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**STATE-OF-THE-ART FOR ASSESSING
EARTHQUAKE HAZARDS IN THE
UNITED STATES.**

Report 8

**DURATION, SPECTRAL CONTENT, AND PREDOMINANT
PERIOD OF STRONG MOTION EARTHQUAKE RECORDS
FROM WESTERN UNITED STATES.**

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The purposes of this investigation were principally to assess the duration and spectral content of strong-earthquake accelerograms and, indirectly, to consider their applicability in earthquake design. Correlations of duration with MM intensity for the near and far fields and for Richter magnitude have been obtained. Difference in durations for soil and rock sites was determined. A set of relations between the duration and distance for soil and rock sites was <p style="text-align: right;">(Continued)</p>		

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20. ABSTRACT (Continued)

established from records of the San Fernando Earthquake of 9 February 1971 (magnitude of 6.5). Values for other magnitudes were extrapolated. Duration is taken to be the time interval between the first and last peaks of acceleration equal to or greater than 0.05 g.

The spectral content in the range of 0.1-10 Hz for strong-motion records in western United States for acceleration level equal to or greater than 0.05 g was processed with the modified Nigam and Jennings' response spectra computer programs. The corrected accelerograms on the digital magnetic tapes of NIS 130, 131, and 132 provided by the California Institute of Technology were the input data for this study. The critical damping ratios of 5.0, 7.5, and 10.0 percent were assigned to the soil (or soft, alluvial), intermediate (firm sediments), and rock (or hard) sites, respectively. The relative response spectral amplitudes of acceleration, velocity, and displacement were reduced to the ground surface by dividing the relative response spectral amplitude by the dynamic amplification factor of $1/2h$, where h is the critical damping ratio. The frequency-amplitude spectra were then plotted as a function of magnitude, epicentral distance, and site conditions.

The characteristics of duration are as follows: (a) duration is greater in the near field than in the far field and greater in alluvium than in rock with the duration-ratio of alluvium to rock approximately 2 to 1; (b) duration increases with magnitude and intensity, as expected; and (c) the maximum duration at a source in rock for magnitude 8.5 was extrapolated to be about 43 sec. The duration is twice as long where there is magnification by alluvium or soil.

Frequency content and spectral shape have the following characteristics: (a) the predominant frequencies of the strong-motion earthquakes for the magnitude of 5.3-7.7 are in the range of 0.1-6.67 Hz; (b) the maximum acceleration, velocity, and displacement levels are within the ranges of 1.5-5.0, 0.5-1.5, and 0.1-0.5 Hz; (c) the predominant period of the acceleration spectra does not increase with distance within the range of 0-90 km, but the predominant period of displacement does; (d) the spectral mode shape depends on the source spectrum function (magnitude), distance, and local geological conditions; (e) generally, the average or upper-bound peak amplitudes have a uniform envelope, but the possible maximum acceleration was found to be about 0.5 g near surface faulting for the discrete frequency range of 4-5 Hz; and (f) the summation of the maximum amplitude level of the predominant frequencies equals approximately the total amplitude of the ground motion in time history if the selected damping ratio corresponds to the geological condition of the recording site. An assumption is made that the amplitudes of all discrete frequencies on the envelope are in phase.

PREFACE

This report is part of ongoing work at the U. S. Army Engineer Waterways Experiment Station (WES) in Civil Works Investigation Study: "Methodologies for Selecting Design Earthquakes," sponsored by the Office, Chief of Engineers (OCE). General direction was by Mr. James P. Sale, Chief, Soils and Pavements Laboratory, and Mr. Don C. Banks, Chief, Engineering Geology and Rock Mechanics Division. Preparation of the report was by Mr. Frank K. Chang, Earthquake Engineering and Vibrations Division and Dr. Ellis L. Krinitzsky, Chief, Engineering Geology Research Facility.

The report was reviewed by Dr. Bruce A. Bolt of the University of California at Berkeley, and Dr. Shan S. Kuo of the University of New Hampshire at Durham. To both of them, the authors wish to express their appreciation.

COL J. L. Cannon, CE, and Mr. F. R. Brown were Director and Technical Director, respectively, of WES during the period of this study.

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STATE-OF-THE-ART FOR ASSESSING EARTHQUAKE
HAZARDS IN THE UNITED STATES

DURATION, SPECTRAL CONTENT, AND PREDOMINANT PERIOD OF STRONG
MOTION EARTHQUAKE RECORDS FROM WESTERN UNITED STATES

PART I: INTRODUCTION

1. This investigation evaluates the duration, spectral content, and predominant period of strong motion records from western United States for parameters that are significant in earthquake design.

Previous Work

2. Gutenberg and Richter¹ presented the following equation for duration as a function of magnitude:

$$\log t_o = -1.4 + 0.32 M \quad (1)$$

where

t_o = time of duration in seconds at point of origin

M = magnitude in the Richter scale

Their source of data was the standard torsion seismograms. Esteva and Rosenblueth² described the duration of an equivalent ground motion with uniform intensity per unit time by the equation:

$$s = 0.02e^{0.74 M} + 0.3\Delta \quad (2)$$

where

s = duration in seconds

Δ = source to station distance in kilometres

Housner³ suggested an upper bound for duration of ground shaking during large earthquakes by a linear law expressed as

$$D = 11.2 M - 53 \quad \text{for } M > 5 \quad (3)$$

where D represents duration in seconds. If M equals 8.5, the duration is about 45 sec. The study of Bolt⁴ for the "bracketed duration" D of acceleration greater than 0.05 g as a function of M yields the formula:

$$D = 17.5 \tanh (M - 6.5) + 19.0 \quad \text{for } f > 1 \text{ Hz} \quad (4)$$

$$D = 7.5 \tanh (M - 6.0) + 7.5 \quad \text{for } f > 1 \text{ Hz} \quad (5)$$

Relating magnitude to duration for threshold values of 0.05 g, Kobayashi⁵ gave this equation

$$\log_{10} t_{0.05} = 0.50 M - 2.26 \text{ sec} \quad (6)$$

An effort was made by Husid,⁶ to compute the effective duration of shaking based on the concept of energy (Arias⁷). In their approach, the digitized acceleration values were squared, and the sum of the values was accumulated. A plot (Figure 1) of the accumulated value against time (adopting the 95 percentile time interval) has a shape resembling a cumulative distribution curve and provides a direct graphical representation of the duration effects.

3. It should be noted that the site effects on duration were not evaluated in any of the above-mentioned papers.

4. Recently, Trifunac and Brady⁸ attempted to give a modified definition of the duration of strong earthquake ground motion from the concept of Husid.⁶ They define the duration of the recorded strong motion to be that time interval during which the most significant contribution is made to an integral of the form $\int_0^T f^2(t) dt$ ^{6,7} where f(t) stands for acceleration a(t), velocity v(t), or displacement d(t), and T is finite or infinite. They arbitrarily delete the first 5 percent and the last 5 percent of the amplitudes of these integrals

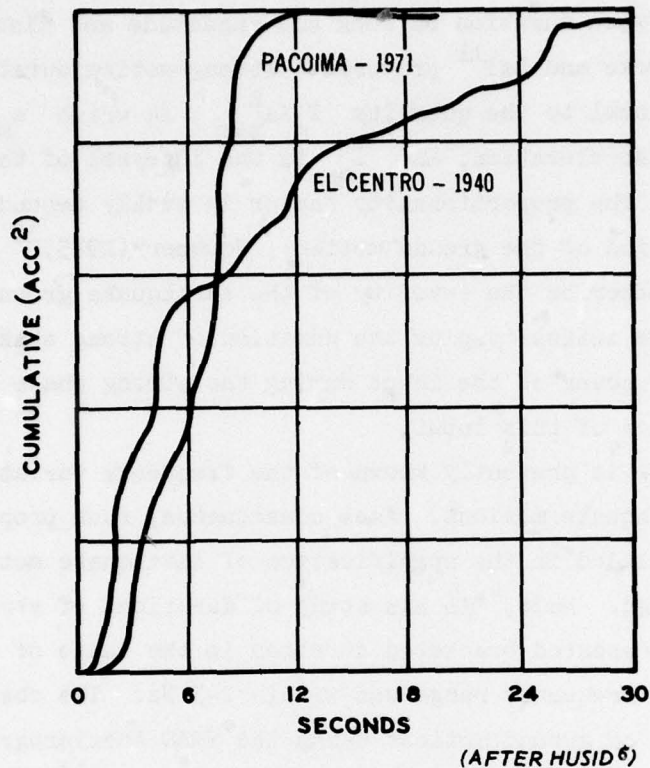


Figure 1. Graph of cumulative squared acceleration values versus time for Pacoima (1971) and El Centro (1940) records; the durations are 12.0 and 25.8 sec, respectively (both durations agree with the results in Appendix B)

and define the remaining 90 percent as the "significant" or "strong-motion" contribution. Their definition of duration is closely related to seismic energy and associated spectral amplitudes. Correlations were established among the following parameters: duration, velocity, displacement, Modified Mercalli (MM) intensity, earthquake magnitude, site geology, and epicentral distance. Hays⁹ studied the durations of earthquakes and nuclear explosions and then defined duration as absolute acceleration > 5 percent g . Site geology was completely ignored. Dobry et al.¹⁰ conducted a study of duration of horizontal records in the western United States on site conditions from rock to soft clay

based on the definition of Trifunac and Brady. They found a consistent correlation between duration on rock and magnitude and distance to the source. Vanmarcke and Lai¹¹ proposed a strong-motion duration that is nearly proportional to the quantity I_o/a_{max}^2 , in which a_{max} is the maximum ground acceleration, and I_o is the integral of the squared accelerations. The proportionality factor is weakly dependent on the predominant period of the ground motion. Housner (1975)¹² suggested two parameters to describe the severity of the earthquake ground motion: (a) the spectrum intensity plus the duration of strong shaking, or (b) the average power of the input during the strong phase of shaking plus the duration of this input.

5. Little is presently known of the frequency variations in time history of earthquake motions. As a consequence, such properties are not usually included in the specification of earthquake motions for structural design. Bolt,⁴ in his study of durations of strong earthquake motion, presented bracketed duration in the range of 0.5-10.0 Hz. The predominant frequency range was within 2-5 Hz. The observed frequency range of ground motions using the SMAC Accelerograph in Japan is approximately between 0.25 and 7.0 Hz (Kobayashi).¹³ A systematic analysis of strong motion accelerograms for the western United States since the Long Beach Earthquake (California) of 1933 has been performed and published in Volumes III and IV of a report series (Volume I contains uncorrected accelerograms and Volume II corrected data) by the California Institute of Technology (CIT).¹⁴ Volumes III and IV deal with response spectra and Fourier amplitude spectra, respectively. The undamped response spectra of 0 percent critical damping and Fourier amplitude spectra are in good correlation. The response spectral data for the period range between 0.04 and 15.0 sec, or 0.06 and 25.0 Hz, have been presented both graphically and numerically. Based on the presentations of Fourier amplitude spectrum of acceleration in Volume IV, the predominant peaks at 95 percent confidence level are within 0-5 Hz; however, there are some cases where the 95 percent confidence level extends to about 10 Hz.

6. Newmark¹⁵ established the frequency bands of the response

spectra at the critical damping ratio of 0.5, 2.0, 5.0, and 10.0 percent. They are used for averaging the amplifications of displacement, velocity, and acceleration as follows:

Horizontal displacement	0.2-0.4 Hz
Horizontal velocity	0.4-2.0 Hz
Horizontal acceleration	2.0-6.0 Hz
Vertical displacement	0.1-0.3 Hz
Vertical velocity	0.3-3.0 Hz
Vertical acceleration	3.0-10.0 Hz

These values indicate that the predominant frequency range of the strong earthquakes is within 0.1-10.0 Hz. The site condition is completely ignored.

7. Blume¹⁶ studied the response spectrum shapes for 33 significant and different accelerograms generated by 12 major earthquakes with damping ratios of 0.005, 0.01, 0.02, 0.05, 0.07, and 0.10. He found that the effect of duration on the shape of the response spectrum is small for frequencies greater than 2 Hz and that the dynamic amplification factor at longer periods, however, tends to be higher for long duration motions than for short ones.

Definition of Duration and Scope

8. The "bracketed" duration is defined as the time interval between the first and last peaks of acceleration equal to or greater than 0.05 g for the strong earthquake record. This definition has been used by Page et al.¹⁷ and Bolt.⁴ Durations in Appendix B were computed in this manner. Figure 1 (Husid⁶) shows the "effective durations," formed by summing the squared digitized accelerations and the values accumulated against time, for the horizontal components of the Pacoima Dam record of the San Fernando Earthquake (California), 9 February 1971, and of the El Centro record of the Imperial Valley Earthquake (California), 18 May 1940. The durations are 12.0 and 25.8 sec, respectively. Appendix B presents approximately the same values of duration for these

two earthquake records, probably a coincident case. For a general case, further investigation is needed.

9. Values for the duration of strong earthquake shaking are determined by magnitude, amplitude, distance, site geology, and wave frequency. These factors will be examined in the following paragraphs.

Definition of Spectral Content

10. Fourier spectrum and relative response spectrum are two useful tools for defining the frequency content of a time signal. Since earthquake engineers are familiar with the response spectrum technique (RST), this method will be used in this study. The frequency bands of the response spectra, established by Newmark¹⁵ within 0.1-10 Hz for acceleration, velocity, and displacement, are also to be adopted. However, only the relative response spectral peak amplitudes, i.e., acceleration, velocity, and displacement of the predominant peak frequencies, will be considered and reduced to the ground surface by dividing the peak amplitudes by the dynamic amplification factor (DAF) or $1/2h$, where h is the critical damping ratio. This relationship can be expressed as

$$\text{Ground peak amplitude spectrum} = \frac{\text{Relative response peak amplitude spectrum}}{\text{DAF}}$$

There are two important justifications for this relationship. First, the peak amplitudes of the discrete predominant frequencies at the ground surface or base could be summed to obtain the approximate resultant amplitude by assuming them in phase, if this computed resultant amplitude is in agreement with the observed maximum amplitude in a seismogram. In this way, the critical damping ratio at a different geological site-model (soil or rock) can be compared. The resultant peak amplitude will be conservative, i.e., an overestimate. For an actual ground motion, the phase angle between the various frequencies should be considered. Secondly, an arbitrary seismogram of any frequency content and duration could be generated using the principle of

mode superposition. Tentatively, the critical damping ratios of 5.0, 7.5, and 10.0 percent will be assigned to the response spectra for the soft (soft alluvium or soil), intermediate (sedimentary rock), and hard rock (basement or crystalline rock) sites, respectively, as classified by Trifunac and Brady.⁸ Usually, the frequencies of seismic waves in rock are higher than in soil; the amplitudes are attenuated more rapidly in the former than in the latter (Duke et al.,¹⁸ Donovan,¹⁹ and Seed et al.²⁰).

PART II: TECHNIQUES FOR DATA PROCESSING

11. The theoretical background of RST can be found in Housner,²¹ Biot,²² Housner et al.,²³ and Hudson.^{24,25} The functions of the RST computer program and the data collection are discussed below.

Computer Program

12. The Nigam and Jennings' integration and response spectral computer programs²⁶ were modified to obtain the following:

- a. The time interval between the first and last peaks of acceleration in the frequency bank of 0.1-10.0 Hz was equal to or greater than 0.05 g for each strong motion accelerogram recorded in the western United States during the past four decades. (The corrected accelerograms in CIT Volume II were used.)
- b. The peak amplitudes (acceleration, velocity, and displacement) of the relative response spectra and the frequencies corresponding to those peaks were compiled in the sequence of magnitude, distance, and site conditions shown in Appendix B.
- c. The relative peak amplitudes of the response spectra were reduced to ground surface by dividing by DAF, or $1/2h$, where h is the critical damping ratio. The critical damping ratios of 0.05, 0.075, and 0.10 were assigned to each recording site in accordance with its classification as soil (soft), intermediate, and hard rock, respectively. This information was provided by the Earthquake Engineering Research Laboratory, CIT (Appendix A). The DAF for 0.05, 0.075, and 0.10 percent critical damping are 10.0, 6.66, and 5.0, respectively.

Data Collection

13. All strong-motion accelerograms ($\text{acc} \geq 0.05 \text{ g}$) recorded on the free-field and basement of a building for the western United States (from the Long Beach Earthquake, 10 March 1933, to the San Fernando Earthquake, 9 February 1971) were included in this study. These data represented 25 of the 57 earthquakes (Appendix A), 107 recording stations, 201 horizontal accelerograms, and 54 vertical accelerograms.

Appendix A and Appendix B list the items of information, such as the record file (CIT system), station location, date of earthquake, epicentral distance, Richter magnitude, MM intensity (Krinitzsky and Chang,²⁷) local MM intensity, and site condition (information provided by Dr. Brady, formerly of CIT).

14. The data in Appendix B, compiled from the output of the modified Nigam and Jennings' integration and response spectra computer programs,²⁶ include the record file (column 1 of Appendix A), instrument component, peak acceleration, duration, predominant period of acceleration, velocity, and displacement peaks. CIT prepared digitizations of the accelerograms on magnetic tape.

15. The spectrum shapes were computed for a period range of 0.1-10.0 sec or a frequency range of 0.10-10.0 Hz.

PART III: DATA ANALYSES

16. The data listed in Appendixes A and B have been processed for the analysis of duration, spectral content, and spectral shape.

Analyses of Durations

17. The duration data in Appendix B have been plotted as a function of frequency, magnitude, intensity, distance, and site condition.

Duration as a function of frequency

18. Generally, the range of the predominant frequency content in the strong-motion earthquake accelerograms does not vary greatly with duration, magnitude, and site geological conditions. Figures 2-6 show these relationships. The frequency band between 0.1 and 6.66 Hz was encompassed in the duration. On alluvial sites, the long-period or low-frequency waves (<2 Hz) appear to be dominant. Also, durations are longer in soil sites than in rock sites. Long-period Rayleigh waves (<1 Hz), which contain about two thirds of the total wave energy, (Miller and Pursey²⁸), are propagated as guide waves and cause motions in the surface soil layer. Rayleigh waves may be the main cause of the longer duration and higher damage potential in alluvium rather than in rock.

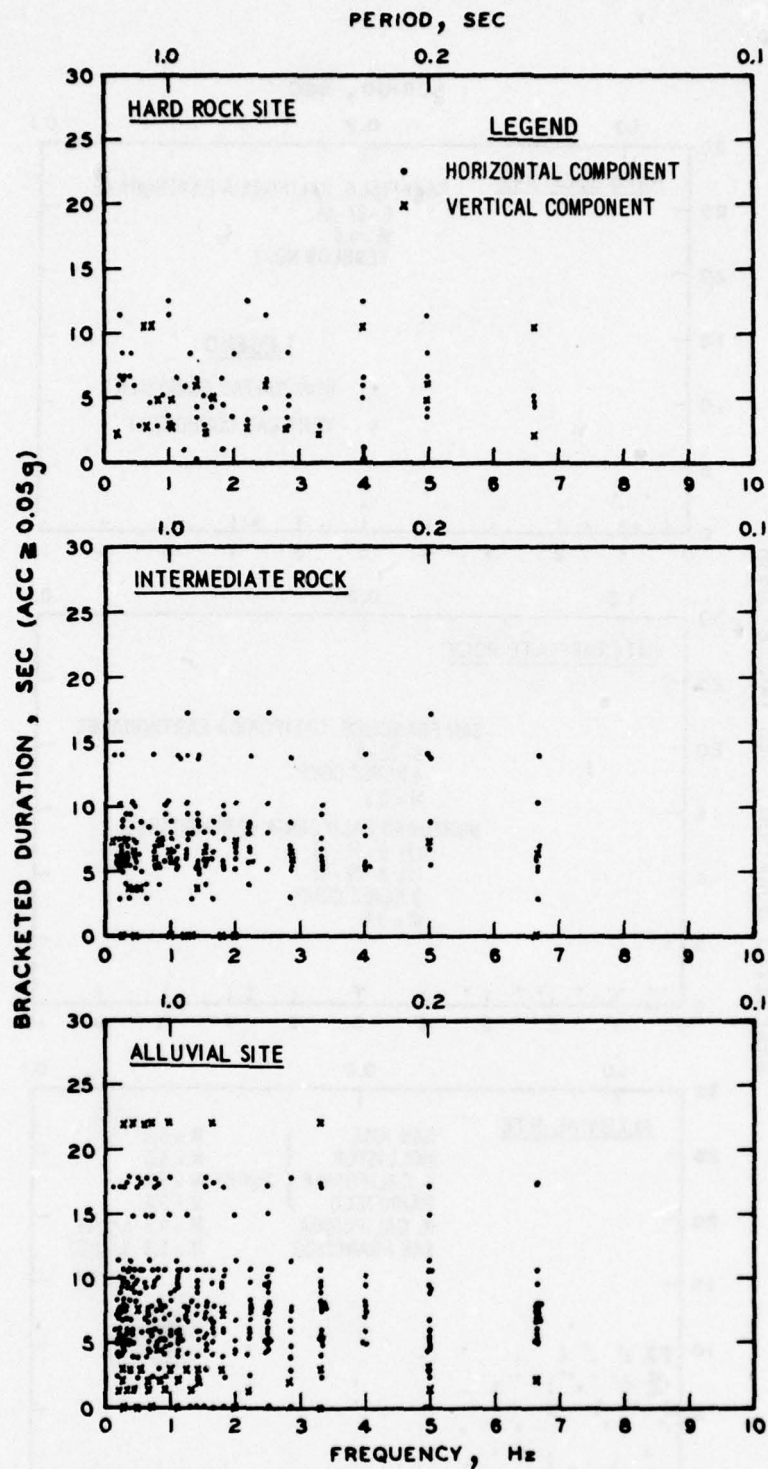


Figure 2. Duration versus frequency for various site conditions, San Fernando Earthquake, 9 February 1971 (M = 6.5)

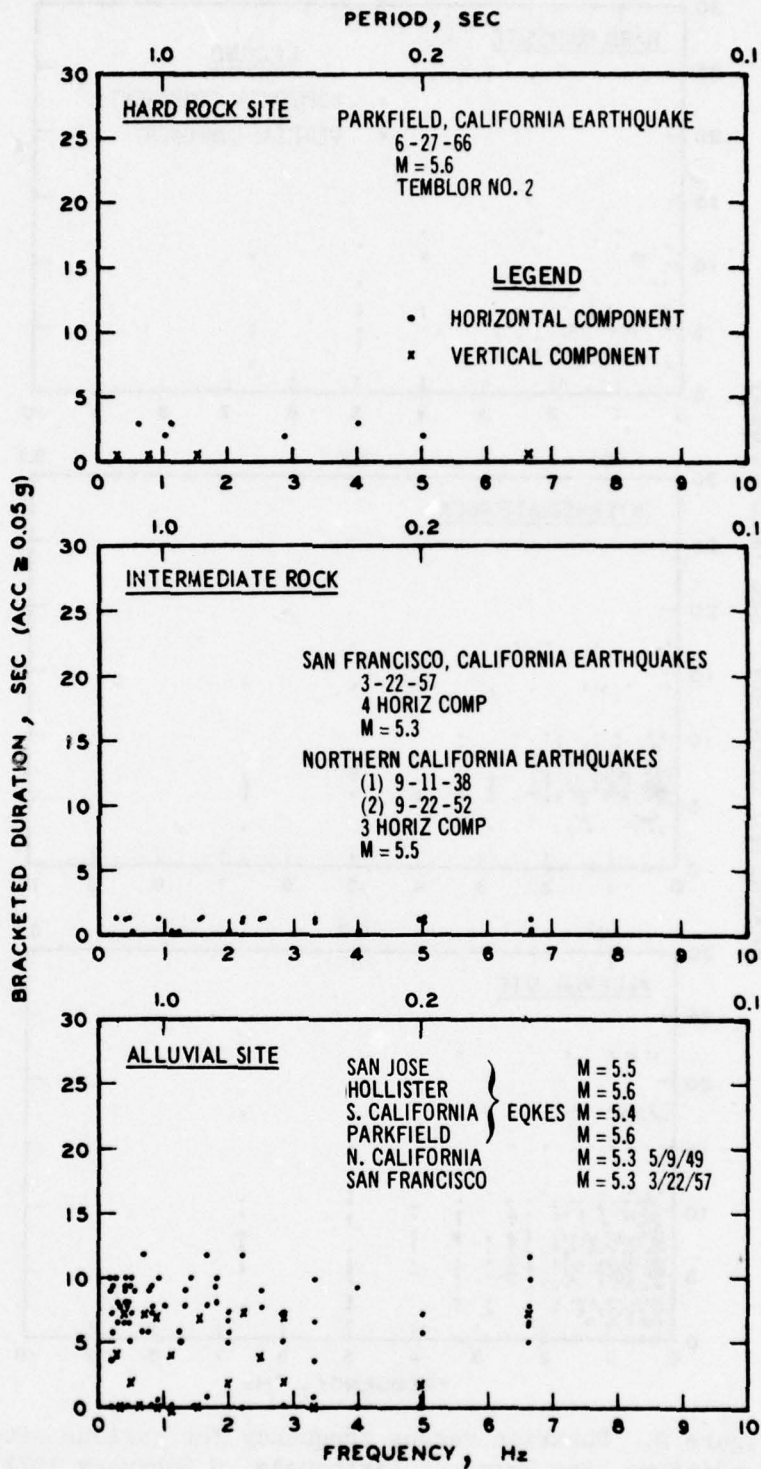


Figure 3. Duration versus frequency for various site conditions, California Earthquakes (M = 5.3-5.6)

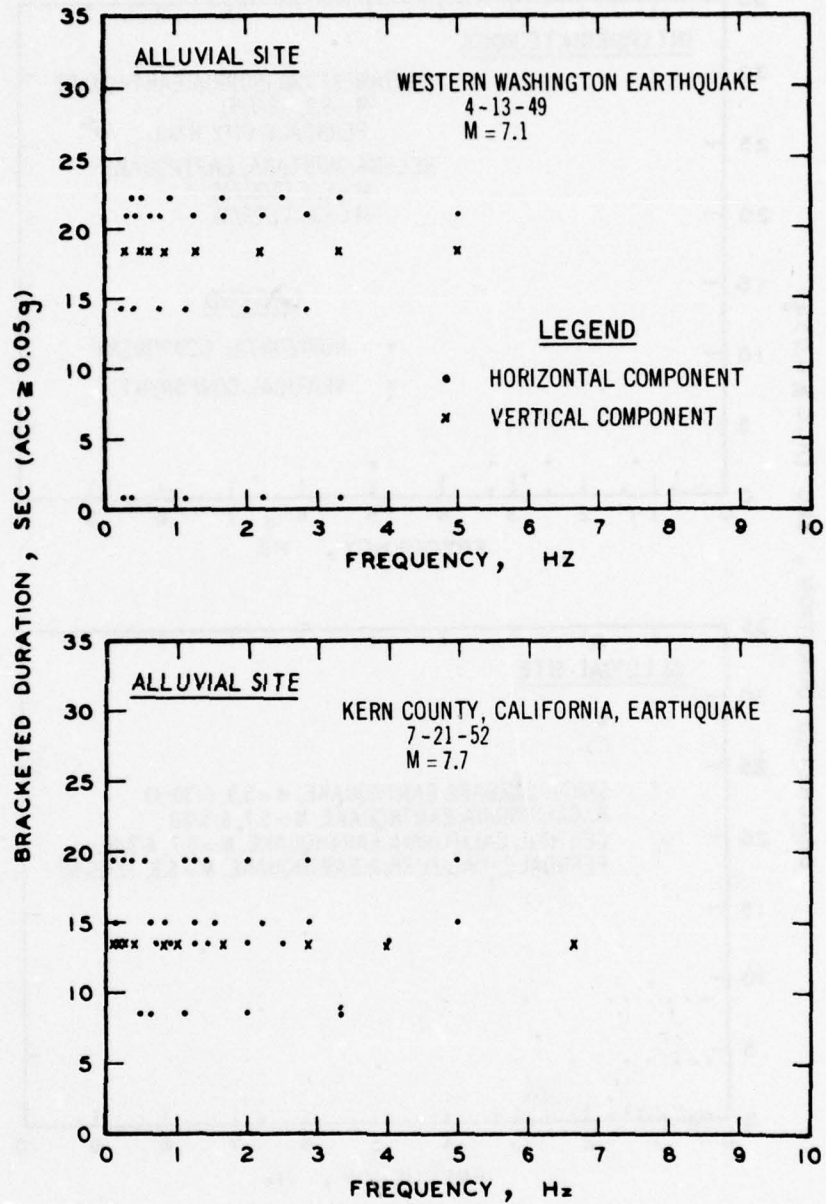


Figure 4. Duration versus frequency for alluvial sites, Western Washington Earthquake, 13 April 1949 (M = 7.1); and Kern County, California, Earthquake, 21 July 1952 (M = 7.5)

