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SPECIAL REPORT ARLCB-SP-78003



INDEX TO BENET WEAPONS LABORATORY (LCWSL)

TECHNICAL REPORTS - 1977

Roy F. Tario
Technical Publications and Editing Unit

February 1978



US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
LARGE CALIBER WEAPON SYSTEMS LABORATORY
BENÉT WEAPONS LABORATORY
WATERVLIET, N. Y. 12189

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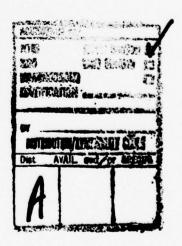
REPORT DOCUMENTATI	ON PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
ARLCB-SP-78003	2. GOVT ACCESSION	NO. 3. RECIPIENT'S CATALOG NUMBER
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Roy F./Tario Technical Publications and E	diting Unit (BWL)	
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US Army Armament Research and Large Caliber Weapon Systems L Dover, New Jersey 07801	aboratory	NUMBER OF PAGES 1275 P.
14. MONITORING AGENCY NAME & ADDRESS(II die	flerent from Controlling Office	UNCLASSIFIED 15. DECLASSIFICATION DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report)		
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19. KEY WORDS (Continue on reverse side if necess	ery and identify by block num	B
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SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

TABLE OF CONTENTS

	Page
List of Reports	1-4
Author Index	5-6
Abstracts-Report Documentation Page (DD Form 14	173) 7-92



TECHNICAL REPORTS 1977

REPORT NUMBER	TITLE	AUTHOR	DATE
WVT-TR-77001	Computer Controlled X-Ray Stress Analysis for Inspection of Manu- factured Components	G. Capsimalis R. Haggerty K. Loomis	Jan 77
WVT-TR-77002	Development of Improved Rifling Procedures and Equipment	C.H. LaRoss	Jan 77
WVT-CR-77003	Machining Tests and Analysis on 1018 and 4330 Steels	J.D. Christopher Metcut Research Associates, Inc.	Jan 77
WVT-TR-77004	Mechanism of Embrittlement and Brittle Fracture in Liquid Metal Environments	M. Kamdar	Jan 77
WVT-TR-77005	The Measurement of Dynamic Young's Modulus in Composite Lam- inates	Y.F. Cheng	Feb 77
WVT-TR-77006	The Stability of a Beam Subjected to a Moving Mass	G.L. Anderson	Feb 77
WVT-TR-77007	Qualitative Stability Character- istics of a Flexible Missile Sub- jected to a Circular Thrust	G.L. Anderson	Feb 77
WVT-TR-77008	The Influence of Support Characteristics on the Stability of an Elastic System Subjected to a Circulatory Force	G.L. Anderson	Mar 77
WVT-TR-77009	Parametric Resonance in Gun Tubes	T.E. Simkins	Feb 77
WVT-TM-77010	Preparation of Economic Analyses	V. Montouri	Feb 77
WVT-TR-77011	Verification of Numerically Con- trolled Machine Programs by the Automatic Drafting Machine	D. Concordia	Mar 77
WVT-TR-77012	Dynamic Analysis of Constant Reaction Systems for a Medium Caliber, Anti-Armor, Automatic Cannon	P.M. Vottis J.K. Jorczak	Mar 77
WVT-TR-77013	Hydraulic Analysis of the Recoil and Counterrecoil Cycle in Medium Caliber, Anti-Armor, Automatic Cannon, Test Bed No. 2	H.J. Scheck	Mar 77

TECHNICAL REPORTS 1977 (CONTINUED)

REPORT NUMBER	TITLE	<u>AUTHOR</u> <u>DATE</u>
WVT-TN-77014	Failure Investigation 105MM M68 Tubes (SN 16244, 7506, and 11837)	A. Campbell Mar 77
WVT~TR-77015	Electrodeposited $C_{\rm u}$ and $C_{\rm u}$ -Al $_2$ O $_3$ Alloys: Physical and Mechanical Properties	G. Lakshmenarayanan Mar 77E. ChenF. Sautter
WVT~TR-77016	Electrodeposition of Cobalt Using an Insoluble Anode	G. Lakshmenarayanan Mar 77E. ChenJ. SadakF. Sautter
WVT~TR-77017	The Effects of Pulse Current Plating on the Mechanical Properties Of Cobalt and Cobalt-Al ₂ O ₃	E. Chen Mar 77 F. Sautter
WVT~TR-77018	The Effects of Chloride Ion on the Codeposition of Alumina with Copper	G. Lakshmenarayanan Mar 77 E. Chen F. Sautter
WVT-TR-77019	Ultrasonic and Acoustic Holographic Techniques for Inspection of Com- posite Gun Tubes and Other Weapon Components	G. Capsimalis Mar 77 G. D'Andrea R. Peterson
WT-TR-77020	Effects of Pressure and Thermal Loadings on a Thin Plating Inside a Thick Tube	S.L. Pu Mar 77 J.J. Wu
ARLCB-TR-77025	The Effect of Autofrettage on Fatigue Crack Propagation in Ex- ternally Flawed Thick Walled Disks	J.A. Kapp Apr 77
ARLCB-MR-77026	Effects of Quenching Techniques Upon Gun Steel	E.H. Niccolls May 77
ARLCB-TR-77027	Analytical and Experimental Tube Temperatures in the 8" XM201 Cannon	R.G. Gast May 77 P.M. Vottis
ARLCB-TR-77028	The Abrasion Characteristics of Certain Protective Coatings on Aluminum and Magnesium Alloys	A. Campbell May 77 W. Mortimer P. Thornton
ARLCB-TR-77029	A Probabilistic Model of Gun Tube Fatigue	R.L. Racicot May 77

TECHNICAL REPORTS 1977 (CONTINUED)

REPORT NUMBER	TITLE	AUTHOR	DATE
ARLCB-TR-77030	Computerizing the Effect of Tempering on the Mechanical Pro- perties of Ni-Cr-Mo Steel	P. Dembowski	Jun 77
ARLCB-TR-77031	Erosion in 81MM Mortar Tubes	V.P. Greco	Jun 77
ARLCB-TR-77032	Development of Prototype Production ESR Facilities	V.J. Colangelo	Jun 77
ARLCB-TR-77033	Automatic Step Threading of Breechblocks	C. Rose	Jun 77
ARLCB-TR-77034	The Influence of Late Wear Life 105MM M68 Gun Tubes on Discarding Sabot Ammunition Flight Stability	A.A. Albright E.E. Coppola G.S. Friar	Jul 77
ARLCB-TR-77035	Evaluation of 155MM M199 Tube Forging Producers	J. Passmore	Jul 77
ARLCB-TR-77036	Reinforced Cobalt Alloy Composite for Turbine Blade Application	I. Ahmad J. Barranco	Jul 77
ARLCB-TR-77037	Investigation of Fastener Failure in 105MM M68 Guns and 152MM M81 and M162 Gun Launchers	M. Longmate	Aug 77
ARLCB-TR-77038	Vibrations of a Helicopter Rotor Blade Using Finite Element-Uncon- strained Variational Formulations	J.J. Wu C.N. Shen	Sep 77
ARLCB-TR-77040	Probabilistic Models on Gun-Tube Fatigue Based on a Fracture-Mech- anics Model	E.E. Coppola	Oct 77
ARLCB-TR-77041	Isoparametric Elements as Singular Elements for Crack Problems	M.A. Hussain W.E. Lorensen	Oct 77
ARLCB-TR-77042	Effect of Damping at the Support of a Rotating Beam on Vibrations	J.D. Vasilakis J.J. Wu	Oct 77
ARLCB-TR-77043	Temper Embrittlement in 4140 Seamless Tubing	S. Tauscher P. Thornton	Nov 77
ARLCB-TR-77044	Design and Production of Ballistic Guns Nos. 2 and 3 and the Initial Test Bed Gun for the Medium Caliber Anti-Armor Automatic Cannon Pro- gram	P.M. Vottis R.L. Billington R.C. Sillery	Nov 77

