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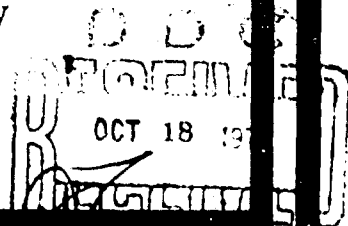
A Critical Compilation of Compressible Turbulent Boundary Layer Data

by

H. H. Fernholz and P. J. Finley

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Section C: Data for a selection of the profiles	
Section D: Additional data.	
The associated microfiche gives the tables of section B complete, and data for all the profiles listed in section B, from which section C is a selection.	
The pages of each section of each entry are numbered individually.	
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i. GENERAL PREFACE

At the 1971 EUROVISC meeting in London the late Dietrich Kùchemann suggested to the first author that the data collection which he had started for his own research purposes would be generally useful if it could be extended and made accessible in standardised form. Thus this project was launched under the auspices of EUROVISC, and it has remained so through the assistance and advice of an informal advisory group, consisting of L.C. Squire (Cambridge), J.L. Stollery (Cranfield) and K.G. Winter (RAE Bedford). The data collection and handling have throughout been funded by the German Research Council (DFG) and the Technical University Berlin. By 1973 the computational framework was established by H.J. Kùster and the actual work had been started. At the beginning of 1974 the team was joined by Miss C. Mohr, who has since handled all the computational work, and by the second author, on leave from Imperial College. During that year we were able to lay the foundations and complete most of the structure of the catalogue. Our work was encouraged by the agreement of the Fluid Dynamics Panel of AGARD to support and arrange publication, with Professor Fanneløp (Trondheim) as AGARD editor. Since that time we have been engaged, principally, on the physical labour of handling all the data and the minutiae of presentation, above all in the inevitably unsuccessful pursuit of consistency. Had we been fully aware of the force of Dr. Johnson's comment that "making dictionaries is dull work" it is doubtful that we would have had the temerity to start. As it is, the final product is the result of the labour of so many hands in addition to our own that the attempt at proper acknowledgement below must needs be hopelessly incomplete.

We hope to follow this volume, which is a compilation of fact, and as little coloured by opinion as we could contrive, with a volume of commentary on the general nature of compressible boundary layer data, and some of the problems of interpretation which arise.

ii. ACKNOWLEDGEMENTS

Firstly we must thank all the authors whose experiments are presented in the entries. The compilation describes their work, and ours is only the secondary occupation of ordering it. We have tested the authors' patience with often lengthy and repeated questionnaires, and must thank specially those who suffered our first attempts, when we were learning our trade. In addition to all those who answered our many questions, and who are mentioned in the entries, we thank J.C. Westkaemper, of the University of Texas in Austin, for assistance in obtaining many DRL reports and then checking our experimental accounts. We also thank K.G. Winter and the RAE for arranging a literature search on our behalf, D.M. Bushnell, lately of NASA Langley, for helping us to obtain a quantity of apparently inaccessible data, and P. Bradshaw of Imperial College for much helpful general advice and detailed criticism.

We could not have hoped to produce the catalogue without the able and uncomplaining assistance of our co-workers. H.J. Kùster and Miss C. Mohr have been mentioned above. Unfortunately only direct experience could make real the sheer quantity of tiresome detail work done by C.M. - let alone the physical effort of continually moving around massive collections of computer printout. We must also thank T. Podtschaske who performed the greater part of the interpolation work which continually proved necessary. Mrs. H. Geib, who prepared the text, earns the special thanks of the second author for coping with endless revisions in his notoriously illegible handwriting, and we thank Mrs. I. Gereke for making all our drawings.

Amongst official bodies, our debt to the DFG and TUB for funding the research work is pre-eminent, while for nearly a whole year out of the last three the second author has been a grateful guest of the Hermann-Fùttinger-Institut in Berlin. The publication is funded by AGARD, and we would thank the Fluid Dynamics Panel and its successive executives, J. Lawford and M. Fischer, for their help and encouragement.

Finally we must thank Cornelia and Sophia for their support and for not complaining too much at those frequent periods during which they have been "Catalogue widows".

iii. FOREWORD

The principal objective of this compilation is to provide ready access to a large body of boundary layer data. The printed volume contains a great part of this, but it has not proved possible to print the complete collection. However, all the data processed was reduced to a standard form and stored on magnetic tape. The original complete processed data tabulation was transcribed onto paper, and accompanies this volume as a microfiche. The precision of the data is an order, or orders, higher than its accuracy and we cannot state too forcefully that there are very few individual data presented here for which it would be possible to claim an accuracy of 1%. The much higher level of precision in the tables, usually at five significant figures, occurs purely as a result of our desire to standardise the presentation in a format which is convenient for the computer, and to eliminate any possibility of editor-induced rounding errors.

Ready access implies that the user should not have to undertake any substantial reprocessing of data, and especially should not be compelled to transcribe the information back into computer-digestible form. To this end, arrangements have been made with the following organizations in NATO countries to hold master copies of the data tape. These organizations will prepare copies on request; enquiries as to terms should be directed to the organization concerned. The tape will probably be an exact transcription of the data in the microfiche tabulation accompanying this publication, but may be modified slightly to make it easier for users to enter the information into their own programme.

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TAPE: GENERAL SPECIFICATION

Seven-track, half inch tape, recorded at 800 BPI
Coded: BCD, even parity
Block length - 1280 characters maximum
Overall length 720 m

iv. LIST OF ABBREVIATIONS

APG	-	adverse pressure gradient
AW	-	adiabatic wall
CC	-	constant current
CCP	-	cone cylinder static pressure probe
CPP	-	circular Pitot probe
CT	-	constant temperature
D	-	D-state is the nominal boundary layer edge state
E	-	estimated by editors
ECP	-	equilibrium cone probe
FEB	-	floating element balance
FPG	-	favourable pressure gradient
FPP	-	flattened Pitot probe
FWP	-	fine wire probe
H	-	height of the test section
HT	-	heat transfer
HWP	-	hot wire probe
MHT	-	moderate heat transfer
NA	-	not available
NC	-	not computed
NM	-	not measured
NPG	-	normal pressure gradient
NX	-	number of X-stations
PC	-	private communication
RUN	-	full 8-digit identification of the profile
RW	-	reflected wave
SH	-	severe heat transfer
SPP	-	static pressure probe
STP	-	static temperature probe
SW	-	simple wave
TPP	-	total pressure probe
TTP	-	total temperature probe
VPG	-	variable pressure gradient
W	-	width of the test wall
ZPG	-	zero pressure gradient

PROBE DIMENSIONS

d_1	-	outside diameter
d_2	-	inside diameter
h_1	-	overall height of face
h_2	-	height of opening
b_1	-	overall width
b_2	-	width of opening
l	-	length of slender portion
α	-	cone semi-angle

v. LIST OF SYMBOLS

Computer	Symbol	Conventional	Meaning	Definition
-		a	velocity of sound	$(\gamma RT)^{1/2}$
CF		c_f	skin friction coefficient	$2\tau_w/\rho_\delta U_\delta^2$
CQ		c_q	heat transfer coefficient	$\dot{q}/(\rho_\delta U_\delta c_p T_{0\delta})$
		c_p	specific heat at constant pressure	
D		δ	boundary layer thickness or boundary layer edge-point selected	
D1		δ_1	displacement thickness	eqn. (3.7.1)
D2		δ_2	momentum defect thickness	eqn. (3.7.2)
D3		δ_3	kinetic energy defect thickness	eqn. (3.7.3)
D4		δ_4	total enthalpy defect thickness	eqn. (3.7.4)
D1K		δ_{1K}	displacement thickness ($\rho/\rho_\delta = 1$)	
D2K		δ_{2K}	momentum defect thickness ($\rho/\rho_\delta = 1$)	
D3K		δ_{3K}	kinetic energy defect thickness ($\rho/\rho_\delta = 1$)	
D1P		δ_{1p}	-	eqn. (3.7.6)
D2P		δ_{2p}	-	eqn. (3.7.7)
D3P		δ_{3p}	-	eqn. (3.7.8)
D4P		δ_{4p}	-	eqn. (3.7.9)
D STAR		δ^*	"true" displacement-thickness	eqn. (3.7.5)
		γ	ratio of specific heats	c_p/c_v
H12		H_{12}	shape factor	δ_1/δ_2
H32		H_{32}	shape factor	δ_3/δ_2
H42		H_{42}	shape factor	δ_4/δ_2
H12K		H_{12K}	shape factor	δ_{1K}/δ_{2K}
H32K		H_{32K}	shape factor	δ_{3K}/δ_{2K}
I		-	Y-station identity	-
KAP		κ, γ	ratio of specific heats	c_p/c_v
-		λ	heat conduction coefficient	
M		M	Mach number	u/a
MD		M_δ	Mach number at δ	u_δ/a_δ
M/MD		-	Mach number ratio	M/M_δ
MUE		μ	dynamic viscosity	eqns. (5.1), (5.2)
MUED		μ_δ	dynamic viscosity at δ	-
MUEW		μ_w	dynamic viscosity at w	-
P		p	static pressure	-
PD		p_δ	static pressure at δ	-
P/PD		-	static pressure ratio	p/p_δ
PI2		Π_2	pressure gradient parameter	$(\delta_2 dp/dx)/\tau_w$
PO		p_0	stagnation pressure	

Computer	Symbol	Conventional	Meaning	Definition
POD		$P_{0\delta}$	stagnation pressure at δ	
PT2		P_{t2}	pitot pressure	
PW		P_w	static pressure at w	
PWD		P_w/P_δ	-	P_w/P_δ
R		r	recovery factor	
RE		-	Reynolds number/m	$\rho_\delta U_\delta / \mu_\delta$
RED2D		Re_{δ_2}	Reynolds number based on δ_2	$\rho_\delta U_\delta \delta_2 / \mu_\delta$
RED2W		Re_{δ_2}	Reynolds number based on δ_2	$\rho_\delta U_\delta \delta_2 / \mu_w$
RGAS		R	gas constant	
RO		ρ	density	
ROD		ρ_δ	density at δ	
ROW		ρ_w	density at w	
RO/ROD		-	ratio of densities	ρ/ρ_δ
RZ		R_z	transverse radius of curvature	
SW		-	number indicating the relative importance of longitudinal curvature in a pressure gradient	eqn. (5.5)
T		T	temperature	
TD		T	temperature at δ	
T/TD		-	temperature ratio	T/T_δ
TO		T_0	stagnation temperature	
TOD		$T_{0\delta}$	stagnation temperature at δ	
TR		T_r	recovery temperature	eqn. (5.3)
TRD		T_r/T_δ	recovery temperature ratio	
TW		T_w	temperature at w	
TWD		T_w/T_δ	wall temperature ratio	
TWR		T_w/T_r	wall-recovery temperature ratio	
U		u	velocity component in x-direction	
UD		u_δ	velocity component in x-direction at δ	
U/UD		-	velocity ratio	u/u_δ
X		x	streamwise or axial coordinate	
Y		y	coordinate normal to wall	

vi. GUIDANCE FOR USERS OF THE CATALOGUE

This volume and the associated microfiche collection provide descriptions of, and the data obtained from, 59 experimental studies of two-dimensional compressible turbulent boundary layers.

Each study is described at the start of the appropriate numbered ENTRY, to be found in § 8 below. The boundary conditions and evaluated data for all the profiles processed are also given, as section B of the entry. Each entry also contains, as section C, a selection of the profile data. The entire collection of data, boundary conditions, evaluated data and complete, detailed, profile data are provided in the microfiche version of the compilation which accompanies this printed volume. The microfiche does not, however, include the additional data which are printed where appropriate as section D of each entry.

The data collected and printed on the microfiche are also recorded in approximately the same form on a magnetic tape, copies of which can be obtained by following the procedure indicated in the Foreword (iii). The way in which an ENTRY is constructed is outlined in § 3, and we recommend, strongly, that readers should not attempt to use the compilation without assessing our own approach as we have there stated it. In particular, subsection § 15 of each entry constitutes our comment on the experiment in question, and is inevitably coloured by our own obsessions. We would therefore recommend that the editors' comments should always be interpreted in conjunction with the associated comment of § 4.

The computational framework is described in § 5, but we feel that, initially, this aspect should not particularly concern the user as the potential for heresy in numerical operations is small. Where, however, numerical procedures are likely to cause crucial differences - as for example in the evaluation of integral quantities, critical readers should ensure that any comparison they make is based on a foundation which is either the same as that which we have used, or which can easily be compared to ours, and so should study our assumptions (§§ 5.2, 5.5, 5.6, 3.6, 3.7).

Finally, and perhaps most important: the reader will wish to know how to find the entry most appropriate to his needs. To this end we have constructed the classified lists of § 7. The principal classification of § 7.1 is based on the considerations outlined in § 6, but our approach should be assessed in connection with the less quantifiable factors discussed in § 2, and especially in § 2.3.

REQUEST FOR FURTHER DATA

The editors hope to be able to issue a supplement to the data presented in this volume, and so would be grateful for an account of any suitable experiment which is not included. The greatest need is for functionally complete measurements in boundary layers on longitudinally curved surfaces, but high quality data of any kind would be appreciated. Cases including information on the turbulence structure are very rare, and it is possible that some information may now be available from "non-intrusive" techniques.

Authors may gain an impression of the information we would require from the present volume. We would especially appreciate the supply of data in some computer digestible form.

Fixed to the inside back cover of this volume are three pockets containing 28 microfiche. These provide a complete listing of the profile data as processed by the computer when preparing the catalogue. They consist of continuous strip photographs of the raw output, before cutting and selection for the printed form of the catalogue. The method of production requires the tables to run 'across' the microfiche when viewed in the normal sense, and in consequence a non-standard square format has been adopted. This allows the microfiche to be placed in the carrier of the older and cheaper forms of viewer with the columns in the right orientation for the reader.

A typical microfiche is headed

AG 223 No. 4 of 28 Profile 60010301-64010803

thus indicating that this is the fourth microfiche, and that it contains all profiles from 60010301 to 64010803. The distribution of profile data is given below:

<u>Microfiche Profiles</u>	<u>Microfiche Profiles</u>
1: 53010101-58020101	15: 70070111-71010401
2: 58020102-58050401	16: 71010501-71030404
3: 58050402-60010207	17: 71030405-72020104
4: 60010301-64010803	18: 72020105-72021005
5: 64010804-65020202	19: 72021101-72060705
6: 65020203-65030803	20: 72070101-73010901
7: 65030804-65051101	21: 73010902-73030304
8: 65051102-67010104	22: 73030305-73040702
9: 67010105-68010803	23: 73040703-73050203
10: 68010901-69020311	24: 73050204-74010307
11: 69020312-70020304	25: 74010308-74021302
12: 70020401-70031202	26: 74021303-76010203
13: 70040101-70040503	27: 76010204-76010409
14: 70040504-70070110	28: Section B - 'Reference flow values'

All computed data - sections B and C - are included. The 'additional data' of section D is given only in printed form, with the entries.

1. INTRODUCTION

1.1 Aims and objectives

Anyone undertaking to prepare a catalogue of boundary layer data must start by paying homage to Coles & Hirst (1968), who prepared the first such compilation. The Stanford Catalogue stemmed from the need to provide sets of boundary layer data which could serve as a basis of comparison for a wide variety of calculation methods. The present data collection can be considered as an extension of the Stanford Catalogue to Mach numbers beyond one, and to flows with heat transfer at the wall. The experimental data are presented as consistently as possible and in a form which has been chosen to suit both the user who wishes to plot or recalculate the data and for entry into a computer if theory and experiment are to be compared. The purpose of the present catalogue is to facilitate the interpretation of experimental data rather than to suggest or to support a particular theoretical analysis of compressible turbulent boundary layers. To that end we have attempted to confine our rôle as editors strictly to describing the general conditions of the experimental arrangement, the initial- and boundary-conditions of the experiment and the experimental data as given by the experimenters themselves. Information and opinion have been separated from each other as distinctly as possible, opinion, we hope, being confined to the introductory chapters and the "editors' comments" at the end of our description of each experiment.

One of our more obvious objectives has been to ensure, so far as it lay in our power, that any data processed by us should be available in a readily re-usable form. It is a sobering thought that every experiment forming the subject of an entry has already been published in some form, usually with numerical information. Nevertheless, with a few exceptions, we have had to arrange for the data to be transcribed once more to punched cards, so that it might be processed. For any modern experiment, this work is essentially unnecessary, since it would have been a simple matter for the originating institutions to have kept the information in some computer-digestible form. We have probably invested one or more person-years in routine number punching, and hope that the existence of the magnetic data tape which forms part of this enterprise will make any repetition of such drudgery needless.

The data compilation contains about 1400 profiles, and the ready availability of so large a data-bank in standard form contains its own dangers. We feel that we must issue a warning against any possible tendency amongst research workers to use only the data we have provided - because it is there and does not require further transcription. Disregarding any more subtle criteria which might be applied in selecting experiments for inclusion, there was no possibility of our preparing an entry unless we had access to the data in reasonably precise form. Data could be inaccessible for many reasons. The experiment could be so old that no full record remained, or so new that the clearance procedures required by authority could not be completed in time. Detailed experimental records often seem to be discarded with alarming rapidity and in some particularly regrettable cases the data were lost or scrapped before official permission to use it could be obtained. The experiments, however, remain valid, and for many purposes numerical values may be obtained with sufficient accuracy from graphical presentations in the published accounts. In the proposed commentary volume, associated with this data compilation, we hope to include a classified list of the experiments known to us, indicating the extent of the available information for each one.

A further simple objective is an indication of the experimental range covered. Only too often an investigation is performed largely because it is possible with the available experimental facility. A glance at figures 6.1 and 6.2 will show that the coverage of adiabatic zero-pressure gradient flows at moderate Mach and Reynolds numbers is almost excessive. There is no object in making more mean flow measurements in this range unless perhaps for the calibration of a new type of instrument. On the other hand, fluctuation measurements are so rare that almost any study of turbulence structure has great potential value. For more complex mean flows the coverage is much less complete. Section II of the classified list § 7.1 shows that experimental descriptions of curved-wall flows are particularly needed. (We have made provision in the list, as nil entries, for some types of flow for which we knew of the existence of appropriate experiments but did not have the necessary data.)

We hope that a thorough indication of the range already covered will help prevent expenditure on unnecessary repeat experiments.

A final scientific application of the data bank is the provision of test cases for theoreticians developing calculation methods. It is perhaps too early to consider the possibility of a Stanford-type tournament for compressible boundary layers, but we do feel that amongst the 59 experiments described here there is enough variety in the basic flows to allow theoretical workers to extract any mean-flow based physical constants they require. There are also several interesting test cases!

1.2 General principles guiding the form and content of the compilation

Since the fundamental purpose of the compilation is to transmit data, we consulted many potential users, and especially the members of the EUROVISC advisory group. The results of these discussions may be summarised as:

- (a) The value of such a collection increases much more rapidly than its size, as extra entries are included.
- (b) Every effort should be made to make a complete presentation of the data for each entry.
- (c) It should be possible for a user to obtain complete tabular data without recourse to a computer.
- (d) Preparation of the data in computer-digestible form would greatly increase the value of the collection.

Considerations (a) and (b) are clearly the principal factors affecting the overall size of the catalogue, without taking any account of the actual method of presentation to be used. In further discussion we have found it convenient to attach specific meanings to certain words, indicating the hierarchy of information. Thus below:

A REFERENCE is any paper consulted in connection with the project.

A SOURCE is the principal reference specifically describing an experiment in which compressible boundary layer data were obtained.

AN ENTRY is the text we have prepared from a source selected for inclusion in the data compilation. We refer to entries as CAT 7201 etc. where 7201 is the entry serial number in the compilation of § 8.

There are 59 entries selected from about 300 sources. Some indication of the principles guiding selection is given in § 2 below, so that (a) will not be discussed further here.

We have accepted point (b) almost without qualification, and often therefore pestered the authors of potential entries for much subsidiary information which did not appear in the source papers. There are however some sources which contain so many data that there was no possibility of our including them all (e. g. CAT 6503). Where we have rejected data, we have tried to ensure that we retained a fully representative selection, or that there were real grounds for believing that the data rejected were in some respect of inferior quality.

The remaining points concern matters of presentation. There is little difficulty in dealing with the publication of the boundary and initial conditions of an experiment, and these are given as "Section B" in the entries forming § 8 below (see also § 3). There are formidable problems, however, in making available the profile data, i. e. velocity-, temperature-, static pressure and fluctuating quantity profiles. For the 59 entries alone, these profiles number about 1400 in all and to print these in full in legible form would require 600 AGARD pages. We therefore had to look for a cheaper and more effective form of publication and the profiles have been made available in the following forms:

1. A magnetic tape of the complete data. Copies of this will be deposited at suitable centres in Europe and America and users will be able to obtain copies of all or part of the data from these on supplying their own blank tapes. (A fee may be charged - see the Foreword)
2. A microfiche copy has been made of the complete profile tables in a format similar to that used for the master tape. This has been issued with the printed collection.

3. A selection of the profiles edited from the complete tabular print-out of form 2 is presented in the printed collection as section C of each entry.

We feel that this will answer the needs of users whilst reducing the size of the printed collection to manageable proportions. The magnetic tape (form 1) allows a user to enter the data directly in his own computer programme, or should he so desire, to prepare his own full-size print-out of all the data, or any section in which he has an interest. The microfiche (form 2) allows a user to read the tabular print-out directly, or to obtain full-size tables of any data in which he has an interest through normal library channels.

The printed selection of form 3 is intended to satisfy the needs of a user who wishes to obtain a general view of the nature of profile data in the type of flow in question and in the relevant experimental range. If he wishes to obtain more detailed information, the complete tabulation of boundary conditions in section B of the entry will allow him to choose the data he wishes to call up from forms 1 or 2. He may assess the likely reliability of the data from the method by which they were obtained (entry-section A) and the internal evidence of scatter and consistency shown by plotting out some of the printed sample profiles of section C (form 3).

4

2. EVALUATION OF DATA

2.1 Experiments considered

With very few exceptions the experiments considered for inclusion had been published previously. Since it was from the open literature that we obtained all our general information, publication was almost a necessary condition, though in a few cases an enquiry about a published source paper led us to unpublished information or material being prepared for publication. In many cases the amount of information finally made available by our correspondents greatly exceeded that in the original source.

The total number of reported compressible boundary layer experiments is very large. We have here restricted ourselves to the study of nominally two-dimensional turbulent boundary layers (some of them transitional) formed on rigid impermeable walls, and have excluded cases in which it would be necessary to take account of chemical reactions or ionization. In fact we have assumed throughout that the test gas was a perfect gas, with constant specific heats, although in a few cases the temperature range is such that the relationship between reservoir conditions and test station conditions is detectably falsified as a result of vibrational excitation. Boundary layers with suction or injection through the wall were excluded, as the data known to us are relatively well documented. The data have been collected by another group and could, in principle, be edited without too great an effort, if need be. Although a number of correspondents have urged us to include these more complex flows, and also shock/boundary layer interactions or three dimensional flows, we have firmly resisted these suggestions, knowing the limits of the financial means available and not wishing to impose too great a load on our patience and perseverance, let alone that of our co-workers. In some cases regretfully, we have excluded any experiment for which we did not have access to tabulated data. In part as a consequence of the limited assistance available to us, but principally because of the lack of precision inherent in the procedure, we have not generally incorporated information scaled from graphs published in the source papers. In a few cases, auxiliary information has been so obtained, and for several entries we found it necessary to prepare our own graphs for interpolation. When this has been done, it is remarked in the text of the entry.

2.2 Principles of selection

In attempting to evaluate an experimental account, we looked to see how far the following conditions were satisfied:

- i) The data should be given in uncorrected form. If corrections were applied by the author, the magnitude and method of correction should be stated, so that the data could be recalculated in their original form if need be.
- ii) A certain minimum of information about the experimental arrangements, test conditions and boundary conditions should be available.
- iii) The information about the boundary layer at a test station should be functionally complete.
- iv) There should be a sequence of profiles, for successive streamwise measurement stations.
- v) The upstream history of the layer should be known.

These are obvious statements of an ideal, and equally obviously there are very few experiments reported which begin to satisfy them all. If therefore we were to insist on a "full set" of measurements, there would be remarkably few entries in the catalogue. We now study the implications of each condition.

In dealing with i) there is an obvious difficulty in distinguishing between "calibration" and "correction". Whenever readings are altered to take account of phenomena not considered in the fundamental calibration procedure, as for instance wall proximity or shear corrections for a Pitot tube, it is clear that we are dealing with a correction. If however the Pitot tube is used in a very severe environment, as in the low density regions near the wall of CAT 7105, it is a moot point whether the adjustment made to the pressure recorded is a correction or a calibration. A possible criterion is to recognise adjustments as a calibration when made as the result of a subsidiary experiment covering the same range of relevant dimensionless groups as for the main tests, whether the calibration were performed by the same authors or no. On this basis we may suggest generally that adjustments to Pitot readings for wall proximity,

shear and perhaps low density are "corrections", that total temperature probes are usually "calibrated" and otherwise uncorrected, but that static pressure probes are usually used with "corrections" - for viscous interaction, low density and thermal effects - which in hypersonic flows are often more than a little speculative. If only because of the "grey area" of indecision, we have usually found that i) therefore did not as a general rule particularly affect our decision as to inclusion in the catalogue, though we may have expressed reservations in the accounts of particular entries.

Condition ii) has also not proved, generally, to be crucial. We have often had difficulty in dealing with source papers, but have usually received assistance from the authors which has made reasonably clear, for us, the nature and extent of their experiments. In one or two cases we could not decide what the author had done, but did not request that he re-write his report as we thought that, on the evidence of the first version, we were unlikely to receive much enlightenment from a revision. Such an experiment was obviously automatically excluded.

For the measurements at a station to be functionally complete, as required by iii), we would need a complete mean flow profile description, wall shear stress and heat flux values, profiles of fluctuation quantities, and a substantial amount of detail describing the free stream flow and the test station geometry. Thus for the mean flow profile description it must be possible to obtain or infer at least three independent property profiles, of which one, or a group, must specify the dynamic state. The usual experimental grouping obtained from measurements is the set (p_{t2}, p, T_o) but other groups are possible if density is measured optically or by electron beam, or if velocity is determined, directly by Laser-doppler-velocimeter or indirectly with a hot wire. Whatever the original grouping, there are many possible sets which may be presented in the tables available to us. Wall shear stress and heat flux values should be measured by instruments on or in the wall (floating element balances, Preston tubes, heat flux meters, steady or unsteady conduction techniques) rather than inferred from the profile measurements. It is possible in simple flow cases to make satisfactory determinations from the profiles, but in the more difficult flows, it usually becomes necessary to differentiate profile data, and it is not usually possible to do so with any precision. Without considering the need for fluctuation measurements, it can be seen already that under iii), alone, the requirements so far are so severe as to eliminate all except about 8 of our entries. If we insist on substantial fluctuation measurements we are left with one.

We have in general given preference to measurements satisfying condition iv), but it proved necessary to include a large number of single-station measurements in order to cover a wide enough range of Mach number, Reynolds number and heat transfer parameter. Some single station tests are also included as comparison cases for other experiments.

Finally we were forced to recognise firstly that many unexplained effects in the experimental region were the consequence of the varied natures of the regions in which the test layer was formed, and secondly that it is rare for the upstream history - as a minimum, wall pressure and temperature - to be recorded. Thus condition v) is not usually observed. The obvious exceptions are the "flat plate type" flows (Category IA in the classified list of § 7.1) which in a sense have no history.

We hope that the discussion above will show that we have thought carefully about the information which is desirable - but have to recognise that we have demonstrated that it is virtually impossible for an experimental worker to satisfy our list of requirements. There is one case, CAT 7205, which does in practice fulfil our specification - but inevitably, as a consequence of the very close detail required of the study, the investigation covers a restricted range.

Our final selection has been guided by a desire to fulfil the conditions listed above. The number of experiments which on a crude marking scheme score 80 % or more is exceedingly small, so that we have drawn a majority of the entries from less "satisfactory" experiments. (We cannot overemphasise that this implies no judgement of the quality of the experiment - we refer simply to the extent to which the criteria of coverage (i) to (v), above are satisfied). We must confess that in the final result, we could not go through the list of entries and defend every one on an absolute basis.

We started by being very selective, only to find that our coverage of Mach and Reynolds number etc. was certainly inadequate if we were to show the extent of the generally successful experimental work. We were encouraged to make the scope of the catalogue as large as possible (see § 1.2 above), and partly in consequence the standards applied for entries which came late to our notice were probably less severe than those applied initially. We have also tended to give slight preference to source-papers which we believed to be difficult to obtain, or to describe experiments which were, quantitatively, unpublished. Our only certainty is that there will be just as many critics who say "why isn't X in" as there are those who say "why on earth did you include Y".

2.3 Scope of the catalogue

The general restrictions which we have observed are listed in § 2.1. Other restrictions are that this volume, with one exception, considers only experiments for which profile tabulations were available. A further limitation is that we have, in general, made no attempt either to "correct" the data, or to "uncorrect" it. We had hoped to be able to do the latter, but it proved impractical. By "correction" here we mean the adjustment of data to account for various secondary effects as discussed in connection with condition 1) of § 2.2 above. We have on several occasions incorporated gross or minor textual corrections observed either by ourselves, or, after correspondence, by the authors.

The coverage in terms of the easily quantifiable variables such as Mach number, Reynolds number and heat transfer parameter (T_w/T_R) is effectively summarised in the tables of § 7 and for zero-pressure-gradient flows, in figures 6.1-3. We consider here the extent to which less quantifiable factors are covered, and concentrate firstly on the "history effects". A convenient division here is between cases in which there is "no" history in the sense that the boundary layer is formed under zero-pressure-gradient and constant wall temperature conditions, though it is still necessary to be aware of possible disturbances introduced by tripping devices, and cases in which there is a varied pressure and/or temperature history which has imprinted certain characteristics on the test layer. For a few experiments this history is either reasonably fully described or varied in a controlled manner.

The importance of the first group lies in the fact that, for the zero-pressure-gradient cases, the influence of Mach number, Reynolds number and heat transfer parameter can in some measure be studied in a "pure" form. If it is thought that these influences are reasonably well described, it is then possible to consider the effects of change of pressure gradient or wall temperature ratio in the test zone, in isolation in so far as the input layer is fully described and related to the full corpus of appropriate experimental data for zero pressure gradient layers.

Experiments of this type are listed in table 2.1. We have not limited this list to experiments described in the catalogue, as the really complex cases are so few that we feel that the free availability of numerical data is almost a secondary consideration.

Table 2.1 PRINCIPAL EXPERIMENTS WITH ZERO-PRESSURE-GRADIENT, CONSTANT TEMPERATURE UPSTREAM HISTORY
(A SELECTION)

1. Zero pressure gradient in test zone

<u>Source</u>	<u>MD</u>	<u>R THETA X 10⁻³</u>	<u>TW/TR</u>
Coles (CAT 5301)	2-4.5	2-10	1.0
Young (CAT 6506) (uniform roughness)	5	5-13	0.6-1.0
Hastings & Sawyer (CAT 7006)	4	2-25	1.0
Peake et al. (CAT 7102)	4	10-60	1.0
Lewis et al. (CAT 7201)	4	4-13	1.0
Horstman & Owen (CAT 7205)	7.2	6-13	0.5
Watson et al. (CAT 7305)	10	1-12	1.0
Mabey et al. (CAT 7402)	2.5-4.5	5-30	1.0
Gran et al. (1974) (Temp. discontinuity)	4	?	0.5

<u>Source</u>	<u>MD</u>	<u>R THETA X 10⁻³</u>	<u>TW/TR</u>
<u>2. Favourable pressure gradient in test zone</u>			
NONE			
<u>3. Adverse pressure gradient in test zone</u>			
Peake et al. (CAT 7102)	4 to 2	10-60	1.0
Lewis et al. (CAT 7201)	4 to 2.4	10	1.0
Gran et al. (1974)	4 to 2.4	?	0.5

Experiments of the second group, for which the history is in part or fully described, often constitute succeeding portions of the first. There are however a number of cases in which a boundary layer was developed on a tunnel wall under, at least partially, described conditions before reaching the test zone of interest (see CAT 7101 as an example of a case in which an unknown history leads to an experimentally described zero pressure gradient region before entering the adverse pressure gradient region which is the point of the experiment).

Table 2.2 PRINCIPAL EXPERIMENTS WITH DESCRIBED UPSTREAM HISTORY

1. Zero pressure gradient in the test zone

<u>Source</u>	<u>MD</u>	<u>R THETA X 10⁻³</u>	<u>TW/TR</u>
Gates (CAT 7301 - temperature history)	4 & 5	8 - 31	0.9 - 1.0
Feller (1973 - temperature history)	6	35 - 50	0.7 - 0.8
Hastings & Sawyer (CAT 7006 - transition)	4	2 - 25	1.0
Fischer & Maddalon (CAT 7103 - transition)	6.5	0.5 - 6	1.0
Voisinnet & Lee (CAT 7202 - transition, temperature history)	5	7 - 58	0.25 - 1.0
Watson et al. (CAT 7305 - transition)	10	1 - 13	1.0
Moore (CAT 5805 - Step)	2 - 4	6 - 14	1.0
Clutter & Kaups (CAT 6401 - blunt increase)	2 - 4	10 - 40	1.0
Peake et al. (CAT 7102 - ring)	4	12 - 30	1.0
Stone & Cary (CAT 7209 - trip)	8	6 - 10	0.8

2. Favourable pressure gradient in the test zone

Boldman et al. (CAT 6901)	0 to 4.1	3 - 12	0.6 - 0.9
Lewis et al. (CAT 7201)	2.4 to 3.7	10	1.0
Back et al. (CAT 7207)	0 to 3.6	10	0.5, 1.1
Voisinnet & Lee (CAT 7304)	3.8 to 4.6	6 - 60	0.25 - 1.0

3. Adverse pressure gradient in test zone

Stroud & Miller (CAT 6503)	5 - 8	2 - 50	0.4 - 1.0
Zwarts (CAT 7007)	4 to 3	35 - 70	1.0
Sturek & Danberg (CAT 7101)	3.5 to 2.8	20 - 40	1.0
Peake et al. (CAT 7102)	4 to 2	10 - 60	1.0
Lewis et al. (CAT 7201)	4 to 2.4	10	1.0
Zakkay & Wang (CAT 7208)	6 to 4.6	100	0.7

Of the experiments listed in table 2.2, those performed by Boldman et al. (CAT 6901), Feller (1973), Gates (CAT 7301) and Sturek (1973 - included in CAT 7101) were specifically performed in part to investigate, and hopefully quantify, the effect of changes in the upstream wall-temperature history. All those experiments which study the "relaxation" of a constant pressure layer after a disturbance - whether a pressure gradient region, a heated or cooled wall region, or a brutal disturbance such as a step - are potentially useful "varied history" cases if measurements on an undisturbed layer with the

same free stream conditions are provided for comparison. Examples are Moore (Step - CAT 5805) Peak et al. (Ring - CAT 7102) Stone & Cary (trips - CAT 7209) and Gran et al. (1974). Some of the "described history" experiments conclude with a constant pressure relaxation region, but do not provide comparison data - e. g. Clutter & Kaups (after a blunt increase in section - CAT 6401) Zwarts (CAT 7007) and Peake et al. (CAT 7102)- both after an adverse pressure gradient region.

The final factor not covered by the lists of § 7 is the existence of fluctuation measurements. Hot-wire measurements are reported by Kistler (CAT 5803), Horstman & Owen (CAT 7205) and Laderman & Demetriades (CAT 7403). In each of these cases, the fluctuation measurements were perhaps the principal objective of the experiment. Further measurements using wedges with a hot wire leading edge, and in the same facility as CAT 7205 are reported by Mikulla & Horstman (1975), who provide a first attempt at determining the shear stress. A valuable comparison between fluctuations in zero-pressure-gradient flow and a simple-wave compression region is provided by Sturek & Danberg in CAT 7101, and very limited observations in ZPG and reflected-wave APG conditions are provided by Waltrup & Schetz (CAT 7104). In some other cases (e.g. CAT 7001/7206) hot wire measurements were made but the problems of interpretation in the hypersonic region are extremely severe, and the authors, understandably, have only reported the results in very general terms.

Approximately over the same period that the catalogue was being prepared, the "non-intrusive" fluctuation measuring instruments such as laser-doppler velocimeters and electron beams have begun to give successful results in supersonic flows. We have not yet obtained tabular information for any of these experiments but hope that both mean flow and fluctuation data obtained using these new measuring techniques may be described in a later supplement to this catalogue.

3. STRUCTURE AND CONTENT OF A CATALOGUE ENTRY

3.1 Large scale structure

An entry is composed of three or sometimes four principal sections. These are:

- SECTION A. Description of the experiment and outline of data reduction procedures. This is concluded by the final subsection "Editors' comments" which is enlarged upon in § 4 below.
- SECTION B. Tables of profile boundary conditions and evaluated data. We list here the controlling parameters, and such calculated quantities as integral thicknesses, for all the profiles we have processed.
- SECTION C. Tables of profile data. In the printed form of the catalogue, we present detailed tables for selected profiles. The total number is such that it is not practical to print the profiles in full. A full tabulation is however given in the attached microfiche, and the complete data are also available on magnetic tape (see the Foreword).
- SECTION D. Tables of additional data which for one reason or another do not fit into the computer processing scheme. These are, in general, printed at the end of the entry, but will sometimes appear at the end of section A, for space-saving reasons.

3.2 List of marginal indexing marks for Section A

We have attempted to standardise our descriptions, so that in general the sequence of points discussed is common to all entries. Inevitably we have found it impossible to be completely consistent in this, but the intention is to present the features of the experiment in the order below. The subsections may, however, appear in any order, or the topic in question may crop up in several places. Accordingly, we have arranged that index marks should be printed in the left hand margin opposite that section of the text concerned with the headings as listed. We suggest that the reader should use a photocopy of the list as a key when reading the entries. The normal sequence is:

1. Description of test section
2. Flow quality
3. Observations of transition and tripping devices (trips)
4. Upstream history of the test boundary layer
5. Measures taken to test for, or ensure, two-dimensional flow
6. Measurements at the test-surface (wall measurements)
7. Probes used for boundary-layer traverses
8. Relative positions of measurement stations
9. Authors' interpolation procedures and assumptions
10. Corrections to the profile data
11. Viscosity law assumed by the authors
12. Editors' assumptions and interpolation procedures. Selection of data.
13. Profiles presented
14. Wall data presented
- § Data summary
15. Editors' comments.

The subheadings are discussed individually in § 3.4 below, where they are indicated by their index marks in the same way as in the entries.

3.3 Recognition panel

Section A, the description, is headed by a standardised "recognition panel" laid out in semi-tabular form. An example is given here:

7201-A-1		(d)		
(c)	Oxissymmetric	$M : 4$, falling to 2.4 then rising to 3.7 (Series 01), $: 4$, ZPG (Series 02). $R \text{ THETA} \times 10^{-3} : 4 - 14$. $TW / TR : 1$.	<div style="font-size: 2em; font-weight: bold;">7201</div> <div style="font-size: 0.8em;">ZPG - APG - FPG (ZPG) AW</div>	(a)
			(b)	
	Continuous tunnel with symmetrical flexible nozzle, $M = N = 1$ m, $L = 5$ m. $PO : 496$ (± 3.5) KN/m^2 , $TO : 318$ (± 1) K, Air: Dew point 239-247 K. $RE/M \times 10^{-6} : 20$ at $M = 4$.		(e)	
	LEWIS J.E., GRAN R.L. and KUBOTA T., 1972, An experiment on the adiabatic compressible turbulent boundary layer in adverse and favourable pressure gradients. J. Fluid Mech. 61, 667-672. And Gran R.L., private communications.		(f)	

Panel (a) in the top right hand corner contains the entry identification. Each individual profile is specified by an 8-digit number such as 72 01 01 02.

This is composed as follows:

72	01	01	02
Year of publication	Serial no. within year	Serial no. of sequence	Serial no. of profile

An entry is specified by the first four digits alone as in this case

"72 01" The first source processed which was published in 1972.

The third pair of digits specify the sequence of profiles in question, which usually consists of a set of profiles for successive streamwise values of X and broadly the same tunnel reservoir conditions. This is not always the case, as we have sometimes followed other schemes, whether for our own convenience or because there is some other rational method of grouping the profiles (e.g. CAT 5804).

The fourth pair of digits gives the position of the profile in the sequence.

The panel just below, (b), contains a number of abbreviations indicating the general nature of the test e.g. Z (A, F, V) PG - AW - MHT - SHT.

i.e. Zero (adverse, favourable, varied) pressure gradient -
 adiabatic wall - moderate heat transfer - severe heat transfer.

Brackets round the abbreviation imply that the appropriate comment should be given relatively less weight. Thus in CAT 7201, the main ZPG - APG - FPG sequence is supported by some additional ZPG data.

Panel (c) in the top left hand corner shows a sketch of the geometry of the test section. We have made no attempt to represent the proportions of the test area - the sketch is intended only to give an instant impression of the nature of the experiment. The actual test stations are indicated by asterisks, arrows, or if there are several stations, by a line parallel to the test surface.

The central panel at the top, (d), outlines the principal dimensionless parameters of the test. The values are only approximate, the precise data being given as a table in section B. The Reynolds number selected for this rapid assessment panel is that based on free-stream properties and momentum thickness, as it was felt that this, whilst not necessarily the most important, would be that most readily interpreted by the greatest number of users.

The panel below, (e), gives an indication of the type of tunnel and the test conditions. Where the tests were made on one of the tunnel walls, the "width" W refers to the test wall, regardless of the vertical orientation of the test section. Again, numerical values are approximate and the user should refer to subheading 1 below and the tabulated data of section B.

The bottom panel (f) gives, in full, a reference to what was, for us, the principal source. This is usually a source with full data tabulation, but in many cases we received the data as a private communication. Supporting references are given only by author / year, and are given in full in the reference list. We have used many of these to fill out the description, and frequently users will find some of these supporting sources more readily accessible, though possibly lacking some tabulated data. We have tried to adopt the convention that the use of the word and - underlined - implies that that source was essential for the completion of the entry, while if we write also, the sources in question are alternatives, or contain comment or an extension of the experiment under consideration.

3.4 Description of the experiment

The index marks to the left of the text in this section are those listed in § 3.2 above, and used throughout the entries. We here discuss the content of each subsection, and define the abbreviations used. Throughout, the mark (E) implies that the figure given or statement made represents an estimate by the editors.

- 1 Description of test section: A general description of the means by which the test flow was produced and observed. The geometry and dimensions of the section are specified where possible, frequently with the aid of the authors' tabulations, and include a statement of the zero for the longitudinal coordinate X. The start of the actual test-measurement area is specified and the way in which probes and other instruments were inserted in the flow. An author's description of a flow region as, for example, "uniform flow" had to be accepted. The wall roughness and waviness are given when known.
- 2 Flow quality: The authors' statement of the uniformity of the test flow in the free stream.
- 3 Transition: Description of the means, if any, used to force transition, and of any tests made by the authors to confirm the fully turbulent nature of the boundary layer.
- 4 Upstream history: Description of the mean-pressure history and wall-temperature history of the flow upstream of the test area, supported or replaced by authors' tables where possible. Also any other upstream information such as a selection of incomplete upstream profile data.
- 5 Tests for two-dimensionality of the boundary layer: Authors' statement, or description of any tests made to check the uniformity of the boundary layer in the crossflow (Z) direction:
- 6 Wall measurements: Nature of and means used to determine quantities at measuring stations fixed in the wall. The sequence and abbreviations used are:
 PW - Wall static-pressure holes with dimensions if possible.
 TW - Wall temperature sensors.
 TAUV - Skin-friction measuring devices such as floating element balances (FEB), Preston tubes, or other surface Pitot tubes such as Stanton tubes.
 Q - Wall heat-flux sensors.
- 7 Probes employed: A description of the sensing devices used for boundary-layer profiles. Where the probes are of the more usual patterns the principal dimensions may be given in a table. In other cases they will usually be described in the sequence below, which is here used to define the geometry and dimensions of the "normal" types.

TTP - Total temperature probes

STP - Stagnation temperature probe of the vented Pitot family. A thermocouple is placed in a vented cavity sensing the air temperature at low velocity after a nominally adiabatic compression. Symbols used for the dimensions are d_1 = outside diameter, d_2 = inside diameter of opening, l = length of parallel or near-parallel section.

ECP (equilibrium cone probe) - equilibrium temperature probe in which the tip of the probe is thermally isolated from the support. A thermocouple records the equilibrium temperature of the isolated tip.

Symbols used for the dimensions are:

- α - cone semi-included angle
- d_1 - base diameter of cone
- d_2 - diameter of support
- l - length of cone support

FWP - fine wire probe in which a thermocouple junction at the centre of a fine wire, set normal to the mean flow, records the equilibrium temperature of the wire. The dimensions given are d - the wire diameter, b - the length of the fine wire, and l - the length of the slender supports for the wire. Where possible the thermocouple materials are stated.

TPP - Total pressure (Pitot) probes

CPP - circular Pitot probe. The symbols used are d_1 - the outside diameter, d_2 - the inside diameter and l - the length of the parallel or slender section of the probe.

FPP - flattened Pitot probe. The symbols used are h_1 - the overall height, h_2 - the height of the opening and l - the length of the slender portion of the probe.

SPP - Static pressure probes

CCP - cone-cylinder probe. The symbols used are α - cone semi-angle, d - cylinder diameter, l_1 - distance from cone tip to static holes, θ - the angle between static holes, and l - the length of the cylinder.

HWP - Hot wire probes, CC - constant current or CT - constant temperature.

- 8 Relative position of measuring stations: The number and longitudinal position of the profile measurements is given first. The X value is to an arbitrary local co-ordinate zero, usually on the centre line and at the X value of the tip of the Pitot probe used. A tabular presentation of the X and Z values, relative to this local zero, may follow for the measuring stations of, in order, PO, TAU, Q, PW, TW, TO, P. The last two entries refer to total temperature and static pressure profiles, and an additional entry ΔY may be given indicating the relative position of the probe: normal to the wall.
- 9 Interpolation procedures and assumptions used by the authors. Notes on the means used by the authors to reduce measured data obtained from a number of neighbouring stations to equivalent, presented, data for a single X - Z station. Authors' assumptions in data reduction.
- 10 Corrections applied to profile data: Corrections for low local Reynolds number, rarefied gas, shear-displacement and wall-proximity effects may be applied to measured probe data. A general description of these is given, with, where possible, an indication of the order of magnitude involved.
- 11 Viscosity law assumed: The viscosity law used by the authors. The most commonly used expression is "Sutherland's law", but at the low temperatures which are found in the free stream of hypersonic test flows, this may be substantially in error. In comparing published R THETA values with those given in section B, readers should bear in mind that we have evaluated viscosity as described in subsection 5.1.
- 12 Selection of data and assumptions used by the editors: A source will often present redundant data. The profile data selected for computation are listed in the computer printout, but any special difficulties or procedures are remarked here, as are any assumptions introduced by the editors in processing the data.
- 13 Profiles presented: For the simpler cases, a general description of the sets of profiles which are tabulated. Where it is more convenient, a table may be used to show which governing variables have been changed. The accent is on the gross differences between sequences, as all relevant variables are tabulated in Section B. In describing a sequence, the abbreviation NX refers to the number of successive X-stations.
- 14 Wall data presented: An account of the wall data in the tables and a note of any procedure used by the editors to relate the profiles to such information.
- § DATA: The description will finish with a straightforward listing of the terminal profile numbers of the data sets, and an abbreviated description of their nature. We list here only measured data - wall data deduced from the profiles do not qualify.
- 15 Editors' comments: In § 1 - 14 we have tried to avoid making any statements which we could not support by appeal to the source, or correspondence with the author. Here we remove that restriction and comment on the experiment, incorporating our own prejudices. Some of the recurrent themes are discussed in § 4 below.

3.5 Section B - Tables of profile boundary conditions and evaluated data.

The heading of a page in this section is arranged so:

RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW	PD
X *	POD *	PW/PD *	RED2D	CQ *	H32	H32K	TW *	TD
RZ *	TOD *	SW *	D2	PI2	H42	D2K	UD	TR

An asterisk against a quantity in the heading indicates that it was one of the input values.

The symbols are defined in the list of symbols (v) and/or in the list of abbreviations (iv) so that only the less usual quantities are remarked here.

RUN - is the full 8-digit identification of the profile.

The "D" state is the arbitrary boundary layer edge state.

SW - the nominal value of $(\partial\theta/\partial x)/(\partial v/\partial x)$, where θ is the flow inclination and v the Prandtl-Meyer angle, is a number indicating the relative importance of simple waves (curvature) and reflected waves in a pressure gradient.

CQ - is a heat transfer coefficient. We give heat transfer data as the coefficient $\dot{q}_w/(\rho_\delta c_p U_\delta T_{0\delta})$. We have preferred this form to the rather commonly met Stanton number as the value of the latter depends on the value of the recovery temperature assumed. Except in ideal conditions it is not possible to evaluate the recovery temperature with any certainty. Users may form their own heat transfer coefficient as they wish from the value of CQ.

PI2 - is the pressure gradient parameter $(\delta_2/\tau_w) (\partial p/\partial x)$, where δ_2 is the momentum defect thickness. This has usually been obtained by manual interpolation and/or differentiation and so is not to be regarded as being a precise value.

H42 - is the ratio of the total enthalpy defect thickness to δ_2 .

K - indicates an "incompressible" or "kinematic" integral quantity

RZ - INFINITE - implies a nominally planar flow.

NM - means "not measured" or "not available".

NC - means "not calculated", though the necessary information is available.

3.6 Evaluated data using a pressure-based reference flow.

In § 4.6 we give a brief account of the causes of normal pressure gradients in high-speed boundary-layers. The effect results in the main from streamline curvature, but whatever the cause, the normal definitions of boundary-layer integral thicknesses break down in the presence of a significant pressure gradient. The difficulty is best illustrated by an example, and we derive here a "true" value of the displacement thickness for a flow with streamline curvature.

We suppose that we have a known supersonic flow outside an axisymmetric boundary layer. We define the transverse curvature of the wall, RZ, written as R below, as positive for an external flow and negative for internal flows such as nozzles. Then an inviscid flow field can be calculated by the method of characteristics which in principle is determinate and fills the whole space occupied by the boundary layer, though possibly the wall may not be a stream surface of this flow. We will see below that it is only the outer part of this region which is important. We will call this flow the reference flow, and denote its local density and velocity values by ρ' and U' .

We then define the displacement surface as a stream surface of this reference flow, such that the mass flow between any surface in the free stream and the displacement surface is equal to the mass flow in the real viscous flow contained by the chosen free stream surface and the wall. This is in essence the normal definition, and gives the equation:

$$\int_0^h \rho U (R + y \cos \alpha) dy = \int_{\delta^*}^h \rho' U' (R + y \cos \alpha) dy \quad (3.6.1)$$

where h is a value of y greater than the boundary layer thickness, α is the inclination of the wall

surface to the axis and δ^* is the distance of the displacement surface from the wall. From this it can be seen that values of ρ' and U' for $y < \delta^*$ do not affect the result. The equation can be rearranged as

$$\int_0^{\delta^*} \rho' U' \left(1 + \frac{y \cos \alpha}{R}\right) dy = \int_0^h (\rho' U' - \rho U) \left(1 + \frac{y \cos \alpha}{R}\right) dy \quad (3.6.2)$$

If there is no normal pressure gradient, $\rho' U'$ are constant at the free stream value and the equation reduces to

$$\delta^* + \frac{\delta^{*2} \cos \alpha}{2R} = \int_0^h \left(1 - \frac{\rho U}{\rho' U'}\right) \left(1 + \frac{y \cos \alpha}{R}\right) dy \quad (3.6.3)$$

which corresponds to the normal definition but taking full account of transverse curvature. [In a hypersonic nozzle flow, δ^* may be of order $0.5 R$ so that the second term becomes significant. The only catalogue entry for which the authors took full account of transverse curvature is CAT 7206 - Kemp & Owen. They solve the quadratic (3.6.3) for δ^* , but the resulting defining equation appears very unfamiliar (see eqn. 5.13) when compared with the usual planar definition. We have therefore left eqn. (3.6.3) as it stands. Kemp & Owen, however, have not taken account of the strong normal pressure gradient effects in their experiment, as a result of which ρ' would vary by as much as a factor of two, so that a proper calculation would require the use of eqn. (3.6.2).]

When ρ' , U' are not constant, it becomes necessary to solve for δ^* as a limit in the original form of equations (3.6.1/2). The values of ρ' , U' for $y < \delta^*$ do not affect the answer, but we do not know the value of δ^* until we have completed the calculation.

Once the δ^* -surface has been found, it is possible to define rational defect-thicknesses for momentum, kinetic energy and total enthalpy by finding the difference between the flux of the quantity in question in the reference flow, as bounded by the δ^* -surface, and the actual flow as bounded by the wall. We have not done this here as we are still working on the interpretation of data in this form.

In all the foregoing, it has been assumed that the property values of the reference flow, ρ' , U' , T' etc. were known. This is usually not the case, and it becomes necessary to deduce, so far as possible, the property values from the experimental results in the boundary layer. We have adopted the device of assuming that the reference flow is adequately represented by an isentropic flow which expands from the free stream reservoir pressure to the local static pressure in the boundary layer. This amounts to the assumption that the isobars in the boundary layer represent an extension of the isobars of the free stream as they would be extended in an inviscid flow. The simple wave data we have inspected in detail so far (CAT 7101, Sturek & Danberg, CAT 7105, Beckwith et al., CAT 7001, Fischer et al.) suggest that the free stream pressure distribution can be extended in to the δ^* -surface without introducing too great error. Within that surface, the differences between a pressure based reference flow and an extended characteristics calculation will become large, but in principle this does not matter if proper integral thickness definitions are used. There is a detailed examination of the influence of the boundary layer on the wave structure associated with pressure gradients in the papers by Myring (1968) and Myring & Young (1968). Their analysis suggests that the isobars in the boundary layer will, in a simple wave, lie close to the local Mach lines, and this leads to broadly the same conclusions.

We have therefore presented, where appropriate, a value of δ^* , D STAR, calculated from eqn. (3.6.2) using the pressure based reference flow as an approximation to $\rho' U'$ (eqn. 3.7.5). Properties and quantities so derived are marked by a subscript p - as $\rho_p U_p$. Because of a remaining uncertainty as to the proper scaling variables to use for definitions of the defect thicknesses, we have not here presented equivalent calculations for momentum thickness, etc. We have however calculated improperly defined quantities which are, ostensibly, in some measure equivalent. The main justification for this is that these integral quantities are in use (see the source papers of CAT 6401/6503/7001/7101/7304 and McLafferty & Barber (1959, 1962), Kepler & O'Brien (1962), Hoydysh & Zakkay (1969) for various approaches to the problem). Their principal virtue is that the values of the integrals in question are insensitive to the choice of the boundary layer edge point, but since the reference flow in all cases extends to the wall rather than the displacement surface, they tend to overestimate the defect of momentum or energy flux.

The integral quantities in question are listed in an addition to the tables of Section B, the table heading appearing so:

RUN	D2PD	H12PD	H32PD	H42PD	RED2PDD	RED2PDW	D STAR
	D2PW	H12PW	H32PW	H42PW	RED2PWD	RED2PWW	

The defining integrals are listed in § 3.7, and the manner of forming the Reynolds numbers is indicated by the last letter, as for the two forms of RED2 in the main tables. We have introduced a $\delta_n^2/2R$ term on the left hand side of the defining equations (3.7.6-9) in an attempt to allow for the axisymmetric correction represented by the $\delta^2/2R$ term in equation (3.6.3), for the constant pressure case. Further work is needed, however, before it is safe to conclude that this is a reasonable procedure in the normal pressure-gradient case.

A comparison of the value of D STAR with the value of D1 from the main tabulation will give an estimate of the significance of normal pressure gradient effects.

3.7 Defining equations for integral thicknesses

i) Thicknesses appearing in, or implicit in, the main tables of Section B.

The defining equations take full account of axisymmetry, but it is assumed that the inclination of the test surface, α , to the axis is small enough for $\cos \alpha$ to be taken as 1 without introducing significant error.

The reference flow properties are assumed constant and set equal to the properties at the D-state point, indicated by subscript δ .

Displacement thickness D1 or δ_1 , or (δ^M)

$$\delta_1 + \frac{\delta_1^2}{2R_z} = \int_0^\delta \left(1 - \frac{\rho U}{\rho_\delta U_\delta}\right) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.1)$$

Momentum defect thickness D2 or δ_2 or (θ)

$$\delta_2 + \frac{\delta_2^2}{2R_z} = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left(1 - \frac{U}{U_\delta}\right) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.2)$$

Kinetic energy defect thickness D3 or δ_3 or (ϵ)

$$\delta_3 + \frac{\delta_3^2}{2R_z} = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left(1 - \frac{U^2}{U_\delta^2}\right) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.3)$$

Total enthalpy defect thickness D4 or δ_4 or (δ_H)

$$\delta_4 + \frac{\delta_4^2}{2R_z} = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left(1 - \frac{T}{T_\delta}\right) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.4)$$

(Here as elsewhere in the catalogue, the fluid is assumed to be a perfect gas, so that the total enthalpy is $c_p T_0$)

The transverse body radius RZ is defined as positive for external, negative for internal, flows.

The "Kinetic" integral thicknesses D1K - D3K are defined by the above equations but with the density ratio ρ/ρ_δ set equal to one throughout.

The values of D1, D3, D4, D1K, D3K are not printed explicitly, but are given by the shape factors H12 (= D1/D2), H12K (= D1K/D2K) etc.

(11) The "true" displacement thickness D STAR as defined in § 3.6. Here full account is taken of axisymmetry except that $\cos \alpha$ is again taken as one.

The reference flow, $\rho'U'$ etc., is calculated on the assumption, discussed in § 3.6, that the pressure-based reference flow adequately represents an extension of the free stream flow for $y > \delta$. The property

values are calculated assuming that the reference flow has expanded isentropically from the free stream reservoir state, assumed constant, to the local measured static pressure. Values so calculated are written ρ_p, U_p etc.

The displacement thickness D^* STAR or δ^* is then found by interpolation between the experimental steps in y from the equation:

$$\int_0^{\delta^*} \rho_p U_p \left(1 + \frac{y}{R_z}\right) dy = \int_0^{\delta} (\rho_p U_p - \rho U) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.5)$$

(iii) Other integral quantities calculated using the pressure-based reference flow.

These are integral thicknesses used by various authors on the grounds that in the absence of a normal pressure gradient they reduce to the constant reference flow expressions (3.7.1 - 3.7.4). They are so formulated that it is not necessary to specify a D-state, so long as the D point is at sufficiently large y .

We have included the transverse curvature correction term in the integrals, and introduced a $\delta_n^2/2R_z$ term on the left hand side as an approximation corresponding to the correct term which appears for the constant pressure case in equations (3.7.1-4). Equation (3.7.5) reduces to (3.7.1) if ρ_p, U_p are constant, but the quantities listed here do not retain their supposed physical significance, and we have not felt therefore that it was worthwhile to refine the definitions further until we have fully analysed their meanings.

The definitions require scaling quantities, which may be evaluated at the wall or at the edge point. These are properties of the pressure-based reference flow, and are indicated by double subscripts. Thus U_{pw} and $U_{p\delta}$ are the velocities of the reference flow at the wall and at the boundary layer edge.

D1P has certain likenesses to the displacement thickness

$$(\rho U)_{pw} \left(D1PW + \frac{(D1PW)^2}{2R_z} \right) = (\rho U)_{p\delta} \left(D1PD + \frac{(D1PD)^2}{2R_z} \right) = \int_0^{\delta} (\rho_p U_p - \rho U) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.6)$$

D2P is related to the momentum defect thickness

$$(\rho U^2)_{pw} \left(D2PW + \frac{(D2PW)^2}{2R_z} \right) = (\rho U^2)_{p\delta} \left(D2PD + \frac{(D2PD)^2}{2R_z} \right) = \int_0^{\delta} \rho U (U_p - U) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.7)$$

D3P is related to the kinetic energy defect thickness

$$(\rho U^3)_{pw} \left(D3PW + \frac{(D3PW)^2}{2R_z} \right) = (\rho U^3)_{p\delta} \left(D3PD + \frac{(D3PD)^2}{2R_z} \right) = \int_0^{\delta} \rho U (U_p^2 - U^2) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.8)$$

D4P is related to the total enthalpy defect thickness

$$(\rho U T_o)_{pw} \left(D4PW + \frac{(D4PW)^2}{2R_z} \right) = (\rho U T_o)_{p\delta} \left(D4PD + \frac{(D4PD)^2}{2R_z} \right) = \int_0^{\delta} \rho U (T_{op} - T_o) \left(1 + \frac{y}{R_z}\right) dy \quad (3.7.9)$$

(Note - $T_{op} = T_{o\delta}$ and is constant, so that $D4PD = D4$)

3.8 Section C. Tables of Profile Data

The printed tables associated with the entries provide only a sample of the total data collection, the full tables being given in the accompanying microfiche, and also recorded on magnetic tape. For access to the recorded data bank, please follow the instructions given in the Foreword (iii).

Each profile is headed by the full 8-digit profile identity, and the data tabulated are:

I, Y, PT2/P, P/PD, TO/TOD, M/MD, U/UD, T/TD, (RO/ROD) (U/UD)

I is the Y-station identity.

The next four columns represent the quantities most likely to be obtained fairly directly from experimental work, while the last five, with P/PD, are generally the most useful for analysis.

At the foot of each profile table there is a short statement listing the variables used as input to the programme and the assumptions made in completing the table. The remark "van Driest" means that the temperature distribution T/TD was determined according to a temperature-velocity relationship, given in subsection 5.3. If there is a remark "trapezoidal rule" the characteristic boundary layer thicknesses were calculated according to this integration procedure.

Instructions for handling the data as recorded on magnetic tape will accompany any copy that is made.

3.9 Section D. Supplementary data

A source often provides additional data which cannot be presented as part of sections B and C. Typically, this might be skin friction or heat transfer data for X-values other than those of the profiles, additional temperature probe data, or tables of fluctuation quantities. It will frequently be presented as a facsimile of the tables in the source when it will bear a label:

FACSIMILE FROM SOURCE PAPER - NB - AUTHORS' SYMBOLS AND UNITS.

The symbols and units will be defined, where appropriate, either on a heading page, or by superposed notes on the facsimile. The tables of this section will usually appear last, but occasionally, for printing reasons, will be attached to section A.

3.10 Closing remarks

We have tried to produce a standardised method of description which is nevertheless sufficiently flexible to cover most boundary layer investigations. We cannot claim that our format is a complete answer to the problem, but would implore any reader of these notes to make sure that any report he publishes should at least provide answers to the questions implied by 1 - 11 of Section A (§ 3.4). Ideally we would like writers to follow our own system, at least in indexing the material points as we have. Since the key numbers do not have to appear in sequence, any number may be added!

We also feel that merely to have provided data for sixty experiments in the same form allows us to make a general appeal to experimenters who are processing data. We beg any worker in the field to keep permanently, or to ensure that some agency keeps, a functionally complete record of his data, preferably in computer-digestible form, and preferably in a form consistent with that used here.

4. GENERAL POINTS IN THE "EDITORS' COMMENTS"

The description of the experiment which forms section A of each entry is concluded by § 15 - the "Editors' comments". Any user reading through these in rapid succession will soon realise that not only is there a large measure of repetition in these comments, but that we have tended to emphasise some features which interest us particularly, or which have caused us trouble in the overall presentation of the data. A reader will also note that we have introduced a certain amount of our own jargon, and that this is used not only in § 15 but appears frequently in the main body of Section A. The remarks made here are intended to enlarge upon, and explain, our preoccupations.

4.1 Remarks relating to the "quality" of the data

We obviously feel that we should, where appropriate, make general observations on the "quality" of the data. In a field for which experimental methods so often require the use of (sometimes complex) calibration procedures, it would be a brave man who commented too severely on any possible systematic errors. We would merely remark that the likely accuracy of any measurement, other than Pitot and wall static measurements in not-too-severe conditions, is very much less than the attainable precision or repeatability. We have not therefore made any assessment of quality on the basis of our appreciation of the likely error margin of the instrumentation used, but rather have inspected the evidence available to us in the form of automatically printed graphs of the velocity profiles in transformed coordinates. Regardless of the geometry, thermal state, and history of the test layer, these were prepared using a slightly modified Van Driest (1951) transformation, according to Fernholz (1969) and compared to the law of the wall, with the constants after Coles (1956) and the outer region correlation of Fernholz (1969). Where no CF value was given, we used an empirical correlation based on that reported in Fernholz (1971). On the evidence of these graphs we have felt free to comment on the degree of scatter visible in the profiles, and also, when the governing conditions were appropriate, on the extent to which the data matched our expectations in such features as the extent and slope of the log-law and the size of the "wake component" in the outer region.

The amount of data for each profile also contributes to the "quality". In general we feel that a profile should be described by at least 20-30 points, and have commented if the data fall "short" of this. But even this comment may not be sufficient for the reader since it does not say whether the data is spread evenly across the boundary layer or - as is often the case - is obtained mostly in the outer layer. If the data show very little scatter, the number of points is of less importance, but an even distribution is important.

4.2 Reliability of integral values

We have regularly commented on the relation of the innermost data point to the "momentum deficit peak". The integrands of D2, D3 and D4 all display a maximum, which may occur very close to the wall. If the data points do not describe this maximum, or "peak", it is not possible to evaluate the integral with much confidence, and the user should not place too great emphasis on the numerical values given in the tables of section B.

It is, in fact, very common for data to be defective in this particular. When considering older sources for which the evaluation of data was made by hand, this difficulty was probably overcome by a reasoned filling-in of the data near the wall. Later data, evaluated by computer, may or may not have had an inner region interpolated. In some cases we have found noticeable differences between the authors' D2 values and our own, which we have provisionally assigned to this cause, but since in general the source papers do not describe the integration procedure used, we cannot be certain. We have not performed any such inner region patching ourselves, as we feel that the way in which it is done must depend strongly on the preconceptions of the person doing it. Some further remarks about integration procedures and the experience we have had with them will be found in chapter 5.

4.3 Temperature values near the wall

In most experiments where total temperature measurements are made, the temperature probe is physically

much larger than the Pitot probe, so that Pitot data are available in a region next to the wall for which there are no temperature measurements. In general, the experimental worker reduces data in this region with an inter-/extrapolated temperature value, but does not necessarily report the method used. If the total temperature distribution is extended to meet the wall temperature, the resultant error is unlikely to be serious unless the wall is very strongly cooled. Interpolations based on static temperature, and extrapolations made with no matching to the wall temperature are likely to be much less reliable.

We are aware that we have not checked every entry to see whether interpolation has taken place, and would recommend that any user intending to refine arguments on the details of the temperature distribution close to the wall should compare the lower values of y with the radius or half-height of the temperature probe used.

A commonly presented temperature-velocity correlation, in which $(T_0 - T_w)/(T_{0D} - T_w)$ is plotted against U/UD , is particularly sensitive to small variations of temperature near the wall, so that caution should be exercised in drawing conclusions as to the significance of apparently widely different temperature-velocity relationships, particularly for experiments in which heat-transfer was not severe.

4.4 Wall data deduced from profile data

We have on a number of occasions presented values of CF and/or CQ as deduced by the authors from the profile data. We would like to emphasise here, as we have intermittently in § 15, that we do not regard such values as data. In the absence of measured values, we feel that there is a justification for giving such deduced wall coefficients, as they are often required for theoretical developments. If the value presented is derived from a profile gradient very close to the wall, it is inherently exceedingly unreliable. If it is deduced by matching the whole profile to, for instance, a transformed version of the Coles' wall and wake law, the degree of fit can be stated statistically, but the reliability of the numerical value is only as good as the assumption that the wall- and wake-law description applies, and applies with the "universal" log-law constants in the particular circumstances of the experiment.

4.5 The boundary layer edge

The selection of a "D-state" point, which is then treated as the boundary layer edge state, will be discussed in the forthcoming commentary volume. A preliminary discussion may be found in Fernholz & Finley (1976). The variation of flow properties near the boundary layer edge may result from either the (asymptotically vanishing) influence of the boundary layer itself, or from variations of the free-stream flow, most obviously manifest as normal pressure gradients. In general the point selected is arbitrary, and the criteria used to guide selection are so various as to permit of variations in the Y -position of the D-point of 60 % or more. Where we feel this might have a real significance, as for instance for the experiments including fluctuation measurements (CAT 5803/7205/7403) we have commented on it in § 15. For the entries as a whole, we have followed no particular rules. If the author appears to have made a self-consistent D-point-selection, we have usually accepted it. If we have taken special measures (c.f. CAT 5901) we have remarked on them in § 12. We have throughout been guided in our action by a calculation of the local value of the total pressure, and would recommend, for future use, that the D-point be set at the Y -value for which $(P_0 - P) = 0.99 (P_{0E} - P)$. For low speeds, this is the U_{995} point, while at hypersonic speeds it reduces, effectively, to the point where $P_0 = 0.99 P_{0E}$.

4.6 Normal pressure gradients

In § 6 below, we describe how the entries have been classified on the basis of the local pressure gradient. We place particular emphasis on the existence, or otherwise, of a gradient normal to the wall. If such a gradient is at all marked, then it becomes very difficult to make any rational calculation of the integral thicknesses or to decide where the boundary layer edge is. (See the discussion of D STAR in § 3.6 above, and the initial treatment of the problem in Fernholz & Finley, 1976.) We therefore distinguish between the types of pressure gradient which are observed on the basis of their origin and mode of propagation.

Normal pressure gradient effects may result from:

- i) Wall curvature, so that the mean flow streamlines are curved and a normal pressure gradient is required to provide the centripetal acceleration. Typical cases are the two-dimensional ramp flow of Sturek & Danberg (CAT 7101) or the various contoured nozzle experiments (CAT 7001/7105/7206). The strength of the normal component is given approximately by

$$(\partial p / \partial y) \approx \pm (M^2 - 1)^{1/2} (\partial p / \partial x) \quad (4.1)$$

and in an ideal flow the effect propagates as a simple wave. The isobars are the local Mach lines (Prandtl-Meyer fan, focussed compression etc.).

- ii) Streamline divergence, so that a line normal to the wall does not intersect straight streamlines away from the wall at right angles. The isobar, on the other hand, is everywhere normal to the streamlines and so curves away from the profile normal. Such a flow would be observed in a pure conical expansion when the strength of the normal pressure component in inviscid flow is given approximately by

$$(1/p) (\partial \gamma / \partial y) \alpha = - (1/y/R^2) M^2 (M^2 - 1)^{-1} \quad (4.2)$$

where R is the radius from the source of the conical flow, y is the distance normal to the solid surface and 1 is 1 for planar and 2 for axisymmetric flow. The effect corresponds to a reflected wave in which the isobars run through successive equally stepped right and left running characteristics.

This effect is much weaker than that caused by a simple wave, and can usually be neglected. In practical cases where the ideal flow is not purely conical, there may be a superimposed simple wave element which swamps the reflected wave pressure gradient.

- iii) Normal components of the Reynolds stresses may become large at high Mach numbers when compared to the static pressure. The mean flow field momentum changes are then the results of a normal stress made up of comparable contributions from the static pressure and the Reynolds stress. There is little evidence which can be used to quantify the effect, but a preliminary analysis based on the results of Fischer et al. (CAT 7001) and Beckwith et al. (CAT 7105) suggests that a pressure dip may be observed in the most intensely turbulent part of the layer, of order given by

$$\Delta p / p_w \approx 3 \gamma M_\infty^2 c_f \quad (4.3)$$

This topic will be developed further in the commentary volume.

- iv) Changes in longitudinal pressure gradient can give rise to substantial normal pressure gradient effects, even on a straight wall. This is, in effect, because the pressure gradient in a reflected wave region is generated elsewhere in the flow, so that there may be substantial regions away from the straight wall in which the incident and reflected waves are simple in character. Figure 4.1 shows an ideal flow field in which expansion is reflected at a straight wall. On the wall, from a to b, there is no pressure gradient, but an expansion fan generated on the other side of the experimental channel is being propagated towards the wall, and causes a negative pressure gradient at the wall from b to c. The region bcd is a "reflected wave region" in that the normal components of the incident and reflected simple waves oppose, while their longitudinal components reinforce. Along the wall abc no normal pressure gradients would be observed in a boundary layer of infinitesimal thickness. However, a traverse made over a finite range of y at AA would be made in an exclusively simple wave region, and traverses just upstream or downstream of AA would inevitably experience simple wave effects sufficiently far from the wall. The dashed arrows show the pressure gradient vectors involved, and taking due account of the reinforcement of the longitudinal pressure gradient in the region bcd it is apparent, from equation (4.1), that the normal pressure gradient on the line AA is given by

$$(\partial p / \partial y) = 1/2 (M^2 - 1)^{1/2} (\partial p / \partial x \text{ along bc}) \quad (4.4)$$

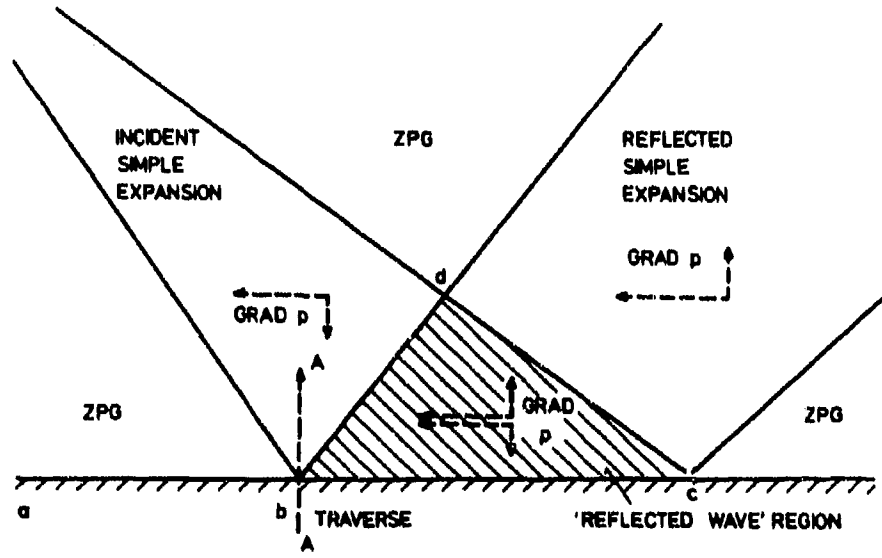


Figure 4.1 Normal pressure gradient effects near a change in longitudinal pressure gradient.

5. DATA PROCESSING

Figure 5.1 shows a flow diagram of the computer programme used to handle the data. We do not claim that it is elegant, or even efficient. It has grown naturally over the years, and we have never found the time to redesign it from scratch. The first version was provided by H.J. Küster and it has been adapted to the specific needs of the various entries, improved and run by Miss C. Mohr. We have not provided here a full listing as the programme is not inherently interesting and the details should not affect users in any significant way. The editors will provide a more detailed description on request.

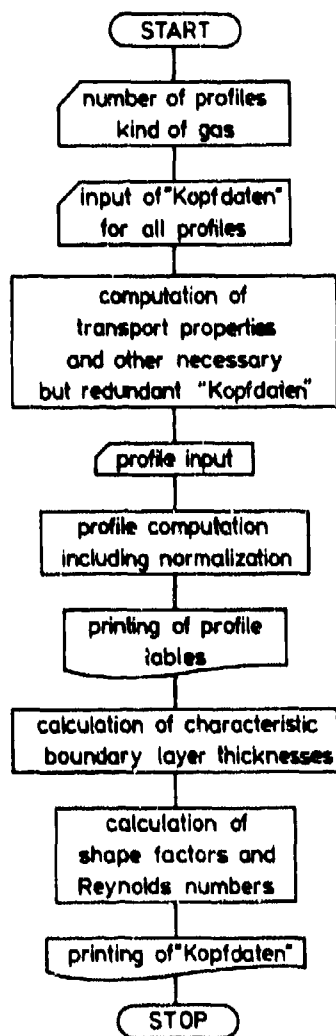


Fig. 5.1 Flow diagram of computer program

The purpose of the programme is to handle published data, as reduced by the original authors, and present it in standard form. In the discussion below we therefore lay most emphasis on the data input, the input of transport properties for the working gas and calculation procedures where we did anything unusual or experienced difficulties.

We use throughout this chapter the word "Kopfdaten" to describe all those quantities which in principle appear at the head of a profile table. The word is not elegant but has no short easily understood equivalent.

5.1 Properties of the working gas, recovery factors

There were only three gases used in the experiments described in the catalogue - air, nitrogen and helium. In some facilities the reservoir temperatures were high enough for the vibrational modes of the diatomic gases to become significantly excited. Very occasionally pressures were high enough for the compressibility factor (pv/RT) to depart detectably from one. In data processing we have ignored these real-gas effects and treated the working fluid as a perfect gas with constant specific heats. This may result in some falsification of the relationship between the free stream static state and the reservoir state, but will not introduce significant error in the inter-relationships between static properties and velocities etc. in the test region if the data input is selected from these variables.

The perfect gas properties assumed are:

Gas:	air	nitrogen	helium
Gas constant R in $m^2/s^2 K$:	287.1387	296.50	2078.739
Specific heat ratio γ :	1.40	1.40	1.667

The transport properties were calculated after Keyes (1952) for the diatomic gases (minor constituents of air being ignored) and Neubert (1974) for helium.

For the diatomic gases the expression

$$\mu = \frac{10^{-6} a_0 T^{1/2}}{1 + a T^{-1} 10^{-a_1/T}} \quad \text{NS/m}^2 \quad (5.1)$$

was used, where the constants and the range of validity are given as

	a_0	a	a_1	range of validity
air:	1.488	122.1	5	$79 < T/K < 1845$
nitrogen:	1.418	116.4	5	$81 < T/K < 1695$

These relations were used also at lower temperatures down to 50 K for lack of better information.

For helium the expression

$$\mu = \left[\frac{50.23 T^{0.647}}{\left[1 + T^{0.5} (T-0.3) e^{-T} \right] (T-0.3)} + e^{-T} (61.2730T^3 - 199.1754T^2 + 179.1353T - 59.05466) \right] \times 10^{-8} \text{ NS/m}^2 \quad (5.2)$$

was used, and the range of validity is $0.4 < T/K < 400$.

At present it is not possible to state a recovery factor with enough confidence to take account of upstream history effects, boundary conditions or other flow parameters. We have therefore chosen to use for all experiments a recovery factor r of 0.896, though this does not imply that we necessarily believe that there will be no heat transfer at a wall which is at the recovery temperature calculated using this. The numerical value represents the cube root of the Prandtl number for air, though a true recovery factor, if it could be defined, would of necessity be in some way a function of the shear stress distribution across the boundary layer, i. e. of the turbulence structure.

5.2 "Kopfdaten" - Boundary conditions and other evaluated data

The data quantities which we call "Kopfdaten" appear in printed tables as section B of each entry. They fall into three distinct groups. These are:

- Boundary conditions given by the authors, or calculated by us from other data given by the authors, and used by us as input for the data processing. Such quantities are marked by an asterisk in the tables.
- Calculated but redundant boundary values at the wall and the boundary layer edge.
- Characteristic boundary layer thicknesses, shape factors and Reynolds numbers RE_{D2} .

A typical input set of group (a) might consist of:

Position X, transverse radius RZ, Mach number MD, longitudinal curvature parameter SW, heat flux at the wall, which in a dimensionless form will give the coefficient CQ, static pressure at the wall PW and the boundary layer edge PD, temperature at the wall TW and at the boundary layer edge TD.

The programme then completes the calculation for the array of boundary conditions by calculating the redundant group (b) from the input values. In this case group (b) consists of:

Total pressure and temperature at the boundary layer edge POD and TOD, the recovery temperature TR, the velocity at the boundary layer edge UD and the ratios PW/PD, TW/TD.

Apart from the obvious gas-dynamic relationships, the following relations and definitions are used:

Recovery temperature TR (T_r)

$$T_r = T_\delta \left(1 + r \frac{\gamma - 1}{2} M_\delta^2 \right) \quad (5.3)$$

Heat transfer coefficient CQ (C_q)

$$C_q = \dot{q}_w / \rho_\delta U_\delta c_p T_{o\delta} \quad (5.4)$$

Longitudinal pressure gradient parameter SW indicating the relative importance of streamline curvature - nominal value of

$$SW = (\partial\theta/\partial x) / (\partial w/\partial x) \quad (5.5)$$

where θ is the inclination of the flow and v the Prandtl-Meyer angle, in principle at the boundary layer edge. In practice we have inserted nominal values of SW to indicate the importance of the simple-wave element of the pressure gradient. Thus SW = 1 for the curved wall studies, which in the test region were all either generating or cancelling a simple wave. SW was set to 0 for straight wall studies, except in one case where the pressure gradients were so severe that there was probably strong streamline curvature even within the boundary layer. For this case (CAT 7208) SW was set at 0.5.

Group (c) of the "Kopfdaten" involves the boundary layer thicknesses, and so is calculated at the end of the programme after the normalised profile data have been assembled. For cases in which transverse curvature is small (δ/R_z of order 10^{-2} or less) the definitions used are

Displacement thickness

$$\delta_1 = \int_0^\delta \left(1 - \frac{\rho U}{\rho_\delta U_\delta} \right) \left(1 + \frac{y}{R_z} \right) dy \quad (5.6)$$

Momentum defect thickness

$$\delta_2 = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left(1 - \frac{U}{U_\delta} \right) \left(1 + \frac{y}{R_z} \right) dy \quad (5.7)$$

Kinetic energy defect thickness

$$\delta_3 = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left[1 - \left(\frac{U}{U_\delta} \right)^2 \right] \left(1 + \frac{y}{R_z} \right) dy \quad (5.8)$$

Enthalpy defect thickness

$$\delta_4 = \int_0^\delta \frac{\rho U}{\rho_\delta U_\delta} \left(1 - \frac{T}{T_{o\delta}} \right) \left(1 + \frac{y}{R_z} \right) dy \quad (5.9)$$

The "kinematic" integral thicknesses for which the density variation is ignored correspond to the "incompressible" definitions

$$\delta_{1K} = \int_0^{\delta} \left(1 - \frac{U}{U_{\delta}}\right) \left(1 + \frac{Y}{R_z}\right) dy \quad (5.10)$$

$$\delta_{2K} = \int_0^{\delta} \frac{U}{U_{\delta}} \left(1 - \frac{U}{U_{\delta}}\right) \left(1 + \frac{Y}{R_z}\right) dy \quad (5.11)$$

$$\delta_{3K} = \int_0^{\delta} \frac{U}{U_{\delta}} \left[1 - \left(\frac{U}{U_{\delta}}\right)^2\right] \left(1 + \frac{Y}{R_z}\right) dy \quad (5.12)$$

where, in (5.6) to (5.12) R_z is defined as positive for flow on the exterior of an axisymmetric body and as negative in an internal flow. The inclination of the surface to the axis is assumed to have negligible effect. These equations reduce to those normally used on plane walls as R_z tends to infinity.

The above definitions hold for conditions in which the assumption of a constant reference flow is appropriate, and under those conditions (see §§ 3.6, 3.7) an exact allowance can be made for the effects of transverse curvature, even when δ is of the same order as R_z . The δ_n values calculated from equations (5.6) to (5.12) are replaced by corrected values δ_i , using the relation (cited by Kemp & Owen CAT 7206)

$$\delta_i = -R_z \left(1 + \frac{\delta_n}{2R_z}\right)^{1/2} \quad (5.13)$$

This is essentially the appropriate solution of a quadratic of the type found in equation (3.6.3) above.

It is then possible to calculate the longitudinal pressure gradient parameter π_2 (π_2)

$$\pi_2 = (\delta_2/\tau_w) (dp_w/dx) \quad (5.14)$$

Although provision was made in the programme for numerical differentiation of $p_w(x)$ so as to calculate π_2 , we have found that in nearly every case a human intelligence is needed to extract sensible values. Thus we have, so far as time allowed, obtained dp_w/dx by plotting $p(x)$ and estimating the gradient. Such values are therefore essentially imprecise, but more accurate than the machine-derived values.

The shape factors are then calculated as ratios of δ_1, δ_2 etc.

$$H_{12} = \delta_1/\delta_2, \quad H_{32} = \delta_3/\delta_2, \quad H_{42} = \delta_4/\delta_2 \quad (5.15)$$

$$H_{12K} = \delta_{1K}/\delta_{2K}, \quad H_{32K} = \delta_{3K}/\delta_{2K} \quad (5.16)$$

and the Reynolds numbers as

$$Re_{\delta_2} = \rho_{\delta} U_{\delta} \delta_2/\mu_w; \quad Re_0 = \rho_{\delta} U_{\delta} \delta_2/\mu_{\delta} \quad (5.17)$$

5.3 Profile data

Profile data reached us in many forms. The programme was designed to cope with five standard types of input, and other variations allowed for by subroutines special to each entry, or in extreme cases by conversion into a standard form using compressible flow tables and hand calculation. Most of the difficulties occurred when authors had not measured a variable and stated their auxiliary assumptions verbally or in analytic form. In particular, the static pressure variation was often fictitious and for many experiments, especially the earlier ones, total temperature was not measured.

When no total temperature profile was supplied, we assumed that the velocity and temperature were related by the expression

$$\frac{T}{T_\delta} = \frac{T_w}{T_\delta} + \frac{T_r - T_w}{T_\delta} \left(\frac{U}{U_\delta}\right) - r \frac{\gamma-1}{2} M_\delta^2 \left(\frac{U}{U_\delta}\right)^2 \quad (5.18)$$

This is a modification by Walz (1966) of van Driest's (1951) expression. When used, whether introduced by ourselves or the original author, a note appears at the foot of the profile tabulation as "VAN DRIEST".

The standard forms of input were:

1. U/U_δ , T/T_δ , $p/p_\delta = 1$. Calculate M/M_δ and ρ/ρ_δ .
2. U/U_δ , $p/p_\delta = 1$. Calculate T/T_δ (Van Driest) according to (5.18), M/M_δ and ρ/ρ_δ . Standard provision was made to deal with an author's set of U/U_δ values which had been calculated assuming that T_0 was constant (isoenergetic), and convert them to "Van Driest" values.
3. U/U_δ , T/T_δ , p/p_δ . Calculate M/M_δ and ρ/ρ_δ .
4. U/U_δ , ρ/ρ_δ , $p/p_\delta = 1$. Calculate M/M_δ , T/T_0 .
5. M/M_δ , $p/p_\delta = 1$. Calculate U/U_δ , ρ/ρ_δ and T/T_δ (Van Driest) according to (5.18).

Profile data were normalised with the boundary layer edge or D-state values. In many cases an author's set of figures was not consistently normalised, or was normalised on an exterior flow condition which was not in fact observed. In these circumstances we required that all normalised values should be 1.0 at the D-state point.

5.4 The D-state and consistency

The boundary layer edge point is a point within the boundary layer, selected arbitrarily or by the application of an arbitrary criterion. Consequently the reservoir state of the tunnel, p_{0r} , T_{0r} is not the same as the total state at the D-point. In fact we recommend (§ 4.5) as an ideal definition of the D-point, that it be set where P_0/P_{0r} is 0.99. In practice this will be found to lie at a much greater Y -value than, for instance, the U_{995} point, and there are other advantages which will be developed in the commentary volume.

In most cases one is not presented with data enough to compare the values of p_0 and p_{0r} , but where it is possible to determine the two independently, a conflict can arise. When this happens, we have calculated p_0 from the profile data for the selected D-point, and readers should not expect $p_{0\delta}$ to match the tunnel reservoir pressure, which as such does not appear in our tables. In most cases, however, $p_{0\delta}$ has been set arbitrarily equal to p_{0r} , because no other information was available.

5.5 The integration procedures

The characteristic boundary layer thicknesses δ_n were determined by one of two integration procedures: INTVAR or a trapezoidal rule. If the latter was used - which is the case for a relatively small number of profiles only - this is noted in the output at the end of the profile in question.

The standard integration procedure "INTVAR" consists of a Simpson type formula using a second order parabola and allowing a variable step size (Haase et al. (1973)). The accuracy of INTVAR is of the order $(h_1 + h_2)^3 (h_1 - h_2)$ and better than that of the trapezoidal rule. The integration procedure is started at the outer edge of the boundary layer with a linear interpolation curve as the first step. This allows a better approximation for the near wall region of the integral, avoiding the disadvantages of a straight line interpolation in this region, especially for the many cases where the measurements do not extend within or as far in as the maximum of the integrands of δ_2 and δ_3 .

INTVAR has, however, been found to be oversensitive to two special distributions of measured data points.

Its answers cannot then be trusted and we have therefore used the trapezoidal rule in these cases. One of these is when measuring stations lie extremely close together or when data are rather erratic over adjacent small intervals. In the first case averaging of the data in question cured the problem, but in the second case the reason for the deviation from the hand calculated result could not be found. The second case for which the trapezoidal rule is superior occurs when there are large gaps between measured data points. Here again INTVAR failed. Since these error sources could not be eliminated in the short time available before the catalogue deadline, all boundary layer thicknesses were checked either against the authors' values, against those obtained by the trapezoidal rule or, in a few cases, against hand calculated data.

5.6 Integral values using a pressure-based reference flow.

In § 3.6 we have briefly outlined some of the questions which arise when it is desired to calculate integral thicknesses for boundary layers experiencing significant normal pressure gradients. The quantities which we finally chose to calculate are defined in § 3.7 by equations (3.7.5) to (3.7.9).

In order to evaluate the integrals it is necessary to calculate the properties of the pressure-based reference flow from the tunnel reservoir state and the local static pressure. When the reservoir state was stated, it was read into the programme as an extra input. More generally the data available did not distinguish between the boundary layer edge state and the reservoir state, so that p_{0r} was not equal to $p_{0\delta}$. The pressure based integral values were then calculated using stored profile data from the main programme.

The solution of equation (3.7.5) for D STAR was performed using a weighted interpolation between values of the integral

$$\int_0^{y_n} \rho_p u_p \left(1 + \frac{y}{R_z}\right) dy$$

for the four experimental values of y_n which lay two above and two below δ^* .

6. NATURE AND CLASSIFICATION OF DATA

6.1 General Considerations

All the data we present were obtained in wind-tunnel studies. Inevitably, therefore, the data do not fully represent the free flight situation. Some of the defects of representation are unavoidable, and result from the essential nature of tunnel tests. For instance, it seems very probable that nearly all hypersonic data are affected in some degree by a fluctuating free stream disturbance level together with a noise level, which have no analogue in free flight. In other cases, the representation is not complete for reasons which are in principle avoidable, though an attempt at proper reproduction of the intended flow would be inherently more expensive, or less convenient, than the course actually followed. A common example is the way in which constant-pressure high Reynolds number data are almost invariably obtained on tunnel side walls. The results are then presumed to describe a two-dimensional "flat-plate" boundary layer, when they must inevitably be influenced to an unknown extent by flow convergence or divergence, and by history effects inherited from the upstream region. The most obvious history effects stem from pressure gradients or wall temperature effects. It may well be valid to use the data as though these effects were negligible, but, if this be the case, some justification is desirable.

Our intention is to provide a data pool of general utility, so that the geometries described here are all, in some degree, simplifications of any "flight" or "application" situation. In selecting the data and classifying them, we need to bear this in mind. However the data were obtained, how are they likely to be used?

There are two principal modes of use. On the one hand we have the application of data to design purposes, where the highest degree of accuracy, and the finest detail of description, are irrelevant, since the situation-match between the data-store and the proposed application is inevitably only approximate. On the other hand, we have the provision of precise and detailed data for clearly defined test-cases, not necessarily of any direct applicability, which display particular phenomena sufficiently clearly to allow of the development of calculation methods. In an ideal world, any given experiment serves both purposes, but experimental technique and turbulence theory are not sufficiently developed to allow of this counsel of perfection.

In general, data obtained in ad-hoc situations on complex geometries are not published, as the results are usually not scientifically sufficiently detailed to allow us to make useful comparisons, and the data are in any case likely to be restricted by the need for commercial or military secrecy. Most of the available data then are not only laboratory data, but are for very simple geometries, and this factor, together with the complications of handling and presenting three-dimensional data, provided a strong incentive to restrict the catalogue to nominally two-dimensional cases.

There are numerous, and inter-related, factors which affect the local characteristics of a two-dimensional boundary layer. We cannot say that one factor is more "important" than another, since in general importance must relate not only to the numerically observed influence of the factor, but to its likely range of variation. The following list therefore is in no particular order of importance, but does perhaps reflect the order in which we think of the factors.

The principal controlling parameters are:

- (i) The Reynolds number
- (ii) The heat transfer condition
- (iii) The Mach number
- (iv) The pressure gradient
- (v) The pressure and temperature history.

Of these, the first three are expressed by numerical values, which cover an essentially continuous range. It is not possible to make a distinction of type between high and low values of the quantity in question - there is a continuous gradation. We have chosen, instead, to make our classification of data on the basis, firstly, of the features of the local pressure gradient, and secondly, where, for the "zero pressure gradient" case, there is a large pool of data, on the history of the experimental boundary layer.

The classified lists of § 7 include a table⁷ giving nominal numerical values of Reynolds number, Mach number and wall temperature ratio TW/TR. The implications of classification by pressure gradient are examined below.

6.2 Classification by pressure gradient

More than half the available data describe tests made in nominally constant pressure layers (Group I) which we have subdivided firstly into cases in which the boundary layer has grown from a well-defined origin under constant pressure conditions throughout (IA). The second group (IB) contains those cases in which the layer is formed on a tunnel wall and passes through the nozzle expansion upstream of the test zone. In two cases (CAT 7202, 7301) this history is in some measure described and in one (7302) the development is so long and gradual that the boundary layer is probably fully "relaxed" so as to have the same characteristics as a flat plate layer. The experimental ranges covered by these two groups are summarised by figures 6.1 to 6.3. Cases with substantial heat transfer are relatively few, and are shown in figure 6.3. There is, in addition, a small group (IC) of cases describing the recovery of a severely disturbed layer, under local zero-pressure-gradient conditions.

The zero-pressure-gradient data form the main body of information for both the modes of use suggested in § 6.1. There is quite a wide range of available data, and it includes a few cases which have been studied in close detail - for instance CAT 7205, where the measurements fully describe the mean flow, and are supported by fluctuation measurements. Regrettably, the cases of practical interest do not generally give rise to any considerable regions of constant-pressure flow.

The pressure gradient cases have been divided on the basis of the manner in which the pressure gradient is produced. The first group (IIA) covers those flows in which a wave structure is generated somewhere else in the flow and imposed on a boundary layer flowing along a straight wall. The test layer thus passes through a "reflected wave", without significant streamline curvature. The second group (IIB) comprises those tests in which the pressure gradient is the result of streamline curvature. This is associated with a "simple wave" which may either be generated in the test-zone itself, and propagate downstream, or may be generated elsewhere and be propagated downstream so as to strike the test-zone. The wall curvature here is such as to cause the wave to be cancelled without reflection, as, for example, in the "bell" of a well designed contoured nozzle.

There is a vital physical distinction between the two cases as the curved mean flow of the simple wave cases is associated with normal pressure gradients, which at high Mach numbers become very large. There is very little available information on what effect this may have on the turbulent structure (CAT 7101 contains the only measurements of fluctuating quantities), but the effects are unlikely to be negligible. There are relatively few available accounts of simple wave flows, and this is especially unfortunate as the boundary layers on a hypervelocity vehicle will always experience locally-generated simple wave structures. The typical cases are the flow over the convex forward surface of a vehicle - a favourable pressure gradient giving rise to a generated simple wave - and the flow approaching an inlet where a concave surface gives rise to a generated simple compression wave. It seems improbable that data from reflected-wave pressure-gradient experiments can be applied very directly to these cases. Unfortunately, the reflected-wave experiments are much easier to perform.

There is a final class (IIC) intended to include cases with no longitudinal pressure gradient but a significant normal pressure gradient. Such a flow may be realised by causing an incident wave to strike a surface so contoured as to give rise, in isolation, to a generated wave of equal and opposite sign. Such an experiment has been performed (CAT 6800) and is the only case we have included in the catalogue for which no profile data is available. It is offered as a challenge to those developing calculation methods.

This classification in itself shows clearly where the gaps in our experimental knowledge lie. Boundary layers with larger longitudinal pressure gradients, with varying wall temperature, along curved walls and those recovering from a strong perturbation still await exploration. In particular, it would be desirable to perform more experiments like Thomann's (CAT 6800) but on a larger scale and including profile and turbulence measurements.

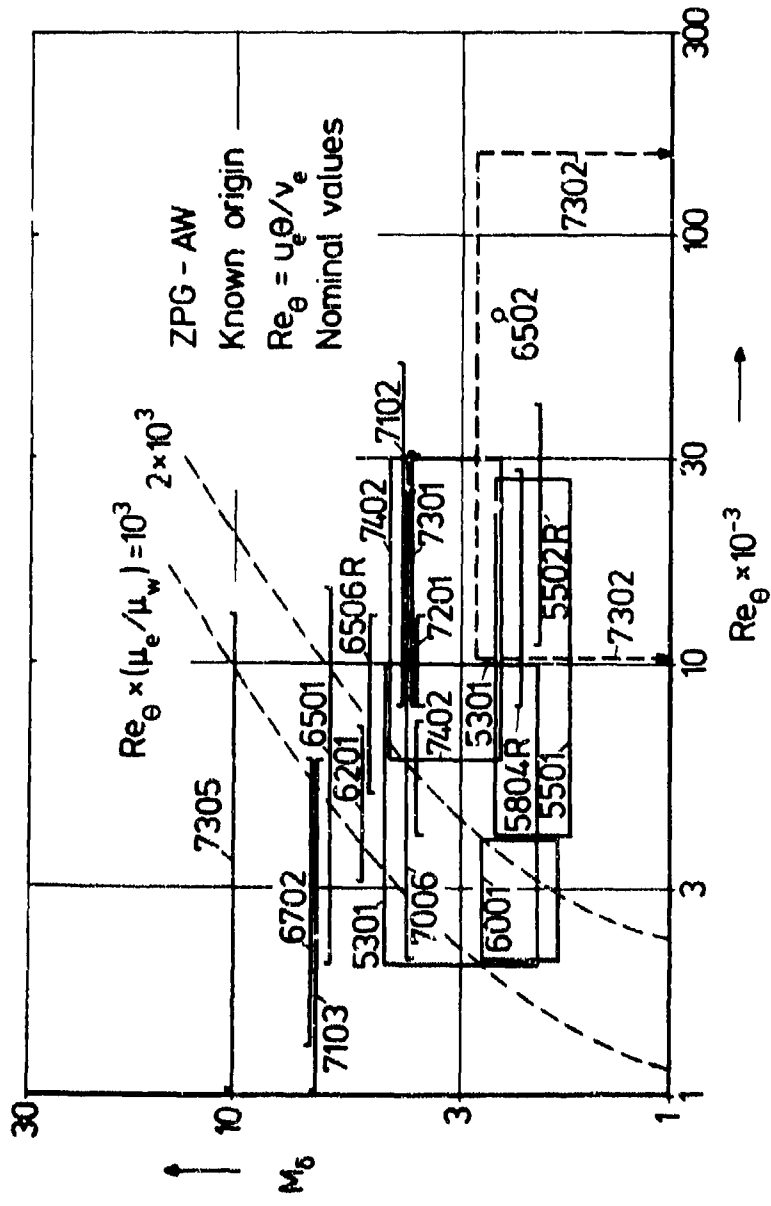


Fig. 6.1 Nominal experimental range for group IA (adiabatic cases)
 Zero pressure gradient boundary layers formed under constant pressure conditions

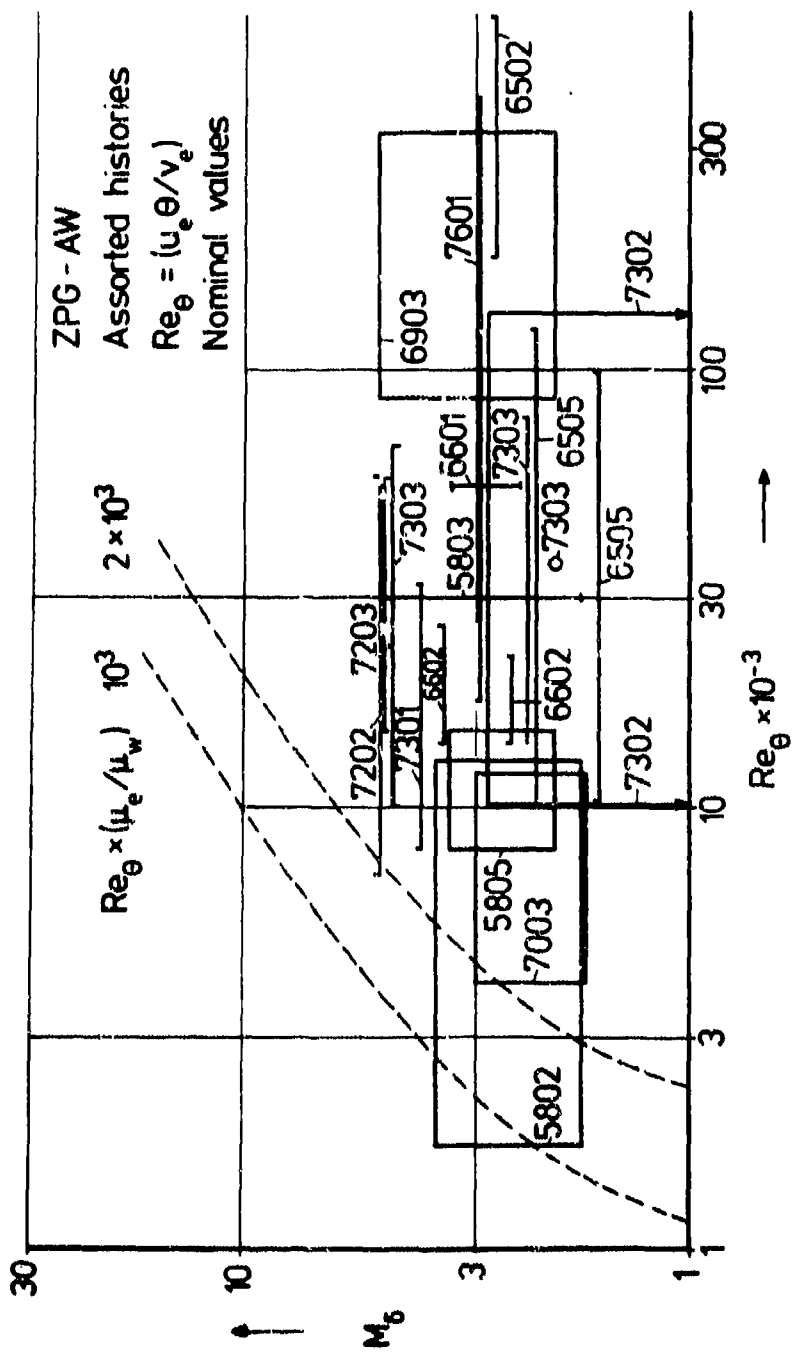


Fig. 6.2 Nominal experimental range for group IB (adiabatic cases)
Zero pressure gradient boundary layers formed on windtunnel nozzle walls

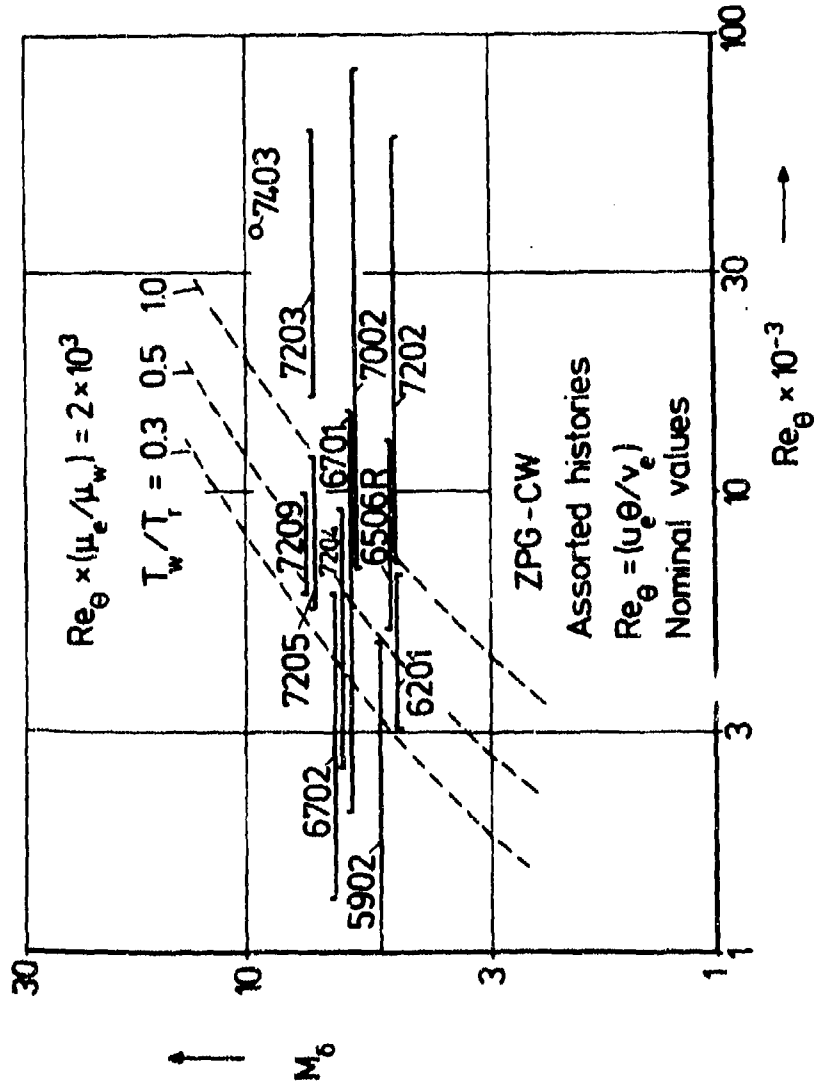


Fig. 6.3 Nominal experimental range for zero pressure gradient boundary layers with substantial heat transfer
 Both groups IA and IB - varied histories

7. CLASSIFIED LISTS OF ENTRIES

As outlined in § 6.2 above, the principal basis of the classification is the type of pressure gradient experienced by the boundary layer in the test region. For the large class of zero- or near-zero pressure gradient flows, we have made further division between those cases in which the whole development of the boundary layer has been under zero pressure gradient conditions, and those with varied upstream histories. The pressure gradient cases are divided into reflected wave flows and simple wave flows. There are further subdivisions based on the geometry of the test zone.

The tabular information consists of nominal values of

- M - Mach number range. For pressure gradient cases, this may be either a local value, or the free stream value.
- R THETA X 10^{-3} - Reynolds number based on momentum defect thickness and boundary layer edge properties.
- TW/TR - The ratio of wall temperature to a nominal adiabatic wall or recovery temperature.
- TO - If total temperature profiles were obtained, the entry is marked P.
- CF - Determination of wall shear stress by:
 - F - Floating element balance (FEB)
 - P - Preston tube
 - S - Stanton tube or surface fence
 - V - Deduction from the velocity profile
- NX - Number of successive stations.
- Q - Measurement of heat flux (Table 7.2).
- PG - Classification as in Table 7.1 (Tables 7.2, 7.3, 7.4).

Brackets round an entry imply that the information is of small quantity or questionable quality.

The tables are, in order:

- 7.1 Classification by local pressure gradient
- 7.2 Experiments with significant heat transfer
- 7.3 Listing in alphabetical order
- 7.4 Listing in numerical order

Readers wishing to select zero pressure-gradient cases for study will find the experimental ranges of Mach number and Reynolds number displayed, approximately, in figures 6.1-3.

Figure 6.1 Nominal experimental range for group I A (Adiabatic cases). Zero pressure-gradient boundary layers formed under constant pressure conditions

Figure 6.2 Nominal experimental range for group I B (adiabatic cases). Zero pressure-gradient boundary layers formed on wind tunnel nozzle walls.

Figure 6.3 Nominal experimental range for zero pressure-gradient boundary layers with significant heat-transfer. (Groups I A & I B together).

TABLE 7.1. LIST OF ENTRIES CLASSIFIED BY LOCAL PRESSURE GRADIENT

I ZERO AND NEAR ZERO PRESSURE-GRADIENT CASES

Flows for which, in principle, the pressure is constant in the test zone.

I (A) Flows with a defined leading edge or origin, developed under ZPG conditions.

		M	R THETA X 10 ⁻³	TW/TR	TO	CF	NX
<u>Type I A 1 FLAT PLATES:</u>							
5301	COLES	2-4.5	2-10	1.0	-	F	1 (2)
5501	SHUTTS et al.	1.7-2.5	6-21	1.0	-	F	3-5
5902	WINKLER & CHA	5.2	1-4.5	0.6-1.0	P	(V)	4
6201	MOORE	5	3-7	0.5-1.0	-	-	(1)
6502	MOORE & HARKNESS	2.7	60	1.0	-	F	1 (2)
6702	DANBERG	6.5	1.3-6	0.5-0.9	P	(V)	4
7006	HASTINGS & SAWYER	4	2-25	1.0	P	F/P	7
7103	FISCHER & MADDALON	6.5	0.5-6	1.0	-	-	7
7204	KEENER & HOPKINS	6.3	2-7	0.3-0.5	P	F	1
7301	GATES	4	8-31	0.9-1.0	P	-	2-3
7305	WATSON et al.	10	1-12	1.0	(P)	F	4
7402	MABEY et al.	2.5-4.5	5-30	1.0	P	F	5

I A 1 R FLAT PLATES WITH ROUGHNESS:

5502	SHUTTS & FENTER	2	11-40	1.0	-	F	5
5804	FENTER & LYONS	2.2/2.7	8-28	1.0	-	-	7/2
6506	YOUNG	4.9	5-13	0.6-1.0	-	F	1

I A 2 CYLINDRICAL: (e-exterior - i-interior)

6001e	MICHEL	1.8-2.7	2-4	1.0	-	-	7
6501e	ADCOCK et al.	6	2-15	1.0	(P)	-	7
6701e	SAMUELS et al.	6	2-15	0.4-0.5	P	-	5
7102i	PEAKE et al.	4	10-60	1.0	-	P	6
7201i	LEWIS et al.	4	4-13	1.0	-	V/(S)	9+
7205e	HURSTMAN & OWEN	7.2	6-13	0.5	P	F	3

(Some nose effects are possible for 7205 and probable for 6001)

I A 3 CONICAL (Divergence)

None

I (B) Flows with an uncertain originI B 1 FLAT WALLS FACING CONTOURED HALF-NOZZLES

5803	KISTLER	1.7-4.8	30	1.0	P	V	1
6602	JEROMIN	2.5-3.5	14-20	1.0	P	V	10
7003	MEIER	1.7-3.0	4-10	0.9-1.0	P	V	6
7202	VOISINET & LEE	4.9	7-58	0.25-1.0	P	F	5
7301	GATES	4.4-9	8-31	0.9-1.0	P	-	2-5

<u>TABLE 7.1 cont.</u>		M	R THETA	TW/TR	TO	CF	NX
<u>I B 2 FLAT TUNNEL WALL AFTER CURVED NOZZLE SURFACE</u>							
5802	STALMACH	1.7-3.7	2-12	1.0	-	F/P	1
5805	MOORE	2-3.5	6-14	1.0	-	F	4-6
6502	MOORE & HARKNESS	2.7	180-700	1.0	-	F	3
6903	THOMKE	2-5	85-350	1.0	-	P	2
7403	LADERMAN & DEMETRIADES	9.4	40	0.4	P	V	1
7601	VAS et al.	2.9	20-400	1.0	-	P	9
<u>I B 3 CYLINDRICAL TUNNEL WALLS AFTER NOZZLE</u>							
7002	JONES & FELLER	5.9	8-80	0.7-0.8	P	-	4
7203	HOPKINS & KEENER	7.2	15-55	0.3-0.5	(P)	F	1
<u>I B 4 PLANE TUNNEL SIDE WALLS (NORMAL TO CURVED NOZZLE WALLS)</u>							
6505	JACKSON et al.	1.6-2.2	10-120	1.0	-	F	2
6601	HOPKINS & KEENER	2.5-3.5	50-60	1.0	-	F/P/S	1
7302	WINTER & GAUDET	0.2-2.8	10-160	1.0	P	F	1
7303	ALLEN	2-4.6	10-80	1.0	-	F/P	1
<u>I (C) Flows recovering from a severe perturbation.</u>							
5805	MOORE (STEP)	2-3.5	6-14	1.0	-	F	4-5
6401	CLUTTER & KAUPS (BLUNT INCREASE)	2-4	10-40	1.0	P	-	5
7102	PEAKE et al. (RING)	4	10-60	1.0	-	P	6
7209	STONE & CARY (TRIPS)	7.7	6-10	0.8	P	-	2
<u>II CLASSIFIED PRESSURE GRADIENT CASES</u>							
<u>II (A) Reflected wave - straight wall</u>							
In principle, normal pressure gradients should be small except near large changes in the pressure gradient, where a simple wave element may be observed.							
<u>II A 1 PLANAR - FPG</u>							
5503	LOBB et al.	5-8	5-12	0.5-1.0	P	(V)	1
5801	NALEID	2	10	1.0	-	F/P	(1)
6504	PASIUK et al.	1.5 to 3	2-10	0.8-1.0	P	-	9
6902	MICHEL	1.4 to 3	4-2	1.0	-	-	12
7304	VOISINET & LEE	3.8 to 4.6	6-50	0.25-1.0	P	F	5
7401	THOMAS	2.5 to 3.0	14-24	1.05	P	S	15-18
<u>II A 2 PLANAR - APG</u>							
5801	NALEID	2	10	1.0	-	F/P	1
7007	ZWARTS	4 to 3	35-70	1.0	-	P	20
7104	WALTRUP & SCHETZ	2.4 to 1.9	20-40	1.0	P	F	4
7401	THOMAS	2.5 to 2.2	14-20	1.0	P	S	15
<u>II A 3 CYLINDRICAL - FPG</u>							
7201f	LEWIS et al.	2.4 to 3.7	10	1.0	-	V/S	7
<u>II A 4 CYLINDRICAL - APG</u>							
7102f	PEAKE et al.	4 to 2	10-50	1.0	-	P	6
7201f	LEWIS et al.	4 to 2.4	10	1.0	-	V/S	12
7208e	ZAKKAY & WANG	6 to 4.6	96-140	0.7	P	-	8

TABLE 7.1 cont.

	M	R THETA	TW/TR	TO	CF	NX
<u>II A 5 CONICAL - FPG - DIVERGENCE (all nozzle walls - internal)</u>						
5901 HILL	8-10	1.5-3.5	0.5	P	V	1-2
6801 PERRY & EAST	8-11.5	6-35	0.3-0.4	P	V	3
6901 BOLDMAN et al.	0- 4.1	3-12	0.6-0.9	P	-	4
7207 BACK et al.	0- 3.6	10	0.5, 1.1	P	-	6

II A 6 CONICAL - APG - DIVERGENCE

None

II (B) Simple wave - curved walls

In these flows the curved streamlines require, in principle, normal pressure gradients, the significance of which increases with Mach number.

II B 1 PLANAR - FPG

None

II B 2 PLANAR - APG

7101 STUREK & DANBERG	3.5 to 2.8	20-40	1.0	P	P	8
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II B 3 AXISYMMETRIC - FPG - (All external, all generated)

6401 CLUTTER & KAUPS	2-4	10-40	0.7-1.0	P	-	5
7005 ALLEN	3	1.4-10	1.0	-	P	7

II B 4 AXISYMMETRIC - APG - (All external, all generated)

6401 CLUTTER & KAUPS	2-4	10-40	1.0	P	-	4
6503 STROUD & MILLER	5-8	2-50	0.4-1.0	P	-	7
7004 WINTER et al.	0.6-2.8	8-40	1.0	-	S	6

II B 5 AXISYMMETRIC - FPG - (All internal, all cancelled)

7001 FISCHER et al.	19-22	4-6	1.0	(P)	-	5
7105 BECKWITH et al.	19.5	2-4	0.2	P	-	1
7206 KEMP & OWEN	19-45	1-8	0.35-0.85	P	F	4

II (C) Normal pressure-gradient cases

If suitable incident waves and generated waves are superimposed, it is possible to generate a region in which there are no streamwise pressure gradients, but nevertheless large transverse gradients. No case is reported in which profiles were measured, but a wide range of heat-transfer measurements were made by THOMANN (6800) in flows with carefully combined gradients giving fields of types A, B and C with a measure of commonality in other features. These results have been included in the catalogue.

TABLE 7.2 FLOWS WITH SIGNIFICANT HEAT TRANSFER

PG - Classification by local pressure-gradient as in Table 7.1 and § 6.2.

Q - Determination of wall heat flux

W - measurement at the wall

P - estimated from temperature profile.

	PG	M	TW/TP	TO	Q
5503 LOBB et al.	II A	5-8	0.5-1.0	P	W
5901 HILL	II A	8-10	0.5	P	P
5902 WINKLER & CHA	I A	5.2	0.6-1.0	P	W
6201 MOORE	I A	5	0.5-1.0	-	-
6401 CLUTTER & KAUPS	II B	1.6-4.5	0.7	P	(W)
6503 STROUD & MILLER	II B	5-8	0.4-1.0	P	W
6504 PASIUK et al.	II A	1-3	0.8-1.0	P	(W)
6506 YOUNG	I A R	5	0.6-1.0	-	W
6701 SAMUELS et al.	I A	6	0.4-0.5	P	(W)
6702 DANBERG	I A	6.5	0.5-0.9	P	P (W)
6800 THOMANN	II C	2.5	0.8	-	W
6801 PERRY & EAST	II A	8-12	0.3-0.4	P	W
6901 BOLDMAN et al.	II A	0-4	0.6-0.9	P	W
7002 JONES & FELLER	I B	6	0.7-0.8	P	-
7105 BECKWITH et al.	II B	20	0.2	P	W
7202 VOISINET & LEE	I B	4.9	0.25-1.0	P	W
7203 HOPKINS & KEENER	I B	7.4	0.3-0.5	(P)	-
7204 KEENER & HOPKINS	IA	6.5	0.3-0.5	(P)	-
7205 HORSTMAN & OWEN	IA	7.2	0.5	P	W
7206 KEMP & OWEN	II B	20-40	0.3-0.9	P	W
7207 BACK et al.	II A	0-3.6	0.5, 1.1	P	W
7208 ZAKKAY & WANG	II A	6	0.7	P	W
7209 STONE & CARY	I C	7.6	0.8	P	(W)
7301 GATES	I A/B	4, 5	0.85-1.0	P	W
7304 VOISINET & LEE	II A	4	0.25-1.0	P	W
7403 LADERMAN & DEMETRIADES	I B	9.4	0.4	P	-

TABLE 7.3 ALPHABETICAL LIST

PG - Classification by local pressure-gradient as in Table 7.1 and § 6.2.

		PG			PG
Adcock et al.	6501	IA	Shutts et al.	5601	IA
Allen	7005	IIB	Stalmach	5802	IB
Allen	7303	IB	Stone & Cary	7209	IC
Back et al.	7207	IIA	Stroud & Miller	6503	IIB
Bockwith et al.	7105	IIB	Sturek & Danberg	7101	IIB
Boldman et al.	6901	IIA	Thomann	6800	IIC
Clutter & Kaups	6401	IIB	Thomas	7401	IIA
Coles	5301	IA	Thomke	6903	IB
Danberg	6702	IA	Voisinnet & Lee (ZPG)	7202	IB
Fenter & Lyons (R)	5804	IA	Voisinnet & Lee (FPG)	7403	IIA
Fischer et al.	7001	IIB	Waltrup & Schetz	7104	IIA
Fischer & Maddalon	7103	IA	Watson et al.	7305	IA
Gates	7301	IA/B	Winkler & Cha	5902	IA
Hastings & Sawyer	7006	IA	Winter & Gaudet	7302	IB
Hill	5901	IIA	Winter et al.	7004	IIB
Hopkins & Keener	6601	IB	Vas et al.	7601	IB
Hopkins & Keener	7203	IB	Young (R)	6506	IA
Horstman & Owen	7205	IA	Zakkay & Wang	7208	IIA
Jackson et al.	6505	IB	Zwarts	7007	IIA
Jeromin	6602	IB			
Jones & Feller	7002	IB			
Keener & Hopkins	7204	IA			
Kemp & Owen	7206	IIB			
Kistler	5803	IB			
Laderman & Demetriades	7403	IB			
Lewis et al.	7201	IIA			
Lobb et al.	5503	IIA			
Mabey et al.	7402	IA			
Meier	7003	IB			
Michel	6001	IA			
Michel et al.	6902	IIA			
Moore (Step)	5805	IC			
Moore	6201	IA			
Moore & Harkness	6502	IB			
Naleid	5801	IIA			
Pasiuk et al.	6504	IIA			
Peake et al.	7102	IIA			
Perry & East	6801	IIA			
Samuels et al.	6701	IA			
Shutts & Fenter (R)	5602	IA			

TABLE 7.4 NUMERICAL LIST

PG - Classification by local pressure-gradient as in Table 7.1 and § 6.2

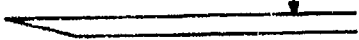
	PG		PG	
5301	IA	Coles	7105	IIB Beckwith et al.
5501	IA	Shutts et al.	7201	IIA Lewis et al.
5502	IA	Shutts & Fenter (R)	7202	IB Voisinet & Lee (Z PG)
5503	IIA	Lobh et al.	7203	IB Hopkins & Keener
5801	IIA	Naleid	7204	IA Keener & Hopkins
5802	IB	Stalmach	7205	IA Horstman & Owen
5803	IB	Kistler	7206	IIB Kemp & Owen
5804	IA	Fenter & Lyons (R)	7207	IIA Back et al.
5805	IC	Moore (Step)	7208	IIA Zakkay & Wang
5901	IIA	Hill	7209	IC Stone et al.
5902	IA	Winkler & Cha	7301	IA/B Gates
6001	IA	Michel	7302	IB Winter & Gaudet
6201	IA	Moore	7303	IB Allen
6401	IIB	Clutter & Kaups	7304	IIA Voisinet & Lee (F PG)
6501	IA	Adcock et al.	7305	IA Watson et al.
6502	IB	Moore & Harkness	7401	IIA Thomas
6503	IIB	Stroud & Miller	7402	IA Mabey et al.
6504	IIA	Pasiuk et al.	7403	IB Laderman & Demetriades
6505	IB	Jackson et al.	7601	IB Vas et al.
6506	IA	Young (R)		
6601	IB	Hopkins & Keener		
6602	IB	Jeromin		
6701	IA	Samuels et al.		
6702	IA	Danberg		
6800	IIC	Thomann		
6801	IIA	Perry & East		
6901	IIA	Boldman et al.		
6902	IIA	Michel et al.		
6903	IB	Thomke		
7001	IIB	Fischer et al.		
7002	IB	Jones & Feller		
7003	IB	Meier		
7004	IIB	Winter et al.		
7005	IIB	Allen		
7006	IA	Hastings & Sawyer		
7007	IIA	Zwarts		
7101	IIB	Sturek & Danberg		
7102	IIA	Peake et al.		
7103	IA	Fischer & Maddalon		
7104	IIA	Waltrup & Schetz		

SECTION 8

THE ENTRIES

The entries are arranged in the sequence given in Table 7.4.

Note: Boundary conditions and evaluated data are given for all profiles as section B of each entry. This data is also printed on the microfiche, which gives complete data for all profiles. The tables of section C of each entry provide only a selection of the profile data. Section D, additional data, is not printed on the microfiche.

	<p>M : 2.0, 2.6, 3.7, 4.5. R THETA X 10⁻³ : 2 - 10. TW/TR : 1.0.</p>	<p>5301</p> <hr/> <p>ZPG - AW</p>
<p>Continuous wind tunnel with symmetrical flexible nozzle. W = H = 0.46 m. 0.067 < P0 < 1.01 MN/m² T0: 310 K. Air. 3 < RE/m × 10⁻⁶ < 16.</p>		
<p>COLES D., 1953. Measurements in the boundary layer on a smooth flat plate in supersonic flow: I. The problem of the turbulent boundary layer, II. Instrumentation and experimental techniques at the Jet-Propulsion Laboratory, and III. Measurements in a flat-plate boundary layer at the Jet-Propulsion Laboratory. JPL. CALTECH. Rep. nos. 20-69, 20-70 and 20-71. (Ph. D thesis, Cal. Inst. Tech., Pasadena, California 1953) <u>Also:</u> Coles, D. (1954).</p>		

- 1 The test boundary layer was formed on the lower surface of a flat plate mounted 13 mm below the tunnel centre-line, completely spanning the tunnel. The leading edge (X = 0) was formed as a 15° wedge with a nose radius estimated as less than 0.013 mm. The overall length was 0.84 m and the width 0.46 m. Measurements were made 'in the central zone' of the plate which was not cooled. Up to 15 minutes was allowed for temperatures to settle. 'Particular attention was paid to the working-surface finish'. The calibration of the empty tunnel showed static pressure variations of order 1 %. With the plate inserted, the pressure field produced by the plate and boundary layer caused static pressure variations of order 5 %. These correspond to 1 % in M at M = 3.7, for which the data on flow-uniformity are presented and which have
- 3 been presumed typical. The profile measurements were mainly made with a fence trip constructed of wires 0.34 mm in diameter spaced at 6.4 mm spanwise intervals and projecting about 2.5 mm normal to the surface of the plate at the leading edge. For some tests this was replaced by a sand strip extending from X = 20 to 30 mm, and for others by a set of airjets issuing from holes 6.4 mm apart at X = 19 mm. The holes were distributed over the central 405 mm width of the plate and connected to a common manifold. The transition region was determined from the boundary layer induced static pressure field and the wall shear-stress
- 5 measurements. The nozzle plates were adjusted to give constant pressure on the tunnel centre-line when empty, so allowing for the four tunnel wall boundary layers. Empty tunnel tests at M = 2.5 showed slight flow convergence in plan view and divergence in elevation. The static pressure on the plate at Z = 70 mm differed from that at Z = 0 by about 1.5 %.
- 6 Twenty seven static pressure holes were provided on the line Z = 70 mm. Additionally each balance incorporated three, one of which was the balance gap. The copper-constantan thermocouples buried in the plate measured TW at X = 245, 425 and 514 mm, Z = 30 mm. TAUW was measured by three JPL-design floating element balances mounted on the centre-line at X = 140, 330 and 610 mm. The element was rectangular, extending 6.4 mm in the X direction and 38.1 mm wide. The balances and their calibration procedure are described in
- 7 JPL Rep. 20-70. A variety of FPP probes were used to measure Pitot pressure, the original intention being to use the tubes as mass-flux probes so as to allow the determination of T0. A typical example is quoted
- 8 as having h₂ = 0.23 mm, b₂ = 1.35 mm. The Pitot pressure profiles presented were measured between X = 542
- 10 and 546 mm, with one exception for which X = 263 mm. No corrections were applied.
- 9 The author's interpolation of CF values for the profile boundary conditions has been accepted. The source
- 11 data were reduced assuming an iso-energetic boundary layer and Sutherland's viscosity law. The tables here
- 12 are calculated assuming a Crocco/Van Driest temperature-velocity relation and constant static pressure.
- 13 TW data were not presented and the editors' recovery temperature has been used. Fourteen individual profiles are presented, the sets for each Mach number being over a range of different total pressures. Most (0101-1101) were taken at X = 546 mm with the fence boundary-layer trip. The exceptions are 1201 (Sand trip, X = 542 mm) 1301 (Air-jet trip X = 263 mm) 1302 (Air-jet trip X = 542 mm).
- § DATA: 5301 0101-1302. PT2 Profiles. NX = 1 except for the pair 1301-2. CF obtained separately with floating element balances.

15 Editors' comments

This investigation was a pioneer attempt at a reasonably complete survey of a ZPG-AW boundary layer. Other early investigations also without TC profiles are those of Shutts et al. - CAT 5501, in which there were up to five successive stations, and of Stalmach - CAT 5802. Later, full, studies are those of Hastings & Sawyer - CAT 7006 and Mabey et al. - CAT 7402. Axisymmetric cases which overlap in Mach number and Reynolds number are the ZPG series of Lewis et al. - CAT 7201 and Peake et al. - CAT 7102. An examination of our wall-law plots suggested that the CF values may be slightly high, though any likely discrepancy lies within the indeterminacy of a single observation. The different types of tripping devices may have influenced the boundary layer at the measuring station.

CAT 5301		COLES		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TW/TR*	REO2M	CF *	H12	H12K	PW	PD			
X *	P00*	PW/PD*	REO2D	CG	H32	H32K	TW	TD			
RZ	T00*	SM *	DZ	F12*	H42	D2K	UD	TR			
53010101	1.9660	1.0000	1.9971 ⁺⁰³	2.7200 ⁻⁰³	3.0784	1.4632	3.5927 ⁺⁰³	3.5927 ⁺⁰³			
5.4559 ⁻⁰¹	2.6664 ⁺⁰⁴	1.0000	3.0805 ⁺⁰³	NM	1.7814	1.7704	2.9170 ⁺⁰²	1.7234 ⁺⁰²			
INFINITE	3.0556 ⁺⁰²	0.0000	9.6329 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0808	1.2144 ⁻⁰³	5.1746 ⁺⁰²	2.9170 ⁺⁰²			
53010201	1.9780	1.0000	4.3574 ⁺⁰³	2.1800 ⁻⁰³	3.1023	1.4704	8.8160 ⁺⁰³	8.8160 ⁺⁰³			
5.4559 ⁻⁰¹	6.6661 ⁺⁰⁴	1.0000	6.7394 ⁺⁰³	NM	1.7873	1.7765	2.8789 ⁺⁰²	1.6924 ⁺⁰²			
INFINITE	3.0167 ⁺⁰²	0.0000	8.3509 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0816	1.0533 ⁻⁰³	5.1592 ⁺⁰²	2.8789 ⁺⁰²			
53010301	1.9820	1.0000	5.7051 ⁺⁰³	2.0200 ⁻⁰³	3.0982	1.4665	1.2441 ⁺⁰⁴	1.2441 ⁺⁰⁴			
5.4559 ⁻⁰¹	9.4659 ⁺⁰⁴	1.0000	8.9041 ⁺⁰³	NM	1.7943	1.7836	2.8892 ⁺⁰²	1.6956 ⁺⁰²			
INFINITE	3.0278 ⁺⁰²	0.0000	7.8697 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0821	9.8475 ⁻⁰⁴	5.1746 ⁺⁰²	2.8892 ⁺⁰²			
53010401	2.5400	1.0000	1.2178 ⁺⁰³	2.4200 ⁻⁰³	4.2269	1.5229	1.9065 ⁺⁰³	1.9065 ⁺⁰³			
5.4559 ⁻⁰¹	3.4664 ⁺⁰⁴	1.0000	2.3359 ⁺⁰³	NM	1.7851	1.7610	2.8818 ⁺⁰²	1.3365 ⁺⁰²			
INFINITE	3.0011 ⁺⁰²	0.0000	7.4744 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1046	1.0617 ⁻⁰³	5.8876 ⁺⁰²	2.8818 ⁺⁰²			
53010501	2.5680	1.0000	3.5017 ⁺⁰³	1.8100 ⁻⁰³	4.2135	1.4648	5.2657 ⁺⁰³	5.2657 ⁺⁰³			
5.4559 ⁻⁰¹	9.9991 ⁺⁰⁴	1.0000	6.7821 ⁺⁰³	NM	1.7910	1.7741	2.9062 ⁺⁰²	1.3320 ⁺⁰²			
INFINITE	3.0089 ⁺⁰²	0.0000	7.7343 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1059	1.1035 ⁻⁰³	5.9424 ⁺⁰²	2.9062 ⁺⁰²			
53010601	2.5780	1.0000	5.4630 ⁺⁰³	1.6800 ⁻⁰³	4.2558	1.4841	9.0560 ⁺⁰³	9.0560 ⁺⁰³			
5.4559 ⁻⁰¹	1.7465 ⁺⁰⁵	1.0000	1.0390 ⁺⁰⁴	NM	1.7903	1.7728	2.8683 ⁺⁰²	1.3548 ⁺⁰²			
INFINITE	3.1556 ⁺⁰²	0.0000	7.1645 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1063	1.0252 ⁻⁰³	6.0162 ⁺⁰²	2.9683 ⁺⁰²			
53010701	3.6900	1.0000	7.5974 ⁺⁰²	2.1100 ⁻⁰³	7.0550	1.3845	7.8984 ⁺⁰²	7.8984 ⁺⁰²			
5.4559 ⁻⁰¹	7.8660 ⁺⁰⁴	1.0000	2.9015 ⁺⁰³	NM	1.8105	1.7836	2.8334 ⁺⁰²	8.2366 ⁺⁰¹			
INFINITE	3.0667 ⁺⁰²	0.0000	6.0025 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1383	1.0585 ⁻⁰³	6.7144 ⁺⁰²	2.8334 ⁺⁰²			
53010801	3.7010	1.0000	1.4842 ⁺⁰³	1.6200 ⁻⁰³	7.1536	1.4803	1.3580 ⁺⁰³	1.3580 ⁺⁰³			
5.4559 ⁻⁰¹	1.3732 ⁺⁰⁵	1.0000	4.4608 ⁺⁰³	NM	1.7980	1.7657	2.8792 ⁺⁰²	8.3345 ⁺⁰¹			
INFINITE	3.1167 ⁺⁰²	0.0000	6.9261 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1370	1.2821 ⁻⁰³	6.7744 ⁺⁰²	2.8792 ⁺⁰²			
53010901	3.6970	1.0000	2.7295 ⁺⁰³	1.3800 ⁻⁰³	7.1461	1.4754	2.8372 ⁺⁰³	2.8372 ⁺⁰³			
5.4559 ⁻⁰¹	2.8531 ⁺⁰⁵	1.0000	8.1884 ⁺⁰³	NM	1.7966	1.7689	2.8845 ⁺⁰²	8.3626 ⁺⁰¹			
INFINITE	3.1222 ⁺⁰²	0.0000	6.1225 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1368	1.1394 ⁻⁰³	6.7764 ⁺⁰²	2.8845 ⁺⁰²			
53011001	4.5120	1.0000	8.8021 ⁺⁰²	1.4800 ⁻⁰³	10.0077	1.5506	6.7166 ⁺⁰²	6.7166 ⁺⁰²			
5.4559 ⁻⁰¹	1.9732 ⁺⁰⁵	1.0000	3.5747 ⁺⁰³	NM	1.8101	1.7692	2.8106 ⁺⁰²	6.0467 ⁺⁰¹			
INFINITE	3.0667 ⁺⁰²	0.0000	5.6944 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1511	1.2502 ⁻⁰³	7.0346 ⁺⁰²	2.8106 ⁺⁰²			
53011101	4.5540	1.0000	1.6027 ⁺⁰³	1.2200 ⁻⁰³	10.0634	1.5002	1.2578 ⁺⁰³	1.2578 ⁺⁰³			
5.4559 ⁻⁰¹	3.8930 ⁺⁰⁵	1.0000	6.6012 ⁺⁰³	NM	1.8067	1.7632	2.8149 ⁺⁰²	5.9788 ⁺⁰¹			
INFINITE	3.0778 ⁺⁰²	0.0000	5.4696 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1514	1.2210 ⁻⁰³	7.0601 ⁺⁰²	2.8149 ⁺⁰²			
53011201	4.5450	1.0000	1.2883 ⁺⁰³	1.3100 ⁻⁰³	9.8558	1.4542	1.3111 ⁺⁰³	1.3111 ⁺⁰³			
5.4229 ⁻⁰¹	4.1130 ⁺⁰⁵	1.0000	5.2739 ⁺⁰³	NM	1.8232	1.7828	2.8557 ⁺⁰²	6.0737 ⁺⁰¹			
INFINITE	3.1167 ⁺⁰²	0.0000	4.3013 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1527	9.1890 ⁻⁰⁴	7.1018 ⁺⁰²	2.8557 ⁺⁰²			
53011301	4.5040	1.0000	7.7640 ⁺⁰²	1.5500 ⁻⁰³	9.8867	1.5498	1.3797 ⁺⁰³	1.3797 ⁺⁰³			
2.6289 ⁻⁰¹	4.0130 ⁺⁰⁵	1.0000	3.1290 ⁺⁰³	NM	1.8259	1.7826	2.8719 ⁺⁰²	6.1958 ⁺⁰¹			
INFINITE	3.1333 ⁺⁰²	0.0000	2.5216 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1523	5.2867 ⁻⁰⁴	7.1081 ⁺⁰²	2.8719 ⁺⁰²			
53011302	4.5440	1.0000	1.3530 ⁺⁰³	1.2600 ⁻⁰³	9.8612	1.4468	1.3171 ⁺⁰³	1.3171 ⁺⁰³			
5.4229 ⁻⁰¹	4.0263 ⁺⁰⁵	1.0000	5.5323 ⁺⁰³	NM	1.8186	1.7795	2.8659 ⁺⁰²	6.0975 ⁺⁰¹			
INFINITE	3.1278 ⁺⁰²	0.0000	4.5190 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1523	9.7838 ⁻⁰⁴	7.1142 ⁺⁰²	2.8659 ⁺⁰²			

53010401		COLES		PROFILE TABULATION				22 POINTS, DELTA AT POINT 22	
I	Y	PT2/P	P/PD	T0/T00	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.3000"+00	1.0000"+00	NM	0.94141	0.00000	0.00000	2.15013	0.00000	
2	6.0706"-04	2.1417"+00	NM	0.96398	0.43402	0.57795	1.76594	0.32654	
3	6.8580"-04	2.3493"+00	NM	0.96522	0.46147	0.61916	1.77571	0.35357	
4	7.5946"-04	2.4832"+00	NM	0.96457	0.48257	0.67897	1.69876	0.37025	
5	8.5344"-04	2.6732"+00	NM	0.96043	0.50685	0.65314	1.66247	0.39307	
6	9.6520"-04	2.8365"+00	NM	0.96794	0.52662	0.67289	1.63265	0.41215	
7	1.1024"-03	3.0020"+00	NM	0.95940	0.54584	0.69124	1.60372	0.43102	
8	1.2598"-03	3.1644"+00	NM	0.97077	0.56197	0.70810	1.57644	0.44918	
9	1.4529"-03	3.3313"+00	NM	0.97215	0.58194	0.72439	1.54947	0.46751	
10	1.6840"-03	3.5102"+00	NM	0.97356	0.60055	0.74081	1.52165	0.48585	
11	1.9710"-03	3.7050"+00	NM	0.97504	0.62021	0.75769	1.49202	0.50768	
12	2.3063"-03	3.9227"+00	NM	0.97662	0.64176	0.77520	1.46136	0.53046	
13	2.7127"-03	4.1770"+00	NM	0.97833	0.66501	0.79431	1.42669	0.55675	
14	3.2004"-03	4.5012"+00	NM	0.98050	0.69407	0.81670	1.38485	0.58480	
15	3.7897"-03	4.9180"+00	NM	0.98304	0.72765	0.84290	1.33464	0.61558	
16	4.4856"-03	5.3868"+00	NM	0.98569	0.76764	0.86931	1.28289	0.67786	
17	5.3391"-03	5.9839"+00	NM	0.98877	0.81333	0.89933	1.22168	0.73590	
18	6.3678"-03	6.7234"+00	NM	0.99219	0.86663	0.93099	1.15406	0.80671	
19	7.5641"-03	7.5303"+00	NM	0.99552	0.92116	0.96101	1.08800	0.88296	
20	9.0576"-03	8.2928"+00	NM	0.99833	0.98904	0.98567	1.03291	0.95427	
21	1.0813"-02	8.7058"+00	NM	0.99974	0.99921	0.99777	1.00516	0.99285	
D 22	1.2974"-02	8.7851"+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P/PPD, T/W*TR, VAN DRIEST

53010601		COLES		PROFILE TABULATION				21 POINTS, DELTA AT POINT 21	
I	Y	PT2/P	P/PD	T0/T00	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000"+00	1.0000"+00	NM	0.94065	0.00000	0.00000	2.19098	0.00000	
2	6.0706"-04	2.1774"+00	NM	0.96274	0.46144	0.61003	1.74777	0.34904	
3	6.8580"-04	2.4070"+00	NM	0.96405	0.47852	0.62785	1.72151	0.36471	
4	7.5946"-04	2.6098"+00	NM	0.96505	0.49154	0.64115	1.70140	0.37684	
5	8.5344"-04	2.7351"+00	NM	0.96023	0.50685	0.65650	1.67768	0.39132	
6	9.6520"-04	2.8542"+00	NM	0.96732	0.52092	0.67332	1.65584	0.40482	
7	1.1024"-03	2.9943"+00	NM	0.96856	0.53693	0.68371	1.63098	0.42043	
8	1.2598"-03	3.1534"+00	NM	0.96991	0.55447	0.70218	1.60376	0.43783	
9	1.4529"-03	3.3175"+00	NM	0.97126	0.57193	0.71816	1.57673	0.45547	
10	1.6840"-03	3.4864"+00	NM	0.97260	0.58930	0.73366	1.54993	0.47335	
11	1.9710"-03	3.6907"+00	NM	0.97415	0.60960	0.75127	1.51879	0.49465	
12	2.3063"-03	3.9161"+00	NM	0.97578	0.63117	0.76940	1.48595	0.51778	
13	2.7127"-03	4.1814"+00	NM	0.97762	0.65561	0.78822	1.44915	0.54461	
14	3.2004"-03	4.5076"+00	NM	0.97975	0.68339	0.81163	1.40843	0.57704	
15	3.7897"-03	5.0088"+00	NM	0.98273	0.72030	0.84251	1.34560	0.62612	
16	4.4856"-03	5.4501"+00	NM	0.98523	0.76123	0.86667	1.29633	0.66859	
17	5.3391"-03	6.1291"+00	NM	0.98867	0.81197	0.89953	1.22730	0.73293	
18	6.3678"-03	7.0077"+00	NM	0.99261	0.87316	0.93567	1.14030	0.81483	
19	7.5641"-03	8.0149"+00	NM	0.99654	0.93835	0.97040	1.04947	0.90737	
20	9.0576"-03	8.8152"+00	NM	0.99930	0.98711	0.99405	1.01412	0.98021	
D 21	1.0813"-02	9.0349"+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P/PPD, T/W*TR, VAN DRIEST

53011101		COLES		PROFILE TABULATION				22 POINTS, DELTA AT POINT 22	
I	Y	PT2/P	P/PD	T0/T00	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000"+00	1.0000"+00	NM	0.91623	0.00000	0.00000	4.71641	0.00000	
2	6.0706"-04	2.7046"+00	NM	0.94088	0.28512	0.54264	3.02210	0.14981	
3	6.8580"-04	3.0661"+00	NM	0.94399	0.30048	0.57581	3.48423	0.18526	
4	7.5946"-04	3.3541"+00	NM	0.94633	0.32016	0.59964	3.38011	0.17740	
5	8.5344"-04	3.7037"+00	NM	0.94892	0.34581	0.62488	3.26527	0.19137	
6	9.6520"-04	4.0511"+00	NM	0.95134	0.36441	0.64798	3.15784	0.20507	
7	1.1024"-03	4.3925"+00	NM	0.95357	0.38176	0.66774	3.05934	0.21826	
8	1.2598"-03	4.7274"+00	NM	0.95561	0.39801	0.68577	2.96886	0.23100	
9	1.4529"-03	5.0855"+00	NM	0.95766	0.41466	0.70341	2.87757	0.24445	
10	1.6840"-03	5.4176"+00	NM	0.95946	0.42950	0.71845	2.79810	0.25676	
11	1.9710"-03	5.8115"+00	NM	0.96146	0.44645	0.73447	2.70942	0.27123	
12	2.3063"-03	6.2439"+00	NM	0.96351	0.46433	0.75135	2.61184	0.28695	
13	2.7127"-03	6.7743"+00	NM	0.96584	0.48534	0.76966	2.51444	0.30604	
14	3.2004"-03	7.4661"+00	NM	0.96860	0.51120	0.79071	2.39265	0.33049	
15	3.7897"-03	8.4107"+00	NM	0.97200	0.54901	0.81601	2.24175	0.36401	
16	4.4856"-03	9.5832"+00	NM	0.97565	0.58379	0.84225	2.08085	0.40492	
17	5.3391"-03	1.1261"+01	NM	0.98003	0.63559	0.87277	1.88555	0.44287	
18	6.3678"-03	1.3571"+01	NM	0.98489	0.70063	0.90539	1.66494	0.54217	
19	7.5641"-03	1.6633"+01	NM	0.98982	0.77303	0.93731	1.45136	0.64352	
20	9.0576"-03	2.0828"+01	NM	0.99481	0.87321	0.96853	1.23023	0.78727	
21	1.0813"-02	2.5168"+01	NM	0.99859	0.96181	0.99152	1.06274	0.93299	
D 22	1.2974"-02	2.7168"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P/PPD, T/W*TR, VAN DRIEST

53011201		COLES		PROFILE TABULATION			19 POINTS, DELTA AT POINT 19		
I	Y	PT2/P	P/PD	T0/T0D	H/H0D	U/U0D	T/T0D	RHO/RHO0*U/U0D	
1	0.0000*+00	1.0000*+00	NM	0.91627	0.00000	0.00000	4.70174	0.00000	
2	4.4704*-04	2.8424*+00	NM	0.94214	0.29470	0.55587	3.55792	0.15624	
3	5.1054*-04	3.1426*+00	NM	0.94468	0.31384	0.58255	3.44552	0.16907	
4	6.0706*-04	3.5724*+00	NM	0.94803	0.33916	0.61589	3.29760	0.18677	
5	7.2644*-04	4.0962*+00	NM	0.95171	0.36748	0.65063	3.13471	0.20756	
6	8.7884*-04	4.6491*+00	NM	0.95533	0.39602	0.68303	2.97476	0.22961	
7	1.0541*-03	5.2658*+00	NM	0.95872	0.42362	0.71202	2.82505	0.25204	
8	1.2700*-03	5.8846*+00	NM	0.96188	0.45041	0.73807	2.68521	0.27487	
9	1.5240*-03	6.4873*+00	NM	0.96467	0.47503	0.76032	2.56184	0.29679	
10	1.8440*-03	7.0740*+00	NM	0.96715	0.49779	0.77953	2.45230	0.31788	
11	2.2276*-03	7.7459*+00	NM	0.96981	0.52335	0.79966	2.33464	0.34252	
12	3.2715*-03	8.4461*+00	NM	0.97646	0.59354	0.84767	2.04060	0.41550	
13	3.9675*-03	1.1443*+01	NM	0.98053	0.64220	0.87604	1.86082	0.47078	
14	4.7955*-03	1.3545*+01	NM	0.98490	0.70111	0.90536	1.66752	0.54294	
15	5.7861*-03	1.6216*+01	NM	0.98930	0.76944	0.93390	1.47318	0.63394	
16	7.0383*-03	2.0065*+01	NM	0.99409	0.85838	0.96405	1.26136	0.76430	
17	8.5217*-03	2.4478*+01	NM	0.99813	0.95017	0.98875	1.08285	0.91309	
18	1.0358*-02	2.6954*+01	NM	0.99993	0.99795	0.99956	1.00324	0.99633	
D 19	1.2593*-02	2.7063*+01	NM	1.00003	1.00000	1.00000	1.00000	1.00000	

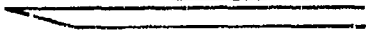
INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD, TW=TR, VAN DRIEST

53011301		COLES		PROFILE TABULATION			17 POINTS, DELTA AT POINT 17		
I	Y	PT2/P	P/PD	T0/T0D	H/H0D	U/U0D	T/T0D	RHO/RHO0*U/U0D	
1	0.0000*+00	1.0000*+00	NM	0.91656	0.00000	0.00000	4.63525	0.00000	
2	4.4196*-04	3.4425*+00	NM	0.94736	0.33475	0.60751	3.29359	0.18445	
3	5.2070*-04	3.9692*+00	NM	0.95116	0.36406	0.64390	3.12807	0.20585	
4	6.1722*-04	4.5716*+00	NM	0.95505	0.39480	0.67918	2.95835	0.22958	
5	7.3660*-04	5.2670*+00	NM	0.95904	0.42753	0.71346	2.78482	0.25620	
6	8.8900*-04	6.0996*+00	NM	0.96318	0.46316	0.74741	2.60435	0.28700	
7	1.0643*-03	6.9934*+00	NM	0.96714	0.49923	0.77853	2.43190	0.32013	
8	1.2802*-03	7.9683*+00	NM	0.97086	0.53514	0.80667	2.26971	0.35541	
9	1.5342*-03	8.9426*+00	NM	0.97411	0.56928	0.83047	2.12812	0.39024	
10	1.8542*-03	9.9814*+00	NM	0.97715	0.60326	0.85216	1.99541	0.42706	
11	2.2377*-03	1.1345*+01	NM	0.98062	0.64515	0.87619	1.84445	0.47504	
12	2.7076*-03	1.3193*+01	NM	0.98455	0.69789	0.90269	1.67305	0.53455	
13	3.2817*-03	1.5642*+01	NM	0.98876	0.76216	0.93022	1.48944	0.62446	
14	3.9776*-03	1.8987*+01	NM	0.99321	0.84202	0.95847	1.29570	0.73973	
15	4.8057*-03	2.2968*+01	NM	0.99720	0.92817	0.98310	1.12186	0.87631	
16	5.7963*-03	2.5811*+01	NM	0.99945	0.98507	0.99672	1.02379	0.97356	
D 17	7.0485*-03	2.6585*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD, TW=TR, VAN DRIEST

53011302		COLES		PROFILE TABULATION			20 POINTS, DELTA AT POINT 20		
I	Y	PT2/P	P/PD	T0/T0D	H/H0D	U/U0D	T/T0D	RHO/RHO0*U/U0D	
1	0.0000*+00	1.0000*+00	NM	0.91627	0.00000	0.00000	4.70011	0.00000	
2	4.2418*-04	2.6565*+00	NM	0.94047	0.28215	0.53761	3.43069	0.14867	
3	5.0292*-04	2.9936*+00	NM	0.94345	0.30458	0.56973	3.49907	0.16242	
4	5.9944*-04	3.4143*+00	NM	0.94684	0.33017	0.60423	3.34921	0.18041	
5	7.1882*-04	3.8956*+00	NM	0.95036	0.35700	0.63801	3.19395	0.19975	
6	8.7122*-04	4.4317*+00	NM	0.95387	0.38455	0.67025	3.03789	0.22063	
7	1.0465*-03	4.9900*+00	NM	0.95720	0.41119	0.69910	2.89128	0.24183	
8	1.2624*-03	5.5668*+00	NM	0.96031	0.43696	0.72518	2.75425	0.26330	
9	1.5164*-03	6.1128*+00	NM	0.96298	0.45999	0.74686	2.63618	0.28331	
10	1.8364*-03	6.6633*+00	NM	0.96545	0.48208	0.76635	2.52799	0.30325	
11	2.2200*-03	7.2861*+00	NM	0.96800	0.50568	0.78601	2.41413	0.32559	
12	2.6899*-03	8.1085*+00	NM	0.97104	0.53567	0.80879	2.27971	0.35478	
13	3.2639*-03	9.2170*+00	NM	0.97464	0.57336	0.83495	2.12064	0.39372	
14	3.9599*-03	1.0685*+01	NM	0.97870	0.61972	0.86347	1.94136	0.44478	
15	4.7879*-03	1.2663*+01	NM	0.98319	0.67717	0.89399	1.74288	0.51294	
16	5.7705*-03	1.5270*+01	NM	0.98787	0.74613	0.92473	1.53604	0.60202	
17	7.0307*-03	1.8989*+01	NM	0.99290	0.83466	0.95667	1.31373	0.72621	
18	8.5141*-03	2.3620*+01	NM	0.99748	0.93322	0.98460	1.11312	0.88453	
19	1.0350*-02	2.6942*+01	NM	0.99993	0.99795	0.99956	1.00324	0.99633	
D 20	1.2586*-02	2.7051*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD, TW=TR, VAN DRIEST

	M : 1.7 - 2.5 R THETA X 10 ⁻³ : 6 - 21 TW / TR : 1.0	5501
		ZPG - AW
Continuous wind tunnel with fixed symmetrical interchangeable nozzles. W = 0.48, H = 0.7, L = 1.0 m. 0.18 < P0 < 0.3 MN/m ² . T0 : 340 K. Air. RE/m X 10 ⁻⁶ : 25.		
SHUTTS W.H., HARTWIG W.H. and WEILER J.E., 1955. Final report on turbulent boundary layer and skin friction measurements on a smooth, thermally insulated flat plate at supersonic speeds. DRL 364.		

- 1 The test boundary layer was formed on the upper surface of a flat plate model 0.482 m wide (spanning the tunnel) and 0.914 m long. The sharp leading edge (X = 0) was chamfered at 6.7° on the underside. Provision was made for eight instrument stations (d = 33.4 mm) in which balances, traverse gear, or blanking plugs could be placed. These were at 101.6 mm intervals along the centre line, the first being centred at X = 147 mm. The surface was machined and polished so that irregularities were less than 2.5 μm. The surface
- 2 was not actively cooled, and was allowed to reach an equilibrium temperature during tests. Mach number variation over the test region of the plate was up to 4 % in some cases, due to irregularity of the nozzle
- 3 walls or reflection of leading edge disturbances. For most tests a boundary layer trip consisting of a 2.54 mm wide band of No 100 Aloxite grit was bonded to the plate transverse to the flow direction 23 mm behind the leading edge. For profile 0401 there was no trip, while for series 02 a second trip, identical to the first, was mounted 124 mm from the leading edge. Transition occurred ahead of the first measuring station "even for the smooth plate".
- 6 Static pressure was measured at 50.8 mm intervals on the centre line of the plate starting at X = 70.6 mm. The static pressure was measured in separate runs, with no traverse gear mounted. Wall shear stress was measured, also in separate runs, using balances developed by Weiler & Hartwig (1952). The balance elements
- 7 were 25.4 mm in diameter. Pitot profiles were obtained with a CPP the tip of which consisted of tubing for which d₁ = 0.508, d₂ = 0.254 mm. Over the first 0.508 mm, the outer surface was ground down to meet the inner diameter, providing a sharp lip. After about 15 [E] diameters, the fine tube was cranked up and held in progressively larger sleeving tubes which were attached to a movable double wedge traverse strut. The
- 8 profile normal was 55.3 mm ahead of the centre of the measuring station.
- 9 The authors have interpolated the static pressure readings to the positions of the profile measurements and assumed that static pressure did not vary through the boundary layer. They reduced the profiles assuming
- 10 constant total temperature. No probe corrections were applied and viscosity was found from the Sutherland
- 11 formula.
- 12 The flat plate could be mounted at small angles of positive and negative incidence, so as to provide a further small range of Mach number variation. The editors have presented only those measurements made at zero incidence, half the total. When the plate was mounted at incidence, the leading edge disturbance was relatively strong, and at M = 1.73 impinged on the plate about 2/3 of the way back from the leading edge, giving rise to sharp variations in local Mach number etc. The editors have interpolated the CF values to the X values of the profiles. The author's assumption of isoenergetic flow has been replaced by the
- 13 Crocco / Van Driest temperature velocity correlation. The profiles presented were measured at a near constant unit Reynolds' number. The series are distinguished by Mach number and tripping arrangements. Those profiles indicated by a star were obtained with extra screens in the settling chamber. The series are:

at M = 1.73	- series 01	- one trip
M = 2.00	02	- two trips
	03	- one trip
	04	- no trips
M = 2.23	05	- one trip

M = 2.5 - series 06 - one trip
0602⁺/3⁺ with extra screens.

14 An interpolated CF value is given for each profile, but the values for 0602⁺/3⁺ were measured without the extra screens.

§ DATA: 5501 0101-0604. Pitot profiles. NX = 3-5. CF measured by an FEB separately.

15 Editors' comments

The entry describes an early, and much quoted, set of systematic flat plate measurements. The authors made a careful investigation of the inaccuracies arising from misalignment of the floating elements, and compared several balances with each other. The authors state that the measured CF values are, on average, 6 - 9 % less than the "theoretical" prediction of Fenter (1955). Our log-law plots show that the CF values are low, as compared to Van Driest values, for about half the measured profiles.

The profiles contain relatively few data-points, and in only one case do measurements extend within the momentum-deficit peak. Profiles 0401/0502/0602/0604 show marked disturbances in the inner region, while the outer region of 0301 seems irregular.

The tests should be compared with the roughly contemporary work of Coles - CAT 5301 and the later work of Mabey et al. - CAT 7402 and Hastings & Sawyer - CAT 7006.

CAT 5501		SHUTTS /H /M		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
ROW	MD *	T1/TR*	REN2W	CF *	H12	H12K	PW	PD			
X *	POD*	PW/POD*	REN2D	CO	H32	H32K	TW	TD			
RZ	TOO*	SN *	02	PI2*	H42	D2K	UD	TR			
55010101	1.7240	1.0000	4.2224 ⁺ +03	2.2400 ⁻ -03	2.6775	1.4546	3.6608 ⁺ +04	3.6608 ⁺ +04			
1.9303 ⁻ -01	1.8737 ⁺ +05	1.0000	5.9278 ⁺ +03	NM	1.8109	1.8042	3.2541 ⁺ +02	2.1232 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	2.7512 ⁻ -04	0.0000 ⁺ +00	0.0702	3.2397 ⁻ -04	5.0367 ⁺ +02	3.2541 ⁺ +02			
55010102	1.8020	1.0000	8.7071 ⁺ +03	1.9600 ⁻ -03	2.6812	1.3614	3.3074 ⁺ +04	3.3074 ⁺ +04			
3.9624 ⁻ -01	1.9062 ⁺ +05	1.0000	1.2554 ⁺ +04	NM	1.8068	1.7987	3.2467 ⁺ +02	2.0524 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	5.8963 ⁻ -04	0.0000 ⁺ +00	0.0740	7.0584 ⁻ -04	5.1760 ⁺ +02	3.2467 ⁺ +02			
55010103	1.7260	1.0000	1.4276 ⁺ +04	1.7800 ⁻ -03	2.5051	1.3096	3.7229 ⁺ +04	3.7229 ⁺ +04			
8.0263 ⁻ -01	1.9113 ⁺ +05	1.0000	2.0055 ⁺ +04	NM	1.8180	1.8113	3.2539 ⁺ +02	2.1214 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	9.1313 ⁻ -04	0.0000 ⁺ +00	0.0706	1.0700 ⁻ -03	5.0403 ⁺ +02	3.2539 ⁺ +02			
55010201	2.0230	1.0000	3.8713 ⁺ +03	1.9400 ⁻ -03	3.1433	1.4598	2.9013 ⁺ +04	2.9013 ⁺ +04			
1.9303 ⁻ -01	2.3529 ⁺ +05	1.0000	6.0357 ⁺ +03	NM	1.8128	1.8046	3.2269 ⁺ +02	1.8616 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	2.5236 ⁻ -04	0.0000 ⁺ +00	0.0849	3.1356 ⁻ -04	5.5341 ⁺ +02	3.2269 ⁺ +02			
55010202	2.0360	1.0000	1.0407 ⁺ +04	1.7400 ⁻ -03	2.9929	1.3294	2.8730 ⁺ +04	2.8730 ⁺ +04			
5.9945 ⁻ -01	2.3776 ⁺ +05	1.0000	1.6302 ⁺ +04	NM	1.8234	1.8145	3.2257 ⁺ +02	1.8509 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	6.7857 ⁻ -04	0.0000 ⁺ +00	0.0860	8.3631 ⁻ -04	5.5536 ⁺ +02	3.2257 ⁺ +02			
55010203	2.0200	1.0000	1.3607 ⁺ +04	1.5600 ⁻ -03	2.4129	1.2899	2.9447 ⁺ +04	2.9447 ⁺ +04			
8.0263 ⁻ -01	2.3769 ⁺ +05	1.0000	2.1192 ⁺ +04	NM	1.8322	1.8251	3.2271 ⁺ +02	1.8641 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	8.7589 ⁻ -04	0.0000 ⁺ +00	0.0856	1.0683 ⁻ -03	5.5296 ⁺ +02	3.2271 ⁺ +02			
55010301	2.0170	1.0000	3.8671 ⁺ +03	2.0300 ⁻ -03	3.1431	1.4683	2.9412 ⁺ +04	2.9412 ⁺ +04			
1.9303 ⁻ -01	2.3630 ⁺ +05	1.0000	6.0159 ⁺ +03	NM	1.8125	1.8033	3.2274 ⁺ +02	1.8666 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	2.4976 ⁻ -04	0.0000 ⁺ +00	0.0846	3.0989 ⁻ -04	5.5251 ⁺ +02	3.2274 ⁺ +02			
55010302	1.9960	1.0000	7.1117 ⁺ +03	1.7900 ⁻ -03	2.9777	1.3685	3.0507 ⁺ +04	3.0507 ⁺ +04			
3.9624 ⁻ -01	2.3722 ⁺ +05	1.0000	1.0980 ⁺ +04	NM	1.8230	1.8156	3.2292 ⁺ +02	1.8841 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	4.4979 ⁻ -04	0.0000 ⁺ +00	0.0841	5.5093 ⁻ -04	5.4931 ⁺ +02	3.2292 ⁺ +02			
55010303	2.0000	1.0000	1.2138 ⁺ +04	1.6400 ⁻ -03	2.9280	1.3219	3.0071 ⁺ +04	3.0071 ⁺ +04			
8.0263 ⁻ -01	2.3529 ⁺ +05	1.0000	1.8767 ⁺ +04	NM	1.8206	1.8123	3.2289 ⁺ +02	1.8807 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	7.7649 ⁻ -04	0.0000 ⁺ +00	0.0842	9.5332 ⁻ -04	5.4993 ⁺ +02	3.2289 ⁺ +02			
55010401	2.0050	1.0000	8.1812 ⁺ +03	1.8200 ⁻ -03	2.9418	1.3356	2.9760 ⁺ +04	2.9760 ⁺ +04			
3.9624 ⁻ -01	2.3468 ⁺ +05	1.0000	1.2672 ⁺ +04	NM	1.8338	1.8255	3.2284 ⁺ +02	1.8766 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	5.2687 ⁻ -04	0.0000 ⁺ +00	0.0850	0.3937 ⁻ -04	5.5069 ⁺ +02	3.2284 ⁺ +02			
55010501	2.2490	1.0000	3.5727 ⁺ +03	1.9600 ⁻ -03	3.5022	1.4319	2.2292 ⁺ +04	2.2292 ⁺ +04			
1.9303 ⁻ -01	2.5737 ⁺ +05	1.0000	6.0527 ⁺ +03	NM	1.8174	1.8105	3.2083 ⁺ +02	1.8829 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	2.5810 ⁻ -04	0.0000 ⁺ +00	0.0951	3.3434 ⁻ -04	5.8496 ⁺ +02	3.2083 ⁺ +02			
55010502	2.2420	1.0000	4.8797 ⁺ +03	1.7800 ⁻ -03	3.4355	1.3936	2.2345 ⁺ +04	2.2345 ⁺ +04			
2.9465 ⁻ -01	2.5516 ⁺ +05	1.0000	8.2457 ⁺ +03	NM	1.8187	1.8094	3.2088 ⁺ +02	1.8882 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	3.5338 ⁻ -04	0.0000 ⁺ +00	0.0948	4.5577 ⁻ -04	5.8406 ⁺ +02	3.2088 ⁺ +02			
55010503	2.2360	1.0000	6.4676 ⁺ +03	1.6800 ⁻ -03	3.3771	1.3583	2.2511 ⁺ +04	2.2511 ⁺ +04			
3.9624 ⁻ -01	2.5466 ⁺ +05	1.0000	1.0904 ⁺ +04	NM	1.8194	1.8091	3.2093 ⁺ +02	1.8927 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	4.8685 ⁻ -04	0.0000 ⁺ +00	0.0946	6.0043 ⁻ -04	5.8328 ⁺ +02	3.2093 ⁺ +02			
55010504	2.2440	1.0000	1.2299 ⁺ +04	1.6230 ⁻ -03	3.3542	1.3268	2.2142 ⁺ +04	2.2142 ⁺ +04			
8.0263 ⁻ -01	2.5364 ⁺ +05	1.0000	2.0797 ⁺ +04	NM	1.8139	1.8014	3.2087 ⁺ +02	1.8867 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	8.9756 ⁻ -04	0.0000 ⁺ +00	0.0947	1.1618 ⁻ -03	5.8432 ⁺ +02	3.2087 ⁺ +02			
55010601	2.5020	1.0000	3.2766 ⁺ +03	1.4050 ⁻ -03	4.1376	1.5177	1.6838 ⁺ +04	1.6838 ⁺ +04			
1.9303 ⁻ -01	2.8059 ⁺ +05	1.0000	6.1082 ⁺ +03	NM	1.7868	1.7629	3.1896 ⁺ +02	1.5033 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	2.6505 ⁻ -04	0.0000 ⁺ +00	0.1033	3.7256 ⁻ -04	6.1505 ⁺ +02	3.1896 ⁺ +02			
55010602	2.5330	1.0000	4.9439 ⁺ +03	1.6100 ⁻ -03	3.9078	1.3366	1.5999 ⁺ +04	1.5999 ⁺ +04			
3.9624 ⁻ -01	2.8774 ⁺ +05	1.0000	9.3263 ⁺ +03	NM	1.8328	1.8227	3.1875 ⁺ +02	1.4827 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	4.1269 ⁻ -04	0.0000 ⁺ +00	0.1071	5.5469 ⁻ -04	6.1840 ⁺ +02	3.1875 ⁺ +02			
55010602*	2.5150	1.0000	4.8131 ⁺ +03	1.6100 ⁻ -03	3.9010	1.3552	1.5616 ⁺ +04	1.5616 ⁺ +04			
3.9624 ⁻ -01	2.7311 ⁺ +05	1.0000	9.0174 ⁺ +03	NM	1.8256	1.8144	3.1887 ⁺ +02	1.4946 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	4.1635 ⁻ -04	0.0000 ⁺ +00	0.1060	5.6277 ⁻ -04	6.1647 ⁺ +02	3.1887 ⁺ +02			
55010603*	2.4160	1.0000	8.8864 ⁺ +03	1.5600 ⁻ -03	3.6014	1.3176	1.8360 ⁺ +04	1.8360 ⁺ +04			
5.9945 ⁻ -01	2.7521 ⁺ +05	1.0000	1.6033 ⁺ +04	NM	1.8199	1.8090	3.1957 ⁺ +02	1.5619 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	6.8694 ⁻ -04	0.0000 ⁺ +00	0.1019	9.2982 ⁻ -04	6.0539 ⁺ +02	3.1957 ⁺ +02			
55010604	2.4510	1.0000	1.0348 ⁺ +04	1.5600 ⁻ -03	3.6873	1.2963	1.8165 ⁺ +04	1.8165 ⁺ +04			
8.0263 ⁻ -01	2.8757 ⁺ +05	1.0000	1.8920 ⁺ +04	NM	1.8310	1.8196	3.1932 ⁺ +02	1.5378 ⁺ +02			
INFINITE	3.3853 ⁺ +02	0.0000	8.0174 ⁻ -04	0.0000 ⁺ +00	0.1039	1.0615 ⁻ -03	6.0939 ⁺ +02	3.1932 ⁺ +02			

55010501		SHUTTS /H /W		PROFILE TABULATION		17 POINTS, DELTA AT POINT 17			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94770	0.00000	0.00000	1.90639	0.00000	
2	2.2860*-04	2.4574*+00	NM	0.97077	0.54113	0.66419	1.50654	0.44087	
3	2.7940*-04	2.5021*+00	NM	0.97122	0.54780	0.67063	1.49874	0.44786	
4	3.3274*-04	2.6016*+00	NM	0.97297	0.57359	0.69508	1.46848	0.47333	
5	4.3180*-04	2.7710*+00	NM	0.97381	0.58604	0.70661	1.45383	0.48604	
6	5.3574*-04	3.0734*+00	NM	0.97650	0.62561	0.74213	1.40719	0.52739	
7	6.8326*-04	3.2490*+00	NM	0.97798	0.64740	0.76095	1.38155	0.55079	
8	8.3820*-04	3.4660*+00	NM	0.97973	0.67319	0.78256	1.35132	0.57910	
9	9.8806*-04	3.7165*+00	NM	0.98164	0.70165	0.80558	1.31819	0.61112	
10	1.2446*-03	4.1336*+00	NM	0.98462	0.74655	0.84018	1.26656	0.66336	
11	1.6256*-03	4.3989*+00	NM	0.98639	0.77368	0.86010	1.23587	0.69594	
12	2.0066*-03	5.3183*+00	NM	0.99190	0.86083	0.91920	1.14042	0.80609	
13	2.3851*-03	6.0051*+00	NM	0.99548	0.92041	0.95579	1.07837	0.88633	
14	2.7661*-03	6.5040*+00	NM	0.99784	0.96132	0.97914	1.03742	0.94382	
15	3.4061*-03	6.9730*+00	NM	0.99990	0.98822	0.99907	1.00169	0.99738	
16	4.0386*-03	6.9961*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 17	4.6761*-03	6.9961*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55010502		SHUTTS /H /W		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94786	0.00000	0.00000	1.90076	0.00000	
2	2.2860*-04	2.5384*+00	NM	0.97175	0.55486	0.67686	1.48809	0.45485	
3	3.0226*-04	2.6816*+00	NM	0.97313	0.57538	0.69622	1.46414	0.47551	
4	3.8100*-04	2.8145*+00	NM	0.97437	0.59367	0.71308	1.44274	0.49425	
5	5.3848*-04	2.9729*+00	NM	0.97579	0.61461	0.73195	1.41818	0.51612	
6	7.3600*-04	3.1340*+00	NM	0.97719	0.63515	0.74995	1.39416	0.53792	
7	9.9314*-04	3.4665*+00	NM	0.97990	0.67529	0.78384	1.34733	0.58177	
8	1.2421*-03	3.7045*+00	NM	0.98172	0.70250	0.80583	1.31583	0.61241	
9	1.6281*-03	4.1465*+00	NM	0.98488	0.75022	0.84256	1.26131	0.66801	
10	2.1361*-03	4.6101*+00	NM	0.98791	0.79706	0.87638	1.20894	0.72491	
11	2.7737*-03	5.3629*+00	NM	0.99231	0.86753	0.92334	1.13281	0.81509	
12	3.4036*-03	6.0636*+00	NM	0.99594	0.92819	0.96023	1.07023	0.89722	
13	4.0437*-03	6.6209*+00	NM	0.99854	0.97368	0.98589	1.02523	0.96163	
14	5.3111*-03	6.9442*+00	NM	0.99995	0.99911	0.99953	1.00085	0.99869	
15	6.5786*-03	6.9557*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 16	7.8486*-03	6.9557*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55010503		SHUTTS /H /W		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94800	0.00000	0.00000	1.89595	0.00000	
2	2.2860*-04	2.3671*+00	NM	0.97015	0.53041	0.65270	1.51426	0.43104	
3	2.7940*-04	2.4483*+00	NM	0.97099	0.54293	0.66492	1.49983	0.44333	
4	3.8354*-04	2.6217*+00	NM	0.97270	0.56843	0.68925	1.47031	0.46878	
5	5.3086*-04	2.7491*+00	NM	0.97391	0.58631	0.70590	1.44951	0.48699	
6	7.8740*-04	3.0246*+00	NM	0.97639	0.62297	0.73891	1.40677	0.52525	
7	1.0414*-03	3.2570*+00	NM	0.97836	0.65206	0.76403	1.37294	0.55649	
8	1.4199*-03	3.5473*+00	NM	0.98067	0.68669	0.79262	1.33307	0.59458	
9	1.8009*-03	3.8497*+00	NM	0.98293	0.72048	0.81961	1.29409	0.63335	
10	2.4409*-03	4.3945*+00	NM	0.98667	0.77773	0.86240	1.22960	0.70137	
11	3.0759*-03	4.9118*+00	NM	0.98989	0.82826	0.89752	1.17422	0.76435	
12	4.3409*-03	5.9620*+00	NM	0.99559	0.92218	0.95661	1.07606	0.88899	
13	5.6134*-03	6.7334*+00	NM	0.99919	0.98524	0.99213	1.01404	0.97840	
14	6.1559*-03	6.9041*+00	NM	0.99993	0.99866	0.99929	1.00127	0.99803	
15	1.0698*-02	6.9098*+00	NM	0.99995	0.99911	0.99953	1.00085	0.99868	
D 16	1.3233*-02	6.9213*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

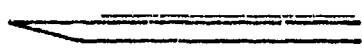
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55010504		SHUTTS /H /H		PROFILE TABULATION		25 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94782	0.00000	0.00000	1.90237	0.00000	
2	2.2860*-04	1.1174*+00	NM	0.96724	0.48752	0.61017	1.56641	0.38953	
3	2.7940*-04	2.1200*+00	NM	0.96727	0.48797	0.61062	1.56591	0.38895	
4	3.2760*-04	2.1173*+00	NM	0.96719	0.48663	0.60925	1.56743	0.38869	
5	4.3190*-04	2.1123*+00	NM	0.96719	0.48663	0.60925	1.56743	0.38869	
6	5.3594*-04	2.1123*+00	NM	0.96719	0.48663	0.60925	1.56743	0.38869	
7	6.8326*-04	2.3077*+00	NM	0.96934	0.51916	0.64221	1.53020	0.41969	
8	8.3820*-04	2.5263*+00	NM	0.97158	0.55258	0.67484	1.49142	0.45248	
9	1.0439*-03	2.8778*+00	NM	0.97499	0.60160	0.72043	1.43403	0.50238	
10	1.2421*-03	2.8344*+00	NM	0.97451	0.59581	0.71518	1.44083	0.49637	
11	1.4986*-03	3.0597*+00	NM	0.97650	0.62522	0.74148	1.40631	0.52722	
12	1.7526*-03	3.2937*+00	NM	0.97847	0.65419	0.76637	1.37238	0.55843	
13	2.1361*-03	3.4208*+00	NM	0.97949	0.66934	0.77906	1.35470	0.57508	
14	2.5146*-03	3.5589*+00	NM	0.98057	0.68538	0.79221	1.33604	0.59296	
15	3.1496*-03	3.8293*+00	NM	0.98259	0.71569	0.81633	1.30103	0.62745	
16	3.7846*-03	4.0911*+00	NM	0.98445	0.74376	0.83783	1.26895	0.66026	
17	4.4176*-03	4.3680*+00	NM	0.98631	0.77228	0.85885	1.23676	0.69444	
18	5.6871*-03	4.8740*+00	NM	0.98947	0.82175	0.89343	1.18208	0.75581	
19	6.9621*-03	5.3928*+00	NM	0.99243	0.86743	0.92460	1.13094	0.81755	
20	8.2296*-03	5.8996*+00	NM	0.99508	0.91355	0.95165	1.08515	0.87697	
21	1.0767*-02	6.7221*+00	NM	0.99894	0.98084	0.98979	1.01833	0.97197	
22	1.3310*-02	6.9327*+00	NM	0.99985	0.99733	0.99859	1.00254	0.99606	
23	1.5852*-02	6.9500*+00	NM	0.99993	0.99866	0.99930	1.00127	0.99803	
D 24	1.8390*-02	6.9672*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
25	2.0932*-02	6.9615*+00	NM	0.99998	0.99955	0.99977	1.00042	0.99934	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55010602		SHUTTS /H /H		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94155	0.00000	0.00000	2.14976	0.00000	
2	2.2860*-04	2.7948*+00	NM	0.96770	0.52310	0.66893	1.63529	0.40906	
3	2.5400*-04	2.8245*+00	NM	0.96797	0.52665	0.67237	1.62997	0.41251	
4	3.0480*-04	2.9798*+00	NM	0.96936	0.54481	0.68973	1.60278	0.43033	
5	4.0386*-04	3.2680*+00	NM	0.97179	0.57674	0.71924	1.55498	0.46254	
6	5.0800*-04	3.4588*+00	NM	0.97331	0.59692	0.73714	1.52500	0.48337	
7	6.0706*-04	3.5745*+00	NM	0.97420	0.60876	0.74743	1.50745	0.49582	
8	7.6200*-04	3.6371*+00	NM	0.97468	0.61508	0.75284	1.49811	0.50253	
9	9.1440*-04	3.8620*+00	NM	0.97633	0.63719	0.77139	1.46560	0.52633	
10	1.0668*-03	4.0488*+00	NM	0.97765	0.65495	0.78586	1.43969	0.54585	
11	1.3208*-03	4.2152*+00	NM	0.97878	0.67035	0.79809	1.41742	0.56306	
12	1.5748*-03	4.5692*+00	NM	0.98107	0.70193	0.82229	1.37233	0.59919	
13	1.8263*-03	4.8131*+00	NM	0.98257	0.72286	0.83769	1.34295	0.62377	
14	2.2123*-03	5.2149*+00	NM	0.98449	0.75602	0.86108	1.29725	0.66378	
15	2.5883*-03	5.5690*+00	NM	0.98681	0.78405	0.87993	1.25953	0.69862	
16	2.9718*-03	6.0903*+00	NM	0.98943	0.82353	0.90509	1.20789	0.74932	
17	3.4798*-03	6.5595*+00	NM	0.99162	0.85748	0.92550	1.16494	0.79446	
18	3.9878*-03	7.0597*+00	NM	0.99378	0.89222	0.94526	1.12243	0.84216	
19	4.4933*-03	7.6646*+00	NM	0.99619	0.93244	0.96683	1.07501	0.89937	
20	5.1308*-03	8.1643*+00	NM	0.99803	0.96447	0.98299	1.03878	0.94630	
21	5.7658*-03	8.5712*+00	NM	0.99944	0.98974	0.99519	1.01104	0.98432	
22	6.4033*-03	8.7200*+00	NM	0.99994	0.99882	0.99945	1.00127	0.99818	
23	7.1628*-03	8.7330*+00	NM	0.99998	0.99961	0.99982	1.00042	0.99939	
D 24	7.9173*-03	8.7395*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

rough 	M : 2 P THETA X 10 ⁻³ : 11 - 40 TW / TR : 1.0	5502
		ZPG (ROUGH) AW
Continuous wind tunnel with fixed symmetrical nozzles. W = 0.48, H = 0.70, L = 1.0 m. 0.18 < P0 < 0.3 MN/m ² . T0 : 340 K. Air. RE/m X 10 ⁻⁶ : 25.		
SHUTTS W.H. and FENTER F.W., 1955. Turbulent boundary layer and skin friction measurements on an artificially roughened, thermally insulated flat plate at supersonic speeds. DRL 366.		

1- The experimental arrangements are as for the previous entry. Shutts, Hartwig and Weiler, CAT 5501, in every to respect save that the surface of the plate and the floating elements of the shear stress balance was given
 -11 a coating of grinding compound grit. Small wires were inserted in the static holes during the coating so as to keep them clear. The balance annuli were cleared, and kept clear, with a thin-walled steel tube. The tests reported here used Aloxite grit of 120 and 180 grain. The corresponding mean particle diameters are 162 and 109 μm respectively (the particles are in fact very irregular in shape). The coating was made by spraying the grit into a bonding layer until no more would adhere. The plate was then cured at about 320 K for three hours. "This procedure gave excellent results both from the standpoint of bonding and uniformity".

8 The coordinate Y is measured from the mean top of the roughness, a slip gauge being rested on the surface
 9 and contact with the probe found electrically. The static pressure through the boundary layer was assumed
 11 constant, and Sutherland's viscosity law was used. The authors' assumption of isoenergetic flow has been
 12 replaced by the Crocco / Van Driest temperature-velocity correlation. Additional tests were made at boundary layer edge Mach numbers of 1.62, 1.66, 1.73, 2.10, 2.18 and 2.33 with roughnesses of mean diameter 54 and 141 μm , but since no balance readings were taken in conjunction with these tests, they are not presented here. For the M = 2 series, the editors have interpolated the reported CF values to X-stations corresponding
 13 to the velocity profiles. The profiles consist of two sets at a common unit Reynolds number, one for each of the roughness sizes. Series 01 describes the boundary layer with mean roughness diameter of 109 μm , while series 02 describes the 162 μm diameter case. There are, additionally, two profiles, 0301 and 0401, for the
 14 162 μm roughness in which the unit Reynolds number has been perturbed by changing the reservoir conditions. CF values are given only for the series 01 and 02.

§ DATA: 5502 0101-0401. Pitot profiles. NX = 5. CF measured with an FEB separately. Roughened surface.

15 Editors' comments

The entry describes one of the very few available experiments in which a boundary layer has developed over a uniformly rough surface. Other relevant tests, also made at the DRL, are those of Fenter & Lyons - CAT 5804 and Young - CAT 6506. A general description of the programme to 1959 is given by Fenter (1960).

The profiles are described in moderate detail, and in most cases measurements extended within the momentum deficit peak. The authors comment that "considerable scatter exists in the skin friction data for rough surfaces. This scatter may be attributed to experimental difficulties; for example, there was a tendency for loosened roughness particles to foul the narrow gaps which surround the floating discs of the skin friction balances." The original paper contains a further 75 profiles without associated CF values.

CAT 5502		SHUTTS /FENTER		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN X * RZ	MD * POD* TOD*	TW/TR* PW/PD* SW *	RED2W RED2D D2	CF * CO PI2*	H12 H32 H42	H12K H32K D2K	PW TW UD	PO TD TR		
55020101 2.9474*-01 INFINITE	2.0220 2.3637*+05 3.3853*+02	1.0000 1.0000 0.0000	1.0533*+04 1.6416*+04 6.8207*-04	3.2100*-03 NM 0.0000*+00	3.1490 1.7689 0.0628	1.4397 1.7542 8.7791*-04	2.9192*+04 3.2270*+02 5.5326*+02	2.9192*+04 1.8624*+02 3.2270*+02		
55020102 3.9624*-01 INFINITE	1.9960 2.3569*+05 3.3853*+02	1.0000 1.0000 0.0000	1.3719*+04 2.1182*+04 8.7226*-04	3.0100*-03 NM 0.0000*+00	3.0788 1.7696 0.0816	1.4181 1.7568 1.1166*-03	3.0311*+04 3.2292*+02 5.4931*+02	3.0311*+04 1.8841*+02 3.2292*+02		
55020103 4.9774*-01 INFINITE	2.0130 2.3806*+05 3.3853*+02	1.0000 1.0000 0.0000	1.6891*+04 2.6239*+04 1.0780*-03	2.8700*-03 NM 0.0000*+00	3.1190 1.7678 0.0823	1.4284 1.7529 1.3851*-03	2.9816*+04 3.2277*+02 5.5190*+02	2.9816*+04 1.8699*+02 3.2277*+02		
55020104 5.9954*-01 INFINITE	2.0290 2.4314*+05 3.3853*+02	1.0000 1.0000 0.0000	1.9144*+04 2.9911*+04 1.2121*-03	2.7800*-03 NM 0.0000*+00	3.1174 1.7716 0.0832	1.4076 1.7573 1.5589*-03	2.9703*+04 3.2263*+02 5.5431*+02	2.9703*+04 1.8566*+02 3.2263*+02		
55020105 7.0104*-01 INFINITE	2.0110 2.4280*+05 3.3853*+02	1.0000 1.0000 0.0000	2.2104*+04 3.4312*+04 1.3810*-03	2.7000*-03 NM 0.0000*+00	3.0657 1.7748 0.0825	1.3924 1.7612 1.7650*-03	3.0505*+04 3.2279*+02 5.5160*+02	3.0505*+04 1.8716*+02 3.2279*+02		
55020201 1.9294*-01 INFINITE	2.0110 2.3569*+05 3.3853*+02	1.0000 1.0000 0.0000	8.7363*+03 1.3562*+04 5.6228*-04	4.1600*-03 NM 0.0000*+00	3.2068 1.7551 0.0816	1.4890 1.7412 7.3067*-04	2.9611*+04 3.2279*+02 5.5160*+02	2.9611*+04 1.8716*+02 3.2279*+02		
55020202 3.9624*-01 INFINITE	2.0020 2.3637*+05 3.3853*+02	1.0000 1.0000 0.0000	1.4924*+04 2.3092*+04 9.5075*-04	3.4200*-03 NM 0.0000*+00	3.0644 1.7765 0.0822	1.4034 1.7636 1.2117*-03	3.0115*+04 3.2287*+02 5.5023*+02	3.0115*+04 1.8791*+02 3.2287*+02		
55020203 5.9954*-01 INFINITE	2.0260 2.3637*+05 3.3853*+02	1.0000 1.0000 0.0000	2.0457*+04 3.1929*+04 1.3291*-03	3.0000*-03 NM 0.0000*+00	3.0532 1.7846 0.0837	1.3675 1.7725 1.6916*-03	2.9011*+04 3.2266*+02 5.5386*+02	2.9011*+04 1.8591*+02 3.2266*+02		
55020204 8.0254*-01 INFINITE	2.0150 2.3637*+05 3.3853*+02	1.0000 1.0000 0.0000	2.6225*+04 4.0768*+04 1.6885*-03	2.6700*-03 NM 0.0000*+00	3.0320 1.7632 0.0831	1.3646 1.7710 2.1463*-03	2.9512*+04 3.2276*+02 5.5221*+02	2.9512*+04 1.8682*+02 3.2276*+02		
55020301 1.9294*-01 INFINITE	2.0200 2.3635*+05 3.2167*+02	1.0000 1.0000 0.0000	9.1715*+03 1.4336*+04 5.1297*-04	NM NM 0.0000*+00	3.1774 1.7692 0.0827	1.4623 1.7568 6.6082*-04	3.1759*+04 3.0682*+02 5.3918*+02	3.1759*+04 1.7723*+02 3.0682*+02		
55020401 1.9294*-01 INFINITE	2.0270 2.2202*+05 3.5353*+02	1.0000 1.0000 0.0000	6.9055*+03 1.0741*+04 5.0322*-04	NM NM 0.0000*+00	3.1688 1.7759 0.0833	1.4508 1.7438 6.4557*-04	2.7306*+04 3.3695*+02 5.6615*+02	2.7306*+04 1.9406*+02 3.3695*+02		

55020101		SHUTTS /FENTER		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/U0	T/TD	RHO/RHO0*U/U0	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.95322	0.00000	0.00000	1.73266	0.00000	
2	2.2860 ⁻ 04	1.5615 ⁺ 00	NM	0.96522	0.40752	0.50649	1.54471	0.32789	
3	2.7432 ⁻ 04	1.6055 ⁺ 00	NM	0.96592	0.42087	0.52120	1.53363	0.33985	
4	3.2512 ⁻ 04	1.6950 ⁺ 00	NM	0.96729	0.44609	0.54856	1.51218	0.36276	
5	3.8862 ⁻ 04	1.8037 ⁺ 00	NM	0.96884	0.47379	0.57793	1.48794	0.38841	
6	4.8006 ⁻ 04	1.8776 ⁺ 00	NM	0.96963	0.49110	0.59592	1.47247	0.40471	
7	5.7912 ⁻ 04	1.9656 ⁺ 00	NM	0.97095	0.51039	0.61564	1.45497	0.42313	
8	7.0612 ⁻ 04	2.0373 ⁺ 00	NM	0.97182	0.52522	0.63056	1.44135	0.43748	
9	7.9248 ⁻ 04	2.0794 ⁺ 00	NM	0.97231	0.53363	0.63892	1.43357	0.44569	
10	9.3472 ⁻ 04	2.1510 ⁺ 00	NM	0.97314	0.54748	0.65255	1.42068	0.45932	
11	1.0439 ⁻ 03	2.2716 ⁺ 00	NM	0.97447	0.56973	0.67406	1.39977	0.48155	
12	1.1633 ⁻ 03	2.3557 ⁺ 00	NM	0.97537	0.58457	0.68814	1.38572	0.49659	
13	1.4402 ⁻ 03	2.4931 ⁺ 00	NM	0.97678	0.60781	0.70976	1.36358	0.52051	
14	1.6739 ⁻ 03	2.6374 ⁺ 00	NM	0.97821	0.63106	0.73086	1.34130	0.54489	
15	2.1895 ⁻ 03	2.9183 ⁺ 00	NM	0.98082	0.67359	0.76812	1.30038	0.59069	
16	2.6975 ⁻ 03	3.2205 ⁺ 00	NM	0.98343	0.71612	0.80367	1.25945	0.63811	
17	3.2131 ⁻ 03	3.5356 ⁺ 00	NM	0.98597	0.75767	0.83676	1.21968	0.68605	
18	5.7175 ⁻ 03	5.0787 ⁺ 00	NM	0.99631	0.93323	0.95979	1.05773	0.90741	
19	6.9926 ⁻ 03	5.5792 ⁺ 00	NM	0.99909	0.98318	0.99019	1.01430	0.97623	
20	8.2677 ⁻ 03	5.7175 ⁺ 00	NM	0.99981	0.99654	0.99800	1.00293	0.99508	
21	9.5377 ⁻ 03	5.7330 ⁺ 00	NM	0.99989	0.99902	0.99886	1.00167	0.99719	
D 22	1.0815 ⁻ 02	5.7537 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55020103		SHUTTS /FENTER		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/U0	T/TD	RHO/RHO0*U/U0	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.95344	0.00000	0.00000	1.72615	0.00000	
2	2.2860 ⁻ 04	1.4267 ⁺ 00	NM	0.96312	0.36314	0.45578	1.57530	0.28933	
3	2.8194 ⁻ 04	1.4523 ⁺ 00	NM	0.96353	0.37258	0.46655	1.56809	0.29753	
4	3.4036 ⁻ 04	1.4732 ⁺ 00	NM	0.96393	0.38003	0.47501	1.56231	0.30404	
5	3.8354 ⁻ 04	1.5153 ⁺ 00	NM	0.96468	0.39444	0.49122	1.55093	0.31672	
6	4.9022 ⁻ 04	1.6241 ⁺ 00	NM	0.96645	0.42822	0.52852	1.52331	0.34695	
7	5.6642 ⁻ 04	1.7042 ⁺ 00	NM	0.96766	0.45057	0.55264	1.50438	0.36735	
8	7.0104 ⁻ 04	1.8160 ⁺ 00	NM	0.96924	0.47889	0.58254	1.47973	0.39368	
9	7.9756 ⁻ 04	1.8798 ⁺ 00	NM	0.97009	0.49379	0.59798	1.46650	0.40776	
10	1.0312 ⁻ 03	2.0011 ⁺ 00	NM	0.97162	0.52012	0.62474	1.44274	0.43302	
11	1.2929 ⁻ 03	2.1484 ⁺ 00	NM	0.97334	0.54943	0.65375	1.41580	0.46175	
12	1.6027 ⁻ 03	2.2854 ⁺ 00	NM	0.97486	0.57476	0.67817	1.39218	0.48713	
13	1.7958 ⁻ 03	2.3614 ⁺ 00	NM	0.97566	0.58818	0.69085	1.37958	0.50077	
14	4.3358 ⁻ 03	3.2937 ⁺ 00	NM	0.98428	0.72926	0.81377	1.24526	0.65351	
15	5.5956 ⁻ 03	3.7605 ⁺ 00	NM	0.98792	0.78937	0.86653	1.18843	0.72409	
16	6.8656 ⁻ 03	4.2066 ⁺ 00	NM	0.99109	0.84252	0.89919	1.13903	0.78903	
17	8.1356 ⁻ 03	4.6879 ⁺ 00	NM	0.99421	0.89617	0.93376	1.09030	0.85826	
18	9.4005 ⁻ 03	5.1224 ⁺ 00	NM	0.99680	0.94188	0.96507	1.04985	0.91925	
19	1.0676 ⁻ 02	5.4529 ⁺ 00	NM	0.99865	0.97516	0.98538	1.02107	0.96505	
20	1.1946 ⁻ 02	5.6149 ⁺ 00	NM	0.99952	0.99106	0.99479	1.00755	0.98734	
21	1.3216 ⁻ 02	5.6763 ⁺ 00	NM	0.99984	0.99702	0.99827	1.00251	0.99577	
D 22	1.4481 ⁻ 02	5.7072 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55020105		SHUTTS /FENTER		PROFILE TABULATION		28 POINTS, DELTA AT POINT 28			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/U0	T/TD	RHO/RHO0*U/U0	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.95350	0.00000	0.00000	1.72471	0.00000	
2	2.2850 ⁻ 04	1.4564 ⁺ 00	NM	0.96370	0.37444	0.46852	1.56563	0.29925	
3	2.6676 ⁻ 04	1.5034 ⁺ 00	NM	0.96453	0.39083	0.48704	1.55280	0.31366	
4	3.1750 ⁻ 04	1.5321 ⁺ 00	NM	0.96535	0.40676	0.50479	1.54004	0.32777	
5	4.1910 ⁻ 04	1.5988 ⁺ 00	NM	0.96610	0.42118	0.52067	1.52824	0.34070	
6	4.8260 ⁻ 04	1.6448 ⁺ 00	NM	0.96682	0.43461	0.53530	1.51704	0.35286	
7	5.8420 ⁻ 04	1.6931 ⁺ 00	NM	0.96755	0.44804	0.54977	1.50567	0.36513	
8	6.7310 ⁻ 04	1.7518 ⁺ 00	NM	0.96840	0.46345	0.56617	1.49240	0.37737	
9	7.9758 ⁻ 04	1.8390 ⁺ 00	NM	0.96961	0.48483	0.58856	1.47366	0.39939	
10	9.9758 ⁻ 04	1.9107 ⁺ 00	NM	0.97066	0.50323	0.60749	1.45726	0.41687	
11	1.1811 ⁻ 03	2.0083 ⁺ 00	NM	0.97175	0.52213	0.62659	1.44017	0.43508	
12	1.4529 ⁻ 03	2.1226 ⁺ 00	NM	0.97310	0.54500	0.64926	1.41921	0.45748	
13	1.7018 ⁻ 03	2.2664 ⁺ 00	NM	0.97405	0.56071	0.66674	1.40447	0.47330	
14	1.9931 ⁻ 03	2.2716 ⁺ 00	NM	0.97476	0.57283	0.67619	1.39335	0.48530	
15	2.3178 ⁻ 03	2.5202 ⁺ 00	NM	0.97734	0.61561	0.71610	1.35308	0.52923	
16	3.5082 ⁻ 03	2.7361 ⁺ 00	NM	0.97943	0.64993	0.74684	1.32048	0.56558	
17	4.7549 ⁻ 03	3.3679 ⁺ 00	NM	0.98260	0.70164	0.79108	1.27118	0.62232	
18	6.0401 ⁻ 03	3.8300 ⁺ 00	NM	0.98548	0.74888	0.82930	1.22630	0.67626	
19	7.2898 ⁻ 03	3.7807 ⁺ 00	NM	0.98812	0.79264	0.86289	1.18511	0.72811	
20	8.6030 ⁻ 03	4.1507 ⁺ 00	NM	0.99076	0.83690	0.89514	1.14402	0.78245	
21	9.8298 ⁻ 03	4.5109 ⁺ 00	NM	0.99315	0.87767	0.92336	1.10682	0.83424	
22	1.1100 ⁻ 02	4.9505 ⁺ 00	NM	0.99526	0.91447	0.94765	1.07189	0.88245	
23	1.2302 ⁻ 02	5.1661 ⁺ 00	NM	0.99711	0.94729	0.96840	1.04507	0.92664	
24	1.3647 ⁻ 02	5.3978 ⁺ 00	NM	0.99840	0.97066	0.98267	1.02490	0.95880	
25	1.4940 ⁻ 02	5.5487 ⁺ 00	NM	0.99922	0.98558	0.99156	1.01218	0.97963	
26	1.6183 ⁻ 02	5.6456 ⁺ 00	NM	0.99973	0.99503	0.99711	1.00419	0.99295	
27	1.7435 ⁻ 02	5.6916 ⁺ 00	NM	0.99997	0.99950	0.99971	1.00042	0.99929	
D 28	1.8727 ⁻ 02	5.6969 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55020201		SHUTTS /FENTER		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95350	0.00000	0.00000	1.72471	0.00000	
2	2.2860*-04	1.6241*+00	NM	0.96650	0.42864	0.52882	1.52204	0.34744	
3	3.5830*-04	1.7211*+00	NM	0.96796	0.45549	0.55773	1.49928	0.37200	
4	5.2070*-04	1.8603*+00	NM	0.96989	0.48281	0.59371	1.46926	0.40409	
5	6.4762*-04	1.9633*+00	NM	0.97120	0.51260	0.61708	1.44875	0.42594	
6	7.7470*-04	2.0325*+00	NM	0.97205	0.52710	0.63156	1.43564	0.43992	
7	9.0678*-04	2.1098*+00	NM	0.97295	0.54252	0.64682	1.42150	0.45503	
8	1.0236*-03	2.2145*+00	NM	0.97413	0.56241	0.66618	1.40308	0.47480	
9	1.1532*-03	2.3415*+00	NM	0.97551	0.58528	0.68797	1.38170	0.49792	
10	1.4122*-03	2.4961*+00	NM	0.97710	0.61164	0.71246	1.35685	0.52598	
11	1.6637*-03	2.6912*+00	NM	0.97901	0.64296	0.74070	1.32711	0.55813	
12	2.2987*-03	3.1907*+00	NM	0.98339	0.71457	0.80174	1.25887	0.63687	
13	2.9312*-03	3.6648*+00	NM	0.98725	0.77822	0.85201	1.19863	0.71082	
14	3.5687*-03	4.1550*+00	NM	0.99077	0.83739	0.89549	1.14356	0.78307	
15	4.1986*-03	4.6741*+00	NM	0.99418	0.89557	0.93532	1.09072	0.85752	
16	4.8387*-03	5.1661*+00	NM	0.99711	0.94729	0.96840	1.04507	0.92664	
17	5.4712*-03	5.6302*+00	NM	0.99897	0.98110	0.98891	1.01598	0.97336	
18	6.1037*-03	5.6251*+00	NM	0.99962	0.99304	0.99595	1.00586	0.99014	
19	6.7437*-03	5.6661*+00	NM	0.99984	0.99702	0.99827	1.00251	0.99577	
20	7.3787*-03	5.6712*+00	NM	0.99987	0.99751	0.99856	1.00209	0.99647	
21	8.0137*-03	5.6918*+00	NM	0.99997	0.99790	0.99971	1.00042	0.99929	
D 22	9.0297*-03	5.6969*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

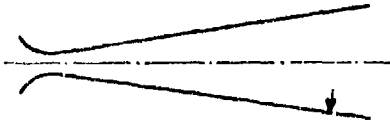
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55020203		SHUTTS /FENTER		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95311	0.00000	0.00000	1.73556	0.00000	
2	2.2860*-04	1.6553*+00	NM	0.96659	0.43435	0.53622	1.52406	0.35184	
3	3.6068*-04	1.7079*+00	NM	0.96738	0.44867	0.55165	1.51172	0.36491	
4	4.6736*-04	1.7970*+00	NM	0.96865	0.47137	0.57572	1.49175	0.38594	
5	6.1214*-04	1.8689*+00	NM	0.96961	0.48815	0.59321	1.47672	0.40171	
6	7.2340*-04	1.9333*+00	NM	0.97044	0.50247	0.60799	1.46373	0.41532	
7	8.6614*-04	1.9797*+00	NM	0.97102	0.51234	0.61794	1.45469	0.42479	
8	1.0033*-03	2.0252*+00	NM	0.97157	0.52172	0.62737	1.44604	0.43386	
9	1.1227*-03	2.0895*+00	NM	0.97233	0.53455	0.64015	1.43413	0.44637	
10	1.2446*-03	2.1432*+00	NM	0.97294	0.54492	0.65036	1.42444	0.45057	
11	1.3614*-03	2.1958*+00	NM	0.97354	0.55479	0.65998	1.41517	0.46636	
12	1.4961*-03	2.2361*+00	NM	0.97398	0.56219	0.66714	1.40818	0.47376	
13	2.1514*-03	2.4426*+00	NM	0.97617	0.59822	0.70320	1.37390	0.51037	
14	2.7711*-03	2.6240*+00	NM	0.97798	0.62784	0.72825	1.34545	0.54127	
15	3.4036*-03	2.8014*+00	NM	0.97965	0.65499	0.75231	1.31926	0.57025	
16	4.0386*-03	2.9833*+00	NM	0.98127	0.68164	0.77524	1.29349	0.59934	
17	5.3086*-03	3.3457*+00	NM	0.98436	0.73149	0.81632	1.24539	0.65547	
18	7.8408*-03	4.0826*+00	NM	0.98989	0.82280	0.86565	1.15860	0.76441	
19	1.0384*-02	4.8131*+00	NM	0.99463	0.90375	0.91103	1.08420	0.86795	
20	1.2929*-02	5.4375*+00	NM	0.99822	0.96742	0.98084	1.02792	0.94519	
21	1.5469*-02	5.6918*+00	NM	0.99957	0.99210	0.99543	1.00671	0.98879	
22	1.8011*-02	5.7433*+00	NM	0.99984	0.99704	0.99829	1.00251	0.99579	
23	2.0549*-02	5.7537*+00	NM	0.99989	0.99803	0.99886	1.00167	0.99719	
D 24	2.3089*-02	5.7744*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

55020204		SHUTTS /FENTER		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95339	0.00000	0.00000	1.72759	0.00000	
2	2.2860*-04	1.5857*+00	NM	0.96579	0.41638	0.51572	1.53408	0.33617	
3	4.0640*-04	1.6571*+00	NM	0.96691	0.43720	0.53845	1.51665	0.35502	
4	4.2164*-04	1.6678*+00	NM	0.96707	0.44020	0.54166	1.51412	0.35774	
5	5.5372*-04	1.7498*+00	NM	0.96827	0.46203	0.56499	1.49533	0.37784	
6	5.6134*-04	1.7596*+00	NM	0.96841	0.46452	0.56762	1.49317	0.38014	
7	6.8326*-04	1.8098*+00	NM	0.96911	0.47692	0.58065	1.48228	0.39173	
8	6.8580*-04	1.8160*+00	NM	0.96919	0.47841	0.58220	1.48097	0.39312	
9	4.5980*-04	1.9018*+00	NM	0.97032	0.49826	0.60273	1.46327	0.41190	
10	1.1887*-03	2.0083*+00	NM	0.97165	0.52109	0.62587	1.44258	0.43385	
11	1.4656*-03	2.0744*+00	NM	0.97249	0.53449	0.63922	1.43029	0.44642	
12	2.0980*-03	2.2716*+00	NM	0.97465	0.57171	0.67541	1.39568	0.48393	
13	2.7280*-03	2.4221*+00	NM	0.97624	0.59801	0.70018	1.37088	0.51075	
14	3.9954*-03	2.7200*+00	NM	0.97718	0.64615	0.74380	1.32596	0.56133	
15	5.2634*-03	2.9867*+00	NM	0.98161	0.68586	0.77810	1.28708	0.60495	
16	6.5324*-03	3.2827*+00	NM	0.98413	0.72705	0.81212	1.24772	0.65089	
17	7.8029*-03	3.5628*+00	NM	0.98637	0.76377	0.84113	1.21282	0.69393	
18	1.0348*-02	4.1422*+00	NM	0.99059	0.83424	0.89340	1.14685	0.77990	
19	1.2880*-02	4.7202*+00	NM	0.99436	0.89376	0.93751	1.08889	0.86161	
20	1.5420*-02	5.2247*+00	NM	0.99733	0.95136	0.97097	1.04161	0.93216	
21	1.7960*-02	5.5335*+00	NM	0.99903	0.98213	0.98954	1.01514	0.97478	
22	2.0500*-02	5.6558*+00	NM	0.99968	0.99403	0.99654	1.00503	0.99156	
23	2.3040*-02	5.6949*+00	NM	0.99989	0.99801	0.99885	1.00167	0.99718	
D 24	2.4369*-02	5.7175*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

	M : 5 - 8.2 R THETA X 10 ⁻³ : 5 - 13 YW/TR : 0.5 - 1.0	5503
		FG-MHT/SHT
Continuous tunnel with two-dimensional adjustable wedge nozzle. W = H = 0.12 m. 0.3 < P ₀ < 3.2 MN/m ² . 320 < T ₀ < 660 K Air: 7 < RE/m X 10 ⁻⁶ < 18.		
LOBB R.K., WINKLER E.M. and PERSH J., 1955. NOL Hypersonic tunnel No. 4 results VII: Experimental investigation of turbulent boundary layers in hypersonic flow. NOL NAVORD Rep. 3880.		

- 1 The test boundary layer was formed on one of the straight diverging walls of the tunnel nozzle. The test station was in the centre of the wall approximately 0.5 m downstream of the throat [E]. The wall was actively cooled and remained close to room temperature everywhere except at the throat, where it approached recovery temperature. Surface probe tests indicated that transition took place just downstream of the throat.
- 4
- 3
- 6 Static pressure was measured at a tapping of 0.64 mm diameter, and the wall temperature was measured by four thermocouples embedded at various distances from the surface. After 10-20 minutes of tunnel operation these recorded a linear variation, giving the local heat-flux and the surface temperature. Previous investigations had shown that lateral temperature variations were negligible.
- 8 Probes were mounted on a sting about 0.3 m long [E] which swung about a pivot mounted in the diffuser about 0.2 m downstream of the nozzle exit plane. The path of the probe tips was thus slightly curved. The
- 7 Pitot profile was measured with a FPP ($h_1 = 0.25$, $l = 70$ mm [E]). Total temperatures were recorded with a STP (Winkler, 1954) of the single shield vented type. The probe used near the wall was flattened ($h_1 = 0.96$ mm) while elsewhere a circular probe was used (E) of about 6 mm [E] diameter. A CCP ($\alpha = 8^\circ$, $d = 3$ mm [E], $l_1 = 17d$, $l_2 = 70$ mm [E]) was used, but since the static pressure outside the boundary layer was within
- 9 1 % of the wall value, it was assumed that the normal pressure gradient was negligible. The temperature gradient in the wall gave a heat flux value which was used to compute the wall temperature gradient in the flow, and the measured T₀ profile was faired in to meet this. The authors have interpolated the T₀ readings to the Y-values of the PT2 readings.
- 12 The editors have presented all the measured profiles, incorporating the author's assumptions and procedure. The C_f value given is that estimated by the authors from the limiting slope of the velocity profile. The
- 13 profiles fall into five Mach number groups. Within the groups for M = 5, 6 and 7 there is a range of heat
- 14 transfer conditions. C_Q and C_F are also given.
- § DATA: 55030101 - 1301. Pitot and T₀ profiles obtained separately. NX = 1. C_Q from temperature profile in wall.
- 15 Editors' comments

The experiment was a very early attempt at obtaining hypersonic cooled-wall data, and in consequence it is not surprising that it is not ideally arranged. The pressure gradient at the test station is not large, but as in all nozzle tests there has been a continuous FPG history. If radial flow is assumed, the high Mach number approximation gives $(1/p)(dp/dx) = -\gamma/x$. The authors state that "the Mach number rise is about 3 % per tunnel caliber at M = 5 and decreases with increasing Mach number". The tests were made on a straight wall so that no pronounced normal pressure gradient effects are expected, and the authors quote a 1 % variation across the layer.

The skin friction data are dubious since they were obtained from the velocity gradient. On a log-law plot, the profiles suggested that in most cases C_f was underestimated. It seems probable that they still display some transitional characteristics. The profiles include data close to the wall in a range for which the

TO data was interpolated. No description is given of any tests to check for cross-flow effects.

A flow of generally the same type is described by Pasiuk et al. - CAT 6504. Other planar straight wall flows are described by Michel - CAT 6902 and Voisin et Lee - CAT 7304. More strictly comparable are the axisymmetric straight wall nozzle tests of Hill - CAT 5901 and Perry & East - CAT 6801.

CAT 5503		LOBB		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PM	PD			
X	POD*	PH/PDA	RED20	CG *	H32	H32K	TM*	TD			
RZ	YOD*	SW *	D2	P12	H42	D2K	UD	TR			
55030101	4.9300	1.0117	1.0238 ⁺⁰³	1.0900 ⁻⁰³	11.4317	1.4166	6.4028 ⁺⁰²	6.4028 ⁺⁰²			
NM	3.1208 ⁺⁰⁵	1.0000	4.7764 ⁺⁰³	NM	1.8418	1.7922	3.0081 ⁺⁰²	5.5520 ⁺⁰¹			
INFINITE	3.2540 ⁺⁰²	0.0000	6.4228 ⁻⁰⁴	NM	0.1126	1.4230 ⁻⁰³	7.3651 ⁺⁰²	2.9733 ⁺⁰²			
55030102	5.0100	0.7800	1.7043 ⁺⁰³	1.0900 ⁻⁰³	8.7442	1.3858	9.4833 ⁺⁰²	9.4833 ⁺⁰²			
NM	5.0764 ⁺⁰⁵	1.0000	6.3683 ⁺⁰³	1.3280 ⁻⁰⁴	1.8255	1.7832	2.8400 ⁺⁰²	6.6229 ⁺⁰¹			
INFINITE	3.9870 ⁺⁰²	0.0000	7.4202 ⁻⁰⁴	NM	0.5266	1.4726 ⁻⁰³	8.1747 ⁺⁰²	3.6412 ⁺⁰²			
55030103	5.0300	0.6302	2.5697 ⁺⁰³	9.4300 ⁻⁰⁴	6.9886	1.4002	1.4517 ⁺⁰³	1.4517 ⁺⁰³			
NM	7.9540 ⁺⁰⁵	1.0000	7.7559 ⁺⁰³	2.0420 ⁻⁰⁴	1.8186	1.7812	2.9524 ⁺⁰²	8.4651 ⁺⁰¹			
INFINITE	5.1300 ⁺⁰²	0.0000	8.4816 ⁻⁰⁴	NM	0.7817	1.5288 ⁻⁰³	9.2788 ⁺⁰²	4.6845 ⁺⁰²			
55030104	4.0600	0.5831	2.6601 ⁺⁰³	9.1800 ⁻⁰⁴	6.6740	1.3998	1.5325 ⁺⁰³	1.5325 ⁺⁰³			
NM	8.6937 ⁺⁰⁵	1.0000	7.4927 ⁺⁰³	NM	1.8180	1.7801	2.9921 ⁺⁰²	9.1819 ⁺⁰¹			
INFINITE	5.6200 ⁺⁰²	0.0000	8.7003 ⁻⁰⁴	NM	0.8309	1.5243 ⁻⁰³	9.7214 ⁺⁰²	5.1310 ⁺⁰²			
55030105	5.7500	0.8943	2.0509 ⁺⁰³	8.2000 ⁻⁰⁴	12.5747	1.3491	1.1155 ⁺⁰³	1.1155 ⁺⁰³			
NM	1.3578 ⁺⁰⁶	1.0000	1.0733 ⁺⁰⁴	4.8800 ⁻⁰⁵	1.8243	1.7786	3.2621 ⁺⁰²	5.2677 ⁺⁰¹			
INFINITE	4.0100 ⁺⁰²	0.0000	6.5611 ⁻⁰⁴	NM	0.3860	1.6179 ⁻⁰³	8.3673 ⁺⁰²	3.6477 ⁺⁰²			
55030106	5.7900	0.8146	2.6756 ⁺⁰³	7.2500 ⁻⁰⁴	10.5036	1.3942	1.3368 ⁺⁰³	1.3368 ⁺⁰³			
NM	1.6972 ⁺⁰⁶	1.0000	3.2849 ⁺⁰⁴	9.6700 ⁻⁰⁵	1.8261	1.7832	3.3117 ⁺⁰²	5.8016 ⁺⁰¹			
INFINITE	4.4700 ⁺⁰²	0.0000	7.5245 ⁻⁰⁴	NM	0.6256	1.6636 ⁻⁰³	8.8422 ⁺⁰²	4.0655 ⁺⁰²			
55030107	5.8200	0.6240	2.8554 ⁺⁰³	7.1000 ⁻⁰⁴	8.4694	1.3847	1.3108 ⁺⁰³	1.3108 ⁺⁰³			
NM	1.7175 ⁺⁰⁶	1.0000	1.0739 ⁺⁰⁴	1.4760 ⁻⁰⁴	1.8236	1.7793	3.1267 ⁺⁰²	7.0873 ⁺⁰¹			
INFINITE	5.5100 ⁺⁰²	0.0000	8.6265 ⁻⁰⁴	NM	0.8611	1.7503 ⁻⁰³	9.8237 ⁺⁰²	5.0107 ⁺⁰²			
55030108	6.8300	0.6779	1.3530 ⁺⁰³	6.8300 ⁻⁰⁴	13.9318	1.4996	4.3761 ⁺⁰²	4.3761 ⁺⁰²			
NM	1.5503 ⁺⁰⁶	1.0000	7.4810 ⁺⁰³	1.2110 ⁻⁰⁴	1.8264	1.7629	2.8720 ⁺⁰²	4.5267 ⁺⁰¹			
INFINITE	4.6760 ⁺⁰²	0.0000	7.8097 ⁻⁰⁴	NM	0.6944	2.1165 ⁻⁰³	9.2135 ⁺⁰²	4.2368 ⁺⁰²			
55030109	6.7800	0.5652	1.8403 ⁺⁰³	6.6600 ⁻⁰⁴	11.7847	1.4583	6.3218 ⁺⁰²	6.3218 ⁺⁰²			
NM	2.1380 ⁺⁰⁶	1.0000	8.2759 ⁺⁰³	1.6400 ⁻⁰⁴	1.8191	1.7680	3.0015 ⁺⁰²	5.7487 ⁺⁰¹			
INFINITE	5.8600 ⁺⁰²	0.0000	8.6375 ⁻⁰⁴	NM	0.8363	2.1240 ⁻⁰³	1.0307 ⁺⁰³	5.3103 ⁺⁰²			
55030110	6.8300	0.5596	2.5703 ⁺⁰³	5.9300 ⁻⁰⁴	10.4067	1.4302	8.1516 ⁺⁰²	8.1516 ⁺⁰²			
NM	2.8878 ⁺⁰⁶	1.0000	1.1623 ⁺⁰⁴	1.4390 ⁻⁰⁴	1.8200	1.7705	2.9711 ⁺⁰²	5.6729 ⁺⁰¹			
INFINITE	5.8600 ⁺⁰²	0.0000	9.1536 ⁻⁰⁴	NM	0.9591	2.1335 ⁻⁰³	1.0314 ⁺⁰³	5.3096 ⁺⁰²			
55030111	6.7800	0.5023	1.0876 ⁺⁰³	6.9400 ⁻⁰⁴	9.5165	1.4624	6.4117 ⁺⁰²	6.4117 ⁺⁰²			
NM	2.1884 ⁺⁰⁶	1.0000	7.9924 ⁺⁰³	1.8730 ⁻⁰⁴	1.8107	1.7650	2.9093 ⁺⁰²	6.2706 ⁺⁰¹			
INFINITE	6.3920 ⁺⁰²	0.0000	8.9057 ⁻⁰⁴	NM	0.9320	2.0524 ⁻⁰³	1.0764 ⁺⁰³	5.7924 ⁺⁰²			
55030112	7.6700	0.5144	1.4428 ⁺⁰³	5.9800 ⁻⁰⁴	12.3029	1.5342	3.2989 ⁺⁰²	3.2989 ⁺⁰²			
NM	2.4521 ⁺⁰⁶	1.0000	7.3864 ⁺⁰³	NM	1.8116	1.7511	2.9997 ⁺⁰²	5.0526 ⁺⁰¹			
INFINITE	6.4500 ⁺⁰²	0.0000	1.0749 ⁻⁰³	NM	1.0240	2.8446 ⁻⁰³	1.0931 ⁺⁰³	5.6317 ⁺⁰²			
55030113	8.1800	0.5076	1.5215 ⁺⁰³	5.3000 ⁻⁰⁴	11.3397	1.5065	2.8558 ⁺⁰²	2.8558 ⁺⁰²			
NM	3.2221 ⁺⁰⁶	1.0000	8.4555 ⁺⁰³	1.3710 ⁻⁰⁴	1.8160	1.7653	3.0030 ⁺⁰²	4.5542 ⁺⁰¹			
INFINITE	6.9500 ⁺⁰²	0.0000	1.1667 ⁻⁰³	NM	1.1591	2.8711 ⁻⁰³	1.1068 ⁺⁰³	5.9162 ⁺⁰²			

55030104		LOBB	PROFILE TABULATION 21 POINTS, DELTA AT POINT 21						
I	Y	P12/P	P/P11	T0/T00	M/M0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000 ⁺ 03	1.0000 ⁺ 00	NM	0.53389	0.00000	0.00000	3.26780	0.00000	
2	2.0000 ⁻ 04	2.014 ⁺ 00	NM	0.62890	0.22777	0.40000	3.03000	0.13201	
3	4.1000 ⁻ 04	3.4893 ⁺ 00	NM	0.67243	0.30037	0.50000	2.81500	0.17904	
4	4.7000 ⁻ 04	3.8799 ⁺ 00	NM	0.70705	0.31984	0.53900	2.80000	0.18979	
5	5.3000 ⁻ 04	4.4507 ⁺ 00	NM	0.71703	0.34530	0.57000	2.75000	0.20917	
6	6.6000 ⁻ 04	5.3218 ⁺ 00	NM	0.72629	0.38275	0.61000	2.50000	0.24016	
7	7.6000 ⁻ 04	5.9022 ⁺ 00	NM	0.73387	0.40524	0.63300	2.44000	0.25943	
8	7.9000 ⁻ 04	5.9363 ⁺ 00	NM	0.73599	0.40652	0.63500	2.44000	0.26025	
9	9.1000 ⁻ 04	6.5300 ⁺ 00	NM	0.74348	0.42820	0.65600	2.34700	0.27951	
10	1.0400 ⁻ 03	6.9320 ⁺ 00	NM	0.75051	0.44227	0.67000	2.29500	0.29194	
11	1.1700 ⁻ 03	7.2774 ⁺ 00	NM	0.75560	0.45400	0.68100	2.25000	0.30267	
12	1.4000 ⁻ 03	7.7136 ⁺ 00	NM	0.76601	0.46839	0.69600	2.20800	0.31522	
13	1.4200 ⁻ 03	7.7398 ⁺ 00	NM	0.76471	0.46924	0.69600	2.20000	0.31636	
14	1.6500 ⁻ 03	8.0563 ⁺ 00	NM	0.77353	0.47939	0.70700	2.17500	0.32506	
15	2.0300 ⁻ 03	8.6296 ⁺ 00	NM	0.78090	0.49725	0.72400	2.12000	0.34151	
16	2.6700 ⁻ 03	9.6917 ⁺ 00	NM	0.80363	0.52871	0.75200	2.02300	0.37173	
17	3.9400 ⁻ 03	1.2118 ⁺ 01	NM	0.83979	0.59433	0.80400	1.83000	0.43934	
18	9.0200 ⁻ 03	2.4884 ⁺ 01	NM	0.93517	0.81724	0.93000	1.29500	0.71815	
19	1.4100 ⁻ 02	3.0819 ⁺ 01	NM	0.98787	0.95956	0.98000	1.05800	0.93289	
20	1.9180 ⁻ 02	3.3297 ⁺ 01	NM	1.00065	0.99801	1.00000	1.00400	0.99602	
0 21	2.1720 ⁻ 02	3.3431 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P#PD

55030105		LOBU	PROFILE TABULATION 20 POINTS, DELTA AT POINT 20						
I	Y	P12/P	P/P11	T0/T00	M/M0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.81261	0.00000	0.00000	6.18600	0.00000	
2	2.8000 ⁻ 04	1.7748 ⁺ 00	NM	0.79082	0.16412	0.37100	5.11000	0.07260	
3	3.5000 ⁻ 04	2.0766 ⁺ 00	NM	0.81267	0.18746	0.42000	5.02000	0.08367	
4	4.1000 ⁻ 04	2.4637 ⁺ 00	NM	0.81968	0.21202	0.46300	4.81000	0.09667	
5	5.3000 ⁻ 04	3.2281 ⁺ 00	NM	0.83041	0.25219	0.53200	4.45000	0.11955	
6	6.1000 ⁻ 04	3.6674 ⁺ 00	NM	0.83396	0.27229	0.56200	4.26000	0.13192	
7	6.6000 ⁻ 04	3.9256 ⁺ 00	NM	0.83667	0.28339	0.57800	4.16000	0.13894	
8	7.9000 ⁻ 04	4.5026 ⁺ 00	NM	0.84579	0.30865	0.61100	3.97000	0.15390	
9	9.9000 ⁻ 04	5.2179 ⁺ 00	NM	0.85642	0.33315	0.64600	3.76000	0.17181	
10	1.1700 ⁻ 03	5.7964 ⁺ 00	NM	0.86036	0.35308	0.66900	3.59000	0.18635	
11	1.5500 ⁻ 03	6.4120 ⁺ 00	NM	0.86785	0.37310	0.69200	3.44000	0.20116	
12	1.6800 ⁻ 03	6.5851 ⁺ 00	NM	0.86984	0.37854	0.69800	3.40000	0.20529	
13	1.8100 ⁻ 03	6.8767 ⁺ 00	NM	0.87391	0.38752	0.70800	3.33000	0.21210	
14	2.1800 ⁻ 03	7.2708 ⁺ 00	NM	0.87980	0.39932	0.72100	3.26000	0.22117	
15	2.0200 ⁻ 03	8.2128 ⁺ 00	NM	0.89060	0.42621	0.74800	3.08000	0.24286	
16	3.4600 ⁻ 03	9.4163 ⁺ 00	NM	0.90209	0.45025	0.77700	2.87500	0.27026	
17	4.7300 ⁻ 03	1.1459 ⁺ 01	NM	0.92185	0.50799	0.81800	2.59300	0.31546	
18	6.0000 ⁻ 03	1.3885 ⁺ 01	NM	0.93976	0.56134	0.85500	2.37000	0.36853	
19	7.2700 ⁻ 03	1.8571 ⁺ 01	NM	0.95065	0.61502	0.88700	2.08000	0.42644	
20	8.5400 ⁻ 03	1.9639 ⁺ 01	NM	0.96933	0.67108	0.91400	1.85500	0.49272	
21	9.7900 ⁻ 03	2.2711 ⁺ 01	NM	0.97915	0.72288	0.93500	1.67300	0.55888	
22	1.1050 ⁻ 02	2.6241 ⁺ 01	NM	0.98595	0.77812	0.95300	1.50000	0.63533	
23	1.2320 ⁻ 02	2.9925 ⁺ 01	NM	0.99180	0.83189	0.96800	1.35400	0.71492	
24	1.4860 ⁻ 02	3.7140 ⁺ 01	NM	0.99675	0.92820	0.98800	1.13300	0.87202	
25	1.6100 ⁻ 02	4.0143 ⁺ 01	NM	0.99749	0.96546	0.99400	1.06000	0.93774	
26	1.7400 ⁻ 02	4.1827 ⁺ 01	NM	0.99782	0.98573	0.99700	1.02300	0.97458	
27	1.8400 ⁻ 02	4.2737 ⁺ 01	NM	0.99892	0.99651	0.99900	1.00500	0.99403	
0 28	1.9900 ⁻ 02	4.3933 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P#PD

55030111		LOBB		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23		
I	Y	P12/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHODAU/UD
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.45929	0.00000	0.00000	4.64110	0.00000
2	3.0700 ⁻ 04	1.3886 ⁺ 00	NM	0.52365	0.10342	0.22800	4.86000	0.04691
3	3.3000 ⁻ 04	1.4624 ⁺ 00	NM	0.53036	0.11170	0.24600	4.85000	0.05072
4	4.1000 ⁻ 04	1.7645 ⁺ 00	NM	0.54921	0.13842	0.30200	4.76000	0.06345
5	4.3000 ⁻ 04	1.8471 ⁺ 00	NM	0.56003	0.14437	0.31600	4.79100	0.06596
6	5.1000 ⁻ 04	2.2914 ⁺ 00	NM	0.57352	0.17097	0.36700	4.60800	0.07964
7	6.1000 ⁻ 04	3.0555 ⁺ 00	NM	0.59936	0.20675	0.43300	4.38600	0.09872
8	7.1000 ⁻ 04	3.8470 ⁺ 00	NM	0.62377	0.23751	0.48600	4.18700	0.11607
9	7.6000 ⁻ 04	4.2625 ⁺ 00	NM	0.63372	0.25205	0.50900	4.07800	0.12482
10	9.6000 ⁻ 04	5.6616 ⁺ 00	NM	0.68105	0.29560	0.58000	3.85000	0.15065
11	1.2200 ⁻ 03	6.9632 ⁺ 00	NM	0.71589	0.33087	0.63100	3.63700	0.17349
12	1.4500 ⁻ 03	7.8572 ⁺ 00	NM	0.73129	0.35303	0.65800	3.47400	0.18941
13	1.7000 ⁻ 03	8.3704 ⁺ 00	NM	0.73736	0.36514	0.67100	3.37700	0.19870
14	2.9700 ⁻ 03	1.0550 ⁺ 01	NM	0.76844	0.41257	0.72100	3.05400	0.23608
15	5.5100 ⁻ 03	1.5729 ⁺ 01	NM	0.81664	0.50776	0.79800	2.87000	0.23008
16	8.0500 ⁻ 03	2.1645 ⁺ 01	NM	0.06127	0.59888	0.85600	2.04300	0.41899
17	1.0590 ⁻ 02	2.8775 ⁺ 01	NM	0.90066	0.69160	0.90200	1.70100	0.53028
18	1.3130 ⁻ 02	3.7216 ⁺ 01	NM	0.93851	0.78801	0.94100	1.42600	0.65989
19	1.5676 ⁻ 02	4.6487 ⁺ 01	NM	0.97129	0.88182	0.97200	1.21500	0.80000
20	1.8210 ⁻ 02	5.5299 ⁺ 01	NM	0.98972	0.96254	0.99100	1.06000	0.93491
21	1.8850 ⁻ 02	5.6628 ⁺ 01	NM	0.98936	0.97414	0.99200	1.01700	0.94661
22	1.9480 ⁻ 02	5.8023 ⁺ 01	NM	0.99277	0.98616	0.99500	1.01800	0.97741
D 23	2.0120 ⁻ 02	5.9649 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

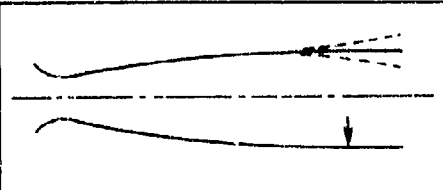
INPUT VARIABLES Y,U/UD,T/TD ASSUME PMPD

55030112		LOBB		PROFILE TABULATION		25 POINTS, DELTA AT POINT 25		
I	Y	P12/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHODAU/UD
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.46535	0.00000	0.00000	5.94060	0.00000
2	4.6000 ⁻ 04	1.2271 ⁺ 00	NM	0.51990	0.07154	0.17900	6.26000	0.02859
3	6.8000 ⁻ 04	1.6171 ⁺ 00	NM	0.52751	0.11185	0.27100	5.87000	0.04617
4	7.7000 ⁻ 04	1.8668 ⁺ 00	NM	0.55129	0.13001	0.31500	5.87000	0.05366
5	9.6000 ⁻ 04	2.7049 ⁺ 00	NM	0.58266	0.16914	0.39900	5.56500	0.07170
6	1.2200 ⁻ 03	3.7955 ⁺ 00	NM	0.61529	0.20830	0.47500	5.20000	0.09135
7	1.4700 ⁻ 03	4.9593 ⁺ 00	NM	0.64649	0.24359	0.53700	4.86000	0.11049
8	1.7300 ⁻ 03	5.7911 ⁺ 00	NM	0.67709	0.26457	0.57600	4.74000	0.12152
9	1.8500 ⁻ 03	6.2038 ⁺ 00	NM	0.69141	0.27472	0.59400	4.67500	0.12706
10	2.4900 ⁻ 03	8.0288 ⁺ 00	NM	0.73265	0.31569	0.65500	4.30500	0.15215
11	3.7600 ⁻ 03	1.0144 ⁺ 01	NM	0.75449	0.35726	0.70100	3.85000	0.18208
12	5.0300 ⁻ 03	1.2280 ⁺ 01	NM	0.77147	0.39482	0.73600	3.47500	0.21180
13	6.3000 ⁻ 03	1.4325 ⁺ 01	NM	0.79209	0.42787	0.76600	3.20800	0.23878
14	7.5700 ⁻ 03	1.6429 ⁺ 01	NM	0.80315	0.45902	0.78800	2.94700	0.26739
15	8.8400 ⁻ 03	1.8603 ⁺ 01	NM	0.81833	0.49283	0.81100	2.70800	0.29948
16	1.0110 ⁻ 02	2.1324 ⁺ 01	NM	0.83694	0.52474	0.83300	2.52000	0.33056
17	1.1380 ⁻ 02	2.4903 ⁺ 01	NM	0.84529	0.56800	0.85200	2.25000	0.37867
18	1.2650 ⁻ 02	2.7613 ⁺ 01	NM	0.86106	0.59867	0.86900	2.10700	0.41243
19	1.3920 ⁻ 02	3.1866 ⁺ 01	NM	0.88170	0.64386	0.89100	1.91500	0.46527
20	1.6460 ⁻ 02	4.0961 ⁺ 01	NM	0.90804	0.71119	0.92200	1.59000	0.57987
21	1.9000 ⁻ 02	5.2047 ⁺ 01	NM	0.93758	0.82524	0.95100	1.32800	0.71611
22	2.1540 ⁻ 02	6.4092 ⁺ 01	NM	0.96085	0.91654	0.97300	1.12700	0.86335
23	2.4080 ⁻ 02	7.4047 ⁺ 01	NM	0.98832	0.98564	0.99300	1.01500	0.97833
24	2.6620 ⁻ 02	7.6208 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
D 25	2.9160 ⁻ 02	7.6208 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME PMPD

55030113		LOBB		PROFILE TABULATION		19 POINTS, DELTA AT POINT 19		
I	Y	P12/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHODAU/UD
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.45873	0.00000	0.00000	6.59340	0.00000
2	1.0000 ⁻ 03	2.4225 ⁺ 00	NM	0.52095	0.14733	0.35500	5.80600	0.06114
3	1.3000 ⁻ 03	3.8097 ⁺ 00	NM	0.56830	0.19575	0.45500	5.40300	0.08421
4	1.4500 ⁻ 03	5.1370 ⁺ 00	NM	0.58666	0.23215	0.51400	4.90200	0.10486
5	1.6500 ⁻ 03	6.1348 ⁺ 00	NM	0.61998	0.23603	0.55800	4.75000	0.11747
6	2.2100 ⁻ 03	8.2923 ⁺ 00	NM	0.65873	0.30114	0.62300	4.28000	0.14356
7	2.5000 ⁻ 03	9.2349 ⁺ 00	NM	0.66958	0.31883	0.64400	4.08000	0.15784
8	3.7300 ⁻ 03	1.2208 ⁺ 01	NM	0.72228	0.36907	0.70800	3.68000	0.19239
9	4.9500 ⁻ 03	1.4813 ⁺ 01	NM	0.74824	0.40801	0.74500	3.33400	0.22346
10	6.2200 ⁻ 03	1.7419 ⁺ 01	NM	0.76713	0.44356	0.77300	3.03700	0.25453
11	8.8000 ⁻ 03	2.2765 ⁺ 01	NM	0.80619	0.50874	0.81700	2.57900	0.31679
12	1.1300 ⁻ 02	2.9026 ⁺ 01	NM	0.83157	0.57577	0.85400	2.20000	0.38818
13	1.3800 ⁻ 02	3.6457 ⁺ 01	NM	0.86106	0.64635	0.88600	1.87900	0.47193
14	1.6400 ⁻ 02	4.5671 ⁺ 01	NM	0.89189	0.72439	0.91600	1.59900	0.57286
15	1.8900 ⁻ 02	5.6676 ⁺ 01	NM	0.92023	0.80776	0.94200	1.36000	0.69265
16	2.1500 ⁻ 02	6.8593 ⁺ 01	NM	0.95032	0.88928	0.96600	1.18000	0.81864
17	2.4000 ⁻ 02	8.0451 ⁺ 01	NM	0.97542	0.96356	0.98500	1.04500	0.94258
18	2.5300 ⁻ 02	8.4240 ⁺ 01	NM	0.97799	0.98612	0.99300	1.01400	0.97929
D 19	2.6500 ⁻ 02	8.6615 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME PMPD

	M : 1.9 P THETA X 10 ⁻³ : 11 - 12 TW / TR : Approx. 1	5801
		(F) APG AW
Continuum flow tunnel with symmetrical flexible nozzle. W = H = 50.8 mm. P0 : 0.27 MN/m ² T0 : 300 K. Air. PE/m X 10 ⁻⁶ : 30.		
NALEID J.F. 1958. Experimental investigation of the impact pressure probe method of measuring local skin friction at supersonic speeds in presence of an adverse pressure gradient. DRL 432.		

- 1 The test boundary layer was formed on the floor of the wind tunnel. The roof of the tunnel was replaced by a flexible plate which could be deflected to cause a range of pressure gradients on the test wall. Measurements were made at a single station. The pressure history upstream of the test section was not given. The pressure was approximately constant for the first 50.8 mm of the flat floor, the imposed pressure gradients spreading over the following 76.2 mm. The pressure gradients (one favourable and seven adverse) ranged from - 41 to + 191 KN/m²/m and were found to be repeatable within the limits + 2 %, - 1 %. The test section floor had 11 static pressure tappings along the centre-line at 12.7 mm intervals. The survey station was midway between the 8th and 9th of these. Wall shear stress was measured with an FEB which had a circular element 6.35 mm in diameter, the maximum gap being 0.153 mm (designed by Moore - CAT 580G). The wall temperature was not reported but the "tunnel was operated for a sufficient length of time to permit all components of the balance to assume the operating temperature".
- 7 Only Pitot profiles were measured, with a CPP ($d_1 = 0.508$, $d_2 = 0.254$, $l = 13$ mm) at the same station. The tip of the probe was brought into contact with the wall for the lowest Y-reading. No corrections were applied to the profile data, and the Pitot probe was also treated as a Preston tube.
- 9 The author interpolated the PW values to give a local value for dp/dx at the survey station. This has been read into the data tabulation below to give a P12 value. The author's assumption of an isoenergetic boundary layer has been replaced by the Crocco / van Driest velocity temperature relation, and the static pressure in the boundary layer has been assumed constant. The edge reservoir state has been arbitrarily set at the reported tunnel reservoir state.
- 13 The eight profiles presented were measured in eight different pressure gradients with approximately the same edge state. The CF values associated with them are those directly measured with the FEB.
- 6 DATA: 58010101-0801. Pitot profiles. NX = 1. CF from an FEB measured separately.
- 15 Editors' comments
- The experiment represents an early attempt to determine the influence of pressure gradients on skin friction, and on the Preston tube calibration. The range of pressure gradients is small, and although arranged to occur with a near constant edge state, may be slightly confused by the varied upstream histories, which are not presented. The consequent CF variation is correspondingly small.
- At this low Mach number, the absence of a T0 determination is not important since the wall is near-adiabatic. The size of the Pitot probe is such that none of the profiles include measurements within the momentum-deficit peak, so that integral values must be treated with reserve. The profiles are so smooth that it seems probable that some smoothing or interpolation was employed which is not reported. The pressure gradient has little effect either in the log-law region or in the outer region.
- The most nearby comparable measurements are those of Thomas - CAT 7401.

CAT 5801 NALEID BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.									
RUN	MJ *	TW/TR*	REN2M	CF *	M12	M12K	QW	PD	
X	P0D*	PW/PD*	REN2D	CQ	M32	M32K	TW	TD	
RZ	T0D*	SW *	D2	P12*	M42	D2K	UD	TR	
58010101	1.9470	1.0000	7.5881 ⁺⁰³	1.8760 ⁻⁰³	2.9955	1.4459	3.7420 ⁺⁰⁴	3.7420 ⁺⁰⁴	
NM	2.6966 ⁺⁰⁵	1.0000	1.1633 ⁺⁰⁴	NM	1.8280	1.8121	2.8957 ⁺⁰²	1.7243 ⁺⁰²	
INFINITE	3.0317 ⁺⁰²	0.0000	3.5293 ⁻⁰⁴	-8.2662 ⁻⁰²	0.0816	4.2939 ⁻⁰⁴	5.1261 ⁺⁰²	2.8957 ⁺⁰²	
58010201	1.9970	1.0000	7.1509 ⁺⁰³	1.8480 ⁻⁰³	3.0664	1.4413	3.4625 ⁺⁰⁴	3.4625 ⁺⁰⁴	
NM	2.6966 ⁺⁰⁵	1.0000	1.1165 ⁺⁰⁴	NM	1.8245	1.8165	2.8917 ⁺⁰²	1.6664 ⁺⁰²	
INFINITE	3.0316 ⁺⁰²	0.0000	3.4620 ⁻⁰⁴	2.0531 ⁻⁰²	0.0812	4.2336 ⁻⁰⁴	5.1996 ⁺⁰²	2.8917 ⁺⁰²	
58010301	1.9360	1.0000	7.7816 ⁺⁰³	1.9160 ⁻⁰³	2.9831	1.4477	3.8040 ⁺⁰⁴	3.8040 ⁺⁰⁴	
NM	2.6949 ⁺⁰⁵	1.0000	1.1879 ⁺⁰⁴	NM	1.8166	1.8086	2.9045 ⁺⁰²	1.7375 ⁺⁰²	
INFINITE	3.0400 ⁺⁰²	0.0000	3.6028 ⁻⁰⁴	2.8967 ⁻⁰²	0.0809	4.3876 ⁻⁰⁴	5.1166 ⁺⁰²	2.9045 ⁺⁰²	
58010401	1.9200	1.0000	7.9377 ⁺⁰³	1.9000 ⁻⁰³	2.9643	1.4511	3.8994 ⁺⁰⁴	3.8994 ⁺⁰⁴	
NM	2.6949 ⁺⁰⁵	1.0000	1.2040 ⁺⁰⁴	NM	1.8137	1.8057	2.9085 ⁺⁰²	1.7515 ⁺⁰²	
INFINITE	3.0428 ⁺⁰²	0.0000	3.6333 ⁻⁰⁴	9.3128 ⁻⁰²	0.0801	4.4223 ⁻⁰⁴	5.0946 ⁺⁰²	2.9085 ⁺⁰²	
58010501	1.9180	1.0000	8.0191 ⁺⁰³	1.8800 ⁻⁰³	2.9719	1.4572	3.9066 ⁺⁰⁴	3.9066 ⁺⁰⁴	
NM	2.6915 ⁺⁰⁵	1.0000	1.2171 ⁺⁰⁴	NM	1.8100	1.8019	2.8821 ⁺⁰²	1.7370 ⁺⁰²	
INFINITE	3.0150 ⁺⁰²	0.0000	3.6267 ⁻⁰⁴	1.1534 ⁻⁰¹	0.0798	4.4267 ⁻⁰⁴	5.0683 ⁺⁰²	2.8821 ⁺⁰²	
58010601	1.8980	1.0000	8.1680 ⁺⁰³	1.8810 ⁻⁰³	2.9469	1.4610	4.0323 ⁺⁰⁴	4.0323 ⁺⁰⁴	
NM	2.6935 ⁺⁰⁵	1.0000	1.2306 ⁺⁰⁴	NM	1.8077	1.7996	2.8663 ⁺⁰²	1.7540 ⁺⁰²	
INFINITE	3.0178 ⁺⁰²	0.0000	3.6385 ⁻⁰⁴	1.6059 ⁻⁰¹	0.0787	4.4328 ⁻⁰⁴	5.0399 ⁺⁰²	2.8663 ⁺⁰²	
58010701	1.8830	1.0000	8.1978 ⁺⁰³	1.8770 ⁻⁰³	2.9262	1.4638	4.1210 ⁺⁰⁴	4.1210 ⁺⁰⁴	
NM	2.6898 ⁺⁰⁵	1.0000	1.2288 ⁺⁰⁴	NM	1.8082	1.8000	2.8780 ⁺⁰²	1.7598 ⁺⁰²	
INFINITE	3.0078 ⁺⁰²	0.0000	3.5994 ⁻⁰⁴	2.3228 ⁻⁰¹	0.0780	4.3702 ⁻⁰⁴	5.0083 ⁺⁰²	2.8780 ⁺⁰²	
58010801	1.8730	1.0000	8.2361 ⁺⁰³	1.9160 ⁻⁰³	2.9189	1.4679	4.1934 ⁺⁰⁴	4.1934 ⁺⁰⁴	
NM	2.6952 ⁺⁰⁵	1.0000	1.2288 ⁺⁰⁴	NM	1.8045	1.7964	2.9123 ⁺⁰²	1.7882 ⁺⁰²	
INFINITE	3.0428 ⁺⁰²	0.0000	3.6346 ⁻⁰⁴	3.8648 ⁻⁰¹	0.0774	4.4183 ⁻⁰⁴	5.0217 ⁺⁰²	2.9123 ⁺⁰²	

58010101 NALEID PROFILE TABULATION 22 POINTS, DELTA AT POINT 21									
I	Y	PT2/P	P/PD	T0/T03	M/ND	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.95515	0.00000	0.00000	1.67931	0.00000	
2	2.5900 ⁻⁰⁴	2.1719 ⁺⁰⁰	NM	0.97535	0.57268	0.67112	1.37335	0.48867	
3	5.1000 ⁻⁰⁴	2.4871 ⁺⁰⁰	NM	0.97571	0.63020	0.72473	1.32251	0.54800	
4	7.6500 ⁻⁰⁴	2.7751 ⁺⁰⁰	NM	0.98150	0.67745	0.76651	1.28019	0.59874	
5	1.0200 ⁻⁰³	3.0005 ⁺⁰⁰	NM	0.98354	0.71186	0.79565	1.24926	0.63690	
6	1.2750 ⁻⁰³	3.2000 ⁺⁰⁰	NM	0.98531	0.74165	0.82003	1.22251	0.67077	
7	1.5300 ⁻⁰³	3.4095 ⁺⁰⁰	NM	0.98698	0.76990	0.84241	1.19723	0.70363	
8	1.7850 ⁻⁰³	3.6135 ⁺⁰⁰	NM	0.98858	0.79712	0.86333	1.17300	0.73600	
9	2.0400 ⁻⁰³	3.8171 ⁺⁰⁰	NM	0.99011	0.82332	0.88285	1.14984	0.76780	
10	2.2950 ⁻⁰³	4.0152 ⁺⁰⁰	NM	0.99154	0.84797	0.90070	1.12822	0.79833	
11	2.5500 ⁻⁰³	4.2195 ⁺⁰⁰	NM	0.99295	0.87262	0.91804	1.10679	0.82946	
12	2.8050 ⁻⁰³	4.4078 ⁺⁰⁰	NM	0.99420	0.89471	0.93315	1.08778	0.85785	
13	3.0600 ⁻⁰³	4.6055 ⁺⁰⁰	NM	0.99548	0.91731	0.94822	1.06853	0.88741	
14	3.3150 ⁻⁰³	4.8178 ⁺⁰⁰	NM	0.99679	0.94041	0.96354	1.04863	0.91886	
15	3.5700 ⁻⁰³	4.9165 ⁺⁰⁰	NM	0.99738	0.95172	0.97039	1.03963	0.93341	
16	3.8250 ⁻⁰³	5.0781 ⁺⁰⁰	NM	0.99831	0.96867	0.98093	1.02559	0.95651	
17	4.0800 ⁻⁰³	5.1758 ⁺⁰⁰	NM	0.99890	0.97946	0.98761	1.01673	0.97137	
18	4.3350 ⁻⁰³	5.2590 ⁺⁰⁰	NM	0.99937	0.98819	0.99291	1.00959	0.98348	
19	4.5900 ⁻⁰³	5.3181 ⁺⁰⁰	NM	0.99970	0.99435	0.99662	1.00458	0.99208	
20	4.8450 ⁻⁰³	5.3480 ⁺⁰⁰	NM	0.99986	0.99743	0.99847	1.00208	0.99640	
D 21	5.1000 ⁻⁰³	5.3729 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
22	5.3550 ⁻⁰³	5.3530 ⁺⁰⁰	NM	0.99989	0.99795	0.99878	1.00166	0.99712	

INPUT VARIABLES Y, H ASSUME P=PD AND VAN DRIEST

58010201		NALEID	PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.95385	0.00000	0.00000	1.71465	0.00000
2	2.5500*-04	2.2606*+00	NM	0.97501	0.57486	0.67704	1.38707	0.48811
3	5.1000*-04	2.6217*+00	NM	0.97871	0.63645	0.73392	1.32972	0.55194
4	7.6500*-04	2.8980*+00	NM	0.98129	0.67902	0.77113	1.28969	0.59791
5	1.0200*-03	3.1412*+00	NM	0.98342	0.71407	0.80050	1.25671	0.63698
6	1.2750*-03	3.3532*+00	NM	0.98518	0.74311	0.82397	1.22945	0.67019
7	1.5300*-03	3.5706*+00	NM	0.98690	0.77166	0.84630	1.20281	0.70360
8	1.7850*-03	3.7880*+00	NM	0.98855	0.79920	0.86715	1.17727	0.73657
9	2.0400*-03	3.9901*+00	NM	0.99001	0.82374	0.88517	1.15471	0.76657
10	2.2950*-03	4.2159*+00	NM	0.99154	0.84977	0.90372	1.13099	0.79905
11	2.5500*-03	4.4122*+00	NM	0.99288	0.87281	0.91965	1.11022	0.82835
12	2.8050*-03	4.6146*+00	NM	0.99415	0.89534	0.93482	1.09013	0.85753
13	3.0600*-03	4.8131*+00	NM	0.99541	0.91688	0.94893	1.07114	0.88591
14	3.3150*-03	4.9925*+00	NM	0.99648	0.93590	0.96109	1.05454	0.91138
15	3.5700*-03	5.1612*+00	NM	0.99746	0.95343	0.97204	1.03941	0.93518
16	3.8250*-03	5.2886*+00	NM	0.99817	0.96645	0.98002	1.02828	0.95307
17	4.0800*-03	5.4228*+00	NM	0.99891	0.97997	0.98817	1.01681	0.97184
18	4.3350*-03	5.5083*+00	NM	0.99938	0.98848	0.99323	1.00964	0.98375
19	4.5900*-03	5.5518*+00	NM	0.99962	0.99299	0.99589	1.00586	0.99009
20	4.8450*-03	5.5945*+00	NM	0.99984	0.99700	0.99824	1.00251	0.99575
21	5.1000*-03	5.6149*+00	NM	0.99995	0.99900	0.99942	1.00084	0.99858
D 22	5.3550*-03	5.6251*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

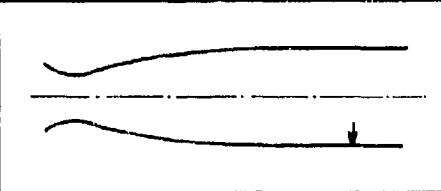
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58010501		NALEID	PROFILE TABULATION		23 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.95592	0.00000	0.00000	1.65923	0.00000
2	2.5500*-04	2.0945*+00	NM	0.97525	0.56569	0.66217	1.37018	0.48327
3	5.1000*-04	2.3330*+00	NM	0.97789	0.61210	0.70606	1.33059	0.53064
4	7.6500*-04	2.6030*+00	NM	0.98064	0.65954	0.74894	1.28946	0.58081
5	1.0200*-03	2.8344*+00	NM	0.98284	0.69708	0.78144	1.25667	0.62183
6	1.2750*-03	3.0492*+00	NM	0.98476	0.72993	0.80885	1.22794	0.65871
7	1.5300*-03	3.2680*+00	NM	0.98662	0.76173	0.83449	1.20016	0.69532
8	1.7850*-03	3.4665*+00	NM	0.98822	0.78936	0.85606	1.17612	0.72787
9	2.0400*-03	3.6648*+00	NM	0.98976	0.81595	0.87620	1.15312	0.75985
10	2.2950*-03	3.8743*+00	NM	0.99132	0.84307	0.89613	1.12984	0.79315
11	2.5500*-03	4.0711*+00	NM	0.99286	0.87018	0.91545	1.10676	0.82714
12	2.8050*-03	4.2977*+00	NM	0.99427	0.89520	0.93276	1.08567	0.85916
13	3.0600*-03	4.4880*+00	NM	0.99552	0.91762	0.94785	1.06697	0.88836
14	3.3150*-03	4.6879*+00	NM	0.99679	0.94056	0.96288	1.04803	0.91876
15	3.5700*-03	4.8224*+00	NM	0.99762	0.95568	0.97257	1.03566	0.93988
16	3.8250*-03	4.9640*+00	NM	0.99846	0.97132	0.98242	1.02298	0.96035
17	4.0800*-03	5.0644*+00	NM	0.99905	0.98227	0.98920	1.01416	0.97539
18	4.3350*-03	5.1369*+00	NM	0.99947	0.99009	0.99399	1.00789	0.98621
19	4.5900*-03	5.1758*+00	NM	0.99969	0.99426	0.99653	1.00456	0.99200
20	4.8450*-03	5.2149*+00	NM	0.99992	0.99844	0.99906	1.00124	0.99782
21	5.1000*-03	5.2198*+00	NM	0.99994	0.99896	0.99937	1.00083	0.99954
D 22	5.3550*-03	5.2296*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
23	5.6100*-03	5.2247*+00	NM	0.99997	0.99940	0.99969	1.00041	0.99927

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58010801		NALEID	PROFILE TABULATION		20 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.95712	0.00000	0.00000	1.62866	0.00000
2	2.5500*-04	1.9892*+00	NM	0.97521	0.55633	0.64959	1.36338	0.47645
3	5.1000*-04	2.2551*+00	NM	0.97828	0.61185	0.70253	1.31838	0.52288
4	7.6500*-04	2.5021*+00	NM	0.98087	0.65777	0.74430	1.28040	0.58130
5	1.0200*-03	2.7329*+00	NM	0.98312	0.69728	0.77877	1.24739	0.62432
6	1.2750*-03	2.9489*+00	NM	0.98511	0.73198	0.80793	1.21830	0.66317
7	1.5300*-03	3.1519*+00	NM	0.98688	0.76295	0.83309	1.19234	0.69871
8	1.7850*+03	3.3532*+00	NM	0.98855	0.79231	0.85621	1.16779	0.73316
9	2.0400*-03	3.5667*+00	NM	0.99025	0.82221	0.87901	1.14292	0.76908
10	2.2950*-03	3.7485*+00	NM	0.99164	0.84677	0.89719	1.12262	0.79919
11	2.5500*-03	3.9568*+00	NM	0.99316	0.87400	0.91678	1.10028	0.83322
12	2.8050*-03	4.0657*+00	NM	0.99393	0.88788	0.92654	1.08897	0.85084
13	3.0600*-03	4.3503*+00	NM	0.99507	0.92312	0.95064	1.06053	0.89639
14	3.3150*-03	4.4285*+00	NM	0.99703	0.94447	0.96479	1.04349	0.92458
15	3.5700*-03	4.4925*+00	NM	0.99807	0.96369	0.97723	1.02830	0.95034
16	3.8250*-03	4.8084*+00	NM	0.99878	0.97704	0.98572	1.01783	0.96845
17	4.0800*-03	4.9023*+00	NM	0.99935	0.98772	0.99241	1.00951	0.98306
18	4.3350*-03	4.9497*+00	NM	0.99963	0.99306	0.99572	1.00537	0.99040
19	4.5900*-03	4.9925*+00	NM	0.99989	0.99786	0.99869	1.00165	0.99704
D 20	4.8450*-03	5.0117*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

	$M : 1.75, 2.75, 3.75$ $P \text{ THETA } \gamma 10^{-3} : 2 - 12$ $TW / TR : 1.0$	5802
		ZPG - AW
Continuous tunnel with symmetrical flexible nozzle $W = H = 50.8 \text{ mm}$. $0.1 < P_0 < 0.8 \text{ MN/m}^2$. $T_0 : 300 \text{ K}$. Air. $8 < PE/m \times 10^{-6} < 40$.		
STALMACH C.J., 1958. Experimental investigation of the surface impact pressure probe method of measuring local skin friction at supersonic speeds. DRL 410. And Fenter and Stalmach (1957)		

- 1 The test boundary layer was formed on a test block constructed as an extension of the lower half of the contoured nozzle. This was attached to the flexible nozzle plate, and moved slightly in the axial direction
- 4 as the Mach number was varied. The boundary layer surveyed, therefore, had passed through a predominately
- 5 simple-wave expansion. Transition was forced by a grit-type trip. No calibration of the tunnel is reported, but the author examined the characteristics of a larger geometrically and mechanically similar tunnel running in the same Reynolds number and Mach number range, and concluded that the flow would be effectively two dimensional over a central strip wider than 50 % of the test block width, and so wider than the balance element.
- 6 Wall static pressure was measured at tapings 0.406 mm in diameter on either side of the probe tip. The test block temperature was monitored by a thermocouple which indicated that slight heat transfer occurred during the runs. Preston tube readings were taken with tube diameters of 0.305, 0.508, 0.890 and 1.65 mm. Direct wall stress measurements were made using FEB of the type used for CAT 5501 and described by Weiler and Hartwig (1952). The balance element was 25.4 mm in diameter, and the annular gap was 0.127 mm.
- 7 Pitot profiles were measured with a CPP for which $d_1 = 0.508$, $l = 10.2 \text{ mm}$, with a square cut end so that
- 8 it could also be used as a Preston tube. The profile normal coincided with the axis of the balance. The
- 9 author found agreement between measured wall static pressure and free stream static pressure calculated from Pitot measurements, and assumed, therefore, constant static pressure through the boundary layer, using
- 10 the Pitot-derived value. The profiles were reduced assuming constant total temperature. No probe corrections
- 11 were applied, and viscosity was calculated from a 0.768 power law.
- 12 The editors have presented 16 of the profiles obtained, out of a total of 42, with associated CF values from the FEB interpolated on the basis of R THETA values. The author's assumption of isoenergetic flow has been replaced by the Crocco / Van Driest temperature-velocity correlation. The boundary layer edge state is as
- 13 selected by the author. The Preston tube data is not presented as it is not available in raw form. The
- 14 profiles presented form three groups, each covering a range of Reynolds number at Mach numbers of about 1.7, 2.7 and 3.7. The CF value is an interpolated value from the balance measurements, by the editors.
- 9 DATA. 5802 0101-0306. Pitot profiles. $NX = 1$. CF values from an FEB measured separately.
- 15 Editors' comments
 The interest of this entry lies in the coverage of the post-transitional turbulent layer. Many of the profiles show exceptionally small "wake components", though as R THETA rises, the profiles may become "normal" (e.g. series 03. 0301-03 show transitional behaviour in the log-law region, while 0304/5 appear to be fully developed).

 The experiment was performed in a very small tunnel, and suffers from the small physical scale. In nearly all cases measurements do not extend within the momentum-deficit peak, so that integral values should be treated with caution.

 The Mach number and Reynolds number range closely matches the flat plate tests of Coles - CAT 5301.

Other comparisons are with Shutts et al. - CAT 5501 who used the same type of balance in a flat plate,
and Moore - CAT 5805 whose flat wall tests provide a repeat experiment in the same facility.

CAT 5802		STALMACH		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	MO *	TW/YR*	RED2W	CF *	H12	H12K	PW	PD		
X	POD*	PH/PD*	RED2D	CG	H32	H32K	TW	TD		
RZ	TOD*	SN *	D2	PI2*	H42	D2K	UD	TR		
58020101	1.7390	1.0000	2.5818 ⁺⁰³	2.5400 ⁻⁰³	2.7507	1.4975	1.9681 ⁺⁰⁴	1.9681 ⁺⁰⁴		
NM	1.0305 ⁺⁰⁵	1.0000	3.6804 ⁺⁰³	NM	1.8060	1.7972	2.8576 ⁺⁰²	1.8533 ⁺⁰²		
INFINITE	2.9742 ⁺⁰²	0.0000	2.6230 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0708	3.1038 ⁻⁰⁴	4.7466 ⁺⁰²	2.8576 ⁺⁰²		
58020102	1.7440	1.0000	5.9748 ⁺⁰³	2.1300 ⁻⁰³	2.7044	1.4496	3.4231 ⁺⁰⁴	3.4231 ⁺⁰⁴		
NM	1.8060 ⁺⁰⁵	1.0000	8.5308 ⁺⁰³	NM	1.8026	1.7943	2.8626 ⁺⁰²	1.8527 ⁺⁰²		
INFINITE	2.9798 ⁺⁰²	0.0000	3.4841 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0709	4.1386 ⁻⁰⁴	4.7595 ⁺⁰²	2.8626 ⁺⁰²		
58020103	1.7390	1.0000	8.8590 ⁺⁰³	1.9900 ⁻⁰³	2.6735	1.4343	5.5181 ⁺⁰⁴	5.5181 ⁺⁰⁴		
NM	2.8893 ⁺⁰⁵	1.0000	1.2610 ⁺⁰⁴	NM	1.8133	1.8068	2.9110 ⁺⁰²	1.8879 ⁺⁰²		
INFINITE	2.0298 ⁺⁰²	0.0000	3.2869 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0711	3.8746 ⁻⁰⁴	4.7907 ⁺⁰²	2.9110 ⁺⁰²		
58020201	2.7350	1.0000	9.5940 ⁺⁰²	2.5550 ⁻⁰³	4.5594	1.4984	4.2411 ⁺⁰³	4.2411 ⁺⁰³		
NM	1.0420 ⁺⁰⁵	1.0000	1.9966 ⁺⁰³	NM	1.8235	1.8011	2.7752 ⁺⁰²	1.1857 ⁺⁰²		
INFINITE	2.9597 ⁺⁰²	0.0000	2.2483 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1137	3.1736 ⁻⁰⁴	5.9712 ⁺⁰²	2.7752 ⁺⁰²		
58020202	2.7290	1.0000	1.5036 ⁺⁰³	2.2350 ⁻⁰³	4.5174	1.4623	5.3473 ⁺⁰³	5.3473 ⁺⁰³		
NM	1.3017 ⁺⁰⁵	1.0000	3.1238 ⁺⁰³	NM	1.8134	1.7943	2.7631 ⁺⁰²	1.1836 ⁺⁰²		
INFINITE	2.9464 ⁺⁰²	0.0000	2.7888 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1128	3.9996 ⁻⁰⁴	5.9526 ⁺⁰²	2.7631 ⁺⁰²		
58020203	2.7310	1.0000	1.8327 ⁺⁰³	2.1150 ⁻⁰³	4.4729	1.4389	6.2226 ⁺⁰³	6.2226 ⁺⁰³		
NM	1.5195 ⁺⁰⁵	1.0000	3.8077 ⁺⁰³	NM	1.8226	1.8042	2.7760 ⁺⁰²	1.1881 ⁺⁰²		
INFINITE	2.9603 ⁺⁰²	0.0000	2.9351 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1135	4.1551 ⁻⁰⁴	5.9684 ⁺⁰²	2.7760 ⁺⁰²		
58020204	2.7280	1.0000	2.9665 ⁺⁰³	1.8400 ⁻⁰³	4.4519	1.4215	9.0308 ⁺⁰³	9.0308 ⁺⁰³		
NM	2.1951 ⁺⁰⁵	1.0000	6.1542 ⁺⁰³	NM	1.8179	1.8012	2.7821 ⁺⁰²	1.1922 ⁺⁰²		
INFINITE	2.9666 ⁺⁰²	0.0000	3.2085 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1131	4.6906 ⁻⁰⁴	5.9721 ⁺⁰²	2.7821 ⁺⁰²		
58020205	2.7240	1.0000	3.1394 ⁺⁰³	1.8150 ⁻⁰³	4.4825	1.4462	1.0694 ⁺⁰⁴	1.0694 ⁺⁰⁴		
NM	2.5835 ⁺⁰⁵	1.0000	6.4832 ⁺⁰³	NM	1.8136	1.7944	2.8380 ⁺⁰²	1.2182 ⁺⁰²		
INFINITE	3.0261 ⁺⁰²	0.0000	3.0218 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1127	4.3275 ⁻⁰⁴	6.0280 ⁺⁰²	2.8380 ⁺⁰²		
58020206	2.7550	1.0000	4.4169 ⁺⁰³	1.6400 ⁻⁰³	4.5562	1.4477	1.4399 ⁺⁰⁴	1.4399 ⁺⁰⁴		
NM	3.6478 ⁺⁰⁵	1.0000	9.2577 ⁺⁰³	NM	1.8128	1.7938	2.7877 ⁺⁰²	1.1812 ⁺⁰²		
INFINITE	2.9742 ⁺⁰²	0.0000	3.0315 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1137	4.3778 ⁻⁰⁴	6.0033 ⁺⁰²	2.7877 ⁺⁰²		
58020207	2.7390	1.0000	5.8533 ⁺⁰³	1.5150 ⁻⁰³	4.5506	1.4642	2.1221 ⁺⁰⁴	2.1221 ⁺⁰⁴		
NM	5.2459 ⁺⁰⁵	1.0000	1.2154 ⁺⁰⁴	NM	1.8092	1.7906	2.8446 ⁺⁰²	1.2134 ⁺⁰²		
INFINITE	3.0339 ⁺⁰²	0.0000	2.8231 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1129	4.0845 ⁻⁰⁴	6.0492 ⁺⁰²	2.8446 ⁺⁰²		
58020301	3.6840	1.0000	7.0193 ⁺⁰²	2.0000 ⁻⁰³	6.8681	1.4197	1.7188 ⁺⁰³	1.7188 ⁺⁰³		
NM	1.6976 ⁺⁰⁵	1.0000	2.1153 ⁺⁰³	NM	1.8409	1.8139	2.7533 ⁺⁰²	8.0223 ⁺⁰¹		
INFINITE	2.9798 ⁺⁰²	0.0000	2.4632 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1399	4.1482 ⁻⁰⁴	6.6157 ⁺⁰²	2.7533 ⁺⁰²		
58020302	3.6720	1.0000	7.1329 ⁺⁰²	1.9900 ⁻⁰³	6.7973	1.4038	1.7387 ⁺⁰³	1.7387 ⁺⁰³		
NM	1.6888 ⁺⁰⁵	1.0000	2.1385 ⁺⁰³	NM	1.8452	1.8217	2.7614 ⁺⁰²	6.0831 ⁺⁰¹		
INFINITE	2.9881 ⁺⁰²	0.0000	2.4977 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1400	4.1614 ⁻⁰⁴	6.6192 ⁺⁰²	2.7614 ⁺⁰²		
58020303	3.6630	1.0000	1.7028 ⁺⁰³	1.4850 ⁻⁰³	6.7481	1.3948	4.3819 ⁺⁰³	4.3819 ⁺⁰³		
NM	4.2032 ⁺⁰⁵	1.0000	5.0735 ⁺⁰³	NM	1.8494	1.8295	2.8002 ⁺⁰²	8.2252 ⁺⁰¹		
INFINITE	3.0298 ⁺⁰²	0.0000	2.4188 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1401	3.9909 ⁻⁰⁴	6.6607 ⁺⁰²	2.8002 ⁺⁰²		
58020304	3.6670	1.0000	2.7139 ⁺⁰³	1.3060 ⁻⁰³	7.0169	1.4658	5.4238 ⁺⁰³	5.4238 ⁺⁰³		
NM	5.2316 ⁺⁰⁵	1.0000	8.1349 ⁺⁰³	NM	1.8010	1.7698	2.7385 ⁺⁰²	8.0315 ⁺⁰¹		
INFINITE	2.9631 ⁺⁰²	0.0000	3.0210 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1365	5.5175 ⁻⁰⁴	6.5890 ⁺⁰²	2.7385 ⁺⁰²		
58020305	3.6610	1.0000	3.4799 ⁺⁰³	1.2400 ⁻⁰³	6.8819	1.4016	7.7655 ⁺⁰³	7.7655 ⁺⁰³		
NM	7.6377 ⁺⁰⁵	1.0000	1.0444 ⁺⁰⁴	NM	1.8270	1.8075	2.7945 ⁺⁰²	8.1516 ⁺⁰¹		
INFINITE	3.0242 ⁺⁰²	0.0000	2.7588 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1388	4.8180 ⁻⁰⁴	6.6634 ⁺⁰²	2.7945 ⁺⁰²		
58020306	3.6610	1.0000	3.4727 ⁺⁰³	1.2200 ⁻⁰³	6.9605	1.4281	7.6736 ⁺⁰³	7.6736 ⁺⁰³		
NM	7.5472 ⁺⁰⁵	1.0000	1.0484 ⁺⁰⁴	NM	1.8149	1.7908	2.7919 ⁺⁰²	8.1442 ⁺⁰¹		
INFINITE	3.0214 ⁺⁰²	0.0000	2.7988 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1379	5.0045 ⁻⁰⁴	6.6604 ⁺⁰²	2.7919 ⁺⁰²		

58020201		STALMACH		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.93767	0.00000	0.00000	2.34046	0.00000
2	2.5400*-04	3.0562*+00	NM	0.96662	0.51261	0.67440	1.73006	0.38964
3	3.0480*-04	3.6371*+00	NM	0.97066	0.56965	0.72751	1.63100	0.44605
4	3.5560*-04	3.8784*+00	NM	0.97242	0.59159	0.74669	1.59409	0.46671
5	4.0640*-04	4.1123*+00	NM	0.97405	0.61207	0.76399	1.55805	0.49035
6	5.3340*-04	4.5490*+00	NM	0.97686	0.64790	0.79290	1.49771	0.52941
7	6.6040*-04	4.8178*+00	NM	0.97854	0.66984	0.80977	1.46147	0.55408
8	7.8740*-04	5.0500*+00	NM	0.97990	0.68775	0.82310	1.43231	0.57466
9	1.0414*-03	5.6302*+00	NM	0.98305	0.73053	0.85332	1.36441	0.62541
10	1.2954*-03	6.1224*+00	NM	0.98550	0.76490	0.87604	1.31172	0.66786
11	1.5494*-03	6.6827*+00	NM	0.98807	0.80219	0.89923	1.25655	0.71563
12	1.8034*-03	7.2465*+00	NM	0.99044	0.83803	0.92014	1.20556	0.76324
13	2.0574*-03	7.8184*+00	NM	0.99288	0.87642	0.94114	1.15315	0.81614
14	2.3114*-03	8.3982*+00	NM	0.99473	0.90476	0.95678	1.11336	0.85936
15	2.5654*-03	8.7851*+00	NM	0.99602	0.92870	0.96759	1.08549	0.89138
16	2.8194*-03	9.0681*+00	NM	0.99693	0.94442	0.97508	1.06597	0.91473
17	3.0734*-03	9.4235*+00	NM	0.99803	0.96380	0.98404	1.04244	0.94398
18	3.3274*-03	9.5322*+00	NM	0.99835	0.96963	0.98669	1.03545	0.95291
19	3.8354*-03	9.8971*+00	NM	0.99941	0.98903	0.99527	1.01265	0.98283
20	4.3434*-03	9.9947*+00	NM	0.99969	0.99415	0.99747	1.00673	0.99082
21	4.8514*-03	1.0072*+01	NM	0.99990	0.99817	0.99922	1.00210	0.99713
22	5.3594*-03	1.0093*+01	NM	0.99996	0.99927	0.99969	1.00084	0.99885
D 23	5.8674*-03	1.0107*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD

58020203		STALMACH		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.93774	0.00000	0.00000	2.33654	0.00000
2	2.5400*-04	2.7104*+00	NM	0.96301	0.47565	0.63710	1.79405	0.35512
3	3.0480*-04	3.0653*+00	NM	0.96615	0.51410	0.67553	1.72662	0.39124
4	3.5560*-04	3.2680*+00	NM	0.96785	0.53497	0.69547	1.69007	0.41151
5	4.0640*-04	3.3214*+00	NM	0.96830	0.54046	0.70062	1.68048	0.41692
6	5.3340*-04	3.6332*+00	NM	0.97070	0.57012	0.72764	1.62890	0.44670
7	6.6040*-04	3.8989*+00	NM	0.97264	0.59429	0.74873	1.58728	0.47170
8	7.8740*-04	4.3371*+00	NM	0.97562	0.63200	0.78003	1.52332	0.51206
9	1.0414*-03	4.7898*+00	NM	0.97845	0.66862	0.80862	1.46262	0.55286
10	1.2954*-03	5.1321*+00	NM	0.98044	0.69498	0.82814	1.41991	0.58324
11	1.5494*-03	5.6507*+00	NM	0.98324	0.73306	0.85485	1.35985	0.62863
12	1.8034*-03	6.1063*+00	NM	0.98550	0.76492	0.87589	1.31118	0.66801
13	2.0574*-03	6.5930*+00	NM	0.98775	0.79751	0.89625	1.26295	0.70965
14	2.3114*-03	6.9672*+00	NM	0.98937	0.82168	0.91063	1.22823	0.74142
15	2.5654*-03	7.5198*+00	NM	0.99160	0.85610	0.93007	1.18034	0.78799
16	2.8194*-03	8.0145*+00	NM	0.99345	0.88576	0.94596	1.14055	0.82939
17	3.0734*-03	8.3537*+00	NM	0.99465	0.90553	0.95609	1.11479	0.85764
18	3.3274*-03	8.7460*+00	NM	0.99597	0.92787	0.96713	1.08642	0.89020
19	3.5814*-03	9.0416*+00	NM	0.99693	0.94434	0.97500	1.06599	0.91465
20	4.0894*-03	9.5869*+00	NM	0.99859	0.97400	0.98862	1.03024	0.95960
21	4.5974*-03	9.9041*+00	NM	0.99951	0.99085	0.99605	1.01053	0.98567
22	5.1054*-03	1.0009*+01	NM	0.99980	0.99634	0.99843	1.00420	0.99425
23	5.6134*-03	1.0037*+01	NM	0.99988	0.99780	0.99906	1.00252	0.99655
D 24	6.1214*-03	1.0079*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58020207		STALMACH		PROFILE TABULATION		21 POINTS, DELTA AT POINT 21		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.93759	0.00000	0.00000	2.34436	0.00000
2	2.5400*-04	2.7073*+00	NM	0.96283	0.47391	0.63594	1.80068	0.35317
3	3.0480*-04	3.0141*+00	NM	0.96556	0.50746	0.66967	1.74148	0.38494
4	3.5560*-04	3.2101*+00	NM	0.96723	0.52761	0.68912	1.70595	0.40395
5	4.0640*-04	3.4024*+00	NM	0.96878	0.54657	0.70690	1.67258	0.42264
6	5.3340*-04	3.7480*+00	NM	0.97140	0.57900	0.73604	1.61605	0.45546
7	6.6040*-04	4.0029*+00	NM	0.97322	0.60170	0.75558	1.57688	0.47916
8	7.8740*-04	4.2196*+00	NM	0.97470	0.62031	0.77106	1.54511	0.49903
9	9.1440*-04	4.4384*+00	NM	0.97612	0.63851	0.78575	1.51436	0.51886
10	1.1684*-03	4.9165*+00	NM	0.97905	0.67653	0.81503	1.45135	0.56156
11	1.4224*-03	5.3785*+00	NM	0.98165	0.71126	0.84018	1.39537	0.60212
12	1.6764*-03	5.8574*+00	NM	0.98413	0.74550	0.86357	1.34181	0.64358
13	1.9304*-03	6.3434*+00	NM	0.98647	0.77869	0.88495	1.29155	0.68519
14	2.1844*-03	6.9486*+00	NM	0.98871	0.81172	0.90505	1.24318	0.72801
15	2.4384*-03	7.3394*+00	NM	0.99074	0.84254	0.92280	1.19957	0.76927
16	2.6924*-03	7.8364*+00	NM	0.99265	0.87264	0.93923	1.15844	0.81077
17	2.9464*-03	8.3269*+00	NM	0.99440	0.90134	0.95412	1.12053	0.85149
18	3.4544*-03	9.3272*+00	NM	0.99766	0.95719	0.98105	1.05047	0.93391
19	3.9624*-03	9.8010*+00	NM	0.99906	0.98253	0.99243	1.02027	0.97272
20	4.4704*-03	1.0087*+01	NM	0.99987	0.99751	0.99893	1.00287	0.99606
D 21	4.9784*-03	1.0135*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

58020301		STALMACH		PROFILE TABULATION		13 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PO	T0/T00	M/M0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	NM	0.92400	0.00000	0.00000	3.4320E	0.00000	
2	2.5400-04	3.7646+00	NM	0.95744	0.43160	0.66331	2.36200	0.28083	
3	2.9718-04	4.1679+00	NM	0.96072	0.45793	0.69038	2.27296	0.30374	
4	3.4798-04	4.4433+00	NM	0.96200	0.47503	0.71673	2.21596	0.31911	
5	3.9878-04	4.8084+00	NM	0.96422	0.49674	0.72750	2.14488	0.33918	
6	4.4958-04	5.1515+00	NM	0.96618	0.51627	0.74500	2.08222	0.35779	
7	5.7658-04	5.6558+00	NM	0.96886	0.54370	0.76826	1.99661	0.38478	
8	7.0358-04	6.0264+00	NM	0.97068	0.56298	0.78375	1.93812	0.40439	
9	8.3058-04	6.4046+00	NM	0.97244	0.58198	0.79837	1.88189	0.42424	
10	1.0846-03	7.1120+00	NM	0.97547	0.61591	0.82291	1.78514	0.46098	
11	1.3386-03	7.8477+00	NM	0.97829	0.64929	0.84523	1.69458	0.49878	
12	1.9736-03	9.9947+00	NM	0.98512	0.73806	0.89675	1.4762E	0.60744	
13	2.6086-03	1.1884+01	NM	0.98981	0.80809	0.93055	1.32607	0.70174	
14	3.2436-03	1.3904+01	NM	0.99387	0.87676	0.95885	1.14602	0.80170	
15	3.8786-03	1.5547+01	NM	0.99664	0.92888	0.97761	1.10768	0.88258	
16	4.5136-03	1.6897+01	NM	0.99862	0.96960	0.99085	1.04431	0.94880	
17	5.1486-03	1.7594+01	NM	0.99955	0.98996	0.99704	1.01437	0.98292	
D 18	5.7836-03	1.7943+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

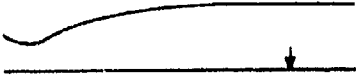
INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

58020304		STALMACH		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PO	T0/T00	M/M0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	NM	0.92417	0.00000	0.00000	3.4096E	0.00000	
2	2.5400-04	2.8977+00	NM	0.95077	0.36976	0.59216	2.56471	0.23089	
3	3.0480-04	3.4096+00	NM	0.95498	0.40877	0.63735	2.43083	0.26220	
4	3.5560-04	3.5821+00	NM	0.95630	0.42109	0.65080	2.38910	0.27240	
5	4.0640-04	3.7484+00	NM	0.95752	0.43250	0.66305	2.35030	0.28211	
6	5.3340-04	4.1213+00	NM	0.96011	0.44708	0.68035	2.26793	0.30351	
7	6.6040-04	4.4076+00	NM	0.96197	0.47504	0.70598	2.20867	0.31964	
8	7.8740-04	4.7070+00	NM	0.96382	0.49313	0.72306	2.14988	0.33632	
9	1.0414-03	5.3149+00	NM	0.96727	0.52777	0.75385	2.04027	0.36949	
10	1.2954-03	5.8896+00	NM	0.97022	0.55852	0.77923	1.94652	0.40032	
11	1.5474-03	6.4774+00	NM	0.97297	0.58827	0.80213	1.85925	0.43143	
12	1.8034-03	7.2542+00	NM	0.97624	0.62539	0.82858	1.75534	0.47203	
13	2.0574-03	7.8286+00	NM	0.97843	0.65146	0.84583	1.68574	0.50175	
14	2.3114-03	8.6812+00	NM	0.98137	0.68831	0.86450	1.59209	0.54551	
15	2.5654-03	9.3437+00	NM	0.98344	0.71562	0.88409	1.52624	0.57926	
16	2.8174-03	1.0019+01	NM	0.98537	0.74243	0.89846	1.46450	0.61349	
17	3.0734-03	1.0786+01	NM	0.98741	0.77174	0.91320	1.40018	0.65220	
18	3.3274-03	1.1810+01	NM	0.98985	0.80920	0.93064	1.32268	0.70360	
19	3.5854-03	1.3591+01	NM	0.99350	0.87049	0.95618	1.20657	0.79248	
20	4.3434-03	1.5376+01	NM	0.99657	0.92786	0.97712	1.10900	0.88108	
21	4.8514-03	1.6865+01	NM	0.99878	0.97314	0.99189	1.03892	0.95474	
22	5.3574-03	1.7643+01	NM	0.99982	0.99596	0.99881	1.00573	0.99312	
D 23	5.8674-03	1.7782+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

58020306		STALMACH		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PO	T0/T00	M/M0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	NM	0.92403	0.00000	0.00000	3.42812	0.00000	
2	2.5400-04	3.1092+00	NM	0.95241	0.38495	0.61122	2.52101	0.24245	
3	2.9718-04	3.3569+00	NM	0.95481	0.40342	0.63237	2.45712	0.25736	
4	3.4798-04	3.6414+00	NM	0.95658	0.42355	0.65451	2.38796	0.27409	
5	3.9878-04	3.9771+00	NM	0.95897	0.44604	0.67814	2.31148	0.29338	
6	4.4958-04	4.2233+00	NM	0.96062	0.46180	0.69402	2.25899	0.30728	
7	5.0038-04	4.2447+00	NM	0.96076	0.46314	0.69534	2.25412	0.30848	
8	6.2738-04	4.6349+00	NM	0.96334	0.48313	0.71934	2.17168	0.33124	
9	7.5438-04	4.8600+00	NM	0.96456	0.50014	0.73040	2.13274	0.34247	
10	8.8138-04	5.1517+00	NM	0.96622	0.51672	0.74518	2.07978	0.35830	
11	1.1354-03	5.7691+00	NM	0.96946	0.55012	0.77331	1.97606	0.39134	
12	1.3894-03	6.5154+00	NM	0.97297	0.58790	0.80263	1.86389	0.43062	
13	1.6434-03	7.1483+00	NM	0.97565	0.61810	0.82423	1.77838	0.46350	
14	2.2784-03	9.0762+00	NM	0.98246	0.70204	0.87701	1.56055	0.56199	
15	2.9134-03	1.1222+01	NM	0.98831	0.78490	0.91988	1.37350	0.66973	
16	3.5484-03	1.3540+01	NM	0.99324	0.86550	0.95446	1.21613	0.78483	
17	4.8184-03	1.7409+01	NM	0.99934	0.98540	0.99567	1.02097	0.97523	
D 18	6.0884-03	1.7915+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

	M : 1.7, 3.6 and 4.8 R THETA X 10 ⁻³ : 26 - 35 TW / TR : 1	5803
		ZPG - AW
Continuous tunnel with asymmetric flexible nozzle. W = H = 0.15 m. 0.2 < PO < 0.64 MN/m ² . TO : 300 K. Air, dewpoint 245 K. 20 < RE/m X 10 ⁻⁶ < 30.		
KISTLER A.L., 1958. Fluctuation measurements in supersonic turbulent boundary layers. BRL Rep 1052. And Kistler A.L. Private communication. Also Kistler (1959), Kistler and Chen (1963).		

- 1 The measurements were made at a single station on the flat wall opposite the flexible nozzle plate. The test surface was allowed to settle to an equilibrium temperature which was within a few degrees of the adiabatic recovery temperature. The surface was polished to a mirror finish. The free stream Mach number
- 2 was constant within ± 0.02 after the termination of the nozzle expansion, at least 0.5 m upstream of the
- 3 test station. Boundary layer profile and hot-wire surveys made to check transition showed that this took
- 5 place near the tunnel throat. Three dimensional effects were small in the central region of the tunnel. Mean velocity profiles taken at 25.4 mm intervals in the Z-direction were identical within experimental accuracy, and oil and lampblack on the floor did not disclose any secondary flow.

- 6 Static pressure holes (d = 1.02 mm) were distributed at 25.4 mm intervals along the centre-line of the
- 7 floor. The wall temperature was monitored by a thermocouple at the measuring station, but buried some
- distance from the surface. The total temperature profile was obtained with an FWP consisting of a 0.5 mm Pt
- wire used as a resistance thermometer. TO was found from the recovery temperature using the data of Laufer
- and McClellan (1956). The FWP used ($h_2 = 0.127$, $b = 1.27$ mm) was formed by flattening a hypodermic needle.
- The hot-wire probe was operated in the constant current mode. The equipment used was basically that
- described by Kovaszny (1953) with modifications to increase the frequency response and improve matching
- with the 1.27 μ m Pt-Rh wires employed. The length / diameter ratio was about 200. The compensated frequency
- response of the wires was flat to approximately 90 KHz.

- 9 The author has interpolated the TO data to the y-stations of the Pitot measurements. The hot-wires were
- operated in ten states, of which seven are in principle redundant, so as to allow separation of the
- fluctuation modes by fitting the data to a response characteristic based on the hypothesis of small
- pressure fluctuation levels. The question is discussed in Kistler and Chen (1963). The friction velocity
- used for scaling the fluctuation results was obtained from a correlation of published data and checked
- by comparing the resulting transformed velocity profile with the profiles obtained by Coles (1963). The
- static pressure was assumed constant through the boundary layer. The editors present the data incorporating
- 12 all the author's assumptions and data-reduction procedures.

- 13 Three mean-flow profiles are presented, each for a different Mach number but at approximately the same
- 14 value of R THETA. The associated fluctuation data is given in section D. The CF value is the author's
- estimate, determined according to Coles (1953).

- 5 DATA 5803 0101-0301. Pitot, TO and fluctuation profiles taken separately. NX = 1.

- 15 Editors' comments
These are the first available systematic hot-wire measurements at supersonic speeds. Even now there are few comparisons, and the interpretation of the measurements remains controversial. Substantial contributions, in each case at a single Mach number, have been made by Horstman & Owen - CAT 7205 and Laderman & Demetriades - CAT 7403. Supporting tabular data are also given in association with Sturek & Danberg - CAT 7101 and Waitrup & Schetz - CAT 7104.

58030101		KISTLER		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RH00*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.00000	0.00000	0.00000	1.53880	0.00000	
2	1.2677*-03	2.1328*+00	NM	0.99700	0.63953	0.72290	1.27770	0.56578	
3	2.5248*-03	2.3872*+00	NM	0.99800	0.69360	0.77120	1.23652	0.62375	
4	3.8049*-03	2.6124*+00	NM	0.99700	0.73721	0.80783	1.20078	0.67276	
5	5.0673*-03	2.7981*+00	NM	0.99950	0.77493	0.83633	1.17699	0.71061	
6	6.3247*-03	2.9764*+00	NM	1.00100	0.80174	0.86137	1.15427	0.74625	
7	7.6098*-03	3.1483*+00	NM	1.00100	0.83023	0.88322	1.13172	0.78042	
8	8.8900*-03	3.4626*+00	NM	1.00100	0.87965	0.91961	1.09790	0.84143	
9	1.0152*-02	3.8279*+00	NM	1.00200	0.88953	0.92712	1.08629	0.85348	
10	1.1397*-02	3.6925*+00	NM	1.00300	0.91395	0.94470	1.06841	0.88421	
11	1.2677*-02	3.8620*+00	NM	1.00200	0.93837	0.96089	1.04856	0.91638	
12	1.3957*-02	4.0110*+00	NM	1.00100	0.95930	0.97433	1.03158	0.94451	
13	1.5271*-02	4.1465*+00	NM	1.00100	0.97791	0.98644	1.01753	0.96945	
14	1.6535*-02	4.2107*+00	NM	1.00100	0.98663	0.99203	1.01098	0.98125	
15	1.7730*-02	4.3021*+00	NM	1.00050	0.99884	0.99952	1.00137	0.99816	
D 16	1.8936*-02	4.3108*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M,T0/T00 ASSUME P=PD

58030201		KISTLER		PROFILE TABULATION		17 POINTS, DELTA AT POINT 17			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RH00*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.00000	0.00000	0.00000	3.37086	0.00000	
2	1.0135*-03	2.7459*+00	NM	0.97500	0.36798	0.58942	2.56574	0.22973	
3	3.5971*-03	4.2672*+00	NM	0.98500	0.48034	0.71195	2.19691	0.32407	
4	6.0808*-03	5.2886*+00	NM	0.99100	0.54213	0.76812	2.00742	0.39264	
5	8.6144*-03	6.3827*+00	NM	0.99400	0.60112	0.81404	1.83385	0.44390	
6	1.1148*-02	7.5920*+00	NM	1.00000	0.66011	0.85550	1.67960	0.50935	
7	1.3628*-02	8.9161*+00	NM	1.00300	0.71910	0.89073	1.53429	0.58054	
8	1.6269*-02	1.0355*+01	NM	1.00300	0.77809	0.92025	1.38878	0.65789	
9	1.8749*-02	1.1228*+01	NM	1.00400	0.81180	0.93554	1.32895	0.70420	
10	2.1336*-02	1.3492*+01	NM	1.00300	0.89326	0.96744	1.17299	0.82477	
11	2.3738*-02	1.4662*+01	NM	1.00250	0.93258	0.98068	1.10581	0.88684	
12	2.6403*-02	1.5530*+01	NM	1.00200	0.96067	0.98938	1.06064	0.93281	
13	2.8804*-02	1.5973*+01	NM	1.00000	0.97472	0.99265	1.03713	0.95711	
14	3.1471*-02	1.6332*+01	NM	1.00000	0.98596	0.99597	1.02041	0.97604	
15	3.3871*-02	1.6513*+01	NM	1.00000	0.99157	0.99759	1.01218	0.98559	
16	3.6271*-02	1.6577*+01	NM	1.00000	0.99354	0.99816	1.00932	0.98894	
D 17	3.8936*-02	1.6787*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M,T0/T00 ASSUME P=PD

58030301		KISTLER		PROFILE TABULATION		21 POINTS, DELTA AT POINT 21			
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RH00*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.00000	0.00000	0.00000	5.12944	0.00000	
2	1.6065*-03	3.4971*+00	NM	0.98500	0.32591	0.61284	3.53593	0.17332	
3	2.6143*-03	4.1038*+00	NM	0.97000	0.35803	0.65391	3.33582	0.19603	
4	3.9433*-03	4.8552*+00	NM	0.97300	0.39400	0.69491	3.11070	0.22339	
5	5.2578*-03	5.4881*+00	NM	0.97800	0.42184	0.72482	2.95230	0.24551	
6	6.2801*-03	6.0583*+00	NM	0.98000	0.44540	0.74755	2.81703	0.26537	
7	7.5946*-03	6.8298*+00	NM	0.98500	0.47537	0.77527	2.65972	0.29149	
8	8.6169*-03	7.4242*+00	NM	0.98600	0.49722	0.79301	2.54372	0.31175	
9	1.0282*-02	8.6486*+00	NM	0.99100	0.53940	0.82543	2.34172	0.35249	
10	1.1976*-02	1.0002*+01	NM	0.99400	0.58244	0.85309	2.14931	0.39728	
11	1.3583*-02	1.1452*+01	NM	0.99900	0.62527	0.87983	1.97999	0.44436	
12	1.6942*-02	1.4920*+01	NM	1.00300	0.71734	0.92355	1.65753	0.55718	
13	1.8694*-02	1.6851*+01	NM	1.00300	0.76381	0.94081	1.51716	0.62011	
14	2.0389*-02	1.8894*+01	NM	1.00500	0.81006	0.95684	1.39521	0.68580	
15	2.3719*-02	2.2269*+01	NM	1.00500	0.88116	0.97662	1.22841	0.79503	
16	2.7165*-02	2.4774*+01	NM	1.00500	0.93041	0.98830	1.12831	0.87591	
17	2.8626*-02	2.5620*+01	NM	1.00000	0.94647	0.98933	1.09262	0.90546	
18	3.2715*-02	2.6852*+01	NM	1.00000	0.96938	0.99407	1.05159	0.94530	
19	3.5636*-02	2.7592*+01	NM	1.00000	0.98287	0.99674	1.02842	0.96919	
20	3.9141*-02	2.8186*+01	NM	1.00000	0.99358	0.99879	1.01053	0.98839	
D 21	4.2647*-02	2.8545*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

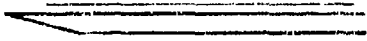
INPUT VARIABLES Y/DELTA,M,T0/T00 ASSUME P=PD

TABLES OF REDUCED TIME-MEAN FLUCTUATION QUANTITIES

Velocity Fluctuation Levels		Static Temperature Fluctuation Levels		Temperature-Velocity Correlation Coefficients	
y/δ	$\frac{\sqrt{\Delta u^2}}{u_\tau}$	y/δ	$\frac{\sqrt{\Delta T^2}}{2T} \frac{T_0 + T_\infty}{T_0 - T_\infty}$	y/δ	$\frac{\Delta T \Delta U}{\sqrt{\Delta T^2} \sqrt{\Delta U^2}}$
58030101	$M_\delta = 1.72$	$u_\tau = 16.66$ m/s		$\delta = 17.78$ mm	
0.153	1.33	.122	0.042	0.161	- 0.566
0.159	1.44	.170	0.054	0.161	- 0.66
0.290	1.31	.255	0.053	0.270	- 0.71
0.353	1.27	.285	0.061	0.306	- 0.70
0.418	1.22	.346	0.065	0.45	- 0.76
0.619	0.92	.418	0.067	0.516	- 0.78
1.016	0.14	.479	0.067	0.75	- 0.76
1.016	0.19	.618	0.066	0.94	- 0.67
		.891	0.040	1.08	- 0.62
		1.018	0.016		
58030201	$M_\delta = 3.56$	$u_\tau = 26.76$ m/s		$\delta = 26.67$ mm	
0.135	1.06	0.139	0.051	.139	- 0.71
.135	1.11	.139	0.056	.139	- 0.74
.182	1.07	.28	0.064	.27	- 0.69
.540	0.91	.28	0.066	.41	- 0.70
.681	0.59	.406	0.078	.59	- 0.67
.816	0.32	.545	0.079	.68	- 0.66
.816	0.35	.685	0.072	.82	- 0.51
.960	0.13	.75	0.058	.95	- 0.47
1.096	0.07	.83	0.042		
		.96	0.020		
		1.09	0.008		
58030301	$M_\delta = 4.67$	$u_\tau = 32.07$ m/s		$\delta = 29.21$ mm	
0.071	0.99	0.066	0.047	0.067	- 0.58
0.130	0.99	.138	0.047	0.134	- 0.52
0.416	0.88	.186	0.058	0.306	- 0.54
.536	0.67	.308	0.064	0.428	- 0.68
.652	0.40	.412	0.084	0.58	- 0.69
.660	0.50	0.577	0.084	0.65	- 0.58
.825	0.22	0.657	0.080	0.83	- 0.52
.092	0.08	.836	0.049	1.00	- 0.47
		1.00	0.018	1.08	- 0.47

The reference velocity and length (u_τ and δ) have the values given by the author in accord with his definitions.

ΔU etc. are more usually written u' etc.

rough 	M : 2.2 and 2.7 R THETA X 10 ⁻³ : 8 - 50 TW / TR : 1	5804 ZPG (ROUGH) AW
Continuous wind tunnel with fixed symmetrical interchangeable nozzles. W = 0.48, H = 0.7, L = 1.0 m. 0.18 < PO < 0.3 MN/m ² . TO: 340 K. Air. RE/m X 10 ⁻⁶ : 25.		
FENTER F.W. and LYONS W.C., 1958. An experimental investigation of the effects of several types of surface roughness on turbulent boundary layer characteristics at supersonic speeds. DRL 411.		

- The experimental arrangements were as for CAT 5501 and 5502 except that no balance measurements were made, and that the surface of the plate was further modified. In the initial tests (series 01) the entire plate surface was coated with spherical beads of 0.105 mm diameter, and seven successive profiles were measured on the centre-line from X = 194 mm to X = 804 mm, in increments of 103 mm (see section B). For the remaining tests, the basic plate was modified to carry 16 different insert plates.
- 1 The roughness of the various inserts is described in Table 1 and the associated figure, with reference to the normal zero plane of the insert, which was carefully adjusted to the plane of the basic plate. The insert extended from X = 230 mm to X = 340 mm, and was 301 mm wide, as compared to the overall plate width of 483 mm. When modified to carry the inserts, the plate had a knurled transition trip extending transversely across the whole width from X = 19 to 25 mm. This was formed by a standard 1/4 inch knurling tool. The peaks of the knurled region were about 0.13 mm high. Otherwise the surface of the basic plate was flat, as was the first 72.2 mm of the insert. The first insert was completely flat, so that the model became a conventional smooth flat plate.
 - 2 Profiles could be measured on the normal at X = 296 mm, just upstream of the start of the roughness on the insert at X = 302 mm, and also on the normal at X = 804 mm, just before the end of the roughness at X = 840 mm.
 - 3 The static pressure through the boundary layer was assumed to be constant.
 - 4 The editors have presented all the profiles for which tabulated data is available except one pair for insert 1 at a slightly lower unit Reynolds number. The author's assumption of isoenergetic flow has been replaced by the Crocco / Van Driest temperature velocity correlation. The profiles consist of the consecutive set of seven (series 01) on a close-packed spherically rough surface, and upstream and downstream profiles for the varied roughnesses listed in table 1. These have been grouped as "series" 02, the upstream profiles, and "series" 03, the downstream profiles. The profile identification number in each case is the number of the relevant insert. All the profiles presented were obtained at the same unit Reynolds number, so that in principle the profiles of series 02 should be identical. No wall data is presented.
 - 5 DATA 5804 0101-0316. Pitot profiles. NX = 7 (Series 01), otherwise 2. Roughened surface.
 - 15 Editors' comments
 The entry describes a further systematic DRL attempt to describe the effects of roughness. For a complete view of the programme to 1959, see Fenter (1960). In the tests with varied roughness inserts the boundary layer was formed on a smooth "flat plate" leading edge with a trip, before encountering a step increase in roughness. A recent series of tests of similar type, but made on a tunnel wall, is described by Reda (1974) who was also able to measure the drag force on the second half of his insert. The absence of any shear stress measurement in the tests described here unfortunately reduces the value of the data greatly. The uniform roughness results (series 01) may be compared with those of Shutts & Fenter - CAT 5502 and Young - CAT 6506. For about half the profiles described, measurements do not extend within the momentum-deficit peak, so that integral values should be treated with caution.

DIMENSIONS OF SURFACE ROUGHNESS FOR PLATE INSERTS (Refer to figure 1)

INSERT NO	Type	h (mm)	w (mm)	d (mm)	β°
1	smooth	-	-	-	-
2	Uniform grain	(No 120 Aloxite, mean diameter		0.185 mm)	
3	"	(No 220 " " "		0.15 mm)	
4	"	(No 400 " " "		0.024 mm)	
5	"	(No 303 Optical grit, mean diameter		0.013 mm)	
6	A	0.51	(forward facing step)		0
7	B	0.127	4.78	19.1	-
8	B	0.127	4.78	9.5	-
9	C	0.127	0.254	10.2	0
10	C	0.127	0.254	2.54	0
11	C	0.127	0.254	1.27	0
12	C	0.127	0.254	0.51	0
13	C	0.127	0.254	0.25	0
14	C	0.127	0.254	0.25	20
15	C	0.127	0.254	0.25	40
16	D	2.6 mm	8.0	40	-

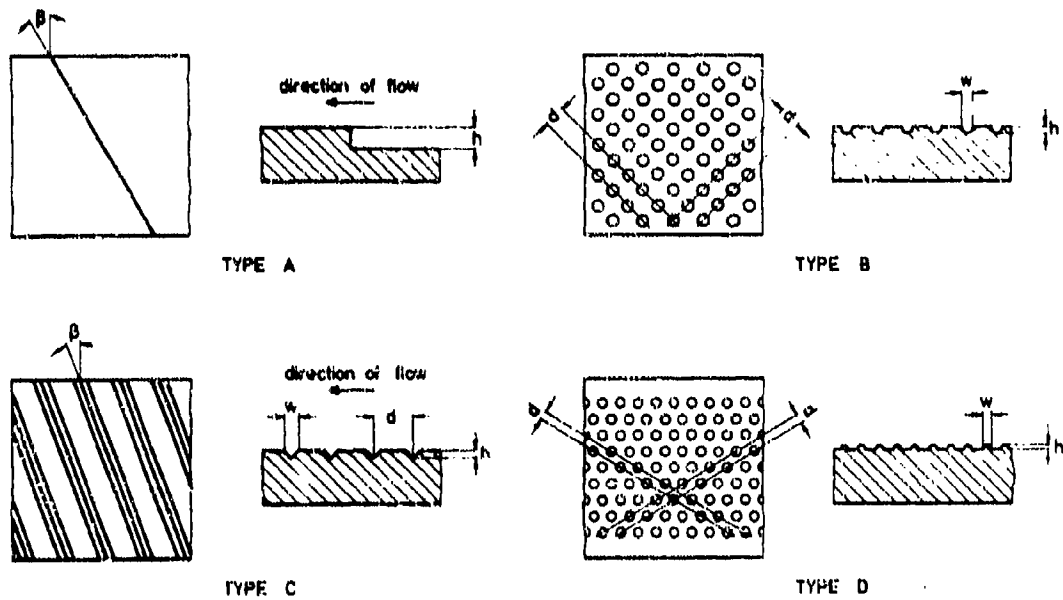


FIG. 1 TYPES OF MACHINED ROUGHNESS TESTED

5804 FENTER

27 PROFILES

CAT 5804		FENTER		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUH	MD *	TW/TR*	RED2W	CF	H1Z	H12K	PW	PD		
X *	POD*	PH/PD*	RED2D	CQ	H3Z	H32K	1W	TD		
RZ	TCD*	SW *	DZ	PI2*	H4Z	D2K	UD	TR		
58040101	2.6990	1.0000	4.0675"+03	NM	4.5245	1.4715	1.4121"+04	1.4121"+04		
1.9446"-01	3.2828"+05	1.0000	8.2436"+03	NM	1.7789	1.7615	3.0150"+02	1.3078"+02		
INFINITE	3.2131"+02	0.0000	3.2496"-04	0.0000"+00	0.1097	4.8635"-04	6.1884"+02	3.0150"+02		
58040102	2.7020	1.0000	6.3178"+03	NM	4.5304	1.4620	1.4001"+04	1.4001"+04		
2.9596"-01	3.2699"+05	1.0000	1.2812"+04	NM	1.7680	1.7479	3.0252"+02	1.3106"+02		
INFINITE	3.2242"+02	0.0000	5.1033"-04	0.0000"+00	0.1091	7.7408"-04	6.2019"+02	3.0252"+02		
58040103	2.7020	1.0000	7.9627"+03	NM	4.4111	1.4002	1.3876"+04	1.3876"+04		
3.9746"-01	3.2408"+05	1.0000	1.6147"+04	NM	1.7865	1.7677	3.0252"+02	1.3106"+02		
INFINITE	3.2242"+02	0.0000	6.4899"-04	0.0000"+00	0.1103	9.6118"-04	6.2019"+02	3.0252"+02		
58040104	2.6990	1.0000	9.6243"+03	NM	4.3527	1.3753	1.4053"+04	1.4053"+04		
4.9926"-01	3.2668"+05	1.0000	1.9920"+04	NM	1.7962	1.7773	3.0045"+02	1.3033"+02		
INFINITE	3.2020"+02	0.0000	7.8517"-04	0.0000"+00	0.1108	1.1464"-03	6.1777"+02	3.0045"+02		
58040105	2.6860	1.0000	1.1367"+04	NM	4.3054	1.3608	1.4249"+04	1.4249"+04		
6.0076"-01	3.2467"+05	1.0000	2.2908"+04	NM	1.7960	1.7786	3.0262"+02	1.3198"+02		
INFINITE	3.2242"+02	0.0000	9.1103"-04	0.0000"+00	0.1103	1.3278"-03	6.1839"+02	3.0262"+02		
58040106	2.6570	1.0000	1.3872"+04	NM	4.3063	1.3977	1.4905"+04	1.4905"+04		
7.0226"-01	3.2479"+05	1.0000	2.7643"+04	NM	1.7859	1.7662	3.0279"+02	1.3368"+02		
INFINITE	3.2242"+02	0.0000	1.0819"-03	0.0000"+00	0.1087	1.5845"-03	6.1593"+02	3.0279"+02		
58040107	2.6350	1.0000	1.4655"+04	NM	4.2551	1.3969	1.5347"+04	1.5347"+04		
8.0406"-01	3.2326"+05	1.0000	2.9321"+04	NM	1.7873	1.7678	3.0502"+02	1.3591"+02		
INFINITE	3.2064"+02	0.0000	1.1504"-03	0.0000"+00	0.1081	1.6728"-03	6.1591"+02	3.0502"+02		
58040201	2.2430	1.0000	5.5257"+03	NM	3.4373	1.3968	2.3163"+04	2.3163"+04		
2.9596"-01	3.6492"+05	1.0000	9.3371"+03	NM	1.8178	1.8041	3.2193"+02	1.6920"+02		
INFINITE	3.3964"+02	0.0000	3.8736"-04	0.0000"+00	0.0948	4.9876"-04	5.8514"+02	3.2193"+02		
58040201A	2.2470	1.0000	5.3640"+03	NM	3.4587	1.4019	2.2671"+04	2.2671"+04		
2.9596"-01	2.6092"+05	1.0000	9.0791"+03	NM	1.8124	1.7998	3.2137"+02	1.6872"+02		
INFINITE	3.3909"+02	0.0000	3.8234"-04	0.0000"+00	0.0947	4.9605"-04	5.8518"+02	3.2137"+02		
58040204	2.2390	1.0000	5.6371"+03	NM	3.4271	1.3965	2.3225"+04	2.3225"+04		
2.9596"-01	2.6397"+05	1.0000	9.5044"+03	NM	1.8196	1.8052	3.2249"+02	1.6988"+02		
INFINITE	3.4020"+02	0.0000	3.9602"-04	0.0000"+00	0.0947	5.0829"-04	5.8510"+02	3.2249"+02		

CAT 5804 FEETER BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD* TOD*	TW/TR* PW/PD* SM *	RED2* RED20 D2	CF CQ P12*	H12 H32 H42	H12K H32K J2K	PW TW UD	PD TD TR
58040301 8.0406*-01 INFINITE	2.2420 2.6593*+05 3.3909*+02	1.0000 1.0000 0.0000	1.1845*+04 2.0011*+04 8.2475*+04	NM NM 0.0000*+00	3.3263 1.8257 0.0951	1.3153 1.8116 1.0558*-03	2.3288*+04 3.2141*+02 5.8454*+02	2.3288*+04 1.6910*+02 3.2141*+02
58040301A 8.0406*-01 INFINITE	2.2430 2.6380*+05 3.3853*+02	1.0000 1.0000 0.0000	1.1988*+04 2.0264*+04 8.4045*+04	NM NM 0.0000*+00	3.3114 1.8257 0.0952	1.3023 1.8154 1.0747*-03	2.3065*+04 3.2088*+02 5.8419*+02	2.3065*+04 1.6874*+02 3.2088*+02
58040302 8.0406*-01 INFINITE	2.2310 2.6600*+05 3.3964*+02	1.0000 1.0000 0.0000	1.8797*+04 3.1621*+04 1.2986*-03	NM NM 0.0000*+00	3.4997 1.7664 0.0916	1.4231 1.7491 1.7559*-03	2.3599*+04 3.2202*+02 5.8358*+02	2.3699*+04 1.7021*+02 3.2202*+02
58040303 8.0406*-01 INFINITE	2.2350 2.6156*+05 3.4020*+02	1.0000 1.0000 0.0000	1.7965*+04 3.0261*+04 1.2692*-03	NM NM 0.0000*+00	3.5299 1.7648 0.0917	1.4403 1.7462 1.7185*-03	2.3158*+04 3.2252*+02 5.8458*+02	2.3158*+04 1.7018*+02 3.2252*+02
58040304 8.0406*-01 INFINITE	2.2350 2.6035*+05 3.4020*+02	1.0000 1.0000 0.0000	1.5079*+04 2.5399*+04 1.0703*-03	NM NM 0.0000*+00	3.4457 1.7838 0.0927	1.3890 1.7680 1.4247*-03	2.3050*+04 3.2252*+02 5.8458*+02	2.3050*+04 1.7018*+02 3.2252*+02
58040305 8.0406*-01 INFINITE	2.2410 2.5950*+05 3.3964*+02	1.0000 1.0000 0.0000	1.2809*+04 2.1628*+04 9.1509*+04	NM NM 0.0000*+00	3.3631 1.8102 0.0943	1.3353 1.7974 1.1883*-03	2.2760*+04 3.2194*+02 5.8488*+02	2.2760*+04 1.6945*+02 3.2194*+02
58040306 8.0406*-01 INFINITE	2.2400 2.6366*+05 3.3853*+02	1.0000 1.0000 0.0000	1.2257*+04 2.0695*+04 8.5748*+04	NM NM 0.0000*+00	3.3184 1.8241 0.0950	1.3122 1.8122 1.0967*-03	2.3162*+04 3.2090*+02 5.8388*+02	2.3162*+04 1.6897*+02 3.2090*+02
58040307 8.0406*-01 INFINITE	2.2330 2.6255*+05 3.4020*+02	1.0000 1.0000 0.0000	1.2081*+04 2.0334*+04 8.4883*+04	NM NM 0.0000*+00	3.2503 1.8421 0.0957	1.2820 1.8311 1.0622*-03	2.3318*+04 3.2253*+02 5.8432*+02	2.3318*+04 1.7033*+02 3.2253*+02
58040308 8.0406*-01 INFINITE	2.2440 2.5909*+05 3.4020*+02	1.0000 1.0000 0.0000	1.1349*+04 2.0025*+04 8.5178*+04	NM NM 0.0000*+00	3.2667 1.8405 0.0960	1.2766 1.8315 1.0714*-03	2.2618*+04 3.2245*+02 5.8575*+02	2.2618*+04 1.6950*+02 3.2245*+02
58040309 8.0406*-01 INFINITE	2.2440 2.6024*+05 3.3964*+02	1.0000 1.0000 0.0000	1.1899*+04 2.0114*+04 8.3075*+04	NM NM 0.0000*+00	3.3147 1.8265 0.0953	1.3046 1.8157 1.0612*-03	2.3242*+04 3.2192*+02 5.8527*+02	2.3242*+04 1.6922*+02 3.2192*+02
58040310 8.0406*-01 INFINITE	2.2560 2.6065*+05 3.3964*+02	1.0000 1.0000 0.0000	1.1891*+04 2.0191*+04 8.5699*+04	NM NM 0.0000*+00	3.3529 1.8227 0.0956	1.3158 1.8104 1.1011*-03	2.2331*+04 3.2183*+02 5.8683*+02	2.2331*+04 1.6832*+02 3.2183*+02
58040311 8.0406*-01 INFINITE	2.2410 2.5855*+05 3.3964*+02	1.0000 1.0000 0.0000	1.2158*+04 2.0529*+04 8.7178*+04	NM NM 0.0000*+00	3.3314 1.8207 0.0949	1.3186 1.8084 1.1192*-03	2.2677*+04 3.2194*+02 5.8488*+02	2.2677*+04 1.6945*+02 3.2194*+02
58040312 8.0406*-01 INFINITE	2.2390 2.5814*+05 3.3964*+02	1.0000 1.0000 0.0000	1.6266*+04 2.7445*+04 1.1661*-03	NM NM 0.0000*+00	3.4342 1.7868 0.0930	1.3763 1.7717 1.5498*-03	2.2712*+04 3.2196*+02 5.8462*+02	2.2712*+04 1.6960*+02 3.2196*+02
58040313 8.0406*-01 INFINITE	2.2390 2.5787*+05 3.3964*+02	1.0000 1.0000 0.0000	1.5202*+04 2.5650*+04 1.0910*-03	NM NM 0.0000*+00	3.4415 1.7851 0.0929	1.3806 1.7698 1.4524*-03	2.2689*+04 3.2196*+02 5.8462*+02	2.2689*+04 1.6960*+02 3.2196*+02
58040314 8.0406*-01 INFINITE	2.2390 2.5787*+05 3.3853*+02	1.0000 1.0000 0.0000	1.4370*+04 2.4256*+04 1.0191*-03	NM NM 0.0000*+00	3.4024 1.7965 0.0935	1.3587 1.7823 1.3416*-03	2.2864*+04 3.2091*+02 5.8367*+02	2.2864*+04 1.6904*+02 3.2091*+02
58040315 8.0406*-01 INFINITE	2.2380 2.6166*+05 3.3909*+02	1.0000 1.0000 0.0000	1.4289*+04 2.4104*+04 1.0100*-03	NM NM 0.0000*+00	3.3864 1.7995 0.0937	1.3496 1.7861 1.3255*-03	2.3005*+04 3.2144*+02 5.8402*+02	2.3005*+04 1.6940*+02 3.2144*+02
58040317 8.0406*-01 INFINITE	2.2260 2.6156*+05 3.3909*+02	1.0000 1.0000 0.0000	2.9359*+04 4.9305*+04 2.0495*-03	NM NM 0.0000*+00	3.4369 1.7649 0.0914	1.3763 1.7537 2.7841*-03	2.3486*+04 3.2154*+02 5.8244*+02	2.3486*+04 1.7031*+02 3.2154*+02

58040201		FENTER	PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/T0	RHO/RHO0*U/UD
1	0.0000*+00	1.0000*+00	NM	0.94784	0.00000	0.00000	1.90156	0.00000
2	2.2860*-04	2.2011*+00	NM	0.96821	0.50201	0.62489	1.54951	0.40328
3	2.8702*-04	2.3843*+00	NM	0.97017	0.53143	0.65425	1.51565	0.43167
4	3.4290*-04	2.5324*+00	NM	0.97166	0.55372	0.67505	1.48975	0.45366
5	4.6990*-04	2.6816*+00	NM	0.97311	0.57512	0.69606	1.46476	0.47520
6	5.9690*-04	2.8778*+00	NM	0.97492	0.60187	0.72060	1.43342	0.50271
7	7.2390*-04	3.0492*+00	NM	0.97644	0.62416	0.74044	1.40728	0.52615
8	9.7790*-04	3.3420*+00	NM	0.97888	0.66028	0.77143	1.36504	0.56514
9	1.2319*-03	3.6018*+00	NM	0.98092	0.69059	0.79637	1.32979	0.59887
10	1.4910*-03	3.8989*+00	NM	0.98312	0.72358	0.82240	1.29179	0.63664
11	1.7399*-03	4.1721*+00	NM	0.98503	0.75256	0.84435	1.25881	0.67075
12	2.2479*-03	4.7202*+00	NM	0.98856	0.80740	0.88360	1.19767	0.73777
13	2.7559*-03	5.2787*+00	NM	0.99182	0.85956	0.91829	1.14131	0.80459
14	3.2639*-03	5.8473*+00	NM	0.99484	0.90950	0.94921	1.08925	0.87144
15	3.7719*-03	6.2085*+00	NM	0.99661	0.93981	0.96696	1.05860	0.91343
16	4.7904*-03	6.8412*+00	NM	0.99948	0.99064	0.99504	1.00892	0.98625
17	5.8039*-03	6.9098*+00	NM	0.99978	0.99599	0.99788	1.00381	0.99409
18	6.8199*-03	6.9155*+00	NM	0.99980	0.99643	0.99812	1.00339	0.99475
19	9.3599*-03	6.8926*+00	NM	0.99971	0.99465	0.99718	1.00509	0.99213
20	1.1902*-02	6.9385*+00	NM	0.99990	0.99822	0.99906	1.00169	0.99737
21	1.4442*-02	6.9500*+00	NM	0.99995	0.99911	0.99953	1.00085	0.99869
D 22	2.3564*-02	6.9615*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040204		FENTER	PROFILE TABULATION		20 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/T0	RHO/RHO0*U/UD
1	0.0000*+00	1.0000*+00	NM	0.94793	0.00000	0.00000	1.89835	0.00000
2	2.2860*-04	2.1931*+00	NM	0.96821	0.50156	0.62412	1.54842	0.40307
3	3.0480*-04	2.3901*+00	NM	0.97032	0.53327	0.65974	1.51206	0.43368
4	4.3180*-04	2.6280*+00	NM	0.97269	0.56856	0.68961	1.47114	0.46976
5	5.6642*-04	2.8344*+00	NM	0.97463	0.59714	0.71602	1.43778	0.49800
6	6.8834*-04	3.0040*+00	NM	0.97614	0.61947	0.73602	1.41169	0.52138
7	9.3930*-04	3.2790*+00	NM	0.97846	0.65386	0.76576	1.37156	0.55831
8	1.1949*-03	3.5783*+00	NM	0.98084	0.68915	0.79495	1.33064	0.59742
9	1.4478*-03	3.8171*+00	NM	0.98262	0.71594	0.81625	1.29982	0.62797
10	1.7018*-03	4.0869*+00	NM	0.98494	0.74498	0.83848	1.26677	0.66190
11	2.2123*-03	4.6466*+00	NM	0.98821	0.80170	0.87949	1.20348	0.73079
12	2.7203*-03	5.2394*+00	NM	0.99170	0.85753	0.91646	1.14317	0.80203
13	3.2258*-03	5.7279*+00	NM	0.99432	0.90085	0.94393	1.09792	0.85974
14	3.7363*-03	6.2572*+00	NM	0.99694	0.94551	0.97016	1.05282	0.92149
15	4.4958*-03	6.7560*+00	NM	0.99921	0.98571	0.99239	1.01361	0.97907
16	5.2603*-03	6.8526*+00	NM	0.99963	0.99330	0.99645	1.00636	0.99016
17	6.3303*-03	6.8640*+00	NM	0.99968	0.99419	0.99693	1.00551	0.99147
18	7.2923*-03	6.8926*+00	NM	0.99980	0.99643	0.99811	1.00339	0.99474
19	9.6698*-03	6.8869*+00	NM	0.99978	0.99598	0.99780	1.00381	0.99409
D 20	2.4310*-02	6.9385*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040301		FENTER	PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/T0	RHO/RHO0*U/UD
1	0.0000*+00	1.0000*+00	NM	0.94786	0.00000	0.00000	1.90076	0.00000
2	2.2860*-04	2.0669*+00	NM	0.96671	0.47904	0.60122	1.57517	0.38164
3	2.7178*-04	2.2415*+00	NM	0.96867	0.50892	0.63180	1.54120	0.40994
4	3.2258*-04	2.3217*+00	NM	0.96953	0.52186	0.64475	1.52634	0.42240
5	4.5212*-04	2.4603*+00	NM	0.97097	0.54326	0.66571	1.50157	0.44334
6	5.7150*-04	2.5968*+00	NM	0.97232	0.56334	0.68491	1.47821	0.46334
7	6.3312*-04	2.8377*+00	NM	0.97458	0.59679	0.71592	1.43908	0.49748
8	1.0871*-03	3.0351*+00	NM	0.97634	0.62266	0.73904	1.40878	0.52460
9	1.3437*-03	3.1951*+00	NM	0.97770	0.64273	0.75648	1.38529	0.54608
10	1.8466*-03	3.4550*+00	NM	0.97981	0.67395	0.78274	1.34888	0.58029
11	2.3546*-03	3.6844*+00	NM	0.98157	0.70027	0.80406	1.31841	0.60987
12	2.8626*-03	3.9030*+00	NM	0.98317	0.72495	0.82294	1.29074	0.63758
13	3.3757*-03	4.1166*+00	NM	0.98467	0.74710	0.84023	1.26484	0.66430
14	3.8786*-03	4.3240*+00	NM	0.98607	0.76851	0.85602	1.24071	0.68995
15	4.8946*-03	4.7387*+00	NM	0.98870	0.80955	0.88504	1.19520	0.74049
16	5.9157*-03	5.1807*+00	NM	0.99130	0.85103	0.91275	1.15032	0.79347
17	6.9268*-03	5.5824*+00	NM	0.99353	0.88760	0.93590	1.11178	0.84180
18	7.9426*-03	5.9945*+00	NM	0.99560	0.92239	0.95684	1.07608	0.88919
19	8.9586*-03	6.3662*+00	NM	0.99738	0.95317	0.97452	1.04531	0.93228
20	1.0483*-02	6.7560*+00	NM	0.99914	0.98439	0.99170	1.01490	0.97714
21	1.2007*-02	6.9155*+00	NM	0.99983	0.99688	0.99835	1.00296	0.99540
22	1.3531*-02	6.9442*+00	NM	0.99995	0.99911	0.99953	1.00085	0.99869
23	1.6071*-02	6.9500*+00	NM	0.99998	0.99955	0.99977	1.00042	0.99934
D 24	2.3685*-02	6.9557*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040304		FENTER	PROFILE TABULATION			29 POINTS, DELTA AT POINT 29			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.94802	0.00000	0.00000	1.89514	0.00000	
2	2.2860 ⁻⁰⁴	1.5631 ⁺⁰⁰	NM	0.95999	0.36913	0.47974	1.68913	0.28402	
3	2.8194 ⁻⁰⁴	1.6072 ⁺⁰⁰	NM	0.96069	0.38121	0.49366	1.67700	0.29437	
4	3.3020 ⁻⁰⁴	1.6553 ⁺⁰⁰	NM	0.96143	0.39374	0.50793	1.66420	0.30521	
5	4.5720 ⁻⁰⁴	1.8160 ⁺⁰⁰	NM	0.96373	0.43132	0.54976	1.62460	0.33840	
6	5.8674 ⁻⁰⁴	1.9471 ⁺⁰⁰	NM	0.96543	0.45817	0.57870	1.59537	0.36274	
7	7.1374 ⁻⁰⁴	2.0570 ⁺⁰⁰	NM	0.96676	0.47875	0.60035	1.57252	0.38178	
8	9.6266 ⁻⁰⁴	2.2469 ⁺⁰⁰	NM	0.96890	0.51141	0.63374	1.53563	0.41269	
9	1.2192 ⁻⁰³	2.4221 ⁺⁰⁰	NM	0.97075	0.53915	0.66117	1.50384	0.43965	
10	1.4834 ⁻⁰³	2.5721 ⁺⁰⁰	NM	0.97225	0.56152	0.68266	1.47799	0.46188	
11	1.7272 ⁻⁰³	2.7008 ⁺⁰⁰	NM	0.97348	0.57987	0.69986	1.45670	0.48044	
12	2.2352 ⁻⁰³	2.9319 ⁺⁰⁰	NM	0.97560	0.61119	0.72837	1.42024	0.51285	
13	2.7559 ⁻⁰³	3.1483 ⁺⁰⁰	NM	0.97747	0.63893	0.75273	1.38796	0.54233	
14	3.2537 ⁻⁰³	3.3308 ⁺⁰⁰	NM	0.97898	0.66130	0.77176	1.36198	0.56664	
15	3.7592 ⁻⁰³	3.5511 ⁺⁰⁰	NM	0.98072	0.68875	0.79317	1.33200	0.59547	
16	4.2672 ⁻⁰³	3.7565 ⁺⁰⁰	NM	0.98227	0.71051	0.81176	1.30529	0.62190	
17	5.0317 ⁻⁰³	4.0657 ⁺⁰⁰	NM	0.98449	0.74407	0.83759	1.26716	0.66100	
18	5.7963 ⁻⁰³	4.3856 ⁺⁰⁰	NM	0.98664	0.77718	0.86196	1.23007	0.70074	
19	6.5583 ⁻⁰³	4.6925 ⁺⁰⁰	NM	0.98859	0.80761	0.88342	1.19655	0.73830	
20	7.3203 ⁻⁰³	5.0212 ⁺⁰⁰	NM	0.99056	0.83893	0.90459	1.16267	0.77803	
21	8.0772 ⁻⁰³	5.3381 ⁺⁰⁰	NM	0.99235	0.86801	0.92344	1.13101	0.81590	
22	8.8392 ⁻⁰³	5.6609 ⁺⁰⁰	NM	0.99408	0.89664	0.94128	1.10204	0.85413	
23	1.0112 ⁻⁰²	6.1708 ⁺⁰⁰	NM	0.99662	0.94004	0.96698	1.05813	0.91386	
24	1.1382 ⁻⁰²	6.6265 ⁺⁰⁰	NM	0.99874	0.97718	0.98776	1.02177	0.95671	
25	1.2649 ⁻⁰²	6.7787 ⁺⁰⁰	NM	0.99941	0.98926	0.99429	1.01019	0.98426	
26	1.3919 ⁻⁰²	6.8583 ⁺⁰⁰	NM	0.99975	0.99553	0.99763	1.00424	0.99342	
27	1.5189 ⁻⁰²	6.8812 ⁺⁰⁰	NM	0.99985	0.99732	0.99858	1.00254	0.99605	
28	1.7729 ⁻⁰²	6.8983 ⁺⁰⁰	NM	0.99993	0.99866	0.99929	1.00127	0.99802	
D 29	2.0269 ⁻⁰²	6.9155 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040308		FENTER	PROFILE TABULATION			29 POINTS, DELTA AT POINT 29			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.94782	0.00000	0.00000	1.90237	0.00000	
2	2.2860 ⁻⁰⁴	2.1693 ⁺⁰⁰	NM	0.96783	0.49643	0.61931	1.55627	0.39794	
3	2.7178 ⁻⁰⁴	2.2716 ⁺⁰⁰	NM	0.96895	0.51337	0.63643	1.53687	0.41411	
4	3.2512 ⁻⁰⁴	2.4017 ⁺⁰⁰	NM	0.97032	0.53387	0.65672	1.51319	0.43400	
5	4.5212 ⁻⁰⁴	2.6698 ⁺⁰⁰	NM	0.97294	0.57264	0.69381	1.46799	0.47263	
6	5.7658 ⁻⁰⁴	2.8477 ⁺⁰⁰	NM	0.97463	0.59759	0.71680	1.43873	0.49821	
7	7.0866 ⁻⁰⁴	2.9558 ⁺⁰⁰	NM	0.97560	0.61185	0.72962	1.42200	0.51310	
8	9.5504 ⁻⁰⁴	3.2314 ⁺⁰⁰	NM	0.97795	0.64661	0.75994	1.38124	0.55019	
9	1.2217 ⁻⁰³	3.3794 ⁺⁰⁰	NM	0.97916	0.66444	0.77498	1.36041	0.56966	
10	1.4757 ⁻⁰³	3.5356 ⁺⁰⁰	NM	0.98039	0.68271	0.79004	1.33914	0.58996	
11	1.9787 ⁻⁰³	3.7204 ⁺⁰⁰	NM	0.98179	0.70365	0.80687	1.31489	0.61364	
12	2.4841 ⁻⁰³	3.9113 ⁺⁰⁰	NM	0.98318	0.72460	0.82324	1.29081	0.63777	
13	2.9870 ⁻⁰³	4.0278 ⁺⁰⁰	NM	0.98401	0.73708	0.83278	1.27655	0.65237	
14	3.4976 ⁻⁰³	4.1550 ⁺⁰⁰	NM	0.98489	0.75045	0.84283	1.26136	0.66819	
15	4.0081 ⁻⁰³	4.3459 ⁺⁰⁰	NM	0.98616	0.77005	0.85724	1.23926	0.69174	
16	4.7701 ⁻⁰³	4.6879 ⁺⁰⁰	NM	0.98834	0.80392	0.88124	1.20160	0.73339	
17	5.5296 ⁻⁰³	5.0069 ⁺⁰⁰	NM	0.99025	0.83422	0.90179	1.16854	0.77172	
18	6.2992 ⁻⁰³	5.0934 ⁺⁰⁰	NM	0.99075	0.84225	0.90709	1.15990	0.78204	
19	7.0561 ⁻⁰³	5.4830 ⁺⁰⁰	NM	0.99292	0.87745	0.92964	1.12251	0.82819	
20	7.8232 ⁻⁰³	5.7433 ⁺⁰⁰	NM	0.99428	0.90018	0.94363	1.09887	0.85873	
21	8.5776 ⁻⁰³	5.9945 ⁺⁰⁰	NM	0.99555	0.92157	0.95639	1.07699	0.88802	
22	9.3396 ⁻⁰³	6.2735 ⁺⁰⁰	NM	0.99689	0.94474	0.96978	1.05371	0.92035	
23	1.0610 ⁻⁰²	6.7221 ⁺⁰⁰	NM	0.99894	0.98084	0.98979	1.01833	0.97197	
24	1.1880 ⁻⁰²	6.8583 ⁺⁰⁰	NM	0.99953	0.99153	0.99552	1.00806	0.98756	
25	1.4420 ⁻⁰²	6.9557 ⁺⁰⁰	NM	0.99995	0.99911	0.99951	1.00085	0.99869	
26	1.5692 ⁻⁰²	6.8185 ⁺⁰⁰	NM	0.99936	0.98841	0.99386	1.01105	0.98300	
27	1.6965 ⁻⁰²	6.8755 ⁺⁰⁰	NM	0.99961	0.99287	0.99623	1.00679	0.98952	
28	1.9502 ⁻⁰²	6.9615 ⁺⁰⁰	NM	0.99998	0.99955	0.99977	1.00042	0.99934	
D 29	2.2090 ⁻⁰²	6.9672 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

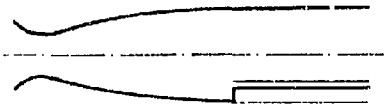
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040312		FENTER		PROFILE TABULATION		29 POINTS, DELTA AT POINT 29		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.94793	0.00000	0.00000	1.89835	0.00000
2	2.2860 ⁻ -04	1.6022 ⁺ +00	NM	0.96052	0.37919	0.49166	1.68120	0.29245
3	2.9210 ⁻ -04	1.6876 ⁺ +00	NM	0.96182	0.40107	0.51654	1.65866	0.31142
4	4.1656 ⁻ -04	1.8285 ⁺ +00	NM	0.96381	0.43323	0.55217	1.62445	0.33991
5	5.4864 ⁻ -04	1.9311 ⁺ +00	NM	0.96514	0.45422	0.57482	1.60152	0.35892
6	6.7310 ⁻ -04	2.0179 ⁺ +00	NM	0.96620	0.47075	0.59231	1.58318	0.37413
7	9.2710 ⁻ -04	2.2333 ⁺ +00	NM	0.96866	0.50826	0.63090	1.54078	0.40947
8	1.1760 ⁻ -03	2.3736 ⁺ +00	NM	0.97020	0.53149	0.65399	1.51412	0.43193
9	1.4554 ⁻ -03	2.5172 ⁺ +00	NM	0.97161	0.55248	0.67435	1.48983	0.45263
10	1.9431 ⁻ -03	2.7556 ⁺ +00	NM	0.97390	0.58642	0.70622	1.45030	0.48695
11	2.4407 ⁻ -03	2.9626 ⁺ +00	NM	0.97578	0.61411	0.73127	1.41795	0.51572
12	2.9616 ⁻ -03	3.1627 ⁺ +00	NM	0.97750	0.63957	0.75356	1.38822	0.54282
13	3.4696 ⁻ -03	3.3606 ⁺ +00	NM	0.97913	0.66369	0.77403	1.36013	0.56908
14	3.9903 ⁻ -03	3.5473 ⁺ +00	NM	0.98060	0.68557	0.79206	1.33477	0.59341
15	4.7371 ⁻ -03	3.8009 ⁺ +00	NM	0.98250	0.71416	0.81485	1.30186	0.62591
16	5.4915 ⁻ -03	4.0869 ⁺ +00	NM	0.98454	0.74498	0.83848	1.26677	0.66190
17	6.2738 ⁻ -03	4.3945 ⁺ +00	NM	0.98660	0.77669	0.86179	1.23116	0.69998
18	7.0282 ⁻ -03	4.6695 ⁺ +00	NM	0.98835	0.80393	0.88104	1.20103	0.73357
19	7.8003 ⁻ -03	4.9592 ⁺ +00	NM	0.99010	0.83162	0.89988	1.17089	0.76854
20	8.5471 ⁻ -03	5.1030 ⁺ +00	NM	0.99093	0.84502	0.90874	1.15649	0.78577
21	9.3091 ⁻ -03	5.5538 ⁺ +00	NM	0.99341	0.88566	0.93462	1.11362	0.83927
22	1.0577 ⁻ -02	6.0317 ⁺ +00	NM	0.99585	0.92675	0.95934	1.07157	0.89527
23	1.1849 ⁻ -02	6.4432 ⁺ +00	NM	0.99781	0.96070	0.97871	1.03785	0.94302
24	1.3119 ⁻ -02	6.7165 ⁺ +00	NM	0.99904	0.98258	0.99071	1.01681	0.97452
25	1.4389 ⁻ -02	6.8640 ⁺ +00	NM	0.99968	0.99419	0.99693	1.00551	0.99147
26	1.5659 ⁻ -02	6.9098 ⁺ +00	NM	0.99988	0.99777	0.99882	1.00212	0.99671
27	1.8199 ⁻ -02	6.9270 ⁺ +00	NM	0.99995	0.99911	0.99953	1.00085	0.99868
28	2.0739 ⁻ -02	6.9327 ⁺ +00	NM	0.99998	0.99955	0.99976	1.00042	0.99934
0 29	2.4173 ⁻ -02	6.9385 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58040316		FENTER		PROFILE TABULATION		29 POINTS, DELTA AT POINT 29		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.94823	0.00000	0.00000	1.88795	0.00000
2	2.2860 ⁻ -04	1.6518 ⁺ +00	NM	0.96159	0.39443	0.50800	1.65880	0.30625
3	2.8194 ⁻ -04	1.7024 ⁺ +00	NM	0.96235	0.40701	0.52215	1.64585	0.31725
4	4.0894 ⁻ -04	1.8119 ⁺ +00	NM	0.96389	0.43217	0.54995	1.61939	0.33961
5	5.3340 ⁻ -04	1.9333 ⁺ +00	NM	0.96547	0.45732	0.57707	1.59225	0.36242
6	6.6294 ⁻ -04	2.0107 ⁺ +00	NM	0.96642	0.47315	0.59273	1.57599	0.37610
7	9.1694 ⁻ -04	2.0845 ⁺ +00	NM	0.96729	0.48562	0.60675	1.56106	0.38868
8	1.1684 ⁻ -03	2.1772 ⁺ +00	NM	0.96835	0.50180	0.62331	1.54296	0.40397
9	1.6789 ⁻ -03	2.3133 ⁺ +00	NM	0.96983	0.52426	0.64584	1.51758	0.42557
10	2.1844 ⁻ -03	2.4367 ⁺ +00	NM	0.97111	0.54359	0.66476	1.49556	0.44449
11	2.6924 ⁻ -03	2.5445 ⁺ +00	NM	0.97219	0.55975	0.68028	1.47703	0.46057
12	3.4544 ⁻ -03	2.6689 ⁺ +00	NM	0.97340	0.57772	0.69719	1.45635	0.47872
13	4.2164 ⁻ -03	2.7849 ⁺ +00	NM	0.97448	0.59389	0.71210	1.43789	0.49531
14	4.9835 ⁻ -03	3.0213 ⁺ +00	NM	0.97660	0.62534	0.74027	1.40136	0.52825
15	5.7429 ⁻ -03	2.9558 ⁺ +00	NM	0.97603	0.61680	0.73273	1.41122	0.51922
16	6.5075 ⁻ -03	3.0457 ⁺ +00	NM	0.97681	0.62848	0.74302	1.39772	0.53160
17	7.7749 ⁻ -03	3.2168 ⁺ +00	NM	0.97826	0.65004	0.76165	1.37284	0.55480
18	9.0424 ⁻ -03	3.4398 ⁺ +00	NM	0.98007	0.67700	0.78422	1.34185	0.58443
19	1.0310 ⁻ -02	3.7244 ⁺ +00	NM	0.98225	0.70979	0.81066	1.30441	0.62148
20	1.1582 ⁻ -02	4.0953 ⁺ +00	NM	0.98491	0.75022	0.84173	1.25883	0.66866
21	1.2856 ⁻ -02	4.5285 ⁺ +00	NM	0.98778	0.79470	0.87403	1.20962	0.72257
22	1.4127 ⁻ -02	4.9973 ⁺ +00	NM	0.99084	0.84007	0.90503	1.16064	0.77977
23	1.5392 ⁻ -02	5.4328 ⁺ +00	NM	0.99308	0.88005	0.93080	1.11864	0.83208
24	1.6662 ⁻ -02	5.8056 ⁺ +00	NM	0.99504	0.91285	0.95089	1.08508	0.87633
25	1.7940 ⁻ -02	6.1278 ⁺ +00	NM	0.99664	0.94025	0.96698	1.05767	0.91426
26	1.9213 ⁻ -02	6.4046 ⁺ +00	NM	0.99795	0.96316	0.97997	1.03521	0.94664
27	2.0483 ⁻ -02	6.6209 ⁺ +00	NM	0.99893	0.98068	0.98963	1.01812	0.97182
28	2.1745 ⁻ -02	6.7900 ⁺ +00	NM	0.99968	0.99416	0.99689	1.00551	0.99143
0 29	2.3012 ⁻ -02	6.8640 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

	M : 2, 2.5, 3, 3.5 R THETA X 10 ⁻³ : 6 - 14 TW/TR : 1.0	5805
		ZPG RECOVERY AW
Continuous flow tunnel with flexible symmetrical nozzle. W = H = 50.8 mm 0.25 < P0 < 0.55 MN/m ² . T0 : 300 K. Air. RE/m X 10 ⁻⁶ : 32		
MOORE D.R., 1958. An experimental investigation of the turbulent boundary layer behind a forward facing step in supersonic flow. DRL 425.		