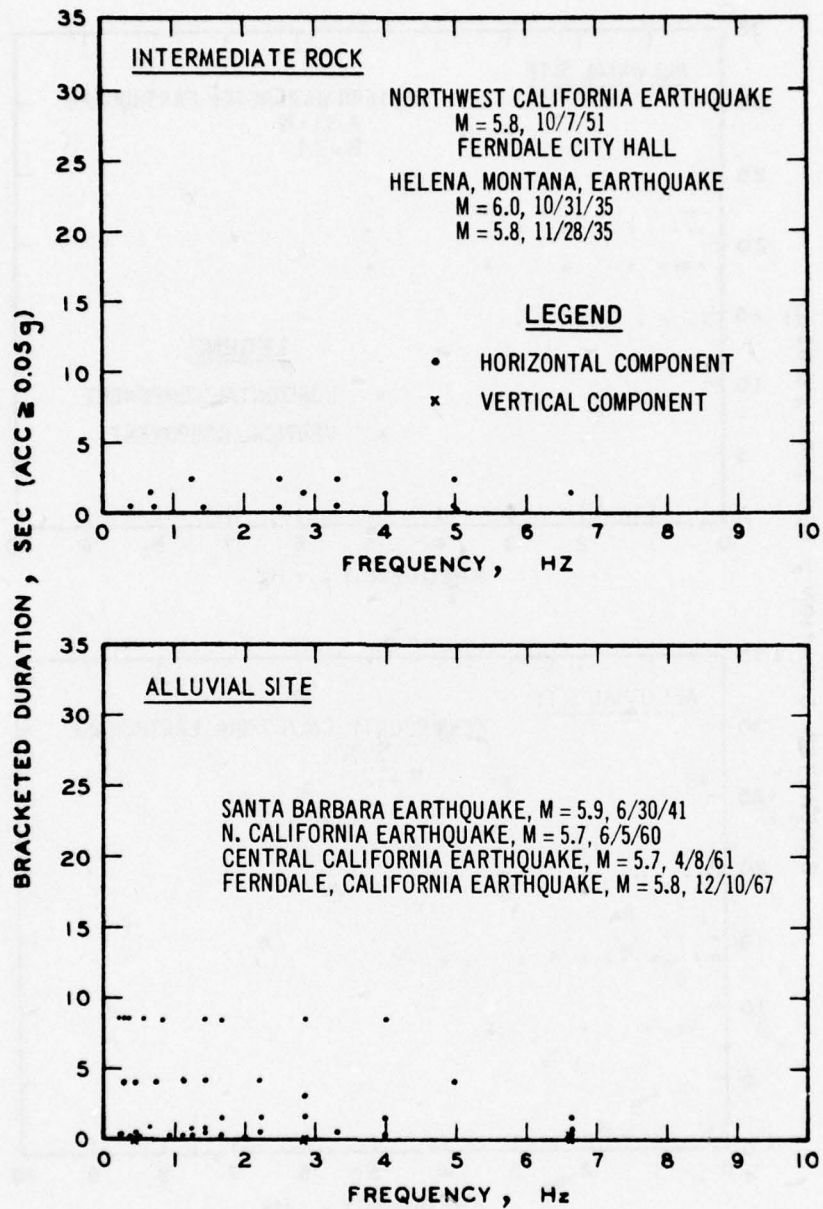


Figure 5. Duration versus frequency for intermediate rock and alluvial sites, California Earthquakes (M = 5.7-5.9); and Helena, Montana, Earthquakes, 31 October and 28 November 1935 (M = 5.7-6.0)

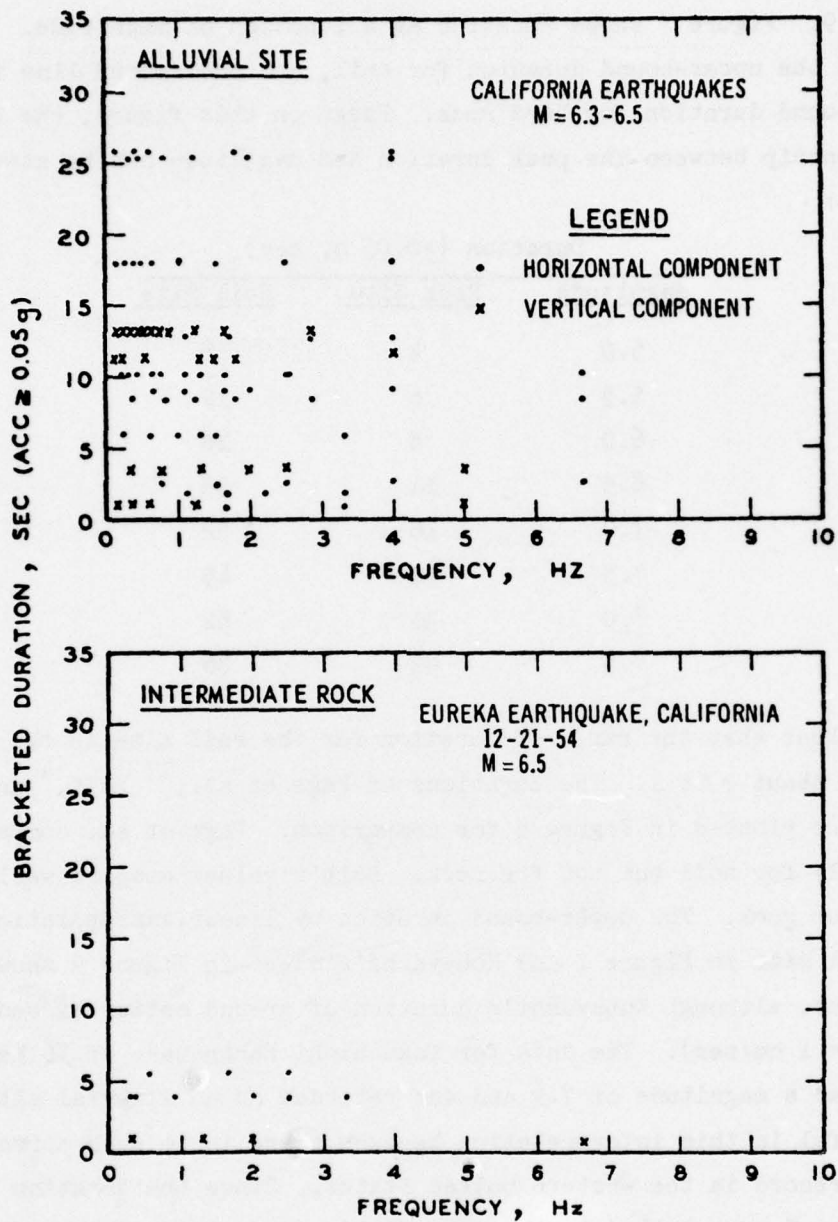


Figure 6. Duration versus frequency for alluvial and intermediate rock sites, California Earthquakes (M = 6.3-6.5)

Duration as a function of
magnitude in the near field

19. Figure 7 shows duration as a function of magnitude. The top line is the upper-bound duration for soil, and the second line is the upper-bound duration for hard rock. Based on this figure, the linear relationship between the peak duration and magnitude can be stated as follows:

Duration (>0.05 g, sec)		
<u>Magnitude</u>	<u>Rock Site</u>	<u>Soil Site</u>
5.0	4	8
5.5	6	12
6.0	8	16
6.5	11	23
7.0	16	32
7.5	22	45
8.0	31	62
8.5	43	86

It is clear that the ratio of duration for the soil site to the rock site is about 2 to 1. The durations of Page et al.,¹⁷ Bolt,⁴ and this study are plotted in Figure 8 for comparison. Page et al. compare favorably for soil but not for rock. Bolt's values compare well with those for rock. The upper-bound duration by linear extrapolation for the soil site in Figure 7 and Kobayashi's data⁵ in Figure 9 show a good agreement, although Kobayashi's duration of ground motion exceeds 30 gal (1 gal = 1 cm/sec). The data for Tokachioki Earthquake of 16 May 1968, which had a magnitude of 7.9 and was recorded on an alluvial site, are useful in this interpretation because there is no such strong-motion record in the western United States. Since the duration data in Figure 7 are plotted in the near field, apparently, the duration for rock site could be interpreted as at the source (or focus); the soil site is in the epicentral region. Of course, the duration is longer on the ground surface than at the source. Based on this interpretation, Housner's maximum duration³ of 45 sec and Bolt's duration

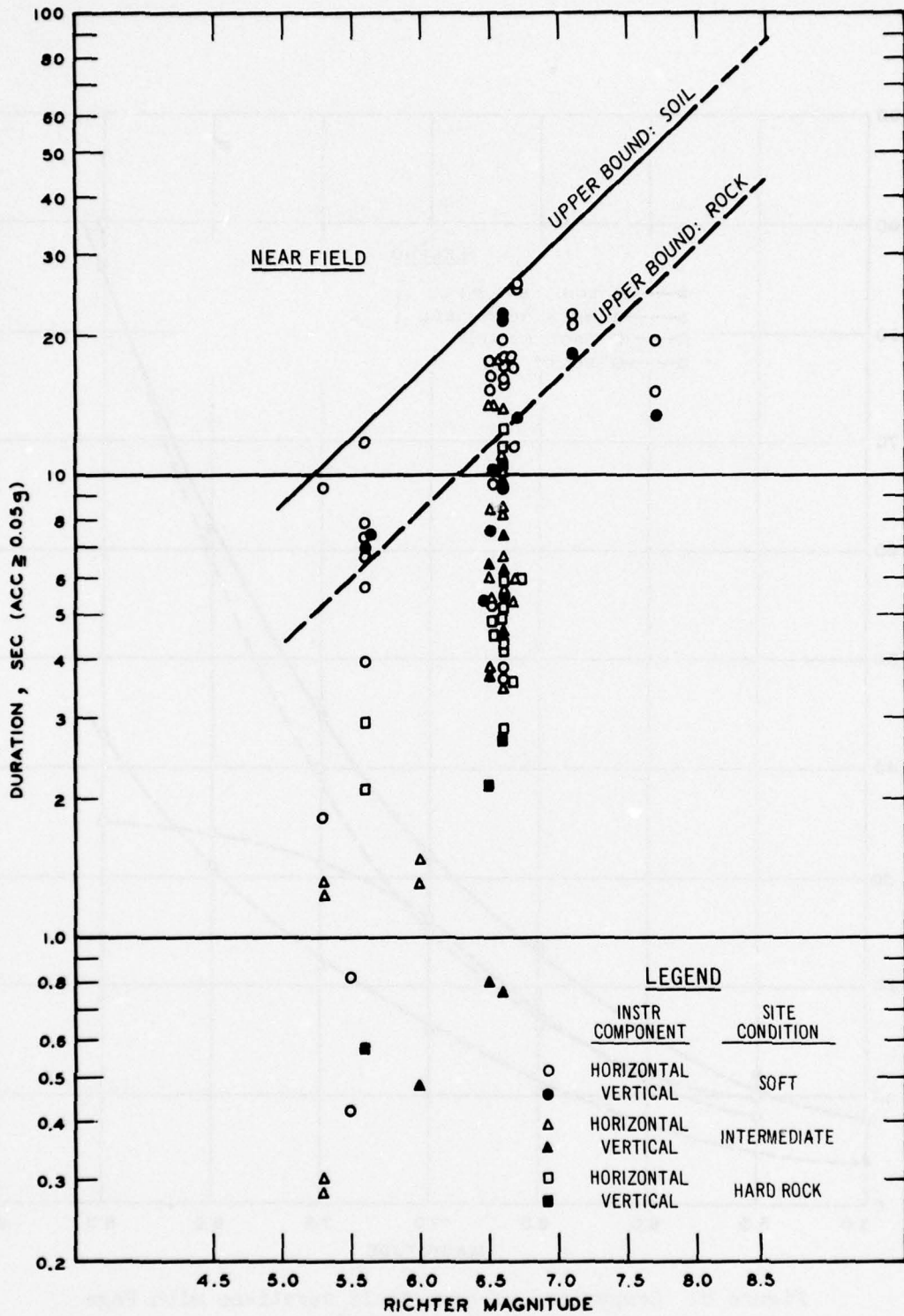


Figure 7. Duration versus Richter magnitude in the near field

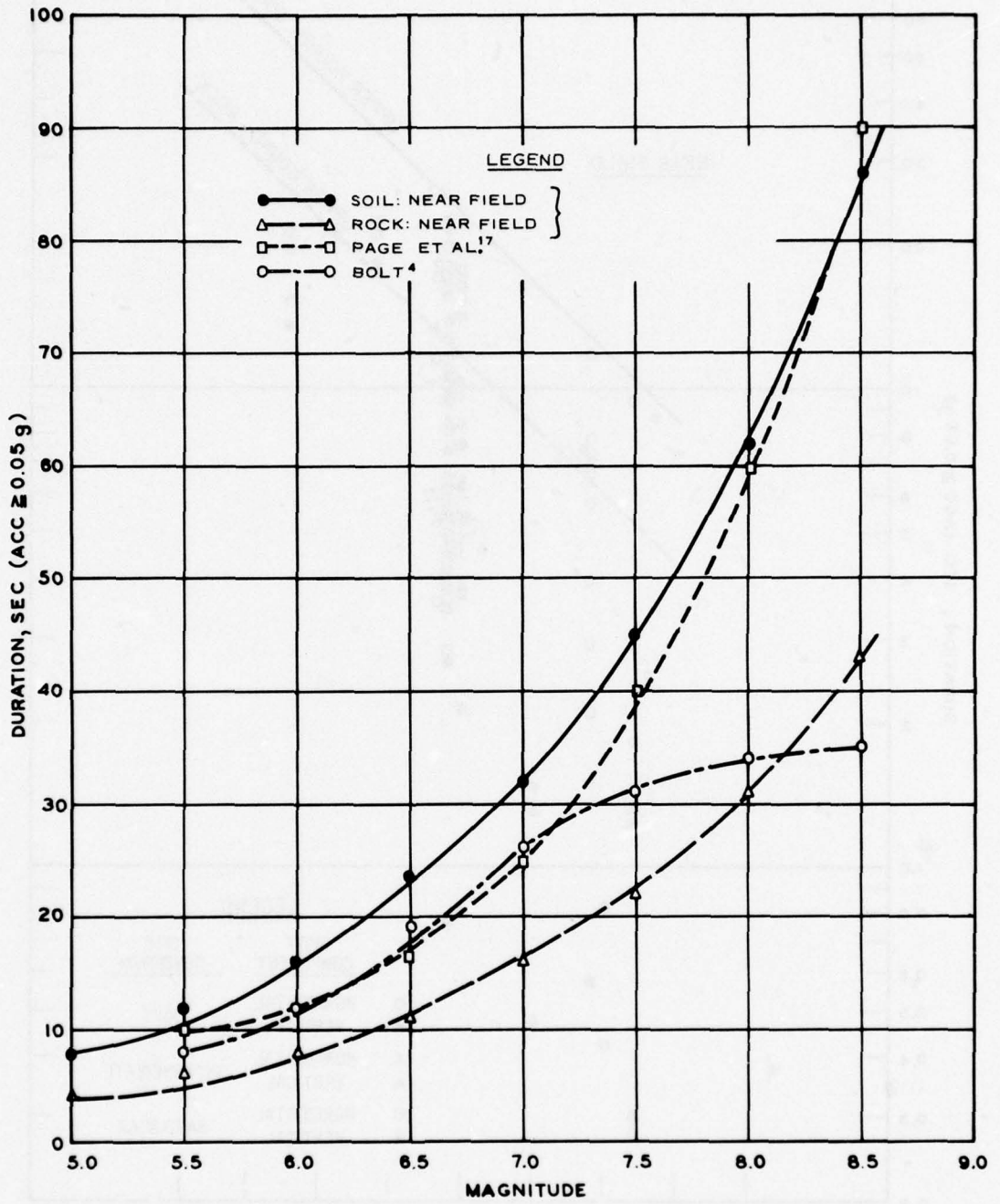


Figure 8. Comparison of near-field durations with Page et al.¹⁷ and Bolt⁴

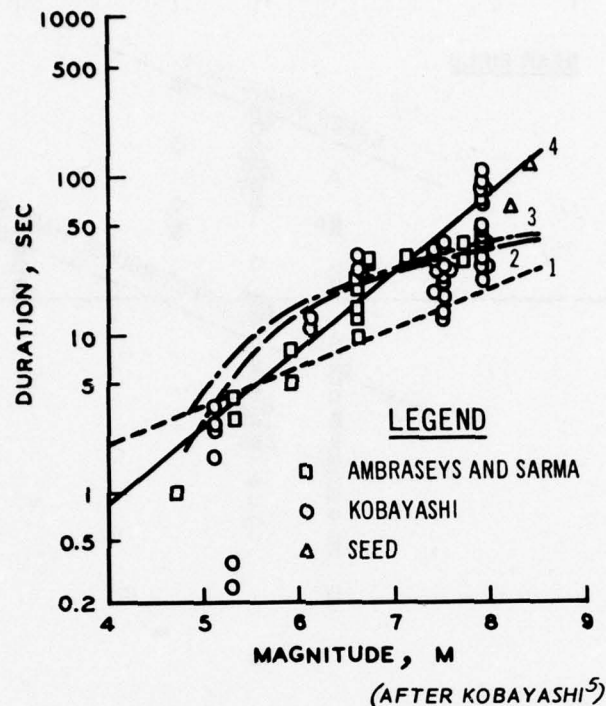


Figure 9. Duration of strong shaking and the earthquake magnitude (1. Gutenberg and Richter, $\log_{10} t_0 = 0.25 M - 0.7$; 2. Housner, $t_0 = 11.0 M - 52$; 3. Ambraseys and Sarma; $t_0 = 11.5 M - 53.0$; and 4. Kobayashi, $\log_{10} t_{30} = 0.50 M - 2.08$)

of 35 sec (+20 percent) for the magnitude 8.5 can be explained as the duration at the source (focus) of a rock site, but Page et al. and Kobayashi's maximum duration for the magnitude 8.5 corresponds to the upper-bound duration of this study for a soil site in an epicentral area.

Duration as a function of site intensity in the near and far fields

20. Figures 10 and 11 present duration as a function of MM intensity in the near field and far field, respectively. The boundary of the near field and far field has been defined by Krinitzsky and Chang.²⁷ The upper-bound durations for the soil and rock sites in the near field are tabulated below. (The average MM intensity and site conditions

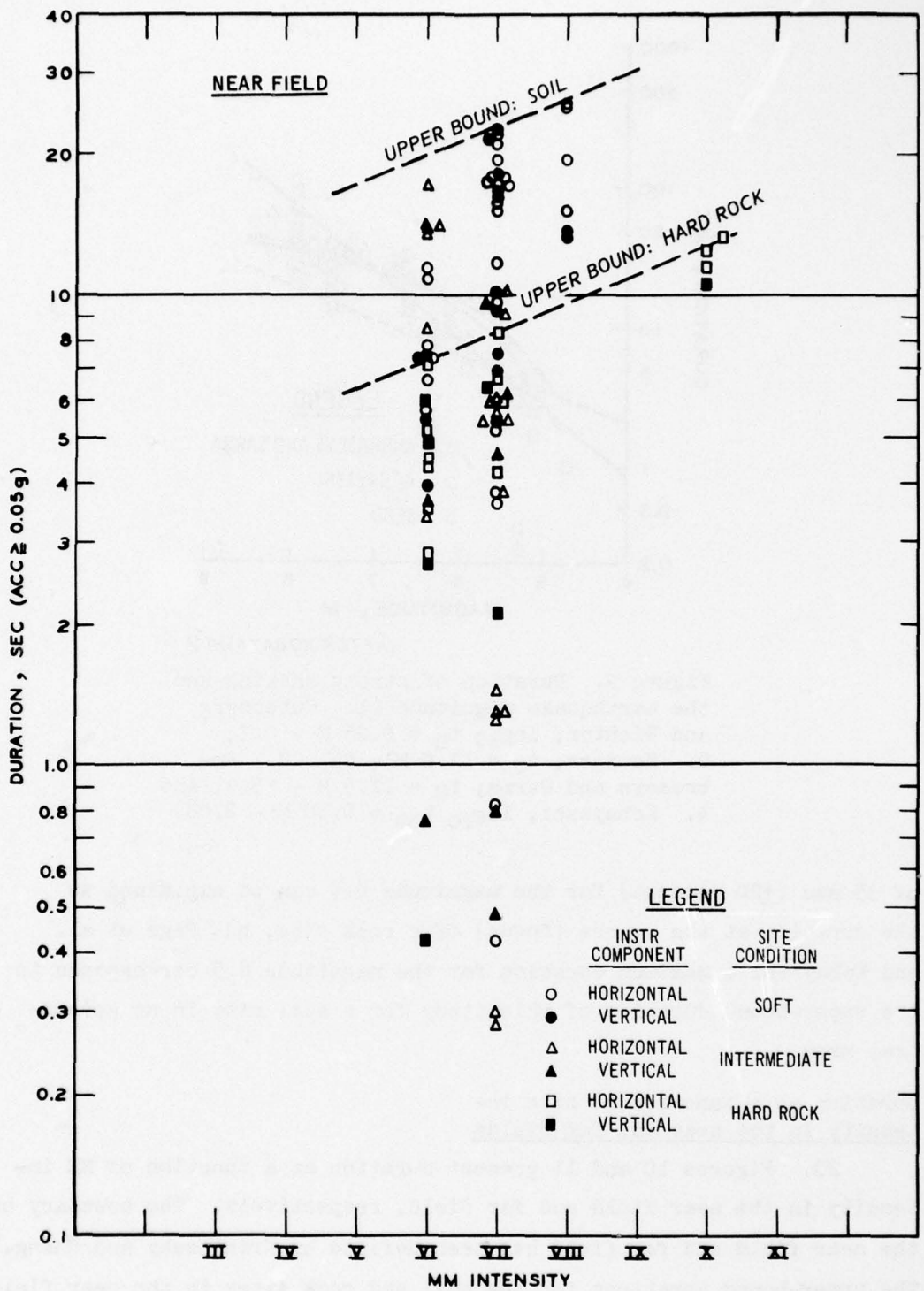


Figure 10. Duration versus MM intensity in the near field

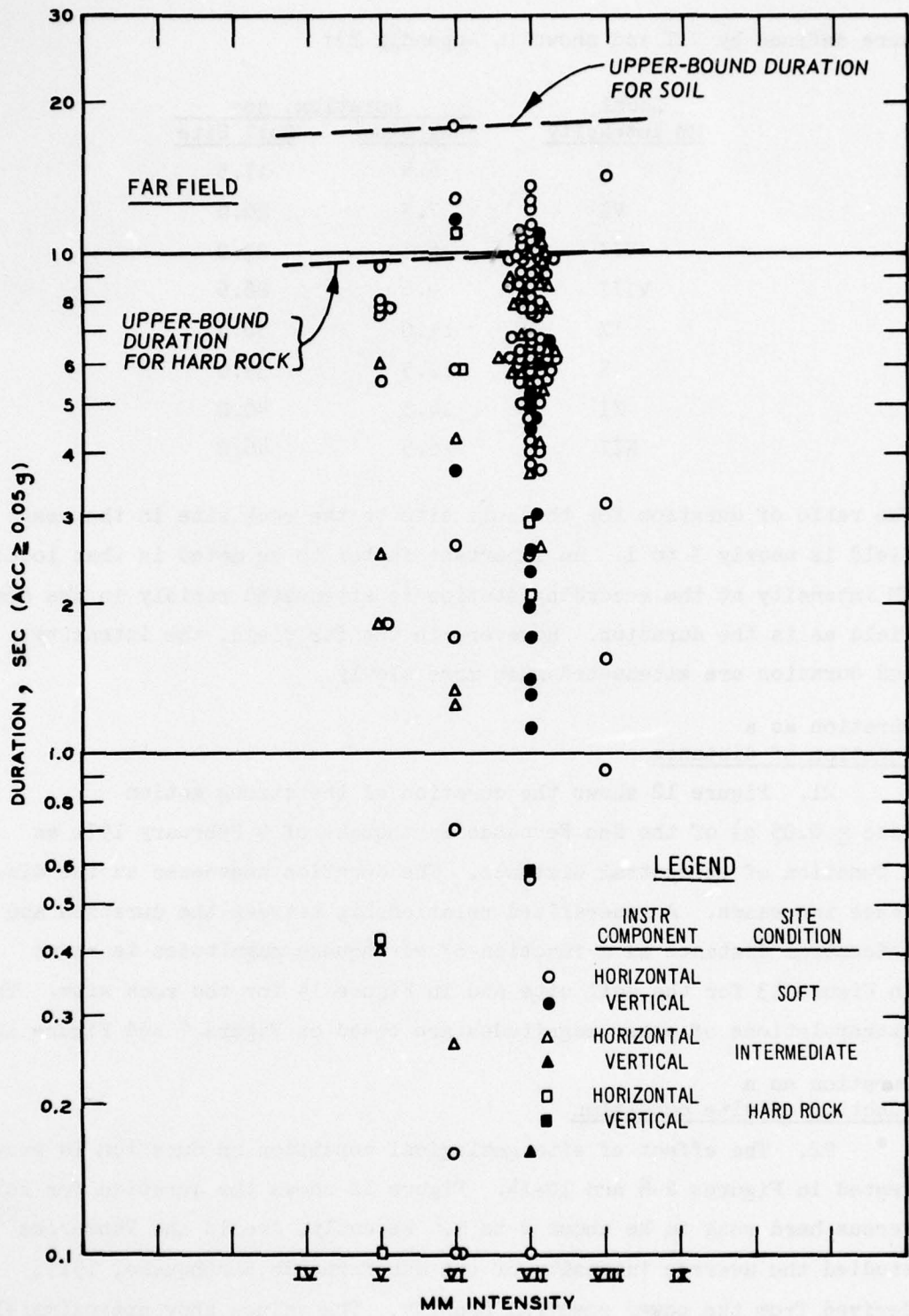


Figure 11. Duration versus MM intensity in the far field

were defined by CIT and shown in Appendix B):

<u>Local</u> <u>MM Intensity</u>	<u>Duration, sec</u>	
	<u>Rock Site</u>	<u>Soil Site</u>
V	6.4	17.5
VI	7.3	20.0
VII	8.3	23.0
VIII	9.6	26.5
IX	11.0	30.0
X	12.5	35.0
XI	14.5	40.0
XII	16.5	46.0

The ratio of duration for the soil site to the rock site in the near field is nearly 3 to 1. An important factor to be noted is that local MM intensity at the recording station is attenuated rapidly in the near field as is the duration. However, in the far field, the intensity and duration are attenuated much more slowly.

Duration as a
function of distance

21. Figure 12 shows the duration of the strong motion ($acc \geq 0.05$ g) of the San Fernando Earthquake of 9 February 1971 as a function of epicentral distance. The duration decreases as the distance increases. A generalized relationship between the duration and epicentral distance as a function of earthquake magnitudes is shown in Figure 13 for the soil site and in Figure 14 for the rock site. The extrapolations of other magnitudes are based on Figure 7 and Figure 12.