TECHNICAL REPORTS 1977 (CONTINUED)

REPORT NUMBER	TITLE	AUTHOR	DATE
ARLCB-TR-77045	Structure Factors in Amorphous and Discorded Harmonic Debye Solids	L. Meisel P. Cote	Dec 77
ARLCB-TR-77046	Embrittlement of Gun Steel by Liquid Lead	M.H. Kamdar	Dec 77
ARLCB-TR-77047	Collapsed 12-Node Triangular Elements as Crack Tip Elements for Elastic Fracture	S.L. Pu M.A. Hussain W.E. Lorensen	Dec 77
ARLCB-TR-77048	Energy and Pressure Calculations	D.M. Gray	Dec 77

AUTHOR INDEX--1977

AUTHOR	REPORT NUMBER
Ahmad, I.	ARLCB-TR-77036
Albright, A.	ARLCB-TR-77034
Anderson, G.	WVT-TR-77006
	WVT-TR-77007
	WVT-TR-77008
Barranco, J.	ARLCB-TR-77034
Billington, R.	ARLCB-TR-77044
Campbell, A.	WVT-TN-77014
Capsimalis, G.	WVT-TR-77001
	WVT-TR-77019
Chen, E.	WVT-TR-77015
	WVT-TR-77016
	WVT-TR-77017
	WVT-TR-77018
Cheng, Y.F.	WVT-TR-77005
Colangelo, V.J.	ARLCB-TR-77032
Concordia, D.	WVT-TR-77011
Coppola, E.E.	ARLCB-TR-77034
	ARLCB-TR-77040
Cote, P.	ARLCB-TR-77045
D'Andrea, G.	WVT-TR-77019
Dembowski, P.	ARLCB-TR-77030
Friar, G.G.	ARLCB-TR-77034
Gast, R.G.	ARLCB-TR-77027
Gray, D.M.	ARLCB-TR-77048
Greco, V.P.	ARLCB-TR-77031
92000, 1121	
Haggerty, R.	WVT-TR-77001
Hussain, M.A.	ARLCB-TR-77041
	ARLCB-TR-77047
Jorczak, J.K.	WVT-TR-77012
Kamdar, M.	WVT-TR-77004
	ARLCB-TR-77046
Lakshmenarayan, G.	WVT-TR-77015
	WVT-TR-77016
	WVT-TR-77018
La Ross, C.	WVT-TR-77002
Longmate, M.	ARLCB-TR-77037
Loomis, K.	WVT-TR-77001
Lorensen, W.E.	ARLCB-TR-77041
	ARLCB-TR-77047
	5

AUTHOR INDEX--1977 (CONT.)

AUTHOR	REPORT NUMBER
Meisel, L.	ARLCB-TR-77045
Montouri, V.	WVT-TR-77010
Mortimer, W.	ARLCB-TR-77028
Niccolls, E.H.	ARLCB-MR-77026
Passmore, J.	ARLCB-TR-77035
Peterson, R.	WVT-TR-77019
Pu, S.L.	WVT-TR-77020
	ARLCB-TR-77047
Racicot, R.L.	ARLCB-TR-77029
Rose, C.	ARLCB-TR-77033
Sadak, J.	WVT-TR-77016
Sautter, F.	WVT-TR-77015
	WVT-TR-77016
	WVT-TR-77017
	WVT-TR-77018
Scheck, H.J.	WVT-TR-77013
Shen, C.N.	ARLCB-TR-77038
Sillery, R.C.	ARLCB-TR-77044
Simkins, T.E.	WVT-TR-77009
Tauscher, S.	ARLCB-TR-77043
Thornton, P.	ARLCB-TR-77028
	ARLCB-TR-77043
Vasilakis, J.D.	ARLCB-TR-77042
Vottis, P.M.	WVT-TR-77012
	ARLCB-TR-77027
	ARLCB-TR-77044
Wu, J.J.	WVT-TR-77020
	ARLCB-TR-77038
	ARLCB-TR-77042

	NTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
WVT-TR-77001		
COMPUTED CONTROLLED V DAY	CTREES ANALYSIS FOR	5. TYPE OF REPORT & PERIOD COVERED
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AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(s)
G.P. Capsimalis, R.F. Hag	gerty, K. Loomis	
PERFORMING ORGANIZATION NAME A	ND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 3297.06.7282
Benet Weapons Laboratory		AMCMS No. 3297.06.7282
Watervliet Arsenal, Water	vliet, N.Y. 12189	
SARWV-RT-TP		Pron No. M1-4-A1527
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U.S. Army Armament Comman		January 1977
Rock Island, Illinois 61		13. NUMBER OF PAGES
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7. DISTRIBUTION STATEMENT (of the ab 18. SUPPLEMENTARY NOTES 9. KEY WORDS (Continue on reverse side in X-Ray Diffraction Non-Destructive Test	I necessary and identify by block number) Residual Sting Computer A	m Report)
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20. problem solutions using FORTRAN IV.		
All operations of the stress goniometer, the modular electonic hardware, logic operations and data processing are performed in real time and are completely computer controlled.		

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REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM	
	3. RECIPIENT'S CATALOG NUMBER	
WVT-TR-77002		
4. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED	
DEVELOPMENT OF IMPROVED RIFLING PROCEDURES AND		
ECUIPMENT	6. PERFORMING ORG. REPORT NUMBER	
7. AUTHOR(a)	8. CONTRACT OR GRANT NUMBER(*)	
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9. PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT PROJECT TASK	
Benet Weapons Laboratory	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 3297.06.7402	
Watervliet Arsenal, Watervliet, N.Y. 12189	PRON No. M1-4-A1678-O1-M7-M7	
SARWV-RT-TP		
11. CONTROLLING OFFICE NAME AND ADDRESS US Army Armament Command	January 1977	
Rock Island, Illinois 61201	13. NUMBER OF PAGES	
14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office)	15. SECURITY CLASS. (of this report)	
MONITORING NOCHCE NAME & ADDRESS(II dillerant from Controlling Office)	13. SECURITY CLASS. (of this report)	
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16. DISTRIBUTION STATEMENT (of this Report)		
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17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number		
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Gun Barrels Rifling Duplex Process		
Rifling Machines		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)		
This report describes a process of rifling two taneously in a horizontal side by side position.	105mm M2A2 gun barrels simul-	
The purpose of the project was to reduce signitime of 105mm gun barrels by a process that would be duction line cuantities.		

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
WVT-CR-77003	. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
MACHINING TESTS AND ANALYSIS ON 1	018 AND 4330	5. TYPE OF REPORT & PERIOD COVERED
STEELS		6. PERFORMING ORG. REPORT NUMBER
AUTHOR(s)		B. CONTRACT OR GRANT NUMBER(*) DAAA22-75-M-0419
Metcut Research Associates Inc. Cincinnati, Ohio 45209		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 3297.16.7119 Pron No. M1-2-23084-01-M7-M
CONTROLLING OFFICE NAME AND ADDRESS Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N SARWV-RT-TP	.Y. 12189	January 1977 13. NUMBER OF PAGES 28
4. MONITORING AGENCY NAME & ADDRESS(If different	from Controlling Office)	15. SECURITY CLASS. (of this report) UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Carbide . High Speed Steel Optimum Tool Geometry Application

20. ABSTRACT (Continue on reverse side if recessary and identify by block number)

An examination of the report "An Investigation to Determine the Single Point Cutting Tool Angles Which Yield Maximum Tool Life by Response Surface Methodology and Evolutionary Operation of Processes," Lloyd Louis Lehn (thesis submitted in partial fulfillment of the requirements for the degree of Doctor of Philosophy in Mechanical Engineering in the Graduate College of the University of Illinois, 1967), necessitated determining the optimum tool geometry which could be used to grind back and side rake tool angles for high speed steel tools. Machining tests and analysis were done on 1018 and 4330 steels.

