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Aerotherm TR-76-13

AEROTHERM GRAPHITE SURFACE KINETICS COMPUTER PROGRAM (GASKET2)
USER'S MANUAL

Acurex Corporation/Aerotherm Division
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December 1976



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Air Force Rocket Propulsion Laboratory
Director of Science and Technology
Air Force Systems Command
Edwards AFB, California 93523

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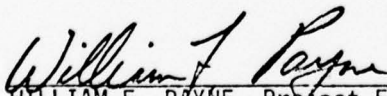
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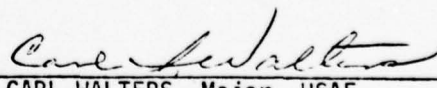
FOREWORD

This report was submitted by Acurex Corporation/ Aerotherm Division, 485 Clyde Avenue, Mountain View, CA 94042 under contract F04611-74-C-0023, Job Order No. 305909HUJ with the Air Force Rocket Propulsion Laboratory, Edwards AFB, California 93523.

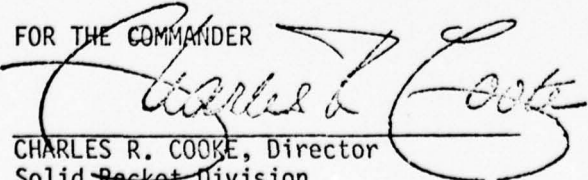
Contract work was performed in the period 1 May 1974 to 31 July 1976 and was documented in this final report and in a second final report (AFRPL-TR-76-71) which is classified CONFIDENTIAL. In addition to the final reports and other written documentation, a 2-day seminar was conducted by Aerotherm at its Mountain View facility to present contract results to the rocket motor community in a timely fashion. The Aerotherm work was managed by Mr. Roger J. Bedard, Manager, Propulsion Systems, and the Air Force Technical Monitor was Mr. William F. Payne.

This report has been reviewed by the Information Office/DOZ and is releasable to the National Technical Information Service (NTIS). At NTIS it will be available to the general public, including foreign nations. This report is unclassified and suitable for general public release.


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The Aerotherm GASKET code was modified. The modified code, entitled GASKET2, includes a generalized computational scheme for combined equilibrium - nonequilibrium systems, sublimation kinetics, and an expanded thermochemistry data bank including the Duff-Bauer hydrocarbon species. GASKET2 predicts higher ablation rates than GASKET at surface temperatures above 5500°R. Both codes predict virtually equal ablation rates at surface			

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cont

temperatures below 5500°R. GASKET2 also accepts an increased number of surface kinetics - controlled reactions.

In addition to the modifications, surface kinetics for ATJ and G-90 bulk graphites, 15% silicon carbide modified pyrolytic graphite and Pyrocarb 901 and Carbitex 700 carbon/carbon materials were added to GASKET2. Also, improved surface kinetics for C plane pyrolytic graphite were included. ↑

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SUMMARY

Recent studies at Aerotherm have shown that the accuracy and versatility of the GASKET code can be improved by some minor code modifications. These modifications were identified and incorporated into the GASKET code. The modified code, entitled GASKET2, includes a generalized computational scheme for combined equilibrium-nonequilibrium systems, sublimation kinetics, and an expanded thermochemistry data bank including the Duff-Bauer hydrocarbon species. With these modifications, GASKET2 predicts higher ablation rates than GASKET at surface temperatures above 5500°R. These rates reach the asymptotic diffusion controlled value at the high temperature limit. At surface temperatures below 5500°R, however, both codes predict results with insignificant discrepancies. In addition to the improved predictions, GASKET2 will also accept a larger number of surface kinetically controlled reactions than GASKET (limited to three). This will allow reactants other than the three currently used; namely, H_2O , CO_2 and H_2 .

In addition to the above modifications, GASKET2 was updated to include the surface kinetics of the following graphitic materials:

- 15% SiC/PG
- ATJ bulk graphite
- G-90 bulk graphite
- Pyrocarb 901 carbon/carbon
- Carbitex 700 carbon/carbon
- C plane pyrolytic graphite (improved kinetics)

Kinetic reaction rates for these materials were obtained from arc plasma generator and rocket motor data.

This report was prepared in two parts. The first part describes the code modifications and updates to GASKET. The differences between GASKET and GASKET2 are illustrated in terms of computational scheme and surface ablation rate predictions. Also, a brief description of the GASKET2 output

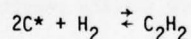
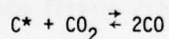
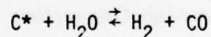
is included, so that users can use this code more effectively. The second part of the report contains an updated user's manual, a partial listing of GASKET2 which shows the locations where FORTRAN changes were made to GASKET, and three sample problems. Finally, it should be noted that this report serves only as an addendum to the earlier published GASKET reports.

SECTION 1
CODE MODIFICATIONS AND UPDATES

The Graphite Surface Kinetics (GASKET) computer code, developed under USAF Contract F04611-69-C-0081, was designed to calculate graphite surface thermochemical ablation rates as a result of exposure to propellant gases. The mathematical model, employed by GASKET, accounts for such thermophysical phenomena as:

- Diffusion of the reactive species from the boundary layer edge to the gaseous region adjacent to the carbon surface
- Adsorption of the reactive species to an active site on the carbon surface
- Formation of reaction products at the carbon surface
- Desorption of reaction products from the carbon surface
- Diffusion of reaction products into the boundary layer

Among all possible heterogeneous reactions occurring at the surface, only the following three were considered to be important at the temperature range and environments of interest:



Also under the same contract, the surface kinetics of the following materials were correlated:

- A-b plane pyrolytic graphite
- C plane pyrolytic graphite
- Bulk graphite

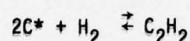
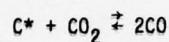
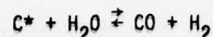
These correlations were then implemented into GASKET.

GASKET has been used extensively in rocket motor applications. The surface temperature range for this type of application is normally between 3000°R and 6000°R. For these applications, GASKET predicts satisfactory results.

Recently, the trend of rocket nozzle design has been altered somewhat. Instead of burning the conventional propellant and fabricating rocket nozzles with pyrolytic graphite, higher enthalpy propellants and graphitic materials such as carbon/carbon composite and bulk graphite are used. The introduction of these new elements into the rocket technology necessitated the assessment of the prediction ability of GASKET in a temperature range exceeding 6000°R and the correlation of the ablation kinetics of these graphitic materials. Under USAF Contract F04611-74-C-0023, GASKET was modified to handle the high temperature calculations, and was updated to contain the surface kinetics of the graphitic materials that were correlated under the same contract.

1.1 GENERAL EQUILIBRIUM-NONEQUILIBRIUM COMPUTATIONAL SCHEME

As mentioned previously, the thermochemical ablation of graphite materials as a result of exposure to propellant gases is assumed to be controlled by the following heterogeneous reactions:



This kinetic model appears to be a viable assumption in the temperature range between 3000°R and 6000°R as satisfactory predictions have been obtained. However, as surface temperature exceeds 6000°R, other surface activities may become significant, e.g., sublimation. Due to the intrinsic weakness of the computational scheme used in GASKET, the inclusion of more than three surface reactions may encounter difficulties (see Reference 1 for detailed discussion). Since more surface reactions are required to be considered in high temperature predictions, it is necessary that such an intrinsic weakness be removed by using a more general computational scheme.

GASKET was modified to accommodate more surface reactions. This capability was made possible by allowing reactants and products to be base as well as nonbase species (see Reference 2). Through internal bookkeeping, the net generation rate for each base species is calculated without the complication of introducing a fictitious base species (as was done in the previous version of GASKET).

A comparison of the computational procedures for the two versions of GASKET is demonstrated schematically in Figure 1. A (H, O) composition edge-gas reaction with a carbon surface was taken as an illustrative example. As can be seen, a fictitious base species (in this case, CO₂) was created in order to accommodate the three kinetically controlled reactions in the previous version of GASKET.

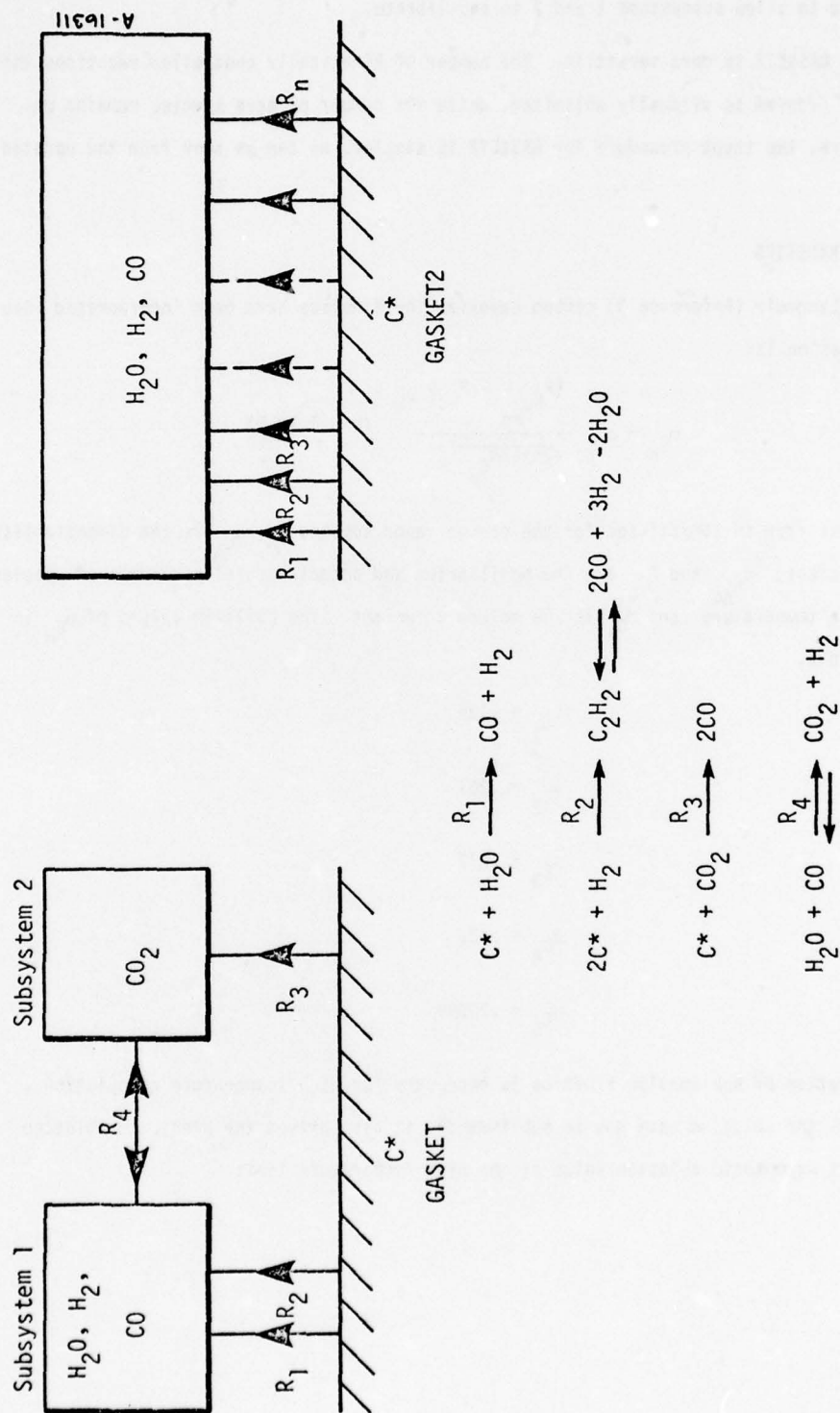


Figure 1. Comparison of computational schemes between the previous and modified versions of GASKET.

If more kinetically controlled reactions are required more fictitious base species should be created accordingly. In addition, since gas phase species are in equilibrium, an artificial infinite rate reaction is required to allow subsystems 1 and 2 to equilibrate.

In contrast, GASKET2 is more versatile. The number of kinetically controlled reactions that can be input to the program is virtually unlimited, while the number of base species remains unchanged. Furthermore, the input procedure for GASKET2 is simpler, as can be seen from the updated input instructions.

1.2 SUBLIMATION KINETICS

The Knudsen-Langmuir (Reference 3) carbon vaporization kinetics have been incorporated into GASKET2. The expression is:

$$m_{C_n} = \alpha_{C_n} \frac{(P_{C_{n,eq}} - P_{C_n})}{\sqrt{2\pi RT/M_{C_n}}} \quad (n = 1 \text{ to } 5)$$

where m_{C_n} is the mass flux in lbm/ft²-sec for the carbon vapor species C_n , α_{C_n} is the dimensionless vaporization coefficient, $P_{C_{n,eq}}$ and P_{C_n} are the equilibrium and actual partial pressures of species C_n , T is the surface temperature, and M_{C_n} is the molecular weight. The built-in values of α_{C_n} in GASKET2 are as follows:

$$\alpha_{C_1} = .125$$

$$\alpha_{C_2} = .261$$

$$\alpha_{C_3} = .012$$

$$\alpha_{C_4} = .130$$

$$\alpha_{C_5} = .00096$$

The incorporation of sublimation kinetics is necessary for high temperature calculations. It not only predicts the ablation rate due to sublimation, it also drives the predicted ablation rates to the correct asymptotic ablation value at the high temperature limit.

1.3 THERMOCHEMICAL EQUILIBRIUM DATA

The determination of a thermodynamic state of a chemical reacting system requires the input of thermochemical equilibrium data describing the formation of each species. In a particular temperature and pressure range of interest, some species can be neglected without affecting the accuracy of the calculation significantly. However, it does not guarantee the same accuracy can be maintained when the range has been surpassed. Therefore, a screening study was initiated to evaluate the built-in thermochemical equilibrium data in GASKET for high temperature calculations.

The results of the evaluation show that the Duff-Bauer hydrocarbon species, formed favorably at temperatures above 6000°R but not below, should be included in the built-in data bank. With the inclusion of the Duff-Bauer hydrocarbon species, GASKET2 predicts higher ablation rates at or above 5500°R. The reason for the increase in the predicted ablation rate is due to a significant increase in the formation of C_3H at temperatures above 5500°R. Carbon molecules which ablate to the gas phase through surface reactions are quickly reacted to form C_3H . Therefore, a larger carbon sink exists in the gas phase with C_3H species than the one without. Furthermore, the existence of C_3H species can alter the reactive species concentration at the carbon surface, and hence the ablation rates.

1.4 COMPARISONS OF GASKET AND GASKET2 PREDICTIONS

A sample problem was run to compare the predictions from GASKET and GASKET2. The selected problem considers the thermochemical ablation at the exit cone location of the rocket nozzle when exposed to PEG/FEFO propellant. The surface material was assumed to be bulk graphite. The comparison of the two solutions in terms of B' versus T_w is shown in Figure 2. Also shown in this figure is the surface equilibrium solution which serves as the baseline solution. As can be seen, both GASKET and GASKET2 solutions predicted B' values below the surface equilibrium value at surface temperatures below 5500°R. This indicates that the surface reactions are kinetically controlled. Also, note that both solutions agree with each other with less than 10 percent discrepancy. As the surface temperature exceeds 5500°R, the B' predicted by GASKET2 gradually approaches the surface equilibrium value, whereas the GASKET B' is still markedly below and has no trend of approaching the surface equilibrium B' .