- 1 The test boundary layer was formed on one of the flexible nozzle plates and one of two extension plates. One of these continued the nozzle contour as a flat plate (L = 0.185 m). The other had a vertical step (X = 0 for both plates) 2.032 mm high approximately 25 mm downstream of the nozzle exit plane. Provision
- 8 was made for 10 survey stations on the centre line at 12.7 mm intervals starting at X = 6.8 mm. The surface was not actively cooled. The tunnel was run for a time sufficient to ensure that all temperatures were constant and the test surface was near-adiabatic. No checks are reported on uniformity of flow, transition,
- 2-6 or two dimensionality. The tunnel was that used by Naleid (CAT 5801) and Stalmach (CAT 5802).
- 6 Static pressure tapings were located just upstream of the first survey station, and half way between succeeding stations. Wall shear stress was measured with a minaturized FEB, following earlier DRL designs,
- 7 with a circular element of 6.35 mm diameter. Pitot profiles were measured with a CPP for which d₁ = 0.508 mm. This was cranked up and mounted in a streamwise tube for which d = 1.65 mm before being led through the wall in a 22° wedge fairing. The traverse gear was so mounted that the profile normal passed through the centre
- 8 line of the next station upstream. Thus profile and CF were determined at common values of X.
- 9 The profile data were reduced assuming constant static pressure through the layer, and this value was obtained from an interpolation of the wall static values. Constant total temperature was also assumed.
- 11 No profile corrections were applied, and the viscosity was calculated from Sutherland's law.
- 12 The editors have presented all the measured profiles and the associated CF values. The assumption of constant total temperature has been replaced by the Crocco / Van Driest temperature correlation with an adiabatic wall.
- 13 The unit Reynolds number for all the profiles was the same. For each of the four Mach numbers a set of profiles were taken on both the flat plate and the stepped plate. For the flat plate there were six in each set, at stations 1 (X = 6.77 mm), 2, 3, 4, 6 and 9 (X = 108.4 mm). For the stepped plate, profiles were taken at stations 2, 3, 4, 6 and 9. For the M = 2.0 stepped case (series 05) there is no profile for station 9.
- 14 CF is presented for each profile.
- 5 DATA 5805 0101 - 0405 (flat plate), 0501 - 0805 (step). PT2 profiles. NX = 4-6. CF from an FEB measured separately.

15 Editors' comments

The two test configurations allow of a direct comparison between a "normal" tunnel wall boundary layer, and the same layer subjected to an abrupt disturbance. Unfortunately, no attempt was made to check on cross-flow effects, which are likely to be marked in the region of the step, and the data throughout do not appear to be very accurate. The only comparisons are the "Ring" measurements of Peake et al. - CAT 7202, series 3 - which should be free of cross-flow effects, and the profiles measured downstream of violent trips by Stone & Cary - CAT 7209.

There are very few profiles for which measurements extend into the momentum-deficit-peak. The integral values should therefore be treated with reserve. The author remarks that data for station 9 (the last profiles) were "extremely erratic" and may have been affected by the tunnel diffuser.

CAT 5805		MOORE		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN X * RZ	MD * POD* TOD*	TW/TR* PW/PD* SW *	RED2W RED2D D2	CF * CQ PI2*	H12 H32 H42	H12K H32K D2K	PW TW UD	PD TD TR		
58050101 6.8072*-03 INFINITE	1.9930 2.5567*+05 2.9983*+02	1.0000 1.0000 0.0000	5.8423*+03 9.1184*+03 2.9319*-04	2.2700*-03 NM 0.0000*+00	3.1155 1.8109 0.0834	1.4768 1.8018 3.6263*-04	3.3034*+04 2.8603*+02 5.1653*+02	3.3034*+04 1.6709*+02 2.8603*+02		
58050102 1.9507*-02 INFINITE	1.9750 2.5699*+05 3.0039*+02	1.0000 1.0000 0.0000	6.0738*+03 9.4156*+03 2.9958*-04	2.2690*-03 NM 0.0000*+00	3.0702 1.8094 0.0803	1.4595 1.7998 3.6982*-04	3.4146*+04 2.8670*+02 5.1439*+02	3.4146*+04 1.6875*+02 2.8670*+02		
58050103 3.2207*-02 INFINITE	1.9980 2.5628*+05 2.9994*+02	1.0000 1.0000 0.0000	6.0240*+03 9.4191*+03 3.0296*-04	2.2480*-03 NM 0.0000*+00	3.1288 1.8027 0.0832	1.4756 1.7923 3.7760*-04	3.2856*+04 2.8610*+02 5.1735*+02	3.2856*+04 1.6678*+02 2.8610*+02		
58050104 4.4907*-02 INFINITE	2.0000 2.5500*+05 3.0206*+02	1.0000 1.0000 0.0000	6.1978*+03 9.6913*+03 3.1661*-04	2.2520*-03 NM 0.0000*+00	3.0787 1.8166 0.0840	1.4424 1.8073 3.8996*-04	3.2590*+04 2.8809*+02 5.1945*+02	3.2590*+04 1.6781*+02 2.8809*+02		
58050105 5.7607*-02 INFINITE	1.9510 2.5093*+05 2.9983*+02	1.0000 1.0000 0.0000	7.0987*+03 1.0910*+04 3.5094*-04	2.2180*-03 NM 0.0000*+00	3.0049 1.8045 0.0811	1.4380 1.7955 4.3298*-04	3.4606*+04 2.8636*+02 5.1038*+02	3.4606*+04 1.7024*+02 2.8636*+02		
58050106 1.0841*-01 INFINITE	1.9090 2.4944*+05 3.0261*+02	1.0000 1.0000 0.0000	8.1130*+03 1.2541*+04 4.1418*-04	2.0920*-03 NM 0.0000*+00	2.9981 1.8070 0.0821	1.4106 1.7980 5.1169*-04	3.3453*+04 2.8887*+02 5.1541*+02	3.3453*+04 1.7045*+02 2.8887*+02		
58050201 6.8072*-03 INFINITE	2.5350 3.2171*+05 2.9956*+02	1.0000 1.0000 0.0000	4.5381*+03 8.7142*+03 2.9058*-04	1.9160*-03 NM 0.0000*+00	4.0695 1.8192 0.1064	1.4448 1.8051 3.9714*-04	1.7832*+04 2.8203*+02 5.8192*+02	1.7832*+04 1.3108*+02 2.8203*+02		
58050202 1.9507*-02 INFINITE	2.5310 3.2347*+05 2.9761*+02	1.0000 1.0000 0.0000	4.6535*+03 8.9296*+03 2.9280*-04	1.9480*-03 NM 0.0000*+00	4.0682 1.8152 0.1060	1.4462 1.8002 4.0176*-04	1.8041*+04 2.8023*+02 5.7962*+02	1.8041*+04 1.3046*+02 2.8023*+02		
58050203 3.2207*-02 INFINITE	2.4850 3.2344*+05 3.0194*+02	1.0000 1.0000 0.0000	5.1447*+03 9.6774*+03 3.1565*-04	1.8150*-03 NM 0.0000*+00	3.9716 1.8134 0.1042	1.4427 1.7988 4.2990*-04	1.9409*+04 2.8459*+02 5.7910*+02	1.9409*+04 1.3510*+02 2.8459*+02		
58050204 4.4907*-02 INFINITE	2.4170 3.1974*+05 3.0094*+02	1.0000 1.0000 0.0000	5.4514*+03 9.9908*+03 3.1719*-04	1.9140*-03 NM 0.0000*+00	3.8565 1.8047 0.1011	1.4495 1.7909 4.3046*-04	2.1297*+04 2.8408*+02 5.7090*+02	2.1297*+04 1.3879*+02 2.8408*+02		
58050205 5.7607*-02 INFINITE	2.4570 3.2834*+05 3.0233*+02	1.0000 1.0000 0.0000	5.8032*+03 1.0796*+04 3.4301*-04	2.0320*-03 NM 0.0000*+00	3.8813 1.8153 0.1033	1.4391 1.8017 4.6345*-04	2.0548*+04 2.8514*+02 5.7653*+02	2.0548*+04 1.3697*+02 2.8514*+02		
58050206 1.0841*-01 INFINITE	2.4340 3.2513*+05 3.0206*+02	1.0000 1.0000 0.0000	6.7602*+03 1.2446*+04 3.9470*-04	1.6340*-03 NM 0.0000*+00	3.8365 1.8052 0.1018	1.4088 1.7929 5.3793*-04	2.1089*+04 2.8502*+02 5.7380*+02	2.1089*+04 1.3825*+02 2.8502*+02		
58050301 6.8072*-03 INFINITE	2.9550 4.2954*+05 3.0094*+02	1.0000 1.0000 0.0000	4.1293*+03 9.3485*+03 2.9473*-04	1.7050*-03 NM 0.0000*+00	4.9542 1.8256 0.1207	1.4144 1.8092 4.3707*-04	1.2513*+04 2.8104*+02 6.2019*+02	1.2513*+04 1.0958*+02 2.8104*+02		
58050302 1.9597*-02 INFINITE	3.0660 4.2909*+05 2.9761*+02	1.0000 1.0000 0.0000	3.5643*+03 8.4465*+03 2.7865*-04	1.8250*-03 NM 0.0000*+00	5.2050 1.8329 0.1244	1.4118 1.8154 4.1792*-04	1.0584*+04 2.7741*+02 6.2489*+02	1.0584*+04 1.0333*+02 2.7741*+02		
58050303 3.2207*-02 INFINITE	3.0460 4.2834*+05 3.0206*+02	1.0000 1.0000 0.0000	3.7268*+03 8.7397*+03 2.9193*-04	1.7980*-03 NM 0.0000*+00	5.1265 1.8395 0.1243	1.4018 1.8225 4.3068*-04	1.0885*+04 2.8164*+02 6.2811*+02	1.0885*+04 1.0578*+02 2.8164*+02		
58050304 4.4907*-02 INFINITE	3.0630 4.2509*+05 2.9828*+02	1.0000 1.0000 0.0000	3.9787*+03 9.4137*+03 3.1399*-04	1.6430*-03 NM 0.0000*+00	5.1724 1.8328 0.1243	1.3954 1.8149 4.7050*-04	1.0532*+04 2.7804*+02 6.2538*+02	1.0532*+04 1.0370*+02 2.7804*+02		
58050305 5.7607*-02 INFINITE	3.0030 4.2848*+05 3.0261*+02	1.0000 1.0000 0.0000	4.4865*+03 1.0342*+04 3.3022*-04	1.7120*-03 NM 0.0000*+00	5.0459 1.8214 0.1219	1.3906 1.8063 5.1132*-04	1.1612*+04 2.8236*+02 6.2553*+02	1.1612*+04 1.0794*+02 2.8236*+02		
58050306 1.0841*-01 INFINITE	2.9620 4.2333*+05 2.9983*+02	1.0000 1.0000 0.0000	5.3342*+03 1.2117*+04 3.8704*-04	1.1930*-03 NM 0.0000*+00	4.9712 1.8139 0.1202	1.4011 1.7950 5.8547*-04	1.2202*+04 2.7997*+02 6.1958*+02	1.2202*+04 1.0854*+02 2.7997*+02		
58050401 6.8072*-03 INFINITE	3.4280 5.5649*+05 2.9983*+02	1.0000 1.0000 0.0000	3.1514*+03 8.9337*+03 2.9484*-04	1.5280*-03 NM 0.0000*+00	6.4686 1.8208 0.1351	1.4127 1.7987 5.0245*-04	7.0120*+03 2.7759*+02 6.5570*+02	7.0120*+03 8.5928*+01 2.7759*+02		
58050402 1.9507*-02 INFINITE	3.4830 5.5401*+05 2.9372*+02	1.0000 1.0000 0.0000	3.3340*+03 9.3252*+03 2.9274*-04	1.4010*-03 NM 0.0000*+00	6.3740 1.8166 0.1338	1.4272 1.7930 4.9737*-04	7.4413*+03 2.7209*+02 6.4658*+02	7.4413*+03 8.5727*+01 2.7209*+02		
58050403 3.2207*-02 INFINITE	3.5410 5.5411*+05 3.0122*+02	1.0000 1.0000 0.0000	3.1389*+03 8.9348*+03 3.0025*-04	1.3680*-03 NM 0.0000*+00	6.4977 1.8233 0.1356	1.4124 1.8006 5.1034*-04	6.8550*+03 2.7883*+02 6.5791*+02	6.8550*+03 8.5674*+01 2.7883*+02		
58050404 4.4907*-02 INFINITE	3.5150 5.5361*+05 2.9606*+02	1.0000 1.0000 0.0000	3.3695*+03 9.5274*+03 3.0805*-04	1.5280*-03 NM 0.0000*+00	6.4531 1.8165 0.1345	1.4202 1.7924 5.2738*-04	7.1054*+03 2.7414*+02 6.5087*+02	7.1054*+03 8.5293*+01 2.7414*+02		

CAT 5805		MOORE		BOUNDARY CONDITIONS AND EVALUATED DATA, 91 UNITS.						
RUN X * RZ	MO * POD * TOD *	TW/TR * PW/PD * SW *	RED2W RED2D D2	CF * CO PI2 *	H12 H32 H42	H12K H32K D2K	PW Th UD	PD TD TR		
58050405 5.7607*-02 INFINITE	3.5240 5.5351*+05 3.0194*+02	1.0000 1.0000 0.0000	3.4146*+03 9.6516*+03 3.2290*-04	1.3540*-03 NM 0.0000*+00	6.4327 1.8234 0.1352	1.4049 1.7989 5.4583*-04	7.0141*+03 2.7956*+02 6.5779*+02	7.0141*+03 8.6673*+01 2.7956*+02		
58050406 1.0841*-01 INFINITE	3.3150 5.4744*+05 2.9650*+02	1.0000 1.0000 0.0000	4.8115*+03 1.2583*+04 3.7036*-04	8.6040*-04 NM 0.0000*+00	5.9558 1.8003 0.1260	1.4254 1.7776 6.2408*-04	9.3613*+03 2.7531*+02 6.4000*+02	9.3613*+03 9.2719*+01 2.7531*+02		
58050501 1.9507*-02 INFINITE	1.9780 2.5770*+05 2.9983*+02	1.0000 1.0000 0.0000	7.0136*+03 1.0886*+04 3.4500*-04	2.1770*-03 NM 0.0000*+00	3.0502 1.8048 0.0824	1.4380 1.7973 4.2822*-04	3.4082*+04 2.8614*+02 5.1435*+02	3.4082*+04 1.6821*+02 2.8614*+02		
58050502 3.2207*-02 INFINITE	1.9950 2.5740*+05 2.9622*+02	1.0000 1.0000 0.0000	6.8671*+03 1.0739*+04 3.3759*-04	2.1240*-03 NM 0.0000*+00	3.0657 1.8131 0.0836	1.4340 1.8057 4.1730*-04	3.3154*+04 2.8257*+02 5.1370*+02	3.3154*+04 1.6493*+02 2.8257*+02		
58050503 4.4907*-02 INFINITE	1.9640 2.5764*+05 2.9594*+02	1.0000 1.0000 0.0000	6.7339*+03 1.0412*+04 3.2219*-04	2.1900*-03 NM 0.0000*+00	2.9937 1.8223 0.0825	1.4228 1.8156 3.9268*-04	3.4822*+04 2.8254*+02 5.0897*+02	3.4822*+04 1.6706*+02 2.8254*+02		
58050504 5.7607*-02 INFINITE	1.9580 2.5743*+05 2.9650*+02	1.0000 1.0000 0.0000	7.9245*+03 1.2223*+04 3.7055*-04	2.1150*-03 NM 0.0000*+00	2.9821 1.8114 0.0818	1.4158 1.8019 4.6462*-04	3.5120*+04 2.8312*+02 5.0857*+02	3.5120*+04 1.6782*+02 2.8312*+02		
58050601 1.9507*-02 INFINITE	2.4630 3.2584*+05 2.9872*+02	1.0000 1.0000 0.0000	6.0244*+03 1.1251*+04 3.5528*-04	1.8470*-03 NM 0.0000*+00	3.9637 1.7961 0.0988	1.4424 1.7835 4.9342*-04	2.0201*+04 2.8169*+02 5.7371*+02	2.0201*+04 1.3497*+02 2.8169*+02		
58050602 3.2207*-02 INFINITE	2.4370 3.2442*+05 2.9733*+02	1.0000 1.0000 0.0000	6.7165*+03 1.2025*+04 3.8621*-04	1.6180*-03 NM 0.0000*+00	3.9011 1.7930 0.1012	1.4407 1.7796 5.3423*-04	2.0945*+04 2.8054*+02 5.6962*+02	2.0945*+04 1.3591*+02 2.8054*+02		
58050603 4.4907*-02 INFINITE	2.4050 3.2570*+05 2.9594*+02	1.0000 1.0000 0.0000	7.0103*+03 1.2816*+04 3.8769*-04	1.8040*-03 NM 0.0000*+00	3.8324 1.7954 0.1001	1.4406 1.7812 5.3058*-04	2.2105*+04 2.7944*+02 5.6484*+02	2.2105*+04 1.3721*+02 2.7944*+02		
58050604 5.7607*-02 INFINITE	2.4830 3.2672*+05 2.9983*+02	1.0000 1.0000 0.0000	6.2635*+03 1.1784*+04 3.7696*-04	1.8550*-03 NM 0.0000*+00	3.9268 1.8121 0.1041	1.4109 1.7981 5.1423*-04	1.9635*+04 2.8261*+02 5.7887*+02	1.9635*+04 1.3427*+02 2.8261*+02		
58050605 1.0841*-01 INFINITE	2.4330 3.2435*+05 2.9817*+02	1.0000 1.0000 0.0000	8.5625*+03 1.5810*+04 4.9244*-04	1.7480*-03 NM 0.0000*+00	3.8059 1.8071 0.1019	1.3920 1.7923 6.6823*-04	2.1072*+04 2.8136*+02 5.6999*+02	2.1072*+04 1.3653*+02 2.8136*+02		
58050701 1.9507*-02 INFINITE	3.0190 4.2862*+05 2.9733*+02	1.0000 1.0000 0.0000	4.4922*+03 1.0451*+04 3.3600*-04	1.7630*-03 NM 0.0000*+00	5.0960 1.8219 0.1224	1.3993 1.8061 5.0916*-04	1.1341*+04 2.7736*+02 6.2123*+02	1.1341*+04 1.0533*+02 2.7736*+02		
58050702 3.2207*-02 INFINITE	3.0090 4.3224*+05 2.9789*+02	1.0000 1.0000 0.0000	4.6435*+03 1.0757*+04 3.4200*-04	1.5410*-03 NM 0.0000*+00	5.0783 1.8199 0.1219	1.4014 1.8040 5.1871*-04	1.1609*+04 2.7793*+02 6.2107*+02	1.1609*+04 1.0598*+02 2.7793*+02		
58050703 4.4907*-02 INFINITE	2.9810 4.2987*+05 2.9983*+02	1.0000 1.0000 0.0000	4.9694*+03 1.1373*+04 3.6148*-04	1.7320*-03 NM 0.0000*+00	5.0086 1.8199 0.1211	1.4001 1.8020 5.4534*-04	1.2041*+04 2.7988*+02 6.2102*+02	1.2041*+04 1.0796*+02 2.7988*+02		
58050704 5.7607*-02 INFINITE	3.0030 4.2851*+05 2.9983*+02	1.0000 1.0000 0.0000	4.4898*+03 1.0365*+04 3.3446*-04	1.7470*-03 NM 0.0000*+00	4.8015 1.8155 0.2061	1.4206 1.7986 4.9560*-04	1.1613*+04 2.7977*+02 6.2265*+02	1.1613*+04 1.0695*+02 2.7977*+02		
58050705 1.0841*-01 INFINITE	2.8970 4.2855*+05 2.9733*+02	1.0000 1.0000 0.0000	6.4752*+03 1.4356*+04 4.3197*-04	1.6530*-03 NM 0.0000*+00	4.7883 1.8156 0.1183	1.3833 1.7986 6.4261*-04	1.3626*+04 2.7796*+02 6.1197*+02	1.3626*+04 1.1101*+02 2.7796*+02		
58050801 1.9507*-02 INFINITE	3.4970 5.5435*+05 2.9528*+02	1.0000 1.0000 0.0000	3.8569*+03 1.0835*+04 3.4518*-04	1.2810*-03 NM 0.0000*+00	6.4387 1.8035 0.1331	1.4195 1.7810 6.0460*-04	7.2991*+03 2.7348*+02 6.4905*+02	7.2991*+03 8.5692*+01 2.7348*+02		
58050802 3.2207*-02 INFINITE	3.5250 5.5445*+05 2.9539*+02	1.0000 1.0000 0.0000	3.8172*+03 1.0840*+04 3.5065*-04	1.1630*-03 NM 0.0000*+00	6.4819 1.8096 0.1342	1.4073 1.7871 6.1109*-04	7.0162*+03 2.7348*+02 6.5066*+02	7.0162*+03 8.4757*+01 2.7348*+02		
58050803 4.4907*-02 INFINITE	3.4640 5.5425*+05 2.9761*+02	1.0000 1.0000 0.0000	3.8948*+03 1.0786*+04 3.4163*-04	1.3110*-03 NM 0.0000*+00	6.2581 1.8186 0.1335	1.3896 1.7994 5.7718*-04	7.6488*+03 2.7576*+02 6.4980*+02	7.6488*+03 8.7536*+01 2.7576*+02		
58050804 5.7607*-02 INFINITE	3.5250 5.5218*+05 2.9900*+02	1.0000 1.0000 0.0000	3.7571*+03 1.0644*+04 3.5201*-04	1.3250*-03 NM 0.0000*+00	6.4443 1.8181 0.1348	1.3993 1.7958 6.0273*-04	6.9875*+03 2.7683*+02 6.5463*+02	6.9875*+03 8.5793*+01 2.7683*+02		
58050805 1.0841*-01 INFINITE	3.2600 5.7113*+05 2.9983*+02	1.0000 1.0000 0.0000	5.3817*+03 1.3746*+04 3.9230*-04	9.5350*-04 NM 0.0000*+00	5.7704 1.8046 0.1276	1.4164 1.7821 6.4632*-04	1.0321*+04 2.7863*+02 6.4019*+02	1.0321*+04 9.5931*+01 2.7863*+02		

58050405		MOORE		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92585	0.00000	0.00000	3.22541	0.00000	
2	2.5400-04	3.1649+00	NM	0.95479	0.40692	0.62472	2.35690	0.26506	
3	3.0480-04	3.4665+00	NM	0.95714	0.42963	0.64961	2.28629	0.28413	
4	3.5560-04	3.6925+00	NM	0.95884	0.44608	0.66696	2.23346	0.29835	
5	4.8260-04	4.1679+00	NM	0.96215	0.47872	0.69965	2.13604	0.32755	
6	7.3660-04	4.7991+00	NM	0.96610	0.51873	0.73677	2.01738	0.36521	
7	9.9060-04	5.3480+00	NM	0.96919	0.55108	0.76452	1.92467	0.39722	
8	1.2446-03	5.8891+00	NM	0.97197	0.58116	0.78162	1.84139	0.42827	
9	1.4986-03	6.4929+00	NM	0.97479	0.61294	0.81239	1.75669	0.46246	
10	1.7526-03	7.0713+00	NM	0.97726	0.64188	0.83262	1.68261	0.49484	
11	2.0066-03	7.6283+00	NM	0.97944	0.66856	0.85015	1.61700	0.52576	
12	2.2606-03	8.2713+00	NM	0.98176	0.69807	0.86835	1.54737	0.56118	
13	2.5146-03	8.8439+00	NM	0.98367	0.72333	0.88301	1.49025	0.59252	
14	2.7686-03	9.3800+00	NM	0.98591	0.75454	0.90001	1.42277	0.63258	
15	3.0226-03	1.0283+01	NM	0.98788	0.78320	0.91463	1.36377	0.67066	
16	3.2766-03	1.0903+01	NM	0.98948	0.80760	0.92636	1.31570	0.70408	
17	3.5306-03	1.1580+01	NM	0.99111	0.83343	0.93810	1.26697	0.74043	
18	4.0386-03	1.3038+01	NM	0.99422	0.86649	0.96026	1.17335	0.81839	
19	4.5466-03	1.4306+01	NM	0.99659	0.93019	0.97670	1.10249	0.88590	
20	5.0546-03	1.5777+01	NM	0.99899	0.97843	0.99316	1.03033	0.96392	
21	6.3246-03	1.6260+01	NM	0.99971	0.99376	0.99805	1.00866	0.98948	
22	7.5946-03	1.6332+01	NM	0.99982	0.99603	0.99876	1.00550	0.99330	
D 23	8.8646-03	1.6459+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58050801		MOORE		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92618	0.00000	0.00000	3.19144	0.00000	
2	2.5400-04	3.1021+00	NM	0.95457	0.40463	0.62012	2.34872	0.26403	
3	3.0480-04	3.3982+00	NM	0.95695	0.42780	0.64566	2.27789	0.28345	
4	3.5560-04	3.6293+00	NM	0.95871	0.44495	0.66382	2.22576	0.29825	
5	4.8260-04	3.9610+00	NM	0.96109	0.46840	0.68764	2.15521	0.31906	
6	7.3660-04	4.3459+00	NM	0.96365	0.49414	0.71248	2.07899	0.34271	
7	9.9060-04	4.6603+00	NM	0.96562	0.51415	0.73089	2.02077	0.36169	
8	1.2446-03	5.0069+00	NM	0.96765	0.53532	0.74951	1.96036	0.38233	
9	1.4986-03	5.4328+00	NM	0.96999	0.56019	0.77034	1.89098	0.40738	
10	1.7526-03	5.9417+00	NM	0.97257	0.58850	0.79271	1.81437	0.43690	
11	2.0066-03	6.4156+00	NM	0.97479	0.61367	0.81145	1.74847	0.46409	
12	2.2606-03	7.1236+00	NM	0.97782	0.64981	0.83635	1.68057	0.50426	
13	2.5146-03	7.8170+00	NM	0.98049	0.68259	0.85775	1.57911	0.54319	
14	2.7686-03	8.5712+00	NM	0.98313	0.71690	0.87830	1.50095	0.58516	
15	3.0226-03	9.2953+00	NM	0.98542	0.74836	0.89580	1.43288	0.62518	
16	3.2766-03	1.0093+01	NM	0.98771	0.78153	0.91300	1.36474	0.66899	
17	3.5306-03	1.0838+01	NM	0.98967	0.81127	0.92738	1.30673	0.70969	
18	3.7846-03	1.1640+01	NM	0.99160	0.84215	0.94136	1.24948	0.75340	
19	4.2926-03	1.3142+01	NM	0.99478	0.89705	0.96402	1.15487	0.83474	
20	5.0546-03	1.5084+01	NM	0.99825	0.96340	0.98809	1.05191	0.93933	
21	6.3246-03	1.6152+01	NM	0.99991	0.99800	0.99937	1.00275	0.99663	
D 22	7.5946-03	1.6215+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58050802		MOORE		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92584	0.00000	0.00000	3.22667	0.00000	
2	2.5400-04	3.0950+00	NM	0.95416	0.40085	0.61794	2.37642	0.26003	
3	3.0480-04	3.3271+00	NM	0.95604	0.41901	0.63818	2.31979	0.27510	
4	4.5720-04	3.9278+00	NM	0.96050	0.46241	0.68367	2.18592	0.31276	
5	7.1120-04	4.4523+00	NM	0.96398	0.49702	0.71710	2.08165	0.34449	
6	9.6520-04	4.8084+00	NM	0.96615	0.51915	0.73721	2.01652	0.36559	
7	1.2192-03	5.1856+00	NM	0.96830	0.54356	0.75662	1.95194	0.38763	
8	1.4732-03	5.5538+00	NM	0.97026	0.56255	0.77397	1.89285	0.40889	
9	1.7272-03	6.0690+00	NM	0.97282	0.59064	0.79594	1.81602	0.43829	
10	1.9812-03	6.5373+00	NM	0.97497	0.61504	0.81395	1.75146	0.46473	
11	2.2352-03	7.1411+00	NM	0.97753	0.64511	0.83485	1.67475	0.49849	
12	2.4892-03	7.7864+00	NM	0.98002	0.67574	0.85474	1.59992	0.53424	
13	2.7432-03	8.4557+00	NM	0.98238	0.70610	0.87314	1.52911	0.57101	
14	2.9972-03	9.1613+00	NM	0.98465	0.73674	0.89050	1.46096	0.60953	
15	3.2512-03	9.8832+00	NM	0.98677	0.76681	0.90641	1.39727	0.64870	
16	3.5052-03	1.0663+01	NM	0.98886	0.79801	0.92185	1.33444	0.68981	
17	3.7592-03	1.1452+01	NM	0.99079	0.82837	0.93588	1.27641	0.73321	
18	4.0132-03	1.2286+01	NM	0.99266	0.85929	0.94924	1.22031	0.77787	
19	4.5212-03	1.3788+01	NM	0.99564	0.91234	0.97018	1.13082	0.85795	
20	5.2832-03	1.5477+01	NM	0.99851	0.96851	0.98991	1.04469	0.94757	
21	6.5532-03	1.6278+01	NM	0.99972	0.99404	0.99814	1.00827	0.98996	
D 22	7.8232-03	1.6468+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58050803		MOORE		PROFILE TABULATION			21 POINTS, DELTA AT POINT 21		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92659	0.00000	0.00000	3.15027	0.00000	
2	2.5400-04	3.3644+00	NM	0.95711	0.42927	0.64480	2.25625	0.28578	
3	3.0480-04	3.5550+00	NM	0.95858	0.44371	0.66011	2.21330	0.29825	
4	4.3180-04	4.0278+00	NM	0.96197	0.47748	0.69423	2.11394	0.32841	
5	6.8580-04	4.6010+00	NM	0.96568	0.51530	0.72971	2.00530	0.36389	
6	9.3990-04	5.0021+00	NM	0.96805	0.54013	0.75151	1.93587	0.38820	
7	1.1938-03	5.2978+00	NM	0.97023	0.56351	0.77101	1.87204	0.41186	
8	1.4478-03	5.8056+00	NM	0.97233	0.58661	0.78932	1.81058	0.43595	
9	1.7018-03	6.2735+00	NM	0.97457	0.61201	0.80844	1.74492	0.46331	
10	1.9558-03	6.7844+00	NM	0.97684	0.63857	0.82731	1.67852	0.49288	
11	2.2090-03	7.3469+00	NM	0.97914	0.66657	0.84606	1.61106	0.52516	
12	2.4638-03	7.9154+00	NM	0.98128	0.69371	0.86316	1.54822	0.55752	
13	2.7178-03	8.5390+00	NM	0.98345	0.72229	0.88010	1.48472	0.59277	
14	2.9718-03	9.1947+00	NM	0.98555	0.75115	0.89616	1.42337	0.62961	
15	3.2258-03	9.8208+00	NM	0.98739	0.77771	0.91007	1.36935	0.66460	
16	3.4798-03	1.0569+01	NM	0.98942	0.80831	0.92513	1.30992	0.70625	
17	3.7338-03	1.1235+01	NM	0.99108	0.83458	0.93728	1.26125	0.74314	
18	4.2418-03	1.2758+01	NM	0.99445	0.89174	0.96147	1.16250	0.82707	
19	4.7498-03	1.4239+01	NM	0.99726	0.94400	0.98116	1.08028	0.90824	
20	5.2578-03	1.5276+01	NM	0.99900	0.97893	0.99316	1.02930	0.96489	
D 21	6.5278-03	1.5919+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

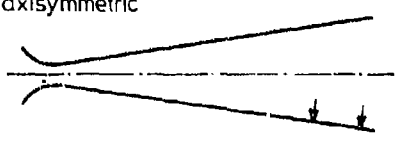
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58050804		MOORE		PROFILE TABULATION			22 POINTS, DELTA AT POINT 22		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92584	0.00000	0.00000	3.22647	0.00000	
2	2.5400-04	3.1305+00	NM	0.95445	0.40369	0.62115	2.36756	0.26236	
3	3.3020-04	3.5356+00	NM	0.95766	0.43461	0.65500	2.27137	0.28837	
4	5.8420-04	4.2977+00	NM	0.96299	0.48709	0.70776	2.11129	0.33524	
5	8.3820-04	4.8318+00	NM	0.96628	0.52057	0.73847	2.01239	0.36696	
6	1.0920-03	5.2935+00	NM	0.96889	0.54790	0.76186	1.93423	0.39388	
7	1.3462-03	5.7537+00	NM	0.97128	0.57362	0.78279	1.86227	0.42034	
8	1.6002-03	6.2139+00	NM	0.97351	0.59830	0.80170	1.79553	0.44650	
9	1.8542-03	6.7165+00	NM	0.97576	0.62411	0.82041	1.72796	0.47478	
10	2.1082-03	7.2172+00	NM	0.97783	0.64879	0.83731	1.66058	0.50272	
11	2.3622-03	7.7742+00	NM	0.97997	0.67518	0.85430	1.60128	0.53356	
12	2.6162-03	8.3346+00	NM	0.98197	0.70071	0.86996	1.54144	0.56438	
13	2.8702-03	8.9096+00	NM	0.98386	0.72596	0.88452	1.48496	0.59582	
14	3.1242-03	9.5254+00	NM	0.98574	0.75206	0.89874	1.42612	0.62931	
15	3.3782-03	1.0184+01	NM	0.98760	0.77907	0.91257	1.37232	0.66494	
16	3.6322-03	1.0823+01	NM	0.98927	0.80426	0.92481	1.32226	0.69942	
17	3.8862-03	1.1535+01	NM	0.99099	0.83149	0.93727	1.27061	0.73765	
18	4.1402-03	1.2270+01	NM	0.99262	0.85872	0.94990	1.22152	0.77773	
19	4.4882-03	1.3755+01	NM	0.99558	0.91121	0.96976	1.13564	0.85619	
20	5.1562-03	1.5058+01	NM	0.99784	0.95489	0.98534	1.06479	0.92533	
21	5.9182-03	1.6018+01	NM	0.99934	0.98582	0.99554	1.01982	0.97619	
D 22	7.1882-03	1.6468+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

58050805		PROFILE TABULATION			22 POINTS, DELTA AT POINT 22			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.92927	0.00000	0.00000	2.90447	0.00000
2	2.5400-04	2.7158+00	NM	0.95438	0.39908	0.59576	2.22852	0.26733
3	3.3480-04	2.9936+00	NM	0.95884	0.42454	0.62427	2.16227	0.28871
4	3.8100-04	3.2387+00	NM	0.96088	0.44571	0.64700	2.10724	0.30704
5	6.3500-04	3.8212+00	NM	0.96331	0.49202	0.69373	1.98793	0.34897
6	8.8900-04	4.2937+00	NM	0.96653	0.52638	0.72580	1.90122	0.38175
7	1.1438-03	4.6877+00	NM	0.96901	0.55337	0.74952	1.81456	0.40856
8	1.3978-03	5.0982+00	NM	0.97140	0.58006	0.77176	1.77015	0.43598
9	1.6518-03	5.5234+00	NM	0.97370	0.60644	0.79258	1.70810	0.46402
10	1.9058-03	5.9364+00	NM	0.97579	0.63098	0.81098	1.65192	0.49093
11	2.1598-03	6.3484+00	NM	0.97772	0.65427	0.82762	1.59999	0.51727
12	2.4138-03	6.7787+00	NM	0.97960	0.67822	0.84389	1.54820	0.54508
13	2.6678-03	7.2760+00	NM	0.98169	0.70460	0.86092	1.49292	0.57667
14	2.9218-03	7.7681+00	NM	0.98359	0.72975	0.87631	1.44399	0.60771
15	3.1758-03	8.2903+00	NM	0.98516	0.75552	0.89127	1.39163	0.64045
16	3.4298-03	8.8117+00	NM	0.98720	0.78037	0.90496	1.34480	0.67293
17	3.6838-03	9.3357+00	NM	0.98883	0.80460	0.91765	1.30075	0.70548
18	3.9378-03	9.8485+00	NM	0.99033	0.82761	0.92913	1.26038	0.73718
19	4.4458-03	1.1028+01	NM	0.99345	0.87822	0.95255	1.17044	0.80469
20	4.9538-03	1.2239+01	NM	0.99628	0.92730	0.97308	1.10117	0.88362
21	5.7158-03	1.3456+01	NM	0.99907	0.98560	0.99355	1.02490	0.96979
D 22	6.9858-03	1.4155+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

axisymmetric 	M : 8 - 10 R THETA X 10 ⁻³ : 1 - 3 TW/TR : 0.5	5901
		FPG - SHT
Conical nozzle. Continuous running. D = 50 mm. 3.4 < PO < 6.2 MN/m ² . TO : 756 K. "Superdry" Nitrogen. 5 < RE/m X 10 ⁻⁶ < 10.		
HILL F.K., 1959. Turbulent boundary layer measurements at Mach numbers from 8 to 10. Physics Fluids, 2, 778-680. And Hill (1956) and private communications.		

- 1 The test boundary layer was formed on the wall of a conical nozzle (semi-apex angle 6^o) with an outlet diameter of 50.8 mm. The surface was of electroformed nickel with a roughness less than 0.13 μm. An insert could be placed in the throat so as to increase the expansion ratio. The nozzle wall was cooled by the
- 2 surrounding room air, and ran until temperatures had reached equilibrium. The flow was "uniform and stable".
- 3 No measurement of transition is reported, but it is stated to be "consistent". The boundary layer had passed
- 4 through the very strong expansion at the throat, but pressure and Mach number gradients in the test area
- 5 were small, the flow in the free stream being very close to a spherical source flow. There was no evidence of cross-flow or separation in the boundary layer, and the nozzle was mounted so that it could be rotated about its own axis, the probes remaining stationary, providing a check on the axial symmetry of the flow. No circumferential variations were found within experimental accuracy.
- 6 Wall pressure was measured using a small static hole at the axial location of the profile normal. The wall temperature was recorded by a thermocouple mounted in an open port, flush with the wall surface, and sealed with cement.
- 7 Pitot measurements were made with a rake carrying four probes at y intervals of 13(E) mm. The two central probes were CPP (d₁ = 1.07, d₂ = 0.71, l = 25 mm) while the two outer probes were FPP (h₁ = 0.20, h₂ = 0.13, b₁ = 1.6 [E], l = 25 mm) formed by flattening the tube used for the inner probes. The rake could be traversed right across the nozzle so that the outer FPP could enter the boundary layer on either side and approach the wall. Four identical total temperature probes were mounted in a similar manner. These were STP consisting of a ceramic tubing shank (d = 2.5 mm) carrying an iron-constantan thermocouple with a vented shield which reduced in diameter towards the tip, so that the tip face had d₁ = 1.27, d₂ = 0.51 mm. The overall slender length of the probes was 51 mm. A static pressure survey showed negligible normal
- 8 pressure gradients. Measurements were made at two stations, 50.8 mm apart, and at distances X from the throat of approximately 190 [E] and 240 [E] mm. Pitot and total temperature traverses were made on the same normal using the same traverse gear, perpendicular to the axis of the nozzle.
- 9 The profiles were obtained in a very large number of runs, for which there were slight variations of total temperature and pressure from the selected nominal values. Spot profile values were cross plotted and normalised to the nominal total state. (For all runs one at least of the probes was in the free stream). The total temperature values were interpolated to the y-values of Pitot measurements. In general the wall temperature was obtained by extrapolating the TO profile to the wall. The value so deduced agreed with that recorded by the thermocouple to "within a few degrees". The author also presents skin friction and heat transfer values obtained from the gradients of the velocity and total temperature profiles close to the wall. The author's recovery factor was 0.85.
- 10 No corrections were applied to the profile data, the possible viscous and rarefied flow effects having been calculated to give errors less than 1 %, and any profile measurements near the wall being rejected when
- 11 interference effects were observed (approximately when Y was less than h₁). Viscosity values for data
- 12 reduction were taken from "Tables of thermal properties of gases" (Hilsenrath, 1955). The editors have presented all those data supplied by the author. Some of the boundary values, especially wall temperature, are revised, correct, values which differ from the published papers. The Y-value for the D-state has been

arbitrarily set well outside the boundary layer, and the D state stagnation values to the nominal tunnel stagnation values. Our standard integration procedures proved unable to handle the scatter in the data sensibly, so that for this entry the integral values have been obtained using a trapezoidal integration rule.

- 13 The profiles consist of three sets. The first two which have been combined in series 01-04 consist of profiles measured at two stations on the nozzle, one about 50 mm upstream of the exit (author's station R) and the other very close to the exit (author's station A). The third set consists of four individual profiles
- 14 taken at the nozzle exit with the throat insert in place, so giving a higher Mach number. The wall shear stress and heat transfer figures are the author's values obtained from the wall profile gradients.
- 5 DATA: 5901 0101-0801. Pitot and TO profiles obtained separately and normalised to nominal reservoir conditions. NX = 1 or 2.

15 Editors' comments

The geometrical arrangement here is similar to that of Perry & East - CAT 6801 and the Mach numbers are similar. The Reynolds numbers are, however, low by comparison and in no case has the inner region become fully turbulent. The outer region conforms very well to the transformed velocity profile expected of a fully developed ZPG boundary layer (Fernholz 1969). There are large differences between the measured temperature profiles and the values given by the Van Driest temperature velocity correlation.

Each profile is described by a great number of data points, which, however, display considerable scatter. The measurements extend within the momentum-deficit peak, but in some cases (0102, 0201, 0301) there remains a significant total pressure gradient in the outer part of the profile, so that the author's D-state position is not sufficiently far out.

CAT 5901 HILL BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.									
RUN	MD *	TW/TR	REN2W	CF *	H12	H12K	PW	PD	
X *	P00*	PW/PD*	REN2D	CG *	H32	H32K	TH*	TD	
RZ *	T00*	SW *	D2	PI2	H42	D2K	UD	TR	
59010101	8.2540	0.5308	3.3245**+02	9.1000*-04	11.3585	1.9687	2.8812**+02	2.8812**+02	
1.9000*-01	3.4474**+06	1.0000	1.8818**+03	1.5310*-04	1.7636	1.6829	3.6222**+02	5.1659**+01	
-2.0069*-02	7.5556**+02	0.0000	3.0094*-04	NM	1.2480	7.5778*-04	1.2087**+03	6.8235**+02	
59010102	9.0400	0.5160	2.5026**+02	9.1300*-04	13.8518	2.1738	1.5865**+02	1.5865**+02	
2.4000*-01	3.4474**+06	1.0000	1.6434**+03	1.6520*-04	1.7360	1.6905	3.5167**+02	4.3562**+01	
-2.5240*-02	7.5556**+02	0.0000	3.3757*-04	NM	1.2923	9.3649*-04	1.2156**+03	6.8151**+02	
59010201	8.2740	0.5537	4.1967**+02	8.4000*-04	10.0068	1.8914	3.4033**+02	3.4033**+02	
1.9000*-01	4.1368**+06	1.0000	2.4602**+03	1.3620*-04	1.7846	1.7045	3.7778**+02	5.1427**+01	
-2.0069*-02	7.5556**+02	0.0000	3.3004*-04	NM	1.3186	7.7347*-04	1.2089**+03	6.8233**+02	
59010202	9.0700	0.5274	2.8031**+02	8.7000*-04	13.9600	2.0820	1.8626**+02	1.8626**+02	
2.4000*-01	4.1368**+06	1.0000	1.8821**+03	1.3750*-04	1.8043	1.7058	3.5944**+02	4.3291**+01	
-2.5240*-02	7.5556**+02	0.0000	3.2515*-04	NM	1.2834	9.0488*-04	1.2159**+03	6.8148**+02	
59010301	8.2860	0.5537	4.4535**+02	7.9600*-04	10.9651	1.8833	3.7927**+02	3.7927**+02	
1.9000*-01	4.6540**+06	1.0000	2.6178**+03	1.2790*-04	1.7907	1.7102	3.7778**+02	5.1288**+01	
-2.0069*-02	7.5556**+02	0.0000	3.1340*-04	NM	1.2941	7.4480*-04	1.2090**+03	6.8231**+02	
59010401	8.2440	0.5423	4.7076**+02	7.3400*-04	11.0830	1.8771	4.1877**+02	4.1877**+02	
1.9000*-01	5.1711**+06	1.0000	2.7307**+03	1.1780*-04	1.7946	1.7139	3.7000**+02	5.1196**+01	
-2.0069*-02	7.5556**+02	0.0000	2.9500*-04	NM	1.2711	7.1514*-04	1.2091**+03	6.8230**+02	
59010402	9.1000	0.5462	3.1666**+02	8.0500*-04	14.2930	2.0420	2.2781**+02	2.2781**+02	
2.4000*-01	5.1711**+06	1.0000	2.1944**+03	1.2890*-04	1.8052	1.7159	3.7222**+02	4.3022**+01	
-2.5240*-02	7.5556**+02	0.0000	3.0609*-04	NM	1.2646	8.5754*-04	1.2161**+03	6.8145**+02	
59010501	10.0300	0.5157	1.3598**+02	8.4100*-04	21.4974	2.4460	9.5549**+01	9.5549**+01	
2.4000*-01	4.1368**+06	1.0000	1.0592**+03	1.7960*-04	1.7859	1.6406	3.8333**+02	3.9062**+01	
-2.5240*-02	8.2500**+02	0.0000	2.7675*-04	NM	1.2078	1.0391*-03	1.2772**+03	7.4326**+02	
59010601	10.0400	0.4918	1.5186**+02	7.6100*-04	22.7155	2.4804	1.1074**+02	1.1074**+02	
2.4000*-01	4.8263**+06	1.0000	1.1490**+03	1.6340*-04	1.7874	1.6518	3.6556**+02	3.8988**+01	
-2.5240*-02	8.2500**+02	0.0000	2.9716*-04	NM	1.1724	9.8498*-04	1.2773**+03	7.4325**+02	
59010701	10.0500	0.4674	1.8767**+02	6.9600*-04	21.0748	2.4556	1.2572**+02	1.2572**+02	
2.4000*-01	5.3158**+06	1.0000	1.3701**+03	1.3890*-04	1.8029	1.6723	3.4888**+02	3.3914**+01	
-2.5240*-02	8.3500**+02	0.0000	2.7000*-04	NM	1.2139	9.4490*-04	1.2773**+03	7.4325**+02	
59010801	10.0600	0.4724	1.9043**+02	6.7300*-04	22.7848	2.4658	1.4050**+02	1.4050**+02	
2.4000*-01	6.2033**+06	1.0000	1.3993**+03	1.6060*-04	1.8012	1.6676	3.5111**+02	3.8840**+01	
-2.5240*-02	8.2500**+02	0.0000	2.4583*-04	NM	1.1682	9.1763*-04	1.2774**+03	7.4324**+02	

TRAPEZOIDAL RULE FOR ALL INTEGRATIONS

59010101		HILL		PROFILE TABULATION			28 POINTS, DELTA AT POINT 28		
I	Y	P2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.00000	0.47941	0.00000	0.00000	7.01173	0.00000	
2	3.1750-04	1.7971+00	1.00000	0.51757	0.11568	0.29270	6.40250	0.04572	
3	3.8106-04	1.8870+00	1.00000	0.52234	0.12083	0.30500	6.37202	0.04787	
4	6.7310-04	2.6478+00	1.00000	0.54065	0.15499	0.37830	5.95740	0.06350	
5	9.0170-04	3.2573+00	1.00000	0.55503	0.17665	0.42160	5.69581	0.07402	
6	9.5290-04	3.3696+00	1.00000	0.55896	0.18032	0.42920	5.66512	0.07576	
7	9.7770-04	7.1879+00	1.00000	0.57267	0.27647	0.56000	4.10274	0.13649	
8	1.6510-03	1.1500+01	1.00000	0.62132	0.35454	0.64890	3.34979	0.19371	
9	1.6891-03	1.5722+01	1.00000	0.63424	0.41699	0.69190	2.75324	0.25130	
10	1.9558-03	1.9835+01	1.00000	0.65914	0.46988	0.72870	2.40510	0.30298	
11	2.5273-03	2.7052+01	1.00000	0.70477	0.55053	0.78040	2.00941	0.38837	
12	2.5908-03	2.9839+01	1.00000	0.71732	0.57868	0.79470	1.88597	0.42138	
13	3.0861-03	3.0990+01	1.00000	0.74216	0.58991	0.81110	1.89052	0.42904	
14	3.2512-03	3.3239+01	1.00000	0.75552	0.61126	0.82330	1.81414	0.45382	
15	3.2766-03	3.7642+01	1.00000	0.76679	0.65102	0.83760	1.65534	0.50600	
16	3.7592-03	3.8629+01	1.00000	0.79072	0.65961	0.85220	1.66921	0.51054	
17	3.7973-03	4.3128+01	1.00000	0.80485	0.69741	0.86640	1.54335	0.56138	
18	4.0513-03	4.2680+01	1.00000	0.81530	0.69374	0.87140	1.57778	0.59230	
19	4.1148-03	4.5924+01	1.00000	0.82502	0.71990	0.88075	1.49679	0.58842	
20	4.2291-03	4.8964+01	1.00000	0.88554	0.74358	0.91605	1.51769	0.60358	
21	5.1308-03	6.3578+01	1.00000	0.91024	0.84824	0.94160	1.23223	0.76414	
22	5.5499-03	6.8639+01	1.00000	0.93634	0.88160	0.95830	1.18158	0.81103	
23	6.1722-03	7.9740+01	1.00000	0.98684	0.95067	0.98980	1.08402	0.91308	
24	6.8961-03	8.4004+01	1.00000	1.00101	0.97590	0.99880	1.04748	0.95353	
25	7.5585-03	8.6135+01	1.00000	1.00444	0.98827	1.00140	1.02676	0.97530	
26	8.0645-03	8.6031+01	1.00000	1.00252	0.98767	1.00040	1.02595	0.97510	
27	8.2423-03	8.7060+01	1.00000	1.00449	0.99359	1.00180	1.01659	0.98545	
D 28	1.5240-02	8.8181+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,U/UD
D=STATE ARTIFICIAL Y=0.6 IN

AT I=4,10,11,12,19,20,25 DATA WERE AVERAGED

59010102		HILL		PROFILE TABULATION			38 POINTS, DELTA AT POINT 38		
I	Y	P2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.00000	0.46544	0.00000	0.00000	8.07276	0.00000	
2	6.4770-04	1.7306+00	1.00000	0.41324	0.10188	0.25220	6.12784	0.04116	
3	7.2390-04	1.8776+00	1.00000	0.40478	0.10985	0.26600	5.86410	0.04536	
4	7.4930-04	1.7754+00	1.00000	0.53189	0.10442	0.29220	7.82485	0.03751	
5	9.0170-04	1.7537+00	1.00000	0.54409	0.10321	0.29260	8.03752	0.03640	
6	9.5250-04	2.2854+00	1.00000	0.55570	0.12799	0.35290	7.60280	0.04642	
7	1.0795-03	2.7751+00	1.00000	0.56125	0.14591	0.39210	7.22173	0.05429	
8	1.1557-03	2.3245+00	1.00000	0.56524	0.12954	0.35930	7.69374	0.04670	
9	1.1938-03	2.9285+00	1.00000	0.57048	0.15100	0.40540	7.20840	0.05624	
10	1.2065-03	3.2643+00	1.00000	0.57161	0.16150	0.42580	6.95092	0.06126	
11	1.2827-03	3.8579+00	1.00000	0.57805	0.17843	0.45820	6.59445	0.06948	
12	1.5113-03	4.5692+00	1.00000	0.55005	0.19668	0.47550	5.84486	0.08135	
13	1.5621-03	5.8712+00	1.00000	0.64198	0.22190	0.55100	6.16564	0.08937	
14	1.9685-03	1.0362+01	1.00000	0.63137	0.30653	0.63700	4.31860	0.14750	
15	2.1209-03	1.0692+01	1.00000	0.65240	0.31162	0.65170	4.37380	0.14900	
16	2.1463-03	1.1671+01	1.00000	0.65612	0.32622	0.66490	4.19432	0.16005	
17	2.3495-03	1.6477+01	1.00000	0.67928	0.39004	0.71700	3.37917	0.21218	
18	2.6543-03	1.9424+01	1.00000	0.69952	0.42445	0.74440	3.07586	0.24201	
19	2.9185-03	2.5212+01	1.00000	0.72321	0.48496	0.78040	2.58959	0.30136	
20	2.9337-03	2.7983+01	1.00000	0.72791	0.51139	0.79120	2.39366	0.33054	
21	3.0353-03	2.5620+01	1.00000	0.73062	0.48894	0.78570	2.58229	0.30426	
22	3.4290-03	3.0211+01	1.00000	0.76000	0.53169	0.81425	2.34528	0.34719	
23	3.4544-03	2.9053+01	1.00000	0.77122	0.52124	0.81730	2.45861	0.33242	
24	3.7719-03	3.4521+01	1.00000	0.77786	0.56892	0.83320	2.14888	0.38046	
25	3.9497-03	3.6713+01	1.00000	0.78506	0.58695	0.84110	2.05351	0.40959	
26	4.2418-03	3.9668+01	1.00000	0.80275	0.61040	0.85540	1.96387	0.43557	
27	5.7023-03	5.7848+01	1.00000	0.87248	0.73850	0.91240	1.52642	0.59774	
28	5.9182-03	5.9075+01	1.00000	0.88098	0.74635	0.91780	1.51221	0.60693	
29	6.2484-03	6.9094+01	1.00000	0.89641	0.78374	0.93010	1.40837	0.66041	
30	7.1628-03	8.2003+01	1.00000	0.94133	0.88031	0.96220	1.19470	0.80539	
31	7.4549-03	8.6006+01	1.00000	0.95417	0.90166	0.97040	1.15829	0.83779	
32	7.6581-03	8.6542+01	1.00000	0.95149	0.90448	0.96925	1.14835	0.84404	
33	7.7851-03	8.8777+01	1.00000	0.95423	0.91615	0.97150	1.12448	0.86395	
34	8.6487-03	1.0026+02	1.00000	0.98476	0.97389	0.99080	1.03502	0.95728	
35	8.6741-03	1.0035+02	1.00000	0.98570	0.97434	0.99130	1.03512	0.95768	
36	9.0678-03	1.0694+02	1.00000	0.99652	1.00597	0.99860	0.98539	1.01340	
37	9.1059-03	1.0346+02	1.00000	0.98330	0.98938	0.99100	1.00328	0.98776	
D 38	1.5240-02	1.0568+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,U/UD
D=STATE ARTIFICIAL Y=0.6 IN

AT I=22,32 DATA WERE AVERAGED

59010401		HILL		PROFILE TABULATION			29 POINTS, DELTA AT POINT 29		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.00000	0.48971	0.00000	0.00000	7.22712	0.00000	
2	3.1750*-04	2.0283*+00	1.00000	0.52915	0.12760	0.32230	6.38015	0.05052	
3	3.8100*-04	2.3091*+00	1.00000	0.53516	0.14052	0.35020	6.21063	0.05639	
4	6.7310*-04	2.9934*+00	1.00000	0.55742	0.16686	0.40695	5.94798	0.06842	
5	9.0170*-04	4.0873*+00	1.00000	0.58138	0.20112	0.47220	5.51234	0.08566	
6	9.5250*-04	4.7442*+00	1.00000	0.58704	0.21898	0.50030	5.21989	0.09584	
7	9.7790*-04	1.2326*+01	1.00000	0.60425	0.36582	0.64810	3.13872	0.20649	
8	1.6510*-03	1.5199*+01	1.00000	0.65890	0.40779	0.70130	1.95758	0.23712	
9	1.6891*-03	1.9382*+01	1.00000	0.69670	0.46211	0.74670	2.61102	0.28598	
10	1.9558*-03	2.2525*+01	1.00000	0.69296	0.49904	0.75855	2.31044	0.32831	
11	2.5273*-03	2.8671*+01	1.00000	0.73933	0.56431	0.80355	2.02763	0.39630	
12	2.5908*-03	3.1898*+01	1.00000	0.80339	0.59573	0.84575	2.01550	0.41962	
13	3.0861*-03	3.2701*+01	1.00000	0.77605	0.60329	0.83300	1.90649	0.43693	
14	3.2512*-03	3.4948*+01	1.00000	0.79085	0.62397	0.84550	1.83612	0.46048	
15	3.2766*-03	3.9948*+01	1.00000	0.80190	0.66768	0.86000	1.65908	0.51836	
16	3.3401*-03	4.2578*+01	1.00000	0.80862	0.68956	0.86740	1.58233	0.54818	
17	3.7592*-03	4.1490*+01	1.00000	0.82726	0.68059	0.87580	1.65593	0.52889	
18	3.7973*-03	4.5499*+01	1.00000	0.81242	0.71307	0.87320	1.49996	0.58230	
19	4.0513*-03	4.4714*+01	1.00000	0.84472	0.70682	0.88940	1.58333	0.56173	
20	4.1148*-03	4.8899*+01	1.00000	0.85719	0.73950	0.90090	1.48415	0.60701	
21	4.2291*-03	5.1487*+01	1.00000	0.92490	0.75900	0.93860	1.52924	0.61377	
22	5.1308*-03	6.7489*+01	1.00000	0.92702	0.86992	0.95250	1.19887	0.79450	
23	5.5499*-03	7.3944*+01	1.00000	0.95183	0.91084	0.96890	1.13155	0.85628	
24	6.1722*-03	8.3474*+01	1.00000	0.98157	0.96811	0.98850	1.04257	0.94814	
25	6.8901*-03	8.6575*+01	1.00000	0.99553	0.98603	0.99680	1.02197	0.97537	
26	7.5565*-03	8.6665*+01	1.00000	0.99606	0.98654	0.99710	1.02153	0.97699	
27	8.0605*-03	8.6093*+01	1.00000	0.99252	0.98329	0.99510	1.02417	0.97162	
28	8.2423*-03	8.6655*+01	1.00000	0.99347	0.98648	0.99580	1.01898	0.97726	
D 29	1.5240*-02	8.9033*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

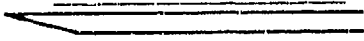
INPUT VARIABLES Y,M,U/UD
D=STATE ARTIFICIAL Y=0.6 IN

AT I=4,10,11,12,20,21,26 DATA WERE AVERAGED

59010402		HILL		PROFILE TABULATION			38 POINTS, DELTA AT POINT 38		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.00000	0.49265	0.00000	0.00000	8.65187	0.00000	
2	6.4770*-04	1.9749*+00	1.00000	0.55678	0.11384	0.32300	8.05027	0.04012	
3	7.4930*-04	2.2091*+00	1.00000	0.56383	0.12407	0.34850	7.89043	0.04417	
4	9.0170*-04	2.7653*+00	1.00000	0.57688	0.14462	0.39670	7.52481	0.05272	
5	9.5250*-04	3.2132*+00	1.00000	0.58121	0.15890	0.42630	7.19742	0.05923	
6	1.0795*-03	4.7063*+00	1.00000	0.59615	0.19868	0.49990	6.33071	0.07896	
7	1.1557*-03	3.5861*+00	1.00000	0.58235	0.16978	0.44670	6.92242	0.06453	
8	1.1938*-03	4.4433*+00	1.00000	0.60612	0.19231	0.49410	6.60141	0.07485	
9	1.2065*-03	4.6466*+00	1.00000	0.60067	0.19725	0.49960	6.41503	0.07788	
10	1.2827*-03	6.7447*+00	1.00000	0.61475	0.24231	0.56690	5.47367	0.10357	
11	1.5113*-03	8.0331*+00	1.00000	0.63856	0.26615	0.60460	5.16025	0.11716	
12	1.5621*-03	8.9030*+00	1.00000	0.64220	0.28110	0.62130	4.88522	0.12718	
13	1.8415*-03	1.7839*+01	1.00000	0.68392	0.40363	0.72740	3.24779	0.22397	
14	2.1209*-03	1.8989*+01	1.00000	0.69419	0.39363	0.72780	3.41866	0.21289	
15	2.1463*-03	1.7962*+01	1.00000	0.69790	0.40505	0.73550	3.29714	0.22307	
16	2.4765*-03	2.6100*+01	1.00000	0.71179	0.49033	0.77670	2.50917	0.30954	
17	2.6492*-03	2.6215*+01	1.00000	0.74038	0.49143	0.79250	2.60063	0.30473	
18	2.9185*-03	2.9259*+01	1.00000	0.75745	0.51967	0.81020	2.43068	0.33332	
19	2.9337*-03	2.9871*+01	1.00000	0.75942	0.52516	0.81280	2.39539	0.33932	
20	3.0353*-03	2.9259*+01	1.00000	0.76420	0.51967	0.81380	2.45233	0.33185	
21	3.4290*-03	3.3274*+01	1.00000	0.78466	0.55473	0.83400	2.26035	0.36897	
22	3.4544*-03	3.4494*+01	1.00000	0.75132	0.56495	0.81850	2.09906	0.38994	
23	3.7719*-03	3.7001*+01	1.00000	0.80292	0.58538	0.85080	2.11238	0.40277	
24	3.9497*-03	3.8609*+01	1.00000	0.80471	0.59813	0.85710	2.05338	0.41741	
25	4.2418*-03	4.1886*+01	1.00000	0.82303	0.62330	0.86910	1.94424	0.44701	
26	5.7023*-03	6.2030*+01	1.00000	0.89263	0.75989	0.92570	1.48402	0.62378	
27	5.9182*-03	6.4276*+01	1.00000	0.90490	0.77363	0.93360	1.45633	0.64106	
28	6.2484*-03	7.0607*+01	1.00000	0.91713	0.81110	0.94380	1.35388	0.69706	
29	7.1628*-03	8.9954*+01	1.00000	0.95783	0.91615	0.97340	1.12888	0.86227	
30	7.4549*-03	9.0470*+01	1.00000	0.96318	0.91879	0.97630	1.12910	0.86467	
31	7.6581*-03	9.0298*+01	1.00000	0.96676	0.91791	0.97805	1.13532	0.86147	
32	7.7851*-03	9.0384*+01	1.00000	0.96838	0.91835	0.97890	1.13621	0.86155	
33	8.6487*-03	1.0536*+02	1.00000	0.99374	0.99187	0.99640	1.00916	0.95736	
34	8.6741*-03	1.0443*+02	1.00000	0.98987	0.98747	0.99420	1.01367	0.98079	
35	9.0678*-03	1.0788*+02	1.00000	0.99778	1.00374	0.99910	0.99078	1.00839	
36	9.1059*-03	1.0680*+02	1.00000	0.99735	0.99868	0.99860	0.99984	0.99876	
37	9.3726*-03	1.0758*+02	1.00000	0.99974	1.00231	1.00000	0.99540	1.00462	
D 38	1.5240*-02	1.0708*+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,U/UD
D=STATE ARTIFICIAL Y=0.6 IN

AT I=2,31 DATA WERE AVERAGED

	M : 5 R THETA X 10 ⁻³ : 1 - 4.5 TW/TR : 0.65 - 0.95	5902
		ZPG-MHT
Continuous tunnel with fixed contoured nozzle, W = H = 0.12 m (E). 0.5 < P0 < 0.75 MN/m ² . 340 < T0 < 500 K. Air. 8 < RE/m X 10 ⁻⁶ < 16.		
WINKLER E.M. and CHA M.H., 1959. Investigation of flat plate hypersonic turbulent boundary layers with heat transfer at a Mach number of 5.2. NOL NAVORD Rep 6631. Also Winkler (1961)		

- 1 The test boundary layer was formed on a smooth stainless steel flat plate 0.604 m long mounted with the test surface on the tunnel centre-line and spanning the tunnel. The leading edge (X = 0) was chamfered on the underside, and except for the first 40 mm (E) the whole length of the test surface could be actively
- 8 cooled. Measurements were made at stations for which X = 0.216, 0.2925, 0.3685 and 0.445 m. The static
- 2 pressure along the plate was constant to within 1.3 % and the plate surface was practically isothermal
- 4 for leading edge distances > 0.14 m. For X < 0.14 m the surface temperature deviated from the isothermal value by amounts dependant on the test conditions; for the lowest TW/TR reported here the deviation was
- 3 about 10 %. The test free stream conditions were selected to cause transition near X = 170 mm.

- 6 Static pressure tappings (d = 0.63 mm) were drilled at X = 70 mm and at subsequent intervals of 76.2 mm, alternately 9 mm to either side of the plate centre line. Thermocouple plugs, of the same material as the plate, were placed 4.75 mm to either side of the centre-line (E) at the same stations. Each plug contained five thermocouple junctions at known distances from the plate surface.

- 7 Boundary layer surveys were made with FPP and STP. The probes used had "nearly rectangular entrance openings of half heights between 0.1 and 0.13 mm" (h₁ = 0.2 - 0.26 mm). The STP was of the type described by Winkler (1954).

- 9 The authors have interpolated the T0 readings to the Y-values of the Pitot readings. The T0 profile was extrapolated to match the wall temperature gradient calculated from the wall heat transfer rate. This was deduced from the temperature gradient in the wall, and the authors present CF values deduced from the slope of the velocity profile near the wall, and from Reynolds analogy (Colburn's formula). Static pressure
- 12 was assumed constant across the boundary layer. The editors have presented all the reported profiles, incorporating the authors assumptions and procedures. The D-state is the authors', at the outermost point.
- 13 The CF value is that deduced from the velocity gradient. The profiles form three groups marked by differing heat transfer conditions. Within each group there are some repeats, and some slight variation of unit
- 14 Reynolds number. There are four successive profiles in each group. Heat transfer values are given for nearly all the profiles, and the authors' CF value referred to above.

- § DATA: 59020101-0306. Pitot and T0 profiles obtained separately. NX = 4. Wall heat flux from temperature gradient in wall.

- 15 Editors' comments
The Reynolds number range of the test is low, and the test layer displays marked transitional characteristics. The experimental range overlaps, in some degree, the tests made by Danberg - CAT 6702 and Samuels et al. - CAT 6701.
The profiles include data taken very close to the plate surface, but it seems probable that the temperature values used in the wall region were interpolated. The CF values quoted should be treated with considerable reserve since they are obtained from the velocity gradient which must inevitably be somewhat ill-defined.
The entry has been prepared from a rather limited published account.

CAT 5902		WINKLER		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN X * RZ	MD * POD* TOD	TW/TR PW/PD* SW *	RED2W RED20 D2	CF * CQ * P12*	H12 H32 H42	H12K H32K D2K	PM TW* UD	PD TD* TR		
59020101 2.1600*-01 INFINITE	5.2100 7.2042**+05 3.8239**+02	0.9773 1.0000 0.0000	4.0164**+02 2.1242**+03 1.7955**+04	1.4650**+03 9.3700**+04 0.0000**+00	10.1251 1.8434 0.5230	1.6742 1.7598 3.7325**+04	1.0694**+03 3.0602**+02 8.0563**+02	1.0694**+03 5.9480**+01 3.4880**+02		
59020102 2.1600*-01 INFINITE	5.1400 7.1738**+05 3.4480**+02	0.9598 1.0000 0.0000	5.7784**+02 2.7364**+03 1.9249**+04	1.3690**+03 NM 0.0000**+00	8.1905 1.8579 0.7277	1.5583 1.7847 3.6338**+04	1.1533**+03 3.0200**+02 7.6338**+02	1.1533**+03 5.4870**+01 3.1465**+02		
59020103 2.9250*-01 INFINITE	5.2000 7.3055**+05 3.6558**+02	0.9193 1.0000 0.0000	6.3024**+02 2.9030**+03 2.2510**+04	1.4320**+03 8.5800**+04 0.0000**+00	11.2967 1.8241 0.3632	1.6730 1.7180 5.0578**+04	1.0968**+03 3.0659**+02 7.8748**+02	1.0968**+03 5.7050**+01 3.3349**+02		
59020104 3.6850*-01 INFINITE	5.2600 7.4069**+05 3.6718**+02	0.9169 1.0000 0.0000	7.5907**+02 3.5535**+03 2.8111**+04	1.3460**+03 8.4700**+04 0.0000**+00	10.0987 1.8602 0.4797	1.4336 1.7954 5.7632**+04	1.0390**+03 3.0702**+02 7.9061**+02	1.0390**+03 5.6200**+01 3.3484**+02		
59020105 4.4500*-01 INFINITE	5.2900 7.1839**+05 3.6283**+02	0.9251 1.0000 0.0000	8.2486**+02 3.4366**+03 3.1963**+04	1.3080**+03 8.0400**+04 0.0000**+00	12.3679 1.8292 0.1830	1.4167 1.7842 7.5294**+04	9.7430**+02 3.0602**+02 7.8659**+02	9.7430**+02 5.5000**+01 3.3081**+02		
59020201 2.1600*-01 INFINITE	4.9800 5.4918**+05 3.8317**+02	0.8286 1.0000 0.0000	4.4438**+02 1.7388**+03 1.7398**+04	1.3350**+03 8.5300**+04 0.0000**+00	11.2871 1.8396 0.2143	1.5629 1.7707 3.8292**+04	1.0625**+03 2.9001**+02 8.0059**+02	1.0625**+03 6.4290**+01 3.5001**+02		
59020202 2.1600*-01 INFINITE	5.1800 7.1029**+05 3.9918**+02	0.8137 1.0000 0.0000	4.3063**+02 1.7570**+03 1.5852**+04	1.6060**+03 NM 0.0000**+00	9.8808 1.8738 0.4748	1.4904 1.8304 3.0278**+04	1.0909**+03 2.9632**+02 8.2238**+02	1.0909**+03 6.2700**+01 3.6418**+02		
59020203 2.9250*-01 INFINITE	5.2000 7.1434**+05 3.7423**+02	0.8223 1.0000 0.0000	6.3665**+02 2.6752**+03 2.1976**+04	1.2480**+03 7.3500**+04 0.0000**+00	11.3023 1.8510 0.3124	1.5198 1.7817 4.7624**+04	1.0724**+03 2.8073**+02 7.9675**+02	1.0724**+03 5.8400**+01 3.4138**+02		
59020204 3.6850*-01 INFINITE	5.2400 7.0826**+05 3.7897**+02	0.8477 1.0000 0.0000	7.6239**+02 3.3134**+03 2.8490**+04	1.1510**+03 7.3800**+04 0.0000**+00	11.3939 1.8350 0.3196	1.5149 1.7699 6.3794**+04	1.0162**+03 2.9301**+02 8.0274**+02	1.0162**+03 5.8380**+01 3.4563**+02		
59020205 4.4500*-01 INFINITE	5.2400 6.6368**+05 3.8378**+02	0.8397 1.0000 0.0000	8.3216**+02 3.5793**+03 3.3473**+04	NM 6.7100**+04 0.0000**+00	11.4975 1.8440 0.2696	1.3612 1.8001 7.6757**+04	9.5224**+02 2.9389**+02 8.0781**+02	9.5224**+02 5.9120**+01 3.5001**+02		
59020301 2.1600*-01 INFINITE	5.1700 6.8597**+05 4.5531**+02	0.6717 1.0000 0.0000	2.8185**+02 9.5886**+02 1.0864**+04	1.4700**+03 9.6800**+04 0.0000**+00	11.7680 1.7670 0.4604	2.0454 1.6257 2.7850**+04	1.0656**+03 2.7904**+02 8.7803**+02	1.0656**+03 7.1750**+01 4.1542**+02		
59020302 2.9250*-01 INFINITE	5.1600 6.7989**+05 4.7647**+02	0.6418 1.0000 0.0000	4.8604**+02 1.5782**+03 1.9184**+04	1.3230**+03 8.3500**+04 0.0000**+00	10.6369 1.8478 0.3731	1.5080 1.7776 4.0161**+04	1.0683**+03 2.7902**+02 8.9793**+02	1.0683**+03 7.5330**+01 4.3475**+02		
59020303 2.9250*-01 INFINITE	5.1000 6.9306**+05 4.6767**+02	0.6324 1.0000 0.0000	5.2358**+02 1.6517**+03 1.8668**+04	1.3350**+03 NM 0.0000**+00	10.4141 1.8568 0.3635	1.4972 1.7919 3.7518**+04	1.1666**+03 2.6997**+02 8.8796**+02	1.1666**+03 7.5410**+01 4.2690**+02		
59020304 3.6850*-01 INFINITE	5.2000 7.6095**+05 4.6753**+02	0.6448 1.0000 0.0000	7.1533**+02 2.3661**+03 2.5492**+04	1.2030**+03 NM 0.0000**+00	10.8378 1.8440 0.3708	1.5619 1.7805 5.2899**+04	1.1424**+03 2.7499**+02 8.9054**+02	1.1424**+03 7.2960**+01 4.2649**+02		
59020305 3.6850*-01 INFINITE	5.1100 7.2954**+05 4.9624**+02	0.6182 1.0000 0.0000	7.8660**+02 2.4160**+03 2.8467**+04	1.2360**+03 7.9900**+04 0.0000**+00	9.9868 1.8532 0.4211	1.4692 1.7973 5.6749**+04	1.2139**+03 2.8000**+02 9.1495**+02	1.2139**+03 7.9750**+01 4.5292**+02		
59020306 4.4500*-01 INFINITE	5.1200 7.0927**+05 4.6641**+02	0.6601 1.0000 0.0000	7.0596**+02 2.3195**+03 2.5748**+04	1.0540**+03 6.7200**+04 0.0000**+00	16.7644 1.7413 -0.2228	1.8501 1.6361 8.6902**+04	1.1667**+03 2.8098**+02 8.8730**+02	1.1667**+03 7.4710**+01 4.2567**+02		

59020103		WINKLER		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.83864	0.00000	0.00000	5.37400	0.00000	
2	1.9200 ⁻ 04	2.0837 ⁺ 00	NM	0.91864	0.20783	0.45400	4.77200	0.09514	
3	2.1800 ⁻ 04	2.2663 ⁺ 00	NM	0.92176	0.22117	0.47800	4.67100	0.10233	
4	2.4300 ⁻ 04	2.4982 ⁺ 00	NM	0.92575	0.23667	0.50500	4.55300	0.11092	
5	2.6900 ⁻ 04	3.0165 ⁺ 00	NM	0.93208	0.26743	0.55500	4.30700	0.12886	
6	2.9400 ⁻ 04	3.0799 ⁺ 00	NM	0.93148	0.27091	0.56000	4.27300	0.13106	
7	3.1900 ⁻ 04	3.6481 ⁺ 00	NM	0.93670	0.30015	0.60300	4.03600	0.14941	
8	3.4500 ⁻ 04	3.8468 ⁺ 00	NM	0.93775	0.30967	0.61600	3.95700	0.15567	
9	3.9600 ⁻ 04	4.5838 ⁺ 00	NM	0.94124	0.34254	0.65800	3.69000	0.17832	
10	4.4600 ⁻ 04	5.1962 ⁺ 00	NM	0.94357	0.36753	0.68700	3.49400	0.19662	
11	4.9700 ⁻ 04	5.7953 ⁺ 00	NM	0.94427	0.39039	0.71100	3.31700	0.21435	
12	5.7300 ⁻ 04	6.6529 ⁺ 00	NM	0.94451	0.42090	0.74000	3.09100	0.23940	
13	7.0000 ⁻ 04	7.9037 ⁺ 00	NM	0.94650	0.46175	0.77500	2.81700	0.27512	
14	8.2700 ⁻ 04	9.0510 ⁺ 00	NM	0.94571	0.49623	0.80000	2.59900	0.30781	
15	9.5400 ⁻ 04	1.0078 ⁺ 01	NM	0.94561	0.52517	0.81900	2.43200	0.33676	
16	1.0810 ⁻ 03	1.1012 ⁺ 01	NM	0.94563	0.55016	0.83400	2.29800	0.36292	
17	1.2080 ⁻ 03	1.1751 ⁺ 01	NM	0.94434	0.56915	0.84400	2.19900	0.38381	
18	1.4620 ⁻ 03	1.2923 ⁺ 01	NM	0.94690	0.59803	0.86000	2.06800	0.41586	
19	1.7160 ⁻ 03	1.3667 ⁺ 01	NM	0.95042	0.61564	0.87000	1.99700	0.43565	
20	2.2240 ⁻ 03	1.5632 ⁺ 01	NM	0.95661	0.65793	0.89200	1.82700	0.48823	
21	2.7320 ⁻ 03	1.8265 ⁺ 01	NM	0.96188	0.71537	0.91500	1.63600	0.55929	
22	3.2400 ⁻ 03	2.0979 ⁺ 01	NM	0.97143	0.76757	0.93600	1.48700	0.62946	
23	3.7480 ⁻ 03	2.3969 ⁺ 01	NM	0.98053	0.82163	0.95500	1.35100	0.70688	
24	5.0150 ⁻ 03	3.4740 ⁺ 01	NM	0.99495	0.93252	0.98600	1.11800	0.88143	
25	6.2880 ⁻ 03	3.4359 ⁺ 01	NM	0.99822	0.98669	0.99700	1.02100	0.97649	
D 26	8.0280 ⁻ 03	3.5290 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

59020105		WINKLER		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.84344	0.00000	0.00000	5.56400	0.00000	
2	1.9100 ⁻ 04	1.6563 ⁺ 00	NM	0.88862	0.16646	0.37500	5.07500	0.07349	
3	2.2600 ⁻ 04	1.8710 ⁺ 00	NM	0.89117	0.18719	0.41500	4.91500	0.08444	
4	2.6700 ⁻ 04	2.2675 ⁺ 00	NM	0.89533	0.21749	0.47000	4.67000	0.10064	
5	3.1700 ⁻ 04	2.5868 ⁺ 00	NM	0.89806	0.23614	0.50500	4.49700	0.11230	
6	3.9400 ⁻ 04	3.1187 ⁺ 00	NM	0.90310	0.26837	0.55300	4.24600	0.13024	
7	4.4400 ⁻ 04	3.4163 ⁺ 00	NM	0.90633	0.28371	0.57600	4.12200	0.13974	
8	5.2100 ⁻ 04	4.2295 ⁺ 00	NM	0.91261	0.32161	0.62800	3.81300	0.16470	
9	7.7500 ⁻ 04	5.7392 ⁺ 00	NM	0.92026	0.38170	0.69800	3.34400	0.20873	
10	1.2830 ⁻ 03	8.0860 ⁺ 00	NM	0.93120	0.45945	0.77100	2.81600	0.27379	
11	1.7910 ⁻ 03	9.7219 ⁺ 00	NM	0.93726	0.50656	0.80700	2.53800	0.31797	
12	2.4260 ⁻ 03	1.1446 ⁺ 01	NM	0.94535	0.55184	0.83800	2.30600	0.36340	
13	3.0610 ⁻ 03	1.3412 ⁺ 01	NM	0.95502	0.59929	0.86700	2.09300	0.41424	
14	3.5940 ⁻ 03	1.5608 ⁺ 01	NM	0.96428	0.64819	0.89300	1.89800	0.47050	
15	4.3310 ⁻ 03	1.8209 ⁺ 01	NM	0.97868	0.70170	0.92000	1.71900	0.53519	
16	4.9660 ⁻ 03	2.0536 ⁺ 01	NM	0.98803	0.74632	0.93900	1.58300	0.59316	
17	5.6010 ⁻ 03	2.3399 ⁺ 01	NM	1.00140	0.79779	0.96000	1.44800	0.66298	
18	6.2360 ⁻ 03	2.6205 ⁺ 01	NM	1.00618	0.84520	0.97400	1.32800	0.73343	
19	6.8710 ⁻ 03	2.9250 ⁺ 01	NM	1.00520	0.89381	0.98400	1.21200	0.81188	
20	7.5060 ⁻ 03	3.1878 ⁺ 01	NM	1.00802	0.93372	0.99300	1.13100	0.87798	
21	8.1410 ⁻ 03	3.3853 ⁺ 01	NM	1.00998	0.96263	0.99900	1.07700	0.92758	
22	9.4110 ⁻ 03	3.5823 ⁺ 01	NM	1.00288	0.99063	1.00000	1.01900	0.98135	
D 23	1.0681 ⁻ 02	3.6495 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

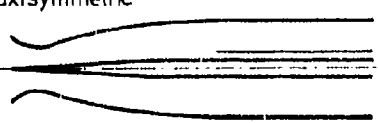
INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

59020302		WINKLER		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.58560	0.00000	0.00000	3.70400	0.00000	
2	1.5200*+04	1.7387*+00	NM	0.88047	0.17931	0.39100	4.75500	0.08223	
3	2.2900*+04	1.7801*+00	NM	0.88232	0.16340	0.39900	4.73300	0.08430	
4	2.5400*+04	1.9248*+00	NM	0.88699	0.19656	0.42400	4.65300	0.09112	
5	2.7900*+04	2.1129*+00	NM	0.89294	0.21167	0.45200	4.56000	0.09912	
6	3.3000*+04	2.5803*+00	NM	0.90405	0.24374	0.50800	4.34400	0.11694	
7	3.8100*+04	3.1587*+00	NM	0.90228	0.27731	0.55800	4.04900	0.13781	
8	4.3200*+04	4.1024*+00	NM	0.91437	0.32396	0.62400	3.71000	0.16819	
9	4.8300*+04	5.0069*+00	NM	0.92263	0.36279	0.67200	3.43100	0.19586	
10	5.3300*+04	5.9069*+00	NM	0.92874	0.39752	0.71000	3.19000	0.22257	
11	5.8400*+04	6.8971*+00	NM	0.93384	0.43251	0.74400	2.95900	0.25144	
12	7.1100*+04	9.1929*+00	NM	0.94151	0.50421	0.80200	2.53000	0.31700	
13	8.3800*+04	1.1000*+01	NM	0.94149	0.55410	0.83300	2.26000	0.36858	
14	1.3460*+03	1.4346*+01	NM	0.95230	0.63619	0.87900	1.90900	0.46045	
15	1.6000*+03	1.6019*+01	NM	0.95573	0.67347	0.89600	1.77000	0.50621	
16	1.8540*+03	1.8824*+01	NM	0.95884	0.69070	0.90400	1.71300	0.52773	
17	2.3620*+03	1.9507*+01	NM	0.96602	0.74522	0.92600	1.54400	0.59974	
18	2.8700*+03	2.2554*+01	NM	0.97303	0.80268	0.94600	1.38900	0.68107	
19	3.3780*+03	2.5551*+01	NM	0.98316	0.85541	0.96400	1.27000	0.75926	
20	3.8860*+03	2.8491*+01	NM	0.99024	0.90416	0.97800	1.17000	0.83590	
21	4.6480*+03	3.1696*+01	NM	0.99725	0.95447	0.99100	1.07800	0.91929	
22	5.9180*+03	3.4272*+01	NM	1.00021	0.99306	0.99900	1.01200	0.98715	
D 23	7.1880*+03	3.4746*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

59020306		WINKLER		PROFILE TABULATION		31 POINTS, DELTA AT POINT 31			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.60245	0.00000	0.00000	3.76100	0.00000	
2	5.9700*+04	4.1368*+00	NM	0.92986	0.32867	0.63200	3.71100	0.11030	
3	6.2200*+04	4.3588*+00	NM	0.93245	0.33807	0.64500	3.64000	0.11720	
4	6.4800*+04	4.3984*+00	NM	0.93222	0.33982	0.64700	3.62500	0.11848	
5	6.7300*+04	4.5832*+00	NM	0.93368	0.34787	0.65700	3.56700	0.12419	
6	8.0000*+04	5.8411*+00	NM	0.94048	0.39021	0.71300	3.20600	0.22240	
7	9.2700*+04	6.8832*+00	NM	0.94512	0.43542	0.74900	2.95900	0.25313	
8	1.0540*+03	7.7811*+00	NM	0.94924	0.46507	0.77500	2.77700	0.27908	
9	1.1810*+03	9.9165*+00	NM	0.95050	0.52886	0.79400	2.25400	0.35226	
10	1.3080*+03	9.2425*+00	NM	0.95099	0.50960	0.80800	2.51400	0.32140	
11	1.4350*+03	9.7098*+00	NM	0.95141	0.52303	0.81700	2.44000	0.33484	
12	1.5620*+03	1.0209*+01	NM	0.95198	0.53700	0.82600	2.36600	0.34911	
13	1.6890*+03	1.0647*+01	NM	0.95364	0.54897	0.83400	2.30800	0.36135	
14	1.8160*+03	1.0936*+01	NM	0.95494	0.55674	0.83900	2.27100	0.36944	
15	2.0700*+03	1.1360*+01	NM	0.95652	0.56793	0.84600	2.21900	0.38125	
16	2.3240*+03	1.1832*+01	NM	0.95737	0.58012	0.85300	2.16200	0.39454	
17	2.5780*+03	1.2405*+01	NM	0.95737	0.59954	0.86300	2.07200	0.41651	
18	2.8320*+03	1.3323*+01	NM	0.95847	0.61706	0.87200	1.99700	0.43665	
19	3.0860*+03	1.4252*+01	NM	0.95894	0.63853	0.88200	1.90800	0.46226	
20	3.3400*+03	1.5081*+01	NM	0.96049	0.65793	0.89100	1.83400	0.48582	
21	3.5940*+03	1.5795*+01	NM	0.96172	0.67364	0.89800	1.77600	0.50563	
22	3.8480*+03	1.6607*+01	NM	0.96222	0.69146	0.90500	1.71300	0.52631	
23	4.1020*+03	1.7714*+01	NM	0.96348	0.71480	0.91400	1.63500	0.55902	
24	4.3560*+03	1.8352*+01	NM	0.96461	0.72790	0.91900	1.59400	0.57654	
25	4.9910*+03	2.0836*+01	NM	0.97245	0.77683	0.93800	1.45800	0.64335	
26	5.6260*+03	2.3384*+01	NM	0.98315	0.82402	0.95600	1.34600	0.71025	
27	6.2610*+03	2.5860*+01	NM	0.98846	0.86739	0.96900	1.24800	0.77644	
28	6.8960*+03	2.8281*+01	NM	0.99121	0.90781	0.97900	1.16300	0.84179	
29	8.1660*+03	3.2380*+01	NM	0.99915	0.97241	0.99500	1.04700	0.95033	
30	9.4360*+03	3.3816*+01	NM	0.99992	0.99404	0.99900	1.01000	0.98911	
D 31	1.0706*+02	3.4217*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

	M : 1.85, 2.10, 2.57 R THETA X 10 ⁻³ : 2 - 4 TW/TR : About 1	6001
		ZPG - AW
Continuous running tunnel with interchangeable fixed nozzles. W = H = 0.30 m 0.05 < P0 < 0.1 MN/m ² . T0 : 313 K. Air. 3 < RE/m X 10 ⁻⁶ < 6.		
MICHEL R., 1960. Résultats sur la couche limite turbulente aux grandes vitesses. X ^{me} Congrès de Mécanique Appliquée Stresa 1960. Publication ONERA no 102. And Michel R., private communications.		

- 1 The tests were made on the outer surface of a circular cylinder (diameter 39.25 mm) aligned with the axis of the 300 mm square tunnel test section. The cylinder had an ogival nose which was continued upstream as a long thin rod, on which transition took place. The seven test stations were between X = 150 and 350 mm from the point of the ogival nose (X = 0). The free stream Mach number did not vary more than 1 % in this region.
- 2
- 3
- 6 Static pressure was measured at intervals along the model surface, as was the wall temperature. The static tappings (d = 0.3 mm) were drilled at 10 mm intervals. Pitot profiles were obtained with an FPP (h₁ = 0.12 h₂ = 0.07, b₁ = 6 mm) at X values of 150, 183, 216, 249, 282, 315 and 348 mm.
- 9 The data were reduced using a linear Crocco temperature relationship with a recovery factor of 0.88, determined from the equilibrium temperature of the model. The static pressure was assumed constant through the boundary layer.
- 12 The editors' have replaced the author's temperature-velocity correlation by the normal Crocco - Van Driest relationship, assuming a recovery factor of 0.896 and using the author's TW value. We thus presume that there is slight heat transfer. We present all the data in our possession, consisting of three sequences of profiles each for a different Mach number. The author also reports measurements at M = 2.97 and a further set at M = 2.57 with moderate heat transfer.
- 13
- 5 DATA: 6001 0101 - 0306. Pitot profiles. NX = 6 or 7.

15 Editors' comments

The entry describes an early experiment in an axisymmetric configuration for which δ/RZ is up to 40 % so that transverse curvature effects may well be considerable. Upstream history effects should be weak, if not negligible. Comparisons should be made with other low Reynolds number tests made on flat plates. (Coles - CAT 5301, Shutts et al. - CAT 5501).

Despite the small physical scale of the experiment, measurements extend within the momentum deficit peak. The computed total pressure gradient in the outer part of the layer is large enough to suggest that measurements should have continued to rather greater values of y .

CAT 6001

MICHEL

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ *	MD * P00* T00*	TW/YR P1/PD* SH *	RED2W RED2D DZ	CF CQ PI2*	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR
60010101 1.5000*-01 1.9625*-02	1.8500 5.3900*+04 3.1500*+02	0.9930 1.0000 0.0000	1.4495*+03 2.1269*+03 3.2671*-04	NM NM 0.0000*+00	2.7262 1.7932 0.0836	1.3817 1.7787 3.9254*-04	8.6884*+03 2.9957*+02 5.0723*+02	8.6884*+03 1.8700*+02 3.0169*+02
60010102 1.8300*-01 1.9625*-02	1.8500 5.4600*+04 3.1800*+02	0.9930 1.0000 0.0000	1.6391*+03 2.4032*+03 3.6913*-04	NM NM 0.0000*+00	2.7425 1.7827 0.0833	1.3944 1.7669 4.4640*-04	8.8012*+03 3.0243*+02 5.0964*+02	8.8012*+03 1.8878*+02 3.0456*+02
60010103 1.9900*-01 1.9625*-02	1.8500 5.4300*+04 3.1500*+02	0.9930 1.0000 0.0000	1.7799*+03 2.8116*+03 3.9821*-04	NM NM 0.0000*+00	2.7283 1.7829 0.0834	1.3851 1.7674 4.8116*-04	8.7529*+03 2.9957*+02 5.0723*+02	8.7529*+03 1.8700*+02 3.0169*+02
60010104 2.1600*-01 1.9625*-02	1.8500 5.6400*+04 3.1800*+02	0.9930 1.0000 0.0000	1.9170*+03 2.8105*+03 4.1793*-04	NM NM 0.0000*+00	2.7221 1.7825 0.0835	1.3816 1.7669 5.0482*-04	9.0914*+03 3.0243*+02 5.0964*+02	9.0914*+03 1.8878*+02 3.0456*+02
60010105 2.4900*-01 1.9625*-02	1.8500 5.4800*+04 3.1500*+02	0.9930 1.0000 0.0000	2.1685*+03 3.1789*+03 4.8028*-04	NM NM 0.0000*+00	2.6995 1.7823 0.0837	1.3684 1.7666 5.7909*-04	8.8335*+03 2.9957*+02 5.0723*+02	8.8335*+03 1.8700*+02 3.0169*+02
60010106 2.8100*-01 1.9625*-02	1.8500 5.4800*+04 3.1500*+02	0.9930 1.0000 0.0000	2.3434*+03 3.4384*+03 5.1951*-04	NM NM 0.0000*+00	2.6866 1.7825 0.0838	1.3613 1.7666 6.2547*-04	8.8335*+03 2.9957*+02 5.0723*+02	8.8335*+03 1.8700*+02 3.0169*+02
60010201 1.5000*-01 1.9625*-02	2.1000 5.5400*+04 3.1300*+02	0.9908 1.0000 0.0000	1.2009*+03 2.0561*+03 3.3992*-04	NM NM 0.0000*+00	3.0920 1.8025 0.0980	1.3808 1.7826 4.2323*-04	6.0582*+03 2.9999*+02 5.4299*+02	6.0582*+03 1.8631*+02 2.9774*+02
60010202 1.8300*-01 1.9625*-02	2.1000 5.5000*+04 3.1500*+02	0.9909 1.0000 0.0000	1.4559*+03 2.3358*+03 3.8677*-04	NM NM 0.0000*+00	3.0725 1.8000 0.0979	1.3683 1.7809 4.8211*-04	6.1019*+03 2.9693*+02 5.4472*+02	6.1019*+03 1.8631*+02 2.9965*+02
60010203 2.1700*-01 1.9625*-02	2.1000 5.6100*+04 3.1600*+02	0.9913 1.0000 0.0000	1.6371*+03 2.6264*+03 4.3445*-04	NM NM 0.0000*+00	3.0651 1.7950 0.0975	1.3637 1.7760 5.4347*-04	6.1347*+03 2.9798*+02 5.4559*+02	6.1347*+03 1.8791*+02 3.0060*+02
60010204 2.4000*-01 1.9625*-02	2.1000 5.7400*+04 3.1500*+02	0.9909 1.0000 0.0000	1.8677*+03 2.9764*+03 4.8232*-04	NM NM 0.0000*+00	3.0502 1.7928 0.0979	1.3565 1.7739 6.0357*-04	6.2769*+03 2.9693*+02 5.4472*+02	6.2769*+03 1.8738*+02 2.9965*+02
60010205 2.8200*-01 1.9625*-02	2.1000 5.7400*+04 3.1600*+02	0.9913 1.0000 0.0000	1.9934*+03 3.1980*+03 5.1703*-04	NM NM 0.0000*+00	3.0477 1.7895 0.0975	1.3558 1.7704 6.4839*-04	6.2769*+03 2.9798*+02 5.4559*+02	6.2769*+03 1.8791*+02 3.0060*+02
60010206 3.1500*-01 1.9625*-02	2.1000 5.6000*+04 3.1500*+02	0.9909 1.0000 0.0000	2.1142*+03 3.3918*+03 5.5370*-04	NM NM 0.0000*+00	3.0452 1.7863 0.0979	1.3569 1.7668 6.9545*-04	6.1894*+03 2.9693*+02 5.4472*+02	6.1894*+03 1.8738*+02 2.9965*+02
60010207 3.4800*-01 1.9625*-02	2.1000 5.7300*+04 3.1500*+02	0.9909 1.0000 0.0000	2.2844*+03 3.6650*+03 5.9098*-04	NM NM 0.0000*+00	3.0415 1.7840 0.0979	1.3572 1.7641 7.4273*-04	6.2659*+03 2.9693*+02 5.4472*+02	6.2659*+03 1.8738*+02 2.9965*+02
60010301 1.5000*-01 1.9625*-02	2.5700 8.7700*+04 3.1700*+02	0.9903 1.0000 0.0000	1.1190*+03 2.1448*+03 2.8960*-04	NM NM 0.0000*+00	4.0322 1.8052 0.1174	1.4545 1.7753 3.9415*-04	4.6042*+03 2.9533*+02 6.0219*+02	4.6042*+03 1.3658*+02 2.9824*+02
60010302 1.8300*-01 1.9625*-02	2.5700 8.8400*+04 3.1500*+02	0.9904 1.0000 0.0000	1.3070*+03 2.5075*+03 3.3290*-04	NM NM 0.0000*+00	3.9941 1.8032 0.1173	1.4316 1.7742 4.5377*-04	4.6409*+03 2.9351*+02 6.0029*+02	4.6409*+03 1.3572*+02 2.9635*+02
60010303 2.1600*-01 1.9625*-02	2.5700 8.9100*+04 3.1500*+02	0.9904 1.0000 0.0000	1.5187*+03 2.9139*+03 3.8381*-04	NM NM 0.0000*+00	3.9778 1.7986 0.1173	1.4252 1.7699 5.2518*-04	4.6777*+03 2.9351*+02 6.0229*+02	4.6777*+03 1.3572*+02 2.9635*+02
60010304 2.4900*-01 1.9625*-02	2.5700 9.0300*+04 3.1600*+02	0.9901 1.0000 0.0000	1.7375*+03 3.3313*+03 4.3491*-04	NM NM 0.0000*+00	3.9509 1.7964 0.1177	1.4131 1.7684 5.9571*-04	4.7406*+03 2.9436*+02 6.0124*+02	4.7406*+03 1.3615*+02 2.9730*+02
60010305 3.1500*-01 1.9625*-02	2.5700 9.0000*+04 3.1600*+02	0.9901 1.0000 0.0000	2.0714*+03 3.9716*+03 5.2023*-04	NM NM 0.0000*+00	3.9029 1.7979 0.1182	1.3970 1.7690 7.0754*-04	4.7249*+03 2.9436*+02 6.0124*+02	4.7249*+03 1.3615*+02 2.9730*+02
60010306 3.4800*-01 1.9625*-02	2.5700 9.0400*+04 3.1600*+02	0.9901 1.0000 0.0000	2.1542*+03 4.1303*+03 5.3862*-04	NM NM 0.0000*+00	3.9108 1.7928 0.1179	1.4008 1.7645 7.3740*-04	4.7459*+03 2.9436*+02 6.0124*+02	4.7459*+03 1.3615*+02 2.9730*+02

60010101		MICHEL		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95100	0.00000	0.00000	1.60197	0.00000	
2	9.9900*-05	1.5177*+00	NM	0.96577	0.43007	0.51680	1.44402	0.35789	
3	1.9980*-04	1.7748*+00	NM	0.97031	0.51010	0.60083	1.38736	0.43307	
4	4.0005*-04	2.1639*+00	NM	0.97602	0.60515	0.69383	1.31459	0.52780	
5	5.9850*-04	2.4701*+00	NM	0.97942	0.66015	0.74417	1.27076	0.58561	
6	8.0100*-04	2.7281*+00	NM	0.98222	0.70514	0.78344	1.23441	0.63467	
7	9.9900*-04	2.9747*+00	NM	0.98471	0.74514	0.81692	1.20194	0.67966	
8	1.2510*-03	3.2032*+00	NM	0.98668	0.78013	0.84511	1.17352	0.72015	
9	1.4985*-03	3.4435*+00	NM	0.98903	0.81512	0.87229	1.14520	0.76169	
10	1.7505*-03	3.6886*+00	NM	0.99087	0.84510	0.89480	1.12106	0.79817	
11	1.9980*-03	3.8443*+00	NM	0.99238	0.87009	0.91301	1.10108	0.82919	
12	2.2500*-03	4.0748*+00	NM	0.99418	0.90008	0.93421	1.07729	0.86718	
13	2.5020*-03	4.2330*+00	NM	0.99537	0.92006	0.94797	1.06158	0.89298	
14	2.7495*-03	4.3949*+00	NM	0.99654	0.94005	0.96142	1.04598	0.91916	
15	3.0015*-03	4.5187*+00	NM	0.99742	0.95504	0.97131	1.03436	0.93904	
16	3.5010*-03	4.6954*+00	NM	0.99863	0.97602	0.98488	1.01824	0.96724	
17	4.0005*-03	4.8155*+00	NM	0.99943	0.99001	0.99375	1.00757	0.98628	
D 18	4.5000*-03	4.9023*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

60010106		MICHEL		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95100	0.00000	0.00000	1.60197	0.00000	
2	9.9930*-05	1.3795*+00	NM	0.96287	0.37505	0.45619	1.47951	0.30834	
3	1.9966*-04	1.5753*+00	NM	0.96687	0.45003	0.53628	1.43037	0.37632	
4	3.9999*-04	1.9231*+00	NM	0.97250	0.54711	0.63794	1.35961	0.46921	
5	5.9965*-04	2.1599*+00	NM	0.97572	0.60015	0.68913	1.31852	0.52265	
6	7.9730*-04	2.3622*+00	NM	0.97818	0.64015	0.72616	1.28680	0.56432	
7	9.9830*-04	2.5368*+00	NM	0.98017	0.67215	0.75441	1.26110	0.59853	
8	1.2529*-03	2.7103*+00	NM	0.98203	0.70214	0.78088	1.23685	0.63135	
9	1.5008*-03	2.8804*+00	NM	0.98373	0.73014	0.80452	1.21413	0.66263	
10	1.7487*-03	3.0582*+00	NM	0.98552	0.75613	0.82751	1.19138	0.69458	
11	2.0033*-03	3.2166*+00	NM	0.98700	0.78213	0.84669	1.17190	0.72249	
12	2.2512*-03	3.3687*+00	NM	0.98836	0.80412	0.86385	1.15409	0.74852	
13	2.4991*-03	3.5099*+00	NM	0.98953	0.82311	0.87836	1.13875	0.77134	
14	2.7470*-03	3.6294*+00	NM	0.99062	0.84111	0.89184	1.12427	0.79326	
15	3.0016*-03	3.7917*+00	NM	0.99196	0.86310	0.90796	1.10666	0.82045	
16	3.4974*-03	4.0591*+00	NM	0.99406	0.89808	0.93282	1.07687	0.86463	
17	3.9979*-03	4.3135*+00	NM	0.99596	0.93006	0.95473	1.05376	0.90602	
18	4.5024*-03	4.5104*+00	NM	0.99736	0.95404	0.97065	1.03514	0.93771	
19	4.9982*-03	4.6445*+00	NM	0.99828	0.97003	0.98103	1.02283	0.95914	
20	5.5007*-03	4.7467*+00	NM	0.99897	0.98202	0.98870	1.01366	0.97538	
21	6.0032*-03	4.8155*+00	NM	0.99943	0.99001	0.99375	1.00757	0.98628	
D 22	6.7000*-03	4.9023*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

60010201		MICHEL		PROFILE TABULATION		20 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94247	0.00000	0.00000	1.77373	0.00000	
2	9.9900*-05	1.4322*+00	NM	0.95609	0.35007	0.44609	1.62385	0.27471	
3	1.9980*-04	1.9594*+00	NM	0.96530	0.49015	0.60012	1.49905	0.40033	
4	4.0014*-04	2.5243*+00	NM	0.97237	0.59017	0.68828	1.39995	0.49879	
5	5.9940*-04	2.8871*+00	NM	0.97624	0.64417	0.74708	1.34502	0.55544	
6	7.9920*-04	3.1949*+00	NM	0.97924	0.68617	0.78500	1.30217	0.60131	
7	9.9900*-04	3.4842*+00	NM	0.98185	0.72316	0.81322	1.26456	0.64308	
8	1.2474*-03	3.7991*+00	NM	0.98444	0.76015	0.84211	1.22724	0.68618	
9	1.5012*-03	4.1034*+00	NM	0.98691	0.79614	0.86898	1.19135	0.72941	
10	1.7496*-03	4.3762*+00	NM	0.98895	0.82613	0.89047	1.16183	0.76644	
11	1.9980*-03	4.6500*+00	NM	0.99088	0.85511	0.91048	1.13368	0.80312	
12	2.2518*-03	4.8445*+00	NM	0.99219	0.87510	0.92385	1.11452	0.82893	
13	2.5002*-03	5.0338*+00	NM	0.99355	0.89609	0.93753	1.09462	0.85648	
14	2.7456*-03	5.2475*+00	NM	0.99477	0.91508	0.94958	1.07684	0.88182	
15	3.0024*-03	5.4139*+00	NM	0.99578	0.93106	0.95951	1.06203	0.90346	
16	3.4992*-03	5.6907*+00	NM	0.99739	0.95704	0.97520	1.03830	0.93922	
17	4.0014*-03	5.9978*+00	NM	0.99856	0.97602	0.98633	1.02123	0.96582	
18	4.4982*-03	6.0196*+00	NM	0.99922	0.98701	0.99265	1.01185	0.98141	
19	5.0004*-03	6.1091*+00	NM	0.99970	0.99501	0.99719	1.00439	0.99283	
D 20	5.4000*-03	6.1654*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

60010206		MICHEL		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.94262	0.00000	0.00000	1.77401	0.00000	
2	1.0010-04	1.3390+00	NM	0.95405	0.31405	0.40363	1.65183	0.24435	
3	2.0020-04	1.6408+00	NM	0.96029	0.41509	0.51992	1.56884	0.33140	
4	3.9970-04	2.1953+00	NM	0.96851	0.53516	0.64556	1.45516	0.44364	
5	5.9990-04	2.4864+00	NM	0.97199	0.58417	0.69270	1.40608	0.49264	
6	7.9800-04	2.7010+00	NM	0.97435	0.61717	0.72306	1.37260	0.52678	
7	1.0010-03	2.8730+00	NM	0.97614	0.64217	0.74534	1.34711	0.55328	
8	1.2530-03	3.0849+00	NM	0.97827	0.67217	0.77124	1.31649	0.58583	
9	1.4980-03	3.3024+00	NM	0.98026	0.70017	0.79461	1.28796	0.61695	
10	1.7500-03	3.4923+00	NM	0.98195	0.72416	0.81403	1.26358	0.64422	
11	2.0020-03	3.6724+00	NM	0.98349	0.74616	0.83134	1.24135	0.66970	
12	2.2470-03	3.8412+00	NM	0.98488	0.76615	0.84668	1.22126	0.69328	
13	2.4990-03	4.0236+00	NM	0.98632	0.78715	0.86238	1.20030	0.71847	
14	2.7510-03	4.2113+00	NM	0.98775	0.80814	0.87768	1.17952	0.74410	
15	3.0030-03	4.3855+00	NM	0.98903	0.82713	0.89118	1.16087	0.76773	
16	3.5000-03	4.6982+00	NM	0.99122	0.86011	0.91386	1.12448	0.80952	
17	3.9970-03	5.0035+00	NM	0.99324	0.89109	0.93431	1.09935	0.84987	
18	4.5010-03	5.2889+00	NM	0.99503	0.91907	0.95209	1.07313	0.88720	
19	4.9980-03	5.5407+00	NM	0.99653	0.94305	0.96682	1.05104	0.91987	
20	5.5020-03	5.7774+00	NM	0.99789	0.96503	0.97992	1.03109	0.95037	
21	5.9990-03	5.9641+00	NM	0.99892	0.98202	0.98979	1.01589	0.97431	
22	6.5030-03	6.0979+00	NM	0.99964	0.99401	0.99662	1.00527	0.99140	
D 23	7.0000-03	6.1654+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

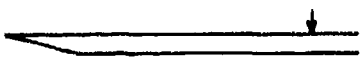
INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

60010301		MICHEL		PROFILE TABULATION		17 POINTS, DELTA AT POINT 17			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.93164	0.00000	0.00000	2.16231	0.00000	
2	1.0185-04	1.2423+00	NM	0.94041	0.22003	0.31515	2.05148	0.15362	
3	1.9885-04	2.1272+00	NM	0.95619	0.42716	0.57123	1.78826	0.31943	
4	3.9770-04	3.1905+00	NM	0.96760	0.56020	0.70506	1.58762	0.44460	
5	6.0140-04	3.3117+00	NM	0.97293	0.62321	0.76135	1.49244	0.51014	
6	8.0025-04	4.2654+00	NM	0.97637	0.66521	0.79553	1.41019	0.55624	
7	9.9910-04	4.7028+00	NM	0.97945	0.70320	0.82460	1.37506	0.59968	
8	1.2413-03	5.1655+00	NM	0.98242	0.74120	0.85199	1.32110	0.64481	
9	1.4986-03	5.6007+00	NM	0.98500	0.77518	0.87513	1.27448	0.68665	
10	1.7508-03	6.0150+00	NM	0.98728	0.80617	0.89516	1.23295	0.72603	
11	1.9982-03	6.3893+00	NM	0.98921	0.83315	0.91180	1.19770	0.76129	
12	2.4977-03	7.1156+00	NM	0.99265	0.88312	0.94076	1.13481	0.82901	
13	2.9973-03	7.7901+00	NM	0.99553	0.92708	0.96437	1.08207	0.89123	
14	3.4968-03	8.3177+00	NM	0.99760	0.96003	0.98100	1.04414	0.93954	
15	4.0012-03	8.6963+00	NM	0.99897	0.98362	0.99203	1.01851	0.97405	
16	4.4957-03	8.8806+00	NM	0.99965	0.99401	0.99723	1.00649	0.99800	
D 17	4.8500-03	8.9820+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

60010306		MICHEL		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.93153	0.00000	0.00000	2.16206	0.00000	
2	9.6200-05	1.1235+00	NM	0.93687	0.16001	0.23206	2.10332	0.11033	
3	1.9980-04	1.5158+00	NM	0.94657	0.30908	0.43170	1.95078	0.22129	
4	3.9960-04	2.3631+00	NM	0.96128	0.48719	0.63494	1.69356	0.37381	
5	5.9940-04	3.0264+00	NM	0.96603	0.54220	0.68903	1.61496	0.42666	
6	7.9920-04	3.3414+00	NM	0.96894	0.57621	0.72043	1.56326	0.46085	
7	9.9900-04	3.6160+00	NM	0.97131	0.60421	0.74515	1.52093	0.48993	
8	1.2506-03	3.9381+00	NM	0.97390	0.63521	0.77133	1.47449	0.52311	
9	1.5022-03	4.2097+00	NM	0.97596	0.66021	0.79156	1.43750	0.55065	
10	1.7464-03	4.4579+00	NM	0.97775	0.68221	0.80874	1.40534	0.57547	
11	1.9980-03	4.6910+00	NM	0.97935	0.70220	0.82385	1.37647	0.59852	
12	2.5012-03	5.1655+00	NM	0.98240	0.74120	0.85198	1.32127	0.64482	
13	2.9970-03	5.6928+00	NM	0.98550	0.78218	0.87973	1.26489	0.69545	
14	3.5002-03	6.2075+00	NM	0.98827	0.82016	0.90387	1.21455	0.74420	
15	3.9960-03	6.7036+00	NM	0.99074	0.85514	0.92483	1.16963	0.79070	
16	4.4992-03	7.1155+00	NM	0.99265	0.88312	0.94076	1.13480	0.82901	
17	4.9950-03	7.5873+00	NM	0.99469	0.91409	0.95757	1.09739	0.87259	
18	5.4982-03	7.9957+00	NM	0.99635	0.94007	0.97103	1.06696	0.91009	
19	6.0014-03	8.3502+00	NM	0.99772	0.96204	0.98198	1.04188	0.94251	
20	6.4972-03	8.6464+00	NM	0.99881	0.98002	0.99066	1.02181	0.96951	
21	7.0004-03	8.8806+00	NM	0.99965	0.99401	0.99723	1.00649	0.99800	
D 22	7.4000-03	8.9820+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/L,U/UD,T/TD ASSUME P=PD AND VAN DRIEST

	M : 5 R THETA X 10 ⁻³ : 3 - 7 TW/TR : 0.55, 0.65, 1.0	6201
		ZPG AW/SHT
Blow-down tunnel with fixed nozzle block. Running time 45-90 secs. W = 0.15, H = 0.18, L = 0.5 m. PD : 1.7 MN/m ² . 330 < T0 < 660 K. Air. 15 < RE/m X 10 ⁻⁶ < 45.		
MOORE D.R., 1962. Velocity similarity in the compressible turbulent boundary layer with heat transfer. DRL 480.		

- 1 The test boundary layer was formed on a flat plate model mounted with the test surface facing downwards near the centre line of the tunnel. Two models were used, and "there was essentially no difference between the constant temperature characteristics of the two plates". The second and principal model, which is described, was fabricated from pure copper with a stainless steel leading edge (X = 0) chamfered at 15° on the upper side (L = 0.425, W = 0.162 m). The plate was actively cooled by two separate circuits which
- 3 were manually controlled to maintain a constant wall temperature. Near the leading edge a 12.7 mm strip of No 80 grit cloth was bonded to the surface to act as a transition trip.
- 6 The plate temperature was monitored by seven thermocouples mounted at roughly 40 mm intervals back from X = about 80 mm. The first two were on the centre line and the remainder about 20 mm to one side. Static
- 7 tappings were placed at X = 135, 240, 310 mm about 25 mm to the same side as the 5 thermocouples. Pitot traverses were made with a double CPP. The two tubes (d₁ = 0.914 mm) were separated by 3.81 mm in the Y-direction and after (E) about 20 mm they were successively sleeved into larger diameter tubing. The
- 8 traverse gear was driven from the floor of the tunnel to give a profile normal at X = 254 mm.
- 9 The author has reduced the data assuming that static pressure is constant at the wall value through the layer and that the temperature and velocity are related by T/TW = 1 - (1 - TD/TW) (U/UD)² (the Crocco
- 10 temperature velocity relation). No probe corrections were applied.
- 12 The editors have presented the four complete profiles tabulated by the author. We have used the Crocco / Van Driest temperature-velocity correlation with recovery factor 0.896 in place of that used by the author. We found it necessary to replace our usual integration procedure with a trapezoidal integration rule. There are in addition some measurements made with the outer Pitot tube removed which do not, however, extend as far as the boundary layer edge. The authors' final measured point has been set as the D-state.
- 5 DATA: 6201 0101-0401. PT2 profiles.
- 15 Editors' comments
This entry is presented primarily as a comparison for the rough surface experiment of Young - CAT 6506. The tunnel is the same, and the model formed the basis for that used by Young. The paper is mainly concerned with fitting SHT data to the law of the wall and includes a description of some attempts to use special forms of Preston tube. An analysis of the results is to be found in Rochelle (1963).
The profile data is sparse, rough, and in two cases (0101, 0201) displays large gaps.

CAT 6201 MOORE BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD* TOD*	TW/TR PW/PD* SH *	RED2W RED2D DZ	CF CQ PI2*	H12 H32 H42	H12K H32K D2K	PW TH* UD	PD TD TR
62010101	4.9180	0.9859	3.0234"+00	NM	11.9516	1.8171	7.3987"+00	7.3987"+00
2.5400"-01	3.5556"+03	1.0000	1.3661"+01	NM	1.8438	1.8319	3.0337"+02	5.7684"+01
INFINITE	3.3672"+02	0.0000	1.6882"-04	0.0000"+00	0.1718	3.7489"-04	7.4890"+02	3.0770"+02
62010201	4.7790	0.9917	3.2714"+00	NM	11.3113	1.8298	6.7097"+00	8.7097"+00
2.5400"-01	3.5472"+03	1.0000	1.4193"+01	NM	1.8606	1.8505	3.0322"+02	6.0038"+01
INFINITE	3.3428"+02	0.0000	1.6285"-04	0.0000"+00	0.1663	3.3271"-04	7.4244"+02	3.0576"+02
62010301	4.8900	0.6467	3.1336"+00	NM	9.3618	1.7503	7.6687"+00	7.6687"+00
2.5400"-01	3.5654"+03	1.0000	9.0736"+00	NM	1.8458	1.8233	3.2757"+02	9.5836"+01
INFINITE	5.5417"+02	0.0000	2.3202"-04	0.0000"+00	0.4817	4.4003"-04	9.5981"+02	5.0650"+02
62010401	4.7900	0.5473	3.1890"+00	NM	8.4349	1.7583	8.5014"+00	8.5014"+00
2.5400"-01	3.5084"+03	1.0000	7.6431"+00	NM	1.8409	1.8241	3.2446"+02	1.1598"+02
INFINITE	6.4817"+02	0.0000	2.3748"-04	0.0000"+00	0.5712	4.2948"-04	1.0343"+03	5.9282"+02

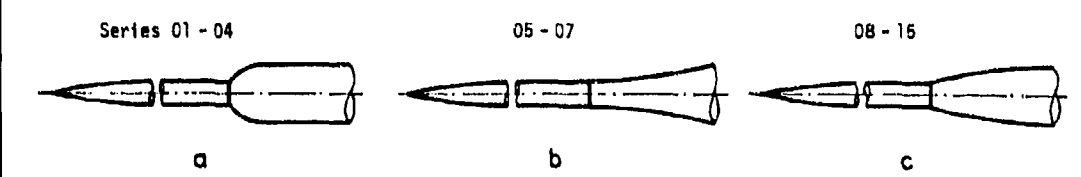
TRAPEZOIDAL RULE FOR ALL INTEGRATIONS

62010301 MOORE		PROFILE TABULATION			21 POINTS, DELTA AT POINT 21				
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	NM	0.59110	0.00000	0.00000	3.41798	0.00000	
2	4.5720"-04	5.5386"+00	NM	0.84631	0.40491	0.67061	2.74300	0.24448	
3	4.8260"-04	5.7433"+00	NM	0.85030	0.41309	0.67970	2.70737	0.25103	
4	5.3340"-04	6.1654"+00	NM	0.85807	0.42945	0.69729	2.63640	0.26449	
5	7.8740"-04	8.3982"+00	NM	0.89118	0.50716	0.77092	2.31065	0.33364	
6	9.1440"-04	8.7200"+00	NM	0.89504	0.51738	0.77948	2.26978	0.34342	
7	1.1684"-03	1.0213"+01	NM	0.91108	0.56237	0.81433	2.09681	0.38837	
8	1.4224"-03	1.1080"+01	NM	0.91908	0.58691	0.83156	2.00746	0.41424	
9	1.6764"-03	1.2138"+01	NM	0.92780	0.61354	0.85022	1.90786	0.44564	
10	1.9304"-03	1.3410"+01	NM	0.93701	0.64826	0.86978	1.80020	0.48316	
11	2.1844"-03	1.4748"+01	NM	0.94548	0.68098	0.88764	1.69904	0.52244	
12	2.4384"-03	1.6062"+01	NM	0.95279	0.71166	0.90298	1.60997	0.56087	
13	2.6924"-03	1.7482"+01	NM	0.95978	0.74335	0.91754	1.52357	0.60223	
14	4.2672"-03	2.6771"+01	NM	0.99060	0.92434	0.98094	1.12622	0.87100	
15	4.7244"-03	2.7592"+01	NM	0.99251	0.93865	0.98482	1.10079	0.89465	
16	4.9784"-03	2.8786"+01	NM	0.99510	0.95910	0.99013	1.06575	0.92904	
17	5.2324"-03	3.0316"+01	NM	0.99822	0.98466	0.99641	1.02400	0.97305	
18	5.4864"-03	3.2876"+01	NM	0.99947	0.99387	0.99858	1.00951	0.98917	
19	5.7404"-03	3.1190"+01	NM	0.99988	0.99898	0.99976	1.00158	0.99819	
20	5.9944"-03	3.1329"+01	NM	1.00014	1.00123	1.00028	0.99811	1.00217	
D 21	6.5024"-03	3.1253"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

62010401 MOORE		PROFILE TABULATION			17 POINTS, DELTA AT POINT 17				
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	NM	0.50058	0.00000	0.00000	2.79765	0.00000	
2	4.5720"-04	6.0051"+00	NM	0.82130	0.43215	0.67943	2.47181	0.27487	
3	4.8260"-04	6.3280"+00	NM	0.82840	0.44468	0.69280	2.42731	0.28542	
4	5.0800"-04	6.6602"+00	NM	0.83531	0.45720	0.70575	2.38279	0.29619	
5	6.0960"-04	7.1762"+00	NM	0.84532	0.47599	0.72442	2.31622	0.31276	
6	6.8580"-04	8.2083"+00	NM	0.86309	0.51148	0.75728	2.19206	0.34547	
7	8.1280"-04	9.3829"+00	NM	0.88034	0.54906	0.78888	2.06432	0.38213	
8	1.0668"-03	1.1006"+01	NM	0.90021	0.59708	0.82489	1.90868	0.43218	
9	1.3208"-03	1.2061"+01	NM	0.91121	0.62630	0.84465	1.81878	0.46440	
10	1.5748"-03	1.3687"+01	NM	0.91714	0.64301	0.85526	1.74916	0.48343	
11	1.8288"-03	1.5374"+01	NM	0.92491	0.66597	0.86910	1.70306	0.51032	
12	4.2926"-03	2.5734"+01	NM	0.98788	0.92484	0.97922	1.12104	0.87349	
13	4.4958"-03	2.7121"+01	NM	0.99213	0.94990	0.98656	1.07868	0.91459	
14	4.6228"-03	2.7474"+01	NM	0.99319	0.95616	0.98833	1.06842	0.92504	
15	4.8768"-03	2.8425"+01	NM	0.99586	0.97286	0.99292	1.04166	0.95321	
16	5.1308"-03	2.9271"+01	NM	0.99812	0.98747	0.99679	1.01845	0.97825	
D 17	5.3848"-03	3.0007"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

<p>Three configurations tested</p> <p>See diagrams below</p>	<p>M : 1.6 - 4.5 (Free stream)</p> <p>R THETA X 10⁻³ : 8 - 45</p> <p>TW/TR : 1.0 and 0.7</p>	<p>6401</p> <p>FPG/APG/Recovery AW/MHT</p>
<p>Continuous tunnel W = H = 0.56 m. L = 1.0 m. 0.16 < P₀ < 0.5 MN/m². 300 < T₀ < 340 K. Air. 14 < RE/m X 10⁻⁶ < 30.</p>		
<p>CLUTTER D.C. and KAUPS K., 1964. Wind tunnel investigation of turbulent boundary layers on axially-symmetric bodies at supersonic speeds. Douglas Aircraft Company Rep. No. LB 31425. And Kaups K., private communication.</p>		
		

- 1 The tests were performed on the surface of a series of axisymmetric models mounted on the tunnel centre line. The boundary layer was formed on a nose piece, which finished as a parallel cylinder of 69.85 mm diameter. The length of the nose-piece used varied with Mach number as below:

Mach number:	1.61	2.50	3.30	4.50
Length of nose piece:	2.108	2.108	1.397	0.864 m

At low Mach numbers ($M < 2.50$) the nose extended upstream through the throat into the settling chamber. The coordinates of the nose fairing are given in table 1 together with those of the three centre bodies used. Each of these had an initial section 127 mm long, the same diameter as the nose piece, followed by a circular arc profile ($X = 0$ at the end of the parallel section) leading to a new parallel section of diameter 139.7 mm. For the blunt model (a) this started at $X = 60.5$ mm, while for the more gradual concave (b) and convex (c) models it started at $X = 304.8$ mm. The radii of curvature of the profiles were 69.85 mm for model (a) and 1.3475 m for the gradual models (b) and (c). Coordinates for the model surfaces are given in table 1. The centre bodies were made of electroformed nickel 2.54 mm thick, and the convex model (c) could be actively cooled with liquid nitrogen. The model surface was highly polished.

- 4 The boundary layer was formed, in each case, under essentially constant pressure conditions on the nose extension. The test zone extended, with one exception, downstream of the nose / centre body junction at $X = 0$. For model (a) all the profiles were measured on the parallel section downstream of the increase in diameter, where the layer was relaxing after traversing a strong shock-induced separation ahead of the junction, and reattaching to the shoulder of the centre-body. The region of study was limited by the downstream reflection of the centre-body bow shock. All the profiles from model (b) were measured on the concave section of the centre body in a region of, nominally, steadily increasing pressure. The sharp change in slope at $X = 0$ for model C caused a bow shock, which was not however strong enough to make the boundary layer separate. For one case ($M = 1.61$) profiles were measured on both sides of the shock. For all other cases measurements commenced at least 0.15 m downstream, and extended beyond the end of the curved portion to include a relaxation region on the parallel section of the body. In this region there is some evidence of a pressure rise after over-expansion. The nose piece was not cooled so that for the heat-transfer runs the wall temperature also changed abruptly near $X = 0$. The cooling system provided uniformly axisymmetric cooling, but could not maintain uniform cooling in the X direction. The wall temperature therefore varied in the X direction.
- 6 Static tappings ($D = 1.23$ mm) were provided at 25.4 mm intervals in the range $-0.102 < X < 0.559$ m and copper-constantan thermocouples were mounted at 50.8 mm intervals in the same range. An FEB was mounted at $X = 0.356$ m in the wall of the blunt model (a) but did not provide usable results. Heat transfer rates

- were determined for the convex model (c) by cutting off the liquid nitrogen cooling and observing the wall temperature as a function of time, using the thin wall transient technique.
- 7 Profiles were measured using a traversing rake mechanism carrying six FPP (flattened 1 mm tube - $h_1 = 0.20$, $h_2 = 0.05$, $b_1 = 0.46$, $b_2 = 0.30$, $l = 12.7$ mm) and six ECP ($\alpha = 5^\circ$, $d_1 = d_2 = 1.6$, $l = 12.7$ mm) of the type designed by Danberg (1961). The lengths given are to the first part of the bracing structure. The rakes continued as a slender bundle of tubes to a distance 114 mm back from their tips, where they were connected to a miniature traverse gear so constructed as to present a mean width to the flow of about 20 mm (E). The whole could be mounted on wedges and strapped to the model so that the probe tips moved normal to the local model surface. A pitot-tube, or a further TTP, could be attached to the top of the traverse gear to monitor the free stream state. A CCP (dimensions not given) could be mounted on the side of the rake, but could not be used simultaneously as it caused disturbances affecting the TPP and TTP. A separate rake carrying six CCP was therefore used for static pressure traverses, on separate occasions.
 - 8 The profile normal always intersected the body surface at X-values for which there were both static holes and thermocouples. The normal for the TPP was on the centre line, with the TTP about 8 mm (E) to one side. The static probe, when mounted, was about 12 mm (E) off to the other side. The six TPP and TTP were mounted at vertical intervals of 5.08 mm.
 - 9 Traverses were made so that the range covered by each probe in the rake overlapped that of its neighbour. Only very small differences were observed between readings from adjacent probes. Data for reduction were taken from a curve faired through the experimental points. The TTP did not approach the surface as closely as the TPP, being mounted to one side, and being larger in size. A fourth order polynomial was fitted to the wall temperature and the innermost few measured data points, to provide TO data in this inner region. The static pressures recorded did not, when extrapolated, match the wall pressures. This discrepancy was attributed to uncertainties of calibration. The normal pressure gradient recorded was however very close, in the outer part of the boundary layer, to that predicted by an inviscid characteristic solution for the flow. The pressure distribution used in the data reduction was therefore taken as the measured distribution shifted so as to match the wall pressure. The shift ranged up to 10 %. No probe shear or displacement corrections were applied and the Sutherland viscosity relation was used. The editors have presented all the profiles published by the authors. The D-state has been set arbitrarily at the outermost point presented. The profile series presented for each centre-body are distinguished by free stream Mach number. All are for a near adiabatic wall excepting series 12-15 for which there was substantial heat transfer. The original heat transfer data is presented graphically and is not reproduced here.
 - 5 DATA: 6401 0101-1503. PT2 and TO profiles simultaneously, P profiles separately. NX up to 7.

15 Editors' comments

This series of tests includes some very interesting flows. Series 01-04 describe the recovery of a boundary layer which has undergone separation ahead of and reattachment to the blunt centre-body, followed by a rapid simple-wave expansion before entering the test-zone. Series 08-15 describe a boundary layer which has passed through a shock, without separation, before undergoing a relatively gentle simple wave expansion in the test-zone. There are no comparable results. Series 05-07, undergoing a simple wave compression, should be compared with Sturek & Danberg - CAT 7101.

The profiles contain a large number of data points and, on the evidence of our calculated P_0 values, extend well out into the free stream. The entropy gradients resulting from the shock systems of series 01-04 and 08-15 are, on the same evidence, not very severe. The shifting of the static pressure profile so as to match the wall pressure could have been checked, with advantage, by a Pitot derived value in the free stream, at least for series 05-07. In the light of the analysis of Myring (1968) and Myring & Young (1968), it would seem that the necessary shift is perhaps greater than that actually used. Any influence on the reduced data is, however, not likely to be very great, a 10 % shift in P resulting in about a 5 % change in local Mach number and changes of order 10 % in the Reynolds numbers.

The profile measurements do not extend within the momentum deficit peak in about half the cases, so that integral values should be treated with reserve. There is considerable scatter in the edge states within a

given series (e.g. series 11) and some unexplained relatively large inconsistencies - as the edge Mach number variation for series O 7, where it seems probable that there is a gross error for either O701 or O702. The author comments that in some cases it may not have been possible to arrange for the probes to be made parallel to the body surface, and that some unusual interference effects could result.

Values of δ/RZ can be as great as 40 %. The effects of transverse curvature, therefore, may well be significant.

Table 1
COORDINATES OF MODEL SURFACE

NOSEPIECE X = 0 at nose		MODEL A X = 0 at "Station O"		MODEL B X = 0 at "Station O"		MODEL C X = 0 at "Station O"	
X	Y	X	Y	X	Y	X	Y
0	0	0	34.93	0	34.93	0	34.93
25.40	4.83	25.40	60.38	25.40	35.17	25.40	40.56
		50.80	69.16				
50.80	9.32	60.49	69.85	50.80	35.89	50.80	45.69
76.20	13.41		constant	76.20	37.08	76.20	50.32
101.60	17.20			101.60	38.76	101.60	54.44
127.00	20.55			127.00	40.93	127.00	58.06
152.40	23.57			152.40	43.59	152.40	61.21
203.20	28.52			177.80	46.71	177.80	63.85
254.00	32.08			203.20	50.34	203.20	66.01
304.80	34.19			228.60	54.46	228.60	67.69
355.60	34.93			254.00	59.08	254.00	68.89
	constant			279.40	64.21	279.40	69.61
"Station O"	34.93			304.80	69.85	304.80	69.85
			constant		constant		constant
		558.80	69.85	558.80	69.85	558.80	69.85

Nominal dimensions in mm.

Actual model coordinates were "within a few 0.001 inch - 0.0254 mm - of these".

The three models have circular profile sections, for which the radii of curvature are A : 69.85 mm B & C : 1.3475 m

CAT 6401		CLUTTER		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUH	4D *	TW/TR	RED2W	CF	H12	H12K	PW	PD*		
X *	POD	PW/PD	RED2D	CO	H32	H32K	TW*	TD*		
RZ *	TOD	SW *	O2	P12	H42	O2K	UD	TR		
64010101	1.7380	0.9713	1.5637"+04	NM	2.2106	1.1769	3.3054"+04	3.3054"+04		
1.0160"-01	1.7281"+05	1.0000	2.1731"+04	NM	1.8790	1.8741	2.8626"+02	1.9122"+02		
6.9850"-02	3.0675"+02	1.0000	9.6268"-04	NM	0.1300	1.0566"-03	4.8187"+02	2.9473"+02		
64010102	1.6780	0.9771	1.8292"+04	NM	2.1375	1.1892	3.6271"+04	3.6271"+04		
1.5240"-01	1.7268"+05	1.0000	2.4995"+04	NM	1.8674	1.8621	2.8956"+02	1.9711"+02		
6.9850"-02	3.0785"+02	1.0000	1.0901"-03	NM	0.1321	1.1934"-03	4.7178"+02	2.9633"+02		
64010201	2.6310	0.9534	1.9178"+04	NM	3.4739	1.1697	1.4280"+04	1.4280"+04		
1.5240"-01	2.9894"+05	1.0000	3.6572"+04	NM	1.8710	1.8593	2.8255"+02	1.3228"+02		
6.9850"-02	3.1541"+02	1.0000	1.4863"-03	NM	0.2069	1.8208"-03	6.0670"+02	2.9636"+02		
64010202	2.6250	0.9540	1.8668"+04	NM	3.4902	1.1839	1.4395"+04	1.4395"+04		
2.0320"-01	2.9856"+05	1.0000	3.5579"+04	NM	1.8642	1.8521	2.8012"+02	1.3139"+02		
6.9850"-02	3.1246"+02	1.0000	1.4240"-03	NM	0.2006	1.7474"-03	6.0328"+02	2.9363"+02		
64010203	2.6340	0.9651	2.1396"+04	NM	3.5230	1.1923	1.6191"+04	1.6191"+04		
3.0480"-01	3.4052"+05	1.0000	4.1290"+04	NM	1.8574	1.8437	2.8349"+02	1.3094"+02		
6.9850"-02	3.1264"+02	1.0000	1.4572"-03	NM	0.2050	1.8242"-03	6.0432"+02	2.9375"+02		
64010204	2.6150	0.9549	2.1966"+04	NM	3.4953	1.2051	1.6674"+04	1.6674"+04		
3.5560"-01	3.4105"+05	1.0000	4.1728"+04	NM	1.8553	1.8394	2.8156"+02	1.3244"+02		
6.9850"-02	3.1372"+02	1.0000	1.4633"-03	NM	0.2078	1.8264"-03	6.0362"+02	2.9487"+02		
64010301	3.2770	0.9824	9.0838"+03	NM	4.7834	1.1937	6.2441"+03	6.2441"+03		
2.5400"-01	3.4551"+05	1.0000	2.2851"+04	NM	1.8711	1.8512	2.8012"+02	9.9500"+01		
6.9850"-02	3.1320"+02	1.0000	1.1313"-03	NM	0.2418	1.5452"-03	6.5539"+02	2.9098"+02		
64010302	3.3090	0.9902	1.0343"+04	NM	4.5948	1.1882	6.5297"+03	6.3829"+03		
3.0480"-01	3.7003"+05	1.0230	2.6496"+04	NM	1.8675	1.8490	2.8857"+02	9.8389"+01		
6.9850"-02	3.1365"+02	1.0000	1.2502"-03	NM	0.2414	1.6978"-03	6.5808"+02	2.9144"+02		
64010303	3.3110	0.9819	9.9382"+03	NM	4.6978	1.1884	6.1748"+03	6.0477"+03		
3.5560"-01	3.5162"+05	1.0210	2.5310"+04	NM	1.8659	1.8482	2.8641"+02	9.8389"+01		
6.9850"-02	3.1411"+02	1.0000	1.2596"-03	NM	0.2490	1.7128"-03	6.5843"+02	2.9168"+02		
64010304	3.2060	1.0043	1.0099"+04	NM	4.6320	1.1923	6.5127"+03	6.5127"+03		
4.0640"-01	3.2482"+05	1.0000	2.5112"+04	NM	1.8640	1.8450	2.9412"+02	1.0306"+02		
6.9850"-02	3.1491"+02	1.0000	1.2824"-03	NM	0.2357	1.7523"-03	6.5254"+02	2.9287"+02		
64010401	4.2430	0.9680	4.0313"+03	NM	7.5304	1.2127	1.3564"+03	1.4168"+03		
2.5400"-01	2.9591"+05	0.9574	1.4446"+04	NM	1.8610	1.8300	2.7728"+02	6.7778"+01		
6.9850"-02	3.1182"+02	1.0000	1.3773"-03	NM	0.3417	2.3078"-03	7.0037"+02	2.8644"+02		
64010402	4.3230	0.9745	4.3254"+03	NM	7.6528	1.2065	1.4382"+03	1.4785"+03		
3.0480"-01	3.4222"+05	0.9727	1.6024"+04	NM	1.8636	1.8320	2.7994"+02	6.6056"+01		
6.9850"-02	3.1295"+02	1.0000	1.3824"-03	NM	0.3105	2.3213"-03	7.0445"+02	2.8727"+02		
64010403	4.0720	0.9840	4.5567"+03	NM	7.3363	1.2174	1.6086"+03	1.6883"+03		
3.5560"-01	2.8204"+05	0.9528	1.5529"+04	NM	1.8569	1.8265	2.8311"+02	7.2444"+01		
6.9850"-02	3.1269"+02	1.0000	1.4305"-03	NM	0.3112	2.3782"-03	6.9490"+02	2.8770"+02		
64010404	4.4880	0.9880	5.0548"+03	NM	7.1534	1.2192	1.6477"+03	1.5753"+03		
4.0640"-01	4.4912"+05	1.0460	2.0033"+04	NM	1.8515	1.8190	2.8589"+02	6.2778"+01		
6.9850"-02	3.1567"+02	1.0000	1.4474"-03	NM	0.3110	2.4411"-03	7.1296"+02	2.8937"+02		

given series (e.g. series 11) and some unexplained relatively large inconsistencies - as the edge Mach number variation for series 07, where it seems probable that there is a gross error for either 0701 or 0702. The author comments that in some cases it may not have been possible to arrange for the probes to be made parallel to the body surface, and that some unusual interference effects could result.

Values of δ/RZ can be as great as 40%. The effects of transverse curvature, therefore, may well be significant.

Table 1
COORDINATES OF MODEL SURFACE

NOSEPIECE X = 0 at nose		MODEL A X = 0 at "Station 0"		MODEL B X = 0 at "Station 0"		MODEL C X = 0 at "Station 0"	
X	Y	X	Y	X	Y	X	Y
0	0	0	34.93	0	34.93	0	34.93
25.40	4.83	25.40	60.38	25.40	35.17	25.40	40.56
50.80	9.32	50.80	69.16	50.80	35.89	50.80	45.69
76.20	13.41	60.49	69.85	76.20	37.08	76.20	50.32
101.60	17.20		constant	101.60	38.76	101.60	54.44
127.00	20.55			127.00	40.93	127.00	58.06
152.40	23.57			152.40	43.59	152.40	61.21
203.20	28.52			177.80	46.71	177.80	63.85
254.00	32.08			203.20	50.34	203.20	66.01
304.80	34.19			228.60	54.46	228.60	67.69
355.60	34.93			254.00	59.08	254.00	68.89
constant				279.40	64.21	279.40	69.61
"Station 0" 34.93				304.80	69.85	304.80	69.85
			constant	constant		constant	
		558.80	69.85	558.80	69.85	558.80	69.85

Nominal dimensions in mm.

Actual model coordinates were "within a few 0.001 inch - 0.0254 mm - of these".

The three models have circular profile sections, for which the radii of curvature are A : 69.85 mm B & C : 1.3475 m

CAT 6401		CLUTTER		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUW	MO *	TW/TR	RED2W	CF	H12	H12K	PW	PD+	
X *	POD	PH/PO	RED2D	CQ	H32	H32K	TW+	TD+	
RZ *	TOD	SH *	D2	P12	H42	D2K	UD	TR	
64010501	1.6010	0.9820	2.8986 ⁺⁰⁴	NM	2.1212	1.2327	4.2793 ⁺⁰⁴	4.2793 ⁺⁰⁴	
NM	1.8216 ⁺⁰⁵	1.0000	3.8795 ⁺⁰⁴	NM	1.8099	1.8010	2.8851 ⁺⁰²	2.0133 ⁺⁰²	
3.4925 ⁻⁰²	3.0454 ⁺⁰²	1.0000	1.5447 ⁻⁰³	NM	0.1078	1.7258 ⁻⁰³	4.5547 ⁺⁰²	2.9381 ⁺⁰²	
64010502	1.5890	0.9797	3.3262 ⁺⁰⁴	NM	1.8547	1.2533	4.6273 ⁺⁰⁴	4.4408 ⁺⁰⁴	
5.0800 ⁻⁰²	1.8570 ⁺⁰⁵	1.0420	4.4260 ⁺⁰⁴	NM	1.7929	1.7851	2.8824 ⁺⁰²	2.0256 ⁺⁰²	
3.5888 ⁻⁰²	3.0484 ⁺⁰²	1.0000	1.7250 ⁻⁰³	NM	0.1119	1.8834 ⁻⁰³	4.5343 ⁺⁰²	2.9421 ⁺⁰²	
64010503	1.4920	0.9829	2.9919 ⁺⁰⁴	NM	1.7970	1.2574	5.2967 ⁺⁰⁴	5.1028 ⁺⁰⁴	
1.5240 ⁻⁰¹	1.8517 ⁺⁰⁵	1.0380	3.8672 ⁺⁰⁴	NM	1.8013	1.7954	2.8951 ⁺⁰²	2.1056 ⁺⁰²	
4.3586 ⁻⁰²	3.0430 ⁺⁰²	1.0000	1.4713 ⁻⁰³	NM	0.1014	1.5922 ⁻⁰³	4.3407 ⁺⁰²	2.9455 ⁺⁰²	
64010504	1.4780	0.9860	2.5432 ⁺⁰⁴	NM	1.9280	1.2453	5.4377 ⁺⁰⁴	5.1640 ⁺⁰⁴	
2.0320 ⁻⁰¹	1.8364 ⁺⁰⁵	1.0530	3.2807 ⁺⁰⁴	NM	1.8163	1.8108	2.9041 ⁺⁰²	2.1167 ⁺⁰²	
5.0338 ⁻⁰²	3.0414 ⁺⁰²	1.0000	1.2539 ⁻⁰³	NM	0.0907	1.3725 ⁻⁰³	4.3113 ⁺⁰²	2.9453 ⁺⁰²	
64010505	1.4310	0.9854	2.5164 ⁺⁰⁴	NM	1.8026	1.2544	5.6496 ⁺⁰⁴	5.5011 ⁺⁰⁴	
2.5400 ⁻⁰¹	1.8291 ⁺⁰⁵	1.0270	3.1960 ⁺⁰⁴	NM	1.8150	1.8102	2.9170 ⁺⁰²	2.1656 ⁺⁰²	
5.9083 ⁻⁰²	3.0525 ⁺⁰²	1.0000	1.2209 ⁻⁰³	NM	0.0929	1.3188 ⁻⁰³	4.2222 ⁺⁰²	2.9602 ⁺⁰²	
64010601	3.4000	0.9806	1.2734 ⁺⁰⁴	NM	4.8533	1.2283	6.7099 ⁺⁰³	6.7099 ⁺⁰³	
NM	4.4364 ⁺⁰⁵	1.0000	3.3500 ⁺⁰⁴	NM	1.8222	1.7940	2.8714 ⁺⁰²	9.5333 ⁺⁰¹	
3.4925 ⁻⁰²	3.1574 ⁺⁰²	1.0000	1.3972 ⁻⁰³	NM	0.2746	2.0554 ⁻⁰³	6.6560 ⁺⁰²	2.9282 ⁺⁰²	
64010602	3.2690	0.9794	1.3419 ⁺⁰⁴	NM	2.0640	1.2526	9.0723 ⁺⁰³	6.7856 ⁺⁰³	
5.0800 ⁻⁰²	3.7112 ⁺⁰⁵	1.3370	3.3518 ⁺⁰⁴	NM	1.8119	1.7911	2.8756 ⁺⁰²	1.0072 ⁺⁰²	
3.5888 ⁻⁰²	3.1597 ⁺⁰²	1.0000	1.5583 ⁻⁰³	NM	0.2213	1.8467 ⁻⁰³	6.5779 ⁺⁰²	2.9360 ⁺⁰²	
64010603	3.1970	0.9765	1.2484 ⁺⁰⁴	NM	2.7100	1.2322	1.0454 ⁺⁰⁴	8.5198 ⁺⁰³	
1.5240 ⁻⁰¹	4.1934 ⁺⁰⁵	1.2270	3.0253 ⁺⁰⁴	NM	1.8294	1.8145	2.8695 ⁺⁰²	1.0378 ⁺⁰²	
4.3586 ⁻⁰²	3.1592 ⁺⁰²	1.0000	1.1964 ⁻⁰³	NM	0.2495	1.4641 ⁻⁰³	6.5299 ⁺⁰²	2.9385 ⁺⁰²	
64010604	3.0670	0.9726	1.0234 ⁺⁰⁴	NM	3.0572	1.2456	1.1548 ⁺⁰⁴	1.0033 ⁺⁰⁴	
2.0320 ⁻⁰¹	4.0738 ⁺⁰⁵	1.1510	2.3512 ⁺⁰⁴	NM	1.8386	1.8234	2.8543 ⁺⁰²	1.0928 ⁺⁰²	
5.0338 ⁻⁰²	3.1486 ⁺⁰²	1.0000	8.8714 ⁻⁰⁴	NM	0.2455	1.1091 ⁻⁰³	6.4282 ⁺⁰²	2.9348 ⁺⁰²	
64010605	3.0100	0.9678	9.1197 ⁺⁰³	NM	3.0686	1.2287	1.2415 ⁺⁰⁴	1.1045 ⁺⁰⁴	
2.5400 ⁻⁰¹	4.1184 ⁺⁰⁵	1.1240	2.8377 ⁺⁰⁴	NM	1.8557	1.8437	2.8719 ⁺⁰²	1.1311 ⁺⁰²	
5.9083 ⁻⁰²	3.1807 ⁺⁰²	1.0000	7.4804 ⁻⁰⁴	NM	0.2651	9.1366 ⁻⁰⁴	6.4184 ⁺⁰²	2.9675 ⁺⁰²	
64010701	4.0590	0.9817	3.2279 ⁺⁰³	NM	6.2267	1.3440	1.8041 ⁺⁰³	1.8041 ⁺⁰³	
NM	2.9626 ⁺⁰⁵	1.0000	1.0903 ⁺⁰⁴	NM	1.7962	1.7553	2.8540 ⁺⁰²	7.3556 ⁺⁰¹	
3.4925 ⁻⁰²	3.1593 ⁺⁰²	1.0000	9.6459 ⁻⁰⁴	NM	0.3932	1.6654 ⁻⁰³	6.9797 ⁺⁰²	2.9072 ⁺⁰²	
64010702	4.4850	0.9827	3.2849 ⁺⁰³	NM	4.9558	1.3013	2.0231 ⁺⁰³	1.4714 ⁺⁰³	
5.0800 ⁻⁰²	4.1793 ⁺⁰⁵	1.3750	1.2959 ⁺⁰⁴	NM	1.8073	1.7724	2.8357 ⁺⁰²	6.2667 ⁺⁰¹	
3.5885 ⁻⁰²	3.1478 ⁺⁰²	1.0000	1.0004 ⁻⁰³	NM	0.2633	1.5650 ⁻⁰³	7.1185 ⁺⁰²	2.8856 ⁺⁰²	
64010703	4.1660	0.9742	3.2884 ⁺⁰³	NM	5.1343	1.3382	2.6972 ⁺⁰³	2.1560 ⁺⁰³	
1.5240 ⁻⁰¹	4.0749 ⁺⁰⁵	1.2510	1.1494 ⁺⁰⁴	NM	1.8147	1.7824	2.8161 ⁺⁰²	7.0333 ⁺⁰¹	
4.3434 ⁻⁰²	3.1447 ⁺⁰²	1.0000	7.7530 ⁻⁰⁴	NM	0.2660	1.2104 ⁻⁰³	7.0050 ⁺⁰²	2.8908 ⁺⁰²	
64010704	3.9600	0.9742	2.9782 ⁺⁰³	NM	4.6085	1.2827	3.2287 ⁺⁰³	2.6684 ⁺⁰³	
2.0320 ⁻⁰¹	3.8406 ⁺⁰⁵	1.2100	9.6389 ⁺⁰³	NM	1.8419	1.8158	2.8376 ⁺⁰²	7.6444 ⁺⁰¹	
5.0338 ⁻⁰²	3.1620 ⁺⁰²	1.0000	8.2596 ⁻⁰⁴	NM	0.2408	9.1196 ⁻⁰⁴	6.9419 ⁺⁰²	2.9126 ⁺⁰²	
64010705	3.7350	0.9626	2.9865 ⁺⁰³	NM	4.1631	1.2526	3.9018 ⁺⁰³	3.3899 ⁺⁰³	
2.5400 ⁻⁰¹	3.5929 ⁺⁰⁵	1.1510	8.8061 ⁺⁰³	NM	1.8592	1.8398	2.8019 ⁺⁰²	8.3167 ⁺⁰¹	
5.9083 ⁻⁰²	3.1521 ⁺⁰²	1.0000	5.4102 ⁻⁰⁴	NM	0.2769	7.3922 ⁻⁰⁴	6.8293 ⁺⁰²	2.9107 ⁺⁰²	

CAT 6401

CLUTTER

BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUJ X * RZ *	MD * POD TOD	TW/TR PW/PD SW *	RED2W RED2D D2	CF CQ PT2	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD* TD* TR
64010801	1.5930	1.0249	2.4584"+04	NM	2.1223	1.2559	4.1039"+04	4.1039"+04
-5.0800"-02	1.7263"+05	1.0000	3.3931"+04	NM	1.8010	1.7922	3.0011"+02	2.0128"+02
3.4925"-02	3.0343"+02	1.0000	1.4153"-03	NM	0.1202	1.5863"-03	4.5313"+02	2.9281"+02
64010802	1.4090	1.0208	2.7668"+04	NM	2.0000	1.2964	5.4082"+04	5.4082"+04
5.0800"-02	1.7430"+05	1.0000	3.5881"+04	NM	1.7795	1.7728	3.0017"+02	2.1689"+02
4.5692"-02	3.0301"+02	1.0000	1.4188"-03	NM	0.0975	1.5762"-03	4.1604"+02	2.7405"+02
64010803	1.4670	1.0176	2.2260"+04	NM	2.0203	1.2593	5.0546"+04	5.0546"+04
1.0160"-01	1.7693"+05	1.0000	2.9334"+04	NM	1.8161	1.8099	2.9751"+02	2.1100"+02
5.4437"-02	3.0182"+02	1.0000	1.1491"-03	NM	0.1010	1.2692"-03	4.2725"+02	2.9237"+02
64010804	1.5050	1.0136	1.7810"+04	NM	2.1764	1.2425	4.6260"+04	4.7041"+04
1.5240"-01	1.7395"+05	0.9834	2.3663"+04	NM	1.8371	1.8305	3.0036"+02	2.1078"+02
6.1214"-02	3.0626"+02	1.0000	9.6952"-04	NM	0.1045	1.0790"-03	4.3809"+02	2.9633"+02
64010805	1.5700	1.0064	1.5397"+04	NM	2.2711	1.1990	4.2236"+04	4.3288"+04
2.0320"-01	1.7602"+05	0.9757	2.0786"+04	NM	1.8651	1.8603	2.9665"+02	2.0444"+02
6.6012"-02	3.0523"+02	1.0000	8.5171"-04	NM	0.1071	9.4704"-04	4.5009"+02	2.9475"+02
64010806	1.6260	1.0124	1.4501"+04	NM	2.4315	1.1914	3.8874"+04	4.0147"+04
2.5400"-01	1.7736"+05	0.9883	2.2046"+04	NM	1.8735	1.8662	2.9616"+02	1.9850"+02
6.8887"-02	3.0346"+02	1.0000	8.2188"-04	NM	0.1143	9.1956"-04	4.5932"+02	2.9255"+02
64010807	1.6530	1.0157	1.3982"+04	NM	2.2400	1.1904	3.7673"+04	3.8422"+04
3.0480"-01	1.7672"+05	0.9805	1.9551"+04	NM	1.8747	1.8709	2.9739"+02	1.9656"+02
6.9850"-02	3.0397"+02	1.0000	8.1308"-04	NM	0.1711	8.9015"-04	4.6465"+02	2.9280"+02
64010901	2.3510	0.9721	1.7314"+04	NM	4.0366	1.1793	2.0267"+04	2.2252"+04
1.5240"-01	3.0135"+05	0.9108	3.0133"+04	NM	1.8745	1.8624	2.8595"+02	1.4773"+02
6.1214"-02	3.1114"+02	1.0000	1.0281"-03	NM	0.2103	1.2907"-03	5.7302"+02	2.9415"+02
64010902	2.5090	0.9802	1.7625"+04	NM	4.1380	1.1947	1.7750"+04	1.9297"+04
2.0320"-01	3.3436"+05	0.9198	3.2818"+04	NM	1.8684	1.8534	2.8706"+02	1.3761"+02
6.6012"-02	3.1087"+02	1.0000	1.0945"-03	NM	0.2424	1.3967"-03	5.9012"+02	2.9285"+02
64010903	2.5120	0.9776	1.4502"+04	NM	5.0302	1.1777	1.6115"+04	1.8249"+04
2.5400"-01	3.1767"+05	0.8831	2.6974"+04	NM	1.8807	1.8675	2.8664"+02	1.3761"+02
6.8887"-02	3.1128"+02	1.0000	9.5016"-04	NM	0.1054	1.2533"-03	5.9082"+02	2.9322"+02
64010904	2.5530	0.9816	1.7188"+04	NM	4.6563	1.1978	1.4758"+04	1.6824"+04
3.0480"-01	3.1213"+05	0.8772	3.2594"+04	NM	1.8676	1.8498	2.8704"+02	1.3489"+02
6.9850"-02	3.1072"+02	1.0000	1.1912"-03	NM	0.2568	1.5718"-03	5.9450"+02	2.9244"+02
64010905	2.6110	0.9830	1.5165"+04	NM	4.1949	1.1913	1.4603"+04	1.4960"+04
3.5560"-01	3.0366"+05	0.9761	2.9447"+04	NM	1.8695	1.8539	2.8732"+02	1.3156"+02
6.9850"-02	3.1093"+02	1.0000	1.1422"-03	NM	0.1223	1.4647"-03	6.0044"+02	2.9277"+02
64010906	2.6350	0.9856	2.1276"+04	NM	3.4668	1.2127	1.5244"+04	1.5244"+04
4.5720"-01	3.2109"+05	1.0000	4.1760"+04	NM	1.8495	1.8324	2.8928"+02	1.3078"+02
6.9850"-02	3.1238"+02	1.0000	1.5619"-03	NM	0.2336	1.9496"-03	6.0417"+02	2.9349"+02
64011001	3.2760	0.9763	9.0277"+03	NM	5.6932	1.2171	7.6394"+03	8.4892"+03
2.0320"-01	4.6906"+05	0.8999	2.2482"+04	NM	1.8529	1.8366	2.9174"+02	1.0222"+02
6.6012"-02	3.2164"+02	1.0000	8.5188"-04	NM	0.2833	1.2857"-03	6.6409"+02	2.9882"+02
64011002	3.2990	0.9850	7.4125"+03	NM	6.0795	1.1951	6.3648"+03	7.3889"+03
2.5400"-01	4.2217"+05	0.8614	1.8788"+04	NM	1.8719	1.8563	2.9044"+02	9.9944"+01
6.8887"-02	3.1749"+02	1.0000	7.8634"-04	NM	0.3188	1.1719"-03	6.0126"+02	2.9487"+02
64011003	3.4770	0.9815	3.6901"+03	NM	8.5066	1.1896	5.4776"+03	5.8715"+03
3.0480"-01	4.3342"+05	0.9329	9.9787"+03	NM	1.9012	1.8866	2.9146"+02	9.3778"+01
6.9850"-02	3.2052"+02	1.0000	4.5399"-04	NM	-0.2989	6.7720"-04	6.7509"+02	2.9694"+02
64011004	3.5030	0.9791	5.1075"+03	NM	5.3519	1.1944	5.7005"+03	5.7499"+03
3.5560"-01	4.4043"+05	0.9914	1.3914"+04	NM	1.8895	1.8725	2.9162"+02	9.3111"+01
6.9850"-02	3.2162"+02	1.0000	6.3491"-04	NM	0.3008	8.6461"-04	6.7772"+02	2.9786"+02
64011005	3.4020	0.9837	5.5550"+03	NM	4.9219	1.2224	5.2817"+03	5.2817"+03
4.5720"-01	3.5022"+05	1.0000	1.4640"+04	NM	1.8697	1.8482	2.9030"+02	9.8000"+01
6.9850"-02	3.1821"+02	1.0000	7.8322"-04	NM	0.3043	1.0759"-03	6.6831"+02	2.9510"+02
64011101	4.4040	0.9775	3.1180"+03	NM	10.3645	1.2619	1.5795"+03	1.8487"+03
3.0480"-01	4.7427"+05	0.8844	1.1843"+04	NM	1.8728	1.8330	2.8875"+02	6.6000"+01
6.9850"-02	3.2202"+02	1.0000	8.0112"-04	NM	0.3407	1.5244"-03	7.1735"+02	2.9339"+02
64011102	4.2950	0.9808	3.3199"+03	NM	8.1600	1.2605	1.5244"+03	1.6432"+03
3.5560"-01	3.6696"+05	0.9277	1.2206"+04	NM	1.8537	1.8180	2.8505"+02	6.7500"+01
6.9850"-02	3.1653"+02	1.0000	9.8516"-04	NM	0.4166	1.7163"-03	7.0750"+02	2.9864"+02
64011103	3.9470	0.9763	3.5929"+03	NM	5.9911	1.2931	2.9971"+03	2.0459"+03
4.5720"-01	2.8938"+05	1.0250	1.1537"+04	NM	1.8251	1.7913	2.9081"+02	7.8556"+01
6.9850"-02	3.2332"+02	1.0000	1.0210"-03	NM	0.3690	1.6730"-03	7.0140"+02	2.9786"+02
64011104	4.2490	0.9820	2.9720"+03	NM	7.7819	1.2965	1.5961"+03	1.6432"+03
5.5880"-01	3.4588"+05	0.9713	1.0717"+04	NM	1.8517	1.8150	2.9044"+02	6.9833"+01
6.9850"-02	3.2199"+02	1.0000	9.2005"-04	NM	0.3552	1.5548"-03	7.1191"+02	2.9376"+02

CAT 6401		CLUTTER		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN	MD *	TW/TR	RED2W	CF	H12	H12K	PW	PD*	
X *	POD	PW/PD	RED2D	CG	H32	H32K	TW*	TD*	
RZ *	TOD	SW *	D2	PI2	H42	D2K	UD	TR	
64011201	1.5070	0.6743	2.5165 ⁺⁰⁴	NM	2.0351	1.2271	4.7375 ⁺⁰⁴	4.8243 ⁺⁰⁴	
1.5240 ⁻⁰¹	1.7891 ⁺⁰⁵	0.9820	2.4074 ⁺⁰⁴	NM	1.8400	1.8381	1.9796 ⁺⁰²	2.0867 ⁺⁰²	
6.1214 ⁻⁰²	3.0345 ⁺⁰²	1.0000	9.4768 ⁻⁰⁴	NM	0.1888	1.0267 ⁻⁰³	4.3647 ⁺⁰²	2.9359 ⁺⁰²	
64011202	1.5700	0.6068	2.2468 ⁺⁰⁴	NM	2.0574	1.2123	4.1589 ⁺⁰⁴	4.2624 ⁺⁰⁴	
2.0320 ⁻⁰¹	1.7332 ⁺⁰⁵	0.9757	2.0048 ⁺⁰⁴	NM	1.8565	1.8555	1.7882 ⁺⁰²	2.0439 ⁺⁰²	
6.6012 ⁻⁰²	3.0515 ⁺⁰²	1.0000	8.3392 ⁻⁰⁴	NM	0.2341	8.9690 ⁻⁰⁴	4.5003 ⁺⁰²	2.9467 ⁺⁰²	
64011203	1.6330	0.6652	2.0676 ⁺⁰⁴	NM	2.2285	1.2206	3.7921 ⁺⁰⁴	3.9114 ⁺⁰⁴	
2.5400 ⁻⁰¹	1.7461 ⁺⁰⁵	0.9695	2.0379 ⁺⁰⁴	NM	1.8530	1.8503	1.9394 ⁺⁰²	1.9728 ⁺⁰²	
6.8887 ⁻⁰²	3.0249 ⁺⁰²	1.0000	8.4685 ⁻⁰⁴	NM	0.2274	9.2652 ⁻⁰⁴	4.5987 ⁺⁰²	2.9155 ⁺⁰²	
64011204	1.6620	0.7773	1.7901 ⁺⁰⁴	NM	2.3097	1.2142	3.7203 ⁺⁰⁴	3.7943 ⁺⁰⁴	
3.0480 ⁻⁰¹	1.7689 ⁺⁰⁵	0.9805	2.0290 ⁺⁰⁴	NM	1.8601	1.8548	2.2756 ⁺⁰²	1.9583 ⁺⁰²	
6.9850 ⁻⁰²	3.0402 ⁺⁰²	1.0000	8.4562 ⁻⁰⁴	NM	0.1500	9.3904 ⁻⁰⁴	4.6632 ⁺⁰²	2.9277 ⁺⁰²	
64011301	2.3630	0.6203	2.6842 ⁺⁰⁴	NM	3.4882	1.2171	2.0418 ⁺⁰⁴	2.2196 ⁺⁰⁴	
1.5240 ⁻⁰¹	3.0628 ⁺⁰⁵	0.9199	3.2541 ⁺⁰⁴	NM	1.8469	1.8369	1.8057 ⁺⁰²	1.4550 ⁺⁰²	
6.1214 ⁻⁰²	3.0799 ⁺⁰²	1.0000	1.0836 ⁻⁰³	NM	0.3584	1.3370 ⁻⁰³	5.7149 ⁺⁰²	2.9109 ⁺⁰²	
64011302	2.5180	0.5735	3.2052 ⁺⁰⁴	NM	2.9578	1.2626	1.8073 ⁺⁰⁴	1.8661 ⁺⁰⁴	
2.0320 ⁻⁰¹	3.2790 ⁺⁰⁵	0.9686	3.8430 ⁺⁰⁴	NM	1.8137	1.8063	1.6837 ⁺⁰²	1.3744 ⁺⁰²	
6.6012 ⁻⁰²	3.1173 ⁺⁰²	1.0000	1.3184 ⁻⁰³	NM	0.5971	1.5757 ⁻⁰³	5.9187 ⁺⁰²	2.9361 ⁺⁰²	
64011303	2.5290	0.6551	2.2207 ⁺⁰⁴	NM	4.3376	1.2205	1.5791 ⁺⁰⁴	1.7825 ⁺⁰⁴	
2.5400 ⁻⁰¹	3.1861 ⁺⁰⁵	0.8659	2.9992 ⁺⁰⁴	NM	1.8458	1.8342	1.9317 ⁺⁰²	1.3739 ⁺⁰²	
6.8887 ⁻⁰²	3.1313 ⁺⁰²	1.0000	1.0718 ⁻⁰³	NM	0.3251	1.4117 ⁻⁰³	5.9433 ⁺⁰²	2.9486 ⁺⁰²	
64011304	2.6350	0.6252	2.3996 ⁺⁰⁴	NM	3.5369	1.2344	1.4894 ⁺⁰⁴	1.5093 ⁺⁰⁴	
3.5560 ⁻⁰¹	3.1791 ⁺⁰⁵	0.9868	3.2441 ⁺⁰⁴	NM	1.8368	1.8239	1.8387 ⁺⁰²	1.3106 ⁺⁰²	
6.9850 ⁻⁰²	3.1305 ⁺⁰²	1.0000	1.2292 ⁻⁰³	NM	0.3115	1.5450 ⁻⁰³	6.0481 ⁺⁰²	2.9412 ⁺⁰²	
64011401	3.2190	0.6388	9.3986 ⁺⁰³	NM	5.0338	1.2686	6.9809 ⁺⁰³	8.0175 ⁺⁰³	
2.5400 ⁻⁰¹	4.0758 ⁺⁰⁵	0.8707	1.6222 ⁺⁰⁴	NM	1.8386	1.8247	1.8960 ⁺⁰²	1.0389 ⁺⁰²	
6.8887 ⁻⁰²	3.1919 ⁺⁰²	1.0000	6.7815 ⁻⁰⁴	NM	0.5925	9.3428 ⁻⁰⁴	6.5783 ⁺⁰²	2.9680 ⁺⁰²	
64011402	3.4020	0.6132	9.1805 ⁺⁰³	NM	4.7794	1.2460	6.1605 ⁺⁰³	6.5572 ⁺⁰³	
3.0480 ⁻⁰¹	4.3479 ⁺⁰⁵	0.9395	1.6452 ⁺⁰⁴	NM	1.8510	1.8368	1.7803 ⁺⁰²	9.4444 ⁺⁰¹	
6.9850 ⁻⁰²	3.1306 ⁺⁰²	1.0000	6.9218 ⁻⁰⁴	NM	0.5421	9.3818 ⁻⁰⁴	6.6288 ⁺⁰²	2.9632 ⁺⁰²	
64011403	3.4560	0.6060	9.8737 ⁺⁰³	NM	3.9248	1.2802	5.4502 ⁺⁰³	5.4876 ⁺⁰³	
3.5560 ⁻⁰¹	3.9313 ⁺⁰⁵	0.9932	1.7862 ⁺⁰⁴	NM	1.8246	1.8117	1.7772 ⁺⁰²	9.3389 ⁺⁰¹	
6.9850 ⁻⁰²	3.1648 ⁺⁰²	1.0000	8.6944 ⁻⁰⁴	NM	0.6388	1.1250 ⁻⁰³	6.6962 ⁺⁰²	2.9327 ⁺⁰²	
64011501	4.0840	0.7228	4.0569 ⁺⁰³	NM	5.4010	1.2906	2.0624 ⁺⁰³	2.1900 ⁺⁰³	
2.5400 ⁻⁰¹	3.7171 ⁺⁰⁵	0.9417	1.0807 ⁺⁰⁴	NM	1.8232	1.8028	2.0934 ⁺⁰²	7.2611 ⁺⁰¹	
6.8887 ⁻⁰²	3.1483 ⁺⁰²	1.0000	7.6783 ⁻⁰⁴	NM	0.7668	1.1530 ⁻⁰³	6.9779 ⁺⁰²	2.8964 ⁺⁰²	
64011502	4.4110	0.6762	3.7773 ⁺⁰³	NM	8.1749	1.2754	1.5452 ⁺⁰³	1.7366 ⁺⁰³	
3.0480 ⁻⁰¹	4.4948 ⁺⁰⁵	0.8898	1.0711 ⁺⁰⁴	NM	1.8365	1.8107	1.9468 ⁺⁰²	6.4167 ⁺⁰¹	
6.9850 ⁻⁰²	3.1386 ⁺⁰²	1.0000	7.3813 ⁻⁰⁴	NM	0.6405	1.2595 ⁻⁰³	7.0844 ⁺⁰²	2.8790 ⁺⁰²	
64011503	4.3270	0.7710	3.6809 ⁺⁰³	NM	5.9722	1.2965	1.5248 ⁺⁰³	1.5542 ⁺⁰³	
3.5560 ⁻⁰¹	3.6198 ⁺⁰⁵	0.9811	1.1284 ⁺⁰⁴	NM	1.8237	1.7984	2.2461 ⁺⁰²	6.6889 ⁺⁰¹	
6.9850 ⁻⁰²	3.1736 ⁺⁰²	1.0000	9.4280 ⁻⁰⁴	NM	0.6536	1.4516 ⁻⁰³	7.0953 ⁺⁰²	2.9131 ⁺⁰²	

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PDD RED2PWD	RED2PDW RED2PWW	DATA
64010301	1.1312 ⁻⁰³ 1.1312 ⁻⁰³	4.7839 4.7839	1.8711 1.8711	0.2419 0.2419	2.2878 ⁺⁰⁴ 2.2878 ⁺⁰⁴	9.0935 ⁺⁰³ 9.0936 ⁺⁰³	5.4091 ⁻⁰³
64010302	1.2351 ⁻⁰³ 1.2190 ⁻⁰³	4.8130 4.8081	1.8663 1.8692	0.2443 0.2439	2.6208 ⁺⁰⁴ 2.6250 ⁺⁰⁴	1.0231 ⁺⁰⁴ 1.0247 ⁺⁰⁴	5.4684 ⁻⁰³
64010303	1.2469 ⁻⁰³ 1.2320 ⁻⁰³	4.7932 4.7887	1.8648 1.8675	0.2515 0.2512	2.5084 ⁺⁰⁴ 2.5121 ⁺⁰⁴	9.8496 ⁺⁰³ 9.8641 ⁺⁰³	5.9055 ⁻⁰³
64010304	1.2827 ⁻⁰³ 1.2826 ⁻⁰³	4.6319 4.6319	1.8640 1.8640	0.2357 0.2357	2.5145 ⁺⁰⁴ 2.5145 ⁺⁰⁴	1.0112 ⁺⁰⁴ 1.0112 ⁺⁰⁴	5.9387 ⁻⁰³
64010401	1.3970 ⁻⁰³ 1.3970 ⁻⁰³	4.8540 4.8539	1.8222 1.8222	0.2746 0.2746	3.3535 ⁺⁰⁴ 3.3535 ⁺⁰⁴	1.2747 ⁺⁰⁴ 1.2747 ⁺⁰⁴	6.7767 ⁻⁰³
64010402	1.3269 ⁻⁰³ 1.1269 ⁻⁰³	4.4435 4.3941	1.7917 1.8318	0.2600 0.2541	2.8576 ⁺⁰⁴ 2.9252 ⁺⁰⁴	1.1440 ⁺⁰⁴ 1.1711 ⁺⁰⁴	5.8362 ⁻⁰³
64010403	1.0741 ⁻⁰³ 9.5745 ⁻⁰⁴	4.3415 4.2972	1.8156 1.8443	0.2780 0.2736	2.7190 ⁺⁰⁴ 2.7636 ⁺⁰⁴	1.1221 ⁺⁰⁴ 1.1405 ⁺⁰⁴	4.1652 ⁻⁰³
64010404	8.1940 ⁻⁰⁴ 7.5710 ⁻⁰⁴	4.2274 4.1901	1.8279 1.8487	0.2662 0.2632	2.1714 ⁺⁰⁴ 2.1968 ⁺⁰⁴	9.4516 ⁺⁰³ 9.5621 ⁺⁰³	3.1986 ⁻⁰³
64010405	8.9712 ⁻⁰⁴ 8.5375 ⁻⁰⁴	4.0546 4.0215	1.8471 1.8650	0.2845 0.2817	1.9013 ⁺⁰⁴ 1.9200 ⁺⁰⁴	8.5091 ⁺⁰³ 8.5931 ⁺⁰³	2.6460 ⁻⁰³
64011001	8.5869 ⁻⁰⁴ 9.4479 ⁻⁰⁴	4.8368 4.8637	1.8582 1.8450	0.2716 0.2735	2.3463 ⁺⁰⁴ 2.3313 ⁺⁰⁴	9.4295 ⁺⁰³ 9.3610 ⁺⁰³	4.5479 ⁻⁰³
64011002	8.3777 ⁻⁰⁴ 9.1399 ⁻⁰⁴	4.7903 4.8251	1.8789 1.8605	0.2992 0.3022	2.0052 ⁺⁰⁴ 1.9852 ⁺⁰⁴	7.9068 ⁺⁰³ 7.8278 ⁺⁰³	4.3481 ⁻⁰³
64011003	4.5063 ⁻⁰⁴ 5.0093 ⁻⁰⁴	7.1994 7.2217	1.9061 1.8982	-0.2823 -0.2835	1.0577 ⁺⁰⁴ 1.0533 ⁺⁰⁴	3.9113 ⁺⁰³ 3.8950 ⁺⁰³	3.5988 ⁻⁰³
64011004	5.4120 ⁻⁰⁴ 6.4450 ⁻⁰⁴	5.1624 5.1644	1.8904 1.8695	0.2978 0.2979	1.4068 ⁺⁰⁴ 1.4061 ⁺⁰⁴	5.1644 ⁺⁰³ 5.1617 ⁺⁰³	3.3261 ⁻⁰³
64011005	7.8321 ⁻⁰⁴ 7.8320 ⁻⁰⁴	4.9222 4.9222	1.8697 1.8697	0.3043 0.3043	1.4657 ⁺⁰⁴ 1.4657 ⁺⁰⁴	5.5616 ⁺⁰³ 5.5616 ⁺⁰³	3.8531 ⁻⁰³

64010301		CLUTTER		PROFILE TABULATION		49 POINTS, DELTA AT POINT 49			
I	Y	#T2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000+00	1.0000+00	1.00000	0.91272	0.00000	0.00000	2.87300	0.00000	
2	1.2700-04	2.2778+00	1.00000	0.93624	0.35222	0.51730	2.32700	0.23090	
3	2.5400-04	3.0674+00	1.00000	0.93814	0.42880	0.62390	2.11700	0.29471	
4	3.8100-04	3.7008+00	1.00000	0.94073	0.48034	0.67590	1.98000	0.34136	
5	5.0800-04	4.0828+00	1.00000	0.94256	0.50871	0.70250	1.90700	0.36838	
6	6.3500-04	4.4457+00	1.00000	0.94434	0.53419	0.72520	1.84300	0.39349	
7	7.6200-04	4.7554+00	1.00000	0.94586	0.55496	0.74290	1.79200	0.41456	
8	8.8900-04	5.0209+00	1.00000	0.94737	0.57215	0.75710	1.75100	0.43238	
9	1.0160-03	5.2537+00	1.00000	0.94886	0.58679	0.76890	1.71700	0.44782	
10	1.1430-03	5.4676+00	1.00000	0.95021	0.59992	0.77920	1.68700	0.46189	
11	1.2700-03	5.6674+00	1.00000	0.95147	0.61192	0.78840	1.66000	0.47494	
12	1.4050-03	6.0072+00	1.00000	0.95690	0.65440	0.81970	1.56900	0.52243	
13	2.5400-03	6.9687+00	1.00000	0.96166	0.68485	0.84100	1.50800	0.55769	
14	3.1750-03	7.4344+00	1.00000	0.96530	0.70910	0.85710	1.46100	0.58665	
15	3.8100-03	7.8660+00	1.00000	0.96863	0.73084	0.87090	1.42000	0.61331	
16	4.4450-03	8.2637+00	1.00000	0.97128	0.75129	0.88320	1.38200	0.63907	
17	5.0800-03	8.5523+00	1.00000	0.97317	0.76414	0.89080	1.35900	0.65548	
18	5.7150-03	8.8258+00	1.00000	0.97477	0.77700	0.89810	1.33600	0.67223	
19	6.3500-03	9.0592+00	1.00000	0.97611	0.78781	0.90410	1.31700	0.68648	
20	6.9850-03	9.2752+00	1.00000	0.97740	0.79768	0.90950	1.30000	0.69962	
21	7.6200-03	9.5124+00	1.00000	0.97890	0.80839	0.91530	1.28200	0.71396	
22	8.2550-03	9.7695+00	1.00000	0.98038	0.81978	0.92130	1.26300	0.72945	
23	8.8900-03	9.9328+00	1.00000	0.98123	0.82701	0.92500	1.25100	0.73941	
24	9.5250-03	1.0129+01	1.00000	0.98222	0.83555	0.92930	1.23700	0.75125	
25	1.0160-02	1.0319+01	1.00000	0.98343	0.84377	0.93350	1.22400	0.76266	
26	1.0795-02	1.0550+01	1.00000	0.98435	0.85361	0.93820	1.20800	0.77666	
27	1.1430-02	1.0870+01	1.00000	0.98603	0.86710	0.94470	1.18700	0.79587	
28	1.2065-02	1.1092+01	1.00000	0.98727	0.87632	0.94910	1.17300	0.80912	
29	1.2700-02	1.1360+01	1.00000	0.98823	0.88730	0.95400	1.15600	0.82525	
30	1.3335-02	1.1578+01	1.00000	0.98945	0.89616	0.95810	1.14300	0.83823	
31	1.3970-02	1.1844+01	1.00000	0.99040	0.90684	0.96270	1.12700	0.85421	
32	1.4605-02	1.2069+01	1.00000	0.99140	0.91581	0.96660	1.11400	0.86768	
33	1.5240-02	1.2324+01	1.00000	0.99277	0.92581	0.97100	1.10000	0.88273	
34	1.5875-02	1.2615+01	1.00000	0.99393	0.93713	0.97570	1.08400	0.90009	
35	1.6510-02	1.2875+01	1.00000	0.99482	0.94711	0.97970	1.07000	0.91561	
36	1.7145-02	1.3130+01	1.00000	0.99605	0.95681	0.98370	1.05700	0.93065	
37	1.7780-02	1.3326+01	1.00000	0.99677	0.96420	0.98660	1.04700	0.94231	
38	1.8415-02	1.3462+01	1.00000	0.99710	0.96930	0.98850	1.04000	0.95048	
39	1.9050-02	1.3606+01	1.00000	0.99772	0.97465	0.99060	1.03300	0.95895	
40	1.9685-02	1.3749+01	1.00000	0.99820	0.97994	0.99260	1.02600	0.96745	
41	2.0320-02	1.3851+01	1.00000	0.99851	0.98372	0.99400	1.02100	0.97356	
42	2.0955-02	1.3915+01	1.00000	0.99878	0.98606	0.99490	1.01800	0.97731	
43	2.1590-02	1.3979+01	1.00000	0.99905	0.98841	0.99580	1.01500	0.98108	
44	2.2225-02	1.4068+01	1.00000	0.99954	0.99166	0.99710	1.01100	0.98625	
45	2.2860-02	1.4171+01	1.00000	0.99972	0.99542	0.99840	1.00600	0.99245	
46	2.3495-02	1.4196+01	1.00000	0.99995	0.99631	0.99880	1.00500	0.99383	
47	2.4130-02	1.4234+01	1.00000	0.99986	0.99770	0.99920	1.00300	0.99621	
48	2.4765-02	1.4262+01	1.00000	1.00023	0.99870	0.99970	1.00200	0.99770	
0 49	2.5400-02	1.4298+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, DELTA, U/UD, T/TD, P/PD

64010302		CLUTTER	PROFILE TABULATION			50 POINTS, DELTA AT POINT 50			
I	Y	PTZ/P	P/PO	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	1.02300	0.91947	0.00000	0.00000	2.93300	0.00000	
2	1.2757"-04	2.6373"+00	1.02300	0.93337	0.36561	0.57790	2.24600	0.26322	
3	2.5514"-04	3.6253"+00	1.02300	0.93530	0.46993	0.66640	2.01100	0.33900	
4	3.8011"-04	3.9947"+00	1.02300	0.93727	0.49746	0.69270	1.93900	0.36546	
5	5.0768"-04	4.2893"+00	1.02200	0.93907	0.51831	0.71180	1.88600	0.38572	
6	6.3525"-04	4.5203"+00	1.02200	0.94066	0.53405	0.72580	1.84700	0.40161	
7	7.6282"-04	4.7450"+00	1.02200	0.94234	0.54892	0.73870	1.81100	0.41687	
8	8.8779"-04	4.9517"+00	1.02200	0.94376	0.56223	0.74990	1.77900	0.43080	
9	1.0154"-03	5.1418"+00	1.02200	0.94524	0.57419	0.75980	1.75100	0.44347	
10	1.1429"-03	5.3111"+00	1.02200	0.94663	0.58463	0.76830	1.72700	0.45466	
11	1.2705"-03	5.4609"+00	1.02200	0.94821	0.59371	0.77570	1.70700	0.46442	
12	1.9058"-03	6.1076"+00	1.02100	0.95472	0.63138	0.80510	1.62600	0.50554	
13	2.5410"-03	6.6426"+00	1.02100	0.95925	0.66088	0.82650	1.56400	0.53955	
14	3.1763"-03	7.1341"+00	1.02000	0.96306	0.68685	0.84430	1.51100	0.56994	
15	3.8089"-03	7.5370"+00	1.02000	0.96586	0.70742	0.85770	1.47000	0.59514	
16	4.4442"-03	7.9150"+00	1.01900	0.96867	0.72618	0.86960	1.43400	0.61794	
17	5.0794"-03	8.2975"+00	1.01800	0.97117	0.74468	0.88080	1.39900	0.64093	
18	5.7147"-03	8.6160"+00	1.01800	0.97307	0.75976	0.88960	1.37100	0.66055	
19	6.3499"-03	8.8694"+00	1.01700	0.97484	0.77150	0.89640	1.35000	0.67529	
20	6.9852"-03	9.1236"+00	1.01700	0.97617	0.78312	0.90280	1.32900	0.69086	
21	7.6204"-03	9.3277"+00	1.01600	0.97749	0.79233	0.90790	1.31300	0.70253	
22	8.2557"-03	9.5057"+00	1.01600	0.97835	0.80027	0.91210	1.29900	0.71339	
23	8.8910"-03	9.6940"+00	1.01500	0.97961	0.80859	0.91660	1.28500	0.72401	
24	9.5262"-03	9.9506"+00	1.01500	0.98098	0.81977	0.92240	1.26600	0.73952	
25	1.0154"-02	1.0124"+01	1.01400	0.98200	0.82982	0.92740	1.24900	0.75291	
26	1.0794"-02	1.0401"+01	1.01300	0.98329	0.83908	0.93210	1.23400	0.76517	
27	1.1429"-02	1.0633"+01	1.01300	0.98431	0.84883	0.93680	1.21800	0.77913	
28	1.2063"-02	1.0952"+01	1.01200	0.98598	0.86210	0.94320	1.19700	0.79743	
29	1.2700"-02	1.1150"+01	1.01200	0.98671	0.87022	0.94690	1.18400	0.80934	
30	1.3335"-02	1.1376"+01	1.01100	0.98792	0.87938	0.95120	1.17000	0.82193	
31	1.3970"-02	1.1667"+01	1.01100	0.98904	0.889107	0.95640	1.15200	0.83934	
32	1.4606"-02	1.1900"+01	1.01000	0.98997	0.90029	0.96040	1.13800	0.85238	
33	1.5241"-02	1.2159"+01	1.00900	0.99108	0.91043	0.96480	1.12300	0.86686	
34	1.5876"-02	1.2411"+01	1.00900	0.99240	0.92024	0.96910	1.10900	0.88171	
35	1.6509"-02	1.2678"+01	1.00800	0.99316	0.93045	0.97320	1.09400	0.89670	
36	1.7144"-02	1.2869"+01	1.00800	0.99418	0.93771	0.97630	1.08400	0.90785	
37	1.7779"-02	1.3072"+01	1.00700	0.99476	0.94540	0.97930	1.07300	0.91906	
38	1.8415"-02	1.3269"+01	1.00700	0.99566	0.95275	0.98230	1.06300	0.93055	
39	1.9050"-02	1.3484"+01	1.00600	0.99640	0.96074	0.98540	1.05200	0.94231	
40	1.9685"-02	1.3702"+01	1.00600	0.99702	0.96874	0.98840	1.04100	0.95517	
41	2.0320"-02	1.3830"+01	1.00500	0.99772	0.97341	0.99030	1.03500	0.96160	
42	2.0956"-02	1.3969"+01	1.00400	0.99797	0.97850	0.99210	1.02200	0.96894	
43	2.1591"-02	1.4098"+01	1.00400	0.99855	0.98314	0.99390	1.02200	0.97639	
44	2.2226"-02	1.4241"+01	1.00300	0.99881	0.98832	0.99570	1.01500	0.98393	
45	2.2859"-02	1.4310"+01	1.00300	0.99924	0.99077	0.99670	1.01200	0.98784	
46	2.3494"-02	1.4351"+01	1.00200	0.99930	0.99225	0.99720	1.01000	0.98930	
47	2.4129"-02	1.4393"+01	1.00200	0.99935	0.99373	0.99770	1.00800	0.99176	
48	2.4764"-02	1.4462"+01	1.00100	0.99978	0.99621	0.99870	1.00500	0.99473	
49	2.5400"-02	1.4529"+01	1.00100	1.00008	0.99860	0.99960	1.00200	0.99860	
D 50	2.6035"-02	1.4569"+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, DELTA, U/UD, T/TD, P/PO

64010303		CLUTTER	PROFILE TABULATION			47 POINTS, DELTA AT POINT 47			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TC	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	1.02100	0.91181	0.00000	0.00000	2.91100	0.00000	
2	1.2789"-04	2.6670"+00	1.02100	0.91515	0.38822	0.57530	2.19600	0.26748	
3	2.5336"-04	3.6857"+00	1.02100	0.91762	0.47426	0.66430	1.96200	0.34569	
4	3.8125"-04	4.2412"+00	1.02100	0.92045	0.51465	0.70170	1.85900	0.38539	
5	5.0914"-04	4.6021"+00	1.02100	0.92321	0.53919	0.72340	1.80000	0.41033	
6	6.3462"-04	4.8116"+00	1.02100	0.92603	0.55291	0.73560	1.77000	0.42432	
7	7.6251"-04	4.9708"+00	1.02100	0.92871	0.56310	0.74470	1.74900	0.43473	
8	8.8798"-04	5.1099"+00	1.02100	0.93151	0.57186	0.75260	1.73200	0.44365	
9	1.0159"-03	5.2505"+00	1.02100	0.93418	0.58057	0.76030	1.71500	0.45263	
10	1.1438"-03	5.3762"+00	1.02000	0.93703	0.58824	0.76720	1.70100	0.46005	
11	1.2692"-03	5.5036"+00	1.02000	0.93985	0.59591	0.77400	1.68700	0.46798	
12	1.9039"-03	6.0888"+00	1.02000	0.95419	0.62993	0.80400	1.62900	0.50343	
13	2.5409"-03	6.6009"+00	1.01900	0.95832	0.65623	0.82450	1.56900	0.53548	
14	3.1755"-03	7.0529"+00	1.01900	0.96196	0.68222	0.84110	1.52000	0.56387	
15	3.8101"-03	7.4633"+00	1.01800	0.96500	0.70328	0.85500	1.47600	0.58890	
16	4.4447"-03	7.8370"+00	1.01700	0.96780	0.72192	0.86690	1.44200	0.61140	
17	5.0794"-03	8.1953"+00	1.01700	0.97028	0.73908	0.87760	1.40900	0.63344	
18	5.7140"-03	8.5150"+00	1.01600	0.97253	0.75454	0.88670	1.38100	0.65234	
19	6.3510"-03	8.7917"+00	1.01600	0.97394	0.76745	0.89400	1.35700	0.66935	
20	6.9856"-03	9.0387"+00	1.01500	0.97569	0.77879	0.90050	1.33700	0.68363	
21	7.6203"-03	9.2738"+00	1.01500	0.97694	0.78943	0.90630	1.31800	0.69795	
22	8.2549"-03	9.4820"+00	1.01400	0.97829	0.79874	0.91140	1.30200	0.70980	
23	8.8895"-03	9.6788"+00	1.01400	0.97937	0.80743	0.91600	1.28700	0.72170	
24	9.5241"-03	9.8443"+00	1.01300	0.98055	0.81902	0.92190	1.26700	0.73708	
25	1.0161"-02	1.0139"+01	1.01200	0.98162	0.82743	0.92420	1.25300	0.74806	
26	1.0796"-02	1.0397"+01	1.01200	0.98300	0.83838	0.93170	1.23500	0.76347	
27	1.1430"-02	1.0660"+01	1.01100	0.98429	0.84946	0.93710	1.21700	0.77848	
28	1.2065"-02	1.0919"+01	1.01100	0.98568	0.86020	0.94230	1.20000	0.79369	
29	1.2700"-02	1.1150"+01	1.01000	0.98669	0.86967	0.94670	1.18500	0.80689	
30	1.3334"-02	1.1352"+01	1.01000	0.98744	0.87790	0.95040	1.17200	0.81903	
31	1.3969"-02	1.1581"+01	1.00900	0.98855	0.88709	0.95460	1.15800	0.83177	
32	1.4606"-02	1.1780"+01	1.00800	0.98939	0.89499	0.95810	1.14600	0.84273	
33	1.5241"-02	1.2005"+01	1.00800	0.99059	0.90387	0.96210	1.13300	0.85595	
34	1.5875"-02	1.2300"+01	1.00700	0.99176	0.91537	0.96700	1.11600	0.87255	
35	1.6510"-02	1.2602"+01	1.00700	0.99282	0.92700	0.97180	1.09900	0.89045	
36	1.7144"-02	1.2862"+01	1.00600	0.99392	0.93689	0.97590	1.08500	0.90484	
37	1.7779"-02	1.3068"+01	1.00600	0.99464	0.94467	0.97900	1.07400	0.91701	
38	1.8418"-02	1.3262"+01	1.00500	0.99541	0.95191	0.98190	1.06400	0.92745	
39	1.9051"-02	1.3459"+01	1.00500	0.99620	0.95924	0.98480	1.05400	0.93902	
40	1.9685"-02	1.3635"+01	1.00400	0.99663	0.96571	0.98720	1.04500	0.94847	
41	2.0320"-02	1.3823"+01	1.00300	0.99761	0.97265	0.99000	1.03600	0.95847	
42	2.0954"-02	1.4031"+01	1.00300	0.99829	0.98014	0.99280	1.02600	0.97054	
43	2.1589"-02	1.4201"+01	1.00200	0.99892	0.98626	0.99510	1.01800	0.97946	
44	2.2226"-02	1.4305"+01	1.00200	0.99914	0.98999	0.99640	1.01300	0.98558	
45	2.2861"-02	1.4412"+01	1.00100	0.99949	0.99383	0.99780	1.00800	0.99087	
46	2.3495"-02	1.4521"+01	1.00100	0.99984	0.99770	0.99920	1.00300	0.99721	
D 47	2.4130"-02	1.4586"+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, DELTA, U/UD, T/TD, P/PD

64010304		CLUTTER	PROFILE TABULATION			48 POINTS, DELTA AT POINT 48			
I	Y	P/T2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	1.00000	0.93400	0.00000	0.00000	2.85400	0.00000	
2	1.2630 ⁻ -04	2.6245 ⁺ +00	1.00000	0.93602	0.39673	0.58320	2.16100	0.26988	
3	2.5508 ⁻ -04	3.2910 ⁺ +00	1.00000	0.93914	0.45766	0.64820	2.00600	0.32313	
4	3.8138 ⁻ -04	3.6995 ⁺ +00	1.00000	0.93908	0.49088	0.66000	1.91900	0.35835	
5	5.0768 ⁻ -04	4.0459 ⁺ +00	1.00000	0.94044	0.51725	0.70430	1.85400	0.37988	
6	6.3398 ⁻ -04	4.3100 ⁺ +00	1.00000	0.94221	0.53643	0.72150	1.80900	0.39884	
7	7.6278 ⁻ -04	4.5140 ⁺ +00	1.00000	0.94365	0.55078	0.73400	1.77600	0.41329	
8	8.8908 ⁻ -04	4.6940 ⁺ +00	1.00000	0.94494	0.56311	0.74450	1.74800	0.42592	
9	1.0154 ⁻ -03	4.8604 ⁺ +00	1.00000	0.94613	0.57427	0.75380	1.72300	0.43749	
10	1.1441 ⁻ -03	4.9868 ⁺ +00	1.00000	0.94747	0.58273	0.76090	1.70500	0.44628	
11	1.2704 ⁻ -03	5.1212 ⁺ +00	1.00000	0.94835	0.59132	0.76740	1.68600	0.45340	
12	1.4044 ⁻ -03	5.2620 ⁺ +00	1.00000	0.95359	0.62636	0.79550	1.61300	0.48318	
13	2.5409 ⁻ -03	6.1878 ⁺ +00	1.00000	0.95827	0.65632	0.81790	1.55300	0.52666	
14	3.1749 ⁻ -03	6.7246 ⁺ +00	1.00000	0.95960	0.68666	0.83790	1.48900	0.56273	
15	3.8089 ⁻ -03	7.0101 ⁺ +00	1.00000	0.96482	0.70226	0.84970	1.46400	0.58040	
16	4.4453 ⁻ -03	7.3668 ⁺ +00	1.00000	0.96776	0.72126	0.86220	1.42900	0.60336	
17	5.0793 ⁻ -03	7.7262 ⁺ +00	1.00000	0.97030	0.73990	0.87390	1.39500	0.62645	
18	5.7158 ⁻ -03	8.0672 ⁺ +00	1.00000	0.97246	0.75717	0.88430	1.36400	0.64831	
19	6.3497 ⁻ -03	8.3845 ⁺ +00	1.00000	0.97428	0.77092	0.89240	1.34000	0.66597	
20	6.9862 ⁻ -03	8.5888 ⁺ +00	1.00000	0.97618	0.78283	0.89940	1.32000	0.68136	
21	7.6202 ⁻ -03	8.8307 ⁺ +00	1.00000	0.97740	0.79444	0.90580	1.30000	0.69677	
22	8.2542 ⁻ -03	9.1094 ⁺ +00	1.00000	0.97901	0.80762	0.91300	1.27800	0.71440	
23	8.8906 ⁻ -03	9.3221 ⁺ +00	1.00000	0.98043	0.81753	0.91840	1.26200	0.72773	
24	9.5246 ⁻ -03	9.5390 ⁺ +00	1.00000	0.98176	0.82751	0.92370	1.24600	0.74133	
25	1.0161 ⁻ -02	9.7561 ⁺ +00	1.00000	0.98276	0.83738	0.92870	1.23000	0.75504	
26	1.0795 ⁻ -02	9.9717 ⁺ +00	1.00000	0.98411	0.84707	0.93370	1.21500	0.76848	
27	1.1429 ⁻ -02	1.0128 ⁺ +01	1.00000	0.98479	0.85403	0.93710	1.20400	0.77832	
28	1.2066 ⁻ -02	1.0317 ⁺ +01	1.00000	0.98559	0.86234	0.94110	1.19100	0.79018	
29	1.2699 ⁻ -02	1.0499 ⁺ +01	1.00000	0.98661	0.87031	0.94500	1.17900	0.80153	
30	1.3336 ⁻ -02	1.0684 ⁺ +01	1.00000	0.98753	0.87829	0.94880	1.16700	0.81302	
31	1.3970 ⁻ -02	1.0901 ⁺ +01	1.00000	0.98845	0.88761	0.95310	1.15300	0.82663	
32	1.4604 ⁻ -02	1.1115 ⁺ +01	1.00000	0.98972	0.89669	0.95740	1.14000	0.83982	
33	1.5240 ⁻ -02	1.1297 ⁺ +01	1.00000	0.99064	0.90434	0.96090	1.12900	0.85111	
34	1.5874 ⁻ -02	1.1514 ⁺ +01	1.00000	0.99156	0.91338	0.96490	1.11600	0.86461	
35	1.6511 ⁻ -02	1.1735 ⁺ +01	1.00000	0.99238	0.92246	0.96880	1.10300	0.87833	
36	1.7145 ⁻ -02	1.1948 ⁺ +01	1.00000	0.99342	0.93115	0.97240	1.09100	0.89148	
37	1.7779 ⁻ -02	1.2163 ⁺ +01	1.00000	0.99434	0.93988	0.97630	1.07900	0.90482	
38	1.8413 ⁻ -02	1.2382 ⁺ +01	1.00000	0.99515	0.94864	0.97990	1.06700	0.91837	
39	1.9049 ⁻ -02	1.2592 ⁺ +01	1.00000	0.99618	0.95697	0.98340	1.05600	0.93125	
40	1.9686 ⁻ -02	1.2780 ⁺ +01	1.00000	0.99675	0.96437	0.98630	1.04600	0.94293	
41	2.0320 ⁻ -02	1.2972 ⁺ +01	1.00000	0.99733	0.97186	0.98920	1.03600	0.95483	
42	2.0956 ⁻ -02	1.3153 ⁺ +01	1.00000	0.99812	0.97887	0.99200	1.02700	0.96592	
43	2.1590 ⁻ -02	1.3276 ⁺ +01	1.00000	0.99869	0.98363	0.99390	1.02100	0.97346	
44	2.2224 ⁻ -02	1.3373 ⁺ +01	1.00000	0.99879	0.98733	0.99520	1.01600	0.97953	
45	2.2861 ⁻ -02	1.3460 ⁺ +01	1.00000	0.99936	0.99067	0.99660	1.01200	0.98478	
46	2.3495 ⁻ -02	1.3538 ⁺ +01	1.00000	0.99947	0.99443	0.99790	1.00700	0.99096	
47	2.4131 ⁻ -02	1.3647 ⁺ +01	1.00000	1.00004	0.99780	0.99930	1.00300	0.99631	
D 48	2.4765 ⁻ -02	1.3705 ⁺ +01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, DELTA, U/UD, T/TD, P/PD

64010601		CLUTTER		PROFILE TABULATION		42 POINTS, DELTA AT POINT 42			
I	Y	PT2/P	P/PD	T0/T00	M/M0	U/U0	T/T0	RHO/RH00*U/U0	
1	0.0000"+00	1.0000"+00	1.00000	0.90969	0.00000	0.00000	3.01290	0.00000	
2	1.2783"-04	2.4207"+00	1.00000	0.91026	0.35427	0.54155	2.33670	0.23176	
3	2.5356"-04	2.9948"+00	1.00000	0.91077	0.40716	0.60126	2.18065	0.27572	
4	3.8138"-04	3.4474"+00	1.00000	0.91167	0.44382	0.63926	2.07462	0.30814	
5	5.0711"-04	3.7848"+00	1.00000	0.91230	0.46912	0.66387	2.00260	0.33150	
6	6.3474"-04	4.0273"+00	1.00000	0.91300	0.48644	0.68007	1.95459	0.34793	
7	7.6276"-04	4.2330"+00	1.00000	0.91399	0.50063	0.69307	1.91657	0.36162	
8	8.8849"-04	4.4060"+00	1.00000	0.91517	0.51224	0.70357	1.88657	0.37294	
9	1.0163"-03	4.5488"+00	1.00000	0.91662	0.52162	0.71207	1.86356	0.38210	
10	1.1420"-03	4.6661"+00	1.00000	0.91828	0.53048	0.72007	1.84255	0.39080	
11	1.2699"-03	4.8078"+00	1.00000	0.92133	0.53820	0.72757	1.82755	0.39811	
12	1.9048"-03	5.3166"+00	1.00000	0.93306	0.56931	0.75668	1.76653	0.42834	
13	2.5397"-03	5.7190"+00	1.00000	0.94081	0.59268	0.77718	1.71952	0.45197	
14	3.1717"-03	6.0920"+00	1.00000	0.94629	0.61362	0.79428	1.67550	0.47405	
15	3.8096"-03	6.4171"+00	1.00000	0.94991	0.63125	0.80773	1.63749	0.49330	
16	4.4416"-03	6.7506"+00	1.00000	0.95298	0.64683	0.82053	1.59948	0.51303	
17	5.0795"-03	7.0719"+00	1.00000	0.95580	0.66533	0.83213	1.56447	0.53193	
18	5.7144"-03	7.4091"+00	1.00000	0.95868	0.68220	0.84368	1.52446	0.55162	
19	6.3494"-03	7.7300"+00	1.00000	0.96122	0.69787	0.85399	1.49745	0.57029	
20	6.9843"-03	8.0601"+00	1.00000	0.96343	0.71363	0.86389	1.46544	0.58951	
21	7.6192"-03	8.3871"+00	1.00000	0.96577	0.72890	0.87329	1.43543	0.60838	
22	8.2542"-03	8.7759"+00	1.00000	0.96851	0.74664	0.88389	1.40142	0.63071	
23	8.8891"-03	9.2335"+00	1.00000	0.97156	0.76700	0.89559	1.36341	0.65688	
24	9.5240"-03	9.5782"+00	1.00000	0.97384	0.78189	0.90389	1.33640	0.67636	
25	1.0159"-02	1.0036"+01	1.00000	0.97647	0.80146	0.91429	1.30139	0.70255	
26	1.0796"-02	1.0439"+01	1.00000	0.97874	0.81817	0.92289	1.27238	0.72533	
27	1.1431"-02	1.0842"+01	1.00000	0.98077	0.83459	0.93099	1.24437	0.74816	
28	1.2066"-02	1.1289"+01	1.00000	0.98320	0.85282	0.93979	1.21436	0.77390	
29	1.2701"-02	1.1699"+01	1.00000	0.98526	0.86844	0.94709	1.18936	0.79631	
30	1.3336"-02	1.2097"+01	1.00000	0.98717	0.88373	0.95400	1.16535	0.81863	
31	1.3971"-02	1.2441"+01	1.00000	0.98875	0.89674	0.95970	1.14534	0.83791	
32	1.4606"-02	1.2794"+01	1.00000	0.99010	0.90986	0.96520	1.12534	0.85770	
33	1.5241"-02	1.3074"+01	1.00000	0.99151	0.92016	0.96960	1.11033	0.87325	
34	1.5876"-02	1.3391"+01	1.00000	0.99250	0.92842	0.97300	1.09833	0.88584	
35	1.6510"-02	1.3531"+01	1.00000	0.99337	0.93670	0.97630	1.08633	0.89872	
36	1.7145"-02	1.3763"+01	1.00000	0.99411	0.94501	0.97950	1.07432	0.91174	
37	1.7780"-02	1.3985"+01	1.00000	0.99492	0.95215	0.98230	1.06432	0.92294	
38	1.8415"-02	1.4192"+01	1.00000	0.99586	0.96014	0.98540	1.05332	0.93552	
39	1.9050"-02	1.4508"+01	1.00000	0.99712	0.97117	0.98960	1.03831	0.95308	
40	1.9685"-02	1.4830"+01	1.00000	0.99813	0.98222	0.99360	1.02731	0.97097	
41	2.0320"-02	1.5167"+01	1.00000	0.99944	0.99368	0.99780	1.00830	0.98958	
0 42	2.0955"-02	1.5354"+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/U0,T/T0,P/PD

64010602		CLUTTER		PROFILE TABULATION		46 POINTS, DELTA AT POINT 46			
I	Y	PT2/P	P/PO	T0/T0D	H/H0	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	1.33700	0.91003	0.00000	0.00000	2.85500	0.00000	
2	1.2687 ⁻ -04	1.8985 ⁺ +00	1.33500	0.91455	0.30667	0.47400	2.38900	0.26488	
3	2.5375 ⁻ -04	2.4007 ⁺ +00	1.33300	0.91841	0.36636	0.54820	2.23900	0.32637	
4	3.0062 ⁻ -04	2.8387 ⁺ +00	1.33100	0.92559	0.40939	0.59860	2.13800	0.37266	
5	5.0749 ⁻ -04	3.1396 ⁺ +00	1.32900	0.92440	0.43608	0.62620	2.06200	0.40360	
6	6.3436 ⁻ -04	3.4286 ⁺ +00	1.32700	0.92685	0.46010	0.65100	2.00200	0.43151	
7	7.6124 ⁻ -04	3.6305 ⁺ +00	1.32500	0.92928	0.47609	0.66720	1.96400	0.45012	
8	8.8811 ⁻ -04	3.8132 ⁺ +00	1.32300	0.93144	0.49007	0.68100	1.93100	0.46658	
9	1.0150 ⁻ -03	3.9745 ⁺ +00	1.32100	0.93337	0.50207	0.69260	1.90300	0.48078	
10	1.1419 ⁻ -03	4.1211 ⁺ +00	1.31900	0.93593	0.51272	0.70300	1.88000	0.49322	
11	1.2711 ⁻ -03	4.2576 ⁺ +00	1.31700	0.93769	0.52242	0.71210	1.85800	0.50476	
12	1.9054 ⁻ -03	4.4834 ⁺ +00	1.30800	0.94462	0.56209	0.74760	1.76900	0.55278	
13	2.5398 ⁻ -03	5.3438 ⁺ +00	1.29900	0.94967	0.59381	0.77400	1.69900	0.59178	
14	3.1742 ⁻ -03	5.8051 ⁺ +00	1.29000	0.95440	0.62157	0.79600	1.64000	0.62612	
15	3.8109 ⁻ -03	6.2365 ⁺ +00	1.28100	0.95823	0.64643	0.81460	1.58800	0.65712	
16	4.4453 ⁻ -03	6.6257 ⁺ +00	1.27200	0.96157	0.66805	0.83010	1.54400	0.68396	
17	5.0798 ⁻ -03	7.0167 ⁺ +00	1.26300	0.96462	0.68907	0.84450	1.50200	0.71012	
18	5.7140 ⁻ -03	7.4024 ⁺ +00	1.25400	0.96761	0.70719	0.85780	1.46300	0.73526	
19	6.3507 ⁻ -03	7.7960 ⁺ +00	1.24400	0.97033	0.72914	0.87040	1.42500	0.75984	
20	6.9851 ⁻ -03	8.2036 ⁺ +00	1.23500	0.97323	0.74924	0.88270	1.38800	0.78540	
21	7.6174 ⁻ -03	8.6083 ⁺ +00	1.22600	0.97587	0.76867	0.89410	1.35300	0.81017	
22	8.2501 ⁻ -03	9.0234 ⁺ +00	1.21700	0.97851	0.78809	0.90510	1.31900	0.83511	
23	8.8905 ⁻ -03	9.4681 ⁺ +00	1.20800	0.98088	0.80838	0.91600	1.28400	0.86178	
24	9.5249 ⁻ -03	9.8724 ⁺ +00	1.19900	0.98311	0.82638	0.92540	1.25400	0.88481	
25	1.0159 ⁻ -02	1.0282 ⁺ +01	1.19000	0.98527	0.84424	0.93440	1.22500	0.90770	
26	1.0796 ⁻ -02	1.0724 ⁺ +01	1.18100	0.98735	0.86309	0.94350	1.19500	0.93245	
27	1.1430 ⁻ -02	1.1069 ⁺ +01	1.17200	0.98924	0.87752	0.95040	1.17300	0.94959	
28	1.2065 ⁻ -02	1.1452 ⁺ +01	1.16300	0.99082	0.89326	0.95750	1.14900	0.96917	
29	1.2699 ⁻ -02	1.1816 ⁺ +01	1.15400	0.99218	0.90797	0.96390	1.12700	0.98699	
30	1.3336 ⁻ -02	1.2130 ⁺ +01	1.14500	0.99356	0.92043	0.96930	1.10900	1.00077	
31	1.3970 ⁻ -02	1.2472 ⁺ +01	1.13600	0.99505	0.93388	0.97500	1.09000	1.01615	
32	1.4604 ⁻ -02	1.2783 ⁺ +01	1.12700	0.99602	0.94588	0.97980	1.07300	1.02911	
33	1.5239 ⁻ -02	1.3011 ⁺ +01	1.11800	0.99685	0.95462	0.98330	1.06100	1.03613	
34	1.5876 ⁻ -02	1.3222 ⁺ +01	1.10900	0.99753	0.96263	0.98640	1.05000	1.04183	
35	1.6510 ⁻ -02	1.3382 ⁺ +01	1.10000	0.99821	0.96867	0.98880	1.04200	1.04384	
36	1.7144 ⁻ -02	1.3440 ⁺ +01	1.09100	0.99833	0.97085	0.98960	1.03900	1.03913	
37	1.7781 ⁻ -02	1.3440 ⁺ +01	1.08200	0.99833	0.97085	0.98960	1.03900	1.03906	
38	1.8415 ⁻ -02	1.3397 ⁺ +01	1.07300	0.99803	0.96923	0.98890	1.04100	1.01930	
39	1.9050 ⁻ -02	1.3450 ⁺ +01	1.06300	0.99789	0.97122	0.98950	1.03800	1.01333	
40	1.9684 ⁻ -02	1.3529 ⁺ +01	1.05400	0.99809	0.97418	0.99060	1.03400	1.00976	
41	2.0321 ⁻ -02	1.3612 ⁺ +01	1.04500	0.99844	0.97725	0.99180	1.03000	1.00624	
42	2.0955 ⁻ -02	1.3731 ⁺ +01	1.03600	0.99869	0.98169	0.99340	1.02400	1.00504	
43	2.1590 ⁻ -02	1.3853 ⁺ +01	1.02700	0.99908	0.98626	0.99510	1.01800	1.00390	
44	2.2224 ⁻ -02	1.3978 ⁺ +01	1.01800	0.99934	0.99077	0.99670	1.01200	1.00261	
45	2.2861 ⁻ -02	1.4104 ⁺ +01	1.00900	0.99973	0.99542	0.99840	1.00600	1.00138	
D 46	2.3495 ⁻ -02	1.4230 ⁺ +01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PO

64010603		CLUTTER		PROFILE TABULATION		39 POINTS, DELTA AT POINT 39			
I	Y	P12/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000*+00	1.0000*+00	1.22700	0.90839	0.00000	0.00000	2.76528	0.00000	
2	1.2764*+04	2.5630*+00	1.22500	0.91053	0.39163	0.56890	2.11021	0.33025	
3	2.5336*+04	3.5379*+00	1.22300	0.91213	0.47938	0.65890	1.88919	0.42655	
4	3.8100*+04	3.9336*+00	1.22200	0.91417	0.51027	0.68770	1.81618	0.46271	
5	5.0864*+04	4.1816*+00	1.22000	0.91581	0.52869	0.70420	1.77418	0.48424	
6	6.3436*+04	4.3422*+00	1.21700	0.91741	0.54024	0.71450	1.74917	0.49794	
7	7.6200*+04	4.4802*+00	1.21700	0.91924	0.54997	0.73320	1.72917	0.50899	
8	8.8963*+04	4.6192*+00	1.21600	0.92114	0.55897	0.73120	1.71117	0.51961	
9	1.0154*+03	4.7303*+00	1.21400	0.92299	0.56713	0.73840	1.69517	0.52881	
10	1.1430*+03	4.8483*+00	1.21300	0.92450	0.57508	0.74520	1.67917	0.53832	
11	1.2706*+03	4.9558*+00	1.21100	0.92656	0.58220	0.75150	1.66617	0.54620	
12	1.9050*+03	5.4593*+00	1.20400	0.93652	0.61441	0.77940	1.60916	0.58316	
13	2.5394*+03	5.9094*+00	1.19600	0.94767	0.64181	0.80320	1.56616	0.61337	
14	3.1756*+03	6.3298*+00	1.18900	0.95639	0.66636	0.82320	1.52615	0.64134	
15	3.8100*+03	6.7426*+00	1.18100	0.96146	0.68959	0.84010	1.48415	0.66650	
16	4.4444*+03	7.1384*+00	1.17400	0.96550	0.71115	0.85490	1.44514	0.69450	
17	5.0806*+03	7.5048*+00	1.16600	0.96925	0.73052	0.86780	1.41114	0.71705	
18	5.7150*+03	7.8690*+00	1.15900	0.97157	0.74929	0.87930	1.37714	0.74002	
19	6.3494*+03	8.2504*+00	1.15100	0.97452	0.76844	0.89090	1.34413	0.76289	
20	6.9856*+03	8.6278*+00	1.14300	0.97664	0.78692	0.90140	1.31213	0.78521	
21	7.6200*+03	9.0055*+00	1.13600	0.97904	0.80499	0.91150	1.28213	0.80761	
22	8.2544*+03	9.4166*+00	1.12800	0.98170	0.82420	0.92190	1.25113	0.83117	
23	8.8906*+03	9.8429*+00	1.12100	0.98397	0.84366	0.93190	1.22012	0.85619	
24	9.5250*+03	1.0310*+01	1.11300	0.98654	0.86449	0.94230	1.18812	0.88272	
25	1.0139*+02	1.0786*+01	1.10600	0.98895	0.88520	0.95220	1.15712	0.91014	
26	1.0796*+02	1.1270*+01	1.09800	0.99119	0.90576	0.96160	1.12711	0.93676	
27	1.1430*+02	1.1677*+01	1.09100	0.99301	0.92270	0.96910	1.10311	0.95846	
28	1.2064*+02	1.2040*+01	1.08300	0.99473	0.93795	0.97570	1.08211	0.97650	
29	1.2701*+02	1.2381*+01	1.07500	0.99618	0.95128	0.98130	1.06411	0.99135	
30	1.3335*+02	1.2660*+01	1.06800	0.99706	0.96235	0.98570	1.04910	1.00345	
31	1.3969*+02	1.2855*+01	1.06000	0.99787	0.97002	0.98880	1.03910	1.00868	
32	1.4606*+02	1.3031*+01	1.05300	0.99852	0.97691	0.99150	1.03010	1.01354	
33	1.5240*+02	1.3148*+01	1.04500	0.99882	0.98144	0.99320	1.02410	1.01347	
34	1.5874*+02	1.3246*+01	1.03800	0.99904	0.98523	0.99460	1.01910	1.01304	
35	1.6511*+02	1.3324*+01	1.03000	0.99920	0.98827	0.99570	1.01510	1.01031	
36	1.7145*+02	1.3404*+01	1.02300	0.99936	0.99131	0.99680	1.01110	1.00853	
37	1.7779*+02	1.3471*+01	1.01500	0.99954	0.99388	0.99790	1.00810	1.00473	
38	1.8416*+02	1.3549*+01	1.00800	0.99987	0.99686	0.99890	1.00410	1.00278	
39	1.9050*+02	1.3631*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/T0,P/PO

64010604		CLUTTER	PROFILE TABULATION			32 POINTS, DELTA AT POINT 32			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.15100	0.90654	0.00000	0.00000	2.61200	0.00000	
2	1.2706*-04	2.2256*+00	1.15000	0.91142	0.37011	0.53481	2.08800	0.29455	
3	2.5413*-04	3.0713*+00	1.14900	0.91588	0.45852	0.63053	1.89100	0.38312	
4	3.8119*-04	3.7312*+00	1.14700	0.91959	0.51571	0.69534	1.76600	0.44512	
5	5.0825*-04	4.2283*+00	1.14600	0.92323	0.55462	0.71994	1.68500	0.48965	
6	6.3532*-04	4.5180*+00	1.14500	0.92618	0.57003	0.73835	1.64300	0.51455	
7	7.6238*-04	4.7071*+00	1.14300	0.92932	0.58956	0.75015	1.61900	0.52960	
8	8.8944*-04	4.8642*+00	1.14200	0.93207	0.60056	0.75765	1.60000	0.54220	
9	1.0165*-03	5.0013*+00	1.14100	0.93517	0.60999	0.76795	1.58500	0.55283	
10	1.1436*-03	5.1249*+00	1.14000	0.93746	0.61836	0.77506	1.57100	0.56242	
11	1.2706*-03	5.2383*+00	1.13800	0.93991	0.62595	0.78156	1.55900	0.57050	
12	1.4045*-03	5.3581*+00	1.13200	0.94917	0.65955	0.80886	1.50400	0.60080	
13	1.5398*-03	6.2268*+00	1.12500	0.95653	0.68842	0.83097	1.45700	0.64162	
14	1.6744*-03	6.6816*+00	1.11900	0.96381	0.71529	0.85087	1.41500	0.67228	
15	1.8104*-03	7.1145*+00	1.11200	0.96878	0.73995	0.86767	1.37500	0.70171	
16	1.9444*-03	7.5162*+00	1.10500	0.97251	0.76211	0.88188	1.33900	0.72776	
17	2.0796*-03	7.8954*+00	1.09900	0.97533	0.78244	0.89418	1.30600	0.75245	
18	2.2149*-03	8.3068*+00	1.09200	0.97823	0.80392	0.90668	1.27200	0.77638	
19	2.3503*-03	8.7888*+00	1.08600	0.98114	0.82836	0.92018	1.23400	0.80082	
20	2.4856*-03	9.2146*+00	1.07900	0.98417	0.84936	0.93157	1.20300	0.83556	
21	2.6194*-03	9.7423*+00	1.07200	0.98713	0.87468	0.94499	1.16600	0.86835	
22	2.7547*-03	1.0236*+01	1.06600	0.98768	0.89770	0.95549	1.13400	0.89820	
23	2.8901*-03	1.0672*+01	1.05900	0.99187	0.91759	0.96499	1.10600	0.92399	
24	3.0255*-03	1.1090*+01	1.05300	0.99383	0.93622	0.97337	1.08100	0.94818	
25	3.1611*-02	1.1439*+01	1.04600	0.99544	0.95150	0.98010	1.06100	0.96624	
26	3.2975*-02	1.1749*+01	1.03900	0.99648	0.96490	0.98570	1.04400	1.03217	
27	3.4330*-02	1.1973*+01	1.03300	0.99798	0.97443	0.98990	1.03200	0.99086	
28	3.5685*-02	1.2142*+01	1.02600	0.99861	0.98157	0.99280	1.02300	0.99571	
29	3.7041*-02	1.2277*+01	1.02000	0.99917	0.98723	0.99510	1.01600	0.99902	
30	3.8394*-02	1.2414*+01	1.01300	0.99973	0.99294	0.99740	1.00900	1.00135	
31	3.9750*-02	1.2523*+01	1.00700	0.99974	0.99750	0.99900	1.00300	1.00298	
0 32	4.1105*-02	1.2584*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64010605		CLUTTER	PROFILE TABULATION			30 POINTS, DELTA AT POINT 30			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.12400	0.90300	0.00000	0.00000	2.53925	0.00000	
2	1.2668*-04	2.6042*+00	1.12200	0.90481	0.42039	0.58360	1.92719	0.33977	
3	2.5336*-04	3.4135*+00	1.12100	0.90661	0.49836	0.66080	1.75918	0.42132	
4	3.8138*-04	4.1110*+00	1.12000	0.90897	0.57898	0.73010	1.59016	0.51423	
5	5.0806*-04	4.9365*+00	1.11900	0.91172	0.61702	0.76000	1.51715	0.56055	
6	6.3475*-04	5.1596*+00	1.11800	0.91462	0.63245	0.77230	1.49115	0.57900	
7	7.6141*-04	5.2977*+00	1.11700	0.91800	0.64180	0.78230	1.47815	0.58965	
8	8.8944*-04	5.4275*+00	1.11500	0.92177	0.65043	0.78790	1.46715	0.59879	
9	1.0161*-03	5.5484*+00	1.11400	0.92591	0.65845	0.79510	1.45815	0.60744	
10	1.1428*-03	5.6571*+00	1.11300	0.93344	0.66553	0.80310	1.45015	0.61385	
11	1.2675*-03	5.7637*+00	1.11200	0.93883	0.67240	0.81000	1.44515	0.62070	
12	1.4056*-03	6.2906*+00	1.10600	0.95627	0.70536	0.83880	1.41414	0.65603	
13	1.5403*-03	6.7498*+00	1.10000	0.96563	0.73233	0.85940	1.37714	0.68645	
14	1.6751*-03	7.1787*+00	1.09400	0.97080	0.75762	0.87640	1.33813	0.71651	
15	1.8098*-03	7.5739*+00	1.08800	0.97395	0.77973	0.89010	1.30313	0.74316	
16	1.9446*-03	8.0163*+00	1.08200	0.97732	0.80375	0.90440	1.26613	0.77288	
17	2.0796*-03	8.4172*+00	1.07700	0.98002	0.82491	0.91640	1.23412	0.79973	
18	2.2149*-03	8.8405*+00	1.07100	0.98279	0.84667	0.92830	1.20212	0.82705	
19	2.3503*-03	9.2768*+00	1.06500	0.98572	0.86852	0.93990	1.17112	0.85473	
20	2.4856*-03	9.6883*+00	1.05900	0.98819	0.88864	0.95010	1.14311	0.88019	
21	2.6194*-03	1.0089*+01	1.05300	0.99051	0.90781	0.95950	1.11711	0.90443	
22	2.7547*-03	1.0477*+01	1.04700	0.99266	0.92595	0.96810	1.09311	0.92726	
23	2.8901*-03	1.0859*+01	1.04100	0.99437	0.94347	0.97600	1.07011	0.94945	
24	3.0255*-03	1.1189*+01	1.03500	0.99594	0.95842	0.98260	1.05111	0.96754	
25	3.1611*-02	1.1460*+01	1.02900	0.99757	0.97073	0.98810	1.03610	0.98133	
26	3.2975*-02	1.1695*+01	1.02400	0.99843	0.98036	0.99210	1.02410	0.99200	
27	3.4330*-02	1.1830*+01	1.01800	0.99877	0.98669	0.99460	1.01610	0.99646	
28	3.5685*-02	1.1946*+01	1.01200	0.99935	0.99170	0.99670	1.01010	0.99857	
29	3.7041*-02	1.2043*+01	1.00600	0.99991	0.99676	0.99880	1.00410	1.00069	
0 30	3.8394*-02	1.2138*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64011001		CLUTTER	PROFILE TABULATION			35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	0.89990	0.90706	0.00000	0.00000	2.85440	0.00000	
2	1.2713-04	3.0792+00	0.90370	0.85101	0.42996	0.59530	1.91700	0.27970	
3	2.5425-04	3.8993+00	0.90150	0.86577	0.49548	0.66180	1.78400	0.33442	
4	3.8138-04	4.4583+00	0.90220	0.87968	0.53521	0.70070	1.71400	0.36883	
5	5.0851-04	4.8776+00	0.90300	0.89201	0.56311	0.72770	1.67000	0.39348	
6	6.3563-04	5.1633+00	0.90380	0.90424	0.58133	0.74650	1.64900	0.40915	
7	7.6276-04	5.3689+00	0.90460	0.91272	0.59408	0.75940	1.63400	0.42041	
8	8.8989-04	5.5437+00	0.90530	0.91955	0.60470	0.76990	1.62100	0.42998	
9	1.0158-03	5.7092+00	0.90610	0.92482	0.61459	0.77910	1.60700	0.43929	
10	1.1425-03	5.8589+00	0.90690	0.92977	0.62339	0.78730	1.59500	0.44765	
11	1.2696-03	5.9941+00	0.90760	0.93457	0.63123	0.79470	1.58500	0.45506	
12	1.9053-03	6.5185+00	0.9150	0.94934	0.66075	0.82050	1.54200	0.48501	
13	2.5392-03	6.9282+00	0.91530	0.95649	0.68291	0.83750	1.50400	0.50968	
14	3.1749-03	7.2682+00	0.91920	0.96094	0.70076	0.85020	1.47200	0.53091	
15	3.8105-03	7.5478+00	0.92300	0.96399	0.71510	0.85990	1.44600	0.54388	
16	4.4445-03	7.8023+00	0.92690	0.96591	0.72790	0.86800	1.42200	0.56579	
17	5.0801-03	8.0634+00	0.93070	0.96768	0.74080	0.87590	1.39800	0.58312	
18	5.7158-03	8.3385+00	0.93460	0.96978	0.75415	0.88400	1.37400	0.60130	
19	6.3477-03	8.6477+00	0.93840	0.97206	0.76888	0.89270	1.34800	0.62145	
20	6.9854-03	8.9893+00	0.94230	0.97413	0.78483	0.90170	1.32000	0.64369	
21	7.6194-03	9.3740+00	0.94610	0.97664	0.80244	0.91140	1.29000	0.66883	
22	8.2550-03	9.8057+00	0.95000	0.97922	0.82168	0.92160	1.25800	0.69596	
23	8.8906-03	1.0331+01	0.95380	0.98214	0.84453	0.93320	1.22100	0.72898	
24	9.5246-03	1.0877+01	0.95770	0.98518	0.86765	0.94450	1.18500	0.76333	
25	1.0160-02	1.1404+01	0.96150	0.98777	0.88940	0.95460	1.15200	0.79674	
26	1.0794-02	1.1948+01	0.96540	0.99043	0.91127	0.96440	1.12000	0.83128	
27	1.1430-02	1.2500+01	0.96920	0.99274	0.93297	0.97360	1.08900	0.86650	
28	1.2066-02	1.2970+01	0.97310	0.99466	0.95104	0.98100	1.06400	0.89719	
29	1.2699-02	1.3391+01	0.97690	0.99672	0.96693	0.98750	1.04300	0.92492	
30	1.3335-02	1.3733+01	0.98080	0.99890	0.97965	0.99230	1.02600	0.94858	
31	1.3971-02	1.4035+01	0.98460	0.99932	0.99077	0.99670	1.01200	0.96971	
32	1.4605-02	1.4182+01	0.98850	0.99968	0.99611	0.99860	1.00500	0.98221	
33	1.5240-02	1.4248+01	0.99230	0.99995	0.99850	0.99950	1.00200	0.98982	
34	1.5874-02	1.4289+01	0.99620	1.00000	1.00000	1.00000	1.00000	0.99620	
D 35	1.6510-02	1.4289+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64011002		CLUTTER	PROFILE TABULATION			35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	0.86140	0.91479	0.00000	0.00000	2.90600	0.00000	
2	1.2713-04	3.1007+00	0.86250	0.86173	0.42880	0.59950	1.95500	0.26451	
3	2.5425-04	4.4025+00	0.86350	0.87102	0.54433	0.71377	1.65800	0.37174	
4	3.8138-04	5.3018+00	0.86460	0.87969	0.58951	0.74357	1.59100	0.40408	
5	5.0851-04	5.6649+00	0.86570	0.88809	0.60767	0.74998	1.56400	0.42066	
6	6.3563-04	5.8995+00	0.86670	0.89397	0.62139	0.77188	1.54300	0.43356	
7	7.6276-04	6.0784+00	0.86780	0.90401	0.63164	0.78308	1.53700	0.44213	
8	8.8989-04	6.2299+00	0.86890	0.91243	0.64018	0.79233	1.53200	0.44941	
9	1.0154-03	6.3850+00	0.86990	0.92053	0.64881	0.80148	1.52600	0.45689	
10	1.1425-03	6.5106+00	0.87100	0.92690	0.65571	0.80868	1.52100	0.46309	
11	1.2696-03	6.6436+00	0.87210	0.93314	0.66294	0.81598	1.51500	0.46971	
12	1.9053-03	7.2170+00	0.87740	0.95196	0.69323	0.84278	1.47800	0.50031	
13	2.5392-03	7.6732+00	0.88270	0.95904	0.71640	0.85939	1.43900	0.52716	
14	3.1749-03	8.0531+00	0.88810	0.96325	0.73514	0.87169	1.40600	0.55060	
15	3.8105-03	8.3534+00	0.89340	0.96575	0.74961	0.88059	1.38000	0.57009	
16	4.4445-03	8.6346+00	0.89870	0.96765	0.76291	0.88839	1.35600	0.58879	
17	5.0801-03	8.9192+00	0.90410	0.96982	0.77613	0.89609	1.33300	0.60777	
18	5.7158-03	9.1863+00	0.90940	0.97172	0.78834	0.90297	1.31200	0.62590	
19	6.3477-03	9.4612+00	0.91470	0.97356	0.80072	0.90979	1.29100	0.64461	
20	6.9854-03	9.7370+00	0.92000	0.97565	0.81293	0.91649	1.27100	0.66339	
21	7.6194-03	1.0016+01	0.92540	0.97742	0.82513	0.92249	1.25100	0.68269	
22	8.2550-03	1.0330+01	0.93070	0.97913	0.83862	0.92969	1.22900	0.70404	
23	8.8906-03	1.0738+01	0.93600	0.98163	0.85593	0.93829	1.20200	0.73065	
24	9.5246-03	1.1197+01	0.94140	0.98426	0.87475	0.94739	1.17300	0.76034	
25	1.0160-02	1.1613+01	0.94670	0.98670	0.89159	0.95530	1.14800	0.78779	
26	1.0794-02	1.2145+01	0.95200	0.98917	0.91268	0.96460	1.11700	0.82211	
27	1.1430-02	1.2585+01	0.95740	0.99144	0.92973	0.97200	1.09300	0.85141	
28	1.2066-02	1.3038+01	0.96270	0.99338	0.94697	0.97910	1.06400	0.88174	
29	1.2699-02	1.3435+01	0.96800	0.99516	0.96182	0.98510	1.04900	0.90903	
30	1.3335-02	1.3740+01	0.97330	0.99639	0.97309	0.98950	1.03400	0.93141	
31	1.3971-02	1.4015+01	0.97870	0.99759	0.98313	0.99340	1.02100	0.95224	
32	1.4605-02	1.4153+01	0.98400	0.99857	0.98812	0.99550	1.01500	0.96510	
33	1.5240-02	1.4259+01	0.98930	0.99991	0.99195	0.99690	1.01000	0.97647	
34	1.5874-02	1.4372+01	0.99470	0.99992	0.99601	0.99850	1.00500	0.98827	
D 35	1.6510-02	1.4484+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64011003		CLUTTER	PROFILE TABULATION			35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	0.93290	0.90942	0.00000	0.00000	3.10831	0.00000	
2	1.2713-04	3.7850+00	0.93340	0.92273	0.45874	0.66323	2.09021	0.29617	
3	2.5425-04	5.4096+00	0.93380	0.93471	0.56208	0.75645	1.81118	0.39001	
4	3.8138-04	6.0630+00	0.93430	0.94568	0.59847	0.74766	1.73217	0.42445	
5	5.0851-04	6.4620+00	0.93480	0.95525	0.61962	0.80626	1.69317	0.44514	
6	6.3563-04	6.7793+00	0.93530	0.96182	0.63592	0.81956	1.66217	0.46134	
7	7.6276-04	7.0796+00	0.93570	0.96801	0.65097	0.83217	1.63416	0.47649	
8	8.8824-04	7.3496+00	0.93620	0.97302	0.66421	0.84257	1.60916	0.49020	
9	1.0154-03	7.5041+00	0.93670	0.97730	0.67549	0.85127	1.58816	0.50208	
10	1.1425-03	7.6163+00	0.93720	0.98096	0.68648	0.85937	1.56716	0.51393	
11	1.2696-03	8.0258+00	0.93760	0.98449	0.69624	0.86657	1.54915	0.52448	
12	1.9053-03	8.8999+00	0.94000	0.99735	0.73596	0.89398	1.47715	0.56889	
13	2.5392-03	9.5693+00	0.94240	1.00517	0.76429	0.91208	1.42414	0.60355	
14	3.1749-03	1.0081+01	0.94470	1.01138	0.78554	0.92519	1.38714	0.63009	
15	3.8105-03	1.0486+01	0.94710	1.01526	0.80195	0.93459	1.35814	0.65174	
16	4.4445-03	1.0841+01	0.94940	1.01866	0.81306	0.94259	1.33413	0.67077	
17	5.0801-03	1.1164+01	0.95180	1.02056	0.82869	0.94869	1.31113	0.68884	
18	5.7158-03	1.1492+01	0.95420	1.02198	0.84132	0.95449	1.28713	0.70760	
19	6.3497-03	1.1808+01	0.95650	1.02303	0.85332	0.95979	1.26513	0.72565	
20	6.9854-03	1.2130+01	0.95890	1.02066	0.86539	0.96409	1.24112	0.74486	
21	7.6194-03	1.2460+01	0.96120	1.01783	0.87777	0.96759	1.21512	0.76540	
22	8.2530-03	1.2893+01	0.96360	1.01492	0.89293	0.97289	1.18712	0.78971	
23	8.8906-03	1.3235+01	0.96600	1.01184	0.90551	0.97700	1.16412	0.81072	
24	9.5246-03	1.3606+01	0.96830	1.00859	0.91859	0.98170	1.14211	0.83230	
25	1.0160-02	1.3962+01	0.97070	1.00449	0.93097	0.98530	1.12011	0.85387	
26	1.0794-02	1.4339+01	0.97310	1.00136	0.94388	0.98910	1.09811	0.87650	
27	1.1430-02	1.4612+01	0.97540	1.00105	0.95314	0.99150	1.08211	0.89373	
28	1.2066-02	1.4935+01	0.97890	1.00185	0.96398	0.99440	1.06411	0.91477	
29	1.2699-02	1.5242+01	0.98120	1.00126	0.97414	0.99730	1.04810	0.93364	
30	1.3335-02	1.5492+01	0.98360	1.00056	0.98239	0.99900	1.03410	0.95021	
31	1.3971-02	1.5684+01	0.98590	1.00076	0.98865	1.00000	1.02310	0.96364	
32	1.4605-02	1.5810+01	0.98870	1.00470	0.99273	1.00020	1.01510	0.97419	
33	1.5240-02	1.5898+01	0.99300	1.00280	0.99558	1.00010	1.00910	0.98414	
34	1.5874-02	1.5978+01	0.99570	1.00148	0.99816	1.00020	1.00410	0.99183	
D 35	1.6510-02	1.6036+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

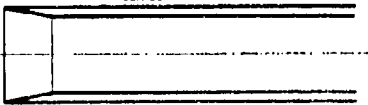
INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64011004		CLUTTER	PROFILE TABULATION			35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	0.99140	0.90881	0.00000	0.00000	3.13231	0.00000	
2	1.2713-04	3.2517+00	0.99140	0.90106	0.41580	0.61460	2.18522	0.27886	
3	2.5425-04	4.7262+00	0.99140	0.90715	0.51736	0.71147	1.89119	0.37297	
4	3.8138-04	5.5153+00	0.99140	0.91242	0.56391	0.75028	1.77018	0.42020	
5	5.0851-04	6.0396+00	0.99140	0.91774	0.59278	0.77338	1.70217	0.45044	
6	6.3563-04	6.3776+00	0.99140	0.92323	0.61064	0.78798	1.66517	0.46914	
7	7.6276-04	6.6679+00	0.99140	0.92860	0.62557	0.80018	1.63616	0.48485	
8	8.8824-04	6.9310+00	0.99140	0.93297	0.63880	0.81058	1.61016	0.49909	
9	1.0154-03	7.1894+00	0.99140	0.93697	0.65192	0.82023	1.58516	0.51303	
10	1.1425-03	7.4392+00	0.99140	0.94098	0.66358	0.82938	1.56216	0.52636	
11	1.2696-03	7.6722+00	0.99140	0.94514	0.67463	0.83778	1.54215	0.53858	
12	1.9053-03	8.6833+00	0.99140	0.95750	0.72062	0.86899	1.45415	0.59245	
13	2.5392-03	9.5266+00	0.99140	0.96679	0.75683	0.89169	1.38814	0.63684	
14	3.1749-03	1.0198+01	0.99140	0.97319	0.78447	0.90779	1.33913	0.67206	
15	3.8105-03	1.0702+01	0.99140	0.97734	0.80456	0.91879	1.30413	0.69847	
16	4.4445-03	1.1157+01	0.99140	0.98017	0.82227	0.92779	1.27313	0.72248	
17	5.0801-03	1.1535+01	0.99140	0.98220	0.83673	0.93479	1.24012	0.74252	
18	5.7158-03	1.1873+01	0.99140	0.98355	0.84945	0.94059	1.22612	0.76053	
19	6.3497-03	1.2193+01	0.99140	0.98487	0.86129	0.94589	1.20612	0.77750	
20	6.9854-03	1.2512+01	0.99140	0.98638	0.87292	0.95110	1.18712	0.79429	
21	7.6194-03	1.2823+01	0.99140	0.98781	0.88415	0.95600	1.16912	0.81068	
22	8.2530-03	1.3194+01	0.99140	0.98922	0.89734	0.96150	1.14811	0.83025	
23	8.8906-03	1.3523+01	0.99140	0.99045	0.90888	0.96620	1.13011	0.84760	
24	9.5246-03	1.3921+01	0.99140	0.99194	0.92266	0.97170	1.10911	0.86657	
25	1.0160-02	1.4158+01	0.99140	0.99289	0.93075	0.97490	1.09711	0.88096	
26	1.0794-02	1.4416+01	0.99140	0.99371	0.93949	0.97820	1.08411	0.89455	
27	1.1430-02	1.4730+01	0.99140	0.99508	0.95002	0.98230	1.06911	0.91090	
28	1.2066-02	1.5110+01	0.99140	0.99630	0.96261	0.98690	1.05111	0.93054	
29	1.2699-02	1.5434+01	0.99140	0.99716	0.97319	0.99060	1.03610	0.94766	
30	1.3335-02	1.5641+01	0.99230	0.99807	0.97991	0.99310	1.02710	0.95993	
31	1.3971-02	1.5840+01	0.99400	0.99844	0.98631	0.99520	1.01810	0.97164	
32	1.4605-02	1.5981+01	0.99520	0.99896	0.99082	0.99680	1.01210	0.98015	
33	1.5240-02	1.6048+01	0.99640	0.99936	0.99457	0.99810	1.00710	0.98749	
34	1.5874-02	1.6217+01	0.99820	0.99976	0.99835	0.99940	1.00210	0.99551	
D 35	1.6510-02	1.6269+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

64011005		CLUTTER	PROFILE TABULATION			43 POINTS, DELTA AT POINT 43			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.00000	0.91229	0.00000	0.00000	3.02400	0.00000	
2	1.2738*-04	2.5503*+00	1.00000	0.86764	0.36681	0.54320	2.19300	0.24770	
3	2.5476*-04	3.4743*+00	1.00000	0.87676	0.44363	0.62880	1.99100	0.31582	
4	3.7998*-04	4.1701*+00	1.00000	0.88593	0.49604	0.67850	1.87100	0.36264	
5	5.0736*-04	4.6021*+00	1.00000	0.89411	0.52477	0.70600	1.81000	0.39006	
6	6.3475*-04	4.9793*+00	1.00000	0.90278	0.54850	0.72850	1.76400	0.41298	
7	7.6213*-04	5.2971*+00	1.00000	0.90984	0.56782	0.74620	1.72700	0.43208	
8	8.8951*-04	5.5999*+00	1.00000	0.91612	0.58556	0.76190	1.69300	0.45003	
9	1.0169*-03	5.8736*+00	1.00000	0.92134	0.60113	0.77520	1.66300	0.46615	
10	1.1421*-03	6.1165*+00	1.00000	0.92623	0.61461	0.78660	1.63800	0.48022	
11	1.2695*-03	6.3445*+00	1.00000	0.93057	0.62699	0.79880	1.61500	0.49337	
12	1.9042*-03	7.2946*+00	1.00000	0.94565	0.67612	0.83440	1.52300	0.54787	
13	2.5390*-03	8.0742*+00	1.00000	0.95675	0.71387	0.86110	1.45500	0.59182	
14	3.1759*-03	8.7514*+00	1.00000	0.96443	0.74510	0.88130	1.39900	0.62995	
15	3.8106*-03	9.3422*+00	1.00000	0.97098	0.77130	0.89750	1.35400	0.66285	
16	4.4454*-03	9.8422*+00	1.00000	0.98869	0.79279	0.90670	1.30800	0.69320	
17	5.0801*-03	1.0292*+01	1.00000	0.97803	0.81164	0.91970	1.28400	0.71628	
18	5.7149*-03	1.0707*+01	1.00000	0.98038	0.82864	0.92830	1.25500	0.73968	
19	6.3496*-03	1.1077*+01	1.00000	0.98221	0.84351	0.93550	1.23000	0.76057	
20	6.9844*-03	1.1399*+01	1.00000	0.98374	0.85626	0.94150	1.20900	0.77874	
21	7.6191*-03	1.1708*+01	1.00000	0.98552	0.86830	0.94720	1.19000	0.79597	
22	8.2560*-03	1.2033*+01	1.00000	0.98679	0.88077	0.95270	1.17000	0.81427	
23	8.8908*-03	1.2307*+01	1.00000	0.98810	0.89114	0.95730	1.15400	0.82955	
24	9.5255*-03	1.2573*+01	1.00000	0.98947	0.90111	0.96170	1.13900	0.84434	
25	1.0160*-02	1.2892*+01	1.00000	0.99064	0.91294	0.96660	1.12100	0.86227	
26	1.0795*-02	1.3264*+01	1.00000	0.99218	0.92654	0.97220	1.10100	0.88302	
27	1.1430*-02	1.3634*+01	1.00000	0.99380	0.93983	0.97760	1.08200	0.90351	
28	1.2064*-02	1.3913*+01	1.00000	0.99492	0.94974	0.98150	1.06800	0.91901	
29	1.2699*-02	1.4154*+01	1.00000	0.99569	0.95823	0.98470	1.05600	0.93248	
30	1.3334*-02	1.4360*+01	1.00000	0.99639	0.96544	0.98740	1.04600	0.94398	
31	1.3971*-02	1.4552*+01	1.00000	0.99713	0.97208	0.98990	1.03700	0.95458	
32	1.4606*-02	1.4702*+01	1.00000	0.99765	0.97725	0.99180	1.03000	0.96291	
33	1.5240*-02	1.4814*+01	1.00000	0.99822	0.98111	0.99330	1.02500	0.96907	
34	1.5875*-02	1.4965*+01	1.00000	0.99860	0.98626	0.99510	1.01800	0.97750	
35	1.6510*-02	1.5078*+01	1.00000	0.99904	0.99009	0.99650	1.01300	0.98371	
36	1.7145*-02	1.5145*+01	1.00000	0.99925	0.99235	0.99730	1.01000	0.98743	
37	1.7779*-02	1.5171*+01	1.00000	0.99951	0.99324	0.99770	1.00900	0.98880	
38	1.8414*-02	1.5212*+01	1.00000	0.99946	0.99462	0.99810	1.00700	0.99116	
39	1.9051*-02	1.5238*+01	1.00000	0.99972	0.99552	0.99850	1.00600	0.99254	
40	1.9686*-02	1.5280*+01	1.00000	0.99967	0.99691	0.99890	1.00400	0.99492	
41	2.0321*-02	1.5309*+01	1.00000	1.00007	0.99790	0.99940	1.00300	0.99641	
42	2.0955*-02	1.5351*+01	1.00000	1.00002	0.99930	0.99980	1.00100	0.99880	
D 43	2.1590*-02	1.5372*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD,P/PD

axisymmetric 	M : 6 R THETA X 10 ⁻³ : 2 - 15 TW/TR : 1	6501
		ZPG - AW
Windtunnel: blow-down but effectively continuous, running time up to 45 minutes with 10 minutes settling time. W = 0.51, H = 0.52 m. PO : 3.6 MN/m ² TO : 480 K. Air, Dew point 186 K. RE/m X 10 ⁻⁶ : 33.		
ADCOCK J.B., PETERSON J.B. and McREE D.I. 1965. Experimental investigation of a turbulent boundary layer at Mach 6, high Reynolds' numbers, and zero heat transfer. NASA TN D-2907. And Peterson J.B. private communication. Also: Samuels, Peterson and Adcock (1967) CAT 6701.		

- 1 The test boundary layer was formed on the exterior of a hollow cylindrical model. The leading edge ($X = 0$) was chamfered at 15° from the outer, test surface ($D = 152.4$ mm) to the hollow interior ($D = 127$ mm). From $X = 0$ to $X = 1.07$ m the diameter was constant. The model then flared out at 20° to a diameter of 203 mm which remained constant to the end of the model at $X = 1.22$ m. The model was supported on the tunnel floor by two pairs of sloping supports at approximately $X = 0.8$ and 1.15 m. Measurements were made on the top generator. The model surface roughness was less than $0.8 \mu\text{m}$. For this experiment the model was
- 2 not actively cooled. There was a slight increase in Mach number along the test surface (see section B)
- 3 but departures from the mean gradient were no greater than 0.33 %. A boundary layer trip could be placed at $X = 29$ mm. This consisted of 1.9 mm diameter rods 0.64 mm high spaced round the periphery at intervals of about 6.4 mm. Schlieren photographs were taken in order to show the boundary layer development for both
- 5 natural and forced transition. After final alignment, the incidence determined from the static pressure distribution around the circumference was less than -0.05° and the angle of yaw less than 0.10° .
- 6 Static pressure holes ($d = 1.02$ mm) were located circumferentially at intervals of 90° for X values
- 8 457, 660 and 864 mm, with an additional tapping on the top generator only at $X = 254$ mm. Five swaged copper-constantan thermocouples were welded to the inner side of the outer surface of the model at
- 7 $X = 152, 366, 762$ and 965 mm. The Pitot tube was a FPP ($h_1 = 0.178, h_2 = 0.076, b_1 = 0.69, l = 12.7$ mm)
- 8 and was carried by a traverse gear attached to the tunnel wall. Surveys were made at $X = 127, 152, 203, 279, 838, 940$ and 1016 mm. At $X = 838$ mm a total temperature survey was made using a STP ($d_1 =$ approximately 0.51, $l = 9.5$ mm) containing a chromel-alumel thermocouple. This was directly calibrated over the greater part of the test range, with an interpolation between the calibration and the free stream reading for the upper unit Reynolds numbers.
- 9 Wall temperature is implicitly interpolated to the boundary layer traverse stations by the authors. The authors have taken the total temperature distribution, scaled on δ , to be the same for all values of X . The value of δ is defined by extrapolation to the free stream value of a near linear PT2 variation in the outer part of the layer. The scaled T_0 variation has then been interpolated to the appropriate Y values of the Pitot profiles. The static pressure has been assumed constant through the layer.
- 12 The editors have accepted the authors' interpolations and prepared the tables using the given U/UD and M/MD data, with the assumption of zero normal pressure gradient. The authors have calculated mean and local wall shear stress values from a longitudinal momentum balance. These have not been presented here.
- 13 The profiles presented were all obtained with forced transition except for one (0201) at $X = 279$ mm for which transition was natural. There is one duplicate (0107 A). Except for 0105 the total temperature data is assumed. The wall temperatures have been determined by the editors from the original data used to prepare the authors' graphical presentation of an "adiabatic recovery factor".
- 6 DATA: 6501 0101-0201. Pitot profiles. One T_0 profile used for all test cases. $NX = 7$.
- 15 Editors' comments
 The entry describes the AW results obtained on the model also used, with a cooled wall, for Samuels et al. - CAT 6701. The experimental range overlaps the results of Danberg - CAT 6702 and Fischer & Maddalon - CAT 7103.

The profiles are given in moderately close detail. Some substantial corrections appear necessary close to the wall for profiles 0106 and 0107. It must be emphasized that the T0 profile is assumed for all profiles except 0105. This measured profile appears to agree closely with the Crocco / Van Driest temperature-velocity correlation.

CAT 6501		ADCOCK		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	MD *	TW/TR	RE02W	CF	H12	H12K	PH	PD		
X *	PO0*	PH/PD*	RE02D	CR	H32	H32K	TW*	TD		
RZ *	T00*	SW *	D2	PI2*	H42	D2K	UD	TR		
65010101	5.9500	0.9875	3.6382 ⁺⁰²	NM	18.5546	1.4050	2.4043 ⁺⁰³	2.4043 ⁺⁰³		
1.2700 ⁻⁰¹	3.6060 ⁺⁰⁶	1.0000	2.0582 ⁺⁰³	NM	1.8851	1.8359	4.3778 ⁺⁰²	6.0365 ⁺⁰¹		
7.6200 ⁻⁰²	4.8778 ⁺⁰²	0.0000	6.9280 ⁻⁰⁵	0.0000 ⁺⁰⁰	-0.2333	1.7070 ⁻⁰⁴	9.2687 ⁺⁰²	4.4333 ⁺⁰²		
65010102	5.9500	0.9865	5.1944 ⁺⁰²	NM	17.2603	1.3501	2.4043 ⁺⁰³	2.4043 ⁺⁰³		
1.5240 ⁻⁰¹	3.6060 ⁺⁰⁶	1.0000	2.9425 ⁺⁰³	NM	1.8656	1.8163	4.3433 ⁺⁰²	5.9952 ⁺⁰¹		
7.6200 ⁻⁰²	4.8444 ⁺⁰²	0.0000	9.8025 ⁻⁰⁵	0.0000 ⁺⁰⁰	-0.0923	2.5275 ⁻⁰⁴	9.2370 ⁺⁰²	4.4030 ⁺⁰²		
65010103	5.9500	0.9865	6.5242 ⁺⁰²	NM	17.6594	1.3324	2.3859 ⁺⁰³	2.3859 ⁺⁰³		
2.0320 ⁻⁰¹	3.5784 ⁺⁰⁶	1.0000	3.6970 ⁺⁰³	NM	1.8660	1.8178	4.3383 ⁺⁰²	5.9884 ⁺⁰¹		
7.6200 ⁻⁰²	4.8389 ⁺⁰²	0.0000	1.2390 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1489	3.2243 ⁻⁰⁴	9.2317 ⁺⁰²	4.3979 ⁺⁰²		
65010104	5.9600	0.9856	6.9252 ⁺⁰²	NM	16.6246	1.3007	2.3796 ⁺⁰³	2.3796 ⁺⁰³		
2.7940 ⁻⁰¹	3.6060 ⁺⁰⁶	1.0000	5.0677 ⁺⁰³	NM	1.8603	1.8209	4.3394 ⁺⁰²	5.9776 ⁺⁰¹		
7.6200 ⁻⁰²	4.8444 ⁺⁰²	0.0000	1.6953 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.0335	4.4368 ⁻⁰⁴	9.2389 ⁺⁰²	4.4028 ⁺⁰²		
65010105	6.0200	0.9807	2.1444 ⁺⁰³	NM	15.9150	1.2545	2.2376 ⁺⁰³	2.2376 ⁺⁰³		
8.3820 ⁻⁰¹	3.6060 ⁺⁰⁶	1.0000	1.2351 ⁺⁰⁴	NM	1.8495	1.8121	4.3117 ⁺⁰²	5.8667 ⁺⁰¹		
7.6200 ⁻⁰²	4.8389 ⁺⁰²	0.0000	4.2294 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0348	1.1458 ⁻⁰³	9.2449 ⁺⁰²	4.3967 ⁺⁰²		
65010106	6.0200	0.9796	2.1758 ⁺⁰³	NM	16.1528	1.2546	2.2376 ⁺⁰³	2.2376 ⁺⁰³		
9.3980 ⁻⁰¹	3.6060 ⁺⁰⁶	1.0000	1.2539 ⁺⁰⁴	NM	1.8511	1.8120	4.2872 ⁺⁰²	5.8397 ⁺⁰¹		
7.6200 ⁻⁰²	4.8147 ⁺⁰²	0.0000	4.2641 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0037	1.1537 ⁻⁰³	9.2237 ⁺⁰²	4.3765 ⁺⁰²		
65010107	6.0200	0.9798	2.3177 ⁺⁰³	NM	15.9606	1.2397	2.2414 ⁺⁰³	2.2414 ⁺⁰³		
1.0160 ⁺⁰⁰	3.6128 ⁺⁰⁶	1.0000	1.3341 ⁺⁰⁴	NM	1.8532	1.8164	4.3078 ⁺⁰²	5.8667 ⁺⁰¹		
7.6200 ⁻⁰²	4.8389 ⁺⁰²	0.0000	4.9594 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0167	1.2213 ⁻⁰³	9.2449 ⁺⁰²	4.3967 ⁺⁰²		
65010107A	6.0200	0.9797	2.2583 ⁺⁰³	NM	16.5266	1.2479	2.2376 ⁺⁰³	2.2376 ⁺⁰³		
1.0160 ⁺⁰⁰	3.6060 ⁺⁰⁶	1.0000	1.3042 ⁺⁰⁴	NM	1.8542	1.8177	4.2578 ⁺⁰²	5.7993 ⁺⁰¹		
7.6200 ⁻⁰²	4.7833 ⁺⁰²	0.0000	4.3889 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.0464	1.1912 ⁻⁰³	9.1917 ⁺⁰²	4.3462 ⁺⁰²		
65010201	5.9600	0.9855	7.6539 ⁺⁰²	NM	17.3812	1.2859	2.3842 ⁺⁰³	2.3842 ⁺⁰³		
2.7940 ⁻⁰¹	3.6128 ⁺⁰⁶	1.0000	4.4426 ⁺⁰³	NM	1.8685	1.8284	4.3939 ⁺⁰²	6.0530 ⁺⁰¹		
7.6200 ⁻⁰²	4.9056 ⁺⁰²	0.0000	1.5117 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1271	3.9446 ⁻⁰⁴	9.2970 ⁺⁰²	4.4583 ⁺⁰²		

65010101 ADCOCK			PROFILE TABULATION						17 POINTS, DELTA AT POINT 17	
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD		
1	0.0000*+00	1.0000*+00	NM	0.92821	0.00000	0.00000	7.50037	0.00000		
2	8.8900*-05	3.9969*+00	NM	0.95108	0.27674	0.61776	4.98306	0.12397		
3	2.3066*-04	5.9585*+00	NM	0.96584	0.34642	0.71158	4.21932	0.16665		
4	2.3876*-04	8.0770*+00	NM	0.97592	0.40824	0.77645	3.61731	0.21465		
5	3.0734*-04	1.0132*+01	NM	0.98766	0.46026	0.82236	3.19243	0.25760		
6	4.1148*-04	1.1981*+01	NM	0.99492	0.50245	0.85329	2.86407	0.29586		
7	5.5372*-04	1.5035*+01	NM	1.00586	0.56526	0.89222	2.49140	0.35812		
8	7.3152*-04	1.6857*+01	NM	1.00995	0.59961	0.90968	2.30167	0.39523		
9	9.4488*-04	1.8449*+01	NM	1.03505	0.62807	0.93263	2.20502	0.42296		
10	1.3208*-03	2.3224*+01	NM	1.01794	0.70658	0.95160	1.81380	0.52464		
11	1.6967*-03	2.8771*+01	NM	1.01626	0.78803	0.97206	1.52160	0.63884		
12	2.0142*-03	3.2857*+01	NM	1.01300	0.84298	0.98204	1.35712	0.72362		
13	2.4486*-03	3.9335*+01	NM	1.00512	0.92345	0.99202	1.15400	0.85963		
14	2.9769*-03	4.4012*+01	NM	1.00077	0.97743	0.99750	1.04150	0.95776		
15	3.5210*-03	4.5511*+01	NM	0.99947	0.99411	0.99900	1.00986	0.98925		
16	4.1580*-03	4.5867*+01	NM	0.99949	0.99804	0.99950	1.00294	0.99658		
D 17	5.0749*-03	4.6046*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000		

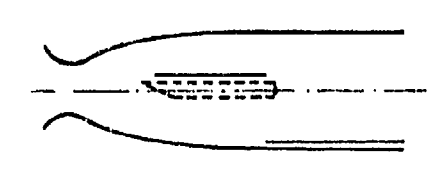
INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD
AT I=2 DATA WERE AVERAGED

65010104 ADCOCK			PROFILE TABULATION						18 POINTS, DELTA AT POINT 18	
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD		
1	0.0000*+00	1.0000*+00	NM	0.88593	0.00000	0.00000	7.17983	0.00000		
2	8.8900*-05	4.0064*+00	NM	0.92697	0.27666	0.61031	4.86633	0.12541		
3	1.7272*-04	4.2883*+00	NM	0.92853	0.28773	0.62631	4.73831	0.13218		
4	2.8448*-04	4.9154*+00	NM	0.93330	0.31087	0.65833	4.48479	0.14679		
5	3.9370*-04	6.7194*+00	NM	0.94655	0.36922	0.72886	3.89703	0.18703		
6	5.9944*-04	8.2609*+00	NM	0.95564	0.41247	0.77239	3.50650	0.22027		
7	1.0287*-03	1.0787*+01	NM	0.97243	0.47485	0.82641	3.02889	0.27284		
8	1.2878*-03	1.1861*+01	NM	0.97958	0.49899	0.84492	2.86710	0.29470		
9	1.5646*-03	1.3230*+01	NM	0.98556	0.52817	0.86443	2.67865	0.32271		
10	2.2073*-03	1.6897*+01	NM	0.99770	0.59859	0.90393	2.28050	0.39638		
11	2.8524*-03	2.1309*+01	NM	1.00730	0.67505	0.93697	1.92654	0.48635		
12	3.4874*-03	2.6504*+01	NM	1.01284	0.75453	0.96248	1.62718	0.59150		
13	4.1783*-03	3.2431*+01	NM	1.01246	0.83602	0.98049	1.37549	0.71283		
14	4.8412*-03	3.7875*+01	NM	1.00700	0.90443	0.99999	1.19817	0.82625		
15	5.5829*-03	4.2328*+01	NM	1.00333	0.95674	0.99600	1.08375	0.91903		
16	6.0579*-03	4.4558*+01	NM	1.00158	0.98189	0.99850	1.03411	0.96556		
17	6.8504*-03	4.6107*+01	NM	0.99925	0.99899	0.99950	1.00101	0.99849		
D 18	7.4498*-03	4.6199*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000		

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD
AT I=2 DATA WERE AVERAGED

65010107 ADCOCK			PROFILE TABULATION						23 POINTS, DELTA AT POINT 23	
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD		
1	0.0000*+00	1.0000*+00	NM	0.88668	0.00000	0.00000	7.31344	0.00000		
2	8.8900*-05	4.0735*+00	NM	0.92287	0.27655	0.61200	4.89718	0.12497		
3	9.3980*-05	4.0735*+00	NM	0.92287	0.27655	0.61200	4.89718	0.12497		
4	1.6764*-04	4.2263*+00	NM	0.92150	0.28257	0.62000	4.81445	0.12878		
5	2.4638*-04	4.4942*+00	NM	0.92395	0.29259	0.63450	4.70282	0.13492		
6	4.1402*-04	5.4702*+00	NM	0.93174	0.32665	0.68000	4.33355	0.15692		
7	5.6134*-04	6.2259*+00	NM	0.93726	0.35070	0.70900	4.08712	0.17347		
8	7.3152*-04	6.8287*+00	NM	0.94347	0.36874	0.73000	3.91932	0.18626		
9	1.0973*-03	7.4983*+00	NM	0.94784	0.38778	0.75000	3.74078	0.20049		
10	1.4300*-03	8.0136*+00	NM	0.95002	0.40180	0.76350	3.61069	0.21146		
11	1.7374*-03	8.4314*+00	NM	0.95263	0.41283	0.77400	3.51519	0.22019		
12	2.4079*-03	9.4645*+00	NM	0.95923	0.43888	0.79750	3.30198	0.24152		
13	3.0175*-03	1.0561*+01	NM	0.96802	0.46493	0.82000	3.11066	0.26361		
14	3.6525*-03	1.1630*+01	NM	0.97552	0.48898	0.83900	2.94405	0.28498		
15	4.6838*-03	1.3681*+01	NM	0.98475	0.53206	0.86800	2.66141	0.32614		
16	5.6642*-03	1.6013*+01	NM	0.99323	0.57715	0.89400	2.39934	0.37260		
17	6.8758*-03	1.9240*+01	NM	1.00212	0.63427	0.92150	2.11079	0.43657		
18	8.2042*-03	2.3161*+01	NM	1.00950	0.69739	0.94600	1.84003	0.51412		
19	9.8146*-03	2.8968*+01	NM	1.01253	0.78156	0.96950	1.53875	0.63006		
20	1.1422*-02	3.5690*+01	NM	1.00846	0.86874	0.98500	1.28547	0.78620		
21	1.3033*-02	4.2656*+01	NM	1.00274	0.95090	0.99500	1.09490	0.90876		
22	1.4635*-02	4.6472*+01	NM	0.99972	0.99299	0.99900	1.01215	0.98701		
D 23	1.5278*-02	4.7125*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000		

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD

	M : 2.8 R THETA X 10 ⁻³ : a) 180-700 b) 57 TW / TR : About 1.0	6502
		ZPG - AW
Blow-down tunnel, running time 10-20 s. W = H = 1.22 m 0.34 < P0 < 1.04 MN/m ² . TO : 285 - 320 K. Air. 30 < RE/m X 10 ⁻⁶ < 90.		
MOORE D.R. and HARKNESS J. 1965. Experimental investigations of the compressible turbulent boundary layer at very high Reynolds numbers. AIAA J. 3. 631-638. And Harkness J., Private communication.		

- 1a The test boundary layer was formed on a continuation of the floor of the 1.22 x 1.22 m tunnel, surveys
8a being made at 9.14, 11.89 and 14.63 m from the throat (X = 0). The test surface was constructed of rolled
1b aluminium finished to 0.63 μ m. For comparison, tests were also made on a flat plate model (L = 3.05,
W = 1.22 m) mounted, on separate occasions, at the centre of the working section. The leading edge (X = 0)
3 was 0.05 - 0.10 mm thick and the surface finish was 0.25 μ m. For the tests described here, transition was
2 natural. Static pressure variations on the test surface were as much as 10 - 20 % on the tunnel floor and
5 - 10 % on the flat plate. The mean pressure variation on the tunnel floor extension showed a slight
adverse pressure gradient.
- 6 Static pressure was measured at 32 - 34 stations for each test series, at intervals of about 85 mm on the
plate and 305 mm on the floor. A FEB (element diameter 50.8 mm) could be mounted at the three floor
stations and at two stations on the plate, data from the downstream station (X = 2.74 m) being presented
here. No wall temperatures were measured, the temperature of the massive structure remaining at room
temperature, about 290 K.
- 7 Pitot pressure profiles were measured with CPP. On the floor, four CPP were mounted as a rake, on a single
traverse gear at vertical intervals of 38.1 mm. For the outer three, d₁ = 1.62 mm, and for the inner,
d₁ = 1.07 mm. For the flat plate tests, a single CPP (d₁ = 1.07 mm) was used.
- 9 The wall shear stress and the profile for a given station were measured on separate occasions. The CF value
has been interpolated to the profile boundary conditions on the basis of a common unit Reynolds number.
11 Sutherland's viscosity law was used.
- 12 The authors assumed that the boundary layer was isoenergetic. The editors have replaced this with the
Crocco / Van Driest temperature / velocity correlation and the assumption TW = 290 K. The static pressure
has also been assumed constant through the layer. The number of data points for each profile was
exceptionally large. We have replaced our usual integration scheme with the trapezoidal rule so as to
improve the handling of the scatter of the data.
- 13 The available profiles consist of two sets for the three successive floor stations at an approximately
constant (10 %) unit Reynolds number. There are also two individual profiles for the first station. Two
14 individual profiles for the flat plate are also given. (0501, 0601). The authors' interpolated wall
shear stress measurements are also presented.
- 5 DATA: 6502 0101-0601. Pitot profiles. NX = 1-3 (a), 1 (b). CF from FEB.
- 15 Editors' comments
The general experimental conditions for this entry would appear to have been fairly rough and ready.
Nevertheless, the data are of value as the profiles were obtained at exceptionally high Reynolds number,
and are supported by direct measurements of wall shear stress. At this moderate Mach number, the absence

of TO profiles is not important for a near-adiabatic boundary layer. Since, for the tunnel wall tests, the X-dimension was as much as 10 times the width, it is probable that some three dimensional effects are present. Despite the large physical scale, the measurements do not generally extend within the momentum deficit peak. The source paper gives a greater range of CF and R THETA values than that presented here. The only comparable experiment is that of Thomke - CAT 6903 with very similar general conditions.

CAT 6502		MOORE/HARKNESS BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW	PD	
X	PODA	PW/PD*	REN2D	CO	H32	H32K	TW*	TD	
RZ	TODA	SW *	D2	PI2	H42	D2K	UD	TR	
65020101	2.8310	1.0405	1.9039 ⁺⁰⁵	9.0000 ⁻⁰⁴	4.4017	1.2235	3.6350 ⁺⁰⁴	3.6350 ⁺⁰⁴	
NM	1.0342 ⁺⁰⁶	1.0000	4.2407 ⁺⁰⁵	NM	1.8634	1.8521	2.9000 ⁺⁰²	1.1440 ⁺⁰²	
INFINITE	2.9778 ⁺⁰²	0.0000	5.1125 ⁻⁰³	NM	0.0978	6.9749 ⁻⁰³	6.0711 ⁺⁰²	2.7871 ⁺⁰²	
65020102	2.7870	0.9811	2.5535 ⁺⁰⁵	8.4900 ⁻⁰⁴	4.1466	1.2156	3.7793 ⁺⁰⁴	3.7793 ⁺⁰⁴	
NM	1.0055 ⁺⁰⁶	1.0000	5.2916 ⁺⁰⁵	NM	1.8629	1.8516	2.9000 ⁺⁰²	1.2358 ⁺⁰²	
INFINITE	3.1596 ⁺⁰²	0.0000	6.9627 ⁻⁰³	NM	0.1457	9.3064 ⁻⁰³	6.2118 ⁺⁰²	2.9559 ⁺⁰²	
65020103	2.6690	1.0146	3.5931 ⁺⁰⁵	8.6200 ⁻⁰⁴	4.0274	1.2176	4.6159 ⁺⁰⁴	4.6159 ⁺⁰⁴	
NM	1.0246 ⁺⁰⁶	1.0000	7.3368 ⁺⁰⁵	NM	1.8582	1.8472	2.9000 ⁺⁰²	1.2556 ⁺⁰²	
INFINITE	3.0444 ⁺⁰²	0.0000	8.4432 ⁻⁰³	NM	0.0999	1.1248 ⁻⁰²	5.9963 ⁺⁰²	2.8584 ⁺⁰²	
65020201	2.8430	1.0626	1.5905 ⁺⁰⁵	9.5300 ⁻⁰⁴	4.4477	1.2257	2.8719 ⁺⁰⁴	2.8719 ⁺⁰⁴	
NM	8.3216 ⁺⁰⁵	1.0000	3.6305 ⁺⁰⁵	NM	1.8609	1.8494	2.9000 ⁺⁰²	1.1147 ⁺⁰²	
INFINITE	2.9167 ⁺⁰²	0.0000	5.3135 ⁻⁰³	NM	0.0941	7.3076 ⁻⁰³	6.0182 ⁺⁰²	2.7293 ⁺⁰²	
65020202	2.8090	0.9781	2.0577 ⁺⁰⁵	8.7400 ⁻⁰⁴	4.1690	1.2171	2.9688 ⁺⁰⁴	2.9688 ⁺⁰⁴	
NM	8.1684 ⁺⁰⁵	1.0000	4.2884 ⁺⁰⁵	NM	1.8613	1.8501	2.9000 ⁺⁰²	1.2283 ⁺⁰²	
INFINITE	3.1667 ⁺⁰²	0.0000	7.0451 ⁻⁰³	NM	0.1493	9.5012 ⁻⁰³	6.2418 ⁺⁰²	2.9651 ⁺⁰²	
65020203	2.6930	1.0282	2.8725 ⁺⁰⁵	8.9100 ⁻⁰⁴	4.1034	1.2187	3.5920 ⁺⁰⁴	3.5920 ⁺⁰⁴	
NM	8.2737 ⁺⁰⁵	1.0000	5.9944 ⁺⁰⁵	NM	1.8572	1.8460	2.9000 ⁺⁰²	1.2265 ⁺⁰²	
INFINITE	3.0056 ⁺⁰²	0.0000	8.4966 ⁻⁰³	NM	0.0928	1.1413 ⁻⁰²	5.9798 ⁺⁰²	2.8205 ⁺⁰²	
65020301	2.8650	1.0510	9.8145 ⁺⁰⁴	9.8700 ⁻⁰⁴	4.5674	1.2260	1.6140 ⁺⁰⁴	1.6140 ⁺⁰⁴	
NM	4.8359 ⁺⁰⁵	1.0000	2.2365 ⁺⁰⁵	NM	1.8598	1.8476	2.9000 ⁺⁰²	1.1167 ⁺⁰²	
INFINITE	2.9500 ⁺⁰²	0.0000	5.7945 ⁻⁰³	NM	0.0725	8.0619 ⁻⁰³	6.0703 ⁺⁰²	2.7593 ⁺⁰²	
65020401	2.8970	1.0738	7.0161 ⁺⁰⁴	1.0200 ⁻⁰³	4.6959	1.2286	1.0961 ⁺⁰⁴	1.0961 ⁺⁰⁴	
NM	3.4474 ⁺⁰⁵	1.0000	1.6524 ⁺⁰⁵	NM	1.8583	1.8454	2.9000 ⁺⁰²	1.0785 ⁺⁰²	
INFINITE	2.8889 ⁺⁰²	0.0000	5.9282 ⁻⁰³	NM	0.0580	8.3569 ⁻⁰³	6.0322 ⁺⁰²	2.7006 ⁺⁰²	
65020501	2.9080	1.0518	2.1687 ⁺⁰⁴	1.2300 ⁻⁰³	4.8277	1.3396	1.0739 ⁺⁰⁴	1.0739 ⁺⁰⁴	
NM	3.4342 ⁺⁰⁵	1.0000	5.0298 ⁺⁰⁴	NM	1.8509	1.8376	2.9000 ⁺⁰²	1.0961 ⁺⁰²	
INFINITE	2.9500 ⁺⁰²	0.0000	1.8784 ⁻⁰³	NM	0.0784	2.6756 ⁻⁰³	6.1043 ⁺⁰²	2.7572 ⁺⁰²	
65020601	2.9100	1.0192	2.1657 ⁺⁰⁴	1.2400 ⁻⁰³	4.7646	1.3487	1.0776 ⁺⁰⁴	1.0776 ⁺⁰⁴	
NM	3.4563 ⁺⁰⁵	1.0000	4.8792 ⁺⁰⁴	NM	1.8514	1.8385	2.9000 ⁺⁰²	1.1302 ⁺⁰²	
INFINITE	3.0444 ⁺⁰²	0.0000	1.8970 ⁻⁰³	NM	0.1031	2.6819 ⁻⁰³	6.2026 ⁺⁰²	2.8454 ⁺⁰²	

TRAPEZOIDAL RULE FOR ALL INTEGRATIONS

65020101		MOORE/HARKNESS		PROFILE TABULATION		72 POINTS, DELTA AT POINT 70			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000+00	1.0000+00	NM	0.96489	0.00000	0.00000	2.51152	0.00000	
2	5.3340-04	2.5558+00	NM	0.96915	0.44143	0.61202	1.92221	0.31839	
3	9.9314-04	3.0245+00	NM	0.97203	0.49203	0.66429	1.82278	0.36444	
4	1.6612-03	3.3777+00	NM	0.97407	0.52651	0.69758	1.75541	0.39739	
5	2.3800-03	3.6790+00	NM	0.97573	0.55408	0.72288	1.70213	0.42469	
6	3.2106-03	3.8891+00	NM	0.97685	0.57245	0.73911	1.66701	0.44337	
7	4.0716-03	4.0707+00	NM	0.97778	0.58784	0.75231	1.63787	0.45932	
8	4.9860-03	4.1727+00	NM	0.97830	0.59630	0.75943	1.62197	0.46822	
9	6.0554-03	4.3240+00	NM	0.97904	0.60862	0.76961	1.59897	0.48131	
10	7.1577-03	4.5972+00	NM	0.98035	0.63023	0.78694	1.55914	0.50472	
11	8.3083-03	4.7159+00	NM	0.98090	0.63938	0.79408	1.54247	0.51481	
12	9.6190-03	4.9103+00	NM	0.98179	0.65407	0.80532	1.51595	0.53123	
13	1.0993-02	4.9835+00	NM	0.98211	0.65952	0.80941	1.50621	0.53738	
14	1.2502-02	5.0956+00	NM	0.98261	0.66779	0.81535	1.49151	0.54680	
15	1.4067-02	5.3103+00	NM	0.98353	0.68329	0.82682	1.46424	0.56468	
16	1.5646-02	5.5365+00	NM	0.98447	0.69925	0.83811	1.43657	0.58341	
17	1.7313-02	5.6651+00	NM	0.98499	0.70817	0.84427	1.42131	0.59401	
18	1.9149-02	5.6870+00	NM	0.98508	0.70967	0.84529	1.41876	0.59580	
19	2.1036-02	5.7530+00	NM	0.98534	0.71419	0.84838	1.41107	0.60123	
20	2.3045-02	6.0511+00	NM	0.98650	0.73426	0.86175	1.37743	0.62562	
21	2.5108-02	6.3448+00	NM	0.98760	0.75347	0.87412	1.34587	0.64940	
22	2.7264-02	6.2946+00	NM	0.98741	0.75022	0.87206	1.35116	0.64541	
23	2.9588-02	6.6846+00	NM	0.98881	0.77511	0.88754	1.31113	0.67692	
24	3.1880-02	6.8217+00	NM	0.98928	0.78367	0.89270	1.29762	0.68795	
25	3.4603-02	6.8217+00	NM	0.98928	0.78367	0.89270	1.29762	0.68795	
26	3.6403-02	7.0783+00	NM	0.99015	0.79944	0.90201	1.27308	0.70853	
27	3.6485-02	7.1076+00	NM	0.99024	0.80122	0.90305	1.27034	0.71087	
28	3.8976-02	7.3482+00	NM	0.99102	0.81569	0.91134	1.24827	0.73008	
29	3.9436-02	7.4413+00	NM	0.99132	0.82122	0.91445	1.23994	0.73749	
30	4.0104-02	7.5042+00	NM	0.99152	0.82494	0.91652	1.23437	0.74250	
31	4.0823-02	7.5679+00	NM	0.99172	0.82868	0.91860	1.22878	0.74757	
32	4.1653-02	7.6976+00	NM	0.99211	0.83625	0.92275	1.21757	0.75786	
33	4.2515-02	7.6976+00	NM	0.99211	0.83625	0.92275	1.21757	0.75786	
34	4.3429-02	7.6324+00	NM	0.99191	0.83245	0.92067	1.22318	0.75269	
35	4.4498-02	7.7968+00	NM	0.99242	0.84200	0.92586	1.20912	0.76573	
36	4.5601-02	8.0354+00	NM	0.99312	0.85566	0.93314	1.18929	0.78462	
37	4.6751-02	8.0007+00	NM	0.99302	0.85369	0.93210	1.19213	0.78187	
38	4.8062-02	8.2122+00	NM	0.99364	0.86564	0.93834	1.17502	0.79857	
39	4.9436-02	8.0354+00	NM	0.99312	0.85566	0.93314	1.18929	0.78462	
40	5.0945-02	8.2122+00	NM	0.99364	0.86564	0.93834	1.17502	0.79857	
41	5.2509-02	8.3208+00	NM	0.99395	0.87171	0.94146	1.16642	0.80714	
42	5.4089-02	8.5824+00	NM	0.99467	0.88467	0.94875	1.14622	0.82772	
43	5.5756-02	8.7764+00	NM	0.99520	0.89674	0.95396	1.13169	0.84299	
44	5.7592-02	8.8958+00	NM	0.99551	0.90318	0.95709	1.12293	0.85231	
45	5.9479-02	8.8558+00	NM	0.99541	0.90103	0.95505	1.12586	0.84917	
46	6.1488-02	9.1091+00	NM	0.99604	0.91410	0.96231	1.10826	0.86830	
47	6.3951-02	9.4412+00	NM	0.99690	0.93204	0.97067	1.08460	0.88495	
48	6.5707-02	9.3975+00	NM	0.99680	0.92976	0.96962	1.08757	0.88155	
49	6.8031-02	9.6636+00	NM	0.99745	0.94356	0.97589	1.06970	0.91231	
50	7.0322-02	9.8475+00	NM	0.99788	0.95297	0.98008	1.05771	0.92660	
51	7.3132-02	9.8011+00	NM	0.99777	0.95060	0.97903	1.06072	0.92299	
52	7.4846-02	1.0036+01	NM	0.99832	0.96253	0.98427	1.04567	0.94128	
53	7.4927-02	9.9412+00	NM	0.99810	0.95773	0.98217	1.05170	0.93389	
54	7.7076-02	9.9412+00	NM	0.99810	0.95773	0.98217	1.05170	0.93389	
55	7.7536-02	9.9412+00	NM	0.99810	0.95773	0.98217	1.05170	0.93389	
56	7.8204-02	1.0036+01	NM	0.99832	0.96253	0.98427	1.04567	0.94128	
57	7.8923-02	9.8942+00	NM	0.99799	0.95534	0.98113	1.05471	0.93023	
58	7.9753-02	1.0230+01	NM	0.99877	0.97227	0.98846	1.03357	0.95635	
59	8.0615-02	1.0181+01	NM	0.99866	0.96952	0.98741	1.03660	0.95245	
60	8.1529-02	1.0280+01	NM	0.99888	0.97474	0.98951	1.03054	0.96019	
61	8.2598-02	1.0380+01	NM	0.99910	0.97970	0.99161	1.02446	0.96793	
62	8.3701-02	1.0481+01	NM	0.99932	0.98470	0.99370	1.01837	0.97578	
63	8.4851-02	1.0490+01	NM	0.99921	0.98219	0.99265	1.02141	0.97184	
64	8.6162-02	1.0584+01	NM	0.99955	0.98975	0.99580	1.01226	0.98374	
65	8.7536-02	1.0390+01	NM	0.99910	0.97970	0.99161	1.02446	0.96793	
66	8.9045-02	1.0584+01	NM	0.99955	0.98975	0.99580	1.01226	0.98374	
67	9.0609-02	1.0430+01	NM	0.99921	0.98219	0.99265	1.02141	0.97184	
68	9.2169-02	1.0584+01	NM	0.99955	0.98975	0.99580	1.01226	0.98374	
69	9.3836-02	1.0636+01	NM	0.99966	0.99230	0.99685	1.00920	0.98776	
D 70	9.5692-02	1.0794+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
71	9.7579-02	1.0741+01	NM	0.99987	0.99742	0.99895	1.00307	0.99589	
72	9.9588-02	1.0688+01	NM	0.99977	0.99485	0.99790	1.00614	0.99181	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

6502U103

MOORE/HARKNESS

PROFILE TABULATION

60 POINTS, DELTA AT POINT 60

I	Y	PTZ/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD=U/UD
1	0.0000+00	1.0000+00	NM	0.95255	0.00000	0.00000	2.30967	0.00000
2	5.3340+04	2.2092+00	NM	0.96505	0.42302	0.57763	1.86460	0.30979
3	9.4234+04	2.3794+00	NM	0.96651	0.44597	0.60255	1.82608	0.33002
4	1.7501+03	2.8481+00	NM	0.97022	0.50248	0.66093	1.73014	0.38201
5	2.7305+03	3.0960+00	NM	0.97202	0.52953	0.68718	1.68410	0.40804
6	3.9141+03	3.4274+00	NM	0.97429	0.56340	0.71858	1.62671	0.44174
7	5.2172+03	3.6520+00	NM	0.97574	0.58515	0.73749	1.59018	0.46403
8	7.0409+03	3.7774+00	NM	0.97653	0.59692	0.74806	1.57054	0.47631
9	9.1897+03	4.1290+00	NM	0.97864	0.62867	0.77459	1.51810	0.51024
10	1.1173+02	4.0865+00	NM	0.97839	0.62492	0.77153	1.52425	0.50617
11	1.4039+02	4.3049+00	NM	0.97964	0.64393	0.78687	1.49322	0.52696
12	1.7178+02	4.6357+00	NM	0.98144	0.67164	0.80839	1.44867	0.55803
13	2.1112+02	4.8740+00	NM	0.98268	0.69089	0.82278	1.41823	0.58015
14	2.5695+02	4.8565+00	NM	0.98259	0.68950	0.82175	1.42043	0.57853
15	3.0246+02	5.3396+00	NM	0.98496	0.72698	0.84855	1.36241	0.62283
16	3.4930+02	5.4395+00	NM	0.98543	0.73448	0.85371	1.35102	0.63190
17	3.9578+02	5.7107+00	NM	0.98666	0.75447	0.86716	1.32183	0.65642
18	3.9271+02	5.8418+00	NM	0.98723	0.76394	0.87337	1.30762	0.66822
19	4.0135+02	5.6254+00	NM	0.98828	0.74824	0.86302	1.33031	0.64873
20	4.1151+02	5.8640+00	NM	0.98733	0.76553	0.87441	1.30467	0.67021
21	4.2393+02	5.9088+00	NM	0.98752	0.76873	0.87648	1.29997	0.67423
22	4.3731+02	6.0926+00	NM	0.98830	0.78173	0.88478	1.28104	0.69067
23	4.5613+02	5.7976+00	NM	0.98704	0.76076	0.87130	1.31170	0.66425
24	4.7841+02	6.1634+00	NM	0.98860	0.78668	0.88749	1.27389	0.69700
25	5.0422+02	6.3085+00	NM	0.98919	0.79671	0.89413	1.25950	0.70991
26	5.3190+02	6.4581+00	NM	0.98979	0.80693	0.90037	1.24500	0.72319
27	5.5977+02	6.4328+00	NM	0.98967	0.80521	0.89933	1.24742	0.72095
28	6.1260+02	6.6915+00	NM	0.99070	0.82262	0.90974	1.22303	0.74384
29	6.4706+02	6.7718+00	NM	0.99101	0.82795	0.91287	1.21565	0.75093
30	6.9291+02	7.2527+00	NM	0.99276	0.85914	0.93061	1.17330	0.79316
31	7.4036+02	7.4030+00	NM	0.99379	0.86866	0.93584	1.16067	0.80630
32	7.7422+02	7.4030+00	NM	0.99329	0.86866	0.93584	1.16067	0.80630
33	7.7470+02	7.4030+00	NM	0.99329	0.86866	0.93584	1.16067	0.80630
34	7.8285+02	7.1066+00	NM	0.99224	0.84978	0.92539	1.18585	0.78036
35	7.9301+02	7.5263+00	NM	0.99371	0.87639	0.94003	1.15051	0.81706
36	8.0543+02	7.3123+00	NM	0.99297	0.86293	0.93270	1.16826	0.79837
37	8.1882+02	7.5891+00	NM	0.99392	0.88030	0.94212	1.14540	0.82253
38	8.3764+02	7.2824+00	NM	0.99287	0.86103	0.93166	1.17078	0.79576
39	8.5492+02	7.6525+00	NM	0.99413	0.88423	0.94422	1.14029	0.82805
40	8.8572+02	7.8806+00	NM	0.99488	0.89822	0.95156	1.12229	0.84787
41	9.1341+02	8.0152+00	NM	0.99532	0.90637	0.95575	1.11193	0.85954
42	9.4127+02	7.8806+00	NM	0.99488	0.89822	0.95156	1.12229	0.84787
43	9.9411+02	8.0837+00	NM	0.99553	0.91050	0.95785	1.10673	0.86548
44	1.0286+01	8.2232+00	NM	0.99597	0.91883	0.96206	1.09630	0.87755
45	1.0744+01	8.7008+00	NM	0.99740	0.94681	0.97573	1.06202	0.91875
46	1.1219+01	8.7008+00	NM	0.99740	0.94681	0.97573	1.06202	0.91875
47	1.1562+01	8.7008+00	NM	0.99740	0.94681	0.97573	1.06202	0.91875
48	1.1552+01	8.9346+00	NM	0.99807	0.96021	0.98205	1.04601	0.93886
49	1.1639+01	8.6626+00	NM	0.99729	0.94461	0.97468	1.06467	0.91547
50	1.1740+01	9.0955+00	NM	0.99852	0.96932	0.98627	1.03527	0.95267
51	1.1864+01	8.8357+00	NM	0.99785	0.95571	0.97994	1.05136	0.93208
52	1.1998+01	9.0955+00	NM	0.99852	0.96932	0.98627	1.03527	0.95267
53	1.2186+01	8.8357+00	NM	0.99785	0.95571	0.97994	1.05136	0.93208
54	1.2409+01	9.1364+00	NM	0.99863	0.97163	0.98732	1.03258	0.95618
55	1.2667+01	9.3449+00	NM	0.99920	0.98328	0.99260	1.01906	0.97404
56	1.2944+01	9.4302+00	NM	0.99943	0.98800	0.99472	1.01363	0.98134
57	1.3223+01	9.3026+00	NM	0.99909	0.98093	0.99155	1.02177	0.97042
58	1.3751+01	9.4733+00	NM	0.99954	0.99038	0.99577	1.01091	0.98502
59	1.4096+01	9.5166+00	NM	0.99966	0.99277	0.99683	1.00819	0.98873
60	1.4554+01	9.6485+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

65020501

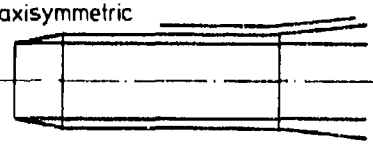
MOORE/HARKNESS

PROFILE TABULATION

73 POINTS, DELTA AT POINT 73

I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000*+00	1.0000*+00	NM	0.97982	0.00000	0.00000	2.63699	0.00000
2	7.0356*+04	2.7425*+00	NM	0.97659	0.45012	0.62977	1.95750	0.32172
3	9.3218*+04	3.0176*+00	NM	0.97775	0.47831	0.65884	1.89727	0.34725
4	1.1455*+03	3.3390*+00	NM	0.97907	0.50901	0.68898	1.83213	0.37605
5	1.3665*+03	3.5642*+00	NM	0.97998	0.52936	0.70811	1.78937	0.39573
6	1.6205*+03	3.7161*+00	NM	0.98058	0.54261	0.72021	1.76175	0.40880
7	1.8821*+03	3.9171*+00	NM	0.98135	0.55963	0.73535	1.72656	0.42591
8	2.1311*+03	4.0442*+00	NM	0.98184	0.57011	0.74445	1.70509	0.43660
9	2.4282*+03	4.1913*+00	NM	0.98238	0.58200	0.75457	1.68091	0.44890
10	2.6772*+03	4.2664*+00	NM	0.98244	0.58321	0.75558	1.67848	0.45016
11	2.9616*+03	4.3138*+00	NM	0.98283	0.59171	0.76267	1.66133	0.45907
12	3.2385*+03	4.3767*+00	NM	0.98306	0.59663	0.76672	1.65147	0.46427
13	3.5306*+03	4.5725*+00	NM	0.98376	0.61167	0.77889	1.62153	0.48034
14	3.8430*+03	4.6744*+00	NM	0.98412	0.61935	0.78498	1.60639	0.48866
15	4.1326*+03	4.7265*+00	NM	0.98430	0.62323	0.78803	1.59877	0.49290
16	4.4983*+03	4.8870*+00	NM	0.98485	0.63506	0.79718	1.57572	0.50591
17	4.8133*+03	4.9792*+00	NM	0.98516	0.64175	0.80226	1.56280	0.51335
18	5.1003*+03	5.0736*+00	NM	0.98548	0.64852	0.80735	1.54980	0.52094
19	5.4483*+03	5.1899*+00	NM	0.98586	0.65677	0.81346	1.53408	0.53026
20	5.8268*+03	5.2693*+00	NM	0.98612	0.66234	0.81754	1.52353	0.53661
21	6.1951*+03	5.3503*+00	NM	0.98638	0.66797	0.82161	1.51293	0.54306
22	6.5354*+03	5.4329*+00	NM	0.98664	0.67367	0.82569	1.50227	0.54963
23	6.9367*+03	5.5815*+00	NM	0.98711	0.68378	0.83284	1.48348	0.56141
24	7.3889*+03	5.6249*+00	NM	0.98724	0.68671	0.83488	1.47809	0.56484
25	7.8410*+03	5.7130*+00	NM	0.98751	0.69262	0.83897	1.46725	0.57180
26	8.2652*+03	5.8486*+00	NM	0.98792	0.70160	0.84510	1.45089	0.58247
27	8.7198*+03	5.9885*+00	NM	0.98834	0.71075	0.85124	1.43440	0.59344
28	9.1059*+03	6.1084*+00	NM	0.98869	0.71849	0.85635	1.42056	0.60283
29	9.6012*+03	6.2066*+00	NM	0.98897	0.72477	0.86045	1.40943	0.61049
30	1.0097*+02	6.2818*+00	NM	0.98919	0.72954	0.86352	1.40105	0.61634
31	1.0554*+02	6.4354*+00	NM	0.98962	0.73920	0.86967	1.38418	0.62829
32	1.0978*+02	6.5673*+00	NM	0.98999	0.74739	0.87480	1.37003	0.63853
33	1.1438*+02	6.7030*+00	NM	0.99035	0.75571	0.87993	1.35579	0.64902
34	1.1968*+02	6.7861*+00	NM	0.99058	0.76077	0.88302	1.34720	0.65544
35	1.2479*+02	6.8707*+00	NM	0.99080	0.76588	0.88610	1.33858	0.66197
36	1.2992*+02	6.9857*+00	NM	0.99110	0.77277	0.89021	1.32704	0.67082
37	1.3498*+02	7.1632*+00	NM	0.99156	0.78328	0.89638	1.30962	0.68446
38	1.4044*+02	7.3159*+00	NM	0.99194	0.79221	0.90153	1.29501	0.69616
39	1.4549*+02	7.4412*+00	NM	0.99225	0.79947	0.90565	1.28325	0.70574
40	1.5014*+02	7.5696*+00	NM	0.99257	0.80683	0.90977	1.27144	0.71554
41	1.5519*+02	7.6349*+00	NM	0.99272	0.81055	0.91183	1.26551	0.72052
42	1.6116*+02	7.9734*+00	NM	0.99352	0.82957	0.92215	1.23565	0.74628
43	1.6713*+02	7.9734*+00	NM	0.99352	0.82957	0.92215	1.23565	0.74628
44	1.7214*+02	8.0791*+00	NM	0.99376	0.83341	0.92525	1.22662	0.75430
45	1.7869*+02	8.3707*+00	NM	0.99441	0.85133	0.93351	1.20239	0.77638
46	1.8423*+02	8.4838*+00	NM	0.99466	0.85743	0.93662	1.19324	0.78494
47	1.8926*+02	8.5220*+00	NM	0.99474	0.85948	0.93765	1.19018	0.78782
48	1.9581*+02	8.6381*+00	NM	0.99499	0.86567	0.94076	1.18099	0.79658
49	2.0140*+02	8.6367*+00	NM	0.99541	0.87617	0.94593	1.16500	0.81154
50	2.0701*+02	8.4771*+00	NM	0.99550	0.87829	0.94697	1.16251	0.81459
51	2.1283*+02	9.2109*+00	NM	0.99618	0.89560	0.95526	1.13766	0.83967
52	2.1864*+02	9.1845*+00	NM	0.99652	0.90448	0.95941	1.12514	0.85270
53	2.2504*+02	9.3630*+00	NM	0.99686	0.91352	0.96356	1.11257	0.86607
54	2.3091*+02	9.2971*+00	NM	0.99635	0.90003	0.95734	1.13141	0.84615
55	2.3708*+02	9.4287*+00	NM	0.99660	0.90673	0.96045	1.12200	0.85601
56	2.4404*+02	9.7464*+00	NM	0.99721	0.92271	0.96772	1.09993	0.87979
57	2.4983*+02	9.9351*+00	NM	0.99756	0.93207	0.97187	1.08724	0.89389
58	2.5565*+02	1.0178*+01	NM	0.99801	0.94400	0.97707	1.07129	0.91205
59	2.6205*+02	1.0278*+01	NM	0.99818	0.94885	0.97916	1.06480	0.91949
60	2.6901*+02	1.0380*+01	NM	0.99836	0.95375	0.98124	1.05847	0.92704
61	2.7470*+02	1.0534*+01	NM	0.99863	0.96118	0.98436	1.04881	0.93855
62	2.8158*+02	1.0692*+01	NM	0.99890	0.96872	0.98749	1.03911	0.95032
63	2.8738*+02	1.0854*+01	NM	0.99917	0.97637	0.99061	1.02939	0.96233
64	2.9390*+02	1.0909*+01	NM	0.99927	0.97894	0.99165	1.02614	0.96640
65	2.9969*+02	1.0964*+01	NM	0.99936	0.98153	0.99270	1.02288	0.97049
66	3.0620*+02	1.1076*+01	NM	0.99954	0.98674	0.99478	1.01636	0.97877
67	3.1199*+02	1.1189*+01	NM	0.99972	0.99201	0.99687	1.00983	0.98717
68	3.1811*+02	1.1189*+01	NM	0.99972	0.99201	0.99687	1.00983	0.98717
69	3.2426*+02	1.1248*+01	NM	0.99982	0.99466	0.99791	1.00656	0.99141
70	3.3040*+02	1.1304*+01	NM	0.99991	0.99732	0.99896	1.00328	0.99569
71	3.3518*+02	1.1362*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
72	3.3917*+02	1.1362*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
D 73	3.4318*+02	1.1362*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIERT

	M : 5, 6 and 8 falling to 3, 3.5, 4. R THETA X 10 ⁻³ : 2 - 72 TW/TR : 0.4 - 1.0	6503
		ZPG - APG AW - MHT - SHT
Tunnel A (M = 5,6) : Continuous flow, variable nozzle. W = H = 1 m. 0.28 < PO < 1.4 MN/m ² . 350 < TO < 400 K. Air. 6 < RE/m X 10 ⁻⁶ < 23. Tunnel B (M = 8) : Axisymmetric continuous flow, fixed nozzle. D = 1.3 m. 2.3 < PO < 5.5 MN/m ² . TO : 750 K. Air. 5 < RE/m X 10 ⁻⁶ < 12.		
STROUD J.F. and MILLER L.D., 1965. An experimental and analytical investigation of hypersonic inlet boundary layers. Technical report AFFDL-TR-65-123 Vol. 1 and Vol. 2 (AD 621343/4) And Stroud and Miller (1966), Stroud J.F., private communication.		

- 1 The tests described here were made on the outer surface of a hollow axisymmetric model mounted on the centre-line of the tunnels. Of the four models used by the authors we here describe only that one which they designate the "Heat transfer Mach 8" model. The stainless steel model consisted of a nose-section, a generating cylinder and the flared model proper. The sharp lipped nose section was 0.248 m long with an initial (and internal) diameter of 48.3 mm. This front section expanded as a cone to a diameter of 76.2 mm and carried two sets of vortex-generators. Each consisted of 16 triangular fins mounted normal to the surface and set alternately at $\pm 18^\circ$ (E) to the flow direction. The first ring was about 90 mm back from the lip and the fins were 16 mm (E) long at the base and 3.3 mm high at their trailing edge which was normal to the surface. The second set were about 200 mm back from the lip, about 30 mm long at the base and 6.6 mm high. The nose section was followed by one of two cylindrical generating surfaces 76.2 mm in diameter and 0.314 or 0.628 m long, finishing at the start of the model proper (X = 0). The short cylinder was used for tests at M = 5, 6 and the long for M = 8. The curved surface of the model was designed to be a streamline of a focused Prandtl-Meyer compression fan, followed by a short conical section intended to avoid any upstream influence from the expansion at the trailing edge of the model. The length of the compression surface was 0.933 m and the coordinates are given in table 1. The model surface was highly polished and gold-plated. It was actively cooled with air which had been pre-cooled to less than 100 K.
- 4 The generating cylinder was also cooled, but not the nose piece. The test section flow, in the absence of a model, was uniform to within 0.3 % in Mach number.
- 6 Static tapings (d = 0.75 - 1.0 mm) were distributed at up to 18 stations along the top generator, with additional tapings at 90°, 180° and 270° at X = 0 and 0.838 m to provide a check on axis-symmetry. Chromel-alumel thermocouples were distributed in the same manner, the majority being arranged to read the absolute temperature of the model wall. At the profile stations, at X = - 95 and, when using the long generating cylinder at - 413 mm, junctions were arranged on either side of a removeable plug, so as to provide values of local heat transfer rate.
- 7 Pitot, P and TO profiles were obtained simultaneously, the three probes being mounted as a three-pronged fork. They were carried on an independent traverse mechanism which could move parallel and normal to the tunnel axis. This could also rotate the probes in pitch so as to traverse normal to the model surface. The Pitot probe was a FPP (h₁ = 0.25, h₂ = 0.20, b₁ = 0.6 (E), l = 15 mm) and the TPP a STP (d₁ = 1.02, d₂ = 0.63, l = 15 mm) with a chromel-alumel thermocouple junction opposite the 0.25 mm vents a distance 0.76 mm behind the sharp probe lip, which was chamfered internally. The SPP was a CCP (α = 10°, d = 0.76, l₁ = 7.6, l₂ = 20 mm) with 4 static holes (d = 0.15 mm) round the circumference on axes at 48° to the profile normal. Additional tests were made with two similar static probes mounted at + 2° and + 4° incidence as a check on the sensitivity of the SPP to flow direction. Static pressure errors were below 5 % for incidence up to 8°. The SPP was kept parallel to the model surface during a traverse while the TTP and TPP were mounted at 3° negative incidence. The supporting structure for the three probes remained slender for about 63 mm back from the profile normal.

- 8 The TPP formed the centre prong of the fork and traversed on the profile normal through the model axis. The TTP and the SPP were mounted 7.6 mm to either side. The tips of the TPP and the TTP and the static holes of the SPP lay on a single line which was perpendicular to the flow and the profile normal. Profiles were measured at seven stations with full wall instrumentation, the X values being given in Section B.
- 9 The TO and P data from the offset probes was interpolated to the Y-values of the central Pitot probe. The static pressure values were additionally fitted to Pitot-derived values at the boundary layer edge and to the measured wall static pressure. No probe corrections were applied, and Sutherland's viscosity law was used.
- 12 The authors present 42 series of profiles, half of which were obtained on three smaller models which are not described here. The editors have chosen to present a selection of the data from the larger model, which was the only one with active cooling and heat transfer instrumentation. We present, for each Mach number and heat transfer condition, the profile series obtained at the higher of two Reynolds numbers measured by the authors. The authors have specified the boundary layer edge state as the Y value for which P_0 is 95 % of the highest value observed. In the original tabulation, an interpolated profile point is given corresponding to this. The editors have set the D-state at the next measured point outwards. We have interpolated the differential thermocouple readings (temperature difference across the plugs), on the basis of the TW value, to give values which are appropriate to the wall temperatures of the profile tests. These data have then been reduced to the heat flux data given as CQ in section B, using conductivity values supplied by the authors. We found it necessary to use a trapezoidal integration rule.
- 13 The ten profile sets correspond to free stream Mach numbers of 5, 6 and 8. For Mach 5 and 6, there are three heat transfer conditions, and for Mach 8, four. Heat transfer values are given for all the profiles, excepting a few cases of instrument-failure.

§ DATA: 6503 0101-1007. Pitot, TO and P-profiles obtained simultaneously, $NX = 6$ or 7 . Steady state heat flux values from local conduction measurements.

15 Editors' comments

The experiment was made under extreme conditions, and understandably, some of the data appear somewhat erratic. The initial profiles are covered by a relatively large number of data points, but as the layer becomes thinner on the curved portion of the model, the number reduces. For the same reason, there is a tendency for measurements in the later profiles not to extend within the momentum deficit peak. The arrangements for tripping the boundary layer seem to be remarkably severe, and possibly explain why we did not get good agreement with ZPG profiles in transformed coordinates even under the nominally ZPG conditions on the generator cylinder. The effects of transverse curvature are likely to be large, as δ/RZ is of order 0.5. The plots of CQ data which we made for the purposes of interpolation suggest that Q data for $X = 0.914$ m are unreliable.