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	N PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
REPORT NUMBERWYT-TR-77004	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
MECHANISM OF EMBRITTLEMENT AND B IN LIQUID METAL ENVIRONMENTS	RITTLE FRACTURE	5. TYPE OF REPORT & PERIOD COVERED
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1. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
US Army Armament Command Rock Island, Illinois 61201		January 1977
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Liquid metal embrittlement is presently considered to result from liquid metal "adsorption-induced reduction in cohesion" of atomic bonds at regions of high stress concentrations in a solid, such as at the tip of cracks or at the sites of crack nucleation. The prerequisites for embrittlement are the same as those for brittle fracture and liquid metal embrittlement is considered a special case of brittle fracture rather than a diffusion or a corrosion type of phenomena.

This paper presents some theoretical considerations (1) concerning the "reduced-cohesion" mechanism of embrittlement and (2) embrittlement to be a special case of brittle fracture. Experimental results utilizing ideal embrittlement systems in support of the mechanism and also in support of various brittle fracture criteria are presented and discussed.

	REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
REPO	WVT-TR-77005	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
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PERF	DRMING ORGANIZATION NAME AND ADDR	ESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
Ben	et Weapons Laboratory		AMCMS Code: 612105.11.H8	
	ervliet Arsenal, Watervlie	t, N.Y. 12189		
	WV-RT-TP		PRON: A1-5-R0005-04-AW-M	
	ROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE	
	Army Armament Command		February 1977	
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. MONI	TORING AGENCY NAME & ADDRESS(II dill	erent from Controlling Office)	15. SECURITY CLASS. (of this report)	
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. SUPP	LEMENTARY NOTES			
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practically the same as the static values. The impact method gave a dynamic (See Other Side)

value of Young's modulus noticeably lower than the static value. The difference between $(E_d)_{i,i}$ from impact and those from vibration increases with the ratio of E_r/E_m —thus showing the effect of the dispersion of stress velocity. In addition $(E_d)_{i,j}$ from impact was always lower than those from vibration and was apparently not related to the ratio of E_r/E_m . It is concluded that, in the dynamic characterisation of fibre-reinforced laminate materials, the resonance-free vibration method is preferable to the impact method.

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REPORT DOCUMENTATIO	N PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
MENORI NUMBER	2. GOVT ACCESSION NO	3. RECIPIENT'S CATALOG NIMBER
WVT-TR-77006		
TITLE (and Subtitle)		S. TYPE OF REPORT & PERIOD COVERED
The Stability of a Beam Subject	ed to a Moving	
Mass		
		6. PLRFORMING ORG. REPORT NUMBER
A () I HOR(a)		B CONTI ACT OR GRANT WINE P
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. STORMING ORGANIZATION NAME AND ADDRE	54	10 PROGRAM FLEMENT PROJECT
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. IROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
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MINITED AND A IT NOV NAME & ADDRESS/IT diffe	rent from Controlling Office)	15. SECURITY CLASS. (of this report)
		INC. COLUMN
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1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
WVT-TR-77007		
4. TITLE (and Subtitio) Qualitative Stability Characteristics of a Flexible Missile Subjected to a Circulatory Thrust		5. TYPE OF REPORT & PERIOD COVERED
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9. PERFORMING ORGANIZATION NAME AND	ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 611102,11.35D00
Benet Weapons Laboratory		
Watervliet Arsenal, Watervlie SARWV-RT-TP	et, N.Y. 12189	DA Proj. No. 1F161102A35D Pron No. EJ-5-Y0015
11. CONTROLLING OFFICE NAME AND ADDRE	ESS	12. REPORT DATE
US Army Armament Command		February 1977
Pock Island, Illinois 61201		13. NUMBER OF PAGES 29
14 MONITORING AGENCY NAME & ADDRESS	if different from Controlling Office)	18. SECURITY CLASS. (of this report)
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Circulatory Thrust Dynamics Flexible Missile Stability

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The stability characteristics of an elastic, flexible missile of constant mass, modelled mathematically as a system consisting of three rigid bars elastically hinged at the joints and subjected to a constant circulatory thrust, are examined. Plots of eigencurves are presented and used to identify the regions of stability, divergence, and flutter in related stability maps. For anti-tangential and sub-tangential thrusts, the system is found to be divergent for any sufficiently small, positive thrust. Moreover, flutter does not occur for anti-tangential and super-tangential thrusts.

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WVT-TR-77009	
6. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED
PARAMETRIC RESONANCE IN GUN TUBES	
	6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s)	8. CONTRACT OR GRANT NUMBER(*)
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PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Benet Weapons Laboratory	
Watervliet Arsenal, Watervliet, N.Y. 12189 SARWV-RT-TP	DA Proj. No. M7-7-R00146-01-M7 AMCMS No. 662603.H78001
U.S. Army Armament Command	February 1977
Rock Island, Illinois 61201	13. NUMBER OF PAGES
14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)	15. SECURITY CLASS. (of this report)
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17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different fro	om Report)
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O. ABSTRACT (Continue on reverse side if necessary and identify by block number) This work examines the likelihood of encou	ntering parametric
resonance in gun tubes. The resonance is induc	
the periodic changes in transverse stiffness in	duced by

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ballistic pressure - "single round parametric resonance".

(ii) the periodic applications of ballistic pressure such as encountered in an automatic weapon - "multiple round parametric resonance".

Results show that ballistic cycles currently employed in the 60mm MCAAAC semi automatic cannon are not likely to excite single round resonance. Unusually brief cycles, however, are shown to be capable of producing resonance amplifications of three orders of magnitude in less than twenty cycles of axial vibration. By proper design of the pressure cycle and/or the fundamental axial frequency of the tube, this type of resonance is rather easily avoided.

Further results show that for the 20mm M139 machine gun, amplifications in excess of fifty can be reached in under five seconds of continuous firing. A special application of the work of Krajcinovic and Herrmann leads to a set of instability contours from which the growth (characteristic) exponent can be determined as a function of the ratio of natural and excitation frequencies and the product of the ballistic impulse and the tube slenderness ratio. Control or elimination of multi-round resonance can be maintained either through control of the initial conditions or by designing for mismatch between the transverse frequencies and integral mulitples of one-half the excitation frequency, i.e., the firing rate.

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Dynamic Analysis of Constant Reaction Systems for a Medium Caliber, Anti-Armor, Automatic Cannon	
	6. PERFORMING ORG. REPORT NUMBER
P. M. Vottis J. K. Jorczak	8. CONTRACT OR GRANT NUMBER(*)
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US Army Armament Research and Development Command Power, New Jersey 07801	12. REPORT DATE March 1977 13. NUMBER OF PAGES 50
MINITORING AGENCY NAME & ADDRESS(II different from Controlling Office)	15. SECURITY CLASS. (of this report) Unclassified
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TH SUPPLEMENTARY NOTES

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Constant Reaction Constant Force Recoil

Automatic Weapons

Guns

Medium Caliber

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This report addresses the methodology used in determining a constant reaction force recoil system for the Medium Caliber, Anti-Armor, Automatic Cannon (MC-AAAC) Program, Test Bed #2. General theory and equations of motion which describe the primary elements are discussed. Solution is effected by numerical math modeling techniques. The results of a parametric study across ranges of key independent variables and system sensitivity analyses are presented. An optimal system candidate is selected and essential parameters established.

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Hydraulic Analysis of the Recoil and Counter- recoil Cycle in Medium Caliber, Anti-Armor,	5. TYPE OF REPORT & PERIOD COVERED
Automatic Cannon, Test Bed No. 2	6. PERFORMING ORG. REPORT NUMBER
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Medium Caliber Recoil Mechanisms Hydraulic Analysis Automatic Weapons

Recoil Buffer

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In this report the various stages of the recoil and counterrecoil stroke of the Medium Caliber, Anti-Armor, Automatic Cannon, Test Bed No. 2 are analyzed from a hydraulic point of view. The resulting equations relate the damping force created by flow of fluid within the device to the recoil velocity, the internal dimensions of the recoil mechanism, and the properties of the fluid. Working formulas are developed which can be integrated into a computer program for the recoil dynamics of the complete gun barrel-recoil mechanism.