From the results of this comparison, the following conclusions can be drawn:

- Both GASKET and GASKET2 predict similar results at or below 5500°R
- At the upper temperature limit, GASKET2 has the correct asymptotic functional behavior

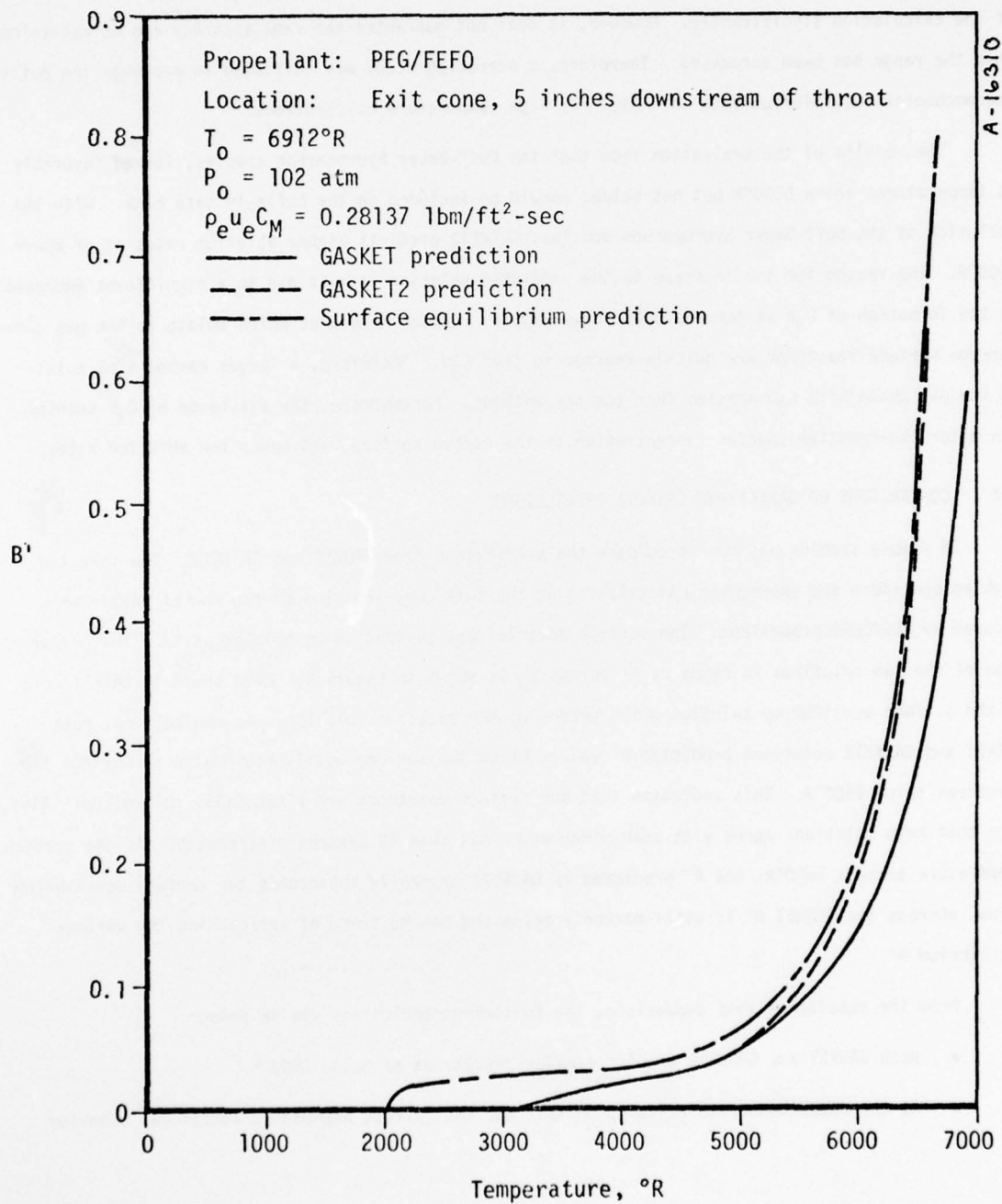


Figure 2. Comparison of GASKET and GASKET2 predictions.

1.5 DESCRIPTION OF GASKET2 OUTPUT ON TRANSPORT PROPERTIES AND SURFACE KINETICS INFORMATION

There are concerns by the users of whether GASKET2 computes transport properties based on both gas and condensed phase species, or on gas phase species alone. It is the purpose of this section to clarify that these properties are computed based on gas phase species only. The reason for neglecting condensed species is due to the common belief within the rocket community that condensed species have a small influence on boundary layer events.* For those users who also use ACE (Aerotherm Chemical Equilibrium code) to perform their inviscid flow field calculations, it should be noted that those transport properties are calculated including both gas and condensed phase species. Therefore, the user should evaluate the implications if those transport properties are being used.

For those users who are interested in obtaining information on how each individual heterogeneous reaction contributes to the total ablation rate, this information is also contained in the GASKET2 output. As an illustration, part of the GASKET2 output was extracted and presented in Figures 3 and 4. Figure 3 shows the printout of the built-in or input surface kinetic constants for each surface reaction. Note that the preexponential factor is normalized by the mass transfer coefficient ($\rho_e u_e C_M$). Shown at the bottom of Figure 4 for each surface reaction are the ablation rate and the ratio of the forward rate and the backward rate indicating how close the reaction is to being in equilibrium. By summing the net rates of all the surface reactions according to the following equation, the sum should be equal to B' .

$$B' = MW_{C*} \sum_{i=1}^N v_{C*i} [\text{Net Rate}]_i$$

N is the total number of surface reactions, and v_{C*i} is the stoichmetric coefficient of carbon for reaction i which can be obtained from the printout for surface kinetics information (see Figure 3).

*This is probably a valid assumption for regions near the nozzle throat; however, the noscap and exit cone regions must be evaluated more carefully.

TRANSFER COEFFICIENT RHOF*UE*CM= .94900+00

KINETIC

REACTION--- 1

1.00H2O +1.00C* -->1.00CO +1.00H2

INHIBITION TERMS

252.67H2O

541A.31CO2

.05CO

.00H2

POISONING TERMS

PRE-EXPONENT FACTOR .726+06 ACTIVATION ENERGY .102+06 T EXPONENT .433+00 8 8 0

8

REACTION--- A

5.00C* -->1.00CS

PRE-EXPONENT FACTOR .101-02 ACTIVATION ENERGY .000 T EXPONENT -.500+00 99 8 0

Figure 3. Typical GASKET2 output.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
 MASS TRANSFER COEFFICIENT ROUCM = .94900+00
 RHO V WALL/RHOE UE CM = .13546+00 BPRIME = .13546+00

STATE ADJACENT TO THE SURFACE
 TEMP = 6119.9999 DEG R = 3400.0000 DEG K PRESS = 31.47837 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LBM	.90329+03	.00000	.90329+03
ENTROPY - BTU/LBM DEG R	.28345+01	.00000	.00000
DENSITY - LBM/FT3	.15112+00		.15112+00
MOLECULAR WEIGHT	21.4580	.0000	21.4580

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM)	
1= .65142-03 2= .13623-02 3= .44967-02 4= .37470-04 5= .71843-04	
6= .28152-04 7= .13733-05 8= .21875-07	

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES

1= .14303+01 2= .14383+01 3= .20688+01 4= .14383+01 5= .20698+01
6= .29756+01 7= .42798+01 8= .61557+01

Figure 4. Typical GASKET2 output.

SECTION 2

INPUT INSTRUCTION MANUAL

2.1 GASKET2 INPUT

This section defines the format and significance of each field of the input data card deck for the modified Aerotherm Graphite Surface Kinetics (GASKET2) program. In the most general case, the input consists of eight card sets. These are:

1. CONTROL CARD
2. FROZEN-EDGE TEMPERATURE ARRAY
3. SURFACE TEMPERATURE ARRAY
4. ELEMENTAL COMPOSITION
5. DIFFUSION FACTOR DATA
6. SPECIES THERMOCHEMICAL EQUILIBRIUM DATA
7. OBLIQUE OR NORMAL SHOCK DATA
8. REACTION RATE DATA

Card Set 1 is a control card which contains a 10-element array, $KRK(I)$. This array controls most of the program options and tells the program what to expect from the remaining card sets. Few problems require all card sets since, in most cases, the user will wish to utilize the data built into the GASKET program to replace card sets 2, 3, 5, 6, and 8. The card sets are described in detail in this section.

CARD SET 1 - CONTROL CARD (2 Cards)

CARD 1

FIELD 1 (Columns 1-10, Format 10I1) the variable array $KRK(10)$ which is used to control the various program options.

COLUMN 1 -- EDGE THERMODYNAMIC STATE

0 Input
 1 Static state behind shock, upstream conditions input
 (card set 7)
 2 Same as 1, except stagnation state behind shock
 3 Isentropic expansion from input chamber conditions
 4 Static state behind shock, upstream conditions calculated
 via isentropic expansion from input chamber conditions
 (card set 7)
 5 Same as 4, except stagnation state behind shock

COLUMN 2 -- STATE OPTION (pertains to Z, cols. 11-20 of this card)

0 Assigned temperature
 2 Assigned enthalpy
 3 Assigned entropy

COLUMN 3 -- SPECIES THERMOCHEMICAL DATA

0 9 Use built-in thermochemistry data
 0 Use built-in diffusion factor data
 12 Read from cards new thermochemistry data, and if provided,
 diffusion factor data
 2 Print out thermochemistry data for allowable species
 9 Update diffusion factor data

COLUMN 4 -- CARBON SURFACE SPECIFICATION

1 Layer-oriented PG
 2 Edge-oriented PG
 3 General Bulk Graphite
 4 G-90 Bulk Graphite
 5 ATJ Bulk Graphite
 6 Carbitex 700 Carbon/Carbon
 7 PC-901 Carbon/Carbon
 8 SiC/PG

COLUMN 5 -- FROZEN -- EDGE TEMPERATURE ARRAY

0 Bypass this calculation
 1 Use built-in temperature array
 2 Read the temperature array from cards (card set 2)

COLUMN 6 -- SURFACE TEMPERATURE ARRAY

0 Bypass this calculation
 1 Use built-in temperature array
 2 Read the temperature array from cards (card set 3)

NOTE: When $KRK(6) \geq 1$, GASKET2 automatically provides two
 equilibrium surface calculations, for 500°K and 1000°K,
 with the restriction of zero ablation; this is done
 in order to provide tables for CMA and/or ASTHMA
 which facilitate smooth interpolation.

COLUMN 7 -- KINETIC CONSTANTS

0 Use built-in Arrhenius/Langmuir model
 1 3 Read from cards the pre-exponential factor, B'_i (lb mole
 reaction/ft²sec), activation energy, E_m (cal/gm mole), and
 temperature exponent, ϕ_m for both reaction and sublimation
 kinetics
 23 Read from cards the partial pressure multiplicative factors,
 ψ_{jm} and F_{jm} (atm⁻¹) for reaction kinetics only

COLUMN 8 -- EDGE GAS ELEMENTAL COMPOSITION

- 1 e.g. does not contain H or O (Kinetically inert surface)
- 2 e.g. does not contain H (reaction 2. only)
- 3 e.g. does not contain O (reaction 3. only)
- 4 e.g. contains both H and O (reactions 1., 2., and 3.)

COLUMN 9 -- PUNCHED CARD OUTPUT

- 0 No punched card output
- 1 3 Punch a card appropriate to CMA input for each convergent frozen edge or surface solution
- 23 Punch a card appropriate to ASTHMA input for each convergent frozen edge or surface solution

COLUMN 10 -- DIAGNOSTIC OUTPUT CONTROL

- 0 No diagnostic output
- 1 Output a single line of diagnostic information per iteration
- j (Where j is a digit greater than one) output full diagnostic information for 5(j-1) iterations and output a single line of diagnostic information for subsequent iterations.

FIELD 2 (Columns 11-20, Format F10.5) Thermodynamic State Variable, Z

- 1) a) If $KRK(2) = 0$, Z is assigned to temperature, °K
- b) If $KRK(2) = 2$, Z is assigned to enthalpy, cal/gm
- c) If $KRK(2) = 3$, Z is assigned to entropy, cal/gm°K
- 2) a) If $KRK(1) = 0$, Z pertains to the edge state
- b) If $KRK(1) = 1$ or 2, Z pertains to the thermodynamic state upstream of a shock wave
- c) If $KRK(1) > 3$, Z pertains to the chamber thermodynamic state
 - i) If $PC = 0$, Z pertains to the actual chamber state
 - ii) If $PC \neq 0$, Z pertains to the ideal chamber state (see PC, Cols. 41-50 of this card)

FIELD 3 (Columns 21-30, Format F10.5) Pressure, PR atm

- 1) If $KRK(1) = 0$, PR pertains to the edge thermodynamic state
- 2) If $KRK(1) \neq 0$, PR pertains to the actual chamber thermodynamic state or to the thermodynamic state upstream of a shock wave

FIELD 4 (Columns 31-40, Format F10.5) Edge or Shock Upstream Thermodynamic State, ZE

- 1) If $KRK(1) \leq 2$, this field is ignored
- 2) a) If $ZE > 0$, it is assigned as the pressure, atm, at either the edge ($KRK(1) = 3$), or the upstream side of a shock wave ($KRK(1) = 4$ or 5)
- b) If $ZE < 0$, it is assigned as the Mach number at either the edge ($KRK(1) = 3$) or the upstream side of a shock wave ($KRK(1) = 4$ or 5)

FIELD 5 (Columns 41-50, Format F10.5) Ideal Chamber Pressure, PC atm

FIELD 6 (Columns 51-60, Format F10.5) Mass Transfer Coefficient, ROUCM lbm/ft²sec

FIELD 7 (Columns 61-70, Format F10.5) Diffusion Coefficient Exponent for Unequal Diffusion Coefficient Model, GAMER

- 1) If $GAMER = 0.0$, it is automatically set to 2/3 (this value is appropriate for most calculations)
- 2) If $GAMER = 10^{-5}$, the diffusion model reduces to equal diffusion coefficients

FIELD 8 (Columns 71-80, Format 2A4,A4) Job Title, TILE (3)

CARD 2 If $KRK(4) \neq 8$, skip this card

FIELD 1 (Columns 1-10, Format F10.0) Mass fraction of SiC in SiC/PG

CARD SET 2 — FROZEN-EDGE TEMPERATURE ARRAY TFA(I) (number of cards = no. of temperatures + 1)

- 1) If KRK(5) = 0 or 1, skip this card set
- 2) If KRK(5) = 2, read in an array of no more than eight temperatures, TFA(I) °K

CARD(S) 1,2,... (Columns 1-10, Format F10.5) one temperature per card

FINAL CARD blank

NOTE: The TFA(I) array built into GASKET2 contains temperatures from 500 to 4000°K in 500°K increments

CARD SET 3 — SURFACE TEMPERATURE ARRAY TSA(I) (number of cards = no. of temperatures + 1)

- 1) If KRK(6) = 0 or 1, skip this card set
- 2) If KRK(6) = 2, read in an array of no more than fifteen temperatures, TSA(I) °K

CARD(S) 1,2,... (Columns 1-10, Format F10.5) one temperature per card

FINAL CARD blank

NOTE: The TSA(I) array built into GASKET2 contains temperatures from 1200 to 4000°K in 2000°K increments. Also, whenever KRK(6) $\geq$ 1 two surface equilibrium, zero-ablation calculations are performed for surface temperatures of 500 and 1000°K.