Duration as a
function of site condition

22. The effect of site geological condition on duration is presented in Figures 2-8 and 10-14. Figure 12 shows the duration for soft versus hard rock to be about 2 to 1. Recently, Arnold and Vanmarcke²⁹ studied the average intensity of the San Fernando Earthquake, 1971, derived from the power spectral density. The values show approximately a linear attenuation with distance from the epicentral area in the

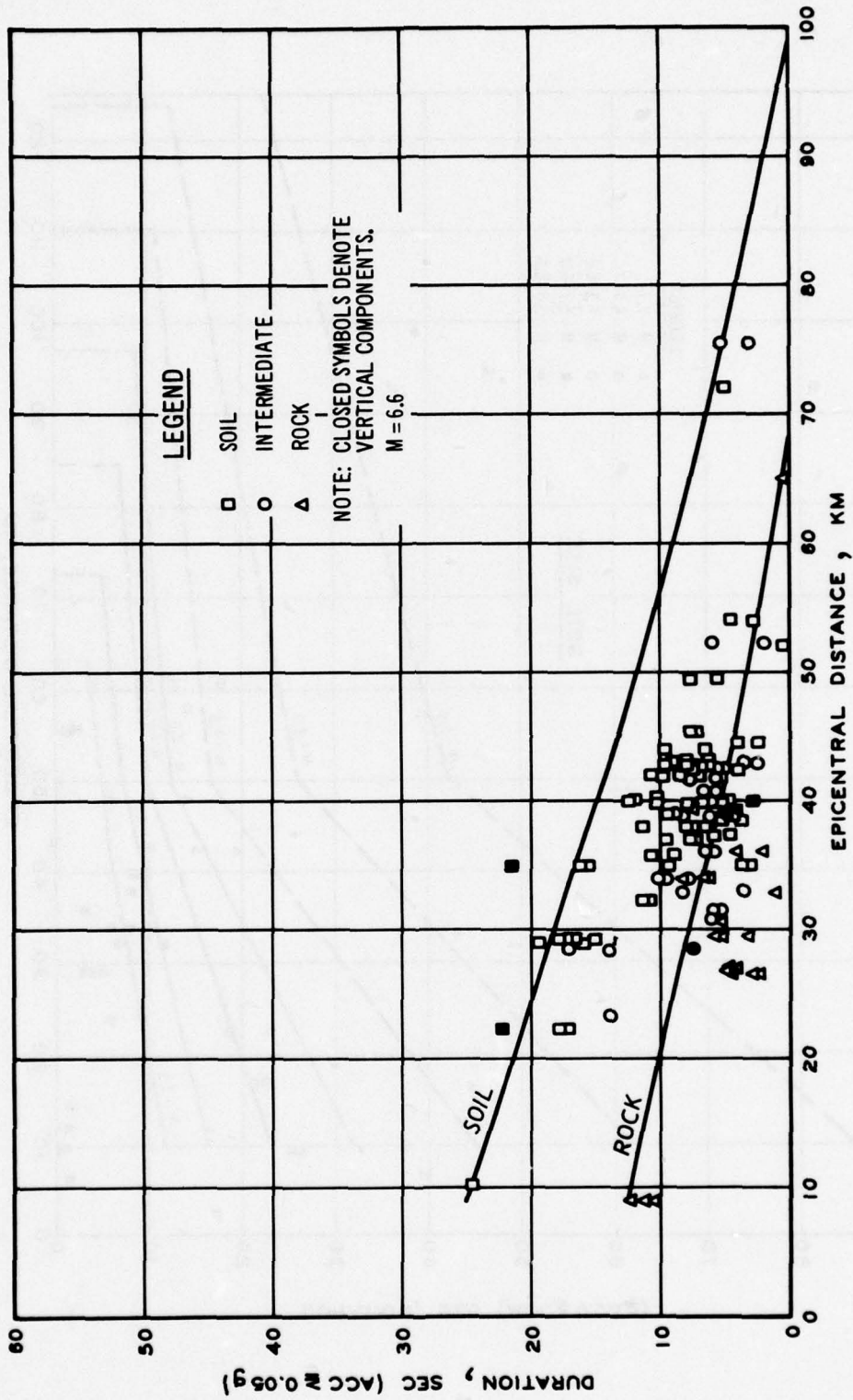


Figure 12. Duration versus epicentral distance, San Fernando Earthquake, California, 9 February 1971 (M - 6.6)

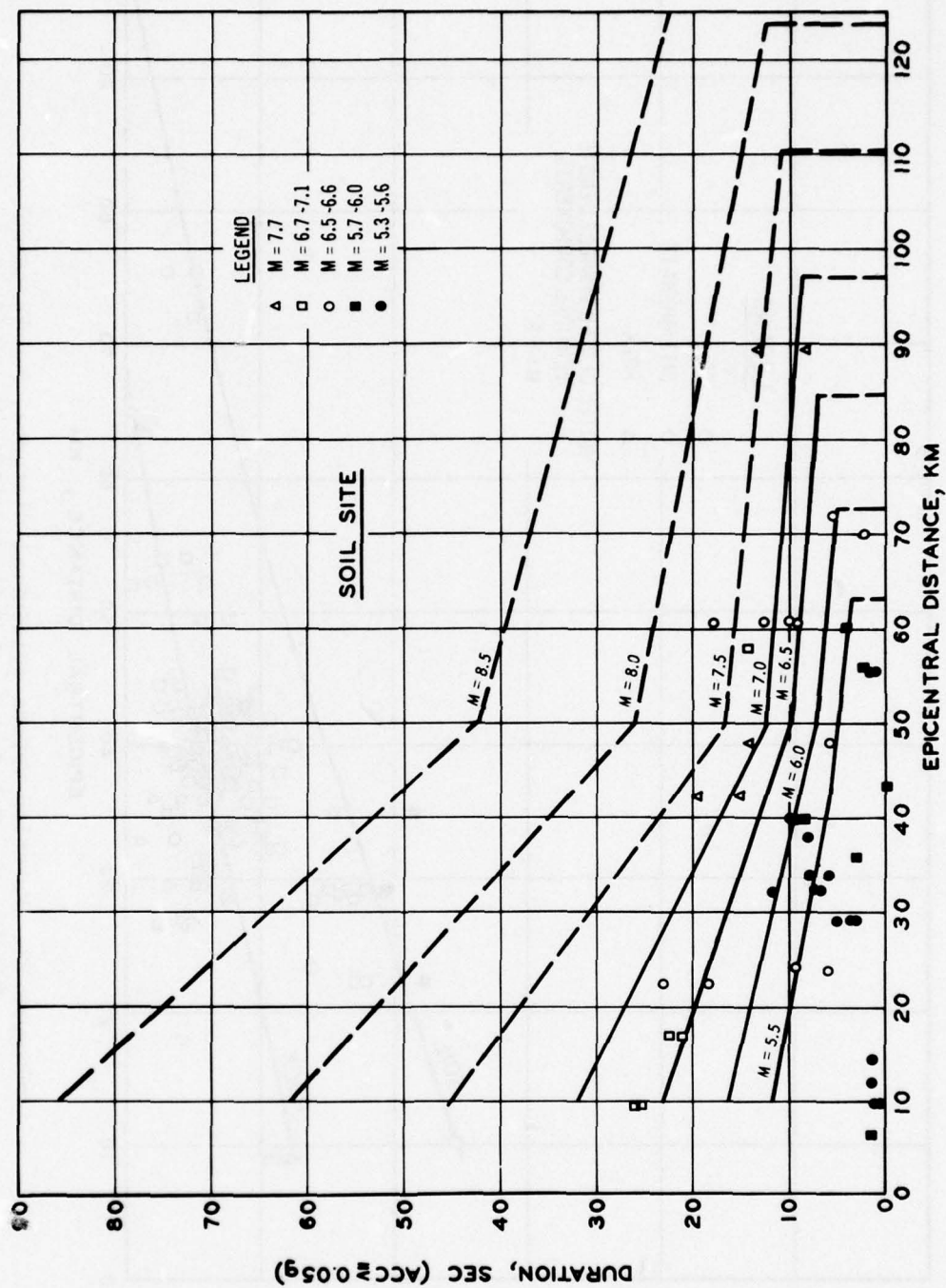


Figure 13. Duration versus epicentral distance and magnitude for the soil site

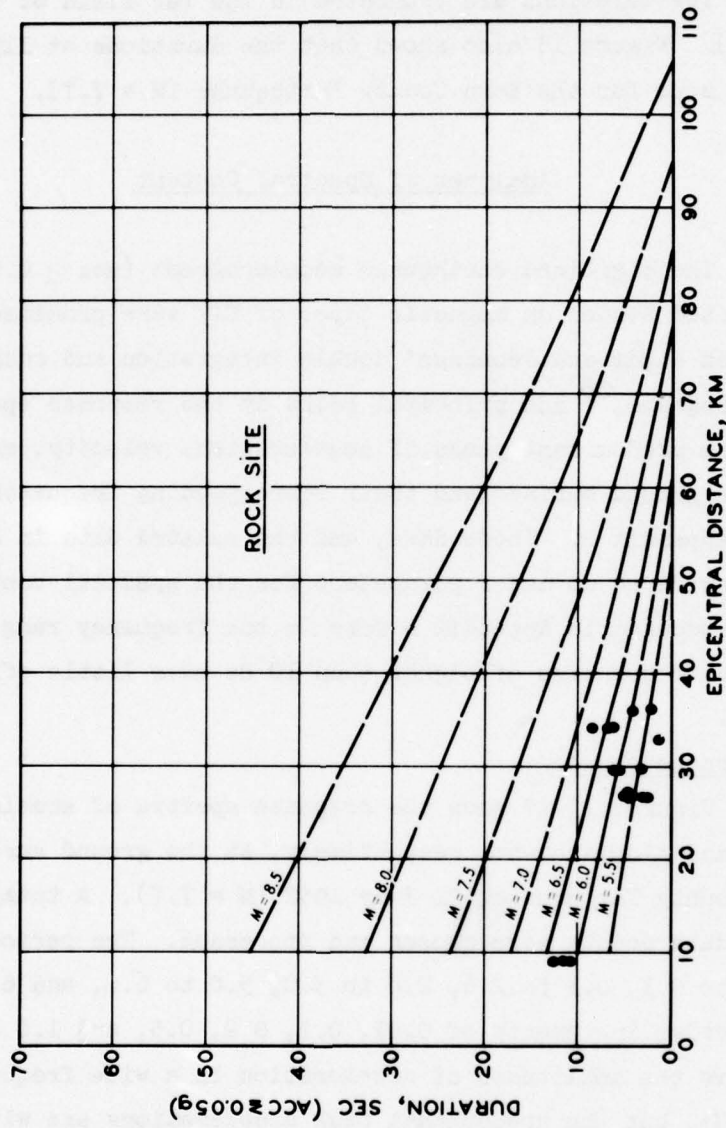


Figure 14. Duration versus epicentral distance and magnitude for the rock site

range of 50 km. Beyond this distance, the intensity seems to be more nearly constant. Since the duration of strong motion is related to peak intensity, the upper-bound line of duration in the near field (Figure 10) shows a linear decrease as the MM intensities decrease with distance. The durations are truncated in the far field of the soil site (Figure 13). Figure 15 also shows that the durations at 119.5 and 126 km are zero for the Kern County Earthquake ($M = 7.7$).

Analyses of Spectral Content

23. The digitized earthquake accelerograms ($\text{acc} \geq 0.05 \text{ g}$) of the western United States on magnetic tapes of CIT were processed through the modified Nigam and Jennings' double integration and response spectra computer programs,²⁶ and principal peaks in the response spectra were chosen. The predominant peaks of acceleration, velocity, and displacement at the ground surface and their corresponding frequencies are listed in Appendix B. These data, and the related data in Appendix A, will be considered as major parameters for the spectral content analyses. The data processed in Appendix B were in the frequency range of 0.1-10 Hz. The frequencies of higher than 10 Hz have little effect on structures.

Frequency range chosen

24. Figures 15-17 show the response spectra of acceleration, velocity, and displacement, respectively, at the ground surface for the Kern County Earthquake, 21 July 1952 ($M = 7.7$). A total of 48-period data points were chosen and processed. The periods are from 0.01 to 0.1, 0.1 to 2.6, 2.6 to 5.0, 5.0 to 6.0, and 6.0 to 9.0 sec with respective increments of 0.01, 0.1, 0.2, 0.5, and 1.0 sec. Figure 15 shows the amplitudes of acceleration in a wide frequency range of 0.1-50 Hz, but the predominant peak accelerations are within 1-10 Hz. Above 10 Hz, the amplitudes of response spectrum become a constant value at the distance range of 43-126 km. The integrated particle velocities and displacements of Figures 16 and 17 do not present any information in the frequency range over 10 Hz. Evidently, the higher

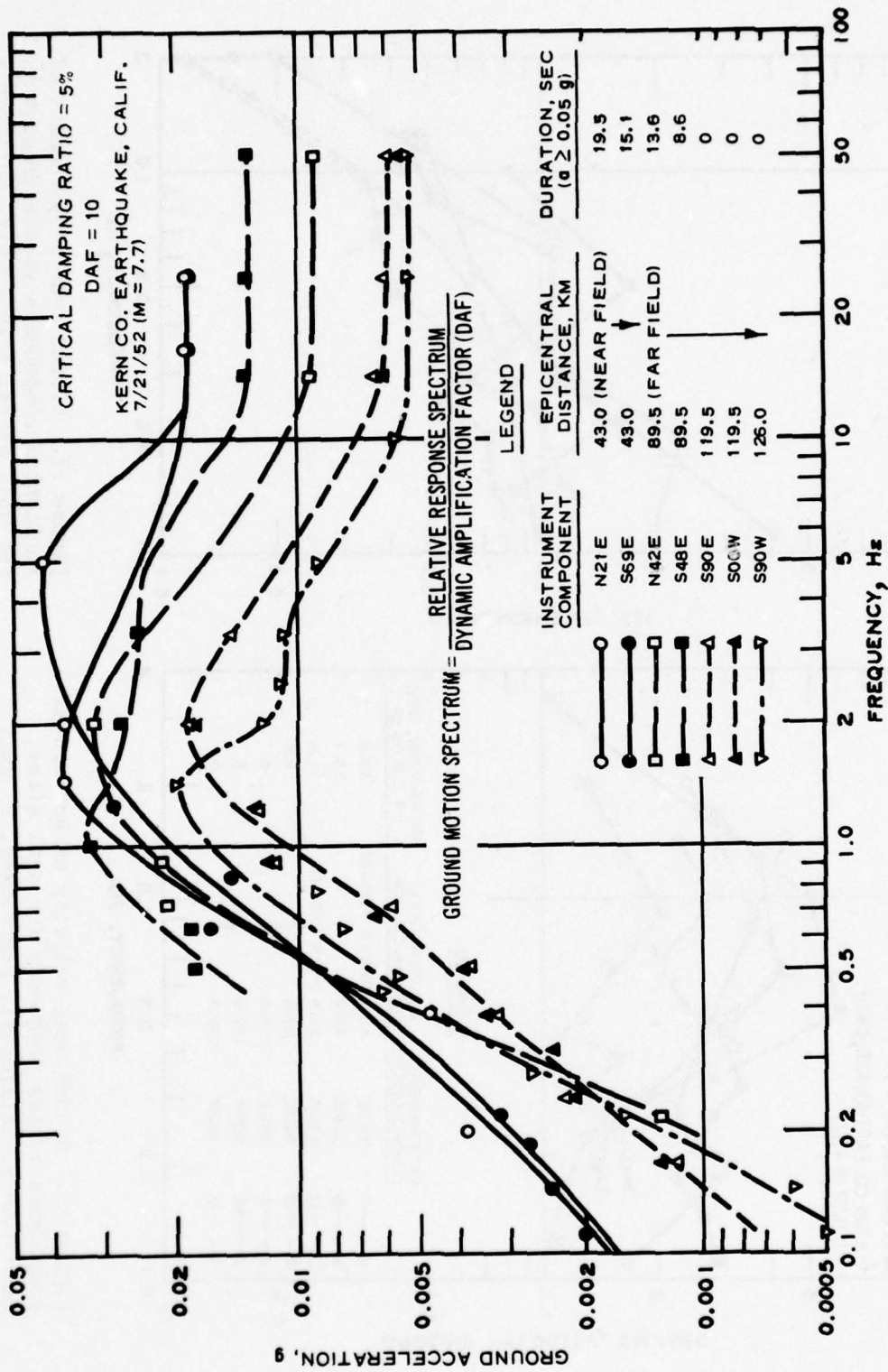


Figure 15. Ground peak acceleration of horizontal components versus frequency for soil sites, Kern County, California, Earthquake, 21 July 1952 (M = 7.7)

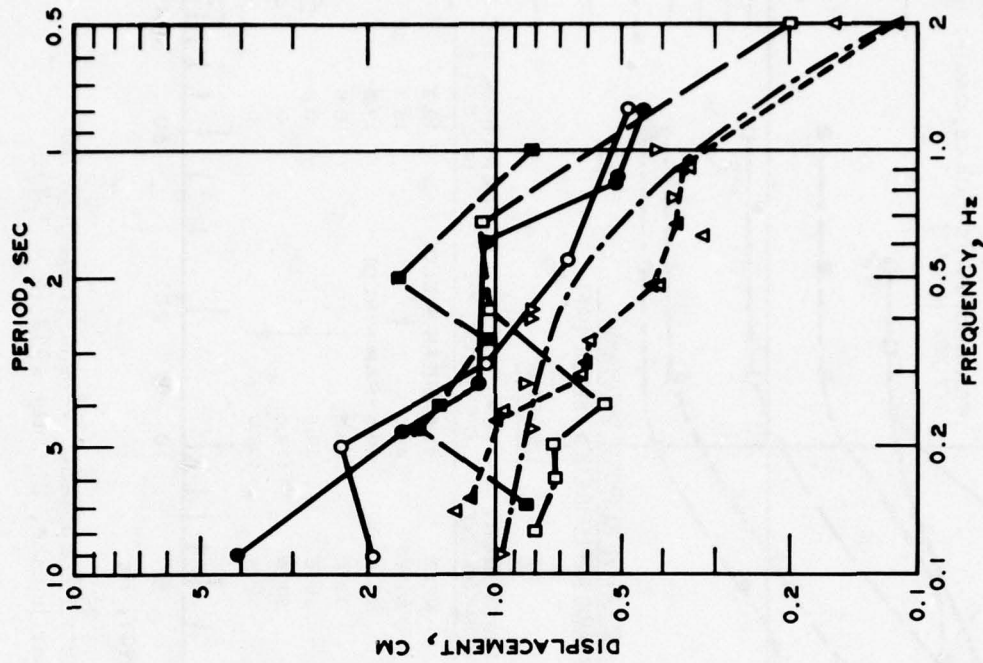


Figure 16. Ground peak velocity of horizontal components versus frequency for soil sites, Kern County, California, Earthquake, 21 July 1952 (M = 7.7)

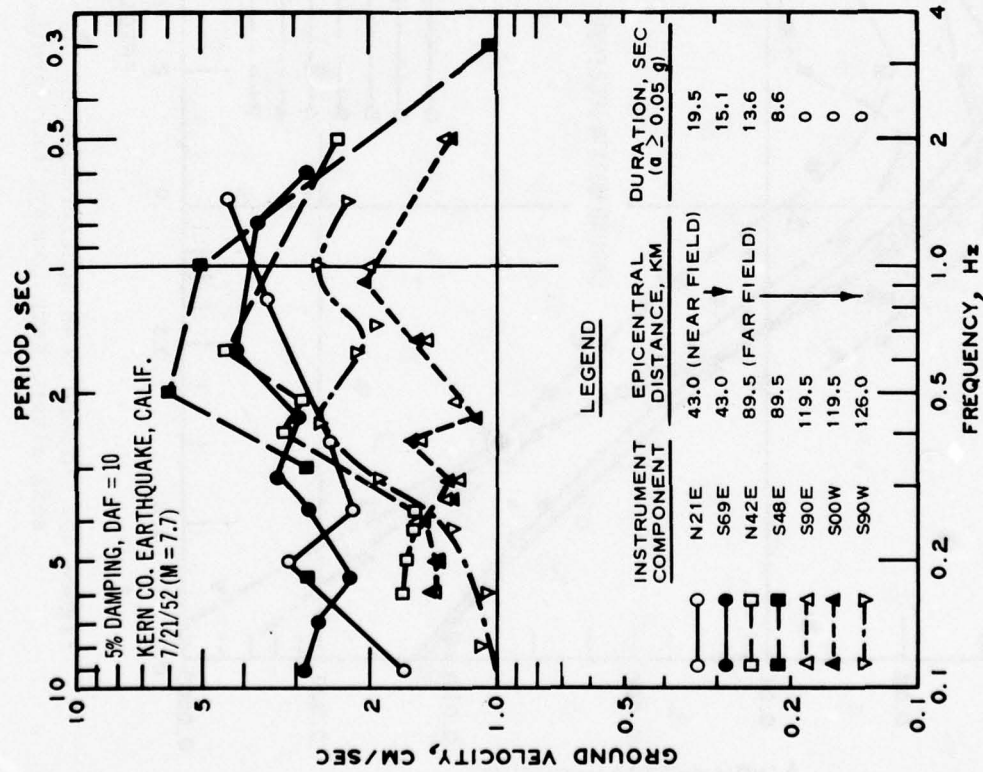


Figure 17. Ground peak displacement of horizontal components versus frequency for soil sites, Kern County, California, Earthquake, 21 July 1952 (M = 7.7)

frequency range above 10 Hz recorded in the accelerograms does not affect or influence the particle velocity and displacement. Based on this relation, the frequency range of 0.1-10 Hz for this study is appropriate. All data in Appendix B were processed in this range. The incremental intervals for the 48 periods chosen were taken as follows:

<u>Period</u> <u>sec</u>	<u>Increment</u> <u>sec</u>
0.1 - 0.8	0.05
0.8 - 1.6	0.10
1.6 - 2.0	0.20
2.0 - 2.6	0.10
2.6 - 5.0	0.20
5.0 - 6.0	0.50
6.0 - 9.0	1.00

Appendix C lists the 48 periods and the corresponding frequency components, which were employed to define the spectral content.

25. The spectra dependent effects of magnitude, distance, recording site condition, and path are discussed in the following sections. The discussions are based mainly on the data presented in Appendixes A, B, and C.

Spectra dependent effect of magnitude

26. The acceleration peak spectra of the San Fernando Earthquake of 9 February 1971, which has a magnitude of 6.5, are plotted in Figures 18 and 19 for the soil and hard rock sites, respectively. Figures 20 and 21 show plots of the other earthquakes of magnitudes that range from 5.3 to 5.9 and 5.7 to 6.0, respectively, with soft and intermediate site conditions. Figure 22 presents the El Centro Earthquake of magnitude 6.7 (1940) and Western Washington Earthquake of magnitude 7.1 (1949), and Figures 15-17, the Kern County Earthquake of magnitude 7.7 (1952). An examination of the above-mentioned figures shows that the predominant frequencies are within the range of 1-6.67 Hz for all earthquakes used.

27. No relationship was found between frequency and magnitude.

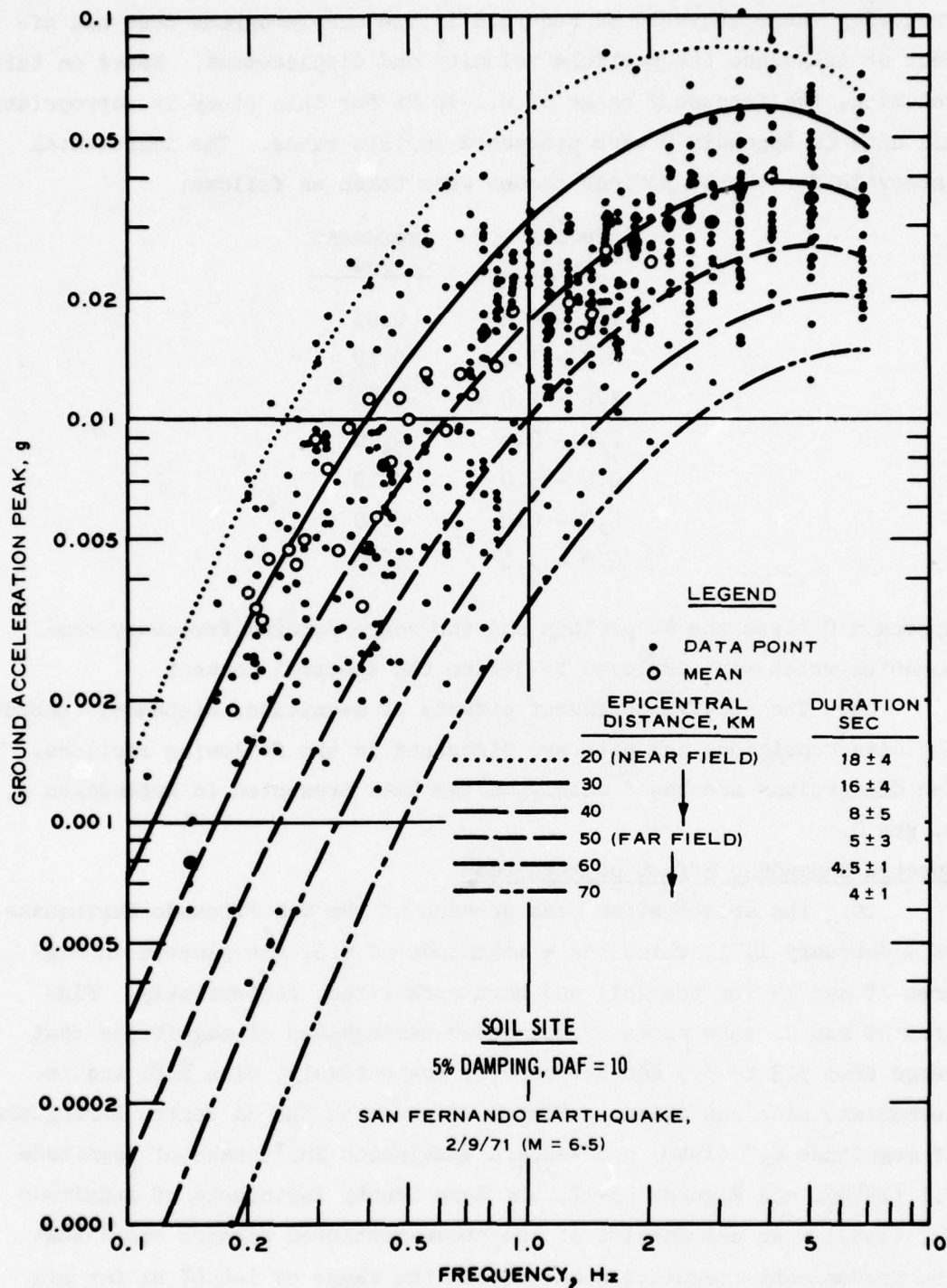


Figure 18. Ground peak acceleration spectra of horizontal components for soil sites at various distances and durations, San Fernando Earthquake, California, 9 February 1971 (M = 6.5)

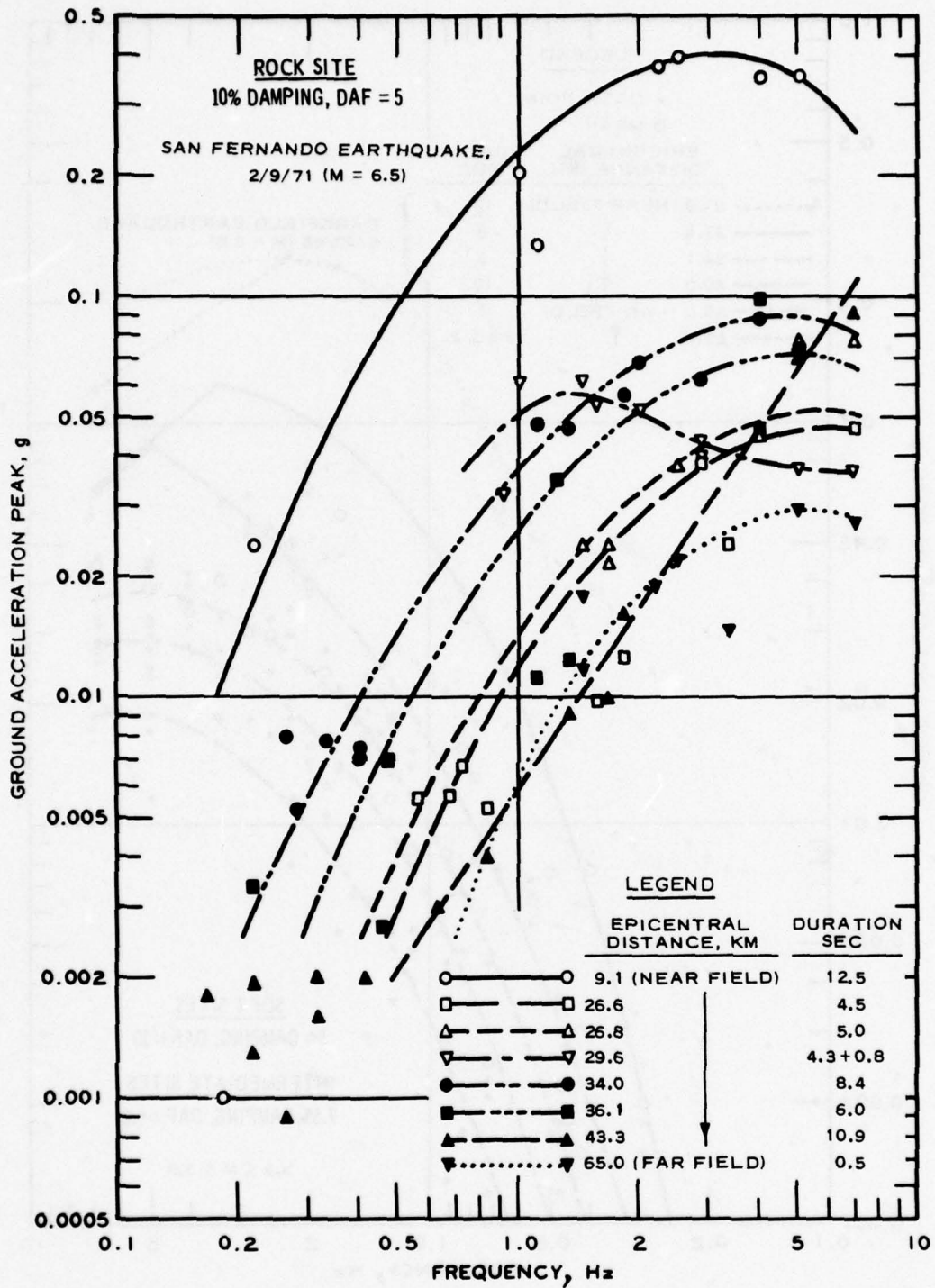


Figure 19. Ground peak acceleration spectra of horizontal components for rock sites at various distances and durations, San Fernando Earthquake, California, 9 February 1971 (M = 6.5)

