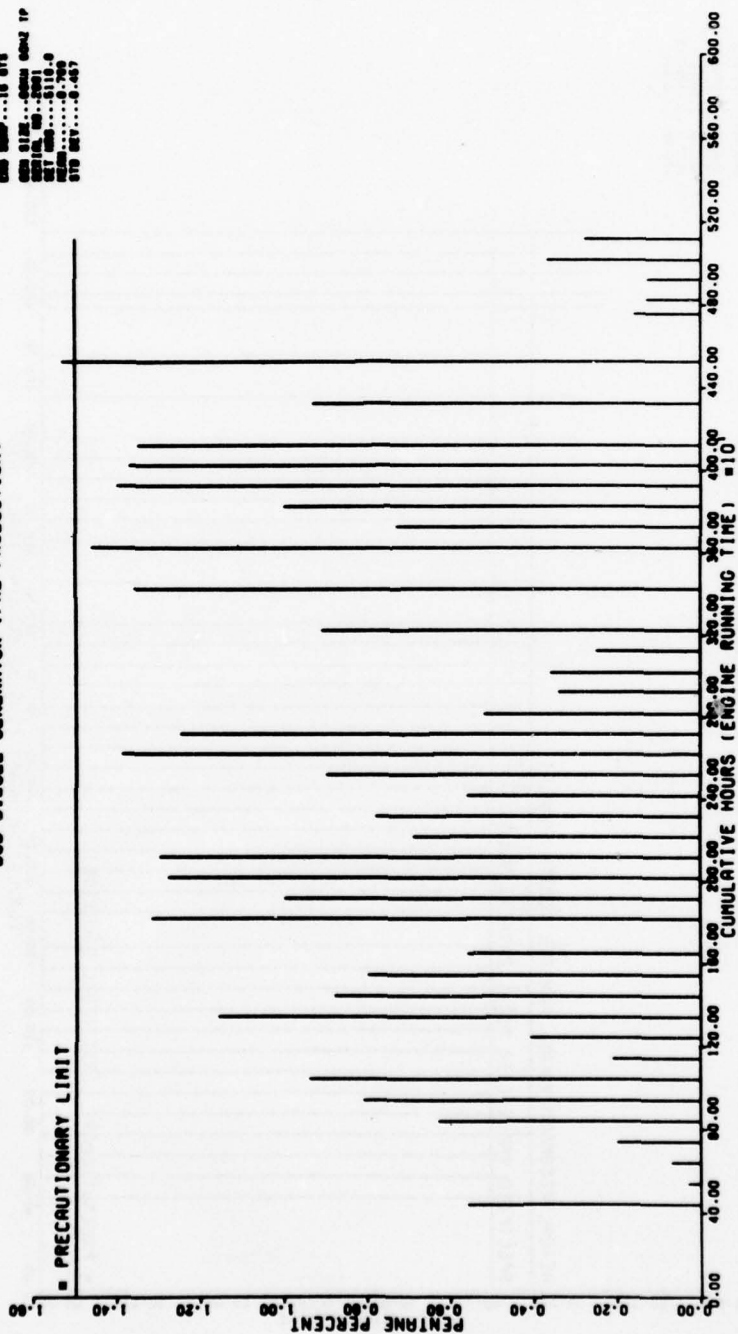
END SIZE...104 0-M.P.
END NAME...AC 3500
END GRP...10 015

NEW SIZE...0000 00-12 1P
SERIAL NO...2001
NEW MSB...5110-0
NEW...440-11
STD DEV...0-0-530



=NOTE! PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

INCLUSIVE DATES
13 MAY 72 14 SEP 73
220 SIZE...104 0-M-P.
220 MAG...AC 2000
220 COMP...16 078
220 SIZE...0000 0002 1P
ORIGINAL NO. 2001
220 MAG...0110-0
220 MAG...0-700
220 MAG...0-457

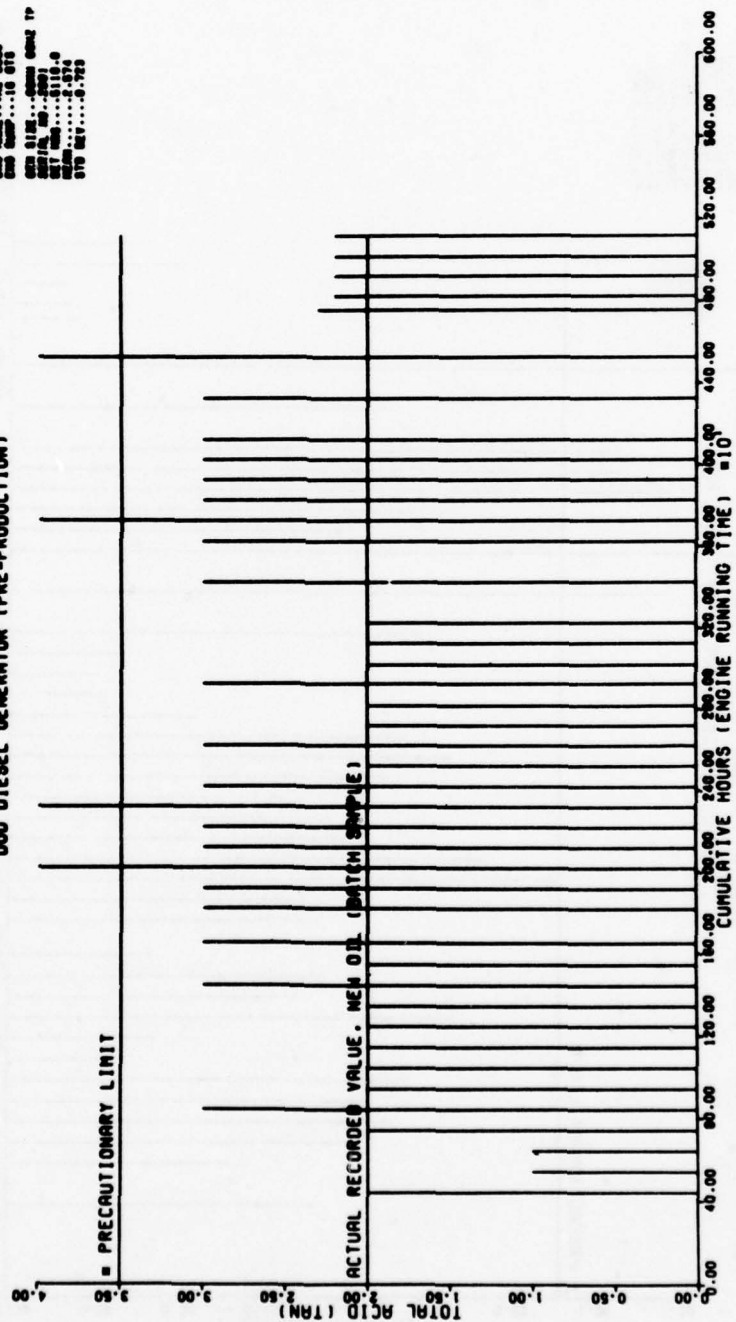


*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF PENTANE INSOLUBLES REACHES 1.50 PERCENT.

INCLUSIVE DATES
13 MAY 72 14 SEP 79

END SIZE...104 8-M.P.
END NAME...AC 2000
END SNIP...10 016

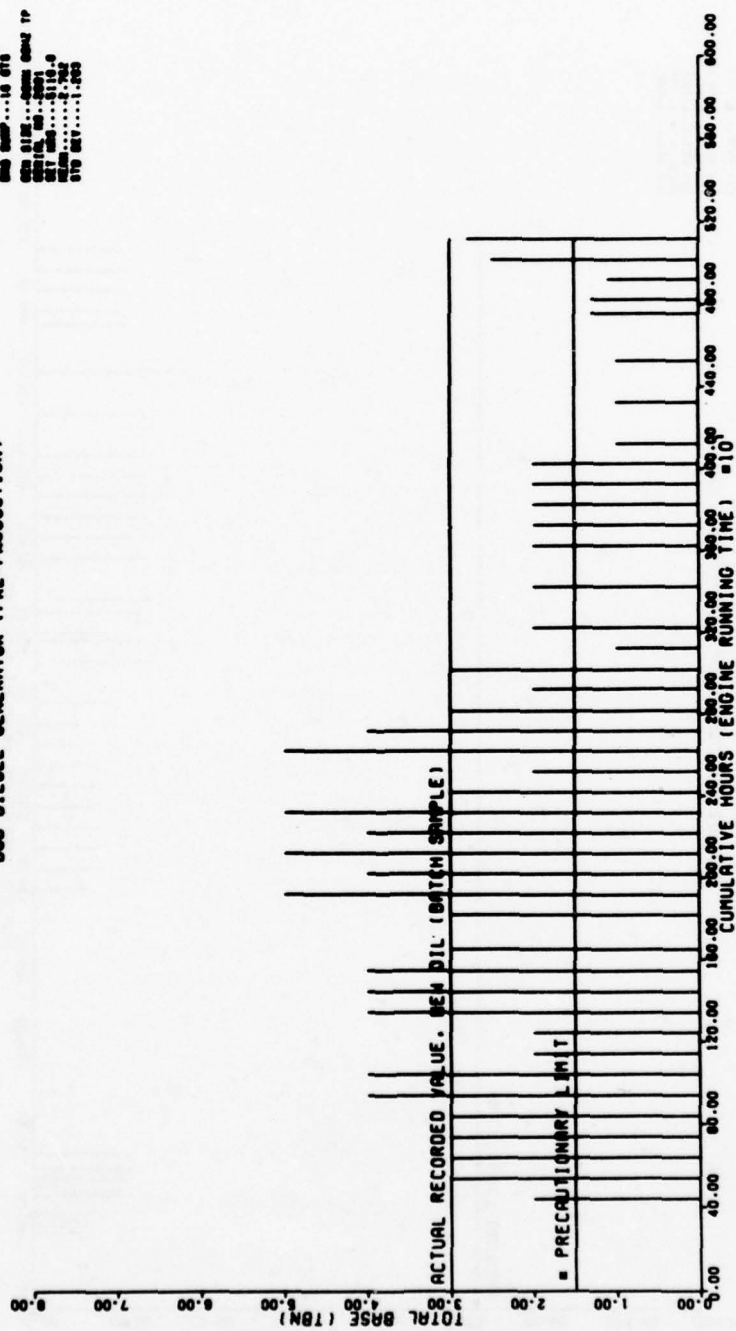
END SIZE...0000 0012 TP
SERIAL NO...2001
REV NO...0110-0
TEAM...2-074
STD DEV...0-723



NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

INCLUSIVE DATES
 12 SEP 72 - 14 SEP 72
 OIL TYPE...104 0.0 P.
 OIL GRADE...15 0.0
 OIL VISC...15 0.0
 OIL DENSITY...15 0.0
 OIL TYPE...104 0.0 P.
 OIL GRADE...15 0.0
 OIL VISC...15 0.0
 OIL DENSITY...15 0.0

TOTAL BASE IN USED OIL DDO DIESEL GENERATOR (PRE-PRODUCTION)

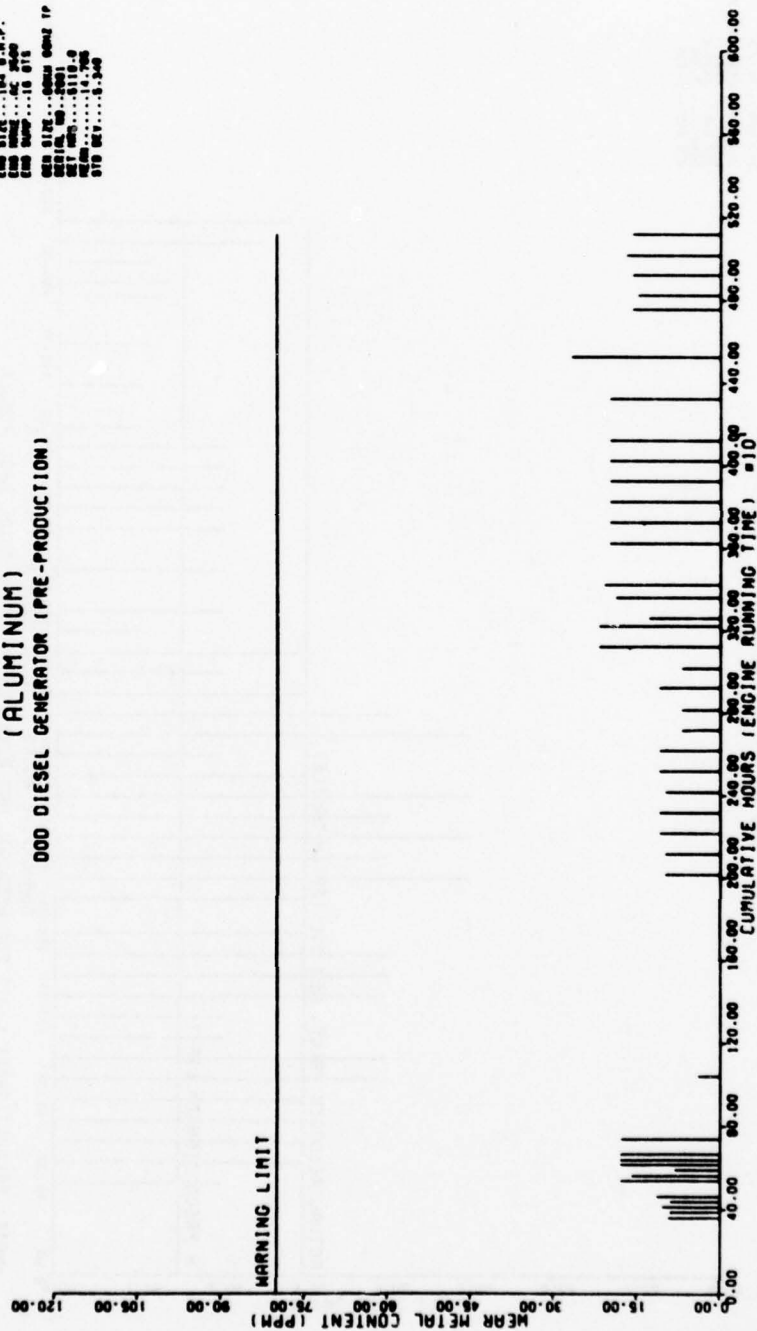


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL BASE NUMBER (TBN) DECREASES TO ONE HALF OF ORIGINAL TBN VALUE OF THE NEW OIL (BATCH SAMPLE)

000 DIESEL GENERATOR (PRE-PRODUCTION)

INCLUSIVE DATES
9 MAY 72 14 SEP 73

END DATE	104 8.M.P.
END DATE	AC 25-00
END DATE	16 015
END DATE	0000 0002 10
END DATE	0000 0001
END DATE	0110-0
END DATE	14 700
END DATE	03-00



NOTES
 * - INDICATES ZERO VALUE (0 PPM)
 NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

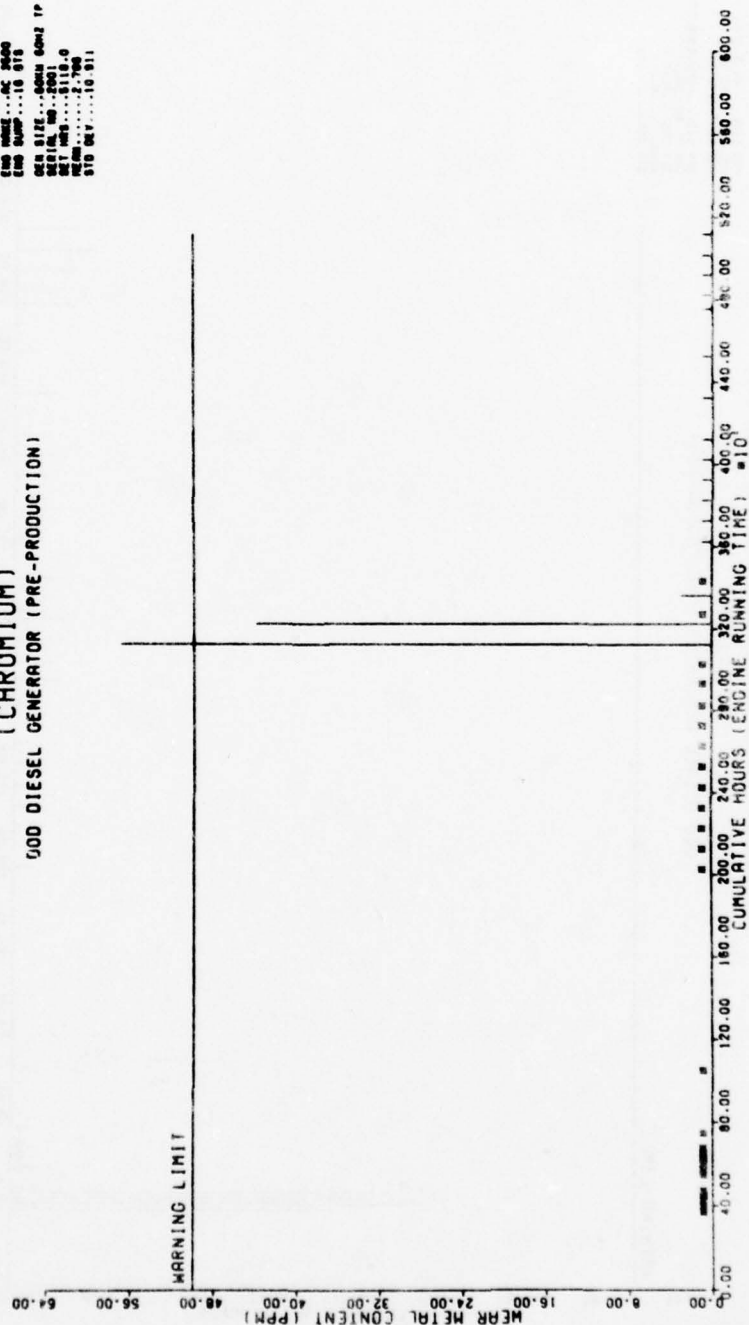
1500 DIESEL GENERATOR (PRE-PRODUCTION)

EXCLUSIVE DATE
9 MAY 72 14 SEP 73

END SIZE...104 8.M.P.
END WAVE...AC 3600
END SUMP...16 818

END SIZE...0000 0002 TP
END WAVE...AC 3600
END SUMP...16 818

116.01...A20 010
001.2...A20 010
011.0...A20 010



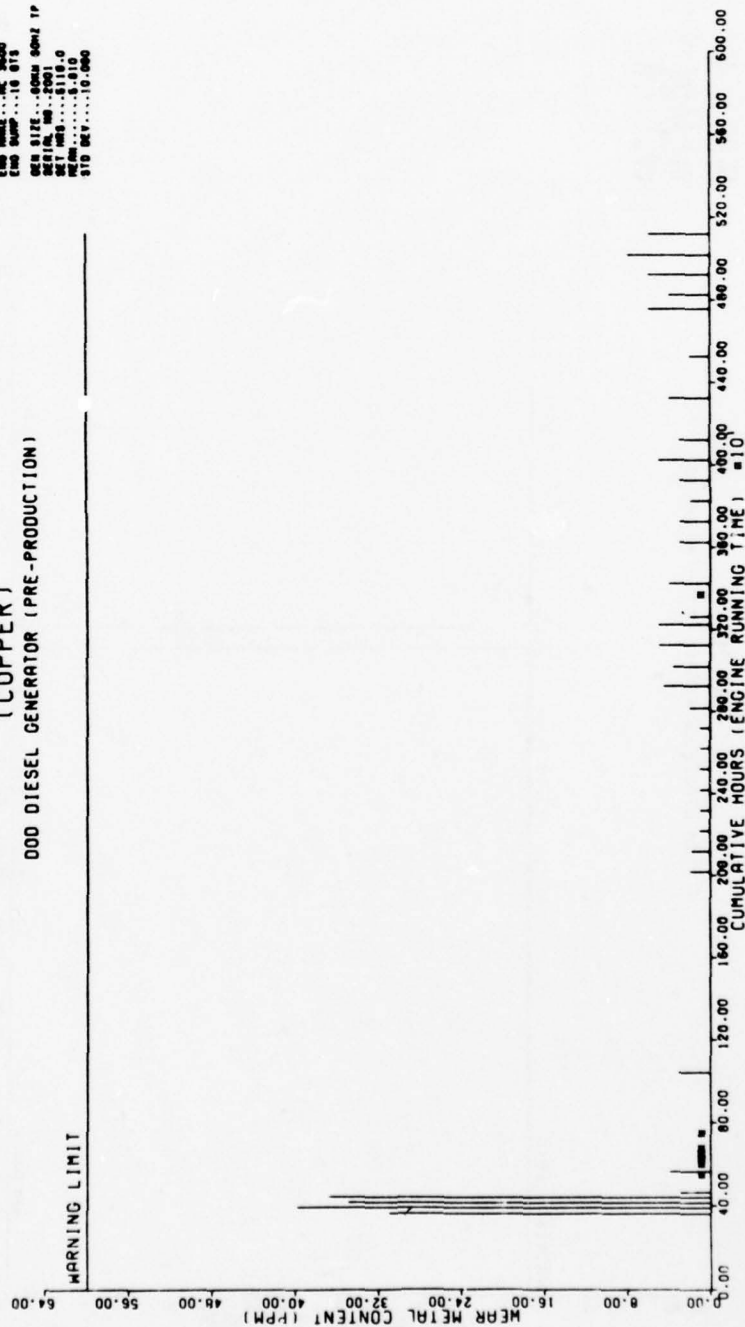
NOTES

- INDICATES ZERO VALUE (0 PPM)

NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS


```
END COMP...10 BYS
GEN SIZE...GOLM 50M2 TP
SERIAL NO...2001
SET MRS...5110.0
MEAN.....5.810
STD DEV...10.080
```

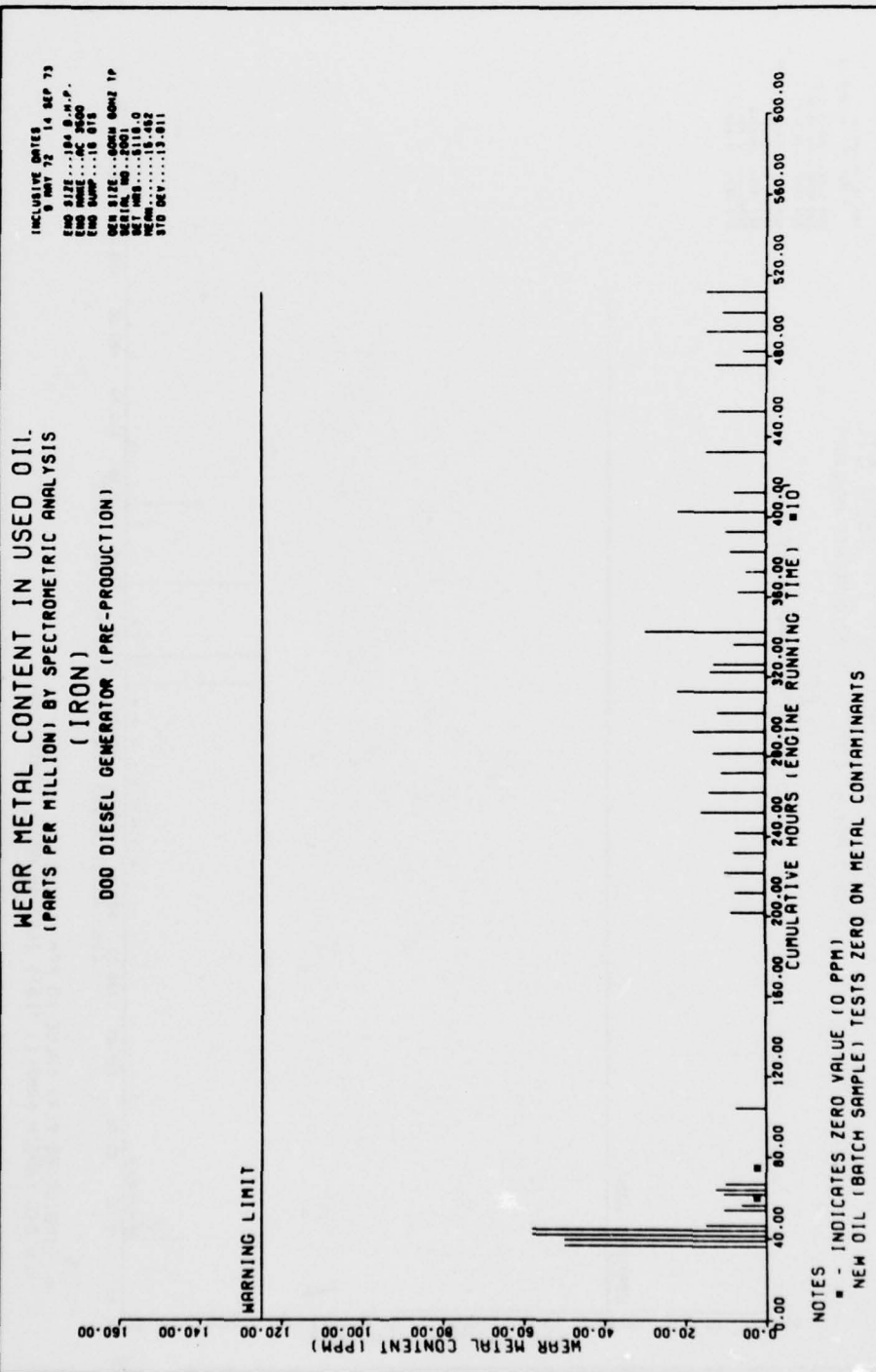
000 DIESEL GENERATOR (PRE-PRODUCTION)

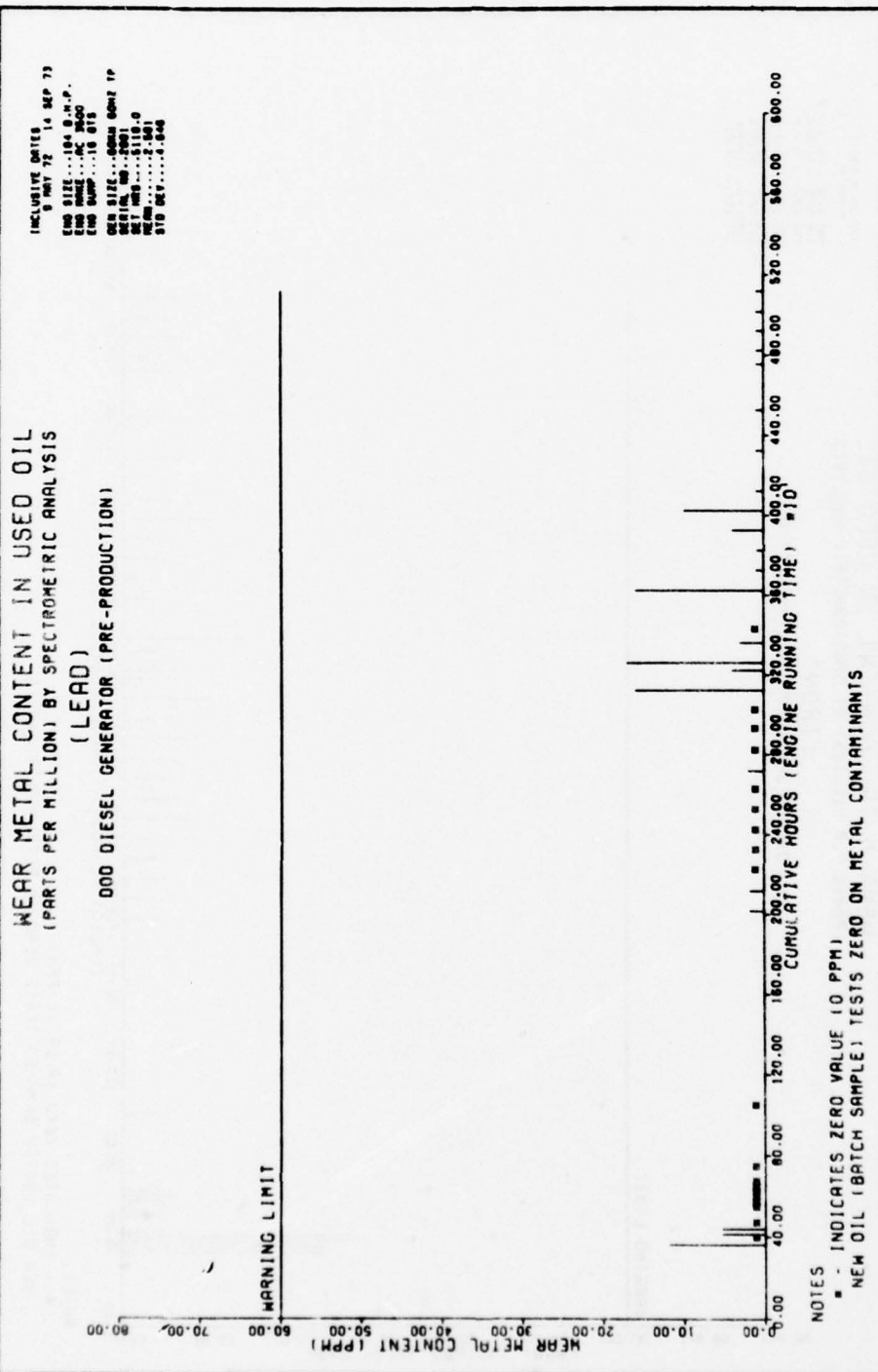


NOTES

* - INDICATES ZERO VALUE (0 PPM)

NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

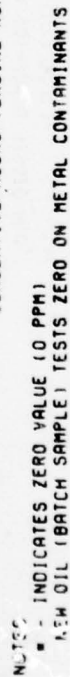


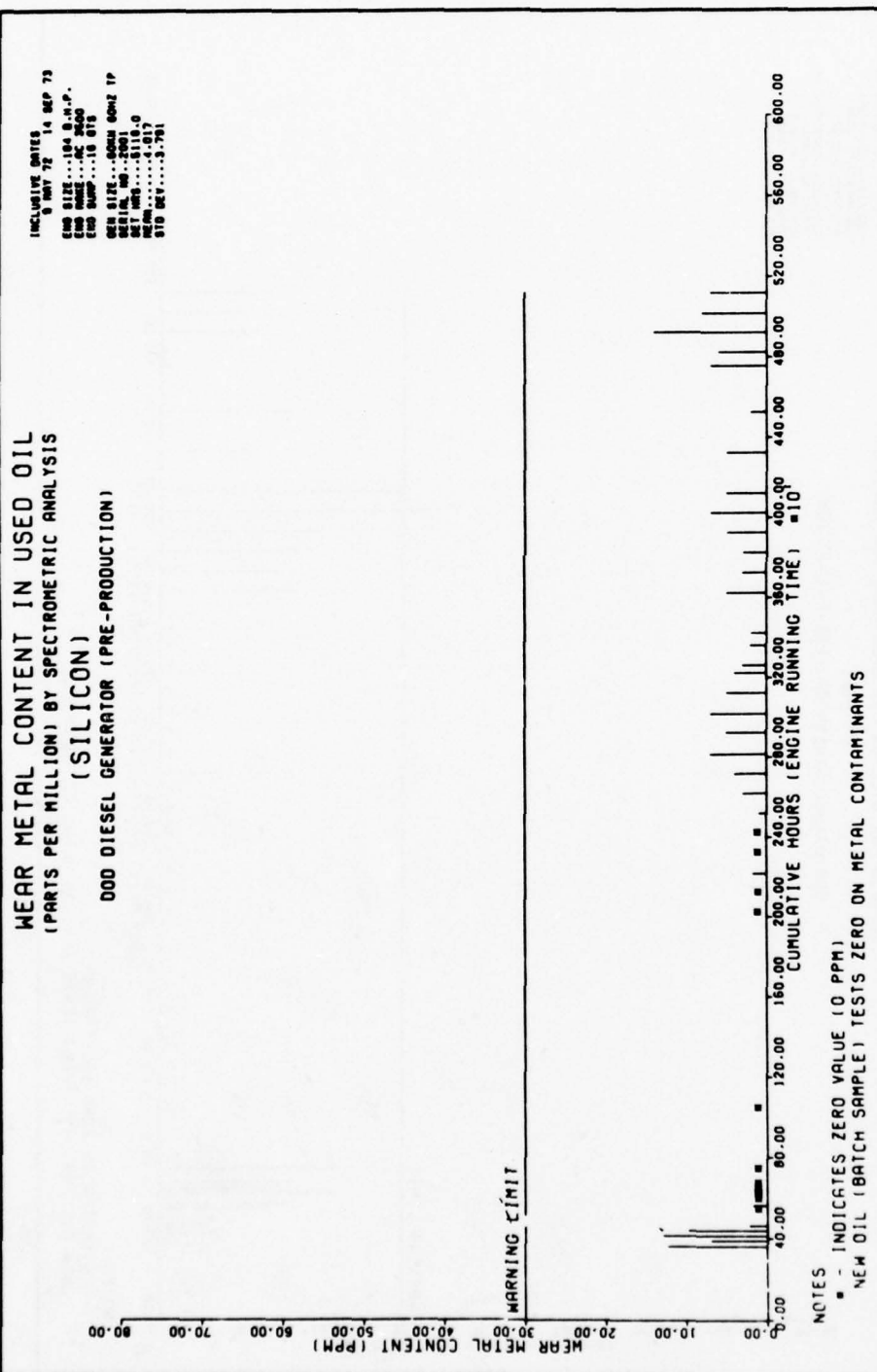


INCLUSIVE DATES
9 MAY 72 14 SEP 73

END SIZE...104 B.M.P.
END PRICE...AC 3500
END DUMP...16 OTS

END SIZE...0000 0001 TP
SERIAL NO...2001
DET WTS...5110.0
WEIGH...7.030
SIC...9-210





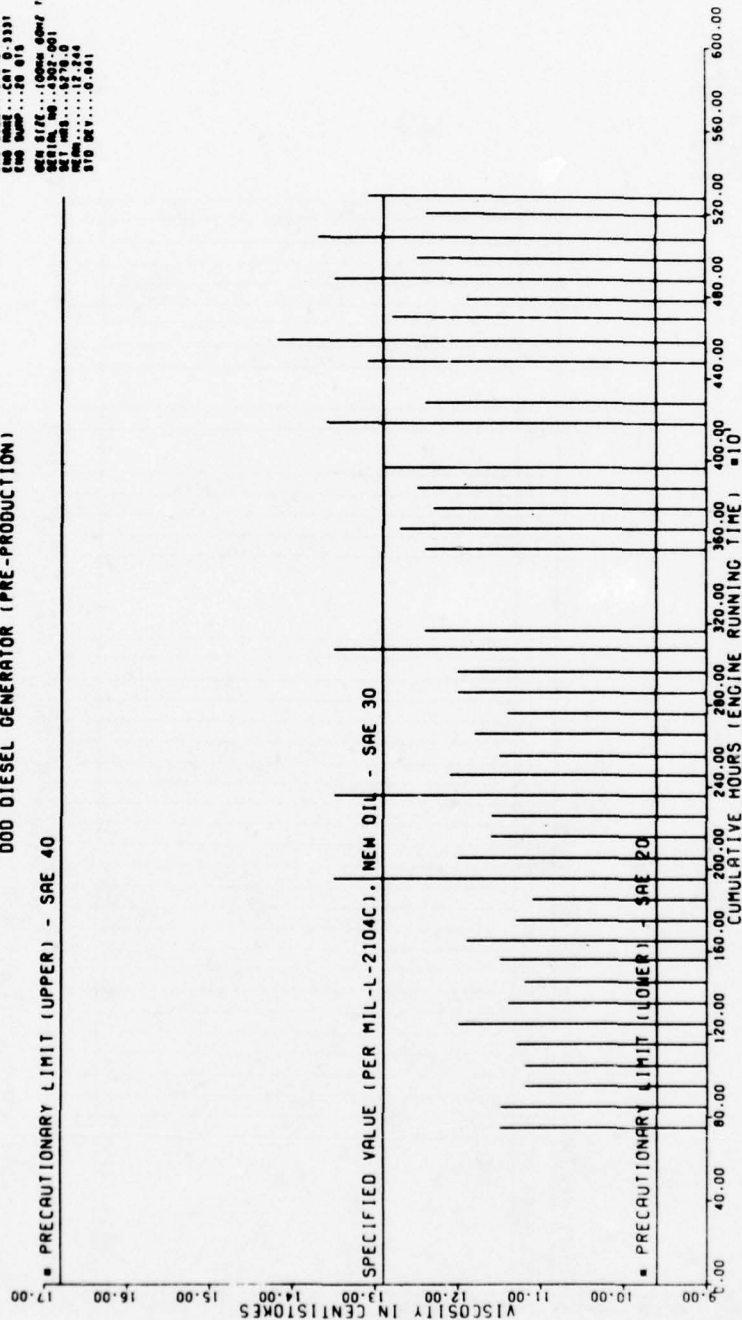
INCLUSIVE DATES
25 OCT 72 23 JUN 73

END SIZE	270 B.W.P.
END NAME	CAT 0.3331
END SUMP	20 015
END SIZE	00000 0000 1P
SERIAL NO	4307-001
SET NO	6278.0
REG	12.244
STD DEV	0.041

■ PRECAUTIONARY LIMIT (UPPER) - SAE 40

SPECIFIED VALUE (PER MIL-L-2104C). NEW OIL - SAE 30

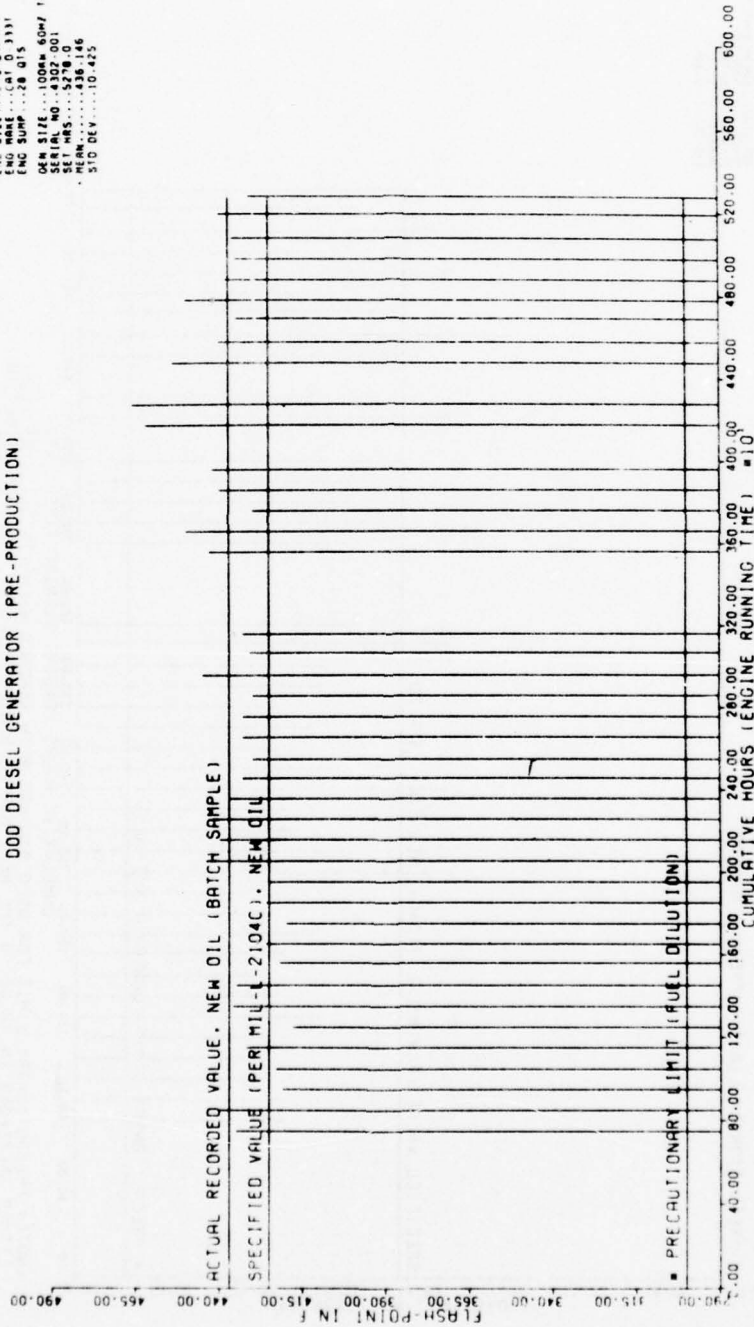
■ PRECAUTIONARY LIMIT (LOWER) - \$AE 20



*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210°F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).

INCLUSIVE DATES
25 OCT 72 - 23 JAN 73
END SIZE...275 0 M.P.
END NAME...CAT 0 3331
END SUMP...28 0/5
OIL SIZE...1000 60W/1P
SERIAL NO...436 001
SET HAS...428 0
MEAN...436.146
STD DEV...10.425

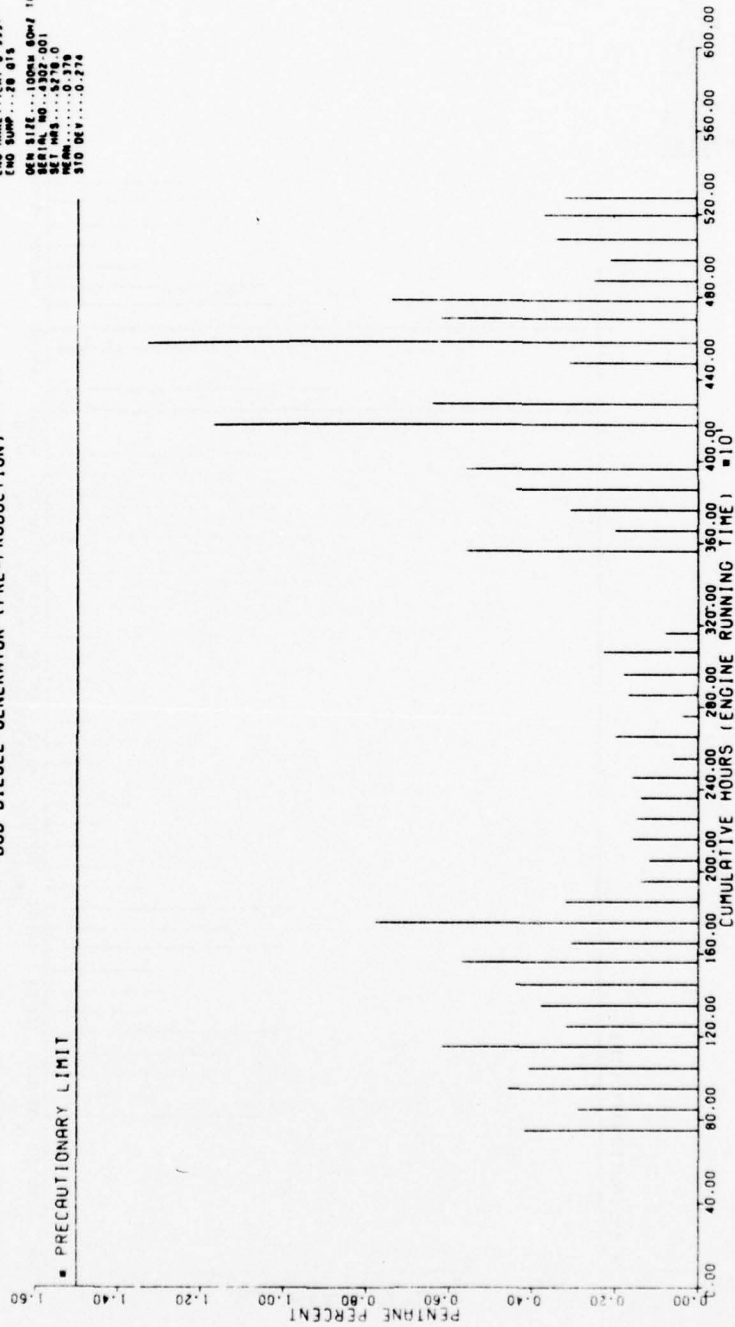
FLASH-POINT OF USED OIL (F) DOD DIESEL GENERATOR (PRE-PRODUCTION)



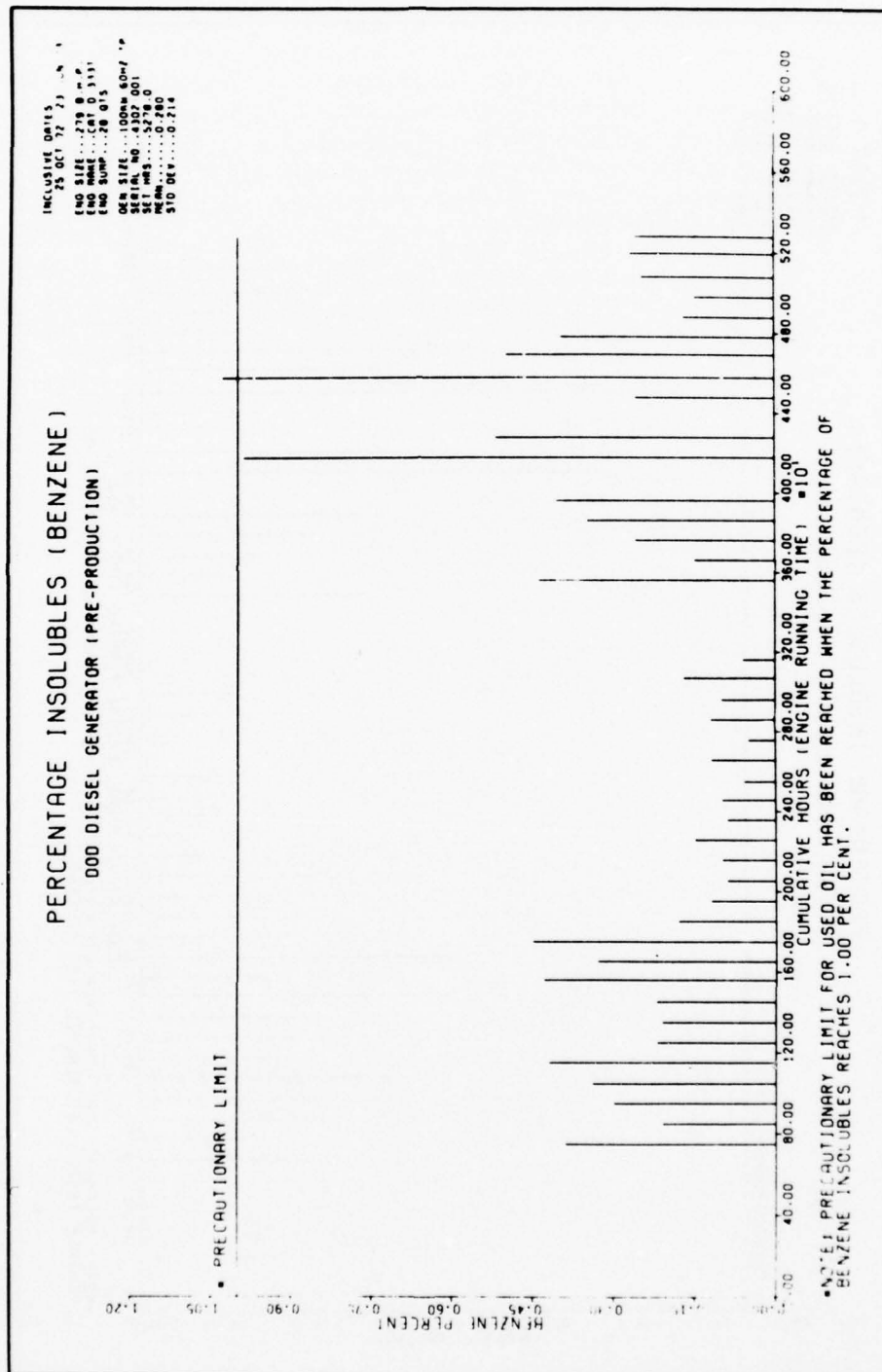
*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

INCLUSIVE DATES
 28 OCT 72 23 JUN 73
 END SIZE ... 278 8 m.p.
 END NAME ... CAT 0 3331
 END SUM ... 28 615
 OEN SIZE ... 100m 60-7 1P
 SERIAL NO ... 2302-001
 S/N ... 0 278
 MFG ... 0 278
 S10 DEV ... 0.278

PERCENTAGE INSOLUBLES (PENTANE) DOD DIESEL GENERATOR (PRE-PRODUCTION)



*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF
 PENTANE INSOLUBLE REACHES 1.50 PERCENT.

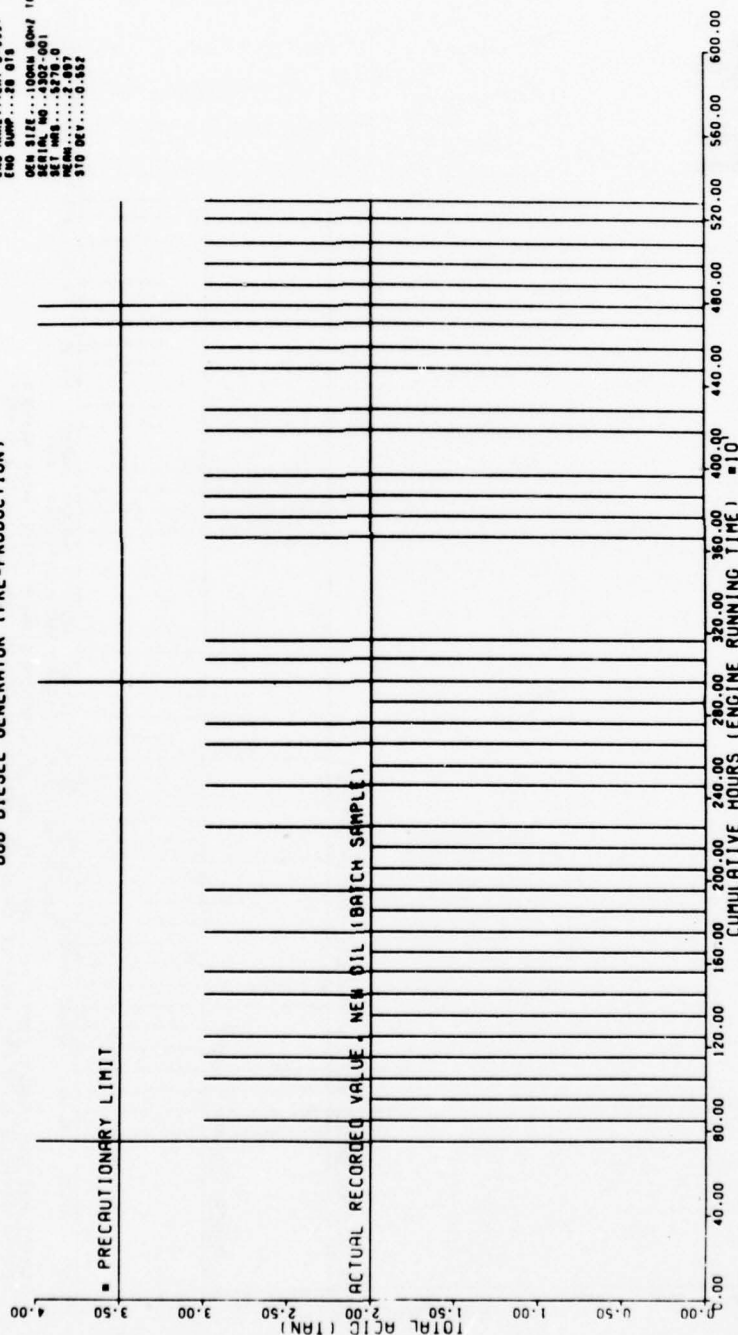


INCLUSIVE DATES
26 OCT 72 23 JUN 73

END SIZE...270 B.M.P.
END SUMS...CUT 0.3331
END SUMS...28 018

OSR SIZE...10000 BOM/ IP
OSR SIZE...10000 BOM/ IP
SET NOS...2.857
MEAN...0.552
STD DEV...0.552

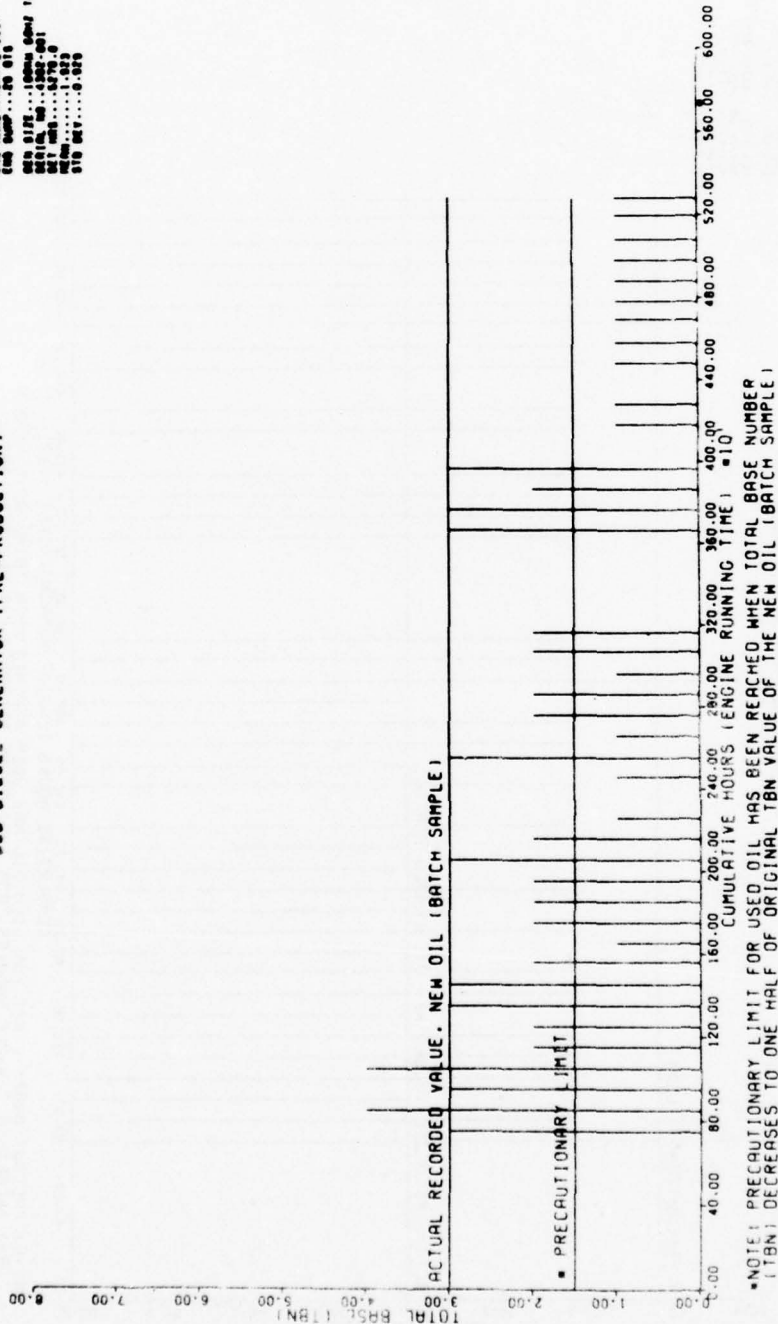
TOTAL ACID IN USED OIL DOD DIESEL GENERATOR (PRE-PRODUCTION)



*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

TOTAL BASE IN USED OIL DOD DIESEL GENERATOR (PRE-PRODUCTION)

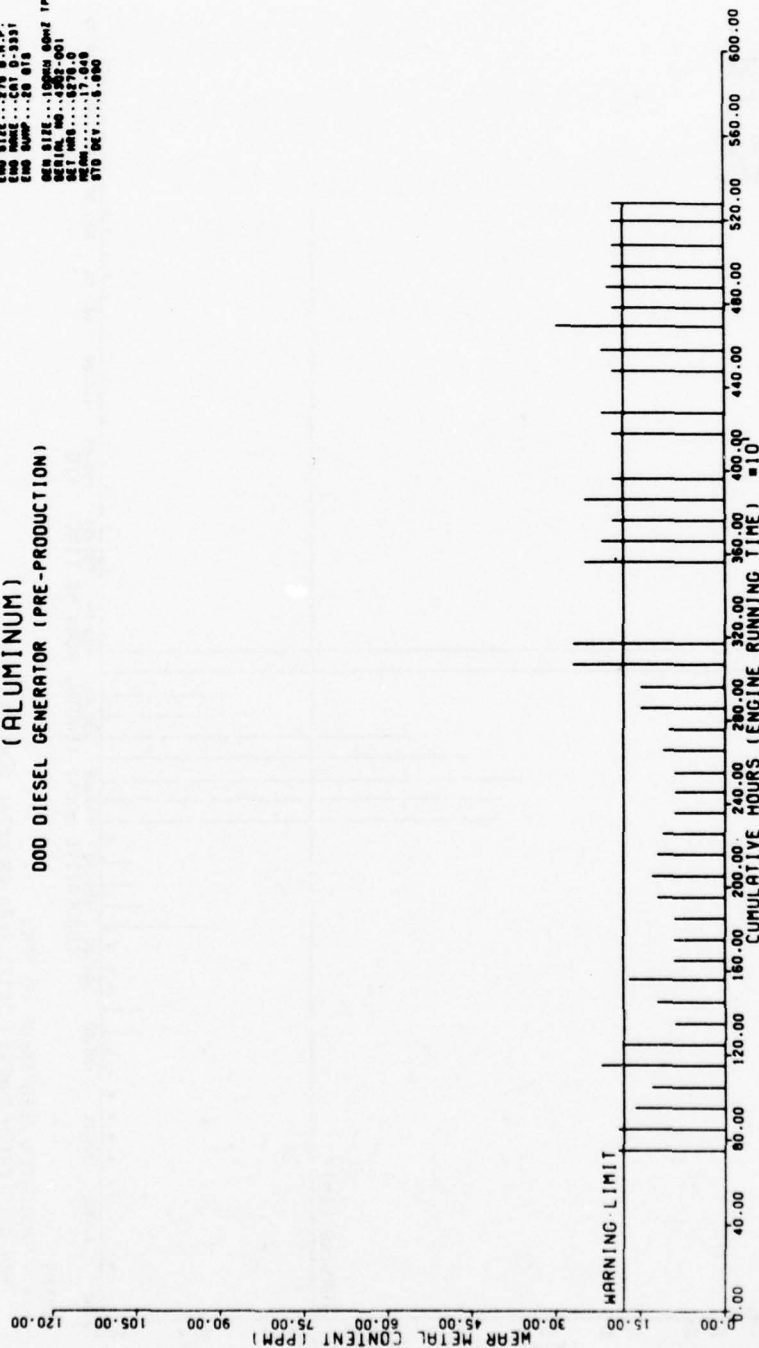
INCLUSIVE DATES
25 OCT 72 TO 23 JUN 73
END DATE...270 8.00 P.
END TIME...041 0.5551
END DATE...25 0.16
END TIME...1000 0.00
END DATE...25 0.16
END TIME...1000 0.00
END DATE...25 0.16
END TIME...1000 0.00
END DATE...25 0.16
END TIME...1000 0.00



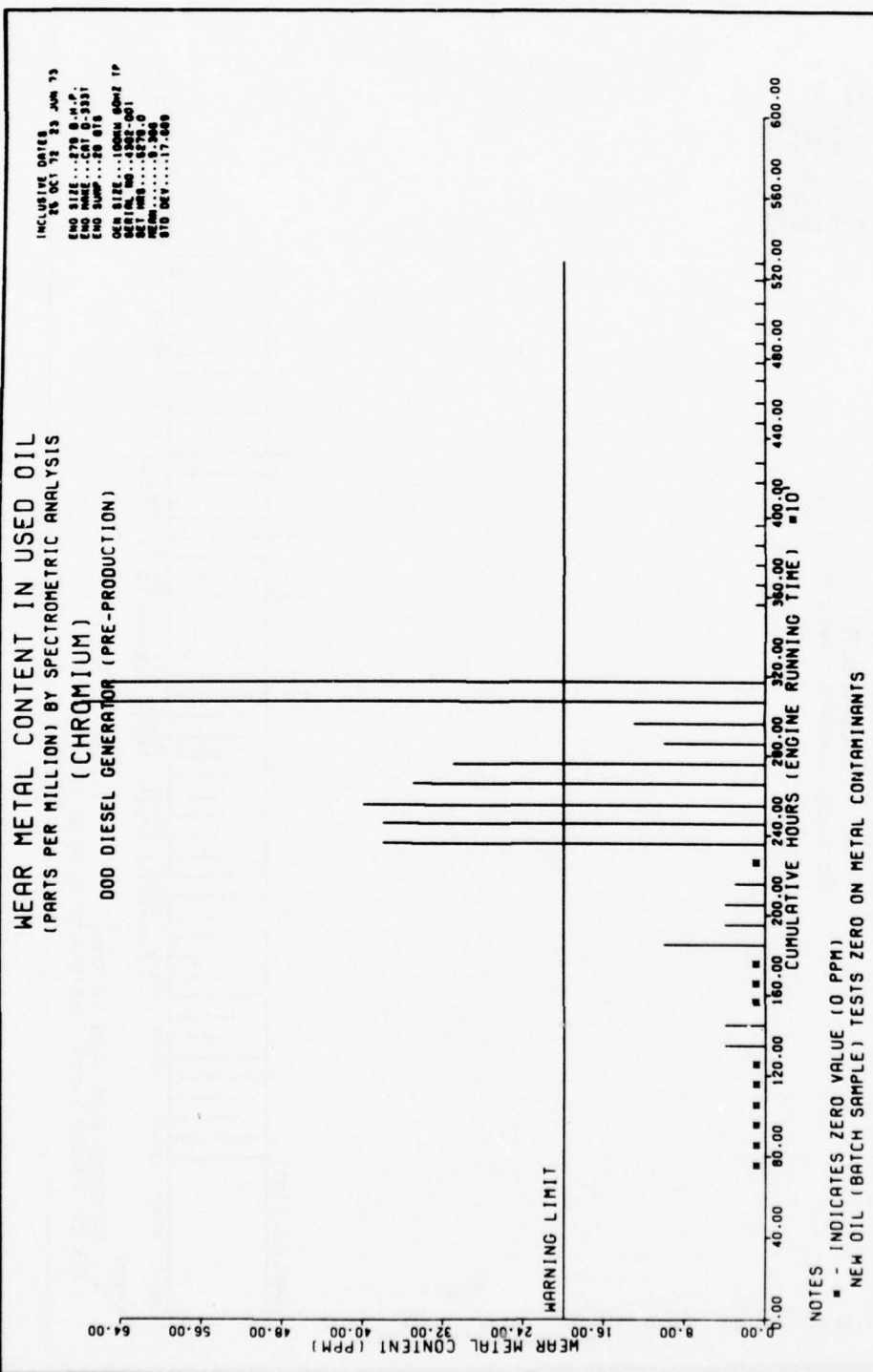
WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (ALUMINUM)

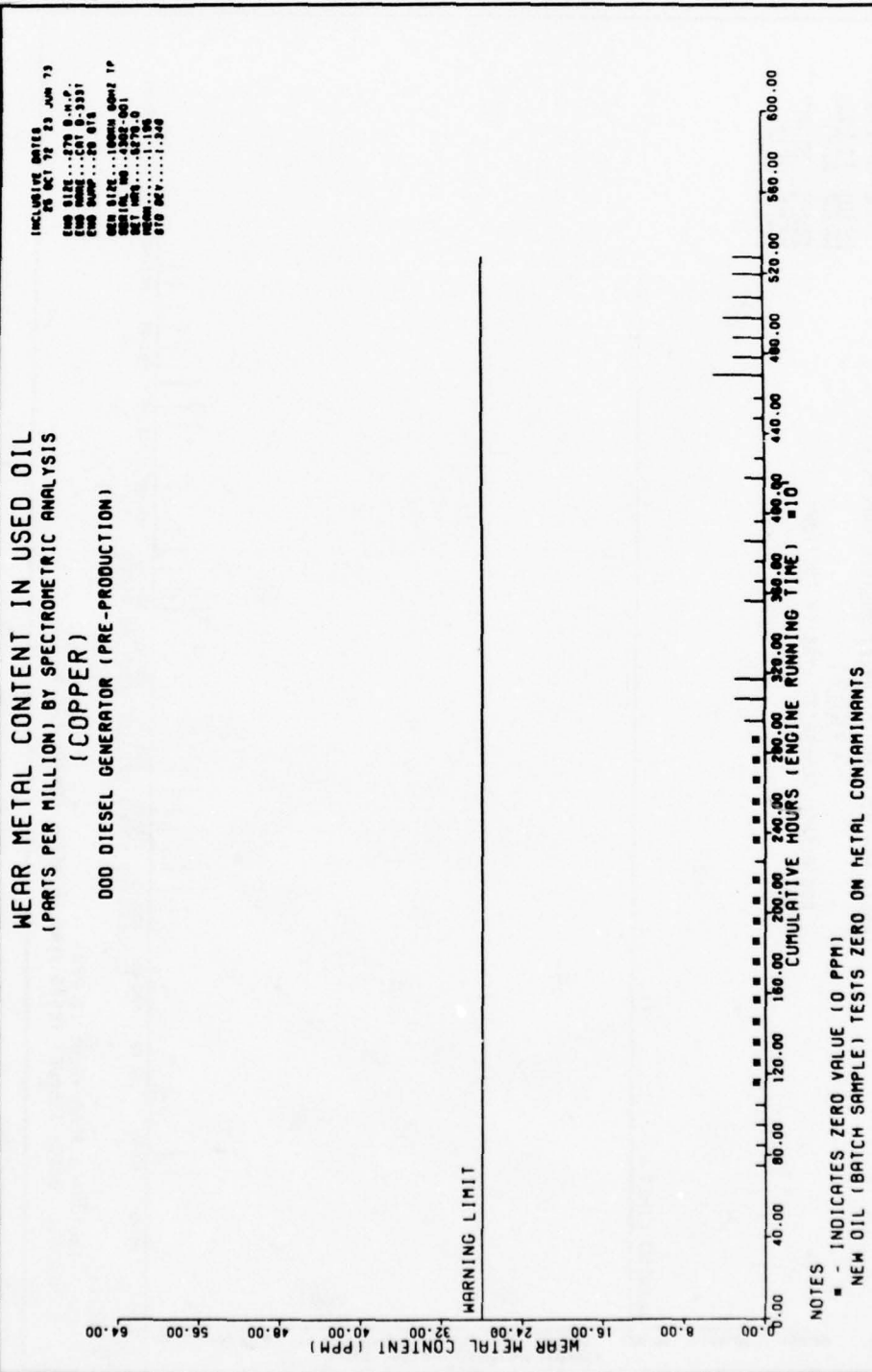
000 DIESEL GENERATOR (PRE-PRODUCTION)