CARD SET 4 — ELEMENTAL COMPOSITION (number of cards = no. of elements +1)

CARD 1 (Columns 1-3, Format I3) the number of elements in the system

CARD 2,3,4 . . . (one card for each element)

FIELD 1 (Columns 1-3, Format I3) the atomic number of the element

FIELD 2 (Columns 4-15, Format 3A4) the name of the element (for output identification only)

FIELD 3 (Columns 16-25, Format F10.5) the atomic weight of the element

FIELD 4 (Columns 26-35, Format F10.5) the relative amount of the element in the edge gas (this is the same as the relative amount of the element in the chamber or at the upstream side of a shock wave, since elements are conserved)

- 1) Positive values are in relative gram-atomic-weights (or moles)
- 2) Negative values are in relative masses

FIELD 5 (Columns 46-55, Format F10.5) the relative amount of the element in the surface material (the present version of GASKET2 allows the surface to be comprised of carbon only; hence, the quantity 1.0 must be entered in this field for the element carbon)

CARD SET 5 — DIFFUSION FACTOR DATA (number of cards = 1/4 x (7 + no. of data items, e.g., diffusion factors, reference molecular weight, diffusion exponent)

- 1) If KRK(3) = 0, this card set must be skipped
- 2) If KRK(3) = 1,2,3, or 4, this card set may be skipped
- 3) If KRK(3) = 9, this card set must not be skipped

CARD 1 (Columns 1-3, Format I3) the total number of data items (e.g., diffusion factors, reference molecular weight, diffusion exponent) to be entered

Diffusion factors may be specified for any or all species individually and/or diffusion factors may be calculated via

$$\text{Diffusion Factor} = \left(\frac{\text{Molec.Wt.}}{\text{REFM}} \right)^{\text{FFA}}$$

where REFM and FFA may be specified here. For species for which diffusion factors are not specified individually, diffusion factors will be calculated via the above correlation, and if REFM and FFA are not specified, diffusion factors will be calculated from the above with REFM = 23.4 and FFA = 0.431.

CARD(S) 2,3, . . .

FIELDS 1,3,5,7 (Columns 1-8, 21-28, 41-48, 61-68, each Format 2A4)

The "name" of the species for which data is to be provided, exactly as it appears in columns 73-80 of the first card of the 3 thermochemical data cards (card set 6) for that species. To specify values of REFM or FFA in the next field, enter the alpha characters "REFM" or "FFA" respectively here.

FIELDS 2,4,6,8 (Columns 9-20, 29-40, 49-60, 69-80, each Format E12.4)

- 1) If the name of a chemical species was entered in the preceding field, this number is presumed to be a diffusion factor.
- 2) If the name REFM or FFA was entered in the preceding field, enter the desired values of REFM or FFA respectively in this field.

The diffusion factors introduced into the solution in this manner replace either the values set automatically (see card 1 above) if the species thermochemical data are read from cards or tape, or the values built into the GASKET2 program (see Volume II).

NOTE: If KRK(3) = 9 and KRK(1) = 1,2,4 or 5, this card set must follow the OBLIQUE OR NORMAL SHOCK DATA card set; if KRK(3) = 1,2,3, or 4 this card set, if used, precedes the SPECIES THERMOCHEMICAL EQUILIBRIUM DATA card set.

CARD SET 6 - SPECIES THERMOCHEMICAL EQUILIBRIUM DATA (number of cards = 1 + 3 x no. of species)

- 1) If KRK(3) = 0 or 9, skip this card set
- 2) If KRK(3) = 1,2,3, or 4, read in this card set; there are three of these cards for each molecular, atomic, or condensed species; the end of this card set is signaled by a blank card

CARDS 1,4,7 . . . Describe the elemental composition of the species and establish its name designation

FIELDS 1,3,5, . . . , 13 (one for each element in the species)
(Columns 1-3, 7-9, 13-15, . . . , 37-39, each format F3.0)

The number of atoms (of atomic number given in the following field) in a molecule of this species

(If field 1 is zero, this card is presumed to represent the end of card set 6)

FIELDS 2,4,6,. . . , 14. (one for each element in the species)
(Columns 4-6, 10-12, 16-18,. . . , 40-42, each format I3)

The atomic numbers of the elements in the molecule (the number of atoms of which was given in the previous field)

(If field 2 is zero, this card is presumed to be the first card of card set 5)

FIELD 15 (Columns 42-72, Format 7A4A2) the source and date of the thermochemical data for this specie. Used for output only

FIELD 16 (Columns 73-80, Format 2A4) the name designation of this species (e.g., AL2O3). This variable is used for output and as a means of identifying data entered in card set 5

CARDS 2,5,8. . . Lower temperature range thermochemical data

FIELDS 1,2,3,4,5 and 6 (Columns 1-54, Format 6E9.6) Input the 5 constants (F1,F2, F3,F4,F5,F6) appropriate to the lower temperature range of the thermodynamic data for this species. These constants are defined as follows, where T is in °K:

F1 = the heat of formation of the species at 298°K from the JANNAF base state (elements in most natural form at 298°K) in cal/mole

F2 = the enthalpy change of the species from 298°K to 3000°K in cal/mole

F3,F4 and F5 are defined by a curve fit to the heat capacity at constant pressure of the form:

$$C_p = F3 + F4 T + \frac{F5}{T^2} \text{ in cal/mole } ^\circ\text{K}$$

F6 = the entropy of the species at 3000°K in cal/mole °K

FIELD 7 (Columns 61-66, Format F6.0) the upper limit of the lower temperature range in °K

FIELD 8 (Column 67, Format I1) the phase specification:

- 1 signifies gaseous species
- 2 signifies solid species
- 3 signifies liquid species

The only phase combination allowed in one three card set is solid-liquid in which case a 2 and 3 would appear in fields 8 of cards 2 and 3, respectively.

CARDS 3,6,9. . . Upper temperature range thermochemical data

These cards are the same as cards 2,5,8. . . except use constants for the upper temperature range and field 7 is ignored

LAST CARD OF CARD SET 6 MUST BE BLANK

The end of the species thermochemical data is signified by a blank card. Hence, the last card of card set 6 must be a blank card.

NOTE: If this data is read in on cards, the atomic number of C* must be 106, rather than the actual value of 6. Finally, all condensed phase species (except C*) must follow the gas phase species.

CARD SET 7 — OBLIQUE OR NORMAL SHOCK DATA (1 card)

1) If KRK(1) = 0 or 3, skip this card set

2) If KRK(1) = 1, 2, 4, or 5, this card set must be read in

FIELD 1 (Column 1, Format I1) Input the variable KVH which determines how the velocity ahead of the shock, the static enthalpy ahead of the shock, and the total enthalpy are calculated (since total enthalpy = static enthalpy + $1/2$ velocity²)

If KVH = 1, velocity is calculated from specified total and static enthalpy

If KVH = 2, total enthalpy is calculated from specified static enthalpy and velocity

If KVH = 3, static enthalpy is calculated from specified total enthalpy and velocity

FIELD 2 (Columns 2-10, Format F9.4) The velocity variable, UR (this field is ignored if KVH = 1)

If UR $\neq$ -9999, then UR is assigned to SVL, the velocity upstream of the shock in ft/sec

If UR = -9999, the velocity calculated in the prior solution is assigned to SVL

FIELD 3 (Columns 11-20, Format F10.4) The total enthalpy variable, HTR (this field is ignored if KVH = 2)

If HTR $\neq$ 0, then HTR is assigned to HCH, the total enthalpy of the system in BTU/lbm

If HTR = 0, HCH is unchanged

FIELD 4 (Columns 21-30, Format F10.4) the static enthalpy variable, HSR (This field is ignored if KVH = 3)

If HSR $\neq$ -9999, then HSR is assigned to SH1, the static enthalpy upstream of the shock in BTU/lbm

If HSR = -9999, the static enthalpy calculated in the prior solution is assigned to SH1

FIELD 5 (Columns 41-50, Format F10.4) the shock angle (0.0 for a normal shock) in degrees

CARD SET 8 — REACTION RATE DATA (number of cards = 3 x MT - 10 at maximum)

1) If KRK(7) = 0, skip this card set

2) If KRK(7) = 1 or 3, the first subset of this card set must be read in

3) If KRK(7) = 2 or 3, the second subset of this card set must be read in

First Subset: MT cards

CARDS 1, 2, . . . , MT

FIELD 1 (Columns 1-10, Format E10.4), FKF(M) the preexponential factor for the Mth reaction, lb mole/ft²sec atm

FIELD 2 (Columns 11-20, Format E10.4), EAK(M), the activation energy for the Mth forward reaction, cal/gm mole

FIELD 3 (Columns 21-30, Format E10.4), EXK(M), the temperature exponent for the Mth reaction

Second Subset: 2 x MT -10 cards

CARDS MT + 1, MT + 3, MT + 5; . . . 3 x MT -13, 3 x MT -11;

FIELDS 1-6 (Columns 1-10 x 6, Format 8F10.6, inhibiting specie partial pressure coefficient, PSI (J,M), J = 1, 6 atm⁻¹)

CARDS MT + 2, MT + 4; MT + 6, 7, . . . 3 x MT - 12, 3 x MT -10

FIELDS 1-6 (Columns 1-10 x 6, Format 8F10.6, inhibiting specie partial pressure coefficient FKK(J,M), J = 1, 6, atm⁻¹)

NOTE: MT = no. of reactions

1) IF KRK(8) = 1, MT = 0, kinetics ignored

2) If KRK(8) = 2, MT = 1 + 5 sublimation kinetics reactions

M = 1 $C^* + CO_2 \rightleftharpoons 2CO$

J = 1 CO_2

J = 2 CO

3) If KRK(8) = 3, MT = 1 + 5 sublimation kinetics reactions

M = 1 $2C^* + H_2 \rightleftharpoons C_2H_2$

J = 1 H_2

4) If KRK(8) = 4, MT = 3 + 5 sublimation kinetics reactions

M = 1 $C^* + H_2O \rightleftharpoons CO + H_2$

M = 2 $C^* + CO_2 \rightleftharpoons 2CO$

M = 3 $2C^* + H_2 \rightleftharpoons C_2H_2$

J = 1 H_2O

J = 2 CO_2

J = 3 CO

J = 4 H_2

J = 5 CLH

J = 6 FH

TO TERMINATE A JOB

KRK(1) = 8 on final card

MULTIPLE JOBS

1) Several jobs may be loaded back to back, with a control card signifying the start of each new job:

CONTROL CARD #1

:

ELEMENTAL COMPOSITION #1

:

additional data as required for job #1

:

CONTROL CARD #2

:

ELEMENTAL COMPOSITION #2

:

additional data as required for job #2

:

KRK(1) = 8

- 2) If jobs following the first job have the same elemental composition as the first job, Card Set #4 (ELEMENTAL COMPOSITION) may be replaced by a single blank card for all jobs after the first:

CONTROL CARD #1

:

ELEMENTAL COMPOSITION #1

:

additional data as required for job #1

:

CONTROL CARD #2

:

blank card

:

additional data as required for job #2

:

KRK(1) = 8

2.2 NEW FORTRAN VARIABLE NAMES USED IN GASKET2

This section describes the names and definitions of the newly introduced FORTRAN variables resulting from the computer code modification. Since this is an addendum to Reference 1, similar format and abbreviations are adopted here.

LIST OF NEW FORTRAN VARIABLES APPEARING IN COMMON STATEMENTS, GASKET2

<u>Variable Name</u>	<u>Description</u>	<u>Routine(s) in Which Variable is Utilized</u>
CPER	Mass fraction of carbon in SiC/PG	KN,IM
FKKS(M)	Same definition as FFX(M)	T,KT
INP(M)	Chemical reaction index (8 = oxidation, 99 = sublimation)	T,KT
NMP(N,M)	Index used to locate the reactants in the thermochemical equilibrium data	T,KT
NMR(N,M)	Index used to locate the products in the thermochemical equilibrium data	T,KT
NPF(N,M)	Index used to locate the poisoning species in the thermochemical equilibrium data	T,KT
NPP(N,M)	Index used to locate the inhibiting species in the thermochemical equilibrium data	T,KT
PERCT	Mass fraction of SiC in SiC/PG	KN,IM
SIPER	Mass fraction of Si in SiC/PG	KN,IM

LIST OF NEW FORTRAN VARIABLES APPEARING IN SUBROUTINE KINET, GASKET2

<u>Variable Name</u>	<u>Description</u>
DBDP	Locally defined variable
VLNI	$(-H/RT + S/R)$ of reactant
VLNII	$(-H/RT + S/R)$ of product
VNNMR	Local variable for $VNU(I,J)$ of reactants
VNNMP	Local variable for $VNU(I,J)$ of products
VNNPP	Local variable for $VNU(I,J)$ of inhibiting species
VNNPF	Local variable for $VNU(I,J)$ of poisoning species
XX(M)	Saved value of preexponential constant

LIST OF NEW FORTRAN VARIABLES APPEARING IN SUBROUTINE THERM GASKET2

Variable Name	
FKKD(I,J,K)	Built-in values for poisoning species
FNAM(I,IZ)	Temporary variable for the chemical symbol of the species involved in the chemical reaction ($IZ < 4$ reactants, $5 < IZ < 8$ products, $9 < IZ < 16$ inhibiting species, $17 < IZ < 24$ poisoning species)
FSS(I)	Sublimation constants built-in value
IIZ	Index to define total number of species involved in the chemical reactions
INHB(I)	First four alphanumeric characters for the chemical symbol of the inhibiting species
IRX	Flag indicating type of surface reaction (1 = reactions involved H ₂ O species, 2 = reaction involved O species only, 3 = reaction involved H species only)
MS	Total number of sublimation kinetic reactions
POIS(I,J)	First four alphanumeric characters for the chemical symbol of the poisoning species
PRSP(I,J)	First four alphanumeric characters for the chemical symbol of products
PSID(I,J,K)	Built-in values for inhibiting coefficients
RXSP(I,J)	First four alphanumeric characters for the chemical symbol of reactants
RUCM	Same as ROUCM
SUBC	Locally defined variable

2.3 LISTING OF THE MODIFIED SUBROUTINES

The listing of the following subroutines are given in this section:

- IMELM
- INPUT
- KINET
- OUTPUT
- THERM
- KININ
- ZIPIN
- AFMAT
- ALPST
- BELCH
- CRECT
- GASKET
- MAT 1
- MAT 2
- MAT 3
- PROPS
- SCALE

The modifications made to the subroutines are shown in the right hand side column. The notation "***-n" means that n lines of FORTRAN statements have been deleted preceeding the line where "***-n" appeared. "*COR" indicates the location where new FORTRAN statements are inserted.

1


```

112.
113.
114.
115.
116.
117.
118.
119.
120.
121.
122.
123.

120  TOL(L)=TG(I,L)*DM(I,K)*TK(K,L)
125  RETURN
130  WRITE (ROUT,150)
135  STOP
140  C
145  FORMAT (13,3A4,4F10.5)
150  FORMAT (54HRELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS
      1 /4XGHA1,NO.3X7HELEMT4X9HATC1C 4TSX21HCO6F GAS
      213.3X3A4,4F10.5,2F13.7))
150  FORMAT (////40X,31HPROGRAM LIMITED TO 10 ELEMENTS )
      END
124.
125.
126.
127.
128.
129.
130.
131.
132.
133.
134.
135.