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Failure Investigation105mm M68 Tubes	
(SN 16244, 7506, and 11837)	S PERFORMING ORG REPORT NUMBER
7 AUTHOR(a)	B CONTRACT OR GRANT NUMBER(A)
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9. PERFORMING ORGANIZATION NAME AND ADDRESS	IU. FROGRAM ELEMENT PROJECT - ASK
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18 SUPPLEMENTARY NOTES

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20 ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report summarizes the investigation of three 105mm M68 gun tube failures which occurred during routine training exercises in April and May of 1976. The tubes involved were Serial Numbers 16244, 7506 and 11837; the failures occured at Forts Knox, Lewis and Bliss, respectively. The conclusion of the investigation is that all three maifunctions were caused by premature, in-bore detonation of the projectiles involved.

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4. TITLE (and Subsited) Electrodeposited Cu and Cu-Al ₂ O ₃ Alloys: Physical and Mechanical Properties		5. TYPE OF REPORT & PERIOD COVERED 6. PERFORMING ORG. REPORT NUMBER
7. Author(*) G.R. Lakshminarayanan E.S. Chen F.K. Sautter		8. CONTRACT OR GRANT NUMBER(*)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 12189 SARWV-RT-TP		AREA & WORK UNIT NUMBERS AMCMS Code: 611101.91A0011 DA Proj. No. 1T161101A91A PRON No. 1A-7-51701-02-M7-M7
US Army Armament Research and Devel Dover, New Jersey 07801	opment Command	April 1977 13. NUMBER OF PAGES 5
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16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the abatract entered in Block 20, 11 different from Report)		
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Cu and Cu-Al ₂ O ₃ alloys were electrodeposited from copper sulfate and copper sulfate-Al ₂ O ₃ plating solutions repectively. Aluminum oxides of different sizes and crystalline phases were used as disperoids in the plating solutions. The properties measured for the deposits include the room temperature yield strength, ultimate tensile strength, elongation, hardness and electrical resistivity. The results show that a codeposition of 1.2 to 2.3 vol per cent calcined gamma oxide (See Other Side)		

20.

with copper increased the yield strength for the as-plated deposits by 65 to 145 per cent and the ultimate tensile strength by 35 to 70 per cent. Hardness was also increase in for the Cu-Al₂O₃ deposits. Elongation generally decreased with an increase in oxide content in the deposits. Annealed Cu-Al₂O₃ deposits retained their higher strength up to 480°C (800°F), after a decrease in strength was observed. Unlike Cu deposits, annealing decreased the ductility of Cu-Al₂O₃ deposits. The effects of cold rolling were about 6 to 10 per cent higher than those of Cu electrodeposits. The properties of electrodeposits prepared under ultrasonic agitation are also reported.

1. REPORT NUMBER WYT-TR-77016	REPORT DOCUMENTATION PAGE	
	2. GOVT ACCESSION NO.	BEFORE COMPLETING FORM 3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Electrodeposition of Cobalt Using an Insoluble Anode		5. TYPE OF REPORT & PERIOD COVERED
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G.R. Lakshminarayanan E.S. Chen J.C. Sadak F.K. Sautter		B. CONTRACT OR GRANT NUMBER(#)
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 12189 SARWV-RT-TP		AMCMS Code: 611101.91A0011 DA Proj. No. 1T161101A91A PRON No. 1A-7-51701-02-M7-M
11. CONTROLLING OFFICE NAME AND ADDRESS US Army Armament Research and Development Command Dover, New Jersey 07801		12. REPORT DATE April 1977
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as a function of additive concentration and plating time. The results show that besides cobalt deposition, vanadium ions of lower oxidation state (V++, V+++, V0++) are formed at the cathode and these ions seem to be responsible for the reduction and suppression of Co^3 + ions and the oxide at the platinum anode. It has also been observed that the concentration of the added electro-chemically active substance changed very little indicating no incorporation of vanadium with the deposit during plating. The mechanical properties of the deposits prepared using an insoluble anode are compared with those obtained using a soluble anode.

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The Effects of Chloride Ion on the Codeposition of Alumina with Copper			
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7. AUTHOR(*)	8. CONTRACT OR GRANT NUMBER(*)		
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9. PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS		
Benet Weapons Laboratory	AMCMS Code: 611101.91A0011		
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11. CONTROLLING OFFICE NAME AND ADDRESS	12 REPORT DATE April 1977		
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Electrodeposition Codeposition Additives	Adsorption		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)			
The inhibitory effect of chloride ions on the codeposition of Al_2O_3 from acid copper sulfate electrolytes was investigated. In general, increasing the chloride ion concentration in the copper electrolyte reduces the oxide codeposition in the deposits. The maximum chloride ion concentration tolerable is dependent on the size, crystalline phase and nature of the suspended particles.			

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The Effects of Pulse Current Platin Mechanical Properties of Cobalt and	ng on the		
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9 PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
Benet Weapons Laboratory		AMCMS Code: 611101.91A0011	
Watervliet Arsenal, Watervliet, N.Y. 12189 SARWV-RT-TP		DA Proj. No. 1T161101A91A PRON No. 1A-7-51701-02-M7-M7	
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE April 1977	
US Army Armament Research and Deve	elopment Command		
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Electrodeposition Codeposition Pulse Current Plating			
Mechanical Properties Structure Dispersion Strengthening			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)			
The effect of high current pulses on the mechanical properties of electro- deposited cobalt and Co-Al ₂ O ₂ was studied along with two other variables, ultra-			
sonic agitation and superimposed direct current. The deposit were prepared at			
pulse current densities between 0 ar	id 100 A/dm², a p	oulse width of 120 usec and	
a pulse repetition time of 18 msec. The strength and hardness of both cobalt and Co-Al ₂ O ₂ deposits made under these conditions showed substantial increases			
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over conventionally prepared deposits. The improvement in mechanical properties is attributed to the refinement in grain structure and the enhancement of ${\rm Al}_2{\rm O}_3$ codeposition associated with the use of current pulses.

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4. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
Ultrasonic and Acoustic Holographi Inspection of Composite Gun Tubes		
Components	and other weapon	6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s)		8 CONTRACT OR GRANT NUMBER(#)
George P. Capsimalis Giuliano D'Andrea		
Ralph E. Peterson		
9 PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
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Acoustics Composite Materials		
Holography		
Ultrasonics		
20 ABSTRACT (Continue on reverse side if necessary and	didentify by block numbers	
Ultrasonic and acoustic holog		as been shown to be an effec-
tive procedure for the nondestruct	ive inspection o	f flaws and voids in composite
and other material structures. Te		
shape and dustribution of flaws in	composites and	conventional materials are
discussed. Additionally a number of test results representing applications of ultrasonic and holographic imaging and their adaptation to typical material		
testing problems are presented.		

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7. AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(*)
San-Li Pu Julian J. Wu		
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Composite Tubes		
Cracks Plating		
Stresses		
Thermal Stresses		
Stress distribution in a thin thick tube is studied based on the mathematical models are used to re conditions. Results from these si chrome plating in a gun tube is ve perties of plating materials and t	n layer of platin e linear theory o epresent a variet imple mathematica ery likely to cra	g on the bore surface of a of elasticity. Several simple by of material and loading all models indicate that the lock. Relative mechanical pro-
the stress level in the plating.		

