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Determination of Charge or Polarization Distribution  
Across Polymer Electrets by the Thermal Pulse Method and Fourier Analysis •

by

10 A.S. DeReggi, C.M. Guttman, F.I. Mopsik  
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Abstract

Fourier analysis, applied to the recently introduced thermal pulse method, yields new and unique relations between the time-dependent, pyroelectric response of a thin specimen and the Fourier coefficients of the charge or polarization distribution across its thickness. The new analysis is applied illustratively to thermal pulse data for a vinylidene fluoride copolymer electret.

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Several new experimental methods have been proposed in recent Letters<sup>(1,2,3)</sup> to probe the spatial distribution of charge and/or polarization across the thickness of thin (thickness of order 10  $\mu\text{m}$ ) dielectric samples. These methods are currently of interest as means to study piezo- and pyroelectric polymers. The electron-beam method of Sessler et al.<sup>(1)</sup> has a resolution of  $\sim 1 \mu\text{m}$ , but is destructive in the sense that the measuring process irreversibly changes the quantities measured. Acoustical methods of generating a propagating pressure step<sup>(2)</sup> across a sample in order to measure its inhomogeneous piezoelectric response are non-destructive; but the step rise time requirements become severe if a resolution of 1  $\mu\text{m}$  is desired (a resolution of 1  $\mu\text{m}$  requires a step rise time of  $\leq 0.5 \text{ ns}$  assuming a sound velocity of 2000 m/s.) Thermal methods of producing transient inhomogeneous strain across a sample in order to measure its inhomogeneous pyroelectric response as, for example, in the Collins's thermal pulse method<sup>(3,4,5)</sup> are both non-destructive and comparatively easy to implement experimentally (thermal equilibration times are  $\sim 1 \text{ ms}$ ). However, because the thermal equilibration process is diffusive rather than propagative (wavelike), information contained in the experimental data about charge and/or polarization distributions is convoluted with a time-dependent temperature distribution and somehow must be deconvoluted. The major and often quoted<sup>(1,2,3,4,5)</sup> objection to the Collins thermal pulse method has been that the deconvolution procedure<sup>(3,4,5)</sup> yields non-unique charge and/or polarization distributions.

In this Letter, we show that the Collins' experiment yields the first few Fourier coefficients of the charge or polarization distribution, not the charge or polarization distribution itself as may be supposed from Collins' papers<sup>(1,2,3)</sup>. Further, we present expressions for the response which allow the Fourier coefficients to be determined from the experimental data by numerical or graphical analysis. We apply the new expressions to thermal pulse data for a copolymer of vinylidene fluoride with tetrafluoroethylene. This example illustrates both the power and the limitations of the thermal pulse method.

Consider, first, the temperature  $T(x,t)$  at time  $t$  across a sample regarded as a slab of infinite extent and of thickness  $d$  (see inset in Fig. 1) after a radiant heat pulse of duration  $t_p$  has been applied to the surface  $x=0$ . Assume that 1) the aluminum electrodes have negligible optical transmission and negligible thermal mass; 2) heat flows in the  $x$ -direction only; and 3) the sample does not lose heat to the surroundings. The initial temperature  $T(x,0)$  taken at the end of the thermal pulse is written

$$T(x,0) = T_1 + \Delta T(x,0) \quad (1)$$

where  $T_1$  is the uniform temperature of the sample prior to the pulse, and  $\Delta T(x,0)$  is the deviation from  $T_1$ . In practice,  $\Delta T(x,0)$  is a sharply localized function extending from  $x=0$  with a width  $\xi \ll d$ . The temperature at  $t > 0$  is  $T(x,t) = T_1 + \Delta T(x,t)$  where<sup>(6)</sup>

$$\Delta T(x,t) = a_0 + \sum_{n=1}^{\infty} a_n \cos(n\pi x/d) \exp(-n^2 t/\tau_1), \quad (2)$$

where  $\tau_1 = d^2/(\pi^2 k)$  where  $k$  is the thermal diffusivity, and where

$$a_0 = \frac{1}{d} \int_0^d \Delta T(x,0) dx = \lim_{t \rightarrow \infty} \Delta T(x,t) \quad (3)$$

and

$$a_n = \frac{2}{d} \int_0^d \Delta T(x,0) \cos(n\pi x/d) dx, \text{ for } n=1,2,\dots \quad (4)$$