We have presented data for the largest model only, partly because of the massive quantity in the original report, but also because it appears to be of better quality. In particular the total temperature readings, for the small models, showed unlikely variations in the free stream. The authors suggest that this may be in part due to the fact that the STP can be at quite large incidence relative to the free stream while still parallel to the model surface at the profile station. In selection we took the authors' advice that the most representative series of profile data should be the high Reynolds number data on the large model. They also remark that the best heat transfer data should be that at $M = 8$. We would remind readers of the difficulties which can be experienced with instrumentation at recovery temperatures of the order of 700 K.

There are no comparable data, the most nearly akin being series 02 of Clutter & Kaups - CAT 6401. In principle, comparisons can also be drawn with the Sturek & Danberg - CAT 7101 tests, but both these studies were made at relatively low Mach number and without significant heat transfer.

Model coordinates

Facsimile from Source paper

NB - Authors' symbols and units

Mach 8 Design

x_c	y_c	x_c	y_c	x_c	y_c
.0045	1.500	27.8505	3.4590	33.5085	4.6935
2.0265	1.5090	28.1880	3.5160	33.6000	4.7220
3.9285	1.5345	28.5105	3.5715	33.6900	4.7490
5.7090	1.5750	28.8165	3.6270	33.7755	4.7760
7.3725	1.6245	29.1090	3.6795	33.8565	4.8015
8.9280	1.6830	29.3880	3.7320	33.9360	4.8270
10.3815	1.7475	29.6535	3.7815	34.0125	4.8510
11.7390	1.8165	29.9070	3.8310	34.0860	4.8750
13.0080	1.8900	30.1485	3.8805	34.1580	4.8990
14.1960	1.9665	30.3810	3.9270	34.2255	4.9230
15.3075	2.0430	30.6015	3.9735	34.2915	4.9455
16.3500	2.1225	30.8130	4.0170	34.3560	4.9645
17.3265	2.2005	31.0155	4.0620	34.4175	4.9890
18.2430	2.2800	31.2090	4.1040	34.4760	5.0100
19.1055	2.3595	31.3935	4.1460	34.5325	5.0505
19.9154	2.4375	31.5705	4.1865	34.5890	5.0895
20.6775	2.5140	31.7415	4.2270	34.6495	5.1270
21.3960	2.5905	31.9140	4.2660	34.8810	5.1630
22.0725	2.6655	32.0595	4.3035	34.9650	5.1960
22.7115	2.7390	32.2095	4.3395	35.0820	5.2455
23.3160	2.8110	32.3520	4.3770	35.1885	5.2905
23.8860	2.8830	32.4900	4.4115	35.3130	5.3460
24.4260	2.9520	32.6220	4.4460	35.4495	5.4105
24.9375	3.0210	32.7495	4.4790	35.5650	5.4675
25.4205	3.0870	32.8710	4.5120	35.6820	5.5290
25.8795	3.1530	32.9880	4.5450	35.8095	5.5995
26.3160	3.2175	33.1005	4.5765	35.9150	5.6670
26.7300	3.2790	33.2085	4.6065	36.0045	5.7240
27.1215	3.3405	33.3120	4.6365	36.0510	5.7570
27.4950	3.4005	33.4125	4.6650	36.0645	5.7675
				Conical	
				36.750	5.188

All dimensions in inches.

CAT 6503		STROUD		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN X *	MD PUD	T/TRA P/TPD	RED2M RED2D	CF CO *	H12 H32	H12K H32K	P#* TW*	PD* TD*			
RZ *	TD	SH *	O2	P12	H42	O2K	UD*	TR			
65030101	4.8300	0.7463	2.4304*+03	NM	11.6022	1.4115	1.9253*+03	1.9253*+03			
-1.9050*-01	8.3348*+05	1.0000	8.4648*+03	NM	1.8298	1.7718	2.4167*+02	6.2511*+01			
2.5400*-02	3.5417*+02	1.0000	4.6200*-04	NM	-0.1811	9.9452*-04	7.6566*+02	3.2384*+02			
65030102	4.8554	0.7454	3.6133*+03	NM	10.6301	1.3950	1.9324*+03	1.9324*+03			
0.0000*+00	8.6233*+05	1.0000	1.2679*+04	NM	1.7978	1.7370	2.4167*+02	6.2050*+01			
2.5400*-02	3.5462*+02	1.0000	6.7820*-04	NM	-0.0196	1.5601*-03	7.6685*+02	3.2419*+02			
65030103	4.5512	0.7424	4.5578*+03	NM	10.4321	1.2685	2.8728*+03	2.8671*+03			
4.7625*-01	8.8426*+05	1.0020	1.4366*+04	NM	1.2944*-04	1.8325	2.4111*+02	6.8928*+01			
5.9098*-02	3.5447*+02	1.0000	6.4713*-04	NM	-0.1534	1.2388*-03	7.5758*+02	3.2477*+02			
65030104	4.2458	0.7251	5.6268*+03	NM	6.4309	1.2313	4.8024*+03	4.1297*+03			
7.3860*-01	8.6366*+05	1.1629	1.5629*+04	NM	1.8990	1.8798	2.3556*+02	7.6789*+01			
9.2961*-02	3.5364*+02	1.0000	6.1578*-04	NM	-0.2541	8.7648*-04	7.4597*+02	3.2485*+02			
65030105	3.9707	0.7125	4.3712*+03	NM	3.3178	1.3459	7.6599*+03	6.0133*+03			
8.3820*-01	8.7793*+05	1.2738	1.0823*+04	NM	1.9217*-04	1.8619	2.3333*+02	8.5611*+01			
1.1553*-01	3.5356*+02	1.0000	3.6807*-04	NM	-0.2371	4.7720*-04	7.3661*+02	3.2749*+02			
65030106	3.7872	0.7036	5.7548*+03	NM	1.6152	1.3601	1.0866*+04	7.7192*+03			
8.7630*-01	8.7906*+05	1.4076	1.3183*+04	NM	2.6934*-04	1.8833	2.3056*+02	9.1783*+01			
1.2747*-01	3.5507*+02	1.0000	4.0579*-04	NM	-0.1660	4.8096*-04	7.2747*+02	3.2769*+02			
65030107	3.0325	0.7018	7.0527*+03	NM	1.3753	1.4636	3.2378*+04	2.2762*+04			
9.1440*-01	8.7786*+05	1.4225	1.2153*+04	NM	4.8333*-04	1.8979	2.2917*+02	1.2332*+02			
1.4531*-01	3.5013*+02	1.0000	2.4328*-04	NM	-0.2166	2.5173*-04	8.7519*+02	3.2654*+02			
65030201	4.8303	0.8490	2.4146*+03	NM	11.1193	1.4415	1.9238*+03	1.9238*+03			
-1.9050*-01	8.3315*+05	1.0000	3.3264*+03	NM	1.8245	1.7558	2.7444*+02	6.2389*+01			
2.5400*-02	3.5352*+02	1.0000	5.0787*-04	NM	-0.0693	1.1248*-03	7.6496*+02	3.2324*+02			
65030202	4.8619	0.8526	3.2761*+03	NM	11.1468	1.4722	1.9200*+03	1.9200*+03			
0.0000*+00	8.6341*+05	1.0000	1.2832*+04	NM	1.7911	1.7153	2.7556*+02	6.1722*+01			
2.5400*-02	3.5352*+02	1.0000	6.8446*-04	NM	-0.0743	1.6522*-03	7.6458*+02	3.2318*+02			
65030203	5.0437	0.8458	3.5289*+03	NM	12.9317	1.2743	2.3318*+03	2.3318*+03			
4.7625*-01	1.2981*+06	1.0000	1.4581*+04	NM	1.1647*-04	1.8660	2.7389*+02	5.8256*+01			
5.9098*-02	3.5465*+02	1.0000	5.6582*-04	NM	-0.2218	1.2293*-03	7.7185*+02	3.2383*+02			
65030204	4.2303	0.8475	5.6349*+03	NM	6.7486	1.2473	5.0030*+03	4.1421*+03			
7.3860*-01	8.5100*+05	1.2078	1.7637*+04	NM	1.8624	1.8611	2.7500*+02	7.7133*+01			
9.2961*-02	3.5320*+02	1.0000	7.0003*-04	NM	-0.2687	1.0508*-03	7.4490*+02	3.2449*+02			
65030205	3.9938	0.8450	7.8365*+03	NM	5.0727	1.2395	7.7705*+03	5.8668*+03			
8.3820*-01	8.8342*+05	1.3245	2.2457*+04	NM	1.7906*-04	1.8627	2.7500*+02	8.4339*+01			
1.1553*-01	3.5343*+02	1.0000	7.6133*-04	NM	-0.2739	1.0384*-03	7.3542*+02	3.2543*+02			
65030206	3.8485	0.8485	1.0070*+04	NM	2.9248	1.2379	1.0997*+04	7.0930*+03			
8.7630*-01	8.7819*+05	1.5504	2.7442*+04	NM	2.3293*-04	1.8673	2.7867*+02	6.9228*+01			
1.2747*-01	3.5353*+02	1.0000	8.6780*-04	NM	-0.2081	1.0315*-03	7.2887*+02	3.2605*+02			
65030207	3.5737	0.8493	2.2688*+04	NM	-0.8112	1.3059	3.3008*+04	1.0561*+04			
9.1440*-01	8.9394*+05	3.1251	5.5853*+04	NM	1.9680*-03	1.8144	2.7722*+02	9.9256*+01			
1.4531*-01	3.5278*+02	1.0000	1.4937*-03	NM	-0.1157	1.0620*-03	7.1384*+02	3.2641*+02			
65030301	4.8274	1.0083	2.5300*+03	NM	10.1505	1.3646	1.9238*+03	1.9238*+03			
-1.9050*-01	8.3029*+05	1.0000	1.1179*+04	NM	1.8312	1.7664	3.2222*+02	6.1739*+01			
2.5400*-02	3.4949*+02	1.0000	5.9959*-04	NM	0.0686	1.2894*-03	7.6051*+02	3.1956*+02			
65030302	4.8644	0.9920	2.9704*+03	NM	11.3654	1.4409	1.9152*+03	1.9152*+03			
0.0000*+00	8.6380*+05	1.0000	1.3083*+04	NM	1.7915	1.7167	3.2111*+02	6.1772*+01			
2.5400*-02	3.5411*+02	1.0000	7.0009*-04	NM	-0.1236	1.7368*-03	7.6654*+02	3.2370*+02			
65030303	5.2006	0.9810	3.1128*+03	NM	14.0108	1.2741	2.2006*+03	2.2006*+03			
4.7625*-01	1.4668*+06	1.0000	1.5177*+04	NM	1.8622	1.8261	3.1778*+02	5.5406*+01			
5.9098*-02	3.5511*+02	1.0000	5.6116*-04	NM	-0.2743	1.3134*-03	7.7814*+02	3.2399*+02			
65030304	4.2644	0.9747	5.4585*+03	NM	7.2728	1.2537	4.9379*+03	4.1033*+03			
7.3860*-01	8.8100*+05	1.2034	1.9264*+04	NM	1.8732	1.8895	3.1667*+02	7.6289*+01			
9.2961*-02	3.5375*+02	1.0000	7.5318*-04	NM	-0.2882	1.1930*-03	7.4679*+02	3.2490*+02			
65030305	4.0030	0.9681	7.8205*+03	NM	5.1248	1.2433	7.8050*+03	5.7911*+03			
8.3820*-01	8.8279*+05	1.3477	2.4965*+04	NM	6.0286*-05	1.8659	3.1611*+02	8.4339*+01			
1.1553*-01	3.5463*+02	1.0000	8.5529*-04	NM	-0.3179	1.2186*-03	7.3707*+02	3.2652*+02			
65030306	3.8847	0.9695	1.0706*+04	NM	3.3078	1.2390	1.1101*+04	6.8879*+03			
8.7630*-01	8.6977*+05	1.4598	3.2765*+04	NM	5.5509*-05	1.9536	3.1667*+02	8.8172*+01			
1.2747*-01	3.5429*+02	1.0000	1.0697*-03	NM	-0.3995	1.3677*-03	7.3137*+02	3.2662*+02			
65030307	3.5952	0.9724	2.6338*+04	NM	-0.6290	1.3244	3.3308*+04	9.8595*+03			
9.1440*-01	8.6018*+05	3.3783	7.2496*+04	NM	7.8262*-04	1.7864	3.1889*+02	9.8894*+01			
1.4531*-01	3.5454*+02	1.0000	2.0335*-03	NM	-0.0037	1.4470*-03	7.1683*+02	3.2795*+02			

CAT 6503		STROUD		BOUNDARY CONDITIONS AND EVALUATED DATA. 51 UNITS.						
RUN X * RZ *	MD POD TOD	TW/TR PW/PD SW *	RED2W RED2D D2	CF CO * PI2	H12 H32 H42	H12K H32K D2K	PW* TWR UD*	PD* TD* TR		
65030401	5.9223	0.6043	1.0957 ⁺ +03	NM	16.1613	1.4619	8.6520 ⁺ +02	8.6520 ⁺ +02		
-1.9050 ⁻ -01	1.2610 ⁺ +06	1.0000	4.4253 ⁺ +03	NM	1.8340	1.7528	2.2083 ⁺ +02	5.0161 ⁺ +01		
2.5400 ⁻ -02	4.0203 ⁺ +02	1.0000	3.1455 ⁻ -04	NM	-0.0935	8.4417 ⁻ -04	8.4097 ⁺ +02	3.6543 ⁺ +02		
65030402	5.9464	0.6063	1.1202 ⁺ +03	NM	16.2063	1.3094	8.6663 ⁺ +02	8.6663 ⁺ +02		
0.0000 ⁺ +00	1.2950 ⁺ +06	1.0000	4.5708 ⁺ +03	NM	1.8666	1.8207	2.2083 ⁺ +02	4.9650 ⁺ +01		
2.5400 ⁻ -02	4.0077 ⁺ +02	1.0000	3.1809 ⁻ -04	NM	-0.1512	7.8046 ⁻ -04	8.4009 ⁺ +02	3.6426 ⁺ +02		
65030403	5.2970	0.6057	1.0953 ⁺ +03	NM	13.3395	1.4661	1.6231 ⁺ +03	1.5159 ⁺ +03		
4.7625 ⁻ -01	1.1266 ⁺ +06	1.0708	3.6564 ⁺ +03	2.7049 ⁻ -04	1.8508	1.8030	2.2306 ⁺ +02	6.1094 ⁺ +01		
5.9098 ⁻ -02	4.0394 ⁺ +02	1.0000	2.2327 ⁻ -04	NM	-0.3107	4.5903 ⁻ -04	8.3012 ⁺ +02	3.6828 ⁺ +02		
65030404	4.5700	0.6503	1.6688 ⁺ +03	NM	6.4315	1.4785	4.7052 ⁺ +03	3.8721 ⁺ +03		
8.3820 ⁻ -01	1.2223 ⁺ +06	1.2152	4.6452 ⁺ +03	2.8613 ⁻ -04	1.0736	1.8487	2.3972 ⁺ +02	7.7733 ⁺ +01		
1.1553 ⁻ -01	4.0242 ⁺ +02	1.0000	1.8469 ⁻ -04	NM	-0.3656	2.8378 ⁻ -04	8.0784 ⁺ +02	3.6865 ⁺ +02		
65030405	4.2193	0.6569	2.3095 ⁺ +03	NM	5.5998	1.4896	7.2189 ⁺ +03	5.8074 ⁺ +03		
8.7630 ⁻ -01	1.1763 ⁺ +06	1.2431	5.7333 ⁺ +03	3.1597 ⁻ -04	1.8587	1.8358	2.4333 ⁺ +02	6.8406 ⁺ +01		
1.2747 ⁻ -01	4.0317 ⁺ +02	1.0000	1.9924 ⁻ -04	NM	-0.1926	2.9761 ⁻ -04	7.9541 ⁺ +02	3.7044 ⁺ +02		
65030406	3.3931	0.6514	3.6747 ⁺ +03	NM	3.1407	1.6216	2.3166 ⁺ +04	1.7966 ⁺ +04		
9.1440 ⁻ -01	1.1761 ⁺ +06	1.2895	6.7110 ⁺ +03	8.2411 ⁻ -04	1.8701	1.8595	2.4833 ⁺ +02	1.2408 ⁺ +02		
1.4531 ⁻ -01	4.0978 ⁺ +02	1.0000	1.5346 ⁻ -04	NM	0.0129	1.8369 ⁻ -04	7.5779 ⁺ +02	3.8007 ⁺ +02		
65030501	6.0432	0.7506	8.1483 ⁺ +02	NM	17.0164	1.5217	8.6520 ⁺ +02	8.6520 ⁺ +02		
-1.9050 ⁻ -01	1.4277 ⁺ +06	1.0000	4.0621 ⁺ +03	NM	1.8637	1.7800	2.7361 ⁺ +02	4.8317 ⁺ +01		
2.5400 ⁻ -02	4.0123 ⁺ +02	1.0000	2.6742 ⁻ -04	NM	-0.0984	6.8504 ⁻ -04	8.4222 ⁺ +02	3.6452 ⁺ +02		
65030502	5.9024	0.7523	9.7664 ⁺ +02	NM	16.5718	1.2865	8.9967 ⁺ +02	8.9967 ⁺ +02		
0.0000 ⁺ +00	1.2845 ⁺ +06	1.0000	4.6838 ⁺ +03	NM	1.0773	1.8332	2.7361 ⁺ +02	5.0211 ⁺ +01		
2.5400 ⁻ -02	4.0006 ⁺ +02	1.0000	3.2173 ⁻ -04	NM	-0.2299	7.7095 ⁻ -04	8.3857 ⁺ +02	3.6368 ⁺ +02		
65030503	5.7855	0.7491	7.4420 ⁺ +02	NM	19.6500	1.4662	1.2770 ⁺ +03	1.2770 ⁺ +03		
4.7625 ⁻ -01	1.6136 ⁺ +06	1.0000	3.4272 ⁺ +03	1.7498 ⁻ -04	1.8601	1.8079	2.7556 ⁺ +02	5.2561 ⁺ +01		
5.9098 ⁻ -02	4.0443 ⁺ +02	1.0000	1.8130 ⁻ -04	NM	-0.5391	4.4391 ⁻ -04	8.4097 ⁺ +02	3.6783 ⁺ +02		
65030504	4.7880	0.7523	7.2218 ⁺ +02	NM	15.7146	1.5559	2.7756 ⁺ +03	2.7756 ⁺ +03		
7.3660 ⁻ -01	1.1434 ⁺ +06	1.0000	2.4297 ⁺ +03	NM	1.9049	1.8935	2.7833 ⁺ +02	7.2411 ⁺ +01		
9.2961 ⁻ -02	4.0449 ⁺ +02	1.0000	1.1569 ⁻ -04	NM	-0.7889	2.0169 ⁻ -04	8.1699 ⁺ +02	3.6995 ⁺ +02		
65030505	4.8082	0.7631	3.0816 ⁺ +03	NM	-1.2339	1.2913	4.8603 ⁺ +03	2.9451 ⁺ +03		
8.3820 ⁻ -01	1.2422 ⁺ +06	1.6503	1.0562 ⁺ +04	2.6161 ⁻ -04	1.9185	1.8951	2.8111 ⁺ +02	7.1633 ⁺ +01		
1.1553 ⁻ -01	4.0264 ⁺ +02	1.0000	4.6444 ⁻ -04	NM	-0.1684	5.0332 ⁻ -04	8.1592 ⁺ +02	3.6840 ⁺ +02		
65030506	4.2694	0.7658	2.3616 ⁺ +03	NM	2.9983	1.4081	7.3707 ⁺ +03	5.2922 ⁺ +03		
8.7630 ⁻ -01	1.1436 ⁺ +06	1.3927	6.7492 ⁺ +03	2.9931 ⁻ -04	1.9088	1.8862	2.8194 ⁺ +02	6.6289 ⁺ +01		
1.2747 ⁻ -01	4.0086 ⁺ +02	1.0000	2.4540 ⁻ -04	NM	-0.3125	3.0311 ⁻ -04	7.9516 ⁺ +02	3.6815 ⁺ +02		
65030507	4.3899	0.7679	1.0183 ⁺ +04	NM	-6.0477	1.2875	2.4207 ⁺ +04	5.0111 ⁺ +03		
9.1440 ⁻ -01	1.2628 ⁺ +06	4.8307	3.0403 ⁺ +04	1.0823 ⁻ -03	1.8875	1.8917	2.8333 ⁺ +02	8.2850 ⁺ +01		
1.4531 ⁻ -01	4.0217 ⁺ +02	1.0000	1.0690 ⁻ -03	NM	-0.0380	5.1356 ⁻ -04	8.0114 ⁺ +02	3.6896 ⁺ +02		
65030601	5.9710	0.9935	6.8475 ⁺ +02	NM	16.6523	1.4281	8.6520 ⁺ +02	8.6520 ⁺ +02		
-1.9050 ⁻ -01	1.3259 ⁺ +06	1.0000	4.1339 ⁺ +03	NM	1.8630	1.7826	3.6389 ⁺ +02	4.9572 ⁺ +01		
2.5400 ⁻ -02	4.0305 ⁺ +02	1.0000	2.8630 ⁻ -04	NM	-0.1254	7.3969 ⁻ -04	8.4289 ⁺ +02	3.6628 ⁺ +02		
65030602	5.8082	0.9897	8.3897 ⁺ +02	NM	15.9494	1.3912	9.0206 ⁺ +02	9.0206 ⁺ +02		
0.0000 ⁺ +00	1.1674 ⁺ +06	1.0000	4.8149 ⁺ +03	NM	1.8583	1.7864	3.6222 ⁺ +02	5.1950 ⁺ +01		
2.5400 ⁻ -02	4.0246 ⁺ +02	1.0000	3.5287 ⁻ -04	NM	-0.1790	8.9901 ⁻ -04	8.3936 ⁺ +02	3.6601 ⁺ +02		
65030603	5.6517	0.9689	5.9483 ⁺ +02	NM	21.8168	1.5089	1.3143 ⁺ +03	1.3143 ⁺ +03		
4.7625 ⁻ -01	1.4412 ⁺ +06	1.0000	3.2008 ⁺ +03	1.5322 ⁻ -05	1.8610	1.7922	3.5694 ⁺ +02	5.4783 ⁺ +01		
5.9098 ⁻ -02	4.0479 ⁺ +02	1.0000	1.7925 ⁻ -04	NM	-0.9252	4.4750 ⁻ -04	8.3075 ⁺ +02	3.6839 ⁺ +02		
65030604	4.9112	0.9633	9.5553 ⁺ +02	NM	12.3911	1.4087	2.6621 ⁺ +03	2.4223 ⁺ +03		
7.3660 ⁻ -01	1.1548 ⁺ +06	1.0990	4.0468 ⁺ +03	NM	1.9016	1.8693	3.5500 ⁺ +02	6.9244 ⁺ +01		
9.2961 ⁻ -02	4.0328 ⁺ +02	1.0000	2.0133 ⁻ -04	NM	-0.8508	3.5418 ⁻ -04	8.1939 ⁺ +02	3.6854 ⁺ +02		
65030605	4.6604	0.9643	2.1849 ⁺ +03	NM	4.5887	1.3283	4.6808 ⁺ +03	3.3234 ⁺ +03		
8.3820 ⁻ -01	1.1723 ⁺ +06	1.4084	8.5166 ⁺ +03	2.1636 ⁻ -06	1.9038	1.8764	3.5500 ⁺ +02	7.5256 ⁺ +01		
1.1553 ⁻ -01	4.0215 ⁺ +02	1.0000	3.6862 ⁻ -04	NM	-0.4053	5.0214 ⁻ -04	8.1059 ⁺ +02	3.6815 ⁺ +02		
65030606	4.4140	0.9668	1.4767 ⁺ +03	NM	2.3036	1.5587	7.0877 ⁺ +03	4.5151 ⁺ +03		
8.7630 ⁻ -01	1.1731 ⁺ +06	1.5698	5.2800 ⁺ +03	1.6055 ⁻ -05	1.7745	1.7861	3.5556 ⁺ +02	8.1878 ⁺ +01		
1.2747 ⁻ -01	4.0093 ⁺ +02	1.0000	2.0134 ⁻ -04	NM	-1.9513	2.6893 ⁻ -04	8.0080 ⁺ +02	3.6775 ⁺ +02		
65030607	3.5133	0.9690	4.2477 ⁺ +03	NM	-0.0257	1.4230	2.2994 ⁺ +04	1.1704 ⁺ +04		
9.1440 ⁻ -01	1.3813 ⁺ +06	1.9647	1.2339 ⁺ +04	1.9854 ⁻ -03	1.8923	1.8876	3.5611 ⁺ +02	1.0192 ⁺ +02		
1.4531 ⁻ -01	3.9854 ⁺ +02	1.0000	2.9009 ⁻ -04	NM	-0.1860	2.6827 ⁻ -04	7.7188 ⁺ +02	3.6751 ⁺ +02		

CAT 6503		STROUD		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN	MO	T//TR	RED2W	CF	H12	H12K	PW*	PD*	
X *	POD	P//PD	RED2D	CG *	H32	H32K	TW*	TD*	
RZ *	TOO	S//S	O2	PI2	H42	O2K	UD*	TR	
65030701	7.8105	0.4093	6.5243 ⁺ +02	NM	30.2895	1.3820	5.2572 ⁺ +02	5.2572 ⁺ +02	
-1.9050 ⁻ -01	4.3939 ⁺ +06	1.0000	2.7809 ⁺ +03	NM	1.8566	1.7956	2.8278 ⁺ +02	5.7906 ⁺ +01	
2.5400 ⁻ -02	7.6439 ⁺ +02	1.0000	3.0630 ⁻ -04	NM	-0.6330	9.9082 ⁻ -04	1.1916 ⁺ +03	6.9092 ⁺ +02	
65030702	7.6275	0.4059	9.0140 ⁺ +02	NM	23.6304	1.3624	5.2477 ⁺ +02	5.2477 ⁺ +02	
0.0000 ⁺ +00	3.7634 ⁺ +06	1.0000	3.6557 ⁺ +03	NM	1.8464	1.7709	2.8000 ⁺ +02	6.0372 ⁺ +01	
2.5400 ⁻ -02	7.6285 ⁺ +02	1.0000	4.3986 ⁻ -04	NM	-0.1672	1.4087 ⁻ -03	1.1883 ⁺ +03	6.8980 ⁺ +02	
65030703	7.0137	0.4083	9.9829 ⁺ +02	NM	22.6164	1.4168	1.0337 ⁺ +03	9.3031 ⁺ +02	
4.7625 ⁻ -01	3.8995 ⁺ +06	1.1112	3.4973 ⁺ +03	3.5288 ⁻ -04	1.8353	1.7913	2.8000 ⁺ +02	6.9861 ⁺ +01	
5.9098 ⁻ -02	7.5718 ⁺ +02	1.0000	3.2146 ⁻ -04	NM	-0.5202	9.2952 ⁻ -04	1.1754 ⁺ +03	6.8570 ⁺ +02	
65030704	6.2351	0.4176	1.8491 ⁺ +03	NM	11.4023	1.3377	2.2710 ⁺ +03	1.8487 ⁺ +03	
7.3660 ⁻ -01	3.7007 ⁺ +06	1.2284	5.3605 ⁺ +03	5.4356 ⁻ -04	1.8736	1.8430	2.8672 ⁺ +02	6.8183 ⁺ +01	
9.2961 ⁻ -02	7.5629 ⁺ +02	1.0000	3.8137 ⁻ -04	NM	0.0346	7.1066 ⁻ -04	1.1606 ⁺ +03	6.8660 ⁺ +02	
65030705	5.7688	0.4433	2.4435 ⁺ +03	NM	2.9563	1.3257	4.3767 ⁺ +03	3.0375 ⁺ +03	
8.3820 ⁻ -01	3.7714 ⁺ +06	1.4409	6.5523 ⁺ +03	7.2676 ⁻ -04	1.8877	1.8787	2.9419 ⁺ +02	9.5306 ⁺ +01	
1.1553 ⁻ -01	7.2965 ⁺ +02	1.0000	3.5565 ⁻ -04	NM	0.4543	4.1797 ⁻ -04	1.1292 ⁺ +03	6.6368 ⁺ +02	
65030706	5.2998	0.4432	2.8434 ⁺ +03	NM	2.4924	1.3742	7.1772 ⁺ +03	4.9235 ⁺ +03	
8.7630 ⁻ -01	3.6703 ⁺ +06	1.4577	6.6254 ⁺ +03	8.4558 ⁻ -04	1.8881	1.8763	2.9941 ⁺ +02	1.1196 ⁺ +02	
1.2747 ⁻ -01	7.4090 ⁺ +02	1.0000	3.0535 ⁻ -04	NM	0.5823	3.4985 ⁻ -04	1.1243 ⁺ +03	6.7549 ⁺ +02	
65030707	4.2992	0.4547	4.3544 ⁺ +03	NM	-0.6477	1.8168	2.9116 ⁺ +04	1.5868 ⁺ +04	
9.1440 ⁻ -01	3.5626 ⁺ +06	1.8349	7.5934 ⁺ +03	1.2011 ⁻ -03	1.8038	1.8332	3.0987 ⁺ +02	1.5805 ⁺ +02	
1.4531 ⁻ -01	7.4229 ⁺ +02	1.0000	2.1818 ⁻ -04	NM	0.7740	1.4544 ⁻ -04	1.0837 ⁺ +03	6.8153 ⁺ +02	
65030801	7.8454	0.4632	7.6149 ⁺ +02	NM	25.9710	1.4709	5.2572 ⁺ +02	5.2572 ⁺ +02	
-1.9050 ⁻ -01	4.5228 ⁺ +06	1.0000	3.6075 ⁺ +03	NM	1.8466	1.7549	3.1722 ⁺ +02	5.6933 ⁺ +01	
2.5400 ⁻ -02	7.5779 ⁺ +02	1.0000	3.8560 ⁻ -04	NM	-0.2381	1.2474 ⁻ -03	1.1869 ⁺ +03	6.8491 ⁺ +02	
65030802	7.7098	0.4590	1.1572 ⁺ +03	NM	18.1712	1.4317	5.2477 ⁺ +02	5.2477 ⁺ +02	
0.0000 ⁺ +00	4.0331 ⁺ +06	1.0000	5.2569 ⁺ +03	NM	1.8137	1.7270	3.1820 ⁺ +02	5.9494 ⁺ +01	
2.5400 ⁻ -02	7.6678 ⁺ +02	1.0000	6.1211 ⁻ -04	NM	0.3598	1.9353 ⁻ -03	1.1923 ⁺ +03	6.9322 ⁺ +02	
65030803	7.0626	0.4693	1.1860 ⁺ +03	NM	17.3681	1.4048	1.0548 ⁺ +03	9.0589 ⁺ +02	
4.7625 ⁻ -01	3.9687 ⁺ +06	1.1644	4.6832 ⁺ +03	3.6168 ⁻ -04	1.8346	1.7928	3.2190 ⁺ +02	6.9011 ⁺ +01	
5.9098 ⁻ -02	7.5747 ⁺ +02	1.0000	4.3104 ⁻ -04	NM	-0.0705	1.1382 ⁻ -03	1.1763 ⁺ +03	6.8587 ⁺ +02	
65030804	6.3789	0.4660	2.2775 ⁺ +03	NM	6.9862	1.3239	2.3437 ⁺ +03	1.7251 ⁺ +03	
7.3660 ⁻ -01	3.9794 ⁺ +06	1.3586	7.4375 ⁺ +03	3.3803 ⁻ -04	1.8724	1.8395	3.2634 ⁺ +02	8.4461 ⁺ +01	
9.2961 ⁻ -02	7.7182 ⁺ +02	1.0000	5.3793 ⁻ -04	NM	0.6224	8.5207 ⁻ -04	1.1754 ⁺ +03	7.0033 ⁺ +02	
65030805	5.9765	0.4803	2.2229 ⁺ +03	NM	4.2310	1.3375	4.5338 ⁺ +03	2.5798 ⁺ +03	
8.3820 ⁻ -01	3.9762 ⁺ +06	1.7574	8.6643 ⁺ +03	8.4229 ⁻ -04	1.8880	1.8609	3.3226 ⁺ +02	9.3483 ⁺ +01	
1.1553 ⁻ -01	7.6130 ⁺ +02	1.0000	3.9962 ⁻ -04	NM	-0.1613	5.2283 ⁻ -04	1.1586 ⁺ +03	6.9185 ⁺ +02	
65030806	5.6557	0.4884	3.1277 ⁺ +03	NM	2.2028	1.3532	7.5086 ⁺ +03	3.6039 ⁺ +03	
8.7630 ⁻ -01	3.9680 ⁺ +06	2.0834	8.6184 ⁺ +03	1.0971 ⁻ -03	1.8731	1.8582	3.3448 ⁺ +02	1.0257 ⁺ +02	
1.2747 ⁻ -01	7.5874 ⁺ +02	1.0000	4.4774 ⁻ -04	NM	-0.2119	5.1451 ⁻ -04	1.1488 ⁺ +03	6.9049 ⁺ +02	
65030807	4.8959	0.4899	6.3889 ⁺ +03	NM	-0.6233	1.4818	3.1158 ⁺ +04	8.4121 ⁺ +03	
9.1440 ⁻ -01	3.9385 ⁺ +06	3.7039	1.4175 ⁺ +04	1.7499 ⁻ -03	1.7993	1.7988	3.3744 ⁺ +02	1.3007 ⁺ +02	
1.4531 ⁻ -01	7.5364 ⁺ +02	1.0000	5.1312 ⁻ -04	NM	0.0461	3.9476 ⁻ -04	1.1195 ⁺ +03	6.8879 ⁺ +02	

CAT 6503		STROUD		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.				
RUN X *	MO POD	T//TR PH/PO	RED2W RED2D	CF CQ *	H12 H32	H12K H32K	PN* TW*	PD* TR
RZ *	TD	SN *	D2	PI2	H42	D2K	UD*	TD*
65030901	7.7309	0.7523	3.2796 ⁺⁰²	NM	44.7305	1.4841	5.2572 ⁺⁰²	5.2572 ⁺⁰²
-1.9050 ⁻⁰¹	4.1126 ⁺⁰⁶	1.0000	2.1616 ⁺⁰³	NM	1.8169	1.7434	5.0333 ⁺⁰²	5.7133 ⁺⁰¹
2.5400 ⁻⁰²	7.4008 ⁺⁰²	1.0000	2.3571 ⁻⁰⁴	NM	-1.9692	1.0536 ⁻⁰³	1.1716 ⁺⁰³	6.6905 ⁺⁰²
65030902	7.6059	0.7483	3.4066 ⁺⁰²	NM	45.4186	1.7223	5.2477 ⁺⁰²	5.2477 ⁺⁰²
0.0000 ⁺⁰⁰	3.6953 ⁺⁰⁶	1.0000	2.2940 ⁺⁰³	NM	1.7279	1.7014	5.0363 ⁺⁰²	5.9211 ⁺⁰¹
2.5400 ⁻⁰²	7.4429 ⁺⁰²	1.0000	2.6882 ⁻⁰⁴	NM	-2.1197	1.4596 ⁻⁰³	1.1734 ⁺⁰³	6.7304 ⁺⁰²
65030903	6.9890	0.7386	6.7346 ⁺⁰²	NM	25.4372	1.7821	1.0108 ⁺⁰³	8.5706 ⁺⁰²
4.7625 ⁻⁰¹	3.5129 ⁺⁰⁶	1.1793	3.6295 ⁺⁰³	1.1434 ⁻⁰⁴	1.7570	1.6968	5.0213 ⁺⁰²	6.9700 ⁺⁰¹
5.9098 ⁻⁰²	7.5062 ⁺⁰²	1.0000	3.6216 ⁻⁰⁴	NM	-0.8870	1.2480 ⁻⁰³	1.1699 ⁺⁰³	6.7980 ⁺⁰²
65030904	6.3081	0.7173	7.5093 ⁺⁰²	NM	18.6247	1.4899	2.1560 ⁺⁰³	1.7007 ⁺⁰³
7.3660 ⁻⁰¹	3.6598 ⁺⁰⁶	1.2677	3.3095 ⁺⁰³	3.2032 ⁻⁰⁵	1.8337	1.8007	4.8871 ⁺⁰²	5.3789 ⁺⁰¹
9.2961 ⁻⁰²	7.5062 ⁺⁰²	1.0000	2.4263 ⁻⁰⁴	NM	-1.4017	5.3120 ⁻⁰⁴	1.1577 ⁺⁰³	6.8127 ⁺⁰²
65030905	5.7454	0.6795	9.3353 ⁺⁰²	NM	7.7043	1.4551	4.1512 ⁺⁰³	3.0428 ⁺⁰³
8.3820 ⁻⁰¹	3.6856 ⁺⁰⁶	1.3643	3.3607 ⁺⁰³	4.3797 ⁻⁰⁴	1.8855	1.8368	4.7527 ⁺⁰²	1.0115 ⁺⁰²
1.1553 ⁻⁰¹	7.6893 ⁺⁰²	1.0000	1.9948 ⁻⁰⁴	NM	-0.4117	3.3037 ⁻⁰⁴	1.1588 ⁺⁰³	6.9948 ⁺⁰²
65030906	5.3917	0.6631	1.1397 ⁺⁰³	NM	4.1378	1.4977	6.6022 ⁺⁰³	4.4629 ⁺⁰³
8.7630 ⁻⁰¹	3.6860 ⁺⁰⁶	1.4793	3.6292 ⁺⁰³	5.4780 ⁻⁰⁴	1.8979	1.8685	4.7005 ⁺⁰²	1.1416 ⁺⁰²
1.2747 ⁻⁰¹	7.7787 ⁺⁰²	1.0000	1.8653 ⁻⁰⁴	NM	-0.2036	2.4792 ⁻⁰⁴	1.1550 ⁺⁰³	7.0884 ⁺⁰²
65030907	4.5538	0.6627	3.1649 ⁺⁰³	NM	0.0930	1.6217	2.5504 ⁺⁰⁴	1.2755 ⁺⁰⁴
9.1440 ⁻⁰¹	3.9470 ⁺⁰⁶	1.9995	7.8459 ⁺⁰³	8.6320 ⁻⁰⁴	1.8233	1.8200	4.6259 ⁺⁰²	1.4000 ⁺⁰²
1.4531 ⁻⁰¹	7.6182 ⁺⁰²	1.0000	2.4161 ⁻⁰⁴	NM	0.2702	2.1562 ⁻⁰⁴	1.1108 ⁺⁰³	6.9799 ⁺⁰²
65031001	7.6682	0.9378	4.3773 ⁺⁰²	NM	29.7280	1.6010	5.2572 ⁺⁰²	5.2572 ⁺⁰²
-1.9050 ⁻⁰¹	3.9019 ⁺⁰⁶	1.0000	3.2599 ⁺⁰³	NM	1.8038	1.7144	6.4722 ⁺⁰²	5.9822 ⁺⁰¹
2.5400 ⁻⁰²	7.6335 ⁺⁰²	1.0000	3.8412 ⁻⁰⁴	NM	-0.6066	1.6431 ⁻⁰³	1.1891 ⁺⁰³	6.9018 ⁺⁰²
65031002	7.6148	0.9297	5.6213 ⁺⁰²	NM	23.4690	1.3949	5.2477 ⁺⁰²	5.2477 ⁺⁰²
0.0000 ⁺⁰⁰	3.7232 ⁺⁰⁶	1.0000	4.1162 ⁺⁰³	NM	1.8242	1.7402	6.3884 ⁺⁰²	6.0322 ⁺⁰¹
2.5400 ⁻⁰²	7.5989 ⁺⁰²	1.0000	4.9547 ⁻⁰⁴	NM	-0.1606	1.7904 ⁻⁰³	1.1858 ⁺⁰³	6.8713 ⁺⁰²
65031003	7.0969	0.8962	7.1759 ⁺⁰²	NM	14.0007	1.3024	9.5952 ⁺⁰²	8.7717 ⁺⁰²
4.7625 ⁻⁰¹	3.9631 ⁺⁰⁶	1.0939	3.4525 ⁺⁰³	3.7581 ⁻⁰⁵	1.8818	1.8382	6.4032 ⁺⁰²	7.1267 ⁺⁰¹
5.9098 ⁻⁰²	7.8915 ⁺⁰²	1.0000	4.4198 ⁻⁰⁴	NM	0.4096	9.4388 ⁻⁰⁴	1.2012 ⁺⁰³	7.1444 ⁺⁰²
65031004	6.2403	0.9028	6.2515 ⁺⁰²	NM	13.8654	1.3814	2.1125 ⁺⁰³	1.8549 ⁺⁰³
7.3660 ⁻⁰¹	3.7340 ⁺⁰⁶	1.1389	3.1173 ⁺⁰³	2.7597 ⁻⁰⁵	1.9019	1.8805	6.4106 ⁺⁰²	8.8994 ⁺⁰¹
9.2961 ⁻⁰²	7.8221 ⁺⁰²	1.0000	2.3156 ⁻⁰⁴	NM	-0.2265	4.0290 ⁻⁰⁴	1.1604 ⁺⁰³	7.1011 ⁺⁰²
65031005	5.7736	0.9563	8.7173 ⁺⁰²	NM	5.1246	1.3858	4.1933 ⁺⁰³	2.9102 ⁺⁰³
8.3820 ⁻⁰¹	3.6313 ⁺⁰⁶	1.4409	4.0333 ⁺⁰³	7.7338 ⁻⁰⁶	1.9158	1.9026	6.4106 ⁺⁰²	9.6128 ⁺⁰¹
1.1553 ⁻⁰¹	7.3699 ⁺⁰²	1.0000	2.3121 ⁻⁰⁴	NM	-0.6857	3.0527 ⁻⁰⁴	1.1350 ⁺⁰³	6.7034 ⁺⁰²
65031006	5.4349	0.9430	1.2648 ⁺⁰³	NM	3.0532	1.3904	6.6822 ⁺⁰³	4.3035 ⁺⁰³
8.7630 ⁻⁰¹	3.7278 ⁺⁰⁶	1.5927	5.2348 ⁺⁰³	6.7542 ⁻⁰⁶	1.9112	1.8987	6.4032 ⁺⁰²	1.0789 ⁺⁰²
1.2747 ⁻⁰¹	7.4529 ⁺⁰²	1.0000	2.5512 ⁻⁰⁴	NM	0.1304	3.0309 ⁻⁰⁴	1.1319 ⁺⁰³	6.7900 ⁺⁰²
65031007	4.3418	0.9179	1.3390 ⁺⁰³	NM	0.4062	1.8255	2.6448 ⁺⁰⁴	1.5258 ⁺⁰⁴
9.1440 ⁻⁰¹	3.6172 ⁺⁰⁶	1.7334	3.8724 ⁺⁰³	1.9327 ⁻⁰⁶	1.9268	1.9285	6.4032 ⁺⁰²	1.5934 ⁺⁰²
1.4531 ⁻⁰¹	7.6010 ⁺⁰²	1.0000	1.1588 ⁻⁰⁴	NM	-0.0091	1.0564 ⁻⁰⁴	1.0989 ⁺⁰³	6.9762 ⁺⁰²

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PDD RED2PMD	RED2PDW RED2PWH	UBTAH
65030101	4.6191 ⁻⁰⁴ 4.6192 ⁻⁰⁴	11.6043 11.6042	1.8298 1.8298	-0.1812 -0.1812	8.4735 ⁺⁰³ 8.4736 ⁺⁰³	2.4329 ⁺⁰³ 2.4329 ⁺⁰³	5.3468 ⁻⁰³
65030102	6.7817 ⁻⁰⁴ 6.7817 ⁻⁰⁴	10.6305 10.6305	1.7978 1.7978	-0.0196 -0.0196	1.2693 ⁺⁰⁴ 1.2693 ⁺⁰⁴	3.6173 ⁺⁰³ 3.6173 ⁺⁰³	7.1991 ⁻⁰³
65030103	6.4656 ⁻⁰⁴ 6.4653 ⁻⁰⁴	10.4710 10.4709	1.8596 1.8597	-0.1536 -0.1536	1.4370 ⁺⁰⁴ 1.4371 ⁺⁰⁴	4.5591 ⁺⁰³ 4.5594 ⁺⁰³	6.7564 ⁻⁰³
65030104	5.5564 ⁻⁰⁴ 5.0517 ⁻⁰⁴	9.5756 9.5392	1.8898 1.9018	-0.2816 -0.2798	1.4120 ⁺⁰⁴ 1.4211 ⁺⁰⁴	5.0833 ⁺⁰³ 5.1161 ⁺⁰³	4.8296 ⁻⁰³
65030105	2.9057 ⁻⁰⁴ 2.5017 ⁻⁰⁴	8.8840 8.7953	1.8666 1.8684	-0.3004 -0.2909	8.3545 ⁺⁰³ 8.6548 ⁺⁰³	3.4551 ⁺⁰³ 3.4956 ⁺⁰³	2.2142 ⁻⁰³
65030106	2.9656 ⁻⁰⁴ 2.4978 ⁻⁰⁴	7.8802 7.7503	1.8469 1.8812	-0.2272 -0.2231	9.6466 ⁺⁰³ 9.8261 ⁺⁰³	4.2109 ⁺⁰³ 4.2693 ⁺⁰³	1.9798 ⁻⁰³
65030107	1.7077 ⁻⁰⁴ 1.4089 ⁻⁰⁴	6.0415 5.8686	1.8652 1.9215	-0.3086 -0.2996	8.5408 ⁺⁰³ 8.7967 ⁺⁰³	4.9634 ⁺⁰³ 5.1133 ⁺⁰³	8.3027 ⁻⁰⁴
65030301	5.9956 ⁻⁰⁴ 5.9956 ⁻⁰⁴	10.1510 10.1510	1.8312 1.8312	0.0687 0.0687	1.1192 ⁺⁰⁴ 1.1192 ⁺⁰⁴	2.5329 ⁺⁰³ 2.5329 ⁺⁰³	6.0632 ⁻⁰³
65030302	7.0016 ⁻⁰⁴ 7.0016 ⁻⁰⁴	11.3641 11.3641	1.7915 1.7915	-0.1236 -0.1236	1.3100 ⁺⁰⁴ 1.3100 ⁺⁰⁴	2.9742 ⁺⁰³ 2.9742 ⁺⁰³	7.9433 ⁻⁰³
65030303	5.6119 ⁻⁰⁴ 5.6118 ⁻⁰⁴	14.0103 14.0103	1.8622 1.8622	-0.2743 -0.2743	1.5196 ⁺⁰⁴ 1.5196 ⁺⁰⁴	3.1167 ⁺⁰³ 3.1167 ⁺⁰³	7.8530 ⁻⁰³
65030304	7.0038 ⁻⁰⁴ 6.2317 ⁻⁰⁴	9.8511 9.8130	1.8650 1.8797	-0.3099 -0.3074	1.7935 ⁺⁰⁴ 1.8078 ⁺⁰⁴	5.0819 ⁺⁰³ 5.1223 ⁺⁰³	6.1604 ⁻⁰³
65030305	7.5094 ⁻⁰⁴ 6.2445 ⁻⁰⁴	8.9344 8.8487	1.8505 1.8772	-0.3621 -0.3567	2.1946 ⁺⁰⁴ 2.2269 ⁺⁰⁴	6.8747 ⁺⁰³ 6.9760 ⁺⁰³	5.5973 ⁻⁰³
65030306	6.7173 ⁻⁰⁴ 6.4062 ⁻⁰⁴	8.8703 8.5042	1.8275 1.8777	-0.4903 -0.4768	2.6734 ⁺⁰⁴ 2.7477 ⁺⁰⁴	6.7356 ⁺⁰³ 6.9784 ⁺⁰³	5.5597 ⁻⁰³
65030307	1.3615 ⁻⁰³ 0.8168 ⁻⁰⁴	5.2596 4.8695	1.7082 1.8672	-0.0055 -0.0051	4.8123 ⁺⁰⁴ 5.2658 ⁺⁰⁴	1.7483 ⁺⁰⁴ 1.9131 ⁺⁰⁴	3.3901 ⁻⁰³
65030801	3.8539 ⁻⁰⁴ 3.8540 ⁻⁰⁴	25.9853 25.9850	1.8465 1.8466	-0.2342 -0.2342	3.6094 ⁺⁰³ 3.6094 ⁺⁰³	7.6199 ⁺⁰² 7.6200 ⁺⁰²	9.9563 ⁻⁰³
65030802	6.1236 ⁻⁰⁴ 6.1237 ⁻⁰⁴	18.1634 18.1637	1.8138 1.8138	0.3596 0.3596	5.2655 ⁺⁰³ 5.2654 ⁺⁰³	1.1591 ⁺⁰³ 1.1591 ⁺⁰³	1.1102 ⁻⁰²
65030803	4.1987 ⁻⁰⁴ 3.7481 ⁻⁰⁴	21.1676 21.2541	1.8290 1.8335	-0.0730 -0.0729	4.5237 ⁺⁰³ 4.5352 ⁺⁰³	1.1456 ⁺⁰³ 1.1486 ⁺⁰³	8.0538 ⁻⁰³
65030804	5.0972 ⁻⁰⁴ 4.1438 ⁻⁰⁴	10.9134 10.9058	1.8661 1.8774	0.6568 0.6530	7.0559 ⁺⁰³ 7.0995 ⁺⁰³	2.1606 ⁺⁰³ 2.1740 ⁺⁰³	4.6003 ⁻⁰³
65030805	3.2621 ⁻⁰⁴ 2.2364 ⁻⁰⁴	15.5592 15.4664	1.8635 1.8875	-0.1977 -0.1951	5.4464 ⁺⁰³ 5.5173 ⁺⁰³	1.8168 ⁺⁰³ 1.8403 ⁺⁰³	3.5355 ⁻⁰³
65030806	3.5031 ⁻⁰⁴ 2.1532 ⁻⁰⁴	14.0667 13.9043	1.8432 1.8785	-0.2708 -0.2656	6.7504 ⁺⁰³ 6.8604 ⁺⁰³	2.4498 ⁺⁰³ 2.4870 ⁺⁰³	3.0636 ⁻⁰³
65030807	3.7915 ⁻⁰⁴ 1.6448 ⁻⁰⁴	8.6166 8.2466	1.7434 1.8331	0.0624 0.0594	1.0486 ⁺⁰⁴ 1.1029 ⁺⁰⁴	4.7264 ⁺⁰³ 4.9708 ⁺⁰³	1.3962 ⁻⁰³
65031001	3.8473 ⁻⁰⁴ 3.8469 ⁻⁰⁴	29.6828 29.6842	1.8040 1.8040	-0.6057 -0.6057	3.2689 ⁺⁰³ 3.2687 ⁺⁰³	4.3894 ⁺⁰² 4.3892 ⁺⁰²	1.1392 ⁻⁰²
65031002	4.9542 ⁻⁰⁴ 4.9542 ⁻⁰⁴	23.4711 23.4709	1.8242 1.8242	-0.1607 -0.1607	4.1207 ⁺⁰³ 4.1207 ⁺⁰³	5.6275 ⁺⁰² 5.6275 ⁺⁰²	1.1601 ⁻⁰²
65031003	4.3174 ⁻⁰⁴ 4.0578 ⁻⁰⁴	16.1650 16.1931	1.8793 1.8820	0.4196 0.4190	4.3516 ⁺⁰³ 4.3581 ⁺⁰³	7.0133 ⁺⁰² 7.0238 ⁺⁰²	6.6324 ⁻⁰³
65031004	2.1572 ⁻⁰⁴ 1.9737 ⁻⁰⁴	18.7523 18.7387	1.8952 1.9000	-0.2430 -0.2424	2.9074 ⁺⁰³ 2.9150 ⁺⁰³	5.8309 ⁺⁰² 5.8457 ⁺⁰²	3.7198 ⁻⁰³
65031005	1.7125 ⁻⁰⁴ 1.3417 ⁻⁰⁴	20.4746 20.3680	1.8896 1.9057	-0.9257 -0.9177	2.9910 ⁺⁰³ 3.0164 ⁺⁰³	6.4646 ⁺⁰² 6.5200 ⁺⁰²	2.7519 ⁻⁰³
65031006	2.0962 ⁻⁰⁴ 1.5669 ⁻⁰⁴	11.3985 11.2932	1.8944 1.9166	0.1587 0.1569	4.3069 ⁺⁰³ 4.3576 ⁺⁰³	1.0406 ⁺⁰³ 1.0528 ⁺⁰³	1.7864 ⁻⁰³
65031007	6.0926 ⁻⁰⁵ 5.7225 ⁻⁰⁵	9.1551 8.9521	1.9034 1.9480	-0.0073 -0.0072	2.7077 ⁺⁰³ 2.7713 ⁺⁰³	9.1627 ⁺⁰² 9.5826 ⁺⁰²	5.1559 ⁻⁰⁴

65030301		STROUD		PROFILE TABULATION			25 POINTS, DELTA AT POINT 19			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD		
1	0.0000 ⁺ 00	1.0000 ⁺ 00	1.00000	0.92198	0.00000	0.00000	5.21911	0.00000		
2	2.5400 ⁻ 04	1.6804 ⁺ 00	1.00000	0.94869	0.18520	0.39850	4.63016	0.08607		
3	4.5720 ⁻ 04	2.2245 ⁺ 00	1.00000	0.96185	0.23506	0.48912	4.32979	0.11297		
4	6.8580 ⁻ 04	3.5840 ⁺ 00	1.00000	0.97415	0.31993	0.61817	3.73330	0.16556		
5	8.6360 ⁻ 04	4.0369 ⁺ 00	1.00000	0.98210	0.34307	0.65003	3.59003	0.18107		
6	1.2954 ⁺ 03	5.3170 ⁺ 00	1.00000	0.98533	0.40099	0.71600	3.18834	0.22457		
7	1.7272 ⁻ 03	6.0447 ⁺ 00	1.00000	0.98667	0.43035	0.74510	2.99775	0.24855		
8	2.1590 ⁻ 03	6.9114 ⁺ 00	1.00000	0.98799	0.46283	0.77428	2.79861	0.27666		
9	2.6162 ⁻ 03	7.8564 ⁺ 00	1.00000	0.98917	0.49580	0.80093	2.60965	0.30691		
10	3.0480 ⁻ 03	8.5840 ⁺ 00	1.00000	0.98996	0.51974	0.81860	2.48070	0.32999		
11	3.4290 ⁻ 03	9.5891 ⁺ 00	1.00000	0.99083	0.55109	0.83977	2.32206	0.36165		
12	4.3180 ⁻ 03	1.1499 ⁺ 01	1.00000	0.99222	0.60619	0.87227	2.07055	0.42127		
13	5.5880 ⁻ 03	1.3386 ⁺ 01	1.00000	1.00776	0.65605	0.90377	1.89778	0.47623		
14	6.8320 ⁻ 03	1.6854 ⁺ 01	1.00000	0.99426	0.73897	0.93110	1.58760	0.58649		
15	8.1280 ⁻ 03	1.9500 ⁺ 01	1.00000	0.99513	0.79644	0.95034	1.42383	0.66746		
16	9.3980 ⁻ 03	2.1800 ⁺ 01	1.00000	0.99621	0.84320	0.96409	1.30730	0.73747		
17	1.1506 ⁺ 02	2.6953 ⁺ 01	1.00000	0.99713	0.93956	0.98705	1.10366	0.89434		
18	1.3665 ⁻ 02	3.0084 ⁺ 01	1.00000	0.99877	0.99355	0.99824	1.00945	0.98839		
D 19	1.4732 ⁻ 02	3.0470 ⁺ 01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
20	1.5824 ⁻ 02	3.0481 ⁺ 01	1.00000	1.00138	1.00018	1.00072	1.00168	0.99964		
21	1.7932 ⁻ 02	3.0521 ⁺ 01	1.00000	1.00427	1.00084	1.00228	1.00288	0.99941		
22	2.0066 ⁻ 02	3.0758 ⁺ 01	1.00000	1.00763	1.00478	1.00465	0.99973	1.00492		
23	2.2149 ⁻ 02	3.0800 ⁺ 01	1.00000	1.01132	1.00548	1.00661	1.00225	1.00435		
24	2.4333 ⁻ 02	3.0797 ⁺ 01	1.00000	1.01553	1.00545	1.00870	1.00648	1.00220		
25	2.6441 ⁻ 02	3.0839 ⁺ 01	1.00000	1.02005	1.00614	1.01106	1.00981	1.00124		

INPUT VARIABLES Y,U,T,P

65030302		STROUD		PROFILE TABULATION			29 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD		
1	0.0000 ⁺ 00	1.0000 ⁺ 00	1.00000	0.90682	0.00000	0.00000	5.19831	0.00000		
2	2.5400 ⁻ 04	1.3868 ⁺ 00	1.00000	0.92743	0.14385	0.31655	4.84225	0.06537		
3	4.3434 ⁻ 04	1.3275 ⁺ 00	1.00000	0.93384	0.13347	0.29635	4.93704	0.06007		
4	5.9430 ⁻ 04	1.7270 ⁺ 00	1.00000	0.94233	0.18895	0.40618	4.62110	0.08790		
5	7.4930 ⁻ 04	2.1626 ⁺ 00	1.00000	0.94873	0.22849	0.47716	4.36109	0.10941		
6	9.2552 ⁻ 04	3.0934 ⁺ 00	1.00000	0.95685	0.29038	0.57497	3.92059	0.14665		
7	1.2040 ⁺ 03	3.6129 ⁺ 00	1.00000	0.96047	0.31902	0.61497	3.71607	0.16549		
8	1.4224 ⁻ 03	3.6992 ⁺ 00	1.00000	0.96454	0.32351	0.62209	3.69772	0.16824		
9	1.8898 ⁻ 03	4.4510 ⁺ 00	1.00000	0.97205	0.36011	0.66917	3.45310	0.19379		
10	2.2708 ⁻ 03	4.9045 ⁺ 00	1.00000	0.97671	0.38041	0.69347	3.32314	0.20868		
11	2.7076 ⁻ 03	5.3377 ⁺ 00	1.00000	0.98487	0.40700	0.72404	3.16476	0.22878		
12	3.1267 ⁻ 03	6.0124 ⁺ 00	1.00000	0.99387	0.42582	0.74564	3.06619	0.24318		
13	3.3839 ⁻ 03	6.5453 ⁺ 00	1.00000	1.00398	0.44598	0.76790	2.96466	0.25902		
14	3.9827 ⁻ 03	7.0809 ⁺ 00	1.00000	1.01074	0.46535	0.78719	2.86150	0.27510		
15	4.3917 ⁻ 03	7.9527 ⁺ 00	1.00000	1.01812	0.48176	0.80345	2.78137	0.28847		
16	4.8616 ⁻ 03	8.2467 ⁺ 00	1.00000	1.02367	0.50491	0.82341	2.65950	0.30961		
17	5.9004 ⁻ 03	9.8087 ⁺ 00	1.00000	1.02871	0.53348	0.85872	2.40732	0.35671		
18	7.3782 ⁻ 03	1.2478 ⁺ 01	1.00000	1.02201	0.62774	0.89769	2.04497	0.43897		
19	8.2372 ⁻ 03	1.4515 ⁺ 01	1.00000	1.01755	0.67894	0.91932	1.83344	0.50142		
20	9.0856 ⁻ 03	1.6494 ⁺ 01	1.00000	1.01543	0.72523	0.93674	1.66832	0.56149		
21	9.9263 ⁻ 03	1.8553 ⁺ 01	1.00000	1.01556	0.77045	0.95248	1.52817	0.62320		
22	1.1478 ⁺ 02	2.2808 ⁺ 01	1.00000	1.01001	0.85633	0.97455	1.29517	0.75245		
23	1.2951 ⁻ 02	2.6155 ⁺ 01	1.00000	1.00366	0.91826	0.98596	1.15289	0.85521		
24	1.5060 ⁻ 02	2.9777 ⁺ 01	1.00000	1.00008	0.98087	0.99662	1.03238	0.96536		
D 25	1.7181 ⁻ 02	3.0931 ⁺ 01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
26	1.9398 ⁻ 02	3.1131 ⁺ 01	1.00000	0.99998	1.00327	1.00056	0.99480	1.00599		
27	2.1443 ⁻ 02	3.1207 ⁺ 01	1.00000	0.99995	1.00451	1.00076	0.99254	1.00828		
28	2.3604 ⁻ 02	3.1289 ⁺ 01	1.00000	0.99996	1.00585	1.00099	0.99038	1.01072		
29	2.5730 ⁻ 02	3.1289 ⁺ 01	1.00000	0.99996	1.00585	1.00099	0.99038	1.01072		

INPUT VARIABLES Y,U,T,P

65030303		STROUD	PROFILE TABULATION			27 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	1.00000	0.89487	0.00000	0.00000	5.73549	0.00000	
2	2.5400 ⁻ 04	2.6333 ⁺ 00	1.00000	0.92774	0.24511	0.51924	4.48772	0.11570	
3	4.8260 ⁻ 04	3.9490 ⁺ 00	1.00000	0.94907	0.31441	0.62594	3.96350	0.15793	
4	6.6040 ⁻ 04	5.1263 ⁺ 00	1.00000	0.96272	0.36473	0.69090	3.58829	0.19254	
5	8.8646 ⁻ 04	6.1313 ⁺ 00	1.00000	0.97486	0.40258	0.73457	3.32939	0.22063	
6	1.1049 ⁻ 03	6.7922 ⁺ 00	1.00000	0.98402	0.42560	0.75962	3.18560	0.23845	
7	1.3233 ⁻ 03	7.5531 ⁺ 00	1.00000	0.99443	0.45063	0.78534	3.03730	0.25857	
8	1.5799 ⁻ 03	8.0725 ⁺ 00	1.00000	1.00048	0.46693	0.80093	2.94234	0.27221	
9	1.6942 ⁻ 03	8.8685 ⁺ 00	1.00000	1.00267	0.49085	0.81998	2.79043	0.29383	
10	2.1717 ⁻ 03	9.5635 ⁺ 00	1.00000	1.01515	0.51062	0.83907	2.69808	0.31099	
11	2.5857 ⁻ 03	9.8393 ⁺ 00	1.00000	1.01970	0.51853	0.84614	2.66279	0.31776	
12	2.9972 ⁻ 03	1.0737 ⁺ 01	1.00000	1.02320	0.54286	0.86311	2.52803	0.34143	
13	3.4823 ⁻ 03	1.0947 ⁺ 01	1.00000	1.02512	0.54838	0.86730	2.50135	0.34673	
14	3.7287 ⁻ 03	1.1468 ⁺ 01	1.00000	1.02547	0.56187	0.87539	2.42735	0.36064	
15	4.1504 ⁻ 03	1.1468 ⁺ 01	1.00000	1.02547	0.56187	0.87539	2.42735	0.36064	
16	4.5745 ⁻ 03	1.2090 ⁺ 01	1.00000	1.02408	0.57759	0.88360	2.34032	0.37756	
17	5.4204 ⁻ 03	1.2924 ⁺ 01	1.00000	1.02339	0.59797	0.89405	2.23544	0.39994	
18	6.7005 ⁻ 03	1.2992 ⁺ 01	1.00000	1.02140	0.59960	0.89401	2.22310	0.40214	
19	8.0035 ⁻ 03	1.4551 ⁺ 01	1.00000	1.02343	0.63588	0.91223	2.05806	0.44325	
20	9.2558 ⁻ 03	1.6769 ⁺ 01	1.00000	1.02692	0.68415	0.93395	1.86353	0.50117	
21	1.0579 ⁻ 02	1.9608 ⁺ 01	1.00000	1.02921	0.74137	0.95527	1.66028	0.57537	
22	1.1674 ⁻ 02	2.3213 ⁺ 01	1.00000	1.02462	0.80821	0.97275	1.44861	0.67150	
23	1.3076 ⁻ 02	2.7784 ⁺ 01	1.00000	1.01342	0.88571	0.98578	1.23874	0.79579	
24	1.5006 ⁻ 02	3.3692 ⁺ 01	1.00000	1.00315	0.97681	0.99784	1.04352	0.95623	
D 25	1.7120 ⁻ 02	3.5288 ⁺ 01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.9271 ⁻ 02	3.5195 ⁺ 01	1.00000	0.99885	0.99866	0.99921	1.00110	0.99811	
27	2.1389 ⁻ 02	3.5011 ⁺ 01	1.00000	0.99627	0.99601	0.99851	1.00501	0.99353	

INPUT VARIABLES Y,U,T,P

65030304		STROUD	PROFILE TABULATION			28 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	1.20338	0.89516	0.00000	0.00000	4.15089	0.00000	
2	2.5400 ⁻ 04	2.9183 ⁺ 00	1.20338	0.94148	0.31939	0.56994	3.18424	0.21539	
3	4.5866 ⁻ 04	3.4586 ⁺ 00	1.20338	0.95976	0.35455	0.61961	3.05411	0.24414	
4	6.8326 ⁻ 04	4.7567 ⁺ 00	1.20338	0.96622	0.42653	0.70038	2.69633	0.31298	
5	8.9908 ⁻ 04	5.0789 ⁺ 00	1.20338	0.97448	0.44250	0.71887	2.63916	0.32778	
6	1.1100 ⁻ 03	6.4104 ⁺ 00	1.20280	0.98268	0.50301	0.77487	2.37300	0.39276	
7	1.3183 ⁻ 03	7.2951 ⁺ 00	1.20222	0.99237	0.53941	0.80654	2.23573	0.43370	
8	1.5215 ⁻ 03	7.9348 ⁺ 00	1.20140	1.00660	0.56424	0.82984	2.16305	0.46091	
9	1.7018 ⁻ 03	8.2704 ⁺ 00	1.19977	1.01273	0.57683	0.84082	2.12475	0.47478	
10	2.1387 ⁻ 03	9.4461 ⁺ 00	1.19802	1.01951	0.61892	0.86988	1.97539	0.52756	
11	2.6035 ⁻ 03	1.0004 ⁺ 01	1.19615	1.02548	0.63790	0.88331	1.91742	0.55104	
12	3.0251 ⁻ 03	1.0622 ⁺ 01	1.19323	1.02761	0.65830	0.89531	1.84969	0.57756	
13	3.4163 ⁻ 03	1.0898 ⁺ 01	1.19020	1.02742	0.66723	0.89988	1.81896	0.58882	
14	3.8151 ⁻ 03	1.1169 ⁺ 01	1.18775	1.02736	0.67585	0.90433	1.79042	0.59993	
15	4.7117 ⁻ 03	1.1392 ⁺ 01	1.17935	1.02530	0.68285	0.90682	1.76355	0.60642	
16	5.5677 ⁻ 03	1.1453 ⁺ 01	1.16978	1.02326	0.68478	0.90686	1.75379	0.60488	
17	6.4643 ⁻ 03	1.1628 ⁺ 01	1.16009	1.02171	0.69023	0.90882	1.73369	0.60813	
18	7.2263 ⁻ 03	1.1920 ⁺ 01	1.15041	1.02138	0.69920	0.91294	1.70485	0.61604	
19	8.0950 ⁻ 03	1.2340 ⁺ 01	1.13839	1.02175	0.71191	0.91898	1.66633	0.62782	
20	8.9306 ⁻ 03	1.3032 ⁺ 01	1.12637	1.02206	0.73240	0.92817	1.60643	0.65096	
21	1.0290 ⁻ 02	1.4719 ⁺ 01	1.10712	1.02435	0.78009	0.94845	1.47823	0.71034	
22	1.1521 ⁻ 02	1.5992 ⁺ 01	1.08915	1.02395	0.81422	0.96061	1.39193	0.75165	
23	1.3150 ⁻ 02	1.9292 ⁺ 01	1.06558	1.01673	0.89662	0.98282	1.20150	0.87163	
24	1.4729 ⁻ 02	2.1405 ⁺ 01	1.04516	1.01008	0.94564	0.99245	1.10144	0.94173	
25	1.6807 ⁻ 02	2.3175 ⁺ 01	1.02112	1.00374	0.98482	0.99853	1.02884	0.99181	
D 26	1.8976 ⁻ 02	2.5881 ⁺ 01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
27	2.0937 ⁻ 02	2.4177 ⁺ 01	0.98016	0.99853	1.00631	1.00061	0.98871	0.99196	
28	2.3020 ⁻ 02	2.4254 ⁺ 01	0.95916	0.99841	1.00793	1.00090	0.98609	0.97356	

INPUT VARIABLES Y,U,T,P

65030305		STROUD	PROFILE TABULATION			24 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.34775	0.89139	0.00000	0.00000	3.74811	0.00000	
2	2.5400*-04	3.3561*+00	1.34634	0.94360	0.37092	0.61550	2.75351	0.30095	
3	4.3688*-04	3.9417*+00	1.34502	0.96405	0.40804	0.66339	2.64324	0.33757	
4	6.4262*-04	4.6262*+00	1.34370	0.98190	0.44730	0.70945	2.51564	0.37894	
5	3.6614*-04	6.0548*+00	1.34163	0.99645	0.51945	0.77864	2.24689	0.46493	
6	1.2725*-03	7.1399*+00	1.33898	1.01573	0.56802	0.82309	2.09973	0.52488	
7	1.7043*-03	7.9784*+00	1.33599	1.02879	0.60285	0.85220	1.99835	0.56957	
8	2.1209*-03	8.2190*+00	1.33154	1.03504	0.61247	0.86101	1.97629	0.58012	
9	2.5400*-03	8.6786*+00	1.32749	1.03645	0.63036	0.87276	1.91694	0.60439	
10	2.9870*-03	8.7705*+00	1.32212	1.03626	0.63397	0.87487	1.90435	0.60738	
11	3.4392*-03	8.8662*+00	1.31674	1.03450	0.63762	0.87631	1.88881	0.61090	
12	4.2901*-03	8.9991*+00	1.30591	1.03087	0.64267	0.87776	1.86542	0.61449	
13	5.1105*-03	9.3175*+00	1.29243	1.02531	0.65459	0.88227	1.81661	0.62769	
14	6.0173*-03	9.6596*+00	1.27631	1.02390	0.66716	0.88868	1.77432	0.63925	
15	6.8097*-03	1.0108*+01	1.26077	1.02421	0.68330	0.89749	1.72516	0.65589	
16	7.6581*-03	1.0765*+01	1.24465	1.02548	0.70625	0.90977	1.65938	0.68239	
17	8.5776*-03	1.1585*+01	1.22439	1.02634	0.73388	0.92337	1.58310	0.71415	
18	1.0226*-02	1.3575*+01	1.18867	1.02931	0.79694	0.95162	1.42586	0.79332	
19	1.1928*-02	1.6196*+01	1.14626	1.02700	0.87308	0.97779	1.25427	0.89359	
20	1.3635*-02	1.8523*+01	1.10376	1.01436	0.93548	0.99049	1.12107	0.97519	
21	1.5339*-02	2.0109*+01	1.05862	1.00505	0.97571	0.99657	1.04321	1.01129	
D 22	1.7460*-02	2.1099*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
23	1.9187*-02	2.1477*+01	0.95692	0.99802	1.00913	1.00116	0.98426	0.97336	
24	2.0884*-02	2.1816*+01	0.91377	0.99735	1.01723	1.00269	0.97161	0.94299	

INPUT VARIABLES Y,U,T,P

65030306		STROUD	PROFILE TABULATION			26 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.65979	0.89379	0.00000	0.00000	3.59146	0.00000	
2	2.5400*-04	3.4813*+00	1.65650	0.96247	0.39073	0.63576	2.64747	0.39779	
3	4.2672*-04	4.2370*+00	1.65478	0.98821	0.43840	0.69498	2.51307	0.45762	
4	6.3754*-04	5.0391*+00	1.65149	1.01026	0.48362	0.74603	2.37962	0.51775	
5	8.3566*-04	5.9416*+00	1.64820	1.02274	0.52976	0.79021	2.22494	0.58337	
6	1.3056*-03	6.7605*+00	1.64318	1.02857	0.56833	0.82217	2.09281	0.64553	
7	1.6916*-03	7.1721*+00	1.63653	1.03022	0.58674	0.83601	2.03018	0.67390	
8	2.1361*-03	7.3606*+00	1.62829	1.02872	0.59498	0.84109	1.99842	0.68531	
9	2.5578*-03	7.6208*+00	1.61999	1.02713	0.60616	0.84797	1.95697	0.70195	
10	2.9820*-03	7.9895*+00	1.61165	1.02412	0.60483	0.84584	1.95577	0.69703	
11	3.3960*-03	7.7203*+00	1.60173	1.02252	0.61038	0.84884	1.93397	0.70302	
12	3.8202*-03	7.7205*+00	1.59092	1.01900	0.61039	0.84738	1.92729	0.69949	
13	4.6914*-03	7.8872*+00	1.56522	1.01632	0.61740	0.85040	1.89900	0.70126	
14	5.5321*-03	8.2761*+00	1.53529	1.01527	0.63345	0.86043	1.84506	0.71597	
15	6.3856*-03	8.1334*+00	1.50294	1.01228	0.63219	0.87393	1.80890	0.72123	
16	6.7920*-03	9.2085*+00	1.48718	1.01838	0.67034	0.88339	1.73669	0.75648	
17	7.6637*-03	9.7353*+00	1.44903	1.01921	0.69030	0.89464	1.67967	0.77180	
18	8.5268*-03	1.0604*+01	1.41001	1.02075	0.72201	0.91152	1.59385	0.80638	
19	1.0241*-02	1.2892*+01	1.32116	1.01827	0.79950	0.94491	1.39682	0.89372	
20	1.1935*-02	1.3508*+01	1.23654	1.01249	0.87974	0.97154	1.21958	0.98504	
21	1.3625*-02	1.7612*+01	1.15435	1.00456	0.93929	0.98604	1.10201	1.03287	
22	1.5324*-02	1.9027*+01	1.07553	1.00017	0.97732	0.99429	1.03503	1.03319	
D 23	1.7041*-02	1.9848*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
24	1.8793*-02	2.0610*+01	0.92948	0.99956	1.01816	1.00421	0.97278	0.95951	
25	2.0419*-02	2.1116*+01	0.87056	0.99875	1.03088	1.00679	0.94382	0.91892	
26	2.2154*-02	2.1439*+01	0.81665	0.99930	1.03891	1.00892	0.94310	0.87364	

INPUT VARIABLES Y,U,T,P

65030307		STROUD	PROFILE TABULATION			19 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	3.37830	0.89944	0.00000	0.00000	3.22454	0.00000	
2	2.5400*-04	3.1717*+00	3.36985	0.97873	0.39901	0.62909	2.48576	0.85284	
3	4.1910*-04	3.8202*+00	3.36310	1.00540	0.44608	0.66820	2.38009	0.97243	
4	6.3246*-04	4.3985*+00	3.35445	1.02912	0.48396	0.73365	2.29867	1.07096	
5	8.5852*-04	4.9750*+00	3.34625	1.04494	0.49481	0.74935	2.29380	1.09347	
6	1.2751*-03	4.6997*+00	3.32425	1.04293	0.50250	0.75580	2.26229	1.11059	
7	1.6891*-03	4.7044*+00	3.29725	1.03578	0.50278	0.75347	2.24577	1.10624	
8	2.1260*-03	4.1215*+00	3.26345	0.87276	0.58184	0.75159	1.66861	1.46996	
9	2.5603*-03	4.7006*+00	3.21955	1.02307	0.50255	0.74862	2.21903	1.08616	
10	2.9870*-03	4.8249*+00	3.16550	1.01887	0.51000	0.75372	2.18415	1.09237	
11	3.4011*-03	4.9136*+00	3.10130	1.01621	0.51524	0.75733	2.16050	1.08712	
12	3.1460*-03	5.9866*+00	2.69590	1.01148	0.57480	0.80385	1.95379	1.10805	
13	6.8174*-03	8.1082*+00	2.16210	1.00670	0.67703	0.87014	1.65152	1.13895	
14	8.5166*-03	1.1118*+01	1.84525	1.00190	0.79972	0.93048	1.35374	1.13084	
15	1.0229*-02	1.4489*+01	1.24320	0.99982	0.91778	0.97479	1.12808	1.07426	
D 16	1.1935*-02	1.7111*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
17	1.3632*-02	1.8301*+01	0.85135	1.00150	1.03516	1.01020	0.95236	0.90306	
18	1.5337*-02	1.9549*+01	0.72970	1.00444	1.07078	1.02058	0.90843	0.81978	
19	1.7051*-02	2.0712*+01	0.62835	1.00595	1.10294	1.02883	0.87012	0.74296	

INPUT VARIABLES Y,U,T,P

65030801		STROUD		PROFILE TABULATION			18 POINTS, DELTA AT POINT 16		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/U	
1	0.0000+00	1.0000+00	1.00000	0.41861	0.00000	0.00000	5.57182	0.00000	
2	2.5400+04	1.8119+00	1.00000	0.57766	0.12262	0.31233	6.48790	0.04814	
3	7.0104+04	2.3323+00	1.00000	0.76751	0.14961	0.42339	8.00898	0.05287	
4	1.1100+03	4.7575+00	1.00000	0.89540	0.23106	0.62093	7.17174	0.08658	
5	1.5596+03	9.7490+00	1.00000	0.89445	0.34206	0.75552	4.87851	0.15487	
6	1.9761+03	1.2948+01	1.00000	0.90642	0.39677	0.80403	4.10646	0.19580	
7	3.3731+03	1.7762+01	1.00000	0.93877	0.46713	0.86004	3.38973	0.25372	
8	4.9962+03	2.1866+01	1.00000	0.96669	0.51963	0.89638	2.97570	0.30123	
9	6.5557+03	2.6453+01	1.00000	0.99092	0.57264	0.92666	2.61866	0.35387	
10	8.6843+03	3.2968+01	1.00000	1.01876	0.64042	0.95886	2.24171	0.42774	
11	1.0818+02	4.0531+01	1.00000	1.03366	0.71104	0.98128	1.90457	0.51522	
12	1.2949+02	5.0573+01	1.00000	1.03156	0.79518	0.99417	1.56313	0.63601	
13	1.5083+02	6.3039+01	1.00000	1.01698	0.88860	0.99851	1.26249	0.79078	
14	1.7211+02	7.2242+01	1.00000	1.00162	0.99170	0.99692	1.09729	0.90853	
15	1.9385+02	7.7629+01	1.00000	0.99863	0.98677	0.99831	1.02352	0.97537	
D 16	2.1481+02	7.9712+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
17	2.3480+02	7.9717+01	1.00000	1.00015	1.00003	1.00008	1.00010	0.99998	
18	2.5781+02	7.9335+01	1.00000	0.99949	0.99762	0.99956	1.00390	0.99568	

INPUT VARIABLES Y,U,T,P

65030802		STROUD		PROFILE TABULATION			19 POINTS, DELTA AT POINT 18		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.00000	0.41498	0.00000	0.00000	5.34840	0.00000	
2	2.5400+04	2.1076+00	1.00000	0.52983	0.14140	0.33212	5.51723	0.06020	
3	8.9716+04	2.3598+00	1.00000	0.74499	0.15350	0.42039	7.50061	0.05605	
4	1.5723+03	6.3997+00	1.00000	0.83395	0.27788	0.65860	5.61742	0.11724	
5	2.1869+03	9.1755+00	1.00000	0.86329	0.33712	0.73337	4.73237	0.15497	
6	3.4519+03	1.2240+01	1.00000	0.89600	0.39212	0.78795	4.03801	0.19513	
7	5.1283+03	1.5883+01	1.00000	0.90619	0.44877	0.83246	3.44084	0.24193	
8	6.4567+03	1.9142+01	1.00000	0.91961	0.49396	0.86104	3.03847	0.28338	
9	7.7216+03	2.2452+01	1.00000	0.93241	0.53597	0.88425	2.72182	0.32487	
10	9.0143+03	2.6577+01	1.00000	0.94409	0.56411	0.90613	2.40657	0.37652	
11	1.0279+02	3.1503+01	1.00000	0.95687	0.63685	0.92691	2.11841	0.43755	
12	1.1600+02	3.7155+01	1.00000	0.96835	0.69239	0.94504	1.86292	0.50729	
13	1.2850+02	4.2591+01	1.00000	0.98171	0.74192	0.96084	1.67719	0.57289	
14	1.4105+02	4.9977+01	1.00000	0.99248	0.80434	0.97579	1.47175	0.64301	
15	1.5469+02	5.5599+01	1.00000	1.00655	0.84877	0.98850	1.35634	0.72880	
16	1.7331+02	6.6803+01	1.00000	1.01627	0.93105	1.00215	1.15856	0.86500	
17	1.9680+02	7.4492+01	1.00000	1.01311	0.98351	1.00521	1.04464	0.96226	
D 18	2.1773+02	7.6996+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
19	2.3929+02	7.7067+01	1.00000	0.99217	1.00047	0.99611	0.99132	1.00484	

INPUT VARIABLES Y,U,T,P

65030803		STROUD		PROFILE TABULATION			17 POINTS, DELTA AT POINT 16		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.16438	0.42497	0.00000	0.00000	4.66447	0.00000	
2	2.5400+04	1.7142+00	1.14438	0.63797	0.12918	0.31650	6.00306	0.06139	
3	6.7310+04	6.0950+00	1.16226	0.82863	0.29548	0.65147	4.86105	0.15577	
4	1.0922+03	9.0958+00	1.15856	0.85666	0.36632	0.74727	4.16133	0.20805	
5	1.5367+03	1.1139+01	1.15751	0.90155	0.40750	0.78647	3.72492	0.24439	
6	1.9882+03	1.2099+01	1.15381	0.91329	0.42547	0.80419	3.57261	0.25972	
7	2.3749+03	1.3169+01	1.15328	0.92112	0.44463	0.82005	3.40155	0.27803	
8	4.4983+03	1.8247+01	1.13848	0.95056	0.52614	0.87625	2.77363	0.35967	
9	6.6751+03	2.4027+01	1.12315	0.97071	0.60568	0.91587	2.28651	0.44988	
10	8.7732+03	3.1527+01	1.11099	0.99286	0.69545	0.95124	1.87087	0.56488	
11	1.0892+02	3.9912+01	1.09355	1.01621	0.78373	0.98041	1.56488	0.68512	
12	1.3053+02	5.0932+01	1.07611	1.03089	0.88647	1.00295	1.28007	0.84315	
13	1.5174+02	5.7721+01	1.05708	1.02159	0.94421	1.00518	1.13331	0.91757	
14	1.7323+02	6.1791+01	1.03647	1.01141	0.97720	1.00378	1.09514	0.98602	
15	1.9439+02	6.4396+01	1.02167	1.00135	0.99774	1.00047	1.00547	1.01658	
D 16	2.0569+02	6.4686+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
17	2.2636+02	6.5370+01	0.96882	0.99980	1.00686	1.00052	0.98744	0.98163	

INPUT VARIABLES Y,U,T,P

65030804		STROUD	PROFILE TABULATION			15 POINTS, DELTA AT POINT 12			
I	Y	PT2/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.35859	0.42282	0.00000	0.00000	3.86378	0.00000	
2	2.5400*-04	3.5585*+00	1.35720	0.71436	0.24109	0.50753	4.43163	0.15543	
3	6.3246*-04	1.0022*+01	1.35554	0.83640	0.42685	0.74893	3.07847	0.32977	
4	1.0160*-03	1.3454*+01	1.35054	0.87215	0.49778	0.80712	2.64204	0.41360	
5	1.4097*-03	1.5672*+01	1.34499	0.88866	0.53866	0.83725	2.41590	0.46612	
6	1.8542*-03	1.7408*+01	1.33805	0.70198	0.56361	0.85668	2.26988	0.50499	
7	2.2682*-03	1.9082*+01	1.33139	0.91057	0.59606	0.87161	2.13833	0.54269	
8	4.3790*-03	2.4612*+01	1.20782	0.93611	0.67888	0.91098	1.80063	0.65153	
9	6.3126*-03	3.0384*+01	1.22537	0.96129	0.75569	0.94248	1.55548	0.74246	
10	8.6665*-03	3.7371*+01	1.15348	0.98841	0.83931	0.97212	1.34151	0.83587	
11	1.0785*-02	4.6044*+01	1.05662	1.00474	0.93274	0.99427	1.13629	0.92456	
D 12	1.2936*-02	5.2854*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
13	1.5143*-02	4.2089*+01	0.93478	0.99304	0.89135	0.98270	1.21548	0.75576	
14	1.7181*-02	4.2840*+01	0.88454	0.98864	0.89936	0.98169	1.19148	0.72880	
15	1.9225*-02	4.1766*+01	0.85734	0.98675	0.88789	0.97907	1.21594	0.69033	

INPUT VARIABLES Y,U,T,P

65030805		STROUD	PROFILE TABULATION			20 POINTS, DELTA AT POINT 19			
I	Y	PT2/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.75742	0.43644	0.00000	0.00000	3.55423	0.00000	
2	2.5400*-04	5.1626*+00	1.75575	0.83765	0.31863	0.63358	3.95394	0.28134	
3	4.7752*-04	7.8870*+00	1.74870	0.89138	0.40130	0.73731	3.37565	0.38195	
4	6.7310*-04	1.1803*+01	1.74703	0.91828	0.49635	0.81703	2.70957	0.52679	
5	9.1948*-04	1.8199*+01	1.73998	0.94794	0.54635	0.85770	2.46449	0.60535	
6	1.1430*-03	1.5207*+01	1.73460	0.95883	0.56607	0.87219	2.37404	0.63727	
7	1.3005*-03	1.8435*+01	1.72940	0.96187	0.58920	0.88398	2.25091	0.67917	
8	1.7450*-03	1.8439*+01	1.71529	0.97130	0.62510	0.90290	2.08629	0.74234	
9	2.1692*-03	1.9680*+01	1.69952	0.97595	0.64634	0.91287	1.99477	0.77775	
10	2.5908*-03	2.0803*+01	1.67836	0.97997	0.66496	0.92115	1.91900	0.80564	
11	2.9972*-03	2.1495*+01	1.65906	0.98508	0.67620	0.92723	1.86031	0.81813	
12	4.2418*-03	2.3888*+01	1.58352	1.00134	0.71363	0.94623	1.75810	0.85225	
13	5.3137*-03	2.4907*+01	1.52209	1.01548	0.74376	0.96117	1.67005	0.87601	
14	6.4897*-03	2.9136*+01	1.43764	1.02767	0.78957	0.97811	1.53462	0.91630	
15	7.4825*-03	3.2285*+01	1.36024	1.03073	0.83180	0.98658	1.41249	0.95202	
16	8.9154*-03	3.7200*+01	1.23719	1.02698	0.89375	0.99808	1.24710	0.99015	
17	9.5834*-03	3.9950*+01	1.17743	1.02130	0.92660	1.00053	1.16592	1.01040	
18	1.0660*-02	4.3622*+01	1.08092	1.01082	0.96873	1.00137	1.06852	1.01299	
D 19	1.1694*-02	4.6453*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
20	1.3884*-02	4.7854*+01	0.91221	0.98279	1.01511	0.99316	0.95721	0.94647	

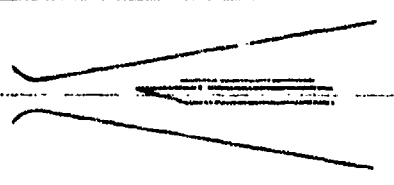
INPUT VARIABLES Y,U,T,P

65030806		STROUD		PROFILE TABULATION			17 POINTS, DELTA AT POINT 16		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	2.08343	0.44088	0.00000	0.00000	3.26108	0.00000	
2	2.5400*-04	5.5759*+00	2.06144	0.72985	0.35139	0.61028	3.01636	0.42112	
3	5.2324*-04	8.5182*+00	2.07187	0.95863	0.44181	0.78457	3.15350	0.51596	
4	7.1628*-04	1.0967*+01	2.06443	0.97230	0.50474	0.83473	2.73497	0.63008	
5	9.4742*-04	1.2620*+01	2.05620	0.97852	0.54310	0.85997	2.50731	0.70525	
6	1.3157*-03	1.4396*+01	2.04172	0.98290	0.58147	0.88160	2.29872	0.78304	
7	1.6358*-03	1.5152*+01	2.02298	1.02058	0.59706	0.90575	2.30132	0.79621	
8	2.1006*-03	1.6170*+01	1.99389	1.02139	0.61742	0.91520	2.19722	0.83051	
9	2.5806*-03	1.6891*+01	1.95842	1.02107	0.63145	0.92096	2.12718	0.84790	
10	2.9464*-03	1.7404*+01	1.92706	1.01942	0.64125	0.92417	2.07708	0.85743	
11	3.9929*-03	1.9868*+01	1.82304	1.01707	0.68278	0.93888	1.88923	0.90560	
12	5.0724*-03	2.3072*+01	1.69576	1.02344	0.74085	0.95974	1.67820	0.96978	
13	6.1747*-03	2.7050*+01	1.54178	1.02866	0.80372	0.97856	1.48348	1.01701	
14	7.2187*-03	3.1333*+01	1.36469	1.02410	0.86573	0.98986	1.30733	1.03329	
15	8.2906*-03	3.6243*+01	1.17710	1.01178	0.93205	0.99575	1.14137	1.02692	
D 16	9.3243*-03	4.1849*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
17	1.1891*-02	4.3100*+01	0.85426	0.98525	1.02932	0.99689	0.93798	0.90791	

INPUT VARIABLES Y,U,T,P

65030807		STROUD		PROFILE TABULATION			14 POINTS, DELTA AT POINT 13		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	3.76391	0.44775	0.00000	0.00000	2.59424	0.00000	
2	2.5400*-04	4.8673*+00	3.69981	0.82580	0.37635	0.63531	2.84970	0.82484	
3	4.8260*-04	5.3046*+00	3.61863	0.96106	0.39487	0.70487	3.18652	0.80046	
4	7.0358*-04	6.5598*+00	3.56702	0.98069	0.44365	0.75856	2.92355	0.92552	
5	9.8298*-04	8.4088*+00	3.49980	1.00571	0.50942	0.82088	2.59668	1.10638	
6	1.5132*-03	9.7791*+00	3.37031	1.00790	0.54962	0.84849	2.38842	1.19731	
7	1.5265*-03	1.0143*+01	3.27771	1.01014	0.55968	0.85606	2.33951	1.19935	
8	1.9583*-03	1.1493*+01	2.92806	1.01160	0.59754	0.87849	2.16145	1.18926	
9	2.3673*-03	1.3014*+01	2.62935	1.01059	0.63749	0.89853	1.98663	1.18922	
10	2.6873*-03	1.7968*+01	1.94416	1.01091	0.75300	0.94509	1.57528	1.16640	
11	3.3426*-03	2.4623*+01	1.42598	1.00947	0.88472	0.98149	1.23073	1.13720	
12	3.6805*-03	2.7615*+01	1.24094	1.00729	0.93791	0.99200	1.11865	1.10043	
D 13	4.3891*-03	3.1327*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
14	5.3873*-03	3.4374*+01	0.75929	0.99040	1.04820	1.00299	0.91560	0.83176	

INPUT VARIABLES Y,U,T,P

	M : 1.0 Rising to 3.0 R THETA X 10 ⁻³ : 3 - 10 TW/TR : 0.80 - 1.0	6504
		FPG - MHT
Special purpose extension of continuous running tunnel (see text). W = 0.4 m, H = 0.14 to 0.42 m. PO : 0.13 MV/m ² . TO : 340 K. Air. $B < PE/m \times 10^{-6} < 17$.		
PASIUK L., HASTINGS S.M. and CHATHAM R., 1965. Experimental Reynolds' analogy factor for a compressible turbulent boundary layer with a pressure gradient. NOLTR 64-200.		

- 1 The test boundary layer was formed on a fiat plate model (W = 0.305 m, L = 1.51 m) placed with its upper surface on the centre line of the tunnel. The leading edge (X = 0) was chamfered on the under side at 5°, and placed at the tunnel throat. The space between the edge of the plate and the tunnel sidewalls was filled with fibre glass spacers insulating it thermally and electrically from the tunnel walls (the size stated in text is not big enough unless there are two on each side). The nozzle blocks were constructed of wood. On the upper (test) side the contour was chosen to give a predicted constant value of the "Pohlhausen parameter" $(\theta^2/\nu_e)(T_o/T_e)(du_e/dx)$ for $x > 0.4$ m. The block ended at X = 0.935 m when the height above the plate was 0.197 m. The plate extended about 0.61 m beyond the exit-plane of the nozzle. The plate was actively cooled.
- 6 There were three static tapings and three thermocouple plugs, located at X = 0.207, 0.592 and 0.898 m. The thermocouple plugs contained four junctions, the uppermost at the plate surface and the others buried at
- 8 intervals of 3.18 mm. These were mounted on the centre line, with the static tapings 12.7 mm to one side.
- 7 Pitot profiles were measured with a CPP ($d_1 = 0.559$ mm) and temperature profiles with an ECP ($\alpha = 5^\circ$, $d = 1.2$ mm) as constructed by Danberg (1961). The Pitot probe was also used for a longitudinal traverse
- 9 in the free stream just outside the boundary layer. Values of static pressure and Mach number deduced from this were used in reducing the profile data. The static pressure values agreed with those measured at the orifices, and accordingly the pressure was assumed constant through the boundary layer. The wall heat flux was deduced from the temperature profiles in the thermocouple plugs. The recovery factor used
- 10 by the authors was 0.88. No profile corrections are reported.
- 12 The editors have presented all the profiles measured, and have interpolated the author's TO profiles to the Y-values of Pitot measurements. The D-state has been selected by the editors. The wall temperatures
- 13 are our interpolations from the three measured values. The profiles consist of three series of nine profiles, each at a different wall heat flux condition. Series 01 is for a near-adiabatic wall, while
- 14 series 02 and 03 describe flows with increasing heat transfer rates. Where available the experimental heat flux is also given.
- § DATA: 6504 0101-0309. Pitot and TO profiles obtained separately. NX = 9. Some heat flux measurements determined from the temperature gradient in the wall.
- 15 Editors' comments
The description of the experiment and presentation of the data in the original source is far from complete. The data itself is rough and generally of doubtful quality, but is presented here as the only other case of a relatively strongly accelerated flow with heat transfer results is the channel wall study of Voisinot & Lee - CAT 7304 at higher Mach numbers. Adiabatic studies, also on channel walls, were made by Michel et al. - CAT 6902 and Thomas - CAT 7401.
In no case do the measurements extend in as far as the momentum-deficit peak, so that integral values should be treated with reserve. We have transformed the profiles using CF values as correlated by Fernholz (1971), and the wall-law plots indicate that CF is substantially higher than for a zero-pressure-gradient flow.
This is a straight-wall, reflected wave, flow, and normal pressure gradient effects are expected to be negligible, as reported by the authors.

CAT 6504

PASIUK

BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUN X * RZ	MD * POD* YOD*	TN/TR PW/PO* SN *	RED2W REO2D R02	CF CQ * PI2	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR
65040101	1.4010	0.9601	3.0242*+03	NM	2.5947	1.5591	4.1468*+04	4.1468*+04
2.6822*-01	1.3215*+05	1.0000	3.7117*+03	NM	1.8271	1.8239	3.1429*+02	2.4216*+02
INFINITE	3.3722*+02	1.0000	2.2265*-04	NM	-0.1609	2.4870*-04	4.3712*+02	3.2734*+02
65040102	1.6895	0.9665	2.7166*+03	NM	2.7370	1.5101	2.7200*+04	2.7200*+04
2.8651*-01	1.3215*+05	1.0000	3.6746*+03	NM	1.8437	1.8398	3.1362*+02	2.1467*+02
INFINITE	3.3722*+02	0.0000	2.3767*-04	NM	-0.0299	2.6961*-04	4.9631*+02	3.2448*+02
65040103	1.9740	0.9660	3.7204*+03	NM	3.0091	1.3929	1.7506*+04	1.7506*+04
3.9014*-01	1.3215*+05	1.0000	5.9530*+03	NM	1.8366	1.8292	3.1092*+02	1.8952*+02
INFINITE	3.3722*+02	0.0000	4.0219*-04	NM	0.0119	4.8282*-04	5.4486*+02	3.2186*+02
65040104	2.2510	0.9666	3.9481*+03	NM	3.2689	1.3536	1.1411*+04	1.1411*+04
4.9073*-01	1.3215*+05	1.0000	6.9257*+03	NM	1.8378	1.8264	3.0890*+02	1.6749*+02
INFINITE	3.3722*+02	0.0000	5.3958*-04	NM	0.1429	6.7181*-04	5.0409*+02	3.1957*+02
65040105	2.4925	0.9678	3.7663*+03	NM	3.7875	1.3332	7.8252*+03	7.8252*+03
5.9131*-01	1.3215*+05	1.0000	6.8264*+03	NM	1.8385	1.8248	3.0755*+02	1.5038*+02
INFINITE	3.3722*+02	0.0000	6.4013*-04	NM	0.0760	5.3757*-04	6.1282*+02	3.1779*+02
65040106	2.6790	0.9673	3.7674*+03	NM	4.2224	1.3224	5.8622*+03	5.8622*+03
6.9494*-01	1.3215*+05	1.0000	7.3324*+03	NM	1.8367	1.8204	3.0620*+02	1.3847*+02
INFINITE	3.3722*+02	0.0000	7.6053*-04	NM	0.0282	1.0382*-03	6.3205*+02	3.1655*+02
65040107	2.8260	0.9658	3.7715*+03	NM	4.5363	1.3196	4.6802*+03	4.6802*+03
7.9553*-01	1.3215*+05	1.0000	7.7597*+03	NM	1.8333	1.8152	3.0485*+02	1.2984*+02
INFINITE	3.3722*+02	0.0000	8.7245*-04	NM	0.0316	1.2323*-03	6.4563*+02	3.1565*+02
65040108	2.9560	0.9659	3.9697*+03	NM	4.7913	1.3065	3.8436*+03	3.8436*+03
8.9611*-01	1.3215*+05	1.0000	8.5898*+03	NM	1.8340	1.8151	3.0417*+02	1.2273*+02
INFINITE	3.3722*+02	0.0000	1.0376*-03	NM	0.0587	1.5058*-03	6.5659*+02	3.1492*+02
65040109	2.9730	0.9662	4.0557*+03	NM	4.8614	1.3065	3.7465*+03	3.7465*+03
9.2354*-01	1.3215*+05	1.0000	8.8357*+03	NM	1.8303	1.8123	3.0417*+02	1.2184*+02
INFINITE	3.3722*+02	0.0000	1.0774*-03	NM	0.0461	1.5838*-03	6.5796*+02	3.1482*+02
65040201	1.6030	0.9164	2.4098*+03	NM	2.5882	1.6241	3.1480*+04	3.1480*+04
2.6822*-01	1.3440*+05	1.0000	3.0401*+03	NM	1.8526	1.8499	2.9909*+02	2.3368*+02
INFINITE	3.3833*+02	0.0000	1.8889*-04	NM	0.0835	2.0871*-04	4.8047*+02	3.2639*+02
65040202	1.7970	0.9195	3.2269*+03	NM	2.5972	1.4756	2.3498*+04	2.3498*+04
2.8651*-01	1.3440*+05	1.0000	4.3563*+03	NM	1.8485	1.8445	2.9841*+02	2.0957*+02
INFINITE	3.3833*+02	0.0000	2.8940*-04	1.5141*-04	0.1578	3.2701*-04	6.2066*+02	3.2453*+02
65040203	2.0680	0.9138	3.6506*+03	NM	2.8438	1.4045	1.5450*+04	1.5450*+04
3.9014*-01	1.3440*+05	1.0000	5.3795*+03	NM	1.8417	1.8348	2.9435*+02	1.8236*+02
INFINITE	3.3833*+02	0.0000	4.6325*-04	NM	0.2291	4.7603*-04	5.5992*+02	3.2211*+02
65040204	2.3260	0.9091	3.4117*+03	NM	3.1235	1.3442	1.0320*+04	1.0320*+04
4.9073*-01	1.3440*+05	1.0000	5.5302*+03	NM	1.8615	1.8542	2.9097*+02	1.6250*+02
INFINITE	3.3833*+02	0.0000	4.6929*-04	NM	0.2850	5.6481*-04	5.9449*+02	3.2005*+02
65040205	2.5560	0.9075	3.4786*+03	NM	1.5691	1.3282	7.2107*+03	7.2107*+03
5.9131*-01	1.3440*+05	1.0000	6.1445*+03	NM	1.8515	1.8406	2.8894*+02	1.4668*+02
INFINITE	3.3833*+02	0.0000	5.8888*-04	1.6846*-04	0.2342	7.4613*-04	6.2066*+02	3.1840*+02
65040206	2.7330	0.9043	3.7238*+03	NM	3.9588	1.3097	5.4872*+03	5.4872*+03
6.9494*-01	1.3440*+05	1.0000	7.0218*+03	NM	1.8506	1.8365	2.8691*+02	1.3967*+02
INFINITE	3.3833*+02	0.0000	7.4102*-04	NM	0.2097	9.7183*-04	6.3824*+02	3.1726*+02
65040207	2.9120	0.9609	3.7683*+03	NM	4.2385	1.3040	4.1774*+03	4.1774*+03
7.9553*-01	1.3440*+05	1.0000	7.5920*+03	NM	1.8438	1.8283	2.8488*+02	1.2550*+02
INFINITE	3.3833*+02	0.0000	8.8421*-04	NM	0.2695	1.2051*-03	6.5406*+02	3.1820*+02
65040208	3.0190	0.9005	3.4268*+03	NM	4.4488	1.3082	3.5561*+03	3.5561*+03
8.9611*-01	1.3440*+05	1.0000	8.2421*+03	NM	1.8354	1.8185	2.8420*+02	1.1985*+02
INFINITE	3.3833*+02	0.0000	1.0184*-03	1.2127*-04	0.2938	1.4315*-03	6.2267*+02	3.1561*+02
65040209	3.0410	0.9008	4.0101*+03	NM	4.5123	1.3135	3.4410*+03	3.4410*+03
9.2354*-01	1.3440*+05	1.0000	8.4913*+03	NM	1.8308	1.8133	2.8420*+02	1.1873*+02
INFINITE	3.3833*+02	0.0000	1.0620*-03	NM	0.2978	1.5126*-03	6.6437*+02	3.1949*+02

CAT 6504		PASIUK		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN	MD *	TW/TR	RED2W	CF	H12	H12K	PW	PD	
X *	PCD*	PW/PD*	RED2D	CO *	H32	H32K	1WA	TD	
RZ	T00*	3W *	D2	PI2	H42	D2K	UD	TR	
65040301	1.5780	0.8768	2.4818 ⁺ +03	NM	2.5070	1.6452	3.0844 ⁺ +04	3.0844 ⁺ +04	
2.6822 ⁻ -01	1.3071 ⁺ +05	1.0000	3.0205 ⁺ +03	NM	1.8274	1.8261	2.8717 ⁺ +02	2.2489 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	1.9352 ⁻ -04	NM	0.1555	2.1456 ⁻ -04	4.8026 ⁺ +02	3.2751 ⁺ +02	
65040302	1.7510	0.8767	3.8480 ⁺ +03	NM	2.5017	1.4761	2.4514 ⁺ +04	2.4514 ⁺ +04	
2.8651 ⁻ -01	1.3071 ⁺ +05	1.0000	4.9269 ⁺ +03	NM	1.8223	1.8191	2.8581 ⁺ +02	2.1042 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	3.3219 ⁻ -04	NM	0.1674	3.7651 ⁻ -04	5.0926 ⁺ +02	3.2603 ⁺ +02	
65040303	1.9830	0.8677	4.4524 ⁺ +03	NM	2.6770	1.4071	1.7153 ⁺ +04	1.7153 ⁺ +04	
3.9014 ⁻ -01	1.3071 ⁺ +05	1.0000	6.1329 ⁺ +03	NM	1.8244	1.8195	2.8106 ⁺ +02	1.9001 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	4.5492 ⁻ -04	NM	0.2230	5.3115 ⁻ -04	5.4805 ⁺ +02	3.2390 ⁺ +02	
65040304	2.2490	0.8610	4.8497 ⁺ +03	NM	3.0739	1.3603	1.1322 ⁺ +04	1.1322 ⁺ +04	
4.9073 ⁻ -01	1.3071 ⁺ +05	1.0000	6.7147 ⁺ +03	NM	1.8393	1.8295	2.7699 ⁺ +02	1.6874 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	5.6583 ⁻ -04	NM	0.1928	6.8365 ⁻ -04	5.8575 ⁺ +02	3.2169 ⁺ +02	
65040305	2.4400	0.8501	4.3937 ⁺ +03	NM	3.2648	1.3456	8.3997 ⁺ +03	8.3997 ⁺ +03	
5.9131 ⁻ -01	1.3071 ⁺ +05	1.0000	7.0525 ⁺ +03	NM	1.8299	1.8212	2.7223 ⁺ +02	1.5495 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	6.9616 ⁻ -04	NM	0.2863	6.2171 ⁻ -04	6.0896 ⁺ +02	3.2026 ⁺ +02	
65040306	2.6600	0.8434	4.5534 ⁺ +03	NM	3.5599	1.3095	5.9708 ⁺ +03	5.9708 ⁺ +03	
6.9494 ⁻ -01	1.3071 ⁺ +05	1.0000	7.9004 ⁺ +03	NM	1.8453	1.8326	2.8088 ⁺ +02	1.4055 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	8.2752 ⁻ -04	NM	0.3059	1.0486 ⁻ -03	6.3228 ⁺ +02	3.1876 ⁺ +02	
65040307	2.8290	0.8376	4.8880 ⁺ +03	NM	3.8516	1.2968	4.6082 ⁺ +03	4.6082 ⁺ +03	
7.9553 ⁻ -01	1.3071 ⁺ +05	1.0000	8.2654 ⁺ +03	NM	1.8417	1.8284	2.6612 ⁺ +02	1.3052 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	9.4990 ⁻ -04	NM	0.3278	1.2487 ⁻ -03	6.4802 ⁺ +02	3.1772 ⁺ +02	
65040308	2.9360	0.8285	4.8792 ⁺ +03	NM	4.0922	1.3269	3.9182 ⁺ +03	3.9182 ⁺ +03	
8.9611 ⁻ -01	1.3071 ⁺ +05	1.0000	9.2844 ⁺ +03	NM	1.8189	1.8045	2.6273 ⁺ +02	1.2461 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	1.1319 ⁻ -03	NM	0.3386	1.5600 ⁻ -03	6.5712 ⁺ +02	3.1710 ⁺ +02	
65040309	2.9360	0.8284	5.1839 ⁺ +03	NM	4.1219	1.3437	3.9182 ⁺ +03	3.9182 ⁺ +03	
9.2354 ⁻ -01	1.3071 ⁺ +05	1.0000	9.8439 ⁺ +03	NM	1.8133	1.7962	2.8205 ⁺ +02	1.2461 ⁺ +02	
INFINITE	3.3944 ⁺ +02	0.0000	1.7001 ⁻ -03	NM	0.3295	1.6620 ⁻ -03	6.5712 ⁺ +02	3.1710 ⁺ +02	

65040101		PASIUK		PROFILE TABULATION		11 POINTS, DELTA AT POINT 11			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHD/RHD0*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93200	0.00000	0.00000	1.29787	0.00000	
2	2.7940 ⁻ -04	1.7976 ⁺ +00	NM	0.98500	0.65166	0.73080	1.16007	0.62996	
3	4.3640 ⁻ -04	1.9563 ⁺ +00	NM	0.99500	0.73374	0.77879	1.14384	0.68085	
4	5.3340 ⁻ -04	2.0155 ⁺ +00	NM	1.00200	0.75161	0.79487	1.14208	0.69599	
5	7.8740 ⁻ -04	2.1798 ⁺ +00	NM	1.00700	0.79800	0.83586	1.12186	0.74507	
6	1.0414 ⁻ -03	2.2937 ⁺ +00	NM	1.00700	0.82798	0.86170	1.10495	0.77986	
7	1.2954 ⁻ -03	2.4338 ⁺ +00	NM	1.00700	0.86296	0.89119	1.08510	0.82130	
8	1.5494 ⁻ -03	2.6500 ⁺ +00	NM	1.00800	0.91363	0.93268	1.05726	0.88217	
9	2.9210 ⁻ -03	3.0213 ⁺ +00	NM	1.01500	0.99358	0.99514	1.01868	0.97689	
10	5.6398 ⁻ -03	3.0527 ⁺ +00	NM	1.00100	1.00000	1.00000	1.00100	0.99900	
D 11	7.0358 ⁻ -03	3.0527 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,T0/T0D ASSUMEP=PD

65040105		PASIUK		PROFILE TABULATION		13 POINTS, DELTA AT POINT 13			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHD/RHD0*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.91220	0.00000	0.00000	2.04562	0.00000	
2	2.7940 ⁻ -04	2.4478 ⁺ +00	NM	0.94012	0.48696	0.62599	1.62843	0.38435	
3	4.0640 ⁻ -04	2.3652 ⁺ +00	NM	0.94712	0.50261	0.64180	1.61654	0.39702	
4	5.3340 ⁻ -04	2.8005 ⁺ +00	NM	0.95211	0.53229	0.67113	1.57918	0.42498	
5	7.8740 ⁻ -04	3.1581 ⁺ +00	NM	0.96210	0.57401	0.71044	1.53082	0.46409	
6	1.0414 ⁻ -03	3.5810 ⁺ +00	NM	0.96709	0.61933	0.75068	1.46872	0.51111	
7	1.2954 ⁻ -03	3.9513 ⁺ +00	NM	0.97008	0.65624	0.78158	1.41713	0.55153	
8	1.5494 ⁻ -03	4.1024 ⁺ +00	NM	0.97308	0.67063	0.79323	1.39980	0.56688	
9	2.9210 ⁻ -03	5.1984 ⁺ +00	NM	0.98405	0.76695	0.86483	1.27495	0.67832	
10	5.6642 ⁻ -03	6.7989 ⁺ +00	NM	0.99902	0.88849	0.94141	1.13099	0.85238	
11	8.3312 ⁻ -03	7.8632 ⁺ +00	NM	1.00401	0.96069	0.98050	1.04880	0.93488	
12	1.1024 ⁻ -02	8.3887 ⁺ +00	NM	1.00100	0.99438	0.99729	1.00725	0.99011	
D 13	1.3691 ⁻ -02	8.4780 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,T0/T0D ASSUMEP=PD

65040109		PASIUK		PROFILE TABULATION		21 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.2000+00	1.0000+00	NM	0.90110	0.00000	0.00000	2.49401	0.00000	
2	2.7940-04	2.5752+00	NM	0.94605	0.42247	0.59550	1.99044	0.29918	
3	4.0640-04	2.7686+00	NM	0.95405	0.44299	0.61792	1.96047	0.31519	
4	5.3340-04	2.8980+00	NM	0.95904	0.45610	0.63188	1.94070	0.32569	
5	6.6040-04	3.0353+00	NM	0.96104	0.46956	0.64591	1.91393	0.33740	
6	7.8740-04	3.1591+00	NM	0.96104	0.48133	0.65793	1.88706	0.34865	
7	9.1440-04	3.3095+00	NM	0.96104	0.50420	0.68063	1.83518	0.37088	
8	1.0414-03	3.5628+00	NM	0.96104	0.51766	0.69350	1.80492	0.38427	
9	1.1884-03	3.6687+00	NM	0.96104	0.52674	0.70216	1.78461	0.39345	
10	1.2954-03	3.7767+00	NM	0.96104	0.53582	0.71061	1.76442	0.40274	
11	1.4224-03	3.8825+00	NM	0.96104	0.54457	0.71862	1.74508	0.41180	
12	1.5494-03	3.9527+00	NM	0.96104	0.55029	0.72379	1.73250	0.41777	
13	2.9210-03	4.4365+00	NM	0.96903	0.61756	0.78089	1.60200	0.48745	
14	5.6388-03	6.5262+00	NM	0.98701	0.72856	0.86116	1.40937	0.61103	
15	8.3312-03	7.5019+00	NM	0.99700	0.78540	0.89631	1.32003	0.67901	
16	1.0498-02	7.5254+00	NM	1.00310	0.89169	0.95282	1.15401	0.82566	
17	1.3691-02	1.0584+01	NM	1.00500	0.94248	0.97612	1.08222	0.90196	
18	1.6358-02	1.1250+01	NM	1.00500	0.97309	0.98914	1.04027	0.95085	
19	1.9025-02	1.1709+01	NM	1.00300	0.99361	0.99747	1.01123	0.98640	
D 20	2.1692-02	1.1854+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
21	2.4384-02	1.1854+01	NM	0.99900	1.00000	1.00000	0.99900	1.00100	

INPUT VARIABLES Y,M,T0/T0D ASSUMEP=PD

65040301		PASIUK		PROFILE TABULATION		10 POINTS, DELTA AT POINT 9			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	NM	0.84431	0.00000	0.00000	1.27552	0.00000	
2	2.7940-04	2.1614+00	NM	0.93513	0.69524	0.74767	1.13302	0.65989	
3	5.3340-04	2.4221+00	NM	0.96806	0.73407	0.80098	1.13335	0.70674	
4	8.1280-04	2.6531+00	NM	0.97904	0.80163	0.84248	1.11359	0.75655	
5	1.3208-03	3.0353+00	NM	0.98703	0.87359	0.90253	1.07293	0.84116	
6	1.8288-03	3.4057+00	NM	0.99800	0.93742	0.95302	1.04066	0.91579	
7	2.3114-03	3.9113+00	NM	1.00200	1.01752	1.01271	0.99016	1.02278	
8	2.9210-03	3.7807+00	NM	1.00200	0.99750	0.99817	1.00369	0.99450	
D 9	4.2672-03	3.7969+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
10	5.6642-03	3.7969+00	NM	0.99800	1.00000	1.00000	0.99800	1.00200	

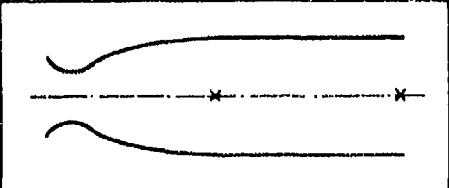
INPUT VARIABLES Y,M,T0/T0D ASSUME P=PD

65040305		PASIUK		PROFILE TABULATION		12 POINTS, DELTA AT POINT 12			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	NM	0.80236	0.00000	0.00000	1.75774	0.00000	
2	2.7940-04	2.7247+00	NM	0.87421	0.33421	0.65488	1.42942	0.45814	
3	5.3340-04	3.1142+00	NM	0.90019	0.58132	0.70029	1.40622	0.49794	
4	7.8740-04	3.4413+00	NM	0.91317	0.61778	0.73368	1.37585	0.53341	
5	1.2954-03	3.8634+00	NM	0.92815	0.66161	0.77183	1.33664	0.57744	
6	1.8034-03	4.3428+00	NM	0.93813	0.70791	0.80979	1.28714	0.62714	
7	2.3114-03	4.6067+00	NM	0.94812	0.73208	0.82869	1.26793	0.65358	
8	2.8954-03	4.7167+00	NM	0.95712	0.74191	0.83620	1.26662	0.64918	
9	5.6388-03	6.7243+00	NM	0.98604	0.90250	0.94519	1.09660	0.86192	
10	8.3312-03	7.7988+00	NM	0.99901	0.97706	0.98780	1.02426	0.96440	
11	1.1024-02	8.1330+00	NM	1.00000	0.99918	0.99957	1.00009	0.99868	
D 12	1.3665-02	8.1455+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,T0/T0D ASSUME P=PD

65040309		PASIUK		PROFILE TABULATION		16 POINTS, DELTA AT POINT 15			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	NM	0.77223	0.00000	0.00000	2.10356	0.00000	
2	2.7940-04	2.2492+00	NM	0.81789	0.38959	0.53660	1.76588	0.30387	
3	5.3340-04	2.6711+00	NM	0.84282	0.43624	0.59201	1.72477	0.34324	
4	7.8740-04	2.9102+00	NM	0.85978	0.46308	0.61892	1.70989	0.36197	
5	1.2954-03	3.6112+00	NM	0.87767	0.52841	0.66526	1.61391	0.42460	
6	1.8034-03	3.8146+00	NM	0.88465	0.54576	0.70180	1.59219	0.44078	
7	2.3114-03	4.2163+00	NM	0.89358	0.57843	0.73174	1.54372	0.47401	
8	2.8954-03	4.7070+00	NM	0.90353	0.61586	0.76417	1.49146	0.51236	
9	5.6642-03	6.3215+00	NM	0.93936	0.72508	0.84795	1.34225	0.63174	
10	8.3312-03	7.7593+00	NM	0.96723	0.80980	0.90288	1.23665	0.73010	
11	1.1024-02	9.4324+00	NM	0.98812	0.89026	0.95212	1.12570	0.84500	
12	1.3691-02	1.0200+01	NM	0.99807	0.93603	0.97090	1.08295	0.89654	
13	1.6358-02	1.0830+01	NM	1.00303	0.96632	0.98509	1.04692	0.94094	
14	1.9025-02	1.1572+01	NM	1.00200	1.00000	1.00000	1.00200	0.99801	
D 15	2.1717-02	1.1572+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	2.4384-02	1.1572+01	NM	0.99900	1.00000	1.00000	0.99900	1.00100	

INPUT VARIABLES Y,M,T0/T0D ASSUME P=PD

	M : 1.6 and 2.2 R THETA X 10 ⁻³ : 9 - 120 TW / TR : 1.0	6505
		ZPG - AW
Two-dimensional continuous tunnel with adjustable nozzle. W = H = 1.2 m. 0.02 < P0 < 0.21 MN/m ² . T0 : 317 K. Air, dew point < 244 K. 0.24 < RE/m X 10 ⁻⁶ < 2.4.		
JACKSON M.W., CZARNECKI K.R. and MONTA W.J. 1965. Turbulent skin friction at high Reynolds numbers and low supersonic velocities. NASA TN D-2687. And Jackson, M.W. Private communication.		

- 1 The test boundary layer was formed on the sidewall of the wind tunnel, which was not actively cooled. Measurements were made at five stations "within the constant Mach number area of the tunnel test section". No indication of flow quality or transition position is given. (The tunnel was also used by Allen CAT 7303). The boundary layer had passed through the three dimensional expansion region of the throat (X = 0). No direct checks on cross flows are reported. A momentum balance using the experimental CF values indicated that the layer was not strictly two-dimensional.
- 6 Static pressure was measured at points on the centre line, and wall temperature was measured on both inner and outer surfaces near the skin friction balances. These were on loan from the DRL and were those used by Shutts et al., CAT 5501. During the tests, the balances at various stations were interchanged.
- 9 Discrepancies between individual balance readings were noted, and the data presented are interpolated from a curve faired through all the experimental values.
- 7 Pitot profiles were measured using an FPP made by flattening tube of 1.27 mm diameter to give a face for which, after honing, h₁ = 0.23, h₂ = 0.076 mm. The slender portion of the probe mount was about 40 mm [E]
- 8 long. The profile normal, nominally, passed through the centre of the balance element at each of the five
- 9 stations at X = 3.36, 3.94, 4.36, 4.79 and 5.24 m. Static pressure was assumed constant through the layer. The tunnel total temperature was adjusted so that the inner and outer wall temperatures were the same and
- 10 equal to room temperature in the test zone, the flow thus being presumed adiabatic. No corrections were
- 11 applied to the probe data, and Sutherland's viscosity law was used.
- 12 Data are presented here for the X = 3.94 and 5.24 m stations only (corresponding to figure 9 of the source paper), as other tabular data could not be found. The author's assumption of isoenergetic flow has been replaced by the Crocco / Van Driest temperature/velocity correlation. The editors have taken CF values
- 13 from the graphical presentation in the source. The profiles consist of seven sets for each of two Mach
- 14 numbers. Each set represents a different unit Reynolds number for two successive stations. The CF values represent the average of values obtained at the same stations using a number of different balances in separate tests.
- 5 DA:A 6505 0101 - 1402. Pitot profiles. NX = 2. CF values obtained separately with a number of FEB.
- 15 Editors' comments
The experiment provides data at modest Mach number for moderate to high Reynolds numbers. Comparable studies are those of Hopkins & Keener - CAT 6601, Winter & Gaudet - CAT 7302, and Allen - CAT 7303, which were obtained in a similar geometric situation. The range overlaps that of the study by Shutts et al. - CAT 5501, using the same balances.
The range of Y values in wall coordinates is very large (10 < y⁺ < 3 x 10⁴), but in about half the profiles it seems that the results at small Y need correction for probe effects. Series 01-07 show velocity profiles with unusually small wake strength. Three dimensional effects may well be considerable as the length/width ratio is up to 4.5.

CAT 6505		JACKSON		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN	MD *	TW/TR*	RED2W	CF *	H12	H12K	PW	PD		
X *	POD	PW/PD*	RED2D	CO	H32	H32K	TW	TD		
RZ	TOD*	SW *	D2	PI2*	H42	D2K	UD	TR		
65050101	1.6100	1.0000	8.9015 ⁺⁰³	2.1200 ⁻⁰³	2.3297	1.2904	4.8352 ⁺⁰³	4.8352 ⁺⁰³		
3.9411 ⁺⁰⁰	2.0859 ⁺⁰⁴	1.0000	1.2102 ⁺⁰⁴	NM	1.8042	1.7995	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	4.3397 ⁻⁰³	0.0000 ⁺⁰⁰	0.0642	5.0102 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050102	1.6100	1.0000	1.1848 ⁺⁰⁴	2.0000 ⁻⁰³	2.3688	1.3204	4.8352 ⁺⁰³	4.8352 ⁺⁰³		
5.2365 ⁺⁰⁰	2.0859 ⁺⁰⁴	1.0000	1.6109 ⁺⁰⁴	NM	1.7938	1.7846	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	5.7763 ⁻⁰³	0.0000 ⁺⁰⁰	0.0649	6.7253 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050201	1.6100	1.0000	1.3604 ⁺⁰⁴	1.9500 ⁻⁰³	2.2879	1.2596	8.0208 ⁺⁰³	8.0208 ⁺⁰³		
3.9411 ⁺⁰⁰	3.4601 ⁺⁰⁴	1.0000	1.8495 ⁺⁰⁴	NM	1.8231	1.8154	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.9981 ⁻⁰³	0.0000 ⁺⁰⁰	0.0647	4.5741 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050202	1.6100	1.0000	1.9936 ⁺⁰⁴	1.8100 ⁻⁰³	2.2973	1.2659	8.0208 ⁺⁰³	8.0208 ⁺⁰³		
5.2365 ⁺⁰⁰	3.4601 ⁺⁰⁴	1.0000	2.7104 ⁺⁰⁴	NM	1.8185	1.8106	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	5.8591 ⁻⁰³	0.0000 ⁺⁰⁰	0.0646	6.7233 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050301	1.6100	1.0000	2.6856 ⁺⁰⁴	1.7700 ⁻⁰³	2.2580	1.2374	1.5871 ⁺⁰⁴	1.5871 ⁺⁰⁴		
3.9411 ⁺⁰⁰	6.8466 ⁺⁰⁴	1.0000	3.6513 ⁺⁰⁴	NM	1.8342	1.8273	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.9889 ⁻⁰³	0.0000 ⁺⁰⁰	0.0651	4.5326 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050302	1.6100	1.0000	3.8518 ⁺⁰⁴	1.5400 ⁻⁰³	2.2621	1.2191	1.5871 ⁺⁰⁴	1.5871 ⁺⁰⁴		
5.2365 ⁺⁰⁰	6.8466 ⁺⁰⁴	1.0000	5.2368 ⁺⁰⁴	NM	1.8304	1.8238	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	5.7211 ⁻⁰³	0.0000 ⁺⁰⁰	0.0650	6.5188 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050401	1.6100	1.0000	3.9487 ⁺⁰⁴	1.6500 ⁻⁰³	2.2436	1.2265	2.3778 ⁺⁰⁴	2.3778 ⁺⁰⁴		
3.9411 ⁺⁰⁰	1.0258 ⁺⁰⁵	1.0000	5.3686 ⁺⁰⁴	NM	1.8393	1.8326	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.9147 ⁻⁰³	0.0000 ⁺⁰⁰	0.0653	4.4342 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050402	1.6100	1.0000	5.4503 ⁺⁰⁴	1.5100 ⁻⁰³	2.2549	1.2335	2.3778 ⁺⁰⁴	2.3778 ⁺⁰⁴		
5.2365 ⁺⁰⁰	1.0258 ⁺⁰⁵	1.0000	7.4101 ⁺⁰⁴	NM	1.8329	1.8265	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	5.4033 ⁻⁰³	0.0000 ⁺⁰⁰	0.0651	6.1480 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050501	1.6100	1.0000	5.3089 ⁺⁰⁴	1.5900 ⁻⁰³	2.2313	1.2176	3.2709 ⁺⁰⁴	3.2709 ⁺⁰⁴		
3.9411 ⁺⁰⁰	1.4110 ⁺⁰⁵	1.0000	7.2178 ⁺⁰⁴	NM	1.8446	1.8383	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.8261 ⁻⁰³	0.0000 ⁺⁰⁰	0.0655	4.3184 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050502	1.6100	1.0000	7.1098 ⁺⁰⁴	1.4600 ⁻⁰³	2.2477	1.2284	3.2709 ⁺⁰⁴	3.2709 ⁺⁰⁴		
5.2365 ⁺⁰⁰	1.4110 ⁺⁰⁵	1.0000	9.6663 ⁺⁰⁴	NM	1.8359	1.8297	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	5.1240 ⁻⁰³	0.0000 ⁺⁰⁰	0.0652	5.8189 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050601	1.6100	1.0000	5.9675 ⁺⁰⁴	1.5600 ⁻⁰³	2.2318	1.2189	3.9137 ⁺⁰⁴	3.9137 ⁺⁰⁴		
3.9411 ⁺⁰⁰	1.6883 ⁺⁰⁵	1.0000	8.1132 ⁺⁰⁴	NM	1.8456	1.8388	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.5943 ⁻⁰³	0.0000 ⁺⁰⁰	0.0655	4.0533 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050602	1.6100	1.0000	8.1624 ⁺⁰⁴	1.4300 ⁻⁰³	2.2408	1.2236	3.9137 ⁺⁰⁴	3.9137 ⁺⁰⁴		
5.2365 ⁺⁰⁰	1.6883 ⁺⁰⁵	1.0000	1.1097 ⁺⁰⁵	NM	1.8390	1.8329	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	4.9164 ⁻⁰³	0.0000 ⁺⁰⁰	0.0653	5.5714 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050701	1.6100	1.0000	7.1070 ⁺⁰⁴	1.5400 ⁻⁰³	2.2286	1.2156	4.5963 ⁺⁰⁴	4.5963 ⁺⁰⁴		
3.9411 ⁺⁰⁰	1.9828 ⁺⁰⁵	1.0000	9.6625 ⁺⁰⁴	NM	1.8455	1.8392	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	3.6450 ⁻⁰³	0.0000 ⁺⁰⁰	0.0655	4.1120 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		
65050702	1.6100	1.0000	9.4051 ⁺⁰⁴	1.4000 ⁻⁰³	2.2353	1.2192	4.5963 ⁺⁰⁴	4.5963 ⁺⁰⁴		
5.2365 ⁺⁰⁰	1.9828 ⁺⁰⁵	1.0000	1.2787 ⁺⁰⁵	NM	1.8408	1.8350	2.9996 ⁺⁰²	2.0482 ⁺⁰²		
INFINITE	3.1100 ⁺⁰²	0.0000	4.8236 ⁻⁰³	0.0000 ⁺⁰⁰	0.0654	5.4604 ⁻⁰³	4.6198 ⁺⁰²	2.9996 ⁺⁰²		

CAT 6505 JACKSON BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.									
RUN	MD *	TW/TR*	RED2W	CF *	H12	H12K	PW	PD	
X *	POD	PW/POD*	RED2D	CO	H32	H32K	TW	TD	
RZ	TOD*	8W *	D2	PI2*	H42	D2K	UD	TR	
65050001	2.2000	1.0000	5.8517 ⁺⁰³	1.7100 ⁻⁰³	3.3091	1.3385	1.9581 ⁺⁰³	1.9581 ⁺⁰³	
3.9411 ⁺⁰⁰	2.0938 ⁺⁰⁴	1.0000	9.8292 ⁺⁰³	NM	1.7909	1.7759	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	4.4715 ⁻⁰³	0.0000 ⁺⁰⁰	0.0916	5.8659 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65050802	2.2000	1.0000	8.0753 ⁺⁰³	1.5500 ⁻⁰³	3.3443	1.3569	1.9581 ⁺⁰³	1.9581 ⁺⁰³	
5.2365 ⁺⁰⁰	2.0938 ⁺⁰⁴	1.0000	1.3564 ⁺⁰⁴	NM	1.7793	1.7645	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	6.1707 ⁻⁰³	0.0000 ⁺⁰⁰	0.0910	8.1904 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65050901	2.2000	1.0000	8.5674 ⁺⁰³	1.6400 ⁻⁰³	3.2556	1.3049	3.2733 ⁺⁰³	3.2733 ⁺⁰³	
3.9411 ⁺⁰⁰	3.5001 ⁺⁰⁴	1.0000	1.4391 ⁺⁰⁴	NM	1.8037	1.7905	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.9163 ⁻⁰³	0.0000 ⁺⁰⁰	0.0923	5.0758 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65050902	2.2000	1.0000	1.3109 ⁺⁰⁴	1.4900 ⁻⁰³	3.2723	1.3139	3.2733 ⁺⁰³	3.2733 ⁺⁰³	
5.2365 ⁺⁰⁰	2.0938 ⁺⁰⁴	1.0000	2.2020 ⁺⁰⁴	NM	1.7978	1.7844	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	5.9926 ⁻⁰³	0.0000 ⁺⁰⁰	0.0920	7.8132 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051001	2.2000	1.0000	1.5602 ⁺⁰⁴	1.5100 ⁻⁰³	3.2015	1.2722	6.4589 ⁺⁰³	6.4589 ⁺⁰³	
3.9411 ⁺⁰⁰	6.9064 ⁺⁰⁴	1.0000	2.6207 ⁺⁰⁴	NM	1.8179	1.8062	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.6145 ⁻⁰³	0.0000 ⁺⁰⁰	0.0933	4.6180 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051002	2.2000	1.0000	2.3688 ⁺⁰⁴	1.3800 ⁻⁰³	3.2363	1.2909	6.4589 ⁺⁰³	6.4589 ⁺⁰³	
5.2365 ⁺⁰⁰	6.9064 ⁺⁰⁴	1.0000	3.9788 ⁺⁰⁴	NM	1.8063	1.7942	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	5.4876 ⁻⁰³	0.0000 ⁺⁰⁰	0.0924	7.0977 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051101	2.2000	1.0000	2.1935 ⁺⁰⁴	1.4600 ⁻⁰³	3.1816	1.2604	9.7030 ⁺⁰³	9.7030 ⁺⁰³	
3.9411 ⁺⁰⁰	1.0375 ⁺⁰⁵	1.0000	3.6844 ⁺⁰⁴	NM	1.8245	1.8132	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.3825 ⁻⁰³	0.0000 ⁺⁰⁰	0.0933	4.2914 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051102	2.2000	1.0000	3.0755 ⁺⁰⁴	1.3200 ⁻⁰³	3.1838	1.2599	9.7030 ⁺⁰³	9.7030 ⁺⁰³	
5.2365 ⁺⁰⁰	1.0375 ⁺⁰⁵	1.0000	5.1660 ⁺⁰⁴	NM	1.8218	1.8110	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	4.7427 ⁻⁰³	0.0000 ⁺⁰⁰	0.0932	6.0366 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051201	2.2000	1.0000	2.7686 ⁺⁰⁴	1.4200 ⁻⁰³	3.1647	1.2498	1.2859 ⁺⁰⁴	1.2859 ⁺⁰⁴	
3.9411 ⁺⁰⁰	1.3750 ⁺⁰⁵	1.0000	4.6505 ⁺⁰⁴	NM	1.8292	1.8187	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.2215 ⁻⁰³	0.0000 ⁺⁰⁰	0.0936	4.0679 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051202	2.2000	1.0000	3.9880 ⁺⁰⁴	1.2900 ⁻⁰³	3.1640	1.2503	1.2859 ⁺⁰⁴	1.2859 ⁺⁰⁴	
5.2365 ⁺⁰⁰	1.3750 ⁺⁰⁵	1.0000	6.6988 ⁺⁰⁴	NM	1.8294	1.8177	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	4.6404 ⁻⁰³	0.0000 ⁺⁰⁰	0.0936	5.8541 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051301	2.2000	1.0000	3.2804 ⁺⁰⁴	1.4000 ⁻⁰³	3.1537	1.2438	1.5782 ⁺⁰⁴	1.5782 ⁺⁰⁴	
3.9411 ⁺⁰⁰	1.6875 ⁺⁰⁵	1.0000	5.5101 ⁺⁰⁴	NM	1.8332	1.8228	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.1102 ⁻⁰³	0.0000 ⁺⁰⁰	0.0938	3.9103 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051302	2.2000	1.0000	4.5954 ⁺⁰⁴	1.2700 ⁻⁰³	3.1552	1.2433	1.5782 ⁺⁰⁴	1.5782 ⁺⁰⁴	
5.2365 ⁺⁰⁰	1.6875 ⁺⁰⁵	1.0000	7.7190 ⁺⁰⁴	NM	1.8308	1.8205	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	4.3569 ⁻⁰³	0.0000 ⁺⁰⁰	0.0937	5.4922 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051401	2.2000	1.0000	3.7604 ⁺⁰⁴	1.3900 ⁻⁰³	3.1432	1.2375	1.8558 ⁺⁰⁴	1.8558 ⁺⁰⁴	
3.9411 ⁺⁰⁰	1.9844 ⁺⁰⁵	1.0000	6.3164 ⁺⁰⁴	NM	1.8364	1.8264	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	3.0319 ⁻⁰³	0.0000 ⁺⁰⁰	0.0939	3.7987 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	
65051402	2.2000	1.0000	5.3072 ⁺⁰⁴	1.2500 ⁻⁰³	3.1642	1.2464	1.8558 ⁺⁰⁴	1.8558 ⁺⁰⁴	
5.2365 ⁺⁰⁰	1.9844 ⁺⁰⁵	1.0000	8.9145 ⁺⁰⁴	NM	1.8264	1.8172	2.9509 ⁺⁰²	1.5803 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	0.0000	4.2790 ⁻⁰³	0.0000 ⁺⁰⁰	0.0934	5.4247 ⁻⁰³	5.5450 ⁺⁰²	2.9509 ⁺⁰²	

PD,POD CALCULATED FROM RE (AUTHOR), CF INTERPOLATED

65050101		JACKSON		PROFILE TABULATION		36 POINTS, DELTA AT POINT 36			
I	Y	PTZ/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.3000+00	1.0000+00	NM	0.76449	0.00000	0.00000	1.46450	0.00000	
2	7.6200-05	1.1634+00	NM	0.96676	0.29197	0.34656	1.40877	0.24601	
3	1.0160-04	1.1599+00	NM	0.96667	0.28896	0.34310	1.40983	0.24336	
4	1.2700-04	1.2040+00	NM	0.96972	0.32461	0.38350	1.39617	0.27472	
5	1.7780-04	1.2266+00	NM	0.97021	0.34049	0.40138	1.38967	0.28884	
6	2.2860-04	1.2733+00	NM	0.97123	0.37129	0.43360	1.37637	0.31646	
7	2.7940-04	1.2961+00	NM	0.97171	0.38521	0.45088	1.37007	0.32909	
8	3.3020-04	1.3417+00	NM	0.97264	0.41106	0.47901	1.35792	0.35275	
9	4.5720-04	1.3854+00	NM	0.97350	0.43395	0.50359	1.34670	0.37394	
10	5.8420-04	1.4476+00	NM	0.97466	0.46372	0.53509	1.33151	0.40187	
11	8.3820-04	1.4791+00	NM	0.97522	0.47776	0.54976	1.32411	0.41519	
12	1.0922-03	1.5330+00	NM	0.97650	0.50870	0.58164	1.30736	0.44490	
13	1.3462-03	1.5817+00	NM	0.97697	0.51962	0.59275	1.30130	0.45551	
14	1.9812-03	1.6934+00	NM	0.97871	0.55970	0.63265	1.27847	0.49501	
15	2.6162-03	1.7472+00	NM	0.97951	0.57742	0.65023	1.26811	0.51276	
16	3.2512-03	1.8424+00	NM	0.98083	0.60661	0.67840	1.25072	0.54241	
17	3.8862-03	1.8836+00	NM	0.98138	0.61847	0.68969	1.24355	0.55461	
18	5.1562-03	1.9863+00	NM	0.98267	0.64647	0.71592	1.22642	0.58375	
19	6.4262-03	2.0733+00	NM	0.98374	0.66867	0.73634	1.21265	0.60722	
20	8.9662-03	2.2634+00	NM	0.98591	0.71368	0.77667	1.18431	0.65580	
21	1.1506-02	2.4066+00	NM	0.98745	0.74514	0.80400	1.16424	0.69058	
22	1.6586-02	2.6625+00	NM	0.99002	0.79749	0.84794	1.13053	0.75004	
23	2.1666-02	2.8923+00	NM	0.99219	0.84118	0.88313	1.10223	0.80122	
24	2.6746-02	3.0993+00	NM	0.99403	0.87841	0.91207	1.07810	0.84599	
25	3.1826-02	3.3017+00	NM	0.99575	0.91314	0.93820	1.05564	0.88875	
26	3.6906-02	3.4875+00	NM	0.99726	0.94379	0.96058	1.03590	0.92729	
27	3.9446-02	3.5637+00	NM	0.99786	0.95605	0.96930	1.02803	0.94293	
28	4.1986-02	3.6271+00	NM	0.99835	0.96612	0.97649	1.02158	0.95586	
29	4.4526-02	3.6872+00	NM	0.99881	0.97556	0.98312	1.01555	0.96806	
30	4.7066-02	3.7263+00	NM	0.99911	0.98165	0.98730	1.01167	0.97597	
31	4.9606-02	3.7727+00	NM	0.99946	0.98683	0.99213	1.00710	0.98534	
32	5.2146-02	3.7854+00	NM	0.99955	0.99070	0.99368	1.00586	0.98789	
33	5.4686-02	3.8050+00	NM	0.99970	0.99379	0.99575	1.00394	0.99184	
34	5.7226-02	3.8178+00	NM	0.99979	0.99576	0.99710	1.00269	0.99442	
35	5.9766-02	3.8377+00	NM	0.99984	0.99879	0.99917	1.00077	0.99840	
D 36	6.2306-02	3.8456+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

65050102		JACKSON		PROFILE TABULATION		44 POINTS, DELTA AT POINT 44			
I	Y	PTZ/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000+00	1.0000+00	NM	0.96384	0.00000	0.00000	1.46392	0.00000	
2	7.6200-05	1.1315+00	NM	0.96740	0.26326	0.31349	1.41797	0.22108	
3	1.0160-04	1.1189+00	NM	0.96697	0.24670	0.29432	1.42336	0.20678	
4	1.2700-04	1.1226+00	NM	0.96717	0.25454	0.30341	1.42085	0.21354	
5	1.5240-04	1.1471+00	NM	0.96778	0.27778	0.33019	1.41298	0.23368	
6	1.7780-04	1.1746+00	NM	0.96845	0.30124	0.35700	1.40444	0.25419	
7	2.0320-04	1.1893+00	NM	0.96880	0.31293	0.37027	1.39997	0.26448	
8	2.2860-04	1.2047+00	NM	0.96916	0.32469	0.38354	1.39533	0.27487	
9	2.5400-04	1.2293+00	NM	0.96973	0.34236	0.40336	1.38810	0.29059	
10	3.0480-04	1.2497+00	NM	0.97018	0.35616	0.41874	1.38224	0.30294	
11	3.8100-04	1.2837+00	NM	0.97092	0.37773	0.44257	1.37273	0.32240	
12	5.3340-04	1.3225+00	NM	0.97174	0.40040	0.46742	1.36225	0.34312	
13	6.6040-04	1.3496+00	NM	0.97230	0.41537	0.48354	1.35514	0.35682	
14	7.8740-04	1.3606+00	NM	0.97252	0.42120	0.48981	1.35231	0.36220	
15	9.1440-04	1.3956+00	NM	0.97320	0.43900	0.50884	1.34350	0.37874	
16	1.0414-03	1.4098+00	NM	0.97348	0.44595	0.51622	1.34000	0.38524	
17	1.1684-03	1.4369+00	NM	0.97399	0.45879	0.52979	1.33342	0.39731	
18	1.4224-03	1.4785+00	NM	0.97475	0.47750	0.54936	1.32363	0.41504	
19	1.6764-03	1.5199+00	NM	0.97542	0.49343	0.56586	1.31510	0.43027	
20	1.9304-03	1.5330+00	NM	0.97572	0.50044	0.57306	1.31130	0.43702	
21	2.1844-03	1.5711+00	NM	0.97636	0.51553	0.58848	1.30300	0.45163	
22	2.4384-03	1.6104+00	NM	0.97701	0.53039	0.60351	1.29469	0.46614	
23	2.6924-03	1.6292+00	NM	0.97732	0.53728	0.61043	1.29080	0.47291	
24	3.3274-03	1.6861+00	NM	0.97821	0.55725	0.63030	1.27937	0.49266	
25	3.9624-03	1.7437+00	NM	0.97907	0.57628	0.64899	1.26829	0.51171	
26	4.5974-03	1.7922+00	NM	0.97977	0.59152	0.66379	1.25929	0.52711	
27	5.2324-03	1.8240+00	NM	0.98022	0.60114	0.67305	1.25354	0.53692	
28	6.5024-03	1.9007+00	NM	0.98126	0.62329	0.69412	1.24019	0.55969	
29	7.7724-03	1.9902+00	NM	0.98242	0.64748	0.71675	1.22540	0.58491	
30	9.0424-03	2.0664+00	NM	0.98336	0.66664	0.73465	1.21335	0.60547	
31	1.1582-02	2.1736+00	NM	0.98463	0.69294	0.75815	1.19709	0.63333	
32	1.7932-02	2.4445+00	NM	0.98761	0.75320	0.81080	1.15880	0.69969	
33	2.4282-02	2.6930+00	NM	0.99014	0.80345	0.85274	1.12644	0.75701	
34	3.0632-02	2.9184+00	NM	0.99228	0.84597	0.88685	1.09898	0.80699	
35	3.6982-02	3.1371+00	NM	0.99425	0.88501	0.91705	1.07371	0.85409	
36	4.3332-02	3.3459+00	NM	0.99604	0.92054	0.94362	1.05079	0.89801	
37	4.9682-02	3.5267+00	NM	0.99752	0.95012	0.96310	1.03179	0.93537	
38	4.9708-02	3.5336+00	NM	0.99757	0.95113	0.96582	1.03114	0.93666	
39	5.4762-02	3.6411+00	NM	0.99843	0.96833	0.97803	1.02014	0.95872	
40	5.9842-02	3.7397+00	NM	0.99919	0.98374	0.98880	1.01032	0.97870	
41	6.4922-02	3.8030+00	NM	0.99968	0.99349	0.99554	1.00413	0.99145	
42	6.7462-02	3.8238+00	NM	0.99984	0.99667	0.99772	1.00211	0.99561	
43	7.0002-02	3.8367+00	NM	0.99993	0.99863	0.99907	1.00087	0.99820	
D 44	7.2542-02	3.8456+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST
AT I=33 DATA WERE AVERAGED

65050801		JACKSON		PROFILE TABULATION			34 POINTS, DELTA AT POINT 34		
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.94885	0.00000	0.00000	1.86733	0.00000	
2	1.2700 ⁻ -04	1.2256 ⁺ +00	NM	0.95445	0.24863	0.33099	1.77231	0.18676	
3	3.3100 ⁻ -04	1.4331 ⁺ +00	NM	0.95859	0.33447	0.43637	1.70217	0.25636	
4	9.6520 ⁻ -04	1.7768 ⁺ +00	NM	0.96403	0.42940	0.54483	1.60987	0.33843	
5	1.5748 ⁻ -03	1.9357 ⁺ +00	NM	0.96613	0.46321	0.58120	1.57435	0.36917	
6	2.4638 ⁻ -03	2.1162 ⁺ +00	NM	0.96828	0.49705	0.61639	1.53780	0.40082	
7	3.7084 ⁻ -03	2.2913 ⁺ +00	NM	0.97022	0.52687	0.64635	1.50498	0.42948	
8	5.0038 ⁻ -03	2.4689 ⁺ +00	NM	0.97206	0.55495	0.67369	1.47369	0.45714	
9	6.2738 ⁻ -03	2.6098 ⁺ +00	NM	0.97346	0.57600	0.69361	1.45096	0.47833	
10	9.9568 ⁻ -03	2.9873 ⁺ +00	NM	0.97693	0.62826	0.74100	1.39109	0.53268	
11	1.1989 ⁻ -02	3.1886 ⁺ +00	NM	0.97866	0.65419	0.76342	1.36184	0.56058	
12	1.3894 ⁻ -02	3.3669 ⁺ +00	NM	0.98012	0.67621	0.78191	1.33706	0.58480	
13	1.5799 ⁻ -02	3.5433 ⁺ +00	NM	0.98151	0.69726	0.79911	1.31347	0.60839	
14	1.7704 ⁻ -02	3.7300 ⁺ +00	NM	0.98293	0.71881	0.81624	1.28947	0.63301	
15	1.9609 ⁻ -02	3.8995 ⁺ +00	NM	0.98417	0.73779	0.83094	1.26647	0.65508	
16	2.1768 ⁻ -02	4.1160 ⁺ +00	NM	0.98569	0.76131	0.84866	1.24266	0.68294	
17	2.3546 ⁻ -02	4.2488 ⁺ +00	NM	0.98659	0.77535	0.85898	1.22737	0.69986	
18	2.5451 ⁻ -02	4.4681 ⁺ +00	NM	0.98803	0.79798	0.87521	1.20295	0.72755	
19	2.7356 ⁻ -02	4.6362 ⁺ +00	NM	0.98909	0.81488	0.88702	1.18491	0.74860	
20	2.9261 ⁻ -02	4.8410 ⁺ +00	NM	0.99035	0.83493	0.90072	1.16367	0.77404	
21	3.1140 ⁻ -02	5.0371 ⁺ +00	NM	0.99150	0.85378	0.91320	1.14404	0.79822	
22	3.3071 ⁻ -02	5.1943 ⁺ +00	NM	0.99240	0.86854	0.92278	1.12879	0.81749	
23	3.7160 ⁻ -02	5.6372 ⁺ +00	NM	0.99481	0.90880	0.94793	1.08797	0.87128	
24	4.0691 ⁻ -02	5.9191 ⁺ +00	NM	0.99625	0.93350	0.96269	1.06351	0.90520	
25	4.2723 ⁻ -02	6.0831 ⁺ +00	NM	0.99706	0.94757	0.97087	1.04497	0.92482	
26	4.4755 ⁻ -02	6.2067 ⁺ +00	NM	0.99766	0.95803	0.97685	1.03968	0.93957	
27	4.7269 ⁻ -02	6.3179 ⁺ +00	NM	0.99819	0.96734	0.98211	1.03076	0.95280	
28	5.0851 ⁻ -02	6.3108 ⁺ +00	NM	0.99900	0.98320	0.99094	1.01564	0.97568	
29	5.3391 ⁻ -02	6.5602 ⁺ +00	NM	0.99930	0.98733	0.99315	1.01184	0.98154	
30	5.7175 ⁻ -02	6.6221 ⁺ +00	NM	0.99958	0.99237	0.99509	1.00711	0.98886	
31	6.1773 ⁻ -02	6.6679 ⁺ +00	NM	0.99978	0.99608	0.99789	1.00365	0.99426	
32	6.6853 ⁻ -02	6.6674 ⁺ +00	NM	0.99978	0.99608	0.99789	1.00365	0.99426	
33	7.1933 ⁻ -02	6.6848 ⁺ +00	NM	0.99986	0.99745	0.99863	1.00237	0.99626	
D 34	7.6225 ⁻ -02	6.7165 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

65050802		JACKSON		PROFILE TABULATION			37 POINTS, DELTA AT POINT 37		
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +30	1.0000 ⁺ +00	NM	0.94885	0.00000	0.00000	1.86733	0.00000	
2	7.6200 ⁻ -05	1.2056 ⁺ +00	NM	0.95401	0.23809	0.31763	1.77982	0.17846	
3	1.2700 ⁻ -04	1.2001 ⁺ +00	NM	0.95388	0.23508	0.31380	1.78192	0.17610	
4	1.7780 ⁻ -04	1.2001 ⁺ +00	NM	0.95388	0.23508	0.31380	1.78192	0.17610	
5	2.2860 ⁻ -04	1.1995 ⁺ +00	NM	0.95388	0.23500	0.31371	1.78197	0.17604	
6	2.7940 ⁻ -04	1.2378 ⁺ +00	NM	0.95472	0.25479	0.33876	1.76780	0.19163	
7	3.3020 ⁻ -04	1.2378 ⁺ +00	NM	0.95471	0.25471	0.33866	1.76785	0.19157	
8	3.8100 ⁻ -04	1.2725 ⁺ +00	NM	0.95546	0.27136	0.35952	1.75522	0.20483	
9	4.5720 ⁻ -04	1.3082 ⁺ +00	NM	0.95619	0.28711	0.37902	1.74273	0.21748	
10	5.8420 ⁻ -04	1.3417 ⁺ +00	NM	0.95686	0.30086	0.39587	1.73140	0.22864	
11	7.1120 ⁻ -04	1.4833 ⁺ +00	NM	0.95948	0.35097	0.45587	1.68708	0.27021	
12	8.3820 ⁻ -04	1.5513 ⁺ +00	NM	0.96062	0.37160	0.47986	1.66761	0.28776	
13	1.0922 ⁻ -03	1.6565 ⁺ +00	NM	0.96228	0.40030	0.51255	1.63947	0.31263	
14	1.3462 ⁻ -03	1.7282 ⁺ +00	NM	0.96334	0.41807	0.53237	1.62152	0.32831	
15	1.9812 ⁻ -03	1.8364 ⁺ +00	NM	0.96484	0.44263	0.55920	1.59611	0.35035	
16	2.6182 ⁻ -03	1.9472 ⁺ +00	NM	0.96627	0.46548	0.58360	1.57192	0.37127	
17	3.8862 ⁻ -03	2.1217 ⁺ +00	NM	0.96834	0.49804	0.61739	1.53673	0.40176	
18	5.1562 ⁻ -03	2.2678 ⁺ +00	NM	0.96996	0.52301	0.64253	1.50926	0.42572	
19	7.6962 ⁻ -03	2.4422 ⁺ +00	NM	0.97179	0.55085	0.66975	1.47828	0.45306	
20	1.0236 ⁻ -02	2.6846 ⁺ +00	NM	0.97417	0.58679	0.70363	1.43791	0.48934	
21	1.5316 ⁻ -02	2.9777 ⁺ +00	NM	0.97685	0.62699	0.73988	1.39253	0.53132	
22	2.0396 ⁻ -02	3.3842 ⁺ +00	NM	0.98026	0.67831	0.78365	1.33470	0.58714	
23	2.4841 ⁻ -02	3.6842 ⁺ +00	NM	0.98259	0.71359	0.81213	1.29527	0.62700	
24	3.0556 ⁻ -02	4.0824 ⁺ +00	NM	0.98546	0.75770	0.84598	1.24660	0.67863	
25	3.7511 ⁻ -02	4.6077 ⁺ +00	NM	0.98892	0.81203	0.88505	1.18793	0.74904	
26	4.3256 ⁻ -02	4.9004 ⁺ +00	NM	0.99070	0.84072	0.90497	1.15765	0.78138	
27	5.0241 ⁻ -02	5.4514 ⁺ +00	NM	0.99382	0.89214	0.93769	1.10472	0.84881	
28	5.5956 ⁻ -02	5.8495 ⁺ +00	NM	0.99590	0.92747	0.95913	1.06945	0.89685	
29	5.8496 ⁻ -02	6.1024 ⁺ +00	NM	0.99716	0.94921	0.97182	1.04820	0.92713	
30	6.1036 ⁻ -02	6.2332 ⁺ +00	NM	0.99779	0.96025	0.97812	1.03755	0.94272	
31	6.2941 ⁻ -02	6.3044 ⁺ +00	NM	0.99812	0.96622	0.98148	1.03183	0.95120	
32	6.6116 ⁻ -02	6.4665 ⁺ +00	NM	0.99888	0.97964	0.98894	1.01407	0.97043	
33	6.8636 ⁻ -02	6.5319 ⁺ +00	NM	0.99917	0.98501	0.99189	1.01401	0.97818	
34	7.1196 ⁻ -02	6.5958 ⁺ +00	NM	0.99946	0.99023	0.99473	1.00911	0.98575	
35	7.3736 ⁻ -02	6.6751 ⁺ +00	NM	0.99982	0.99666	0.99821	1.00310	0.99512	
36	7.5641 ⁻ -02	6.6751 ⁺ +00	NM	0.99982	0.99666	0.99821	1.00310	0.99512	
D 37	7.8816 ⁻ -02	6.7165 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

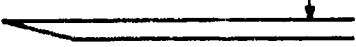
INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

65051401		JACKSON		PROFILE TABULATION		39 POINTS, DELTA AT POINT 39			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.94885	0.00000	0.00000	1.86733	0.00000	
2	1.2700+04	1.7586+00	NM	0.96378	0.42522	0.54024	1.61419	0.33468	
3	1.5240+04	1.7897+00	NM	0.96421	0.43233	0.54802	1.60685	0.34105	
4	1.7780+04	1.8253+00	NM	0.96469	0.44023	0.55661	1.59862	0.34818	
5	2.2860+04	1.8767+00	NM	0.96537	0.45118	0.56840	1.58712	0.35813	
6	2.7940+04	1.9206+00	NM	0.96594	0.46018	0.57800	1.57757	0.36638	
7	3.5560+04	1.9924+00	NM	0.96682	0.47425	0.59281	1.56252	0.37940	
8	4.3180+04	2.0509+00	NM	0.96752	0.48524	0.60424	1.55086	0.38967	
9	5.5880+04	2.1464+00	NM	0.96862	0.50238	0.62191	1.53198	0.40589	
10	6.8580+04	2.2332+00	NM	0.96957	0.51725	0.63679	1.51562	0.42015	
11	8.1280+04	2.3126+00	NM	0.97044	0.53034	0.64978	1.50113	0.43286	
12	9.3980+04	2.4328+00	NM	0.97169	0.54938	0.66834	1.47992	0.45160	
13	1.1938+03	2.4918+00	NM	0.97229	0.55844	0.67702	1.46978	0.46063	
14	1.4478+03	2.5644+00	NM	0.97301	0.56931	0.68733	1.45758	0.47156	
15	1.7918+03	2.6457+00	NM	0.97380	0.59121	0.69847	1.44420	0.48364	
16	2.0828+03	2.7597+00	NM	0.97468	0.59739	0.71337	1.42595	0.50027	
17	2.4638+03	2.8317+00	NM	0.97544	0.60736	0.72240	1.41470	0.51064	
18	3.0988+03	2.9507+00	NM	0.97661	0.62342	0.73673	1.39657	0.52753	
19	4.3688+03	3.1499+00	NM	0.97833	0.64929	0.75924	1.36736	0.55526	
20	5.3848+03	3.2866+00	NM	0.97947	0.66639	0.77373	1.34809	0.57395	
21	6.5278+03	3.5389+00	NM	0.98146	0.69675	0.79870	1.31404	0.60782	
22	8.0264+03	3.6525+00	NM	0.98235	0.70996	0.80926	1.29931	0.62284	
23	9.9568+03	3.8439+00	NM	0.98376	0.73163	0.82621	1.27527	0.64787	
24	1.1989+02	4.0516+00	NM	0.98524	0.75439	0.84351	1.25022	0.67469	
25	1.3874+02	4.2719+00	NM	0.98674	0.77776	0.86074	1.22475	0.70279	
26	1.5779+02	4.4523+00	NM	0.98793	0.79637	0.87408	1.20468	0.72557	
27	1.7704+02	4.6559+00	NM	0.98922	0.81683	0.88837	1.18283	0.75106	
28	1.9583+02	4.8537+00	NM	0.99042	0.83622	0.90155	1.16237	0.77562	
29	2.2149+02	5.1286+00	NM	0.99203	0.86240	0.91882	1.13511	0.80945	
30	2.4689+02	5.3998+00	NM	0.99354	0.88746	0.93477	1.10946	0.84254	
31	2.7356+02	5.6702+00	NM	0.99498	0.91173	0.94971	1.08504	0.87527	
32	3.0331+02	5.9481+00	NM	0.99640	0.93601	0.96416	1.06106	0.90868	
33	3.3452+02	6.2398+00	NM	0.99782	0.96081	0.97843	1.03701	0.94351	
34	3.6827+02	6.4042+00	NM	0.99855	0.97451	0.98610	1.02394	0.96305	
35	3.9421+02	6.4827+00	NM	0.99895	0.98098	0.98968	1.01781	0.97236	
36	4.3231+02	6.5863+00	NM	0.99942	0.98946	0.99431	1.00984	0.98462	
37	4.8311+02	6.6534+00	NM	0.99973	0.99490	0.99726	1.00475	0.99255	
38	5.5931+02	6.6970+00	NM	0.99991	0.99843	0.99916	1.00146	0.99770	
D 39	6.3551+02	6.7165+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST
AT I=12 DATA WERE AVERAGED

65051402		JACKSON		PROFILE TABULATION		35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.94885	0.00000	0.00000	1.86733	0.00000	
2	7.6200+05	1.5764+00	NM	0.96103	0.37876	0.48810	1.66069	0.29392	
3	1.0160+04	1.6093+00	NM	0.96147	0.38676	0.49724	1.65288	0.30083	
4	1.5240+04	1.6704+00	NM	0.96249	0.40385	0.51653	1.63592	0.31574	
5	2.0320+04	1.6931+00	NM	0.96283	0.40955	0.52290	1.63018	0.32076	
6	3.3020+04	1.8182+00	NM	0.96460	0.43866	0.55491	1.60026	0.34676	
7	4.5720+04	1.9081+00	NM	0.96578	0.45743	0.57530	1.58027	0.36405	
8	5.8420+04	1.9999+00	NM	0.96691	0.47569	0.59432	1.56098	0.38073	
9	7.1120+04	2.0530+00	NM	0.96755	0.48562	0.60464	1.55024	0.39003	
10	8.3820+04	2.1262+00	NM	0.96839	0.49862	0.61819	1.53587	0.40250	
11	9.6520+04	2.1761+00	NM	0.96896	0.50754	0.62704	1.52632	0.41082	
12	1.0922+03	2.2225+00	NM	0.96947	0.51544	0.63498	1.51762	0.41840	
13	1.2192+03	2.2770+00	NM	0.97006	0.52453	0.64401	1.50757	0.42720	
14	1.3462+03	2.3202+00	NM	0.97052	0.53157	0.65077	1.49977	0.43406	
15	1.6002+03	2.4019+00	NM	0.97138	0.54453	0.66369	1.48520	0.44685	
16	1.8542+03	2.5514+00	NM	0.97288	0.56738	0.68561	1.45975	0.46961	
17	2.1082+03	2.5335+00	NM	0.97271	0.56471	0.68290	1.46275	0.46692	
18	2.3622+03	2.5936+00	NM	0.97330	0.57362	0.69138	1.45274	0.47591	
19	2.6162+03	2.6420+00	NM	0.97377	0.58066	0.69790	1.44481	0.48308	
20	3.2512+03	2.8276+00	NM	0.97550	0.60680	0.72189	1.41534	0.51005	
21	3.8862+03	2.8640+00	NM	0.97583	0.61177	0.72636	1.40973	0.51525	
22	5.1562+03	3.0299+00	NM	0.97731	0.63384	0.74589	1.38479	0.53863	
23	6.4262+03	3.1518+00	NM	0.97835	0.64952	0.75944	1.36709	0.55592	
24	7.6962+03	3.2718+00	NM	0.97935	0.66457	0.77220	1.35013	0.57194	
25	8.9662+03	3.3893+00	NM	0.98030	0.67893	0.78416	1.33400	0.58763	
26	1.0236+02	3.4854+00	NM	0.98106	0.69043	0.79358	1.32112	0.60069	
27	1.4300+02	3.8201+00	NM	0.98359	0.72897	0.82413	1.27821	0.64477	
28	1.7856+02	4.1147+00	NM	0.98565	0.76117	0.84856	1.24281	0.68277	
29	2.2733+02	4.3574+00	NM	0.98731	0.78664	0.86715	1.21515	0.71361	
30	2.5476+02	4.6468+00	NM	0.98916	0.81593	0.88775	1.18379	0.74992	
31	2.9286+02	4.9215+00	NM	0.99083	0.84275	0.90592	1.15553	0.78399	
32	3.3096+02	5.2364+00	NM	0.99264	0.87245	0.92528	1.12478	0.82263	
33	3.6906+02	5.4993+00	NM	0.99413	0.89737	0.94093	1.09984	0.85582	
34	4.0716+02	5.7689+00	NM	0.99549	0.92043	0.95494	1.07640	0.88716	
D 35	5.5956+02	6.7165+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

rough 	M : 4.95 R THETA X 10 ⁻³ : 4 - 12 TW / TR : 0.6 - 1.0	6506 ZPG (ROUGH) AW-MHT-SHT
Blow-down tunnel with fixed nozzle block. Running time 45-90 s. W = 0.15, H = 0.18, L = 0.50 m. PD : 17.5 MN/m ² . 340 < T0 < 610 K. Air. 16 < RE/m X 10 ⁻⁶ < 50.		
YOUNG F.L., 1965. Experimental investigation of the effects of surface roughness on compressible turbulent boundary layer skin friction and heat transfer. DRL 532.		

- 1 The test boundary layer was formed on a flat plate machined from solid copper (W = 0.152, L = 0.371 m) with a sharp leading edge (X = 0) chamfered at 15°. Various fairings and covers brought the overall length up to 0.487 m. The test surface was mounted facing downwards a little above [E] the tunnel centre line. The test stations were near X = 0.3 m. The plate was actively cooled by two separate circuits and maintained at a temperature close to 310 K throughout the tests. Four plate surfaces were employed. For the first series, 01, the basic upper plate was machined and ground to give an effectively smooth and flat surface. For the tests with a rough surface (series 02-04) the basic plate was covered with a layer of tin-lead solder approximately, after machining, 0.76 mm thick. The roughness was then formed in this solder layer under pressure by specially machined rollers. Both the plate surface and the balance and calorimeter elements had surfaces formed in this manner, and were held in suitable jigs so as to prevent distortion during the process. The roughness pattern had a regular 90° saw tooth (V-groove) section aligned across the plate, with wavelength of 0.127, 0.254 or 0.762 mm, and, correspondingly, peak to trough heights of one half the wavelength. This roughness started about 12.7 mm behind a boundary layer trip consisting of a strip of "number 80 grit-cloth" running from X = 12 to 25 mm.
- 3
- 6 The plate contained buried iron-constantan thermocouples on the centre line at X = 50, 140, 185, 270 and 315 mm, used to record TW and to allow adjustment of the cooling system. Static tappings (d = 1.6 mm) were placed at X = 115, 240 and 370 mm. The FEB and isolated mass calorimeter were mounted at X = 317.5 mm and 25.4 mm to either side of the centre line. The FEB had an element of 25.4 mm diameter, with a nominal annular clearance of 0.05 mm. The balance was calibrated in a wide range of thermal conditions, and it was found that errors resulting from thermal strains in the flexures outweighed any other source of error. By trial and error selection and mounting of flexures, it is claimed that it was possible to obtain a repeatable calibration. The insulated mass calorimeter consisted of a small section of the surface, 26.4 mm in diameter and 3.8 mm thick, which was separated from the mass of the plate by a small teflon insulating ring and not cooled by the plate cooling system. Heat transfer determinations were made by cooling the insulated mass to a temperature below that of the plate, by means of an external supply tube delivering water directly on to the surface of the calorimeter during a tunnel run. The external supply was then removed, and an observation of the rate of change of temperature of the isolated mass as it passed through the temperature of the plate used to calculate the local heat flux.
- 7 The Pitot probes used for profile measurements were CPP for which d₁ ranged from 0.5 to 0.9 mm. The tubes were kept as short and as large as possible to minimise the effects of time lags, and to provide sufficient strength at the high temperatures used. The small tubes were rapidly faired, telescopically, to 2.6 mm diameter. The elbow of the probe was stiffened by a web (details in the photograph are obscure), after which it was soldered into a double wedge drive shaft. "The length of the unstiffened probe tip was then only" 12.7 mm. The traverse gear was driven from the floor of the tunnel.
- 8 The balance and calorimeter were centred (text) on X = 317.5 mm and 25.4 mm to either side of the centre line. The profiles were measured in a range from X = 286 to 297 mm (tables in source paper).
- 9 No significant difference was found between the pressures recorded at the three static tappings when

- running with the smooth surface, and the average of the three was used for the wall measurement runs. For profile measurements the static pressure was taken as constant at an average value determined from the reservoir pressure and the free stream PT2 value, and assumed constant through the layer. Total temperature was assumed to be given by the Crocco / Van Driest correlation. No probe corrections were applied, and viscosity was determined from power laws matched over a range to the Sutherland formula.
- 12 The editors have presented all the author's profile data, incorporating the author's assumptions and procedures. The CF and CQ data have been interpolated on the basis of both Reynolds number and TW/TR values. These variables are strongly correlated, as unit Reynolds number was changed by ranging the tunnel reservoir temperature while changes in model temperature were relatively small. The values given are an average of the two interpolations. The differences between the two showed no systematic variation. The scatter of the results, which became apparent during interpolation, is about $\pm 10\%$. The profiles consist of four sets, one for each roughness, each describing five different TW/TR states.
- § DATA 6506 0101-0405. Pitot profiles. NX = 1. CF measured with an FEB, CQ with an isolated mass calorimeter, separately. Roughened surface.

16 Editors' comments

This difficult experiment is very fully described in the source paper, and seems to have been performed very carefully. There are no comparable experiments, though the smooth-wall adiabatic tests are supplemented by the earlier work of Moore - CAT 6201 with the same apparatus. The smooth-wall experimental range overlaps that of Voisinnet & Lee - CAT 7202 who studied a tunnel-wall boundary layer.

For the majority of the profiles, measurements did not extend within the momentum-deficit peak, and it should be noted that, unfortunately, there are no measured TO data.

CAT 6506		YOUNG		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN X * RZ	MD * POD* TOD*	TH/TR PW/PO* SW * D2	RED2W RED2D	CF + CO * PI2*	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR		
65060101	4.8855	0.9721	2.0046"+03	1.0300"-03	10.9815	1.5343	3.8015"+03	3.8015"+03		
2.9169"-01	1.7580"+06	1.0000	8.8595"+03	NM	1.7990	1.8386	2.9964"+02	5.8407"+01		
INFINITE	3.3722"+02	0.0000	2.1857"-04	0.0000"+00	0.1969	4.7606"-04	7.4861"+02	3.0823"+02		
65060102	4.9149	0.7105	1.9037"+03	1.2700"-03	9.3021	1.4394	3.6716"+03	3.6716"+03		
2.8743"-01	1.7580"+06	1.0000	6.2204"+03	7.1000"-04	1.8396	1.8147	2.9728"+02	7.8523"+01		
INFINITE	4.5789"+02	0.0000	2.4620"-04	0.0000"+00	0.4208	4.9064"-04	8.7322"+02	4.1843"+02		
65060103	4.9051	0.6585	1.9255"+03	1.3300"-03	8.9661	1.4459	3.7143"+03	3.7143"+03		
2.8743"-01	1.7580"+06	1.0000	5.8127"+03	7.7000"-04	1.8349	1.8078	2.9892"+02	8.5465"+01		
INFINITE	4.9672"+02	0.0000	2.5841"-04	0.0000"+00	0.4658	5.0821"-04	9.0918"+02	4.5395"+02		
65060104	4.8953	0.5951	1.9142"+03	1.4100"-03	8.4156	1.4338	3.7576"+03	3.7576"+03		
2.8743"-01	1.7580"+06	1.0000	5.2137"+03	8.6000"-04	1.8384	1.8142	3.0059"+02	9.5406"+01		
INFINITE	5.5267"+02	0.0000	2.6999"-04	0.0000"+00	0.5345	5.0855"-04	9.5869"+02	5.0511"+02		
65060105	4.8609	0.5228	1.9460"+03	1.4800"-03	7.7394	1.4275	3.9141"+03	3.9141"+03		
2.8743"-01	1.7580"+06	1.0000	4.6194"+03	9.2000"-04	1.8386	1.8157	3.0494"+02	1.1143"+02		
INFINITE	6.3800"+02	0.0000	2.8997"-04	0.0000"+00	0.6135	5.2066"-04	1.0288"+03	5.8324"+02		
65060201	4.9698	0.9442	1.8173"+03	1.0500"-03	11.0895	1.4619	3.4421"+03	3.4421"+03		
2.9688"-01	1.7580"+06	1.0000	7.9657"+03	NM	1.8569	1.8354	3.0845"+02	6.0206"+01		
INFINITE	3.5761"+02	0.0000	2.2334"-04	0.0000"+00	0.1982	4.7265"-04	7.7316"+02	3.2668"+02		
65060202	4.9500	0.7476	1.8554"+03	1.2300"-03	9.7284	1.4784	3.5230"+03	3.5230"+03		
2.9688"-01	1.7580"+06	1.0000	6.3953"+03	6.7000"-04	1.8468	1.8195	3.0897"+02	7.6660"+01		
INFINITE	4.5233"+02	0.0000	2.5273"-04	0.0000"+00	0.3854	5.0467"-04	8.6896"+02	4.1326"+02		
65060203	4.9500	0.6770	1.8100"+03	1.3100"-03	9.2588	1.4837	3.5230"+03	3.5230"+03		
2.9688"-01	1.7580"+06	1.0000	5.6463"+03	7.6000"-04	1.8412	1.8135	3.1158"+02	6.5379"+01		
INFINITE	5.0378"+02	0.0000	2.6187"-04	0.0000"+00	0.4542	5.1392"-04	9.1704"+02	4.6026"+02		
65060204	4.9500	0.6011	1.7606"+03	1.3900"-03	8.6453	1.4473	3.5230"+03	3.5230"+03		
2.9688"-01	1.7580"+06	1.0000	4.8828"+03	8.5000"-04	1.8584	1.8396	3.1446"+02	9.7045"+01		
INFINITE	5.7261"+02	0.0000	2.7347"-04	0.0000"+00	0.5250	4.9802"-04	9.7769"+02	5.2315"+02		
65060205	4.8708	0.5550	1.7094"+03	1.4700"-03	8.0136	1.5017	3.8683"+03	3.8683"+03		
2.9688"-01	1.7580"+06	1.0000	4.2791"+03	9.3000"-04	1.8411	1.8169	3.1609"+02	1.0845"+02		
INFINITE	6.2306"+02	0.0000	2.6082"-04	0.0000"+00	0.5960	4.7006"-04	1.0170"+03	5.6954"+02		
65060301	4.9400	0.9621	2.0588"+03	1.1500"-03	11.1202	1.4578	3.5646"+03	3.5646"+03		
2.9688"-01	1.7580"+06	1.0000	9.1468"+03	NM	1.8292	1.7939	3.0279"+02	5.8572"+01		
INFINITE	3.4444"+02	0.0000	2.3901"-04	0.0000"+00	0.1925	5.4508"-04	7.9802"+02	3.1471"+02		
65060302	4.9894	0.7382	1.9364"+03	1.3500"-03	9.9333	1.4418	3.3641"+03	3.3641"+03		
2.9047"-01	1.7580"+06	1.0000	6.7252"+03	8.0000"-04	1.8290	1.7996	2.9899"+02	7.4169"+01		
INFINITE	4.4344"+02	0.0000	2.6282"-04	0.0000"+00	0.3744	5.5881"-04	8.8153"+02	4.0504"+02		
65060303	4.9400	0.6693	1.8727"+03	1.4400"-03	9.1666	1.4958	3.5646"+03	3.5646"+03		
2.9200"-01	1.7580"+06	1.0000	5.7088"+03	8.6000"-04	1.8259	1.7973	3.0395"+02	8.4523"+01		
INFINITE	4.9706"+02	0.0000	2.6193"-04	0.0000"+00	0.4598	5.3240"-04	9.1059"+02	4.5415"+02		
65060304	4.9400	0.5972	1.8491"+03	1.5500"-03	8.6680	1.4492	3.5646"+03	3.5646"+03		
2.8956"-01	1.7580"+06	1.0000	5.1155"+03	9.3000"-04	1.8267	1.8001	3.0388"+02	9.4697"+01		
INFINITE	5.5689"+02	0.0000	2.7371"-04	0.0000"+00	0.5257	5.3710"-04	9.6384"+02	5.0882"+02		
65060305	4.8412	0.5420	1.8453"+03	1.7000"-03	7.7099	1.4455	4.0069"+03	4.0069"+03		
2.9047"-01	1.7580"+06	1.0000	4.4893"+03	1.0200"-03	1.8345	1.8118	3.1061"+02	1.1020"+02		
INFINITE	6.2678"+02	0.0000	2.7202"-04	0.0000"+00	0.6151	4.9096"-04	1.0190"+03	5.7305"+02		
65060401	4.9748	0.9669	2.5355"+03	1.4900"-03	11.6718	1.4965	3.4220"+03	3.4220"+03		
2.8560"-01	1.7580"+06	1.0000	1.1497"+04	NM	1.7928	1.7504	2.9790"+02	5.6688"+01		
INFINITE	3.3728"+02	0.0000	2.9580"-04	0.0000"+00	0.1722	7.5558"-04	7.5098"+02	3.0810"+02		
65060402	4.9500	0.6964	2.4775"+03	1.7700"-03	9.5421	1.4777	3.5230"+03	3.5230"+03		
2.8560"-01	1.7580"+06	1.0000	8.0002"+03	9.0000"-04	1.7893	1.7563	3.0220"+02	8.0492"+01		
INFINITE	4.7494"+02	0.0000	3.3995"-04	0.0000"+00	0.4319	7.6428"-04	8.8941"+02	4.3392"+02		
65060403	4.9698	0.6550	2.4529"+03	1.8200"-03	9.4091	1.4896	3.4421"+03	3.4421"+03		
2.8560"-01	1.7580"+06	1.0000	7.5049"+03	9.5000"-04	1.7855	1.7504	3.0221"+02	8.5029"+01		
INFINITE	5.0506"+02	0.0000	3.9266"-04	0.0000"+00	0.4612	7.8795"-04	9.1883"+02	4.6137"+02		
65060404	4.9599	0.5948	2.4679"+03	1.9000"-03	8.9464	1.5016	3.4823"+03	3.4823"+03		
2.8560"-01	1.7580"+06	1.0000	6.8468"+03	1.0200"-03	1.7747	1.7445	3.0332"+02	9.4283"+01		
INFINITE	5.5817"+02	0.0000	3.7111"-04	0.0000"+00	0.5200	8.0774"-04	9.6560"+02	5.0992"+02		
65060405	4.9253	0.5409	2.1676"+03	2.0300"-03	8.3595	1.5116	3.6268"+03	3.6268"+03		
2.8560"-01	1.7580"+06	1.0000	5.4138"+03	1.0800"-03	1.7839	1.7503	3.0780"+02	1.0642"+02		
INFINITE	6.2272"+02	0.0000	3.3861"-04	0.0000"+00	0.5829	6.9783"-04	1.0187"+03	5.6903"+02		

PEAK-TO-PEAK ROUGHNESS SPACING SERIES 020 0.127MM, SERIES 030 0.254MM, SERIES 040 0.762MM

65060101		YOUNG		PROFILE TABULATION			16 POINTS, DELTA AT POINT 16		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.88138	0.00000	0.00000	5.08676	0.00000	
2	4.5720 ⁻ -04	4.8612 ⁺ +00	NM	0.94147	0.37686	0.67832	3.23927	0.20940	
3	5.0800 ⁻ -04	5.3355 ⁺ +00	NM	0.94488	0.39698	0.70046	3.11324	0.22499	
4	6.3500 ⁻ -04	6.1735 ⁺ +00	NM	0.95025	0.43015	0.73419	2.91322	0.25202	
5	7.6200 ⁻ -04	6.9949 ⁺ +00	NM	0.95484	0.46030	0.76204	2.74079	0.27804	
6	8.8900 ⁻ -04	7.6928 ⁺ +00	NM	0.95832	0.48442	0.78255	2.60964	0.29987	
7	1.2700 ⁻ -03	9.3618 ⁺ +00	NM	0.96537	0.53769	0.82282	2.34179	0.35136	
8	1.9050 ⁻ -03	1.2061 ⁺ +01	NM	0.97407	0.61407	0.87027	2.00850	0.43329	
9	2.5400 ⁻ -03	1.9121 ⁺ +01	NM	0.98129	0.69045	0.90804	1.72959	0.52500	
10	3.1750 ⁻ -03	1.8634 ⁺ +01	NM	0.98742	0.76884	0.93903	1.49171	0.62950	
11	3.8100 ⁻ -03	2.2474 ⁺ +01	NM	0.99242	0.84623	0.96367	1.29661	0.74311	
12	4.4450 ⁻ -03	2.6171 ⁺ +01	NM	0.99613	0.91457	0.98158	1.15190	0.85214	
13	5.0800 ⁻ -03	2.9073 ⁺ +01	NM	0.99850	0.96482	0.99288	1.05901	0.93756	
14	5.7150 ⁻ -03	3.0582 ⁺ +01	NM	0.99958	0.98993	0.99803	1.01639	0.98194	
15	6.3500 ⁻ -03	3.1073 ⁺ +01	NM	0.99992	0.99799	0.99961	1.00325	0.99637	
D 16	6.9850 ⁻ -03	3.1196 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

65060105		YOUNG		PROFILE TABULATION			18 POINTS, DELTA AT POINT 18		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.47084	0.00000	0.00000	2.69585	0.00000	
2	3.5560 ⁻ -04	5.4333 ⁺ +00	NM	0.78866	0.40303	0.64417	2.55465	0.25216	
3	4.0640 ⁻ -04	5.7330 ⁺ +00	NM	0.79649	0.41515	0.65817	2.51337	0.26187	
4	5.0800 ⁻ -04	6.7702 ⁺ +00	NM	0.82062	0.45455	0.70085	2.37738	0.29480	
5	6.3500 ⁻ -04	7.6927 ⁺ +00	NM	0.83894	0.48687	0.73283	2.26360	0.32346	
6	7.6200 ⁻ -04	8.3641 ⁺ +00	NM	0.85077	0.50909	0.75331	2.18955	0.34805	
7	8.8900 ⁻ -04	8.9360 ⁺ +00	NM	0.86002	0.52727	0.76920	2.12816	0.36144	
8	1.2700 ⁻ -03	1.0245 ⁺ +01	NM	0.87873	0.56667	0.80110	1.99856	0.40084	
9	1.9050 ⁻ -03	1.2831 ⁺ +01	NM	0.90815	0.63737	0.85037	1.78087	0.47762	
10	2.5400 ⁻ -03	1.5810 ⁺ +01	NM	0.93352	0.71010	0.89259	1.58062	0.56492	
11	3.1750 ⁻ -03	1.8920 ⁺ +01	NM	0.95386	0.77879	0.92553	1.41234	0.65531	
12	3.8100 ⁻ -03	2.2317 ⁺ +01	NM	0.97071	0.84747	0.95313	1.26488	0.75353	
13	4.4450 ⁻ -03	2.5441 ⁺ +01	NM	0.98320	0.90606	0.97320	1.15369	0.84355	
14	5.0800 ⁻ -03	2.8068 ⁺ +01	NM	0.99146	0.95253	0.98720	1.07414	0.91907	
15	5.7150 ⁻ -03	2.9551 ⁺ +01	NM	0.99634	0.97778	0.99419	1.03388	0.96164	
16	6.3500 ⁻ -03	3.0155 ⁺ +01	NM	0.99803	0.98788	0.99667	1.01828	0.97897	
17	6.9850 ⁻ -03	3.0888 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 18	7.6200 ⁻ -03	3.0888 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

65060205		YOUNG		PROFILE TABULATION			18 POINTS, DELTA AT POINT 18		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.49517	0.00000	0.00000	2.84473	0.00000	
2	4.5720 ⁻ -04	6.1856 ⁺ +00	NM	0.81503	0.43191	0.68069	2.48377	0.27406	
3	5.0800 ⁻ -04	6.6207 ⁺ +00	NM	0.82444	0.44817	0.69793	2.42511	0.28779	
4	6.3500 ⁻ -04	7.8711 ⁺ +00	NM	0.84816	0.49187	0.74083	2.26848	0.32658	
5	7.6200 ⁻ -04	8.7809 ⁺ +00	NM	0.86289	0.52134	0.76711	2.16505	0.35431	
6	8.8900 ⁻ -04	9.5067 ⁺ +00	NM	0.87340	0.54370	0.78571	2.08839	0.37623	
7	1.2700 ⁻ -03	1.1051 ⁺ +01	NM	0.89283	0.58841	0.81974	1.94082	0.42237	
8	1.9050 ⁻ -03	1.3596 ⁺ +01	NM	0.91830	0.65349	0.86368	1.73612	0.49748	
9	2.5400 ⁻ -03	1.6598 ⁺ +01	NM	0.94111	0.72663	0.90243	1.54244	0.58507	
10	3.1750 ⁻ -03	2.0008 ⁺ +01	NM	0.96078	0.79980	0.93541	1.36787	0.68384	
11	3.8100 ⁻ -03	2.3745 ⁺ +01	NM	0.97728	0.87297	0.96276	1.21629	0.79155	
12	4.4450 ⁻ -03	2.7226 ⁺ +01	NM	0.98937	0.93598	0.98265	1.10221	0.89152	
13	5.0800 ⁻ -03	2.9590 ⁺ +01	NM	0.99613	0.97561	0.99370	1.03742	0.95785	
14	5.7150 ⁻ -03	3.0456 ⁺ +01	NM	0.99857	0.99085	0.99768	1.01382	0.98408	
15	6.3500 ⁻ -03	3.0764 ⁺ +01	NM	0.99937	0.99543	0.99897	1.00611	0.99291	
16	6.9850 ⁻ -03	3.1012 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
17	7.6200 ⁻ -03	3.1012 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 18	8.2550 ⁻ -03	3.1012 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

65060305		YOUNG		PROFILE TABULATION		18 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.49084	0.00000	0.00000	2.73475	0.00000	
2	3.5560 ⁻ 04	5.2962 ⁺ 00	NM	0.78564	0.39898	0.63823	2.55891	0.24942	
3	4.0640 ⁻ 04	5.5684 ⁺ 00	NM	0.79286	0.41020	0.65130	2.52697	0.25835	
4	5.0800 ⁻ 04	6.5410 ⁺ 00	NM	0.81602	0.44796	0.69275	2.39154	0.28967	
5	6.3500 ⁻ 04	7.4349 ⁺ 00	NM	0.83237	0.47653	0.72162	2.29320	0.31468	
6	7.6200 ⁻ 04	7.9326 ⁺ 00	NM	0.84347	0.49694	0.74100	2.22344	0.33327	
7	8.8900 ⁻ 04	8.5556 ⁺ 00	NM	0.85407	0.51735	0.75937	2.15449	0.35246	
8	1.2700 ⁻ 03	1.1044 ⁺ 01	NM	0.88879	0.59184	0.81866	1.91339	0.42786	
9	1.9050 ⁻ 03	1.3142 ⁺ 01	NM	0.91119	0.64796	0.85620	1.74606	0.49036	
10	2.5400 ⁻ 03	1.6131 ⁺ 01	NM	0.93598	0.72041	0.89712	1.55076	0.57850	
11	3.1750 ⁻ 03	1.9535 ⁺ 01	NM	0.95733	0.79490	0.93186	1.37430	0.67806	
12	3.8100 ⁻ 03	2.2902 ⁺ 01	NM	0.97363	0.86224	0.95809	1.23467	0.77599	
13	4.4450 ⁻ 03	2.6600 ⁺ 01	NM	0.98779	0.93061	0.98061	1.11034	0.88316	
14	5.0800 ⁻ 03	2.9423 ⁺ 01	NM	0.99659	0.97959	0.99462	1.03092	0.96479	
15	5.7150 ⁻ 03	3.0457 ⁺ 01	NM	0.99950	0.99694	0.99921	1.00456	0.99467	
D 16	6.3500 ⁻ 03	3.0642 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
17	6.9850 ⁻ 03	3.0642 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	7.6200 ⁻ 03	3.0642 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

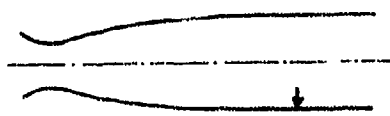
INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

65060401		YOUNG		PROFILE TABULATION		19 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.89043	0.00000	0.00000	5.29783	0.00000	
2	3.5560 ⁻ 04	3.1753 ⁺ 00	NM	0.93380	0.28850	0.57236	3.93434	0.14548	
3	4.0640 ⁻ 04	3.2291 ⁺ 00	NM	0.93432	0.29154	0.57669	3.91260	0.14739	
4	5.0800 ⁻ 04	3.3755 ⁺ 00	NM	0.93572	0.29950	0.58008	3.85545	0.15253	
5	6.3500 ⁻ 04	3.7010 ⁺ 00	NM	0.93865	0.31642	0.61145	3.73416	0.16374	
6	7.6200 ⁻ 04	3.9629 ⁺ 00	NM	0.94085	0.32935	0.62856	3.64222	0.17258	
7	8.8900 ⁻ 04	4.2575 ⁺ 00	NM	0.94317	0.34328	0.64627	3.54427	0.18234	
8	1.2700 ⁻ 03	5.3402 ⁺ 00	NM	0.95062	0.35005	0.70061	3.22633	0.21715	
9	1.9050 ⁻ 03	7.0723 ⁺ 00	NM	0.95988	0.45473	0.76394	2.82237	0.27067	
10	2.5400 ⁻ 03	8.9759 ⁺ 00	NM	0.96757	0.51642	0.81347	2.48133	0.32784	
11	3.1750 ⁻ 03	1.1755 ⁺ 01	NM	0.97584	0.59502	0.86420	2.10938	0.40969	
12	3.8100 ⁻ 03	1.5058 ⁺ 01	NM	0.98286	0.67662	0.90937	1.79047	0.50566	
13	4.4450 ⁻ 03	1.8787 ⁺ 01	NM	0.98856	0.75821	0.93767	1.52948	0.61308	
14	5.0800 ⁻ 03	2.2887 ⁺ 01	NM	0.99314	0.83881	0.96305	1.31819	0.73059	
15	5.7150 ⁻ 03	2.6995 ⁺ 01	NM	0.99660	0.91244	0.98184	1.15791	0.84794	
16	6.3500 ⁻ 03	3.0518 ⁺ 01	NM	0.99896	0.97111	0.99445	1.04857	0.94838	
17	6.9850 ⁻ 03	3.1825 ⁺ 01	NM	0.99972	0.99204	0.99851	1.01308	0.98561	
D 18	7.6200 ⁻ 03	3.2330 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
19	8.2550 ⁻ 03	3.2330 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

65060405		YOUNG		PROFILE TABULATION		18 POINTS, DELTA AT POINT 17			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.49055	0.00000	0.00000	2.87055	0.00000	
2	3.5560 ⁻ 04	3.8406 ⁺ 00	NM	0.75050	0.32663	0.55564	2.69381	0.19201	
3	4.0640 ⁻ 04	4.0458 ⁺ 00	NM	0.75769	0.33668	0.56944	2.64057	0.19907	
4	5.0800 ⁻ 04	4.4316 ⁺ 00	NM	0.77032	0.35477	0.59351	2.79867	0.21207	
5	6.3500 ⁻ 04	4.8155 ⁺ 00	NM	0.78187	0.37186	0.61534	2.73822	0.22472	
6	7.6200 ⁻ 04	5.2912 ⁺ 00	NM	0.79497	0.39196	0.63990	2.66529	0.24009	
7	1.2700 ⁻ 03	7.0436 ⁺ 00	NM	0.83447	0.45829	0.71272	2.41756	0.29469	
8	1.9050 ⁻ 03	9.2394 ⁺ 00	NM	0.87078	0.52965	0.78809	2.15814	0.36053	
9	2.5400 ⁻ 03	1.1869 ⁺ 01	NM	0.90246	0.60402	0.83349	1.98641	0.43747	
10	3.1750 ⁻ 03	1.5016 ⁺ 01	NM	0.93002	0.68241	0.88179	1.66971	0.52811	
11	3.8100 ⁻ 03	1.8595 ⁺ 01	NM	0.95289	0.76181	0.92092	1.46134	0.63019	
12	4.4450 ⁻ 03	2.2253 ⁺ 01	NM	0.97037	0.83518	0.95048	1.29519	0.74386	
13	5.0800 ⁻ 03	2.6134 ⁺ 01	NM	0.98462	0.90653	0.97439	1.15531	0.84340	
14	5.7150 ⁻ 03	2.9723 ⁺ 01	NM	0.99508	0.96784	0.99183	1.05318	0.94443	
15	6.3500 ⁻ 03	3.1137 ⁺ 01	NM	0.99865	0.99095	0.99776	1.01379	0.98419	
16	6.9850 ⁻ 03	3.1636 ⁺ 01	NM	0.99985	0.99899	0.99975	1.00152	0.99824	
D 17	7.6200 ⁻ 03	3.1699 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	8.2550 ⁻ 03	3.1699 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

	M : 2.4, 3.0, 3.4 R THETA $\times 10^{-3}$: 55 TW/TR : 1.0	6601
		ZPG - AW
Continuous wind tunnel with flexible nozzle. W = 2.44 H = 2.13 m L = 10 m. $0.09 < P_0 < 0.15 \text{ MN/m}^2$. $310 < T_0 < 330 \text{ K}$. Air, absolute humidity $< 4 \times 10^{-4}$. $RE/m \times 10^{-6}$: 8.		
HOPKINS E.J. and KEENER E.R. 1966. Study of surface Pitots for measuring skin friction at supersonic Mach numbers - adiabatic wall. NASA TN D 3478. And Hopkins and Keener - private communications. Also Keener and Hopkins (1971)		

- 1 The test-boundary layer was formed on the side-wall of the tunnel (W = 2.44 m) which in the nozzle region is flexible. Observations were made on a single vertical in a central region about 1 m wide.
- 4 The layer was thus formed in a largely simple wave favourable pressure gradient but without strong three-dimensional effects, reaching a near-zero-pressure-gradient in the test-zone. The wall had a hand-rubbed painted surface, finished to 0.8 μm , and was not actively cooled. A free-stream Pitot
- 1 survey showed that the flow was "quite uniform for $M < 3$ but less uniform at $M > 3$ ". There was free transition, the position of which is not known.
- 6 The static pressure was measured at a tapping 0.81 mm in diameter on the test vertical, 241 mm off the centre line, and at three points 152 mm upstream, one ahead of the traverse vertical and the other two ahead of a Pitot rake and a Stanton tube used in the calibration exercise which was the main concern of the source paper. A thermocouple measured the wall temperature. A skin friction balance (developed by NASA Ames Instrument Division) with a floating element 50.8 mm diameter was mounted on the centre line. This was calibrated directly over a range of working temperature. A buoyancy force correction was applied following the techniques of Smith and Walker (1959). Two forms of Stanton tube and six sizes of Preston tube were mounted at varying distances from the centre line.
- 7 The velocity profile was measured by Pitot tubes at two stations. At one, 175 mm off the centre line, a traversing FPP ($h_1 = 0.33$, $h_2 = 0.23$, $b_1 = 2.0$, $l = 6.35 \text{ mm}$) was employed, while at the other, 356 mm off, a rake was employed with 12 CPP ($d_1 = 1.07$, $l = 10.4 \text{ mm}$) at vertical intervals increasing from 2.5 to 38 mm. Values from the traversing FPP are presented here.
- 12 The authors reduced the profile data assuming constant total temperature. The editors have replaced this with the Crocco / van Driest temperature velocity correlation for an adiabatic wall and the assumed constant static pressure. The source paper provides a wide range of Preston and Stanton tube calibration data not presented here. The profiles obtained with the rake are presented graphically in Keener & Hopkins (1971), and compared with those given here.
- 13 The three profiles presented (Hopkins & Keener, PC) are for three Mach numbers at a near common momentum thickness Reynolds number.
- 14 The CF values are the author's values measured with the balance.
- 5 DATA 6601 0101 - 0301. PT2 profiles. NX = 1. CF from FEB.
- 15 Editors' comments
The special value of this investigation lies in the comparisons, made in the source paper, between the three different methods used to measure wall shear stress. The only comparable exercise with this geometry is that of Fenter & Stalmach (1957), based on the profiles measured by Stalmach (CAT 5802), at lower Reynolds numbers than here. With a slightly different geometry, similar Mach number and Reynolds number ranges are covered by Winter & Gaudet (CAT 7302) and Allen (CAT 7303).

The profiles presented include data as far in as the momentum deficit peak.

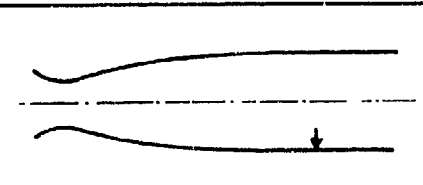
CAT 6601 HOPKINS BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUN	MD *	TN/TR	RED2W	CF *	H12	H12K	PW	PD*
X	PO5	PW/PD*	RED2D	CO	H32	H32K	TN*	TD*
RZ	TUD	SN *	D2	PI2*	H42	D2K	UD	TR
66010101	2.4450	0.9955	3.4192 ⁺⁰⁴	1.2600 ⁻⁰³	3.5699	1.2349	5.6930 ⁺⁰³	5.6930 ⁺⁰³
NM	8.9285 ⁺⁰⁴	1.0000	6.2758 ⁺⁰⁴	NM	1.8424	1.8307	2.9556 ⁺⁰²	1.4333 ⁺⁰²
INFINITE	3.1470 ⁺⁰²	0.0000	7.7104 ⁻⁰³	0.0000 ⁺⁰⁰	0.1086	1.0024 ⁻⁰²	5.8690 ⁺⁰²	2.9688 ⁺⁰²
66010201	2.9610	0.9678	2.6906 ⁺⁰⁴	1.1100 ⁻⁰³	4.5693	1.2334	3.4665 ⁺⁰³	3.4665 ⁺⁰³
NM	1.2009 ⁺⁰⁵	1.0000	5.8747 ⁺⁰⁴	NM	1.8460	1.8312	2.9444 ⁺⁰²	1.1833 ⁺⁰²
INFINITE	3.2583 ⁺⁰²	0.0000	7.4542 ⁻⁰³	0.0000 ⁺⁰⁰	0.1524	1.0587 ⁻⁰²	6.4581 ⁺⁰²	3.0425 ⁺⁰²
66010301	3.4430	0.9712	2.1745 ⁺⁰⁴	9.1000 ⁻⁰⁴	5.7658	1.2356	2.1738 ⁺⁰³	2.1738 ⁺⁰³
NM	1.5286 ⁺⁰⁵	1.0000	5.7318 ⁺⁰⁴	NM	1.8491	1.8300	2.9500 ⁺⁰²	9.7222 ⁺⁰¹
INFINITE	3.2772 ⁺⁰²	0.0000	7.4999 ⁻⁰³	0.0000 ⁺⁰⁰	0.1620	1.1702 ⁻⁰²	6.8066 ⁺⁰²	3.0375 ⁺⁰²

66010101 HOPKINS PROFILE TABULATION 28 POINTS, DELTA AT POINT 22

I	Y	PT3/P	F/PD	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.93916	0.00000	0.00000	2.06202	0.00000
2	4.0640 ⁻⁰⁴	1.4014 ⁺⁰⁰	NM	0.95816	0.41057	0.54326	1.75087	0.31028
3	6.6040 ⁻⁰⁴	2.0298 ⁺⁰⁰	NM	0.95984	0.43310	0.56823	1.72137	0.33010
4	9.1440 ⁻⁰⁴	2.1496 ⁺⁰⁰	NM	0.96130	0.45254	0.58926	1.69550	0.34754
5	1.1684 ⁻⁰³	2.2547 ⁺⁰⁰	NM	0.96253	0.46864	0.60631	1.67381	0.36223
6	1.4224 ⁻⁰³	2.2870 ⁺⁰⁰	NM	0.96290	0.47345	0.61133	1.66731	0.36666
7	1.9304 ⁻⁰³	2.4078 ⁺⁰⁰	NM	0.96509	0.50193	0.64052	1.62844	0.39333
8	2.4384 ⁻⁰³	2.5933 ⁺⁰⁰	NM	0.96618	0.51610	0.65464	1.60897	0.40687
9	4.9784 ⁻⁰³	3.0386 ⁺⁰⁰	NM	0.97047	0.57135	0.70732	1.53260	0.46151
10	7.5134 ⁻⁰³	3.3495 ⁺⁰⁰	NM	0.97319	0.60655	0.73889	1.48398	0.49791
11	1.0058 ⁻⁰²	3.5479 ⁺⁰⁰	NM	0.97482	0.62788	0.75728	1.45467	0.52059
12	1.2598 ⁻⁰²	3.7608 ⁺⁰⁰	NM	0.97650	0.64993	0.77572	1.42456	0.54453
13	2.5298 ⁻⁰²	4.4707 ⁺⁰⁰	NM	0.98159	0.71825	0.82426	1.33300	0.62210
14	3.7998 ⁻⁰²	5.1332 ⁺⁰⁰	NM	0.98576	0.77637	0.87073	1.25786	0.69223
15	5.0698 ⁻⁰²	5.6727 ⁺⁰⁰	NM	0.98881	0.82057	0.89992	1.20276	0.74821
16	6.3398 ⁻⁰²	6.3120 ⁺⁰⁰	NM	0.99209	0.86997	0.93030	1.14349	0.81356
17	7.6098 ⁻⁰²	6.8360 ⁺⁰⁰	NM	0.99453	0.90842	0.95239	1.09914	0.86640
18	8.8798 ⁻⁰²	7.3331 ⁺⁰⁰	NM	0.99668	0.94342	0.97139	1.06016	0.91626
19	1.0150 ⁻⁰¹	7.7546 ⁺⁰⁰	NM	0.99839	0.97210	0.98621	1.02922	0.95820
20	1.1420 ⁻⁰¹	7.9781 ⁺⁰⁰	NM	0.99925	0.98697	0.99363	1.01355	0.98035
21	1.2690 ⁻⁰¹	8.1098 ⁺⁰⁰	NM	0.99975	0.99562	0.99788	1.00453	0.99333
D 22	1.3960 ⁻⁰¹	8.1769 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000
23	1.5230 ⁻⁰¹	8.2107 ⁺⁰⁰	NM	1.00012	1.00220	1.00106	0.99773	1.00334
24	1.6500 ⁻⁰¹	8.2107 ⁺⁰⁰	NM	1.00012	1.00220	1.00106	0.99773	1.00334
25	1.7770 ⁻⁰¹	8.1769 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000
26	1.9040 ⁻⁰¹	8.1769 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000
27	2.1580 ⁻⁰¹	8.1769 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000
28	2.4120 ⁻⁰¹	8.1769 ⁺⁰⁰	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD AND VAN DRIEST

	M : 2.4, 3.0, 3.4 R THETA x 10 ⁻³ : 55 TW/TR : 1.0	6601
		ZPG - AW
Continuous wind tunnel with flexible nozzle. W = 2.44 H = 2.13 m L = 10 m. 0.09 < P ₀ < 0.15 MN/m ² . 310 < T ₀ < 330 K. Air, absolute humidity < 4 x 10 ⁻⁴ . RE/m x 10 ⁻⁶ : 8.		
HOPKINS E.J. and KEENER E.R. 1966. Study of surface Pitots for measuring skin friction at supersonic Mach numbers - adiabatic wall. NASA TN D 3478. <u>And Hopkins and Keener - private communications. Also Keener and Hopkins (1971)</u>		

- 1 The test-boundary layer was formed on the side-wall of the tunnel (W = 2.44 m) which in the nozzle region is flexible. Observations were made on a single vertical in a central region about 1 m wide.
- 4 The layer was thus formed in a largely simple wave favourable pressure gradient but without strong three-dimensional effects, reaching a near-zero-pressure-gradient in the test-zone. The wall had a hand-rubbed painted surface, finished to 0.8 μm, and was not actively cooled. A free-stream Pitot survey showed that the flow was "quite uniform for M < 3 but less uniform at M > 3". There was free transition, the position of which is not known.
- 6 The static pressure was measured at a tapping 0.81 mm in diameter on the test vertical, 241 mm off the centre line, and at three points 152 mm upstream, one ahead of the traverse vertical and the other two ahead of a Pitot rake and a Stanton tube used in the calibration exercise which was the main concern of the source paper. A thermocouple measured the wall temperature. A skin friction balance (developed by NASA Ames Instrument Division) with a floating element 50.8 mm diameter was mounted on the centre line. This was calibrated directly over a range of working temperature. A buoyancy force correction was applied following the techniques of Smith and Walker (1959). Two forms of Stanton tube and six sizes of Preston tube were mounted at varying distances from the centre line.
- 7 The velocity profile was measured by Pitot tubes at two stations. At one, 175 mm off the centre line, a traversing FPP (h₁ = 0.33, h₂ = 0.23, b₁ = 2.0, l = 6.35 mm) was employed, while at the other, 356 mm off, a rake was employed with 12 CPP (d₁ = 1.07, l = 10.4 mm) at vertical intervals increasing from 2.5 to 38 mm. Values from the traversing FPP are presented here.
- 12 The authors reduced the profile data assuming constant total temperature. The editors have replaced this with the Crocco / van Driest temperature velocity correlation for an adiabatic wall and the assumed constant static pressure. The source paper provides a wide range of Preston and Stanton tube calibration data not presented here. The profiles obtained with the rake are presented graphically in Keener & Hopkins (1971), and compared with those given here.
- 13 The three profiles presented (Hopkins & Keener, PC) are for three Mach numbers at a near common momentum thickness Reynolds number.
- 14 The CF values are the author's values measured with the balance.
- § DATA 6601 0101 - 0301. PT2 profiles. NX = 1. CF from FEB.
- 15 Editors' comments
The special value of this investigation lies in the comparisons, made in the source paper, between the three different methods used to measure wall shear stress. The only comparable exercise with this geometry is that of Fenter & Stalmach (1957), based on the profiles measured by Stalmach (CAT 5802), at lower Reynolds numbers than here. With a slightly different geometry, similar Mach number and Reynolds number ranges are covered by Winter & Gaudet (CAT 7302) and Allen (CAT 7303).

The profiles presented include data as far in as the momentum deficit peak.

CAT 6601		HOPKINS		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PM	PD*			
X	POD	PH/PO*	RED2D	CO	H32	H32K	TW*	TD*			
RZ	TOD	SH *	D2	P12*	H42	D2K	UD	TR			
66010101	2.4450	0.9955	3.4192 ⁺ +04	1.2600 ⁻ -03	3.5699	1.2349	5.6930 ⁺ +03	5.6930 ⁺ +03			
NM	8.9285 ⁺ +04	1.0000	6.2758 ⁺ +04	NM	1.8424	1.8307	2.9556 ⁺ +02	1.4333 ⁺ +02			
INFINITE	3.1470 ⁺ +02	0.0000	7.7104 ⁻ -03	0.0000 ⁺ +00	0.1086	1.0024 ⁻ -02	5.8690 ⁺ +02	2.9688 ⁺ +02			
66010201	2.9610	0.9678	2.6906 ⁺ +04	1.1100 ⁻ -03	4.5693	1.2334	3.4665 ⁺ +03	3.4665 ⁺ +03			
NM	1.2009 ⁺ +05	1.0000	5.8747 ⁺ +04	NM	1.8460	1.8312	2.9444 ⁺ +02	1.1833 ⁺ +02			
INFINITE	3.2583 ⁺ +02	0.0000	7.4542 ⁻ -03	0.0000 ⁺ +00	0.1524	1.0587 ⁻ -02	6.4581 ⁺ +02	3.0425 ⁺ +02			
66010301	3.4430	0.9712	2.1745 ⁺ +04	9.1000 ⁻ -04	5.7658	1.2356	2.1738 ⁺ +03	2.1738 ⁺ +03			
NM	1.5206 ⁺ +05	1.0000	5.7316 ⁺ +04	NM	1.8491	1.8300	2.9500 ⁺ +02	9.7222 ⁺ +01			
INFINITE	3.2772 ⁺ +02	0.0000	7.4999 ⁻ -03	0.0000 ⁺ +00	0.1620	1.1702 ⁻ -02	6.8066 ⁺ +02	3.0375 ⁺ +02			

66010101		HOPKINS		PROFILE TABULATION							
				28 POINTS, DELTA AT POINT 22							
1	Y	PT2/P	P/PD	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD			
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93916	0.00000	0.00000	2.06202	0.00000			
2	4.0640 ⁻ -04	1.9014 ⁺ +00	NM	0.95816	0.41057	0.54326	1.75087	0.31028			
3	6.6040 ⁻ -04	2.0298 ⁺ +00	NM	0.95984	0.43310	0.56823	1.72137	0.33010			
4	9.1440 ⁻ -04	2.1496 ⁺ +00	NM	0.96130	0.45254	0.58926	1.69550	0.34754			
5	1.1684 ⁻ -03	2.2547 ⁺ +00	NM	0.96253	0.46864	0.60631	1.67381	0.36223			
6	1.4224 ⁻ -03	2.2870 ⁺ +00	NM	0.96290	0.47345	0.61133	1.66731	0.36666			
7	1.4304 ⁻ -03	2.4678 ⁺ +00	NM	0.96509	0.50193	0.64052	1.62844	0.39333			
8	2.4384 ⁻ -03	2.5933 ⁺ +00	NM	0.96618	0.51610	0.65464	1.60897	0.40687			
9	4.9784 ⁻ -03	3.0386 ⁺ +00	NM	0.97047	0.57135	0.70732	1.53260	0.46151			
10	7.5184 ⁻ -03	3.3495 ⁺ +00	NM	0.97319	0.60655	0.73889	1.48398	0.49791			
11	1.0058 ⁻ -02	3.5479 ⁺ +00	NM	0.97482	0.62788	0.75728	1.45467	0.52059			
12	1.2598 ⁻ -02	3.7608 ⁺ +00	NM	0.97650	0.64993	0.77572	1.42456	0.54453			
13	2.5298 ⁻ -02	4.4707 ⁺ +00	NM	0.98159	0.71825	0.82926	1.33300	0.62210			
14	3.7998 ⁻ -02	5.1332 ⁺ +00	NM	0.98576	0.77637	0.87073	1.25786	0.69223			
15	5.0698 ⁻ -02	5.6727 ⁺ +00	NM	0.98881	0.82057	0.89992	1.20276	0.74821			
16	6.3398 ⁻ -02	6.3120 ⁺ +00	NM	0.99209	0.86997	0.93030	1.14349	0.81356			
17	7.6098 ⁻ -02	6.8360 ⁺ +00	NM	0.99453	0.90842	0.95239	1.09914	0.86448			
18	8.8798 ⁻ -02	7.3331 ⁺ +00	NM	0.99668	0.94342	0.97139	1.06016	0.91626			
19	1.0150 ⁻ -01	7.7546 ⁺ +00	NM	0.99839	0.97210	0.98621	1.02922	0.95820			
20	1.1420 ⁻ -01	7.9781 ⁺ +00	NM	0.99925	0.98697	0.99363	1.01355	0.98035			
21	1.2690 ⁻ -01	8.1098 ⁺ +00	NM	0.99975	0.99562	0.99788	1.00453	0.99338			
D 22	1.3960 ⁻ -01	8.1769 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000			
23	1.5230 ⁻ -01	8.2107 ⁺ +00	NM	1.00012	1.00220	1.00106	0.99773	1.00334			
24	1.6500 ⁻ -01	8.2107 ⁺ +00	NM	1.00012	1.00220	1.00106	0.99773	1.00334			
25	1.7770 ⁻ -01	8.1769 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000			
26	1.9040 ⁻ -01	8.1769 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000			
27	2.1580 ⁻ -01	8.1769 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000			
28	2.4120 ⁻ -01	8.1769 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000			


INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD AND VAN DRIEST

66010201		HOPKINS		PROFILE TABULATION		28 POINTS, DELTA AT POINT 22			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.90367	0.00000	0.00000	2.48826	0.00000	
2	4.0640-04	2.1772+00	NM	0.93952	0.37724	0.54240	2.07034	0.26218	
3	6.6400-04	2.3292+00	NM	0.94180	0.39604	0.56441	2.03386	0.27770	
4	9.1440-04	2.5044+00	NM	0.94426	0.41633	0.54790	1.94397	0.29484	
5	1.1684-03	2.5944+00	NM	0.94546	0.42629	0.54897	1.97424	0.30339	
6	1.4224-03	2.6799+00	NM	0.94657	0.43548	0.60905	1.95594	0.31138	
7	1.9304-03	2.8610+00	NM	0.94907	0.45625	0.63128	1.91446	0.32974	
8	2.4884-03	3.0391+00	NM	0.95093	0.47184	0.64750	1.88321	0.34383	
9	4.9784-03	3.6836+00	NM	0.95776	0.53014	0.70463	1.76658	0.39887	
10	7.5184-03	4.0830+00	NM	0.96150	0.56302	0.73444	1.70165	0.43160	
11	1.0058-02	4.4059+00	NM	0.96430	0.58817	0.75613	1.65266	0.45752	
12	1.2578-02	4.6561+00	NM	0.96634	0.60692	0.77167	1.61663	0.47733	
13	2.5278-02	4.6757+00	NM	0.97371	0.67777	0.82592	1.48496	0.55619	
14	3.7998-02	6.5565+00	NM	0.97909	0.73335	0.86383	1.38748	0.62259	
15	5.0698-02	7.4350+00	NM	0.98376	0.78487	0.89564	1.30218	0.67870	
16	6.3398-02	8.2609+00	NM	0.98761	0.83024	0.92124	1.23122	0.74823	
17	7.6098-02	9.0503+00	NM	0.99090	0.87143	0.94268	1.17020	0.80557	
18	8.8798-02	9.9050+00	NM	0.99410	0.91392	0.96315	1.11062	0.86722	
19	1.0150-01	1.0720+01	NM	0.99685	0.95265	0.98045	1.05921	0.92565	
20	1.1420-01	1.1223+01	NM	0.99842	0.97579	0.99021	1.02979	0.96157	
21	1.2690-01	1.1639+01	NM	0.99965	0.99452	0.99752	1.00665	0.99123	
D 22	1.3960-01	1.1762+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
23	1.5230-01	1.1762+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
24	1.6500-01	1.1824+01	NM	1.00018	1.00276	1.00109	0.99667	1.00444	
25	1.7770-01	1.1824+01	NM	1.00018	1.00276	1.00109	0.99667	1.00444	
26	1.9040-01	1.1824+01	NM	1.00018	1.00276	1.00109	0.99667	1.00444	
27	2.1580-01	1.1824+01	NM	1.00018	1.00276	1.00109	0.99667	1.00444	
28	2.4120-01	1.1762+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD AND VAN DRIEST

66010301		HOPKINS		PROFILE TABULATION		28 POINTS, DELTA AT POINT 24			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.90015	0.00000	0.00000	3.03429	0.00000	
2	4.0640-04	2.2061+00	NM	0.93370	0.32759	0.51889	2.50902	0.20601	
3	6.6040-04	2.4903+00	NM	0.93759	0.35669	0.55580	2.42809	0.22890	
4	9.1440-04	2.6556+00	NM	0.93967	0.37229	0.57483	2.38408	0.24111	
5	1.1684-03	2.7962+00	NM	0.94136	0.38496	0.54990	2.34815	0.25122	
6	1.4224-03	2.8451+00	NM	0.94193	0.38926	0.59493	2.33594	0.25469	
7	1.9304-03	3.1508+00	NM	0.94532	0.41496	0.62420	2.26278	0.27588	
8	2.4384-03	3.3010+00	NM	0.94689	0.42694	0.63737	2.22868	0.28598	
9	4.9784-03	3.9664+00	NM	0.95318	0.47613	0.68830	2.08984	0.32936	
10	7.5184-03	4.5144+00	NM	0.95772	0.51289	0.72321	1.98830	0.36373	
11	1.0058-02	4.8619+00	NM	0.96035	0.53483	0.74282	1.92980	0.38508	
12	1.2598-02	5.2020+00	NM	0.96275	0.55544	0.76043	1.87435	0.40570	
13	2.5298-02	6.6221+00	NM	0.97138	0.63410	0.82099	1.67635	0.48975	
14	3.7998-02	7.5636+00	NM	0.97609	0.68117	0.85262	1.56674	0.54420	
15	5.0698-02	8.7855+00	NM	0.98132	0.73775	0.88660	1.44425	0.61388	
16	6.3398-02	9.8452+00	NM	0.98521	0.78348	0.91119	1.35258	0.67367	
17	7.6098-02	1.0810+01	NM	0.98833	0.82290	0.93052	1.27867	0.72773	
18	8.8798-02	1.1792+01	NM	0.99117	0.86115	0.94779	1.21134	0.78243	
19	1.0150-01	1.3068+01	NM	0.99442	0.90844	0.96729	1.13575	0.85317	
20	1.1420-01	1.4128+01	NM	0.99681	0.94593	0.98143	1.07648	0.91170	
21	1.2690-01	1.5038+01	NM	0.99868	0.97497	0.99234	1.03171	0.96184	
22	1.3960-01	1.5529+01	NM	0.99962	0.99331	0.99791	1.00909	0.98882	
23	1.5230-01	1.5630+01	NM	0.99991	0.99664	0.99891	1.00455	0.99438	
D 24	1.6500-01	1.5733+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
25	1.7770-01	1.5836+01	NM	1.00019	1.00338	1.00109	0.99544	1.00568	
26	1.9040-01	1.5836+01	NM	1.00019	1.00338	1.00109	0.99544	1.00568	
27	2.1580-01	1.5836+01	NM	1.00019	1.00338	1.00109	0.99544	1.00568	
28	2.4120-01	1.5733+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOENERGETIC)
ASSUME P=PD AND VAN DRIEST

	M : 2.5, 3.5 R THETA X 10 ⁻³ : 14 - 20 TW/TR : 1.0	6602
		ZPG - AW
Blow-down wind tunnel with half block nozzle. Running time 50 seconds. W = 0.114, H = 0.083 m. PO = 0.52, 0.81 MN/m ² . TO : 295 K. Air. RE/m X 10 ⁻⁶ : 50.		
JEROMIN L.O.F., 1966. Compressible turbulent boundary layer with fluid injection. Ph.D. thesis Cambridge. And Jeromin (1968)		

- 1 The test boundary layer was formed on a solid straight wall opposing a block half-nozzle. The test zone extended from X = 0.33 to 0.45 m where X = 0 at the throat. The ten measuring stations were at intervals
- 2 of 12.7 mm on the centre line. The surface was polished and was not actively cooled. The free stream Mach
- 3 number varied by 1 1/2 % over the test zone. From earlier investigations it was known that the boundary
- 4 layer was fully turbulent at the start of the test zone. No specific checks on the two-dimensionality of the layer are reported, but a correction for three-dimensional effects caused a 20 % change in the value of CF derived from a momentum analysis at the higher Mach number.
- 6 Static pressure holes (D = 0.25 mm) were drilled in the surface of the plate, and the wall temperature was
- 7 measured by a thermocouple. The Pitot probe used was a FPP made from 1.068 mm diameter tubing flattened so that h₁ = 0.204 mm. This small diameter tubing, cranked up from the surface, continued inside a long slender support structure of 6.25 mm diameter which was further stiffened by three slender fins. The TTP was an ECP (α = 5°, d₁ = 1.53, d₂ = 1.58, l = 25.4 mm) mounted on a support similar to that of the TPP. An additional, cranked, TPP was constructed to make possible measurements 25.4 mm off the centre line.
- 9 The experimental Pitot and TO readings were recorded continuously on an X - Y plotter, and the tabulated values measured from the trace. In data reduction a Crocco - Van Driest temperature-velocity relationship was used, with recovery factor 0.89, as this was indistinguishable from the experimental temperature data. The static pressure was set equal to that determined from the Pitot probe outside the boundary layer, as that was considered a more accurate measurement than a value obtained from the static tappings. No profile corrections were applied and Sutherland's viscosity law was used.
- 10 The editors have accepted all the authors assumptions and reduction procedures. Only the two sets of
- 13 profiles measured on a solid plate are presented here. The author also gives data for three distributed mass injection rates.
- 5 DATA: 6602 0101-0210. Pitot and TO profiles. NX = 10.
- 16 Editors' comments

This entry is included principally as a reference case for the pressure gradient experiments of Thomas - CAT 7401 who used the same facility and similar instrumentation. No CF measurements were made, but the author gives some values deduced from a momentum balance. These do not give a good fit to the wall law in transformed coordinates. Two other CF values are tabulated, but these are obtained from various correlation schemes, and do not represent data. The profile data do transform reasonably well using CF values from the correlation of Fernholz (1971). The CF value is however slightly high. The profiles 0101-0107 show no or very little log-law region.

The profiles are given in fine detail, with stations at close intervals so that the layer development may be followed in detail.

CAT 6602		JEROMIN		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN	MD *	TW/TR	RED2W	CF	H12	H12K	PW	PD		
X *	POD*	PW/PD*	RED2D	CQ	H32	H32K	TH*	TD		
RZ	TUD*	SM *	D2	PI2*	H42	D2K	UD	TR		
66020101	2.5516	1.0283	7.6517 ⁺ +03	NM	4.1720	1.4197	2.7589 ⁺ +04	2.7589 ⁺ +04		
3.3400 ⁻ -01	5.1073 ⁺ +05	1.0000	1.5147 ⁺ +04	NM	1.7909	1.7707	2.8550 ⁺ +02	1.2814 ⁺ +02		
INFINITE	2.9500 ⁺ +02	0.0000	3.1404 ⁻ -04	0.0000 ⁺ +00	0.0822	4.4888 ⁻ -04	5.7912 ⁺ +02	2.7765 ⁺ +02		
66020102	2.5414	1.0350	8.1041 ⁺ +03	NM	4.1613	1.4116	2.8029 ⁺ +04	2.8029 ⁺ +04		
3.4650 ⁻ -01	5.1073 ⁺ +05	1.0000	1.6083 ⁺ +04	NM	1.7907	1.7706	2.8450 ⁺ +02	1.2741 ⁺ +02		
INFINITE	2.9200 ⁺ +02	0.0000	3.2687 ⁻ -04	0.0000 ⁺ +00	0.0744	4.6748 ⁻ -04	5.7516 ⁺ +02	2.7488 ⁺ +02		
66020103	2.5503	1.0280	8.2762 ⁺ +03	NM	4.1599	1.4115	2.7645 ⁺ +04	2.7645 ⁺ +04		
3.5950 ⁻ -01	5.1073 ⁺ +05	1.0000	1.6388 ⁺ +04	NM	1.7925	1.7726	2.8350 ⁺ +02	1.2735 ⁺ +02		
INFINITE	2.9300 ⁺ +02	0.0000	3.3626 ⁻ -04	0.0000 ⁺ +00	0.0808	4.7980 ⁻ -04	5.7703 ⁺ +02	2.7577 ⁺ +02		
66020104	2.5520	1.0195	8.4726 ⁺ +03	NM	4.1228	1.4012	2.7577 ⁺ +04	2.7577 ⁺ +04		
3.7200 ⁻ -01	5.1083 ⁺ +05	1.0000	1.6651 ⁺ +04	NM	1.7930	1.7736	2.8450 ⁺ +02	1.2877 ⁺ +02		
INFINITE	2.9650 ⁺ +02	0.0000	3.4773 ⁻ -04	0.0000 ⁺ +00	0.0894	4.9465 ⁻ -04	5.8063 ⁺ +02	2.7906 ⁺ +02		
66020105	2.5537	1.0336	8.5647 ⁺ +03	NM	4.1574	1.3968	2.7505 ⁺ +04	2.7505 ⁺ +04		
3.8450 ⁻ -01	5.1083 ⁺ +05	1.0000	1.7046 ⁺ +04	NM	1.7954	1.7767	2.8600 ⁺ +02	1.2759 ⁺ +02		
INFINITE	2.9400 ⁺ +02	0.0000	3.5202 ⁻ -04	0.0000 ⁺ +00	0.0764	5.0198 ⁻ -04	5.7834 ⁺ +02	2.7669 ⁺ +02		
66020106	2.5571	1.0287	8.9385 ⁺ +03	NM	4.1446	1.3985	2.7365 ⁺ +04	2.7365 ⁺ +04		
3.9750 ⁻ -01	5.1093 ⁺ +05	1.0000	1.7689 ⁺ +04	NM	1.7950	1.7759	2.8400 ⁺ +02	1.2761 ⁺ +02		
INFINITE	2.9450 ⁺ +02	0.0000	3.6679 ⁻ -04	0.0000 ⁺ +00	0.0840	5.2220 ⁻ -04	5.7917 ⁺ +02	2.7714 ⁺ +02		
66020107	2.5600	1.0231	9.1631 ⁺ +03	NM	4.1273	1.3892	2.7208 ⁺ +04	2.7208 ⁺ +04		
4.0300 ⁻ -01	5.1093 ⁺ +05	1.0000	1.8133 ⁺ +04	NM	1.7947	1.7797	2.8400 ⁺ +02	1.2762 ⁺ +02		
INFINITE	2.9500 ⁺ +02	0.0000	3.7763 ⁻ -04	0.0000 ⁺ +00	0.0867	5.3515 ⁻ -04	5.8002 ⁺ +02	2.7759 ⁺ +02		
66020108	2.5644	1.0215	9.0477 ⁺ +03	NM	4.1098	1.3817	2.7057 ⁺ +04	2.7057 ⁺ +04		
4.2200 ⁻ -01	5.1093 ⁺ +05	1.0000	1.7899 ⁺ +04	NM	1.8028	1.7847	2.8450 ⁺ +02	1.2785 ⁺ +02		
INFINITE	2.9600 ⁺ +02	0.0000	3.7529 ⁻ -04	0.0000 ⁺ +00	0.0904	5.2914 ⁻ -04	5.8136 ⁺ +02	2.7851 ⁺ +02		
66020109	2.5754	1.0358	9.3494 ⁺ +03	NM	4.1914	1.3862	2.6600 ⁺ +04	2.6600 ⁺ +04		
4.3500 ⁻ -01	5.1093 ⁺ +05	1.0000	1.8811 ⁺ +04	NM	1.7987	1.7797	2.8500 ⁺ +02	1.2572 ⁺ +02		
INFINITE	2.9250 ⁺ +02	0.0000	3.9004 ⁻ -04	0.0000 ⁺ +00	0.0747	5.5687 ⁻ -04	5.7898 ⁺ +02	2.7516 ⁺ +02		
66020110	2.5619	1.0320	9.5686 ⁺ +03	NM	4.1345	1.3753	2.7162 ⁺ +04	2.7162 ⁺ +04		
4.4850 ⁻ -01	5.1093 ⁺ +05	1.0000	1.9081 ⁺ +04	NM	1.8022	1.7842	2.8550 ⁺ +02	1.2713 ⁺ +02		
INFINITE	2.9400 ⁺ +02	0.0000	3.9570 ⁻ -04	0.0000 ⁺ +00	0.0773	5.6036 ⁻ -04	5.7915 ⁺ +02	2.7665 ⁺ +02		
66020201	3.6058	1.0485	4.3211 ⁺ +03	NM	7.0109	1.4462	9.1738 ⁺ +03	9.1738 ⁺ +03		
3.3400 ⁻ -01	8.1238 ⁺ +05	1.0000	1.3122 ⁺ +04	NM	1.7920	1.7577	2.8800 ⁺ +02	8.2492 ⁺ +01		
INFINITE	2.9700 ⁺ +02	0.0000	3.0488 ⁻ -04	0.0000 ⁺ +00	0.0930	5.6623 ⁻ -04	6.5862 ⁺ +02	2.7469 ⁺ +02		
66020202	3.6007	1.0501	4.5140 ⁺ +03	NM	6.9470	1.4207	9.2397 ⁺ +03	9.2397 ⁺ +03		
3.4680 ⁻ -01	8.1238 ⁺ +05	1.0000	1.3708 ⁺ +04	NM	1.7949	1.7632	2.8750 ⁺ +02	8.2382 ⁺ +01		
INFINITE	2.9600 ⁺ +02	0.0000	3.1603 ⁻ -04	0.0000 ⁺ +00	0.0926	5.8405 ⁻ -04	6.5526 ⁺ +02	2.7378 ⁺ +02		
66020203	3.5882	1.0428	4.7823 ⁺ +03	NM	6.9132	1.4320	9.4021 ⁺ +03	9.4021 ⁺ +03		
3.5900 ⁻ -01	8.1228 ⁺ +05	1.0000	1.4364 ⁺ +04	NM	1.7910	1.7592	2.8650 ⁺ +02	8.3076 ⁺ +01		
INFINITE	2.9700 ⁺ +02	0.0000	3.3066 ⁻ -04	0.0000 ⁺ +00	0.0980	6.1229 ⁻ -04	6.5573 ⁺ +02	2.7479 ⁺ +02		
66020204	3.5916	1.0627	4.8374 ⁺ +03	NM	6.9700	1.4133	9.3562 ⁺ +03	9.3562 ⁺ +03		
3.7200 ⁻ -01	8.1219 ⁺ +05	1.0000	1.4790 ⁺ +04	NM	1.7942	1.7631	2.8950 ⁺ +02	8.2264 ⁺ +01		
INFINITE	2.9450 ⁺ +02	0.0000	3.3687 ⁻ -04	0.0000 ⁺ +00	0.0793	6.2568 ⁻ -04	6.5314 ⁺ +02	2.7243 ⁺ +02		
66020205	3.5780	1.0515	5.0527 ⁺ +03	NM	6.8731	1.4129	9.5368 ⁺ +03	9.5368 ⁺ +03		
3.8450 ⁻ -01	8.1219 ⁺ +05	1.0000	1.5241 ⁺ +04	NM	1.7949	1.7654	2.8650 ⁺ +02	8.2719 ⁺ +01		
INFINITE	2.9450 ⁺ +02	0.0000	3.4468 ⁻ -04	0.0000 ⁺ +00	0.0909	6.3443 ⁻ -04	6.5244 ⁺ +02	2.7247 ⁺ +02		
66020206	3.5768	1.0461	5.1485 ⁺ +03	NM	6.8481	1.4096	9.5518 ⁺ +03	9.5518 ⁺ +03		
3.9700 ⁻ -01	8.1209 ⁺ +05	1.0000	1.5450 ⁺ +04	NM	1.7931	1.7633	2.8600 ⁺ +02	8.3036 ⁺ +01		
INFINITE	2.9550 ⁺ +02	0.0000	3.5096 ⁻ -04	0.0000 ⁺ +00	0.0952	6.4710 ⁻ -04	6.5349 ⁺ +02	2.7340 ⁺ +02		
66020207	3.5721	1.0424	5.2877 ⁺ +03	NM	6.8207	1.4122	9.6152 ⁺ +03	9.6152 ⁺ +03		
4.1000 ⁻ -01	8.1209 ⁺ +05	1.0000	1.5791 ⁺ +04	NM	1.7948	1.7645	2.8550 ⁺ +02	8.3334 ⁺ +01		
INFINITE	2.9600 ⁺ +02	0.0000	3.5870 ⁻ -04	0.0000 ⁺ +00	0.0978	6.5733 ⁻ -04	6.5380 ⁺ +02	2.7388 ⁺ +02		
66020208	3.5527	1.0405	5.5273 ⁺ +03	NM	6.7751	1.4222	9.8817 ⁺ +03	9.8817 ⁺ +03		
4.2300 ⁻ -01	8.1209 ⁺ +05	1.0000	1.6348 ⁺ +04	NM	1.7929	1.7623	2.8600 ⁺ +02	8.4271 ⁺ +01		
INFINITE	2.9700 ⁺ +02	0.0000	3.6939 ⁻ -04	0.0000 ⁺ +00	0.0993	6.7506 ⁻ -04	6.5390 ⁺ +02	2.7468 ⁺ +02		
66020209	3.5504	1.0369	5.7808 ⁺ +03	NM	6.7557	1.4194	9.9139 ⁺ +03	9.9139 ⁺ +03		
4.3500 ⁻ -01	8.1209 ⁺ +05	1.0000	1.7031 ⁺ +04	NM	1.7912	1.7612	2.8550 ⁺ +02	8.4491 ⁺ +01		
INFINITE	2.9750 ⁺ +02	0.0000	3.8530 ⁻ -04	0.0000 ⁺ +00	0.1023	7.0578 ⁻ -04	6.5432 ⁺ +02	2.7535 ⁺ +02		
66020210	3.5529	1.0405	5.7557 ⁺ +03	NM	6.7511	1.4094	9.8789 ⁺ +03	9.8789 ⁺ +03		
4.4800 ⁻ -01	8.1209 ⁺ +05	1.0000	1.7020 ⁺ +04	NM	1.7941	1.7647	2.8650 ⁺ +02	8.4406 ⁺ +01		
INFINITE	2.9750 ⁺ +02	0.0000	3.8558 ⁻ -04	0.0000 ⁺ +00	0.0995	7.0380 ⁻ -04	6.5446 ⁺ +02	2.7534 ⁺ +02		

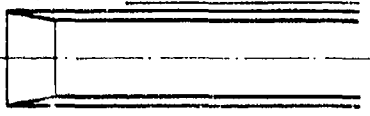
66020106		JEROMIN		PROFILE TABULATION		42 POINTS, DELTA AT POINT 42			
I	Y	PTZ/P	P/PD	T0/T00	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.96464	0.00000	0.00000	2.22614	0.00000	
2	1.1400*-04	1.6524*+00	NM	0.96635	0.34350	0.47745	1.93198	0.24713	
3	1.6500*-04	1.8676*+00	NM	0.96815	0.38654	0.52845	1.86906	0.28273	
4	2.0200*-04	2.0070*+00	NM	0.96921	0.41041	0.55534	1.83295	0.30314	
5	2.7400*-04	2.3237*+00	NM	0.97155	0.45783	0.60734	1.75973	0.34513	
6	3.4700*-04	2.6146*+00	NM	0.97357	0.49616	0.64684	1.69961	0.38058	
7	4.2000*-04	2.8672*+00	NM	0.97514	0.52671	0.67683	1.65130	0.40988	
8	4.9300*-04	3.0195*+00	NM	0.97615	0.54416	0.69343	1.62389	0.42702	
9	5.6600*-04	3.1337*+00	NM	0.97688	0.55684	0.70523	1.60398	0.43967	
10	6.3800*-04	3.2730*+00	NM	0.97770	0.57188	0.71893	1.58037	0.45491	
11	7.8400*-04	3.5002*+00	NM	0.97894	0.59552	0.73983	1.54336	0.47936	
12	9.2900*-04	3.7032*+00	NM	0.98013	0.61580	0.75722	1.51205	0.50079	
13	1.0750*-03	3.8933*+00	NM	0.98121	0.63417	0.77252	1.48395	0.52059	
14	1.2210*-03	4.0443*+00	NM	0.98195	0.64836	0.78402	1.46224	0.53618	
15	1.3660*-03	4.2346*+00	NM	0.98292	0.66579	0.79782	1.43593	0.55561	
16	1.5120*-03	4.4372*+00	NM	0.98394	0.68383	0.81172	1.40992	0.57609	
17	1.6570*-03	4.6149*+00	NM	0.98485	0.69926	0.82332	1.38632	0.59369	
18	1.8030*-03	4.8040*+00	NM	0.98565	0.71528	0.83502	1.36281	0.61272	
19	1.9480*-03	5.0191*+00	NM	0.98667	0.73308	0.84772	1.33720	0.63395	
20	2.0940*-03	5.1969*+00	NM	0.98749	0.74745	0.85771	1.31640	0.65137	
21	2.2390*-03	5.4116*+00	NM	0.98838	0.76444	0.86921	1.29249	0.67230	
22	2.3850*-03	5.5768*+00	NM	0.98912	0.77726	0.87771	1.27518	0.68830	
23	2.5310*-03	5.8037*+00	NM	0.98996	0.79451	0.88881	1.25148	0.71021	
24	2.6760*-03	6.0194*+00	NM	0.99083	0.81056	0.89891	1.22987	0.73090	
25	2.8220*-03	6.2343*+00	NM	0.99164	0.82624	0.90851	1.20996	0.75142	
26	2.9670*-03	6.4375*+00	NM	0.99241	0.84078	0.91721	1.19006	0.77073	
27	3.1130*-03	6.6648*+00	NM	0.99319	0.85676	0.92651	1.16945	0.79226	
28	3.2580*-03	6.8678*+00	NM	0.99396	0.87077	0.93451	1.15175	0.81138	
29	3.4040*-03	7.0829*+00	NM	0.99464	0.88538	0.94261	1.13344	0.83163	
30	3.5500*-03	7.3116*+00	NM	0.99544	0.90064	0.95090	1.11473	0.85303	
31	3.6950*-03	7.5250*+00	NM	0.99603	0.91465	0.95830	1.09773	0.87299	
32	3.8410*-03	7.7157*+00	NM	0.99668	0.92699	0.96470	1.08302	0.89075	
33	3.9860*-03	7.9312*+00	NM	0.99738	0.94074	0.97170	1.06692	0.91076	
34	4.1320*-03	8.1210*+00	NM	0.99787	0.95267	0.97760	1.05302	0.92838	
35	4.2770*-03	8.3358*+00	NM	0.99851	0.96601	0.98410	1.03781	0.94825	
36	4.4230*-03	8.5130*+00	NM	0.99908	0.97687	0.98930	1.02561	0.96460	
37	4.5680*-03	8.6268*+00	NM	0.99925	0.98378	0.99250	1.01781	0.97514	
38	4.7140*-03	8.7294*+00	NM	0.99957	0.98797	0.99540	1.01100	0.98457	
39	4.8600*-03	8.8077*+00	NM	0.99984	0.99467	0.99760	1.00590	0.99175	
40	5.0050*-03	8.8594*+00	NM	0.99995	0.99775	0.99900	1.00250	0.99651	
41	5.1510*-03	8.8853*+00	NM	1.00001	0.99930	0.99970	1.00080	0.99890	
D 42	5.2960*-03	8.8971*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

66020205		JEROMIN		PROFILE TABULATION		43 POINTS, DELTA AT POINT 43			
I	Y	PT2/P	P/PO	10/TOD	M/MD	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.97284	0.00000	0.00000	3.46370	0.00000	
2	1.1400 ⁻ -04	1.6992 ⁺ +00	NM	0.96541	0.25274	0.43440	2.95410	0.14705	
3	2.0200 ⁻ -04	2.3135 ⁺ +00	NM	0.96789	0.32619	0.53680	2.70830	0.19821	
4	2.7400 ⁻ -04	2.7477 ⁺ +00	NM	0.96979	0.36629	0.58720	2.57000	0.22848	
5	3.4700 ⁻ -04	3.0368 ⁺ +00	NM	0.97098	0.39028	0.61550	2.48710	0.24748	
6	4.9300 ⁻ -04	3.5785 ⁺ +00	NM	0.97314	0.43126	0.66070	2.34710	0.28150	
7	6.3800 ⁻ -04	3.9405 ⁺ +00	NM	0.97461	0.45642	0.68660	2.26300	0.30340	
8	7.8400 ⁻ -04	4.2655 ⁺ +00	NM	0.97577	0.47781	0.70750	2.19250	0.32269	
9	9.2900 ⁻ -04	4.5015 ⁺ +00	NM	0.95620	0.48012	0.70250	2.14090	0.32813	
10	1.0750 ⁻ -03	4.8072 ⁺ +00	NM	0.97767	0.51139	0.73840	2.08490	0.35417	
11	1.2210 ⁻ -03	5.0602 ⁺ +00	NM	0.97851	0.52630	0.75140	2.03830	0.36864	
12	1.3660 ⁻ -03	5.3142 ⁺ +00	NM	0.97942	0.54086	0.76370	1.99380	0.38304	
13	1.5120 ⁻ -03	5.5308 ⁺ +00	NM	0.98011	0.55295	0.77360	1.95730	0.39524	
14	1.6570 ⁻ -03	5.8204 ⁺ +00	NM	0.98101	0.56871	0.78610	1.91060	0.41144	
15	1.8030 ⁻ -03	6.1453 ⁺ +00	NM	0.98196	0.58588	0.79920	1.86080	0.42949	
16	1.9480 ⁻ -03	6.4699 ⁺ +00	NM	0.98281	0.60253	0.81140	1.81350	0.44742	
17	2.0940 ⁻ -03	6.7599 ⁺ +00	NM	0.98367	0.61702	0.82170	1.77350	0.46332	
18	2.2390 ⁻ -03	7.1213 ⁺ +00	NM	0.98458	0.63460	0.83370	1.72590	0.48305	
19	2.3850 ⁻ -03	7.4822 ⁺ +00	NM	0.98547	0.65168	0.84490	1.68090	0.50265	
20	2.6030 ⁻ -03	7.9526 ⁺ +00	NM	0.98665	0.67330	0.85850	1.62580	0.52805	
21	2.8220 ⁻ -03	8.4948 ⁺ +00	NM	0.98760	0.69735	0.87240	1.56650	0.55717	
22	3.0400 ⁻ -03	9.1097 ⁺ +00	NM	0.98909	0.72366	0.88760	1.50440	0.59000	
23	3.2580 ⁻ -03	9.6880 ⁺ +00	NM	0.99025	0.74756	0.90030	1.45040	0.62073	
24	3.4040 ⁻ -03	1.0157 ⁺ +01	NM	0.99108	0.76638	0.90980	1.40930	0.64557	
25	3.5500 ⁻ -03	1.0592 ⁺ +01	NM	0.99188	0.78344	0.91810	1.37330	0.66854	
26	3.6950 ⁻ -03	1.1026 ⁺ +01	NM	0.99264	0.80009	0.92590	1.33920	0.69138	
27	3.8410 ⁻ -03	1.1423 ⁺ +01	NM	0.99323	0.81500	0.93260	1.30940	0.71223	
28	3.9860 ⁻ -03	1.1838 ⁺ +01	NM	0.99352	0.82301	0.93610	1.29370	0.72358	
29	4.1320 ⁻ -03	1.2470 ⁺ +01	NM	0.99475	0.85315	0.94880	1.23680	0.76714	
30	4.2770 ⁻ -03	1.2975 ⁺ +01	NM	0.99544	0.87095	0.95590	1.20460	0.79354	
31	4.4230 ⁻ -03	1.3481 ⁺ +01	NM	0.99609	0.88841	0.96260	1.17400	0.81993	
32	4.5680 ⁻ -03	1.3990 ⁺ +01	NM	0.99680	0.90561	0.96900	1.14490	0.84636	
33	4.7140 ⁻ -03	1.4421 ⁺ +01	NM	0.99727	0.91995	0.97410	1.12120	0.86880	
34	4.8600 ⁻ -03	1.4930 ⁺ +01	NM	0.99795	0.93660	0.97990	1.09460	0.89521	
35	5.0050 ⁻ -03	1.5398 ⁺ +01	NM	0.99842	0.95165	0.98490	1.07110	0.91952	
36	5.1510 ⁻ -03	1.5833 ⁺ +01	NM	0.99896	0.96542	0.98940	1.05030	0.94202	
37	5.2960 ⁻ -03	1.6159 ⁺ +01	NM	0.99925	0.97563	0.99260	1.03510	0.95894	
38	5.4420 ⁻ -03	1.6411 ⁺ +01	NM	0.99948	0.98341	0.99500	1.02370	0.97196	
39	5.5870 ⁻ -03	1.6626 ⁺ +01	NM	0.99965	0.99004	0.99700	1.01410	0.98314	
40	5.7330 ⁻ -03	1.6773 ⁺ +01	NM	0.99989	0.99453	0.99840	1.00780	0.99047	
41	5.8790 ⁻ -03	1.6879 ⁺ +01	NM	0.99986	0.99775	0.99930	1.00310	0.99621	
42	6.0240 ⁻ -03	1.6918 ⁺ +01	NM	0.99999	0.99895	0.99970	1.00150	0.99820	
D 43	6.1700 ⁻ -03	1.6952 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD

ASSUME P=PD

	M : 6 R THETA X 10 ⁻³ : 3 - 14 TW/TR : 0.4 - 0.5	6701
		ZPG - SHT
Windtunnel: blow-down but effectively continuous, running time up to 45 minutes with 10 minutes settling time. W = 0.51, H = 0.52 m. PO : 3.6 MN/m ² . TO : 480, 550 K. Air, dewpoint 186 K. RE/m x 10 ⁻⁶ : 33, 29.		
SAMUELS R.D., PETERSON J.B. and ADCOCK J.B. 1967. Experimental investigation of the turbulent boundary layer at a Mach number of 6 with heat transfer at high Reynolds' numbers. NASA TN D-3858. And Adcock, Peterson and McCree (1965) - CAT 6501., Peterson J.B. private communication.		

The test arrangements were generally those for Adcock et al. CAT 6501 and only the differences will be described here.

- 1 The model was actively cooled by passing cold Freon in the gap between the inner ($t = 2.39$ mm) and outer ($t = 3.05$ mm) skins. The variation in TW/TR was obtained mainly as a result of changing the reservoir TO. The wall temperature was effectively independent of X for the TW/TR = 0.44 case, but varied by about 8 % [E]
- 3 for the TW/TR = 0.5 case. Transition was forced.
- 6 Provision was made to measure the heat-flux at X = 305, 610 and 914 mm, using a differential thermocouple
- 7 heat-flow meter of the type described by Beckwith & Gallagher (1957). The total temperature in the boundary layer was measured with a STP for which $d_1 = 0.61$, $d_2 = 0.36$ and $l = 9.5$ mm. The tip was chamfered towards the outside surface at 45°, and contained a chromel-alumel thermocouple 1.1 mm back from the entry. There
- 8 were two vent-holes 0.18 mm in diameter 1.27 mm back. The probe was calibrated as in CAT 6501. Pitot profiles were taken at X = 203, 279, 838, 940 and 1016 mm. TO profiles were taken for all these stations when TW/TR = 0.44, but only for the last three for TW/TR = 0.50.
- 9 The authors have interpolated the TO data to the Y-values of the Pitot data. For those cases (0201,2) for which no TO profile was measured an assumed profile was used based on that observed downstream at the same station for TW/TR = 0.44. The authors found an unexpectedly large "overshoot" in the TO profiles, and in the calculation of their integral data, replaced the measured distribution in the outer part of the layer with an exponential variation without overshoot. Wall data necessary for the reduction of the profiles was adjusted to the appropriate X-value. No TW data is explicitly presented in the source paper, the measurements being absorbed in global average values of TW/TR.
- 12 The editors have presented the profiles using the measured temperature data, with overshoot. They have accepted the notional TO profiles for 0201,2. It has been assumed that there is no normal pressure gradient.
- 13 Sets of profiles, each for 5 successive X values, are given for each of two TW/TR values. The heat transfer
- 16 data in Section D is a global average of up to 12 readings for each X and TW/TR value, prepared from the authors' original data. No attempt has been made to interpolate it to the X values of the profiles.
- 5 DATA: 6701 0101-0204. Pitot and TO profiles, obtained separately. NX = 5. Some heat flux data.
- 15 Editors' comments
The results should be taken in conjunction with the earlier AM case reported by Adcock et al. - CAT 6501. There remains little comparable data, the closest comparisons being Danberg - CAT 6702 and Keener & Hopkins - CAT 7204.

The overshoot of the measured temperature profiles is large enough to cause an apparent associated overshoot in the velocity profiles. This seems improbable, but we have presented the measured values as users are free to insert their own assumptions if they so wish. Leaving aside the overshoot question, there are substantial differences between the measured TO values and the Van Driest correlation. The temperature measurements must clearly be treated with reserve. The innermost TO values (sometimes up to 6) are interpolations.

CAT 6701		SAMUELS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF	H12	H12K	PW	PD			
X *	POD*	PW/PD*	RED2D	CG	H32	H32K	TW*	TD			
RZ *	YOD*	SW *	D2	PI2*	H42	D2K	UD	TR			
67010101	5.9200	0.4867	4.6556 ⁺⁰²	NM	16.4048	1.4250	2.4759 ⁺⁰³	2.4759 ⁺⁰³			
2.0300 ⁻⁰¹	3.6000 ⁺⁰⁶	1.0000	3.1481 ⁺⁰³	NM	1.8265	1.7885	2.1500 ⁺⁰²	6.0680 ⁺⁰¹			
7.6200 ⁻⁰²	4.8600 ⁺⁰²	0.0000	1.0424 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.0440	2.4948 ⁻⁰⁴	9.2460 ⁺⁰²	4.4177 ⁺⁰²			
67010102	5.9400	0.4867	1.7517 ⁺⁰³	NM	14.8045	1.3130	2.4319 ⁺⁰³	2.4319 ⁺⁰³			
2.7900 ⁻⁰¹	3.6100 ⁺⁰⁶	1.0000	5.7452 ⁺⁰³	NM	1.8437	1.8156	2.1500 ⁺⁰²	6.0322 ⁺⁰¹			
7.6200 ⁻⁰²	4.8600 ⁺⁰²	0.0000	1.9130 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1225	4.3928 ⁻⁰⁴	9.2499 ⁺⁰²	4.4173 ⁺⁰²			
67010103	5.9800	0.4848	3.2404 ⁺⁰³	NM	14.4950	1.2994	2.3338 ⁺⁰³	2.3338 ⁺⁰³			
8.3800 ⁻⁰¹	3.6100 ⁺⁰⁶	1.0000	1.0710 ⁺⁰⁴	NM	1.8214	1.7998	2.1500 ⁺⁰²	5.9862 ⁺⁰¹			
7.6200 ⁻⁰²	4.8800 ⁺⁰²	0.0000	3.6489 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0908	8.8912 ⁻⁰⁴	9.2766 ⁺⁰²	4.4347 ⁺⁰²			
67010104	5.9800	0.4898	3.2529 ⁺⁰³	NM	15.3237	1.3565	2.3338 ⁺⁰³	2.3338 ⁺⁰³			
9.4000 ⁻⁰¹	3.6100 ⁺⁰⁶	1.0000	1.0863 ⁺⁰⁴	NM	1.8263	1.7919	2.1500 ⁺⁰²	5.9249 ⁺⁰¹			
7.6200 ⁻⁰²	4.8300 ⁺⁰²	0.0000	3.6442 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0729	8.9571 ⁻⁰⁴	9.2289 ⁺⁰²	4.3893 ⁺⁰²			
67010105	5.9700	0.4888	3.5480 ⁺⁰³	NM	14.8384	1.3019	2.3579 ⁺⁰³	2.3579 ⁺⁰³			
1.0180 ⁺⁰⁰	3.6100 ⁺⁰⁶	1.0000	1.1790 ⁺⁰⁴	NM	1.8264	1.8000	2.1500 ⁺⁰²	5.9546 ⁺⁰¹			
7.6200 ⁻⁰²	4.8400 ⁺⁰²	0.0000	3.9507 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1021	9.5084 ⁻⁰⁴	9.2366 ⁺⁰²	4.3986 ⁺⁰²			
67010201	5.9900	0.4272	9.1304 ⁺⁰²	NM	15.0323	1.4448	2.3100 ⁺⁰³	2.3100 ⁺⁰³			
2.0300 ⁻⁰¹	3.6100 ⁺⁰⁶	1.0000	2.6759 ⁺⁰³	NM	1.8180	1.7882	2.1000 ⁺⁰²	6.6169 ⁺⁰¹			
7.6200 ⁻⁰²	5.4100 ⁺⁰²	0.0000	1.0691 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1361	2.3900 ⁻⁰⁴	9.7693 ⁺⁰²	4.9162 ⁺⁰²			
67010202	5.9800	0.4248	1.3737 ⁺⁰³	NM	13.9348	1.3864	2.3274 ⁺⁰³	2.3274 ⁺⁰³			
2.7900 ⁻⁰¹	3.6000 ⁺⁰⁶	1.0000	3.9918 ⁺⁰³	NM	1.8232	1.7971	2.1000 ⁺⁰²	6.6731 ⁺⁰¹			
7.6200 ⁻⁰²	5.4400 ⁺⁰²	0.0000	1.6059 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2476	3.5719 ⁻⁰⁴	9.7944 ⁺⁰²	4.9436 ⁺⁰²			
67010203	6.0800	0.4345	3.1343 ⁺⁰³	NM	13.9278	1.3246	2.1016 ⁺⁰³	2.1016 ⁺⁰³			
8.3800 ⁻⁰¹	3.5000 ⁺⁰⁶	1.0000	9.5907 ⁺⁰³	NM	1.8332	1.7979	2.1000 ⁺⁰²	6.3364 ⁺⁰¹			
7.6200 ⁻⁰²	5.3200 ⁺⁰²	0.0000	3.8848 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2774	9.1382 ⁻⁰⁴	9.7052 ⁺⁰²	4.8326 ⁺⁰²			
67010204	6.0400	0.4257	3.4933 ⁺⁰³	NM	13.7921	1.3053	2.1949 ⁺⁰³	2.1949 ⁺⁰³			
9.4000 ⁻⁰¹	3.6100 ⁺⁰⁶	1.0000	1.0391 ⁺⁰⁴	NM	1.8241	1.7973	2.1000 ⁺⁰²	6.9451 ⁺⁰¹			
7.6200 ⁻⁰²	5.4300 ⁺⁰²	0.0000	4.2462 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2617	1.0057 ⁻⁰³	9.7972 ⁺⁰²	4.4333 ⁺⁰²			

67010101		SAMUELS		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PD	TU/UD	M/MD	U/UD	1/18	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.44239	0.00000	0.00000	3.54320	0.00000	
2	8.9000 ⁻⁰⁵	3.5866 ⁺⁰⁰	NM	0.62392	0.26100	0.48000	3.33222	0.14192	
3	1.0400 ⁻⁰⁴	3.8223 ⁺⁰⁰	NM	0.63099	0.27100	0.49500	3.33635	0.14837	
4	2.7200 ⁻⁰⁴	7.1369 ⁺⁰⁰	NM	0.82216	0.38400	0.69100	3.23813	0.21340	
5	3.2000 ⁻⁰⁴	9.3726 ⁺⁰⁰	NM	0.85079	0.44400	0.75100	2.86097	0.26250	
6	4.7800 ⁻⁰⁴	1.2768 ⁺⁰¹	NM	0.90532	0.52200	0.82400	2.49160	0.33068	
7	8.9000 ⁻⁰⁴	1.3921 ⁺⁰¹	NM	0.93709	0.54800	0.85100	2.42926	0.35331	
8	8.3200 ⁻⁰⁴	1.8357 ⁺⁰¹	NM	0.98578	0.57400	0.87300	2.31318	0.37941	
9	1.0690 ⁻⁰³	1.6660 ⁺⁰¹	NM	0.96984	0.59900	0.89000	2.20763	0.40315	
10	1.3310 ⁻⁰³	1.9474 ⁺⁰¹	NM	0.98301	0.64900	0.91600	1.99206	0.45983	
11	1.6990 ⁻⁰³	2.2767 ⁺⁰¹	NM	1.00288	0.70300	0.94300	1.79934	0.52408	
12	1.9810 ⁻⁰³	2.5713 ⁺⁰¹	NM	1.01008	0.74800	0.95900	1.64374	0.58342	
13	2.6160 ⁻⁰³	3.2153 ⁺⁰¹	NM	1.02159	0.83800	0.98500	1.38161	0.71294	
14	3.3120 ⁻⁰³	3.9240 ⁺⁰¹	NM	1.02857	0.92700	1.00300	1.17069	0.85676	
15	4.0130 ⁻⁰³	4.3272 ⁺⁰¹	NM	1.01079	0.97400	1.00200	1.05832	0.94678	
16	5.0290 ⁻⁰³	4.4958 ⁺⁰¹	NM	0.99976	0.99300	0.99900	1.01212	0.98704	
17	6.0710 ⁻⁰³	4.5497 ⁺⁰¹	NM	1.00025	0.99900	1.00000	1.00200	0.99800	
0 18	7.1860 ⁻⁰³	4.5587 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD

67010105		SAMUELS		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.44510	0.00000	0.00000	3.61708	0.00000	
2	8.9000-05	2.9671+00	NM	0.53547	0.23054	0.40959	3.15654	0.12976	
3	1.3000-04	3.4640+00	NM	0.58185	0.25349	0.45654	3.24364	0.14075	
4	2.3900-04	4.4243+00	NM	0.69152	0.29242	0.54645	3.49226	0.15648	
5	4.4500-04	7.2575+00	NM	0.80092	0.38423	0.68432	3.17195	0.21574	
6	4.9000-04	7.9405+00	NM	0.81040	0.40319	0.70450	3.05129	0.23082	
7	7.7500-04	8.8119+00	NM	0.83579	0.42615	0.73327	2.96076	0.24766	
8	9.8800-04	9.1264+00	NM	0.84735	0.43413	0.74426	2.93901	0.25323	
9	1.3110-03	9.8555+00	NM	0.86376	0.45210	0.76424	2.85755	0.26744	
10	1.5240-03	1.0443+01	NM	0.87414	0.46607	0.77822	2.78810	0.27912	
11	1.8420-03	1.1181+01	NM	0.88799	0.48303	0.79520	2.71021	0.29341	
12	2.1590-03	1.1991+01	NM	0.89961	0.50100	0.81119	2.62163	0.30942	
13	2.5300-03	1.2784+01	NM	0.91159	0.51796	0.82617	2.54416	0.32473	
14	2.7180-03	1.3652+01	NM	0.92577	0.53593	0.84216	2.46930	0.34105	
15	4.1480-03	1.6759+01	NM	0.95856	0.59541	0.88511	2.20692	0.40106	
16	5.7050-03	2.0924+01	NM	0.98679	0.66766	0.92667	1.92386	0.48136	
17	7.3510-03	2.6313+01	NM	1.01171	0.75050	0.96104	1.63977	0.58608	
18	8.9690-03	3.2256+01	NM	1.02319	0.83234	0.98501	1.40052	0.70332	
19	1.0627-02	3.8982+01	NM	1.02559	0.91617	1.00100	1.19376	0.83853	
20	1.2159-02	4.3913+01	NM	1.01497	0.97305	1.00400	1.06461	0.94307	
21	1.3848-02	4.5714+01	NM	1.00374	0.99301	1.00100	1.01615	0.98509	
D 22	1.5433-02	4.6353+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD

67010201		SAMUELS		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.38895	0.00000	0.00000	3.18003	0.00000	
2	8.9000-05	3.3589+00	NM	0.62519	0.24800	0.46703	3.54632	0.13170	
3	1.0200-04	4.0611+00	NM	0.64532	0.27745	0.51149	3.39874	0.15049	
4	1.4500-04	6.3181+00	NM	0.68351	0.35529	0.60839	2.93226	0.20748	
5	2.5100-04	9.7115+00	NM	0.75784	0.44711	0.71329	2.54512	0.28026	
6	5.2600-04	1.3988+01	NM	0.86949	0.54092	0.81918	2.29349	0.35718	
7	6.7600-04	1.6216+01	NM	0.90212	0.58303	0.85415	2.14036	0.39907	
8	8.0800-04	1.6487+01	NM	0.92695	0.58882	0.86513	2.15873	0.40076	
9	1.2070-03	1.9670+01	NM	0.95582	0.64471	0.90310	1.96218	0.46025	
10	1.8320-03	2.3142+01	NM	0.97897	0.70060	0.93207	1.76993	0.52661	
11	1.9280-03	2.7043+01	NM	1.00281	0.75848	0.95904	1.59876	0.59987	
12	2.6670-03	3.4180+01	NM	1.02037	0.85429	0.98801	1.33756	0.73867	
13	3.4270-03	4.1468+01	NM	1.02770	0.94212	1.00597	1.14020	0.88229	
14	4.0640-03	4.5107+01	NM	1.01835	0.98303	1.00699	1.04934	0.95964	
15	5.0270-03	4.6385+01	NM	0.99874	0.99701	0.99900	1.00401	0.99501	
D 16	6.0550-03	4.6661+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD
AT I=2 DATA WERE AVERAGED

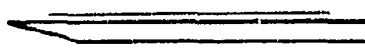
67010204		SAMUELS		PROFILE TABULATION		21 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.38674	0.00000	0.00000	3.20852	0.00000	
2	8.9000-05	2.8630+00	NM	0.48557	0.22278	0.38312	2.95747	0.12954	
3	1.6300-04	3.7765+00	NM	0.59072	0.26374	0.47552	3.25092	0.14627	
4	2.6900-04	5.6572+00	NM	0.72153	0.33167	0.60440	3.32074	0.18201	
5	3.0700-04	6.9608+00	NM	0.74510	0.35964	0.64136	3.18028	0.20167	
6	4.8300-04	7.6847+00	NM	0.79133	0.39161	0.68931	3.08932	0.22248	
7	6.9900-04	8.7477+00	NM	0.81599	0.41958	0.72228	2.96332	0.24374	
8	1.0190-03	9.2240+00	NM	0.83431	0.43157	0.73926	2.93424	0.25194	
9	1.3410-03	9.8011+00	NM	0.84797	0.44555	0.75524	2.87325	0.26285	
10	1.6050-03	1.0481+01	NM	0.85744	0.46154	0.77023	2.78500	0.27656	
11	2.3550-03	1.2099+01	NM	0.88813	0.49750	0.80619	2.62596	0.30701	
12	3.0000-03	1.3739+01	NM	0.90455	0.53147	0.83217	2.45170	0.33943	
13	3.7010-03	1.5435+01	NM	0.92842	0.56444	0.85914	2.31686	0.37082	
14	5.0930-03	1.9311+01	NM	0.96447	0.63337	0.90410	2.03760	0.44371	
15	6.3830-03	2.3371+01	NM	0.98930	0.69830	0.93706	1.80074	0.52038	
16	7.6680-03	2.7820+01	NM	1.00755	0.76324	0.96304	1.59209	0.60489	
17	9.2130-03	3.4016+01	NM	1.02116	0.84515	0.98701	1.36387	0.72369	
18	1.0932-02	4.1183+01	NM	1.01851	0.93107	1.00000	1.19355	0.86689	
19	1.2487-02	4.7946+01	NM	1.00796	0.98402	1.00200	1.03688	0.96636	
D 20	1.4094-02	4.7415+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
21	1.6121-02	4.7154+01	NM	0.99873	0.99700	0.99900	1.00401	0.99501	

INPUT VARIABLES Y,U/UD,M/MD ASSUME P=PD
AT I=2 DATA WERE AVERAGED

6701 SECTION D: ADDITIONAL DATA: HEAT TRANSFER MEASUREMENTS

The data are presented for mean values of the wall temperature in each case. The number of readings given is steadily reduced by eliminating the least characteristic point.

TW/TR (nominal)	X (m)	Number of Readings	CO mean $\times 10^4$	Standard deviation %
0.5	0.305	9	3.77	3.2
(series	"	8	3.80	2.8
01)	0.610	9	3.73	2.3
	"	8	3.76	0.5
	0.914	3	3.03	-
0.44	0.305	12	4.32	5.1
(series	"	11	4.36	3.7
02)	"	10	4.39	3.3
	0.610	12	4.63	6.0
	"	11	4.48	3.8
	"	10	4.45	3.2
	0.914	8	3.81	7.8
		7	3.90	3.2

	M : 6.5 R THETA X 10 ⁻³ : 1.3 - 6 TW/TR : 0.5 - 0.9	6702
		ZPG MHT / SHT
Continuous tunnel with symmetrical nozzle. W = H = 0.25 m. 1.5 < PD < 4 MW/m ² . T ₀ : 550 K. Air, dew point 215 K. B < RE/m X 10 ⁻⁶ < 20.		
DANBERG J.E., 1967. Characteristics of the turbulent boundary layer with heat and mass transfer: Data tabulation NOLTR 67-6. And Danberg (1964); Danberg J.E., private communications.		

- 1 The test boundary layer was formed on a flat plate model 0.59 m long spanning the tunnel and aligned with the plane of symmetry of the nozzle. The leading edge (X = 0), chamfered at 10⁰, had a radius of approximately 0.015 mm and was located approximately in the nozzle exit plane. Tunnel wall boundary layers were compensated for by increasing the working section and the plate widths from 0.254 to 0.272 m over their length. The plate was designed for tests with mass addition, and for X > 50.8 mm, the surface was composed of a sintered steel insert 10.67 mm thick. The roughness was less than 1.8 μm and the surface was flat within ± 0.127 mm. The insert was actively cooled by passing a coolant through 15 passages aligned with
- 2 the long axis of the plate, buried in the under surface of the sintered portion. Static pressure variation
- 3 along the surface of the plate was about ± 4 %. No boundary layer trip was used, a local wall temperature maximum indicating that natural transition occurred at or before X = 0.33 m for all runs. This local temperature rise could not be controlled by the cooling system, and reached its greatest value of about 25 K in the highest unit Reynolds number runs. The detail variation is given graphically in Danberg (1964)
- 5 figure 9. Some off-centre boundary layer surveys were made and these indicated that the flow was symmetrical with nearly constant properties across the region studied.
- 6 Static pressure and wall temperature were measured at 9 successive stations, starting at X = 123.8 mm and then at intervals of 50.8 mm, the static holes (d = 0.635 mm) alternating with temperature stations 5.56 mm on each side of the centre line. Four thermocouples were mounted at each temperature station, one at approximately 1.27 mm below the surface, and three others at intervals of about 2.29 mm, so allowing a determination of the heat transfer rate from the temperature gradient.
- 7 Total temperature profiles were measured with an ECP (Danberg 1961) for which α = 5⁰, d₁ = 1.14 mm, l = 25 mm. Pitot profiles were mostly made with a CPP (d₁ = 0.559, d₂ = 0.264 mm with a 10⁰ bevelled tip) though some data were obtained with an FPP. Static pressure surveys were made using a 1.14 mm probe with the orifices 76.2 mm behind the sharp tip. This probe was affected by aerodynamic loading, and profiles were only presented graphically for their qualitative value. The pressure at the boundary layer edge is close to the wall value though both are higher than the free stream value. The difference was explained as due to the
- 8 displacement effect of the boundary layer itself. Profiles were obtained at four stations for which X = 0.378, 0.49, 0.479 and 0.530 m, thus coinciding with wall static pressure and temperature measurements.
- 9 The author has interpolated the Pitot profile data to the Y-values of the T₀ data. The static pressure was set constant and equal to the wall static pressure. Heat transfer values were obtained from the limiting gradient of the T₀ profiles extrapolated to the wall temperature. This agreed with the values obtained from temperature measurements within the plate to within 20 %, which were considered the less reliable in view of the experimental and constructional difficulties. A skin friction value was estimated from the
- 10 limiting slope of the Mach number profile. No corrections were applied to the profile data and viscosity
- 11 values were taken from Hilsenrath (1955).
- 12 The editors have incorporated the author's calibration and interpolation procedures. The heat transfer data is derived from the Stanton number presented by the author, based on a adiabatic wall recovery factor of
- 13 the one-third power of the wall-state Prandtl number (0.896). The profiles presented, all with zero mass addition, are three series for three different wall temperatures at a single unit Reynolds number and

one for a higher unit RE. There are also six supplementary individual profiles. The wall data consists of heat transfer and shear stress as determined by the author from profile measurements.

5 DATA: 6702 0101-1001. Pitot and TO profiles. NX = 4. Additional single station runs.

15 Editors' comments

The experiment provides data on a transitional boundary layer. The outer part of the layer is perhaps fully turbulent for the highest Reynolds number runs, but despite the relatively high R THETA values, the high Mach number and wall cooling influences are such that the inner regions are not characteristic of fully developed turbulence. The few possible comparison cases of a high Mach number layer developed under constant pressure conditions are Keener & Hopkins - CAT 7204, Samuels et al. - CAT 6701 and the earlier studies of Winkler & Cha - CAT 5902.

The author reports a difference between wall and free stream static pressure of up to 10 % at low values of x, which decreases downstream (Danberg 1964, figure 10). It is difficult to conceive of a mechanism which would cause this, other than a convex curvature of the displacement surface. The necessary radius of curvature is of order 500 δ , and so feasible. Static pressure measurement at high Mach numbers is very difficult (for an extreme case see Beckwith et al. - CAT 7105) so that we have followed the author here in setting the static pressure at the wall value, which is at least accurately measurable.

The wall data, being derived from the limiting gradients of the profiles, should be treated with reserve. The CF value especially should only be regarded as an approximation. The profiles themselves are presented in fair detail. The inner values of TO are interpolations.

CAT 6702		DANBERG		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN X *	MD *	TW/TR PW/POD *	RED2W RED2D	CF * CO *	H12 H32	H12K H32K	PW TW *	PO TO *		
RZ	TOD	SW *	D2	PI2 *	H42	D2K	UD	TR		
67020101	6.6000	0.5082	4.7225 ⁺ +02	1.4580 ⁻ -03	13.3435	1.5610	5.3878 ⁺ +02	5.3878 ⁺ +02		
3.7780 ⁻ -01	1.5381 ⁺ +06	1.0000	1.8892 ⁺ +03	2.2163 ⁻ -04	1.8119	1.7629	2.5234 ⁺ +02	5.6400 ⁺ +01		
INFINITE	5.4776 ⁺ +02	0.0000	2.3093 ⁺ +03	0.0000 ⁺ +00	0.6145	5.2166 ⁺ +04	9.9379 ⁺ +02	4.9666 ⁺ +02		
67020102	6.5500	0.5156	6.0653 ⁺ +02	1.3850 ⁻ -03	12.2585	1.5010	5.6399 ⁺ +02	5.6399 ⁺ +02		
4.2860 ⁻ -01	1.5351 ⁺ +06	1.0000	2.4215 ⁺ +03	2.1830 ⁻ -04	1.8292	1.7819	2.5626 ⁺ +02	5.7200 ⁺ +01		
INFINITE	5.4800 ⁺ +02	0.0000	2.9103 ⁺ +04	0.0000 ⁺ +00	0.6926	6.2026 ⁺ +04	9.9323 ⁺ +02	4.9696 ⁺ +02		
67020103	6.5400	0.5169	6.4516 ⁺ +02	1.4460 ⁻ -03	12.9536	1.5287	5.6942 ⁺ +02	5.6942 ⁺ +02		
4.7940 ⁻ -01	1.5351 ⁺ +06	1.0000	2.5743 ⁺ +03	2.3088 ⁻ -04	1.8313	1.7818	2.5665 ⁺ +02	5.7300 ⁺ +01		
INFINITE	5.4746 ⁺ +02	0.0000	3.0772 ⁺ +04	0.0000 ⁺ +00	0.6347	6.7488 ⁺ +04	9.9258 ⁺ +02	4.9649 ⁺ +02		
67020104	6.4900	0.5251	8.2427 ⁺ +02	1.3360 ⁻ -03	12.5506	1.4792	5.9942 ⁺ +02	5.9942 ⁺ +02		
5.3020 ⁻ -01	1.5401 ⁺ +06	1.0000	3.2892 ⁺ +03	1.8472 ⁻ -04	1.9345	1.7881	2.5997 ⁺ +02	5.7900 ⁺ +01		
INFINITE	5.4565 ⁺ +02	0.0000	3.8222 ⁺ +04	0.0000 ⁺ +00	0.6492	8.2499 ⁺ +04	9.9013 ⁺ +02	4.9492 ⁺ +02		
67020201	6.6300	0.4870	7.7406 ⁺ +02	1.1860 ⁻ -03	14.6362	1.4585	5.5971 ⁺ +02	6.5971 ⁺ +02		
4.7940 ⁻ -01	2.0316 ⁺ +06	1.0000	3.0541 ⁺ +03	2.8647 ⁻ -04	1.8435	1.7983	2.4315 ⁺ +02	5.5500 ⁺ +01		
INFINITE	5.5081 ⁺ +02	0.0000	2.9401 ⁺ +04	0.0000 ⁺ +00	0.5274	6.8907 ⁺ +04	9.9778 ⁺ +02	4.9930 ⁺ +02		
67020301	6.4100	0.4922	1.2178 ⁺ +03	9.4600 ⁻ -04	13.4013	1.4709	1.0632 ⁺ +03	1.0632 ⁺ +03		
4.7940 ⁻ -01	2.5281 ⁺ +06	1.0000	4.4981 ⁺ +03	2.4420 ⁻ -04	1.8359	1.7892	2.4696 ⁺ +02	6.0000 ⁺ +01		
INFINITE	5.5306 ⁺ +02	0.0000	3.1492 ⁺ +04	0.0000 ⁺ +00	0.5472	7.1912 ⁺ +04	9.9551 ⁺ +02	5.0178 ⁺ +02		
67020401	6.4600	0.6428	3.7946 ⁺ +02	1.5600 ⁻ -03	15.5648	1.6212	6.1786 ⁺ +02	6.1786 ⁺ +02		
3.7780 ⁻ -01	1.5422 ⁺ +06	1.0000	1.7544 ⁺ +03	2.1937 ⁻ -04	1.8125	1.7390	3.1991 ⁺ +02	5.8700 ⁺ +01		
INFINITE	5.4863 ⁺ +02	0.0000	2.0292 ⁺ +04	0.0000 ⁺ +00	0.4009	5.2369 ⁺ +04	9.9234 ⁺ +02	4.9768 ⁺ +02		
67020402	6.4600	0.6034	4.7416 ⁺ +02	1.1850 ⁻ -03	14.4813	1.7110	6.1908 ⁺ +02	6.1908 ⁺ +02		
4.2860 ⁻ -01	1.5452 ⁺ +06	1.0000	2.0879 ⁺ +03	2.3095 ⁻ -04	1.8287	1.7414	3.0022 ⁺ +02	5.8800 ⁺ +01		
INFINITE	5.4956 ⁺ +02	0.0000	2.4164 ⁺ +04	0.0000 ⁺ +00	0.5224	5.7923 ⁺ +04	9.9319 ⁺ +02	4.9852 ⁺ +02		
67020403	6.6200	0.6463	4.7353 ⁺ +02	1.4740 ⁻ -03	16.7567	1.5758	5.2515 ⁺ +02	5.2515 ⁺ +02		
4.7940 ⁻ -01	1.5280 ⁺ +06	1.0000	2.2785 ⁺ +03	2.1454 ⁻ -04	1.8391	1.7740	3.2043 ⁺ +02	5.6000 ⁺ +01		
INFINITE	5.4683 ⁺ +02	0.0000	2.8431 ⁺ +04	0.0000 ⁺ +00	0.3428	7.1886 ⁺ +04	9.9326 ⁺ +02	4.9578 ⁺ +02		
67020404	6.4500	0.6419	6.3590 ⁺ +02	1.2100 ⁻ -03	14.6140	1.5112	6.1977 ⁺ +02	6.1977 ⁺ +02		
5.3020 ⁻ -01	1.5320 ⁺ +06	1.0000	2.9318 ⁺ +03	1.6829 ⁻ -04	1.8363	1.7838	3.1802 ⁺ +02	5.8600 ⁺ +01		
INFINITE	5.4618 ⁺ +02	0.0000	3.3771 ⁺ +04	0.0000 ⁺ +00	0.4598	8.0905 ⁺ +04	9.8996 ⁺ +02	4.9547 ⁺ +02		
67020501	6.5300	0.6460	3.3223 ⁺ +02	1.6620 ⁻ -03	18.3046	1.8598	5.7111 ⁺ +02	5.7111 ⁺ +02		
3.7780 ⁻ -01	1.5249 ⁺ +06	1.0000	1.5736 ⁺ +03	2.3213 ⁻ -04	1.8171	1.7316	3.1985 ⁺ +02	5.7300 ⁺ +01		
INFINITE	5.4596 ⁺ +02	0.0000	1.8784 ⁺ +04	0.0000 ⁺ +00	0.2307	5.0555 ⁺ +04	9.9106 ⁺ +02	4.9514 ⁺ +02		
67020601	6.3100	0.9360	2.7519 ⁺ +02	1.9540 ⁻ -03	21.0877	1.6757	7.1063 ⁺ +02	7.1063 ⁺ +02		
3.7780 ⁻ -01	1.5320 ⁺ +06	1.0000	1.6036 ⁺ +03	1.6451 ⁻ -04	1.8433	1.7547	4.6674 ⁺ +02	6.1300 ⁺ +01		
INFINITE	5.4945 ⁺ +02	0.0000	1.7624 ⁺ +04	0.0000 ⁺ +00	-0.1588	5.2440 ⁺ +04	9.9053 ⁺ +02	4.9868 ⁺ +02		
67020602	6.4500	0.9201	2.9733 ⁺ +02	1.7700 ⁻ -03	22.2856	1.7344	6.1690 ⁺ +02	6.1690 ⁺ +02		
4.2860 ⁻ -01	1.5249 ⁺ +06	1.0000	1.7778 ⁺ +03	2.1297 ⁻ -04	1.8520	1.7617	4.6058 ⁺ +02	5.9200 ⁺ +01		
INFINITE	5.5177 ⁺ +02	0.0000	2.0892 ⁺ +04	0.0000 ⁺ +00	-0.1929	6.1177 ⁺ +04	9.9502 ⁺ +02	5.0055 ⁺ +02		
67020603	6.6100	0.9151	3.1817 ⁺ +02	1.5740 ⁻ -03	22.4341	1.6337	5.3157 ⁺ +02	5.3157 ⁺ +02		
4.7940 ⁻ -01	1.5320 ⁺ +06	1.0000	1.9828 ⁺ +03	1.7936 ⁻ -04	1.8509	1.7649	4.5571 ⁺ +02	5.6400 ⁺ +01		
INFINITE	5.4925 ⁺ +02	0.0000	2.4528 ⁺ +04	0.0000 ⁺ +00	-0.1438	7.2966 ⁺ +04	9.9529 ⁺ +02	4.9799 ⁺ +02		
67020604	6.6200	0.9056	3.9779 ⁺ +02	1.4500 ⁻ -03	21.1812	1.5576	5.2515 ⁺ +02	5.2515 ⁺ +02		
5.3020 ⁻ -01	1.5280 ⁺ +06	1.0000	2.4683 ⁺ +03	1.7624 ⁻ -04	1.8620	1.7782	4.5061 ⁺ +02	5.6200 ⁺ +01		
INFINITE	5.4879 ⁺ +02	0.0000	3.0696 ⁺ +04	0.0000 ⁺ +00	-0.0468	8.6774 ⁺ +04	9.9503 ⁺ +02	4.9756 ⁺ +02		
67020701	6.4300	0.9282	5.3154 ⁺ +02	1.4560 ⁻ -03	18.5322	1.5036	8.3628 ⁺ +02	8.3628 ⁺ +02		
4.7940 ⁻ -01	2.0275 ⁺ +06	1.0000	3.1871 ⁺ +03	1.5037 ⁻ -04	1.8620	1.7893	4.6128 ⁺ +02	5.9100 ⁺ +01		
INFINITE	5.4780 ⁺ +02	0.0000	2.7643 ⁺ +04	0.0000 ⁺ +00	0.1021	7.5047 ⁺ +04	9.9109 ⁺ +02	4.9697 ⁺ +02		
67020801	6.3400	0.8607	1.0724 ⁺ +03	9.9200 ⁻ -04	17.2894	1.4263	1.7372 ⁺ +03	1.7372 ⁺ +03		
5.3020 ⁻ -01	3.8574 ⁺ +06	1.0000	5.9341 ⁺ +03	1.0496 ⁻ -04	1.8475	1.7878	4.3066 ⁺ +02	6.1000 ⁺ +01		
INFINITE	5.5139 ⁺ +02	0.0000	2.6356 ⁺ +04	0.0000 ⁺ +00	0.1588	7.1559 ⁺ +04	9.9281 ⁺ +02	5.0039 ⁺ +02		
67020901	6.5000	0.5443	9.5628 ⁺ +02	6.2600 ⁻ -04	15.1900	1.3402	1.4869 ⁺ +03	1.4869 ⁺ +03		
4.2860 ⁻ -01	3.8574 ⁺ +06	1.0000	3.9293 ⁺ +03	1.9036 ⁻ -04	1.8717	1.8463	2.7104 ⁺ +02	5.8100 ⁺ +01		
INFINITE	5.4904 ⁺ +02	0.0000	1.8480 ⁺ +04	0.0000 ⁺ +00	0.4163	4.5617 ⁺ +04	9.9337 ⁺ +02	4.9799 ⁺ +02		
67020902	6.4900	0.5539	1.2571 ⁺ +03	6.9700 ⁻ -04	13.8729	1.5022	1.5013 ⁺ +03	1.5013 ⁺ +03		
4.7940 ⁻ -01	3.8574 ⁺ +06	1.0000	5.2164 ⁺ +03	1.8086 ⁻ -04	1.8365	1.7902	2.7747 ⁺ +02	5.8600 ⁺ +01		
INFINITE	5.5223 ⁺ +02	0.0000	2.4652 ⁺ +04	0.0000 ⁺ +00	0.5487	5.8639 ⁺ +04	9.9610 ⁺ +02	5.0091 ⁺ +02		
67020903	6.3700	0.5682	1.0583 ⁺ +03	6.8100 ⁻ -04	13.4771	1.4612	1.6842 ⁺ +03	1.6842 ⁺ +03		
5.3020 ⁻ -01	3.8514 ⁺ +06	1.0000	7.6203 ⁺ +03	1.5672 ⁻ -04	1.8432	1.7887	2.8294 ⁺ +02	6.0200 ⁺ +01		
INFINITE	5.4875 ⁺ +02	0.0000	3.4061 ⁺ +04	0.0000 ⁺ +00	0.5386	7.9617 ⁺ +04	9.9094 ⁺ +02	4.9794 ⁺ +02		
67021001	6.3400	0.5266	1.8695 ⁺ +03	7.7300 ⁻ -04	14.7078	1.4798	1.5976 ⁺ +03	1.5976 ⁺ +03		
5.3020 ⁻ -01	3.8474 ⁺ +06	1.0000	6.3945 ⁺ +03	1.9934 ⁻ -04	1.8279	1.7812	1.6222 ⁺ +02	6.0700 ⁺ +01		
INFINITE	5.4667 ⁺ +02	0.0000	3.0654 ⁺ +04	0.0000 ⁺ +00	0.3987	7.4919 ⁺ +04	9.9036 ⁺ +02	4.9793 ⁺ +02		

67020601		DANBERG		PROFILE TABULATION		21 POINTS, DELTA AT POINT 17			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.84947	0.00000	0.00000	7.61400	0.00000	
2	2.7900-04	1.5651+00	NM	0.88024	0.13094	0.34500	6.94200	0.04970	
3	4.8300-04	2.7712+00	NM	0.91407	0.20884	0.51500	6.08100	0.08469	
4	6.1000-04	3.7873+00	NM	0.93534	0.25287	0.59600	5.55500	0.10729	
5	7.3700-04	5.0996+00	NM	0.95059	0.29973	0.66800	4.96700	0.13449	
6	9.9100-04	8.0290+00	NM	0.97852	0.38373	0.77100	4.03700	0.19098	
7	1.2450-03	1.0480+01	NM	0.99619	0.44177	0.82600	3.49600	0.23627	
8	1.4990-03	1.2424+01	NM	1.00164	0.48284	0.89600	3.14300	0.27235	
9	1.8800-03	1.4732+01	NM	1.00766	0.52744	0.88400	2.80900	0.31470	
10	2.5150-03	1.7744+01	NM	1.00766	0.58050	0.90900	2.45200	0.37072	
11	3.7850-03	2.5516+01	NM	1.00788	0.69902	0.95000	1.84700	0.51435	
12	4.4200-03	3.0426+01	NM	1.00927	0.76448	0.96700	1.60000	0.60437	
13	5.0550-03	3.4923+01	NM	1.00853	0.81985	0.97800	1.42300	0.68728	
14	6.3250-03	4.2907+01	NM	1.00891	0.90990	0.99300	1.19100	0.83375	
15	7.5950-03	4.7873+01	NM	1.00504	0.96166	0.99800	1.07700	0.92665	
16	8.8650-03	5.0674+01	NM	1.00234	0.98966	1.00000	1.02100	0.97943	
D 17	1.0140-02	5.1728+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	1.1410-02	5.1728+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
19	1.3940-02	5.1728+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
20	1.7760-02	5.1728+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
21	2.4100-02	5.1728+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020602		DANBERG		PROFILE TABULATION		27 POINTS, DELTA AT POINT 27			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.83472	0.00000	0.00000	7.76000	0.00000	
2	2.7900-04	1.4660+00	NM	0.87188	0.11782	0.31800	7.28500	0.04365	
3	3.1800-04	1.8072+00	NM	0.87732	0.14880	0.39100	6.90500	0.05663	
4	4.4500-04	2.4228+00	NM	0.89473	0.18686	0.47500	6.46200	0.07351	
5	5.7200-04	3.1302+00	NM	0.90985	0.22061	0.54200	6.03600	0.08979	
6	6.9900-04	4.2534+00	NM	0.92754	0.26498	0.61900	5.45700	0.11343	
7	9.5300-04	7.1525+00	NM	0.96071	0.35286	0.74000	4.39800	0.16826	
8	1.2070-03	9.5493+00	NM	0.98408	0.41155	0.80300	3.80700	0.21093	
9	1.4610-03	1.1525+01	NM	0.99447	0.45421	0.83900	3.41200	0.24590	
10	2.0960-03	1.4688+01	NM	1.00207	0.51519	0.87900	2.91100	0.30196	
11	2.7310-03	1.7208+01	NM	1.00119	0.55902	0.90000	2.59200	0.34722	
12	3.3660-03	2.0035+01	NM	0.99963	0.60439	0.91800	2.30700	0.37792	
13	4.0010-03	2.2895+01	NM	1.00015	0.64707	0.93300	2.07900	0.44877	
14	4.6360-03	2.5856+01	NM	1.00358	0.68848	0.94700	1.89200	0.50053	
15	5.2710-03	2.9411+01	NM	1.00780	0.73511	0.96100	1.70900	0.56232	
16	5.9060-03	3.3094+01	NM	1.00983	0.78048	0.97200	1.55100	0.62669	
17	6.5410-03	3.6818+01	NM	1.01125	0.82382	0.98100	1.41800	0.69182	
18	7.1760-03	4.0439+01	NM	1.01175	0.86388	0.98800	1.30800	0.75535	
19	7.8110-03	4.3773+01	NM	1.01314	0.89919	0.99400	1.22200	0.81342	
20	8.4460-03	4.6523+01	NM	1.01139	0.92729	0.99700	1.15600	0.86246	
21	9.0810-03	4.8929+01	NM	1.00927	0.95171	0.99900	1.10300	0.90571	
22	9.7160-03	5.0618+01	NM	1.00730	0.96764	1.00000	1.06800	0.93633	
23	1.0350-02	5.1869+01	NM	1.00451	0.97964	1.00000	1.04200	0.95969	
24	1.0990-02	5.2722+01	NM	1.00268	0.98773	1.00000	1.02500	0.97561	
25	1.1620-02	5.3446+01	NM	1.00118	0.99454	1.00000	1.01100	0.98912	
26	1.2260-02	5.3762+01	NM	1.00054	0.99751	1.00000	1.00500	0.99502	
D 27	1.2890-02	5.4028+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020603		DANBERG		PROFILE TABULATION		23 POINTS, DELTA AT POINT 21			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.82970	0.00000	0.00000	8.08000	0.00000	
2	2.7900-04	1.4862+00	NM	0.86384	0.11712	0.32100	7.51200	0.04273	
3	3.5600-04	1.8352+00	NM	0.89247	0.14724	0.39800	7.30700	0.05447	
4	4.8300-04	2.1040+00	NM	0.89010	0.16471	0.43600	7.00700	0.06222	
5	6.1000-04	2.9712+00	NM	0.90549	0.20340	0.52700	6.39500	0.08241	
6	7.3700-04	4.0588+00	NM	0.92037	0.25134	0.60400	5.77500	0.10459	
7	8.6400-04	5.1954+00	NM	0.93446	0.28911	0.66300	5.25900	0.12607	
8	1.1180-03	7.7630+00	NM	0.96113	0.35978	0.75400	4.39200	0.17168	
9	1.3720-03	9.9151+00	NM	0.97322	0.40962	0.80300	3.94300	0.20895	
10	1.6260-03	1.1466+01	NM	0.98727	0.44205	0.83300	3.55100	0.23458	
11	2.2610-03	1.4408+01	NM	0.99060	0.49775	0.86900	3.04800	0.28510	
12	2.8960-03	1.6880+01	NM	0.99167	0.54025	0.89100	2.72000	0.32757	
13	4.1660-03	2.1732+01	NM	0.99157	0.61482	0.92100	2.24400	0.41043	
14	5.4360-03	2.7315+01	NM	0.99975	0.69085	0.94800	1.88300	0.50345	
15	6.7060-03	3.3458+01	NM	1.00694	0.76582	0.96900	1.60100	0.60525	
16	7.9760-03	4.0073+01	NM	1.01210	0.83910	0.98500	1.37800	0.71480	
17	9.2460-03	4.6077+01	NM	1.01374	0.90046	0.99500	1.22100	0.81491	
18	1.0520-02	5.0636+01	NM	1.01043	0.94439	0.99900	1.11900	0.89276	
19	1.1790-02	5.3435+01	NM	1.00637	0.97037	1.00000	1.06200	0.94162	
20	1.4330-02	5.6162+01	NM	1.00103	0.99504	1.00000	1.01000	0.99010	
D 21	1.6740-02	5.6717+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
22	1.8140-02	5.6719+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
23	1.9410-02	5.6719+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020604		DANBERG		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.82111	0.00000	0.00000	8.01800	0.00000	
2	2.7900 ⁻⁰⁴	1.4690 ⁺⁰⁰	NM	0.85589	0.11511	0.31500	7.48800	0.04207	
3	4.0600 ⁻⁰⁴	1.8398 ⁺⁰⁰	NM	0.87166	0.14734	0.39400	7.15100	0.05510	
4	5.3300 ⁻⁰⁴	2.1092 ⁺⁰⁰	NM	0.88769	0.16477	0.43600	7.00200	0.06227	
5	6.6000 ⁻⁰⁴	3.2587 ⁺⁰⁰	NM	0.90315	0.22031	0.54800	6.18700	0.08857	
6	7.8700 ⁻⁰⁴	4.2715 ⁺⁰⁰	NM	0.91932	0.25846	0.61500	5.66200	0.10862	
7	1.0410 ⁻⁰³	6.7442 ⁺⁰⁰	NM	0.94649	0.33307	0.72100	4.68600	0.15386	
8	1.6760 ⁻⁰³	1.0924 ⁺⁰¹	NM	0.97538	0.43033	0.82000	3.63100	0.22583	
9	2.3110 ⁻⁰³	1.3594 ⁺⁰¹	NM	0.97578	0.48225	0.85400	3.13600	0.27232	
10	2.9460 ⁻⁰³	1.5631 ⁺⁰¹	NM	0.97679	0.51835	0.87400	2.84300	0.30742	
11	3.5810 ⁻⁰³	1.7803 ⁺⁰¹	NM	0.97942	0.55426	0.89200	2.59000	0.34440	
12	4.2160 ⁻⁰³	2.0105 ⁺⁰¹	NM	0.98264	0.58993	0.90800	2.36900	0.38328	
13	4.8510 ⁻⁰³	2.2262 ⁺⁰¹	NM	0.98626	0.62150	0.92100	2.19600	0.41940	
14	6.1210 ⁻⁰³	2.7057 ⁺⁰¹	NM	0.99353	0.68648	0.94400	1.89100	0.49921	
15	7.3910 ⁻⁰³	3.2435 ⁺⁰¹	NM	1.00626	0.75271	0.96600	1.64700	0.58652	
16	8.6610 ⁻⁰³	3.7863 ⁺⁰¹	NM	1.01044	0.81413	0.98000	1.44900	0.67633	
17	9.9310 ⁻⁰³	4.2984 ⁺⁰¹	NM	1.01088	0.86808	0.98900	1.29800	0.76194	
18	1.1200 ⁻⁰²	4.7368 ⁺⁰¹	NM	1.01061	0.91173	0.99500	1.19100	0.83543	
19	1.2470 ⁻⁰²	5.0486 ⁺⁰¹	NM	1.00502	0.94155	0.99600	1.11900	0.89008	
20	1.3740 ⁻⁰²	5.2646 ⁺⁰¹	NM	1.00430	0.96166	0.99800	1.07700	0.92665	
21	1.7550 ⁻⁰²	5.5456 ⁺⁰¹	NM	1.00066	0.98722	0.99900	1.02400	0.97559	
D 22	2.3900 ⁻⁰²	5.6889 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020901		DANBERG		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.49365	0.00000	0.00000	4.66500	0.00000	
2	3.0400 ⁻⁰⁴	4.3723 ⁺⁰⁰	NM	0.69950	0.26677	0.54200	4.12800	0.13130	
3	4.0600 ⁻⁰⁴	4.3354 ⁺⁰⁰	NM	0.73260	0.26948	0.55300	4.33900	0.12745	
4	4.3100 ⁻⁰⁴	4.8888 ⁺⁰⁰	NM	0.76481	0.28417	0.58900	4.29600	0.13710	
5	4.6200 ⁻⁰⁴	5.9181 ⁺⁰⁰	NM	0.78807	0.31592	0.63500	4.04000	0.15718	
6	6.0900 ⁻⁰⁴	8.6824 ⁺⁰⁰	NM	0.84114	0.38834	0.72600	3.49500	0.20773	
7	7.3600 ⁻⁰⁴	1.0711 ⁺⁰¹	NM	0.86582	0.43379	0.77100	3.15900	0.24406	
8	8.6300 ⁻⁰⁴	1.1642 ⁺⁰¹	NM	0.88643	0.45311	0.79300	3.06300	0.25890	
9	1.1170 ⁻⁰³	1.3164 ⁺⁰¹	NM	0.90401	0.48302	0.81900	2.87500	0.28487	
10	1.3710 ⁻⁰³	1.4694 ⁺⁰¹	NM	0.91868	0.51134	0.84100	2.70500	0.31091	
11	1.6250 ⁻⁰³	1.6242 ⁺⁰¹	NM	0.92694	0.53846	0.85800	2.53900	0.33793	
12	1.8790 ⁻⁰³	1.7990 ⁺⁰¹	NM	0.93614	0.56754	0.87500	2.37700	0.36811	
13	2.1330 ⁻⁰³	1.9912 ⁺⁰¹	NM	0.94490	0.59787	0.89100	2.22100	0.40117	
14	2.6310 ⁻⁰³	2.4139 ⁺⁰¹	NM	0.96265	0.65967	0.92000	1.94500	0.47301	
15	3.1490 ⁻⁰³	2.9065 ⁺⁰¹	NM	0.97620	0.72508	0.94400	1.69500	0.55693	
16	3.7840 ⁻⁰³	3.5354 ⁺⁰¹	NM	0.99452	0.80085	0.96900	1.46400	0.66189	
17	4.4190 ⁻⁰³	4.1659 ⁺⁰¹	NM	0.99906	0.87022	0.98300	1.27600	0.77038	
18	5.0540 ⁻⁰³	4.5892 ⁺⁰¹	NM	1.00260	0.91384	0.99100	1.17600	0.84269	
19	5.6890 ⁻⁰³	5.0001 ⁺⁰¹	NM	0.99830	0.95427	0.99400	1.08500	0.91613	
20	6.3240 ⁻⁰³	5.2153 ⁺⁰¹	NM	0.99752	0.97479	0.99600	1.04400	0.95402	
21	6.9590 ⁻⁰³	5.3562 ⁺⁰¹	NM	0.99854	0.98817	0.99800	1.02000	0.97843	
22	7.5840 ⁻⁰³	5.4269 ⁺⁰¹	NM	0.99916	0.99453	0.99900	1.00900	0.99009	
23	8.2290 ⁻⁰³	5.4591 ⁺⁰¹	NM	1.00053	0.99751	1.00000	1.00500	0.99502	
24	8.8640 ⁻⁰³	5.4645 ⁺⁰¹	NM	1.00042	0.99801	1.00000	1.00400	0.99602	
25	9.4990 ⁻⁰³	5.4753 ⁺⁰¹	NM	1.00021	0.99900	1.00000	1.00200	0.99800	
D 26	1.0770 ⁻⁰²	5.4862 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020902		DANBERG		PROFILE TABULATION		32 POINTS, DELTA AT POINT 31			
I	Y	PT2/P	P/PPD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.50244	0.00000	0.00000	4.73500	0.00000	
2	3.7900-04	4.3219+00	NM	0.71555	0.26541	0.54600	4.23200	0.12902	
3	4.3000-04	5.1384+00	NM	0.73743	0.29265	0.58800	4.03700	0.14565	
4	5.0600-04	6.7903+00	NM	0.76794	0.34099	0.65200	3.65600	0.17834	
5	5.3200-04	7.2615+00	NM	0.77889	0.35407	0.66900	3.57000	0.18739	
6	5.5700-04	7.6965+00	NM	0.78674	0.36475	0.68200	3.49600	0.19508	
7	7.6000-04	1.0103+01	NM	0.84576	0.42133	0.75300	3.19400	0.23575	
8	1.0140-03	1.1497+01	NM	0.87697	0.45086	0.78700	3.04700	0.25829	
9	1.2680-03	1.2727+01	NM	0.88796	0.47536	0.80700	2.88200	0.28001	
10	1.5520-03	1.4041+01	NM	0.89270	0.50021	0.82300	2.70700	0.30403	
11	1.7760-03	1.7550+01	NM	0.89974	0.56121	0.85500	2.32100	0.36838	
12	2.0300-03	1.6995+01	NM	0.90802	0.55202	0.85500	2.39900	0.35640	
13	2.2840-03	1.8689+01	NM	0.91774	0.57964	0.87100	2.25800	0.38574	
14	2.6650-03	2.1146+01	NM	0.93057	0.61750	0.89100	2.08200	0.42795	
15	2.9190-03	2.2513+01	NM	0.93756	0.63758	0.90100	1.99700	0.45118	
16	3.3000-03	2.5090+01	NM	0.95024	0.67384	0.91800	1.85600	0.49461	
17	3.5540-03	2.6790+01	NM	0.96013	0.69671	0.92900	1.77800	0.52250	
18	3.9350-03	2.9907+01	NM	0.96870	0.73681	0.94300	1.63800	0.57570	
19	4.5700-03	3.5007+01	NM	0.98755	0.79809	0.96500	1.46200	0.66005	
20	5.2050-03	4.0233+01	NM	0.99543	0.85634	0.97900	1.30700	0.74904	
21	5.8400-03	4.4705+01	NM	1.00156	0.90321	0.99900	1.19900	0.82485	
22	6.4750-03	4.8135+01	NM	1.00246	0.93757	0.99400	1.12400	0.88434	
23	7.1100-03	5.0796+01	NM	1.00218	0.96339	0.99700	1.07100	0.93091	
24	7.7450-03	5.2405+01	NM	1.00267	0.97866	0.99900	1.04200	0.95873	
25	8.3800-03	5.3269+01	NM	1.00287	0.98677	1.00000	1.02700	0.97371	
26	9.6500-03	5.3999+01	NM	1.00138	0.99356	1.00000	1.01300	0.98717	
27	1.0920-02	5.4317+01	NM	0.99874	0.99651	0.99900	1.00500	0.99403	
28	1.3460-02	5.4478+01	NM	0.99843	0.99800	0.99900	1.00200	0.99701	
29	1.6000-02	5.4478+01	NM	0.99843	0.99800	0.99900	1.00200	0.99701	
30	1.8540-02	5.4533+01	NM	1.00032	0.99850	1.00000	1.00300	0.99701	
0 31	2.1080-02	5.4695+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
32	2.3620-02	5.4695+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020903		DANBERG		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PPD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.51561	0.00000	0.00000	4.76000	0.00000	
2	3.3600-04	3.2260+00	NM	0.70486	0.22755	0.48400	4.52400	0.10698	
3	4.6300-04	5.1569+00	NM	0.74779	0.29876	0.59400	3.95300	0.15027	
4	5.9000-04	6.7885+00	NM	0.78385	0.34737	0.66000	3.61000	0.18283	
5	8.4400-04	8.6120+00	NM	0.82685	0.39456	0.72000	3.33000	0.21622	
6	1.0980-03	9.5193+00	NM	0.85048	0.41603	0.74700	3.22400	0.23170	
7	1.3520-03	1.0519+01	NM	0.86394	0.43846	0.76900	3.07600	0.25000	
8	1.9870-03	1.3065+01	NM	0.88274	0.49095	0.81000	2.72200	0.29758	
9	2.6220-03	1.5674+01	NM	0.90059	0.53945	0.84300	2.44200	0.34521	
10	3.2570-03	1.8909+01	NM	0.92169	0.59412	0.87600	2.17400	0.40294	
11	3.8920-03	2.2254+01	NM	0.93838	0.64577	0.90200	1.95100	0.46233	
12	5.1620-03	2.9339+01	NM	0.96821	0.74342	0.94300	1.60900	0.58608	
13	6.4320-03	3.7157+01	NM	0.99075	0.83805	0.97300	1.34800	0.72181	
14	7.7020-03	4.4089+01	NM	1.00137	0.91369	0.99000	1.17400	0.84327	
15	8.9720-03	4.8511+01	NM	1.00555	0.95899	0.99800	1.08300	0.92151	
16	1.0240-02	5.0026+01	NM	1.00392	0.97400	0.99900	1.05200	0.94962	
17	1.1510-02	5.0594+01	NM	1.00061	0.97956	0.99800	1.03800	0.96146	
18	1.4050-02	5.1429+01	NM	0.99875	0.98768	0.99800	1.02100	0.97747	
19	1.6590-02	5.1579+01	NM	0.99842	0.98914	0.99800	1.01800	0.98035	
20	1.9130-02	5.1882+01	NM	0.99776	0.99207	0.99800	1.01200	0.98617	
21	2.1670-02	5.2190+01	NM	0.99910	0.99503	0.99900	1.00800	0.99107	
22	2.4210-02	5.2499+01	NM	0.99844	0.99800	0.99900	1.00200	0.99701	
0 23	2.6750-02	5.2708+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020604		DANBERG		PROFILE TABULATION		22 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.82111	0.00000	0.00000	8.01800	0.00000	
2	2.7900*-04	1.4690*+00	NM	0.85589	0.11511	0.31500	7.48800	0.04207	
3	4.0600*-04	1.8398*+00	NM	0.87166	0.14734	0.39400	7.15100	0.05510	
4	5.3300*-04	2.1092*+00	NM	0.88769	0.16477	0.43600	7.00200	0.06227	
5	6.6000*-04	3.2587*+00	NM	0.90315	0.22031	0.54800	6.18700	0.08857	
6	7.8700*-04	4.2715*+00	NM	0.91932	0.25346	0.61500	5.66200	0.10862	
7	1.0410*-03	6.7442*+00	NM	0.94649	0.33307	0.72100	4.68600	0.15386	
8	1.6760*-03	1.0924*+01	NM	0.97538	0.43033	0.82000	3.63100	0.22583	
9	2.3110*-03	1.3594*+01	NM	0.97578	0.48225	0.85400	3.13600	0.27232	
10	2.9460*-03	1.5631*+01	NM	0.97679	0.51835	0.87400	2.84300	0.30742	
11	3.5810*-03	1.7803*+01	NM	0.97942	0.55426	0.89200	2.59000	0.34440	
12	4.2160*-03	2.0105*+01	NM	0.98264	0.58993	0.90800	2.36900	0.38128	
13	4.8510*-03	2.2262*+01	NM	0.98626	0.62150	0.92100	2.19600	0.41940	
14	6.1210*-03	2.7057*+01	NM	0.99353	0.68648	0.94400	1.89100	0.49921	
15	7.3910*-03	3.2435*+01	NM	1.00626	0.75271	0.96600	1.64700	0.58652	
16	8.6610*-03	3.7863*+01	NM	1.01044	0.81413	0.98000	1.44900	0.67633	
17	9.9310*-03	4.2984*+01	NM	1.01088	0.86808	0.98900	1.29800	0.76194	
18	1.1200*-02	4.7368*+01	NM	1.01061	0.91173	0.99500	1.19100	0.83543	
19	1.2470*-02	5.0486*+01	NM	1.00502	0.94155	0.99600	1.11900	0.89008	
20	1.3740*-02	5.2646*+01	NM	1.00430	0.96166	0.99800	1.07700	0.92665	
21	1.7550*-02	5.5456*+01	NM	1.00066	0.98722	0.99900	1.02400	0.97559	
D 22	2.3900*-02	5.6889*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020901		DANBERG		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.49365	0.00000	0.00000	4.66500	0.00000	
2	3.0400*-04	4.3723*+00	NM	0.69950	0.26677	0.54200	4.12800	0.13130	
3	4.0600*-04	4.3354*+00	NM	0.73260	0.26548	0.55300	4.33900	0.12745	
4	4.3100*-04	4.8888*+00	NM	0.76481	0.28417	0.58900	4.29600	0.13710	
5	4.8200*-04	5.9181*+00	NM	0.78807	0.31592	0.63500	4.04000	0.15718	
6	6.0900*-04	8.6824*+00	NM	0.84114	0.38834	0.72600	3.49500	0.20773	
7	7.3600*-04	1.0711*+01	NM	0.86582	0.43379	0.77100	3.19900	0.24406	
8	8.6300*-04	1.1642*+01	NM	0.88643	0.45311	0.79300	3.06300	0.25890	
9	1.1170*-03	1.3164*+01	NM	0.90401	0.48302	0.81900	2.87500	0.28487	
10	1.3710*-03	1.4694*+01	NM	0.91868	0.51134	0.84100	2.70500	0.31091	
11	1.6250*-03	1.6242*+01	NM	0.92694	0.53846	0.85800	2.53900	0.33793	
12	1.8790*-03	1.7990*+01	NM	0.93614	0.56754	0.87500	2.37700	0.36811	
13	2.1330*-03	1.9912*+01	NM	0.94490	0.59787	0.89100	2.22100	0.40117	
14	2.6310*-03	2.4139*+01	NM	0.96265	0.65967	0.92000	1.94500	0.47301	
15	3.1490*-03	2.9065*+01	NM	0.97620	0.72508	0.94400	1.69500	0.55693	
16	3.7840*-03	3.5354*+01	NM	0.99452	0.80085	0.96900	1.46400	0.66189	
17	4.4190*-03	4.1659*+01	NM	0.99906	0.87022	0.98300	1.27600	0.77038	
18	5.0540*-03	4.5892*+01	NM	1.00260	0.91384	0.99100	1.17600	0.84269	
19	5.6890*-03	5.0001*+01	NM	0.99830	0.95427	0.99400	1.08500	0.91613	
20	6.3240*-03	5.2153*+01	NM	0.99752	0.97479	0.99600	1.04400	0.95402	
21	6.9590*-03	5.3582*+01	NM	0.99854	0.98817	0.99800	1.02000	0.97843	
22	7.5840*-03	5.4269*+01	NM	0.99916	0.99453	0.99900	1.00900	0.99009	
23	8.2290*-03	5.4591*+01	NM	1.00053	0.99751	1.00000	1.00500	0.99502	
24	8.8640*-03	5.4645*+01	NM	1.00042	0.99801	1.00000	1.00400	0.99602	
25	9.4990*-03	5.4753*+01	NM	1.00021	0.99900	1.00000	1.00200	0.99800	
D 26	1.0770*-02	5.4862*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020902		DANBERG		PROFILE TABULATION		32 POINTS, DELTA AT POINT 31			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.50244	0.00000	0.00000	4.73500	0.00000	
2	3.7900*-04	4.3219*+00	NM	0.71555	0.26541	0.54600	4.23200	0.12902	
3	4.3000*-04	5.1384*+00	NM	0.73743	0.29265	0.58800	4.03700	0.14565	
4	5.0600*-04	6.7903*+00	NM	0.76794	0.34099	0.65200	3.65600	0.17834	
5	5.3200*-04	7.2815*+00	NM	0.77089	0.35407	0.66900	3.57000	0.18739	
6	5.3700*-04	7.6965*+00	NM	0.78674	0.36475	0.68200	3.49600	0.19508	
7	7.6000*-04	1.0103*+01	NM	0.84576	0.42133	0.75300	3.19400	0.23575	
8	1.0140*-03	1.1497*+01	NM	0.87697	0.45086	0.78700	3.04700	0.25829	
9	1.2680*-03	1.2727*+01	NM	0.88796	0.47536	0.80700	2.89200	0.28001	
10	1.5520*-03	1.4041*+01	NM	0.89270	0.50021	0.82300	2.70700	0.30403	
11	1.7760*-03	1.7550*+01	NM	0.89974	0.56121	0.85500	2.32100	0.36838	
12	2.0300*-03	1.6995*+01	NM	0.90802	0.55202	0.85500	2.39900	0.35640	
13	2.2840*-03	1.8689*+01	NM	0.91774	0.57964	0.87100	2.25800	0.38574	
14	2.6650*-03	2.1146*+01	NM	0.93057	0.61750	0.89100	2.08200	0.42795	
15	2.9190*-03	2.2513*+01	NM	0.93736	0.63758	0.90100	1.99700	0.45118	
16	3.3000*-03	2.5090*+01	NM	0.95024	0.67384	0.91800	1.85600	0.49461	
17	3.5540*-03	2.6790*+01	NM	0.96013	0.69671	0.92900	1.77800	0.52250	
18	3.9350*-03	2.9907*+01	NM	0.96870	0.73681	0.94300	1.63800	0.57570	
19	4.5700*-03	3.5007*+01	NM	0.98755	0.79809	0.96500	1.46200	0.66005	
20	5.2050*-03	4.0233*+01	NM	0.99543	0.85634	0.97900	1.30700	0.74904	
21	5.8400*-03	4.4705*+01	NM	1.00156	0.90321	0.98900	1.19900	0.82485	
22	6.4750*-03	4.8135*+01	NM	1.00246	0.93757	0.99400	1.12400	0.88434	
23	7.1100*-03	5.0796*+01	NM	1.00218	0.96339	0.99700	1.07100	0.93091	
24	7.7450*-03	5.2405*+01	NM	1.00267	0.97866	0.99900	1.04200	0.95873	
25	8.3800*-03	5.3269*+01	NM	1.00287	0.98677	1.00000	1.02700	0.97371	
26	9.6500*-03	5.3999*+01	NM	1.00138	0.99356	1.00000	1.01300	0.98717	
27	1.0920*-02	5.4317*+01	NM	0.99874	0.99651	0.99900	1.00500	0.99403	
28	1.3460*-02	5.4478*+01	NM	0.99843	0.99800	0.99900	1.00200	0.99701	
29	1.6000*-02	5.4478*+01	NM	0.99843	0.99800	0.99900	1.00200	0.99701	
30	1.8540*-02	5.4533*+01	NM	1.00032	0.99850	1.00000	1.00300	0.99701	
D 31	2.1080*-02	5.4695*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
32	2.3620*-02	5.4695*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

67020903		DANBERG		PROFILE TABULATION		23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.51561	0.00000	0.00000	4.70000	0.00000	
2	3.3600*-04	3.2260*+00	NM	0.70486	0.22755	0.48400	4.52400	0.10698	
3	4.6300*-04	5.1569*+00	NM	0.74779	0.29876	0.59400	3.95300	0.15027	
4	5.9000*-04	6.7885*+00	NM	0.78385	0.34737	0.66000	3.61000	0.18283	
5	6.4400*-04	8.6120*+00	NM	0.82685	0.39456	0.72000	3.33000	0.21622	
6	1.0980*-03	9.5193*+00	NM	0.85048	0.41603	0.74700	3.22400	0.23170	
7	1.3520*-03	1.0519*+01	NM	0.86394	0.43866	0.76900	3.07600	0.25000	
8	1.9870*-03	1.3065*+01	NM	0.88274	0.49095	0.81000	2.72200	0.29750	
9	2.6220*-03	1.5674*+01	NM	0.90059	0.53945	0.84300	2.44200	0.34521	
10	3.2570*-03	1.8909*+01	NM	0.92169	0.59412	0.87600	2.17400	0.40294	
11	3.8920*-03	2.2254*+01	NM	0.93838	0.64577	0.90200	1.95100	0.46233	
12	5.1620*-03	2.9339*+01	NM	0.96821	0.74342	0.94300	1.60900	0.58608	
13	6.4320*-03	3.7157*+01	NM	0.99075	0.83805	0.97300	1.34800	0.72181	
14	7.7020*-03	4.4080*+01	NM	1.00137	0.91369	0.99000	1.17400	0.84327	
15	8.9720*-03	4.8511*+01	NM	1.00555	0.95899	0.99800	1.08300	0.92151	
16	1.0240*-02	5.0026*+01	NM	1.00392	0.97400	0.99900	1.05200	0.94962	
17	1.1510*-02	5.0594*+01	NM	1.00061	0.97956	0.99800	1.03800	0.96146	
18	1.4050*-02	5.1429*+01	NM	0.99875	0.98768	0.99800	1.02100	0.97747	
19	1.6590*-02	5.1579*+01	NM	0.99842	0.98914	0.99800	1.01800	0.98035	
20	1.9130*-02	5.1882*+01	NM	0.99776	0.99207	0.99800	1.01200	0.98617	
21	2.1670*-02	5.2190*+01	NM	0.99910	0.99503	0.99900	1.00800	0.99107	
22	2.4210*-02	5.2499*+01	NM	0.99844	0.99800	0.99900	1.00200	0.99701	
D 23	2.6750*-02	5.2708*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

For model arrangements see figure 1, on following pages.	M : ZPG, NPG, 2.5 APG, 2.5 to 1.6 FPG, 2.5 to 3.25 R THETA X 10 ⁻³ : 7 TW/TR : 0.8	6800
		ZPG. APG. FPG. NORMAL PG. MHT
Blow-down wind-tunnel, effectively continuous running. W = 0.234, H = 0.334 m. PO : 0.1 MN/m ² TO : 290 K. Air, specific humidity 1-3 X 10 ⁻⁴ . RE/m: 14 X 10 ⁶ at M = 2.5		
THOMANN H. 1968. Effect of streamwise wall curvature on heat-transfer in a turbulent boundary layer. J. Fluid Mech. 33, 283-292. <u>And</u> Drougge, G. Private communications. <u>Also</u> Thomann H. (1967).		

- 1 The test surfaces were two flexible stainless steel sheets, one with pressure taps and the other with thermocouples attached. In all cases these were mounted so that the first 317.5 mm (= L) from the leading edge (X = 0) formed a flat plate on which the test boundary layer was grown under identical conditions.
- 2 The Mach number in this region was 2.48 with a small high velocity region (M = 2.51) around X = 100 mm. A boundary layer trip of carborundum grains either 0.22 or 0.35 mm in diameter extended 3.5 mm downstream from X = 25 mm. The larger trip was used for all tests except the flat plate case. Heat transfer data indicate that transition took place near X = 100 mm.
- 1 The supporting structure after X = 317.5 mm could be changed so as to give either a straight continuation of the flat surface, or provide a bend in either direction with radii of curvature of either 150 or 300 mm. The curvature ceased when the deflection was 20°, with a further straight section downstream. With no further addition this provided for ZPG - flat plate tests and APG, FPG - SW (simple wave) generated expansions and compressions of two strengths. Additionally various ramps could be mounted over the test surfaces. One of these was shaped to give, if mounted above the test surface when arranged as a continuous flat plate, an APG-RW (reflected wave) compression with the same longitudinal pressure history as the more gentle (RZ = 300 mm) simple wave APG case. Other bodies were shaped and mounted as to produce on the curved surfaces incident waves of equal and opposite strength to those produced by the curved surfaces themselves. The results were flows with zero longitudinal pressure gradients but strong normal pressure gradients - the NPG cases. The NPG is negative on a concave surface, which without the body would cause an APG, and vice versa. In all cases the imposed pressure gradient started at X = 317.5 mm. The various arrangements are shown in figure 1. Great care was taken to ensure that the flow was two-dimensional.
- 4
- 5
- 6 The stainless steel sheet used for pressure plotting had tappings (d = 0.8 mm) on the centre-line at X = 47.5 mm and thereafter at intervals of 30 mm until X = 317.5 mm. On the rear part of the sheet the tappings were placed at longitudinal and lateral intervals of 10 mm in the locations shown in figure 2 and listed in the table below. The placing of the 0.25 mm iron constantan thermocouples on the heat transfer plate was the same. Heat transfer was measured by a transient technique. The model was covered by a layer of crushed solid Carbon Dioxide, to precool the thin stainless steel sheet. The CO₂ was blown away when the tunnel started and the subsequent time history allowed the heat transfer rate to be determined. The large number of thermocouples on the rear portion (X > 317.5 mm) allowed the longitudinal conduction correction to be determined for those points, 7 in all, surrounded by 4 other thermocouples.
- 9 Some interpolation or adjustment is implicit in the use of curve fitting to obtain the temperature differentials needed for the heat transfer determination. The author's values have been accepted.
- 14 The wall data is presented in the tables below. These consist of tabulated wall pressure values and uncorrected Stanton numbers for each of the ten two dimensional configurations tested. Conduction corrections, when applied, were in general less than 5 %. The larger corrections are indicated by arrows in figures 4 to 7 of the source paper.
- 6 DATA: 6800. No profiles. Heat transfer by the transient technique, wall pressures.

15 Editors' comments

This, the only entry which is not profile-based, and for which there are in fact no profiles, is included because of the complete coverage of the possible types of pressure gradient which is provided. We feel that, in spite of the high quality of this experiment, a repeat on a larger scale, incorporating profile measurements, would be invaluable. The lack of profile information at the start of the pressure gradients may be easily overcome by correlating known flat plate data. The differences in succeeding wall heat transfer provide a very good test for any advanced turbulence calculation method. There is a 30 - 40 % range in the local heat transfer coefficients for different values of the normal pressure gradient, and while some part of this for the concave configurations 06 and 07 may result from longitudinal vortex structures, the differences of up to 20 % for the convex configurations 08 and 09 is unlikely to have any such cause.

The Mach numbers presented are based on the wall pressure measurements, and because of the normal component of the pressure gradients, the Mach number at the boundary layer edge will be significantly different for all cases except configurations 1 and 10.