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Disks		6. PERFORMING ORG. REPORT NUMBER
J. A. Kapp		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Benet Weap ons Laboratory Watervliet Arsenal, Watervliet, N.Y	12189	AMCMS No. 3110.15.0003
DRDAR-LCB-TL	. 12105	PRON No. 32-6-P4957
"105 AFRO TAMBAREISE RESEARCH and Develo	onment Command	12. REPORT DATE
Large Caliber Weapon System Laborate	ory	May 1977 13. NUMBER OF PAGES 44
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18. SUPPLEMENTARY NOTES		
This report was presented as a	thesis for Grad	duate Studies.
19. KEY WORDS (Continue on reverse side if necessary and i	dentify by block number)	
Pressure vessels F	atique	Fracture Mechanics
Autofrettage S	tress Analysis	NASTRAN
20 ABSTRACT (Continue on reverse side if necessary and in	dentify by block number)	The office A of the other
residual stress distribution on the owalled disks has been investigated. the Paris power law relation. Stress ternally pressurized, externally flaw approximate technique and with the us program. A simple experiment was devon crack growth rate. The the test in	rack growth rat The crack growt intensity fact ed, non-autofre e of the NASTRA rised to determi	The effect of the autofrettage te in externally flawed thick- th rate was modeled by using tors were calculated for in- ettaged cylinders, by an AN finite element computer ine the effect of autofrettage
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cut from autofrettaged cylinders. NASTRAN was used to determine the stres intensity factors for this loading geometry. The experimentally observed results show that autofrettage increases the crack growth rate in external flawed cylinders, but the test did not supply sufficient data to mathemat ally model the increase. The faster crack growth rate is believed to be caused by the local relaxation of the tensile autofrettage residual stress due to large plastic zones accompanying crack growth.	ly ic-

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EFFECTS OF QUENCHING TECHN	NIQUES UPON	
GUN STEEL		6. PERFORMING ORG. REPORT NUMBER
AUTHOR(s)		8 CONTRACT OR GRANT NUMBER(a)
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Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 12189		AMCMS No.3297.06.7236
DRDAR-LCB-TL	11.11. 12.103	PRON No.M1-6-A1735-01-M7-M7
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Analytical and Experimental Tube	Temperatures	
in the 8" XM201 Cannon		
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(a)		8. CONTRACT OR GRANT NUMBER(.)
R. G. Gast		
P. M. Vottis		
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM FLEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Benet Weapons Laboratory	12100	AMCMS No. 664602.12.38900
Watervliet Arsenal, Watervliet, N.Y DRDAR-LCB-TL	. 12109	DA Proj. No. 1W664602D389
		Pron. No. 26-6-94012
US Army Armament Research and Devel	opment Command	
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Gun Barrels		
Guns		
Heat Transfer		
Thermal Test		
Temperature		
20 ABSTRACT (Continue on reverse side if necessary and		
A comparison is made between measured and predicted temperatures in the		
8" XM201 cannon. The gross construction of the thermal model is given and		
data from firing tests on the XM201 cannon are presented. Correlation is		
found to be good.		

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ARLCB-TR-77028		
1. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
The Abrasion Characteristics of Cer	rtain	
Protective Coatings on Aluminum and	d Magnesium	
Alloys		6. PERFORMING ORG. REPORT NUMBER
AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(.)
A. Campbell		
W. Mortimer		
P. Thornton PERFORMING ORGANIZATION NAME AND ADDRESS		
Benet Weapons Laboratory		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Watervliet Arsenal, Watervliet, N.Y.	12189	AMCMS No. 3297.06.7234
DRDAR-LCB-TL	12105	Pron No. M1-3-23021-01-M7-M7
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Abrasion		
Anodic Coatings		
Films		
0 ABSTRACT (Continue on reverse side if necessary and ide	ntify by block numbers	
The abrasion resistances of two aluminum and the other to ZK60A magnetirst anodized. Subsequently, a blue applied to the 2014 aluminum; the ZK6	finishing sys esium, were ev e-wash primer	aluated. Both alloys were and semigloss paint were
and a polyurethane topcoat. The test abrasion resistances of the two syste Abraser Model 503. Abrasion rates we	ts, performed ems, were carr	to compare the relative ied out using the Taber

Block 20 (cont)

Analysis of the data indicated that, under the test conditions applied, the topcoats contributed little to the overall abrasion resistance of the two coating systems; rather, the anodic layer of each appeared to be the most important parameter. Further, the rate of abrasion of the anodic layer was relatively constant in each case and could be approximated by a straight line relationship. The anodic film on the 2014 aluminum demonstrated significantly better resistance to abrasion than that on the ZK60A magnesium.

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A PROBABILISTIC MODEL OF GUN T	UBE FATIGUE	
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7. AUTHOR(s)		B. CONTRACT OR GRANT NUMBER(#)
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Cannon Gun Barrel Variability S	Probability ! tatistical Analys	
20 ARTTRACT (Continue on reverse side if necessary an	(identify by block sumber)	
A probabilistic model of gun tube crack initiation, growth and failu In the model, tube fatigue life is design parameters. The fatigue te M113El tubes are used as a base to meters. Monte Carlo Simulation st	fatigue is constree theories into given as a functor stresults for the estimate and valudies are then constructions.	a probabilistic framework, tion of random material and he 105MM M137A1 and 175MM riances of the model para- onducted by assuming various
probability distributions for the	model parameters	and computing the statistics

20.

of the distribution of fatigue life.

Results of the Monte Carlo studies indicate that (1) the best fit theoretical distributions of fatigue lives are the 2- and 3-parameter lognormal; (2) the greatest variability in fatigue life results from variability in residual stresses followed by variability in initial crack and fracture toughness; and (3) an effective means of increasing safe life might be through better control of the autofrettage residual stresses. Finally, use of the probabilistic model of gun tube fatigue might lead to (1) improved methods for statistical computation of safe life from test data and (2) improvement in the initial design approach for proposed gun tubes.

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COMPUTERIZING THE EFFECT OF TEMPERING ON THE	
MECHANICAL PROPERTIES OF A Ni-Cr-Mo STEEL	5. PERFORMING ORG. REPORT NUMBER
AUTHOR(a)	8 CONTRACT OR GRANT NUMBER(#)
Peter Dembowski	
PERFORMING ORGANIZATION VIME AND ADJIRESS	10. PROGRAM ELEMENT, PROJECT TASK
Benet Weapons Laboratory	AMCMS No. 3297.06.7588
Watervliet Arsenal, Watervliet. N.Y. 12189	PRON No. M1-6-A1726-01-M7-M
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Dover, New Jersey 07801	2 4
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results for the material austenitized at 845°C are presented in the form of three dimensional plots and contour maps which interrelate the mechanical property of interest and tempering temperature and time. Examples showing the use of the plots are presented.

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EROSION IN SIMM MORIAR IUB	E5	6 0505000000000000000000000000000000000
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V. Peter Greco		
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Coatings Mortars		
Erosion Particles		
Fins Propellants		
Gases Tubes		
Ignition Wear		
0. ABSTRACT (Continue on reverse side if necessary an	nd identify by block number)	
A laboratory erosion tester ha		and developed for predicting
the service performance of protect	ive coating mater	ials in the bores of mortar
systems using rounds with tail fine		
tion, the service life of 81MM more		
third of its original life as the		
lar groove erosion formed in the bo	ore. Preliminary	efforts to apply wear resis-
tant bore coatings and test fire th	hem in the field	have been extremely costly ar
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time consuming because of the large number of rounds required (approximately 7500).

The laboratory erosion tester has been designed to ignite the actual tail fin assembly (which causes the erosion) in a chamber which holds eight test specimens to be evaluated at the same time. The erosion rate of the test material can be increased so that less rounds are required, by merely reducing the distance of the jet stream and moving the specimens closer to the tail fin assembly which upon ignition, radially discharges the mixture of hot gases and associated burning particles onto the specimen surface.

This progress report presents the erosive behavior of eight candidate coatings which have been tested in the laboratory erosion tester. Laboratory results have shown that a five mil thick cobalt or cobalt alloy deposit should be suitable to resist erosion and increase the service life of the 81MM mortar system. An overlay of 2/10 of a mil of chromium over cobalt further increases the erosion resistance. Further testing is necessary to specifically determine the best cobalt system and chromium combination. The next effort would be to field test the coating in the actual mortar system to verify the laboratory results.