In the limiting case where  $\Delta T(x,0) \rightarrow \delta(x)$  all  $a_n$ 's are

$$a_n = 2a_0, \text{ for } n=1,2,\dots \quad (5)$$

However, for a general  $\Delta T(x,0)$ , the temperature at the surfaces are described by

$$\Delta T(0,t) = a_0 + \sum_{n=1}^{\infty} a_n \exp(-n^2 t/\tau_1) \quad (6)$$

and

$$\Delta T(d,t) = a_0 + \sum_{n=1}^{\infty} (-1)^n a_n \exp(-n^2 t/\tau_1). \quad (7)$$

Expressions (6) and (7) have been used previously as the basis for thermal diffusivity measurements<sup>(7)</sup>. In the present case, the dimensionless quantities  $\Delta T(0,t)/a_0$  and  $\Delta T(d,t)/a_0$  can be obtained by measuring the transient resistance of one or both electrodes as done by Collins<sup>(4)</sup>. Then the  $a_n/a_0$ 's and  $\tau_1$  can be determined without knowing the detailed shape of the light pulse.

Consider, now, the inhomogeneous pyroelectric response. Assume that real charge of volume density  $\rho(x)$  and elementary dipoles responsible for polarization  $\vec{P}(x) = \hat{x} P(x)$  move reversibly when the sample thermally expands or contracts. Following Collins,<sup>(5)</sup> the open-circuit voltage due to charge,  $\Delta V_\rho$ , and that due to polarization,  $\Delta V_p$ , are

$$\Delta V_\rho(t) = \frac{\alpha_x - \alpha_\epsilon}{\epsilon \epsilon_0} \int_0^d \rho(x) \int_0^x \Delta T(x', t) dx' dx, \quad (8)$$

and

$$\Delta V_p(t) = \frac{\alpha_p + \alpha_x - \alpha_\epsilon}{\epsilon \epsilon_0} \int_0^d P(x) \Delta T(x, t) dx, \quad (9)$$

where  $\alpha_x$ ,  $\alpha_\epsilon$ , and  $\alpha_p$  are temperature coefficients  $(1/x)(dx/dT)$ ,  $(1/\epsilon)(d\epsilon/dT)$ , and  $(1/P)(dP/dT)$  respectively,  $\epsilon$  is the relative permittivity and  $\epsilon_0$  is the permittivity of vacuum. Substitution of (2) into the above equations gives

$$\Delta V_\rho(t) = \frac{\alpha_x - \alpha_\epsilon}{\epsilon \epsilon_0} [a_0 A_0 + \frac{d}{\pi} \sum_{n=1}^{\infty} \frac{a_n \cdot A_n}{n} \exp(-n^2 t / \tau_1)], \quad (10)$$

where

$$A_0 = \int_0^d x \rho(x) dx \quad (11)$$

$$A_n = \int_0^d \rho(x) \sin(n\pi x/d) dx, \quad \text{for } n=1, 2, \dots \quad (12)$$



and

$$\Delta V_p(t) = \frac{\alpha_p + \alpha_x - \alpha_\epsilon}{\epsilon \epsilon_0} [a_0 B_0 + \sum_{n=1}^{\infty} a_n \cdot B_n \exp(-n^2 t / \tau_1)], \quad (13)$$

where

$$B_0 = \int_0^d P(x) dx \quad (14)$$

and

$$B_n = \int_0^d P(x) \cos(n\pi x/d) dx \quad \text{for } n=1,2,\dots \quad (15)$$

It should now be noted that  $a_n$ ,  $A_n$  and  $B_n$  are coefficients of Fourier series expansions for  $\Delta T(x,0)$ ,  $\rho(x)$  and  $P(x)$  respectively if these are expanded as cosine, sine and cosine series respectively.