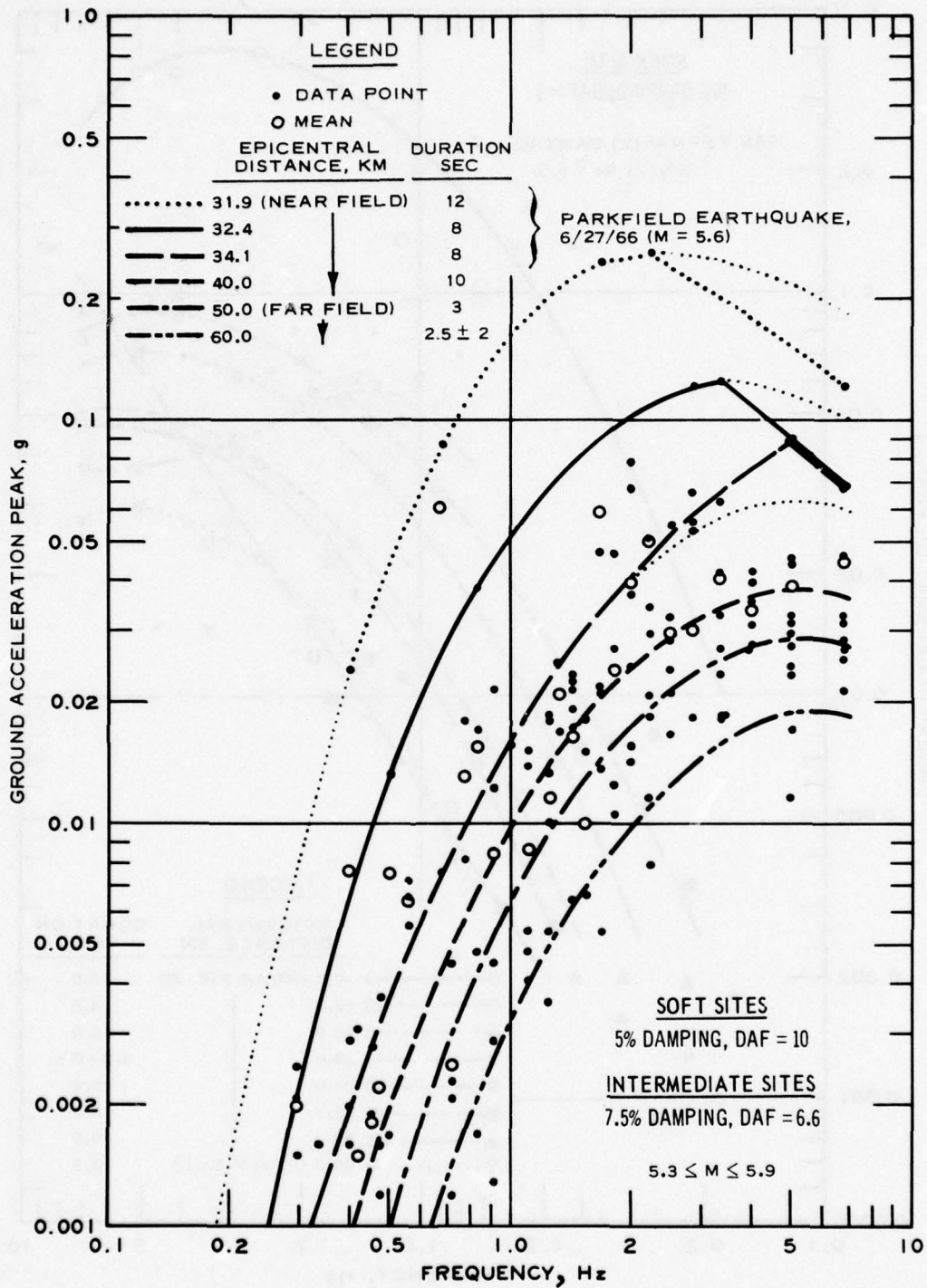


Figure 20. Ground peak acceleration spectra of horizontal components for soft and intermediate sites at various distances and durations for earthquake magnitudes of 5.3-5.9 in western United States

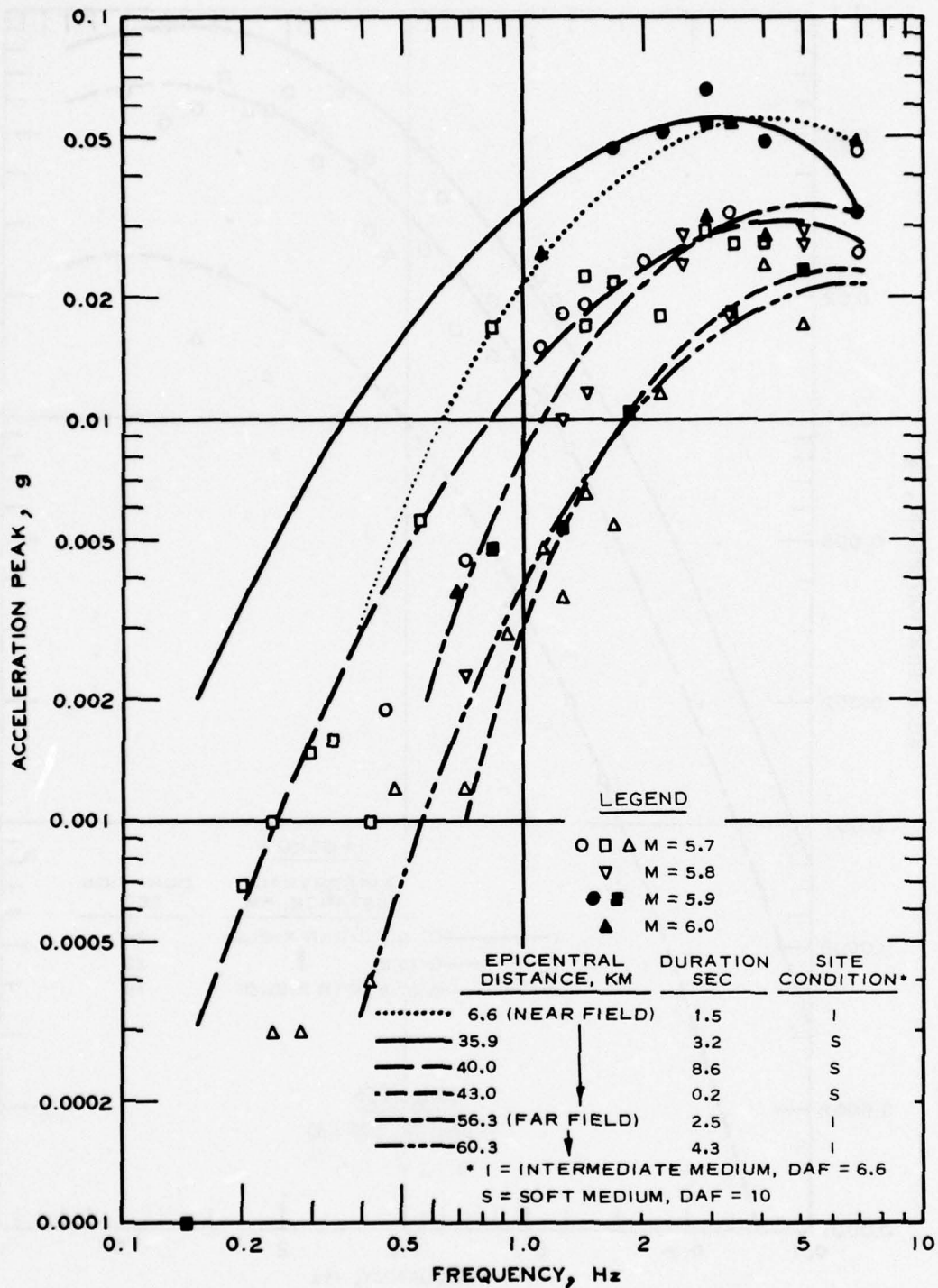


Figure 21. Ground peak acceleration spectra of horizontal components for soft and intermediate sites at various distances and durations for earthquake magnitudes of 5.7-6.0 in western United States

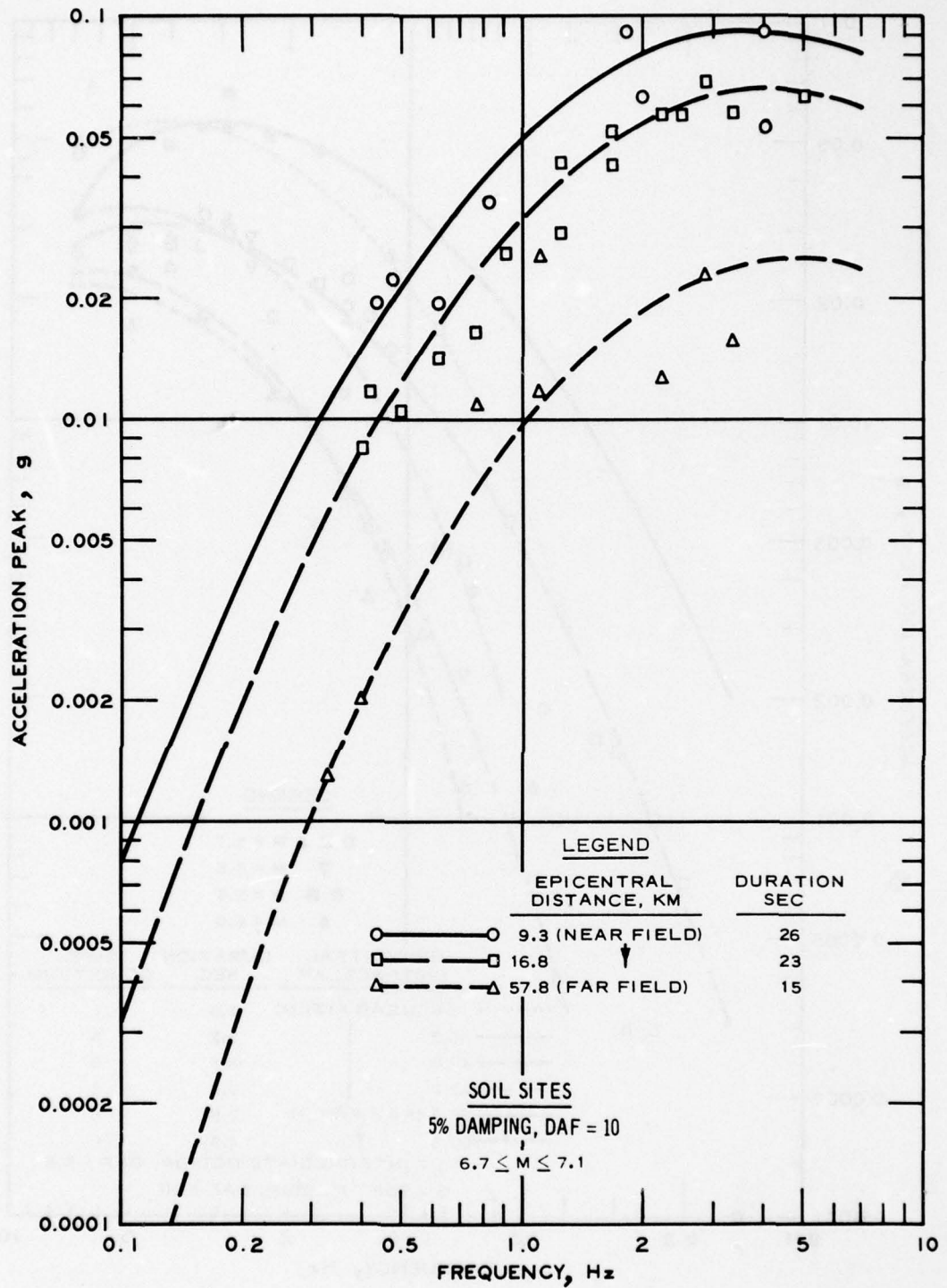


Figure 22. Ground peak acceleration spectra of horizontal components for soil sites at various distances and durations for earthquake magnitudes of 6.7-7.1 in western United States

Effect of distance on spectra

28. The acceleration response spectra of Figures 18-22 do not show any notable increase of the predominant period with distance ($6.6 \text{ km} \leq \Delta < 126 \text{ km}$). Apparently, a reverse case is indicated in Figures 18 and 20. Of course, the distance was limited to within 90 km in this study due to the criteria of time duration ($\text{acc} \geq 0.05 \text{ g}$). The peak acceleration spectrum has a wide frequency range from 1.0 to 7.0 Hz at a short epicentral distance.

Effect of site geology on spectra

29. A comparison of the acceleration spectra of Figures 18 and 19 for the soil and rock sites of the San Fernando Earthquake shows the soil site with a wider frequency range of maximum acceleration than the rock site, but the rock site has higher accelerations in the near field. The dispersion phenomena are more pronounced in the low-frequency (f) range ($0.5 \text{ Hz} > f > 0.1 \text{ Hz}$) for the soil site than for the rock site; the amplitude range for the soil site is between 0.0001 and 0.03 g and for the rock site between 0.001 and 0.1 g. However, it is noted that the maximum displacement is in the low-cycle region between 0.1 and 0.4 Hz (see paragraph 38). Kasiraj and Yao (1968)³⁰ presented the results of a theoretical variation of parameter study that investigated damage based on a low-cycle fatigue damage factor using an inelastic model, which included a low-cycle fatigue hysteresis loop. A similar process probably influences the soil site more so than the rock site, so that the maximum displacement, low frequency, and longer duration are affected and show up as important damage criteria.

Spectra-dependent effect of path and topography

30. The effect of wave transmission path and topography, from the earthquake source to the recording station, on the ground motion history is well known. Especially, after the recording of 1.25 g at the Pacoima Dam during the San Fernando Earthquake, an extensive study of the effect of topography on the ground motion was made. Chang³¹ found a linear relationship between the ground motion and the elevation in the San Fernando Valley region of the San Fernando Earthquake. He used

this new relationship, elevation gradient method, to predict the acceleration of 2.29 g at the top of Kagel Mountain, which was also confirmed by the after-shock study.

31. In Figure 19, the acceleration response spectra recorded at the Santa Anita Reservoir, Arcadia (distance = 43.3 km), and the Lake Hughes Array No. 1, California (distance = 29.6 km), both on rock, have different characteristics in comparison with other paths. The former shows a linear increase in acceleration between 0.5 and 7.0 Hz and is nearly constant under 0.5 Hz; the latter shows maximum accelerations that changed from the usual spread of 2-7 Hz for other paths to a range of 1-2 Hz. The duration for the former is longer at the far distance than the near distance. Also, the accelerograms of the Lake Hughes Array (distance from 26.6 to 29.6 km) have lesser durations than those for other paths. The site of the Santa Anita Reservoir is nearly at the southeastern front of the San Gabriel Mountain range and the source-station path is almost entirely within the crystalline mass of the San Gabriel Mountains. The site of Lake Hughes Array No. 1 is at the northern edge of the San Gabriel Mountain range and on the north side of the San Andreas Fault. The source-station path for Lake Hughes Array No. 1 is probably not entirely within the more uniform basement complex, and also the discontinuity of the San Andreas Fault might cause the difference in wave spectra.

Spectra dependent effect of integration process (on acceleration, particle velocity, and particle displacement)

32. The integration procedures tend to smooth out the rapid oscillations of the acceleration and allow the lower frequencies to become predominant. As an example, let us consider the Kern County, California, Earthquake of 21 July 1952 (magnitude 7.7).

33. The highest frequency of the acceleration response spectra in Figure 15 is 50 Hz. However, the accelerations reached a constant value at 14 Hz; the effective frequency was from 0.1 to 10 Hz. Figure 15 also indicates that the predominant frequencies of the acceleration response spectra are between 1 and 5 Hz because the maximum

accelerations are in this frequency range. Figures 16 and 17 show that the predominant frequencies of the velocity response spectra and the displacement spectra are between 0.5 and 1.5 Hz and 0.1 and 0.4 Hz, respectively. Newmark's tripartite logarithmic response spectra technique¹⁵ is based on these predominant frequency ranges. This also explains why the frequencies of maximum acceleration, maximum velocity, and maximum displacement cannot be correlated.

Average and Upper-Bound Spectral Shape

34. The spectral shape is dependent on magnitude, focal mechanism, propagation path, distance, duration, site geology, and damping ratio. At the present time, there is not enough instrumental data of strong earthquakes for a sufficient analysis of the above-mentioned parameters. Based on the total horizontal components of 201 in Appendix B, general average horizontal response spectra of acceleration, velocity, and displacement for the soil, intermediate rock, and hard rock sites are presented in Figures 23, 24, and 25, respectively. The upper-bound spectral shape can thus be extrapolated for the respective sites. Epicentral distances are in the range of 6-90 km. About 70 percent of these data were collected from the San Fernando, California, Earthquake of 9 February 1971. The amplitudes of acceleration, velocity, and displacement listed in Appendix B are not the relative amplitudes of response spectra, for they have to be multiplied by the dynamic amplification factor of 10, 6.67, and 5 for the soft, intermediate rock, and hard rock sites, respectively, to get the relative response spectral amplitudes. However, the average spectral shape is not changed. The processed spectral frequency range is between 0.1 and 10 Hz (see Appendix C), but the effective spectral peak frequency range is between 0.111 and 6.667 Hz (see Appendix B - predominant frequency range).

Average acceleration-peak spectra

35. Figures 23, 24, and 25 show the acceleration-peak distributions within the frequency range of 0.111-6.667 Hz for the magnitudes of 5.3-7.7 at soil, intermediate rock, and hard rock sites, respectively.

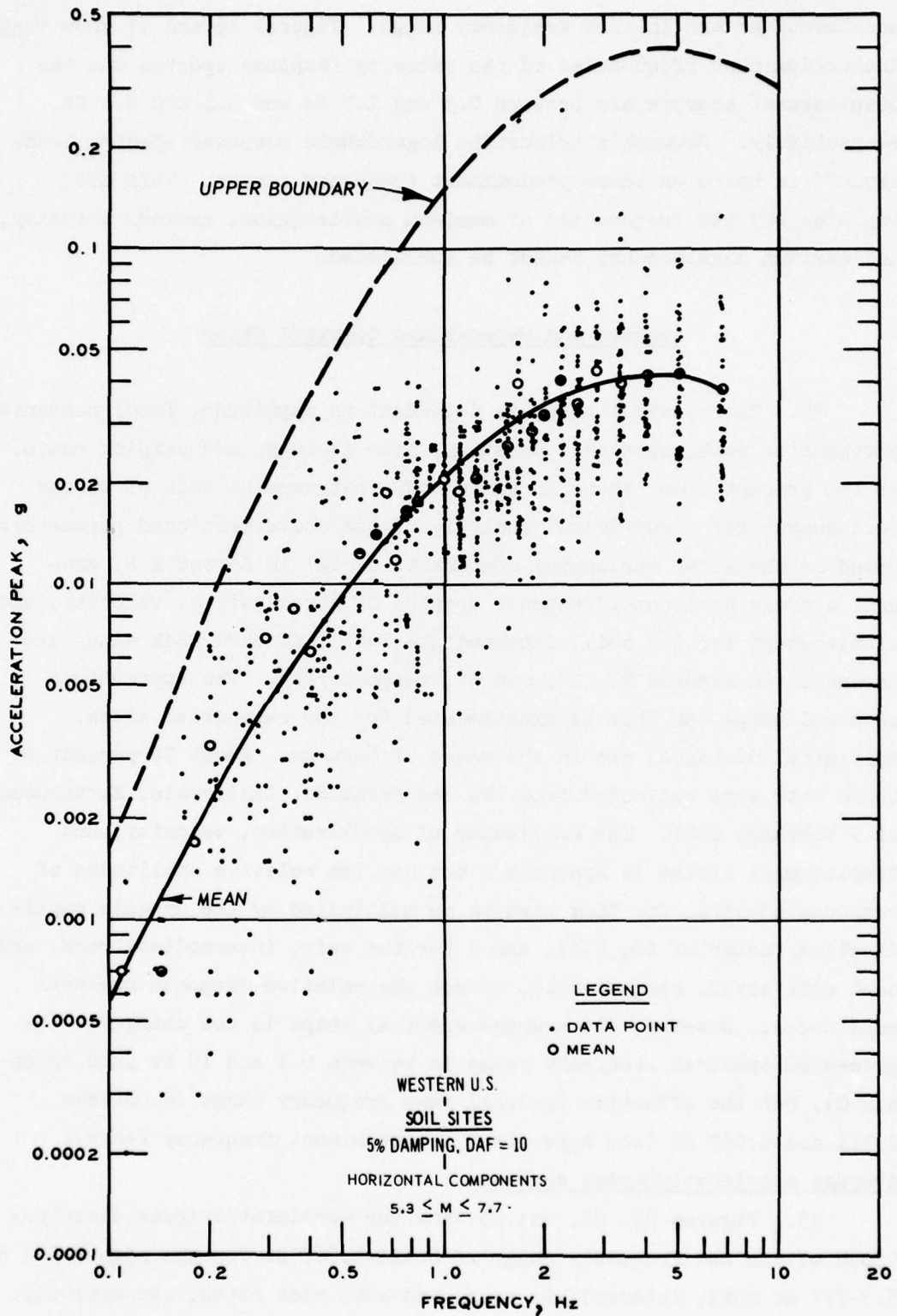


Figure 23. Average ground peak acceleration spectrum (mode shape) and upper-bound envelope of horizontal components for soil sites for earthquake magnitudes of 5.3-7.7 in western United States

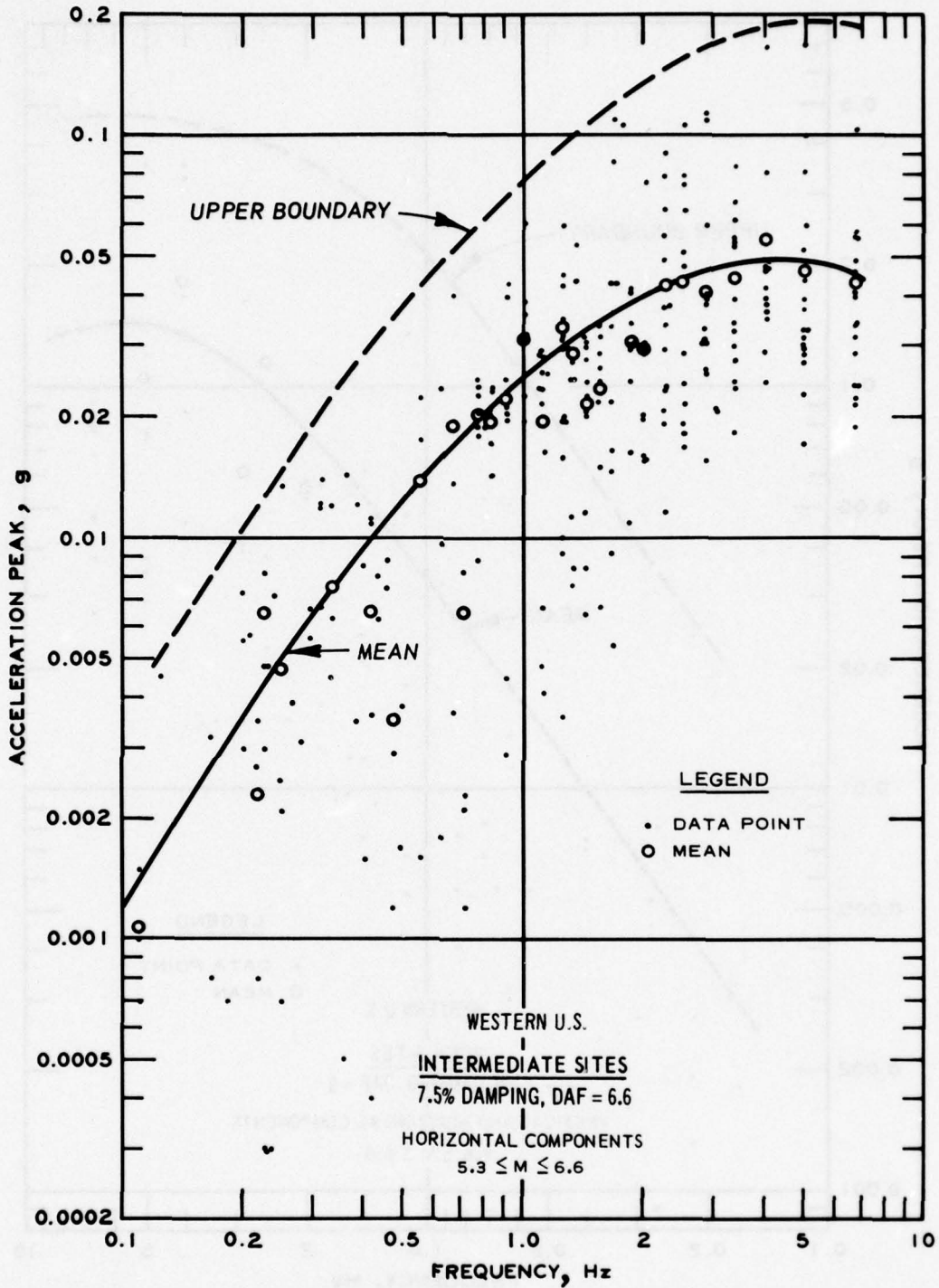


Figure 24. Average ground peak acceleration spectrum (mode shape) and upper-bound envelope of horizontal components for intermediate sites for earthquake magnitudes of 5.3-6.6 in western United States

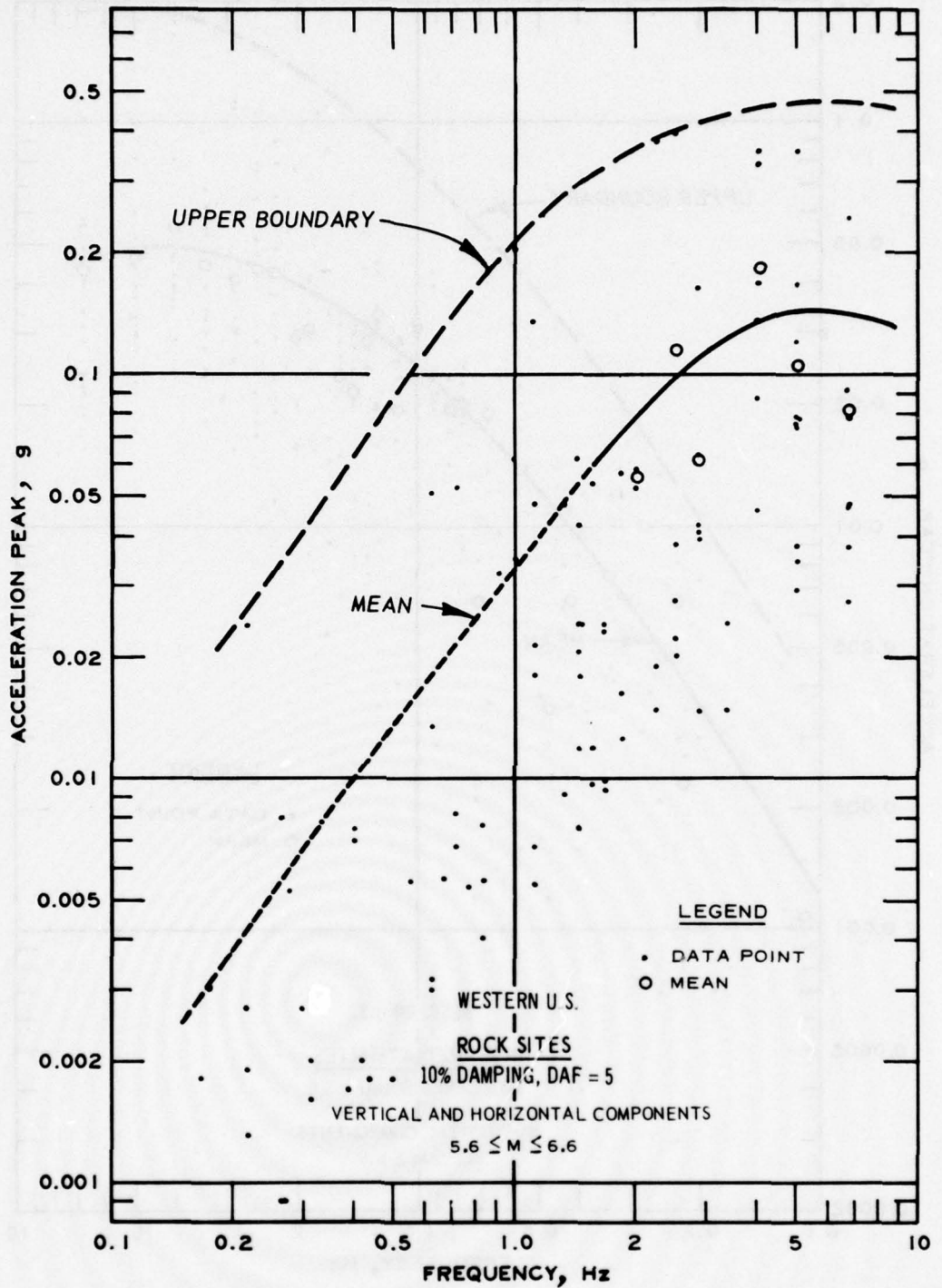


Figure 25. Average ground peak acceleration spectrum (mode shape) and upper-bound envelope of vertical and horizontal components for rock sites for earthquake magnitudes of 5.6-6.6 in western United States

The average acceleration curves of Figures 23-25 are presented in Figure 26, which shows a narrow frequency band of maximum peak accelerations between 2.5 and 5 Hz for the hard rock site and a wider frequency band between 2 and 6 Hz for the intermediate rock and soil sites. The differences between intermediate rock and soil sites are slight.

36. The general pattern of the three average acceleration curves of Figure 26 indicates that the amplitude increases from the lowest at a frequency of 0.11 Hz to the highest at 4 Hz for the soil site and 5 Hz for the intermediate and hard rock sites. In the frequency range of 0.1-2.0 Hz on the average acceleration spectrum for the hard rock site, the acceleration seems to increase linearly with frequency, but the intermediate rock and soil sites do not. The acceleration distribution is between 0.00003 g at 0.11 Hz and 0.4 g at 5 Hz for the soil site and 0.00008 g at 0.11 Hz and 0.45 g at 5 Hz for the hard rock site, according to the extrapolation of the upper-bound envelopes. Both 0.4 and 0.45 g at the discrete frequency of 5 Hz are probably the upper-bound or near upper-bound accelerations for the soil and rock sites at or near the fault rupture. At this point, it should be noted that the 1.25 g of the Pacoima record was the resultant amplitude obtained from the sum of the amplitudes of the predominant frequencies.

Average velocity-peak spectra

37. Figures 27-29 present the upper-bound velocity-peak and the average velocity-peak curves for the western United States strong earthquakes. The maximum average velocity peaks are located in the frequency range of 0.2-1.5 Hz (Figures 27 and 28) for soil and intermediate rock sites and 0.2-2.5 Hz (Figure 29) for the hard rock site. The ground-surface peak-amplitudes are within the range of 0.4-25 cm/sec for soil and intermediate rock sites, and 0.6 to 36 cm/sec for the hard rock site. In general, the soil and intermediate sites have the approximate same characteristics in average velocity spectral content, but the hard rock site has a different characteristic, which shows three peak-regions of 0.2-0.3, 0.7-0.8, and 2-3 Hz. Since the soil and intermediate rock sites have common spectral characteristics, they can be combined into a single representative alluvial or sedimentary site.