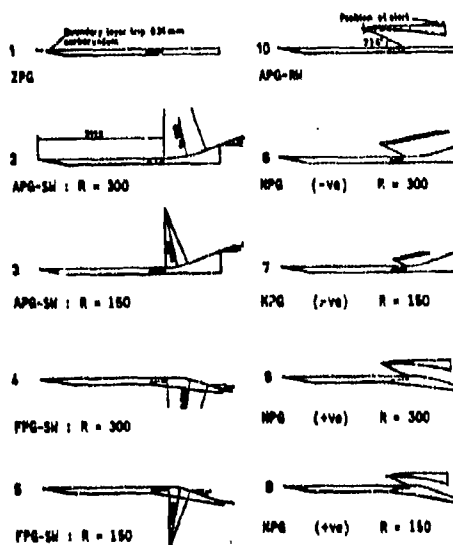


Figure 1 - ARRANGEMENT OF MODELS (FACSIMILE)

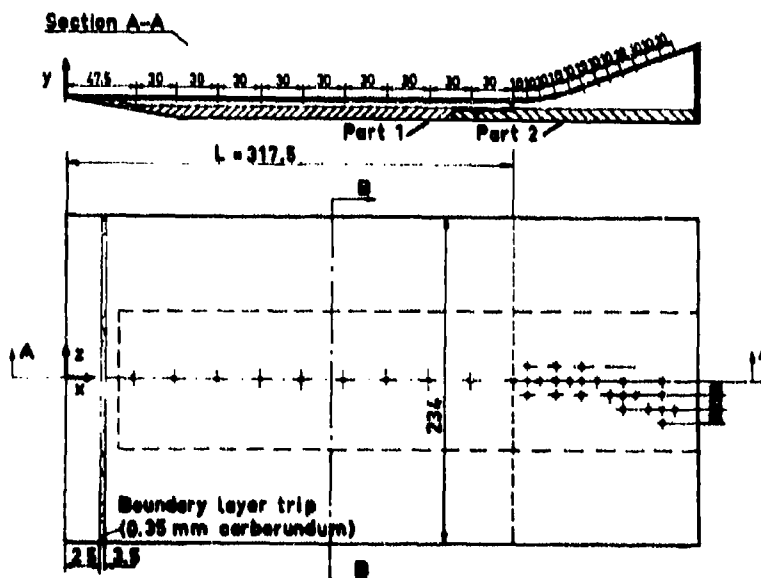


FIGURE 2: LOCATION OF MEASURING STATIONS (FACSIMILE)

The nominal position of each measuring station is given by x -distance from the leading edge, x -distance from the start of the pressure gradient, z -distance from the centre line. All dimensions are in mm, and the actual placing of instrumentation was within 0.1 mm of its nominal position.

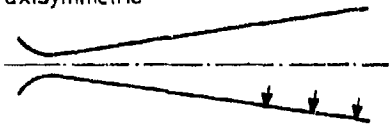
The Stanton numbers given represent the mean of a large number of determinations taken as the model temperature rose. They are normalised to conditions for which $T_0 = 290$ K, $T_d = 212.5$ K.

Location of measuring station		Configuration 1 ZPG			Configuration 2 APG SM RX = 300			Configuration 3 APG SM RX = 150			Configuration 4 FPG SM RX = 300			Configuration 5 FPG SM RX = 150		
X	Z	StX10 ³	p/po	M	StX10 ³	p/po	M	StX10 ³	p/po	M	StX10 ³	p/po	M	StX10 ³	p/po	M
47.5	- 270	1.28051	0.0586	2.49	3.28328	0.0591	2.49	3.56489	0.0596	2.49	0.44175	0.0600	2.48	-	0.0596	2.49
77.5	- 240	2.09516	0.0580	2.51	1.67991	0.0577	2.51	1.95582	0.0584	2.50	1.91033	0.0585	2.50	-	0.0584	2.50
107.5	- 210	1.76443	0.0584	2.50	1.73825	0.0573	2.51	1.77047	0.0580	2.51	1.73723	0.0578	2.51	-	0.0576	2.51
137.5	- 180	1.71698	0.0596	2.49	1.70850	0.0587	2.50	1.74729	0.0590	2.49	1.70132	0.0588	2.50	-	0.0582	2.50
167.5	- 150	1.57596	0.0594	2.49	1.53036	0.0587	2.50	1.54925	0.0590	2.49	1.54843	0.0586	2.50	-	0.0580	2.50
197.5	- 120	1.51350	0.0596	2.49	1.44462	0.0591	2.49	1.49733	0.0590	2.49	1.47186	0.0588	2.50	-	0.0586	2.50
227.5	- 90	1.43051	0.0603	2.48	1.40718	0.0595	2.49	1.43502	0.0594	2.49	1.42264	0.0598	2.50	-	0.0594	2.49
257.5	- 60	1.37567	0.0601	2.48	1.36394	0.0593	2.49	1.38841	0.0590	2.49	1.39985	0.0602	2.48	-	0.0596	2.49
287.5	- 30	1.39556	0.0600	2.48	1.39887	0.0600	2.48	1.39866	0.0606	2.48	1.39158	0.0604	2.48	1.48616	0.0602	2.48
317.5	0	1.39166	0.0605	2.48	1.36430	0.0664	2.42	1.43841	0.0712	2.37	1.44049	0.0558	2.52	1.38876	0.0535	2.56
327.5	10	1.38115	0.0609	2.47	1.35253	0.0710	2.37	1.45057	0.0801	2.30	1.46428	0.0524	2.57	1.38376	0.0460	2.65
327.5	10	1.37134	0.0603	2.48	1.36270	0.0702	2.38	1.47193	0.0797	2.30	1.48945	0.0520	2.57	1.34630	0.0485	2.66
327.5	10	1.36530	0.0611	2.47	1.36258	0.0710	2.37	1.46855	0.0824	2.30	1.48215	0.0485	2.57	1.31365	0.0462	2.86
327.5	20	1.33040	0.0609	2.47	1.36361	0.0763	2.33	1.45229	0.0965	2.18	1.41595	0.0485	2.62	1.20676	0.0371	2.80
347.5	30	1.28976	-	-	1.37511	0.0637	2.27	1.44195	0.1226	2.01	1.47939	0.0451	2.67	0.97301	0.0290	2.96
347.5	30	1.31751	0.0611	2.47	1.38342	0.0639	2.27	1.46737	0.1216	2.03	1.36330	0.0451	2.67	1.13582	0.0290	2.96
347.5	30	1.30888	0.0611	2.47	1.39108	0.0633	2.27	1.46407	0.1216	2.03	1.30901	0.0445	2.67	1.08955	0.0290	2.96
367.5	40	1.3000	0.0609	2.47	1.42403	0.0934	2.20	1.53909	0.1457	1.92	1.34088	0.0401	2.74	1.0231	0.0231	3.11
367.5	50	1.29974	0.0607	2.48	1.44556	0.1050	2.13	1.62906	0.1596	1.86	1.35882	0.0345	2.84	0.82899	0.0192	3.24
367.5	50	1.30954	0.0605	2.48	1.44466	0.1058	2.12	1.62748	0.1615	1.85	1.33279	0.0343	2.84	0.98040	0.0190	3.24
367.5	50	1.29532	0.0615	2.47	1.44486	0.1052	2.12	1.63907	0.1600	1.85	1.27841	0.0345	2.84	1.03477	0.0192	3.24
377.5	60	1.31600	0.0603	2.48	1.49032	0.1187	2.05	1.68707	0.1724	1.81	1.26095	0.0293	2.93	0.95242	0.0164	3.34
387.5	70	1.30312	0.0613	2.47	1.51676	0.1349	1.96	1.67458	0.1860	1.75	1.13116	0.0255	3.04	0.99621	0.0149	3.41
387.5	80	1.28802	0.0623	2.46	1.57405	0.1498	1.90	1.66661	0.1951	1.72	1.09584	0.0217	3.17	0.91605	0.0139	3.46
397.5	80	1.27719	0.0607	2.48	1.57325	0.1484	1.90	1.65027	0.1975	1.72	0.93265	0.0221	3.14	0.79991	0.0139	3.46
397.5	80	1.30711	0.0615	2.47	1.54682	0.1510	1.89	1.64295	0.2003	1.70	1.13845	0.0221	3.14	1.06147	0.0139	3.46
407.5	90	1.27329	0.0609	2.47	1.58002	0.1552	1.83	1.63668	0.2003	1.70	1.06278	0.0193	3.23	0.86099	0.0160	3.36
417.5	100	1.26309	0.0617	2.47	1.56793	0.1799	1.78	1.59156	0.1860	1.75	1.10255	0.0183	3.27	0.83968	0.0176	3.29
427.5	110	1.25501	0.0623	2.46	1.57685	0.1927	1.73	1.62908	0.2003	1.70	1.18705	0.0163	3.35	0.68973	0.0225	3.13
427.5	110	1.20326	0.0619	2.46	1.54752	0.1925	1.73	1.58847	0.2003	1.70	0.99820	0.0163	3.35	0.55933	0.0223	3.13
427.5	110	1.21238	0.0619	2.46	1.45007	0.1918	1.74	1.52246	0.1949	1.72	1.13260	0.0179	3.28	1.03981	0.0223	3.13
427.5	110	1.25121	0.0621	2.46	1.54435	0.1916	1.74	1.52581	0.1904	1.74	0.95900	0.0173	3.28	0.90468	0.0222	3.13
427.5	110	1.53155	0.0623	2.46	1.71354	-	-	1.62788	-	-	1.26004	-	-	1.19532	-	-
427.5	110	1.0	0.0621	2.46	-	0.1892	1.75	-	0.2003	1.70	-	0.0167	3.33	-	0.0231	3.11
427.5	110	1.0	0.0633	2.45	-	0.1914	1.74	-	0.1937	1.73	-	0.0155	3.33	-	0.0237	3.09
427.5	110	1.0	0.0629	2.45	-	0.1918	1.74	-	0.1884	1.74	-	0.0167	3.33	-	0.0237	3.09
427.5	110	1.0	0.0623	2.46	-	0.1927	1.73	-	0.1947	1.73	-	0.0165	3.33	-	0.0237	3.09
437.5	120	1.26720	0.0619	2.46	1.55546	0.1991	1.71	1.56186	0.2003	1.70	1.28173	0.0181	3.27	0.18604	0.1934	1.73

The nominal position of each measuring station is given by X-distance from the leading edge, x-distance from the start of the pressure gradient, z-distance from the centre line. All dimensions are in mm, and the actual placing of instrumentation was within 0.1 mm of its nominal position.

The Stanton numbers given represent the mean of a large number of determinations taken as the model temperature rose. They are normalised to conditions for which $T_0 = 290$ K, $T_M = 212.5$ K.

X mm	x mm	z mm	Configuration 6 -ve RX = 300				Configuration 7 -ve RX = 150				Configuration 8 +ve RX = 300				Configuration 9 +ve RX = 150				Configuration 10 +ve RX = 150			
			Stx10 ³	p/po	M	Stx10 ³	p/po	M	Stx10 ³	p/po	M	Stx10 ³	p/po	M	Stx10 ³	p/po	M	Stx10 ³	p/po	M	Stx10 ³	p/po
47.5	-270	0	1.51364	0.0595	2.49	2.91960	0.0594	2.49	0.49306	0.0597	2.49	1.23496	0.0587	2.50	2.55807	0.0589	2.50					
77.5	-240	0	1.96926	0.0581	2.50	1.95175	0.0578	2.51	1.88348	0.0585	2.50	1.99142	0.0573	2.51	1.98614	0.0579	2.51					
107.5	-210	0	1.75473	0.0579	2.50	1.74957	0.0576	2.51	1.70887	0.0575	2.51	1.79312	0.0567	2.52	1.74977	0.0575	2.51					
137.5	-180	0	1.72734	0.0591	2.49	1.72764	0.0586	2.50	1.67757	0.0587	2.50	1.76199	0.0577	2.51	1.73848	0.0585	2.50					
167.5	-150	0	1.54416	0.0589	2.49	1.58836	0.0586	2.50	1.53566	0.0585	2.50	1.61005	0.0575	2.51	1.54748	0.0583	2.50					
197.5	-120	0	1.45863	0.0593	2.49	1.51237	0.0586	2.50	1.47519	0.0589	2.50	1.52650	0.0579	2.51	1.50282	0.0587	2.50					
227.5	-90	0	1.41029	0.0597	2.49	1.45344	0.0590	2.51	1.40816	0.0601	2.48	1.47112	0.0587	2.50	1.44709	0.0595	2.49					
257.5	-60	0	1.38747	0.0595	2.49	1.41949	0.0586	2.50	1.37282	0.0601	2.48	1.40830	0.0593	2.49	1.40577	0.0591	2.48					
287.5	-30	0	1.36544	0.0609	2.47	1.38057	0.0604	2.48	1.37179	0.0603	2.48	1.55170	0.0605	2.48	1.38444	0.0607	2.48					
317.5	0	0	1.35880	0.0647	2.44	1.43052	0.0667	2.42	1.38487	0.0577	2.51	1.45738	0.0573	2.51	1.41086	0.0607	2.48					
347.5	10	0	1.31156	0.0575	2.51	1.38096	0.0562	2.52	1.36517	0.0625	2.57	1.36682	0.0486	2.62	1.37853	0.0573	2.51					
377.5	10	0	1.35643	0.0567	2.52	1.45011	0.0560	2.53	1.36639	0.0523	2.57	1.41799	0.0490	2.61	1.43096	0.0567	2.52					
327.5	10	-10	1.37286	0.0575	2.51	1.46410	0.0562	2.52	1.37955	0.0523	2.57	1.41145	0.0492	2.61	1.41745	0.0575	2.51					
347.5	20	0	1.36237	0.0546	2.54	1.36580	0.0588	2.50	1.35045	0.0513	1.58	1.30053	0.0505	2.60	1.40813	0.0625	2.46					
367.5	30	0	1.42363	0.0538	2.55	1.42723	0.0533	2.56	1.36888	0.0541	2.55	1.25722	0.0531	2.56	1.36306	0.0744	2.35					
347.5	30	-10	1.41745	0.0540	2.55	1.40141	0.0551	2.54	1.31769	0.0537	2.56	1.27124	0.0553	2.56	1.35861	0.0786	2.34					
347.5	30	10	1.36524	0.0538	2.55	1.40956	0.0541	2.55	1.29482	0.0527	2.57	1.24492	0.0531	2.56	1.34764	0.0780	2.33					
357.5	40	0	1.41615	0.0536	2.56	1.41411	0.0537	2.56	1.30373	0.0555	2.53	1.23244	0.0533	2.56	1.31449	0.0866	2.25					
367.5	50	0	1.43610	0.0546	2.55	1.48472	0.0503	2.60	1.34560	0.0539	2.56	1.17595	0.0557	2.53	1.33039	0.0948	2.19					
367.5	50	10	1.42795	0.0546	2.55	1.48028	0.0513	2.59	1.30617	0.0543	2.55	1.19860	0.0549	2.54	1.33145	0.0954	2.19					
367.5	50	-10	1.44824	0.0548	2.55	1.48719	0.0497	2.61	1.28337	0.0641	2.55	1.19976	0.0557	2.53	1.33953	0.0950	2.19					
377.5	60	0	1.42134	0.0573	2.51	1.60907	0.0476	2.63	1.27626	0.0625	2.57	1.17597	0.0579	2.52	1.33635	0.1059	2.12					
387.5	70	-10	1.48656	0.0556	2.52	1.93023	0.0564	2.52	1.18953	0.0535	2.56	1.14720	0.0619	2.47	1.35068	0.1261	2.01					
397.5	80	0	1.46188	0.0573	2.51	1.57025	0.1196	2.04	1.13210	0.0555	2.53	1.12711	0.0561	2.53	1.34520	0.1400	1.94					
397.5	80	-10	1.48159	0.0571	2.51	1.62355	0.1181	2.05	1.10385	0.0557	2.53	1.10660	0.0561	2.53	1.33076	0.1394	1.94					
397.5	80	20	1.50144	0.0579	2.51	1.54022	0.1210	2.04	1.12578	0.0671	2.51	1.21923	0.0573	2.51	1.33317	0.1412	1.94					
407.5	90	-10	1.45267	0.0573	2.51	1.57329	0.1521	1.89	1.11362	0.0577	2.51	1.19585	0.0541	2.55	1.32193	0.1560	1.87					
417.5	100	-20	1.50014	0.0567	2.52	1.46403	0.1740	1.80	1.09024	0.0615	2.47	1.23214	0.0533	2.56	1.33217	0.1891	1.74					
427.5	110	0	1.50031	0.0567	2.52	1.44818	0.1872	1.75	1.05568	0.0609	2.48	1.20676	0.0543	2.55	1.37007	0.1967	1.72					
427.5	110	-10	1.38757	0.0563	2.52	1.40190	0.1862	1.76	1.03323	0.0603	2.48	1.18767	0.0543	2.55	1.31420	0.1967	1.72					
427.5	110	20	1.77479	0.0565	2.52	1.40393	0.1895	1.74	1.10038	0.0597	2.49	1.21949	0.0545	2.55	1.30890	0.1967	1.72					
427.5	110	-30	1.43805	0.0567	2.52	1.19492	0.1895	1.74	1.04596	0.0585	2.50	1.23647	0.0553	2.54	1.30933	0.1967	1.72					
427.5	110	-40	1.75001	-	-	1.65838	-	-	1.17167	-	-	1.49688	-	-	1.43090	-	-					
427.5	110	20	-	0.0561	2.53	-	0.1872	1.75	-	0.0607	2.48	-	0.0569	2.52	-	0.1963	1.72					
427.5	110	20	-	0.0567	2.53	-	0.1901	1.74	-	0.0593	2.49	-	0.0705	2.38	-	0.1963	1.72					
427.5	110	30	-	0.0571	2.53	-	0.1911	1.74	-	0.0575	2.51	-	0.0962	2.18	-	0.1967	1.72					
427.5	110	40	-	0.0565	2.53	-	0.1886	1.75	-	0.0571	2.51	-	0.0876	2.24	-	0.1967	1.72					
437.5	120	-20	1.74096	0.0579	2.51	1.40623	0.1988	1.71	1.10879	0.0597	2.49	1.26375	0.0587	2.50	1.30649	0.1779	1.79					

axisymmetric 	M : 8 to 9 and 10 to 11.6 R THETA X 10 ⁻³ : 4 - 30 TW/TR : 0.3 - 0.4	6801
		FPG - SHT
Axisymmetric gun-tunnel. Running time 10 - 20 ms. D = 0.1 m PO : 12 - 32 MN/m ² . TO : 823 - 1120 K. Nitrogen. RE/m X 10 ⁻⁶ : 9 - 47.		
PERRY J.H. and EAST R.A. 1968. Experimental measurements of cold wall turbulent hypersonic boundary layers. AGARD CP no 30. And Perry J.H., PhD Thesis, University of Southampton 1968, East R.A., private communications.		

- 1 The test boundary layer was formed on the wall of a 7.5° included angle conical nozzle. Two different throat blocks were used, the throat (X = 0) diameters being 4.80 and 2.44 mm. Measurements were made at three instrumentation ports in the downstream half of the nozzle. The diameter at the middle port was
- 3 87.7 mm. The test surface was finished to within 1.3 μm, and was not actively cooled. The throat Reynolds numbers were in the range 9.7 - 27 X 10⁶ and "should have been sufficiently high to ensure transition of the boundary layer at the throat".
- 6 Wall static pressure was measured with piezo-electric (Kistler 7013) transducers mounted in cavities immediately behind the static tappings (d = 0.4 mm) while it was assumed that, during the very short run, the wall temperature did not vary significantly from room temperature, approximately 290 K, except perhaps at the throat. The wall heat transfer rate was measured using platinum thin-film gauges mounted flush with the surface on a Pyrex substrate.
- 7 Pitot profiles were measured by a rapidly traversed FPP (h₁ = 1.12, h₂ = 0.56, b₁ = 1.78, b₂ = 1.22, l = 51 mm) the observed pressures being compared to values obtained with an identical fixed FPP. Agreement inside the inner 15 % of the boundary layer was good, but only values from the fixed probe were used in the inner region. For some of the low Mach number runs a fixed FPP with h₁ = 0.56 mm was used. Total temperature profiles were measured with a special STP (East and Perry 1967). This had a heating circuit built into the outer shield so that the probe could be pre-heated to temperatures near those expected in the run. The procedure used required two readings, with the probe body temperature slightly above and below that recorded by the thermocouple bead. For the front face d₁ = 1.78, d₂ = 0.79 mm, while a conical fairing ran back to the main probe body for which d₁ = 2.79 mm.
- 8 The three measuring stations were at 101.6 mm axial intervals, the first at X = 549 mm with the large throat and at 565 mm with the small throat. The design of the probes was such that TO profiles were taken 17.8 mm downstream of the equivalent PT2 profiles, with additional values 33 mm upstream of the last station. The
- 9 authors have interpolated the TO data to the X and Y stations of the PT2 data. The data presented is calculated from curves faired through the original data points of the Mach number and TO profiles. The
- 12 editors have accepted this. In association with the profiles the editors have quoted the Stanton number and the CF value as obtained from the velocity gradient at the wall by the authors. Static pressure was assumed
- 10 constant through the boundary layer and no corrections were applied to the profile data.
- 13 The profiles presented consist of four sets of three obtained at Mach numbers near 9 with the large throat and four sets of three and one individual profile at Mach numbers near 10.5 with the small throat. The wall
- 14 data consists of the measured heat flux and CF deduced from the wall velocity gradient.
- 5 DATA: 6801 0101-0903. Pitot and TO profiles obtained piecemeal separately in a great number of runs. NX = 3. Heat transfer measurements.
- 15 Editors' comments
 It is probably impossible at present to interpret these measurements in terms of correlations drawn directly from flat plate experience. Despite the apparently high Reynolds numbers, the majority of the profiles

display marked transitional characteristics in both the inner and outer regions. There are no available direct comparisons, the geometrically similar study by Hill - CAT 5901 being made at much lower Reynolds number. The profiles form a self-consistent set differing markedly from both ZPG results and FPG results measured in contoured nozzles.

The profiles are presented in fine detail, which is notable in view of the great amount of work required (each TO measurement required two runs) and the difficulty of normalising the data in a facility of this type, for which free stream conditions are never entirely repeatable. The TTP was larger than the TPP so that some TO data near the wall are interpolated.

The layer is growing on a straight (conical) wall so that the assumption of zero normal pressure gradient is reasonable (Hill reports no detectable difference across the layer in CAT 5901).

CAT 6801		PERRY		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW	PD		
X *	POD*	PW/PO*	RED2D	CO *	H32	H32K	TW*	TD		
RZ *	YOD*	SW *	DZ	PI2	H42	D2K	UD	YR		
68010101	8.0000	0.3900	3.2655 ⁺⁰³	5.2300 ⁻⁰⁴	8.8645	1.4765	1.3771 ⁺⁰³	1.3771 ⁺⁰³		
5.4864 ⁻⁰¹	1.3445 ⁺⁰⁷	1.0000	1.3558 ⁺⁰⁴	2.1791 ⁻⁰⁴	1.8235	1.7858	2.9000 ⁺⁰²	5.9638 ⁺⁰¹		
-3.6820 ⁻⁰²	8.2300 ⁺⁰²	0.0000	5.8050 ⁻⁰⁴	NM	1.3029	1.2233 ⁻⁰³	1.2587 ⁺⁰³	7.4361 ⁺⁰²		
68010102	8.5000	0.3903	2.6483 ⁺⁰³	5.4600 ⁻⁰⁴	10.8667	1.4945	8.9894 ⁺⁰²	8.9894 ⁺⁰²		
6.5024 ⁻⁰¹	1.3031 ⁺⁰⁷	1.0000	1.2309 ⁺⁰⁴	2.9653 ⁻⁰⁴	1.8210	1.7816	2.9000 ⁺⁰²	5.3269 ⁺⁰¹		
-4.3830 ⁻⁰²	8.2300 ⁺⁰²	0.0000	6.4150 ⁻⁰⁴	NM	1.2629	1.4846 ⁻⁰³	1.2640 ⁺⁰³	7.4295 ⁺⁰²		
68010103	8.8700	0.3906	2.9693 ⁺⁰³	5.9400 ⁻⁰⁴	9.7352	1.4905	6.6162 ⁺⁰²	6.6162 ⁺⁰²		
7.5184 ⁻⁰¹	1.2686 ⁺⁰⁷	1.0000	1.4949 ⁺⁰⁴	3.7092 ⁻⁰⁴	1.8217	1.7824	2.9000 ⁺⁰²	4.9177 ⁺⁰¹		
-5.0810 ⁻⁰²	8.2300 ⁺⁰²	0.0000	8.9981 ⁻⁰⁴	NM	1.3657	2.0364 ⁻⁰³	1.2673 ⁺⁰³	7.4252 ⁺⁰²		
68010201	8.0300	0.3504	3.1118 ⁺⁰³	5.4800 ⁻⁰⁴	7.8731	1.5142	1.2958 ⁺⁰³	1.2958 ⁺⁰³		
5.4864 ⁻⁰¹	1.2962 ⁺⁰⁷	1.0000	1.1694 ⁺⁰⁴	2.1804 ⁻⁰⁴	1.8161	1.7743	2.9000 ⁺⁰²	6.5917 ⁺⁰¹		
-3.6820 ⁻⁰²	9.1600 ⁺⁰²	0.0000	6.1575 ⁻⁰⁴	NM	1.3582	1.2305 ⁻⁰³	1.3283 ⁺⁰³	8.2759 ⁺⁰²		
68010202	8.6100	0.3508	2.6141 ⁺⁰³	5.7900 ⁻⁰⁴	9.2609	1.5167	8.2631 ⁺⁰²	8.2631 ⁺⁰²		
6.5024 ⁻⁰¹	1.3031 ⁺⁰⁷	1.0000	1.1183 ⁺⁰⁴	2.9861 ⁻⁰⁴	1.8130	1.7733	2.9000 ⁺⁰²	5.7878 ⁺⁰¹		
-4.3830 ⁻⁰²	9.1600 ⁺⁰²	0.0000	7.0889 ⁻⁰⁴	NM	1.3490	1.5356 ⁻⁰³	1.3346 ⁺⁰³	8.2676 ⁺⁰²		
68010203	8.7000	0.3508	3.2876 ⁺⁰³	5.3900 ⁻⁰⁴	9.1855	1.5085	7.6772 ⁺⁰²	7.6772 ⁺⁰²		
7.5184 ⁻⁰¹	1.2962 ⁺⁰⁷	1.0000	1.4341 ⁺⁰⁴	3.1494 ⁻⁰⁴	1.8066	1.7745	2.9000 ⁺⁰²	5.6760 ⁺⁰¹		
-5.0810 ⁻⁰²	9.1600 ⁺⁰²	0.0000	9.4044 ⁻⁰⁴	NM	1.3586	2.0220 ⁻⁰³	1.3354 ⁺⁰³	8.2664 ⁺⁰²		
68010301	8.0500	0.3452	7.0854 ⁺⁰³	2.7500 ⁻⁰⁴	6.1211	1.4588	2.8756 ⁺⁰³	2.8756 ⁺⁰³		
5.4864 ⁻⁰¹	2.9234 ⁺⁰⁷	1.0000	2.6350 ⁺⁰⁴	9.7150 ⁻⁰⁵	1.8421	1.7942	2.9000 ⁺⁰²	6.6417 ⁺⁰¹		
-3.6820 ⁻⁰²	9.3000 ⁺⁰²	0.0000	6.3355 ⁻⁰⁴	NM	1.4684	1.1300 ⁻⁰³	1.3386 ⁺⁰³	8.4021 ⁺⁰²		
68010302	8.5000	0.3454	6.5750 ⁺⁰³	3.2000 ⁻⁰⁴	8.3153	1.4524	2.1070 ⁺⁰³	2.1070 ⁺⁰³		
6.5024 ⁻⁰¹	3.0544 ⁺⁰⁷	1.0000	2.7047 ⁺⁰⁴	1.1932 ⁻⁰⁴	1.8238	1.7908	2.9000 ⁺⁰²	6.0194 ⁺⁰¹		
-4.3830 ⁻⁰²	9.3000 ⁺⁰²	0.0000	7.2232 ⁻⁰⁴	NM	1.3793	1.4550 ⁻⁰³	1.3436 ⁺⁰³	8.3954 ⁺⁰²		
68010303	9.0500	0.3457	6.7155 ⁺⁰³	2.9600 ⁻⁰⁴	8.2852	1.4891	1.4175 ⁺⁰³	1.4175 ⁺⁰³		
7.5184 ⁻⁰¹	3.1026 ⁺⁰⁷	1.0000	3.1073 ⁺⁰⁴	1.5682 ⁻⁰⁴	1.8173	1.7806	2.9000 ⁺⁰²	5.3508 ⁺⁰¹		
-5.0810 ⁻⁰²	9.3000 ⁺⁰²	0.0000	9.7113 ⁻⁰⁴	NM	1.4355	2.0068 ⁻⁰³	1.3488 ⁺⁰³	8.3884 ⁺⁰²		

CAT 6801 PERRY BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.								
RUH X * RZ *	MD * POD* TOD*	TH/TR PH/PO* SH * DZ	RED2W RED2D	CF * CO * PI2	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR
68010401 5.4864*-01 -3.6820*-02	8.0600 2.9027*+07 1.0100*+03	0.3178 1.0000 0.0000	7.3012*+03 2.50A1*+04 6.8909*-04	2.8000*-04 9.4267*-05 NM	5.6353 1.8376 1.4852	1.4472 1.8009 1.1530*-03	2.8323*+03 2.9000*+02 1.3952*+03	2.8323*+03 7.2180*+01 9.1247*+02
68010402 6.5024*-01 -4.3830*-02	8.5000 3.0337*+07 1.0100*+03	0.3181 1.0000 0.0000	6.8165*+03 2.5829*+04 7.8572*-04	2.9400*-04 1.1502*-04 NM	7.3676 1.8250 1.4249	1.4555 1.7927 1.4808*-03	2.0928*+03 2.9000*+02 1.4002*+03	2.0928*+03 6.5372*+01 9.1176*+02
68010403 7.5184*-01 -5.0810*-02	9.0000 3.0682*+07 1.0100*+03	0.3183 1.0000 0.0000	6.7473*+03 2.8451*+04 1.0021*-03	2.9200*-04 1.4822*-04 NM	6.0104 1.8130 1.4411	1.4959 1.7773 2.0531*-03	1.4539*+03 2.9000*+02 1.4051*+03	1.4539*+03 5.8721*+01 9.1107*+02
68010501 5.6388*-01 -3.6820*-02	9.9500 1.3583*+07 9.1000*+02	0.3537 1.0000 0.0000	1.1878*+03 6.7200*+03 6.0511*-04	5.7700*-04 5.6637*-04 NM	14.8158 1.8365 1.3195	1.6158 1.7780 1.6906*-03	3.3092*+02 2.9000*+02 1.3409*+03	3.3092*+02 4.3749*+01 8.1991*+02
68010502 6.6548*-01 -4.3830*-02	10.6000 1.3721*+07 9.1000*+02	0.3539 1.0000 0.0000	8.8535*+02 5.6457*+03 6.0222*-04	5.9700*-04 7.5385*-04 NM	17.7132 1.8364 1.2962	1.6403 1.7726 1.8902*-03	2.1900*+02 2.9000*+02 1.3447*+03	2.1900*+02 3.8770*+01 8.1939*+02
68010503 7.6708*-01 -5.0810*-02	11.2700 1.3652*+07 9.1000*+02	0.3541 1.0000 0.0000	7.5485*+02 5.4009*+03 6.9061*-04	5.9700*-04 1.0143*-03 NM	18.3505 1.8434 1.3480	1.6612 1.7755 2.1934*-03	1.4435*+02 2.9000*+02 1.3480*+03	1.4435*+02 3.4466*+01 8.1894*+02
68010601 5.6388*-01 -3.6820*-02	9.9000 1.2617*+07 1.0200*+03	0.3155 1.0000 0.0000	1.0679*+03 5.3401*+04 6.0547*-04	5.6300*-04 5.6292*-04 NM	14.6900 1.8378 1.3184	1.6227 1.7793 1.6859*-03	3.1790*+02 2.9000*+02 1.4192*+03	3.1790*+02 4.9510*+01 9.1907*+02
68010602 6.6548*-01 -4.3830*-02	10.4800 1.3100*+07 1.0200*+03	0.3157 1.0000 0.0000	8.8818*+02 4.9500*+03 6.3472*-04	6.2100*-04 7.0768*-04 NM	16.7123 1.8303 1.3107	1.6178 1.7773 1.8963*-03	2.2567*+02 2.9000*+02 1.4230*+03	2.2567*+02 4.4413*+01 9.1854*+02
68010603 7.6708*-01 -5.0810*-02	11.2000 1.3100*+07 1.0200*+03	0.3159 1.0000 0.0000	7.3121*+02 4.6241*+03 7.1668*-04	5.8700*-04 9.7037*-04 NM	18.0365 1.8438 1.3334	1.6640 1.7775 2.2500*-03	1.4445*+02 2.9000*+02 1.4268*+03	1.4445*+02 3.9098*+01 9.1799*+02
68010701 7.6708*-01 -5.0810*-02	11.4300 2.1650*+07 1.0000*+03	0.3223 1.0000 0.0000	1.1853*+03 7.9429*+03 7.6699*-04	5.4600*-04 6.5313*-04 NM	15.5523 1.8360 1.4222	1.6149 1.7714 2.2597*-03	2.0818*+02 2.9000*+02 1.4139*+03	2.0818*+02 3.6861*+01 8.9983*+02
68010801 5.6388*-01 -3.6820*-02	10.2500 2.9923*+07 1.0200*+03	0.3157 1.0000 0.0000	2.2164*+03 1.1841*+04 6.2427*-04	4.3800*-04 2.7878*-04 NM	12.9600 1.8414 1.3908	1.5176 1.7965 1.5746*-03	5.9795*+02 2.9000*+02 1.4216*+03	5.9795*+02 4.6337*+01 9.1874*+02
68010802 6.6548*-01 -4.3830*-02	10.8700 3.1095*+07 1.0200*+03	0.3158 1.0000 0.0000	1.7622*+03 1.0529*+04 6.3104*-04	5.9500*-04 3.5384*-04 NM	15.7326 1.8346 1.3597	1.5190 1.7823 1.8597*-03	4.1926*+02 2.9000*+02 1.4252*+03	4.1926*+02 4.1411*+01 9.1823*+02
68010803 7.6708*-01 -5.0810*-02	11.5000 3.1716*+07 1.0200*+03	0.3160 1.0000 0.0000	1.9563*+03 1.3007*+04 8.9856*-04	5.5300*-04 4.5451*-04 NM	12.7100 1.8355 1.4916	1.5399 1.7833 2.3769*-03	2.9267*+02 2.9000*+02 1.4282*+03	2.9267*+02 3.7158*+01 9.1778*+02
68010901 5.6388*-01 -3.6820*-02	10.2000 2.9578*+07 1.1200*+03	0.2875 1.0000 0.0000	2.3088*+03 1.1130*+04 6.7362*-04	4.2400*-04 2.6396*-04 NM	12.0183 1.8290 1.4097	1.5461 1.7891 1.6344*-03	6.1069*+02 2.9000*+02 1.4893*+03	6.1069*+02 5.1357*+01 1.0084*+03
68010902 6.6548*-01 -4.3830*-02	10.6500 3.0682*+07 1.1200*+03	0.2876 1.0000 0.0000	2.1376*+03 1.1191*+04 7.3765*-04	5.4900*-04 3.1116*-04 NM	12.9819 1.8259 1.4151	1.5337 1.7794 1.9409*-03	4.7452*+02 2.9000*+02 1.4921*+03	4.7452*+02 4.7288*+01 1.0084*+03
68010903 7.6708*-01 -5.0810*-02	11.6000 3.1026*+07 1.1200*+03	0.2878 1.0000 0.0000	1.9350*+03 1.1927*+04 9.9224*-04	5.4100*-04 4.6270*-04 NM	11.5067 1.8330 1.5259	1.5537 1.7817 2.4718*-03	2.7006*+02 2.9000*+02 1.4971*+03	2.7006*+02 4.0126*+01 1.0077*+03

CF AUTHOR (DU/DY)H

68010301		PERRY		PROFILE TABULATION		51 POINTS, DELTA AT POINT 51			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/TD	KHC/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.31183	0.00000	0.00000	4.35330	0.00000	
2	2.7940*-04	3.8463*+00	NM	0.46237	0.20002	0.41240	4.25100	0.09701	
3	5.5880*-04	7.6522*+00	NM	0.53548	0.24316	0.55130	3.53640	0.15589	
4	8.3820*-04	1.1006*+01	NM	0.58601	0.35528	0.62590	3.10370	0.20166	
5	1.1176*-03	1.3903*+01	NM	0.62684	0.40122	0.67560	2.83540	0.23827	
6	1.3970*-03	1.6334*+01	NM	0.64738	0.43605	0.70430	2.60880	0.26997	
7	1.6764*-03	1.8383*+01	NM	0.66883	0.46337	0.72890	2.46840	0.29493	
8	1.9558*-03	2.0866*+01	NM	0.68500	0.49444	0.74890	2.29410	0.32645	
9	2.2352*-03	2.3286*+01	NM	0.70535	0.52297	0.76980	2.16670	0.35529	
10	2.5146*-03	2.5617*+01	NM	0.72145	0.54904	0.78660	2.05260	0.38322	
11	2.7940*-03	2.8184*+01	NM	0.73435	0.57637	0.80120	1.93230	0.41464	
12	3.0734*-03	2.9763*+01	NM	0.74735	0.59257	0.81240	1.81960	0.43222	
13	3.3528*-03	3.2139*+01	NM	0.75580	0.61613	0.82260	1.78250	0.46149	
14	3.6322*-03	3.4220*+01	NM	0.76778	0.63605	0.83340	1.71680	0.48544	
15	3.9116*-03	3.7043*+01	NM	0.78065	0.66212	0.84560	1.63100	0.51845	
16	4.1910*-03	3.9988*+01	NM	0.78708	0.67950	0.85230	1.57330	0.54173	
17	4.4704*-03	4.1132*+01	NM	0.79679	0.69816	0.86080	1.52020	0.56624	
18	4.7498*-03	4.3336*+01	NM	0.80653	0.71682	0.86910	1.47000	0.59122	
19	5.0292*-03	4.6044*+01	NM	0.81396	0.73912	0.87650	1.40630	0.62327	
20	5.3086*-03	4.8374*+01	NM	0.82259	0.75777	0.88380	1.36030	0.64971	
21	5.5880*-03	5.0918*+01	NM	0.82900	0.77763	0.88990	1.30960	0.67952	
22	5.8674*-03	5.2704*+01	NM	0.83865	0.79128	0.89680	1.28450	0.69817	
23	6.1468*-03	5.5194*+01	NM	0.84511	0.80991	0.90250	1.24170	0.72683	
24	6.4262*-03	5.7570*+01	NM	0.85376	0.82731	0.90910	1.20750	0.75288	
25	6.7056*-03	5.9473*+01	NM	0.86017	0.84098	0.91400	1.18120	0.77379	
26	6.9850*-03	6.6022*+01	NM	0.91577	0.88642	0.94930	1.14690	0.82771	
27	7.2644*-03	6.3918*+01	NM	0.87207	0.87208	0.92350	1.12140	0.82352	
28	7.5438*-03	6.5914*+01	NM	0.88060	0.88569	0.92930	1.10090	0.84413	
29	7.8232*-03	6.8321*+01	NM	0.88594	0.90183	0.93360	1.07170	0.87114	
30	8.1026*-03	6.9263*+01	NM	0.89249	0.90807	0.93760	1.06610	0.87947	
31	8.3820*-03	7.0784*+01	NM	0.89788	0.91805	0.94130	1.05130	0.89537	
32	8.6614*-03	7.2316*+01	NM	0.90544	0.92800	0.94610	1.03940	0.91024	
33	8.9408*-03	7.4054*+01	NM	0.91076	0.93915	0.94980	1.02280	0.92863	
34	9.2202*-03	7.6000*+01	NM	0.91713	0.95149	0.95410	1.00550	0.94888	
35	9.4996*-03	7.6796*+01	NM	0.92465	0.95649	0.95840	1.00400	0.95458	
36	9.7790*-03	7.7905*+01	NM	0.93010	0.96397	0.96180	0.99550	0.96615	
37	1.0058*-02	7.9392*+01	NM	0.93542	0.97262	0.96520	0.98480	0.98010	
38	1.0338*-02	8.0216*+01	NM	0.94090	0.97768	0.96840	0.98110	0.98786	
39	1.0617*-02	8.1230*+01	NM	0.94624	0.98388	0.97160	0.97520	0.99631	
40	1.0897*-02	8.2039*+01	NM	0.95159	0.98879	0.97470	0.97170	1.00309	
41	1.1176*-02	8.2653*+01	NM	0.95478	0.99251	0.97660	0.96820	1.00868	
42	1.1455*-02	8.3082*+01	NM	0.96030	0.99509	0.97960	0.96910	1.01083	
43	1.1735*-02	8.3698*+01	NM	0.96783	0.99880	0.98370	0.97000	1.01412	
44	1.2014*-02	8.3900*+01	NM	0.97101	1.00001	0.98540	0.97100	1.01483	
45	1.2294*-02	8.3903*+01	NM	0.97535	1.00003	0.98760	0.97530	1.01261	
46	1.2573*-02	8.3907*+01	NM	0.98069	1.00005	0.99030	0.98060	1.00989	
47	1.2852*-02	8.3896*+01	NM	0.98387	0.99998	0.99190	0.98390	1.00813	
48	1.3132*-02	8.3894*+01	NM	0.98705	0.99997	0.99350	0.98710	1.00648	
49	1.3411*-02	8.3908*+01	NM	0.99360	1.00006	0.99680	0.99350	1.00332	
50	1.3691*-02	8.3907*+01	NM	0.99899	1.00005	0.99950	0.99890	1.00060	
D 51	1.3970*-02	8.3899*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

68010401		PERRY		PROFILE TABULATION		51 POINTS, DELTA AT POINT 50			
I	Y	PTZ/P	P/PO	T0/TOD	H/H0	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.28770	0.00000	0.00000	4.02575	0.00000	
2	2.7940*-04	3.8874*+00	NM	0.42167	0.20102	0.39540	3.86904	0.10219	
3	5.5880*-04	1.1830*+01	NM	0.49109	0.36808	0.58098	2.48597	0.23370	
4	8.3820*-04	1.4662*+01	NM	0.55952	0.41190	0.64384	2.44329	0.26352	
5	1.1176*-03	1.7809*+01	NM	0.60513	0.45531	0.68937	2.29248	0.30072	
6	1.3970*-03	2.0251*+01	NM	0.63590	0.48634	0.71882	2.18457	0.32904	
7	1.6764*-03	2.1692*+01	NM	0.66276	0.50374	0.74004	2.15822	0.34289	
8	1.9558*-03	2.4057*+01	NM	0.68354	0.53101	0.76046	2.05090	0.37079	
9	2.2352*-03	2.5846*+01	NM	0.69839	0.55085	0.77457	1.97725	0.39174	
10	2.5146*-03	2.7945*+01	NM	0.71126	0.57317	0.78779	1.88908	0.41702	
11	2.7940*-03	3.0010*+01	NM	0.72429	0.59433	0.80030	1.81323	0.44137	
12	3.0734*-03	3.1762*+01	NM	0.73618	0.61170	0.81091	1.75741	0.46142	
13	3.3528*-03	3.3563*+01	NM	0.74709	0.62906	0.82072	1.70220	0.48215	
14	3.6322*-03	3.5141*+01	NM	0.76086	0.64388	0.83133	1.66703	0.49849	
15	3.9116*-03	3.7455*+01	NM	0.77184	0.66501	0.84143	1.60100	0.52557	
16	4.1910*-03	3.9412*+01	NM	0.77780	0.68230	0.84785	1.54379	0.54920	
17	4.4704*-03	4.1562*+01	NM	0.78668	0.70096	0.85546	1.49078	0.57410	
18	4.7498*-03	4.4035*+01	NM	0.79568	0.71341	0.86276	1.44675	0.58991	
19	5.0292*-03	4.5293*+01	NM	0.80275	0.73209	0.86947	1.41052	0.61642	
20	5.3086*-03	4.7435*+01	NM	0.81052	0.74938	0.87618	1.36703	0.64093	
21	5.5880*-03	4.9160*+01	NM	0.81946	0.76301	0.88288	1.33888	0.65942	
22	5.8674*-03	5.1246*+01	NM	0.82946	0.77918	0.89037	1.30581	0.68187	
23	6.1468*-03	5.3198*+01	NM	0.83532	0.79402	0.89540	1.27164	0.70412	
24	6.4262*-03	5.5369*+01	NM	0.84236	0.81020	0.90110	1.23697	0.72847	
25	6.7056*-03	5.7579*+01	NM	0.85128	0.82635	0.90771	1.20661	0.75228	
26	6.9850*-03	5.9123*+01	NM	0.86010	0.83744	0.91361	1.19018	0.76763	
27	7.2644*-03	6.0705*+01	NM	0.86615	0.84866	0.91892	1.17014	0.78454	
28	7.5438*-03	6.3012*+01	NM	0.87402	0.86475	0.92382	1.14178	0.80946	
29	7.8232*-03	6.4821*+01	NM	0.87797	0.87718	0.92713	1.11713	0.82992	
30	8.1026*-03	6.6290*+01	NM	0.88397	0.88713	0.93123	1.10190	0.84511	
31	8.3820*-03	6.8325*+01	NM	0.89282	0.90073	0.93714	1.08246	0.86574	
32	8.6614*-03	6.9836*+01	NM	0.90087	0.91071	0.94224	1.07044	0.88024	
33	8.9408*-03	7.1158*+01	NM	0.90576	0.91934	0.94555	1.05782	0.89377	
34	9.2202*-03	7.2989*+01	NM	0.91181	0.93059	0.94965	1.04138	0.91191	
35	9.4996*-03	7.4447*+01	NM	0.91871	0.94047	0.95405	1.02906	0.92711	
36	9.7790*-03	7.5620*+01	NM	0.92567	0.94791	0.95826	1.02194	0.93768	
37	1.0058*-02	7.7192*+01	NM	0.93247	0.95778	0.96256	1.01002	0.95301	
38	1.0338*-02	7.8199*+01	NM	0.93855	0.96404	0.96617	1.00441	0.96194	
39	1.0617*-02	7.9402*+01	NM	0.94446	0.97147	0.96977	0.99649	0.97318	
40	1.0897*-02	8.0413*+01	NM	0.94883	0.97768	0.97227	0.98898	0.98311	
41	1.1176*-02	8.1433*+01	NM	0.95438	0.98389	0.97578	0.98357	0.99208	
42	1.1455*-02	8.2247*+01	NM	0.95937	0.98884	0.97868	0.97956	0.99910	
43	1.1735*-02	8.2869*+01	NM	0.96727	0.99258	0.98298	0.98076	1.00227	
44	1.2014*-02	8.3492*+01	NM	0.97328	0.99632	0.98629	0.97996	1.00646	
45	1.2294*-02	8.3906*+01	NM	0.97728	0.99880	0.98849	0.97946	1.00922	
46	1.2573*-02	8.4098*+01	NM	0.98207	0.99995	0.99097	0.98216	1.00899	
47	1.2852*-02	8.4094*+01	NM	0.98604	0.99993	0.99299	0.98617	1.00692	
48	1.3132*-02	8.4101*+01	NM	0.99002	0.99997	0.99499	0.99008	1.00496	
49	1.3411*-02	8.4099*+01	NM	0.99501	0.99996	0.99750	0.99509	1.00242	
0 50	1.3691*-02	8.4106*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
51	1.3970*-02	8.4106*+01	NM	1.00200	1.00000	1.00100	1.00200	0.99900	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PO

68010501		PERRY		PROFILE TABULATION		51 POINTS, DELTA AT POINT 49			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.31868	0.00000	0.00000	6.62870	0.00000	
2	4.5720-04	1.8281+00	NM	0.40987	0.09747	0.26110	7.17560	0.03639	
3	9.1440-04	4.5322+00	NM	0.49227	0.17787	0.44630	6.29560	0.07089	
4	1.3716-03	9.5856+00	NM	0.56479	0.26732	0.58960	4.86470	0.12120	
5	1.8288-03	1.1678+01	NM	0.62415	0.29647	0.64530	4.73750	0.13621	
6	2.2860-03	1.3737+01	NM	0.66479	0.32260	0.68570	4.51800	0.15177	
7	2.7432-03	1.6064+01	NM	0.69894	0.34977	0.72090	4.24810	0.16970	
8	3.2004-03	1.7810+01	NM	0.71866	0.36883	0.74200	4.04710	0.18334	
9	3.6576-03	1.9753+01	NM	0.74072	0.38897	0.76380	3.85600	0.19808	
10	4.1148-03	2.2008+01	NM	0.75610	0.41108	0.78200	3.61880	0.21609	
11	4.5720-03	2.4493+01	NM	0.76919	0.43415	0.79830	3.38100	0.23611	
12	5.0292-03	2.6890+01	NM	0.78248	0.45530	0.81300	3.18850	0.25498	
13	5.4864-03	2.9269+01	NM	0.79444	0.47535	0.82590	3.01870	0.27359	
14	5.9436-03	3.2012+01	NM	0.80547	0.49748	0.83830	2.83950	0.29523	
15	6.4008-03	3.4219+01	NM	0.81432	0.51459	0.84760	2.71310	0.31241	
16	6.8580-03	3.7317+01	NM	0.82089	0.53769	0.85680	2.53920	0.33743	
17	7.3152-03	3.9976+01	NM	0.82849	0.55675	0.86510	2.41440	0.35831	
18	7.7724-03	4.2735+01	NM	0.83292	0.57586	0.87140	2.28980	0.38056	
19	8.2296-03	4.5743+01	NM	0.84179	0.59600	0.87990	2.17960	0.40370	
20	8.6868-03	4.8843+01	NM	0.84612	0.61607	0.88570	2.06690	0.42852	
21	9.1440-03	5.2223+01	NM	0.85391	0.63722	0.89320	1.96480	0.45460	
22	9.6012-03	5.5528+01	NM	0.85929	0.65726	0.89900	1.87090	0.48052	
23	1.0058-02	5.8775+01	NM	0.86477	0.67636	0.90450	1.78840	0.50576	
24	1.0516-02	6.2842+01	NM	0.87041	0.69954	0.91040	1.69370	0.53752	
25	1.0973-02	6.6277+01	NM	0.87685	0.71855	0.91600	1.62510	0.56366	
26	1.1430-02	7.0023+01	NM	0.88468	0.73872	0.92230	1.55880	0.59167	
27	1.1887-02	7.3856+01	NM	0.88900	0.75879	0.92660	1.49120	0.62138	
28	1.2344-02	7.7200+01	NM	0.89450	0.77589	0.93110	1.44010	0.64655	
29	1.2802-02	8.1440+01	NM	0.90009	0.79704	0.93590	1.37880	0.67878	
30	1.3259-02	8.5572+01	NM	0.90667	0.81712	0.94100	1.32620	0.70955	
31	1.3716-02	8.8529+01	NM	0.91436	0.83119	0.94610	1.29560	0.73024	
32	1.4173-02	9.2614+01	NM	0.91758	0.85025	0.94920	1.24630	0.76161	
33	1.4630-02	9.6358+01	NM	0.92530	0.86735	0.95440	1.21080	0.78824	
34	1.5088-02	9.9495+01	NM	0.93082	0.88142	0.95820	1.18180	0.81080	
35	1.5545-02	1.0314+02	NM	0.93405	0.89749	0.96090	1.14630	0.83826	
36	1.6002-02	1.0638+02	NM	0.93956	0.91154	0.96460	1.11980	0.86140	
37	1.6459-02	1.0967+02	NM	0.94612	0.92561	0.96880	1.09550	0.88435	
38	1.6916-02	1.1255+02	NM	0.95063	0.93772	0.97180	1.07400	0.90484	
39	1.7374-02	1.1545+02	NM	0.95500	0.94976	0.97470	1.05320	0.92547	
40	1.7831-02	1.1764+02	NM	0.95934	0.95879	0.97740	1.03920	0.94053	
41	1.8288-02	1.1962+02	NM	0.96480	0.96682	0.98060	1.02870	0.95324	
42	1.8745-02	1.2086+02	NM	0.96922	0.97184	0.98310	1.02330	0.96072	
43	1.9152-02	1.2260+02	NM	0.97246	0.97886	0.98510	1.01280	0.97265	
44	1.9600-02	1.2411+02	NM	0.97799	0.98491	0.98820	1.00670	0.98162	
45	2.0117-02	1.2488+02	NM	0.98245	0.98794	0.99060	1.00540	0.98528	
46	2.0574-02	1.2614+02	NM	0.98792	0.99295	0.99360	1.00130	0.99231	
47	2.1031-02	1.2693+02	NM	0.99240	0.99605	0.99600	0.99990	0.99610	
48	2.1488-02	1.2769+02	NM	1.00009	0.99905	1.00000	1.00190	0.99810	
D 49	2.1946-02	1.2793+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
50	2.2403-02	1.2793+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
51	2.2860-02	1.2793+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

68010401

PERRY

PROFILE TABULATION

51 POINTS, DELTA AT POINT 50

I	Y	PT2/P	P/PD	T0/T0D	H/H0	U/U0	T/T0	RHO/RHO0*U/U0
1	0.0000*+00	1.0000*+00	NM	0.28770	0.00000	0.00000	4.02575	0.00000
2	2.7940*-04	3.8874*+00	NM	0.42167	0.20102	0.39540	3.86904	0.10219
3	5.5880*-04	1.1830*+01	NM	0.49109	0.36848	0.58098	2.48597	0.23370
4	8.3820*-04	1.4662*+01	NM	0.55952	0.41190	0.64384	2.44329	0.26352
5	1.1176*-03	1.7809*+01	NM	0.60513	0.45531	0.68937	2.29248	0.30072
6	1.3970*-03	2.0251*+01	NM	0.63590	0.48634	0.71862	2.18457	0.32904
7	1.6764*-03	2.1692*+01	NM	0.66276	0.50374	0.74004	2.15822	0.34289
8	1.9558*-03	2.4052*+01	NM	0.68354	0.53101	0.76046	2.05090	0.37079
9	2.2352*-03	2.5846*+01	NM	0.69839	0.55085	0.77457	1.97725	0.39174
10	2.5146*-03	2.7945*+01	NM	0.71126	0.57317	0.78779	1.88908	0.41702
11	2.7940*-03	3.0010*+01	NM	0.72427	0.59433	0.80030	1.81323	0.44137
12	3.0734*-03	3.1762*+01	NM	0.73618	0.61170	0.81091	1.75741	0.46142
13	3.3528*-03	3.3563*+01	NM	0.74709	0.62906	0.82072	1.70220	0.48215
14	3.6322*-03	3.5141*+01	NM	0.76086	0.64388	0.83133	1.66703	0.49849
15	3.9116*-03	3.7455*+01	NM	0.77184	0.66501	0.84144	1.60100	0.52557
16	4.1910*-03	3.9412*+01	NM	0.77780	0.68238	0.84785	1.54379	0.54920
17	4.4704*-03	4.1562*+01	NM	0.78668	0.70096	0.85546	1.49078	0.57101
18	4.7498*-03	4.3035*+01	NM	0.79568	0.71341	0.86276	1.44253	0.58991
19	5.0292*-03	4.5293*+01	NM	0.80275	0.73209	0.86947	1.41052	0.61642
20	5.3086*-03	4.7435*+01	NM	0.81052	0.74938	0.87618	1.36703	0.64093
21	5.5880*-03	4.9160*+01	NM	0.81946	0.76391	0.88268	1.33888	0.65942
22	5.8674*-03	5.1240*+01	NM	0.82946	0.77918	0.89037	1.30581	0.68187
23	6.1468*-03	5.3198*+01	NM	0.83532	0.79402	0.89540	1.27164	0.70412
24	6.4262*-03	5.5369*+01	NM	0.84236	0.81020	0.90110	1.24697	0.72847
25	6.7056*-03	5.7579*+01	NM	0.85128	0.82635	0.90771	1.20661	0.75228
26	6.9850*-03	5.9123*+01	NM	0.86010	0.83744	0.91361	1.19018	0.76763
27	7.2644*-03	6.0705*+01	NM	0.86615	0.84866	0.91802	1.17014	0.78454
28	7.5438*-03	6.3012*+01	NM	0.87402	0.86475	0.92382	1.14128	0.80946
29	7.8232*-03	6.4821*+01	NM	0.87797	0.87718	0.92713	1.11713	0.82992
30	8.1026*-03	6.6290*+01	NM	0.88397	0.88713	0.93123	1.10190	0.84511
31	8.3820*-03	6.8325*+01	NM	0.89282	0.90073	0.93714	1.08246	0.86574
32	8.6614*-03	6.9836*+01	NM	0.90087	0.91071	0.94224	1.07044	0.88024
33	8.9408*-03	7.1158*+01	NM	0.90576	0.91934	0.94555	1.05782	0.89317
34	9.2202*-03	7.2898*+01	NM	0.91181	0.93059	0.94965	1.04138	0.91191
35	9.4996*-03	7.4447*+01	NM	0.91871	0.94049	0.95405	1.02906	0.92711
36	9.7790*-03	7.5620*+01	NM	0.92567	0.94791	0.95826	1.02194	0.93768
37	1.0058*-02	7.7192*+01	NM	0.93249	0.95778	0.96256	1.01002	0.95301
38	1.0338*-02	7.8199*+01	NM	0.93855	0.96404	0.96617	1.00441	0.96195
39	1.0617*-02	7.9402*+01	NM	0.94446	0.97147	0.96977	0.99649	0.97318
40	1.0897*-02	8.0413*+01	NM	0.94843	0.97768	0.97227	0.98998	0.98311
41	1.1176*-02	8.1433*+01	NM	0.95438	0.98389	0.97578	0.98357	0.99208
42	1.1455*-02	8.2249*+01	NM	0.95937	0.98884	0.97868	0.97956	0.99910
43	1.1735*-02	8.2869*+01	NM	0.96729	0.99258	0.98298	0.98076	1.00227
44	1.2014*-02	8.3492*+01	NM	0.97328	0.99632	0.98629	0.97996	1.00646
45	1.2294*-02	8.3906*+01	NM	0.97728	0.99880	0.98849	0.97946	1.00922
46	1.2573*-02	8.4498*+01	NM	0.98207	0.99995	0.99099	0.98216	1.00899
47	1.2852*-02	8.4094*+01	NM	0.98604	0.99993	0.99299	0.98617	1.00692
48	1.3132*-02	8.4101*+01	NM	0.99002	0.99997	0.99499	0.99008	1.00496
49	1.3411*-02	8.4099*+01	NM	0.99501	0.99996	0.99750	0.99509	1.00242
D 50	1.3691*-02	8.4106*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
51	1.3970*-02	8.4106*+01	NM	1.00200	1.00000	1.00100	1.00200	0.99900

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PO

68010502		PERRY		PROFILE TABULATION		51 POINTS, DELTA AT POINT 49			
I	Y	PT2/P	P/PPD	TQ/TOD	H/HO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.31868	0.00000	0.00000	7.48010	0.00000	
2	5.0000 ⁺ -04	1.5875 ⁺ +00	NM	0.41980	0.07926	0.23290	8.63460	0.02697	
3	1.0100 ⁺ -03	4.1376 ⁺ +00	NM	0.50328	0.15848	0.43550	7.55100	0.05767	
4	1.5240 ⁺ -03	8.3989 ⁺ +00	NM	0.57365	0.23397	0.57490	6.03750	0.09522	
5	2.0320 ⁺ -03	1.1831 ⁺ +01	NM	0.62639	0.28017	0.64620	5.31880	0.12149	
6	2.5400 ⁺ -03	1.3328 ⁺ +01	NM	0.66810	0.29810	0.68190	5.23250	0.13032	
7	3.0480 ⁺ -03	1.5354 ⁺ +01	NM	0.69781	0.32076	0.71330	4.94530	0.14424	
8	3.5560 ⁺ -03	1.7158 ⁺ +01	NM	0.72533	0.33964	0.73940	4.73930	0.15601	
9	4.0640 ⁺ -03	1.9254 ⁺ +01	NM	0.73139	0.36036	0.75790	4.42340	0.17134	
10	4.5720 ⁺ -03	2.1793 ⁺ +01	NM	0.75598	0.38394	0.77880	4.11450	0.18928	
11	5.0800 ⁺ -03	2.4312 ⁺ +01	NM	0.77029	0.39999	0.79340	3.93450	0.20165	
12	5.5880 ⁺ -03	2.6306 ⁺ +01	NM	0.78348	0.42263	0.80940	3.66780	0.22068	
13	6.0960 ⁺ -03	2.8303 ⁺ +01	NM	0.79224	0.43866	0.81980	3.49270	0.23472	
14	6.6040 ⁺ -03	3.1130 ⁺ +01	NM	0.80225	0.46040	0.83220	3.26730	0.25471	
15	7.1120 ⁺ -03	3.4348 ⁺ +01	NM	0.81098	0.48396	0.84370	3.03920	0.27761	
16	7.6200 ⁺ -03	3.6632 ⁺ +01	NM	0.81868	0.50000	0.85200	2.90360	0.29343	
17	8.1280 ⁺ -03	4.0120 ⁺ +01	NM	0.82630	0.52356	0.86170	2.70880	0.31811	
18	8.6360 ⁺ -03	4.3476 ⁺ +01	NM	0.83292	0.54527	0.86990	2.54520	0.34178	
19	9.1440 ⁺ -03	4.6811 ⁺ +01	NM	0.84170	0.56661	0.87860	2.40950	0.36464	
20	9.6520 ⁺ -03	5.0279 ⁺ +01	NM	0.84619	0.58681	0.88470	2.27300	0.38922	
21	1.0160 ⁺ -02	5.3207 ⁺ +01	NM	0.85283	0.60381	0.89100	2.17750	0.40918	
22	1.0660 ⁺ -02	5.6551 ⁺ +01	NM	0.86047	0.62266	0.89790	2.07950	0.43179	
23	1.1170 ⁺ -02	6.0698 ⁺ +01	NM	0.86868	0.64527	0.90450	1.96490	0.46033	
24	1.1680 ⁺ -02	6.4822 ⁺ +01	NM	0.87366	0.66699	0.91080	1.86470	0.48844	
25	1.2190 ⁺ -02	6.8507 ⁺ +01	NM	0.88123	0.68582	0.91700	1.78780	0.51292	
26	1.2700 ⁺ -02	7.2305 ⁺ +01	NM	0.88680	0.70470	0.92200	1.71180	0.53861	
27	1.3200 ⁺ -02	7.7195 ⁺ +01	NM	0.89117	0.72829	0.92670	1.61910	0.57236	
28	1.3710 ⁺ -02	8.1426 ⁺ +01	NM	0.89774	0.74809	0.93200	1.55210	0.60048	
29	1.4220 ⁺ -02	8.5565 ⁺ +01	NM	0.90222	0.76698	0.93600	1.48930	0.62848	
30	1.4730 ⁺ -02	9.0241 ⁺ +01	NM	0.91106	0.78777	0.94230	1.43080	0.65858	
31	1.5240 ⁺ -02	9.6352 ⁺ +01	NM	0.91644	0.81414	0.94710	1.35330	0.69984	
32	1.5748 ⁺ -02	1.0107 ⁺ +02	NM	0.92302	0.83394	0.95190	1.30290	0.73060	
33	1.6256 ⁺ -02	1.0522 ⁺ +02	NM	0.92974	0.85097	0.95650	1.26340	0.75708	
34	1.6764 ⁺ -02	1.0944 ⁺ +02	NM	0.93407	0.86793	0.95980	1.22290	0.78486	
35	1.7272 ⁺ -02	1.1422 ⁺ +02	NM	0.93947	0.88674	0.96370	1.18110	0.81593	
36	1.7780 ⁺ -02	1.1917 ⁺ +02	NM	0.94536	0.90583	0.96780	1.14150	0.84783	
37	1.8288 ⁺ -02	1.2286 ⁺ +02	NM	0.95270	0.91981	0.97230	1.11740	0.87014	
38	1.8796 ⁺ -02	1.3110 ⁺ +02	NM	0.95996	0.95027	0.97520	1.09680	0.90737	
39	1.9304 ⁺ -02	1.2870 ⁺ +02	NM	0.95935	0.94150	0.97680	1.07640	0.90747	
40	1.9812 ⁺ -02	1.3206 ⁺ +02	NM	0.96486	0.95377	0.98020	1.05620	0.92804	
41	2.0320 ⁺ -02	1.3441 ⁺ +02	NM	0.96919	0.96224	0.98280	1.04320	0.94210	
42	2.0828 ⁺ -02	1.3705 ⁺ +02	NM	0.97465	0.97168	0.98600	1.02970	0.95756	
43	2.1336 ⁺ -02	1.3946 ⁺ +02	NM	0.97804	0.98019	0.98810	1.01620	0.97235	
44	2.1844 ⁺ -02	1.4080 ⁺ +02	NM	0.98238	0.98490	0.99050	1.01140	0.97934	
45	2.2352 ⁺ -02	1.4240 ⁺ +02	NM	0.98785	0.99053	0.99350	1.00600	0.98757	
46	2.2860 ⁺ -02	1.4323 ⁺ +02	NM	0.98899	0.99341	0.99420	1.00160	0.99261	
47	2.3368 ⁺ -02	1.4403 ⁺ +02	NM	0.99334	0.99620	0.99650	1.00060	0.99590	
48	2.3876 ⁺ -02	1.4487 ⁺ +02	NM	0.99788	0.99910	0.99890	0.99960	0.99930	
D 49	2.4384 ⁺ -02	1.4513 ⁺ +02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
50	2.4892 ⁺ -02	1.4513 ⁺ +02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
51	2.5400 ⁺ -02	1.4513 ⁺ +02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

68010503		PERRY		PROFILE TABULATION		51 POINTS, DELTA AT POINT 48			
I	Y	PT2/P	P/PD	T0/T0D	H/H0D	U/UD	T/TD	RHO/RHO0+U/UD	
1	0.3000+00	1.0000+00	NM	0.31349	0.00000	0.00000	8.40895	0.00000	
2	5.8420-04	1.4133+00	NM	0.42510	0.06395	0.20392	10.16750	0.02006	
3	1.1684-03	3.3434+00	NM	0.51647	0.13144	0.40464	9.47671	0.04270	
4	1.7526-03	7.4834+00	NM	0.58587	0.20691	0.56324	7.40975	0.07601	
5	2.3368-03	1.2081+01	NM	0.62668	0.26642	0.64729	5.90286	0.10966	
6	2.9210-03	1.4947+01	NM	0.66199	0.29752	0.69011	5.38017	0.12827	
7	3.5052-03	1.7843+01	NM	0.68954	0.32595	0.72313	4.92195	0.14692	
8	4.0894-03	1.9783+01	NM	0.71035	0.34367	0.74415	4.68839	0.15872	
9	4.6736-03	2.2149+01	NM	0.72692	0.36412	0.76326	4.39396	0.17371	
10	5.2578-03	2.4765+01	NM	0.74133	0.38546	0.78047	4.09964	0.19037	
11	5.8420-03	2.7055+01	NM	0.75565	0.40322	0.79518	3.88297	0.20447	
12	6.4262-03	2.9321+01	NM	0.76854	0.42006	0.80709	3.69168	0.21862	
13	7.0104-03	3.2201+01	NM	0.77549	0.44053	0.81859	3.45293	0.23707	
14	7.5946-03	3.4673+01	NM	0.78640	0.45736	0.82940	3.28853	0.25221	
15	8.1788-03	3.8493+01	NM	0.79740	0.48223	0.84191	3.04807	0.27621	
16	8.7630-03	4.1636+01	NM	0.80290	0.50176	0.84951	2.86648	0.29636	
17	9.3472-03	4.4906+01	NM	0.81394	0.52131	0.85962	2.71907	0.31614	
18	9.9314-03	4.7990+01	NM	0.81952	0.53907	0.86612	2.58125	0.33554	
19	1.0516+02	5.1986+01	NM	0.82834	0.56130	0.87482	2.42914	0.36014	
20	1.1100+02	5.5127+01	NM	0.83382	0.57816	0.88053	2.31951	0.37962	
21	1.1684+02	5.8881+01	NM	0.84368	0.59768	0.88873	2.21107	0.40195	
22	1.2268+02	6.2942+01	NM	0.84808	0.61811	0.89394	2.09165	0.42738	
23	1.2852+02	6.6589+01	NM	0.85564	0.63589	0.90034	2.00470	0.44912	
24	1.3437+02	7.0526+01	NM	0.86354	0.65454	0.90664	1.91865	0.47254	
25	1.4021+02	7.4568+01	NM	0.87119	0.67316	0.91275	1.83850	0.49646	
26	1.4605+02	7.9546+01	NM	0.87786	0.69540	0.91855	1.74475	0.52646	
27	1.5189+02	8.3627+01	NM	0.88551	0.71312	0.92425	1.67979	0.55022	
28	1.5773+02	8.7411+01	NM	0.89002	0.72917	0.92806	1.61993	0.57299	
29	1.6358+02	9.1910+01	NM	0.89987	0.74779	0.93476	1.56256	0.59822	
30	1.6942+02	9.6310+01	NM	0.90543	0.76557	0.93906	1.50460	0.62413	
31	1.7526+02	1.0171+02	NM	0.91300	0.78683	0.94457	1.44114	0.65543	
32	1.8110+02	1.0565+02	NM	0.91753	0.80199	0.94797	1.39716	0.67850	
33	1.8694+02	1.1011+02	NM	0.92409	0.81882	0.95247	1.35309	0.70392	
34	1.9279+02	1.1589+02	NM	0.92851	0.84014	0.95607	1.29502	0.73827	
35	1.9863+02	1.2032+02	NM	0.93505	0.85610	0.96038	1.25844	0.76315	
36	2.0447+02	1.2611+02	NM	0.93948	0.87653	0.96378	1.20897	0.79719	
37	2.1031+02	1.3337+02	NM	0.98377	0.90828	0.98789	1.18299	0.83508	
38	2.1615+02	1.3493+02	NM	0.95170	0.90679	0.97156	1.14801	0.84632	
39	2.2200+02	1.3891+02	NM	0.95830	0.92011	0.97559	1.12423	0.86778	
40	2.2784+02	1.4431+02	NM	0.96378	0.93787	0.97919	1.09005	0.89830	
41	2.3368+02	1.4731+02	NM	0.96806	0.94760	0.98179	1.07346	0.91461	
42	2.3952+02	1.5117+02	NM	0.97353	0.95999	0.98509	1.05297	0.93554	
43	2.4536+02	1.5428+02	NM	0.97589	0.96983	0.98669	1.03508	0.95325	
44	2.5121+02	1.5739+02	NM	0.97907	0.97958	0.98869	1.01869	0.97055	
45	2.5705+02	1.5966+02	NM	0.98567	0.98664	0.99230	1.01149	0.98102	
46	2.6289+02	1.6167+02	NM	0.99116	0.99287	0.99530	1.00490	0.99045	
47	2.6873+02	1.6313+02	NM	0.99560	0.99735	0.99770	1.00070	0.99700	
48	2.7457+02	1.6400+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
49	2.8042+02	1.6429+02	NM	1.00113	1.00090	1.00060	0.99940	1.00120	
50	2.8626+02	1.6429+02	NM	1.00113	1.00090	1.00060	0.99940	1.00120	
51	2.9210+02	1.6429+02	NM	1.00113	1.00090	1.00060	0.99940	1.00120	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

68010901


PERRY

PROFILE TABULATION

51 POINTS, DELTA AT POINT 50

I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.26033	0.00000	0.00000	5.67736	0.00000
2	4.0840 ⁻⁰⁴	2.4963 ⁺⁰⁰	NM	0.34562	0.12059	0.29008	5.78635	0.05013
3	8.1280 ⁻⁰⁴	1.0498 ⁺⁰¹	NM	0.43540	0.27354	0.52712	3.71355	0.14195
4	1.2192 ⁻⁰³	1.3985 ⁺⁰¹	NM	0.52511	0.31763	0.61055	3.69495	0.16524
5	1.0256 ⁻⁰³	1.6697 ⁺⁰¹	NM	0.57995	0.34805	0.65968	3.59230	0.18364
6	2.0320 ⁻⁰³	1.8768 ⁺⁰¹	NM	0.61402	0.36960	0.68996	3.48482	0.19799
7	2.4384 ⁻⁰³	2.1069 ⁺⁰¹	NM	0.64278	0.39217	0.71643	3.33742	0.21467
8	2.8448 ⁻⁰³	2.3503 ⁺⁰¹	NM	0.67413	0.41469	0.74311	3.21114	0.23142
9	3.2512 ⁻⁰³	2.5965 ⁺⁰¹	NM	0.69399	0.43630	0.76206	3.05077	0.24979
10	3.6576 ⁻⁰³	2.7707 ⁺⁰¹	NM	0.71181	0.45095	0.77680	2.96722	0.26179
11	4.0640 ⁻⁰³	3.0130 ⁺⁰¹	NM	0.72532	0.47058	0.79033	2.82063	0.28020
12	4.4704 ⁻⁰³	3.2015 ⁺⁰¹	NM	0.73795	0.48531	0.80146	2.72733	0.29386
13	4.8768 ⁻⁰³	3.4479 ⁺⁰¹	NM	0.75223	0.50391	0.81420	2.61070	0.31187
14	5.2832 ⁻⁰³	3.6907 ⁺⁰¹	NM	0.76307	0.52158	0.82643	2.49839	0.32998
15	5.6896 ⁻⁰³	3.9131 ⁺⁰¹	NM	0.77295	0.53727	0.83335	2.40589	0.34638
16	6.0960 ⁻⁰³	4.1709 ⁺⁰¹	NM	0.78367	0.55489	0.84288	2.30736	0.36330
17	6.5024 ⁻⁰³	4.4228 ⁺⁰¹	NM	0.79450	0.57158	0.85200	2.22190	0.38346
18	6.9088 ⁻⁰³	4.6354 ⁺⁰¹	NM	0.80435	0.58530	0.85982	2.15805	0.39842
19	7.3152 ⁻⁰³	4.9313 ⁺⁰¹	NM	0.81144	0.60388	0.86684	2.06053	0.42069
20	7.7216 ⁻⁰³	5.1891 ⁺⁰¹	NM	0.81869	0.61961	0.87326	1.98633	0.43963
21	8.1280 ⁻⁰³	5.4528 ⁺⁰¹	NM	0.82589	0.63529	0.87947	1.91645	0.45891
22	8.5344 ⁻⁰³	5.7738 ⁺⁰¹	NM	0.83298	0.65389	0.88589	1.83551	0.48264
23	8.9408 ⁻⁰³	5.9993 ⁺⁰¹	NM	0.84016	0.66663	0.89141	1.78906	0.49853
24	9.3472 ⁻⁰³	6.3191 ⁺⁰¹	NM	0.84920	0.68431	0.89843	1.72371	0.52122
25	9.7536 ⁻⁰³	6.6285 ⁺⁰¹	NM	0.85551	0.70098	0.90374	1.66218	0.54371
26	1.0150 ⁻⁰²	6.9075 ⁺⁰¹	NM	0.86361	0.71568	0.90766	1.61552	0.56307
27	1.0566 ⁻⁰²	7.1931 ⁺⁰¹	NM	0.86902	0.73042	0.91407	1.56606	0.58367
28	1.0973 ⁻⁰²	7.5030 ⁺⁰¹	NM	0.87441	0.74609	0.91848	1.51548	0.60606
29	1.1379 ⁻⁰²	7.8204 ⁺⁰¹	NM	0.88342	0.76181	0.92470	1.47336	0.62761
30	1.1786 ⁻⁰²	8.1426 ⁺⁰¹	NM	0.89050	0.77743	0.92981	1.43042	0.65002
31	1.2192 ⁻⁰²	8.4733 ⁺⁰¹	NM	0.89502	0.79315	0.93352	1.38528	0.67389
32	1.2598 ⁻⁰²	8.7881 ⁺⁰¹	NM	0.90216	0.80783	0.93843	1.34949	0.69540
33	1.3005 ⁻⁰²	9.1089 ⁺⁰¹	NM	0.90574	0.82252	0.94144	1.31007	0.71862
34	1.3411 ⁻⁰²	9.4798 ⁺⁰¹	NM	0.91380	0.83918	0.94666	1.27307	0.74376
35	1.3818 ⁻⁰²	9.8370 ⁺⁰¹	NM	0.92019	0.85492	0.95127	1.23809	0.76834
36	1.4224 ⁻⁰²	1.0130 ⁺⁰²	NM	0.92552	0.86763	0.95488	1.21124	0.78835
37	1.4630 ⁻⁰²	1.0429 ⁺⁰²	NM	0.93092	0.88038	0.95849	1.18530	0.80865
38	1.5037 ⁻⁰²	1.0778 ⁺⁰²	NM	0.93890	0.89507	0.96350	1.15876	0.83150
39	1.5443 ⁻⁰²	1.1231 ⁺⁰²	NM	0.94319	0.91378	0.96681	1.11945	0.86365
40	1.5850 ⁻⁰²	1.1471 ⁺⁰²	NM	0.94975	0.92351	0.97072	1.10487	0.87859
41	1.6256 ⁻⁰²	1.1741 ⁺⁰²	NM	0.95428	0.93434	0.97363	1.08586	0.89664
42	1.6662 ⁻⁰²	1.2062 ⁺⁰²	NM	0.96062	0.94708	0.97754	1.06535	0.91757
43	1.7069 ⁻⁰²	1.2236 ⁺⁰²	NM	0.96504	0.95394	0.98015	1.05570	0.92843
44	1.7475 ⁻⁰²	1.2538 ⁺⁰²	NM	0.97039	0.96566	0.98346	1.03720	0.94818
45	1.7882 ⁻⁰²	1.2742 ⁺⁰²	NM	0.97577	0.97353	0.98656	1.02695	0.96088
46	1.8288 ⁻⁰²	1.2923 ⁺⁰²	NM	0.98126	0.98045	0.98967	1.01890	0.97131
47	1.8694 ⁻⁰²	1.3128 ⁺⁰²	NM	0.98650	0.98822	0.99268	1.00905	0.98378
48	1.9101 ⁻⁰²	1.3285 ⁺⁰²	NM	0.98934	0.99413	0.99438	1.00050	0.99389
49	1.9507 ⁻⁰²	1.3388 ⁺⁰²	NM	0.99458	0.99800	0.99719	0.99839	0.99880
50	1.9914 ⁻⁰²	1.3442 ⁺⁰²	NM	1.00000	1.00000	1.00000	1.00000	1.00000
51	2.0320 ⁻⁰²	1.3442 ⁺⁰²	NM	1.00542	1.00000	1.00271	1.00543	0.99729

INPUT VARIABLES Y,U/UD,T/TD ASSUME P8PD

axisymmetric 	M : Subsonic to 4.4 R THETA X 10 ⁻³ : 0.6 - 7.0 TW/TR : 0.85 to 0.65	6901
		FPG SHT (TEMP. HISTORY)
Special purpose rig. Continuous running. D = (inlet) 0.165 m, (throat) 37.85 mm. PO : 2.1 MN/m ² . TO : 540 K. Air: RE/m X 10 ⁻⁶ of order 50.		
BOLDMAN D.R., SCHMIDT J.F. and EHLERS R.C. 1969. Experimental and theoretical turbulent boundary layer development in a Mach 4.4 water-cooled conical nozzle. NASA TN D-5377. And Boldman, Schmidt and Fortini (1966), Boldman, Schmidt and Gallagher (1968), Boldman and Graham (1972) and extensive supporting bibliography (see references), Boldman D.R., private communications.		

- 1 The test boundary layer was formed in a conical convergent-divergent nozzle and one of two cylindrical inlet-passages leading to it. The inlets were 0.165 m diameter and met the conical convergence with no fairing. The 30° semiangle convergence was faired into the throat (X = 0, D = 37.85 mm) by a part of the wall having a constant radius in longitudinal direction of 37.85 mm. This circular contour was carried through the throat until the tangent point (X = 10.16 mm) with the 15° semi angle divergent section, which ran from this point to X = 0.280 m where the diameter was 0.186 m. Provision was made for boundary layer traverses in the cylindrical inlet, the convergence, and at three stations in the divergence. The test surfaces were machine-turned to a finish of 1.6 μm rms, and both the nozzle and one of the inlet cylinders could be actively cooled. The earlier tests (1966, 1968) showed that the boundary layer became turbulent after natural transition very near the start of the inlet sections. Of these one (series 01) was uncooled, and ran from X = -0.552 to X = -0.120 m the start of the convergent portion. The other (series 02) was 0.955 m long (X = -1.075 to -0.120 m) and actively cooled by water passages from X = -0.734 m. The upstream edges of the inlets were machined to give a leading edge radius of 0.76 mm and a boundary layer bleed bypass outside the inlets ensured that the experimental boundary layer started at this leading edge. The wall temperature and pressure history for the nozzle itself is presented in section D.
- 6 Static pressure was measured by tappings of 0.79 mm diameter at the points indicated in the wall data table of section D. The wall temperature and heat flux rate were measured with a plug type heat flux meter. A conducting rod of constant cross section is placed in a cavity in the wall so shaped that it is in thermal contact with the wall at the test surface and insulated elsewhere by the cavity. The temperature gradient in the plug then gives the heat flux, and can be extrapolated to give the test surface temperature (Boldman et al. 1967). Uncertainty in correction procedures to allow for the local distortion of the heat flux pattern is believed to give a residual uncertainty of 10 % in heat flux.
- 7 Boundary layer profiles were measured with TPP and TTP. The FPP were constructed from tubing (d₁ = 0.711, d₂ = 0.355 mm) flattened to give a rectangular opening (h₂ = 0.051, b₂ = 0.76 mm) and ground down so as to have a sharp lip. The overall probe lengths were 19 and 15.2 mm for the subsonic and supersonic profiles respectively. About the last 5 mm (E) of the tube was unsupported. The TTP for the subsonic profiles consisted of an unshielded Chromel-Alumel thermocouple bead 0.13 mm in diameter mounted at the end of a short cylindrical support (d = 0.35, l = 2.5 mm). This in turn was mounted in a conical (15°) housing. For the supersonic profiles, the bead size was reduced to 0.08 mm and the diameter of the support to 0.2 mm. The overall lengths were as for the TPP. The profiles were obtained normal to the conical surfaces of the nozzle at the X-stations indicated in section B. At any given value of X the Pitot and TO profiles were obtained on opposite sides of the nozzle.
- 9 The calibration procedure for the TTP is described in an appendix to the source paper. The authors have interpolated the TO data to the Y values of the Pitot data, and PW and TW values to the profile position.
- 12 The editors have accepted the authors' calibration and interpolation procedures. For one of the profiles (0101) the data was received in raw form and interpolated by the editors. In data reduction for this profile the input values of T/TD were assumed, for computing reasons, equal to the measured value of TO/TOD.

- Resulting error is less than 0.13 %. The wall data is presented in normalised form from the tables in Boldman & Graham (1972), so that the profile wall temperatures do not agree with the values in Section D. These differences are caused by seasonal variations in the temperature of the cooling water supply. The
- 13 two sets of profile data are differentiated by their upstream thermal history. For series 01 the inlet duct was not cooled, and the flow in this region was near adiabatic. For series 02 a cooled inlet duct was used. All measurements are taken in the nozzle itself, which is actively cooled. In each series one
- 14 profile is in the subsonic, convergent, part of the nozzle and three are in the divergent part. The wall data with the profiles are scaled to the wall temperature of the profile. Full normalised data is given in section D.
- 5 DATA: 6901 0101-0204. Pitot and TD profiles. $MX = 4$. Heat flux from conduction measurements in the nozzle wall.

15 Editors' comments

This entry is included principally as a challenge for calculation methods. The state of the boundary layer in the contraction is described, and there is very complete wall temperature and pressure information for the flow through to the three measuring stations in the conical expansion. Series 02 is very similar to the CW case of Back et al. (7207 series 01), and series 01 provides an interesting difference in the upstream history.

The experiments form part of a continuing study into which many other effects are introduced - wall roughness etc. There is a large number of reports concerned with the tests, and the normalisation procedures vary from one to the next. We believe that the data given with the profiles is appropriate to the test conditions in each case, but repeat that the extended wall data tables are differently normalised.

Note added in proof. We remain uncertain of the proper free stream conditions at the first station. For profile 0101 the Mach number corresponds to the wall data given in section D, while for profile 0201 the free stream velocity was taken as stated in figure 7a of NASA TN D-4788. The Mach numbers in the two cases should be in close agreement, and we have not yet reconciled the conflict. The dimensionless profile data is not affected by this discrepancy.

CAT 6901		BOLDMAN		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUI	MD *	TW/TR	RED2W	CF	M12	M12K	PW	PD		
X *	POD*	PW/PD*	RED2O	CQ *	M32	M32K	TW*	TD		
RZ *	TUD*	SW *	D2	PI2	H42	D2K	UD	TR		
69010101	0.0789	0.7463	1.2920 ⁺⁰³	NM	0.0306	1.2651	2.0594 ⁺⁰⁶	2.0594 ⁺⁰⁶		
-6.3800 ⁻⁰²	2.0684 ⁺⁰⁶	1.0000	1.0537 ⁺⁰³	NC	1.9442	1.9485	4.0080 ⁺⁰²	5.3642 ⁺⁰²		
-4.9960 ⁻⁰²	5.3709 ⁺⁰²	0.0000	6.0592 ⁻⁰⁵	NC	1.1721	5.6663 ⁻⁰⁵	3.6657 ⁺⁰¹	5.3702 ⁺⁰²		
69010102	2.1000	0.8507	4.5980 ⁺⁰³	NM	1.4683	1.4852	2.2619 ⁺⁰⁵	2.2619 ⁺⁰⁵		
3.1010 ⁻⁰²	2.0684 ⁺⁰⁶	1.0000	6.2829 ⁺⁰³	1.4197 ⁻⁰⁴	1.8548	1.8400	4.3778 ⁺⁰²	2.8746 ⁺⁰²		
-2.5935 ⁻⁰²	5.4100 ⁺⁰²	0.0000	5.7545 ⁻⁰⁵	NC	0.9550	6.3224 ⁻⁰⁵	7.1387 ⁺⁰²	5.1463 ⁺⁰²		
69010103	3.7000	0.7107	2.9339 ⁺⁰³	NM	4.7431	1.3428	2.0483 ⁺⁰⁴	2.0483 ⁺⁰⁴		
1.3889 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	6.1393 ⁺⁰³	2.4985 ⁻⁰⁴	1.0371	1.8160	3.5389 ⁺⁰²	1.4419 ⁺⁰²		
-5.4890 ⁻⁰²	5.3900 ⁺⁰²	0.0000	1.3970 ⁻⁰⁴	NC	0.6058	2.0432 ⁻⁰⁴	8.9081 ⁺⁰²	4.9794 ⁺⁰²		
69010104	4.4000	0.6404	3.1127 ⁺⁰³	NM	5.9197	1.3753	8.1033 ⁺⁰³	8.1033 ⁺⁰³		
1.3889 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	7.6571 ⁺⁰³	2.6476 ⁻⁰⁴	1.8280	1.7942	3.1667 ⁺⁰²	1.1063 ⁺⁰²		
-8.2600 ⁻⁰²	5.3900 ⁺⁰²	0.0000	2.5384 ⁻⁰⁴	NC	0.7138	4.2262 ⁻⁰⁴	9.2790 ⁺⁰²	4.9445 ⁺⁰²		
69010201	0.0307	0.6205	3.7287 ⁺⁰³	NM	0.8665	1.1891	2.0671 ⁺⁰⁶	2.0671 ⁺⁰⁶		
-6.3800 ⁻⁰²	2.0684 ⁺⁰⁶	1.0000	2.6535 ⁺⁰³	NC	1.8670	1.8707	3.3510 ⁺⁰²	5.3995 ⁺⁰²		
-4.9960 ⁻⁰²	5.4005 ⁺⁰²	0.0000	3.9401 ⁻⁰⁴	NC	0.2657	3.7568 ⁻⁰⁴	1.4300 ⁺⁰¹	5.4004 ⁺⁰²		
69010202	2.1000	0.8338	7.9357 ⁺⁰³	NM	0.5650	1.3556	2.2619 ⁺⁰⁵	2.2619 ⁺⁰⁵		
3.1010 ⁻⁰²	2.0684 ⁺⁰⁶	1.0000	1.0692 ⁺⁰⁴	1.1293 ⁻⁰⁴	1.8859	1.8695	4.2833 ⁺⁰²	2.8693 ⁺⁰²		
-2.5935 ⁻⁰²	5.4000 ⁺⁰²	0.0000	9.7700 ⁻⁰⁵	NC	1.3364	1.0231 ⁻⁰⁴	7.1321 ⁺⁰²	5.1368 ⁺⁰²		
69010203	3.6000	0.7028	6.1900 ⁺⁰³	NM	1.8924	1.2574	2.3548 ⁺⁰⁴	2.3548 ⁺⁰⁴		
1.3889 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	1.2397 ⁺⁰⁴	2.0291 ⁻⁰⁴	1.8923	1.8620	3.5167 ⁺⁰²	1.5061 ⁺⁰²		
-5.4890 ⁻⁰²	5.4100 ⁺⁰²	0.0000	2.6804 ⁻⁰⁴	NC	1.2653	3.2784 ⁻⁰⁴	8.8581 ⁺⁰²	5.0040 ⁺⁰²		
69010204	4.5000	0.6432	4.3092 ⁺⁰³	NM	3.8684	1.3012	7.1469 ⁺⁰³	7.1469 ⁺⁰³		
2.4179 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	1.0997 ⁺⁰⁴	2.4071 ⁻⁰⁴	1.8718	1.8265	3.1778 ⁺⁰²	1.0673 ⁺⁰²		
-8.2500 ⁻⁰²	5.3900 ⁺⁰²	0.0000	3.6367 ⁻⁰⁴	NC	1.1207	5.7179 ⁻⁰⁴	9.3212 ⁺⁰²	4.9404 ⁺⁰²		

TRAPEZOIDAL RULE FOR ALL INTEGRATIONS - FOR 0201 UD FROM NASA TN D-4788 FIG.7A

69010101		BOLDMAN		PROFILE TABULATION		22 POINTS, DELTA AT POINT 32			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.74531	0.00000	0.00000	0.74624	0.00000	
2	2.5400 ⁻ -05	1.0032 ⁺ +00	NM	0.80589	0.85537	0.76800	0.86615	0.95267	
3	3.5560 ⁻ -05	1.0036 ⁺ +00	NM	0.81631	0.90194	0.81500	0.81650	0.99816	
4	5.0800 ⁻ -05	1.0038 ⁺ +00	NM	0.83188	0.93187	0.85000	0.83201	1.02162	
5	6.3500 ⁻ -05	1.0040 ⁺ +00	NM	0.84020	0.95454	0.87500	0.84029	1.04131	
6	7.6200 ⁻ -05	1.0042 ⁺ +00	NM	0.84748	0.97761	0.90000	0.84753	1.06191	
7	9.1440 ⁻ -05	1.0042 ⁺ +00	NM	0.85990	0.97915	0.90800	0.85994	1.05588	
8	1.0160 ⁻ -04	1.0042 ⁺ +00	NM	0.86611	0.98209	0.91400	0.86615	1.05525	
9	1.5240 ⁻ -04	1.0042 ⁺ +00	NM	0.89405	0.98566	0.93200	0.89408	1.04242	
10	1.7780 ⁻ -04	1.0042 ⁺ +00	NM	0.90749	0.98568	0.93900	0.90752	1.03468	
11	2.2860 ⁻ -04	1.0043 ⁺ +00	NM	0.92923	0.99380	0.95800	0.92925	1.03094	
12	3.0480 ⁻ -04	1.0042 ⁺ +00	NM	0.95404	0.98488	0.96200	0.95407	1.00831	
13	3.5560 ⁻ -04	1.0043 ⁺ +00	NM	0.96438	0.98672	0.96900	0.96442	1.00475	
14	4.0640 ⁻ -04	1.0042 ⁺ +00	NM	0.97058	0.98457	0.97000	0.97062	0.99936	
15	5.8420 ⁻ -04	1.0043 ⁺ +00	NM	0.97785	0.99406	0.98300	0.97786	1.00525	
16	8.3820 ⁻ -04	1.0043 ⁺ +00	NM	0.98404	0.98992	0.98200	0.98407	0.99790	
17	1.0414 ⁻ -03	1.0043 ⁺ +00	NM	0.98714	0.98836	0.98200	0.98717	0.99476	
18	1.1176 ⁻ -03	1.0043 ⁺ +00	NM	0.98715	0.99037	0.98400	0.98717	0.99679	
19	1.2954 ⁻ -03	1.0043 ⁺ +00	NM	0.98818	0.98885	0.98300	0.98821	0.99473	
20	1.5748 ⁻ -03	1.0043 ⁺ +00	NM	0.98922	0.99135	0.98600	0.98924	0.99672	
21	1.8542 ⁻ -03	1.0044 ⁺ +00	NM	0.99131	0.99835	0.99400	0.99131	1.00271	
D 22	5.0800 ⁻ -03	1.0044 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UE,T0 ASSUME T/TD = T0/T00 AND P=PO

69010102		BOLDMAN		PROFILE TABULATION		25 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.80921	0.00000	0.00000	1.52292	0.00000	
2	3.2000 ⁻ -05	2.1328 ⁺ +00	NM	0.87431	0.52381	0.60291	1.32484	0.45508	
3	6.2000 ⁻ -05	2.4075 ⁺ +00	NM	0.86355	0.57143	0.64928	1.29102	0.50292	
4	8.8000 ⁻ -05	3.0492 ⁺ +00	NM	0.89094	0.66667	0.73168	1.20456	0.60743	
5	1.1300 ⁻ -04	3.4133 ⁺ +00	NM	0.89834	0.71429	0.77129	1.16598	0.66150	
6	1.6400 ⁻ -04	4.2238 ⁺ +00	NM	0.91312	0.80952	0.84479	1.08904	0.77573	
7	2.1500 ⁻ -04	5.1418 ⁺ +00	NM	0.92606	0.90476	0.91022	1.01211	0.89933	
8	2.2700 ⁻ -04	5.1418 ⁺ +00	NM	0.92976	0.90476	0.91204	1.01615	0.89734	
9	2.4000 ⁻ -04	5.1418 ⁺ +00	NM	0.93346	0.90476	0.91385	1.02019	0.89576	
10	2.5300 ⁻ -04	5.6404 ⁺ +00	NM	0.93715	0.95238	0.94273	0.97985	0.96213	
11	2.6500 ⁻ -04	5.1418 ⁺ +00	NM	0.94085	0.90476	0.91746	1.02827	0.89224	
12	2.7800 ⁻ -04	5.1418 ⁺ +00	NM	0.94455	0.90476	0.91926	1.03231	0.89049	
13	2.9100 ⁻ -04	5.1418 ⁺ +00	NM	0.94824	0.90476	0.92106	1.03635	0.88875	
14	3.0400 ⁻ -04	5.1418 ⁺ +00	NM	0.95009	0.90476	0.92196	1.03837	0.88789	
15	3.1600 ⁻ -04	5.1418 ⁺ +00	NM	0.95144	0.90476	0.92285	1.04039	0.88703	
16	3.4200 ⁻ -04	5.6404 ⁺ +00	NM	0.95564	0.95238	0.95199	0.99917	0.95278	
17	3.6700 ⁻ -04	5.6404 ⁺ +00	NM	0.95933	0.95238	0.95383	1.00304	0.95094	
18	3.9200 ⁻ -04	5.6404 ⁺ +00	NM	0.96118	0.95238	0.95474	1.00497	0.95002	
19	4.1800 ⁻ -04	5.6404 ⁺ +00	NM	0.96488	0.95238	0.95658	1.00884	0.94820	
20	4.6900 ⁻ -04	6.1654 ⁺ +00	NM	0.97227	1.00000	0.98604	0.97227	1.01416	
21	5.1900 ⁻ -04	6.1654 ⁺ +00	NM	0.97782	1.00000	0.98885	0.97782	1.01128	
22	5.3200 ⁻ -04	6.1654 ⁺ +00	NM	0.97967	1.00000	0.98978	0.97967	1.01032	
23	1.0270 ⁻ -03	6.1654 ⁺ +00	NM	0.99076	1.00000	0.99537	0.99076	1.00465	
24	4.8200 ⁻ -03	6.1654 ⁺ +00	NM	0.99815	1.00000	0.99908	0.99815	1.00093	
D 25	8.6300 ⁻ -03	6.1654 ⁺ +00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,M ASSUME P=PO

69010103		BOLDMAN		PROFILE TABULATION		31 POINTS, DELTA AT POINT 31			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.65657	0.00000	0.00000	2.45425	0.00000	
2	3.2000 ⁻⁰⁵	2.4075 ⁺⁰⁰	NM	0.76252	0.32432	0.48247	2.21297	0.21802	
3	4.4000 ⁻⁰⁵	2.7136 ⁺⁰⁰	NM	0.77365	0.35135	0.51654	2.16138	0.23899	
4	5.7000 ⁻⁰⁵	3.0492 ⁺⁰⁰	NM	0.78479	0.37838	0.54929	2.10742	0.26065	
5	7.0000 ⁻⁰⁵	3.4133 ⁺⁰⁰	NM	0.79406	0.40541	0.58003	2.04764	0.28335	
6	8.3000 ⁻⁰⁵	3.8050 ⁺⁰⁰	NM	0.80519	0.43243	0.61012	1.99062	0.30650	
7	9.5000 ⁻⁰⁵	4.2238 ⁺⁰⁰	NM	0.81633	0.45946	0.63892	1.93373	0.33041	
8	1.0800 ⁻⁰⁴	4.6695 ⁺⁰⁰	NM	0.82746	0.48649	0.66844	1.86010	0.35218	
9	1.2100 ⁻⁰⁴	4.6695 ⁺⁰⁰	NM	0.83488	0.48649	0.66946	1.89368	0.35352	
10	1.3300 ⁻⁰⁴	4.6695 ⁺⁰⁰	NM	0.84230	0.48649	0.67243	1.91051	0.35196	
11	1.5900 ⁻⁰⁴	5.6404 ⁺⁰⁰	NM	0.85158	0.54054	0.71883	1.76844	0.40647	
12	1.8400 ⁻⁰⁴	5.6404 ⁺⁰⁰	NM	0.85714	0.54054	0.72117	1.78000	0.40515	
13	1.9700 ⁻⁰⁴	6.1654 ⁺⁰⁰	NM	0.85900	0.56757	0.74135	1.70613	0.41352	
14	2.1000 ⁻⁰⁴	6.1654 ⁺⁰⁰	NM	0.86085	0.56757	0.74215	1.70981	0.43405	
15	2.8600 ⁻⁰⁴	6.7165 ⁺⁰⁰	NM	0.87570	0.59459	0.78684	1.66329	0.46104	
16	3.3700 ⁻⁰⁴	7.2937 ⁺⁰⁰	NM	0.88312	0.62162	0.78729	1.60403	0.49082	
17	4.3800 ⁻⁰⁴	7.8969 ⁺⁰⁰	NM	0.89610	0.64865	0.80926	1.55652	0.51991	
18	7.5600 ⁻⁰⁴	9.8624 ⁺⁰⁰	NM	0.92393	0.72973	0.86499	1.40507	0.61562	
19	1.0730 ⁻⁰³	1.2061 ⁺⁰¹	NM	0.94620	0.81081	0.91128	1.26317	0.72142	
20	1.4030 ⁻⁰³	1.3695 ⁺⁰¹	NM	0.96475	0.86486	0.94074	1.18315	0.79511	
21	1.7080 ⁻⁰³	1.5354 ⁺⁰¹	NM	0.97774	0.91892	0.96530	1.10350	0.87477	
22	2.0380 ⁻⁰³	1.7195 ⁺⁰¹	NM	0.98887	0.97297	0.98701	1.02906	0.95914	
23	2.3560 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99258	1.00000	0.99628	0.99258	1.00373	
24	2.6730 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99629	1.00000	0.99814	0.99629	1.00186	
25	3.0040 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99629	1.00000	0.99814	0.99629	1.00186	
26	3.3080 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99814	1.00000	0.99907	0.99814	1.00093	
27	3.6370 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99814	1.00000	0.99907	0.99814	1.00093	
28	3.9560 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99814	1.00000	0.99907	0.99814	1.00093	
29	4.2740 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.99814	1.00000	0.99907	0.99814	1.00093	
30	4.9090 ⁻⁰³	1.8095 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 31	6.3060 ⁻⁰³	1.8095 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,M ASSUME P=PD

69010104		BOLDMAN		PROFILE TABULATION		25 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.58751	0.00000	0.00000	2.86237	0.00000	
2	3.2000 ⁻⁰⁵	1.2755 ⁺⁰⁰	NM	0.71429	0.13636	0.24569	3.24627	0.07568	
3	7.6000 ⁻⁰⁵	1.8929 ⁺⁰⁰	NM	0.74212	0.22727	0.39450	3.01299	0.13093	
4	8.3000 ⁻⁰⁵	2.7136 ⁺⁰⁰	NM	0.74383	0.29545	0.48689	2.71574	0.17929	
5	1.3300 ⁻⁰⁴	3.4133 ⁺⁰⁰	NM	0.77551	0.34091	0.55030	2.60571	0.21119	
6	1.8400 ⁻⁰⁴	4.2238 ⁺⁰⁰	NM	0.79777	0.38636	0.60637	2.46309	0.24618	
7	2.3500 ⁻⁰⁴	5.1418 ⁺⁰⁰	NM	0.80891	0.43182	0.65326	2.28861	0.28544	
8	3.3700 ⁻⁰⁴	5.6404 ⁺⁰⁰	NM	0.82189	0.45455	0.67796	2.22459	0.30476	
9	4.3800 ⁻⁰⁴	6.7165 ⁺⁰⁰	NM	0.83302	0.50000	0.71803	2.06224	0.34818	
10	5.9100 ⁻⁰⁴	7.2937 ⁺⁰⁰	NM	0.84787	0.52273	0.74058	2.00719	0.36896	
11	7.1800 ⁻⁰⁴	7.8969 ⁺⁰⁰	NM	0.85714	0.54545	0.75983	1.94052	0.39156	
12	1.0480 ⁻⁰³	9.8624 ⁺⁰⁰	NM	0.87941	0.61364	0.81016	1.74307	0.46479	
13	1.6570 ⁻⁰³	1.2846 ⁺⁰¹	NM	0.91280	0.70455	0.86918	1.52196	0.57109	
14	2.1910 ⁻⁰³	1.5354 ⁺⁰¹	NM	0.93878	0.77273	0.90806	1.38095	0.65756	
15	2.6230 ⁻⁰³	1.8095 ⁺⁰¹	NM	0.95547	0.84091	0.93841	1.24534	0.75354	
16	3.0800 ⁻⁰³	2.0051 ⁺⁰¹	NM	0.96846	0.88636	0.95765	1.16733	0.82038	
17	3.6000 ⁻⁰³	2.3179 ⁺⁰¹	NM	0.98145	0.95455	0.98091	1.05601	0.92889	
18	3.8040 ⁻⁰³	2.3179 ⁺⁰¹	NM	0.98516	0.95455	0.98277	1.06000	0.92714	
19	4.0450 ⁻⁰³	2.4273 ⁺⁰¹	NM	0.98887	0.97727	0.98965	1.02549	0.96505	
20	4.2480 ⁻⁰³	2.4273 ⁺⁰¹	NM	0.99072	0.97727	0.99058	1.02742	0.96415	
21	4.4010 ⁻⁰³	2.5393 ⁺⁰¹	NM	0.99258	1.00000	0.99628	0.99258	1.00373	
22	4.5280 ⁻⁰³	2.5393 ⁺⁰¹	NM	0.99258	1.00000	0.99628	0.99258	1.00373	
23	4.6550 ⁻⁰³	2.5393 ⁺⁰¹	NM	0.99258	1.00000	0.99628	0.99258	1.00373	
24	5.0100 ⁻⁰³	2.5393 ⁺⁰¹	NM	0.99443	1.00000	0.99721	0.99443	1.00279	
D 25	1.2275 ⁻⁰²	2.5393 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,M ASSUME P=PD

69010201		BOLDMAN	PROFILE TABULATION		22 POINTS, DELTA AT POINT 22				
I	Y	PT2/P	P/PD	T0/T0D	H/H0	U/UD	T/TD	RHO/RH0D*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.62038	0.00000	0.00000	0.62050	0.00000	
2	1.4000 ⁻ 05	1.0003 ⁺ 00	NM	0.74038	0.69264	0.59601	0.74045	0.80493	
3	4.6000 ⁻ 05	1.0003 ⁺ 00	NM	0.88639	0.72809	0.68551	0.88647	0.77331	
4	7.8000 ⁻ 05	1.0004 ⁺ 00	NM	0.89100	0.75916	0.71662	0.89108	0.80422	
5	1.4200 ⁻ 04	1.0004 ⁺ 00	NM	0.89876	0.77104	0.73099	0.89883	0.81327	
6	2.0600 ⁻ 04	1.0004 ⁺ 00	NM	0.90595	0.78802	0.75008	0.90602	0.82788	
7	3.6600 ⁻ 04	1.0004 ⁺ 00	NM	0.92228	0.81331	0.78109	0.92233	0.84686	
8	5.2600 ⁻ 04	1.0005 ⁺ 00	NM	0.93433	0.83504	0.80718	0.93438	0.86387	
9	8.4600 ⁻ 04	1.0015 ⁺ 00	NM	0.95137	0.86528	0.84400	0.95142	0.88709	
10	1.1660 ⁻ 03	1.0005 ⁺ 00	NM	0.96314	0.88778	0.87129	0.96318	0.90459	
11	1.4860 ⁻ 03	1.0005 ⁺ 00	NM	0.97247	0.90430	0.89178	0.97250	0.91699	
12	1.8060 ⁻ 03	1.0006 ⁺ 00	NM	0.97973	0.91967	0.91031	0.97976	0.92912	
13	2.1260 ⁻ 03	1.0006 ⁺ 00	NM	0.98491	0.93145	0.92441	0.98493	0.93855	
14	2.4460 ⁻ 03	1.0006 ⁺ 00	NM	0.98857	0.94226	0.93687	0.98859	0.94768	
15	2.7660 ⁻ 03	1.0006 ⁺ 00	NM	0.99138	0.95158	0.94748	0.99139	0.95570	
16	3.4060 ⁻ 03	1.0006 ⁺ 00	NM	0.99539	0.96539	0.96317	0.99541	0.96762	
17	4.0460 ⁻ 03	1.0006 ⁺ 00	NM	0.99758	0.97582	0.97465	0.99759	0.97700	
18	4.6860 ⁻ 03	1.0006 ⁺ 00	NM	0.99869	0.98324	0.98261	0.99870	0.98388	
19	5.3260 ⁻ 03	1.0006 ⁺ 00	NM	0.99900	0.98956	0.98907	0.99900	0.99006	
20	5.9660 ⁻ 03	1.0006 ⁺ 00	NM	0.99936	0.99244	0.99213	0.99936	0.99276	
21	7.2460 ⁻ 03	1.0007 ⁺ 00	NM	1.00000	0.99766	0.99766	1.00000	0.99766	
0 22	8.5260 ⁻ 03	1.0007 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UE,T0 ASSUME T/TD = T0/T0D AND P=PD

69010202		BOLDMAN	PROFILE TABULATION		37 POINTS, DELTA AT POINT 37				
I	Y	PT2/P	P/PD	T0/T0D	H/H0	U/UD	T/TD	RHO/RH0D*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.79320	0.00000	0.00000	1.49281	0.00000	
2	3.2000 ⁻ 05	1.8929 ⁺ 00	NM	0.87037	0.47619	0.55635	1.36503	0.40758	
3	1.0300 ⁻ 04	3.0492 ⁺ 00	NM	0.87593	0.66667	0.72549	1.18426	0.61261	
4	1.1600 ⁻ 04	3.0492 ⁺ 00	NM	0.87778	0.66667	0.72626	1.18677	0.61196	
5	1.4100 ⁻ 04	3.4133 ⁺ 00	NM	0.88148	0.71429	0.76402	1.14410	0.66779	
6	1.5400 ⁻ 04	3.8090 ⁺ 00	NM	0.88333	0.76190	0.79891	1.09949	0.72662	
7	2.0400 ⁻ 04	4.2238 ⁺ 00	NM	0.89074	0.80952	0.83438	1.06234	0.78541	
8	2.2700 ⁻ 04	4.6695 ⁺ 00	NM	0.89630	0.85714	0.86713	1.02356	0.84722	
9	2.5000 ⁻ 04	5.1418 ⁺ 00	NM	0.90370	0.90476	0.89917	0.98767	0.91039	
10	2.6500 ⁻ 04	5.1418 ⁺ 00	NM	0.90556	0.90476	0.90009	0.98970	0.90946	
11	2.8100 ⁻ 04	5.6404 ⁺ 00	NM	0.91111	0.95238	0.92954	0.95262	0.97578	
12	3.1100 ⁻ 04	5.6404 ⁺ 00	NM	0.91852	0.95238	0.93331	0.96036	0.97184	
13	3.1600 ⁻ 04	5.6404 ⁺ 00	NM	0.92037	0.95238	0.93426	0.96230	0.97086	
14	3.2100 ⁻ 04	5.6404 ⁺ 00	NM	0.92222	0.95238	0.93519	0.96423	0.96988	
15	3.2600 ⁻ 04	5.6404 ⁺ 00	NM	0.92407	0.95238	0.93613	0.96617	0.96891	
16	3.3700 ⁻ 04	5.6404 ⁺ 00	NM	0.92593	0.95238	0.93707	0.96811	0.96794	
17	3.4400 ⁻ 04	5.6404 ⁺ 00	NM	0.92778	0.95238	0.93801	0.97004	0.96697	
18	3.4900 ⁻ 04	5.6404 ⁺ 00	NM	0.92778	0.95238	0.93801	0.97004	0.96697	
19	3.5200 ⁻ 04	5.6404 ⁺ 00	NM	0.92778	0.95238	0.93801	0.97004	0.96697	
20	3.5700 ⁻ 04	5.6404 ⁺ 00	NM	0.92763	0.95238	0.93894	0.97198	0.96601	
21	3.6700 ⁻ 04	5.6404 ⁺ 00	NM	0.93148	0.95238	0.93988	0.97392	0.96505	
22	3.7200 ⁻ 04	5.6404 ⁺ 00	NM	0.93148	0.95238	0.93988	0.97392	0.96505	
23	3.9500 ⁻ 04	5.6404 ⁺ 00	NM	0.93704	0.95238	0.94268	0.97972	0.96219	
24	4.3300 ⁻ 04	5.6404 ⁺ 00	NM	0.94074	0.95238	0.94454	0.98360	0.96029	
25	4.5800 ⁻ 04	6.1654 ⁺ 00	NM	0.94259	1.00000	0.97087	0.94259	1.03000	
26	4.8400 ⁻ 04	6.1654 ⁺ 00	NM	0.94444	1.00000	0.97103	0.94444	1.02899	
27	5.0900 ⁻ 04	6.1654 ⁺ 00	NM	0.94630	1.00000	0.97278	0.94630	1.02798	
28	5.3500 ⁻ 04	6.1654 ⁺ 00	NM	0.94815	1.00000	0.97373	0.94815	1.02698	
29	5.8500 ⁻ 04	6.1654 ⁺ 00	NM	0.95000	1.00000	0.97468	0.95000	1.02598	
30	7.1200 ⁻ 04	6.1654 ⁺ 00	NM	0.95370	1.00000	0.97658	0.95370	1.02398	
31	8.3900 ⁻ 04	6.1654 ⁺ 00	NM	0.95741	1.00000	0.97847	0.95741	1.02200	
32	2.1090 ⁻ 03	6.1654 ⁺ 00	NM	0.97407	1.00000	0.98695	0.97407	1.01322	
33	3.3790 ⁻ 03	6.1654 ⁺ 00	NM	0.98519	1.00000	0.99256	0.98519	1.00749	
34	4.6490 ⁻ 03	6.1654 ⁺ 00	NM	0.99444	1.00000	0.99722	0.99444	1.00279	
35	5.9190 ⁻ 03	6.1654 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
36	7.1890 ⁻ 03	6.1654 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
0 37	7.8240 ⁻ 03	6.1654 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,P ASSUME P=PD

69010203		BOLDMAN		PROFILE TABULATION		32 POINTS, DELTA AT POINT 32			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.3000+00	NM	0.65004	0.00000	0.00000	2.33493	0.00000	
2	3.2000-05	2.1328+00	NM	0.78189	0.30556	0.45948	2.26130	0.20319	
3	1.0800-04	3.4133+00	NM	0.81146	0.41667	0.59075	2.01018	0.29388	
4	1.3300-04	4.2238+00	NM	0.82070	0.47222	0.64544	1.86816	0.34549	
5	1.5900-04	4.6695+00	NM	0.82625	0.50000	0.67099	1.80090	0.37258	
6	2.1000-04	5.6404+00	NM	0.83734	0.55556	0.71814	1.67096	0.42978	
7	2.6000-04	6.1654+00	NM	0.84658	0.58333	0.74150	1.61579	0.45891	
8	3.1100-04	6.7165+00	NM	0.85582	0.61111	0.76378	1.56205	0.48896	
9	4.1300-04	7.2937+00	NM	0.86691	0.63889	0.78588	1.51310	0.51939	
10	4.6400-04	7.2937+00	NM	0.87246	0.63889	0.78839	1.52277	0.51773	
11	5.4000-04	7.8969+00	NM	0.87816	0.66667	0.80621	1.46243	0.55128	
12	6.6700-04	9.1813+00	NM	0.88540	0.72222	0.83983	1.35219	0.62109	
13	7.9400-04	9.8624+00	NM	0.89464	0.75000	0.85756	1.30738	0.65593	
14	1.0480-03	1.1302+01	NM	0.90943	0.80556	0.88903	1.21799	0.72992	
15	1.1750-03	1.2061+01	NM	0.91867	0.83333	0.90466	1.17852	0.76763	
16	1.3020-03	1.2846+01	NM	0.92421	0.86111	0.91785	1.13613	0.80788	
17	1.3780-03	1.3656+01	NM	0.92791	0.88889	0.92953	1.09352	0.85003	
18	1.5560-03	1.4492+01	NM	0.93715	0.91667	0.94343	1.05924	0.89067	
19	1.7840-03	1.5354+01	NM	0.94640	0.94444	0.95683	1.02640	0.93222	
20	1.9370-03	1.6242+01	NM	0.95009	0.97222	0.96696	0.98920	0.97752	
21	2.0640-03	1.6242+01	NM	0.95194	0.97222	0.96790	0.99112	0.97657	
22	2.2160-03	1.7156+01	NM	0.95379	1.00000	0.97662	0.95379	1.02394	
23	2.3180-03	1.7156+01	NM	0.95564	1.00000	0.97757	0.95564	1.02295	
24	2.4190-03	1.7156+01	NM	0.95564	1.00000	0.97757	0.95564	1.02295	
25	2.4560-03	1.7156+01	NM	0.95749	1.00000	0.97851	0.95749	1.02196	
26	2.5720-03	1.7156+01	NM	0.95749	1.00000	0.97851	0.95749	1.02196	
27	2.8260-03	1.7156+01	NM	0.95933	1.00000	0.97746	0.95933	1.02097	
28	3.5880-03	1.7156+01	NM	0.96303	1.00000	0.98134	0.96303	1.01901	
29	4.3500-03	1.7156+01	NM	0.96673	1.00000	0.98322	0.96673	1.01706	
30	6.3820-03	1.7156+01	NM	0.97597	1.00000	0.98791	0.97597	1.01224	
31	1.1970-02	1.7156+01	NM	0.99630	1.00000	0.99815	0.99630	1.00185	
D 32	1.6796-02	1.7156+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,M ASSUME P=PD

69010204		BOLDMAN		PROFILE TABULATION		31 POINTS, DELTA AT POINT 31			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.58957	0.00000	0.00000	2.97735	0.00000	
2	3.2000-05	1.6913+00	NM	0.74212	0.20000	0.35918	3.22520	0.11137	
3	1.0800-04	3.0492+00	NM	0.77180	0.31111	0.52059	2.79999	0.18592	
4	2.6000-04	4.6695+00	NM	0.81262	0.40000	0.63120	2.49012	0.25348	
5	3.6200-04	5.6404+00	NM	0.82560	0.44444	0.67641	2.31627	0.29203	
6	5.1400-04	6.7165+00	NM	0.83859	0.48889	0.71716	2.15187	0.33327	
7	9.2100-04	8.5261+00	NM	0.86271	0.55556	0.77306	1.93630	0.39925	
8	1.5810-03	1.2061+01	NM	0.89239	0.66667	0.84577	1.60450	0.52549	
9	2.1400-03	1.5354+01	NM	0.91466	0.75556	0.89227	1.39463	0.63979	
10	2.6480-03	1.8095+01	NM	0.93135	0.82222	0.92230	1.25825	0.73300	
11	3.1560-03	2.1068+01	NM	0.94620	0.88889	0.94811	1.13769	0.83337	
12	3.3590-03	2.2111+01	NM	0.94991	0.91111	0.95547	1.09973	0.86882	
13	3.6130-03	2.3179+01	NM	0.95547	0.93333	0.96347	1.06562	0.90414	
14	3.8670-03	2.4273+01	NM	0.95918	0.95556	0.97028	1.03105	0.94106	
15	4.0700-03	2.5393+01	NM	0.96104	0.97778	0.97549	0.99615	0.97967	
16	4.3240-03	2.5393+01	NM	0.96289	0.97778	0.97684	0.99807	0.97872	
17	4.4770-03	2.5393+01	NM	0.96475	0.97778	0.97778	1.00000	0.97778	
18	4.6800-03	2.6539+01	NM	0.96475	1.00000	0.98222	0.96475	1.01811	
19	4.9340-03	2.6539+01	NM	0.96475	1.00000	0.98222	0.96475	1.01811	
20	5.0360-03	2.6539+01	NM	0.96475	1.00000	0.98222	0.96475	1.01811	
21	5.1880-03	2.6539+01	NM	0.96660	1.00000	0.98316	0.96660	1.01713	
22	5.6960-03	2.6539+01	NM	0.96660	1.00000	0.98316	0.96660	1.01713	
23	6.2040-03	2.6539+01	NM	0.96846	1.00000	0.98410	0.96846	1.01615	
24	6.4580-03	2.6539+01	NM	0.97032	1.00000	0.98505	0.97032	1.01518	
25	7.9820-03	2.6539+01	NM	0.97403	1.00000	0.98693	0.97403	1.01325	
26	9.5060-03	2.6539+01	NM	0.97774	1.00000	0.98881	0.97774	1.01132	
27	1.0116-02	2.6539+01	NM	0.97959	1.00000	0.98974	0.97959	1.01036	
28	1.2300-02	2.6539+01	NM	0.98701	1.00000	0.99349	0.98701	1.00856	
29	1.6110-02	2.6539+01	NM	0.99443	1.00000	0.99721	0.99443	1.00279	
30	1.8650-02	2.6539+01	NM	0.99814	1.00000	0.99907	0.99814	1.00093	
D 31	2.1952-02	2.6539+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,T0,M ASSUME P=PD

SECTION D: ADDITIONAL DATA - WALL PRESSURE, TEMPERATURE AND HEAT TRANSFER.
 From Boldman & Graham (1972).

PROFILE CAT 6901	STATIONS AUTHOR'S NUMBER	X mm (AXIAL)	Diameter mm	PW/POD EXPERIMENTAL	MD	Series 01		Series 02	
						TW K	h_f kg/m ² s	TW K	h_f kg/m ² s
XX01	2	- 114.68	158.75	0.99946	0.02778	406.6	0.717	376.2	0.448
	3	- 89.28	129.34	0.99847	0.04667	415.7	0.823	389.3	0.598
		- 63.80	99.92	0.99565	0.07894	446.6	1.294	419.6	0.970
	5	- 54.81	89.61	0.99325	0.09841	449.4	1.455	423.8	1.097
	6	- 46.02	79.45	0.98887	0.12655	448.1	1.638	427.7	1.174
	7	- 37.08	69.14	0.9804	0.16840	454.8	1.891	434.6	1.336
	8	- 28.19	58.83	0.9624	0.23463	463.9	2.390	444.4	1.715
	9	- 15.57	44.70	0.8399	0.50553	479.5	3.122	456.9	2.088
	10	- 4.55	38.35	0.5733	0.92813	481.0	3.382	457.3	2.348
	THROAT	11	0	37.90	0.4600	1.11446	478.8	3.347	457.7
12		3.30	38.15	0.3733	1.27507	468.9	2.587	445.9	1.828
13		6.48	39.12	0.2785	1.48469	459.8	2.383	441.3	1.701
14		9.96	40.74	0.2084	1.68125	451.7	2.229	436.7	1.708
15		16.10	43.99	0.1820	1.77070	452.5	2.299	434.5	1.610
XX02	16	31.01	51.87	0.1125	2.08183	444.2	1.955	424.8	1.399
	17	69.49	72.59	0.0375	2.78852	411.0	0.970	397.8	0.893
XX03	18	138.89	109.78	0.0094	3.73770	365.8	0.412	350.5	0.356
	19	208.31	147.12	0.0038	4.42415	330.0	0.214	321.6	0.193
XX04	19a	241.79	165.19	0.0027	4.70038	-	-	-	-
	20	280.21	185.93	0.0024	4.7980	321.6	0.174	316.7	0.141

NOTES:

a) All data have been normalised to the reservoir conditions:

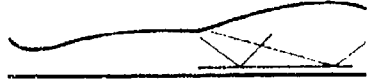
$$P_0 = 2.068 \text{ MN/m}^2 \quad T_0 = 539 \text{ K.}$$

b) The wall temperatures given here were taken over a period of time, and do not necessarily match the values given with the profiles. The shape of the distribution and the variation and values of the enthalpy heat transfer coefficient should, however, be representative.

c) The heat transfer coefficient h_f is defined as

$$h_f = q / (t_{ad} - t_w)$$

where q = heat flux rate / unit area
 t = enthalpy of fluid
 ad = at recovery temperature
 w = at wall temperature

	M : Approximately 1.4 rising to 3 R THETA X 10 ⁻³ : 4 - 2 TH/TR : 1	6902
		FPG - AW
Continuous running tunnel with a single block half-nozzle. W = 80 mm. PO : 0.1 MN/m ² . TO : 300 K. Air. RE/m X 10 ⁻⁶ : 10 - 15.		
MICHEL R., QUEMARD C. and ELENA M-P., 1969. Distributions de vitesses des couches limites turbulentes en écoulement compressible, uniform ou accéléré. La Recherche Aéronautique no 128, 33-47. And Michel R., private communication.		

- 1 The test boundary layer was formed on a straight wall (W = 80 mm) opposite a rigid nozzle block. Three tests were made. For series 01 the throat height was 35 mm and the flow expanded to the nozzle design Mach number of 1.4. The nominally uniform flow is then accelerated by expansion waves originating from a convex circular arc continuation (radius 182 mm) of the upper surface of the nozzle. For the second test the circular arc was replaced by a sharp corner turning the flow through 21°. For the third, the sharp corner was retained but the flat surface was closer to the nozzle block so that the throat height was reduced to 20 mm giving a nominal (one-dimensional) Mach number of 1.55 just before the expansion. The test area on the flat wall extended from X = - 19 to X = 120 mm, in all cases including an initial constant pressure region before entering (X = 0) the reflected wave expansion. The tests were complete upstream of any second reflection of the expansion.
- 6 Static pressure (tapping diameter 0.5 mm) could be measured at 10 mm intervals along the flat test surface.
- 7 The wall "was adiabatic" but no measurements of temperature were made. Pitot profiles were obtained with an FPP (h₁ = 0.18, h₂ = 0.08, b₁ = 2 mm) and the data was reduced assuming no normal pressure gradient and a modified Crocco relationship (Michel, 1963) for the total temperature, with a recovery factor of 0.9. For each case at least two profiles out of a total of 12 were taken in the flow upstream of the expansion. The editors have assumed that the flow was adiabatic and applied the usual Crocco-Van Driest temperature velocity relationship with a recovery factor of 0.896.
- 9 DATA: 6902 0101-0313. Pitot profiles. NX = 12, 13.
- 15 Editors' comments

These tests were performed at relatively low Reynolds number, and the profiles downstream of the fourth station almost certainly display marked re-laminarisation characteristics. Comparisons are not possible, the most nearly matched available data (Pasiuk et al. - CAT 6504, Thomas - CAT 7401) being at much higher Reynolds number.

The expansion was applied as a reflected wave so that normal pressure gradient effects should be small except at the start, near X = 0. The author writes that "results from regions where a normal pressure gradient could be noticed have not been retained".

The physical scale of the equipment is small, and measurements do not extend within the momentum deficit peak, so that integral values should be treated with reserve.

CAT 6902

MICHEL

BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUH X * RZ	MD * POD* TOD*	TW/TR* PW/PD* SW *	RED2W RED2D D2	CF CQ PI2	H12 H32 H42	H12K H32K D2K	PH TW UD	PD TD TR
69020101 -7.0000*-03 INFINITE	1.1900 1.0023*+05 2.9700*+02	1.0000 1.0000 0.0000	2.5908*+03 3.2909*+03 2.1969*-04	NM NM NM	2.1978 1.7916 0.0519	1.4030 1.7850 2.4702*-04	3.1942*+04 2.8839*+02 4.0790*+02	3.1942*+04 2.1422*+02 2.8839*+02
69020102 1.2000*-02 INFINITE	1.4420 1.0160*+05 2.9500*+02	1.0000 1.0000 0.0000	2.7192*+03 3.5121*+03 2.3125*-04	NM NM NM	2.1949 1.8130 0.0554	1.3539 1.8071 2.5949*-04	3.0082*+04 2.8599*+02 4.1732*+02	3.0082*+04 2.0835*+02 2.8599*+02
69020103 1.8000*-02 INFINITE	1.5400 9.9750*+04 3.0200*+02	1.0000 1.0000 0.0000	2.4082*+03 3.1642*+03 2.2162*-04	NM NM NM	2.2409 1.8242 0.0589	1.3379 1.8183 2.4937*-04	2.7172*+04 2.9225*+02 4.3403*+02	2.7172*+04 2.0828*+02 2.9225*+02
69020104 2.4000*-02 INFINITE	1.5700 9.9220*+04 2.9700*+02	1.0000 1.0000 0.0000	2.2515*+03 3.0301*+03 2.1231*-04	NM NM NM	2.3154 1.8319 0.0629	1.3313 1.8254 2.4022*-04	2.4401*+04 2.8680*+02 4.4398*+02	2.4401*+04 1.9893*+02 2.8680*+02
69020105 2.8500*-02 INFINITE	1.6150 9.9950*+04 2.9700*+02	1.0000 1.0000 0.0000	2.1938*+03 2.9973*+03 2.1114*-04	NM NM NM	2.3590 1.8385 0.0655	1.3226 1.8315 2.3940*-04	2.2998*+04 2.8641*+02 4.5238*+02	2.2998*+04 1.9518*+02 2.8641*+02
69020106 3.9000*-02 INFINITE	1.7000 9.7750*+04 2.9700*+02	1.0000 1.0000 0.0000	2.0626*+03 2.9010*+03 2.1463*-04	NM NM NM	2.4475 1.8490 0.0704	1.3083 1.8409 2.4443*-04	1.9804*+04 2.8569*+02 4.6761*+02	1.9804*+04 1.8821*+02 2.8569*+02
69020107 4.7500*-02 INFINITE	1.7700 1.0015*+05 2.9550*+02	1.0000 1.0000 0.0000	1.9762*+03 2.8494*+03 2.0943*-04	NM NM NM	2.5425 1.8494 0.0741	1.3076 1.8409 2.4093*-04	1.8247*+04 2.8366*+02 4.7833*+02	1.8247*+04 1.8167*+02 2.8366*+02
69020108 5.6000*-02 INFINITE	1.8350 9.9450*+04 2.9700*+02	1.0000 1.0000 0.0000	1.9779*+03 2.9173*+03 2.2264*-04	NM NM NM	2.6046 1.8600 0.0778	1.2881 1.8509 2.5645*-04	1.8405*+04 2.8457*+02 4.9014*+02	1.8405*+04 1.7748*+02 2.8457*+02
69020109 7.0000*-02 INFINITE	1.9400 1.0028*+05 2.9700*+02	1.0000 1.0000 0.0000	1.9636*+03 3.0054*+03 2.3790*-04	NM NM NM	2.7517 1.8614 0.0831	1.2828 1.8507 2.7749*-04	1.4068*+04 2.8373*+02 5.0633*+02	1.4068*+04 1.6945*+02 2.8373*+02
69020110 8.8000*-02 INFINITE	2.0500 9.9750*+04 2.9700*+02	1.0000 1.0000 0.0000	1.8185*+03 2.9016*+03 2.4213*-04	NM NM NM	3.0087 1.8383 0.0873	1.3422 1.8206 2.9302*-04	1.1793*+04 2.8289*+02 5.2212*+02	1.1793*+04 1.6137*+02 2.8289*+02
69020111 1.0000*-01 INFINITE	2.1450 9.8950*+04 2.9700*+02	1.0000 1.0000 0.0000	1.8178*+03 3.0060*+03 2.6430*-04	NM NM NM	3.0669 1.8652 0.0930	1.2776 1.8511 3.1633*-04	1.0086*+04 2.8220*+02 5.3486*+02	1.0086*+04 1.5467*+02 2.8220*+02
69020112 1.1600*-01 INFINITE	2.2600 9.9550*+04 2.9700*+02	1.0000 1.0000 0.0000	1.6884*+03 2.9171*+03 2.6962*-04	NM NM NM	3.2772 1.8612 0.0976	1.2856 1.8452 3.3006*-04	8.4756*+03 2.8139*+02 5.4923*+02	8.4756*+03 1.4692*+02 2.8139*+02

CAT 6902 MICHEL BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.									
RUN X * RZ	MD * POD* TOD*	TW/TR* PW/PD* SW *	RED2W RED2D D2	CF CQ PIZ	H12 H32 H42	H12K H32K D2K	PW TW UD	PD TD TR	
69020201	1.3800	1.0000	2.8033 ⁺⁰³	NM	2.2186	1.4297	3.2725 ⁺⁰⁴	3.2725 ⁺⁰⁴	
-1.9000 ⁻⁰²	1.0126 ⁺⁰⁵	1.0000	3.5492 ⁺⁰³	NM	1.7900	1.7841	2.8945 ⁺⁰²	2.1580 ⁺⁰²	
INFINITE	2.9800 ⁺⁰²	0.0000	2.3524 ⁻⁰⁴	NM	0.0510	2.6444 ⁻⁰⁴	4.0646 ⁺⁰²	2.8945 ⁺⁰²	
69020202	1.3800	1.0000	2.8960 ⁺⁰³	NM	2.2095	1.4214	3.2359 ⁺⁰⁴	3.2359 ⁺⁰⁴	
-6.0000 ⁻⁰³	1.0012 ⁺⁰⁵	1.0000	3.6650 ⁺⁰³	NM	1.7874	1.7809	2.9178 ⁺⁰²	2.1754 ⁺⁰²	
INFINITE	3.0040 ⁺⁰²	0.0000	2.4830 ⁻⁰⁴	NM	0.0509	2.7932 ⁻⁰⁴	4.0800 ⁺⁰²	2.9178 ⁺⁰²	
69020203	1.4200	1.0000	2.9352 ⁺⁰³	NM	2.2013	1.3758	3.0587 ⁺⁰⁴	3.0587 ⁺⁰⁴	
6.5000 ⁻⁰³	1.0012 ⁺⁰⁵	1.0000	3.7577 ⁺⁰³	NM	1.7965	1.7904	2.9608 ⁺⁰²	2.749 ⁺⁰²	
INFINITE	3.0520 ⁺⁰²	0.0000	2.8166 ⁻⁰⁴	NM	0.0533	2.9510 ⁻⁰⁴	4.1987 ⁺⁰²	2.9608 ⁺⁰²	
69020204	1.6200	1.0000	2.3391 ⁺⁰³	NM	2.3461	1.3082	2.2639 ⁺⁰⁴	2.2639 ⁺⁰⁴	
2.0000 ⁻⁰²	9.9125 ⁺⁰⁴	1.0000	3.2027 ⁺⁰³	NM	1.8460	1.8402	2.8444 ⁺⁰²	1.9346 ⁺⁰²	
INFINITE	2.9500 ⁺⁰²	0.0000	2.2576 ⁻⁰⁴	NM	0.0661	2.5506 ⁻⁰⁴	4.5177 ⁺⁰²	2.8444 ⁺⁰²	
69020205	1.7500	1.0000	1.8969 ⁺⁰³	NM	2.5126	1.3100	1.8781 ⁺⁰⁴	1.8781 ⁺⁰⁴	
2.7500 ⁻⁰²	9.9992 ⁺⁰⁴	1.0000	2.7079 ⁺⁰³	NM	1.8572	1.8493	2.9449 ⁺⁰²	1.9014 ⁺⁰²	
INFINITE	3.0660 ⁺⁰²	0.0000	2.0808 ⁻⁰⁴	NM	0.0734	2.3720 ⁻⁰⁴	4.8382 ⁺⁰²	2.9449 ⁺⁰²	
69020206	1.8500	1.0000	1.7341 ⁺⁰³	NM	2.6456	1.3074	1.6075 ⁺⁰⁴	1.6075 ⁺⁰⁴	
3.4000 ⁻⁰²	9.9725 ⁺⁰⁴	1.0000	2.5651 ⁺⁰³	NM	1.8632	1.8527	2.9269 ⁺⁰²	1.8142 ⁺⁰²	
INFINITE	3.0560 ⁺⁰²	0.0000	2.0437 ⁻⁰⁴	NM	0.0783	2.3481 ⁻⁰⁴	4.9960 ⁺⁰²	2.9269 ⁺⁰²	
69020207	1.8900	1.0000	1.7830 ⁺⁰³	NM	2.6843	1.2932	1.5034 ⁺⁰⁴	1.5034 ⁺⁰⁴	
3.7000 ⁻⁰²	9.9192 ⁺⁰⁴	1.0000	2.6849 ⁺⁰³	NM	1.8695	1.8602	2.8126 ⁺⁰²	1.7149 ⁺⁰²	
INFINITE	2.9400 ⁺⁰²	0.0000	2.0730 ⁻⁰⁴	NM	0.0806	2.3833 ⁻⁰⁴	4.9623 ⁺⁰²	2.8126 ⁺⁰²	
69020208	2.0500	1.0000	1.6457 ⁺⁰³	NM	2.9041	1.2809	1.1885 ⁺⁰⁴	1.1885 ⁺⁰⁴	
4.8000 ⁻⁰²	1.0052 ⁺⁰⁵	1.0000	2.6178 ⁺⁰³	NM	1.8795	1.8672	2.9166 ⁺⁰²	1.8637 ⁺⁰²	
INFINITE	3.0620 ⁺⁰²	0.0000	2.2609 ⁻⁰⁴	NM	0.0890	2.6267 ⁻⁰⁴	5.3015 ⁺⁰²	2.9166 ⁺⁰²	
69020209	2.1800	1.0000	1.5353 ⁺⁰³	NM	3.1290	1.2912	9.6873 ⁺⁰³	9.6873 ⁺⁰³	
5.8000 ⁻⁰²	1.0039 ⁺⁰⁵	1.0000	2.5646 ⁺⁰³	NM	1.8759	1.8589	2.9011 ⁺⁰²	1.5668 ⁺⁰²	
INFINITE	3.0560 ⁺⁰²	0.0000	2.3518 ⁻⁰⁴	NM	0.0948	2.7882 ⁻⁰⁴	5.4711 ⁺⁰²	2.9011 ⁺⁰²	
69020210	2.2900	1.0000	1.4445 ⁺⁰³	NM	3.2955	1.2761	8.1227 ⁺⁰³	8.1227 ⁺⁰³	
6.7000 ⁻⁰²	9.9992 ⁺⁰⁴	1.0000	2.5173 ⁺⁰³	NM	1.8814	1.8638	2.8810 ⁺⁰²	1.4852 ⁺⁰²	
INFINITE	3.0430 ⁺⁰²	0.0000	2.4326 ⁻⁰⁴	NM	0.0998	2.9105 ⁻⁰⁴	5.5956 ⁺⁰²	2.8810 ⁺⁰²	
69020211	2.3800	1.0000	1.4313 ⁺⁰³	NM	3.4493	1.2740	7.0469 ⁺⁰³	7.0469 ⁺⁰³	
7.6500 ⁻⁰²	9.9658 ⁺⁰⁴	1.0000	2.5795 ⁺⁰³	NM	1.8864	1.8685	2.8985 ⁺⁰²	1.4384 ⁺⁰²	
INFINITE	3.0680 ⁺⁰²	0.0000	2.6433 ⁻⁰⁴	NM	0.1038	3.1819 ⁻⁰⁴	5.7231 ⁺⁰²	2.8985 ⁺⁰²	
69020212	2.5600	1.0000	1.3537 ⁺⁰³	NM	3.8321	1.2951	5.3208 ⁺⁰³	5.3208 ⁺⁰³	
9.9000 ⁻⁰²	9.9792 ⁺⁰⁴	1.0000	2.6160 ⁺⁰³	NM	1.8735	1.8500	2.8889 ⁺⁰²	1.3286 ⁺⁰²	
INFINITE	3.0700 ⁺⁰²	0.0000	2.9508 ⁻⁰⁴	NM	0.1101	3.7161 ⁻⁰⁴	5.9162 ⁺⁰²	2.8889 ⁺⁰²	

CAT 6902

NICHEL

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD * TUD *	T _h /TR * PW/PD * SW * *	RED2W RED2D D2	CF CQ PI2	H12 H32 H42	H12K H32K D2K	PW TW UD	PD TD TR
69020301	1.5400	1.0000	2.2327 ⁺⁰³	NM	2.3915	1.4121	2.5844 ⁺⁰⁴	2.5844 ⁺⁰⁴
-1.3000 ⁻⁰²	1.0056 ⁺⁰⁵	1.0000	2.9735 ⁺⁰³	NM	1.7879	1.7803	2.8958 ⁺⁰²	2.0321 ⁺⁰²
INFINITE	2.9960 ⁺⁰²	0.0000	2.0637 ⁻⁰⁴	NM	0.0598	2.3846 ⁻⁰⁴	4.4015 ⁺⁰²	2.8958 ⁺⁰²
69020302	1.5450	1.0000	2.2929 ⁺⁰³	NM	2.3532	1.3774	2.5308 ⁺⁰⁴	2.5308 ⁺⁰⁴
-3.0000 ⁻⁰³	9.9200 ⁺⁰⁴	1.0000	3.0617 ⁺⁰³	NM	1.8005	1.7944	2.8518 ⁺⁰²	1.9974 ⁺⁰²
INFINITE	2.9510 ⁺⁰²	0.0000	2.1134 ⁻⁰⁴	NM	0.0605	2.4289 ⁻⁰⁴	4.3370 ⁺⁰²	2.8518 ⁺⁰²
69020303	1.7450	1.0000	1.7612 ⁺⁰³	NM	2.5625	1.3473	1.9043 ⁺⁰⁴	1.9043 ⁺⁰⁴
1.1000 ⁻⁰²	1.0062 ⁺⁰⁵	1.0000	2.5115 ⁺⁰³	NM	1.8343	1.8251	2.9203 ⁺⁰²	1.8894 ⁺⁰²
INFINITE	3.0400 ⁺⁰²	0.0000	1.8924 ⁻⁰⁴	NM	0.0722	2.1934 ⁻⁰⁴	4.8091 ⁺⁰²	2.9203 ⁺⁰²
69020304	1.9300	1.0000	1.6487 ⁺⁰³	NM	2.7565	1.2992	1.4083 ⁺⁰⁴	1.4083 ⁺⁰⁴
1.9000 ⁻⁰²	9.8850 ⁺⁰⁴	1.0000	2.5180 ⁺⁰³	NM	1.8611	1.8513	2.8228 ⁺⁰²	1.6929 ⁺⁰²
INFINITE	2.9540 ⁺⁰²	0.0000	1.9965 ⁻⁰⁴	NM	0.0826	2.3269 ⁻⁰⁴	5.0347 ⁺⁰²	2.8228 ⁺⁰²
69020305	2.1150	1.0000	1.3688 ⁺⁰³	NM	3.0572	1.3128	1.0561 ⁺⁰⁴	1.0561 ⁺⁰⁴
2.7500 ⁻⁰²	9.8870 ⁺⁰⁴	1.0000	2.2389 ⁺⁰³	NM	1.8655	1.8504	2.8146 ⁺⁰²	1.5623 ⁺⁰²
INFINITE	2.9600 ⁺⁰²	0.0000	1.9333 ⁻⁰⁴	NM	0.0916	2.3001 ⁻⁰⁴	5.3003 ⁺⁰²	2.8146 ⁺⁰²
69020306	2.2350	1.0000	1.3097 ⁺⁰³	NM	3.2808	1.3331	8.8607 ⁺⁰³	8.8607 ⁺⁰³
3.4000 ⁻⁰²	1.0008 ⁺⁰⁵	1.0000	2.2445 ⁺⁰³	NM	1.8650	1.8442	2.7815 ⁺⁰²	1.4677 ⁺⁰²
INFINITE	2.9340 ⁺⁰²	0.0000	2.0037 ⁻⁰⁴	NM	0.0969	2.4219 ⁻⁰⁴	5.4288 ⁺⁰²	2.7815 ⁺⁰²
69020307	2.3500	1.0000	1.2140 ⁺⁰³	NM	3.4714	1.3234	7.3920 ⁺⁰³	7.3920 ⁺⁰³
4.0000 ⁻⁰²	9.9950 ⁺⁰⁴	1.0000	2.1717 ⁺⁰³	NM	1.8680	1.8459	2.8069 ⁺⁰²	1.4108 ⁺⁰²
INFINITE	2.9690 ⁺⁰²	0.0000	2.0908 ⁻⁰⁴	NM	0.1020	2.5637 ⁻⁰⁴	5.5964 ⁺⁰²	2.8069 ⁺⁰²
69020308	2.4600	1.0000	1.0846 ⁺⁰³	NM	3.6778	1.3329	6.2388 ⁺⁰³	6.2388 ⁺⁰³
4.6000 ⁻⁰²	1.0016 ⁺⁰⁵	1.0000	2.0247 ⁺⁰³	NM	1.8761	1.8525	2.8028 ⁺⁰²	1.3446 ⁺⁰²
INFINITE	2.9720 ⁺⁰²	0.0000	2.0617 ⁻⁰⁴	NM	0.1068	2.5418 ⁻⁰⁴	5.7193 ⁺⁰²	2.8028 ⁺⁰²
69020309	2.5450	1.0000	1.0235 ⁺⁰³	NM	3.7990	1.3030	5.4902 ⁺⁰³	5.4902 ⁺⁰³
5.1000 ⁻⁰²	1.0060 ⁺⁰⁵	1.0000	1.9736 ⁺⁰³	NM	1.8816	1.8581	2.8145 ⁺⁰²	1.3026 ⁺⁰²
INFINITE	2.9900 ⁺⁰²	0.0000	2.1102 ⁻⁰⁴	NM	0.1104	2.6157 ⁻⁰⁴	5.8238 ⁺⁰²	2.8145 ⁺⁰²
69020310	2.6300	1.0000	9.5665 ⁺⁰²	NM	4.0270	1.3500	4.8054 ⁺⁰³	4.8054 ⁺⁰³
5.6000 ⁻⁰²	1.0044 ⁺⁰⁵	1.0000	1.9017 ⁺⁰³	NM	1.8774	1.8469	2.8659 ⁺⁰²	1.2797 ⁺⁰²
INFINITE	3.0500 ⁺⁰²	0.0000	2.1920 ⁻⁰⁴	NM	0.1133	2.7600 ⁻⁰⁴	5.9651 ⁺⁰²	2.8659 ⁺⁰²
69020311	2.7250	1.0000	9.1127 ⁺⁰²	NM	4.1678	1.3062	4.1613 ⁺⁰³	4.1613 ⁺⁰³
6.2500 ⁻⁰²	1.0068 ⁺⁰⁵	1.0000	1.8818 ⁺⁰³	NM	1.8813	1.8539	2.8464 ⁺⁰²	1.2213 ⁺⁰²
INFINITE	3.0390 ⁺⁰²	0.0000	2.2614 ⁻⁰⁴	NM	0.1169	2.8814 ⁻⁰⁴	6.0378 ⁺⁰²	2.8464 ⁺⁰²
69020312	2.8000	1.0000	8.8394 ⁺⁰²	NM	4.3207	1.3062	3.6996 ⁺⁰³	3.6996 ⁺⁰³
6.8000 ⁻⁰²	1.0040 ⁺⁰⁵	1.0000	1.8800 ⁺⁰³	NM	1.8843	1.8547	2.8423 ⁺⁰²	1.1819 ⁺⁰²
INFINITE	3.0350 ⁺⁰²	0.0000	2.3595 ⁻⁰⁴	NM	0.1197	3.0226 ⁻⁰⁴	6.1031 ⁺⁰²	2.8423 ⁺⁰²
69020313	2.9050	1.0000	9.0619 ⁺⁰²	NM	4.6022	1.3455	3.0964 ⁺⁰³	3.0964 ⁺⁰³
7.8500 ⁻⁰²	9.8570 ⁺⁰⁴	1.0000	2.0082 ⁺⁰³	NM	1.8797	1.8422	2.8415 ⁺⁰²	1.1310 ⁺⁰²
INFINITE	3.0400 ⁺⁰²	0.0000	2.7245 ⁻⁰⁴	NM	0.1228	3.5632 ⁻⁰⁴	6.1943 ⁺⁰²	2.8415 ⁺⁰²

69020302		MICHEL		PROFILE TABULATION		27 POINTS, DELTA AT POINT 27			
I	Y	PT2/P	P/PD	T0/T0D	H/H0	U/UD	T/T0	RHO/RHO0=U/UD	
1	0.3000E+00	1.0000E+00	NM	0.96639	0.00000	0.00000	1.42775	0.00000	
2	9.0000E-05	1.5591E+00	NM	0.97852	0.53232	0.60070	1.27340	0.47173	
3	1.0000E-04	1.5669E+00	NM	0.97865	0.53550	0.60390	1.27175	0.47406	
4	1.2000E-04	1.6029E+00	NM	0.97924	0.54980	0.61820	1.26428	0.48897	
5	1.4000E-04	1.6366E+00	NM	0.97977	0.56271	0.63100	1.25744	0.50181	
6	1.6000E-04	1.6791E+00	NM	0.98043	0.57818	0.64620	1.24914	0.51732	
7	1.8000E-04	1.7163E+00	NM	0.98098	0.59122	0.65890	1.24205	0.53050	
8	2.0000E-04	1.7622E+00	NM	0.98165	0.60667	0.67380	1.23355	0.54623	
9	2.5000E-04	1.8481E+00	NM	0.98285	0.63391	0.69779	1.21833	0.57431	
10	3.0000E-04	1.9095E+00	NM	0.98366	0.65208	0.71670	1.20803	0.59328	
11	3.5000E-04	1.9692E+00	NM	0.98442	0.66895	0.73230	1.19837	0.61108	
12	4.0000E-04	2.0230E+00	NM	0.98509	0.68372	0.74580	1.18983	0.62681	
13	4.5000E-04	2.0732E+00	NM	0.98568	0.69677	0.75760	1.18224	0.64082	
14	5.0000E-04	2.1245E+00	NM	0.98631	0.71039	0.76980	1.17427	0.65556	
15	6.0000E-04	2.2266E+00	NM	0.98745	0.73496	0.79150	1.15978	0.68246	
16	7.0000E-04	2.3204E+00	NM	0.98848	0.75698	0.81060	1.14669	0.70690	
17	8.0000E-04	2.4095E+00	NM	0.98942	0.77714	0.82780	1.13463	0.72957	
18	1.0000E-03	2.5921E+00	NM	0.99128	0.81650	0.86060	1.11095	0.77466	
19	1.2000E-03	2.7868E+00	NM	0.99316	0.85603	0.89250	1.08702	0.82105	
20	1.4000E-03	2.9615E+00	NM	0.99477	0.88976	0.91890	1.06657	0.86155	
21	1.6000E-03	3.1547E+00	NM	0.99647	0.92543	0.94600	1.04495	0.90531	
22	1.8000E-03	3.2968E+00	NM	0.99767	0.95070	0.96470	1.02967	0.93691	
23	2.0000E-03	3.4203E+00	NM	0.99868	0.97208	0.98020	1.01677	0.96403	
24	2.2000E-03	3.5122E+00	NM	0.99942	0.98765	0.99130	1.00741	0.98401	
25	2.4000E-03	3.5545E+00	NM	0.99975	0.99473	0.99630	1.00316	0.99316	
26	2.8000E-03	3.5784E+00	NM	0.99994	0.99872	0.99910	1.00077	0.99833	
D 27	2.8000E-03	3.5861E+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/T0 ASSUME P=PD

69020305		MICHEL		PROFILE TABULATION		37 POINTS, DELTA AT POINT 37			
I	Y	PT2/P	P/PD	T0/T0D	H/H0	U/UD	T/T0	RHO/RHO0=U/UD	
1	0.0000E+00	1.0000E+00	NM	0.95089	0.00000	0.00000	1.80160	0.00000	
2	9.0000E-05	2.0002E+00	NM	0.96901	0.49497	0.60740	1.50586	0.40336	
3	1.0000E-04	2.0712E+00	NM	0.96985	0.50862	0.62130	1.44217	0.41637	
4	1.2000E-04	2.1950E+00	NM	0.97126	0.53132	0.64400	1.46915	0.43035	
5	1.4000E-04	2.3693E+00	NM	0.97313	0.56112	0.67300	1.43853	0.46784	
6	1.6000E-04	2.5162E+00	NM	0.97463	0.58470	0.69530	1.41407	0.49170	
7	1.8000E-04	2.6778E+00	NM	0.97621	0.60936	0.71800	1.38836	0.51716	
8	2.0000E-04	2.8176E+00	NM	0.97752	0.62975	0.73630	1.36702	0.53862	
9	2.5000E-04	3.1121E+00	NM	0.98012	0.67037	0.77150	1.32448	0.58249	
10	3.0000E-04	3.3826E+00	NM	0.98236	0.70537	0.80050	1.28794	0.62194	
11	3.5000E-04	3.6607E+00	NM	0.98453	0.73947	0.82760	1.25257	0.66072	
12	4.0000E-04	3.9240E+00	NM	0.98646	0.77025	0.85110	1.22094	0.69708	
13	4.5000E-04	4.1384E+00	NM	0.98797	0.79439	0.86890	1.19640	0.72626	
14	5.0000E-04	4.2987E+00	NM	0.98905	0.81193	0.88150	1.17472	0.74784	
15	6.0000E-04	4.4842E+00	NM	0.99026	0.83174	0.89540	1.15892	0.77261	
16	7.0000E-04	4.5925E+00	NM	0.99095	0.84309	0.90320	1.14768	0.78698	
17	8.0000E-04	4.6435E+00	NM	0.99127	0.84838	0.90690	1.14246	0.79373	
18	9.0000E-04	4.7069E+00	NM	0.99167	0.85490	0.91120	1.13664	0.80208	
19	1.0000E-03	4.7580E+00	NM	0.99198	0.86013	0.91470	1.13092	0.80881	
20	1.2000E-03	4.8232E+00	NM	0.99238	0.86675	0.91910	1.12445	0.81738	
21	1.4000E-03	4.9323E+00	NM	0.99303	0.87770	0.92630	1.11380	0.83166	
22	1.6000E-03	5.0714E+00	NM	0.99384	0.89147	0.93520	1.10052	0.84978	
23	1.8000E-03	5.1875E+00	NM	0.99451	0.90279	0.94240	1.08969	0.86484	
24	2.0000E-03	5.3395E+00	NM	0.99533	0.91701	0.95130	1.07617	0.88396	
25	2.2000E-03	5.4766E+00	NM	0.99610	0.93036	0.95950	1.06361	0.90211	
26	2.4000E-03	5.5881E+00	NM	0.99670	0.94078	0.96560	1.05389	0.91641	
27	2.6000E-03	5.7358E+00	NM	0.99747	0.95439	0.97390	1.04130	0.93528	
28	2.8000E-03	5.8294E+00	NM	0.99795	0.96292	0.97890	1.03347	0.94720	
29	3.0000E-03	5.9307E+00	NM	0.99846	0.97206	0.98420	1.02513	0.96007	
30	3.2000E-03	6.0106E+00	NM	0.99886	0.97921	0.98830	1.01865	0.97021	
31	3.4000E-03	6.0899E+00	NM	0.99925	0.98625	0.99230	1.01230	0.98025	
32	3.6000E-03	6.1442E+00	NM	0.99951	0.99105	0.99500	1.00800	0.98711	
33	3.8000E-03	6.1869E+00	NM	0.99972	0.99479	0.99710	1.00464	0.99249	
34	4.0000E-03	6.2134E+00	NM	0.99984	0.99712	0.99840	1.00256	0.99585	
35	4.2000E-03	6.2361E+00	NM	0.99995	0.99910	0.99950	1.00080	0.99870	
36	4.4000E-03	6.2402E+00	NM	0.99997	0.99946	0.99970	1.00048	0.99922	
D 37	4.6000E-03	6.2464E+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

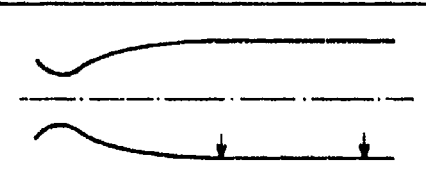
INPUT VARIABLES Y,U/UD,T/T0 ASSUME P=PD

69020309		MICHEL		PROFILE TABULATION		37 POINTS, DELTA AT POINT 37		
I	Y	PT2/P	P/PD	T0/T0D	M/HD	U/UD	T/T0	RHD/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.94131	0.00000	0.00000	2.16068	0.00000
2	9.0000+05	1.7889+00	NM	0.95654	0.37356	0.50940	1.85950	0.27394
3	1.0000+04	1.9485+00	NM	0.95734	0.38488	0.52260	1.84369	0.28345
4	1.2000+04	2.0653+00	NM	0.96003	0.42174	0.56440	1.79095	0.31514
5	1.4000+04	2.3342+00	NM	0.96296	0.46147	0.60740	1.73247	0.35060
6	1.6000+04	2.5777+00	NM	0.96536	0.49320	0.64020	1.68497	0.37995
7	1.8000+04	2.8524+00	NM	0.96798	0.52747	0.67410	1.63326	0.41273
8	2.0000+04	3.1352+00	NM	0.97044	0.55965	0.70450	1.58461	0.44459
9	2.3000+04	3.8058+00	NM	0.97567	0.62876	0.76520	1.48107	0.51665
10	3.0000+04	4.2511+00	NM	0.97877	0.67045	0.79890	1.41989	0.56265
11	4.0000+04	5.1008+00	NM	0.98399	0.74324	0.85280	1.31656	0.64775
12	4.5000+04	5.3565+00	NM	0.98542	0.76373	0.86690	1.28841	0.67284
13	5.0000+04	5.6482+00	NM	0.98697	0.78645	0.88200	1.25776	0.70125
14	6.0000+04	6.0464+00	NM	0.98896	0.81641	0.90110	1.21823	0.73968
15	7.0000+04	6.3334+00	NM	0.99033	0.83733	0.91390	1.19127	0.76717
16	8.0000+04	6.5026+00	NM	0.99110	0.84941	0.92110	1.17593	0.78329
17	9.0000+04	6.6039+00	NM	0.99156	0.85656	0.92530	1.16693	0.79294
18	1.0000+03	6.6431+00	NM	0.99173	0.85931	0.92690	1.16349	0.79666
19	1.1000+03	6.6471+00	NM	0.99173	0.85931	0.92690	1.16349	0.79666
20	1.2000+03	6.6900+00	NM	0.99194	0.86259	0.92880	1.15940	0.80111
21	1.3000+03	6.7223+00	NM	0.99208	0.86485	0.93010	1.15659	0.80417
22	1.4000+03	6.7851+00	NM	0.99235	0.86921	0.93260	1.15119	0.81012
23	1.6000+03	6.9052+00	NM	0.99287	0.87748	0.93730	1.14099	0.82148
24	1.8000+03	7.0546+00	NM	0.99350	0.88767	0.94300	1.12855	0.83559
25	2.0000+03	7.1349+00	NM	0.99363	0.89310	0.94600	1.12197	0.84316
26	2.2000+03	7.3077+00	NM	0.99453	0.90466	0.95230	1.10809	0.85941
27	2.4000+03	7.4259+00	NM	0.99500	0.91249	0.95650	1.09878	0.87051
28	2.6000+03	7.5409+00	NM	0.99545	0.92004	0.96050	1.08988	0.88129
29	2.8000+03	7.6317+00	NM	0.99580	0.92596	0.96360	1.08296	0.88978
30	3.0000+03	7.7540+00	NM	0.99627	0.93387	0.96770	1.07377	0.90122
31	3.5000+03	8.0383+00	NM	0.99732	0.95200	0.97690	1.05300	0.92773
32	4.0000+03	8.2938+00	NM	0.99823	0.96300	0.98480	1.03502	0.95148
33	4.5000+03	8.4988+00	NM	0.99894	0.98064	0.99090	1.02103	0.97049
34	5.0000+03	8.6475+00	NM	0.99944	0.98971	0.99520	1.01112	0.98426
35	5.5000+03	8.7462+00	NM	0.99977	0.99569	0.99800	1.00464	0.99339
36	6.0000+03	8.7926+00	NM	0.99992	0.99849	0.99930	1.00162	0.99768
D 37	6.5000+03	8.8178+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

69020313		MICHEL		PROFILE TABULATION		41 POINTS, DELTA AT POINT 41		
I	Y	PT2/P	P/PD	T0/T0D	M/HD	U/UD	T/T0	RHD/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.93469	0.00000	0.00000	2.51227	0.00000
2	9.0000+05	1.5027+00	NM	0.94550	0.27041	0.40670	2.26214	0.17979
3	1.0000+04	1.5233+00	NM	0.94584	0.27314	0.41310	2.25420	0.18326
4	1.2000+04	1.6524+00	NM	0.94787	0.30236	0.44920	2.20713	0.20352
5	1.4000+04	2.0380+00	NM	0.95294	0.36567	0.52860	2.08972	0.25295
6	1.6000+04	2.2936+00	NM	0.95377	0.39930	0.56810	2.02421	0.28065
7	1.8000+04	2.5720+00	NM	0.95057	0.43261	0.60470	1.95929	0.30863
8	2.0000+04	2.8311+00	NM	0.96099	0.45990	0.63450	1.90345	0.33334
9	2.5000+04	3.3857+00	NM	0.96565	0.51383	0.68850	1.79541	0.38348
10	3.0000+04	3.8605+00	NM	0.96421	0.55506	0.72700	1.71299	0.42440
11	3.5000+04	4.3099+00	NM	0.97228	0.59201	0.75860	1.64200	0.46200
12	4.0000+04	4.7187+00	NM	0.97404	0.62330	0.78810	1.58251	0.49548
13	4.5000+04	5.1455+00	NM	0.97733	0.65431	0.80800	1.52406	0.52945
14	5.0000+04	5.5314+00	NM	0.97942	0.68109	0.82760	1.47648	0.56052
15	6.0000+04	6.2622+00	NM	0.98304	0.72906	0.86040	1.39276	0.61777
16	7.0000+04	6.7798+00	NM	0.98536	0.76117	0.88980	1.33904	0.65779
17	8.0000+04	7.0652+00	NM	0.98656	0.77830	0.89120	1.31117	0.67976
18	9.0000+04	7.3370+00	NM	0.98766	0.79426	0.90060	1.28570	0.70048
19	1.0000+03	7.5762+00	NM	0.98860	0.80805	0.90850	1.26408	0.71870
20	1.2000+03	7.8788+00	NM	0.98972	0.82492	0.91790	1.23812	0.74156
21	1.4000+03	8.0669+00	NM	0.99041	0.83560	0.92370	1.22197	0.75591
22	1.6000+03	8.3180+00	NM	0.99130	0.84935	0.93100	1.20149	0.77487
23	1.8000+03	8.5196+00	NM	0.99196	0.85975	0.93640	1.18624	0.78938
24	2.0000+03	9.0122+00	NM	0.99266	0.87095	0.94210	1.17005	0.80518
25	2.4000+03	9.0122+00	NM	0.99360	0.88625	0.94970	1.14831	0.82704
26	2.8000+03	9.2805+00	NM	0.99443	0.90011	0.95640	1.12900	0.84712
27	3.2000+03	9.4713+00	NM	0.99501	0.90983	0.96100	1.11566	0.86130
28	3.6000+03	9.6547+00	NM	0.99555	0.91907	0.96530	1.10313	0.87505
29	4.0000+03	9.8565+00	NM	0.99613	0.92914	0.96990	1.08967	0.88009
30	4.5000+03	1.0073+01	NM	0.99674	0.93944	0.97470	1.07555	0.90623
31	5.0000+03	1.0307+01	NM	0.99738	0.95122	0.97970	1.06078	0.92357
32	5.5000+03	1.0480+01	NM	0.99784	0.95756	0.98330	1.05009	0.93640
33	6.0000+03	1.0652+01	NM	0.99829	0.96779	0.98640	1.03966	0.94416
34	6.5000+03	1.0828+01	NM	0.99874	0.97615	0.99030	1.02920	0.94221
35	7.0000+03	1.1004+01	NM	0.99918	0.98439	0.99370	1.01899	0.97318
36	7.5000+03	1.1130+01	NM	0.99949	0.99029	0.99610	1.01177	0.98451
37	8.0000+03	1.1188+01	NM	0.99963	0.99301	0.99720	1.00846	0.98864
38	8.5000+03	1.1258+01	NM	0.99980	0.99624	0.99850	1.00453	0.99399
39	9.0000+03	1.1280+01	NM	0.99986	0.99724	0.99890	1.00333	0.99557
40	9.5000+03	1.1301+01	NM	0.99991	0.99824	0.99930	1.00212	0.99719
D 41	1.0000+02	1.1340+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

	M : 2 - 5 R THETA X 10 ⁻³ : 85 - 350 TW/TR : Approximately 1	6903
		ZPG - AW
Blow down tunnel with flexible symmetrical nozzle. Running time 10 - 100 s. W = H = 1.22, L = 5.2 m. 0.16 < P0 < 1.6 MN/m ² T0 : 300 K. Air, dewpoint 228 K. 1.3 < RE/m X 10 ⁻⁶ < 5.6.		
THOMKE G.J., Boundary layer and skin friction characteristics in the supersonic test section of the Mc Donnell-Douglas Aerophysics Laboratory Four-Foot Trisonic Wind Tunnel (Unpublished DAC Report - Private communication) And Thomke and Roshko (1969), Roshko and Thomke (1970)		

- 1 The test boundary layer was formed on the lower nozzle plate. Measurements were made on the floor of the tunnel test section, extending from the nozzle exit plane (X = 0) to X = 1.52 m, and a rectangular plate-steel extension continuing to X = 5.18 m. The test stations were X = 1.83, 4.19 and 4.38 m. All joints and seals were filled and faired with a jointing compound, resulting in flow uniformity within $\pm 0.5\%$ in
- 2 Mach number with a mean Mach number gradient of $-0.013/\text{m}$ and $-0.0065/\text{m}$ at M = 2 and M = 5 respectively.
- 3 Transition was believed to occur naturally upstream of the nozzle. The test layer had passed through the nozzle expansion, growing on one of the curved flexible nozzle plates. Pitot profiles obtained on the
- 4 tunnel centre-line at the last station agreed well with those obtained 0.38 m to the side. Preston tubes on the centre line and 102 mm to either side agreed well with the average reading.
- 5
- 6 Wall static pressure was found at orifices (d = 1.27 mm). These were placed 25.4 mm ahead of Preston tubes and Pitot rakes. An additional three tapings were placed at 25.4 mm intervals ahead of the rakes. A copper constantan thermocouple was buried 1.6 mm below the tunnel floor at X = 3.61 m. Wall shear stress was determined using Preston tubes (d₁ = 1.6, d₂ = 1.1, l = 51 mm) mounted in accordance with the practice of Hopkins and Keener (CAT 6601). The data were obtained as the average of readings from the three tubes
- 7 mounted at 102 mm spanwise intervals. Pitot profiles were obtained using rakes mounting 30 CPP (d₁ = 1.24 d₂ = 0.89 l = 12.4 mm) at the Y values given in the profile tables of section B. The rake mounting body
- 8 had a wedge cross-section with a total included leading edge angle of 7°. Profiles and Preston tube measurements for each station were made at the same value of X. The front rake was 0.38 m to the "right" of the centre line while the rear rake was 0.38 m to the "left". The Preston tubes were no closer than 152 mm (spanwise) to the rakes. Check runs at the downstream station, with and without the upstream rake in position, showed that it had no measurable influence at the downstream station.
- 9 The Mach number profiles obtained from the Pitot measurements were reduced to velocity profiles using
- 10 the Crocco / Van Driest velocity temperature correlation, the measured wall temperature, and a recovery
- 11 factor of 0.89. No corrections were applied to the Pitot data, and Sutherland's viscosity law was used.
- 12 The editors have presented the data incorporating all the assumptions and interpolation procedures of the
- 13 author, but using a recovery factor of 0.896. The sixteen sets of profiles represent measurements at two
- 14 streamwise stations for a range of Mach and Reynolds number. The associated wall shear stress data were obtained simultaneously for half the profile series.
- 5 DATA: 69030101-1602. PT2 profiles, NX = 2, CF obtained from Preston tubes for half the series.

15 Editors' comments

This experiment provides data at a virtually unmatched Reynolds Number over a range of Mach Number. Moore & Harkness - CAT 6502 describe a boundary layer at M = 2.7 and even higher Reynolds Number, but their experiment is not fully reported. In both cases the test layer develops over a streamwise distance which is large compared to the width of the test surface, so that the results are not necessarily completely typical of a two-dimensional flow.

Despite the very large scale of the experiment, the measurements do not reach further in than the momentum-deficit peak in 60 % of the cases. There is some evidence, in the velocity profiles, that the points nearest the wall are affected by probe interference effects, and that profiles 0502, 0801/2 and 1001 are not completely normal in the outer region.

CAT 6903		THOMKE		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN X * RZ	MD * POD TOD	TW/TR * PW/PR * SW *	RED2W RED2D D2	CF * CO PI2	H12 H32 H42	H12K H32K D2K	PH TWA UD	PD TD TR			
69030101 2.1336*+00 INFINITE	1.9900 2.0923*+05 2.8169*+02	1.0666 1.0000 0.0000	8.6475*+04 1.4282*+05 5.1456*+03	1.3060*+03 NM NM	2.9851 1.8381 0.0075	1.2588 1.8293 6.3143*+03	2.7159*+04 2.8722*+02 5.0042*+02	2.7159*+04 1.5730*+02 2.6893*+02			
69030102 4.3764*+00 INFINITE	1.9500 2.0737*+05 2.8178*+02	1.0590 1.0000 0.0000	1.1529*+05 1.8638*+05 6.6563*+03	1.2060*+03 NM NM	2.8764 1.8344 0.0253	1.2582 1.8305 8.0614*+03	2.8643*+04 2.8500*+02 4.9463*+02	2.8643*+04 1.6006*+02 2.6912*+02			
69030201 2.1336*+00 INFINITE	2.4900 1.8715*+05 2.8519*+02	1.0790 1.0000 0.0000	5.0135*+04 1.0106*+05 5.2757*+03	NM NM NM	3.8837 1.8472 0.0256	1.2421 1.8362 7.0290*+03	1.1125*+04 2.9000*+02 5.6351*+02	1.1125*+04 1.2731*+02 2.6877*+02			
69030202 4.1910*+00 INFINITE	2.4500 1.8419*+05 2.8520*+02	1.0780 1.0000 0.0000	6.3047*+04 1.2501*+05 6.4951*+03	NM NM NM	3.8523 1.8455 0.0081	1.2474 1.8339 8.6390*+03	1.1653*+04 2.9000*+02 5.5923*+02	1.1653*+04 1.2961*+02 2.6902*+02			
69030301 2.1336*+00 INFINITE	2.4800 4.1306*+05 2.8182*+02	1.0770 1.0000 0.0000	9.8961*+04 1.9877*+05 4.5984*+03	1.0890*+03 NM NM	3.8530 1.8503 0.0272	1.2412 1.8397 6.0849*+03	2.4940*+04 2.8611*+02 5.5897*+02	2.4940*+04 1.2637*+02 2.6586*+02			
69030302 4.3764*+00 INFINITE	2.4600 4.1611*+05 2.8191*+02	1.0720 1.0000 0.0000	1.3395*+05 2.6595*+05 6.0472*+03	4.7800*+04 NM NM	3.8653 1.8467 0.0099	1.2453 1.8359 8.0454*+03	2.5919*+04 2.8500*+02 5.5702*+02	2.5919*+04 1.2754*+02 2.6586*+02			
69030401 2.1336*+00 INFINITE	2.9700 2.0097*+05 2.8505*+02	1.0880 1.0000 0.0000	3.4288*+04 8.4053*+04 5.2297*+03	NM NM NM	5.0478 1.8511 0.0257	1.2377 1.8371 7.6843*+03	5.7196*+03 2.8944*+02 6.0614*+02	5.7196*+03 1.0224*+02 2.6803*+02			
69030402 4.1910*+00 INFINITE	2.9400 2.0770*+05 2.8330*+02	1.0840 1.0000 0.0000	4.7532*+04 1.1496*+05 6.8008*+03	NM NM NM	4.9112 1.8516 0.0284	1.2389 1.8369 9.7776*+03	6.1885*+03 2.8889*+02 6.0274*+03	6.1885*+03 1.0455*+02 2.6650*+02			
69030501 2.1336*+00 INFINITE	2.9000 2.7506*+05 2.8607*+02	1.0860 1.0000 0.0000	4.4402*+04 1.0922*+05 5.0641*+03	NM NM NM	5.0034 1.8544 0.0275	1.2330 1.8407 7.3739*+03	7.7164*+03 2.9000*+02 6.0652*+02	7.7164*+03 1.0305*+02 2.6703*+02			
69030502 4.1910*+00 INFINITE	2.9300 2.7561*+05 2.8635*+02	1.0840 1.0000 0.0000	6.3820*+04 1.5365*+05 6.8297*+03	NM NM NM	4.8704 1.8551 0.0284	1.2315 1.8413 9.9454*+03	8.3366*+03 2.9000*+02 6.0309*+02	8.3366*+03 1.0539*+02 2.6753*+02			
69030601 2.1336*+00 INFINITE	2.9000 4.5192*+05 3.1104*+02	0.9950 1.0000 0.0000	7.0927*+04 1.6064*+05 5.1187*+03	9.8500*+04 NM NM	4.6720 1.8578 0.1249	1.2279 1.8450 7.2061*+03	1.2678*+04 2.8889*+02 6.3243*+02	1.2678*+04 1.1204*+02 2.9034*+02			
69030602 4.3764*+00 INFINITE	2.9600 4.4717*+05 3.1119*+02	0.9980 1.0000 0.0000	8.7752*+04 1.9764*+05 6.2716*+03	9.3100*+04 NM NM	4.6682 1.8579 0.1106	1.2260 1.8461 3.8296*+03	1.2986*+04 2.9000*+02 6.3105*+02	1.2986*+04 1.1306*+02 2.9959*+02			
69030701 2.1336*+00 INFINITE	2.9800 7.8930*+05 3.0281*+02	1.0240 1.0000 0.0000	1.1150*+05 2.5742*+05 4.5528*+03	9.2900*+04 NM NM	4.7571 1.8598 0.0980	1.2280 1.8471 6.4333*+03	2.2143*+04 2.8944*+02 6.2401*+02	2.2143*+04 1.0908*+02 2.8266*+02			
69030702 4.3764*+00 INFINITE	2.9500 7.8698*+05 3.0294*+02	1.0250 1.0000 0.0000	1.5069*+05 3.4671*+05 6.0073*+03	8.0500*+04 NM NM	4.6856 1.8597 0.0962	1.2243 1.8479 8.4467*+03	2.3097*+04 2.9000*+02 6.2186*+02	2.3097*+04 1.1054*+02 2.8293*+02			
69030801 2.1336*+00 INFINITE	3.4000 2.8117*+05 2.8303*+02	1.0690 1.0000 0.0000	3.2234*+04 9.6985*+04 5.6694*+03	NM NM NM	6.5562 1.8583 -0.0197	1.2325 1.8385 7.2248*+03	3.7930*+03 2.8556*+02 6.3457*+02	3.7930*+03 8.2714*+01 2.6222*+02			
69030802 4.1910*+00 INFINITE	3.4200 2.7847*+05 2.8302*+02	1.0840 1.0000 0.0000	3.8401*+04 1.1246*+05 6.4746*+03	NM NM NM	6.1306 1.8507 0.0527	1.2430 1.8334 1.0373*+02	4.0631*+03 2.8444*+02 6.3128*+02	4.0631*+03 8.4756*+01 2.6240*+02			

CAT 6903		THOMKE		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUH X RZ	MD * POD TOD	TN/TR* TN/PO* SN	RED2H RED2D DZ	CF * CO PIZ	H1Z H3Z H4Z	H12K H32K D2K	PH TW* UD	PD TD TR	
69030901	3.4800	1.0910	5.0674"+04	NM	6.6788	1.2216	6.1050"+03	6.1050"+03	
2.1336"+00	4.5250"+05	1.0000	1.5260"+05	NM	1.8640	1.8451	2.8611"+02	8.2723"+01	
INFINITE	2.8300"+02	0.0000	5.5461"-03	NM	-0.0588	9.9969"-03	6.3460"+02	2.6225"+02	
69030902	3.4300	1.0860	5.9004"+04	NM	6.1960	1.2319	6.5010"+03	6.5010"+03	
4.1910"+00	4.4874"+05	1.0000	1.7372"+05	NM	1.8573	1.8410	2.8500"+02	8.4430"+01	
INFINITE	2.8309"+02	0.0000	6.1972"-03	NM	0.0351	9.8535"-03	6.3191"+02	2.6243"+02	
69031001	3.4500	1.0230	8.3135"+04	6.1600"-04	6.1621	1.2174	1.0559"+04	1.0559"+04	
2.1336"+00	7.5001"+05	1.0000	2.3250"+05	NM	1.8651	1.8484	2.8944"+02	9.0311"+01	
INFINITE	3.0530"+02	0.0000	5.6081"-03	NM	0.0471	8.7460"-03	6.5735"+02	2.6294"+02	
69031002	3.4300	1.0240	9.6711"+04	7.0500"-04	5.9633	1.2309	1.0817"+04	1.0817"+04	
4.3764"+00	7.4662"+05	1.0000	2.6790"+05	NM	1.8572	1.8410	2.9000"+02	9.1113"+01	
INFINITE	3.0550"+02	0.0000	6.4283"-03	NM	0.0536	1.0041"-02	6.5644"+02	2.8320"+02	
69031101	3.9900	1.0520	4.2911"+04	NM	7.6877	1.2228	4.5031"+03	4.5031"+03	
2.1336"+00	6.7466"+05	1.0000	1.5124"+05	NM	1.8635	1.8441	2.8667"+02	7.0725"+01	
INFINITE	2.9592"+02	0.0000	5.1426"-03	NM	.9828	8.7460"-03	6.7278"+02	2.7550"+02	
69031102	4.0100	1.0490	4.9386"+04	NM	7.6909	1.2111	4.4732"+03	4.4732"+03	
4.1910"+00	6.8830"+05	1.0000	1.7484"+05	NM	1.8722	1.8545	2.8611"+02	7.0267"+01	
INFINITE	2.9625"+02	0.0000	5.9005"-03	NM	0.0862	1.0040"-02	6.7396"+02	2.7275"+02	
69031201	3.9400	0.9440	6.2496"+04	7.4900"-04	7.0652	1.2303	6.8532"+03	6.8532"+03	
2.1336"+00	9.6025"+05	1.0000	1.9412"+05	NM	1.8600	1.8406	2.8722"+02	8.0453"+01	
INFINITE	3.3024"+02	0.0000	5.3235"-03	NM	0.1827	8.9387"-03	7.0856"+02	3.0426"+02	
69031202	3.4300	0.9910	7.5054"+04	6.6200"-04	7.0508	1.2244	7.0147"+03	7.0147"+03	
4.3764"+00	9.6770"+05	1.0000	2.3399"+05	NM	1.8628	1.8445	2.8944"+02	8.0780"+01	
INFINITE	3.3031"+02	0.0000	6.3124"-03	NM	0.1762	1.0526"-02	7.0820"+02	3.0436"+02	
69031301	3.9400	1.0150	9.0782"+04	6.9500"-04	7.3203	1.2270	1.0821"+04	1.0821"+04	
2.1336"+00	1.5163"+06	1.0000	3.0247"+05	NM	1.8629	1.8450	2.8944"+02	7.5305"+01	
INFINITE	3.0951"+02	0.0000	4.7697"-03	NM	0.1266	8.1110"-03	6.8597"+02	2.8517"+02	
69031302	3.9300	1.0170	1.1033"+05	6.4700"-04	7.3660	1.2180	1.1022"+04	1.1022"+04	
4.3764"+00	1.5238"+06	1.0000	3.6681"+05	NM	1.8676	1.8500	2.9000"+02	7.5083"+01	
INFINITE	3.0947"+02	0.0000	5.7247"-03	NM	0.1051	9.6440"-03	6.8549"+02	2.6515"+02	
69031401	4.4000	1.0370	3.1809"+04	NM	8.9542	1.2292	2.8947"+03	2.8947"+03	
2.1336"+00	7.3889"+05	1.0000	1.2018"+05	NM	1.8607	1.8393	2.8722"+02	6.1972"+01	
INFINITE	1.0193"+02	0.0000	5.0415"-03	NM	0.1126	9.5706"-03	6.9448"+02	2.7697"+02	
69031402	4.4300	1.0320	3.6611"+04	NM	8.8893	1.2126	2.8423"+03	2.8423"+03	
4.1910"+00	7.5351"+05	1.0000	1.4891"+05	NM	1.8719	1.8524	2.8611"+02	6.1380"+01	
INFINITE	3.0229"+02	0.0000	5.6238"-03	NM	0.1305	1.0675"-02	7.0587"+02	2.7724"+02	
69031501	4.4400	0.9750	5.3791"+04	6.5500"-04	8.7974	1.2235	5.1050"+03	5.1050"+03	
2.1336"+00	1.3703"+06	1.0000	2.0629"+05	NM	1.8671	1.8446	2.8944"+02	6.5455"+01	
INFINITE	3.2372"+02	0.0000	4.9546"-03	NM	0.1560	9.1375"-03	7.2044"+02	2.9687"+02	
69031607	4.4000	0.9800	6.6532"+04	6.0200"-04	6.6981	1.2257	5.3741"+03	5.3741"+03	
4.3764"+00	1.3718"+06	1.0000	2.5254"+05	NM	1.8692	1.8426	2.9111"+02	6.6465"+01	
INFINITE	3.2382"+02	0.0000	5.9440"-03	NM	0.1531	1.0958"-02	7.1921"+02	2.9705"+02	
69031601	4.9200	0.9880	2.0393"+04	NM	10.8718	1.2355	1.5504"+03	1.5504"+03	
2.1336"+00	7.4683"+05	1.0000	9.3017"+04	NM	1.8632	1.8355	2.9500"+02	5.5938"+01	
INFINITE	3.2675"+02	0.0000	5.2348"-03	NM	0.1169	1.0979"-02	7.3778"+02	2.9858"+02	
69031602	4.9200	0.9940	2.2331"+04	NM	10.4543	1.2228	1.5542"+03	1.5542"+03	
4.1910"+00	7.4064"+05	1.0000	1.0230"+05	NM	1.8687	1.8447	2.9722"+02	5.6014"+01	
INFINITE	3.2722"+02	0.0000	9.7599"-03	NM	0.1720	1.1625"-02	7.3632"+02	2.9902"+02	

PD,POD CALCULATED FROM RE/IN/DELTA R (AUTHOR), TOD CALCULATED FROM TN/TR, R (AUTHOR)

69030101		THOMKE		PROFILE TABULATION			31 POINTS, DELTA AT POINT 25		
I	Y	PTZ/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RH00*U/UD	
1	0.0000+00	1.0000+00	NM	1.02522	0.00000	0.00000	1.83721	0.00000	
2	5.8420+04	1.7970+00	NM	1.00070	0.17977	0.59064	1.51675	0.38941	
3	2.0320+03	2.1691+00	NM	0.99955	0.55977	0.67032	1.43508	0.46710	
4	3.5560+03	2.3913+00	NM	0.99919	0.60021	0.70817	1.39308	0.50335	
5	5.0546+03	2.5685+00	NM	0.99900	0.63007	0.73506	1.36199	0.53970	
6	7.4422+03	2.8165+00	NM	0.99884	0.66914	0.76892	1.32135	0.58192	
7	9.7790+03	2.9681+00	NM	0.99878	0.69176	0.78785	1.29792	0.60701	
8	1.2725+02	3.1653+00	NM	0.99874	0.71996	0.81076	1.26887	0.63896	
9	1.5113+02	3.2931+00	NM	0.99876	0.73760	0.82470	1.25082	0.65933	
10	1.7450+02	3.3594+00	NM	0.99877	0.74656	0.83167	1.24169	0.66979	
11	2.0244+02	3.4967+00	NM	0.99879	0.76478	0.84562	1.22322	0.69131	
12	2.2733+02	3.6728+00	NM	0.99884	0.78745	0.86235	1.20041	0.71855	
13	2.5324+02	3.7924+00	NM	0.99889	0.80247	0.87351	1.18543	0.73687	
14	3.0351+02	3.9868+00	NM	0.99897	0.82623	0.89044	1.16195	0.76633	
15	3.5331+02	4.2311+00	NM	0.99910	0.85511	0.91036	1.13379	0.80294	
16	4.0411+02	4.5076+00	NM	0.99926	0.88661	0.93127	1.10360	0.84385	
17	4.5542+02	4.8899+00	NM	0.99938	0.90676	0.94422	1.07460	0.87057	
18	5.0521+02	4.9119+00	NM	0.99952	0.93066	0.95916	1.06238	0.90284	
19	5.6885+02	5.1470+00	NM	0.99969	0.95532	0.97410	1.03984	0.93678	
20	6.3297+02	5.3624+00	NM	0.99984	0.97734	0.98705	1.02004	0.96766	
21	6.9571+02	5.5007+00	NM	0.99994	0.99121	0.99502	1.00774	0.98738	
22	7.6022+02	5.5537+00	NM	0.99997	0.99647	0.99801	1.00310	0.99492	
23	8.2296+02	5.5537+00	NM	0.99997	0.99647	0.99801	1.00310	0.99492	
24	8.8671+02	5.5894+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 25	9.5377+02	5.5894+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.0132+01	5.5183+00	NM	0.99995	0.99296	0.99602	1.00619	0.98989	
27	1.1151+01	5.5183+00	NM	0.99995	0.99296	0.99602	1.00619	0.98989	
28	1.2174+01	5.5183+00	NM	0.99995	0.99296	0.99602	1.00619	0.98989	
29	1.3183+01	5.5183+00	NM	0.99995	0.99296	0.99602	1.00619	0.98989	
30	1.4133+01	5.5183+00	NM	0.99995	0.99296	0.99602	1.00619	0.98989	
31	1.5260+01	5.5359+00	NM	0.99996	0.99471	0.99701	1.00465	0.99240	

INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIEST

69030102		THOMKE		PROFILE TABULATION			29 POINTS, DELTA AT POINT 25		
I	Y	PTZ/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RH00*U/UD	
1	0.0000+00	1.0000+00	NM	1.01142	0.00000	0.00000	1.78061	0.00000	
2	7.1120+04	1.6839+00	NM	0.99404	2.49947	0.36490	1.50791	0.37403	
3	2.6162+03	2.0440+00	NM	0.99392	0.54614	0.65207	1.42626	0.45714	
4	3.9116+03	2.3035+00	NM	0.99414	0.59668	0.70900	1.37728	0.50825	
5	5.5800+03	2.4616+00	NM	0.99435	0.62518	0.72600	1.34944	0.53300	
6	7.8740+03	2.6814+00	NM	0.99463	0.66149	0.75600	1.31390	0.57691	
7	1.0617+02	2.8842+00	NM	0.99503	0.69329	0.78500	1.28284	0.61193	
8	1.2802+02	3.0134+00	NM	0.99527	0.71267	0.80100	1.26396	0.63372	
9	2.0777+02	3.3305+00	NM	0.99589	0.75791	0.83700	1.22020	0.68595	
10	2.3216+02	3.3968+00	NM	0.99602	0.76699	0.84400	1.21149	0.69666	
11	2.5857+02	3.4646+00	NM	0.99616	0.77616	0.85100	1.20271	0.70757	
12	3.0632+02	3.7420+00	NM	0.99672	0.81250	0.87000	1.16872	0.75157	
13	3.6043+02	3.9075+00	NM	0.99706	0.83338	0.88300	1.14863	0.77744	
14	4.1097+02	4.0701+00	NM	0.99739	0.85135	0.90700	1.13007	0.80260	
15	4.6203+02	4.1180+00	NM	0.99747	0.85915	0.91100	1.12472	0.80998	
16	5.1283+02	4.3040+00	NM	0.99787	0.88123	0.92600	1.10446	0.83842	
17	5.7887+02	4.5177+00	NM	0.99830	0.90549	0.94200	1.08250	0.87020	
18	6.4084+02	4.6793+00	NM	0.99863	0.92416	0.95400	1.06551	0.89509	
19	7.0637+02	4.8819+00	NM	0.99903	0.94650	0.96800	1.04604	0.92535	
20	7.6708+02	5.0030+00	NM	0.99926	0.95955	0.97600	1.03470	0.94327	
21	8.2906+02	5.2210+00	NM	0.99969	0.98290	0.99000	1.01455	0.97580	
22	8.9103+02	5.2881+00	NM	0.99981	0.98969	0.99400	1.00875	0.98536	
23	9.5479+02	5.3211+00	NM	0.99987	0.99311	0.99600	1.00584	0.99022	
24	1.0190+01	5.3543+00	NM	0.99944	0.99655	0.99300	1.00292	0.99507	
D 25	1.1191+01	5.3878+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.2197+01	5.3710+00	NM	0.99997	0.99827	0.99900	1.00146	0.99754	
27	1.3226+01	5.3710+00	NM	0.99997	0.99827	0.99900	1.00146	0.99754	
28	1.4232+01	5.3878+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
29	1.5321+01	5.3710+00	NM	0.99997	0.99827	0.99900	1.00146	0.99754	

INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIEST

69030701		THOMKE		PROFILE TABULATION		31 POINTS, DELTA AT POINT 29			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95587	0.00000	0.00000	2.65356	0.00000	
2	5.6420*+04	2.8342*+00	NM	0.96954	0.44863	0.63100	1.98070	0.31857	
3	2.0320*+03	3.8218*+00	NM	0.97455	0.53931	0.71900	1.78617	0.40254	
4	3.5400*+03	4.0859*+00	NM	0.97598	0.55766	0.73800	1.74093	0.42391	
5	5.0546*+03	4.3409*+00	NM	0.97730	0.57940	0.75500	1.69949	0.44425	
6	7.4422*+03	4.7805*+00	NM	0.97947	0.61252	0.78200	1.63177	0.47924	
7	9.7790*+03	5.0959*+00	NM	0.98083	0.63440	0.79900	1.58794	0.50317	
8	1.2725*+02	5.5129*+00	NM	0.98268	0.66272	0.82000	1.53253	0.53506	
9	1.5113*+02	5.7484*+00	NM	0.98364	0.67813	0.83100	1.50294	0.55292	
10	1.7450*+02	6.0291*+00	NM	0.98470	0.69357	0.84300	1.47073	0.57338	
11	2.0244*+02	6.2591*+00	NM	0.98560	0.71052	0.85300	1.44262	0.59129	
12	2.2733*+02	6.5105*+00	NM	0.98651	0.72590	0.86300	1.41469	0.61003	
13	2.5324*+02	6.8297*+00	NM	0.98762	0.74496	0.87500	1.38875	0.63171	
14	3.0353*+02	7.3485*+00	NM	0.98931	0.77492	0.89300	1.32899	0.67194	
15	3.5331*+02	7.8547*+00	NM	0.99081	0.80306	0.90700	1.28211	0.70589	
16	4.0411*+02	8.3371*+00	NM	0.99221	0.82899	0.92300	1.24042	0.74410	
17	4.5542*+02	9.1000*+00	NM	0.99418	0.86037	0.94300	1.17979	0.79929	
18	5.0521*+02	9.6051*+00	NM	0.99539	0.89352	0.95500	1.14280	0.83567	
19	5.6845*+02	1.0247*+01	NM	0.99681	0.92443	0.96900	1.09906	0.88166	
20	6.3277*+02	1.0591*+01	NM	0.99752	0.94059	0.97600	1.07696	0.90625	
21	6.9571*+02	1.1058*+01	NM	0.99845	0.96211	0.98500	1.04832	0.93960	
22	7.6022*+02	1.1443*+01	NM	0.99917	0.97946	0.99200	1.02586	0.96700	
23	8.2296*+02	1.1614*+01	NM	0.99948	0.98707	0.99500	1.01618	0.97915	
24	8.8671*+02	1.1788*+01	NM	0.99979	0.99479	0.99800	1.00648	0.99157	
25	9.5377*+02	1.1907*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.0132*+01	1.1907*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
27	1.1151*+01	1.1907*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
28	1.2174*+01	1.1907*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
29	1.3183*+01	1.1907*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 30	1.4193*+01	1.1730*+01	NM	0.99967	0.99221	0.99700	1.00972	0.98740	
31	1.5200*+01	1.1499*+01	NM	0.99927	0.98198	0.99300	1.02264	0.97102	

INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIEST

69030702		THOMKE		PROFILE TABULATION		31 POINTS, DELTA AT POINT 29			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.95730	0.00000	0.00000	2.62348	0.00000	
2	7.1120*+04	2.7466*+00	NM	0.96875	0.44415	0.62400	1.97632	0.31574	
3	2.6162*+03	3.6595*+00	NM	0.97433	0.52963	0.70900	1.79418	0.39517	
4	3.9116*+03	4.0291*+00	NM	0.97637	0.56078	0.73700	1.72925	0.42620	
5	5.3880*+03	4.2941*+00	NM	0.97774	0.58175	0.75500	1.68622	0.44775	
6	7.8740*+03	4.6303*+00	NM	0.97938	0.60727	0.77600	1.63473	0.47469	
7	1.0617*+02	4.9624*+00	NM	0.98091	0.63142	0.79500	1.58697	0.50095	
8	1.2802*+02	5.1681*+00	NM	0.98182	0.64590	0.80600	1.55860	0.51706	
9	1.5601*+02	5.4494*+00	NM	0.98300	0.66492	0.82000	1.52241	0.53062	
10	1.7932*+02	5.6535*+00	NM	0.98377	0.67751	0.82700	1.49869	0.53315	
11	2.0777*+02	5.8973*+00	NM	0.98481	0.69476	0.84100	1.46667	0.53341	
12	2.3216*+02	5.9697*+00	NM	0.98507	0.69917	0.84400	1.45859	0.53664	
13	2.5957*+02	6.1330*+00	NM	0.98577	0.71109	0.85200	1.43692	0.54294	
14	3.0632*+02	6.4485*+00	NM	0.98685	0.72948	0.86400	1.40404	0.61537	
15	3.6043*+02	6.8443*+00	NM	0.98821	0.75341	0.87900	1.36231	0.64523	
16	4.1097*+02	7.1843*+00	NM	0.98932	0.77335	0.89100	1.32841	0.67072	
17	4.6203*+02	7.6098*+00	NM	0.99063	0.79761	0.90500	1.28831	0.70247	
18	5.1283*+02	8.0360*+00	NM	0.99186	0.82117	0.91800	1.25052	0.73410	
19	5.7887*+02	8.9692*+00	NM	0.99331	0.84473	0.93300	1.20624	0.77347	
20	6.4084*+02	9.1120*+00	NM	0.99468	0.87783	0.94700	1.16432	0.81335	
21	7.0617*+02	9.6187*+00	NM	0.99586	0.90316	0.95900	1.12788	0.85027	
22	7.6708*+02	1.0068*+01	NM	0.99686	0.92523	0.96900	1.09717	0.88318	
23	8.3906*+02	1.0481*+01	NM	0.99767	0.94355	0.97700	1.07238	0.91105	
24	8.9103*+02	1.0804*+01	NM	0.99837	0.96012	0.98400	1.05053	0.93667	
25	9.5479*+02	1.1120*+01	NM	0.99898	0.97473	0.99000	1.03167	0.95961	
26	1.0140*+01	1.1450*+01	NM	0.99959	0.98975	0.99600	1.01271	0.98350	
27	1.1191*+01	1.1621*+01	NM	0.99990	0.99742	0.99900	1.00318	0.99583	
28	1.2197*+01	1.1678*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 29	1.3226*+01	1.1678*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
30	1.4232*+01	1.1563*+01	NM	0.99980	0.99485	0.99800	1.00636	0.99169	
31	1.5221*+01	1.1621*+01	NM	0.99990	0.99742	0.99900	1.00318	0.99583	

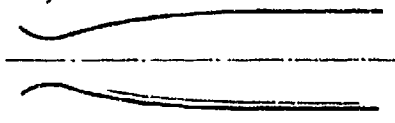
INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIEST

69031201		THOMKC		PROFILE TABULATION			31 POINTS, DELTA AT POINT 2A		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.87442	0.00000	0.00000	3.58927	0.00000	
2	5.8420*+04	2.9515*+00	NM	0.92966	0.34831	0.57942	2.77192	0.20903	
3	2.0320*+03	4.3039*+00	NM	0.94433	0.43615	0.60032	2.43722	0.27914	
4	1.5560*+03	4.7431*+00	NM	0.94832	0.46091	0.70529	2.34556	0.30069	
5	5.0546*+03	5.1337*+00	NM	0.95177	0.48181	0.72527	2.26972	0.31954	
6	7.4422*+03	5.7254*+00	NM	0.95586	0.51181	0.75225	2.16378	0.34765	
7	9.7790*+03	6.1418*+00	NM	0.95866	0.53188	0.76923	2.09499	0.36718	
8	1.2725*+02	6.7683*+00	NM	0.96252	0.56070	0.79221	1.99935	0.39623	
9	1.5113*+02	7.0972*+00	NM	0.96439	0.57524	0.80320	1.95256	0.41136	
10	1.7450*+02	7.3496*+00	NM	0.96576	0.58616	0.81119	1.91810	0.42291	
11	2.0244*+02	7.7897*+00	NM	0.96800	0.60454	0.82418	1.86135	0.44278	
12	2.2733*+02	8.2950*+00	NM	0.97044	0.62532	0.83816	1.79918	0.46586	
13	2.5324*+02	8.7683*+00	NM	0.97255	0.64401	0.85015	1.74501	0.48719	
14	3.0353*+02	9.3239*+00	NM	0.97486	0.66529	0.86314	1.68543	0.51212	
15	3.5331*+02	1.0028*+01	NM	0.97754	0.69131	0.87812	1.61550	0.54356	
16	4.0411*+02	1.0755*+01	NM	0.98007	0.71719	0.89211	1.54910	0.57589	
17	4.5542*+02	1.1391*+01	NM	0.98207	0.73873	0.90310	1.49615	0.60361	
18	5.0521*+02	1.2002*+01	NM	0.98408	0.76146	0.91409	1.44254	0.63367	
19	5.6445*+02	1.2947*+01	NM	0.98647	0.79003	0.92707	1.37829	0.67262	
20	6.3297*+02	1.3854*+01	NM	0.98868	0.81825	0.93906	1.31816	0.71240	
21	6.9571*+02	1.4860*+01	NM	0.99090	0.84850	0.95105	1.25721	0.75647	
22	7.6022*+02	1.5786*+01	NM	0.99276	0.87544	0.96104	1.20581	0.79701	
23	8.2296*+02	1.6597*+01	NM	0.99425	0.89828	0.96903	1.16429	0.83230	
24	8.8671*+02	1.7599*+01	NM	0.99592	0.92549	0.97802	1.11714	0.87547	
25	9.5377*+02	1.8552*+01	NM	0.99741	0.95117	0.98601	1.07486	0.91734	
26	1.0132*+01	1.9331*+01	NM	0.99852	0.97145	0.99201	1.04291	0.95119	
27	1.1131*+01	2.0164*+01	NM	0.99963	0.99269	0.99800	1.01076	0.98738	
D 28	1.2174*+01	2.0455*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
29	1.3183*+01	2.0164*+01	NM	0.99963	0.99269	0.99800	1.01076	0.98738	
30	1.4133*+01	1.9880*+01	NM	0.99926	0.98550	0.99600	1.02150	0.97504	
31	1.5260*+01	2.0021*+01	NM	0.99945	0.98908	0.99700	1.01613	0.98117	

INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIFT

69031202		THOMKC		PROFILE TABULATION			30 POINTS, DELTA AT POINT 30		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.88100	0.00000	0.00000	3.60239	0.00000	
2	7.1120*+04	3.0593*+00	NM	0.93301	0.35697	0.59041	2.74017	0.21546	
3	2.6162*+03	4.4095*+00	NM	0.94798	0.44284	0.60871	2.41296	0.28484	
4	3.9116*+03	4.9882*+00	NM	0.95239	0.47534	0.71920	2.29352	0.31361	
5	5.5880*+03	5.1911*+00	NM	0.95392	0.48604	0.72927	2.25503	0.32340	
6	7.8740*+03	5.6783*+00	NM	0.95734	0.51058	0.75125	2.16839	0.34645	
7	1.0617*+02	6.2671*+00	NM	0.96115	0.53914	0.77522	2.07080	0.37436	
8	1.2802*+02	6.5931*+00	NM	0.96309	0.55420	0.78721	2.02080	0.38955	
9	1.5621*+02	6.9413*+00	NM	0.96504	0.56984	0.79920	1.97000	0.40568	
10	1.7932*+02	7.2183*+00	NM	0.96652	0.58198	0.80819	1.93138	0.41845	
11	2.0777*+02	7.5769*+00	NM	0.96834	0.59733	0.81918	1.88356	0.43491	
12	2.3216*+02	8.0321*+00	NM	0.97051	0.61624	0.83217	1.82618	0.45569	
13	2.5847*+02	8.3307*+00	NM	0.97185	0.62834	0.84016	1.79040	0.46926	
14	3.0632*+02	8.8076*+00	NM	0.97389	0.64714	0.85215	1.73606	0.49085	
15	3.6943*+02	9.4129*+00	NM	0.97628	0.67034	0.86613	1.67165	0.51813	
16	4.1097*+02	9.9302*+00	NM	0.97818	0.68950	0.87712	1.62028	0.54134	
17	4.6203*+02	1.0128*+01	NM	0.97887	0.69670	0.88112	1.60143	0.55021	
18	5.1283*+02	1.0813*+01	NM	0.98113	0.72101	0.89411	1.53957	0.58075	
19	5.7867*+02	1.1505*+01	NM	0.98324	0.74480	0.90609	1.48162	0.61156	
20	6.4084*+02	1.2956*+01	NM	0.98713	0.79231	0.92807	1.37331	0.67979	
21	7.0637*+02	1.3629*+01	NM	0.98873	0.81342	0.93706	1.32822	0.70550	
22	7.6708*+02	1.4397*+01	NM	0.99033	0.83564	0.94605	1.28269	0.73756	
23	8.2906*+02	1.4527*+01	NM	0.99069	0.84074	0.94805	1.27251	0.74503	
24	8.9103*+02	1.5331*+01	NM	0.99230	0.86447	0.95704	1.22642	0.78036	
25	9.5479*+02	1.6105*+01	NM	0.99373	0.88672	0.96503	1.18507	0.81433	
26	1.0190*+01	1.7163*+01	NM	0.99553	0.91624	0.97502	1.13289	0.86065	
27	1.1191*+01	1.8376*+01	NM	0.99732	0.94789	0.98501	1.08015	0.91192	
28	1.3226*+01	2.0064*+01	NM	0.99964	0.99269	0.99800	1.01076	0.98738	
29	1.4232*+01	2.0354*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 30	1.5321*+01	2.0354*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD ASSUME P=PD AND VAN DRIFT

axisymmetric 	M : 19 to 21.6 R THETA X 10 ⁻³ : 8-12 TW/TR : 1.1	7001
		FPG / ZPG MHT / AW
Axially symmetric blow-down tunnel. Running time: 50 s. D = 0.56 m. PO : 13.6 MN/m ² . TO : 300 K. Helium. RE/m X 10 ⁻⁶ : 45.		
FISCHER M.C., MADDALON D.V., WEINSTEIN L.M. and WAGNER R.D. 1970. Boundary layer surveys on a nozzle wall at M = 20 including hot-wire fluctuation measurements. AIAA Paper 70-746. <u>And</u> Fischer M.C. private communications. <u>Also</u> Fischer, Maddalon, Weinstein & Wagner (1971) and Wagner, Maddalon & Weinstein (1970).		

- 1 The test boundary layer was formed on the wall of a contoured axisymmetric nozzle approximately 4 m long. The nozzle radius at the measuring stations is given in table 1, with X = 0 at the throat. The nozzle wall had a smooth polished surface and was not actively cooled. Calibration tests reported by Arrington et al.
- 2 (1964) indicate that Mach number variations across the test section at X = 3.531 m are about ± 0.3 so that
- 3 longitudinal variations from the mean expansion may be expected to be of the same order. Preston tube tests
- 4 by Wagner et al. (1970) at X = 2.066 indicated that transition at this point occurred when PO was about 3 MN/m². PO for the test described here is about 14 MN/m². The test boundary layer was formed by expansion in the nozzle, with a very strong simple wave generated expansion in the throat region followed by an extended simple wave cancelled expansion in which the nozzle contour and boundary layer growth give near zero longitudinal pressure gradient conditions at X = 3.53 m. The last test station (3.76 m) may be affected by the upstream influence of the APG flow in the diffuser.
- 6 Wall pressure measurements were made at 17 stations along the wall between X = 1.47 and 3.81 m with holes
- 7 2.3 mm in diameter. At the X = 3.53 m station the velocity profile was determined from PO, TO and P traverses. The Pitot probe was a CPP (d₁ = 3.2, d₂ = 2.6 mm) while two static probes (CCP - α = 42.5°, d = 3.2, l₁ = 11.7, l₂ = 94 mm) were mounted on a rake, separated vertically by 166 mm so that the outer
- 8 tube was always in the free stream. TO was measured with shielded tungsten resistance thermometers with
- 7 an oval shield entrance for which b₁ = 0.76, b₂ = 3 mm. At all other stations a Pitot rake only was used with 18 CPP (d₁ = 1.5, d₂ = 1.0, l = 25.4 mm) mounted at intervals of 6.4 mm near the wall, increasing to 19 mm in the outer region on the layer. At station X = 3.53 m a hot-wire survey of the layer was also made using the constant current techniques described by Wagner et al. (1970).
- 9 The static pressure profile measured at X = 3.5 m was replaced in data reduction by a series of linear variations (see source figure 14 inset and tables of section C below) and this variation was applied to all the other profiles presented here. The total temperature was within a few percent of tunnel total temperature throughout and the measured values were replaced by the isoenergetic assumption. A wall temperature of 300 K
- 10 was assumed. The Pitot measurements were corrected for real gas effects (Erickson, 1960) and viscous interaction and rarefaction effects (Beckwith et al., 1971 and Rogers et al., 1966). The maximum correction was a 20 % reduction of PT2, and at the relatively high pressure levels considered in this entry, only the first few data points near the wall received significant adjustments. Uncorrected Pitot data is tabulated
- 11 in the source. The viscosity law assumed was $\mu = 5.0236 (T/K)^{0.647} \times 10^{-7} \text{ N s/m}^2$.
- 12 The editors have accepted all the assumptions and adjustments made by the authors.† In order to do this it proved necessary to reconstitute the assumed static pressure profiles from the authors' description and the wall and free-stream static pressures. This procedure was followed since the tabulated data, although functionally complete, required the use of computed density data which was presented to one significant
- 13 figure. This profile set is the only one tabulated, but a great quantity of reduced integral data is also given in the source paper for a range of tunnel reservoir pressures. For this integral data, the static pressure was assumed constant. The hot wire data are presented graphically in the source and Fischer et al.
- 14 (1971). We present the authors' CF values estimated from the slope of the velocity profile at the wall.

† We have however calculated viscosity as discussed in the introduction.

§ DATA: 7001 0101-0105. Pitot profiles. TO and P profiles for 0104 only. $M_X = 5$.

15 Editors' comments

The three hypersonic contoured nozzle wall studies, including this entry, Beckwith et al. - CAT 7105 and Kemp & Owen - CAT 7206 provide the highest Mach number data in the catalogue. In all three there are strong normal pressure gradient effects, as although the radii of curvature are large, the dynamic pressure is orders of magnitude greater than the static pressure. The most thorough attack on the problems of measurement which result from this is that of Beckwith et al., whose correction procedures are used here. In addition to normal pressure gradient effects due to streamline curvature, at these Mach numbers, it is necessary to distinguish between the normal stress which must balance the centrifugal effects, and its component parts, the static pressure as such and the normal Reynolds stress due to turbulence, which is of the same order.

The profiles are given in average detail, and the measurements extend within the momentum deficit peak. With the boundary conditions used, replacement of the measured TO profile by the assumption of constant TO will have little effect on the reduced data. The influence of the PT2 corrections can be seen by comparing the tabulated values with the uncorrected values given in the source paper. The Mach number range of the series is not large so that the balance between the components of the static pressure variation should not change much from one station to another, and therefore the static pressure profile used at each station will be valid in so far as it represents the variation at the station at which it was measured.

As is typically the case with very high Mach number measurements, the profiles display marked transitional features.

TABLE 1

MEASURING STATION X:	2.007	2.743	3.302	3.631	3.760 m
NOZZLE RADIUS R:	203.2	236.2	273.1	278.1	279.4 mm

CAT 7001 FISCHER BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUN	MD *	T1/TR	RED2W	CF *	H12	H12K	PM	PD
X *	POD *	PK/PO	RED2D	CO	H32	H32K	TM*	TD
RZ *	TOD*	SI: *	D2	PI2	H42	D2K	UD	TR
70010101	19.0000	1.1150	2.4599 ⁺⁰²	2.6000 ⁻⁰⁴	337.7607	2.0510	1.1881 ⁺⁰²	6.6108 ⁺⁰¹
2.0066 ⁺⁰⁰	1.4238 ⁺⁰⁷	1.3500	8.2764 ⁺⁰³	NM	1.9520	1.7422	3.0000 ⁺⁰²	2.4713 ⁺⁰⁰
-2.0320 ⁻⁰¹	3.0000 ⁺⁰²	1.0000	1.6432 ⁻⁰⁴	NM	-0.3401	1.7740 ⁻⁰³	1.7583 ⁺⁰³	2.6906 ⁺⁰²
70010102	20.8000	1.1152	2.0476 ⁺⁰²	1.9500 ⁻⁰⁴	342.0757	2.0033	7.5831 ⁺⁰¹	5.6171 ⁺⁰¹
2.7432 ⁺⁰⁰	1.4238 ⁺⁰⁷	1.3500	8.3710 ⁺⁰³	NM	1.9277	1.6873	3.0000 ⁺⁰²	2.0649 ⁺⁰⁰
-2.3622 ⁻⁰¹	3.0000 ⁺⁰²	1.0000	1.7094 ⁻⁰⁴	NM	-0.0313	2.6614 ⁻⁰³	1.7595 ⁺⁰³	2.6901 ⁺⁰²
70010103	21.6000	1.1152	2.2405 ⁺⁰²	1.8000 ⁻⁰⁴	324.0265	2.0521	6.2873 ⁺⁰¹	4.6573 ⁺⁰¹
3.3020 ⁺⁰⁰	1.4233 ⁺⁰⁷	1.3500	9.4151 ⁺⁰³	NM	1.9396	1.7287	3.0000 ⁺⁰²	1.9157 ⁺⁰⁰
-2.7305 ⁻⁰¹	3.0000 ⁺⁰²	1.0000	2.1994 ⁻⁰⁴	NM	0.1973	2.8089 ⁻⁰³	1.7599 ⁺⁰³	2.6900 ⁺⁰²
70010104	21.6000	1.1152	2.4039 ⁺⁰²	1.7500 ⁻⁰⁴	303.6261	1.9064	6.1350 ⁺⁰¹	4.5444 ⁺⁰¹
3.5306 ⁺⁰⁰	1.3893 ⁺⁰⁷	1.3500	1.0531 ⁺⁰⁴	NM	1.9329	1.7383	3.0000 ⁺⁰²	1.9157 ⁺⁰⁰
-2.7813 ⁻⁰¹	3.0000 ⁺⁰²	1.0000	2.4285 ⁻⁰⁴	NM	0.3212	3.4172 ⁻⁰³	1.7599 ⁺⁰³	2.6900 ⁺⁰²
70010105	21.5000	1.1152	2.7945 ⁺⁰²	NM	328.4272	2.1372	6.4027 ⁺⁰¹	4.7427 ⁺⁰¹
3.7592 ⁺⁰⁰	1.4169 ⁺⁰⁷	1.3500	1.2144 ⁺⁰⁴	NM	1.9437	1.7314	3.0000 ⁺⁰²	1.9335 ⁺⁰⁰
-2.7940 ⁻⁰¹	3.0000 ⁺⁰²	1.0000	2.7077 ⁻⁰⁴	NM	0.1531	3.2355 ⁻⁰³	1.7599 ⁺⁰³	2.6900 ⁺⁰²

CF ESTIMATED FROM FIG.7

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD	H12PD	H32PD	H42PD	RED2PD	RED2PDH	DBTAK
	D2PH	H12PH	H32PH	H42PH	RED2PHD	RED2PHH	
70010101	1.6666 ⁻⁰⁴	341.0896	1.9527	-0.3347	8.3955 ⁺⁰³	2.4953 ⁺⁰²	5.4084 ⁻⁰²
	1.3937 ⁻⁰⁴	330.7443	1.9536	-0.3346	8.3995 ⁺⁰³	2.4965 ⁺⁰²	
70010102	1.6050 ⁻⁰⁴	355.2281	1.9283	-0.0310	8.4438 ⁺⁰³	2.0654 ⁺⁰²	5.9167 ⁻⁰²
	1.5089 ⁻⁰⁴	344.8848	1.9291	-0.0310	8.4472 ⁺⁰³	2.0662 ⁺⁰²	
70010103	2.2300 ⁻⁰⁴	333.3162	1.9407	0.1942	9.9965 ⁺⁰³	2.2819 ⁺⁰²	6.7386 ⁻⁰²
	1.8647 ⁻⁰⁴	323.5885	1.9413	0.1942	1.0000 ⁺⁰⁴	2.2827 ⁺⁰²	
70010104	2.4534 ⁻⁰⁴	312.5020	1.9341	0.3153	1.0727 ⁺⁰⁴	2.4487 ⁺⁰²	6.9143 ⁻⁰²
	2.0507 ⁻⁰⁴	303.2406	1.9348	0.3152	1.0731 ⁺⁰⁴	2.4495 ⁺⁰²	
70010105	2.7366 ⁻⁰⁴	350.1207	1.9444	0.1513	1.2274 ⁺⁰⁴	2.6244 ⁺⁰²	8.3128 ⁻⁰²
	2.2875 ⁻⁰⁴	336.2742	1.9451	0.1512	1.2279 ⁺⁰⁴	2.6254 ⁺⁰²	

70010102 FISCHER PROFILE TABULATION 21 POINTS, DELTA AT POINT 19

I	Y	PT2/P	P/PO	T0/T00	H/H0	U/UD	T/TD	RHO/RH00*U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	1.35000	1.07875	0.00000	0.00000	156.72600	0.00000
2	1.7780 ⁻⁰³	1.2490 ⁺⁰⁰	1.35000	1.07107	0.02539	0.30300	142.36354	0.00287
3	5.0800 ⁻⁰³	2.6250 ⁺⁰⁰	1.35000	1.05179	0.05750	0.58400	103.60086	0.00761
4	7.5692 ⁻⁰³	4.9406 ⁺⁰⁰	1.35000	1.03751	0.08377	0.72500	74.89436	0.01307
5	1.0100 ⁻⁰²	2.2428 ⁺⁰¹	1.35000	1.01123	0.18596	0.92100	24.52859	0.05069
6	1.3538 ⁻⁰²	3.7394 ⁺⁰¹	1.35000	1.00737	0.24111	0.95200	15.59008	0.08244
7	1.9736 ⁻⁰²	5.3797 ⁺⁰¹	1.35000	1.00532	0.28973	0.96700	11.13916	0.11719
8	2.6111 ⁻⁰²	8.1195 ⁺⁰¹	1.24500	1.00377	0.35644	0.97900	7.54369	0.16157
9	3.2944 ⁻⁰²	1.2609 ⁺⁰²	1.10500	1.00138	0.44463	0.98700	4.92772	0.22133
10	3.7675 ⁻⁰²	2.0393 ⁺⁰²	0.91500	1.00046	0.56583	0.99300	3.07983	0.28501
11	4.6482 ⁻⁰²	2.3844 ⁺⁰²	0.80500	0.99940	0.61192	0.99400	2.63862	0.30325
12	5.8242 ⁻⁰²	3.1839 ⁺⁰²	0.88000	1.00084	0.70728	0.99700	1.98706	0.42147
13	7.1196 ⁻⁰²	3.9663 ⁺⁰²	0.88000	1.00014	0.78957	0.99800	1.59763	0.54972
14	8.4455 ⁻⁰²	5.0431 ⁺⁰²	0.92000	0.99980	0.89037	0.99900	1.25890	0.73007
15	9.7155 ⁻⁰²	5.6912 ⁺⁰²	0.96000	0.99881	0.94590	0.99900	1.11543	0.85980
16	1.1062 ⁻⁰¹	5.8845 ⁺⁰²	1.00000	0.99856	0.96185	0.99900	1.07875	0.92607
17	1.2954 ⁻⁰¹	5.9860 ⁺⁰²	1.00000	1.00043	0.97011	1.00000	1.06257	0.94112
18	1.4880 ⁻⁰¹	6.1804 ⁺⁰²	1.00000	1.00020	0.98575	1.00000	1.02913	0.97170
19	1.6744 ⁻⁰¹	6.3803 ⁺⁰²	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
20	1.8618 ⁻⁰¹	6.2657 ⁺⁰²	1.00000	1.00010	0.99253	1.00000	1.01510	0.98512
21	2.0599 ⁻⁰¹	6.3671 ⁺⁰²	1.00000	0.99999	1.00054	1.00000	0.99892	1.00108

INPUT VARIABLES Y,U/UD,T/TD,P/PO

70010103		FISCHER	PROFILE TABULATION			20 POINTS, DELTA AT POINT 18			
I	Y	PTZ/P	P/PD	T/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	1.35000	1.00805	0.00000	0.00000	157.85988	0.00000	
2	1.7730"-03	1.1104"+00	1.35000	1.00764	0.01658	0.20400	151.31956	0.00182	
3	5.0800"-03	2.9774"+00	1.35000	1.00479	0.05991	0.60200	100.95867	0.00805	
4	7.5672"-03	1.9116"+01	1.35000	1.00087	0.11388	0.03200	49.02621	0.02291	
5	1.0160"-02	2.1579"+01	1.35000	1.00082	0.17562	0.71300	27.02520	0.04561	
6	1.3538"-02	3.3779"+01	1.35000	1.00051	0.22056	0.94300	18.31250	0.06952	
7	1.9736"-02	5.7221"+01	1.35000	0.99883	0.26749	0.76100	12.71673	0.10202	
8	2.6111"-02	6.2145"+01	1.35000	0.99957	0.30074	0.96900	10.43044	0.12542	
9	3.2944"-02	9.0563"+01	1.29250	0.99887	0.36261	0.97900	7.28931	0.17359	
10	3.9675"-02	1.1469"+02	1.16750	0.99971	0.44256	0.98700	4.97379	0.23168	
11	5.5242"-02	2.7860"+02	0.82500	0.99928	0.63705	0.99500	2.43952	0.33649	
12	7.1176"-02	3.5963"+02	0.82500	1.00009	0.71478	0.99700	1.94556	0.42277	
13	8.4455"-02	4.1804"+02	0.85500	0.99930	0.58310	0.99300	1.52520	0.55946	
14	9.7155"-02	5.7934"+02	0.88250	0.99989	0.37843	0.99700	1.24335	0.68166	
15	1.1062"-01	6.1599"+02	0.91250	0.99873	0.74697	0.99900	1.11290	0.81911	
16	1.2954"-01	6.7163"+02	0.95500	0.99814	0.98957	0.99900	1.01915	0.93612	
17	1.4834"-01	6.8037"+02	1.00000	1.00005	0.99597	1.00000	1.00000	0.99200	
D 18	1.6744"-01	6.8586"+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
19	1.8613"-01	6.8051"+02	1.00000	0.99825	0.98135	0.99900	1.03629	0.96402	
20	2.0579"-01	6.8037"+02	1.00000	1.00005	0.99597	1.00000	1.00000	0.99200	

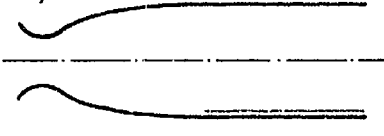
INPUT VARIABLES Y,U/UD,T/TD,P/PD

70010104		FISCHER	PROFILE TABULATION			21 POINTS, DELTA AT POINT 20			
I	Y	PTZ/P	P/PD	T/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	1.35000	1.00000	0.00000	0.00000	156.59700	0.00000	
2	1.7750"-03	1.1247"+00	1.35000	0.99998	0.01757	0.21500	149.40200	0.00194	
3	3.3020"-03	1.2809"+00	1.35000	0.99957	0.02567	0.30800	141.77600	0.00293	
4	4.0640"-03	1.9766"+00	1.35000	0.99972	0.04488	0.49000	119.19500	0.00555	
5	5.3340"-03	2.7423"+00	1.35000	0.99900	0.05685	0.58000	104.08200	0.00752	
6	6.8580"-03	4.9773"+00	1.35000	0.99984	0.09101	0.71300	77.47200	0.01242	
7	8.1280"-03	8.0213"+00	1.35000	0.99901	0.10501	0.79700	57.60000	0.01868	
8	1.2446"-02	1.7514"+01	1.35000	0.99914	0.15778	0.89400	32.10300	0.03759	
9	1.7018"-02	2.8970"+01	1.35000	0.99851	0.20400	0.93300	20.91800	0.06021	
10	2.1082"-02	3.8088"+01	1.35000	0.99968	0.23422	0.94900	16.41600	0.07904	
11	3.7338"-02	7.5500"+01	1.22500	0.99849	0.37241	0.98000	6.92500	0.17336	
12	5.1054"-02	1.9606"+02	0.93000	0.99980	0.53423	0.99200	3.44800	0.26756	
13	6.2738"-02	2.7406"+02	0.90500	0.99951	0.61183	0.99500	2.09800	0.32297	
14	7.4422"-02	3.6912"+02	0.83000	0.99946	0.73360	0.99700	1.84700	0.44803	
15	9.2964"-02	5.0483"+02	0.87000	0.99329	0.85767	0.99000	1.35400	0.64126	
16	1.0414"-01	5.5337"+02	0.89550	0.99946	0.90224	0.99900	1.22600	0.72959	
17	1.1074"-01	6.2303"+02	0.90550	0.99864	0.95330	0.99900	1.09800	0.82386	
18	1.2649"-01	6.7305"+02	0.94250	0.99812	0.99062	0.99900	1.01700	0.92582	
19	1.3605"-01	6.7772"+02	0.96500	0.99803	0.99404	0.99900	1.01000	0.95449	
D 20	1.5240"-01	6.8586"+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
21	1.8034"-01	7.0149"+02	1.00000	0.99985	1.01170	1.00000	0.97700	1.02344	

INPUT VARIABLES Y,U/UD,T/TD,P/PD

70010105		FISCHER	PROFILE TABULATION			20 POINTS, DELTA AT POINT 19			
I	Y	PTZ/P	P/PD	T/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	1.35000	1.01833	0.00000	0.00000	158.00407	0.00000	
2	3.1496"-03	1.2168"+00	1.35000	1.01674	0.02302	0.27800	145.84420	0.00257	
3	6.3500"-03	1.2531"+00	1.35000	1.01089	0.06358	0.02500	96.63136	0.00873	
4	8.7154"-03	1.2162"+01	1.35000	1.00423	0.13130	0.85700	42.60183	0.02718	
5	1.0160"-02	1.9018"+01	1.35000	1.00235	0.16536	0.90300	29.62179	0.04088	
6	1.4910"-02	3.1329"+01	1.35000	1.00099	0.21326	0.93900	19.38798	0.06538	
7	2.1107"-02	4.3857"+01	1.35000	1.00013	0.25284	0.95600	14.29633	0.09027	
8	2.7483"-02	5.2873"+01	1.35000	1.00088	0.27786	0.96400	12.03666	0.10812	
9	3.4315"-02	6.4804"+01	1.35000	1.00088	0.30786	0.97100	9.94807	0.13177	
10	4.1046"-02	9.5636"+01	1.35000	0.99946	0.35419	0.97800	7.62424	0.17317	
11	5.9614"-02	1.8156"+02	1.11000	0.99948	0.51643	0.98100	3.68228	0.29873	
12	7.2568"-02	2.6838"+02	0.93500	0.99982	0.62814	0.99500	2.50916	0.37077	
13	8.5827"-02	3.5116"+02	0.80500	1.00001	0.71865	0.99700	1.92404	0.41700	
14	9.8527"-02	4.1401"+02	0.82500	1.00013	0.78039	0.99800	1.63544	0.50344	
15	1.1179"-01	4.8349"+02	0.84500	0.99861	0.84340	0.99800	1.40020	0.60228	
16	1.3091"-01	5.5971"+02	0.87500	0.99930	0.90750	0.99900	1.21811	0.72134	
17	1.5022"-01	6.2476"+02	0.90750	0.99857	0.95883	0.99900	1.08554	0.83515	
18	1.6881"-01	6.4847"+02	0.93750	0.99831	0.97687	0.99900	1.04582	0.89553	
D 19	1.8759"-01	6.7953"+02	0.96750	1.00000	1.00000	1.00000	1.00000	0.96750	
20	2.0737"-01	6.6610"+02	1.00000	0.99833	0.99007	0.99910	1.01833	0.98112	

INPUT VARIABLES Y,U/UD,T/TD,P/PD

axisymmetric 	M : 5.9 R THETA X 10 ⁻³ : 8 - 80 TW/TR : 0.7 - 0.8	7002
		ZFG (FPG HISTORY) MHT
Axisymmetric blow-down tunnel, maximum running time 6 minutes. D = 305 mm. 0.45 < P0 < 4.24 MN/m ² . 460 < T0 < 500 K. Air, dew point : 211 K. 4 < RE/m X 10 ⁻⁶ < 35.		
JONES R.A. and FELLER W.V., 1970. Preliminary surveys of the wall boundary layer in a Mach 6 axisymmetric tunnel. NASA TN D-5620. And Feller W.V., private communication, Also Feller (1973).		

- 1 The test boundary layer was formed on a cylindrical extension (D = 0.305, L = 4.0 m) of a contoured axisymmetric nozzle. The cylinder was constructed in four interchangeable sections (L = 0.457, 0.761, 1.22 and 1.525 m) of which the longest carried the survey equipment. Four stations (X = 2.388, 3.150, 4.369, 5.461 m) were studied in the test zone stretching up to more than 6 m from the throat (X = 0). The test surface when constructed was finished to better than 1.6 μ m rms with a maximum departure from the prescribed ordinates of 0.013 mm. The surface was not actively cooled. Pitot surveys in the "inviscid" core flow showed
- 2 no asymmetry or waves. Natural transition was believed to occur upstream of the throat, and the pressure
- 3 history of the layer is represented by the Mach number distribution in Table 1. The wall temperature history is discussed by Feller (1973) and in the cases discussed here probably corresponds to TW/TR between 0.7 and
- 4 0.8 throughout (E).
- 6 Wall measurements generally suffered from undetermined instrumental difficulties, so that the static pressure presented with the profiles is deduced from Pitot measurements in the free stream. The wall temperatures were measured by thermocouples, each held by a screw in contact with the bottom of a drilled hole so as to sense the temperature 2 mm from the test surface.
- 7 A CPP and a circular STP were mounted permanently in the free stream and their readings recorded in conjunction with the traversing probes, which were in general of the same construction. Two probes were mounted on the traverse strut at any one time. The probe dimensions and Y separation are listed in table 2. The Pitot probes were FPP and the T0 probes flattened circular STP in which the chromel-alumel thermocouple bead had itself been flattened so as to increase the surface area to volume ratio, with the aim of giving a more rapid response and reducing sensitivity to conduction errors. The TTP were calibrated directly in the free stream over a wide range of Reynolds numbers. The calibration was extrapolated where necessary in the low Reynolds
- 10 number range. No corrections other than this calibration were applied to probe data. An empirical curve
- 11 fitted to a compilation of viscosity data was used.
- 9 Since the PT2 and T0 profiles were taken on separate occasions and at different Y values, the Pitot data were faired and interpolated to the Y values of the T0 data. All values were normalized with the simultaneous value recorded by the fixed free stream probes. The wall temperature values presented were obtained from the initial no-flow value with a correction based on a heat transfer calculation. The computed variation of TW was usually less than 22 K in the course of a run. Long period total pressure fluctuations of up to 2.5 % were observed in the middle part of the layer and it is suggested that these fluctuations may account for some of the scatter in the profile data.
- 12 The profile measurements are presented in the tables for all Y values of both the T0 probes. Where two Y values coincided, the profile data were averaged. The U/UD and M values have been taken as presented by the authors, and the variations in edge conditions averaged to give reference values representative of the whole profile (The source paper gives TOD and TW values for every profile point). The static pressure has been assumed constant through the boundary layer. Our normal integration procedure proved unable to
- 13 handle the scatter of the data and was replaced by a trapezoidal integration rule. Four successive profiles are presented for each of four total pressure levels. The reservoir pressure variation within each series is negligible except for the last series, where there is a fall of 17 % from 0401 to 0404. Measurements
- 14

of skin friction in the same facility have been made by Srokowski et al. (1976). The possible use of this data is discussed in § 15 below.

§ DATA: 7002 0101-0404. Pitot and TO profiles obtained separately. NX = 4.

15 Editors' comments

The experiment provides data in a region which is not well covered. In Reynolds number and Mach number range it falls between Voisinet & Lee - CAT 7202 and Hopkins & Keener - CAT 7203. The test area is cylindrical and δ/RZ is of order 0.7, so that the effect of transverse curvature may well be substantial. Although we have described the flow as having a nominally zero pressure gradient, the growth of the boundary layer results in a rise in pressure ratio (P/P_0) of 36 - 55 % between stations 1 and 4 (see source, figures 7 and 8). In the tables of reduced data below, this is masked for series 04 by the fall in POD.

The data is fairly rough, and showed much scatter. As remarked above, our spline-fit integration procedure was replaced by a trapezoidal rule. We still found differences of 50 % between the authors' integral values and ours, and so made a check by "counting squares". The trapezoidal rule and quadrature values agreed to 1 %, so that we presume that the authors' integration procedure was also unsuited to the spread of the data.

We give below a table of CF values based on the measurements of Srokowski et al. (1976). These measurements were made between Stations 1 and 2, with two different balances. Six or more years have passed between the two sets of measurements, so that there may well have been significant changes in the facility. We have not therefore entered any of these values in the profile tables. The scatter of the data was about 7 %, and we have interpolated on the basis of the authors' RE (x) values. We have very slightly extrapolated the curve in two cases, and although the Reynolds number range overlaps, values for stations 3 and 4 should only be used for very approximate arguments.

CF FROM SROKOWSKI et al. (1976)

PROFILE:	0103	0104	0202	0203	0204	0301	0302	0303	0401
CFX10 ⁴ :	8.60	8.05	8.30	7.65	7.30	7.40	6.98	6.53	6.60
NOTE:	a,b	a	b	a	a	-	-	a	-

a) Profile station remote from balance station

b) Extrapolated value.

Table 1. Design Mach number history in nozzle

X (m)	0	0.051	0.102	0.152	0.200	0.254	0.381
M	1.0	1.22	1.44	1.66	1.87	2.08	2.65
X (m)	0.584	0.788	0.939	1.270	1.421	1.929	2.260
M	3.54	4.29	4.70	5.32	5.54	5.89	5.99

Table 2. Dimensions of probes (mm)

	Outer TPP	Inner TPP	Outer TTP	Inner TTP
h_1	0.46	0.33	1.8	1.1
h_2	0.25	0.10	-	-
b_1	1.9	0.79	3.9	4.6
b_2	1.6	0.41	-	-
l	47.6	35 (E)	47.6	47.6
shank dia.	1.52	0.508	3.15	3.15
Separation in Y		24.1		20.5

CAT 7002		JOHNS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.					
RUN X *	ID * Y00*	TOTR PW/PD*	RED2W RLD2D	CF C7	H12 H32	H12M H32K	PH UD*	PD TD	
RZ *	T00*	SW *	D2	P12	H42	D2K	UD	TR	
70020101	5.8600	0.8037	1.5522 ⁺⁰³	MM	12.3030	1.3754	3.2938 ⁺⁰²	3.2938 ⁺⁰²	
2.3876 ⁺⁰⁰	4.5000 ⁺⁰⁵	1.0000	7.4970 ⁺⁰³	MM	1.8490	1.8192	3.3308 ⁺⁰²	5.7936 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.5584 ⁺⁰²	0.0000	1.7580 ⁻⁰³	MM	0.5522	4.1650 ⁻⁰³	8.9430 ⁺⁰²	4.1446 ⁺⁰²	
70020102	5.7600	0.8118	2.0486 ⁺⁰³	MM	12.6203	1.3905	3.6583 ⁺⁰²	3.6583 ⁺⁰²	
3.1496 ⁺⁰⁰	4.5000 ⁺⁰⁵	1.0000	9.7178 ⁺⁰³	MM	1.8373	1.8090	3.3098 ⁺⁰²	5.8702 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.4022 ⁺⁰²	0.0000	2.1292 ⁻⁰³	MM	0.5107	5.2677 ⁻⁰³	8.8483 ⁺⁰²	4.0771 ⁺⁰²	
70020103	5.5800	0.8043	3.1905 ⁺⁰³	MM	11.4970	1.4011	4.4340 ⁺⁰²	4.4340 ⁺⁰²	
4.3688 ⁺⁰⁰	4.5000 ⁺⁰⁵	1.0000	1.4107 ⁺⁰⁴	MM	1.8251	1.8037	3.3966 ⁺⁰²	6.4184 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.6388 ⁺⁰²	0.0000	3.0111 ⁻⁰³	MM	0.5964	7.3751 ⁻⁰³	8.9631 ⁺⁰²	4.2231 ⁺⁰²	
70020104	5.4500	0.7748	4.4337 ⁺⁰³	MM	12.1542	1.4306	5.1091 ⁺⁰²	5.1091 ⁺⁰²	
5.4610 ⁺⁰⁰	4.5000 ⁺⁰⁵	1.0000	1.8384 ⁺⁰⁴	MM	1.8052	1.7942	3.2509 ⁺⁰²	6.6358 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.6056 ⁺⁰²	0.0000	3.6577 ⁻⁰³	MM	0.5238	9.3664 ⁻⁰³	8.9013 ⁺⁰²	4.1956 ⁺⁰²	
70020201	5.8700	0.8097	2.5419 ⁺⁰³	MM	11.6110	1.3632	5.7226 ⁺⁰²	5.7226 ⁺⁰²	
2.3876 ⁺⁰⁰	7.9000 ⁺⁰⁵	1.0000	1.2380 ⁺⁰⁴	MM	1.8602	1.8275	3.3600 ⁺⁰²	5.7335 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.5640 ⁺⁰²	0.0000	1.6637 ⁻⁰³	MM	0.6174	3.7770 ⁻⁰³	8.9504 ⁺⁰²	4.1495 ⁺⁰²	
70020202	5.8300	0.7487	3.2924 ⁺⁰³	MM	12.0163	1.3742	5.9666 ⁺⁰²	5.9666 ⁺⁰²	
3.1496 ⁺⁰⁰	7.9000 ⁺⁰⁵	1.0000	1.5490 ⁺⁰⁴	MM	1.8445	1.8171	3.3097 ⁺⁰²	5.9183 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.6149 ⁺⁰²	0.0000	2.0813 ⁻⁰³	MM	0.5865	4.7849 ⁻⁰³	8.9924 ⁺⁰²	4.1969 ⁺⁰²	
70020203	5.6700	0.7926	4.3691 ⁺⁰³	MM	12.5872	1.3731	7.0666 ⁺⁰²	7.0666 ⁺⁰²	
4.3688 ⁺⁰⁰	7.9000 ⁺⁰⁵	1.0000	1.9659 ⁺⁰⁴	MM	1.8326	1.8127	3.3322 ⁺⁰²	6.2181 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.6199 ⁺⁰²	0.0000	2.4784 ⁻⁰³	MM	0.4917	6.1600 ⁻⁰³	8.9644 ⁺⁰²	4.2041 ⁺⁰²	
70020204	5.5400	0.7672	6.2762 ⁺⁰³	MM	11.6539	1.3836	8.1291 ⁺⁰²	8.1291 ⁺⁰²	
5.4610 ⁺⁰⁰	7.9000 ⁺⁰⁵	1.0000	2.6359 ⁺⁰⁴	MM	1.8292	1.8133	3.2876 ⁺⁰²	6.5930 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.7063 ⁺⁰²	0.0000	3.2182 ⁻⁰³	MM	0.5637	7.7343 ⁻⁰³	9.0191 ⁺⁰²	4.2854 ⁺⁰²	
70020301	5.9500	0.7668	4.7789 ⁺⁰³	MM	12.3317	1.3310	1.4469 ⁺⁰³	1.4469 ⁺⁰³	
2.3876 ⁺⁰⁰	2.1700 ⁺⁰⁶	1.0000	2.2413 ⁺⁰⁴	MM	1.8690	1.8475	3.4306 ⁺⁰²	6.0914 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.9222 ⁺⁰²	0.0000	1.2709 ⁻⁰³	MM	0.5396	2.8207 ⁻⁰³	9.3108 ⁺⁰²	4.4736 ⁺⁰²	
70020302	5.9500	0.7643	7.8028 ⁺⁰³	MM	9.7060	1.3196	1.4469 ⁺⁰³	1.4469 ⁺⁰³	
3.1496 ⁺⁰⁰	2.1700 ⁺⁰⁶	1.0000	3.6559 ⁺⁰⁴	MM	1.8719	1.8443	3.4134 ⁺⁰²	6.0810 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.9130 ⁺⁰²	0.0000	2.0676 ⁻⁰³	MM	0.8341	4.2843 ⁻⁰³	9.3028 ⁺⁰²	4.4660 ⁺⁰²	
70020303	5.7500	0.7661	1.0545 ⁺⁰⁴	MM	10.2534	1.3180	1.7828 ⁺⁰³	1.7828 ⁺⁰³	
4.3688 ⁺⁰⁰	2.1700 ⁺⁰⁶	1.0000	4.6425 ⁺⁰⁴	MM	1.8607	1.8403	3.4868 ⁺⁰²	6.5729 ⁺⁰¹	
-1.5240 ⁻⁰¹	5.0036 ⁺⁰²	0.0000	2.4787 ⁻⁰³	MM	0.7274	5.3635 ⁻⁰³	9.3466 ⁺⁰²	4.5516 ⁺⁰²	
70020304	5.6000	0.7817	1.2465 ⁺⁰⁴	MM	11.4150	1.3146	1.9619 ⁺⁰³	1.9619 ⁺⁰³	
5.4610 ⁺⁰⁰	2.1700 ⁺⁰⁶	1.0000	5.4772 ⁺⁰⁴	MM	1.8552	1.8423	3.4222 ⁺⁰²	6.4944 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.8103 ⁺⁰²	0.0000	2.6513 ⁻⁰³	MM	0.5835	5.9767 ⁻⁰³	9.1453 ⁺⁰²	4.3778 ⁺⁰²	
70020401	5.9000	0.7773	9.2357 ⁺⁰³	MM	10.6693	1.3223	2.7411 ⁺⁰³	2.7411 ⁺⁰³	
2.3876 ⁺⁰⁰	4.2400 ⁺⁰⁶	1.0000	4.3839 ⁺⁰⁴	MM	1.8751	1.8527	3.6122 ⁺⁰²	6.2730 ⁺⁰¹	
-1.5240 ⁻⁰¹	5.1138 ⁺⁰²	0.0000	1.3645 ⁻⁰³	MM	0.7196	2.8301 ⁻⁰³	9.4961 ⁺⁰²	4.6472 ⁺⁰²	
70020402	5.8200	0.7887	1.1752 ⁺⁰⁴	MM	11.4914	1.3251	3.1497 ⁺⁰³	3.1497 ⁺⁰³	
3.1496 ⁺⁰⁰	4.1400 ⁺⁰⁶	1.0000	5.4753 ⁺⁰⁴	MM	1.8630	1.8421	3.6259 ⁺⁰²	6.3028 ⁺⁰¹	
-1.5240 ⁻⁰¹	5.0556 ⁺⁰²	0.0000	1.6035 ⁻⁰³	MM	0.5906	3.5356 ⁻⁰³	9.4099 ⁺⁰²	4.5975 ⁺⁰²	
70020403	5.7000	0.7988	1.7731 ⁺⁰⁴	MM	10.0131	1.3058	3.0964 ⁺⁰³	3.0964 ⁺⁰³	
4.3688 ⁺⁰⁰	3.8900 ⁺⁰⁶	1.0000	8.1749 ⁺⁰⁴	MM	1.8646	1.8466	3.5508 ⁺⁰²	6.3625 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.8873 ⁺⁰²	0.0000	2.3807 ⁻⁰³	MM	0.7507	5.0029 ⁻⁰³	9.2438 ⁺⁰²	4.4853 ⁺⁰²	
70020404	5.6900	0.7673	1.7247 ⁺⁰⁴	MM	12.0339	1.3142	3.1085 ⁺⁰³	3.1085 ⁺⁰³	
5.4610 ⁺⁰⁰	3.5500 ⁺⁰⁶	1.0000	7.4837 ⁺⁰⁴	MM	1.8585	1.8435	3.4621 ⁺⁰²	6.6336 ⁺⁰¹	
-1.5240 ⁻⁰¹	4.9580 ⁺⁰²	0.0000	2.3480 ⁻⁰³	MM	0.5181	5.3277 ⁻⁰³	9.2918 ⁺⁰²	4.5121 ⁺⁰²	


TRAPEZOIDAL RULE FOR ALL INTEGRATIONS

70020401		JONES		PROFILE TABULATION		50 POINTS, DELTA AT POINT 46			
I	Y	PT2/P	P/PD	T0/T00	M/HN	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.70510	0.00000	0.00000	5.74800	0.00000	
2	6.0960+04	4.9023+00	NM	0.79957	0.30936	0.60855	3.86950	0.15727	
3	1.0668+03	6.3280+00	NM	0.83777	0.35619	0.67399	3.58059	0.18824	
4	1.2192+03	6.5484+00	NM	0.84108	0.36288	0.68189	3.53107	0.19311	
5	1.6744+03	7.5319+00	NM	0.85893	0.39130	0.71536	3.34207	0.21405	
6	1.5258+03	7.7742+00	NM	0.86424	0.39799	0.72335	3.30327	0.21898	
7	2.2860+03	8.4620+00	NM	0.86771	0.41639	0.73993	3.15784	0.23432	
8	2.7432+03	8.9820+00	NM	0.87502	0.42977	0.75342	3.07335	0.24515	
9	3.2004+03	9.5186+00	NM	0.87880	0.44314	0.76491	2.97943	0.25673	
10	3.6576+03	1.0142+01	NM	0.88652	0.45819	0.77880	2.88903	0.26957	
11	4.1148+03	1.0859+01	NM	0.89189	0.47492	0.79219	2.78281	0.28471	
12	5.1816+03	1.1951+01	NM	0.89903	0.50000	0.81067	2.62875	0.30839	
13	5.3340+03	1.2061+01	NM	0.90398	0.50167	0.81387	2.63189	0.30973	
14	5.6388+03	1.2294+01	NM	0.90357	0.50669	0.81657	2.59716	0.31441	
15	7.0104+03	1.3574+01	NM	0.90647	0.53344	0.83235	2.43464	0.34188	
16	8.2296+03	1.4662+01	NM	0.91004	0.55518	0.84474	2.31511	0.36488	
17	1.1175+02	1.7156+01	NM	0.92092	0.60201	0.87032	2.09003	0.41641	
18	1.3868+02	2.0051+01	NM	0.92379	0.65217	0.89020	1.86315	0.47779	
19	1.6107+02	2.2749+01	NM	0.93659	0.69565	0.91005	1.71150	0.53175	
20	1.8288+02	2.5054+01	NM	0.94244	0.73077	0.92267	1.59416	0.57878	
21	2.0574+02	2.7829+01	NM	0.93947	0.77090	0.93106	1.45867	0.63829	
22	2.1031+02	2.8425+01	NM	0.93786	0.77926	0.93216	1.43091	0.64145	
23	2.1184+02	2.8545+01	NM	0.94476	0.78094	0.93596	1.43642	0.65159	
24	2.1641+02	2.9150+01	NM	0.95244	0.78930	0.94185	1.42391	0.66145	
25	2.1793+02	2.9393+01	NM	0.94723	0.79264	0.93975	1.40564	0.66856	
26	2.1946+02	2.9638+01	NM	0.95405	0.79599	0.94385	1.40603	0.67129	
27	2.2230+02	3.0007+01	NM	0.94566	0.80100	0.94075	1.37938	0.68201	
28	2.2708+02	3.0627+01	NM	0.94940	0.80936	0.94435	1.36137	0.69347	
29	2.3165+02	3.1127+01	NM	0.94667	0.81605	0.94135	1.33915	0.70519	
30	2.3622+02	3.1695+01	NM	0.95993	0.82358	0.95244	1.33742	0.71215	
31	2.4079+02	3.2325+01	NM	0.95950	0.83445	0.95434	1.30800	0.72962	
32	2.5146+02	3.3954+01	NM	0.95125	0.85284	0.95364	1.25035	0.76270	
33	2.5298+02	3.3951+01	NM	0.96343	0.85284	0.95774	1.26639	0.75785	
34	2.5603+02	3.4481+01	NM	0.95881	0.85953	0.95864	1.24390	0.77067	
35	2.6518+02	3.5683+01	NM	0.96420	0.87450	0.96393	1.21476	0.79351	
36	2.6975+02	3.6359+01	NM	0.96418	0.88244	0.96533	1.19533	0.80759	
37	2.8194+02	3.7731+01	NM	0.96634	0.89767	0.96913	1.18038	0.83518	
38	2.9718+02	3.9412+01	NM	0.96595	0.91973	0.97203	1.11695	0.87025	
39	3.1090+02	4.0841+01	NM	0.97896	0.93645	0.98102	1.09744	0.88392	
40	3.1547+02	4.1275+01	NM	0.97992	0.94147	0.98172	1.08732	0.90288	
41	3.3833+02	4.3330+01	NM	0.97967	0.96488	0.98531	1.07280	0.94486	
42	3.6271+02	4.5111+01	NM	0.99198	0.98495	0.99411	1.01868	0.97588	
43	3.6576+02	4.5283+01	NM	0.98280	0.98662	0.99971	1.00627	0.98154	
44	3.8405+02	4.5893+01	NM	0.99586	0.99331	0.99710	1.00765	0.98953	
45	4.1910+02	4.6507+01	NM	1.00180	1.00000	1.00000	1.00180	0.99910	
D 46	4.3886+02	4.6507+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
47	4.6402+02	4.6507+01	NM	0.99401	1.00000	0.99700	0.99401	1.00301	
48	4.9682+02	4.6507+01	NM	0.99023	1.00000	0.99510	0.99023	1.00492	
49	5.1511+02	4.6507+01	NM	0.99740	1.00000	0.99870	0.99740	1.00130	
50	5.6540+02	4.6507+01	NM	0.99401	1.00000	0.99700	0.99401	1.00301	

INPUT VARIABLES Y/R,U/UD,H ASSUME P=PD
AT I=2,21,30 DATA WERE AVERAGED

70020404		JONES		PROFILE TABULATION		27 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/T00	M/HN	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.69743	0.00000	0.00000	5.21344	0.00000	
2	6.0960+04	3.2278+00	NM	0.81087	0.25483	0.52642	4.26723	0.12336	
3	1.8238+03	5.4378+00	NM	0.85032	0.34446	0.65615	3.62818	0.18084	
4	3.0400+03	6.9484+00	NM	0.87893	0.38137	0.70152	3.38366	0.20733	
5	4.1148+03	7.2388+00	NM	0.88822	0.40246	0.72451	3.24072	0.22356	
6	5.6388+03	8.0830+00	NM	0.90102	0.42907	0.75089	3.08821	0.24302	
7	7.9248+03	9.2443+00	NM	0.91351	0.45870	0.77598	2.85899	0.27129	
8	1.3259+02	1.1492+01	NM	0.92121	0.51318	0.81876	2.54548	0.32165	
9	1.8136+02	1.3167+01	NM	0.92280	0.55185	0.84075	2.32111	0.36222	
10	2.0574+02	1.4193+01	NM	0.92330	0.57293	0.85139	2.20824	0.38555	
11	2.1793+02	1.4748+01	NM	0.92465	0.58524	0.85774	2.18805	0.39931	
12	2.3012+02	1.5354+01	NM	0.93262	0.59754	0.86693	2.10492	0.41186	
13	2.4079+02	1.5884+01	NM	0.93403	0.60808	0.87215	2.05700	0.42398	
14	2.5603+02	1.6604+01	NM	0.93979	0.62214	0.88062	2.00355	0.43953	
15	2.7889+02	1.7622+01	NM	0.93967	0.64148	0.88812	1.91683	0.46333	
16	3.0785+02	1.9158+01	NM	0.94461	0.66760	0.90081	1.80904	0.49784	
17	3.3223+02	2.0394+01	NM	0.95290	0.69069	0.91161	1.74203	0.52330	
18	3.8109+02	2.2856+01	NM	0.95428	0.73296	0.92500	1.59308	0.58084	
19	4.1300+02	2.4710+01	NM	0.96054	0.76274	0.93609	1.50621	0.62149	
20	5.0749+02	3.0791+01	NM	0.98030	0.85237	0.96608	1.28459	0.74205	
21	5.6083+02	3.5012+01	NM	0.97304	0.91037	0.97307	1.14250	0.85170	
22	6.1265+02	3.9567+01	NM	0.99076	0.95606	0.98917	1.07045	0.92407	
23	7.6048+02	4.2150+01	NM	1.00172	1.00000	1.00000	1.00172	0.99914	
D 24	7.7114+02	4.2150+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
25	8.2144+02	4.2150+01	NM	0.99672	1.00000	0.99836	0.99672	1.00164	
26	1.0211+01	4.2150+01	NM	1.02972	1.00000	1.01475	1.02972	0.98546	
27	9.7079+02	4.2150+01	NM	1.02992	1.00000	1.01485	1.02992	0.98537	

INPUT VARIABLES Y/R,U/UD,H ASSUME P=PD
AT I=2,10 DATA WERE AVERAGED

	M : 1.75 to 3.00 in steps of 0.25 R THETA X 10 ⁻³ : 4 - 10 TW/TR : 0.9 - 1.02	7003
		7PG-AW-MHT
Continuous channel with interchangeable nozzle blocks. W = H = 0.10 m, L = 1 m. PO : 0.1 MN/m ² , 280 < TO < 420 K. Air, dew point 240 K. $5 < RE/M \times 10^{-6} < 14$.		
MEIER H.U., 1970. Experimentelle und theoretische Untersuchungen von turbulenten Grenzschichten bei Oberschallströmung. Mitt. M.P.I. und AVA no. 49. And Meier H.U. private communications. Also (Data superseded) Meier (1969) and (1967)		

- 1 The test boundary layer was formed on a flat wall facing an interchangeable nozzle block. The throat ($X=0$) was always at the same position and measurements could be made using six ports spaced at 45 mm intervals from $X = 425$ to 660 mm. The surface of the plate was polished and it was not actively cooled. Constant wall temperature was reached after one hour's running time. A calibration of the tunnel (Fütterer, 1967) showed that the maximum Mach number variation in the test region was 2 % and usually it was less. The nozzle walls were polished but disturbances due to joints could not be completely avoided. The location of the unforced transition zone was not determined. The test boundary layer had experienced the strong acceleration of the throat region.
- 6 Static pressure and wall temperature were measured at each profile station using an instrumented plug. The static tapping ($d = 0.4 - 0.5$ mm) and the thermocouple (chromel alumel) were 5 mm to either side of the centre line. Measurements were made simultaneously with the profile traverse.
- 7 Total pressure and total temperature profiles were obtained in a single traverse with a combined pitot / total temperature probe. The front face is circular ($d_1 = 0.48$, $d_2 = 0.40$ mm) and is followed by a conical section ($\alpha = 6.6^\circ(E)$, $i = 4.4$ mm) leading to a cylindrical support ($d_3 = 1.5$ mm). The overall length is 45 mm and the probe was inclined at 7° to the wall. A thermocouple bead is supported by its own leads 0.4 mm behind the opening. The leads are kept coaxial with the support tube by an insulating spacer so that the l/d ratio is greater than 100. The supporting spacer is located only by three ridges which allow air to pass through the probe and minimise conduction errors. The probe is used alternately as a CPP and as an STP, when the probe passage is switched to one of a series of calibrated orifices so that the mass flow may be regulated and measured. The effective thermocouple recovery temperature calibration is obtained as a function of the mass flow with the probe in the free stream, and becomes nearly constant when the mass flow is large enough. The design and procedure are further discussed by Meier (1967, 1969). In the test zone the wall static tappings and thermocouple beads were located in the plugs at each station on lines at $Z = \pm 5$ mm and at the X-value of the port centre. The traverses were made on the centre-line-normals through the port centres.
- 9 The data were reduced assuming constant static pressure through the layer. The wall shear stress was determined from the velocity profile using a best-fit matching procedure to Rotta's wall law and Coles' wake law in transformed coordinates. The author assumed a recovery factor of 0.896 and used Sutherland's viscosity law.
- 12 The editors have presented the data incorporating the authors' assumptions and calibration procedures. The boundary layer edge state (D state) is here calculated from the experimental data at the author's selected edge point. The author presents adiabatic wall data for six successive stations at six Mach numbers. This is presented in full (0101-0606). A series of single station tests was made at each Mach number, in which TW/TR was varied. These are presented as series 07 to 14. The author's shear stress data, deduced from the profiles, are also presented.
- 6 DATA: 7003 0101-1402. Pitot and TO profiles. NX = 6 or 1.

15 Editors' comments

The special interest of the experiment is the use of a fully developed combined pressure-temperature probe. The thermal conditions, however, are never severe. The experimental range is covered fully and systematically, but the upstream history is not known. Experiments with significantly overlapping ranges are those of Stalmach - CAT 5802 on a tunnel wall, and the flat plate tests of Coles - CAT 5301, Shutts et al. - CAT 5501 and Mabey et al. - CAT 7402.

The profiles are described in fine detail, but in about half the cases measurements do not extend within the momentum-deficit peak. There is evidence of considerable disturbance in the outer region of profile 0506.

CAT 7003

MEIER

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD TOD*	TW/TR PW/PD* SW *	RED2M RED2D D2	CF * CO PIZ*	M12 M32 M42	M12K M32K M2K	PM TM* UM	PD TD TR
70030101 4.2500*-01 INFINITE	1.7170 9.5170**+04 2.8600**+02	1.0031 1.0000 0.0000	4.8122**+03 6.8447**+03 4.9697**+04	2.3820**+03 NM 0.0000**+00	2.6760 1.8101 0.0200	1.3993 1.0015 5.8569**+04	1.0792**+04 2.7501**+02 4.0176**+02	1.0792**+04 1.7992**+02 2.7497**+02
70030102 4.7000*-01 INFINITE	1.6980 9.3094**+04 2.9830**+02	1.0031 1.0000 0.0000	5.0410**+03 7.1023**+03 5.5485**+04	2.2670**+03 NM 0.0000**+00	2.5881 1.8179 0.0300	1.3559 1.8124 0.4900**+04	1.0889**+04 2.0784**+02 4.0846**+02	1.0889**+04 1.8912**+02 2.8649**+02
70030103 5.1500*-01 INFINITE	1.7080 9.4047**+04 2.9240**+02	1.0054 1.0000 0.0000	5.6311**+03 7.9051**+03 6.0280**+04	2.1690**+03 NM 0.0000**+00	2.6860 1.8002 0.0162	1.3945 1.7909 7.1810**+04	1.0825**+04 2.0271**+02 4.0515**+02	1.0825**+04 1.8906**+02 2.8120**+02
70030104 5.6000*-01 INFINITE	1.6810 9.1139**+04 2.9350**+02	1.0031 1.0000 0.0000	6.4039**+03 8.9776**+03 6.9664**+04	2.0870**+03 NM 0.0000**+00	2.6735 1.7613 0.0280	1.4316 1.7647 0.3249**+04	1.4000**+04 2.0339**+02 4.0153**+02	1.4000**+04 1.8752**+02 2.8248**+02
70030105 6.0500*-01 INFINITE	1.7000 9.4926**+04 2.9010**+02	1.0034 1.0000 0.0000	7.1463**+03 1.0096**+04 7.4501**+04	2.0570**+03 NM 0.0000**+00	2.6178 1.8023 0.0210	1.3550 1.7955 0.0527**+04	1.4231**+04 2.7998**+02 4.0217**+02	1.4231**+04 1.8384**+02 2.7809**+02
70030106 6.5000*-01 INFINITE	1.6970 9.1874**+04 2.8560**+02	1.0072 1.0000 0.0000	7.0582**+03 1.0093**+04 7.4580**+04	2.0230**+03 NM 0.0000**+00	2.5947 1.8020 0.0297	1.3585 1.7961 0.8235**+04	1.0647**+04 2.0673**+02 4.5893**+02	1.0647**+04 1.8122**+02 2.7474**+02
70030201 4.2500*-01 INFINITE	1.9630 9.5574**+04 2.9370**+02	1.0151 1.0000 0.0000	3.6830**+03 5.7635**+03 4.7596**+04	2.3000**+03 NM 0.0000**+00	3.0390 1.8178 0.0361	1.3818 1.8081 5.0863**+04	1.2938**+04 2.0863**+02 5.0688**+02	1.2938**+04 1.8587**+02 2.8041**+02
70030202 4.7000*-01 INFINITE	1.9830 9.5250**+04 2.9840**+02	1.0078 1.0000 0.0000	3.9597**+03 6.1976**+03 5.2904**+04	2.2030**+03 NM 0.0000**+00	3.1271 1.8242 -0.0140	1.3868 1.8170 0.5518**+04	1.2900**+04 2.0847**+02 5.1384**+02	1.2900**+04 1.8703**+02 2.8474**+02
70030203 5.1500*-01 INFINITE	1.9410 9.6803**+04 2.9720**+02	1.0041 1.0000 0.0000	4.8637**+03 7.4777**+03 6.1377**+04	2.0450**+03 NM 0.0000**+00	3.0677 1.7860 0.0390	1.4201 1.7758 7.0727**+04	1.3550**+04 2.0508**+02 5.0669**+02	1.3550**+04 1.8048**+02 2.8342**+02
70030204 5.6000*-01 INFINITE	1.9020 9.5834**+04 2.9650**+02	0.9995 1.0000 0.0000	5.1829**+03 8.0432**+03 6.6686**+04	1.9880**+03 NM 0.0000**+00	2.9620 1.7994 0.0607	1.3739 1.7905 0.2719**+04	1.2945**+04 2.0244**+02 5.0914**+02	1.2945**+04 1.8752**+02 2.8309**+02
70030205 6.0500*-01 INFINITE	1.9410 9.9070**+04 2.9270**+02	1.0202 1.0000 0.0000	5.6131**+03 8.7506**+03 7.8971**+04	1.9270**+03 NM 0.0000**+00	2.9913 1.7960 0.0392	1.3703 1.7877 0.6800**+04	1.3428**+04 2.0542**+02 5.0780**+02	1.3428**+04 1.8642**+02 2.7862**+02
70030206 6.5000*-01 INFINITE	1.9680 9.5434**+04 2.9030**+02	1.0094 1.0000 0.0000	5.8200**+03 8.0453**+03 7.0115**+04	1.9160**+03 NM 0.0000**+00	3.0729 1.7914 0.0343	1.3883 1.7807 9.3210**+04	1.2819**+04 2.7973**+02 5.0467**+02	1.2819**+04 1.8950**+02 2.7712**+02
70030301 4.2500*-01 INFINITE	2.1940 9.6453**+04 2.9320**+02	1.0169 1.0000 0.0000	3.2377**+03 5.2345**+03 4.0202**+04	2.1700**+03 NM 0.0000**+00	3.3687 1.8233 0.0494	1.3419 1.8106 0.5981**+04	4.1054**+03 4.0293**+02 5.3765**+02	4.1054**+03 1.4038**+02 2.7824**+02
70030302 4.7000*-01 INFINITE	2.1990 9.6121**+04 2.9760**+02	1.0077 1.0000 0.0000	3.4194**+03 5.8052**+03 5.4081**+04	2.0650**+03 NM 0.0000**+00	3.4923 1.8025 0.0384	1.3944 1.7896 7.0809**+04	4.0034**+03 4.0457**+02 5.4238**+02	4.0034**+03 1.5129**+02 2.8238**+02
70030303 5.1500*-01 INFINITE	2.2140 9.7815**+04 2.9760**+02	1.0030 1.0000 0.0000	3.8156**+03 6.8914**+03 5.9862**+04	1.9910**+03 NM 0.0000**+00	3.4913 1.8010 0.0445	1.3820 1.7893 7.0504**+04	0.9444**+03 2.8312**+02 5.0417**+02	0.9444**+03 1.5848**+02 2.8228**+02
70030304 5.6000*-01 INFINITE	2.2390 9.9514**+04 2.9300**+02	0.9982 1.0000 0.0000	4.2562**+03 7.2962**+03 6.5489**+04	1.9150**+03 NM 0.0000**+00	3.4675 1.7984 0.0660	1.3605 1.7895 0.6076**+04	0.9544**+03 2.7724**+02 5.4300**+02	0.9544**+03 1.4631**+02 2.7774**+02
70030305 6.0500*-01 INFINITE	2.2180 9.6401**+04 2.8090**+02	1.0114 1.0000 0.0000	4.9944**+03 7.9213**+03 7.0556**+04	1.8750**+03 NM 0.0000**+00	3.4832 1.7963 0.0481	1.3754 1.7849 9.2813**+04	0.7651**+03 2.7424**+02 5.3878**+02	0.7651**+03 1.4801**+02 2.7210**+02
70030306 6.5000*-01 INFINITE	2.1780 9.6650**+04 2.8880**+02	1.0064 1.0000 0.0000	5.0222**+03 8.4789**+03 7.4565**+04	1.7850**+03 NM 0.0000**+00	3.4165 1.7874 0.0531	1.3856 1.7767 4.8168**+04	4.3500**+03 2.7595**+02 5.3161**+02	4.3500**+03 1.4820**+02 2.7418**+02

CAT 7003

MEIER

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X RZ	MD # P00 T00#	TW/TR PW/PD# SW #	REL2M RED2D D2	CF # CO PI2#	H12 H32 H42	H12M H32M H2K	PW TW# UD	PD ID TR
70030401 4.2500*-01 INFINITE	2.4170 9.7219*+04 2.9950*+02	1.0230 1.0000 0.0000	2.6499*+03 4.9466*+03 5.1301*-04	2.0610*-03 NM 0.0000*+00	3.7489 1.8077 0.9953	1.3759 1.7973 0.6733*-04	0.4756*+03 2.6923*+02 5.6730*+02	0.4756*+03 1.3412*+02 2.0272*+02
70030402 4.7000*-01 INFINITE	2.4180 9.6770*+04 2.9630*+02	1.0153 1.0000 0.0000	2.9743*+03 5.5293*+03 5.6773*-04	1.0990*-03 NM 0.0000*+00	3.8882 1.7987 0.9343	1.3830 1.7859 1.6101*-04	0.4756*+03 2.6796*+02 5.6730*+02	0.4756*+03 1.3459*+02 2.0209*+02
70030403 5.1500*-01 INFINITE	2.4190 9.6240*+04 2.9750*+02	1.0053 1.0000 0.0000	3.1290*+03 5.8181*+03 5.9874*-04	1.6810*-03 NM 0.0000*+00	3.9057 1.7974 0.9009	1.3814 1.7857 0.2312*-04	0.4756*+03 2.6796*+02 5.6998*+02	0.4756*+03 1.3459*+02 2.0209*+02
70030404 5.6000*-01 INFINITE	2.4260 9.7737*+04 2.9730*+02	1.0101 1.0000 0.0000	3.3405*+03 6.2751*+03 6.5374*-04	1.8290*-03 NM 0.0000*+00	3.9050 1.7907 0.9089	1.4011 1.7749 0.1294*-04	0.4756*+03 2.6796*+02 5.7100*+02	0.4756*+03 1.3475*+02 2.0209*+02
70030405 6.0500*-01 INFINITE	2.4460 9.8270*+04 2.9180*+02	1.0077 1.0000 0.0000	3.4077*+03 6.4423*+03 6.6524*-04	1.8050*-03 NM 0.0000*+00	3.9153 1.7964 0.9013	1.3643 1.7858 0.2336*-04	0.4756*+03 2.7733*+02 5.6524*+02	0.4756*+03 1.3477*+02 2.0272*+02
70030406 6.5000*-01 INFINITE	2.4560 9.7481*+04 2.8840*+02	1.0221 1.0000 0.0000	3.4642*+03 7.3565*+03 7.3600*-04	1.7290*-03 NM 0.0000*+00	3.9470 1.7904 0.9051	1.3633 1.7858 1.0255*-03	0.4756*+03 2.7802*+02 5.6298*+02	0.4756*+03 1.3471*+02 2.0209*+02
70030501 4.2500*-01 INFINITE	2.4830 9.7734*+04 2.9310*+02	1.0197 1.0000 0.0000	2.2728*+03 4.6975*+03 5.4083*-04	1.9290*-03 NM 0.0000*+00	4.3090 1.8035 0.9075	1.3818 1.7890 1.7407*-04	0.4756*+03 2.7048*+02 5.6902*+02	0.4756*+03 1.3488*+02 2.0211*+02
70030502 4.7000*-01 INFINITE	2.4870 9.7666*+04 2.9330*+02	1.0206 1.0000 0.0000	2.3777*+03 4.6597*+03 5.7632*-04	1.8470*-03 NM 0.0000*+00	4.4430 1.7905 0.9070	1.4163 1.7714 0.4726*-04	0.4756*+03 2.6140*+02 5.9107*+02	0.4756*+03 1.3480*+02 2.0272*+02
70030503 5.1500*-01 INFINITE	2.4910 9.8713*+04 2.9420*+02	1.0181 1.0000 0.0000	2.4829*+03 5.3454*+03 6.1523*-04	1.8090*-03 NM 0.0000*+00	4.4131 1.8008 0.9071	1.3654 1.7808 0.9230*-04	0.4756*+03 2.7098*+02 5.9148*+02	0.4756*+03 1.3481*+02 2.0211*+02
70030504 5.6000*-01 INFINITE	2.4920 9.9890*+04 2.9470*+02	1.0120 1.0000 0.0000	2.9042*+03 6.0244*+03 6.9107*-04	1.7030*-03 NM 0.0000*+00	4.5550 1.7822 0.9064	1.4152 1.7852 1.0334*-03	0.4756*+03 2.7963*+02 5.9293*+02	0.4756*+03 1.3479*+02 2.0272*+02
70030505 6.0500*-01 INFINITE	2.4730 9.6020*+04 2.9150*+02	1.0220 1.0000 0.0000	2.9205*+03 6.6048*+03 7.0053*-04	1.6810*-03 NM 0.0000*+00	4.3404 1.7904 0.9059	1.3730 1.7774 1.0290*-03	0.4756*+03 2.6013*+02 5.8741*+02	0.4756*+03 1.3481*+02 2.0299*+02
70030506 6.5000*-01 INFINITE	2.4560 9.7142*+04 2.8690*+02	1.0211 1.0000 0.0000	3.3701*+03 4.9624*+03 7.6936*-04	1.6760*-03 NM 0.0000*+00	4.4293 1.7784 0.9064	1.4208 1.7804 1.1349*-03	0.4756*+03 2.7478*+02 5.8052*+02	0.4756*+03 1.3488*+02 2.0209*+02
70030601 4.2500*-01 INFINITE	2.4210 9.9380*+04 2.9640*+02	1.0158 1.0000 0.0000	1.8720*+03 4.2439*+03 5.9531*-04	1.8720*-03 NM 0.0000*+00	4.9725 1.7900 0.1125	1.4447 1.7805 0.5423*-04	3.0874*+03 2.6139*+02 6.1289*+02	3.0874*+03 1.0952*+02 2.7846*+02
70030602 4.7000*-01 INFINITE	2.8980 9.8599*+04 2.9670*+02	1.0224 1.0000 0.0000	2.1364*+03 4.8228*+03 6.2914*-04	1.7420*-03 NM 0.0000*+00	4.7682 1.8065 0.9999	1.3252 1.7929 0.5772*-04	3.1303*+03 2.6336*+02 6.1140*+02	3.1303*+03 1.1078*+02 2.7738*+02
70030603 5.1500*-01 INFINITE	2.9030 9.9133*+04 2.9670*+02	1.0202 1.0000 0.0000	2.2238*+03 5.0218*+03 6.5334*-04	1.7030*-03 NM 0.0000*+00	4.8887 1.7933 0.9425	1.3758 1.7779 1.0042*-03	3.1239*+03 2.6299*+02 6.1179*+02	3.1239*+03 1.1048*+02 2.7737*+02
70030604 5.6000*-01 INFINITE	2.9020 1.0070*+05 2.9570*+02	1.0314 1.0000 0.0000	2.4600*+03 5.6037*+03 7.1382*-04	1.6610*-03 NM 0.0000*+00	4.9320 1.7799 0.9457	1.4065 1.7826 1.1100*-03	3.1799*+03 2.6504*+02 6.1068*+02	3.1799*+03 1.1016*+02 2.7848*+02
70030605 6.0500*-01 INFINITE	2.9140 9.8344*+04 2.9180*+02	1.0194 1.0000 0.0000	2.8042*+03 5.4195*+03 7.1858*-04	1.6810*-03 NM 0.0000*+00	5.0710 1.7783 0.1044	1.4553 1.7525 1.1321*-03	2.9568*+03 2.7748*+02 6.0911*+02	2.9568*+03 1.0721*+02 2.7800*+02
70030606 6.5000*-01 INFINITE	2.8820 9.6620*+04 2.8920*+02	1.0276 1.0000 0.0000	2.8109*+03 6.3574*+03 9.0846*-04	1.6810*-03 NM 0.0000*+00	5.2497 1.7537 0.9889	1.4013 1.7122 1.2857*-03	3.1427*+03 2.7768*+02 6.0237*+02	3.1427*+03 1.0867*+02 2.7843*+02

CAT 7003		MEIER		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN X *	MD *	TH/TR	RED2W	LF *	H12	H12K	PW	PD		
RZ	POD	PW/PD*	RED2D	CO	H3P	H32K	TM*	TD		
	TOD*	SW *	D2	PT2*	H42	WPK	UD	TR		
70030701	1.6820	0.9881	6.9771 ⁺⁰³	2.0940 ⁻⁰³	2.6229	1.4370	1.9111 ⁺⁰⁴	1.9111 ⁺⁰⁴		
6.0500 ⁻⁰¹	9.1807 ⁺⁰⁴	1.0000	9.5940 ⁺⁰³	NM	1.7777	1.7656	3.0800 ⁺⁰²	2.0685 ⁺⁰²		
INFINITE	3.2339 ⁺⁰²	0.0000	8.4427 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0586	1.0039 ⁻⁰³	4.6503 ⁺⁰²	3.1172 ⁺⁰²		
70030702	1.6980	0.9435	5.3066 ⁺⁰³	2.0990 ⁻⁰³	2.4470	1.4054	1.6734 ⁺⁰⁴	1.6734 ⁺⁰⁴		
6.0500 ⁻⁰¹	9.2194 ⁺⁰⁴	1.0000	6.9672 ⁺⁰³	NM	1.7825	1.7733	3.8266 ⁺⁰²	2.0741 ⁺⁰²		
INFINITE	4.2161 ⁺⁰²	0.0000	8.6831 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1133	1.0180 ⁻⁰³	5.5672 ⁺⁰²	4.0557 ⁺⁰²		
70030801	1.9640	0.9910	4.8819 ⁺⁰³	2.0430 ⁻⁰³	3.0034	1.4081	1.2334 ⁺⁰⁴	1.2334 ⁺⁰⁴		
6.0500 ⁻⁰¹	9.1253 ⁺⁰⁴	1.0000	7.4314 ⁺⁰³	NM	1.7880	1.7706	3.6638 ⁺⁰²	1.8280 ⁺⁰²		
INFINITE	3.2383 ⁺⁰²	0.0000	7.3449 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0751	9.1621 ⁻⁰⁴	5.3241 ⁺⁰²	3.0416 ⁺⁰²		
70030802	1.9840	0.9335	4.3461 ⁺⁰³	2.0860 ⁻⁰³	2.8803	1.3847	1.2382 ⁺⁰⁴	1.2382 ⁺⁰⁴		
6.0500 ⁻⁰¹	9.4502 ⁺⁰⁴	1.0000	6.2221 ⁺⁰³	NM	1.7869	1.7766	3.7717 ⁺⁰²	2.3692 ⁺⁰²		
INFINITE	4.2343 ⁺⁰²	0.0000	8.5769 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1317	1.0565 ⁻⁰³	6.1228 ⁺⁰²	4.0708 ⁺⁰²		
70030901	2.1950	0.9880	4.1536 ⁺⁰³	1.9780 ⁻⁰³	3.3321	1.3713	8.7341 ⁺⁰³	8.7341 ⁺⁰³		
6.0500 ⁻⁰¹	9.2663 ⁺⁰⁴	1.0000	6.8716 ⁺⁰³	NM	1.7922	1.7857	3.0213 ⁺⁰²	1.6411 ⁺⁰²		
INFINITE	3.2225 ⁺⁰²	0.0000	7.8016 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.0914	9.6062 ⁻⁰⁴	5.6379 ⁺⁰²	3.0581 ⁺⁰²		
70030902	2.1640	0.9236	3.8531 ⁺⁰³	1.9820 ⁻⁰³	3.2376	1.4443	9.4538 ⁺⁰³	9.4538 ⁺⁰³		
6.0500 ⁻⁰¹	9.5549 ⁺⁰⁴	1.0000	5.8267 ⁺⁰³	NM	1.7696	1.7546	3.7136 ⁺⁰²	2.1838 ⁺⁰²		
INFINITE	4.2329 ⁺⁰²	0.0000	8.6710 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1502	1.1233 ⁻⁰³	6.4146 ⁺⁰²	4.0207 ⁺⁰²		
70031001	2.4380	0.9888	3.4567 ⁺⁰³	1.8620 ⁻⁰³	3.8585	1.4403	6.0514 ⁺⁰³	6.0514 ⁺⁰³		
6.0500 ⁻⁰¹	9.3876 ⁺⁰⁴	1.0000	6.2731 ⁺⁰³	NM	1.7768	1.7577	3.0140 ⁺⁰²	1.4708 ⁺⁰²		
INFINITE	3.2306 ⁺⁰²	0.0000	7.5766 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1153	1.0514 ⁻⁰³	5.9386 ⁺⁰²	3.0881 ⁺⁰²		
70031002	2.4440	0.9187	2.9832 ⁺⁰³	1.9730 ⁻⁰³	3.7956	1.4991	6.2046 ⁺⁰³	6.2046 ⁺⁰³		
6.0500 ⁻⁰¹	9.7157 ⁺⁰⁴	1.0000	4.9713 ⁺⁰³	NM	1.7639	1.7413	3.6348 ⁺⁰²	1.9118 ⁺⁰²		
INFINITE	4.1940 ⁺⁰²	0.0000	8.3363 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1716	1.1862 ⁻⁰³	6.7740 ⁺⁰²	3.9506 ⁺⁰²		
70031101	2.6840	0.9896	2.7506 ⁺⁰³	1.7850 ⁻⁰³	4.3232	1.4418	4.1948 ⁺⁰³	4.1948 ⁺⁰³		
6.0500 ⁻⁰¹	9.5294 ⁺⁰⁴	1.0000	5.4951 ⁺⁰³	NM	1.7774	1.7566	2.9913 ⁺⁰²	1.3194 ⁺⁰²		
INFINITE	3.2206 ⁺⁰²	0.0000	7.4261 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1442	1.0890 ⁻⁰³	6.1816 ⁺⁰²	3.0729 ⁺⁰²		
70031102	2.7350	0.9105	2.1890 ⁺⁰³	1.9920 ⁻⁰³	4.1461	1.4121	3.8646 ⁺⁰³	3.8646 ⁺⁰³		
6.0500 ⁻⁰¹	9.7906 ⁺⁰⁴	1.0000	4.0610 ⁺⁰³	NM	1.7798	1.7628	3.5881 ⁺⁰²	1.8697 ⁺⁰²		
INFINITE	4.2042 ⁺⁰²	0.0000	8.0657 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2346	1.1624 ⁻⁰³	7.1375 ⁺⁰²	3.9406 ⁺⁰²		
70031201	2.9050	0.9967	2.4697 ⁺⁰³	1.7220 ⁻⁰³	4.7274	1.4055	3.0625 ⁺⁰³	3.0625 ⁺⁰³		
6.0500 ⁻⁰¹	9.7493 ⁺⁰⁴	1.0000	5.4216 ⁺⁰³	NM	1.7880	1.7637	2.9537 ⁺⁰²	1.1796 ⁺⁰²		
INFINITE	3.1706 ⁺⁰²	0.0000	7.9009 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1614	1.2087 ⁻⁰³	6.3259 ⁺⁰²	2.9639 ⁺⁰²		
70031202	2.8630	0.8960	2.1634 ⁺⁰³	1.9060 ⁻⁰³	4.3233	1.4304	3.2951 ⁺⁰³	3.2951 ⁺⁰³		
6.0500 ⁻⁰¹	9.8426 ⁺⁰⁴	1.0000	4.1286 ⁺⁰³	NM	1.7777	1.7555	3.5169 ⁺⁰²	1.5899 ⁺⁰²		
INFINITE	4.1964 ⁺⁰²	0.0000	8.6495 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2647	1.2745 ⁻⁰³	7.2380 ⁺⁰²	3.9253 ⁺⁰²		

POD CALCULATED FROM TOD, R110D (AUTHOR)

70030401		MEIER		PROFILE TABULATION			25 POINTS, DELTA AT POINT 25		
I	Y	P12/P	P/PD	T0/T00	M/M0	U/UD	T/T0	RHO/RHO0*U/UD	
1	0.0000+00	1.0000+00	NM	0.95487	0.00000	0.00000	2.07052	0.00000	
2	2.8000+04	2.2077+00	NM	0.96175	0.46693	0.00197	1.66205	0.36218	
3	3.0000+04	2.2184+00	NM	0.96286	0.46854	0.00598	1.66164	0.36388	
4	3.2000+04	2.2709+00	NM	0.96221	0.47652	0.01191	1.64895	0.37109	
5	3.5000+04	2.3400+00	NM	0.96300	0.48743	0.02315	1.63445	0.38126	
6	4.0000+04	2.4291+00	NM	0.96307	0.49935	0.03520	1.61688	0.39286	
7	5.0000+04	2.5766+00	NM	0.96328	0.51984	0.05499	1.58752	0.41258	
8	7.5000+04	2.8825+00	NM	0.96371	0.55912	0.09174	1.53061	0.45193	
9	1.0000+03	3.1543+00	NM	0.96653	0.59174	0.12160	1.44731	0.48521	
10	1.3000+03	3.4402+00	NM	0.97047	0.62355	0.15006	1.44700	0.51876	
11	1.6000+03	3.7404+00	NM	0.97396	0.66243	0.17827	1.39613	0.56063	
12	1.9000+03	4.0300+00	NM	0.97785	0.68454	0.20129	1.37018	0.58480	
13	2.2000+03	4.3250+00	NM	0.98123	0.71302	0.22378	1.33481	0.61715	
14	2.5000+03	4.6200+00	NM	0.98342	0.74028	0.24400	1.30003	0.64926	
15	3.0000+03	5.1362+00	NM	0.98889	0.78562	0.27690	1.24586	0.70385	
16	3.5000+03	5.6324+00	NM	0.99340	0.82682	0.30881	1.19755	0.75525	
17	4.0000+03	6.0833+00	NM	0.99706	0.86267	0.32770	1.15646	0.80219	
18	4.5000+03	6.5267+00	NM	0.99919	0.89619	0.34746	1.11774	0.84766	
19	5.0000+03	6.9667+00	NM	1.00023	0.92406	0.36285	1.08570	0.88684	
20	5.5000+03	7.2224+00	NM	1.00129	0.94658	0.37490	1.06072	0.91909	
21	6.0000+03	7.4960+00	NM	1.00146	0.96567	0.38444	1.03925	0.94726	
22	6.5000+03	7.6444+00	NM	1.00143	0.97587	0.39136	1.02784	0.96256	
23	7.0000+03	7.8019+00	NM	1.00169	0.98657	0.39458	1.01630	0.97866	
24	7.5000+03	7.9069+00	NM	1.00088	0.99364	0.39749	1.00777	0.98980	
D 25	8.0000+03	8.0020+00	NM	1.00030	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, U/UD, T/T0 ASSUME P=PD

70030402		MEIER		PROFILE TABULATION			28 POINTS, DELTA AT POINT 28		
I	Y	P12/P	P/PD	T0/T00	M/M0	U/UD	T/T0	RHO/RHO0*U/UD	
1	0.0000+00	1.0000+00	NM	0.95624	0.00000	0.00000	2.07442	0.00000	
2	2.8000+04	2.1163+00	NM	0.96097	0.45225	0.58659	1.68232	0.38868	
3	3.0000+04	2.1163+00	NM	0.96097	0.45225	0.58659	1.68232	0.38868	
4	3.2000+04	2.1576+00	NM	0.96198	0.45886	0.59379	1.67457	0.35454	
5	3.5000+04	2.2304+00	NM	0.96179	0.47019	0.60541	1.65787	0.36517	
6	4.0000+04	2.3030+00	NM	0.96184	0.48111	0.61652	1.64210	0.37544	
7	5.0000+04	2.4177+00	NM	0.96234	0.50055	0.63694	1.61461	0.39393	
8	7.5000+04	2.6857+00	NM	0.96461	0.53402	0.66897	1.56976	0.42630	
9	1.0000+03	2.9211+00	NM	0.96646	0.56398	0.69720	1.52814	0.45622	
10	1.3000+03	3.1824+00	NM	0.96464	0.59455	0.72533	1.48870	0.48735	
11	1.6000+03	3.4524+00	NM	0.97339	0.62461	0.75215	1.45088	0.51870	
12	1.9000+03	3.7113+00	NM	0.97712	0.65207	0.77588	1.41578	0.54882	
13	2.2000+03	3.9802+00	NM	0.98008	0.67933	0.79830	1.38093	0.57804	
14	2.5000+03	4.2202+00	NM	0.98285	0.70358	0.81762	1.35044	0.60584	
15	3.0000+03	4.6985+00	NM	0.98858	0.74867	0.85075	1.29822	0.65532	
16	3.5000+03	5.1504+00	NM	0.99235	0.78655	0.87988	1.24911	0.70376	
17	4.0000+03	5.6173+00	NM	0.99720	0.82523	0.90561	1.20427	0.75199	
18	4.5000+03	6.0724+00	NM	0.99938	0.86131	0.92683	1.16093	0.79939	
19	5.0000+03	6.4765+00	NM	1.00214	0.89207	0.94665	1.12009	0.84065	
20	5.5000+03	6.8791+00	NM	1.00248	0.92103	0.96236	1.09176	0.88146	
21	6.0000+03	7.2223+00	NM	1.00369	0.94619	0.97588	1.06374	0.91710	
22	6.5000+03	7.4707+00	NM	1.00307	0.96552	0.98418	1.04335	0.94530	
23	7.0000+03	7.6780+00	NM	1.00310	0.97775	0.99104	1.02771	0.96454	
24	7.5000+03	7.8220+00	NM	1.00238	0.98757	0.99540	1.01590	0.97981	
25	8.0000+03	7.8940+00	NM	1.00167	0.99230	0.99730	1.00993	0.98749	
26	8.5000+03	7.9467+00	NM	1.00080	0.99584	0.99850	1.00574	0.99329	
27	9.0000+03	7.9977+00	NM	1.00085	0.99930	1.00010	1.00186	0.99850	
D 28	9.5000+03	8.0033+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y, U/UD, T/T0 ASSUME P=PD

70030403 MEIER PROFILE TABULATION 20 POINTS, DELTA AT POINT 28

I	Y	P12/P	P/PO	TU/T0U	H/H0	U/UD	T/T0	RHO/RHO0*U/UD
1	0.0000+00	1.0000+00	NM	0.94775	0.00000	0.00000	2.07534	0.00000
2	2.8000-04	2.1685+00	NM	0.95957	0.45062	0.59240	1.08356	0.35191
3	3.0000-04	2.1890+00	NM	0.96046	0.45992	0.59610	1.08074	0.35481
4	3.2000-04	2.2373+00	NM	0.96012	0.46603	0.60270	1.07014	0.36092
5	3.5000-04	2.2851+00	NM	0.96021	0.47433	0.61088	1.05664	0.36830
6	4.0000-04	2.3586+00	NM	0.96146	0.48504	0.62209	1.04493	0.37810
7	5.0000-04	2.4853+00	NM	0.96137	0.50285	0.63969	1.01831	0.39520
8	7.5000-04	2.7480+00	NM	0.96439	0.53748	0.67380	1.57162	0.42873
9	1.0000-03	2.9705+00	NM	0.96634	0.56470	0.69981	1.53483	0.45503
10	1.3000-03	3.2234+00	NM	0.96911	0.59402	0.72622	1.49444	0.48588
11	1.6000-03	3.4870+00	NM	0.97262	0.62304	0.75203	1.45693	0.51617
12	1.9000-03	3.6986+00	NM	0.97628	0.64515	0.77143	1.42474	0.53454
13	2.2000-03	3.9304+00	NM	0.97904	0.66857	0.79094	1.39456	0.54513
14	2.5000-03	4.1627+00	NM	0.98157	0.69118	0.80914	1.37045	0.54942
15	3.0000-03	4.5849+00	NM	0.98701	0.73041	0.83985	1.32112	0.53523
16	3.5000-03	4.9880+00	NM	0.99163	0.76584	0.86596	1.27974	0.52693
17	4.0000-03	5.4281+00	NM	0.99527	0.80280	0.89167	1.23340	0.52200
18	4.5000-03	5.8580+00	NM	0.99881	0.83669	0.91397	1.19320	0.74593
19	5.0000-03	6.2724+00	NM	1.00156	0.86911	0.93400	1.15510	0.80860
20	5.5000-03	6.6836+00	NM	1.00357	0.89463	0.95189	1.11455	0.84504
21	6.0000-03	7.0532+00	NM	1.00464	0.92615	0.96639	1.08674	0.88750
22	6.5000-03	7.3797+00	NM	1.00472	0.94896	0.97799	1.06112	0.92080
23	7.0000-03	7.6771+00	NM	1.00392	0.96918	0.98750	1.03610	0.95170
24	7.5000-03	7.9282+00	NM	1.00327	0.98809	0.99520	1.01186	0.97707
25	8.0000-03	8.1664+00	NM	1.00241	0.99520	0.99900	1.00786	0.99111
26	8.5000-03	8.0965+00	NM	1.00077	0.99720	0.99910	1.00382	0.99530
27	9.0000-03	8.1170+00	NM	1.00088	0.99860	0.99980	1.00281	0.99700
D 28	9.5000-03	8.1390+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,H/H0 ASSUMPL P=PD

70030404 MEIER PROFILE TABULATION 20 POINTS, DELTA AT POINT 28

I	Y	P12/P	P/PO	TU/T0U	H/H0	U/UD	T/T0	RHO/RHO0*U/UD
1	0.0000+00	1.0000+00	NM	0.94831	0.00000	0.00000	2.09233	0.00000
2	2.8000-04	2.0960+00	NM	0.95950	0.44215	0.57864	1.71303	0.33782
3	3.0000-04	2.1513+00	NM	0.95859	0.45078	0.58751	1.69863	0.34587
4	3.2000-04	2.1940+00	NM	0.95957	0.45750	0.59481	1.69033	0.35184
5	3.5000-04	2.2490+00	NM	0.95961	0.46373	0.60332	1.67810	0.35952
6	4.0000-04	2.3253+00	NM	0.95981	0.47087	0.61474	1.66181	0.36492
7	5.0000-04	2.4553+00	NM	0.95913	0.48523	0.63280	1.63303	0.38754
8	7.5000-04	2.7050+00	NM	0.96092	0.52625	0.66530	1.58614	0.41943
9	1.0000-03	2.9223+00	NM	0.96222	0.55504	0.69053	1.54774	0.44614
10	1.3000-03	3.1510+00	NM	0.96461	0.58174	0.71510	1.51131	0.47321
11	1.6000-03	3.3786+00	NM	0.96767	0.60702	0.73794	1.47803	0.49930
12	1.9000-03	3.5961+00	NM	0.97032	0.63011	0.75811	1.44756	0.52371
13	2.2000-03	3.8131+00	NM	0.97380	0.65220	0.77723	1.41981	0.54742
14	2.5000-03	4.0310+00	NM	0.97688	0.67376	0.79495	1.39212	0.57104
15	3.0000-03	4.4001+00	NM	0.98197	0.70858	0.82304	1.34932	0.61000
16	3.5000-03	4.7691+00	NM	0.98638	0.74170	0.84832	1.30817	0.64847
17	4.0000-03	5.1501+00	NM	0.98998	0.77431	0.87173	1.26751	0.68770
18	4.5000-03	5.5415+00	NM	0.99351	0.80642	0.89377	1.22837	0.72761
19	5.0000-03	5.9420+00	NM	0.99720	0.83803	0.91460	1.19107	0.76788
20	5.5000-03	6.3334+00	NM	0.99911	0.86774	0.93262	1.15513	0.80737
21	6.0000-03	6.7250+00	NM	1.00108	0.89444	0.94834	1.12151	0.84606
22	6.5000-03	7.0844+00	NM	1.00294	0.92193	0.96360	1.09258	0.88200
23	7.0000-03	7.4634+00	NM	1.00311	0.94812	0.97697	1.06174	0.92012
24	7.5000-03	7.8000+00	NM	1.00333	0.97080	0.98804	1.03493	0.95381
25	8.0000-03	8.0171+00	NM	1.00243	0.98515	0.99439	1.01886	0.97594
26	8.5000-03	8.1370+00	NM	1.00160	0.99298	0.99760	1.00933	0.98838
27	9.0000-03	8.1804+00	NM	1.00083	0.99574	0.99850	1.00546	0.99302
D 28	9.5000-03	8.2461+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,H/H0 ASSUMPL P=PD

70030405		METER		PROFILE TABULATION		28 POINTS, DELTA AT POINT 2A			
I	Y	PT2/P	P/PD	T0/T0D	H/H/D	U/U/D	T/T/D	RHO/RHO0*U/U/D	
1	0.0000+00	1.0000+00	NM	0.95057	0.00000	0.00000	2.08800	0.00000	
2	2.8000-04	2.0830+00	NM	0.96154	0.44180	0.57810	1.71270	0.33764	
3	3.0000-04	2.1052+00	NM	0.96152	0.44530	0.58180	1.70703	0.34093	
4	3.2000-04	2.1480+00	NM	0.95233	0.45220	0.58930	1.69879	0.34700	
5	3.5000-04	2.2020+00	NM	0.96250	0.46060	0.59310	1.69616	0.35471	
6	4.0000-04	2.3000+00	NM	0.96257	0.47330	0.61220	1.68444	0.36841	
7	5.0000-04	2.3990+00	NM	0.96324	0.48940	0.62760	1.68452	0.38163	
8	7.5000-04	2.6600+00	NM	0.96514	0.52460	0.66250	1.59483	0.41540	
9	1.0000-03	2.8662+00	NM	0.96696	0.55050	0.68730	1.55876	0.44093	
10	1.3000-03	3.0943+00	NM	0.96901	0.57760	0.71240	1.52172	0.46831	
11	1.6000-03	3.3597+00	NM	0.97107	0.60700	0.73870	1.48101	0.49878	
12	1.9000-03	3.5181+00	NM	0.97411	0.62450	0.75430	1.45889	0.51704	
13	2.2000-03	3.7142+00	NM	0.97675	0.64490	0.77190	1.43264	0.53800	
14	2.5000-03	3.9319+00	NM	0.97925	0.66680	0.79010	1.40402	0.56274	
15	3.0000-03	4.2900+00	NM	0.98241	0.70130	0.81760	1.35917	0.60154	
16	3.5000-03	4.6494+00	NM	0.98723	0.73410	0.84290	1.31636	0.63934	
17	4.0000-03	5.0377+00	NM	0.99178	0.76540	0.86620	1.28074	0.67633	
18	4.5000-03	5.3990+00	NM	0.99435	0.79820	0.88860	1.23934	0.71700	
19	5.0000-03	5.8025+00	NM	0.99791	0.83050	0.91010	1.20078	0.75780	
20	5.5000-03	6.1608+00	NM	1.00058	0.85820	0.92760	1.16827	0.79399	
21	6.0000-03	6.6281+00	NM	1.00241	0.89300	0.94790	1.12674	0.84288	
22	6.5000-03	7.0093+00	NM	1.00313	0.92040	0.96280	1.09426	0.87987	
23	7.0000-03	7.4110+00	NM	1.00413	0.94480	0.97730	1.06231	0.92017	
24	7.5000-03	7.8831+00	NM	1.00382	0.96690	0.98820	1.04032	0.94796	
25	8.0000-03	7.9332+00	NM	1.00256	0.98360	0.99370	1.02064	0.97360	
26	8.5000-03	8.0630+00	NM	1.00175	0.99220	0.99730	1.01031	0.98713	
27	9.0000-03	8.1599+00	NM	1.00092	0.99790	0.99950	1.00321	0.99630	
28	9.5000-03	8.1831+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,H/HD ASSUME P=PD

70030406		METER		PROFILE TABULATION		31 POINTS, DELTA AT POINT 3I			
I	Y	PT2/P	P/PD	T0/T0D	H/H/D	U/U/D	T/T/D	RHO/RHO0*U/U/D	
1	0.0000+00	1.0000+00	NM	0.96402	0.00000	0.00000	4.12700	0.00000	
2	2.8000-04	2.0866+00	NM	0.96500	0.44050	0.57860	1.72530	0.33536	
3	3.0000-04	2.0972+00	NM	0.96431	0.44220	0.58020	1.72154	0.33702	
4	3.2000-04	2.1400+00	NM	0.96434	0.44910	0.58750	1.71131	0.34530	
5	3.5000-04	2.1941+00	NM	0.96471	0.45740	0.59630	1.69956	0.35085	
6	4.0000-04	2.2694+00	NM	0.96383	0.46880	0.60780	1.68092	0.36159	
7	5.0000-04	2.3893+00	NM	0.96345	0.48590	0.62500	1.65450	0.37776	
8	7.5000-04	2.6140+00	NM	0.96435	0.51650	0.65530	1.60968	0.40710	
9	1.0000-03	2.7972+00	NM	0.96550	0.53980	0.67770	1.57619	0.42596	
10	1.3000-03	3.0019+00	NM	0.96788	0.56450	0.70110	1.54252	0.45451	
11	1.6000-03	3.2601+00	NM	0.97030	0.59400	0.72790	1.50166	0.48473	
12	1.9000-03	3.3897+00	NM	0.97220	0.60820	0.74070	1.48317	0.49940	
13	2.2000-03	3.5730+00	NM	0.97431	0.62770	0.75770	1.45710	0.52000	
14	2.5000-03	3.7666+00	NM	0.97750	0.64760	0.77500	1.43215	0.54114	
15	3.0000-03	4.0676+00	NM	0.98078	0.67730	0.79980	1.39305	0.57385	
16	3.5000-03	4.4014+00	NM	0.98490	0.70870	0.82440	1.35317	0.60924	
17	4.0000-03	4.7468+00	NM	0.98908	0.73970	0.84810	1.31457	0.64516	
18	4.5000-03	5.0798+00	NM	0.99234	0.76880	0.86890	1.27869	0.67952	
19	5.0000-03	5.4360+00	NM	0.99543	0.79790	0.88930	1.24222	0.71589	
20	5.5000-03	5.7805+00	NM	0.99861	0.82540	0.90770	1.20936	0.75056	
21	6.0000-03	6.1899+00	NM	1.00092	0.85690	0.92730	1.17106	0.79184	
22	6.5000-03	6.4905+00	NM	1.00322	0.87930	0.94180	1.14526	0.82135	
23	7.0000-03	6.8900+00	NM	1.00463	0.90820	0.95730	1.11195	0.86162	
24	7.5000-03	7.2881+00	NM	1.00503	0.93610	0.97190	1.07795	0.90162	
25	8.0000-03	7.6211+00	NM	1.00555	0.95880	0.98340	1.05197	0.93482	
26	8.5000-03	7.8904+00	NM	1.00408	0.97680	0.99130	1.02991	0.96251	
27	9.0000-03	8.0521+00	NM	1.00336	0.98740	0.99590	1.01729	0.97897	
28	9.5000-03	8.1380+00	NM	1.00259	0.99300	0.99810	1.01030	0.98793	
29	1.0000-02	8.1920+00	NM	1.00179	0.99650	0.99930	1.00563	0.99371	
30	1.0500-02	8.2130+00	NM	1.00091	0.99790	0.99950	1.00321	0.99830	
31	1.1000-02	8.2461+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

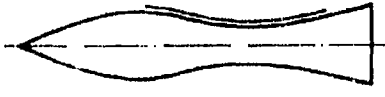
INPUT VARIABLES Y,U/UD,H/HD ASSUME P=PD

70030901		MEIER		PROFILE TABULATION		30 POINTS, DELTA AT POINT 30			
I	Y	P12/P	F/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHO0+U/UD	
1	0.0000+00	1.0000+00	NM	0.93756	0.00000	0.00000	1.84100	0.00000	
2	2.8000-04	1.9280+00	NM	0.95390	0.46267	0.57674	1.55256	0.37148	
3	5.0000-04	1.9280+00	NM	0.95390	0.46267	0.57674	1.55256	0.37148	
4	5.2000-04	1.9010+00	NM	0.95470	0.46975	0.58355	1.54651	0.37733	
5	5.5000-04	2.0300+00	NM	0.95480	0.48428	0.59888	1.52925	0.39162	
6	4.0000-04	2.1125+00	NM	0.95560	0.49749	0.61230	1.51500	0.40418	
7	5.0000-04	2.2335+00	NM	0.95650	0.51845	0.63323	1.49180	0.42448	
8	7.5000-04	2.4722+00	NM	0.95780	0.55672	0.66997	1.44822	0.46261	
9	1.0000-03	2.6180+00	NM	0.96150	0.57659	0.69129	1.42752	0.48426	
10	1.5000-03	2.8270+00	NM	0.96400	0.60820	0.71847	1.39550	0.51485	
11	1.0000-03	3.0283+00	NM	0.96650	0.63508	0.74244	1.36667	0.54325	
12	1.5000-03	3.1483+00	NM	0.96890	0.65057	0.75020	1.35139	0.55963	
13	2.2000-03	3.3234+00	NM	0.97130	0.67244	0.77504	1.32843	0.58342	
14	2.5000-03	3.4856+00	NM	0.97370	0.69203	0.79153	1.30824	0.60503	
15	5.0000-03	3.7807+00	NM	0.97430	0.72020	0.82000	1.27503	0.64312	
16	5.5000-03	4.0446+00	NM	0.98260	0.75535	0.84281	1.24497	0.67697	
17	4.0000-03	4.2890+00	NM	0.98660	0.78132	0.86292	1.21977	0.70744	
18	4.5000-03	4.6010+00	NM	0.98990	0.81321	0.88607	1.18722	0.74634	
19	5.0000-03	4.8552+00	NM	0.99310	0.83877	0.90391	1.16274	0.77740	
20	5.5000-03	5.1711+00	NM	0.99630	0.86634	0.92431	1.13308	0.81575	
21	6.0000-03	5.4677+00	NM	0.99880	0.89567	0.94201	1.10616	0.85161	
22	6.5000-03	5.6609+00	NM	0.99960	0.91298	0.95254	1.08452	0.87508	
23	7.0000-03	5.9101+00	NM	1.00100	0.93485	0.96566	1.06780	0.90502	
24	7.5000-03	6.1270+00	NM	1.00100	0.95353	0.97594	1.04767	0.93158	
25	8.0000-03	6.3007+00	NM	1.00100	0.96811	0.98380	1.03281	0.95261	
26	8.5000-03	6.4708+00	NM	1.00100	0.98223	0.99133	1.01860	0.97322	
27	9.0000-03	6.5484+00	NM	1.00100	0.98861	0.99465	1.01225	0.98261	
28	9.5000-03	6.6042+00	NM	1.00100	0.99317	0.99770	1.00774	0.98935	
29	1.0000-02	6.6500+00	NM	1.00000	0.99727	0.99861	1.00249	0.99593	
D 30	1.0500-02	6.6883+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,T0/T0D ASSUME P=PD

70030902		MEIER		PROFILE TABULATION		31 POINTS, DELTA AT POINT 31			
I	Y	P12/P	F/PD	T0/T0D	M/MO	U/UD	T/TD	RHO/RHO0+U/UD	
1	0.0000+00	1.0000+00	NM	0.87732	0.00000	0.00000	1.69900	0.00000	
2	3.0000-04	1.6895+00	NM	0.92620	0.41543	0.51022	1.54408	0.33432	
3	5.2000-04	1.7113+00	NM	0.92630	0.42089	0.52207	1.53898	0.33932	
4	5.0000-04	1.7333+00	NM	0.92810	0.42625	0.52827	1.53597	0.34393	
5	4.0000-04	1.7988+00	NM	0.93100	0.44149	0.54497	1.52305	0.35782	
6	5.0000-04	1.9311+00	NM	0.93160	0.46496	0.57460	1.49489	0.38438	
7	7.5000-04	2.1320+00	NM	0.93560	0.50832	0.61396	1.45883	0.42086	
8	1.0000-03	2.3245+00	NM	0.93900	0.54153	0.64643	1.42708	0.45298	
9	1.5000-03	2.4842+00	NM	0.94230	0.56654	0.67107	1.40306	0.47829	
10	1.6000-03	2.8047+00	NM	0.94710	0.61368	0.71458	1.35589	0.52702	
11	1.7000-03	2.8544+00	NM	0.94960	0.62061	0.72147	1.35146	0.53385	
12	2.2000-03	2.8980+00	NM	0.95440	0.62662	0.72842	1.35133	0.53904	
13	2.5000-03	3.1269+00	NM	0.95770	0.65712	0.75514	1.32059	0.57182	
14	3.0000-03	3.4095+00	NM	0.96290	0.69270	0.78570	1.28655	0.61070	
15	3.5000-03	3.5979+00	NM	0.96800	0.71534	0.80528	1.26776	0.63545	
16	4.0000-03	3.8702+00	NM	0.97260	0.74677	0.83063	1.23724	0.67135	
17	4.5000-03	4.1445+00	NM	0.97630	0.77720	0.85497	1.20994	0.70662	
18	5.0000-03	4.4740+00	NM	0.98230	0.81192	0.88053	1.17614	0.74866	
19	5.5000-03	4.7155+00	NM	0.98560	0.83641	0.89818	1.15314	0.77890	
20	6.0000-03	5.0260+00	NM	0.98950	0.86691	0.91935	1.12464	0.81746	
21	6.5000-03	5.2117+00	NM	0.99270	0.88494	0.93193	1.10903	0.84031	
22	7.0000-03	5.4573+00	NM	0.99480	0.90573	0.94537	1.08946	0.86775	
23	7.5000-03	5.7072+00	NM	0.99800	0.93072	0.96054	1.06625	0.90080	
24	8.0000-03	5.9101+00	NM	0.99820	0.94824	0.97137	1.04937	0.92567	
25	7.5000-03	6.0857+00	NM	0.99900	0.96349	0.98015	1.03488	0.94712	
26	9.0000-03	6.1923+00	NM	0.99970	0.97274	0.98549	1.02640	0.96014	
27	9.5000-03	6.3007+00	NM	0.99920	0.98198	0.99017	1.01676	0.97385	
28	1.0000-02	6.3991+00	NM	0.99930	0.99030	0.99461	1.00872	0.98600	
29	1.0500-02	6.4647+00	NM	0.99990	0.99584	0.99780	1.00393	0.99389	
30	1.0000-02	6.5151+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 31	1.1500-02	6.5151+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,T0/T0D ASSUME P=PD

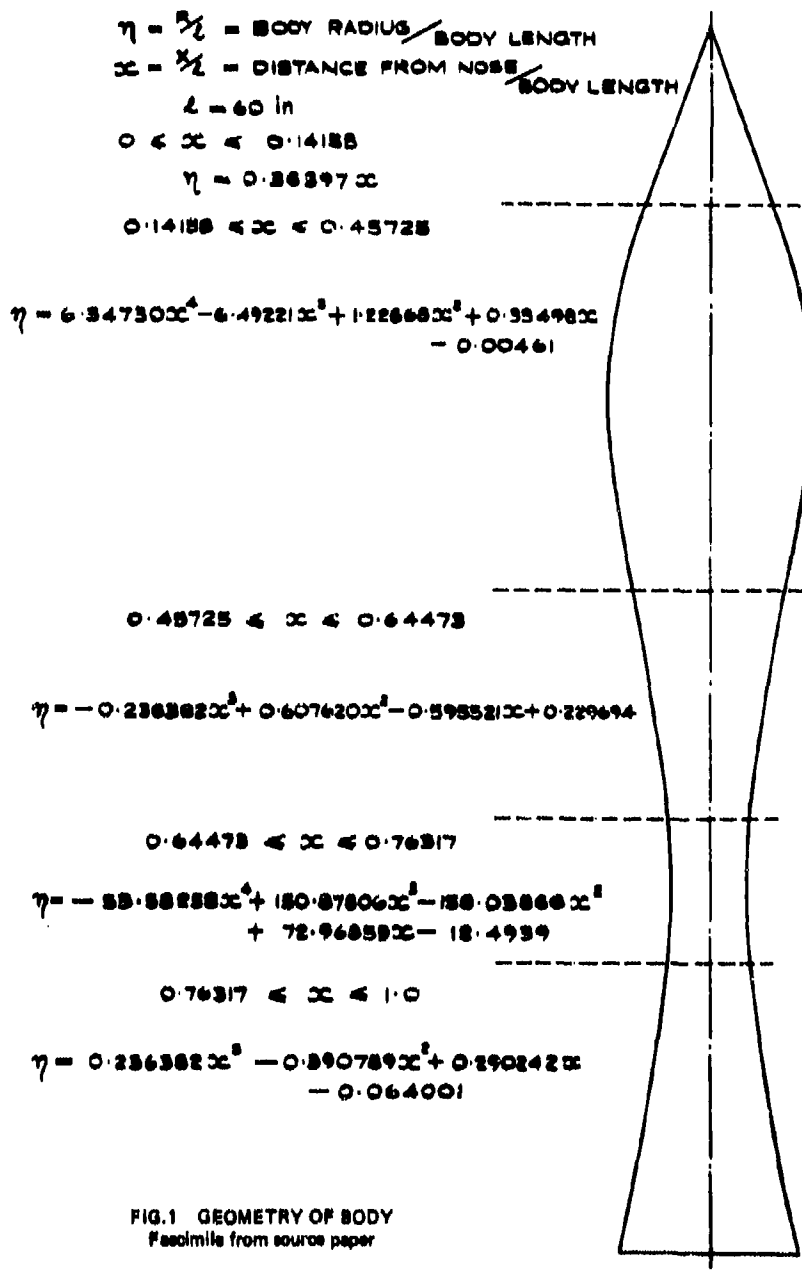
axisymmetric 	M : 1.4 - 2.8 (free stream) R THETA X 10 ⁻³ : 8-40 TW/TR : 1.0	7004
		APG (VPG) AW
Continuous wind tunnel with flexible nozzle: W = H = 2.4 m. 0.04 < PO < 0.08 MN/m ² . TO : 290 K. Air, dew-point 243 K. 5 < RE/m X 10 ⁻⁶ < 13.		
WINTER K.G., ROTTA J.C. and SMITH K.G., 1970. Studies of the turbulent boundary layer on a twisted body of revolution in subsonic and supersonic flow. ARC R & M 3633 (replaces RAE TR 68215, 197d) And Winter K.G., private communication. Also Winter et al. (1965 a & b).		

- 1 The test boundary layer was formed on the exterior surface of a pointed body of revolution aligned with the axis of the wind-tunnel. The model was constructed of fibreglass on a steel core. The overall length was 1.524 m and the maximum diameter approximately 0.25 m. The body geometry is specified in figure 1.
- 4 The resultant pressure history is tabulated in section D. The free stream Mach number was uniform to within
 3 ± 0.006 . A transition trip consisting of 0.127 mm ballotini was attached 38 mm from the nose of the model. This size proved inadequate at Mach numbers greater than 1.4, transition occurring downstream of the trip.
- 6 Static holes ($d = 0.762$ mm) were provided at 29 stations along each of two generators separated by 30° and extra holes were drilled 90° apart at $X = 0.152, 0.610, 1.067$ and 1.499 m. The pressures recorded at these
 5 stations provide a check on twodimensionality and are given in section D. Skin friction was measured by the
 6 razor-blade technique (Smith et al. 1972) the calibration however being based on later measurements taken during the floating element balance tests of CAT 7302. The height of the razor blades was about 0.13 mm, and for some tests alternate blades were removed to check that the results were not affected by the presence
 7 of the blades. The data are presented in section D. The Pitot surveys were obtained by traversing a rake carrying 5 CPP ($d_1 = 0.50, d_2 = 0.25$ mm) mounted at 2.54 mm intervals. The traverse mechanism actually moved the rake along a circular arc of radius 76.2 mm, but the data was reduced using the normal distance from the surface. The tubes could not be aligned exactly with the local direction of a body generator, but
 8 the misalignment was less than 5° except in the body waist at $X = 1.067$ m, where it was 11° . Assigning the value $\theta = 0$ to the generator on which static pressure measurements were made the skin-friction measurements were made by mounting razor blades over the holes at $\theta = 30^\circ$. The X-positions are given (in the author's units) in Section D. X is measured axially and is 0 at the nose of the body. The profiles were taken at $X = 0.610, 0.724, 0.838, 1.067, 1.269$ and 1.498 m (24, 28.5, 33, 42, 50, 59 in).
- 9 The authors have assumed negligible static pressure variation across the boundary layer, calculating the free stream Mach number from the measured wall pressure at subsonic speeds, and from the Pitot tube reading outside the boundary layer at supersonic speeds. They present profile data calculated either with the assumption of isoenergetic flow or using the Crocco / Van Driest relationship with a recovery factor of 0.89.
 12 The editors have presented the data as calculated by the authors with a recovery factor of 0.89. The boundary layer edge state has been set arbitrarily to agree with the stated Reynolds numbers and mean total temperature at the authors' specified edge point. We have not included the authors' case with subsonic ($M = 0.6$) free
 13 stream flow. The profiles presented consist of 6 sets at a single Reynolds number, each for a different Mach
 14 number. One set at $M = 1.4$ (02) is for a higher Reynolds number. The wall data of section D cover a wider range of Reynolds numbers.
- 6 DATA: 7004 0101-0606. Pitot profiles. NX = 5 or 6. CF from razor blade surface Pitots.
- 15 Editors' comments

The entry describes an interesting flow which provides a good test case for calculation methods owing to the simultaneous presence of both longitudinal and transverse curvature. In the profile test zone, for the supersonic cases presented here, the pressure gradient is always positive, but the full pressure and skin friction history is given including values for the forepart of the body in the region of accelerated flow.

The pressure gradient is a simple wave one generated by curvature of the body itself, but the maximum static pressure change likely to occur across the boundary layer is only of the order 10 %. The authors present the results of calculations allowing for static pressure variation (source paper figures 33 and 34). "Though appreciable changes of the profiles result" ... "there is no significant improvement in the relationship with "law of the wall" lines". There is also very little effect on the values of H_{12K} . The effects are more marked than in the only comparable study - Allen, CAT 7005, but still not large.

Comparing the profiles in transformed wall law coordinates, we find that there is considerable scatter in the C_f values and that on average the values seem to be low as compared to ZPG values. Series O6, as far as the inner region is concerned, appears to display transitional characteristics. The profiles are given in fine detail, but in about half the cases measurements do not extend within the momentum deficit peak. At stations 3 and 4 it appears that some correction of the innermost values is necessary. This is the zone in which the authors report difficulty in aligning the probes, which might make angles of up to 11° with the local generator of the model.