```

[illegible]

[illegible]

31

[illegible]

33

34

35

454.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4454	*COR
455.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4455	*COR
456.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4456	*COR
457.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4457	*COR
458.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4458	*COR
459.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4459	*COR
460.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4460	*COR
461.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4461	*COR
462.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/65	44H	INPU4462	*COR
463.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/64	44H	INPU4463	*COR
464.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/63	44H	INPU4464	*COR
465.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/63	44H	INPU4465	*COR
466.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/64	44H	INPU4466	*COR
467.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	4,44H/65	44H	INPU4467	*COR
468.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/65	44H	INPU4468	*COR
469.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/63	44H	INPU4469	*COR
470.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4470	*COR
471.	DATA (SOFCY(T)1=55,746)								
472.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/63	44H	INPU4472	*COR
473.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4473	*COR
474.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4474	*COR
475.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/67	44H	INPU4475	*COR
476.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4476	*COR
477.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/65	44H	INPU4477	*COR
478.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4478	*COR
479.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4479	*COR
480.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4480	*COR
481.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/62	44H	INPU4481	*COR
482.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	9,44H/63	44H	INPU4482	*COR
483.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4483	*COR
484.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4484	*COR
485.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4485	*COR
486.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/64	44H	INPU4486	*COR
487.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4487	*COR
488.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4488	*COR
489.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/63	44H	INPU4489	*COR
490.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4490	*COR
491.	DATA (SOFCY(T)1=73,849)								
492.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4492	*COR
493.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4493	*COR
494.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4494	*COR
495.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4495	*COR
496.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4496	*COR
497.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/67	44H	INPU4497	*COR
498.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4498	*COR
499.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4499	*COR
500.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/66	44H	INPU4500	*COR
501.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/61	44H	INPU4501	*COR
502.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4502	*COR
503.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/69	44H	INPU4503	*COR
504.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/70	44H	INPU4504	*COR
505.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/70	44H	INPU4505	*COR
506.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/60	44H	INPU4506	*COR
507.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	6,44H/70	44H	INPU4507	*COR
508.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/68	44H	INPU4508	*COR
509.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	12,44H/60	44H	INPU4509	*COR
510.	*2HJA-44HAE	44HTAPE	44H	7/7	44H1	3,44H/61	44H	INPU4510	*COR

[illegible]

568.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/65	4H	4H	INPU568	*COR
569.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/67	4H	4H	INPU569	*COR
570.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/66	4H	4H	INPU570	*COR
571.	DATA (SOURCE(1),1E1345,1496)/							*COR
572.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU572	*COR
573.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/70	4H	4H	INPU573	*COR
574.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/66	4H	4H	INPU574	*COR
575.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/66	4H	4H	INPU575	*COR
576.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU576	*COR
577.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/60	4H	4H	INPU577	*COR
578.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/64	4H	4H	INPU578	*COR
579.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU579	*COR
580.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/60	4H	4H	INPU580	*COR
581.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/62	4H	4H	INPU581	*COR
582.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/66	4H	4H	INPU582	*COR
583.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/60	4H	4H	INPU583	*COR
584.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/62	4H	4H	INPU584	*COR
585.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/64	4H	4H	INPU585	*COR
586.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/61	4H	4H	INPU586	*COR
587.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/63	4H	4H	INPU587	*COR
588.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/64	4H	4H	INPU588	*COR
589.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/67	4H	4H	INPU589	*COR
590.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/64	4H	4H	INPU590	*COR
591.	DATA (SOURCE(1),1E1497,1648)/							*COR
592.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/64	4H	4H	INPU592	*COR
593.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/64	4H	4H	INPU593	*COR
594.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/64	4H	4H	INPU594	*COR
595.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/62	4H	4H	INPU595	*COR
596.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/67	4H	4H	INPU596	*COR
597.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	9.4H/67	4H	4H	INPU597	*COR
598.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/61	4H	4H	INPU598	*COR
599.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/67	4H	4H	INPU599	*COR
600.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/67	4H	4H	INPU600	*COR
601.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/67	4H	4H	INPU601	*COR
602.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/70	4H	4H	INPU602	*COR
603.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU603	*COR
604.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/66	4H	4H	INPU604	*COR
605.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU605	*COR
606.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU606	*COR
607.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/65	4H	4H	INPU607	*COR
608.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU608	*COR
609.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/65	4H	4H	INPU609	*COR
610.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/70	4H	4H	INPU610	*COR
611.	DATA (SOURCE(1),1E1649,1800)/							*COR
612.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/63	4H	4H	INPU612	*COR
613.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/65	4H	4H	INPU613	*COR
614.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/65	4H	4H	INPU614	*COR
615.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/62	4H	4H	INPU615	*COR
616.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU616	*COR
617.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/64	4H	4H	INPU617	*COR
618.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/65	4H	4H	INPU618	*COR
619.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	12.4H/64	4H	4H	INPU619	*COR
620.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/65	4H	4H	INPU620	*COR
621.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/63	4H	4H	INPU621	*COR
622.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	3.4H/63	4H	4H	INPU622	*COR
623.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/60	4H	4H	INPU623	*COR
624.	*2HJA.4HJAE	*HTAPE.4H	7/7.4H1	6.4H/63	4H	4H	INPU624	*COR

625.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU625	*COR
626.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU626	*COR
627.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/63	4H	INPU627	*COR
628.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/63	4H	INPU628	*COR
629.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/63	4H	INPU629	*COR
630.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU630	*COR
631.	DATA (SORCY(1),1=1901,1952)/						
632.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/67	4H	INPU632	*COR
633.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU633	*COR
634.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU634	*COR
635.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/64	4H	INPU635	*COR
636.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU636	*COR
637.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU637	*COR
638.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU638	*COR
639.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/64	4H	INPU639	*COR
640.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU640	*COR
641.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU641	*COR
642.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU642	*COR
643.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/65	4H	INPU643	*COR
644.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/66	4H	INPU644	*COR
645.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/66	4H	INPU645	*COR
646.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU646	*COR
647.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU647	*COR
648.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU648	*COR
649.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU649	*COR
650.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU650	*COR
651.	DATA (SORCY(1),1=1953,2104)/						
652.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/70	4H	INPU652	*COR
653.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU653	*COR
654.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/66	4H	INPU654	*COR
655.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU655	*COR
656.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU656	*COR
657.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/66	4H	INPU657	*COR
658.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/66	4H	INPU658	*COR
659.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU659	*COR
660.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU660	*COR
661.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU661	*COR
662.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU662	*COR
663.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	3.4H/67	4H	INPU663	*COR
664.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/67	4H	INPU664	*COR
665.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	9.4H/67	4H	INPU665	*COR
666.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/67	4H	INPU666	*COR
667.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU667	*COR
668.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU668	*COR
669.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/68	4H	INPU669	*COR
670.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU670	*COR
671.	DATA (SORCY(1),1=2105,2216)/						
672.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU672	*COR
673.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU673	*COR
674.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/69	4H	INPU674	*COR
675.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU675	*COR
676.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	6.4H/70	4H	INPU676	*COR
677.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/60	4H	INPU677	*COR
678.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/60	4H	INPU678	*COR
679.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/61	4H	INPU679	*COR
680.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	**4H/61	4H	INPU680	*COR
681.	*2HJA.4HNAF	*HTAPE.4H	7/7.4H1	12.4H/70	4H	INPU681	*COR

682.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/70	4H	*COR
683.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/70	4H	*COR
684.	*2HCO,4HJAT	*HHR	2D,4H1H-12,4H2	12,4H/61	4H	*COR
685.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
686.	DATA (SQRX(1))=2217,23281/					
687.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
688.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
689.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
690.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
691.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
692.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
693.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
694.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
695.	*2HJU,4HJEF	*HHAUER,4H	6/6,4H1	4H	4H	*COR
696.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/63	4H	*COR
697.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
698.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
699.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/65	4H	*COR
700.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
701.	DATA (SQRX(1))=2329,24801/					
702.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/60	4H	*COR
703.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/65	4H	*COR
704.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/62	4H	*COR
705.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/64	4H	*COR
706.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/66	4H	*COR
707.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/70	4H	*COR
708.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
709.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/61	4H	*COR
710.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/62	4H	*COR
711.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/67	4H	*COR
712.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/65	4H	*COR
713.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/66	4H	*COR
714.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	0,4H/62	4H	*COR
715.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/66	4H	*COR
716.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
717.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	*COR
718.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
719.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
720.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
721.	DATA (SQRX(1))=2481,26321/					
722.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
723.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/65	4H	*COR
724.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/61	4H	*COR
725.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/63	4H	*COR
726.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/63	4H	*COR
727.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
728.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/62	4H	*COR
729.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/69	4H	*COR
730.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/66	4H	*COR
731.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/64	4H	*COR
732.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
733.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	3,4H/67	4H	*COR
734.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	12,4H/64	4H	*COR
735.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/65	4H	*COR
736.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/70	4H	*COR
737.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	6,4H/67	4H	*COR
738.	*2HJA,4HJAE	*HTAPE,4H	7/7,4H1	9,4H/64	4H	*COR

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1195. * 2.4146E+1, 2.3695E+1, 2.2074E+1, 3.5026E+1, 1.2408E+1, 1.1942E+1, INPU1169
1196. * 4.0773E+1, 4.0808E+1, 4.1234E+1, 4.4455E+1, 1.1280E+1, 1.0388E+1, INPU1170
1197. * 6.8219E+0, 6.7984E+0, 3.0774E+1, 3.3646E+1, 3.2724E+1, 4.3491E+1, INPU1171
1198. * 3.3567E+1, 4.0269E+1, 2.5809E+0, 7.5808E+0, 2.8773E+1, 3.4622E+1, INPU1172
1199. * 5.6046E+0, 7.5001E+0, -1.7944E+0, 2.9604E+1, 2.3000E+1, 3.2520E+1, INPU1173
1200. * 4.2931E+0, 7.9250E+0, 1.0222E+1, 1.6000E+1, 1.8114E+1, 2.2002E+1, INPU1174
1201. * 3.2065E+1, 3.2001E+1, 1.7521E+1, 1.0053E+1, 1.5340E+1, INPU1175
1202. * 9.5257E+0, 2.0740E+1, 1.7445E+1, 2.4000E+1, 1.7404E+1, 2.0511E+1, INPU1176
1203. * 5.4604E+0, 6.5000E+0, 1.8374E+1, 3.4558E+1, 2.2462E+1, 2.9020E+1, INPU1177
1204. * 1.1016E+1, 1.3845E+1, 3.0894E+1, 4.0000E+1, 3.5032E+1, 3.9538E+1, INPU1178
1205. * 4.7458E+1, 1.0114E+2, 6.1414E+1, 7.6250E+1, 1.1045E+2, 1.1088E+2, INPU1179
1206. * 3.7206E+1, 6.0372E+1, 7.0681E+0, 4.4321E+1, 3.2377E+1, 3.3346E+1, INPU1180
1207. * 2.2149E+1, 5.5500E+1, 1.2060E+2, 1.1204E+2, 7.0971E+1, 6.6165E+1, INPU1181
1208. * 3.7941E+1, 6.4517E+1, 8.4657E+1, 1.7419E+2, 3.7210E+0, 1.4900E+1, INPU1182
1209. * 1.3631E+1, 2.3636E+1, 2.6043E+1, 4.2291E+1, 5.9686E+1, 6.7238E+1, INPU1183
1210. * 2.9515E+1, 2.7617E+1, 2.8410E+1, 2.7439E+1, 5.1062E+1, 6.0000E+1, INPU1184
1211. DATA (BOX(1),I=1,108)/
1212. * 7.3366E-4, 2.0963E-4, 9.3467E-4, 3.6202E-4, 1.8325E-3, 2.3113E-4, INPU1186
1213. * 4.4145E-4, 4.6597E-5, 2.4001E-4, 2.1613E-4, 2.1387E-3, 4.5148E-4, INPU1187
1214. * 7.1091E-4, 1.3281E-4, 2.0861E-4, 1.3413E-4, 7.5355E-5, 7.6670E-5, INPU1189
1215. * 7.5222E-4, 4.4717E-4, 1.0863E-3, 2.3058E-4, 7.0445E-4, 5.8077E-5, INPU1189
1216. * 9.4415E-4, 7.7518E-5, 3.0453E-5, 2.7501E-4, 1.2781E-4, 1.0929E-4,
1217. * 1.5288E-4, 6.7172E-6, 2.5615E-5, 2.8001E-5, 6.5923E-5, 6.2719E-6, INPU1192
1218. * 4.1685E-5, 3.8524E-6, 8.0914E-6, 9.4384E-7, 4.0810E-5, 3.6685E-6, INPU1193
1219. * 1.9832E-5, 1.5300E-6, 1.1616E-4, 9.8950E-5, 6.4798E-5, 6.2062E-6, INPU1194
1220. * 5.8266E-5, 5.5773E-6, 9.6150E-5, 8.8091E-6, 3.8821E-4, 1.7961E-4, INPU1195
1221. * 3.4415E-4, 3.0878E-4, 9.7846E-4, 6.8802E-4, 1.3162E-4, 9.4657E-5, INPU1196
1222. * 1.6050E-3, -2.3623E-4, 3.4088E-5, 3.2431E-6, 6.7860E-5, 6.3272E-6, INPU1197
1223. * 1.9485E-4, 1.7666E-4, 1.0876E-5, 1.0434E-4, 1.2265E-4, 9.6225E-5, INPU1198
1224. * 1.3827E-4, 1.2620E-5, 2.8693E-4, 2.5576E-5, 3.0983E-4, 2.5995E-5, INPU1199
1225. * 6.5913E-5, 6.1657E-6, 1.8822E-4, 1.7170E-5, 1.0708E-4, 1.0014E-5, INPU1200
1226. * 2.1969E-4, 8.6130E-5, 3.7019E-4, 3.1900E-5, 2.3841E-4, 2.1384E-5, INPU1201
1227. * 3.8529E-4, 3.4161E-5, 5.4728E-4, 1.7700E-4, 7.8441E-4, 6.2918E-5, INPU1202
1228. * 1.3535E-3, 1.0251E-4, 1.0922E-3, 8.3036E-5, 1.4850E-3, 1.1442E-4, INPU1203
1229. * 2.2724E-3, 1.7133E-4, 2.6030E-3, 1.9311E-4, 3.7280E-4, 1.3944E-4, INPU1204
1230. DATA (BOX(1),I=109,222)/
1231. * 3.6453E-4, 2.9024E-4, 1.6625E-4, 1.0010E-4, 1.4660E-4, 1.6391E-5, INPU1206
1232. * 7.6907E-4, 2.9316E-4, 7.0071E-4, 5.7198E-5, 0.7299E-4, 7.1736E-5, INPU1207
1233. * 5.2082E-4, 4.8174E-5, 6.8102E-4, 8.7424E-5, 2.9162E-3, 2.1768E-4, INPU1208
1234. * 5.1844E-3, 3.9393E-4, 5.7402E-3, 4.6456E-4, 8.5585E-3, 6.9335E-4, INPU1209
1235. * 6.5025E-4, 1.6529E-3, 5.4078E-4, 4.9508E-4, 1.2468E-4, 2.0527E-4, INPU1210
1236. * 1.2237E-4, 1.1101E-5, 7.4204E-5, 6.6708E-6, 1.8597E-4, 8.7495E-5, INPU1211
1237. * 1.9885E-4, 1.7524E-5, 5.8003E-4, 1.7303E-4, 9.8146E-4, 7.2205E-5, INPU1212
1238. * 8.8052E-4, 7.3480E-5, 1.7328E-3, 1.7202E-4, 2.3777E-4, 8.3268E-5, INPU1213
1239. * 4.5384E-4, 4.1206E-6, 3.1763E-4, 2.8757E-5, 9.2717E-4, 8.2272E-5, INPU1214
1240. * 7.5243E-4, 6.8660E-5, 9.5619E-4, 2.5661E-4, 1.1273E-3, 1.0265E-4, INPU1215
1241. * 1.8477E-4, 2.8724E-4, 4.0880E-4, 3.6643E-5, 3.0731E-4, 2.7982E-5, INPU1216
1242. * 7.2948E-4, 3.0807E-4, 3.3204E-4, 2.1001E-5, 1.3028E-4, 1.2769E-5, INPU1217
1243. * 7.1462E-4, 6.5675E-6, 2.0691E-4, 1.8755E-4, 5.1259E-4, 4.0900E-5, INPU1218
1244. * 2.1250E-4, 6.4005E-4, 5.0949E-4, 4.3546E-5, 3.0722E-4, 2.7627E-5, INPU1219
1245. * 4.1370E-4, 3.7228E-5, 1.2231E-3, 1.4108E-4, 1.0262E-3, 8.0162E-5, INPU1220
1246. * 9.7387E-4, 7.5660E-5, 8.9112E-4, 6.8070E-5, 1.1768E-3, 9.1902E-5, INPU1221
1247. * 1.1804E-3, 9.3656E-5, 1.2157E-3, 8.7004E-5, 1.3106E-3, 9.7479E-5, INPU1222
1248. * 8.9487E-4, 1.6437E-4, 1.4627E-4, 1.0672E-4, 1.8070E-3, 1.3783E-4, INPU1223
1249. * 1.6948E-3, 1.2012E-4, 1.4300E-3, 1.4010E-4, 1.7955E-3, 1.3899E-4, INPU1224
1250. DATA (BOX(1),I=223,336)/
1251. * 2.2465E-3, 1.6416E-4, 2.4725E-3, 1.6643E-4, 7.2006E-3, 2.5752E-3, INPU1226