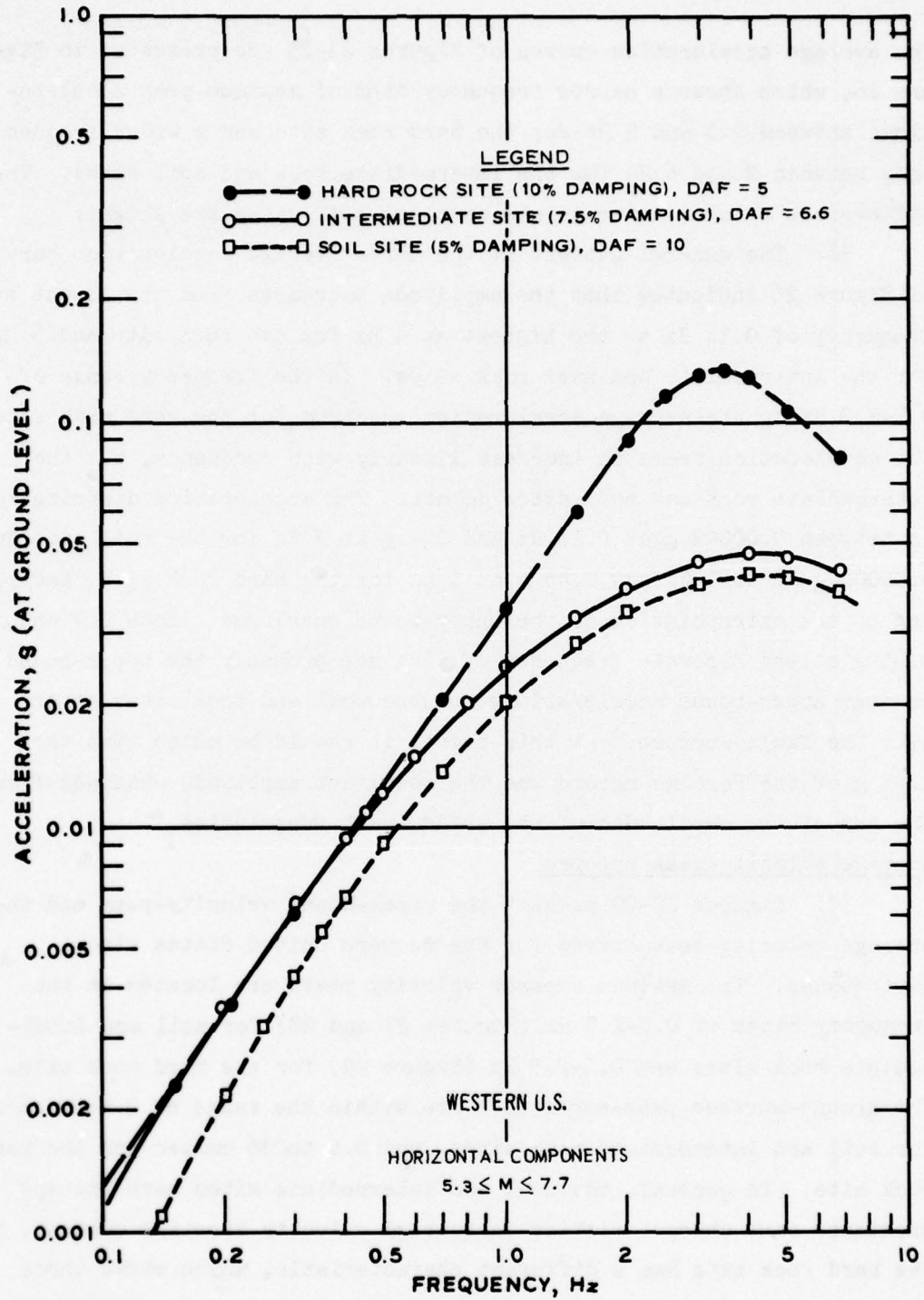


Figure 26. Average ground peak acceleration spectra of horizontal components for various site conditions for earthquake magnitudes of 5.3-7.7 in western United States

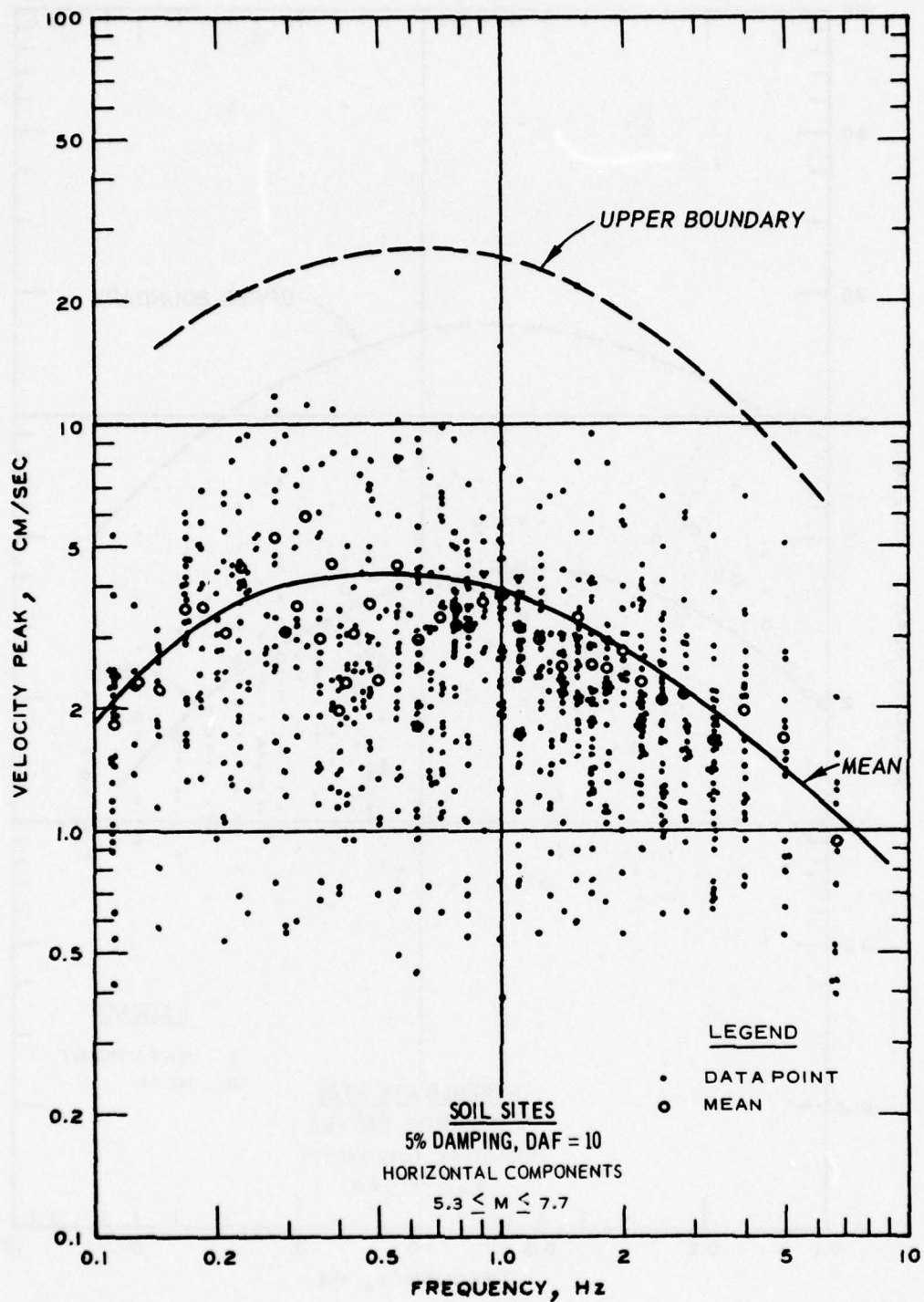


Figure 27. Average ground peak velocity spectrum and upper-bound envelope of horizontal components for soil sites for earthquake magnitudes of 5.3-7.7 in western United States

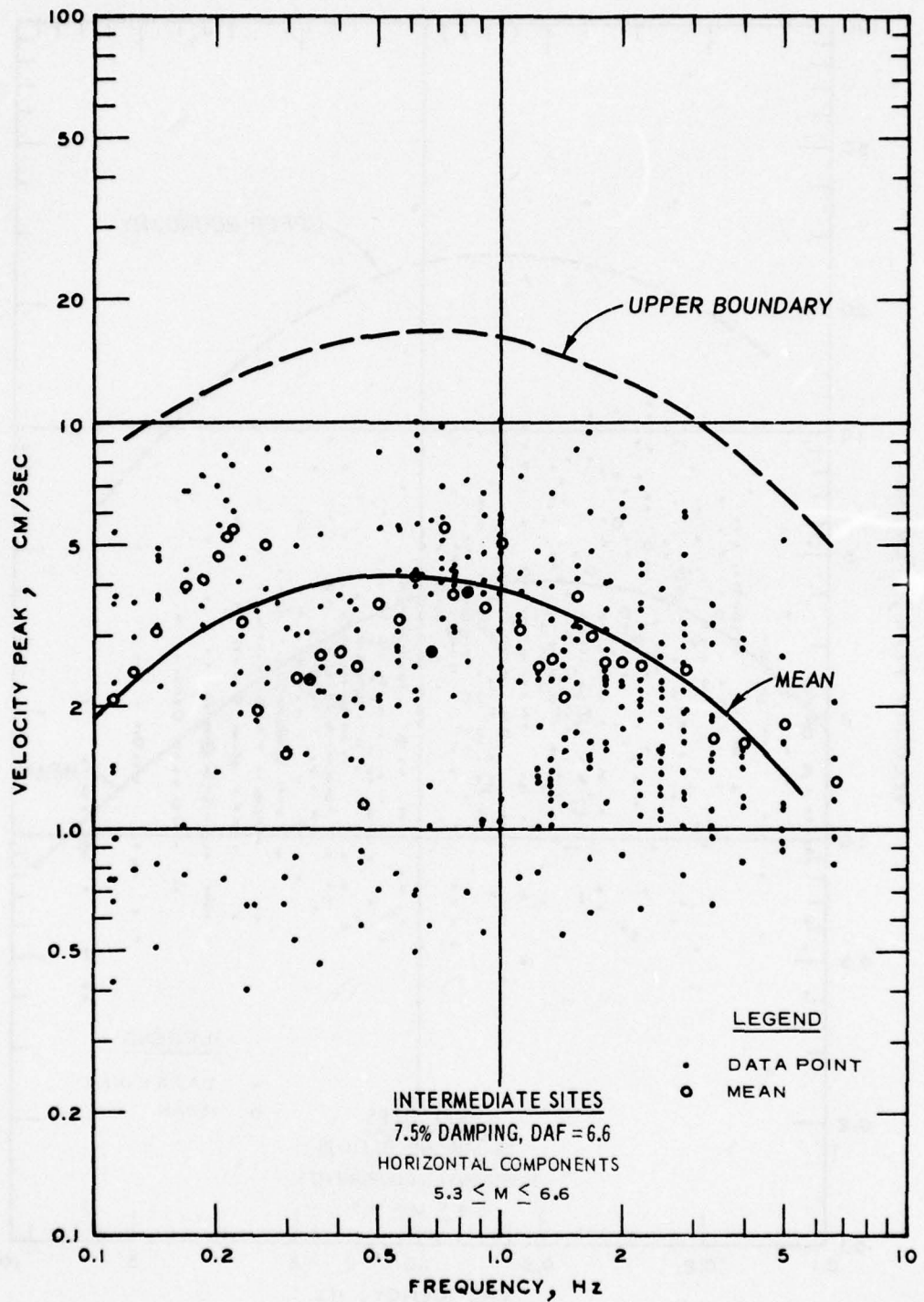


Figure 28. Average ground peak velocity spectrum and upper-bound envelope of horizontal components for intermediate sites for earthquake magnitudes of 5.3-6.6 in western United States

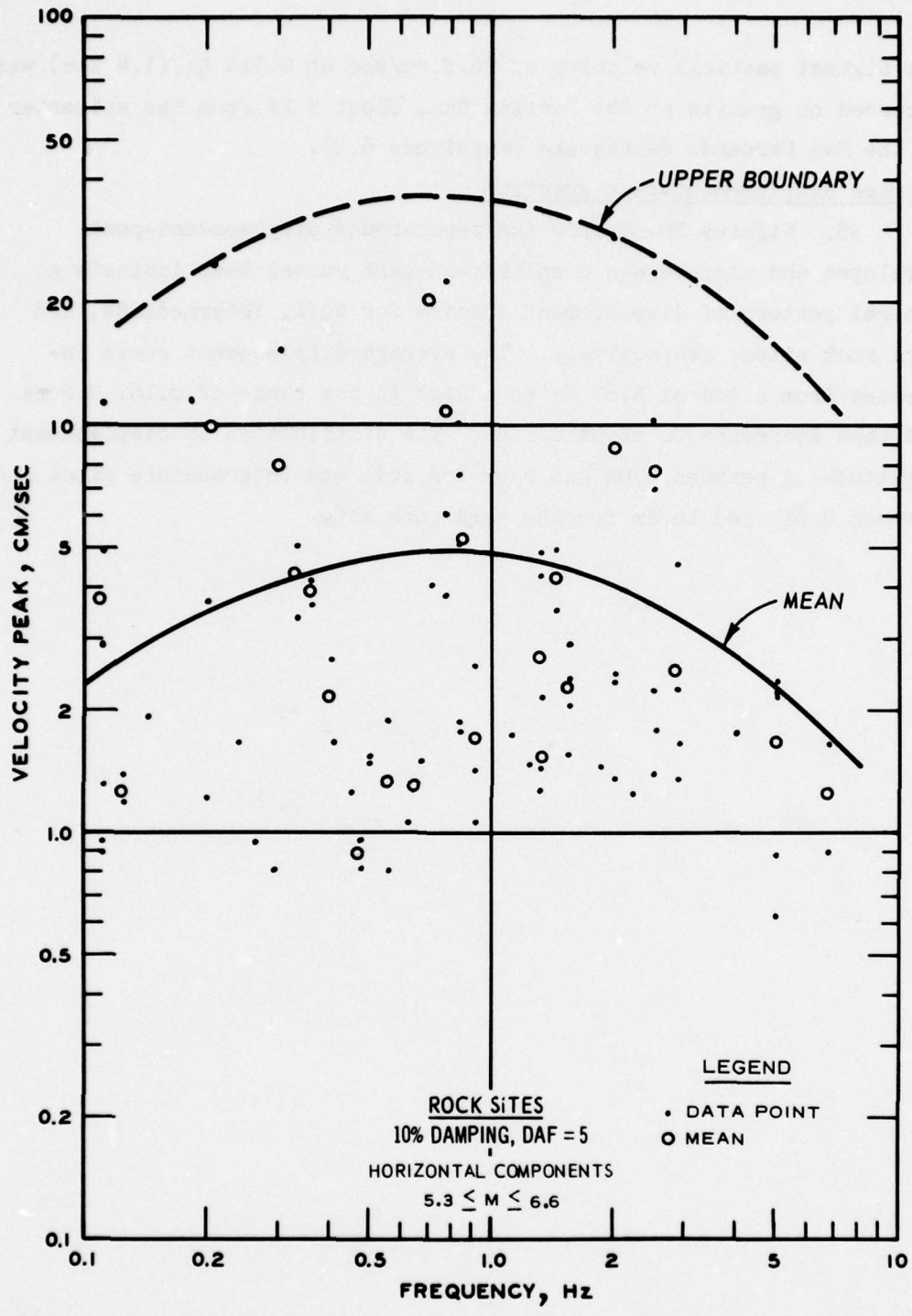
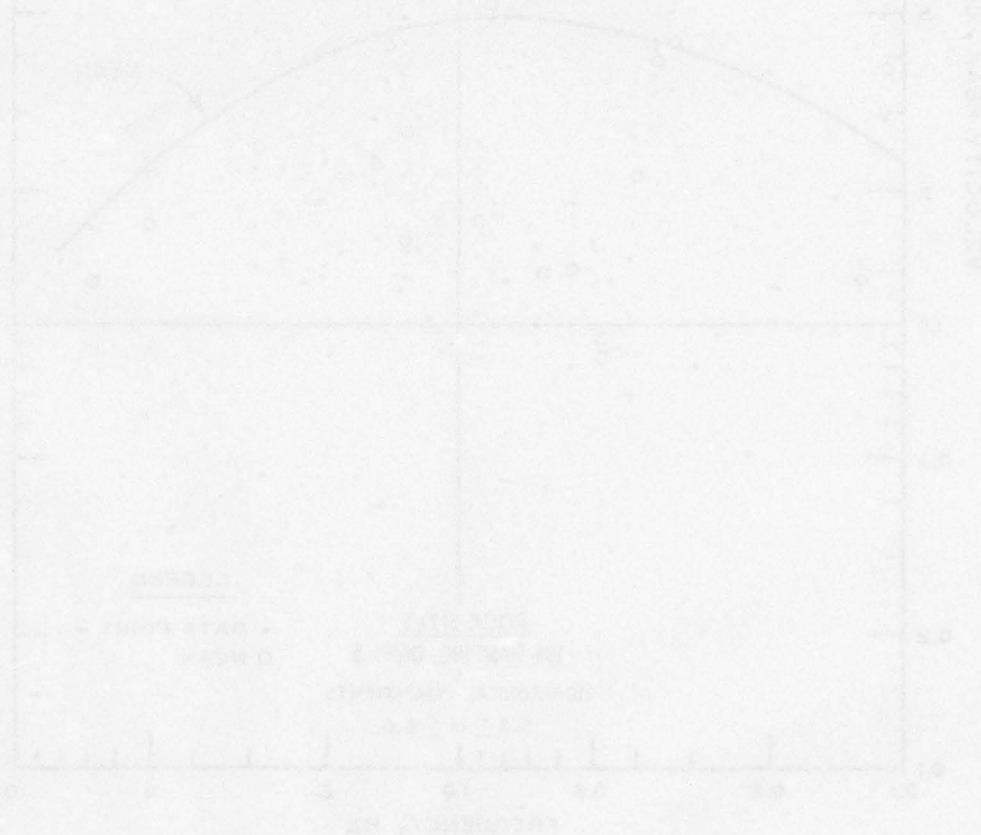


Figure 29. Average ground peak velocity spectrum and upper-bound envelope of horizontal components for rock sites for earthquake magnitudes of 5.6-6.6 in western United States

The highest particle velocity of 36.5 cm/sec at 0.714 Hz (1.4 sec) was recorded on granite at the Pacoima Dam, about 9 km from the epicenter of the San Fernando Earthquake (magnitude 6.5).

Average displacement-peak spectrum

38. Figures 30-32 show the upper-bound displacement-peak envelopes and the average displacement-peak curves that indicate a general pattern of displacement spectra for soil, intermediate, and hard rock sites, respectively. The average displacement curve increases from a low of 6.67 Hz to a high in the range of 0.167-0.2 Hz and then decreases to about 0.1 Hz. The distribution of displacement amplitude is between 0.02 and 8 cm for soil and intermediate sites and between 0.015 and 16 cm for the hard rock site.



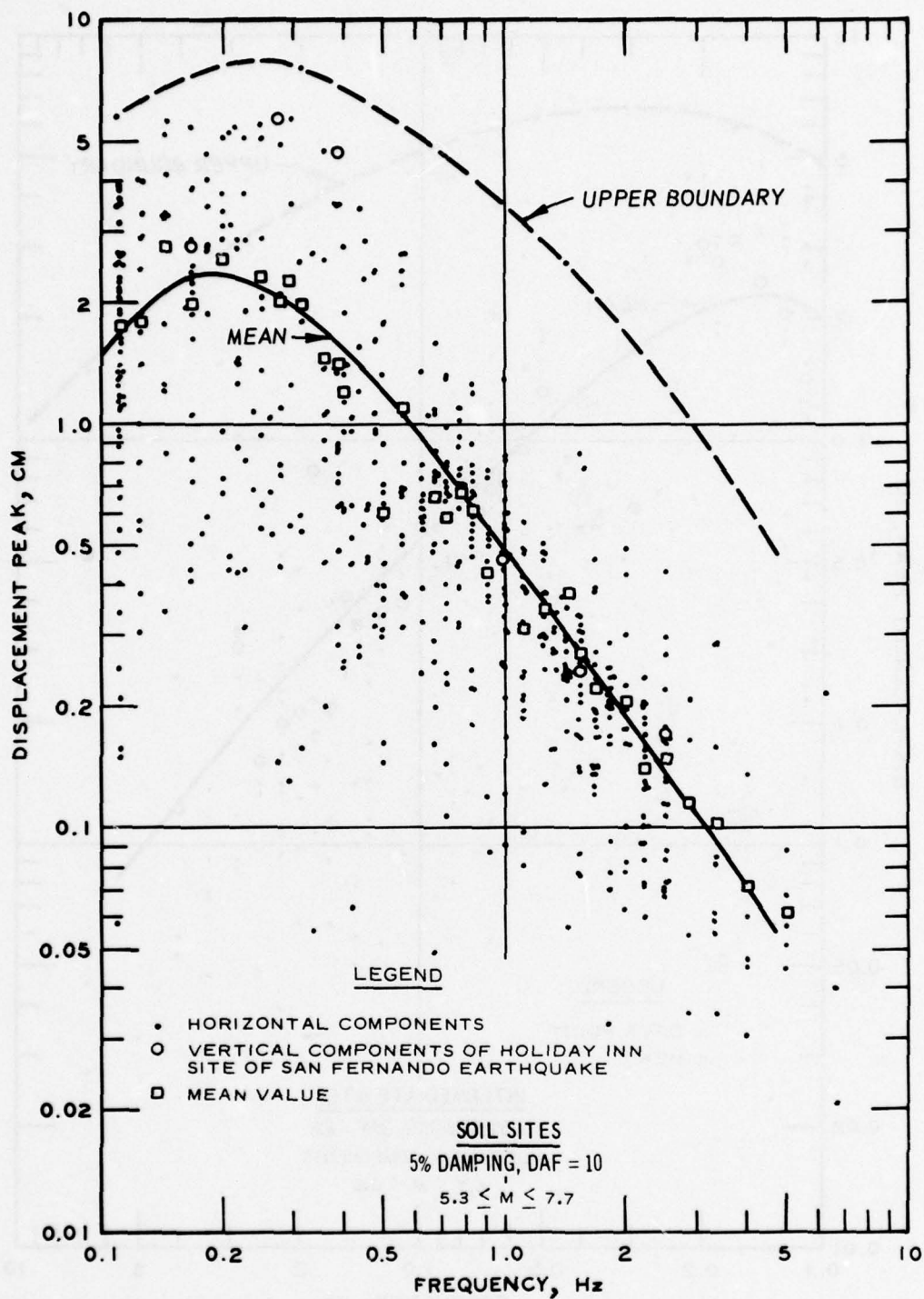


Figure 30. Average ground peak displacement spectrum and upper-bound envelope of horizontal components for soil sites for earthquake magnitude of 5.3-7.7 in western United States

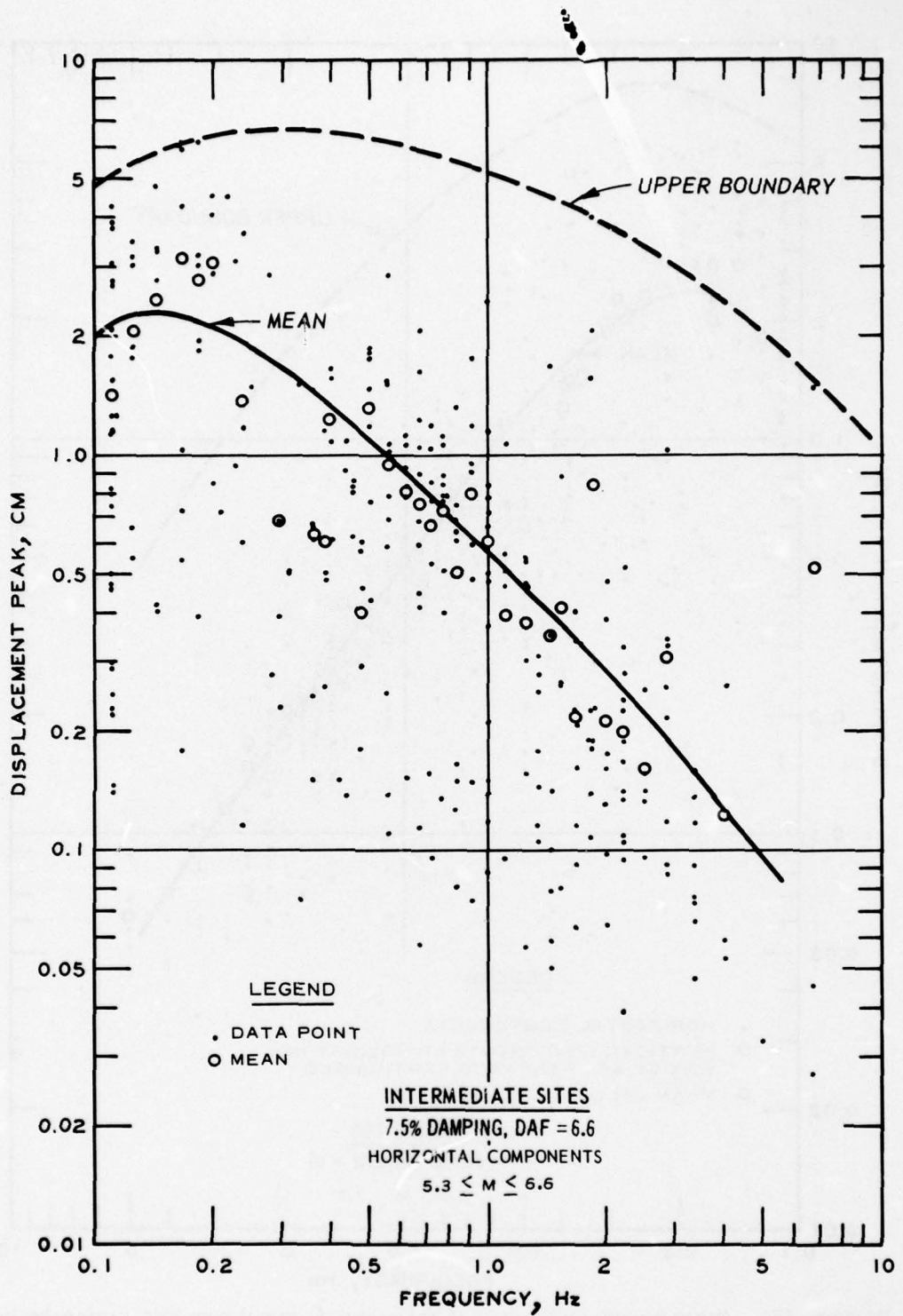


Figure 31. Average ground peak displacement spectra and upper-bound envelope of horizontal components for intermediate sites for earthquake magnitude of 5.3-6.6 in western United States

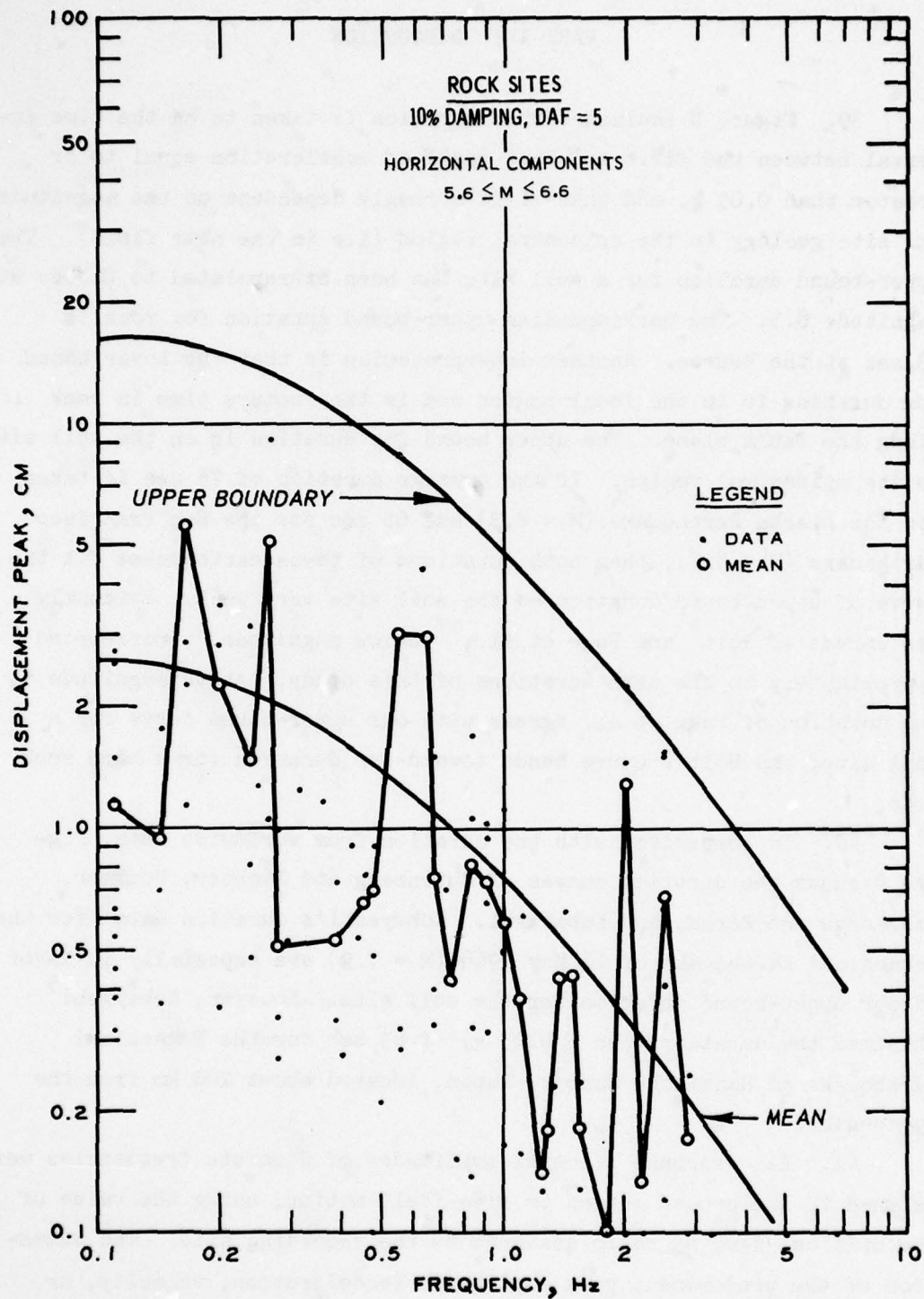


Figure 32. Average ground peak displacement spectrum and upper-bound envelope of horizontal components for rock sites for earthquake magnitudes of 5.6-6.6 in western United States

PART IV: DISCUSSION

39. Figure 8 indicates that duration is taken to be the time interval between the first and last peaks of acceleration equal to or greater than 0.05 g, and that it is strongly dependent on the magnitude and site geology in the epicentral region (i.e. in the near field). The upper-bound duration for a soil site has been extrapolated to 86 sec at magnitude 8.5. The corresponding upper-bound duration for rock is 43 sec at the source. Another interpretation is that the lower bound for duration is in the focal region and is the rupture time in rock along the fault plane. The upper bound for duration is on the soil site in the epicentral region. If the average duration of 75 sec is taken for the Alaska Earthquake ($M = 8.3$) and 65 sec for the San Francisco Earthquake ($M = 8.2$), then both durations of these earthquakes fit the curve of upper-bound duration on the soil site very well. Evidently, the curves of Bolt⁴ and Page et al.,¹⁷ below magnitude 7, correspond approximately to the mean durations of this study. Above magnitude 7, the duration of Page et al. agrees with our upper-bound curve for a soil site, and Bolt's curve bends toward our duration for a hard rock site.