The foregoing analysis shows that the inhomogeneous pyroelectric response consists of exponentially decaying components with relaxation times  $\tau_1/n^2$ . Measurement of this response yields Fourier coefficient combinations  $(\frac{a_n}{a_0}) (\frac{A_n}{A_0})$  ( $\frac{d}{\pi}$ ) in the charge case, or  $(\frac{a_n}{a_0}) (\frac{B_n}{B_0})$  in the polarization case (or a linear combination of these in the mixed case). For sufficiently short pulse duration ( $t_r \ll \tau_1/n^2$  up to the highest  $n$  of interest), the approximation  $a_n/a_0 \approx 2$  can be made. Otherwise,  $a_n/a_0$  can be obtained from a separate measurement of the transient resistance of the electrodes. Thus, Fourier coefficients of the charge or polarization distribution,  $A_n/A_0$  or  $B_n/B_0$ , can be determined up to terms with  $n$  of order  $N = \sqrt{\tau_1/t_r}$ . The spatial resolution of the thermal pulse experiment is roughly  $d/N$ .

Limiting cases of charge and polarization distributions are of interest. Note that if  $\rho(x) \rightarrow \delta(x)$ , then  $\Delta V_p(t) \rightarrow 0$  (i.e., charge on surface  $x = 0$  does not contribute to  $\Delta V_p(t)$ ), while if  $\rho(x) \rightarrow \delta(x-d)$ ,  $\Delta V_p(t)$  becomes indistinguishable from  $\Delta V_p(t)$  for uniform polarization. This is a manifestation of the electrostatic equivalence of  $\rho(x)$  and  $-dP/dx$ . Note also that if  $P(x) \rightarrow \delta(x)$ , then  $\Delta V_p(t)$  becomes proportional to  $\Delta T(0,t)$  in (7), while if  $P(x) \rightarrow \delta(x-d)$ , then  $\Delta V_p(t)$  becomes proportional to  $\Delta T(d,t)$  in (8). This is a consequence of the symmetrical roles played by  $a_n$  and  $B_n$ .

Figure 1 shows signals proportional to open-circuit voltages for two copolymer samples 50  $\mu\text{m}$  thick (vinylidene fluoride with 27% by weight of tetrafluoroethylene). For each sample Curve A is for light pulsed at  $x=0$  and Curve B is for light pulsed at  $x=d$ . The difference in the samples is in the poling treatment. Both samples were stored for long periods under short-circuit conditions after poling. Sample (a) was poled at room temperature by corona charging<sup>(8)</sup> with a bias voltage of -2000 V. Curve A, shown in Figure 1(a) is nearly proportional to the  $\Delta T(0,t)$  signal (not shown) at times  $t \gg t_r$  where  $t_r \approx 20 \mu\text{s}$  while Curve B is nearly proportional to  $\Delta T(d,t)$ . These observations indicate (assuming that all  $B_n = 0$  for  $n > N$ ) a sample with strong localization of polarization towards  $x=0$  as shown qualitatively by (a) in the inset (or a sample with a charge layer imbedded just inside the sample close to  $x=0$ ). Sample (b) was poled during crystallization by maintaining 300 V across the sample as it was cooled from 130°C and crystallized for 6 hours at 118.5°C before cooling further to 100°C (0.3 K/min) followed by quenching to room temperature. The signals for this case, shown in Figure 1(b), indicate a distributed asymmetric pyroelectric activity.

Note that series (10) and (13) acquire alternating signs if the direction of irradiation is changed (in which case  $a_n$  changes to  $(-1)^n a_n$ ) or if the sample is reversed (in which case  $A_n$  and  $B_n$  change to  $-(-1)^n A_n$  and  $-(-1)^n B_n$ ). Thus, if separate response signals are obtained by thermally pulsing opposite surfaces in turn, the even and odd Fourier coefficients can be obtained separately from the sum and the difference of the two signals. Visual comparison of the two signals also reveals whether the distribution of pyroelectric responsivity is symmetric or asymmetric.