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DATA (PFX(1),I=557,562)/
* 5.0A3F-4, 2.464F-4, 9.592F-4, 3.647F-4, 7.660F-4, 4.5624F-4,
* 5.2A66F-4, 5.771F-4, 9.5056F-4, 7.332F-4, 5.7434F-4, 4.0251F-4,
* 7.3A92F-4, 4.5640F-4,
* 0.0000F+0, 0.0000F+0,
* 4.6546F-4, -1.1031F-4, 9.7467F-4, 1.2402F-4, 0.7132F-4, 4.1360F-4, INPUT244
DATA (PFX(1),I=563,569)/
* 2.4245F-4, 2.4465F-4, 2.4549F-4, 9.2427F-4, 4.1041F-4, 1.2406F-4, INPUT244
* 4.6160F-4, -2.7460F-4, 1.6211F-4, 1.0457F-4, 4.3324F-4, -4.7945F-4, INPUT247
* 8.1342F-4, 1.6317F-4, 2.9332F-4, -1.6090F-4, -1.0744F-4, 1.1715F-4, INPUT248
* 6.7773F-4, 6.7655F-4, 2.4553F-4, 7.2447F-4, 4.1934F-4, 3.0361F-4, INPUT249
* -3.4000F-4, -5.5234F-4, 3.1212F-4, 2.4790F-4, 7.0302F-4, 5.6028F-4, INPUT291
* 5.3363F-4, 2.1469F-4, 5.6164F-4, 1.1641F-4, 2.2394F-4, 1.6019F-4, INPUT291
* 7.8947F-4, -1.2806F-4, 3.7012F-4, 1.4524F-4, 5.3457F-4, 4.2766F-4, INPUT292
* 2.2470F-4, -1.2664F-4, 1.5556F-4, -3.3230F-4, 2.1540F-4, 4.8056F-4, INPUT294
* 2.5913F-4, -1.2664F-4, 5.0024F-4, -2.2434F-4, 3.42970F-4, 2.7940F-4, INPUT294
* 1.0640F-4, -2.60534F-4, 3.5049F-4, 3.6321F-4, 2.9909F-4, -2.2319F-4, INPUT295
* 9.1830F-4, 2.7540F-4, 1.1681F-4, -3.5856F-4, 3.2700F-4, 2.6077F-4, INPUT296
* 7.9007F-4, 2.7075F-4, 6.3162F-4, 3.3419F-4, 7.9272F-4, 6.4265F-4, INPUT297
* 2.6444F-4, 7.5265F-4, 1.6795F-4, 1.6077F-4, 1.4481F-4, 1.4015F-4, INPUT299
* 2.0141F-4, 4.5364F-4, 3.6115F-4, -4.8666F-4, 3.6519F-4, 3.0395F-4, INPUT299
* 3.5052F-4, 1.8624F-4, 7.2511F-4, 9.6566F-4, 3.1135F-4, 4.6023F-4, INPUT300
* 1.7105F-4, -4.8290F-4, 4.1024F-4, -1.8685F-4, 1.2609F-4, -6.0536F-4, INPUT301
* 9.3034F-4, -1.6243F-4, 1.4124F-4, -3.1587F-4, 1.1499F-4, 3.1862F-4, INPUT301
* -4.0594F-4, 9.8653F-4, 8.0419F-4, 1.1652F-4, 7.4406F-4, 1.0431F-4, INPUT303
DATA (PFX(1),I=1,108)/
* 7.5454F+5, -2.3397F+4, 6.1192F+4, -1.4686F+6, -3.0537F+5, -4.8199F+6, INPUT305
* -2.6202F+5, -1.5517F+5, -5.5646F+5, 1.3133F+6, -9.0356F+5, -3.8598F+6, INPUT306
* -1.3620F+5, -9.6431F+5, 2.0080F+4, -2.4202F+4, 2.2087F+9, -7.8207F+6, INPUT307
* 1.8767F+5, 2.4237F+5, -4.4592F+5, -2.7025F+6, -1.1239F+6, -9.2315F+5, INPUT308
* -1.2537F+6, -1.2764F+6, 2.3393F+4, 4.2753F+6, -1.5010F+5, -1.2884F+5,
* 5.5425F+4, 7.4690F+6, -2.5515F+5, -2.2401F+5, -4.8925F+5, -4.0093F+5, INPUT311
* 3.3255F+5, -2.7931F+5, -1.5681F+5, -1.4502F+5, -3.8557F+5, -3.3371F+5, INPUT312
* -2.8367F+5, -2.5430F+5, -1.6192F+5, -2.5325F+5, -4.9024F+5, -3.3371F+5, INPUT312
* 3.6152F+5, -2.7584F+5, -5.9316F+5, -4.7044F+5, -3.0152F+3, -1.7169F+5, INPUT314
* 9.2207F+5, -6.1044F+5, -8.1720F+5, -2.1306F+6, -1.9755F+5, -1.4604F+5, INPUT315
* 4.9078F+4, 5.8440F+5, -6.1080F+5, -5.5656F+5, -3.7134F+5, -2.8505F+5, INPUT316
* 9.4781F+5, -7.0767F+5, 3.9783F+3, 1.5432F+6, -1.7425F+5, -1.3641F+5, INPUT317
* 5.0053F+5, -3.4550F+5, -0.9623F+5, -6.2244F+5, -5.2422F+5, -9.2955F+5, INPUT318
* 3.6464F+5, -2.8292F+5, -7.2449F+5, -6.5544F+5, -6.0255F+5, -6.5705F+5, INPUT319
* 2.8742F+5, -3.3772F+5, -2.4804F+5, -2.44572F+5, -5.8394F+5, -1.5799F+5, INPUT320
* 1.0456F+6, -7.0136F+5, -2.4299F+5, -2.8193F+5, -7.9721F+5, -7.8006F+5, INPUT321
* -1.0900F+6, -2.7675F+6, -7.5323F+5, -1.3506F+6, -1.5903F+6, -2.3962F+6, INPUT322
* -1.2396F+6, -2.4809F+6, -2.0028F+6, -5.0075F+6, -2.6400F+5, -2.1633F+6, INPUT323
DATA (PFX(1),I=109,222)/
* -2.4444F+4, 2.7500F+4, -2.2066F+5, -1.5702F+5, -9.7323F+5, -8.1497F+5, INPUT325
* 3.7939F+4, -4.3406F+6, -9.0272F+5, -7.5324F+5, -1.2447F+5, -1.0443F+6, INPUT327
* -2.4061F+6, -1.7075F+6, -2.9596F+6, -2.0141F+6, -3.7641F+5, -7.8884F+6, INPUT327
* 5.1242F+6, -9.3543F+6, -7.4612F+6, -7.2422F+6, -1.2339F+7, -1.2056F+7, INPUT329
* 2.3222F+4, 1.4011F+7, -6.9566F+5, -4.7298F+5, -1.7104F+5, 1.5106F+6, INPUT329
* 3.9923F+5, -2.7519F+5, -3.2309F+5, -2.3590F+5, -2.6939F+5, -1.5799F+5, INPUT330
* 4.4.9720F+5, -3.3772F+5, -2.4804F+5, -2.44572F+5, -5.8394F+5, -1.5799F+5, INPUT330
* -1.1207F+6, -7.8756F+5, -1.2869F+6, -3.4952F+5, -2.9400F+5, -1.6583F+5, INPUT332
* 4.5954F+5, -4.0189F+5, -1.0619F+6, -7.1104F+5, -2.3217F+6, -1.4800F+6, INPUT333
* -2.9253F+6, -2.0856F+6, -3.7585F+6, -2.6669F+6, -6.6626F+6, -3.3910F+6, INPUT334
* -1.6167F+5, 2.0250F+6, -9.3453F+5, -7.0009F+5, -1.2554F+6, -9.1340F+5, INPUT335
* -4.8370F+4, -5.1415F+5, -7.5237F+5, -5.7552F+5, -8.5223F+5, -6.7942F+5, INPUT336

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-6.5052E+5, -5.6480E+5, -2.6692E+5, 1.1260E+6, -5.8892E+5, -6.1417E+5, INPUT1337
 -6.1477E+5, 3.0059E+6, -1.1277E+6, -8.2684E+5, -1.0609E+6, -7.3597E+5, INPUT1338
 -1.4684E+6, -1.0382E+6, -1.5722E+5, 8.3461E+5, -1.4660E+6, -1.9919E+6, -1.7678E+6, INPUT1339
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 -1.7235E+6, -2.1241E+6, -6.0798E+5, -3.2513E+6, -9.3415E+5, -2.5933E+6, INPUT1341
 -7.2517E+5, -1.1444E+6, -7.8497E+5, -2.5867E+6, -1.7275E+6, -3.0560E+6, INPUT1342
 -1.5574E+6, -2.5883E+6, -1.9968E+6, -3.0755E+6, -1.4260E+6, -2.2441E+6, INPUT1343
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 -1.5940E+6, -8.0020E+6, -1.1531E+6, -3.1502E+6, -1.9174E+6, -4.8745E+6, INPUT1346
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 -1.3750E+5, -3.4187E+5, -4.4067E+5, -3.2621E+5, -1.7988E+5, -1.3923E+5, INPUT1353
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 -5.8013E+5, 1.6552E+6, -1.0305E+5, -2.3544E+5, 8.6210E+4, -2.1789E+6, INPUT1372
 -1.2670E+6, -1.3260E+6, -1.0227E+6, 2.6258E+5, -1.0501E+5, -7.9957E+5, INPUT1373
 -1.2621E+6, -9.2555E+5, -2.2201E+6, -2.2044E+6, -4.1166E+5, -3.0171E+5, INPUT1374
 -1.4563E+6, -3.6299E+6, -5.5940E+5, -7.2386E+5, -1.0473E+6, -7.3497E+5, INPUT1375
 -5.4094E+6, -6.4924E+5, -5.4200E+5, -3.4732E+5, -1.4545E+5, -1.9093E+5, INPUT1376
 3.2434E+6, -2.2870E+6, -3.2624E+6, -7.1782E+6, -9.0505E+5, -1.0574E+6, INPUT1377
 -6.8763E+5, -1.1755E+6, -3.4689E+6, -7.8610E+5, -3.5522E+5, -2.6099E+5, INPUT1378
 -1.0030E+6, -2.3123E+6, -6.0978E+5, 3.1691E+5, -2.5652E+5, -1.5444E+5, INPUT1379
 -2.1697E+6, -2.3123E+6, -9.5200E+5, -2.4924E+6, -1.5233E+6, -2.8375E+6, INPUT1380
 -2.1697E+6, -2.3123E+6, -9.5200E+5, -2.4924E+6, -1.5233E+6, -2.8375E+6, INPUT1381
 DATA (PFX(1),1=543,5561/
 -7.2642E+5, -2.3110E+6, -1.5808E+6, -1.2264E+5, -5.8226E+5, -1.9251E+6, INPUT1383
 -2.4470E+5, -2.3110E+5, -1.6078E+5, -1.1203E+5, -1.1253E+6, -8.1434E+5, INPUT1386
 -1.5544E+6, -8.2694E+5, -5.4651E+5, 1.1025E+7, -5.4578E+5, -4.4220E+5, INPUT1387
 -1.0204E+6, -7.4080E+5, -9.2695E+5, -6.603E+5, -1.2535E+6, -3.0707E+6, INPUT1388
 -3.0131E+5, -1.1702E+6, -3.2624E+6, -7.1782E+6, -9.0505E+5, -7.4072E+5, INPUT1389
 -1.0043E+6, -7.4660E+5, -6.6703E+5, -2.7205E+5, -5.9105E+5, -6.9513E+5, INPUT1390
 -5.1403E+5, -1.0944E+6, -6.6120E+5, 0.0684E+6, -1.1301E+5, -9.6533E+5, INPUT1391
 -6.1403E+5, -6.1021E+5, -2.5330E+5, 5.1899E+5, -4.3872E+5, -2.8643E+5, INPUT1392
 -4.3827E+5, -3.8031E+5, -1.3854E+7, 5.1622E+5, -1.8744E+6, INPUT1393