40. In comparison with the duration from worldwide data, Figure 9 shows the duration curves of Gutenberg and Richter, Housner, Ambraseys and Sarma, and Kobayashi. Kobayashi's duration data⁵ for the Tokachioki Earthquake of 16 May 1968 ($M = 7.9$) are especially in favor of our upper-bound duration for the soil site. However, Kobayashi⁵ obtained the duration ($\text{acc} \geq 0.05 \text{ g}$) of 63 sec for the Tokachioki Earthquake at Hachinohe Harbor, Japan, located about 180 km from the hypocenter.

41. All response spectral amplitudes of discrete frequencies were reduced to the ground motion or free-field motion, using the value of the critical damping ratio assigned to the recording site. The summation of the predominant peak amplitudes (acceleration, velocity, or displacement) of the corresponding discrete frequencies will approximately equal the maximum amplitude in time history. This is based on

the theory of the one degree of freedom system with the base shaken by a single frequency at a given time. Therefore, the relative response spectral amplitude does not contain mixed frequencies. This technique provides a simple decomposition procedure to separate the wave frequencies from a seismogram and to provide clues to determine the equivalent damping ratio of various geological sites. Since the equivalent damping ratio is a basic, important factor in earthquake engineering, if the equivalent damping ratio of the site is not known, then the response spectra cannot be considered adequate.

42. A complete analysis of response spectra of acceleration for the San Fernando Earthquake, 9 February 1971, as a function of distance, site geology, and duration, has been made in this report. The data of other moderate and strong earthquakes with magnitudes of 5.3-7.7 in the western United States have also been analyzed and presented.

43. The upper-bound and average curves of the mixed data of acceleration, velocity, and displacement for all magnitudes ($5.3 < M < 7.7$ including San Fernando Earthquake) are presented in Figures 23-25 and 27-32 for different site conditions. Since about 70 percent of the total data were collected from the San Fernando Earthquake of magnitude 6.5, and the average magnitude between 5.3 and 7.7 is also 6.5, the average curves of acceleration, velocity, and displacement are naturally represented by the magnitude 6.5. If the magnitude, epicentral distance, site condition, maximum amplitude, and duration of a design earthquake are given, a synthetic seismogram of displacement could be predicted by the following simple equation of free vibration at any point on the ground surface:

$$y(t, p_i, n_i, \phi_i, \text{ and } c_i) = \sum_i c_i e^{-n_i p_i t} \sin(p_i t + \phi_i) \quad (1)$$

where

y = amplitudes of the time history of a synthetic seismogram

t = time duration (it is assumed that all predominant frequencies have the same duration)

p_i = 2π times the frequency of vibration of the i^{th} mode (predominant one)

n_i = ratio of damping in i^{th} mode to critical damping (small damping); but in this case, it is assumed that all predominant frequencies have the same damping

ϕ_i = phase angle of the i^{th} normal mode

c_i = amplitude or coefficient of each predominant frequency in the time history

In this equation, c_i can be chosen from the average smoothed ground-motion curves for different magnitude earthquakes, ϕ_i is the only parameter not known. Since it is assumed that all predominant frequencies are harmonic motions and have the same duration, or that all frequencies start to vibrate at the same time, then ϕ_i can be determined from the complex Fourier coefficients. An alternate way to compute ϕ_i is by a simple oscillator procedure, which is suggested by Khattri and Paul.³² The predominant frequency band of all moderate and strong earthquakes ($5.3 < M < 7.7$) is found approximately in the range of 0.1-7 Hz. Therefore, the frequency content in a synthetic seismogram should be evenly distributed in this range.

44. The networks of strong-motion instruments for the United States are growing. Eventually, it will be practicable to have all of the representative response spectra for the entire country. For the present, the data used in this report are restricted to the western United States and are of limited extent.

PART V: CONCLUSIONS

45. From the investigation of the strong-motion data (acc \geq 0.05 g) of western United States earthquakes, the following conclusions may be reached:

- a. The bracketed duration generally decreases with increasing distance.
- b. The duration is generally greater on soil sites than on rock sites.
- c. The maximum duration at the source (focus) in rock for the magnitude 8.5 was extrapolated to be about 43 sec but the duration is twice as long on soil or alluvium.
- d. The effective frequency content for all geological sites can be limited to a narrow range of 0.1-6.67 Hz. The possible maximum acceleration was found to be about 0.5 g at near-surface faulting for the discrete frequency range of 4-5 Hz.
- e. The predominant frequency bands for maximum ground motions of acceleration, velocity, and displacement are established as follows:

Horizontal acceleration for the soft and intermediate sites	2.0-6.0 Hz
Horizontal acceleration for the hard rock site	2.5-5.0 Hz*
Horizontal velocity for the soft and intermediate sites	0.3-2.0 Hz
Horizontal velocity for the hard rock site	0.5-2.5 Hz
Horizontal displacement for the soft and intermediate sites	0.15-0.3 Hz
Horizontal displacement for the hard rock site	0.1-0.5 Hz

- f. The acceleration response spectra do not positively indicate that the predominant periods increase with distance.
- g. The displacement response spectra do show the predominant periods increasing with distance.

* Bolt⁴ found 10 Hz for Pacoima record.

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APPENDIX A: STRONG MOTION DATA, EARTHQUAKES OF WESTERN UNITED STATES*

Record	Station Location	Date of Earthquake	Epicentral Location	Epicentral Distance km	Richter Magnitude M	Maximum MM Intensity	Local MM Intensity	Site Conditions**
A1	El Centro Site Imperial Valley	5-18-40	32°44'N 115°27'W	9.3	6.7	X	VIII	S
A2	Northwest California Earthquake, Ferndale City Hall	10-7-51	40°17'N 124°48'W	56.3	5.8	VII	V	I
A3	Kern County Earthquake, California, Cal Tech Athenaeum	7-21-52	35°00'N 119°02'W	126.0	7.7	XI	VII	S
A4	Kern County Earthquake, California, Taft Lincoln School	7-21-52	35°00'N 119°02'W	43.0	7.7	XI		S
A5	Kern County Earthquake, California, Santa Barbara Courthouse	7-21-52	35°00'N 119°02'W	89.5	7.7	XI		S
A6	Kern County Earthquake, California, Hollywood Storage Basement	7-21-52	35°00'N 119°02'W	119.5	7.7	XI		S
A8	Eureka Earthquake, Eureka Federal Building	12-21-54	32°38'N 117°07'W	24.0	6.5	VII		I
A9	Eureka Earthquake, Ferndale City Hall	12-21-54	32°38'N 117°07'W	40.0	6.5			I
A10	San Jose Earthquake, San Jose Bank of America Basement	9-4-55	37°22'N 121°53'W	9.8	5.5			S
A15	San Francisco Earthquake, San Francisco Golden Gate Park	3-22-57	37°40'N 122°29'W	11.8	5.3			I
A16	San Francisco Earthquake, San Francisco State Building Basement	3-22-57	37°40'N 122°29'W	14.6	5.3			I
A18	Hollister Earthquake	4-8-61	36°40'N 121°18'W	40.0	5.6			S
A19	Borrego Mt. Earthquake	4-8-68	33°09'N 116°08'W	69.8	6.5		VI	S
B21	Long Beach Earthquake, Vernon CMD Building	3-10-33	33°35'N 117°59'W	47.8	6.3	IX	VI	S
B22	Southern California Earthquake, Hollywood Storage Building Penthouse	10-2-33	33°47'N 118°08'W	38.2	5.4	VI	V	S
B24	Lower California Earthquake, El Centro Imperial Valley	12-30-34	32°12'N 115°30'W	60.8	6.5	IX	VI	S
B25	Helena, Montana, Earthquake, Helena, Montana, Carroll College	10-31-35	46°37'N 111°58'W	6.6	6.0	VIII	VII	I
B26	First Northwest California Earthquake, Ferndale City Hall	9-11-38	40°18'N 124°48'W	55.3	5.5	VI	VI	I
B28	Western Washington Earthquake, District Engineers Office at Army Base, Seattle	4-13-49	46°06'N 122°42'W	57.8	7.1	VIII	VIII	S
B29	Western Washington Earthquake, Olympia, Washington, Highway Test Lab	4-13-49	46°06'N 122°42'W	16.8	7.1	VIII	VIII	S
B30	Northern California Earthquake, Ferndale City Hall	9-22-52	40°12'N 124°25'W	43.2	5.5	VII	VI	S
B31	Wheeler Ridge, California, Earthquake, Taft Lincoln School Tunnel	1-12-54	35°00'N 119°01'W	43.0	5.9	VIII	VI	S
B32	Puget Sound, Washington, Earthquake, Olympia, Washington	4-29-65	47°24'N 122°18'W	61.1	6.5	VIII	VII	S
B33	Parkfield, California, Earthquake, Cholame, Shandon Array No. 2	6-27-66	35°54'N 120°54'W	31.9	5.6	VII	VII	S
B34	Parkfield, California, Earthquake, Cholame, Shandon Array No. 5	6-27-66		32.4	5.6		VI	S
B35	Parkfield, California, Earthquake, Cholame, Shandon Array No. 8	6-27-66		34.1	5.6		VI	S
B36	Parkfield, California, Earthquake, Cholame, Shandon Array No. 12	6-27-66		36.5	5.6		VI	S
B37	Parkfield, California, Earthquake, Temblor No. 2	6-27-66		31.0	5.6		VII	H
C41	San Fernando Earthquake, Pacoima Dam	2-9-71	34°24'N 118°23'42"W	9.1	6.6	XI	X	H
C48	San Fernando Earthquake, 8444 Orion Boulevard, First Floor Holiday Inn			22.4			VII	S
C51	San Fernando Earthquake, 250 E. First Street Basement, Los Angeles			42.8			VII	S
C54	San Fernando Earthquake, 445 Figueroa Street Subbasement Los Angeles			41.9			VII	I
D56	San Fernando Earthquake, Old Ridge Route, Castaic			28.6			VI	I
D57	San Fernando Earthquake, Hollywood Storage Basement			37.1			VII	S
D58	San Fernando Earthquake, Hollywood Storage P. E. Lot		34°24'N 118°23.7"W	37.1			VII	S

* Uniformly processed at California Institute of Technology.
 ** Site conditions: S = soft, I = intermediate, and H = hard rock.

Record	Station Location	Date of Earthquake	Epicentral Location	Epicentral Distance km	Richter Magnitude M	Maximum MM Intensity	Local MM Intensity	Site Conditions
D59	San Fernando Earthquake, 1901 Avenue, the Stars Subbasement	2-9-71	34°24'N 118°23.7'W	39.8	6.6	XI	VII	S
D62	San Fernando Earthquake, 1640 S. Marengo Street, First Floor, Los Angeles			42.8				S
D65	San Fernando Earthquake, 3710 Wilshire Boulevard Basement, Los Angeles			40.0				S
D68	San Fernando Earthquake, 7080 Hollywood Boulevard Basement, Los Angeles			35.0				S
E72	San Fernando Earthquake, 4680 Wilshire Boulevard Basement, Los Angeles			39.5				S
E75	San Fernando Earthquake, 3470 Wilshire Boulevard Sub-basement, Los Angeles			40.1				S
E78	San Fernando Earthquake, Water & Power Building Basement, Los Angeles			42.5				I
E81	San Fernando Earthquake, Santa Felicia Dam, California, Outlet Works (Piru)			32.9			VI	I
E83	San Fernando Earthquake, 3407 6th Street, Basement, Los Angeles			40.0			VII	S
F86	San Fernando Earthquake, Vernon, CMD Building			49.4			V	S
F88	San Fernando Earthquake, 633 East Broadway, Glendale			34.1			VII	I
F89	San Fernando Earthquake, 808 S. Olive, Los Angeles			44.0				S
F92	San Fernando Earthquake, 2011 Zonal Avenue Basement, Los Angeles			43.1				I
F95	San Fernando Earthquake, 120 N. Robertson Boulevard Sub-basement, Los Angeles			37.4				S
F98	San Fernando Earthquake, 646 S. Olive Avenue Basement, Los Angeles			42.7				S
F103	San Fernando Earthquake, Pumping Plant, Pearblossom, California			45.4			V	S
F104	San Fernando Earthquake, Oso Pumping Plant, Gorman, California			52.2			V	I
F105	San Fernando Earthquake, UCLA Reactor Lab (Boelter Hall), Los Angeles			38.7			VII	S
G106	San Fernando Earthquake, Seismological Lab, CIT, Pasadena			36.1				H
G107	San Fernando Earthquake, Athenaeum, CIT, Pasadena			39.8				S
G108	San Fernando Earthquake, Millikan Library, CIT, Pasadena			39.8				S
G110	San Fernando Earthquake, Jet Propulsion Laboratory, CIT, Pasadena			31.5				I
G112	San Fernando Earthquake, 611 W. Sixth Street, Los Angeles			42.5				S
G114	San Fernando Earthquake, Fire Station, Palmdale			32.3			VI	S
H115	San Fernando Earthquake, 15250 Ventura Boulevard, Los Angeles			29.3			VII	S
H121	San Fernando Earthquake, 900 S. Fremont Avenue, Alhambra			43.1			VII	S
H128	San Fernando Earthquake, 435 N. Oakhurst Avenue, Beverly Hills			36.0				S
H131	San Fernando Earthquake, 450 N. Roxbury Drive, Beverly Hills			38.2			VI	S
H134	San Fernando Earthquake, 1800 Century Park East, Los Angeles			38.9			VII	S
H137	San Fernando Earthquake, 15910 Ventura Boulevard, Los Angeles			29.0			VII	S

Record	Station Location	Date of Earthquake	Epicentral Location	Epicentral Distance km	Richter Magnitude M	Maximum MM Intensity	Local MM Intensity	Site Conditions**
J141	San Fernando Earthquake, Lake Hughes Array No. 1	2-9-71	34°24'N 118°23.7'W	29.6	6.6	XI	VI	H
J142	San Fernando Earthquake, Lake Hughes Array No. 4			26.8				H
J143	San Fernando Earthquake, Lake Hughes Array No. 9			26.6				H
J144	San Fernando Earthquake, Lake Hughes Array No. 12			23.3				I
J145	San Fernando Earthquake, 15107 Vanowen Street, Los Angeles			34.9			VII	S
J148	San Fernando Earthquake, 616 S. Normandie Avenue, Los Angeles			39.9				I
L166	San Fernando Earthquake, 3838 Lankershim Boulevard, Sheraton Universal Hotel, Los Angeles			30.8				I
M176	San Fernando Earthquake, 1150 S. Hill Street, Los Angeles			42.9				S
N185	San Fernando Earthquake, Carbon Canyon Dam, Brea			75.6			V	I
N186	San Fernando Earthquake, Whittier Narrows Dam, Whittier			54.1			VI	S
N187	San Fernando Earthquake, San Antonio Dam, Upland			72.1			VI	S
N188	San Fernando Earthquake, 1880 Century Park East, Los Angeles			38.9			VII	S
N192	San Fernando Earthquake, 2500 Wilshire Boulevard, Los Angeles			40.7				I
0198	San Fernando Earthquake, Griffith Park Observatory, Los Angeles			34.0				H
0199	San Fernando Earthquake, 1625 Olympic Boulevard, Los Angeles			42.0				S
0207	San Fernando Earthquake, Fairmont Reservoir, Fairmont			32.8			VI	H
F214	San Fernando Earthquake, 4867 Sunset Boulevard, Los Angeles			36.2			VII	I
F217	San Fernando Earthquake, 3345 Wilshire Boulevard, Los Angeles			40.0			VII	S
F221	San Fernando Earthquake, Santa Anita Reservoir, Arcadia			43.3			VI	H
F223	San Fernando Earthquake, Puddingstone Reservoir, San Dimas			65.0			V	H
Q233	San Fernando Earthquake, 14724 Ventura Boulevard, Los Angeles			29.3			VII	S
Q236	San Fernando Earthquake, 1760 N. Orchid Avenue, Los Angeles			34.9				S
Q239	San Fernando Earthquake, 9100 Wilshire Boulevard, Los Angeles			38.0				S
Q241	San Fernando Earthquake, 800 W. First Street, Los Angeles			41.8				I
R244	San Fernando Earthquake, 222 Figueroa Street, Los Angeles			41.9				I
R246	San Fernando Earthquake, 6464 Sunset Boulevard, Los Angeles			35.7				S
R248	San Fernando Earthquake, 6430 Sunset Boulevard, Los Angeles			35.7				S
R249	San Fernando Earthquake, 1900 Avenue of the Stars, Los Angeles			39.2				S
R251	San Fernando Earthquake, 234 S. Figueroa Street, Los Angeles			41.8				I
R253	San Fernando Earthquake, 533 S. Fremont Avenue, Los Angeles			42.0				S
S255	San Fernando Earthquake, 6200 Wilshire Boulevard, Los Angeles			38.9				I
S258	San Fernando Earthquake, 3440 University Avenue, Los Angeles			44.6				S

Record	Station Location	Date of Earthquake	Epicentral Location	Epicentral Distance km	Richter Magnitude M	Maximm MM Intensity	Local MM Intensity	Site Conditions
S261	San Fernando Earthquake, 1177 Beverly Drive, Los Angeles	2-9-71	34°24'N 118°23.7'W	39.6	6.6	XI	VII	S
S262	San Fernando Earthquake, 5900 Wilshire Boulevard, Los Angeles	↓	↓	39.0	↓	↓	↓	I
S265	San Fernando Earthquake, 3411 Wilshire Boulevard, Los Angeles	↓	↓	39.9	↓	↓	↓	I
S266	San Fernando Earthquake, 3550 Wilshire Boulevard, Los Angeles	↓	↓	40.0	↓	↓	↓	S
S267	San Fernando Earthquake, 5260 Century Boulevard, Los Angeles	↓	↓	52.0	↓	↓	VI	S
U297	Helena, Montana, Federal Building	11-28-35	46°37'N 111°58'W	5.8	↓	VI	VI	H
U299	Santa Barbara Courthouse, California	6-30-41	34°22'N 119°35'W	35.9	5.9	VIII	VIII	S
U301	Northern California Earthquake, Public Library, Hollister, California	3- 9-49	37°06'N 121°18'W	29.3	5.3	VII	VII	S
U305	Central California Earthquake, Public Library, Hollister, California	4-25-54	36°48'N 121°48'W	36.2	5.3	VII	VI	S
U308	Northern California Earthquake, Ferdale City Hall	6- 5-60	40°49'N 124°55'W	60.3	5.7	VI	VI	I
U309	Central California Earthquake, Public Library, Hollister, California	4- 8-61	36°30'N 121°18'W	40.0	5.7	VII	VII	S
U312	Northern California Earthquake, City Hall, Ferdale	12-10-67	40°30'N 124°36'W	30.6	5.8	VI	VI	S
V321	San Francisco Earthquake	3-22-57	37°40'N 122°29'W	24.3	5.3	VII	V	S

Record	Instrument Direction	Peak Acceleration cm/sec	Duration sec (Acc \geq 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks	
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm
A10	N59°E	105.8	0.42			0.111 (9.00) 1.000 (1.00)	0.4194 0.3880	5.000 (6.20) 1.818 (0.55)	0.0445 0.0322
A15	N10°E	81.8	0.28	4.000 (0.25) 6.667 (0.15) 1.111 (0.90) 0.500 (2.00)	0.0351 0.0314 0.0041 0.0017	3.333 (0.30) 1.250 (0.80) 0.111 (9.00) 0.500 (2.00)	1.3971 0.7843 0.7505 0.7129	0.111 (9.00) 1.000 (1.00) 3.333 (0.30) 1.429 (0.70)	0.4620 0.0876 0.0662 0.0592
	S80°E			102.8	1.30	5.000 (0.20) 2.500 (0.40) 1.538 (0.65)	0.0438 0.0167 0.0067	4.000 (0.25) 2.222 (0.45) 1.000 (1.00)	1.5268 1.2154 1.1881
A16	S09°W	83.8	0.30	4.000 (0.25) 6.667 (0.15) 2.000 (0.50) 0.714 (1.40)	0.0418 0.0285 0.0156 0.0021	3.333 (0.30) 1.667 (0.60) 2.500 (0.40) 0.667 (1.50)	1.8609 1.5137 1.3746 1.0161	0.111 (9.00) 0.294 (3.40) 0.476 (2.10) 1.818 (0.55)	0.2986 0.2313 0.1824 0.1087
	S81°W			55.1	1.26	2.500 (0.40) 6.667 (0.15) 1.538 (0.65) 0.400 (2.50)	0.0214 0.0213 0.0150 0.0016	1.333 (0.75) 2.222 (0.45) 0.556 (1.80) 0.294 (3.40)	1.4840 1.4570 0.7797 0.7625
A18	S01°W	63.4	10.00	1.818 (0.55) 1.429 (0.70) 3.333 (0.30) 6.667 (0.15) 0.909 (1.10)	0.0271 0.0225 0.0187 0.0181 0.0122	1.333 (0.75) 0.909 (1.10) 1.818 (0.55) 0.769 (1.30) 0.400 (2.50)	2.6131 2.3438 2.2093 2.1556 1.3856	0.167 (6.00) 0.417 (2.40) 0.714 (1.40) 0.500 (2.00) 0.909 (1.10)	0.8176 0.4539 0.4063 0.3679 0.3637
	N89°W			175.7	9.04	2.500 (0.40) 1.333 (0.75) 0.769 (1.30) 0.556 (1.80)	0.0552 0.0250 0.0180 0.0072	0.769 (1.30) 2.222 (0.45) 1.333 (0.75) 0.500 (2.00)	3.6520 3.6392 3.0625 2.8771
A19	S00°W	127.8	2.56	4.000 (0.25) 0.769 (1.30) 2.500 (0.40) 6.667 (0.15) 1.538 (0.65)	0.0253 0.0244 0.0227 0.0208 0.0205	0.756 (1.80) 0.417 (2.40) 1.538 (0.65) 2.500 (0.40) 3.333 (0.30)	5.9603 5.0258 2.0954 2.9612 0.7200	0.400 (2.50) 0.313 (3.20) 0.111 (9.00) 2.000 (0.50)	1.8945 1.8035 1.3019 0.1004
	B21			S08°W	130.6	1.72	3.333 (0.30) 2.222 (0.45) 1.667 (0.60) 1.111 (0.90)	0.0336 0.0324 0.0312 0.0243	1.000 (1.00) 0.435 (2.30) 1.667 (0.60) 0.111 (9.00)
B21	S82°W	151.5	5.82	3.333 (0.300) 1.538 (0.650) 1.000 (1.000) 1.333 (0.750) 0.625 (1.600)	0.0324 0.0216 0.0191 0.0177 0.0101	1.000 (1.00) 0.263 (3.80) 1.000 (1.00) 0.417 (2.40) 1.538 (0.65) 3.333 (0.30) 2.500 (0.40)	3.4127 3.3328 3.0674 2.9798 2.0732 1.4746 1.4129	0.111 (9.00) 0.167 (6.00) 0.250 (4.00) 0.227 (4.40) 0.833 (1.20) 1.333 (0.75) 1.538 (0.65)	2.6346 2.0449 1.9287 1.9006 0.5451 0.2465 0.2256
	DOWN			149.5	3.64	5.000 (0.20) 2.500 (0.40) 2.000 (0.50) 0.769 (1.30) 1.333 (0.75)	0.0268 0.0221 0.0147 0.0069 0.0065	0.278 (3.60) 0.143 (7.00) 2.500 (0.40) 0.769 (1.30) 0.625 (1.60)	2.2832 1.6259 1.4417 1.3307 1.1444
B22	N90°E	85.4	8.04	1.818 (0.55) 0.294 (3.40) 0.400 (2.50) 0.455 (2.20)	0.0462 0.0025 0.0020 0.0019	1.667 (0.60) 0.227 (4.40) 0.294 (3.40) 0.435 (2.30) 0.111 (9.00)	4.0599 1.4753 1.4251 0.9572 0.9518	0.111 (9.00) 0.217 (4.60) 0.278 (3.60) 1.667 (0.60) 0.833 (1.20)	1.0947 0.8734 0.7470 0.3829 0.1781
B24	N00°E	156.8	12.86	4.000 (0.25) 2.857 (0.35) 1.818 (0.55) 1.111 (0.90) 0.400 (2.50)	0.0608 0.0380 0.0350 0.0212 0.0055	1.667 (0.60) 1.111 (0.90) 0.769 (1.30) 0.400 (2.50) 4.000 (0.25)	3.1244 3.1240 3.1006 2.4152 2.3029	0.217 (4.60) 0.385 (2.60) 0.125 (8.00) 0.278 (3.60) 0.909 (1.10)	1.2536 0.8985 0.8095 0.7026 0.5542
	N90°W			179.1	18.12	4.000 (0.25) 2.500 (0.40) 1.538 (0.65) 0.667 (1.50) 0.500 (2.00)	0.0635 0.0463 0.0330 0.0066 0.0065	1.429 (0.70) 2.000 (0.50) 1.111 (0.90) 0.909 (1.10) 0.417 (2.40)	3.9192 3.0587 2.8593 2.7684 2.2843
B24	UP	68.1	11.70	4.000 (0.25) 2.857 (0.35) 1.818 (0.55) 1.538 (0.65) 1.333 (0.75) 0.556 (1.80)	0.0218 0.0106 0.0093 0.0074 0.0030	0.143 (7.00) 1.538 (0.65) 1.818 (0.55) 0.500 (2.00) 0.417 (2.40) 2.857 (0.35) 1.000 (1.00)	1.3040 1.0780 1.0553 1.0533 0.9610 0.8865 0.7710	0.111 (9.00) 0.400 (2.50) 0.476 (2.10) 1.000 (1.00) 1.250 (0.80) 1.538 (0.65) 1.818 (0.55)	1.6326 0.2999 0.2879 0.1255 0.1146 0.0973 0.0800
	B25			S00°W	143.5	1.46	6.667 (0.15) 2.857 (0.35) 4.000 (0.25) 0.667 (1.50)	0.0490 0.0308 0.0285 0.0037	2.000 (0.50) 2.500 (0.40) 0.667 (1.50) 6.667 (0.15)
B25	S90°W	142.5	1.30	3.333 (0.30) 6.667 (0.15) 1.111 (0.90)	0.0542 0.0456 0.0057	0.667 (1.50) 0.833 (1.20) 1.111 (0.90)	3.8217 3.8212 3.7863	0.111 (9.00) 0.500 (2.00) 0.833 (1.20)	0.1606 0.1447 0.0271
	DOWN			87.5	0.48	4.000 (0.25) 6.667 (0.15) 2.857 (0.35) 0.625 (1.60) 1.250 (0.80)	0.0292 0.0288 0.0276 0.0097 0.0072	0.476 (2.10) 0.208 (4.80) 2.500 (0.40) 1.250 (0.80) 6.667 (0.15)	2.6009 1.6967 1.5971 0.7535 0.6696
B26	N45°E	140.9	1.32	3.333 (0.30) 5.000 (0.20) 2.222 (0.45) 0.909 (1.10)	0.0342 0.0313 0.0295 0.0045	2.000 (0.50) 3.333 (0.30) 0.909 (1.10) 0.313 (3.20)	2.22874 1.5236 1.0356 0.8525	0.111 (9.00) 2.000 (0.50) 0.833 (1.20) 1.333 (0.75) 3.333 (0.30)	0.8051 0.1757 0.1481 0.1156 0.0759