Figure 2 shows semi-log plots of the curves A and B from Figure 1(b) together with (A+B) containing only even terms of the response and (A-B) containing only odd terms of the response. Assume that the responses are associated with polarization. Graphical analysis of the linear part of the odd response gives  $\tau_1 = 4.8$  ms (in good agreement with the value expected from the thermal properties and the thickness of the film) and  $2a_1B_1 = 14$ . Removal of this linear part gives a remainder (Curve D) with a slope  $9/\tau_1$  indicating that  $2a_3B_3 \approx 1.5$  and that  $2a_5B_5 \approx 0$ . Similar analysis of the even response gives  $2a_0B_0 = 10.2$ ,  $2a_2B_2 \approx 5$  (from Curve C) and  $2a_4B_4 \approx 0$ . As the pulse duration of  $t_r \approx 20$   $\mu$ s should allow about 10 terms to be observed ( $N = \sqrt{\tau_1/t_r} > 10$ ), and terms for  $n \geq 4$  do not appear in the pyroelectric response (though they appear in the  $x=0$  resistance signal), it is concluded that the  $B_n$ 's for  $n \geq 4$  are negligible compared to the four leading coefficients. The values of  $a_2B_2$  and  $a_3B_3$  are then corrected to the values 2.675 and 0.775 respectively by forcing coefficients  $a_0B_0$ ,  $-a_1B_1$ ,  $a_2B_2$ ,  $-a_3B_3$  when inserted into (13) to yield a curve B' in Figure 2 within experimental uncertainty of measured Curve B. The polarization distribution obtained from the determined coefficients assuming  $a_1 = a_2 = a_3 = 2a_0$  is the distribution (b) in the inset of Figure 1.

The samples discussed in this Letter were chosen to illustrate the theory. Other copolymer samples and homopolymer (polyvinylidene fluoride) samples under different poling conditions can exhibit nearly uniform polarization<sup>(9)</sup>. In such cases, the response is nearly step-like and  $B_n/B_0 = 0$  for all n.

The present work indicates the source of ambiguity in the Collins' deconvolution procedure. The thermal pulse data (under conditions similar to those in Collins' experiments) yields no more than 10 or 15 coefficients (based on  $N = \sqrt{\tau_1/\tau_r}$ ). The Collins' electrical analog sought to obtain discrete distributions characterized by 20 adjustable parameters. Any discrete distribution (of which there are many) consistent with the determinable Fourier coefficients would reproduce the measured transients within the noise in the data.

Partial support of this work by the Office of Naval Research is gratefully acknowledged.

## FIGURE CAPTIONS

FIGURE 1                      Inhomogeneous pyroelectric response of two copolymer samples: (a) sample with pyroelectric activity concentrated towards surface  $x=0$ ; and (b) sample with distributed pyroelectric activity. Signals marked A are for thermal pulse applied to surface  $x=0$  and those marked B for thermal pulse applied to surface  $x=d$ . Inset shows thermal pulse arrangement. Polymer samples have vacuum-deposited, reflecting (partially absorbing, non-transmitting) electrodes. Polarizations (a) and (b) shown in the inset are obtained from first few Fourier moments of corresponding signals.

FIGURE 2                      Graphical analysis of response of Fig. 1(b). A and B, experimental data;  $A + B$  and  $A - B$  are even and odd response (see text). The relaxation time  $\tau_1 = 4.18$  ms, coefficients  $a_0 B_0 = 5.1$ ,  $a_1 B_1 = 7$ ,  $a_2 B_2 = 2.675$ ,  $a_3 B_3 = 0.775$ ,  $a_n B_n = 0$  for  $n \geq 4$  are determined as explained in text.  $B'$  is a plot of Eq.(13) with  $a_n$  replaced by  $(-1)^n a_n$  using these  $a_n B_n$ 's. C and D represent the  $n = 2$  and  $n = 3$  terms respectively.