53

1440. * 1.4045E+2, 1.4045E+2, 1.9019E+2, 1.9019E+2, 1.0396E+2, 3.1670E+2, 3.1635E+2, INPUT447
1441. * 4.040E+1, 4.040E+1, 6.1650E+1, 6.1650E+1, 9.2640E+1, 7.1911E+1, 7.1906E+1, INPUT448
1442. * 9.2640E+1, 9.2640E+1, 9.2640E+1, 9.2640E+1, 9.2640E+1, 6.9403E+1, 6.9403E+1, INPUT449
1443. * 6.9403E+1, 6.9403E+1, 6.9403E+1, 6.9403E+1, 6.9403E+1, 7.8525E+1, 7.8525E+1, INPUT450
1444. * 7.8525E+1, 7.8525E+1, 7.8525E+1, 7.8525E+1, 7.8525E+1, 6.6146E+1, 6.6146E+1, INPUT451
1445. * 6.6146E+1, 6.6146E+1, 6.6146E+1, 6.6146E+1, 6.6146E+1, 1.2472E+2, 1.2472E+2, INPUT452
1446. * 1.2472E+2, 1.2472E+2, 1.2472E+2, 1.2472E+2, 1.2472E+2, 2.1159E+2, 2.1159E+2, INPUT453
1447. * 2.1159E+2, 2.1159E+2, 2.1159E+2, 2.1159E+2, 2.1159E+2, 1.2067E+2, 1.2067E+2, INPUT454
1448. * 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2067E+2, 1.2691E+2, 1.2691E+2, INPUT455
1449. * 1.2691E+2, 1.2691E+2, 1.2691E+2, 1.2691E+2, 1.2691E+2, 6.3628E+1, 6.3628E+1, INPUT456
1450. * 6.3628E+1, 6.3628E+1, 6.3628E+1, 6.3628E+1, 6.3628E+1, 1.0309E+2, 1.0309E+2, INPUT457
1451. * 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.0309E+2, 1.1582E+2, 1.1582E+2, INPUT458
1452. * 1.1582E+2, 1.1582E+2, 1.1582E+2, 1.1582E+2, 1.1582E+2, 9.4440E+1, 9.4440E+1, INPUT459
1453. * 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.4440E+1, 9.3005E+1, 9.3005E+1, INPUT460
1454. * 9.3005E+1, 9.3005E+1, 9.3005E+1, 9.3005E+1, 9.3005E+1, 1.0765E+2, 1.0765E+2, INPUT461
1455. * 1.0765E+2, 1.0765E+2, 1.0765E+2, 1.0765E+2, 1.0765E+2, 8.4916E+1, 8.4916E+1, INPUT462
DATA (PFX(1),1=225,336)/
1456. * 7.9413E+1, 7.9413E+1, 9.7425E+1, 9.7425E+1, 1.6706E+2, 1.6706E+2, 1.6706E+2, INPUT464
1457. * 1.6706E+2, 1.6706E+2, 1.6706E+2, 1.6706E+2, 1.6706E+2, 1.5327E+2, 1.5327E+2, INPUT465
1458. * 1.5327E+2, 1.5327E+2, 1.5327E+2, 1.5327E+2, 1.5327E+2, 1.3449E+2, 1.3449E+2, INPUT466
1459. * 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 1.3449E+2, 9.8562E+1, 9.8562E+1, INPUT467
1500. * 1.1726E+2, 1.1726E+2, 1.1726E+2, 1.1726E+2, 1.1726E+2, 1.3314E+2, 1.3314E+2, INPUT468
1501. * 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.3314E+2, 1.0691E+2, 1.0691E+2, INPUT469
1502. * 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.0691E+2, 1.1041E+2, 1.1041E+2, INPUT470
1503. * 1.1041E+2, 1.1041E+2, 1.1041E+2, 1.1041E+2, 1.1041E+2, 1.2895E+2, 1.2895E+2, INPUT471
1504. * 1.2895E+2, 1.2895E+2, 1.2895E+2, 1.2895E+2, 1.2895E+2, 7.1250E+1, 7.1250E+1, INPUT472
1505. * 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.1250E+1, 7.4094E+1, 7.4094E+1, INPUT473
1506. * 7.4094E+1, 7.4094E+1, 7.4094E+1, 7.4094E+1, 7.4094E+1, 1.1835E+2, 1.1835E+2, INPUT474
1507. * 1.1835E+2, 1.1835E+2, 1.1835E+2, 1.1835E+2, 1.1835E+2, 9.8560E+1, 9.8560E+1, INPUT475
1508. * 9.8560E+1, 9.8560E+1, 9.8560E+1, 9.8560E+1, 9.8560E+1, 1.4921E+2, 1.4921E+2, INPUT476
1509. * 1.4921E+2, 1.4921E+2, 1.4921E+2, 1.4921E+2, 1.4921E+2, 7.9375E+1, 7.9375E+1, INPUT477
1510. * 7.9375E+1, 7.9375E+1, 7.9375E+1, 7.9375E+1, 7.9375E+1, 8.4499E+1, 8.4499E+1, INPUT478
1511. * 8.4499E+1, 8.4499E+1, 8.4499E+1, 8.4499E+1, 8.4499E+1, 1.2133E+2, 1.2133E+2, INPUT479
1512. * 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.2133E+2, 1.0957E+2, 1.0957E+2, INPUT480
1513. * 1.0957E+2, 1.0957E+2, 1.0957E+2, 1.0957E+2, 1.0957E+2, 9.1212E+1, 9.1212E+1, INPUT481
1514. * 9.1212E+1, 9.1212E+1, 9.1212E+1, 9.1212E+1, 9.1212E+1, 1.0334E+2, 1.0334E+2, INPUT482
1515. * 1.0334E+2, 1.0334E+2, 1.0334E+2, 1.0334E+2, 1.0334E+2, 7.7799E+1, 7.7799E+1, INPUT483
1516. * 7.7799E+1, 7.7799E+1, 7.7799E+1, 7.7799E+1, 7.7799E+1, 6.5935E+1, 6.5935E+1, INPUT484
1517. * 6.5935E+1, 6.5935E+1, 6.5935E+1, 6.5935E+1, 6.5935E+1, 9.2543E+1, 9.2543E+1, INPUT485
1518. * 9.2543E+1, 9.2543E+1, 9.2543E+1, 9.2543E+1, 9.2543E+1, 7.0615E+1, 7.0615E+1, INPUT486
1519. * 7.0615E+1, 7.0615E+1, 7.0615E+1, 7.0615E+1, 7.0615E+1, 4.4087E+1, 4.4087E+1, INPUT487
1520. * 4.4087E+1, 4.4087E+1, 4.4087E+1, 4.4087E+1, 4.4087E+1, 7.1948E+1, 7.1948E+1, INPUT488
1521. * 7.1948E+1, 7.1948E+1, 7.1948E+1, 7.1948E+1, 7.1948E+1, 1.3492E+2, 1.3492E+2, INPUT489
1522. * 1.3492E+2, 1.3492E+2, 1.3492E+2, 1.3492E+2, 1.3492E+2, 6.9742E+1, 6.9742E+1, INPUT490
1523. * 6.9742E+1, 6.9742E+1, 6.9742E+1, 6.9742E+1, 6.9742E+1, 5.1990E+1, 5.1990E+1, INPUT491
1524. * 5.1990E+1, 5.1990E+1, 5.1990E+1, 5.1990E+1, 5.1990E+1, 1.2563E+2, 1.2563E+2, INPUT492
1525. * 1.2563E+2, 1.2563E+2, 1.2563E+2, 1.2563E+2, 1.2563E+2, 9.2667E+1, 9.2667E+1, INPUT493
1526. * 9.2667E+1, 9.2667E+1, 9.2667E+1, 9.2667E+1, 9.2667E+1, 1.0154E+2, 1.0154E+2, INPUT494
1527. * 1.0154E+2, 1.0154E+2, 1.0154E+2, 1.0154E+2, 1.0154E+2, 6.8967E+1, 6.8967E+1, INPUT495
1528. * 6.8967E+1, 6.8967E+1, 6.8967E+1, 6.8967E+1, 6.8967E+1, 1.1554E+2, 1.1554E+2, INPUT496
1529. * 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.1554E+2, 1.6604E+2, 1.6604E+2, INPUT497
1530. * 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.6604E+2, 1.2162E+2, 1.2162E+2, INPUT498
1531. * 1.2162E+2, 1.2162E+2, 1.2162E+2, 1.2162E+2, 1.2162E+2, 6.9295E+1, 6.9295E+1, INPUT499
1532. * 6.9295E+1, 6.9295E+1, 6.9295E+1, 6.9295E+1, 6.9295E+1, 1.1087E+2, 1.1087E+2, INPUT500
1533. * 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.1087E+2, 1.0951E+2, 1.0951E+2, INPUT501
1534. * 1.0951E+2, 1.0951E+2, 1.0951E+2, 1.0951E+2, 1.0951E+2, 1.0952E+2, 1.0952E+2, INPUT502
1535. * 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, 1.0952E+2, INPUT503
DATA (PFX(1),1=451,556)/


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1702.  NFI=K*NEF
1709.  IF (KR(3) - 5) 90,100,100
1710.  READ (WIN,400) (NFIAT(I),NFIAT(I),NFIAT(I),I=INF,NEF)
1711.  IF (KR(3) - 3) 10,95,95
1712.  WRITE (JAW) (NFIAT(I),NFIAT(I),NFIAT(I),I=INF,NEF)
1713.  GO TO 10
1714.  READ (JAW) (NFIAT(I),NFIAT(I),NFIAT(I),I=INF,NEF)
1715.  GO TO 10
1716.  DO 110 K=1,IS
1717.  C(I)=0.
1718.  DO 136 I=1,7
1719.  IF (JAT(I)) 115,130,115
1720.  DO 120 K=1,IS
1721.  IF (JAT(I) - K) 120,125,120
1722.  COS TIME
1723.  KK=1
1724.  GO TO 255
1725.  C(I)=ALPT(I)
1726.  COS TIME
1727.  WT=0.
1728.  IF (C(I) 140,135,140
1729.  WRITE (KOUT,405) (ALPT(K),JAT(K),K=1,7),SOURCE,ANCA,ANOR
1730.  I=1
1731.  LAKK=0
1732.  DO 155 I=1,IS
1733.  IF (C(I)) 145,150,145
1734.  LAKK=LAKK+1
1735.  I=1
1736.  ALPT(I)=C(I)
1737.  UT=WT+C(I)*VAT(I)
1738.  IF (J - IS) 160,160,220
1739.  J=J-1
1740.  IF (J) 160,190,165
1741.  DO 185 I=1,JP
1742.  T(I)=T(I)
1743.  U(I)=C(I)
1744.  U(I)=0.
1745.  IF (UG) 170,185,170
1746.  DO 175 I=1,IL
1747.  U(I,U)=U(I,U)-U(I,I)*UG
1748.  DO 180 I=JPL,JS
1749.  C(I)=C(I)-TAUT(I,L)*UG
1750.  U(I,U)=0.
1751.  DO 195 I=1,IS
1752.  IF (KRC(C(I)) - .001) 165,195,200
1753.  TAU(I,U)=0.
1754.  GO TO 220
1755.  V(I,U)=1
1756.  U(I,U)=1.
1757.  DO 205 L=1,LD
1758.  U(I,U)=U(I,U)/C(I)
1759.  DO 210 L=1,LS
1760.  TAU(I,U)=C(I)/C(I)
1761.  VC=V(I,U)
1762.  DO 215 L=1,IS
1763.  C(I,U)=ALPT(I)
1764.  KK=J

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INPUT 713
INPUT 714
INPUT 715
INPUT 716
INPUT 717
INPUT 718
INPUT 719
INPUT 720
INPUT 721
INPUT 722
INPUT 723
INPUT 724
INPUT 725
INPUT 726
INPUT 727
INPUT 728
INPUT 729
INPUT 730
INPUT 731
INPUT 732
INPUT 733
INPUT 734
INPUT 735
INPUT 736
INPUT 737
INPUT 738
INPUT 739
INPUT 740
INPUT 741
INPUT 742
INPUT 743
INPUT 744
INPUT 745
INPUT 746
INPUT 747
INPUT 748
INPUT 749
INPUT 750
INPUT 751
INPUT 752
INPUT 753
INPUT 754
INPUT 755
INPUT 756
INPUT 757
INPUT 758
INPUT 759
INPUT 760
INPUT 761
INPUT 762
INPUT 763
INPUT 764
INPUT 765
INPUT 766
INPUT 767
INPUT 768
INPUT 769

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1765.	KKK=J	INPUT 777
1766.	J=J+1	INPUT 777
1767.	GO TO 255	INPUT 777
1768.	CONTINUE	INPUT 775
1769.	IF (J - 10) 225,225,200	INPUT 776
1770.	GO 256	INPUT 777
1771.	WRITE(11,1)=W(1,0)	INPUT 779
1772.	GO 255	INPUT 777
1773.	WRITE(11,1)=0.	INPUT 777
1774.	GO TO 250	INPUT 779
1775.	GO 245	INPUT 780
1776.	WRITE(11,1)=0.	INPUT 781
1777.	GO 245	INPUT 782
1778.	WRITE(11,1)=W(11,1)+C(1)*W(1,1)	INPUT 783
1779.	WRITE(11,1)	INPUT 783
1780.	KKK=1	INPUT 785
1781.	IF=11+1	INPUT 796
1782.	VC=0.	INPUT 787
1783.	IF (KK(13) - 5) 260,290,290	INPUT 789
1784.	IF (KK(13)-1) 275,265,275	INPUT 789
1785.	GO 270	INPUT 790
1786.	WRITE(11,1)=W(1,0)	INPUT 791
1787.	WRITE(11,1)=W(1,0)	INPUT 792
1788.	PC(KK,K)=SC(K,K+JAN)	INPUT 793
1789.	PC(KK,K)=SC(K,K+JAN)	INPUT 794
1790.	PC(KK,K)=SC(K,K+JAN)	INPUT 795
1791.	PC(KK,K)=SC(K,K+JAN)	INPUT 796
1792.	PC(KK,K)=SC(K,K+JAN)	INPUT 797
1793.	PC(KK,K)=SC(K,K+JAN)	INPUT 798
1794.	GO TO 266	INPUT 799
1795.	WRITE(11,1)=W(1,0)	INPUT 800
1796.	1,WRITE(11,1)=W(1,0)	INPUT 801
1797.	IF (KK(13)-1) 295,205,265	INPUT 802
1798.	WRITE(11,1)=W(1,0)	INPUT 803
1799.	100,WRITE(11,1)=W(1,0)	INPUT 804
1800.	GO TO 295	INPUT 805
1801.	PC(KK,K)=SC(KK,K)	INPUT 807
1802.	1,WRITE(11,1)=W(1,0)	INPUT 809
1803.	IF (KK(13)-1) 300,310,300	INPUT 810
1804.	IF (KK(13)-1) 305,310,310	INPUT 811
1805.	IF (PC(KK,1) + PC(KK,2) - 5) 310,320,310	INPUT 812
1806.	WRITE(11,1)=W(1,0)	INPUT 813
1807.	STOP	INPUT 814
1808.	IF (PC(KK,1)-1) 310,330,325	INPUT 815
1809.	WRITE(11,1)=W(1,0)	INPUT 817
1810.	PC(KK,1)=1,PC+10	INPUT 819
1811.	IF (KK(13)-1) 335,335,340	INPUT 821
1812.	IF (KK(13)-1) 340,340,340	INPUT 822
1813.	IF (KK(13)-1) 345,345,345	INPUT 823
1814.	IF (KK(13)-1) 350,350,350	INPUT 824
1815.	IF (KK(13)-1) 355,355,355	INPUT 825
1816.	IF (KK(13)-1) 360,360,360	INPUT 826
1817.	IF (KK(13)-1) 365,365,365	INPUT 827
1818.	IF (KK(13)-1) 370,370,370	INPUT 828
1819.	IF (KK(13)-1) 375,375,375	INPUT 829
1820.	IF (KK(13)-1) 380,380,380	INPUT 830
1821.	IF (KK(13)-1) 385,385,385	INPUT 831
1822.	IF (KK(13)-1) 390,390,390	INPUT 832
1823.	IF (KK(13)-1) 395,395,395	INPUT 833
1824.	IF (KK(13)-1) 400,400,400	INPUT 834
1825.	IF (KK(13)-1) 405,405,405	INPUT 835
1826.	IF (KK(13)-1) 410,410,410	INPUT 836
1827.	IF (KK(13)-1) 415,415,415	INPUT 837
1828.	IF (KK(13)-1) 420,420,420	INPUT 838
1829.	IF (KK(13)-1) 425,425,425	INPUT 839
1830.	IF (KK(13)-1) 430,430,430	INPUT 840
1831.	IF (KK(13)-1) 435,435,435	INPUT 841
1832.	IF (KK(13)-1) 440,440,440	INPUT 842
1833.	IF (KK(13)-1) 445,445,445	INPUT 843
1834.	IF (KK(13)-1) 450,450,450	INPUT 844
1835.	IF (KK(13)-1) 455,455,455	INPUT 845
1836.	IF (KK(13)-1) 460,460,460	INPUT 846
1837.	IF (KK(13)-1) 465,465,465	INPUT 847
1838.	IF (KK(13)-1) 470,470,470	INPUT 848
1839.	IF (KK(13)-1) 475,475,475	INPUT 849
1840.	IF (KK(13)-1) 480,480,480	INPUT 850
1841.	IF (KK(13)-1) 485,485,485	INPUT 851
1842.	IF (KK(13)-1) 490,490,490	INPUT 852
1843.	IF (KK(13)-1) 495,495,495	INPUT 853
1844.	IF (KK(13)-1) 500,500,500	INPUT 854
1845.	IF (KK(13)-1) 505,505,505	INPUT 855
1846.	IF (KK(13)-1) 510,510,510	INPUT 856
1847.	IF (KK(13)-1) 515,515,515	INPUT 857
1848.	IF (KK(13)-1) 520,520,520	INPUT 858
1849.	IF (KK(13)-1) 525,525,525	INPUT 859
1850.	IF (KK(13)-1) 530,530,530	INPUT 860
1851.	IF (KK(13)-1) 535,535,535	INPUT 861
1852.	IF (KK(13)-1) 540,540,540	INPUT 862
1853.	IF (KK(13)-1) 545,545,545	INPUT 863
1854.	IF (KK(13)-1) 550,550,550	INPUT 864
1855.	IF (KK(13)-1) 555,555,555	INPUT 86