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A. VILLE (and Saturde) DEVELOPMENT OF PROTOTYPE PRODUCTION ESR FACILITIES	5 TYPE OF REPORT & PERIOD COVERED
	6 PERFORMING ORG. REPORT NUMBER
/ AUTHOR(s)	B CONTRACT OR GRANT NUMBER(*)
V.J. Colangelo	
PERSORMING ORGANIZATION NOTE AND ADDRESS Benet Veapons Laboratory	10 PROGRAM ELIMENT PROJECT TAN AREA & WORK UNIT NUMBERS
Waterviet Arsenal, Watervliet, N.Y. 12189 URDAR-LCB-IL	AMCMS No. 3297.06.7550 PRON No. M1-4-A1552
US Army Armament Research and Development Command	July 1977
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19 KEY WORDS (Continue on reverse side if necessary and identify by block number)	
Electroslag Remelting ESR Cas	st Hollows Near Net Shapes
This report describes the procedures employed to technique to manufacture Electroslag Refined Hollows to the Nutek Corp., Washington, Pa. The report describes together with the results obtained for each approach designs are included in the report.	s under a contract granted cribes the approaches taken

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Automatic Step Threading of Breechblocks		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(*) C. Rose		8 CONTRACT OR GRANT NUMBER(*)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 12189		10. PROGRAM ELEMENT PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 4497.06.6771 Pron No. M-1-1-23034
DRDAR-LCB-TL		
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
US Army Armament Research and Devel		June 1977
Large Caliter Weapon System Laborat	ory	13. NUMBER OF PAGES
Dover, New Jersey 07801		26
14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING
16. DISTRIBUTION STATEMENT (at this Report)		SCHEDULE

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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identity by block number)

Threads Step Threads Thread Shaping Blade Type Tooling

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report details the engineering design, development and application of equipment to produce step threads (constant lead thread on two or more diameters) on the breechblock of cannon. The equipment uses a blade type tool with the part being threaded through shaper type cuts until finish size is reached. The use of this equipment will reduce the floor to floor time from 7.5 hours to 2.0 hours while producing better thread finishes and more accurate dimensional sizes.

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
ARLCB-TR-77034	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
THE IMPLUENCE OF LATE WEAR LIFE 105MM M68 GUN TUBES ON DISCARDING SABOT AMMUNITION FLIGHT STABILITY AUTHORO Allan A. Albright Eugene E. Coppola Glenn S. Friar		5. TYPE OF REPORT & PERIOD COVERED
		6. PERFORMING ORG. REPORT NUMBER
		8. CONTRACT OR GRANT NUMBER(*)
Benet Weapons Laboratory Watervliet Arsenal, Watervliet, NY 12189 URDAR-LCB-UP		AMCMS No. A4110.16.2976 PRON No. M1-5-X9098-01-M7-M7
US Army Armament Research and Development Command Large Caliber Weapon Systems Laboratory Dover, New Jersey 07801 MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)		12. REPORT DATE July 1977 13. NUMBER OF PAGES 56
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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse aide if necessary and identify by block number)

Ammunition

Ammunition Dispersion

Erosion Gun Barrels

Tanks (Combat Vehicles)

20. ABSTRACT (Continue on reverse eide if necessary and identify by block number)

This report describes testing and analysis of 105mm M68 Gun tube wear and its influence on discarding sabot (DS) ammunition performance. Tests, conducted to identify gun tube wear parameters which influence DS projectile flight stability, are described. Models are developed to characterize gun tube wear in the fielded population and estimate outcomes of wear life reductions to exclude undesirable wear conditions. Impacts of tube wear life reductions are discussed, with consideration given changes in ammunition usage.

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ARLCB-TR-77035		
. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
EVALUATION OF 155MM M199 TUBE	FORGING PRODUCERS	
		6. PERFORMING ORG. REPORT NUMBER
AUTHOR(e)		8. CONTRACT OR GRANT NUMBER(a)
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J. Passmore		
PERFORMING ORGANIZATION NAME AND ADDI	ESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Benet Weapons Laboratory	N V 12100	AMCMS No. 3210,16.0015
Watervliet Arsenal, Watervliet, N.Y. 12189 DRDAR-LCB-TL		PRON No. M7-5-P4850-01-M7-M
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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identity by block number)

Cannon Tubes Forging Steel

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Two 155mm M199 howitzer tube forgings, produced by different vendors, were destructively tested to determine the quality of each vendor's forgings. Vendor A's forging did not meet military specifications in all cases; several RA values were below specification. Vendor B's forging was found to be acceptable, exceeding the requirements of the specifications in all cases.

REPORT DOCUMENTATION	N PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
I. REPORT NUMBER	2. GOVT ACCESSION NO.	
ARLCB-TR-77036		
. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
Reinforced Cobalt Alloy Composite for Turbine		
Blade Application		
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(*)		8. CONTRACT OR GRANT NUMBER(*)
I. Ahmad & J.M. Barr	ranco	
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Benet Weapons Laboratory		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Watervliet Arsenal, Watervliet,	N.Y. 12189	AMCMS No. 612105.H840011 DA Project No. 1L162105AH84
DRDAR-LCB-TL		PRON No. AW-7-R0003
1. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
US Army Armament Research and Dev	velopment Command	July 1977
Large Caliber Weapon System Labor	ratory	13. NUMBER OF PAGES
Dover, New Jersey 07801		12
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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
ARLCB-MR-77037		
4. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
Investigation of Fastener Failures in 105MM M68 Guns and 152MM M81 and M162 Gun Launchers		
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(6)
Morgan D. Longmate		
9 PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK
Benet Weapons Laboratory		AREA & WORK UNIT NUMBERS
Watervliet Arsenal, Watervliet, NY	12189	AMCMS No. 3110.15.9003 PRON No. M7-5-P4818-10-M7-M7
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11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
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Hydrogen Embrittlement		
Cadmium Embrittlement		
20. ABSTRACT (Continue on reverse side if necessary and	d identify by block number)	
This study was performed to deter	mine the cause(s) of the recurring bolt
failures occurring on the 105mm M		

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ARLCB-TR-77038		
4. TITLE (and Subtitle)		5. TYPE OF REPORT & PERIOD COVERED
VIBRATIONS OF A HELICOPTER ROTO	OR BLADE USING FINITE	
ELEMENT-UNCONSTRAINED VARIATION		6. PERFORMING ORG. REPORT NUMBER
7 *OTHOR(*)		8. CONTRACT OR GRANT NUMBER(a)
J.J. Wu		
C.N. Shen		
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URDAR-LCB-TL		PRON No. EJ-7-Y0011-01-EJ-M7
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Beams (Radiation) Rotation Coupling Effect Stabili Dynamics Vibration Flutter Helicopter Rotors O ABSTRACT (Continue on reverse side II necess In the past several years a generalized Rayleigh-Ritz - concept of Lagrange multiplies one to deal with problems asso	ty on s, a numerical method finite element discre rs and adjoint variab ociated with nonconser y conditions in a rout ation and dynamic stal	etization using the combined les. This approach enables rvative forces, coupling eff- tine fashion; and it appears bility problems associated

Block 20 (cont)

the first application of the general method of the vibration problem of such a rotor blade.

The basic differential equations in this paper are taken from the linear, but fully coupled set developed by Houbolt and Brooks in 1956. These equations are further reduced to a simplest possible case and yet still contain the coupling of flap and root torsion modes. An unconstrained, adjoint variational statement has been established which is both the necessary and sufficient condition for the coupled differential equations and some general, but physical meaningful boundary conditions. The finite element matrix equations are then derived from this variational statement illustrating the way that coupling terms could be handled in general.

The numerical results from some demonstrative examples show that instability of flutter can occur in the range of operational rotor speed due to the coupled motion of flapping and root torsion without any aerodynamic force, if the torsional spring (or the pitch control link) is not sufficiently stiff. This instability does not appear to have been reported previously.