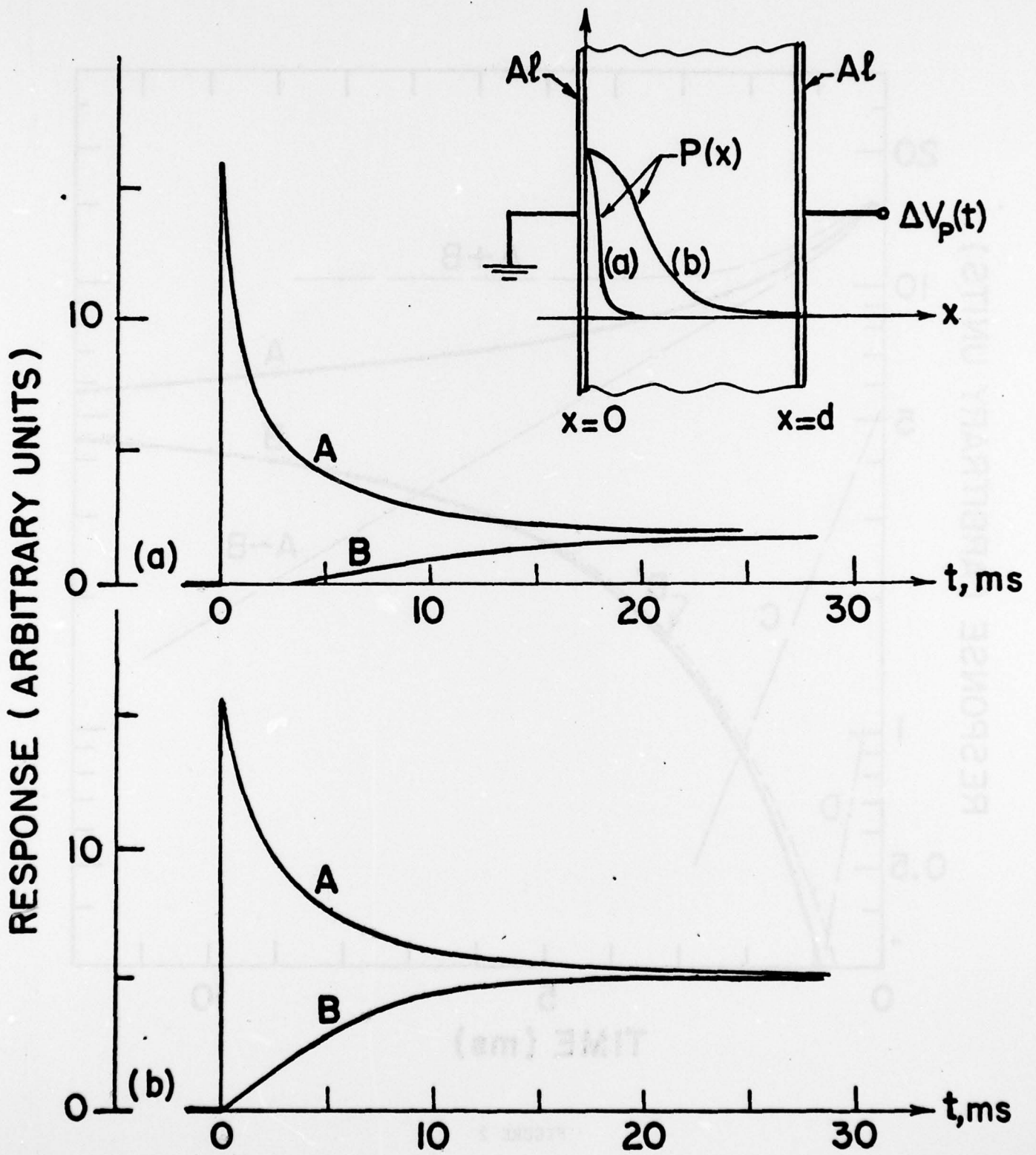


FIGURE 1

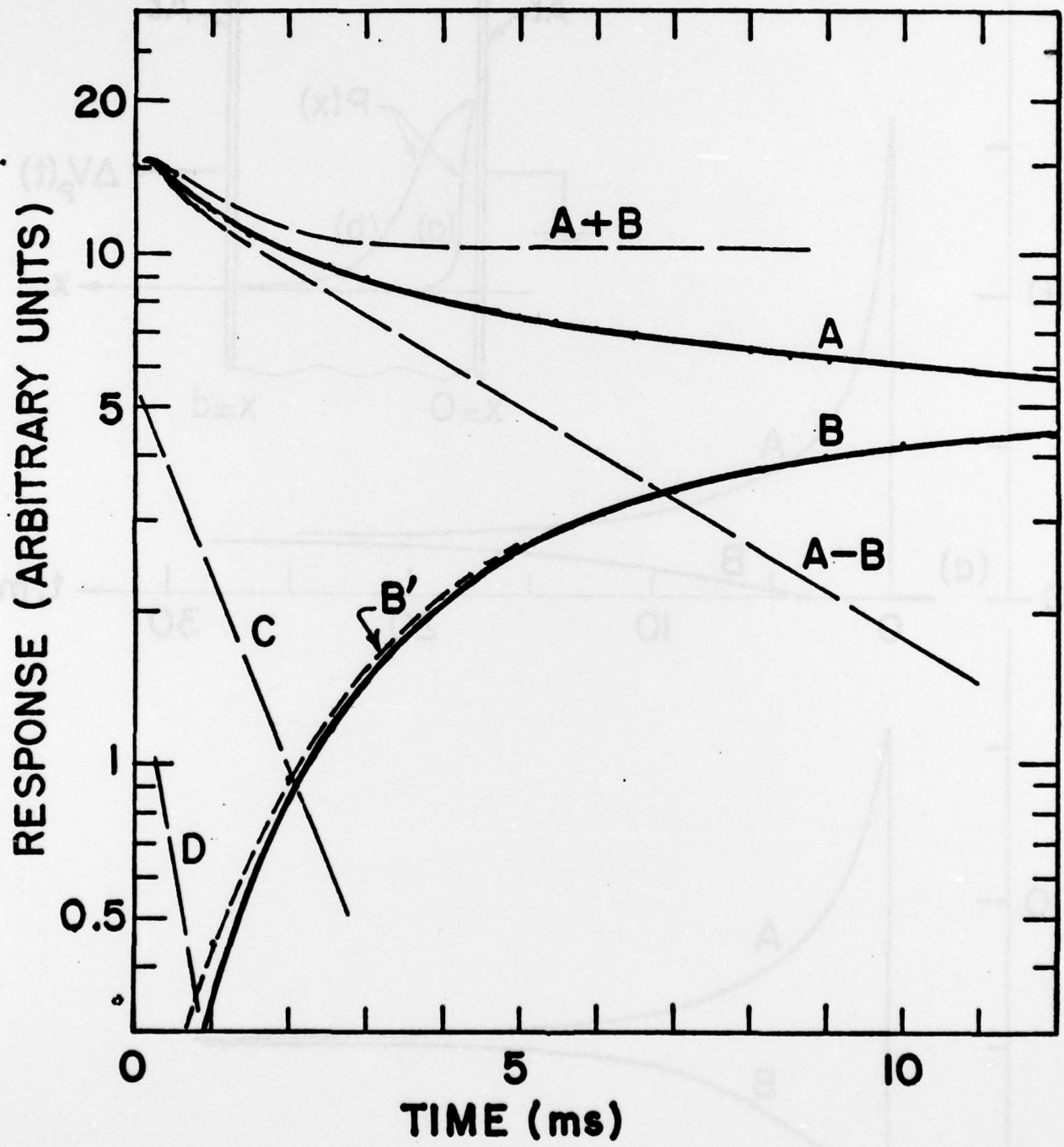


FIGURE 2

### References

1. G. M. Sessler, J. E. West, D. A. Berkley, and G. Morgenstern, Phys. Rev. Lett. 38, 368 (1977).
2. P. Laurenceau, G. Dreyfus, and J. Lewiner, Phys. Rev. Lett., 38, 4-6 (1977).
3. R. E. Collins, Appl. Phys. Lett., 26, 675 (1975).
4. R. E. Collins, Rev. Sci. Inst., 48, 83 (1977).
5. R. E. Collins, J. Appl. Phys., 47, 4804 (1976).
6. See for instance R. V. Churchill "Fourier Series and Boundary Value Problems", McGraw Hill 1941, p. 109.
7. W. J. Parker, R. J. Jenkins, C. P. Butler, and G. L. Abbott, J. Appl. Phys., 32, 1679 (1961).
8. A. D. Southgate, Appl. Phys. Lett., 28, 250 (1976).
9. M. G. Broadhurst, G. T. Davis, S. C. Roth, and R. E. Collins, Proceedings of the 45th Annual Conference on Electrical Insulation and Dielectric Phenomena, Buck Hill Falls, October 1976 (in press).



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