INCLUSIVE DATES
26 OCT 72 23 JUN 73
END SIZE...270 8-H.P.
END NAME...CAT 0-3331
END BUMP...26 018
END SIZE...10000 00H2 1P
END NAME...10000 00H2 1P
END BUMP...17.049
END DATE...010 DEC 73



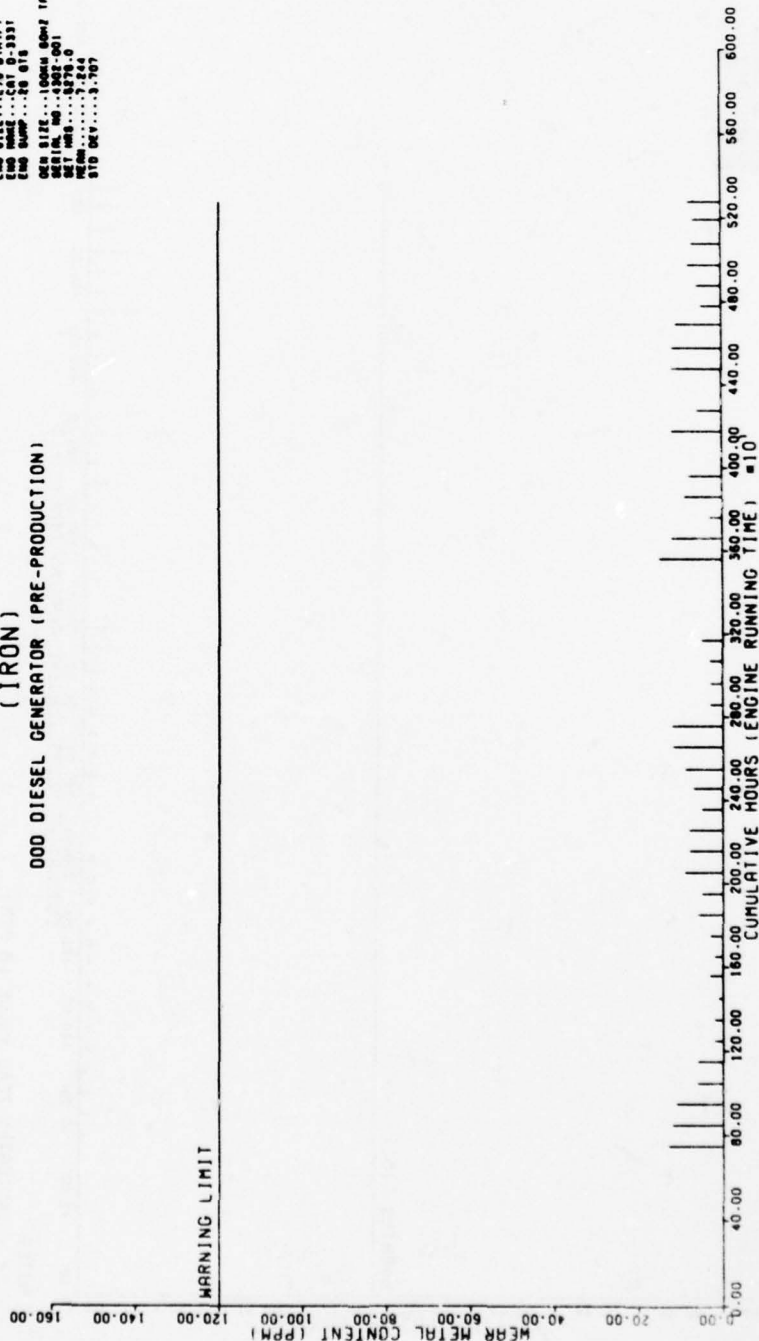
NOTES
■ - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS





WEAR METAL CONTENT IN USED OIL
(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS
(IRON)
000 DIESEL GENERATOR (PRE-PRODUCTION)

INCLUSIVE DATES
25 OCT 72 23 JUN 73
END SIZE...278 S.H.P.
END NAME...C01 0-3357
END SNIP...20 018
OEN SIZE...10004 80412 1P
SERIAL NO...0302-001
SET HRS...0278.0
NEW...3.244
S10 OCT...3.107

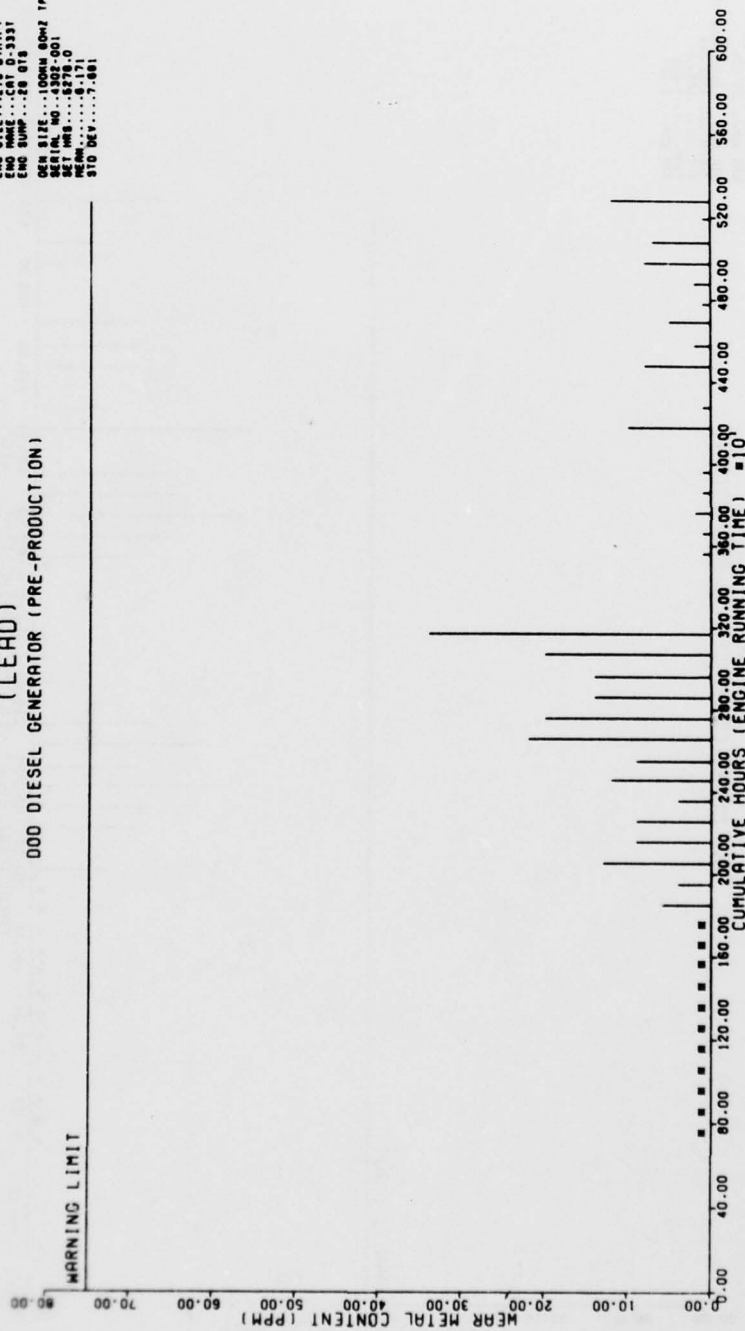


NOTES
* - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (LEAD)

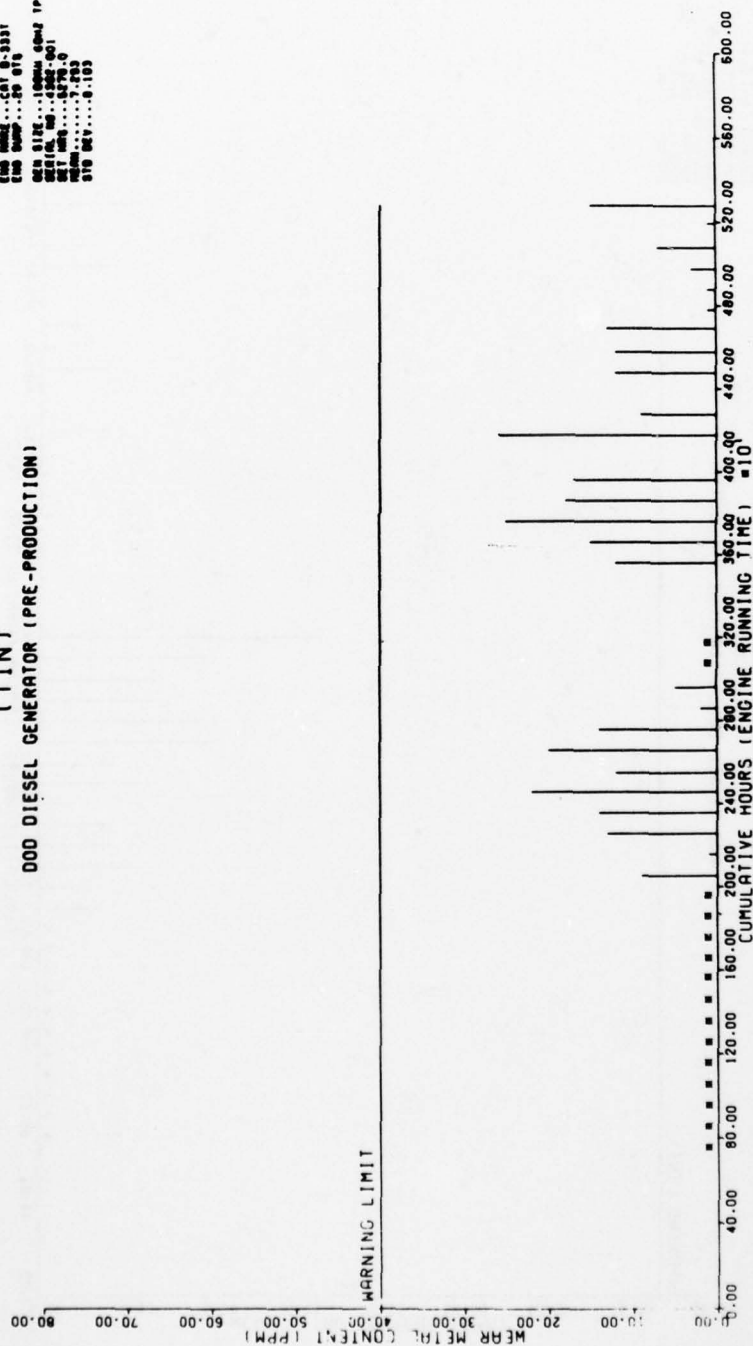
000 DIESEL GENERATOR (PRE-PRODUCTION)

INCLUSIVE DATES
26 OCT 72 23 JUN 73
END SIZE...278 B.H.P.
END NAME...CMT D-3337
END RUM...28 618
OER SIZE...1000H 80WZ 1P
TEST NO...2252-001
SET WRS...5278.0
MEAN...8.171
STD DEV...7.981



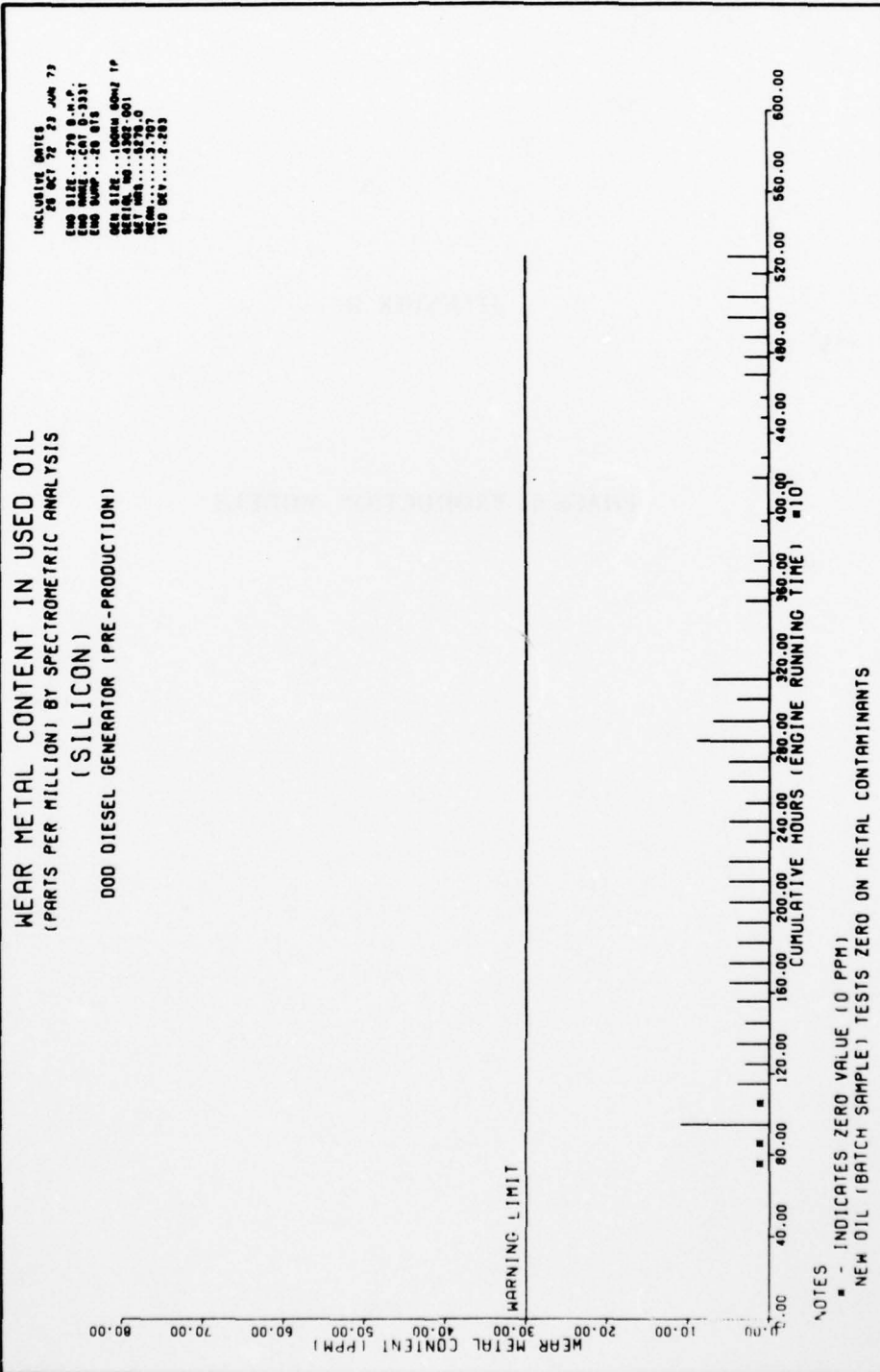
NOTES
■ - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

DOD DIESEL GENERATOR (PRE-PRODUCTION)

[illegible]

NOTES

- * - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

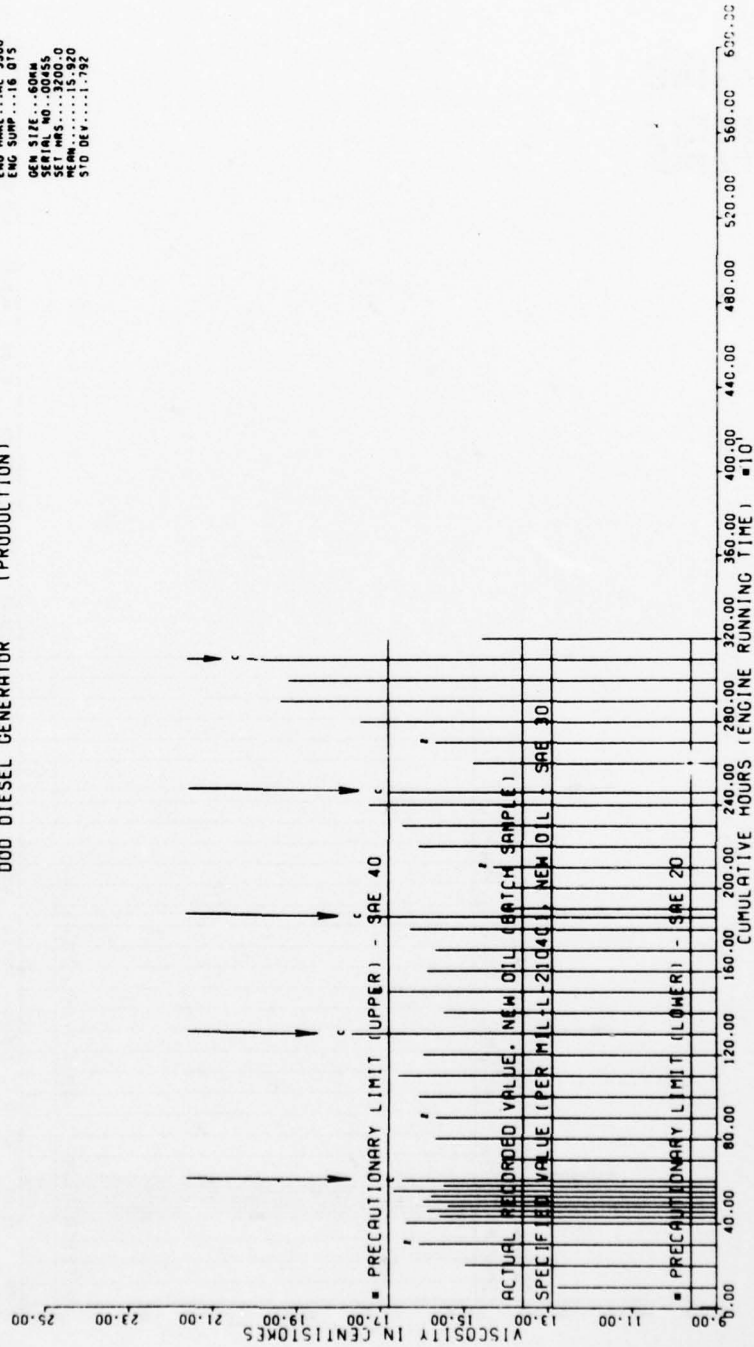


APPENDIX B

PHASE II PRODUCTION MODELS

VISCOSITY OF USED OIL AT 210 F 000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
 8 FEB 74 13 NOV 74
 ENG SIZE...184 B.H.P.
 ENG NAME...AC 3500
 ENG SUMP...16 QTS
 GEN SIZE...60MM
 SERIAL NO...00455
 SAE GRADE...32000
 STD DEV...1.192



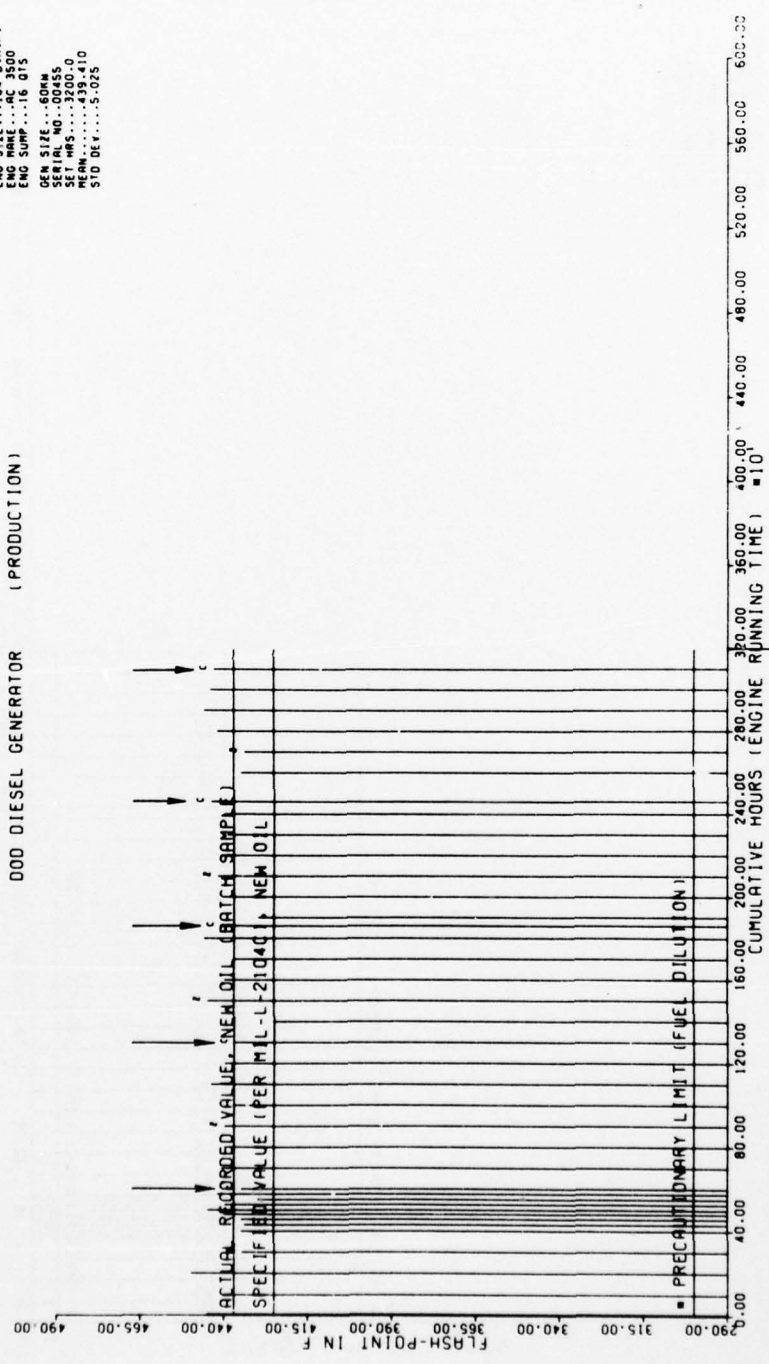
NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).

REMARKS: #10 #11 #12 #13 #14 #15 #16 #17 #18 #19 #20 #21 #22 #23 #24 #25 #26 #27 #28 #29 #30 #31 #32 #33 #34 #35 #36 #37 #38 #39 #40 #41 #42 #43 #44 #45 #46 #47 #48 #49 #50 #51 #52 #53 #54 #55 #56 #57 #58 #59 #60 #61 #62 #63 #64 #65 #66 #67 #68 #69 #70 #71 #72 #73 #74 #75 #76 #77 #78 #79 #80 #81 #82 #83 #84 #85 #86 #87 #88 #89 #90 #91 #92 #93 #94 #95 #96 #97 #98 #99 #100

INCLUSIVE DATES
 8 FEB 74 13 NOV 74
 ENG SIZE...184 0.H.P.
 ENG NAME...AC 2500
 ENG SUMP...16 815
 OIL SIZE...60MM
 OIL NAME...DIESEL
 SET NOS...3200-0
 MEAN.....439.410
 STD DEV.....5.025

FLASH-POINT OF USED OIL (F)

OOD DIESEL GENERATOR (PRODUCTION)

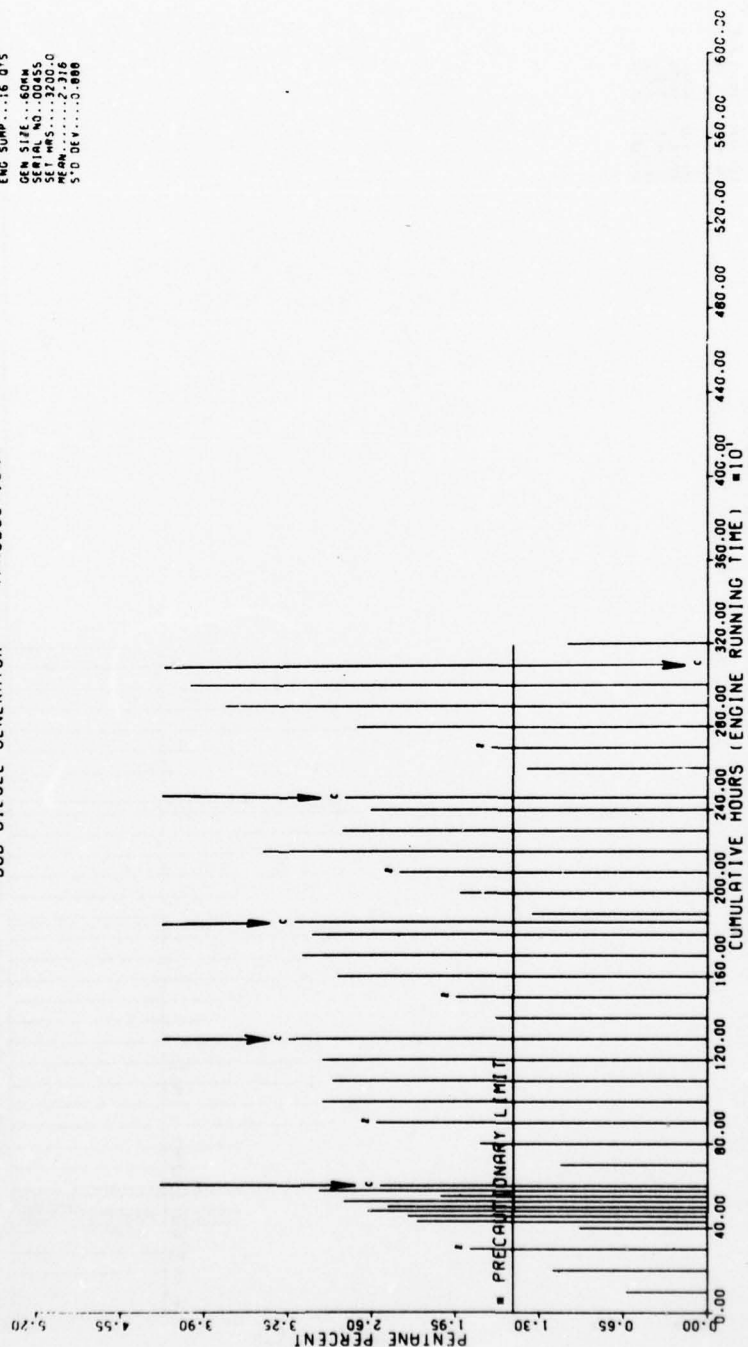


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

F REPRESENTS THE END OF A CYCLE C REPRESENTS NEW OIL CHANGE

INCLUSIVE DATES
 0 FEB 74 TO 13 NOV 74
 ENG SIZE...184.000 P.
 ENG SIZE...16.000
 ENG SUPP...16.000
 GEN SIZE...6000
 SERIAL NO...00465
 SET MRS...3200.0
 MEAN...2.316
 STD DEV...0.888

PERCENTAGE INSOLUBLES (PENTANE) DOD DIESEL GENERATOR (PRODUCTION)

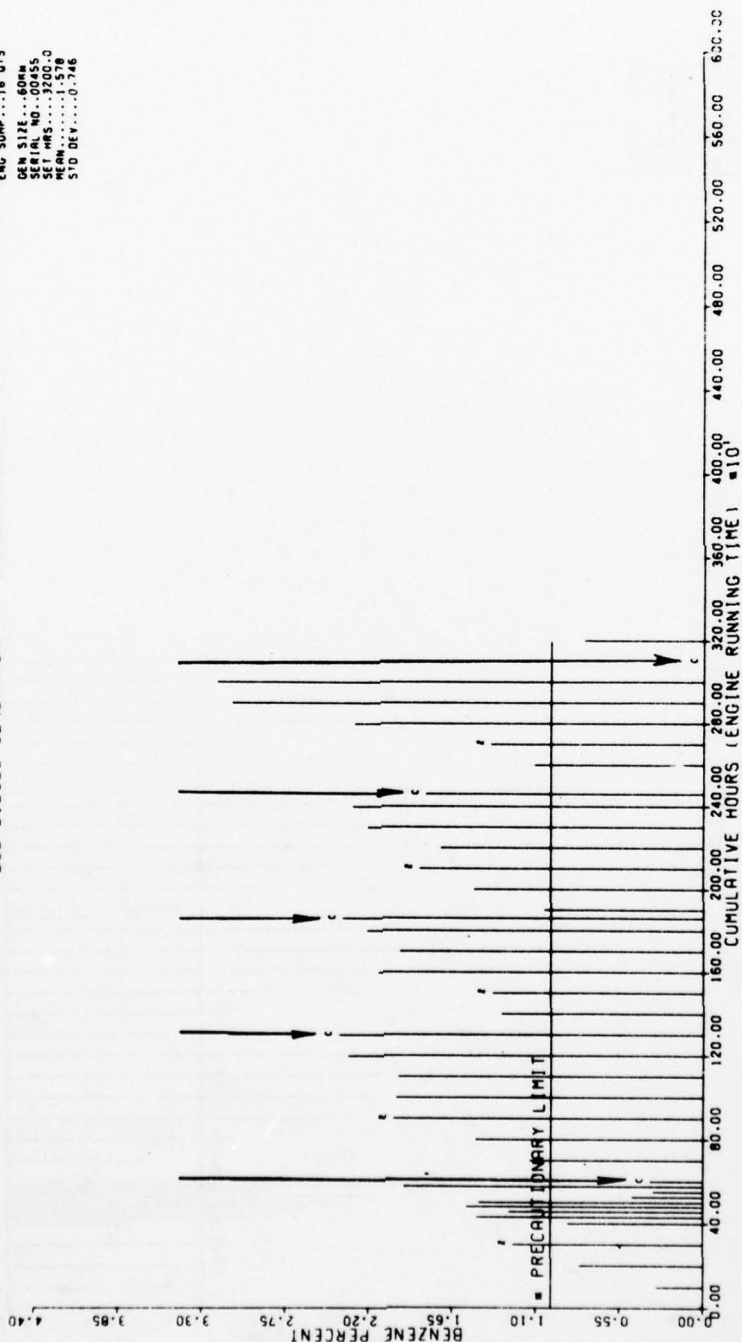


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF PENTANE INSOLUBLES REACHES 1.50 PERCENT.

A REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

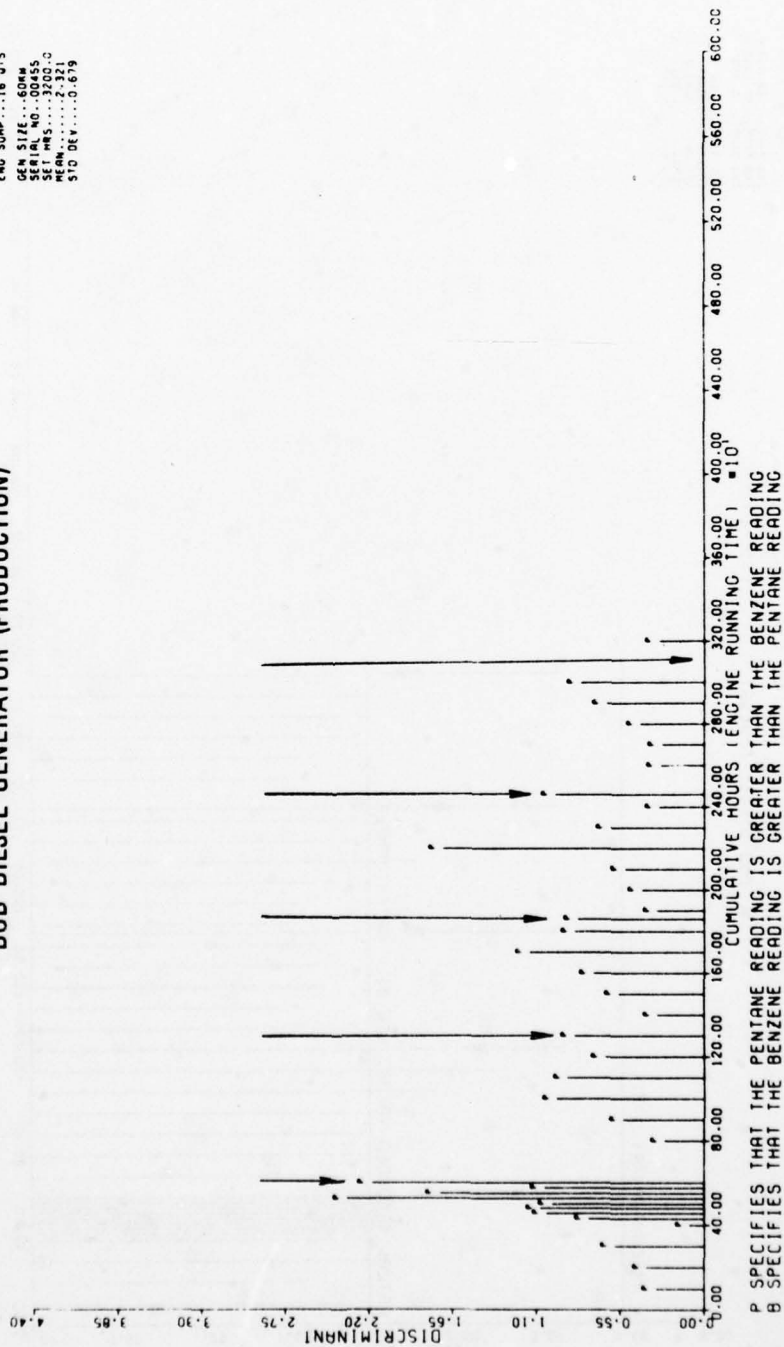
INCLUSIVE DATES
 0 FEB 74 13 NOV 74
 ENG SIZE...184 B.H.P.
 ENG NAME...AC 3500
 ENG SUMP...16 QTS
 DEN SIZE...60MM
 SERIAL NO...00455
 SET WBS...3200.0
 CEN...1.578
 STD DEV...0.46

PERCENTAGE INSOLUBLES (BENZENE) 000 DIESEL GENERATOR (PRODUCTION)



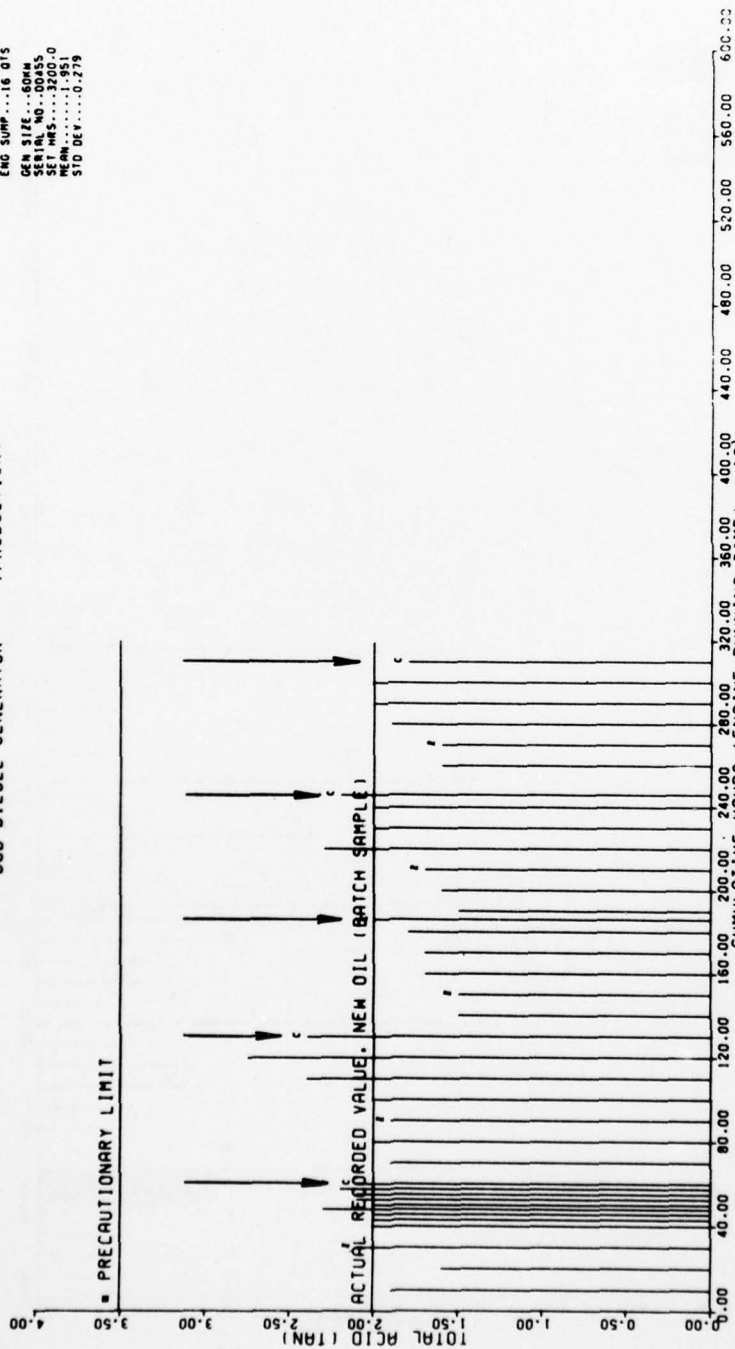
INCLUSIVE DATES
 0 FEB 74 13 NOV 74
 ENG SIZE...104 B-M-P.
 ENG MAKE...AC 3500
 ENG SUMP...16 QTS
 GEN SIZE...60MM
 SERIAL NO...00455
 REF RMS...3200.0
 STD DEV...0.679

PENTANE .VS. BENZENE
 DOD DIESEL GENERATOR (PRODUCTION)



INCLUSIVE DATES
 8 FEB 74 13 NOV 74
 ENG SIZE...184 B.M.P.
 ENG NAME...AC 3500
 ENG SUMP...16 QTS
 GEN SIZE...60MM
 SERIAL NO...00455
 REC HRS...3200.0
 MEAN...0.279
 STD DEV...0.279

TOTAL ACID IN USED OIL DDD DIESEL GENERATOR (PRODUCTION)



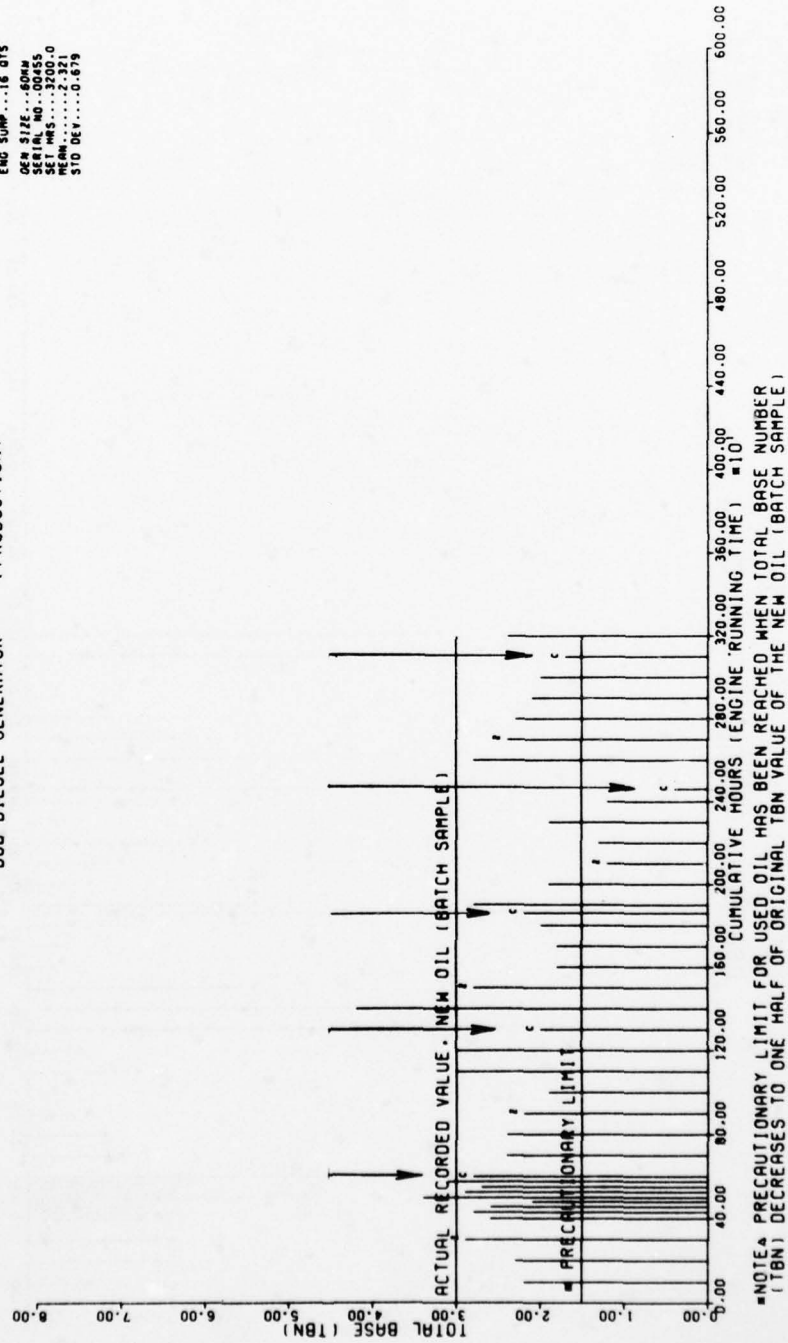
NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
 8 FEB 74 13 NOV 74
 ENG SIZE...184 B.M.P.
 ENG TIME...AC 3500
 ENG SUPP...16 875
 GEN SIZE...60MW
 GEN NO...00000
 SET PWS...3700.0
 MEAN...2.321
 STD DEV...0.679

TOTAL BASE IN USED OIL (PRODUCTION)

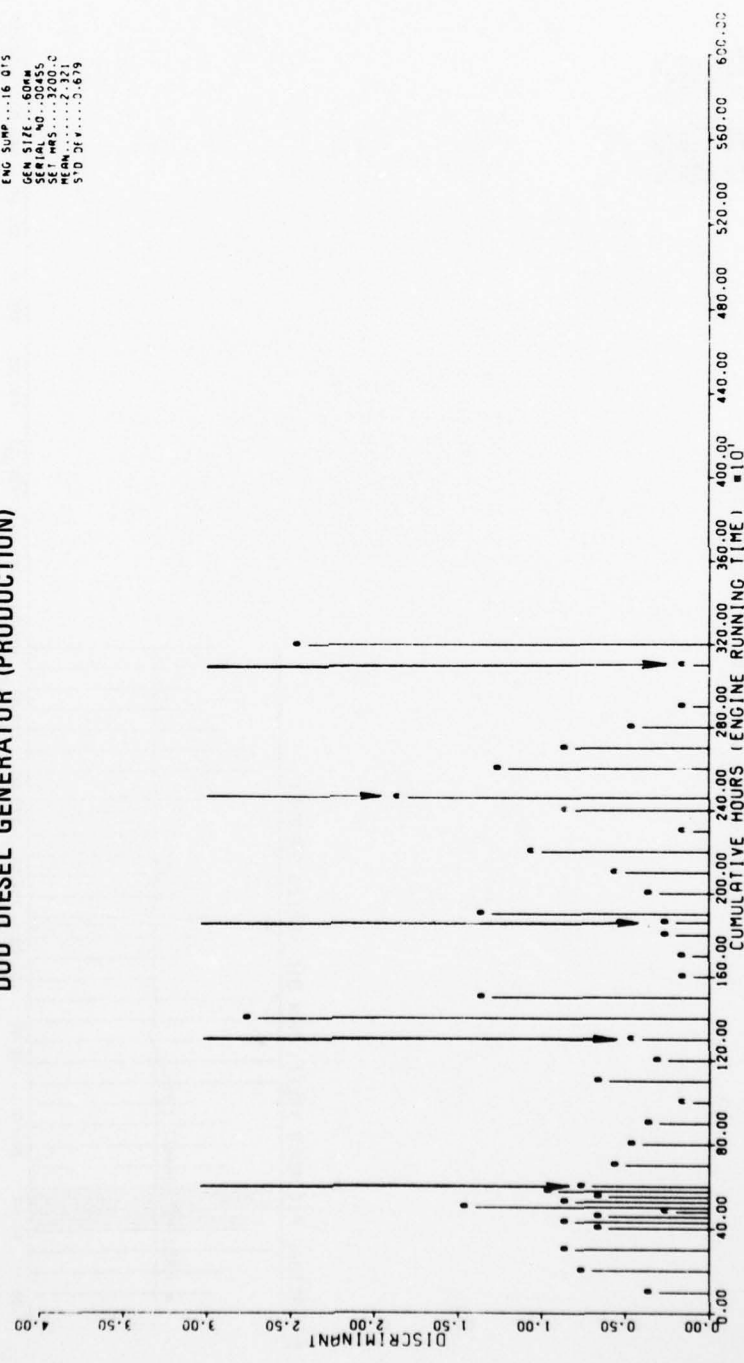
000 DIESEL GENERATOR



Z REPRESENTS THE END OF A CYCLE C REPRESENTS THE OIL CHANGE

INCLUSIVE DATES
 8 FEB 74 13 NOV 74
 ENG SIZE...104 B.M.P.
 ENG RPM...1500
 ENG SUMP...16 QTS
 GEN SIZE...60MM
 SER NO...2055
 SET PMS...3200.0
 MEAN...2.321
 STD DEV...0.679

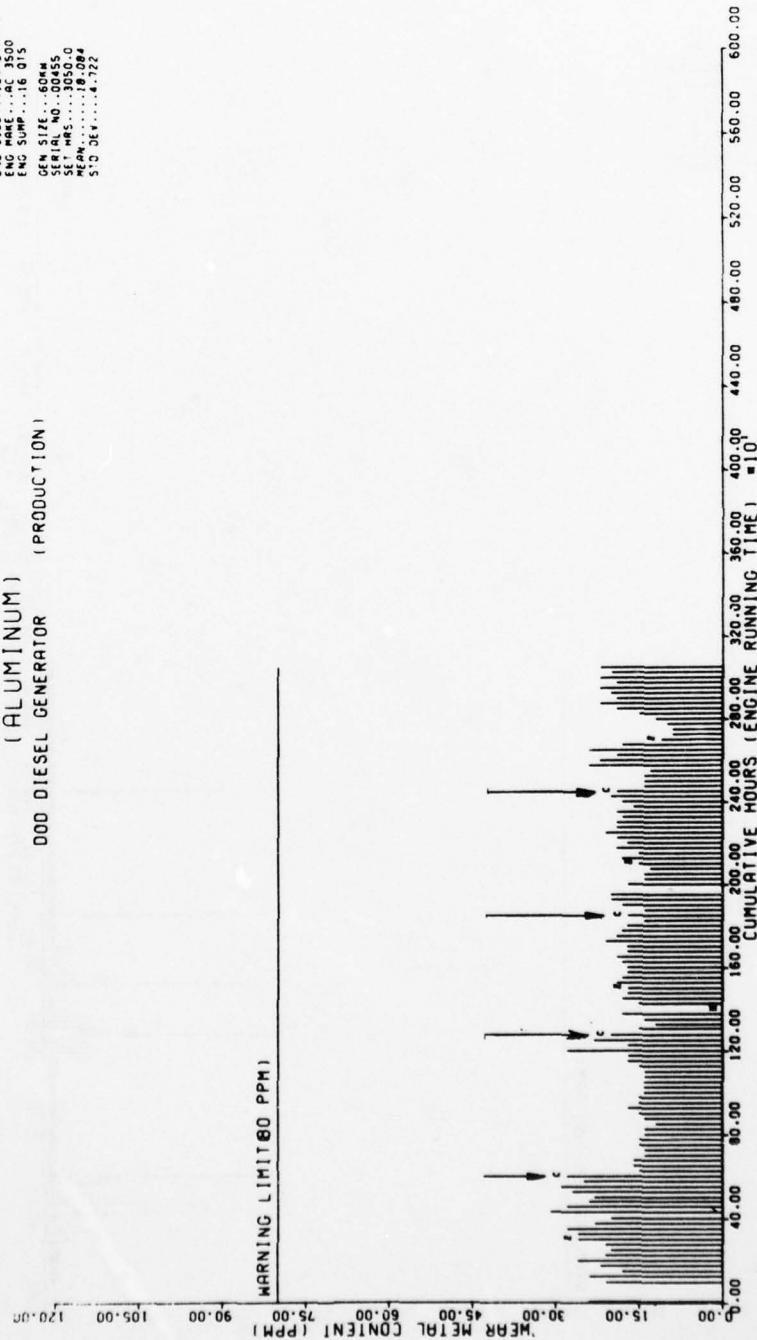
TOTAL ACID .VS. TOTAL BASE DOD DIESEL GENERATOR (PRODUCTION)



A SPECIFIES THAT THE TOTAL ACID READING IS GREATER THAN THE TOTAL BASE READING
 B SPECIFIES THAT THE TOTAL BASE READING IS GREATER THAN THE TOTAL ACID READING

WEAR METAL CONTENT IN USED OIL
(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS
(ALUMINUM)
DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
8 FEB 74 TO 19 JUL 74
ENG SIZE...184 B.H.P.
ENG MAKE...AC 3500
ENG SUMP...16 QTS
GEN SIZE...60MM
SERIAL NO...00455
DEPT...3050.0
STATION...0004
STD 084...4.722

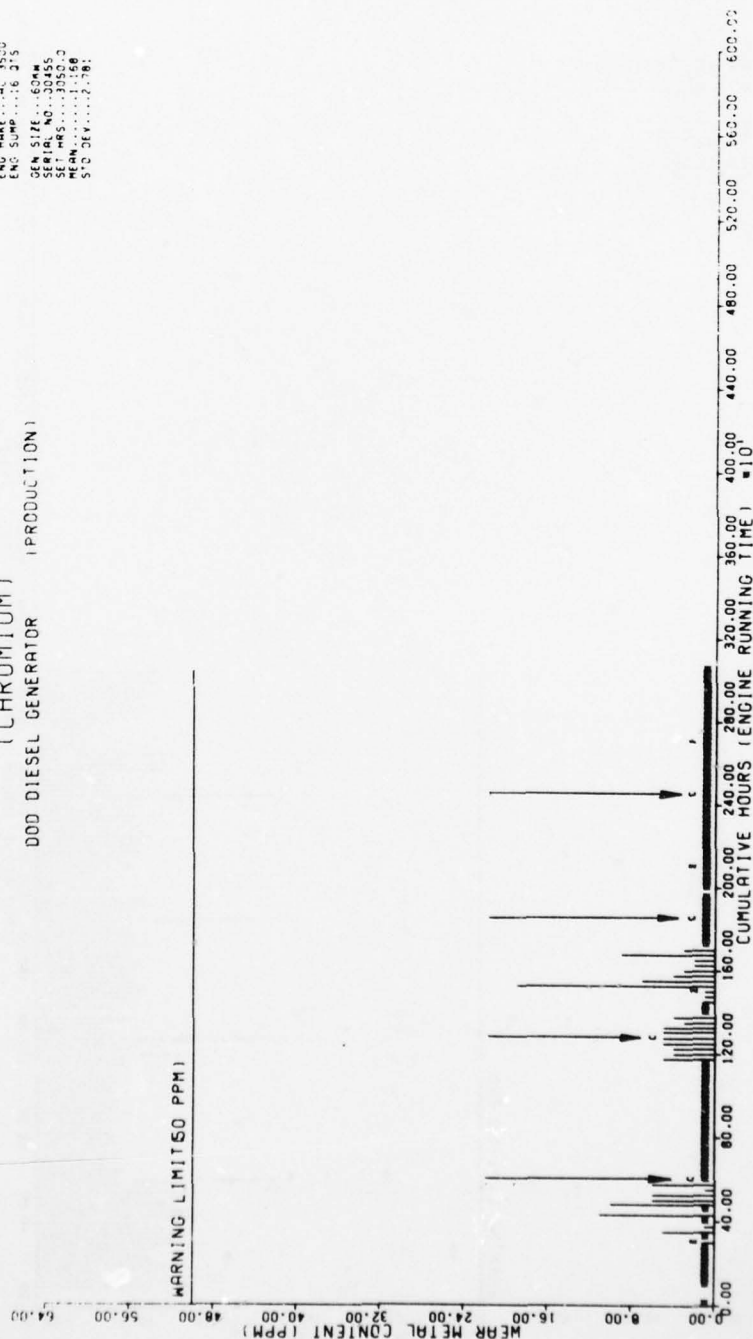


NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE); TESTS ZERO ON METAL CONTAMINANTS
c REPRESENTS THE END OF A CYCLE c REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (CHROMIUM)

DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
8 FEB 74 TO 13 JUL 74
ENG SIZE...184 B.H.P.
MAKE...AC 1550
ENG SUPP...16 275
GEN SIZE...60KW
SERIAL NO...30455
SET RES...3050.2
MEAN...1.180
STD DEV...2.180



NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

AD-A056 216

ARMY MOBILITY EQUIPMENT RESEARCH AND DEVELOPMENT COMM--ETC F/6 11/8
EXTENDED OIL-CHANGE AND OIL-FILTER-CHANGE INTERVALS FOR DOD 5- --ETC(U)
MAR 78 C R GURSKI, E FITZGIBBONS, J W DREGER

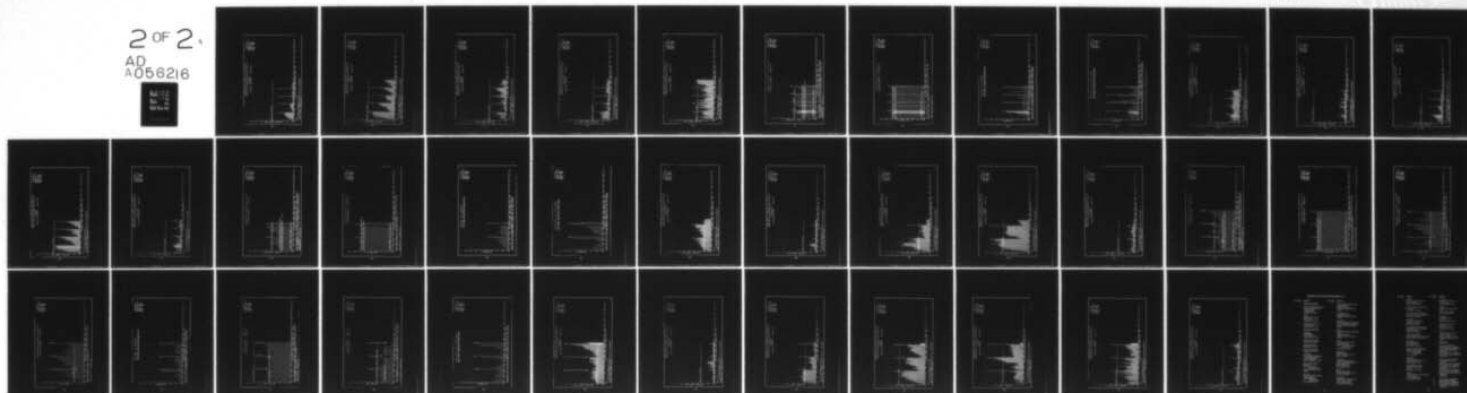
UNCLASSIFIED

NERADCOM-2234

NL

2 OF 2

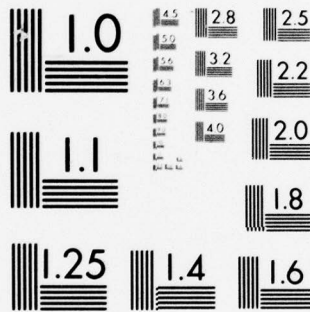
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A056216



END
DATE
FILMED

8 -78

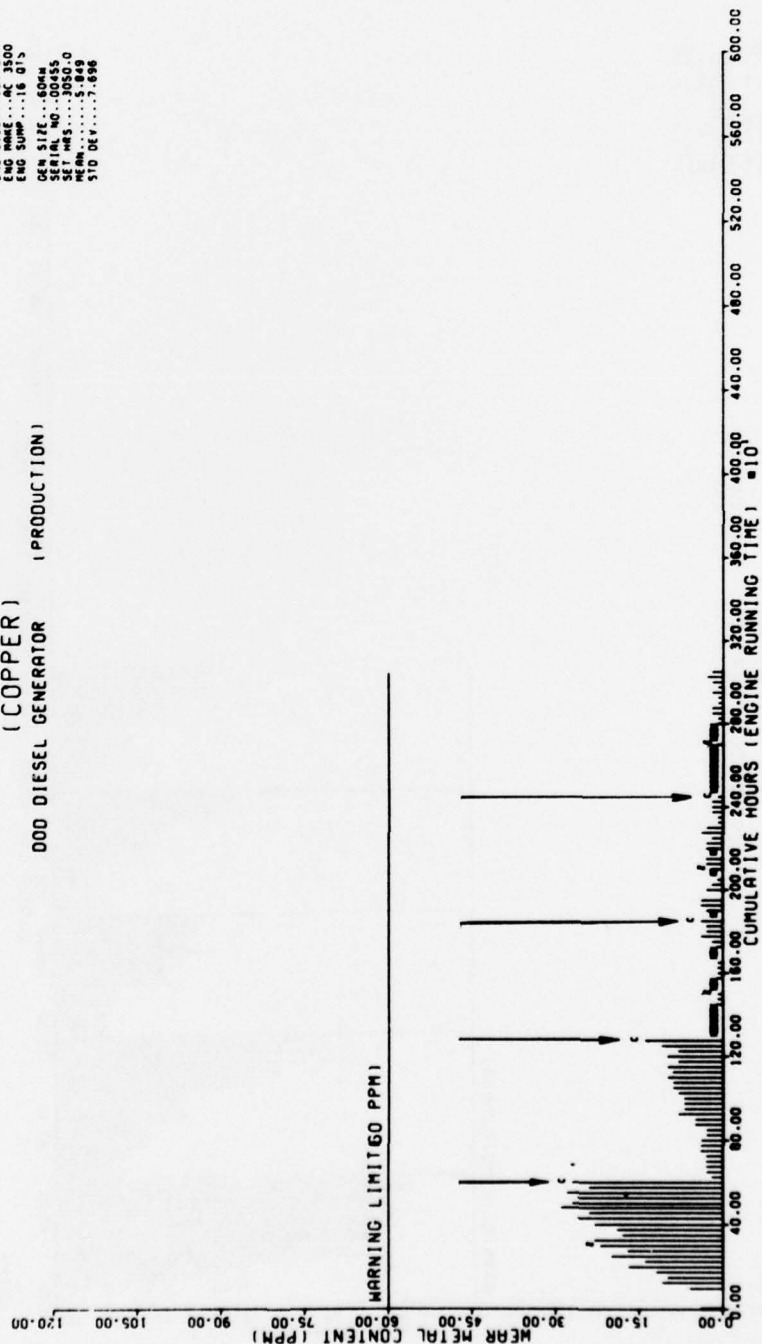
DDC



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (COPPER) 000 DIESEL GENERATOR (PRODUCTION)

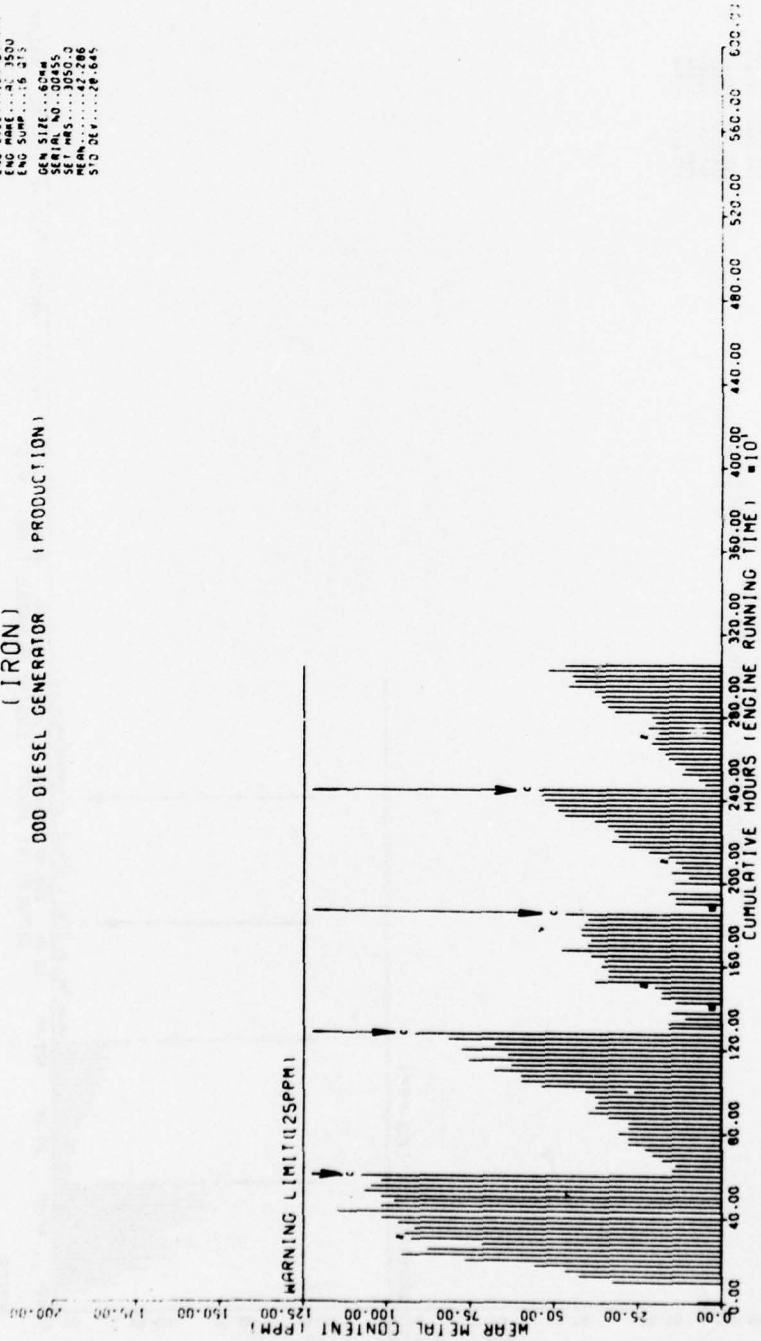
INCLUSIVE DATES
8 FEB 74 TO 19 JUL 74
ENG SIZE...184 0.00 P.
ENG MAKE...AC 3500
ENG SUMP...16 015
OEN SIZE...60MM
SERIAL NO...00455
DE MES...3050.0
TEMP...15.00
STD DEV...7.686



NOTES
- INDICATES ZERO VALUE (0.00 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
P REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL
(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS
(IRON)
000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
0 FEB 74 TO 2 MAR 74
END SIZE 100.00 PPM
END NAME 000 3500
END SUMP 000 015
GEN SIZE 100.00 PPM
SERIAL NO 00455
SET HMS 0050.0
STATION 000000
STD OIL 000000