CAT 7004		WINTER/9/3		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN	MD *	IN/TR*	RED2K	CF *	H12	H12K	PW	PD	
X *	P/D	PH/PD*	RED2D	CO	H32	H32K	TW	TD	
RZ *	T/D*	SN *	D2	PI2	H42	D2K	UD	TR	
70040101	1.7060	1.0000	2.5161 ⁺⁰³	2.7200 ⁻⁰³	2.6970	1.4195	7.8386 ⁺⁰³	7.8386 ⁺⁰³	
6.0960 ⁻⁰¹	4.2762 ⁺⁰⁴	1.0000	3.6215 ⁺⁰³	NM	1.7778	1.7678	2.7775 ⁺⁰²	1.7860 ⁺⁰²	
1.1070 ⁻⁰¹	2.9000 ⁺⁰²	1.0000	6.0676 ⁻⁰⁴	NC	0.0743	7.3318 ⁻⁰⁴	4.7319 ⁺⁰²	2.7775 ⁺⁰²	
70040102	1.6330	1.0000	4.1587 ⁺⁰³	1.9200 ⁻⁰³	2.6578	1.5310	9.6234 ⁺⁰³	9.6234 ⁺⁰³	
7.2390 ⁻⁰¹	4.2760 ⁺⁰⁴	1.0000	5.7165 ⁺⁰³	NM	1.7304	1.7194	2.7890 ⁺⁰²	1.8913 ⁺⁰²	
8.9278 ⁻⁰²	2.9000 ⁺⁰²	1.0000	9.1206 ⁻⁰⁴	NC	0.0673	1.1013 ⁻⁰³	4.5027 ⁺⁰²	2.7890 ⁺⁰²	
70040103	1.4540	1.0000	7.7421 ⁺⁰³	1.4300 ⁻⁰³	2.3801	1.4969	1.2368 ⁺⁰⁴	1.2368 ⁺⁰⁴	
6.3820 ⁻⁰¹	4.2493 ⁺⁰⁴	1.0000	1.0033 ⁺⁰⁴	NM	1.7022	1.6929	2.8052 ⁺⁰²	2.0382 ⁺⁰²	
7.1071 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.5474 ⁻⁰³	NC	0.0588	1.8180 ⁻⁰³	4.1620 ⁺⁰²	2.8052 ⁺⁰²	
70040104	1.2880	1.0000	1.7733 ⁺⁰⁴	8.3000 ⁻⁰⁴	2.3057	1.5992	1.5759 ⁺⁰⁴	1.5759 ⁺⁰⁴	
1.0668 ⁺⁰⁰	4.2960 ⁺⁰⁴	1.0000	2.1840 ⁺⁰⁴	NM	1.6386	1.6290	2.8205 ⁺⁰²	2.1775 ⁺⁰²	
8.4649 ⁻⁰²	2.9000 ⁺⁰²	1.0000	3.2593 ⁻⁰³	NC	0.0510	3.7692 ⁻⁰³	3.8107 ⁺⁰²	2.8205 ⁺⁰²	
70040105	1.2540	1.0000	1.7428 ⁺⁰⁴	1.7100 ⁻⁰³	1.9680	1.3412	1.6509 ⁺⁰⁴	1.6509 ⁺⁰⁴	
1.2700 ⁺⁰⁰	4.2991 ⁺⁰⁴	1.0000	1.5153 ⁺⁰⁴	NM	1.7595	1.7537	2.8237 ⁺⁰²	2.2062 ⁺⁰²	
9.1120 ⁻⁰²	2.9000 ⁺⁰²	1.0000	2.2564 ⁻⁰³	NC	0.0467	2.4988 ⁻⁰³	3.7344 ⁺⁰²	2.8237 ⁺⁰²	
70040106	1.2150	1.0000	9.2078 ⁺⁰³	2.1700 ⁻⁰³	1.8108	1.2438	1.7263 ⁺⁰⁴	1.7263 ⁺⁰⁴	
1.4986 ⁺⁰⁰	4.2992 ⁺⁰⁴	1.0000	1.1200 ⁺⁰⁴	NM	1.8278	1.8239	2.8273 ⁺⁰²	2.2390 ⁺⁰²	
9.8153 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.6743 ⁻⁰³	NC	0.0468	1.8029 ⁻⁰³	3.6451 ⁺⁰²	2.8273 ⁺⁰²	
70040201	1.7770	1.0000	4.4281 ⁺⁰³	2.3100 ⁻⁰³	2.7341	1.4389	1.4917 ⁺⁰⁴	1.4917 ⁺⁰⁴	
6.0960 ⁻⁰¹	8.2732 ⁺⁰⁴	1.0000	6.3982 ⁺⁰³	NM	1.7759	1.7652	2.7765 ⁺⁰²	1.7775 ⁺⁰²	
1.1070 ⁻⁰¹	2.9000 ⁺⁰²	1.0000	5.5618 ⁻⁰⁴	NC	0.0773	0.7441 ⁻⁰⁴	4.7500 ⁺⁰²	2.7765 ⁺⁰²	
70040202	1.6460	1.0000	6.8832 ⁺⁰³	1.7300 ⁻⁰³	2.6602	1.5291	1.8160 ⁺⁰⁴	1.8160 ⁺⁰⁴	
7.2390 ⁻⁰¹	8.2657 ⁺⁰⁴	1.0000	9.5035 ⁺⁰³	NM	1.7385	1.7281	2.7879 ⁺⁰²	1.8808 ⁺⁰²	
8.9278 ⁻⁰²	2.9000 ⁺⁰²	1.0000	7.9118 ⁻⁰⁴	NC	0.0747	9.5331 ⁻⁰⁴	4.5260 ⁺⁰²	2.7879 ⁺⁰²	
70040203	1.4700	1.0000	1.3070 ⁺⁰⁴	1.4000 ⁻⁰³	2.5058	1.5776	2.3700 ⁺⁰⁴	2.3700 ⁺⁰⁴	
6.3820 ⁻⁰¹	8.3318 ⁺⁰⁴	1.0000	1.7025 ⁺⁰⁴	NM	1.6872	1.6768	2.8037 ⁺⁰²	2.0249 ⁺⁰²	
7.1071 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.3434 ⁻⁰³	NC	0.0576	1.5955 ⁻⁰³	3.1940 ⁺⁰²	2.8037 ⁺⁰²	
70040204	1.2890	1.0000	3.0131 ⁺⁰⁴	8.6000 ⁻⁰⁴	2.2680	1.5622	2.9767 ⁺⁰⁴	2.9767 ⁺⁰⁴	
1.0668 ⁺⁰⁰	8.1256 ⁺⁰⁴	1.0000	3.7121 ⁺⁰⁴	NM	1.6594	1.6499	2.8204 ⁺⁰²	2.1767 ⁺⁰²	
8.4649 ⁻⁰²	2.9000 ⁺⁰²	1.0000	2.9290 ⁻⁰³	NC	0.0477	3.3701 ⁻⁰³	3.8129 ⁺⁰²	2.8204 ⁺⁰²	
70040205	1.2690	1.0000	2.0361 ⁺⁰⁴	1.6500 ⁻⁰³	1.9382	1.3051	3.0538 ⁺⁰⁴	3.0538 ⁺⁰⁴	
1.2700 ⁺⁰⁰	8.1141 ⁺⁰⁴	1.0000	2.4937 ⁺⁰⁴	NM	1.7822	1.7774	2.8223 ⁺⁰²	2.1935 ⁺⁰²	
9.1120 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.9683 ⁻⁰³	NC	0.0491	2.1665 ⁻⁰³	3.7683 ⁺⁰²	2.8223 ⁺⁰²	
70040206	1.2110	1.0000	1.6042 ⁺⁰⁴	1.9500 ⁻⁰³	1.7841	1.2237	3.3818 ⁺⁰⁴	3.3818 ⁺⁰⁴	
1.4986 ⁺⁰⁰	8.3196 ⁺⁰⁴	1.0000	1.9322 ⁺⁰⁴	NM	1.8444	1.8413	2.8277 ⁺⁰²	2.2423 ⁺⁰²	
9.8153 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.4859 ⁻⁰³	NC	0.0462	1.5865 ⁻⁰³	3.6358 ⁺⁰²	2.8277 ⁺⁰²	
70040301	2.0870	1.0000	2.1389 ⁺⁰³	2.3400 ⁻⁰³	3.2544	1.4720	5.1063 ⁺⁰³	5.1063 ⁺⁰³	
6.0960 ⁻⁰¹	4.5757 ⁺⁰⁴	1.0000	3.4612 ⁺⁰³	NM	1.7883	1.7743	2.7515 ⁺⁰²	1.5499 ⁺⁰²	
1.1070 ⁻⁰¹	2.9000 ⁺⁰²	1.0000	8.1953 ⁻⁰⁴	NC	0.0916	7.9124 ⁻⁰⁴	5.2093 ⁺⁰²	2.7515 ⁺⁰²	
70040302	1.8150	1.0000	6.3596 ⁺⁰³	1.4700 ⁻⁰³	2.7976	1.4576	7.7785 ⁺⁰³	7.7785 ⁺⁰³	
6.3820 ⁻⁰¹	4.5732 ⁺⁰⁴	1.0000	9.3140 ⁺⁰³	NM	1.7333	1.7153	2.7733 ⁺⁰²	1.7482 ⁺⁰²	
7.1071 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.4860 ⁻⁰³	NC	0.0786	1.8482 ⁻⁰³	4.8115 ⁺⁰²	2.7733 ⁺⁰²	
70040303	1.5970	1.0000	1.2576 ⁺⁰⁴	8.3000 ⁻⁰⁴	2.6469	1.5665	1.0803 ⁺⁰⁴	1.0803 ⁺⁰⁴	
1.0668 ⁺⁰⁰	4.5715 ⁺⁰⁴	1.0000	1.7078 ⁺⁰⁴	NM	1.6662	1.6522	2.7922 ⁺⁰²	1.9204 ⁺⁰²	
8.4649 ⁻⁰²	2.9000 ⁺⁰²	1.0000	2.5337 ⁻⁰³	NC	0.0651	3.1113 ⁻⁰³	4.4372 ⁺⁰²	2.7922 ⁺⁰²	
70040304	1.5290	1.0000	9.5346 ⁺⁰³	1.9300 ⁻⁰³	2.2562	1.3302	1.1727 ⁺⁰⁴	1.1727 ⁺⁰⁴	
1.2700 ⁺⁰⁰	4.4904 ⁺⁰⁴	1.0000	1.2659 ⁺⁰⁴	NM	1.7730	1.7655	2.7984 ⁺⁰²	1.9761 ⁺⁰²	
9.1120 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.8782 ⁻⁰³	NC	0.0633	2.1648 ⁻⁰³	4.3094 ⁺⁰²	2.7984 ⁺⁰²	
70040305	1.4950	1.0000	7.2441 ⁺⁰³	2.4300 ⁻⁰³	2.0853	1.2101	1.2623 ⁺⁰⁴	1.2623 ⁺⁰⁴	
1.4986 ⁺⁰⁰	4.6007 ⁺⁰⁴	1.0000	9.5123 ⁺⁰³	NM	1.8460	1.8407	2.8015 ⁺⁰²	2.0041 ⁺⁰²	
9.8153 ⁻⁰²	2.9000 ⁺⁰²	1.0000	1.3666 ⁻⁰³	NC	0.0615	1.5065 ⁻⁰³	4.2434 ⁺⁰²	2.8015 ⁺⁰²	

CAT 7004

WINTER/R/S

BOUNDARY CONDITIONS AND EVALUATED DATA. 51 UNITS.

RUN X RZ	MD * POD TODA	TH/TR* PK/PO* SA *	RED2W RED2D D2	CF * CQ PI2	H12 H32 H42	H12K H32K D2K	PW TW UD	PD TD TR
70040401 6.0900*-01 1.1070*-01	2.4140 4.9645*+04 2.9000*+02	1.0000 1.0000 1.0000	1.7019*+03 3.1220*+03 6.0447*-04	1.5400*-03 NM NC	3.7897 1.7872 0.1033	1.4230 1.7667 8.2656*-04	3.3223*+03 2.7283*+02 5.6010*+02	3.3223*+03 1.3392*+02 2.7283*+02
70040402 7.2370*-01 8.9278*-02	2.3330 4.9525*+04 2.9000*+02	1.0000 1.0000 1.0000	2.4824*+03 4.4128*+03 8.2234*-04	1.6000*-03 NM NC	3.6075 1.7618 0.1150	1.4229 1.7446 1.1308*-03	3.7614*+03 2.7337*+02 5.5119*+02	3.7614*+03 1.3885*+02 2.7337*+02
70040403 8.3820*-01 7.1071*-02	2.1530 4.9457*+04 2.9000*+02	1.0000 1.0000 1.0000	4.2232*+03 7.0066*+03 1.1968*-03	1.7400*-03 NM NC	3.5640 1.6743 0.0870	1.5639 1.6574 1.7025*-03	4.9783*+03 2.7465*+02 5.2954*+02	4.9783*+03 1.5049*+02 2.7465*+02
70040404 1.0666*+00 8.4649*-02	1.9150 5.0626*+04 2.9000*+02	1.0000 1.0000 1.0000	9.2704*+03 1.4091*+04 2.1079*+03	0.5000*-04 NM NC	3.0406 1.6902 0.0845	1.3132 1.6713 2.7635*-03	7.3772*+03 2.7648*+02 4.9707*+02	7.3772*+03 1.6708*+02 2.7648*+02
70040405 1.2700*+00 9.1120*-02	1.8040 5.0862*+04 2.9000*+02	1.0000 1.0000 1.0000	7.7444*+03 1.1304*+04 1.6148*-03	1.9400*-03 NM NC	2.6048 1.7822 0.0817	1.3275 1.7717 1.9451*-03	8.7980*+03 2.7742*+02 4.7939*+02	8.7980*+03 1.7566*+02 2.7742*+02
70040406 1.4986*+00 9.8153*-02	1.7510 5.0948*+04 2.9000*+02	1.0000 1.0000 1.0000	5.9817*+03 8.5643*+03 1.1979*-03	2.3700*-03 NM NC	2.4100 1.8488 0.0753	1.2367 1.8414 1.3642*-03	9.5548*+03 2.7787*+02 4.7071*+02	9.5548*+03 1.7977*+02 2.7787*+02
70040501 6.0960*-01 1.1070*-01	2.8810 6.1454*+04 2.9000*+02	1.0000 1.0000 1.0000	6.3969*+02 1.4105*+03 2.8299*-04	1.5000*-03 NM NC	5.1984 1.7576 0.1239	1.6602 1.7084 4.4955*-04	2.0019*+03 2.7009*+02 6.0313*+02	2.0019*+03 1.0908*+02 2.7009*+02
70040502 8.3820*-01 7.1071*-02	2.6150 6.1134*+04 2.9000*+02	1.0000 1.0000 1.0000	2.0331*+03 4.0354*+03 7.0543*-04	1.2400*-03 NM NC	3.9863 1.7823 0.1702	1.3861 1.7601 1.0126*-03	2.9935*+03 2.7157*+02 5.8026*+02	2.9935*+03 1.2248*+02 2.7157*+02
70040503 1.0666*+00 8.4649*-02	2.3540 5.9897*+04 2.9000*+02	1.0000 1.0000 1.0000	4.8747*+03 8.7720*+03 1.3661*-03	9.1000*-04 NM NC	3.5062 1.7720 0.1169	1.3393 1.7607 1.8698*-03	4.4021*+03 2.7323*+02 5.5354*+02	4.4021*+03 1.9236*+02 2.7323*+02
70040504 1.2700*+00 9.1120*-02	2.1450 6.0071*+04 2.9000*+02	1.0000 1.0000 1.0000	4.9384*+03 8.1684*+03 1.1444*-03	1.9000*-03 NM NC	2.9668 1.8542 0.1021	1.2332 1.8438 1.3720*-03	6.1228*+03 2.7471*+02 5.2852*+02	6.1228*+03 1.5103*+02 2.7471*+02
70040505 1.4986*+00 9.8153*-02	2.0960 5.9872*+04 2.9000*+02	1.0000 1.0000 1.0000	3.7371*+03 6.0679*+03 8.3356*-04	2.1500*-03 NM NC	2.9143 1.8668 0.0997	1.2478 1.8547 9.8054*-04	6.5882*+03 2.7508*+02 5.2213*+02	6.5882*+03 1.5437*+02 2.7508*+02
70040601 6.0960*-01 1.1070*-01	3.3270 7.5149*+04 2.9000*+02	1.0000 1.0000 1.0000	6.0479*+02 1.5899*+03 3.3211*-04	1.1300*-03 NM NC	6.1246 1.8048 0.1326	1.5690 1.7680 5.4840*-04	1.2629*+03 2.6803*+02 6.3366*+02	1.2629*+03 9.0236*+01 2.6803*+02
70040602 8.3820*-01 7.1071*-02	3.0530 7.5189*+04 2.9000*+02	1.0000 1.0000 1.0000	1.5794*+03 3.7278*+03 6.7105*-04	1.1300*-03 NM NC	4.9465 1.8237 0.1247	1.3175 1.8024 1.0045*-03	1.8909*+03 2.6924*+02 6.1594*+02	1.8909*+03 1.0125*+02 2.6924*+02
70040603 1.0666*+00 8.4649*-02	2.7590 7.3078*+04 2.9000*+02	1.0000 1.0000 1.0000	2.4485*+03 5.1444*+03 8.1280*-04	8.3000*-04 NM NC	4.1883 1.8516 0.1102	1.2621 1.8349 1.0900*-03	2.8670*+03 2.7075*+02 5.9313*+02	2.8670*+03 1.1497*+02 2.7075*+02
70040604 1.2700*+00 9.1120*-02	2.4760 7.2768*+04 2.9000*+02	1.0000 1.0000 1.0000	3.4034*+03 6.3964*+03 8.7068*-04	1.6400*-03 NM NC	3.5304 1.8533 0.1361	1.2501 1.8413 1.1064*-03	4.4332*+03 2.7243*+02 5.6661*+02	4.4332*+03 1.3027*+02 2.7243*+02
70040605 1.4986*+00 9.8153*-02	2.4270 7.3272*+04 2.9000*+02	1.0000 1.0000 1.0000	2.9001*+03 5.3471*+03 7.0664*-04	1.8800*-03 NM NC	3.4733 1.8872 0.0966	1.2240 1.8756 8.5497*-04	4.8050*+03 2.7275*+02 5.6149*+02	4.8050*+03 1.3315*+02 2.7275*+02

POD, PD CALCULATED FROM RE (AUTHOR) - TRAPEZOIDAL RULE FOR RUN 0102,0202,0203,0301,0601

70040201		WINTER/R/S		PROFILE TABULATION		40 POINTS, DELTA AT POINT 36			
I	Y	PTZ/P	P/PD	TQ/TOD	M/MO	U/UD	T/TD	RHO/RHOD=U/UD	
1	0.0000+00	1.0000+00	NM	0.95725	0.00000	0.00000	1.56180	0.00000	
2	2.5400-04	1.7126+00	NM	0.97270	0.51294	0.59838	1.36088	0.43970	
3	3.3020-04	1.7665+00	NM	0.97346	0.52870	0.61428	1.34994	0.45504	
4	4.0640-04	1.7892+00	NM	0.97405	0.53399	0.61968	1.34670	0.46015	
5	4.3180-04	1.8291+00	NM	0.97441	0.54603	0.63157	1.33789	0.47207	
6	5.5880-04	1.9297+00	NM	0.97599	0.57197	0.65707	1.31971	0.49789	
7	7.1120-04	2.0084+00	NM	0.97685	0.59093	0.67526	1.30580	0.51713	
8	1.0468-03	2.2349+00	NM	0.97966	0.64073	0.72186	1.26927	0.56872	
9	1.4732-03	2.4727+00	NM	0.98238	0.68777	0.76405	1.23412	0.61910	
10	1.8542-03	2.6997+00	NM	0.98471	0.72912	0.79964	1.20278	0.66483	
11	2.2352-03	2.9134+00	NM	0.98679	0.76564	0.82993	1.17499	0.70633	
12	2.4892-03	3.1779+00	NM	0.98820	0.80824	0.86393	1.14293	0.75614	
13	2.5400-03	3.2261+00	NM	0.98979	0.81572	0.86983	1.13705	0.76498	
14	2.6162-03	3.2326+00	NM	0.98988	0.81673	0.87063	1.13632	0.76618	
15	2.6670-03	3.2707+00	NM	0.98993	0.82259	0.87502	1.13156	0.77329	
16	2.7940-03	3.3582+00	NM	0.99068	0.83497	0.88452	1.12423	0.78818	
17	2.9210-03	3.4104+00	NM	0.99138	0.84369	0.89122	1.11586	0.79869	
18	3.1242-03	3.3832+00	NM	0.99107	0.83964	0.88812	1.11883	0.79380	
19	3.3020-03	3.5921+00	NM	0.99207	0.87030	0.91102	1.09576	0.83141	
20	3.6576-03	3.7546+00	NM	0.99409	0.89337	0.92771	1.07836	0.86030	
21	4.0386-03	3.9308+00	NM	0.99544	0.91768	0.94491	1.06023	0.89123	
22	4.3942-03	3.9789+00	NM	0.99592	0.92421	0.94951	1.05551	0.89958	
23	4.4196-03	4.0941+00	NM	0.99675	0.93962	0.96011	1.04408	0.91958	
24	4.8260-03	4.2842+00	NM	0.99820	0.96449	0.97690	1.02590	0.95224	
25	4.9622-03	4.3097+00	NM	0.99819	0.96745	0.97890	1.02341	0.95652	
26	4.9530-03	4.3218+00	NM	0.99824	0.96933	0.98000	1.02214	0.95878	
27	5.0292-03	4.3337+00	NM	0.99852	0.97085	0.98110	1.02123	0.96071	
28	5.1308-03	4.3715+00	NM	0.99881	0.97569	0.98430	1.01773	0.96716	
29	5.2578-03	4.4287+00	NM	0.99910	0.98295	0.98900	1.01235	0.97694	
30	5.3088-03	4.3622+00	NM	0.99870	0.97451	0.98350	1.01854	0.96560	
31	5.6388-03	4.4487+00	NM	0.99934	0.98548	0.99070	1.01062	0.98029	
32	5.9948-03	4.5339+00	NM	0.99970	0.99617	0.99750	1.00267	0.99485	
33	6.0198-03	4.4769+00	NM	0.99958	0.98903	0.99300	1.00885	0.98007	
34	6.3754-03	4.5520+00	NM	0.99993	0.99842	0.99900	1.00115	0.99785	
35	6.5786-03	4.5502+00	NM	1.00001	0.99820	0.99890	1.00140	0.99750	
D 36	6.7564-03	4.5646+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
37	9.3726-03	4.5764+00	NM	1.00021	1.00146	1.00100	0.99908	1.00193	
38	1.1735-02	4.5832+00	NM	1.00017	1.00231	1.00150	0.99839	1.00311	
39	1.3462-02	4.9941+00	NM	1.00032	1.00366	1.00240	0.99749	1.00492	
40	1.5037-02	4.6393+00	NM	1.00054	1.00423	1.00590	0.99341	1.01257	

INPUT VARIABLES Y,M,U/UD ASSUME P=PD
AT I=31 DATA WERE AVERAGED

70040202		WINTER/R/S		PROFILE TABULATION		44 POINTS, DELTA AT POINT 41			
I	Y	PT2/P	P/PD	T0/TOD	M/ND	U/UD	T/YD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.96064	0.00000	0.00000	1.48118	0.00000	
2	2.5400 ⁻ 04	1.4443 ⁺ 00	NM	0.97127	0.45367	0.52680	1.34718	0.39104	
3	3.3020 ⁻ 04	1.4797 ⁺ 00	NM	0.97230	0.46755	0.54130	1.34038	0.40384	
4	3.8100 ⁻ 04	1.5058 ⁺ 00	NM	0.97236	0.47849	0.55260	1.33378	0.41431	
5	4.5720 ⁻ 04	1.5258 ⁺ 00	NM	0.97270	0.48663	0.56110	1.32949	0.42204	
6	5.3820 ⁻ 04	1.5445 ⁺ 00	NM	0.97505	0.53434	0.60970	1.30197	0.46829	
7	1.2440 ⁻ 03	1.7785 ⁺ 00	NM	0.97705	0.57445	0.64940	1.27797	0.50815	
8	1.6510 ⁻ 03	1.9022 ⁺ 00	NM	0.97886	0.61006	0.68370	1.25597	0.54436	
9	2.0574 ⁻ 03	2.0464 ⁺ 00	NM	0.98099	0.64744	0.71880	1.23258	0.58317	
10	2.4304 ⁻ 03	2.2115 ⁺ 00	NM	0.98279	0.68646	0.75420	1.20710	0.62400	
11	2.6416 ⁻ 03	2.2434 ⁺ 00	NM	0.98316	0.69363	0.76060	1.20242	0.63256	
12	2.7178 ⁻ 03	2.2746 ⁺ 00	NM	0.98353	0.70165	0.76770	1.19712	0.64129	
13	2.7686 ⁻ 03	2.3055 ⁺ 00	NM	0.98412	0.70731	0.77280	1.19377	0.64736	
14	2.8448 ⁻ 03	2.3312 ⁺ 00	NM	0.98456	0.71715	0.78140	1.18721	0.65818	
15	3.2254 ⁻ 01	2.4540 ⁺ 00	NM	0.98566	0.73867	0.80000	1.17296	0.68203	
16	3.6322 ⁻ 03	2.6812 ⁺ 00	NM	0.97834	0.78364	0.83370	1.13185	0.71658	
17	4.0132 ⁻ 03	2.8357 ⁺ 00	NM	0.98951	0.81251	0.86130	1.12371	0.76648	
18	4.2926 ⁻ 03	2.9808 ⁺ 00	NM	0.99108	0.83858	0.88210	1.10649	0.79721	
19	4.4196 ⁻ 03	3.0260 ⁺ 00	NM	0.99133	0.84660	0.88830	1.10093	0.80686	
20	4.8260 ⁻ 03	3.2122 ⁺ 00	NM	0.99307	0.87833	0.91270	1.07980	0.84525	
21	4.9530 ⁻ 03	3.2747 ⁺ 00	NM	0.99356	0.88872	0.92050	1.07280	0.85804	
22	5.1562 ⁻ 03	3.3332 ⁺ 00	NM	0.99413	0.89632	0.92770	1.06647	0.86988	
23	5.2070 ⁻ 03	3.3930 ⁺ 00	NM	0.99469	0.90817	0.93500	1.05996	0.88211	
24	5.2324 ⁻ 03	3.3533 ⁺ 00	NM	0.99423	0.90160	0.93010	1.06421	0.87398	
25	5.2832 ⁻ 03	3.3886 ⁺ 00	NM	0.99470	0.90732	0.93440	1.06059	0.88102	
26	5.3594 ⁻ 03	3.4184 ⁺ 00	NM	0.99489	0.91212	0.93790	1.05731	0.88705	
27	5.6134 ⁻ 03	3.5088 ⁺ 00	NM	0.99566	0.92652	0.94840	1.04778	0.90515	
28	5.7404 ⁻ 03	3.5630 ⁺ 00	NM	0.99625	0.93503	0.95460	1.04230	0.91584	
29	5.9844 ⁻ 03	3.6619 ⁺ 00	NM	0.99702	0.95035	0.96590	1.03214	0.93543	
30	6.1480 ⁻ 03	3.6972 ⁺ 00	NM	0.99727	0.95576	0.96930	1.02854	0.94240	
31	6.2972 ⁻ 03	3.7308 ⁺ 00	NM	0.99757	0.96086	0.97290	1.02522	0.94897	
32	6.5278 ⁻ 03	3.8053 ⁺ 00	NM	0.99809	0.97210	0.98070	1.01776	0.96358	
33	6.6548 ⁻ 03	3.8480 ⁺ 00	NM	0.99840	0.97849	0.98510	1.01357	0.97192	
34	6.9342 ⁻ 03	3.9133 ⁺ 00	NM	0.99906	0.98815	0.99180	1.00740	0.98451	
35	7.3132 ⁻ 03	3.9609 ⁺ 00	NM	0.99932	0.99514	0.99650	1.00274	0.99378	
36	7.6200 ⁻ 03	3.9826 ⁺ 00	NM	0.99961	0.99830	0.99870	1.00080	0.99790	
37	7.6962 ⁻ 03	3.9822 ⁺ 00	NM	0.99949	0.99824	0.99860	1.00073	0.99788	
38	7.7216 ⁻ 03	3.9868 ⁺ 00	NM	0.99962	0.99891	0.99910	1.00039	0.99871	
39	7.7470 ⁻ 03	3.9918 ⁺ 00	NM	0.99967	0.99964	0.99960	0.99993	0.99967	
40	7.8232 ⁻ 03	3.9910 ⁺ 00	NM	0.99963	0.99951	0.99950	0.99997	0.99953	
41	7.9756 ⁻ 03	3.9943 ⁺ 00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
42	1.0465 ⁻ 02	3.9943 ⁺ 00	NM	0.99960	1.00000	0.99980	0.99960	1.00020	
43	1.2700 ⁻ 02	4.0068 ⁺ 00	NM	0.99964	1.00182	1.00100	0.99836	1.00265	
44	1.5418 ⁻ 02	3.9843 ⁺ 00	NM	0.99949	0.99854	0.99880	1.00052	0.99826	

INPUT VARIABLES Y,M,U/UD ASSUME P/ND
 AT I=14,16,35 DATA WERE AVERAGED

70040203

WINTER/R/S

PROFILE TABULATION

59 POINTS, DELTA AT POINT 56

I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RH00*U/UD
1	0.3000"+00	1.0000"+00	NM	0.96635	0.00000	0.00000	1.38399	0.00000
2	2.5400"-04	1.2765"+00	NM	0.97375	0.40883	0.46625	1.30064	0.35848
3	3.3020"-04	1.2726"+00	NM	0.97386	0.40618	0.46349	1.30191	0.35598
4	3.8100"-04	1.2817"+00	NM	0.97392	0.41237	0.47005	1.29934	0.36176
5	4.5720"-04	1.3015"+00	NM	0.97450	0.42536	0.48393	1.29444	0.37387
6	5.8420"-04	1.3137"+00	NM	0.97462	0.43312	0.49215	1.29116	0.38117
7	9.9060"-04	1.3814"+00	NM	0.97595	0.47306	0.53405	1.27447	0.41903
8	1.3718"-03	1.4290"+00	NM	0.97721	0.49844	0.56034	1.26384	0.44337
9	1.7780"-03	1.4730"+00	NM	0.97788	0.52034	0.58264	1.25379	0.46471
10	2.1590"-03	1.5159"+00	NM	0.97886	0.54041	0.60294	1.24479	0.48437
11	2.6670"-03	1.5955"+00	NM	0.97997	0.57488	0.63704	1.22810	0.51872
12	2.7432"-03	1.5994"+00	NM	0.98022	0.57640	0.63864	1.22758	0.52024
13	2.7886"-03	1.5970"+00	NM	0.98007	0.57130	0.63364	1.23012	0.51510
14	2.7940"-03	1.6043"+00	NM	0.98029	0.57845	0.64064	1.22858	0.52229
15	2.8702"-03	1.6202"+00	NM	0.98067	0.58483	0.64694	1.22362	0.52471
16	2.9972"-03	1.6244"+00	NM	0.98054	0.58811	0.65003	1.22169	0.53208
17	3.3020"-03	1.6945"+00	NM	0.98189	0.61342	0.67463	1.20955	0.55776
18	3.4036"-03	1.7121"+00	NM	0.98189	0.61988	0.68073	1.20597	0.56447
19	3.7846"-03	1.7835"+00	NM	0.98335	0.64492	0.70463	1.19375	0.59027
20	4.1910"-03	1.8511"+00	NM	0.98404	0.66717	0.72533	1.18146	0.61367
21	4.5974"-03	1.9066"+00	NM	0.98499	0.68445	0.74133	1.17311	0.63193
22	5.1816"-03	2.0047"+00	NM	0.98669	0.72343	0.77662	1.15246	0.67388
23	5.2978"-03	2.0899"+00	NM	0.98726	0.73683	0.78852	1.14521	0.68854
24	5.3340"-03	2.0979"+00	NM	0.98754	0.73901	0.79052	1.14426	0.69056
25	5.3848"-03	2.1104"+00	NM	0.98757	0.74235	0.79342	1.14234	0.69456
26	5.4610"-03	2.1343"+00	NM	0.98796	0.74867	0.79902	1.13902	0.70150
27	5.5880"-03	2.1522"+00	NM	0.98814	0.75337	0.80312	1.13644	0.70670
28	5.7638"-03	2.2014"+00	NM	0.98869	0.76684	0.81452	1.12905	0.72168
29	5.8166"-03	2.2449"+00	NM	0.98919	0.77704	0.82362	1.12346	0.73310
30	5.9944"-03	2.2775"+00	NM	0.98966	0.78514	0.83062	1.11920	0.74215
31	6.1754"-03	2.3691"+00	NM	0.99076	0.81202	0.85331	1.10431	0.77271
32	6.7818"-03	2.4845"+00	NM	0.99106	0.83501	0.87241	1.09159	0.79971
33	7.1628"-03	2.5955"+00	NM	0.99323	0.85889	0.89201	1.07861	0.82700
34	7.7216"-03	2.7481"+00	NM	0.99471	0.89162	0.91811	1.06030	0.86369
35	7.7728"-03	2.7306"+00	NM	0.99453	0.88794	0.91521	1.06235	0.86147
36	7.7978"-03	2.7316"+00	NM	0.99476	0.89237	0.91871	1.05991	0.86678
37	7.8486"-03	2.7636"+00	NM	0.99471	0.89488	0.92061	1.05832	0.86988
38	7.9248"-03	2.7954"+00	NM	0.99507	0.90148	0.92581	1.05469	0.87780
39	8.0518"-03	2.8214"+00	NM	0.99533	0.90686	0.93011	1.05193	0.88419
40	8.2804"-03	2.9261"+00	NM	0.99657	0.92809	0.94641	1.04009	0.91002
41	8.3312"-03	2.9274"+00	NM	0.99657	0.92795	0.94641	1.04017	0.90985
42	8.3820"-03	2.9061"+00	NM	0.99633	0.92407	0.94341	1.04278	0.90513
43	8.4582"-03	2.9587"+00	NM	0.99670	0.93380	0.95080	1.03675	0.91710
44	8.8372"-03	3.0703"+00	NM	0.99775	0.95646	0.96790	1.02408	0.94315
45	9.2456"-03	3.1415"+00	NM	0.99845	0.97013	0.97810	1.01650	0.96223
46	9.6920"-03	3.2009"+00	NM	0.99904	0.98136	0.98640	1.01030	0.97634
47	9.7282"-03	3.1814"+00	NM	0.99887	0.97766	0.98370	1.01235	0.97170
48	1.0135"-02	3.2746"+00	NM	0.99966	0.99510	0.99640	1.00261	0.99360
49	1.0236"-02	3.2599"+00	NM	0.99949	0.99236	0.99440	1.00408	0.99036
50	1.0262"-02	3.2715"+00	NM	0.99949	0.99440	0.99620	1.00262	0.99360
51	1.0312"-02	3.2735"+00	NM	0.99954	0.99440	0.99620	1.00262	0.99360
52	1.0339"-02	3.2816"+00	NM	0.99964	0.99639	0.99730	1.00182	0.99549
53	1.0516"-02	3.2893"+00	NM	0.99967	0.99707	0.99780	1.00146	0.99635
54	1.0795"-02	3.2973"+00	NM	0.99988	0.99837	0.99880	1.00087	0.99793
55	1.0846"-02	3.2967"+00	NM	0.99984	0.99913	0.99740	1.00043	0.99897
56	1.3922"-02	3.3011"+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
57	1.3360"-02	3.3004"+00	NM	0.99986	0.99986	0.99999	1.00007	0.99983
58	1.3875"-02	3.2923"+00	NM	0.99988	0.99837	0.99880	1.00087	0.99793
59	1.8410"-02	3.2886"+00	NM	0.99983	0.99769	0.99830	1.00123	0.99767

INPUT VARIABLES Y,M,U/UD ASSUME P/PO
 AT 106,16,27,39,53 DATA WERE AVERAGED

70040204		WINTER/R/3		PROFILE TABULATION		82 POINTS, DELTA AT POINT 79			
I	Y	PT2/P	P/PD	TU/TOD	M/HD	U/UUD	T/TD	RHO/RHOD*U/UUD	
1	0.0000+00	1.0000+00	NM	0.97304	0.00000	0.00000	1.29638	0.00000	
2	2.5400-04	1.1797+00	NM	0.97735	0.36141	0.42507	1.24208	0.34223	
3	3.0480-04	1.1892+00	NM	0.97798	0.39079	0.43517	1.24003	0.35093	
4	3.8100-04	1.1922+00	NM	0.97788	0.39373	0.43827	1.23900	0.35373	
5	4.3180-04	1.2020+00	NM	0.97816	0.40304	0.44817	1.23646	0.36246	
6	5.0800-04	1.2053+00	NM	0.97821	0.40606	0.45136	1.23557	0.36531	
7	6.3500-04	1.2116+00	NM	0.97854	0.41180	0.45750	1.23413	0.37076	
8	7.6200-04	1.2179+00	NM	0.97833	0.41754	0.46364	1.23206	0.37617	
9	8.8900-04	1.2247+00	NM	0.97864	0.42529	0.47166	1.22993	0.38348	
10	1.1176-03	1.2362+00	NM	0.97911	0.43351	0.48036	1.22779	0.39124	
11	1.3970-03	1.2463+00	NM	0.97918	0.44204	0.48925	1.22562	0.39938	
12	1.6256-03	1.2526+00	NM	0.97920	0.44724	0.49463	1.22328	0.40437	
13	1.8796-03	1.2591+00	NM	0.97973	0.45251	0.50025	1.22214	0.40932	
14	2.2606-03	1.2717+00	NM	0.97960	0.46251	0.51055	1.21851	0.41899	
15	2.5654-03	1.2905+00	NM	0.98027	0.47693	0.52554	1.21423	0.43282	
16	2.6162-03	1.2905+00	NM	0.98027	0.47693	0.52554	1.21423	0.43282	
17	2.6416-03	1.2837+00	NM	0.98008	0.47182	0.52024	1.21582	0.42789	
18	2.6928-03	1.2936+00	NM	0.97996	0.47926	0.52784	1.21302	0.43515	
19	2.7432-03	1.2972+00	NM	0.98034	0.48190	0.53064	1.21254	0.43763	
20	2.8194-03	1.3004+00	NM	0.98050	0.48430	0.53314	1.21187	0.43993	
21	2.9464-03	1.3034+00	NM	0.98044	0.48647	0.53534	1.21101	0.44206	
22	3.0734-03	1.3097+00	NM	0.98057	0.49104	0.54004	1.20950	0.44650	
23	3.2004-03	1.3194+00	NM	0.98064	0.49515	0.54424	1.20808	0.45050	
24	3.4944-03	1.3249+00	NM	0.98118	0.50190	0.55123	1.20626	0.45698	
25	3.7084-03	1.3351+00	NM	0.98103	0.50896	0.55833	1.20344	0.46395	
26	3.9624-03	1.3477+00	NM	0.98136	0.51748	0.56703	1.20065	0.47227	
27	4.2164-03	1.3572+00	NM	0.98176	0.52384	0.57353	1.19869	0.47806	
28	4.5974-03	1.3731+00	NM	0.98201	0.53116	0.58392	1.19503	0.48863	
29	4.9530-03	1.3920+00	NM	0.98237	0.54610	0.59392	1.19080	0.50044	
30	5.0038-03	1.3952+00	NM	0.98236	0.54811	0.59792	1.19000	0.50245	
31	5.0800-03	1.3992+00	NM	0.98236	0.54811	0.59792	1.19000	0.50245	
32	5.1308-03	1.4011+00	NM	0.98265	0.55176	0.60162	1.18891	0.50603	
33	5.2070-03	1.4018+00	NM	0.98237	0.55214	0.60192	1.18843	0.50648	
34	5.3340-03	1.4090+00	NM	0.98283	0.55594	0.60582	1.18747	0.51017	
35	5.4610-03	1.4176+00	NM	0.98295	0.56168	0.61152	1.18532	0.51591	
36	5.5850-03	1.4230+00	NM	0.98306	0.56580	0.61522	1.18396	0.51962	
37	5.8420-03	1.4301+00	NM	0.98352	0.57432	0.62411	1.18092	0.52850	
38	6.1214-03	1.4550+00	NM	0.98363	0.58339	0.63301	1.17734	0.53766	
39	6.3246-03	1.4651+00	NM	0.98390	0.58905	0.63861	1.17534	0.54334	
40	6.6040-03	1.4807+00	NM	0.98413	0.59774	0.64711	1.17201	0.55213	
41	6.9850-03	1.5031+00	NM	0.98459	0.60960	0.65870	1.16759	0.56416	
42	7.3660-03	1.5217+00	NM	0.98488	0.61929	0.66810	1.16384	0.57405	
43	7.4422-03	1.5306+00	NM	0.98547	0.63387	0.68270	1.15930	0.58696	
44	7.4930-03	1.5339+00	NM	0.98534	0.63550	0.68369	1.15744	0.59070	
45	7.5692-03	1.5386+00	NM	0.98532	0.63782	0.68599	1.15642	0.59312	
46	7.6200-03	1.5397+00	NM	0.98528	0.63837	0.68639	1.15613	0.59370	
47	7.6942-03	1.5399+00	NM	0.98564	0.63844	0.68659	1.15653	0.59367	
48	7.8232-03	1.5491+00	NM	0.98567	0.64775	0.69539	1.15252	0.60337	
49	7.9532-03	1.5918+00	NM	0.98626	0.65380	0.70129	1.14956	0.60952	
50	8.0772-03	1.5918+00	NM	0.98626	0.65380	0.70129	1.14956	0.60952	
51	8.3312-03	1.6134+00	NM	0.98642	0.66388	0.71079	1.14632	0.62006	
52	8.5832-03	1.6325+00	NM	0.98671	0.67256	0.71898	1.14282	0.62913	
53	8.8372-03	1.6490+00	NM	0.98689	0.67993	0.72588	1.13975	0.63688	
54	8.9642-03	1.6663+00	NM	0.98670	0.66977	0.71639	1.14405	0.62618	
55	9.0932-03	1.6615+00	NM	0.98720	0.68543	0.73108	1.13764	0.64263	
56	9.4742-03	1.6902+00	NM	0.98763	0.69776	0.74258	1.13254	0.65565	
57	9.7770-03	1.7253+00	NM	0.98816	0.71234	0.75607	1.12657	0.67113	
58	9.8298-03	1.7281+00	NM	0.98827	0.71350	0.75717	1.12617	0.67234	
59	9.9060-03	1.7296+00	NM	0.98837	0.71412	0.75777	1.12599	0.67294	
60	9.9568-03	1.7402+00	NM	0.98856	0.71838	0.76167	1.12414	0.67756	
61	1.0033-02	1.7467+00	NM	0.98850	0.72102	0.76407	1.12298	0.68040	
62	1.0160-02	1.7500+00	NM	0.98852	0.72234	0.76527	1.12240	0.68182	
63	1.0287-02	1.7629+00	NM	0.98874	0.72746	0.76997	1.12030	0.68729	
64	1.0389-02	1.7758+00	NM	0.98892	0.73250	0.77457	1.11817	0.69271	
65	1.0668-02	1.8006+00	NM	0.98933	0.74203	0.78327	1.11422	0.70297	
66	1.0922-02	1.8292+00	NM	0.98996	0.75281	0.79306	1.10980	0.71460	
67	1.1176-02	1.8495+00	NM	0.98990	0.75678	0.79836	1.10704	0.72116	
68	1.1227-02	1.8290+00	NM	0.98978	0.75273	0.79296	1.10974	0.71459	
69	1.1405-02	1.8613+00	NM	0.99025	0.76452	0.80356	1.10474	0.72738	
70	1.1611-02	1.9024+00	NM	0.99079	0.77910	0.81656	1.09807	0.74336	
71	1.2167-02	1.9337+00	NM	0.99111	0.78987	0.82605	1.09370	0.75528	
72	1.3964-02	2.0700+00	NM	0.99293	0.83415	0.86464	1.07445	0.80473	
73	1.5189-02	2.2474+00	NM	0.99509	0.88687	0.90923	1.05105	0.86507	
74	1.6078-02	2.3741+00	NM	0.99656	0.92200	0.93812	1.03528	0.90615	
75	1.7374-02	2.5107+00	NM	0.99804	0.95797	0.96701	1.01895	0.94902	
76	1.8313-02	2.5999+00	NM	0.99904	0.97961	0.98410	1.00920	0.97513	
77	1.9710-02	2.6303+00	NM	0.99959	0.99310	0.99460	1.00303	0.99160	
78	2.1285-02	2.6689+00	NM	0.99990	0.99767	0.99820	1.00106	0.99715	
79	2.2200-02	2.6785+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
80	2.4384-02	2.6785+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
81	2.5679-02	2.6785+00	NM	0.99976	0.99922	0.99910	1.00019	0.99915	
82	2.8118-02	2.6793+00	NM	0.99976	0.99922	0.99930	1.00015	0.99913	

INPUT VARIABLES Y,M,U/UD ASSUME P/PD
 AT I=4,16,29,31,45,59 DATA WERE AVERAGED

70040205

WINTER/R/3

PROFILE TABULATION

89 POINTS, DELTA AT POINT B4

I	Y	PT/P	P/PD	T0/T0D	M/Z/D	U/U/D	T/T/D	H/D/RHDD*U/U/D
1	0.0000+00	1.0000+00	NM	0.97305	0.00000	0.00000	1.28644	0.00000
2	2.5400-04	1.4179+00	NM	0.78115	0.57073	0.61840	1.17482	0.52674
3	3.3020-04	1.4321+00	NM	0.8360	0.57724	0.62750	1.17357	0.53470
4	3.8100-04	1.4440+00	NM	0.98405	0.58657	0.63480	1.17170	0.54201
5	4.5720-04	1.4568+00	NM	0.98430	0.59353	0.64170	1.16869	0.54908
6	5.0800-04	1.4662+00	NM	0.98431	0.59894	0.64690	1.16655	0.55454
7	6.0030-04	1.4842+00	NM	0.98471	0.60895	0.65670	1.16297	0.56468
8	7.8740-04	1.4968+00	NM	0.98503	0.61581	0.66340	1.16054	0.57163
9	9.1440-04	1.5281+00	NM	0.98536	0.63236	0.67940	1.15431	0.58457
10	1.0414-03	1.5377+00	NM	0.98579	0.63732	0.68420	1.15251	0.59366
11	1.3208-03	1.5526+00	NM	0.98588	0.64489	0.69140	1.14945	0.60151
12	1.5748-03	1.5804+00	NM	0.98640	0.65860	0.70450	1.14424	0.61567
13	1.8542-03	1.5864+00	NM	0.98655	0.66152	0.70730	1.14371	0.61870
14	2.0828-03	1.5989+00	NM	0.98685	0.66751	0.71300	1.14095	0.62492
15	2.3368-03	1.6183+00	NM	0.98723	0.67476	0.71990	1.13878	0.63245
16	2.6870-03	1.6237+00	NM	0.98716	0.67907	0.72390	1.13632	0.63706
17	2.7432-03	1.6362+00	NM	0.98735	0.68485	0.72930	1.13404	0.64310
18	2.8194-03	1.6456+00	NM	0.98753	0.68710	0.73330	1.13239	0.64757
19	2.8702-03	1.6456+00	NM	0.98753	0.68710	0.73330	1.13239	0.64757
20	2.9464-03	1.6456+00	NM	0.98753	0.68710	0.73330	1.13239	0.64757
21	2.9972-03	1.6484+00	NM	0.98763	0.69036	0.73450	1.13196	0.64888
22	3.1496-03	1.6545+00	NM	0.98778	0.69312	0.73710	1.13093	0.65170
23	3.2766-03	1.6607+00	NM	0.98795	0.69588	0.73970	1.12991	0.65465
24	3.4036-03	1.6752+00	NM	0.98805	0.70226	0.74560	1.12723	0.66144
25	3.5306-03	1.6738+00	NM	0.98800	0.70163	0.74500	1.12744	0.66079
26	3.8100-03	1.6887+00	NM	0.98823	0.70009	0.75100	1.12486	0.66764
27	4.0640-03	1.7008+00	NM	0.98864	0.71329	0.75590	1.12303	0.67309
28	4.3130-03	1.7163+00	NM	0.98879	0.71984	0.76190	1.12029	0.68009
29	4.5812-03	1.7349+00	NM	0.98907	0.72756	0.76900	1.11716	0.68835
30	4.8006-03	1.7111+00	NM	0.98913	0.73008	0.77130	1.11610	0.69107
31	5.1308-03	1.7627+00	NM	0.98947	0.73883	0.77930	1.11256	0.70004
32	5.2070-03	1.7661+00	NM	0.98947	0.74017	0.78050	1.11199	0.70192
33	5.2832-03	1.7754+00	NM	0.98968	0.74387	0.78390	1.11051	0.70589
34	5.3340-03	1.7754+00	NM	0.98968	0.74387	0.78390	1.11051	0.70589
35	5.4102-03	1.7784+00	NM	0.98979	0.74505	0.78500	1.11010	0.70714
36	5.4610-03	1.7754+00	NM	0.98968	0.74387	0.78390	1.11051	0.70589
37	5.6134-03	1.7814+00	NM	0.98965	0.74624	0.78600	1.10941	0.70849
38	5.7404-03	1.8036+00	NM	0.99007	0.75491	0.79390	1.10598	0.71783
39	5.8674-03	1.8038+00	NM	0.99017	0.75498	0.79400	1.10602	0.71789
40	5.9944-03	1.8065+00	NM	0.99014	0.75601	0.79490	1.10553	0.71902
41	6.2738-03	1.8249+00	NM	0.99035	0.76302	0.80120	1.10257	0.72667
42	6.5278-03	1.8370+00	NM	0.99091	0.76759	0.80530	1.10086	0.73185
43	6.8072-03	1.8491+00	NM	0.99086	0.77209	0.80940	1.09949	0.73649
44	7.0358-03	1.8730+00	NM	0.99123	0.78113	0.81790	1.09524	0.74641
45	7.3132-03	1.8894+00	NM	0.99127	0.78674	0.82220	1.09269	0.75263
46	7.6200-03	1.9107+00	NM	0.99143	0.79439	0.82920	1.08959	0.76104
47	7.7724-03	1.9363+00	NM	0.99202	0.80322	0.83700	1.08589	0.77079
48	7.8456-03	1.9363+00	NM	0.99202	0.80322	0.83700	1.08589	0.77079
49	7.8994-03	1.9363+00	NM	0.99202	0.80322	0.83700	1.08589	0.77079
50	7.9756-03	1.9424+00	NM	0.99194	0.80534	0.83880	1.08481	0.77322
51	8.0264-03	1.9424+00	NM	0.99194	0.80534	0.83880	1.08481	0.77322
52	8.1788-03	1.9549+00	NM	0.99227	0.80960	0.84260	1.08319	0.77789
53	8.3058-03	1.9614+00	NM	0.99228	0.81181	0.84450	1.08217	0.78038
54	8.4328-03	1.9726+00	NM	0.99241	0.81599	0.84780	1.08059	0.78460
55	8.5598-03	1.9830+00	NM	0.99273	0.81906	0.85090	1.07927	0.78840
56	8.6392-03	2.0071+00	NM	0.99295	0.82709	0.85780	1.07563	0.79749
57	9.0932-03	2.0222+00	NM	0.99320	0.83198	0.86210	1.07372	0.80291
58	9.3726-03	2.0375+00	NM	0.99343	0.83695	0.86640	1.07162	0.80849
59	9.3900-03	2.0375+00	NM	0.99343	0.83695	0.86640	1.07162	0.80849
60	9.6012-03	2.0624+00	NM	0.99365	0.84491	0.87320	1.06810	0.81753
61	9.8832-03	2.0779+00	NM	0.99388	0.84979	0.87740	1.06603	0.82305
62	1.0185+02	2.1037+00	NM	0.99423	0.85846	0.88480	1.06231	0.83240
63	1.0211+02	2.1064+00	NM	0.99402	0.85870	0.88490	1.06196	0.83327
64	1.0287+02	2.1125+00	NM	0.99430	0.86090	0.88660	1.06137	0.83534
65	1.0338+02	2.1184+00	NM	0.99451	0.86240	0.88820	1.06073	0.83735
66	1.0414+02	2.1248+00	NM	0.99443	0.86437	0.88980	1.05970	0.83967
67	1.0465+02	2.1248+00	NM	0.99443	0.86437	0.88980	1.05970	0.83967
68	1.0617+02	2.1359+00	NM	0.99482	0.87383	0.89780	1.05562	0.85050
69	1.0744+02	2.1502+00	NM	0.99467	0.87209	0.89630	1.05428	0.84854
70	1.0871+02	2.1614+00	NM	0.99490	0.87548	0.89920	1.05491	0.85239
71	1.0998+02	2.1656+00	NM	0.99504	0.87674	0.90030	1.05446	0.85380
72	1.1278+02	2.1960+00	NM	0.99539	0.88391	0.90790	1.05051	0.86425
73	1.1532+02	2.2139+00	NM	0.99537	0.89109	0.91220	1.04795	0.87046
74	1.1786+02	2.2355+00	NM	0.99574	0.89739	0.91750	1.04532	0.87772
75	1.1836+02	2.2385+00	NM	0.99595	0.89826	0.91830	1.04512	0.87885
76	1.2014+02	2.2573+00	NM	0.99594	0.90370	0.92270	1.04250	0.88508
77	1.2268+02	2.2757+00	NM	0.99624	0.90898	0.92710	1.04027	0.89121
78	1.2624+02	2.3035+00	NM	0.99660	0.91686	0.93360	1.03686	0.90041
79	1.4326+02	2.4270+00	NM	0.99793	0.95090	0.96120	1.02178	0.94072
80	1.5977+02	2.5166+00	NM	0.99892	0.97442	0.98010	1.01127	0.96918
81	1.6866+02	2.5988+00	NM	0.99936	0.98581	0.98890	1.00627	0.98274
82	1.8390+02	2.5940+00	NM	0.99964	0.99456	0.99570	1.00229	0.99383
83	1.9279+02	2.6061+00	NM	0.99998	0.99764	0.99820	1.00113	0.99707
84	2.0833+02	2.6155+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
85	2.2530+02	2.6155+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
86	2.3393+02	2.6186+00	NM	1.00001	1.00009	1.00000	0.99962	1.00098
87	2.5832+02	2.6155+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
88	2.9870+02	2.6155+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000
89	3.2263+02	2.6155+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M,U/UD ASSUME P=PD
AT I=9,24,38,53,69 DATA WERE AVERAGED

70040206	WINTER/R/S	PROFILE TABULATION	98 POINTS, DELTA AT POINT 94					
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RRHO*U/UD
1	0.0000*+00	1.0000*+00	NM	0.97453	0.00000	0.00000	1.26036	0.00000
2	2.5400*-04	1.4405*+00	NM	0.98529	0.61219	0.65595	1.14808	0.57135
3	3.3020*-04	1.4551*+00	NM	0.98584	0.62104	0.66466	1.14542	0.58028
4	3.8100*-04	1.4866*+00	NM	0.98634	0.63948	0.68249	1.13902	0.59919
5	4.5720*-04	1.4976*+00	NM	0.98670	0.64577	0.68860	1.13703	0.60561
6	5.0800*-04	1.5115*+00	NM	0.98681	0.65354	0.69600	1.13416	0.61367
7	5.8420*-04	1.5226*+00	NM	0.98716	0.65966	0.70191	1.13219	0.61996
8	6.6040*-04	1.5481*+00	NM	0.98746	0.67339	0.71493	1.12717	0.63427
9	7.8740*-04	1.5620*+00	NM	0.98774	0.68067	0.72184	1.12462	0.64185
10	1.0414*-03	1.6184*+00	NM	0.98892	0.70904	0.74857	1.11462	0.67159
11	1.1684*-03	1.6414*+00	NM	0.98905	0.72012	0.75879	1.11076	0.68343
12	1.2954*-03	1.6579*+00	NM	0.98960	0.72790	0.76610	1.10771	0.69160
13	1.4478*-03	1.6760*+00	NM	0.98990	0.73625	0.77301	1.10462	0.70052
14	1.7018*-03	1.6899*+00	NM	0.99020	0.74254	0.77961	1.10236	0.70722
15	1.9558*-03	1.7127*+00	NM	0.99056	0.75271	0.78693	1.09855	0.71815
16	2.2098*-03	1.7414*+00	NM	0.99089	0.76320	0.80024	1.09369	0.73169
17	2.4892*-03	1.7531*+00	NM	0.99109	0.77016	0.80475	1.09183	0.73706
18	2.7432*-03	1.7730*+00	NM	0.99156	0.77851	0.81236	1.08883	0.74608
19	2.8194*-03	1.7676*+00	NM	0.99126	0.77628	0.81025	1.08944	0.74373
20	2.8702*-03	1.7762*+00	NM	0.99163	0.77984	0.81356	1.08835	0.74751
21	2.9464*-03	1.7814*+00	NM	0.99163	0.78199	0.81546	1.08744	0.74989
22	2.9972*-03	1.7814*+00	NM	0.99163	0.78199	0.81546	1.08744	0.74989
23	3.0734*-03	1.7870*+00	NM	0.99153	0.78430	0.81746	1.08635	0.75249
24	3.1496*-03	1.7898*+00	NM	0.99172	0.78546	0.81856	1.08607	0.75370
25	3.2768*-03	1.8067*+00	NM	0.99187	0.79232	0.82467	1.08332	0.76125
26	3.4036*-03	1.8121*+00	NM	0.99214	0.79448	0.82667	1.08270	0.76353
27	3.5306*-03	1.8125*+00	NM	0.99203	0.79464	0.82677	1.08251	0.76376
28	3.6830*-03	1.8264*+00	NM	0.99311	0.80018	0.83208	1.08132	0.76951
29	3.8100*-03	1.8308*+00	NM	0.99211	0.80192	0.83318	1.07949	0.77183
30	3.9370*-03	1.8428*+00	NM	0.99256	0.80663	0.83749	1.07797	0.77691
31	4.2164*-03	1.8567*+00	NM	0.99263	0.81201	0.84219	1.07573	0.78290
32	4.4958*-03	1.8679*+00	NM	0.99280	0.81631	0.84600	1.07407	0.78766
33	4.7498*-03	1.8851*+00	NM	0.99316	0.82284	0.85181	1.07164	0.79486
34	5.0038*-03	1.8937*+00	NM	0.99320	0.82607	0.85461	1.07030	0.79848
35	5.2324*-03	1.9000*+00	NM	0.99345	0.82838	0.85671	1.06957	0.80099
36	5.2832*-03	1.9082*+00	NM	0.99339	0.83144	0.85932	1.06817	0.80448
37	5.3086*-03	1.9000*+00	NM	0.99345	0.82838	0.85671	1.06957	0.80099
38	5.3594*-03	1.9024*+00	NM	0.99317	0.82946	0.85751	1.06879	0.80232
39	5.4356*-03	1.9031*+00	NM	0.99323	0.82954	0.85761	1.06883	0.80239
40	5.4864*-03	1.9136*+00	NM	0.99361	0.83343	0.86112	1.06755	0.80663
41	5.5628*-03	1.9136*+00	NM	0.99361	0.83343	0.86112	1.06755	0.80663
42	5.6388*-03	1.9190*+00	NM	0.99361	0.83541	0.86282	1.06669	0.80898
43	5.7658*-03	1.9306*+00	NM	0.99360	0.83963	0.86643	1.06484	0.81367
44	5.8928*-03	1.9388*+00	NM	0.99396	0.84261	0.86913	1.06394	0.81690
45	6.0198*-03	1.9356*+00	NM	0.99393	0.84145	0.86813	1.06441	0.81560
46	6.1722*-03	1.9425*+00	NM	0.99390	0.84393	0.87023	1.06329	0.81843
47	6.2492*-03	1.9517*+00	NM	0.99409	0.84724	0.87314	1.06206	0.82212
48	6.4262*-03	1.9636*+00	NM	0.99413	0.85146	0.87674	1.06026	0.82691
49	6.6802*-03	1.9718*+00	NM	0.99424	0.85435	0.87924	1.05911	0.83017
50	6.9596*-03	1.9942*+00	NM	0.99461	0.86221	0.88605	1.05406	0.83901

70040206		WINTER/R/S		PROFILE TABULATION		98 POINTS, DELTA AT POINT 94			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
51	7.2136*-03	1.9973*+00	NM	0.99460	0.86329	0.88695	1.05558	0.84025	
52	7.4930*-03	2.0117*+00	NM	0.99488	0.86825	0.89126	1.05370	0.84583	
53	7.7724*-03	2.0236*+00	NM	0.99489	0.87230	0.89466	1.05193	0.85050	
54	7.8486*-03	2.0238*+00	NM	0.99496	0.87238	0.89476	1.05196	0.85057	
55	7.8794*-03	2.0324*+00	NM	0.99513	0.87528	0.89727	1.05087	0.85383	
56	7.9756*-03	2.0294*+00	NM	0.99520	0.87429	0.89647	1.05138	0.85266	
57	8.0264*-03	2.0346*+00	NM	0.99530	0.87602	0.89797	1.05173	0.85462	
58	8.1026*-03	2.0431*+00	NM	0.99527	0.87892	0.90037	1.04941	0.85798	
59	8.1788*-03	2.0486*+00	NM	0.99523	0.88074	0.90187	1.04857	0.86010	
60	8.3058*-03	2.0486*+00	NM	0.99523	0.88074	0.90187	1.04857	0.86010	
61	8.4328*-03	2.0597*+00	NM	0.99546	0.88446	0.90508	1.04716	0.86431	
62	8.7122*-03	2.0732*+00	NM	0.99566	0.88893	0.90888	1.04540	0.86941	
63	8.8392*-03	2.0754*+00	NM	0.99584	0.88967	0.90958	1.04526	0.87019	
64	8.9862*-03	2.0847*+00	NM	0.99577	0.89273	0.91209	1.04383	0.87379	
65	9.2456*-03	2.1009*+00	NM	0.99605	0.89802	0.91659	1.04178	0.87983	
66	9.3980*-03	2.1090*+00	NM	0.99610	0.90067	0.91879	1.04065	0.88290	
67	9.4742*-03	2.1090*+00	NM	0.99610	0.90067	0.91879	1.04065	0.88290	
68	9.7282*-03	2.1230*+00	NM	0.99637	0.90538	0.92280	1.03884	0.88830	
69	1.0008*-02	2.1381*+00	NM	0.99659	0.91002	0.92670	1.03701	0.89363	
70	1.0168*-02	2.1363*+00	NM	0.99654	0.90944	0.92620	1.03721	0.89297	
71	1.0236*-02	2.1394*+00	NM	0.99651	0.91043	0.92701	1.03674	0.89415	
72	1.0287*-02	2.1500*+00	NM	0.99679	0.91382	0.92991	1.03552	0.89801	
73	1.0364*-02	2.1477*+00	NM	0.99659	0.91308	0.92921	1.03565	0.89722	
74	1.0434*-02	2.1527*+00	NM	0.99663	0.91465	0.93051	1.03499	0.89906	
75	1.0496*-02	2.1555*+00	NM	0.99675	0.91556	0.93131	1.03471	0.90007	
76	1.0566*-02	2.1591*+00	NM	0.99681	0.91638	0.93201	1.03440	0.90102	
77	1.0629*-02	2.1608*+00	NM	0.99686	0.91721	0.93271	1.03409	0.90197	
78	1.0820*-02	2.1721*+00	NM	0.99688	0.92077	0.93562	1.03251	0.90615	
79	1.0973*-02	2.1747*+00	NM	0.99694	0.92159	0.93632	1.03221	0.90710	
80	1.1100*-02	2.1871*+00	NM	0.99704	0.92548	0.93952	1.03057	0.91165	
81	1.1227*-02	2.1935*+00	NM	0.99723	0.92747	0.94122	1.02989	0.91391	
82	1.1354*-02	2.1967*+00	NM	0.99723	0.92846	0.94202	1.02943	0.91509	
83	1.1633*-02	2.2217*+00	NM	0.99764	0.93615	0.94843	1.02641	0.92403	
84	1.1887*-02	2.2271*+00	NM	0.99757	0.93780	0.94973	1.02560	0.92603	
85	1.1913*-02	2.2241*+00	NM	0.99764	0.93690	0.94903	1.02608	0.92491	
86	1.2141*-02	2.2387*+00	NM	0.99766	0.94136	0.95264	1.02410	0.93022	
87	1.2421*-02	2.2532*+00	NM	0.99785	0.94574	0.95624	1.02232	0.93536	
88	1.2700*-02	2.2614*+00	NM	0.99809	0.94823	0.95835	1.02146	0.93821	
89	1.4427*-02	2.3249*+00	NM	0.99877	0.96708	0.97367	1.01366	0.96054	
90	1.6078*-02	2.3736*+00	NM	0.99937	0.98123	0.98508	1.00787	0.97739	
91	1.6942*-02	2.3938*+00	NM	0.99954	0.98702	0.98969	1.00542	0.98435	
92	1.8491*-02	2.4168*+00	NM	0.99978	0.99355	0.99407	1.00271	0.99221	
93	1.9380*-02	2.4253*+00	NM	0.99987	0.99545	0.99680	1.00170	0.99510	
D 94	2.1031*-02	2.4397*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
95	2.5044*-02	2.4456*+00	NM	1.00025	1.00165	1.00140	0.99450	1.00191	
96	2.7639*-02	2.4426*+00	NM	1.00012	1.00083	1.00070	0.99975	1.00095	
97	3.0150*-02	2.4426*+00	NM	1.00012	1.00083	1.00070	0.99975	1.00095	
98	3.2614*-02	2.4426*+00	NM	1.00012	1.00083	1.00070	0.99975	1.00095	

INPUT VARIABLES Y,M,U/UD ASSUME P=PD
 AT I=11,18,28,46,53,62,72,80 DATA WERE AVERAGED

SECTION D: ADDITIONAL DATA.

FACSIMILE FROM SOURCE PAPER: NB. AUTHORS' SYMBOLS AND UNITS

PRESSURE DISTRIBUTION AND SKIN FRICTION.

x in	ϕ deg	$M_{\infty} = 0.597$ $Re_{\ell} = 9.85 \times 10^6$			$M_{\infty} = 0.801$ $Re_{\ell} = 9.98 \times 10^6$			$M_{\infty} = 1.390$ $Re_{\ell} = 5.04 \times 10^6$			$M_{\infty} = 1.398$ $Re_{\ell} = 10.2 \times 10^6$		
		C_p	M_{δ}	$10^3 a_f$	C_p	M_{δ}	$10^3 a_f$	C_p	M_{δ}	$10^3 a_f$	C_p	M_{δ}	$10^3 a_f$
3.0	0	0.311	0.493	3.92	0.371	0.631	3.66	0.413	1.050	2.52	0.417	1.053	3.88
3.0	90	0.310			0.369			0.407			0.406		
3.0	-180	0.314			0.374			0.409			0.402		
3.0	-90	0.310			0.368			0.411			0.401		
6.0	0	0.202	0.530	3.70	0.262	0.681	3.70	0.427	1.040	1.91	0.433	1.042	3.79
12.0	0	-0.222	0.666	3.59	-0.218	0.900	3.87	0.153	1.251	0.68	0.151	1.260	1.01
15.0	0	-0.382	0.715	2.80	-0.458	1.012	3.37	-0.040	1.427	2.24	-0.042	1.438	3.56
18.0	0	-0.399	0.720	2.37	-0.499	1.032	2.72	-0.180	1.582	1.78	-0.181	1.593	3.17
21.0	0	-0.313	0.694	2.45	-0.349	0.960	2.37	-0.281	1.715	1.69	-0.281	1.727	3.37
21.0	90	-0.313			-0.348			-0.280			-0.284		
21.0	-180	-0.310			-0.346			-0.279			-0.275		
21.0	-90	-0.313			-0.350			-0.279			-0.280		
24.0	0	-0.145	0.642	1.83	-0.133	0.861	1.62	-0.273			-0.302	1.759	2.72
27.0	0	-0.004	0.598	1.53	0.027	0.788	1.27	-0.256	1.679	0.65	-0.258	1.695	2.23
28.5	0	0.037	0.585	1.42	0.068	0.770	1.25	-0.248	1.669	0.71	-0.208	1.626	1.92
30.0	0	0.058	0.578	1.35	0.095	0.758	1.20	-0.204	1.611	0.74	-0.154	1.561	1.54
31.5	0	0.073	0.573	1.59	0.108	0.752	1.48	-0.116	1.508	1.97	-0.109	1.509	1.58
33.0	0	0.084	0.569	1.47	0.117	0.748	1.39	-0.062	1.450	2.99	-0.070	1.467	1.43
34.5	0	0.090	0.567	1.47	0.123	0.745	1.42	-0.021	1.409	2.90	-0.038	1.434	1.34
36.0	0	0.103	0.563	1.48	0.137	0.739	1.44	0.009	1.379	2.50	-0.010	1.406	1.31
37.5	0	0.115	0.559	1.31	0.149	0.733	1.35	0.034	1.356	2.58	0.016	1.381	1.16
40.0	0	0.158	0.545	1.31	0.197	0.711	1.19	0.091	1.304	2.24	0.093	1.310	1.00
42.0	0	0.183	0.537	1.43	0.221	0.700	1.38	0.196	1.215	1.73	0.166	1.247	0.83
42.0	90	0.181			0.218			0.191			0.166		
42.0	-180	0.182			0.222			0.198			0.168		
42.0	-90	0.178			0.219			0.191			0.165		
44.0	0	0.168	0.542	1.40	0.208	0.707	1.29	0.249	1.173	1.75	0.200	1.219	0.91
45.5	0	0.138	0.552	1.62	0.178	0.720	1.53	0.228	1.182	2.02	0.198	1.221	1.14
47.0	0	0.116	0.558	1.72	0.150	0.733	1.74	0.208	1.206	2.24	0.188	1.229	1.33
48.5	0	0.103	0.563	1.76	0.133	0.740	1.79	0.191	1.219	2.46	0.178	1.237	1.56
50.0	0	0.092	0.567	1.85	0.128	0.743	1.84	0.188	1.222	2.50	0.176	1.238	1.71
51.5	0	0.086	0.569	1.79	0.124	0.745	1.70	0.186	1.223	2.30	0.178	1.237	1.70
53.0	0	0.074	0.573	2.12	0.116	0.748	2.02	0.197	1.215	2.63	0.188	1.229	1.97
54.5	0	0.058	0.578	2.10	0.097	0.757	2.06	0.197	1.215	2.63	0.190	1.227	2.05
56.0	0	0.037	0.585	2.10	0.077	0.766	2.09	0.218	1.197	2.44	0.207	1.213	2.00
57.5	0	-0.000	0.597	2.27	0.038	0.783	2.30	0.229	1.189	2.63	0.222	1.201	2.09
59.0	0	-0.083	0.623	3.47	-0.047	0.822	2.54	0.248	1.174	2.56	0.236	1.189	2.17
59.0	90	-0.074			-0.037			0.254			0.244		
59.0	-180	-0.080			-0.044			0.246			0.237		
59.0	-90	-0.081			-0.045			0.253			0.237		

SECTION D: ADDITIONAL DATA.

FACSIMILE FROM SOURCE PAPER: NB. AUTHORS' SYMBOLS AND UNITS

PRESSURE DISTRIBUTION AND SKIN FRICTION.


x in	φ deg	$M_{\infty} = 1.404$ $Re_{\ell} = 19.97 \times 10^6$			$M_{\infty} = 1.700$ $Re_{\ell} = 10.08 \times 10^6$			$M_{\infty} = 1.996$ $Re_{\ell} = 4.98 \times 10^6$			$M_{\infty} = 2.000$ $Re_{\ell} = 9.96 \times 10^6$		
		C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$
3.0	0	0.417	1.057	3.95	0.360	1.319	1.40	0.333	1.553	1.91	0.325	1.567	1.27
3.0	90	0.403			0.354			0.334			0.327		
3.0	-180	0.400			0.350			0.330			0.324		
3.0	-90	0.408			0.350			0.329			0.323		
6.0	0	0.437	1.043	3.20	0.368	1.311	3.93	0.333	1.553	1.44	0.336	1.556	3.63
12.0	0	0.155	1.261	0.91	0.166	1.501	3.69	0.166	1.737	1.42	0.163	1.749	3.20
15.0	0	-0.040	1.442		0.000	1.696		0.029	1.933	1.46	0.022	1.954	2.54
18.0	0	-0.179	1.598	2.76	-0.115	1.870	2.58	-0.075	2.130	1.12	-0.080	2.154	2.10
21.0	0	-0.282	1.738	2.99	-0.201	2.036	2.75	-0.141	2.298	1.14	-0.150	2.341	2.19
21.0	90	-0.284			-0.199			-0.140			-0.149		
21.0	-180	-0.279			-0.198			-0.141			-0.149		
21.0	-90	-0.277			-0.196			-0.140			-0.148		
24.0	0	-0.299	1.763	2.31	-0.223	2.086	2.34	-0.162	2.360	0.29	-0.173	2.416	1.88
27.0	0	-0.253	1.695	1.93	-0.196	2.025	1.96	-0.139	2.291	0.36	-0.160	2.372	1.73
28.5	0	-0.206	1.632	1.73	-0.168	1.966	1.90	-0.138			-0.140	2.310	1.69
30.0	0	-0.156	1.570	1.46	-0.134	1.903	1.60	-0.134			-0.116	2.244	1.50
31.5	0	-0.110	1.517	1.59	-0.104	1.852	1.67	-0.115			-0.094	2.187	1.47
33.0	0	-0.069	1.472	1.40	-0.074	1.803	1.47	-0.083	2.149	0.30	-0.070	2.134	1.44
34.5	0	-0.038	1.441	1.40	-0.050	1.767	1.38	-0.056	2.089	1.56	-0.051	2.093	1.34
36.0	0	-0.010	1.412	1.45	-0.029	1.737	1.38	-0.025	2.029	2.60	-0.033	2.054	1.33
37.5	0	0.016	1.386	1.26	-0.007	1.706	1.20	0.001	1.981	2.38	-0.015	2.021	1.16
40.0	0	0.089	1.318	1.13	0.046	1.637	1.07	0.038	1.917	2.49	0.024	1.951	1.11
42.0	0	0.174	1.245	0.86	0.123	1.547	0.83	0.118	1.799	2.24	0.095	1.840	0.85
42.0	90	0.171			0.122			0.106			0.092		
42.0	-180	0.174			0.125			0.112			0.100		
42.0	-90	0.169			0.122			0.108			0.093		
44.0	0	0.211	1.215	0.90	0.169	1.498	0.92	0.181	1.718	2.20	0.147	1.770	0.94
45.5	0	0.205	1.219	1.17	0.172	1.495	1.18	0.181	1.719	2.51	0.154	1.761	1.23
47.0	0	0.191	1.231	1.40	0.163	1.504	1.46	0.173	1.728	2.45	0.150	1.765	1.53
48.5	0	0.180	1.241	1.54	0.156	1.512	1.75	0.163	1.740	2.60	0.145	1.772	1.82
50.0	0	0.181	1.239	1.65	0.156	1.512	1.93	0.157	1.748	2.64	0.144	1.773	1.98
51.5	0	0.182	1.239	1.56	0.154	1.513	1.54	0.153	1.753	2.44	0.142	1.776	1.96
53.0	0	0.194	1.229	1.83	0.164	1.504	2.23	0.157	1.748	2.75	0.148	1.767	2.26
54.5	0	0.194	1.229	1.87	0.162	1.505	2.38	0.160	1.744	2.69	0.150	1.766	2.35
56.0	0	0.210	1.216	1.83	0.178	1.489	2.27	0.174	1.727	2.44	0.165	1.746	2.17
57.5	0	0.224	1.204	1.90	0.190	1.476	2.38	0.184	1.715	2.59	0.175	1.734	2.33
59.0	0	0.239	1.192	1.55	0.202	1.464	2.43	0.194	1.702	2.58	0.185	1.721	2.37
59.0	90	0.249			0.211			0.199			0.188		
59.0	-180	0.240			0.204			0.191			0.181		
59.0	-90	0.245			0.206			0.194			0.184		

SECTION D: ADDITIONAL DATA.

FACSIMILE FROM SOURCE PAPER: NB. AUTHORS' SYMBOLS AND UNITS

PRESSURE DISTRIBUTION AND SKIN FRICTION.

x in	ϕ deg	$M_{\infty} = 2.002$ $Re_{\ell} = 16.85 \times 10^6$			$M_{\infty} = 2.401$ $Re_{\ell} = 10.03 \times 10^6$			$M_{\infty} = 2.793$ $Re_{\ell} = 5.03 \times 10^6$			$M_{\infty} = 2.799$ $Re_{\ell} = 10.05 \times 10^6$		
		C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$	C_p	M_b	$10^3 c_f$
3.0	0	0.330	1.564	3.50	0.307	1.868	1.11	0.300	2.133	1.49	0.291	2.153	1.06
3.0	90	0.331			0.306			0.298			0.289		
3.0	-180	0.323			0.304			0.299			0.288		
3.0	-90	0.322			0.302			0.294			0.286		
6.0	0	0.337	1.557	2.99	0.312	1.862	3.35	0.301	2.132	1.10	0.292	2.151	2.34
12.0	0	0.162	1.752	2.83	0.165	2.058	2.73	0.168	2.336	1.12	0.158	2.364	2.35
15.0	0	0.019	1.962	2.40	0.038	2.292	2.05	0.056	2.580	0.85	0.040	2.636	1.83
18.0	0	-0.081	2.162	2.01	-0.050	2.528	1.73	-0.028	2.859	0.93	-0.036	2.908	1.57
21.0	0	-0.153	2.354	2.17	-0.109	2.756	1.78	-0.048	2.950	1.06	-0.082	3.162	1.45
21.0	90	-0.152			-0.108			-0.049			-0.080		
21.0	-180	-0.150			-0.110			-0.046			-0.080		
21.0	-90	-0.151			-0.106			-0.041			-0.078		
24.0	0	-0.176	2.430	1.82	-0.130	2.865	1.50	-0.074			-0.101	3.301	1.13
27.0	0	-0.163	2.385	1.60	-0.123	2.826	1.39	-0.065			-0.096	3.261	1.04
28.5	0	-0.142	2.321	1.58	-0.111	2.766	1.39	-0.068	3.050	0.35	-0.089	3.208	1.09
30.0	0	-0.118	2.252	1.35	-0.094	2.691	1.31	-0.066	3.043	0.45	-0.077	3.131	1.21
31.5	0	-0.096	2.196	1.42	-0.080	2.633	1.29	-0.068	3.051	0.87	-0.066	3.064	1.14
33.0	0	-0.074	2.143	1.35	-0.063	2.571	1.24	-0.066	3.039	0.41	-0.056	3.005	1.13
34.5	0	-0.053	2.099	1.27	-0.048	2.522	1.18	-0.061	3.011	0.31	-0.045	2.954	1.23
36.0	0	-0.035	2.061	1.26	-0.036	2.484	1.22	-0.050			-0.031	2.890	1.03
37.5	0	-0.017	2.026	1.11	-0.022	2.444	1.09	-0.037			-0.021	2.844	0.95
40.0	0	0.022	1.957	1.11	0.009	2.361	1.04	0.008	2.724	0.63	0.004	2.751	0.98
42.0	0	0.095	1.842	0.93	0.066	2.233	0.91	0.068	2.547	1.55	0.053	2.600	0.83
42.0	90	0.091			0.064			0.066			0.048		
42.0	-180	0.093			0.069			0.070			0.052		
42.0	-90	0.090			0.064			0.069			0.050		
44.0	0	0.147	1.771	0.88	0.119	2.134	1.00	0.131	2.407	1.96	0.106	2.468	0.93
45.5	0	0.153	1.763	1.22	0.131	2.114	1.33	0.147	2.376	2.19	0.122	2.435	1.21
47.0	0	0.148	1.769	1.55	0.132	2.112	1.53	0.145	2.378	2.06	0.125	2.429	1.36
48.5	0	0.143	1.776	1.79	0.127	2.120	1.78	0.137	2.395	2.18	0.120	2.438	1.56
50.0	0	0.143	1.776	1.93	0.128	2.118	1.90	0.136	2.397	2.20	0.121	2.437	1.68
51.5	0	0.140	1.780	1.87	0.129	2.117	1.77	0.138	2.393	1.73	0.122	2.435	1.51
53.0	0	0.147	1.771	2.13	0.133	2.110	2.08	0.140	2.389	2.06	0.126	2.426	1.77
54.5	0	0.148	1.770	2.20	0.135	2.106	2.12	0.136	2.397	2.20	0.127	2.424	1.83
56.0	0	0.162	1.752	2.04	0.148	2.036	1.94	0.149	2.372	2.01	0.137	2.404	1.72
57.5	0	0.174	1.737	2.14	0.157	2.070	2.09	0.152	2.366	2.19	0.144	2.390	1.87
59.0	0	0.183	1.726	2.14	0.167	2.056	2.15	0.167	2.337	2.05	0.155	2.369	1.88
59.0	90	0.186			0.170			0.172			0.159		
59.0	-180	0.176			0.164			0.168			0.152		
59.0	-90	0.181			0.167			0.166			0.156		

axisymmetric 	M : 2.96 (free stream) R THETA X 10 ⁻³ : 1.4 - 10 TW/TR : 1	7005
		VPG - AW
Continuous tunnel with asymmetric sliding block variable nozzle. PO : 0.17 MN/m ² . TO : 340 K. Dried Air. RE/m X 10 ⁻⁶ : 10 (in free stream).		
ALLEN J.M., 1970. Experimental Preston tube and law-of-the-wall study of turbulent skin friction on axis-symmetric bodies at supersonic speeds. NASA TN D-5560. And Allen J.M., private communication.		

- 1 The test boundary layer was formed on a "Haack-Adams body" constructed of aluminium and mounted on the centre line of the test section. The body was not actively cooled, the temperatures being allowed to settle for up to 30 minutes. The form of the body is given by

$$\frac{r}{r_{\max}} = \left\{ 0.70700 [1-z^2]^{1.5} + 0.16934 Z [1-z^2]^{0.5} + 0.16934 \cos^{-1} -Z \right\}^{0.5}$$

where $Z = \left(\frac{2x}{l} - 1\right)$, $r_{\max} = 45.72$ mm and $l = 914.4$ mm.

- 4 Surveys were made at seven stations on the model surface such that the boundary layer initially accelerated before reaching a maximum edge velocity and then slowed down slightly. The stations and MD values are listed in section B. A transition strip of No 60 carborundum grit 3.2 mm wide was placed at $X = 12.7$ mm, where $X = 0$ at the model nose. At two stations, $X = 0.1778$ and $X = 0.6604$ m, static holes at 90° intervals round the model provided a check on axis-symmetry
- 6 Wall static pressure was measured by static tappings ($d = 0.9$ mm) along a single generator of the model, except for the two stations mentioned above. A circular Preston tube ($d_1 = 0.71$, $d_2 = 0.41$, $l = 15$ mm) was used to determine wall shear stress, and also to obtain a free stream Pitot value. Pitot profiles were obtained with a FPP for which $h_1 = 0.28$, $h_2 = 0.13$, $b_1 = 1.6 [E]$, $l = 15$ mm. The static pressure was assumed constant through the boundary layer and no profile corrections were applied. Viscosity was determined from Sutherlands' law.
- 12 The editors present all the profiles measured by the author, replacing the isoenergetic assumption by the Crocco / Van Driest correlation, assuming that the model was adiabatic. The CF values are those reduced by the author, using the Hopkins and Keener (CAT 6601) calibration. He also presents values reduced using the Fenter & Stalmach (1957) Preston tube calibration, and the Baronti & Libby (1966) velocity profile correlation. The boundary layer edge has been set at the point with the highest velocity, as reported by the author. The POD value is calculated from the reported unit RE value. The author also reports additional Preston tube CF data for $M = 2.5$, 4 and 4.5, but without associated profile measurements.
- 13 profiles form a single set at seven successive stations, presented with Preston tube CF values at the same positions.
- 14
- 5 DATA 7005 0101-0107. Pitot profiles. NX = 7. Preston tube CF values obtained separately.
- 15 Editors' comments

These profiles are included as providing a test case in which the edge Mach number varies systematically. The pressure gradient is not very severe, so that the effects of acceleration should not be expected to be very marked. However, there is very little comparable data and the only similar test case is the experiment with a waisted body made by Winter et al. - CAT 7004. In that experiment the pressure gradients are stronger and more varied, but profiles were measured at relatively wide intervals.

The effects of normal pressure gradients here should be small - the simple wave element would give rise to

about 1% change in static pressure across the boundary layer. That there is a detectable effect is demonstrated by the experimentally observed velocity maximum used to specify the boundary layer edge.

There are not many data points for each profile, and it seems likely that the first one or two profiles are still influenced by the transition process. A further experiment of this type, with more detailed measurements, would be valuable.

CAT 7005		ALLEN		BOUNDARY CONDITIONS		EVALUATED DATA, SI UNITS.			
RUN	NO *	T ₁ /TR*	REDO ₂ W	CF *	H12	H12A	PV ¹	PD	
X *	POD	RU/PR*	RLN ₂ O	CO	H32	H32A	TW	TD	
RZ *	TUN*	SU *	D2	PI2*	H42	DPK	UD	TR	
70050101	2.8520	1.0000	6.4643 ⁺ 02	2.7180 ⁻ 03	4.8745	1.5611	5.7398 ⁺ 03	5.7398 ⁺ 03	
1.2700 ⁻ 01	1.6350 ⁺ 05	1.0000	1.4526 ⁺ 03		1.7901	1.7603	3.1728 ⁺ 02	1.3018 ⁺ 02	
2.4130 ⁻ 02	3.3900 ⁺ 02	1.0000	1.3339 ⁻ 04	NC	0.1152	2.0025 ⁻ 04	6.4786 ⁺ 02	3.1728 ⁺ 02	
70050102	2.9730	1.0000	1.1157 ⁺ 03	2.1960 ⁻ 03	4.9835	1.4423	4.8788 ⁺ 03	4.8788 ⁺ 03	
2.5400 ⁻ 01	1.7209 ⁺ 05	1.0000	2.4733 ⁺ 03	NM	1.8117	1.7829	3.1648 ⁺ 02	1.2248 ⁺ 02	
3.6300 ⁻ 02	3.3900 ⁺ 02	1.0000	2.3521 ⁻ 04	NC	0.1210	3.5265 ⁻ 04	6.5969 ⁺ 02	3.1648 ⁺ 02	
70050103	3.0380	1.0000	1.5245 ⁺ 03	1.0910 ⁻ 03	5.0607	1.4025	4.4449 ⁺ 03	4.4449 ⁺ 03	
3.8100 ⁻ 01	1.7283 ⁺ 05	1.0000	3.4937 ⁺ 03	NM	1.8130	1.7845	3.1613 ⁺ 02	1.1912 ⁺ 02	
4.3080 ⁻ 02	3.3900 ⁺ 02	1.0000	3.4019 ⁻ 04	NC	0.1232	5.1493 ⁻ 04	6.6480 ⁺ 02	3.1613 ⁺ 02	
70050104	3.0500	1.0000	1.9553 ⁺ 03	1.6820 ⁻ 03	5.0829	1.4023	4.2067 ⁺ 03	4.2067 ⁺ 03	
5.0800 ⁻ 01	1.6053 ⁺ 05	1.0000	4.5016 ⁺ 03	NM	1.8039	1.7724	3.1607 ⁺ 02	1.1851 ⁺ 02	
4.5670 ⁻ 02	3.3900 ⁺ 02	1.0000	4.5794 ⁻ 04	NC	0.1230	7.0373 ⁻ 04	6.6472 ⁺ 02	3.1607 ⁺ 02	
70050105	3.0720	1.0000	2.4024 ⁺ 03	1.5840 ⁻ 03	5.0810	1.3852	4.0117 ⁺ 03	4.0117 ⁺ 03	
6.3500 ⁻ 01	1.6410 ⁺ 05	1.0000	5.5784 ⁺ 03	NM	1.8025	1.7713	3.1595 ⁺ 02	1.1741 ⁺ 02	
4.4500 ⁻ 02	3.3900 ⁺ 02	1.0000	5.8290 ⁻ 04	NC	0.1239	8.9914 ⁻ 04	6.6738 ⁺ 02	3.1595 ⁺ 02	
70050106	3.0710	1.0000	3.0435 ⁺ 03	1.4390 ⁻ 03	5.0059	1.3703	3.9147 ⁺ 03	3.9147 ⁺ 03	
7.6200 ⁻ 01	1.5990 ⁺ 05	1.0000	7.0641 ⁺ 03	NM	1.7988	1.7662	3.1596 ⁺ 02	1.1746 ⁺ 02	
4.0030 ⁻ 02	3.3900 ⁺ 02	1.0000	7.5714 ⁻ 04	NC	0.1242	1.1653 ⁻ 03	6.6731 ⁺ 02	3.1596 ⁺ 02	
70050107	2.9350	1.0000	4.0896 ⁺ 03	1.3100 ⁻ 03	4.6507	1.3726	4.3956 ⁺ 03	4.3956 ⁺ 03	
8.8900 ⁻ 01	1.4642 ⁺ 05	1.0000	4.0059 ⁺ 03	NM	1.7819	1.7484	3.1609 ⁺ 02	1.2450 ⁺ 02	
3.4010 ⁻ 02	3.3900 ⁺ 02	1.0000	9.7783 ⁻ 04	NC	0.1201	1.4806 ⁻ 03	6.5661 ⁺ 02	3.1609 ⁺ 02	

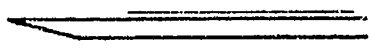
PD,POD CALCULATED FROM RE (AUTHOR) = CF (HOPKINS/KEENER)

70050103		ALLEN		PROFILE TABULATION		12 POINTS, DELTA AT POINT 11			
I	Y	PY2/P	P/PO	TU/TUD	H/HO	U/UD	T/TC	RHO/RHO000/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.93254	0.00000	0.00000	2.65392	0.90900	
2	1.2700 ⁻ 04	1.8050 ⁺ 00	NM	0.94890	0.32807	0.49240	2.25289	0.21457	
3	5.0800 ⁻ 04	3.5044 ⁺ 00	NM	0.96460	0.50503	0.64997	1.96655	0.31985	
4	8.8900 ⁻ 04	4.7472 ⁺ 00	NM	0.97277	0.59804	0.77227	1.66750	0.46312	
5	1.2700 ⁻ 03	5.5202 ⁺ 00	NM	0.97711	0.65054	0.81241	1.56117	0.52006	
6	2.1590 ⁻ 03	7.1583 ⁺ 00	NM	0.98467	0.74947	0.87903	1.37579	0.63397	
7	3.4290 ⁻ 03	9.7195 ⁺ 00	NM	0.98344	0.81194	0.94317	1.16072	0.81060	
8	4.6970 ⁻ 03	1.1087 ⁺ 01	NM	0.98852	0.87149	0.98897	1.03624	0.95433	
9	5.9670 ⁻ 03	1.2143 ⁺ 01	NM	0.99950	0.90097	0.99057	1.01133	0.98541	
10	7.2390 ⁻ 03	1.2295 ⁺ 01	NM	0.99987	0.99745	0.99903	1.00314	0.99586	
11	8.5070 ⁻ 03	1.2356 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
12	9.7790 ⁻ 03	1.2249 ⁺ 01	NM	0.99977	0.99547	0.99028	1.00567	0.99266	

INPUT VARIABLES Y,U/UD (ISOTHERMATIC) ASSUME P=PD AND VAN DRIEST

70050106		ALLEN		PROFILE TABULATION		13 POINTS, DELTA AT POINT 13			
I	Y	PY2/P	P/PO	TU/TUD	H/HO	U/UD	T/TC	RHO/RHO000/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.93283	0.00000	0.00000	2.69084	0.90000	
2	1.2700 ⁻ 04	1.4659 ⁺ 00	NM	0.94210	0.24743	0.38632	2.43781	0.15847	
3	7.6200 ⁻ 04	3.1703 ⁺ 00	NM	0.96117	0.46648	0.65171	1.96562	0.33308	
4	1.3970 ⁻ 03	3.9768 ⁺ 00	NM	0.96727	0.53461	0.72002	1.81388	0.39695	
5	2.0320 ⁻ 03	4.4747 ⁺ 00	NM	0.97114	0.57936	0.75902	1.71636	0.44222	
6	2.0670 ⁻ 03	5.1881 ⁺ 00	NM	0.97477	0.62179	0.79311	1.62697	0.48748	
7	3.3020 ⁻ 03	5.8481 ⁺ 00	NM	0.97821	0.66383	0.82427	1.54179	0.53462	
8	3.7370 ⁻ 03	6.4334 ⁺ 00	NM	0.98103	0.69985	0.84903	1.47177	0.57687	
9	6.4770 ⁻ 03	8.9688 ⁺ 00	NM	0.99063	0.83021	0.92852	1.23298	0.75107	
10	9.0170 ⁻ 03	1.1243 ⁺ 01	NM	0.98749	0.84132	0.98105	1.06346	0.92250	
11	1.1537 ⁻ 02	1.2463 ⁺ 01	NM	0.99968	0.99369	0.99764	1.00797	0.99975	
12	1.4077 ⁻ 02	1.2583 ⁺ 01	NM	0.99987	0.99741	0.99903	1.00326	0.99579	
13	1.6637 ⁻ 02	1.2615 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD (ISOTHERMATIC) ASSUME P=PD AND VAN DRIEST

	M : 4 P THETA X 10 ⁻³ : 2 - 25 TW/TR : 1	7006
		ZPG - AW
Continuous tunnel with fixed symmetrical nozzle. W = 0.91, H = 1.22 m. 0.084 < P0 < 0.68 MK/MP. T0: 313 K. Air, Dew-point 243 K. 3.7 < RE/m x 10 ⁻⁶ < 29.		
HASTINGS P.C. and SAWYER W.G. 1970. Turbulent boundary layers on a large flat plate at M = 4. RAE TR 70040. (Also ARC R & M 3678). Also Mabey et al. CAT 7402.		

- 1 The test boundary layer was formed on a mild-steel plate 1.65 m long and 0.89 m wide. A clearance of 12.7 mm was allowed on each side between the plate and the tunnel wall. The plate leading edge was chamfered at 10° to a thickness of 0.25 mm, and ground smooth on the test surface to within 0.64 μm. Twenty two instrument ports were placed in alternate staggered rows of three and two in the central 127 mm of the plate. The port diameter was 41.3 mm and the plugs were ground flush with the plate surface to within 13 μm. The plate was not actively cooled. Surface temperature varied along the plate but was within +2, -3 % of the adiabatic value for a recovery factor of 0.89. The Mach number along the surface varied by about 1 %. Transition was observed by sublimation of a surface coating of azobenzene. Transition was complete by approximately X = 0.2 m at the highest unit Reynolds numbers and by about X = 0.6 m for the lowest. The profiles presented are in all cases from stations downstream of transition as indicated not only by the sublimation technique but also by surface Pitot measurements. The sublimation patterns also indicated some flow convergence, which was confirmed by an imbalance in the two dimensional momentum integral equation of up to 25 %.
- 2 Two configurations of pressure tapped plugs were used. In one, static holes (d = 1 mm) were drilled 12.7 mm upstream and downstream of the plug centre while in the other, used in conjunction with surface Pitot shear stress sensors, a row of three tapings was drilled 6.35 mm downstream of the centre on the cantreline and 10.16 mm to either side. Sections of razor blade were ground down and mounted over two of the static holes on each of two similar plugs. The blades were about 6.35 mm square with the sharp edge mounted over the front of the static hole. It was found that only the blades with the larger value of h (0.566 and 0.323 mm) on each plug gave reliable readings. The smaller blades (h = 0.152 and 0.157 mm) were thought to suffer from interference from the larger ones. The calibration function used was that presented in figure 18 of Hopkins and Keener 1966 (CAT 6601). A floating element balance was also mounted in a plug. The element was circular (d = 7.925 mm) with a mean gap of 0.127 mm.
- 3 Profile measurements were made with two combined Pitot / temperature probe assemblies. These consisted of small (d₁ = 0.36 mm) CPP which after an approximately 10 mm length nearly parallel to the flow was bent up nearly normal to the test surface before entering a larger diameter crook-shaped holding tube. This looped round to re-enter the plug to which the traverse gear was attached. The profile normal lay 12.7 mm ahead of the centre of the plug. A thermocouple bead was mounted inside the holding tube near the end of the narrow-bore Pitot. The probe could be connected either to a pressure sensor for Pitot measurements or to a vacuum pump which ensured that the inflow was choked, when the thermocouple was used as a T0 sensor.
- 4 For one of the assemblies (No 1) d₂ was 0.28 mm whilst for no 2 it was 0.13 mm. A thermocouple used for measuring wall temperature was fitted to the same plug.
- 5 The arrangement of the ports was such that there were five longitudinal rows, one on the centre line and two on each side at distances of 31.75 and 63.5 mm. In each row the distance between successive ports was 254 mm. The FEB was used only at stations on the centre line for which X = 0.622, 0.876 and 1.120 m. Pitot traverses were made in the rows 63.5 mm to either side, no 1 being used for traverses on normals at X = 0.859, 0.813 and 1.067 m, and no 2 for traverses at X = 0.406, 0.660, 0.914 and 1.168 m. Razor blade shear stress determinations were made on the centre line and 31.75 mm to one side, as were the associated

static measurements. The X-values are to be found in section D.

- 9 The authors have interpolated static pressure values to the profile stations. By a leap-frog deployment of the two razor-blade sensors it was possible to extend the calibration function to lower readings, and the low-dynamic-head skin friction results were obtained in this manner. The R-THETA values presented with the shear stress data are those interpolated by the authors from their own integral value calculations.
- 10
- 11 No profile corrections were employed and Sutherland's viscosity law was used.
- 12 The editors have presented all the data available to them using the authors' tabulated values for the measured temperature distribution (values determined from the Crocco / Van Driest temperature relation for recovery factors of 1 and 0.89 were also given). The boundary layer edge reservoir state has been arbitrarily set at the nominal tunnel reservoir conditions given by the authors. The CF values given with the profiles have been interpolated by the editors from the data given in section D. The authors' R THETA values were used throughout. The relationship between CF and R THETA was fitted in two separate ranges, with a discontinuity in the value of CF at R THETA = 6800 (see fig. 10 of the source paper). The skin friction data is also presented in its original form in section D. Balance readings are only available for the higher unit Reynolds numbers.
- 13
- 14
- 6 DATA: 7006 0101-0407. NX up to 7. Pitot and T0 profiles measured with the same probe. CF measured at different stations with FEB and Stanton tubes.

16 Editors' comments

The data cover a 10 : 1 Reynolds number range, starting with boundary layers which are still strongly influenced by the transition process. Low Reynolds number effects are evident both in the profiles and in the anomalous CF behaviour which we have attempted to describe by using a two-branch data fit for interpolation. Comparable but fully turbulent data is presented by Coles - CAT 5301, and the development of the transition process is fully described by Watson et al. - CAT 7305, though at high Mach numbers.

Mabay et al. used a modification of the same plate to extend the experiment, covering a higher Reynolds number range for Mach numbers from 2.5 to 4.5 - CAT 7402. They observed disturbances caused by the gaps at the sides of the plate which are not remarked here.

The profiles are described in close detail, and measurements extend to within the momentum deficit peak.

CAT 7000		HAUSTINGS		BOUNDARY CONDITIONS AND EVALUATED DATA, ST UNITS.					
RUN	MD *	TU/TP	PL02W	CF *	H12	H12K	PW	PD	
X *	P0D*	PH/PDA	PL02D	CO	H52	H52K	TH*	TD	
RZ	T0D*	SH	02	P12*	H42	0PA	UD	TR	
70060101	3.9130	1.0026	6.9708 ⁺ +02	NM	7.0514	1.3384	6.2657 ⁺ +02	6.2657 ⁺ +02	
8.1280 ⁺ +01	8.4660 ⁺ +04	1.0000	2.2714 ⁺ +03	NM	1.8541	1.8107	2.8921 ⁺ +02	7.7050 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	6.4340 ⁺ +04	0.0000 ⁺ +00	0.2150	1.0803 ⁺ +03	6.8866 ⁺ +02	2.8846 ⁺ +02	
70060102	3.9160	1.0070	8.3739 ⁺ +02	1.6500 ⁺ +03	7.3623	1.3052	6.2404 ⁺ +02	6.2404 ⁺ +02	
9.1440 ⁺ +01	8.4660 ⁺ +04	1.0000	2.7415 ⁺ +03	NM	1.8443	1.8117	2.4046 ⁺ +02	7.6961 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	7.7760 ⁺ +04	0.0000 ⁺ +00	0.1420	1.3601 ⁺ +03	6.8879 ⁺ +02	2.8845 ⁺ +02	
70060103	3.8930	1.0002	9.7986 ⁺ +02	1.5200 ⁺ +03	7.4449	1.3439	6.4372 ⁺ +02	6.4372 ⁺ +02	
1.0660 ⁺ +00	8.4660 ⁺ +04	1.0000	3.1349 ⁺ +03	NM	1.8435	1.8059	2.8859 ⁺ +02	7.7646 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	8.7864 ⁺ +04	0.0000 ⁺ +00	0.1219	1.5356 ⁺ +03	6.8779 ⁺ +02	2.8852 ⁺ +02	
70060104	3.8990	0.9949	1.0801 ⁺ +03	1.4300 ⁺ +03	7.2253	1.3105	6.3852 ⁺ +02	6.3852 ⁺ +02	
1.1684 ⁺ +00	8.4660 ⁺ +04	1.0000	3.4809 ⁺ +03	NM	1.8340	1.8031	2.8702 ⁺ +02	7.7467 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	9.7866 ⁺ +04	0.0000 ⁺ +00	0.1674	1.7304 ⁺ +03	6.8805 ⁺ +02	2.8850 ⁺ +02	
70060201	3.9420	1.0000	7.5096 ⁺ +02	NM	7.3744	1.3341	1.2052 ⁺ +03	1.2052 ⁺ +03	
5.3880 ⁺ +01	1.6932 ⁺ +05	1.0000	2.8691 ⁺ +03	NM	1.8531	1.8214	2.8837 ⁺ +02	7.6195 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	3.5492 ⁺ +04	0.0000 ⁺ +00	0.1625	0.0837 ⁺ +00	6.8991 ⁺ +02	2.8837 ⁺ +02	
70060202	3.9430	0.9997	8.7508 ⁺ +02	1.4500 ⁺ +03	7.4036	1.3649	1.2035 ⁺ +03	1.2035 ⁺ +03	
6.6040 ⁺ +01	1.6932 ⁺ +05	1.0000	2.8776 ⁺ +03	NM	1.8397	1.8032	2.8827 ⁺ +02	7.6166 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	4.1384 ⁺ +04	0.0000 ⁺ +00	0.1627	7.1681 ⁺ +04	6.8995 ⁺ +02	2.8837 ⁺ +02	
70060203	3.9210	1.0016	1.3247 ⁺ +03	1.2700 ⁺ +03	7.3423	1.3343	1.2397 ⁺ +03	1.2397 ⁺ +03	
8.1280 ⁺ +01	1.6932 ⁺ +05	1.0000	4.3269 ⁺ +03	NM	1.8387	1.8057	2.8890 ⁺ +02	7.6813 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	6.1524 ⁺ +04	0.0000 ⁺ +00	0.1654	1.0893 ⁺ +03	6.8901 ⁺ +02	2.8844 ⁺ +02	
70060204	3.9370	1.0126	1.4082 ⁺ +03	1.2300 ⁺ +03	7.5581	1.3346	1.2133 ⁺ +03	1.2133 ⁺ +03	
9.1440 ⁺ +01	1.6932 ⁺ +05	1.0000	4.8524 ⁺ +03	NM	1.8320	1.8000	2.9203 ⁺ +02	7.6342 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	8.9569 ⁺ +04	0.0000 ⁺ +00	0.1346	1.2657 ⁺ +03	6.8908 ⁺ +02	2.8838 ⁺ +02	
70060205	3.9150	0.9972	1.8202 ⁺ +03	1.2050 ⁺ +03	7.3072	1.2986	1.2498 ⁺ +03	1.2498 ⁺ +03	
1.0660 ⁺ +00	1.6932 ⁺ +05	1.0000	5.9119 ⁺ +03	NM	1.8352	1.8073	2.8765 ⁺ +02	7.6490 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	8.3799 ⁺ +04	0.0000 ⁺ +00	0.1467	1.5085 ⁺ +03	6.8875 ⁺ +02	2.8845 ⁺ +02	
70060206	3.9150	0.9972	1.9784 ⁺ +03	1.4400 ⁺ +03	7.2280	1.3113	1.2498 ⁺ +03	1.2498 ⁺ +03	
1.1684 ⁺ +00	1.6932 ⁺ +05	1.0000	6.4259 ⁺ +03	NM	1.8313	1.8017	2.8765 ⁺ +02	7.6490 ⁺ +01	
INFINITE	3.1300 ⁺ +02	0.0000	9.1085 ⁺ +04	0.0000 ⁺ +00	0.1830	1.6379 ⁺ +03	6.8875 ⁺ +02	2.8845 ⁺ +02	

CAT 7006

HASTINGS

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X RZ	MD POD TOD	TW/TR PW/PD SW	RLD2W PLED2D DZ	CF CO PI2A	H12 H32 H42	H12K H32K H42K	PH TW UP	PD TD TR
70060301 4.0640*-01 INFINITE	3.9760 3.3864*+05 3.1300*+02	1.0000 1.0000 0.0000	9.9705*+02 3.3200*+03 2.4284*+04	1.4200*-03 NM 0.0000*+00	7.6307 1.8327 0.1691	1.3905 1.8020 4.4068*-04	2.3029*+03 2.8827*+02 6.9138*+02	2.3029*+03 7.5209*+01 2.8827*+02
70060302 5.5880*-01 INFINITE	3.9400 3.3864*+05 3.1300*+02	0.9975 1.0000 0.0000	1.6902*+03 5.5424*+03 3.9793*-04	1.2100*-03 NM 0.0000*+00	7.4084 1.8406 0.1595	1.3222 1.6139 7.0545*-04	2.4168*+03 2.8709*+02 6.8982*+02	2.4168*+03 7.6258*+01 2.8838*+02
70060303 6.6040*-01 INFINITE	3.9430 3.3864*+05 3.1300*+02	0.9964 1.0000 0.0000	1.9724*+03 7.4695*+03 4.6571*-04	1.3300*-03 NM 0.0000*+00	7.5262 1.8317 0.1477	1.3377 1.8031 8.4203*-04	2.4071*+03 2.8733*+02 6.8995*+02	2.4071*+03 7.6166*+01 2.8837*+02
70060304 8.1280*-01 INFINITE	3.9360 3.3864*+05 3.1300*+02	1.0115 1.0000 0.0000	2.5063*+03 8.4985*+03 6.8862*-04	1.2500*-03 NM 0.0000*+00	7.4426 1.8361 0.1560	1.3222 1.8018 1.1100*-03	2.4299*+03 2.9172*+02 6.8965*+02	2.4299*+03 7.6371*+01 2.8839*+02
70060305 9.1440*-01 INFINITE	3.9460 3.3864*+05 3.1300*+02	1.0117 1.0000 0.0000	2.7094*+03 9.2018*+03 6.6272*-04	1.2050*-03 NM 0.0000*+00	7.5803 1.8288 0.1583	1.3272 1.7991 1.2255*-03	2.3974*+03 2.9172*+02 6.9008*+02	2.3974*+03 7.6678*+01 2.8839*+02
70060306 1.0669*+00 INFINITE	3.9290 3.3864*+05 3.1300*+02	1.0114 1.0000 0.0000	3.3493*+03 1.1077*+04 7.8555*-04	1.1350*-03 NM 0.0000*+00	7.5188 1.8271 0.1526	1.3127 1.7997 1.4524*-03	2.4661*+03 2.9172*+02 6.8918*+02	2.4661*+03 7.6695*+01 2.8842*+02
70060307 1.1684*+00 INFINITE	3.9270 3.3864*+05 3.1300*+02	0.9854 1.0000 0.0000	3.8070*+03 1.2306*+04 8.7758*-04	1.1250*-03 NM 0.0000*+00	7.2142 1.8290 0.1939	1.3044 1.8018 1.5912*-03	2.4598*+03 2.8828*+02 6.8926*+02	2.4598*+03 7.6636*+01 2.8842*+02
70060401 4.0640*-01 INFINITE	3.9720 6.7728*+05 3.1300*+02	1.0032 1.0000 0.0000	2.6149*+03 8.7179*+03 3.1810*-04	1.2200*-03 NM 0.0000*+00	7.4571 1.8307 0.1892	1.3368 1.8032 5.7833*-04	4.6306*+03 2.8921*+02 6.9117*+02	4.6306*+03 7.5324*+01 2.8828*+02
70060402 5.5880*-01 INFINITE	3.9550 6.7728*+05 3.1300*+02	0.9868 1.0000 0.0000	3.8266*+03 1.1203*+04 4.0538*-04	1.1700*-03 NM 0.0000*+00	7.5141 1.8294 0.1599	1.3431 1.8016 7.3985*-04	4.7373*+03 2.8852*+02 6.9046*+02	4.7373*+03 7.5816*+01 2.8836*+02
70060403 6.6040*-01 INFINITE	3.9590 6.7728*+05 3.1300*+02	0.9944 1.0000 0.0000	3.8422*+03 1.2790*+04 4.6366*-04	1.0950*-03 NM 0.0000*+00	8.0347 1.8166 0.0481	1.3442 1.7933 8.7582*-04	4.7119*+03 2.8671*+02 6.9063*+02	4.7119*+03 7.5707*+01 2.8842*+02
70060404 8.1280*-01 INFINITE	3.9500 6.7728*+05 3.1300*+02	1.0106 1.0000 0.0000	4.8781*+03 1.6207*+04 5.8490*-04	1.0700*-03 NM 0.0000*+00	7.4694 1.8323 0.1569	1.3110 1.8043 1.0684*-03	4.7642*+03 2.9140*+02 6.9025*+02	4.7642*+03 7.5962*+01 2.8835*+02
70060405 9.1440*-01 INFINITE	3.9550 6.7728*+05 3.1300*+02	1.0085 1.0000 0.0000	5.3571*+03 1.7816*+04 6.4455*-04	1.0600*-03 NM 0.0000*+00	7.5580 1.8320 0.1383	1.3056 1.8066 1.1836*-03	4.7373*+03 2.9078*+02 6.9046*+02	4.7373*+03 7.5816*+01 2.8837*+02
70060406 1.0669*+00 INFINITE	3.9380 6.7728*+05 3.1300*+02	0.9790 1.0000 0.0000	6.7514*+03 2.1892*+04 7.8184*-04	1.0500*-03 NM 0.0000*+00	7.9627 1.8247 0.2316	1.3118 1.7999 1.4025*-03	4.8867*+03 2.8233*+02 6.8974*+02	4.8867*+03 7.6312*+01 2.8838*+02
70060407 1.1684*+00 INFINITE	3.9320 6.7728*+05 3.1300*+02	0.9637 1.0000 0.0000	7.4053*+03 2.3568*+04 8.4236*-04	1.0400*-03 NM 0.0000*+00	7.1283 1.8321 0.2067	1.2944 1.8078 1.5029*-03	4.8859*+03 2.7794*+02 6.8944*+02	4.8859*+03 7.6488*+01 2.8840*+02

70060401		HASTINGS		PROFILE TABULATION		34 POINTS, DELTA AT POINT 32			
I	Y	P12/P	P/PO	TQ/100	M/HO	U/UO	T/TD	RHO/RHO0+U/UD	
1	0.0000+00	1.0000+00	NM	0.92399	0.00000	0.00000	3.83952	0.00000	
2	1.7780-04	3.1140+00	NM	0.93499	0.35709	0.54424	2.76932	0.21458	
3	2.2860-04	3.4197+00	NM	0.93768	0.37887	0.61954	2.68578	0.23072	
4	2.7940-04	3.7362+00	NM	0.94052	0.39853	0.68304	2.60349	0.24699	
5	3.3020-04	3.9912+00	NM	0.94242	0.41421	0.66023	2.54065	0.25987	
6	3.8100-04	4.2373+00	NM	0.94498	0.42878	0.67593	2.48574	0.27200	
7	4.3180-04	4.4652+00	NM	0.94664	0.44182	0.68933	2.43427	0.28318	
8	4.8260-04	4.6900+00	NM	0.94806	0.46510	0.71243	2.34632	0.30364	
9	5.3340-04	5.2130+00	NM	0.95248	0.48203	0.72843	2.28463	0.31878	
10	5.8420-04	5.4047+00	NM	0.95445	0.49680	0.74183	2.27965	0.33271	
11	6.3500-04	5.7803+00	NM	0.95603	0.51035	0.75362	2.18055	0.34561	
12	1.0668-03	6.0913+00	NM	0.96174	0.52522	0.76832	2.13945	0.35904	
13	1.1938-03	6.4036+00	NM	0.96820	0.53973	0.77822	2.07970	0.37432	
14	1.4478-03	7.0683+00	NM	0.96379	0.56536	0.80112	1.97981	0.40465	
15	1.8288-03	8.4400+00	NM	0.96981	0.62802	0.84032	1.86018	0.46638	
16	2.4638-03	9.9375+00	NM	0.97609	0.68240	0.87461	1.64231	0.53255	
17	2.7178-03	1.0767+01	NM	0.97884	0.71180	0.89051	1.58514	0.56095	
18	2.9718-03	1.1579+01	NM	0.98116	0.73921	0.90441	1.49611	0.60451	
19	3.4798-03	1.3163+01	NM	0.98556	0.79043	0.92790	1.37170	0.67328	
20	3.9878-03	1.4827+01	NM	0.98908	0.84060	0.94831	1.27213	0.74527	
21	4.6228-03	1.7002+01	NM	0.99371	0.90215	0.97050	1.14727	0.83661	
22	5.2578-03	1.8873+01	NM	0.99686	0.95188	0.98620	1.07142	0.94875	
23	5.8928-03	2.0010+01	NM	0.99863	0.98883	0.99460	1.02828	0.96725	
24	6.5278-03	2.0415+01	NM	0.99940	0.99995	0.99750	1.01327	0.98443	
25	7.1628-03	2.0598+01	NM	0.99978	0.99950	0.99800	1.00664	0.99221	
26	7.7978-03	2.0643+01	NM	0.99988	0.99960	0.99910	1.00503	0.99410	
27	8.4328-03	2.0694+01	NM	1.00004	0.99975	0.99950	1.00351	0.99620	
28	9.0678-03	2.0734+01	NM	0.99995	0.99985	0.99970	1.00170	0.99800	
29	9.7028-03	2.0770+01	NM	1.00005	0.99965	0.99970	1.00210	0.99760	
30	1.0138-02	2.0690+01	NM	0.99999	0.99975	0.99990	1.00210	0.99690	
31	1.1608-02	2.0740+01	NM	0.99999	0.99920	0.99980	1.00120	0.99880	
D 32	1.2878-02	2.0781+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
33	1.5418-02	2.0760+01	NM	0.99924	0.99990	0.99990	1.00000	0.99990	
34	1.7958-02	2.0765+01	NM	0.99939	0.99960	0.99960	1.00000	0.99960	

INPUT VARIABLES Y,U/UD,M/HO/RHO0
AT I=19 DATA WERE AVERAGED ASSUME P=PO

70060403		HASTINGS		PROFILE TABULATION		37 POINTS, DELTA AT POINT 37			
I	Y	P12/P	P/PO	TQ/100	M/HO	U/UO	T/TD	RHO/RHO0+U/UD	
1	0.0000+00	1.0000+00	NM	0.92352	0.00000	0.00000	3.81850	0.00000	
2	1.7780-04	2.7461+00	NM	0.93289	0.33091	0.56075	2.87195	0.19578	
3	2.2860-04	3.0477+00	NM	0.93561	0.35710	0.59366	2.76371	0.21451	
4	2.7940-04	3.3440+00	NM	0.93781	0.37454	0.61453	2.69212	0.22827	
5	3.3020-04	3.5394+00	NM	0.93888	0.38721	0.62898	2.63888	0.23836	
6	3.8100-04	3.7421+00	NM	0.93982	0.39997	0.64302	2.59478	0.24674	
7	4.3180-04	3.9047+00	NM	0.94236	0.41030	0.65526	2.55047	0.25692	
8	4.8260-04	4.2345+00	NM	0.94617	0.43003	0.67073	2.47654	0.27326	
9	5.3340-04	4.5001+00	NM	0.94833	0.44524	0.68238	2.41833	0.28631	
10	5.8420-04	4.7281+00	NM	0.95104	0.45789	0.70533	2.37274	0.29726	
11	6.3500-04	4.9697+00	NM	0.95279	0.47089	0.71787	2.32411	0.30886	
12	1.0668-03	5.1780+00	NM	0.95504	0.48180	0.72870	2.28505	0.31869	
13	1.1938-03	5.4974+00	NM	0.95688	0.49303	0.73884	2.24568	0.32900	
14	1.4478-03	6.0773+00	NM	0.95942	0.51334	0.75670	2.17284	0.34625	
15	1.9558-03	6.8170+00	NM	0.96297	0.53100	0.78700	2.04000	0.38577	
16	2.4638-03	7.8070+00	NM	0.96717	0.58578	0.81300	1.92662	0.42203	
17	2.9718-03	9.2002+00	NM	0.97121	0.62903	0.83720	1.81871	0.46084	
18	3.4798-03	9.1670+00	NM	0.97598	0.65003	0.85984	1.71784	0.50053	
19	3.9878-03	1.0040+01	NM	0.97982	0.68864	0.87900	1.62920	0.53950	
20	4.6228-03	1.1240+01	NM	0.98627	0.73061	0.90228	1.52596	0.59124	
21	5.2578-03	1.2000+01	NM	0.99105	0.77539	0.92415	1.42040	0.65056	
22	5.8928-03	1.3312+01	NM	0.99492	0.81701	0.94231	1.33025	0.70837	
23	6.5278-03	1.5341+01	NM	0.99861	0.85882	0.95876	1.24740	0.76897	
24	7.1628-03	1.6726+01	NM	0.99996	0.89792	0.97281	1.17287	0.82674	
25	7.7978-03	1.8057+01	NM	1.00144	0.93350	0.98335	1.10990	0.88630	
26	8.4328-03	1.9142+01	NM	1.00380	0.96190	0.99187	1.06317	0.93294	
27	9.0678-03	1.9883+01	NM	1.00399	0.97983	0.99699	1.03533	0.96297	
28	9.7028-03	2.0266+01	NM	1.00485	0.99043	1.00010	1.01941	0.98105	
29	1.0338-02	2.0440+01	NM	1.00615	0.99443	1.00181	1.01408	0.98789	
30	1.0973-02	2.0331+01	NM	1.00600	0.99717	1.00231	1.01032	0.99207	
31	1.1608-02	2.0350+01	NM	1.00621	0.99757	1.00251	1.00992	0.99265	
32	1.2243-02	2.0372+01	NM	1.00493	0.99812	1.00201	1.00780	0.99426	
33	1.2878-02	2.0603+01	NM	1.00346	0.99887	1.00171	1.00569	0.99684	
34	1.3513-02	2.0660+01	NM	1.00316	0.99967	1.00130	1.00488	0.99684	
35	1.4148-02	2.0574+01	NM	1.00290	0.99817	1.00100	1.00564	0.99534	
36	1.6688-02	2.0635+01	NM	1.00438	0.99967	1.00211	1.00498	0.99724	
D 37	1.9228-02	2.0600+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/HO/RHO0
AT I=13,P1 DATA WERE AVERAGED ASSUME P=PO

70060405		HASTINGS		PROFILE TABULATION		30 POINTS, DELTA AT POINT 31			
I	Y	P12/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHO0	U/UD
1	0.0000+00	1.0000+00	NM	0.93640	0.00000	0.00000	3.84108	0.00000	
2	1.7780+04	2.6072+00	NM	0.94714	0.32061	0.59924	2.93174	0.19075	
3	2.2860+04	2.9117+00	NM	0.94870	0.34088	0.59145	2.85098	0.20338	
4	2.7940+04	3.1772+00	NM	0.95099	0.36310	0.60536	2.77963	0.21779	
5	3.3020+04	3.3705+00	NM	0.95241	0.37040	0.62127	2.72443	0.22604	
6	3.8100+04	3.5404+00	NM	0.95359	0.38767	0.63438	2.67781	0.23690	
7	4.3180+04	3.6757+00	NM	0.95446	0.39640	0.64429	2.64178	0.24388	
8	4.8260+04	3.9830+00	NM	0.95673	0.41550	0.66540	2.56466	0.25945	
9	5.3340+04	4.2212+00	NM	0.95820	0.42968	0.68041	2.50751	0.27135	
10	5.8420+04	4.4237+00	NM	0.95974	0.44136	0.69252	2.46190	0.28129	
11	6.3500+04	4.6175+00	NM	0.96041	0.45224	0.70322	2.41791	0.29084	
12	6.8580+04	4.7903+00	NM	0.96205	0.46196	0.71293	2.38189	0.29934	
13	7.3660+04	4.9761+00	NM	0.96288	0.47169	0.72213	2.34374	0.30811	
14	7.8740+04	5.1300+00	NM	0.96506	0.48912	0.73834	2.27873	0.32404	
15	8.3820+04	5.2970+00	NM	0.96859	0.52304	0.76770	2.15464	0.34632	
16	8.8900+04	5.4053+00	NM	0.97108	0.55125	0.79027	2.05570	0.36492	
17	9.3980+04	5.7065+00	NM	0.97415	0.57779	0.81039	1.96720	0.41195	
18	9.9060+04	5.9320+00	NM	0.97613	0.60416	0.82870	1.88146	0.44045	
19	1.0478+05	6.4471+00	NM	0.97795	0.62899	0.84471	1.80353	0.46636	
20	1.0922+05	6.2044+00	NM	0.98051	0.65827	0.86292	1.71843	0.50216	
21	1.1378+05	6.0043+00	NM	0.98288	0.68439	0.88053	1.63137	0.53975	
22	1.1834+05	6.0983+00	NM	0.98530	0.72234	0.89794	1.54524	0.58108	
23	1.2290+05	6.1827+00	NM	0.98890	0.75081	0.91165	1.47471	0.61835	
24	1.2746+05	6.3826+00	NM	0.99111	0.81430	0.92981	1.33090	0.70585	
25	1.3202+05	6.5794+00	NM	0.99348	0.87229	0.94108	1.21394	0.74197	
26	1.3658+05	6.7854+00	NM	0.99702	0.92911	0.97989	1.11226	0.80070	
27	1.4114+05	6.9508+00	NM	0.99862	0.97232	0.99240	1.04171	0.85266	
28	1.4570+05	7.0303+00	NM	1.00029	0.99245	0.99830	1.01182	0.89664	
29	1.5026+05	7.0537+00	NM	1.00025	0.99025	0.99970	1.00290	0.90091	
30	1.5482+05	7.0603+00	NM	1.00025	0.99040	1.00010	1.00000	0.90070	
31	1.5938+05	7.0607+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
32	1.6394+05	7.0595+00	NM	0.99995	0.99970	0.99990	1.00000	0.99990	
33	1.6850+05	7.0591+00	NM	1.00019	0.99960	1.00000	1.00000	0.99920	
34	1.7306+05	7.0583+00	NM	1.00029	0.99940	1.00000	1.00120	0.99880	
35	1.7762+05	7.0573+00	NM	0.99999	0.99920	0.99980	1.00120	0.99840	
36	1.8218+05	7.0565+00	NM	1.00055	0.99845	0.99990	1.00240	0.99700	
37	1.8674+05	7.0551+00	NM	1.00028	0.99860	0.99980	1.00240	0.99740	
38	1.9130+05	7.0547+00	NM	1.00000	0.99900	0.99990	1.00160	0.99620	

INPUT VARIABLES Y,U/UD,RHO/MD ASSUME P=PD
AT I=24 DATA WERE AVERAGED

70060401		HASTINGS		PROFILE TABULATION		32 POINTS, DELTA AT POINT 32			
I	Y	P12/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHO0	U/UD
1	0.0000+00	1.0000+00	NM	0.88337	0.00000	0.00000	3.61486	0.00000	
2	1.7780+04	2.6316+00	NM	0.92247	0.32405	0.54702	2.84461	0.19196	
3	2.2860+04	2.7506+00	NM	0.92399	0.33353	0.55944	2.81335	0.19885	
4	2.7940+04	2.9186+00	NM	0.92677	0.35050	0.58117	2.74807	0.21146	
5	3.3020+04	3.1698+00	NM	0.92858	0.36441	0.59810	2.69374	0.22203	
6	3.8100+04	3.3494+00	NM	0.93088	0.37712	0.61382	2.64574	0.23195	
7	4.3180+04	3.5065+00	NM	0.93242	0.38770	0.62574	2.60487	0.24022	
8	4.8260+04	3.6236+00	NM	0.93368	0.40004	0.64077	2.57244	0.24669	
9	5.3340+04	3.8500+00	NM	0.93818	0.42250	0.66460	2.47340	0.26870	
10	5.8420+04	4.2693+00	NM	0.93997	0.43471	0.67742	2.42753	0.27906	
11	6.3500+04	4.4373+00	NM	0.94153	0.44472	0.68763	2.39077	0.28762	
12	6.8580+04	4.6183+00	NM	0.94272	0.45493	0.69775	2.35244	0.29617	
13	7.3660+04	4.7720+00	NM	0.94413	0.46386	0.70016	2.32154	0.30412	
14	7.8740+04	4.9091+00	NM	0.94604	0.47439	0.72148	2.24303	0.31853	
15	8.3820+04	5.0592+00	NM	0.95116	0.50996	0.74872	2.15885	0.34682	
16	8.8900+04	5.1354+00	NM	0.95457	0.53266	0.76835	2.08074	0.36427	
17	9.3980+04	5.2636+00	NM	0.95802	0.55713	0.78798	2.00800	0.38393	
18	9.9060+04	5.4077+00	NM	0.96056	0.57553	0.80200	1.94183	0.41301	
19	1.0478+05	5.5951+00	NM	0.96283	0.59652	0.81703	1.87392	0.43353	
20	1.0922+05	5.6700+00	NM	0.96609	0.62142	0.83415	1.80185	0.46294	
21	1.1378+05	5.7604+00	NM	0.96888	0.64502	0.84937	1.73401	0.48893	
22	1.1834+05	5.8161+00	NM	0.97165	0.67012	0.86460	1.66466	0.51938	
23	1.2290+05	6.0046+00	NM	0.97414	0.69418	0.87032	1.60090	0.54864	
24	1.2746+05	6.1446+00	NM	0.97990	0.74243	0.90380	1.48212	0.60984	
25	1.3202+05	6.3083+00	NM	0.98355	0.78963	0.92579	1.37460	0.67350	
26	1.3658+05	6.4297+00	NM	0.98778	0.83339	0.94842	1.28414	0.73342	
27	1.4114+05	6.5935+00	NM	0.99172	0.88142	0.96264	1.19281	0.80704	
28	1.4570+05	6.7809+00	NM	0.99492	0.92521	0.97757	1.11637	0.87568	
29	1.5026+05	6.8647+00	NM	0.99715	0.96040	0.98898	1.05852	0.93393	
30	1.5482+05	6.9724+00	NM	0.99851	0.98367	0.99514	1.02136	0.97228	
31	1.5938+05	7.0167+00	NM	0.99936	0.99478	0.99840	1.00724	0.99117	
32	1.6394+05	7.0374+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

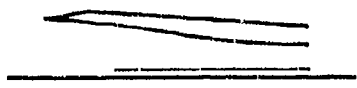
INPUT VARIABLES Y,U/UD,RHO/MD ASSUME P=PD
AT I=26,29 DATA WERE AVERAGED

SECTION D: ADDITIONAL DATA

NB. FACSIMILE FROM SOURCE PAPER. AUTHORS SYMBOLS AND UNITS

Local Skin-Friction Coefficients.

X in from l.e.	P_0 in Hg	C_f		Interpolation from Table 3	
		Floating element	Surface pitot $h = 0.0223$	$R\delta_2$	M_s
54.75 48.75 44.75 44.5 38.75 34.75 34.5 28.75 24.75 24.5 18.75 14.75	200	0.00103 0.00108 0.00115	0.00100 0.00106 0.00106 0.00105 0.00112	24035 23820 18695 18590 16180 14125 13945	3.934 3.934 3.953 3.953 3.955 3.958 3.957
54.75 48.75 44.75 44.5 38.75 34.75 34.5 28.75 24.75 24.5 18.75 14.75	100	0.00114 0.00124 0.00137	0.00115 0.00116 0.00120 0.00123 0.00139	12455 12360 9480 9420 8125 7035 6930	3.926 3.926 3.942 3.942 3.940 3.942 3.942
54.75 48.75 44.75 38.75 34.75 28.75 24.75	50		0.00123 0.00120 0.00124 0.00132 0.00152	6504 5065 3910 3115	3.915 3.932 3.933 3.943
54.75 48.75 44.75 38.75	25		0.00174 0.00145	3455	3.897

	M : 4 falling to 2.95 R THETA X 10 ⁻³ : 35 - 70 TW/TR : 1	7007
		ZPG - APG - ZPG AW
Continuous tunnel, fixed nozzle. W = H = 0.127 m. PO: 1.5 MN/m ² . TO: 295 K. Air, absolute humidity 2 x 10 ⁻⁴ . RE/m : 6.5 x 10 ⁷ at M = 4.		
ZWARTS F.J. 1970 The compressible turbulent boundary layer in a pressure gradient. PhD Thesis McGill University, Montreal. And Zwarts F.J., Private communications.		

- 1 The test boundary layer was formed on the floor of the 0.127 m square wind tunnel. The test section started
- 4 about 0.75 m downstream of the nozzle throat so that the starting boundary layer thickness was about 10 mm. A contoured splitter plate was designed by the method of characteristics to give a Mach number distribution on the tunnel floor such that the initial flow at M = 4 passed through a constant Mach number gradient falling to M = 3 over a distance of 0.15 m, followed by a second region of constant Mach number flow. The
- 3 test surface roughness was less than 0.9 μm , and it was not actively cooled. No boundary layer trip was used as it was presumed that the prevailing high Reynolds number levels would ensure fully turbulent flow a short distance downstream of the nozzle throat. Surface flow visualisation tests showed that there was
- 5 considerable flow convergence in the APG region as well as divergence in the ZPG regions. This was attributed to inflow/outflow from the tunnel sidewall driven by the significant pressure differences normal to the test surface. Pitot traverses and Preston tube measurements were made at stations 38.1 mm to either side of the centre line, at streamwise intervals of 50.8 mm. CF differed from the centre line value by up to 10 %. Differences in integral thicknesses were up to 5 %.
- 6 The test wall was provided with 48 static holes of 1.04 mm diameter. "Goose-necked" Pitot tubes could be
- 7 inserted into the static holes and were also used as Preston tubes. The Pitot probes were CPP for which d_s was either 0.419 or 0.813 mm. The tubes emerged from the wall normally and then curved over in a series of approximate circular arcs to finish parallel to the surface. The overall upstream extension was 6.35 mm for the smaller tube and 12.7 mm for the larger. The end faces were ground square to the test surface. The profile traverses were taken with the small tube, the larger one being used to supply supplementary Preston
- 8 tube data. On the centre line the static holes extended at 12.7 mm intervals from the first (X = 0) to X = 228.6 mm. There were then holes at X = 254 and 279.4 mm followed by holes at 50.8 mm intervals until X = 431.8 mm. Holes were also drilled on lines 38.1 mm to either side of the centre line at 50.8 mm intervals from X = 0 to X = 457.2 mm. Pitot traverses were made with the small CPP mounted in all these holes excepting those for X = 457.2 mm. The profile traverse was thus in each case at an X value 6.35 mm upstream of the static hole.
- 9 The author has interpolated the static pressure data to the X-stations of the profiles. Static pressure was assumed constant through the layer, the characteristic solution having shown that the limiting isobars of the ideal flow approached normally. The total temperature was assumed constant. The boundary layer edge was specified by fitting a power law to the outer two thirds of the velocity profile, and the edge stagnation state set equal to the reservoir state. The effects of finite static hole size (d_s) were allowed for by an adjustment in the form

$$\Delta p / \tau_w = 0.0045 (u_t d_s / \nu) \quad \text{for } u_t d_s / \nu \leq 611$$

$$\Delta p / \tau_w = 2.75 \quad \text{for } u_t d_s / \nu > 611$$

The fluid properties were evaluated at an intermediate reference temperature (T^*) and Sutherland's viscosity law was used. The correction varied from 1 % to 1.5 %. A Pitot tube displacement and shear correction was applied in the form of an effective centre-position displacement Δy given in terms of the

tube diameter d_p by

$$\Delta y/d_p = 0.15 - 0.04 \left(\frac{d_p}{y} - 0.5 \right) \text{ for } \frac{d_p}{2} \leq y \leq 2 d_p; \quad \Delta y/d_p = 0.15 \text{ for } y > 2 d_p.$$

- 12 The editors have replaced the author's assumption of isoenergetic flow by the assumption of an adiabatic wall and the Crocco/Van Driest temperature relation. The boundary layer edge and edge stagnation state
- 13 have been retained at the authors' values. The profiles presented are those for the centre line in the region covered by the designed pressure distribution. In this region variation of Mach number across the tunnel is small. The author gives further data downstream, where the pressure gradient is rather irregular,
- 14 and, although symmetrical, the flow displays threedimensional variations. The author presents CF values reduced from the Preston tube measurements with the calibration functions of Sigalla (1966), Hopkins and Keener (1966 - Reference Temperature) and Fenter and Stalmach (1957). The Hopkins and Keener value has been selected for the profile tabulation of section B. The other values are given in Section D.
- 5 DATA 70070101 - 0120. PT2 profiles. NX = 20. CF from Preston tubes.

15 Editors' comments

The test layer is described at close intervals as it passes from a constant pressure region into an adverse pressure gradient followed by a region of constant pressure. An inspection of our transformed log-law plots suggests that the outer region has not reached equilibrium at the last station presented here. We have not presented further profiles downstream as the pressure history after profile 20 is rather random. The pressure gradient is imposed as a reflected wave, so that normal pressure gradients should be negligible except at the start and end of the APG (profiles 03, 15, 16).

The wall temperature was not measured, but "should be between room temperature (same as total temperature) and the adiabatic wall temperature". We have arbitrarily chosen the latter, but variation in this range should have little effect on the numerical results. The profiles extend in as far as the momentum deficit peak. The power-law velocity profile determination of the boundary layer edge results in a D-state at which there is still a marked total pressure deficit. Three-dimensional effects (see § 5 above) are to be expected as the length to width ratio of the tunnel floor is about 8.

Comparable planar investigations are those of Waltrup & Schetz - CAT 7104 and Thomas - CAT 7401. The closest comparison is with Lewis et al. - CAT 7201 - who, however, used an axisymmetric test arrangement.

7007 ZWARTS. SECTION D. ADDITIONAL DATA.

SKIN FRICTION COEFFICIENT USING DIFFERENT CALIBRATIONS.

A - SIGALLA, B - HOPKINS & KEENER, C - STALMACH, VALUES OF CF X 10⁴

PROFILE 7007	CALIBRATION			PROFILE 7007	CALIBRATION		
	A	B	C		A	B	C
0101	8.92	8.22	8.35	0111	8.44	7.57	7.98
0102	9.11	8.45	8.54	0112	8.52	7.68	8.10
0103	9.32	8.72	8.77	0113	8.23	7.36	7.83
0104	8.73	7.96	8.16	0114	7.95	7.04	7.55
0105	8.09	7.20	7.52	0115	8.16	7.27	7.79
0106	8.16	7.26	7.59	0116	8.80	7.98	8.47
0107	8.15	7.24	7.61	0117	9.30	8.57	9.01
0108	8.52	7.66	8.01	0118	9.80	9.16	9.55
0109	8.25	7.35	7.75	0119	10.17	9.62	9.96
0110	8.23	7.34	7.75	0120	11.52	11.38	11.46

CAT 7007		ZWARTS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.					
RUN X *	MD *	TN/TR*	RED2W	CF *	H12	H12K	PW	PD	
RZ	POD*	PH/PA*	RED2D	CU	H32	H32K	TH	TD	
	YOD*	SW *	O2	PI2	H42	D2K	UD	TR	
70070101	4.0203	1.0000	1.0435 ⁺ +04	8.2200 ⁻ -04	7.8489	1.3617	9.4452 ⁺ +03	9.4452 ⁺ +03	
-6.3500 ⁻ -03	1.4734 ⁺ +06	1.0000	3.5786 ⁺ +04	NM	1.8289	1.8017	2.7106 ⁺ +02	6.9566 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.6166 ⁻ -04	NC	0.1453	1.0525 ⁻ -03	6.7231 ⁺ +02	7.7106 ⁺ +02	
70070102	4.0206	1.0000	1.0634 ⁺ +04	8.4500 ⁻ -04	7.8142	1.3492	9.4414 ⁺ +03	9.4414 ⁺ +03	
6.3500 ⁻ -03	1.4734 ⁺ +06	1.0000	3.6473 ⁺ +04	NM	1.8332	1.8077	2.7106 ⁺ +02	6.9559 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.7253 ⁻ -04	NC	0.1456	1.0625 ⁻ -03	6.7232 ⁺ +02	7.7106 ⁺ +02	
70070103	4.0156	1.0000	1.0773 ⁺ +04	8.7200 ⁻ -04	7.8485	1.3626	9.5044 ⁺ +03	9.5044 ⁺ +03	
1.9050 ⁻ -02	1.4734 ⁺ +06	1.0000	3.6880 ⁺ +04	NM	1.8248	1.7965	2.7107 ⁺ +02	6.9691 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.7744 ⁻ -04	NC	0.1449	1.0915 ⁻ -03	6.7212 ⁺ +02	7.7107 ⁺ +02	
70070104	3.9342	1.0000	1.1807 ⁺ +04	7.7600 ⁻ -04	7.8634	1.3547	1.0598 ⁺ +04	1.0598 ⁺ +04	
3.1750 ⁻ -02	1.4734 ⁺ +06	1.0000	3.9210 ⁺ +04	NM	1.8221	1.7954	2.7130 ⁺ +02	7.1893 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.8878 ⁻ -04	NC	0.1432	1.0994 ⁻ -03	6.6882 ⁺ +02	2.7130 ⁺ +02	
70070105	3.8250	1.0000	1.2981 ⁺ +04	7.2000 ⁻ -04	7.3351	1.3668	1.2287 ⁺ +04	1.2287 ⁺ +04	
4.4450 ⁻ -02	1.4734 ⁺ +06	1.0000	4.1375 ⁺ +04	NM	1.8094	1.7798	2.7162 ⁺ +02	7.4996 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.8712 ⁻ -04	NC	0.1402	1.0971 ⁻ -03	6.6414 ⁺ +02	2.7162 ⁺ +02	
70070106	3.7270	1.0000	1.4189 ⁺ +04	7.2600 ⁻ -04	7.0156	1.3841	1.4036 ⁺ +04	1.4036 ⁺ +04	
5.7150 ⁻ -02	1.4713 ⁺ +06	1.0000	4.3487 ⁺ +04	NM	1.8132	1.7831	2.7460 ⁺ +02	7.8699 ⁺ +01	
INFINITE	2.9733 ⁺ +02	0.0000	5.9569 ⁻ -04	NC	0.1387	1.0759 ⁻ -03	6.6291 ⁺ +02	2.7460 ⁺ +02	
70070107	3.6099	1.0000	1.5731 ⁺ +04	7.2400 ⁻ -04	6.7578	1.4159	1.6520 ⁺ +04	1.6520 ⁺ +04	
6.9850 ⁻ -02	1.4713 ⁺ +06	1.0000	4.6093 ⁺ +04	NM	1.7992	1.7664	2.7529 ⁺ +02	8.2541 ⁺ +01	
INFINITE	2.9767 ⁺ +02	0.0000	5.9451 ⁻ -04	NC	0.1352	1.0733 ⁻ -03	6.5757 ⁺ +02	2.7529 ⁺ +02	
70070108	3.5375	1.0000	1.6304 ⁺ +04	7.6600 ⁻ -04	6.6259	1.4300	1.8292 ⁺ +04	1.8292 ⁺ +04	
8.2550 ⁻ -02	1.4713 ⁺ +06	1.0000	4.6460 ⁺ +04	NM	1.7821	1.7557	2.7539 ⁺ +02	8.4933 ⁺ +01	
INFINITE	2.9750 ⁺ +02	0.0000	5.7618 ⁻ -04	NC	0.1324	1.0594 ⁻ -03	6.5365 ⁺ +02	2.7539 ⁺ +02	
70070109	3.4640	1.0000	1.7939 ⁺ +04	7.3500 ⁻ -04	6.4277	1.4379	2.0305 ⁺ +04	2.0305 ⁺ +04	
9.5250 ⁻ -02	1.4713 ⁺ +06	1.0000	4.9676 ⁺ +04	NM	1.7804	1.7525	2.7587 ⁺ +02	8.7564 ⁺ +01	
INFINITE	2.9772 ⁺ +02	0.0000	5.9300 ⁻ -04	NC	0.1307	1.0720 ⁻ -03	6.4992 ⁺ +02	2.7587 ⁺ +02	
70070110	3.3956	1.0000	1.9240 ⁺ +04	7.3400 ⁻ -04	6.2865	1.4528	2.2395 ⁺ +04	2.2395 ⁺ +04	
1.0795 ⁻ -01	1.4713 ⁺ +06	1.0000	5.1877 ⁺ +04	NM	1.7699	1.7437	2.7628 ⁺ +02	9.0105 ⁺ +01	
INFINITE	2.9789 ⁺ +02	0.0000	5.9745 ⁻ -04	NC	0.1284	1.0813 ⁻ -03	6.4325 ⁺ +02	2.7628 ⁺ +02	
70070111	3.3412	1.0000	2.0116 ⁺ +04	7.5700 ⁻ -04	6.1407	1.4504	2.4223 ⁺ +04	2.4223 ⁺ +04	
1.2065 ⁻ -01	1.4713 ⁺ +06	1.0000	5.3104 ⁺ +04	NM	1.7668	1.7437	2.7639 ⁺ +02	9.2114 ⁺ +01	
INFINITE	2.9778 ⁺ +02	0.0000	5.9360 ⁻ -04	NC	0.1269	1.0866 ⁻ -03	6.4295 ⁺ +02	2.7639 ⁺ +02	
70070112	3.2661	1.0000	2.2101 ⁺ +04	7.6800 ⁻ -04	5.9539	1.4574	2.7028 ⁺ +04	2.7028 ⁺ +04	
1.3335 ⁻ -01	1.4720 ⁺ +06	1.0000	5.6771 ⁺ +04	NM	1.7625	1.7398	2.7359 ⁺ +02	9.3967 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	5.9909 ⁻ -04	NC	0.1248	1.0824 ⁻ -03	6.3479 ⁺ +02	2.7359 ⁺ +02	
70070113	3.1723	1.0000	2.4455 ⁺ +04	7.3600 ⁻ -04	5.7799	1.4827	3.0978 ⁺ +04	3.0978 ⁺ +04	
1.4605 ⁻ -01	1.4713 ⁺ +06	1.0000	6.0555 ⁺ +04	NM	1.7471	1.7267	2.7318 ⁺ +02	9.7714 ⁺ +01	
INFINITE	2.9444 ⁺ +02	0.0000	6.0782 ⁻ -04	NC	0.1214	1.0774 ⁻ -03	6.2883 ⁺ +02	2.7398 ⁺ +02	
70070114	3.0722	1.0000	2.7478 ⁺ +04	7.0400 ⁻ -04	5.5419	1.4977	3.5958 ⁺ +04	3.5958 ⁺ +04	
1.5875 ⁻ -01	1.4713 ⁺ +06	1.0000	6.5202 ⁺ +04	NM	1.7427	1.7203	2.7919 ⁺ +02	1.0374 ⁺ +02	
INFINITE	2.9956 ⁺ +02	0.0000	6.3542 ⁻ -04	NC	0.1185	1.1004 ⁻ -03	6.2737 ⁺ +02	2.7919 ⁺ +02	
70070115	2.9867	1.0000	3.0051 ⁺ +04	7.2700 ⁻ -04	5.3258	1.4995	4.0863 ⁺ +04	4.0863 ⁺ +04	
1.7145 ⁻ -01	1.4713 ⁺ +06	1.0000	7.0325 ⁺ +04	NM	1.7410	1.7189	2.7944 ⁺ +02	1.0754 ⁺ +02	
INFINITE	2.9939 ⁺ +02	0.0000	6.5364 ⁻ -04	NC	0.1160	1.1085 ⁻ -03	6.2098 ⁺ +02	2.7944 ⁺ +02	
70070116	2.9640	1.0000	3.1425 ⁺ +04	7.9800 ⁻ -04	5.1858	1.4646	4.2282 ⁺ +04	4.2282 ⁺ +04	
1.8415 ⁻ -01	1.4713 ⁺ +06	1.0000	7.1455 ⁺ +04	NM	1.7553	1.7349	2.7965 ⁺ +02	1.0863 ⁺ +02	
INFINITE	2.9950 ⁺ +02	0.0000	6.5035 ⁻ -04	NC	0.1163	1.0855 ⁻ -03	6.1939 ⁺ +02	2.7965 ⁺ +02	
70070117	2.9635	1.0000	3.2099 ⁺ +04	9.5700 ⁻ -04	5.0894	1.4271	4.2313 ⁺ +04	4.2313 ⁺ +04	
1.9685 ⁻ -01	1.4713 ⁺ +06	1.0000	7.2975 ⁺ +04	NM	1.7740	1.7538	2.7960 ⁺ +02	1.0863 ⁺ +02	
INFINITE	2.9944 ⁺ +02	0.0000	6.6993 ⁻ -04	NC	0.1176	1.0786 ⁻ -03	6.1929 ⁺ +02	2.7960 ⁺ +02	
70070118	2.9578	1.0000	3.1532 ⁺ +04	9.1600 ⁻ -04	5.0581	1.4162	4.2718 ⁺ +04	4.2718 ⁺ +04	
2.0935 ⁻ -01	1.4727 ⁺ +06	1.0000	7.1545 ⁺ +04	NM	1.7760	1.7585	2.7916 ⁺ +02	1.0872 ⁺ +02	
INFINITE	2.9894 ⁺ +02	0.0000	6.5259 ⁻ -04	NC	0.1175	1.0478 ⁻ -03	6.1834 ⁺ +02	2.7916 ⁺ +02	
70070119	2.9725	1.0000	3.2157 ⁺ +04	9.6200 ⁻ -04	5.0156	1.3845	4.1783 ⁺ +04	4.1783 ⁺ +04	
2.2225 ⁻ -01	1.4727 ⁺ +06	1.0000	7.3416 ⁺ +04	NM	1.7920	1.7751	2.7842 ⁺ +02	1.0777 ⁺ +02	
INFINITE	2.9822 ⁺ +02	0.0000	6.7267 ⁻ -04	NC	0.1190	1.0582 ⁻ -03	6.1871 ⁺ +02	2.7842 ⁺ +02	
70070120	2.9742	1.0000	3.1554 ⁺ +04	1.1380 ⁻ -03	4.9061	1.3403	4.1677 ⁺ +04	4.1677 ⁺ +04	
2.4765 ⁻ -01	1.4727 ⁺ +06	1.0000	7.1683 ⁺ +04	NM	1.8179	1.8024	2.7721 ⁺ +02	1.0723 ⁺ +02	
INFINITE	2.9694 ⁺ +02	0.0000	6.4331 ⁻ -04	NC	0.1208	9.8674 ⁻ -04	6.1751 ⁺ +02	2.7721 ⁺ +02	

70070103		ZWARTS	PROFILE TABULATION		22 POINTS, DELTA AT POINT 19				
I	Y	PT2/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RHOD0=U/UD	
1	0.0030"+00	1.0000"+00	NM	0.92062	0.00000	0.00000	3.84961	0.00000	
2	2.0638"-04	2.8739"+00	NM	0.94689	0.33590	0.57527	2.93328	0.19612	
3	5.8420"-04	3.4103"+00	NM	0.95130	0.37335	0.62168	2.77280	0.22421	
4	9.0678"-04	4.2809"+00	NM	0.95744	0.42062	0.68113	2.54902	0.26721	
5	1.2243"+03	4.7342"+00	NM	0.96142	0.46238	0.71696	2.40427	0.29820	
6	1.5415"+03	5.4819"+00	NM	0.96443	0.49043	0.74292	2.29473	0.32375	
7	2.1768"+03	6.4865"+00	NM	0.96925	0.53761	0.78268	2.11947	0.34928	
8	2.8118"+03	7.3563"+00	NM	0.97286	0.57540	0.81126	1.98782	0.40812	
9	3.4468"+03	8.1037"+00	NM	0.97591	0.60915	0.83456	1.87702	0.44462	
10	4.0818"+03	9.0418"+00	NM	0.97872	0.64225	0.85555	1.77451	0.48213	
11	4.7168"+03	9.9134"+00	NM	0.98128	0.67420	0.87420	1.68128	0.51996	
12	5.3518"+03	1.0824"+01	NM	0.98369	0.70602	0.89134	1.59386	0.55923	
13	5.9868"+03	1.1831"+01	NM	0.98607	0.73961	0.90801	1.50719	0.60245	
14	6.6218"+03	1.3230"+01	NM	0.98899	0.78410	0.92805	1.40087	0.66248	
15	7.2568"+03	1.4573"+01	NM	0.99141	0.82416	0.94432	1.31285	0.71929	
16	7.8918"+03	1.5732"+01	NM	0.99327	0.85737	0.95666	1.24502	0.76839	
17	9.1618"+03	1.7962"+01	NM	0.99636	0.91793	0.97682	1.13242	0.86259	
18	1.0432"-02	1.9869"+01	NM	0.99859	0.96667	0.99110	1.05119	0.94284	
D 19	1.1420"-02	2.1229"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
20	1.1702"-02	2.1513"+01	NM	1.00028	1.00681	1.00174	0.98995	1.01191	
21	1.1829"-02	2.1693"+01	NM	1.00045	1.01113	1.00283	0.98365	1.01949	
22	1.1956"-02	2.1785"+01	NM	1.00054	1.01330	1.00337	0.98050	1.02332	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

70070105		ZWARTS	PROFILE TABULATION		23 POINTS, DELTA AT POINT 20				
I	Y	PT2/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RHOD0=U/UD	
1	0.0000"+00	1.0000"+00	NM	0.92249	0.00000	0.00000	3.62181	0.00000	
2	2.4638"-04	2.3570"+00	NM	0.94394	0.30915	0.52610	2.89613	0.18166	
3	5.8608"-04	2.6993"+00	NM	0.94725	0.33871	0.56518	2.78434	0.20298	
4	7.1374"-04	3.5132"+00	NM	0.95402	0.39900	0.63781	2.55525	0.24961	
5	1.0338"+03	4.1069"+00	NM	0.95873	0.44220	0.68425	2.39430	0.28578	
6	1.3513"+03	4.6818"+00	NM	0.96189	0.47129	0.71301	2.28891	0.31151	
7	1.6608"+03	5.0966"+00	NM	0.96430	0.49429	0.73443	2.20765	0.33267	
8	1.9863"+03	5.5106"+00	NM	0.96693	0.51620	0.75376	2.13222	0.35351	
9	2.6213"+03	6.3548"+00	NM	0.97063	0.55815	0.78806	1.99354	0.39531	
10	3.2563"+03	7.0720"+00	NM	0.97371	0.59141	0.81290	1.88931	0.43026	
11	3.8913"+03	8.0145"+00	NM	0.97730	0.63242	0.84087	1.76794	0.47563	
12	4.5263"+03	9.2363"+00	NM	0.98131	0.68189	0.87114	1.63214	0.53374	
13	5.1613"+03	1.0205"+01	NM	0.98408	0.71869	0.89142	1.53845	0.57343	
14	5.7963"+03	1.1145"+01	NM	0.98643	0.75263	0.90859	1.45739	0.62344	
15	6.4313"+03	1.2079"+01	NM	0.98862	0.78494	0.92370	1.38482	0.66702	
16	7.0663"+03	1.3155"+01	NM	0.99084	0.82055	0.93707	1.30476	0.71698	
17	7.7013"+03	1.4269"+01	NM	0.99290	0.85585	0.94931	1.24017	0.76852	
18	8.3363"+03	1.5025"+01	NM	0.99476	0.89379	0.96150	1.09610	0.89545	
19	1.0241"-02	1.8885"+01	NM	0.99750	0.98876	0.99086	1.01645	0.98072	
D 20	1.1027"-02	1.9306"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
21	1.1511"-02	1.9875"+01	NM	1.00034	1.00792	1.00217	0.98862	1.01371	
22	1.1638"-02	1.9951"+01	NM	1.00039	1.00912	1.00299	0.98691	1.01579	
23	1.1755"-02	1.9727"+01	NM	1.00047	1.01113	1.00304	0.98405	1.01929	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

70070109		ZWARTS	PROFILE TABULATION		24 POINTS, DELTA AT POINT 23				
I	Y	PT2/P	P/PD	T0/T00	H/HD	U/UD	T/TD	RHO/RHOD0=U/UD	
1	0.0000"+00	1.0000"+00	NM	0.92659	0.00000	0.00000	3.15027	0.00000	
2	2.4638"-04	2.2279"+00	NM	0.94679	0.32794	0.52456	2.58660	0.20502	
3	5.8608"-04	2.4550"+00	NM	0.94912	0.35110	0.55404	2.49021	0.22249	
4	5.2076"-04	2.7161"+00	NM	0.95161	0.37552	0.58384	2.41731	0.24152	
5	6.5024"-04	2.9033"+00	NM	0.95329	0.39191	0.60310	2.36815	0.25467	
6	7.7976"-04	3.0870"+00	NM	0.95486	0.40726	0.62060	2.32210	0.26726	
7	1.0338"+03	3.3681"+00	NM	0.95714	0.42956	0.64511	2.25539	0.28603	
8	1.3513"+03	3.7278"+00	NM	0.95986	0.45636	0.67317	2.17587	0.30938	
9	1.6608"+03	4.0549"+00	NM	0.96216	0.47934	0.69604	2.10852	0.33011	
10	1.9863"+03	4.4559"+00	NM	0.96478	0.50601	0.72125	2.03169	0.35500	
11	2.3038"+03	4.7871"+00	NM	0.96680	0.52697	0.74010	1.97247	0.37522	
12	2.6213"+03	5.2018"+00	NM	0.96917	0.55206	0.76156	1.90310	0.40018	
13	3.2563"+03	6.0591"+00	NM	0.97356	0.60050	0.79991	1.77440	0.45081	
14	3.8913"+03	6.7482"+00	NM	0.97753	0.64685	0.83298	1.65830	0.50231	
15	4.5263"+03	7.4724"+00	NM	0.98140	0.69637	0.86478	1.54219	0.56075	
16	5.1613"+03	9.1534"+00	NM	0.98542	0.74733	0.89520	1.42787	0.62730	
17	5.7963"+03	1.0277"+01	NM	0.98863	0.79650	0.91944	1.33251	0.69000	
18	6.4313"+03	1.1427"+01	NM	0.99154	0.84200	0.94059	1.24789	0.75375	
19	7.0663"+03	1.2629"+01	NM	0.99419	0.88706	0.95960	1.17024	0.82001	
20	7.7013"+03	1.3851"+01	NM	0.99656	0.93081	0.97632	1.10064	0.88705	
21	8.3363"+03	1.4670"+01	NM	0.99880	0.95869	0.98631	1.05845	0.93185	
22	8.9713"+03	1.5408"+01	NM	0.99921	0.98330	0.99461	1.02313	0.97212	
D 23	9.0957"+03	1.5919"+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
24	9.6063"+03	1.5559"+01	NM	0.99945	0.98825	0.99622	1.01521	0.98034	

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

70070114		ZWARTS	PROFILE TABULATION	22 POINTS, DELTA AT POINT 21				
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93202	0.10000	0.00000	2.69136	0.00000
2	2.4638 ⁻ -04	1.9747 ⁺ +00	NM	0.94946	0.33718	0.50659	2.25730	0.22442
3	3.8608 ⁻ -04	2.1435 ⁺ +00	NM	0.95141	0.35937	0.53413	2.20883	0.24182
4	5.2070 ⁻ -04	2.3473 ⁺ +00	NM	0.95355	0.38379	0.56275	2.15572	0.26105
5	6.5024 ⁻ -04	2.4888 ⁺ +00	NM	0.95502	0.39957	0.58166	2.11913	0.27448
6	7.7978 ⁻ -04	2.6013 ⁺ +00	NM	0.95611	0.41157	0.59529	2.09200	0.28456
7	1.0330 ⁻ -03	2.7956 ⁺ +00	NM	0.95791	0.43117	0.61719	2.04709	0.30149
8	1.3513 ⁻ -03	3.0487 ⁺ +00	NM	0.96113	0.45565	0.64308	1.99189	0.32285
9	1.6688 ⁻ -03	3.2531 ⁺ +00	NM	0.96183	0.47124	0.66219	1.94971	0.33963
10	1.9863 ⁻ -03	3.4953 ⁺ +00	NM	0.96374	0.49526	0.68307	1.90271	0.35909
11	2.3038 ⁻ -03	3.7292 ⁺ +00	NM	0.96549	0.51468	0.70167	1.85864	0.37752
12	2.6213 ⁻ -03	4.0187 ⁺ +00	NM	0.96754	0.53767	0.72287	1.80755	0.39992
13	3.2563 ⁻ -03	4.4471 ⁺ +00	NM	0.97159	0.58343	0.76292	1.70690	0.44697
14	3.8913 ⁻ -03	5.4045 ⁺ +00	NM	0.97595	0.63581	0.80385	1.59844	0.50290
15	4.5263 ⁻ -03	6.3287 ⁺ +00	NM	0.98053	0.69336	0.84475	1.48439	0.56709
16	5.1613 ⁻ -03	7.7016 ⁺ +00	NM	0.98509	0.74493	0.88354	1.37102	0.64444
17	5.7963 ⁻ -03	8.6657 ⁺ +00	NM	0.98963	0.82079	0.92059	1.25796	0.73181
18	6.4313 ⁻ -03	1.0025 ⁺ +01	NM	0.99375	0.88645	0.95291	1.15555	0.82463
19	7.0663 ⁻ -03	1.1357 ⁺ +01	NM	0.99718	0.94634	0.97901	1.07074	0.91476
20	7.7013 ⁻ -03	1.2175 ⁺ +01	NM	0.99904	0.98129	0.99292	1.02385	0.96979
D 21	7.9461 ⁻ -03	1.2675 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
22	8.3363 ⁻ -03	1.2545 ⁺ +01	NM	0.99985	0.99712	0.99893	1.00363	0.99532


INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

70070117		ZWARTS	PROFILE TABULATION	24 POINTS, DELTA AT POINT 23				
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93373	0.00000	0.00000	2.57379	0.00000
2	2.4638 ⁻ -04	2.2225 ⁺ +00	NM	0.95403	0.38265	0.54342	2.09178	0.26457
3	3.8608 ⁻ -04	2.4765 ⁺ +00	NM	0.95665	0.41284	0.58812	2.02904	0.28980
4	5.2070 ⁻ -04	2.6799 ⁺ +00	NM	0.95861	0.43511	0.61271	1.98297	0.30899
5	6.5024 ⁻ -04	2.8085 ⁺ +00	NM	0.95977	0.44851	0.62710	1.95489	0.32078
6	7.7978 ⁻ -04	2.9195 ⁺ +00	NM	0.96078	0.45972	0.63889	1.93140	0.33079
7	1.0338 ⁻ -03	3.1446 ⁺ +00	NM	0.96270	0.48151	0.66121	1.88573	0.35064
8	1.3513 ⁻ -03	3.3645 ⁺ +00	NM	0.96449	0.50178	0.68127	1.84335	0.36958
9	1.6688 ⁻ -03	3.5998 ⁺ +00	NM	0.96600	0.51906	0.69783	1.80742	0.38609
10	1.9863 ⁻ -03	3.7875 ⁺ +00	NM	0.96765	0.53802	0.71544	1.76824	0.40466
11	2.3038 ⁻ -03	4.0130 ⁺ +00	NM	0.96929	0.55699	0.73249	1.72940	0.42355
12	2.6213 ⁻ -03	4.2643 ⁺ +00	NM	0.97079	0.57680	0.74968	1.68930	0.44378
13	3.2563 ⁻ -03	4.8318 ⁺ +00	NM	0.97452	0.61920	0.78451	1.60520	0.48873
14	3.8913 ⁻ -03	5.5304 ⁺ +00	NM	0.97841	0.66758	0.82109	1.51276	0.54278
15	4.5263 ⁻ -03	6.3116 ⁺ +00	NM	0.98225	0.71773	0.85571	1.42141	0.60201
16	5.1613 ⁻ -03	7.2347 ⁺ +00	NM	0.98624	0.77273	0.89011	1.32688	0.67083
17	5.7963 ⁻ -03	8.2308 ⁺ +00	NM	0.98997	0.82793	0.92125	1.23812	0.74407
18	6.4313 ⁻ -03	9.2034 ⁺ +00	NM	0.99317	0.87846	0.94705	1.16226	0.81483
19	7.0663 ⁻ -03	1.0095 ⁺ +01	NM	0.99577	0.92231	0.96755	1.10049	0.87919
20	7.7013 ⁻ -03	1.0731 ⁺ +01	NM	0.99746	0.95231	0.98065	1.06031	0.92487
21	8.3363 ⁻ -03	1.1102 ⁺ +01	NM	0.99839	0.96909	0.98781	1.03815	0.95151
22	8.9713 ⁻ -03	1.1252 ⁺ +01	NM	0.99876	0.97629	0.99058	1.02950	0.96220
D 23	9.0272 ⁻ -03	1.1781 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
24	9.6063 ⁻ -03	1.1263 ⁺ +01	NM	0.99879	0.97682	0.99080	1.02883	0.96303

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

70070120		ZWARTS	PROFILE TABULATION	26 POINTS, DELTA AT POINT 24				
I	Y	PT2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93356	0.00000	0.00000	2.58518	0.00000
2	2.4638 ⁻ -04	2.8331 ⁺ +00	NM	0.95983	0.44940	0.62888	1.95826	0.32114
3	3.8608 ⁻ -04	3.2711 ⁺ +00	NM	0.96356	0.49151	0.67201	1.86431	0.35950
4	5.2070 ⁻ -04	3.4637 ⁺ +00	NM	0.96580	0.50880	0.68885	1.83209	0.37581
5	6.5024 ⁻ -04	3.6090 ⁺ +00	NM	0.96619	0.52143	0.70081	1.80657	0.38794
6	7.7978 ⁻ -04	3.7301 ⁺ +00	NM	0.96709	0.53171	0.71041	1.78516	0.39796
7	1.0338 ⁻ -03	3.9963 ⁺ +00	NM	0.96871	0.55036	0.72735	1.74657	0.41644
8	1.3513 ⁻ -03	4.1875 ⁺ +00	NM	0.97029	0.56875	0.74380	1.70899	0.43508
9	1.6688 ⁻ -03	4.4017 ⁺ +00	NM	0.97169	0.58524	0.75754	1.67549	0.45213
10	1.9863 ⁻ -03	4.6228 ⁺ +00	NM	0.97307	0.60177	0.77120	1.64239	0.46956
11	2.3038 ⁻ -03	4.8470 ⁺ +00	NM	0.97442	0.61806	0.78427	1.61016	0.48708
12	2.6213 ⁻ -03	5.0871 ⁺ +00	NM	0.97581	0.63503	0.79748	1.57705	0.50568
13	3.2563 ⁻ -03	5.6258 ⁺ +00	NM	0.97872	0.67149	0.82447	1.50761	0.54688
14	3.8913 ⁻ -03	6.1809 ⁺ +00	NM	0.98146	0.70704	0.84912	1.44226	0.58874
15	4.5263 ⁻ -03	6.8564 ⁺ +00	NM	0.98446	0.74766	0.87532	1.37064	0.63862
16	5.1613 ⁻ -03	7.6001 ⁺ +00	NM	0.98748	0.79058	0.90091	1.29959	0.69376
17	5.7963 ⁻ -03	8.4068 ⁺ +00	NM	0.99040	0.83429	0.92493	1.22907	0.75244
18	6.4313 ⁻ -03	9.1792 ⁺ +00	NM	0.99291	0.87408	0.94513	1.16918	0.80837
19	7.0663 ⁻ -03	9.8980 ⁺ +00	NM	0.99503	0.90953	0.96190	1.11848	0.86001
20	7.7013 ⁻ -03	1.0516 ⁺ +01	NM	0.99672	0.93894	0.97500	1.07828	0.90422
21	8.3363 ⁻ -03	1.0872 ⁺ +01	NM	0.99769	0.95646	0.98282	1.05511	0.93115
22	8.9713 ⁻ -03	1.1107 ⁺ +01	NM	0.99822	0.96623	0.98856	1.04244	0.94635
23	9.6063 ⁻ -03	1.1205 ⁺ +01	NM	0.99846	0.97066	0.98834	1.03676	0.95330
D 24	1.0180 ⁻ -02	1.1863 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
25	1.0241 ⁻ -02	1.1458 ⁺ +01	NM	0.99906	0.98204	0.99294	1.02232	0.97126
26	1.0876 ⁻ -02	1.1856 ⁺ +01	NM	0.99997	0.99972	0.99989	1.00034	0.99955

INPUT VARIABLES Y,U/UD (ISOENERGETIC) ASSUME P=PD AND VAN DRIEST

	M : 3.5 falling to 2.8 R THETA X 10 ⁻³ : 18 - 42 TH/TR : 1.0	7101
		ZPG - APG AW
Continuous wind tunnel with asymmetric flexible nozzle. W = H = 0.15 m. 0.26 < PO < 0.40 MN/m ² . TO : 307 K. Air: Dewpoint < 245 K. 14 < RE/m X 10 ⁻⁶ < 30.		
STUREK W.B. and DANBERG J.E., 1971. Supersonic turbulent boundary-layer in an adverse pressure gradient. Data tabulation. Dept. Mech. & Aerosp. Engrg. Univ. Delaware. Tech. Rep. No. 141. And Danberg J.E., Sturek W.B. Private communications, Sturek 1973. Also Extensive bibliography referring to same experiment listed under Sturek or Sturek & Danberg 1970-74.		

- 1 The tests took place on a ramp forming a continuation of the flat test wall opposite the flexible plate nozzle. The test section extended 559 mm downstream from the nozzle exit plane (X = 0). The curved ramp started with a faired step ($\Delta Y = 0.254$ mm) at X = 305 mm with a maximum height and surface inclination of 35.6 mm and 14.65°. The coordinates are given in table 1. The test zone includes a ZPG region before the ramp (from X = 0 to X = 0.279 m) followed by a simple wave isentropic compression. The test surface was allowed an hour to settle to a bulk equilibrium temperature. Thus only small local heat transfer is likely, as a consequence of the variation of recovery temperature. The surface was "polished to a mirror finish" and the mean dimensions were held to 0.0254 mm. The Mach number in the ZPG region was constant within limits of ± 0.01 . A schlieren photographic study indicated that natural transition occurred in the nozzle region, the transition zone extending from X = - 0.6 to X = - 0.35 m. The test boundary layer was formed in the favourable pressure gradient of the nozzle (throat at X = - 1.25 m). The temperature of the metal test wall was constant within about ± 1 K. Oil flow visualisation did not show appreciable divergence of the streamlines near the centreline, but streamlines near the side walls diverged considerably. Wall pressure measurements on lines normal to the centre line at the last three stations on the ramp showed that the lateral pressure gradient was very small compared to the streamwise pressure gradient. The values are presented graphically in figure 8 of Sturek & Danberg 1972a.
- 2 Wall static pressure was measured by six static holes of 1.02 mm diameter on the centre line at the measuring stations on the ramp and the test wall. Eight additional measurements were made upstream on the test wall, and, with 11 holes of 0.64 mm diameter on lines normal to the flow at the last three measuring stations. The holes were drilled normal to the local surface. For the test described, the wall temperature was monitored at one station (X = 50.8 mm) in the ZPG region. The wall shear stress was determined using a Preston tube of 3.18 mm diameter.
- 3 The total temperature probe used was a wedge recovery probe formed by placing an iron constantan thermocouple junction (diameter 0.127 mm) at the centre of the leading edge of an insulated wedge. The probe was calibrated in the range $1.5 < M < 3.5$, and for lower Mach numbers the calibration was extrapolated using the trend of the data of Spangenberg (1956). The Pitot probe was a FPP for which $h_1 = 0.127$ (E), $h_2 = 0.076$, $b_1 = 1.58$ (E) and $b_2 = 1.52$ mm. Two static pressure probes were used. One, a CCP for which $\alpha = 10^\circ$, $d = 1.27$, $l_1 = 12.7$, $l_2 = 19$ mm with two holes of 0.34 mm diameter. The other was a flat plate probe approximately 35 mm square. The leading edge was chamfered on the underside (which was curved so as to fit flush with the model) at 20° and ten 1.03 mm diameter static holes were drilled at 3 mm intervals along a line 28.5 mm back from the leading edge. At two stations a constant temperature hot-wire probe ($d = 0.0063$, $l = 2.54$ mm) was used for the measurement of fluctuating quantities.
- 4 Profiles and Preston readings were made at the same nominal X values, X = 152.4, 203.2, 254.0, 433.1, 458.8, 484.6, 510.8 and 536.7 mm all on the centre line (Z = 0). The coordinates and local surface slopes of the measuring stations are given in table 2. The results are presented for Y values corresponding to PO measurements.

- 9 The P and T0 values in the tables are interpolated from smoothed curves such as those presented in figure 11 of Sturek & Danberg 1972a. The Preston tube readings were reduced using the calibration of Yanta et al., 10 equation 2b, (1969). No corrections were applied to the profile data (the authors remark upon a 5 K 11 discrepancy between the T0 probe in the free stream and the tunnel reservoir temperature). Sutherland's viscosity law was used.
- 12 The editors have incorporated the calibrations and interpolations of the authors. The integral data of section B is presented in two forms. In the main tables the reference flow is a single state flow corresponding to a D state taken at pU (max), which was also set as the D state for the profile tables whilst an auxiliary table gives integral values based on a reference flow which has the tunnel reservoir pressure and local static pressure.
- 13 The main portion of the data consists of three sets of eight profiles, each set for a different reservoir pressure. In each case three ZPG stations were followed by five on the curved ramp. To these are added two individual profiles (Sturek, 1973) measured at $X = 458.8$ mm for which the tunnel total temperature was 4 varied so as to cause, in the nozzle region, heat flux from the flow (0401) or to the flow (0501). The Mach 9 number distribution was taken to be the same as for the profile of the earlier set (0205) with the same total pressure. The total temperature was measured using a probe consisting of an iron-constantan thermocouple mounted in a truncated cone-cylinder body. The thermocouple consisted of a 0.25 mm diameter wire sheathed in stainless steel with magnesium dioxide insulation. The thermocouple junction was worked to a sharp tip with a conical epoxy filling to the diameter of the sheath. The probe tip presented a frontal 9 area to the flow of 0.08 mm diameter. The probe was calibrated in the free stream and the calibration was assumed to vary through the boundary layer in the same general manner as the probe used earlier.
- 13 The earlier hot wire data (Sturek & Danberg 1972a) was presented graphically, as sufficient data had not been obtained to provide more than a qualitative assessment. Further data (Danberg, PC) is given here for 8 profiles taken at $X = 203.2$ and 458.8 mm. The general conditions correspond to profiles 0202 and 0205.
- 14 The CF values given with the profiles are those evaluated by the authors. The raw Preston tube data is given in section D.
- 5 DATA: 7101 0101-0501. Pitot, T0 and P profiles obtained separately. NX = 8. CF from Preston tubes. Some supporting hot wire data.
- 15 Editors' comments

Sturek and Danberg provide the only fully documented account of a simple wave flow. The experiment is therefore of the first importance to any research worker wishing to consider the effects of streamline curvature. The Mach number is high enough for the static pressure to vary by 50 % across a boundary layer for which the ratio δ/RX is about 0.02, but not so high that the interpretation of static pressure measurements becomes too contentious. The value of the experiment is further increased by the inclusion of wall shear stress measurements in association with each profile, and the fluctuation measurements, however restricted they may be. There is room for differences of opinion as to the precise calibration of the sensors, but the qualitative results and the trends established must stand.

The authors present a full analysis of the original data in Sturek & Danberg (1972b). This is extended by Sturek (1974) to include a determination, from the mean flow data, of shear stress, mixing length and eddy viscosity.

There is a marked fall in the general level of CF as the flow passes on to the ramp, followed by a rising tendency. The shear stress itself, however, rises continuously, so that the change in CF is associated rather with the change in the reference dynamic pressure. Both the numerical value of CF and the trend with X are sensitive to the choice of reference state, there being differences of up to 15 % between values calculated using the arbitrary D-state (at pU max) and those calculated using the wall-state of the pressure-based reference flow mentioned in § 12 above.

The two additional profiles, 0401, 0501, of Sturek (1973) are both for near adiabatic flow in the test region but correspond to, respectively, heat transfer from and to the flow in the throat region. The

author shows a considerable difference between the two on a "Van Driest" plot of $(T_0 - T_w) / (T_{0D} - T_w)$ against U/UD . It should be noted that this choice of axes is very sensitive to T_0 variations, and the variation noted is 4 - 8 K, or less than 3%. We are not completely sure of the extent to which total temperature data near the wall are interpolations. In Sturek 1973, it is stated that measurements can be made to within 0.25 mm of the wall. Another description (Danberg, PC) suggests much larger values, perhaps as much as 5 mm.

The ZPG data from the first three stations can be compared with the results of Mabey et al. - CAT 7402, on a flat plate, and those of Voisin et al. - CAT 7202 on a tunnel wall. Comparisons may also be made with the other reported simple wave compression tests, Clutter & Kaups - CAT 6401 and Stroud & Miller - CAT 6503 which do not, however, provide so much detail.

FACSIMILES OF TABLES SUPPLIED BY AUTHORS. DIMENSIONS IN INCHES.

TABLE 1		CORRECTED MODEL COORDINATES (INCHES)			
X	Y	X	Y	X	Y
12.006	.010	13.756	.224	18.861	.673
12.914	.023	16.000	.252	18.901	.722
13.141	.030	16.243	.282	06 19.141	.772
13.368	.038	16.488	.313	19.380	.824
13.594	.049	16.729	.346	19.619	.877
13.821	.061	16.971	.381	07 19.858	.932
14.048	.074	04 17.213	.418	07 20.097	.989
14.272	.090	17.455	.455	20.368	1.055
14.537	.108	17.697	.496	20.638	1.124
14.791	.128	05 17.938	.538	08 20.908	1.194
15.025	.149	18.180	.581	08 21.178	1.266
15.269	.172	18.420	.627	21.447	1.341
15.513	.197				

CORRECTED TABLE 2				
STA	X	Y	ϕ	CAT 7101
116	16.000	.262	6.75	-
117	17.019	.368	8.13	04
118	18.035	.559	9.85	05
119	19.021	.747	11.48	06
120	20.024	.969	13.24	07
121	21.016	1.215	14.65	08

CAT 7101		STUREK		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN X + RZ	MD * POD TOD	TN/TR PH/PO SH *	RED2W REN2D DZ	CF CO PI2+	H12 H32 H42	H12K H32K D2K	PW* TW* UD	PD* TD* TR		
71010101 1.5240*-01 INFINITE	3.5090 2.5977*+05 3.0721*+02	1.0213 0.9999 1.0000	6.5554*+03 1.8664*+04 1.3540*-03	1.0722*-03 NM 0.0000*+00	6.5853 1.8023 0.0666	1.3544 1.7738 2.3769*-03	3.3623*+03 2.9056*+02 6.6268*+02	3.3626*+03 8.8722*+01 2.8449*+02		
71010102 2.0320*-01 INFINITE	3.5320 2.6716*+05 3.0640*+02	1.0244 1.0001 1.0000	6.7225*+03 1.9365*+04 1.3775*-03	1.0929*-03 NM 0.0000*+00	6.7025 1.7988 0.0573	1.3510 1.7704 2.4621*-03	3.3477*+03 2.9056*+02 6.6305*+02	3.3474*+03 8.7667*+01 2.8365*+02		
71010103 2.5400*-01 INFINITE	3.4890 2.5379*+05 3.0702*+02	1.0217 1.0001 1.0000	7.0625*+03 1.9961*+04 1.4651*-03	1.0846*-03 NM 0.0000*+00	6.5986 1.7990 0.0517	1.3571 1.7713 2.5870*-03	3.3800*+03 2.9056*+02 6.6138*+02	3.3798*+03 8.9389*+01 2.8438*+02		
71010104 4.3307*-01 INFINITE	3.2450 2.5819*+05 3.0698*+02	1.0183 1.2366 1.0000	1.0678*+04 2.7381*+04 1.7313*-03	9.3101*-04 NM 1.5068*+00	4.2465 1.7368 0.0755	1.4812 1.7128 2.6448*-03	6.0456*+03 2.9056*+02 6.4681*+02	4.8891*+03 9.8833*+01 2.8533*+02		
71010105 4.5377*-01 INFINITE	3.1650 2.6316*+05 3.0518*+02	1.0230 1.2161 1.0000	1.1430*+04 2.8538*+04 1.8805*-03	9.1943*-04 NM 1.4557*+00	4.3163 1.7346 0.0397	1.4765 1.7118 2.5843*-03	6.8158*+03 2.9056*+02 6.3967*+02	5.6047*+03 1.0161*+02 2.8401*+02		
71010106 4.8463*-01 INFINITE	3.0550 2.5318*+05 3.0243*+02	1.0305 1.2035 1.0000	1.1879*+04 2.8612*+04 1.6278*-03	9.3654*-04 NM 1.3830*+00	4.0283 1.7412 0.0443	1.4614 1.7199 2.4219*-03	7.6395*+03 2.9056*+02 6.2914*+02	6.3480*+03 1.0550*+02 2.8195*+02		
71010107 5.1079*-01 INFINITE	2.9820 2.6391*+05 3.0609*+02	1.0169 1.1717 1.0000	1.2814*+04 2.9620*+04 1.5809*-03	9.1815*-04 NM 1.3116*+00	4.1472 1.7365 0.0513	1.4635 1.7165 2.3780*-03	8.3486*+03 2.9056*+02 6.2754*+02	7.3615*+03 1.1017*+02 2.8572*+02		
71010108 5.3670*-01 INFINITE	2.9050 2.6424*+05 3.0551*+02	1.0175 1.1412 1.0000	1.3377*+04 3.0022*+04 1.5303*-03	9.7906*-04 NM 1.1699*+00	4.1479 1.7417 0.0612	1.4673 1.7226 2.2869*-03	9.4723*+03 2.9056*+02 6.2097*+02	8.3006*+03 1.1367*+02 2.8556*+02		
71010201 1.5240*-01 INFINITE	3.5100 3.2436*+05 3.0753*+02	1.0183 1.0001 1.0000	8.1975*+03 2.3290*+04 1.3360*-03	1.0429*-03 NM 0.0000*+00	6.6118 1.7688 0.0662	1.3598 1.7688 2.4033*-03	4.1929*+03 2.9000*+02 6.8308*+02	4.1927*+03 8.8778*+01 2.8478*+02		
71010202 2.0320*-01 INFINITE	3.5400 3.3493*+05 3.0661*+02	1.0218 1.0000 1.0000	8.0409*+03 2.3186*+04 1.3226*-03	1.0578*-03 NM 0.0000*+00	6.7987 1.8008 0.0354	1.3490 1.7739 2.3621*-03	4.1494*+03 2.9000*+02 6.6371*+02	4.1493*+03 8.7444*+01 2.8382*+02		
71010203 2.5400*-01 INFINITE	3.5000 3.2047*+05 3.0743*+02	1.0185 1.0001 1.0000	8.6932*+03 2.4608*+04 1.4417*-03	1.0567*-03 NM 0.0000*+00	6.6072 1.7998 0.0588	1.3582 1.7716 2.5480*-03	4.2020*+03 2.9000*+02 6.6244*+02	4.2017*+03 8.9111*+01 2.8473*+02		
71010204 4.3307*-01 INFINITE	3.2350 3.1856*+05 3.0776*+02	1.0136 1.2333 1.0000	1.2718*+04 3.2354*+04 1.6552*-03	9.2766*-04 NM 1.3927*+00	4.1686 1.7462 0.0743	1.4575 1.7229 2.4931*-03	7.5495*+03 2.9000*+02 6.4699*+02	6.1212*+03 9.9500*+01 2.8610*+02		
71010205 4.5872*-01 INFINITE	3.1610 3.2830*+05 3.0733*+02	1.0139 1.2123 1.0000	1.3762*+04 3.4024*+04 1.6191*-03	9.0079*-04 NM 1.4103*+01	4.1987 1.7435 0.0677	1.4503 1.7216 2.4508*-03	8.5265*+03 2.9000*+02 6.4165*+02	7.0333*+03 1.0250*+02 2.8603*+02		
71010206 4.8412*-01 INFINITE	3.0670 3.2796*+05 3.0702*+02	1.0134 1.1842 1.0000	1.4135*+04 3.3676*+04 1.5217*-03	9.6454*-04 NM 1.3443*+00	4.3941 1.7451 0.0641	1.4642 1.7185 2.3669*-03	9.5647*+03 2.9000*+02 6.3476*+02	8.0772*+03 1.0656*+02 2.8617*+02		
71010207 5.1079*-01 INFINITE	2.9950 3.3493*+05 3.0750*+02	1.0106 1.1767 1.0000	1.5429*+04 3.5649*+04 1.5199*-03	9.1215*-04 NM 1.2884*+00	4.1367 1.7401 0.0629	1.4512 1.7210 2.2807*-03	1.0809*+04 2.9000*+02 6.2996*+02	9.1866*+03 1.1066*+02 2.8696*+02		
71010208 5.3670*-01 INFINITE	2.9090 3.3357*+05 3.0754*+02	1.0089 1.1392 1.0000	1.5908*+04 3.5486*+04 1.4498*-03	9.7347*-04 NM 1.1273*+00	4.1065 1.7524 0.0717	1.4280 1.7360 2.1466*-03	1.1865*+04 2.9000*+02 6.2335*+02	1.0415*+04 1.1422*+02 2.8743*+02		

CAT 7101		STUREK		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN X RZ	MD * PUD TOD	TW/TR PH/PO S/I *	RED2M RED2D D2	CF CO P12*	H12 H32 H42	H12K H32K D2K	PM* TW* UD	PD* TD* TR	
71010301	3.5120	1.0156	9.3955 ⁺⁰³	1.0254 ⁻⁰³	6.5465	1.3398	5.0136 ⁺⁰³	5.0139 ⁺⁰³	
1.5240 ⁻⁰¹	3.8899 ⁺⁰⁵	0.9999	2.8654 ⁺⁰⁴	NM	1.8073	1.7796	2.8944 ⁺⁰²	8.8778 ⁺⁰¹	
INFINITE	3.0778 ⁺⁰²	1.0000	1.2969 ⁻⁰³	0.0000 ⁺⁰⁰	0.0705	2.2561 ⁻⁰³	6.6346 ⁺⁰²	2.8500 ⁺⁰²	
71010302	3.5360	1.0169	9.4905 ⁺⁰³	1.0443 ⁻⁰³	6.7104	1.3463	4.9635 ⁺⁰³	4.9635 ⁺⁰³	
2.0320 ⁻⁰¹	3.9840 ⁺⁰⁵	1.0000	2.7206 ⁺⁰⁴	NM	1.8017	1.7744	2.8944 ⁺⁰²	8.7833 ⁺⁰¹	
INFINITE	3.0747 ⁺⁰²	1.0000	1.3073 ⁻⁰³	0.0000 ⁺⁰⁰	0.0525	2.3197 ⁻⁰³	6.6443 ⁺⁰²	2.8643 ⁺⁰²	
71010303	3.5050	1.0139	9.7002 ⁺⁰³	1.0300 ⁻⁰³	6.4990	1.3365	5.0262 ⁺⁰³	5.0263 ⁺⁰³	
2.5400 ⁻⁰¹	3.8610 ⁺⁰⁵	1.0000	2.7401 ⁺⁰⁴	NM	1.8088	1.7812	2.8944 ⁺⁰²	8.9167 ⁺⁰¹	
INFINITE	3.0825 ⁺⁰²	1.0000	1.3413 ⁻⁰³	0.0000 ⁺⁰⁰	0.0745	2.3205 ⁻⁰³	6.6359 ⁺⁰²	2.8546 ⁺⁰²	
71010304	3.2300	1.0120	1.4577 ⁺⁰⁴	9.2243 ⁻⁰⁴	4.1979	1.4355	9.0125 ⁺⁰³	7.3560 ⁺⁰³	
4.3307 ⁻⁰¹	3.8003 ⁺⁰⁵	1.2252	3.6968 ⁺⁰⁴	NM	1.7537	1.7318	2.8944 ⁺⁰²	9.9667 ⁺⁰¹	
INFINITE	3.0763 ⁺⁰²	1.0000	1.5800 ⁻⁰³	1.4348 ⁺⁰⁰	0.0693	2.3761 ⁻⁰³	6.4653 ⁺⁰²	2.8600 ⁺⁰²	
71010305	3.1400	1.0135	1.5638 ⁺⁰⁴	8.9997 ⁻⁰⁴	4.2659	1.4338	1.0244 ⁺⁰⁴	8.5240 ⁺⁰³	
4.5872 ⁻⁰¹	3.8572 ⁺⁰⁵	1.2018	3.8347 ⁺⁰⁴	NM	1.7494	1.7290	2.8944 ⁺⁰²	1.0322 ⁺⁰²	
INFINITE	3.0677 ⁺⁰²	1.0000	1.5313 ⁻⁰³	1.3739 ⁺⁰⁰	0.0560	2.3188 ⁻⁰³	6.3963 ⁺⁰²	2.8560 ⁺⁰²	
71010306	3.0550	1.0070	1.6567 ⁺⁰⁴	8.9979 ⁻⁰⁴	4.3486	1.4419	1.1507 ⁺⁰⁴	9.8084 ⁺⁰³	
4.8463 ⁻⁰¹	3.9111 ⁺⁰⁵	1.1734	3.9063 ⁺⁰⁴	NM	1.7438	1.7256	2.8944 ⁺⁰²	1.0756 ⁺⁰²	
INFINITE	3.0832 ⁺⁰²	1.0000	1.4795 ⁻⁰³	1.2832 ⁺⁰⁰	0.0447	2.2585 ⁻⁰³	6.3524 ⁺⁰²	2.8744 ⁺⁰²	
71010307	2.9700	1.0119	1.7702 ⁺⁰⁴	9.1775 ⁻⁰⁴	4.0224	1.4227	1.3032 ⁺⁰⁴	1.1075 ⁺⁰⁴	
5.1079 ⁻⁰¹	3.8889 ⁺⁰⁵	1.1767	4.0567 ⁺⁰⁴	NM	1.7484	1.7308	2.8944 ⁺⁰²	1.1083 ⁺⁰²	
INFINITE	3.0636 ⁺⁰²	1.0000	1.4616 ⁻⁰³	1.2413 ⁺⁰⁰	0.0599	2.1594 ⁻⁰³	6.2690 ⁺⁰²	2.8603 ⁺⁰²	
71010308	2.9000	1.0001	1.8800 ⁺⁰⁴	9.7469 ⁻⁰⁴	4.0561	1.4230	1.4423 ⁺⁰⁴	1.2643 ⁺⁰⁴	
5.3670 ⁻⁰¹	3.9944 ⁺⁰⁵	1.1408	4.1457 ⁺⁰⁴	NM	1.7555	1.7404	2.8944 ⁺⁰²	1.1544 ⁺⁰²	
1.0000 ⁺⁰⁶	3.0962 ⁺⁰²	1.0000	1.4212 ⁻⁰³	1.1108 ⁺⁰⁰	0.0869	2.0863 ⁻⁰³	6.2473 ⁺⁰²	2.8943 ⁺⁰²	
71010401	3.1742	0.9918	1.4189 ⁺⁰⁴	NM	4.0402	1.4845	8.5247 ⁺⁰³	6.9609 ⁺⁰³	
4.8463 ⁻⁰¹	3.3130 ⁺⁰⁵	1.2247	3.4491 ⁺⁰⁴	NM	1.7433	1.7223	2.8700 ⁺⁰²	1.0315 ⁺⁰²	
INFINITE	3.1100 ⁺⁰²	1.0000	1.6667 ⁻⁰³	0.0000 ⁺⁰⁰	0.1077	2.4699 ⁻⁰³	6.4636 ⁺⁰²	2.8938 ⁺⁰²	
71010501	3.1277	1.0272	1.3685 ⁺⁰⁴	NM	4.2527	1.4926	8.5247 ⁺⁰³	7.1511 ⁺⁰³	
4.8463 ⁻⁰¹	3.1775 ⁺⁰⁵	1.1921	3.4480 ⁺⁰⁴	NM	1.7430	1.7232	2.8600 ⁺⁰²	1.0113 ⁺⁰²	
INFINITE	2.9900 ⁺⁰²	1.0000	1.5956 ⁻⁰³	0.0000 ⁺⁰⁰	0.1030	2.4032 ⁻⁰³	6.3064 ⁺⁰²	2.7842 ⁺⁰²	

FREE STREAM DEFINITION ARBITRARY - INPUT TAUM NOT CF - RUN 0401,0501 TOD INPUT

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PD RED2PW	RED2PDW RED2PDW	DATA
71010101	1.3901 ⁻⁰³ 1.3722 ⁻⁰³	6.6601 6.6715	1.8075 1.8044	0.0649 0.0650	1.9184 ⁺⁰⁴ 1.9152 ⁺⁰⁴	6.7382 ⁺⁰³ 6.7266 ⁺⁰³	9.1541 ⁻⁰³
71010102	1.3877 ⁻⁰³ 1.3841 ⁻⁰³	6.7022 6.7053	1.8003 1.7995	0.0569 0.0569	1.9532 ⁺⁰⁴ 1.9524 ⁺⁰⁴	6.7806 ⁺⁰³ 6.7776 ⁺⁰³	9.2611 ⁻⁰³
71010103	1.5415 ⁻⁰³ 1.5061 ⁻⁰³	6.4965 6.7188	1.8091 1.8031	0.0491 0.0493	2.1027 ⁺⁰⁴ 2.0958 ⁺⁰⁴	7.4396 ⁺⁰³ 7.4149 ⁺⁰³	1.0119 ⁻⁰²
71010104	1.6335 ⁻⁰³ 1.4226 ⁻⁰³	5.9865 5.9054	1.7216 1.7453	0.0800 0.0790	2.5865 ⁺⁰⁴ 2.6221 ⁺⁰⁴	1.0087 ⁺⁰⁴ 1.0225 ⁺⁰⁴	8.4536 ⁻⁰³
71010105	1.6071 ⁻⁰³ 1.4265 ⁻⁰³	5.7336 5.6652	1.7229 1.7437	0.0416 0.0411	2.7325 ⁺⁰⁴ 2.7654 ⁺⁰⁴	1.0944 ⁺⁰⁴ 1.1076 ⁺⁰⁴	8.1357 ⁻⁰³
71010106	1.6572 ⁻⁰³ 1.4568 ⁻⁰³	5.1762 5.1539	1.7460 1.7536	0.0433 0.0433	2.9165 ⁺⁰⁴ 2.9291 ⁺⁰⁴	1.2108 ⁺⁰⁴ 1.2160 ⁺⁰⁴	7.5477 ⁻⁰³
71010107	1.5383 ⁻⁰³ 1.3932 ⁻⁰³	5.2187 5.1699	1.7294 1.7457	0.0527 0.0522	2.8856 ⁺⁰⁴ 2.9128 ⁺⁰⁴	1.2483 ⁺⁰⁴ 1.2601 ⁺⁰⁴	7.2426 ⁻⁰³
71010108	1.4631 ⁻⁰³ 1.3711 ⁻⁰³	5.0345 4.9885	1.7337 1.7497	0.0631 0.0625	2.9128 ⁺⁰⁴ 2.9396 ⁺⁰⁴	1.2979 ⁺⁰⁴ 1.3198 ⁺⁰⁴	6.8754 ⁻⁰³
71010201	1.5970 ⁻⁰³ 1.5791 ⁻⁰³	6.6693 6.6813	1.8043 1.8010	0.0643 0.0644	2.4028 ⁺⁰⁴ 2.5980 ⁺⁰⁴	8.4957 ⁺⁰³ 8.4405 ⁺⁰³	9.2148 ⁻⁰³
71010202	1.3226 ⁻⁰³ 1.3227 ⁻⁰³	6.7975 6.7975	1.8009 1.8009	0.0354 0.0354	2.3215 ⁺⁰⁴ 2.3215 ⁺⁰⁴	8.0511 ⁺⁰³ 8.0511 ⁺⁰³	8.9909 ⁻⁰³
71010203	1.4498 ⁻⁰³ 1.4728 ⁻⁰³	6.6898 6.7065	1.8076 1.8031	0.0565 0.0567	2.5425 ⁺⁰⁴ 2.5561 ⁺⁰⁴	9.0523 ⁺⁰³ 9.0298 ⁺⁰³	9.8778 ⁻⁰³
71010204	1.5721 ⁻⁰³ 1.5643 ⁻⁰³	5.9243 5.8503	1.7332 1.7551	0.0783 0.0773	3.0767 ⁺⁰⁴ 3.1156 ⁺⁰⁴	1.2094 ⁺⁰⁴ 1.2247 ⁺⁰⁴	8.0384 ⁻⁰³
71010205	1.5175 ⁻⁰³ 1.3492 ⁻⁰³	5.7213 5.6408	1.7270 1.7517	0.0722 0.0712	3.1928 ⁺⁰⁴ 3.2384 ⁺⁰⁴	1.2914 ⁺⁰⁴ 1.3098 ⁺⁰⁴	7.6757 ⁻⁰³
71010206	1.4578 ⁻⁰³ 1.3145 ⁻⁰³	5.4657 5.4025	1.7344 1.7547	0.0669 0.0661	3.2299 ⁺⁰⁴ 3.2677 ⁺⁰⁴	1.3555 ⁺⁰⁴ 1.3716 ⁺⁰⁴	7.3871 ⁻⁰³
71010207	1.4449 ⁻⁰³ 1.3176 ⁻⁰³	5.2332 5.1671	1.7271 1.7492	0.0662 0.0653	3.3928 ⁺⁰⁴ 3.4362 ⁺⁰⁴	1.4685 ⁺⁰⁴ 1.4873 ⁺⁰⁴	6.8677 ⁻⁰³
71010208	1.3505 ⁻⁰³ 1.2842 ⁻⁰³	5.0036 4.9466	1.7403 1.7605	0.0753 0.0745	3.3831 ⁺⁰⁴ 3.4223 ⁺⁰⁴	1.5166 ⁺⁰⁴ 1.5341 ⁺⁰⁴	6.3955 ⁻⁰³
71010301	1.3424 ⁻⁰³ 1.3260 ⁻⁰³	6.5711 6.5839	1.8139 1.8104	0.0682 0.0683	2.7622 ⁺⁰⁴ 2.7568 ⁺⁰⁴	9.7367 ⁺⁰³ 9.7177 ⁺⁰³	8.7302 ⁻⁰³
71010302	1.3064 ⁻⁰³ 1.3031 ⁻⁰³	6.7755 6.7752	1.8016 1.8016	0.0526 0.0526	2.7219 ⁺⁰⁴ 2.7221 ⁺⁰⁴	9.4951 ⁺⁰³ 9.4955 ⁺⁰³	0.8286 ⁻⁰³
71010303	1.3878 ⁻⁰³ 1.3667 ⁻⁰³	6.5930 6.6040	1.8152 1.8117	0.0720 0.0721	2.8386 ⁺⁰⁴ 2.8310 ⁺⁰⁴	1.0049 ⁺⁰⁴ 1.0029 ⁺⁰⁴	9.0284 ⁻⁰³
71010304	1.5106 ⁻⁰³ 1.5141 ⁻⁰³	5.8868 5.8186	1.7427 1.7632	0.0725 0.0717	3.5388 ⁺⁰⁴ 3.5801 ⁺⁰⁴	1.3953 ⁺⁰⁴ 1.4117 ⁺⁰⁴	7.7104 ⁻⁰³
71010305	1.4817 ⁻⁰³ 1.3131 ⁻⁰³	5.6109 5.5521	1.7413 1.7598	0.0579 0.0572	3.7150 ⁺⁰⁴ 3.7544 ⁺⁰⁴	1.5150 ⁺⁰⁴ 1.5310 ⁺⁰⁴	7.3613 ⁻⁰³
71010306	1.4040 ⁻⁰³ 1.2701 ⁻⁰³	5.5888 5.5189	1.7305 1.7524	0.0471 0.0465	3.7117 ⁺⁰⁴ 3.7582 ⁺⁰⁴	1.5741 ⁺⁰⁴ 1.5940 ⁺⁰⁴	7.0744 ⁻⁰³
71010307	1.4421 ⁻⁰³ 1.2971 ⁻⁰³	5.0473 5.0068	1.7451 1.7594	0.0607 0.0602	4.0076 ⁺⁰⁴ 4.0404 ⁺⁰⁴	1.7488 ⁺⁰⁴ 1.7630 ⁺⁰⁴	6.5486 ⁻⁰³
71010308	1.3330 ⁻⁰³ 1.2341 ⁻⁰³	5.0658 5.0161	1.7400 1.7441	0.0927 0.0914	3.8932 ⁺⁰⁴ 3.9473 ⁺⁰⁴	1.7654 ⁺⁰⁴ 1.7900 ⁺⁰⁴	6.2376 ⁻⁰³
71010401	1.5533 ⁻⁰³ 1.3949 ⁻⁰³	5.5232 5.4408	1.7253 1.7514	0.1156 0.1138	3.2181 ⁺⁰⁴ 3.2668 ⁺⁰⁴	1.3201 ⁺⁰⁴ 1.3401 ⁺⁰⁴	7.5978 ⁻⁰³
71010501	1.5066 ⁻⁰³ 1.3648 ⁻⁰³	5.4747 5.4022	1.7284 1.7516	0.1091 0.1077	3.2522 ⁺⁰⁴ 3.2959 ⁺⁰⁴	1.3127 ⁺⁰⁴ 1.3303 ⁺⁰⁴	7.4326 ⁻⁰³

71010201

STUREK

PROFILE TABULATION

70 POINTS, DELTA AT POINT 69

I	Y	PT2/P	P/PD	T0/T0D	A/1/D	U/UD	T/1/D	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	1.00006	0.94300	0.00000	0.00000	3.26650	0.00000
2	0.8900*-05	1.3862*+00	1.00000	0.94440	0.19922	0.34391	2.97997	0.11541
3	1.9050*-04	1.7600*+00	1.00000	0.94537	0.26084	0.44539	2.78596	0.15997
4	2.7940*-04	2.0674*+00	1.00000	0.94606	0.30603	0.49938	2.60270	0.18755
5	3.8100*-04	2.3029*+00	1.00000	0.94792	0.33142	0.52996	2.55695	0.20726
6	0.5024*-04	2.5836*+00	1.00100	0.94813	0.35861	0.56274	2.46245	0.22853
7	9.4996*-04	2.8087*+00	1.00000	0.94761	0.37869	0.58866	2.39987	0.24445
8	1.1989*-03	3.0077*+00	1.00000	0.94800	0.39546	0.60629	2.35044	0.25795
9	1.4529*-03	3.2465*+00	1.00000	0.94850	0.41457	0.62818	2.29599	0.27360
10	1.7069*-03	3.4349*+00	1.00000	0.94895	0.42098	0.64432	2.25594	0.28561
11	2.2149*-03	3.6809*+00	1.00000	0.94924	0.44703	0.66460	2.21026	0.30069
12	2.7229*-03	3.9755*+00	1.00000	0.94962	0.46766	0.68626	2.15332	0.31870
13	3.2309*-03	4.2749*+00	1.00000	0.95012	0.48768	0.70621	2.09700	0.33677
14	3.7389*-03	4.4053*+00	1.00000	0.95099	0.50252	0.72061	2.05032	0.35043
15	4.2469*-03	4.8297*+00	1.00000	0.95170	0.52267	0.73904	1.99437	0.36964
16	4.7549*-03	5.0827*+00	1.00000	0.95244	0.53783	0.75247	1.95745	0.38441
17	5.2629*-03	5.3658*+00	1.00000	0.95270	0.55427	0.76640	1.91176	0.40089
18	5.7709*-03	5.6498*+00	1.00000	0.95208	0.57012	0.77974	1.86621	0.41715
19	6.2789*-03	5.8783*+00	1.00000	0.95442	0.58289	0.79009	1.83730	0.43003
20	6.7869*-03	6.2152*+00	1.00000	0.95707	0.60092	0.80420	1.79099	0.44903
21	7.2949*-03	6.4342*+00	1.00000	0.95933	0.61751	0.81664	1.74896	0.46692
22	7.8029*-03	6.8030*+00	1.00000	0.96153	0.63113	0.82673	1.71589	0.48181
23	8.3109*-03	7.1724*+00	1.00000	0.96391	0.64939	0.83956	1.67146	0.50229
24	8.8189*-03	7.4259*+00	1.00000	0.96570	0.66162	0.84798	1.64268	0.51622
25	9.3269*-03	7.7907*+00	1.00000	0.96758	0.67883	0.85920	1.60200	0.53633
26	9.8349*-03	8.1270*+00	1.00000	0.96967	0.69432	0.86913	1.56696	0.55460
27	1.03343*-02	8.4615*+00	1.00000	0.97141	0.70937	0.87837	1.53317	0.57291
28	1.0851*-02	8.8447*+00	1.00000	0.97327	0.72025	0.88813	1.49025	0.59372
29	1.1359*-02	9.1625*+00	1.00000	0.97514	0.73994	0.89635	1.46746	0.61082
30	1.1867*-02	9.4635*+00	1.00000	0.97674	0.75686	0.90564	1.43179	0.63252
31	1.2375*-02	9.9195*+00	1.00000	0.97825	0.77157	0.91351	1.40175	0.65164
32	1.2883*-02	1.0277*+01	1.00000	0.97936	0.78607	0.92086	1.37234	0.67102
33	1.3391*-02	1.0678*+01	1.00000	1.00025	0.80201	0.92854	1.34043	0.69272
34	1.3899*-02	1.1003*+01	1.00000	1.00125	0.81470	0.93461	1.31102	0.71018
35	1.4407*-02	1.1426*+01	1.00000	1.00185	0.83093	0.94183	1.28473	0.73110
36	1.4915*-02	1.1750*+01	1.00000	1.00264	0.84315	0.94724	1.26220	0.75048
37	1.5423*-02	1.2087*+01	1.00000	1.00298	0.85566	0.95245	1.23905	0.76870
38	1.5931*-02	1.2485*+01	1.00000	1.00339	0.87022	0.95837	1.21277	0.79021
39	1.6439*-02	1.2750*+01	1.00000	1.00360	0.87976	0.96206	1.19587	0.80444
40	1.6947*-02	1.3091*+01	1.00000	1.00376	0.89193	0.96666	1.17454	0.82298
41	1.7455*-02	1.3388*+01	1.00000	1.00422	0.90238	0.97066	1.15707	0.83890
42	1.7963*-02	1.3646*+01	1.00000	1.00440	0.91135	0.97393	1.14205	0.85274
43	1.8471*-02	1.3946*+01	1.00000	1.00413	0.92167	0.97738	1.12453	0.86914
44	1.8979*-02	1.4176*+01	1.00000	1.00386	0.92950	0.97991	1.11134	0.88164
45	1.9487*-02	1.4396*+01	1.00000	1.00350	0.93611	0.98243	1.09950	0.89353
46	1.9995*-02	1.4616*+01	1.00000	1.00387	0.94433	0.98483	1.08761	0.90550
47	2.0503*-02	1.4794*+01	1.00000	1.00380	0.95025	0.98671	1.07822	0.91513
48	2.1011*-02	1.4999*+01	1.00000	1.00313	0.95703	0.98855	1.06696	0.92651
49	2.1519*-02	1.5143*+01	1.00000	1.00291	0.96175	0.98993	1.05445	0.93438
50	2.2027*-02	1.5294*+01	1.00000	1.00294	0.96671	0.99144	1.05194	0.94254
51	2.2535*-02	1.5437*+01	1.00000	1.00246	0.97134	0.99264	1.04443	0.95046
52	2.3043*-02	1.5535*+01	1.00000	1.00225	0.97454	0.99356	1.03942	0.95888
53	2.3551*-02	1.5675*+01	1.00000	1.00209	0.97905	0.99485	1.03254	0.96350
54	2.4059*-02	1.5774*+01	1.00000	1.00181	0.98225	0.99568	1.02753	0.96900
55	2.4567*-02	1.5857*+01	1.00000	1.00133	0.98487	0.99623	1.02315	0.97368
56	2.5075*-02	1.5935*+01	1.00000	1.00122	0.98789	0.99692	1.01940	0.97795
57	2.5583*-02	1.6035*+01	1.00000	1.00080	0.99060	0.99770	1.01439	0.98354
58	2.6091*-02	1.6091*+01	1.00000	1.00095	0.99237	0.99825	1.01189	0.98852
59	2.6599*-02	1.6137*+01	1.00000	1.00055	0.99383	0.99848	1.00939	0.99420
60	2.7107*-02	1.6174*+01	1.00000	1.00034	0.99498	0.99871	1.00751	0.99927
61	2.7615*-02	1.6210*+01	1.00000	1.00012	0.99614	0.99894	1.00563	0.99335
62	2.8123*-02	1.6251*+01	1.00000	1.00010	0.99744	0.99931	1.00375	0.99557
63	2.8631*-02	1.6275*+01	1.00000	1.00058	0.99821	0.99977	1.00113	0.99665
64	2.9139*-02	1.6298*+01	1.00000	1.00035	0.99892	0.99986	1.00188	0.99799
65	2.9647*-02	1.6314*+01	1.00000	0.99979	0.99941	0.99972	1.00063	0.99910
66	3.0155*-02	1.6326*+01	1.00000	0.99974	0.99982	0.99982	1.00000	0.99982
67	3.0663*-02	1.6321*+01	1.00000	1.00012	0.99964	0.99995	1.00063	0.99933
68	3.1171*-02	1.6334*+01	1.00000	1.00007	0.99905	1.00005	1.00000	1.00005
69	3.1679*-02	1.6332*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
70	3.2187*-02	1.6327*+01	1.00000	1.00038	0.99983	1.00014	1.00063	0.99951

INPUT VARIABLES Y,U,T,P

71010202	STUREK	PROFILE TABULATION	70 POINTS, DELTA AT POINT 70					
I	Y	R1Z/P	P/PD	T0/T0D	A/A0	U/U0	T/T0	RHO/RHO0*U/U0
1	0.0000+00	1.0000+00	1.00003	0.94583	0.00000	0.00000	3.31639	0.00000
2	1.1938+04	1.5378+00	1.00000	0.94602	0.22847	0.39130	2.93329	0.13340
3	2.2078+04	1.9524+00	1.00000	0.94722	0.28992	0.48020	2.74333	0.17504
4	3.9878+04	2.4278+00	1.00000	0.93967	0.34095	0.54461	2.55146	0.21345
5	5.4102+04	2.8250+00	1.00000	0.93894	0.35933	0.56671	2.48729	0.22784
6	6.7056+04	2.7663+00	1.00000	0.93908	0.37183	0.58146	2.44536	0.23778
7	8.1026+04	2.8992+00	1.00000	0.93940	0.38315	0.59455	2.40788	0.24692
8	9.2964+04	3.0704+00	1.00000	0.94003	0.39209	0.60480	2.37429	0.25419
9	1.1806+03	3.1964+00	1.00000	0.94205	0.40716	0.62198	2.33355	0.26054
10	1.4046+03	3.3616+00	1.00000	0.94492	0.41985	0.63645	2.29797	0.27096
11	1.6506+03	3.6107+00	1.00000	0.94879	0.43821	0.65671	2.24587	0.29241
12	2.1666+03	3.8933+00	1.00000	0.95445	0.45809	0.67840	2.19314	0.30433
13	2.6746+03	4.1512+00	1.00000	0.95829	0.47595	0.69832	2.14485	0.32464
14	3.1826+03	4.4047+00	1.00000	0.96258	0.49189	0.71299	2.10102	0.33936
15	3.6906+03	4.6998+00	1.00000	0.96818	0.51033	0.73027	2.04765	0.35664
16	4.1986+03	4.9030+00	1.00000	0.96767	0.52268	0.74175	2.01398	0.36830
17	4.7066+03	5.1900+00	1.00000	0.96992	0.53952	0.75655	1.96633	0.38475
18	5.2146+03	5.4356+00	1.00000	0.97161	0.55355	0.76840	1.92694	0.39877
19	5.7226+03	5.6775+00	1.00000	0.97407	0.56701	0.77979	1.89136	0.41229
20	6.2306+03	5.9982+00	1.00000	0.97621	0.58436	0.79362	1.84435	0.43030
21	6.7386+03	6.2399+00	1.00000	0.97857	0.59712	0.80378	1.81194	0.44360
22	7.2466+03	6.6023+00	1.00000	0.98093	0.61572	0.81777	1.76360	0.46364
23	7.7546+03	6.9019+00	1.00000	0.98345	0.63068	0.82877	1.72081	0.47994
24	8.2626+03	7.1440+00	1.00000	0.98582	0.64251	0.83745	1.69486	0.49295
25	8.7706+03	7.4783+00	1.00000	0.98725	0.65849	0.84811	1.65583	0.51127
26	9.2786+03	7.7834+00	1.00000	0.98924	0.67274	0.85762	1.62716	0.52772
27	9.7866+03	8.1737+00	1.00000	0.99117	0.69054	0.86888	1.58833	0.54880
28	1.0295+02	8.5271+00	1.00000	0.99279	0.70626	0.87843	1.54701	0.56783
29	1.0803+02	8.8220+00	1.00000	0.99478	0.71974	0.88634	1.51906	0.58348
30	1.1311+02	9.2477+00	1.00000	0.99648	0.73726	0.89663	1.47403	0.60623
31	1.1819+02	9.4961+00	1.00000	0.99800	0.74765	0.90260	1.45743	0.61931
32	1.2327+02	9.8894+00	1.00000	0.99935	0.76381	0.91119	1.42313	0.64027
33	1.2835+02	1.0355+01	1.00000	1.00075	0.78252	0.92070	1.38437	0.66507
34	1.3343+02	1.0886+01	1.00000	1.00231	0.79551	0.92736	1.35896	0.68241
35	1.3851+02	1.1130+01	1.00000	1.00310	0.81265	0.93531	1.32465	0.70608
36	1.4359+02	1.1436+01	1.00000	1.00397	0.82427	0.94089	1.30241	0.72220
37	1.4867+02	1.1837+01	1.00000	1.00505	0.83920	0.94740	1.27446	0.74337
38	1.5375+02	1.2197+01	1.00000	1.00547	0.85242	0.95291	1.24968	0.76252
39	1.5883+02	1.2560+01	1.00000	1.00580	0.86554	0.95817	1.22554	0.78185
40	1.6391+02	1.2949+01	1.00000	1.00619	0.87973	0.96375	1.20013	0.80301
41	1.6899+02	1.3208+01	1.00000	1.00647	0.88946	0.96710	1.18488	0.81624
42	1.7407+02	1.3569+01	1.00000	1.00674	0.90097	0.97174	1.16328	0.83535
43	1.7915+02	1.3849+01	1.00000	1.00670	0.91057	0.97510	1.14676	0.85031
44	1.8423+02	1.4090+01	1.00000	1.00650	0.91872	0.97781	1.13278	0.86319
45	1.8931+02	1.4411+01	1.00000	1.00657	0.92950	0.98148	1.11499	0.88026
46	1.9439+02	1.4615+01	1.00000	1.00621	0.93627	0.98355	1.10356	0.89126
47	1.9947+02	1.4858+01	1.00000	1.00584	0.94431	0.98509	1.09422	0.90440
48	2.0455+02	1.5100+01	1.00000	1.00565	0.95221	0.98832	1.07751	0.91732
49	2.0963+02	1.5263+01	1.00000	1.00506	0.96750	0.98980	1.06681	0.92625
50	2.1471+02	1.5450+01	1.00000	1.00527	0.96380	0.99187	1.05409	0.93655
51	2.1979+02	1.5582+01	1.00000	1.00503	0.96778	0.99297	1.05273	0.94323
52	2.2487+02	1.5745+01	1.00000	1.00469	0.97299	0.99439	1.04447	0.95205
53	2.2995+02	1.5887+01	1.00000	1.00419	0.97647	0.99531	1.03812	0.95877
54	2.3503+02	1.5948+01	1.00000	1.00421	0.97944	0.99600	1.03431	0.96305
55	2.4011+02	1.6063+01	1.00000	1.00389	0.98306	0.99701	1.02859	0.96930
56	2.4519+02	1.6144+01	1.00000	1.00385	0.98561	0.99775	1.02478	0.97362
57	2.5027+02	1.6229+01	1.00000	1.00337	0.98830	0.99830	1.02033	0.97841
58	2.5535+02	1.6303+01	1.00000	1.00294	0.99061	0.99876	1.01652	0.98253
59	2.6043+02	1.6350+01	1.00000	1.00254	0.99208	0.99899	1.01396	0.98572
60	2.6551+02	1.6423+01	1.00000	1.00269	0.99437	0.99972	1.01180	0.98904
61	2.7059+02	1.6474+01	1.00000	1.00242	0.99594	1.00005	1.00876	0.99185
62	2.7567+02	1.6513+01	1.00000	1.00227	0.99716	1.00032	1.00635	0.99401
63	2.8075+02	1.6507+01	1.00000	1.00201	0.99608	1.00014	1.00635	0.99382
64	2.8583+02	1.6546+01	1.00000	1.00186	0.99820	1.00041	1.00445	0.99598
65	2.9091+02	1.6551+01	1.00000	1.00206	0.99933	1.00095	1.00445	0.99612
66	2.9599+02	1.6593+01	1.00000	1.00204	0.99965	1.00092	1.00254	0.99838
67	3.0107+02	1.6585+01	1.00000	1.00043	0.99941	1.00005	1.00127	0.99878
68	3.0615+02	1.6585+01	1.00000	1.00043	0.99941	1.00005	1.00127	0.99878
69	3.1123+02	1.6596+01	1.00000	1.00025	0.99973	1.00005	1.00064	0.99941
0 70	3.1631+02	1.6604+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y, U, T, P

71010203 STUREK		PROFILE TABULATION		70 POINTS, DELTA AT POINT 70				
I	Y	PT2/P	P/PD	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	1.00007	0.94329	0.00000	0.00000	3.25436	0.00000
2	1.2954-04	1.4341+00	1.00000	0.94469	0.21045	0.36005	2.94015	0.12273
3	1.3970-04	1.4935+00	1.00000	0.94476	0.22262	0.37954	2.90648	0.13058
4	2.3876-04	1.7990+00	1.00000	0.94421	0.27306	0.45317	2.75436	0.16453
5	5.5118-04	2.5847+00	1.00000	0.93820	0.35973	0.56395	2.45761	0.22947
6	8.6900-04	2.9491+00	1.00000	0.93789	0.39173	0.60072	2.35162	0.25545
7	1.1100-03	3.1197+00	1.00000	0.93977	0.40571	0.61669	2.31047	0.26691
8	1.3589-03	3.3035+00	1.00000	0.94230	0.42019	0.63298	2.26933	0.27893
9	1.5129-03	3.4919+00	1.00000	0.94506	0.43447	0.64899	2.23130	0.29086
10	2.1209-03	3.6507+00	1.00000	0.95003	0.44613	0.66248	2.20511	0.30043
11	2.6289-03	3.8970+00	1.00000	0.95556	0.46358	0.68126	2.15966	0.31545
12	3.1369-03	4.1623+00	1.00000	0.95933	0.48163	0.69966	2.11035	0.33154
13	3.6449-03	4.4080+00	1.00000	0.96264	0.49773	0.71554	2.06671	0.34622
14	4.1529-03	4.6511+00	1.00000	0.96528	0.51314	0.73008	2.02431	0.36066
15	4.6609-03	4.9042+00	1.00000	0.96695	0.52869	0.74394	1.98005	0.37572
16	5.1689-03	5.1598+00	1.00000	0.96935	0.54392	0.75737	1.93690	0.39062
17	5.6769-03	5.3290+00	1.00000	0.97125	0.55376	0.76598	1.91334	0.40034
18	6.1849-03	5.5976+00	1.00000	0.97349	0.56903	0.77873	1.87282	0.41581
19	6.6929-03	5.8535+00	1.00000	0.97598	0.58320	0.79037	1.83666	0.43033
20	7.2009-03	6.1158+00	1.00000	0.97815	0.59716	0.80156	1.80050	0.44519
21	7.7089-03	6.3790+00	1.00000	0.98095	0.61124	0.81232	1.76621	0.45993
22	8.2169-03	6.6728+00	1.00000	0.98275	0.62635	0.82355	1.72880	0.47637
23	8.7249-03	6.9575+00	1.00000	0.98471	0.64066	0.83382	1.69389	0.49225
24	9.2329-03	7.2494+00	1.00000	0.98667	0.65500	0.84380	1.65960	0.50844
25	9.7409-03	7.5756+00	1.00000	0.98872	0.67065	0.85434	1.62282	0.52646
26	1.0249-02	7.9162+00	1.00000	0.99070	0.68661	0.86470	1.58603	0.54519
27	1.0757-02	8.2026+00	1.00000	0.99213	0.69974	0.87289	1.55611	0.56094
28	1.1265-02	8.5524+00	1.00000	0.99389	0.71545	0.88242	1.52120	0.58008
29	1.1773-02	8.8742+00	1.00000	0.99558	0.72961	0.89079	1.49065	0.59759
30	1.2281-02	9.2195+00	1.00000	0.99707	0.74449	0.89921	1.45885	0.61638
31	1.2789-02	9.5423+00	1.00000	0.99873	0.75814	0.90665	1.43080	0.63381
32	1.3297-02	9.8770+00	1.00000	0.99988	0.77203	0.91417	1.40212	0.65199
33	1.3805-02	1.0243+01	1.00000	1.00117	0.78693	0.92181	1.37219	0.67178
34	1.4313-02	1.0574+01	1.00000	1.00217	0.80018	0.92834	1.34661	0.68970
35	1.4821-02	1.0929+01	1.00000	1.00286	0.81415	0.93488	1.31858	0.70901
36	1.5329-02	1.1295+01	1.00000	1.00380	0.82830	0.94141	1.29177	0.72878
37	1.5837-02	1.1646+01	1.00000	1.00447	0.84165	0.94731	1.26683	0.74777
38	1.6345-02	1.1972+01	1.00000	1.00492	0.85382	0.95246	1.24439	0.76540
39	1.6853-02	1.2288+01	1.00000	1.00527	0.86552	0.95725	1.22319	0.78258
40	1.7361-02	1.2624+01	1.00000	1.00553	0.87775	0.96208	1.20137	0.80082
41	1.7869-02	1.3002+01	1.00000	1.00523	0.89131	0.96700	1.17766	0.82154
42	1.8377-02	1.3246+01	1.00000	1.00520	0.89993	0.97013	1.16209	0.83481
43	1.8885-02	1.3563+01	1.00000	1.00480	0.91104	0.97391	1.14277	0.85223
44	1.9393-02	1.3811+01	1.00000	1.00429	0.91966	0.97667	1.12781	0.86999
45	1.9901-02	1.4060+01	1.00000	1.00454	0.92819	0.97970	1.11409	0.89388
46	2.0409-02	1.4278+01	1.00000	1.00413	0.93562	0.98201	1.10162	0.89142
47	2.0917-02	1.4492+01	1.00000	1.00388	0.94285	0.98426	1.08978	0.90318
48	2.1425-02	1.4651+01	1.00000	1.00357	0.94820	0.98587	1.08105	0.91196
49	2.1933-02	1.4837+01	1.00000	1.00326	0.95438	0.98771	1.07107	0.92217
50	2.2441-02	1.4962+01	1.00000	1.00282	0.95852	0.98862	1.06421	0.92915
51	2.2949-02	1.5116+01	1.00000	1.00254	0.96362	0.99029	1.05611	0.93768
52	2.3457-02	1.5275+01	1.00000	1.00233	0.96883	0.99181	1.04800	0.94638
53	2.3965-02	1.5369+01	1.00000	1.00198	0.97191	0.99259	1.04302	0.95165
54	2.4473-02	1.5490+01	1.00000	1.00224	0.97584	0.99393	1.03741	0.95809
55	2.4981-02	1.5587+01	1.00000	1.00196	0.97901	0.99475	1.03242	0.96332
56	2.5489-02	1.5652+01	1.00000	1.00134	0.98111	0.99508	1.02868	0.96733
57	2.5997-02	1.5715+01	1.00000	1.00121	0.98314	0.99563	1.02556	0.97081
58	2.6505-02	1.5836+01	1.00000	1.00128	0.98703	0.99682	1.01995	0.97333
59	2.7013-02	1.5934+01	1.00000	1.00088	0.99018	0.99756	1.01496	0.98285
60	2.7521-02	1.5987+01	1.00000	1.00071	0.99093	0.99770	1.01372	0.98420
61	2.8029-02	1.6019+01	1.00000	1.00046	0.99291	0.99816	1.01060	0.98769
62	2.8537-02	1.6041+01	1.00000	1.00023	0.99362	0.99825	1.00935	0.98900
63	2.9045-02	1.6090+01	1.00000	0.99996	0.99517	0.99857	1.00686	0.99177
64	2.9553-02	1.6117+01	1.00000	0.99993	0.99601	0.99880	1.00561	0.99323
65	3.0061-02	1.6145+01	1.00000	0.99996	0.99691	0.99908	1.00436	0.99474
66	3.0569-02	1.6163+01	1.00000	0.99953	0.99748	0.99903	1.00312	0.99593
67	3.1077-02	1.6206+01	1.00000	0.99964	0.99887	0.99944	1.00125	0.99825
68	3.1585-02	1.6225+01	1.00000	0.99946	0.99946	0.99977	1.00062	0.99915
69	3.2093-02	1.6219+01	1.00000	0.99959	0.99927	0.99959	1.00062	0.99996
D 70	3.2601-02	1.6242+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U,T,P

71010204		STUREK	PROFILE TABULATION			66 POINTS, DELTA AT POINT 50			
I	Y	PTZ/P	P/PD	T0/T00	M/M0	U/UD	T/T0	RHO/RH00*U/UD	
1	0.0000+00	1.0000+00	1.23334	0.94230	0.00000	0.00000	2.91457	0.00000	
2	1.7272+04	1.5464+00	1.23316	0.94196	0.25175	0.40374	2.57231	0.19356	
3	1.9304+04	1.6235+00	1.23305	0.94186	0.26635	0.42421	2.53657	0.20621	
4	2.6416+04	1.7914+00	1.23305	0.94058	0.29427	0.46181	2.46287	0.23121	
5	3.7338+04	1.9264+00	1.23282	0.93917	0.31374	0.48692	2.40871	0.24922	
6	4.7496+04	2.0187+00	1.23271	0.93944	0.32541	0.50186	2.37856	0.26009	
7	5.6674+04	2.0975+00	1.23260	0.93997	0.33576	0.51496	2.35232	0.26984	
8	7.1628+04	2.1884+00	1.23237	0.94135	0.34659	0.52867	2.32663	0.28003	
9	8.0772+04	2.2356+00	1.23226	0.94233	0.35204	0.53555	2.31435	0.28515	
10	1.0312+03	2.3544+00	1.23203	0.94562	0.36524	0.55228	2.28643	0.29759	
11	1.2624+03	2.4655+00	1.23170	0.94816	0.37704	0.56884	2.26019	0.30890	
12	1.4961+03	2.5630+00	1.23102	0.95011	0.38703	0.57890	2.23730	0.31853	
13	2.0041+03	2.7866+00	1.22914	0.95369	0.40881	0.60434	2.18537	0.33999	
14	2.5121+03	2.9560+00	1.22787	0.95630	0.42444	0.62206	2.14796	0.35560	
15	3.0201+03	3.1451+00	1.22629	0.95826	0.44114	0.64020	2.10609	0.37276	
16	3.5281+03	3.3105+00	1.22449	0.96016	0.45519	0.65514	2.07147	0.38727	
17	4.0361+03	3.5243+00	1.22269	0.96221	0.47266	0.67309	2.02792	0.40582	
18	4.5441+03	3.7236+00	1.22088	0.96395	0.48834	0.68869	1.98883	0.42276	
19	5.0521+03	3.9416+00	1.21784	0.96615	0.50490	0.70480	1.94863	0.44048	
20	5.5601+03	4.1615+00	1.21469	0.96900	0.52103	0.72030	1.91122	0.45779	
21	6.0681+03	4.4386+00	1.21153	0.97119	0.54063	0.73807	1.86376	0.47978	
22	6.5761+03	4.6779+00	1.20782	0.97328	0.55698	0.75249	1.82524	0.49794	
23	7.0841+03	4.9752+00	1.20342	0.97598	0.57662	0.76931	1.78001	0.52011	
24	7.5921+03	5.2623+00	1.19914	0.97890	0.59495	0.78462	1.73425	0.54096	
25	8.1001+03	5.5930+00	1.19441	0.98098	0.61549	0.80069	1.69135	0.56510	
26	8.6081+03	5.8870+00	1.18968	0.98338	0.63295	0.81812	1.65438	0.58544	
27	9.1161+03	6.2544+00	1.18566	0.98574	0.65430	0.82971	1.60804	0.61147	
28	9.6241+03	6.5991+00	1.17966	0.98793	0.67330	0.84328	1.56328	0.63472	
29	1.0132+02	6.9526+00	1.17335	0.99018	0.69288	0.85638	1.52764	0.65777	
30	1.0640+02	7.3257+00	1.16715	0.99209	0.71265	0.86915	1.48744	0.68200	
31	1.1148+02	7.7016+00	1.16085	0.99421	0.73202	0.88131	1.44947	0.70582	
32	1.1656+02	8.1416+00	1.15431	0.99629	0.75406	0.89445	1.40704	0.73380	
33	1.2164+02	8.5269+00	1.14778	0.99799	0.77283	0.90501	1.37130	0.75749	
34	1.2672+02	8.8610+00	1.14125	0.99946	0.78875	0.91401	1.34283	0.77680	
35	1.3180+02	9.3622+00	1.13460	1.00154	0.81204	0.92660	1.30151	0.80760	
36	1.3688+02	9.7720+00	1.12807	1.00234	0.83059	0.93549	1.26657	0.83189	
37	1.4196+02	1.0216+01	1.11906	1.00302	0.85024	0.94468	1.23451	0.85634	
38	1.4704+02	1.0653+01	1.10993	1.00356	0.86910	0.95312	1.20268	0.87962	
39	1.5212+02	1.1079+01	1.10081	1.00400	0.88713	0.96084	1.17309	0.90164	
40	1.5720+02	1.1449+01	1.09203	1.00436	0.90250	0.96721	1.14852	0.91963	
41	1.6228+02	1.1836+01	1.08335	1.00477	0.91831	0.97357	1.12395	0.93040	
42	1.6736+02	1.2152+01	1.07457	1.00431	0.93099	0.97814	1.10385	0.95219	
43	1.7244+02	1.2476+01	1.06578	1.00369	0.94384	0.98257	1.08375	0.96627	
44	1.7752+02	1.2797+01	1.05699	1.00323	0.95482	0.98629	1.06700	0.97704	
45	1.8260+02	1.3032+01	1.04753	1.00253	0.96546	0.98968	1.05081	0.98660	
46	1.8768+02	1.3249+01	1.03796	1.00216	0.97379	0.99237	1.03853	0.99183	
47	1.9276+02	1.3404+01	1.02838	1.00196	0.97967	0.99406	1.02959	0.99290	
48	1.9784+02	1.3632+01	1.01870	1.00127	0.98820	0.99680	1.01731	0.99816	
49	2.0292+02	1.3787+01	1.00935	1.00035	0.99410	0.99826	1.00838	0.99922	
50	2.0800+02	1.3946+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
51	2.1308+02	1.4019+01	0.99054	0.99976	1.00272	1.00075	0.99609	0.99517	
52	2.1816+02	1.4168+01	0.98051	0.99877	1.00824	1.00203	0.98772	0.99472	
53	2.2324+02	1.4272+01	0.96959	0.99825	1.01205	1.00297	0.98213	0.99016	
54	2.2832+02	1.4409+01	0.95866	0.99813	1.01705	1.00448	0.97543	0.98721	
55	2.3340+02	1.4483+01	0.94762	0.99776	1.01976	1.00514	0.97152	0.98041	
56	2.3848+02	1.4560+01	0.93670	0.99722	1.02278	1.00590	0.96706	0.97422	
57	2.4356+02	1.4678+01	0.92577	0.99745	1.02684	1.00716	0.96203	0.96920	
58	2.4864+02	1.4733+01	0.91485	0.99776	1.02881	1.00792	0.95980	0.96471	
59	2.5372+02	1.4869+01	0.90392	0.99733	1.03372	1.00919	0.95310	0.95711	
60	2.5880+02	1.4912+01	0.89288	0.99706	1.03527	1.00952	0.95087	0.94796	
61	2.6388+02	1.4985+01	0.88196	0.99700	1.03788	1.01027	0.94752	0.94037	
62	2.6896+02	1.5057+01	0.87171	0.99689	1.04044	1.01098	0.94417	0.93339	
63	2.7404+02	1.5126+01	0.86236	0.99664	1.04292	1.01159	0.94082	0.92723	
64	2.7912+02	1.5189+01	0.85289	0.99721	1.04514	1.01253	0.93850	0.92010	
65	2.8420+02	1.5265+01	0.84355	0.99786	1.04786	1.01366	0.93579	0.91374	
66	2.8928+02	1.5374+01	0.83273	0.99750	1.05171	1.01465	0.93076	0.90779	

INPUT VARIABLES Y,U,T,P

71010205		STUREK	PROFILE TABULATION			64 POINTS, DELTA AT POINT 47			
I	Y	P12/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.21230	0.94360	0.00000	0.00000	2.82927	0.00000	
2	1.2192*-04	1.5841*+00	1.21204	0.94234	0.26512	0.41730	2.47751	0.20415	
3	1.6256*-04	1.6940*+00	1.21204	0.94229	0.26518	0.44458	2.43035	0.22172	
4	2.0320*-04	1.7671*+00	1.21194	0.94183	0.29732	0.46060	2.40000	0.23259	
5	3.2512*-04	1.8967*+00	1.21165	0.94045	0.31690	0.48565	2.34851	0.25056	
6	4.7752*-04	2.0239*+00	1.21145	0.94153	0.33423	0.50775	2.30786	0.26653	
7	5.3848*-04	2.0875*+00	1.21125	0.94218	0.34236	0.51797	2.28889	0.27410	
8	6.0264*-04	2.2451*+00	1.21076	0.94505	0.36138	0.54173	2.24715	0.29188	
9	1.0160*-03	2.3502*+00	1.21037	0.94849	0.37333	0.55680	2.22439	0.30297	
10	1.5240*-03	2.4695*+00	1.20949	0.95338	0.39676	0.58508	2.17453	0.32542	
11	2.0320*-03	2.7499*+00	1.20704	0.95739	0.41443	0.60585	2.13713	0.34218	
12	2.5400*-03	2.9187*+00	1.20469	0.95916	0.43092	0.62410	2.09756	0.35844	
13	3.0480*-03	3.0958*+00	1.20233	0.96104	0.44708	0.64154	2.05908	0.37461	
14	3.5560*-03	3.2745*+00	1.19988	0.96254	0.46276	0.65789	2.02114	0.39057	
15	4.0640*-03	3.4570*+00	1.19674	0.96444	0.47817	0.67367	1.98482	0.40619	
16	4.5720*-03	3.6394*+00	1.19361	0.96611	0.49306	0.68845	1.94959	0.42149	
17	5.0800*-03	3.8220*+00	1.19037	0.96790	0.50750	0.70247	1.91599	0.43643	
18	5.5880*-03	4.0039*+00	1.18724	0.97037	0.52446	0.71863	1.87751	0.45442	
19	6.0960*-03	4.2921*+00	1.18410	0.97271	0.54277	0.73541	1.83577	0.47435	
20	6.6040*-03	4.6025*+00	1.18086	0.97474	0.56480	0.75456	1.78482	0.49923	
21	7.1120*-03	4.8987*+00	1.17616	0.97742	0.58501	0.77177	1.74038	0.52157	
22	7.6200*-03	5.1714*+00	1.17136	0.97942	0.60300	0.78641	1.70081	0.54160	
23	8.1280*-03	5.4708*+00	1.16655	0.98291	0.62213	0.80200	1.66179	0.56299	
24	8.6360*-03	5.8367*+00	1.16185	0.98519	0.64472	0.81896	1.61355	0.58970	
25	9.1440*-03	6.1929*+00	1.15704	0.98726	0.66361	0.83270	1.57453	0.61191	
26	9.6520*-03	6.5125*+00	1.15234	0.98979	0.68445	0.84739	1.53279	0.63706	
27	1.0160*-02	6.8861*+00	1.14753	0.99218	0.70543	0.86155	1.49160	0.66282	
28	1.0668*-02	7.3096*+00	1.14185	0.99448	0.72847	0.87633	1.44715	0.69145	
29	1.1176*-02	7.6862*+00	1.13616	0.99637	0.74836	0.88855	1.40976	0.71610	
30	1.1684*-02	8.0631*+00	1.13038	0.99839	0.76774	0.90010	1.37453	0.74022	
31	1.2192*-02	8.4461*+00	1.12469	1.00026	0.78694	0.91107	1.34038	0.76447	
32	1.2700*-02	8.8924*+00	1.11901	1.00171	0.80873	0.92277	1.30190	0.79314	
33	1.3208*-02	9.3417*+00	1.11185	1.00372	0.83009	0.93483	1.26612	0.82022	
34	1.3716*-02	9.7817*+00	1.10470	1.00435	0.85048	0.94377	1.23144	0.84664	
35	1.4224*-02	1.0152*+01	1.09754	1.00491	0.86875	0.95152	1.20379	0.86753	
36	1.4732*-02	1.0612*+01	1.09038	1.00527	0.88766	0.96046	1.17073	0.89454	
37	1.5240*-02	1.0992*+01	1.08333	1.00502	0.90417	0.96716	1.14417	0.91572	
38	1.5748*-02	1.1379*+01	1.07578	1.00514	0.92070	0.97381	1.11870	0.93645	
39	1.6256*-02	1.1681*+01	1.06823	1.00461	0.93337	0.97856	1.09919	0.95100	
40	1.6764*-02	1.1967*+01	1.06068	1.00401	0.94523	0.98265	1.08076	0.96440	
41	1.7272*-02	1.2235*+01	1.05313	1.00315	0.95616	0.98626	1.06396	0.97623	
42	1.7780*-02	1.2417*+01	1.04558	1.00235	0.96354	0.98855	1.05257	0.98198	
43	1.8288*-02	1.2644*+01	1.03804	1.00222	0.97267	0.99173	1.03937	0.99027	
44	1.8796*-02	1.2873*+01	1.02853	1.00135	0.98180	0.99449	1.02602	0.99692	
45	1.9304*-02	1.3044*+01	1.01902	1.00081	0.98853	0.99653	1.01626	0.99923	
46	1.9812*-02	1.3147*+01	1.00951	1.00033	0.99257	0.99767	1.01030	0.99689	
47	2.0320*-02	1.3337*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
48	2.0828*-02	1.3440*+01	0.99039	0.99934	1.00400	1.00100	0.99404	0.99733	
49	2.1336*-02	1.3526*+01	0.98088	0.99886	1.00733	1.00185	0.98916	0.99347	
50	2.1844*-02	1.3659*+01	0.97138	0.99854	1.01247	1.00337	0.98211	0.99240	
51	2.2352*-02	1.3721*+01	0.96187	0.99835	1.01482	1.00404	0.97886	0.98661	
52	2.2860*-02	1.3809*+01	0.95236	0.99836	1.01819	1.00513	0.97453	0.98227	
53	2.3368*-02	1.3886*+01	0.94187	0.99781	1.02113	1.00580	0.97019	0.97644	
54	2.3876*-02	1.3960*+01	0.93138	0.99819	1.02396	1.00689	0.96694	0.96986	
55	2.4384*-02	1.4013*+01	0.92089	0.99805	1.02598	1.00746	0.96423	0.96218	
56	2.4892*-02	1.4083*+01	0.91040	0.99762	1.02863	1.00808	0.96000	0.95557	
57	2.5400*-02	1.4149*+01	0.90001	0.99806	1.03111	1.00908	0.95772	0.94827	
58	2.5908*-02	1.4214*+01	0.88952	0.99843	1.03354	1.01003	0.95501	0.94076	
59	2.6416*-02	1.4267*+01	0.87903	0.99823	1.03555	1.01055	0.95230	0.93280	
60	2.6924*-02	1.4319*+01	0.86854	0.99910	1.03751	1.01160	0.95068	0.92420	
61	2.7432*-02	1.4363*+01	0.85805	0.99726	1.03914	1.01117	0.94888	0.91631	
62	2.7940*-02	1.4436*+01	0.84756	0.99739	1.04186	1.01207	0.94363	0.90904	
63	2.8448*-02	1.4522*+01	0.83492	0.99817	1.04508	1.01345	0.94030	0.89979	
64	2.8956*-02	1.4627*+01	0.82217	0.99751	1.04899	1.01431	0.93496	0.89195	

INPUT VARIABLES Y,U,T,P

71010206 STUREK		PROFILE TABULATION 65 POINTS, DELTA AT POINT 44						
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	1.18416	0.94457	0.00000	0.00000	2.72158	0.00000
2	1.9304+04	1.6511+00	1.18370	0.94201	0.28615	0.43884	2.35193	0.22086
3	2.5400+04	1.7926+00	1.18353	0.94174	0.31058	0.47068	2.29686	0.24255
4	3.7846+04	1.9231+00	0.32966	0.94252	0.33045	0.49599	2.25287	0.07258
5	5.4102+04	2.0322+00	1.18284	0.94449	0.34558	0.51515	2.22211	0.27422
6	6.7310+04	2.1310+00	1.18250	0.94570	0.35842	0.53095	2.19447	0.28611
7	8.7884+04	2.2407+00	1.18199	0.94821	0.37193	0.54762	2.16788	0.29858
8	1.1328+03	2.3725+00	1.18122	0.95152	0.38732	0.56635	2.13816	0.31288
9	1.6408+03	2.5621+00	1.17909	0.95704	0.40813	0.59137	2.09958	0.33210
10	2.1488+03	2.7526+00	1.17695	0.96061	0.42780	0.61385	2.05892	0.35090
11	2.6568+03	2.9118+00	1.17465	0.96209	0.44345	0.63081	2.02346	0.36619
12	3.1648+03	3.0713+00	1.17226	0.96363	0.45852	0.64675	1.98957	0.38107
13	3.6728+03	3.2419+00	1.16987	0.96518	0.47404	0.66274	1.95464	0.39666
14	4.1808+03	3.4273+00	1.16679	0.96677	0.49028	0.67903	1.91814	0.41305
15	4.6888+03	3.6242+00	1.16347	0.96796	0.50692	0.69507	1.88008	0.43013
16	5.1968+03	3.8336+00	1.16014	0.96979	0.52398	0.71125	1.84254	0.44783
17	5.7048+03	4.0449+00	1.15689	0.97146	0.54061	0.72853	1.80605	0.46539
18	6.2128+03	4.2801+00	1.15356	0.97341	0.55851	0.74252	1.76747	0.48462
19	6.7208+03	4.5605+00	1.15023	0.97565	0.57910	0.76029	1.72367	0.50735
20	7.2288+03	4.7985+00	1.14691	0.97866	0.59598	0.77484	1.69030	0.52575
21	7.7368+03	5.1263+00	1.14341	0.98109	0.61845	0.79295	1.64390	0.55153
22	8.2448+03	5.3398+00	1.13922	0.98316	0.63919	0.80894	1.60167	0.57538
23	8.7528+03	5.7897+00	1.13478	0.98585	0.66154	0.82570	1.55787	0.60146
24	9.2608+03	6.1241+00	1.12924	0.98829	0.68220	0.84059	1.51825	0.62521
25	9.7688+03	6.5085+00	1.12377	0.99084	0.70519	0.85644	1.47497	0.65252
26	1.0277+02	6.8402+00	1.11822	0.99287	0.72843	0.86917	1.43952	0.67517
27	1.0785+02	7.2992+00	1.11268	0.99516	0.74972	0.88507	1.39364	0.70663
28	1.1293+02	7.7299+00	1.10713	0.99753	0.77363	0.89952	1.35193	0.73664
29	1.1801+02	8.1248+00	1.10166	0.99948	0.79449	0.91158	1.31648	0.76284
30	1.2309+02	8.6001+00	1.09612	1.00137	0.81387	0.92493	1.27581	0.79466
31	1.2817+02	9.0026+00	1.09057	1.00305	0.83897	0.93555	1.24348	0.82050
32	1.3325+02	9.4555+00	1.08485	1.00444	0.86101	0.94654	1.20855	0.84966
33	1.3833+02	9.8766+00	1.07862	1.00522	0.88101	0.95591	1.17727	0.87581
34	1.4341+02	1.0279+01	1.07247	1.00617	0.89971	0.96446	1.14911	0.90013
35	1.4849+02	1.0815+01	1.06624	1.00603	0.91501	0.97080	1.12565	0.91956
36	1.5357+02	1.0954+01	1.05975	1.00571	0.93020	0.97680	1.10271	0.93875
37	1.5865+02	1.1308+01	1.05224	1.00543	0.94581	0.98281	1.07977	0.95775
38	1.6373+02	1.1547+01	1.04481	1.00489	0.95791	0.98718	1.06204	0.97116
39	1.6881+02	1.1828+01	1.03730	1.00424	0.96827	0.99073	1.04692	0.98163
40	1.7389+02	1.2079+01	1.02988	1.00317	0.97890	0.99409	1.03126	0.99274
41	1.7897+02	1.2203+01	1.02236	1.00245	0.98415	0.99563	1.02346	0.99456
42	1.8405+02	1.2337+01	1.01494	1.00169	0.99060	0.99755	1.01406	0.99840
43	1.8913+02	1.2471+01	1.00751	1.00115	0.99532	0.99894	1.00730	0.99915
44	1.9421+02	1.2584+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
45	1.9929+02	1.2635+01	0.99257	1.00016	1.00212	1.00082	0.99739	0.99598
46	2.0437+02	1.2717+01	0.98472	0.99985	1.00550	1.00183	0.99270	0.99377
47	2.0945+02	1.2789+01	0.97559	0.99947	1.00844	1.00264	0.98853	0.98951
48	2.1453+02	1.3421+01	0.96645	0.98469	1.03402	1.00365	0.94213	1.02956
49	2.1961+02	1.2926+01	0.95732	0.99933	1.01403	1.00447	0.98123	0.97999
50	2.2469+02	1.2995+01	0.94819	0.99926	1.01684	1.00538	0.97758	0.97515
51	2.2977+02	1.3040+01	0.93897	0.99949	1.01908	1.00624	0.97497	0.96908
52	2.3485+02	1.3112+01	0.92949	0.99954	1.02159	1.00711	0.97185	0.96322
53	2.3993+02	1.3146+01	0.91993	0.99915	1.02378	1.00764	0.96872	0.95689
54	2.4501+02	1.3234+01	0.91037	0.99946	1.02651	1.00869	0.96554	0.95101
55	2.5009+02	1.3304+01	0.90081	0.99933	1.02934	1.00956	0.96194	0.94540
56	2.5517+02	1.3367+01	0.89117	0.99988	1.03186	1.01066	0.95933	0.93885
57	2.6025+02	1.3437+01	0.88118	0.99969	1.03467	1.01148	0.95568	0.93262
58	2.6533+02	1.3507+01	0.87119	0.99977	1.03753	1.01234	0.95203	0.92638
59	2.7041+02	1.3577+01	0.86112	0.99976	1.04023	1.01330	0.94891	0.91956
60	2.7549+02	1.3646+01	0.85113	1.00000	1.04298	1.01431	0.94576	0.91281
61	2.8057+02	1.3726+01	0.84114	0.99964	1.04613	1.01513	0.94161	0.90682
62	2.8565+02	1.3792+01	0.83090	1.00076	1.04873	1.01652	0.93952	0.89900
63	2.9073+02	1.3884+01	0.82015	1.00097	1.05236	1.01777	0.93535	0.89241
64	2.9581+02	1.3954+01	0.80939	1.00004	1.05511	1.01815	0.93118	0.88499
65	3.0089+02	1.4033+01	0.79855	0.99892	1.05818	1.01854	0.92649	0.87789

INPUT VARIABLES Y,U,T,P

71010207		STUREK	PROFILE TABULATION		60 POINTS, DELTA AT POINT 47			
I	Y	P12/P	P/PD	T0/T00	U/UD	U/UD	T/T0	RHD/RHOD*U/UD
1	0.0000*+00	1.0000*+00	1.17665	0.94310	0.00000	0.00000	2.63503	0.00000
2	1.2192*-04	1.5310*+00	1.17637	0.94415	0.26858	0.41047	2.33569	0.20674
3	2.6670*-04	1.6742*+00	1.17600	0.94388	0.33103	0.49143	2.20394	0.26222
4	4.1148*-04	1.9664*+00	1.17562	0.94379	0.34468	0.50818	2.17365	0.27465
5	6.0706*-04	2.1462*+00	1.17510	0.94732	0.36900	0.53818	2.12721	0.29730
6	8.5344*-04	2.3112*+00	1.17450	0.95054	0.38941	0.56267	2.08783	0.31653
7	1.0490*-03	2.4364*+00	1.17390	0.95505	0.40397	0.58038	2.06411	0.33007
8	1.3691*-03	2.5441*+00	1.17240	0.95816	0.41598	0.59456	2.04291	0.34121
9	1.5215*-03	2.5909*+00	1.17165	0.95969	0.42106	0.60056	2.03433	0.34589
10	1.8923*-03	2.6945*+00	1.16984	0.96231	0.43207	0.61119	2.01413	0.35615
11	2.1463*-03	2.7722*+00	1.16864	0.96406	0.44010	0.62224	1.99899	0.36377
12	2.4003*-03	2.8577*+00	1.16744	0.96556	0.44874	0.63173	1.98183	0.37213
13	2.6543*-03	2.9242*+00	1.16617	0.96666	0.45573	0.63928	1.96769	0.37887
14	2.9083*-03	3.0079*+00	1.16497	0.96717	0.46329	0.64712	1.95103	0.38639
15	3.1623*-03	3.0846*+00	1.16376	0.96764	0.47081	0.65481	1.93438	0.39395
16	3.4163*-03	3.1634*+00	1.16256	0.96794	0.47820	0.66221	1.91772	0.40145
17	3.6703*-03	3.2414*+00	1.16129	0.96677	0.48539	0.66952	1.90257	0.40866
18	4.1783*-03	3.3335*+00	1.16009	0.96991	0.49173	0.67794	1.88541	0.41714
19	4.4323*-03	3.5211*+00	1.15878	0.96986	0.51026	0.69348	1.84705	0.43432
20	4.9403*-03	3.7076*+00	1.15311	0.97207	0.52614	0.70877	1.81474	0.45036
21	5.4483*-03	3.9265*+00	1.14853	0.97322	0.54814	0.72513	1.77587	0.46897
22	5.9563*-03	4.1723*+00	1.14365	0.97513	0.56362	0.74250	1.73549	0.48929
23	6.4543*-03	4.4210*+00	1.13877	0.97704	0.58263	0.75890	1.69662	0.50938
24	6.9723*-03	4.7135*+00	1.13472	0.97860	0.60419	0.77662	1.65220	0.53338
25	7.4803*-03	4.9799*+00	1.13104	0.98091	0.62315	0.79201	1.61335	0.55455
26	7.9883*-03	5.3200*+00	1.12736	0.98355	0.64652	0.81020	1.57042	0.58162
27	8.4963*-03	5.5972*+00	1.12376	0.98539	0.66495	0.82414	1.53609	0.60292
28	9.0043*-03	5.9036*+00	1.11918	0.98861	0.68979	0.84204	1.49016	0.63242
29	9.5123*-03	6.3646*+00	1.11431	0.99095	0.71342	0.85826	1.44775	0.66081
30	1.0020*-02	6.7513*+00	1.10943	0.99348	0.73673	0.87369	1.40636	0.68922
31	1.0528*-02	7.1448*+00	1.10380	0.99554	0.75948	0.88797	1.36699	0.71701
32	1.1036*-02	7.5809*+00	1.09794	0.99764	0.78402	0.90268	1.32559	0.74766
33	1.1544*-02	8.0038*+00	1.09201	0.99952	0.80711	0.91589	1.28773	0.77669
34	1.2052*-02	8.4280*+00	1.08616	1.00130	0.82961	0.92823	1.25189	0.80535
35	1.2560*-02	8.8664*+00	1.08031	1.00317	0.85223	0.94019	1.21706	0.83454
36	1.3068*-02	9.3136*+00	1.07445	1.00435	0.87470	0.95127	1.18274	0.86418
37	1.3576*-02	9.7141*+00	1.06860	1.00521	0.89434	0.96051	1.15346	0.88985
38	1.4084*-02	1.0084*+01	1.06267	1.00601	0.91210	0.96859	1.12771	0.91273
39	1.4592*-02	1.0456*+01	1.05681	1.00634	0.92962	0.97609	1.10247	0.93567
40	1.5100*-02	1.0763*+01	1.05096	1.00593	0.94363	0.98160	1.08178	0.95369
41	1.5608*-02	1.1044*+01	1.04406	1.00518	0.95663	0.98635	1.06310	0.96868
42	1.6116*-02	1.1288*+01	1.03670	1.00461	0.96763	0.99032	1.04745	0.98016
43	1.6624*-02	1.1495*+01	1.02935	1.00350	0.97689	0.99327	1.03382	0.98897
44	1.7132*-02	1.1654*+01	1.02199	1.00224	0.98390	0.99526	1.02222	0.99406
45	1.7640*-02	1.1807*+01	1.01464	1.00146	0.99061	0.99734	1.01363	0.99933
46	1.8148*-02	1.1915*+01	1.00736	1.00055	0.99534	0.99860	1.00656	0.99938
47	1.8656*-02	1.2022*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
48	1.9164*-02	1.2071*+01	0.99264	0.99966	1.00210	1.00058	0.99697	0.99624
49	1.9672*-02	1.2139*+01	0.98529	0.99989	1.00505	1.00174	0.99344	0.99353
50	2.0180*-02	1.2177*+01	0.97891	0.99942	1.00666	1.00208	0.99091	0.99093
51	2.0688*-02	1.2237*+01	0.97013	0.99916	1.00924	1.00286	0.98738	0.98533
52	2.1196*-02	1.2283*+01	0.96262	0.99968	1.01125	1.00382	0.98536	0.98005
53	2.1704*-02	1.2334*+01	0.95399	1.00034	1.01341	1.00494	0.98334	0.97474
54	2.2212*-02	1.2372*+01	0.94589	1.00042	1.01504	1.00552	0.98132	0.96921
55	2.2720*-02	1.2413*+01	0.93786	1.00008	1.01679	1.00595	0.97880	0.96387
56	2.3228*-02	1.2463*+01	0.92923	0.99968	1.01890	1.00648	0.97577	0.95848
57	2.3736*-02	1.2512*+01	0.92044	1.00027	1.02099	1.00750	0.97375	0.95235
58	2.4244*-02	1.2554*+01	0.91159	1.00089	1.02279	1.00823	0.97173	0.94582
59	2.4752*-02	1.2612*+01	0.90271	1.00047	1.02522	1.00905	0.96670	0.94041
60	2.5260*-02	1.2660*+01	0.89403	1.00045	1.02725	1.00973	0.96618	0.93432

INPUT VARIABLES Y,U,T,Z

71010208		STUREK		PROFILE TABULATION		60 POINTS, DELTA AT POINT 41			
I	Y	PT/P	P/PD	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.13924	0.94297	0.00000	0.00000	2.53891	0.00000	
2	2.6924-04	1.9872+00	1.13869	0.74409	0.35792	0.51711	2.08901	0.28198	
3	3.1020-04	2.0610+00	1.13855	0.94340	0.36837	0.52944	2.06566	0.29182	
4	5.8928-04	2.2777+00	1.13802	0.94485	0.39678	0.56235	2.00875	0.31259	
5	6.7310-04	2.3651+00	1.13789	0.94622	0.40746	0.57463	1.90881	0.32877	
6	8.1788-04	2.4536+00	1.13756	0.95045	0.41791	0.58734	1.97519	0.33827	
7	1.0744-03	2.5778+00	1.13710	0.95492	0.43206	0.60392	1.95379	0.35148	
8	1.3233-03	2.6584+00	1.13644	0.95915	0.44093	0.61463	1.94309	0.35947	
9	1.5824-03	2.7579+00	1.13511	0.96203	0.45160	0.62666	1.92558	0.36941	
10	1.7780-03	2.8394+00	1.13012	0.96432	0.46012	0.63615	1.91148	0.37744	
11	2.2860-03	2.9996+00	1.13154	0.96764	0.47596	0.65317	1.88327	0.39245	
12	2.7940-03	3.1336+00	1.12929	0.96937	0.48947	0.66701	1.85700	0.40562	
13	3.3020-03	3.2806+00	1.12737	0.97005	0.50342	0.68060	1.82782	0.41978	
14	3.8100-03	3.4466+00	1.12545	0.97086	0.51867	0.69513	1.79621	0.43555	
15	4.3180-03	3.6229+00	1.12267	0.97181	0.53434	0.70970	1.76411	0.45165	
16	4.8260-03	3.8186+00	1.11989	0.97293	0.55117	0.72496	1.73006	0.46928	
17	5.3340-03	4.0152+00	1.11717	0.97415	0.56754	0.73944	1.69747	0.48665	
18	5.8420-03	4.2513+00	1.11419	0.97500	0.58657	0.75553	1.65905	0.50740	
19	6.3500-03	4.4950+00	1.11095	0.97693	0.60555	0.77147	1.62305	0.52806	
20	6.8580-03	4.7432+00	1.10771	0.97822	0.62426	0.78683	1.58706	0.54890	
21	7.3660-03	5.0470+00	1.10400	0.98162	0.64640	0.80428	1.54815	0.57354	
22	7.8740-03	5.3474+00	1.09970	0.98329	0.66754	0.82008	1.50924	0.59754	
23	8.3820-03	5.6590+00	1.09539	0.98585	0.68877	0.83573	1.47228	0.62179	
24	8.8900-03	5.9917+00	1.09109	0.98747	0.71071	0.85089	1.43337	0.64770	
25	9.3980-03	6.3695+00	1.08685	0.99017	0.73482	0.86727	1.39300	0.67667	
26	9.9060-03	6.7365+00	1.08255	0.99274	0.75745	0.88209	1.35603	0.70419	
27	1.0414-02	7.0871+00	1.07798	0.99464	0.77823	0.89495	1.32247	0.72950	
28	1.0922-02	7.5164+00	1.07315	0.99651	0.80352	0.90982	1.28210	0.76154	
29	1.1430-02	7.9278+00	1.06832	0.99860	0.82675	0.92307	1.24660	0.79106	
30	1.1938-02	8.3755+00	1.06355	1.00071	0.85130	0.93647	1.21012	0.82305	
31	1.2446-02	8.7626+00	1.05845	1.00178	0.87197	0.94694	1.17947	0.84982	
32	1.2954-02	9.1130+00	1.05309	1.00368	0.89025	0.95643	1.15418	0.87266	
33	1.3462-02	9.5334+00	1.04773	1.00477	0.91171	0.96660	1.12403	0.90099	
34	1.3970-02	9.9873+00	1.04237	1.00553	0.92939	0.97462	1.09971	0.92380	
35	1.4478-02	1.0217+01	1.03701	1.00515	0.94556	0.98122	1.07685	0.94492	
36	1.4986-02	1.0504+01	1.03164	1.00501	0.95942	0.98680	1.05788	0.96232	
37	1.5494-02	1.0715+01	1.02575	1.00408	0.96965	0.99041	1.04329	0.97177	
38	1.6002-02	1.0959+01	1.01933	1.00337	0.98097	0.99447	1.02772	0.98635	
39	1.6510-02	1.1142+01	1.01284	1.00222	0.98949	0.99716	1.01556	0.99449	
40	1.7018-02	1.1260+01	1.00642	1.00142	0.99496	0.99883	1.00778	0.99748	
D 41	1.7526-02	1.1369+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
42	1.8034-02	1.1443+01	0.99325	0.99985	1.00337	1.00117	0.99562	0.99879	
43	1.8542-02	1.1493+01	0.98610	0.99884	1.00568	1.00152	0.99173	0.99583	
44	1.9050-02	1.1548+01	0.97895	0.99850	1.00815	1.00225	0.98833	0.99274	
45	1.9558-02	1.1586+01	0.97180	0.99870	1.00988	1.00298	0.98638	0.98816	
46	2.0066-02	1.1618+01	0.96465	0.99908	1.01137	1.00372	0.98492	0.98306	
47	2.0574-02	1.1645+01	0.95657	0.99861	1.01257	1.00391	0.98296	0.97695	
48	2.1082-02	1.1691+01	0.94856	0.99826	1.01467	1.00450	0.98006	0.97222	
49	2.1590-02	1.1724+01	0.94055	0.99865	1.01616	1.00523	0.97860	0.96615	
50	2.2098-02	1.1764+01	0.93248	0.99842	1.01797	1.00577	0.97617	0.96076	
51	2.2606-02	1.1801+01	0.92447	0.99900	1.01983	1.00665	0.97471	0.95476	
52	2.3114-02	1.1844+01	0.91639	0.99841	1.02155	1.00704	0.97179	0.94963	
53	2.3622-02	1.1901+01	0.90838	0.99862	1.02414	1.00807	0.96887	0.94513	
54	2.4130-02	1.1918+01	0.90030	0.99906	1.02489	1.00856	0.96839	0.93765	
55	2.4638-02	1.1978+01	0.89117	0.99892	1.02759	1.00944	0.96498	0.93223	
56	2.5146-02	1.2040+01	0.88197	0.99901	1.03033	1.01086	0.96235	0.92623	
57	2.5654-02	1.2101+01	0.87277	1.00016	1.03305	1.01198	0.95963	0.92038	
58	2.6162-02	1.2160+01	0.86390	0.99885	1.03566	1.01223	0.95525	0.91542	
59	2.6670-02	1.2219+01	0.85529	0.99956	1.03829	1.01350	0.95282	0.90976	
60	2.7178-02	1.2266+01	0.84678	1.00113	1.04037	1.01501	0.95185	0.90294	

INPUT VARIABLES Y,U,T,P

SECTION D, ADDITIONAL DATA, TABLE 1, RAW PRESTON TUBE DATA
 FACSIMILE FROM SOURCE PAPER. NB - AUTHORS SYMBOLS AND UNITS.

Run	$T_w, ^\circ R$	p_w/p_o	p_s/p_o	p_o, psia	τ_w, psf	CAT 7101 RUN SERIAL
06200	523	.01253	.03877	38.674	.64902	0101
06250	522	.01252	.04023	48.342	.78759	0201
06300	521	.01250	.04165	58.011	.92721	0301
08200	523	.01245	.03954	38.674	.66722	0102
08250	522	.01239	.04074	48.342	.80412	0202
08300	521	.01238	.04224	58.011	.94751	0302
10200	523	.01257	.03899	38.674	.65237	0103
10250	522	.01254	.04058	48.342	.79518	0203
10300	521	.01253	.04191	58.011	.92982	0303
117203	523	.02253	.05488	38.674	.70073	0104
117253	522	.02253	.05759	48.342	.86879	0204
117303	521	.02247	.05987	58.011	1.03496	0304
118203	523	.02540	.06162	38.674	.75468	0105
118253	522	.02546	.06422	48.342	.92550	0205
118303	521	.02554	.06708	58.011	1.10573	0305
119203	523	.02847	.06838	38.674	.81120	0106
119253	522	.02856	.07233	48.342	1.00475	0206
119303	521	.02869	.07578	58.011	1.20397	0306
120201	523	.03190	.07755	38.674	.88108	0107
120250	522	.03207	.08195	48.342	1.09889	0207
120300	521	.03228	.08567	58.011	1.31077	0307
121201	523	.03530	.08970	38.674	1.00266	0108
121251	522	.03543	.09501	48.342	1.25435	0208
121301	521	.03564	.10044	58.011	1.51514	0308

Preston tube diameter: 3.18 mm.

Preston tube pressure reading: p_s

Wall shear τ_w from Yanta, Brott and Lee (1969)

NOTE: Reservoir conditions are not identical with those of the profile runs.

SECTION D, ADDITIONAL DATA, TABLE 2, REDUCED HOT-WIRE OBSERVATIONS
 FACSIMILE FROM TABLES SUPPLIED BY AUTHORS. NR. AUTHORS SYMBOLS AND UNITS.

TABLULATED FLUCTUATION DATA
 (UNPUBLISHED)

7101 0202
 STA 08250

$dp/dx = 0$

$$A = \frac{1}{2} \frac{T_{re} + T_c}{T_{re} - T_c} \frac{\Delta T}{T}$$

y/δ	$\frac{\Delta u}{u}$	$\frac{\Delta u}{u_t}$	$\frac{\Delta(\rho u)}{(\rho u)}$	$\frac{\Delta T_t}{T_{re} - T_c}$	A	R_{mT_t}	R_{uT}
.044	.0466	.670	.0862	.0159	.0367	-.092	-.923
.089	.0520	.836	.1023	.0215	.0502	.171	-.920
.200	.0393	.705	.0922	.0243	.0543	.502	-.677
.312	.0304	.589	.0891	.0241	.0500	-.143	-.873
.423	.0231	.477	.0852	.0214	.0620	-.343	-.663
.534	.0204	.441	.0822	.0212	.0632	-.326	-.653
.645	.0122	.274	.0694	.0185	.0563	-.550	-.855
.756	.0092	.213	.0551	.0131	.0457	-.482	-.650
.868	.0042	.098	.0324	.0077	.0235	-.823	-.656
.979	.0027	.064	.0194	.0049	.0178	-.946	-.751
1.090	.0012	.028	.0123	.0035	.0113	-.895	-.755
1.201	.0016	.039	.0101	.0030	.0089	-.492	-.601

$\delta = 22.8 \text{ mm}$

7101 0205
 STA 118250

$$A = \frac{1}{2} \frac{T_{re} + T_c}{T_{re} - T_c} \frac{\Delta T}{T}$$

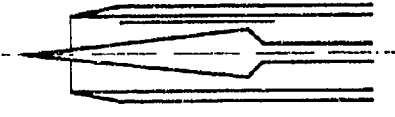
$\frac{dp}{dx} \frac{\theta}{TW} = 1.36$

y/δ	$\frac{\Delta u}{u}$	$\frac{\Delta u}{u_t}$	$\frac{\Delta(\rho u)}{(\rho u)}$	$\frac{\Delta T_t}{T_{re} - T_c}$	A	R_{mT_t}	R_{uT}
.051	.072	1.234	.114	.0237	.0387	.051	-.662
.102	.073	1.389	.125	.0255	.0490	.053	-.800
.204	.074	1.533	.140	.0305	.0699	.115	-.920
.306	.061	1.389	.133	.0305	.0774	-.046	-.921
.408	.046	1.139	.126	.0356	.0488	-.315	-.664
.510	.039	1.039	.119	.0389	.0683	-.249	-.643
.611	.029	.824	.112	.0318	.0913	-.479	-.800
.739	.016	.467	.090	.0252	.0894	-.554	-.805
.841	.008	.243	.048	.0184	.0437	-.507	-.660
.943	.002	.059	.019	.0092	.0199	-1.122	-.114
1.045	.002	.060	.010	.0054	.0099	-.480	-.302
1.121	.003	.091	.012	.0043	.0112	-.237	-.721

$\delta = 19.9 \text{ mm}$

T_{re} = wire recovery temperature at edge of boundary-layer

T_c = static temperature at edge of boundary-layer

axisymmetric 	M : 4 (ZPG-Series 01) : 4 falling to 2 (02) - followed by recovery : 4 (03) recovery after step-induced separation R THETA X 10 ⁻³ : 10 - 60 TW / TR : 1.0	7102
		ZPG - APG Recovery AW
Blow-down wind-tunnel with 12 seconds running time. W = H = 1.5 m. PO : 1.16 MN/m ² . TO : 298 K. Air: absolute humidity 2 x 10 ⁻⁴ . RE/m X 10 ⁻⁶ : 50 at M = 4.		
PEAKE D.J., BRAKMANN G. and ROMESKIE J.M., 1971. Comparisons between some high Reynolds number turbulent boundary layer experiments at Mach 4 and various recent calculation procedures. AGARD-CP-93-71 paper 11. And Peake D.J., private communications.		

- 1 The test boundary layer was formed on the inner surface of a cylinder (D = 0.229, L = 0.838 m) mounted on the centre-line of the wind tunnel. The exterior of the leading edge (X = 0) was chamfered at 14° (E). A retractable centre body could be placed so as to cause a streamwise pressure gradient. Three cases were studied:

Series 01: Centre-body retracted. ZPG

Series 02: Centrebody forward. APG followed by recovery as tabulated in sections B and D.

Series 03: Centrebody retracted and a ring of rectangular cross section (height 3.8 and length 12.3 mm) mounted at X = 0.254 m, giving a test boundary layer recovering in nearly constant pressure from the disturbance of flowing up and down a step ("RPG").

Traversing probes could be inserted at six X stations such that in the APG case, one was just before the start of the pressure gradient, two during it and three in the constant pressure recovery region which followed. In the RPG case the last survey station was after a second disturbance caused by the shock structure of the ring, transmitted across the duct. The test duct was not actively cooled, but received some preliminary cooling due to "Canadian winter air reaching the model from the exhaust area". Measurements indicated that the surface temperature resulting was close to the recovery temperature. The surface roughness was close to 0.25 μm rms., with waviness less than 2 x 10⁻⁴ m/m.

- 2 Mach number variation in the ZPG case was less than 0.02. The authors calculate, on the basis of acoustic measurements, that turbulent velocity fluctuations are probably less than 0.1%. No trips were used and
- 3 Preston tube readings (Section D) showed that natural transition occurred between X = 50 and 165 mm. The flow was therefore fully turbulent before being perturbed in the RPG case. Oil dot flow visualisation
- 5 confirmed these conclusions. Incidence and yaw of the model were less than 10' wind off. The maximum eccentricity of the centrebody was within ± 0.013 mm. Circumferential Mach number variations were less than 0.03 as determined from static pressure surveys at X = 299 and 552 mm. Oil dot streak-lines showed no perceptible convergence and boundary layer yaw measurements at X = 422 and 804 mm showed a maximum yaw very close to the wall of order 1° relative to a generator and 1.5° relative to the free stream.
- 6 Seventy static holes of 1.016 mm diameter were drilled normal to the surface from X = 6.3 to 831.8 mm at 12.7 mm intervals. At two stations (X = 299, 552 mm) three additional holes gave a check on two-dimensionality. An iron-constantan thermocouple bead was attached to a thin plate mounted in the duct surface at X = 426 mm, and this thin plate achieved an equilibrium temperature during the run. Small Preston tubes (d₁ = 0.406, d₂ = 0.203, l = 5.54 mm) could be mounted in each static hole and ten Preston tube readings were collected in any one run. Four calibration relationships were used to give the results presented in section D.
- 7 A single combined Pitot, yaw and equilibrium temperature probe was employed. The unshielded thermocouple did not function. The face normal to the flow was 0.305 mm high (h₁) and 0.71 mm (b₁) wide, the opening being 0.127 (~h₂) by 0.508 mm (b₂) and the lower lip 0.102 mm thick. The two side tubes were chamfered at 45° and a servo-mechanism kept the probe aligned with the local flow direction. In section the top
- 8 surface was inclined at 7.5° to the axis. The six ports for the probe allowed traverses at X = 295, 422,

523, 574, 676 and 803 mm. Static pressure holes were 9.4 mm ahead of and 3.3 mm behind each traverse normal. The face of a Preston tube lay 5.5 mm ahead of the static hole in which the tube was mounted.

- 9 The authors have interpolated static pressure data to the X values of the Preston tube tips as presented in section D, and to those of the normals for the velocity profiles presented in sections B and C. The Crocco/Van Driest parabolic temperature-velocity distribution was assumed, as was constant static pressure through the boundary layer. The Pitot data have been adjusted for the effects of shear and wall proximity by applying an outward displacement Δ of the effective probe centre given by $\Delta/h = 0.24 - 0.04 ((h/y) - 0.5)$, in which h is the overall height of the probe face and y is the height of the geometric centre. Static hole errors were assessed using a curve-fit to the hole size corrections of Franklin & Wallace (1970).
- 10 Sutherland's viscosity law was assumed.
- 11 The CF values presented with the profiles in sections B and C are interpolated from the measured values of section D, the editors having arbitrarily chosen those reduced with the calibration of Hopkins & Keener (TR method), 1966. The data are presented with the author's recovery factor of 0.89. The three sequences of profiles are distinguished by their different pressure histories. The very full static pressure and Preston tube data obtained by the authors is presented in facsimile in section D.
- 12 DATA: 7102 0101-0306. PY2 profiles. NX = 6. CF from Preston tubes.

15 Editors' comments

The axi-symmetric configuration eliminates end-effects, and δ/RZ at ~ 0.05 is small enough for there to be negligible distortion by axi-symmetry. The three sequences presented include the ZPG case, and ZPG regions in which the boundary layer recovers from a strong APG and from the severe disturbance of flowing over a rectangular fence.

The pressure gradient of series O2 is imposed as a reflected wave, so that in most of the test boundary layer there should be very little normal pressure gradient. However, profiles O1 and O3 are taken at stations which coincide with the start and finish of the longitudinal wall-pressure gradient. Consequently they are taken in regions traversed by simple waves, with the associated normal pressure gradients. The authors present data for profiles O2 (where there should be no significant $\delta p/\delta y$) and for O3, assuming a linear static pressure variation through the boundary layer given by

$$\delta p/\delta y = - \cot \mu \delta p/\delta x$$

where μ is the Mach angle at the boundary layer edge. This assumes a wave structure corresponding to that generated by a curved wall (as for Sturek & Danberg CAT 7101), with the isobars extrapolated into the boundary layer. A more detailed study of the wave structure suggests that the appropriate relationships are, while still assuming that the isobars may be extrapolated,

$$O201 : \delta p/\delta y = 1/2 \cot \mu. \delta p/\delta x \text{ (at wall, downstream)}$$

$$O203 : \delta p/\delta y = - 1/2 \cot \mu. \delta p/\delta x \text{ (at wall, upstream).}$$

The authors' calculations for O203 therefore show the effect of a normal pressure gradient of double the probable magnitude, and, for this station, of the correct sign. The most obvious change in the calculated integral values is a 5 % increase in the momentum thickness. It seems probable that there is a printer's error in the calculated 90 % increase in THETA reported for O202, since it is not reflected in the associated R THETA and shape factor values. These calculations should be regarded as a numerical experiment suggesting the magnitude of possible normal pressure gradient effects.

The wall temperature is stated to be measured by a thermocouple attached to a thin plate mounted in the model surface. Temperatures measured there are stated to reach equilibrium temperature, as might be expected. The editors feel, however, that this does not guarantee that the bulk temperature of the model had dropped to the recovery temperature.

Direct comparisons for the ZPG and APG data may be made with Lewis et al. - CAT 7201. The most appropriate planar ZPG comparisons are with Hastings & Sawyer - CAT 7006, and Mabey et al. - CAT 7402. Comparable planar APG cases are those of Zwarts - CAT 7007 and Thomas - CAT 7401. There are no strictly comparable recovery cases except possibly Moore - CAT 5805 who studied a planar flow which had mounted a step.

CAT 7102		PEAKE	BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN X * RL *	MD * P00 T00	TW/TR* PW/PD* SW *	RED2* RED20 DR	CF * CG PI2	H12 H32 H42	H12K H32K D2K	PW TW UD	PD* TD* TR	
71020101	3.9256	1.0000	3.1079 ⁺⁰³	1.1482 ⁻⁰³	7.8621	1.5237	8.4668 ⁺⁰³	8.4668 ⁺⁰³	
2.9515 ⁻⁰¹	1.1636 ⁺⁰⁶	1.0000	1.0221 ⁺⁰⁴	NM	1.8177	1.7776	2.7345 ⁺⁰²	7.3056 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9822 ⁺⁰²	0.0000	1.9721 ⁻⁰⁴	NC	0.1517	3.6777 ⁻⁰⁴	6.7273 ⁺⁰²	2.7345 ⁺⁰²	
71020102	3.9051	1.0000	4.6275 ⁺⁰³	1.0782 ⁻⁰³	7.6641	1.4409	8.6667 ⁺⁰³	8.6667 ⁺⁰³	
4.2215 ⁻⁰¹	1.1586 ⁺⁰⁶	1.0000	1.5106 ⁺⁰⁴	NM	1.8188	1.7870	2.7322 ⁺⁰²	7.3556 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9790 ⁺⁰²	0.0000	2.8916 ⁻⁰⁴	NC	0.1531	5.3869 ⁻⁰⁴	6.7151 ⁺⁰²	2.7322 ⁺⁰²	
71020103	3.9006	1.0000	5.6030 ⁺⁰³	1.0400 ⁻⁰³	7.5614	1.3991	8.7563 ⁺⁰³	8.7563 ⁺⁰³	
5.2375 ⁻⁰¹	1.1635 ⁺⁰⁶	1.0000	1.8255 ⁺⁰⁴	NM	1.8300	1.8022	2.7358 ⁺⁰²	7.3778 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9828 ⁺⁰²	0.0000	3.4782 ⁻⁰⁴	NC	0.1520	6.3288 ⁻⁰⁴	6.7174 ⁺⁰²	2.7358 ⁺⁰²	
71020104	3.9046	1.0000	6.2526 ⁺⁰³	1.0300 ⁻⁰³	7.5628	1.3776	8.7081 ⁺⁰³	8.7081 ⁺⁰³	
5.7455 ⁻⁰¹	1.1633 ⁺⁰⁶	1.0000	2.0499 ⁺⁰⁴	NM	1.8265	1.8019	2.7358 ⁺⁰²	7.3667 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9829 ⁺⁰²	0.0000	3.9147 ⁻⁰⁴	NC	0.1518	7.2135 ⁻⁰⁴	6.7193 ⁺⁰²	2.7358 ⁺⁰²	
71020105	3.9212	1.0000	7.1874 ⁺⁰³	1.0200 ⁻⁰³	7.6709	1.3985	8.5219 ⁺⁰³	8.5219 ⁺⁰³	
6.7615 ⁻⁰¹	1.1642 ⁺⁰⁶	1.0000	2.3596 ⁺⁰⁴	NM	1.8221	1.7902	2.7362 ⁺⁰²	7.3222 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9839 ⁺⁰²	0.0000	4.5438 ⁻⁰⁴	NC	0.1517	8.4552 ⁻⁰⁴	6.7274 ⁺⁰²	2.7362 ⁺⁰²	
71020106	3.9016	1.0000	7.7588 ⁺⁰³	1.0246 ⁻⁰³	7.6187	1.3891	8.7563 ⁺⁰³	8.7563 ⁺⁰³	
8.0315 ⁻⁰¹	1.1651 ⁺⁰⁶	1.0000	2.5286 ⁺⁰⁴	NM	1.8164	1.7859	2.7369 ⁺⁰²	7.3778 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9839 ⁺⁰²	0.0000	4.8167 ⁻⁰⁴	NC	0.1508	9.0558 ⁻⁰⁴	6.7192 ⁺⁰²	2.7369 ⁺⁰²	
71020201	3.9256	1.0000	3.0026 ⁺⁰³	1.1000 ⁻⁰³	7.9374	1.5535	8.4874 ⁺⁰³	8.4874 ⁺⁰³	
2.9515 ⁻⁰¹	1.1664 ⁺⁰⁶	1.0000	9.8750 ⁺⁰³	NM	1.8112	1.7681	2.7345 ⁺⁰²	7.3056 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9822 ⁺⁰²	0.0000	1.9007 ⁻⁰⁴	NC	0.1511	3.5911 ⁻⁰⁴	6.7273 ⁺⁰²	2.7345 ⁺⁰²	
71020202	2.9013	1.0000	1.0088 ⁺⁰⁴	1.3764 ⁻⁰³	5.1018	1.5616	3.7032 ⁺⁰⁴	3.7032 ⁺⁰⁴	
4.2215 ⁻⁰¹	1.1723 ⁺⁰⁶	1.0000	2.2317 ⁺⁰⁴	NM	1.7681	1.7585	2.7801 ⁺⁰²	1.1128 ⁺⁰²	
-1.1445 ⁻⁰¹	2.9861 ⁺⁰²	0.0000	2.4759 ⁻⁰⁴	NC	0.1232	3.8147 ⁻⁰⁴	6.1363 ⁺⁰²	2.7801 ⁺⁰²	
71020203	2.0752	1.0000	2.5701 ⁺⁰⁴	1.4244 ⁻⁰³	3.2802	1.4928	1.3270 ⁺⁰⁵	1.3270 ⁺⁰⁵	
5.2375 ⁻⁰¹	1.1674 ⁺⁰⁶	1.0000	4.1285 ⁺⁰⁴	NM	1.7477	1.7846	2.8314 ⁺⁰²	1.6028 ⁺⁰²	
-1.1445 ⁻⁰¹	2.9832 ⁺⁰²	0.0000	2.9961 ⁻⁰⁴	NC	0.0913	3.8053 ⁻⁰⁴	5.2675 ⁺⁰²	2.8314 ⁺⁰²	
71020204	2.0002	1.0000	3.5972 ⁺⁰⁴	1.6214 ⁻⁰³	2.4932	1.3862	1.4917 ⁺⁰⁵	1.4917 ⁺⁰⁵	
5.7455 ⁻⁰¹	1.1675 ⁺⁰⁶	1.0000	5.6197 ⁺⁰⁴	NM	1.8344	1.8252	2.8384 ⁺⁰²	1.6578 ⁺⁰²	
-1.1445 ⁻⁰¹	2.9843 ⁺⁰²	0.0000	3.9439 ⁻⁰⁴	NC	0.0894	4.7805 ⁻⁰⁴	5.1635 ⁺⁰²	2.8384 ⁺⁰²	
71020205	1.9882	1.0000	3.9146 ⁺⁰⁴	1.5782 ⁻⁰³	2.4666	1.3868	1.5193 ⁺⁰⁵	1.5193 ⁺⁰⁵	
6.7615 ⁻⁰¹	1.1671 ⁺⁰⁶	1.0000	6.0887 ⁺⁰⁴	NM	1.8395	1.8267	2.8384 ⁺⁰²	1.6661 ⁺⁰²	
-1.1445 ⁻⁰¹	2.9833 ⁺⁰²	0.0000	4.2502 ⁻⁰⁴	NC	0.0890	5.1044 ⁻⁰⁴	5.1454 ⁺⁰²	2.8384 ⁺⁰²	
71020206	2.0120	1.0000	3.6446 ⁺⁰⁴	1.4364 ⁻⁰³	2.9641	1.3733	1.4636 ⁺⁰⁵	1.4636 ⁺⁰⁵	
8.0315 ⁻⁰¹	1.1665 ⁺⁰⁶	1.0000	5.7186 ⁺⁰⁴	NM	1.8456	1.8337	2.8370 ⁺⁰²	1.6489 ⁺⁰²	
-1.1445 ⁻⁰¹	2.9837 ⁺⁰²	0.0000	4.0363 ⁻⁰⁴	NC	0.0905	4.8425 ⁻⁰⁴	5.1800 ⁺⁰²	2.8370 ⁺⁰²	
71020301	3.7884	1.0000	3.9930 ⁺⁰³	1.2029 ⁻⁰³	7.3123	1.4151	7.2946 ⁺⁰³	7.2946 ⁺⁰³	
2.9515 ⁻⁰¹	8.3205 ⁺⁰⁵	1.0000	1.2471 ⁺⁰⁴	NM	1.8099	1.7898	2.7391 ⁺⁰²	7.7056 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9824 ⁺⁰²	0.0000	3.1338 ⁻⁰⁴	NC	0.1473	5.3382 ⁻⁰⁴	6.6676 ⁺⁰²	2.7391 ⁺⁰²	
71020302	3.6210	1.0000	7.3655 ⁺⁰³	1.0100 ⁻⁰³	6.9696	1.4646	9.1976 ⁺⁰³	9.1976 ⁺⁰³	
4.2215 ⁻⁰¹	8.3202 ⁺⁰⁵	1.0000	2.1981 ⁺⁰⁴	NM	1.7866	1.7555	2.7467 ⁺⁰²	8.2307 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9844 ⁺⁰²	0.0000	4.9707 ⁻⁰⁴	NC	0.1418	9.2543 ⁻⁰⁴	6.5898 ⁺⁰²	2.7467 ⁺⁰²	
71020303	3.6080	1.0000	8.5712 ⁺⁰³	1.0100 ⁻⁰³	6.7254	1.3804	9.3631 ⁺⁰³	9.3631 ⁺⁰³	
5.2375 ⁻⁰¹	8.3170 ⁺⁰⁵	1.0000	2.4991 ⁺⁰⁴	NM	1.8137	1.7404	2.7459 ⁺⁰²	8.2778 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9827 ⁺⁰²	0.0000	5.7147 ⁻⁰⁴	NC	0.1435	1.0117 ⁻⁰³	6.5816 ⁺⁰²	2.7459 ⁺⁰²	
71020304	3.6190	1.0000	9.1030 ⁺⁰³	1.0200 ⁻⁰³	6.7221	1.3665	9.2252 ⁺⁰³	9.2252 ⁺⁰³	
5.7455 ⁻⁰¹	8.3218 ⁺⁰⁵	1.0000	2.6652 ⁺⁰⁴	NM	1.8193	1.7404	2.7465 ⁺⁰²	8.2444 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9840 ⁺⁰²	0.0000	6.1279 ⁻⁰⁴	NC	0.1450	1.0760 ⁻⁰³	6.5884 ⁺⁰²	2.7465 ⁺⁰²	
71020305	3.6160	1.0000	8.4222 ⁺⁰³	1.0136 ⁻⁰³	6.5371	1.3115	9.2665 ⁺⁰³	9.2665 ⁺⁰³	
6.6599 ⁻⁰¹	8.3241 ⁺⁰⁵	1.0000	2.4630 ⁺⁰⁴	NM	1.8475	1.8286	2.7470 ⁺⁰²	8.2556 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9845 ⁺⁰²	0.0000	5.6555 ⁻⁰⁴	NC	0.1472	9.3381 ⁻⁰⁴	6.5874 ⁺⁰²	2.7470 ⁺⁰²	
71020406	3.1983	1.0000	1.2826 ⁺⁰⁴	1.0808 ⁻⁰³	5.5376	1.3663	1.6871 ⁺⁰⁴	1.6871 ⁺⁰⁴	
8.0315 ⁻⁰¹	8.3199 ⁺⁰⁵	1.0000	3.1897 ⁺⁰⁴	NM	1.8179	1.7985	2.7628 ⁺⁰²	4.7444 ⁺⁰¹	
-1.1445 ⁻⁰¹	2.9832 ⁺⁰²	0.0000	5.8518 ⁻⁰⁴	NC	0.1337	9.3316 ⁻⁰⁴	6.5463 ⁺⁰²	2.7628 ⁺⁰²	

71020201		PEAKE	PROFILE TABULATION			59 POINTS, DELTA AT POINT 59			
I	Y	P12/P	P/PO	TU/TOD	M/MD	U/UO	T/TO	RHO/RHO0*J/UO	
1	0.0000+00	1.0000+00	NM	0.91844	0.00000	0.00000	3.74099	0.00000	
2	2.2860-04	2.5910+00	NM	0.94160	0.32130	0.54465	2.91589	0.18816	
3	3.4290-04	3.3354+00	NM	0.94839	0.37682	0.61836	2.69291	0.22963	
4	4.2672-04	4.0648+00	NM	0.95404	0.42355	0.67077	2.50774	0.26748	
5	4.7498-04	4.8465+00	NM	0.95925	0.46824	0.71577	2.33670	0.30632	
6	5.5880-04	5.3097+00	NM	0.96201	0.49273	0.73447	2.24621	0.32876	
7	6.4262-04	5.9145+00	NM	0.96530	0.52294	0.75469	2.13825	0.35762	
8	7.0104-04	6.1925+00	NM	0.96674	0.53656	0.77588	2.09095	0.37106	
9	7.8232-04	6.5838+00	NM	0.96859	0.55440	0.78998	2.03043	0.38907	
10	8.4074-04	6.9324+00	NM	0.97017	0.57009	0.80188	1.97850	0.40530	
11	9.2202-04	7.2539+00	NM	0.97156	0.58418	0.81218	1.93293	0.42018	
12	9.9314-04	7.5039+00	NM	0.97260	0.59490	0.81978	1.89893	0.43171	
13	1.0744-03	7.6126+00	NM	0.97304	0.59950	0.82298	1.88452	0.43671	
14	1.1328-03	7.7444+00	NM	0.97356	0.60504	0.82678	1.86733	0.44276	
15	1.2040-03	8.0322+00	NM	0.97467	0.61694	0.83478	1.83089	0.45594	
16	1.2852-03	8.4167+00	NM	0.97609	0.63249	0.84488	1.78439	0.47349	
17	1.3564-03	8.7767+00	NM	0.97735	0.64671	0.85379	1.74295	0.48985	
18	1.4021-03	9.0488+00	NM	0.97827	0.65725	0.86019	1.71288	0.50214	
19	1.4834-03	9.4796+00	NM	0.97966	0.67360	0.86979	1.66735	0.52186	
20	1.5418-03	9.9498+00	NM	0.98109	0.69099	0.87959	1.62035	0.54284	
21	1.6256-03	1.0561+01	NM	0.98284	0.71298	0.89134	1.56307	0.57028	
22	1.6942-03	1.1059+01	NM	0.98417	0.73039	0.90029	1.51436	0.59255	
23	1.7526-03	1.1547+01	NM	0.98545	0.74773	0.90879	1.47720	0.61521	
24	1.8237-03	1.2038+01	NM	0.98658	0.76344	0.91619	1.44018	0.63616	
25	1.8821-03	1.2657+01	NM	0.98798	0.78363	0.92529	1.39425	0.66365	
26	1.9634-03	1.3047+01	NM	0.98882	0.79608	0.93469	1.36477	0.68094	
27	2.0345-03	1.3363+01	NM	0.98947	0.80603	0.93489	1.34529	0.69494	
28	2.0803-03	1.3643+01	NM	0.99004	0.81476	0.93849	1.32681	0.70733	
29	2.1615-03	1.3851+01	NM	0.99045	0.82117	0.94109	1.31341	0.71653	
30	2.2200-03	1.4006+01	NM	0.99075	0.82592	0.94299	1.30380	0.72338	
31	2.2784-03	1.4080+01	NM	0.99099	0.82819	0.94389	1.29694	0.72666	
32	2.3368-03	1.4164+01	NM	0.99104	0.83072	0.94489	1.29376	0.73035	
33	2.5019-03	1.4680+01	NM	0.99200	0.84626	0.95090	1.26258	0.75313	
34	2.6314-03	1.5264+01	NM	0.99302	0.86348	0.95730	1.22911	0.77886	
35	2.7711-03	1.5845+01	NM	0.99398	0.88028	0.96330	1.19752	0.80441	
36	2.8981-03	1.6429+01	NM	0.99490	0.89686	0.96900	1.16732	0.83010	
37	3.0404-03	1.7015+01	NM	0.99578	0.91319	0.97440	1.13856	0.85582	
38	3.1572-03	1.7588+01	NM	0.99659	0.92886	0.97940	1.11178	0.88093	
39	3.2969-03	1.8093+01	NM	0.99728	0.94247	0.98360	1.08918	0.90307	
40	3.4366-03	1.8532+01	NM	0.99786	0.95414	0.98710	1.07427	0.92229	
41	3.5535-03	1.9015+01	NM	0.99847	0.96683	0.99080	1.05021	0.94343	
42	3.6830-03	1.9190+01	NM	0.99865	0.97137	0.99210	1.04314	0.95107	
43	3.8354-03	1.9561+01	NM	0.99913	0.98095	0.99480	1.02843	0.96729	
44	3.9751-03	1.9744+01	NM	0.99935	0.98564	0.99610	1.02134	0.97529	
45	4.1148-03	1.9886+01	NM	0.99952	0.98928	0.99710	1.01588	0.98152	
46	4.2570-03	1.9987+01	NM	0.99963	0.99184	0.99780	1.01205	0.98592	
47	4.3840-03	2.0088+01	NM	0.99975	0.99442	0.99850	1.00822	0.99036	
48	4.5237-03	2.0132+01	NM	0.99980	0.99553	0.99880	1.00656	0.99228	
49	4.6533-03	2.0162+01	NM	0.99983	0.99627	0.99900	1.00548	0.99356	
50	4.7930-03	2.0206+01	NM	0.99988	0.99739	0.99930	1.00384	0.99548	
51	4.9225-03	2.0206+01	NM	0.99988	0.99739	0.99930	1.00384	0.99548	
52	5.0749-03	2.0235+01	NM	0.99992	0.99813	0.99950	1.00274	0.99677	
53	5.2019-03	2.0235+01	NM	0.99992	0.99813	0.99950	1.00274	0.99677	
54	5.3543-03	2.0279+01	NM	0.99997	0.99925	0.99980	1.00110	0.99871	
55	5.4839-03	2.0279+01	NM	0.99997	0.99925	0.99980	1.00110	0.99871	
56	5.6134-03	2.0279+01	NM	0.99997	0.99925	0.99980	1.00110	0.99871	
57	5.7302-03	2.0279+01	NM	0.99997	0.99925	0.99980	1.00110	0.99871	
58	5.8572-03	2.0279+01	NM	0.99997	0.99925	0.99980	1.00110	0.99871	
0 59	5.9868-03	2.0309+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES

Y, U/UO

ASSUME P=PO AND VAN DRIEST

71020202		PEAKE		PROFILE TABULATION		60 POINTS, DELTA AT POINT 60			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/T0	RHO/RHOD+U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93099	0.00000	0.00000	2.49832	0.00000	
2	2.2860 ⁻ -04	2.0679 ⁺ +00	NM	0.95060	0.37031	0.53310	2.07251	0.25722	
3	3.3020 ⁻ -04	2.8004 ⁺ +00	NM	0.95844	0.45728	0.63070	1.90232	0.33154	
4	4.2672 ⁻ -04	3.1825 ⁺ +00	NM	0.96193	0.49545	0.66960	1.82653	0.36660	
5	5.1054 ⁻ -04	3.5183 ⁺ +00	NM	0.96476	0.52649	0.69950	1.76519	0.39627	
6	5.9436 ⁻ -04	3.7897 ⁺ +00	NM	0.96689	0.55018	0.72130	1.71878	0.41966	
7	6.7818 ⁻ -04	4.0284 ⁺ +00	NM	0.96868	0.57014	0.73900	1.68006	0.43987	
8	7.5946 ⁻ -04	4.2344 ⁺ +00	NM	0.97015	0.58678	0.75330	1.64808	0.45708	
9	8.4074 ⁻ -04	4.4004 ⁺ +00	NM	0.97157	0.60295	0.76680	1.61734	0.47411	
10	9.2202 ⁻ -04	4.6321 ⁺ +00	NM	0.97284	0.61759	0.77870	1.58978	0.48982	
11	1.0058 ⁻ -03	4.7751 ⁺ +00	NM	0.97375	0.62829	0.78720	1.56984	0.50145	
12	1.0871 ⁻ -03	4.9467 ⁺ +00	NM	0.97483	0.64087	0.79700	1.54657	0.51533	
13	1.1684 ⁻ -03	5.1222 ⁺ +00	NM	0.97589	0.65349	0.80660	1.52351	0.52944	
14	1.2497 ⁻ -03	5.3151 ⁺ +00	NM	0.97702	0.66707	0.81670	1.49894	0.54485	
15	1.3208 ⁻ -03	5.4420 ⁺ +00	NM	0.97774	0.67585	0.82310	1.48322	0.55494	
16	1.4249 ⁻ -03	5.6333 ⁺ +00	NM	0.97881	0.68886	0.83240	1.46015	0.57008	
17	1.5088 ⁻ -03	5.9866 ⁺ +00	NM	0.98058	0.71096	0.84770	1.42163	0.59629	
18	1.5773 ⁻ -03	6.2362 ⁺ +00	NM	0.98195	0.72833	0.85930	1.39197	0.61733	
19	1.6713 ⁻ -03	6.5190 ⁺ +00	NM	0.98332	0.74611	0.87080	1.36216	0.63928	
20	1.7526 ⁻ -03	6.8159 ⁺ +00	NM	0.98470	0.76433	0.88220	1.33221	0.66221	
21	1.8364 ⁻ -03	7.1307 ⁺ +00	NM	0.98610	0.78317	0.89360	1.30188	0.68639	
22	1.9279 ⁻ -03	7.4289 ⁺ +00	NM	0.98736	0.80060	0.90380	1.27441	0.70919	
23	2.0117 ⁻ -03	7.8206 ⁺ +00	NM	0.98894	0.82294	0.91640	1.24005	0.73900	
24	2.0803 ⁻ -03	8.1345 ⁺ +00	NM	0.99015	0.84040	0.92590	1.21382	0.76280	
25	2.1742 ⁻ -03	8.4195 ⁺ +00	NM	0.99120	0.85594	0.93410	1.19097	0.78432	
26	2.3495 ⁻ -03	8.9695 ⁺ +00	NM	0.99313	0.88516	0.94890	1.14422	0.82599	
27	2.5146 ⁻ -03	9.4403 ⁺ +00	NM	0.99467	0.90941	0.96060	1.11574	0.86095	
28	2.6899 ⁻ -03	9.8353 ⁺ +00	NM	0.99589	0.92927	0.96980	1.08913	0.89043	
29	2.8651 ⁻ -03	1.0193 ⁺ +01	NM	0.99696	0.94691	0.97770	1.06608	0.91710	
30	3.0277 ⁻ -03	1.0459 ⁺ +01	NM	0.99771	0.95977	0.98330	1.04963	0.93681	
31	3.2029 ⁻ -03	1.0571 ⁺ +01	NM	0.99803	0.96514	0.98560	1.04284	0.94511	
32	3.3680 ⁻ -03	1.0799 ⁺ +01	NM	0.99863	0.97556	0.99000	1.02982	0.96134	
33	3.5077 ⁻ -03	1.0917 ⁺ +01	NM	0.99897	0.98157	0.99250	1.02239	0.97076	
34	3.6830 ⁻ -03	1.0979 ⁺ +01	NM	0.99913	0.98448	0.99370	1.01882	0.97534	
35	3.8354 ⁻ -03	1.1025 ⁺ +01	NM	0.99926	0.98667	0.99460	1.01614	0.97880	
36	4.0107 ⁻ -03	1.1072 ⁺ +01	NM	0.99938	0.98887	0.99550	1.01345	0.98228	
37	4.1732 ⁻ -03	1.1088 ⁺ +01	NM	0.99942	0.99060	0.99580	1.01256	0.98345	
38	4.3485 ⁻ -03	1.1120 ⁺ +01	NM	0.99950	0.99198	0.99640	1.01077	0.98578	
39	4.5136 ⁻ -03	1.1136 ⁺ +01	NM	0.99955	0.99182	0.99670	1.00987	0.98698	
40	4.6761 ⁻ -03	1.1151 ⁺ +01	NM	0.99959	0.99256	0.99700	1.00898	0.98813	
41	4.8514 ⁻ -03	1.1151 ⁺ +01	NM	0.99959	0.99256	0.99700	1.00898	0.98813	
42	5.0165 ⁻ -03	1.1151 ⁺ +01	NM	0.99959	0.99256	0.99700	1.00898	0.98813	
43	5.1791 ⁻ -03	1.1162 ⁺ +01	NM	0.99961	0.99305	0.99720	1.00838	0.98891	
44	5.3442 ⁻ -03	1.1162 ⁺ +01	NM	0.99961	0.99305	0.99720	1.00838	0.98891	
45	5.5067 ⁻ -03	1.1178 ⁺ +01	NM	0.99966	0.99379	0.99750	1.00748	0.99009	
46	5.6820 ⁻ -03	1.1178 ⁺ +01	NM	0.99966	0.99379	0.99750	1.00748	0.99009	
47	5.8471 ⁻ -03	1.1194 ⁺ +01	NM	0.99970	0.99453	0.99780	1.00659	0.99127	
48	6.0096 ⁻ -03	1.1194 ⁺ +01	NM	0.99970	0.99453	0.99780	1.00659	0.99127	
49	6.1620 ⁻ -03	1.1210 ⁺ +01	NM	0.99974	0.99527	0.99810	1.00569	0.99245	
50	6.3246 ⁻ -03	1.1210 ⁺ +01	NM	0.99974	0.99527	0.99810	1.00569	0.99245	
51	6.5126 ⁻ -03	1.1226 ⁺ +01	NM	0.99978	0.99602	0.99840	1.00479	0.99364	
52	6.6650 ⁻ -03	1.1226 ⁺ +01	NM	0.99978	0.99602	0.99840	1.00479	0.99364	
53	6.8402 ⁻ -03	1.1226 ⁺ +01	NM	0.99978	0.99602	0.99840	1.00479	0.99364	
54	7.0155 ⁻ -03	1.1242 ⁺ +01	NM	0.99982	0.99676	0.99870	1.00389	0.99483	
55	7.1806 ⁻ -03	1.1253 ⁺ +01	NM	0.99986	0.99751	0.99900	1.00300	0.99602	
56	7.3304 ⁻ -03	1.1269 ⁺ +01	NM	0.99989	0.99800	0.99920	1.00240	0.99681	
57	7.4828 ⁻ -03	1.1269 ⁺ +01	NM	0.99989	0.99800	0.99920	1.00240	0.99681	
58	7.6708 ⁻ -03	1.1280 ⁺ +01	NM	0.99992	0.99850	0.99940	1.00180	0.99761	
59	7.8232 ⁻ -03	1.1296 ⁺ +01	NM	0.99996	0.99925	0.99970	1.00090	0.99880	
60	7.9858 ⁻ -03	1.1312 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES

Y, U/UD

ASSUME P=PO AND VAN DRIEST

71020203	PEAKE	PROFILE TABULATION				43 POINTS, DELTA AT POINT 43			
I	Y	PT2/P	P/PD	T0/T0D	M/HD	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000*+00	1.0000*+00	NM	0.94910	0.00000	0.00000	1.76655	0.00000	
2	2.2660*+04	1.8414*+00	NM	0.96611	0.97039	0.57810	1.51037	0.38275	
3	3.1750*+04	2.1245*+00	NM	0.96979	0.52850	0.63750	1.45502	0.43814	
4	4.1656*+04	2.4216*+00	NM	0.97319	0.58059	0.68790	1.40381	0.49002	
5	5.0038*+04	2.5821*+00	NM	0.97489	0.60633	0.71180	1.37817	0.51648	
6	5.7150*+04	2.7268*+00	NM	0.97636	0.62843	0.73180	1.35604	0.53966	
7	6.6548*+04	2.9017*+00	NM	0.97806	0.65396	0.75439	1.33041	0.56697	
8	7.3660*+04	3.0394*+00	NM	0.97935	0.67328	0.77090	1.31100	0.58802	
9	8.3058*+04	3.1465*+00	NM	0.98032	0.68788	0.78320	1.29635	0.60416	
10	9.2202*+04	3.2609*+00	NM	0.98133	0.70109	0.79580	1.28110	0.62119	
11	1.0058*+03	3.3830*+00	NM	0.98239	0.71896	0.80870	1.26523	0.63917	
12	1.0973*+03	3.4825*+00	NM	0.98322	0.73159	0.81880	1.25283	0.65367	
13	1.1684*+03	3.5360*+00	NM	0.98367	0.73829	0.82410	1.24595	0.66142	
14	1.2497*+03	3.5906*+00	NM	0.98411	0.74505	0.82940	1.23924	0.66928	
15	1.3457*+03	3.7123*+00	NM	0.98509	0.75991	0.84090	1.22451	0.68672	
16	1.4249*+03	3.8043*+00	NM	0.98581	0.77074	0.84930	1.21363	0.69980	
17	1.5088*+03	3.8968*+00	NM	0.98653	0.78184	0.85750	1.20290	0.71286	
18	1.6002*+03	3.9751*+00	NM	0.98711	0.79073	0.86410	1.19419	0.72359	
19	1.6902*+03	4.0813*+00	NM	0.98791	0.80314	0.87320	1.18207	0.73870	
20	1.7653*+03	4.1656*+00	NM	0.98853	0.81268	0.88010	1.17280	0.75043	
21	1.8466*+03	4.2042*+00	NM	0.98880	0.81700	0.88320	1.16661	0.75577	
22	1.9406*+03	4.2890*+00	NM	0.98941	0.82643	0.88990	1.15950	0.76748	
23	2.0117*+03	4.3890*+00	NM	0.98911	0.83740	0.89760	1.14895	0.78123	
24	2.1031*+03	4.4743*+00	NM	0.98970	0.84663	0.90400	1.14011	0.79290	
25	2.1859*+03	4.5740*+00	NM	0.99137	0.85730	0.91130	1.12995	0.80649	
26	2.2682*+03	4.6892*+00	NM	0.99213	0.86945	0.91950	1.11845	0.82212	
27	2.3495*+03	4.8064*+00	NM	0.99290	0.88164	0.92760	1.10698	0.83796	
28	2.4562*+03	4.8597*+00	NM	0.99324	0.88712	0.93120	1.10185	0.84513	
29	2.6314*+03	5.1546*+00	NM	0.99507	0.91685	0.95030	1.07430	0.88457	
30	2.7940*+03	5.3630*+00	NM	0.99630	0.93726	0.96300	1.05568	0.91221	
31	2.9620*+03	5.5659*+00	NM	0.99747	0.95672	0.97480	1.03815	0.93898	
32	3.1344*+03	5.7218*+00	NM	0.99833	0.97139	0.98350	1.02509	0.95943	
33	3.3096*+03	5.7990*+00	NM	0.99876	0.97857	0.98770	1.01874	0.96953	
34	3.4722*+03	5.8775*+00	NM	0.99918	0.98582	0.99190	1.01237	0.97978	
35	3.6373*+03	5.9078*+00	NM	0.99934	0.98860	0.99350	1.00993	0.98373	
36	3.8125*+03	5.9401*+00	NM	0.99951	0.99157	0.99520	1.00734	0.98795	
37	3.9624*+03	5.9631*+00	NM	0.99963	0.99367	0.99640	1.00551	0.99094	
38	4.1275*+03	5.9862*+00	NM	0.99976	0.99577	0.99760	1.00368	0.99395	
39	4.3028*+03	5.9939*+00	NM	0.99980	0.99648	0.99800	1.00306	0.99495	
40	4.4780*+03	6.0094*+00	NM	0.99988	0.99788	0.99880	1.00184	0.99697	
41	4.6406*+03	6.0172*+00	NM	0.99992	0.99859	0.99920	1.00123	0.99798	
42	4.7930*+03	6.0250*+00	NM	0.99996	0.99929	0.99960	1.00061	0.99899	
0 43	4.9809*+03	6.0327*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES

Y, U/U0

ASSUME P=PD AND VAN ORNST

71020204		PEAKE	PROFILE TABULATION		60 POINTS, DELTA AT POINT 60				
I	Y	PTP/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.95111	0.00000	0.00000	1.71214	0.00000	
2	2.2860*-04	1.9159+00	NM	0.96914	0.50511	0.60800	1.44889	0.41963	
3	3.4036*-04	2.3419+00	NM	0.97435	0.58852	0.64970	1.37339	0.50219	
4	4.0132*-04	2.5867+00	NM	0.97790	0.62981	0.72770	1.33503	0.54508	
5	4.9022*-04	2.7805+00	NM	0.97895	0.66026	0.75470	1.30653	0.57764	
6	5.7912*-04	3.0129+00	NM	0.98117	0.69472	0.78420	1.27426	0.61545	
7	6.5278*-04	3.1670+00	NM	0.98258	0.71853	0.80230	1.25375	0.63992	
8	7.4168*-04	3.2058+00	NM	0.98292	0.72191	0.80670	1.24671	0.64603	
9	8.1534*-04	3.2706+00	NM	0.98349	0.73079	0.81390	1.24040	0.65616	
10	9.0170*-04	3.3351+00	NM	0.98405	0.73751	0.82090	1.23275	0.66618	
11	9.7536*-04	3.3736+00	NM	0.98438	0.74465	0.82500	1.22744	0.67213	
12	1.0643*-03	3.4126+00	NM	0.98472	0.74983	0.82910	1.22261	0.67814	
13	1.1506*-03	3.4637+00	NM	0.98515	0.75657	0.83440	1.21633	0.68600	
14	1.2395*-03	3.5070+00	NM	0.98547	0.76156	0.83830	1.21169	0.69185	
15	1.3411*-03	3.5278+00	NM	0.98568	0.76490	0.84090	1.20856	0.69578	
16	1.4300*-03	3.5518+00	NM	0.98580	0.76826	0.84350	1.20546	0.69973	
17	1.5164*-03	3.5922+00	NM	0.98621	0.77319	0.84730	1.20088	0.70556	
18	1.5900*-03	3.6445+00	NM	0.98663	0.77985	0.85240	1.19471	0.71348	
19	1.6764*-03	3.6956+00	NM	0.98704	0.78630	0.85730	1.18874	0.72118	
20	1.7653*-03	3.7475+00	NM	0.98745	0.79280	0.86220	1.18274	0.72898	
21	1.8517*-03	3.7733+00	NM	0.98766	0.79600	0.86460	1.17979	0.73284	
22	1.9253*-03	3.8243+00	NM	0.98805	0.80230	0.86930	1.17399	0.74047	
23	2.0142*-03	3.8762+00	NM	0.98845	0.80865	0.87400	1.16815	0.74819	
24	2.1006*-03	3.9153+00	NM	0.98875	0.81311	0.87750	1.16379	0.75400	
25	2.1742*-03	3.9664+00	NM	0.98914	0.81957	0.88200	1.15815	0.76156	
26	2.2371*-03	4.0182+00	NM	0.98953	0.82577	0.88650	1.15248	0.76921	
27	2.3343*-03	4.1207+00	NM	0.99029	0.83790	0.89520	1.14144	0.78427	
28	2.4232*-03	4.1859+00	NM	0.99076	0.84552	0.90060	1.13454	0.79380	
29	2.4968*-03	4.2623+00	NM	0.99131	0.85435	0.90680	1.12656	0.80493	
30	2.5994*-03	4.3403+00	NM	0.99186	0.86327	0.91300	1.11852	0.81626	
31	2.6848*-03	4.4174+00	NM	0.99240	0.87200	0.91900	1.11069	0.82741	
32	2.7584*-03	4.5082+00	NM	0.99302	0.88216	0.92590	1.10163	0.84048	
33	2.8321*-03	4.6231+00	NM	0.99380	0.89484	0.93440	1.09037	0.85696	
34	2.9058*-03	4.6756+00	NM	0.99414	0.90058	0.93820	1.08530	0.86446	
35	3.1090*-03	4.8173+00	NM	0.99507	0.91586	0.94820	1.07187	0.88462	
36	3.2715*-03	4.9078+00	NM	0.99564	0.92548	0.95440	1.06347	0.89744	
37	3.4468*-03	4.9717+00	NM	0.99604	0.93222	0.95870	1.05761	0.90648	
38	3.6068*-03	5.0230+00	NM	0.99636	0.93759	0.96210	1.05296	0.91371	
39	3.7821*-03	5.0489+00	NM	0.99652	0.94029	0.96380	1.05063	0.91736	
40	3.9573*-03	5.0373+00	NM	0.99676	0.94428	0.96630	1.04719	0.92276	
41	4.1046*-03	5.1136+00	NM	0.99692	0.94700	0.96800	1.04485	0.92645	
42	4.2799*-03	5.1903+00	NM	0.99739	0.95489	0.97290	1.03808	0.93722	
43	4.4397*-03	5.2556+00	NM	0.99778	0.96156	0.97700	1.03238	0.94636	
44	4.5872*-03	5.3073+00	NM	0.99808	0.96680	0.98020	1.02792	0.95357	
45	4.7625*-03	5.3317+00	NM	0.99823	0.96926	0.98170	1.02583	0.95698	
46	4.9073*-03	5.3976+00	NM	0.99861	0.97588	0.98570	1.02022	0.96616	
47	5.0823*-03	5.4359+00	NM	0.99883	0.97971	0.98800	1.01694	0.97150	
48	5.2453*-03	5.4611+00	NM	0.99898	0.98222	0.98950	1.01488	0.97500	
49	5.4051*-03	5.4746+00	NM	0.99906	0.98356	0.99030	1.01375	0.97687	
50	5.5651*-03	5.5136+00	NM	0.99928	0.98743	0.99260	1.01050	0.98229	
51	5.7277*-03	5.5650+00	NM	0.99957	0.99250	0.99560	1.00625	0.98941	
52	5.8877*-03	5.5771+00	NM	0.99964	0.99369	0.99630	1.00526	0.99109	
53	6.0477*-03	5.5909+00	NM	0.99972	0.99505	0.99710	1.00412	0.99300	
54	6.1951*-03	5.5909+00	NM	0.99972	0.99505	0.99710	1.00412	0.99300	
55	6.3856*-03	5.6031+00	NM	0.99979	0.99624	0.99780	1.00313	0.99469	
56	6.5608*-03	5.6152+00	NM	0.99985	0.99744	0.99850	1.00213	0.99637	
57	6.7208*-03	5.6152+00	NM	0.99985	0.99744	0.99850	1.00213	0.99637	
58	6.8656*-03	5.6292+00	NM	0.99993	0.99880	0.99930	1.00100	0.99831	
59	7.0409*-03	5.6292+00	NM	0.99993	0.99880	0.99930	1.00100	0.99831	
D 60	7.2034*-03	5.6415+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES

Y, U/UD

ASSUME P=PD AND VAN DRIEST

71020205		PEAKE	PROFILE TABULATION		60 POINTS, DELTA AT POINT 60				
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	NM	0.95143	0.00000	0.00000	1.70362	0.00000	
2	2.2860"-04	1.7840"+00	NM	0.96766	0.47696	0.57800	1.46855	0.39358	
3	3.2512"-04	2.4349"+00	NM	0.97572	0.60827	0.70720	1.35172	0.52319	
4	4.0132"-04	2.7051"+00	NM	0.97854	0.65252	0.74710	1.31089	0.56992	
5	5.0546"-04	2.8817"+00	NM	0.98027	0.67958	0.77060	1.28579	0.59932	
6	5.9436"-04	3.0902"+00	NM	0.98130	0.69561	0.78820	1.27092	0.61704	
7	6.8326"-04	3.0986"+00	NM	0.98230	0.71120	0.79720	1.25645	0.63449	
8	7.8486"-04	3.1930"+00	NM	0.98315	0.72449	0.80810	1.24414	0.64953	
9	8.5852"-04	3.2745"+00	NM	0.98387	0.73573	0.81720	1.23373	0.66238	
10	9.4742"-04	3.3566"+00	NM	0.98458	0.74666	0.82610	1.22344	0.67523	
11	1.0338"-03	3.3971"+00	NM	0.98492	0.75229	0.83040	1.21843	0.68153	
12	1.1227"-03	3.4652"+00	NM	0.98550	0.76133	0.83750	1.21010	0.69209	
13	1.1938"-03	3.5192"+00	NM	0.98595	0.76840	0.84300	1.20359	0.70040	
14	1.2675"-03	3.5330"+00	NM	0.98606	0.77021	0.84440	1.20193	0.70254	
15	1.3564"-03	3.5470"+00	NM	0.98618	0.77202	0.84580	1.20027	0.70468	
16	1.4300"-03	3.5741"+00	NM	0.98640	0.77553	0.84850	1.19705	0.70883	
17	1.5316"-03	3.6014"+00	NM	0.98662	0.77904	0.85120	1.19382	0.71301	
18	1.6332"-03	3.6557"+00	NM	0.98706	0.78599	0.85650	1.18745	0.72129	
19	1.7049"-03	3.6963"+00	NM	0.98739	0.79114	0.86040	1.18274	0.72746	
20	1.7932"-03	3.7375"+00	NM	0.98771	0.79633	0.86430	1.17801	0.73370	
21	1.8974"-03	3.7652"+00	NM	0.98793	0.79980	0.86690	1.17484	0.73789	
22	1.9685"-03	3.8062"+00	NM	0.98825	0.80490	0.87070	1.17019	0.74407	
23	2.0574"-03	3.8334"+00	NM	0.98846	0.80827	0.87320	1.16713	0.74816	
24	2.1463"-03	3.8674"+00	NM	0.98888	0.81491	0.87810	1.16109	0.75627	
25	2.2327"-03	3.9424"+00	NM	0.98930	0.82161	0.88300	1.15502	0.76449	
26	2.3216"-03	3.9834"+00	NM	0.98961	0.82657	0.88660	1.15033	0.77060	
27	2.4079"-03	4.0376"+00	NM	0.99002	0.83308	0.89130	1.14465	0.77866	
28	2.4968"-03	4.0786"+00	NM	0.99032	0.83796	0.89480	1.14026	0.78474	
29	2.5679"-03	4.1475"+00	NM	0.99082	0.84612	0.90060	1.13293	0.79493	
30	2.6568"-03	4.2020"+00	NM	0.99122	0.85250	0.90510	1.12721	0.80296	
31	2.7305"-03	4.2710"+00	NM	0.99171	0.86051	0.91070	1.12006	0.81308	
32	2.8169"-03	4.3388"+00	NM	0.99219	0.86831	0.91610	1.11312	0.82301	
33	2.9058"-03	4.4078"+00	NM	0.99267	0.87618	0.92150	1.10613	0.83308	
34	2.9921"-03	4.4351"+00	NM	0.99286	0.87926	0.92360	1.10341	0.83704	
35	3.0658"-03	4.4901"+00	NM	0.99324	0.88545	0.92780	1.09794	0.84504	
36	3.1674"-03	4.5313"+00	NM	0.99352	0.89006	0.93090	1.09388	0.85101	
37	3.2410"-03	4.5581"+00	NM	0.99370	0.89304	0.93290	1.09126	0.85488	
38	3.4163"-03	4.5864"+00	NM	0.99389	0.89619	0.93500	1.08850	0.85898	
39	3.6068"-03	4.6410"+00	NM	0.99426	0.90221	0.93900	1.08322	0.86686	
40	3.7541"-03	4.6943"+00	NM	0.99462	0.90827	0.94300	1.07793	0.87483	
41	3.9294"-03	4.7243"+00	NM	0.99480	0.91132	0.94500	1.07527	0.87885	
42	4.1046"-03	4.7652"+00	NM	0.99507	0.91577	0.94790	1.07141	0.88472	
43	4.2647"-03	4.8339"+00	NM	0.99551	0.92317	0.95270	1.06499	0.89456	
44	4.4120"-03	4.8892"+00	NM	0.99587	0.92909	0.95650	1.05988	0.90246	
45	4.5872"-03	4.9586"+00	NM	0.99630	0.93646	0.96120	1.05350	0.91235	
46	4.7473"-03	5.0261"+00	NM	0.99673	0.94358	0.96570	1.04744	0.92196	
47	4.8920"-03	5.0687"+00	NM	0.99699	0.94804	0.96850	1.04363	0.92801	
48	5.0698"-03	5.1242"+00	NM	0.99733	0.95381	0.97210	1.03871	0.93587	
49	5.2578"-03	5.2056"+00	NM	0.99782	0.96222	0.97730	1.03156	0.94738	
50	5.4331"-03	5.2485"+00	NM	0.99808	0.96463	0.98000	1.02786	0.95343	
51	5.5956"-03	5.2886"+00	NM	0.99832	0.97072	0.98250	1.02441	0.95909	
52	5.7556"-03	5.3716"+00	NM	0.99880	0.97915	0.98760	1.01734	0.97077	
53	5.9157"-03	5.4185"+00	NM	0.99905	0.98347	0.99020	1.01372	0.97680	
54	6.0762"-03	5.4562"+00	NM	0.99929	0.98766	0.99270	1.01024	0.98264	
55	6.2362"-03	5.5101"+00	NM	0.99960	0.99305	0.99590	1.00576	0.99020	
56	6.3856"-03	5.5254"+00	NM	0.99969	0.99457	0.99680	1.00450	0.99234	
57	6.5735"-03	5.5391"+00	NM	0.99977	0.99592	0.99760	1.00337	0.99425	
58	6.7361"-03	5.5527"+00	NM	0.99984	0.99728	0.99840	1.00225	0.99616	
59	6.8961"-03	5.5665"+00	NM	0.99992	0.99864	0.99920	1.00113	0.99808	
0 60	7.0409"-03	5.5802"+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES

Y, U/UD

ASSUME P=PD AND VAN DRIEST

71020206		PEAKE	PROFILE TABULATION			61 POINTS, DELTA AT POINT 61		
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TP	RHO/RHO0*U/UD
1	0.0000"+00	1.0000"+00	NM	0.95079	0.00000	0.00000	1.72057	0.00000
2	2.2660"-04	1.9625"+00	NM	0.96947	0.51226	0.61620	1.44697	0.42586
3	3.2512"-04	2.3152"+00	NM	0.97374	0.58037	0.68290	1.38453	0.49324
4	4.0132"-04	2.4977"+00	NM	0.97573	0.61160	0.71200	1.35528	0.52535
5	4.9022"-04	2.7572"+00	NM	0.97840	0.65283	0.74900	1.31633	0.56901
6	5.6388"-04	2.9096"+00	NM	0.97987	0.67567	0.78880	1.29467	0.59382
7	6.4008"-04	3.0630"+00	NM	0.98131	0.69778	0.78750	1.27370	0.61828
8	7.1374"-04	3.1859"+00	NM	0.98242	0.71494	0.80170	1.25744	0.63756
9	7.8486"-04	3.2934"+00	NM	0.98336	0.72958	0.81360	1.24359	0.65423
10	8.8900"-04	3.3700"+00	NM	0.98402	0.73981	0.82180	1.23393	0.66600
11	9.6012"-04	3.4633"+00	NM	0.98481	0.75207	0.83150	1.22237	0.68023
12	1.0338"-03	3.4938"+00	NM	0.98507	0.75603	0.83460	1.21865	0.68886
13	1.1074"-03	3.5245"+00	NM	0.98532	0.76000	0.83770	1.21492	0.68951
14	1.1811"-03	3.5860"+00	NM	0.98583	0.76789	0.84380	1.20753	0.69878
15	1.2522"-03	3.6178"+00	NM	0.98608	0.77191	0.84690	1.20375	0.70355
16	1.3411"-03	3.6791"+00	NM	0.98658	0.77963	0.85280	1.19652	0.71273
17	1.4148"-03	3.7107"+00	NM	0.98683	0.78358	0.85580	1.19283	0.71745
18	1.5011"-03	3.7880"+00	NM	0.98744	0.79314	0.86380	1.18391	0.72894
19	1.5748"-03	3.8185"+00	NM	0.98768	0.79699	0.86580	1.18042	0.73347
20	1.6637"-03	3.8986"+00	NM	0.98792	0.80066	0.86860	1.17692	0.73803
21	1.7501"-03	3.8649"+00	NM	0.98804	0.80254	0.87000	1.17517	0.74032
22	1.8390"-03	3.8962"+00	NM	0.98828	0.80633	0.87280	1.17165	0.74493
23	1.9101"-03	3.9426"+00	NM	0.98863	0.81191	0.87690	1.16649	0.75175
24	1.9837"-03	3.9746"+00	NM	0.98887	0.81575	0.87970	1.16294	0.75644
25	2.0726"-03	4.0058"+00	NM	0.98911	0.81946	0.88240	1.15951	0.76101
26	2.1463"-03	4.0361"+00	NM	0.98933	0.82305	0.88500	1.15620	0.76544
27	2.2327"-03	4.0833"+00	NM	0.98968	0.82860	0.88900	1.15109	0.77231
28	2.2911"-03	4.1456"+00	NM	0.99014	0.83588	0.89420	1.14401	0.78137
29	2.3927"-03	4.2090"+00	NM	0.99060	0.84322	0.89940	1.13769	0.79055
30	2.4663"-03	4.2548"+00	NM	0.99092	0.84848	0.90310	1.13288	0.79717
31	2.6264"-03	4.3645"+00	NM	0.99170	0.86099	0.91180	1.12150	0.81302
32	2.7737"-03	4.4600"+00	NM	0.99236	0.87164	0.91910	1.11187	0.82662
33	2.9337"-03	4.5535"+00	NM	0.99299	0.88197	0.92610	1.10257	0.83995
34	3.0810"-03	4.7122"+00	NM	0.99405	0.89925	0.93760	1.08712	0.86246
35	3.2258"-03	4.8223"+00	NM	0.99476	0.91102	0.94530	1.07667	0.87798
36	3.4163"-03	4.9176"+00	NM	0.99537	0.92109	0.95180	1.06779	0.89137
37	3.5636"-03	4.9885"+00	NM	0.99576	0.92767	0.95600	1.06202	0.90018
38	3.7236"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
39	3.8710"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
40	4.0157"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
41	4.1758"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
42	4.3383"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
43	4.4704"-03	5.0612"+00	NM	0.99626	0.93604	0.96130	1.05469	0.91145
44	4.6304"-03	5.0920"+00	NM	0.99645	0.93923	0.96330	1.05192	0.91575
45	4.7752"-03	5.1403"+00	NM	0.99675	0.94419	0.96640	1.04761	0.92248
46	4.9225"-03	5.1718"+00	NM	0.99694	0.94740	0.96840	1.04482	0.92686
47	5.0978"-03	5.2035"+00	NM	0.99713	0.95063	0.97040	1.04203	0.93126
48	5.2451"-03	5.2315"+00	NM	0.99742	0.95550	0.97340	1.03782	0.93792
49	5.4051"-03	5.3000"+00	NM	0.99770	0.96039	0.97640	1.03381	0.94465
50	5.5499"-03	5.3475"+00	NM	0.99798	0.96516	0.97930	1.02952	0.95122
51	5.5972"-03	5.3955"+00	NM	0.99826	0.96995	0.98220	1.02542	0.95785
52	5.8725"-03	5.4440"+00	NM	0.99854	0.97477	0.98510	1.02131	0.96454
53	5.9893"-03	5.4931"+00	NM	0.99883	0.97962	0.98800	1.01719	0.97130
54	6.1366"-03	5.5720"+00	NM	0.99927	0.98737	0.99260	1.01062	0.98216
55	6.2967"-03	5.6050"+00	NM	0.99946	0.99059	0.99450	1.00790	0.98670
56	6.4567"-03	5.6050"+00	NM	0.99946	0.99059	0.99450	1.00790	0.98670
57	6.6192"-03	5.6208"+00	NM	0.99955	0.99212	0.99540	1.00661	0.98806
58	6.7640"-03	5.6366"+00	NM	0.99964	0.99366	0.99630	1.00532	0.99103
59	6.9240"-03	5.6542"+00	NM	0.99973	0.99537	0.99730	1.00389	0.99344
60	7.0714"-03	5.6860"+00	NM	0.99991	0.99845	0.99910	1.00130	0.99781
D 61	7.2187"-03	5.7020"+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y, U/UD ASSUME P=PO AND VAN DRIEST

SECTION D - SUPPLEMENTARY DATA - CAT 7102Wall pressure and wall shear stress correlationsFACSIMILE FROM SOURCE PAPER - NB - AUTHORS' SYMBOLS AND UNITS

Table 2: Zero pressure gradient - profiles 0101 - 0106

Table 3: Adverse pressure gradient - profiles 0201 - 0206

Table 4: "Ring" pressure gradient - profiles 0301 - 0306

SYMBOLS (where not as in CAT)

- Subscripts: 0 - Reservoir stagnation state
 E - Boundary layer edge ($\bar{0}$) state
- AP_{F+W} - Static pressure hole-size correction based on wall property values using the deep hole correlation of Franklin + Wallace (1970)
- T' - Reference temperature as specified by Sommer and Short (1955)
- C_{pp} - Preston tube pressure coefficient
 ($= (P_p - P_E) / q_E$ where P_p is the Preston tube pressure and q_E is the free stream dynamic pressure)
- R_D - Reynolds' number based on Preston tube diameter and local free-stream conditions.
- $(u_{TW} d_s / \nu_w)$ - Wall-similarity static hole Reynolds number.
 (d_s - static hole diameter)

Subscripts to CF indicate the Preston tube correlation used as:

- F + S - Fenter & Stalmach (1957)
 HKTR - Hopkins & Keener (1966) Equation 9
 HKT' - Hopkins & Keener (1966) Equation 4
 SIG - Sigalla (1966)

UNITS - are indicated at the foot of each table.