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
ARLCB-TR-77040	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
PROBABILISTIC MODELS OF GUN-TUBE FATIGUE BASED ON A FRACTURE-MECHANICS MODEL 7. AUTHOR(*) E. E. Coppola		5. TYPE OF REPORT & PERIOD COVERED 6. PERFORMING ORG. REPORT NUMBER
		8. CONTRACT OR GRANT NUMBER(s)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 12189 URDAR-LCB-TL		10. PROGRAM ELEMENT PROJECT TASK AREA & WORK UNIT NUMBERS AMCMS No. 611102.H540011 DA Proj. No. 1L61102AH54 PRON No. 1A-7-51700-1A-M7
US Army Armament Research and Development Command Large Caliber Weapon System Laboratory Dover, New Jersey 07801		12. REPORT DATE October 1977 13. NUMBER OF PAGES 52
14 MONITORING AGENCY NAME & ADDRESS(II differe	nt from Controlling Office)	15. SECURITY CLASS. (of this report) UNCLASSIFIED 15a. DECLASSIFICATION DOWNGRADING SCHEDULE

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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Fatigue Mathematical Models
Fracture (Mechanics) Monte Carlo Method
Gun Barrels Probability
Life Span Simulation

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Two probabilistic models of gun tube fatigue (those of Racicot and of Proschan and Sethuraman) have been recently developed by adding probabilistic elements to a deterministic model of fatigue failure. These probabilistic models are examined to determine if they give adequate representations when certain questionable assumptions are lifted. In addition, the deterministic model is cast into a more general probabilistic framework, and the effects of certain statistical assumptions are examined.

(Continued on reverse side)

Continued from block 20.

Monte Carlo simulation studies are conducted to approximate possible distributions for gun tube fatigue lives. These generated distributions are compared to various theoretical distributions to determine their adequacy in representing fatigue data. A randomizing method of selecting distributions for material properties of the gun tube is used to give some independence from unwarranted assumptions.

Results of the simulation studies indicate that the lognormal distribution generally gives the best fit to the fatigue lives, but in most cases the lognormal distribution can be rejected by goodness-of-fit tests.

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
ARLCB-TR-77041	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
ISOPARAMETRIC ELEMENTS AS SINGI CRACK PROBLEMS	ULAR ELEMENTS FOR	5. TYPE OF REPORT & PERIOD COVERED	
M. A. Hussain W. E. Lorensen		6. PERFORMING ORG. REPORT NUMBER 8. CONTRACT OR GRANT NUMBER(s)	
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7. DISTRIBUTION STATEMENT (of the abetract en	ntered in Block 20, if different fro	m Report)	
8 SUPPLEMENTARY NOTES			
9. KEY WORDS (Continue on reverse alde if necess Finite Elements Fracture (Mechanics) (soparametric	ary and identify by block number)		
The quadratic isoparametric singularity, are used for calcularacks. The elements used are triangular (6-node) and three-distingularity elements are obtained at quarter points in the value of the same of the sam	c elements, which em lating the stress in the quadratic quadri imensional quadratic ed in a simple manne	lateral (8-node), quadratic 'brick' (20-node) elements. r by placing the mid-side	

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Block 20 (cont)		
ments are implemented in <u>NASTRAN</u> as dummy (user) elements. The method eliminates the use of special crack tip elements and in addition, these elements satisfy the constant strain and rigid body modes required for convergence. The stability of two-dimensional elements is also investigated.		

	REPORT DOCUMENTATION	PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
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	Rotating Beam	Beam Vibrations	Damping
	Finite Elemen	ts Vari	ational Statement
20 ARSTR	ACT (Continue on reverse side if necessary an	d Identify by block number)	
The structur first de of a rot che supp can obvi	e paper presents a formulational problems and a specific a rived from the versatile undating beam is used here as a port can be present due to enough affect the frequencies	on for the study application. A fromstrained variate concrete example ther local deflects of the rotating	of damping effects in dynamic linite element formulation is tional approach. The vibration of the viscous damping terms at action or rotation. These terms beam. They are easily incomposition of unconstrained (See Reverse

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered) Continued from Block 20. variations. Numerical data will be presented to demonstrate the qualitative as well as quantitative effects on the vibratory behavior of this rotating beam due to such damping terms.

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Steve Tausche Peter Thornton	n ,		
PERFORMING ORGANIZATION NAME AND AD Benet Weapons Laboratory Watervliet Arsenal, Watervliet DRDAR-LCB-TL		10. PROGRAM ELEMENT, PROJECT, TASK AMCMS No. 3111.16.2223 PRON No. M1-7-RN114-01-M7-1A	
US Army Armament Research and Large Caliber Weapon Systems L. Dover, New Jersey 07801	Development Command	November 1977 13. NUMBER OF PAGES 20	
14 MONITORING AGENCY NAME & ADDRESS(III	different from Controlling Office)	15. SECURITY CLASS. (of this report) UNCLASSIFIED	
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19. KEY WORDS (Continue on reverse side if neces	ssary and identify by block number)		
Split Ring Temper Embrittlement Transition Temperature			

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

In November 1976, several 155mm Howitzer M185 split rings failed during various stages of manufacture. A failure analysis consisting of metallography, SEM, and mechanical testing, was undertaken. This investigation concluded that the heat treatment was responsible for embrittling the steel, thereby causing the failures. Furthermore, it was shown that the required hardness could not be achieved without seriously compromising the toughness of this material.

DEAD INSTRUCTIONS

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
ARLCB-TR-77044	SSION NO. 3. RECIPIENT'S CATALOG NUMBER
A. TITLE (and Subtitle) DESIGN AND PRODUCTION OF BALLISTIC GUNS NO AND 3 AND THE INITIAL TEST BED GUN FOR THE	
MEDIUM CALIBER ANTI-ARMOR AUTOMATIC CANNON PROGRAM	6. PERFORMING ORG, REPORT NUMBER
P.M. Vottis R.L. Billington R.C. Sillery	8. CONTRACT OR GRANT NUMBER(*)
9. PERFORMING ORGANIZATION NAME AND ADDRESS Benet Weapons Laboratory Watervliet Arsenal, Watervliet, N.Y. 1218 DRDAR-LCB-DS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS US Army Armament Research and Development	12. REPORT DATE Command Novermber 1977
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16. DISTRIBUTION STATEMENT (of this Report)

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- 18. SUPPLEMENTARY NOTES
- 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Medium caliber Automatic cannon Ballistic gun Test gun

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Design rationale and construction details are presented for Ballistic Guns Nos 2 and 3 and the Initial Test Bed gun for the Medium Caliber Anti-Armor Automatic Cannon Program.