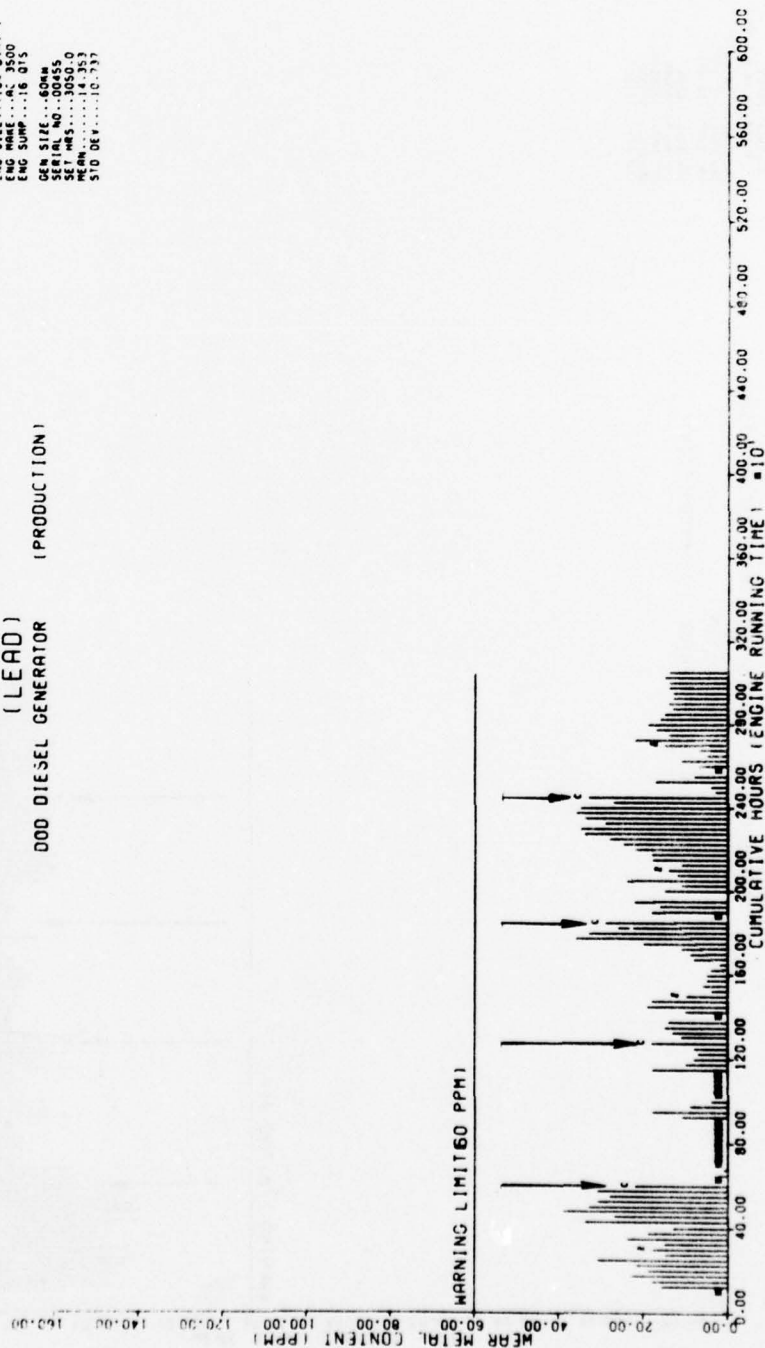
NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

DDO DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
0 FEB 74 19 00 74

ENG SIZE...104 0.00
ENG MAKE...AL 3500
ENG SURP...16 Q15

GEN SIZE...60mm
SERIAL NO...00455
SET HAS...3050.0
MEAN...14.353
STD DEV...16.737



NOTES

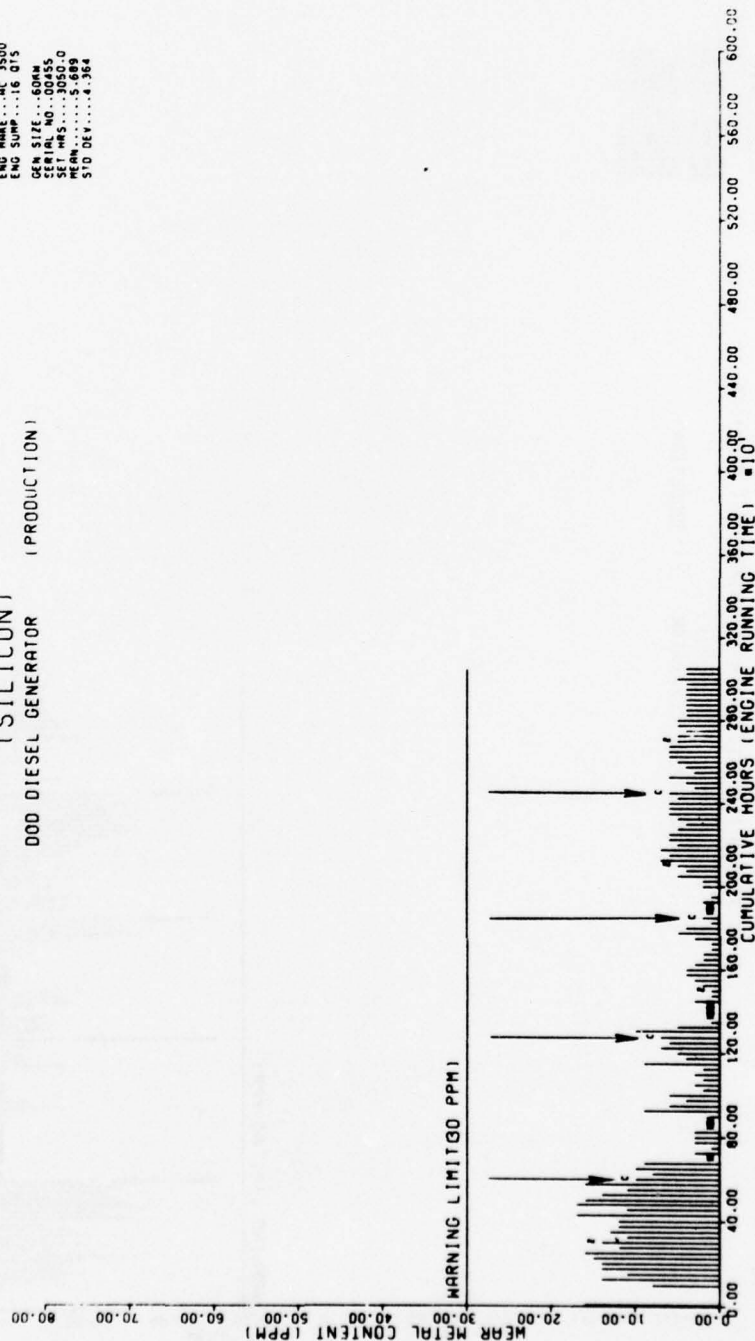
■ - INDICATES ZERO VALUE (0 PPM)

NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

REMARKS: THE END OF A CYCLE CONTAMINANTS ARE ALL CORRECT

WEAR METAL CONTENT IN USED OIL
(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS
(SILICON)
DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
0 FEB 74 TO 19 JUL 74
END SIZE...104 B.M.P.
END MAKE...AC 3500
END SUMP...16 QTS
GEN SIZE...50MM
SERIAL NO...00455
SET HRS...3050.0
TEMP...5.68
STD DEV...4.384

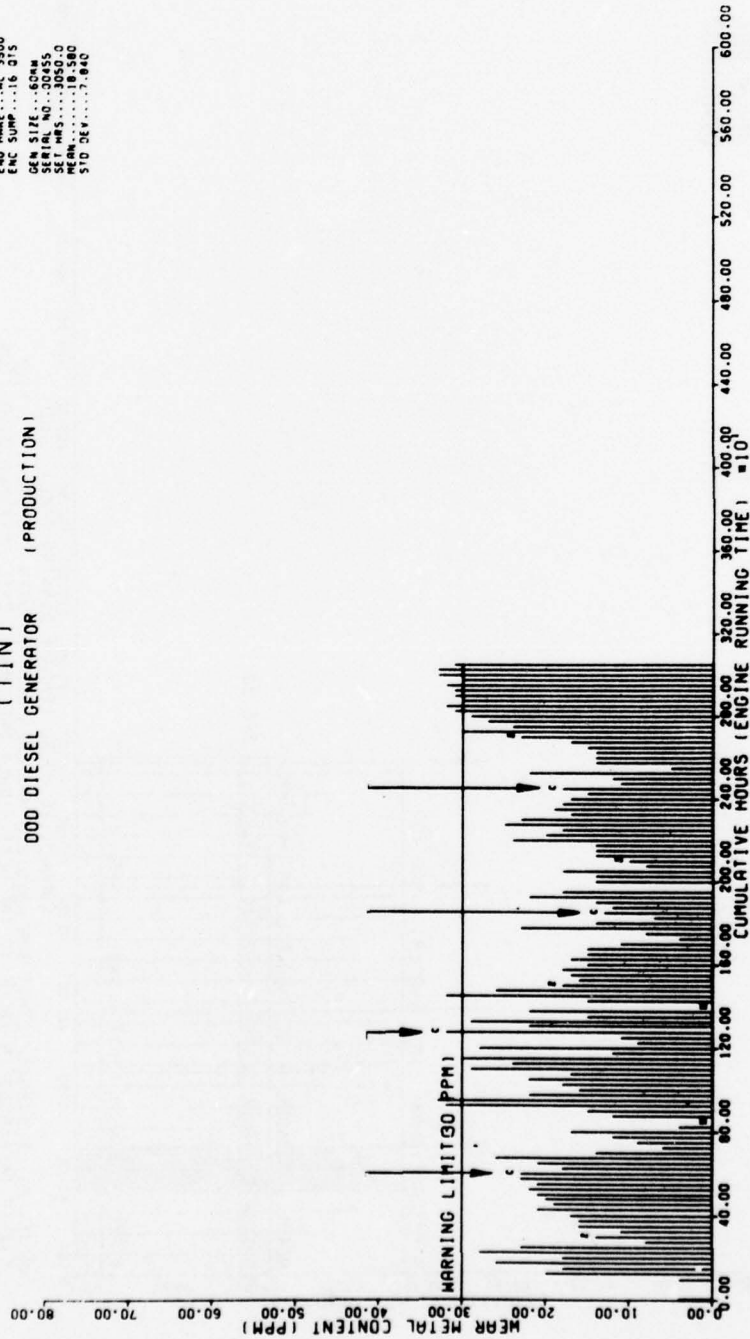


NOTES
a - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
b REPRESENTS THE END OF A CYCLE c REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (TIN)

000 DIESEL GENERATOR (PRODUCTION)

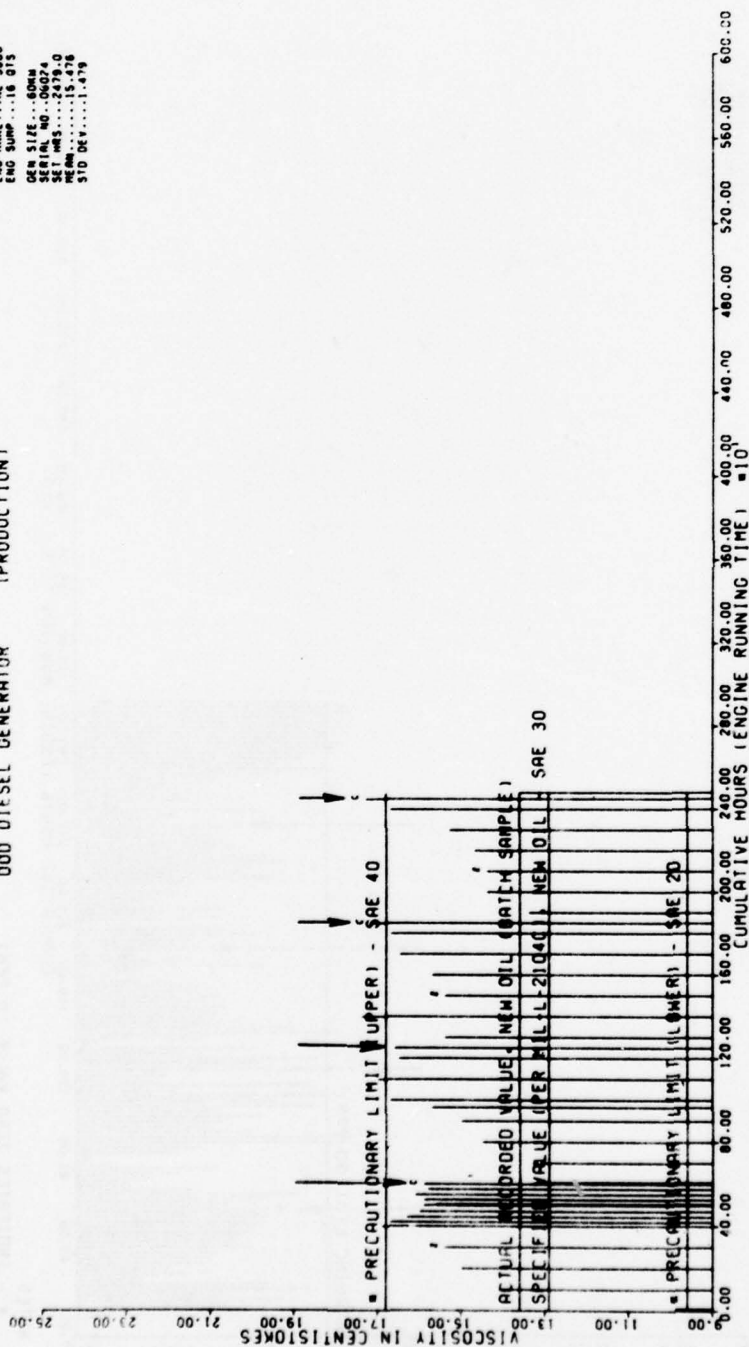
INCLUSIVE DATES
0 10 74 19 2 74
END SIZE...104 B.A.P.
END TIME...1500
END SUPP...16 015
GEN SIZE...60WAS
GEN WAB...30WAS
SET HAS...3050.0
MEAN...18.580
STD DEV...7.840



NOTES
a - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
c REPRESENTS THE END OF A CYCLE c REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
9 FEB 74 20 NOV 74
ENG SIZE...184 B.H.P.
ENG NAME...MC 3500
ENG SUMP...16 QTS
GEN SIZE...60MM
SERIAL NO...08024
SET WBS...2479.0
MEMO...15.476
STD DEV...1.476

VISCOSITY OF USED OIL AT 210 F 000 DIESEL GENERATOR (PRODUCTION)



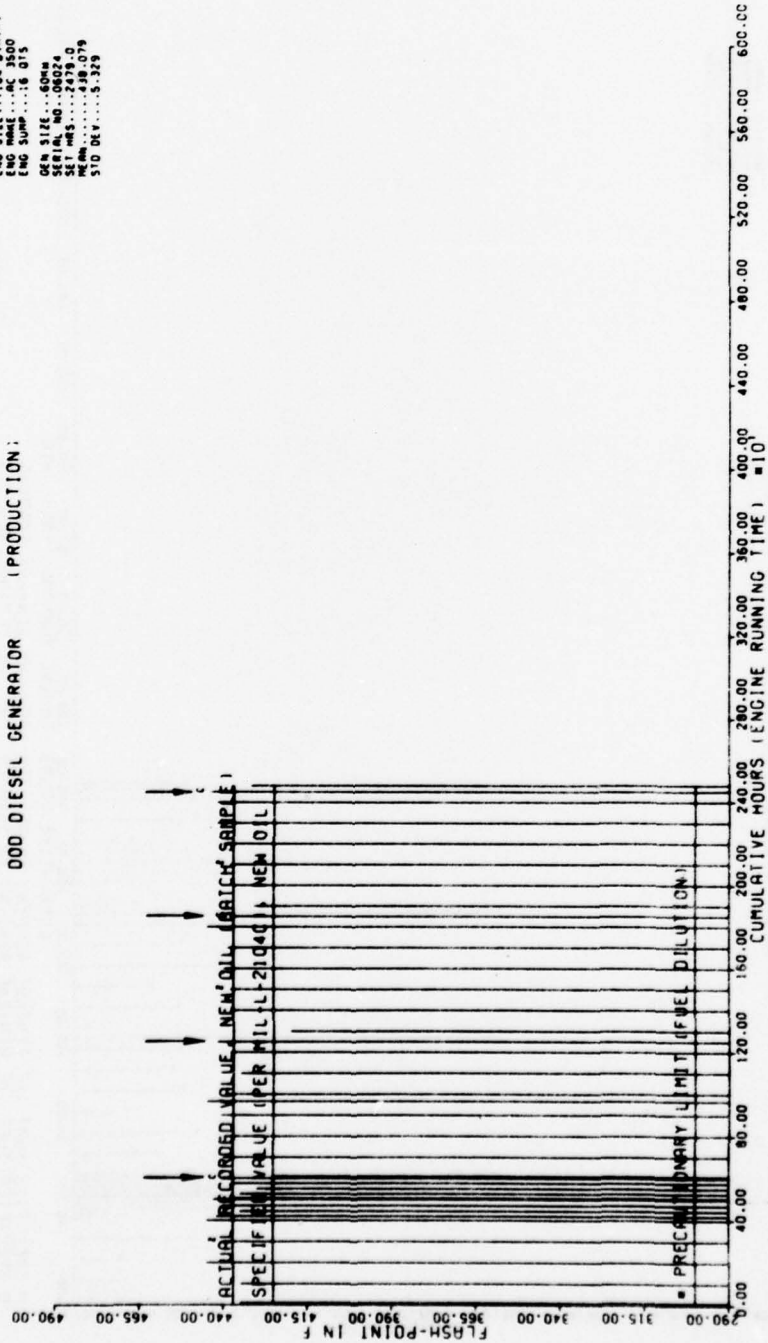
NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210 F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).

SAE GRADE LIMITS ARE BASED ON OIL COMPOSITION.

INCLUSIVE DATES
 8 FEB 74 20 NOV 74
 ENG SIZE...184 B.M.P.
 ENG MAKE...AC 3500
 ENG SUMP...16 OTS
 OEM SIZE...60MM
 SERIAL NO...08024
 SET RES...2479.0
 CUMULATIVE...192.079
 STD DEV...5.329

FLASH-POINT OF USED OIL (F)

000 DIESEL GENERATOR (PRODUCTION)

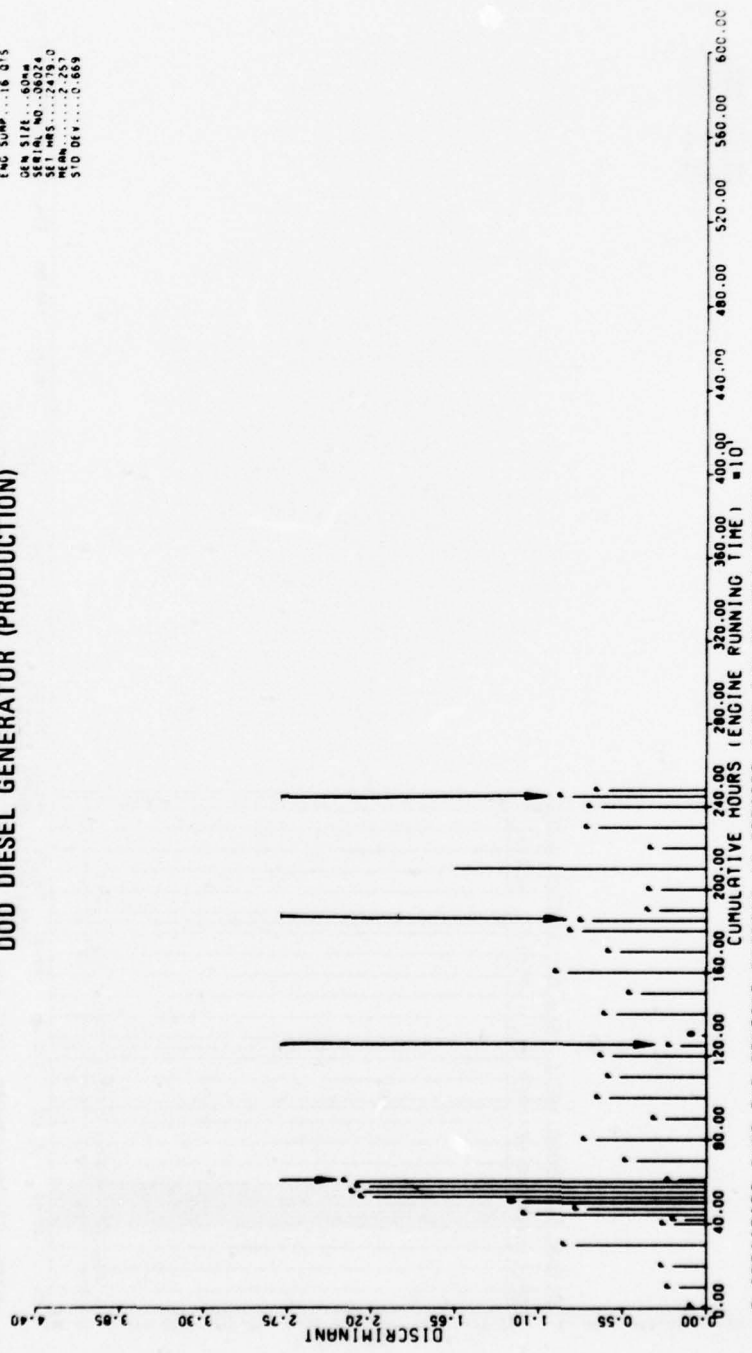


*NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

1 REPRESENTS THE END OF A CYCLE 2 REPRESENTS THE END OF A CYCLE

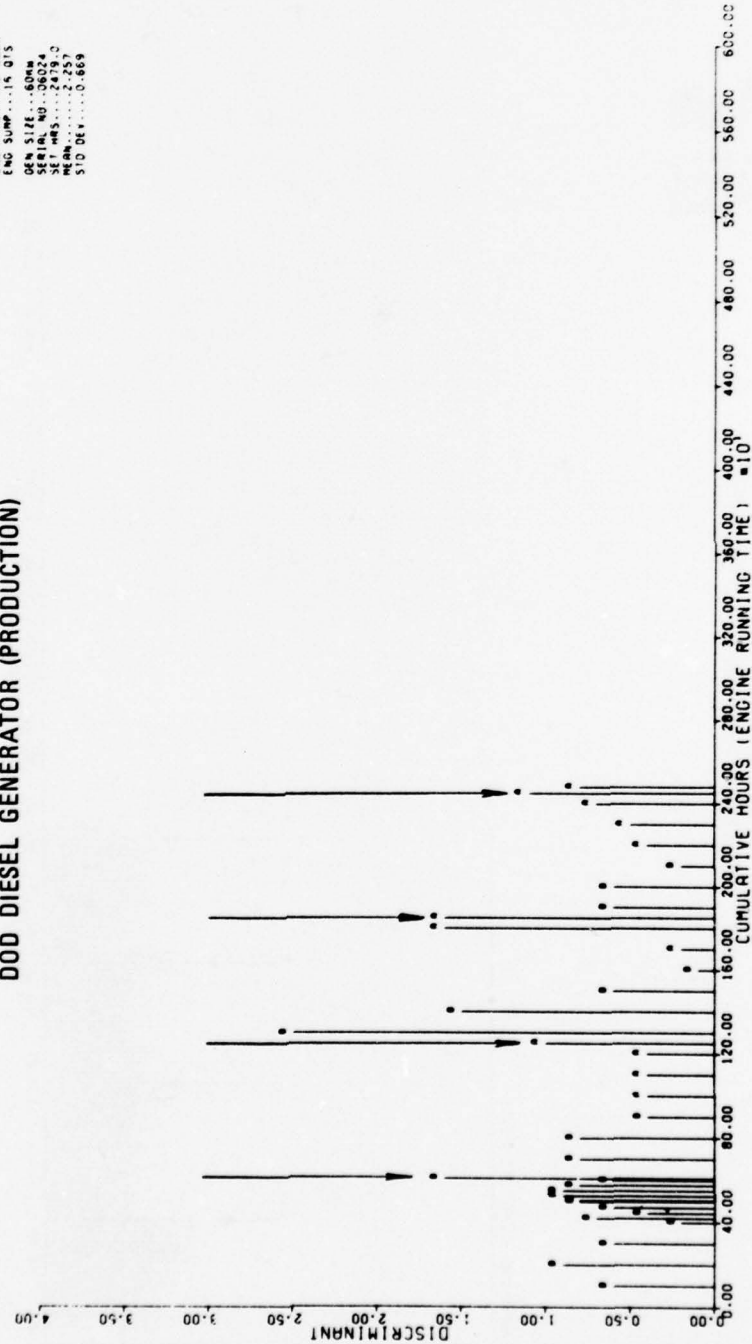
INCLUSIVE DATES
 0 FEB 74 TO NOV 74
 END SIZE...104 B-M-P
 END NAME...AC 3503
 END SUMP...16 QTS
 GEN SIZE...60mm
 SERIAL NO...00024
 SENSITIVITY...2.5%
 MEAN...0.669
 STD DEV...0.669

PENTANE .VS. BENZENE DOD DIESEL GENERATOR (PRODUCTION)



INCLUSIVE DATES
 0 FEB 74 TO NOV 74
 END SIZE...184.8...P.
 END TIME...15.000
 END SUM...15.075
 DEN SIZE...6000
 DEN SUM...15.075
 SET PHS...2.257
 MEAN...2.257
 STD DEV...0.669

TOTAL ACID .VS. TOTAL BASE
 DOD DIESEL GENERATOR (PRODUCTION)



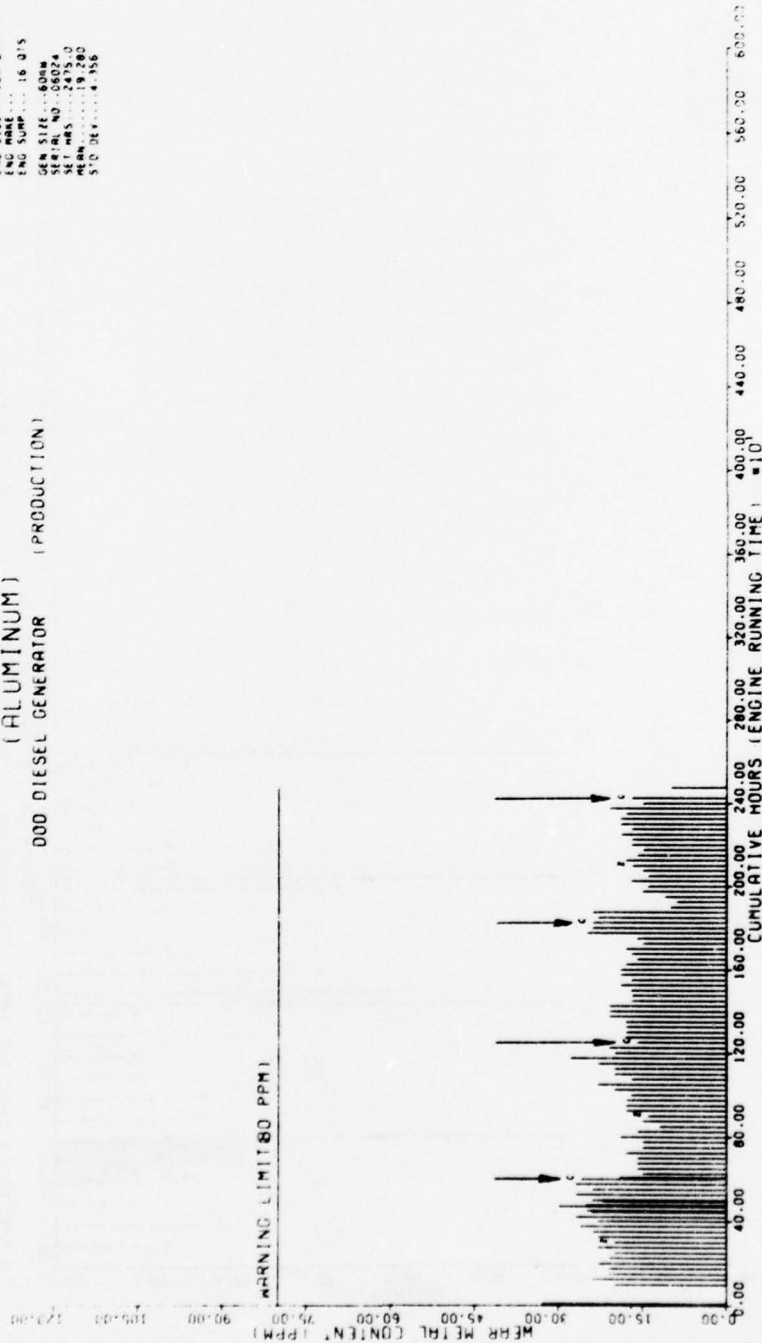
WEAR METAL CONTENT IN USED OIL

(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(ALUMINUM)

000 DIESEL GENERATOR (PRODUCTION)

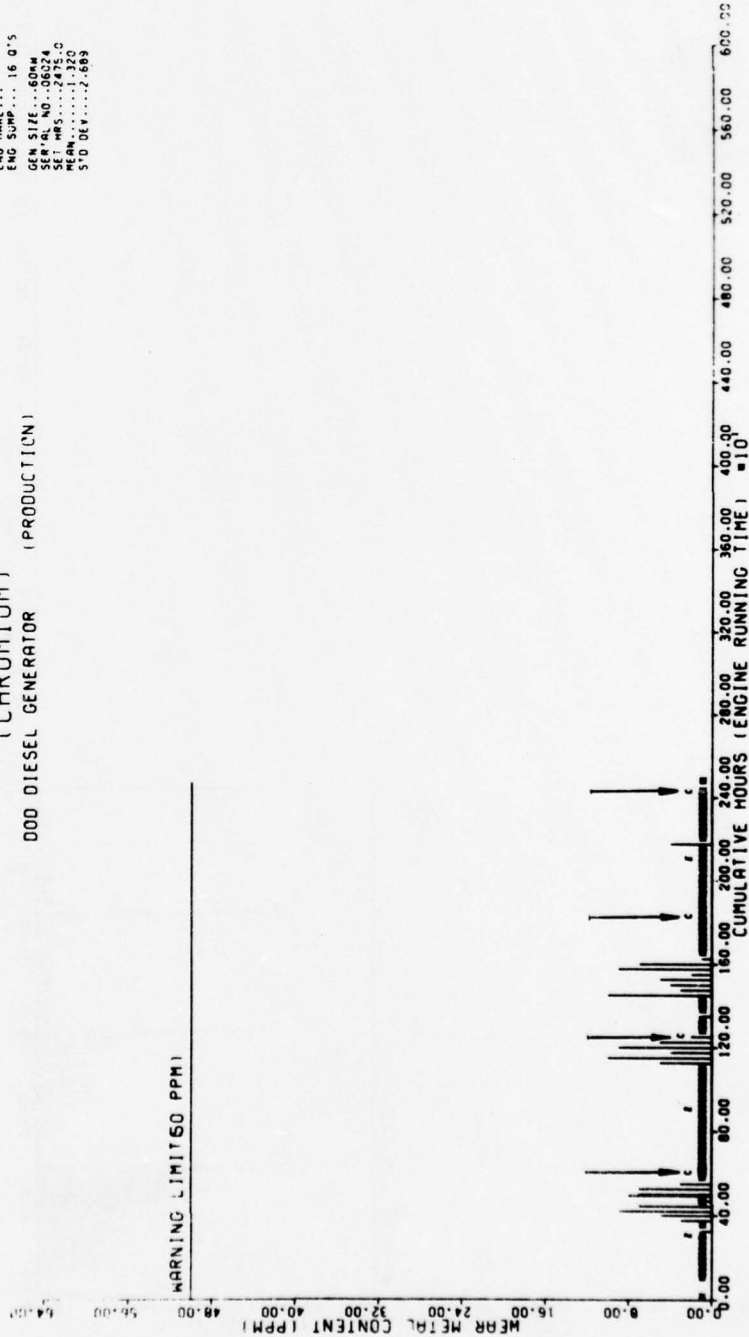
INCLUSIVE DATES
0 FEB 74 TO 4 JUL 74
END SIZE 104.0 - P
END MAKE
END SUPP 16 QTS
GEN SIZE 600W
SERIAL NO 00024
REMARKS 2475.0
ANALYST 4158
STD DEVIATION 4.158



NOTES
* INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
P REPRESENTS THE END OF A CYCLE C REPRESENTS THE OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (CHROMIUM) DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
0 FEB 74 16 4.3 74
END SIZE...184 B...P.
END MAKE...
END SUMP... 16 O'S
GEN SIZE...60MM
SERIAL NO...06024
TEST NO...28320
MEAN...2.689
STD DEV...2.689



NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
* DENOTES THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