TABLE 2: SKIN FRICTION CORRELATIONS IN ZERO PRESSURE GRADIENT FLOW

CF CALCULATED FROM CORRELATIONS BY FENTER & STALMACH, HOPKINS & KEENER, AND SIGALLA;
 HOPKINS & KEENER CORRELATION WITH (1): ADIABATIC WALL RECOVERY TEMPERATURE, °R, AND (2): INTERMEDIATE TEMPERATURE, °F, AS INPUT;
 STATIC PRESSURES CORRECTED FOR HOLE ERROR GIVEN BY FRANKLIN & WALLACE

Pc = 168.9 PSIA; T0 = 537.0 °R

X	Pw	ΔP	PAW	ME	UE	TE	OE	TR	T'	CPP	RD	$\frac{u_{rms}}{v_w}$	Cp	PLS	Cp	HCTR	Cp	HKT'	uTW	Cp	SIG
0.03	1.187	0.025	3.952	2210.5	130.2	0.00076	492.3	364.3	0.420	0.230E	05	0.247E	03	0.00143	0.00227	0.00187	131.2	0.00157			
0.53	1.205	0.012	3.941	2208.9	130.8	0.00077	492.3	364.6	0.234	0.231E	05	0.199E	03	0.00103	0.00137	0.00118	104.1	0.00113			
1.03	1.215	0.005	3.934	2208.0	131.1	0.00078	492.4	364.7	0.132	0.232E	05	0.162E	03	0.00073	0.00084	0.00078	84.2	0.00087			
1.53	1.220	0.003	3.931	2207.7	131.3	0.00078	492.4	364.8	0.093	0.232E	05	0.144E	03	0.00059	0.00062	0.00060	74.4	0.00072			
2.03	1.222	0.003	3.930	2207.4	131.3	0.00078	492.4	364.8	0.089	0.232E	05	0.141E	03	0.00057	0.00059	0.00059	73.1	0.00070			
2.53	1.223	0.005	3.929	2207.4	131.4	0.00078	492.4	364.8	0.115	0.232E	05	0.155E	03	0.00067	0.00074	0.00070	79.9	0.00082			
3.03	1.222	0.007	3.930	2207.4	131.3	0.00078	492.4	364.8	0.161	0.232E	05	0.175E	03	0.00082	0.00099	0.00089	90.2	0.00097			
3.53	1.220	0.010	3.931	2207.6	131.3	0.00078	492.4	364.8	0.207	0.232E	05	0.191E	03	0.00095	0.00123	0.00107	99.1	0.00111			
4.03	1.219	0.014	3.932	2207.7	131.2	0.00078	492.4	364.8	0.264	0.232E	05	0.209E	03	0.00110	0.00151	0.00129	108.6	0.00126			
4.53	1.219	0.015	3.932	2207.8	131.2	0.00078	492.4	364.7	0.280	0.232E	05	0.214E	03	0.00114	0.00159	0.00135	111.2	0.00129			
5.03	1.219	0.016	3.932	2207.7	131.2	0.00078	492.4	364.8	0.292	0.232E	05	0.218E	03	0.00117	0.00165	0.00139	112.9	0.00132			
5.53	1.219	0.016	3.932	2207.7	131.2	0.00078	492.4	364.8	0.303	0.232E	05	0.221E	03	0.00119	0.00171	0.00144	114.6	0.00134			
6.03	1.220	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.303	0.232E	05	0.221E	03	0.00119	0.00170	0.00144	114.6	0.00134			
6.53	1.220	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.300	0.232E	05	0.221E	03	0.00119	0.00169	0.00143	114.2	0.00132			
7.03	1.220	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.294	0.232E	05	0.219E	03	0.00117	0.00166	0.00140	113.2	0.00132			
7.53	1.222	0.015	3.930	2207.5	131.3	0.00078	492.4	364.8	0.285	0.232E	05	0.216E	03	0.00115	0.00161	0.00137	111.8	0.00130			
8.03	1.223	0.014	3.929	2207.4	131.4	0.00078	492.4	364.8	0.272	0.232E	05	0.212E	03	0.00112	0.00155	0.00132	109.8	0.00127			
8.53	1.225	0.013	3.928	2207.3	131.4	0.00078	492.4	364.8	0.259	0.232E	05	0.209E	03	0.00109	0.00149	0.00127	107.7	0.00124			
9.03	1.226	0.012	3.928	2207.1	131.4	0.00078	492.4	364.8	0.246	0.232E	05	0.205E	03	0.00106	0.00142	0.00122	105.5	0.00121			
9.53	1.227	0.012	3.927	2207.1	131.5	0.00078	492.4	364.9	0.238	0.232E	05	0.202E	03	0.00104	0.00138	0.00119	104.2	0.00119			
10.03	1.227	0.011	3.927	2207.0	131.5	0.00078	492.4	364.9	0.231	0.232E	05	0.199E	03	0.00102	0.00135	0.00117	103.1	0.00117			
10.53	1.228	0.011	3.926	2207.0	131.5	0.00078	492.4	364.9	0.226	0.232E	05	0.198E	03	0.00101	0.00132	0.00115	102.2	0.00116			
11.03	1.229	0.011	3.926	2206.9	131.5	0.00078	492.4	364.9	0.223	0.232E	05	0.198E	03	0.00100	0.00131	0.00114	101.8	0.00115			
11.53	1.229	0.011	3.926	2206.9	131.6	0.00078	492.4	364.9	0.221	0.232E	05	0.197E	03	0.00099	0.00129	0.00113	101.3	0.00115			
12.03	1.230	0.011	3.925	2206.8	131.6	0.00078	492.4	364.9	0.219	0.232E	05	0.197E	03	0.00099	0.00129	0.00112	101.0	0.00114			
12.53	1.232	0.011	3.924	2206.7	131.6	0.00079	492.4	364.9	0.219	0.232E	05	0.197E	03	0.00099	0.00129	0.00112	100.9	0.00114			
13.03	1.234	0.011	3.923	2206.4	131.7	0.00079	492.4	365.0	0.217	0.232E	05	0.196E	03	0.00098	0.00128	0.00111	100.6	0.00114			
13.53	1.234	0.011	3.923	2206.2	131.8	0.00079	492.4	365.0	0.215	0.232E	05	0.196E	03	0.00098	0.00127	0.00110	100.2	0.00113			
14.03	1.241	0.011	3.921	2205.9	131.9	0.00079	492.4	365.0	0.213	0.232E	05	0.196E	03	0.00097	0.00126	0.00110	99.8	0.00113			
14.53	1.246	0.011	3.919	2205.9	132.1	0.00079	492.5	365.1	0.213	0.232E	05	0.196E	03	0.00097	0.00125	0.00109	99.6	0.00112			
15.03	1.252	0.011	3.916	2205.5	132.2	0.00079	492.5	365.2	0.210	0.232E	05	0.196E	03	0.00096	0.00124	0.00108	99.0	0.00112			
15.53	1.256	0.011	3.909	2205.0	132.4	0.00080	492.5	365.2	0.209	0.232E	05	0.196E	03	0.00096	0.00123	0.00108	98.8	0.00111			
16.03	1.261	0.011	3.907	2204.2	132.5	0.00080	492.5	365.3	0.207	0.232E	05	0.196E	03	0.00095	0.00122	0.00107	98.3	0.00111			
16.53	1.265	0.011	3.904	2203.9	132.6	0.00080	492.5	365.3	0.207	0.232E	05	0.196E	03	0.00095	0.00121	0.00106	98.1	0.00111			
17.03	1.268	0.010	3.903	2203.7	132.7	0.00080	492.5	365.4	0.205	0.232E	05	0.196E	03	0.00095	0.00120	0.00105	97.4	0.00110			
17.53	1.269	0.010	3.902	2203.6	132.8	0.00080	492.5	365.4	0.205	0.232E	05	0.196E	03	0.00095	0.00120	0.00105	97.7	0.00110			
18.03	1.271	0.010	3.901	2203.5	132.8	0.00080	492.5	365.4	0.203	0.232E	05	0.196E	03	0.00094	0.00120	0.00105	97.1	0.00109			
18.53	1.271	0.010	3.901	2203.4	132.8	0.00080	492.5	365.4	0.202	0.232E	05	0.196E	03	0.00094	0.00119	0.00105	97.1	0.00109			
19.03	1.271	0.010	3.901	2203.4	132.8	0.00080	492.5	365.4	0.201	0.232E	05	0.195E	03	0.00093	0.00118	0.00104	96.9	0.00109			
19.53	1.270	0.010	3.901	2203.3	132.8	0.00080	492.5	365.4	0.200	0.232E	05	0.194E	03	0.00093	0.00118	0.00104	96.8	0.00109			
20.03	1.270	0.010	3.901	2203.3	132.7	0.00080	492.5	365.4	0.200	0.232E	05	0.194E	03	0.00093	0.00118	0.00104	96.8	0.00109			
20.53	1.269	0.010	3.902	2203.6	132.7	0.00080	492.5	365.4	0.199	0.232E	05	0.194E	03	0.00093	0.00118	0.00104	96.7	0.00108			
21.03	1.267	0.010	3.903	2203.7	132.7	0.00080	492.5	365.4	0.199	0.232E	05	0.194E	03	0.00093	0.00118	0.00104	96.7	0.00108			

TABLE 2: (continued)

X	P _W	AP _{P&W}	M _E	U _E	T _E	ρ _E	T _R	T _I	C _{PP}	R _D	$\frac{U_{TMS}}{V_W}$	C _P P&S	C _F EKTR	C _F EKTR†	U _{TM}	C _P SIG
22.03	1.265	0.010	3.904	2203.9	132.6	0.00080	492.5	365.3	0.198	0.235E 05	0.193E 03	0.00093	0.00117	0.00103	96.6	0.00108
22.53	1.263	0.010	3.905	2204.1	132.6	0.00080	492.5	365.3	0.197	0.235E 05	0.193E 03	0.00093	0.00117	0.00103	96.4	0.00108
23.03	1.260	0.010	3.907	2204.3	132.5	0.00080	492.5	365.3	0.196	0.235E 05	0.192E 03	0.00092	0.00116	0.00103	96.4	0.00108
23.53	1.257	0.010	3.909	2204.6	132.4	0.00080	492.5	365.2	0.196	0.235E 05	0.191E 03	0.00092	0.00116	0.00103	96.3	0.00107
24.03	1.254	0.010	3.911	2204.9	132.3	0.00080	492.5	365.2	0.195	0.234E 05	0.191E 03	0.00092	0.00116	0.00102	96.2	0.00107
24.53	1.250	0.009	3.913	2205.2	132.2	0.00079	492.5	365.1	0.194	0.234E 05	0.190E 03	0.00092	0.00116	0.00102	96.2	0.00107
25.03	1.247	0.009	3.915	2205.4	132.1	0.00079	492.4	365.1	0.194	0.234E 05	0.190E 03	0.00092	0.00115	0.00102	96.1	0.00107
25.53	1.242	0.009	3.918	2205.8	131.9	0.00079	492.4	365.1	0.193	0.234E 05	0.189E 03	0.00091	0.00115	0.00102	96.1	0.00107
26.03	1.239	0.009	3.920	2206.1	131.8	0.00079	492.4	365.0	0.192	0.233E 05	0.188E 03	0.00091	0.00115	0.00102	96.1	0.00107
26.53	1.236	0.009	3.922	2206.3	131.8	0.00079	492.4	365.0	0.193	0.233E 05	0.188E 03	0.00091	0.00115	0.00102	96.2	0.00107
27.03	1.233	0.009	3.923	2206.6	131.7	0.00078	492.4	364.9	0.193	0.233E 05	0.188E 03	0.00092	0.00115	0.00102	96.3	0.00107
27.53	1.230	0.009	3.925	2206.8	131.6	0.00078	492.4	364.9	0.194	0.233E 05	0.188E 03	0.00092	0.00116	0.00102	96.5	0.00107
28.03	1.226	0.009	3.927	2207.1	131.5	0.00078	492.4	364.8	0.194	0.233E 05	0.188E 03	0.00092	0.00116	0.00102	96.7	0.00107
28.53	1.223	0.009	3.929	2207.4	131.4	0.00078	492.4	364.8	0.195	0.232E 05	0.187E 03	0.00092	0.00117	0.00103	96.8	0.00108
29.03	1.220	0.009	3.931	2207.6	131.3	0.00078	492.4	364.8	0.196	0.232E 05	0.187E 03	0.00092	0.00117	0.00103	97.0	0.00108
29.53	1.217	0.009	3.933	2207.9	131.2	0.00078	492.4	364.7	0.196	0.232E 05	0.187E 03	0.00092	0.00117	0.00103	97.2	0.00108
30.03	1.214	0.009	3.935	2208.2	131.1	0.00078	492.3	364.7	0.197	0.232E 05	0.187E 03	0.00093	0.00118	0.00103	97.3	0.00108
30.53	1.216	0.009	3.934	2208.0	131.1	0.00078	492.4	364.7	0.196	0.232E 05	0.187E 03	0.00093	0.00117	0.00103	97.2	0.00108
31.03	1.225	0.009	3.928	2207.2	131.4	0.00078	492.4	364.8	0.195	0.233E 05	0.188E 03	0.00092	0.00116	0.00103	96.8	0.00107
31.53	1.261	0.009	3.907	2204.2	132.5	0.00080	492.5	365.3	0.190	0.235E 05	0.190E 03	0.00091	0.00113	0.00100	95.2	0.00106
32.03	1.308	0.010	3.880	2200.4	133.9	0.00082	492.7	365.9	0.185	0.238E 05	0.193E 03	0.00089	0.00110	0.00098	93.3	0.00104
32.53	1.511	0.010	3.774	2185.0	139.5	0.00091	493.3	368.3	0.158	0.250E 05	0.203E 03	0.00080	0.00093	0.00086	85.1	0.00094

INS. PSIA PSIA FT/SEC °R SLUGS/ CU.FT. °R °R

FT/SEC

TABLE 3: SKIN FRICTION CORRELATIONS IN ADVERSE PRESSURE GRADIENT FLOW

CP CALCULATED FROM CORRELATIONS BY FENTER & STALWACH, HOPKINS & KEENER, AND SIGALLA; HOPKINS & KEENER CORRELATION WITH (U): ADIABATIC WALL RECOVERY TEMPERATURE, T_R, AND (C): INTERMEDIATE TEMPERATURE, T_I, AS INPUT; STATIC PRESSURES CORRECTED FOR HOLE ERROR GIVEN BY FRANKLIN & WALLACE

P₀ = 169.2 PSIA; T₀ = 537.0 °R

X	P _W	ΔP _{F&W}	M _E	u _E	T _E	ρ _E	T _R	T _I	C _{PP}	R _D	$\frac{u_{TW}^2 S}{vW}$	C _P P&S	C _P HKTR	C _P HKT	u _{TW}	C _P SIG
0.03	1.189	0.025	3.952	2210.5	130.2	0.00077	492.3	364.3	0.420	0.230E 05	0.247E 03	0.00143	0.00227	0.00186	131.2	0.00157
0.53	1.207	0.012	3.941	2208.9	130.8	0.00077	492.3	364.6	0.234	0.232E 05	0.159E 03	0.00103	0.00137	0.00118	164.1	0.00118
1.03	1.217	0.005	3.924	2208.0	131.1	0.00078	492.4	364.7	0.132	0.232E 05	0.162E 03	0.00073	0.00084	0.00077	84.2	0.00087
1.53	1.222	0.003	3.931	2207.7	131.3	0.00078	492.4	364.8	0.093	0.233E 05	0.144E 03	0.00059	0.00062	0.00060	74.3	0.00072
2.03	1.224	0.003	3.930	2207.4	131.3	0.00078	492.4	364.8	0.089	0.233E 05	0.142E 03	0.00057	0.00059	0.00059	73.1	0.00070
2.53	1.225	0.005	3.929	2207.4	131.4	0.00078	492.4	364.8	0.115	0.233E 05	0.155E 03	0.00067	0.00074	0.00070	79.9	0.00081
3.03	1.224	0.007	3.930	2207.4	131.3	0.00078	492.4	364.8	0.161	0.233E 05	0.175E 03	0.00082	0.00099	0.00089	90.2	0.00097
3.53	1.222	0.010	3.931	2207.6	131.3	0.00078	492.4	364.8	0.207	0.233E 05	0.192E 03	0.00095	0.00123	0.00107	99.1	0.00111
4.03	1.221	0.014	3.932	2207.7	131.2	0.00078	492.4	364.8	0.264	0.233E 05	0.210E 03	0.00110	0.00151	0.00129	108.6	0.00125
4.53	1.221	0.016	3.932	2207.8	131.2	0.00078	492.4	364.7	0.280	0.232E 05	0.218E 03	0.00114	0.00159	0.00135	111.2	0.00129
5.03	1.221	0.016	3.932	2207.7	131.2	0.00078	492.4	364.8	0.292	0.233E 05	0.218E 03	0.00117	0.00165	0.00139	112.9	0.00132
5.53	1.222	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.303	0.233E 05	0.221E 03	0.00119	0.00170	0.00144	114.6	0.00134
6.03	1.222	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.303	0.233E 05	0.222E 03	0.00119	0.00170	0.00144	114.6	0.00134
6.53	1.222	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.300	0.233E 05	0.221E 03	0.00119	0.00169	0.00143	114.1	0.00134
7.03	1.222	0.016	3.931	2207.6	131.3	0.00078	492.4	364.8	0.294	0.233E 05	0.219E 03	0.00115	0.00166	0.00140	113.2	0.00132
7.53	1.224	0.015	3.930	2207.5	131.3	0.00078	492.4	364.8	0.285	0.233E 05	0.219E 03	0.00115	0.00161	0.00137	111.8	0.00130
8.03	1.225	0.014	3.928	2207.4	131.4	0.00078	492.4	364.8	0.272	0.233E 05	0.213E 03	0.00112	0.00155	0.00132	109.7	0.00127
8.53	1.226	0.013	3.928	2207.3	131.4	0.00078	492.4	364.8	0.259	0.233E 05	0.209E 03	0.00109	0.00149	0.00127	107.6	0.00124
9.03	1.228	0.012	3.928	2207.1	131.4	0.00078	492.4	364.8	0.246	0.233E 05	0.205E 03	0.00106	0.00142	0.00122	105.5	0.00121
9.53	1.229	0.012	3.927	2207.1	131.5	0.00078	492.4	364.9	0.238	0.233E 05	0.203E 03	0.00104	0.00138	0.00119	104.2	0.00119
10.03	1.229	0.011	3.927	2207.0	131.5	0.00078	492.4	364.9	0.226	0.233E 05	0.199E 03	0.00101	0.00132	0.00115	102.2	0.00116
10.53	1.231	0.010	3.926	2206.9	131.5	0.00079	492.4	364.9	0.213	0.233E 05	0.195E 03	0.00097	0.00126	0.00110	100.0	0.00113
11.03	1.232	0.010	3.925	2206.8	131.6	0.00078	492.4	364.9	0.213	0.233E 05	0.195E 03	0.00097	0.00126	0.00110	100.0	0.00113
11.53	1.232	0.010	3.925	2206.8	131.6	0.00078	492.4	364.9	0.206	0.240E 05	0.205E 03	0.00095	0.00120	0.00106	96.6	0.00110
12.03	1.234	0.011	3.862	2197.9	134.8	0.00084	492.4	365.3	0.192	0.251E 05	0.218E 03	0.00090	0.00110	0.00099	91.4	0.00105
12.53	1.510	0.013	3.775	2185.2	139.5	0.00091	493.3	368.2	0.192	0.251E 05	0.218E 03	0.00090	0.00110	0.00099	88.6	0.00103
13.03	1.711	0.015	3.685	2171.3	144.5	0.00099	493.8	370.4	0.184	0.262E 05	0.239E 03	0.00089	0.00106	0.00097	82.6	0.00099
13.53	2.145	0.020	3.524	2144.4	154.2	0.00117	494.9	374.5	0.184	0.284E 05	0.275E 03	0.00087	0.00098	0.00092	84.0	0.00107
14.03	2.541	0.031	3.405	2122.9	161.8	0.00132	495.7	377.7	0.217	0.301E 05	0.334E 03	0.00095	0.00109	0.00102	84.0	0.00107
14.53	3.018	0.044	3.286	2099.7	170.0	0.00149	496.6	381.2	0.250	0.320E 05	0.398E 03	0.00102	0.00118	0.00111	84.6	0.00114
15.03	3.623	0.066	3.161	2073.5	179.1	0.00170	497.6	385.1	0.301	0.341E 05	0.487E 03	0.00114	0.00133	0.00125	86.5	0.00124
15.53	4.398	0.086	3.031	2043.8	189.3	0.00195	498.7	389.4	0.323	0.365E 05	0.574E 03	0.00118	0.00136	0.00129	84.4	0.00127
16.03	5.168	0.111	2.924	2017.4	196.2	0.00219	499.7	393.2	0.361	0.386E 05	0.671E 03	0.00128	0.00145	0.00138	81.2	0.00133
16.53	6.293	0.137	2.794	1982.9	209.7	0.00252	501.0	398.0	0.378	0.413E 05	0.784E 03	0.00128	0.00144	0.00140	84.2	0.00140
17.03	7.451	0.164	2.684	1951.3	220.0	0.00284	502.1	402.4	0.401	0.437E 05	0.902E 03	0.00132	0.00147	0.00144	79.2	0.00138
17.53	8.983	0.188	2.563	1913.7	232.1	0.00325	503.5	407.6	0.405	0.466E 05	1.039E 03	0.00133	0.00142	0.00143	75.5	0.00137
18.03	10.416	0.210	2.468	1882.0	242.1	0.00361	504.6	411.8	0.413	0.489E 05	1.155E 03	0.00135	0.00141	0.00144	72.9	0.00138
18.53	11.948	0.235	2.368	1850.9	251.8	0.00398	505.6	415.9	0.430	0.511E 05	1.288E 03	0.00138	0.00142	0.00147	71.1	0.00140
19.03	13.841	0.254	2.286	1815.4	262.6	0.00442	506.8	420.5	0.429	0.535E 05	1.419E 03	0.00138	0.00137	0.00145	67.9	0.00143
19.53	16.479	0.273	2.174	1770.5	276.0	0.00501	508.3	426.2	0.421	0.564E 05	1.568E 03	0.00137	0.00131	0.00142	64.0	0.00138
20.03	18.999	0.291	2.083	1731.2	287.5	0.00555	509.6	431.1	0.420	0.589E 05	1.738E 03	0.00137	0.00127	0.00141	61.2	0.00137
20.53	20.378	0.317	2.038	1710.9	293.3	0.00583	510.2	433.6	0.453	0.606E 05	1.868E 03	0.00144	0.00134	0.00149	61.5	0.00143
21.03	20.981	0.339	2.019	1702.3	295.6	0.00595	510.5	434.6	0.489	0.606E 05	1.957E 03	0.00151	0.00142	0.00157	62.6	0.00149

TABLE 3: (continued)

X	P _W	AP _{FEV}	M _E	U _E	T _E	ρ _E	T _R	T _I	C _{PP}	R _D	$\frac{u_{rms}}{v_w}$	C _P P&S	C _P HKTR	C _P HKT'	U _{TW}	C _P SIG		
22.03	21.361	0.348	2.008	1696.9	297.3	0.00603	510.6	435.2	0.502	0.609E	05	0.199E	04	0.00154	0.00145	0.00160	62.9	0.00152
22.53	21.608	0.355	2.001	1693.4	298.3	0.00608	510.7	435.7	0.512	0.611E	05	0.202E	04	0.00156	0.00147	0.00162	63.1	0.00153
23.03	21.758	0.357	1.996	1691.3	298.9	0.00611	510.8	436.1	0.514	0.612E	05	0.203E	04	0.00156	0.00147	0.00163	63.0	0.00154
23.53	21.859	0.358	1.993	1689.9	299.3	0.00613	510.8	436.1	0.514	0.613E	05	0.204E	04	0.00156	0.00146	0.00163	62.9	0.00154
24.03	21.918	0.357	1.990	1688.3	299.7	0.00615	510.9	436.3	0.512	0.614E	05	0.204E	04	0.00156	0.00146	0.00162	62.7	0.00153
24.53	22.013	0.356	1.989	1687.8	299.9	0.00616	510.9	436.3	0.509	0.614E	05	0.204E	04	0.00155	0.00146	0.00161	62.6	0.00153
25.03	22.066	0.354	1.987	1687.1	300.2	0.00617	510.9	436.4	0.505	0.614E	05	0.204E	04	0.00155	0.00144	0.00160	62.4	0.00152
25.53	22.101	0.353	1.986	1686.6	300.2	0.00618	511.0	436.5	0.502	0.614E	05	0.204E	04	0.00154	0.00144	0.00160	62.2	0.00152
26.03	22.059	0.351	1.987	1687.0	300.1	0.00617	510.9	436.4	0.498	0.614E	05	0.203E	04	0.00153	0.00143	0.00159	62.0	0.00151
26.53	22.038	0.348	1.988	1687.4	299.9	0.00616	510.9	436.4	0.493	0.614E	05	0.202E	04	0.00153	0.00142	0.00158	61.9	0.00150
27.03	22.024	0.345	1.988	1687.6	299.9	0.00616	510.9	436.3	0.488	0.614E	05	0.201E	04	0.00152	0.00141	0.00157	61.6	0.00149
27.53	21.994	0.342	1.989	1688.1	299.8	0.00616	510.9	436.3	0.482	0.614E	05	0.200E	04	0.00150	0.00139	0.00155	61.4	0.00148
28.03	21.912	0.340	1.992	1689.2	299.5	0.00614	510.9	436.2	0.478	0.613E	05	0.199E	04	0.00150	0.00138	0.00154	61.3	0.00148
28.53	21.796	0.337	1.995	1690.8	299.0	0.00612	510.8	436.0	0.474	0.612E	05	0.198E	04	0.00149	0.00137	0.00153	61.2	0.00147
29.03	21.530	0.333	2.000	1693.1	298.3	0.00608	510.7	435.7	0.470	0.611E	05	0.196E	04	0.00148	0.00136	0.00152	61.2	0.00146
29.53	21.497	0.331	2.004	1695.0	297.8	0.00606	510.7	435.5	0.466	0.610E	05	0.195E	04	0.00147	0.00136	0.00152	61.1	0.00146
30.03	21.366	0.326	2.008	1696.8	297.3	0.00603	510.6	435.2	0.460	0.609E	05	0.193E	04	0.00146	0.00134	0.00150	60.9	0.00144
30.53	21.337	0.322	2.009	1697.2	297.2	0.00602	510.6	435.2	0.452	0.608E	05	0.192E	04	0.00144	0.00132	0.00148	60.6	0.00143
31.03	21.308	0.317	2.010	1697.6	297.1	0.00602	510.6	435.2	0.443	0.608E	05	0.192E	04	0.00143	0.00130	0.00146	60.2	0.00141
31.53	21.228	0.312	2.012	1698.8	296.8	0.00600	510.6	435.0	0.435	0.608E	05	0.189E	04	0.00141	0.00128	0.00144	59.9	0.00140
32.03	21.233	0.307	2.012	1698.7	296.8	0.00600	510.6	435.0	0.425	0.608E	05	0.187E	04	0.00139	0.00125	0.00142	59.4	0.00138
32.53	21.239	0.301	2.012	1698.6	296.8	0.00601	510.6	435.0	0.413	0.608E	05	0.185E	04	0.00137	0.00123	0.00139	58.8	0.00136

IMS. PSIA

FT/SEC °R SLUGS/
CU.FT.

°R

FT/SEC

TABLE 4: SKIN FRICTION CORRELATIONS IN RING PRESSURE GRADIENT FLOW


CF CALCULATED FROM CORRELATIONS BY FENTER & STALKACH, HOPKINS & KEENER, AND SIGALLA;
 HOPKINS & KEENER CORRELATION WITH (1): ADIABATIC WALL, RECOVERY TEMPERATURE, TR, AND (2): INTERMEDIATE TEMPERATURE, T', AS INPUT
 STATIC PRESSURES CORRECTED FOR HOLE ERROR GIVEN BY FRANKLIN & WALLACE

P₀ = 120.7 PSIA; T₀ = 537.0 °R

X	P _w	ΔP FEM	M _E	U _E	T _E	PE	T _R	T'	C _{PP}	F _D	$\frac{U_{TW}^2}{\rho W}$	C _F PMS	C _F HKTR	C _F HKT	U _{TW}	C _F SLU
11.53	1.044	0.007	3.798	2188.6	138.2	0.00663	493.1	367.7	0.224	0.177E 05	0.167E 03	0.00106	0.00139	0.00121	101.5	0.00124
12.03	1.123	0.008	3.775	2180.6	141.1	0.00667	493.5	369.0	0.218	0.181E 05	0.175E 03	0.00104	0.00133	0.00117	98.7	0.00121
12.53	1.173	0.008	3.743	2175.7	142.9	0.00669	493.6	369.7	0.206	0.186E 05	0.177E 03	0.00101	0.00126	0.00112	95.6	0.00118
13.03	1.212	0.008	3.689	2172.0	144.3	0.00671	493.8	370.3	0.194	0.186E 05	0.177E 03	0.00097	0.00119	0.00107	92.8	0.00114
13.53	1.240	0.007	3.673	2169.5	145.2	0.00672	493.9	370.7	0.185	0.188E 05	0.177E 03	0.00094	0.00113	0.00103	90.7	0.00111
14.03	1.260	0.007	3.662	2167.6	145.9	0.00672	494.0	371.0	0.180	0.189E 05	0.177E 03	0.00093	0.00110	0.00101	89.4	0.00109
14.53	1.278	0.007	3.651	2165.9	146.5	0.00673	494.0	371.2	0.179	0.190E 05	0.179E 03	0.00092	0.00109	0.00100	88.8	0.00108
15.03	1.304	0.008	3.637	2162.8	147.6	0.00675	494.1	371.6	0.181	0.191E 05	0.181E 03	0.00092	0.00109	0.00099	88.4	0.00109
15.53	1.313	0.008	3.632	2162.8	147.6	0.00675	494.2	371.7	0.181	0.192E 05	0.183E 03	0.00093	0.00110	0.00100	88.7	0.00109
16.03	1.325	0.008	3.626	2161.7	148.0	0.00675	494.2	371.9	0.182	0.192E 05	0.185E 03	0.00093	0.00110	0.00101	88.6	0.00109
16.53	1.332	0.008	3.622	2161.1	148.2	0.00675	494.2	371.9	0.184	0.193E 05	0.186E 03	0.00093	0.00111	0.00101	88.8	0.00109
17.03	1.343	0.008	3.616	2160.1	148.6	0.00676	494.3	372.1	0.183	0.193E 05	0.187E 03	0.00093	0.00110	0.00101	88.5	0.00109
17.53	1.353	0.008	3.611	2159.2	148.9	0.00676	494.3	372.2	0.183	0.194E 05	0.188E 03	0.00093	0.00110	0.00101	88.3	0.00109
18.03	1.358	0.008	3.608	2158.8	149.0	0.00676	494.3	372.3	0.182	0.194E 05	0.188E 03	0.00093	0.00109	0.00100	88.1	0.00109
18.53	1.362	0.009	3.606	2158.5	149.1	0.00677	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.2	0.00109
19.03	1.360	0.009	3.607	2158.6	149.1	0.00677	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.3	0.00109
19.53	1.358	0.009	3.608	2158.8	149.0	0.00676	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.3	0.00109
20.03	1.358	0.009	3.608	2158.8	149.0	0.00676	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.3	0.00109
20.53	1.358	0.009	3.608	2158.8	149.0	0.00676	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.3	0.00109
21.03	1.358	0.009	3.608	2158.8	149.0	0.00676	494.3	372.3	0.183	0.194E 05	0.189E 03	0.00093	0.00110	0.00101	88.3	0.00109
21.53	1.350	0.008	3.612	2159.5	148.8	0.00676	494.3	372.2	0.185	0.194E 05	0.188E 03	0.00094	0.00111	0.00102	88.7	0.00110
22.03	1.345	0.008	3.615	2160.0	148.6	0.00676	494.3	372.1	0.186	0.193E 05	0.188E 03	0.00094	0.00111	0.00102	88.9	0.00110
22.53	1.338	0.008	3.619	2160.6	148.4	0.00676	494.3	372.0	0.187	0.193E 05	0.188E 03	0.00094	0.00112	0.00102	89.2	0.00110
23.03	1.337	0.008	3.620	2160.7	148.3	0.00676	494.2	372.0	0.186	0.193E 05	0.187E 03	0.00094	0.00112	0.00102	89.1	0.00110
23.53	1.337	0.008	3.619	2160.7	148.3	0.00676	494.2	372.0	0.186	0.193E 05	0.187E 03	0.00094	0.00112	0.00102	89.1	0.00110
24.03	1.337	0.008	3.619	2160.7	148.3	0.00676	494.2	372.0	0.186	0.193E 05	0.187E 03	0.00094	0.00112	0.00102	89.1	0.00110
24.53	1.330	0.008	3.623	2161.3	148.1	0.00675	494.2	371.9	0.183	0.193E 05	0.185E 03	0.00093	0.00110	0.00101	88.6	0.00109
25.03	1.328	0.008	3.624	2161.4	148.1	0.00675	494.2	371.9	0.183	0.193E 05	0.185E 03	0.00093	0.00110	0.00101	88.7	0.00109
25.53	1.330	0.008	3.623	2161.3	148.1	0.00675	494.2	371.9	0.184	0.193E 05	0.186E 03	0.00093	0.00111	0.00101	88.9	0.00109
26.03	1.337	0.008	3.623	2161.3	148.1	0.00675	494.2	371.9	0.184	0.193E 05	0.186E 03	0.00093	0.00111	0.00101	88.9	0.00109
26.53	1.342	0.008	3.617	2160.3	148.5	0.00676	494.3	372.1	0.183	0.193E 05	0.186E 03	0.00093	0.00110	0.00101	88.6	0.00109
27.03	1.351	0.009	3.612	2159.4	148.8	0.00676	494.3	372.2	0.187	0.194E 05	0.189E 03	0.00094	0.00112	0.00103	89.1	0.00110
27.53	1.363	0.009	3.606	2158.4	149.2	0.00677	494.3	372.4	0.192	0.194E 05	0.192E 03	0.00096	0.00115	0.00104	89.8	0.00112
28.03	1.377	0.010	3.598	2157.1	149.6	0.00678	494.4	372.6	0.198	0.198E 05	0.196E 03	0.00097	0.00117	0.00107	90.5	0.00113
28.53	1.390	0.012	3.593	2156.0	150.0	0.00678	494.4	372.7	0.211	0.199E 05	0.202E 03	0.00101	0.00123	0.00116	92.4	0.00117
29.03	1.467	0.012	3.553	2149.5	152.3	0.00681	494.7	373.7	0.225	0.199E 05	0.215E 03	0.00105	0.00129	0.00116	93.4	0.00121
29.53	2.548	0.017	3.171	2075.5	178.4	0.00120	497.5	384.8	0.150	0.192E 05	0.215E 03	0.00105	0.00129	0.00116	70.3	0.00092
30.03	2.580	0.023	3.162	2073.7	179.0	0.00120	497.6	385.0	0.152	0.204E 05	0.306E 03	0.00097	0.00099	0.00098	76.4	0.00106
30.53	2.565	0.025	3.166	2074.6	178.7	0.00120	497.6	384.9	0.204	0.243E 05	0.312E 03	0.00097	0.00105	0.00102	78.3	0.00110
31.03	2.529	0.026	3.176	2076.7	178.0	0.00119	497.5	384.6	0.213	0.243E 05	0.313E 03	0.00099	0.00109	0.00105	79.7	0.00112
31.53	2.475	0.026	3.190	2079.8	176.9	0.00117	497.4	384.1	0.217	0.240E 05	0.311E 03	0.00104	0.00112	0.00107	80.8	0.00114
32.03	2.320	0.025	3.234	2089.1	173.7	0.00112	497.0	382.8	0.231	0.239E 05	0.303E 03	0.00104	0.00119	0.00113	80.9	0.00118
32.53	2.296	0.025	3.242	2090.7	173.1	0.00111	497.0	382.5	0.229	0.233E 05	0.300E 03	0.00104	0.00119	0.00112	83.9	0.00118

INS. PSIA FSIA FT/SEC °R SLUGS/ CU.FT. °R

FT/SEC

	M : 6.5 R THETA X 10 ⁻³ : 0.5 - 5.5 TW/TR : 1.0	7103
		ZPG - AW
Axially-symmetric blow-down tunnel, contoured nozzle. Running time 50 s. D = 0.56 m. 3.5 < P0 < 21 MN/m ² . T0 : 350 K. Helium. 6 < RE/m X 10 ⁻⁶ < 25.		
FISCHER M.C. and MADDALON D.V., 1971. Experimental laminar, transitional and turbulent boundary layer profiles on a wedge at local Mach number 6.5 and comparisons with theory. NASA TN D-6462. And Fischer M.C., private communication.		

- 1 The test boundary layer was formed on the lower surface of a 5° half-angle wedge the test surface being at 10° incidence to the M = 20 free stream. Two wedges (L = 0.406, W = 0.279 m) were used, the leading edges (X = 0) being 51 μm thick. One was fitted with wall static tapings, and had a local surface depression, of maximum depth 0.38 mm, extending from X = 0.305 to X = 0.381 m. The other, used for profile measurements, could be fitted with a rear extension which increased the length to 0.610 m. The last four of the seven survey stations were on the extension surface. Measurements of the model surface "indicated excellent surface uniformity". The surface was not actively cooled. A detailed survey of the M = 20 free stream was made by Arrington et al. (1964) and showed transverse Mach number variations of ± 0.3. Heat transfer studies showed that the boundary layer did not become fully turbulent on the basic wedge models, and prompted the construction of the extension to X = 0.61 m. Chamfered swept end plates were used to help maintain two dimensional flow in the test region.
- 2
- 3
- 5 The pressure instrumented wedge had 12 static holes (d = 1.02 mm) mounted along the centre-line from X = 0.105 to 0.376 m. The model used for profile studies had numerous thermocouples along the centre line at intervals of about 12.5 mm for the same range of X. Thermocouples were also fitted to the extension.
- 6
- 7 Pitot profiles were obtained with two CPP. For the three upstream stations, d₁ = 1.02, d₂ = 0.51, l = 20 mm while for the four downstream stations, on the model extension, d₁ = 2.29, d₂ = 1.78, l = 20 mm. All measurements were made on the model centre line, the profiles at X values of 99.1, 180.3, 228.6, 431.8, 482.6, 533.4 and 599.4 mm.
- 8
- 9 The authors compared the measured PW values to both the inviscid calculated values and values calculated using a laminar viscous interaction correction following Bertram 1966. The initial values agreed well with the pressure predicted by Bertram, but further downstream departures were noted. These were attributed to the surface depression remarked in § 1 above. The wall pressure values used in data reduction are extrapolations of the initial measured values guided by the trends predicted by Bertram's analysis. Static pressure was assumed constant through the boundary layer. Wall temperatures changed by less than 4 K during a run, and average values were used.
- 10 Viscous interaction and rarefaction effects in the Pitot measurements were assessed following Beckwith et al. (CAT 7105) and estimated at less than 2 %. Real gas effects were estimated as less than 1 % following Erikson (1960). These possible corrections were therefore ignored. Probe wall-interference effects were assessed by recalculating the integral thicknesses with the low y-value replaced by a curve faired in to the wall static value. Changes in D1 and D2 were negligible. The Pitot pressure displayed an "overshoot" in the outer part of the layer for the lowest values of X. This was attributed to the relatively large size of the Pitot (d/D1 up to 0.5). These overshoots were replaced by a faired curve, following Munayhan (1965) for the affected profiles (0101, 0201/2, 0301/2, 0401/2). Viscosity values for helium took account of quantum effects, after Maddalon and Jackson (1970).
- 11
- 12 The editors have presented all the data available, incorporating the authors' assumptions and procedures. We have however calculated viscosity as discussed in the introduction. The 'D' state is the authors' based on the experimental position at which PTZ was either a maximum, or became effectively constant. The data
- 13

consists of four sets of six or seven successive profiles, each at a different unit Reynolds number. They range from laminar to fully turbulent.

§ DATA: 7103 0101-0407. Pitot profiles. $NX = 6$ or 7 .

15 Editors' comments

The measurements are made in a Mach number range for which there are no really satisfying data. They overlap the studies by Danberg - CAT 6702 and Adcock et al. - CAT 6501, but have more in common with the measurements, at higher Mach number, of Watson et al. - CAT 7305. Both 7103 and 7305 provide a number of profile sequences spanning the transition region.

This is an adiabatic layer, so that the absence of T_0 profiles is not crucial, though regrettable at these high Mach numbers. More of a pity is the lack of CF measurements. In these respects the study is superseded by Watson et al. (CAT 7305).

CAT 7103 FISCHER BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.									
RUN X * Rz	MD * POD TOD*	TW/TR* PW/PD* SW A	RED2W PED20 D2	CF CQ PI2*	H12 H32 H42	H12K H32K D2K	PM* TW UD	PD* TD TR	
71030101 9.9100*-02 INFINITE	6.1000 4.4975*+05 3.4500*+02	1.0000 1.0000 0.0000	8.8629*+01 4.3774*+02 7.9483*+05	NM NM 0.0000*+00	36.1020 1.5683 0.1740	2.4447 1.4866 6.2277*-04	6.7300*+02 3.0672*+02 1.8264*+03	6.7300*+02 2.5980*+01 3.0672*+02	
71030102 1.8030*-01 INFINITE	6.1000 4.4240*+05 3.4500*+02	1.0000 1.0000 0.0000	1.4344*+02 7.0846*+02 1.3078*-04	NM NM 0.0000*+00	33.4072 1.6645 0.1847	2.3906 1.5480 8.4356*-04	6.6200*+02 3.0672*+02 1.8264*+03	6.6200*+02 2.5980*+01 3.0672*+02	
71030103 2.2860*-01 INFINITE	6.2000 4.7504*+05 3.4500*+02	1.0000 1.0000 0.0000	1.5452*+02 7.7804*+02 1.3713*-04	NM NM 0.0000*+00	35.6291 1.6341 0.1818	2.4729 1.5156 9.6421*-04	6.5900*+02 3.0663*+02 1.8286*+03	6.5900*+02 2.5210*+01 3.0663*+02	
71030104 4.3180*-01 INFINITE	6.2000 4.4837*+05 3.4500*+02	1.0000 1.0000 0.0000	2.2297*+02 1.1227*+03 2.0964*-04	NM NM 0.0000*+00	30.1898 1.7745 0.1974	2.0588 1.6586 1.0570*-03	6.2200*+02 3.0663*+02 1.8266*+03	6.2200*+02 2.5210*+01 3.0663*+02	
71030105 4.8260*-01 INFINITE	6.4000 5.1674*+05 3.4500*+02	1.0000 1.0000 0.0000	2.7961*+02 1.4622*+03 2.4880*-04	NM NM 0.0000*+00	30.7855 1.8060 0.2018	1.9379 1.6957 1.1944*-03	6.1800*+02 3.0645*+02 1.8327*+03	6.1800*+02 2.3766*+01 3.0645*+02	
71030106 5.3340*-01 INFINITE	6.3000 4.7926*+05 3.4500*+02	1.0000 1.0000 0.0000	2.9158*+02 1.4964*+03 2.6793*-04	NM NM 0.0000*+00	28.9406 1.8362 0.2047	1.8864 1.7187 1.1045*-03	6.1700*+02 3.0654*+02 1.8307*+03	6.1700*+02 2.4472*+01 3.0654*+02	
71030107 5.9940*-01 INFINITE	6.4000 5.1507*+05 3.4500*+02	1.0000 1.0000 0.0000	3.3185*+02 1.7353*+03 2.9623*-04	NM NM 0.0000*+00	29.2235 1.8496 0.2067	1.8101 1.7343 1.1821*-03	6.1600*+02 3.0645*+02 1.8327*+03	6.1600*+02 2.3766*+01 3.0645*+02	
71030201 9.9100*-02 INFINITE	6.3000 8.3268*+05 3.5300*+02	1.0000 1.0000 0.0000	1.2011*+02 6.1639*+02 6.5215*-05	NM NM 0.0000*+00	37.2507 1.8440 0.1833	2.5938 1.5213 4.6016*-04	1.0720*+03 3.1364*+02 1.8518*+03	1.0720*+03 2.5040*+01 3.1364*+02	
71030202 1.8030*-01 INFINITE	6.4000 8.7628*+05 3.5300*+02	1.0000 1.0000 0.0000	1.6841*+02 8.8063*+02 9.0717*-05	NM NM 0.0000*+00	35.2723 1.7366 0.1940	2.5428 1.5749 5.2142*-04	1.0480*+03 3.1356*+02 1.8539*+03	1.0480*+03 2.4317*+01 3.1356*+02	
71030203 2.2860*-01 INFINITE	6.3000 8.0782*+05 3.5300*+02	1.0000 1.0000 0.0000	1.7151*+02 8.8019*+02 9.5990*-05	NM NM 0.0000*+00	35.4134 1.7092 0.1906	2.5279 1.5978 5.9669*-04	1.0400*+03 3.1364*+02 1.8518*+03	1.0400*+03 2.5040*+01 3.1364*+02	
71030204 4.3180*-01 INFINITE	6.6000 9.5254*+05 3.5300*+02	1.0000 1.0000 0.0000	3.1838*+02 1.7273*+03 1.7170*-04	NM NM 0.0000*+00	31.4993 1.8471 0.2072	1.9097 1.7342 7.3129*-04	9.8600*+02 3.1340*+02 1.8577*+03	9.8600*+02 2.2960*+01 3.1340*+02	
71030205 4.8260*-01 INFINITE	6.7000 1.0132*+06 3.5300*+02	1.0000 1.0000 0.0000	4.0554*+02 2.2403*+03 2.1392*-04	NM NM 0.0000*+00	31.8785 1.8623 0.2093	1.8442 1.7774 8.8181*-04	9.7900*+02 3.1332*+02 1.8595*+03	9.7900*+02 2.2322*+01 3.1332*+02	
71030206 5.3340*-01 INFINITE	6.7000 1.0131*+06 3.5300*+02	1.0000 1.0000 0.0000	4.4044*+02 2.4331*+03 2.3281*-04	NM NM 0.0000*+00	30.9944 1.8769 0.2110	1.7183 1.7897 8.3509*-04	9.7700*+02 3.1332*+02 1.8595*+03	9.7700*+02 2.2322*+01 3.1332*+02	
71030207 5.9940*-01 INFINITE	6.7000 1.0100*+06 3.5300*+02	1.0000 1.0000 0.0000	4.8853*+02 2.6987*+03 2.5902*-04	NM NM 0.0000*+00	30.9597 1.8737 0.2106	1.6970 1.7801 9.9727*-04	9.7400*+02 3.1332*+02 1.8595*+03	9.7400*+02 2.2322*+01 3.1332*+02	

CAT 7103		FISCHER		BOUNDARY CONDITIONS AND EVALUATED DATA. 31 UNITS.						
RUN	MD *	TW/TR*	RED2M	CF	M12	M12K	PN*	PD*		
X *	POD	PH/PD*	RED2D	CG	M32	M32K	TW	TD		
RZ	T00*	SW *	O2	P12*	M42	D2K	UD	TR		
71030301	6.5000	1.0000	1.6691"+02	NM	40.9361	2.5079	1.4780"+03	1.4780"+03		
9.9100"-02	1.2947"+06	1.0000	9.0689"+02	NM	1.6284	1.5463	3.1420"+02	2.2965"+01		
INFINITE	3.4800"+02	0.0000	6.0899"-05	0.0000"+00	0.1582	4.9257"-04	1.8353"+03	3.1420"+02		
71030302	6.5000	1.0000	1.8175"+02	NM	37.7308	2.5808	1.4200"+03	1.4200"+03		
1.8030"-01	1.2439"+06	1.0000	9.8754"+02	NM	1.7527	1.6396	3.1420"+02	2.2965"+01		
INFINITE	3.4800"+02	0.0000	6.9023"-05	0.0000"+00	0.1703	4.1463"-04	1.8353"+03	3.1420"+02		
71030303	6.5000	1.0000	1.8253"+02	NM	37.0351	2.4879	1.4050"+03	1.4050"+03		
2.2860"-01	1.2307"+06	1.0000	9.9181"+02	NM	1.7465	1.6174	3.1420"+02	2.2965"+01		
INFINITE	3.4800"+02	0.0000	7.0061"-05	0.0000"+00	0.1696	4.1922"-04	1.8353"+03	3.1420"+02		
71030304	6.8000	1.0000	4.3629"+02	NM	33.5703	1.9109	1.3500"+03	1.3500"+03		
4.3180"-01	1.4599"+06	1.0000	2.5028"+03	NM	1.8769	1.7688	3.1400"+02	2.1103"+01		
INFINITE	3.4800"+02	0.0000	1.5963"-04	0.0000"+00	0.1834	6.2817"-04	1.8405"+03	3.1400"+02		
71030305	6.9000	1.0000	5.6175"+02	NM	33.9156	1.8370	1.3380"+03	1.3380"+03		
4.8260"-01	1.5894"+06	1.0000	3.2799"+03	NM	1.8443	1.8351	3.1394"+02	2.0532"+01		
INFINITE	3.4800"+02	0.0000	2.0156"-04	0.0000"+00	0.1854	7.5100"-04	1.8421"+03	3.1394"+02		
71030306	6.8000	1.0000	5.6617"+02	NM	32.3727	1.6112	1.3350"+03	1.3350"+03		
5.3340"-01	1.4437"+06	1.0000	3.2480"+03	NM	1.8846	1.8159	3.1400"+02	2.1103"+01		
INFINITE	3.4800"+02	0.0000	2.0947"-04	0.0000"+00	0.1841	8.0821"-04	1.8405"+03	3.1400"+02		
71030401	6.6000	1.0000	2.1587"+02	NM	44.6265	3.1624	2.5640"+03	2.5640"+03		
9.9100"-02	2.4770"+06	1.0000	1.1712"+03	NM	1.6478	1.5090	3.1420"+02	2.3025"+01		
INFINITE	3.5400"+02	0.0000	4.4915"-05	0.0000"+00	0.1849	3.3777"-04	1.8603"+03	3.1420"+02		
71030402	6.5000	1.0000	3.1340"+02	NM	31.8068	2.1325	2.4830"+03	2.4830"+03		
1.8030"-01	2.2327"+06	1.0000	1.6695"+03	NM	1.7626	1.6548	3.1436"+02	2.3691"+01		
INFINITE	3.5400"+02	0.0000	6.9364"-05	0.0000"+00	0.1974	3.9618"-04	1.8584"+03	3.1436"+02		
71030403	6.5000	1.0000	2.8206"+02	NM	33.6431	2.7753	2.4750"+03	2.4750"+03		
2.2860"-01	2.2255"+06	1.0000	1.5025"+03	NM	1.8702	1.8165	3.1436"+02	2.3691"+01		
INFINITE	3.5400"+02	0.0000	6.2630"-05	0.0000"+00	0.2094	2.4139"-04	1.8584"+03	3.1436"+02		
71030404	6.6000	1.0000	7.1518"+02	NM	31.0356	1.8315	2.4200"+03	2.4200"+03		
4.3180"-01	2.3379"+06	1.0000	3.8801"+03	NM	1.8592	1.7779	3.1428"+02	2.3025"+01		
INFINITE	3.5400"+02	0.0000	1.5766"-04	0.0000"+00	0.2086	6.4704"-04	1.8603"+03	3.1428"+02		
71030405	6.8000	1.0000	9.0475"+02	NM	32.7169	1.8551	2.4060"+03	2.4060"+03		
4.8260"-01	2.6754"+06	1.0000	5.0879"+03	NM	1.8696	1.8013	3.1413"+02	2.1772"+01		
INFINITE	3.5400"+02	0.0000	1.8928"-04	0.0000"+00	0.2106	7.7661"-04	1.8638"+03	3.1413"+02		
71030406	6.7000	1.0000	9.4384"+02	NM	31.4399	1.7125	2.3990"+03	2.3990"+03		
5.3340"-01	2.4876"+06	1.0000	5.2139"+03	NM	1.8609	1.7908	3.1421"+02	2.2386"+01		
INFINITE	3.5400"+02	0.0000	2.0384"-04	0.0000"+00	0.2092	8.5472"-04	1.8621"+03	3.1421"+02		

TRAPEZOIDAL RULE FOR 0203,0302,0401,0403

71030201		FISCHER		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26		
I	Y	PT/P	P/PD	T0/T00	M/MD	U/UD	T/T0	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.38851	0.00000	0.00000	12.52598	0.00000
2	5.0430*-04	1.3703*+00	NM	0.90126	0.10100	0.33813	11.20816	0.03017
3	8.4510*-04	1.4211*+00	NM	0.90264	0.10700	0.35594	11.06573	0.03217
4	1.2042*-03	1.5757*+00	NM	0.90650	0.12300	0.40170	10.66607	0.03766
5	1.5903*-03	2.1532*+00	NM	0.91745	0.16500	0.50948	9.53420	0.05344
6	1.7955*-03	3.4456*+00	NM	0.93316	0.22500	0.63242	7.91030	0.08000
7	2.0007*-03	4.8764*+00	NM	0.94494	0.27500	0.71142	6.69247	0.10630
8	2.0520*-03	5.7398*+00	NM	0.95040	0.30100	0.74508	6.12737	0.12160
9	2.1789*-03	7.6255*+00	NM	0.95961	0.35100	0.79855	5.17600	0.15428
10	2.3085*-03	9.9944*+00	NM	0.96748	0.40300	0.84164	4.36153	0.19297
11	2.4624*-03	1.3022*+01	NM	0.97498	0.46500	0.88066	3.58884	0.24553
12	2.5137*-03	1.5158*+01	NM	0.97673	0.50300	0.89959	3.19852	0.28125
13	2.5650*-03	1.7399*+01	NM	0.98189	0.54000	0.91518	2.87229	0.31862
14	2.6406*-03	2.0819*+01	NM	0.98563	0.59200	0.93333	2.48554	0.37550
15	2.7189*-03	2.3811*+01	NM	0.98816	0.63400	0.94543	2.22370	0.42516
16	2.7945*-03	2.7165*+01	NM	0.99044	0.67800	0.95614	1.98878	0.48077
17	2.8241*-03	3.4728*+01	NM	0.99414	0.76800	0.97335	1.80625	0.60598
18	2.9907*-03	3.7923*+01	NM	0.99530	0.80300	0.97871	1.48552	0.65883
19	3.1023*-03	4.1164*+01	NM	0.99632	0.83700	0.98336	1.36031	0.71242
20	3.1536*-03	4.5352*+01	NM	0.99744	0.87900	0.98846	1.26456	0.78166
21	3.2319*-03	4.9106*+01	NM	0.99830	0.91500	0.99233	1.17617	0.84370
22	3.3075*-03	5.2349*+01	NM	0.99894	0.94500	0.99525	1.10918	0.89728
23	3.3831*-03	5.4794*+01	NM	0.99939	0.96700	0.99724	1.06352	0.93768
24	3.5370*-03	5.6151*+01	NM	0.99962	0.97900	0.99827	1.03976	0.96010
25	3.7692*-03	5.7295*+01	NM	0.99980	0.98900	0.99911	1.02055	0.97899
26	3.9987*-03	5.7755*+01	NM	0.99987	0.99300	0.99944	1.01300	0.98661
27	4.2309*-03	5.8102*+01	NM	0.99993	0.99600	0.99968	1.00740	0.99233
0 28	5.2920*-03	5.8566*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

71030207		FISCHER		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26		
I	Y	PT/P	P/PD	T0/T00	M/MD	U/UD	T/T0	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	NM	0.88759	0.00000	0.00000	14.03606	0.00000
2	1.1280*-03	2.6611*+00	NM	0.92353	0.18000	0.56544	9.86604	0.05730
3	1.7680*-03	4.0599*+00	NM	0.93775	0.23300	0.66799	8.21921	0.08127
4	2.1440*-03	6.2305*+00	NM	0.95212	0.29600	0.75768	6.55227	0.11564
5	2.4880*-03	8.4233*+00	NM	0.96169	0.34800	0.81189	5.44304	0.14916
6	2.9440*-03	1.0975*+01	NM	0.96940	0.40000	0.85310	4.54864	0.18755
7	3.3760*-03	1.3181*+01	NM	0.97429	0.44000	0.87815	3.98324	0.22046
8	3.9600*-03	1.9851*+01	NM	0.97877	0.48400	0.90061	3.46247	0.26011
9	4.5520*-03	1.8226*+01	NM	0.98187	0.52000	0.91584	3.10193	0.29525
10	5.3440*-03	2.0407*+01	NM	0.98421	0.55100	0.92711	2.83113	0.32747
11	6.2640*-03	2.3331*+01	NM	0.98677	0.59000	0.93930	2.53457	0.37060
12	7.1120*-03	2.6788*+01	NM	0.98917	0.63300	0.95063	2.25337	0.42150
13	7.7200*-03	2.9430*+01	NM	0.99069	0.66400	0.95767	2.09017	0.46038
14	8.3840*-03	3.2382*+01	NM	0.99212	0.69700	0.96439	1.91409	0.50379
15	8.8720*-03	3.5381*+01	NM	0.99336	0.72900	0.97000	1.77046	0.54788
16	9.4050*-03	3.7719*+01	NM	0.99420	0.75300	0.97386	1.67264	0.58223
17	1.0104*-02	4.1161*+01	NM	0.99528	0.78700	0.97880	1.54682	0.63278
18	1.0736*-02	4.4754*+01	NM	0.99626	0.82100	0.98321	1.43416	0.68555
19	1.1456*-02	4.9177*+01	NM	0.99727	0.86100	0.98780	1.31622	0.75048
20	1.2168*-02	5.2666*+01	NM	0.99800	0.89300	0.99107	1.23171	0.80463
21	1.3038*-02	5.7178*+01	NM	0.99874	0.92900	0.99439	1.14574	0.86791
22	1.4040*-02	5.9772*+01	NM	0.99914	0.95000	0.99617	1.09957	0.90597
23	1.5344*-02	6.3192*+01	NM	0.99962	0.97700	0.99831	1.04409	0.95615
24	1.6696*-02	6.4747*+01	NM	0.99982	0.98900	0.99920	1.02074	0.97890
25	1.8312*-02	6.5525*+01	NM	0.99992	0.99500	0.99964	1.00935	0.99038
0 26	2.0352*-02	6.6191*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

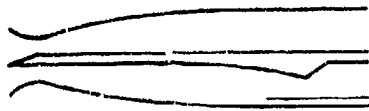
INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

71030401		FISCHER		PROFILE TABULATION		25 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NH	0.89760	0.00000	0.00000	13.64982	0.00000	
2	5.8000*-04	1.2893*+00	NH	0.89816	0.00800	0.30384	12.48203	0.02434	
3	8.0600*-04	1.3040*+00	NH	0.89861	0.00800	0.31028	12.43198	0.02496	
4	9.8200*-04	1.8823*+00	NH	0.90594	0.11800	0.40199	11.60565	0.03464	
5	1.1080*-03	1.9587*+00	NH	0.91352	0.14600	0.47871	10.75091	0.04453	
6	1.2600*-03	2.5368*+00	NH	0.92217	0.17700	0.55341	9.77567	0.05661	
7	1.3600*-03	3.3984*+00	NH	0.93195	0.21300	0.62727	8.67256	0.07233	
8	1.4620*-03	4.9933*+00	NH	0.94498	0.26600	0.71390	7.20288	0.09911	
9	1.5620*-03	6.8377*+00	NH	0.95538	0.31600	0.77606	6.03131	0.12867	
10	1.6880*-03	9.9631*+00	NH	0.96690	0.38600	0.83964	4.73168	0.17745	
11	1.7380*-03	1.3776*+01	NH	0.97563	0.45700	0.88474	3.74799	0.23606	
12	1.8140*-03	1.6082*+01	NH	0.97934	0.49500	0.90324	3.32961	0.27127	
13	1.8640*-03	1.9536*+01	NH	0.98357	0.54700	0.92387	2.85266	0.32366	
14	1.9400*-03	2.3184*+01	NH	0.98849	0.59700	0.93977	2.47795	0.37925	
15	1.9640*-03	2.6657*+01	NH	0.99334	0.64100	0.95129	2.20245	0.43192	
16	2.0160*-03	3.0466*+01	NH	0.99146	0.68600	0.96118	1.96317	0.48960	
17	2.0900*-03	3.4907*+01	NH	0.99342	0.73500	0.97021	1.74244	0.55681	
18	2.1660*-03	3.7290*+01	NH	0.99429	0.76000	0.97424	1.64326	0.59287	
19	2.2160*-03	4.1168*+01	NH	0.99553	0.79900	0.97988	1.50400	0.65151	
20	2.3420*-03	4.6641*+01	NH	0.99695	0.85100	0.98634	1.34335	0.73423	
21	2.4440*-03	5.3152*+01	NH	0.99830	0.90900	0.99239	1.19188	0.83262	
22	2.5440*-03	5.9355*+01	NH	0.99932	0.96100	0.99698	1.07628	0.92632	
23	2.6460*-03	6.1777*+01	NH	0.99966	0.98000	0.99849	1.03810	0.96185	
24	2.6960*-03	6.2712*+01	NH	0.99980	0.98800	0.99911	1.03261	0.97702	
D 25	2.9720*-03	6.4233*+01	NH	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

71030406		FISCHER		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NH	0.89759	0.00000	0.00000	14.03606	0.00000	
2	1.1392*-03	3.8231*+00	NH	0.93571	0.22500	0.65427	8.45571	0.07738	
3	1.8944*-03	5.2696*+00	NH	0.94656	0.27000	0.72432	7.19677	0.10065	
4	2.4512*-03	7.7539*+00	NH	0.95913	0.33300	0.79777	5.73941	0.13900	
5	3.0784*-03	1.0922*+01	NH	0.96927	0.39900	0.85241	4.56405	0.18677	
6	3.5840*-03	1.3647*+01	NH	0.97515	0.44800	0.88260	3.88124	0.22740	
7	4.0640*-03	1.6494*+01	NH	0.97968	0.49400	0.90510	3.35689	0.26962	
8	4.6976*-03	1.9477*+01	NH	0.98327	0.53800	0.92257	2.94059	0.31374	
9	5.2544*-03	2.2183*+01	NH	0.98583	0.57500	0.93485	2.64330	0.35367	
10	5.7856*-03	2.5150*+01	NH	0.98810	0.61300	0.94561	2.37958	0.39738	
11	6.2912*-03	2.8478*+01	NH	0.99017	0.65300	0.95527	2.14007	0.44637	
12	6.6944*-03	3.1382*+01	NH	0.99166	0.68600	0.96218	1.96729	0.48909	
13	7.1744*-03	3.5094*+01	NH	0.99325	0.72600	0.96949	1.78326	0.54366	
14	7.5008*-03	3.7917*+01	NH	0.99427	0.75500	0.97417	1.66484	0.58514	
15	7.9296*-03	4.1057*+01	NH	0.99525	0.78600	0.97866	1.55032	0.63126	
16	8.3328*-03	4.4109*+01	NH	0.99609	0.81500	0.98246	1.45318	0.67608	
17	8.7360*-03	4.7717*+01	NH	0.99696	0.84800	0.98637	1.35297	0.72904	
18	9.0944*-03	5.1005*+01	NH	0.99765	0.87700	0.98948	1.27295	0.77731	
19	9.4976*-03	5.3810*+01	NH	0.99817	0.90100	0.99184	1.21161	0.81848	
20	9.9008*-03	5.6448*+01	NH	0.99863	0.92300	0.99387	1.15945	0.85719	
21	1.0355*-02	5.9398*+01	NH	0.99909	0.94700	0.99593	1.10600	0.90048	
22	1.0912*-02	6.1660*+01	NH	0.99941	0.96500	0.99738	1.06623	0.93367	
23	1.1565*-02	6.3836*+01	NH	0.99970	0.98200	0.99868	1.03427	0.96559	
24	1.2454*-02	6.5133*+01	NH	0.99987	0.99200	0.99942	1.01502	0.98463	
25	1.3414*-02	6.5918*+01	NH	0.99997	0.99800	0.99986	1.00373	0.99615	
D 26	1.4445*-02	6.6181*+01	NH	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD ASSUME P=PD AND VAN DRIEST

	M : 2.4 falling to 1.9 R THETA X 10 ⁻³ : 20 - 40 TW/TR : 1.05	7104
		APG - AW
Fixed symmetrical nozzle blow down wind tunnel, running time 15 sec., W = H = 0.229 m. PO : 0.35 MN/m ² . TO : 289 K. Air. RE/m X 10 ⁻⁶ : 4.		
WALTRUP P.J. and SCHETZ J.A., 1971. An experimental investigation of a compressible turbulent boundary layer subjected to a systematic variation of adverse pressure gradients. Virginia Poly. Inst. VPI-E-71-18. And Waltrup P.J., Schetz J.A., private communications. Also Waltrup & Schetz (1973).		

- 1 The test boundary layer was formed on the bottom nozzle block and test section wall of the wind tunnel. The highly polished instrumental section started at the end of the nozzle block ($X = 0$) and extended 0.23 m downstream. Pressure gradients could be imposed by three ramps of the full tunnel width. These were mounted in the centre of the tunnel as an extension of a plate running through the nozzle into the settling chamber so as to eliminate leading edge disturbances. The resulting reflected wave pressure histories are listed with the wall temperature histories in section D. The test layer had undergone a largely two dimensional expansion in the nozzle, and all three imposed pressure gradients commenced at $X = 22.2$ mm. Weak disturbances were generated by the nozzle / wall junction ($X = 0$) and several small machining slope-discontinuities on the ramps. It was believed that the effect was small, probably less than 1 % in Mach number. Spark schlieren photographs clearly established that the boundary layer was turbulent. Changes of static pressure across the test-surface were less than 1 % in the central 100 mm.
- 2
- 3
- 4
- 5
- 6 Static pressure was measured at up to 38 tappings of 0.78 mm diameter, and wall temperature by means of 0.25 mm copper-constantan thermocouples press-fitted into the test-surface at up to 15 stations. Wall shear stress could be determined at three stations using a FEB copied from the NOL balance of Bruno, Yanta and Risher (1969). The element was rectangular ($\Delta X = 12.7$, $\Delta Z = 25.4$ mm) set across the centre line.
- 7 The Pitot probe used was a FPP made by flattening 3.2 mm diameter tubing to give a rectangular probe tip for which $h_1 = 0.66$, $h_2 = 0.254$, $b_1 = 3.58$, $b_2 = 3.2$ mm. Total temperature was found with a STP ($d_1 = 1.57$, $d_2 = 0.97$ mm) containing a copper-constantan thermocouple bead 0.13 mm in diameter about 2.5 mm back from the opening. The cone static probe was a 10° semi-angle cone with a base diameter of 1.6 mm and four static holes ($D = 0.33$ mm) drilled in the conical surface about 3/4 of the way back from the tip. This was directly calibrated and its sensitivity to angle of attack found in the wind tunnel. The total temperature probe was calibrated directly for M between 1.95 and 2.36, results for lower Mach numbers being taken from an extrapolation of the data of Hottel & Kalitinsky (1945). The various probes deflected under aerodynamic loading, and a correction, found from photographs to be constant for each particular probe, was applied to allow for this. Traverses were taken with a DISA type 55 F 31 boundary layer probe and associated commercial hot-wire anemometer electronics at the $X = 22.2$ and 178 mm stations using ramp 2. The probe wire was of platinum plated tungsten ($d = 5$ μ m, $l/d = 250$).
- 8 The detailed disposition of all the wall measurement positions is to be found in figure 2 of Waltrup and Schetz (1973). The four stations are at $X = 22.2$, 76.2, 127 and 178 mm. At the last three, provision for inserting the FEB was made on the centre line. Profiles could be obtained at all four X-values at points 12.7 mm off the centre line. Rows of 6-7 static pressure tappings and 3-4 thermocouples were arranged at each station. Data from other X-values is presented in section D.
- 9 Pitot, static pressure and total temperature profiles were taken on separate occasions. The authors have interpolated the TO and P data to the Y values of the Pitot measurements. A polynomial approximation and the Rayleigh-Pitot formula (Volluz 1961) were used to allow Mach number determination without iteration. The recovery factor used was 0.89.
- 10
- 11
- 12 The tables computed by the editors incorporate the varied calibration and data reduction procedures of the

13 authors. The profiles presented consist of three sets for four successive X-stations. The first profile in each set is very nearly the same, the $X = 22.2$ mm station being upstream of the start of the imposed pressure gradient. The three succeeding stations of a set describe the development of the layer under an adverse pressure gradient on a straight wall, the pressure history of each set being different. The wall pressure and temperature data is presented in section D, together with the measured shear stress. Also presented are the author's reduced hot-wire measurements.

5 DATA: 7104 0101-0304. Pitot, TO and P profiles measured separately. $NX = 4$. CF from FEB. Some hot-wire measurements.

15 Editors' comments

The entry describes three APG flows of varied severity. Similar examples of nominally planar straight-wall compressions are Zwarts - CAT 7007 and Thomas - CAT 7401. Axisymmetric examples are Peake et al. - CAT 7102 and Lewis et al. - CAT 7201. As with all nominally planar cases, cross flow effects cannot be eliminated with confidence.

The Mach number is low, and the flow near-adiabatic so that the rather simple approach to TO probe calibrations is probably adequate. All TO profiles show an outer region overshoot. The static pressure profiles show a dip of 10 % in the outer part of the layer. In a straight wall flow at these low Mach numbers, streamline curvature, streamline divergence, and normal turbulent stresses are unlikely to produce a dip of this magnitude. The location of the pressure drop suggests that it may be caused by turbulence effects on the calibration of the static probe used, which is not of a common type for this Mach number range.

The three test cases are intended to be distinguished by -ve, zero and +ve values of $\delta^2 p / \delta x^2$. On a transformed log-law plot we find that the outer regions of the profile do not differ very much from ZPG profiles, but that there are sometimes peculiarities in the inner regions. The calculated PO values for the profiles suggest that the D-state should be taken further out towards the free stream, and that measurements for profiles 0101/3, 0203 should have been continued to higher values of Y . Measurements do not extend within the momentum deficit peak for 0101, 0102 and series 03.

CAT 7104		WALTRUP		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.				
RUN	MD *	TH/TR	RED2M	CF *	M12	M12K	PW*	PD*
X *	POD	PH/PD	RED2D	CO	H32	H32K	TW*	TD*
RZ	TOD	SM *	D2	PI2	H42	D2K	UD	TR
71040101	2.3610	1.0437	1.5030 ⁺⁰⁴	NM	1.7794	1.4673	2.0717 ⁺⁰⁴	2.5959 ⁺⁰⁴
2.2225 ⁻⁰²	3.5709 ⁺⁰⁵	1.0292	2.8009 ⁺⁰⁴	NM	1.8006	1.8007	2.8568 ⁺⁰²	1.3693 ⁺⁰²
INFINITE	2.8960 ⁺⁰²	0.0000	7.3280 ⁻⁰⁴	NC	0.8663	7.4989 ⁻⁰⁴	5.5394 ⁺⁰²	2.7372 ⁺⁰²
71040102	2.0980	1.0391	1.7391 ⁺⁰⁴	1.3432 ⁻⁰³	3.5453	1.6069	4.0128 ⁺⁰⁴	3.7818 ⁺⁰⁴
7.6200 ⁻⁰²	3.4475 ⁺⁰⁵	1.0611	2.9191 ⁺⁰⁴	NM	1.7413	1.7244	2.8620 ⁺⁰²	1.5398 ⁺⁰²
INFINITE	2.8953 ⁺⁰²	0.0000	6.9553 ⁻⁰⁴	NC	-0.0296	9.1750 ⁻⁰⁴	5.2197 ⁺⁰²	2.7543 ⁺⁰²
71040103	1.9340	1.0367	2.1823 ⁺⁰⁴	1.3136 ⁻⁰³	3.4991	1.5753	4.8298 ⁺⁰⁴	4.7712 ⁺⁰⁴
1.2700 ⁻⁰¹	3.3696 ⁺⁰⁵	1.0123	3.4403 ⁺⁰⁴	NM	1.7414	1.7283	2.8617 ⁺⁰²	1.6527 ⁺⁰²
INFINITE	2.8891 ⁺⁰²	0.0000	7.7742 ⁻⁰⁴	NC	-0.0165	1.0244 ⁻⁰³	4.9850 ⁺⁰²	2.7605 ⁺⁰²
71040104	1.8820	0.9800	2.6107 ⁺⁰⁴	1.4036 ⁻⁰³	3.2447	1.5425	5.5469 ⁺⁰⁴	5.4090 ⁺⁰⁴
1.7780 ⁻⁰¹	3.5250 ⁺⁰⁵	1.0255	3.8638 ⁺⁰⁴	NM	1.7359	1.7250	2.7121 ⁺⁰²	1.6929 ⁺⁰²
INFINITE	2.8921 ⁺⁰²	0.0000	8.1806 ⁻⁰⁴	NC	-0.0157	1.0580 ⁻⁰³	4.9096 ⁺⁰²	2.7674 ⁺⁰²
71040201	2.3760	1.0446	1.1845 ⁺⁰⁴	NM	3.9479	1.4479	2.6959 ⁺⁰⁴	2.5580 ⁺⁰⁴
2.2225 ⁻⁰²	3.6022 ⁺⁰⁵	1.0539	2.2253 ⁺⁰⁴	NM	1.8076	1.7937	2.8591 ⁺⁰²	1.3607 ⁺⁰²
INFINITE	2.8970 ⁺⁰²	0.0000	5.8186 ⁻⁰⁴	NC	-0.0161	7.7572 ⁻⁰⁴	5.5569 ⁺⁰²	2.7372 ⁺⁰²
71040202	2.2780	1.0453	1.2090 ⁺⁰⁴	1.4693 ⁻⁰³	4.1336	1.4687	2.8855 ⁺⁰⁴	2.8510 ⁺⁰⁴
7.6200 ⁻⁰²	3.4443 ⁺⁰⁵	1.0121	2.1847 ⁺⁰⁴	NM	1.7989	1.7827	2.8614 ⁺⁰²	1.4184 ⁺⁰²
INFINITE	2.8906 ⁺⁰²	0.0000	5.6687 ⁻⁰⁴	NC	-0.0328	7.6978 ⁻⁰⁴	5.4396 ⁺⁰²	2.7375 ⁺⁰²
71040203	2.1080	1.0400	1.6805 ⁺⁰⁴	1.3539 ⁻⁰³	3.8223	1.4902	3.7404 ⁺⁰⁴	3.7163 ⁺⁰⁴
1.2700 ⁻⁰¹	3.4412 ⁺⁰⁵	1.0065	2.8340 ⁺⁰⁴	NM	1.7789	1.7837	2.8603 ⁺⁰²	1.5311 ⁺⁰²
INFINITE	2.8919 ⁺⁰²	0.0000	6.7847 ⁻⁰⁴	NC	-0.0279	9.0883 ⁻⁰⁴	5.2298 ⁺⁰²	2.7503 ⁺⁰²
71040204	1.9500	1.0365	2.1577 ⁺⁰⁴	1.3439 ⁻⁰³	3.3490	1.5433	4.8884 ⁺⁰⁴	4.7609 ⁺⁰⁴
1.7780 ⁻⁰¹	3.4468 ⁺⁰⁵	1.0268	3.4213 ⁺⁰⁴	NM	1.7458	1.7321	2.8597 ⁺⁰²	1.6409 ⁺⁰²
INFINITE	2.8888 ⁺⁰²	0.0000	7.6086 ⁻⁰⁴	NC	-0.0517	9.8796 ⁻⁰⁴	5.0082 ⁺⁰²	2.7590 ⁺⁰²
71040301	2.3720	1.0496	1.1186 ⁺⁰⁴	NM	4.4248	1.4652	2.6717 ⁺⁰⁴	2.6062 ⁺⁰⁴
2.2225 ⁻⁰²	3.6473 ⁺⁰⁵	1.0251	2.1036 ⁺⁰⁴	NM	1.8117	1.7977	2.8620 ⁺⁰²	1.3578 ⁺⁰²
INFINITE	2.8857 ⁺⁰²	0.0000	5.3915 ⁻⁰⁴	NC	-0.0636	7.3380 ⁻⁰⁴	5.5416 ⁺⁰²	2.7268 ⁺⁰²
71040302	2.2970	1.0477	1.2274 ⁺⁰⁴	1.5686 ⁻⁰³	3.7779	1.4593	2.8613 ⁺⁰⁴	2.7372 ⁺⁰⁴
7.6200 ⁻⁰²	3.4067 ⁺⁰⁵	1.0453	2.2388 ⁺⁰⁴	NM	1.8033	1.7880	2.8617 ⁺⁰²	1.4040 ⁺⁰²
INFINITE	2.8856 ⁺⁰²	0.0000	5.9148 ⁻⁰⁴	NC	-0.0284	7.8145 ⁻⁰⁴	5.4570 ⁺⁰²	2.7315 ⁺⁰²
71040303	2.2200	1.0431	1.8625 ⁺⁰⁴	1.5069 ⁻⁰³	3.3980	1.4177	3.1716 ⁺⁰⁴	3.0372 ⁺⁰⁴
1.2700 ⁻⁰¹	3.3506 ⁺⁰⁵	1.0443	2.9800 ⁺⁰⁴	NM	1.8023	1.7904	2.8600 ⁺⁰²	1.4560 ⁺⁰²
INFINITE	2.8912 ⁺⁰²	0.0000	6.6893 ⁻⁰⁴	NC	0.0309	8.6308 ⁻⁰⁴	5.3709 ⁺⁰²	2.7419 ⁺⁰²
71040304	2.1240	1.0412	1.8470 ⁺⁰⁴	1.4067 ⁻⁰³	3.5375	1.4802	3.7600 ⁺⁰⁴	3.6784 ⁺⁰⁴
1.7780 ⁻⁰¹	3.4923 ⁺⁰⁵	1.0244	3.1366 ⁺⁰⁴	NM	1.7769	1.7626	2.8612 ⁺⁰²	1.5196 ⁺⁰²
INFINITE	2.8906 ⁺⁰²	0.0000	7.4504 ⁻⁰⁴	NC	-0.0274	9.8428 ⁻⁰⁴	5.2496 ⁺⁰²	2.7480 ⁺⁰²

INPUT TAUW NOT CF

71040101		WALTRUP		PROFILE TABULATION			27 POINTS, DELTA AT POINT 19		
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.02922	0.89681	0.00000	0.00000	1.89682	0.00000	
2	4.2672*-04	3.1153*+00	1.02922	0.70363	0.60097	0.61900	1.06091	0.60051	
3	8.5852*-04	3.6339*+00	1.02922	0.73982	0.65954	0.67700	1.05364	0.66131	
4	1.0541*-03	4.1066*+00	1.02922	0.77228	0.70845	0.72500	1.04727	0.71250	
5	1.4554*-03	4.5553*+00	1.02789	0.80231	0.75178	0.76700	1.04091	0.75741	
6	1.6764*-03	4.9640*+00	1.02656	0.82952	0.78913	0.80300	1.03545	0.79610	
7	1.9837*-03	5.2388*+00	1.02390	0.84755	0.81316	0.82600	1.03182	0.81966	
8	2.3597*-03	5.4712*+00	1.02125	0.86300	0.83297	0.84500	1.02909	0.83850	
9	2.9464*-03	5.7507*+00	1.00797	0.88114	0.84617	0.86700	1.02545	0.85222	
10	3.6068*-03	6.0937*+00	0.99203	0.90311	0.85361	0.89300	1.02091	0.86774	
11	4.1910*-03	6.3931*+00	0.98008	0.92236	0.90720	0.91500	1.01727	0.88155	
12	4.8768*-03	6.6892*+00	0.97477	0.94113	0.92968	0.93600	1.01364	0.90011	
13	5.6388*-03	7.0384*+00	0.96680	0.96297	0.95567	0.96000	1.00909	0.91977	
14	6.2484*-03	7.2010*+00	0.96946	0.97331	0.96749	0.97100	1.00727	0.93454	
15	6.8834*-03	7.3861*+00	0.97078	0.98438	0.98077	0.98300	1.00455	0.94996	
16	7.5946*-03	7.4908*+00	0.97875	0.99123	0.98820	0.99000	1.00364	0.96545	
17	8.3058*-03	7.5459*+00	0.98938	0.99351	0.99210	0.99300	1.00182	0.98067	
18	8.9662*-03	7.6235*+00	0.99602	0.99832	0.99755	0.99800	1.00091	0.99312	
D 19	9.6774*-03	7.6586*+00	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
20	1.0389*-02	7.6586*+00	1.01726	1.00000	1.00000	1.00000	1.00000	1.01726	
21	1.1125*-02	7.5950*+00	1.03586	0.99622	0.99555	0.99600	1.00091	1.03078	
22	1.1735*-02	7.5808*+00	1.04117	0.99517	0.99455	0.99500	1.00091	1.03502	
23	1.2344*-02	7.5808*+00	1.04648	0.99517	0.99455	0.99500	1.00091	1.04030	
24	1.3030*-02	7.5523*+00	1.05445	0.99308	0.99255	0.99300	1.00091	1.04612	
25	1.3691*-02	7.5459*+00	1.05710	0.99351	0.99210	0.99300	1.00182	1.04780	
26	1.4300*-02	7.5459*+00	1.06242	0.99351	0.99210	0.99300	1.00182	1.05307	
27	1.4935*-02	7.5808*+00	1.05578	0.99517	0.99455	0.99500	1.00091	1.04954	

INPUT VARIABLES Y,U/UD,T/TD,P/PO

71040102		WALTRUP		PROFILE TABULATION			27 POINTS, DELTA AT POINT 20		
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.06108	0.98753	0.00000	0.00000	1.85687	0.00000	
2	4.6482*-04	1.5563*+00	1.06108	0.98490	0.39117	0.50100	1.60036	0.32407	
3	7.8994*-04	1.6667*+00	1.06016	0.99042	0.42251	0.53800	1.60434	0.35308	
4	1.0338*-03	1.7992*+00	1.05925	0.99156	0.45557	0.57200	1.57642	0.38435	
5	1.2852*-03	2.0282*+00	1.05834	0.99300	0.50441	0.62300	1.52547	0.43222	
6	1.5215*-03	2.2694*+00	1.05743	0.99460	0.54854	0.66700	1.47852	0.47703	
7	1.7399*-03	2.4134*+00	1.05652	0.99711	0.57295	0.69100	1.45455	0.50191	
8	2.0752*-03	2.7029*+00	1.05469	0.99961	0.61804	0.73300	1.40659	0.54962	
9	2.3876*-03	2.8960*+00	1.04923	1.00112	0.66604	0.75800	1.37662	0.57773	
10	2.6677*-03	3.1931*+00	1.04740	1.00135	0.68658	0.79200	1.33067	0.62340	
11	2.9972*-03	3.3609*+00	1.03737	1.00263	0.70832	0.81000	1.30764	0.64256	
12	3.6322*-03	3.8237*+00	1.02461	1.00450	0.76483	0.85400	1.24675	0.70184	
13	4.2418*-03	4.2315*+00	1.01732	1.00430	0.81114	0.88700	1.19580	0.75461	
14	4.9022*-03	4.7020*+00	1.00456	1.00738	0.86132	0.92200	1.14585	0.80831	
15	5.6134*-03	5.0489*+00	1.00000	1.00694	0.89645	0.94400	1.10889	0.85130	
16	6.2454*-03	5.3399*+00	0.99362	1.00866	0.92486	0.96200	1.08192	0.88349	
17	6.8530*-03	5.7554*+00	0.98997	1.00547	0.96393	0.98300	1.03496	0.93575	
18	7.5946*-03	6.0377*+00	0.98724	1.00317	0.98959	0.99600	1.01299	0.97068	
19	8.2804*-03	6.1154*+00	0.99318	1.00172	0.99651	0.99900	1.00500	0.99222	
D 20	8.8900*-03	6.1546*+00	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
21	9.6012*-03	6.1153*+00	1.00912	0.99972	0.99651	0.99800	1.00300	1.00409	
22	1.0008*-02	6.1153*+00	1.01185	0.99972	0.99651	0.99800	1.00300	1.00681	
23	1.0973*-02	6.0763*+00	1.01823	0.99945	0.99303	0.99600	1.00599	1.00812	
24	1.1659*-02	6.0430*+00	1.02461	0.99865	0.99005	0.99400	1.00799	1.01039	
25	1.2243*-02	6.0210*+00	1.02917	0.99878	0.98808	0.99300	1.00999	1.01186	
26	1.2827*-02	6.0155*+00	1.03099	0.99931	0.98759	0.99300	1.01099	1.01265	
27	1.3411*-02	6.0321*+00	1.03099	0.99971	0.98907	0.99400	1.00999	1.01467	

INPUT VARIABLES Y,U/UD,T/TD,P/PO

71040103		WALTRUP		PROFILE TABULATION			27 POINTS, DELTA AT POINT 22			
I	Y	PT2/P	P/PD	T0/T0D	M/M0	U/UD	T/TD	RHD/RHD0*U/UD		
1	0.0000+00	1.0000+00	1.01228	0.99043	0.00000	0.00000	1.73134	0.00000		
2	5.1054-04	1.5764+00	1.01228	0.99025	0.43087	0.53120	1.51995	0.35378		
3	7.8994-04	1.6572+00	1.01228	0.99214	0.45558	0.55820	1.50125	0.37639		
4	1.0046-03	1.7854+00	1.01228	0.99330	0.49069	0.59520	1.47135	0.40949		
5	1.2751-03	1.9426+00	1.01228	0.99411	0.52847	0.63360	1.43746	0.44619		
6	1.4732-03	2.0794+00	1.01228	0.99418	0.55791	0.66240	1.40966	0.47567		
7	1.8059-03	2.2551+00	1.01228	0.99770	0.59254	0.69640	1.38126	0.51037		
8	2.2504-03	2.4136+00	1.01156	0.99994	0.62155	0.72380	1.35606	0.53992		
9	2.5400-03	2.6062+00	1.01012	1.00064	0.65462	0.75340	1.32457	0.57454		
10	2.9972-03	2.7719+00	1.00361	1.00015	0.68150	0.77630	1.29757	0.60043		
11	3.6322-03	3.0597+00	0.99639	1.00111	0.72544	0.81290	1.25567	0.64504		
12	3.9878-03	3.3053+00	0.99061	1.00170	0.76067	0.84090	1.22208	0.68163		
13	4.2926-03	3.4898+00	0.98483	1.00395	0.78598	0.86110	1.20028	0.70653		
14	4.5974-03	3.7126+00	0.98338	1.00401	0.81542	0.88280	1.17208	0.74067		
15	4.9784-03	3.9118+00	0.97977	1.00674	0.84082	0.90210	1.15108	0.76784		
16	5.6642-03	4.2503+00	0.97543	1.00808	0.88216	0.93100	1.11379	0.81535		
17	6.4262-03	4.5337+00	0.97616	1.00546	0.91528	0.95140	1.08049	0.85953		
18	7.0612-03	4.8649+00	0.98121	1.00290	0.95301	0.97370	1.04390	0.91523		
19	7.6962-03	5.0890+00	0.98338	1.00300	0.97678	0.98800	1.02310	0.94965		
20	8.4328-03	5.2444+00	0.98555	1.00173	0.99328	0.99700	1.00758	0.97528		
21	9.1186-03	5.2888+00	0.99566	1.00035	0.99795	0.99900	1.00210	0.99258		
D 22	9.8298-03	5.3084+00	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
23	1.0516-02	5.3055+00	1.00361	1.00034	0.99970	1.00000	1.00060	1.00301		
24	1.1227-02	5.2948+00	1.00867	1.00034	0.99990	0.99960	1.00120	1.00706		
25	1.1862-02	5.2941+00	1.01084	1.00032	0.99850	0.99930	1.00160	1.00852		
26	1.2497-02	5.2594+00	1.01662	1.00030	0.99487	0.99720	1.00470	1.00903		
27	1.3157-02	5.2698+00	1.01806	0.99944	0.99596	0.99740	1.00290	1.01248		

INPUT VARIABLES Y,U/UD,T/TD,P/PO

71040104		WALTRUP		PROFILE TABULATION			27 POINTS, DELTA AT POINT 21			
I	Y	PT2/P	P/PD	T0/T0D	M/M0	U/UD	T/TD	RHD/RHD0*U/UD		
1	0.0000+00	1.0000+00	1.02549	0.93776	0.00000	0.00000	1.60205	0.00000		
2	1.8862-04	1.5682+00	1.02486	0.98383	0.44006	0.53500	1.47800	0.37097		
3	6.9850-04	1.6178+00	1.02358	0.98388	0.45606	0.55200	1.46500	0.38568		
4	1.0109-03	1.7269+00	1.02231	0.98529	0.48833	0.58600	1.44000	0.41602		
5	1.2649-03	1.8654+00	1.02103	0.98628	0.52466	0.62300	1.41000	0.45114		
6	1.5773-03	2.0314+00	1.01912	0.99704	0.56299	0.66400	1.39100	0.48648		
7	1.9710-03	2.2130+00	1.01721	1.00100	0.60066	0.70100	1.36200	0.52354		
8	2.6924-03	2.4025+00	1.01402	1.00132	0.63670	0.73400	1.32900	0.56004		
9	3.2512-03	2.6543+00	1.01020	1.00228	0.68085	0.77300	1.28900	0.60581		
10	3.5306-03	2.8727+00	1.00765	1.00257	0.71651	0.80300	1.25600	0.64422		
11	3.8100-03	2.9729+00	1.00446	1.00310	0.73220	0.81600	1.24200	0.65994		
12	4.3688-03	3.2566+00	1.00191	1.00435	0.77465	0.85000	1.20400	0.70733		
13	5.0038-03	3.5322+00	0.99873	1.00596	0.81356	0.88000	1.17000	0.75118		
14	5.5890-03	3.9101+00	0.99299	1.00392	0.86382	0.91500	1.12200	0.80979		
15	6.2230-03	4.2355+00	0.98853	1.00891	0.90473	0.94500	1.09100	0.85624		
16	6.6548-03	4.4940+00	0.98759	1.00639	0.93588	0.96400	1.06100	0.89757		
17	6.9342-03	4.5853+00	0.98725	1.00476	0.94662	0.97000	1.05000	0.91203		
18	7.4930-03	4.8564+00	0.98789	1.00439	0.97782	0.98900	1.02300	0.95506		
19	8.2042-03	4.9610+00	0.98853	1.00230	0.98957	0.99500	1.01100	0.97288		
20	8.7630-03	5.0503+00	0.99490	1.00059	0.99950	1.00000	1.00100	0.99391		
D 21	9.3980-03	5.0548+00	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
22	9.7536-03	4.9608+00	1.00637	1.00031	0.98956	0.99400	1.00000	0.99141		
23	1.0058-02	4.9432+00	1.01083	1.00065	0.98756	0.99300	1.01100	0.99284		
24	1.0897-02	4.9256+00	1.01530	1.00100	0.98561	0.99200	1.01300	0.99425		
25	1.1455-02	4.9125+00	1.01721	1.00076	0.98413	0.99100	1.01400	0.99414		
26	1.2065-02	4.8993+00	1.02167	1.00093	0.98266	0.99000	1.01500	0.99651		
27	1.2725-02	4.8819+00	1.02304	1.00088	0.98070	0.98900	1.01700	0.99974		

INPUT VARIABLES Y,U/UD,T/TD,P/PO

SECTION D - ADDITIONAL DATA

NB FACSIMILE FROM SOURCE PAPER: AUTHORS' SYMBOLS AND UNITS

TABLE B-I
WALL PRESSURE, TEMPERATURE, AND
SHEAR FOR RAMP 1

CAT 7104
0101-0104

x(in.)	Station	$\frac{P_w}{P_o}$	$\frac{T_w}{T_o}$	$\frac{T_w - T_{aw}}{T_{aw}}$	$\frac{\tau_w}{(lb/in^2)}$
0.00					
0.875	1	0.0775	0.9889	0.0495	
1.50		0.0759	0.9905		
2.00		0.0896	0.9908		
2.50		0.1078	0.9901		
3.00	2	0.1164	0.9907	0.0434	0.0227
3.50		0.1222	0.9909		
4.00		0.1286	0.9905		
4.50		0.1350	0.9907		
5.00	3	0.1401	0.9906	0.0391	0.0236
5.50		0.1443	0.9903		
6.00		0.1491	0.9897		
6.50		0.1555	0.9900		
7.00	4	0.1609	0.9388	0.0353	0.0275
7.50		0.1668	0.9899		
8.00		0.1727	0.9901		
8.50		0.1819	0.9890		
9.00		0.1871	0.9908		

TABLE B-VI
WALL PRESSURE, TEMPERATURE, AND
SHEAR FOR RAMP 2

CAT 7104
0201-0204

x (in.)	Station	$\frac{P_w}{P_o}$	$\frac{T_w}{T_o}$	$\frac{T_w - T_{aw}}{T_{aw}}$	$\frac{\tau_w}{(lb/in^2)}$
0.00					
0.875	1	0.0782	0.9897	0.0494	
1.50		0.0779	0.9902		
2.00		0.0757	0.9907		
2.50		0.0762	0.9901		
3.00	2	0.0837	0.9905	0.0468	.02207
3.50		0.0945	0.9908		
4.00		0.0983	0.9910		
4.50		0.1077	0.9902		
5.00	3	0.1085	0.9901	0.0415	.02270
5.50		0.1143	0.9898		
6.00		0.1216	0.9889		
6.50		0.1331	0.9900		
7.00	4	0.1418	0.9899	0.0393	.0217
7.50		0.1489	0.9904		
8.00		0.1530	0.9895		
8.50		0.1572	0.9901		
9.00		0.1662	0.9902		

SECTION D (CONT.) - ADDITIONAL DATA
 NB FACSIMILE FROM SOURCE PAPER: AUTHORS' SYMBOLS AND UNITS

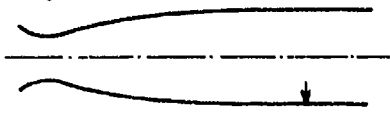
TABLE D-XI
 WALL PRESSURE, TEMPERATURE, AND
 SHEAR FOR RAMP 3 CAT 7104
 0301-0304

x (in.)	Station	$\frac{P_w}{P_o}$	$\frac{T_w}{T_o}$	$\frac{T_w - T_{RW}}{T_{RW}}$	$\frac{\tau_w}{(\text{lb.}/\text{in.}^2)}$
0.00					
0.875	1	0.0775	0.9907	0.0514	
1.50		0.0763	0.9911		
2.00		0.0773	0.9901		
2.50		0.0803	0.9904		
3.00	2	0.0830	0.9906	0.0492	0.0230
3.50		0.0875	0.9903		
4.00		0.0898	0.9907		
4.50		0.0908	0.9906		
5.00	3	0.0920	0.9900	0.0472	0.0229
5.50		0.0945	0.9911		
6.00		0.0988	0.9908		
6.50		0.1053	0.9905		
7.00	4	0.1093	0.9904	0.0413	0.0237
7.50		0.1171	0.9901		
8.00		0.1204	0.9905		
8.50		0.1325	0.9899		
9.00		0.1418	0.9902		

SECTION D - ADDITIONAL DATA
 NB FACSIMILE FROM SOURCE PAPER: AUTHORS' SYMBOLS AND UNITS

7104 TABLE D-XVI 7104
 0201 HOT WIRE MEASUREMENTS 0204

RAMP 2, STATION 1			RAMP 2, STATION 4		
y	$\rho u/\rho_o U_o$	$\sqrt{U'^2}/U$	y	$\rho u/\rho_o U_o$	$\sqrt{U'^2}/U$
.0886	.609	.0524	.0787	.521	.0679
.116	.676	.0495	.111	.601	.0715
.150	.738	.0468	.141	.668	.0726
.189	.801	.0428	.169	.720	.0677
.213	.841	.0370	.204	.805	.0585
.221	.896	.0312	.218	.848	.0476
.276	.933	.0252	.267	.936	.0370
.311	.962	.0150	.300	.976	.0317
.339	.980	.0103	.330	.992	.0211
.378	1.000	.00625	.342	.997	.0136
.419	1.011	.00445	.367	1.000	.00885

axisymmetric 	M : 19.5 R THETA X 10 ⁻³ : 2 - 4 TW/TR : 0.2	7105
		FPG - SHT
Axially symmetric blow down tunnel. Effectively continuous. D = 0.406 m. 29 < PO < 55 MN/m ² . TO : 1780 K. Nitrogen. 2 < RE/m X 10 ⁻⁶ < 3.		
BECKWITH I.E., HARVEY W.D. and CLARK F.L. 1971. Comparisons of turbulent boundary layer measurements at Mach number 19.5 with theory and an assessment of probe errors. NASA TN D-6192. And Harvey W.D., private communications, Harvey & Clark (1972).		

- 1 The test boundary layer was formed on the wall of a contoured axi symmetric nozzle approximately 2.25 m long from throat to exit. Profiles were measured at a single station near the nozzle exit and 2.083 m axially from the throat (X=0) at which the wall was inclined to the axis at 3.5°. The nozzle wall was finished to 0.4 µm and was actively cooled. Some disturbances in the flow originate from the nozzle wall in the neighbourhood of the contour point of inflection. There was a mean axial decrease in Mach number in the vicinity of the survey station of about 1.64 /m, where the radius of curvature in the longitudinal direction was about 32 m. Transition occurred naturally, and the boundary layer was believed to be turbulent over the full nozzle length except possibly in the immediate throat region, where calculations indicated that laminarisation could have occurred (PC and source, figure 12). The available wall pressure history is given in table 1 below. The wall temperature was kept nearly constant in the cooled part of the nozzle extending from X = 0.145 m downstream of the throat, at about 0.17 TO (330-300 K) but the high heat transfer rates in the throat region caused the wall temperature to reach an estimated value of about 0.8 TO.
- 2 Limited Pitot surveys were made on the opposite side of the nozzle at the 2.083 m station, and the results confirmed the axisymmetric nature of the flow.
- 3 Wall static pressure was measured at the stations listed in table 1 with holes 2.3 mm in diameter. Thermocouples used to monitor TW were placed at 0.305 m intervals along the nozzle, embedded 2.4 mm from the test surface.
- 4 The profile data as presented was all obtained with a single TPP (FPP) and a single TTP (FWP). Other probes were used however in assessing the correction procedures and all are discussed here. The FPP (h₁ = 0.28, h₂ = 0.13, b₁ = 3.81, b₂ = 3.66, l = 31.8 mm) was mounted on a rake which also carried 2 CPP (d₁ = 3.18, d₂ = 2.3, l (E) = 45 and 60 mm) separated in the Y-direction by 25.4 mm. The FPP could be replaced by the FWP (d = 0.25, b = 6.35, l (E) = 10 mm). The FWP was an unshielded 0.25 mm chromel-alumel thermocouple wire placed perpendicular to the flow and the profile normal. In addition to the central junction, two subsidiary junctions were established at the ends of the crossflow wire to allow a proper conduction and radiation correction procedure (Appendix A, source), which was applied to all observations. Static pressure profiles were obtained with a CCP (α = 17.5° semi angle, d = 3.18, l₁ = 50.8, l (E) = 100 mm) with four static holes (d = 0.78 mm) aligned on the diameters normal to and parallel to the wall.
- 5 All profile measurements were made normal to the wall at an axial distance of 2.083 m from the throat. The static holes in the CCP were on the same normal, as was the relevant static hole. The TO and PT2 profiles were taken on separate occasions and with a great many data points. All readings were normalized with the instantaneous tunnel reservoir conditions, which varied by up to 9 % during a two hour run. The profiles presented are obtained from faired curves through the corrected profile data, at greater Y-intervals than the original readings.
- 6 A major topic of the source paper is probe correction procedures. In the wall region, the viscous and rarefaction effects on the Pitot data involve correction factors of up to 2.14 as assessed by the authors. These completely outweigh the other possible corrections so that no adjustments have been made for wall proximity, shear displacement, thermal diffusion or turbulence effects. The corrections applied exceed 10 % for y/δ less than 0.4 - 0.5. Corrections to the TO data would be more properly described as a calib-

ration procedure. They may be summarised as amounting to finding a probe recovery factor of about 0.7 to 0.75 when the probe and its support are in a flow region where the total temperature is reasonably uniform. Conduction and radiation corrections were applied to all data however, and close to the wall where the probe was at a markedly lower temperature than the support, these were large and resulted in an effective recovery factor near one. The authors found large differences between the static pressure found at the wall and that calculated from PT2 measurements in the inviscid core. This was investigated with the CCP, the readings being corrected for bluntness and viscous-induced pressure effects after Bertram & Blackstock (1961). The surface temperature of the probe was estimated, assuming a linear variation of probe temperature with distance from 0.2 TO at the wall to 0.6 TO at the boundary layer edge. The resultant profile matches closely the static pressure values outside the boundary layer as predicted by a characteristics solution starting from the axial Mach number distribution. Both however lie about 20 % below the value found from Pitot measurements. A better match was found by using only the first order correction of Behrens (1963) (Source, fig. 7). Because of the very large correction factors involved (greater than 2) these static pressure distributions were not used in the profiles as presented by the authors, who instead assumed that P falls linearly with distance to PD. The authors present Mach number profiles computed on this basis with, for comparison, a profile with an alternative artificial static pressure distribution which represents the data in the wall region more exactly (Source figure 8a). The viscosity of Nitrogen was computed from equation 44 of Ahtye and Peng (1962).

The editors have first presented the profiles in the authors' final, corrected form, with the linear static pressure distribution. The edge stagnation state has been arbitrarily set to the nominal tunnel reservoir conditions. We have also reconstructed the authors' corrected static pressure distribution by scaling the data from figure 7 of the source paper. This, together with the authors' corrected TO data, was interpolated to the Y stations of the original Pitot measurements, and the revised profile O201 is presented as O201 P. The interpolation procedure introduces no additional uncertainty or error at greater than 2 %, except in those regions where the original data are themselves uncertain. O201 P therefore reports all the original, unsmoothed, Pitot data, in conjunction with smoothed P and TO data. The authors originally determined a CF value from the Mach number gradient at the wall. A later paper (Harvey & Clark 1972) describes shear stress measurements made at $X = 2.28$ m, that is 0.117 m downstream of the profile station. The balance used was an FEB for which the element diameter was 12.7 mm, with a peripheral gap of 0.076 mm, as described by Paros (1970). The editors have interpolated these measurements on the basis of the authors' R THETA values so as to give CF data in association with the profiles. For profiles O201, O301 the values are similar to the profile-derived values, but there is marked disagreement for profile O101. The authors remark on the possibility that this arises from the large Pitot tube errors involved (see § 10 above). The CQ value presented with the profiles is that derived by the authors from the limiting slope of the corrected TO profile.

5 DATA: 7105 O101-O301, O201 P, Pitot, TO and P profiles separately. NX = 1. CF from FEB in later experiment.

15 Editors' comments

The measurements presented here, with the addition of the later shear stress measurements, provide the only functionally complete description of the mean flow in a hypersonic boundary layer subject to substantial normal pressure gradients. The extent to which probe measurements required correction is such that a user should not refine too much upon any precise numerical value, but the qualitative picture is probably complete.

Attention is drawn to figure 7 of the source paper in particular. Here the problems of static pressure measurement in hypersonic conditions are graphically displayed. The profile tables for O201 P assume that the final adjusted static pressure variation is correct, but since the adjustments are so large, with calibration factors of up to 2, the accuracy is not high. A variation of this kind is, however, easily explained by a combination of the effects of streamline curvature and the separate contributions to normal stress of mean static pressure and normal Reynolds stress. A very similar variation is reported by Fischer et al. - CAT 7001 and comparison should be made between 7105O201 P and 7001O104. Kemp & Owen - CAT 7206 made no static pressure measurements, and also assumed a linear variation of P from PW to PO. Their data should show, even more markedly, a pressure variation like to that of O201 P as their range extends to even higher Mach numbers.

For many purposes the assumed static pressure variation used by the authors and retained for the data tables of 0101-0301 will not introduce too great a level of inaccuracy. It is unfortunately not possible to make a direct comparison with 0201P, for which the measured static profile was used, as the static pressure values in the free stream differ quite markedly. We have chosen to prepare 0201P assuming that the reported PT2 and P values are correct. As a consequence, the POD value which is calculated from them on the assumption that the D-point is outside the boundary layer is much higher than the measured tunnel reservoir pressure. (The appropriate small difference normal shock equation for very high Mach number is

$$\frac{dp_o}{p_o} = \left(\frac{\gamma}{\gamma-1}\right) \frac{dp_{t2}}{p_{t2}} - \left(\frac{1}{\gamma-1}\right) \frac{dp}{p}$$

so that a relatively modest underestimate of the value of PD results in a noticeably high value of POD).

The profiles 0101-0301 with assumed P(Y) are from smoothed curves, 0201 P has all original data points and will show scatter despite interpolated P and T0 values. Using van Driest coordinates no log-law region exists and the profiles show - at least in the inner region - a transitional behaviour.

TABLE 1: WALL AND FREE STREAM STATIC PRESSURE

POR - Reservoir pressure

P INF - 'Free stream' static pressure at x = 2.057 m from Pitot measurements.

7105		0101	0201	0301
x	-RZ	PW	PW	PW
(m)	(mm)	(N/m ²)	(N/m ²)	(N/m ²)
0.610	96.9	68.6	91.4	120.0
0.991	133.4	32.4	41.0	65.6
1.219	150.8	22.4	31.0	40.3
1.524	170.1	17.6	23.4	31.4
1.702	179.7	15.5	20.0	27.2
1.969	192.3	13.1	16.9	22.4
2.057	196.0	15.2	17.2	22.1
POR (MN/m ²)		29.65	43.09	65.50
P INF (N/m ²)		7.93	10.69	13.45

NB : NORMALISED VALUES

CAT 7105		BECKWITH		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW*	PD*		
X *	POD*	PW/PD	RED2D	CO *	H32	H32K	TW*	TD		
RZ *	TOD*	SW *	D2	PI2*	H42	D2K	UD	TR		
71050101	19.2600	0.1990	2.1370 ⁺⁰²	4.9000 ⁻⁰⁴	37.9916	2.3995	1.1613 ⁺⁰¹	7.9893 ⁺⁰⁰		
2.0830 ⁺⁰⁰	2.9700 ⁺⁰⁷	1.4535	2.3444 ⁺⁰³	3.1400 ⁻⁰⁴	1.8099	1.6327	3.0000 ⁺⁰²	2.2344 ⁺⁰¹		
-1.9750 ⁻⁰¹	1.6800 ⁺⁰³	1.0000	1.7085 ⁻⁰³	-4.6629 ⁺⁰¹	1.4420	1.0160 ⁻⁰²	1.8548 ⁺⁰³	1.5076 ⁺⁰³		
71050201	19.4200	0.1878	3.5633 ⁺⁰²	4.6000 ⁻⁰⁴	25.1921	2.3201	1.6766 ⁺⁰¹	1.1034 ⁺⁰¹		
2.0830 ⁺⁰⁰	4.3100 ⁺⁰⁷	1.5195	3.7699 ⁺⁰³	2.0600 ⁻⁰⁴	1.8187	1.6581	3.0000 ⁺⁰²	2.3290 ⁺⁰¹		
-1.9750 ⁻⁰¹	1.7800 ⁺⁰³	1.0000	2.0887 ⁻⁰³	-6.7667 ⁺⁰¹	1.5567	9.2971 ⁻⁰³	1.9095 ⁺⁰³	1.5973 ⁺⁰³		
71050301	19.6500	0.1822	3.2319 ⁺⁰²	4.6000 ⁻⁰⁴	31.2883	2.2886	2.1645 ⁺⁰¹	1.3098 ⁺⁰¹		
2.0830 ⁺⁰⁰	5.9500 ⁺⁰⁷	1.6525	3.3977 ⁺⁰³	1.6700 ⁻⁰⁴	1.8377	1.6783	3.0000 ⁺⁰²	2.3458 ⁺⁰¹		
-1.9750 ⁻⁰¹	1.8350 ⁺⁰³	1.0000	1.5828 ⁻⁰³	-8.7135 ⁺⁰¹	1.4735	7.7165 ⁻⁰³	1.9390 ⁺⁰³	1.6486 ⁺⁰³		
71050201P	21.7700	0.1973	2.4621 ⁺⁰²	4.3595 ⁻⁰⁴	41.0455	2.3512	1.6760 ⁺⁰¹	8.7893 ⁺⁰⁰		
2.0830 ⁺⁰⁰	7.5600 ⁺⁰⁷	1.9069	3.2713 ⁺⁰³	2.0600 ⁻⁰⁴	1.8211	1.6621	3.0000 ⁺⁰²	1.7696 ⁺⁰¹		
-1.9750 ⁻⁰¹	1.6950 ⁺⁰³	1.0000	1.4087 ⁻⁰³	-1.1869 ⁺⁰²	1.5436	8.5711 ⁻⁰³	1.8658 ⁺⁰³	1.5206 ⁺⁰³		

POD IS INPUT FOR 0101-0301. PD IS INPUT FOR 0201P.

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PH	H12PD H12PH	H32PI H32PA	H43PD H43PH	RED2PDD RED2PHD	HED2PDW HED2PHW	DBSTAR
71050101	1.7037 ⁻⁰³ 1.3016 ⁻⁰³	41.8254 47.7740	1.8094 1.8092	1.4441 1.4448	2.3131 ⁺⁰³ 2.3124 ⁺⁰³	2.0602 ⁺⁰² 2.0596 ⁺⁰²	8.7573 ⁻⁰²
71050201	2.0813 ⁻⁰³ 1.5439 ⁻⁰³	35.1465 32.8767	1.8180 1.8175	1.5822 1.5597	3.7168 ⁺⁰³ 3.7149 ⁺⁰³	3.4332 ⁺⁰² 3.4314 ⁺⁰²	5.5355 ⁻⁰²
71050301	1.5755 ⁻⁰³ 1.1007 ⁻⁰³	48.3993 42.9650	1.8369 1.8369	1.4804 1.4781	3.3456 ⁺⁰³ 3.3448 ⁺⁰³	3.1101 ⁺⁰² 3.1094 ⁺⁰²	5.2460 ⁻⁰²
71050201P	1.4093 ⁻⁰³ 8.8941 ⁻⁰⁴	51.4188 46.9629	1.8211 1.8211	1.5430 1.5402	3.2407 ⁺⁰³ 3.2399 ⁺⁰³	2.3813 ⁺⁰² 2.3806 ⁺⁰²	5.7265 ⁻⁰²

71050101		BECKWITH		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHO0*U/UD	
1	0.0000*+00	1.0000*+00	1.45353	0.17857	0.00000	0.00000	13.42670	0.00000	
2	2.0160*-03	1.4113*+00	1.44537	0.22160	0.03734	0.14510	15.10000	0.01389	
3	7.1680*-03	1.6274*+00	1.42451	0.32328	0.04486	0.20630	21.15000	0.01389	
4	1.2208*-02	2.1771*+00	1.40410	0.40050	0.05799	0.28470	24.10000	0.01659	
5	1.7248*-02	3.5931*+00	1.38369	0.48609	0.08031	0.39930	24.72000	0.02235	
6	2.2400*-02	6.1420*+00	1.36283	0.59406	0.10881	0.53060	23.78000	0.03041	
7	2.7440*-02	1.0175*+01	1.34242	0.70108	0.14250	0.65350	21.03000	0.04172	
8	3.2592*-02	1.5994*+01	1.32155	0.77039	0.18029	0.74290	16.98000	0.05782	
9	3.7632*-02	2.4722*+01	1.30114	0.82243	0.22536	0.81160	12.97000	0.08142	
10	4.2784*-02	3.5801*+01	1.28028	0.84059	0.27201	0.84890	9.74000	0.11158	
11	4.7824*-02	5.2142*+01	1.25987	0.83515	0.32910	0.86760	6.95000	0.15728	
12	5.2976*-02	7.9411*+01	1.23901	0.82378	0.40657	0.87860	4.67000	0.23310	
13	5.8016*-02	1.1391*+02	1.21860	0.82722	0.48737	0.89070	3.34000	0.32497	
14	6.3168*-02	1.4876*+02	1.19774	0.84713	0.57723	0.90710	2.65000	0.40999	
15	6.8208*-02	1.8802*+02	1.17733	0.86569	0.62666	0.92100	2.16000	0.50200	
16	7.3248*-02	2.3105*+02	1.15692	0.88630	0.69483	0.93440	1.81000	0.59751	
17	7.8400*-02	2.7418*+02	1.13606	0.89711	0.75703	0.94250	1.55000	0.69080	
18	8.3440*-02	3.1371*+02	1.11565	0.91801	0.80985	0.95440	1.39000	0.76635	
19	8.8592*-02	3.5667*+02	1.09479	0.93699	0.86384	0.96580	1.25000	0.84586	
20	9.3632*-02	3.9792*+02	1.07438	0.95122	0.91223	0.97400	1.14000	0.91793	
21	9.8784*-02	4.3928*+02	1.05352	0.96585	0.95853	0.98220	1.05000	0.98549	
22	1.0382*-01	4.6123*+02	1.03311	0.97484	0.98220	0.98710	1.01000	1.00968	
23	1.0886*-01	4.7636*+02	1.01270	0.98649	0.99820	0.99320	0.99000	1.01597	
D 24	1.1200*-01	4.7808*+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,T/TD P/PD=PW/PD+(1-PW/PD)*Y

71050201		BECKWITH		PROFILE TABULATION		21 POINTS, DELTA AT POINT 21			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHO0*U/UD	
1	0.0000*+00	1.0000*+00	1.51953	0.16854	0.00000	0.00000	12.88100	0.00000	
2	2.0022*-03	1.1647*+00	1.50847	0.24231	0.02430	0.10230	17.73000	0.00870	
3	6.3074*-03	1.5597*+00	1.48467	0.30633	0.04237	0.19240	20.62000	0.01385	
4	1.1383*-02	2.7901*+00	1.45662	0.41698	0.06816	0.33110	23.60000	0.02044	
5	1.6450*-02	5.3733*+00	1.42861	0.55420	0.10026	0.49210	24.09000	0.02918	
6	2.1526*-02	9.7238*+00	1.40056	0.65097	0.13800	0.62360	20.42000	0.04277	
7	2.6583*-02	2.1220*+01	1.37261	0.69798	0.20673	0.73470	12.63000	0.07985	
8	3.1654*-02	3.4221*+01	1.34455	0.73768	0.26366	0.79230	9.03000	0.11797	
9	3.6715*-02	5.4790*+01	1.31660	0.74224	0.33448	0.82000	6.01000	0.17964	
10	4.1783*-02	8.2507*+01	1.28840	0.75531	0.41105	0.84240	4.20000	0.25846	
11	4.6840*-02	1.1764*+02	1.26065	0.77883	0.49123	0.86490	3.10000	0.35172	
12	5.1888*-02	1.5912*+02	1.23275	0.76840	0.57161	0.86500	2.29000	0.46565	
13	5.6983*-02	2.0112*+02	1.20459	0.78288	0.64283	0.87670	1.86000	0.56778	
14	6.2040*-02	2.4347*+02	1.17664	0.84668	0.70743	0.91420	1.67000	0.64412	
15	6.7116*-02	2.8590*+02	1.14859	0.86933	0.76548	0.92810	1.47000	0.72517	
16	7.2192*-02	3.2927*+02	1.12053	0.91983	0.82288	0.95610	1.35000	0.79359	
17	7.7268*-02	3.7720*+02	1.09248	0.94232	0.88082	0.96890	1.21000	0.87479	
18	8.2156*-02	4.2735*+02	1.06546	0.95997	0.93762	0.97890	1.09000	0.95686	
19	8.7420*-02	4.6550*+02	1.03637	0.99658	0.97862	0.99800	1.04000	0.99451	
20	9.2496*-02	4.8028*+02	1.00831	0.99816	0.99404	0.99900	1.01000	0.99733	
D 21	9.4000*-02	4.8605*+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

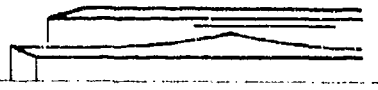
INPUT VARIABLES Y/DELTA,U/UD,T/TD P/PD=PW/PD+(1-PW/PD)*Y

71050301		BECKWITH		PROFILE TABULATION			20 POINTS, DELTA AT POINT 20			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD		
1	0.0000+00	1.0000+00	1.65254	0.16349	0.00000	0.00000	12.78875	0.00000		
2	2.0241-03	1.1625+00	1.63727	0.22608	0.02386	0.09820	16.94000	0.00949		
3	7.1103-03	1.8155+00	1.59890	0.38351	0.04905	0.24670	25.30000	0.01559		
4	9.6534-03	2.9006+00	1.57972	0.49602	0.06905	0.36770	28.36000	0.02048		
5	1.4740-02	6.1919+00	1.54135	0.64282	0.10712	0.55310	26.66000	0.03198		
6	1.9826-02	1.3836+01	1.50298	0.76208	0.16396	0.72180	19.38000	0.05598		
7	2.4921-02	2.5835+01	1.46454	0.78760	0.22589	0.79770	12.47000	0.09369		
8	3.0007-02	4.2065+01	1.42618	0.79634	0.28928	0.83590	8.35000	0.14277		
9	3.5093-02	6.5029+01	1.38781	0.80450	0.36038	0.86190	5.72000	0.20912		
10	4.0179-02	9.5150+01	1.34944	0.82131	0.43642	0.88260	4.09000	0.29120		
11	4.5265-02	1.3377+02	1.31107	0.83250	0.51783	0.89690	3.00000	0.39197		
12	5.0360-02	1.7454+02	1.27263	0.85671	0.59173	0.91480	2.39000	0.48711		
13	5.5446-02	2.1868+02	1.23426	0.87884	0.66253	0.92990	1.97000	0.58261		
14	6.0533-02	2.6581+02	1.19589	0.90128	0.73057	0.94410	1.67000	0.67607		
15	6.5628-02	3.1599+02	1.15746	0.92703	0.79666	0.95930	1.45000	0.76576		
16	7.0714-02	3.6495+02	1.11909	0.95016	0.85624	0.97250	1.29000	0.84365		
17	7.5800-02	4.1611+02	1.08072	0.97226	0.91436	0.98480	1.16000	0.91749		
18	8.0886-02	4.6079+02	1.04235	0.98249	0.96225	0.99070	1.06000	0.97420		
19	8.5972-02	4.8592+02	1.00398	0.99631	0.98817	0.99800	1.02000	0.98233		
D 20	8.6500-02	4.9762+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		

INPUT VARIABLES Y/DELTA,U/UD,T/TD P/PD=M/PD+(1-M/PD)*Y

71050201P		BECKWITH		PROFILE TABULATION			44 POINTS, DELTA AT POINT 43			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD		
1	0.0000+00	1.0000+00	1.90686	0.17699	0.00000	0.00000	16.45336	0.00000		
2	2.7430-03	1.2066+00	1.90686	0.26200	0.02412	0.11761	23.78494	0.00943		
3	5.2830-03	1.4150+00	1.89216	0.30600	0.03316	0.17087	26.54337	0.01218		
4	7.8230-03	1.7794+00	1.86275	0.35300	0.04336	0.23229	28.69791	0.01508		
5	1.0361-02	2.5082+00	1.81373	0.41000	0.05668	0.31101	30.10422	0.01874		
6	1.2903-02	3.3794+00	1.71569	0.47300	0.06849	0.38355	31.36269	0.02098		
7	1.5443-02	5.0741+00	1.60784	0.55000	0.08663	0.48066	30.78336	0.02511		
8	1.7993-02	7.8109+00	1.43627	0.62200	0.10960	0.57849	27.95901	0.02982		
9	2.0523-02	1.0969+01	1.34804	0.67600	0.13114	0.65070	24.61851	0.03563		
10	2.3063-02	1.3557+01	1.27451	0.71100	0.14644	0.69396	22.45687	0.03936		
11	2.5603-02	1.9099+01	1.21569	0.74200	0.17474	0.74651	18.25170	0.04972		
12	2.8143-02	2.5620+01	1.16176	0.76100	0.20303	0.78251	14.85417	0.06120		
13	3.0683-02	3.4597+01	1.10784	0.77600	0.23647	0.81223	11.79776	0.07627		
14	3.3223-02	4.7280+01	1.06863	0.78100	0.27699	0.83296	9.04348	0.09843		
15	3.5763-02	6.2261+01	1.02941	0.78500	0.31824	0.84761	7.09401	0.12300		
16	3.8303-02	7.4577+01	0.99510	0.78800	0.36851	0.85596	6.03235	0.14120		
17	4.0843-02	8.9440+01	0.96569	0.79200	0.38186	0.86392	5.11855	0.16299		
18	4.3383-02	1.0701+02	0.94608	0.80000	0.41787	0.87314	4.36607	0.18920		
19	4.5923-02	1.3574+02	0.93137	0.80900	0.47083	0.88340	3.52033	0.23372		
20	4.8463-02	1.6779+02	0.91667	0.81400	0.52366	0.89001	2.88864	0.28243		
21	5.1003-02	2.0423+02	0.90686	0.81900	0.57786	0.89571	2.30264	0.33808		
22	5.3543-02	2.3235+02	0.90686	0.82400	0.61644	0.90011	2.13208	0.38285		
23	5.6083-02	2.5717+02	0.90196	0.83800	0.64860	0.90891	1.96378	0.41746		
24	5.8623-02	2.8900+02	0.90686	0.85100	0.68764	0.91717	1.77901	0.46754		
25	6.1163-02	3.1020+02	0.91667	0.87100	0.71245	0.92858	1.69877	0.50107		
26	6.3703-02	3.4634+02	0.92157	0.88800	0.75287	0.93860	1.55425	0.55653		
27	6.6243-02	3.6820+02	0.93627	0.90100	0.77630	0.94596	1.48487	0.59647		
28	6.8783-02	3.9163+02	0.95098	0.91000	0.80064	0.95116	1.41134	0.64091		
29	7.1323-02	4.1485+02	0.96569	0.92400	0.82407	0.95849	1.35396	0.68391		
30	7.3863-02	4.3922+02	0.98039	0.93600	0.84796	0.96550	1.29647	0.73012		
31	7.6403-02	4.5650+02	0.99510	0.94800	0.86449	0.97194	1.26403	0.76515		
32	7.8943-02	5.0626+02	1.00000	0.95400	0.91043	0.97568	1.14848	0.84954		
33	8.1483-02	5.1189+02	1.00980	0.96300	0.91548	0.98034	1.14671	0.86329		
34	8.4023-02	5.3314+02	1.01471	0.97000	0.93431	0.98414	1.10950	0.90006		
35	8.6563-02	5.6990+02	1.01961	0.97800	0.96601	0.98837	1.04726	0.96247		
36	8.9103-02	5.8352+02	1.01961	0.98300	0.97749	0.99122	1.02828	0.98289		
37	9.1643-02	5.9121+02	1.01961	0.99000	0.98392	0.99482	1.02227	0.99223		
38	9.4183-02	6.0174+02	1.01471	0.99600	0.99265	0.99792	1.01065	1.00193		
39	9.6723-02	6.0508+02	1.00980	1.00000	0.99541	0.99995	1.00915	1.00060		
40	9.9263-02	6.0341+02	1.00980	1.00000	0.99403	0.99994	1.01192	0.99784		
41	1.0180-01	6.0508+02	1.00980	1.00000	0.99541	0.99995	1.00915	1.00060		
42	1.0434-01	6.1670+02	1.00490	1.00000	1.00059	1.00005	0.99097	1.01411		
D 43	1.0942-01	6.1048+02	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000		
44	1.1450-01	6.0493+02	0.99020	1.00000	0.99495	0.99995	1.01088	0.98027		

INPUT VARIABLES Y,P/PD,M,T0/T0D

	<p>M : 4, falling to 2.4 then rising to 3.7 (Series 01). : 4, ZPG (Series 02). R THETA X 10⁻³ : 4 - 14. TW / TR : 1.</p>	<p>7201</p>
		<p>ZPG - APG - FPG (ZPG) AW</p>
<p>Continuous tunnel with symmetrical flexible nozzle, W = H = 1 m. L = 5 m. PO : 496 (± 3.5) KN/m². TO : 318 (± 1) K. Air: Dew point 239-247 K. RE/m X 10⁻⁶ : 20 at M = 4.</p>		
<p>LEWIS J.E., GRAN R.L. and KUBOTA T., 1972. An experiment on the adiabatic compressible turbulent boundary layer in adverse and favourable pressure gradients. J. Fluid Mech. 51, 657-672. And Gran R.L., private communications.</p>		

- 1 The tests were performed on the inner surface of a cylinder (D = 0.508, L = 1.3 m) mounted on the centre line of the windtunnel. A pressure gradient could be imposed by a centre-body, itself hollow, causing the streamwise pressure variation tabulated in section B. The leading edge of the cylinder (X = 0) was chamfered on the outside at 11° with a nose radius of 0.05 mm. The profiles were measured in the range 0.29 < X < 0.88 m. Maximum deviation from a straight generator was less than 5 x 10⁻⁴ m/m in the test-area with no local slope exceeding 0.06°. Surface roughness was less than 2.5 µm. The test-surface was not cooled, the greatest departure of TW from TR being 2.5 % at the pressure maximum (X = 0.47 m). Tunnel
- 2 calibration tests gave the empty-tunnel Mach number as 4.026 (+ 0.022, - 0.026).
- 3 The boundary layer was tripped 3 mm back from the leading edge using 0.15 mm thick fibre-glass tape with a serrated upstream edge. Transition is believed to have been complete upstream of X = 0.204 m, the
- 5 upstream limit for measurements. Static pressure and heat-transfer measurements made at three streamwise stations showed the flow to be uniform round the circumference, and good agreement was reached in a streamwise momentum balance.
- 6 Static holes (diameter 0.51 mm) were drilled along one generator from X = 50.8 to 1016 mm at 12.7 mm
- 8 intervals, with additional holes at 6.35 mm intervals between X = 356 and 635 mm. Additional tappings were also distributed circumferentially at 45° intervals for X = 63.5, 444 and 673 mm. Wall temperature was found from the heat-flux gauges (see below) and checked using four thermocouples. Stanton tubes were mounted on generators 8.6° to either side of the PW generator at nominal 25.4 mm intervals from X = 51 to X = 965 mm. The tubes were formed by placing a 4.8 mm square piece of thin metal, with a sharp leading edge chamfered at 6° on the underside, approximately 0.51 mm ahead of the centre-line of a 0.51 mm diameter static hole. The side and back edges of the thin plate were sealed. The Stanton tube heights were within the range 0.12 < h < 0.21 mm. Steady state heat-flux meters after Gardon (1960) were mounted on a generator 6° from the PW generator. Gauges of 6.35 mm diameter were placed at nominal 25.4 mm intervals from X = 50.8 to 1016 mm except between X = 356 and 661 mm where gauges of 3.18 mm diameter were placed at 12.7 mm intervals.
- 7 Traverses were made with Pitot, TO and P-probes. The transducer attached to the latter failed so that P-traverse measurements were not used. The TTP (d₁ = 1.52 mm, l = 29 mm) was of STP type, inclined at 10° to the wall. The TPP was an FPP (h₁ = 0.46 mm, b₁ = 2.1 mm, l = 15.2 mm) formed by flattening a 1.6 mm
- 8 diameter tube, and inclined at 6° to the wall. All traverses for a given X-value were made simultaneously, with the PO traverse over the PW generator and the TO and P traverses slightly to either side. The X-value
- 9 was the same for all three within 0.5 mm. The TO data points were interpolated to the Y values of the PO measurements. The PW (X) data were fitted to analytic expressions for interpolation where necessary.
- 10 No corrections were applied to the probe-data. Sutherland's viscosity law was used.
- 11 The authors state that within experimental accuracy the data satisfied the relation (TO - TW) / (TOD - TW)
- 12 = U/UD and this has been used together with the assumption P = PW to construct the tables below. The total conditions at the layer edge have been set arbitrarily equal to the nominal reservoir conditions. The wall temperature has been set constant at 293 K following the authors' statement that (TOD - TW) / TOD was nearly constant at 0.08. No heat transfer data is presented, the authors stating that Q was zero within experimental accuracy.

- 13 The data presented consists of two profile sequences. The first, 0101 - 0119 consists of ZPG (01-05) followed by APG (06-14) and FPG (15-19). Duplicate profiles were obtained for 01 11/12/14/16, but since they had relatively few data points, they are not presented here. The second set, 0201 - 0209, provides, for comparison, ZPG data in the downstream portion ($X < 495$ mm), obtained with no centrebody. The CF values presented are the authors', obtained by the curve-fitting procedure of Coles & Hirst (1969) applied to equivalent incompressible velocity profiles transformed as suggested by Van Driest (1951). The resultant calibration function for the Stanton tubes was presented (source, figure 3) as evidence of consistency.

5 DATA: 7201 0101 to 0209. PT2 and T0 simultaneously, $NX = 19$ and 9. CF from profiles (curve fitting). Confirmatory Stanton tube observations.

15 Editors' comments

The axi-symmetric configuration chosen results in a flow free of significant end effects. Axial symmetry corrections were small as $\delta/RZ < 0.07$. The pressure gradient was applied as a reflected wave on a straight surface so that little or no normal pressure gradient is to be expected except at the changes from ZPG to APG and APG to FPG. The authors state that static pressure measurements showed the pressure to be constant within 10 % across the layer. There are very small intervals between successive profiles, so that the layer development can be followed in detail.

The authors give a full discussion of the profiles in relation to the "wall law" and "wake law" in the source paper. The values of CF given here assume that this is a valid and complete description, so that they should be used with caution in the FPG region.

Comparisons should be made with the similar flow observed by Peake et al. - CAT 7102, series 02 - though there is little detail in the compression region and the study is more concerned with the constant-pressure relaxation which follows. Nominally planar APG flows of the same type are studied in some detail by Zwarts - CAT 7007, Thomas - CAT 7401 and with fewer stations by Waltrup and Schetz - CAT 7104. The FPG case is covered by Michel - CAT 6902 and Voisinet et al. - CAT 7304. The authors have repeated the investigation with a strongly cooled wall (Gran et al. 1974) but the numerical data is not at present available.

CAT 7201		LEWIS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	MD *	TH/TR	PE2M	CF *	H12	H12K	PW	PD		
X *	POD*	PH/PO*	RED2D	CO	H32	H32K	TH*	TD		
RZ *	TOO*	SH *	D2	PI2*	H42	D2K	UD	TR		
72010101	3.9800	1.0005	1.4803"+03	1.5154"-03	7.9198	1.4601	3.3551"+03	3.3551"+03		
2.9159"-01	4.9600"+05	1.0000	4.9214"+03	NM	1.8339	1.8099	2.9300"+02	7.6294"+01		
-2.5400"-01	3.1800"+02	0.0000	2.5217"-04	0.0000"+00	0.1444	4.6448"-04	6.9701"+02	2.9286"+02		
72010102	3.9800	1.0005	1.3601"+03	1.6157"-03	7.7991	1.4026	3.3551"+03	3.3551"+03		
3.0455"-01	4.9600"+05	1.0000	4.5217"+03	NM	1.8344	1.8054	2.9300"+02	7.6294"+01		
-2.5400"-01	3.1800"+02	0.0000	2.3169"-04	0.0000"+00	0.1445	4.2450"-04	6.9701"+02	2.9286"+02		
72010103	3.9800	1.0005	1.5468"+03	1.5501"-03	7.7648	1.3919	3.3551"+03	3.3551"+03		
3.1674"-01	4.9600"+05	1.0000	5.1425"+03	NM	1.8416	1.8169	2.9300"+02	7.6294"+01		
-2.5400"-01	3.1800"+02	0.0000	2.6350"-04	0.0000"+00	0.1450	4.7561"-04	6.9701"+02	2.9286"+02		
72010104	3.9800	1.0005	1.6522"+03	1.4531"-03	7.8327	1.4013	3.3551"+03	3.3551"+03		
3.2969"-01	4.9600"+05	1.0000	5.4930"+03	NM	1.8291	1.7917	2.9300"+02	7.6294"+01		
-2.5400"-01	3.1800"+02	0.0000	2.8146"-04	0.0000"+00	0.1436	5.2785"-04	6.9701"+02	2.9286"+02		
72010105	3.9800	1.0005	1.5143"+03	1.4530"-03	7.8375	1.4032	3.3551"+03	3.3551"+03		
3.4265"-01	4.9600"+05	1.0000	5.0346"+03	NM	1.8239	1.7927	2.9300"+02	7.6294"+01		
-2.5400"-01	3.1800"+02	0.0000	2.5797"-04	0.0000"+00	0.1436	4.8452"-04	6.9701"+02	2.9286"+02		
72010106	3.8329	0.9989	1.7003"+03	1.4466"-03	7.3983	1.4061	4.0919"+03	4.0919"+03		
3.5509"-01	4.9600"+05	1.0000	5.3443"+03	NM	1.8146	1.7880	2.9300"+02	8.0747"+01		
-2.5400"-01	3.1800"+02	0.0000	2.5369"-04	3.0310"-01	0.1418	4.6959"-04	6.9056"+02	2.9333"+02		
72010107	3.5295	0.9952	2.2417"+03	1.3768"-03	6.5996	1.4481	6.2366"+03	6.2366"+03		
3.8049"-01	4.9600"+05	1.0000	6.2620"+03	NM	1.7943	1.7674	2.9300"+02	9.1079"+01		
-2.5400"-01	3.1800"+02	0.0000	2.5311"-04	3.8798"-01	0.1375	4.5352"-04	6.7536"+02	2.9440"+02		
72010108	3.3775	0.9932	2.8211"+03	1.2666"-03	6.3806	1.5758	7.7487"+03	7.7487"+03		
3.9319"-01	4.9600"+05	1.0000	7.4206"+03	NM	1.7926	1.7655	2.9300"+02	9.6907"+01		
-2.5400"-01	3.1800"+02	0.0000	2.7635"-04	5.1195"-01	0.1358	4.7740"-04	6.6663"+02	2.9501"+02		
72010109	3.2267	0.9910	2.9751"+03	1.2688"-03	5.8675	1.4972	9.6474"+03	9.6474"+03		
4.0589"-01	4.9600"+05	1.0000	7.3685"+03	NM	1.7727	1.7483	2.9300"+02	1.0317"+02		
-2.5400"-01	3.1800"+02	0.0000	2.5281"-04	5.2098"-01	0.1328	4.3478"-04	6.5712"+02	2.9566"+02		
72010110	3.0747	0.9886	3.5624"+03	1.1742"-03	5.6828	1.6260	1.2077"+04	1.2077"+04		
4.1859"-01	4.9600"+05	1.0000	8.3002"+03	NM	1.7680	1.7464	2.9300"+02	1.1001"+02		
-2.5400"-01	3.1800"+02	0.0000	2.6205"-04	6.5298"-01	0.1308	4.3643"-04	6.4658"+02	2.9983"+02		
72010111	2.9207	0.9860	4.1226"+03	1.2271"-03	5.1226	1.5220	1.5211"+04	1.5211"+04		
4.3129"-01	4.9600"+05	1.0000	9.0268"+03	NM	1.7594	1.7373	2.9300"+02	1.1750"+02		
-2.5400"-01	3.1800"+02	0.0000	2.6195"-04	7.0225"-01	0.1283	4.2337"-04	6.3482"+02	2.4715"+02		
72010112	2.7713	0.9833	4.4661"+03	1.1809"-03	5.0278	1.7057	1.9096"+04	1.9096"+04		
4.4400"-01	4.9600"+05	1.0000	9.2038"+03	NM	1.7662	1.7479	2.9300"+02	1.2539"+02		
-2.5400"-01	3.1800"+02	0.0000	2.4610"-04	7.7118"-01	0.1268	3.7944"-04	6.2220"+02	2.9797"+02		
72010113	2.6169	0.9803	5.7028"+03	1.5257"-03	4.2220	1.4395	2.4216"+04	2.4216"+04		
4.5669"-01	4.9600"+05	1.0000	1.1040"+04	NM	1.7496	1.7808	2.9300"+02	1.3420"+02		
-2.5400"-01	3.1800"+02	0.0000	2.7150"-04	7.4629"-01	0.1263	3.8797"-04	6.0781"+02	2.9888"+02		
72010114	2.4661	0.9772	6.7840"+03	1.7262"-03	3.8493	1.4210	3.0603"+04	3.0603"+04		
4.6939"-01	4.9600"+05	1.0000	1.2357"+04	NM	1.8182	1.8086	2.9300"+02	1.4348"+02		
-2.5400"-01	3.1800"+02	0.0000	2.8041"-04	7.7286"-01	0.1252	3.7717"-04	5.9227"+02	2.9985"+02		
72010115	2.5545	0.9790	6.7071"+03	1.8069"-03	3.9027	1.3867	2.6673"+04	2.6673"+04		
4.8209"-01	4.9600"+05	1.0000	1.2661"+04	NM	1.8199	1.8298	2.9300"+02	1.3796"+02		
-2.5400"-01	3.1800"+02	0.0000	3.0110"-04	-4.6879"-01	0.1280	4.0063"-04	6.0157"+02	2.9928"+02		
72010116	2.6504	0.9810	6.3462"+03	1.9101"-03	4.0313	1.3145	2.2995"+04	2.2995"+04		
4.4979"-01	4.9600"+05	1.0000	1.2453"+04	NM	1.8614	1.8511	2.9300"+02	1.3233"+02		
-2.5400"-01	3.1800"+02	0.0000	3.1183"-04	-4.0969"-01	0.1306	4.0931"-04	6.1106"+02	2.9860"+02		
72010117	2.9977	0.9874	5.4645"+03	1.9004"-03	4.6944	1.2617	1.3550"+04	1.3550"+04		
5.4559"-01	4.9600"+05	1.0000	1.2342"+04	NM	1.8886	1.8762	2.9300"+02	1.1368"+02		
-2.5400"-01	3.1800"+02	0.0000	3.7357"-04	-3.2206"-01	0.1378	4.9625"-04	6.4084"+02	2.9678"+02		
72010118	3.5347	0.9953	4.7450"+03	1.6705"-03	6.0271	1.2326	6.1909"+03	6.1909"+03		
6.4719"-01	4.9600"+05	1.0000	1.3282"+04	NM	1.8930	1.8737	2.9300"+02	9.0888"+01		
-2.5400"-01	3.1800"+02	0.0000	5.3835"-04	-2.4024"-01	0.1447	7.7625"-04	6.7564"+02	2.9438"+02		
72010119	3.6361	0.9966	4.4744"+03	1.6387"-03	6.3213	1.2365	5.3685"+03	5.3685"+03		
6.7259"-01	4.9600"+05	1.0000	1.3032"+04	NM	1.8922	1.8710	2.9300"+02	8.7261"+01		
-2.5400"-01	3.1800"+02	0.0000	5.5762"-04	-2.0772"-01	0.1457	8.2026"-04	6.8101"+02	2.9400"+02		

CAT 7201

LEWIS

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ *	MD * MOD* TOD*	TW/TR PW/PO* SW * F2	PEO2W REFD2D F2	CF * CO PI2*	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR
72010201	3.9800	1.0005	2.2878 ⁺⁰³	1.3574 ⁻⁰³	7.8179	1.3900	3.3551 ⁺⁰³	3.3551 ⁺⁰³
4.9479 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	7.6062 ⁺⁰³	NM	1.8294	1.8044	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	3.8973 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1440	7.2586 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010202	3.9800	1.0005	2.4727 ⁺⁰³	1.3542 ⁻⁰³	7.8492	1.4161	3.3551 ⁺⁰³	3.3551 ⁺⁰³
5.4559 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	8.2209 ⁺⁰³	NM	1.8368	1.8152	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	4.2123 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1446	7.7220 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010203	3.9800	1.0005	2.6543 ⁺⁰³	1.3289 ⁻⁰³	7.7659	1.3601	3.3551 ⁺⁰³	3.3551 ⁺⁰³
5.9665 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	8.8247 ⁺⁰³	NM	1.8298	1.8035	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	4.5217 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1440	8.4055 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010204	3.9800	1.0005	2.6314 ⁺⁰³	1.3531 ⁻⁰³	7.7436	1.3574	3.3551 ⁺⁰³	3.3551 ⁺⁰³
5.9690 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	8.7482 ⁺⁰³	NM	1.8352	1.8108	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	4.4825 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1444	8.2342 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010205	3.9800	1.0005	2.8840 ⁺⁰³	1.3043 ⁻⁰³	7.7463	1.3475	3.3551 ⁺⁰³	3.3551 ⁺⁰³
6.4719 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	9.5863 ⁺⁰³	NM	1.8299	1.8045	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	4.9129 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1440	9.1418 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010206	3.9800	1.0005	2.9769 ⁺⁰³	1.2999 ⁻⁰³	7.7040	1.3285	3.3551 ⁺⁰³	3.3551 ⁺⁰³
6.7259 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	9.8971 ⁺⁰³	NM	1.8330	1.8086	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	5.0712 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1442	9.3727 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010207	3.9800	1.0005	3.2951 ⁺⁰³	1.2367 ⁻⁰³	7.8520	1.3950	3.3551 ⁺⁰³	3.3551 ⁺⁰³
7.7368 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.0955 ⁺⁰⁴	NM	1.8261	1.7979	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	5.6132 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1436	1.0529 ⁻⁰³	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010208	3.9800	1.0005	3.7273 ⁺⁰³	1.2117 ⁻⁰³	7.7980	1.3690	3.3551 ⁺⁰³	3.3551 ⁺⁰³
8.7478 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2392 ⁺⁰⁴	NM	1.8315	1.8068	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	6.3494 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1440	1.1786 ⁻⁰³	6.9701 ⁺⁰²	2.9286 ⁺⁰²
72010209	3.9800	1.0005	3.6475 ⁺⁰³	1.2263 ⁻⁰³	7.7222	1.3229	3.3551 ⁺⁰³	3.3551 ⁺⁰³
8.7579 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2127 ⁺⁰⁴	NM	1.8295	1.8081	2.9300 ⁺⁰²	7.6294 ⁺⁰¹
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	6.2135 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1439	1.1617 ⁻⁰³	6.9701 ⁺⁰²	2.9286 ⁺⁰²

CAT 7201		LEWIS		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN	MD *	TW/TR	RED2H	CF *	H12	H12K	PW	PD		
X *	POD*	PW/PO*	RED2D	CO	H32	H32K	UD*	TD		
RZ *	TOD*	SW *	O2	PI2*	H42	D2K	UD	TR		
72010101	3.9800	1.0005	1.4803 ⁺⁰³	1.5154 ⁻⁰³	7.9198	1.4601	3.3551 ⁺⁰³	3.3551 ⁺⁰³		
2.9159 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	4.9214 ⁺⁰³	NM	1.8339	1.8099	2.9300 ⁺⁰²	7.6294 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.5217 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1444	4.6448 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²		
72010102	3.9800	1.0005	1.3601 ⁺⁰³	1.6150 ⁻⁰³	7.7991	1.4026	3.3551 ⁺⁰³	3.3551 ⁺⁰³		
3.0455 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	4.5217 ⁺⁰³	NM	1.8344	1.8054	2.9300 ⁺⁰²	7.6294 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.3169 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1445	4.2450 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²		
72010103	3.9800	1.0005	1.5465 ⁺⁰³	1.5501 ⁻⁰³	7.7648	1.3919	3.3551 ⁺⁰³	3.3551 ⁺⁰³		
3.1674 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	5.1425 ⁺⁰³	NM	1.8416	1.8169	2.9300 ⁺⁰²	7.6294 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.6350 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1450	4.7361 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²		
72010104	3.9800	1.0005	1.6522 ⁺⁰³	1.4531 ⁻⁰³	7.8327	1.4013	3.3551 ⁺⁰³	3.3551 ⁺⁰³		
3.2969 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	5.4930 ⁺⁰³	NM	1.8241	1.7917	2.9300 ⁺⁰²	7.6294 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.8146 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1436	5.2785 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²		
72010105	3.9800	1.0005	1.5143 ⁺⁰³	1.4530 ⁻⁰³	7.8375	1.4032	3.3551 ⁺⁰³	3.3551 ⁺⁰³		
3.4265 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	5.0346 ⁺⁰³	NM	1.8239	1.7927	2.9300 ⁺⁰²	7.6294 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.5797 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1436	4.8452 ⁻⁰⁴	6.9701 ⁺⁰²	2.9286 ⁺⁰²		
72010106	3.8329	0.9989	1.7003 ⁺⁰³	1.4466 ⁻⁰³	7.3983	1.4061	4.0919 ⁺⁰³	4.0919 ⁺⁰³		
3.3509 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	5.3443 ⁺⁰³	NM	1.8156	1.7880	2.9300 ⁺⁰²	8.0747 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.4369 ⁻⁰⁴	3.0310 ⁻⁰¹	0.1418	4.6959 ⁻⁰⁴	6.9056 ⁺⁰²	2.9333 ⁺⁰²		
72010107	3.5295	0.9952	2.2417 ⁺⁰³	1.3768 ⁻⁰³	6.9996	1.4481	6.2366 ⁺⁰³	6.2366 ⁺⁰³		
3.8049 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	6.2620 ⁺⁰³	NM	1.7943	1.7674	2.9300 ⁺⁰²	9.1079 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.5311 ⁻⁰⁴	3.8798 ⁻⁰¹	0.1375	4.5352 ⁻⁰⁴	6.7536 ⁺⁰²	2.9440 ⁺⁰²		
72010108	3.3775	0.9932	2.8211 ⁺⁰³	1.2666 ⁻⁰³	6.3806	1.5758	7.7487 ⁺⁰³	7.7487 ⁺⁰³		
3.9319 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	7.4206 ⁺⁰³	NM	1.7926	1.7655	2.9300 ⁺⁰²	9.6907 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.7635 ⁻⁰⁴	5.1195 ⁻⁰¹	0.1358	4.7740 ⁻⁰⁴	6.6663 ⁺⁰²	2.9501 ⁺⁰²		
72010109	3.2267	0.9910	2.9751 ⁺⁰³	1.2688 ⁻⁰³	5.8675	1.4972	9.6474 ⁺⁰³	9.6474 ⁺⁰³		
4.0589 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	7.3685 ⁺⁰³	NM	1.7727	1.7483	2.9300 ⁺⁰²	8.0317 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.5281 ⁻⁰⁴	5.2098 ⁻⁰¹	0.1328	4.3478 ⁻⁰⁴	6.5712 ⁺⁰²	2.9566 ⁺⁰²		
72010110	3.0747	0.9886	3.5624 ⁺⁰³	1.1742 ⁻⁰³	5.6828	1.6260	1.2077 ⁺⁰⁴	1.2077 ⁺⁰⁴		
4.1859 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	8.3002 ⁺⁰³	NM	1.7680	1.7464	2.9300 ⁺⁰²	1.1011 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.6205 ⁻⁰⁴	6.5298 ⁻⁰¹	0.1308	4.3643 ⁻⁰⁴	6.4658 ⁺⁰²	2.9637 ⁺⁰²		
72010111	2.9209	0.9860	4.1226 ⁺⁰³	1.2271 ⁻⁰³	5.1226	1.5220	1.9211 ⁺⁰⁴	1.5211 ⁺⁰⁴		
4.3129 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	9.0268 ⁺⁰³	NM	1.7594	1.7373	2.9300 ⁺⁰²	1.1750 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.6195 ⁻⁰⁴	7.0225 ⁻⁰¹	0.1262	4.2337 ⁻⁰⁴	6.3482 ⁺⁰²	2.9715 ⁺⁰²		
72010112	2.7713	0.9833	4.4661 ⁺⁰³	1.1809 ⁻⁰³	5.0278	1.7057	1.9096 ⁺⁰⁴	1.9096 ⁺⁰⁴		
4.4440 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	9.2038 ⁺⁰³	NM	1.7682	1.7479	2.9300 ⁺⁰²	1.2339 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.4610 ⁻⁰⁴	7.7118 ⁻⁰¹	0.1268	3.7944 ⁻⁰⁴	6.2220 ⁺⁰²	2.9797 ⁺⁰²		
72010113	2.6169	0.9803	5.7028 ⁺⁰³	1.5257 ⁻⁰³	4.2220	1.4395	2.4216 ⁺⁰⁴	2.4216 ⁺⁰⁴		
4.5669 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.1040 ⁺⁰⁴	NM	1.7956	1.7808	2.9300 ⁺⁰²	1.3420 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.7150 ⁻⁰⁴	7.4629 ⁻⁰¹	0.1263	3.8797 ⁻⁰⁴	6.0781 ⁺⁰²	2.9888 ⁺⁰²		
72010114	2.4661	0.9772	6.7840 ⁺⁰³	1.7262 ⁻⁰³	3.8493	1.4210	3.0603 ⁺⁰⁴	3.0603 ⁺⁰⁴		
4.6939 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2357 ⁺⁰⁴	NM	1.8182	1.8086	2.9300 ⁺⁰²	1.4348 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	2.8041 ⁻⁰⁴	7.7286 ⁻⁰¹	0.1252	3.7717 ⁻⁰⁴	5.9227 ⁺⁰²	2.9985 ⁺⁰²		
72010115	2.5545	0.9790	6.7071 ⁺⁰³	1.8069 ⁻⁰³	3.9027	1.3467	2.6673 ⁺⁰⁴	2.6673 ⁺⁰⁴		
4.8209 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2661 ⁺⁰⁴	NM	1.8399	1.8298	2.9300 ⁺⁰²	1.3796 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	3.0110 ⁻⁰⁴	-4.6879 ⁻⁰¹	0.1280	4.0063 ⁻⁰⁴	6.0157 ⁺⁰²	2.9928 ⁺⁰²		
72010116	2.6504	0.9810	6.3462 ⁺⁰³	1.9101 ⁻⁰³	4.0313	1.3145	2.2995 ⁺⁰⁴	2.2995 ⁺⁰⁴		
4.9479 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2453 ⁺⁰⁴	NM	1.8614	1.8514	2.9300 ⁺⁰²	1.3223 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	3.1183 ⁻⁰⁴	-4.0969 ⁻⁰¹	0.1308	4.0938 ⁻⁰⁴	6.1106 ⁺⁰²	2.9868 ⁺⁰²		
72010117	2.9977	0.9874	5.3645 ⁺⁰³	1.9004 ⁻⁰³	4.6944	1.2617	1.3550 ⁺⁰⁴	1.3550 ⁺⁰⁴		
5.4359 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.2342 ⁺⁰⁴	NM	1.8886	1.8762	2.9300 ⁺⁰²	1.1368 ⁺⁰²		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	3.7357 ⁻⁰⁴	-3.2206 ⁻⁰¹	0.1378	4.9625 ⁻⁰⁴	6.4084 ⁺⁰²	2.9875 ⁺⁰²		
72010118	3.5347	0.9953	4.7450 ⁺⁰³	1.6705 ⁻⁰³	6.0271	1.2326	6.1909 ⁺⁰³	6.1909 ⁺⁰³		
6.4719 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.3282 ⁺⁰⁴	NM	1.8430	1.8337	2.9300 ⁺⁰²	9.0888 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	5.3835 ⁻⁰⁴	-2.4024 ⁻⁰¹	0.1447	7.7625 ⁻⁰⁴	6.7564 ⁺⁰²	2.9438 ⁺⁰²		
72010119	3.6361	0.9966	4.4744 ⁺⁰³	1.6387 ⁻⁰³	6.3213	1.2365	5.3685 ⁺⁰³	5.3685 ⁺⁰³		
6.7259 ⁻⁰¹	4.9600 ⁺⁰⁵	1.0000	1.3032 ⁺⁰⁴	NM	1.8922	1.8710	2.9300 ⁺⁰²	8.7261 ⁺⁰¹		
-2.5400 ⁻⁰¹	3.1800 ⁺⁰²	0.0000	5.5762 ⁻⁰⁴	-2.0772 ⁻⁰¹	0.1457	8.2026 ⁻⁰⁴	6.8101 ⁺⁰²	2.9400 ⁺⁰²		

72010101		LEWIS		PROFILE TABULATION		21 POINTS, DELTA AT POINT 15			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	3.54040	0.00000	
2	3.5326-04	3.4595+00	NM	0.95219	0.37994	0.62700	2.72334	0.23023	
3	4.1041-04	3.4465+00	NM	0.95209	0.37909	0.62600	2.72689	0.22957	
4	6.2341-04	4.6355+00	NM	0.96015	0.45039	0.70300	2.43627	0.28856	
5	8.6238-04	6.1482+00	NM	0.96816	0.52684	0.77200	2.14725	0.35953	
6	1.2780-03	7.5520+00	NM	0.97405	0.58878	0.81900	1.93490	0.42328	
7	1.6988-03	8.7200+00	NM	0.97813	0.63568	0.85000	1.78790	0.47540	
8	2.2079-03	1.0470+01	NM	0.98319	0.70004	0.89700	1.60548	0.55248	
9	2.7170-03	1.2246+01	NM	0.98746	0.76105	0.91700	1.45180	0.63163	
10	3.2157-03	1.4354+01	NM	0.99142	0.82505	0.94400	1.30912	0.72109	
11	3.7812-03	1.6465+01	NM	0.99473	0.88560	0.96600	1.18980	0.81190	
12	4.2911-03	1.8454+01	NM	0.99734	0.93908	0.98300	1.09572	0.89712	
13	4.7431-03	1.9669+01	NM	0.99874	0.97029	0.99200	1.04525	0.94905	
14	5.2678-03	2.0553+01	NM	0.99968	0.99239	0.99800	1.01135	0.98680	
D 15	5.8133-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	6.3224-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
17	6.8990-03	2.0707+01	NM	0.99984	0.99618	0.99900	1.00568	0.99336	
18	7.3926-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
19	7.7458-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
20	8.4160-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
21	8.9563-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD ASSUME P=PD AND VAN DRIEST

72010103		LEWIS		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	3.84040	0.00000	
2	2.2441-04	3.5118+00	NM	0.95259	0.38337	0.63100	2.70940	0.23292	
3	3.5577-04	3.4208+00	NM	0.95189	0.37739	0.62400	2.73399	0.22824	
4	5.1998-04	4.9410+00	NM	0.96194	0.46688	0.71900	2.37166	0.30316	
5	7.9365-04	6.3344+00	NM	0.96902	0.53547	0.77900	2.11642	0.36807	
6	1.3082-03	7.1207+00	NM	0.97431	0.59165	0.82100	1.92559	0.42660	
7	1.7351-03	8.8458+00	NM	0.97853	0.64053	0.85300	1.77347	0.48098	
8	2.2879-03	1.0633+01	NM	0.98361	0.70574	0.89000	1.59034	0.55943	
9	2.8079-03	1.2493+01	NM	0.98789	0.76769	0.92000	1.43615	0.64060	
10	3.2129-03	1.4268+01	NM	0.99127	0.82250	0.94300	1.31448	0.71739	
11	3.8588-03	1.6359+01	NM	0.99458	0.88266	0.96500	1.19529	0.80734	
12	4.4116-03	1.8076+01	NM	0.99688	0.92915	0.98000	1.11244	0.88054	
13	4.8549-03	1.9528+01	NM	0.99859	0.96671	0.99100	1.05088	0.94302	
14	5.3749-03	2.0402+01	NM	0.99953	0.98863	0.99700	1.01701	0.98054	
15	5.8402-03	2.0553+01	NM	0.99968	0.99239	0.99800	1.01135	0.98680	
16	6.3656-03	2.0553+01	NM	0.99968	0.99239	0.99800	1.01135	0.98680	
17	6.8528-03	2.0553+01	NM	0.99968	0.99239	0.99800	1.01135	0.98680	
D 18	7.8051-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD ASSUME P=PD AND VAN DRIEST

72010105		LEWIS		PROFILE TABULATION		18 POINTS, DELTA AT POINT 17			
I	Y	PT2/P	P/PO	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	3.84040	0.00000	
2	1.5075-04	2.5754+00	NM	0.94471	0.31559	0.54600	2.99319	0.18241	
3	3.0191-04	3.4725+00	NM	0.95229	0.38080	0.62800	2.71977	0.23090	
4	4.5226-04	4.2353+00	NM	0.95764	0.42780	0.68000	2.52661	0.26914	
5	7.1218-04	5.5605+00	NM	0.96529	0.49857	0.74800	2.25085	0.33232	
6	1.0189-03	6.3562+00	NM	0.97000	0.54558	0.78700	2.08084	0.37821	
7	1.6323-03	8.3178+00	NM	0.97680	0.61904	0.84000	1.83597	0.45752	
8	2.1417-03	1.0154+01	NM	0.98236	0.68887	0.88100	1.63560	0.53864	
9	2.7335-03	1.2286+01	NM	0.98746	0.76105	0.91700	1.45180	0.63163	
10	3.3010-03	1.4528+01	NM	0.99172	0.83021	0.94600	1.29839	0.72860	
11	3.8572-03	1.6901+01	NM	0.99534	0.89760	0.97000	1.18782	0.83061	
12	4.4550-03	1.8979+01	NM	0.99796	0.95268	0.98700	1.07335	0.91955	
13	4.9177-03	2.0252+01	NM	0.99937	0.98490	0.99600	1.02267	0.97392	
14	5.3986-03	2.0553+01	NM	0.99968	0.99239	0.99800	1.01135	0.98680	
15	6.2224-03	2.0707+01	NM	0.99984	0.99618	0.99900	1.00568	0.99336	
16	6.8555-03	2.0707+01	NM	0.99984	0.99618	0.99900	1.00568	0.99336	
D 17	7.3089-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	7.8599-03	2.0863+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD ASSUME P=PD AND VAN DRIEST

72010106		LEWIS		PROFILE TABULATION			20 POINTS, DELTA AT POINT 15		
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.92138	0.00000	0.00000	3.62862	0.00000	
2	1.5039*-04	2.7897*+00	NM	0.94754	0.34529	0.57400	2.76354	0.20770	
3	2.7652*-04	3.1192*+00	NM	0.95040	0.37043	0.60500	2.66744	0.22681	
4	4.0750*-04	3.8646*+00	NM	0.95617	0.42151	0.66300	2.47406	0.26198	
5	6.5490*-04	5.1396*+00	NM	0.96417	0.49559	0.73600	2.20549	0.33371	
6	9.7508*-04	6.0035*+00	NM	0.96866	0.53998	0.77400	2.05456	0.37672	
7	1.6882*-03	8.1502*+00	NM	0.97752	0.63679	0.84400	1.75669	0.48045	
8	2.1588*-03	9.7450*+00	NM	0.98265	0.70076	0.88200	1.58417	0.55670	
9	2.7506*-03	1.2005*+01	NM	0.98829	0.78081	0.92200	1.39436	0.66123	
10	3.3230*-03	1.4480*+01	NM	0.99313	0.86060	0.95500	1.23143	0.77552	
11	3.9488*-03	1.7145*+01	NM	0.99721	0.93893	0.98200	1.09385	0.89775	
12	4.3854*-03	1.8847*+01	NM	0.99938	0.98570	0.99600	1.02100	0.97551	
13	5.0452*-03	1.9383*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
14	5.5934*-03	1.9522*+01	NM	1.00016	1.00365	1.00100	0.99474	1.00630	
D 15	6.1852*-03	1.9383*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	6.7722*-03	1.9247*+01	NM	0.99984	0.99638	0.99900	1.00526	0.99377	
17	7.3107*-03	1.9383*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	7.8734*-03	1.9383*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
19	8.4604*-03	1.9522*+01	NM	1.00016	1.00365	1.00100	0.99474	1.00630	
20	9.0462*-03	1.9561*+01	NM	1.00031	1.00732	1.00200	0.98947	1.01267	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PD AND VAN DRIEST

72010107		LEWIS		PROFILE TABULATION			19 POINTS, DELTA AT POINT 12		
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.92138	0.00000	0.00000	3.21694	0.00000	
2	1.5377*-04	2.3725*+00	NM	0.94540	0.33656	0.54000	2.57433	0.20976	
3	2.4775*-04	2.9691*+00	NM	0.95121	0.36978	0.60500	2.40919	0.25112	
4	3.3017*-04	3.5074*+00	NM	0.95540	0.43198	0.65200	2.27803	0.28621	
5	4.0344*-04	4.4131*+00	NM	0.96236	0.49389	0.71400	2.08992	0.34164	
6	6.5255*-04	5.1676*+00	NM	0.96770	0.53982	0.75500	1.95609	0.37597	
7	1.5078*-03	6.7808*+00	NM	0.97515	0.62654	0.82200	1.77125	0.47756	
8	2.0888*-03	8.7091*+00	NM	0.98259	0.71634	0.87900	1.50549	0.58379	
9	2.6625*-03	1.1045*+01	NM	0.98952	0.81333	0.92900	1.30465	0.71207	
10	3.2720*-03	1.3501*+01	NM	0.99489	0.90131	0.96600	1.14870	0.84053	
11	3.8273*-03	1.5713*+01	NM	0.99878	0.97487	0.99200	1.03565	0.95804	
D 12	4.4167*-03	1.6509*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
13	4.9655*-03	1.6931*+01	NM	1.00061	1.01307	1.00400	0.98217	1.02223	
14	5.5231*-03	1.6813*+01	NM	1.00015	1.00324	1.00100	0.99555	1.00508	
15	6.0712*-03	1.6509*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	6.6336*-03	1.6509*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
17	7.2231*-03	1.6509*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	7.8083*-03	1.6509*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
19	8.4234*-03	1.6406*+01	NM	0.99985	0.99679	0.99900	1.00445	0.99458	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PD AND VAN DRIEST

72010109		LEWIS		PROFILE TABULATION			18 POINTS, DELTA AT POINT 11		
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.92138	0.00000	0.00000	2.84000	0.00000	
2	1.5058*-04	2.2140*+00	NM	0.94548	0.35046	0.53400	2.32172	0.23000	
3	3.2751*-04	2.8500*+00	NM	0.95272	0.41581	0.61100	2.15921	0.28297	
4	4.6680*-04	3.2132*+00	NM	0.95610	0.44813	0.64600	2.07603	0.31087	
5	7.3408*-04	3.9430*+00	NM	0.96200	0.50630	0.70400	1.93343	0.36412	
6	1.0616*-03	4.7697*+00	NM	0.96786	0.56457	0.75600	1.79512	0.42161	
7	1.5924*-03	6.2493*+00	NM	0.97622	0.65541	0.82600	1.58831	0.52005	
8	2.1759*-03	8.3992*+00	NM	0.98541	0.76863	0.89700	1.36190	0.65864	
9	2.7067*-03	1.0670*+01	NM	0.99259	0.87210	0.94900	1.18414	0.80143	
10	3.2751*-03	1.2935*+01	NM	0.99808	0.96420	0.98700	1.04786	0.94192	
D 11	3.8737*-03	1.3877*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
12	4.4120*-03	1.4109*+01	NM	1.00045	1.00663	1.00300	0.98687	1.01429	
13	4.9993*-03	1.4031*+01	NM	1.00030	1.00574	1.00200	0.99258	1.00944	
14	5.5790*-03	1.3877*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
15	6.1512*-03	1.3881*+01	NM	0.99985	0.99716	0.99900	1.00370	0.99931	
16	6.6444*-03	1.3877*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
17	7.2957*-03	1.3877*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
18	7.8566*-03	1.3877*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PD AND VAN DRIEST

72010111		LEWIS		PROFILE TABULATION		26 POINTS, DELTA AT POINT 15			
I	Y	PT2/P	P/PP	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	2.49357	0.00000	
2	1.5257+04	2.0576+00	NM	0.94663	0.36641	0.52900	2.08440	0.25379	
3	3.1555+04	2.5591+00	NM	0.95282	0.42810	0.60000	1.96436	0.30544	
4	4.9240+04	2.9204+00	NM	0.95669	0.46650	0.64100	1.86661	0.33951	
5	7.0046+04	3.4491+00	NM	0.96171	0.51677	0.69100	1.78796	0.38647	
6	1.0160+03	4.9800+00	NM	0.96694	0.57050	0.74000	1.68248	0.43983	
7	1.1547+03	4.8702+00	NM	0.97261	0.63103	0.79000	1.56729	0.50405	
8	1.6540+03	5.7893+00	NM	0.97824	0.69460	0.83700	1.45204	0.57643	
9	1.9488+03	6.8563+00	NM	0.98377	0.76163	0.88100	1.33802	0.65644	
10	2.2297+03	7.8952+00	NM	0.98835	0.82157	0.91600	1.24310	0.73687	
11	2.5036+03	8.9230+00	NM	0.99227	0.87680	0.94500	1.16161	0.81353	
12	2.7567+03	9.7866+00	NM	0.99517	0.92063	0.96600	1.10100	0.87739	
13	3.0688+03	1.0774+01	NM	0.99799	0.96592	0.98600	1.04201	0.94624	
14	3.3254+03	1.1135+01	NM	0.99914	0.98513	0.99400	1.01808	0.97635	
D 15	3.6237+03	1.1459+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	3.9253+03	1.1514+01	NM	1.00014	1.00252	1.00100	0.99698	1.00404	
17	4.2305+03	1.1404+01	NM	0.99986	0.99749	0.99900	1.00302	0.99599	
18	4.4906+03	1.1295+01	NM	0.99957	0.99252	0.99700	1.00905	0.98805	
19	4.7610+03	1.1241+01	NM	0.99942	0.99005	0.99600	1.01207	0.98413	
20	5.0835+03	1.1295+01	NM	0.99957	0.99252	0.99700	1.00905	0.98805	
21	5.7285+03	1.1295+01	NM	0.99957	0.99252	0.99700	1.00905	0.98805	
22	6.2764+03	1.1295+01	NM	0.99957	0.99252	0.99700	1.00905	0.98805	
23	6.8416+03	1.1295+01	NM	0.99957	0.99252	0.99700	1.00905	0.98805	
24	7.4311+03	1.1188+01	NM	0.99928	0.98754	0.99500	1.01507	0.98022	
25	7.9790+03	1.0926+01	NM	0.99856	0.97544	0.99000	1.03007	0.96110	
26	8.5268+03	1.0774+01	NM	0.99814	0.96828	0.98700	1.03903	0.94992	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PPD AND VAN DRIEST

72010113		LEWIS		PROFILE TABULATION		22 POINTS, DELTA AT POINT 12			
I	Y	PT2/P	P/PPD	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	2.18334	0.00000	
2	1.5406+04	2.3181+00	NM	0.95368	0.44660	0.59500	1.77498	0.33522	
3	2.9686+04	2.8579+00	NM	0.96017	0.51360	0.66400	1.67139	0.39727	
4	4.2086+04	3.2084+00	NM	0.96379	0.55121	0.70000	1.61271	0.43405	
5	6.1166+04	3.8471+00	NM	0.96983	0.61517	0.75700	1.51329	0.50023	
6	1.0146+03	4.2488+00	NM	0.97318	0.65182	0.78700	1.45777	0.53987	
7	1.6233+03	5.3803+00	NM	0.98127	0.74458	0.85600	1.32167	0.64767	
8	2.1757+03	6.6572+00	NM	0.98864	0.83666	0.91500	1.19603	0.76503	
9	2.7393+03	7.9993+00	NM	0.99495	0.92344	0.96300	1.08751	0.88551	
10	3.3143+03	8.8810+00	NM	0.99848	0.97621	0.98900	1.02637	0.96359	
11	3.8967+03	9.2559+00	NM	0.99986	0.99780	0.99900	1.00241	0.98660	
D 12	4.4453+03	9.2946+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
13	5.0127+03	9.2946+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
14	5.5914+03	9.2946+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
15	6.2114+03	9.2946+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
16	6.7488+03	9.2174+00	NM	0.99972	0.99561	0.99800	1.00482	0.99322	
17	7.3575+03	9.1792+00	NM	0.99958	0.99342	0.99700	1.00722	0.98985	
18	7.8648+03	9.0657+00	NM	0.99945	0.98691	0.99400	1.01442	0.97987	
19	8.4585+03	8.9912+00	NM	0.99889	0.98261	0.99200	1.01921	0.97331	
20	9.0147+03	8.8447+00	NM	0.99834	0.97410	0.98800	1.02875	0.96039	
21	9.5407+03	8.7369+00	NM	0.99793	0.96779	0.98500	1.03588	0.95088	
22	1.0172+02	8.5268+00	NM	0.99711	0.95537	0.97900	1.05068	0.93231	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PPD AND VAN DRIEST

72010114		LEWIS		PROFILE TABULATION		21 POINTS, DELTA AT POINT 10			
I	Y	PT2/P	P/PPD	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.92138	0.00000	0.00000	2.04204	0.00000	
2	1.8590+04	2.7872+00	NM	0.96183	0.53634	0.67400	1.57918	0.42680	
3	3.9713+04	3.2086+00	NM	0.96648	0.58584	0.72000	1.51150	0.47635	
4	7.0958+04	3.7702+00	NM	0.97283	0.64571	0.77200	1.42942	0.54008	
5	1.0225+03	4.1819+00	NM	0.97560	0.68541	0.80400	1.37599	0.58431	
6	1.6055+03	4.9293+00	NM	0.98141	0.75248	0.85400	1.28803	0.66303	
7	2.1147+03	5.8865+00	NM	0.98775	0.83026	0.90600	1.19077	0.76085	
8	2.6829+03	6.9345+00	NM	0.99362	0.90777	0.95200	1.09482	0.86560	
9	3.2448+03	7.7850+00	NM	0.99771	0.96580	0.98300	1.03593	0.94891	
D 10	3.8532+03	8.3099+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
11	4.4574+03	8.2777+00	NM	0.99986	0.99794	0.99900	1.00213	0.99888	
12	4.9982+03	8.2457+00	NM	0.99973	0.99588	0.99800	1.00426	0.99377	
13	5.5686+03	8.0881+00	NM	0.99905	0.98570	0.99300	1.01487	0.97845	
14	6.1094+03	8.0571+00	NM	0.99892	0.98368	0.99200	1.01699	0.97543	
15	6.7009+03	7.9650+00	NM	0.99851	0.97767	0.98900	1.02332	0.96646	
16	7.2755+03	7.8743+00	NM	0.99811	0.97171	0.98600	1.02963	0.95762	
17	7.8386+03	7.8106+00	NM	0.99784	0.96777	0.98400	1.03383	0.95180	
18	8.3402+03	7.7850+00	NM	0.99771	0.96580	0.98300	1.03593	0.94891	
19	9.0120+03	7.7262+00	NM	0.99744	0.96190	0.98100	1.04011	0.94317	
20	9.5782+03	7.6680+00	NM	0.99718	0.95801	0.97900	1.04429	0.93748	
21	1.0153+02	7.6104+00	NM	0.99691	0.95416	0.97700	1.04846	0.93184	

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PPD AND VAN DRIEST

72010115 LEWIS

PROFILE TABULATION

23 POINTS, DELTA AT POINT 14

I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TO	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	IM	0.92138	0.00000	0.00000	2.12388	0.00000
2	1.5417-04	2.8037+00	IM	0.96055	0.51975	0.66500	1.63700	0.40623
3	2.0708-04	3.0954+00	IM	0.96374	0.55319	0.69700	1.58749	0.43906
4	4.3061-04	3.7938+00	IM	0.97050	0.62527	0.76100	1.48129	0.51374
5	7.1769-04	4.4116+00	IM	0.97566	0.68227	0.80700	1.39404	0.57643
6	9.8350-04	4.5979+00	IM	0.97704	0.69800	0.81900	1.37677	0.59487
7	1.2918-03	4.8796+00	IM	0.97915	0.72232	0.83700	1.34273	0.62536
8	1.8394-03	5.5673+00	IM	0.98373	0.77693	0.87500	1.26838	0.68985
9	2.3923-03	6.3915+00	IM	0.98861	0.83837	0.91400	1.18857	0.76899
10	2.9452-03	7.1937+00	IM	0.99275	0.89372	0.96000	1.12043	0.84432
11	3.5831-03	8.0709+00	IM	0.99673	0.95051	0.97000	1.05436	0.92568
12	4.1094-03	8.5299+00	IM	0.99863	0.97890	0.99000	1.02282	0.96792
13	4.8464-03	8.8084+00	IM	0.99973	0.99572	0.99800	1.00456	0.99345
D 14	5.3003-03	8.8800+00	IM	1.00000	1.00000	1.00000	1.00000	1.00000
15	5.9276-03	8.8800+00	IM	1.00000	1.00000	1.00000	1.00000	1.00000
16	6.4433-03	8.8441+00	IM	0.99986	0.99786	0.99900	1.00229	0.99672
17	7.0068-03	8.7041+00	IM	0.99986	0.99786	0.99900	1.00229	0.99672
18	7.5543-03	8.7729+00	IM	0.99959	0.99359	0.99700	1.00687	0.99020
19	8.1179-03	8.7729+00	IM	0.99959	0.99359	0.99700	1.00687	0.99020
20	8.7186-03	8.7025+00	IM	0.99931	0.98936	0.99500	1.01144	0.98375
21	9.1709-03	8.5984+00	IM	0.99890	0.98306	0.99200	1.01627	0.97420
22	9.8297-03	8.5299+00	IM	0.99863	0.97890	0.99000	1.02202	0.96792
23	1.0420-02	8.4286+00	IM	0.99822	0.97270	0.98700	1.02961	0.95861

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PD AND V=V DRIEST

72010119 LEWIS

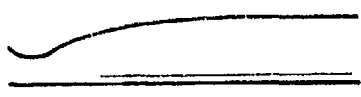
PROFILE TABULATION

32 POINTS, DELTA AT POINT 23

I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TO	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	IM	0.92138	0.00000	0.00000	3.35775	0.00000
2	1.6122-04	2.9892+00	IM	0.95063	0.34028	0.60200	2.50604	0.24022
3	3.0454-04	3.5554+00	IM	0.95332	0.42274	0.65000	2.36421	0.27493
4	4.6976-04	4.6801+00	IM	0.96311	0.49567	0.72300	2.12759	0.33982
5	7.7930-04	6.1649+00	IM	0.97122	0.57752	0.79200	1.88071	0.42112
6	1.0032-03	6.9061+00	IM	0.97458	0.61422	0.81900	1.77797	0.46064
7	1.7914-03	8.1989+00	IM	0.97961	0.67339	0.85800	1.62346	0.52850
8	2.7229-03	9.5644+00	IM	0.98410	0.73065	0.89100	1.48709	0.59916
9	3.5469-03	1.0822+01	IM	0.98759	0.77965	0.91600	1.38035	0.66360
10	4.4426-03	1.1512+01	IM	0.98930	0.80527	0.92800	1.32606	0.69876
11	5.3562-03	1.2269+01	IM	0.99103	0.83245	0.94000	1.27509	0.73720
12	6.1445-03	1.2816+01	IM	0.99219	0.85154	0.94800	1.23940	0.76489
13	7.0581-03	1.3325+01	IM	0.99322	0.86893	0.95500	1.20792	0.79062
14	7.9179-03	1.3786+01	IM	0.99411	0.88439	0.96100	1.18075	0.81349
15	8.7420-03	1.4189+01	IM	0.99489	0.89769	0.96600	1.15798	0.83421
16	9.6018-03	1.4697+01	IM	0.99574	0.91418	0.97200	1.13500	0.85980
17	1.0408-02	1.5142+01	IM	0.99650	0.92839	0.97700	1.10747	0.88219
18	1.1304-02	1.5609+01	IM	0.99725	0.94305	0.98200	1.08432	0.90564
19	1.2164-02	1.5999+01	IM	0.99786	0.95512	0.98600	1.06571	0.92520
20	1.3059-02	1.6404+01	IM	0.99847	0.96751	0.99000	1.04701	0.94553
21	1.3973-02	1.6719+01	IM	0.99893	0.97702	0.99300	1.03297	0.96130
22	1.4833-02	1.7245+01	IM	0.99969	0.99332	0.99800	1.00944	0.98866
D 23	1.5531-02	1.7492+01	IM	1.00000	1.00000	1.00000	1.00000	1.00000
24	1.6517-02	1.7723+01	IM	1.00031	1.00078	1.00200	0.99054	1.01157
25	1.7412-02	1.8079+01	IM	1.00077	1.01712	1.00500	0.97631	1.02939
26	1.8093-02	1.8323+01	IM	1.00108	1.02415	1.00700	0.96679	1.04159
27	1.9186-02	1.8447+01	IM	1.00124	1.02779	1.00800	0.96203	1.04778
28	1.9956-02	1.9221+01	IM	1.00217	1.04458	1.01400	0.93336	1.08640
29	2.0726-02	1.9996+01	IM	1.00295	1.06859	1.01900	0.90933	1.12060
30	2.1658-02	2.0935+01	IM	1.00406	1.09653	1.02600	0.87550	1.17191
31	2.2392-02	2.2055+01	IM	1.00517	1.12014	1.03300	0.84143	1.22767
32	2.3843-02	2.2741+01	IM	1.00580	1.14386	1.03700	0.82186	1.26178

INPUT VARIABLES Y/DELTA,U/UD

ASSUME P=PD AND V=V DRIEST

	M : 4.9 R THETA X 10 ⁻³ : 7 - 58. TW/TR : 1.0, 0.8, 0.25.	7202
		ZPG AW - MHT - SHT
Boundary-layer channel. Effectively continuous. W = 0.33 H = 0.272 m. 0.1 < PO < 1.1 MN/m ² . 320 < TO < 451 K. Air, dew point 215-233 K. 1.7 < RE/m X 10 ⁻⁶ < 25.		
VOISINET R.L.P. and LEE R.E., 1972. Measurements of a Mach 4.9 zero-pressure-gradient turbulent boundary-layer with heat transfer. Part I-Data compilation. NOL TR 72-232. And Voisinnet R.L.P., private communications, Lee et al (1966). Also Lee, Yanta and Leonas (1968) (1969), Gates (1973) (CAT 7301)		

- 1 The test boundary layer was formed on a flat copper surface opposite the flexible half-nozzle. The plate was 2.69 m long and extended upstream of the nozzle throat (X = 0). The plate increased in width from 305 mm at the throat to 343 mm at the channel exit. The nozzle contours are presented in table 1 of section A and the height of the parallel section, as operated, was 272 mm. The plate could be actively cooled with water or liquid nitrogen, and the specification called for a surface finish with roughness below 0.8 μm r.m.s. and waviness less than 5×10^{-3} m/m. The zero pressure gradient region started at X = 1.397 m and instrumentation could be attached to or inserted through five removable ports downstream of this point. (A full description of the basic facility is given by Lee et al., 1966). Axial Pitot surveys
- 2 showed the flow to be shock free with less than 1 % variation of Mach number in the test zone. In a central region along the test plate, about 150 mm wide, the flow did not exhibit any effects due to cross-flow.
- 3 Skin friction coefficients measured at a point 0.254 m downstream of the nozzle throat were very close to turbulent values at high PO. Low pressure tests (PO = 0.05 MN/m² - PC) gave data which appeared to deviate from turbulent flow prediction. The authors therefore present only data for PO = 0.1 MN/m² or above, which is believed to represent fully turbulent flow. The test boundary layer passed through the strong reflected-wave expansion of the nozzle, the pressure distribution being given in table 2 of section A. The wall temperature histories are given in table 3 of section A. Substantial heat-transfer from the flow occurred in the nozzle region.
- 4
- 5
- 6 Measurements were made at the five instrumentation ports centred on X = 1.524, 1.778, 1.981, 2.134, 2.286 m.
- 7 Skin friction and heat flux measurements were made at these stations while traverses were made 76.2 mm upstream. The relative positions of the various measurements, taking a local zero on the centre line at the X-value of the Pitot-probe tip are:

	PT2	TAUW	0	PW (a)	PW (b,c)	TW	TO
X :	0	+ 76.2	+ 76.2	0	76.2	0 (E)	0 mm
Z :	+ 12.7	0	0	0	\pm 76.2	- 50.8 (E)	- 12.7 mm

The static hole diameter was 0.79 mm, and wall temperature was measured by thermocouples attached to the underside of the copper plate. Temperature differences over the thickness of the plate were less than 1^oK. Wall shear stress was measured using two FEB. For the AW and some MHT tests a Kistler balance (model 322 M 107) was used (Paros 1970). For the SHT and some MHT tests, a NOL design intended to operate in strongly cooled-wall and pressure-gradient conditions was employed. This was a modification of the design of Bruno et al. (1969). The floating element cooling system did not function, so that the temperature of the element was higher than that of the surrounding wall. In the SHT case, this difference could be as much as 100^oK which, the authors suggest, could result in the balance recording a value as much as 20 % below the true wall stress. The heat-flux was measured with a thermo-pile gauge attached to the centre of each port, using the manufacturers calibration. (RdF Corp. Hudson, New Hampshire, Model 20463-3.)

- 7 Pitot, TO and P profiles were measured, however only Pitot and TO results, measured simultaneously, are presented (but see § 9 below). Two TTP were used, one an ECP (Danberg 1961) for which $\alpha = 5^{\circ}$, d = 1.27, l = 12.7 mm, and the other an FWP (Yanta, 1970) with a chromel / alumel junction, for which d = 0.0254, b = 3.66, l = 20 (E) mm. The TPP was an FPP for which $h_1 = 0.127$, $h_2 = 0.076$, $b_1 = 2.54$, l = 20 (E) mm.

- 9 Any small differences in Y between the TTP and the TPP were eliminated by the authors who normalised the TO data to the Y values of the PT2 probe. The values for Y less than 0.635 mm were obtained by extrapolating the profile to meet the wall temperature. The static pressure distribution presented is an interpolation giving zero normal pressure gradient at the wall, agreeing with the measured value of PW, and with the values and trend of the static pressure in the free stream as determined from PT2 and the tunnel reservoir pressure (Voisin et al. 1971). Substantial pressure variation is only observed at the first station, where the profile normal in the outer part of the boundary layer intercepts the last part of the nozzle expansion, here reflected as a simple wave. Corrections were applied to the Pitot data for viscous and molecular effects, and also for probe-wall interference. Both corrections were based on calibration experiments.
- 10 (Source, Appendix A). Sutherland's viscosity relation was used.
- 11 The editors have accepted the interpolations and corrections made by the authors. The edge reservoir state has been calculated from the static pressure and temperature data with the Mach number distribution as presented. The authors present their wall shear stress and heat transfer data as measured on separate occasions at the centre of the ports - that is, 76.2 mm downstream of the profiles. The wall temperature histories for these runs were not exactly as for the profile measurements. The CF and CQ values presented with the profiles have been interpolated by the editors on the basis of the author's R THETA values alone. No adjustment has been made for the small X-difference, introducing a systematic error which is, however, very small as compared to the scatter of the data. Following the author's stated preference, the CF values presented for the MHT case are those measured with the NOL balance where possible. For the AW and SHT, data is only available from the Kistler and NOL balances respectively. Where comparison is possible, the Kistler balance appears to read systematically about 3 % higher. (Skin friction values for profiles 0601, 0701, 0801, 0901 and 1001 were measured with a Kistler balance. The authors state that the two balances agreed to within 5 % in comparative measurements.) We present revised data for profile 1201 (private communication).
- 12 The profile sets presented are distinguished by total pressure (Reynolds number), by the heat transfer on the experimental wall, and by the TTP used. The data sets are:

CODE 7202	HT	NX	TTP	FEB	POD ₂ MN/m ²	TOD K	TW K
0101-5	AW	5	ECP	Kistler	0.1	355	300
0201-5	AW	5	ECP	Kistler	0.5	355	295
0301-5	AW	5	ECP	Kistler	1.0	355	295
0401-4	AW	4	FWP	Kistler	0.1	355	295
0501-5	AW	5	FWP	Kistler	0.5	350	295
0601-5	MHT	5	ECP	NOL	0.1	415	300
0701-5	MHT	5	ECP	NOL	0.5	415	300
0801-5	MHT	5	ECP	NOL	1.0	415	300
0901-5	MHT	5	FWP	NOL	0.1	425	295
1001-5	MHT	5	FWP	NOL	0.5	420	295
1101-3	SHT	3	ECP	NOL	0.1	425	85
1201-3	SHT	3	ECP	NOL	0.5	425	90
1301-3	SHT	3	ECP	NOL	1.0	425	100
1401-2	SHT	2	FWP	NOL	0.1	425	85
1501-2	SHT	2	FWP	NOL	0.5	425	90

- § Data: 7202 0101-1502. Pitot and TO profiles simultaneously. NX = 2 to 5. CF from FEB, CQ from thermopiles, measured separately and with slightly different thermal histories.

15 Editors' comments

This entry describes the ZPG case which forms part of a comprehensive study using the same facility and the same instrumentation. The FPG case is described in CAT 7304, and the APG case in Voisin et al. 1971. Taken together, the three data-sets cover a very wide range of systematically varied governing parameters. They provide the only fully documented case with a wide range of TW/TR values. These data supersede the earlier comparable tests in the same facility reported by Lee et al. (1968, 1969 - ZPG), Brott et al. (1969, 1970 - FPG). Tabular data for the APG (1971) case are not at present available.

In many cases substantial heat transfer took place in the nozzle region, so that there is a downstream heat-transfer history effect in addition to any downstream effect of the nozzle pressure-gradient. Thus, in the AW case, the zero-heat-transfer wall temperature is the TW value given in section B or table 3, and was determined by adjusting the wall cooling rate so as to have no measurable heat flux at the

measuring ports. This adiabatic wall temperature, TAW, differs noticeably from the "flat plate recovery temperature" TR. Further tests to assess the effect of upstream heat transfer are reported by Gates (CAT 7301). On a transformed wall-law plot many of the profiles show inner region characteristics which could be described as transitional.

Static pressure variations normal to the test surface were generally small, except for the first station, where the profile normal extends into the last, simple wave, part of the nozzle expansion. The reduced data of section B have been prepared both with a fixed reference state (the D-state) and also with a varying pressure-based reference state, the tables for which follow the normal section B.

There are no truly comparable experiments, but the same Mach number and Reynolds number ranges are covered in part for the adiabatic wall case by Gates (CAT 7301), Allen (CAT 7303) and Mabey et al. (CAT 7402), with various geometries.

TABLE 1
NOZZLE CONTOUR COORDINATES

x (m)	y (m)
0.0000	0.01077
0.2794	0.02959
0.3810	0.04598
0.5588	0.08738
0.7366	0.12970
0.9144	0.16475
1.0668	0.18952
1.2446	0.21296
1.4224	0.23107
1.6002	0.24485
1.7780	0.25518
1.9558	0.26264
2.1591	0.26838
2.3368	0.27162

TABLE 2
NOZZLE WALL PRESSURE DISTRIBUTION

x (meters)	$P_{sw}/P_o \times 10^3$	
	Design	Experiment
0.000	528.30	-
0.127	194.04	-
0.257	70.02	-
0.385	29.24	-
0.559	11.47	10.68
0.635	8.25	8.00
0.711	6.22	6.04
0.787	5.22	4.68
0.864	3.97	3.95
0.940	3.32	3.44
1.067	2.66	2.67
1.143	2.41	2.43
1.194	2.31	2.29
1.270	2.20	2.10
1.448	2.12	1.99
1.524	2.12	1.99
1.702	2.12	2.04
1.778	2.12	2.09
1.905	2.12	2.04
1.981	2.12	2.02
2.057	2.12	2.03
2.134	2.12	2.05
2.210	2.12	2.11
2.286	2.12	2.14

TABLE 3
NOZZLE WALL TEMPERATURE DISTRIBUTION

CAT 7202 SERIES	Code	P_o atm	T_o °K	x (meters)												
				0.000	0.279	0.467	0.711	0.864	1.067	1.194	1.448	1.702	1.905	2.057	2.210	
				Average T_w (°K)												
03	ZPG-AH	T01	10.	307.	306.	303.	297.	297.	297.	297.	297.	297.	297.	297.	297.	297.
02		T02	5.	348.	296.	297.	299.	298.	298.	298.	298.	298.	298.	298.	298.	298.
01		T03	1.	348.	278.	283.	294.	298.	298.	298.	298.	298.	298.	298.	298.	298.
06		T04	5.	348.	300.	294.	294.	296.	296.	296.	296.	296.	296.	296.	296.	296.
04		T05	1.	348.	281.	284.	290.	296.	296.	296.	296.	296.	296.	296.	296.	296.
08	ZPG-MHT	T06	10.	423.	338.	300.	298.	298.	298.	298.	-	-	-	300.	299.	299.
07		T07	5.	423.	327.	301.	299.	299.	299.	299.	297.	-	-	302.	301.	301.
06		T08	1.	423.	288.	301.	299.	299.	299.	299.	299.	299.	300.	301.	301.	301.
10		T09	5.	423.	342.	333.	319.	300.	299.	299.	299.	299.	299.	299.	299.	299.
09		T010	1.	423.	300.	302.	303.	299.	299.	298.	299.	299.	299.	299.	299.	299.
13	ZPG-CW	T011	10.	423.	332.	311.	288.	178.	124.	97.	-	87.	91.	91.	97.	-
12,18		T012	5.	423.	320.	-	275.	142.	94.	88.	-	86.	86.	87.	89.	-
11,14		T013	1.	423.	28.	287.	160.	88.	85.	84.	-	84.	84.	85.	85.	-

CAT 7202		VOISINET		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.				
RUN X RZ	MD * POD TOD	TH/TR PH/PD SN * D2	RED2W RED2D	CF * CQ * PI2	H12 H32 H42	H12K H32K D2K	PH* TW* UD	PD* TD* TR
72020101 1.4480"+00 INFINITE	4.7553 1.0124"+05 3.5431"+02	0.9249 0.9133 0.0000	1.5563"+03 6.2612"+03 2.7169"-03	8.9000"-04 NM 0.0000"+00	9.1155 1.8320 0.6266	1.4493 1.7768 5.6121"-03	2.3360"+02 2.9980"+02 7.6368"+02	2.5577"+02 6.4157"+01 3.2418"+02
72020102 1.7020"+00 INFINITE	4.7662 1.0068"+05 3.5247"+02	0.9211 0.9942 0.0000	1.7524"+03 7.0625"+03 3.0735"-03	8.7000"-04 NM 0.0000"+00	8.1573 1.8135 0.5728	1.4693 1.7583 6.3059"-03	2.4960"+02 2.9700"+02 7.6201"+02	2.5105"+02 6.3585"+01 3.2243"+02
72020103 1.9050"+00 INFINITE	4.7879 1.0132"+05 3.5745"+02	0.9250 0.9918 0.0000	1.7791"+03 7.2225"+03 3.2230"-03	8.4000"-04 NM 0.0000"+00	8.4273 1.8163 0.5428	1.4528 1.7614 6.6964"-03	2.4410"+02 3.0240"+02 7.6800"+02	2.4613"+02 6.4004"+01 3.2693"+02
72020104 2.0570"+00 INFINITE	4.7910 1.0196"+05 3.5709"+02	0.9124 1.0318 0.0000	1.9555"+03 7.8659"+03 3.4881"-03	8.3000"-04 NM 0.0000"+00	8.0701 1.7496 0.5182	1.4732 1.7476 7.2663"-03	2.5460"+02 2.9800"+02 7.6770"+02	2.4676"+02 6.3872"+01 3.2860"+02
72020105 2.2100"+00 INFINITE	4.8041 1.0355"+05 3.5321"+02	0.9195 1.0219 0.0000	2.1045"+03 8.5751"+03 3.7060"-03	8.2000"-04 NM 0.0000"+00	8.0043 1.8005 0.5382	1.4545 1.7496 7.7278"-03	2.5210"+02 2.4700"+02 7.6368"+02	2.4671"+02 6.2894"+01 3.2301"+02
72020201 1.4480"+00 INFINITE	4.7804 4.8745"+05 3.5370"+02	0.9149 0.9036 0.0000	5.1742"+03 2.0828"+04 1.8947"-03	7.2000"-04 NM 0.0000"+00	9.8440 1.8442 0.5249	1.3470 1.7939 3.9409"-03	1.0820"+03 2.9600"+02 7.6374"+02	1.1949"+03 6.3496"+01 3.2352"+02
72020202 1.7020"+00 INFINITE	4.8117 4.9190"+05 3.5130"+02	0.9204 0.9971 0.0000	5.9030"+03 2.4164"+04 2.1885"-03	6.5500"-04 NM 0.0000"+00	8.5729 1.8250 0.4935	1.3910 1.7722 4.4849"-03	1.1580"+03 2.9570"+02 7.6204"+02	1.1614"+03 6.2393"+01 3.2125"+02
72020203 1.9050"+00 INFINITE	4.8546 5.1780"+05 3.5554"+02	0.9079 1.0082 0.0000	6.6989"+03 2.7453"+04 2.4942"-03	6.4000"-04 NM 0.0000"+00	8.3388 1.8211 0.5140	1.3870 1.7690 5.0172"-03	1.1710"+03 2.9510"+02 7.6782"+02	1.1615"+03 6.2829"+01 3.2503"+02
72020204 2.0570"+00 INFINITE	4.8092 5.1439"+05 3.5459"+02	0.9153 0.9696 0.0000	6.0013"+03 2.7638"+04 2.4246"-03	6.3000"-04 NM 0.0000"+00	9.1178 1.8136 0.4767	1.4059 1.7424 5.2234"-03	1.1810"+03 2.9680"+02 7.6553"+02	1.2181"+03 6.3031"+01 3.2427"+02
72020205 2.2100"+00 INFINITE	4.8232 5.0521"+05 3.5248"+02	0.9277 1.0132 0.0000	6.9625"+03 2.8764"+04 2.5631"-03	6.2000"-04 NM 0.0000"+00	8.6262 1.8075 0.4474	1.3975 1.7587 5.4606"-03	1.1920"+03 2.9900"+02 7.6364"+02	1.1765"+03 6.2357"+01 3.2231"+02
72020301 1.4480"+00 INFINITE	4.8042 1.0057"+06 3.5617"+02	0.9272 0.9291 0.0000	9.5304"+03 3.9008"+04 1.7578"-03	6.3000"-04 NM 0.0000"+00	10.1926 1.8496 0.4137	1.3118 1.8038 3.6081"-03	2.2260"+03 3.0200"+02 7.6709"+02	2.3958"+03 6.3420"+01 3.2573"+02
72020302 1.7020"+00 INFINITE	4.8160 9.9751"+05 3.5115"+02	0.9165 1.0000 0.0000	1.1919"+04 4.8707"+04 2.1782"-03	5.7000"-04 NM 0.0000"+00	8.3082 1.8423 0.5042	1.3382 1.7907 4.2405"-03	2.3430"+03 2.9430"+02 7.6199"+02	2.3430"+03 6.2274"+01 3.2111"+02
72020303 1.9050"+00 INFINITE	4.8645 1.0796"+06 3.5550"+02	0.9124 0.9451 0.0000	1.0371"+04 4.2808"+04 1.8437"-03	5.8000"-04 NM 0.0000"+00	10.0107 1.8266 0.4713	1.3489 1.7808 3.9889"-03	2.2620"+03 2.9650"+02 7.6805"+02	2.3934"+03 6.2012"+01 3.2497"+02
72020304 2.0570"+00 INFINITE	4.8200 1.0390"+06 3.5881"+02	0.9207 0.9391 0.0000	1.1506"+04 4.7013"+04 2.0892"-03	5.6500"-04 NM 0.0000"+00	10.0475 1.8262 0.5009	1.3579 1.7781 4.5131"-03	2.2810"+03 3.0210"+02 7.7038"+02	2.4288"+03 6.3546"+01 3.2811"+02
72020305 2.2100"+00 INFINITE	4.8016 1.0022"+06 3.4942"+02	0.9131 1.0000 0.0000	1.3252"+04 5.3799"+04 2.3608"-03	5.5500"-04 NM 0.0000"+00	8.5063 1.8196 0.4671	1.3745 1.7707 4.8934"-03	2.3950"+03 2.9180"+02 7.5971"+02	2.3950"+03 6.2273"+01 3.1956"+02

CAT 7202		VOISINET		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN X * RZ	MD * P00 TOD	TH/TR PW/PD SH *	PE02W RED2D O2	CF * CQ * PI2	H12 H32 H42	H12K H32K D2K	PW* TW* UD	PD* TD* TR			
72020401 1.4480"+00 INFINITE	4.7417 1.0268"+05 3.5361"+02	0.9118 0.8934 0.0000	1.6627"+03 6.5885"+03 2.7921"-03	8.8000"-04 NM 0.0000"+00	8.7507 1.8368 0.7551	1.4401 1.7798 5.6349"-03	2.3560"+02 2.9500"+02 7.6252"+02	2.6371"+02 6.4330"+01 3.2352"+02			
72020402 1.9050"+00 INFINITE	4.7889 1.0194"+05 3.5321"+02	0.9092 0.9869 0.0000	1.9554"+03 7.8576"+03 3.4246"-03	8.2000"-04 NM 0.0000"+00	7.9236 1.8172 0.6440	1.4601 1.7618 6.8993"-03	2.4410"+02 2.9370"+02 7.6345"+02	2.4735"+02 6.3222"+01 3.2305"+02			
72020403 2.0570"+00 INFINITE	4.8253 1.0526"+05 3.5491"+02	0.9066 1.0000 0.0000	2.1020"+03 5.5238"+03 3.6870"-03	8.1000"-04 NM 0.0000"+00	7.6275 1.8143 0.6627	1.4562 1.7584 7.4124"-03	2.4450"+02 2.9420"+02 7.6632"+02	2.4450"+02 6.2741"+01 3.2452"+02			
72020404 2.2100"+00 INFINITE	4.7951 1.0274"+05 3.5228"+02	0.9045 0.9849 0.0000	2.0581"+03 8.2597"+03 3.5683"-03	8.1500"-04 NM 0.0000"+00	8.1837 1.8054 0.6128	1.4656 1.7516 7.4723"-03	2.4370"+02 2.9140"+02 7.6262"+02	2.4743"+02 6.2922"+01 3.2218"+02			
72020501 1.4480"+00 INFINITE	4.8684 3.2136"+05 3.4843"+02	0.9278 0.9231 0.0000	5.0612"+03 2.1289"+04 1.8455"-03	7.2000"-04 NM 0.0000"+00	10.2367 1.8481 0.5250	1.3482 1.7972 3.8644"-03	1.0620"+03 2.9550"+02 7.6048"+02	1.1505"+03 6.0499"+01 3.1850"+02			
72020502 1.7020"+00 INFINITE	4.8770 5.1342"+05 3.4659"+02	0.9258 0.9711 0.0000	5.4531"+03 2.4681"+04 2.1641"-03	6.5000"-04 NM 0.0000"+00	9.4066 1.8292 0.4862	1.3896 1.7731 4.6129"-03	1.0890"+03 2.9330"+02 7.5870"+02	1.1215"+03 6.0202"+01 3.1680"+02			
72020503 1.9050"+00 INFINITE	4.8610 4.9664"+05 3.5009"+02	0.9246 0.9940 0.0000	5.9597"+03 2.4912"+04 2.2754"-03	6.5000"-04 NM 0.0000"+00	9.2694 1.8226 0.4312	1.3945 1.7701 4.8749"-03	1.0990"+03 2.9590"+02 7.6208"+02	1.1056"+03 6.1141"+01 3.2004"+02			
72020504 2.0570"+00 INFINITE	4.8902 5.1664"+05 3.5016"+02	0.9224 0.9820 0.0000	6.4075"+03 2.6997"+04 2.4039"-03	6.3500"-04 NM 0.0000"+00	9.3105 1.8251 0.4797	1.3837 1.7723 5.1813"-03	1.0910"+03 2.9520"+02 7.6295"+02	1.1110"+03 6.0551"+01 3.2004"+02			
72020505 2.2100"+00 INFINITE	4.9018 5.2275"+05 3.5056"+02	0.9248 1.0002 0.0000	6.6369"+03 2.8122"+04 2.4927"-03	6.1500"-04 NM 0.0000"+00	9.1184 1.8206 0.4512	1.3866 1.7685 5.3806"-03	1.1090"+03 2.9630"+02 7.6370"+02	1.1088"+03 6.0383"+01 3.2038"+02			
72020601 1.4480"+00 INFINITE	4.7747 1.0027"+05 4.1512"+02	0.7845 0.9436 0.0000	1.8649"+03 6.8159"+03 3.5977"-03	1.0550"-03 7.0100"-04 0.0000"+00	6.8257 1.8247 0.8668	1.4442 1.7733 6.5603"-03	2.3350"+02 2.9790"+02 8.2722"+02	2.4746"+02 6.4667"+01 3.7971"+02			
72020602 1.7020"+00 INFINITE	4.8182 1.0229"+05 4.1260"+02	0.7888 0.9965 0.0000	1.9743"+03 6.9301"+03 3.8539"-03	1.0350"-03 6.7800"-05 0.0000"+00	6.3306 1.8152 0.8434	1.4471 1.7628 6.9861"-03	2.3880"+02 2.9760"+02 8.2604"+02	2.3964"+02 7.3117"+01 3.7729"+02			
72020603 1.9050"+00 INFINITE	4.8303 1.0348"+05 4.1738"+02	0.7939 0.9780 0.0000	1.9620"+03 6.9317"+03 3.8989"-03	1.0250"-03 6.5800"-05 0.0000"+00	6.7650 1.8130 0.8410	1.4461 1.7613 7.3032"-03	2.3370"+02 3.0300"+02 8.3119"+02	2.3896"+02 7.3660"+01 3.8164"+02			
72020604 2.0570"+00 INFINITE	4.8128 1.0272"+05 4.1591"+02	0.7988 0.9963 0.0000	2.0609"+03 7.2784"+03 4.0688"-03	1.0100"-03 6.3700"-05 0.0000"+00	6.6339 1.8038 0.8021	1.4549 1.7531 7.6801"-03	2.4130"+02 3.0380"+02 8.2919"+02	2.4217"+02 7.3840"+01 3.8034"+02			
72020605 2.2100"+00 INFINITE	4.8114 1.0369"+05 4.1434"+02	0.7965 0.9730 0.0000	1.9739"+03 6.9588"+03 3.8292"-03	1.0320"-03 6.5800"-05 0.0000"+00	7.2503 1.7938 6.7803	1.4642 1.7462 7.6203"-03	2.3830"+02 3.0180"+02 8.2757"+02	2.4490"+02 7.3595"+01 3.7890"+02			
72020701 1.4480"+00 INFINITE	4.8228 5.1190"+05 4.1363"+02	0.7890 0.8586 0.0000	5.7897"+03 2.0346"+04 2.2744"-03	8.0500"-04 5.1000"-05 0.0000"+00	8.9558 1.8421 0.8117	1.3463 1.7938 4.5215"-03	1.0240"+03 2.9840"+02 8.2721"+02	1.1927"+03 7.3184"+01 3.7822"+02			
72020702 1.7020"+00 INFINITE	4.8632 5.0535"+05 4.1448"+02	0.7905 0.9616 0.0000	6.4523"+03 2.3006"+04 2.6638"-03	7.1000"-04 4.6600"-05 0.0000"+00	7.5705 1.8280 0.7654	1.3707 1.7786 5.0798"-03	1.0790"+03 2.9930"+02 8.2928"+02	1.1221"+03 7.2333"+01 3.7889"+02			
72020703 1.9050"+00 INFINITE	4.9358 5.1957"+05 4.1813"+02	0.7921 1.0012 0.0000	6.3813"+03 2.3297"+04 2.7511"-03	7.1000"-04 4.6600"-05 0.0000"+00	7.1484 1.8205 0.7422	1.3873 1.7703 5.2627"-03	1.0600"+03 3.0280"+02 8.3505"+02	1.0587"+03 7.1202"+01 3.8205"+02			
72020704 2.0570"+00 INFINITE	4.8892 5.1346"+05 4.1400"+02	0.7934 0.9824 0.0000	7.0974"+03 2.5604"+04 2.9489"-03	6.8500"-04 4.5800"-05 0.0000"+00	7.3365 1.8191 0.7493	1.3874 1.7697 5.6919"-03	1.0860"+03 3.0020"+02 8.2957"+02	1.1054"+03 7.1616"+01 3.7839"+02			
72020705 2.2100"+00 INFINITE	4.8904 5.1973"+05 4.1537"+02	0.7915 0.9988 0.0000	7.0273"+03 2.5298"+04 2.8944"-03	6.9000"-04 4.6200"-05 0.0000"+00	7.4664 1.8039 0.6890	1.4067 1.7564 5.7761"-03	1.1160"+03 3.0050"+02 8.3097"+02	1.1173"+03 7.1823"+01 3.7964"+02			

CAT 7202		VOISINET							BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.		
RUN X *	MD *	TW/TR	PER2W	CF *	H12	H12K	PW*	PD*			
RZ	POD	PW/PD	RED20	CO *	H32	H32K	TW*	TD*			
	TO0	SW *	D2	PI2	H42	D2K	UD	TR			
7202001	4.8067	0.7986	1.2025 ⁺ +04	6.7000 ⁻ -04	7.5164	1.3264	2.3610 ⁺ +03	2.3900 ⁺ +03			
1.4480 ⁺ +00	1.0063 ⁺ +06	0.9578	4.2388 ⁺ +04	4.1200 ⁻ -05	1.8429	1.7984	3.0330 ⁺ +02	7.3867 ⁺ +01			
INFINITE	4.1531 ⁺ +02	0.0000	2.4065 ⁻ -03	0.0000 ⁺ +00	0.6568	4.3725 ⁻ -03	4.2840 ⁺ +02	3.7980 ⁺ +02			
7202002	4.8851	0.7892	1.2551 ⁺ +04	5.9000 ⁻ -04	7.4224	1.3336	2.2260 ⁺ +03	2.2414 ⁺ +03			
1.7020 ⁺ +00	1.0360 ⁺ +06	0.9931	4.4892 ⁺ +04	4.3700 ⁻ -05	1.8394	1.7918	3.0270 ⁺ +02	7.2695 ⁺ +01			
INFINITE	4.1985 ⁺ +02	0.0000	2.6101 ⁻ -03	0.0000 ⁺ +00	0.6873	4.7915 ⁻ -03	8.3509 ⁺ +02	3.8357 ⁺ +02			
7202003	4.9188	0.8009	1.0954 ⁺ +04	6.1000 ⁻ -04	7.6779	1.3591	2.1510 ⁺ +03	2.1510 ⁺ +03			
1.9030 ⁺ +00	1.0356 ⁺ +06	1.0000	4.0146 ⁺ +04	4.1200 ⁻ -05	1.8249	1.7775	3.0480 ⁺ +02	7.1323 ⁺ +01			
INFINITE	4.1645 ⁺ +02	0.0000	2.3475 ⁻ -03	0.0000 ⁺ +00	0.6503	4.5673 ⁻ -03	8.3288 ⁺ +02	3.6056 ⁺ +02			
7202004	4.8760	0.8035	1.2100 ⁺ +04	5.9500 ⁻ -04	8.0428	1.3604	2.2700 ⁺ +03	2.2648 ⁺ +03			
2.0700 ⁺ +00	1.0356 ⁺ +06	1.0023	4.4032 ⁺ +04	4.0500 ⁻ -05	1.8245	1.7774	2.9980 ⁺ +02	7.0925 ⁺ +01			
INFINITE	4.0818 ⁺ +02	0.0000	2.4462 ⁻ -03	0.0000 ⁺ +00	0.5608	4.8303 ⁻ -03	8.2333 ⁺ +02	3.7310 ⁺ +02			
7202005	4.8558	0.7965	1.2724 ⁺ +04	5.9000 ⁻ -04	7.7016	1.3739	2.2930 ⁺ +03	2.2930 ⁺ +03			
2.2100 ⁺ +00	1.0237 ⁺ +06	1.0000	4.5418 ⁺ +04	4.2200 ⁻ -05	1.8132	1.7678	1.0500 ⁺ +02	7.3200 ⁺ +01			
INFINITE	4.1885 ⁺ +02	0.0000	2.6277 ⁻ -03	0.0000 ⁺ +00	0.6256	5.2151 ⁻ -03	8.3342 ⁺ +02	3.8291 ⁺ +02			
7202001	4.7175	0.7502	1.9254 ⁺ +03	1.0500 ⁻ -03	6.7291	1.4120	2.2940 ⁺ +02	2.6298 ⁺ +02			
1.4480 ⁺ +00	9.9446 ⁺ +04	0.8723	6.2887 ⁺ +03	7.8400 ⁻ -05	1.8296	1.7788	2.9820 ⁺ +02	7.0477 ⁺ +01			
INFINITE	4.2925 ⁺ +02	0.0000	3.6357 ⁻ -03	0.0000 ⁺ +00	1.1256	4.5239 ⁻ -03	8.3934 ⁺ +02	3.9280 ⁺ +02			
7202002	4.7856	0.7617	2.1836 ⁺ +03	9.9000 ⁻ -04	5.8837	1.4499	2.3580 ⁺ +02	2.4674 ⁺ +02			
1.7020 ⁺ +00	1.0129 ⁺ +05	0.9557	7.3248 ⁺ +03	7.3800 ⁻ -05	1.8164	1.7623	2.9730 ⁺ +02	7.6474 ⁺ +01			
INFINITE	4.2675 ⁺ +02	0.0000	4.2592 ⁻ -03	0.0000 ⁺ +00	1.0181	7.4885 ⁻ -03	8.3908 ⁺ +02	3.9033 ⁺ +02			
7202003	4.8212	0.7606	2.3677 ⁺ +03	9.6500 ⁻ -04	5.7833	1.4396	2.3900 ⁺ +02	2.4581 ⁺ +02			
1.9050 ⁺ +00	1.0530 ⁺ +05	0.9560	8.0275 ⁺ +03	7.2600 ⁻ -05	1.8146	1.7618	2.9730 ⁺ +02	7.5598 ⁺ +01			
INFINITE	4.2703 ⁺ +02	0.0000	4.5716 ⁻ -03	0.0000 ⁺ +00	1.0380	8.0127 ⁻ -03	8.4046 ⁺ +02	3.9049 ⁺ +02			
7202004	4.8076	0.7602	2.4769 ⁺ +03	9.5500 ⁻ -04	5.6144	1.4547	2.4320 ⁺ +02	2.4320 ⁺ +02			
2.0570 ⁺ +00	1.0250 ⁺ +05	1.0000	8.3014 ⁺ +03	7.2000 ⁻ -05	1.8057	1.7545	2.9600 ⁺ +02	7.5729 ⁺ +01			
INFINITE	4.2579 ⁺ +02	0.0000	4.6190 ⁻ -03	0.0000 ⁺ +00	0.9397	8.4862 ⁻ -03	8.3882 ⁺ +02	3.8938 ⁺ +02			
7202005	4.8361	0.7569	2.5657 ⁺ +03	9.5000 ⁻ -04	5.5801	1.4551	2.4150 ⁺ +02	2.4150 ⁺ +02			
2.2100 ⁺ +00	1.0531 ⁺ +05	1.0000	8.7287 ⁺ +03	6.6300 ⁻ -05	1.8029	1.7507	2.9250 ⁺ +02	7.4446 ⁺ +01			
INFINITE	4.2267 ⁺ +02	0.0000	4.9298 ⁻ -03	0.0000 ⁺ +00	0.9547	8.6981 ⁻ -03	8.3667 ⁺ +02	3.8646 ⁺ +02			
72021001	4.9029	0.7674	6.0830 ⁺ +03	8.0000 ⁻ -04	7.3705	1.3357	1.0140 ⁺ +03	1.1007 ⁺ +03			
1.4480 ⁺ +00	5.1951 ⁺ +05	0.9212	2.1413 ⁺ +04	5.5800 ⁻ -05	1.8457	1.7986	2.9480 ⁺ +02	7.2376 ⁺ +01			
INFINITE	4.2033 ⁺ +02	0.0000	2.5092 ⁻ -03	0.0000 ⁺ +00	0.9328	4.5748 ⁻ -03	8.3629 ⁺ +02	3.8415 ⁺ +02			
72021002	4.9068	0.7713	6.5377 ⁺ +03	7.0000 ⁻ -04	7.3743	1.3701	1.0300 ⁺ +03	1.0922 ⁺ +03			
1.7020 ⁺ +00	5.1799 ⁺ +05	0.9430	2.3124 ⁺ +04	5.0700 ⁻ -05	1.8301	1.7794	2.9680 ⁺ +02	7.2408 ⁺ +01			
INFINITE	4.2108 ⁺ +02	0.0000	2.7304 ⁻ -03	0.0000 ⁺ +00	0.8634	5.1751 ⁻ -03	8.3715 ⁺ +02	3.8481 ⁺ +02			
72021003	4.8955	0.7685	7.5390 ⁺ +03	6.8500 ⁻ -04	6.6925	1.3860	1.1020 ⁺ +03	1.1020 ⁺ +03			
1.9050 ⁺ +00	5.1569 ⁺ +05	1.0000	2.6489 ⁺ +04	5.0300 ⁻ -05	1.8229	1.7722	2.9590 ⁺ +02	7.2722 ⁺ +01			
INFINITE	4.2129 ⁺ +02	0.0000	3.1273 ⁻ -03	0.0000 ⁺ +00	0.7945	5.7705 ⁻ -03	8.3703 ⁺ +02	3.8504 ⁺ +02			
72021004	4.9817	0.7670	7.9489 ⁺ +03	6.7000 ⁻ -04	6.3561	1.3753	1.0530 ⁺ +03	1.0530 ⁺ +03			
2.0570 ⁺ +00	5.4535 ⁺ +05	1.0000	2.8674 ⁺ +04	5.0500 ⁻ -05	1.8264	1.7745	2.9800 ⁺ +02	7.0844 ⁺ +01			
INFINITE	4.2248 ⁺ +02	0.0000	3.3478 ⁻ -03	0.0000 ⁺ +00	0.8749	6.1056 ⁻ -03	8.4070 ⁺ +02	3.8591 ⁺ +02			
72021005	4.9055	0.7754	7.5623 ⁺ +03	6.8000 ⁻ -04	6.6535	1.3837	1.0800 ⁺ +03	1.0800 ⁺ +03			
2.2100 ⁺ +00	5.1141 ⁺ +05	1.0000	2.6816 ⁺ +04	4.9300 ⁻ -05	1.8174	1.7675	2.9990 ⁺ +02	7.2807 ⁺ +01			
INFINITE	4.2321 ⁺ +02	0.0000	3.2295 ⁻ -03	0.0000 ⁺ +00	0.8081	6.0775 ⁻ -03	8.3923 ⁺ +02	3.8677 ⁺ +02			
72021101	4.8224	0.2141	7.9050 ⁺ +03	1.6500 ⁻ -03	3.8377	1.4027	2.3390 ⁺ +02	2.3390 ⁺ +02			
1.9050 ⁺ +00	1.0035 ⁺ +05	1.0000	8.9359 ⁺ +03	4.2500 ⁻ -04	1.7845	1.7579	8.5430 ⁺ +01	7.5455 ⁺ +01			
INFINITE	4.2640 ⁺ +02	0.0000	5.3315 ⁻ -03	0.0000 ⁺ +00	1.1440	7.6100 ⁻ -03	8.3988 ⁺ +02	3.8990 ⁺ +02			
72021102	4.8357	0.2168	8.2024 ⁺ +03	1.8500 ⁻ -03	4.0450	1.4080	2.3500 ⁺ +02	2.3500 ⁺ +02			
2.0570 ⁺ +00	1.0243 ⁺ +05	1.0000	9.2166 ⁺ +03	3.9600 ⁻ -04	1.7796	1.7531	8.3910 ⁺ +01	7.4573 ⁺ +01			
INFINITE	4.2334 ⁺ +02	0.0000	5.3635 ⁻ -03	0.0000 ⁺ +00	1.1161	7.8395 ⁻ -03	8.3726 ⁺ +02	3.8707 ⁺ +02			
72021103	4.8220	0.2163	8.7199 ⁺ +03	1.6200 ⁻ -03	3.8978	1.4138	2.4510 ⁺ +02	2.3883 ⁺ +02			
2.2100 ⁺ +00	1.0241 ⁺ +05	1.0263	9.7327 ⁺ +03	4.0100 ⁻ -04	1.7741	1.7475	8.4340 ⁺ +01	7.5459 ⁺ +01			
INFINITE	4.2637 ⁺ +02	0.0000	5.6882 ⁻ -03	0.0000 ⁺ +00	1.0994	8.2556 ⁻ -03	8.3981 ⁺ +02	3.8987 ⁺ +02			

CAT 7202		VOISINET		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW*	PC*			
X *	PGD	PW/PD	RED2D	CG *	H32	H32K	TW*	TD*			
RZ	TOD	SW *	O2	PI2	H42	O2K	UD	TR			
72021201	4.9151	0.2237	2.3652 ⁺⁰⁴	1.1550 ⁻⁰³	5.5707	1.3604	1.1050 ⁺⁰³	1.1050 ⁺⁰³			
1.9050 ⁺⁰⁰	5.2921 ⁺⁰⁵	1.0000	2.8137 ⁺⁰⁴	NM	1.8011	1.7713	8.6850 ⁺⁰¹	7.2842 ⁺⁰¹			
INFINITE	4.2479 ⁺⁰²	0.0000	3.3081 ⁻⁰³	0.0000 ⁺⁰⁰	0.9182	5.4065 ⁻⁰³	8.4107 ⁺⁰²	3.8819 ⁺⁰²			
72021202	4.9030	0.2414	2.3004 ⁺⁰⁴	1.2000 ⁻⁰³	5.4713	1.3577	1.0480 ⁺⁰³	1.0929 ⁺⁰³			
2.0570 ⁺⁰⁰	5.1597 ⁺⁰⁵	0.9590	2.9354 ⁺⁰⁴	2.4800 ⁻⁰⁴	1.8021	1.7719	9.4010 ⁺⁰¹	7.3305 ⁺⁰¹			
INFINITE	4.2610 ⁺⁰²	0.0000	3.4334 ⁺⁰³	0.0000 ⁺⁰⁰	1.0194	5.7217 ⁻⁰³	8.4201 ⁺⁰²	3.8941 ⁺⁰²			
72021203	4.8574	0.2279	3.3764 ⁺⁰⁴	1.1100 ⁻⁰³	3.4594	1.3378	1.1890 ⁺⁰³	1.1494 ⁺⁰³			
2.2100 ⁺⁰⁰	5.1411 ⁺⁰⁵	1.0344	4.0140 ⁺⁰⁴	2.5400 ⁻⁰⁴	1.8231	1.7862	8.7960 ⁺⁰¹	7.3811 ⁺⁰¹			
INFINITE	4.2211 ⁺⁰²	0.0000	4.6820 ⁻⁰³	0.0000 ⁺⁰⁰	1.0771	6.9945 ⁻⁰³	8.3671 ⁺⁰²	3.8589 ⁺⁰²			
72021301	4.8910	0.2365	3.8033 ⁺⁰⁴	9.9500 ⁻⁰⁴	5.8639	1.3284	2.2210 ⁺⁰³	2.2210 ⁺⁰³			
1.9050 ⁺⁰⁰	1.0338 ⁺⁰⁶	1.0000	4.7373 ⁺⁰⁴	2.2200 ⁻⁰⁴	1.8145	1.7841	9.2620 ⁺⁰¹	7.4084 ⁺⁰¹			
INFINITE	4.2853 ⁺⁰²	0.0000	2.8557 ⁻⁰³	0.0000 ⁺⁰⁰	0.8657	4.7075 ⁻⁰³	8.4405 ⁺⁰²	3.9167 ⁺⁰²			
72021302	4.8578	0.2684	3.3669 ⁺⁰⁴	1.0350 ⁻⁰³	6.4238	1.3377	2.2040 ⁺⁰³	2.2774 ⁺⁰³			
2.0570 ⁺⁰⁰	1.0191 ⁺⁰⁶	0.9678	4.6874 ⁺⁰⁴	2.1400 ⁻⁰⁴	1.8093	1.7788	1.0430 ⁺⁰²	7.4320 ⁺⁰¹			
INFINITE	4.2508 ⁺⁰²	0.0000	2.7877 ⁻⁰³	0.0000 ⁺⁰⁰	0.8572	4.8000 ⁻⁰³	8.3986 ⁺⁰²	3.8860 ⁺⁰²			
72021303	4.8903	0.2604	3.6276 ⁺⁰⁴	9.7000 ⁻⁰⁴	6.4718	1.3477	2.1910 ⁺⁰³	2.2556 ⁺⁰³			
2.2100 ⁺⁰⁰	1.0491 ⁺⁰⁶	0.9713	4.9617 ⁺⁰⁴	2.1500 ⁻⁰⁴	1.8029	1.7742	9.9740 ⁺⁰¹	7.2464 ⁺⁰¹			
INFINITE	4.1906 ⁺⁰²	0.0000	2.8497 ⁻⁰³	0.0000 ⁺⁰⁰	0.8437	4.9312 ⁻⁰³	8.3466 ⁺⁰²	3.8302 ⁺⁰²			
72021401	4.7916	0.2107	6.9631 ⁺⁰³	1.7200 ⁻⁰³	4.2333	1.3808	2.2620 ⁺⁰²	2.4509 ⁺⁰²			
1.4480 ⁺⁰⁰	1.0134 ⁺⁰⁵	0.9229	7.4976 ⁺⁰³	4.3700 ⁻⁰⁴	1.7894	1.7658	8.2140 ⁺⁰¹	7.6218 ⁺⁰¹			
INFINITE	4.2620 ⁺⁰²	0.0000	4.3618 ⁻⁰³	0.0000 ⁺⁰⁰	1.2249	6.2735 ⁻⁰³	8.3872 ⁺⁰²	3.8980 ⁺⁰²			
72021402	4.8206	0.2208	7.7693 ⁺⁰³	1.7000 ⁻⁰³	3.7397	1.3984	2.2510 ⁺⁰²	2.3766 ⁺⁰²			
1.7020 ⁺⁰⁰	1.0174 ⁺⁰⁵	0.9471	8.8442 ⁺⁰³	3.9900 ⁻⁰⁴	1.7837	1.7581	8.6780 ⁺⁰¹	7.6089 ⁺⁰¹			
INFINITE	4.2973 ⁺⁰²	0.0000	5.2607 ⁻⁰³	0.0000 ⁺⁰⁰	1.2552	7.3688 ⁻⁰³	8.4309 ⁺⁰²	3.9295 ⁺⁰²			
72021501	4.9286	0.2242	2.1288 ⁺⁰⁴	1.3000 ⁻⁰³	6.1920	1.3368	9.8710 ⁺⁰²	1.0967 ⁺⁰³			
1.4480 ⁺⁰⁰	5.3265 ⁺⁰⁵	0.9001	2.5494 ⁺⁰⁴	2.8300 ⁻⁰⁴	1.8106	1.7834	8.6050 ⁺⁰¹	7.1708 ⁺⁰¹			
INFINITE	4.2008 ⁺⁰²	0.0000	2.9417 ⁻⁰³	0.0000 ⁺⁰⁰	1.0384	4.7990 ⁻⁰³	8.3679 ⁺⁰²	3.8385 ⁺⁰²			
72021502	4.9186	0.2283	2.5476 ⁺⁰⁴	1.2100 ⁻⁰³	4.6625	1.3727	1.0550 ⁺⁰³	1.0773 ⁺⁰³			
1.7020 ⁺⁰⁰	5.1806 ⁺⁰⁵	0.9793	3.0948 ⁺⁰⁴	2.5900 ⁻⁰⁴	1.7961	1.7660	8.9000 ⁺⁰¹	7.3065 ⁺⁰¹			
INFINITE	4.2659 ⁺⁰²	0.0000	3.7463 ⁻⁰³	0.0000 ⁺⁰⁰	1.0912	5.7415 ⁻⁰³	8.4296 ⁺⁰²	3.8982 ⁺⁰²			

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PH	H12PD	H32PD	H42PD	RED2PDD	RED2PDW	DSTAK
	D2PW	H12PW	H32PW	H42PW	RED2PDG	RED2PDW	
72020101	2.7904*-03 2.9603*-03	7.8417 7.8638	1.8365 1.8313	0.6101 0.6118	6.4383*+03 6.4202*+03	1.6003*+03 1.5958*+03	2.3230*-02
72020201	1.9545*-03 2.0953*-03	8.3511 8.3766	1.8490 1.8434	0.5069 0.5104	2.1511*+04 2.1446*+04	5.3439*+03 5.3276*+03	1.7415*-02
72020301	1.8043*-03 1.8930*-03	8.9484 8.9685	1.8535 1.8494	0.4030 0.4039	4.0087*+04 3.9997*+04	9.7938*+03 9.7719*+03	1.6938*-02
72020302	2.1784*-03 2.1784*-03	8.3076 8.3076	1.8423 1.8423	0.5042 0.5042	4.8768*+04 4.8768*+04	1.1934*+04 1.1934*+04	1.8097*-02
72020303	1.8885*-03 1.9597*-03	8.8951 8.9101	1.8307 1.8276	0.4601 0.4609	4.3901*+04 4.3827*+04	1.0636*+04 1.0618*+04	1.7451*-02
72020304	2.1567*-03 2.2471*-03	8.6413 8.6577	1.8317 1.8282	0.4853 0.4862	4.8592*+04 4.8499*+04	1.1892*+04 1.1870*+04	1.9453*-02
72020305	2.3606*-03 2.3606*-03	8.5064 8.5064	1.8196 1.8196	0.4872 0.4872	5.3860*+04 5.3860*+04	1.3267*+04 1.3267*+04	2.0080*-02
72020401	2.8997*-03 3.1209*-03	7.0728 7.0778	1.8429 1.8365	0.7271 0.7297	6.8507*+03 6.8267*+03	1.7289*+03 1.7228*+03	2.2120*-02
72020501	1.9107*-03 2.0136*-03	8.6345 8.6351	1.8534 1.8490	0.5071 0.5083	2.2068*+04 2.2016*+04	5.2464*+03 5.2339*+03	1.7418*-02
72020601	3.6530*-03 3.7939*-03	6.1802 6.1714	1.8274 1.8241	0.8537 0.8552	6.5224*+03 6.5106*+03	1.8958*+03 1.8924*+03	2.3389*-02
72020701	2.3859*-03 2.6363*-03	6.7776 6.8086	1.8496 1.8412	0.7738 0.7773	2.1370*+04 2.1273*+04	6.0810*+03 6.0533*+03	1.7897*-02
72020801	2.4232*-03 2.4425*-03	7.2531 7.2559	1.8440 1.8433	0.6523 0.6526	4.2732*+04 4.2716*+04	1.2123*+04 1.2118*+04	1.7723*-02
72020901	3.8383*-03 4.1956*-03	4.7203 4.7406	1.8388 1.8310	1.0661 1.0707	6.6470*+03 6.6186*+03	2.0351*+03 2.0264*+03	1.9898*-02
72021001	2.5938*-03 2.7371*-03	6.0154 6.0299	1.8508 1.8464	0.9024 0.9046	2.2161*+04 2.2108*+04	6.2956*+03 6.2805*+03	1.6505*-02
72021101	5.3312*-03 5.3311*-03	3.8382 3.8382	1.7845 1.7845	1.1430 1.1440	8.9458*+03 8.9458*+03	7.9141*+03 7.9141*+03	2.0462*-02
72021201	3.3083*-03 3.3083*-03	5.5702 5.5703	1.8011 1.8011	0.9182 0.9182	2.8175*+04 2.8175*+04	2.3682*+04 2.3682*+04	1.8428*-02
72021301	2.8559*-03 2.8559*-03	5.8634 5.8634	1.8146 1.8146	0.8656 0.8656	4.7433*+04 4.7433*+04	3.8081*+04 3.8081*+04	1.6745*-02
72021401	4.4612*-03 4.7010*-03	3.4434 3.4519	1.7941 1.7897	1.1976 1.2006	7.6778*+03 7.6584*+03	7.1305*+03 7.1139*+03	1.6227*-02
72021501	3.0264*-03 3.2430*-03	5.0047 5.0199	1.8160 1.8105	1.0094 1.0124	2.6261*+04 2.6181*+04	2.1928*+04 2.1862*+04	1.6265*-02

72020201		VOISINET	PROFILE TARULATION	55 POINTS, DELTA AT POINT 42				
I	Y	P1/P1	P/P0	T0/T0D	H/H0	U/UD	T/TD	RHO/RHO0*U/UD
1	0.0000+00	1.0000+00	0.90555	0.83686	0.00000	0.00000	4.66170	0.00000
2	0.3000-05	1.0176+00	0.90555	0.83889	0.03307	0.07130	4.64975	0.01384
3	1.4500-04	1.0917+00	0.90555	0.84350	0.07451	0.15740	4.58240	0.03152
4	2.6900-04	1.2758+00	0.90555	0.85179	0.12558	0.26420	4.42580	0.05406
5	3.9400-04	1.5578+00	0.90555	0.86144	0.17187	0.35340	4.22780	0.07567
6	5.1800-04	1.9422+00	0.90555	0.87160	0.21376	0.42840	4.01640	0.09659
7	7.4400-04	2.6581+00	0.90555	0.88554	0.26830	0.51690	3.71170	0.12611
8	9.7000-04	3.1294+00	0.90555	0.89260	0.29761	0.55990	3.53940	0.14325
9	1.2400-03	3.5703+00	0.90555	0.89487	0.32234	0.59260	3.37980	0.15878
10	1.6310-03	3.9217+00	0.90555	0.89392	0.34067	0.61450	3.25370	0.17102
11	1.9410-03	4.1935+00	0.90555	0.89317	0.35415	0.62980	3.16250	0.18034
12	2.5980-03	4.6175+00	0.90555	0.89254	0.37416	0.65150	3.03190	0.19459
13	3.1340-03	4.9674+00	0.90555	0.89403	0.38974	0.66820	2.93450	0.20585
14	3.7310-03	5.1251+00	0.90555	0.89627	0.40528	0.68440	2.85180	0.21732
15	4.3540-03	5.7201+00	0.90555	0.89919	0.42162	0.70090	2.76360	0.22966
16	4.8030-03	6.0171+00	0.90555	0.90125	0.43349	0.71240	2.70080	0.23686
17	5.3490-03	6.3343+00	0.90562	0.90354	0.44581	0.72400	2.63740	0.24866
18	6.6220-03	7.1518+00	0.90691	0.90972	0.47608	0.75110	2.48910	0.27367
19	7.7240-03	7.8978+00	0.90791	0.91484	0.50208	0.77260	2.36790	0.29623
20	8.9150-03	8.7610+00	0.90899	0.92047	0.53056	0.79450	2.24240	0.32206
21	9.9430-03	9.5024+00	0.90990	0.92479	0.55385	0.81110	2.14470	0.34411
22	1.1153-02	1.0446+01	0.91098	0.92995	0.58213	0.82990	2.03240	0.37199
23	1.3444-02	1.2254+01	0.91298	0.93882	0.63278	0.86000	1.84710	0.42508
24	1.4816-02	1.3380+01	0.91424	0.94299	0.66235	0.87570	1.74600	0.45801
25	1.4790-02	1.3325+01	0.91424	0.94261	0.66092	0.87490	1.75230	0.45647
26	1.6325-02	1.4573+01	0.91624	0.94765	0.69231	0.89050	1.65450	0.49315
27	1.8049-02	1.6002+01	0.91877	0.95219	0.72657	0.90580	1.55420	0.53547
28	2.0157-02	1.7595+01	0.92194	0.95654	0.76294	0.92050	1.45570	0.58298
29	2.3033-02	1.9622+01	0.92620	0.96206	0.80684	0.93680	1.34810	0.64342
30	2.5817-02	2.1370+01	0.93027	0.96650	0.84286	0.94900	1.26770	0.69640
31	2.8143-02	2.2919+01	0.93380	0.97074	0.87353	0.95890	1.20500	0.74309
32	3.1051-02	2.4188+01	0.93860	0.97463	0.89789	0.96660	1.15890	0.78286
33	3.3282-02	2.5126+01	0.94367	0.97755	0.91548	0.97200	1.12730	0.81367
34	3.5994-02	2.6085+01	0.94992	0.98118	0.93312	0.97760	1.09760	0.84607
35	3.9754-02	2.7232+01	0.95862	0.98451	0.95378	0.98350	1.06330	0.88667
36	4.3574-02	2.8145+01	0.96740	0.98818	0.96991	0.98850	1.03870	0.92065
37	4.6533-02	2.8531+01	0.97428	0.99081	0.97665	0.99110	1.02480	0.93767
38	4.9301-02	2.9122+01	0.98062	0.99358	0.98660	0.99440	1.01530	0.96044
39	5.2548-02	2.9602+01	0.98814	0.99637	0.99511	0.99730	1.00440	0.98115
40	5.5126-02	2.9743+01	0.99411	0.99806	0.99760	0.99860	1.00200	0.99074
41	5.7700-02	2.9883+01	1.00027	1.00004	0.99990	1.00000	1.00020	1.00007
42	5.7700-02	2.9889+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
43	6.0952-02	3.0289+01	1.00752	1.00238	1.00679	1.00240	0.99130	1.01880
44	6.3434-02	3.0223+01	1.01385	1.00338	1.00567	1.00270	0.99410	1.02263
45	6.6283-02	3.0226+01	1.01385	1.00456	1.00572	1.00330	0.99520	1.02211
46	6.8181-02	3.0130+01	1.02345	1.00554	1.00410	1.00350	0.99880	1.02827
47	7.0508-02	3.0033+01	1.03305	1.00633	1.00245	1.00360	1.00230	1.03439
48	7.2738-02	3.0000+01	1.03622	1.00613	1.00190	1.00340	1.00300	1.03664
49	7.5453-02	3.0033+01	1.03296	1.00513	1.00245	1.00300	1.00110	1.03492
50	8.0145-02	2.9874+01	1.04897	1.00630	0.99976	1.00310	1.00670	1.04324
51	8.3487-02	2.9810+01	1.05542	1.00649	0.99867	1.00300	1.00670	1.04946
52	8.6733-02	2.9656+01	1.07172	1.00644	0.99605	1.00250	1.01300	1.06061
53	8.8834-02	2.9628+01	1.07498	1.00642	0.99555	1.00240	1.01380	1.06289
54	8.9886-02	2.9596+01	1.07824	1.00642	0.99501	1.00230	1.01470	1.06506
55	9.0744-02	2.9538+01	1.08476	1.00638	0.99403	1.00210	1.01630	1.06960

INPUT VARIABLES Y,U/UD,T/TD,P/P0
 AT I=2 DATA WERE AVERAGED

72020202		VOISINET		PROFILE TABULATION		48 POINTS, DELTA AT POINT ()			
I	Y	PTZ/P	P/PD	TQ/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	0.99711	0.84172	0.00000	0.00000	4.73930	0.00000	
2	6.3000*-05	1.0112*+00	0.99711	0.84366	0.02624	0.05710	4.73510	0.01202	
3	1.0400*-04	1.0326*+00	0.99711	0.84586	0.04456	0.09680	4.71920	0.02045	
4	2.6200*-04	1.1508*+00	0.99711	0.85325	0.09403	0.20200	4.61530	0.04364	
5	3.5800*-04	1.3101*+00	0.99711	0.86019	0.13162	0.27870	4.48360	0.06198	
6	5.3600*-04	1.5326*+00	0.99711	0.87626	0.20200	0.41150	4.14970	0.09888	
7	8.3300*-04	2.4702*+00	0.99711	0.88906	0.25302	0.49840	3.85560	0.12889	
8	1.1480*-03	2.9522*+00	0.99711	0.89349	0.28513	0.54510	3.65490	0.14871	
9	1.7700*-03	3.4536*+00	0.99711	0.89228	0.31395	0.58310	3.44960	0.16855	
10	2.3320*-03	3.7647*+00	0.99711	0.89130	0.33045	0.60330	3.33310	0.18048	
11	3.3830*-03	4.2701*+00	0.99711	0.89283	0.35952	0.63310	3.17110	0.19907	
12	4.4550*-03	4.7949*+00	0.99711	0.89669	0.37972	0.66070	3.02750	0.21760	
13	5.6390*-03	5.3370*+00	0.99711	0.90076	0.40314	0.68580	2.89390	0.23630	
14	6.8980*-03	6.1096*+00	0.99711	0.90666	0.43428	0.71690	2.72510	0.26231	
15	8.0060*-03	6.7085*+00	0.99711	0.91148	0.45692	0.73810	2.60940	0.28204	
16	9.2080*-03	7.3528*+00	0.99711	0.91625	0.48008	0.75840	2.49560	0.30302	
17	1.0312*-02	7.9936*+00	0.99711	0.92051	0.50203	0.77640	2.39170	0.32366	
18	1.1460*-02	8.7335*+00	0.99711	0.92536	0.52623	0.79510	2.28290	0.34728	
19	1.2426*-02	9.4725*+00	0.99711	0.92938	0.54433	0.81160	2.18280	0.37074	
20	1.5128*-02	1.1362*+01	0.99711	0.93908	0.60492	0.84740	1.96240	0.43057	
21	1.7506*-02	1.3619*+01	0.99711	0.94719	0.66412	0.87930	1.75300	0.50015	
22	1.9901*-02	1.5372*+01	0.99711	0.95285	0.70704	0.89950	1.61850	0.55415	
23	2.2799*-02	1.7256*+01	0.99711	0.95800	0.75042	0.91760	1.49520	0.61192	
24	2.4457*-02	1.9070*+01	0.99711	0.96199	0.78994	0.93240	1.39260	0.66746	
25	2.6617*-02	2.0820*+01	0.99721	0.96570	0.82629	0.94450	1.30660	0.72085	
26	2.9022*-02	2.2503*+01	0.99741	0.96958	0.85977	0.95520	1.23430	0.77187	
27	3.1427*-02	2.3731*+01	0.99761	0.97259	0.88342	0.96240	1.18680	0.80898	
28	3.3543*-02	2.4832*+01	0.99771	0.97541	0.90409	0.96860	1.14780	0.84194	
29	3.5756*-02	2.5731*+01	0.99791	0.97818	0.92062	0.97360	1.11840	0.86871	
30	3.7681*-02	2.6445*+01	0.99801	0.98053	0.93354	0.97750	1.09640	0.88978	
31	3.9959*-02	2.7217*+01	0.99821	0.98291	0.94730	0.98150	1.07350	0.91266	
32	4.2426*-02	2.7862*+01	0.99840	0.98560	0.95867	0.98510	1.05590	0.93146	
33	4.4609*-02	2.8349*+01	0.99860	0.98789	0.96750	0.98780	1.04240	0.94630	
34	4.7353*-02	2.9016*+01	0.99880	0.99017	0.97866	0.99120	1.02580	0.96511	
35	4.9342*-02	2.9334*+01	0.99890	0.99176	0.98409	0.99380	1.01820	0.97418	
36	5.1351*-02	2.9524*+01	0.99910	0.99317	0.98731	0.99430	1.01420	0.97950	
37	5.4087*-02	2.9779*+01	0.99930	0.99500	0.99165	0.99600	1.00880	0.98662	
38	5.6528*-02	2.9902*+01	0.99950	0.99644	0.99373	0.99710	1.00680	0.98987	
39	5.9949*-02	3.0150*+01	0.99980	0.99855	0.99790	0.99890	1.00200	0.99671	
40	6.2482*-02	3.0275*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
41	6.5565*-02	3.0335*+01	1.00020	1.00085	1.00100	1.00060	0.99920	1.00160	
42	6.9195*-02	3.0581*+01	1.00050	1.00199	1.00512	1.00190	0.99360	1.00886	
43	7.2060*-02	3.0769*+01	1.00070	1.00289	1.00826	1.00290	0.98940	1.01435	
44	7.5400*-02	3.0635*+01	1.01356	1.00287	1.00603	1.00250	0.99300	1.02326	
45	7.9411*-02	3.0635*+01	1.01356	1.00366	1.00602	1.00290	0.99380	1.02284	
46	8.2639*-02	3.0502*+01	1.02642	1.00345	1.00381	1.00240	0.99720	1.03178	
47	8.6094*-02	3.0376*+01	1.03729	1.00340	1.00170	1.00200	1.00060	1.04074	
48	8.9532*-02	3.0361*+01	1.04028	1.00349	1.00145	1.00210	1.00130	1.04111	

INPUT VARIABLES Y,U/UD,T/TD,P/PH

72020203		VOISINET	PROFILE TABULATION		46 POINTS, DELTA AT POINT 41			
I	Y	PT2/P	P/PO	TU/TOD	U/UD	U/UD	T/TO	RHO/RHOD*U/UD
1	0.0000*+00	1.0000*+00	1.00817	0.83001	0.00000	0.00000	4.74226	0.00000
2	6.3000*-05	1.0172*+00	1.00817	0.83170	0.03224	0.07010	4.72870	0.01495
3	1.4200*-04	1.0654*+00	1.00817	0.83607	0.06224	0.13480	4.69120	0.02897
4	2.0200*-04	1.2048*+00	1.00817	0.84318	0.10771	0.23070	4.56770	0.05081
5	3.5800*-04	1.3925*+00	1.00817	0.84797	0.14509	0.30460	4.40750	0.06967
6	6.3500*-04	2.0504*+00	1.00817	0.86387	0.21986	0.44080	4.01980	0.11055
7	9.9100*-04	2.7405*+00	1.00817	0.87870	0.26951	0.52120	3.74000	0.14050
8	1.2850*-03	3.0942*+00	1.00817	0.88236	0.29102	0.55240	3.60300	0.15457
9	1.8190*-03	3.4471*+00	1.00817	0.88024	0.31082	0.57780	3.45560	0.16857
10	2.4100*-03	3.7328*+00	1.00817	0.88020	0.32589	0.59660	3.35130	0.17947
11	3.0400*-03	4.0303*+00	1.00817	0.88132	0.34083	0.61480	3.25380	0.19049
12	4.1170*-03	4.4922*+00	1.00817	0.88498	0.36274	0.64060	3.12080	0.20701
13	5.2170*-03	4.9542*+00	1.00817	0.88914	0.38334	0.66410	3.00130	0.22308
14	6.2840*-03	5.4149*+00	1.00817	0.89302	0.40280	0.68490	2.89120	0.23883
15	7.4090*-03	5.9213*+00	1.00817	0.89719	0.42113	0.70550	2.78000	0.25585
16	8.7430*-03	6.5510*+00	1.00817	0.90276	0.44709	0.72880	2.65570	0.27659
17	9.8120*-03	7.0839*+00	1.00817	0.90865	0.46640	0.74590	2.55770	0.29401
18	1.0988*-02	7.7027*+00	1.00817	0.91128	0.48784	0.76420	2.45390	0.31397
19	1.2167*-02	8.3778*+00	1.00817	0.91591	0.51020	0.78210	2.34990	0.33554
20	1.3866*-02	9.4888*+00	1.00817	0.92266	0.54497	0.80770	2.19660	0.37071
21	1.6645*-02	1.1335*+01	1.00817	0.93267	0.59627	0.84250	1.98310	0.42831
22	1.9713*-02	1.3519*+01	1.00817	0.94218	0.65574	0.87490	1.77850	0.49572
23	2.2685*-02	1.5781*+01	1.00817	0.94982	0.71035	0.90030	1.60630	0.56506
24	2.5463*-02	1.8132*+01	1.00817	0.95668	0.76297	0.92190	1.46080	0.63659
25	2.8158*-02	2.0324*+01	1.00766	0.96200	0.80894	0.93840	1.34570	0.70268
26	3.1333*-02	2.2456*+01	1.00716	0.96698	0.85127	0.95220	1.25120	0.76648
27	3.3929*-02	2.3940*+01	1.00675	0.97007	0.88028	0.96080	1.19130	0.81198
28	3.7104*-02	2.5383*+01	1.00625	0.97435	0.90617	0.96880	1.14300	0.85289
29	3.9977*-02	2.6590*+01	1.00575	0.97770	0.92787	0.97510	1.10440	0.88800
30	4.2939*-02	2.7661*+01	1.00524	0.98106	0.94670	0.98060	1.07290	0.91876
31	4.5804*-02	2.8475*+01	1.00474	0.98458	0.96076	0.98510	1.04130	0.94147
32	4.8666*-02	2.9029*+01	1.00434	0.98739	0.97023	0.98830	1.01760	0.95662
33	5.1234*-02	2.9385*+01	1.00383	0.98915	0.97625	0.99030	1.02900	0.96606
34	5.4292*-02	2.9736*+01	1.00333	0.99238	0.98216	0.99300	1.02220	0.97467
35	5.6982*-02	2.9999*+01	1.00292	0.99538	0.98656	0.99530	1.01780	0.98075
36	6.0135*-02	3.0278*+01	1.00242	0.99711	0.99122	0.99700	1.01170	0.98785
37	6.2638*-02	3.0424*+01	1.00202	0.99824	0.99364	0.99800	1.00880	0.99129
38	6.5532*-02	3.0511*+01	1.00151	0.99873	0.99507	0.99890	1.00690	0.99316
39	6.8486*-02	3.0592*+01	1.00101	0.99926	0.99641	0.99970	1.00520	0.99483
40	7.1355*-02	3.0727*+01	1.00050	0.99987	0.99865	0.99970	1.00210	0.99811
41	7.4689*-02	3.0809*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
42	7.7211*-02	3.0836*+01	0.99978	0.99984	1.00045	1.00000	0.99910	0.99828
43	8.0434*-02	3.0821*+01	0.99869	1.00213	1.00020	1.00110	1.00180	0.99799
44	8.3373*-02	3.0830*+01	0.99808	1.00288	1.00035	1.00150	1.00230	0.99729
45	8.6121*-02	3.0803*+01	1.00060	1.00344	0.99990	1.00170	1.00360	0.99871
46	8.9248*-02	3.0770*+01	1.00393	1.00343	0.99935	1.00160	1.00450	1.00103

INPUT VARIABLES Y,U/UD,T/TO,P/PW

72020204		VOISINET		PROFILE TABULATION		49 POINTS, DELTA AT POINT 41			
I	Y	PT2/P	P/PD	T0/T0D	U/UD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	0.96956	0.83702	0.00000	0.00000	4.70880	0.00000	
2	6.3000"+05	1.0131"+00	0.96956	0.83776	0.02843	0.06160	4.69540	0.01272	
3	1.2200"+04	1.0350"+00	0.96956	0.83827	0.04623	0.09990	4.66970	0.02074	
4	2.0100"+04	1.0706"+00	0.96956	0.83998	0.06522	0.14040	4.63430	0.02937	
5	3.2000"+04	1.1935"+00	0.96956	0.84541	0.10586	0.22510	4.52160	0.04827	
6	4.3900"+04	1.3811"+00	0.96956	0.85215	0.14454	0.30220	4.37150	0.06703	
7	7.9200"+04	2.2231"+00	0.96956	0.87255	0.23584	0.46600	3.90470	0.11572	
8	5.7700"+04	1.7135"+00	0.96956	0.86170	0.18963	0.38660	4.15630	0.09018	
9	1.1280"+03	2.7804"+00	0.96956	0.88140	0.27460	0.52650	3.67620	0.13886	
10	1.7600"+03	3.2498"+00	0.96956	0.88090	0.30276	0.56480	3.48010	0.15735	
11	2.2910"+03	3.5295"+00	0.96956	0.88059	0.31823	0.58450	3.37360	0.16798	
12	3.1010"+03	3.8702"+00	0.96956	0.88155	0.33602	0.60650	3.25780	0.18050	
13	4.0060"+03	4.2491"+00	0.96956	0.88458	0.35470	0.62910	3.14570	0.19390	
14	5.1050"+03	4.6935"+00	0.96956	0.88856	0.37537	0.65300	3.02630	0.20921	
15	6.2810"+03	5.1481"+00	0.96956	0.89281	0.39535	0.67500	2.91510	0.22450	
16	7.4370"+03	5.6264"+00	0.96956	0.89653	0.41530	0.69560	2.80540	0.24040	
17	8.5780"+03	6.1256"+00	0.96956	0.90057	0.43512	0.71510	2.70090	0.25670	
18	9.7740"+03	6.6056"+00	0.96956	0.90425	0.45335	0.73210	2.60780	0.27219	
19	1.1041"+02	7.1727"+00	0.96985	0.90930	0.47397	0.75070	2.50860	0.29023	
20	1.2435"+02	7.9113"+00	0.97043	0.91532	0.49953	0.77230	2.39030	0.31354	
21	1.4041"+02	8.7754"+00	0.97101	0.92383	0.52784	0.79540	2.27070	0.34013	
22	1.5761"+02	9.8199"+00	0.97169	0.92971	0.56015	0.81820	2.13360	0.37263	
23	1.8626"+02	1.1644"+01	0.97276	0.93931	0.61246	0.85130	1.93200	0.42863	
24	2.1011"+02	1.3252"+01	0.97392	0.94620	0.65512	0.87480	1.78310	0.47781	
25	2.3208"+02	1.5029"+01	0.97537	0.95222	0.69920	0.89610	1.64250	0.53214	
26	2.5690"+02	1.6786"+01	0.97702	0.95728	0.74023	0.91370	1.52340	0.58592	
27	2.7600"+02	1.8433"+01	0.97828	0.96144	0.77671	0.92750	1.42690	0.63610	
28	2.9987"+02	2.0131"+01	0.97993	0.96522	0.81259	0.94040	1.33930	0.68807	
29	3.2565"+02	2.1686"+01	0.98158	0.96823	0.84413	0.95050	1.26790	0.73585	
30	3.4666"+02	2.2863"+01	0.98303	0.97114	0.86722	0.95780	1.21980	0.77159	
31	3.7722"+02	2.4361"+01	0.98507	0.97582	0.89578	0.96690	1.16510	0.81749	
32	4.0109"+02	2.5368"+01	0.98662	0.97828	0.91446	0.97230	1.13050	0.84855	
33	4.2019"+02	2.6033"+01	0.98798	0.98047	0.92659	0.97600	1.10930	0.86910	
34	4.4310"+02	2.6880"+01	0.98943	0.98355	0.94181	0.98070	1.08430	0.89490	
35	4.6698"+02	2.7738"+01	0.99108	0.98627	0.95699	0.98510	1.05960	0.92140	
36	4.9182"+02	2.8532"+01	0.99273	0.98873	0.97082	0.98900	1.03780	0.94605	
37	5.2428"+02	2.9261"+01	0.99476	0.99163	0.98336	0.99280	1.01930	0.96890	
38	5.5293"+02	2.9623"+01	0.99661	0.99337	0.98952	0.99480	1.01070	0.98093	
39	5.7678"+02	3.0051"+01	0.99806	0.99536	0.99675	0.99710	1.00070	0.99447	
40	6.0830"+02	3.0244"+01	1.00000	0.99820	1.00000	0.99910	0.99820	1.00090	
41	6.3643"+02	3.0244"+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
42	6.6916"+02	3.0274"+01	0.99690	1.00162	1.00050	1.00090	1.00040	0.99700	
43	6.9571"+02	3.0307"+01	0.99370	1.00223	1.00105	1.00130	1.00090	0.99449	
44	7.2507"+02	3.0339"+01	0.99060	1.00303	1.00160	1.00180	1.00040	0.99198	
45	7.5352"+02	3.0387"+01	0.98604	1.00395	1.00240	1.00240	1.00000	0.98840	
46	7.7828"+02	3.0426"+01	0.98288	1.00472	1.00305	1.00290	0.99970	0.98598	
47	8.1265"+02	3.0465"+01	0.98429	1.00585	1.00270	1.00340	1.00140	0.98628	
48	8.4607"+02	3.0441"+01	0.98119	1.00524	1.00330	1.00320	0.99980	0.98453	
49	8.9573"+02	3.0625"+01	0.96422	1.00535	1.00637	1.00380	0.99490	0.97285	

INPUT VARIABLES Y,U/UD,T/TD,P/PH

72020205		VOISINET		PROFILE TABULATION		41 POINTS, DELTA AT POINT 34			
I	Y	PTZ/P	P/PPD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	1.01317	0.84627	0.00000	0.00000	4.79500	0.00000	
2	6.3000 ⁻⁰⁵	1.0251 ⁺⁰⁰	1.01317	0.84952	0.03911	0.08540	4.76810	0.01815	
3	2.0100 ⁻⁰⁴	1.1503 ⁺⁰⁰	1.01317	0.85458	0.09367	0.20180	4.64120	0.04405	
4	3.4000 ⁻⁰⁴	1.3506 ⁺⁰⁰	1.01317	0.86165	0.13882	0.29350	4.46980	0.06653	
5	4.3900 ⁻⁰⁴	1.5087 ⁺⁰⁰	1.01317	0.86873	0.17433	0.36160	4.30230	0.08516	
6	6.9300 ⁻⁰⁴	2.1325 ⁺⁰⁰	1.01317	0.88088	0.22804	0.45660	4.00930	0.11539	
7	1.0290 ⁻⁰³	2.7063 ⁺⁰⁰	1.01317	0.88913	0.26906	0.52170	3.79960	0.14059	
8	1.6030 ⁻⁰³	3.1438 ⁺⁰⁰	1.01317	0.88769	0.29561	0.55860	3.56600	0.15671	
9	2.1540 ⁻⁰³	3.4132 ⁺⁰⁰	1.01317	0.88669	0.31099	0.57820	3.45670	0.16947	
10	3.3550 ⁻⁰³	3.8914 ⁺⁰⁰	1.01317	0.88864	0.33612	0.60990	3.29250	0.18768	
11	4.4580 ⁻⁰³	4.3187 ⁺⁰⁰	1.01317	0.89165	0.35698	0.63500	3.16410	0.20333	
12	5.5780 ⁻⁰³	4.7386 ⁺⁰⁰	1.01317	0.89509	0.37631	0.65720	3.05010	0.21831	
13	6.7970 ⁻⁰³	5.2005 ⁺⁰⁰	1.01317	0.89900	0.39643	0.67920	2.93540	0.23443	
14	7.8610 ⁻⁰³	5.6591 ⁺⁰⁰	1.01317	0.90279	0.41542	0.69890	2.83050	0.25017	
15	9.0750 ⁻⁰³	6.0796 ⁺⁰⁰	1.01317	0.90623	0.43208	0.71540	2.74140	0.26440	
16	1.0282 ⁻⁰²	6.5938 ⁺⁰⁰	1.01317	0.91054	0.45160	0.73390	2.64100	0.28155	
17	1.1377 ⁻⁰²	7.0568 ⁺⁰⁰	1.01317	0.91374	0.46847	0.74890	2.55560	0.29690	
18	1.3655 ⁻⁰²	7.9986 ⁺⁰⁰	1.01317	0.92053	0.50100	0.77620	2.40030	0.32764	
19	1.6998 ⁻⁰²	9.7586 ⁺⁰⁰	1.01317	0.93045	0.55668	0.81700	2.15390	0.38431	
20	1.9576 ⁻⁰²	1.1235 ⁺⁰¹	1.01317	0.93840	0.59940	0.84460	1.98550	0.43099	
21	2.2154 ⁻⁰²	1.3021 ⁺⁰¹	1.01317	0.94606	0.64728	0.87160	1.81320	0.48703	
22	2.5400 ⁻⁰²	1.5366 ⁺⁰¹	1.01317	0.95378	0.70521	0.89950	1.62690	0.56017	
23	2.8456 ⁻⁰²	1.7869 ⁺⁰¹	1.01317	0.96065	0.76219	0.92300	1.46650	0.63768	
24	3.1130 ⁻⁰²	1.9925 ⁺⁰¹	1.01317	0.96504	0.80597	0.93860	1.33620	0.70120	
25	3.4282 ⁻⁰²	2.2127 ⁺⁰¹	1.01317	0.97094	0.85038	0.95360	1.25750	0.76632	
26	3.7816 ⁻⁰²	2.4380 ⁺⁰¹	1.01236	0.97525	0.89352	0.96620	1.16930	0.83652	
27	4.0965 ⁻⁰²	2.5874 ⁺⁰¹	1.01125	0.97970	0.92102	0.97450	1.11950	0.88027	
28	4.4498 ⁻⁰²	2.7229 ⁺⁰¹	1.01003	0.98445	0.94527	0.98190	1.07900	0.91914	
29	4.8222 ⁻⁰²	2.8230 ⁺⁰¹	1.00871	0.98875	0.96278	0.98750	1.05200	0.94687	
30	5.1852 ⁻⁰²	2.9037 ⁺⁰¹	1.00740	0.99208	0.97668	0.99180	1.03120	0.96891	
31	5.5952 ⁻⁰²	2.9442 ⁺⁰¹	1.00669	0.99392	0.98358	0.99400	1.02130	0.97978	
32	5.8059 ⁻⁰²	2.9938 ⁺⁰¹	1.00517	0.99707	0.99196	0.99710	1.01040	0.99194	
33	6.1877 ⁻⁰²	3.0159 ⁺⁰¹	1.00223	0.99874	0.99567	0.99860	1.00590	0.99496	
D 34	6.4544 ⁻⁰²	3.0418 ⁺⁰¹	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
35	6.8049 ⁻⁰²	3.0574 ⁺⁰¹	0.99706	1.00188	1.00260	1.00140	0.99760	1.00086	
36	7.1463 ⁻⁰²	3.0686 ⁺⁰¹	0.99433	1.00243	1.00446	1.00200	0.99510	1.00122	
37	7.5443 ⁻⁰²	3.0755 ⁺⁰¹	0.99178	1.00342	1.00562	1.00270	0.99420	0.99629	
38	7.9065 ⁻⁰²	3.0801 ⁺⁰¹	0.98828	1.00396	1.00638	1.00310	0.99350	0.99278	
39	8.1836 ⁻⁰²	3.0804 ⁺⁰¹	0.98328	1.00434	1.00642	1.00330	0.99380	0.99268	
40	8.6228 ⁻⁰²	3.0864 ⁺⁰¹	0.97781	1.00560	1.00743	1.00410	0.99340	0.98834	
41	9.0429 ⁻⁰²	3.0840 ⁺⁰¹	0.98014	1.00594	1.00702	1.00420	0.99440	0.98980	

INPUT VARIABLES Y,U/UD,T/TD,P/PP

72021201		VOISINET	PROFILE TABULATION		35 POINTS, DELTA AT POINT 30			
I	Y	PT2/P	P/PD	T0/T00	H/MD	U/UD	T/TD	RHG/RHOD*U/UD
1	0.0000+00	1.0000+00	1.00000	0.20445	0.00000	0.00000	1.19230	0.00000
2	6.3000+05	1.2759+00	1.00000	0.31703	0.12214	0.16040	1.72450	0.09301
3	1.4000+04	1.6579+00	1.00000	0.38161	0.17934	0.24490	1.92610	0.12922
4	3.9400+04	3.6232+00	1.00000	0.54512	0.31626	0.46300	2.14320	0.21605
5	6.4800+04	4.4390+00	1.00000	0.59043	0.35585	0.52010	2.13020	0.24347
6	9.0200+04	4.7084+00	1.00000	0.60419	0.36794	0.53700	2.13010	0.25210
7	1.1300+03	4.8437+00	1.00000	0.61096	0.37385	0.54520	2.12670	0.25636
8	1.3590+03	4.9632+00	1.00000	0.61709	0.37901	0.55240	2.12430	0.26004
9	1.6350+03	5.1292+00	1.00000	0.62712	0.38604	0.56290	2.12620	0.26474
10	1.9150+03	5.2696+00	1.00000	0.63641	0.39188	0.57200	2.13050	0.26848
11	2.1440+03	5.4150+00	1.00000	0.64294	0.39785	0.57990	2.12460	0.27295
12	2.4920+03	6.0398+00	1.00000	0.69862	0.45199	0.64720	2.05030	0.31566
13	7.4240+03	8.1353+00	1.00000	0.74013	0.49611	0.69660	1.97160	0.35332
14	9.9360+03	9.4924+00	1.00000	0.77578	0.53637	0.73910	1.88470	0.39216
15	1.2118+02	1.0711+01	1.00000	0.80538	0.57366	0.77250	1.81340	0.42600
16	1.4989+02	1.2362+01	1.00000	0.83897	0.61825	0.81050	1.71860	0.47160
17	1.7501+02	1.3937+01	1.00000	0.86533	0.65796	0.84060	1.63220	0.51501
18	1.9866+02	1.5490+01	1.00000	0.88747	0.69490	0.86590	1.55270	0.55767
19	2.2652+02	1.7426+01	1.00000	0.90930	0.73834	0.89190	1.45920	0.61123
20	2.4938+02	1.9015+01	1.00000	0.92303	0.77218	0.90940	1.38700	0.65566
21	3.0190+02	2.2436+01	1.00000	0.94339	0.84041	0.93840	1.24680	0.75265
22	3.5065+02	2.4868+01	1.00000	0.95435	0.88573	0.95470	1.16180	0.82174
23	4.0267+02	2.7333+01	1.00000	0.96376	0.92938	0.96870	1.08640	0.89166
24	4.5344+02	2.9278+01	1.00000	0.97350	0.96245	0.98000	1.03680	0.94522
25	5.0089+02	2.9841+01	1.00000	0.98121	0.97180	0.98560	1.02860	0.95820
26	5.5446+02	3.0554+01	1.00000	0.98657	0.98354	0.99040	1.01400	0.97673
27	6.0546+02	3.0887+01	1.00000	0.99025	0.98296	0.99320	1.00860	0.98473
28	6.5674+02	3.1177+01	1.00000	0.99479	0.98367	0.99630	1.00530	0.99105
29	7.0800+02	3.1301+01	1.00000	0.99849	0.98567	0.99890	1.00570	0.99284
D 30	7.5801+02	3.1570+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
31	8.0978+02	3.1514+01	1.00000	1.00031	0.99910	1.00060	1.00300	0.99761
32	8.5954+02	3.1128+01	1.00000	1.00207	0.99287	0.99990	1.01400	0.98600
33	9.1029+02	3.1397+01	1.00000	1.00276	0.99722	1.00090	1.00740	0.99355
34	9.5496+02	3.1744+01	1.00000	1.00344	1.00280	1.00230	0.99900	1.00330
35	1.0309+01	3.1632+01	1.00000	1.00526	1.00100	1.00280	1.00360	0.99920

INPUT VARIABLES Y,U/UD,T/TD,P/PH

72021202		VOISINET	PROFILE TABULATION		36 POINTS, DELTA AT POINT 32			
I	Y	PT2/P	P/PD	T0/T00	H/MD	U/UD	T/TD	RHD/RHOD*U/UD
1	0.0000+00	1.0000+00	0.95896	0.22063	0.00000	0.00000	1.28140	0.00000
2	6.3000+05	1.2719+00	0.95896	0.32211	0.12164	0.16075	1.74655	0.08826
3	1.1400+04	1.4317+00	0.95896	0.35075	0.14986	0.20320	1.83860	0.10598
4	1.6500+04	1.8166+00	0.95896	0.40099	0.19667	0.27560	1.96370	0.13459
5	2.4100+04	2.3446+00	0.95896	0.44930	0.24028	0.34340	2.04250	0.16123
6	4.1900+04	3.4442+00	0.95896	0.54886	0.32850	0.47590	2.09880	0.21744
7	7.2400+04	4.9497+00	0.95896	0.58941	0.36176	0.52260	2.08690	0.24014
8	1.1300+03	4.9233+00	0.95896	0.60338	0.37823	0.54500	2.07630	0.25171
9	1.5370+03	5.1432+00	0.95896	0.61332	0.38758	0.55740	2.06630	0.25844
10	1.7650+03	5.2926+00	0.95896	0.62044	0.39380	0.56580	2.06430	0.26284
11	2.0140+03	5.4412+00	0.95896	0.62727	0.39989	0.57390	2.05960	0.26721
12	2.4000+03	5.7020+00	0.95896	0.63734	0.41036	0.58690	2.04550	0.27515
13	4.6040+03	6.8951+00	0.95896	0.67723	0.45512	0.63890	1.97070	0.31854
14	7.4790+03	8.3317+00	0.95896	0.71371	0.50368	0.69070	1.88050	0.35222
15	9.8630+03	9.6426+00	0.95896	0.75078	0.54419	0.72990	1.79900	0.38907
16	1.2022+02	1.0825+01	0.95896	0.77759	0.57828	0.76100	1.73180	0.42139
17	1.5067+02	1.2523+01	0.95896	0.81183	0.62396	0.79930	1.64100	0.46709
18	1.7658+02	1.4138+01	0.95896	0.83830	0.66450	0.82970	1.55900	0.51036
19	2.0119+02	1.5774+01	0.95896	0.86153	0.70317	0.85590	1.48160	0.55398
20	2.2809+02	1.7416+01	0.95896	0.88237	0.73996	0.87890	1.41080	0.59741
21	2.5197+02	1.9167+01	0.95896	0.90200	0.77725	0.90030	1.34170	0.64347
22	3.0249+02	2.2590+01	0.96250	0.92871	0.84543	0.93220	1.21580	0.73799
23	3.5377+02	2.5319+01	0.96634	0.94400	0.89608	0.95170	1.12600	0.81531
24	4.0455+02	2.7158+01	0.97008	0.95661	0.92865	0.96490	1.07960	0.86702
25	4.5583+02	2.8574+01	0.97392	0.96461	0.95296	0.97370	1.04400	0.90834
26	5.0609+02	2.9695+01	0.97766	0.97292	0.97178	0.98140	1.01990	0.94075
27	5.5687+02	3.0591+01	0.98140	0.98045	0.98509	0.98760	1.00510	0.96431
28	6.0510+02	3.0985+01	0.98494	0.98629	0.99235	0.99180	0.99690	0.97794
29	6.5316+02	3.1013+01	0.98888	0.99148	0.99346	0.99460	1.00230	0.98128
30	7.0976+02	3.1087+01	0.99271	0.99465	0.99466	0.99640	1.00350	0.98569
31	7.6225+02	3.1341+01	0.99664	0.99871	1.00201	0.99870	0.99540	1.00095
D 32	8.0769+02	3.1417+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
33	8.5794+02	3.1370+01	1.00451	1.00026	0.99925	1.00000	1.00150	1.00300
34	9.1382+02	3.1399+01	1.01016	1.00120	0.99826	1.00030	1.00410	1.00634
35	9.5951+02	3.1312+01	1.00949	1.00239	0.99831	1.00090	1.00520	1.00516
36	1.0166+01	3.1315+01	1.00969	1.00297	0.99836	1.00120	1.00570	1.00517

INPUT VARIABLES Y,U/UD,T/TD,P/PH
AT I=2 DATA WERE AVERAGED

72021203		VOISINFT	PROFILE TABULATION			34 POINTS, DELTA AT POINT 29			
I	Y	PTZ/P	P/PD	T0/T0D	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	1.03445	0.20838	0.00000	0.00000	1.19170	0.00000	
2	6.3000+05	1.2322+00	1.03445	0.31544	0.11414	0.14880	1.69450	0.09057	
3	1.9100+04	2.0209+00	1.03445	0.43535	0.21775	0.31000	2.03620	0.15744	
4	5.7200+04	3.9178+00	1.03445	0.57604	0.33507	0.49170	2.15340	0.23620	
5	7.7500+04	4.2236+00	1.03445	0.59310	0.34997	0.51310	2.14950	0.24693	
6	1.0540+03	4.4072+00	1.03445	0.60268	0.35860	0.52520	2.14500	0.25328	
7	1.3340+03	4.5338+00	1.03445	0.60891	0.36443	0.53320	2.14070	0.25766	
8	1.5620+03	4.6826+00	1.03445	0.61551	0.37115	0.54210	2.13330	0.26287	
9	1.7400+03	4.7513+00	1.03445	0.62049	0.37422	0.54700	2.13690	0.26483	
10	2.1720+03	4.9615+00	1.03445	0.63310	0.38343	0.56060	2.13760	0.27124	
11	4.5570+03	6.0784+00	1.03445	0.67584	0.42899	0.61700	2.06860	0.30854	
12	7.2240+03	7.2104+00	1.03445	0.71493	0.47059	0.66540	1.99430	0.34428	
13	9.7610+03	8.2676+00	1.03445	0.74849	0.50632	0.70470	1.93710	0.37632	
14	1.2301+02	9.3822+00	1.03445	0.77934	0.54142	0.74040	1.87010	0.40955	
15	1.4991+02	1.0650+01	1.03445	0.80953	0.57875	0.77470	1.79180	0.44725	
16	1.7429+02	1.1903+01	1.03445	0.83442	0.61340	0.80430	1.71930	0.48392	
17	1.9967+02	1.3323+01	1.03445	0.85917	0.65041	0.83290	1.63490	0.52539	
18	2.2431+02	1.4796+01	1.03445	0.87980	0.68671	0.85770	1.56000	0.56875	
19	2.5121+02	1.6423+01	1.03445	0.89908	0.72468	0.88110	1.47830	0.61695	
20	3.0223+02	1.9922+01	1.03134	0.92810	0.80024	0.91930	1.31970	0.71843	
21	3.5123+02	2.3117+01	1.02814	0.94611	0.86347	0.94490	1.19750	0.81126	
22	4.0251+02	2.5232+01	1.02483	0.95772	0.90299	0.95980	1.13000	0.87047	
23	4.5380+02	2.7105+01	1.02141	0.96618	0.93644	0.97110	1.07540	0.92235	
24	5.0458+02	2.9455+01	1.01790	0.97333	0.97686	0.98750	1.02190	0.98073	
25	5.5279+02	3.1398+01	1.01831	0.97471	0.95888	0.97980	1.04410	0.95560	
26	6.0663+02	3.3093+01	1.01148	0.98783	0.98756	0.99170	1.00840	0.99473	
27	6.5740+02	3.0574+01	1.00817	0.99397	0.95955	0.99620	1.00130	1.00304	
28	7.0669+02	3.0801+01	1.00486	0.99745	0.99930	0.99860	0.99860	1.00486	
29	7.5565+02	3.0844+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
30	8.1023+02	3.0811+01	1.00559	1.00099	0.99945	1.00040	1.00190	1.00406	
31	8.5923+02	3.0802+01	1.00455	1.00225	0.99930	1.00100	1.00340	1.00215	
32	9.1128+02	3.0826+01	1.00217	1.00331	0.99970	1.00160	1.00380	0.99998	
33	9.6383+02	3.0888+01	0.99772	1.00366	1.00040	1.00190	1.00300	0.99663	
34	1.0278+01	3.1063+01	0.97683	1.00475	1.00360	1.00300	0.99890	0.98094	

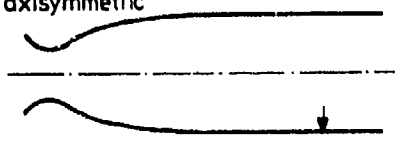
INPUT VARIABLES Y,U/UD,T/T0,P/PW

72021501		VOISINFT	PROFILE TABULATION			45 POINTS, DELTA AT POINT 38			
I	Y	PTZ/P	P/PD	T0/T0D	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	0.90009	0.20484	0.00000	0.00000	1.20000	0.00000	
2	6.3000+05	1.3808+00	0.90009	0.31846	0.14099	0.18390	1.70130	0.09729	
3	1.1400+04	1.9298+00	0.90009	0.38482	0.20624	0.28190	1.86830	0.13581	
4	1.6500+04	2.2371+00	0.90009	0.41172	0.23118	0.31990	1.91480	0.15038	
5	1.9100+04	2.6458+00	0.90009	0.44321	0.25944	0.36290	1.95660	0.16694	
6	2.6700+04	3.3652+00	0.90009	0.49255	0.30176	0.42880	2.00050	0.19203	
7	2.9200+04	3.6417+00	0.90009	0.50109	0.31635	0.44460	1.97520	0.20260	
8	3.6800+04	4.1143+00	0.90009	0.51593	0.33975	0.47260	1.93500	0.21984	
9	3.9400+04	4.2375+00	0.90009	0.51978	0.34533	0.47950	1.92800	0.22386	
10	4.7000+04	4.5826+00	0.90009	0.53010	0.36135	0.49810	1.90010	0.23595	
11	5.2100+04	4.6759+00	0.90009	0.53333	0.36550	0.50310	1.89470	0.23900	
12	5.4600+04	4.7880+00	0.90009	0.53634	0.37041	0.50860	1.88530	0.24282	
13	6.4800+04	5.0260+00	0.90009	0.54680	0.38063	0.52190	1.88000	0.24987	
14	6.5100+04	5.3650+00	0.90009	0.56338	0.39472	0.54100	1.87850	0.25922	
15	1.1300+03	5.5634+00	0.90009	0.57796	0.40273	0.55420	1.89370	0.26342	
16	1.4100+03	5.7257+00	0.90009	0.59044	0.40916	0.56510	1.90750	0.26665	
17	1.6380+03	5.8940+00	0.90009	0.59825	0.41572	0.57380	1.90510	0.27110	
18	1.9180+03	6.1194+00	0.90009	0.60822	0.42435	0.58500	1.90050	0.27706	
19	2.1970+03	6.3603+00	0.90009	0.61722	0.43337	0.59590	1.89070	0.28369	
20	2.4260+03	6.5685+00	0.90009	0.62654	0.44095	0.60580	1.88750	0.28884	
21	2.7050+03	6.7664+00	0.90009	0.63697	0.44817	0.61590	1.88860	0.29353	
22	5.1690+03	6.8246+00	0.90009	0.69524	0.51034	0.68430	1.79790	0.34258	
23	7.9370+03	1.0582+01	0.90009	0.74541	0.56845	0.74100	1.69920	0.39252	
24	1.0503+02	1.2359+01	0.90036	0.78240	0.61648	0.78230	1.61030	0.43740	
25	1.2891+02	1.3929+01	0.90252	0.81374	0.65597	0.81470	1.54250	0.47668	
26	1.5431+02	1.5656+01	0.90477	0.84276	0.69683	0.84880	1.46980	0.52004	
27	1.7920+02	1.7480+01	0.90693	0.86883	0.73749	0.87180	1.39740	0.56581	
28	2.0561+02	1.9481+01	0.90927	0.89280	0.77968	0.89680	1.32300	0.61635	
29	2.2771+02	2.1044+01	0.91125	0.90835	0.81112	0.91340	1.26810	0.65637	
30	2.5743+02	2.3058+01	0.91413	0.92881	0.84989	0.93360	1.20670	0.70725	
31	3.0721+02	2.5567+01	0.92142	0.94556	0.89585	0.95260	1.13070	0.77629	
32	3.5674+02	2.7105+01	0.92880	0.95969	0.92291	0.96540	1.09420	0.81947	
33	4.0881+02	2.8441+01	0.93663	0.96996	0.94527	0.97500	1.06390	0.85837	
34	4.6037+02	2.9492+01	0.94496	0.97807	0.96337	0.98250	1.04010	0.89641	
35	5.1219+02	3.0556+01	0.96148	0.98629	0.98087	0.98980	1.01830	0.93457	
36	5.6147+02	3.0723+01	0.97399	0.99131	0.98360	0.99280	1.01880	0.94913	
37	6.1074+02	3.1136+01	0.98641	0.99675	0.99078	0.99670	1.01300	0.97054	
38	6.6434+02	3.1741+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
39	7.1158+02	3.1281+01	1.01197	1.00174	0.99263	0.99960	1.01410	0.99750	
40	7.6543+02	3.1198+01	1.02304	1.00304	0.99063	0.99990	1.01880	1.00406	
41	8.1267+02	3.0780+01	1.06463	1.00541	0.98452	1.00000	1.03174	1.03191	
42	8.6474+02	3.0558+01	1.08335	1.00389	0.98091	0.99860	1.03680	1.04384	
43	9.1681+02	3.0458+01	1.09352	1.00509	0.97927	0.99690	1.04050	1.04980	
44	9.6761+02	3.0256+01	1.11620	1.00327	0.97597	0.99740	1.04440	1.06597	
45	1.0174+01	3.0122+01	1.12988	1.00368	0.97377	0.99720	1.04870	1.07440	

INPUT VARIABLES Y,U/UD,T/T0,P/PW

72021502		VOISINET	PROFILE TABULATION			46 POINTS, DELTA AT POINT 40			
I	Y	PT2/P	P/PO	TQ/TOD	H/HO	U/UD	T/TO	RHO/RHO+U/UD	
1	0.0000+00	1.0000+00	0.97934	0.20863	0.00000	0.00000	1.21810	0.00000	
2	0.3000-05	1.4093+00	0.97934	0.31050	0.14526	0.18630	1.64490	0.11092	
3	1.1400-04	1.6604+00	0.97934	0.34106	0.17950	0.23560	1.72270	0.13394	
4	1.4000-04	1.9072+00	0.97934	0.36317	0.20462	0.27170	1.76320	0.15091	
5	1.9100-04	2.1902+00	0.97934	0.39397	0.22809	0.30920	1.81760	0.16479	
6	2.4100-04	2.6941+00	0.97934	0.42815	0.26307	0.36000	1.87270	0.18826	
7	2.9200-04	2.9523+00	0.97934	0.44820	0.27894	0.38460	1.90110	0.19812	
8	3.4300-04	3.4211+00	0.97934	0.47307	0.30539	0.42130	1.90320	0.21679	
9	4.1400-04	3.7440+00	0.97934	0.49122	0.32222	0.44520	1.90900	0.22839	
10	4.4400-04	3.8836+00	0.97934	0.49676	0.32921	0.45410	1.90260	0.23374	
11	5.2100-04	4.0649+00	0.97934	0.50605	0.33807	0.46630	1.90250	0.24003	
12	5.4600-04	4.1259+00	0.97934	0.50955	0.34099	0.47050	1.90390	0.24202	
13	6.2500-04	4.4993+00	0.97934	0.53563	0.36283	0.50150	1.91040	0.25709	
14	1.0600-03	4.7937+00	0.97934	0.55209	0.37141	0.51640	1.93310	0.26162	
15	1.3080-03	4.9496+00	0.97934	0.56331	0.37811	0.52720	1.94410	0.26558	
16	1.5880-03	5.1054+00	0.97934	0.57346	0.38476	0.53740	1.95080	0.26978	
17	1.8160-03	5.2728+00	0.97934	0.58234	0.39174	0.54720	1.95120	0.27463	
18	2.0960-03	5.4720+00	0.97934	0.59092	0.39947	0.55770	1.94520	0.28078	
19	2.3490-03	5.6202+00	0.97934	0.59881	0.40581	0.56570	1.94320	0.28510	
20	2.6800-03	5.8168+00	0.97934	0.60656	0.41356	0.57570	1.93780	0.29095	
21	3.2450-03	7.2868+00	0.97934	0.66102	0.46737	0.64020	1.87630	0.33415	
22	7.8870-03	8.7571+00	0.97934	0.70585	0.51553	0.69220	1.80280	0.37602	
23	1.0401-02	1.0152+01	0.97934	0.74150	0.55735	0.73300	1.72960	0.41504	
24	1.2801-02	1.1630+01	0.97934	0.77388	0.59846	0.76950	1.65330	0.45582	
25	1.5354-02	1.3206+01	0.97934	0.80392	0.63938	0.80270	1.57610	0.49877	
26	1.7970-02	1.4960+01	0.97934	0.83293	0.68203	0.83420	1.49600	0.54610	
27	2.0460-02	1.6711+01	0.97934	0.85747	0.72209	0.86080	1.42110	0.59321	
28	2.3076-02	1.8620+01	0.97934	0.88028	0.76336	0.88550	1.34560	0.64447	
29	2.5819-02	2.0643+01	0.97934	0.90246	0.80480	0.90860	1.27460	0.69826	
30	3.0924-02	2.4105+01	0.98169	0.92654	0.87114	0.93740	1.15790	0.79474	
31	3.5776-02	2.6412+01	0.98374	0.93999	0.91268	0.95330	1.09100	0.85958	
32	4.0831-02	2.8130+01	0.98590	0.95348	0.94241	0.96610	1.05090	0.90634	
33	4.5637-02	2.9204+01	0.98795	0.96221	0.96187	0.97420	1.02580	0.93826	
34	5.0635-02	3.0140+01	0.99001	0.97115	0.97604	0.98130	1.01080	0.96112	
35	5.5994-02	3.0941+01	0.99236	0.97922	0.98978	0.98780	0.99600	0.98419	
36	6.1024-02	3.1034+01	0.99442	0.98388	0.99063	0.99030	0.99930	0.98546	
37	6.6154-02	3.1646+01	0.99667	0.99085	1.00092	0.99550	0.99000	1.00221	
38	7.1387-02	3.1637+01	0.99736	0.99209	1.00036	0.99610	0.99150	1.00198	
39	7.6035-02	3.1642+01	0.99667	0.99625	1.00045	0.99820	0.99950	0.99937	
40	8.1445-02	3.1614+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
41	8.6500-02	3.1544+01	1.00470	0.99947	0.99920	0.99970	1.00100	1.00340	
42	9.1681-02	3.1398+01	1.02419	1.00220	0.99652	1.00050	1.00800	1.01657	
43	9.3891-02	3.1300+01	1.03349	1.00375	0.99495	1.00100	1.01220	1.02206	
44	9.6787-02	3.1294+01	1.02429	1.00378	0.99495	1.00100	1.01240	1.01275	
45	9.8361-02	3.1377+01	1.01743	1.00412	0.99618	1.00140	1.01090	1.00827	
46	1.0288-01	3.1343+01	1.07869	1.00391	0.99564	1.00120	1.01120	1.01852	

INPUT VARIABLES Y,U/UD,T/TO,P/PH

axisymmetric 	M : 7.4 R THETA X 10 ⁻³ : 20 - 60 TW / TR : 0.32 - 0.47	7203
		ZPG (FPG) - SHT
Axis-symmetric contoured nozzle. Running time 2-3 minutes. D = 1.07, L = 10 m. 1.2 < PO < 5.7 MN/m ² . 700 < TO < 1050 K. Air, dewpoint 205 K. 1.5 < RE/m X 10 ⁻⁶ < 14.		
HOPKINS E.J. and KEENER E.R. 1972 Pressure gradient effects on hypersonic turbulent skin friction and boundary layer profiles. AIAA J. 10, 1141-1142. And private communications. Also Keener & Hopkins (1969, 1973)		

- 1 The test boundary layer was formed on the wall of an axisymmetric tunnel fed by a contoured nozzle. A selection from the full nozzle contour geometrical data is given in Table 1, from which it may be seen that the test section is slightly divergent. The test station was 10.13 m downstream of the throat, which was uncooled. The surface finish was smooth to 0.8 μ m. The test section flow was surveyed with Pitot rakes and 'was not entirely uniform but relatively so for this type of facility'. No observations were made to determine position of natural transition. The tests were made under ZPG or near ZPG conditions 2.7 m downstream of the start of the test section, after the nozzle expansion, predominately simple wave, was complete. (The downstream part of the throat was probably actively cooled, keeping the wall temperature in the region of 300 - 350 K.)
- 2 An instrumentation panel about 0.3 m long carried all the measuring equipment. A row of static holes was drilled at 25.4 mm intervals on the centre line and an FEB (Kistler, diameter 12.7 mm) 30.2 mm to one side. The panel and balance conformed to the tunnel wall curvature. Profile measurements were made with rakes mounted 47.8 mm to either side of the static holes and 54 mm behind the centre of the FEB. The pitot rake had 10 CPP of 1.016 mm diameter in the inner 50 mm and 11 CPP of 3.175 mm diameter between y = 50 and 355 mm. The precise positions appear as the y values in section C. The total temperature rake had 5 triply-shielded STP of 6.35 mm diameter, the innermost at y = 25.4 mm and the outermost at y = 357 mm.
- 3 Temperatures needed for the Y values of the Pitot tubes were interpolated from a free-hand fairing of the measured temperatures. In the region between the innermost STP and the wall, total temperatures were taken from the empirical relation

$$(T_0 - T_W) / (T_{0D} - T_W) = (U/U_D)^{1.66}$$
- 4 which had been found to fit the data further out. Real gas corrections for a calorically imperfect thermally perfect diatomic gas were applied to all calculated values. Keyes' viscosity law was used.
- 5 The editors have accepted the authors U/U_D and M/MD data together with the stated values of MD, TD, TW, PD and CF. Some of the MD values represent revised data which differ from the published tabulation. The other values presented in the tables of sections B and C are calculated assuming a diatomic perfect gas. No attempt has been made to allow for real gas effects. Resulting error in static properties stated is negligible, but the tabulated T₀ and P_{T2} values may be up to 3 % in error. The static pressure has been assumed constant through the boundary layer. The boundary layer thickness is such that integrals cannot be evaluated using the axisymmetric correction as in the source paper. They must be found using a full axisymmetric treatment and this has been done here. (See also Kemp & Owen 1972.)
- 6 The fifteen individual profiles presented cover a range of TW/TR values, obtained by varying T_{0D}, and Reynolds numbers, as a result of the T_{0D} variation and four P_{0D} levels. The CF values have not been adjusted to allow for the small difference in X.
- 7 DATA 72030101 - 72031501. P₀ and T₀ (interpolated) profiles. N_X = 1. CF from an FEB.

15 Editors' comments

Apart from its value as an addition to the data available, this experiment is of interest in that it shows upstream history effects. The next entry, CAT 7204, provides a comparison case performed in the same facility and by the same authors, where there are no history effects. It is unfortunate that the thermal history, especially, is not recorded.

The boundary layer was relatively thick, but even so there were no observations closer to the wall than the momentum deficit peak, so that integral values should be treated with some reserve. The T0 profile used is based on measurements at only five points.

The only comparable investigation is that of Jones & Feller (CAT 7002), since other nozzle boundary layer studies such as Fischer et al. (7001) and Beckwith et al. (7105) describe tests which were made in a simple wave cancellation region, where there are normal pressure gradients.

Table 1 Coordinates for the Ames 3.5 Ft. W.T. Nozzle ($M_\infty = 7.4$)

x (m)	y (m)	x (m)	y (m)	x (m)	y (m)
0	0.041602	0.801289	0.153375	6.328562	0.520294
0.030480	0.042824	1.001451	0.182392	7.566172	0.533400
0.060960	0.046147	1.219200	0.213970	8.074182	0.541812
0.091440	0.040475	1.524000	0.257343	8.582162	0.547207
0.161209	0.060564	1.905000	0.306294	9.090172	0.552602
0.234361	0.071171	2.539990	0.372862	9.598182	0.557967
0.353233	0.088422	3.301990	0.430621	10.106223	0.563362
0.453817	0.102992	3.810000	0.458175	10.252222*	0.568757
0.609265	0.125517	4.825990	0.494721		

* - centre of balance element.

CAT 7203 HOPKINS/KEENER BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ *	MD * POD TOD	TU/TR PH/PO* SU *	RLD2K REN2D ND	CF * CO PI2*	H12 H32 H42	H12K H32K D2K	PW TM* UD	PD* TD* TF
72030101 1.0130**+01 -5.3500**+01	7.4200 1.3993**+06 9.7171**+02	0.3492 1.0000 0.0000	6.3273**+03 2.0578**+04 8.8867**+03	9.1200**+04 NM 0.0000**+00	7.6392 1.8631 1.3034	1.3457 1.8436 1.6473**+02	2.3300**+02 3.0700**+02 1.3361**+03	2.3300**+02 8.0900**+01 8.7907**+02
72030201 1.0130**+01 -5.3500**+01	7.4400 2.7191**+06 1.0405**+03	0.3325 1.0000 0.0000	1.0241**+04 3.1759**+04 7.8686**+03	8.4300**+04 NM 0.0000**+00	7.8601 1.8721 1.2901	1.3377 1.8543 1.4314**+02	4.4500**+02 3.1300**+02 1.3850**+03	4.4500**+02 8.6200**+01 9.4125**+02
72030301 1.0130**+01 -5.3500**+01	7.4600 4.0221**+06 1.0929**+03	0.3136 1.0000 0.0000	1.4504**+04 4.2759**+04 7.7577**+03	8.1300**+04 NM 0.0000**+00	7.9989 1.8749 1.2844	1.3339 1.9574 1.4117**+02	6.4700**+02 3.1000**+02 1.4197**+03	6.4700**+02 9.0100**+01 9.8865**+02
72030401 1.0130**+01 -5.3500**+01	7.9500 1.3900**+06 9.1640**+02	0.3656 1.0000 0.0000	4.7640**+03 1.6777**+04 7.0034**+03	8.8600**+04 NM 0.0000**+00	10.7005 1.8547 1.1220	1.3634 1.8362 1.5054**+02	2.0700**+02 3.0300**+02 1.3013**+03	2.0700**+02 7.3900**+01 8.2878**+02
72030501 1.0130**+01 -5.3500**+01	7.4000 1.4225**+06 8.3066**+02	0.4098 1.0000 0.0000	4.7825**+03 1.8131**+04 6.0505**+03	8.0800**+04 NM 0.0000**+00	12.4602 1.8579 0.9775	1.3651 1.8390 1.3637**+02	2.4100**+02 3.0400**+02 1.2369**+03	2.4100**+02 6.9500**+01 7.5150**+02
72030601 1.0130**+01 -5.3500**+01	7.5900 2.8623**+06 8.9330**+02	0.3829 1.0000 0.0000	7.8340**+03 2.9014**+04 5.7616**+03	7.8200**+04 NM 0.0000**+00	12.2072 1.8665 1.0299	1.3548 1.8494 1.2707**+02	4.1200**+02 3.1000**+02 1.2868**+03	4.1200**+02 7.1500**+01 8.0962**+02
72030701 1.0130**+01 -5.3500**+01	7.4700 2.7339**+06 9.7160**+02	0.3550 1.0000 0.0000	8.8087**+03 2.9362**+04 6.6077**+03	7.9700**+04 NM 0.0000**+00	9.9050 1.8666 1.1560	1.3497 1.8499 1.3266**+02	4.3600**+02 3.1200**+02 1.3388**+03	4.3600**+02 7.9900**+01 8.7866**+02
72030801 1.0130**+01 -5.3500**+01	7.4700 4.1447**+06 8.0014**+02	0.4283 1.0000 0.0000	1.1745**+04 4.7266**+04 5.2478**+03	6.7000**+04 NM 0.0000**+00	12.7354 1.8709 0.9693	1.3560 1.8337 1.1718**+02	6.6100**+02 3.1000**+02 1.2149**+03	6.6100**+02 8.5800**+01 7.2377**+02
72030901 1.0130**+01 -5.3500**+01	7.4900 4.2739**+06 7.7231**+02	0.4323 1.0000 0.0000	1.2622**+04 5.1844**+04 5.3305**+03	6.8400**+04 NM 0.0000**+00	12.3232 1.8748 1.0002	1.3492 1.8587 1.1580**+02	6.7000**+02 3.0200**+02 1.1939**+03	6.7000**+02 6.3200**+01 6.9856**+02
72031001 1.0130**+01 -5.3500**+01	7.4700 4.0883**+06 9.4241**+02	0.3625 1.0000 0.0000	1.5467**+04 5.2744**+04 7.5848**+03	7.3300**+04 NM 0.0000**+00	8.4755 1.8731 1.2568	1.3368 1.8544 1.4365**+02	6.5200**+02 3.0900**+02 1.3185**+03	6.5200**+02 7.7500**+01 8.5246**+02
72031101 1.0130**+01 -5.3500**+01	7.4900 5.4477**+06 8.9695**+02	0.3899 1.0000 0.0000	1.4605**+04 5.3472**+04 5.3988**+03	7.1200**+04 NM 0.0000**+00	11.5854 1.8746 1.0473	1.3531 1.8577 1.1352**+02	8.5400**+02 3.1600**+02 1.2866**+03	8.5400**+02 7.3400**+01 8.1130**+02
72031201 1.0130**+01 -5.3500**+01	7.3900 1.4395**+06 7.2011**+02	0.4635 1.0000 0.0000	4.5329**+03 1.9486**+04 5.1659**+03	7.1400**+04 NM 0.0000**+00	15.2925 1.8642 0.7878	1.3600 1.8457 1.2906**+02	2.4600**+02 3.0200**+02 1.1515**+03	2.4600**+02 6.0400**+01 6.5150**+02
72031301 1.0130**+01 -5.3500**+01	7.5400 2.8562**+06 7.7438**+02	0.4498 1.0000 0.0000	7.3040**+03 3.1283**+04 4.9189**+03	7.2600**+04 NM 0.0000**+00	14.1666 1.8682 0.8912	1.3604 1.8514 1.1614**+02	4.2900**+02 3.1500**+02 1.1961**+03	4.2900**+02 8.2600**+01 7.0036**+02
72031401 1.0130**+01 -5.3500**+01	7.5000 5.5847**+06 7.6072**+02	0.4476 1.0000 0.0000	1.3133**+04 5.4748**+04 4.3033**+03	6.5000**+04 NM 0.0000**+00	15.3739 1.8709 0.7458	1.3637 1.8474 1.0396**+02	8.6800**+02 3.0800**+02 1.1850**+03	8.6800**+02 6.2100**+01 6.8807**+02
72031501 1.0130**+01 -5.3500**+01	7.4800 5.3023**+06 7.5335**+02	0.4637 1.0000 0.0000	1.4077**+04 6.1222**+04 4.6932**+03	6.3000**+04 NM 0.0000**+00	13.5947 1.8769 0.9148	1.3560 1.8588 1.0725**+02	8.7000**+02 3.1600**+02 1.1790**+03	8.7000**+02 6.1800**+01 6.8143**+02

72030301		HOPKINS/KEENER		PROFILE TABULATION		19 POINTS, DELTA AT POINT 19			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.26364	0.00000	0.00000	3.44062	0.00000	
2	4.9500 ⁻ -03	1.1206 ⁺ +01	NM	0.65506	0.38700	0.66800	2.97941	0.22421	
3	9.6500 ⁻ -03	1.3720 ⁺ +01	NM	0.59701	0.43000	0.71500	2.76487	0.25080	
4	1.4990 ⁻ -02	1.6231 ⁺ +01	NM	0.73472	0.46900	0.75400	2.58462	0.29173	
5	2.0070 ⁻ -02	1.8382 ⁺ +01	NM	0.76081	0.50000	0.78100	2.43984	0.32010	
6	2.5400 ⁻ -02	2.0444 ⁺ +01	NM	0.78428	0.52800	0.80400	2.31670	0.34675	
7	3.0480 ⁻ -02	2.2271 ⁺ +01	NM	0.78983	0.55100	0.81500	2.16782	0.37252	
8	3.5560 ⁻ -02	2.4075 ⁺ +01	NM	0.80061	0.57400	0.82800	2.08083	0.39792	
9	4.0640 ⁻ -02	2.5409 ⁺ +01	NM	0.80873	0.59000	0.83700	2.01255	0.41589	
10	4.5470 ⁻ -02	2.7041 ⁺ +01	NM	0.81773	0.60900	0.84700	1.93434	0.43788	
11	5.0550 ⁻ -02	2.8815 ⁺ +01	NM	0.82501	0.62900	0.85600	1.85202	0.46220	
12	6.3250 ⁻ -02	3.3015 ⁺ +01	NM	0.84916	0.67400	0.87900	1.70082	0.51681	
13	8.8650 ⁻ -02	4.2777 ⁺ +01	NM	0.88522	0.76800	0.91500	1.41945	0.64462	
14	1.1405 ⁻ -01	5.2355 ⁺ +01	NM	0.92106	0.85100	0.94500	1.23312	0.76635	
15	1.3945 ⁻ -01	6.0807 ⁺ +01	NM	0.94948	0.91800	0.96700	1.10960	0.87148	
16	1.6485 ⁻ -01	6.4300 ⁺ +01	NM	0.97077	0.97300	0.98300	1.02066	0.96310	
17	1.9025 ⁻ -01	7.1545 ⁺ +01	NM	0.98273	0.99600	0.99100	0.98999	1.00103	
18	2.1565 ⁻ -01	7.1687 ⁺ +01	NM	0.99450	0.99700	0.99700	1.00000	0.99700	
D 19	2.4105 ⁻ -01	7.2117 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/MD

ASSUME P=PD

72030501		HOPKINS/KEENER		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.37079	0.00000	0.00000	4.43165	0.00000	
2	4.9500 ⁻ -03	1.9815 ⁺ +00	NM	0.69048	0.33900	0.64800	3.65385	0.17735	
3	9.6500 ⁻ -03	1.0710 ⁺ +01	NM	0.73352	0.38100	0.70100	3.38521	0.20708	
4	1.4990 ⁻ -02	1.2210 ⁺ +01	NM	0.75823	0.40800	0.73100	3.21007	0.22772	
5	2.0070 ⁻ -02	1.3997 ⁺ +01	NM	0.78324	0.43800	0.76100	3.01471	0.25209	
6	2.5400 ⁻ -02	1.5454 ⁺ +01	NM	0.80111	0.46100	0.78200	2.87748	0.27177	
7	3.0480 ⁻ -02	1.7054 ⁺ +01	NM	0.81613	0.48500	0.80100	2.72761	0.29366	
8	3.5560 ⁻ -02	1.8449 ⁺ +01	NM	0.82657	0.50500	0.81500	2.60455	0.31291	
9	4.0640 ⁻ -02	1.9827 ⁺ +01	NM	0.83713	0.52400	0.82800	2.49688	0.33161	
10	4.5470 ⁻ -02	2.1179 ⁺ +01	NM	0.84551	0.54200	0.83900	2.39621	0.35014	
11	5.0550 ⁻ -02	2.2736 ⁺ +01	NM	0.85545	0.56200	0.85100	2.29291	0.37114	
12	6.3250 ⁻ -02	2.6873 ⁺ +01	NM	0.87654	0.61200	0.87700	2.05351	0.42707	
13	8.8650 ⁻ -02	3.5012 ⁺ +01	NM	0.91811	0.70000	0.91900	1.72359	0.53319	
14	1.1405 ⁻ -01	4.5025 ⁺ +01	NM	0.95245	0.79500	0.95300	1.43698	0.66320	
15	1.3945 ⁻ -01	5.8082 ⁺ +01	NM	0.97837	0.90700	0.98000	1.17521	0.83389	
16	1.6485 ⁻ -01	6.3693 ⁺ +01	NM	0.98954	0.94700	0.99000	1.09287	0.90587	
17	1.9025 ⁻ -01	6.9426 ⁺ +01	NM	0.99387	0.98900	0.99600	1.01421	0.98205	
D 18	2.1565 ⁻ -01	7.0969 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	


INPUT VARIABLES Y,U/UD,M/MD

ASSUME P=PD

72031401		HOPKINS/KEENER		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.40488	0.00000	0.00000	4.45974	0.00000	
2	4.9500 ⁻ -03	1.0072 ⁺ +01	NM	0.74546	0.36400	0.69700	3.66659	0.19009	
3	9.6500 ⁻ -03	1.2588 ⁺ +01	NM	0.78687	0.40900	0.74800	3.34470	0.22364	
4	1.4990 ⁻ -02	1.4941 ⁺ +01	NM	0.81960	0.44700	0.78400	3.07622	0.25486	
5	2.0070 ⁻ -02	1.6879 ⁺ +01	NM	0.83686	0.47600	0.80900	2.88857	0.28007	
6	2.5400 ⁻ -02	1.8792 ⁺ +01	NM	0.85493	0.50300	0.83000	2.72283	0.30483	
7	3.0480 ⁻ -02	2.0582 ⁺ +01	NM	0.86152	0.52700	0.84300	2.58879	0.32985	
8	3.5560 ⁻ -02	2.2216 ⁺ +01	NM	0.87210	0.54800	0.85600	2.43998	0.35082	
9	4.0640 ⁻ -02	2.3832 ⁺ +01	NM	0.88052	0.56800	0.86700	2.32492	0.37212	
10	4.5470 ⁻ -02	2.5506 ⁺ +01	NM	0.88794	0.58800	0.87700	2.22456	0.39423	
11	5.0550 ⁻ -02	2.7503 ⁺ +01	NM	0.89862	0.61100	0.88900	2.11700	0.41993	
12	6.3250 ⁻ -02	2.3098 ⁺ +01	NM	0.97683	0.55900	0.91000	2.65008	0.34339	
13	8.8650 ⁻ -02	4.3293 ⁺ +01	NM	0.95140	0.76900	0.94900	1.52291	0.62314	
14	1.1405 ⁻ -01	5.5660 ⁺ +01	NM	0.98085	0.87300	0.97800	1.25562	0.77927	
15	1.3945 ⁻ -01	6.6793 ⁺ +01	NM	1.00146	0.95700	0.99700	1.08534	0.91860	
D 16	1.6485 ⁻ -01	7.2887 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,M/MD

ASSUME P=PD

	M : 6.2 - 6.5 R THETA X 10 ⁻³ : 2 - 7 TW / TR : 0.32 - 0.51	7204
		ZPG - MHT - SHT
Axisymmetric blow down tunnel. Running time 2-3 minutes. D = 1.07 m. 3.8 < PO < 6.7 MN/m ² . 680 < TO < 1100 K. Air, dew point 205 K. 5 < RE/m X 10 ⁻⁶ < 14.		
KEENER E.R. and HOPKINS E.J. 1972 Turbulent boundary layer velocity profiles on a non-adiabatic flat plate at Mach number 6.5 NASA TN D-6907. And Hopkins, Keener and Louie (1970), Keener and Hopkins (1969), private communications.		

- 1 The test boundary layer was formed on a flat plate (W = 0.457, L = 1.22 m) mounted on a sting at 3° negative incidence in the wind tunnel used for CAT 7203. The leading edge (X = 0) was chamfered at 23° with an average edge thickness of 0.13 mm. The surface of the plate was smooth to 0.8 μm. A row of boundary layer trip elements 1.65 mm high could be mounted at 19 mm (typical) intervals on the line X = 100 mm. In plan view these were symmetrical pentagons with a triangular front and rectangular back, 7.1 mm long overall and 6.4 mm wide. The triangular portion was 4.8 mm long. Surveys were made at a single test station with X = 965 to 996 mm. The plate cooling system maintained
- 2 the surface temperature constant to within 30 K in the central region. Surface pressures were "not as uniform as expected for a flat plate", varying by about 10 % which corresponds to 1.5 % in MD at this
- 3 Mach number. The sublimation technique was used to detect transition, which in all cases is complete upstream of the measuring station (figure 5, source). There were noticeable differences between boundary layers with forced and with natural transition.
- 6 Surface pressures were measured at close intervals (20 mm, E) along the centre line, surface temperature
- 8 at a single point, 16 mm off the centre line at X = 989 mm, and surface shear stress, 45.7 mm off at X = 965 mm, by a FEB (Kistler, diameter of element 9.4 mm). A cooling system was provided to keep the
- 7 electrical components of the balance below 370 K. The boundary layer profiles were surveyed simultaneously by a FPP, a flattened STP and a CCP mounted on a single traverse gear giving a profile normal at X = 996 mm.
- 8 The three probes registered at, respectively, 19.0, 24.7 and 29.8 mm off the centre line. The TTP was constructed from platinum tubing (1.02 mm OD with wall thickness 0.1 mm) flattened to give an opening with h₂ = 0.15 mm and ground so that h₁ = 0.25 mm. A platinum / platinum-rhodium thermocouple was mounted about 5 mm back from the opening with a 0.25 mm diameter vent hole 5.6 mm back on the top surface. The FPP was formed in the same manner from tube 0.76 mm in diameter, again with h₁ = 0.25, h₂ = 0.15 mm. The CCP was 1.02 mm in diameter, but was not used. The TTP and TPP were bent down so as to be able to come close to the plate surface.
- 9 Total temperature profiles were taken for three of the cases presented (0101, 0201, 0401). The values fitted the relationship.
$$U/UD = (T0 - TW) / (T0D - TW)$$

within the margin of experimental error, and this relationship was used for all profiles in reduction.
- 10 The air was treated as a calorically imperfect, thermally perfect, diatomic gas and Keyes' viscosity law
- 11 was used.
- 12 The editors have reduced the data using the same assumptions and simplifications as for CAT 7203. The
- 13 profiles presented form three pairs, each specified by a TU/TR value. In each pair, one profile (0201,
- 14 0401, 0601) was obtained with the boundary layer trips on, and the other with natural transition. No adjustment has been made for the small X difference of the CF value obtained from the FEB balance.
- 9 DATA. 72040101-0601. PO and (3) TO profiles. NX = 1. CF from balance.

15 Editors' comments

This experiment provides a reference case, with no upstream history, for comparison with the previous entry (CAT 7203). The authors compare the temperature velocity correlations obtained, and find the marked difference displayed by the two equations quoted in § 9 for each case.

The profiles were relatively "short" and the measurements did not extend within the momentum-deficit peak, so that it is not advisable to place too great a reliance on values of the integral parameters. (The authors suggest a tolerance of 8 %). Comparisons may be made with the results of Danberg (CAT 6702), Samuels et al. (6701), and with possible small history effects, Horstman & Owen (CAT 7205).