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1. SUBROUTINE KINUT
2. DIMENSION XY(20),PRMU(10,50)
3.
4. REAL NFA(1),NFI(1),NFI(1),TAU(10,10)
5. EQUIVALENCE (NFI(1),A(1)), (NFI(1),A(1)), (NFI(1),A(1)),
6. 1(TAU(1),A(1))
7. DIMENSION TE(10),CIJ(10,1)
8. DIMENSION X(1),VLAM(10,1)
9.
10. COMMON
11. FMOA(10),FAOR(10),RA(10,2),RC(10,2),
12. M(10,2),RE(10,2),RE(10,2),TU(10,2),VN(10),
13. Y(10),WM(10),VM(10,10),FE(10),IFC(10),
14. IP(10),CP(10),H(10),SR(10),TC(10),VLIN(10),
15. E(10),LMT(10),GAMK(1,1)
16.
17. COMMON /PARA1/ KIN,KOUT,JAN,MOL,NAE,IOC,KXX(3),KR(10),TILE(3),
18. TIMO,TTNAX,VISC,PR(1)
19.
20. COMMON /PARA2/ W,SCH,PHO,VEL,RI,NFF,FFA,TS,ISP,P,T,SP,HIP,
21. EL,ENL,FLIO,M,DEL,ISFG,KVALP,CPE,IRE,IER,BA,ITS,
22. IM,IL,IT,MOFF,HRELT,SEL,T,TRAX,TRIM,MET,SCMB,
23. SUPL,JG,H6,CPG,SWA,SWR,SWC,SWD,SUMC,NXC,SAT,
24. VACH,KR2Z,SP1,GAN,THI,MX,FRCHT,HCH,NCV,TOT,
25. IERZ,FOAT,SP1,IXG,SVI,KKJ,TXC,NXG,SH1,NOATO,
26. SA2,FFEANS,PV,CNF,VA,HCS,CUMI,CUM2,FP,IFCJC,
27. ISD2,LTG,VF02,VTI
28.
29. COMMON /GAMAYS/ A(16,16),P(16),P(3),XC(50),XG(50),ZKE(10),
30. TLO(10),DELC(10),VALJP(10),FIR(10),ALP(10),
31. GAM(10),GAMF(10),T0(10,3),TK(10,3),WAT(10),
32. IP(10),ICAT(10),KAT(10),UN(10,10),FPL(10)
33.
34. COMMON /KINUT/ MT,EKE(50),EAK(50),EYK(50),PRU(10,50),RPU(10,50),
35. PRP(50),PKK(50)
36.
37. EQUIVALENCE (H(1),X(1)), (GAMK(1),VALP(1))
38.
39. COMMON /TEEFER/ TE(11),KAT(50),PKE(50),PKR(50),KAT(50),DUR(50),
40. LL(50),NA(50)
41.
42. COMMON /CCKIN/ PRP(10),ROUCC,ICC
43. COMMON /ZKIN/ PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),
44. *PRP(50),PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),PRP(10,50),
45. *PRP(10,50)
46.
47. 254 TEPR(10,50) 554,553,254
48. 331 KAT(10,50) 554,553,331
49.
50. 662 X(10,50) 554,553,662
51. 331 X(10,50) 554,553,331
52.
53. IF(TE(1),E,54) GO TO 504
54. PRP(10,50)
55. FKS(P)=0.0

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55. DO 602 J=1,3
56. I=PP(J,8)
57. PDX(N)=PDX(N)+DSI(J,8)*VU(1)
58. ISI=DSI(1,N)
59. IS2=DSI(2,N)
60. IF (ISI.GT.0) FKS(N)=FKS(N)+VU(1,8)*VU(1,8)
61. IF (IS2.GT.0) FKS(N)=FKS(N)+VU(2,8)*VU(2,8)
62. FKS(N)=1.0+FKS(N)
63. PDX(N)=1.0+PDX(N)
64. FAF(N)=XX(N)/PDX(N)+FKS(N)
65. GO TO 603
66. VI=VU(1,N)
67. VII=VU(2,N)
68. PFX(N)=1.0
69. FKS(N)=1.0
70. FAK(N)=PDX(N)+VII*VII-PDX(N)+VI*VI
71. FKF(N)=XX(N)/SQRT(PDX(N)+VII*VII)*35.167*EXP((PDX(N)+VII*VII)-K40(1,N)*
72. 1SR(1,1))/1.9869)
73. 603 CONTINUE
74. GO TO 10
75. 334 IF (P(9).EQ.3) GO TO 801
76. KR(9)=3
77. DO 802 M=1,NT
78. X0(M)=SEKE(M)
79. 801 DO 800 M=1,NT
80. IF (X0(M).EQ.1) GO TO 800
81. PDX(M)=PDX(M)+1
82. GO TO 800
83. 804 PDX(N)=0.0
84. GO 803 J=2,3
85. I=PP(J,8)
86. VI=VU(1,N)
87. PDX(N)=PDX(N)+DSI(J,8)*VU(1) +KK(J,8)*VU(1,1)
88. VII=VU(2,N)
89. I=PP(J,8)
90. PDX(N)=VU(1,1)+PDX(N)+FKS(1,N)*VU(1,1)
91. FKF(N)=XX(N)+VU(1,1)
92. IF (KR(9).EQ.3) GO TO 10
93. DO 11 M=1,NT
94. 11 PDX(N)=1.0
95. 10 RT=1.9869 * I
96. DO 40 N=1,NT
97. SUMC=0.
98. SUMK=0.
99. SUMW=0.
100. SUMP=0.
101. DO 15 IZ=1,4
102. IF (APS(RNN(IZ,8)),I,1,1,-6) GO TO 17
103. I=PP(IZ,8)
104. IF (IFC(I),F,8,-1,6,I,0,JC) GO TO 14
105. IF (IFC(I),F,8,0,0,JC,IFC(I),F,0,1) GO TO 14
106. 12 VU2=0.0
107. VU1=0.0
108. GO TO 35
109. 14 SUMC=SUMC+VU(IZ,8)*V(I)
110. 15 SUMI=VU(1)/NT+SUMC(1)/1.0069
111. SUMK=SUMK
SUMW=SUMW
SUMP=SUMP
-K40(1,7)*VU(1,1)

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K1NF0330
K1NF0340
K1NF0350
K1NF0360
K1NF0370
K1NF0380


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112.      SUMO=SUMO
113.      IF (A6S(PH(I2,M),I,T,1,F=5) GO TO 15
114.      IT=MP(I2,M)
115.      IF (IC(I1,M)=0.-1.000,11,IC,JC) GO TO 22
116.      IF (IC(I1,M)=1.000,12,IC,JC) GO TO 22
117.      SUMO=SUMO+P10(I2,M)*Y(I1)
118.      VLM1=H(I1)/H1+SR(I1)/1.9069
119.      SUMO=SUMO+VLM1*(I2,M)*H(I1)
120.      SUMO=SUMO+P10(I2,M)*H(I1)
121.      15 CONTINUE
122.      DO 16 I=1,J3
123.      PH(I1,M)=0.0
124.      DO 16 I2=1,M
125.      IT=MP(I2,M)
126.      VLMR=VLM(I1,I)
127.      IF (MP(I2,M)=1,IC,IS) GO TO 704
128.      VLMR=0.0
129.      IF (H(I2,M)=E0,1) VLMR=1.0
130.      IT=MP(I2,M)
131.      VLMR=VLM(I1,I)
132.      IF (MP(I2,M)=1,IC,IS) GO TO 16
133.      VLMR=0.0
134.      IF (MP(I2,M)=E0,1) VLMR=1.0
135.      PH(I1,M)=PH(I1,M)+VLMR*PH(I2,M)-VLMR*PH(I2,M)
136.      EQUILIBRIUM CONSTANTS FOR KINETIC REACTIONS IN TERMS OF HASE SPECIES
137.      LOG KP-S
138.      DERIVATIVES OF LOGS OF ABOVE KP-S WITH RESPECT TO LOG T
139.      DKPT(M) = SUMD / ST
140.      RIGHT HAND SIDE (OR REVERSE PART) OF DRIVING POTENTIAL
141.      VK1ALOG(AA*EXP(M))+EXP(M)*ALOG(T)-FAK(M)/PT
142.      PK(M)=EXP(LN(M)*(SUMO-SUMR+VLM1,M0,1))
143.      LEFT HAND SIDE (OR FORWARD PART) OF DRIVING POTENTIAL
144.      PK(M)=EXP(LN(M)*(SUMR+VLM1,M0,1))
145.      VK1 = PKR(M) - PKP(M)
146.      IF (VK1) 25,20,25
147.      VK1=1.F-9+SIGN(PKR(M),SUMR-SUMP+SUMV)
148.      25 CONTINUE
149.      PM TIMES FORWARD RATE OF REACTION 1 (PK=AA)
150.      PKR(M)=AA*VK1
151.      PKP(M)=AA*VK1
152.      PKR(M)=PKR(M)/PKP(M)
153.      RAT(M)=AA*VK1*(PKP(M)-PKR(M))
154.      IF (KR(7)-1) 40,40,36
155.      IF (M-1) 37,37,39
156.      37 WRITE(KOUT,38)
157.      38 FORMAT(2X1H7X3HLP6X6H1KZUL7X4HPP6X4HPP9X3HPP9X3HPP)
158.      39 WRITE(KOUT,41) P,SUMR,DKPT(M),PKR(M),PKP(M),RAT(M)
159.      40 M(M) = M
160.      41 FORMAT(13,2X,6E12,5)
161.      45 FORMAT(1X2H(I,J),I=1,8,J=1,8,1P,1P)
162.      50 FORMAT(1X12L10,3)
163.      55 FORMAT(1X2H(I,J),I=1,8,J=1,8,1P,1P)
164.      IF (KR(7) - 1) 60,60,65
165.      65 CONTINUE
166.      WRITE(KOUT,50) ((PPMU(I1,J),J=1,MT),I=1,IS)
167.      WRITE(KOUT,215)
168.

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226.  PRAD(J,N) = LUP1
227.  C*****ADJ CONTROLLING REACTION 1 TO ITS MASS BALANCE
228.  I1 = 1
229.  I2 = 1
230.  170 DO 175 J=1,15
231.  SUM=0.0
232.  DO 500 JJ=1,N
233.  I=PPF(JJ,N)
234.  V=VPE=VNU(I,J)
235.  IF(PPF(JJ,N).GT.15) GO TO 502
236.  V=VPP=0.
237.  IF(NPP(JJ,N).EQ.0) V=VPP=1.0
238.  I1 =NPF(JJ,N)
239.  V=VPE=VNU(I1,J)
240.  IF(NPF(JJ,N).GT.15) GO TO 503
241.  V=VPP=0.
242.  IF(NPF(JJ,N).EQ.0) V=VPE=1.0
243.  SUM=SUM+PPR(I1)*V
244.  100 I11 = PPR(JJ,N)/PPRS(N)*V=VPE
245.  GO CONTINUE
246.  DO 501 I2=1,4
247.  I11=NPP(I2,N)
248.  V=VPP=VNU(I11,J)
249.  IF(NPP(I2,N).GT.15) GO TO 504
250.  V=VKK=0.0
251.  IF(NPP(I2,N).EQ.0) V=VPP=1.0
252.  I11=NPP(I2,N)
253.  V=VPP=VNU(I11,J)
254.  IF(NPP(I2,N).GT.15) GO TO 505
255.  V=VPP=0.0
256.  IF(NPP(I2,N).EQ.0) V=VPP=1.0
257.  SUM=SUM+RPP(I2,N)*PPR(N)*V=VPP=VNU(I2,N)*PPR(N)*V=VPP
258.  GO CONTINUE
259.  175 I11=I1,I2
260.  I1 = I1 + 2*IJ + 2) = N(I1 + 2*IJ + 2) - SUM + PPR(I1,N)
261.  SUM=0.0
262.  SUM=0.0
263.  DO 506 JJ=1,N
264.  PPR=0.0
265.  I11=NPP(JJ,N)
266.  IF(NPP(JJ,N).GT.15)
267.  *PPR = PPR(I1)*V=V(I1)
268.  SUM=SUM+PPR(I11)
269.  SUM=SUM+PPR(I11)
270.  PPR=0.0
271.  I1=NPF(JJ,N)
272.  IF(NPF(JJ,N).GT.15)
273.  *PPR = PPR(I1)*V=V(I1)
274.  SUM=SUM+PPR(I1)
275.  SUM=SUM+PPR(I1)
276.  DO 507 I2=1,4
277.  PPR=0.0
278.  I11=NPP(I2,N)
279.  *PPR = PPR(I2,N)*V=V(I1)
280.  I11=NPP(I2,N)
281.  SUM=SUM+PPR(I11)
282.  SUM=SUM+PPR(I11)

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KINE1400
 KINE1410
 KINE1420
 KINE1430
 KINE1440

KINE1460
 KINE1470

2923.	NOI=0.0	*COR
2924.	IF (I-2) * (12.0) * (1.0)	*COR
2925.	* (I-2) * (12.0) * (1.0) * (1.0)	*COR
2926.	IF (I-2) * (12.0) * (1.0)	*COR
2927.	NOI=0.0	*COR
2928.	NOI=0.0	*COR
2929.	NOI=0.0	*COR
2930.	NOI=0.0	*COR
2931.	NOI=0.0	*COR
2932.	NOI=0.0	*COR
2933.	NOI=0.0	*COR
2934.	NOI=0.0	*COR
2935.	NOI=0.0	*COR
2936.	NOI=0.0	*COR
2937.	NOI=0.0	*COR
2938.	NOI=0.0	*COR
2939.	NOI=0.0	*COR
2940.	NOI=0.0	*COR
2941.	NOI=0.0	*COR
2942.	NOI=0.0	*COR
2943.	NOI=0.0	*COR
2944.	NOI=0.0	*COR
2945.	NOI=0.0	*COR
2946.	NOI=0.0	*COR
2947.	NOI=0.0	*COR
2948.	NOI=0.0	*COR
2949.	NOI=0.0	*COR
2950.	NOI=0.0	*COR
2951.	NOI=0.0	*COR
2952.	NOI=0.0	*COR
2953.	NOI=0.0	*COR
2954.	NOI=0.0	*COR
2955.	NOI=0.0	*COR
2956.	NOI=0.0	*COR
2957.	NOI=0.0	*COR
2958.	NOI=0.0	*COR
2959.	NOI=0.0	*COR
2960.	NOI=0.0	*COR
2961.	NOI=0.0	*COR
2962.	NOI=0.0	*COR
2963.	NOI=0.0	*COR
2964.	NOI=0.0	*COR
2965.	NOI=0.0	*COR
2966.	NOI=0.0	*COR
2967.	NOI=0.0	*COR
2968.	NOI=0.0	*COR
2969.	NOI=0.0	*COR
2970.	NOI=0.0	*COR
2971.	NOI=0.0	*COR
2972.	NOI=0.0	*COR
2973.	NOI=0.0	*COR
2974.	NOI=0.0	*COR
2975.	NOI=0.0	*COR
2976.	NOI=0.0	*COR
2977.	NOI=0.0	*COR
2978.	NOI=0.0	*COR
2979.	NOI=0.0	*COR
2980.	NOI=0.0	*COR
2981.	NOI=0.0	*COR
2982.	NOI=0.0	*COR
2983.	NOI=0.0	*COR
2984.	NOI=0.0	*COR
2985.	NOI=0.0	*COR
2986.	NOI=0.0	*COR
2987.	NOI=0.0	*COR
2988.	NOI=0.0	*COR
2989.	NOI=0.0	*COR
2990.	NOI=0.0	*COR
2991.	NOI=0.0	*COR
2992.	NOI=0.0	*COR
2993.	NOI=0.0	*COR
2994.	NOI=0.0	*COR
2995.	NOI=0.0	*COR
2996.	NOI=0.0	*COR
2997.	NOI=0.0	*COR
2998.	NOI=0.0	*COR
2999.	NOI=0.0	*COR
3000.	NOI=0.0	*COR