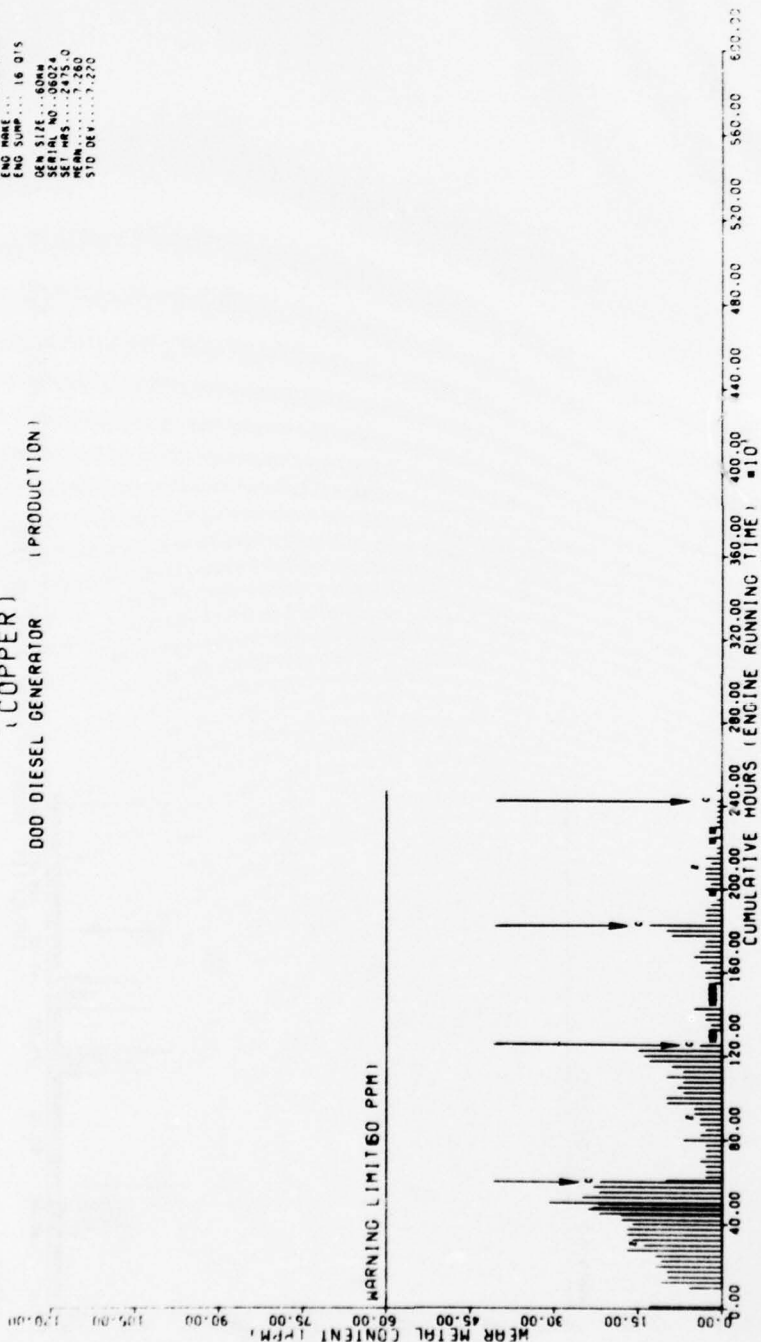
WEAR METAL CONTENT IN USED OIL

(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(COPPER)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
8 FEB 74 TO 16 JUL 74
END SIZE...184 B.M.P.
END MAKE...
END SUMP...16 DTS
OEN SIZE...60mm
SERIAL NO...06024
SET. HRS...2475.0
MID. HRS...1600
STD. DEVIATION...7.220

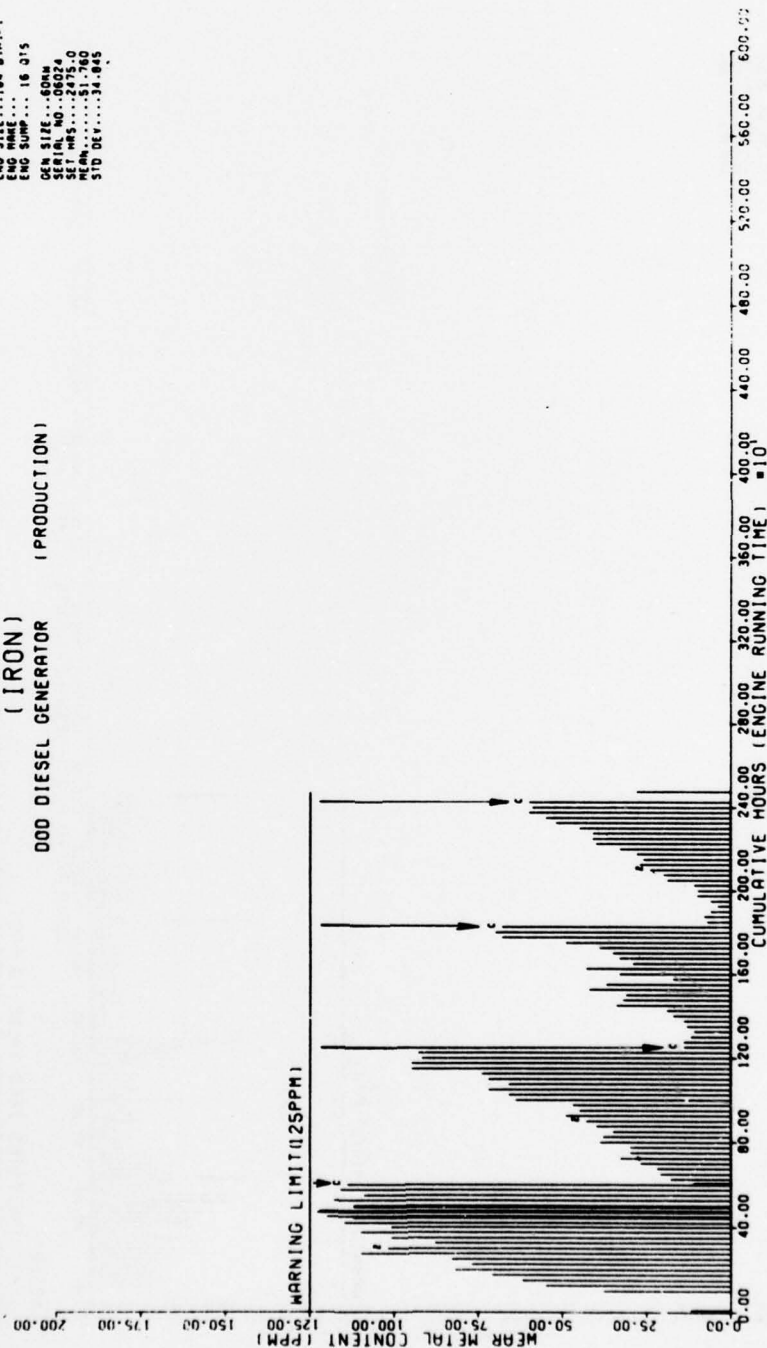


NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (IRON)

000 DIESEL GENERATOR (PRODUCTION)

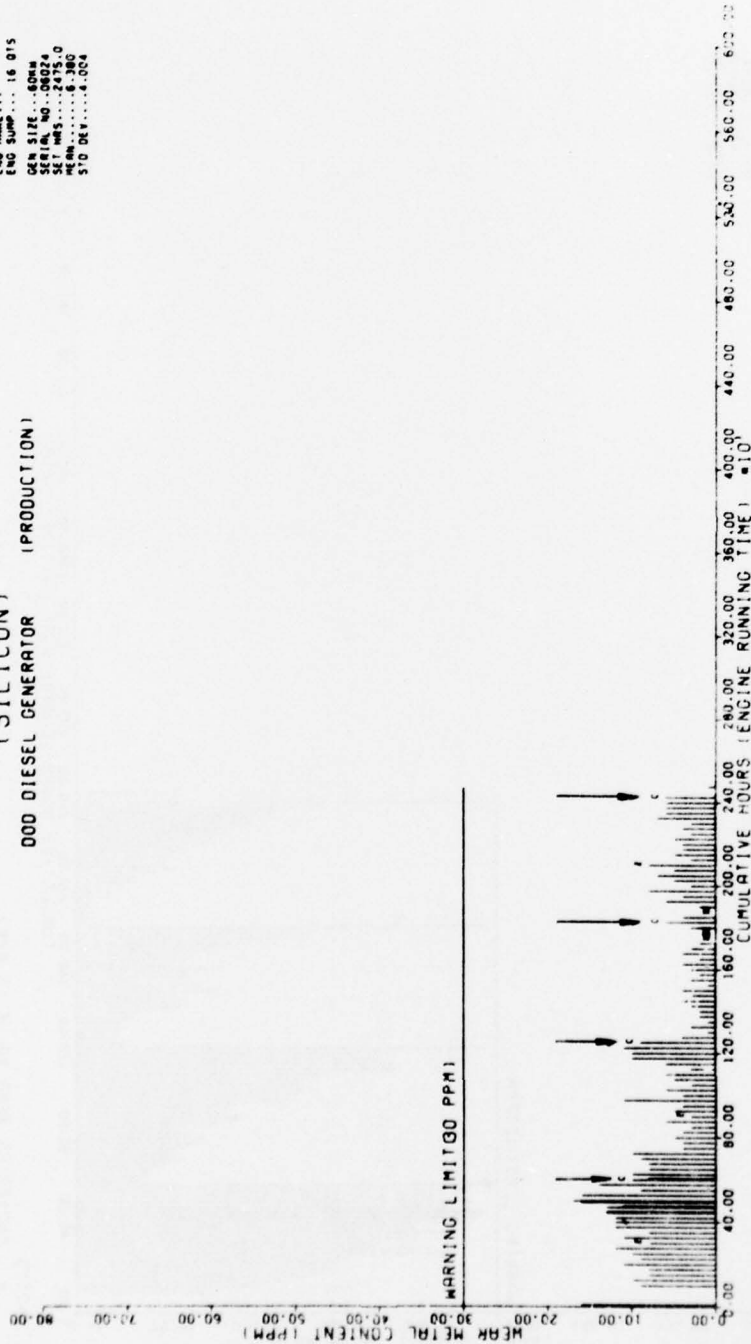
INCLUSIVE DATES
8 FEB 74 16 AUG 74
END SIZE...184 8.00 P.
END NAME...
END SUMP... 16 QTS
OIL SIZE...600W
SERIAL NO...06024
SET NRS...2475.0
MEAN...51.760
STD DEV...34.845



NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (SILICON) 000 DIESEL GENERATOR (PRODUCTION)

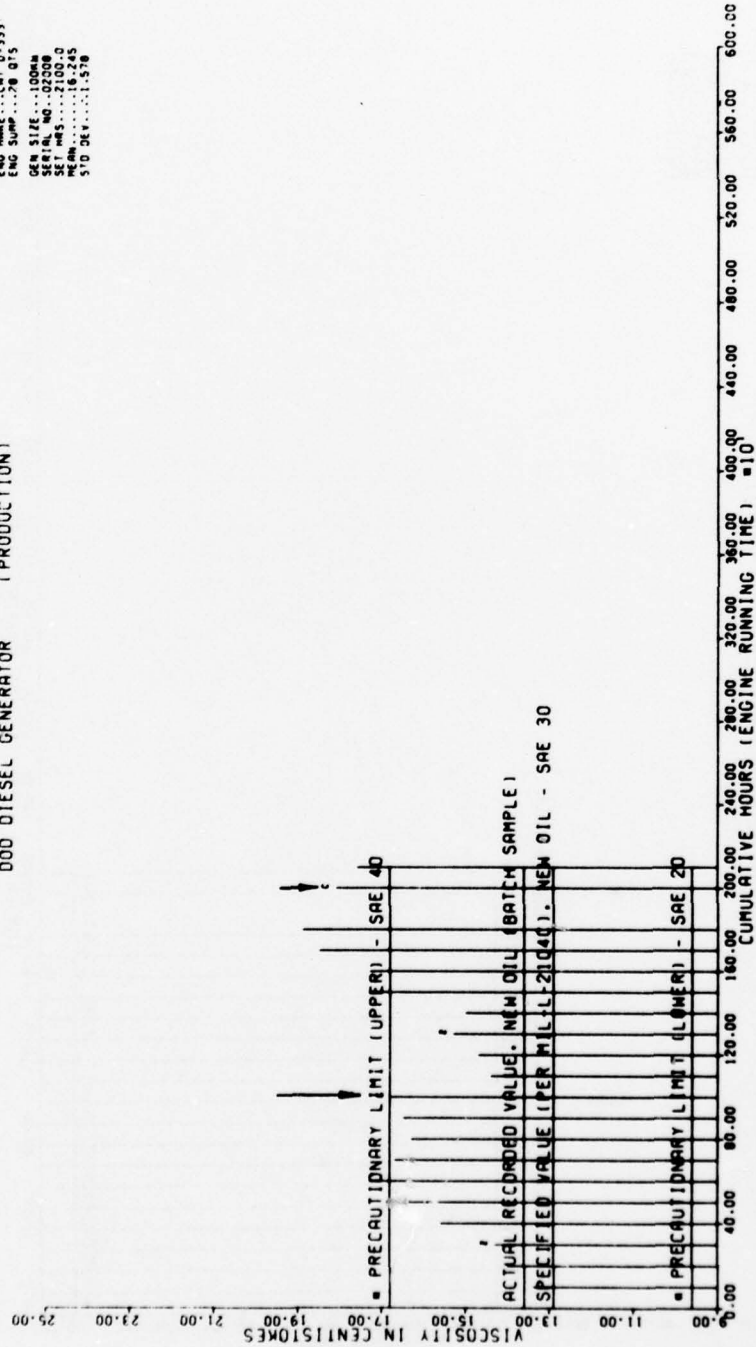
INCLUSIVE DATES
0 FEB 74 TO 0 JUL 74
ENG SIZE 1800 B.H.P.
ENG MAKE
ENG SUMP 16 QTS
GEN SIZE 600W
SERIAL NO 08024
SET NOS 2475.0
MEAN 8.380
STD DEV 4.004



NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F INDICATES THE END OF A CYCLE C INDICATES THE END OF A RUN

VISCOSITY OF USED OIL AT 210 F DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
 9 JULY 74 - 8 NOV 74
 ENG SIZE...275 B-M-P
 ENG TYPE...D-333
 ENG SUMP...28 Q15
 GEN SIZE...100kW
 SET NO...2100-0
 SET PMS...18-245
 MEAN...1.578
 STD DEV...1.578

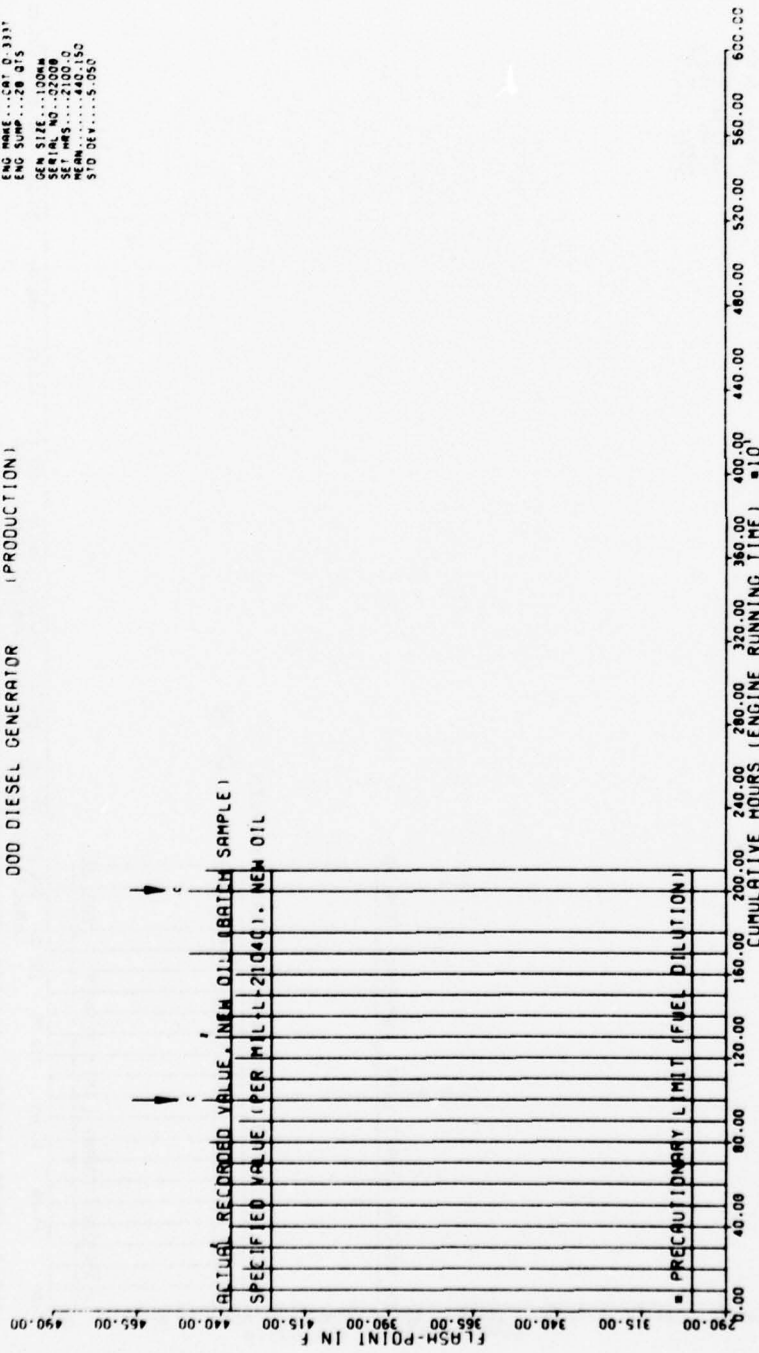


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL ECONOMY LIMIT).

REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
 3 JULY 74 8 NOV 74
 END SIZE...279 8-1/2"
 END NAME...CAT 0.3331
 END SUM...28 QTS
 GEN SIZE...100MM
 SERIAL NO...22009
 SET NO...440.0
 MEAN...440.150
 STD DEV...5.050

FLASH-POINT OF USED OIL (F) 000 DIESEL GENERATOR (PRODUCTION)

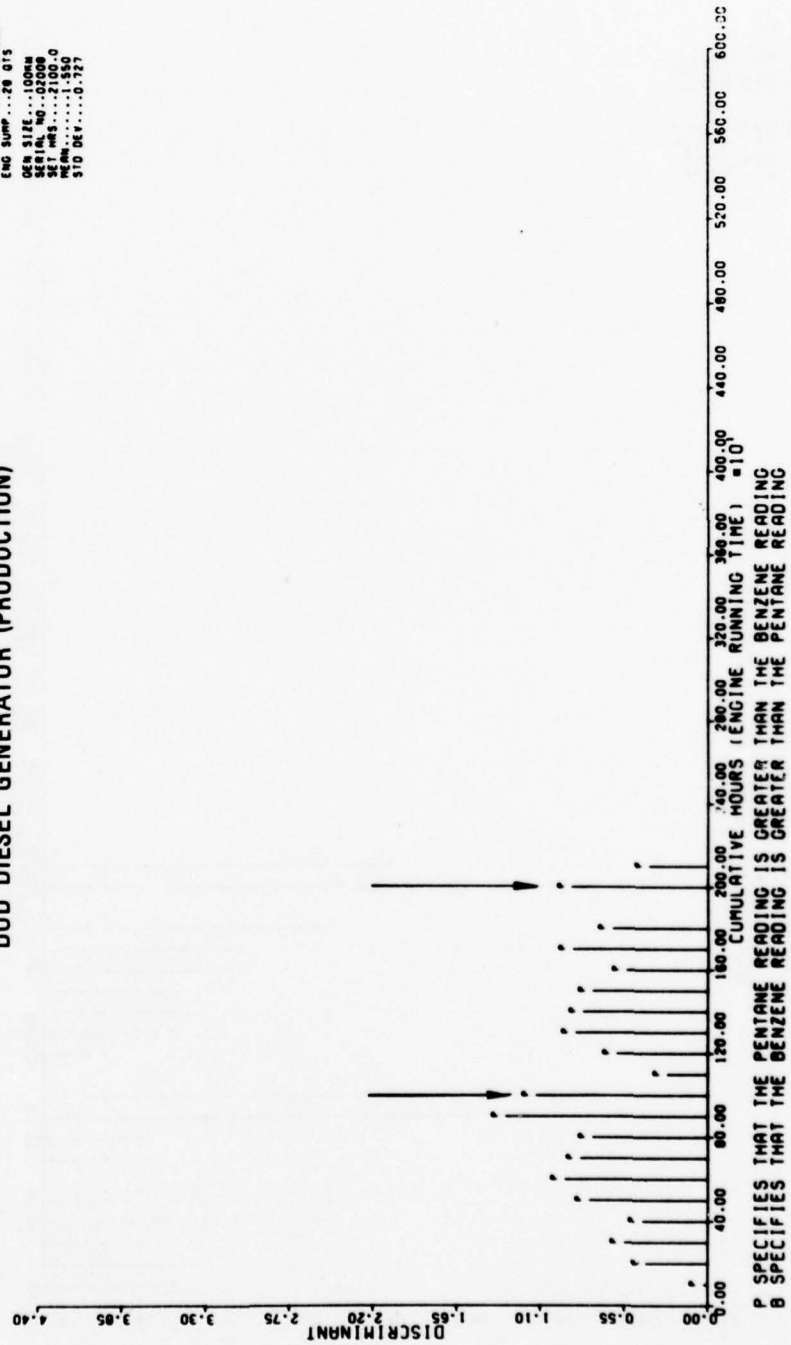


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

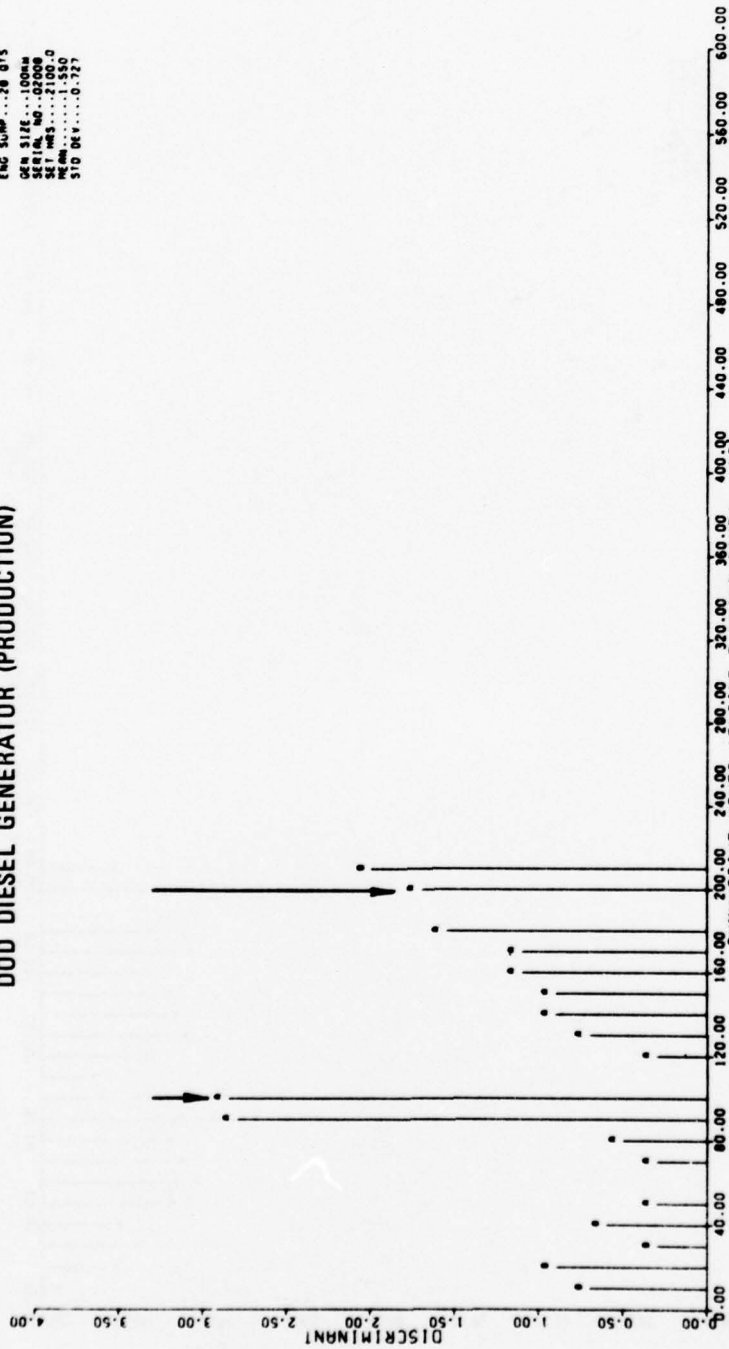
INCLUSIVE DATES
 3 JULY 74 8 NOV 74
 ENG SIZE...279 B-M-P
 ENG NAME...CAT 0-3337
 ENG SUPP...28 615
 GEN SIZE...100MM
 GEN NO...02500
 SET NO...1-550
 MEAN...1.550
 STD DEV...0.127

PENTANE .VS. BENZENE DOD DIESEL GENERATOR (PRODUCTION)



INCLUSIVE DATES
 3 JULY 74 8 NOV 74
 ENG SIZE...279 B-H-P-
 ENG NAME...CAT 0-3331
 ENG SUMP...28 015
 GEN SIZE...100kW
 SERIAL NO...02000
 ST. HRS...11500.0
 WGT...1.550
 STD DEV...0.727

TOTAL ACID .VS. TOTAL BASE
 DOD DIESEL GENERATOR (PRODUCTION)



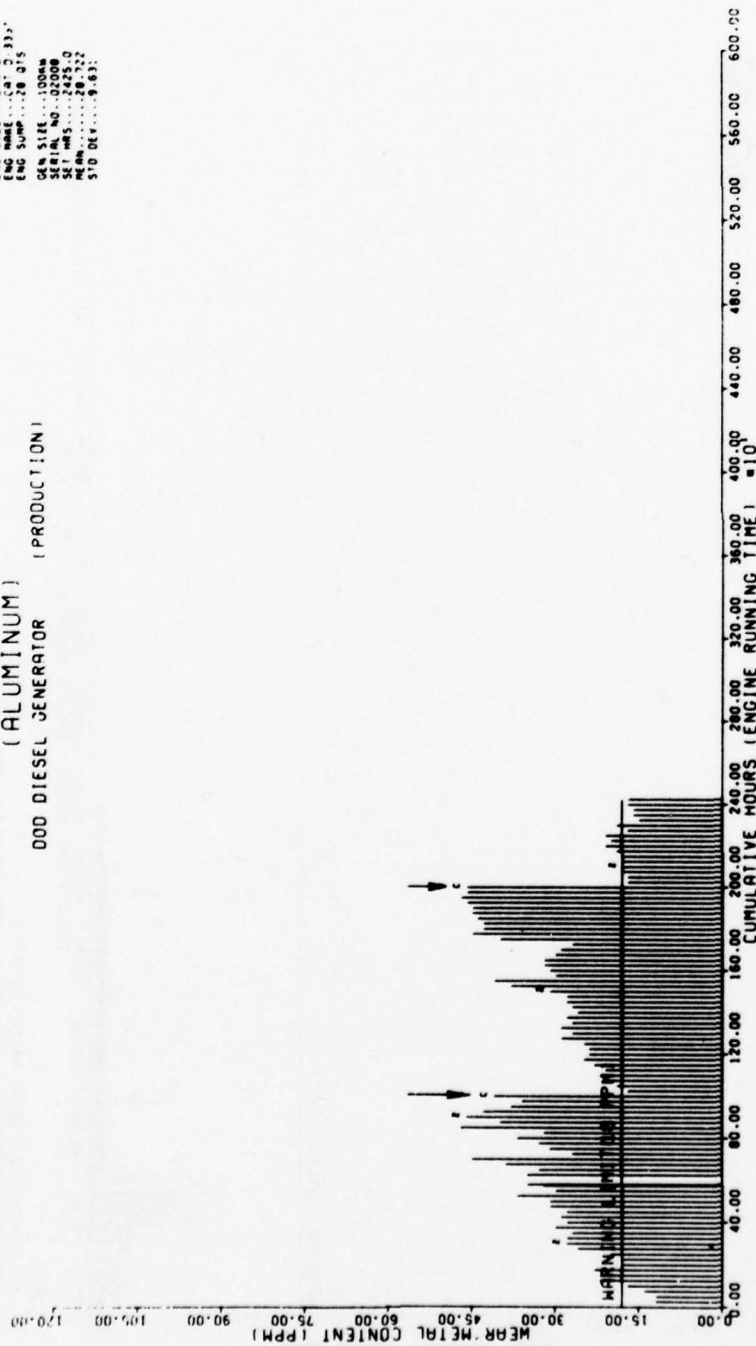
A SPECIFIES THAT THE TOTAL ACID READING IS GREATER THAN THE TOTAL BASE READING
 B SPECIFIES THAT THE TOTAL BASE READING IS GREATER THAN THE TOTAL ACID READING

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(ALUMINUM)

000 DIESEL GENERATOR (PRODUCTION)

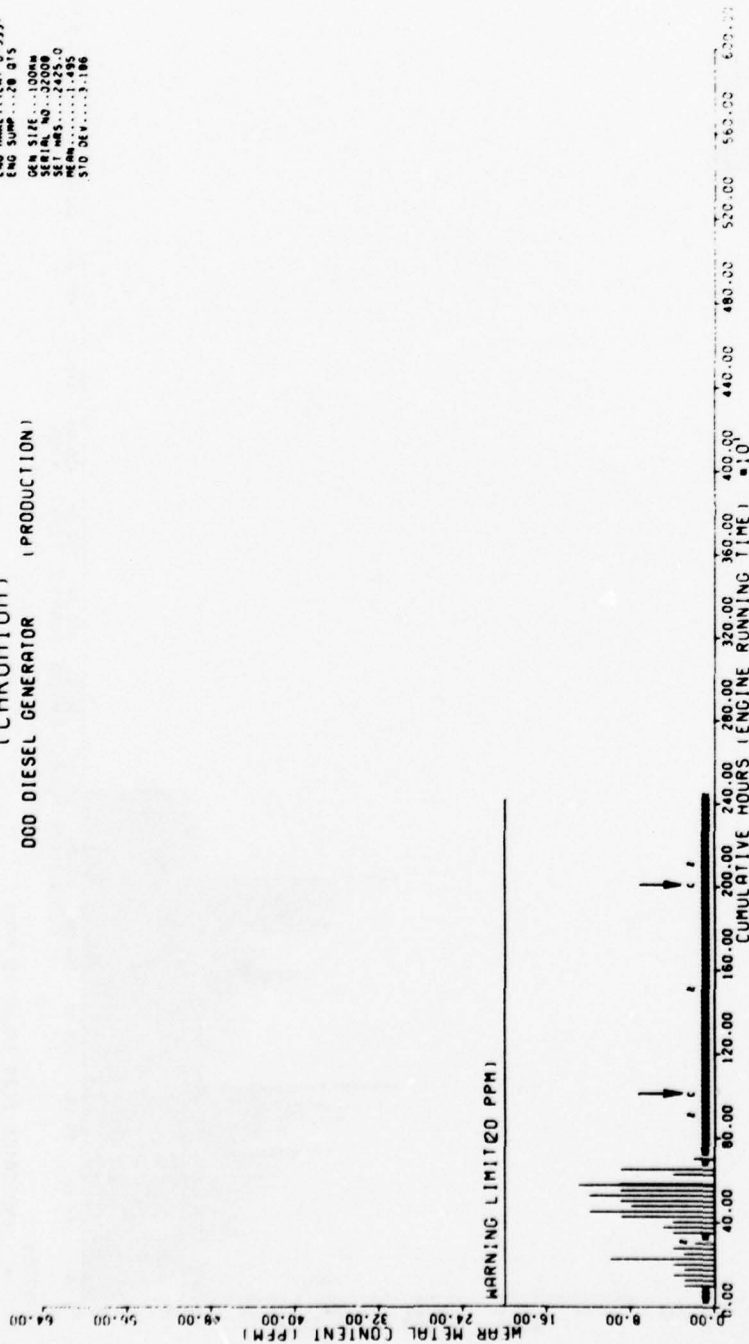
INCLUSIVE DATES
27 JUNE 74 TO 2 JUL 74
ENG SIZE 270 B HP
ENG MAKE CAT 2 337
ENG SUMP 28 QTS
GEN SIZE 1000W
SERIAL NO 02008
SET NOS 2425-0
MEAN 28.722
STD DEV 9.633



NOTES
INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (CHROMIUM) DDO DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
27 JUNE 74 - 19 AUG 74
ENG SIZE...279 B.M.P.
ENG MAKE...CAT D 333
ENG SUMP...28 Q'S
OEN SIZE...100MM
SERIAL NO...32000
SET MTS...2425.0
CUMULATIVE HOURS...1895
STD DEV...1.180