CAT 7204		KEENER/HOPKINS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN X ° RZ	MD * POD TOD	TW/TR PW/PD* SW * DZ	REN2W REN2D	CF * CQ P12*	H12 H32 H42	H12K H32K D2K	PW TW* UD	PO* TD* TR		
72040101 9.9600*-01 INFINITE	6.2100 2.2647*+06 1.0717*+03	0.3330 1.0000 0.0000	1.0662*+03 2.4161*+03 4.6174*-04	1.5600*-03 NM 0.0000*+00	11.6676 1.9035 0.7330	1.9071 1.8892 8.1643*-04	1.1600*+03 3.2400*+02 1.3809*+03	1.1600*+03 1.2300*+02 9.7301*+02		
72040201 9.9600*-01 INFINITE	6.3900 4.3372*+06 1.1458*+03	0.3136 1.0000 0.0000	2.2811*+03 5.1160*+03 6.0639*-04	1.2200*-03 NM 0.0000*+00	11.6544 1.8641 0.7554	1.6167 1.8423 1.2605*-03	1.8600*+03 3.2600*+02 1.4324*+03	1.8600*+03 1.2500*+02 1.0396*+03		
72040301 9.9600*-01 INFINITE	6.4200 2.7371*+06 7.8569*+02	0.4377 1.0000 0.0000	1.4209*+03 4.4565*+03 4.8922*-04	1.2300*-03 NM 0.0000*+00	13.4564 1.8876 0.6269	1.8011 1.8690 1.0076*-03	1.1400*+03 3.1200*+02 1.1867*+03	1.1400*+03 8.5000*+01 7.1281*+02		
72040401 9.9600*-01 INFINITE	6.4200 1.6567*+06 8.0417*+02	0.4194 1.0000 0.0000	1.2470*+03 3.7665*+03 7.0706*-04	1.2500*-03 NM 0.0000*+00	12.9200 1.8807 0.6445	1.6096 1.8593 1.4824*-03	6.9000*+02 3.0600*+02 1.2006*+03	6.9000*+02 8.7000*+01 7.2956*+02		
72040501 9.9600*-01 INFINITE	6.5000 3.4503*+06 6.8985*+02	0.5082 1.0000 0.0000	1.7931*+03 6.6526*+03 4.9145*-04	1.0600*-03 NM 0.0000*+00	14.1756 1.8743 0.5616	1.6019 1.8504 1.1182*-03	1.3500*+03 3.1800*+02 1.1135*+03	1.3500*+03 7.3000*+01 6.2570*+02		
72040601 9.9600*-01 INFINITE	6.5000 3.4503*+06 6.9430*+02	0.5014 1.0000 0.0000	2.3441*+03 8.5540*+03 6.4684*-04	1.0000*-03 NM 0.0000*+00	13.8981 1.8552 0.5689	1.4829 1.8258 1.5691*-03	1.3300*+03 3.1800*+02 1.1211*+03	1.3300*+03 7.4000*+01 6.3427*+02		

72040201		KEENER/HOPKINS		PROFILE TABULATION		18 POINTS, DELTA AT POINT 18			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.28452	0.00000	0.00000	2.50000	0.00000	
2	1.7000 ⁻ 03	1.1147 ⁺ 01	NM	0.81739	0.45057	0.75650	2.81900	0.20836	
3	2.8000 ⁻ 03	1.3983 ⁺ 01	NM	0.85326	0.50695	0.80540	2.52400	0.31910	
4	4.0000 ⁻ 03	1.6251 ⁺ 01	NM	0.87581	0.54789	0.83560	2.32600	0.35924	
5	4.7000 ⁻ 03	1.8885 ⁺ 01	NM	0.89629	0.59187	0.86340	2.12800	0.40573	
6	5.2000 ⁻ 03	2.0170 ⁺ 01	NM	0.90498	0.61217	0.87500	2.04300	0.42829	
7	6.4000 ⁻ 03	2.3503 ⁺ 01	NM	0.92453	0.66196	0.90060	1.85100	0.48655	
8	6.8000 ⁻ 03	2.4721 ⁺ 01	NM	0.93050	0.67923	0.90850	1.78900	0.50783	
9	7.7000 ⁻ 03	2.7310 ⁺ 01	NM	0.94200	0.71463	0.92350	1.67000	0.55299	
10	9.1000 ⁻ 03	3.1044 ⁺ 01	NM	0.95537	0.76266	0.94120	1.52300	0.61799	
11	9.4000 ⁻ 03	3.2359 ⁺ 01	NM	0.95943	0.77889	0.94660	1.47700	0.64089	
12	1.0100 ⁻ 02	3.4102 ⁺ 01	NM	0.96461	0.80036	0.95340	1.41900	0.67188	
13	1.0600 ⁻ 02	3.6105 ⁺ 01	NM	0.96977	0.82336	0.96020	1.36000	0.70603	
14	1.1200 ⁻ 02	3.8243 ⁺ 01	NM	0.97484	0.84770	0.96690	1.30100	0.74320	
15	1.2500 ⁻ 02	4.2966 ⁺ 01	NM	0.98442	0.89913	0.97960	1.18700	0.82527	
16	1.3000 ⁻ 02	4.4269 ⁺ 01	NM	0.98679	0.91281	0.98270	1.15900	0.84789	
17	1.4600 ⁻ 02	4.8417 ⁺ 01	NM	0.99360	0.95505	0.99160	1.07800	0.91955	
D 18	1.7800 ⁻ 02	5.3036 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD

ASSUME P=PD

72040501		KEENER/HOPKINS		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.46095	0.00000	0.00000	4.35000	0.00000	
2	1.4000 ⁻ 03	1.0107 ⁺ 01	NM	0.86715	0.42077	0.76240	3.28300	0.23223	
3	2.8000 ⁻ 03	1.3116 ⁺ 01	NM	0.89612	0.48211	0.81490	2.85700	0.28523	
4	4.0000 ⁻ 03	1.5645 ⁺ 01	NM	0.91407	0.52816	0.84720	2.57300	0.32927	
5	5.5000 ⁻ 03	2.0507 ⁺ 01	NM	0.93876	0.60694	0.89140	2.15700	0.41326	
6	6.4000 ⁻ 03	2.3153 ⁺ 01	NM	0.94886	0.64621	0.90930	1.98000	0.45924	
7	7.6000 ⁻ 03	2.7214 ⁺ 01	NM	0.96116	0.70122	0.93050	1.76200	0.52826	
8	8.9000 ⁻ 03	3.2030 ⁺ 01	NM	0.97199	0.76175	0.95020	1.55600	0.61067	
9	1.0200 ⁻ 02	3.6845 ⁺ 01	NM	0.98044	0.81779	0.96520	1.39300	0.69299	
10	1.1600 ⁻ 02	4.2844 ⁺ 01	NM	0.98862	0.88265	0.97970	1.23200	0.79521	
11	1.2500 ⁻ 02	4.6299 ⁺ 01	NM	0.99242	0.91792	0.98650	1.15500	0.85411	
12	1.4100 ⁻ 02	5.0186 ⁺ 01	NM	0.99606	0.95605	0.99310	1.07900	0.92039	
13	1.5500 ⁻ 02	5.2465 ⁺ 01	NM	0.99806	0.97772	0.99660	1.03900	0.95990	
14	1.6300 ⁻ 02	5.3677 ⁺ 01	NM	0.99915	0.98905	0.99840	1.01900	0.97978	
15	1.6800 ⁻ 02	5.3982 ⁺ 01	NM	0.99934	0.99188	0.99880	1.01400	0.98501	
D 16	1.9500 ⁻ 02	5.4862 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	


INPUT VARIABLES Y,U/UD,T/TD

ASSUME P=PD

72040601		KEENER/HOPKINS		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PT2/P	P/PO	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.45471	0.00000	0.00000	4.29700	0.00000	
2	1.2000 ⁻ 03	7.9100 ⁺ 00	NM	0.83472	0.36950	0.70720	3.66200	0.19312	
3	2.5000 ⁻ 03	1.9030 ⁺ 01	NM	0.86404	0.41908	0.75980	3.28700	0.23115	
4	3.6000 ⁻ 03	1.1415 ⁺ 01	NM	0.87901	0.44848	0.78670	3.07700	0.25567	
5	5.1000 ⁻ 03	1.4839 ⁺ 01	NM	0.90733	0.51394	0.83710	2.65300	0.31553	
6	6.0000 ⁻ 03	1.6757 ⁺ 01	NM	0.91930	0.54718	0.85840	2.46100	0.34880	
7	7.4000 ⁻ 03	1.9621 ⁺ 01	NM	0.93384	0.59337	0.88410	2.22000	0.39824	
8	8.6000 ⁻ 03	2.2779 ⁺ 01	NM	0.94656	0.64044	0.90640	2.00300	0.45252	
9	9.8000 ⁻ 03	2.6529 ⁺ 01	NM	0.95840	0.69217	0.92710	1.79400	0.51678	
10	1.1300 ⁻ 02	3.0930 ⁺ 01	NM	0.96932	0.74835	0.94600	1.59800	0.54199	
11	1.2600 ⁻ 02	3.3761 ⁺ 01	NM	0.97824	0.80551	0.96190	1.42600	0.67454	
12	1.3700 ⁻ 02	3.9368 ⁺ 01	NM	0.98379	0.84567	0.97160	1.32000	0.73606	
13	1.4900 ⁻ 02	4.3516 ⁺ 01	NM	0.98920	0.88962	0.98100	1.21600	0.80674	
14	1.7600 ⁻ 02	5.1677 ⁺ 01	NM	0.99686	0.96458	0.99450	1.06300	0.93556	
15	2.2500 ⁻ 02	5.4291 ⁺ 01	NM	0.99952	0.99473	0.99920	1.00900	0.99029	
D 16	2.5200 ⁻ 02	5.4862 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD

ASSUME P=PD

 <p>axisymmetric</p>	<p>M : 7.2</p> <p>R THETA X 10⁻³ : 6 - 13</p> <p>TW / TR : 0.5</p>	<p>7205</p>
		<p>ZPG - SHT</p>
<p>Blow-down axisymmetric wind tunnel. Useful running time 2 minutes. D = 1.07 m. PO : 3.5 MN/m². TO : 667 K. Air, dew point 205 K. RE/m X 10⁻⁶ : 11.</p>		
<p>HORSTMAN C.C. and OWEN F.K. 1972 Turbulent properties of a compressible boundary layer. AIAA Jour. 10. 1418-1424. And Horstman, C.C., private communications, Owen & Horstman (1974), Owen et al. (1975).</p>		

- 1 The test boundary layer was formed on a 10° semi-apex angle cone-on-cylinder 3.30 m long and 205 mm in diameter with a shoulder fairing radius of 810 mm. The model was mounted on the centre-line of the tunnel used for CAT 7203/7204. All measurements were made on the parallel portion downstream of the tangent point at X = 647 mm (X = 0 at the nose). The model surface was finished to 1.0 μm. It was not actively cooled, the wall temperature in the test zone rising by 10 K during a run, which was always less than a minute,
- 2 while the temperature of the nose-cone rose by about 40 K. The wind tunnel Mach number and total temperature were uniform to within ± 0.05 and ± 3 % respectively over a 0.9 m core, in which the stream angles had a maximum deflection of 0.5°.
- 3 Natural transition was detected by a hot wire close to the model surface, following Owen (1970), starting and finishing at X = 370 and 800 mm respectively. The development of the flow over the surface of the model is presented in table 1. The pressure gradient in the test zone (1/p)dp/dx was - 4 %/m. Model alignment was checked by surface pressure and heat transfer measurements at 90° intervals round the model, and skin friction measurements 180° apart. Circumferential variations were within the accuracy of measurement.
- 6 The surface pressure, wall shear stress and heat transfer were obtained along the cylindrical portion of the model from X = 0.85 to 2.37 m. The wall shear stress was measured directly using a contoured floating-element balance. Direct calibrations using weights hung from the sensing element were performed before and after each test series. These calibrations were repeatable to within 5 %. The heat transfer rate was measured using the thin-wall transient technique. Lateral and radial conduction errors were computed and found to be less than 5 % of the convective heat transfer. Pitot pressure and total temperature profiles were obtained at X = 1.15, 1.76 and 2.37 m. To provide reliable mean flow profiles extra care was taken to use flow field instrumentation which required little or no experimental correction. Single probes were traversed through the boundary layer, stopping every few seconds to ensure no time lag in pressure or temperature. Pitot pressure was measured with an FPP (h₁ = 0.75, h₂ = 0.65, b₁ = 1.9, b₂ = 1.8 mm). Independent calibrations in a free-jet facility, matching Mach number, velocity and density with the present test conditions indicated that rarefaction effects were less than 0.5 %. The minimum local probe Reynolds number based on conditions behind the normal shock and probe height was 60. The Pitot probe height was less than 4.5 % of the smallest boundary-layer thickness traversed.
- 7 Total temperature profiles were obtained using two types of probes; a single shielded chromel-alumel probe 1.4 mm in diameter was used in the outer 90 % of the boundary layer and an unshielded butt-welded chromel-alumel wire 3 mm long by 0.07 mm thick was used close to the wall. Independent calibrations of these probes in a free-jet facility, matching test conditions, indicated a maximum total temperature error of 2 % for the shielded probe and 5 % for the unshielded probe. Corrections were only applied to the unshielded probe. For portions of the boundary layer where measurements with both probes were taken the corrected data agreed to within 2 %. The shielded probe diameter was less than 5 % of the smallest boundary-layer thickness traversed. The caloric imperfections of air were taken into account in data reduction.
- 7 The fluctuating properties of the layer were measured with a constant temperature HWP and the results presented in Owen & Hartmann (1972). A comparison between these observations and later surveys made using a constant current HWP is made in Owen & Horstman (1974) and Owen et al. (1975). The CC-HWP data

were taken at slightly different free stream conditions. The data was reduced assuming that the signal was not affected by pressure fluctuations. A sample profile is given in section D. The mean turbulent shear flow was analysed in Horstman & Owen 1972. A tabulation of certain of these quantities is given in section D. The three total temperature profiles, scaled on δ (table 1) were indistinguishable and the mean T0 profile has been used for all three profiles presented. The static pressure has been assumed constant through the layer. The CF value for $X = 1.15$ m is an interpolation of values measured at $X = 0.85$ and 1.46 m. The CF values presented are averaged from the measurements on either side of the model at each X station. The editors have accepted the data as presented by the authors.

5 DATA: 7205 0101-0103. Pitot and T0 profiles separately. NX = 3 CF from a number of FEB and CQ by the transient technique separately. Hot wire measurements.

15 Editors' comments

This experiment is very fully and accessibly reported. We suggest that recourse should be had to the original papers, particularly for a treatment of the turbulence quantities which we have not discussed in any detail here.

The experimental range is small, but the coverage of that range is exceptionally complete. This is the only case we have found in which, for one set of conditions, the mean flow profile information is complete, both wall shear stress and heat flux have been measured, and significant information on the fluctuating quantities is provided. Additionally there is a high probability that there are not significant history effects.

The same model and test conditions were used by Mikulla & Horstman (1975) for pioneer Reynolds stress measurements using fine wires mounted on the leading edges of thin ceramic wedges.

Data for boundary layers in broadly the same experimental range may be found in Keener & Hopkins - CAT 7204, Danberg - CAT 6702, and Samuels et al. - CAT 6701.

TABLE 1: BOUNDARY LAYER HISTORY

X (m)	UD/UR	HD/MR	RHOD/RHOR	(RED/m)/ (RER/m)	δ (mm)
0.00	0.975	0.795	2.39	1.54	-
0.20	0.975	0.795	2.39	1.54	-
0.40	0.975	0.795	2.39	1.54	-
0.60	0.995	0.945	1.12	0.96	-
0.80	1.00	1.017	0.79	0.81	-
1.00	1.00	1.005	0.85	0.85	15.0
1.20	1.00	1.000	0.83	0.825	17.6
1.40	1.00	1.000	0.83	0.815	20.2
1.60	1.00	0.995	0.82	0.805	22.8
1.80	1.00	0.990	0.81	0.80	25.5
2.00	1.00	0.985	0.795	0.78	28.2
2.20	1.00	0.980	0.78	0.76	30.8
2.40	1.00	0.975	0.765	0.74	33.5

REFERENCE VALUES:

MR = 7.2 TOR = 667 K TW = 310 K UR = 1110 m/s RER/m = 10.9

The boundary layer edge, δ , is defined as that point at which PO/POR = 0.99.

CAT 7205

HORSTMAN

BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUN X * RZ *	MD * POD TOD	TW/TR PW/PD* SW * D2	REDZW REDZD D2	CF * CO * PI2*	M12 M32 M42	M12K M32K D2K	PW TW* UD	PD* TD* TR
72050101 1.1500 ⁺⁰⁰ 1.0150 ⁻⁰¹	7.2000 3.3777 ⁺⁰⁶ 6.7071 ⁺⁰²	0.5035 1.0000 0.0000	1.3951 ⁺⁰³ 4.1983 ⁺⁰³ 5.8730 ⁻⁰⁴	9.0000 ⁻⁰⁴ 2.2328 ⁻⁰⁴ -2.6755 ⁻⁰⁶	14.3126 1.8191 0.7473	1.5630 1.7505 1.6545 ⁻⁰³	6.8192 ⁺⁰² 3.0570 ⁺⁰² 1.1088 ⁺⁰³	6.8192 ⁺⁰² 5.9000 ⁺⁰¹ 6.0709 ⁺⁰²
72050102 1.7600 ⁺⁰⁰ 1.0150 ⁻⁰¹	7.2000 3.3777 ⁺⁰⁶ 6.7071 ⁺⁰²	0.4984 1.0000 0.0000	2.1011 ⁺⁰³ 9.2612 ⁺⁰³ 8.7751 ⁻⁰⁴	8.5000 ⁻⁰⁴ 2.0139 ⁻⁰⁴ -4.2327 ⁻⁰⁶	14.0416 1.8282 0.7078	1.4345 1.7802 2.3232 ⁻⁰³	6.8192 ⁺⁰² 3.0256 ⁺⁰² 1.1088 ⁺⁰³	6.8192 ⁺⁰² 5.9000 ⁺⁰¹ 6.0709 ⁺⁰²
72050103 2.3700 ⁺⁰⁰ 1.0150 ⁻⁰¹	7.2000 3.3777 ⁺⁰⁶ 6.7071 ⁺⁰²	0.4764 1.0000 0.0000	3.0423 ⁺⁰³ 1.2950 ⁺⁰⁴ 1.2271 ⁻⁰³	8.0000 ⁻⁰⁴ 2.1015 ⁻⁰⁴ -6.2887 ⁻⁰⁶	12.2653 1.8303 0.8326	1.3941 1.7755 3.0195 ⁻⁰³	6.8192 ⁺⁰² 2.8922 ⁺⁰² 1.1088 ⁺⁰³	6.8192 ⁺⁰² 5.9000 ⁺⁰¹ 6.0709 ⁺⁰²

TW CHANGED TO BE CONSISTENT WITH RHOH/RHOD

72050101		HURSTMAN		PROFILE TABULATION		16 POINTS, DELTA AT POINT 16			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.45578	0.00000	0.00000	5.18135	0.00000	
2	1.2070 ⁻⁰³	5.0023 ⁺⁰⁰	NM	0.77091	0.25987	0.59000	5.15464	0.11446	
3	1.4960 ⁻⁰³	7.7709 ⁺⁰⁰	NM	0.78484	0.33048	0.67600	4.18410	0.16156	
4	2.0910 ⁻⁰³	1.0301 ⁺⁰¹	NM	0.80226	0.36368	0.72900	3.61011	0.20193	
5	3.0940 ⁻⁰³	1.2772 ⁺⁰¹	NM	0.82591	0.42927	0.77100	3.22581	0.23901	
6	4.7940 ⁻⁰³	1.5847 ⁺⁰¹	NM	0.86152	0.47999	0.81600	2.89017	0.28234	
7	5.7800 ⁻⁰³	1.9091 ⁺⁰¹	NM	0.88256	0.52822	0.84800	2.57732	0.32902	
8	7.4800 ⁻⁰³	2.3887 ⁺⁰¹	NM	0.91274	0.59236	0.88600	2.23714	0.39604	
9	8.5000 ⁻⁰³	2.8366 ⁺⁰¹	NM	0.92544	0.64653	0.90800	1.97239	0.46036	
10	9.8090 ⁻⁰³	3.3770 ⁺⁰¹	NM	0.94941	0.70639	0.93400	1.74825	0.53425	
11	1.1186 ⁻⁰²	4.2988 ⁺⁰¹	NM	0.97384	0.79819	0.96300	1.49560	0.66158	
12	1.2597 ⁻⁰²	5.2025 ⁺⁰¹	NM	0.98327	0.87892	0.97900	1.24069	0.78907	
13	1.3906 ⁻⁰²	5.9697 ⁺⁰¹	NM	0.99705	0.94204	0.99300	1.11111	0.89370	
14	1.5011 ⁻⁰²	6.4359 ⁺⁰¹	NM	0.99591	0.97841	0.99600	1.03627	0.96114	
15	1.6324 ⁻⁰²	6.6608 ⁺⁰¹	NM	1.00080	0.99549	1.00000	1.00908	0.99100	
D 16	1.7000 ⁻⁰²	6.7209 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,RHO/RHOD ASSUME P=PD

72050102		HURSTMAN		PROFILE TABULATION		14 POINTS, DELTA AT POINT 14			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.45111	0.00000	0.00000	5.12821	0.00000	
2	1.2000 ⁻⁰³	4.3314 ⁺⁰⁰	NM	0.75768	0.27480	0.60400	4.83092	0.12503	
3	1.9000 ⁻⁰³	7.2021 ⁺⁰⁰	NM	0.77887	0.36154	0.70100	3.75940	0.18647	
4	3.1000 ⁻⁰³	1.1241 ⁺⁰¹	NM	0.80236	0.40164	0.74200	3.41297	0.21741	
5	5.8000 ⁻⁰³	1.5017 ⁺⁰¹	NM	0.84834	0.46685	0.80300	2.95858	0.27141	
6	8.5000 ⁻⁰³	1.9216 ⁺⁰¹	NM	0.88490	0.53281	0.85100	2.55102	0.33359	
7	1.1200 ⁻⁰²	2.5541 ⁺⁰¹	NM	0.91812	0.61293	0.89500	2.13220	0.41975	
8	1.3400 ⁻⁰²	3.2631 ⁺⁰¹	NM	0.94873	0.69420	0.93100	1.79856	0.51764	
9	1.6525 ⁻⁰²	4.1665 ⁺⁰¹	NM	0.97592	0.78567	0.96200	1.49925	0.64165	
10	1.9200 ⁻⁰²	5.2311 ⁺⁰¹	NM	0.99677	0.88135	0.98600	1.25156	0.78781	
11	2.1925 ⁻⁰²	6.2422 ⁺⁰¹	NM	1.00277	0.96347	0.99800	1.07246	0.93014	
12	2.2600 ⁻⁰²	6.3672 ⁺⁰¹	NM	1.00492	0.97314	1.00000	1.05597	0.94700	
13	2.4625 ⁻⁰²	6.6608 ⁺⁰¹	NM	1.00080	0.99549	1.00000	1.00908	0.99100	
D 14	2.5000 ⁻⁰²	6.7209 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,RHO/RHOD ASSUME P=PD

72050103		HURSTMAN		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.43121	0.00000	0.00000	4.90196	0.00000	
2	1.0890 ⁻⁰³	4.3474 ⁺⁰⁰	NM	0.72433	0.24005	0.54500	5.15464	0.10573	
3	1.6830 ⁻⁰³	7.8871 ⁺⁰⁰	NM	0.75440	0.33300	0.66600	4.00000	0.16650	
4	2.6070 ⁻⁰³	1.0052 ⁺⁰¹	NM	0.77318	0.37877	0.71200	3.53357	0.20150	
5	3.1020 ⁻⁰³	1.0816 ⁺⁰¹	NM	0.77992	0.39365	0.72600	3.40136	0.21344	
6	4.3890 ⁻⁰³	1.2212 ⁺⁰¹	NM	0.79861	0.41937	0.75200	3.21543	0.23387	
7	5.7090 ⁻⁰³	1.3919 ⁺⁰¹	NM	0.81842	0.44886	0.77900	3.01205	0.25863	
8	6.9960 ⁻⁰³	1.5673 ⁺⁰¹	NM	0.83295	0.47725	0.80100	2.81690	0.28435	
9	8.3160 ⁻⁰³	1.7434 ⁺⁰¹	NM	0.84597	0.50415	0.82000	2.64550	0.30996	
10	9.5040 ⁻⁰³	1.9083 ⁺⁰¹	NM	0.85581	0.52810	0.83500	2.50000	0.33400	
11	1.1121 ⁻⁰²	2.1547 ⁺⁰¹	NM	0.87846	0.56197	0.85800	2.33100	0.36806	
12	1.2408 ⁻⁰²	2.3669 ⁺⁰¹	NM	0.89406	0.58959	0.87600	2.20751	0.39683	
13	1.3627 ⁻⁰²	2.6367 ⁺⁰¹	NM	0.89996	0.62293	0.88900	2.03666	0.43650	
14	1.5213 ⁻⁰²	2.9229 ⁺⁰¹	NM	0.91618	0.65646	0.90600	1.90478	0.47565	
15	1.6302 ⁻⁰²	3.1920 ⁺⁰¹	NM	0.92791	0.68649	0.91900	1.79211	0.51280	
16	1.7622 ⁻⁰²	3.4747 ⁺⁰¹	NM	0.94081	0.71710	0.93200	1.68414	0.55174	
17	1.8909 ⁻⁰²	3.8812 ⁺⁰¹	NM	0.95321	0.75798	0.94600	1.55763	0.60733	
18	2.0326 ⁻⁰²	4.2399 ⁺⁰¹	NM	0.96352	0.79264	0.95700	1.45773	0.66650	
19	2.1516 ⁻⁰²	4.6213 ⁺⁰¹	NM	0.97284	0.82790	0.96700	1.36426	0.70881	
20	2.2935 ⁻⁰²	4.9487 ⁺⁰¹	NM	0.98495	0.85676	0.97700	1.30034	0.75131	
21	2.4123 ⁻⁰²	5.3630 ⁺⁰¹	NM	0.99202	0.89250	0.98500	1.21803	0.80869	
22	2.6829 ⁻⁰²	6.0442 ⁺⁰¹	NM	0.99183	0.94795	0.99100	1.09290	0.90676	
23	2.9205 ⁻⁰²	6.3966 ⁺⁰¹	NM	0.99440	0.97540	0.99500	1.04058	0.95620	
24	3.0723 ⁻⁰²	6.4078 ⁺⁰¹	NM	0.99751	0.99149	0.99800	1.01317	0.98503	
25	3.1944 ⁻⁰²	6.6942 ⁺⁰¹	NM	1.00035	0.99800	1.00000	1.00402	0.99600	
D 26	3.5000 ⁻⁰²	6.7209 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,U/UD,RHO/RHOD ASSUME P=PD

SECTION D: SUPPLEMENTARY DATA

D 1. CONSTANT CURRENT HOT WIRE DATA (Owen et al., 1975, figures 8-11)

AUTHORS' SYMBOLS AND UNITS

$X = 224$ cm. $R_{\theta\theta} = 8500$ $T_0 = 667$ K $T_w = 310$ K $\delta = 3.3$ cm $\theta = 0.134$ cm

$\rho_e = 0.0294$ kg/m³ $u_e = 1100$ m/s $u_\tau/u_e = 0.0416$

y/b	u/u_e	M/M_e	ρ/ρ_e	$\frac{\langle(\rho u)'\rangle}{\rho u}$	$\frac{\langle T_0' \rangle}{T_0}$	$R(\rho u)T_0$	$\frac{\langle \rho' \rangle}{\rho}$	$\frac{\langle u' \rangle}{u_\tau} \left(\frac{\rho}{\rho_w}\right)^{1/2}$	$\frac{\langle u' \rangle}{u_\tau}$
0	0	0	0.24	-	-	-	-	-	-
0.04	0.64	0.32	0.26	13.0	4.3	0.6	7.0	1.12	1.06
0.04	0.64	0.32	0.26	15.0	4.8	0.75	7.5	1.31	1.25
0.12	0.74	0.41	0.31	14.0	3.0	0.5	9.5	1.04	0.89
0.22	0.81	0.49	0.36	12.0	3.6	0.4	8.2	0.91	0.72
0.23	0.81	0.49	0.37	13.5	4.2	0.5	9.7	1.13	0.90
0.41	0.89	0.62	0.48	11.6	3.3	0.35	9.6	0.88	0.60
0.43	0.90	0.64	0.50	12.0	2.6	0.4	10.0	0.79	0.54
0.56	0.94	0.74	0.62	11.5	2.5	0.5	10.0	0.77	0.46
0.63	0.96	0.80	0.69	10.0	3.3	0.5	8.8	0.89	0.51
0.81	0.99	0.93	0.88	8.0	2.3	0.0	7.8	0.60	0.31
0.96	1.0	0.99	0.99	6.5	2.2	- 0.4	6.7	0.54	0.26
1.1	1.0	1.0	1.0	1.5	1.4	- 0.5	1.9	0.36	0.17
				%	%		%		

D 2. TURBULENCE QUANTITIES DEDUCED FROM MEAN FLOW MEASUREMENTS

(Horstman & Owen, 1972, figures 6-14)

AUTHORS' SYMBOLS AND UNITS

7205 0101

 $X = 1.15$ m

y/b	$\frac{d(u/u_e)}{d(y/b)}$	$\frac{d(M/M_e)}{d(y/b)}$	$\frac{\tau_w}{\rho_e u_e^2}$	$10^4 \frac{q_w}{\rho_e u_e H_e}$	$10^4 \frac{q_t}{\rho_e u_e H_e}$	$10^4 \frac{g}{u_e b_1^2}$	$\frac{1}{\delta}$	P_{x_T}	P_{x_t}
0.071	4.0	0.49	3.25	2.69	- 0.80	0.00278	0.0102	0.15	3.82
0.088	2.5	0.49	3.74	2.50	- 2.12	0.00416	0.0158	0.29	1.83
0.123	1.0	0.47	4.07	2.29	- 3.10	0.00976	0.0383	0.83	1.12
0.182	0.62	0.41	4.03	2.18	- 3.47	0.0139	0.0581	1.22	0.86
0.282	0.47	0.34	3.79	1.96	- 3.67	0.0185	0.0704	1.39	0.79
0.340	0.45	0.31	3.64	1.81	- 3.64	0.0135	0.0671	1.35	0.83
0.440	0.41	0.29	3.10	1.48	- 3.52	0.0112	0.0642	1.48	0.80
0.500	0.38	0.28	2.77	1.21	- 3.36	0.00955	0.0615	1.67	0.75
0.577	0.34	0.27	2.28	0.82	- 3.05	0.00777	0.0687	2.22	0.67
0.658	0.27	0.23	1.59	0.31	- 2.46	0.00568	0.0663	4.29	0.58
0.741	0.18	0.14	1.10	- 0.017	- 2.11	0.00802	0.0648	- 4.99	0.52
0.818	0.11	0.07	0.56	- 0.040	- 1.40	0.00375	0.0716	- 0.89	0.47
0.883	0.07	0.04	0.42	- 0.040	- 1.15	0.00409	0.0938	- 0.59	0.45
0.972	0.027	0.015	0.19	- 0.039	- 0.74	0.00466	0.1612	- 0.26	0.32
1.0	0.020	0.01	0.19	- 0.039	- 0.74	0.00616	0.2153	- 0.23	0.34

TABLE D 2 CONT.

7205 0102

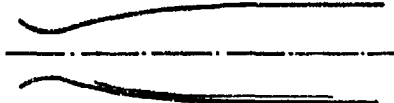
X = 1.76 m

y/b	$\frac{d(u/u_e)}{d(y/b)}$	$\frac{d(H/H_e)}{d(y/b)}$	$\frac{\tau_w}{\rho_e u_e^2}$	$10^4 \frac{q_w}{\rho_e u_e H_e}$	$10^4 \frac{q_t}{\rho_e u_e H_e}$	$10^4 \frac{g}{u_e b_i}$	$\frac{1}{b}$	P_{xT}	P_{xt}
0.048	6.0	0.50	2.99	2.49	- 0.81	0.00173	0.0063	0.10	3.75
0.076	2.5	0.49	3.70	2.18	- 2.54	0.00400	0.0149	0.33	1.57
0.124	0.68	0.47	3.90	1.98	- 3.29	0.01409	0.0537	1.36	0.78
0.232	0.60	0.37	3.63	1.78	- 3.50	0.0155	0.0656	1.51	0.74
0.340	0.42	0.31	3.24	1.49	- 3.50	0.0141	0.0684	1.60	0.75
0.448	0.37	0.28	2.69	1.12	- 3.26	0.0111	0.0647	1.82	0.72
0.556	0.33	0.28	2.05	0.60	- 2.89	0.00804	0.0582	2.91	0.60
0.661	0.26	0.22	1.31	- 0.05	- 2.34	0.00544	0.0539	-23.48	0.51
0.768	0.16	0.11	0.55	- 0.57	- 1.55	0.00308	0.0517	- 0.66	0.39
0.877	0.08	0.04	0.04	- 0.68	- 0.75	0.00038	0.0256	- 0.03	0.07
0.904	0.06	0.03	- 0.06	- 0.68	- 0.57	-0.00077	-	0.04	- 0.14
0.985	0.02	0.01	- 0.07	- 0.67	- 0.55	-0.00241	-	0.05	- 0.16
1.0	0.02	0.01	- 0.07	- 0.67	- 0.54	-0.00244	-	0.05	- 0.16

7205 0103

X = 2.37 m

0.033	9.0	1.2	2.39	2.70	+ 0.34	0.00104	0.0039	0.12	- 6.50
0.051	4.0	0.50	3.32	2.38	- 1.65	0.00253	0.0091	0.17	2.18
0.079	1.0	0.49	3.69	2.16	- 2.63	0.00994	0.0361	0.84	1.13
0.094	0.82	0.49	3.68	2.13	- 2.75	0.0116	0.0432	1.04	0.97
0.133	0.65	0.47	3.61	2.06	- 2.90	0.0136	0.0524	1.27	0.81
0.173	0.56	0.42	3.50	1.98	- 2.98	0.0143	0.0580	1.33	0.78
0.212	0.50	0.36	3.38	1.89	- 3.03	0.0145	0.0517	1.36	0.78
0.252	0.47	0.36	3.24	1.80	- 3.04	0.0139	0.0623	1.38	0.78
0.288	0.46	0.33	3.11	1.73	- 3.00	0.0132	0.0620	1.32	0.82
0.337	0.43	0.31	2.88	1.54	- 2.96	0.0119	0.0603	1.35	0.82
0.376	0.41	0.30	2.67	1.42	- 2.85	0.0110	0.0592	1.38	0.81
0.413	0.40	0.29	2.49	1.27	- 2.76	0.00966	0.0563	1.42	0.81
0.461	0.38	0.28	2.23	1.05	- 2.62	0.00850	0.0542	1.56	0.78
0.494	0.37	0.28	2.00	0.90	- 2.44	0.00738	0.0512	1.68	0.75
0.534	0.34	0.28	1.74	0.71	- 2.24	0.00660	0.0505	2.02	0.68
0.573	0.31	0.27	1.44	0.48	- 2.00	0.00551	0.0483	2.61	0.61
0.616	0.27	0.25	1.16	0.17	- 1.85	0.00479	0.0482	6.32	0.51
0.652	0.24	0.23	0.89	- 0.07	- 1.62	0.00385	0.0459	-12.51	0.44
0.695	0.20	0.19	0.58	- 0.33	- 1.36	0.00288	0.0434	- 1.65	0.35
0.731	0.16	0.16	0.31	- 0.53	- 1.08	0.00179	0.0383	- 0.58	0.23
0.813	0.10	0.08	0.06	- 0.75	- 0.86	0.00054	0.0265	- 0.07	0.07
0.885	0.06	0.04	- 0.19	- 0.79	- 0.55	- 0.00174	-	0.11	- 0.28
0.931	0.04	0.025	- 0.30	- 0.78	- 0.25	- 0.00573	-	0.24	- 1.51
0.968	0.03	0.015	- 0.42	- 0.77	- 0.02	- 0.0106	-	0.27	-
1.0	0.02	0.01	- 0.42	- 0.76	0	- 0.0159	-	0.27	-

axisymmetric 	M : 19 to 45 R THETA X 10 ⁻³ : 1 - 8 TW/TR : 0.35 - 0.85	7206
		FPG - SHT
Blow-down tunnel with axisymmetric contoured nozzle. Test time up to 20 minutes. Open test section: $6.6 < P_0 < 28 \text{ MN/m}^2$ $315 < T_0 < 988 \text{ K Helium}$. $2 < RE/m \times 10^{-6} < 35$. $D = 0.77 \text{ m}$.		
KEMP J.H., OWEN F.K. 1972. Experimental study of nozzle wall boundary layers at Mach numbers 20 to 47. NASA TN D-6965. And Kemp J.H., private communications, Kemp & Srekanth (1969)		

- 1 The tests were conducted on the wall of the axisymmetric contoured nozzle designed to give a Mach number 50 core and equipped with an alternative throat section intended to give a Mach 40 core. The throat sections were furnished with heating coils around the outside to provide a more uniform temperature distribution in the nozzle wall (Kemp, 1970). Radii of the nozzle contour are given in section C for the measuring stations. The nozzle was about 3.60 m long and 0.72 m in diameter at the exit. The profiles were measured in the range $0.50 < X < 3.5 \text{ m}$, ($X = 0$ at the nozzle throat) where X is measured along the nozzle axis. The nozzle was equipped with an injector at the end but no difference was found, in these tests, between
- 2 data obtained with or without the injector, so long as the boundary layer remained attached. The Mach 40 throat was found to provide an inviscid test core approximately 0.10 m in diameter in which the pitot pressure variation was less than $\pm 5 \%$ and the Mach number variation was less than $\pm 1.8 \%$. A reasonably sized uniform core was obtained for $10 < P_0 < 14 \text{ MN/m}^2$ (Kemp 1970). "The uniform Mach core is very much dependent on the reservoir conditions so that care must be exercised in judging the uniform flow conditions."
- 4 The nozzle throat was heated to very nearly the recovery temperature. The temperature dropped off rapidly with distance down the nozzle where the wall temperature was nearly room temperature for all test stations $X > 1.5 \text{ m}$. Coordinates for the nozzle are given in table 1.
- 6 There were 10 static holes ($d = 6.35 \text{ mm}$) along one generator from $X = 0.508$ to 3.56 m , at the 5 profile measuring stations, and distributed between these stations. No corrections were made for rarefaction effects on the wall pressure measurements. Wall temperature was measured at the 5 profile measuring stations using chromel-alumel thermocouples. Skin friction was measured at the last 4 survey stations using a floating element, magnetically nulling balance (Spangler 1963). At each station the elements were contoured to the local nozzle surface. The diameter of the floating element was 12.7 mm and the centre line of the floating element was aligned with the profile measuring station. Wall heat transfer was determined from the steady-state heat conduction in thin-skin gauges contoured to the nozzle wall and positioned at the last four survey stations.
- 7 Traverses were made with Pitot and T0-probes at five survey stations and with hot-wire probes at the last two survey stations. T0 was measured with a single shielded thermocouple probe ($d_1 = 1.78 \text{ mm}$) designed to have low conduction losses in very low density flow conditions and calibrated in a free-jet facility in the relevant Mach number range (the calibration curve is given). Pitot pressure was measured with a CPP ($d_1 = 4.76 \text{ mm}$) at survey stations 1.067 m to 3.56 m and with a CPP ($d_1 = 1.59 \text{ mm}$) at $X = 0.508 \text{ m}$. Fluctuation measurements at $X = 3.56 \text{ m}$ were obtained with a water-cooled platinum film probe (McCroskey 1966). Mass flow and temperature fluctuation intensities were measured at $X = 2.793 \text{ m}$ using a HWP (CT) with a "Platinum 10 % Iridium" wire ($d_1 = 0.0063 \text{ mm}$, $i_1 = 3.17 \text{ mm}$). A preliminary probe calibration was made in a free-jet facility.
- 8 Pitot and T0 profiles were taken at a station corresponding to the centre of the balance.
- 9 The T0 and PT2 profiles were obtained on separate occasions, and the T0 data were interpolated to the Y-values of the Pitot values. The tunnel reservoir conditions differed for each run and the profiles are presented as having the reservoir pressure of the pressure run and the reservoir temperature of the temperature run. The T0 data showed some "hysteresis effects due to variations in support temperature"

and the data were faired giving "velocity values that vary as much as 5 % from the value given by unweighted fairing". The fairing was weighted toward high temperature values in the outer part of the layer, and towards low values in the inner part. The static pressure at the wall differed greatly from that near the boundary layer edge, by a factor of up to three. The authors reduced data assuming a linear static pressure variation from the wall to the free stream. The recovery factor used was 0.8. The temperature and Pitot data were corrected for real gas effects (Erikson, 1963) and raw data are tabulated in the source paper. The viscosity law assumed was Akin's (1960).

The editors have taken values from the authors' final, adjusted profile tabulations, so incorporating all the authors assumptions and calibration procedures. The edge state reservoir values given in section B are calculated from the static properties at the D-state profile point, assuming that helium can be treated as a perfect gas. Ignoring typographical error, random differences between the calculated edge state and the tabulated reservoir conditions are found at the 10 % level. With the exception of four profiles, all the data obtained are presented, giving seven sets of runs for different ranges of Mach number, Reynolds number and heat transfer. CF data are not available for the first station.

DATA: 7206 0101-0705. Pitot and T0 profiles obtained separately. NX = 5. CF from FEB,CQ from steady state film gauges. Some hot wire data.

15 Editors' comments

These measurements were made in a Mach number range unmatched by any other reported experiment. The instrumental and conceptual difficulties are such that no great emphasis should be placed on any precise numerical value. Unfortunately, the experiment is not very clearly reported, and it has not proved possible to decide exactly what was done in every particular.

The editors have inadvertently introduced some scatter in the outer region of the profiles by using the authors' T/TD data as an input for the profiles. These are tabulated in rounded form, to one decimal place, so that for the outermost profile points the pressures may be up to 5 % in error from this cause. The effect of the scatter on evaluated data will however be small. Large differences between our Reynolds number values and those of the original arise from our choosing a different viscosity law for helium at low temperatures, as stated in the introduction.

The velocity profiles cannot be related directly to any correlation based on adiabatic flat plate data. There are strong thermal and pressure history effects, and, for the Mach number, the Reynolds number is so low that the profiles should be considered transitional. (In transformed coordinates the maximum value of y_{τ}/v is of order 40 and the M_{12K} value is appropriate to a laminar layer.) There are also strong, and inadequately described, normal pressure gradient effects which will only very approximately be accounted for by the linear static pressure variation assumed. The probable shape of the static pressure variation can be seen in Beckwith et al. - CAT 7106 P and, approximately, in Fischer et al. - CAT 7001. The normal stress gradient required to turn the flow is provided by a static pressure gradient with a normal Reynolds stress component superimposed on it which is of the same order.

TABLE 1 NOZZLE COORDINATES: AUTHORS' UNITS (INCHES)

X (Inches)	R (Radius-Inches)	X (Inches)	R (Radius-Inches)	X (Inches)	R (Radius-Inches)
- 0.50	0.231	8.000	1.4640	80.000	6.4240
- 0.100	0.1007	10.000	1.7320	64.000 (03)	6.7280
0	0.0984	15.000	2.3280	68.000	7.0270
0.150	0.1140	20.000 (01)	2.8790	80.000	7.8680
0.350	0.1508	25.000	3.4000	90.000	8.5830
0.600	0.1975	30.000	3.8820	100.000	9.2130
1.000	0.2732	35.000	4.3380	110.000 (04)	9.8360
2.000	0.4700	39.000	4.6950	120.000	10.4240
3.000	0.6620	42.000 (02)	4.9690	130.000	10.9760
4.000	0.8430	45.000	5.2170	140.000 (05)	11.5140
6.000	1.1720	50.000	5.6280		

(Figures from NASA Ames)

CAT 7206 KEMP BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.									
RUN	MD *	TW/TR	RED2M	CF *	H12	H12K	PN*	PDA	
X *	POD	PH/PD	RED2D	CO *	H32	H32K	TM*	TD*	
RZ *	TOD	SH *	DZ	PI2	H42	D2K	UD	TR	
72060101	14.4000	0.8098	7.5368 ⁺⁰¹	NM	91.0592	2.3489	5.3297 ⁺⁰¹	3.7896 ⁺⁰¹	
5.0800 ⁻⁰¹	6.7979 ⁺⁰⁶	1.4122	1.6971 ⁺⁰³	NM	1.9071	1.6268	3.6200 ⁺⁰²	3.9400 ⁺⁰⁰	
-7.3127 ⁻⁰²	4.9647 ⁺⁰²	1.0000	1.6328 ⁻⁰⁴	NC	1.2692	1.8040 ⁻⁰³	2.2668 ⁺⁰³	4.4704 ⁺⁰²	
72060102	27.3000	0.7004	5.4270 ⁺⁰¹	3.6200 ⁻⁰⁴	156.3718	2.8490	1.4692 ⁺⁰¹	6.9104 ⁺⁰⁰	
1.0670 ⁺⁰⁰	6.7704 ⁺⁰⁶	1.8917	2.3499 ⁺⁰³	2.1410 ⁻⁰⁵	1.8654	1.5665	3.1500 ⁺⁰²	2.0100 ⁺⁰⁰	
-1.2596 ⁻⁰¹	5.0160 ⁺⁰²	1.0000	2.9909 ⁻⁰⁴	NC	1.2405	5.6321 ⁻⁰³	2.2784 ⁺⁰³	4.4969 ⁺⁰²	
72060103	30.9000	0.6571	6.7521 ⁺⁰¹	2.6600 ⁻⁰⁴	143.2889	2.5437	7.0725 ⁺⁰⁰	3.7693 ⁺⁰⁰	
1.6280 ⁺⁰⁰	6.8441 ⁺⁰⁶	1.8917	3.3561 ⁺⁰³	1.6190 ⁻⁰⁵	1.8848	1.5736	3.0100 ⁺⁰²	1.8000 ⁺⁰⁰	
-1.7089 ⁻⁰¹	5.1109 ⁺⁰²	1.0000	5.2217 ⁻⁰⁴	NC	1.5031	9.6920 ⁻⁰³	2.3008 ⁺⁰³	4.3810 ⁺⁰²	
72060201	19.2000	0.5444	6.4465 ⁺⁰¹	NM	84.6881	2.3630	5.3297 ⁺⁰¹	3.9821 ⁺⁰¹	
5.0800 ⁻⁰¹	6.7853 ⁺⁰⁶	1.3532	4.6382 ⁺⁰²	NM	1.8668	1.8042	3.9700 ⁺⁰²	6.5600 ⁺⁰⁰	
-7.3127 ⁻⁰²	8.1309 ⁺⁰²	1.0000	1.8394 ⁻⁰⁴	NC	1.3258	2.2278 ⁻⁰³	2.8448 ⁺⁰³	7.2918 ⁺⁰²	
72060202	26.4000	0.4375	4.8990 ⁺⁰¹	3.8000 ⁻⁰⁴	130.3095	2.6730	1.4692 ⁺⁰¹	7.9439 ⁺⁰⁰	
1.0670 ⁺⁰⁰	6.5868 ⁺⁰⁶	1.8483	1.1037 ⁺⁰³	5.6860 ⁻⁰⁵	1.8207	1.5627	3.5800 ⁺⁰²	3.9100 ⁺⁰⁰	
-1.2596 ⁻⁰¹	9.1274 ⁺⁰²	1.0000	3.6797 ⁻⁰⁴	NC	1.3609	6.3685 ⁻⁰³	3.0730 ⁺⁰³	8.1822 ⁺⁰²	
72060203	30.6000	0.4127	5.7165 ⁺⁰¹	3.0000 ⁻⁰⁴	132.4749	2.7784	7.0725 ⁺⁰⁰	3.8408 ⁺⁰⁰	
1.6280 ⁺⁰⁰	6.6421 ⁺⁰⁶	1.6892	1.7579 ⁺⁰³	4.2350 ⁻⁰⁵	1.8177	1.5442	3.2100 ⁺⁰²	2.7700 ⁺⁰⁰	
-1.7089 ⁻⁰¹	8.6777 ⁺⁰²	1.0000	6.0103 ⁻⁰⁴	NC	1.8037	1.0831 ⁻⁰²	2.9980 ⁺⁰³	7.7781 ⁺⁰²	
72060301	19.8000	0.4561	1.0826 ⁺⁰²	NM	61.1823	2.5443	8.7241 ⁺⁰¹	5.5830 ⁺⁰¹	
5.0800 ⁻⁰¹	1.1082 ⁺⁰⁷	1.5965	1.8757 ⁺⁰³	NM	1.8691	1.6032	4.0000 ⁺⁰²	7.9900 ⁺⁰⁰	
-7.3127 ⁻⁰²	9.7360 ⁺⁰²	1.0000	2.2787 ⁻⁰⁴	NC	1.4438	1.9617 ⁻⁰³	3.1685 ⁺⁰³	8.7311 ⁺⁰²	
72060302	27.4000	0.4032	9.1269 ⁺⁰¹	3.2200 ⁻⁰⁴	100.1961	2.8510	2.0670 ⁺⁰¹	1.1348 ⁺⁰¹	
1.0670 ⁺⁰⁰	1.1323 ⁺⁰⁷	1.8271	2.1111 ⁺⁰³	5.3300 ⁻⁰⁵	1.8619	1.9529	3.2800 ⁺⁰²	3.6100 ⁺⁰⁰	
-1.2596 ⁻⁰¹	9.0748 ⁺⁰²	1.0000	4.1990 ⁻⁰⁴	NC	1.5139	5.4217 ⁻⁰³	3.0646 ⁺⁰³	8.1347 ⁺⁰²	
72060303	32.5000	0.4053	7.0156 ⁺⁰¹	2.6800 ⁻⁰⁴	146.3628	2.7491	1.0518 ⁺⁰¹	4.7724 ⁺⁰⁰	
1.6280 ⁺⁰⁰	1.1145 ⁺⁰⁷	2.2563	2.4476 ⁺⁰³	4.0420 ⁻⁰⁵	1.8240	1.5534	3.1700 ⁺⁰²	2.4700 ⁺⁰⁰	
-1.7089 ⁻⁰¹	8.7255 ⁺⁰²	1.0000	5.2345 ⁻⁰⁴	NC	1.4400	9.6892 ⁻⁰³	3.0068 ⁺⁰³	7.8206 ⁺⁰²	
72060304	37.9000	0.3558	4.9990 ⁺⁰¹	1.9000 ⁻⁰⁴	248.7335	2.8250	4.0023 ⁺⁰⁰	2.2697 ⁺⁰⁰	
2.7930 ⁺⁰⁰	1.1407 ⁺⁰⁷	1.7595	2.1464 ⁺⁰³	3.2100 ⁻⁰⁵	1.7847	1.5438	3.0000 ⁺⁰²	1.9600 ⁺⁰⁰	
-2.4983 ⁻⁰¹	9.4088 ⁺⁰²	1.0000	5.7810 ⁻⁰⁴	NC	1.4393	1.7703 ⁻⁰²	3.1239 ⁺⁰³	8.4324 ⁺⁰²	
72060401	20.1000	0.7610	1.7867 ⁺⁰²	NM	85.6343	2.2555	1.3578 ⁺⁰²	9.7576 ⁺⁰¹	
5.0800 ⁻⁰¹	2.0869 ⁺⁰⁷	1.3983	4.0995 ⁺⁰³	NM	1.9395	1.7156	3.5200 ⁺⁰²	3.8000 ⁺⁰⁰	
-7.3127 ⁻⁰²	5.1980 ⁺⁰²	1.0000	1.3993 ⁻⁰⁴	NC	1.2950	1.1809 ⁻⁰³	2.3069 ⁺⁰³	4.6255 ⁺⁰²	
72060402	29.4000	0.6650	1.3098 ⁺⁰²	2.7300 ⁻⁰⁴	115.9050	2.5224	3.1613 ⁺⁰¹	1.4084 ⁺⁰¹	
1.0670 ⁺⁰⁰	1.9998 ⁺⁰⁷	2.2386	6.1453 ⁺⁰³	2.3220 ⁻⁰⁵	1.9194	1.5869	3.1900 ⁺⁰²	1.8500 ⁺⁰⁰	
-1.2596 ⁻⁰¹	5.3514 ⁺⁰²	1.0000	3.1809 ⁻⁰⁴	NC	1.4038	4.0443 ⁻⁰³	2.3540 ⁺⁰³	4.7968 ⁺⁰²	
72060403	34.5000	0.6607	1.1424 ⁺⁰²	1.9600 ⁻⁰⁴	157.0778	2.4637	1.4692 ⁺⁰¹	6.6368 ⁺⁰⁰	
1.6280 ⁺⁰⁰	2.0873 ⁺⁰⁷	2.2062	6.1540 ⁺⁰³	1.4340 ⁻⁰⁵	1.9121	1.5937	3.0400 ⁺⁰²	1.2900 ⁺⁰⁰	
-1.7089 ⁻⁰¹	5.1335 ⁺⁰²	1.0000	4.0612 ⁻⁰⁴	NC	1.4635	7.0988 ⁻⁰³	2.3067 ⁺⁰³	4.6010 ⁺⁰²	
72060404	42.2000	0.6712	6.2783 ⁺⁰¹	1.4700 ⁻⁰⁴	329.9712	2.6176	5.6033 ⁺⁰⁰	2.4521 ⁺⁰⁰	
2.7930 ⁺⁰⁰	2.1066 ⁺⁰⁷	2.2740	3.6102 ⁺⁰³	6.3900 ⁻⁰⁶	1.8844	1.5787	2.9700 ⁺⁰²	8.3000 ⁺⁰¹	
-2.4983 ⁻⁰¹	4.4378 ⁺⁰²	1.0000	3.9022 ⁻⁰⁴	NC	1.3401	1.3367 ⁻⁰²	2.2632 ⁺⁰³	4.4251 ⁺⁰²	
72060405	43.8000	0.6231	6.5332 ⁺⁰¹	9.2000 ⁻⁰⁵	368.8574	3.0453	5.1068 ⁺⁰⁰	2.0569 ⁺⁰⁰	
3.5560 ⁺⁰⁰	2.1277 ⁺⁰⁷	2.5253	3.7568 ⁺⁰³	NM	1.8510	1.5335	2.9700 ⁺⁰²	8.3000 ⁺⁰¹	
-2.9246 ⁻⁰¹	5.3166 ⁺⁰²	1.0000	4.6639 ⁻⁰⁴	NC	1.3475	1.8451 ⁻⁰²	2.3490 ⁺⁰³	4.7664 ⁺⁰²	

CAT 7206		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TW/TR	RED2H	CF *	H12	H12K	PWA	PD*	
X *	POD	PW/PO	RED2D	CO	H32	H32K	TWA	TD*	
RZ *	TOD	SW *	D2	P12	H42	D2K	UD	TR	
72060501	20.0000	0.4806	1.9515 ⁺⁰²	NM	56.0666	2.1539	1.3578 ⁺⁰²	9.8589 ⁺⁰¹	
5.0600 ⁺⁰¹	2.0570 ⁺⁰⁷	1.3920	2.8071 ⁺⁰³	NM	1.9230	1.6370	4.0200 ⁺⁰²	6.9400 ⁺⁰⁰	
-7.3127 ⁺⁰²	9.3274 ⁺⁰²	1.0000	2.2388 ⁻⁰⁴	NC	1.5160	1.5740 ⁻⁰³	3.1015 ⁺⁰³	6.3645 ⁺⁰²	
72060502	29.0000	0.4464	1.1353 ⁺⁰²	3.0100 ⁻⁰⁴	108.8460	2.8738	3.1613 ⁺⁰¹	1.4496 ⁺⁰¹	
1.0670 ⁺⁰⁰	1.4449 ⁺⁰⁷	2.0850	3.2390 ⁺⁰³	4.0890 ⁻⁰⁵	1.8942	1.5821	3.4800 ⁺⁰²	3.0900 ⁺⁰⁰	
-1.2596 ⁺⁰¹	8.6975 ⁺⁰²	1.0000	3.5894 ⁻⁰⁴	NC	1.4660	4.3614 ⁻⁰³	3.0009 ⁺⁰³	7.7962 ⁺⁰²	
72060503	34.9000	0.4091	1.1048 ⁺⁰²	2.4500 ⁻⁰⁴	120.4938	2.5938	1.4692 ⁺⁰¹	6.2619 ⁺⁰⁰	
1.6260 ⁺⁰⁰	2.0859 ⁺⁰⁷	2.3904	4.5304 ⁺⁰³	3.9680 ⁻⁰⁵	1.8797	1.5833	3.2100 ⁺⁰²	2.1500 ⁺⁰⁰	
-1.7089 ⁺⁰¹	8.7549 ⁺⁰²	1.0000	5.5029 ⁻⁰⁴	NC	1.5450	8.0650 ⁻⁰³	3.0124 ⁺⁰³	7.8467 ⁺⁰²	
72060504	42.1000	0.3578	4.9863 ⁺⁰¹	1.7900 ⁻⁰⁴	318.6740	2.7960	5.6033 ⁺⁰⁰	2.4723 ⁺⁰⁰	
2.7930 ⁺⁰⁰	2.0990 ⁺⁰⁷	2.3358	3.4888 ⁺⁰³	2.7180 ⁻⁰⁵	1.7887	1.5475	3.0000 ⁺⁰²	1.5600 ⁺⁰⁰	
-2.4983 ⁺⁰¹	9.3552 ⁺⁰²	1.0000	4.2787 ⁻⁰⁴	NC	1.3063	1.5005 ⁻⁰²	3.1151 ⁺⁰³	8.3839 ⁺⁰²	
72060601	20.3000	0.7018	2.9953 ⁺⁰²	NM	72.2043	2.1649	1.8340 ⁺⁰²	1.2970 ⁺⁰²	
5.0800 ⁺⁰¹	2.9135 ⁺⁰⁷	1.4165	6.7110 ⁺⁰³	NM	1.4406	1.6800	3.1800 ⁺⁰²	3.6500 ⁺⁰⁰	
-7.3127 ⁺⁰²	5.0528 ⁺⁰²	1.0000	1.6037 ⁻⁰⁴	NC	1.4026	1.1771 ⁻⁰³	2.2800 ⁺⁰³	4.9311 ⁺⁰²	
72060602	29.9000	0.7059	1.4880 ⁺⁰²	2.0300 ⁻⁰⁴	135.3709	2.6128	3.9111 ⁺⁰¹	1.8846 ⁺⁰¹	
1.0670 ⁺⁰⁰	2.9047 ⁺⁰⁷	2.0823	7.4560 ⁺⁰³	1.6430 ⁻⁰⁵	1.9406	1.8420	3.1800 ⁺⁰²	1.8600 ⁺⁰⁰	
-1.2596 ⁺⁰¹	5.6258 ⁺⁰²	1.0000	2.5254 ⁻⁰⁴	NC	1.3696	3.0454 ⁻⁰³	2.2814 ⁺⁰³	4.5048 ⁺⁰²	
72060603	35.8000	0.6554	1.4814 ⁺⁰²	1.8800 ⁻⁰⁴	133.2784	2.5434	1.9049 ⁺⁰¹	7.5183 ⁺⁰⁰	
1.6260 ⁺⁰⁰	2.8434 ⁺⁰⁷	2.5482	8.0499 ⁺⁰³	1.7210 ⁻⁰⁵	1.9250	1.6031	3.0200 ⁺⁰²	1.2000 ⁺⁰⁰	
-1.7089 ⁺⁰¹	5.1411 ⁺⁰²	1.0000	4.3025 ⁻⁰⁴	NC	1.4873	6.1451 ⁻⁰³	2.3086 ⁺⁰³	4.6077 ⁺⁰²	
72060604	41.6000	0.6460	8.1181 ⁺⁰¹	1.4400 ⁻⁰⁴	259.9784	2.6995	6.8672 ⁺⁰⁰	2.5433 ⁺⁰⁰	
2.7930 ⁺⁰⁰	2.8795 ⁺⁰⁷	2.6399	4.7992 ⁺⁰³	1.1170 ⁻⁰⁵	1.9088	1.5811	3.0000 ⁺⁰²	7.8000 ⁺⁰¹	
-2.4983 ⁺⁰¹	5.1822 ⁺⁰²	1.0000	4.4912 ⁻⁰⁴	NC	1.4384	1.2222 ⁻⁰²	2.3187 ⁺⁰³	4.6441 ⁺⁰²	
72060605	45.9000	0.6452	8.2696 ⁺⁰¹	5.6000 ⁻⁰⁵	328.6326	2.9451	6.5355 ⁺⁰⁰	2.2089 ⁺⁰⁰	
3.5560 ⁺⁰⁰	2.8866 ⁺⁰⁷	2.9926	4.9947 ⁺⁰³	NM	1.8629	1.5460	2.9700 ⁺⁰²	7.3000 ⁺⁰¹	
-2.9246 ⁺⁰¹	5.1344 ⁺⁰²	1.0000	4.9196 ⁻⁰⁴	NC	1.3525	1.7568 ⁻⁰²	2.3086 ⁺⁰³	4.6030 ⁺⁰²	
72060701	20.2000	0.4589	2.4250 ⁺⁰²	NM	63.3799	2.3482	1.8441 ⁺⁰²	1.2767 ⁺⁰²	
5.0800 ⁺⁰¹	2.7985 ⁺⁰⁷	1.4504	3.4814 ⁺⁰³	NM	1.9291	1.6379	3.6100 ⁺⁰²	6.4000 ⁺⁰⁰	
-7.3127 ⁺⁰²	8.7732 ⁺⁰²	1.0000	1.9053 ⁻⁰⁴	NC	1.4740	1.3847 ⁻⁰³	3.0082 ⁺⁰³	7.8674 ⁺⁰²	
72060702	29.6000	0.4358	1.3589 ⁺⁰²	2.5800 ⁻⁰⁴	115.1301	2.7134	3.9010 ⁺⁰¹	1.9150 ⁺⁰¹	
1.0670 ⁺⁰⁰	2.8070 ⁺⁰⁷	1.9774	4.0054 ⁺⁰³	4.1800 ⁻⁰⁵	1.8975	1.6040	3.3900 ⁺⁰²	2.9600 ⁺⁰⁰	
-1.2596 ⁺⁰¹	8.6787 ⁺⁰²	1.0000	3.1717 ⁻⁰⁴	NC	1.4435	3.9100 ⁻⁰³	2.9978 ⁺⁰³	7.7792 ⁺⁰²	
72060703	35.1000	0.3975	1.3074 ⁺⁰²	2.1700 ⁻⁰⁴	127.8709	2.6741	1.8948 ⁺⁰¹	8.0452 ⁺⁰⁰	
1.6260 ⁺⁰⁰	2.7573 ⁺⁰⁷	2.4124	5.3107 ⁺⁰³	3.4570 ⁻⁰⁵	1.8838	1.5817	3.1400 ⁺⁰²	2.1400 ⁺⁰⁰	
-1.7089 ⁺⁰¹	8.8141 ⁺⁰²	1.0000	4.9567 ⁻⁰⁴	NC	1.5219	7.3718 ⁻⁰³	3.0828 ⁺⁰³	7.8997 ⁺⁰²	
72060704	43.5000	0.3692	6.6167 ⁺⁰¹	1.6500 ⁻⁰⁴	289.7081	2.8746	6.6672 ⁺⁰⁰	2.8472 ⁺⁰⁰	
2.7930 ⁺⁰⁰	2.8460 ⁺⁰⁷	2.3967	3.4251 ⁺⁰³	3.0970 ⁻⁰⁵	1.7977	1.5310	2.9700 ⁺⁰²	1.4200 ⁺⁰⁰	
-2.4983 ⁺⁰¹	8.9753 ⁺⁰²	1.0000	4.4941 ⁻⁰⁴	NC	1.3615	1.4208 ⁻⁰²	3.0514 ⁺⁰³	6.0034 ⁺⁰²	
72060705	45.1000	0.3782	9.1399 ⁺⁰¹	6.1000 ⁻⁰⁵	247.4689	3.0927	6.5355 ⁺⁰⁰	2.3609 ⁺⁰⁰	
3.5560 ⁺⁰⁰	2.8260 ⁺⁰⁷	2.8194	4.8499 ⁺⁰³	NM	1.8298	1.5427	2.9700 ⁺⁰²	1.2900 ⁺⁰⁰	
-2.9246 ⁺⁰¹	8.7635 ⁺⁰²	1.0000	6.8827 ⁻⁰⁴	NC	1.4884	1.9658 ⁻⁰²	3.0154 ⁺⁰³	7.8555 ⁺⁰²	

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PDD RED2PWD	RED2PDW RED2PWW	DSTAR
72060101	1.6532 ⁻⁰⁴ 1.3466 ⁻⁰⁴	112.2894 109.2512	1.9075 1.9083	1.2887 1.2879	1.7183 ⁺⁰³ 1.7190 ⁺⁰³	7.6312 ⁺⁰¹ 7.6341 ⁺⁰¹	1.5595 ⁻⁰²
72060102	2.9560 ⁻⁰⁴ 1.8820 ⁻⁰⁴	292.5824 232.4460	1.8638 1.8644	1.2551 1.2541	2.3225 ⁺⁰³ 2.3231 ⁺⁰³	5.3637 ⁺⁰¹ 5.3653 ⁺⁰¹	5.0030 ⁻⁰²
72060103	5.1921 ⁻⁰⁴ 3.5609 ⁻⁰⁴	265.4817 200.1613	1.8841 1.8841	1.5116 1.5106	3.3370 ⁺⁰³ 3.3369 ⁺⁰³	6.7138 ⁺⁰¹ 6.7135 ⁺⁰¹	7.9675 ⁻⁰²
72060201	1.8240 ⁻⁰⁴ 1.5526 ⁻⁰⁴	104.6585 101.8386	1.8656 1.8662	1.3369 1.3362	9.5577 ⁺⁰² 9.5605 ⁺⁰²	6.3926 ⁺⁰¹ 6.3945 ⁺⁰¹	1.6305 ⁻⁰²
72060202	3.6551 ⁻⁰⁴ 2.5294 ⁻⁰⁴	211.8333 178.8039	1.8194 1.8199	1.3700 1.3690	1.0964 ⁺⁰³ 1.0965 ⁺⁰³	4.8663 ⁺⁰¹ 4.8670 ⁺⁰¹	5.0360 ⁻⁰²
72060203	5.9808 ⁻⁰⁴ 4.1478 ⁻⁰⁴	266.6124 182.7825	1.8167 1.8168	1.5111 1.5100	1.7492 ⁺⁰³ 1.7491 ⁺⁰³	5.8885 ⁺⁰¹ 5.8880 ⁺⁰¹	8.3741 ⁻⁰²
72060301	2.2580 ⁻⁰⁴ 1.7294 ⁻⁰⁴	83.7323 80.5531	1.8678 1.8686	1.4571 1.4557	1.4623 ⁺⁰³ 1.4628 ⁺⁰³	1.0728 ⁺⁰² 1.0732 ⁺⁰²	1.4825 ⁻⁰²
72060302	4.1692 ⁻⁰⁴ 2.9111 ⁻⁰⁴	159.7140 140.2107	1.8608 1.8610	1.5247 1.5235	2.0961 ⁺⁰³ 2.0962 ⁺⁰³	9.0637 ⁺⁰¹ 9.0641 ⁺⁰¹	4.4797 ⁻⁰²
72060303	5.1972 ⁻⁰⁴ 3.2330 ⁻⁰⁴	NOT REAL 222.0764	1.8227 1.8228	1.4504 1.4492	2.4302 ⁺⁰³ 2.4301 ⁺⁰³	6.9656 ⁺⁰¹ 6.9654 ⁺⁰¹	8.1806 ⁻⁰²
72060304	5.7538 ⁻⁰⁴ 4.0952 ⁻⁰⁴	NOT REAL 333.7050	1.7837 1.7837	1.4460 1.4454	2.1364 ⁺⁰³ 2.1363 ⁺⁰³	4.9756 ⁺⁰¹ 4.9754 ⁺⁰¹	1.5070 ⁻⁰¹
72060401	1.3825 ⁻⁰⁴ 1.1389 ⁻⁰⁴	109.8360 106.3875	1.9388 1.9385	1.3107 1.3099	4.0501 ⁺⁰³ 4.0515 ⁺⁰³	1.7652 ⁺⁰² 1.7658 ⁺⁰²	1.2709 ⁻⁰²
72060402	3.1362 ⁻⁰⁴ 1.9326 ⁻⁰⁴	220.3895 186.6027	1.9182 1.9186	1.4258 1.4226	6.0591 ⁺⁰³ 6.0603 ⁺⁰³	1.2914 ⁺⁰² 1.2916 ⁺⁰²	4.1015 ⁻⁰²
72060403	4.0200 ⁻⁰⁴ 2.4970 ⁻⁰⁴	318.6338 241.9913	1.9112 1.9113	1.4786 1.4775	6.0918 ⁺⁰³ 6.0921 ⁺⁰³	1.1308 ⁺⁰² 1.1309 ⁺⁰²	6.8913 ⁻⁰²
72060404	3.8705 ⁻⁰⁴ 2.3584 ⁻⁰⁴	NOT REAL 494.4936	1.8834 1.8835	1.3512 1.3506	3.5810 ⁺⁰³ 3.5811 ⁺⁰³	6.2274 ⁺⁰¹ 6.2276 ⁺⁰¹	1.3651 ⁻⁰¹
72060405	4.6311 ⁻⁰⁴ 2.6849 ⁻⁰⁴	NOT REAL 574.4069	1.8499 1.8500	1.3570 1.3564	3.7304 ⁺⁰³ 3.7305 ⁺⁰³	6.4673 ⁺⁰¹ 6.4674 ⁺⁰¹	1.8329 ⁻⁰¹
72060501	2.2716 ⁻⁰⁴ 1.6347 ⁻⁰⁴	71.5308 69.8677	1.9223 1.9228	1.5277 1.5267	2.7854 ⁺⁰³ 2.7861 ⁺⁰³	1.9364 ⁺⁰² 1.9369 ⁺⁰²	1.3380 ⁻⁰²
72060502	3.5497 ⁻⁰⁴ 2.2711 ⁻⁰⁴	196.5228 167.3242	1.8929 1.8933	1.4823 1.4810	3.2032 ⁺⁰³ 3.2037 ⁺⁰³	1.1228 ⁺⁰² 1.1229 ⁺⁰²	4.2722 ⁻⁰²
72060503	5.4638 ⁻⁰⁴ 3.2769 ⁻⁰⁴	NOT REAL 193.4044	1.8788 1.8787	1.5561 1.5548	4.4982 ⁺⁰³ 4.4975 ⁺⁰³	1.0970 ⁺⁰² 1.0968 ⁺⁰²	7.2305 ⁻⁰²
72060504	4.2565 ⁻⁰⁴ 2.6062 ⁻⁰⁴	NOT REAL 480.8302	1.7876 1.7877	1.3130 1.3125	2.4758 ⁺⁰³ 2.4758 ⁺⁰³	4.9602 ⁺⁰¹ 4.9602 ⁺⁰¹	1.4523 ⁻⁰¹
72060601	1.5896 ⁻⁰⁴ 1.2925 ⁻⁰⁴	91.7923 89.7212	1.9400 1.9406	1.4151 1.4142	6.6522 ⁺⁰³ 6.6544 ⁺⁰³	2.9691 ⁺⁰² 2.9700 ⁺⁰²	1.2237 ⁻⁰²
72060602	2.4937 ⁻⁰⁴ 1.6106 ⁻⁰⁴	231.0715 205.0608	1.9397 1.9402	1.3868 1.3858	7.3623 ⁺⁰³ 7.3640 ⁺⁰³	1.4693 ⁺⁰² 1.4691 ⁺⁰²	3.7047 ⁻⁰²
72060603	4.2487 ⁻⁰⁴ 2.4338 ⁻⁰⁴	321.2168 230.9244	1.9240 1.9241	1.5061 1.5049	7.9493 ⁺⁰³ 7.9494 ⁺⁰³	1.4629 ⁺⁰² 1.4629 ⁺⁰²	6.4505 ⁻⁰²
72060604	4.4559 ⁻⁰⁴ 2.5003 ⁻⁰⁴	NOT REAL 438.0560	1.9080 1.9080	1.4498 1.4491	4.7615 ⁺⁰³ 4.7612 ⁺⁰³	8.0543 ⁺⁰¹ 8.0539 ⁺⁰¹	1.2853 ⁻⁰¹
72060605	4.8751 ⁻⁰⁴ 2.5443 ⁻⁰⁴	NOT REAL 567.4926	1.8616 1.8618	1.3649 1.3641	4.9497 ⁺⁰³ 4.9497 ⁺⁰³	8.1951 ⁺⁰¹ 8.1951 ⁺⁰¹	1.7564 ⁻⁰¹
72060701	1.8895 ⁻⁰⁴ 1.5169 ⁻⁰⁴	81.6771 79.6075	1.9284 1.9291	1.4863 1.4853	3.4525 ⁺⁰³ 3.4536 ⁺⁰³	2.4049 ⁺⁰² 2.4057 ⁺⁰²	1.2755 ⁻⁰²
72060702	3.1394 ⁻⁰⁴ 2.0501 ⁻⁰⁴	199.6752 174.8504	1.8964 1.8967	1.4565 1.4574	3.9644 ⁺⁰³ 3.9649 ⁺⁰³	1.3450 ⁺⁰² 1.3452 ⁺⁰²	3.9911 ⁻⁰²
72060703	4.9164 ⁻⁰⁴ 2.9421 ⁻⁰⁴	297.1975 207.0648	1.8828 1.8828	1.5344 1.5332	5.2675 ⁺⁰³ 5.2671 ⁺⁰³	1.2968 ⁺⁰² 1.2967 ⁺⁰²	6.9387 ⁻⁰²
72060704	4.4648 ⁻⁰⁴ 2.6907 ⁻⁰⁴	NOT REAL 451.0117	1.7964 1.7964	1.3704 1.3698	3.4028 ⁺⁰³ 3.4026 ⁺⁰³	6.5735 ⁺⁰¹ 6.5733 ⁺⁰¹	1.3889 ⁻⁰¹
72060705	6.8464 ⁻⁰⁴ 3.7179 ⁻⁰⁴	NOT REAL 409.5137	1.8248 1.8247	1.4923 1.4914	4.8243 ⁺⁰³ 4.8238 ⁺⁰³	9.0920 ⁺⁰¹ 9.0906 ⁺⁰¹	1.8272 ⁻⁰¹

72060103		KEMP	PROFILE TABULATION			23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.89173	0.58636	0.00000	0.00000	187.20000	0.00000	
2	6.3448*+03	1.2628*+00	1.84380	0.60353	0.01753	0.25230	175.60000	0.00244	
3	1.2700*+02	1.7200*+00	1.79872	0.62461	0.02759	0.34960	160.60000	0.00392	
4	1.9063*+02	2.3623*+00	1.76358	0.65476	0.03594	0.43750	148.20000	0.00521	
5	2.5413*+02	3.1280*+00	1.72160	0.69082	0.04485	0.52020	134.50000	0.00666	
6	3.1763*+02	4.7073*+00	1.67912	0.74089	0.05488	0.60320	120.80000	0.00838	
7	3.8112*+02	6.9270*+00	1.63332	0.80859	0.06787	0.69450	104.70000	0.01083	
8	4.4462*+02	1.1736*+01	1.59767	0.90407	0.08968	0.80760	81.10000	0.01591	
9	5.0825*+02	2.8609*+01	1.55168	0.96283	0.14169	0.91390	41.60000	0.03409	
10	5.7175*+02	1.1880*+02	1.50960	0.98845	0.29049	0.96780	11.10000	0.13162	
11	6.3525*+02	2.4162*+02	1.47976	0.96269	0.42317	0.97420	5.30000	0.27200	
12	6.9875*+02	3.8166*+02	1.41400	0.95919	0.52132	0.97530	3.50000	0.39402	
13	7.6225*+02	5.1436*+02	1.36396	0.95773	0.60529	0.97600	2.60000	0.51201	
14	8.2575*+02	6.3696*+02	1.33875	0.95636	0.67364	0.97620	2.10000	0.62233	
15	8.8925*+02	7.4398*+02	1.33470	0.95679	0.72806	0.97680	1.80000	0.72430	
16	9.5288*+02	8.9671*+02	1.24980	0.96014	0.79935	0.97900	1.50000	0.81570	
17	1.0184*+01	1.0403*+03	1.18430	0.96498	0.86110	0.98180	1.30000	0.89442	
18	1.0799*+01	1.1336*+03	1.17120	0.97016	0.89881	0.98460	1.20000	0.96097	
19	1.1434*+01	1.2465*+03	1.11991	0.97752	0.94250	0.98850	1.10000	1.00639	
20	1.2070*+01	1.2566*+03	1.14389	0.98542	0.94631	0.99250	1.10000	1.03210	
21	1.2323*+01	1.3852*+03	1.04540	0.98728	0.99380	0.99380	1.00000	1.03871	
22	1.2958*+01	1.3933*+03	1.02630	0.99303	0.99650	0.99650	1.00000	1.02271	
D 23	1.3340*+01	1.4031*+03	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

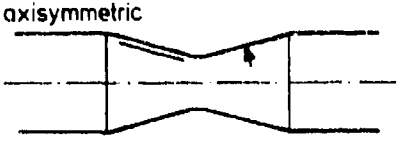
INPUT VARIABLES Y,U/UD,T/TD,RHO/RHOD

72060405		KEMP	PROFILE TABULATION			24 POINTS, DELTA AT POINT 24			
I	Y	PT2/P	P/PD	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	2.52547	0.55509	0.00000	0.00000	355.70000	0.00000	
2	1.2731*+02	1.0948*+00	2.42692	0.57752	0.00760	0.14350	356.40000	0.00098	
3	2.5433*+02	1.3008*+00	2.39020	0.60940	0.01317	0.24690	351.50000	0.00188	
4	3.8164*+02	1.6867*+00	2.30112	0.65096	0.01907	0.35080	338.40000	0.00239	
5	5.0866*+02	2.2811*+00	2.22939	0.70149	0.02473	0.44450	323.10000	0.00307	
6	6.3597*+02	3.2774*+00	2.18892	0.75189	0.03135	0.53920	295.80000	0.00399	
7	7.6328*+02	4.7890*+00	2.11815	0.80714	0.03909	0.63220	261.50000	0.00512	
8	8.9030*+02	7.1975*+00	2.05200	0.86754	0.04960	0.72890	216.00000	0.00692	
9	1.0176*+01	1.3427*+01	1.98264	0.92471	0.06785	0.83150	150.20000	0.01098	
10	1.1444*+01	4.0275*+01	1.91556	0.95906	0.11888	0.93000	81.20000	0.02911	
11	1.2719*+01	1.1484*+02	1.84920	0.96798	0.20147	0.96620	23.00000	0.07768	
12	1.3993*+01	2.4167*+02	1.78640	0.97462	0.29256	0.97910	11.20000	0.15617	
13	1.5263*+01	4.1822*+02	1.71860	0.97218	0.38502	0.98160	6.50000	0.25954	
14	1.6536*+01	6.4859*+02	1.65360	0.97094	0.47956	0.98280	4.20000	0.38771	
15	1.7804*+01	9.0989*+02	1.57740	0.97123	0.56805	0.98390	3.00000	0.51733	
16	1.9078*+01	1.1903*+03	1.50719	0.97309	0.64975	0.98540	2.30000	0.64573	
17	2.0352*+01	1.4452*+03	1.44780	0.97542	0.71597	0.98690	1.90000	0.75202	
18	2.1622*+01	1.7192*+03	1.34976	0.97672	0.78092	0.98780	1.60000	0.83331	
19	2.2894*+01	1.8412*+03	1.34895	0.98052	0.80817	0.98980	1.50000	0.89013	
20	2.4166*+01	2.1313*+03	1.22018	0.98337	0.86952	0.99140	1.30000	0.93053	
21	2.5438*+01	2.3186*+03	1.17012	0.98737	0.90694	0.99350	1.20000	0.96876	
22	2.6712*+01	2.5401*+03	1.10099	0.99139	0.94927	0.99560	1.10000	0.99650	
23	2.7727*+01	2.5488*+03	1.11078	0.99477	0.95059	0.99730	1.10000	1.00707	
D 24	2.9000*+01	2.8188*+03	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD,RHO/RHOD

72060705		KEMP	PROFILE TABULATION			23 POINTS, DELTA AT POINT 23			
I	Y	PT2/P	P/PD	T0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	2.81942	0.34018	0.00000	0.00000	231.10000	0.00000	
2	1.2714*+02	1.1601*+00	2.74804	0.37006	0.00950	0.14620	236.90000	0.00170	
3	2.5401*+02	1.4883*+00	2.65440	0.40871	0.01990	0.24480	237.00000	0.00274	
4	3.8119*+02	2.0049*+00	2.58112	0.46043	0.02175	0.33470	236.80000	0.00365	
5	5.0830*+02	2.8242*+00	2.48940	0.51653	0.02775	0.42130	230.50000	0.00455	
6	6.3544*+02	4.1245*+00	2.42368	0.58153	0.03489	0.51320	216.40000	0.00575	
7	7.6230*+02	6.2341*+00	2.35046	0.65445	0.04392	0.60950	192.60000	0.00737	
8	8.8949*+02	9.6919*+00	2.28260	0.73328	0.05599	0.70510	160.90000	0.00987	
9	1.0186*+01	1.7540*+01	2.16960	0.81164	0.07562	0.80390	113.00000	0.01543	
10	1.1439*+01	3.5059*+01	2.08884	0.88140	0.10763	0.88490	47.60000	0.02734	
11	1.2706*+01	9.4390*+01	2.00160	0.91367	0.17731	0.93490	27.80000	0.04731	
12	1.3977*+01	1.9962*+02	1.91526	0.93199	0.28818	0.95560	13.70000	0.13359	
13	1.5249*+01	3.6642*+02	1.82704	0.94066	0.34997	0.96480	7.60000	0.23144	
14	1.6518*+01	6.1114*+02	1.77054	0.94551	0.45208	0.96960	4.80000	0.37320	
15	1.7789*+01	9.1470*+02	1.64641	0.95165	0.55314	0.97390	3.10000	0.51724	
16	1.9060*+01	1.2441*+03	1.55388	0.95924	0.64514	0.97840	2.30000	0.66101	
17	2.0329*+01	1.6019*+03	1.46952	0.96595	0.73209	0.98220	1.80000	0.80187	
18	2.1598*+01	1.9438*+03	1.42545	0.97632	0.80645	0.98770	1.50000	0.93861	
19	2.2863*+01	2.4618*+03	1.20888	0.98875	0.90758	0.99420	1.20000	1.00156	
20	2.4137*+01	2.6976*+03	1.13355	0.99317	0.95013	0.99650	1.10000	1.02689	
21	2.6049*+01	2.7034*+03	1.13553	0.99516	0.95108	0.99750	1.10000	1.02972	
22	2.6683*+01	2.7088*+03	1.12717	0.99715	0.95203	0.99850	1.10000	1.02314	
D 23	2.7700*+01	2.9886*+03	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD,RHO/RHOD

	M : 0.06 to 3.6 R THETA X 10 ⁻³ : 6 - 26 TW/TR : About 0.5 and 1.1	7207
		FPG-MHT-SHT
Special purpose rig: continuous running. D (inlet) 127 mm. PO : 1 MN/m ² . TO : 830 and 290 K. Air and a small quantity of the combustion products of Methanol. RE/m X 10 ⁻⁶ at inlet about 30 and 100.		
BACK L.H. and CUFFEL R.F., 1972. Turbulent-boundary-layer measurements along a supersonic nozzle with and without wall cooling. Heat Transfer. Trans. Am. Soc. Mech. Engrg. 94, 242-243. And Back & Cuffel (1971) and private communications. Also Back, Cuffel and Messier (1970). Many associated papers. See References.		

- 1 The test boundary layer was formed on the inside surface of a circular duct finishing in a convergent-divergent nozzle. The air supply is compressed and then heated by the combustion of methanol before entering a large settling chamber containing baffles and screens (Back, Messier & Cuffel, 1967). From this it passes through an area contraction of 11.6:1 and enters the duct which has the dimensions listed in Table 1. These may be summarised as describing a conical convergent-divergent nozzle of closely 10° semi vertex angle fed by a cooled-wall approach duct about 1 m long and 127 mm in diameter. The throat (diameter 40.4 mm) and the junctions of duct and nozzle are fairred in section with circular arcs. There are five traverse stations
- 8 upstream of the throat and one downstream. The first station, in the approach duct, has been selected as the X = 0 point. The surface was finished to 0.8 μm and could be actively cooled by small circumferential coolant
- 3 passages, of which there were 36 in the nozzle and 31 in the approach section. The boundary layer was tripped by a 1.5 mm square step mounted inside the duct at the outlet from the settling chamber contraction (X = - 1.110 m). The velocity profile at the first traverse station was typical of a fully developed turbulent
- 4 layer. The cooled approach duct allowed the thermal layer to form with approximately the same wall temperature as in the nozzle, and from a point just downstream of the boundary layer trip.
- 6 There were some 45 static pressure taps (d = 0.51 mm) in the nozzle and 9 in the cooled approach duct. Thermocouples were fixed in the coolant passages, and the "gas-side" wall temperatures were calculated from these "water-side" measurements and the heat-flux, which was determined calorimetrically. The technique is described by Back, Messier and Cuffel (1967).
- 8 The 6 profile traverse stations were at X (axial) = 0, 90.50, 147.57, 185.67, 223.80 and 528.04 mm (the
- 7 throat is at 313.06 mm - see table 1). The Pitot tube was an FPP (h₁ = 0.127, b₁ = 1.65, l = 12.7 mm) and two types of TTP were used. In the subsonic region an exposed thermocouple 0.1 mm thick in the direction normal to the wall was mounted on a support for which h₁ = 0.25, b₁ = 6.86, l = 12.7 mm. At the supersonic
- 8 station, an STP was used for which h₁ = 0.25 mm. The Pitot probe was always located 90° circumferentially from the TTP at the same X-station. Only one pair of probes was in use at any one time.
- 9 The authors have interpolated the static pressure measurements to the nominal X-values of the heat-flux measurements. These values are presented together in section D. The heat flux measurements are the average of at least 5 runs. The authors' CF values, quoted for the profiles, are based on a momentum balance for the four stations in the converging cone, on a form of Reynolds analogy in the approach duct, and in the supersonic diverging flow, on the velocity profile in the sublayer. Very close to the wall the TTP gave readings below those indicated by an extrapolation of the TO profile to meet the TW value, and the values
- 11 were adjusted to fit the extrapolation. Transport properties were taken as for air, from Hilsenrath et al. (1955).
- 12 The heat flux and pressure values are given separately in section D for the O1 series with strong wall cooling. The authors state that, for the O2 series (heat transfer to the gas but near adiabatic), the temperature differences were too small to allow of meaningful distributed values, and suggest that the wall temperature be taken as constant at 1.10 TOD. The editors have accepted this, and the presumption that the pressure distribution is effectively the same in the two cases. Boundary conditions for the

profiles are thus taken from the authors' interpolations. It has been assumed that $P = PD$ through the boundary layer.

- 13 The two sets of six profiles describe the development of the boundary layer through a nozzle expansion. The low velocity history is fully described (profiles 1-5) but there is only one supersonic profile. The
- 14 two cases are firstly (Series 01) a flow with strongly cooled wall in which the wall heat-flux and
- 14 temperature are given in detail. The second series (02) describes a near-adiabatic set, and is without a detailed temperature history. The CF values are as estimated by the authors.
- 5 DATA: 7207 0101-0206. Pitot and TO profiles measured simultaneously. NX = 6. Heat flux by calorimetry.

15 Editors' comments

This entry is included principally as a challenge for calculation methods. In both series, the state of the boundary layer upstream of the throat is very fully described, and a fully developed calculation scheme should be able to predict the subsequent heat transfer distribution and the final velocity profile from the full wall pressure and temperature data given. The heat transfer case (series 01) is similar to the "cooled inlet" series of Boldman et al. - CAT 6901, series 02 - for which, however, the emphasis in measurement lay on the supersonic side of the throat.

The authors' CF values appear quite reasonable when the profiles are plotted out in comparison with the wall law, though the values for the supersonic profiles, 0106, 0206 are probably too high. In general measurements do not extend within the momentum-deficit peak.

The measurements described here form only part of an extended project described in about ten frequently overlapping papers.

TABLE 1 GEOMETRY OF DUCT - DIMENSIONS in mm

	X (Axial)	X (Contour)	- RZ
End of contraction (E)	- 1110.00	- 1110.00	63.50
Start of cooled approach	- 1053.85	- 1053.85	63.50
First profile station	0	0	63.50
End of parallel approach	+ 59.95	+ 59.95	63.50
Circular arc fairing with radius 40.64			
Start of conical contraction	67.01	-	59.51
Second profile station	90.50	90.91	58.67
Third profile station	147.57	148.89	48.51
Fourth profile station	185.67	187.55	41.88
Fifth profile station	223.80	226.26	35.16
End of conical contraction	304.29	-	20.96
Circular arc fairing with radius 50.47			
Throat	313.06	317.07	20.19
Start of conical expansion	321.84	-	20.96
Sixth profile station	528.04	535.08	57.76
End of conical expansion	556.87	-	63.06

CAT 7207		BACK/CUFFEL		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	MD *	TW/TR	RED2W	CF *	H12	H12K	PW	PD			
X *	POD*	PW/PD*	RED2D	CO *	H32	H32K	TW*	TD			
RZ *	TOD*	SH *	D2	PI2	H42	D2K	UD	TR			
72070101	0.0637	0.4627	1.7644 ⁺⁰⁴	3.2000 ⁻⁰³	0.5627	1.3644	1.0285 ⁺⁰⁶	1.0285 ⁺⁰⁶			
0.0000 ⁺⁰⁰	1.0315 ⁺⁰⁶	1.0000	1.0512 ⁺⁰⁴	1.0500 ⁻⁰³	1.7922	1.7982	3.8556 ⁺⁰²	8.3266 ⁺⁰²			
-6.3500 ⁻⁰²	8.3333 ⁺⁰²	0.0000	2.4872 ⁻⁰³	NC	0.6063	2.1549 ⁻⁰³	3.6854 ⁺⁰¹	8.3326 ⁺⁰²			
72070102	0.0723	0.4545	1.6106 ⁺⁰⁴	5.0000 ⁻⁰³	0.3536	1.2397	1.0311 ⁺⁰⁶	1.0311 ⁺⁰⁶			
9.0907 ⁻⁰²	1.0349 ⁺⁰⁶	1.0000	9.4763 ⁺⁰³	8.9000 ⁻⁰⁴	1.8481	1.8514	3.8000 ⁺⁰²	8.3524 ⁺⁰²			
-5.8674 ⁻⁰²	8.3611 ⁺⁰²	0.0000	1.9774 ⁻⁰³	NC	0.7208	1.7260 ⁻⁰³	4.1894 ⁺⁰¹	8.3602 ⁺⁰²			
72070103	0.1038	0.4759	1.3303 ⁺⁰⁴	5.2000 ⁻⁰³	-0.0469	1.1548	1.0299 ⁺⁰⁶	1.0299 ⁺⁰⁶			
1.4884 ⁻⁰¹	1.0377 ⁺⁰⁶	1.0000	8.0969 ⁺⁰²	8.9000 ⁻⁰⁴	1.9041	1.9033	3.9778 ⁺⁰²	8.3431 ⁺⁰²			
-4.8514 ⁻⁰²	8.3611 ⁺⁰²	0.0000	1.1768 ⁻⁰³	NC	1.0634	1.0327 ⁻⁰³	6.0113 ⁺⁰¹	9.3592 ⁺⁰²			
72070104	0.1367	0.4910	1.2926 ⁺⁰⁴	4.0000 ⁻⁰³	-0.3372	1.1576	1.0228 ⁺⁰⁶	1.0228 ⁺⁰⁶			
1.8755 ⁻⁰¹	1.0363 ⁺⁰⁶	1.0000	8.0337 ⁺⁰³	8.5000 ⁻⁰⁴	1.9054	1.9110	3.9944 ⁺⁰²	8.1086 ⁺⁰²			
-4.1865 ⁻⁰²	8.1389 ⁺⁰²	0.0000	8.6448 ⁻⁰⁴	NC	1.3511	7.4842 ⁻⁰⁴	7.8046 ⁺⁰¹	8.1357 ⁺⁰²			
72070105	0.1944	0.4997	1.4951 ⁺⁰⁴	4.6000 ⁻⁰³	-0.2625	1.1591	1.0046 ⁺⁰⁶	1.0046 ⁺⁰⁶			
2.2626 ⁻⁰¹	1.0315 ⁺⁰⁶	1.0000	9.4510 ⁺⁰³	7.5000 ⁻⁰⁴	1.9085	1.9144	4.1611 ⁺⁰²	8.2708 ⁺⁰²			
-3.5154 ⁻⁰²	8.3333 ⁺⁰²	0.0000	7.4453 ⁻⁰⁴	NC	1.2860	6.4975 ⁻⁰⁴	1.1209 ⁺⁰²	8.3268 ⁺⁰²			
72070106	3.3663	0.4613	1.0570 ⁺⁰⁴	1.7600 ⁻⁰³	-0.3221	1.2399	1.6464 ⁺⁰⁴	1.6464 ⁺⁰⁴			
5.3508 ⁻⁰¹	1.0370 ⁺⁰⁶	1.0000	1.3681 ⁺⁰⁴	3.3000 ⁻⁰⁴	1.8840	1.8692	3.5667 ⁺⁰²	2.5512 ⁺⁰²			
-5.7760 ⁻⁰²	8.3333 ⁺⁰²	0.0000	9.2060 ⁻⁰⁴	NC	1.7826	9.0831 ⁻⁰⁴	1.0780 ⁺⁰³	7.7320 ⁺⁰²			
72070201	0.0650	1.1087	2.4142 ⁺⁰⁴	1.7600 ⁻⁰³	1.4542	1.3290	1.0339 ⁺⁰⁶	1.0339 ⁺⁰⁶			
0.0000 ⁺⁰⁰	1.0370 ⁺⁰⁶	1.0000	2.6144 ⁺⁰⁴	HM	1.8203	1.8189	3.2333 ⁺⁰²	2.7142 ⁺⁰²			
-6.3500 ⁻⁰²	2.9167 ⁺⁰²	0.0000	1.7223 ⁻⁰³	NC	-0.0944	1.7550 ⁻⁰³	2.2248 ⁺⁰¹	2.9164 ⁺⁰²			
72070202	0.0740	1.0246	2.2065 ⁺⁰⁴	3.3600 ⁻⁰³	1.2195	1.1785	1.0289 ⁺⁰⁶	1.0289 ⁺⁰⁶			
9.0907 ⁻⁰²	1.0328 ⁺⁰⁶	1.0000	2.2494 ⁺⁰⁴	HM	1.8859	1.8857	3.0278 ⁺⁰²	2.9523 ⁺⁰²			
-5.8674 ⁻⁰²	2.9556 ⁺⁰²	0.0000	1.3301 ⁻⁰³	NC	-0.0317	1.3371 ⁻⁰³	2.5493 ⁺⁰¹	2.9552 ⁺⁰²			
72070203	0.1030	1.0245	1.3560 ⁺⁰⁴	3.5400 ⁻⁰³	1.1911	1.1128	1.0266 ⁺⁰⁶	1.0266 ⁺⁰⁶			
1.4884 ⁻⁰¹	1.0342 ⁺⁰⁶	1.0000	1.3836 ⁺⁰⁴	HM	1.9425	1.9422	3.0500 ⁺⁰²	2.9715 ⁺⁰²			
-4.8514 ⁻⁰²	2.9778 ⁺⁰²	0.0000	5.9383 ⁻⁰⁴	NC	-0.0674	5.9683 ⁻⁰⁴	3.5599 ⁺⁰¹	2.9771 ⁺⁰²			
72070204	0.1380	1.0807	5.7686 ⁺⁰³	3.4400 ⁻⁰³	1.8703	1.1968	1.0253 ⁺⁰⁶	1.0253 ⁺⁰⁶			
1.8755 ⁻⁰¹	1.0390 ⁺⁰⁶	1.0000	6.1400 ⁺⁰³	HM	1.9281	1.9267	3.1389 ⁺⁰²	2.8945 ⁺⁰²			
-4.1865 ⁻⁰²	2.9056 ⁺⁰²	0.0000	1.9046 ⁻⁰⁴	NC	-0.6319	1.9467 ⁻⁰⁴	4.7074 ⁺⁰¹	2.9044 ⁺⁰²			
72070205	0.1970	1.0940	7.0765 ⁺⁰³	3.9400 ⁻⁰³	1.8389	1.1821	1.0093 ⁺⁰⁶	1.0093 ⁺⁰⁶			
2.2626 ⁻⁰¹	1.0370 ⁺⁰⁶	1.0000	7.6228 ⁺⁰³	HM	1.9453	1.9441	3.1944 ⁺⁰²	2.8997 ⁺⁰²			
-3.5154 ⁻⁰²	2.9222 ⁺⁰²	0.0000	1.6865 ⁻⁰⁴	NC	-0.6053	1.7239 ⁻⁰⁴	8.7260 ⁺⁰¹	2.9199 ⁺⁰²			
72070206	3.6140	1.1682	2.6698 ⁺⁰³	1.3600 ⁻⁰³	8.1010	1.3604	1.1599 ⁺⁰⁴	1.1599 ⁺⁰⁴			
5.3508 ⁻⁰¹	1.0390 ⁺⁰⁶	1.0000	8.8815 ⁺⁰³	HM	1.8362	1.8671	3.1389 ⁺⁰²	8.0437 ⁺⁰¹			
-5.7760 ⁻⁰²	2.9056 ⁺⁰²	0.0000	1.5684 ⁻⁰⁴	NC	-0.2268	2.7857 ⁻⁰⁴	6.4987 ⁺⁰²	2.6870 ⁺⁰²			

TRAPEZOIDAL RULE FOR RUN 0106

72070101		BACK/CUFFEL	PROFILE TABULATION	31 POINTS, DELTA AT POINT 31				
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD=U/UD
1	0.0000+00	1.0000+00	NM	0.46163	0.00000	0.00000	0.46200	0.00000
2	1.7780-04	1.0009+00	NM	0.71290	0.54963	0.46420	0.71330	0.65078
3	2.0320-04	1.0009+00	NM	0.72160	0.56490	0.46800	0.72200	0.66442
4	2.5400-04	1.0010+00	NM	0.73611	0.58716	0.50390	0.73650	0.68418
5	3.0480-04	1.0010+00	NM	0.74322	0.60152	0.51870	0.74360	0.69755
6	3.5560-04	1.0011+00	NM	0.74952	0.61272	0.53060	0.74990	0.70756
7	4.3180-04	1.0011+00	NM	0.75653	0.62655	0.54510	0.75690	0.72017
8	4.9530-04	1.0011+00	NM	0.76173	0.63598	0.55520	0.76210	0.72851
9	5.5880-04	1.0012+00	NM	0.76754	0.64396	0.56430	0.76790	0.73486
10	6.8580-04	1.0012+00	NM	0.77574	0.65837	0.58000	0.77610	0.74733
11	8.1280-04	1.0013+00	NM	0.78256	0.67630	0.59840	0.78290	0.76434
12	9.3980-04	1.0013+00	NM	0.78896	0.68132	0.60530	0.78930	0.76686
13	1.1938-03	1.0014+00	NM	0.79997	0.69741	0.62390	0.80030	0.77958
14	1.4478-03	1.0015+00	NM	0.80858	0.71549	0.64350	0.80890	0.79552
15	1.8288-03	1.0015+00	NM	0.81839	0.73208	0.66240	0.81870	0.80909
16	2.2098-03	1.0016+00	NM	0.82880	0.74812	0.68120	0.82910	0.82161
17	2.7178-03	1.0017+00	NM	0.83852	0.76846	0.70380	0.83880	0.83906
18	3.3528-03	1.0018+00	NM	0.85004	0.78819	0.72680	0.85030	0.85476
19	3.9878-03	1.0018+00	NM	0.85975	0.80314	0.74480	0.86000	0.86605
20	5.2578-03	1.0020+00	NM	0.87638	0.83235	0.77930	0.87640	0.88900
21	6.5278-03	1.0021+00	NM	0.89181	0.85764	0.81000	0.89200	0.90807
22	7.7978-03	1.0022+00	NM	0.90603	0.88020	0.83790	0.90620	0.92463
23	9.0678-03	1.0023+00	NM	0.91776	0.90129	0.86350	0.91790	0.94073
24	1.0338-02	1.0024+00	NM	0.92908	0.92007	0.88690	0.92920	0.95448
25	1.2878-02	1.0026+00	NM	0.94752	0.94920	0.92400	0.94760	0.97509
26	1.5418-02	1.0027+00	NM	0.96025	0.97056	0.95110	0.96030	0.99042
27	1.7958-02	1.0028+00	NM	0.97038	0.98458	0.96990	0.97040	0.99948
28	2.0498-02	1.0028+00	NM	0.97839	0.99318	0.98240	0.97840	1.00409
29	2.5578-02	1.0028+00	NM	0.98920	0.99831	0.99290	0.98920	1.00374
30	3.0658-02	1.0028+00	NM	0.99540	1.00000	0.99770	0.99540	1.00231
0 31	3.5738-02	1.0028+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

72070102		BACK/CUFFEL	PROFILE TABULATION	24 POINTS, DELTA AT POINT 24				
I	Y	PT2/P	P/PD	T0/T0D	H/HD	U/UD	T/TD	RHO/RHOD=U/UD
1	0.0000+00	1.0000+00	NM	0.45652	0.00000	0.00000	0.45700	0.00000
2	6.3500-05	1.0013+00	NM	0.67395	0.60066	0.49400	0.67640	0.73034
3	8.3620-05	1.0016+00	NM	0.68907	0.65682	0.54540	0.68950	0.79101
4	1.0922-04	1.0018+00	NM	0.71521	0.69308	0.58630	0.71560	0.81931
5	1.3462-04	1.0019+00	NM	0.73252	0.71406	0.61130	0.73290	0.83400
6	1.7272-04	1.0020+00	NM	0.74894	0.73572	0.63600	0.74730	0.85106
7	2.2352-04	1.0021+00	NM	0.75846	0.75147	0.65460	0.75880	0.86268
8	2.9972-04	1.0022+00	NM	0.77287	0.76957	0.67670	0.77320	0.87519
9	4.2672-04	1.0023+00	NM	0.78149	0.78716	0.69600	0.78180	0.89025
10	6.8072-04	1.0024+00	NM	0.79441	0.80441	0.71710	0.79470	0.90235
11	9.3472-04	1.0024+00	NM	0.80442	0.81411	0.73030	0.80470	0.90754
12	1.4427-03	1.0025+00	NM	0.82003	0.82610	0.74520	0.82030	0.91211
13	1.9507-03	1.0026+00	NM	0.83294	0.83786	0.76480	0.83320	0.91791
14	2.4587-03	1.0026+00	NM	0.84295	0.84486	0.77580	0.84320	0.92007
15	3.7287-03	1.0027+00	NM	0.86417	0.86326	0.80260	0.86440	0.92851
16	4.9987-03	1.0028+00	NM	0.88409	0.88114	0.82860	0.88430	0.93701
17	7.5387-03	1.0031+00	NM	0.90949	0.91394	0.87170	0.90970	0.95823
18	1.0079-02	1.0032+00	NM	0.93379	0.93938	0.90780	0.93390	0.97205
19	1.2619-02	1.0034+00	NM	0.95212	0.95798	0.93480	0.95220	0.98173
20	1.5159-02	1.0035+00	NM	0.96605	0.97426	0.95760	0.96610	0.99120
21	1.7699-02	1.0036+00	NM	0.97737	0.98621	0.97500	0.97740	0.99754
22	2.0239-02	1.0036+00	NM	0.98439	0.99610	0.98830	0.98440	1.00396
23	2.5319-02	1.0037+00	NM	0.99580	1.00000	0.99790	0.99580	1.00211
0 24	3.0399-02	1.0037+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

72070103		BACK/CUFFEL	PROFILE TABULATION	24 POINTS, DELTA AT POINT 24				
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000+00	1.0000+00	NM	0.47597	0.00000	0.00000	0.47700	0.00000
2	6.3570-05	1.0038+00	NM	0.68816	0.70663	0.58650	0.68890	0.85136
3	7.6200-05	1.0043+00	NM	0.69386	0.75801	0.63170	0.69450	0.40958
4	1.0160-04	1.0047+00	NM	0.71231	0.78523	0.66300	0.71290	0.93000
5	1.2700-04	1.0048+00	NM	0.72832	0.79461	0.67840	0.72890	0.93072
6	1.6510-04	1.0050+00	NM	0.73357	0.81420	0.69760	0.73410	0.95028
7	2.1590-04	1.0052+00	NM	0.74711	0.83353	0.72070	0.74760	0.96402
8	2.9210-04	1.0055+00	NM	0.76356	0.85577	0.74800	0.76400	0.97906
9	3.6830-04	1.0057+00	NM	0.77360	0.87170	0.76690	0.77400	0.99083
10	4.9530-04	1.0061+00	NM	0.78497	0.89621	0.79420	0.78530	1.01133
11	7.4930-04	1.0064+00	NM	0.80274	0.92010	0.82450	0.80300	1.02677
12	1.0033-03	1.0066+00	NM	0.81817	0.93185	0.84300	0.81840	1.03006
13	1.5113-03	1.0067+00	NM	0.83910	0.94189	0.86290	0.83930	1.02812
14	2.5273-03	1.0068+00	NM	0.86451	0.94721	0.88000	0.86470	1.01862
15	3.7973-03	1.0069+00	NM	0.88213	0.95411	0.89620	0.88230	1.01575
16	5.0673-03	1.0070+00	NM	0.89885	0.95934	0.90960	0.89900	1.01179
17	6.3373-03	1.0070+00	NM	0.91026	0.96390	0.91970	0.91040	1.01022
18	7.6073-03	1.0071+00	NM	0.92678	0.96837	0.93230	0.92690	1.00583
19	1.0147-02	1.0072+00	NM	0.95011	0.97663	0.95200	0.95020	1.00189
20	1.2687-02	1.0073+00	NM	0.96813	0.98326	0.96750	0.96820	0.99926
21	1.5227-02	1.0074+00	NM	0.97915	0.98803	0.97770	0.97920	0.99847
22	2.0307-02	1.0075+00	NM	0.99248	0.99424	0.99050	0.99250	0.99798
23	2.5387-02	1.0075+00	NM	0.99849	0.99785	0.99710	0.99850	0.99860
D 24	3.0467-02	1.0076+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

72070104		BACK/CUFFEL	PROFILE TABULATION	27 POINTS, DELTA AT POINT 27				
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000+00	1.0000+00	NM	0.48021	0.00000	0.00000	0.48200	0.00000
2	6.3500-05	1.0065+00	NM	0.68022	0.70391	0.58110	0.68150	0.85268
3	6.8900-05	1.0073+00	NM	0.69785	0.74743	0.62490	0.69900	0.89399
4	1.1430-04	1.0080+00	NM	0.71226	0.77980	0.65860	0.71330	0.92331
5	1.3970-04	1.0083+00	NM	0.72082	0.79639	0.67660	0.72180	0.93738
6	1.6510-04	1.0086+00	NM	0.72657	0.80932	0.69030	0.72750	0.94887
7	2.1590-04	1.0090+00	NM	0.73804	0.82853	0.71220	0.73890	0.96387
8	2.6670-04	1.0093+00	NM	0.74670	0.84365	0.72940	0.74750	0.97579
9	3.1750-04	1.0096+00	NM	0.75466	0.85740	0.74520	0.75540	0.98650
10	3.9370-04	1.0102+00	NM	0.76386	0.86030	0.76970	0.76450	1.00680
11	5.2070-04	1.0108+00	NM	0.77629	0.90845	0.80170	0.77880	1.02940
12	6.4770-04	1.0113+00	NM	0.79248	0.92616	0.82470	0.79290	1.04011
13	7.7470-04	1.0117+00	NM	0.80526	0.94201	0.84350	0.80560	1.04953
14	1.0287-03	1.0121+00	NM	0.82655	0.95811	0.87120	0.82680	1.05370
15	1.2827-03	1.0123+00	NM	0.83920	0.96705	0.88600	0.83940	1.05552
16	1.5367-03	1.0124+00	NM	0.84913	0.97257	0.89630	0.84930	1.05534
17	2.0447-03	1.0125+00	NM	0.86316	0.97725	0.90800	0.86330	1.05178
18	2.8067-03	1.0126+00	NM	0.87446	0.97861	0.91520	0.87460	1.04642
19	3.8227-03	1.0126+00	NM	0.88687	0.98003	0.92300	0.88700	1.04059
20	5.0927-03	1.0127+00	NM	0.90228	0.98184	0.93270	0.90240	1.03358
21	6.3627-03	1.0127+00	NM	0.91669	0.98319	0.94140	0.91680	1.02683
22	7.6327-03	1.0128+00	NM	0.93041	0.98639	0.95150	0.93050	1.02257
23	1.0173-02	1.0129+00	NM	0.95684	0.99099	0.96940	0.95690	1.01306
24	1.2713-02	1.0130+00	NM	0.97476	0.99461	0.98200	0.97480	1.00739
25	1.5253-02	1.0131+00	NM	0.98398	0.99690	0.98990	0.98600	1.00396
26	2.0333-02	1.0131+00	NM	0.99440	1.00000	0.99720	0.99440	1.00282
D 27	2.5413-02	1.0131+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

72070105		BACK/CUFFEL	PROFILE TABULATION	33 POINTS, DELTA AT POINT 33				
I	Y	PT2/P	P/PD	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.49923	0.00000	0.00000	0.50300	0.00000
2	6.3500-05	1.0129+00	NM	0.68713	0.69593	0.57800	0.68980	0.83792
3	8.1280-05	1.0150+00	NM	0.69920	0.75004	0.62820	0.70150	0.89551
4	9.3980-05	1.0159+00	NM	0.70646	0.77330	0.65100	0.70870	0.91858
5	1.0930-04	1.0168+00	NM	0.71990	0.79468	0.67520	0.72190	0.93531
6	1.3208-04	1.0170+00	NM	0.72422	0.79819	0.68020	0.72620	0.93666
7	1.4478-04	1.0175+00	NM	0.72871	0.80983	0.69220	0.73060	0.94744
8	1.7018-04	1.0179+00	NM	0.73887	0.81893	0.70480	0.74070	0.95153
9	1.9558-04	1.0183+00	NM	0.74624	0.82799	0.71610	0.74800	0.95735
10	2.4634-04	1.0192+00	NM	0.75800	0.84803	0.73910	0.75960	0.97301
11	2.9718-04	1.0202+00	NM	0.76840	0.87077	0.76400	0.76980	0.99247
12	3.4798-04	1.0210+00	NM	0.77857	0.88839	0.78450	0.77980	1.00603
13	3.9878-04	1.0217+00	NM	0.78611	0.90268	0.80090	0.78720	1.01740
14	4.4958-04	1.0223+00	NM	0.79142	0.91415	0.81400	0.79290	1.02661
15	5.5118-04	1.0231+00	NM	0.80220	0.93137	0.83460	0.80300	1.03935
16	6.7818-04	1.0240+00	NM	0.81128	0.94826	0.85580	0.81450	1.05071
17	8.0518-04	1.0246+00	NM	0.82351	0.96935	0.87190	0.82600	1.05557
18	9.3218-04	1.0247+00	NM	0.83418	0.96556	0.88210	0.83460	1.05691
19	1.0592-03	1.0252+00	NM	0.84144	0.97090	0.89080	0.84180	1.05821
20	1.3132-03	1.0254+00	NM	0.85160	0.97629	0.90110	0.85190	1.05775
21	1.6212-03	1.0256+00	NM	0.86574	0.98012	0.91220	0.86620	1.05311
22	2.3292-03	1.0257+00	NM	0.87689	0.98085	0.91860	0.87710	1.04732
23	3.0912-03	1.0257+00	NM	0.88595	0.98122	0.92370	0.88620	1.04232
24	3.8532-03	1.0257+00	NM	0.89726	0.98167	0.93000	0.89750	1.03621
25	5.1232-03	1.0258+00	NM	0.91476	0.98217	0.93930	0.91460	1.02701
26	6.3932-03	1.0259+00	NM	0.93178	0.98409	0.95000	0.93200	1.01931
27	7.6632-03	1.0259+00	NM	0.94589	0.98553	0.95850	0.94610	1.01311
28	8.9332-03	1.0260+00	NM	0.96001	0.98653	0.96670	0.96020	1.00677
29	1.0203-02	1.0261+00	NM	0.97143	0.98823	0.97410	0.97160	1.00257
30	1.2743-02	1.0261+00	NM	0.98559	0.99222	0.98510	0.98570	0.99939
31	1.5283-02	1.0264+00	NM	0.99412	0.99479	0.99190	0.99420	0.99769
32	2.0363-02	1.0267+00	NM	1.00999	0.99930	0.99930	1.00000	0.99930
D 33	2.2903-02	1.0267+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

72070106		BACK/CUFFEL	PROFILE TABULATION	41 POINTS, DELTA AT POINT 41				
I	Y	PT2/P	P/PD	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.42616	0.00000	0.00000	1.39200	0.00000
2	6.3500-05	1.9728+00	NM	0.55208	0.30747	0.37470	1.48510	0.25231
3	8.3900-05	2.4442+00	NM	0.58982	0.36020	0.43950	1.48880	0.29520
4	1.1830-04	3.0130+00	NM	0.61964	0.41280	0.49880	1.46010	0.34162
5	1.3970-04	3.4947+00	NM	0.64933	0.45194	0.53250	1.44090	0.37650
6	1.6510-04	3.9373+00	NM	0.65601	0.46489	0.57330	1.39790	0.41012
7	2.1590-04	4.7107+00	NM	0.67057	0.53737	0.61830	1.32390	0.46703
8	2.6670-04	5.4130+00	NM	0.67998	0.58077	0.65160	1.25880	0.51764
9	3.1750-04	6.0058+00	NM	0.68600	0.61496	0.67550	1.20660	0.55984
10	3.9370-04	6.6684+00	NM	0.69654	0.63100	0.70130	1.16050	0.60431
11	4.6950-04	7.0873+00	NM	0.70678	0.67277	0.71620	1.13960	0.63022
12	5.7150-04	7.3484+00	NM	0.71782	0.68599	0.73070	1.13460	0.64402
13	6.9850-04	7.4971+00	NM	0.72843	0.69341	0.73990	1.13660	0.64983
14	8.2550-04	7.7582+00	NM	0.73792	0.70623	0.75120	1.13140	0.66396
15	1.0745-03	8.5641+00	NM	0.76040	0.74441	0.78110	1.10100	0.70945
16	1.3335-03	9.2743+00	NM	0.77364	0.77651	0.80240	1.06780	0.75145
17	1.5875-03	1.0033+01	NM	0.78694	0.80932	0.82320	1.03460	0.79567
18	1.8415-03	1.0679+01	NM	0.80131	0.83629	0.84150	1.01250	0.83111
19	2.0955-03	1.1271+01	NM	0.81117	0.86024	0.85580	0.98970	0.86471
20	2.6035-03	1.2345+01	NM	0.82905	0.90207	0.88020	0.95210	0.92448
21	3.1115-03	1.3324+01	NM	0.84523	0.93854	0.90090	0.92140	0.97775
22	3.6195-03	1.4451+01	NM	0.85949	0.96473	0.91670	0.90290	1.01528
23	4.1275-03	1.4453+01	NM	0.86739	0.97895	0.92520	0.89320	1.03583
24	5.1435-03	1.4903+01	NM	0.88577	0.99463	0.93960	0.89240	1.05289
25	6.4135-03	1.5219+01	NM	0.89197	1.00542	0.94600	0.88530	1.06856
26	7.6835-03	1.5416+01	NM	0.90405	1.01212	0.95430	0.88900	1.07345
27	1.0224-02	1.5614+01	NM	0.92348	1.01679	0.96640	0.89980	1.07402
28	1.2002-02	1.4733+01	NM	0.93703	1.02278	0.97460	0.90800	1.07335
29	1.2764-02	1.6174+01	NM	0.94338	1.03748	0.98200	0.89590	1.06610
30	1.3780-02	1.7813+01	NM	0.95178	1.02546	0.98300	0.91890	1.06976
31	1.5304-02	1.5826+01	NM	0.96066	1.02590	0.98780	0.92710	1.06547
32	1.6828-02	1.5946+01	NM	0.96701	1.02992	0.99210	0.92790	1.06619
33	1.8606-02	1.5884+01	NM	0.97572	1.02518	0.99520	0.94240	1.05603
34	2.2415-02	1.5791+01	NM	0.98383	1.02473	0.99920	0.95080	1.05090
35	2.4955-02	1.5561+01	NM	0.99301	1.01702	1.00160	0.96990	1.03268
36	2.6987-02	1.5645+01	NM	0.99593	1.01983	1.00390	0.96990	1.03602
37	2.8512-02	1.5195+01	NM	0.99601	1.00459	0.99940	0.98970	1.00980
38	2.9782-02	1.5164+01	NM	0.99686	1.00352	0.99950	0.99200	1.00756
39	3.0797-02	1.4824+01	NM	0.99703	0.99184	0.99600	1.00840	0.98770
40	3.2830-02	1.4739+01	NM	0.99847	0.98890	0.99580	1.01400	0.98205
D 41	3.5115-02	1.5061+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

SECTION D: ADDITIONAL DATA
 WALL TEMPERATURE, PRESSURE, AND HEAT FLUX
 AUTHORS UNITS

X, RZ - inches. TW - °R Q/A - BTU/in²sec. PO = 150.0 psia TO = 1500°R

Normalised average data, five runs. Brackets mark an interpolated value.

X AXIAL in	-RZ in	TW °R	PH/PO -	MD -	Q/A BTU/ in ² sec.
- 39.97	2.500	710	.99740	.06100	.1370
- 38.95	2.500	706	.99740	.06098	.1258
- 38.00	2.500	707	.99740	.06096	.1180
- 37.06	2.500	709	.99740	.06095	.1121
- 36.09	2.500	708	.99740	.06095	.1179
- 35.11	2.500	705	.99741	.06093	.1199
- 33.86	2.500	705	.99741	.06091	.1167
- 32.33	2.500	704	.99741	.06089	.1070
- 30.85	2.500	703	.99741	.06088	.1021
- 29.39	2.500	702	.99739	.06114	.1004
- 27.93	2.500	701	.99737	.06141	.1009
- 26.47	2.500	705	.99734	.06167	.0965
- 24.99	2.500	706	.99732	.06193	.1027
- 23.50	2.500	705	.99730	.06219	.0985
- 21.73	2.500	696	.99727	.06250	.0946
- 19.71	2.500	698	.99724	.06284	.0888
- 17.73	2.500	699	.99724	.06289	.0888
- 15.76	2.500	697	.99723	.06295	.0879
- 13.80	2.500	697	.99723	.06301	.0898
- 11.83	2.500	699	.99722	.06306	.0897
- 9.86	2.500	698	.99722	.06312	.0903
- 7.88	2.500	702	.99721	.06318	.0944
- 5.89	2.500	699	.99720	.06326	.0927
- 4.35	2.500	691	.99720	.06328	.0993
- 3.32	2.500	691	.99720	.06331	.0885
- 2.36	2.500	691	.99720	.06336	.0903
- 1.41	2.500	692	.99719	.06338	.0844
- 0.46	2.500	691	.99719	.06344	.0860
0.00	2.500	(691)	.9972	.06346	(.0904)
0.564	2.500	692	.9972	.06349	.0946
1.625	2.500	690	.9972	.06335	.0964
2.309	2.497	683	.9973	.06194	.1073
2.612	2.477	676	.9973	.06180	.0762
2.885	2.429	692	.9971	.06443	.0882
3.161	2.380	688	.9969	.06715	.0810
3.436	2.332	690	.9965	.07052	.0894
3.663	2.310	(691)			(.0945)
3.943	2.242	692	.9959	.07693	.0996
4.692	2.110	698	.9947	.08731	.1129
5.441	1.978	703	.9933	.09823	.1219
5.810	1.910	(707)			(.1335)
6.189	1.846	711	.9912	.11263	.1451
6.937	1.714	718	.9884	.12917	.1640
7.310	1.649	(724)			(.1694)
7.681	1.583	730	.9838	.15290	.1749
8.426	1.452	739	.9773	.18125	.1928
8.811	1.384	(743)			(.2129)
9.176	1.320	747	.9674	.21818	.2330
9.923	1.188	760	.9491	.2741	.2591
10.667	1.056	789	.9215	.3438	.3001

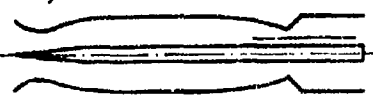
SECTION D (CONT.): ADDITIONAL DATA
WALL TEMPERATURE, PRESSURE, AND HEAT FLUX

AUTHORS UNITS

X, RZ - inches. TW - °R Q/A - BTU/in²sec. PO = 150.0 psia TO = 1500°R

Normalised average data, five runs. Brackets mark an interpolated value.

X AXIAL in	- RZ in	TW °R	PH/PO -	MD -	Q/A BTU/in ² sec.
11.189	0.966	812	.8780	.4351	.3088
11.465	0.916	834	.8403	.5048	.3309
11.741	0.867	842	.7897	.5907	.3469
12.032	0.816	810	.6605	.7931	.3732
12.336	0.798	806	.4807	1.0789	.3353
12.646	0.821	780	.2984	1.4366	.2996
12.933	0.872	783	.2554	1.5442	.2716
13.460	0.963	776	.1783	1.784	.2076
14.196	1.096	741	.1161	2.062	.1660
14.931	1.225	730	.0731	2.357	.1217
15.657	1.353	720	.0501	2.600	.0984
16.393	1.483	707	.0364	2.808	.0715
17.130	1.614	693	.0276	2.990	.0642
17.865	1.744	665	.0250	3.057	.0586
18.560	1.866	672	.0211	3.171	.0484
19.015	1.949	666	.0187	3.254	
19.315	2.004	660	.0171	3.315	.0472
19.752	2.084	658	.0152	3.395	.0428
20.294	2.184	655	.0144	3.435	.0380
20.789	2.274	(649)			(.0352)
20.830	2.282	649	.0120	3.563	.0352
21.369	2.380	647	.0104	3.662	.0316

	M : 6 falling to 4.6 R THETA X 10 ⁻³ : 96 - 140 TW/TR : 0.7	7208
		APG - MHT
Blow-down axisymmetrical tunnel with contoured nozzle. D = 0.3048 m. PO : 13.4 MN/m ² . TO : 460 K. Air. RE/m X 10 ⁻⁶ : 124.		
ZAKKAY V. and WANG C.-R., 1972. Turbulent boundary layer in an adverse pressure gradient without effect of wall curvature. NASA CR 11-2247.		

- 1 The test boundary layer was formed on an axisymmetric centre body. This started with a small diameter section passing through the throat and having a streamlined nose. The nose section was faired into a parallel sided section 116.5 mm in diameter. The test region started at 0.1554 m downstream of the throat. (X = 0). A contoured compression sleeve was fitted inside the tunnel test section, and formed a compression
- 4 which was focused onto the centre body. The static pressure then increased approximately linearly from X = 0 to X = 120 mm, then rather more rapidly before reaching a maximum at about X = 190 mm, and then
- 6 falling. The pressure increased, overall, by a factor of about seven. The cylindrical portion of the model was equipped with pressure taps and thermocouples at approximately 10 mm [E] intervals. Heat transfer was determined using the transient thin-wall technique.
- 7 A combined, triple, probe was used to measure Pitot, TO and static pressure profiles. The FPP was made from flattened 1 mm tube so that at the tip [E] $h_1 = 0.35$, $h_2 = 0.05$ mm. The TTP was an "unshielded" open tip chromel-alumel thermocouple about [E] 1 mm in diameter. The SPP "had a conical tip faired into" a 1 mm diameter tube. The available sketch suggests that [E] the effective slender length of the probes was of the order of 10 mm. The SPP was mounted in the centre, with the FPP and the TTP 3.2 mm to either side.
- 9 No details are given of reduction or interpolation procedures. The integral data, presented graphically, uses a pressure-based reference flow. No profile corrections are reported, nor is the viscosity law used.
- 11
- 12 The editors present the eight profiles measured. These are given in the source directly as measured by the SPP, the TPP and the TTP. We have reduced the data assuming the test gas to be air. The heat transfer data given has been scaled from the original graphical presentation. We have selected a D-state on the basis of the computed PO values.
- 13 The eight profiles form a sequence, with the first five showing the development from a near-constant-pressure region through the compression, and the last three describing a region in which, again, the flow is not varying rapidly. Heat transfer values appropriate to the profiles have been interpolated by the editors.
- 14
- 5 DATA 7208 0101-0108. Pitot, TO and P profiles obtained simultaneously. NX = 8. Heat transfer data from the transient technique.
- 15 Editors' comments
- The experiment describes a very interesting and difficult flow case. Unfortunately the data is not of particularly good quality, and is very badly reported. Much of the description above has required considerable imagination on the part of the editors. New and more careful data of this type would be valuable.
- The flow undergoes a very strong reflected-wave compression, and streamline curvature is quite marked at relatively small distances from the straight wall, so that there are large normal pressure gradients. Hence SM has been arbitrarily set at 0.5. There will also be a "focusing" of the compression wave as the waves approach the axis, in contrast to the other reflected wave compression experiments (Peake et al. - CAT 7102, Lewis et al. - CAT 7201) in which the compression is radiated out from a centrebody. Effects of transverse curvature are likely to be significant, as d/RZ is of order 0.2.
- There are relatively few data points in each profile, and, in half the cases, measurements do not extend within the momentum deficit peak.

CAT 7208 ZAKKAY BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X RZ *	MD * PO TOD*	TW/TR PW/PD SM *	RED2W RED2O O2	CF CO * PI2	H1Z H3Z H4Z	H12K H32K D2K	PH* TK* UD	PD* TD TR
72080101	6.0000	0.7190	1.7962 ⁺⁰⁴	NM	14.7096	1.4747	9.2000 ⁺⁰³	6.6000 ⁺⁰³
NM	1.3578 ⁺⁰⁷	1.0698	8.3303 ⁺⁰⁴	6.8649 ⁻⁰⁵	1.8608	1.8154	2.9400 ⁺⁰²	5.4878 ⁺⁰¹
5.8250 ⁻⁰²	4.5000 ⁺⁰²	0.5000	6.7335 ⁻⁰⁴	NC	0.1121	1.8047 ⁻⁰³	6.9117 ⁺⁰²	4.0891 ⁺⁰²
72080102	5.6000	0.7098	2.5829 ⁺⁰⁴	NM	8.1243	1.5046	1.6500 ⁺⁰⁴	1.1700 ⁺⁰⁴
3.8100 ⁻⁰²	1.2133 ⁺⁰⁷	1.4103	1.0497 ⁺⁰⁵	9.5661 ⁻⁰⁵	1.8356	1.7918	2.9400 ⁺⁰²	6.2569 ⁺⁰¹
5.8250 ⁻⁰²	4.5900 ⁺⁰²	0.5000	8.1423 ⁻⁰⁴	NC	0.2789	1.6332 ⁻⁰³	8.8813 ⁺⁰²	4.1419 ⁺⁰²
72080103	5.3500	0.7152	2.6774 ⁺⁰⁴	NM	9.9820	1.5606	2.2000 ⁺⁰⁴	1.5800 ⁺⁰⁴
6.9800 ⁻⁰²	1.2459 ⁺⁰⁷	1.3924	1.0148 ⁺⁰⁵	9.5510 ⁻⁰⁶	1.8088	1.7768	2.9400 ⁺⁰²	6.7068 ⁺⁰¹
5.8250 ⁻⁰²	4.5100 ⁺⁰²	0.5000	6.7731 ⁻⁰⁴	NC	0.2921	1.4522 ⁻⁰³	8.7846 ⁺⁰²	4.1107 ⁺⁰²
72080104	4.4000	0.7008	3.2724 ⁺⁰⁴	NM	5.2605	1.5712	2.9300 ⁺⁰⁴	1.7900 ⁺⁰⁴
1.0160 ⁻⁰¹	8.4212 ⁺⁰⁶	1.6369	1.0523 ⁺⁰⁵	1.2562 ⁻⁰⁵	1.8138	1.7717	2.9400 ⁺⁰²	7.9111 ⁺⁰¹
5.8250 ⁻⁰²	4.5900 ⁺⁰²	0.5000	8.6648 ⁻⁰⁴	NC	0.2861	1.4841 ⁻⁰³	8.7382 ⁺⁰²	4.1949 ⁺⁰²
72080105	4.8000	0.7019	3.3385 ⁺⁰⁴	NM	3.6632	1.5659	3.3800 ⁺⁰⁴	1.9300 ⁺⁰⁴
1.3340 ⁻⁰¹	5.0809 ⁺⁰⁶	1.7513	1.0404 ⁺⁰⁵	1.5601 ⁻⁰⁵	1.8363	1.7987	2.9400 ⁺⁰²	8.1669 ⁺⁰¹
5.8250 ⁻⁰²	4.5800 ⁺⁰²	0.5000	8.5037 ⁻⁰⁴	NC	0.2674	1.2498 ⁻⁰³	8.6972 ⁺⁰²	4.1886 ⁺⁰²
72080106	4.6000	0.6933	3.4761 ⁺⁰⁴	NM	2.4959	1.6375	4.2000 ⁺⁰⁴	2.6800 ⁺⁰⁴
1.6260 ⁻⁰¹	8.7795 ⁺⁰⁶	1.5672	1.0013 ⁺⁰⁵	1.3904 ⁻⁰⁵	1.8447	1.8215	2.9400 ⁺⁰²	8.8494 ⁺⁰¹
5.8250 ⁻⁰²	4.6300 ⁺⁰²	0.5000	6.9260 ⁻⁰⁴	NC	0.3661	9.8589 ⁻⁰⁴	8.6761 ⁺⁰²	4.2405 ⁺⁰²
72080107	4.6000	0.7133	4.4774 ⁺⁰⁴	NM	3.7044	1.6421	5.4100 ⁺⁰⁴	3.1700 ⁺⁰⁴
1.9050 ⁻⁰¹	1.0385 ⁺⁰⁷	1.7066	1.3261 ⁺⁰⁵	1.2588 ⁻⁰⁵	1.8144	1.7922	2.9400 ⁺⁰²	8.6009 ⁺⁰¹
5.8250 ⁻⁰²	4.5000 ⁺⁰²	0.5000	7.4395 ⁻⁰⁴	NC	0.3009	1.0850 ⁻⁰³	8.5534 ⁺⁰²	4.1214 ⁺⁰²
72080108	4.6000	0.7609	4.3718 ⁺⁰⁴	NM	0.2292	1.8183	4.8300 ⁺⁰⁴	2.6800 ⁺⁰⁴
2.1640 ⁻⁰¹	8.7795 ⁺⁰⁶	1.8022	1.2727 ⁺⁰⁵	NM	1.8491	1.8548	2.9400 ⁺⁰²	8.7538 ⁺⁰¹
5.8250 ⁻⁰²	4.5800 ⁺⁰²	0.5000	8.6636 ⁻⁰⁴	NC	0.3645	9.8095 ⁻⁰⁴	8.6291 ⁺⁰²	4.1947 ⁺⁰²

TRAPEZOIDAL RULE FOR RUN 0108

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PDD RED2PWD	HED2PDW RED2PDW	DATA
72080101	6.6177 ⁻⁰⁴ 6.3523 ⁻⁰⁴	14.8432 14.8609	1.8616 1.8649	0.1110 0.1104	8.1970 ⁺⁰⁴ 8.2121 ⁺⁰⁴	1.7675 ⁺⁰⁴ 1.7707 ⁺⁰⁴	9.8484 ⁻⁰³
72080102	7.0596 ⁻⁰⁴ 5.4382 ⁻⁰⁴	14.3541 14.5084	1.8531 1.8660	0.2583 0.2585	9.1119 ⁺⁰⁴ 9.1776 ⁺⁰⁴	2.2422 ⁺⁰⁴ 2.2583 ⁺⁰⁴	9.8387 ⁻⁰³
72080103	5.7562 ⁻⁰⁴ 4.5156 ⁻⁰⁴	13.9947 14.0832	1.8259 1.8397	0.2688 0.2688	8.6352 ⁺⁰⁴ 8.7027 ⁺⁰⁴	2.2782 ⁺⁰⁴ 2.2960 ⁺⁰⁴	7.8799 ⁻⁰³
72080104	7.9804 ⁻⁰⁴ 4.9369 ⁻⁰⁴	15.1817 15.6152	1.8687 1.8805	0.2058 0.2045	9.7037 ⁺⁰⁴ 9.7691 ⁺⁰⁴	3.0175 ⁺⁰⁴ 3.0378 ⁺⁰⁴	1.0954 ⁻⁰²
72080105	8.0536 ⁻⁰⁴ 4.6963 ⁻⁰⁴	13.5154 13.9729	1.8968 1.8986	0.1723 0.1721	7.8652 ⁺⁰⁴ 8.0774 ⁺⁰⁴	3.1656 ⁺⁰⁴ 3.1895 ⁺⁰⁴	9.4067 ⁻⁰³
72080106	5.8997 ⁻⁰⁴ 3.8067 ⁻⁰⁴	13.4655 13.6579	1.8772 1.8940	0.2952 0.2930	8.5392 ⁺⁰⁴ 8.6088 ⁺⁰⁴	2.9645 ⁺⁰⁴ 2.9887 ⁺⁰⁴	6.9530 ⁻⁰³
72080107	7.0716 ⁻⁰⁴ 4.5879 ⁻⁰⁴	9.2566 9.3974	1.8769 1.8825	0.2082 0.2076	1.2627 ⁺⁰⁵ 1.2668 ⁺⁰⁵	4.2634 ⁺⁰⁴ 4.2772 ⁺⁰⁴	6.0996 ⁻⁰³
72080108	6.1807 ⁻⁰⁴ 3.5986 ⁻⁰⁴	13.8996 14.0533	1.8910 1.9223	0.3150 0.3102	8.9729 ⁺⁰⁴ 9.1243 ⁺⁰⁴	3.0822 ⁺⁰⁴ 3.1342 ⁺⁰⁴	7.4022 ⁻⁰³

72080102		ZAKKAY	PROFILE TABULATION		20 POINTS, DELTA AT POINT 20				
I	Y	RTZ/P	P/PD	T0/T0D	H/HD	U/UH	T/TD	RHC/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.41026	0.64615	0.00000	0.00000	5.41236	0.00000	
2	1.3000*-03	5.0461*+00	1.41026	0.88132	0.33575	0.67400	4.03065	0.23584	
3	2.6000*-03	4.2182*+00	1.38462	0.89890	0.37675	0.72256	3.67430	0.27199	
4	3.9000*-03	8.5667*+00	1.29060	0.92308	0.44755	0.79065	3.12086	0.32696	
5	5.2000*-03	1.0653*+01	1.08547	0.94066	0.50206	0.83343	2.75666	0.38229	
6	6.5000*-03	1.4198*+01	1.05983	0.95165	0.58307	0.87497	2.27246	0.40993	
7	7.8000*-03	1.5434*+01	1.23432	0.96484	0.60876	0.89565	2.16461	0.51279	
8	9.1000*-03	1.9079*+01	1.23932	0.98022	0.67891	0.92743	1.86612	0.61592	
9	1.0400*-02	2.2509*+01	1.21368	0.98901	0.73884	0.94851	1.64806	0.69850	
10	1.1700*-02	2.8110*+01	1.17949	1.00000	0.82743	0.97359	1.38446	0.82944	
11	1.3000*-02	3.4151*+01	1.14530	1.00000	0.91339	0.98835	1.17088	0.96676	
12	1.4300*-02	3.5302*+01	1.17949	1.00000	0.92667	0.99064	1.13743	1.02727	
13	1.5600*-02	3.6339*+01	1.14530	1.00000	0.94286	0.99263	1.10835	1.02572	
14	1.6900*-02	3.5302*+01	1.17949	1.00000	0.92807	0.99064	1.13743	1.02727	
15	1.8200*-02	3.5549*+01	1.17949	1.00000	0.93216	0.99111	1.13049	1.03407	
16	1.9500*-02	3.5822*+01	1.20513	1.00000	0.93578	0.99163	1.12203	1.06422	
17	2.0800*-02	3.6234*+01	1.17949	1.00000	0.94122	0.99240	1.11172	1.05289	
18	2.2100*-02	3.7093*+01	1.08547	1.00000	0.96295	0.99535	1.06843	1.01123	
19	2.3400*-02	3.9601*+01	1.02564	1.00000	0.98452	0.99811	1.02780	0.99602	
D 20	2.4700*-02	4.0841*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

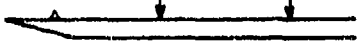
INPUT VARIABLES Y,P,T0,H

72080104		ZAKKAY	PROFILE TABULATION		20 POINTS, DELTA AT POINT 20				
I	Y	RTZ/P	P/PD	T0/T0D	H/HD	U/UH	T/TD	RHC/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.63687	0.64052	0.00000	0.00000	4.99167	0.00000	
2	1.3000*-03	3.8151*+00	1.63687	0.87146	0.32704	0.64822	3.93346	0.26992	
3	2.6000*-03	5.0470*+00	1.61453	0.89760	0.38363	0.71753	3.49767	0.33121	
4	3.9000*-03	6.9203*+00	1.53631	0.92375	0.44183	0.77727	3.09479	0.38585	
5	5.2000*-03	9.3200*+00	1.42458	0.93900	0.53483	0.84333	2.48637	0.48319	
6	6.5000*-03	1.1591*+01	1.42458	0.96078	0.59969	0.88436	2.17470	0.57932	
7	7.8000*-03	1.5303*+01	1.36313	0.97821	0.69269	0.92669	1.78974	0.70580	
8	9.1000*-03	1.9241*+01	1.36313	0.99129	0.77968	0.95883	1.50601	0.86609	
9	1.0400*-02	2.3531*+01	1.40782	1.00000	0.86376	0.97885	1.28425	1.07304	
10	1.1700*-02	2.9648*+01	1.38547	1.00000	0.90254	0.98571	1.19279	1.14494	
11	1.3000*-02	2.6546*+01	1.32961	1.00000	0.91850	0.98832	1.15781	1.13497	
12	1.4300*-02	2.7144*+01	1.22905	1.00000	0.92896	0.98997	1.13565	1.07139	
13	1.5600*-02	2.8379*+01	1.11732	1.00000	0.95024	0.99318	1.09241	1.01582	
14	1.6900*-02	2.8876*+01	1.11732	1.00000	0.95865	0.99439	1.07590	1.03261	
15	1.8200*-02	2.8846*+01	1.07821	1.00000	0.95882	0.99442	1.07563	0.99680	
16	1.9500*-02	2.9448*+01	1.03911	1.00000	0.96826	0.99575	1.05760	0.97634	
17	2.0800*-02	3.0307*+01	1.00000	1.00000	0.98250	0.99770	1.03119	0.96753	
18	2.2100*-02	3.1093*+01	0.98324	1.00000	0.99537	0.99940	1.00812	0.97473	
19	2.3400*-02	3.1421*+01	0.98324	1.00000	1.00069	1.00009	0.99880	0.98450	
D 20	2.4700*-02	3.1379*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,P,T0,H

72080106		ZAKKAY	PROFILE TABULATION		20 POINTS, DELTA AT POINT 15				
I	Y	RTZ/P	P/PD	T0/T0D	H/HD	U/UH	T/TD	RHC/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	1.60224	0.64192	0.00000	0.00000	3.92902	0.00000	
2	1.3000*-03	7.6485*+00	1.72388	0.91266	0.51146	0.74032	2.38771	0.57060	
3	2.6000*-03	8.1740*+00	1.78731	0.92576	0.53142	0.80882	2.31644	0.62407	
4	3.9000*-03	1.1549*+01	1.60821	0.93450	0.63874	0.86914	1.85157	0.75491	
5	5.2000*-03	1.4048*+01	1.36716	0.95652	0.70543	0.90727	1.65177	0.86080	
6	6.5000*-03	1.6340*+01	1.55597	0.96725	0.76324	0.93052	1.48638	0.97409	
7	7.8000*-03	1.9661*+01	1.54104	0.98908	0.83933	0.96210	1.31395	1.12639	
8	9.1000*-03	2.2197*+01	1.51866	0.99782	0.89308	0.97882	1.20123	1.23746	
9	1.0400*-02	2.3693*+01	1.49254	1.00000	0.92332	0.98616	1.14075	1.29027	
10	1.1700*-02	2.3972*+01	1.44030	1.00000	0.92885	0.98725	1.12970	1.25869	
11	1.3000*-02	2.4627*+01	1.35075	1.00000	0.94170	0.99073	1.10461	1.21027	
12	1.4300*-02	2.5239*+01	1.23307	1.00000	0.95356	0.99145	1.08214	1.13214	
13	1.5600*-02	2.6203*+01	1.13060	1.00000	0.97194	0.99525	1.04855	1.07313	
14	1.6900*-02	2.6560*+01	1.06716	1.00000	0.97866	0.99642	1.03663	1.02577	
D 15	1.8200*-02	2.7710*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
16	1.9500*-02	2.7764*+01	0.95149	1.00000	1.00099	1.00016	0.99835	0.95322	
17	2.0800*-02	2.8556*+01	0.88806	1.00000	1.01542	1.00247	0.97467	0.91339	
18	2.2100*-02	2.9349*+01	0.82090	1.00000	1.02964	1.00467	0.95208	0.86624	
19	2.3400*-02	3.0007*+01	0.74627	1.00000	1.04130	1.00641	0.93411	0.80403	
20	2.4700*-02	2.9962*+01	0.68284	1.00000	1.04051	1.00630	0.93331	0.73466	

INPUT VARIABLES Y,P,T0,H

	M : 7.5 - 7.8 R THETA X 10 ⁻³ : 6 - 10 TW/TR : 0.8	7209
		ZPG (Recovery) MHT
Blow-down tunnel with axi-symmetric contoured nozzle. D = 0.53 m. Air, P ₀ : 14 MN/m ² , T ₀ : 840 K, RE/m X 10 ⁻⁶ : 20.		
STONE D.R. and CARY A.M. 1972. Discrete sonic jets used as boundary-layer trips at Mach number of 6 and 8.5. NASA TN D 6802. And Morrisette, Stone and Cary. (1968), Stone, (1971), Morrisette E.L., private communication.		

- 1 The test boundary layer was formed on the surface of a flat-plate model (L = 0.521, W = 0.279 m) with a leading edge (X = 0) 0.03 mm thick and chamfered at 15° on the underside. From X = 38 mm back the working surface consisted of a removable plate. Two were used, one for heat transfer studies, and the other for
- 3 the profile studies reported here. At X = 25 mm, a row of 17 jet orifices was drilled. These were spaced symmetrically about the centreline at intervals of 6.4 mm, and converged from a supply pipe diameter of 2.3 mm to a parallel sided outlet 0.8 mm long and 0.4 mm in diameter at the test surface. (A second such row at X = 76 mm could be employed on the heat transfer model.) When employed, the discharge through the jets was at a constant value, 2.5, of a "mass flow parameter" λ where $\lambda = P_{0j} \gamma_j / P_{\infty} M_{\infty}^2 \gamma_{\infty}$. The boundary layer could also be tripped by spherical balls of 1.5 mm diameter at X = 12.7 mm, or of 3.0 mm diameter at X = 25.4 mm. The balls were distributed symmetrically at intervals of 50.8 and 12.0 mm respectively, and spanned the full width of the plate. The test plates were provided with sharp, swept side plates. Surface oil flow patterns were observed, but two-dimensionality in the region of profile measurements is not reported. An oil pattern published by Morrisette et al. (1968) in a not dissimilar case shows strong three dimensional effects in the immediate vicinity of the trips, but little or no large-scale divergence far downstream.
- 6 The central 19 mm of the heat transfer plate was reduced in thickness from 3.18 mm to 0.8 mm and instrumented with 95 thermocouples to allow heat-flux determination by the thin wall transient technique. These
- 3 measurements showed that the mass flow, at X = 1.0 was sufficient to cause transition as defined by a local peak heat flux, at X = 127 mm. The mass flow was such that any further increase would not cause transition to move further forward. (For these tests, however, TW/TR was about 0.45).
- 6 The pressure plate, also used for profile measurements, had three rows of static holes (d = 2.3 mm) in the central 40 mm of the plate. The total number was 36, the greater number providing a very close grid for X less than 200 mm. The largest interval downstream was less than 50 mm. The plate also had three thermocouples mounted 18 mm off the centre line at X = 168, 280 and 485 mm.
- 7 Pitot and T₀ profiles were measured at two stations for which X = 0.279 and 0.465 mm. The Pitot probe was
- 8 an FPP for which h₁ = 0.25, h₂ = 0.18, b₁ = 2.03, b₂ = 1.42 mm. The T₀ probe was an STP with a constant d₁ of 1.9 mm. The interior of the probe tip was chamfered so as to give a sharp leading edge. The thermocouple was mounted 0.8 mm back from the probe face and there were two vent-holes (d = 0.04 mm) 3.6 mm back. The probe was calibrated over a wide range of Reynolds number at M = 3.6 and 8.5, and found to have a probe recovery factor near to one, which value was assumed for all subsequent work.
- 9 The authors have interpolated T₀ profile measurements to the Y values of the Pitot profiles, and extrapolated the T₀ profile at low values of Y so as to match the wall temperature. Static pressure has been assumed
- 10 constant through the layer. No probe corrections have been applied, and Sutherland's viscosity law was used.
- 11
- 12 All profiles tabulated by the authors have been presented, incorporating the authors' procedures. While a
- 13 great deal of heat transfer data was obtained, it is only presented as small scale graphs and is not
- 14 reproduced here. The profiles consist of a single reference profile taken with natural transition, and three pairs for the jet trip (0201/2), the small ball trip (U301/2) and the large ball trip (0401/2).

5 DATA: 7209 0101 0402. Pitot and TO profiles obtained separately. NX = 2.

15 Editors' comments

The interest of this experiment lies in the effect of the relatively brutal tripping devices used. The reference case, 0101, is turbulent but still markedly transitional, while the downstream tripped profiles are relatively well developed and fully turbulent in character. We find less distortion introduced by the trips than is reported by the authors, and in general the interesting result is that the trips, at least at the downstream station of the two, do not seem to leave any special mark on the mean profile characteristics. On a transformed log-law plot, no effect can be seen which could not be accounted for by the general experimental scatter. Tests in the same range with no trip, or modest trips, are described by Danberg - CAT 6702 and Keener & Hopkins - CAT 7204. Abruptly disturbed flows, but in different experimental ranges, are the step flow of Moore - CAT 5805 and the flow over a rectangular cross-section protrusion described by Peake et al. - CAT 7102.

CAT 7209		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	STONE	TW/TR	RED2W	CF	H12	H12K	PH	PD	
X *	MD *	PW/PD*	RED2D	CG	H32	H32K	TW*	TD	
RZ	TOD*	SH *	D2	F12*	H42	D2K	UD	TR	
72090101	7.8200	0.8054	9.6805 ⁺⁰²	NM	14.9431	1.4544	1.6038 ⁺⁰³	1.6038 ⁺⁰³	
4.5500 ⁻⁰¹	1.3510 ⁺⁰⁷	1.0000	6.5609 ⁺⁰³	NM	1.8907	1.8040	6.0642 ⁺⁰²	6.2961 ⁺⁰¹	
INFINITE	8.3300 ⁺⁰²	0.0000	2.6839 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.6873	6.5647 ⁻⁰⁴	1.2441 ⁺⁰³	7.5292 ⁺⁰²	
72090201	7.7400	0.7489	1.1046 ⁺⁰³	NM	14.4141	1.3864	1.7495 ⁺⁰³	1.7495 ⁺⁰³	
2.7900 ⁻⁰¹	1.3790 ⁺⁰⁷	1.0000	8.9671 ⁺⁰³	NM	1.8744	1.8068	5.7159 ⁺⁰²	6.5015 ⁺⁰¹	
INFINITE	8.4400 ⁺⁰²	0.0000	2.7702 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.6967	7.1863 ⁻⁰⁴	1.2513 ⁺⁰³	7.6299 ⁺⁰²	
72090202	7.7800	0.7666	1.5120 ⁺⁰³	NM	16.5466	1.3593	1.6836 ⁺⁰³	1.6836 ⁺⁰³	
4.5500 ⁻⁰¹	1.3720 ⁺⁰⁷	1.0000	9.8229 ⁺⁰³	NM	1.8712	1.8067	5.7727 ⁺⁰²	6.3560 ⁺⁰¹	
INFINITE	8.3300 ⁺⁰²	0.0000	3.4026 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.7528	1.0798 ⁻⁰³	1.2436 ⁺⁰³	7.5298 ⁺⁰²	
72090301	7.5500	0.7740	1.3079 ⁺⁰³	NM	17.0201	1.4268	2.0537 ⁺⁰³	2.0537 ⁺⁰³	
2.7900 ⁻⁰¹	1.3790 ⁺⁰⁷	1.0000	8.0926 ⁺⁰³	NM	1.8601	1.7924	5.8310 ⁺⁰²	6.7175 ⁺⁰¹	
INFINITE	8.3300 ⁺⁰²	0.0000	2.9516 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.6801	8.7867 ⁻⁰⁴	1.2407 ⁺⁰³	7.5335 ⁺⁰²	
72090302	7.8000	0.8076	1.4368 ⁺⁰³	NM	17.9876	1.3880	1.6680 ⁺⁰³	1.6680 ⁺⁰³	
4.5500 ⁻⁰¹	1.3820 ⁺⁰⁷	1.0000	9.6973 ⁺⁰³	NM	1.8694	1.8021	6.1028 ⁺⁰²	6.3487 ⁺⁰¹	
INFINITE	8.3600 ⁺⁰²	0.0000	3.6722 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.6714	1.1387 ⁻⁰³	1.2461 ⁺⁰³	7.5566 ⁺⁰²	
72090401	7.5400	0.7740	1.4433 ⁺⁰³	NM	21.1472	1.4433	2.0712 ⁺⁰³	2.0712 ⁺⁰³	
2.7900 ⁻⁰¹	1.3790 ⁺⁰⁷	1.0000	8.9087 ⁺⁰³	NM	1.8558	1.7872	5.8310 ⁺⁰²	6.7339 ⁺⁰¹	
INFINITE	8.3300 ⁺⁰²	0.0000	3.2377 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.3657	1.0250 ⁻⁰³	1.2405 ⁺⁰³	7.5337 ⁺⁰²	
72090402	7.8700	0.7967	1.3245 ⁺⁰³	NM	20.2526	1.5305	1.5663 ⁺⁰³	1.5663 ⁺⁰³	
4.5500 ⁻⁰¹	1.3750 ⁺⁰⁷	1.0000	8.9920 ⁺⁰³	NM	1.8493	1.7560	6.0480 ⁺⁰²	6.2746 ⁺⁰¹	
INFINITE	8.4000 ⁺⁰²	0.0000	3.7233 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.5865	1.2641 ⁻⁰³	1.2499 ⁺⁰³	7.5917 ⁺⁰²	

72090101		STONE		PROFILE TABULATION		25 POINTS, DELTA AT POINT 25			
I	Y	P2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.72800	0.00000	0.00000	9.63179	0.00000	
2	1.0000 ⁻⁰⁴	2.3747 ⁺⁰⁰	NM	0.81972	0.15200	0.44200	8.45585	0.05227	
3	1.9000 ⁻⁰⁴	2.6570 ⁺⁰⁰	NM	0.81797	0.16400	0.44800	8.14337	0.05747	
4	2.8000 ⁻⁰⁴	2.7836 ⁺⁰⁰	NM	0.83994	0.16900	0.44500	8.23586	0.05889	
5	3.8000 ⁻⁰⁴	5.7307 ⁺⁰⁰	NM	0.85963	0.25800	0.64600	6.26939	0.10304	
6	7.7000 ⁻⁰⁴	1.2757 ⁺⁰¹	NM	0.89491	0.39500	0.77700	4.07120	0.19577	
7	1.1200 ⁻⁰³	1.6698 ⁺⁰¹	NM	0.90885	0.45400	0.83900	3.41517	0.24561	
8	1.5200 ⁻⁰³	1.9142 ⁺⁰¹	NM	0.91300	0.40700	0.85700	3.09673	0.27674	
9	1.8800 ⁻⁰³	2.1350 ⁺⁰¹	NM	0.91539	0.51500	0.87000	2.85380	0.30486	
10	2.4000 ⁻⁰³	2.5246 ⁺⁰¹	NM	0.92039	0.56100	0.88900	2.51118	0.35402	
11	3.0500 ⁻⁰³	2.9190 ⁺⁰¹	NM	0.92476	0.60400	0.90400	2.24008	0.40356	
12	3.4700 ⁻⁰³	3.2816 ⁺⁰¹	NM	0.92796	0.64100	0.91500	2.03763	0.44905	
13	4.1000 ⁻⁰³	3.7625 ⁺⁰¹	NM	0.93401	0.68700	0.92800	1.82466	0.50859	
14	4.5000 ⁻⁰³	4.0829 ⁺⁰¹	NM	0.93704	0.71600	0.93500	1.70529	0.54830	
15	5.0800 ⁻⁰³	4.5584 ⁺⁰¹	NM	0.94331	0.75700	0.94500	1.55837	0.60640	
16	5.5600 ⁻⁰³	5.0981 ⁺⁰¹	NM	0.94854	0.80100	0.95400	1.41851	0.67254	
17	6.2200 ⁻⁰³	5.7216 ⁺⁰¹	NM	0.95650	0.84900	0.96400	1.28925	0.74772	
18	6.9900 ⁻⁰³	6.4098 ⁺⁰¹	NM	0.96369	0.89900	0.97400	1.17381	0.82976	
19	7.5100 ⁻⁰³	6.8416 ⁺⁰¹	NM	0.97390	0.92900	0.98100	1.11588	0.87976	
20	8.1700 ⁻⁰³	7.2724 ⁺⁰¹	NM	0.98276	0.95600	0.98800	1.06361	0.92891	
21	8.6700 ⁻⁰³	7.5465 ⁺⁰¹	NM	0.98777	0.97600	0.99200	1.03306	0.96026	
22	9.1300 ⁻⁰³	7.8855 ⁺⁰¹	NM	0.99432	0.98500	0.99600	1.02246	0.97412	
23	9.8900 ⁻⁰³	7.8414 ⁺⁰¹	NM	0.99676	0.99500	0.99800	1.00604	0.99201	
24	1.0550 ⁻⁰²	7.9042 ⁺⁰¹	NM	0.99815	0.99900	0.99900	1.00000	0.99900	
D 25	1.1100 ⁻⁰²	7.9199 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD,U/UD ASSUME P/PPD

72090202		STONE		PROFILE TABULATION		27 POINTS, DELTA AT POINT 27			
I	Y	P2/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD	U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.69300	0.00000	0.00000	9.08224	0.00000	
2	1.8000 ⁻⁰⁴	1.9010 ⁺⁰⁰	NM	0.79549	0.12900	0.38000	8.67736	0.04379	
3	2.8000 ⁻⁰⁴	2.4247 ⁺⁰⁰	NM	0.81915	0.19500	0.44700	8.31671	0.05375	
4	6.8000 ⁻⁰⁴	5.8387 ⁺⁰⁰	NM	0.85726	0.26200	0.64900	6.13602	0.10577	
5	1.0200 ⁻⁰³	9.5389 ⁺⁰⁰	NM	0.86983	0.34100	0.74200	4.73477	0.15671	
6	1.5200 ⁻⁰³	1.1846 ⁺⁰¹	NM	0.88236	0.38200	0.78100	4.17999	0.18684	
7	2.0600 ⁻⁰³	1.3700 ⁺⁰¹	NM	0.88546	0.41200	0.80300	3.79871	0.21139	
8	2.5400 ⁻⁰³	1.5353 ⁺⁰¹	NM	0.89628	0.43700	0.82300	3.54680	0.23204	
9	3.2500 ⁻⁰³	1.8574 ⁺⁰¹	NM	0.90679	0.48200	0.85100	3.11720	0.27300	
10	4.0600 ⁻⁰³	2.1703 ⁺⁰¹	NM	0.91950	0.52200	0.87400	2.80338	0.31177	
11	4.6700 ⁻⁰³	2.5149 ⁺⁰¹	NM	0.92857	0.56300	0.89300	2.51586	0.35495	
12	5.2600 ⁻⁰³	2.8428 ⁺⁰¹	NM	0.93276	0.59900	0.90600	2.28772	0.39693	
13	5.7700 ⁻⁰³	3.1495 ⁺⁰¹	NM	0.93757	0.63100	0.91700	2.11193	0.43420	
14	6.9500 ⁻⁰³	3.6078 ⁺⁰¹	NM	0.94332	0.67600	0.93000	1.89266	0.49137	
15	7.1400 ⁻⁰³	3.9972 ⁺⁰¹	NM	0.94716	0.71200	0.93900	1.73929	0.53986	
16	7.5900 ⁻⁰³	4.2795 ⁺⁰¹	NM	0.95033	0.73700	0.94500	1.64410	0.57478	
17	8.3800 ⁻⁰³	4.8121 ⁺⁰¹	NM	0.95423	0.78200	0.95400	1.48828	0.64101	
18	9.1700 ⁻⁰³	5.3893 ⁺⁰¹	NM	0.95982	0.82800	0.96300	1.35267	0.71193	
19	9.7800 ⁻⁰³	5.8102 ⁺⁰¹	NM	0.96618	0.86000	0.97000	1.27217	0.76247	
20	1.0390 ⁻⁰²	6.2471 ⁺⁰¹	NM	0.97323	0.89200	0.97700	1.19966	0.81440	
21	1.0800 ⁻⁰²	6.5425 ⁺⁰¹	NM	0.97702	0.91500	0.98100	1.15451	0.84971	
22	1.1180 ⁻⁰²	6.7433 ⁺⁰¹	NM	0.98035	0.92700	0.98400	1.12676	0.87330	
23	1.1660 ⁻⁰²	7.0059 ⁺⁰¹	NM	0.98507	0.94500	0.98800	1.09308	0.90387	
24	1.2140 ⁻⁰²	7.2286 ⁺⁰¹	NM	0.99045	0.96000	0.99200	1.06778	0.92903	
25	1.2500 ⁻⁰²	7.3337 ⁺⁰¹	NM	0.99327	0.96700	0.99400	1.05662	0.94073	
26	1.4930 ⁻⁰²	7.6537 ⁺⁰¹	NM	0.99986	0.98800	0.99900	1.02239	0.97712	
D 27	1.7400 ⁻⁰²	7.8396 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD,U/UD ASSUME P/PPD

72090401		STONE		PROFILE TABULATION		31 POINTS, DELTA AT POINT 31			
I	Y	PTZ/P	P/PD	T0/T00	M/MD	U/UD	T/TD	RHD/RHD0*U/UD	
1	0.0000+00	1.0000+00	NM	0.70000	0.00000	0.00000	8.65922	0.00000	
2	1.8000-04	1.4373+00	NM	0.81250	0.09800	0.29500	9.06133	0.03256	
3	4.1000-04	2.0587+00	NM	0.85696	0.14200	0.41700	8.62374	0.04835	
4	7.1000-04	5.1788+00	NM	0.89099	0.25300	0.63900	6.37912	0.10017	
5	9.4000-04	6.8974+00	NM	0.90249	0.29600	0.70000	5.59259	0.12517	
6	1.2400-03	9.0895+00	NM	0.91077	0.34300	0.75300	4.81950	0.15624	
7	1.5500-03	1.0334+01	NM	0.91492	0.36700	0.77600	4.47086	0.17357	
8	1.9800-03	1.1550+01	NM	0.92049	0.39900	0.79600	4.18723	0.19010	
9	2.2100-03	1.2185+01	NM	0.92305	0.40000	0.80500	4.05016	0.19876	
10	2.5400-03	1.3323+01	NM	0.92540	0.41900	0.81900	3.82067	0.21436	
11	2.6900-03	1.4069+01	NM	0.92627	0.43100	0.82700	3.68177	0.22462	
12	2.9700-03	1.4706+01	NM	0.93067	0.44100	0.83500	3.58505	0.23291	
13	3.3000-03	1.5891+01	NM	0.93248	0.45900	0.84600	3.39715	0.24903	
14	3.5800-03	1.7124+01	NM	0.93384	0.47700	0.85600	3.22041	0.26580	
15	3.7800-03	1.8115+01	NM	0.93646	0.49100	0.86400	3.09645	0.27903	
16	4.0400-03	1.9136+01	NM	0.93779	0.50500	0.87100	2.97477	0.29280	
17	4.2900-03	2.0720+01	NM	0.94019	0.52600	0.88100	2.80531	0.31405	
18	4.6500-03	2.2529+01	NM	0.94263	0.54900	0.89100	2.63397	0.33827	
19	5.2100-03	2.5688+01	NM	0.94706	0.58700	0.90600	2.38221	0.38032	
20	5.4600-03	2.7614+01	NM	0.94995	0.60900	0.91400	2.25246	0.40578	
21	5.7200-03	2.8422+01	NM	0.95090	0.61800	0.91700	2.20172	0.41649	
22	6.2000-03	3.2544+01	NM	0.95658	0.66200	0.93100	1.97780	0.47072	
23	6.8600-03	3.4611+01	NM	0.97765	0.68300	0.94600	1.91841	0.49312	
24	7.3400-03	3.6743+01	NM	0.98912	0.70400	0.95600	1.84404	0.51843	
25	7.8700-03	4.0873+01	NM	0.98001	0.74300	0.95900	1.66594	0.57565	
26	8.2000-03	4.2169+01	NM	1.00239	0.75500	0.97200	1.65744	0.58645	
27	9.7500-03	4.7077+01	NM	1.00263	0.79800	0.97900	1.50508	0.65046	
28	1.0310-02	5.2236+01	NM	1.00269	0.84100	0.98500	1.37177	0.71805	
29	1.0790-02	5.6506+01	NM	1.00435	0.87500	0.99000	1.26013	0.77336	
30	1.2600-02	6.9336+01	NM	0.99705	0.97000	0.99600	1.05433	0.94468	
D 31	1.4000-02	7.3662+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD,U/UD ASSUME P=PD

72090402		STONE		PROFILE TABULATION		24 POINTS, DELTA AT POINT 24			
I	Y	PTZ/P	P/PD	T0/T	M/MD	U/UD	T/TD	RHD/RHD0*U/UD	
1	0.0000+00	1.0000+00	NM	0.72000	0.00000	0.00000	9.63891	0.00000	
2	1.8000-04	1.4075+00	NM	0.75762	0.09100	0.27600	9.19889	0.03000	
3	6.8000-04	2.1375+00	NM	0.87169	0.14000	0.47900	9.38985	0.04569	
4	8.9000-04	3.9894+00	NM	0.89266	0.20900	0.58200	7.75449	0.07505	
5	1.7000-03	9.0572+00	NM	0.91590	0.32800	0.75200	5.25640	0.14306	
6	1.8300-03	1.0300+01	NM	0.91755	0.35100	0.77400	4.86259	0.15917	
7	2.3400-03	1.1215+01	NM	0.91643	0.36700	0.78800	4.61021	0.17093	
8	3.0000-03	1.3231+01	NM	0.90440	0.40000	0.80600	4.06023	0.19851	
9	3.3800-03	1.3877+01	NM	0.92546	0.41000	0.82200	4.01954	0.20450	
10	4.2400-03	1.8010+01	NM	0.93117	0.46900	0.85800	3.34679	0.25636	
11	4.8000-03	1.8765+01	NM	0.93377	0.47900	0.86400	3.25334	0.26556	
12	5.4800-03	2.3292+01	NM	0.94176	0.53900	0.89100	2.77363	0.32124	
13	6.4000-03	2.6649+01	NM	0.95045	0.57300	0.90800	2.51109	0.36160	
14	6.8100-03	3.1120+01	NM	0.94971	0.62000	0.92100	2.20666	0.41737	
15	7.6700-03	3.3951+01	NM	0.95826	0.64800	0.93200	2.06863	0.45054	
16	8.0500-03	3.9095+01	NM	0.95791	0.69600	0.94200	1.83162	0.51424	
17	9.3200-03	5.0992+01	NM	0.96542	0.79600	0.96200	1.46058	0.65864	
18	1.0390-02	6.0269+01	NM	0.97230	0.86600	0.97400	1.26498	0.76998	
19	1.1630-02	6.7521+01	NM	0.98194	0.91700	0.98400	1.15147	0.85456	
20	1.2880-02	7.2889+01	NM	0.99149	0.95300	0.99200	1.08352	0.91553	
21	1.4300-02	7.6427+01	NM	0.99371	0.97600	0.99500	1.03931	0.95736	
22	1.5370-02	7.7678+01	NM	0.99445	0.98400	0.99600	1.02454	0.97214	
23	1.6760-02	7.9255+01	NM	0.99890	0.99400	0.99900	1.01009	0.98903	
D 24	1.7960-02	8.0209+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M/MD,U/UD ASSUME P=PD

<p>Three configurations tested</p> <p>See diagrams below</p>	<p>M : a) 4.9 b, c) 4.0</p> <p>R THETA X 10⁻³ : 8 - 30</p> <p>TW/TR : 0.85 - 1.0</p>	<p>7301</p> <p>ZPG (HISTORY)</p> <p>AW - MHT</p>
<p>Windtunnels: (a) as for CAT 7202 (b, c) effectively continuous, fixed nozzle, W = H = 0.4 m.</p> <p>PO : (a) 0.61 (b) 0.21 (c) 0.43 MN/m² TO: (a) 305-375, (b) 350, (c) 330 K.</p> <p>Dry air, dew point 215-233 K. RE/m x 10⁻⁶ : a) 10-16 b) 6.5 c) 15</p>		
<p>GATES D.F. 1973. Measurements of upstream history effects in compressible turbulent boundary layers. NOLTR 73-152.</p> <p>And Gates D.F., private communications, Voisinnet & Lee CAT 7202.</p>		

- 1 The test boundary layers were all formed on flat surfaces, and in the region of study were at constant pressure. The emphasis of the tests was on a controlled variation of the upstream history of the layers. In each case, upstream of the test zone, a part of the flat surface could be made to transfer heat to or from the flow (the sketches in the heading indicate this region with the symbol Q). The pressure history and origin of the boundary layer is different in each case. The combinations are listed in table 1.
- 4
- 1a a) Series 01-06. The test layer was formed on the flat wall of the boundary layer channel described in CAT 7202, and experienced the pressure history given in table 2 of that entry. The plate cooling system was arranged so that near the throat (X = 0), from X = - 165 to + 457 mm, the wall temperature could be controlled to give heating, cooling, or near-adiabatic conditions independently of the controlled cooling in the test zone.
- 4a
- 1b b, c) Series 07-10: The basic structure for these tests consisted of a rectangular cross section channel constructed as an extension of the tunnel nozzle 3.86 m long and closed on the plane of symmetry by the test plate. A long (b, series 07-08) or short (c, series 09-10) leading edge section could be attached, which ran into the normal tunnel test section on the centre plane. The cross section of the channel was W = 411, H = 222 mm at entry, increasing to W = 436, H = 274 mm at exit, to allow for boundary layer growth (there is also a slight divergence in the tunnel proper). The test surface was fitted with removable plugs (D = 47.6 mm) at intervals along the centre-line which could be replaced by instrumented units. Test surface roughness was held to 0.8 μ m rms, and all other flow surfaces to 1.6 μ m rms.
- 1c
- 1b b) Series 07-08: The test plate in the channel was extended upstream by a plate of similar construction 1.83 m long on which was mounted a leading edge section 0.23 m long. The leading edge was formed by a half-wedge of 19^o included angle and was 153 mm upstream of the throat (X = 0). The leading edge section could be cooled by liquid nitrogen giving the temperature histories shown in table II, columns 2 and 3. A limited amount of pressure history is available and is given as a Mach number distribution at the foot of columns 1 and 2.
- 4b
- 1c c) Series 09-10: The short leading edge section was 0.686 m long. The leading edge (X = 0) was formed by a half-wedge of 10^o included angle and was thus 1.219 m downstream of the throat and in the constant pressure region. The leading edge section did not contain instrumentation ports and could be cooled by liquid nitrogen in passages between X = 76 and 533 mm. Sample temperature distributions are given in table II columns 5 and 6.
- 4c
- 2 "Pitot pressure profiles, oil streak tests and several sets of schlieren photographs all indicate uniformity of the pressure-velocity field" and the (PC) wall pressure distributions in the uniform flow region (not

- 3 presented) show the Mach number constant within limits of ± 0.04 for (b) and ± 0.02 for (c). Transition was natural with no information as to the precise location. Flow angularity as shown by oil streak observations ranged from immeasurable at the centre line to a few degrees near the corners.
- 6 The instrumentation of the channel is described in CAT 7202. The plates in the windtunnel tests were drilled with up to 26 static tapings of 0.79 mm diameter at intervals of 305 or 153 mm along the centre line. Copper-constantan thermocouples were mounted at 305 mm intervals 76.2 mm from the centre line. Additional thermocouples were mounted on the centre line of the cooled leading edge sections, 3 for the long plate (b) and 5 for the short (c) as indicated by table II. Thermopiles (RdF corporation, Hudson, New Hampshire, model 7 no 20463-3) could be mounted at the centre of the ports. The probes employed were identical to those used for CAT 7202. The results presented were obtained with the FPP and the ECP. The relative positions of measuring stations were the same as in CAT 7202 except that there were no static holes to the sides of each port in the plates. The X values for which measurements were made are given in table I.
- 9 The author has interpolated his TO data to the Y stations of the PT2 values and applied the same probe corrections as in CAT 7202. In the region adjacent to the wall ($y < 0.6 - 1.0$ mm) temperature values were again obtained by extrapolating the profiles to meet the wall temperature. Sutherland's viscosity law was assumed. The editors have presented the data as prepared by the author.
- 13 The 26 ZPG profiles presented have varied upstream histories as listed in table I. PO and TO were measured simultaneously. A limited amount of wall data is presented, and no attempt has been made to adjust the values to take account of the slight differences in X value.
- 5 DATA. /301 0101-1003 ZPG PT2 and TO simultaneously. NX = 2 to 4. CQ from Thermopiles.

15 Editors' comments

The experiments constitute a systematic attempt to identify the influence of pressure and temperature history effects. Configuration c) (series 09, 10) involves no pressure history, so that any differences observed between the cooled and uncooled leading edge cases can be ascribed to the temperature history alone. Configurations a) and b) both involve a predominately reflected-wave expansion in the nozzle region, with differing initial boundary-layer thicknesses. Tests on configuration a) include both relative heating and cooling in the nozzle region, coupled with differing test-region thermal conditions. Configuration b) provided a stronger throat-region cooling effect, but was associated only with a near-adiabatic test-region wall.

An obvious gross effect of upstream heating is to modify the downstream adiabatic wall temperature. For example, tests on the short flat plate, configuration c), gave an "experimental recovery factor", in the absence of any leading-edge cooling, of about 0.80. The corresponding value with a cool leading edge was 0.78 at the first measuring station ($X = 0.914$ m) relaxing to 0.86 at the most downstream station ($X = 2.743$ m). Similar effects are observed in the other cases, and reported at length also by Voisinnet & Lee (CAT 7202).

The profiles are specified by a fairly large number of data points and in every case the measurements extend within the momentum deficit maximum. In most cases the measurements extend well out into the free stream, as indicated by the PO deficit. By the same criterion, the D-state should in general be taken at a larger value of Y. It is a pity that in an investigation on this large scale no CF information was obtained.

Comparisons, on the basis of Mach number and Reynolds number in the test-zone, may be made with the adiabatic flat plate studies of Hastings & Sawyer (CAT 7006) and Mabey et al. (CAT 7402). Corresponding cases where the layer was produced on a flat wall facing a contoured half-nozzle are Voisinnet & Lee (CAT 7202) and, at lower Mach number, Meier (CAT 7003) and Jeromin (CAT 6602).

TABLE I GROSS THERMAL HISTORY OF TEST BOUNDARY LAYERS

Run. IDENT 7301-	Reservoir TOD K	Throat or leading edge condition	Nominal temperature K	Wall condition	Nominal temperature K	PORT X m	PROFILE X m	
0101	347	COOL	308	ADIAB.	301	1.778	1.702	Boundary layer channel
0102	348	"	311	"	296	2.286	2.210	MD = 4.9
0201	373	"	328	COOL	270	1.778	1.702	PO = 515 KN/m ²
0202	374	"	332	"	279	2.286	2.210	
0301	338	ADIAB.	325	ADIAB.	304	1.778	1.702	
0302	324	"	319	"	296	2.286	2.210	
0401	333	"	327	COOL	265	1.778	1.702	
0402	333	"	317	"	267	2.286	2.210	
0501	311	HOT	323	ADIAB.	294	1.778	1.702	
0502	311	"	332	"	293	2.286	2.210	
0601	311	"	323	COOL	269	1.778	1.702	
0602	311	"	339	"	262	2.286	2.210	
0701	340	UNCOOLED	304	ISOTHERMAL	298	1.524	1.448	Long flat plate
0702	341	"	306	IN	298	2.134	2.057	MD = 4.0
0703	344	"	308	TEST	297	2.743	2.667	PO = 215 KN/m ²
0704	343	"	301	REGION	294	3.962	3.886	
0801	341	COOLED	249	AND	297	1.524	1.448	
0802	343	"	256	NEARLY	298	2.134	2.057	
0803	343	"	252	ADIABATIC	298	2.743	2.667	
0804	343	"	257	"	298	3.962	3.886	
0901	332	UNCOOLED	301	NEARLY	300	0.914	0.838	Short flat plate
0902	327	"	299	ADIABATIC	301	1.524	1.448	MD = 4.0
0903	327	"	301	SLIGHT HEAT	298	2.743	2.667	PO = 430 KN/m ²
1001	333	COOLED	129	TRANSFER TO	298	0.914	0.838	
1002	331	"	112	OR FROM THE	296	1.524	1.448	
1003	333	"	104	PLATE	298	2.743	2.667	

TABLE II TEMPERATURE HISTORY FOR FLAT PLATE TESTS

LONG PLATE			SHORT PLATE		
1) X/m from M = 1	2) T/K LE COOLED	3) T/K LE ADIAB	4) X/m from LE	5) T/K LE COOLED	6) T/K LE ADIAB
- 0.076	277	-	0.000	283 +	-
- 0.015	251	-	0.003	269 +	-
+ 0.061	262	321	0.015	243 +	-
0.305	299	306	0.030	216 +	-
0.533	299	302	0.046	190 +	-
0.838	298	300	0.061	161 +	-
1.143	298	298	0.091	104	301
1.448	299	300	0.183	93	300
1.753	298	299	0.305	92	299
2.057	298	299	0.427	91	298
2.362	298	-	0.610	101	298
2.667	297	298	0.701	132 +	-
2.972	298	299	0.701	253 +	-
3.277	299	300	0.838	272	299
3.581	300	301	1.143	289	299
3.886	301	301	1.448	296	301
4.191	302	302	1.753	298	300
4.496	304	306	2.057	298	299
4.801	308	310	2.362	298	300
X/m MD	MD		2.667	299	300
0.305	3.22		3.277	300	301
0.457	3.53				
0.610	3.81				
0.762	3.96				

+ Calculated from fin Bessel function.
Sample sets. Typical except for column 5, for which values were in general 0 - 15 K higher.

Long plate: X=0 at throat, Cooled leading edge X = -153 to + 76 mm, Leading edge extension X = + 76 mm to 1905 mm
Short plate: Cooled leading edge X = 0 to 686 mm, Cooling passages X = 76 to 533 mm.

CAT 7301		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
GATES									
RUN	MO *	TW/TR	RED2W	CF	H12	H12K	PW	PD*	
X *	POD	PW/PD*	RED2D	CO *	H32	H32K	TW*	TD*	
RZ	YOD	SW *	D2	PI2*	H42	D2K	UD	TR	
73010101	4.9307	0.9659	5.7592 ⁺⁰³	NM	8.8708	1.3863	1.0459 ⁺⁰³	1.0459 ⁺⁰³	
1.7018 ⁺⁰⁰	5.1022 ⁺⁰⁵	1.0000	2.5595 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8315	1.7767	3.0356 ⁺⁰²	5.8667 ⁺⁰¹	
INFINITE	3.4393 ⁺⁰²	0.0000	2.2892 ⁻⁰³	0.0000 ⁺⁰⁰	0.4965	4.7488 ⁻⁰³	7.5721 ⁺⁰²	3.1426 ⁺⁰²	
73010102	4.8633	0.9488	6.5279 ⁺⁰³	NM	9.6147	1.3947	1.1487 ⁺⁰³	1.1487 ⁺⁰³	
2.2098 ⁺⁰⁰	5.1740 ⁺⁰⁵	1.0000	2.8056 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8161	1.7663	2.9461 ⁺⁰²	5.9278 ⁺⁰¹	
INFINITE	3.3968 ⁺⁰²	0.0000	2.3530 ⁻⁰³	0.0000 ⁺⁰⁰	0.3587	5.1945 ⁻⁰³	7.5074 ⁺⁰²	3.1052 ⁺⁰²	
73010201	4.9343	0.7936	6.4884 ⁺⁰³	NM	8.2150	1.3742	1.0425 ⁺⁰³	1.0425 ⁺⁰³	
1.7018 ⁺⁰⁰	5.1070 ⁺⁰⁵	1.0000	2.4315 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8307	1.7791	2.7072 ⁺⁰²	6.3611 ⁺⁰¹	
INFINITE	3.7336 ⁺⁰²	0.0000	2.4628 ⁻⁰³	0.0000 ⁺⁰⁰	0.5834	4.8837 ⁻⁰³	7.8905 ⁺⁰²	3.4115 ⁺⁰²	
73010202	4.8539	0.8335	6.9989 ⁺⁰³	NM	8.8172	1.3900	1.1521 ⁺⁰³	1.1521 ⁺⁰³	
2.2098 ⁺⁰⁰	5.1318 ⁺⁰⁵	1.0000	2.6589 ⁺⁰⁴	NC	1.8142	1.7662	2.8194 ⁺⁰²	6.4778 ⁺⁰¹	
INFINITE	3.7002 ⁺⁰²	0.0000	2.5459 ⁻⁰³	0.0000 ⁺⁰⁰	0.4661	5.3689 ⁻⁰³	7.8327 ⁺⁰²	3.3627 ⁺⁰²	
73010301	4.9651	0.9881	4.6022 ⁺⁰³	NM	11.1257	1.3967	1.0211 ⁺⁰³	1.0211 ⁺⁰³	
1.7018 ⁺⁰⁰	5.1866 ⁺⁰⁵	1.0000	2.1145 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8241	1.7721	3.0483 ⁺⁰²	5.6944 ⁺⁰¹	
INFINITE	3.3771 ⁺⁰²	0.0000	1.8392 ⁻⁰³	0.0000 ⁺⁰⁰	0.1633	4.2396 ⁻⁰³	7.5121 ⁺⁰²	3.0851 ⁺⁰²	
73010302	4.8479	1.0022	5.6063 ⁺⁰³	NM	11.3321	1.3955	1.1500 ⁺⁰³	1.1500 ⁺⁰³	
2.2098 ⁺⁰⁰	5.0983 ⁺⁰⁵	1.0000	2.5241 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8105	1.7638	2.9994 ⁺⁰²	5.7389 ⁺⁰¹	
INFINITE	3.2736 ⁺⁰²	0.0000	2.0192 ⁻⁰³	0.0000 ⁺⁰⁰	0.0908	4.8226 ⁻⁰³	7.3664 ⁺⁰²	2.9929 ⁺⁰²	
73010401	4.9329	0.8707	4.8841 ⁺⁰³	NM	11.3511	1.3983	1.0170 ⁺⁰³	1.0170 ⁺⁰³	
1.7018 ⁺⁰⁰	4.9738 ⁺⁰⁵	1.0000	2.0199 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8172	1.7697	2.6372 ⁺⁰²	5.6500 ⁺⁰¹	
INFINITE	3.3147 ⁺⁰²	0.0000	1.7548 ⁻⁰³	0.0000 ⁺⁰⁰	0.1217	4.0426 ⁻⁰³	7.4342 ⁺⁰²	3.0287 ⁺⁰²	
73010402	4.8632	0.8848	6.8751 ⁺⁰³	NM	9.9085	1.3857	1.1356 ⁺⁰³	1.1356 ⁺⁰³	
2.2098 ⁺⁰⁰	5.1144 ⁺⁰⁵	1.0000	2.8168 ⁺⁰⁴	NC	1.8182	1.7703	2.8650 ⁺⁰²	5.7500 ⁺⁰¹	
INFINITE	3.2948 ⁺⁰²	0.0000	2.2825 ⁻⁰³	0.0000 ⁺⁰⁰	0.3123	5.0977 ⁻⁰³	7.5938 ⁺⁰²	3.0120 ⁺⁰²	
73010501	4.7424	1.0212	3.7895 ⁺⁰³	NM	11.2671	1.4121	1.0142 ⁺⁰³	1.0142 ⁺⁰³	
1.7018 ⁺⁰⁰	3.9525 ⁺⁰⁵	1.0000	1.6878 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8131	1.7664	2.9167 ⁺⁰²	5.6778 ⁺⁰¹	
INFINITE	3.1217 ⁺⁰²	0.0000	1.5406 ⁻⁰³	0.0000 ⁺⁰⁰	0.0387	3.6275 ⁻⁰³	7.1647 ⁺⁰²	2.8561 ⁺⁰²	
73010502	4.8687	1.0462	3.8730 ⁺⁰³	NM	17.4113	1.4240	1.1438 ⁺⁰³	1.1438 ⁺⁰³	
2.2098 ⁺⁰⁰	5.1854 ⁺⁰⁵	1.0000	1.8429 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.7772	1.7505	2.9278 ⁺⁰²	5.3328 ⁺⁰¹	
INFINITE	3.0615 ⁺⁰²	0.0000	1.3218 ⁻⁰³	0.0000 ⁺⁰⁰	-0.8314	3.9106 ⁻⁰³	7.1285 ⁺⁰²	2.7985 ⁺⁰²	
73010601	4.7510	0.9222	4.2406 ⁺⁰³	NM	10.8335	1.3959	1.0128 ⁺⁰³	1.0128 ⁺⁰³	
1.7018 ⁺⁰⁰	3.9883 ⁺⁰⁵	1.0000	1.7488 ⁺⁰⁴	0.0000 ⁺⁰⁰	1.8120	1.7684	2.8311 ⁺⁰²	5.6556 ⁺⁰¹	
INFINITE	3.1187 ⁺⁰²	0.0000	1.5862 ⁻⁰³	0.0000 ⁺⁰⁰	0.1001	3.6420 ⁻⁰³	7.1636 ⁺⁰²	2.8932 ⁺⁰²	
73010602	4.8856	0.9350	4.2170 ⁺⁰³	NM	16.4525	1.4344	1.1107 ⁺⁰³	1.1107 ⁺⁰³	
2.2098 ⁺⁰⁰	5.1373 ⁺⁰⁵	1.0000	1.8481 ⁺⁰⁴	NC	1.7686	1.7464	2.6139 ⁺⁰²	5.2972 ⁺⁰¹	
INFINITE	3.0585 ⁺⁰²	0.0000	1.3467 ⁻⁰³	0.0000 ⁺⁰⁰	-0.7524	3.9106 ⁻⁰³	7.1294 ⁺⁰²	2.7955 ⁺⁰²	

CAT 7301		GATES		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.					
RUN X * HZ	MD * POD TOD	TN/TR PH/PO* SH *	REC2W RED2D D2	CF CO * PI2*	H12 H32 H42	H12K H32K D2K	PM TW* UD	PO* TO* TR	
73010701 1.4478*+00 INFINITE	3.9566 1.8375*+05 3.5205*+02	0.9136 1.0000 0.0000	2.7655*+03 8.3145*+03 1.3266*+03	NM NC 0.0000*+00	7.5927 1.8116 0.1401	1.3335 1.7845 2.4666*+03	1.2776*+03 2.9628*+02 7.3233*+02	1.2776*+03 8.5222*+01 3.2430*+02	
73010702 2.0574*+00 INFINITE	4.0148 1.9240*+05 3.5456*+02	0.9215 1.0000 0.0000	3.4346*+03 1.0603*+04 1.6765*+03	NM NC 0.0000*+00	7.8998 1.8119 0.1155	1.3334 1.7855 3.2018*+03	1.2424*+03 3.0078*+02 7.3751*+02	1.2424*+03 8.3944*+01 3.2641*+02	
73010703 2.6670*+00 INFINITE	3.9557 1.8717*+05 3.5170*+02	0.9191 1.0000 0.0000	4.6940*+03 1.4177*+04 2.2079*+03	NM NC 0.0000*+00	7.7931 1.8103 0.0984	1.3323 1.7851 4.1995*+03	1.3079*+03 2.9778*+02 7.3193*+02	1.3079*+03 8.5167*+01 3.2348*+02	
73010704 3.8862*+00 INFINITE	3.9284 1.7377*+05 3.4485*+02	0.9364 1.0000 0.0000	5.6507*+03 1.7211*+04 2.7646*+03	NM NC 0.0000*+00	7.8416 1.8192 0.0584	1.3141 1.7945 5.1868*+03	1.2597*+03 2.9756*+02 7.2355*+02	1.2597*+03 8.4389*+01 3.1776*+02	
73010801 1.4478*+00 INFINITE	4.0269 1.9823*+05 3.4676*+02	0.9329 1.0000 0.0000	3.0578*+03 9.8177*+03 1.4370*+03	NM NC 0.0000*+00	7.5276 1.8112 0.2050	1.3384 1.7809 2.7095*+03	1.2597*+03 2.9778*+02 7.2988*+02	1.2597*+03 8.1722*+01 3.1920*+02	
73010802 2.0574*+00 INFINITE	4.0506 1.9438*+05 3.4537*+02	0.9381 1.0000 0.0000	4.0815*+03 1.3016*+04 1.9959*+03	NM NC 0.0000*+00	7.6374 1.8200 0.1887	1.3235 1.7905 3.7263*+03	1.1969*+03 2.9817*+02 7.2942*+02	1.1969*+03 8.0667*+01 3.1784*+02	
73010803 2.6670*+00 INFINITE	4.0472 2.0075*+05 3.4517*+02	0.9391 1.0000 0.0000	5.0559*+03 1.6120*+04 2.3670*+03	NM NC 0.0000*+00	7.8179 1.8147 0.1539	1.3304 1.7854 4.5417*+03	1.2417*+03 2.9833*+02 7.2906*+02	1.2417*+03 8.0722*+01 3.1766*+02	
73010804 3.8862*+00 INFINITE	3.9879 1.8222*+05 3.4978*+02	0.9262 1.0000 0.0000	6.3177*+03 1.9445*+04 3.1375*+03	NM NC 0.0000*+00	7.4346 1.8133 0.1897	1.3264 1.7872 5.8192*+03	1.2197*+03 2.9833*+02 7.3136*+02	1.2197*+03 8.3667*+01 3.2211*+02	
73010901 8.3820*+01 INFINITE	4.0640 4.0699*+05 3.3207*+02	1.0224 1.0000 0.0000	2.6492*+03 9.1490*+03 6.3630*+04	NM 0.0000*+00 0.0000*+00	8.1451 1.8167 0.1086	1.3759 1.7835 1.2309*+03	2.4621*+03 3.1239*+02 7.1578*+02	2.4621*+03 7.7167*+01 3.0556*+02	
73010902 1.4478*+00 INFINITE	4.0851 4.1052*+05 3.3207*+02	0.9880 1.0000 0.0000	4.4124*+03 1.4959*+04 1.0427*+03	NM 0.0000*+00 0.0000*+00	8.1445 1.8141 0.1204	1.3476 1.7843 2.0209*+03	2.4152*+03 3.0183*+02 7.1664*+02	2.4152*+03 7.6556*+01 3.0549*+02	
73010903 2.6670*+00 INFINITE	4.1103 4.1153*+05 3.2891*+02	0.9814 1.0000 0.0000	6.7779*+03 2.3121*+04 1.6054*+03	NM 0.0000*+00 0.0000*+00	8.3574 1.8273 0.0865	1.3275 1.7972 3.0982*+03	2.3421*+03 2.9689*+02 7.1423*+02	2.3421*+03 7.5111*+01 3.0251*+02	
73011001 8.3820*+01 INFINITE	4.0528 4.0741*+05 3.3161*+02	0.9796 1.0000 0.0000	2.5653*+03 8.5408*+03 5.8880*+04	NM NC 0.0000*+00	6.5354 1.8120 0.4364	1.4063 1.7783 1.0270*+03	2.5014*+03 2.9894*+02 7.1483*+02	2.5014*+03 7.7389*+01 3.0517*+02	
73011002 1.4478*+00 INFINITE	4.0847 4.1452*+05 3.3105*+02	0.9717 1.0000 0.0000	4.3409*+03 1.4537*+04 9.9867*+04	NM NC 0.0000*+00	7.1894 1.8043 0.3235	1.3893 1.7724 1.8483*+03	2.4401*+03 2.9594*+02 7.1553*+02	2.4401*+03 7.6333*+01 3.0456*+02	
73011003 2.6670*+00 INFINITE	4.1069 4.0800*+05 3.3456*+02	0.9597 1.0000 0.0000	7.1399*+03 2.3820*+04 1.7082*+03	NM 0.0000*+00 0.0000*+00	7.4812 1.8176 0.2817	1.3841 1.7811 3.1863*+03	2.3325*+03 2.9533*+02 7.2020*+02	2.3325*+03 7.6500*+01 3.0772*+02	

73010101		GATES		PROFILE TABULATION		48 POINTS, DELTA AT POINT 43			
I	Y	R12/R	P/PP	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.88249	0.00000	0.00000	5.17359	0.00000	
2	6.3500*-05	1.0102*+00	NM	0.88142	0.02441	0.05540	5.15230	0.01075	
3	2.1590*-04	1.0807*+00	NM	0.87205	0.06792	0.15190	5.00240	0.03037	
4	3.6830*-04	1.2798*+00	NM	0.87199	0.12256	0.26750	4.76400	0.05615	
5	5.9690*-04	1.7288*+00	NM	0.86613	0.18660	0.39330	4.44270	0.08853	
6	8.5090*-04	2.3185*+00	NM	0.85526	0.23706	0.48130	4.12200	0.11676	
7	1.1811*-03	2.8832*+00	NM	0.84280	0.27412	0.53670	3.83330	0.14001	
8	1.5621*-03	3.2516*+00	NM	0.90074	0.29541	0.56880	3.70730	0.15343	
9	2.1209*-03	3.6012*+00	NM	0.90261	0.31412	0.59400	3.57580	0.16612	
10	2.6289*-03	3.8915*+00	NM	0.90607	0.32879	0.61350	3.46160	0.17621	
11	3.2655*-03	4.2503*+00	NM	0.90150	0.34602	0.63240	3.34030	0.18932	
12	4.1783*-03	4.6580*+00	NM	0.89906	0.36455	0.65230	3.20170	0.20374	
13	5.1435*-03	5.1341*+00	NM	0.90379	0.38502	0.67560	3.07900	0.21942	
14	6.2103*-03	5.6961*+00	NM	0.91157	0.40782	0.70100	2.95460	0.23726	
15	7.2517*-03	6.2268*+00	NM	0.91897	0.42821	0.72250	2.84680	0.25379	
16	8.2169*-03	6.7634*+00	NM	0.92685	0.44787	0.74280	2.75070	0.27004	
17	9.2075*-03	7.2530*+00	NM	0.92676	0.46507	0.75680	2.64610	0.28579	
18	1.0224*-02	7.7796*+00	NM	0.92688	0.48014	0.77300	2.52830	0.30574	
19	1.0884*-02	8.2728*+00	NM	0.92549	0.49896	0.78170	2.45440	0.31849	
20	1.2814*-02	9.4703*+00	NM	0.92958	0.53601	0.80820	2.27350	0.35549	
21	1.4008*-02	1.0262*+01	NM	0.93181	0.55913	0.82320	2.16760	0.37977	
22	1.5354*-02	1.1208*+01	NM	0.93870	0.58558	0.84110	2.06310	0.40769	
23	1.6472*-02	1.2118*+01	NM	0.94440	0.60992	0.85630	1.97110	0.43443	
24	1.7945*-02	1.3295*+01	NM	0.95123	0.64003	0.87380	1.86390	0.46880	
25	1.8961*-02	1.4106*+01	NM	0.95634	0.65999	0.88500	1.79810	0.49219	
26	2.0409*-02	1.5321*+01	NM	0.95516	0.68879	0.89630	1.69330	0.52932	
27	2.1679*-02	1.6316*+01	NM	0.95656	0.71151	0.90560	1.62000	0.55901	
28	2.2847*-02	1.7572*+01	NM	0.95016	0.73917	0.91230	1.52330	0.59890	
29	2.4244*-02	1.8335*+01	NM	0.95768	0.75549	0.92130	1.48710	0.61953	
30	2.5514*-02	1.9350*+01	NM	0.96153	0.77667	0.92980	1.43320	0.64876	
31	2.7826*-02	2.1139*+01	NM	0.96521	0.81264	0.94200	1.34370	0.70105	
32	3.0493*-02	2.2979*+01	NM	0.96992	0.84805	0.95360	1.26440	0.75419	
33	3.2855*-02	2.4314*+01	NM	0.97500	0.87283	0.96210	1.21500	0.79185	
34	3.5039*-02	2.5313*+01	NM	0.97633	0.89093	0.96690	1.17780	0.82094	
35	3.8189*-02	2.6593*+01	NM	0.97832	0.91360	0.97280	1.13380	0.85800	
36	4.0780*-02	2.7524*+01	NM	0.97967	0.92974	0.97680	1.10380	0.88494	
37	4.3142*-02	2.8263*+01	NM	0.98025	0.94236	0.97960	1.08080	0.90653	
38	4.5860*-02	2.9021*+01	NM	0.98275	0.95511	0.98330	1.05990	0.92773	
39	4.7917*-02	2.9554*+01	NM	0.98521	0.96399	0.98620	1.04660	0.94229	
40	5.0356*-02	3.0210*+01	NM	0.98826	0.97480	0.98970	1.03080	0.96013	
41	5.4242*-02	3.0824*+01	NM	0.99168	0.98482	0.99320	1.01710	0.97650	
42	5.8788*-02	3.1367*+01	NM	0.99521	0.99357	0.99650	1.00590	0.99066	
D 43	6.3970*-02	3.1768*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
44	6.8212*-02	3.1646*+01	NM	1.00027	0.99805	0.99980	1.00350	0.99631	
45	7.3266*-02	3.1606*+01	NM	1.00109	0.99741	1.00010	1.00540	0.99473	
46	7.8346*-02	3.1500*+01	NM	1.00087	0.99573	0.99970	1.00880	0.99177	
47	8.4036*-02	3.1375*+01	NM	1.00217	0.99371	1.00000	1.01270	0.98746	
48	8.8633*-02	3.1317*+01	NM	1.00229	0.99278	0.99990	1.01440	0.98571	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

73010501		GATES		PROFILE TABULATION		48 POINTS, DELTA AT POINT 36		
I	Y	PT2/P	P/PD	TQ/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	0.93447	0.00000	0.00000	5.13780	0.00000
2	6.3500 ⁻⁰⁵	1.0126 ⁺⁰⁰	NM	0.93520	0.02819	0.06380	5.12356	0.01245
3	1.6510 ⁻⁰⁴	1.0557 ⁺⁰⁰	NM	0.93084	0.05889	0.13220	5.03920	0.02623
4	3.6830 ⁻⁰⁴	1.2631 ⁺⁰⁰	NM	0.93841	0.12386	0.27210	4.82640	0.05638
5	5.4610 ⁻⁰⁴	1.6893 ⁺⁰⁰	NM	0.94516	0.18954	0.40090	4.47360	0.08961
6	7.7470 ⁻⁰⁴	2.2525 ⁺⁰⁰	NM	0.94323	0.24144	0.48940	4.10860	0.11912
7	1.1303 ⁻⁰³	2.8512 ⁺⁰⁰	NM	0.95159	0.28299	0.55500	3.84640	0.14429
8	1.5113 ⁻⁰³	3.2950 ⁺⁰⁰	NM	0.96422	0.30762	0.59590	3.70410	0.16086
9	2.0701 ⁻⁰³	3.6347 ⁺⁰⁰	NM	0.95503	0.32840	0.61750	3.53570	0.17465
10	2.4765 ⁻⁰³	3.8485 ⁺⁰⁰	NM	0.95051	0.33964	0.63000	3.44070	0.18310
11	3.3901 ⁻⁰³	4.2763 ⁺⁰⁰	NM	0.95289	0.36102	0.65610	3.30280	0.19865
12	4.2037 ⁻⁰³	4.7077 ⁺⁰⁰	NM	0.96154	0.38130	0.68170	3.19630	0.21328
13	5.0414 ⁻⁰³	5.1381 ⁺⁰⁰	NM	0.96834	0.40048	0.70430	3.09280	0.22772
14	6.0579 ⁻⁰³	5.6893 ⁺⁰⁰	NM	0.96699	0.42373	0.72670	2.94120	0.24708
15	7.1755 ⁻⁰³	6.2307 ⁺⁰⁰	NM	0.96715	0.44537	0.74660	2.81020	0.26568
16	8.1153 ⁻⁰³	6.7940 ⁺⁰⁰	NM	0.97617	0.46679	0.76850	2.71050	0.28353
17	9.1821 ⁻⁰³	7.4870 ⁺⁰⁰	NM	0.98852	0.48184	0.79350	2.60280	0.30486
18	1.0274 ⁻⁰²	8.1276 ⁺⁰⁰	NM	0.98667	0.51390	0.80920	2.47940	0.32637
19	1.1443 ⁻⁰²	8.8032 ⁺⁰⁰	NM	0.98648	0.53618	0.82460	2.36520	0.34864
20	1.2738 ⁻⁰²	9.6792 ⁺⁰⁰	NM	0.98694	0.56374	0.84250	2.23350	0.37721
21	1.3983 ⁻⁰²	1.0467 ⁺⁰¹	NM	0.98663	0.58740	0.85640	2.12560	0.40290
22	1.5354 ⁻⁰²	1.1544 ⁺⁰¹	NM	0.99652	0.61830	0.87760	2.01460	0.43562
23	1.6396 ⁻⁰²	1.2466 ⁺⁰¹	NM	1.00574	0.64357	0.89440	1.93140	0.46308
24	1.7869 ⁻⁰²	1.3781 ⁺⁰¹	NM	1.00585	0.67795	0.91030	1.80290	0.50491
25	1.8961 ⁻⁰²	1.4672 ⁺⁰¹	NM	1.00460	0.70031	0.91920	1.72280	0.53355
26	2.0307 ⁻⁰²	1.5749 ⁺⁰¹	NM	1.00054	0.72640	0.92760	1.63070	0.56884
27	2.1577 ⁻⁰²	1.6837 ⁺⁰¹	NM	1.00166	0.75183	0.93750	1.55490	0.60293
28	2.2974 ⁻⁰²	1.8164 ⁺⁰¹	NM	1.00676	0.78171	0.94990	1.47660	0.64330
29	2.4143 ⁻⁰²	1.9349 ⁺⁰¹	NM	1.01001	0.80747	0.95950	1.41200	0.67953
30	2.5336 ⁻⁰²	2.0381 ⁺⁰¹	NM	1.00878	0.82926	0.96530	1.35500	0.71240
31	2.7978 ⁻⁰²	2.2484 ⁺⁰¹	NM	1.00595	0.87197	0.97540	1.25130	0.77951
32	3.0620 ⁻⁰²	2.4274 ⁺⁰¹	NM	1.00226	0.90674	0.98200	1.17290	0.83724
33	3.2630 ⁻⁰²	2.5587 ⁺⁰¹	NM	1.00021	0.93141	0.98650	1.12180	0.87939
34	3.5649 ⁻⁰²	2.6975 ⁺⁰¹	NM	0.99616	0.95679	0.98980	1.07020	0.92487
35	3.8240 ⁻⁰²	2.8244 ⁺⁰¹	NM	0.99686	0.97944	0.99460	1.03120	0.96451
36	4.0526 ⁻⁰²	2.9423 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000
37	4.3167 ⁻⁰²	3.0325 ⁺⁰¹	NM	0.99709	1.01546	1.00130	0.97230	1.02983
38	4.5656 ⁻⁰²	3.0944 ⁺⁰¹	NM	0.99429	1.02594	1.00170	0.95330	1.05077
39	4.8450 ⁻⁰²	3.1475 ⁺⁰¹	NM	0.99092	1.03484	1.00150	0.93660	1.06929
40	5.1016 ⁻⁰²	3.1880 ⁺⁰¹	NM	0.98656	1.04157	1.00040	0.92250	1.08444
41	5.4191 ⁻⁰²	3.2198 ⁺⁰¹	NM	0.98232	1.04682	0.99910	0.91090	1.09683
42	5.7899 ⁻⁰²	3.2171 ⁺⁰¹	NM	0.97991	1.04638	0.99780	0.90930	1.09733
43	6.3792 ⁻⁰²	3.2174 ⁺⁰¹	NM	0.97871	1.04644	0.99720	0.90810	1.09812
44	6.8466 ⁻⁰²	3.2086 ⁺⁰¹	NM	0.97976	1.04498	0.99750	0.91120	1.09471
45	7.4079 ⁻⁰²	3.1961 ⁺⁰¹	NM	0.97944	1.04291	0.99700	0.91390	1.09093
46	7.8727 ⁻⁰²	3.1772 ⁺⁰¹	NM	0.98064	1.03977	0.99710	0.91960	1.08428
47	8.3858 ⁻⁰²	3.1530 ⁺⁰¹	NM	0.98071	1.03589	0.99650	0.92540	1.07863
48	8.9040 ⁻⁰²	3.1336 ⁺⁰¹	NM	0.98103	1.03252	0.99610	0.93070	1.07027

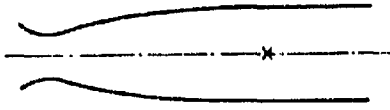
INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

73011001		GATES		PROFILE TABULATION			37 POINTS, DELTA AT POINT 23		
I	Y	PT2/P	P/PD	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.90139	0.00000	0.00000	3.86250	0.00000	
2	6.3500+05	1.1111+00	NM	0.87364	0.09640	0.18340	3.63260	0.05060	
3	1.1450+00	1.1912+00	NM	0.86985	0.12491	0.23520	3.54540	0.06634	
4	4.1910+04	3.3390+00	NM	0.87913	0.36523	0.59110	2.61930	0.22567	
5	6.2230+04	4.3553+00	NM	0.88771	0.42690	0.65850	2.37940	0.27675	
6	8.2550+04	4.9979+00	NM	0.89427	0.46184	0.69290	2.25480	0.30730	
7	1.1557+03	5.5473+00	NM	0.88767	0.48897	0.71370	2.13040	0.33501	
8	1.5367+03	6.1415+00	NM	0.89078	0.51706	0.73710	2.03220	0.36271	
9	1.8161+03	6.6431+00	NM	0.89361	0.53961	0.75490	1.95710	0.38572	
10	2.2479+03	7.2369+00	NM	0.89841	0.56513	0.77460	1.87870	0.41231	
11	2.7305+03	7.9783+00	NM	0.90713	0.59543	0.79790	1.79570	0.44434	
12	3.1115+03	8.6906+00	NM	0.91109	0.62314	0.81620	1.71560	0.47575	
13	3.4163+03	9.2013+00	NM	0.91499	0.64227	0.82870	1.66480	0.49778	
14	4.6355+03	1.1455+01	NM	0.94257	0.72060	0.88040	1.49270	0.56980	
15	5.4737+03	1.3068+01	NM	0.95553	0.77174	0.90820	1.38490	0.65579	
16	6.6167+03	1.5548+01	NM	0.97651	0.84438	0.94480	1.25200	0.75463	
17	7.6581+03	1.7708+01	NM	0.98987	0.90286	0.96960	1.15330	0.84072	
18	8.6995+03	1.9536+01	NM	0.99412	0.94954	0.98460	1.07520	0.91574	
19	9.7155+03	2.0728+01	NM	0.99734	0.97879	0.99360	1.03050	0.96419	
20	1.1214+02	2.1395+01	NM	0.99805	0.99477	0.99780	1.00610	0.99175	
21	1.2230+02	2.1546+01	NM	0.99717	0.99835	0.99820	0.99970	0.99850	
22	1.3830+02	2.1567+01	NM	0.99854	0.99885	0.99900	1.00030	0.99870	
23	1.4922+02	2.1615+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
24	1.6345+02	2.1620+01	NM	0.99895	1.00010	0.99950	0.99880	1.00070	
25	1.7158+02	2.1634+01	NM	1.00059	1.00045	1.00040	0.99990	1.00050	
26	1.8478+02	2.1620+01	NM	1.00235	1.00010	1.00120	0.99920	0.99900	
27	2.0841+02	2.1582+01	NM	1.00117	0.99920	1.00040	1.00240	0.99800	
28	2.3152+02	2.1584+01	NM	1.00235	0.99925	1.00100	1.00350	0.99751	
29	2.4016+02	2.1567+01	NM	1.00331	0.99891	1.00140	1.00500	0.99642	
30	2.6556+02	2.1563+01	NM	1.00255	0.99876	1.00100	1.00450	0.99652	
31	2.8918+02	2.1563+01	NM	1.00098	0.99875	1.00020	1.00290	0.99731	
32	3.1229+02	2.1520+01	NM	0.99526	0.99775	0.99710	0.99870	0.99840	
33	3.3947+02	2.1482+01	NM	0.98711	0.99685	0.99280	0.99190	1.00091	
34	3.6766+02	2.1917+01	NM	0.99094	1.00712	0.99710	0.98020	1.01724	
35	3.8951+02	2.1500+01	NM	1.00028	0.99726	0.99950	1.00450	0.99502	
36	4.1719+02	2.1169+01	NM	0.99681	0.98939	0.99550	1.01320	0.98293	
37	4.4437+02	2.0698+01	NM	0.99484	0.97807	0.99220	1.02910	0.96414	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

73011003		GATES		PROFILE TABULATION			39 POINTS, DELTA AT POINT 29		
I	Y	PT2/P	P/PD	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.88246	0.00000	0.00000	3.85930	0.00000	
2	6.3500+05	1.0757+00	NM	0.87763	0.07902	0.15320	3.75900	0.04076	
3	3.4290+04	1.2689+00	NM	0.88176	0.14444	0.27420	3.60260	0.07611	
4	1.0287+03	2.3429+00	NM	0.91024	0.30326	0.52860	3.03820	0.17398	
5	1.4097+03	3.0857+00	NM	0.92369	0.34342	0.58380	2.88990	0.20201	
6	1.9431+03	3.9630+00	NM	0.92653	0.39096	0.64780	2.63650	0.24570	
7	2.7305+03	4.9944+00	NM	0.92437	0.43961	0.68770	2.44720	0.28102	
8	3.3655+03	5.1572+00	NM	0.92480	0.46341	0.70970	2.34540	0.30259	
9	3.9243+03	5.5186+00	NM	0.92433	0.48115	0.72490	2.26980	0.31937	
10	4.6101+03	5.9628+00	NM	0.92956	0.50208	0.74420	2.19700	0.33873	
11	5.6515+03	6.5409+00	NM	0.93571	0.52808	0.76680	2.10870	0.36364	
12	6.7437+03	7.0648+00	NM	0.93978	0.55051	0.78480	2.03230	0.38616	
13	7.5819+03	7.4870+00	NM	0.94544	0.56795	0.79920	1.98010	0.40362	
14	8.3185+03	7.9010+00	NM	0.95121	0.58454	0.81260	1.93250	0.42049	
15	9.8425+03	8.6775+00	NM	0.96192	0.61444	0.83580	1.85030	0.45171	
16	1.1367+02	9.4506+00	NM	0.96558	0.64282	0.85420	1.76580	0.48375	
17	1.3195+02	1.0354+01	NM	0.96874	0.67445	0.87200	1.67160	0.52166	
18	1.4973+02	1.1289+01	NM	0.97116	0.70570	0.88840	1.58480	0.56058	
19	1.6396+02	1.2077+01	NM	0.97378	0.73098	0.90110	1.51960	0.59298	
20	1.8275+02	1.3128+01	NM	0.97536	0.76340	0.91560	1.43850	0.63650	
21	1.9520+02	1.3910+01	NM	0.97824	0.78667	0.92600	1.38660	0.66830	
22	2.1146+02	1.5343+01	NM	0.98073	0.82756	0.94200	1.29570	0.72702	
23	2.2542+02	1.6471+01	NM	0.98238	0.85838	0.95300	1.23260	0.77316	
24	2.5286+02	1.8598+01	NM	0.98977	0.91360	0.97310	1.13430	0.85749	
25	2.7140+02	1.9909+01	NM	0.99336	0.94616	0.98360	1.08070	0.91015	
26	2.9654+02	2.1095+01	NM	0.99514	0.97760	0.99160	1.03520	0.95788	
27	3.2423+02	2.1843+01	NM	0.99483	0.99213	0.99560	1.00700	0.98868	
28	3.4884+02	2.2062+01	NM	0.99649	0.99720	0.99780	1.00080	0.99680	
29	3.7529+02	2.2184+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
30	4.0373+02	2.2220+01	NM	1.00081	1.00000	1.00060	0.99940	1.00110	
31	4.3269+02	2.2236+01	NM	0.99885	1.00120	0.99970	0.99700	1.00271	
32	4.6063+02	2.2281+01	NM	0.99001	1.00274	0.99590	0.98660	1.00902	
33	4.8654+02	2.2306+01	NM	0.98577	1.00282	0.99350	0.98150	1.01223	
34	5.0863+02	2.2318+01	NM	0.98288	1.00309	0.99210	0.97820	1.01421	
35	5.2464+02	2.2298+01	NM	0.98189	1.00264	0.99150	0.97780	1.01341	
36	5.5893+02	2.2323+01	NM	0.98025	1.00322	0.99080	0.97540	1.01574	
37	5.8407+02	2.2323+01	NM	0.97630	1.00330	0.98890	0.97170	1.01770	
38	6.0844+02	2.2311+01	NM	0.97741	1.00283	0.98830	0.97300	1.01675	
39	6.3055+02	2.2325+01	NM	0.98301	1.00325	0.99220	0.97810	1.01442	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

	M : 0.2 to 2.8 R THETA X 10 ⁻³ : 10 - 160 TW/TR : Approx 1	7302
		ZPG - AW
Continuous running windtunnel with variable nozzle: W = H : 2.4 m. L : 10 m. 0.01 < P0 < 0.4 MN/m ² . T0 : 284 - 294 K. Air, dew point below 243 K. 1.5 < RE/m × 10 ⁻⁶ < 18.		
WINTER K.G. and GAUDET L., 1973. Turbulent boundary-layer studies at high Reynolds numbers at Mach numbers between 0.2 and 2.8. ARC (London) R & M 3712. And Winter K.G. private communications. Also: Winter & Gaudet (1970) (1968) and Winter, Smith & Gaudet (1965).		

- 1 The tests were performed at a single station approximately 10.7 m downstream of the throat on the centre line of the plane side wall of a closed-circuit wind-tunnel with a flexible roof and floor. The Mach number at the test station was set to nominal values in steps of 0.2, from 0.2 to 0.8 and from 1.4 to 2.8. All the walls in the nozzle and test-section were coated with a thin layer of epoxy resin providing some thermal
- 2 insulation and giving a good surface finish (typically 6-13 μm). Localised disturbances in the test-area
- 3 caused Mach number perturbations less than 0.006 in the supersonic test cases. Transition occurred naturally and no experimental observations are available. The design is such that the final Mach number is approached
- 4 asymptotically, and has a value within 1 % of its final value for the last 25 % of the effective run. The pressure history is presented graphically in figure 6 of the source, and the temperature history probably
- 5 corresponds to a very slight heat transfer to the flow. No systematic investigation of possible flow convergence was made, but accidental hydraulic leaks showed approximately parallel streak-patterns.
- 6 The instruments were attached to replaceable plugs inserted just upstream of the main tunnel windows. At subsonic speeds the wall static pressure was measured with tapings 3.2 mm in diameter, and corrected for hole size after Gaudet (1965), whilst at supersonic speeds it was assumed constant through the boundary layer and computed from the tunnel reservoir pressure and the pitot pressure just outside the boundary layer. Some measurements of TW were made on the balance plate and the rake mounting plate, the values being closely adiabatic. The wall shear stress was measured using a floating element balance (diameter 368.3 mm), the force on the plate being found by strain gauge techniques. Corrections to the measurements were made to allow for the effects of temperature differences between the back plate and the floating plate.
- 7 Profile surveys were made using rakes mounted so that the profile normal passed through the X-value of the
- 8 balance centre. Thirteen TTP were mounted on a strut. These were STP's with a thermistor bead in a vented stainless steel tube for which d₁ = 2, d₂ = 1.6 and l = 25.4 mm. These were calibrated in the flow near the centre line of the tunnel over a range of Mach number (0.8 < M < 2.8) and Reynolds number, by comparison with an ECP. On separate runs the same strut carried 49 CPP mounted in five columns, so as to avoid mutual interference in an array of densely packed tubes. For the tubes near the wall, d₁ = 0.50 mm, d₂ = 0.25 mm, while further out d₁ = 1.00 mm and d₂ = 0.60 mm. Static pressure probes were also mounted but not used.
- 9 Profile T0 measurements were interpolated to the Y-values of the P0 measurements, and correlation of profile measurements and CF measurements on different occasions was made by interpolation of the data on the basis
- 10 of unit Reynolds number. No corrections were applied to the profile data. Sutherland's viscosity law was
- 11 used.
- 12 The editors have presented the data using the measured temperature distribution - the profiles resulting from a Crocco / Van Driest-relation with recovery factors of 0.89 and 1.0 (isoenergetic) are also tabulated by the authors. The boundary conditions are calculated from the authors' unit Reynolds number values, M0 and TOD. TW has been taken as TR with a recovery factor of 0.896. The profiles in the tables below include some of the wide range of measurements made at subsonic Mach numbers. Those whose serial numbers are/
- 13 followed by a star form a set for all of which the unit Reynolds number was close to 7 × 10⁶/m. The CF values presented with the profiles are as interpolated by the authors. The full Mach number range is covered, from 0.2 to 2.8, with a range of Reynolds number covered at M = 0.8, 1.4, 2.2 and 2.8.

5 DATA: 730101 to 1203 Pitot and TO profiles. $MX = 1$. CF from balance.

16 Editors' comments

The exceptional size of the floating element balance made it possible for the peripheral gap to be fully pressure plotted. Thus aerodynamically induced errors could be eliminated, and the reading of the balance itself is unusually trustworthy. The scale is such however that a substantial variation of CF could occur over the width of the element (Fernholz 1964) so that the recorded value might not be appropriate to the profile recorded at the centre of the plate. The profiles are described in fine detail, but in spite of the large physical scale of the experiment, measurements do not extend within the momentum-deficit peak in about half the cases. Integral values, therefore, should be treated with caution. Log-law plots indicate that substantial probe corrections could reasonably be applied to the data-points closest to the wall. The TO readings in this region are interpolated, but any error introduced in this way will be negligible for an AW case at these relatively low Mach numbers.

The Reynolds number and Mach number ranges are unusually wide and systematically varied and of particular interest since the whole range from $M = 0.2$ to $M = 2.8$ was covered with the same instrumentation. Comparisons should be made with the data of Allen - CAT 7303 and Jackson et al. - CAT 6506 with broadly the same geometry and Reynolds number range. Hopkins & Keener - CAT 6601 whose Reynolds number fall in the range of CAT 7302, give measurements made not on the flat side wall, but on the wall which, upstream, was curved to form the nozzle. Similar tests were made at ultra-high Reynolds number by Moore & Harkness - CAT 6502 and Thomke - CAT 6903. Further high Reynolds number experiments at higher Mach numbers and with varied geometries and boundary layer histories are those of Voisinet & Lee - CAT 7202, Gates - CAT 7301, Jones & Feller - CAT 7002 and Hopkins & Keener - CAT 7203.

CAT 7302		WINTER/GAUDET		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
RUN	MD *	TH/TR*	RED2*	CF *	H12	H12K	PH	PD*		
X	P00*	PH/PD*	REN2D	CO	H32	H32K	TH	TD*		
RZ	T0D*	SN *	D2	P12*	H42	D2K	UD*	TR		
73020101*	0.2007	1.0000	9.5756 ⁺⁰⁴	1.7700 ⁻⁰³	1.2609	1.2451	1.4282 ⁺⁰⁵	1.4282 ⁺⁰⁵		
NM	1.4688 ⁺⁰⁵	1.0000	9.6292 ⁺⁰⁴	NM	1.8201	1.9200	2.8370 ⁺⁰²	2.8168 ⁺⁰²		
INFINITE	2.8395 ⁺⁰²	0.0000	1.4240 ⁻⁰²	0.0000 ⁺⁰⁰	0.0017	1.4272 ⁻⁰²	6.7536 ⁺⁰¹	2.8370 ⁺⁰²		
73020102*	0.2013	1.0000	9.4304 ⁺⁰⁴	1.8300 ⁻⁰³	1.2607	1.2446	1.3787 ⁺⁰⁵	1.3787 ⁺⁰⁵		
NM	1.4182 ⁺⁰⁵	1.0000	9.4834 ⁺⁰⁴	NM	1.8233	1.8231	2.8520 ⁺⁰²	2.8316 ⁺⁰²		
INFINITE	2.8545 ⁺⁰²	0.0000	1.4582 ⁻⁰²	0.0000 ⁺⁰⁰	0.0015	1.4615 ⁻⁰²	6.7915 ⁺⁰¹	2.8520 ⁺⁰²		
73020201*	0.3978	1.0000	8.4937 ⁺⁰⁴	1.7800 ⁻⁰³	1.2898	1.2364	6.8472 ⁺⁰⁴	6.8472 ⁺⁰⁴		
NM	7.6362 ⁺⁰⁴	1.0000	8.6803 ⁺⁰⁴	NM	1.8265	1.8261	2.8469 ⁺⁰²	2.7689 ⁺⁰²		
INFINITE	2.8565 ⁺⁰²	0.0000	1.3214 ⁻⁰²	0.0000 ⁺⁰⁰	0.0136	1.3317 ⁻⁰²	1.3272 ⁻⁰²	2.8469 ⁺⁰²		
73020301*	0.5952	1.0000	8.1145 ⁺⁰⁴	1.7600 ⁻⁰³	1.3896	1.2375	4.4336 ⁺⁰⁴	4.4336 ⁺⁰⁴		
NM	5.6339 ⁺⁰⁴	1.0000	8.5141 ⁺⁰⁴	NM	1.8264	1.8255	2.8337 ⁺⁰²	2.8656 ⁺⁰²		
INFINITE	2.8545 ⁺⁰²	0.0000	1.2739 ⁻⁰²	0.0000 ⁺⁰⁰	0.0023	1.2998 ⁻⁰²	1.9484 ⁺⁰²	2.8337 ⁺⁰²		
73020401*	0.7904	1.0000	7.2951 ⁺⁰⁴	1.7400 ⁻⁰³	1.5286	1.2371	3.1465 ⁺⁰⁴	3.1465 ⁺⁰⁴		
NM	4.7510 ⁺⁰⁴	1.0000	7.9288 ⁺⁰⁴	NM	1.8274	1.8258	2.8393 ⁺⁰²	2.5552 ⁺⁰²		
INFINITE	2.8745 ⁺⁰²	0.0000	1.1916 ⁻⁰²	0.0000 ⁺⁰⁰	-0.0150	1.2362 ⁻⁰²	2.5332 ⁺⁰²	2.8393 ⁺⁰²		
73020402	0.7930	1.0000	1.0879 ⁺⁰⁵	1.6500 ⁻⁰³	1.5227	1.2360	4.7015 ⁺⁰⁴	4.7015 ⁺⁰⁴		
NM	7.1172 ⁺⁰⁴	1.0000	1.1831 ⁺⁰⁵	NM	1.8278	1.8262	2.8293 ⁺⁰²	2.5445 ⁺⁰²		
INFINITE	2.8645 ⁺⁰²	0.0000	1.1797 ⁻⁰²	0.0000 ⁺⁰⁰	-0.0096	1.2236 ⁻⁰²	2.5362 ⁺⁰²	2.8293 ⁺⁰²		
73020403	0.7933	1.0000	1.4182 ⁺⁰⁵	1.5800 ⁻⁰³	1.5201	1.2329	6.2479 ⁺⁰⁴	6.2479 ⁺⁰⁴		
NM	9.4610 ⁺⁰⁴	1.0000	1.5422 ⁺⁰⁵	NM	1.8292	1.8277	2.8391 ⁺⁰²	2.5531 ⁺⁰²		
INFINITE	2.8745 ⁺⁰²	0.0000	1.1618 ⁻⁰²	0.0000 ⁺⁰⁰	-0.0102	1.2047 ⁻⁰²	2.5415 ⁺⁰²	2.8391 ⁺⁰²		
73020501	1.3943	1.0000	1.3702 ⁺⁰⁴	1.9700 ⁻⁰³	2.1014	1.2597	3.4812 ⁺⁰³	3.4812 ⁺⁰³		
NM	1.0990 ⁺⁰⁴	1.0000	1.7425 ⁺⁰⁴	NM	1.8166	1.8118	2.8170 ⁺⁰²	2.0928 ⁺⁰²		
INFINITE	2.9065 ⁺⁰²	0.0000	1.0315 ⁻⁰²	0.0000 ⁺⁰⁰	0.0090	1.1926 ⁻⁰²	4.0442 ⁺⁰²	2.8170 ⁺⁰²		
73020502	1.3951	1.0000	2.9589 ⁺⁰⁴	1.7600 ⁻⁰³	2.1556	1.2649	6.3239 ⁺⁰³	6.3239 ⁺⁰³		
NM	2.6307 ⁺⁰⁴	1.0000	3.7634 ⁺⁰⁴	NM	1.8157	1.8108	2.8227 ⁺⁰²	2.0964 ⁺⁰²		
INFINITE	2.9125 ⁺⁰²	0.0000	9.3327 ⁻⁰³	0.0000 ⁺⁰⁰	-0.0236	1.0447 ⁻⁰²	4.0500 ⁺⁰²	2.8227 ⁺⁰²		
73020503*	1.4003	1.0000	4.5658 ⁺⁰⁴	1.6500 ⁻⁰³	2.1097	1.2477	1.3723 ⁺⁰⁴	1.3723 ⁺⁰⁴		
NM	4.3688 ⁺⁰⁴	1.0000	5.8160 ⁺⁰⁴	NM	1.8255	1.8207	2.8272 ⁺⁰²	2.0957 ⁺⁰²		
INFINITE	2.9175 ⁺⁰²	0.0000	8.7123 ⁻⁰³	0.0000 ⁺⁰⁰	-0.0029	9.7646 ⁻⁰³	4.0643 ⁺⁰²	2.8272 ⁺⁰²		
73020504	1.3999	1.0000	8.7352 ⁺⁰⁴	1.5000 ⁻⁰³	2.0688	1.2410	2.6523 ⁺⁰⁴	2.6523 ⁺⁰⁴		
NM	8.4393 ⁺⁰⁴	1.0000	1.1134 ⁺⁰⁵	NM	1.8292	1.8245	2.7903 ⁺⁰²	2.0687 ⁺⁰²		
INFINITE	2.8795 ⁺⁰²	0.0000	8.4831 ⁻⁰³	0.0000 ⁺⁰⁰	0.0181	9.4136 ⁻⁰³	4.0370 ⁺⁰²	2.7903 ⁺⁰²		
73020505	1.4003	1.0000	9.6076 ⁺⁰⁴	1.4800 ⁻⁰³	2.1302	1.2401	3.0134 ⁺⁰⁴	3.0134 ⁺⁰⁴		
NM	9.5936 ⁺⁰⁴	1.0000	1.2245 ⁺⁰⁵	NM	1.8292	1.8248	2.7990 ⁺⁰²	2.0748 ⁺⁰²		
INFINITE	2.8885 ⁺⁰²	0.0000	8.2420 ⁻⁰³	0.0000 ⁺⁰⁰	-0.0240	9.1681 ⁻⁰³	4.0441 ⁺⁰²	2.7990 ⁺⁰²		
73020601*	1.5970	1.0000	4.0241 ⁺⁰⁴	1.5900 ⁻⁰³	2.3395	1.2456	1.0699 ⁺⁰⁴	1.0699 ⁺⁰⁴		
NM	4.5274 ⁺⁰⁴	1.0000	5.4625 ⁺⁰⁴	NM	1.8283	1.8223	2.8091 ⁺⁰²	1.9320 ⁺⁰²		
INFINITE	2.9175 ⁺⁰²	0.0000	8.2501 ⁻⁰³	0.0000 ⁺⁰⁰	0.0113	9.4320 ⁻⁰³	4.4506 ⁺⁰²	2.8091 ⁺⁰²		
73020701*	1.8002	1.0000	3.5558 ⁺⁰⁴	1.5300 ⁻⁰³	2.6196	1.2416	8.5372 ⁺⁰³	8.5372 ⁺⁰³		
NM	4.9668 ⁺⁰⁴	1.0000	5.1780 ⁺⁰⁴	NM	1.8305	1.8235	2.7894 ⁺⁰²	1.7690 ⁺⁰²		
INFINITE	2.9155 ⁺⁰²	0.0000	7.7130 ⁻⁰³	0.0000 ⁺⁰⁰	0.0202	9.1102 ⁻⁰³	4.8005 ⁺⁰²	2.7894 ⁺⁰²		
73020801*	2.0002	1.0000	3.1338 ⁺⁰⁴	1.4600 ⁻⁰³	2.8926	1.2456	6.6819 ⁺⁰³	6.6819 ⁺⁰³		
NM	5.2299 ⁺⁰⁴	1.0000	4.9070 ⁺⁰⁴	NM	1.8310	1.8223	2.7728 ⁺⁰²	1.6195 ⁺⁰²		
INFINITE	2.9135 ⁺⁰²	0.0000	7.4463 ⁻⁰³	0.0000 ⁺⁰⁰	0.0501	9.0729 ⁻⁰³	5.1019 ⁺⁰²	2.7728 ⁺⁰²		

CAT 7302

WINTER/GAUDET

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X RZ	MD * POD* TOD*	TW/TR* PW/PD* SW * D2	RED2* REN2D	CF * C0 PI2*	H12 H32 H42	H12K H32K D2K	PW TW UD*	PO* TO* TR
73020901*	2.1865	1.0000	8.3321*+03	1.7000*-03	3.2648	1.2573	1.3975*+03	1.3975*+03
NM	1.4630*+04	1.0000	1.3993*+04	NM	1.8211	1.8118	2.7578*+02	1.4899*+02
INFINITE	2.9145*+02	0.0000	8.2677*-03	0.0000*+00	0.0420	1.0559*-02	5.3511*+02	2.7578*+02
73020902	2.1972	1.0000	1.7468*+04	1.4900*-03	3.2783	1.2521	3.2427*+03	3.2427*+03
NM	3.4522*+04	1.0000	2.9453*+04	NM	1.8269	1.8180	2.7589*+02	1.4838*+02
INFINITE	2.9165*+02	0.0000	7.4206*-03	0.0000*+00	0.0424	9.4579*-03	5.3662*+02	2.7589*+02
73020903	2.2014	1.0000	2.7113*+04	1.3800*-03	3.2913	1.2457	5.4045*+03	5.4045*+03
NM	5.7915*+04	1.0000	4.5791*+04	NM	1.8326	1.8225	2.7576*+02	1.4865*+02
INFINITE	2.9155*+02	0.0000	6.8874*-03	0.0000*+00	0.0322	8.7266*-03	5.3705*+02	2.7576*+02
73020904	2.2064	1.0000	4.9459*+04	1.2800*-03	3.3165	1.2348	1.0458*+04	1.0458*+04
NM	1.1295*+05	1.0000	8.3762*+04	NM	1.8381	1.8287	2.7365*+02	1.4661*+02
INFINITE	2.8935*+02	0.0000	6.4078*-03	0.0000*+00	0.0141	8.0676*-03	5.3564*+02	2.7365*+02
73020905	2.1984	1.0000	1.0864*+04	1.6100*-03	3.5115	1.2888	1.9162*+03	1.9162*+03
NM	2.0438*+04	1.0000	1.8153*+04	NM	1.8132	1.8013	2.7247*+02	1.4647*+02
INFINITE	2.8895*+02	0.0000	7.6800*-03	0.0000*+00	-0.0392	1.0022*-02	5.3345*+02	2.7247*+02
73020906	2.1992	1.0000	1.4142*+04	1.5400*-03	3.3233	1.2722	2.5471*+03	2.5471*+03
NM	2.7201*+04	1.0000	2.3879*+04	NM	1.8207	1.8046	2.7428*+02	1.4739*+02
INFINITE	2.8995*+02	0.0000	7.5812*-03	0.0000*+00	0.0343	9.7108*-03	5.3530*+02	2.7428*+02
73020907	2.2005	1.0000	1.6653*+04	1.4900*-03	3.4495	1.2694	3.1937*+03	3.1937*+03
NM	3.4176*+04	1.0000	2.8123*+04	NM	1.8223	1.8116	2.7521*+02	1.4781*+02
INFINITE	2.9095*+02	0.0000	7.1449*-03	0.0000*+00	-0.0256	9.1992*-03	5.3639*+02	2.7521*+02
73020908	2.2012	1.0000	1.8926*+04	1.4600*-03	3.5084	1.2620	3.8033*+03	3.8033*+03
NM	4.0744*+04	1.0000	3.1955*+04	NM	1.8253	1.8153	2.7633*+02	1.4837*+02
INFINITE	2.9215*+02	0.0000	6.8511*-03	0.0000*+00	-0.0581	8.8231*-03	5.3758*+02	2.7633*+02
73020909	2.2025	1.0000	2.1892*+04	1.4300*-03	3.4343	1.2568	4.4345*+03	4.4345*+03
NM	4.7603*+04	1.0000	3.6971*+04	NM	1.8275	1.8184	2.7699*+02	1.4864*+02
INFINITE	2.9285*+02	0.0000	6.8116*-03	0.0000*+00	-0.0263	8.7171*-03	5.3839*+02	2.7699*+02
73020910*	2.2040	1.0000	2.5495*+04	1.3900*-03	3.4721	1.2533	5.3465*+03	5.3465*+03
NM	5.7527*+04	1.0000	4.3074*+04	NM	1.8307	1.8207	2.7726*+02	1.4869*+02
INFINITE	2.9315*+02	0.0000	6.5888*-03	0.0000*+00	-0.0446	8.4304*-03	5.3885*+02	2.7726*+02
73020911	2.2054	1.0000	2.9789*+04	1.3700*-03	3.3878	1.2510	6.2876*+03	6.2876*+03
NM	6.7802*+04	1.0000	5.0351*+04	NM	1.8316	1.8219	2.7744*+02	1.4870*+02
INFINITE	2.9335*+02	0.0000	6.5379*-03	0.0000*+00	-0.0082	8.3099*-03	5.3920*+02	2.7744*+02
73020912	2.2064	1.0000	3.5004*+04	1.3300*-03	3.4064	1.2463	7.5204*+03	7.5204*+03
NM	8.1223*+04	1.0000	5.9189*+04	NM	1.8341	1.8245	2.7742*+02	1.4863*+02
INFINITE	2.9335*+02	0.0000	6.4183*-03	0.0000*+00	-0.0179	8.1642*-03	5.3933*+02	2.7742*+02
73020913	2.2071	1.0000	4.0203*+04	1.3100*-03	3.4179	1.2431	8.8038*+03	8.8038*+03
NM	9.5188*+04	1.0000	6.7996*+04	NM	1.8357	1.8264	2.7743*+02	1.4859*+02
INFINITE	2.9335*+02	0.0000	6.2945*-03	0.0000*+00	-0.0254	7.9974*-03	5.3941*+02	2.7743*+02
73020914	2.2082	1.0000	4.6532*+04	1.2900*-03	3.3832	1.2415	1.0272*+04	1.0272*+04
NM	1.1125*+05	1.0000	7.8719*+04	NM	1.8362	1.8271	2.7799*+02	1.4882*+02
INFINITE	2.9395*+02	0.0000	6.2557*-03	0.0000*+00	-0.0101	7.9241*-03	5.4010*+02	2.7799*+02
73021001*	2.4020	1.0000	2.1827*+04	1.3500*-03	3.7448	1.2481	4.2027*+03	4.2027*+03
NM	6.1636*+04	1.0000	3.9815*+04	NM	1.8330	1.8214	2.7502*+02	1.3568*+02
INFINITE	2.9225*+02	0.0000	6.2427*-03	0.0000*+00	0.0085	8.2434*-03	5.4098*+02	2.7502*+02
73021101*	2.5993	1.0000	2.0262*+04	1.2900*-03	4.0346	1.2491	3.4311*+03	3.4311*+03
NM	6.8389*+04	1.0000	3.9907*+04	NM	1.8344	1.8208	2.7462*+02	1.4868*+02
INFINITE	2.9315*+02	0.0000	6.7808*-03	0.0000*+00	0.0633	8.5716*-03	5.4192*+02	2.7462*+02
73021201	2.7894	1.0000	5.4382*+03	1.5300*-03	4.5242	1.2555	7.1397*+02	7.1397*+02
NM	1.9865*+04	1.0000	1.1563*+04	NM	1.8262	1.8127	2.7072*+02	1.1351*+02
INFINITE	2.9015*+02	0.0000	7.1222*-03	0.0000*+00	0.0526	1.0306*-02	5.9585*+02	2.7072*+02
73021202	2.7972	1.0000	1.1064*+04	1.3200*-03	4.5486	1.2605	1.6936*+03	1.6936*+03
NM	4.9786*+04	1.0000	2.3561*+04	NM	1.8277	1.8130	2.7347*+02	1.1429*+02
INFINITE	2.9315*+02	0.0000	8.1812*-03	0.0000*+00	0.0484	8.8605*-03	5.9958*+02	2.7347*+02
73021203*	2.7996	1.0000	1.7532*+04	1.2100*-03	4.5447	1.2446	2.8189*+03	2.8189*+03
NM	7.6434*+04	1.0000	3.7394*+04	NM	1.8410	1.8251	2.7225*+02	1.1367*+02
INFINITE	2.9185*+02	0.0000	5.8242*-03	0.0000*+00	0.0374	8.2116*-03	5.9845*+02	2.7225*+02

73020402		WINTER/GAUGET		PROFILE TABULATION		39 POINTS, DELTA AT POINT 39		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.98761	0.00000	0.00000	1.11182	0.00000
2	3.0480+04	1.1129+00	NM	0.99206	0.49664	0.51710	1.08320	0.47738
3	3.5560+04	1.1098+00	NM	0.99200	0.49003	0.51020	1.08402	0.47066
4	8.3820+04	1.1367+00	NM	0.99323	0.54458	0.56540	1.07794	0.52452
5	1.1938+03	1.1492+00	NM	0.99353	0.56762	0.56850	1.07493	0.54748
6	1.4478+03	1.1590+00	NM	0.99414	0.58513	0.60610	1.07297	0.56488
7	1.6002+03	1.1617+00	NM	0.99427	0.58962	0.61080	1.07239	0.56957
8	2.1844+03	1.1700+00	NM	0.99438	0.60402	0.62490	1.07033	0.58384
9	2.5400+03	1.1789+00	NM	0.99473	0.61879	0.63960	1.06838	0.59866
10	3.0988+03	1.1911+00	NM	0.99520	0.63825	0.65890	1.06576	0.61824
11	3.4544+03	1.1937+00	NM	0.99507	0.64226	0.66280	1.06497	0.62237
12	4.2672+03	1.2053+00	NM	0.99550	0.66009	0.68040	1.06248	0.64039
13	5.0546+03	1.2082+00	NM	0.99534	0.66445	0.68460	1.06158	0.64489
14	6.4770+03	1.2212+00	NM	0.99627	0.68352	0.70350	1.05933	0.66410
15	7.4930+03	1.2367+00	NM	0.99669	0.70533	0.72480	1.05597	0.68638
16	8.8900+03	1.2435+00	NM	0.99667	0.71465	0.73380	1.05430	0.69601
17	1.1252+02	1.2539+00	NM	0.99717	0.72869	0.74750	1.05230	0.71035
18	1.2294+02	1.2616+00	NM	0.99691	0.73878	0.75710	1.05020	0.72091
19	1.5037+02	1.2688+00	NM	0.99748	0.74805	0.76620	1.04910	0.73034
20	1.7501+02	1.2815+00	NM	0.99792	0.76411	0.78170	1.04658	0.74691
21	2.2606+02	1.2971+00	NM	0.99855	0.78320	0.80010	1.04363	0.76665
22	2.5197+02	1.3080+00	NM	0.99855	0.79619	0.81240	1.04113	0.78031
23	3.0226+02	1.3203+00	NM	0.99864	0.81057	0.82600	1.03843	0.79543
24	3.5560+02	1.3344+00	NM	0.99908	0.82856	0.84120	1.03574	0.81218
25	4.0564+02	1.3452+00	NM	0.99909	0.83842	0.85230	1.03338	0.82477
26	4.5491+02	1.3571+00	NM	0.99935	1.85139	0.86450	1.03104	0.83848
27	5.0724+02	1.3689+00	NM	0.99966	0.86394	0.87630	1.02881	0.85176
28	5.5677+02	1.3795+00	NM	1.00032	0.87497	0.88680	1.02722	0.86330
29	6.1214+02	1.3919+00	NM	1.00082	0.88762	0.89870	1.02512	0.87668
30	6.6192+02	1.4004+00	NM	1.00072	0.89615	0.90650	1.02323	0.88592
31	7.0764+02	1.4106+00	NM	1.00156	0.90620	0.91610	1.02197	0.89640
32	7.6022+02	1.4218+00	NM	1.00126	0.91706	0.92590	1.01937	0.90831
33	8.8722+02	1.4455+00	NM	1.00192	0.93447	0.94660	1.01523	0.93240
34	1.0140+01	1.4686+00	NM	1.00271	0.96063	0.96610	1.01143	0.95518
35	1.1410+01	1.4853+00	NM	1.00261	0.97547	0.97940	1.00807	0.97156
36	1.2677+01	1.4997+00	NM	1.00284	0.98797	0.99070	1.00553	0.98525
37	1.3955+01	1.5080+00	NM	1.00191	0.99510	0.99660	1.00301	0.99361
38	1.5217+01	1.5129+00	NM	1.00073	0.99925	0.99970	1.00090	0.99880
D 39	1.6490+01	1.5138+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD

73020505		WINTER/GAUGET		PROFILE TABULATION		38 POINTS, DELTA AT POINT 38		
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	0.98892	0.00000	0.00000	1.34889	0.00000
2	3.0480+04	1.3432+00	NM	0.97994	0.47357	0.53030	1.29395	0.42290
3	3.5560+04	1.3390+00	NM	0.97981	0.47098	0.52760	1.25489	0.42043
4	8.3820+04	1.4224+00	NM	0.98196	0.51969	0.57780	1.23012	0.46743
5	1.1938+03	1.4633+00	NM	0.98265	0.54130	0.59960	1.22702	0.48866
6	1.4478+03	1.5014+00	NM	0.98386	0.56034	0.61880	1.21454	0.50740
7	1.6002+03	1.5060+00	NM	0.98399	0.56254	0.62100	1.21865	0.50958
8	2.1844+03	1.5620+00	NM	0.98531	0.58867	0.64690	1.20761	0.53564
9	2.5400+03	1.5918+00	NM	0.98600	0.60182	0.65980	1.20195	0.54894
10	3.0988+03	1.6312+00	NM	0.98663	0.61856	0.67600	1.19434	0.56600
11	3.4544+03	1.6398+00	NM	0.98725	0.62202	0.67950	1.19334	0.56941
12	4.2672+03	1.6855+00	NM	0.98705	0.64044	0.69680	1.18373	0.58865
13	5.0546+03	1.7194+00	NM	0.98824	0.65349	0.70940	1.17843	0.60149
14	6.4770+03	1.7618+00	NM	0.98886	0.66924	0.72420	1.17098	0.61846
15	7.4930+03	1.8206+00	NM	0.99028	0.68999	0.74370	1.16173	0.64017
16	8.8900+03	1.8474+00	NM	0.99020	0.69919	0.75200	1.15676	0.65009
17	1.0211+02	1.8723+00	NM	0.99052	0.70739	0.75950	1.15276	0.65886
18	1.1252+02	1.9100+00	NM	0.99127	0.71960	0.77070	1.14707	0.67189
19	1.2294+02	1.9361+00	NM	0.99148	0.72784	0.77810	1.14267	0.68083
20	1.5037+02	1.9665+00	NM	0.99251	0.73724	0.78680	1.13897	0.69080
21	2.2606+02	2.1132+00	NM	0.99467	0.78007	0.82490	1.11796	0.73777
22	2.5197+02	2.1567+00	NM	0.99484	0.79211	0.83510	1.11149	0.75133
23	3.0226+02	2.2240+00	NM	0.99611	0.81074	0.85130	1.10255	0.77212
24	3.5560+02	2.3080+00	NM	0.99701	0.83104	0.86850	1.09214	0.79519
25	4.0564+02	2.3699+00	NM	0.99796	0.84766	0.88250	1.08390	0.81419
26	4.5491+02	2.4386+00	NM	0.99899	0.86455	0.89660	1.07551	0.83365
27	5.0724+02	2.5096+00	NM	0.99972	0.88158	0.91050	1.06867	0.85359
28	5.5677+02	2.5682+00	NM	1.00079	0.89557	0.92200	1.05984	0.86990
29	6.1214+02	2.6373+00	NM	1.00190	0.91122	0.93470	1.05219	0.88833
30	6.6192+02	2.6947+00	NM	1.00219	0.92416	0.94480	1.04516	0.90398
31	7.0764+02	2.7498+00	NM	1.00295	0.93550	0.95380	1.03951	0.91755
32	7.6022+02	2.8032+00	NM	1.00403	0.94806	0.96380	1.03349	0.93257
33	8.8722+02	2.9198+00	NM	1.00600	0.97297	0.98330	1.02135	0.96275
34	1.0140+01	3.0054+00	NM	1.00713	0.99080	0.99690	1.01235	0.98474
35	1.1410+01	3.0363+00	NM	1.00594	0.99714	1.00090	1.00756	0.99339
36	1.2677+01	3.0451+00	NM	1.00392	0.99894	1.00120	1.00452	0.99669
37	1.3955+01	3.0481+00	NM	1.00225	0.99955	1.00080	1.00251	0.99830
D 38	1.5217+01	3.0503+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD

73020908		WINTER/GAUGET		PROFILE TABULATION		35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94586	0.00000	0.00000	1.86246	0.00000	
2	3.0480*-04	1.5886*+00	NM	0.96287	0.38197	0.49230	1.66113	0.29836	
3	9.6520*-04	1.9025*+00	NM	0.96913	0.45626	0.57495	1.58793	0.36207	
4	1.2192*-03	1.9680*+00	NM	0.96971	0.46930	0.58870	1.57356	0.37412	
5	1.4478*-03	2.0310*+00	NM	0.97164	0.48129	0.60160	1.56250	0.38502	
6	1.5748*-03	2.0580*+00	NM	0.97232	0.48623	0.60690	1.55763	0.38963	
7	2.6416*-03	2.2454*+00	NM	0.97506	0.51900	0.64000	1.52253	0.42061	
8	3.0480*-03	2.3448*+00	NM	0.97644	0.53524	0.65660	1.50489	0.43631	
9	3.6068*-03	2.4467*+00	NM	0.97726	0.55124	0.67210	1.48655	0.45212	
10	4.7244*-03	2.5871*+00	NM	0.97804	0.57235	0.69270	1.46477	0.47291	
11	4.9530*-03	2.5750*+00	NM	0.97950	0.57057	0.69090	1.46628	0.47119	
12	6.2738*-03	2.7490*+00	NM	0.98190	0.59557	0.71440	1.43885	0.49651	
13	7.4168*-03	2.8760*+00	NM	0.98343	0.61306	0.73040	1.41945	0.51457	
14	8.8900*-03	2.9835*+00	NM	0.98469	0.62742	0.74330	1.40351	0.52960	
15	9.9314*-03	3.0560*+00	NM	0.98605	0.63690	0.75190	1.39373	0.53949	
16	1.0693*-02	3.1175*+00	NM	0.98613	0.64481	0.75860	1.38408	0.54809	
17	1.2294*-02	3.2104*+00	NM	0.98671	0.65656	0.76860	1.37043	0.56095	
18	1.4961*-02	3.3798*+00	NM	0.99483	0.67740	0.78880	1.35593	0.58174	
19	1.7272*-02	3.4905*+00	NM	0.99015	0.69066	0.79750	1.33333	0.59812	
20	1.9634*-02	3.5710*+00	NM	0.99103	0.70246	0.80710	1.32013	0.61138	
21	2.2403*-02	3.7265*+00	NM	0.99230	0.71803	0.81960	1.30293	0.62904	
22	3.0277*-02	4.0957*+00	NM	0.99579	0.75871	0.85120	1.25865	0.67628	
23	3.5560*-02	4.3276*+00	NM	0.99613	0.78313	0.86950	1.23274	0.70534	
24	4.0183*-02	4.5247*+00	NM	0.99989	0.80327	0.88410	1.21134	0.72982	
25	4.5618*-02	4.7628*+00	NM	1.00223	0.82692	0.90090	1.18894	0.75901	
26	5.0851*-02	4.9836*+00	NM	1.00343	0.84223	0.91520	1.16414	0.78616	
27	5.5626*-02	5.1783*+00	NM	1.00450	0.86657	0.92720	1.14482	0.80991	
28	6.1062*-02	5.4048*+00	NM	1.00724	0.89743	0.94120	1.12486	0.83673	
29	6.6192*-02	5.6095*+00	NM	1.00739	0.90584	0.95220	1.10497	0.86174	
30	7.0815*-02	5.7898*+00	NM	1.00926	0.92175	0.96230	1.08992	0.88291	
31	7.6098*-02	5.9876*+00	NM	1.01094	0.93889	0.97280	1.07354	0.90616	
32	8.8773*-02	6.3852*+00	NM	1.01324	0.97241	0.99220	1.04112	0.95301	
33	1.0140*-01	6.6261*+00	NM	1.01514	0.99215	1.00350	1.02302	0.98092	
34	1.1417*-01	6.7108*+00	NM	1.00362	0.99900	1.00100	1.00402	0.99700	
D 35	1.2687*-01	6.7233*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
AT I=J DATA WERE AVERAGED

73020910*		WINTER/GAUGET		PROFILE TABULATION		35 POINTS, DELTA AT POINT 35			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94579	0.00000	0.00000	1.86486	0.00000	
2	3.0480*-04	1.6259*+00	NM	0.96728	0.39160	0.50450	1.65975	0.30396	
3	9.6520*-04	1.9394*+00	NM	0.97402	0.46310	0.58360	1.58919	0.36736	
4	1.2192*-03	2.0097*+00	NM	0.97511	0.47669	0.59820	1.57480	0.37986	
5	1.4478*-03	2.0713*+00	NM	0.97596	0.48808	0.61010	1.56240	0.39046	
6	1.5748*-03	2.1088*+00	NM	0.97649	0.49484	0.61710	1.55521	0.39680	
7	2.6416*-03	2.3122*+00	NM	0.97845	0.52932	0.65180	1.51630	0.42986	
8	3.0480*-03	2.4211*+00	NM	0.98043	0.54658	0.66900	1.49813	0.44656	
9	3.6068*-03	2.5317*+00	NM	0.98175	0.56345	0.68530	1.47929	0.46326	
10	4.7244*-03	2.6694*+00	NM	0.98329	0.58355	0.70430	1.45866	0.48350	
11	4.9530*-03	2.6427*+00	NM	0.98438	0.57971	0.70120	1.46306	0.47927	
12	6.2738*-03	2.8469*+00	NM	0.98512	0.60834	0.72710	1.42857	0.50897	
13	7.4168*-03	2.9624*+00	NM	0.98728	0.62383	0.74140	1.41243	0.52491	
14	8.8900*-03	3.0763*+00	NM	0.98780	0.63871	0.75430	1.39470	0.54083	
15	9.9314*-03	3.1473*+00	NM	0.98824	0.64778	0.76210	1.38408	0.55062	
16	1.0693*-02	3.2035*+00	NM	0.98905	0.65486	0.76830	1.37646	0.55817	
17	1.2294*-02	3.3011*+00	NM	0.98969	0.66697	0.77850	1.36240	0.57142	
18	1.4961*-02	3.4752*+00	NM	0.99150	0.68797	0.79610	1.33905	0.59453	
19	1.7272*-02	3.5962*+00	NM	0.99164	0.70217	0.80730	1.32188	0.61072	
20	1.9634*-02	3.6897*+00	NM	0.99238	0.71292	0.81590	1.30976	0.62294	
21	2.2403*-02	3.8208*+00	NM	0.99377	0.72772	0.82770	1.29366	0.63981	
22	3.0277*-02	4.2008*+00	NM	0.99596	0.78891	0.85870	1.24719	0.68851	
23	3.5560*-02	4.4361*+00	NM	0.99917	0.79326	0.87710	1.22249	0.71747	
24	4.0183*-02	4.6367*+00	NM	0.99975	0.81345	0.89100	1.19976	0.74265	
25	4.5618*-02	4.8755*+00	NM	1.00150	0.83680	0.90710	1.17504	0.77194	
26	5.0851*-02	5.0947*+00	NM	1.00312	0.85766	0.92110	1.15340	0.79859	
27	5.5626*-02	5.2945*+00	NM	1.00404	0.87623	0.93300	1.13379	0.82291	
28	6.1062*-02	5.5184*+00	NM	1.00592	0.89655	0.94610	1.11354	0.84960	
29	6.6192*-02	5.7289*+00	NM	1.00713	0.91585	0.95780	1.09469	0.87477	
30	7.0815*-02	5.9035*+00	NM	1.00738	0.93046	0.96640	1.07875	0.89585	
31	7.6098*-02	6.0961*+00	NM	1.00926	0.94695	0.97650	1.06338	0.91830	
32	8.8773*-02	6.4701*+00	NM	1.01107	0.97816	0.99420	1.03306	0.96239	
33	1.0140*-01	6.6702*+00	NM	1.00970	0.99446	1.00200	1.01523	0.98697	
34	1.1417*-01	6.7328*+00	NM	1.00231	0.99950	1.00100	1.00301	0.99800	
D 35	1.2687*-01	6.7391*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	


INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
AT I=J DATA WERE AVERAGED

73021101*		WINTER/GAUGET		PROFILE TABULATION		38 POINTS, DELTA AT POINT 38			
I	Y	P12/P	P/PO	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0700*+00	1.0000*+00	NM	0.93678	0.00000	0.00000	2.20263	0.00000	
2	3.0480*+04	1.7260*+00	NM	0.95445	0.35340	0.48970	1.92012	0.25504	
3	3.5560*+04	1.6864*+00	NM	0.95271	0.34521	0.47950	1.92438	0.24852	
4	8.3820*+04	2.1468*+00	NM	0.96050	0.42526	0.57290	1.81488	0.31567	
5	1.1938*+03	2.2623*+00	NM	0.96244	0.44190	0.59130	1.79051	0.33024	
6	1.4478*+03	2.3660*+00	NM	0.97160	0.45613	0.60910	1.78317	0.34158	
7	1.6002*+03	2.3917*+00	NM	0.96322	0.45988	0.61030	1.76149	0.34647	
8	2.1844*+03	2.6192*+00	NM	0.96490	0.48867	0.64000	1.71527	0.37312	
9	2.5400*+03	2.7006*+00	NM	0.96626	0.49858	0.65020	1.70068	0.38232	
10	3.0988*+03	2.8526*+00	NM	0.96675	0.51647	0.66760	1.67084	0.39956	
11	3.4544*+03	2.9380*+00	NM	0.95966	0.52621	0.67430	1.64204	0.41065	
12	4.2672*+03	3.0632*+00	NM	0.97018	0.54014	0.69090	1.63613	0.42228	
13	5.0546*+03	3.2253*+00	NM	0.97133	0.55758	0.70710	1.60823	0.43967	
14	6.4770*+03	3.4127*+00	NM	0.97294	0.57702	0.72480	1.57778	0.45938	
15	7.4930*+03	3.5638*+00	NM	0.97380	0.59218	0.73810	1.55352	0.47511	
16	8.8900*+03	3.6814*+00	NM	0.97550	0.60370	0.74840	1.53681	0.48698	
17	1.0211*+02	3.8471*+00	NM	0.97683	0.61953	0.76190	1.51240	0.50377	
18	1.1252*+02	3.9484*+00	NM	0.97706	0.62900	0.76960	1.49701	0.51409	
19	1.2294*+02	4.0220*+00	NM	0.97888	0.63579	0.77570	1.48854	0.52112	
20	1.5037*+02	4.2391*+00	NM	0.98010	0.65538	0.79140	1.45815	0.54274	
21	1.7501*+02	4.4112*+00	NM	0.98095	0.67040	0.80310	1.43472	0.55976	
22	1.9837*+02	4.5626*+00	NM	0.98309	0.68347	0.81360	1.41703	0.57416	
23	2.2606*+02	4.7877*+00	NM	0.98442	0.70233	0.82770	1.38889	0.59594	
24	2.5197*+02	4.9329*+00	NM	0.98554	0.71422	0.83650	1.37174	0.60981	
25	3.0226*+02	5.3016*+00	NM	0.98804	0.74352	0.85740	1.32974	0.64476	
26	3.5560*+02	5.6657*+00	NM	0.99082	0.77141	0.87660	1.29132	0.67884	
27	4.0564*+02	5.9838*+00	NM	0.99227	0.79481	0.89170	1.25865	0.70846	
28	4.5491*+02	6.3147*+00	NM	0.99398	0.81880	0.90670	1.22624	0.73941	
29	5.0724*+02	6.6714*+00	NM	0.99606	0.84330	0.92160	1.19432	0.77166	
30	5.5677*+02	6.9924*+00	NM	0.99743	0.86499	0.93410	1.16618	0.80099	
31	6.1214*+02	7.3462*+00	NM	0.99858	0.88827	0.94690	1.13636	0.83327	
32	6.6192*+02	7.6543*+00	NM	1.00019	0.90805	0.95770	1.11235	0.86097	
33	7.0764*+02	7.9357*+00	NM	1.00166	0.92574	0.96710	1.09135	0.88615	
34	7.6022*+02	8.2414*+00	NM	1.00253	0.94458	0.97650	1.06872	0.91371	
35	8.8722*+02	8.8192*+00	NM	1.00446	0.97920	0.99320	1.02881	0.96539	
36	1.1410*+01	9.1610*+00	NM	0.99897	0.99910	0.99910	1.00000	0.99910	
37	1.2677*+01	9.1801*+00	NM	1.00023	1.00020	1.00020	1.00000	1.00020	
D 38	1.3955*+01	9.1766*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD

73021203*		WINTER/GAUGET		PROFILE TABULATION		38 POINTS, DELTA AT POINT 38			
I	Y	P12/P	P/PO	T0/T0D	H/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.93284	0.00000	0.00000	2.39512	0.00000	
2	3.0480*+04	1.7792*+00	NM	0.95165	0.33786	0.48640	2.07254	0.23469	
3	3.5560*+04	1.7929*+00	NM	0.95176	0.34030	0.48740	2.06825	0.23662	
4	8.3820*+04	2.2948*+00	NM	0.95806	0.41448	0.57700	1.93798	0.29773	
5	1.1938*+03	2.4304*+00	NM	0.96014	0.43143	0.59600	1.90840	0.31230	
6	1.4478*+03	2.5466*+00	NM	0.96147	0.44531	0.61110	1.88324	0.32449	
7	1.6002*+03	2.5929*+00	NM	0.96302	0.45068	0.61720	1.87547	0.32904	
8	2.1844*+03	2.8369*+00	NM	0.96423	0.47784	0.64520	1.82315	0.35389	
9	2.5400*+03	2.9208*+00	NM	0.96449	0.48677	0.65410	1.80571	0.36224	
10	3.0988*+03	3.0840*+00	NM	0.96716	0.50361	0.67130	1.77683	0.37781	
11	3.4544*+03	3.2078*+00	NM	0.96768	0.51528	0.68250	1.75439	0.38902	
12	4.2672*+03	3.3718*+00	NM	0.96857	0.52899	0.69550	1.72861	0.40235	
13	5.0546*+03	3.5180*+00	NM	0.97062	0.54559	0.71120	1.69924	0.41854	
14	6.4770*+03	3.7674*+00	NM	0.97357	0.56818	0.73200	1.65975	0.44103	
15	7.4930*+03	3.9251*+00	NM	0.97366	0.58199	0.74370	1.63292	0.45544	
16	8.8900*+03	4.0712*+00	NM	0.97493	0.59448	0.75450	1.61082	0.46839	
17	1.0211*+02	4.2497*+00	NM	0.97621	0.60937	0.76700	1.58426	0.48413	
18	1.1252*+02	4.3612*+00	NM	0.97726	0.61847	0.77460	1.56863	0.49381	
19	1.2294*+02	4.4642*+00	NM	0.97840	0.62676	0.78150	1.55473	0.50266	
20	1.5037*+02	4.7272*+00	NM	0.97903	0.64742	0.79740	1.51694	0.52565	
21	1.7501*+02	4.9377*+00	NM	0.98077	0.66295	0.80950	1.49098	0.54293	
22	1.9837*+02	5.1260*+00	NM	0.98690	0.67751	0.82660	1.46854	0.55531	
23	2.2606*+02	5.3867*+00	NM	0.98435	0.69645	0.83450	1.43575	0.58123	
24	2.5197*+02	5.5823*+00	NM	0.98547	0.71032	0.84430	1.41283	0.59760	
25	3.0226*+02	6.0240*+00	NM	0.98826	0.74066	0.86510	1.36426	0.63412	
26	3.5560*+02	6.4741*+00	NM	0.99112	0.77033	0.88450	1.31839	0.67089	
27	4.0564*+02	6.8673*+00	NM	0.99239	0.79532	0.89960	1.27943	0.70313	
28	4.5491*+02	7.2983*+00	NM	0.99481	0.82182	0.91540	1.24069	0.73781	
29	5.0724*+02	7.7297*+00	NM	0.99723	0.84751	0.93010	1.20438	0.77226	
30	5.5677*+02	8.1233*+00	NM	0.99870	0.87029	0.94230	1.17233	0.80378	
31	6.1214*+02	8.5607*+00	NM	1.00161	0.89490	0.95560	1.14025	0.83806	
32	6.6192*+02	8.9690*+00	NM	1.00353	0.91728	0.96690	1.11111	0.87021	
33	7.0764*+02	9.2917*+00	NM	1.00571	0.93459	0.97570	1.08992	0.89520	
34	7.6022*+02	9.6631*+00	NM	1.00827	0.95411	0.98540	1.06667	0.92381	
35	8.8722*+02	9.6659*+00	NM	1.00834	0.95426	0.98530	1.06655	0.92400	
36	1.1410*+01	1.0542*+01	NM	0.99854	0.99880	0.99880	1.00000	0.99880	
37	1.2677*+01	1.0562*+01	NM	0.99976	0.99980	0.99980	1.00000	0.99980	
D 38	1.3955*+01	1.0567*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD

	M : a) 2.0 b) 2.3, 4.6 R THETA X 10 ⁻³ : 10 - 80 TW/TR : 1.0	7303
		ZPG - AW
Windtunnels a) symmetrical flexible nozzle, b) asymmetric block nozzle. Both: W = H = 1.22 m, continuous, 30 minutes settling time. a) PO : 0.07 MN/m ² TO : 314 K. b) 0.02 < PO < 0.62 MN/m ² . 339 < TO < 352 Dried air, dew point 244 K. 2 < RE/m X 10 ⁻⁶ < 17.		
ALLEN J.M. 1973a. Evaluation of compressible-flow Preston tube calibrations. NASA TN D-7190. And Allen (1972), and private communications.		

- 1 The test boundary layers were formed on the flat side walls of the two wind-tunnels by expansion through two-dimensional nozzles. For a) the test station was "about 5 m from the throat" on the centre line of the test section wall, while for b) it was "midway of the test section" which was 2.13 m long. The test section walls were not cooled and were allowed to reach equilibrium temperature. The surfaces were smooth to 0.8 μ m.
- 6 Wall shear stress was measured using a commercial balance (Kistler, d = 9.27 mm) as described by Paros (1970), and a wide range of Preston tubes (d₁ from 1.3 to 48 mm) were used as the principal aim of the investigation was to calibrate these. For case a) the static pressure was measured at orifices on the tunnel sidewall about 1.6 m upstream of the test station.
- 7 Pitot pressure profiles were taken using an asymmetric FPP for which h₁ = 0.26, h₂ = 0.08, b₁ = 0.88 (E) mm.
- 8 The wall thickness next to the tunnel wall was 0.13 mm. The profile normal was "a few cm" upstream of the balance centre, no adjustment to the values being made as it was estimated that the difference would be below 0.03 % in CF. The static pressure was assumed to be constant through the layer and equal to the value calculated from Pitot measurements at the boundary layer edge. No Pitot corrections were applied
- 10 and Sutherland's viscosity law was assumed. The author tabulates profiles of M and U/UD calculated on the basis of iso-energetic flow. The editors have replaced this assumption with the van Driest / Crocco temperature-velocity correlation assuming an adiabatic wall. The edge total state has been arbitrarily set at the tunnel stagnation conditions.
- 12
- 13 The profiles presented here are for three different Mach numbers, the sets for M = 2.3 (02) and M = 4.6 (03)
- 14 covering a range of Reynolds number. The CF values associated with the profiles are those measured with the balance. The value for 0301 is the author's extrapolation from other measurements at that Mach number, no balance measurement having been taken. The Preston tube results are not presented here but are fully tabulated in the source. The results are summarized in Allen (1973b).
- 5 DATA: 7303 0101-0306. Pitot profiles NX = 1. CF from Balance.

15 Editors' comments

This experiment provides, together with Hopkins & Keener - CAT 6601, the principal body of calibration data for Preston tubes at high Reynolds numbers and moderate Mach number. There is no information relating to symmetry or cross flow in the tunnel wall boundary layers - all profiles except 0101 are taken in an asymmetric configuration - and whether from this cause or another, the profile characteristics do not match typical zero-pressure-gradient data in the outer region. In the inner region, transformed wall law plots show that the balance readings vary by at least ± 15 % from the mean. The balance is very small for an experiment on this scale, and correspondingly very difficult to use (d = 0.3 mm; cf. CAT 6601, d = 50.8 mm; CAT 7302, d = 368.3 mm).

Experiments comparable in range are Jackson et al. - CAT 6505, Hopkins & Keener - CAT 6601 and Winter & Gaudet - CAT 7302. Mabey et al. - CAT 7402 provide flat plate data for comparison and contrast.

Note added in proof. The author has recently obtained fresh CF data using two more Kistler balances, giving values about 10% higher.
See also J.M. Allen (1976) NASA TN4D-8291) for tests with a much larger balance.

CAT 7303

ALLEN

BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.

RUN X RZ	MD * POD* TOD*	TW/TR* PW/PD* SW * DZ	RED2W RED2D DZ	CF * CQ PI2*	H12 H32 H42	H12K H32K D2K	PW TW UD	PD TD TR
73030101 NM INFINITE	1.9830 6.9914 ⁺⁰⁴ 3.1400 ⁺⁰²	1.0000 1.0000 0.0000	2.6469 ⁺⁰⁴ 4.0975 ⁺⁰⁴ 5.1107 ⁻⁰³	1.7600 ⁻⁰³ NM 0.0000 ⁺⁰⁰	2.8385 1.8212 0.0834	1.2734 1.8110 6.2415 ⁻⁰³	9.1747 ⁺⁰³ 2.9962 ⁺⁰² 5.2711 ⁺⁰²	9.1747 ⁺⁰³ 1.7577 ⁺⁰² 2.9962 ⁺⁰²
73030201 NM INFINITE	2.3250 2.2292 ⁺⁰⁴ 3.3900 ⁺⁰²	1.0000 1.0000 0.0000	9.0391 ⁺⁰³ 1.5754 ⁺⁰⁴ 8.0781 ⁻⁰³	1.8240 ⁻⁰³ NM 0.0000 ⁺⁰⁰	3.3693 1.8305 0.0992	1.2412 1.8246 1.0351 ⁻⁰²	1.7143 ⁺⁰³ 3.2068 ⁺⁰² 5.9495 ⁺⁰²	1.7143 ⁺⁰³ 1.6289 ⁺⁰² 3.2068 ⁺⁰²
73030202 NM INFINITE	2.3190 3.6477 ⁺⁰⁴ 3.3900 ⁺⁰²	1.0000 1.0000 0.0000	1.4131 ⁺⁰⁴ 2.4574 ⁺⁰⁴ 7.6766 ⁻⁰³	1.7600 ⁻⁰³ NM 0.0000 ⁺⁰⁰	3.3437 1.8409 0.0992	1.2329 1.8295 9.7729 ⁻⁰³	2.8317 ⁺⁰³ 3.2073 ⁺⁰² 5.9422 ⁺⁰²	2.8317 ⁺⁰³ 1.6333 ⁺⁰² 3.2073 ⁺⁰²
73030203 NM INFINITE	2.3180 7.2954 ⁺⁰⁴ 3.3900 ⁺⁰²	1.0000 1.0000 0.0000	2.6212 ⁺⁰⁴ 4.5564 ⁺⁰⁴ 7.1132 ⁻⁰³	1.6260 ⁻⁰³ NM 0.0000 ⁺⁰⁰	3.3207 1.8473 0.0995	1.2205 1.8367 8.9874 ⁻⁰³	5.6723 ⁺⁰³ 3.2074 ⁺⁰² 5.9409 ⁺⁰²	5.6723 ⁺⁰³ 1.6340 ⁺⁰² 3.2074 ⁺⁰²
73030204 NM INFINITE	2.3170 1.1044 ⁺⁰⁵ 3.3900 ⁺⁰²	1.0000 1.0000 0.0000	3.8282 ⁺⁰⁴ 6.6450 ⁺⁰⁴ 6.8489 ⁻⁰³	1.5360 ⁻⁰³ NM 0.0000 ⁺⁰⁰	3.2998 1.8535 0.0998	1.2099 1.8434 8.5858 ⁻⁰³	6.6007 ⁺⁰³ 3.2075 ⁺⁰² 5.9397 ⁺⁰²	6.6007 ⁺⁰³ 1.6348 ⁺⁰² 3.2075 ⁺⁰²
73030205 NM INFINITE	2.3210 1.4692 ⁺⁰⁵ 3.3900 ⁺⁰²	1.0000 1.0000 0.0000	4.8315 ⁺⁰⁴ 8.4080 ⁺⁰⁴ 6.5279 ⁻⁰³	1.4690 ⁻⁰³ NM 0.0000 ⁺⁰⁰	3.3001 1.8556 0.1001	1.2058 1.8456 8.1680 ⁻⁰³	1.1370 ⁺⁰⁴ 3.2072 ⁺⁰² 5.9446 ⁺⁰²	1.1370 ⁺⁰⁴ 1.6318 ⁺⁰² 3.2072 ⁺⁰²
73030301 NM INFINITE	4.6220 7.4981 ⁺⁰⁴ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	2.6742 ⁺⁰³ 1.0927 ⁺⁰⁴ 5.9457 ⁻⁰³	1.0290 ⁻⁰³ NM 0.0000 ⁺⁰⁰	9.5638 1.8586 0.1566	1.2453 1.8267 1.1691 ⁻⁰²	2.2278 ⁺⁰² 3.2234 ⁺⁰² 7.5718 ⁺⁰²	2.2278 ⁺⁰² 6.6761 ⁺⁰¹ 3.2234 ⁺⁰²
73030302 NM INFINITE	4.6000 1.2463 ⁺⁰⁵ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	4.2603 ⁺⁰³ 1.7276 ⁺⁰⁴ 5.5954 ⁻⁰³	9.8900 ⁻⁰⁴ NM 0.0000 ⁺⁰⁰	9.4688 1.8611 0.1566	1.2427 1.8288 1.0859 ⁻⁰²	3.8044 ⁺⁰² 3.2239 ⁺⁰² 7.5649 ⁺⁰²	3.8044 ⁺⁰² 6.7278 ⁺⁰¹ 3.2239 ⁺⁰²
73030303 NM INFINITE	4.6120 2.4926 ⁺⁰⁵ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	7.8086 ⁺⁰³ 3.1796 ⁺⁰⁴ 5.1793 ⁻⁰³	5.0400 ⁻⁰⁴ NM 0.0000 ⁺⁰⁰	9.4461 1.8687 0.1574	1.2225 1.8389 9.8431 ⁻⁰³	7.4973 ⁺⁰² 3.2236 ⁺⁰² 7.5687 ⁺⁰²	7.4973 ⁺⁰² 6.6995 ⁺⁰¹ 3.2236 ⁺⁰²
73030304 NM INFINITE	4.6190 3.7389 ⁺⁰⁵ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	1.1106 ⁺⁰⁴ 4.5332 ⁺⁰⁴ 4.9396 ⁻⁰³	8.8300 ⁻⁰⁴ NM 0.0000 ⁺⁰⁰	9.4259 1.8741 0.1579	1.2087 1.8464 9.2386 ⁻⁰³	1.1150 ⁺⁰³ 3.2234 ⁺⁰² 7.5709 ⁺⁰²	1.1150 ⁺⁰³ 6.6831 ⁺⁰¹ 3.2234 ⁺⁰²
73030305 NM INFINITE	4.6220 4.9852 ⁺⁰⁵ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	1.4243 ⁺⁰⁴ 5.8198 ⁺⁰⁴ 4.7630 ⁻⁰³	8.6100 ⁻⁰⁴ NM 0.0000 ⁺⁰⁰	9.4120 1.8771 0.1582	1.2007 1.8508 8.8313 ⁻⁰³	1.4812 ⁺⁰³ 3.2234 ⁺⁰² 7.5718 ⁺⁰²	1.4812 ⁺⁰³ 6.6761 ⁺⁰¹ 3.2234 ⁺⁰²
73030306 NM INFINITE	4.6400 6.2315 ⁺⁰⁵ 3.5200 ⁺⁰²	1.0000 1.0000 0.0000	1.6996 ⁺⁰⁴ 6.9877 ⁺⁰⁴ 4.6151 ⁻⁰³	8.4000 ⁻⁰⁴ NM 0.0000 ⁺⁰⁰	9.4507 1.8803 0.1587	1.1932 1.8553 8.4950 ⁻⁰³	1.8110 ⁺⁰³ 3.2229 ⁺⁰² 7.5774 ⁺⁰²	1.8110 ⁺⁰³ 6.6341 ⁺⁰¹ 3.2229 ⁺⁰²

73030201		ALLEN		PROFILE TABULATION		27 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94597	0.00000	0.00000	1.96869	0.00000	
2	1.8000*-04	1.7976*+00	NM	0.96140	0.41075	0.53432	1.69213	0.31576	
3	6.4000*-04	1.7895*+00	NM	0.96129	0.40903	0.53239	1.69412	0.31426	
4	1.1900*-03	2.0645*+00	NM	0.96475	0.46151	0.58957	1.63190	0.36126	
5	5.0800*-03	2.7784*+00	NM	0.97215	0.56774	0.69540	1.50025	0.46352	
6	8.8900*-03	3.1448*+00	NM	0.97533	0.61376	0.73712	1.44236	0.51105	
7	1.2700*-02	3.4322*+00	NM	0.97767	0.64731	0.76600	1.40031	0.54702	
8	1.6510*-02	3.6806*+00	NM	0.97998	0.67484	0.78874	1.36606	0.57739	
9	2.0320*-02	3.8784*+00	NM	0.98104	0.69591	0.80559	1.34003	0.60117	
10	2.4130*-02	4.0404*+00	NM	0.98218	0.71269	0.81865	1.31948	0.62044	
11	3.3020*-02	4.4746*+00	NM	0.98508	0.75570	0.85079	1.26751	0.67123	
12	4.0640*-02	4.7991*+00	NM	0.98710	0.78624	0.87245	1.23134	0.70854	
13	4.8260*-02	5.0885*+00	NM	0.98880	0.81247	0.89033	1.20083	0.74143	
14	5.5880*-02	5.4629*+00	NM	0.99088	0.84516	0.91167	1.16357	0.78351	
15	6.3500*-02	5.7433*+00	NM	0.99235	0.86882	0.92649	1.13718	0.81473	
16	7.1120*-02	6.1010*+00	NM	0.99413	0.89806	0.94413	1.10522	0.85425	
17	7.8740*-02	6.3389*+00	NM	0.99526	0.91699	0.95515	1.08495	0.88036	
18	8.6360*-02	6.6434*+00	NM	0.99665	0.94065	0.96849	1.06008	0.91360	
19	9.3980*-02	6.8526*+00	NM	0.99757	0.95656	0.97721	1.04365	0.93634	
20	1.0160*-01	7.0481*+00	NM	0.99840	0.97118	0.98505	1.02875	0.95751	
21	1.0922*-01	7.1546*+00	NM	0.99886	0.97935	0.98935	1.02052	0.96995	
22	1.1684*-01	7.2465*+00	NM	0.99922	0.98581	0.99271	1.01406	0.97894	
23	1.2446*-01	7.3647*+00	NM	0.99969	0.99441	0.99715	1.00552	0.99168	
24	1.3208*-01	7.3825*+00	NM	0.99976	0.99570	0.99781	1.00424	0.99359	
D 25	1.3970*-01	7.4420*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.4732*-01	7.4420*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
27	1.5240*-01	7.4420*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

73030205		ALLEN		PROFILE TABULATION		26 POINTS, DELTA AT POINT 25			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.94606	0.00000	0.00000	1.96536	0.00000	
2	1.8000*-04	2.1149*+00	NM	0.96543	0.47092	0.59916	1.61880	0.37012	
3	6.4000*-04	2.1693*+00	NM	0.96604	0.47997	0.60859	1.60780	0.37852	
4	1.1900*-03	2.4192*+00	NM	0.96871	0.51874	0.64793	1.56009	0.41531	
5	5.0800*-03	3.2241*+00	NM	0.97608	0.62430	0.74605	1.42805	0.52242	
6	8.8900*-03	3.6214*+00	NM	0.97923	0.66954	0.78417	1.37174	0.57166	
7	1.2700*-02	3.8416*+00	NM	0.98086	0.69324	0.80323	1.34252	0.59830	
8	1.6510*-02	4.0531*+00	NM	0.98236	0.71521	0.82036	1.31567	0.62353	
9	2.0320*-02	4.2585*+00	NM	0.98376	0.73589	0.83602	1.29064	0.64775	
10	2.4130*-02	4.4836*+00	NM	0.98523	0.75786	0.85216	1.26434	0.67400	
11	3.3020*-02	4.9402*+00	NM	0.98803	0.80052	0.88210	1.21421	0.72640	
12	4.0640*-02	5.3084*+00	NM	0.99013	0.83326	0.90388	1.17667	0.76816	
13	4.8260*-02	5.6047*+00	NM	0.99172	0.85868	0.92008	1.14813	0.80138	
14	5.5880*-02	5.9206*+00	NM	0.99334	0.88496	0.93622	1.11921	0.83651	
15	6.3500*-02	6.2789*+00	NM	0.99508	0.91383	0.95325	1.08814	0.87604	
16	7.1120*-02	6.5651*+00	NM	0.99619	0.93623	0.96598	1.06456	0.90740	
17	7.8740*-02	6.8014*+00	NM	0.99744	0.95433	0.97590	1.04585	0.93318	
18	8.6360*-02	6.9615*+00	NM	0.99813	0.96639	0.98247	1.03355	0.95058	
19	9.3980*-02	7.1178*+00	NM	0.99878	0.97803	0.98864	1.02181	0.96753	
20	1.0160*-01	7.2465*+00	NM	0.99931	0.98751	0.99350	1.01235	0.98146	
21	1.0922*-01	7.3173*+00	NM	0.99960	0.99268	0.99625	1.00722	0.98911	
22	1.1684*-01	7.3351*+00	NM	0.99967	0.99397	0.99692	1.00594	0.99103	
23	1.2446*-01	7.3944*+00	NM	0.99991	0.99828	0.99912	1.00169	0.99743	
24	1.3208*-01	7.4122*+00	NM	0.99998	0.99957	0.99978	1.00042	0.99936	
D 25	1.3970*-01	7.4182*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
26	1.4732*-01	7.4182*+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

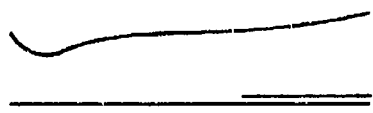
INPUT VARIABLES Y,M ASSUME P=PD AND VAN DRIEST

73030301		ALLEN		PROFILE TABULATION		28 POINTS, DELTA AT POINT 27			
I	Y	P12/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.91572	0.00000	0.00000	4.42823	0.00000	
2	1.8000*-04	2.1719*+00	NM	0.93509	0.24124	0.47936	3.94855	0.12140	
3	6.4000*-04	2.1746*+00	NM	0.93512	0.24145	0.47971	3.94726	0.12153	
4	1.1900*-03	2.3700*+00	NM	0.93715	0.25682	0.50423	3.85491	0.13080	
5	5.0800*-03	4.8505*+00	NM	0.95583	0.39788	0.68987	3.00629	0.22948	
6	8.8900*-03	5.7900*+00	NM	0.96085	0.43899	0.73174	2.77846	0.26336	
7	1.2700*-02	6.4542*+00	NM	0.96395	0.46582	0.75649	2.63742	0.28683	
8	1.6510*-02	7.1236*+00	NM	0.96678	0.49135	0.77851	2.50920	0.31018	
9	2.0320*-02	7.7498*+00	NM	0.96918	0.51406	0.79641	2.40013	0.33162	
10	2.4130*-02	8.3728*+00	NM	0.97137	0.53570	0.81255	2.30069	0.35318	
11	3.3020*-02	9.8277*+00	NM	0.97583	0.58308	0.84453	2.09783	0.40257	
12	4.0640*-02	1.1117*+01	NM	0.97918	0.62203	0.86770	1.94592	0.44591	
13	4.8260*-02	1.2380*+01	NM	0.98201	0.65794	0.88689	1.81705	0.48809	
14	5.5880*-02	1.3590*+01	NM	0.98440	0.69061	0.90272	1.70860	0.52834	
15	6.3500*-02	1.4885*+01	NM	0.98666	0.72393	0.91744	1.60605	0.57124	
16	7.1120*-02	1.6027*+01	NM	0.98843	0.75206	0.92885	1.52541	0.60891	
17	7.8740*-02	1.7276*+01	NM	0.99018	0.78170	0.93996	1.44591	0.65008	
18	8.6360*-02	1.8459*+01	NM	0.99168	0.80874	0.94935	1.37796	0.68896	
19	9.3980*-02	1.9553*+01	NM	0.99294	0.83297	0.95722	1.32056	0.72486	
20	1.0160*-01	2.0883*+01	NM	0.99435	0.86153	0.96587	1.25688	0.76847	
21	1.0922*-01	2.2058*+01	NM	0.99548	0.88598	0.97278	1.20555	0.80692	
22	1.1684*-01	2.3039*+01	NM	0.99635	0.90588	0.97811	1.16580	0.83900	
23	1.2446*-01	2.4006*+01	NM	0.99763	0.93682	0.98587	1.10744	0.89022	
24	1.3208*-01	2.5586*+01	NM	0.99837	0.95565	0.99031	1.07385	0.92220	
25	1.3970*-01	2.6492*+01	NM	0.99902	0.97274	0.99417	1.04454	0.95177	
26	1.4732*-01	2.7309*+01	NM	0.99957	0.98788	0.99745	1.01947	0.97841	
D 27	1.5494*-01	2.7971*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
28	1.5621*-01	2.7983*+01	NM	1.00001	1.00022	1.00004	0.99966	1.00039	

INPUT VARIABLES Y,H ASSUME P=PU AND VAN DRIEST

73030306		ALLEN		PROFILE TABULATION		28 POINTS, DELTA AT POINT 27			
I	Y	P12/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.91560	0.00000	0.00000	4.85810	0.00000	
2	1.8000*-04	3.2168*+00	NM	0.94460	0.31185	0.58614	3.53263	0.16592	
3	6.4000*-04	3.4436*+00	NM	0.94837	0.32500	0.60380	3.45155	0.17493	
4	1.1900*-03	4.0404*+00	NM	0.95065	0.35711	0.64439	3.25606	0.19791	
5	5.0800*-03	6.1654*+00	NM	0.96251	0.45259	0.74555	2.71361	0.27474	
6	8.8900*-03	7.2819*+00	NM	0.96727	0.49526	0.78245	2.49603	0.31348	
7	1.2700*-02	8.2777*+00	NM	0.97091	0.53039	0.80954	2.32966	0.34749	
8	1.6510*-02	9.2751*+00	NM	0.97410	0.56336	0.83254	2.18394	0.38121	
9	2.0320*-02	1.0079*+01	NM	0.97639	0.58858	0.84869	2.07919	0.40818	
10	2.4130*-02	1.0874*+01	NM	0.97845	0.61250	0.86245	1.98501	0.43473	
11	3.3020*-02	1.2576*+01	NM	0.98229	0.66078	0.88890	1.80966	0.49120	
12	4.0640*-02	1.3946*+01	NM	0.98492	0.69720	0.90624	1.68956	0.53638	
13	4.8260*-02	1.5323*+01	NM	0.98723	0.73211	0.92128	1.58353	0.58179	
14	5.5880*-02	1.6833*+01	NM	0.98945	0.76832	0.93541	1.48226	0.63107	
15	6.3500*-02	1.8124*+01	NM	0.99114	0.79806	0.94603	1.40520	0.67323	
16	7.1120*-02	1.9543*+01	NM	0.99280	0.82953	0.95638	1.32423	0.71950	
17	7.8740*-02	2.0771*+01	NM	0.99410	0.85582	0.96440	1.26983	0.75947	
18	8.6360*-02	2.1974*+01	NM	0.99526	0.88082	0.97153	1.21657	0.79858	
19	9.3980*-02	2.3461*+01	NM	0.99657	0.91078	0.97950	1.15660	0.84688	
20	1.0160*-01	2.4684*+01	NM	0.99756	0.93470	0.98544	1.11152	0.88657	
21	1.0922*-01	2.5734*+01	NM	0.99835	0.95474	0.99016	1.07557	0.92059	
22	1.1684*-01	2.6794*+01	NM	0.99909	0.97457	0.99460	1.04154	0.95494	
23	1.2446*-01	2.7462*+01	NM	0.99954	0.98685	0.99725	1.02118	0.97656	
24	1.3208*-01	2.7900*+01	NM	0.99982	0.99483	0.99893	1.00826	0.99074	
25	1.3970*-01	2.8055*+01	NM	0.99992	0.99763	0.99951	1.00378	0.99575	
26	1.4732*-01	2.8150*+01	NM	0.99998	0.99935	0.99987	1.00103	0.99884	
D 27	1.5494*-01	2.8186*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
28	1.5621*-01	2.8186*+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,H ASSUME P=PD AND VAN DRIEST

	M : 3.8 rising to 4.5 R THETA X 10 ⁻³ : 6 - 50 TW/TR : 1.0, 0.8, 0.25	7304
		FPG AW-MHT-SHT
Boundary layer channel. Effectively continuous. W = 0.33 H = 0.272 m. 0.1 < PO < 1.1 MN/m ² . TO : 336, 423 K. Air, dew point 215-233 K. 2 < RE/m X 10 ⁻⁶ < 40.		
VOISINET R.L.P. and LEE R.E., 1973. Measurements of a supersonic favourable pressure-gradient turbulent boundary layer with heat transfer - Part I, Data compilation. NOLTR 73-224. And Voisinet and Lee (1972) CAT 7202 with associated references, Brott et al. (1969)		

- 1- The tests were performed in the purpose-built channel used for CAI 7202 and described in that entry.
- 11 The flexible wall was set to give a monotonically accelerating flow, the coordinates being given in table 1, and the resulting pressure history in table 2. The plate surface temperature history is given in table 3. (Tables 2 and 3 are facsimiles of the authors' tables 2&3.) The instrumentation employed was also as for CAT 7202.
- 8 The relative positions of profiles and wall measurements at any one station were again as for CAT 7202, but profiles and wall measurements were made at an additional upstream station (X = 1.194 m for profiles, 1.270 m for wall measurements). The positions at which differing measurements were made are given in table 4. The heat transfer measurements in the AW condition were made to ensure that the wall temperature had been adjusted to a practical zero heat transfer condition, taking into account the effect of nozzle region heat transfer.
- 12 The editors have accepted the interpolations and corrections made by the authors. In several cases, differing repeated data for a single Y-value have been averaged. The edge state has been calculated from the static pressure and temperature data with the Mach number as presented. The authors interpolated the CF data to agree with the boundary conditions or the measured profiles, and these are the values given here. The editors have interpolated the CQ data in their original form, as Stanton numbers, to match the profiles on the basis of the authors' R THETA values alone. No heat transfer data are presented for the SHT condition, as the only measurements were at a station not associated with a profile.
- 13 The profiles presented and their associated instrumentation are listed in table 5. CF data is given for 14 all while CQ is not given for the SHT case since it was not effectively measured.
- 5 DATA: 7304 0101-1503. Pitot and TO profiles measured simultaneously. NX up to 5. CF from FEB, CQ from thermopiles measured separately.
- 15 Editors' comments
The remarks made in the first three paragraphs of § 15 CAT 7202 apply equally here, except that in this case the measurements were all made in a fully reflected-wave flow-region. Static pressure variation along a normal is therefore found to be small. There are no properly comparable experiments, but similar pressure histories were studied by Michel (CAT 6902) and Thomas (CAT 7401) at lower Mach numbers and without heat-transfer.

Many of the profiles display characteristics which could be interpreted as transitional characteristics were it not for the high Reynolds numbers.

TABLE 1 NOZZLE CONTOUR COORDINATES

<u>x (meters)</u>	<u>y (meters)</u>	<u>x (meters)</u>	<u>y (meters)</u>	<u>x (meters)</u>	<u>y (meters)</u>
0.0000	0.01016	0.9144	0.08534	1.8034	0.18263
0.2794	0.02128	1.0668	0.10312	1.9812	0.19939
0.3810	0.02784	1.2446	0.12319	2.1591	0.21768
0.5588	0.04597	1.4224	0.14275	2.3368	0.23952
0.7366	0.06591	1.6002	0.16154		

Facsimile from source paper

TABLE 2
AVERAGE NOZZLE WALL-PRESSURE AND PRESSURE-GRADIENT DISTRIBUTIONS

x (meters)	P_{sw}/P_o	$\frac{1}{P_o} \frac{dP_{sw}}{dx}$ (meters)
1.016	.9895E-02	-.1649E-01
1.041	.9488E-02	-.1557E-01
1.067	.9103E-02	-.1470E-01
1.092	.8740E-02	-.1387E-01
1.118	.8398E-02	-.1308E-01
1.143	.8076E-02	-.1233E-01
1.168	.7772E-02	-.1162E-01
1.194	.7485E-02	-.1095E-01
1.219	.7215E-02	-.1031E-01
1.245	.6961E-02	-.9709E-02
1.270	.6722E-02	-.9142E-02
1.295	.6496E-02	-.8607E-02
1.321	.6284E-02	-.8104E-02
1.346	.6084E-02	-.7632E-02
1.372	.5896E-02	-.7188E-02
1.397	.5719E-02	-.6773E-02
1.422	.5552E-02	-.6385E-02
1.448	.5394E-02	-.6022E-02
1.473	.5246E-02	-.5683E-02
1.499	.5106E-02	-.5368E-02
1.524	.4973E-02	-.5075E-02
1.549	.4848E-02	-.4803E-02
1.575	.4729E-02	-.4550E-02
1.600	.4616E-02	-.4316E-02
1.626	.4509E-02	-.4099E-02
1.651	.4408E-02	-.3898E-02
1.676	.4311E-02	-.3712E-02
1.702	.4219E-02	-.3539E-02
1.727	.4131E-02	-.3379E-02
1.753	.4048E-02	-.3231E-02
1.778	.3967E-02	-.3092E-02
1.803	.3890E-02	-.2963E-02
1.829	.3817E-02	-.2841E-02
1.854	.3746E-02	-.2725E-02
1.880	.3678E-02	-.2615E-02
1.905	.3613E-02	-.2509E-02
1.930	.3551E-02	-.2406E-02
1.956	.3491E-02	-.2305E-02
1.981	.3434E-02	-.2204E-02
2.007	.3379E-02	-.2103E-02
2.032	.3327E-02	-.1999E-02
2.057	.3277E-02	-.1893E-02
2.083	.3231E-02	-.1783E-02
2.108	.3187E-02	-.1667E-02
2.134	.3146E-02	-.1544E-02
2.159	.3108E-02	-.1413E-02
2.184	.3074E-02	-.1274E-02
2.210	.3044E-02	-.1124E-02
2.235	.3017E-02	-.9630E-03
2.261	.2995E-02	-.7893E-03
2.286	.2977E-02	-.6018E-03

Facsimile from source paper

TABLE 3
NOZZLE WALL-TEMPERATURE DISTRIBUTION

Flow	Code	P ₀ atm	T ₀ °K	x (meters)													
				0.000	0.279	0.457	0.711	0.864	1.067	1.194	1.448	1.702	1.905	2.057	2.210		
EPG-AW	TD14	10	336.	323.	311.	305.	295.	294.	294.	294.	294.	294.	294.	294.	294.	294.	294.
	TD15	5	336.	321.	310.	303.	292.	291.	291.	291.	291.	291.	291.	291.	291.	291.	291.
	TD16	1	336.	314.	306.	300.	292.	291.	291.	291.	251.	291.	291.	291.	291.	291.	291.
EPG-NHT	TD17	10	423.	355.	352.	342.	304.	300.	300.	302.	299.	299.	298.	298.	298.	298.	298.
	TD18	5	423.	341.	341.	332.	298.	296.	296.	296.	295.	295.	295.	295.	295.	295.	295.
	TD19	1	423.	301.	306.	305.	293.	293.	293.	293.	293.	293.	293.	293.	293.	293.	293.
EPG-CW	TD20	10	423.	359.	357.	351.	300.	291.	291.	202.	160.	119.	99.	116.	117.	118.	118.
	TD21	5	423.	348.	346.	334.	267.	202.	125.	103.	97.	98.	100.	97.	101.	101.	101.
	TD22	1	423.	308.	303.	288.	193.	144.	94.	89.	88.	88.	88.	89.	87.	87.	88.

7304
SERIES03
02, 05

01, 04

08

07, 10

06, 09

13

12, 15

11, 14

TABLE 4
LOCATION OF MEASUREMENTS

X-Station: m	Wall condition		
	AW	MHT	SHT
1.194 (P)	P	P	
1.270 (W)	K K K	K Q	N Q
1.448 (P)	P	P	P
1.524 (W)	K K K, Q	K K, Q	
1.702 (P)	P	P	P
1.778 (W)	K Q	K Q	N
1.905 (P)	P	P	P
1.981 (W)	K K, Q	K Q	N
2.057 (P)	P	P	P
2.134 (W)	K Q	K Q	N
2.286 (W)	Q		

KEY: P - profile, W - wall measurement, K - CF using Kistler FEB,
N - CF using NOL FEB, Q - CQ using thermopile.