Record	Instrument Direction	Peak Acceleration cm/sec ²	Duration sec (Acc \geq 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks		
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm	
B34	N85°E	425.7	7.30	0.500 (2.00)	0.0133	1.111 (0.90)	3.6092	0.833 (1.20)	0.7592	
						0.667 (1.50)	3.1034	2.500 (0.40)	0.4313	
	DOWN	116.9	7.32	6.667 (0.15)	0.0400	2.000 (0.50)	1.7252	2.000 (0.50)	0.4005	
				2.222 (0.45)	0.0231	0.208 (4.80)	1.1067	0.111 (9.00)	0.4322	
B35	N50°E	232.6	7.84	6.667 (0.15)	0.0686	1.000 (1.00)	2.6059	0.111 (9.00)	1.1138	
				2.500 (0.40)	0.0325	1.667 (0.60)	2.1080	1.000 (1.00)	0.3944	
				1.667 (0.60)	0.0209	1.250 (0.80)	2.0862	1.667 (0.60)	0.1859	
				1.333 (0.75)	0.0169	2.222 (0.45)	2.0702	2.222 (0.45)	0.1514	
	N40°W	269.6	5.70	1.000 (1.00)	0.0156	5.000 (0.20)	1.8664	5.000 (0.20)	0.0570	
				5.000 (0.20)	0.0890	2.000 (0.50)	3.0493	0.111 (9.00)	1.0094	
				2.000 (0.50)	0.0368	1.250 (0.80)	2.9962	0.395 (2.60)	0.6303	
				1.250 (0.80)	0.0185	5.000 (0.20)	2.7443	0.556 (1.80)	0.5301	
				0.769 (1.30)	0.0082	2.857 (0.35)	2.6980	1.000 (1.00)	0.3569	
				0.667 (1.50)	0.0076	0.714 (1.40)	2.5467	2.000 (0.50)	0.2250	
						0.476 (2.10)	1.9132	1.538 (0.65)	0.1699	
						1.538 (0.65)	1.8721	5.000 (0.20)	0.0877	
	DOWN	77.7	3.94	1.111 (0.90)	0.0090	1.000 (1.00)	1.3279	0.111 (9.00)	0.3104	
				2.500 (0.40)	0.0079	0.769 (1.30)	1.1155	0.208 (4.80)	0.2892	
				0.278 (3.60)	0.0007	0.182 (5.50)	0.5370	0.714 (1.40)	0.1979	
						4.000 (0.25)	0.4953	0.417 (2.40)	0.1343	
	B37	N65°W	264.3	2.90	4.000 (0.25)	0.1365	2.500 (0.40)	7.0274	0.250 (4.000)	1.2888
					1.111 (0.90)	0.0180	0.333 (3.00)	5.0506	0.313 (3.20)	1.2535
					0.625 (1.60)	0.0135	0.714 (1.40)	4.0648	0.111 (9.00)	1.1436
							1.429 (0.70)	3.5016	0.476 (2.10)	0.9054
S25°W		340.8	2.08	2.857 (0.35)	0.1624	2.500 (0.40)	10.2746	0.111 (9.00)	0.4119	
				5.000 (0.20)	0.1201	0.833 (1.20)	7.5019	0.167 (6.00)	1.5028	
				1.000 (1.00)	0.0350	0.111 (9.00)	4.9159	0.278 (3.60)	0.9916	
						1.333 (0.75)	4.8882	0.909 (1.10)	0.9509	
DOWN		129.8	0.58	6.667 (0.15)	0.0468	2.857 (0.35)	3.6368	0.714 (1.40)	0.7072	
				1.538 (0.65)	0.0120	1.333 (0.75)	1.7799	0.111 (9.00)	0.6340	
				0.769 (1.30)	0.0054	0.625 (1.60)	1.4624	0.238 (4.20)	0.3368	
				0.263 (3.80)	0.0009	0.833 (1.20)	1.3852	0.500 (2.00)	0.3280	
C41	S16°E	1148.1	11.36	2.500 (0.40)	0.3957	0.714 (1.40)	36.4629	0.167 (6.00)	15.8704	
				5.000 (0.20)	0.3549	0.208 (4.80)	25.0099	0.263 (3.80)	9.1517	
				1.000 (1.00)	0.2042	2.500 (0.40)	23.6821	0.556 (1.80)	8.4209	
				0.217 (4.60)	0.0240			2.500 (0.40)	1.5366	
	S74°W	1054.9	12.44	2.222 (0.45)	0.3780	2.000 (0.50)	28.8445	2.000 (0.50)	1.4654	
				4.000 (0.25)	0.3525	0.769 (1.30)	22.4607	0.625 (1.60)	4.3962	
				1.111 (0.90)	0.1350	0.333 (3.00)	15.2945	0.200 (5.00)	3.1244	
						0.182 (5.50)	11.4690	0.111 (9.00)	2.8298	
	DOWN	696.0	10.50	4.000 (0.25)	0.3336	0.111 (9.00)	11.2648	2.000 (0.50)	2.2208	
				6.667 (0.15)	0.2427	2.857 (0.35)	16.6026	0.125 (8.00)	8.2036	
				0.714 (1.40)	0.0527	0.455 (2.20)	15.5078	0.333 (3.00)	5.0793	
				0.625 (1.60)	0.0512	0.357 (2.80)	15.0347	1.538 (0.65)	0.8104	
C48	N00°W	250.0	17.22	1.538 (0.65)	0.0810	0.556 (1.80)	10.2220	0.217 (4.60)	5.4476	
				1.818 (0.55)	0.0739	0.769 (1.30)	9.2299	0.455 (2.20)	2.8314	
				3.333 (0.30)	0.0693	0.217 (4.60)	8.1832	0.556 (1.80)	2.6390	
				2.500 (0.40)	0.0662	1.538 (0.65)	8.1015	0.111 (9.00)	2.5089	
	S90°W	131.7	17.82	5.000 (0.20)	0.0573	0.455 (2.20)	7.5525	1.538 (0.65)	0.8447	
				0.769 (1.30)	0.0399	0.278 (3.60)	6.5595			
				0.476 (2.10)	0.0247	1.250 (0.80)	6.2827			
				0.227 (4.40)	0.0110	2.222 (0.45)	4.1531			
	DOWN	167.5	22.22	0.263 (3.80)	0.0101	0.111 (9.00)	11.6005			
				0.111 (9.00)	0.0013		9.2975			
				2.857 (0.35)	0.0545	0.333 (0.30)	8.5784			
				1.538 (0.65)	0.0323	0.667 (1.50)				
0.769 (1.30)				0.0301	0.476 (2.10)					
1.000 (1.00)				0.0293	0.227 (4.40)					
0.667 (1.50)				0.0287	1.000 (1.00)					
0.357 (2.80)				0.0245	1.538 (0.65)					
C51	N36°E	97.8	8.16	2.500 (0.40)	0.0317	0.769 (1.30)	3.0489	0.111 (9.00)	2.6356	
				3.333 (0.30)	0.0288	0.143 (7.00)	2.8214	0.833 (1.20)	0.6563	
				1.538 (0.65)	0.0196	0.278 (3.60)	2.5429	1.250 (0.80)	0.3035	
				1.333 (0.75)	0.0194	1.250 (0.80)	2.4115	1.538 (0.65)	0.2044	
	N54°W	122.7	6.16	0.833 (1.20)	0.0185	1.538 (0.65)	2.1061	2.222 (0.45)	0.1563	
				0.455 (2.20)	0.0057	2.222 (0.45)	2.0949			
				0.313 (3.20)	0.0048	3.333 (0.30)	1.4120			
				2.222 (0.45)	0.0248	0.714 (1.40)	3.3737	0.111 (9.00)	2.5171	
	DOWN	122.7	6.16	1.818 (0.55)	0.0283	1.000 (1.00)	3.3316	0.714 (1.40)	0.6501	
				5.000 (0.20)	0.0254	1.538 (0.65)	2.7852	0.625 (1.60)	0.6476	
				1.000 (1.00)	0.0212	0.111 (9.00)	2.4557	1.000 (1.00)	0.5250	
				0.769 (1.30)	0.0142	1.818 (0.55)	2.3989	1.429 (0.70)	0.2736	

Record	Instrument Direction	Peak Acceleration cm/sec ²	Duration sec (Acc ≥ 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks	
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm
C51	N54°W	122.7	6.16	0.417 (2.40) 0.217 (4.60)	0.0027 0.0004	0.167 (6.00) 2.222 (0.45)	2.1147 2.0129		
C54	N52°W	147.1	5.52	2.222 (0.45) 4.000 (0.25) 1.667 (0.60) 1.000 (1.00) 0.200 (5.00) 0.0030	0.0564 0.0460 0.0477 0.0357 0.0030	0.909 (1.10) 0.625 (1.60) 1.538 (0.65) 4.1245 3.6036 2.222 (0.45) 3.5971	5.8706 5.6074 4.1245 4.5297 3.6036 2.222 (0.45) 3.5971	0.556 (1.80) 0.909 (1.10) 1.538 (0.65) 0.4137 0.2830 2.222 (0.45) 0.111 (9.00) 3.7455	1.0586 0.9143 0.4137 0.2830 3.7455
	S38°W			117.0	9.92	4.000 (0.25) 2.000 (0.50) 1.333 (0.75) 1.111 (0.90) 0.833 (1.20) 0.313 (3.20)	0.0470 0.0298 0.0247 0.0232 0.0171 0.0119	0.208 (4.80) 0.556 (1.80) 1.111 (0.90) 1.429 (0.70) 0.833 (1.20) 1.818 (0.55) 2.222 (0.45) 3.333 (0.30)	6.4462 2.8202 2.8029 2.7608 2.5963 2.3263 2.1948 1.8884
D56	N21°E	309.4	13.78	2.857 (0.35) 6.667 (0.15) 2.222 (0.45) 1.250 (0.80) 0.111 (9.00)	0.1127 0.1042 0.0796 0.0317 0.0010	2.000 (0.50) 2.857 (0.35) 1.000 (1.00) 1.250 (0.80) 0.556 (1.80)	6.3364 6.0272 5.6499 4.8263 3.0971	0.111 (9.00) 0.208 (4.80) 0.357 (2.80) 0.833 (1.20) 2.000 (5.00) 2.857 (0.35) 0.111 (9.00) 0.385 (2.60) 1.000 (1.00) 0.769 (1.30)	2.0883 0.7233 0.6709 0.6371 0.4798 0.3396 2.7315 1.1432 1.1415 1.1247
	N69°W			265.4	17.24	5.000 (0.20) 2.500 (0.40) 2.000 (0.50) 1.250 (0.80) 0.111 (9.00)	0.0811 0.0794 0.0763 0.0598 0.0015	1.000 (1.00) 1.667 (0.60) 0.357 (2.80) 4.000 (0.25) 4.000 (0.25)	3.0942 7.8559 6.0484 5.2922 2.4433
D57	DOWN	153.3	7.42	5.000 (0.20) 2.000 (0.50) 0.833 (1.20) 0.111 (9.00)	0.0743 0.0242 0.0049 0.0006	4.000 (0.25) 2.222 (0.45) 0.476 (2.10) 0.111 (9.00)	2.7895 1.9117 1.6684 1.4747	0.111 (9.00) 1.818 (0.55) 1.111 (0.90) 3.333 (0.30)	1.2382 0.1604 0.1566 0.1072
	S00°W			103.8	9.70	4.000 (0.25) 1.818 (0.55) 2.222 (0.45) 1.429 (0.70) 1.111 (0.90) 0.769 (1.30) 0.500 (2.00) 4.000 (0.25) 2.857 (0.35) 1.250 (0.80) 0.294 (3.40)	0.0351 0.0317 0.0298 0.0191 0.0158 0.0078 0.0071 0.0532 0.0459 0.0292 0.0282 0.0084	0.227 (4.40) 1.818 (0.55) 1.000 (1.00) 2.417 (2.40) 1.429 (0.70) 0.625 (1.60) 2.857 (0.35) 0.714 (1.40) 0.227 (4.40) 1.111 (0.90) 2.500 (0.40) 1.667 (0.60)	4.1332 2.7966 2.6307 2.5367 2.3430 1.7759 1.5770 5.8458 4.5297 3.7515 2.7782 2.0579
D58	N90°E	148.2	7.74	4.000 (0.25) 1.818 (0.55) 2.222 (0.45) 1.429 (0.70) 1.111 (0.90) 0.556 (1.80) 0.263 (3.80) 4.000 (0.25) 2.857 (0.35) 1.818 (0.55) 1.250 (0.80) 0.769 (1.30) 0.313 (3.20)	0.0492 0.0316 0.0310 0.0192 0.0165 0.0048 0.0039 0.0741 0.0549 0.0319 0.0302 0.0287 0.0092	1.818 (0.55) 0.200 (5.00) 1.000 (1.00) 1.429 (0.70) 0.111 (9.00) 0.625 (1.60) 3.333 (0.30) 0.714 (1.40) 0.227 (4.40) 0.278 (3.60) 1.111 (0.90) 2.500 (0.40) 1.667 (0.60) 4.000 (0.25)	2.9036 2.8208 2.7560 2.4014 2.1716 1.9507 1.8200 5.8730 4.6407 4.5556 3.8357 3.1076 3.0672 2.5374	0.167 (6.00) 1.000 (1.00) 0.556 (1.80) 1.818 (0.55) 1.429 (0.70)	2.2180 0.3879 0.3819 0.2362 0.2328
	S00°W			167.3	5.98	4.000 (0.25) 1.818 (0.55) 2.222 (0.45) 1.429 (0.70) 1.111 (0.90) 0.556 (1.80) 0.263 (3.80) 4.000 (0.25) 2.857 (0.35) 1.818 (0.55) 1.250 (0.80) 0.769 (1.30) 0.313 (3.20)	0.0492 0.0316 0.0310 0.0192 0.0165 0.0048 0.0039 0.0741 0.0549 0.0319 0.0302 0.0287 0.0092	1.818 (0.55) 0.200 (5.00) 1.000 (1.00) 1.429 (0.70) 0.111 (9.00) 0.625 (1.60) 3.333 (0.30) 0.714 (1.40) 0.227 (4.40) 0.278 (3.60) 1.111 (0.90) 2.500 (0.40) 1.667 (0.60) 4.000 (0.25)	2.9036 2.8208 2.7560 2.4014 2.1716 1.9507 1.8200 5.8730 4.6407 4.5556 3.8357 3.1076 3.0672 2.5374
D59	UP	87.0	6.00	2.857 (0.35) 1.429 (0.70) 0.833 (1.20) 0.263 (3.80)	0.0116 0.0062 0.0058 0.0011	0.769 (1.30) 0.200 (5.00) 1.111 (0.90) 1.333 (0.75) 2.857 (0.35) 4.000 (0.25)	1.2574 0.8997 0.6880 0.6851 0.6348 0.5039	0.167 (6.00) 0.769 (1.30) 1.111 (0.90) 2.222 (0.45) 4.000 (0.25)	0.5568 0.2369 0.0877 0.0382 0.0190
	N46°W			133.8	6.14	6.667 (0.15) 3.333 (0.30) 2.500 (0.40) 1.667 (0.60) 1.000 (1.00) 0.769 (1.30) 0.625 (1.60) 0.357 (2.80) 0.143 (7.00) 6.667 (0.15) 2.500 (0.40) 1.667 (0.66) 1.250 (0.80) 0.667 (1.50) 0.400 (2.50)	0.0579 0.0274 0.0206 0.0152 0.0124 0.0075 0.0068 0.0025 0.0007 0.0529 0.0409 0.0201 0.0138 0.0113 0.0047	0.556 (1.80) 1.000 (1.00) 3.333 (0.30) 1.667 (0.60) 2.222 (0.45) 6.667 (0.15) 0.294 (3.40) 0.417 (2.40) 0.111 (9.00) 0.200 (5.00) 2.500 (0.40) 0.625 (1.60) 1.667 (0.60) 1.111 (0.90) 0.400 (2.50) 6.667 (0.15)	2.0821 1.9949 1.3927 1.3749 1.3564 1.3208 1.2323 1.1644 0.9939 3.8799 2.5781 2.5305 1.8458 1.7538 1.5764 1.1670
D62	N38°W	118.0	6.68	5.000 (0.20) 2.857 (0.35) 1.667 (0.60) 0.260 (3.80) 1.250 (0.80) 0.909 (1.10) 0.417 (2.40)	0.0381 0.0374 0.0260 0.0215 0.0195 0.0059	0.769 (1.30) 1.250 (0.80) 0.238 (4.20) 0.143 (7.00) 1.667 (0.60) 0.455 (2.20) 2.857 (0.35) 2.222 (0.45)	3.9336 2.8211 2.7591 2.6558 2.5317 2.0965 1.8479 1.6017	0.111 (9.00) 0.385 (2.60) 0.833 (1.20) 0.667 (1.50) 1.250 (0.80) 2.857 (0.35)	3.2981 0.8647 0.6842 0.6780 0.3389 0.1133
	S52°W			130.0	6.68	4.000 (0.25) 2.222 (0.45) 1.250 (0.80) 1.538 (0.65) 0.909 (1.10)	0.0395 0.0314 0.0291 0.0280 0.0253	0.833 (1.20) 1.250 (0.80) 1.667 (0.60) 0.111 (9.00)	5.1660 3.4784 2.8502 1.8870
D65	S00°W	146.7	5.78	3.333 (0.30) 5.000 (0.20) 1.667 (0.60) 2.222 (0.45) 0.385 (2.60)	0.0409 0.0333 0.0309 0.0302 0.0024	1.538 (0.65) 0.833 (1.20) 1.111 (0.90) 0.111 (9.00) 0.435 (2.30)	2.9725 2.8680 2.6408 1.9568 1.8413	0.111 (9.00) 0.833 (1.20) 1.538 (0.65)	2.1439 0.4737 0.3010

Record	Instrument Direction	Peak Acceleration cm/sec ²	Duration sec (Acc ≥ 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks	
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm
D65	S00°W	146.7	5.78	0.227 (4.40)	0.0020	0.167 (6.00)	1.7566		
				3.333 (0.30)		3.333 (0.30)	1.5861		
				0.833 (1.20)	0.0562	0.833 (1.20)	4.5119	0.111 (9.00)	1.8733
				1.538 (0.65)	0.0296	1.538 (0.65)	2.9938	0.769 (1.30)	0.8754
				0.400 (2.50)	0.0036	0.357 (2.80)	2.7432	0.385 (2.60)	0.7596
				0.200 (5.00)	0.0016	2.222 (0.45)	2.4920	1.538 (0.65)	0.3085
	DOWN	73.1	2.56	3.333 (0.30)	0.0320	3.333 (0.30)	1.5514	0.143 (7.00)	0.5638
				5.000 (0.20)	0.0284	0.714 (1.40)	1.4381	0.400 (2.50)	0.2633
				1.538 (0.65)	0.0077	2.500 (0.40)	1.3829	0.714 (1.40)	0.2455
				0.833 (1.20)	0.0061	0.227 (4.40)	0.9837	0.625 (1.60)	0.2409
						1.538 (0.65)	0.9182	0.833 (1.20)	0.2156
						0.385 (2.60)	0.8722	2.500 (0.40)	0.0759
D68	N00°E	81.2	3.60	3.333 (0.30)	0.0268	1.818 (0.55)	2.4840	0.125 (8.00)	1.7037
				1.818 (0.55)	0.0265	0.111 (9.00)	1.9309	0.667 (1.50)	0.2589
				5.000 (0.20)	0.0240	1.208 (4.80)	1.7378	1.111 (0.90)	0.2052
				1.250 (0.80)	0.0109	1.111 (0.90)	1.7006	1.818 (0.55)	0.1975
				0.714 (1.40)	0.0050	0.667 (1.50)	1.5766		
				0.278 (3.60)	0.0025	3.333 (0.30)	1.2400		
	N90°E	98.0	3.84	2.857 (0.35)	0.0303	2.500 (0.40)	1.2394		
				6.667 (0.15)	0.0211	0.714 (1.40)	3.5462	0.143 (7.00)	1.2205
				0.769 (1.30)	0.0167	0.400 (2.50)	1.8389	0.667 (1.50)	0.7658
				0.455 (2.20)	0.0044	2.222 (0.45)	1.8074	0.385 (2.60)	0.6249
				0.217 (4.60)	0.0016	1.667 (0.60)	1.4359	2.222 (0.45)	0.1237
						0.182 (5.50)	1.3650	1.667 (0.60)	0.1219
E72	N75°W	82.2	7.76	1.818 (0.55)	0.0251	0.167 (6.00)	5.7712	0.167 (6.00)	5.4092
				4.000 (0.25)	0.0206	0.714 (1.40)	3.5285	0.476 (2.10)	0.8033
				1.333 (0.75)	0.0200	0.313 (3.20)	3.2023	0.714 (1.40)	0.7231
				2.500 (0.40)	0.0192	1.333 (0.75)	2.4794	1.333 (0.75)	0.2782
				0.769 (1.30)	0.0158	1.818 (0.55)	2.2347	1.818 (0.55)	0.1885
				0.500 (2.00)	0.0077	0.476 (2.10)	2.2271		
	N15°E	115.0	5.50	0.200 (5.00)	0.0071	4.000 (0.25)	0.6960	0.111 (9.00)	2.4728
				6.667 (0.15)	0.0343	1.111 (0.90)	3.1892	0.357 (2.80)	0.8239
				4.000 (0.25)	0.0296	1.429 (0.70)	2.7002	0.667 (1.50)	0.4827
				2.857 (0.35)	0.0288	0.111 (9.00)	2.5144	1.000 (1.00)	0.4771
				2.222 (0.45)	0.0277	1.818 (0.55)	2.2885	1.429 (0.70)	0.2972
				1.818 (0.55)	0.0275	0.357 (2.80)	2.2884	1.818 (0.55)	0.2063
DOWN	64.80	1.70	1.538 (0.65)	0.0255	0.667 (1.50)	2.2383	2.222 (0.45)	0.1378	
			1.111 (0.90)	0.0208	0.167 (6.00)	2.0739			
			0.714 (1.40)	0.0092	2.222 (0.45)	1.8667			
			0.400 (2.50)	0.0047	2.857 (0.35)	1.5726			
			0.208 (4.80)	0.0023	4.000 (0.25)	0.9458			
			6.667 (0.15)	0.0203	0.333 (1.20)	1.1637	0.111 (9.00)	0.4938	
E75	N00°E	133.8	5.10	3.333 (0.30)	0.0445	1.111 (0.90)	4.3913	0.111 (9.00)	2.3057
				5.000 (0.20)	0.0355	0.667 (1.50)	3.8797	0.667 (1.50)	0.7477
				1.538 (0.65)	0.0318	0.833 (1.20)	3.5488	1.000 (1.00)	0.6980
				1.111 (0.90)	0.0287	1.538 (0.65)	3.4484	0.357 (2.80)	0.4554
				0.714 (1.40)	0.0151	0.111 (9.00)	2.7831	1.429 (0.70)	0.3760
				0.400 (2.50)	0.0026	0.238 (4.20)	2.3222		
	S90°W	111.8	10.44	3.333 (0.30)	0.0379	0.167 (6.00)	5.3101	0.143 (7.00)	5.1677
				1.818 (0.55)	0.0287	0.769 (1.30)	3.8790	0.385 (2.60)	1.3045
				2.500 (0.40)	0.0285	0.400 (2.50)	3.0146	0.833 (1.20)	0.7887
				6.667 (0.15)	0.0265	1.111 (0.90)	2.5212	0.556 (1.80)	0.6776
				0.833 (1.20)	0.0222	1.818 (0.55)	2.4206	1.818 (0.55)	0.2160
				1.250 (0.80)	0.0168	0.556 (1.80)	2.4140	1.538 (0.65)	0.2155
E78	N50°W	126.5	5.26	2.857 (0.35)	0.0392	0.714 (1.40)	5.3855	0.111 (9.00)	3.8416
				2.222 (0.45)	0.0372	0.111 (9.00)	3.7710	0.714 (1.40)	1.0375
				6.667 (0.15)	0.0338	1.538 (0.65)	2.9259	1.111 (0.90)	0.5617
				1.538 (0.65)	0.0316	0.217 (4.60)	2.2521	1.429 (0.70)	0.3501
				1.111 (0.90)	0.0282	2.222 (0.45)	2.0782		
				0.769 (1.30)	0.0238				
S40°W	169.2	5.68	3.333 (0.30)	0.0456	0.769 (1.30)	4.2831	0.667 (1.50)	0.8919	
			1.333 (0.75)	0.0347	0.625 (1.60)	4.2445	0.455 (2.20)	0.8486	
			0.833 (1.20)	0.0314	1.250 (0.80)	4.0167	0.833 (1.20)	0.7554	
			0.714 (1.40)	0.0180	0.385 (2.60)	2.9433	1.250 (0.80)	0.5373	
					0.143 (7.00)	2.2506	0.111 (9.00)	0.5055	
					2.500 (0.40)	2.2049	0.182 (5.50)	0.3936	
E81	S08°E	213.0	8.48	3.333 (0.30)	0.0300	1.000 (1.00)	3.0965	0.111 (9.00)	1.2555
				1.000 (1.00)	0.0195	0.263 (3.80)	2.2617	0.227 (4.40)	0.9368
				1.667 (0.60)	0.0165	0.769 (1.30)	2.1160	0.294 (3.40)	0.6782
				0.427 (2.40)	0.0036	6.667 (0.15)	2.0498	1.000 (1.00)	0.4779
				0.250 (4.00)	0.0021	0.556 (1.80)	2.0283	0.500 (2.00)	0.4275
				0.111 (9.00)	0.0007	2.000 (0.50)	1.7458	0.769 (1.30)	0.3989
S82°W	198.3	3.48	1.818 (0.55)	0.0188	1.667 (0.60)	1.6370	2.000 (0.50)	0.1303	
					2.500 (0.40)	1.5866	6.667 (0.15)	0.0456	
					0.435 (2.30)	1.4884			
					0.111 (9.00)	1.4266			
					1.429 (0.70)	1.6748	1.429 (0.70)	1.6748	