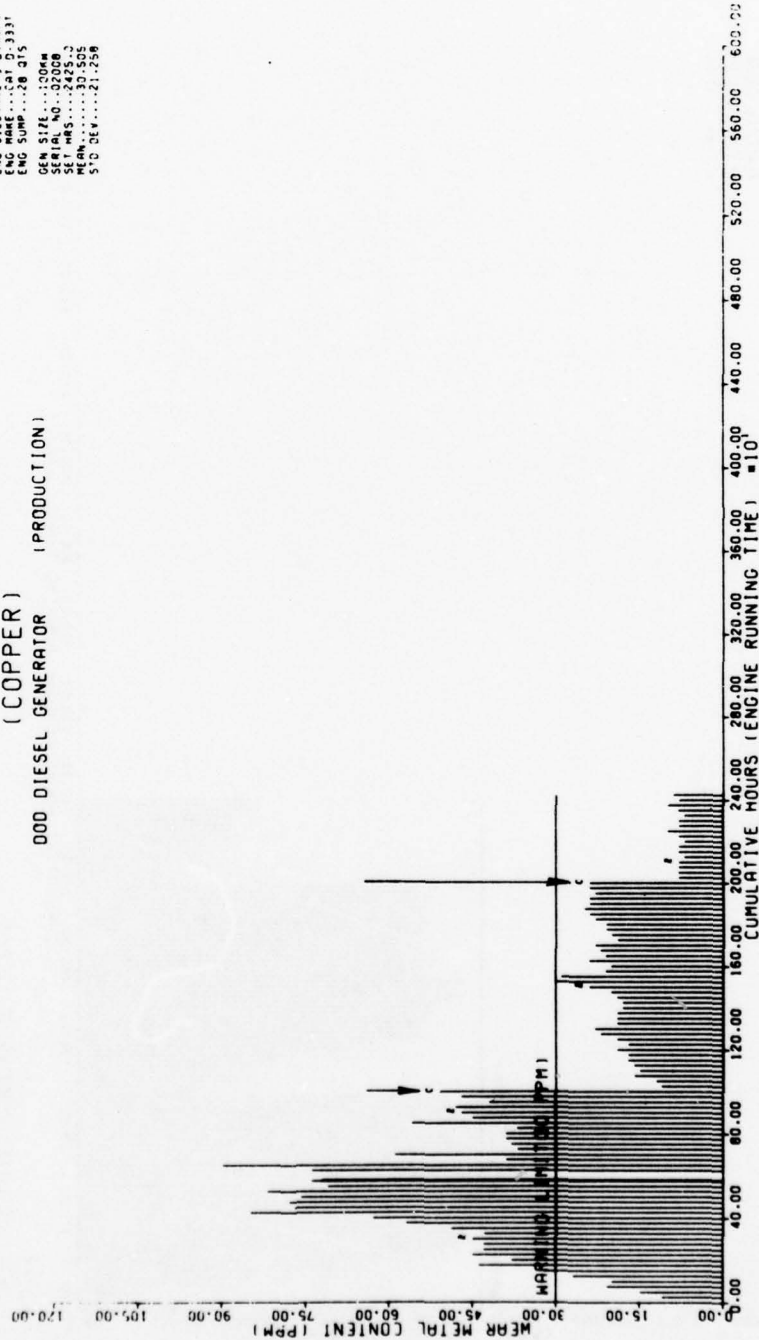


NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (COPPER)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
27 JAN 74 - 3 JUL 74
ENG SIZE... 27 8.157
ENG SUMP... 28 3.337
ENG SUMP... 28 3.75
GEN SIZE... 1004
SERIAL NO... 02008
SET NOS... 2425-3
MEAN... 30.505
STD DEV... 21.258



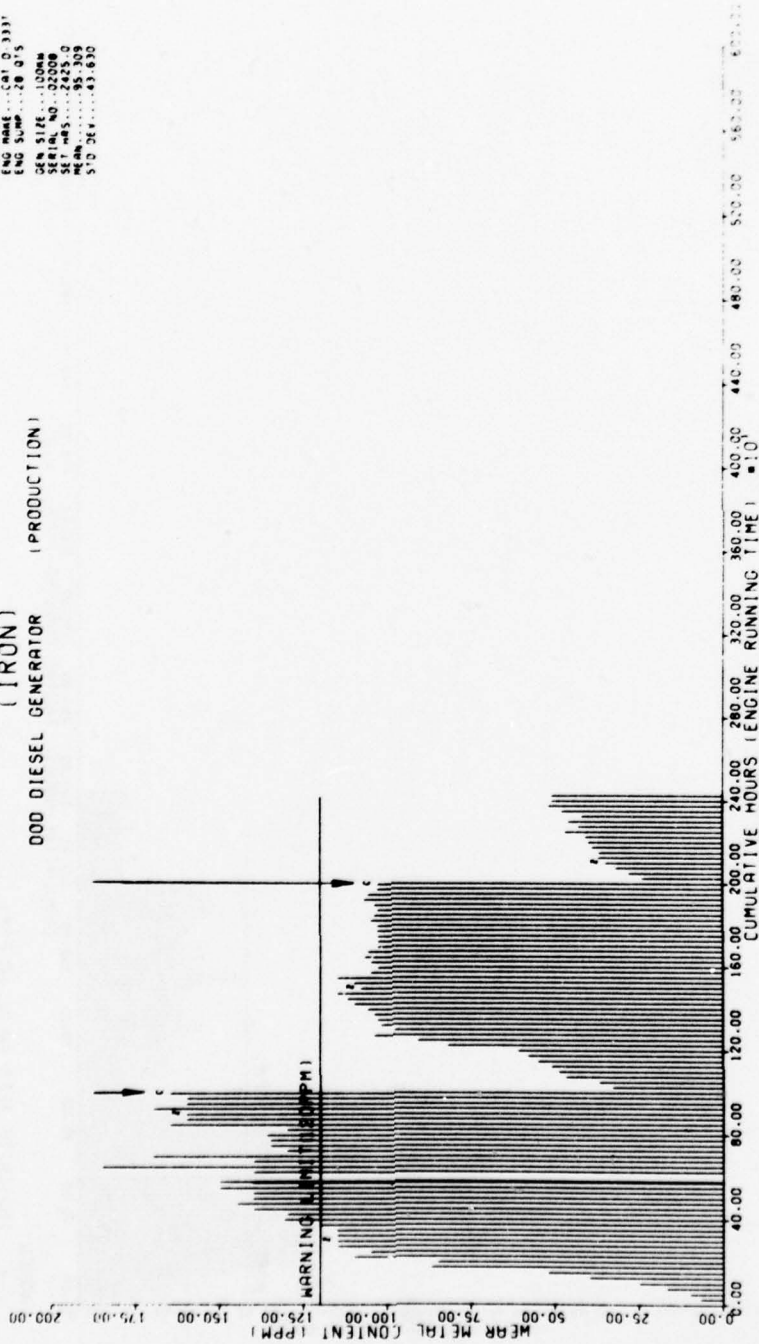
NOTES
M - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(IRON)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
27 JUNE 74 TO 4 JUL 74
END SIZE...279 8 m.p.
END NAME...Cat 0 333
END SUMP...28 Q'S
OIL SIZE...100mm
SERIAL NO...22000
TEST NO...43-630
MEAN...95.309
STD DEV...43.630



NOTES

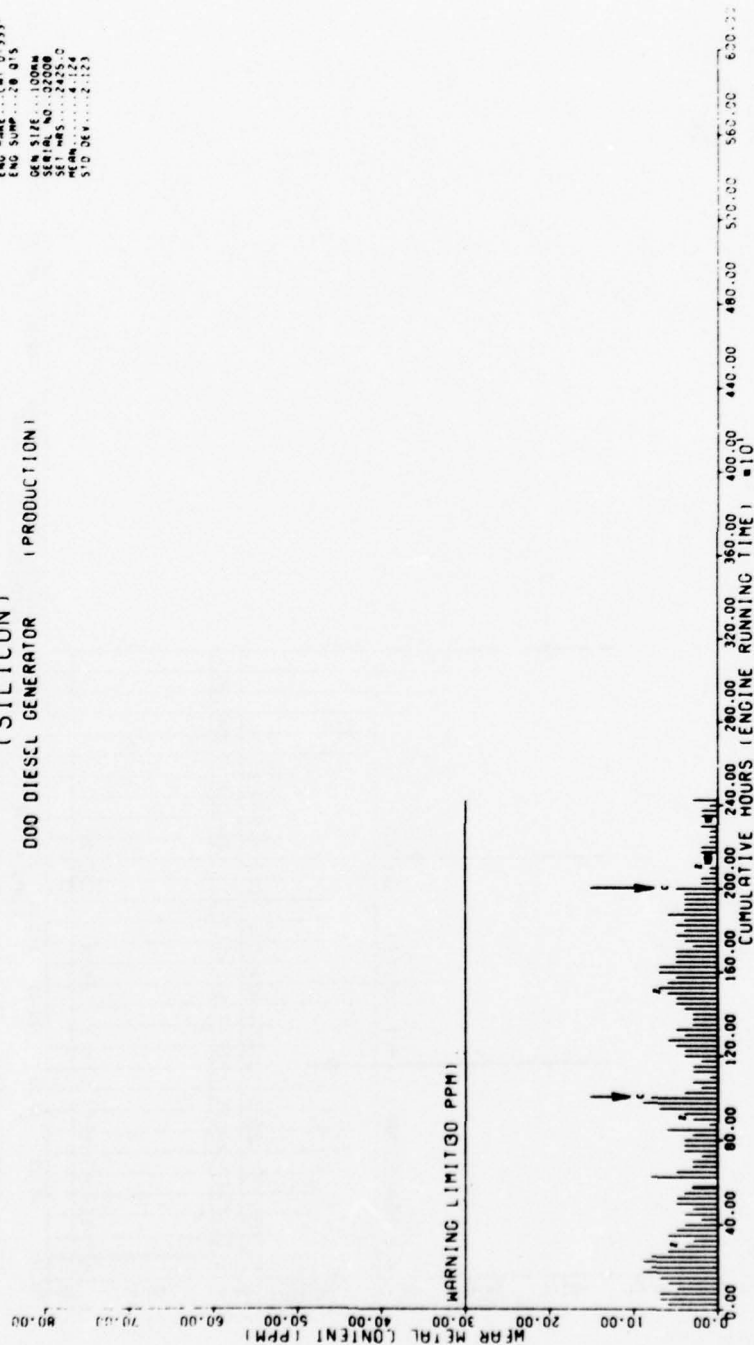
N - INDICATES ZERO VALUE (0 PPM)

NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS

F REPRESENTS THE END OF A CYCLE L REPRESENTS OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS (SILICON) DOD DIESEL GENERATOR (PRODUCTION)

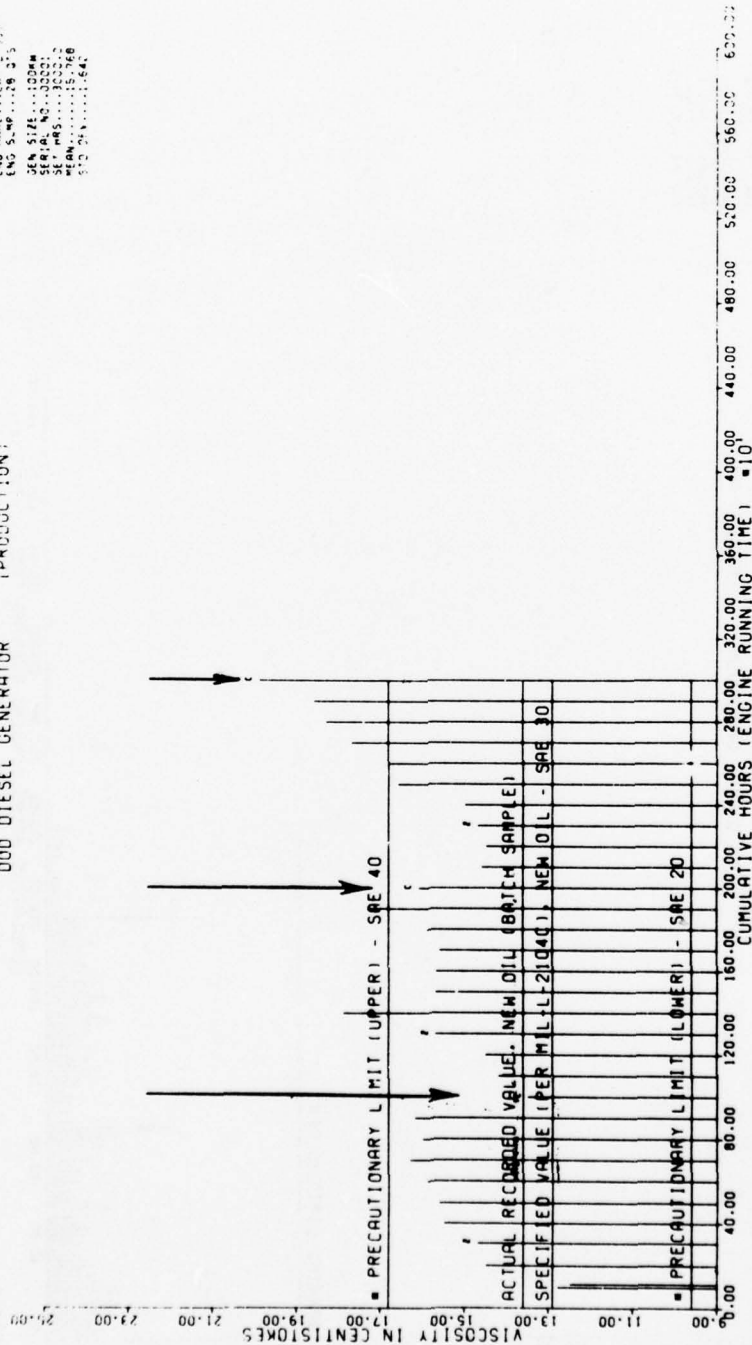
INCLUSIVE DATES
27 JUNE 74 19 4.0 '74
END SIZE 279 8-M-P
END NAME CAT 0 333
END SUMP 28 Q'S
GEN SIZE 100MM
SERIAL NO 3250W
SPELIMS 4420
MEAN 2.124
STD DEV 2.123



NOTES
M - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
P REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

IN-USE DATE
 10 NOV 19 6 45.74
 END SIZE 1000MM
 END MAKE 1000MM
 END SIZE 1000MM
 END MAKE 1000MM
 END SIZE 1000MM
 END MAKE 1000MM
 END SIZE 1000MM
 END MAKE 1000MM

VISCOSITY OF USED OIL AT 210 F DOD DIESEL GENERATOR (PRODUCTION)

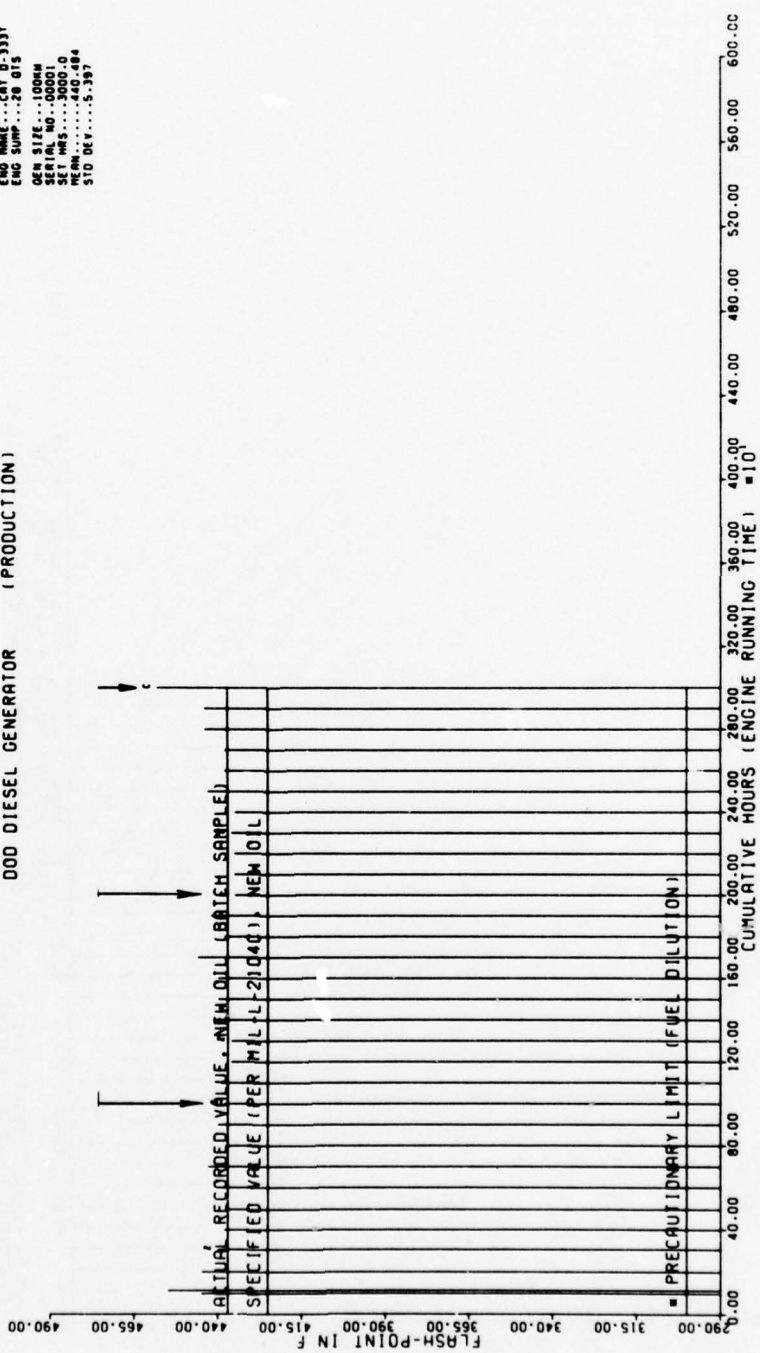


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN VISCOSITY AT 210F EITHER INCREASES IN VALUE TO THE NEXT HIGHER SAE GRADE LEVEL (MAXIMUM OXIDATION LIMIT) OR DECREASES IN VALUE TO THE NEXT LOWER SAE GRADE LEVEL (MAXIMUM FUEL DILUTION LIMIT).

SAE GRADE LIMITS ARE BASED ON 100% OIL CONCENTRATION

INCLUSIVE DATES
 30 NOV 73 8 NOV 74
 ENG SIZE...278 B.H.P.
 ENG NAME...CAT D-333T
 ENG SUMP...28 QTS
 GEN SIZE...100MM
 SERIAL NO...00001
 TEST NO...20000
 TEST DATE...240 284
 STD DEV...5.397

FLASH-POINT OF USED OIL (F) DOD DIESEL GENERATOR (PRODUCTION)

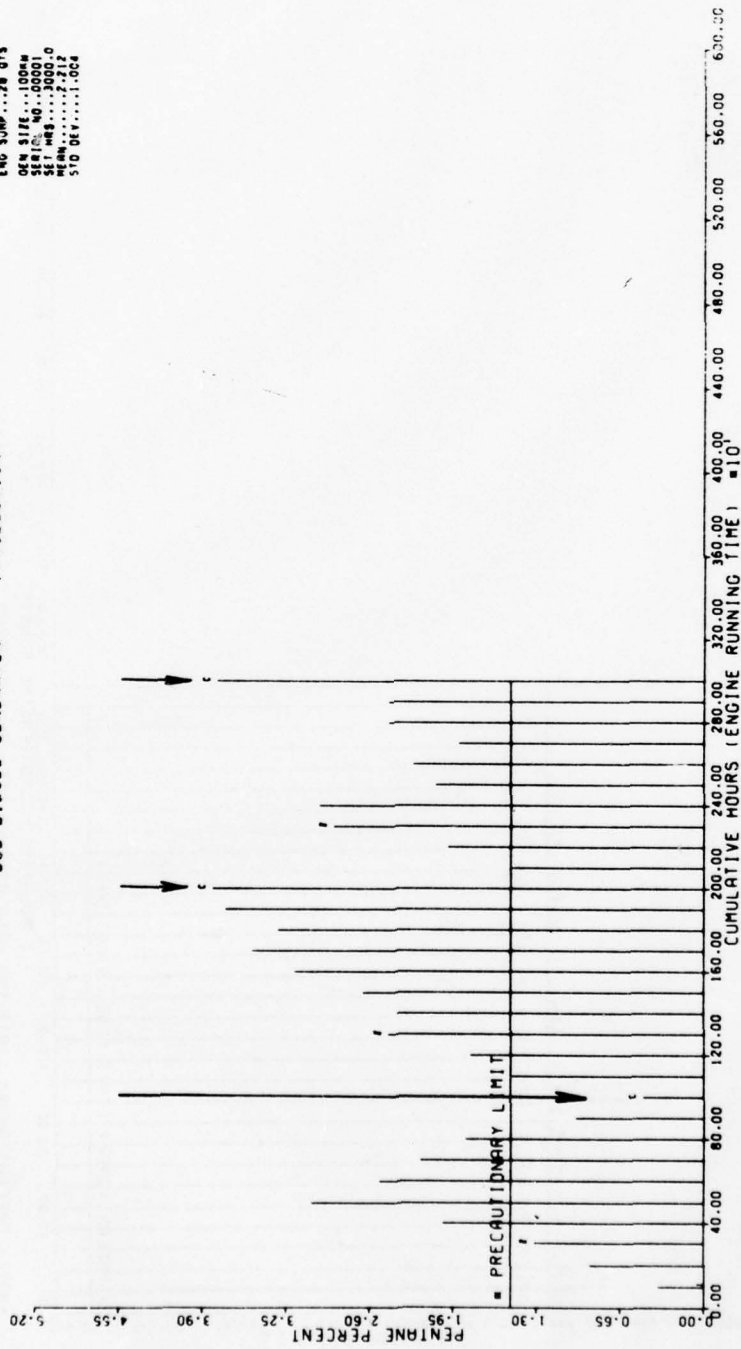


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE FLASH POINT
 REACHES 300F OR LOWER (MAXIMUM FUEL DILUTION).

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
 30 NOV 73 6 NOV 74
 ENG SIZE...270 B.H.P.
 ENG MAKE...CAT D-319
 ENG SUMP...28 QTS
 OIL SIZE...100W
 SERIAL NO...30001
 SET WBS...3000.0
 MEAN...2.212
 STD DEV...1.004

PERCENTAGE INSOLUBLES (PENTANE) DOD DIESEL GENERATOR (PRODUCTION)

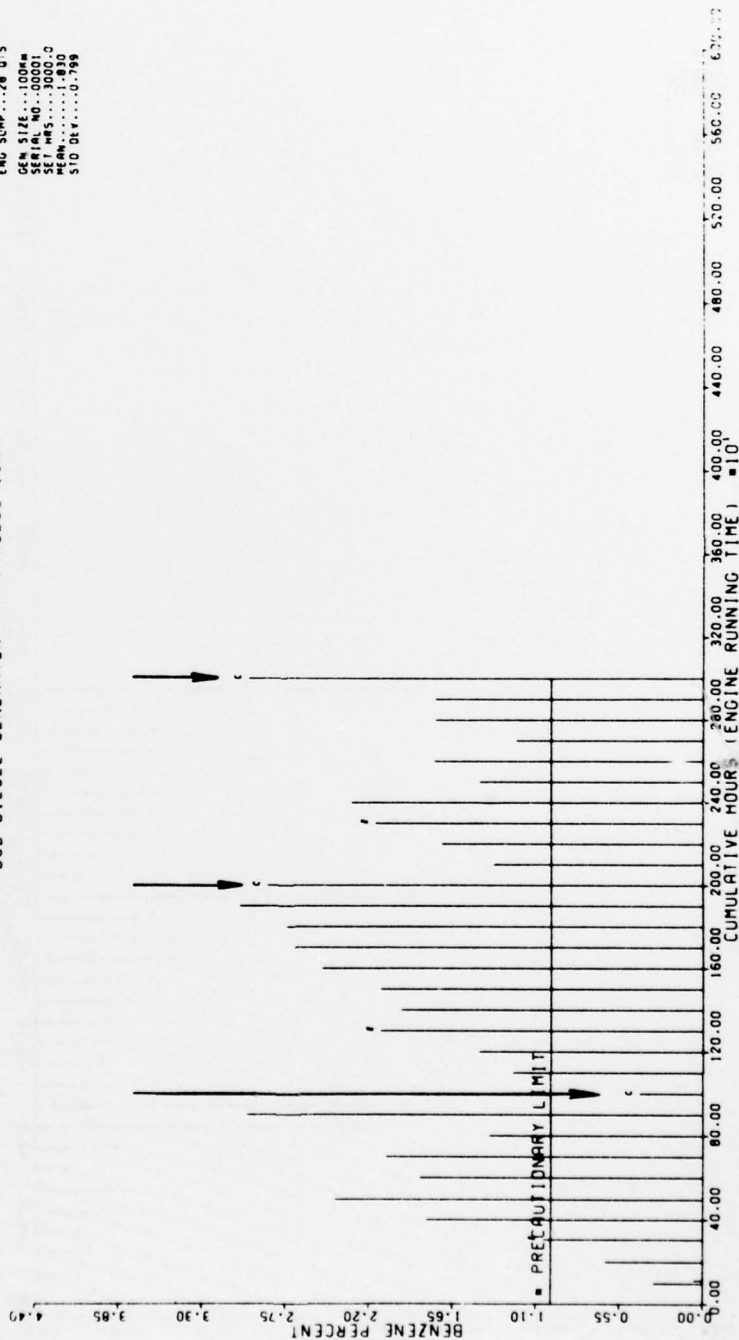


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF PENTANE INSOLUBLES REACHES 1.50 PERCENT.

A REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

INCLUSIVE DATES
30 NOV 73 6 NOV 74
ENG SIZE...275 B-M-P
ENG NAME...CAL D 331
ENG SUMP...28 Q'S
GEN SIZE...100MM
SERIAL NO...00001
SET HRS...3000.0
MEAN...1.830
STD DEV...0.199

PERCENTAGE INSOLUBLES (BENZENE) (PRODUCTION) 000 DIESEL GENERATOR

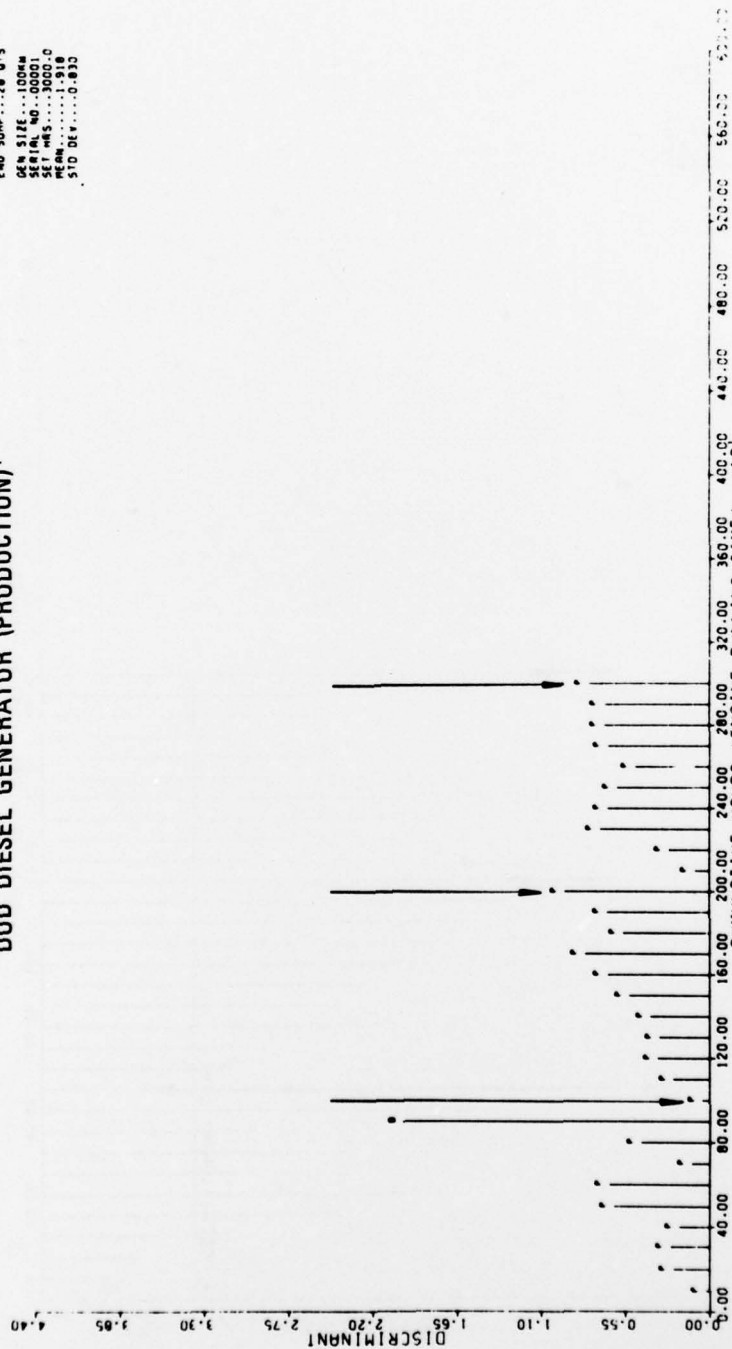


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN THE PERCENTAGE OF BENZENE INSOLUBLES REACHES 1.00 PER CENT.

P REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

PENTANE .VS. BENZENE DOD DIESEL GENERATOR (PRODUCTION)

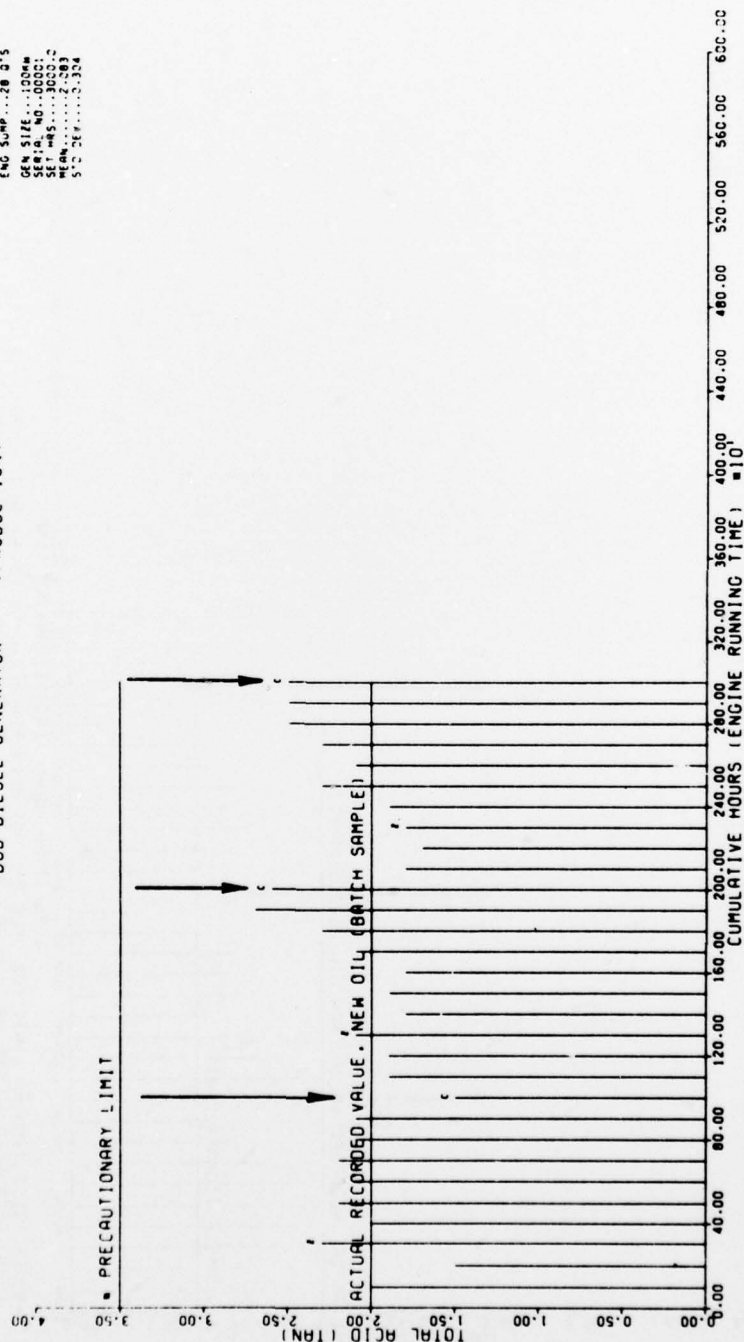
INCLUSIVE DATES
30 NOV 73 6 NOV 74
ENG SIZE...270 B.H.P.
ENG MAKE...CAT D-333
ENG SUMP...20 Q'S
GEN SIZE...1000W
SERIAL NO...00001
SET PHS...3000.0
MEAN...1.910
STD DEV...0.830



P SPECIFIES THAT THE PENTANE READING IS GREATER THAN THE BENZENE READING
B SPECIFIES THAT THE BENZENE READING IS GREATER THAN THE PENTANE READING

INCLUSIVE DATES
 30 NOV 73 5 NOV 74
 ENG SIZE.....200 00000
 ENG MAKE.....C-133
 ENG SNR.....28 015
 GEN SIZE.....10000
 SER NO.....10000
 SET HAS.....3000.0
 MEAN.....2.283
 STD DEV.....0.304

TOTAL ACID IN USED OIL 000 DIESEL GENERATOR (PRODUCTION)

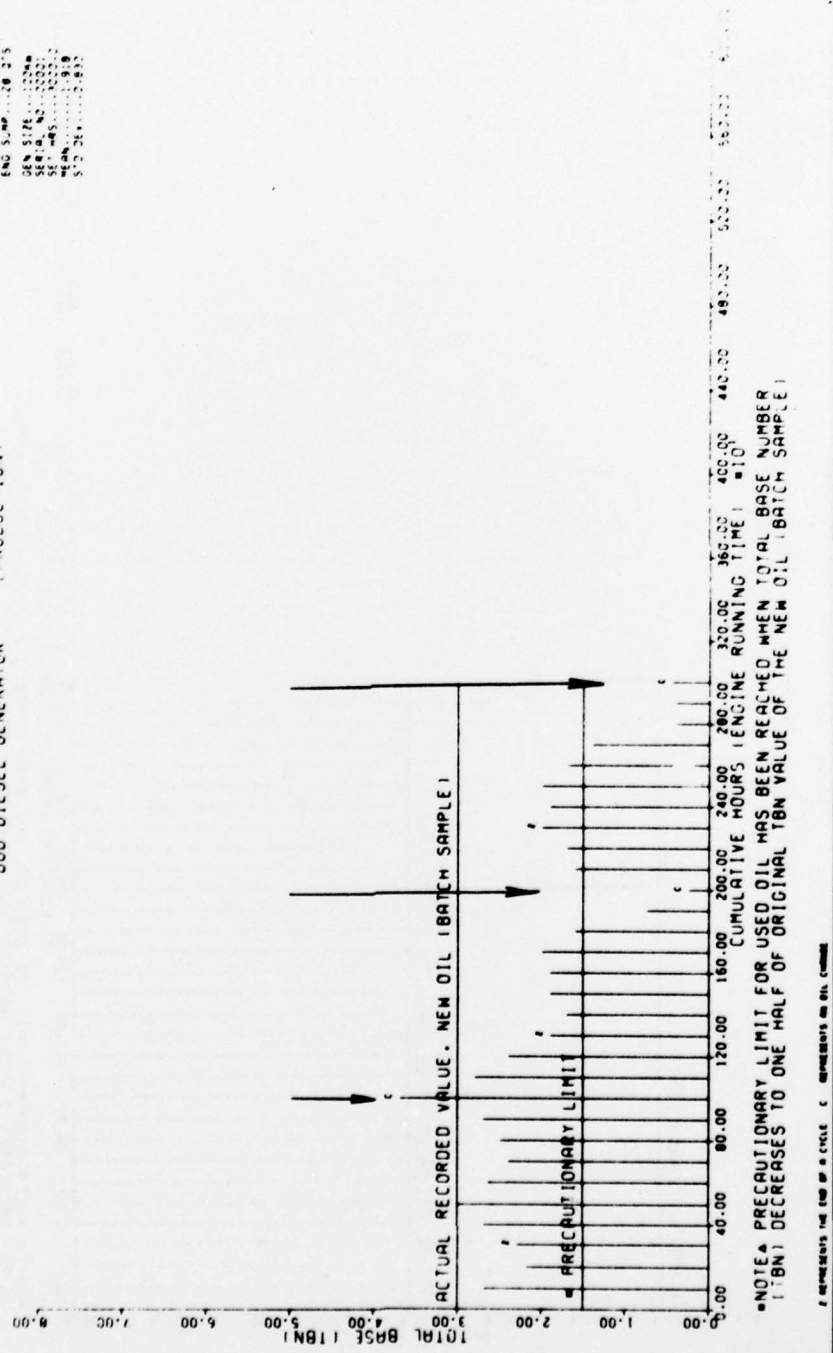


NOTE: PRECAUTIONARY LIMIT FOR USED OIL HAS BEEN REACHED WHEN TOTAL ACID NUMBER (TAN) INCREASES 2 WHOLE NUMBERS FROM THAT VALUE RECORDED FOR NEW OIL (BATCH SAMPLE) OR WHEN A TAN VALUE OF 3.50 IS REACHED.