TABLE 5
PROFILE SERIES PRESENTED

CODE 7304	HT	NX	TTP	FEB	POD ₂ MN/m ²	TOD K	TW K
0101-5	AW	5	ECP	Kistler	0.1	336	291
0201-5	AW	5	ECP	Kistler	0.5	336	291
0301-5	AW	5	ECP	Kistler	1.0	336	294
0401-5	AW	5	FWP	Kistler	0.1	336	291
0501-5	AW	5	FWP	Kistler	0.5	336	291
0601-4	MHT	4	ECP	Kistler	0.1	423	293
0701-4	MHT	4	ECP	Kistler	0.5	423	295
0801-4	MHT	4	ECP	Kistler	1.0	423	299
0901-5	MHT	5	FWP	Kistler	0.1	423	293
1001-5	MHT	3	FWP	Kistler	0.5	423	295
1101-2	SHT	2	ECP	NOL	0.1	423	90
1201-4	SHT	4	ECP	NOL	0.5	423	100
1301-4	SHT	4	ECP	NOL	1.0	423	120
1401-3	SHT	3	FWP	NOL	0.1	423	90
1501-3	SHT	3	FWP	NOL	0.5	423	100

(Nominal values)

CAT 7304		VOISINETY		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN	MD *	TN/TR	FED2%	CF *	H12	H12K	PH*	PD*			
X *	POD	PW/PD	REL2D	CG *	H32	H32K	1M*	TD*			
RZ	TOD	SW *	DZ	PI2*	H42	D2K	UD	TR			
73040101	3.8501	0.9371	2.2846*+03	1.2400*-03	6.1913	1.3554	8.4160*+02	8.3379*+02			
1.4480*+00	1.0346*+05	1.0130	6.7783*+03	0.0000*+00	1.8277	1.7916	2.9480*+02	6.6043*+01			
INFINITE	3.4113*+02	0.0000	1.7274*-03	-1.7879*-01	0.3328	2.9001*-03	7.1634*+02	3.1466*+02			
73040102	4.0862	0.9460	2.1197*+03	1.2200*-03	7.5115	1.3831	5.9880*+02	5.4958*+02			
1.4480*+00	1.0206*+05	0.9987	6.4228*+03	0.0000*+00	1.8248	1.7876	2.9470*+02	7.8031*+01			
INFINITE	3.3861*+02	0.0000	1.9993*-03	-1.4544*-01	0.2575	3.6425*-03	7.2371*+02	3.1151*+02			
73040103	4.2954	0.9415	2.0112*+03	1.1100*-03	7.9558	1.3720	4.6730*+02	4.6305*+02			
1.7020*+00	1.0346*+05	1.0092	7.0463*+03	0.0000*+00	1.8269	1.7880	2.9440*+02	7.2739*+01			
INFINITE	3.4115*+02	0.0000	2.2572*-03	-1.2041*-01	0.2664	4.2474*-03	7.3451*+02	3.1324*+02			
73040104	4.3873	0.9502	2.0073*+03	1.0600*-03	8.6077	1.3863	4.0160*+02	4.0614*+02			
1.9050*+00	1.0202*+05	0.9880	7.3275*+03	0.0000*+00	1.8265	1.7857	2.9580*+02	6.9969*+01			
INFINITE	3.3933*+02	0.0000	2.4721*-03	-1.1636*-01	0.2648	4.8512*-03	7.3580*+02	3.1131*+02			
73040105	4.4796	0.9521	1.9997*+03	1.0400*-03	8.4224	1.4029	3.6750*+02	3.5589*+02			
2.0570*+00	1.0041*+05	1.0326	7.9585*+03	0.0000*+00	1.8206	1.7793	2.9530*+02	6.7485*+01			
INFINITE	3.3833*+02	0.0000	2.6998*-03	-9.4350*-02	0.2513	5.3114*-03	7.3782*+02	3.1016*+02			
73040201	3.8838	0.9299	8.0606*+03	8.6200*-04	6.5726	1.2899	3.9510*+03	3.9297*+03			
1.4480*+00	5.1042*+05	1.0054	2.4138*+04	0.0000*+00	1.8412	1.8113	2.8860*+02	8.3814*+01			
INFINITE	3.3666*+02	0.0000	1.2445*-03	-1.9444*-01	0.2643	2.0817*-03	7.1289*+02	3.1036*+02			
73040202	4.1149	0.9495	7.3158*+03	8.3800*-04	7.9016	1.3052	2.7810*+03	2.8502*+03			
1.4480*+00	5.0384*+05	0.9757	2.9229*+04	0.0000*+00	1.8418	1.8080	2.9440*+02	7.6855*+01			
INFINITE	3.3712*+02	0.0000	1.4880*-03	-1.6486*-01	0.2342	2.6939*-03	7.2328*+02	3.1005*+02			
73040203	4.3125	0.9423	7.3908*+03	8.1000*-04	8.1481	1.3038	2.2170*+03	2.2064*+03			
1.7020*+00	5.0387*+05	1.0048	2.6155*+04	0.0000*+00	1.8395	1.8054	2.9080*+02	7.1231*+01			
INFINITE	3.3618*+02	0.0000	1.6973*-03	-1.3123*-01	0.2205	3.1439*-03	7.2975*+02	3.0862*+02			
73040204	4.4378	0.9454	7.3047*+03	7.7900*-04	8.9909	1.3051	1.8640*+03	1.9074*+03			
1.9050*+00	5.1066*+05	0.9772	2.7045*+04	0.0000*+00	1.8423	1.8059	2.9400*+02	6.8661*+01			
INFINITE	3.3910*+02	0.0000	1.8671*-03	-1.2003*-01	0.2304	3.6173*-03	7.3728*+02	3.1098*+02			
73040205	4.5237	0.9512	7.2875*+03	7.7200*-04	8.7977	1.3190	1.7130*+03	1.7008*+03			
2.0570*+00	5.0699*+05	1.0072	2.7957*+04	0.0000*+00	1.8383	1.8009	2.9490*+02	6.7485*+01			
INFINITE	3.3829*+02	0.0000	2.0204*-03	-1.0396*-01	0.2339	3.9276*-03	7.3921*+02	3.1001*+02			
73040301	3.9022	0.9426	1.4099*+04	6.6500*-04	6.4477	1.2606	7.7550*+03	7.6177*+03			
1.4480*+00	1.0144*+06	1.0180	4.2980*+04	0.0000*+00	1.8526	1.8253	2.9190*+02	8.3049*+01			
INFINITE	3.3597*+02	0.0000	1.1224*-03	-2.2854*-01	0.2454	1.8245*-03	7.1299*+02	3.0966*+02			
73040302	4.0996	0.9434	1.3838*+04	6.8500*-04	7.7956	1.2671	5.6200*+03	5.7526*+03			
1.4480*+00	9.9664*+05	0.9769	4.5374*+04	0.0000*+00	1.8522	1.8219	2.9210*+02	7.7178*+01			
INFINITE	3.3660*+02	0.0000	1.3392*-03	-1.3267*-01	0.2277	2.3613*-03	7.2211*+02	3.0962*+02			
73040303	4.3062	0.9455	1.3416*+04	6.7900*-04	7.9648	1.2709	4.4570*+03	4.4120*+03			
1.7020*+00	9.9949*+05	1.0102	4.7481*+04	0.0000*+00	1.8507	1.8193	2.9230*+02	7.1511*+01			
INFINITE	3.3672*+02	0.0000	1.5522*-03	-1.3383*-01	0.2156	2.7886*-03	7.3011*+02	3.0914*+02			
73040304	4.4370	0.9458	1.3046*+04	6.6900*-04	9.0537	1.2683	3.6950*+03	3.8077*+03			
1.9050*+00	1.0184*+06	0.9704	4.8284*+04	0.0000*+00	1.8549	1.8211	2.9460*+02	6.8795*+01			
INFINITE	3.3967*+02	0.0000	1.6750*-03	-1.2634*-01	0.2213	3.1682*-03	7.3787*+02	3.1150*+02			
73040305	4.5339	0.9460	1.2895*+04	6.5800*-04	9.0376	1.2791	3.3610*+03	3.3731*+03			
2.0570*+00	1.0183*+06	0.9964	4.9413*+04	0.0000*+00	1.8509	1.8165	2.9370*+02	6.6289*+01			
INFINITE	3.3882*+02	0.0000	1.7911*-03	-1.0922*-01	0.2101	3.4234*-03	7.4012*+02	3.1048*+02			
73040401	3.8630	0.9287	2.0201*+03	1.2400*-03	6.8128	1.3784	8.0850*+02	7.9742*+02			
1.4480*+00	1.0070*+05	1.0139	5.9870*+03	0.0000*+00	1.0224	1.7884	2.9060*+02	8.5165*+01			
INFINITE	3.3934*+02	0.0000	1.5660*-03	-1.6715*-01	0.2158	2.7072*-03	7.1477*+02	3.1291*+02			
73040402	4.0987	0.9259	1.9422*+03	1.2200*-03	7.6004	1.3822	5.5930*+02	5.6075*+02			
1.4480*+00	9.7035*+04	0.9974	6.2663*+03	0.0000*+00	1.8242	1.7881	2.8840*+02	7.7669*+01			
INFINITE	3.3863*+02	0.0000	1.9158*-03	-1.3908*-01	0.2488	3.5000*-03	7.2423*+02	3.1149*+02			
73040403	4.2888	0.9250	1.9938*+03	1.1100*-03	7.8228	1.3867	4.5480*+02	4.4934*+02			
1.7020*+00	9.9549*+04	1.0121	6.8801*+03	0.0000*+00	1.8250	1.7862	2.8860*+02	7.2626*+01			
INFINITE	3.3980*+02	0.0000	2.2693*-03	-1.2362*-01	0.2862	4.2409*-03	7.3281*+02	3.1201*+02			
73040404	4.4001	0.9327	2.0052*+03	1.0600*-03	8.5580	1.3957	3.9350*+02	3.9803*+02			
1.9050*+00	1.0161*+05	0.9886	7.2514*+03	0.0000*+00	1.8259	1.7848	2.8980*+02	6.9518*+01			
INFINITE	3.3870*+02	0.0000	2.4651*-03	-1.0920*-01	0.2855	4.8225*-03	7.3557*+02	3.1071*+02			
73040405	4.4756	0.9251	1.9749*+03	1.0400*-03	8.3438	1.3972	3.5820*+02	3.4907*+02			
2.0570*+00	9.7991*+04	1.0262	7.2908*+03	0.0000*+00	1.8195	1.7795	2.8680*+02	6.7549*+01			
INFINITE	3.3816*+02	0.0000	2.6612*-03	-9.6710*-02	0.2771	5.2069*-03	7.3752*+02	3.1002*+02			

CAT 7304 VOISINET BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * PW/PD TOD	TW/TR PW/PT SM *	RED2W RED2D D2	CF * CO * PIZ*	H12 H32 H42	H12K H32K D2K	PH* TM* JD	PD* TD* TK
73040501 1.1940*+00 INFINITE	3.8912 4.9506*+05 3.3994*+02	0.9334 1.0142 0.0000	7.3633*+03 2.2132*+04 1.1981*+03	8.6200*+04 0.0000*+00 -1.8640*+01	6.7211 1.8410 0.2026	1.2945 1.8115 2.0175*+03	3.8270*+03 2.9250*+02 7.1670*+02	3.7734*+03 8.4389*+01 3.1336*+02
73040502 1.4480*+00 INFINITE	4.1561 5.0791*+05 3.3649*+02	0.9303 0.9922 0.0000	7.4249*+03 2.4586*+04 1.4648*+03	8.3400*+04 0.0000*+00 -1.6381*+01	7.9587 1.8434 0.1951	1.3048 1.8109 2.8509*+03	2.7010*+03 2.8780*+02 7.2422*+02	2.7223*+03 7.5536*+01 3.0935*+02
73040503 1.7020*+00 INFINITE	4.3301 5.0077*+05 3.3714*+02	0.9316 1.0075 0.0000	7.2355*+03 2.5525*+04 1.6886*+03	8.1000*+04 0.0000*+00 -1.3308*+01	8.2050 1.8426 0.2171	1.3104 1.8067 3.1333*+03	2.1600*+03 2.8830*+02 7.3142*+02	2.1440*+03 7.0977*+01 3.0946*+02
73040504 1.9050*+00 INFINITE	4.4555 5.1474*+05 3.3588*+02	0.9376 0.9752 0.0000	7.3190*+03 2.7156*+04 1.8477*+03	7.7900*+04 0.0000*+00 -1.1849*+01	9.0274 1.8551 0.2144	1.2453 1.8313 3.5163*+03	1.8340*+03 2.8800*+02 7.3414*+02	1.8806*+03 6.7537*+01 3.0779*+02
73040505 2.0570*+00 INFINITE	4.4962 4.6910*+05 3.3653*+02	0.9349 1.0126 0.0000	6.9313*+03 2.6015*+04 1.9892*+03	7.7200*+04 0.0000*+00 -1.0274*+01	8.7853 1.8425 0.1990	1.3007 1.8063 3.8250*+03	1.6490*+03 2.8840*+02 7.3640*+02	1.6286*+03 6.6733*+01 3.0847*+02
73040601 1.1940*+00 INFINITE	3.8656 1.0216*+05 4.2277*+02	0.7557 1.0263 0.0000	2.8969*+03 7.0218*+03 2.5031*+03	1.4100*+03 1.0687*+04 -2.3243*+01	4.0252 1.8168 0.7849	1.3603 1.7860 3.6063*+03	8.2730*+02 2.9460*+02 7.9794*+02	8.0612*+02 1.0549*+02 3.8982*+02
73040602 1.4480*+00 INFINITE	4.1071 1.0416*+05 4.2224*+02	0.7586 0.9864 0.0000	2.8622*+03 7.5881*+03 3.0082*+03	1.2700*+03 8.5240*+05 -2.1150*+01	4.8162 1.8217 0.8143	1.3644 1.7870 4.6366*+03	5.8720*+02 2.9490*+02 8.0910*+02	5.9530*+02 1.0543*+01 3.8839*+02
73040603 1.7020*+00 INFINITE	4.2792 1.0329*+05 4.2216*+02	0.7576 0.9991 0.0000	2.8336*+03 7.9752*+03 3.4829*+03	1.1700*+03 8.1380*+05 -1.5256*+01	4.9708 1.8236 0.8299	1.3697 1.7862 5.4727*+03	4.7160*+02 2.9370*+02 8.1641*+02	4.7202*+02 9.0548*+01 3.8767*+02
73040604 2.0570*+00 INFINITE	4.5035 1.0297*+05 4.2520*+02	0.7646 1.0456 0.0000	2.7559*+03 8.4326*+03 4.1797*+03	1.1300*+03 7.5180*+05 -1.3643*+01	5.1585 1.8159 0.8192	1.3887 1.7768 6.7671*+03	3.7040*+02 2.9800*+02 8.2802*+02	3.5425*+02 1.0549*+02 3.8972*+02
73040701 1.1940*+00 INFINITE	3.9016 5.1397*+05 4.2141*+02	0.7636 1.0119 0.0000	9.5017*+03 2.3731*+04 1.7061*+03	9.3500*+04 7.8230*+05 -2.4392*+01	4.6772 1.8352 0.6627	1.2947 1.8075 2.5377*+03	3.9090*+03 2.9660*+02 7.9850*+02	3.8622*+03 1.0419*+02 3.8842*+02
73040702 1.4480*+00 INFINITE	4.1372 5.1647*+05 4.2239*+02	0.7652 0.9674 0.0000	9.1942*+03 2.4802*+04 2.0152*+03	9.0000*+04 6.9300*+05 -2.0841*+01	5.8435 1.8367 0.6605	1.2996 1.8059 3.2566*+03	2.7450*+03 2.9720*+02 8.1059*+02	2.8375*+03 9.5492*+01 3.8839*+02
73040703 1.7020*+00 INFINITE	4.3245 5.1384*+05 4.2155*+02	0.7644 0.9965 0.0000	9.1791*+03 2.6438*+04 2.3700*+03	8.5500*+04 6.4680*+05 -1.7642*+01	5.7946 1.8366 0.6876	1.3114 1.8026 3.8668*+03	2.2080*+03 2.9580*+02 8.1766*+02	2.2157*+03 8.4093*+01 3.8696*+02
73040704 2.0570*+00 INFINITE	4.5584 5.1774*+05 4.2168*+02	0.7693 1.0104 0.0000	8.9418*+03 2.8057*+04 2.8076*+03	8.3000*+04 6.0770*+05 -1.3343*+01	6.1979 1.8345 0.6830	1.3154 1.7989 4.7654*+03	1.6810*+03 2.9720*+02 8.2654*+02	1.6637*+03 8.1788*+01 3.8633*+02
73040801 1.1940*+00 INFINITE	3.9245 1.0304*+06 4.1338*+02	0.7778 1.0220 0.0000	1.6470*+04 4.1870*+04 1.4777*+03	7.6800*+04 6.6070*+05 -2.5788*+01	4.8932 1.8481 0.5727	1.2629 1.8222 2.1963*+03	7.6740*+03 2.9630*+02 7.9199*+02	7.5090*+03 1.0131*+02 3.8042*+02
73040802 1.4480*+00 INFINITE	4.1488 1.0494*+06 4.1391*+02	0.7749 0.9746 0.0000	1.6616*+04 4.5629*+04 1.7817*+03	7.6000*+04 6.2620*+05 -2.1579*+01	6.1938 1.8501 0.5744	1.2619 1.8218 2.8637*+03	5.5360*+03 2.9490*+02 8.0291*+02	5.6788*+03 9.3169*+01 3.8055*+02
73040803 1.7020*+00 INFINITE	4.3478 1.0359*+06 4.1183*+02	0.7805 1.0074 0.0000	1.6031*+04 4.7534*+04 2.0662*+03	7.4100*+04 5.4960*+05 -1.7344*+01	6.0149 1.8496 0.6132	1.2701 1.8186 3.3529*+03	4.3680*+03 2.9500*+02 8.0908*+02	4.3361*+03 8.6144*+01 3.7796*+02
73040804 2.0570*+00 INFINITE	4.5727 1.0436*+06 4.0950*+02	0.8093 0.9999 0.0000	1.4856*+04 4.9025*+04 2.3458*+03	7.1800*+04 4.7130*+05 -1.3025*+01	6.8210 1.8487 0.5993	1.2781 1.8152 4.0273*+03	3.2950*+03 3.0360*+02 8.1502*+02	3.2953*+03 7.9025*+01 3.7513*+02

CAT 7304		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.						
VOISINET								
RUN	MD *	TH/TR	RED2M	CF *	H12	H12K	PH*	PD*
X *	POD	PH/PO	RED2D	CO *	H32	H32K	TH*	TD*
RZ	TOD	SM *	D2	PI2*	H42	O2K	UD	TR
73040901	3.8686	0.7404	3.0272 ⁺⁰³	1.4100 ⁻⁰³	3.8273	1.3604	8.2690 ⁺⁰²	8.1185 ⁺⁰²
1.1940 ⁺⁰⁰	1.0330 ⁺⁰⁵	1.0185	7.2190 ⁺⁰³	1.1275 ⁻⁰⁴	1.8181	1.7875	2.9110 ⁺⁰²	1.0678 ⁺⁰²
INFINITE	4.2639 ⁺⁰²	0.0000	2.5808 ⁻⁰³	-2.4286 ⁻⁰¹	0.8443	3.6508 ⁻⁰³	8.0150 ⁺⁰²	3.9315 ⁺⁰²
73040902	4.1164	0.7429	2.9291 ⁺⁰³	1.2700 ⁻⁰³	4.6060	1.3691	5.7860 ⁺⁰²	5.8653 ⁺⁰²
1.4480 ⁺⁰⁰	1.0388 ⁺⁰⁵	0.9865	7.6622 ⁺⁰³	9.0320 ⁻⁰⁵	1.8219	1.7875	2.8930 ⁺⁰²	9.6472 ⁺⁰¹
INFINITE	4.2341 ⁺⁰²	0.0000	3.0727 ⁻⁰³	-2.2058 ⁻⁰¹	0.8589	4.6550 ⁻⁰³	8.1064 ⁺⁰²	3.8941 ⁺⁰²
73040903	4.3173	0.7531	2.8904 ⁺⁰³	1.1700 ⁻⁰³	4.5778	1.3766	4.6170 ⁺⁰²	4.5154 ⁺⁰²
1.7020 ⁺⁰⁰	1.0376 ⁺⁰⁵	1.0225	8.2058 ⁺⁰³	8.2210 ⁻⁰⁵	1.8196	1.7830	2.9200 ⁺⁰²	8.9332 ⁺⁰¹
INFINITE	4.2235 ⁺⁰²	0.0000	3.6398 ⁻⁰³	-1.9116 ⁻⁰¹	0.8686	5.5671 ⁻⁰³	8.1814 ⁺⁰²	3.8771 ⁺⁰²
73040904	4.4122	0.7519	2.9231 ⁺⁰³	1.1400 ⁻⁰³	4.9297	1.3791	3.9470 ⁺⁰²	3.9900 ⁺⁰²
1.9050 ⁺⁰⁰	1.0343 ⁺⁰⁵	0.9892	8.5569 ⁺⁰³	8.2960 ⁻⁰⁵	1.8222	1.7831	2.9290 ⁺⁰²	8.6788 ⁺⁰¹
INFINITE	4.2470 ⁺⁰²	0.0000	4.0273 ⁻⁰³	-1.7132 ⁻⁰¹	0.9047	6.3778 ⁻⁰³	8.2413 ⁺⁰²	3.8955 ⁺⁰²
73040905	4.5108	0.7496	2.8738 ⁺⁰³	1.1300 ⁻⁰³	5.0134	1.3852	3.6770 ⁺⁰²	3.5454 ⁺⁰²
2.0570 ⁺⁰⁰	1.0400 ⁺⁰⁵	1.0371	8.6932 ⁺⁰³	7.9880 ⁻⁰⁵	1.8161	1.7779	2.9010 ⁺⁰²	8.3297 ⁺⁰¹
INFINITE	4.2227 ⁺⁰²	0.0000	4.2383 ⁻⁰³	-1.4368 ⁻⁰¹	0.8374	6.7831 ⁻⁰³	8.2543 ⁺⁰²	3.8702 ⁺⁰²
73041001	3.9226	0.7494	9.8746 ⁺⁰³	9.3500 ⁻⁰⁴	4.5004	1.2892	3.8090 ⁺⁰³	3.7728 ⁺⁰³
1.1940 ⁺⁰⁰	5.1641 ⁺⁰⁵	1.0096	2.4267 ⁺⁰⁴	8.3170 ⁻⁰⁵	1.8373	1.8099	2.9230 ⁺⁰²	1.0381 ⁺⁰²
INFINITE	4.2327 ⁺⁰²	0.0000	1.7672 ⁻⁰³	-2.5797 ⁻⁰¹	0.7293	2.5935 ⁻⁰³	8.0132 ⁺⁰²	3.9005 ⁺⁰²
73041002	4.1721	0.7530	9.4149 ⁺⁰³	9.0000 ⁻⁰⁴	5.5726	1.2954	2.6920 ⁺⁰³	2.7442 ⁺⁰³
1.4480 ⁺⁰⁰	5.2279 ⁺⁰⁵	0.9810	2.5409 ⁺⁰⁴	7.2930 ⁻⁰⁵	1.8374	1.8075	2.9160 ⁺⁰²	9.4007 ⁺⁰¹
INFINITE	4.2127 ⁺⁰²	0.0000	2.0687 ⁻⁰³	-2.1668 ⁻⁰¹	0.6933	3.2837 ⁻⁰³	8.1104 ⁺⁰²	3.8724 ⁺⁰²
73041003	4.3595	0.7527	9.4683 ⁺⁰³	8.5500 ⁻⁰⁴	5.5849	1.2949	2.1280 ⁺⁰³	2.1333 ⁺⁰³
1.7020 ⁺⁰⁰	5.1729 ⁺⁰⁵	0.9975	2.7273 ⁺⁰⁴	6.7850 ⁻⁰⁵	1.8408	1.8078	2.9140 ⁺⁰²	8.7872 ⁺⁰¹
INFINITE	4.2188 ⁺⁰²	0.0000	2.4748 ⁻⁰³	-1.8478 ⁻⁰¹	0.7360	3.9684 ⁻⁰³	8.1935 ⁺⁰²	3.8714 ⁺⁰²
73041004	4.4628	0.7555	9.2389 ⁺⁰³	8.4000 ⁻⁰⁴	6.2408	1.3023	1.7940 ⁺⁰³	1.8672 ⁺⁰³
1.9050 ⁺⁰⁰	5.1583 ⁺⁰⁵	0.9608	2.7651 ⁺⁰⁴	6.6960 ⁻⁰⁵	1.8404	1.8056	2.9290 ⁺⁰²	8.4825 ⁺⁰¹
INFINITE	4.2271 ⁺⁰²	0.0000	2.6579 ⁻⁰³	-1.6040 ⁻⁰¹	0.7667	4.4630 ⁻⁰³	8.2410 ⁺⁰²	3.8757 ⁺⁰²
73041005	4.6027	0.7523	8.4996 ⁺⁰³	8.3000 ⁻⁰⁴	6.1769	1.3002	1.6350 ⁺⁰³	1.6092 ⁺⁰³
2.0570 ⁺⁰⁰	5.2891 ⁺⁰⁵	1.0161	2.7874 ⁺⁰⁴	6.5490 ⁻⁰⁵	1.8366	1.8023	2.9020 ⁺⁰²	8.0430 ⁺⁰¹
INFINITE	4.2121 ⁺⁰²	0.0000	2.7856 ⁻⁰³	-1.3735 ⁻⁰¹	0.6911	4.7057 ⁻⁰³	8.2762 ⁺⁰²	3.8577 ⁺⁰²

CAT 7304		VOISINET		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.					
RUN X * RZ	MD * POD TUD	TN/TR PW/PO SW	RED2W RED2D D2	CF * CO * PIZ*	H1Z H3Z H4Z	H1ZK H3ZK D2K	PW* TW* UD	PD* TD* TW	
73041101 1.4480**00 INFINITE	4.1051 1.0394**05 4.2299**02	0.2337 0.9597 0.0000	3.7632**03 8.2470**03 3.2814**03	2.1000**03 NM -1.4340**01	4.0198 1.8057 1.0038	1.3376 1.7894 4.5104**03	5.7160**02 9.0910**01 8.0972**02	5.9561**02 9.6785**01 3.8905**02	
73041102 1.7020**00 INFINITE	4.3312 1.0534**05 4.2502**02	0.2378 1.0233 0.0000	8.3288**03 8.6302**03 3.8325**03	1.8600**03 NM -1.2407**01	3.7073 1.7957 0.9828	1.3628 1.7792 5.1988**03	4.6090**02 9.2770**01 8.2128**02	4.5039**02 8.9443**01 3.9012**02	
73041201 1.4480**00 INFINITE	4.1241 5.0601**05 4.2262**02	0.2330 0.4522 0.0000	2.7443**04 2.5929**04 2.1375**03	1.4350**03 NM -2.8020**01	5.1203 1.8271 0.8446	1.2898 1.8051 3.1631**03	2.6930**03 9.0560**01 8.1022**02	2.8282**03 9.6014**01 3.8865**02	
73041202 1.7020**00 INFINITE	4.3881 5.1809**05 4.2291**02	0.2429 1.0391 0.0000	2.6339**04 2.8414**04 2.6211**03	1.3500**03 NM -1.2213**01	4.3236 1.8143 0.8441	1.3165 1.7950 3.7849**03	2.1410**03 9.4240**01 8.2147**02	2.0605**03 8.7179**01 3.8799**02	
73041203 1.9050**00 INFINITE	4.5018 5.3836**05 4.2134**02	0.2321 1.0043 0.0000	2.8058**04 3.0123**04 2.8151**03	1.3400**03 NM -1.0236**01	5.0707 1.8178 0.8323	1.3067 1.7979 4.2343**03	1.8640**03 8.9650**01 8.2419**02	1.8560**03 8.3380**01 3.8619**02	
73041204 2.0570**00 INFINITE	4.6116 5.4194**05 4.2032**02	0.2328 1.0105 0.0000	2.8328**04 3.1633**04 3.0890**03	1.3500**03 NM -8.9960**02	5.1300 1.8198 0.8403	1.3056 1.7992 4.6326**03	1.6480**03 8.9530**01 8.2705**02	1.6309**03 8.0009**01 3.8492**02	
73041301 1.4480**00 INFINITE	4.1393 1.0175**06 4.2446**02	0.3236 1.0000 0.0000	3.7482**04 4.8658**04 2.0214**03	1.1930**03 NM -1.5229**01	4.9158 1.8415 0.7335	1.2592 1.8207 2.9765**03	5.5750**03 1.2630**02 8.1267**02	5.5750**03 9.5885**01 3.9029**02	
73041302 1.7020**00 INFINITE	4.3817 1.0245**06 4.1175**02	0.2558 1.0312 0.0000	4.4527**04 5.0400**04 2.2528**03	1.1220**03 NM -1.2734**01	4.5542 1.8301 0.8090	1.2812 1.8101 3.2630**03	4.2360**03 9.6620**01 8.1032**02	4.1076**03 8.5075**01 3.7778**02	
73041303 1.9050**00 INFINITE	4.5095 1.0894**06 4.2756**02	0.2407 1.0000 0.0000	4.7571**04 5.3022**04 2.5122**03	1.1100**03 NM -1.1048**01	5.5929 1.8360 0.7556	1.2779 1.8143 3.8424**03	3.7200**03 9.4310**01 3.9189**02	3.7200**03 8.4379**01 3.9189**02	
73041304 2.0570**00 INFINITE	4.5081 7.8188**05 4.2226**02	0.2586 0.9808 0.0000	4.1822**04 4.9960**04 2.5763**03	1.1200**03 NM -9.4430**02	5.5874 1.8371 0.8209	1.2705 1.8152 3.9578**03	3.2940**03 1.0010**02 8.2532**02	3.3586**03 8.3375**01 3.8702**02	
73041401 1.7020**00 INFINITE	4.3171 1.0246**05 4.2589**02	0.2211 1.0284 0.0000	9.7940**03 9.4064**03 4.2769**03	1.8600**03 NM -1.4624**01	3.1033 1.7967 1.0725	1.3605 1.7795 5.4981**03	4.5870**02 8.6440**01 8.2156**02	4.4604**02 9.0089**01 3.9099**02	
73041402 1.9050**00 INFINITE	4.4549 1.0273**05 4.2641**02	0.2249 0.9889 0.0000	9.1819**03 9.4038**03 4.5797**03	1.8000**03 NM -1.2265**01	3.4719 1.7836 1.1194	1.3817 1.7679 6.0996**03	3.7140**02 8.7930**01 8.2740**02	3.7556**02 8.5810**01 3.9099**02	
73041403 2.0570**00 INFINITE	4.5527 1.0561**05 4.2615**02	0.2181 1.0396 0.0000	9.7557**03 1.0028**04 4.9805**03	1.8100**03 NM -1.0987**01	3.2560 1.7859 1.0926	1.3689 1.7691 6.5655**03	3.5530**02 8.5140**01 8.3071**02	3.4176**02 8.2821**01 3.9044**02	
73041501 1.7020**00 INFINITE	4.3708 5.1697**05 4.1767**02	0.2286 1.0240 0.0000	2.9503**04 3.1095**04 2.7976**03	1.3500**03 NM -1.3084**01	4.2674 1.8077 0.8848	1.3252 1.7898 3.9854**03	2.1520**03 9.1430**01 8.1569**02	2.1016**03 8.6639**01 3.8324**02	
73041502 1.9050**00 INFINITE	4.5118 5.1955**05 1.2893**02	0.2882 0.9599 0.0000	2.1995**04 2.9174**04 2.8351**03	1.3400**03 NM -1.1347**01	5.2479 1.8079 0.9508	1.3336 1.7882 4.3180**03	1.6980**03 1.1120**02 8.2415**02	1.7690**03 8.3004**01 3.8579**02	
73041503 2.0570**00 INFINITE	4.6183 5.2938**05 4.2350**02	0.2529 1.0000 0.0000	2.5870**04 3.1395**04 3.1823**03	1.3500**03 NM -9.6480**02	4.8191 1.8101 0.9203	1.3158 1.7917 4.7036**03	1.5800**03 9.4070**01 8.3040**02	1.5800**03 8.0425**01 3.8782**02	

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD D2PW	H12PD H12PW	H32PD H32PW	H42PD H42PW	RED2PDD RED2PWD	RED2PDW RED2PWW	DSTAR
73040301	1.1130 ⁻⁰³ 1.1007 ⁻⁰³	6.6935 6.6879	1.8513 1.8529	0.2474 0.2472	4.2671 ⁺⁰⁴ 4.2707 ⁺⁰⁴	1.3998 ⁺⁰⁴ 1.4009 ⁺⁰⁴	7.3629 ⁻⁰³
73040302	1.3518 ⁻⁰³ 1.3718 ⁻⁰³	7.4733 7.4806	1.8536 1.8518	0.2256 0.2258	4.5853 ⁺⁰⁴ 4.5809 ⁺⁰⁴	1.3984 ⁺⁰⁴ 1.3970 ⁺⁰⁴	1.0256 ⁻⁰²
73040303	1.5461 ⁻⁰³ 1.5361 ⁻⁰³	8.1147 8.1115	1.8502 1.8509	0.2195 0.2194	4.7351 ⁺⁰⁴ 4.7369 ⁺⁰⁴	1.3379 ⁺⁰⁴ 1.3384 ⁺⁰⁴	1.2461 ⁻⁰²
73040304	1.6928 ⁻⁰³ 1.7258 ⁻⁰³	8.6177 8.6271	1.8565 1.8544	0.2190 0.2192	4.8855 ⁺⁰⁴ 4.8802 ⁺⁰⁴	1.3200 ⁺⁰⁴ 1.3186 ⁺⁰⁴	1.4867 ⁻⁰²
73040305	1.7935 ⁻⁰³ 1.7977 ⁻⁰³	8.9811 8.9822	1.8511 1.8508	0.2098 0.2099	4.9539 ⁺⁰⁴ 4.9532 ⁺⁰⁴	1.2928 ⁺⁰⁴ 1.2926 ⁺⁰⁴	1.6146 ⁻⁰²
73041301	2.0231 ⁻⁰³ 2.0231 ⁻⁰³	4.9161 4.9161	1.8415 1.8415	0.7336 0.7336	4.8710 ⁺⁰⁴ 4.8710 ⁺⁰⁴	3.7522 ⁺⁰⁴ 3.7522 ⁺⁰⁴	9.9458 ⁻⁰³
73041302	2.2246 ⁻⁰³ 2.1812 ⁻⁰³	4.9342 4.9284	1.8280 1.8301	0.8192 0.8183	4.9829 ⁺⁰⁴ 4.9867 ⁺⁰⁴	4.4023 ⁺⁰⁴ 4.4074 ⁺⁰⁴	1.0750 ⁻⁰²
73041303	2.5122 ⁻⁰³ 2.5122 ⁻⁰³	5.5925 5.5925	1.8360 1.8360	0.7556 0.7556	5.3090 ⁺⁰⁴ 5.3090 ⁺⁰⁴	4.7629 ⁺⁰⁴ 4.7629 ⁺⁰⁴	1.4050 ⁻⁰²
73041304	2.5998 ⁻⁰³ 2.5325 ⁻⁰³	5.2924 5.2960	1.8386 1.8374	0.8115 0.8110	5.0475 ⁺⁰⁴ 5.0441 ⁺⁰⁴	4.2254 ⁺⁰⁴ 4.2225 ⁺⁰⁴	1.3942 ⁻⁰²

73040301		VOISINET	PROFILE TABULATION		35 POINTS, DELTA AT POINT 25			
I	Y	PTP/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	1.01802	0.86883	0.00000	0.00000	3.51480	0.00000
2	6.3000-05	1.3595+00	1.01802	0.87969	0.17353	0.31330	3.25980	0.09784
3	1.4000-04	1.8224+00	1.01802	0.89117	0.24783	0.43190	3.03710	0.14477
4	2.1600-04	2.4187+00	1.01802	0.89926	0.30850	0.51810	2.82040	0.18701
5	2.9200-04	3.0844+00	1.01802	0.90989	0.36134	0.58640	2.63370	0.22666
6	5.2100-04	3.8669+00	1.01802	0.92109	0.41392	0.64770	2.44860	0.26928
7	6.9800-04	4.3458+00	1.01802	0.92662	0.44262	0.67840	2.34700	0.29426
8	9.7800-04	4.7626+00	1.01802	0.93062	0.46644	0.70190	2.26440	0.31556
9	1.2070-03	5.0144+00	1.01802	0.93382	0.48013	0.71530	2.21950	0.32809
10	1.4630-03	5.2718+00	1.01802	0.93797	0.49372	0.72860	2.17780	0.34059
11	1.7170-03	5.5458+00	1.01802	0.93977	0.50777	0.74100	2.12960	0.35422
12	1.9960-03	5.8184+00	1.01802	0.93974	0.52136	0.75190	2.07990	0.36802
13	2.2760-03	6.0817+00	1.01802	0.94411	0.53416	0.76360	2.04360	0.38039
14	2.4260-03	6.2111+00	1.01802	0.94120	0.54033	0.76710	2.01550	0.38746
15	5.1230-03	8.5416+00	1.01802	0.96055	0.64128	0.84230	1.72520	0.49703
16	7.7420-03	1.0774+01	1.01629	0.97273	0.72479	0.89170	1.51360	0.59872
17	1.0030-02	1.2623+01	1.01476	0.97924	0.78723	0.92210	1.37200	0.68201
18	1.2624-02	1.4442+01	1.01303	0.98559	0.84416	0.94670	1.25770	0.76253
19	1.5420-02	1.6012+01	1.01110	0.99160	0.89037	0.96510	1.17490	0.83055
20	1.7988-02	1.7330+01	1.00937	0.99498	0.92736	0.97800	1.11220	0.88757
21	2.0480-02	1.8417+01	1.00784	0.99640	0.95681	0.98700	1.06410	0.93463
22	2.2718-02	1.9150+01	1.00529	0.99810	0.97616	0.99300	1.03480	0.96469
23	2.3073-02	1.9236+01	1.00499	1.00035	0.97840	0.99470	1.03360	0.96717
24	2.5489-02	1.9792+01	1.00244	0.99899	0.99280	0.99770	1.00990	0.99033
D 25	2.7854-02	2.0073+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
26	3.0549-02	2.0170+01	0.99715	0.99739	1.00246	0.99930	0.99370	1.00277
27	3.2990-02	2.0249+01	0.99480	0.99880	1.00448	1.00050	0.99210	1.00303
28	3.5303-02	2.0263+01	0.99277	0.99983	1.00482	1.00110	0.99260	1.00127
29	3.8227-02	2.0285+01	0.99033	0.99996	1.00538	1.00130	0.99190	0.99971
30	4.0795-02	2.0317+01	0.98615	0.99996	1.00619	1.00150	0.99070	0.99691
31	4.3261-02	2.0339+01	0.98310	1.00089	1.00674	1.00210	0.99080	0.99431
32	4.6007-02	2.0314+01	0.98615	1.00199	1.00613	1.00250	0.99280	0.99579
33	4.8397-02	2.0314+01	0.98636	1.00179	1.00613	1.00240	0.99260	0.99610
34	5.0305-02	2.0344+01	0.98208	1.00142	1.00689	1.00240	0.99110	0.99328
35	5.2746-02	2.0408+01	0.97414	1.00203	1.00881	1.00310	0.98930	0.98773

INPUT VARIABLES Y,U/UD,T/TD,P/PH

73040302		VOISINET		PROFILE TABULATION		57 POINTS, DELTA AT POINT 42		
I	Y	PT2/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	0.97694	0.86778	0.00000	0.00000	3.78470	0.00000
2	6.3000-05	1.2438+00	0.97694	0.87136	0.13834	0.26140	3.57060	0.07152
3	1.4000-04	1.5739+00	0.97694	0.86083	0.20288	0.37270	3.37470	0.10789
4	2.1600-04	2.0264+00	0.97694	0.89146	0.25795	0.45980	3.17730	0.14138
5	3.4300-04	2.8480+00	0.97694	0.90562	0.32712	0.55760	2.90550	0.10749
6	4.9500-04	3.3573+00	0.97694	0.91373	0.36225	0.60240	2.76530	0.21282
7	5.7200-04	3.7283+00	0.97694	0.91670	0.38564	0.63030	2.67140	0.23050
8	7.4900-04	4.0775+00	0.97694	0.92364	0.40633	0.65400	2.59060	0.24663
9	1.0540-03	4.5121+00	0.97694	0.92868	0.43062	0.68020	2.49510	0.26633
10	1.2810-03	4.7673+00	0.97694	0.93080	0.44423	0.69400	2.44060	0.27770
11	1.5620-03	5.0072+00	0.97694	0.93300	0.45665	0.70630	2.39230	0.28843
12	2.0960-03	5.5090+00	0.97694	0.93764	0.48155	0.73000	2.29810	0.31033
13	2.6030-03	5.9303+00	0.97694	0.94035	0.50147	0.74760	2.22250	0.32862
14	3.0350-03	6.3095+00	0.97694	0.94178	0.51874	0.76180	2.15670	0.34508
15	3.6200-03	6.7531+00	0.97694	0.94632	0.53822	0.77830	2.09110	0.36362
16	4.1270-03	7.1258+00	0.97694	0.94861	0.55405	0.79060	2.03620	0.37932
17	4.6860-03	7.5397+00	0.97694	0.95239	0.57110	0.80390	1.98140	0.39637
18	5.0670-03	7.8393+00	0.97694	0.95439	0.58314	0.81270	1.94230	0.40877
19	5.7020-03	8.2730+00	0.97733	0.95649	0.60012	0.82440	1.91710	0.42696
20	6.1340-03	8.5984+00	0.97763	0.95788	0.61255	0.83260	1.884750	0.44058
21	6.7180-03	9.0007+00	0.97802	0.96028	0.62758	0.84250	1.850220	0.45721
22	7.1760-03	9.3668+00	0.97831	0.95964	0.64094	0.850980	1.75790	0.47293
23	7.7850-03	9.7943+00	0.97870	0.96182	0.65020	0.85910	1.71400	0.49055
24	8.7250-03	1.0480+01	0.97929	0.96321	0.67996	0.87430	1.65330	0.51787
25	9.5300-03	1.1058+01	0.97978	0.97082	0.69935	0.88550	1.60140	0.54147
26	1.0223-02	1.1553+01	0.98027	0.97280	0.71556	0.89350	1.55420	0.56174
27	1.1468-02	1.2409+01	0.98105	0.97705	0.74271	0.90750	1.49300	0.59632
28	1.2891-02	1.3332+01	0.98193	0.98059	0.77070	0.92080	1.42670	0.63374
29	1.4033-02	1.4019+01	0.98271	0.98314	0.79124	0.92990	1.38170	0.66161
30	1.5431-02	1.4861+01	0.98359	0.98627	0.81550	0.94030	1.32950	0.69565
31	1.6396-02	1.5477+01	0.98417	0.98832	0.83276	0.94730	1.29400	0.72048
32	1.7844-02	1.6321+01	0.98515	0.99107	0.85589	0.95630	1.24840	0.75465
33	1.8885-02	1.6878+01	0.98583	0.99247	0.87079	0.96170	1.21970	0.77730
34	2.0440-02	1.7729+01	0.98681	0.99461	0.89310	0.96950	1.17840	0.81188
35	2.1425-02	1.8182+01	0.98759	0.99463	0.90476	0.97290	1.15630	0.83095
36	2.2847-02	1.8857+01	0.98877	0.99484	0.92184	0.97780	1.12510	0.85931
37	2.4346-02	1.9481+01	0.99004	0.99730	0.93736	0.98320	1.10020	0.88475
38	2.5540-02	1.9902+01	0.99101	0.99830	0.94767	0.98640	1.08340	0.90228
39	2.7927-02	2.0593+01	0.99297	0.99963	0.96438	0.99130	1.05660	0.93160
40	3.1280-02	2.1390+01	0.99576	1.00001	0.98330	0.99610	1.02620	0.96650
41	3.3922-02	2.1851+01	0.99784	1.00033	0.99409	0.99880	1.00950	0.98727
42	3.6487-02	2.2106+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
43	4.0526-02	2.2305+01	1.00332	0.99991	1.00457	1.00100	0.99290	1.01151
44	4.3472-02	2.2340+01	1.00567	0.99995	1.00538	1.00120	0.99170	1.01530
45	4.5036-02	2.2377+01	1.00772	0.99936	1.00625	1.00110	0.98980	1.01922
46	4.7943-02	2.2401+01	1.00488	1.00111	1.00679	1.00210	0.99070	1.01645
47	5.0711-02	2.2381+01	1.00723	1.00131	1.00634	1.00210	0.99160	1.01789
48	5.2870-02	2.2335+01	1.01290	1.00180	1.00527	1.00210	0.99170	1.02146
49	5.5766-02	2.2313+01	1.01544	1.00223	1.00477	1.00220	0.99490	1.02289
50	5.7721-02	2.2304+01	1.01671	1.00232	1.00456	1.00220	0.99530	1.02375
51	6.1049-02	2.2322+01	1.01456	1.00273	1.00497	1.00290	0.99510	1.02210
52	6.3411-02	2.2335+01	1.01270	1.00340	1.00527	1.00290	0.99530	1.02043
53	6.6154-02	2.2278+01	1.01973	1.00359	1.00396	1.00270	0.99750	1.02505
54	6.8674-02	2.2289+01	1.01876	1.00368	1.00421	1.00280	0.99720	1.02448
55	7.0777-02	2.2252+01	1.02325	1.00387	1.00334	1.00270	0.99870	1.02735
56	7.3851-02	2.2213+01	1.02814	1.00448	1.00245	1.00280	1.00070	1.03024
57	7.6365-02	2.2197+01	1.03048	1.00380	1.00210	1.00240	1.00060	1.03233

INPUT VARIABLES Y,U/UD,Y/TD,P/PW

73040303		VUISHFT		PROFILE TABULATION		55 POINTS, DELTA AT POINT 37			
I	Y	PT2/P	P/PD	T0/T00	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	1.01020	0.86009	0.00000	0.00000	4.08750	0.00000	
2	0.3000-05	1.1562+00	1.01020	0.87089	0.10683	0.21190	3.93420	0.05441	
3	1.4000-04	1.5100+00	1.01020	0.88054	0.18356	0.35240	3.68540	0.09659	
4	2.1600-04	2.0700+00	1.01020	0.89248	0.24969	0.46130	3.41320	0.13653	
5	3.5800-04	2.9154+00	1.01020	0.90610	0.31609	0.55770	3.11300	0.18098	
6	5.7200-04	3.5748+00	1.01020	0.91577	0.35811	0.61210	2.92160	0.21165	
7	8.2500-04	4.0581+00	1.01020	0.92105	0.38577	0.64520	2.79730	0.23300	
8	1.0800-03	4.3456+00	1.01020	0.92294	0.40126	0.66190	2.72100	0.24574	
9	1.4600-03	4.7162+00	1.01020	0.92619	0.42036	0.68230	2.63460	0.26162	
10	2.0450-03	5.2204+00	1.01020	0.92957	0.44497	0.70690	2.52300	0.28295	
11	2.7770-03	5.5827+00	1.01020	0.93342	0.46209	0.72370	2.45260	0.29806	
12	3.6880-03	6.1509+00	1.01020	0.93762	0.48705	0.74650	2.34920	0.32101	
13	4.0010-03	6.7152+00	1.01020	0.94138	0.51084	0.76670	2.25260	0.34343	
14	4.4580-03	7.0357+00	1.01020	0.94417	0.52387	0.77760	2.20330	0.35653	
15	5.0670-03	7.4391+00	1.01020	0.94690	0.53980	0.79020	2.14290	0.37252	
16	6.0580-03	8.0858+00	1.01020	0.95158	0.56441	0.80890	2.05400	0.39784	
17	7.0490-03	8.7997+00	1.01020	0.95594	0.59033	0.82720	1.96350	0.42559	
18	8.1140-03	9.4782+00	1.01020	0.96027	0.61401	0.84310	1.88540	0.45174	
19	9.1820-03	1.0280+01	1.01020	0.96457	0.64082	0.85980	1.80020	0.48249	
20	1.0223-02	1.0978+01	1.01020	0.96819	0.66327	0.87300	1.73240	0.50407	
21	1.1417-02	1.1746+01	1.00980	0.97225	0.68713	0.88640	1.66410	0.53788	
22	1.2789-02	1.2610+01	1.00939	0.97580	0.71349	0.90000	1.59070	0.57110	
23	1.3957-02	1.3351+01	1.00899	0.97912	0.73486	0.91040	1.53650	0.59784	
24	1.5354-02	1.4221+01	1.00859	0.98239	0.75889	0.92170	1.47510	0.63020	
25	1.6294-02	1.4804+01	1.00828	0.98399	0.77483	0.92850	1.43600	0.65194	
26	1.7691-02	1.5649+01	1.00788	0.98626	0.79736	0.93770	1.38300	0.68336	
27	1.8783-02	1.6321+01	1.00748	0.98736	0.81481	0.94420	1.34290	0.70841	
28	2.0434-02	1.7324+01	1.00697	0.98905	0.84034	0.95400	1.28180	0.74538	
29	2.3025-02	1.8764+01	1.00616	0.99388	0.87538	0.96610	1.21800	0.79807	
30	2.5413-02	1.9840+01	1.00546	0.99612	0.90078	0.97430	1.16490	0.83735	
31	2.7927-02	2.0886+01	1.00465	0.99777	0.92478	0.98140	1.12620	0.87548	
32	3.0391-02	2.1789+01	1.00394	0.99854	0.94501	0.98680	1.09040	0.90855	
33	3.2880-02	2.2591+01	1.00313	0.99960	0.96262	0.99150	1.06090	0.93751	
34	3.5522-02	2.3294+01	1.00232	1.00045	0.97781	0.99540	1.03630	0.96276	
35	3.7503-02	2.3716+01	1.00172	1.00070	0.98680	0.99750	1.02180	0.97789	
36	4.0323-02	2.4112+01	1.00081	1.00086	0.99518	0.99940	1.00850	0.99178	
37	4.2862-02	2.4342+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
38	4.5885-02	2.4590+01	0.99909	1.00041	1.00518	1.00130	0.99230	1.00815	
39	4.8247-02	2.4633+01	0.99838	1.00043	1.00607	1.00150	0.99090	1.00906	
40	5.0838-02	2.4685+01	0.99754	0.99979	1.00716	1.00140	0.98880	1.01049	
41	5.3200-02	2.4704+01	0.99545	1.00122	1.00755	1.00220	0.98490	1.00835	
42	5.5308-02	2.4711+01	0.99444	1.00115	1.00771	1.00220	0.98410	1.00761	
43	5.8458-02	2.4731+01	0.99232	1.00139	1.00811	1.00240	0.98870	1.00607	
44	6.0388-02	2.4748+01	0.99050	1.00164	1.00847	1.00260	0.98840	1.00473	
45	6.3589-02	2.4703+01	0.98535	1.00222	1.00755	1.00270	0.98040	1.00771	
46	6.6027-02	2.4704+01	0.98535	1.00082	1.00756	1.00200	0.98400	1.00844	
47	6.8446-02	2.4694+01	0.98646	1.00170	1.00735	1.00240	0.99020	1.00874	
48	7.0930-02	2.4703+01	0.98586	1.00423	1.00754	1.00370	0.99240	1.00720	
49	7.3215-02	2.4673+01	0.98677	1.00331	1.00734	1.00320	0.99180	1.00822	
50	7.7940-02	2.4611+01	1.00616	1.00383	1.00562	1.00330	0.99500	1.01435	
51	8.2436-02	2.4546+01	1.01394	1.00349	1.00426	1.00260	0.99670	1.01994	
52	8.6677-02	2.4543+01	1.01424	1.00442	1.00421	1.00310	0.99780	1.01963	
53	9.2113-02	2.4514+01	1.01647	1.00544	1.00370	1.00350	0.99960	1.02043	
54	9.6914-02	2.4404+01	1.03041	1.00586	1.00130	1.00320	1.00380	1.02779	
55	1.0194-01	2.4356+01	1.03596	1.00488	1.00030	1.00250	1.00440	1.03400	

INPUT VARIABLES Y, U/U0, T/T0, P/P0

73040304		VOISINET		PROFILE TABULATION		56 POINTS, DELTA AT POINT 43			
I	Y	P12/P	P/PD	T0/T0D	M/M0	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	0.97040	0.86732	0.00000	0.00000	4.28230	0.00000	
2	6.3000*-05	1.1404*+00	0.97040	0.87354	0.09857	0.20090	4.15410	0.04693	
3	6.9000*-05	1.2455*+00	0.97040	0.87854	0.12822	0.25840	4.07400	0.06164	
4	2.4100*-04	1.9508*+00	0.97040	0.89349	0.23115	0.44130	3.64470	0.11750	
5	3.4300*-04	2.9357*+00	0.97040	0.90214	0.28017	0.51640	3.40260	0.14739	
6	4.4400*-04	2.9691*+00	0.97040	0.90835	0.31032	0.55960	3.25190	0.16699	
7	5.2100*-04	3.2871*+00	0.97040	0.91327	0.33045	0.58660	3.15340	0.18056	
8	6.7300*-04	3.7109*+00	0.97040	0.91841	0.35533	0.61840	3.02880	0.19813	
9	6.5100*-04	3.9948*+00	0.97040	0.92241	0.37100	0.63760	2.95360	0.20948	
10	1.0030*-03	4.2213*+00	0.97040	0.92252	0.38301	0.65080	2.88720	0.21874	
11	1.2570*-03	4.4407*+00	0.97040	0.92212	0.39428	0.66260	2.82420	0.22767	
12	1.6130*-03	4.8039*+00	0.97040	0.92666	0.41222	0.68250	2.74120	0.24161	
13	2.0190*-03	5.1467*+00	0.97040	0.93166	0.42845	0.70010	2.67010	0.25444	
14	2.4260*-03	5.4533*+00	0.97040	0.93480	0.44244	0.71430	2.60650	0.26593	
15	2.8320*-03	5.7362*+00	0.97040	0.93711	0.45495	0.72640	2.54930	0.27651	
16	3.3910*-03	6.1525*+00	0.97040	0.94026	0.47275	0.74290	2.46440	0.29194	
17	4.0010*-03	6.5403*+00	0.97040	0.94188	0.48874	0.75660	2.39650	0.30637	
18	4.6860*-03	7.0070*+00	0.97040	0.94137	0.50730	0.77080	2.30860	0.32400	
19	5.4230*-03	7.4573*+00	0.97060	0.94592	0.52458	0.78540	2.24160	0.34007	
20	6.3630*-03	8.0670*+00	0.97118	0.95031	0.54709	0.80290	2.15360	0.36204	
21	7.4040*-03	8.7131*+00	0.97186	0.95496	0.56997	0.81990	2.06880	0.38512	
22	8.3440*-03	9.3311*+00	0.97244	0.95799	0.59101	0.83400	1.99130	0.40728	
23	9.3600*-03	1.0000*+01	0.97312	0.96176	0.61297	0.84830	1.91520	0.43102	
24	1.0376*-02	1.0621*+01	0.97370	0.96246	0.63268	0.85930	1.84470	0.45357	
25	1.1621*-02	1.1435*+01	0.97448	0.96694	0.65759	0.87400	1.76650	0.48214	
26	1.2992*-02	1.2242*+01	0.97535	0.97102	0.68143	0.88720	1.69510	0.51049	
27	1.4211*-02	1.2970*+01	0.97613	0.97455	0.70218	0.89810	1.63350	0.53589	
28	1.5405*-02	1.3677*+01	0.97690	0.97713	0.72180	0.90760	1.58110	0.56077	
29	1.6700*-02	1.4428*+01	0.97768	0.98031	0.74205	0.91720	1.52780	0.58694	
30	1.8351*-02	1.5408*+01	0.97875	0.98486	0.76766	0.92900	1.46450	0.62087	
31	2.0358*-02	1.6586*+01	0.98001	0.98821	0.79737	0.94100	1.39270	0.66216	
32	2.3178*-02	1.8142*+01	0.98176	0.99182	0.83501	0.95480	1.30750	0.71693	
33	2.5768*-02	1.9400*+01	0.98341	0.99411	0.86423	0.96450	1.24550	0.76154	
34	2.8232*-02	2.0521*+01	0.98496	0.99571	0.88946	0.97220	1.19470	0.80152	
35	3.0518*-02	2.1518*+01	0.98632	0.99583	0.91130	0.97790	1.15150	0.83762	
36	3.3105*-02	2.2525*+01	0.98806	0.99690	0.93265	0.98370	1.11200	0.87406	
37	3.5877*-02	2.3301*+01	0.98971	0.99892	0.94912	0.98850	1.08470	0.90194	
38	3.8189*-02	2.3819*+01	0.99117	1.00069	0.95984	0.99180	1.06770	0.92071	
39	4.0907*-02	2.4410*+01	0.99292	1.00175	0.97199	0.99500	1.04790	0.94279	
40	4.3294*-02	2.4968*+01	0.99437	1.00016	0.98317	0.99660	1.02750	0.96447	
41	4.6012*-02	2.5534*+01	0.99612	0.99845	0.99447	0.99710	1.00530	0.98799	
42	4.8628*-02	2.5733*+01	0.99777	1.00025	0.99840	0.99980	1.00280	0.99476	
43	5.2261*-02	2.5814*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
44	5.6147*-02	2.5839*+01	1.00243	1.00020	1.00050	1.00020	0.99940	1.00323	
45	5.9830*-02	2.5918*+01	1.00475	1.00017	1.00205	1.00050	0.99690	1.00838	
46	6.3665*-02	2.5888*+01	1.00825	1.00061	1.00145	1.00060	0.99830	1.01057	
47	6.7475*-02	2.5880*+01	1.00873	1.00127	1.00130	1.00090	0.99920	1.01045	
48	7.1484*-02	2.5867*+01	1.01058	1.00178	1.00105	1.00110	1.00010	1.01154	
49	7.5298*-02	2.5852*+01	1.01184	1.00250	1.00075	1.00140	1.00130	1.01194	
50	7.9032*-02	2.5870*+01	1.01019	1.00256	1.00110	1.00150	1.00080	1.01090	
51	8.3071*-02	2.5941*+01	1.00243	1.00337	1.00250	1.00220	0.99940	1.00523	
52	8.6652*-02	2.5982*+01	0.99767	1.00307	1.00330	1.00220	0.99780	1.00207	
53	9.0589*-02	2.5862*+01	1.01077	1.00342	1.00095	1.00190	1.00190	1.01077	
54	9.4298*-02	2.5799*+01	1.01776	1.00412	0.99970	1.00200	1.00460	1.01512	
55	9.7904*-02	2.5961*+01	0.99981	1.00463	1.00290	1.00290	1.00000	1.00271	
56	1.0189*-01	2.4068*+01	0.98845	1.00539	1.00501	1.00370	0.99740	0.99470	

INPUT VARIABLES Y,U/UD,T/TD,P/PH

73040505		VOISINET		PROFILE TABULATION		43 POINTS, DELTA AT POINT 35		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/U0	T/TD	RHO/RHO0*U/U0
1	0.0000*+00	1.0000*+00	0.99641	0.86683	0.00000	0.00000	4.43060	0.00000
2	0.3000*-05	1.0953*+00	0.99641	0.86640	0.08006	0.16630	4.31470	0.03840
3	1.4000*-04	1.3006*+00	0.99641	0.87242	0.13772	0.28010	4.13660	0.06747
4	1.9100*-04	1.5762*+00	0.99641	0.87953	0.18376	0.36510	3.94750	0.09216
5	2.4100*-04	1.7206*+00	0.99641	0.88311	0.20197	0.39710	3.86550	0.10236
6	2.6700*-04	1.9364*+00	0.99641	0.88785	0.22483	0.43540	3.75720	0.11557
7	3.4300*-04	2.4460*+00	0.99641	0.89703	0.26757	0.50360	3.54230	0.14166
8	4.1400*-04	2.6628*+00	0.99641	0.90082	0.28321	0.52700	3.46250	0.15166
9	4.9500*-04	2.9500*+00	0.99641	0.90606	0.30272	0.55520	3.36380	0.16446
10	5.2100*-04	3.1167*+00	0.99641	0.90481	0.31302	0.56960	3.31130	0.17140
11	5.7200*-04	3.2244*+00	0.99641	0.90984	0.31961	0.57840	3.27500	0.17598
12	6.3000*-04	3.5903*+00	0.99641	0.91600	0.34100	0.60690	3.16760	0.19091
13	6.2500*-04	3.6491*+00	0.99641	0.92022	0.35529	0.62520	3.09650	0.20118
14	1.1050*-03	4.1432*+00	0.99641	0.92370	0.37081	0.64400	3.01620	0.21275
15	1.3080*-03	4.3157*+00	0.99641	0.92305	0.37961	0.65340	2.96270	0.21975
16	1.5880*-03	4.5933*+00	0.99641	0.92544	0.39333	0.66880	2.89120	0.23049
17	1.8670*-03	4.8323*+00	0.99641	0.92768	0.40475	0.68130	2.83330	0.23960
18	2.1460*-03	5.0659*+00	0.99641	0.92893	0.41560	0.69250	2.77640	0.24853
19	2.3750*-03	5.2068*+00	0.99641	0.92925	0.42201	0.69880	2.74260	0.25394
20	3.9500*-03	6.2861*+00	0.99641	0.93721	0.46810	0.74310	2.52010	0.29381
21	5.2200*-03	7.0792*+00	0.99641	0.94333	0.49921	0.77040	2.38160	0.32232
22	6.1410*-03	8.8531*+00	0.99641	0.95426	0.56252	0.81900	2.11980	0.38497
23	1.0223*-02	1.0142*+01	0.99641	0.96157	0.60435	0.84710	1.96470	0.42961
24	1.2891*-02	1.1688*+01	0.99661	0.96937	0.65092	0.87500	1.80700	0.48259
25	1.4922*-02	1.2806*+01	0.99681	0.97451	0.68845	0.89320	1.70100	0.52343
26	1.8199*-02	1.4815*+01	0.99701	0.98078	0.73619	0.91740	1.55290	0.58900
27	2.0942*-02	1.6461*+01	0.99731	0.98478	0.77732	0.93430	1.44470	0.64497
28	2.3508*-02	1.7946*+01	0.99751	0.98873	0.81261	0.94760	1.36040	0.69497
29	2.6759*-02	1.9598*+01	0.99771	0.99303	0.85016	0.96110	1.27800	0.75031
30	3.2220*-02	2.2133*+01	0.99821	0.99714	0.90476	0.97730	1.16750	0.83584
31	3.6614*-02	2.3818*+01	0.99851	0.99939	0.93931	0.98690	1.10390	0.89268
32	4.0551*-02	2.4960*+01	0.99880	1.00058	0.96201	0.99450	1.06440	0.93134
33	4.7262*-02	2.6311*+01	0.99940	1.00110	0.98817	0.99820	1.02040	0.97766
34	5.1448*-02	2.6765*+01	0.99970	1.00045	0.99681	0.99970	1.00580	0.99364
35	5.3359*-02	2.6933*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
36	6.1532*-02	2.7079*+01	1.00050	1.00032	1.00276	1.00070	0.99590	1.00532
37	6.7069*-02	2.7119*+01	0.99631	1.00143	1.00351	1.00140	0.99580	1.00192
38	7.1920*-02	2.7103*+01	0.99791	1.00175	1.00321	1.00150	0.99660	1.00281
39	7.9730*-02	2.7202*+01	0.99825	1.00243	1.00507	1.00220	0.99430	0.99509
40	8.2613*-02	2.7244*+01	0.99836	1.00412	1.00587	1.00320	0.99470	0.99476
41	8.9421*-02	2.7193*+01	0.99834	1.00429	1.00491	1.00310	0.99440	0.99449
42	9.3055*-02	2.7204*+01	0.99825	1.00582	1.00511	1.00370	0.99720	0.99366
43	1.0194*-01	2.7174*+01	0.99004	1.00543	1.00455	1.00360	0.99810	0.99549

INPUT VARIABLES Y,U/UD,T/TD,P/PH

73041301

VOISINET

PROFILE TABULATION

33 POINTS, DELTA AT POINT 32

I	Y	P12/P	P/PO	TU/TOD	H/HD	U/UD	T/TO	RHO/RHOD*U/UD
1	0.0000"+00	1.0000"+00	1.00000	0.29702	0.00000	0.00000	1.31483	0.00000
2	0.3000"-05	1.8168"+00	1.00000	0.51498	0.23299	0.32302	1.92214	0.16805
3	1.4000"-04	2.7647"+00	1.00000	0.60117	0.31768	0.44693	1.97674	0.22609
4	2.4100"-04	3.6130"+00	1.00000	0.65611	0.37491	0.52491	1.96027	0.26778
5	3.1700"-04	4.1983"+00	1.00000	0.68713	0.40927	0.56295	1.93252	0.29441
6	3.9400"-04	4.5521"+00	1.00000	0.70438	0.42863	0.59291	1.91346	0.30986
7	4.7000"-04	4.6956"+00	1.00000	0.71121	0.43623	0.60220	1.90567	0.31600
8	5.7200"-04	4.9381"+00	1.00000	0.72212	0.44476	0.61717	1.89140	0.32631
9	0.4800"-04	5.0282"+00	1.00000	0.72562	0.45131	0.62237	1.88481	0.33020
10	0.2500"-04	5.2426"+00	1.00000	0.73348	0.46400	0.63425	1.86644	0.33949
11	1.1300"-03	5.4615"+00	1.00000	0.75237	0.47465	0.65072	1.87952	0.34622
12	1.3570"-03	5.7163"+00	1.00000	0.76560	0.48674	0.66570	1.87093	0.35589
13	1.6640"-03	5.9896"+00	1.00000	0.77950	0.49938	0.68118	1.86065	0.36610
14	1.8670"-03	6.2213"+00	1.00000	0.78699	0.50984	0.69206	1.84256	0.37559
15	2.1720"-03	6.4603"+00	1.00000	0.79604	0.52040	0.70354	1.82771	0.38493
16	2.4510"-03	6.6634"+00	1.00000	0.80364	0.52921	0.71303	1.81533	0.39278
17	2.5780"-03	6.7771"+00	1.00000	0.80762	0.53408	0.71812	1.80795	0.39720
18	5.5250"-03	8.7539"+00	1.00000	0.85920	0.61247	0.79011	1.68470	0.47477
19	7.9120"-03	1.0339"+01	1.00000	0.89144	0.66868	0.83475	1.55839	0.53565
20	1.0401"-02	1.1967"+01	1.00000	0.91533	0.72182	0.87059	1.45468	0.59848
21	1.2992"-02	1.3503"+01	1.00000	0.93315	0.76857	0.89825	1.36594	0.65761
22	1.5558"-02	1.4922"+01	1.00000	0.94671	0.80936	0.91982	1.29158	0.71217
23	1.8047"-02	1.6280"+01	1.00000	0.95657	0.84657	0.93709	1.22529	0.76479
24	2.0637"-02	1.7611"+01	1.00000	0.96437	0.88152	0.95167	1.16550	0.81653
25	2.3050"-02	1.9618"+01	1.00000	0.97000	0.90705	0.96176	1.12428	0.85545
26	2.5489"-02	1.9418"+01	1.00000	0.97488	0.92682	0.96955	1.09433	0.88597
27	3.0696"-02	2.0867"+01	1.00000	0.98372	0.96161	0.98283	1.04462	0.94085
28	3.5649"-02	2.1776"+01	1.00000	0.98974	0.98280	0.99091	1.01657	0.97476
29	4.0602"-02	2.2393"+01	1.00000	0.99320	0.99695	0.99591	0.99740	0.99800
30	4.5885"-02	2.2723"+01	1.00000	0.99642	1.00443	0.99920	0.98962	1.00966
31	5.0965"-02	2.2501"+01	1.00000	0.99728	0.99940	0.99850	0.99820	1.00030
32	5.6195"-02	2.2527"+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000
33	6.1430"-02	2.2616"+01	1.00000	1.00150	1.00200	1.00120	0.99840	1.00280

INPUT VARIABLES Y,U/UD,T/TO,P/PO

73041502		VOISINET		PROFILE TABULATION		53 POINTS, DELTA AT POINT 50			
I	Y	PT2/P	P/PD	T0/T00	M/10	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.03125	0.23466	0.00000	0.00000	1.13570	0.00000	
2	0.3000+05	1.6257+00	1.03125	0.42528	0.19694	0.26360	1.79150	0.15174	
3	0.9000+05	1.7333+00	1.03125	0.44064	0.21052	0.24420	1.82250	0.16081	
4	1.1400+04	1.8212+00	1.03125	0.45190	0.22057	0.22930	1.84120	0.16764	
5	1.4000+04	2.2048+00	1.03125	0.49304	0.25730	0.35490	1.90260	0.19236	
6	1.9100+04	2.6135+00	1.03125	0.52959	0.28947	0.40310	1.93920	0.21436	
7	2.1600+04	3.0598+00	1.03125	0.56320	0.32020	0.44790	1.95580	0.23611	
8	2.6700+04	3.4847+00	1.03125	0.59213	0.34662	0.48540	1.96110	0.25525	
9	3.1700+04	3.8549+00	1.03125	0.61424	0.36795	0.51460	1.96000	0.27131	
10	3.9400+04	4.4498+00	1.03125	0.64712	0.39972	0.55690	1.94110	0.29586	
11	4.9500+04	4.8460+00	1.03125	0.66624	0.41948	0.58190	1.92430	0.31164	
12	5.2100+04	4.9936+00	1.03125	0.67276	0.42660	0.59060	1.91670	0.31776	
13	0.2200+04	5.1652+00	1.03125	0.68080	0.43472	0.60070	1.90940	0.32443	
14	0.9800+04	5.3440+00	1.03125	0.68829	0.44302	0.61060	1.89960	0.33148	
15	1.2570+03	5.4791+00	1.03125	0.71042	0.46696	0.63890	1.87140	0.35201	
16	1.6890+03	6.3506+00	1.03125	0.73248	0.48706	0.64340	1.85520	0.36876	
17	2.0990+03	6.7501+00	1.03125	0.74819	0.50345	0.66200	1.83510	0.38325	
18	2.2220+03	6.8549+00	1.03125	0.75175	0.50766	0.66650	1.82670	0.38713	
19	2.4010+03	6.9796+00	1.03125	0.75731	0.51262	0.66940	1.82440	0.39138	
20	2.6290+03	7.1530+00	1.03125	0.76376	0.51944	0.66990	1.81550	0.39756	
21	2.7300+03	7.2681+00	1.03125	0.76671	0.52392	0.70420	1.80660	0.40197	
22	2.9080+03	7.3780+00	1.03125	0.77050	0.52816	0.70870	1.80050	0.40591	
23	3.1620+03	7.6042+00	1.03125	0.77652	0.53678	0.71700	1.78420	0.41442	
24	3.4670+03	7.7977+00	1.03125	0.78253	0.54397	0.72430	1.77290	0.42131	
25	3.7210+03	7.9773+00	1.03125	0.78779	0.55070	0.73090	1.76150	0.42790	
26	4.0770+03	8.4051+00	1.03125	0.79457	0.55903	0.73910	1.74800	0.43604	
27	4.3310+03	8.4165+00	1.03125	0.79890	0.56656	0.74560	1.73190	0.44396	
28	5.6260+03	8.2781+00	1.03125	0.82170	0.59667	0.77340	1.68010	0.47471	
29	6.7690+03	8.0031+01	1.03125	0.84167	0.62107	0.79580	1.64180	0.49986	
30	8.0390+03	8.0000+01	1.03125	0.85997	0.64815	0.81800	1.59290	0.52961	
31	8.9790+03	1.1441+01	1.03125	0.87242	0.66607	0.83240	1.56180	0.54963	
32	1.0859+02	1.2616+01	1.03125	0.89348	0.70089	0.85790	1.49820	0.59051	
33	1.2154+02	1.3361+01	1.03125	0.90501	0.72209	0.87220	1.45900	0.61649	
34	1.2992+02	1.3875+01	1.03125	0.91072	0.73637	0.88060	1.43010	0.63500	
35	1.3830+02	1.4396+01	1.03125	0.91795	0.75053	0.88950	1.40460	0.65306	
36	1.5024+02	1.5090+01	1.03125	0.92665	0.76904	0.90050	1.37110	0.67729	
37	1.7081+02	1.6308+01	1.03001	0.93831	0.80045	0.91700	1.31240	0.71969	
38	1.8834+02	1.7425+01	1.02877	0.94754	0.82821	0.93040	1.26200	0.75845	
39	2.0155+02	1.8272+01	1.02795	0.95291	0.84864	0.93920	1.22490	0.78825	
40	2.2517+02	1.9676+01	1.02630	0.96145	0.88147	0.95270	1.16610	0.83705	
41	2.4930+02	2.0862+01	1.02465	0.96780	0.90832	0.96290	1.12380	0.87794	
42	2.8207+02	2.2172+01	1.02248	0.97431	0.93703	0.97320	1.07870	0.92248	
43	3.1001+02	2.3064+01	1.02032	0.98024	0.95610	0.98060	1.03190	0.95116	
44	3.4760+02	2.3899+01	1.01598	0.98563	0.97362	0.98720	1.02810	0.97557	
45	3.7173+02	2.4311+01	1.01320	0.98893	0.98214	0.99070	1.01750	0.98651	
46	3.9611+02	2.4546+01	1.01042	0.99132	0.98778	0.99310	1.01080	0.99272	
47	4.1440+02	2.4794+01	1.00835	0.99333	0.99203	0.99500	1.00800	0.99733	
48	4.4183+02	2.5026+01	1.00516	0.99653	0.99680	0.99760	1.00160	1.00114	
49	4.6723+02	2.5110+01	1.00227	0.99884	0.99843	0.99910	1.00130	1.00007	
50	4.8654+02	2.5186+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
51	5.1194+02	2.5303+01	0.99711	1.00243	1.00235	1.00170	0.99870	1.00011	
52	5.3556+02	2.5325+01	0.99484	1.00405	1.00280	1.00260	0.99960	0.99783	
53	5.6401+02	2.5322+01	0.99577	1.00527	1.00275	1.00320	1.00090	0.99806	


INPUT VARIABLES Y, U/UD, T/TD, P/PW

73041303		VOISINET		PROFILE TABULATION		52 POINTS, DELTA AT POINT 44			
I	Y	PT2/P	P/PD	T0/T0D	H/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	1.00000	0.22058	0.00000	0.00000	1.11770	0.00000	
2	6.3000-05	1.4222+00	1.00000	0.38614	0.16134	0.21460	1.76930	0.12129	
3	1.1000-04	1.5534+00	1.00000	0.41077	0.18159	0.24600	1.83530	0.13404	
4	1.9100-04	2.1567+00	1.00000	0.48867	0.24596	0.34680	1.98800	0.17445	
5	2.4100-04	2.7638+00	1.00000	0.54489	0.29173	0.41780	2.05110	0.20370	
6	3.1700-04	3.6426+00	1.00000	0.60787	0.34580	0.49780	2.07230	0.24022	
7	4.1900-04	4.2679+00	1.00000	0.64481	0.37923	0.54450	2.06150	0.26413	
8	4.9500-04	4.6378+00	1.00000	0.66400	0.39762	0.56900	2.04780	0.27786	
9	5.9700-04	4.8469+00	1.00000	0.67464	0.40763	0.58220	2.03990	0.28541	
10	7.2400-04	5.1466+00	1.00000	0.68806	0.42155	0.59970	2.02380	0.29632	
11	9.0200-04	5.3952+00	1.00000	0.70390	0.43275	0.61580	2.02490	0.30411	
12	1.1560-03	5.5930+00	1.00000	0.71617	0.44145	0.62810	2.02440	0.31026	
13	1.3360-03	5.8295+00	1.00000	0.72259	0.45162	0.63890	2.00130	0.31924	
14	1.6410-03	6.1383+00	1.00000	0.72949	0.46497	0.65180	1.98550	0.33112	
15	1.8690-03	6.4064+00	1.00000	0.73537	0.47531	0.66250	1.94110	0.34130	
16	2.1490-03	6.6456+00	1.00000	0.74101	0.48507	0.67190	1.91870	0.35019	
17	2.3770-03	6.8533+00	1.00000	0.74629	0.49321	0.68000	1.90090	0.35773	
18	3.4700-03	7.5925+00	1.00000	0.77332	0.52114	0.71110	1.86190	0.38192	
19	4.6150-03	8.3699+00	1.00000	0.79685	0.54879	0.73930	1.81480	0.40737	
20	5.8600-03	9.1431+00	1.00000	0.81742	0.57529	0.76440	1.76580	0.43297	
21	7.2850-03	9.9847+00	1.00000	0.83944	0.60263	0.78970	1.71720	0.45998	
22	8.9290-03	1.0712+01	1.00000	0.85629	0.62530	0.80930	1.67510	0.48314	
23	1.0284-02	1.1687+01	1.00000	0.87502	0.65442	0.83220	1.61710	0.51462	
24	1.1735-02	1.2539+01	1.00000	0.88911	0.67886	0.84990	1.56740	0.54224	
25	1.3310-02	1.3351+01	1.00000	0.90263	0.70135	0.86590	1.52430	0.56606	
26	1.5065-02	1.4170+01	1.00000	0.91484	0.72860	0.88260	1.46740	0.60147	
27	1.6360-02	1.5078+01	1.00000	0.92423	0.74692	0.89490	1.43260	0.62404	
28	1.8141-02	1.6004+01	1.00000	0.93435	0.77025	0.90720	1.38720	0.65378	
29	1.9997-02	1.7075+01	1.00000	0.94293	0.79639	0.92010	1.33480	0.68932	
30	2.1293-02	1.7715+01	1.00000	0.94885	0.81158	0.92780	1.30690	0.70992	
31	2.3200-02	1.8716+01	1.00000	0.95515	0.83482	0.93790	1.26220	0.74307	
32	2.5540-02	1.9936+01	1.00000	0.96292	0.86229	0.94950	1.21250	0.78309	
33	2.7295-02	2.0614+01	1.00000	0.96717	0.87716	0.95560	1.18680	0.80519	
34	2.9863-02	2.1585+01	1.00000	0.97187	0.89809	0.96330	1.15050	0.83729	
35	3.2355-02	2.2390+01	1.00000	0.97557	0.91504	0.96930	1.12210	0.86383	
36	3.4770-02	2.2966+01	1.00000	0.97853	0.92699	0.97360	1.10310	0.88260	
37	3.7846-02	2.3618+01	1.00000	0.98180	0.94033	0.97830	1.08240	0.90382	
38	4.0617-02	2.4300+01	1.00000	0.98589	0.95408	0.98340	1.06240	0.92564	
39	4.2906-02	2.4896+01	1.00000	0.98899	0.96799	0.98850	1.03890	0.93097	
40	4.4737-02	2.4875+01	1.00000	0.99015	0.96952	0.99800	1.04710	0.94356	
41	4.7584-02	2.5306+01	1.00000	0.99477	0.97401	0.99210	1.03750	0.95624	
42	4.9720-02	2.5481+01	1.00000	0.99553	0.97744	0.99320	1.03250	0.96194	
43	5.2339-02	2.6404+01	1.00000	0.99846	0.99532	0.99830	1.00600	0.99235	
44	5.4755-02	2.6649+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
45	5.7374-02	2.6412+01	1.00000	1.00020	0.99547	0.99920	1.00750	0.99176	
46	5.9789-02	2.6297+01	1.00000	1.00188	0.99326	0.99960	1.01280	0.98697	
47	6.2408-02	2.6244+01	1.00000	1.00230	0.99274	0.99960	1.01490	0.98492	
48	6.5001-02	2.6249+01	1.00000	1.00246	0.99233	0.99970	1.01490	0.98502	
49	6.7874-02	2.6285+01	1.00000	1.00195	0.99302	0.99960	1.01330	0.98648	
50	7.1204-02	2.6380+01	1.00000	1.00165	0.99485	1.00000	1.01200	0.98893	
51	7.4102-02	2.6392+01	1.00000	1.00047	0.99431	1.00110	1.01170	0.98757	
52	7.6599-02	2.6267+01	1.00000	1.00312	0.99268	1.00010	1.01580	0.98532	

INPUT VARIABLES Y,U/UD,T/TD,P/PN

73041304		VOISINET		PROFILE TABULATION		55 POINTS, DELTA AT POINT 44			
I	Y	PTZ/P	P/PD	T0/T00	U/U0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0090*+00	1.0000*+00	0.98078	0.23706	0.00000	0.00000	1.20060	0.00000	
2	0.3000*-05	1.4271*+00	0.98078	0.40610	0.17786	0.24010	1.82240	0.12922	
3	1.4000*-04	2.3248*+00	0.98078	0.49889	0.25978	0.36590	1.98280	0.15094	
4	1.6500*-04	2.7305*+00	0.98078	0.53292	0.28953	0.41040	2.01310	0.20014	
5	2.4100*-04	3.4836*+00	0.98078	0.58514	0.33683	0.47970	2.02820	0.23197	
6	3.1700*-04	3.9958*+00	0.98078	0.61519	0.36520	0.51910	2.02040	0.25199	
7	3.6800*-04	4.4776*+00	0.98078	0.64078	0.38989	0.55220	2.00590	0.27010	
8	4.7000*-04	4.7482*+00	0.98078	0.65580	0.40545	0.57210	1.99100	0.28182	
9	6.7300*-04	5.2801*+00	0.98078	0.67676	0.42774	0.59970	1.96570	0.29922	
10	1.0030*-03	5.5985*+00	0.98078	0.68946	0.44183	0.61650	1.94700	0.31055	
11	1.2320*-03	5.7561*+00	0.98078	0.70051	0.44863	0.62670	1.93140	0.31498	
12	1.4600*-03	5.9749*+00	0.98078	0.71265	0.45791	0.63920	1.94860	0.32172	
13	1.6890*-03	6.1751*+00	0.98078	0.72308	0.46623	0.65010	1.94430	0.32793	
14	1.9690*-03	6.4376*+00	0.98078	0.73304	0.47692	0.66240	1.92910	0.33677	
15	2.1970*-03	6.6545*+00	0.98078	0.73993	0.48557	0.67170	1.91360	0.34427	
16	4.1020*-03	8.0263*+00	0.98078	0.78385	0.53701	0.72580	1.82670	0.38967	
17	5.0420*-03	8.6198*+00	0.98078	0.80132	0.55778	0.74670	1.79210	0.40865	
18	6.3120*-03	9.3980*+00	0.98078	0.82134	0.58389	0.77100	1.74360	0.43369	
19	7.6100*-03	1.0217*+01	0.98078	0.84118	0.61014	0.79440	1.69520	0.45961	
20	9.7920*-03	1.1357*+01	0.98078	0.86357	0.64522	0.82240	1.62460	0.48649	
21	1.1087*-02	1.2069*+01	0.98078	0.87627	0.66569	0.83790	1.58430	0.51871	
22	1.2662*-02	1.2977*+01	0.98078	0.88996	0.69131	0.85560	1.53180	0.54782	
23	1.4186*-02	1.3840*+01	0.98078	0.90162	0.71475	0.87180	1.48420	0.57543	
24	1.6167*-02	1.4923*+01	0.98078	0.91372	0.74318	0.88750	1.42610	0.61036	
25	1.7977*-02	1.5856*+01	0.98078	0.92387	0.76687	0.90090	1.38010	0.64023	
26	2.0256*-02	1.7053*+01	0.98078	0.93458	0.79610	0.91590	1.32340	0.67867	
27	2.1933*-02	1.7978*+01	0.98078	0.94220	0.81800	0.92650	1.28240	0.70830	
28	2.3609*-02	1.8786*+01	0.98078	0.94839	0.83668	0.93510	1.24410	0.73423	
29	2.6459*-02	2.0206*+01	0.98117	0.95690	0.86852	0.94820	1.19190	0.78056	
30	2.8867*-02	2.1245*+01	0.98225	0.96436	0.89110	0.96480	1.15530	0.81433	
31	3.1255*-02	2.2325*+01	0.98323	0.96948	0.91397	0.98600	1.11710	0.85024	
32	3.3642*-02	2.3695*+01	0.98421	0.97345	0.92994	0.97200	1.09250	0.87565	
33	3.6385*-02	2.5775*+01	0.98529	0.97810	0.94278	0.97700	1.07390	0.89438	
34	3.9510*-02	2.8532*+01	0.98666	0.98195	0.95900	0.98250	1.04960	0.92354	
35	4.1643*-02	2.4915*+01	0.98754	0.98388	0.96662	0.98810	1.03860	0.93667	
36	4.3929*-02	2.5362*+01	0.98843	0.98718	0.97542	0.98860	1.02720	0.95128	
37	4.6419*-02	2.5767*+01	0.98951	0.98991	0.98333	0.99160	1.01690	0.96484	
38	4.9695*-02	2.6084*+01	0.99088	0.99281	0.98946	0.99430	1.00980	0.97567	
39	5.2083*-02	2.6195*+01	0.99186	0.99475	0.99454	0.99570	1.00630	0.97966	
40	5.4674*-02	2.6246*+01	0.99294	0.99445	0.99258	0.99600	1.00690	0.98219	
41	5.6883*-02	2.6316*+01	0.99382	0.99442	0.99392	0.99700	1.00620	0.98473	
42	5.9423*-02	2.6367*+01	0.99490	0.99722	0.99492	0.99760	1.00540	0.98718	
43	6.1934*-02	2.6638*+01	0.99588	0.99836	1.00010	0.99920	0.99820	0.99688	
D 44	7.1844*-02	2.6633*+01	1.00000	1.00000	1.00000	1.00000	1.00000	1.00000	
45	7.4689*-02	2.6651*+01	0.99784	1.00066	1.00035	1.00040	1.00010	0.99814	
46	7.7132*-02	2.6646*+01	0.99853	1.00110	1.00025	1.00060	1.00070	0.99843	
47	7.9667*-02	2.6638*+01	0.99909	1.00196	1.00010	1.00100	1.00180	0.99901	
48	8.2664*-02	2.6664*+01	0.99958	1.00216	1.00060	1.00120	1.00120	0.99978	
49	8.4620*-02	2.6659*+01	0.99935	1.00260	1.00000	1.00140	1.00180	0.99955	
50	8.7135*-02	2.6586*+01	1.00586	1.00256	0.99910	1.00110	1.00400	1.00298	
51	8.9344*-02	2.6674*+01	0.99953	1.00329	1.00080	1.00180	1.00200	0.99933	
52	4.1707*-02	2.6724*+01	0.99931	1.00371	1.00175	1.00220	1.00090	0.99954	
53	4.0753*-02	2.6703*+01	0.99235	1.00427	1.00135	1.00240	1.00210	0.99265	
54	1.0034*-01	2.6745*+01	0.98745	1.00516	1.00215	1.00300	1.00170	0.98873	
55	1.0303*-01	2.6787*+01	0.98284	1.00605	1.00295	1.00360	1.00130	0.98509	

INPUT VARIABLES Y,U/UD,T/TD,P/PH

	$M : 9 - 10$ $R \text{ THETA} \times 10^{-3} : 1 - 12$ $TW / TR : 1.0$	7305
		ZPG - AH
Axially symmetric blow down tunnel. Running time 5 s. $D = 1.52 \text{ m}$. $2.8 < PD < 13.8 \text{ MN/m}^2$. $T_0 : 300 \text{ K}$, Helium. $0.9 < RE/m \times 10^{-6} < 5$.		
WATSON R.D., HARRIS J.E. and ANDEPS J.B., 1973. Measurements in a transitional / turbulent Mach 10 boundary layer at high Reynolds numbers. AIAA P 73-165. And Watson R.D., private communications.		

- 1 The test boundary layer was formed on a flat plate ($L = 2.36, W = 1.015 \text{ m}$) placed at 5° negative incidence in the working section of the Mach 20 wind tunnel described in Watson and Bushnell (1971). The leading edge ($X = 0$) was 0.13 mm thick and chamfered so that the under side was at 17° to the free stream flow. It was positioned 0.127 m below the tunnel centre line, 0.425 m downstream of the end of the nozzle. The test zone extended from $X = 0.74$ to $X = 2.11 \text{ m}$. End-plates were mounted on the surface 0.305 m to either side of the centre line. The surface consisted of steel plates 4.76 mm thick finished to $0.8 \mu\text{m r.m.s.}$ forming interchangeable instrument sections 153 mm (E) wide along the centre line. The surface was not actively cooled. The transition zone was located from heat transfer measurements. In all cases transition commenced at about $X = 0.61 \text{ m}$ and extended over the first three measuring stations to between $X = 1.4$ and 2.0 m . The flow was fully turbulent at the last station ($X = 2.11 \text{ m}$) though by no means in equilibrium even for the highest RE/m case. No trip was used. Preliminary oil-flow tests showed that, with the end-plates fitted, no discernable surface-flow divergence was present over the central 0.15 m wide instrumented strip.
- 2 Wall static pressure was measured at static tapings of diameter 2.29 mm . The wall temperature was obtained by thermocouples. Heat transfer rates were found using the transient technique from the rate of change of wall temperature. Floating element balances (Kistler model 322, serial 121) were installed at each profile location to measure the wall shear stress. Profile traverses were made with Pitot, static and total temperature probes. The FPP ($h_1 = 1, b_1 = 3.02, l = 50.8 \text{ mm}$) was formed from flattened 1.52 mm tube. The SPP was a CPP ($\alpha = 42.5^\circ, d = 3.2, l_n = 12.2, l = 50.8^+ \text{ mm}$) and because of wall interference effects could only be used in the outer part of the layer. Pitot-static values gave an edge Mach number which matched that calculated using the wall pressure and values from an exterior flow field calculation so that it was assumed that $P = P_W = P_D$. The TTP was an STP with a resistive temperature sensor ($h_1 = 1.6, b_1 = 4.35, l = 10.2 \text{ mm}$) and was used only at the last ($X = 2.11 \text{ m}$) station (see Weinstein 1971). All sets of profile measurements were made on a common normal.
- 3 The authors have reduced the profile data on the assumption of no normal pressure gradient and with the linear Crocco total temperature distribution. The static pressure at a profile normal was measured with the probe well clear of the surface. When this was not possible, due to instrument failure or the presence of a skin-friction gauge, the value was determined from the tunnel stagnation pressure and the results of earlier measurements. The heat transfer measurements showed that the model temperature did not change significantly during a run, so that the wall temperature measured at a single station at the start of the run was taken to apply to all stations. The authors found, particularly in the transitional zone, that probe interference effects were evidently large, the wall static pressure rising by as much as 80% as a probe approached the wall. In the absence of a rational correction procedure, no profile corrections were applied. Viscosity values were determined from the power law $\mu = 5.0277 \times 10^{-7} T^{0.647} \text{ kg/ms}$.
- 4 The editors have presented the profile data replacing the authors' temperature velocity correlation by the Crocco - Van Driest relationship. The edge Mach number has been interpolated on the basis of tunnel reservoir pressure for each station. Adjustments from neighbouring measured points were less than 0.5% except for profile 0502 where it was necessary to extrapolate, the resulting adjustment being 1.5% . The edge point is that selected by the authors, and the edge stagnation pressure (the source paper tabulates tunnel values)

has been calculated using the authors' D2 and RED2D values, with the authors' viscosity law. We have then replaced this with the helium viscosity law used throughout the catalogue. The different viscosity value causes the differences that can be observed between their RED2D values and ours. We have interpolated the CF values for each station, also on the basis of tunnel reservoir pressure. The biggest adjustment was 3 % for run 0504.

- 13 The five sets of four profiles are distinguished by increasing values of unit Reynolds number. Measured
- 14 TO profiles corresponding to runs at station 4 for series 02-05 are given in section D. Interpolated CF values are associated with the profiles. Heat transfer measurements were made, but with the small temperature differences involved the heat flux values are not very accurate. We have therefore regarded the flow as adiabatic.
- 5 DATA 7305 0101-0504. Pitot profiles. $NX = 4$. CF from FEB. Some additional TO profiles. CQ measured but not presented (near zero).

15 Editors' comments

The entry gives a very clear description of the development of a layer through the transition region. The development is free of history effects, and transition is unforced. In this respect it can be regarded as an extension of the data of Fischer et al. - CAT 7103 to higher Mach numbers. The value of the measurements is greatly enhanced by the provision for direct wall shear stress measurements.

Measurements extend within the momentum-deficit peak, and the profile is described at close intervals. Values near the wall should not be given too great emphasis as no corrections were applied, and it is far from certain how they should be.

CAT 7305 WATSON BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD TOD*	TH/TR* PH/PD* SH * D2	RED2W RED2D	CF * CQ PI2	H12 H32 H42	H12K H32K D2K	PH TN UD	PD TD TR
73050101 7.4200*-01 INFINITE	9.5800 1.1395*+06 3.0000*+02	1.0000 1.0000 0.0000	1.6983*+02 1.4911*+03 1.7811*-04	1.9900*-04 NM 0.0000*+00	74.0466 1.7547 0.1988	2.3571 1.5983 2.0118*-03	2.0341*+02 2.6974*+02 1.7374*+03	2.0341*+02 9.4914*+00 2.6974*+02
73050102 9.9600*-01 INFINITE	8.9500 9.2435*+05 3.0000*+02	1.0000 1.0000 0.0000	2.3371*+02 1.8771*+03 2.4878*-04	2.2300*-04 NM 0.0000*+00	65.3323 1.7296 0.1736	2.1673 1.5838 2.7477*-03	2.2917*+02 2.6993*+02 1.7334*+03	2.2917*+02 1.0825*+01 2.6993*+02
73050103 1.2500*+00 INFINITE	9.7000 1.1949*+06 3.0000*+02	1.0000 1.0000 0.0000	2.4149*+02 2.1562*+03 2.5031*-04	2.6200*-04 NM 0.0000*+00	65.6644 1.8173 0.1839	1.5072 1.7136 2.4239*-03	2.0083*+02 2.0976*+02 1.7381*+03	2.0083*+02 9.2653*+00 2.0976*+02
73050104 2.1100*+00 INFINITE	9.2000 1.1694*+06 3.0000*+02	1.0000 1.0000 0.0000	4.1494*+02 3.4534*+03 3.7767*-04	4.3400*-04 NM 0.0000*+00	64.4725 1.8477 0.1842	2.5962 1.6022 2.5749*-03	2.5386*+02 2.6987*+02 1.7351*+03	2.5386*+02 1.0264*+01 2.6987*+02
73050201 7.4200*-01 INFINITE	9.7900 2.4954*+06 3.0000*+02	1.0000 1.0000 0.0000	2.2749*+02 2.0569*+03 1.5955*-04	1.4800*-04 NM 0.0000*+00	86.7190 1.6044 0.1656	2.1385 1.6371 2.2174*-03	4.0103*+02 2.6975*+02 1.7386*+03	4.0103*+02 9.1008*+00 2.6975*+02
73050202 9.9600*-01 INFINITE	9.5100 2.1986*+06 3.0000*+02	1.0000 1.0000 0.0000	3.1272*+02 2.7188*+03 1.6645*-04	2.3000*-04 NM 0.0000*+00	66.4819 1.8097 0.1900	1.9147 1.6980 1.5492*-03	4.0664*+02 2.6980*+02 1.7370*+03	4.0664*+02 9.2653*+00 2.6980*+02
73050203 1.2500*+00 INFINITE	9.6800 2.3260*+06 3.0000*+02	1.0000 1.0000 0.0000	3.0568*+02 2.7217*+03 1.6181*-04	3.4700*-04 NM 0.0000*+00	83.8491 1.9433 0.2039	7.3594 1.9263 6.5300*-04	3.9484*+02 2.6977*+02 1.7380*+03	3.9484*+02 9.3024*+00 2.6977*+02
73050204 2.1100*+00 INFINITE	9.7400 2.7820*+06 3.0000*+02	1.0000 1.0000 0.0000	6.6240*+02 5.9475*+03 2.9841*-04	3.3700*-04 NM 0.0000*+00	78.7582 1.8497 0.1840	4.4223 1.2727 1.7707*-03	4.5832*+02 2.6976*+02 1.7383*+03	4.5832*+02 9.1916*+00 2.6976*+02
73050301 7.4200*-01 INFINITE	9.8500 3.6491*+06 3.0000*+02	1.0000 1.0000 0.0000	3.5236*+02 3.2129*+03 1.2499*-04	1.3500*-04 NM 0.0000*+00	75.9805 1.7498 0.1849	2.3869 1.6181 1.2522*-03	5.6932*+02 2.6974*+02 1.7339*+03	5.6932*+02 8.9433*+00 2.6974*+02
73050302 9.9600*-01 INFINITE	9.7300 3.2888*+06 3.0000*+02	1.0000 1.0000 0.0000	2.7034*+02 2.4239*+03 1.0272*-04	2.6800*-04 NM 0.0000*+00	72.7464 1.8030 0.2011	2.1827 1.6932 1.0526*-03	5.4453*+02 2.6976*+02 1.7382*+03	5.4453*+02 9.2100*+00 2.6976*+02
73050303 1.2500*+00 INFINITE	9.8000 3.3954*+06 3.0000*+02	1.0000 1.0000 0.0000	4.4400*+02 4.0202*+03 1.6681*-04	3.7800*-04 NM 0.0000*+00	63.4262 1.9140 0.1937	1.5419 1.8531 9.2138*-04	5.4297*+02 2.6974*+02 1.7386*+03	5.4297*+02 9.0824*+00 2.6974*+02
73050304 2.1100*+00 INFINITE	9.8300 4.0599*+06 3.0000*+02	1.0000 1.0000 0.0000	1.0786*+03 9.8070*+03 3.4188*-04	3.0400*-04 NM 0.0000*+00	62.4785 1.9222 0.2080	1.4429 1.8800 1.7636*-03	6.3969*+02 2.6974*+02 1.7386*+03	6.3969*+02 9.0291*+00 2.6974*+02
73050401 7.4200*-01 INFINITE	9.9400 4.7452*+06 3.0000*+02	1.0000 1.0000 0.0000	3.7077*+02 3.4234*+03 1.0382*-04	1.2800*-04 NM 0.0000*+00	77.3118 1.7884 0.1865	2.2098 1.6145 1.1158*-03	7.0838*+02 2.6972*+02 1.7394*+03	7.0838*+02 8.9363*+00 2.6972*+02
73050402 9.9600*-01 INFINITE	9.6800 4.2175*+06 3.0000*+02	1.0000 1.0000 0.0000	3.7548*+02 3.3432*+03 1.0962*-04	3.0000*-04 NM 0.0000*+00	70.3553 1.8260 0.1948	2.0422 1.7834 1.0508*-03	7.1593*+02 2.6977*+02 1.7380*+03	7.1593*+02 9.3024*+00 2.6977*+02
73050403 1.2500*+00 INFINITE	10.0200 4.8915*+06 3.0000*+02	1.0000 1.0000 0.0000	5.4825*+02 5.1191*+03 1.5240*-04	3.6000*-04 NM 0.0000*+00	67.7094 1.9145 0.1960	1.8090 1.8608 8.7302*-04	7.0237*+02 2.6970*+02 1.7398*+03	7.0237*+02 8.6988*+00 2.6970*+02
73050404 2.1100*+00 INFINITE	10.0200 5.5879*+06 3.0000*+02	1.0000 1.0000 0.0000	1.3010*+03 1.2147*+04 3.1656*-04	2.7300*-04 NM 0.0000*+00	65.8399 1.9150 0.2078	1.5704 1.8594 1.7998*-03	8.0237*+02 2.6970*+02 1.7398*+03	8.0237*+02 8.6994*+00 2.6970*+02
73050501 7.4200*-01 INFINITE	10.1600 6.1859*+06 3.0000*+02	1.0000 1.0000 0.0000	4.6204*+02 4.3994*+03 1.0570*-04	1.2200*-04 NM 0.0000*+00	77.1491 1.8063 0.1844	2.0302 1.6520 1.1194*-03	8.3036*+02 2.6968*+02 1.7405*+03	8.3036*+02 8.4684*+00 2.6968*+02
73050502 9.9600*-01 INFINITE	9.8400 5.4435*+06 3.0000*+02	1.0000 1.0000 0.0000	5.2842*+02 4.8114*+03 1.2529*-04	3.0900*-04 NM 0.0000*+00	75.6685 1.8792 0.1958	3.1484 1.7034 5.6721*-04	8.5348*+02 2.6974*+02 1.7388*+03	8.5348*+02 9.0114*+00 2.6974*+02
73050503 1.2500*+00 INFINITE	10.3100 6.6939*+06 3.0000*+02	1.0000 1.0000 0.0000	6.7762*+02 6.5889*+03 1.0944*-04	3.2800*-04 NM 0.0000*+00	69.0221 1.9250 0.2133	1.5806 1.8854 8.0894*-04	8.3678*+02 2.6966*+02 1.7412*+03	8.3678*+02 8.2305*+00 2.6966*+02
73050504 2.1100*+00 INFINITE	10.3100 7.5576*+06 3.0000*+02	1.0000 1.0000 0.0000	1.5502*+03 1.5074*+04 3.0280*-04	2.4600*-04 NM 0.0000*+00	70.2460 1.9045 0.1999	1.5612 1.8184 1.9432*-03	9.4475*+02 2.6966*+02 1.7412*+03	9.4475*+02 8.2305*+00 2.6966*+02

PD,POD CALCULATED WITH AUTHOR'S MUE-LAW FROM RED2,DELTA2 (AUTHOR) = TRAPEZOIDAL RULE FOR RUN 0203

73050101		WATSON		PROFILE TABULATION		33 POINTS, DELTA AT POINT 33			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.88673	0.00000	0.00000	20.02710	0.00000	
2	1.0222*+03	1.0401*+00	NM	0.88851	0.02386	0.12536	27.60236	0.00454	
3	1.7870*+03	1.1981*+00	NM	0.89402	0.04951	0.25381	26.28598	0.00966	
4	3.1327*+03	1.9547*+00	NM	0.91181	0.10024	0.47062	22.04094	0.02135	
5	4.1685*+03	2.1555*+00	NM	0.91505	0.10842	0.50003	21.26964	0.02351	
6	5.0314*+03	2.8062*+00	NM	0.92360	0.13010	0.57053	19.22475	0.02467	
7	6.4005*+03	4.4918*+00	NM	0.93905	0.17239	0.67965	15.54267	0.04373	
8	7.2342*+03	5.6326*+00	NM	0.94644	0.19560	0.72607	13.77914	0.05269	
9	7.9131*+03	8.2055*+00	NM	0.95816	0.23964	0.79415	10.98181	0.07231	
10	8.7579*+03	1.0305*+01	NM	0.96469	0.27026	0.82965	9.42386	0.08804	
11	9.4968*+03	1.5338*+01	NM	0.97471	0.33228	0.88131	7.03493	0.12528	
12	1.0104*+02	2.1601*+01	NM	0.98195	0.39796	0.91685	5.30783	0.17273	
13	1.0934*+02	2.7792*+01	NM	0.98607	0.45035	0.93649	4.32409	0.21657	
14	1.1450*+02	3.4727*+01	NM	0.98927	0.50425	0.95146	3.56034	0.26724	
15	1.2005*+02	4.2176*+01	NM	0.99165	0.55634	0.96243	2.99262	0.32160	
16	1.2147*+02	5.2471*+01	NM	0.99391	0.62120	0.97276	2.45221	0.39669	
17	1.2545*+02	5.8893*+01	NM	0.99495	0.68641	0.97747	2.20399	0.44350	
18	1.3033*+02	6.5819*+01	NM	0.99586	0.69634	0.98157	1.98704	0.48199	
19	1.3167*+02	7.1708*+01	NM	0.99651	0.72702	0.98446	1.83357	0.53691	
20	1.3532*+02	8.0083*+01	NM	0.99727	0.76856	0.98786	1.65211	0.59794	
21	1.4066*+02	8.8003*+01	NM	0.99786	0.80587	0.99051	1.51072	0.65565	
22	1.4670*+02	9.4938*+01	NM	0.99830	0.83718	0.99247	1.40541	0.70618	
23	1.5243*+02	1.0048*+02	NM	0.99863	0.86308	0.99395	1.32624	0.74945	
24	1.5930*+02	1.0636*+02	NM	0.99891	0.88634	0.99517	1.26063	0.78942	
25	1.6465*+02	1.1185*+02	NM	0.99916	0.90901	0.99627	1.20122	0.82934	
26	1.6992*+02	1.1587*+02	NM	0.99932	0.92526	0.99702	1.16111	0.85867	
27	1.7868*+02	1.1991*+02	NM	0.99948	0.94134	0.99772	1.12337	0.88615	
28	1.8745*+02	1.2347*+02	NM	0.99961	0.95525	0.99829	1.09216	0.91406	
29	2.0051*+02	1.2661*+02	NM	0.99972	0.96736	0.99878	1.06601	0.93693	
30	2.1259*+02	1.3026*+02	NM	0.99984	0.98123	0.99931	1.03717	0.96350	
31	2.2068*+02	1.3265*+02	NM	0.99993	0.99100	0.99967	1.01759	0.98239	
32	2.3305*+02	1.3458*+02	NM	0.99998	0.99743	0.99991	1.00498	0.99495	
D 33	2.4596*+02	1.3527*+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050102		WATSON		PROFILE TABULATION		41 POINTS, DELTA AT POINT 41			
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000*+00	1.0000*+00	NM	0.89964	0.00000	0.00000	24.93289	0.00000	
2	2.9187*+03	1.8947*+00	NM	0.92132	0.10453	0.46473	19.76409	0.02351	
3	4.1413*+03	2.1317*+00	NM	0.92480	0.11507	0.50070	18.93280	0.02645	
4	5.1901*+03	2.1856*+00	NM	0.92553	0.11727	0.50793	18.75850	0.02708	
5	6.0008*+03	3.0873*+00	NM	0.93557	0.14790	0.59832	16.36513	0.03656	
6	6.7542*+03	3.8138*+00	NM	0.94177	0.16794	0.64793	14.88557	0.04353	
7	8.1921*+03	5.5986*+00	NM	0.95300	0.20867	0.72914	12.20925	0.05972	
8	9.3981*+03	7.0244*+00	NM	0.95939	0.23606	0.77160	10.66389	0.07222	
9	1.0479*+02	8.9648*+00	NM	0.96589	0.26084	0.81250	9.13362	0.08896	
10	1.1354*+02	1.0555*+01	NM	0.96996	0.29293	0.83703	8.16506	0.10251	
11	1.1721*+02	1.2463*+01	NM	0.97382	0.31945	0.85973	7.24305	0.11870	
12	1.2024*+02	1.4541*+01	NM	0.97714	0.34601	0.87878	6.45052	0.13623	
13	1.2326*+02	1.6618*+01	NM	0.97981	0.37066	0.89378	5.81448	0.15372	
14	1.3084*+02	2.6475*+01	NM	0.98758	0.47030	0.93608	3.96171	0.23628	
15	1.2692*+02	1.8699*+01	NM	0.98200	0.39380	0.90591	5.29201	0.17118	
16	1.2918*+02	2.0945*+01	NM	0.98396	0.41734	0.91663	4.82403	0.19001	
17	1.3141*+02	2.3707*+01	NM	0.98595	0.44458	0.92735	4.35099	0.21314	
18	1.4057*+02	3.0802*+01	NM	0.98962	0.50789	0.94647	3.47564	0.27243	
19	1.4276*+02	3.4251*+01	NM	0.99092	0.53598	0.95368	3.16598	0.30123	
20	1.4493*+02	3.8044*+01	NM	0.99210	0.56525	0.95984	2.88348	0.33288	
21	1.4944*+02	4.2789*+01	NM	0.99350	0.59929	0.96603	2.59838	0.37178	
22	1.5211*+02	4.8052*+01	NM	0.99441	0.63605	0.97173	2.33404	0.41633	
23	1.5481*+02	5.3051*+01	NM	0.99526	0.66661	0.97608	2.13118	0.45800	
24	1.5577*+02	5.7009*+01	NM	0.99583	0.69331	0.97901	1.99398	0.49098	
25	1.6155*+02	6.0477*+01	NM	0.99628	0.71425	0.98128	1.88751	0.51988	
26	1.6363*+02	6.7020*+01	NM	0.99700	0.75217	0.98495	1.71474	0.57440	
27	1.6720*+02	7.2710*+01	NM	0.99753	0.78365	0.98763	1.58834	0.62180	
28	1.7089*+02	7.4509*+01	NM	0.99785	0.80399	0.98921	1.51383	0.65345	
29	1.7651*+02	8.1004*+01	NM	0.99818	0.82740	0.99089	1.43421	0.69089	
30	1.8155*+02	8.4294*+01	NM	0.99840	0.84413	0.99201	1.38105	0.71830	
31	1.8454*+02	8.8778*+01	NM	0.99868	0.86680	0.99340	1.31466	0.75564	
32	1.8961*+02	9.1552*+01	NM	0.99884	0.87990	0.99420	1.27667	0.77875	
33	1.9339*+02	9.4664*+01	NM	0.99901	0.89480	0.99504	1.23660	0.80466	
34	1.9829*+02	9.7441*+01	NM	0.99915	0.90789	0.99575	1.20291	0.82779	
35	2.0635*+02	1.0213*+02	NM	0.99937	0.92956	0.99666	1.15004	0.86661	
36	2.1502*+02	1.0578*+02	NM	0.99953	0.94613	0.99766	1.11189	0.89727	
37	2.2344*+02	1.0927*+02	NM	0.99967	0.96168	0.99837	1.07776	0.92634	
38	2.4026*+02	1.1209*+02	NM	0.99978	0.97404	0.99892	1.05171	0.94979	
39	2.5349*+02	1.1422*+02	NM	0.99986	0.98327	0.99931	1.03249	0.96759	
40	2.6831*+02	1.1651*+02	NM	0.99994	0.99315	0.99972	1.01328	0.98662	
C 41	2.7940*+02	1.1812*+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050103		WATSON		PROFILE TABULATION		26 POINTS, DELTA AT POINT 26			
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.89878	0.00000	0.00000	29.10169	0.00000	
2	1.3455+04	2.1515+00	NM	0.92427	0.10693	0.50162	22.02493	0.02278	
3	9.2471+04	2.2058+00	NM	0.92500	0.10895	0.50895	21.82243	0.02332	
4	2.2756+03	3.1173+00	NM	0.93508	0.13728	0.59881	19.02530	0.03147	
5	3.4293+03	3.2011+00	NM	0.93585	0.13954	0.60520	18.80908	0.03218	
6	5.2243+03	4.9598+00	NM	0.94075	0.18003	0.70258	15.23008	0.04613	
7	7.8748+03	8.4080+00	NM	0.96352	0.23976	0.79977	11.12681	0.07188	
8	9.7017+03	1.2198+01	NM	0.97266	0.29148	0.85433	8.59089	0.09945	
9	1.1457+02	1.8016+01	NM	0.98067	0.35648	0.89946	6.36638	0.14128	
10	1.2594+02	2.3179+01	NM	0.98495	0.40552	0.92269	5.17715	0.17822	
11	1.3518+02	2.8917+01	NM	0.98817	0.45400	0.93974	4.28460	0.21933	
12	1.4478+02	3.4497+01	NM	0.99037	0.49633	0.95125	3.67319	0.25897	
13	1.5131+02	4.3084+01	NM	0.99276	0.55541	0.96358	3.00987	0.32014	
14	1.5921+02	5.0870+01	NM	0.99429	0.60349	0.97136	2.58643	0.37556	
15	1.6364+02	6.1271+01	NM	0.99576	0.66337	0.97883	2.17722	0.44958	
16	1.7085+02	6.9458+01	NM	0.99663	0.70660	0.98320	1.93613	0.50782	
17	1.7750+02	7.6623+01	NM	0.99724	0.74238	0.98629	1.76506	0.55879	
18	1.8475+02	8.6638+01	NM	0.99794	0.78967	0.98979	1.57104	0.63002	
19	1.9192+02	9.4007+01	NM	0.99837	0.82274	0.99190	1.45349	0.68242	
20	2.0033+02	1.0362+02	NM	0.99883	0.86347	0.99421	1.32422	0.75079	
21	2.1364+02	1.1388+02	NM	0.99925	0.90590	0.99627	1.20945	0.82373	
22	2.2450+02	1.1965+02	NM	0.99945	0.92864	0.99727	1.15326	0.86474	
23	2.3964+02	1.2666+02	NM	0.99967	0.95558	0.99837	1.09156	0.91463	
24	2.5665+02	1.3206+02	NM	0.99983	0.97582	0.99914	1.04837	0.95304	
25	2.7816+02	1.3547+02	NM	0.99993	0.98982	0.99965	1.01994	0.98010	
D 26	2.9963+02	1.3867+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050104		WATSON		PROFILE TABULATION		52 POINTS, DELTA AT POINT 52			
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.94030	0.00000	0.00000	26.31533	0.00000	
2	3.8710+03	1.3749+00	NM	0.91203	0.07104	0.34314	23.33283	0.01471	
3	5.9331+03	6.0642+00	NM	0.95547	0.21208	0.74393	12.30430	0.06046	
4	7.1343+03	8.6103+00	NM	0.96496	0.25600	0.80533	9.89623	0.08138	
5	8.5717+03	1.1581+01	NM	0.97219	0.29912	0.84918	8.05956	0.10536	
6	9.8093+03	1.3281+01	NM	0.97524	0.32118	0.86698	7.28636	0.11899	
7	1.1242+02	1.5827+01	NM	0.97884	0.35165	0.88759	6.37102	0.13932	
8	1.2620+02	1.8374+01	NM	0.98164	0.37967	0.90327	5.66014	0.15958	
9	1.4062+02	2.1344+01	NM	0.98421	0.40993	0.91741	5.00850	0.18317	
10	1.5038+02	2.2620+01	NM	0.98514	0.42227	0.92248	4.77237	0.19330	
11	1.6388+02	2.4743+01	NM	0.98651	0.44203	0.92988	4.42542	0.21012	
12	1.7072+02	2.8132+01	NM	0.98832	0.47186	0.93961	3.96520	0.23696	
13	1.8172+02	3.0252+01	NM	0.98927	0.48959	0.94468	3.72305	0.25374	
14	1.9585+02	3.5334+01	NM	0.99115	0.52970	0.95457	3.24758	0.29393	
15	2.0141+02	3.8299+01	NM	0.99203	0.55175	0.95922	3.02240	0.31737	
16	2.0495+02	3.8303+01	NM	0.99204	0.55178	0.95923	3.02211	0.31740	
17	2.0848+02	3.8306+01	NM	0.99204	0.55180	0.95923	3.02190	0.31743	
18	2.1394+02	4.0426+01	NM	0.99260	0.56704	0.96217	2.87918	0.33418	
19	2.1874+02	4.2122+01	NM	0.99301	0.57894	0.96432	2.77437	0.34758	
20	2.3161+02	4.5937+01	NM	0.99384	0.60486	0.96861	2.56436	0.37772	
21	2.4201+02	4.9750+01	NM	0.99455	0.62971	0.97228	2.38400	0.40780	
22	2.5506+02	5.3562+01	NM	0.99517	0.65359	0.97545	2.22740	0.43794	
23	2.6537+02	5.8644+01	NM	0.99587	0.68415	0.97908	2.04802	0.47806	
24	2.7031+02	6.2453+01	NM	0.99633	0.70619	0.98143	1.93144	0.50813	
25	2.7230+02	6.2456+01	NM	0.99633	0.70620	0.98143	1.93136	0.50815	
26	2.7485+02	6.1190+01	NM	0.99618	0.69895	0.98068	1.96861	0.49816	
27	2.7684+02	6.3306+01	NM	0.99643	0.71103	0.98192	1.90712	0.51487	
28	2.7798+02	6.6692+01	NM	0.99678	0.72992	0.98374	1.81639	0.54159	
29	2.8025+02	6.7963+01	NM	0.99691	0.73690	0.98438	1.78450	0.55163	
30	2.8252+02	6.6274+01	NM	0.99674	0.72762	0.98353	1.82711	0.53830	
31	2.8536+02	6.7122+01	NM	0.99683	0.73229	0.98396	1.80547	0.54499	
32	2.9748+02	7.1359+01	NM	0.99722	0.75520	0.98598	1.70460	0.57843	
33	3.1370+02	7.6864+01	NM	0.99768	0.78396	0.98829	1.58920	0.62188	
34	3.2497+02	8.1947+01	NM	0.99805	0.80962	0.99016	1.49573	0.66199	
35	3.3446+02	8.6606+01	NM	0.99835	0.83243	0.99168	1.41921	0.69876	
36	3.4079+02	8.7458+01	NM	0.99840	0.83654	0.99195	1.40666	0.70548	
37	3.4450+02	8.9154+01	NM	0.99850	0.84465	0.99245	1.38056	0.71887	
38	3.4873+02	9.1272+01	NM	0.99862	0.85468	0.99306	1.35004	0.73558	
39	3.5707+02	9.4665+01	NM	0.99880	0.87049	0.99398	1.30384	0.76235	
40	3.6634+02	9.8055+01	NM	0.99897	0.88602	0.99484	1.26073	0.78910	
41	3.8400+02	1.0314+02	NM	0.99921	0.90878	0.99602	1.20119	0.82919	
42	3.9449+02	1.0737+02	NM	0.99939	0.92734	0.99692	1.15570	0.86261	
43	4.0174+02	1.1034+02	NM	0.99950	0.94013	0.99751	1.12581	0.88604	
44	4.0826+02	1.1204+02	NM	0.99957	0.94736	0.99784	1.10940	0.89944	
45	4.1846+02	1.1459+02	NM	0.99966	0.95811	0.99831	1.08568	0.91952	
46	4.3963+02	1.1798+02	NM	0.99976	0.97223	0.99890	1.05562	0.94627	
47	4.5715+02	1.2052+02	NM	0.99987	0.98269	0.99933	1.03415	0.96633	
48	4.6378+02	1.2306+02	NM	0.99995	0.99304	0.99973	1.01353	0.98639	
49	4.6802+02	1.2306+02	NM	0.99995	0.99305	0.99973	1.01350	0.98642	
50	4.7684+02	1.2392+02	NM	0.99997	0.99652	0.99987	1.00674	0.99318	
51	4.8598+02	1.2478+02	NM	1.00000	0.99996	1.00000	1.00007	0.99993	
D 52	5.0771+02	1.2479+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050501		WATSON		PROFILE TABULATION		37 POINTS, DELTA AT POINT 37			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	NM	0.89792	0.00000	0.00000	31.80938	0.00000	
2	5.2475"-04	1.1028"+00	NM	0.90155	0.03405	0.18869	30.71239	0.00614	
3	1.2774"-03	2.0155"+00	NM	0.92139	0.09097	0.48158	24.66408	0.01953	
4	1.9878"-03	2.9187"+00	NM	0.93246	0.12579	0.58169	21.38470	0.02720	
5	3.0235"-03	4.7102"+00	NM	0.94662	0.16697	0.69070	17.11133	0.04036	
6	3.7590"-03	6.4942"+00	NM	0.95592	0.19933	0.75182	14.30230	0.05271	
7	4.2199"-03	8.8984"+00	NM	0.96448	0.23588	0.80751	11.71934	0.06890	
8	4.7315"-03	1.0550"+01	NM	0.96876	0.25798	0.83307	10.42772	0.07989	
9	5.1859"-03	1.4337"+01	NM	0.97573	0.30258	0.87306	8.32547	0.10487	
10	5.5890"-03	1.9001"+01	NM	0.98121	0.34977	0.90331	6.66990	0.13543	
11	5.7987"-03	2.5043"+01	NM	0.98574	0.40272	0.92752	5.30432	0.17486	
12	5.9654"-03	2.9322"+01	NM	0.98796	0.43637	0.93920	4.63248	0.20274	
13	6.2776"-03	3.4612"+01	NM	0.99004	0.47466	0.94997	4.00545	0.23171	
14	6.4943"-03	4.0402"+01	NM	0.99175	0.51331	0.95876	3.48866	0.27482	
15	6.7115"-03	4.6066"+01	NM	0.99305	0.54849	0.96536	3.09769	0.31184	
16	6.8860"-03	5.0472"+01	NM	0.99387	0.57437	0.96952	2.84432	0.34027	
17	7.1473"-03	5.7143"+01	NM	0.99489	0.61146	0.97467	2.54083	0.38360	
18	7.2501"-03	6.6197"+01	NM	0.99597	0.65848	0.98008	2.21531	0.44241	
19	7.5469"-03	7.5635"+01	NM	0.99684	0.70416	0.98437	1.95433	0.50370	
20	7.7538"-03	8.3436"+01	NM	0.99741	0.73978	0.98725	1.78091	0.55435	
21	7.9594"-03	9.1488"+01	NM	0.99791	0.77484	0.98970	1.63148	0.60663	
22	8.2605"-03	1.0005"+02	NM	0.99835	0.81044	0.99169	1.49790	0.66218	
23	8.3749"-03	1.0671"+02	NM	0.99865	0.83711	0.99335	1.40812	0.70545	
24	8.7343"-03	1.1326"+02	NM	0.99891	0.86252	0.99463	1.32980	0.74798	
25	9.1970"-03	1.1830"+02	NM	0.99909	0.88159	0.99552	1.27516	0.78070	
26	9.5598"-03	1.2345"+02	NM	0.99927	0.90209	0.99642	1.22009	0.81668	
27	1.0370"-02	1.2764"+02	NM	0.99939	0.91586	0.99697	1.18501	0.84134	
28	1.1081"-02	1.3169"+02	NM	0.99950	0.93031	0.99757	1.14981	0.86760	
29	1.1951"-02	1.3436"+02	NM	0.99958	0.93972	0.99793	1.12772	0.88490	
30	1.2631"-02	1.3740"+02	NM	0.99966	0.95033	0.99832	1.10354	0.90465	
31	1.3163"-02	1.4031"+02	NM	0.99973	0.96036	0.99868	1.08139	0.92351	
32	1.4099"-02	1.4159"+02	NM	0.99976	0.96477	0.99883	1.07187	0.93186	
33	1.5186"-02	1.4426"+02	NM	0.99983	0.97385	0.99915	1.05262	0.94920	
34	1.5982"-02	1.4592"+02	NM	0.99986	0.97945	0.99933	1.04101	0.95997	
35	1.6941"-02	1.4696"+02	NM	0.99989	0.98293	0.99945	1.03390	0.96668	
36	1.7743"-02	1.4877"+02	NM	0.99993	0.98932	0.99966	1.02102	0.97908	
D 37	2.0239"-02	1.5209"+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050502		WATSON		PROFILE TABULATION		33 POINTS, DELTA AT POINT 33			
I	Y	PTZ/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000"+00	1.0000"+00	NM	0.89531	0.00000	0.00000	29.80610	0.00000	
2	1.2051"-03	1.0814"+00	NM	0.89830	0.03138	0.16896	28.98371	0.00563	
3	1.5689"-03	1.9687"+00	NM	0.91153	0.07819	0.39361	25.34315	0.01553	
4	3.1127"-03	2.0896"+00	NM	0.95736	0.21577	0.76989	12.73184	0.06047	
5	3.9869"-03	1.0769"+01	NM	0.96856	0.26925	0.83646	9.65128	0.08667	
6	4.7970"-03	1.5065"+01	NM	0.97627	0.32052	0.87942	7.52816	0.11682	
7	5.7470"-03	2.1451"+01	NM	0.98301	0.38425	0.91528	5.67393	0.16131	
8	6.1337"-03	2.8827"+01	NM	0.98758	0.44667	0.93881	4.41745	0.21252	
9	6.5119"-03	3.5814"+01	NM	0.99037	0.49878	0.95290	3.64979	0.26108	
10	7.0162"-03	4.3701"+01	NM	0.99254	0.55145	0.96369	3.05396	0.31555	
11	7.3961"-03	5.0585"+01	NM	0.99392	0.59372	0.97054	2.67221	0.36320	
12	7.8333"-03	5.6730"+01	NM	0.99490	0.62905	0.97533	2.40398	0.40571	
13	7.9074"-03	6.1279"+01	NM	0.99550	0.65398	0.97828	2.23771	0.43718	
14	8.2889"-03	6.4657"+01	NM	0.99632	0.69250	0.98228	2.01201	0.48821	
15	8.6652"-03	7.4434"+01	NM	0.99684	0.72123	0.98488	1.86474	0.52816	
16	9.0600"-03	8.2795"+01	NM	0.99751	0.76088	0.98802	1.68614	0.58597	
17	9.3322"-03	8.7466"+01	NM	0.99782	0.78216	0.98952	1.60050	0.61836	
18	9.6057"-03	9.2506"+01	NM	0.99812	0.80450	0.99098	1.51733	0.65311	
19	9.9424"-03	9.7300"+01	NM	0.99838	0.82518	0.99223	1.44587	0.68625	
20	1.0151"-02	1.0222"+02	NM	0.99862	0.84547	0.99340	1.37923	0.72025	
21	1.0359"-02	1.0677"+02	NM	0.99883	0.86457	0.99438	1.32284	0.75170	
22	1.0889"-02	1.1180"+02	NM	0.99903	0.88481	0.99538	1.26554	0.78653	
23	1.1287"-02	1.1586"+02	NM	0.99919	0.90078	0.99612	1.22290	0.81456	
24	1.1815"-02	1.2041"+02	NM	0.99935	0.91834	0.99690	1.17840	0.84598	
25	1.2724"-02	1.2495"+02	NM	0.99950	0.93556	0.99762	1.13706	0.87736	
26	1.3169"-02	1.2740"+02	NM	0.99958	0.94473	0.99799	1.11593	0.89431	
27	1.3726"-02	1.3035"+02	NM	0.99967	0.95563	0.99881	1.09153	0.91469	
28	1.4557"-02	1.3341"+02	NM	0.99976	0.96884	0.99883	1.06727	0.93587	
29	1.5497"-02	1.3622"+02	NM	0.99983	0.97701	0.99920	1.04594	0.95532	
30	1.6465"-02	1.3806"+02	NM	0.99988	0.98388	0.99944	1.03249	0.96798	
31	1.7456"-02	1.3977"+02	NM	0.99993	0.98968	0.99965	1.02025	0.97980	
32	1.8513"-02	1.4184"+02	NM	0.99998	0.99703	0.99990	1.00576	0.99417	
D 33	1.9960"-02	1.4269"+02	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,M/MD ASSUME P=PD AND VAN DRIEST

73050503		WATSON		PROFILE TABULATION		30 POINTS, DELTA AT POINT 30			
I	Y	PTZ/P	P/PO	T0/T0D	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	NM	0.8918	0.0000	0.0000	32.41028	0.0000	
2	1.2882-03	8.7180+00	NM	0.9605	0.2295	0.8025	12.18056	0.06589	
3	1.6289-03	9.7912+00	NM	0.9637	0.2447	0.8204	11.26460	0.07284	
4	2.2590-03	1.3019+01	NM	0.9711	0.2836	0.8593	9.18623	0.09358	
5	2.7719-03	1.5047+01	NM	0.9748	0.3057	0.8773	8.23422	0.10655	
6	3.8846-03	1.9109+01	NM	0.9797	0.3456	0.9026	6.81849	0.13238	
7	5.1852-03	2.4970+01	NM	0.9845	0.3962	0.9262	5.46308	0.16954	
8	6.1720-03	3.0471+01	NM	0.9872	0.4389	0.9408	4.80411	0.20436	
9	6.7961-03	3.5980+01	NM	0.9897	0.4770	0.9512	3.97791	0.23917	
10	7.6456-03	4.1366+01	NM	0.9914	0.5119	0.9592	3.51161	0.27320	
11	8.1598-03	4.8077+01	NM	0.9927	0.5523	0.9660	3.06304	0.31557	
12	8.6037-03	5.4430+01	NM	0.9938	0.5879	0.9720	2.73298	0.35566	
13	9.0463-03	6.0542+01	NM	0.9949	0.6203	0.9762	2.47624	0.39423	
14	9.4908-03	6.7014+01	NM	0.9958	0.6529	0.9796	2.25221	0.43507	
15	9.9245-03	7.1686+01	NM	0.9967	0.6754	0.9820	2.11416	0.46454	
16	1.0521+02	7.6355+01	NM	0.9965	0.6972	0.9840	1.99210	0.49399	
17	1.0994+02	8.1866+01	NM	0.9969	0.7209	0.9861	1.86504	0.52875	
18	1.1465+02	8.6898+01	NM	0.9971	0.7447	0.9879	1.74238	0.56049	
19	1.1750+02	9.3012+01	NM	0.9970	0.7693	0.9895	1.65191	0.59904	
20	1.2230+02	9.9843+01	NM	0.9980	0.7973	0.9913	1.54380	0.64212	
21	1.2462+02	1.0824+02	NM	0.9984	0.8308	0.9931	1.42883	0.69508	
22	1.2322+02	1.1507+02	NM	0.9987	0.8566	0.9946	1.34728	0.73812	
23	1.3562+02	1.1998+02	NM	0.9989	0.8749	0.9951	1.29408	0.76912	
24	1.4066+02	1.2886+02	NM	0.9992	0.9062	0.9968	1.20800	0.82507	
25	1.4930+02	1.3472+02	NM	0.9994	0.9271	0.9975	1.15711	0.86206	
26	1.6029+02	1.4202+02	NM	0.9996	0.9521	0.9982	1.09945	0.90810	
27	1.7137+02	1.4824+02	NM	0.9998	0.9728	0.9993	1.05469	0.94732	
28	1.7781+02	1.5135+02	NM	0.9998	0.9836	0.9996	1.03366	0.96692	
29	1.8733+02	1.5421+02	NM	0.9999	0.9923	0.9997	1.01503	0.98496	
0 30	1.9431+02	1.5660+02	NM	1.0000	1.0000	1.0000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,H/M/D ASSUME P=PD AND VAN DRIEST

73050504		WATSON		PROFILE TABULATION		30 POINTS, DELTA AT POINT 30			
I	Y	PTZ/P	P/PO	T0/T0D	H/H0	U/U0	T/T0	RHO/RHO0*U/U0	
1	0.0000+00	1.0000+00	NM	0.8950	0.0000	0.0000	32.62373	0.0000	
2	2.2212-03	4.8861+00	NM	0.9460	0.1679	0.6974	17.24124	0.04045	
3	2.5803-03	5.9710+00	NM	0.9520	0.1876	0.7372	15.43520	0.04776	
4	3.2110-03	7.6012+00	NM	0.9590	0.2137	0.7806	13.34162	0.05853	
5	4.0537-03	9.8725+00	NM	0.9660	0.2453	0.8226	11.22463	0.07329	
6	6.2150-03	1.3008+01	NM	0.9727	0.2833	0.8606	9.20984	0.09343	
7	7.1909-03	1.4201+01	NM	0.9740	0.2967	0.8712	8.62123	0.10105	
8	7.9311-03	1.6043+01	NM	0.9772	0.3159	0.8855	7.84679	0.11280	
9	9.2090-03	1.8751+01	NM	0.9803	0.3423	0.9013	6.93207	0.13002	
10	1.0130+02	2.2100+01	NM	0.9832	0.3726	0.9164	6.05855	0.15128	
11	1.1367+02	2.9773+01	NM	0.9856	0.4027	0.9294	5.32313	0.17455	
12	1.2909+02	2.9878+01	NM	0.9876	0.4344	0.9390	4.68708	0.20053	
13	1.3880+02	3.2590+01	NM	0.9889	0.4533	0.9453	4.24547	0.21761	
14	1.4500+02	3.5606+01	NM	0.9898	0.4745	0.9510	4.01745	0.23674	
15	1.5182+02	3.9279+01	NM	0.9910	0.4986	0.9568	3.68035	0.25994	
16	1.5905+02	4.3919+01	NM	0.9922	0.5274	0.9625	3.32759	0.28925	
17	1.7151+02	4.8125+01	NM	0.9936	0.5525	0.9686	3.06156	0.31581	
18	1.8578+02	5.3951+01	NM	0.9947	0.5836	0.9713	2.75636	0.35258	
19	1.9377+02	5.8265+01	NM	0.9949	0.6085	0.9749	2.56684	0.37980	
20	1.9956+02	6.1503+01	NM	0.9952	0.6253	0.9765	2.44093	0.40024	
21	2.0613+02	6.6147+01	NM	0.9957	0.6486	0.9795	2.28045	0.42954	
22	2.1166+02	7.0034+01	NM	0.9961	0.6673	0.9816	2.16152	0.45406	
23	2.2019+02	7.4629+01	NM	0.9964	0.6940	0.9847	1.98492	0.49693	
24	2.3273+02	8.4593+01	NM	0.9972	0.7308	0.9874	1.80828	0.54590	
25	2.3690+02	9.1814+01	NM	0.9977	0.7643	0.9893	1.67270	0.59144	
26	2.4833+02	9.7745+01	NM	0.9980	0.7893	0.9908	1.57565	0.62885	
27	2.5846+02	1.0368+02	NM	0.9983	0.8130	0.9922	1.48924	0.66626	
28	2.5938+02	1.0767+02	NM	0.9985	0.8285	0.9930	1.43622	0.69145	
29	2.6368+02	1.1188+02	NM	0.9987	0.8447	0.9931	1.38426	0.71801	
30	2.6894+02	1.1598+02	NM	0.9988	0.8608	0.9946	1.33712	0.74388	
31	2.7617+02	1.2008+02	NM	0.9990	0.8753	0.9953	1.29311	0.76974	
32	2.9020+02	1.2806+02	NM	0.9992	0.9040	0.9965	1.21529	0.82004	
33	2.9939+02	1.3475+02	NM	0.9994	0.9274	0.9972	1.15693	0.86221	
34	3.1004+02	1.3864+02	NM	0.9996	0.9403	0.9980	1.12550	0.88673	
35	3.1894+02	1.4447+02	NM	0.9997	0.9603	0.9987	1.08142	0.92352	
36	3.3208+02	1.4836+02	NM	0.9998	0.9732	0.9995	1.05390	0.94805	
37	3.5392+02	1.5117+02	NM	0.9998	0.9827	0.9995	1.03486	0.96378	
38	3.6793+02	1.5355+02	NM	0.9999	0.9909	0.9997	1.01928	0.98078	
0 39	3.9243+02	1.5660+02	NM	1.0000	1.0000	1.0000	1.00000	1.00000	

INPUT VARIABLES Y/DELTA,H/M/D ASSUME P=PD AND VAN DRIEST

SECTION D, ADDITIONAL DATA, TEMPERATURE PROFILES

	0204		0304		0404		0504	
POD	$P_o = 5.378 \text{ MN/m}^2$		$P_o = 7.929 \text{ MN/m}^2$		$P_o = 10.76 \text{ MN/m}^2$		$P_o = 13.24 \text{ MN/m}^2$	
TOD	$T_T = 302 \text{ K}$		$T_T = 301 \text{ K}$		$T_T = 300 \text{ K}$		$T_T = 302 \text{ K}$	
TW	$T_w = 283 \text{ K}$		$T_w = 283 \text{ K}$		$T_w = 283 \text{ K}$		$T_w = 283 \text{ K}$	
δ	$\delta = 50.80 \text{ mm}$		$\delta = 40.64 \text{ mm}$		$\delta = 40.64 \text{ mm}$		$\delta = 40.64 \text{ mm}$	
	Y/ δ	TO/TOD	Y/ δ	TO/TOD	Y/ δ	TO/TOD	y/ δ	TO/TOD
	0.093	0.852	0.117	0.876	0.184	0.903	0.348	0.910
	0.108	0.869	0.141	0.887	0.208	0.905	0.376	0.910
	0.129	0.883	0.160	0.892	0.222	0.907	0.406	0.912
	0.154	0.889	0.189	0.898	0.252	0.906	0.424	0.912
	0.187	0.893	0.221	0.902	0.281	0.905	0.437	0.912
	0.196	0.896	0.236	0.905	0.313	0.903	0.451	0.911
	0.213	0.899	0.249	0.905	0.328	0.903	0.463	0.912
	0.236	0.899	0.262	0.906	0.342	0.903	0.482	0.915
	0.266	0.897	0.286	0.906	0.365	0.902	0.509	0.921
	0.299	0.896	0.308	0.906	0.386	0.901	0.518	0.924
	0.316	0.896	0.331	0.905	0.422	0.898	0.543	0.931
	0.341	0.895	0.351	0.904	0.448	0.898	0.557	0.934
	0.364	0.895	0.368	0.904	0.466	0.900	0.565	0.937
	0.390	0.894	0.379	0.903	0.476	0.901	0.577	0.940
	0.417	0.895	0.402	0.901	0.488	0.902	0.588	0.945
	0.427	0.896	0.426	0.901	0.506	0.905	0.604	0.951
	0.447	0.898	0.441	0.900	0.515	0.906	0.635	0.965
	0.465	0.900	0.469	0.901	0.538	0.913	0.655	0.973
	0.478	0.902	0.475	0.902	0.564	0.921	0.678	0.981
	0.492	0.904	0.489	0.902	0.582	0.926	0.698	0.988
	0.518	0.911	0.501	0.903	0.598	0.930	0.726	0.995
	0.535	0.916	0.516	0.904	0.612	0.935	0.774	0.998
	0.548	0.913	0.542	0.909	0.622	0.939	0.805	0.998
	0.567	0.921	0.570	0.915	0.630	0.943	0.858	0.999
	0.566	0.923	0.594	0.919	0.651	0.953	0.912	0.999
	0.581	0.929	0.598	0.924	0.671	0.962	0.945	0.999
	0.592	0.932	0.613	0.928	0.698	0.969	1.025	1.001
	0.602	0.935	0.623	0.931	0.707	0.975		
	0.608	0.937	0.636	0.934	0.727	0.982		
	0.626	0.942	0.643	0.937	0.749	0.987		
	0.645	0.950	0.661	0.944	0.771	0.991		
	0.664	0.958	0.684	0.951	0.791	0.995		
	0.679	0.963	0.706	0.956	0.829	0.998		
	0.692	0.968	0.716	0.959	0.836	0.999		
	0.698	0.970	0.730	0.963	0.848	0.999		
	0.706	0.973	0.741	0.967	0.862	0.999		
	0.719	0.978	0.752	0.970	0.891	0.999		
	0.734	0.982	0.759	0.972	0.948	1.000		
	0.757	0.987	0.773	0.979	0.962	1.000		
	0.768	0.989	0.787	0.984	0.978	1.000		
	0.781	0.992	0.815	0.991	1.020	1.000		
	0.796	0.994	0.842	0.995				
	0.808	0.996	0.858	0.997				
	0.816	0.997	0.863	0.999				
	0.827	0.997	0.877	1.000				
	0.836	0.997	0.888	1.000				
	0.853	0.998	0.918	1.000				
	0.879	0.999	0.974	1.000				
	0.914	1.000						
	0.936	1.000						
	0.949	1.000						

	M : A, 2.56 to 3; B, 2.51 to 2.19; C, 2.57 to 3.24. R THETA X 10 ⁻³ : 14 - 24. TW/TR : 1.05	7401
		FPG - APG AH
Blow-down tunnel with fixed half-nozzle. Running time 50 s, W = 0.114, H = 0.083 m. Air; 0.3 < P0 < 0.6 MN/m ² . T0 : 300 K. 3 < RE/m X 10 ⁻⁶ < 6.		
THOMAS G.D., 1974. Compressible turbulent boundary layers with combined air injection and pressure gradient. ARC (London) R & M 3779. <u>And</u> Ph.D. Thesis, Cambridge (1973), Squire, L.C., private communication.		

- 1 The test boundary layer was formed on a flat surface extending upstream into the settling chamber and facing one of a number of contoured nozzle blocks. For the FPG cases these were cast in Araldite to a design calculated by the method of characteristics. The flow was initially accelerated to give a uniform free stream at M = 2.5 - 2.6. A 5° or 10° expansion was then produced by a curved surface and reflected from the test surface, where the design pressure gradients were linear. The stronger of the two expansion fields was not completed within the test zone. For the APG tests, the second half of the contoured nozzle was formed of a flexible metal plate. This was rolled to an approximate design shape, and then adjusted manually to give a linear APG on the test surface.

Two test surfaces were used, one a solid metal plate, and the other a plate with a sintered section for the injection tests which are not reported here. The plates were 0.1 mm wide and tests extended over a streamwise distance of up to 0.2 m, starting 0.44 m from the tunnel throat.
- 2 Other than slight disturbances (about 1 % in M) at the start of the pressure gradients, the favourable gradients were "free from disturbance" until the large changes occurring at their ends. "One or two weak disturbances were evident" in the APG case and "these did affect some of the boundary layer parameters".
- 3 The evidence of earlier tests (Jeromin, 1966. Squire, 1970) was that transition occurred well upstream, and that the velocity profiles were fully developed after experiencing the throat region expansion.
- 6 Static pressure was measured along the test surface centre line at intervals of 12.7 mm using tappings of 0.30 mm diameter. The plate temperature was monitored by 7 thermocouples mounted 25 mm from the centre line at intervals of 50 mm. The wall shear stress was estimated using the razor-blade technique after Smith, Gaudet and Winter (1964). A section of blade 6.35 mm long and 3.8 mm wide was mounted with its leading edge just over the upstream edge of a static hole. The leading edge was 0.14 mm above the plate surface, and the upper side of the blade had been ground down so that the chamfering of the upper side was about 0.03 mm in height. The sensors were calibrated against the Spalding and Chi (1964) CF correlation for ZPG flow.
- 7 Pitot, temperature, and static pressure measurements were made. The CCP used has a 2.5° semi-angle tip, was of 1 mm diameter and the static holes were 20 mm from the tip. No pressure variation through the boundary layer was observed. The T0 profile was measured with an ECP for which d = 1.65 mm, l = 2.5 mm and the semi-angle α was 5°. The readings had been compared earlier with a long slender ECP, and no difference was found, so that the shorter probe was used as being less fragile. The Pitot probes used were FPP for which, approximately, h₁ = 0.13, h₂ = 0.035, b₁ = 1.5, b₂ = 1.0 mm. (These are representative figures, the source paper giving much more detail.) Profiles, static pressure, and razor blade CF determinations were made on the same normal at streamwise intervals of 12.7 mm. For gradient B, series 02, the interval was 6.35 mm.
- 8 The readings were recorded continuously on X-Y-plotters, and the tabulated values obtained from values measured from the trace. The author also extrapolated the T0 profile to meet the measured wall temperature. The static pressure was taken as constant on the basis of the static pressure traverses made. The author's 10 recovery factor was 0.89. No profile corrections were made and Sutherland's viscosity law was used.
- 12 The editors have presented only those profiles measured on a solid surface. The author also presents profiles for each pressure gradient at two wall mass flux rates. The boundary layer edge state is that

- 13 selected by the author. The profiles form three sets, 01 for the FPG "A" case with 15 successive profiles,
14 02 for the APG "B" case with 15 profiles, and 03 for the FPG "C" case with 18 profiles. The CF value is as
reduced by the author.
- 5 DATA 7401 0101-0318. Pitot, TO (and P) profiles measured separately. NX = 15-18. CF from razor blades.

15 Editors' comments

The experiment is one of a series intended to provide comprehensive information on the effects of mass injection. Here we consider only the "solid wall" case, which together with the ZPG experiment of Jeromin - CAT 6602 provides a systematically varied set of pressure gradients observed in a single facility. The principal uncertainty here must be the question of three-dimensionality, as the length/width ratio of the experimental surface is over 5 : 1. A momentum balance for the centre line profile sequence of CAT 6602 showed discrepancies at the 20 - 30 % level.

The profiles are given in fine detail, and at close intervals so that the layer development is easily followed. Comparable tests with broadly similar geometry are those of Michel - CAT 6902 for the FPG case and Zwarts - CAT 7007 in an APG. Lewis et al. - CAT 7201 give profiles at close intervals on an axisymmetric model.

The author states that no normal pressure gradients were observed, but the frequency at which static pressure profiles were measured is not stated, and normal pressure variations might occur in those regions where the longitudinal pressure gradient is changing rapidly.

CAT 7401		THOMAS		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	MD *	TH/TR	RED2W	CF *	H12	H12K	PH	PD			
X *	POD*	PH/PO*	RED2D	CO	H32	H32K	Y*	TD			
RZ	TOA*	SH *	D2	PI2	H42	D2K	UD	TR			
74010101	2.5600	1.0543	8.2541 ⁺⁰³	1.5300 ⁻⁰³	4.2081	1.3845	2.1968 ⁺⁰⁴	2.1968 ⁺⁰⁴			
0.0000 ⁺⁰⁰	4.1200 ⁺⁰⁵	1.0000	1.6742 ⁺⁰⁴	NM	1.7913	1.7727	2.8960 ⁺⁰²	1.2632 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.2574 ⁻⁰⁴	NC	0.0613	6.1560 ⁻⁰⁴	5.7689 ⁺⁰²	2.7468 ⁺⁰²			
74010102	2.5600	1.0547	8.4568 ⁺⁰³	1.5200 ⁻⁰³	4.2257	1.3675	2.1968 ⁺⁰⁴	2.1968 ⁺⁰⁴			
1.2700 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.7157 ⁺⁰⁴	NM	1.7959	1.7790	2.8970 ⁺⁰²	1.2632 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.3631 ⁻⁰⁴	NC	0.0433	6.2911 ⁻⁰⁴	5.7689 ⁺⁰²	2.7468 ⁺⁰²			
74010103	2.5600	1.0550	8.3664 ⁺⁰³	1.5100 ⁻⁰³	4.4007	1.3564	2.1968 ⁺⁰⁴	2.1968 ⁺⁰⁴			
2.5400 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.6978 ⁺⁰⁴	NM	1.8014	1.7830	2.8980 ⁺⁰²	1.2632 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.3176 ⁻⁰⁴	NC	-0.0297	6.2738 ⁻⁰⁴	5.7689 ⁺⁰²	2.7468 ⁺⁰²			
74010104	2.5900	1.0561	9.0630 ⁺⁰³	1.5350 ⁻⁰³	4.2581	1.3474	2.0970 ⁺⁰⁴	2.0970 ⁺⁰⁴			
3.8100 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.8625 ⁺⁰⁴	NM	1.8045	1.7880	2.8990 ⁺⁰²	1.2666 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.8122 ⁻⁰⁴	NC	0.0395	6.8914 ⁻⁰⁴	5.7979 ⁺⁰²	2.7451 ⁺⁰²			
74010105	2.6300	1.0573	8.6351 ⁺⁰³	1.5650 ⁻⁰³	4.3749	1.3348	1.9712 ⁺⁰⁴	1.9712 ⁺⁰⁴			
5.0800 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.8044 ⁺⁰⁴	NM	1.8117	1.7955	2.9000 ⁺⁰²	1.2247 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.7624 ⁻⁰⁴	NC	0.0201	6.8377 ⁻⁰⁴	5.8356 ⁺⁰²	2.7428 ⁺⁰²			
74010106	2.6700	1.0585	8.2509 ⁺⁰³	1.5650 ⁻⁰³	4.4754	1.3423	1.8532 ⁺⁰⁴	1.8532 ⁺⁰⁴			
6.3500 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.7532 ⁺⁰⁴	NM	1.8100	1.7928	2.9010 ⁺⁰²	1.2033 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.7271 ⁻⁰⁴	NC	0.0198	6.8416 ⁻⁰⁴	5.8724 ⁺⁰²	2.7406 ⁺⁰²			
74010107	2.7100	1.0597	7.8151 ⁺⁰³	1.5550 ⁻⁰³	4.6449	1.3091	1.7425 ⁺⁰⁴	1.7425 ⁺⁰⁴			
7.6200 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.6886 ⁺⁰⁴	NM	1.8266	1.8102	2.9020 ⁺⁰²	1.1823 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.6516 ⁻⁰⁴	NC	-0.0274	6.7310 ⁻⁰⁴	5.9081 ⁺⁰²	2.7384 ⁺⁰²			
74010108	2.7500	1.0606	8.0148 ⁺⁰³	1.5500 ⁻⁰³	4.5364	1.3040	1.8385 ⁺⁰⁴	1.8385 ⁺⁰⁴			
8.8900 ⁻⁰²	4.1200 ⁺⁰⁵	1.0000	1.7605 ⁺⁰⁴	NM	1.8290	1.8126	2.9020 ⁺⁰²	1.1618 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	4.9551 ⁻⁰⁴	NC	0.0386	7.0985 ⁻⁰⁴	5.9430 ⁺⁰²	2.7363 ⁺⁰²			
74010109	2.7900	1.0614	8.0299 ⁺⁰³	1.5500 ⁻⁰³	4.6097	1.2924	1.5415 ⁺⁰⁴	1.5415 ⁺⁰⁴			
1.0160 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.7930 ⁺⁰⁴	NM	1.8337	1.8171	2.9020 ⁺⁰²	1.1417 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.1567 ⁻⁰⁴	NC	0.0403	7.4132 ⁻⁰⁴	5.9770 ⁺⁰²	2.7342 ⁺⁰²			
74010110	2.8400	1.0620	7.7689 ⁺⁰³	1.5500 ⁻⁰³	4.7451	1.3015	1.4284 ⁺⁰⁴	1.4284 ⁺⁰⁴			
1.1430 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.7685 ⁺⁰⁴	NM	1.8311	1.8128	2.9010 ⁺⁰²	1.1171 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.2254 ⁻⁰⁴	NC	0.0394	7.6046 ⁻⁰⁴	6.0182 ⁺⁰²	2.7316 ⁺⁰²			
74010111	2.8800	1.0624	7.7504 ⁺⁰³	1.5450 ⁻⁰³	4.7735	1.2894	1.3442 ⁺⁰⁴	1.3442 ⁺⁰⁴			
1.2700 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.7949 ⁺⁰⁴	NM	1.8368	1.8187	2.9000 ⁺⁰²	1.0978 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.4195 ⁻⁰⁴	NC	0.0351	7.8726 ⁻⁰⁴	6.0502 ⁺⁰²	2.7296 ⁺⁰²			
74010112	2.9000	1.0624	7.6718 ⁺⁰³	1.5350 ⁻⁰³	4.9305	1.2880	1.3040 ⁺⁰⁴	1.3040 ⁺⁰⁴			
1.3970 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.7909 ⁺⁰⁴	NM	1.8370	1.8189	2.8990 ⁺⁰²	1.0884 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.4663 ⁻⁰⁴	NC	0.0349	8.0274 ⁻⁰⁴	6.0659 ⁺⁰²	2.7286 ⁺⁰²			
74010113	2.9300	1.0626	7.6564 ⁺⁰³	1.5250 ⁻⁰³	5.0128	1.2838	1.2462 ⁺⁰⁴	1.2462 ⁺⁰⁴			
1.5240 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.8059 ⁺⁰⁴	NM	1.8412	1.8218	2.8980 ⁺⁰²	1.0744 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.6120 ⁻⁰⁴	NC	0.0345	8.2663 ⁻⁰⁴	6.0891 ⁺⁰²	2.7272 ⁺⁰²			
74010114	2.9600	1.0628	7.9515 ⁺⁰³	1.5150 ⁻⁰³	4.9022	1.2953	1.1911 ⁺⁰⁴	1.1911 ⁺⁰⁴			
1.6510 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.9014 ⁺⁰⁴	NM	1.8363	1.8156	2.8970 ⁺⁰²	1.0606 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.9957 ⁻⁰⁴	NC	0.0796	8.8113 ⁻⁰⁴	6.1118 ⁺⁰²	2.7257 ⁺⁰²			
74010115	3.0000	1.0632	7.3685 ⁺⁰³	1.5050 ⁻⁰³	5.0682	1.2793	1.1216 ⁺⁰⁴	1.1216 ⁺⁰⁴			
1.7780 ⁻⁰¹	4.1200 ⁺⁰⁵	1.0000	1.7906 ⁺⁰⁴	NM	1.8430	1.8236	2.8960 ⁺⁰²	1.0425 ⁺⁰²			
INFINITE	2.9190 ⁺⁰²	0.0000	5.7704 ⁻⁰⁴	NC	0.0484	8.5230 ⁻⁰⁴	6.1414 ⁺⁰²	2.7238 ⁺⁰²			

CAT 7401		THOMAS		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.					
RUN	MD *	TN/TR	RED2W	CF *	H12	H12K	PW	PD	
X *	P00*	PH/PD*	REN2D	CO	H32	H32K	TH*	TD	
RZ	T00*	SH *	OZ	PI2	H42	D2K	UD	TR	
74010201	2.5200	1.0528	7.4141 ⁺⁰³	1.8850 ⁻⁰³	4.0624	1.3718	1.7475 ⁺⁰⁴	1.7475 ⁺⁰⁴	
0.0000 ⁺⁰⁰	3.0800 ⁺⁰⁵	1.0000	1.4770 ⁺⁰⁴	NM	1.7424	1.7753	2.9160 ⁺⁰²	1.2955 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.9722 ⁻⁰⁴	NC	0.0726	7.0706 ⁻⁰⁴	5.7509 ⁺⁰²	2.7699 ⁺⁰²	
74010202	2.5200	1.0528	7.0616 ⁺⁰³	1.5900 ⁻⁰³	4.2791	1.3606	1.7475 ⁺⁰⁴	1.7475 ⁺⁰⁴	
1.2700 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.4067 ⁺⁰⁴	NM	1.7960	1.7747	2.9160 ⁺⁰²	1.2955 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.7358 ⁻⁰⁴	NC	-0.0134	6.8488 ⁻⁰⁴	5.7509 ⁺⁰²	2.7699 ⁺⁰²	
74010203	2.5300	1.0533	6.6629 ⁺⁰³	1.6050 ⁻⁰³	4.2456	1.3580	1.7205 ⁺⁰⁴	1.7205 ⁺⁰⁴	
2.5400 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.3331 ⁺⁰⁴	NM	1.7989	1.7829	2.9170 ⁺⁰²	1.2898 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.5116 ⁻⁰⁴	NC	0.0028	6.4750 ⁻⁰⁴	5.7608 ⁺⁰²	2.7693 ⁺⁰²	
74010204	2.5200	1.0531	6.4112 ⁺⁰³	1.6200 ⁻⁰³	4.2324	1.3513	1.7475 ⁺⁰⁴	1.7475 ⁺⁰⁴	
3.8100 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.3572 ⁺⁰⁴	NM	1.8005	1.7853	2.9170 ⁺⁰²	1.2955 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.5691 ⁻⁰⁴	NC	-0.0053	6.5383 ⁻⁰⁴	5.7509 ⁺⁰²	2.7699 ⁺⁰²	
74010205	2.4800	1.0526	7.0614 ⁺⁰³	1.5950 ⁻⁰³	4.2129	1.3652	1.8596 ⁺⁰⁴	1.8596 ⁺⁰⁴	
5.0800 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.3846 ⁺⁰⁴	NM	1.7831	1.7672	2.9180 ⁺⁰²	1.3188 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.5646 ⁻⁰⁴	NC	-0.0080	6.5966 ⁻⁰⁴	5.7102 ⁺⁰²	2.7723 ⁺⁰²	
74010206	2.4500	1.0519	7.4753 ⁺⁰³	1.5500 ⁻⁰³	4.2704	1.3760	1.9486 ⁺⁰⁴	1.9486 ⁺⁰⁴	
6.3500 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.4479 ⁺⁰⁴	NM	1.7846	1.7712	2.9180 ⁺⁰²	1.3365 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.6942 ⁻⁰⁴	NC	-0.0610	6.8009 ⁻⁰⁴	5.6789 ⁺⁰²	2.7741 ⁺⁰²	
74010207	2.4400	1.0520	7.9849 ⁺⁰³	1.5150 ⁻⁰³	4.0452	1.3837	1.9792 ⁺⁰⁴	1.9792 ⁺⁰⁴	
7.6200 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.5407 ⁺⁰⁴	NM	1.7823	1.7667	2.9190 ⁺⁰²	1.3425 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	4.9745 ⁻⁰⁴	NC	0.0018	7.1077 ⁻⁰⁴	5.6683 ⁺⁰²	2.7748 ⁺⁰²	
74010208	2.4100	1.0516	8.4707 ⁺⁰³	1.4900 ⁻⁰³	4.0123	1.3833	2.0741 ⁺⁰⁴	2.0741 ⁺⁰⁴	
8.8900 ⁻⁰²	3.0800 ⁺⁰⁵	1.0000	1.6150 ⁺⁰⁴	NM	1.7819	1.7662	2.9200 ⁺⁰²	1.3606 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	5.1342 ⁻⁰⁴	NC	0.0097	7.2868 ⁻⁰⁴	5.6362 ⁺⁰²	2.7766 ⁺⁰²	
74010209	2.3900	1.0508	8.7173 ⁺⁰³	1.4650 ⁻⁰³	3.9743	1.3638	2.1399 ⁺⁰⁴	2.1399 ⁺⁰⁴	
1.0160 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	1.6481 ⁺⁰⁴	NM	1.7876	1.7737	2.9190 ⁺⁰²	1.3727 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	5.1857 ⁻⁰⁴	NC	-0.0048	7.3079 ⁻⁰⁴	5.6148 ⁺⁰²	2.7779 ⁺⁰²	
74010210	2.3400	1.0492	9.9867 ⁺⁰³	1.4450 ⁻⁰³	3.9143	1.3658	2.3138 ⁺⁰⁴	2.3138 ⁺⁰⁴	
1.1430 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	1.8496 ⁺⁰⁴	NM	1.7759	1.7618	2.9180 ⁺⁰²	1.4037 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	5.6731 ⁻⁰⁴	NC	-0.0076	7.9982 ⁻⁰⁴	5.5886 ⁺⁰²	2.7811 ⁺⁰²	
74010211	2.3300	1.0490	9.5620 ⁺⁰³	1.4300 ⁻⁰³	4.0818	1.3733	2.3502 ⁺⁰⁴	2.3502 ⁺⁰⁴	
1.2700 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	1.7635 ⁺⁰⁴	NM	1.7817	1.7682	2.9180 ⁺⁰²	1.4100 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	5.3826 ⁻⁰⁴	NC	-0.0055	7.6380 ⁻⁰⁴	5.5473 ⁺⁰²	2.7818 ⁺⁰²	
74010212	2.3000	1.0479	1.0824 ⁺⁰⁴	1.4200 ⁻⁰³	3.7444	1.3874	2.4632 ⁺⁰⁴	2.4632 ⁺⁰⁴	
1.3970 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	1.9720 ⁺⁰⁴	NM	1.7742	1.7605	2.9170 ⁺⁰²	1.4291 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	5.9278 ⁻⁰⁴	NC	0.0266	8.2121 ⁻⁰⁴	5.5127 ⁺⁰²	2.7838 ⁺⁰²	
74010213	2.2800	1.0474	1.1267 ⁺⁰⁴	1.4100 ⁻⁰³	3.6786	1.3778	2.5415 ⁺⁰⁴	2.5415 ⁺⁰⁴	
1.5240 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	2.0361 ⁺⁰⁴	NM	1.7779	1.7646	2.9170 ⁺⁰²	1.4419 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	6.0594 ⁻⁰⁴	NC	0.0312	8.3285 ⁻⁰⁴	5.4893 ⁺⁰²	2.7851 ⁺⁰²	
74010214	2.2700	1.0468	1.1530 ⁺⁰⁴	1.4000 ⁻⁰³	3.6738	1.3683	2.5815 ⁺⁰⁴	2.5815 ⁺⁰⁴	
1.6510 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	2.0748 ⁺⁰⁴	NM	1.7805	1.7679	2.9160 ⁺⁰²	1.4484 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	6.1439 ⁻⁰⁴	NC	0.0186	8.4268 ⁻⁰⁴	5.4774 ⁺⁰²	2.7858 ⁺⁰²	
74010215	2.2100	1.0452	1.3467 ⁺⁰⁴	1.3950 ⁻⁰³	3.6765	1.3960	2.8357 ⁺⁰⁴	2.8357 ⁺⁰⁴	
1.7760 ⁻⁰¹	3.0800 ⁺⁰⁵	1.0000	2.3654 ⁺⁰⁴	NM	1.7687	1.7546	2.9160 ⁺⁰²	1.4877 ⁺⁰²	
INFINITE	2.9410 ⁺⁰²	0.0000	6.8087 ⁻⁰⁴	NC	-0.0111	9.3861 ⁻⁰⁴	5.4044 ⁺⁰²	2.7899 ⁺⁰²	

CAT 7401

THOMAS

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * PUD* TOP*	TW/TR PW/PD* SW * DZ	PER2K PER2D DZ	CF * CN PIZ	H12 H32 H42	H12K H32K D2K	PW TW* UD	PD TD TR
74010301 0.0000*-00 INFINITE	2.5700 4.1200*+05 2.9020*+02	1.0534 1.0000 0.0000	7.8294*+03 1.5946*+04 4.0427*+04	1.5400*-03 NM NC	4.2753 1.8009 0.0230	1.3585 1.7854 5.8024*-04	2.1630*+04 2.8760*+02 5.7618*+02	2.1630*+04 1.2503*+02 2.7302*+02
74010302 1.2700*-02 INFINITE	2.6100 4.1200*+05 2.9020*+02	1.0546 1.0000 0.0000	7.4201*+03 1.5367*+04 3.9794*+04	1.5400*-03 NM NC	4.3007 1.8106 0.0310	1.3368 1.7965 5.6773*-04	2.0330*+04 2.8770*+02 5.7999*+02	2.0330*+04 1.2284*+02 2.7279*+02
74010303 2.5400*-02 INFINITE	2.5800 4.1200*+05 2.9020*+02	1.0543 1.0000 0.0000	8.4180*+03 1.7225*+04 4.3901*-04	1.5600*-03 NM NC	4.2646 1.8081 0.0240	1.3393 1.7932 6.2718*-04	2.1297*+04 2.8780*+02 5.7714*+02	2.1297*+04 1.2448*+02 2.7297*+02
74010304 3.8100*-02 INFINITE	2.6100 4.1200*+05 2.9020*+02	1.0554 1.0000 0.0000	7.7180*+03 1.5993*+04 4.1414*+04	1.5900*-03 NM NC	4.3757 1.8114 0.0043	1.3365 1.7964 5.9432*-04	2.0330*+04 2.8790*+02 5.7999*+02	2.0330*+04 1.2284*+02 2.7279*+02
74010305 5.0800*-02 INFINITE	2.6100 4.1200*+05 2.9020*+02	1.0557 1.0000 0.0000	9.0069*+03 1.8668*+04 4.8344*+04	1.6000*-03 NM NC	4.2318 1.8099 0.0533	1.3293 1.7954 6.8809*-04	2.0330*+04 2.8800*+02 5.7999*+02	2.0330*+04 1.2284*+02 2.7279*+02
74010306 6.3500*-02 INFINITE	2.6700 4.1200*+05 2.9020*+02	1.0574 1.0000 0.0000	7.7906*+03 1.8555*+04 4.4265*+04	1.5950*-03 NM NC	4.4879 1.8265 -0.0085	1.3057 1.8119 6.3159*-04	1.8532*+04 2.8810*+02 5.8552*+02	1.8532*+04 1.1963*+02 2.7246*+02
74010307 7.6200*-02 INFINITE	2.7200 4.1200*+05 2.9020*+02	1.0588 1.0000 0.0000	7.5048*+03 1.8284*+04 4.4722*+04	1.5850*-03 NM NC	4.6149 1.8365 -0.0256	1.2845 1.8231 6.3851*-04	1.7160*+04 2.8820*+02 5.8997*+02	1.7160*+04 1.1703*+02 2.7219*+02
74010308 8.8900*-02 INFINITE	2.7700 4.1200*+05 2.9020*+02	1.0602 1.0000 0.0000	7.7780*+03 1.7232*+04 4.4617*+04	1.5900*-03 NM NC	4.5552 1.8382 0.0367	1.2831 1.8220 6.9360*-04	1.5894*+04 2.8830*+02 5.9427*+02	1.5894*+04 1.1450*+02 2.7193*+02
74010309 1.0160*-01 INFINITE	2.8400 4.1200*+05 2.9020*+02	1.0620 1.0000 0.0000	7.2846*+03 1.6615*+04 4.8682*+04	1.5900*-03 NM NC	4.7223 1.8440 0.0273	1.2689 1.8301 6.9792*-04	1.4284*+04 2.8840*+02 6.0006*+02	1.4284*+04 1.1105*+02 2.7157*+02
74010310 1.1430*-01 INFINITE	2.9000 4.1200*+05 2.9020*+02	1.0635 1.0000 0.0000	7.1275*+03 1.6688*+04 5.0447*+04	1.5800*-03 NM NC	4.7929 1.8464 0.0493	1.2673 1.8315 7.2426*-04	1.3040*+04 2.8850*+02 6.0483*+02	1.3040*+04 1.0820*+02 2.7127*+02
74010311 1.2700*-01 INFINITE	2.9600 4.1200*+05 2.9020*+02	1.0650 1.0000 0.0000	6.9357*+03 1.6628*+04 5.1992*+04	1.5800*-03 NM NC	4.8672 1.8536 0.0647	1.2539 1.8387 7.4515*-04	1.1911*+04 2.8860*+02 6.0940*+02	1.1911*+04 1.0544*+02 2.7098*+02
74010312 1.3970*-01 INFINITE	3.0100 4.1200*+05 2.9020*+02	1.0663 1.0000 0.0000	6.7756*+03 1.6585*+04 5.3283*+04	1.5750*-03 NM NC	4.9599 1.8560 0.0735	1.2510 1.8402 7.6814*-04	1.1049*+04 2.8870*+02 6.1308*+02	1.1049*+04 1.0320*+02 2.7075*+02
74010313 1.5240*-01 INFINITE	3.0500 4.1200*+05 2.9020*+02	1.0674 1.0000 0.0000	6.5898*+03 1.6401*+04 5.3847*+04	1.5650*-03 NM NC	5.1620 1.8598 0.0362	1.2440 1.8441 7.8146*-04	1.0408*+04 2.8880*+02 6.1594*+02	1.0408*+04 1.0145*+02 2.7057*+02
74010314 1.6510*-01 INFINITE	3.1000 4.1200*+05 2.9020*+02	1.0686 1.0000 0.0000	6.4730*+03 1.6956*+04 5.7199*+04	1.5500*-03 NM NC	5.1780 1.8584 0.0729	1.2469 1.8413 8.3453*-04	9.6609*+03 2.8890*+02 6.1941*+02	9.6609*+03 9.9316*+01 2.7035*+02
74010315 1.7780*-01 INFINITE	3.1300 4.1200*+05 2.9020*+02	1.0695 1.0000 0.0000	6.4931*+03 1.6706*+04 5.7202*+04	1.5350*-03 NM NC	5.5413 1.8578 -0.0149	1.2485 1.8405 8.5200*-04	9.2405*+03 2.8900*+02 6.2144*+02	9.2405*+03 9.8061*+01 2.7022*+02
74010316 1.9050*-01 INFINITE	3.1700 4.1200*+05 2.9020*+02	1.0706 1.0000 0.0000	6.6873*+03 1.7493*+04 6.1294*+04	1.5200*-03 NM NC	5.0774 1.8587 0.1530	1.2436 1.8419 8.8840*-04	8.7101*+03 2.8910*+02 6.2409*+02	8.7101*+03 9.6419*+01 2.7005*+02
74010317 2.0320*-01 INFINITE	3.2200 4.1200*+05 2.9020*+02	1.0718 1.0000 0.0000	6.4555*+03 1.7185*+04 6.1864*+04	1.5100*-03 NM NC	5.1767 1.8597 0.1618	1.2456 1.8413 9.0269*-04	8.0927*+03 2.8920*+02 6.2731*+02	8.0927*+03 9.4415*+01 2.6984*+02
74010318 2.1590*-01 INFINITE	3.2400 4.1200*+05 2.9020*+02	1.0724 1.0000 0.0000	7.5749*+03 2.0397*+04 7.4228*+04	1.5000*-03 NM NC	4.6268 1.8559 0.3354	1.2438 1.8378 1.0561*-03	7.8590*+03 2.8930*+02 6.2857*+02	7.8590*+03 9.3627*+01 2.6976*+02

74010101		THOMAS		PROFILE TABULATION		29 POINTS, DELTA AT POINT 29			
I	Y	PTZ/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000+00	1.0000+00	NM	0.99212	0.00000	0.00000	2.29251	0.00000	
2	1.0000+04	1.7555+00	NM	0.99720	0.36481	0.51100	1.96200	0.26045	
3	2.0000+04	1.9767+00	NM	0.99112	0.40497	0.55600	1.88500	0.29496	
4	3.0000+04	2.2451+00	NM	0.98664	0.44622	0.60000	1.80000	0.33186	
5	4.0000+04	2.5069+00	NM	0.98332	0.48197	0.65000	1.74200	0.36510	
6	5.0000+04	2.7469+00	NM	0.98135	0.51184	0.66500	1.68800	0.39396	
7	6.0000+04	2.9429+00	NM	0.97884	0.53486	0.68000	1.64500	0.41702	
8	8.0000+04	3.2008+00	NM	0.97571	0.56351	0.71100	1.59200	0.44661	
9	1.0000+03	3.4392+00	NM	0.97855	0.58861	0.73400	1.55500	0.47203	
10	1.2000+03	3.6632+00	NM	0.98115	0.61117	0.75400	1.52200	0.49540	
11	1.4000+03	3.8805+00	NM	0.98332	0.63223	0.77200	1.44100	0.51777	
12	1.6000+03	4.1276+00	NM	0.98545	0.65531	0.79100	1.45700	0.54240	
13	1.8000+03	4.3864+00	NM	0.98783	0.67508	0.80700	1.42900	0.56473	
14	2.0000+03	4.5997+00	NM	0.98971	0.69715	0.82400	1.39700	0.58484	
15	2.2000+03	4.8319+00	NM	0.99218	0.71681	0.83900	1.37000	0.61241	
16	2.4000+03	5.0659+00	NM	0.99393	0.73606	0.85300	1.34300	0.63515	
17	2.6000+03	5.3453+00	NM	0.99657	0.75038	0.86900	1.31300	0.66194	
18	2.8000+03	5.5909+00	NM	0.99823	0.77746	0.88200	1.28700	0.68531	
19	3.0000+03	5.8176+00	NM	0.99861	0.79466	0.89200	1.26000	0.70794	
20	3.3000+03	6.2099+00	NM	0.99813	0.82354	0.91000	1.22100	0.74524	
21	3.6000+03	6.6405+00	NM	0.99724	0.85410	0.92700	1.17800	0.78693	
22	3.9000+03	7.0573+00	NM	0.99626	0.88265	0.94200	1.13900	0.82704	
23	4.2000+03	7.4927+00	NM	0.99446	0.91151	0.95600	1.10000	0.86909	
24	4.5000+03	7.9075+00	NM	0.99634	0.93817	0.97000	1.06900	0.90734	
25	4.8000+03	8.2877+00	NM	0.99596	0.96195	0.98100	1.04000	0.94327	
26	5.2000+03	8.5947+00	NM	0.99693	0.98073	0.99000	1.01900	0.97154	
27	5.6000+03	8.7909+00	NM	0.99850	0.99253	0.99600	1.00700	0.98908	
28	6.0000+03	8.8909+00	NM	0.99939	0.99850	0.99900	1.00100	0.99800	
D 29	6.4000+03	8.9161+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

74010115		THOMAS		PROFILE TABULATION		40 POINTS, DELTA AT POINT 40			
I	Y	PTZ/P	P/PO	T0/T00	M/MD	U/UD	T/TD	RHO/RHOD+U/UD	
1	0.0000+00	1.0000+00	NM	0.99212	0.00000	0.00000	2.77794	0.00000	
2	1.0000+04	1.6976+00	NM	0.99971	0.33404	0.51000	2.33100	0.21879	
3	2.0000+04	2.4882+00	NM	1.00291	0.40912	0.60100	2.15800	0.27850	
4	3.0000+04	2.9181+00	NM	1.00375	0.45398	0.65000	2.05000	0.31707	
5	4.0000+04	3.2841+00	NM	1.00170	0.48519	0.68100	1.97000	0.34569	
6	5.0000+04	3.4928+00	NM	0.99876	0.50906	0.70100	1.91200	0.36663	
7	6.0000+04	3.7817+00	NM	0.99711	0.53142	0.72300	1.85100	0.39060	
8	8.0000+04	4.1983+00	NM	0.99161	0.56469	0.75000	1.76400	0.42517	
9	1.0000+03	4.4226+00	NM	0.98336	0.58178	0.76100	1.71100	0.44477	
10	1.2000+03	4.7277+00	NM	0.98125	0.60421	0.77800	1.65800	0.46924	
11	1.4000+03	4.9734+00	NM	0.98044	0.62166	0.79100	1.61900	0.48857	
12	1.6000+03	5.1840+00	NM	0.98099	0.63623	0.80200	1.58400	0.50472	
13	1.8000+03	5.3927+00	NM	0.98065	0.65033	0.81200	1.55400	0.52085	
14	2.0000+03	5.5980+00	NM	0.98187	0.66390	0.82200	1.53300	0.53620	
15	2.2000+03	5.8120+00	NM	0.98322	0.67775	0.83200	1.50700	0.55209	
16	2.4000+03	6.0490+00	NM	0.98253	0.69024	0.84000	1.48100	0.56718	
17	2.6000+03	6.2080+00	NM	0.98480	0.70264	0.84900	1.46000	0.58151	
18	2.8000+03	6.3827+00	NM	0.98533	0.71333	0.85600	1.44000	0.59444	
19	3.0000+03	6.5588+00	NM	0.98628	0.72396	0.86300	1.42100	0.60732	
20	3.3000+03	6.7908+00	NM	0.98955	0.73771	0.87100	1.39400	0.62482	
21	3.6000+03	7.0580+00	NM	0.98753	0.75324	0.88100	1.36800	0.64401	
22	3.9000+03	7.3374+00	NM	0.98964	0.76913	0.89100	1.34200	0.66393	
23	4.2000+03	7.5873+00	NM	0.99027	0.78307	0.89900	1.31800	0.68209	
24	4.5000+03	7.8639+00	NM	0.99218	0.79821	0.90800	1.29400	0.70170	
25	4.8000+03	8.1012+00	NM	0.99286	0.81097	0.91500	1.27300	0.71877	
26	5.2000+03	8.4047+00	NM	0.99497	0.82711	0.92400	1.24800	0.74038	
27	5.6000+03	8.7264+00	NM	0.99639	0.84366	0.93300	1.22300	0.76288	
28	6.0000+03	9.0538+00	NM	0.99866	0.86028	0.94200	1.19900	0.78565	
29	6.4000+03	9.3700+00	NM	1.00018	0.87603	0.95000	1.17600	0.80782	
30	6.8000+03	9.6380+00	NM	1.00039	0.88916	0.95600	1.15600	0.82698	
31	7.2000+03	1.0025+01	NM	1.00222	0.90780	0.96500	1.13000	0.85398	
32	7.6000+03	1.0339+01	NM	1.00379	0.92258	0.97200	1.11000	0.87568	
33	8.0000+03	1.0586+01	NM	1.00434	0.93408	0.97700	1.09400	0.89305	
34	8.5000+03	1.1021+01	NM	1.00443	0.95402	0.98500	1.06600	0.92402	
35	9.0000+03	1.1343+01	NM	1.00527	0.96850	0.99100	1.04700	0.94651	
36	9.5000+03	1.1612+01	NM	1.00430	0.98040	0.99500	1.03000	0.96602	
37	1.0000+02	1.1799+01	NM	1.00222	0.98863	0.99700	1.01700	0.98033	
38	1.0500+02	1.1901+01	NM	1.00100	0.99305	0.99800	1.01000	0.98812	
39	1.1000+02	1.1985+01	NM	1.00050	0.99651	0.99900	1.00500	0.99403	
D 40	1.1500+02	1.2061+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

74010208		THOMAS		PROFILE TABULATION		32 POINTS, DELTA AT POINT 32			
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.99286	0.00000	0.00000	2.14619	0.00000	
2	1.0000+04	1.7260+00	NM	0.99864	0.38115	0.51800	1.84700	0.28045	
3	2.0000+04	1.9975+00	NM	0.99726	0.43382	0.57700	1.76900	0.32617	
4	3.0000+04	2.1488+00	NM	0.99387	0.45898	0.60300	1.72600	0.34936	
5	4.0000+04	2.2919+00	NM	0.99081	0.48105	0.62500	1.68800	0.37026	
6	5.0000+04	2.4273+00	NM	0.98804	0.50075	0.64400	1.65400	0.38936	
7	6.0000+04	2.5120+00	NM	0.98600	0.51256	0.65500	1.63300	0.40110	
8	8.0000+04	2.7463+00	NM	0.98374	0.54363	0.68400	1.58300	0.43209	
9	1.0000+03	2.9446+00	NM	0.98167	0.56836	0.70600	1.54300	0.45755	
10	1.2000+03	3.1112+00	NM	0.98255	0.58821	0.72400	1.51500	0.47789	
11	1.4000+03	3.3081+00	NM	0.98398	0.61074	0.74400	1.48400	0.50135	
12	1.6000+03	3.4883+00	NM	0.98418	0.62733	0.75800	1.46000	0.51918	
13	1.8000+03	3.6295+00	NM	0.98671	0.64567	0.77400	1.43700	0.53862	
14	2.0000+03	3.7930+00	NM	0.98782	0.66268	0.78800	1.41400	0.55728	
15	2.2000+03	3.9838+00	NM	0.99081	0.68194	0.80400	1.39000	0.57842	
16	2.4000+03	4.1500+00	NM	0.99202	0.69827	0.81700	1.36900	0.59679	
17	2.6000+03	4.3643+00	NM	0.99190	0.71874	0.83200	1.34000	0.62090	
18	2.8000+03	4.5345+00	NM	0.99345	0.73461	0.84400	1.32000	0.63939	
19	3.0000+03	4.7417+00	NM	0.99562	0.75339	0.85800	1.29700	0.66153	
20	3.3000+03	5.0660+00	NM	0.99762	0.78187	0.87800	1.26100	0.69627	
21	3.6000+03	5.3504+00	NM	1.00086	0.80601	0.89500	1.23300	0.72567	
22	3.9000+03	5.6648+00	NM	1.00303	0.83185	0.91200	1.20200	0.75874	
23	4.2000+03	5.9997+00	NM	1.00531	0.85899	0.92900	1.17100	0.79334	
24	4.5000+03	6.3148+00	NM	1.00571	0.88281	0.94300	1.14100	0.82647	
25	4.8000+03	6.5966+00	NM	1.00639	0.90401	0.95500	1.11600	0.85573	
26	5.2000+03	7.0228+00	NM	1.00340	0.93512	0.97000	1.07600	0.90149	
27	5.6000+03	7.3652+00	NM	1.00700	0.95937	0.98400	1.05200	0.93536	
28	6.0000+03	7.6758+00	NM	1.00604	0.98085	0.99400	1.02700	0.96787	
29	6.4000+03	7.8261+00	NM	1.00233	0.99107	0.99700	1.01200	0.98518	
30	6.8000+03	7.9067+00	NM	1.00124	0.99641	0.99900	1.00500	0.99403	
31	7.2000+03	7.9512+00	NM	1.00046	0.99930	1.00000	1.00100	0.99900	
D 32	7.6000+03	7.9587+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

74010215		THOMAS		PROFILE TABULATION		36 POINTS, DELTA AT POINT 36			
I	Y	PT2/P	P/PO	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.99150	0.00000	0.00000	1.96002	0.00000	
2	1.0000+04	1.5212+00	NM	1.00369	0.36106	0.47900	1.76000	0.27216	
3	2.0000+04	1.7092+00	NM	1.00347	0.41162	0.53700	1.70200	0.31551	
4	3.0000+04	1.8774+00	NM	1.00229	0.44929	0.57800	1.65500	0.34924	
5	4.0000+04	1.9996+00	NM	1.00018	0.47347	0.60300	1.62200	0.37176	
6	5.0000+04	2.0971+00	NM	0.99842	0.49140	0.62100	1.59700	0.38885	
7	6.0000+04	2.1804+00	NM	0.99598	0.50598	0.63500	1.57900	0.40317	
8	8.0000+04	2.3146+00	NM	0.99384	0.52891	0.65700	1.54300	0.42579	
9	1.0000+03	2.4683+00	NM	0.99218	0.55238	0.67900	1.51100	0.44937	
10	1.2000+03	2.5670+00	NM	0.99137	0.56643	0.69200	1.49200	0.46381	
11	1.4000+03	2.6560+00	NM	0.99004	0.58006	0.70400	1.47300	0.47794	
12	1.6000+03	2.7581+00	NM	0.98925	0.59586	0.71800	1.45400	0.49449	
13	1.8000+03	2.8561+00	NM	0.99004	0.60792	0.72900	1.43800	0.50695	
14	2.0000+03	2.9631+00	NM	0.99139	0.62223	0.74200	1.42200	0.52180	
15	2.2000+03	3.0648+00	NM	0.99081	0.63549	0.75300	1.40400	0.53632	
16	2.4000+03	3.1717+00	NM	0.99182	0.64910	0.76500	1.38900	0.55076	
17	2.6000+03	3.2914+00	NM	0.99364	0.66396	0.77800	1.37300	0.56664	
18	2.8000+03	3.4241+00	NM	0.99340	0.68003	0.79100	1.35300	0.58463	
19	3.0000+03	3.5367+00	NM	0.99468	0.69534	0.80200	1.33800	0.59940	
20	3.3000+03	3.7103+00	NM	0.99585	0.71333	0.81800	1.31500	0.62205	
21	3.6000+03	3.9274+00	NM	0.99773	0.73751	0.83700	1.29600	0.64984	
22	3.9000+03	4.1409+00	NM	0.99826	0.76050	0.85400	1.26100	0.67724	
23	4.2000+03	4.3697+00	NM	1.00098	0.78435	0.87200	1.23600	0.70550	
24	4.5000+03	4.5992+00	NM	1.00363	0.80751	0.88900	1.21200	0.73350	
25	4.8000+03	4.8248+00	NM	1.00488	0.82974	0.90400	1.18700	0.76158	
26	5.2000+03	5.1422+00	NM	1.00615	0.85977	0.92400	1.15500	0.80000	
27	5.6000+03	5.4621+00	NM	1.00851	0.88907	0.94300	1.12500	0.83822	
28	6.0000+03	5.7459+00	NM	1.00894	0.91425	0.95800	1.09000	0.87250	
29	6.4000+03	6.0240+00	NM	1.00767	0.93826	0.97100	1.07100	0.90663	
30	6.8000+03	6.3244+00	NM	1.00607	0.96350	0.98400	1.04300	0.94343	
31	7.2000+03	6.5289+00	NM	1.00477	0.97983	0.99200	1.02500	0.96780	
32	7.6000+03	6.6129+00	NM	1.00316	0.98713	0.99500	1.01000	0.97933	
33	8.0000+03	6.6861+00	NM	1.00169	0.99304	0.99700	1.00800	0.98909	
34	8.5000+03	6.7418+00	NM	1.00053	0.99750	0.99900	1.00300	0.99601	
35	9.0000+03	6.7668+00	NM	1.00051	0.99930	1.00000	1.00100	0.99900	
D 36	9.5000+03	6.7730+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

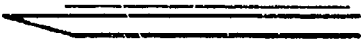
INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

74010306		THOMAS		PROFILE TABULATION		33 POINTS, DELTA AT POINT 33			
I	Y	PT2/P	P/PU	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.99276	0.00000	0.00000	2.40823	0.00000	
2	1.0000-04	2.0880+00	NM	0.99885	0.40540	0.56800	1.96300	0.28935	
3	2.0000-04	2.6029+00	NM	1.00235	0.47377	0.64300	1.84200	0.34908	
4	3.0000-04	2.8434+00	NM	0.99887	0.50176	0.67000	1.78300	0.37577	
5	4.0000-04	3.1176+00	NM	0.99706	0.53160	0.69800	1.72400	0.40487	
6	5.0000-04	3.3566+00	NM	0.99561	0.55615	0.72000	1.67600	0.42959	
7	6.0000-04	3.5489+00	NM	0.99363	0.57507	0.73600	1.63800	0.44933	
8	8.0000-04	3.8270+00	NM	0.99021	0.60129	0.75700	1.58500	0.47760	
9	1.0000-03	4.0822+00	NM	0.98828	0.62431	0.77500	1.54100	0.50292	
10	1.2000-03	4.2767+00	NM	0.98745	0.64127	0.78800	1.51000	0.52185	
11	1.4000-03	4.4816+00	NM	0.98681	0.65864	0.80100	1.47900	0.54158	
12	1.6000-03	4.6733+00	NM	0.98747	0.67446	0.81300	1.45300	0.55953	
13	1.8000-03	4.8543+00	NM	0.98858	0.68906	0.82400	1.43000	0.57622	
14	2.0000-03	5.0398+00	NM	0.99023	0.70370	0.83500	1.40800	0.59304	
15	2.2000-03	5.2397+00	NM	0.99121	0.71912	0.84600	1.38400	0.61127	
16	2.4000-03	5.4520+00	NM	0.99191	0.73514	0.85700	1.35900	0.63061	
17	2.6000-03	5.6118+00	NM	0.99259	0.74697	0.86500	1.34100	0.64504	
18	2.8000-03	5.8332+00	NM	0.99436	0.76304	0.87600	1.31800	0.66464	
19	3.0000-03	6.0181+00	NM	0.99626	0.77620	0.88500	1.30000	0.68077	
20	3.2000-03	6.3544+00	NM	0.99839	0.79957	0.90000	1.26700	0.71034	
21	3.6000-03	6.6454+00	NM	1.00194	0.81924	0.91300	1.24200	0.73510	
22	3.9000-03	6.9669+00	NM	1.00445	0.84043	0.92600	1.21400	0.76277	
23	4.2000-03	7.2661+00	NM	1.00578	0.85967	0.93700	1.18800	0.78872	
24	4.5000-03	7.6050+00	NM	1.00560	0.88096	0.94800	1.15800	0.81865	
25	4.8000-03	7.9533+00	NM	1.00833	0.90229	0.96000	1.13200	0.84806	
26	5.2000-03	8.3540+00	NM	1.00722	0.92623	0.97100	1.09900	0.88353	
27	5.6000-03	8.7584+00	NM	1.00748	0.94973	0.98200	1.06900	0.91862	
28	6.0000-03	9.1203+00	NM	1.00719	0.97036	0.99100	1.04300	0.95014	
29	6.4000-03	9.3514+00	NM	1.00403	0.98327	0.99500	1.02400	0.97168	
30	6.8000-03	9.4747+00	NM	1.00225	0.99009	0.99700	1.01400	0.98323	
31	7.2000-03	9.5735+00	NM	1.00171	0.99552	0.99900	1.00700	0.99206	
32	7.6000-03	9.6371+00	NM	1.00082	0.99900	1.00000	1.00200	0.99800	
D 33	8.0000-03	9.6554+00	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

74010317		THOMAS		PROFILE TABULATION		44 POINTS, DELTA AT POINT 44			
I	Y	PT2/P	P/PU	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000+00	1.0000+00	NM	0.99635	0.00000	0.00000	3.06309	0.00000	
2	1.0000-04	2.4938+00	NM	0.99451	0.38175	0.57300	2.25300	0.25433	
3	2.0000-04	2.8997+00	NM	0.99781	0.42126	0.61800	2.15200	0.28717	
4	3.0000-04	3.3171+00	NM	0.96110	0.45786	0.65700	2.05900	0.31909	
5	4.0000-04	3.7315+00	NM	0.96311	0.49123	0.69000	1.97300	0.34972	
6	5.0000-04	4.0681+00	NM	0.96534	0.51663	0.71400	1.91000	0.37382	
7	6.0000-04	4.3306+00	NM	0.96662	0.53556	0.73100	1.86300	0.39236	
8	8.0000-04	4.7413+00	NM	0.96791	0.56384	0.75500	1.79300	0.42108	
9	1.0000-03	5.0891+00	NM	0.96792	0.58668	0.77300	1.73600	0.44528	
10	1.2000-03	5.4150+00	NM	0.96917	0.60728	0.78900	1.68800	0.46742	
11	1.4000-03	5.7163+00	NM	0.97086	0.62570	0.80300	1.64700	0.48755	
12	1.6000-03	5.9722+00	NM	0.97180	0.64093	0.81400	1.61300	0.50465	
13	1.8000-03	6.1956+00	NM	0.97231	0.65392	0.82300	1.58400	0.51957	
14	2.0000-03	6.4649+00	NM	0.97452	0.66924	0.83400	1.55300	0.53703	
15	2.2000-03	6.7099+00	NM	0.97527	0.68287	0.84300	1.52400	0.55315	
16	2.4000-03	6.9421+00	NM	0.97563	0.69553	0.85100	1.49700	0.56847	
17	2.6000-03	7.1859+00	NM	0.97654	0.70647	0.85800	1.47500	0.58169	
18	2.8000-03	7.3316+00	NM	0.97700	0.71628	0.86400	1.45500	0.59381	
19	3.0000-03	7.4828+00	NM	0.97797	0.72417	0.86900	1.44000	0.60347	
20	3.3000-03	7.7323+00	NM	0.97958	0.73700	0.87700	1.41600	0.61935	
21	3.6000-03	8.0188+00	NM	0.97966	0.75146	0.88500	1.38700	0.63807	
22	3.9000-03	8.2670+00	NM	0.98057	0.76376	0.89200	1.36400	0.65396	
23	4.2000-03	8.5187+00	NM	0.98187	0.77604	0.89900	1.34200	0.66990	
24	4.5000-03	8.8108+00	NM	0.98381	0.79004	0.90700	1.31800	0.68816	
25	4.8000-03	9.0575+00	NM	0.98434	0.80168	0.91300	1.29700	0.70393	
26	5.2000-03	9.2994+00	NM	0.98558	0.81292	0.91900	1.27800	0.71909	
27	5.6000-03	9.4394+00	NM	0.98708	0.82647	0.92700	1.25200	0.74042	
28	6.0000-03	9.9010+00	NM	0.98843	0.84023	0.93300	1.23300	0.75669	
29	6.4000-03	1.0216+01	NM	0.99012	0.85419	0.94000	1.21100	0.77622	
30	6.8000-03	1.0531+01	NM	0.99027	0.86793	0.94600	1.18800	0.79630	
31	7.2000-03	1.0833+01	NM	0.99144	0.88088	0.95200	1.16800	0.81507	
32	7.6000-03	1.1078+01	NM	0.99300	0.89125	0.95700	1.15300	0.83001	
33	8.0000-03	1.1401+01	NM	0.99427	0.90471	0.96300	1.13300	0.84996	
34	8.5000-03	1.1800+01	NM	0.99559	0.92110	0.97000	1.10900	0.87466	
35	9.0000-03	1.2137+01	NM	0.99532	0.93474	0.97500	1.08600	0.89614	
36	9.5000-03	1.2479+01	NM	0.99738	0.94837	0.98100	1.07000	0.91682	
37	1.0000-02	1.2809+01	NM	0.99816	0.96132	0.98600	1.05200	0.93726	
38	1.0500-02	1.3089+01	NM	0.99861	0.97218	0.99000	1.03700	0.95468	
39	1.1000-02	1.3302+01	NM	0.99905	0.98034	0.99300	1.02600	0.96784	
40	1.1500-02	1.3493+01	NM	0.99815	0.98762	0.99500	1.01500	0.98030	
41	1.2000-02	1.3675+01	NM	0.99758	0.99452	0.99700	1.00500	0.99204	
42	1.2500-02	1.3715+01	NM	0.99861	0.99601	0.99800	1.00400	0.99402	
43	1.3000-02	1.3794+01	NM	0.99865	0.99900	0.99900	1.00000	0.99900	
D 44	1.3500-02	1.3821+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,T/TD ASSUME P=PD

	M : 2.5 - 4.5 (6 values) R THETA X 10 ⁻³ : 5 - 30 TW/TR : 1	7402
		ZPG - AW
Continuous wind tunnel with flexible nozzle. W = 0.91, H = 1.22 m. 0.06 < P0 < 0.88 MN/m ² . T0 : 315 K. Air: Dew point 243 K. 6 < RE/m X 10 ⁻⁶ < 30.		
MABEY D.G., MEIER H.U. and SAWYER W.G. 1974. Experimental and theoretical studies of the boundary layer on a flat plate at Mach numbers from 2.5 to 4.5. RAE TR 74127. And Mabey D.G. private communications, Hastings & Sawyer - CAT 7006, Mabey et al. (1971), Mabey & Sawyer (1974).		

- 1 The test boundary layer was formed on a flat plate 1.65 m long and 0.889 m wide. It was mounted on the tunnel centre line with a gap of 13 mm on each side between the plate and the tunnel wall. The leading edge (X = 0) was chamfered at 10° with a 0.25 mm nose thickness. Twenty two removable instrument plugs (diameter 41.3 mm) were arranged in five longitudinal rows in the central 127 mm of the plate, which was a modification of that used by Hastings & Sawyer (CAT 7006). An attempt was made to minimize heat transfer by providing layers of heat insulation on the back surface of the plate and between the plate and its support. Surface roughness was within 0.64 μm except for the transition strip from X = 2.54 to 5.08 mm where
- 3 Ballotini (small glass spheres) of 0.28 mm diameter were distributed sparsely. All measurements were made in fully turbulent flow. The transition position was derived from surface hot-film measurements.
- 2 A comprehensive programme of improvements to the tunnel (Mabey & Sawyer 1974) had reduced total temperature fluctuations in the working section to about 0.1 %, and Mach number variations along the plate to about 0.3 %. The spanwise total temperature distribution across the empty tunnel in the plane of the plate was found to
- 5 be steady and uniform within ± 0.5 K. There was evidence of flow convergence towards the centre line. This was very slight but nevertheless its contribution to the momentum equation was up to 14 % at M = 4.
- 6 Twenty one static pressure tapings of 1 mm diameter were distributed over the whole plate surface. Surface temperatures were measured using chromel-alumel surface thermocouples. The results agreed well with those derived from the cold resistance of platinum surface hot films installed to detect the beginning and end of transition. Wall shear stress was found using two Kistler type 322 m 102 balances with an element diameter of 9.75 mm. Of the four FEB available, only two were used for the results presented here. These two gave consistent and repeatable readings to within 1 % at the higher stress levels (Mabey & Gaudet, 1975).
- 7 The profiles were measured with a combined Pitot and T0 probe (Meier 1969). The principle on which this operates is described in CAT 7003. For the probe used here, d₁ = 0.61, d₂ = 0.63, l = 20 mm. The first 13 mm of the probe were inclined downwards towards the surface at 3°22', and this portion was tapered so that at the back end d₁ = 1.2 mm. The probe support was circular (d = 2 mm) and passed through the surface of the instrument plug.
- 8 All the measurements were made on one row of plugs, on the centre line. The profile normals were at X = 0.368, 0.623, 0.876, 1.130 and 1.384 m. The balance centres were 12 mm downstream of the profile normals.
- 9 No correction has been made to the CF values to allow for the small systematic x difference, as the appropriate
- 10 adjustments would have been very much smaller than the likely error of the balance measurements. A probe displacement correction was applied by adding y = 0.15 d₁ to all ordinates.
- 12 The data were received as a private communication before the catalogue project came in to existence. The profiles are given in great detail - about 80 points each. The experimental scatter was very small, so at that time punched cards were prepared, as a general rule, only for every other data point. To save labour, the editors have chosen to use the existing card-deck, so that only about half the data-points are presented.
- 13 Some profiles which were not included in the original card-deck have been punched in full. The 72 profiles presented form 18 sets of up to five successive stations. For each of six Mach numbers, three different

values of unit Reynolds number are given. There is additionally (0100) one odd profile at a specially low unit Reynolds number providing a check on low Reynolds number effects. The authors present an additional 19 profiles which were influenced by flow from the gap between the tunnel wall and the side of the plate. This effect was eliminated by the addition of fences on the plate, and only those runs with the fences 14 are presented here. The CF value is the authors', obtained by interpolation on the basis of unit Reynolds number.

§ DATA 7402 0100-1805. NX up to 5. PT2 and T0 profiles taken with the same probe. CF obtained separately with FEB.

15 Editors' comments

The tests described here provide a very large pool of very carefully observed basic flat plate data. In the earlier tests by Hastings & Sawyer - CAT 7006, an enthalpy deficit was observed in the boundary layer. In these later tests, special efforts were made to eliminate the possibility of heat-transfer. Nevertheless, an enthalpy deficit was still observed. This has been ascribed to various possible instrumental effects, but represents a minor departure from the first law of thermodynamics as compared to many other experiments. Some further measurements have been made using an ECP for the T0 profile (private communication). The apparent enthalpy deficit is reduced but not eliminated.*

The profiles were originally described in very fine detail (see § 12 above) and conform in most respects to the behaviour expected of a ZPG layer. On a transformed wall-law plot, series 16 appears non-characteristic, showing a "hump" in the innermost part of the log-law region. Some slight disturbance is also visible in 1301/03/05 and 1001.

The comment above is in no way intended to be adverse, and these must be regarded, for the present, as the basic source for adiabatic flat plate data in this range of Mach and Reynolds number.

*Note added in proof: These studies are described, together with the original experiment, by Mabey and Sawyer (1976) ARC R&M 37.84.

CAT 7402		HABEY		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	MD *	TN/TR	REN2h	CF *	H12	H12K	PM	PD		
X *	P0D	PN/PD*	RE02D	CO	H32	H32K	TM*	TD		
RZ	T0D*	SW *	D2	PI2	H42	D2K	UD	TR		
74020100	2.4701	1.0069	3.5148*+03	1.8000*-03	3.8319	1.3819	3.9084*+03	3.4084*+03		
8.7600*-01	6.3743*+04	1.0000	6.5823*+03	NM	1.7915	1.7755	2.4526*+02	1.4077*+02		
INFINITE	3.1100*+02	0.0000	1.1284*-03	0.0000*+00	0.1169	1.5564*-03	5.8614*+02	2.9322*+02		
74020101	2.4929	1.0133	3.0988*+03	1.8500*-03	3.9413	1.4577	7.6903*+03	7.6903*+03		
3.6800*-01	1.2995*+05	1.0000	5.8885*+03	NM	1.7925	1.7772	2.9506*+02	1.3777*+02		
INFINITE	3.0900*+02	0.0000	4.9677*-04	0.0000*+00	0.1268	6.8061*-04	5.8666*+02	2.9119*+02		
74020102	2.4920	1.0050	4.6668*+03	1.7200*-03	3.9023	1.3855	7.6339*+03	7.6339*+03		
6.2300*-01	1.2882*+05	1.0000	8.8087*+03	NM	1.8025	1.7887	2.9265*+02	1.3782*+02		
INFINITE	3.0900*+02	0.0000	7.4932*-04	0.0000*+00	0.1059	1.0281*-03	5.8657*+02	2.9120*+02		
74020103	2.4816	1.0015	6.0672*+03	1.6000*-03	3.9177	1.3445	7.7526*+03	7.7526*+03		
8.7600*-01	1.2872*+05	1.0000	1.1370*+04	NM	1.8121	1.7907	2.9265*+02	1.3891*+02		
INFINITE	3.1000*+02	0.0000	9.6706*-04	0.0000*+00	0.0700	1.3248*-03	5.8642*+02	2.9221*+02		
74020201	2.4947	1.0050	3.9386*+03	1.7200*-03	4.0047	1.4437	1.0170*+04	1.0170*+04		
3.6800*-01	1.7234*+05	1.0000	7.4423*+03	NM	1.8012	1.7860	2.9265*+02	1.3766*+02		
INFINITE	3.0900*+02	0.0000	4.7389*-04	0.0000*+00	0.1012	6.5317*-04	5.8685*+02	2.9118*+02		
74020202	2.4900	1.0017	5.9449*+03	1.6400*-03	3.9029	1.3944	1.0140*+04	1.0140*+04		
6.2300*-01	1.7057*+05	1.0000	1.1179*+04	NM	1.8038	1.7887	2.9265*+02	1.3839*+02		
INFINITE	3.1000*+02	0.0000	7.2070*-04	0.0000*+00	0.1072	9.8518*-04	5.8731*+02	2.9215*+02		
74020203	2.4939	1.0083	7.8437*+03	1.6200*-03	3.9154	1.3490	1.0195*+04	1.0195*+04		
8.7600*-01	1.7255*+05	1.0000	1.4861*+04	NM	1.8149	1.8013	2.9265*+02	1.3726*+02		
INFINITE	3.0800*+02	0.0000	9.4037*-04	0.0000*+00	0.0836	1.2864*-03	5.8582*+02	2.9024*+02		
74020301	2.4957	1.0083	4.7735*+03	1.6700*-03	4.0646	1.4430	1.2656*+04	1.2656*+04		
3.6800*-01	2.1479*+05	1.0000	9.0504*+03	NM	1.8036	1.7881	2.9265*+02	1.3715*+02		
INFINITE	3.0800*+02	0.0000	4.6858*-04	0.0000*+00	0.0802	6.3763*-04	5.8601*+02	2.9023*+02		
74020302	2.4974	1.0019	7.2433*+03	1.6000*-03	3.9122	1.3900	1.2753*+04	1.2753*+04		
6.2300*-01	2.1701*+05	1.0000	1.3662*+04	NM	1.8076	1.7926	2.9265*+02	1.3794*+02		
INFINITE	3.1000*+02	0.0000	6.9498*-04	0.0000*+00	0.1079	9.4994*-04	5.8808*+02	2.9211*+02		
74020303	2.5001	1.0019	9.0948*+03	1.5600*-03	3.8610	1.3446	1.2589*+04	1.2589*+04		
8.7600*-01	2.1513*+05	1.0000	1.7172*+04	NM	1.8172	1.8044	2.9265*+02	1.3777*+02		
INFINITE	3.1000*+02	0.0000	8.8247*-04	0.0000*+00	0.1039	1.1965*-03	5.8637*+02	2.9209*+02		
74020401	2.7820	1.0012	3.8751*+03	1.6300*-03	4.5214	1.3989	5.5606*+03	5.5606*+03		
6.2300*-01	1.4681*+05	1.0000	8.1563*+03	NM	1.8019	1.7843	2.9265*+02	1.2234*+02		
INFINITE	3.1200*+02	0.0000	7.2124*-04	0.0000*+00	0.1212	1.0523*-03	6.1724*+02	2.9229*+02		
74020402	2.7876	0.9981	5.0023*+03	1.5400*-03	4.4643	1.3497	5.5076*+03	5.5076*+03		
8.7600*-01	1.4666*+05	1.0000	1.0521*+04	NM	1.8114	1.7959	2.9265*+02	1.2255*+02		
INFINITE	3.1300*+02	0.0000	7.3844*-04	0.0000*+00	0.1118	1.3592*-03	6.1871*+02	2.9319*+02		
74020501	2.7933	1.0047	3.2220*+03	1.6600*-03	4.6023	1.4444	7.2803*+03	7.2803*+03		
3.6800*-01	1.9556*+05	1.0000	6.8333*+03	NM	1.8039	1.7854	2.9265*+02	1.2146*+02		
INFINITE	3.1100*+02	0.0000	4.5432*-04	0.0000*+00	0.1295	6.6649*-04	6.1723*+02	2.9129*+02		
74020502	2.7884	1.0014	4.9158*+03	1.5300*-03	4.5118	1.3957	7.3505*+03	7.3505*+03		
6.2300*-01	1.9598*+05	1.0000	1.0374*+04	NM	1.8058	1.7877	2.9265*+02	1.2211*+02		
INFINITE	3.1200*+02	0.0000	6.8958*-04	0.0000*+00	0.1296	1.0053*-03	6.1779*+02	2.9225*+02		
74020503	2.7915	0.9982	6.4362*+03	1.4800*-03	4.4999	1.3491	7.3149*+03	7.3149*+03		
8.7600*-01	1.9595*+05	1.0000	1.3559*+04	NM	1.8121	1.7974	2.9265*+02	1.2234*+02		
INFINITE	3.1300*+02	0.0000	9.0707*-04	0.0000*+00	0.1063	1.3096*-03	6.1905*+02	2.9317*+02		
74020601	2.7923	1.0079	3.9257*+03	1.5900*-03	4.6837	1.4441	9.1020*+03	9.1020*+03		
3.6800*-01	2.4413*+05	1.0000	8.3474*+03	NM	1.8040	1.7869	2.9265*+02	1.2112*+02		
INFINITE	3.1000*+02	0.0000	4.4230*-04	0.0000*+00	0.0950	6.4739*-04	6.1615*+02	2.9036*+02		
74020602	2.7898	1.0046	6.0846*+03	1.4800*-03	4.3616	1.3812	9.2160*+03	9.2160*+03		
6.1700*-01	2.4624*+05	1.0000	1.2886*+04	NM	1.8125	1.7953	2.9265*+02	1.2165*+02		
INFINITE	3.1100*+02	0.0000	6.7912*-04	0.0000*+00	0.1734	9.7532*-04	6.1692*+02	2.9131*+02		
74020603	2.7932	0.9983	7.8129*+03	1.4300*-03	4.4375	1.3816	9.0793*+03	9.0793*+03		
8.7600*-01	2.4385*+05	1.0000	1.6470*+04	NM	1.8191	1.8032	2.9265*+02	1.2225*+02		
INFINITE	3.1300*+02	0.0000	8.0626*-04	0.0000*+00	0.1292	1.2748*-03	6.1920*+02	2.9316*+02		

CAT 7402		MABEY BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.							
RUN X * RZ	MD * POD TOD*	TW/TR PW/PD* SW * DZ	RED2M RED2D	CF * CD PIZ	H1Z H3Z H4Z	H12K H32K D2K	PM TW* UD	PD TD TR	
74020701 3.6800*-01 INFINITE	2.9922 1.6683*+05 3.1200*+02	1.0026 1.0000 0.0000	2.3737*+03 5.4314*+03 4.7405*-04	1.6800*-03 NM 0.0000*+00	4.9490 1.8080 0.1604	1.4270 1.7888 7.1723*-04	4.5953*+03 2.9195*+02 6.3434*+02	4.5953*+03 1.1180*+02 2.9118*+02	
74020702 6.2300*-01 INFINITE	2.9863 1.6693*+05 3.1100*+02	1.0047 1.0000 0.0000	3.5460*+03 8.1124*+03 7.0211*-04	1.5500*-03 NM 0.0000*+00	4.9064 1.8097 0.1451	1.3763 1.7919 1.0624*-03	4.6388*+03 2.9185*+02 6.3288*+02	4.6388*+03 1.1173*+02 2.9028*+02	
74020703 8.7600*-01 INFINITE	2.9857 1.6641*+05 3.1400*+02	0.9943 1.0000 0.0000	4.3400*+03 1.0283*+04 9.0493*-04	1.4600*-03 NM 0.0000*+00	4.8943 1.8113 0.1423	1.3646 1.7917 1.3666*-03	4.6286*+03 2.9140*+02 6.3588*+02	4.6286*+03 1.1283*+02 2.9308*+02	
74020704 1.1300*+00 INFINITE	2.9593 1.6934*+05 3.1000*+02	1.0058 1.0000 0.0000	6.1329*+03 1.3901*+04 1.1632*-03	1.4100*-03 NM 0.0000*+00	4.8899 1.8062 0.1202	1.3546 1.7870 1.7666*-03	4.9008*+03 2.9115*+02 6.2979*+02	4.9008*+03 1.1267*+02 2.8948*+02	
74020801 3.6800*-01 INFINITE	2.9959 2.2324*+05 3.1100*+02	1.0059 1.0000 0.0000	2.9995*+03 6.8944*+03 4.4853*-04	1.5700*-03 NM 0.0000*+00	5.0294 1.8079 0.1429	1.4339 1.7885 6.8302*-04	6.1149*+03 2.9195*+02 6.3361*+02	6.1149*+03 1.1127*+02 2.9023*+02	
74020802 6.2300*-01 INFINITE	2.9910 2.2406*+05 3.1100*+02	1.0048 1.0000 0.0000	4.5040*+03 1.0335*+04 6.6813*-04	1.4700*-03 NM 0.0000*+00	4.9106 1.8113 0.1517	1.3834 1.7920 1.0109*-03	6.1826*+03 2.9185*+02 6.3324*+02	6.1826*+03 1.1150*+02 2.9025*+02	
74020803 8.7600*-01 INFINITE	2.9869 2.2431*+05 3.1300*+02	0.9975 1.0000 0.0000	5.9021*+03 1.3415*+04 6.7236*-04	1.3800*-03 NM 0.0000*+00	4.9115 1.8188 0.1292	1.3446 1.8006 1.3145*-03	6.2279*+03 2.9140*+02 6.3496*+02	6.2279*+03 1.1242*+02 2.9214*+02	
74020804 1.1300*+00 INFINITE	2.9702 2.2302*+05 3.1100*+02	1.0027 1.0000 0.0000	7.5206*+03 1.7071*+04 1.0961*-03	1.3700*-03 NM 0.0000*+00	4.8351 1.8152 0.1324	1.3346 1.7983 1.6411*-03	6.3494*+03 2.9115*+02 6.3165*+02	6.3494*+03 1.1250*+02 2.9036*+02	
74020901 3.6800*-01 INFINITE	2.9982 2.7764*+05 3.1000*+02	1.0092 1.0000 0.0000	3.5187*+03 8.1201*+03 4.2331*-04	1.4900*-03 NM 0.0000*+00	5.1791 1.8064 0.1035	1.4468 1.7863 6.4988*-04	7.5789*+03 2.9195*+02 6.3276*+02	7.5789*+03 1.1060*+02 2.8928*+02	
74020902 6.2300*-01 INFINITE	2.9943 2.7707*+05 3.1000*+02	1.0081 1.0000 0.0000	5.3560*+03 1.2331*+04 6.4278*-04	1.4200*-03 NM 0.0000*+00	4.9723 1.8109 0.1388	1.3936 1.7911 9.7445*-04	7.6076*+03 2.9185*+02 6.3247*+02	7.6076*+03 1.1099*+02 2.8930*+02	
74020903 8.7600*-01 INFINITE	2.9910 2.7777*+05 3.1300*+02	0.9975 1.0000 0.0000	7.2296*+03 1.6460*+04 8.6632*-04	1.3500*-03 NM 0.0000*+00	4.8716 1.8132 0.1514	1.3645 1.7940 1.3015*-03	7.6647*+03 2.9140*+02 6.3527*+02	7.6647*+03 1.1222*+02 2.9212*+02	
74020904 1.1300*+00 INFINITE	2.9732 2.7816*+05 3.1100*+02	1.0028 1.0000 0.0000	9.1120*+03 2.0708*+04 1.0679*-03	1.3400*-03 NM 0.0000*+00	4.7570 1.8214 0.1528	1.3233 1.8053 1.5813*-03	7.8836*+03 2.9115*+02 6.3188*+02	7.8836*+03 1.1236*+02 2.9034*+02	
74021001 3.6800*-01 INFINITE	3.4828 2.8811*+05 3.1300*+02	1.0098 1.0000 0.0000	2.2783*+03 6.3415*+03 4.2043*-04	1.4700*-03 NM 0.0000*+00	6.1576 1.8190 0.1717	1.4113 1.7975 7.0026*-04	3.8709*+03 2.9280*+02 6.6745*+02	3.8709*+03 9.1361*+01 2.8995*+02	
74021002 6.2300*-01 INFINITE	3.4917 2.8898*+05 3.1400*+02	1.0052 1.0000 0.0000	3.3643*+03 9.3574*+03 6.2440*-04	1.3500*-03 NM 0.0000*+00	6.1663 1.8132 0.1746	1.3925 1.7884 1.0517*-03	3.8338*+03 2.9235*+02 6.6971*+02	3.8338*+03 9.1322*+01 2.9084*+02	
74021003 8.7600*-01 INFINITE	3.4974 2.8631*+05 3.1700*+02	0.9942 1.0000 0.0000	4.3758*+03 1.2071*+04 8.2640*-04	1.2900*-03 NM 0.0000*+00	5.7448 1.8301 0.2279	1.2819 1.8216 1.3237*-03	3.7704*+03 2.9190*+02 6.7252*+02	3.7704*+03 9.1981*+01 2.9360*+02	
74021004 1.1300*+00 INFINITE	3.4888 2.8997*+05 3.1500*+02	0.9990 1.0000 0.0000	5.4676*+03 1.5109*+04 1.0079*-03	1.2300*-03 NM 0.0000*+00	5.9480 1.8205 0.2029	1.3358 1.7978 1.6690*-03	3.8628*+03 2.9150*+02 6.6991*+02	3.8628*+03 9.1721*+01 2.9178*+02	
74021101 3.6800*-01 INFINITE	3.4867 3.6082*+05 3.1400*+02	1.0067 1.0000 0.0000	2.7783*+03 7.6990*+03 4.1035*-04	1.3900*-03 NM 0.0000*+00	6.1832 1.8122 0.1900	1.4428 1.7867 6.9082*-04	4.8210*+03 2.9280*+02 6.6873*+02	4.8210*+03 9.1307*+01 2.9086*+02	
74021102 6.2300*-01 INFINITE	3.4955 3.6051*+05 3.1400*+02	1.0052 1.0000 0.0000	4.0028*+03 1.1150*+04 5.9781*-04	1.2900*-03 NM 0.0000*+00	6.1994 1.8167 0.1682	1.3817 1.7931 1.0058*-03	4.7569*+03 2.9235*+02 6.6922*+02	4.7569*+03 9.1181*+01 2.9083*+02	
74021103 8.7600*-01 INFINITE	3.5012 3.5950*+05 3.1600*+02	0.9974 1.0000 0.0000	5.2031*+03 1.4419*+04 7.8469*-04	1.2300*-03 NM 0.0000*+00	6.0338 1.8220 0.1907	1.3460 1.8008 1.2972*-03	4.7053*+03 2.9190*+02 6.7167*+02	4.7053*+03 9.1350*+01 2.9266*+02	
74021104 1.1300*+00 INFINITE	3.4907 3.6159*+05 3.1300*+02	1.0055 1.0000 0.0000	6.5344*+03 1.8194*+04 9.6518*-04	1.1900*-03 NM 0.0000*+00	6.0056 1.8224 0.1867	1.3369 1.7999 1.5927*-03	4.8039*+03 2.9150*+02 6.6789*+02	4.8039*+03 9.1088*+01 2.8992*+02	

CAT 7402		HABEY		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.					
RUN	MD *	TW/TR	RED2H	CF *	H12	H12K	PH	PD	
X *	PUD	PW/PD*	RED2D	CQ	H32	H32K	TH*	TD	
RZ	TOD*	SW *	DZ	PI2	H42	D2K	UD	TR	
74021201	3.4888	1.0067	3.2060 ⁺⁰³	1.3300 ⁻⁰³	6.2751	1.4288	5.8184 ⁺⁰³	5.8184 ⁺⁰³	
3.6800 ⁻⁰¹	4.3677 ⁺⁰⁵	1.0000	8.4175 ⁺⁰³	NM	1.8147	1.7926	2.9280 ⁺⁰²	9.1429 ⁺⁰¹	
INFINITE	3.1400 ⁺⁰²	0.0000	3.9308 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1604	6.6248 ⁻⁰⁴	6.6885 ⁺⁰²	2.9085 ⁺⁰²	
74021202	3.4978	1.0085	4.7335 ⁺⁰³	1.2500 ⁻⁰³	6.1010	1.3860	5.7027 ⁺⁰³	5.7027 ⁺⁰³	
6.2300 ⁻⁰¹	4.3360 ⁺⁰⁵	1.0000	1.3238 ⁺⁰⁴	NM	1.8194	1.7944	2.9235 ⁺⁰²	9.0808 ⁺⁰¹	
INFINITE	3.1300 ⁺⁰²	0.0000	5.8790 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.1922	9.6845 ⁻⁰⁴	6.6828 ⁺⁰²	2.8989 ⁺⁰²	
74021203	3.5029	0.9974	6.2503 ⁺⁰³	1.1900 ⁻⁰³	6.0382	1.3721	5.6621 ⁺⁰³	5.6621 ⁺⁰³	
8.7600 ⁻⁰¹	4.3364 ⁺⁰⁵	1.0000	1.7333 ⁺⁰⁴	NM	1.8188	1.7929	2.9190 ⁺⁰²	9.1486 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	7.8269 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2048	1.3018 ⁻⁰³	6.7176 ⁺⁰²	2.9265 ⁺⁰²	
74021204	3.4962	1.0023	7.6089 ⁺⁰³	1.1700 ⁻⁰³	5.9227	1.3350	5.7147 ⁺⁰³	5.7147 ⁺⁰³	
1.1300 ⁺⁰⁰	4.3353 ⁺⁰⁵	1.0000	2.1153 ⁺⁰⁴	NM	1.8260	1.8032	2.9150 ⁺⁰²	9.1155 ⁺⁰¹	
INFINITE	3.1400 ⁺⁰²	0.0000	9.4314 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2094	1.5401 ⁻⁰³	6.6926 ⁺⁰²	2.9108 ⁺⁰²	
74021301	3.4973	1.0084	1.6951 ⁺⁰³	1.4000 ⁻⁰³	7.2268	1.4173	2.4426 ⁺⁰³	2.4426 ⁺⁰³	
3.6800 ⁻⁰¹	3.8954 ⁺⁰⁵	1.0000	5.7141 ⁺⁰³	NM	1.8267	1.7976	2.9340 ⁺⁰²	7.5316 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	3.9279 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2743	7.0393 ⁻⁰⁴	6.9553 ⁺⁰²	2.9097 ⁺⁰²	
74021302	3.4853	1.0036	2.5602 ⁺⁰³	1.2600 ⁻⁰³	7.3378	1.3510	2.4838 ⁺⁰³	2.4838 ⁺⁰³	
6.2300 ⁻⁰¹	3.9980 ⁺⁰⁵	1.0000	8.5608 ⁺⁰³	NM	1.8284	1.8046	2.9205 ⁺⁰²	7.5661 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	5.8442 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2231	1.0650 ⁻⁰³	6.9504 ⁺⁰²	2.9100 ⁺⁰²	
74021303	3.4840	0.9933	3.2960 ⁺⁰³	1.1800 ⁻⁰³	7.2833	1.3582	2.4629 ⁺⁰³	2.4629 ⁺⁰³	
8.7600 ⁻⁰¹	3.6605 ⁺⁰⁵	1.0000	1.0913 ⁺⁰⁴	NM	1.8186	1.7926	2.9090 ⁺⁰²	7.6178 ⁺⁰¹	
INFINITE	3.1800 ⁺⁰²	0.0000	7.5928 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2344	1.3914 ⁻⁰³	6.9718 ⁺⁰²	2.9285 ⁺⁰²	
74021304	3.4869	0.9985	4.1841 ⁺⁰³	1.1200 ⁻⁰³	7.2528	1.3451	2.4679 ⁺⁰³	2.4679 ⁺⁰³	
1.1300 ⁺⁰⁰	3.6822 ⁺⁰⁵	1.0000	1.3954 ⁺⁰⁴	NM	1.8217	1.7932	2.8965 ⁺⁰²	7.5376 ⁺⁰¹	
INFINITE	3.1500 ⁺⁰²	0.0000	9.5294 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2418	1.7514 ⁻⁰³	6.9400 ⁺⁰²	2.9082 ⁺⁰²	
74021305	3.4888	0.9758	4.8600 ⁺⁰³	1.0700 ⁻⁰³	7.1988	1.3168	2.5158 ⁺⁰³	2.5158 ⁺⁰³	
1.3840 ⁺⁰⁰	3.6638 ⁺⁰⁵	1.0000	1.5750 ⁺⁰⁴	NM	1.8290	1.8024	2.8850 ⁺⁰²	7.7344 ⁺⁰¹	
INFINITE	3.2100 ⁺⁰²	0.0000	1.1015 ⁻⁰³	0.0000 ⁺⁰⁰	0.2295	1.4988 ⁻⁰³	6.9981 ⁺⁰²	2.9566 ⁺⁰²	
74021401	4.0034	1.0116	2.0929 ⁺⁰³	1.3000 ⁻⁰³	7.3910	1.4069	3.0175 ⁺⁰³	3.0175 ⁺⁰³	
3.6800 ⁻⁰¹	4.6025 ⁺⁰⁵	1.0000	7.0938 ⁺⁰³	NM	1.8246	1.7995	2.9340 ⁺⁰²	7.5661 ⁺⁰¹	
INFINITE	3.1500 ⁺⁰²	0.0000	3.9090 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2476	7.1203 ⁻⁰⁴	6.9469 ⁺⁰²	2.9103 ⁺⁰²	
74021402	3.9890	1.0036	3.1607 ⁺⁰³	1.1800 ⁻⁰³	7.3775	1.3712	3.0709 ⁺⁰³	3.0709 ⁺⁰³	
6.2300 ⁻⁰¹	4.3947 ⁺⁰⁵	1.0000	1.0584 ⁺⁰⁴	NM	1.8239	1.7926	2.9205 ⁺⁰²	7.5554 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	5.8262 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2375	1.0905 ⁻⁰³	6.9519 ⁺⁰²	2.9099 ⁺⁰²	
74021403	3.9887	0.9934	4.0408 ⁺⁰³	1.1200 ⁻⁰³	7.2649	1.3340	3.0537 ⁺⁰³	3.0537 ⁺⁰³	
8.7600 ⁻⁰¹	4.5672 ⁺⁰⁵	1.0000	1.3403 ⁺⁰⁴	NM	1.8253	1.8019	2.9090 ⁺⁰²	7.6041 ⁺⁰¹	
INFINITE	3.1800 ⁺⁰²	0.0000	7.4921 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2339	1.3677 ⁻⁰³	2.9284 ⁺⁰²	2.9084 ⁺⁰²	
74021404	3.9871	0.9954	5.0302 ⁺⁰³	1.0700 ⁻⁰³	7.2093	1.3387	3.0598 ⁺⁰³	3.0598 ⁺⁰³	
1.1300 ⁺⁰⁰	4.5665 ⁺⁰⁵	1.0000	1.6724 ⁺⁰⁴	NM	1.8241	1.7967	2.8965 ⁺⁰²	7.5609 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	9.2541 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2477	1.6901 ⁻⁰³	6.9511 ⁺⁰²	2.9100 ⁺⁰²	
74021405	3.9734	0.9789	5.9837 ⁺⁰³	1.0400 ⁻⁰³	7.2217	1.3284	3.1251 ⁺⁰³	3.1251 ⁺⁰³	
1.3840 ⁺⁰⁰	4.6093 ⁺⁰⁵	1.0000	1.9485 ⁺⁰⁴	NM	1.8259	1.7987	2.8850 ⁺⁰²	7.6968 ⁺⁰¹	
INFINITE	3.2000 ⁺⁰²	0.0000	1.0879 ⁻⁰³	0.0000 ⁺⁰⁰	0.2307	1.9780 ⁻⁰³	6.9892 ⁺⁰²	2.9472 ⁺⁰²	
74021501	4.0088	1.0117	2.7857 ⁺⁰³	1.1900 ⁻⁰³	7.3545	1.4417	4.1993 ⁺⁰³	4.1993 ⁺⁰³	
3.6800 ⁻⁰¹	6.4512 ⁺⁰⁵	1.0000	9.4613 ⁺⁰³	NM	1.8161	1.7859	2.9340 ⁺⁰²	7.4749 ⁺⁰¹	
INFINITE	3.1500 ⁺⁰²	0.0000	3.7298 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2299	6.9491 ⁻⁰⁴	6.9491 ⁺⁰²	2.9001 ⁺⁰²	
74021502	3.9951	1.0069	4.0773 ⁺⁰³	1.1100 ⁻⁰³	7.4974	1.4001	4.2486 ⁺⁰³	4.2486 ⁺⁰³	
6.2300 ⁻⁰¹	6.4089 ⁺⁰⁵	1.0000	1.3728 ⁺⁰⁴	NM	1.8166	1.7864	2.9205 ⁺⁰²	7.5140 ⁺⁰¹	
INFINITE	3.1500 ⁺⁰²	0.0000	9.4091 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2165	1.0068 ⁻⁰³	6.9434 ⁺⁰²	2.9005 ⁺⁰²	
74021503	3.9948	0.9935	5.4533 ⁺⁰³	1.0500 ⁻⁰³	7.2031	1.3441	4.2500 ⁺⁰³	4.2500 ⁺⁰³	
8.7600 ⁻⁰¹	6.4083 ⁺⁰⁵	1.0000	1.8131 ⁺⁰⁴	NM	1.8280	1.8017	2.9090 ⁺⁰²	7.5464 ⁺⁰¹	
INFINITE	3.1800 ⁺⁰²	0.0000	7.2494 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2549	1.3137 ⁻⁰³	6.9763 ⁺⁰²	2.9282 ⁺⁰²	
74021504	3.9929	0.9954	6.5636 ⁺⁰³	1.0300 ⁻⁰³	7.2446	1.3286	4.2624 ⁺⁰³	4.2624 ⁺⁰³	
1.1300 ⁺⁰⁰	6.4109 ⁺⁰⁵	1.0000	2.1870 ⁺⁰⁴	NM	1.8304	1.8048	2.8965 ⁺⁰²	7.5442 ⁺⁰¹	
INFINITE	3.1600 ⁺⁰²	0.0000	8.6459 ⁻⁰⁴	0.0000 ⁺⁰⁰	0.2357	1.5587 ⁻⁰³	6.9535 ⁺⁰²	2.9098 ⁺⁰²	
74021505	3.9810	0.9820	8.0893 ⁺⁰³	1.0000 ⁻⁰³	7.1309	1.3187	4.3384 ⁺⁰³	4.3384 ⁺⁰³	
1.3840 ⁺⁰⁰	6.4223 ⁺⁰⁵	1.0000	2.6500 ⁺⁰⁴	NM	1.8325	1.8061	2.8850 ⁺⁰²	7.6505 ⁺⁰¹	
INFINITE	3.1900 ⁺⁰²	0.0000	1.0541 ⁻⁰³	0.0000 ⁺⁰⁰	0.2475	1.8821 ⁻⁰³	6.9815 ⁺⁰²	2.9378 ⁺⁰²	

CAT 7402

HABEY

BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.

RUN X * RZ	MD * POD TOD*	TW/TR PW/PD* SW *	RED2W RED2D D2	CF * CO PI2	H12 H32 H42	H12K H32K O2K	PW TW* UD	PD TD TR
74021601 3.6800*-01 INFINITE	4.4967 4.6220*+05 3.1500*+02	1.0208 1.0000 0.0000	1.0792*+03 4.4028*+03 3.0942*-04	1.3700*-03 NM 0.0000*+00	8.4073 1.8447 0.3512	1.4254 1.8092 5.9010*-04	1.6036*+03 2.9473*+02 7.1247*+02	1.6036*+03 6.2450*+01 2.6873*+02
74021602 6.2300*-01 INFINITE	4.4898 4.6022*+05 3.1600*+02	1.0127 1.0000 0.0000	1.7891*+03 7.2311*+03 5.1109*-04	1.2400*-03 NM 0.0000*+00	8.3617 1.8324 0.3464	1.3942 1.7944 9.9601*-04	1.6106*+03 2.9335*+02 7.1339*+02	1.6106*+03 6.2802*+01 2.6867*+02
74021603 8.7600*-01 INFINITE	4.4851 4.6103*+05 3.1800*+02	1.0027 1.0000 0.0000	2.3256*+03 9.2968*+03 6.6083*-04	1.1500*-03 NM 0.0000*+00	8.4056 1.8352 0.3189	1.3408 1.8046 1.2933*-03	1.6229*+03 2.9230*+02 7.1549*+02	1.6229*+03 6.3306*+01 2.9151*+02
74021604 1.1300*+00 INFINITE	4.4835 4.6259*+05 3.1500*+02	1.0088 1.0000 0.0000	3.0658*+03 1.2335*+04 8.6063*-04	1.0500*-03 NM 0.0000*+00	8.5812 1.8285 0.2956	1.3558 1.7927 7.1206*+02	1.6316*+03 2.9130*+02 7.1206*+02	1.6316*+03 6.2745*+01 2.8877*+02
74021605 1.3840*+00 INFINITE	4.4719 4.6134*+05 3.1800*+02	0.9920 1.0000 0.0000	3.5518*+03 1.4018*+04 9.8910*-04	1.0100*-03 NM 0.0000*+00	8.5780 1.8305 0.2841	1.3409 1.7958 1.9748*-03	1.6510*+03 2.8920*+02 7.1507*+02	1.6510*+03 6.3655*+01 2.9154*+02
74021701 3.6800*-01 INFINITE	4.5009 4.7819*+05 3.1500*+02	1.0209 1.0000 0.0000	1.5280*+03 6.2431*+03 3.5146*-04	1.3000*-03 NM 0.0000*+00	8.6529 1.8418 0.2980	1.3887 1.8126 6.6239*-04	1.9955*+03 2.9475*+02 7.1261*+02	1.9955*+03 6.2358*+01 2.8873*+02
74021702 8.7600*-01 INFINITE	4.4985 4.7754*+05 3.1500*+02	1.0210 1.0000 0.0000	2.3095*+03 9.4294*+03 5.3062*-04	1.1300*-03 NM 0.0000*+00	8.6799 1.8346 0.2822	1.3455 1.8068 1.0568*-03	1.9993*+03 2.9480*+02 7.1253*+02	1.9993*+03 6.2410*+01 2.8873*+02
74021703 8.7600*-01 INFINITE	4.4956 4.7967*+05 3.1800*+02	1.0028 1.0000 0.0000	2.9413*+03 1.1805*+04 6.7064*-04	1.0600*-03 NM 0.0000*+00	8.6713 1.8295 0.2826	1.3486 1.7988 1.3431*-03	2.0139*+03 2.9230*+02 7.1582*+02	2.0139*+03 6.3069*+01 2.9149*+02
74021704 1.1300*+00 INFINITE	4.4876 4.7468*+05 3.1700*+02	1.0024 1.0000 0.0000	3.8391*+03 1.5372*+04 8.7329*-04	9.9000*-04 NM 0.0000*+00	8.6390 1.8248 0.2854	1.3468 1.7925 1.7663*-03	2.0167*+03 2.9130*+02 7.1444*+02	2.0167*+03 6.3051*+01 2.9059*+02
74021705 1.3840*+00 INFINITE	4.4793 4.7863*+05 3.1700*+02	0.9952 1.0000 0.0000	4.3197*+03 1.7148*+04 9.6361*-04	9.5000*-04 NM 0.0000*+00	8.8762 1.8336 0.2260	1.3210 1.8039 1.9340*-03	2.0517*+03 2.8920*+02 7.1418*+02	2.0517*+03 6.3258*+01 2.9061*+02
74021801 3.6800*-01 INFINITE	4.5169 4.7199*+05 3.1400*+02	1.0242 1.0000 0.0000	2.3098*+03 9.5222*+03 3.3719*-04	1.0800*-03 NM 0.0000*+00	9.3884 1.8263 0.2105	1.428 1.790 7.0941*-04	3.1193*+03 2.9475*+02 7.1197*+02	3.1193*+03 6.1805*+01 2.8777*+02
74021802 6.2300*-01 INFINITE	4.5099 4.7690*+05 3.1500*+02	1.0161 1.0000 0.0000	3.6569*+03 1.4935*+04 9.2676*-04	9.8000*-04 NM 0.0000*+00	8.6125 1.8222 0.3133	1.3872 1.7907 1.0585*-03	3.1634*+03 2.9335*+02 7.1289*+02	3.1634*+03 6.2157*+01 2.8870*+02
74021803 8.7600*-01 INFINITE	4.5098 4.7588*+05 3.1800*+02	1.0029 1.0000 0.0000	4.5851*+03 1.8496*+04 6.6244*-04	9.5000*-04 NM 0.0000*+00	8.6185 1.8358 0.2941	1.3249 1.8080 3.3207*-03	3.1603*+03 2.9230*+02 7.1627*+02	3.1603*+03 6.2751*+01 2.9145*+02
74021804 1.1300*+00 INFINITE	4.5003 4.7169*+05 3.1600*+02	1.0057 1.0000 0.0000	5.8311*+03 2.3529*+04 8.3466*-04	9.1000*-04 NM 0.0000*+00	8.4562 1.8373 0.3204	1.3236 1.8052 1.6598*-03	3.1635*+03 2.9130*+02 7.1372*+02	3.1635*+03 6.2568*+01 2.8964*+02
74021805 1.3840*+00 INFINITE	4.4928 4.7698*+05 3.2100*+02	0.9829 1.0000 0.0000	6.8131*+03 2.6837*+04 9.6565*-04	8.8000*-04 NM 0.0000*+00	8.5307 1.8403 0.2820	1.2853 1.8163 1.8947*-03	3.2319*+03 2.8920*+02 7.1910*+02	3.2319*+03 6.3728*+01 2.9424*+02

PO,POD CALCULATED WITH AUTHOR'S MUE-LAW FROM RED2,D2 (AUTHOR)

74021801

MABEY

PROFILE TABULATION

41 POINTS, DELTA AT POINT 41

I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000 ⁺ 00	1.0000 ⁺ 00	NM	0.94043	0.00000	0.00000	4.77783	0.00000
2	3.6300 ⁻ 04	3.4114 ⁺ 00	NM	0.94112	0.33198	0.60290	3.29815	0.18280
3	3.8900 ⁻ 04	3.5898 ⁺ 00	NM	0.94086	0.34225	0.61550	3.23415	0.19031
4	4.1400 ⁻ 04	3.7605 ⁺ 00	NM	0.93951	0.35179	0.62650	3.17158	0.19754
5	4.3900 ⁻ 04	3.9211 ⁺ 00	NM	0.93866	0.36051	0.63640	3.11624	0.20422
6	4.6500 ⁻ 04	4.0785 ⁺ 00	NM	0.93780	0.36884	0.64560	3.06373	0.21072
7	4.9000 ⁻ 04	4.2196 ⁺ 00	NM	0.93741	0.37615	0.65360	3.01932	0.21647
8	5.1600 ⁻ 04	4.3462 ⁺ 00	NM	0.93763	0.38258	0.66070	2.98240	0.22153
9	5.4100 ⁻ 04	4.4815 ⁺ 00	NM	0.93505	0.38932	0.66700	2.93513	0.22725
10	5.6600 ⁻ 04	4.5999 ⁺ 00	NM	0.93617	0.39513	0.67350	2.90529	0.23182
11	5.9200 ⁻ 04	4.7133 ⁺ 00	NM	0.93574	0.40061	0.67900	2.87274	0.23636
12	6.1700 ⁻ 04	4.8227 ⁺ 00	NM	0.93602	0.40582	0.68440	2.84414	0.24064
13	6.4800 ⁻ 04	5.0215 ⁺ 00	NM	0.93616	0.41512	0.69370	2.79252	0.24841
14	7.1900 ⁻ 04	5.2015 ⁺ 00	NM	0.93674	0.42336	0.70190	2.74876	0.25535
15	7.7000 ⁻ 04	5.3590 ⁺ 00	NM	0.93567	0.43043	0.70820	2.70709	0.26161
16	8.2000 ⁻ 04	5.5009 ⁺ 00	NM	0.93509	0.43670	0.71380	2.67165	0.26718
17	8.7100 ⁻ 04	5.6457 ⁺ 00	NM	0.93525	0.44301	0.71960	2.63852	0.27273
18	9.9800 ⁻ 04	5.9772 ⁺ 00	NM	0.93766	0.45711	0.73300	2.57156	0.28506
19	1.1250 ⁻ 03	6.2674 ⁺ 00	NM	0.94122	0.46910	0.74460	2.51953	0.29553
20	1.2520 ⁻ 03	6.5486 ⁺ 00	NM	0.94419	0.48042	0.75510	2.47036	0.30566
21	1.3790 ⁻ 03	6.8435 ⁺ 00	NM	0.94760	0.49202	0.76570	2.42189	0.31616
22	1.5060 ⁻ 03	7.1328 ⁺ 00	NM	0.94821	0.50313	0.77450	2.36967	0.32684
23	1.6330 ⁻ 03	7.4354 ⁺ 00	NM	0.95171	0.51449	0.78440	2.32450	0.33745
24	1.8670 ⁻ 03	8.0870 ⁺ 00	NM	0.95404	0.53812	0.80210	2.22173	0.36103
25	2.1410 ⁻ 03	8.7680 ⁺ 00	NM	0.95885	0.56175	0.81940	2.12766	0.38512
26	2.3950 ⁻ 03	9.4807 ⁺ 00	NM	0.95533	0.58545	0.83280	2.02347	0.41137
27	2.6490 ⁻ 03	1.0224 ⁺ 01	NM	0.96261	0.60917	0.84960	1.94515	0.43678
28	2.9030 ⁻ 03	1.1012 ⁺ 01	NM	0.96452	0.63335	0.86340	1.85839	0.46460
29	3.4110 ⁻ 03	1.2622 ⁺ 01	NM	0.96631	0.68007	0.88680	1.70039	0.52153
30	3.9190 ⁻ 03	1.4370 ⁺ 01	NM	0.97722	0.72741	0.91190	1.57159	0.58024
31	4.4270 ⁻ 03	1.6348 ⁺ 01	NM	0.98007	0.77748	0.93180	1.43637	0.64872
32	4.9350 ⁻ 03	1.8567 ⁺ 01	NM	0.98207	0.83005	0.94970	1.30907	0.72548
33	5.4430 ⁻ 03	2.0815 ⁺ 01	NM	0.98681	0.88011	0.96610	1.20496	0.80177
34	6.0780 ⁻ 03	2.3422 ⁺ 01	NM	0.99051	0.93481	0.98140	1.10217	0.89042
35	6.7130 ⁻ 03	2.5243 ⁺ 01	NM	0.99955	0.97118	0.99390	1.04734	0.94898
36	7.3480 ⁻ 03	2.6122 ⁺ 01	NM	1.00209	0.98826	0.99870	1.02124	0.97793
37	7.9830 ⁻ 03	2.6438 ⁺ 01	NM	1.00145	0.99434	0.99960	1.01061	0.98910
38	8.6180 ⁻ 03	2.6588 ⁺ 01	NM	1.00211	0.99719	1.00050	1.00664	0.99390
39	9.2530 ⁻ 03	2.6637 ⁺ 01	NM	1.00274	0.99814	1.00100	1.00573	0.99529
40	9.8880 ⁻ 03	2.6716 ⁺ 01	NM	1.00214	0.99965	1.00100	1.00271	0.99830
0 41	1.0520 ⁻ 02	2.6735 ⁺ 01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
ALL MEASURED POINTS

74021802		MABEV	PROFILE TABULATION			47 POINTS, DELTA AT POINT 47		
I	Y	PT2/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD+U/UD
1	0.0000+00	1.0000+00	NM	0.93597	0.00000	0.00000	4.74336	0.00000
2	3.6300+04	3.0990+00	NM	0.93442	0.31356	0.57670	3.38261	0.17049
3	1.8900+04	3.2495+00	NM	0.93402	0.32284	0.59860	3.32414	0.17707
4	4.1400+04	3.3979+00	NM	0.93305	0.33170	0.59950	3.26658	0.18353
5	4.3900+04	3.5328+00	NM	0.93403	0.33954	0.60950	3.22237	0.18915
6	4.6500+04	3.6661+00	NM	0.93153	0.34709	0.61780	3.16825	0.19500
7	4.9000+04	3.8149+00	NM	0.93204	0.35532	0.62770	3.12079	0.20114
8	5.1600+04	3.9384+00	NM	0.93178	0.36160	0.63510	3.08136	0.20611
9	5.4100+04	4.0285+00	NM	0.93072	0.36678	0.64040	3.04848	0.21007
10	5.6600+04	4.1449+00	NM	0.93068	0.37288	0.64720	3.01265	0.21483
11	5.9200+04	4.2136+00	NM	0.93122	0.37642	0.65130	2.99371	0.21756
12	6.1700+04	4.3001+00	NM	0.93117	0.38084	0.65610	2.96794	0.22106
13	6.4800+04	4.4783+00	NM	0.93100	0.38978	0.66560	2.91601	0.22826
14	7.1900+04	4.6241+00	NM	0.93112	0.39692	0.67310	2.87575	0.23406
15	7.7000+04	4.7513+00	NM	0.93172	0.40305	0.67960	2.84305	0.23904
16	8.2000+04	4.8585+00	NM	0.93109	0.40815	0.68450	2.81266	0.24336
17	8.7100+04	4.9891+00	NM	0.93092	0.41426	0.69050	2.77827	0.24854
18	9.9800+04	5.2293+00	NM	0.93110	0.42527	0.70120	2.71860	0.25793
19	1.1250+03	5.4339+00	NM	0.93380	0.43442	0.71040	2.67711	0.26551
20	1.2520+03	5.6359+00	NM	0.93644	0.44327	0.71990	2.63756	0.27294
21	1.3790+03	5.8400+00	NM	0.93722	0.45203	0.72800	2.59377	0.28047
22	1.5060+03	6.0440+00	NM	0.93963	0.46061	0.73640	2.55598	0.28811
23	1.6330+03	6.2446+00	NM	0.93958	0.46890	0.74340	2.51357	0.29575
24	1.8670+03	6.6617+00	NM	0.94386	0.48566	0.75880	2.44116	0.31084
25	2.1410+03	7.0854+00	NM	0.95517	0.50210	0.77620	2.38982	0.32479
26	2.3950+03	7.5107+00	NM	0.95516	0.51608	0.78610	2.31405	0.34057
27	2.6490+03	7.9514+00	NM	0.95065	0.53412	0.79760	2.22993	0.35768
28	2.9030+03	8.3975+00	NM	0.95151	0.54988	0.80860	2.16241	0.37393
29	3.4110+03	9.3377+00	NM	0.95588	0.58168	0.83050	2.03853	0.40740
30	3.9190+03	1.0266+01	NM	0.96148	0.61145	0.85010	1.93292	0.43980
31	4.4270+03	1.1274+01	NM	0.96458	0.64219	0.86770	1.82543	0.47529
32	4.9350+03	1.2419+01	NM	0.96811	0.67542	0.88530	1.71804	0.51530
33	5.4430+03	1.3672+01	NM	0.97155	0.70998	0.90200	1.61404	0.55884
34	6.0780+03	1.5316+01	NM	0.97272	0.75294	0.91940	1.49105	0.61461
35	6.7130+03	1.7072+01	NM	0.97736	0.79623	0.93670	1.38194	0.67683
36	7.3480+03	1.8912+01	NM	0.98078	0.83921	0.95170	1.28605	0.74002
37	7.9830+03	2.0840+01	NM	0.98347	0.88202	0.96490	1.19677	0.80625
38	8.6180+03	2.2683+01	NM	0.98739	0.92106	0.97660	1.12424	0.86867
39	9.2530+03	2.4276+01	NM	0.99498	0.95352	0.98780	1.07320	0.92843
40	9.8880+03	2.5382+01	NM	0.99578	0.97542	0.99290	1.03617	0.98824
41	1.0520+02	2.5997+01	NM	0.99946	0.98738	0.99720	1.01499	0.97745
42	1.1158+02	2.6312+01	NM	0.99780	0.99345	0.99760	1.00837	0.98932
43	1.1799+02	2.6455+01	NM	0.99911	0.99620	0.99880	1.00523	0.99361
44	1.2428+02	2.6512+01	NM	0.99867	0.99730	0.99880	1.00301	0.99580
45	1.3060+02	2.6549+01	NM	0.99919	0.99800	0.99920	1.00241	0.99680
46	1.4333+02	2.6625+01	NM	0.99762	0.99945	0.99880	0.99870	1.00010
0 47	1.5000+02	2.6653+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
ALL MEASURED POINTS

74021803		NAMEY		PROFILE TABULATION		47 POINTS, DELTA AT PUII		47	
I	Y	PTP/P	P/PO	TU/TOD	M/MO	U/UO	T/TD	/RHOD#U/UD	
1	0.0000 ⁺ +00	1.0000 ⁺ +00	NM	0.93212	0.00000	0.00000	4.72367	0.00000	
2	3.6300 ⁻ -04	2.9609 ⁺ +00	NM	0.93305	0.30478	0.56460	3.43171	0.16452	
3	3.8900 ⁻ -04	3.0557 ⁺ +00	NM	0.93245	0.31084	0.57250	3.39213	0.16877	
4	4.1400 ⁻ -04	3.2097 ⁺ +00	NM	0.93309	0.32042	0.58520	3.33556	0.17544	
5	4.3900 ⁻ -04	3.3528 ⁺ +00	NM	0.93222	0.32904	0.59590	3.27976	0.18169	
6	4.6500 ⁻ -04	3.4985 ⁺ +00	NM	0.93070	0.33757	0.60600	3.22269	0.18804	
7	4.9000 ⁻ -04	3.6100 ⁺ +00	NM	0.93074	0.34439	0.61430	3.18167	0.19307	
8	5.1600 ⁻ -04	3.7358 ⁺ +00	NM	0.93059	0.35098	0.62210	3.14169	0.19801	
9	5.4100 ⁻ -04	3.8462 ⁺ +00	NM	0.92914	0.35703	0.62870	3.10078	0.20276	
10	5.6600 ⁻ -04	3.9595 ⁺ +00	NM	0.92941	0.36313	0.63580	3.06580	0.20740	
11	5.9200 ⁻ -04	4.0623 ⁺ +00	NM	0.92896	0.36857	0.64180	3.03214	0.21167	
12	6.1700 ⁻ -04	4.1331 ⁺ +00	NM	0.92803	0.37227	0.64560	3.00752	0.21466	
13	6.4800 ⁻ -04	4.2060 ⁺ +00	NM	0.92798	0.38115	0.65530	2.99596	0.22169	
14	7.1900 ⁻ -04	4.4380 ⁺ +00	NM	0.92655	0.38778	0.66260	2.91471	0.22694	
15	7.7000 ⁻ -04	4.5671 ⁺ +00	NM	0.92884	0.39415	0.66940	2.88434	0.23208	
16	8.2000 ⁻ -04	4.6832 ⁺ +00	NM	0.92823	0.39979	0.67500	2.85063	0.23679	
17	8.7100 ⁻ -04	4.7811 ⁺ +00	NM	0.93023	0.40448	0.68050	2.83046	0.24042	
18	9.9800 ⁻ -04	5.0086 ⁺ +00	NM	0.92988	0.41518	0.69100	2.77008	0.24945	
19	1.1250 ⁻ -03	5.2543 ⁺ +00	NM	0.93409	0.42641	0.70340	2.72109	0.25850	
20	1.2520 ⁻ -03	5.4165 ⁺ +00	NM	0.93751	0.43366	0.71150	2.69179	0.26432	
21	1.3790 ⁻ -03	5.5788 ⁺ +00	NM	0.93761	0.44080	0.71810	2.65393	0.27058	
22	1.5060 ⁻ -03	5.7574 ⁺ +00	NM	0.93828	0.44851	0.72510	2.61506	0.27735	
23	1.6870 ⁻ -03	6.3090 ⁺ +00	NM	0.94540	0.47153	0.74790	2.51572	0.29729	
24	2.1410 ⁻ -03	6.6532 ⁺ +00	NM	0.94775	0.48533	0.76010	2.45278	0.30989	
25	2.3950 ⁻ -03	7.0005 ⁺ +00	NM	0.94996	0.49886	0.77160	2.39234	0.32253	
26	2.6490 ⁻ -03	7.3538 ⁺ +00	NM	0.95072	0.51225	0.78200	2.33046	0.33556	
27	2.9030 ⁻ -03	7.6980 ⁺ +00	NM	0.95166	0.52497	0.79160	2.27376	0.34815	
28	3.4110 ⁻ -03	8.3890 ⁺ +00	NM	0.95479	0.54959	0.80980	2.17108	0.37299	
29	3.9190 ⁻ -03	9.0637 ⁺ +00	NM	0.95919	0.57261	0.82640	2.08290	0.39675	
30	4.4270 ⁻ -03	9.7663 ⁺ +00	NM	0.95976	0.59562	0.84040	1.99084	0.42213	
31	4.9350 ⁻ -03	1.0511 ⁺ +01	NM	0.96475	0.61907	0.85570	1.91058	0.44787	
32	5.4430 ⁻ -03	1.1308 ⁺ +01	NM	0.96876	0.64323	0.87010	1.82983	0.47551	
33	6.0780 ⁻ -03	1.2394 ⁺ +01	NM	0.96313	0.67473	0.88270	1.71145	0.51576	
34	6.7130 ⁻ -03	1.3511 ⁺ +01	NM	0.97093	0.70566	0.89990	1.62628	0.55335	
35	7.3480 ⁻ -03	1.4707 ⁺ +01	NM	0.97506	0.73732	0.91460	1.53870	0.59440	
36	7.9830 ⁻ -03	1.5974 ⁺ +01	NM	0.97447	0.76947	0.92620	1.44886	0.63926	
37	8.6180 ⁻ -03	1.7285 ⁺ +01	NM	0.97909	0.80135	0.93920	1.37363	0.68374	
38	9.2530 ⁻ -03	1.7634 ⁺ +01	NM	0.98134	0.83290	0.95010	1.30124	0.73015	
39	1.0520 ⁻ -02	2.1045 ⁺ +01	NM	0.98354	0.86504	0.96830	1.17041	0.82732	
40	1.1158 ⁻ -02	2.2847 ⁺ +01	NM	0.98697	0.92447	0.97720	1.11732	0.87459	
41	1.1790 ⁻ -02	2.4061 ⁺ +01	NM	0.98964	0.94923	0.98420	1.07504	0.91550	
42	1.2428 ⁻ -02	2.5045 ⁺ +01	NM	0.99375	0.96882	0.99150	1.04526	0.94761	
43	1.3060 ⁻ -02	2.5721 ⁺ +01	NM	0.99503	0.98205	0.99590	1.02428	0.97034	
44	1.4333 ⁻ -02	2.6370 ⁺ +01	NM	0.99894	0.99460	0.99840	1.00766	0.99081	
45	1.5600 ⁻ -02	2.6553 ⁺ +01	NM	0.99915	0.99810	0.99920	1.00220	0.99700	
46	1.6873 ⁻ -02	2.6631 ⁺ +01	NM	0.99976	0.99960	0.99980	1.00040	0.99940	
D 47	1.8140 ⁻ -02	2.6652 ⁺ +01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

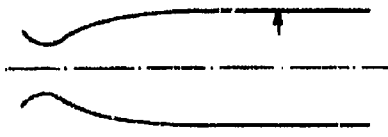
INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P/PO
ALL MEASURED POINTS

74021804		HABEY		PROFILE TABULATION		52 POINTS, DELTA AT POINT 52		
I	Y	PY2/P	P/PD	T0/T00	M/MD	U/UD	T/T0	RHO/RHOD+U/UD
1	0.0000+00	1.0000+00	NM	0.93264	0.00000	0.00000	4.71032	0.00000
2	3.6300+04	2.8547+00	NM	0.92940	0.29845	0.35430	3.44947	0.16069
3	3.8900+04	3.0002+00	NM	0.92902	0.30796	0.36700	3.38983	0.16727
4	4.1400+04	3.1229+00	NM	0.92927	0.31573	0.37730	3.34336	0.17267
5	4.3900+04	3.2490+00	NM	0.92861	0.32349	0.38710	3.29381	0.17824
6	4.6300+04	3.3822+00	NM	0.92716	0.33148	0.39670	3.24044	0.18414
7	4.9000+04	3.4675+00	NM	0.92595	0.33648	0.40250	3.20816	0.18792
8	5.1400+04	3.5880+00	NM	0.92707	0.34342	0.41130	3.16857	0.19293
9	5.4100+04	3.6906+00	NM	0.92465	0.34920	0.41740	3.12598	0.19751
10	5.6600+04	3.7752+00	NM	0.92369	0.35390	0.42260	3.09502	0.20116
11	5.9200+04	3.8637+00	NM	0.92367	0.35873	0.42820	3.06654	0.20486
12	6.1700+04	3.9212+00	NM	0.92308	0.36184	0.43190	3.04971	0.20720
13	6.4800+04	4.0542+00	NM	0.92322	0.36892	0.43960	3.00571	0.21279
14	7.1900+04	4.1733+00	NM	0.92410	0.37514	0.44680	2.97265	0.21798
15	7.7000+04	4.2882+00	NM	0.92430	0.38105	0.45330	2.93945	0.22225
16	8.2000+04	4.3941+00	NM	0.92421	0.38640	0.45900	2.90867	0.22656
17	8.7100+04	4.4774+00	NM	0.92395	0.39056	0.46330	2.88434	0.22997
18	9.9800+04	4.6792+00	NM	0.93102	0.40044	0.467610	2.85063	0.23718
19	1.1250+03	4.8689+00	NM	0.92741	0.40948	0.468390	2.78940	0.24518
20	1.2820+03	5.0364+00	NM	0.92976	0.41734	0.469250	2.75330	0.25152
21	1.3790+03	5.2021+00	NM	0.93184	0.42498	0.470660	2.71813	0.25775
22	1.5066+03	5.3598+00	NM	0.93370	0.43205	0.470800	2.68528	0.26366
23	1.6330+03	5.5085+00	NM	0.93476	0.43865	0.471450	2.65322	0.26930
24	1.8670+03	5.8263+00	NM	0.93323	0.45241	0.472780	2.58799	0.28122
25	2.1410+03	6.1133+00	NM	0.93171	0.46448	0.473820	2.52589	0.29225
26	2.3950+03	6.3940+00	NM	0.94171	0.47598	0.474960	2.48016	0.30225
27	2.6490+03	6.6897+00	NM	0.95232	0.48780	0.476340	2.44918	0.31170
28	2.9030+03	6.9418+00	NM	0.94953	0.49765	0.477000	2.38406	0.32163
29	3.4110+03	7.4707+00	NM	0.94777	0.51770	0.478430	2.29516	0.34172
30	3.9190+03	8.0042+00	NM	0.94937	0.53715	0.479870	2.21092	0.36125
31	4.4270+03	8.5295+00	NM	0.95072	0.55563	0.481160	2.13356	0.38040
32	4.9350+03	9.0690+00	NM	0.95443	0.57349	0.482480	2.06494	0.39945
33	5.4430+03	9.6794+00	NM	0.95672	0.59407	0.483780	1.98886	0.42125
34	6.0780+03	1.0461+01	NM	0.95864	0.61881	0.485250	1.89789	0.44918
35	6.7130+03	1.1263+01	NM	0.95880	0.64324	0.486530	1.80463	0.47816
36	7.3480+03	1.2113+01	NM	0.96260	0.66812	0.487410	1.73130	0.50777
37	7.9830+03	1.3010+01	NM	0.96816	0.69340	0.489310	1.65893	0.53836
38	8.6180+03	1.3918+01	NM	0.96666	0.71805	0.490280	1.58078	0.57111
39	9.2530+03	1.4954+01	NM	0.97081	0.74283	0.491450	1.51561	0.60339
40	9.8880+03	1.5882+01	NM	0.97222	0.76878	0.492470	1.44676	0.63919
41	1.0520+02	1.6910+01	NM	0.97296	0.79403	0.493370	1.38274	0.67525
42	1.1158+02	1.8006+01	NM	0.97808	0.82008	0.494450	1.32644	0.71206
43	1.1790+02	1.9140+01	NM	0.97706	0.84619	0.495180	1.26518	0.75230
44	1.2428+02	2.0291+01	NM	0.98079	0.87190	0.496080	1.21433	0.79122
45	1.3060+02	2.1495+01	NM	0.98079	0.89713	0.496740	1.16279	0.83196
46	1.4333+02	2.3607+01	NM	0.98795	0.94202	0.498170	1.08601	0.90395
47	1.5600+02	2.5172+01	NM	0.99187	0.97336	0.499050	1.03352	0.95653
48	1.6873+02	2.5996+01	NM	0.99362	0.98946	0.499470	1.01061	0.98426
49	1.8140+02	2.6329+01	NM	0.99623	0.99590	0.499730	1.00261	0.99491
50	1.9413+02	2.6446+01	NM	0.99514	0.99815	0.499730	0.99830	0.99400
51	2.0683+02	2.6498+01	NM	0.99774	0.99915	0.499870	0.99910	0.99460
52	2.1950+02	2.6542+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
ALL MEASURED POINTS

74021805		HAREY		PROFILE TABULATION		55 POINTS, DELTA AT POINT 55			
I	Y	P1/P1	P/PU	T0/T00	M/MD	U/U0	T/T0	RHO/RHOD*U/U0	
1	0.0000+00	1.0000+00	NM	0.92988	0.00000	0.00000	4.68384	0.00000	
2	3.6300*-04	2.8355+00	NM	0.93267	0.29766	0.55370	3.46021	0.16002	
3	3.8900*-04	2.9248+00	NM	0.93221	0.30358	0.56160	3.42231	0.16410	
4	4.1400*-04	3.0769+00	NM	0.93343	0.31336	0.57500	3.36700	0.17077	
5	4.3900*-04	3.1887+00	NM	0.93126	0.32034	0.58340	3.31675	0.17590	
6	4.6500*-04	3.3151+00	NM	0.93093	0.32803	0.59310	3.26904	0.18143	
7	4.9000*-04	3.4187+00	NM	0.93126	0.33419	0.60090	3.23311	0.18586	
8	5.1600*-04	3.5105+00	NM	0.92948	0.33954	0.60690	3.19489	0.18996	
9	5.4100*-04	3.6026+00	NM	0.93041	0.34482	0.61360	3.16656	0.19377	
10	5.6600*-04	3.6904+00	NM	0.92886	0.34978	0.61900	3.13185	0.19765	
11	5.9200*-04	3.7618+00	NM	0.92802	0.35375	0.62340	3.10559	0.20073	
12	6.1700*-04	3.8336+00	NM	0.92923	0.35769	0.62800	3.08642	0.20360	
13	6.4300*-04	3.9067+00	NM	0.92722	0.36457	0.63560	3.07491	0.20911	
14	7.1000*-04	4.0699+00	NM	0.92773	0.37037	0.64230	3.06752	0.21356	
15	7.7000*-04	4.1816+00	NM	0.92400	0.37620	0.64920	2.97796	0.21800	
16	8.2000*-04	4.2724+00	NM	0.92532	0.38087	0.65300	2.93945	0.22215	
17	8.7100*-04	4.3566+00	NM	0.92841	0.38516	0.65870	2.92483	0.22521	
18	9.9800*-04	4.5896+00	NM	0.93015	0.39577	0.67050	2.87026	0.23360	
19	1.1250*-03	4.7500+00	NM	0.93131	0.40453	0.67990	2.82486	0.24068	
20	1.2520*-03	4.9153+00	NM	0.93631	0.41238	0.68690	2.79642	0.24660	
21	1.3790*-03	5.0620+00	NM	0.93572	0.41922	0.69610	2.75710	0.25248	
22	1.5060*-03	5.2070+00	NM	0.93678	0.42588	0.70290	2.72405	0.25803	
23	1.6330*-03	5.3598+00	NM	0.94100	0.43278	0.71100	2.69906	0.26343	
24	1.8870*-03	5.6532+00	NM	0.94368	0.44571	0.72390	2.63783	0.27443	
25	2.1410*-03	5.9337+00	NM	0.94616	0.45773	0.73550	2.58198	0.28486	
26	2.3950*-03	6.1939+00	NM	0.94742	0.46859	0.74530	2.52972	0.29462	
27	2.6490*-03	6.4486+00	NM	0.94961	0.47899	0.75480	2.48324	0.30396	
28	2.9030*-03	6.6951+00	NM	0.95202	0.48883	0.76370	2.44081	0.31289	
29	3.4110*-03	7.1514+00	NM	0.95076	0.50654	0.77690	2.35239	0.33026	
30	3.9190*-03	7.6078+00	NM	0.95544	0.52364	0.79140	2.28415	0.34647	
31	4.4270*-03	8.0395+00	NM	0.95454	0.53931	0.80200	2.21141	0.36266	
32	4.9350*-03	8.5023+00	NM	0.95575	0.55562	0.81340	2.14316	0.37953	
33	5.4430*-03	8.9320+00	NM	0.95974	0.57034	0.82450	2.08986	0.39492	
34	6.0780*-03	9.5371+00	NM	0.96067	0.59044	0.83710	2.01005	0.41646	
35	6.7130*-03	1.0181+01	NM	0.96497	0.61110	0.85080	1.93836	0.43893	
36	7.3480*-03	1.0822+01	NM	0.96247	0.63097	0.86040	1.85943	0.46272	
37	7.9830*-03	1.1503+01	NM	0.96691	0.65145	0.87280	1.79501	0.48624	
38	8.6180*-03	1.2182+01	NM	0.97022	0.67122	0.88380	1.73370	0.50978	
39	9.2530*-03	1.2928+01	NM	0.97467	0.69230	0.89540	1.67280	0.53527	
40	9.8880*-03	1.3679+01	NM	0.97909	0.71287	0.90440	1.60953	0.56190	
41	1.0520*-02	1.4457+01	NM	0.97496	0.73357	0.91270	1.54799	0.58960	
42	1.1158*-02	1.5268+01	NM	0.98048	0.75457	0.92330	1.49723	0.61667	
43	1.1790*-02	1.6091+01	NM	0.97739	0.77528	0.92930	1.43678	0.64674	
44	1.2428*-02	1.6939+01	NM	0.97830	0.79606	0.93680	1.38485	0.67646	
45	1.3040*-02	1.7811+01	NM	0.97894	0.81686	0.94380	1.33494	0.70700	
46	1.4333*-02	1.9651+01	NM	0.98529	0.85913	0.95940	1.24704	0.76934	
47	1.5600*-02	2.1557+01	NM	0.98308	0.90081	0.96940	1.18808	0.83708	
48	1.6873*-02	2.3313+01	NM	0.98984	0.94782	0.98160	1.09601	0.89561	
49	1.8140*-02	2.4765+01	NM	0.99524	0.96693	0.99080	1.04998	0.94364	
50	1.9413*-02	2.5659+01	NM	0.99524	0.98456	0.99450	1.02030	0.97471	
51	2.0680*-02	2.6142+01	NM	0.99722	0.99395	0.99740	1.00695	0.99052	
52	2.1953*-02	2.6352+01	NM	0.99760	0.99800	0.99840	1.00080	0.99760	
53	2.3223*-02	2.6432+01	NM	1.00058	0.99955	1.00020	1.00130	0.99890	
54	2.4493*-02	2.6448+01	NM	1.00006	0.99985	1.00000	1.00030	0.99970	
0 55	2.5760*-02	2.6455+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,U/UD,RHO/RHOD ASSUME P=PD
 ALL MEASURED POINTS

	M : 9.4	7403
	R THETA X 10 ⁻³ : 40	
	TW/TR : 0.42	ZPG - SHT
Continuous tunnel, with symmetrical flexible nozzle. W = 0.51, H = 0.53 m. PO : 4.3 MN/m ² . TO : 790 K. Dried air, RE/m X 10 ⁻⁶ : 12.7.		
LADERMAN A.J. and DEMETRIADES A., 1974. Mean and fluctuating flow measurements in the hypersonic boundary layer over a cooled wall. J. Fluid Mech. 63, 121-144. And Demetriades, A., Private communications. Also Laderman & Demetriades (1972), McDonald (1975)		

- 1 The test boundary layer was formed on the upper wall of the contoured flexible nozzle and test section of the tunnel. Measurements were made at a single station on the centre-line 4.064 m downstream of the throat (X = 0). The test surface was "polished to micro-inch finish" and was actively cooled. Surveys by Laufer et al. (1967) showed that the Mach number on the axis was constant within 0.3 % for nearly 2 m leading up to and passing through the test zone. Variation across the central 0.25 m of the flow was less than 1 %
- 2 0.3 m upstream of the test station. Differences in Pitot reading, for a given value of Y, within the central
- 3 0.3 m of the boundary layer were about 5 %. Transition was "thought to be within a few cm of the throat".
- 4 Static pressure on the side wall and roof agreed within 3 % but showed greater longitudinal variation than on the centre line. The pressure at X = 2 m was about 8 % higher than at the test station and fell to a minimum about 16 % below the test value at X = 3.0 m before rising again so that the gradient was about + 25 %/m at the test station (Editors' estimate from information supplied in graphical form).
- 6 Static pressure was measured on both sidewalls and roof of the tunnel at 0.305 m intervals, with a tapping (d = 1.70 mm) at the test station. The temperature of the wall was measured at X = 4.070 m by a thermocouple mounted in the wall of a recess used for instrumentation. Pitot, hot-wire, static pressure and total
- 7 temperature probes were mounted on a single traverse gear. The HMP and TTP were mounted 76 mm to either side
- 8 of the Pitot probe which was on the centre-line. Additional Pitot probes were mounted at Z = ± 152 mm and
- 7 used to check two-dimensionality. In the outer part of the layer, the Pitot probes were CPP (d₁ or d₂ = 3.17, l = 38.1 mm). For measurements near the wall a cranked FPP (h₁ = 0.36, h₂ = 0.2, b₁ = 1.68, b₂ = 1.52, l = 38.1 mm) was fitted to the tip of one of the outboard Pitot tubes. The HMP carried a Pt - 10 % Rh wire (typically d = 0.25, l = 76 mm). These were mounted slackly (to avoid strain gauge effects) to two sharp-pointed prongs. These, and the initial part of the support body (d = 0.79, l = 6.3 mm) were cranked towards the surface at about 20° and mounted to a slender cylindrical support aligned with the flow (l, overall, 38.1 mm). The wires were operated in the constant-current mode. The TTP was a vented STP (d₁ = 3.2, d₂ = 2.4, l = 38 mm) with the iron-constantan thermocouple mounted 11 mm back from the front face, and vented by three holes at the same position (d = 0.79 mm). The static pressure probe was "a sharply pointed 1.27 mm diameter tube, aligned in the direction of flow, with three sensing holes (0.38 mm diameter)
- 8 located 19 mm from its tip". The static probe was mounted with its axis 8 mm further from the tunnel wall than the line containing the tips of the CPP and STP.
- 9 The authors have interpolated the profile measurements to the Y value of the Pitot measurements. TO values in the inner part of the layer (y < 1.6 mm) are obtained by fitting a third degree polynomial to the innermost measured values to meet the wall temperature (see source figure 6 and page 128). The authors obtained a CF value by fitting the transformed velocity profile data to the law of the wall and Coles' (1966) wake function (see source paper p 132 for details).
- 10 The Pitot probe readings are uncorrected. The authors calculated thermal, viscous, and rarefaction corrections, which were negligible for the large probes. For the small probe, the viscous correction could be up to 10 % but was not applied because of the lack of experimental data on such corrections. The STP was calibrated at M = 9.5 and M = 6 at 800 K, and at M = 4 for TO from 300 to 800 K. The calibration was found to depend on the probe Reynolds Number, being essentially independent of Mach number. Large corrections

- for viscous interaction effects were applied to the static pressure readings (up to 60 %). For a discussion of these see the source paper and Beckwith et al. 1971. The calibration and reduction procedures for the hot-wire probes will not be discussed here in detail. The fundamental assumption is that the pressure-entropy and pressure-vorticity correlations are negligible while the entropy / vorticity correlation is - 1.
- 11 For a full discussion see the source paper and associated references. Viscosity values were taken from NAVORD report 1488 vol. 5 section 15 (1953).
- 12 The editors have accepted all the corrections and interpolations used by the authors. For the profile tables we have set the D-state at the point for which we computed the highest value of P_0 and arbitrarily set the D-state reservoir properties to the stated tunnel values. We found it necessary to use a trapezoidal
- 13 integration rule in calculating the integral values. There is one profile presented, supplemented by the
- 14 hot wire data in section D. We have presented the CF value obtained by the authors from a curve fit to the transformed profile.
- 5 DATA 7403 0101. Single profile, Pitot, T_0 and P measured simultaneously. Turbulence quantities measured with constant current hot-wire probe.
- 15 Editors' comments

The special value of this entry lies in the provision of hot wire data at $M \approx 10$. These are tabulated in section D for two different wires. The difficulty of obtaining such data cannot be overestimated, and the pool of available turbulence information is small. In the catalogue the whole Mach number range from 1.7 to 10 is covered by, successively, Kistler - CAT 5803, Horstman & Owen - CAT 7206 and the present entry. A contrast between ZPG and simple wave APG behaviour is given by Sturek & Danberg - CAT 7101, and a limited observation in a reflected wave APG is given by Waltrup & Schetz - CAT 7104. It is, however, difficult to form these disparate studies into any unified whole as the types of equipment, the assumptions made in data-reduction and the prejudices of each research worker are so varied.

The authors' preferred scaling length is the boundary layer thickness for 50 % intermittency, here 103 mm. At this point P_0/P_{0D} is about 0.6 and U/UD is about 0.95. Thus δ (intermittency) is here less than most values based on mean flow data, and arguments relying on the relative position of turbulence features should take account of this.

The reported static pressure variation is very difficult to explain. If the mean flow streamlines are straight and parallel, there can be no pressure difference across the boundary layer as a whole. A local dip in the region of intense momentum fluctuations could be observed as a part of the total normal stress would then be supplied by the normal Reynolds stress. The calibration procedure for the static probe requires very large corrections, so that no great emphasis should be placed on the details of the variation reported. The overall difference however can also be inferred from the wall static pressure and a Pitot-derived value in the free stream, and the adjusted static pressure variation given in the profile tables agrees with these two observations.

If the longitudinal pressure gradient of 25 %/m estimated by the editors, and referred to in § 4 above, is assumed to propagate as a simple wave from the wall on which it is measured, the static pressure would fall by about 30 % across the boundary layer, which at this level of argument is quite good agreement with the 40 % reported. The subsequent development of the, necessarily curved, mean flow streamline is, however, difficult to visualise unless the whole phenomenon is an upstream influence of the diffuser. The centre line Pitot data in Laufer et al. (1967) rule out any possibility of a wave structure from upstream having this effect. As a last comment on this puzzling apparent behaviour, McDonald (1976) reports a "balance chamber pressure" at this X-station of about 1.2 PD, and quotes a variety of static pressure determinations by Demetriades and Gupta which show much increased differences between wall and "free stream isentropic" pressures as the tunnel reservoir pressure falls. It is possible that this represents an increasing upstream influence of the diffuser.

The profile is given in great detail, and using the authors' CF value, fits both inner and outer laws well in transformed coordinates. The wake region is rather more pronounced than for low speed ZPG profiles. Measurements extend well within the momentum-deficit peak. There are no available mean flow data which

can be directly compared. The cooled tunnel wall measurements of Hopkins & Keener - CAT 7203 were made at $M = 7$, while the $M = 10$ flat plate study by Watson et al. - CAT 7305 was at lower Reynolds number and without heat transfer.

CAT 7403		LADERMAN		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.						
RUN	ND *	TW/TR	RED2W	CF *	H12	H12K	PH	PD		
X	P0D*	PH/PD	RED2D	CO	H32	H32K	TW*	TD		
RZ	T0D*	SW *	D2	P12	H42	D2K	UD	TR		
74030101	9.3730	0.4257	6.5232 ⁺⁰³	4.0600 ⁻⁰⁴	7.2559	1.4188	2.1927 ⁺⁰²	1.5458 ⁺⁰²		
NM	4.2863 ⁺⁰⁶	1.4185	4.0009 ⁺⁰⁴	NM	1.8135	1.7449	3.0400 ⁺⁰²	4.2648 ⁺⁰¹		
INFINITE	7.9200 ⁺⁰²	0.0000	7.8778 ⁻⁰³	NC	1.3305	1.7010 ⁻⁰²	1.2273 ⁺⁰³	7.1407 ⁺⁰²		

TRAPEZOIDAL RULE FOR ALL INTEGRATIONS

EVALUATED DATA - PRESSURE BASED REFERENCE FLOW

RUN	D2PD	H12PD	H32PD	H42PD	RED2PDD	RED2PDW	DSTAR
	D2PW	H12PW	H32PW	H42PW	RED2PMD	RED2PWW	
74030101	7.7782 ⁻⁰³	10.0290	1.8111	1.3476	3.9551 ⁺⁰⁴	6.4485 ⁺⁰³	6.4165 ⁻⁰²
	6.0962 ⁻⁰³	9.4487	1.8166	1.3435	3.9671 ⁺⁰⁴	6.4681 ⁺⁰³	

74030101		LADERMAN		PROFILE TABULATION		73 POINTS, DELTA AT POINT 71		
I	Y	PT2/P	P/PD	Y0/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	1.41850	0.38307	0.00000	0.00000	7.11388	0.00000
2	2.5400-04	1.2203+00	1.40051	0.44261	0.05772	0.16084	7.76509	0.02898
3	3.8100-04	1.2775+00	1.40807	0.47047	0.08423	0.18332	8.14645	0.03165
4	4.5720-04	1.4661+00	1.42319	0.50785	0.08108	0.23576	8.45446	0.03965
5	5.5880-04	1.2826+00	1.37129	0.49146	0.06475	0.18881	8.50032	0.03043
6	7.8740-04	1.5906+00	1.42404	0.54613	0.08983	0.26773	8.88244	0.04288
7	9.3980-04	1.5922+00	1.42199	0.57802	0.08994	0.27572	9.39836	0.04168
8	1.2446-03	2.2118+00	1.42131	0.58828	0.12056	0.35564	8.70220	0.05803
9	1.3716-03	2.0895+00	1.41599	0.59839	0.11554	0.34665	9.02101	0.05448
10	1.4478-03	2.8913+00	1.41775	0.59168	0.14446	0.40959	8.03932	0.07216
11	1.6002-03	2.2145+00	1.41179	0.61078	0.12067	0.36244	9.03186	0.05663
12	1.7780-03	2.5875+00	1.41447	0.61443	0.13443	0.39560	8.66041	0.06455
13	1.9050-03	2.5906+00	1.40903	0.61990	0.13454	0.39760	8.73424	0.06408
14	2.2352-03	3.4019+00	1.40962	0.62334	0.15971	0.45155	7.99323	0.07955
15	2.7940-03	4.0953+00	1.40679	0.63318	0.17817	0.48951	7.54829	0.09114
16	3.0988-03	4.1038+00	1.39969	0.63738	0.17838	0.49151	7.59183	0.09053
17	4.3888-03	5.2002+00	1.39292	0.64472	0.20399	0.53646	6.91611	0.10794
18	5.3086-03	5.6609+00	1.38479	0.64828	0.21361	0.55245	6.67642	0.11447
19	5.5626-03	5.6661+00	1.38170	0.65027	0.21391	0.55345	6.69391	0.11412
20	5.6388-03	5.9259+00	1.38147	0.64903	0.21925	0.56044	6.53418	0.11837
21	6.7934-03	6.4652+00	1.36985	0.65738	0.22992	0.57842	6.32924	0.12506
22	7.7978-03	6.6771+00	1.36910	0.65912	0.23397	0.58442	6.23912	0.12812
23	8.1788-03	6.8812+00	1.36645	0.65948	0.23781	0.58741	6.14289	0.13098
24	8.2296-03	6.7504+00	1.36850	0.65966	0.23536	0.58641	6.20804	0.12914
25	9.3980-03	7.3588+00	1.36064	0.66038	0.24656	0.60040	5.92977	0.13763
26	1.0338-02	7.5740+00	1.35883	0.66153	0.25040	0.60539	5.84532	0.14059
27	1.0719-02	7.7132+00	1.35741	0.66195	0.25285	0.60839	5.78931	0.14251
28	1.1889-02	8.1330+00	1.34916	0.66401	0.26011	0.61738	5.63376	0.14770
29	1.3233-02	8.2903+00	1.34468	0.66642	0.26278	0.62138	5.59166	0.14928
30	1.5850-02	9.1279+00	1.33599	0.67040	0.27654	0.63736	5.31203	0.16014
31	1.8339-02	9.8347+00	1.32775	0.67339	0.28763	0.64935	5.09655	0.16900
32	2.0523-02	1.1072+01	1.32084	0.67325	0.30609	0.66533	4.72472	0.18581
33	2.0701-02	1.1213+01	1.32316	0.68001	0.30812	0.67033	4.73304	0.18721
34	2.3190-02	1.2053+01	1.31773	0.68544	0.31996	0.68731	4.61438	0.19608
35	2.7026-02	1.3705+01	1.31045	0.68973	0.34205	0.70030	4.19178	0.21871
36	3.4595-02	1.7008+01	1.30073	0.70675	0.38237	0.73327	3.67744	0.25910
37	3.8481-02	1.8507+01	1.30133	0.72648	0.39934	0.75225	3.54846	0.27560
38	4.2215-02	2.0811+01	1.29506	0.72747	0.42409	0.76424	3.24741	0.30447
39	4.9835-02	2.4807+01	1.29423	0.74895	0.46389	0.79121	2.90911	0.35165
40	5.2222-02	2.6086+01	1.29670	0.75064	0.47573	0.79620	2.80111	0.36821
41	5.3696-02	2.7556+01	1.29349	0.76865	0.48930	0.81019	2.74077	0.38198
42	5.7607-02	3.1152+01	1.28828	0.77375	0.52096	0.82218	2.49169	0.42467
43	6.5075-02	3.7358+01	1.28095	0.79751	0.57111	0.84715	2.20032	0.49269
44	6.8885-02	4.1886+01	1.27112	0.81295	0.60514	0.86214	2.02973	0.51938
45	7.0129-02	4.2708+01	1.27338	0.80480	0.61112	0.84914	1.97642	0.55298
46	7.2746-02	4.6815+01	1.26202	0.82148	0.64014	0.87313	1.86041	0.59170
47	7.6905-02	5.1032+01	1.25157	0.83184	0.66652	0.88312	1.74451	0.63294
48	7.9146-02	5.8797+01	1.22750	0.84549	0.71813	0.89719	1.56057	0.70493
49	8.4023-02	6.2498+01	1.22246	0.85180	0.74032	0.90310	1.48810	0.74128
50	8.4099-02	6.1781+01	1.22246	0.86214	0.73626	0.90209	1.52122	0.72902
51	8.9103-02	7.1561+01	1.18905	0.87159	0.79281	0.91908	1.34391	0.81236
52	9.1745-02	7.7896+01	1.16619	0.87889	0.82738	0.92607	1.25281	0.86118
53	9.4183-02	7.9885+01	1.16524	0.88099	0.83794	0.92807	1.22070	0.88069
54	9.4289-02	8.2331+01	1.14987	0.88891	0.85074	0.93307	1.20290	0.89104
55	9.6799-02	8.7587+01	1.13101	0.89410	0.87763	0.93806	1.14206	0.92773
56	9.9314-02	8.8671+01	1.12882	0.89906	0.88307	0.94106	1.13565	0.93466
57	9.9339-02	9.2985+01	1.11217	0.89811	0.90441	0.94206	1.08500	0.96464
58	1.0193-01	9.5159+01	1.10464	0.90630	0.91497	0.94705	1.07136	0.97549
59	1.0198-01	9.5490+01	1.09807	0.91185	0.91657	0.95005	1.07439	0.97002
60	1.0432-01	9.4960+01	1.11193	0.90260	0.91401	0.94505	1.06909	0.98195
61	1.0450-01	9.8950+01	1.08879	0.91173	0.93311	0.95105	1.02893	0.99578
62	1.0700-01	1.0092+02	1.08094	0.92215	0.94239	0.95704	1.03134	1.00207
63	1.0945-01	1.0017+02	1.08576	0.92064	0.93887	0.95604	1.03693	1.00007
64	1.0970-01	1.0252+02	1.07561	0.92513	0.94986	0.95904	1.01943	1.01088
65	1.1217-01	1.0459+02	1.06602	0.93175	0.95946	0.96304	1.00747	1.01799
66	1.1453-01	1.0295+02	1.07485	0.93262	0.95188	0.96304	1.02357	1.01027
67	1.1455-01	1.0494+02	1.06751	0.93157	0.94606	0.96304	1.00042	1.02381
68	1.2222-01	1.0842+02	1.04795	0.93312	0.97696	0.97502	0.99605	1.02480
69	1.2982-01	1.0949+02	1.03672	0.96827	0.98176	0.98302	1.00257	1.01549
70	1.3721-01	1.1168+02	1.02375	0.97904	0.99157	0.98901	0.94884	1.01673
71	1.5281-01	1.1358+02	1.00100	1.00000	1.00000	1.00000	1.00000	1.00000
72	1.7818-01	1.1290+02	0.98702	1.02243	0.99701	1.01099	1.02823	0.96950
73	2.0361-01	1.1336+02	0.98731	1.01817	0.99904	1.00899	1.02002	0.97566

INPUT VARIABLES Y,M,U/UD,RHO/RHOD
AT I=2 DATA WERE AVERAGED

SECTION D. ADDITIONAL DATA - TURBULENCE MEASUREMENTS. RESULTS FROM CONSTANT-CURRENT HOT WIRE PROBES

Fluctuation levels relative to local mean value of relevant property.

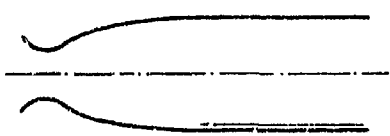
FACSIMILE FROM TABLE SUPPLIED BY AUTHORS. NB: AUTHORS SYMBOLS AND UNITS

Fluctuation levels (%):

T' - static temperature, u' - velocity, p' - static pressure, ρ' - density, σ' - entropy, τ' - vorticity.
 Y-distance from wall in inches. L_u , L_T , L_p . Integral scales (x direction) in cm - for velocity, temperature and pressure. SRA - "Strong Reynolds Analogy" = $T' / (\gamma - 1) M^2 u'$.

WIRE: A12-1						METHOD: p' ≠ Q				
y (in)	T' (%)	u' (%)	p' (%)	ρ' (%)	SRA	L_u	L_T	L_p	σ' (%)	τ' (%)
.063	4.86	8.69	16.5	11.8	.943	.85	.86	.84	1.18	3.5
.078	6.13	9.60	16.87	12.6	.856	.99	.97	.67	3.78	7.09
.104	6.87	8.41	18.52	13.9	.856	1.12	1.14	1.01	4.39	6.33
.116	6.66	7.56	17.55	13.3	.849	1.23	1.19	.72	4.38	5.81
.26	6.16	4.60	13.48	10.8	.748	1.34	1.24	.63	4.81	4.74
.365	5.30	3.57	12.48	9.73	.722	1.75	1.65	.56	3.92	3.12
.469	5.37	3.22	11.95	9.48	.708	1.96	1.86	.504	4.15	2.88
.562	5.62	3.08	11.47	9.38	.700	1.97	1.85	.479	4.57	2.81
.665	6.24	3.14	11.76	9.91	.685	2.00	1.89	.489	5.26	2.92
.763	6.01	2.90	11.8	9.78	.652	2.06	2.03	.38	4.97	2.70
.861	5.80	2.75	11.05	9.27	.61	2.12	2.16	.47	4.86	2.59
1.462	8.84	2.79	14.4	12.9	.588	1.99	2.10	.51	7.83	2.69
2.011	8.15	2.06	14.3	12.4	.504	1.79	1.81	.36	7.05	1.99
2.513	7.79	1.56	14.8	12.4	.446	2.06	1.96	.55	6.55	1.51
2.716	9.83	1.59	14.5	13.7	.477	2.46	3.27	.66	8.90	1.56
3.263	10.3	1.2	13.9	13.7	.453	1.52	1.37	.18	9.50	1.18
3.413	7.03	.89	11.26	10.2	.376	1.97	1.89	.15	6.25	.88
3.663	7.89	.74	12.36	11.3	.438	1.81	1.65	.84	7.05	.725
3.865	5.46	.525	8.95	8.01	.381	1.81	1.39	.37	4.82	.516
4.062	2.44	.222	6.31	4.8	.372	2.88	4.15	1.86	1.63	.214
4.264	1.59	.160	4.76	3.5	.318	1.85	1.67	1.87	.83	.154
4.464	1.26	.115	3.76	2.76	.342	1.8	1.10	1.47	.66	.11
4.613	1.22	.089	3.09	2.36	.420	2.68	.59	1.11	.85	.085
5.54	1.50	.061	3.17	2.56	.709	1.93	1.21	2.50	1.20	.055
6.512	2.11	.037	3.05	2.9	1.61	5.55	4.68	2.28	1.93	.028

WIRE: 6-3						METHOD: p' ≠ Q				
y	T' (%)	u' (%)	p' (%)	ρ' (%)	SRA	L_u	L_T	L_p	σ' (%)	τ' (%)
.027	.79	3.12	2.69	1.93	.929	.26	.26	.24	.18	1.33
.047	4.83	10.0	16.8	12.0	.995	.486	.48	.467	.58	1.72
.090	3.07	3.82	8.90	6.58	.932	1.21	1.15	.64	1.73	2.44
.11	3.59	3.78	11.3	8.22	.956	1.31	1.27	.84	1.59	1.95
.128	3.74	3.46	11.56	8.44	.963	1.52	1.45	.57	1.76	1.82
.144	3.65	3.10	10.92	8.02	.947	1.46	1.39	.79	1.89	1.82
.187	3.77	2.78	9.37	7.2	.893	1.48	1.41	.62	2.66	2.15
.212	3.40	2.33	9.10	6.86	.910	1.56	1.45	.59	2.18	1.67
.23	3.46	2.34	9.20	6.94	.885	1.19	1.09	.50	2.25	1.73
1.02	5.24	1.57	11.21	9.01	.849	2.75	2.59	1.03	4.14	1.34
1.318	5.44	1.44	10.85	8.94	.776	3.03	3.23	1.27	4.47	1.29
1.618	6.54	1.42	12.30	10.4	.769	2.95	3.21	1.32	5.52	1.29
2.224	5.80	.875	12.39	9.97	.727	3.3	3.24	1.58	4.50	.784
2.82	6.72	.701	16.29	12.6	.687	3.51	3.40	.45	4.85	.616
3.122	6.58	.614	13.43	11.0	.622	2.92	3.50	2.85	5.35	.572
3.971	2.94	.197	7.36	5.64	.522	2.98	2.64	.59	2.06	.183
5.047	2.08	.081	6.53	4.75	.752	1.19	.52	.38	.92	.060
6.971	3.67	.185	2.41	3.99	.565	.63	.36	.097	3.6	.184

	M : 2.96 falling to 2.80 R THETA X 10 ⁻³ : 23 - 415 TW/TR : 1.05	7601
		ZPG - AW
Blow down tunnel with two-dimensional symmetrical fixed nozzle blocks. Minimum running time 20 secs. W = H = 0.232, L = 2.56 m. 0.3 < P0 < 3.4 MN/m ² . T0 : 275 K. Dry air. 35 < RE/m X 10 ⁻⁶ < 300.		
VAS I.E., SETTLES G.S. and BOGDONOFF S.M. 1976. An experimental study of the compressible turbulent boundary layer over a wide range of Reynolds number. Princeton University report in preparation. <u>And Settles (1975), Vas & Bogdonoff (1971), Vas I.E., private communications.</u>		

- 1 The test boundary layer was formed on the lower wall of a 0.232 m square constant area test channel, following the contoured nozzle block. There were nine test stations on the centre line, approximately equally distributed in the range $X = 0.89$ to 3.45 , where $X = 0$ at the tunnel throat. The test surface was
- 2 machined to $1.7 \mu\text{m}$, and was not actively cooled. Pitot surveys showed the free stream "to be even within
- 3 3 %." No boundary layer trip devices were used, and natural transition was believed to occur upstream of
- 4 the throat. The test layer experienced a predominately simple wave favourable pressure gradient when
- 5 passing over the nozzle block, and as a result of boundary layer growth, was subject to a slight adverse
- 6 pressure gradient in the constant-area test section. Spanwise static pressure surveys and surface flow
- 7 patterns were frequently repeated, and showed the flow to be 'uniform and non-converging'.
- 8 Wall pressure was measured by static pressure tapings ($d = 0.8 \text{ mm}$), and wall temperature by thermocouples,
- 9 both at the same X -stations as for the profiles. Wall shear stress was determined using Preston tubes
- 10 ($d_2 = 0.6 \text{ mm}$; $d_1 = 1.57, 2.39, 3.18 \text{ mm}$) and the Hopkins & Keener (1966) T/calibration.
- 11 Pitot profiles were measured with a FPP for which $h_1 = 0.178$, $h_2 = 0.089$, $b_1 = 0.762$, $l = 2 \text{ mm}$.
- 12 20-30 total temperature surveys were made using a FWP consisting of a chromel alumel thermocouple junction
- 13 at the centre of a fine wire 2.54 mm long, and either 51 or $102 \mu\text{m}$ in diameter. The profiles were measured
- 14 at the nine stations listed in section B below, and Preston tube observations were made at the same positions.
- 15 The T0 profile surveys all showed "a roughly linear increase in T0/T0D from 1.0 at the boundary layer edge
- 16 to 1.05 at the wall. Thus this linear total temperature profile was assumed" in data reduction. The authors
- comment that a Crocco-Van Driest correlation could have been used, with little consequent material differ-
- ences in the reduced data. The static pressure was assumed constant through the boundary layer, and given
- the value obtained from the Pitot measurements at the boundary layer edge. This did not differ significantly
- from the measured values of PW. No profile corrections were applied and Sutherland's viscosity formula was
- used.
- The editors' have accepted all the assumptions of the authors, and adopted the authors' selection of a
- D-state. The data form four sets of nine successive profile observations at increasing unit Reynolds
- number. For about 2/3 of the profiles, a Preston tube CF observation is provided. The raw and reduced
- data are given in table 1 of section D.
- DATA: 7601 0101-0409. Pitot and T0 profiles. NX = 9. CF from Preston tubes measured separately.
- Editors' comments
- The Reynolds number range of this experiment is both very wide and very high. The experimental coverage
- is relatively complete. Although temperature profiles were not obtained for each and every Pitot profile,
- a great deal of data was obtained. The reduced data are not very sensitive to small differences in the
- temperature profile at this relatively modest Mach number and with a near-adiabatic wall, so that the
- linear variation used to describe the measurements is probably adequate. The value of the data is greatly
- increased by the inclusion of shear stress measurements and the large number of streamwise stations.

Some of the profiles are extremely long but even so measurements for about half the profiles do not extend within the momentum deficit peak.

The obvious comparison experiments are those of Moore & Harkness - CAT 6502 and Thomke - CAT 6903.

SECTION D, ADDITIONAL DATA, RAW PRESTON TUBE READINGS

DP - Preston tube diameter - inches

PP - Preston tube pressure - psia

CF - As reduced by authors.

CAT 7601	DP in	PP psia	CF X10 ³	CAT 7601	DP in	PP psia	CF X10 ³
0101	0.062	6.012	1.38	0201	0.062	10.57	1.27
0102	-	NM	-	0202	-	NM	-
0103	0.062	5.76	1.21	0203	0.062	9.98	1.10
0104	0.125	7.4	1.31	0204	0.125	12.7	1.18
0105	0.094	6.63	1.23	0205	0.094	11.5	1.13
0106	0.125	7.54	1.26	0206	0.0625	10.52	1.14
0107	0.062	6.19	1.21	0207	0.062	10.62	1.15
0108	-	NM	-	0208	-	NM	-
0109	-	NM	-	0209	0.062	10.58	1.07
0301	0.062	35.48	1.08	0401	-	NM	-
0302	-	NM	-	0402	-	NM	-
0303	0.062	31.65	0.92	0403	0.062	52.97	0.86
0304	0.125	42.5	1.00	0404	-	NM	-
0305	0.094	38.0	0.93	0405	-	NM	-
0306	0.125	42.45	0.95	0406	-	NM	-
0307	0.062	33.60	0.90	0407	-	NM	-
0308	-	NM	-	0408	-	NM	-
0309	0.062	33.15	0.84	0409	0.062	56.76	0.76

CAT 7601		BOUNDARY CONDITIONS AND EVALUATED DATA. SI UNITS.							
RUN	VAS	TW/TR	REN2W	CF *	H12	H12K	PW	PD	
X *	POD*	PW/PD*	REN2D	CG	H32	H32K	TW*	TD	
RZ	TOD*	SW *	D2	P12*	H42	D2K	UD	TR	
76010101	2.9600	1.1245	9.1522 ⁺⁰³	1.3600 ⁻⁰³	5.6106	1.2374	1.1960 ⁺⁰⁴	1.1960 ⁺⁰⁴	
8.8900 ⁻⁰¹	4.1369 ⁺⁰⁵	1.0000	2.3198 ⁺⁰⁴	NM	1.8535	1.8390	2.8292 ⁺⁰²	9.7897 ⁺⁰¹	
INFINITE	2.6944 ⁺⁰²	0.0000	6.4826 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1713	9.9077 ⁻⁰⁴	5.8720 ⁺⁰²	2.5160 ⁺⁰²	
76010102	2.9200	1.1237	1.2637 ⁺⁰⁴	NM	5.5008	1.2512	1.2704 ⁺⁰⁴	1.2704 ⁺⁰⁴	
1.1938 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	3.1445 ⁺⁰⁴	NM	1.8487	1.8318	2.8583 ⁺⁰²	1.0063 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	8.7298 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1684	1.3206 ⁻⁰³	5.8728 ⁺⁰²	2.5438 ⁺⁰²	
76010103	2.9000	1.1233	1.4052 ⁺⁰⁴	1.2100 ⁻⁰³	5.7442	1.2463	1.3094 ⁺⁰⁴	1.3094 ⁺⁰⁴	
1.4986 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	3.4677 ⁺⁰⁴	NM	1.8485	1.8328	2.8583 ⁺⁰²	1.0150 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	9.5241 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2744	1.4512 ⁻⁰³	5.8579 ⁺⁰²	2.5447 ⁺⁰²	
76010104	2.8800	1.1229	1.7315 ⁺⁰⁴	1.3100 ⁻⁰³	5.5513	1.2412	1.3497 ⁺⁰⁴	1.3497 ⁺⁰⁴	
1.7907 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	4.2376 ⁺⁰⁴	NM	1.8496	1.8334	2.8583 ⁺⁰²	1.0238 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	1.1514 ⁻⁰³	0.0000 ⁺⁰⁰	-0.2291	1.7363 ⁻⁰³	5.8427 ⁺⁰²	2.5456 ⁺⁰²	
76010105	2.8700	1.1227	1.9562 ⁺⁰⁴	1.2300 ⁻⁰³	5.7958	1.2200	1.3703 ⁺⁰⁴	1.3703 ⁺⁰⁴	
2.0955 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	4.7675 ⁺⁰⁴	NM	1.8582	1.8444	2.8583 ⁺⁰²	1.0283 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	1.2886 ⁻⁰³	0.0000 ⁺⁰⁰	-0.3425	1.9308 ⁻⁰³	5.8351 ⁺⁰²	2.5461 ⁺⁰²	
76010106	2.8800	1.1229	2.2504 ⁺⁰⁴	1.2600 ⁻⁰³	5.1555	1.2224	1.3497 ⁺⁰⁴	1.3497 ⁺⁰⁴	
2.4003 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	5.4988 ⁺⁰⁴	NM	1.8412	1.8433	2.8875 ⁺⁰²	1.0343 ⁺⁰²	
INFINITE	2.7500 ⁺⁰²	0.0000	1.5164 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1098	2.2031 ⁻⁰³	5.8725 ⁺⁰²	2.5716 ⁺⁰²	
76010107	2.8700	1.1227	2.3712 ⁺⁰⁴	1.2100 ⁻⁰³	5.3302	1.2345	1.3703 ⁺⁰⁴	1.3703 ⁺⁰⁴	
2.6928 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	5.7543 ⁺⁰⁴	NM	1.8555	1.8392	2.8583 ⁺⁰²	1.0335 ⁺⁰²	
INFINITE	2.7889 ⁺⁰²	0.0000	1.6109 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1699	2.3796 ⁻⁰³	5.9081 ⁺⁰²	2.6084 ⁺⁰²	
76010108	2.8100	1.1214	2.8761 ⁺⁰⁴	NM	4.9893	1.2235	1.5013 ⁺⁰⁴	1.5013 ⁺⁰⁴	
2.9972 ⁺⁰⁰	4.1369 ⁺⁰⁵	1.0000	6.8037 ⁺⁰⁴	NM	1.8582	1.8425	2.9400 ⁺⁰²	1.0856 ⁺⁰²	
INFINITE	2.8000 ⁺⁰²	0.0000	1.8548 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1123	2.6759 ⁻⁰³	5.8702 ⁺⁰²	2.6217 ⁺⁰²	
76010201	2.9600	1.1245	1.4722 ⁺⁰⁴	1.2700 ⁻⁰³	5.4105	1.2971	1.9933 ⁺⁰⁴	1.9933 ⁺⁰⁴	
8.8900 ⁻⁰¹	6.8948 ⁺⁰⁵	1.0000	3.7245 ⁺⁰⁴	NM	1.8474	1.8217	2.8583 ⁺⁰²	9.8906 ⁺⁰¹	
INFINITE	2.7222 ⁺⁰²	0.0000	6.3392 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.0865	9.4582 ⁻⁰⁴	5.9022 ⁺⁰²	2.5420 ⁺⁰²	
76010202	2.9400	1.1241	1.8616 ⁺⁰⁴	NM	5.7530	1.2492	2.0543 ⁺⁰⁴	2.0543 ⁺⁰⁴	
1.1938 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	4.6710 ⁺⁰⁴	NM	1.8518	1.8358	2.8583 ⁺⁰²	7.9762 ⁺⁰¹	
INFINITE	2.7222 ⁺⁰²	0.0000	7.8649 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2341	1.2009 ⁻⁰³	5.8876 ⁺⁰²	2.5429 ⁺⁰²	
76010203	2.9300	1.1239	2.2049 ⁺⁰⁴	1.1000 ⁻⁰³	5.5334	1.2388	2.0855 ⁺⁰⁴	2.0855 ⁺⁰⁴	
1.4986 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	5.5095 ⁺⁰⁴	NM	1.8538	1.8186	2.8583 ⁺⁰²	1.0019 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	9.2269 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1794	1.3876 ⁻⁰³	5.8803 ⁺⁰²	2.5433 ⁺⁰²	
76010204	2.9200	1.1237	2.6459 ⁺⁰⁴	1.1800 ⁻⁰³	5.3333	1.2740	2.1173 ⁺⁰⁴	2.1173 ⁺⁰⁴	
1.7907 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	6.5718 ⁺⁰⁴	NM	1.8437	1.8203	2.8875 ⁺⁰²	1.0165 ⁺⁰²	
INFINITE	2.7500 ⁺⁰²	0.0000	1.1110 ⁻⁰³	0.0000 ⁺⁰⁰	-0.0990	1.6757 ⁻⁰³	5.9027 ⁺⁰²	2.5697 ⁺⁰²	
76010205	2.8700	1.1227	3.2356 ⁺⁰⁴	1.1300 ⁻⁰³	5.2707	1.2504	2.2636 ⁺⁰⁴	2.2636 ⁺⁰⁴	
2.0955 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	7.8861 ⁺⁰⁴	NM	1.8564	1.8417	2.8583 ⁺⁰²	1.0283 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	1.2788 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1424	1.8773 ⁻⁰³	5.8351 ⁺⁰²	2.5461 ⁺⁰²	
76010206	2.8800	1.1229	3.7780 ⁺⁰⁴	1.1400 ⁻⁰³	5.2897	1.2298	2.2494 ⁺⁰⁴	2.2494 ⁺⁰⁴	
2.4003 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	9.3505 ⁺⁰⁴	NM	1.8564	1.8391	2.8833 ⁺⁰²	9.6114 ⁺⁰¹	
INFINITE	2.5556 ⁺⁰²	0.0000	1.3899 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1471	2.0514 ⁻⁰³	5.6610 ⁺⁰²	2.3897 ⁺⁰²	
76010207	2.8500	1.1222	4.0634 ⁺⁰⁴	1.1500 ⁻⁰³	5.1476	1.2180	2.3543 ⁺⁰⁴	2.3543 ⁺⁰⁴	
2.6924 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	9.8216 ⁺⁰⁴	NM	1.8632	1.8494	2.8583 ⁺⁰²	1.0372 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	1.5756 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1370	2.2785 ⁻⁰³	5.8196 ⁺⁰²	2.5470 ⁺⁰²	
76010208	2.8300	1.1218	4.2019 ⁺⁰⁴	NM	5.1085	1.2232	2.4270 ⁺⁰⁴	2.4270 ⁺⁰⁴	
2.9972 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	9.9606 ⁺⁰⁴	NM	1.8605	1.8453	3.0450 ⁺⁰²	1.1146 ⁺⁰²	
INFINITE	2.9000 ⁺⁰²	0.0000	1.7328 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1388	2.5036 ⁻⁰³	5.9905 ⁺⁰²	2.7143 ⁺⁰²	
76010209	2.8000	1.1212	4.7141 ⁺⁰⁴	1.0700 ⁻⁰³	5.0914	1.2095	2.5406 ⁺⁰⁴	2.5406 ⁺⁰⁴	
3.3147 ⁺⁰⁰	6.8948 ⁺⁰⁵	1.0000	1.1160 ⁺⁰⁵	NM	1.8625	1.8485	2.8583 ⁺⁰²	1.0601 ⁺⁰²	
INFINITE	2.7222 ⁺⁰²	0.0000	1.7430 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1687	2.5043 ⁻⁰³	5.7801 ⁺⁰²	2.5494 ⁺⁰²	

CAT 7601		BOUNDARY CONDITIONS AND EVALUATED DATA, SI UNITS.								
VAS	MD *	TW/TR	RE02W	CF *	H12	H12K	PW	PD		
RUN	P00*	PW/PD*	RE02D	CG	H32	H32K	TH*	TD		
X *	T00*	SW *	O2	PI2*	H42	D2K	UD	TR		
RZ										
76010301	2.9600	1.1245	3.4141 ⁺⁰⁴	1.0800 ⁻⁰³	5.7107	1.2327	5.9799 ⁺⁰⁴	5.9799 ⁺⁰⁴		
8.6900 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	8.6376 ⁺⁰⁴	NM	1.8703	1.8573	2.8583 ⁺⁰²	9.8906 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	9.9005 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2267	7.1927 ⁻⁰⁴	5.9022 ⁺⁰²	2.5420 ⁺⁰²		
76010302	3.0000	1.1252	1.7092 ⁺⁰⁴	NM	5.6431	1.2363	5.6310 ⁺⁰⁴	5.6310 ⁺⁰⁴		
1.1938 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	1.2113 ⁺⁰⁵	NM	1.8540	1.8371	2.8583 ⁺⁰²	9.7222 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	7.0219 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1626	1.0795 ⁻⁰³	5.9308 ⁺⁰²	2.5402 ⁺⁰²		
76010303	2.9200	1.1237	5.7673 ⁺⁰⁴	9.2000 ⁻⁰⁴	5.5719	1.2724	6.3516 ⁺⁰⁴	6.3516 ⁺⁰⁴		
1.4986 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	1.4351 ⁺⁰⁵	NM	1.8547	1.8381	2.8583 ⁺⁰²	1.0063 ⁺⁰²		
INFINITE	2.7222 ⁺⁰²	0.0000	7.9685 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1655	1.1944 ⁻⁰³	5.8728 ⁺⁰²	2.5438 ⁺⁰²		
76010304	2.9300	1.1239	6.6344 ⁺⁰⁴	1.0000 ⁻⁰³	5.5741	1.1990	6.2566 ⁺⁰⁴	6.2566 ⁺⁰⁴		
1.7907 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	1.6577 ⁺⁰⁵	NM	1.8730	1.8591	2.8583 ⁺⁰²	1.0019 ⁺⁰²		
INFINITE	2.7222 ⁺⁰²	0.0000	9.2543 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2262	1.3459 ⁻⁰³	5.8803 ⁺⁰²	2.5433 ⁺⁰²		
76010305	2.9400	1.1241	6.9094 ⁺⁰⁴	9.3000 ⁻⁰⁴	5.7547	1.1916	6.1629 ⁺⁰⁴	6.1629 ⁺⁰⁴		
2.0555 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	1.7336 ⁺⁰⁵	NM	1.8679	1.8554	2.8583 ⁺⁰²	9.9762 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	9.7302 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2789	1.4406 ⁻⁰³	5.8876 ⁺⁰²	2.5429 ⁺⁰²		
76010306	2.8700	1.1227	9.2577 ⁺⁰⁴	9.5000 ⁻⁰⁴	5.8050	1.2162	6.8515 ⁺⁰⁴	6.8515 ⁺⁰⁴		
2.4003 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	2.2572 ⁺⁰⁵	NM	1.8526	1.8406	2.8583 ⁺⁰²	1.0262 ⁺⁰²		
INFINITE	2.7167 ⁺⁰²	0.0000	1.2164 ⁻⁰³	0.0000 ⁺⁰⁰	-0.3516	1.8227 ⁻⁰³	5.8291 ⁺⁰²	2.5409 ⁺⁰²		
76010307	2.8900	1.1231	8.7449 ⁺⁰⁴	9.0000 ⁻⁰⁴	5.5262	1.2164	6.6468 ⁺⁰⁴	6.6468 ⁺⁰⁴		
2.6924 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	2.1445 ⁺⁰⁵	NM	1.8683	1.8540	2.8583 ⁺⁰²	1.0319 ⁺⁰²		
INFINITE	2.7556 ⁺⁰²	0.0000	1.1926 ⁻⁰³	0.0000 ⁺⁰⁰	-0.2358	1.7409 ⁻⁰³	5.8860 ⁺⁰²	2.5763 ⁺⁰²		
76010308	2.8500	1.1222	1.1113 ⁺⁰⁵	NM	5.5135	1.2256	7.0628 ⁺⁰⁴	7.0628 ⁺⁰⁴		
2.9972 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	2.6843 ⁺⁰⁵	NM	1.8576	1.8432	2.8700 ⁺⁰²	1.0415 ⁺⁰²		
INFINITE	2.7333 ⁺⁰²	0.0000	1.4439 ⁻⁰³	0.0000 ⁺⁰⁰	-0.2615	2.1315 ⁻⁰³	5.8119 ⁺⁰²	2.5574 ⁺⁰²		
76010309	2.8500	1.1222	1.1875 ⁺⁰⁵	8.4000 ⁻⁰⁴	5.4027	1.2196	7.0628 ⁺⁰⁴	7.0628 ⁺⁰⁴		
3.3147 ⁺⁰⁰	2.0684 ⁺⁰⁶	1.0000	2.8591 ⁺⁰⁵	NM	1.8605	1.8459	2.9223 ⁺⁰²	1.0405 ⁺⁰²		
INFINITE	2.7833 ⁺⁰²	0.0000	1.5796 ⁻⁰³	0.0000 ⁺⁰⁰	-0.2242	2.3198 ⁻⁰³	5.8846 ⁺⁰²	2.6042 ⁺⁰²		
76010401	2.9600	1.1245	5.4494 ⁺⁰⁴	NM	5.3187	1.2112	9.7273 ⁺⁰⁴	9.7273 ⁺⁰⁴		
8.6900 ⁻⁰¹	2.0684 ⁺⁰⁶	1.0000	1.3787 ⁺⁰⁵	NM	1.8826	1.8717	2.8583 ⁺⁰²	9.8906 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	4.8085 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.1111	6.8046 ⁻⁰⁴	5.9022 ⁺⁰²	2.5420 ⁺⁰²		
76010402	2.9900	1.1250	6.2414 ⁺⁰⁴	NM	6.2722	1.3177	9.3364 ⁺⁰⁴	9.3364 ⁺⁰⁴		
1.1938 ⁺⁰⁰	2.3784 ⁺⁰⁶	1.0000	1.5988 ⁺⁰⁵	NM	1.8632	1.8445	2.8583 ⁺⁰²	9.7640 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	5.8438 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.3376	8.9640 ⁻⁰⁴	5.9237 ⁺⁰²	2.5407 ⁺⁰²		
76010403	2.9600	1.1245	7.8242 ⁺⁰⁴	8.6000 ⁻⁰⁴	5.7942	1.3262	9.7273 ⁺⁰⁴	9.7273 ⁺⁰⁴		
1.4986 ⁺⁰⁰	2.3646 ⁺⁰⁶	1.0000	1.9795 ⁺⁰⁵	NM	1.8590	1.8398	2.8583 ⁺⁰²	9.8906 ⁺⁰¹		
INFINITE	2.7333 ⁺⁰²	0.0000	6.9039 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2006	1.0331 ⁻⁰³	5.9022 ⁺⁰²	2.5420 ⁺⁰²		
76010404	2.9700	1.1246	9.4872 ⁺⁰⁴	NM	5.7095	1.1930	9.6213 ⁺⁰⁴	9.6213 ⁺⁰⁴		
1.7907 ⁺⁰⁰	2.3784 ⁺⁰⁶	1.0000	2.4102 ⁺⁰⁵	NM	1.8764	1.8644	2.8583 ⁺⁰²	9.8882 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	8.4176 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.2393	1.2200 ⁻⁰³	5.9094 ⁺⁰²	2.5415 ⁺⁰²		
76010405	2.9500	1.1243	1.0239 ⁺⁰⁵	9.3000 ⁻⁰⁴	6.0734	1.2511	9.9154 ⁺⁰⁴	9.9154 ⁺⁰⁴		
2.0955 ⁺⁰⁰	2.3784 ⁺⁰⁶	1.0000	2.5798 ⁺⁰⁵	NM	1.8616	1.8425	2.8583 ⁺⁰²	9.4333 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	8.9129 ⁻⁰⁴	0.0000 ⁺⁰⁰	-0.3470	1.3408 ⁻⁰³	5.8949 ⁺⁰²	2.5424 ⁺⁰²		
76010406	2.9300	1.1233	1.2167 ⁺⁰⁵	9.5000 ⁻⁰⁴	5.6976	1.2170	1.0693 ⁺⁰⁵	1.0693 ⁺⁰⁵		
2.4003 ⁺⁰⁰	2.3784 ⁺⁰⁶	1.0000	3.0025 ⁺⁰⁵	NM	1.8714	1.8599	2.8583 ⁺⁰²	1.0150 ⁺⁰²		
INFINITE	2.7222 ⁺⁰²	0.0000	1.0098 ⁻⁰³	0.0000 ⁺⁰⁰	-0.2882	1.4744 ⁻⁰³	5.8579 ⁺⁰²	2.5447 ⁺⁰²		
76010407	2.9100	1.1235	1.3737 ⁺⁰⁵	NM	5.3360	1.2091	1.0490 ⁺⁰⁵	1.0490 ⁺⁰⁵		
2.6924 ⁺⁰⁰	2.3646 ⁺⁰⁶	1.0000	3.4042 ⁺⁰⁵	NM	1.8700	1.8567	2.8583 ⁺⁰²	1.0106 ⁺⁰²		
INFINITE	2.7222 ⁺⁰²	0.0000	1.1358 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1571	1.6687 ⁻⁰³	5.8654 ⁺⁰²	2.5442 ⁺⁰²		
76010408	2.9500	1.1243	1.4306 ⁺⁰⁵	NM	5.3768	1.2048	1.0118 ⁺⁰⁵	1.0118 ⁺⁰⁵		
2.9972 ⁺⁰⁰	2.4474 ⁺⁰⁶	1.0000	3.6112 ⁺⁰⁵	NM	1.8735	1.8589	2.8293 ⁺⁰²	9.8319 ⁺⁰¹		
INFINITE	2.6944 ⁺⁰²	0.0000	1.2085 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1365	1.7414 ⁻⁰³	5.8648 ⁺⁰²	2.5165 ⁺⁰²		
76010409	2.9700	1.1246	1.5925 ⁺⁰⁵	7.6000 ⁻⁰⁴	5.5902	1.2035	9.7194 ⁺⁰⁴	9.7194 ⁺⁰⁴		
3.3147 ⁺⁰⁰	2.4129 ⁺⁰⁶	1.0000	4.0437 ⁺⁰⁵	NM	1.8775	1.8622	2.8583 ⁺⁰²	9.8882 ⁺⁰¹		
INFINITE	2.7222 ⁺⁰²	0.0000	1.3986 ⁻⁰³	0.0000 ⁺⁰⁰	-0.1966	2.0157 ⁻⁰³	5.9094 ⁺⁰²	2.5415 ⁺⁰²		

76010103		VAS		PROFILE TABULATION		49 POINTS, DELTA AT POINT 49			
I	Y	PT2/P	P/PD	TU/TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	1.05205	0.00000	0.00000	2.82161	0.00000	
2	1.0160 ⁻⁰⁴	2.0325 ⁺⁰⁰	NM	1.02221	0.36552	0.54667	2.23852	0.24430	
3	3.5560 ⁻⁰⁴	2.6778 ⁺⁰⁰	NM	1.02718	0.46552	0.66146	2.01899	0.32762	
4	6.0960 ⁻⁰⁴	3.0144 ⁺⁰⁰	NM	1.03154	0.47931	0.67708	1.99549	0.33931	
5	8.6360 ⁻⁰⁴	3.4694 ⁺⁰⁰	NM	1.04004	0.52414	0.72396	1.90781	0.37947	
6	1.1176 ⁻⁰³	3.7244 ⁺⁰⁰	NM	1.03010	0.54483	0.73958	1.84271	0.40136	
7	1.3716 ⁻⁰³	3.9693 ⁺⁰⁰	NM	1.02263	0.56532	0.75521	1.78337	0.42347	
8	1.6256 ⁻⁰³	4.0953 ⁺⁰⁰	NM	1.02170	0.57586	0.76562	1.76765	0.43313	
9	1.8796 ⁻⁰³	4.2238 ⁺⁰⁰	NM	1.03114	0.58621	0.77604	1.75254	0.44281	
10	2.1336 ⁻⁰³	4.4880 ⁺⁰⁰	NM	1.02750	0.60690	0.79167	1.70159	0.46525	
11	2.3876 ⁻⁰³	4.6237 ⁺⁰⁰	NM	1.03307	0.61724	0.80208	1.68661	0.47500	
12	2.6416 ⁻⁰³	4.7618 ⁺⁰⁰	NM	1.03896	0.62759	0.81250	1.67610	0.48476	
13	3.2766 ⁻⁰³	4.9973 ⁺⁰⁰	NM	1.03194	0.64483	0.82292	1.62864	0.50528	
14	3.9116 ⁻⁰³	5.3878 ⁺⁰⁰	NM	1.03355	0.67241	0.84375	1.57454	0.53587	
15	4.5466 ⁻⁰³	5.8094 ⁺⁰⁰	NM	1.02270	0.68621	0.84896	1.53060	0.55466	
16	5.1816 ⁻⁰³	5.8473 ⁺⁰⁰	NM	1.02203	0.70345	0.86458	1.51060	0.57234	
17	5.8166 ⁻⁰³	6.1654 ⁺⁰⁰	NM	1.02455	0.72414	0.87500	1.46007	0.59929	
18	6.4516 ⁻⁰³	6.4377 ⁺⁰⁰	NM	1.02347	0.74158	0.88542	1.42631	0.62077	
19	7.0866 ⁻⁰³	6.7730 ⁺⁰⁰	NM	1.01853	0.76207	0.89583	1.38187	0.64828	
20	7.7216 ⁻⁰³	7.0597 ⁺⁰⁰	NM	1.01928	0.77931	0.90625	1.35231	0.67015	
21	8.3566 ⁻⁰³	7.3578 ⁺⁰⁰	NM	1.02076	0.79655	0.91667	1.32433	0.69218	
22	8.9916 ⁻⁰³	7.5319 ⁺⁰⁰	NM	1.01967	0.80690	0.92187	1.30529	0.70626	
23	9.6266 ⁻⁰³	7.8969 ⁺⁰⁰	NM	1.01826	0.82759	0.93229	1.26905	0.73464	
24	1.0262 ⁻⁰²	8.1455 ⁺⁰⁰	NM	1.02541	0.84138	0.94271	1.25537	0.75094	
25	1.0897 ⁻⁰²	8.3356 ⁺⁰⁰	NM	1.01411	0.85172	0.94271	1.22506	0.76952	
26	1.1532 ⁻⁰²	8.8505 ⁺⁰⁰	NM	1.01885	0.87931	0.95833	1.18782	0.80680	
27	1.2167 ⁻⁰²	9.0482 ⁺⁰⁰	NM	1.01961	0.88966	0.96354	1.17300	0.82143	
28	1.2802 ⁻⁰²	9.3155 ⁺⁰⁰	NM	1.01726	0.90345	0.96875	1.14979	0.84255	
29	1.3437 ⁻⁰²	9.5849 ⁺⁰⁰	NM	1.01530	0.91724	0.97396	1.12749	0.86383	
30	1.4072 ⁻⁰²	9.8624 ⁺⁰⁰	NM	1.01369	0.93103	0.97917	1.10607	0.88527	
31	1.4707 ⁻⁰²	1.0072 ⁺⁰¹	NM	1.01539	0.94138	0.98438	1.09343	0.90026	
32	1.5342 ⁻⁰²	1.0355 ⁺⁰¹	NM	1.01435	0.95517	0.98958	1.07335	0.92146	
33	1.5977 ⁻⁰²	1.0498 ⁺⁰¹	NM	1.00863	0.96207	0.98958	1.05802	0.93532	
34	1.6612 ⁻⁰²	1.0642 ⁺⁰¹	NM	1.01362	0.96897	0.99479	1.05402	0.94381	
35	1.7247 ⁻⁰²	1.0859 ⁺⁰¹	NM	1.00537	0.97931	0.99479	1.03187	0.96407	
36	1.7882 ⁻⁰²	1.0933 ⁺⁰¹	NM	1.01320	0.98276	1.00000	1.03540	0.96581	
37	1.8517 ⁻⁰²	1.1080 ⁺⁰¹	NM	1.00784	0.98966	1.00000	1.02102	0.97942	
38	1.9152 ⁻⁰²	1.1154 ⁺⁰¹	NM	1.00520	0.99310	1.00000	1.01394	0.98625	
39	1.9787 ⁻⁰²	1.1228 ⁺⁰¹	NM	1.00258	0.99655	1.00000	1.00693	0.99312	
40	2.0422 ⁻⁰²	1.1228 ⁺⁰¹	NM	1.01306	0.99655	1.00521	1.01745	0.98797	
41	2.1057 ⁻⁰²	1.1228 ⁺⁰¹	NM	1.00258	0.99655	1.00000	1.00693	0.99312	
42	2.1692 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.01044	1.00000	1.00521	1.01044	0.99482	
43	2.2327 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
44	2.2962 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
45	2.3597 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
46	2.4232 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
47	2.4867 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
48	2.5400 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
0 49	2.6162 ⁻⁰²	1.1302 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,U ASSUME P=PD

76010203

VAB

PROFILE TABULATION

73 POINTS, DELTA AT POINT 68

I	Y	PTZ/P	P/PD	T./TOD	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	1.04200	0.00000	0.00000	2.83109	0.00000
2	8.8900-05	1.8697+00	NM	1.02384	0.33767	0.51503	2.32632	0.22139
3	5.1562-04	3.5482+00	NM	1.02315	0.52397	0.72021	1.88929	0.38121
4	9.4234-04	1.9509+00	NM	1.02333	0.55822	0.74130	1.81139	0.41476
5	1.3716-03	4.2056+00	NM	1.03159	0.57877	0.77202	1.77930	0.43389
6	1.7983-03	4.4701+00	NM	1.02756	0.59932	0.74756	1.72688	0.45606
7	2.2276-03	4.6518+00	NM	1.02594	0.61301	0.79793	1.69428	0.47095
8	2.6416-03	4.8849+00	NM	1.01846	0.63014	0.80829	1.64537	0.49125
9	3.0734-03	5.1247+00	NM	1.02516	0.64726	0.82363	1.62003	0.50853
10	3.5052-03	5.2717+00	NM	1.01938	0.65753	0.82902	1.59960	0.52152
11	3.9370-03	5.5221+00	NM	1.01496	0.67466	0.83938	1.54792	0.54226
12	4.3688-03	5.7792+00	NM	1.02400	0.69178	0.85492	1.52727	0.55977
13	4.8006-03	5.8838+00	NM	1.02535	0.69863	0.86010	1.51568	0.56747
14	5.2070-03	6.1501+00	NM	1.01105	0.71575	0.86528	1.46148	0.59208
15	5.6388-03	6.4229+00	NM	1.02196	0.73288	0.88063	1.44451	0.60978
16	6.0706-03	6.5898+00	NM	1.01925	0.74315	0.88601	1.42142	0.62333
17	6.5024-03	6.7591+00	NM	1.01687	0.75342	0.89119	1.39914	0.63695
18	6.9342-03	6.9884+00	NM	1.02200	0.76712	0.90155	1.38114	0.65274
19	7.3660-03	7.1631+00	NM	1.02028	0.77740	0.90674	1.36041	0.66651
20	7.7724-03	7.3998+00	NM	1.01458	0.79110	0.91192	1.32878	0.68628
21	8.2042-03	7.5197+00	NM	1.01769	0.79795	0.91710	1.32095	0.69427
22	8.6360-03	7.8857+00	NM	1.01617	0.81849	0.92746	1.28399	0.72233
23	9.0678-03	8.0098+00	NM	1.00836	0.82534	0.92740	1.26277	0.73447
24	9.4996-03	8.1979+00	NM	1.00817	0.83562	0.93264	1.24571	0.74868
25	9.9314-03	8.3884+00	NM	1.00821	0.84589	0.93782	1.22918	0.76297
26	1.0338-02	8.5812+00	NM	1.00847	0.85616	0.94301	1.21314	0.77732
27	1.0770-02	8.8420+00	NM	1.01649	0.86986	0.94337	1.20121	0.79367
28	1.1201-02	9.1738+00	NM	1.01048	0.88699	0.95855	1.16787	0.82077
29	1.1633-02	9.2409+00	NM	1.00718	0.89041	0.95855	1.15891	0.82712
30	1.2065-02	9.3083+00	NM	1.01480	0.89384	0.96373	1.16251	0.82901
31	1.2497-02	9.4439+00	NM	1.00832	0.90068	0.96373	1.14489	0.84176
32	1.2903-02	9.7182+00	NM	1.00653	0.91438	0.96891	1.12282	0.86292
33	1.3335-02	9.9267+00	NM	1.00809	0.92466	0.97409	1.10474	0.87773
34	1.3767-02	1.0208+01	NM	1.00688	0.93836	0.97927	1.08411	0.89915
35	1.4199-02	1.0422+01	NM	1.00883	0.94863	0.98446	1.07696	0.91411
36	1.4631-02	1.0639+01	NM	1.01094	0.95890	0.98964	1.06513	0.92913
37	1.5062-02	1.0897+01	NM	1.00267	0.96918	0.98964	1.04267	0.94914
38	1.5494-02	1.0931+01	NM	1.11047	0.97260	0.99482	1.04621	0.95088
39	1.5900-02	1.1070+01	NM	1.00511	0.97945	0.99482	1.03162	0.96434
40	1.6312-02	1.1192+01	NM	1.00247	0.98288	0.99482	1.02445	0.97108
41	1.6764-02	1.1301+01	NM	1.00768	0.98973	1.00000	1.02087	0.97956
42	1.7196-02	1.1301+01	NM	1.00768	0.98973	1.00000	1.02087	0.97956
43	1.7628-02	1.1376+01	NM	1.00509	0.99315	1.00000	1.01384	0.98635
44	1.8059-02	1.1442+01	NM	1.00253	0.99658	1.00000	1.00688	0.99316
45	1.8486-02	1.1452+01	NM	1.00253	0.99658	1.00000	1.00688	0.99316
46	1.8898-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
47	1.9329-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
48	1.9761-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
49	2.0193-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
50	2.0625-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
51	2.1031-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
52	2.1463-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
53	2.1895-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
54	2.2327-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
55	2.2758-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
56	2.3190-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
57	2.3597-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
58	2.4028-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
59	2.4460-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
60	2.4892-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
61	2.5324-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
62	2.5654-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
63	2.6162-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
64	2.6670-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
65	2.6924-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
66	2.7432-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
67	2.7940-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
68	2.8194-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
69	2.8702-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
70	2.9210-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
71	2.9718-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
72	2.9972-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
73	3.0480-02	1.1527+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,H,U ASSUME P=PD

76010303

VAS

PROFILE TABULATION

67 POINTS, DELTA AT POINT 67

I	Y	P12/P	P/PD	T0/T0D	M/MD	U/U0D	T/TD	RHO/RHOD*U/U0D
1	0.0000+00	1.0000+00	NM	1.04651	0.00000	0.00000	2.83109	0.00000
2	1.7526-04	1.9152+00	NM	1.03903	0.34589	0.52850	2.33458	0.22638
3	6.0960-04	3.7244+00	NM	1.02467	0.54110	0.73572	1.84890	0.39794
4	1.0459-03	4.1379+00	NM	1.02734	0.57534	0.76684	1.77646	0.43167
5	1.4703-03	4.4880+00	NM	1.02209	0.60274	0.78756	1.70731	0.46129
6	1.9152-03	4.8084+00	NM	1.02670	0.62671	0.80829	1.66341	0.48592
7	2.3495-03	4.9973+00	NM	1.02659	0.64081	0.81865	1.63411	0.50098
8	2.7940-03	5.2394+00	NM	1.02081	0.65755	0.82902	1.58460	0.52152
9	3.2258-03	5.4881+00	NM	1.01630	0.67466	0.83938	1.54792	0.54226
10	3.6576-03	5.5894+00	NM	1.02982	0.68151	0.84974	1.55445	0.54658
11	4.0894-03	5.8473+00	NM	1.02659	0.69863	0.86010	1.51568	0.56747
12	4.5212-03	6.0583+00	NM	1.01739	0.71233	0.86528	1.47556	0.58641
13	4.9530-03	6.3280+00	NM	1.01599	0.72945	0.87565	1.44100	0.60766
14	5.3848-03	6.5484+00	NM	1.02026	0.74315	0.88601	1.42142	0.62333
15	5.8166-03	6.7730+00	NM	1.02498	0.75685	0.89637	1.40268	0.63904
16	6.2738-03	7.0597+00	NM	1.01391	0.77397	0.91194	1.35685	0.66445
17	6.7056-03	7.2937+00	NM	1.01966	0.78767	0.91192	1.34036	0.68035
18	7.1374-03	7.5319+00	NM	1.01429	0.80137	0.91710	1.30968	0.70025
19	7.5692-03	7.8525+00	NM	1.01792	0.80822	0.92228	1.30217	0.70876
20	8.0010-03	7.8969+00	NM	1.01290	0.82192	0.92746	1.27331	0.72839
21	8.4328-03	8.1455+00	NM	1.00877	0.83562	0.93264	1.24571	0.74888
22	8.8646-03	8.5905+00	NM	1.01650	0.85959	0.94819	1.21676	0.77927
23	9.2964-03	8.8505+00	NM	1.01348	0.87329	0.95337	1.19181	0.79993
24	9.7282-03	9.0482+00	NM	1.01423	0.88356	0.95855	1.17694	0.81444
25	1.0185-02	9.3029+00	NM	1.00866	0.90068	0.96373	1.14489	0.84176
26	1.0617-02	9.6554+00	NM	1.00682	0.91438	0.96891	1.12282	0.86292
27	1.1049-02	9.7931+00	NM	1.01140	0.92123	0.97409	1.11805	0.87124
28	1.1481-02	1.0002+01	NM	1.01303	0.93151	0.97927	1.10519	0.88607
29	1.1913-02	1.0213+01	NM	1.00416	0.94178	0.97927	1.08121	0.90572
30	1.2344-02	1.0355+01	NM	1.00900	0.94863	0.98446	1.07696	0.91411
31	1.2776-02	1.0498+01	NM	1.00332	0.95548	0.98446	1.06157	0.92736
32	1.3208-02	1.0714+01	NM	1.00551	0.96575	0.98964	1.05007	0.94245
33	1.3665-02	1.0933+01	NM	1.00766	0.97603	0.99482	1.03888	0.95759
34	1.4097-02	1.1080+01	NM	1.00252	0.98288	0.99482	1.02445	0.97108
35	1.4529-02	1.1154+01	NM	0.99990	0.98630	0.99482	1.01735	0.97786
36	1.4961-02	1.1154+01	NM	0.99990	0.98630	0.99482	1.01735	0.97786
37	1.5392-02	1.1228+01	NM	1.00771	0.98973	1.00000	1.02087	0.97956
38	1.5824-02	1.1302+01	NM	1.00512	0.99315	1.00000	1.01384	0.98635
39	1.6256-02	1.1302+01	NM	1.00512	0.99315	1.00000	1.01384	0.98635
40	1.6688-02	1.1302+01	NM	1.00512	0.99315	1.00000	1.01384	0.98635
41	1.7120-02	1.1302+01	NM	0.99473	0.99315	0.99482	1.00336	0.99149
42	1.7577-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
43	1.8009-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
44	1.8440-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
45	1.8872-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
46	1.9304-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
47	1.9736-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
48	2.0168-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
49	2.0599-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
50	2.1057-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
51	2.1488-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
52	2.3647-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
53	2.4079-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
54	2.4536-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
55	2.4968-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
56	2.5400-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
57	2.5908-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
58	2.2784-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
59	2.3216-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
60	2.1920-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
61	2.2352-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
62	2.6162-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
63	2.6670-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
64	2.7178-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
65	2.7686-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
66	2.7940-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
D 67	2.8448-02	1.1452+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M,U ASSUME P=PD

76010403

VAS

PROFILE TABULATION

73 POINTS, DELTA AT POINT 73

I	Y	P12/P	P/PD	T0/T0D	M/MD	U/UD	T/TD	RHO/RHOD*U/UD
1	0.0000+00	1.0000+00	NM	1.04613	0.00000	0.00000	2.87927	0.00000
2	3.6322-04	2.3786+00	NM	1.03135	0.40203	0.59794	2.21209	0.27031
3	6.3246-04	3.5667+00	NM	1.03059	0.52027	0.72165	1.92395	0.37509
4	9.0170-04	4.3108+00	NM	1.02391	0.58108	0.77320	1.77054	0.43670
5	1.1709-03	4.5330+00	NM	1.02800	0.59797	0.78866	1.73447	0.45339
6	1.4376-03	4.7618+00	NM	1.01990	0.61486	0.74897	1.68850	0.47318
7	1.7069-03	4.9023+00	NM	1.02614	0.62500	0.80928	1.67062	0.48268
8	1.9761-03	5.0934+00	NM	1.02629	0.63851	0.81959	1.64760	0.49744
9	2.2454-03	5.3381+00	NM	1.02104	0.65541	0.82990	1.60335	0.51760
10	2.5121-03	5.4378+00	NM	1.02179	0.66216	0.83505	1.59037	0.52807
11	2.7688-03	5.5894+00	NM	1.02945	0.67230	0.84536	1.56111	0.53466
12	3.0480-03	5.7433+00	NM	1.02490	0.68243	0.85052	1.55326	0.54757
13	3.3274-03	5.8923+00	NM	1.01539	0.69595	0.85567	1.51169	0.56604
14	3.5814-03	6.1117+00	NM	1.02397	0.70608	0.86598	1.50420	0.57571
15	3.8608-03	6.3280+00	NM	1.01562	0.71959	0.87113	1.46553	0.59482
16	4.1148-03	6.4929+00	NM	1.02477	0.72973	0.88144	1.45903	0.60413
17	4.3942-03	6.7165+00	NM	1.01746	0.74324	0.88660	1.42296	0.62307
18	4.6482-03	6.9442+00	NM	1.02253	0.75676	0.89691	1.40470	0.63851
19	4.9276-03	7.1762+00	NM	1.01636	0.77027	0.90206	1.37147	0.65773
20	5.2070-03	7.2937+00	NM	1.01929	0.77703	0.90722	1.36317	0.66552
21	5.4610-03	7.5319+00	NM	1.01392	0.79054	0.91237	1.33197	0.68498
22	5.7404-03	7.5970+00	NM	1.02126	0.79392	0.91753	1.33562	0.68696
23	5.9944-03	7.7132+00	NM	1.01310	0.80068	0.91753	1.31310	0.69871
24	6.2738-03	7.8969+00	NM	1.01253	0.81081	0.92268	1.29498	0.71250
25	6.5278-03	8.0207+00	NM	1.01604	0.81757	0.92784	1.28796	0.72040
26	6.8072-03	8.2083+00	NM	1.01584	0.82770	0.93299	1.27099	0.73450
27	7.0866-03	8.3982+00	NM	1.01588	0.83784	0.93814	1.25377	0.74826
28	7.3406-03	8.5241+00	NM	1.00862	0.84459	0.93814	1.23379	0.76037
29	7.6200-03	8.7200+00	NM	1.00905	0.85473	0.94330	1.21798	0.77448
30	7.8740-03	8.7851+00	NM	1.01659	0.85811	0.94845	1.22165	0.77637
31	8.1534-03	8.8505+00	NM	1.01311	0.86149	0.94845	1.21209	0.78249
32	8.4074-03	9.1813+00	NM	1.00720	0.87838	0.95361	1.17863	0.80908
33	8.6868-03	9.3155+00	NM	1.01153	0.88814	0.95876	1.17328	0.81716
34	8.9662-03	9.3155+00	NM	1.01153	0.88814	0.95876	1.17328	0.81716
35	9.2202-03	9.5869+00	NM	1.00958	0.89865	0.96392	1.15094	0.83780
36	9.4946-03	9.5869+00	NM	1.00958	0.89865	0.96392	1.15094	0.83780
37	9.7436-03	9.7931+00	NM	1.01103	0.90878	0.96907	1.13708	0.85225
38	1.0033-02	9.8624+00	NM	1.00798	0.91216	0.96907	1.12867	0.85859
39	1.0267-02	1.0002+01	NM	1.01246	0.91892	0.97423	1.12400	0.86675
40	1.0566-02	1.0213+01	NM	1.01445	0.92905	0.97938	1.11128	0.88131
41	1.0846-02	1.0355+01	NM	1.00864	0.93581	0.97938	1.09529	0.89418
42	1.1100-02	1.0498+01	NM	1.00295	0.94257	0.97938	1.07964	0.90714
43	1.1379-02	1.0642+01	NM	1.00791	0.94932	0.98454	1.07556	0.91537
44	1.1633-02	1.0714+01	NM	1.00515	0.95270	0.98454	1.06794	0.92190
45	1.1913-02	1.0859+01	NM	1.01020	0.95946	0.98969	1.06401	0.93015
46	1.2167-02	1.1006+01	NM	1.00481	0.96622	0.98969	1.04918	0.94330
47	1.2446-02	1.1080+01	NM	1.00216	0.96959	0.98969	1.04188	0.94991
48	1.2725-02	1.1154+01	NM	1.00997	0.97297	0.99485	1.04547	0.95158
49	1.2979-02	1.1228+01	NM	1.00735	0.97635	0.99485	1.03824	0.95820
50	1.3259-02	1.1302+01	NM	1.00475	0.97973	0.99485	1.03109	0.96484
51	1.3513-02	1.1452+01	NM	0.99964	0.98649	0.99485	1.01702	0.97820
52	1.3792-02	1.1452+01	NM	0.99964	0.98649	0.99485	1.01702	0.97820
53	1.4046-02	1.1527+01	NM	1.00748	0.98986	1.00000	1.02058	0.97983
54	1.4326-02	1.1603+01	NM	1.00496	0.99324	1.00000	1.01365	0.98653
55	1.4605-02	1.1603+01	NM	1.00496	0.99324	1.00000	1.01365	0.98653
56	1.4859-02	1.1603+01	NM	1.00496	0.99324	1.00000	1.01365	0.98653
57	1.5138-02	1.1603+01	NM	1.00496	0.99324	1.00000	1.01365	0.98653
58	1.5392-02	1.1603+01	NM	1.00496	0.99324	1.00000	1.01365	0.98653
59	1.5672-02	1.1678+01	NM	1.00247	0.99662	1.00000	1.00679	0.99325
60	1.5951-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
61	1.6205-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
62	1.6485-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
63	1.6739-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
64	1.7018-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
65	1.7272-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
66	1.7551-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
67	1.7831-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
68	1.8085-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
69	1.8364-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
70	1.9050-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
71	2.0320-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
72	2.1590-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000
D 73	2.2860-02	1.1754+01	NM	1.00000	1.00000	1.00000	1.00000	1.00000

INPUT VARIABLES Y,M,U ASSUME P=PD

76010409		VAR		PROFILE TABULATION		34 POINTS, DELTA AT POINT 34			
I	Y	PT2/P	P/PO	T0/T0D	M/MO	U/UD	T/TD	RHO/RHOD*U/UD	
1	0.0000 ⁺⁰⁰	1.0000 ⁺⁰⁰	NM	1.04164	0.00000	0.00000	2.87927	0.00000	
2	1.0160 ⁻⁰⁴	2.0168 ⁺⁰⁰	NM	1.02916	0.35473	0.54124	2.32798	0.23249	
3	1.3716 ⁻⁰³	4.6514 ⁺⁰⁰	NM	1.02555	0.60473	0.79381	1.72312	0.46068	
4	2.6416 ⁻⁰³	5.0758 ⁺⁰⁰	NM	1.01819	0.63514	0.81443	1.64429	0.49531	
5	3.9116 ⁻⁰³	5.6237 ⁺⁰⁰	NM	1.01560	0.67230	0.84021	1.56188	0.53794	
6	5.1816 ⁻⁰³	6.0423 ⁺⁰⁰	NM	1.02110	0.69932	0.86082	1.51521	0.56812	
7	6.4516 ⁻⁰³	6.3125 ⁺⁰⁰	NM	1.01953	0.71622	0.87113	1.47939	0.58885	
8	7.7216 ⁻⁰³	6.7585 ⁺⁰⁰	NM	1.01647	0.74324	0.88660	1.42296	0.62307	
9	8.9916 ⁻⁰³	7.1040 ⁺⁰⁰	NM	1.02432	0.76351	0.90206	1.39585	0.64624	
10	1.0262 ⁻⁰²	7.2803 ⁺⁰⁰	NM	1.02276	0.77365	0.90722	1.37510	0.65975	
11	1.1532 ⁻⁰²	7.6400 ⁺⁰⁰	NM	1.02049	0.79392	0.91753	1.33562	0.68696	
12	1.2802 ⁻⁰²	8.0091 ⁺⁰⁰	NM	1.00796	0.81419	0.92268	1.28426	0.71845	
13	1.4072 ⁻⁰²	8.2604 ⁺⁰⁰	NM	1.01522	0.82770	0.93299	1.27059	0.73430	
14	1.5342 ⁻⁰²	8.5805 ⁺⁰⁰	NM	1.01917	0.84459	0.94330	1.24734	0.75623	
15	1.6612 ⁻⁰²	8.9070 ⁺⁰⁰	NM	1.01263	0.86149	0.94845	1.21209	0.78249	
16	1.7882 ⁻⁰²	9.2401 ⁺⁰⁰	NM	1.00678	0.87838	0.95361	1.17863	0.80908	
17	1.9152 ⁻⁰²	9.5113 ⁺⁰⁰	NM	1.00473	0.89189	0.95876	1.15557	0.82968	
18	2.0422 ⁻⁰²	9.8561 ⁺⁰⁰	NM	1.01072	0.90878	0.96907	1.13768	0.85225	
19	2.1692 ⁻⁰²	1.0137 ⁺⁰¹	NM	1.00941	0.92230	0.97423	1.11578	0.87314	
20	2.2962 ⁻⁰²	1.0421 ⁺⁰¹	NM	1.00842	0.93581	0.97938	1.09529	0.89418	
21	2.4232 ⁻⁰²	1.0710 ⁺⁰¹	NM	1.00775	0.94932	0.98454	1.07556	0.91537	
22	2.5400 ⁻⁰²	1.1077 ⁺⁰¹	NM	1.00470	0.96622	0.98969	1.04918	0.94330	
23	2.6570 ⁻⁰²	1.1300 ⁺⁰¹	NM	1.00727	0.97635	0.99485	1.03824	0.95820	
24	2.7740 ⁻⁰²	1.1451 ⁺⁰¹	NM	1.00213	0.98311	0.99485	1.02402	0.97151	
25	2.9210 ⁻⁰²	1.1602 ⁺⁰¹	NM	0.99709	0.98486	0.99485	1.01009	0.98491	
26	3.0480 ⁻⁰²	1.1678 ⁺⁰¹	NM	1.00494	0.99324	1.00000	1.01365	0.98653	
27	3.1750 ⁻⁰²	1.1678 ⁺⁰¹	NM	1.00494	0.99324	1.00000	1.01365	0.98653	
28	3.3020 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
29	3.4290 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
30	3.5560 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
31	3.6830 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
32	3.8100 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
33	3.9370 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	
D 34	4.0640 ⁻⁰²	1.1831 ⁺⁰¹	NM	1.00000	1.00000	1.00000	1.00000	1.00000	

INPUT VARIABLES Y,M,U ASSUME P=PD

SECTION 9
REFERENCES

9. REFERENCES

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