Record	Instrument Direction	Peak Acceleration cm/sec ²	Duration sec (Acc ≥ 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks	
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm
E81	S80°W	198.3	3.48	0.625 (1.60) 0.250 (4.00)	0.0034 0.0013	1.818 (0.55) 6.667 (0.15) 0.167 (6.00) 2.857 (0.35)	1.5700 1.4836 1.0169 1.0168	1.818 (0.55) 6.667 (0.15) 0.167 (6.00) 2.857 (0.35)	1.5700 1.4836 1.0169 1.0168
	DOWN	63.7	0.76	3.333 (0.30) 1.667 (0.60)	0.0146 0.0079	1.429 (0.70) 0.833 (1.20) 1.818 (0.55) 2.857 (0.35) 0.111 (9.00)	0.9378 0.8722 0.8203 0.7884 0.4733	1.000 (1.00) 0.111 (9.00) 0.625 (1.60) 0.833 (1.20) 2.857 (0.35)	0.1117 0.1108 0.1102 0.1088 0.0433
E83	S00°W	158.2	12.32	3.333 (0.30) 5.000 (0.20) 1.538 (0.65) 1.111 (0.90) 0.769 (1.30) 0.500 (2.00)	0.0569 0.0430 0.0319 0.0292 0.0158 0.0090	1.111 (0.90) 1.538 (0.65) 0.833 (1.20) 1.818 (0.55) 0.625 (1.60) 2.857 (0.35)	4.3900 3.5589 3.2173 3.1926 3.0918 2.7971	0.167 (6.00) 0.278 (3.60) 0.111 (9.00) 0.476 (2.10) 0.769 (1.30) 1.000 (1.00)	2.3226 2.0788 2.0238 0.9505 0.6594 0.6481
	N90°E	161.9	12.60	3.333 (0.30) 6.667 (0.15) 3.333 (0.30) 1.538 (0.65) 2.222 (0.45) 0.909 (1.10) 1.250 (0.80) 0.417 (2.40)	0.0719 0.0338 0.0338 0.0272 0.0207 0.0205 0.0177 0.0093	0.200 (5.00) 0.167 (6.00) 0.833 (1.20) 0.833 (1.20) 0.400 (2.50) 1.538 (0.65) 3.333 (0.30) 6.667 (0.15)	4.3715 4.2734 3.8759 3.5254 2.7621 1.8081 1.5268	0.208 (4.80) 0.125 (8.00) 0.400 (2.50) 0.769 (1.30) 0.625 (1.60) 1.429 (0.70) 0.111 (9.00)	3.1020 2.9143 1.4022 0.7121 0.5453 0.2884 0.0399
E86	DOWN	55.5	0.02	3.333 (0.30) 2.000 (0.50) 1.429 (0.70) 1.250 (0.80) 0.455 (2.20)	0.0170 0.0079 0.0043 0.0040 0.0009	2.000 (0.50) 1.250 (0.80) 0.833 (1.20) 0.143 (7.00) 0.500 (2.00)	0.7967 0.7087 0.3769 0.3241 0.3860	0.111 (9.00) 0.556 (1.80) 1.111 (9.00) 2.000 (0.50) 3.333 (0.30)	0.6808 0.0969 0.0762 0.0492 0.0377
	N83°W	104.6	5.52	2.222 (0.45) 4.000 (0.25) 1.000 (1.00) 1.818 (0.55) 1.429 (0.70) 0.417 (2.40)	0.0315 0.0281 0.0226 0.0215 0.0196 0.0045	1.000 (1.00) 0.833 (1.20) 1.429 (0.70) 1.667 (0.60) 0.111 (9.00) 2.222 (0.45)	3.4465 3.2903 2.1565 2.0395 2.0154 1.8577	0.111 (9.00) 0.385 (2.600) 0.769 (1.300) 0.500 (2.00) 1.000 (1.00) 1.429 (0.70)	2.6166 0.7128 0.6206 0.5948 0.5573 0.2369
E88	S07°W	80.5	7.72	4.000 (0.25) 2.857 (0.35) 1.250 (0.80) 1.429 (0.70) 0.833 (1.20)	0.0252 0.0248 0.0156 0.0136 0.0060	0.227 (4.40) 1.250 (0.80) 2.222 (0.45) 0.111 (9.00) 1.000 (1.00)	1.8762 1.7901 1.5209 1.4890 1.4385	0.111 (9.00) 0.500 (2.00) 1.250 (0.80) 1.000 (1.00) 2.222 (0.45)	1.6017 0.3384 0.2459 0.2096 0.1063
	S70°E	265.7	8.02	1.667 (0.60) 1.250 (0.80) 2.222 (0.45) 3.333 (0.30) 5.000 (0.20)	0.1098 0.1071 0.0901 0.0684 0.0598	1.000 (1.00) 1.667 (0.60) 0.625 (1.60) 0.111 (9.00) 5.000 (0.20)	15.0470 9.4654 8.5561 5.3867 1.8072	0.125 (8.00) 1.000 (1.00) 0.500 (2.00) 0.294 (3.40) 1.8072	2.9696 2.4144 1.7587 1.6820
E88	S20°W	209.1	10.20	5.000 (0.20) 2.500 (0.40) 1.000 (1.00) 1.333 (0.75)	0.1004 0.0757 0.0606 0.0535	1.000 (1.00) 0.714 (1.40) 0.625 (1.00) 1.333 (0.75)	10.0056 9.7703 9.2055 6.7316	0.667 (1.50) 0.500 (2.00) 0.909 (1.10) 0.333 (3.00)	2.0460 1.8049 1.7643 1.5080
	DOWN	131.5	9.62	1.250 (0.80) 1.667 (0.60) 4.000 (0.25) 2.222 (0.45) 0.385 (2.60) 0.263 (3.80)	0.0553 0.0454 0.0406 0.0395 0.0056 0.0032	1.111 (0.90) 1.667 (0.60) 0.278 (3.60) 2.222 (0.45) 0.111 (9.00)	7.3479 4.0944 3.3603 2.3875 2.3644	0.111 (9.00) 0.217 (4.60) 0.111 (9.00) 0.333 (3.00) 0.667 (1.50) 2.222 (0.45)	0.0997 1.3876 1.2879 1.0606 1.0373 0.7372 0.1966
E89	S53°E	131.9	6.52	2.222 (0.45) 2.857 (0.35) 5.000 (0.20) 1.000 (1.00) 1.250 (0.80) 0.400 (2.50)	0.0409 0.0385 0.0378 0.0329 0.0321 0.0317	1.000 (1.00) 0.625 (1.60) 0.167 (6.00) 1.538 (0.65) 1.818 (0.55) 2.857 (0.35)	5.1903 4.3444 3.2656 2.9652 2.9452 1.7871	0.125 (8.00) 0.667 (1.50) 1.000 (1.00) 0.556 (1.80) 1.538 (0.65) 1.818 (0.55)	3.3291 0.8601 0.8136 0.7983 0.3315 0.2478
	S37°W	139.0	9.76	0.400 (2.50) 6.667 (0.15) 2.857 (0.35) 1.333 (0.75) 1.818 (0.55) 0.909 (1.10) 0.313 (3.20) 0.556 (1.80) 3.333 (0.30)	0.0049 0.0342 0.0342 0.0218 0.0175 0.0170 0.0091 0.0086 0.0278	4.000 (0.25) 0.208 (4.80) 0.833 (1.20) 1.250 (0.80) 0.556 (1.80) 1.818 (0.55) 2.500 (0.40) 5.000 (0.20) 0.208 (4.80)	1.3446 4.6380 2.9957 4.3024 2.8503 2.6463 7.3479 4.0944 3.3603	0.182 (5.50) 0.833 (1.20) 1.333 (0.75) 2.500 (0.40) 2.000 (0.50) 0.111 (9.00) 0.217 (4.60) 0.111 (9.00) 0.333 (3.00)	3.4546 0.5607 0.3043 0.0877
E92	DOWN	75.3	2.96	0.909 (1.10) 0.313 (3.20) 0.556 (1.80) 3.333 (0.30) 6.667 (0.15) 0.833 (1.20) 1.429 (0.70) 0.556 (1.80) 0.250 (4.00)	0.0091 0.0086 0.0086 0.0278 0.0175 0.0096 0.0078 0.0037 0.0027	2.500 (0.40) 5.000 (0.20) 0.208 (4.80) 0.833 (1.20) 1.5768 1.2990 2.3894 1.0023 1.429 (0.70) 2.222 (0.45)	1.4597 1.2720 0.8085 1.8985 1.5768 0.833 (1.20) 1.2990 1.429 (0.70) 1.0023 0.9190	0.182 (5.50) 0.435 (2.30) 0.833 (1.20) 1.429 (0.70) 0.385 (2.6) 0.6607 0.111 (9.00) 0.238 (4.20) 0.667 (1.50) 0.385 (2.60) 1.333 (0.75)	1.3820 0.3512 0.3399 0.0945 0.0618 0.0617 0.0612
	S28°W	79.1	3.66	2.857 (0.35) 4.000 (0.25) 6.667 (0.15) 1.538 (0.65) 0.833 (1.20) 0.167 (6.00)	0.0330 0.0291 0.0238 0.0216 0.0143 0.0008	0.714 (1.40) 1.250 (0.80) 1.429 (0.70) 0.455 (2.20) 2.500 (0.40) 0.294 (3.40) 0.200 (5.00) 0.111 (9.00)	3.3031 2.3571 2.3380 1.9759 1.7925 1.5366 1.3768 1.3707	0.111 (9.00) 0.238 (4.20) 0.667 (1.50) 0.385 (2.60) 1.333 (0.75)	1.2467 0.6005 0.5938 0.4828 0.2787
E95	S88°E	96.2	4.70	3.333 (0.30)	0.0235	0.769 (1.30)	3.4604	0.167 (6.00)	1.0585

Record	Instrument Direction	Peak Acceleration cm/sec	Duration sec (Acc \geq 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks	
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm
P217	S00°W	108.0	5.32	2.222 (0.45)	0.0327	1.000 (1.00)	3.6584	0.111 (9.00)	2.1188
				3.333 (0.30)	0.0310	0.695 (1.60)	2.9120	1.000 (1.00)	0.6033
				1.111 (0.90)	0.0248	0.769 (1.30)	2.7003	0.714 (1.40)	0.6008
				1.538 (0.65)	0.0241	1.538 (0.65)	2.4968	0.455 (2.20)	0.4682
				5.000 (0.20)	0.0238	2.000 (0.50)	2.1919	1.538 (0.65)	0.2505
				0.769 (1.30)	0.0135	0.182 (5.50)	2.1811		
				0.278 (3.60)	0.0038	0.227 (4.40)	2.0950		
						0.357 (2.80)	1.9261		
						0.833 (1.20)	3.9686	0.111 (9.00)	1.9176
						0.435 (2.30)	1.9951	0.769 (1.30)	0.7128
	N90°E	88.1	5.32	6.667 (0.15)	0.0219	0.435 (2.30)	0.7622	0.769 (1.30)	0.6338
				0.833 (1.20)	0.0195	1.429 (0.70)	1.7070	0.417 (2.40)	0.6333
				0.833 (1.20)	0.0184	0.425 (8.00)	1.6425	0.455 (2.20)	0.6333
				2.500 (0.50)	0.0166	2.500 (0.40)	1.0441	1.429 (0.70)	0.1734
				1.429 (0.70)	0.0143	3.333 (0.30)	0.9579	2.500 (0.40)	0.0725
				1.111 (0.90)	0.0135				
				0.182 (5.50)	0.0014				
				5.000 (0.20)	0.0136	0.217 (4.60)	1.0924	0.111 (9.00)	0.9775
				3.333 (0.30)	0.0120	1.000 (1.00)	0.8164	0.200 (5.00)	0.8059
				1.818 (0.55)	0.0100	1.818 (0.55)	0.7622	0.556 (1.80)	0.2264
	DOWN	60.1	3.00	1.429 (0.70)	0.0065	0.111 (9.00)	0.7363	1.000 (1.00)	0.1313
				1.250 (0.80)	0.0056	0.556 (1.80)	0.7327	1.429 (0.70)	0.0789
				1.000 (1.00)	0.0053	0.833 (1.20)	0.6624	1.818 (0.55)	0.0751
				0.556 (1.80)	0.0028	3.333 (0.30)	0.6629	2.500 (0.40)	0.0346
				0.263 (3.80)	0.0018	1.250 (0.80)	0.6056		
				0.385 (2.60)	0.0016	2.500 (0.40)	0.5296		
P221	N03°E	137.0	10.88	5.000 (0.20)	0.0734	5.000 (0.20)	2.1518	0.143 (7.00)	1.7606
				1.667 (0.60)	0.0099	0.143 (7.00)	1.9427	0.294 (3.40)	0.5315
				1.333 (0.75)	0.0092	1.333 (0.75)	1.4473	0.500 (2.00)	0.2151
				0.833 (1.20)	0.0040	0.625 (1.60)	1.0530	0.769 (1.30)	0.1523
				0.625 (1.60)	0.0030	0.476 (2.10)	0.9494	1.250 (0.80)	0.1276
	N87°W	165.0	5.80	0.417 (2.40)	0.0020			2.857 (0.35)	0.0868
				0.313 (3.20)	0.0020				
				0.167 (6.00)	0.0018				
				0.217 (4.60)	0.0013				
				0.313 (3.20)	0.0016	0.111 (9.00)	2.3241	0.111 (9.00)	2.2582
	N55°E	69.7	0.42	6.667 (0.15)	0.0219	5.000 (0.20)	2.2116	0.556 (1.80)	0.2894
				1.818 (0.55)	0.0163	2.500 (0.40)	1.7852	2.500 (0.40)	0.1571
				0.217 (4.60)	0.0019	1.538 (0.65)	1.5590	1.538 (0.65)	0.1285
				0.313 (3.20)	0.0016	0.667 (1.50)	1.4997	2.857 (0.35)	0.0882
						0.909 (1.10)	1.4211	5.000 (0.20)	0.0691
N35°W	53.2	0.02	5.000 (0.20)	0.0294	1.333 (0.75)	2.1436	0.143 (7.00)	0.3701	
			2.500 (0.40)	0.0222	1.538 (0.65)	2.0641	1.333 (0.75)	0.2313	
			1.429 (0.70)	0.0179	2.500 (0.40)	1.3918	2.222 (0.45)	0.1001	
					0.263 (3.80)	0.9572			
					0.111 (9.00)	0.9481			
Q233	S12°W	243.0	17.48	6.667 (0.15)	0.0277	5.000 (0.20)	0.8826	0.111 (9.00)	0.5410
				2.222 (0.45)	0.0190	0.556 (1.80)	0.8024	0.200 (5.00)	0.3626
				3.333 (0.30)	0.0149	1.250 (0.80)	1.4749	1.250 (0.80)	0.1631
				1.429 (0.70)	0.0119	0.294 (3.40)	1.1890	1.250 (0.80)	0.1631
				0.263 (3.80)	0.0069	0.476 (2.10)	0.8154	0.833 (1.20)	0.1387
	N78°W	197.0	15.12	5.000 (0.20)	0.0646	5.000 (0.20)	0.7650	1.818 (0.55)	0.1114
				2.500 (0.40)	0.0385	0.476 (2.10)	0.7650	0.476 (2.10)	0.1009
				2.000 (0.50)	0.0358	2.500 (0.40)	4.9557	2.500 (0.40)	0.2950
				1.250 (0.80)	0.0189	3.333 (0.30)	4.8358	1.429 (0.70)	0.3845
				0.625 (1.60)	0.0149	0.556 (1.80)	4.5836	2.500 (0.40)	0.2950
	UP	96.0	7.54	0.417 (2.40)	0.0149	1.250 (0.80)	0.9474		
				0.714 (1.40)	0.0131	0.714 (1.40)	3.5905		
				1.000 (1.00)	0.0124	2.000 (0.50)	3.4946		
						1.250 (0.80)	3.0606		
						0.357 (2.80)	6.0685	0.167 (6.00)	3.8220
Q236	SOUTH	167.0	9.50	5.000 (0.20)	0.0518	0.769 (1.30)	3.5009	0.182 (5.50)	1.8830
				2.500 (0.40)	0.0477	0.667 (1.50)	3.1927	0.714 (1.40)	0.7046
				1.818 (0.55)	0.0217	2.500 (0.40)	2.9574	1.429 (0.70)	0.2060
				1.429 (0.70)	0.0171	0.263 (3.80)	2.5719	2.222 (0.45)	0.2042
				1.111 (0.90)	0.0166	0.313 (3.20)	2.5381	1.818 (0.55)	0.1616
	EAST	122.0	5.20	0.769 (1.30)	0.0164	0.476 (2.10)	2.4849	5.000 (0.20)	0.0509
				0.417 (2.40)	0.0055	1.111 (0.90)	2.4838		
				0.263 (3.80)	0.0044	2.208 (4.80)	2.4803		
						1.818 (0.55)	2.0961		
						1.429 (0.70)	1.9431		
			5.000 (0.20)	1.5548					
			0.208 (4.80)	2.1313	0.167 (6.00)	1.6206			
			0.143 (7.00)	1.8171	0.500 (2.00)	0.2977			
			4.000 (0.25)	1.5661	0.714 (1.40)	0.2288			
			1.000 (1.00)	1.2703	1.000 (1.00)	0.1667			

Record	Instrument Direction	Peak Acceleration cm/sec ²	Duration sec (Acc ≥ 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks		
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm	
S258	N29°E	56.3	4.02	0.500 (2.00)	0.0047	0.400 (2.50)	1.2414			
				0.435 (2.30)	0.0041	2.857 (0.35)	1.1791			
						0.625 (1.60)	1.1213			
						0.714 (1.40)	4.4738	0.143 (7.00)	2.2802	
						0.909 (1.10)	3.9852	0.714 (1.40)	1.0340	
	S61°E	83.3	2.48	0.222 (0.45)	0.0218	0.909 (1.10)	2.7929	0.263 (3.80)	0.8411	
				0.714 (1.40)	0.0214	0.111 (9.00)	2.5775	0.417 (2.40)	0.6221	
				1.429 (0.70)	0.0206	0.435 (2.30)	2.0140	1.429 (0.70)	0.2496	
				1.818 (0.55)	0.0194	0.182 (5.50)	1.8499	2.222 (0.45)	0.1094	
				5.000 (0.20)	0.0172	1.538 (0.65)	1.1437			
	UP	54.5	0.00	3.333 (0.30)	0.0393	2.000 (2.50)	1.0523	0.227 (4.40)	0.6166	
				2.000 (0.50)	0.0229	0.250 (4.00)	0.9912	0.111 (9.00)	0.4287	
				1.111 (0.90)	0.0041	2.857 (0.35)	0.9136	0.500 (2.00)	0.2064	
				0.714 (1.40)	0.0205	1.538 (0.65)	0.6597	0.625 (1.60)	0.1407	
				0.500 (2.00)	0.0021	0.714 (1.40)	0.6438	1.111 (0.90)	0.0814	
S261	N59°E	97.7	6.82	2.857 (0.35)	0.0360	0.227 (4.40)	4.0151	0.167 (6.00)	3.0926	
				5.000 (0.20)	0.0278	0.769 (1.30)	3.2081	0.667 (1.50)	0.7548	
				2.000 (0.50)	0.0208	0.667 (1.50)	3.1500	1.111 (0.90)	0.3275	
				1.667 (0.60)	0.0183	0.143 (7.00)	3.1304	1.538 (0.65)	0.1680	
				1.111 (0.90)	0.0164	1.111 (0.90)	2.3653	2.857 (0.35)	0.1091	
	N31°W	107.0	4.78	0.769 (1.30)	0.0141	2.857 (0.35)	1.8047			
				0.263 (3.80)	0.0058	1.538 (0.65)	1.6289			
				0.357 (2.80)	0.0051	2.000 (0.50)	1.3861			
						1.333 (0.75)	1.3855			
						5.000 (0.20)	0.8686			
	UP	64.0	4.50	2.857 (0.35)	0.0314	1.667 (0.60)	1.6830	0.125 (8.00)	1.2976	
				5.000 (0.20)	0.0249	0.769 (1.30)	1.6719	0.500 (2.00)	0.3067	
				1.538 (0.65)	0.0174	2.857 (0.35)	1.6486	0.714 (1.40)	0.2975	
				0.909 (1.10)	0.0083	1.333 (0.75)	1.6091	1.250 (0.80)	0.2074	
				0.263 (3.80)	0.0022	0.208 (4.80)	1.5805	1.429 (0.70)	0.1873	
S262	N83°W	68.3	8.80	2.857 (0.35)	0.0260	0.208 (4.80)	8.2890	0.182 (5.50)	6.1968	
				1.000 (1.00)	0.0255	0.769 (1.30)	4.4405	0.500 (2.00)	1.4734	
				2.222 (0.45)	0.0232	0.556 (1.80)	4.3479	1.333 (0.75)	0.3113	
				5.000 (0.20)	0.0229	1.333 (0.75)	2.3224			
				1.429 (0.70)	0.0226	1.667 (0.60)	1.4978			
	S07°W	93.6	4.10	1.667 (0.60)	0.0218	0.556 (1.80)	1.3449			
				0.556 (1.80)	0.0175	0.476 (2.10)	0.5763			
				0.250 (4.00)	0.0134	0.125 (8.00)	0.5628			
				2.222 (0.45)	0.0376	0.200 (5.00)	6.9539	0.167 (6.00)	5.9747	
				1.538 (0.65)	0.0337	0.556 (1.80)	5.2556	0.556 (1.80)	1.5349	
	S265	SOUTH	104.0	6.08	0.625 (1.60)	0.0234	0.769 (1.30)	3.7463	2.222 (0.45)	0.1883
					0.833 (1.20)	0.0204	1.111 (0.90)	3.3630		
					0.313 (3.20)	0.0121	1.333 (0.75)	3.2762		
							2.222 (0.45)	2.5392		
							1.000 (1.00)	4.1607	0.167 (6.00)	3.3686
WEST		125.0	10.30	1.111 (0.90)	0.0206	0.667 (1.50)	3.8113	0.714 (1.40)	0.7600	
				2.000 (0.50)	0.0284	0.167 (6.00)	3.8112	1.000 (1.00)	0.7085	
				1.538 (0.65)	0.0244	0.769 (1.30)	3.7190	2.857 (0.35)	0.0862	
				0.769 (1.30)	0.0180	1.538 (0.65)	2.2894			
				0.227 (4.40)	0.0048	0.357 (2.80)	2.1839			
UP		53.7	0.00	2.857 (0.35)	0.0376	2.857 (0.35)	1.6391			
				2.000 (0.50)	0.0050	5.000 (0.20)	1.1317			
				1.000 (1.00)	0.0033	0.167 (6.00)	6.7475	0.167 (6.00)	6.1523	
				1.333 (0.75)	0.0022	0.769 (1.30)	3.8988	0.400 (2.50)	1.6490	
						0.909 (1.10)	3.7065	0.769 (1.30)	0.7422	
S266	NORTH	153.0	5.76	2.500 (0.40)	0.0192	1.538 (0.65)	1.7226	1.818 (1.50)	0.1393	
				0.417 (2.40)	0.0159	5.000 (0.20)	1.2417	4.000 (0.25)	0.0530	
				0.227 (4.40)	0.0082	2.500 (0.40)	1.1177			
				2.000 (0.50)	0.0050	0.714 (1.40)	0.6720	0.111 (9.00)	0.1396	
				1.000 (1.00)	0.0033	0.909 (1.10)	0.5824	0.167 (6.00)	0.1376	
	WEST	129.0	10.30	1.333 (0.75)	0.0022	2.000 (0.50)	0.4589	0.250 (4.00)	0.1351	
						5.000 (0.20)	0.3799	0.625 (1.60)	0.1268	
						0.385 (2.60)	0.3241	2.000 (0.50)	0.0308	
						1.538 (0.65)	0.3600	1.538 (0.65)	0.0293	
						0.200 (5.00)	0.3474	5.000 (0.20)	0.0126	
	S266	NORTH	153.0	5.76	3.333 (0.30)	0.0482	1.111 (0.900)	3.8563	0.167 (6.00)	1.7874
					2.500 (0.40)	0.0397	0.667 (1.50)	3.1389	0.714 (1.40)	0.6209
					6.667 (0.15)	0.0350	1.538 (0.65)	2.5398	1.000 (1.00)	0.5227
					1.111 (0.90)	0.0259	1.818 (0.55)	2.2678	1.429 (0.70)	0.2731
					1.538 (0.65)	0.0254	0.125 (8.00)	2.2668	2.500 (0.40)	0.1576
WEST		129.0	10.30	0.714 (1.40)	0.0128	2.500 (0.40)	2.2558			
				0.417 (2.40)	0.0031	0.182 (5.50)	2.1193			
				0.333 (3.00)	0.0030	0.385 (2.60)	2.0554			
				0.208 (4.80)	0.0025	0.455 (2.20)	2.0295			
				4.000 (0.25)	0.0415	0.167 (6.00)	4.6819	0.143 (7.00)	4.5660	
WEST		129.0	10.30	1.818 (0.55)	0.0344	0.909 (1.10)	4.2990	0.400 (2.50)	1.2791	
				2.500 (0.40)	0.0277	1.111 (0.90)	3.1670	0.833 (1.20)	0.7826	
				0.833 (1.20)	0.0220	0.400 (2.50)	2.9811	0.556 (1.80)	0.7209	
				1.111 (0.90)	0.0218	1.818 (0.55)	2.9382	1.111 (0.90)	0.4359	
				0.417 (2.40)	0.0085	0.556 (1.80)	2.5528	1.429 (0.70)	0.2813	
WEST	129.0	10.30	0.217 (4.60)	0.0060	2.222 (0.45)	1.9162				
					3.333 (0.30)	1.6797				

Record	Instrument Direction	Peak Acceleration cm/sec	Duration sec (Acc \geq 0.05 g)	Predominant Acceleration Peaks		Predominant Velocity Peaks		Predominant Displacement Peaks					
				Frequency (Period) Hz (sec)	Amplitude (g)	Frequency (Period) Hz (sec)	Amplitude cm/sec	Frequency (Period) Hz (sec)	Amplitude cm				
U309	N89°W	168.0	8.60	0.833 (1.20)	0.0170	2.857 (0.35)	1.5768	0.556 (1.80)	0.4478				
				0.556 (1.80)	0.0096	0.333 (3.00)	1.4624	0.278 (3.60)	0.4400				
				0.333 (3.00)	0.0016	0.111 (9.00)	1.2723	0.333 (3.00)	0.3439				
				0.294 (3.40)	0.0015	0.182 (5.50)	1.2165	1.333 (0.75)	0.2914				
				0.238 (4.20)	0.0010			2.222 (0.45)	0.1143				
	S01°W	74.9	0.56	3.333 (0.30)	0.0074	1.429 (0.70)	1.8998	0.111 (9.00)	0.7073				
				2.222 (0.45)	0.0183	2.000 (0.50)	1.3778	1.429 (0.70)	0.2078				
				1.429 (0.70)	0.0171	3.333 (0.30)	1.1967	0.313 (3.20)	0.1736				
				0.417 (2.40)	0.0010	0.667 (1.50)	0.8156	0.909 (1.10)	0.1709				
				0.200 (5.00)	0.0007	0.250 (4.00)	0.6739	0.395 (2.60)	0.1506				
						0.385 (2.60)	0.6593	0.625 (1.60)	0.1099				
						0.111 (9.00)	0.5948	2.857 (0.35)	0.0699				
						0.476 (2.10)	0.5879						
						0.167 (6.00)	0.5763						
				U312	N46°W	103.0	0.16	6.667 (0.15)	0.0257	1.333 (0.75)	2.2134	0.909 (1.10)	0.3403
								2.000 (0.50)	0.0247	0.909 (1.10)	2.0575	0.111 (9.00)	0.3281
								1.111 (0.90)	0.0151	1.111 (0.90)	2.0489	1.333 (0.75)	0.2713
								0.455 (2.20)	0.0019	0.357 (2.80)	1.3803	0.400 (2.50)	0.2615
										0.208 (4.80)	1.3710	0.625 (1.60)	0.2419
S44°W	232.0	0.70	6.667 (0.15)		0.0465	6.667 (0.15)	0.5225	0.250 (4.00)	0.2400				
			1.429 (0.70)		0.0190	1.250 (0.80)	2.5000	1.250 (0.80)	0.2369				
			1.250 (0.80)		0.0181	1.429 (0.70)	2.1212	0.111 (9.00)	0.2407				
			0.714 (1.40)		0.0045	4.000 (0.25)	1.3903	0.455 (2.20)	0.2354				
						2.500 (0.40)	1.3719	0.909 (1.10)	0.2342				
						0.217 (4.60)	1.2186	1.429 (0.70)	0.2316				
						0.714 (1.40)	1.1909	0.250 (4.00)	0.2265				
						0.111 (9.00)	1.1579	0.400 (2.50)	0.2206				
V321	N26°E	88.4	9.32	0.833 (1.20)	0.0387	0.833 (1.20)	7.1605	0.833 (1.20)	1.3794				
				4.000 (0.25)	0.0277	0.357 (2.80)	1.6927	0.385 (2.60)	0.4630				
				1.818 (0.55)	0.0123	0.417 (2.40)	1.6700	0.111 (9.00)	0.3962				
				0.400 (2.50)	0.0029	0.200 (5.00)	1.1402	0.182 (5.50)	0.3799				
				0.455 (2.20)	0.0028	2.857 (0.35)	1.1322	1.667 (0.60)	0.0943				
	N46°W	59.9	0.02	0.208 (4.80)	0.0006	0.125 (8.00)	1.1210	2.857 (0.35)	0.2192				
				4.000 (0.25)	0.0311	4.000 (0.25)	1.0393	0.111 (9.00)	0.1201				
				2.222 (0.45)	0.0079	2.500 (0.40)	0.6013	0.500 (2.00)	0.0895				
				0.833 (1.20)	0.0017	2.000 (0.50)	0.5979	4.000 (0.25)	0.0482				
						0.435 (2.30)	0.4586	1.818 (0.55)	0.0430				
						0.769 (1.30)	0.4457						
UP	96.4	1.80	5.000 (0.20)	0.0223	2.000 (0.50)	1.3025	0.111 (9.00)	0.1146					
			2.857 (0.35)	0.0168	4.000 (0.25)	1.2038	2.000 (0.50)	0.0994					
			2.000 (0.50)	0.0150	2.500 (0.40)	1.0409	0.182 (5.50)	0.0684					
			0.500 (2.00)	0.0006	0.625 (1.60)	0.4502	0.435 (2.30)	0.0628					
				4.000 (0.25)		0.0474							

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APPENDIX C: PERIODS AND FREQUENCIES OF THE RESPONSE SPECTRA

<u>Period</u> <u>sec</u>	<u>Frequency</u> <u>Hz</u>	<u>Period</u> <u>sec</u>	<u>Frequency</u> <u>Hz</u>
0.10	10.00	2.00	0.50
0.15	6.67	2.10	0.48
0.20	5.00	2.20	0.45
0.25	4.00	2.30	0.43
0.30	3.33	2.40	0.42
0.35	2.86	2.50	0.40
0.40	2.50	2.60	0.38
0.45	2.22	2.80	0.36
0.50	2.00	3.00	0.33
0.55	1.82	3.20	0.31
0.60	1.67	3.40	0.29
0.65	1.54	3.60	0.28
0.70	1.43	3.80	0.26
0.75	1.33	4.00	0.25
0.80	1.25	4.20	0.24
0.90	1.11	4.40	0.23
1.00	1.00	4.60	0.22
1.10	0.91	4.80	0.21
1.20	0.83	5.00	0.20
1.30	0.77	5.50	0.18
1.40	0.71	6.00	0.17
1.50	0.67	7.00	0.14
1.60	0.63	8.00	0.13
1.80	0.56	9.00	0.11

In accordance with letter from DAEN-RDC, DAEN-ASI dated 22 July 1977, Subject: Facsimile Catalog Cards for Laboratory Technical Publications, a facsimile catalog card in Library of Congress MARC format is reproduced below.

Chang, Frank K

State-of-the-art for assessing earthquake hazards in the United States; Report 8: Duration, spectral content, and predominant period of strong motion earthquake records from western United States / by Frank K. Chang, Ellis L. Krinitzsky. Vicksburg, Miss. : U. S. Waterways Experiment Station ; Springfield, Va. : available from National Technical Information Service, 1977.

58, c24 p. : ill. ; 27 cm. (Miscellaneous paper - U. S. Army Engineer Waterways Experiment Station ; S-73-1, Report 8)

Prepared for Office, Chief of Engineers, U. S. Army, Washington, D. C.

References: p. 56-58.

1. Earthquake engineering. 2. Earthquake hazards. 3. Earthquake resistant structures. 4. Earthquakes. 5. Ground motion. 6. State-of-the-art studies. I. United States. Army. Corps of Engineers. II. Krinitzsky, Ellis Louis, joint author. III. Series: United States. Waterways Experiment Station, Vicksburg, Miss. Miscellaneous paper ; S-73-1 Report 8.
TA7.W34m no.S-73-1 Report 8