F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

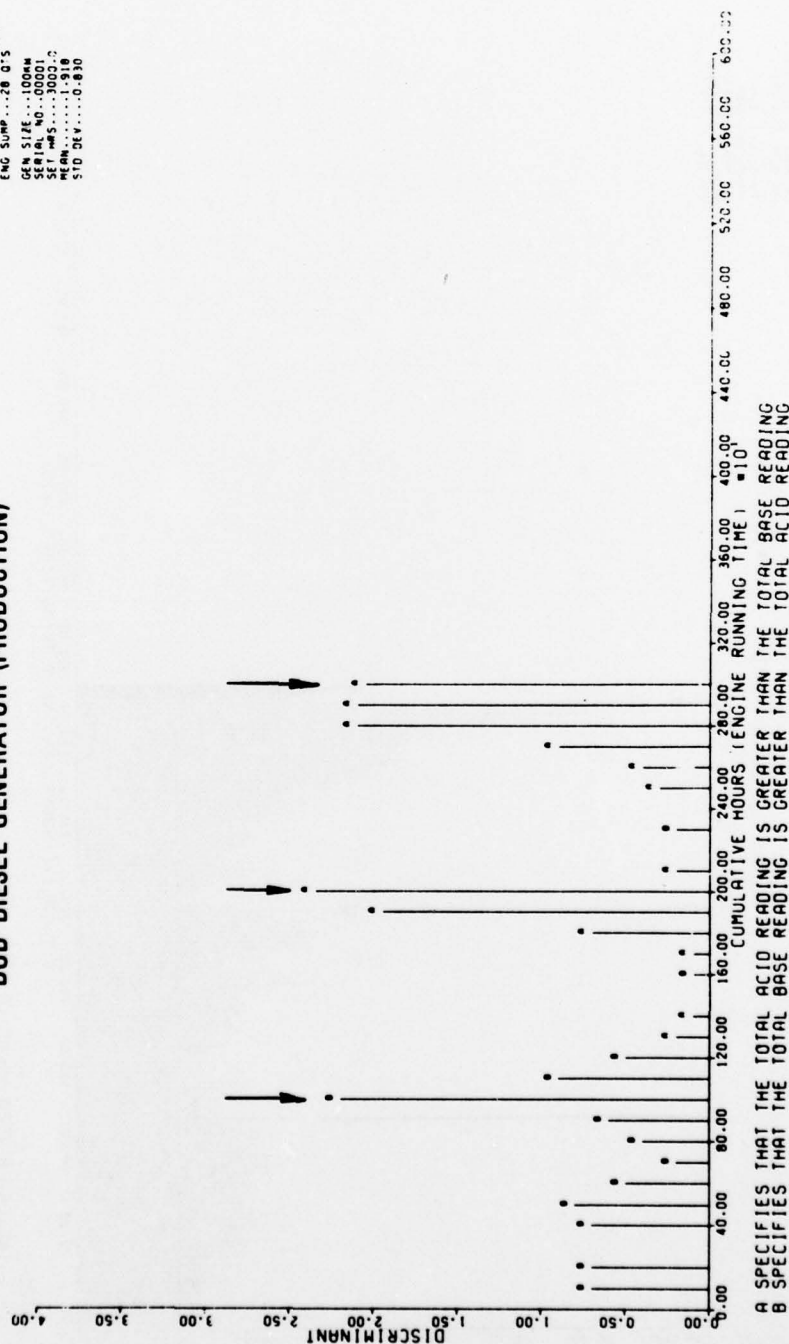
INCLUDE DATES
 END DATE 11/11/79
 END SIZE 120.00
 END MAKE 120.00
 END SAMP 120.00
 DEN SIZE 120.00
 SER. NO. 120.00
 SE. NO. 120.00
 SE. NO. 120.00
 SE. NO. 120.00
 SE. NO. 120.00

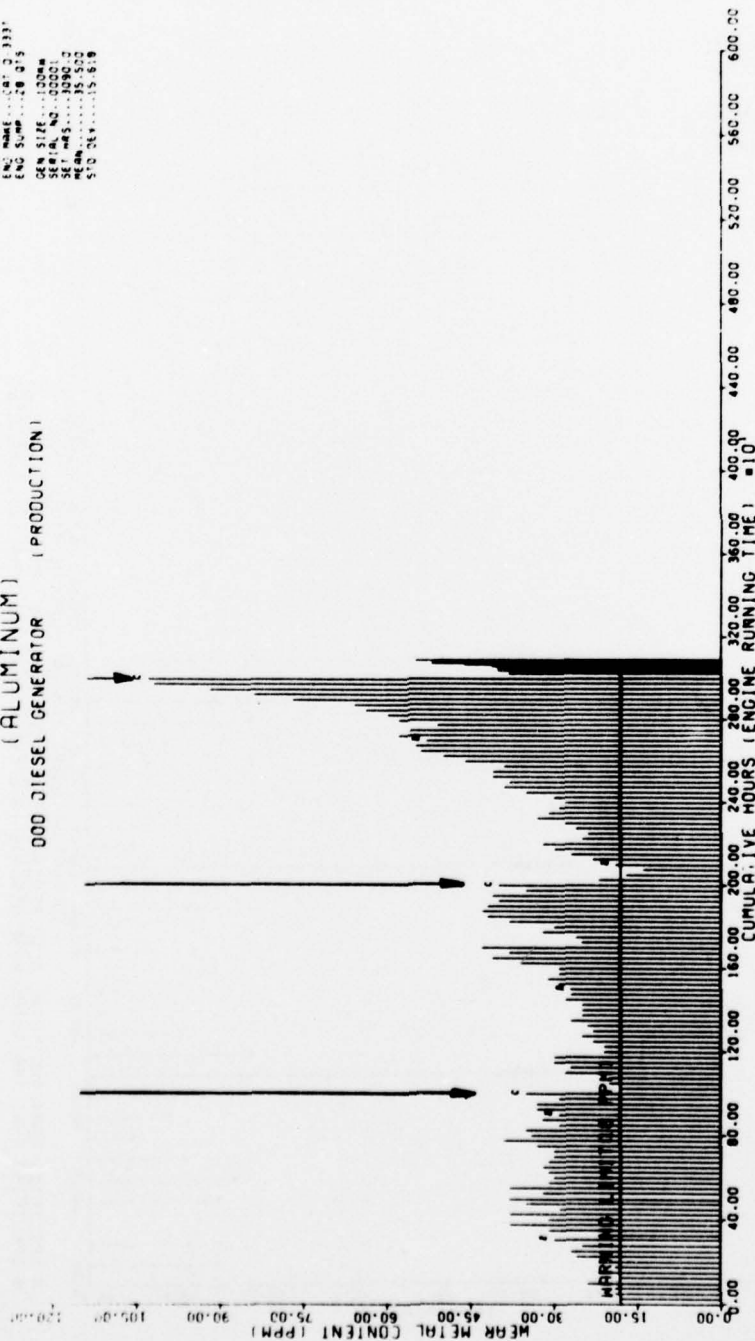
TOTAL BASE IN USED OIL
 DDD DIESEL GENERATOR (PRODUCTION)



INCLUDE DATES
 30 NOV 73 6 42V 74
 ENG SIZE...279 B-M-P
 ENG MAKE...CAT D-331
 ENG SUMP...28 Q'S
 GEN SIZE...100MM
 SERIAL NO...00001
 SET HMS...3000.0
 MEAN...1.918
 STD DEV...0.830

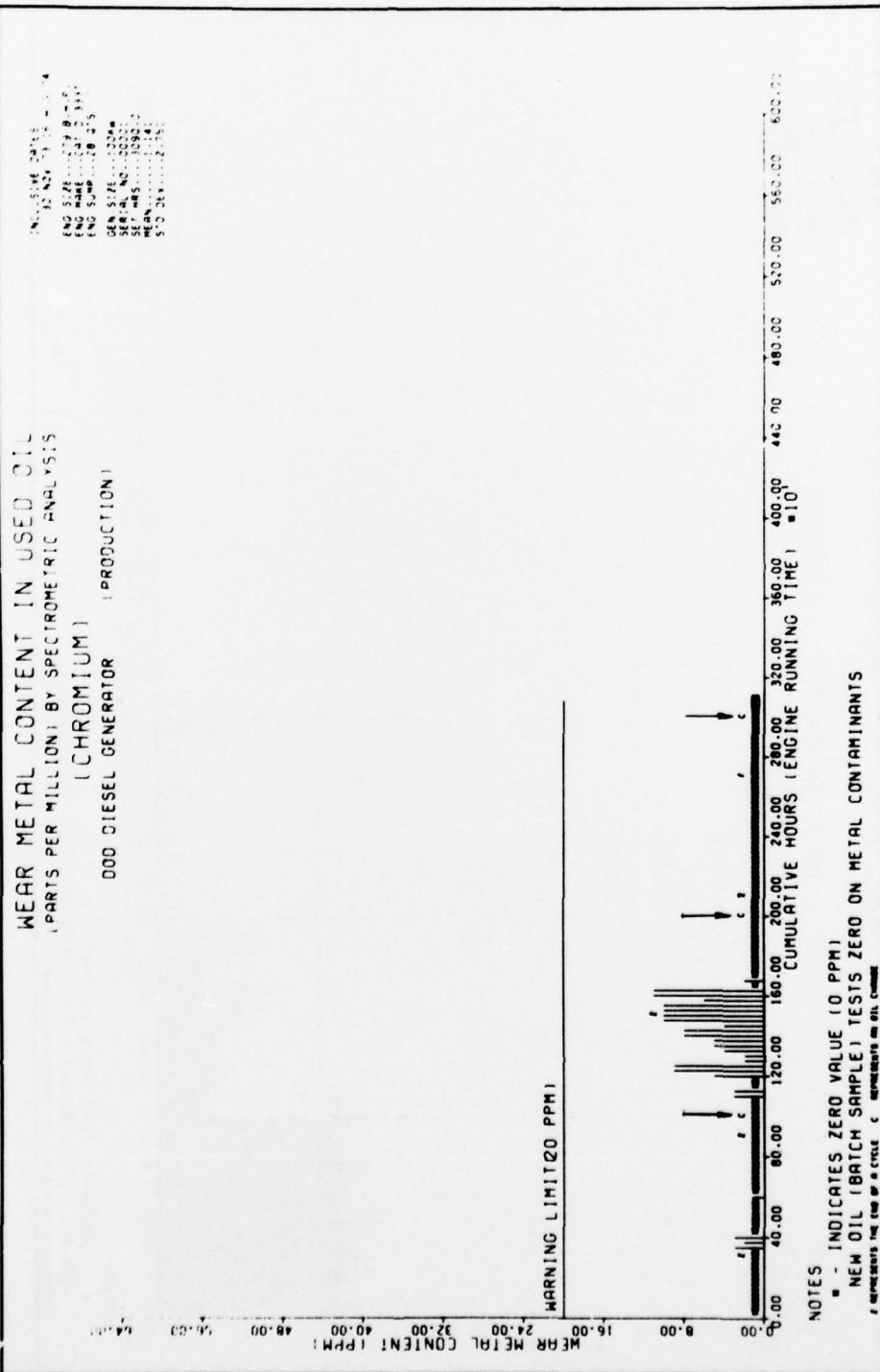
TOTAL ACID .VS. TOTAL BASE DOD DIESEL GENERATOR (PRODUCTION)



[illegible]

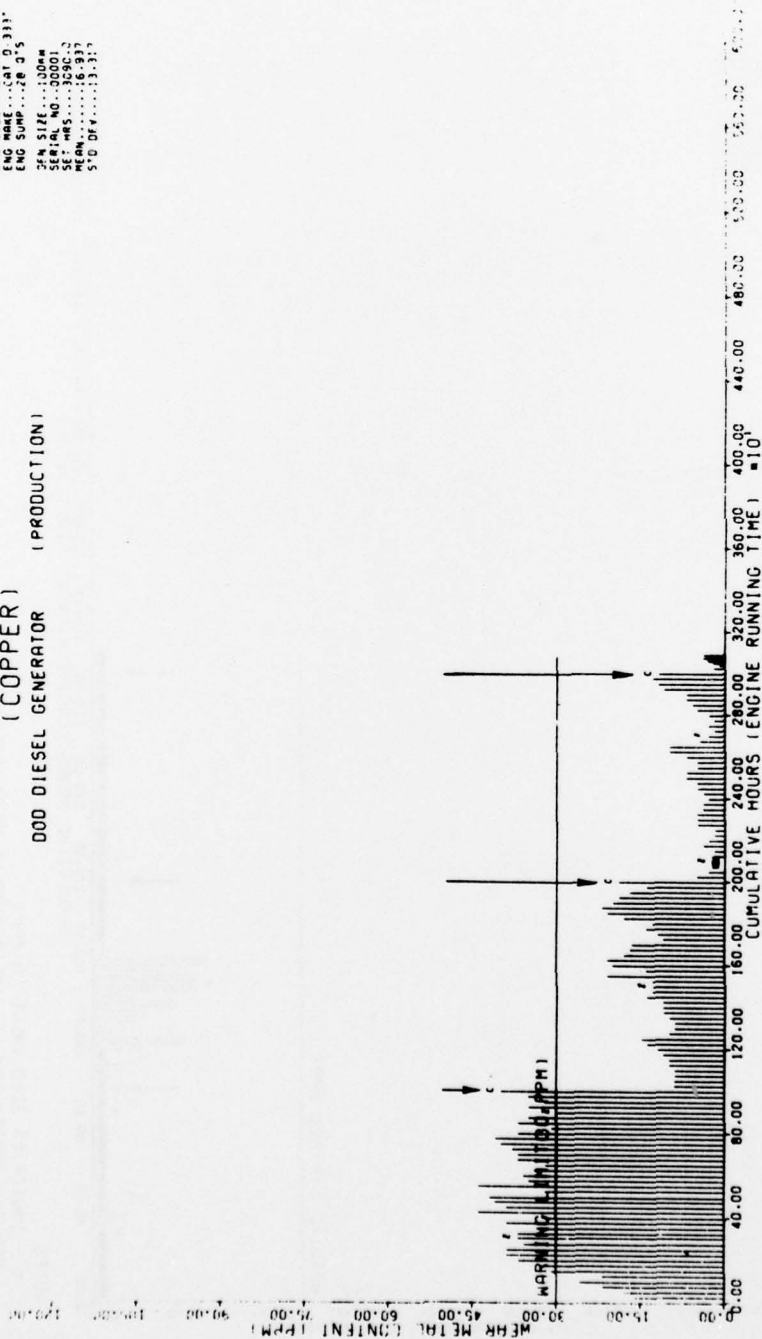
NOTES

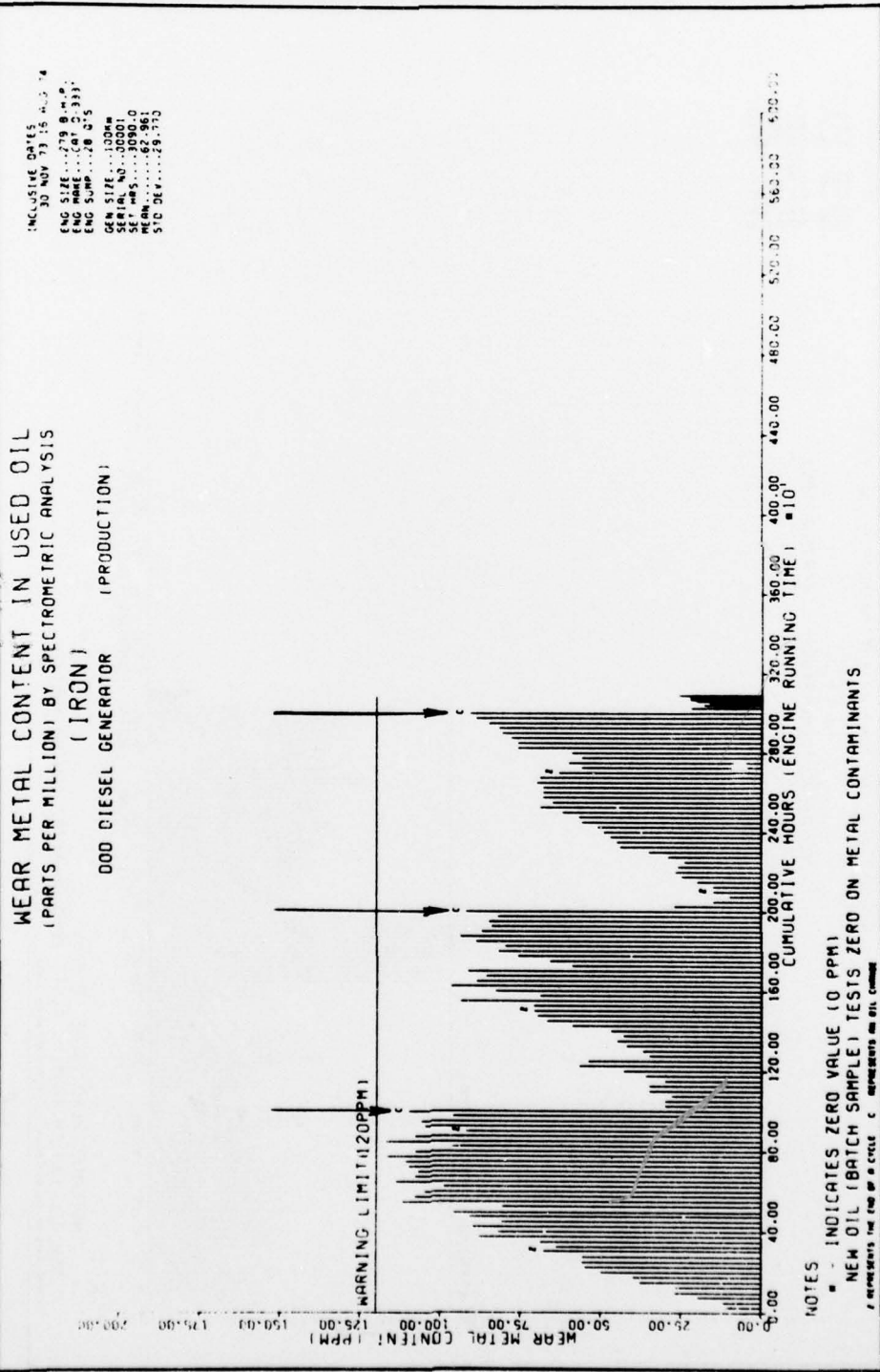
- - INDICATES ZERO VALUE (0 PPM)
- NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
- * REPRESENTS THE END OF A CYCLE
- † REPRESENTS AN OIL CHANGE



WEAR METAL CONTENT IN USED OIL
(PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS
(COPPER)
DOD DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
30 NOV 73 - 18 JUL 74
ENG SIZE...279 B.M.P.
ENG MAKE...Cat D. 333
ENG SUMP...28 D'S
2FN SIZE...100mm
SERIAL NO...30001
SUMP NO...10001
MEAN...16.937
STD DEV...13.317





NOTES

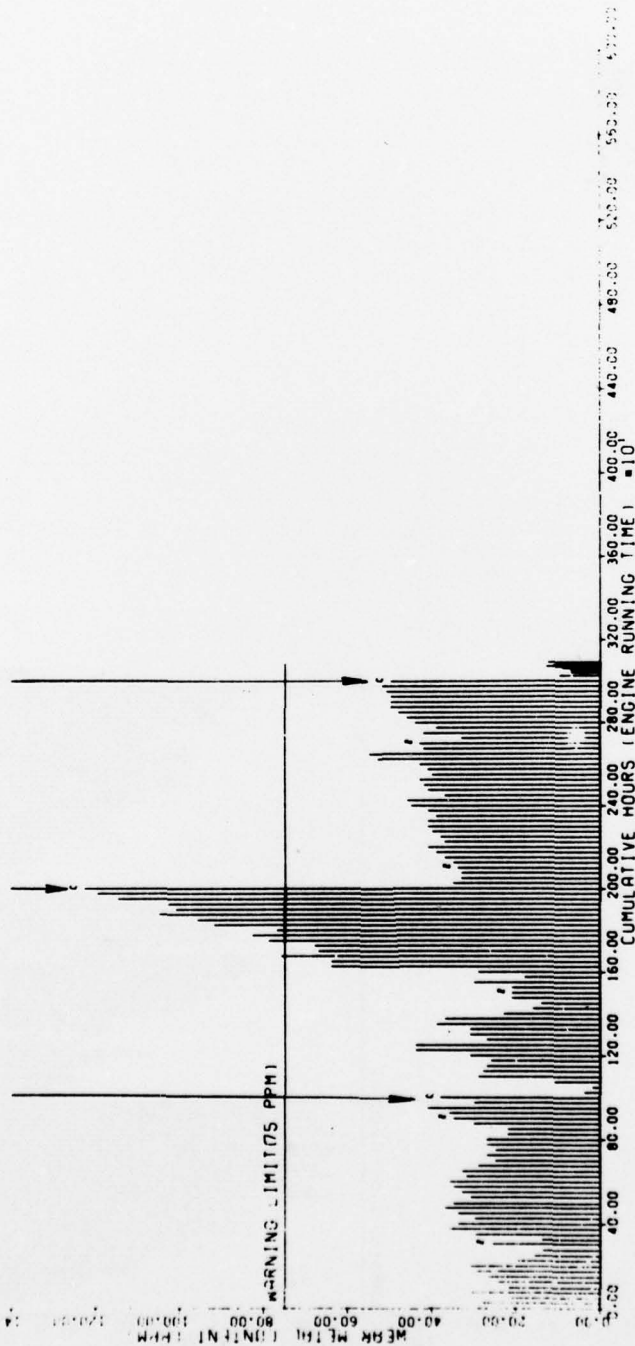
- - INDICATES ZERO VALUE (0 PPM)
- NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
- ↑ REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(LEAD)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
10 NOV 73 16 4 3 74
ENG SIZE...270 B...
ENG SUMP...28 QTS
SERIAL NO...1000M
SET PWS...3090.0
MEAN...38.773
STD DEV...23.225



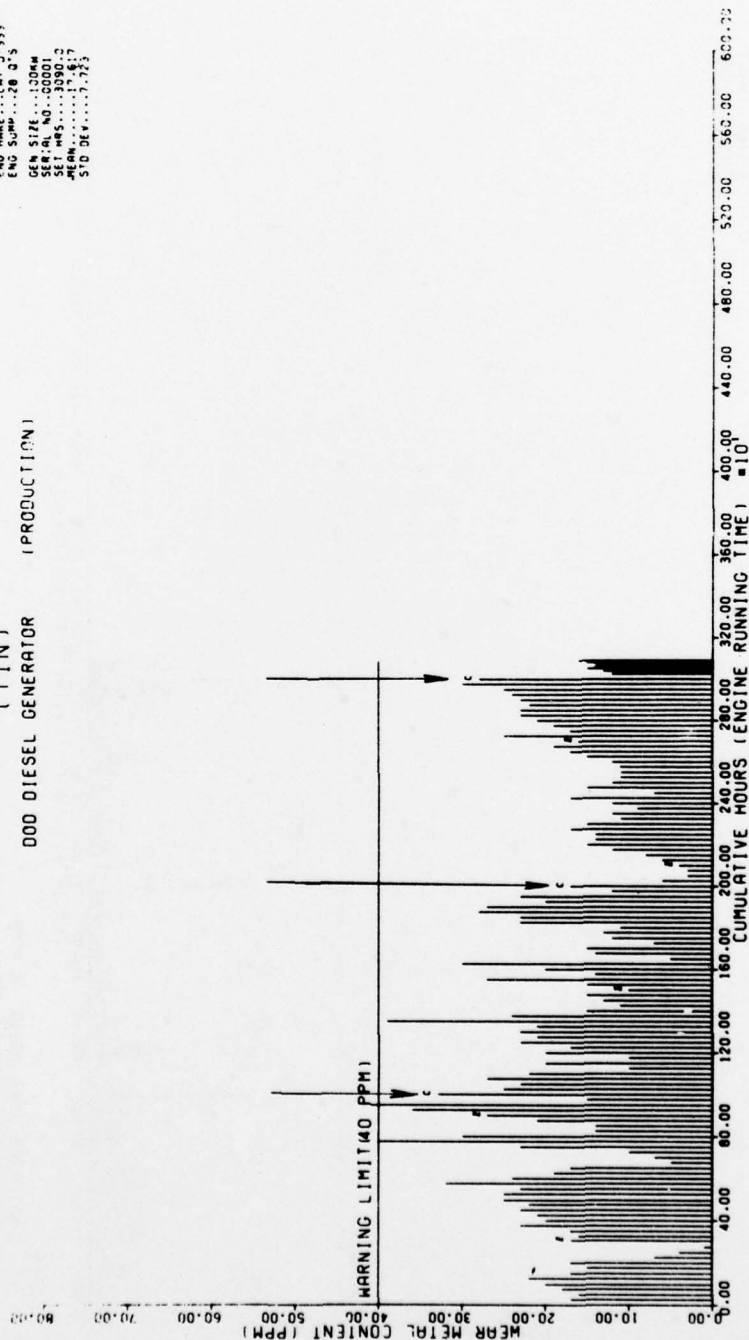
NOTES
- INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
P REPRESENTS THE TOP OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(TIN)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
30 NOV 73 TO 01 DEC 74
ENG SIZE...279 B-4-P
ENG MAKE...C-335
ENG SUPP...C-3
GEN SIZE...100KW
GEN MAKE...C-335
SERIAL NO...3080-2
SET HRS...17-6:17
MEAN...7.723
STD DEV...7.723



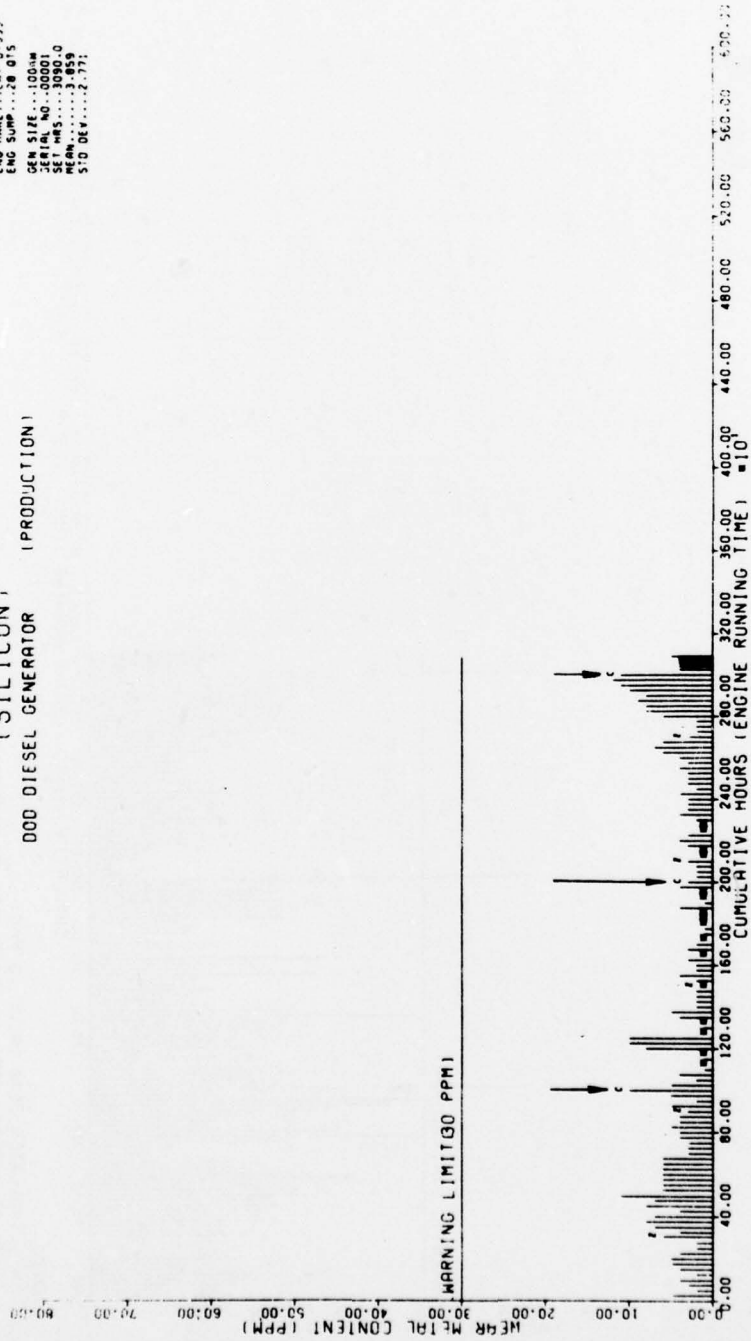
NOTES
■ - INDICATES ZERO VALUE (0 PPM)
NEW OIL (BATCH SAMPLE) TESTS ZERO ON METAL CONTAMINANTS
F REPRESENTS THE END OF A CYCLE C REPRESENTS AN OIL CHANGE

WEAR METAL CONTENT IN USED OIL (PARTS PER MILLION) BY SPECTROMETRIC ANALYSIS

(SILICON)

000 DIESEL GENERATOR (PRODUCTION)

INCLUSIVE DATES
30 NOV 73 15 4.3 74
ENG SIZE 270 B.H.P.
ENG MAKE CAT 0.333
ENG SUMP 128 QTS
GEN SIZE 1000W
SERIAL NO 30901
SET WRS 3.859
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