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ARLCB-TR-77045		
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STRUCTURE FACTORS IN AMORPHOUS AND DISORERED HARMONIC DEBYE SOLIDS		6. PERFORMING ORG, REPORT NUMBER
7. AUTHOR(s)		8. CONTRACT OR GRANT NUMBER(s)
L.V. Meisel and P.J. Cote		
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK
Benet Weapons Laboratory		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 611101.91A0011
Watervliet Arsenal, Watervliet, New York 12189		
DRDAR-LCB-RP		PRON No. 1A-7-51701-(02)-M7
1. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE
US Army Armament Research and Deve	elopment Command	December 1977
Large Caliber Weapon Systems Labor	ratory	13. NUMBER OF PAGES
Dover, New Jersey 07081		3
4. MONITORING AGENCY NAME & ADDRESS(II different	from Controlling Office)	15. SECURITY CLASS. (of this report)
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18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Amorphous Solids

Disordered Crystals

X-Ray Scattering

Neutron Scattering

Electrical Transport

Structure Factors

20. ABSTRACT (Continue as reverse side if necessary and identity by block number)

Expressions for the static and dynamic structure factor of Van Hove and for the static structure factors appropriate for x-ray and neutron scattering and for resistivity are presented in harmonic approximation for amorphous and disordered solids having a Debye phonon spectrum. A useful model dynamic structure containing a temperature-dependent function of K is defined. The high- and low- temperature limiting forms are examined in detail and the entire

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ARLCB-TR-77046					
4. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED				
EMBRITTLEMENT OF GUN STEEL BY LIQUID LEAD					
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7. AUTHOR(e)	8. CONTRACT OR GRANT NUMBER(*)				
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M.H. Kamdar					
9. PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 611102.H540011				
Benet Weapons Laboratory	AMCMS No. 611102.H540011 DA Proj. No. 1L161102AH54				
Watervliet Arsenal, Watervliet, N.Y. 12189 DRDAR-LCB-TL	PRON. No. 1A-7-51700-1A-M7				
11. CONTROLLING OFFICE NAME AND ADDRESS	12. REPORT DATE				
US Army Armanent Research and Development Command					
Large Caliber Weapon Systems Laboratory	13. NUMBER OF PAGES				
Dover, New Jersey 07801 14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)	15. SECURITY CLASS. (of this report)				
	Unclassified 15a. DECLASSIFICATION/DOWNGRADING				
	SCHEDULE				
16. DISTRIBUTION STATEMENT (of this Report)					
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17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different fro	om Report)				
18. SUPPLEMENTARY NOTES					
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)					
Fracture					
Guns Liquid Lead Embrittlement					
Steel					
20. ABSTRACT (Continue on reverse side if recessary and identify by block number)					
	A study has been made of the fracture behavior of gun steel in liquid lead and inert argon environments at 630°K in monotonic, static and cyclic				
fatigue test conditions. Smooth and notched specimens tested under the above					
conditions were severely embrittled by liquid lead and failed by intergranu-					
lar mode as compared to a ductile mode in argon. Smooth specimens tested					
monotonically and in static fatigue failed in a catastrophic manner near the					

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yield stress of the steel. Specimens with machined notches and with a fatigue crack at the root of the notch tested in liquid lead failed at the stress intensity values of 35 Ksi/In and 7 Ksi /In static fatigue and cyclic fatigue tests respectively, whereas in inert argon environment fatigue precracked specimens failed in cyclic fatigue at 135 Ksi /In. The susceptibility to embrittlement of steel specimens in liquid lead tested in cyclic fatigue was the same whether the notch was as machined or had a fatigue precrack at the root of the notch, i.e., embrittlement was independent of the sharpness of the root radii. These and other results are discussed in terms of the prevalent "reduction in cohesion" mechanism of liquid metal embrittlement proposed by Westwood and Kamdar. The critical conditions and prerequisites for the occurrence of embrittlement of gun steel in liquid lead are also duscussed.

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Benet Weapons Laboratory		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Watervliet Arsenal, Water		
DRDAR-LCB-RA	12103	
1. CONTROLLING OFFICE NAME AND	ADDRESS	12. REPORT DATE
	ch and Development Command	December 1977
Large Caliber Weapon Sys		13. NUMBER OF PAGES
Dover, New Jersey 0708	DRESS(If different from Controlling Office)	15. SECURITY CLASS. (of this report)
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		UNCLASSIFIED
		15a. DECLASSIFICATION DOWNGRADING
6. DISTRIBUTION STATEMENT (of this	Report	1
17. DISTRIBUTION STATEMENT (of the	abstract entered in Block 20, if different fro	om Report)
8. SUPPLEMENTARY NOTES		
9. KEY WORDS (Continue on reverse aid	le if necessary and identify by block number))
Fracture Mechanics	Finite-Element Method	Cubic, quadrilateral
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Isoprametric Elements	Singular Elements	Stress Intensity Factors
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shown that the inverse s tip can be obtained by selements into triangular mid-side nodes of each s	the simple technique of col r elements around the crack	the strain field at the cra- llapsing the quadrilateral tip and placing the two 9 and 4/9 of the length of
,	is analyous to practi	ig the mid side nodes at

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quarter points in the vicinity of the crack tip for the quadratic, isoparametric element.

The advantage of this method are that the displacement compatibility is satisfied throughout the region and that there is no need of special crack tip elements. The stress intensity factors can be accurately obtained by using general purpose programs having isoparametric elements such as NASTRAN. The use of 12-node isoparametric element program APES may be simplified by eliminating the special crack tip elements.

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ARLCB-TR-77048					
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ENERGY AND PRESSURE CALCULATION F	OR METALLIC				
NH ₄		6. PERFORMING ORG. REPORT NUMBER			
7. AUTHOR(a)		8. CONTRACT OR GRANT NUMBER(#)			
No monto					
D.M. Gray					
1					
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 611102.11.AH60			
Benet Weapons Laboratory					
Watervliet Arsenal, Watervliet,	I.Y. 12189	DA Proj No. 1L161102AH60			
DRDAR-LCB-TL		PRON No. GG-8-25496-GG			
11. CONTROLLING OFFICE NAME AND ADDRESS	1	12. REPORT DATE			
US Army Armament Research and Dev		December 1977			
Large Caliber Weapon Systems Labo	ratory	69			
Dover, New Jersey 0708]	t from Controlling Office)	15. SECURITY CLASS. (of this report)			
		UNCLASSIFIED			
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE			
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16. DISTRIBUTION STATEMENT (of this Report)					
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18. SUPPLEMENTARY NOTES					
19. KEY WORDS (Continue on reverse side if necessary at	d identify by block number)				
Equations of State	Phase Tran	sformations			
Funny Sodium Pressure					
Metallic Ammonium					
20. ABSTRACT (Continue on reverse side if necessary an					
It has long been known that	the ammonium ion	NH ₄ behaves in many ways			
like an alkali metal ion. This report discusses a possible transition (under					
pressure) from a mixture of ammonia and hydrogen (NH3-½H2) to metallic NH ₄					
in the "funny sodium" form. This form may be defined as a lattice composed of metallic NH ₄ ⁺ ions and s-like electrons (one per ion). The ion has the sodium Z number but only seven protons (those from N) are in the nucleus; the					
sodium 7 number but only seven pe	cotons (those fro	m N) are in the nucleus: the			
30d ruin & number but only seven pr	otons (those fro	m n, are in the nucleus; the			

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other four protons (those from the four H atoms) form a tetrahedral arrangement around the N nucleus. This tetrahedral arrangement is then approximated by a spherical shell at a radius determined by a variational calculation for the total energy of the tetrahedral ion. (The resulting radius lies well out in the ion electron cloud.) Since a Wigner-Seitz polyhedra approach is used no specific lattice structure is considered. We comment on the earlier calculation of Bernal and Massey (BM) and the more recent calculation of Stevenson. Emphasis is on the BM metallic calculation which we have essentially repeated.

The concept of exchange is described, derivation of the Fock equations is given, and the principal equation of BM (one electron outside a closed shell) is then derived from the Fock equations.

The BM equation is then solved by computer for both the no-exchange and exchange-included cases. Our (unsuccessful) attempts to reproduce the BM results for the no-exchange case are described briefly. Our calculation for the exchange-included case is then described in some detail. For this case we find the internal energy at the equilibrium volume to be about 0.5 ev higher than that obtained by BM (our value is very close to Stevenson's -5.36 ev). Stevenson's equilibrium radius is 5.35 a.u., BM's is 4.23 a.u.; we obtain 4.99 a.u., i.e., shifted considerably toward Stevenson's value. In spite of these differences in U vs V between our results and BM's, our Gibbs energy vs pressure curve is about like theirs.

If the Stevenson mixture curve for U vs V is accepted, the BM and the present metallic calculation make a transition to "funny sodium" NH₄ unlikely (at least below the Mbar region). Acceptance of the Stevenson metallic U vs V curve would make such a transition unlikely at any pressure. We consider transition to the "funy sodium" form to be unlikely; transition to other metallic forms are probably in the Mbar (and above) range.

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