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1. SUPROUTINE OUTPI
2. DIMENSION IO(25)
3. DIMENSION SPIE(10,10)
4.
5. C
6. REAL NFIA(1),NFIE(1),FFIN(1),TAU(10,10)
7. EQUIVALENCE (NFIA(1),A(1)), (NFIE(1),A(51)), (FFIN(1),A(101)),
8. 1(TAU(1),A(151))
9. DIMENSION TF(180),CIJ(180,1)
10. DIMENSION X(1),VLAM(180,1)
11. C
12. COMMON
13. FARMOR(180),FARMOR(180),RH(180,2),RC(180,2),
14. RN(180,2),RE(180,2),RE(180,2),TU(180,2),VN(180),
15. Y(180),YTR(180),VNU(180,10),FF(180),IFC(180),
16. IP(180),CPI(180),H(180),SB(180),TC(180),VLNK(180),
17. E(180),LAMI(180),GANK(1,1)
18. C
19. COMMON /PARAM1/ KJH,KOUT,JAN,MUL,NAP,IOC,N,KXX(3),KR(10),TILE(3),
20. TTRIN,TMAX,VISC,PR(1)
21. C
22. COMMON /PARAM2/ WM,SCH,RHU,VEL,H1,MFF,FFA,IS,ISP,P,T,SP,HIP,
23. EL,EML,FLTO,NG,IEL,ISQ,KRALP,CPF,IRE,IFR,AA,ITS,
24. IN,IL,IT,MODE,HMELT,SMELT,TMAX,THIN,MELT,SUMN,
25. SUML,JC,HG,CPG,SVA,SVC,SVD,SUMC,NXC,SAI,
26. VMACH,KRZZ,SP1,GAM,THI,MX,DRCNT,HCH,NCV,INT,
27. IFRZ,MOAT,SP1,XIG,SVI,KRQ,IXC,HXG,SHI,MOATO,
28. SAP,FFF,WS,RV,CMF,VA,HOS,DUM1,DUM2,FP,IFC,IC,
29. ISP2,WTG,VHU2,WTL
30. C
31. COMMON /APRAYS/ A(16,16),R(16),W(3),XC(50),XG(50),ZKE(10),
32. TI(10),DMPLO(10),WALJP(10),FR(10),ALP(10),
33. GASH(10),GAMF(10),TO(10,3),TK(10,3),WAT(10),
34. JP(10),TOAT(10),KAT(10),DE(10,10),PHL(10)
35. EQUIVALENCE (TU(180),TF(1)), (VNU(1),CIJ(1))
36. C
37. COMMON /XNETX/ MT,PRF(50),FAK(50),FXK(50),PRU(10,50),RHU(10,50),
38. PRP(50),PKK(50)
39. C
40. EQUIVALENCE (R(1),X(1)), (GANK(1),VLAM(1))
41. C
42. COMMON/ACI1/GAMEY,PEEN,PCH,ACHSO,SGMAK,SXP
43. C
44. COMMON /UTEEF/ IR(11),FRU(10),PRUS(10),SLAM(10),PF(10),RY(10),
45. JRC(10),JUL(10),SLR(16),SLA(16,16)
46. C
47. COMMON/CARKIN/ KKK(10),POUCH,NCC
48. DATA (SPIC(1,1),I=1,9)/44LATE,44R-OR,44HIFT,44FD P,44YEQI,44HYTC,
49. 44H GRA,44HUIT,44PE /
50. DATA (SPIC(2,1),I=1,9)/44ERGE,44F-DEI,44HEWTE,44HO PY,44HROLY,44HTIC ,
51. 44HCRAP,44HJIC,44H /
52. DATA (SPIC(3,1),I=1,9)/44HRLK,44H GHA,44HPII,44HE 44H 44H ,
53. 44H 44H 44H /
54. DATA (SPIC(4,1),I=1,9)/44G-90,44H 44H 44H 44H ,
55. 44H 44H 44H /
56. DATA (SPIC(5,1),I=1,9)/44ATJ 44HCRAP,44HFTF,44H 44H 44H ,

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112.  H1=HL+VM*(C*(T)+FLIC+VVELT
113.  SL=SL+VM*(C*FLT)+FLIC+VVELT
114.  H1P=(H1+H1C)/AA
115.  STP=(SL+SLC)/AA
116.  H1=K*(1)-TFR2+KRF
117.  FAFSGAN=EX
118.  IF (KR(4)) 60,50,55
119.  HTL=H1C/AA
120.  FAF=0.
121.  WSG=APAX1*(WS-W(3)+PPON,1,F-30)
122.  H1P=(H1C*(H1-VTH+H1C)/WSD)/AA
123.  STP=0.
124.  H1C=H1C*(1+1.5146)
125.  H1C=H1C*(1+1.5146)
126.  H1C=H1C*(1+1.5146)
127.  H1=H1/WT*1.8
128.  SL=SL/WT*1.8
129.  SG=SG/WT*1.8
130.  H1C=H1C*(1.8)
131.  WSG=WTG/P
132.  WML=WTL/SP
133.  IF (KR(6)) 65,70,70
134.  WRITE (KOUT,355) WTR
135.  WRITE (KOUT,360) T1,T,P
136.  GO TO 100
137.  WRITE (KOUT,435)
138.  NSPIE = KKK(4)
139.  WRITE (KOUT,415) (SPIE(NSPIE,I),I=1,9)
140.  WRITE (KOUT,430) HOUTP
141.  WRITE (KOUT,410) RV,PPRF
142.  WRITE (KOUT,440) T1,T,P
143.  WRITE (KOUT,365) H1C,H1,HRP,SG,SL,SJP,RRHG,RHO,WMG,WML,W
144.  IF (KKJ) 105,110,110
145.  VELSQ=(SV1*SI(SA1))*2.+(SR1/RHO)*SV1*Cos(SA1))
146.  1*2.1/45054.
147.  SA2=(ATAN(RHO/SR1*TAN(SA1)))*57.29577
148.  SP1=SA1*57.29577
149.  SH1=SH1*1.8
150.  SOMAK=VELSQ/GAM*WM/(1.9469*T)
151.  VMACH=ASQRT(SOMAK)
152.  VEL=ASQRT(VELSQ*45054.)
153.  FLUX=VEL*FV
154.  WRITE (KOUT,380) VEL,VMACH,SA2
155.  HRH=HCH*1.8
156.  WRITE (KOUT,385) SV1,SH1,PRH,SP1,SR1,SO1
157.  SH1=SH1/1.8
158.  GO TO 140
159.  IF (KR(5)-1) 115,130,125
160.  IF (KR(5)) 120,140,140
161.  WRITE (KOUT,395)
162.  HRH=HCH*1.8
163.  SO1=SA1*57.29577
164.  SH1=SH1*1.8
165.  WRITE (KOUT,400) SV1,SR1,HRH,SP1,SR1,SO1
166.  GO TO 140
167.  HCH=HIP
168.  SCH=SHIP

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[illegible]


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226.      WRITE (KOUT,460) (I,PERIL(I),I=1,N)
227.      WRITE (KOUT,462) (I,PKKK(I),I=1,NT)
228.      462 FORMAT(6HP RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PPG
229.      462
230.      205 IF (KR(1)) 215,220,210
231.      210 WRITE (KOUT,450)
232.      60 TO 240
233.      215 IF (KR(5)) 230,220,220
234.      220 IF (KR(4)) 235,225,235
235.      225 WRITE (KOUT,370)
236.      60 TO 240
237.      230 WRITE (KOUT,405)
238.      60 TO 240
239.      235 WRITE (KOUT,390)
240.      60 TO 255 I=1,N
241.      IF (IFC(I)-1) 255,245,255
242.      245 IF (KR(6)) 255,250,250
243.      250 V(I)=UN(I)/QK(I)*I
244.      255 V(I)=V(I)/P
245.      IF (ICV) 260,260,260
246.      260 IF (KR(7)-1) 265,265,260
247.      265 IF (I-E0) 270,270,275
248.      270 WRITE (KOUT,505) (FAMCA(I),FAMOB(I),V(I),I=1,N)
249.      60 TO 265
250.      275 WRITE (KOUT,510) (FAMCA(I),FAMOB(I),V(I),I=1,N)
251.      60 TO 265
252.      240 WRITE (KOUT,465) (FAMCA(I),FAMOB(I),V(I),IC(I),Y(I),VLPK(I),IFC(I),OUTP235
253.      1),F(I),CE(I),I=1,N)
254.      285 10 300 I=1,N
255.      IF (IFC(I)-1) 300,290,300
256.      290 IF (KR(6)) 300,295,295
257.      295 V(I)=V(I)/VTE(I)*W
258.      300 V(I)=V(I)*P
259.      305 IF (FLT(I)) 315,315,310
260.      FSOL=1.-FLT
261.      WRITE (KOUT,455) FAMOB(I),FAMOB(I),FAMOB(I),FLIO,FSOL
262.      315 IF (ITS) 320,345,345
263.      320 IF (KR(5)) 325,340,325
264.      325 IF (KR(4)*P(I)) 335,335,335
265.      330 K(I)=1
266.      K(I)=4
267.      K(I)=7
268.      K(2)=1
269.      V(I)=X
270.      ACOS=0.
271.      ITS=0
272.      GASE=GAZ/(CAP - 1.)
273.      C      TEST CURVES OF STAGNATION PRESSURE PERFORM SUCCESS
274.      271 G = ( (GAS - 1.) / 2.) * (SOMER) * * GASE)*P
275.      CALL ETIE
276.      335 STOP
277.      340 RETURN
278.      345 HRES=1P
279.      STESS=1P
280.      280.      RETURN
281.      C      350 FORMAT (13HP SOLUTION TYPES,10X,13HP ITERATIONS = ,14,23,7HP I=1,NF = OUTP265
282.      282.

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340.
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1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54.
SUBROUTINE THERK
  DIMENSION PLNK(50), RC(30)
  REAL NFIA(1), NFIB(1), FEETM(1), TAU(10,10)
  EQUIVALENCE (NFIA(1),A(1)), (NFIB(1),A(51)), (FEETM(1),A(101)),
    1(TAU(1),A(151))
  DIMENSION TFI(180), CIJ(180,1)
  DIMENSION X(1), VLAM(180,1)
  DIMENSION FRAM(10,50)
  COMMON /PARAM1/ FARM(180), R3(180,2), RC(180,2),
    1 RC(180,2), RE(150,2), RF(180,2), TU(180,2), VP(180),
    2 Y(180), VTM(180), VNU(10,3), FF(180), IFF(180),
    3 IP(180), CP(180), H(180), SB(180), TC(180), VLAM(180),
    4 E(180), LAMI(180), GAPK(1,1)
  COMMON /PARAM2/ KTH(KOUT, JAM, 4UL, VAR, TFC, N, KFX(3), KR(10), TILF(3),
    1 TTMIN, TTMAX, VISC, PR(1)
  COMMON /PARAM3/ W3, SCF, PHU, VFL(81), MFC, FFA, T3, TSP, P, T, SIF, MTP,
    1 EL, ENL, FLI, 10, 10, IEL, ISQ, KVALP, CPE, TRF, TER, AA, ITS,
    2 IM, IL, IT, MOFF, IMELT, IMAX, TMIN, MELT, SUMN,
    3 SPRL, JC, HG, CP, G, SVA, SVS, SVC, SVD, SUPRC, NXC, SAI,
    4 VMACH, KRZ, SPI, SAB, THT, FX, DUCHI, HCH, NCV, TPT,
    5 IFRZ, NOAT, SK1, IXG, SVI, KXJ, IAC, IXG, SHI, NGATO,
    6 SLP, FFF, XS, RV, CFE, VAA, HOS, HUP1, DUM2, EP, TEC, JC,
    7 ISP2, WTG, VNU2, WTL
  COMMON /APPAYS/ A(16,16), R(16), W(3), XC(50), XC(50), ZKE(10),
    1 TLO(10), DMCLC(10), CALJP(10), FH(10), ALP(10),
    2 GAMH(10), GAMF(10), STC(10,3), TK(10,3), VAT(10),
    3 IR(10), IOAT(10), KAT(10), MU(10,10), FUL(10)
  EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))
  COMMON /KINETX/ MT, FKE(50), FAK(50), FVW(50), PRU(10,50), PRU(10,50),
    1 PWP(50), PKKK(50)
  EQUIVALENCE (R(1),X(1)), (GAPK(1),V(1),A(1))
  COMMON /REFERR/ IR(11), PRU(10), PRUS(10), SLAM(10), RF(10), FY(10),
    1 IRC(10), JJJ(10), SLB(16), SLA(16,16)
  COMMON /ZKTH/ PRU(10,50), PRF(10,50), MFC(10,50), MFE(10,50), FKKK(50),
    1 PRX(50), PSJ(10,50), FKK(10,50), IMP(50)
  COMMON /CAKTH/ PRK(10), ROUCM, MCC
  REAL ITHR
  DIMENSION FRED(3,10), FAKD(3,10), FXK(3,10), PSIG(8,3,10), FKKP(8,3,1)
  *0, RYSP(8,4), PRSP(8,4), THHR(6), PCIS(8), FSS(2)
  DATA (RXSP(1,1), I=1,4)/4H20, 4HC*, 4H /, (RYSP(2,1), I=1
    1, 4)/4HC2, 4HC*, 4H /, (RXSP(3,1), I=1,4)/4H2, 4HC*, 4H
    2, 4H /, (RXSP(4,1), I=1,4)/4HC*, 4H /, (RYSP(5,1), I=1,4)/4HC*
    3, 4H /, (RYSP(6,1), I=1,4)/4HC*, 4H /, (RYSP(7,1), I=1,4)/4HC*, 4H
    4, 4H /, (RYSP(8,1), I=1,4)/4HC*, 4H /, (RYSP(9,1), I=1,4)/4HC*, 4H
    5, 4H /, (RYSP(10,1), I=1,4)/4HC*, 4H /, (RYSP(11,1), I=1,4)/4HC*, 4H
    6, 4H /, (RYSP(12,1), I=1,4)/4HC*, 4H /, (RYSP(13,1), I=1,4)/4HC*, 4H
    7, 4H /, (RYSP(14,1), I=1,4)/4HC*, 4H /, (RYSP(15,1), I=1,4)/4HC*, 4H
    8, 4H /, (RYSP(16,1), I=1,4)/4HC*, 4H /, (RYSP(17,1), I=1,4)/4HC*, 4H
    9, 4H /, (RYSP(18,1), I=1,4)/4HC*, 4H /, (RYSP(19,1), I=1,4)/4HC*, 4H
    10, 4H /, (RYSP(20,1), I=1,4)/4HC*, 4H /, (RYSP(21,1), I=1,4)/4HC*, 4H
    11, 4H /, (RYSP(22,1), I=1,4)/4HC*, 4H /, (RYSP(23,1), I=1,4)/4HC*, 4H
    12, 4H /, (RYSP(24,1), I=1,4)/4HC*, 4H /, (RYSP(25,1), I=1,4)/4HC*, 4H
    13, 4H /, (RYSP(26,1), I=1,4)/4HC*, 4H /, (RYSP(27,1), I=1,4)/4HC*, 4H
    14, 4H /, (RYSP(28,1), I=1,4)/4HC*, 4H /, (RYSP(29,1), I=1,4)/4HC*, 4H
    15, 4H /, (RYSP(30,1), I=1,4)/4HC*, 4H /, (RYSP(31,1), I=1,4)/4HC*, 4H
    16, 4H /, (RYSP(32,1), I=1,4)/4HC*, 4H /, (RYSP(33,1), I=1,4)/4HC*, 4H
    17, 4H /, (RYSP(34,1), I=1,4)/4HC*, 4H /, (RYSP(35,1), I=1,4)/4HC*, 4H
    18, 4H /, (RYSP(36,1), I=1,4)/4HC*, 4H /, (RYSP(37,1), I=1,4)/4HC*, 4H
    19, 4H /, (RYSP(38,1), I=1,4)/4HC*, 4H /, (RYSP(39,1), I=1,4)/4HC*, 4H
    20, 4H /, (RYSP(40,1), I=1,4)/4HC*, 4H /, (RYSP(41,1), I=1,4)/4HC*, 4H
    21, 4H /, (RYSP(42,1), I=1,4)/4HC*, 4H /, (RYSP(43,1), I=1,4)/4HC*, 4H
    22, 4H /, (RYSP(44,1), I=1,4)/4HC*, 4H /, (RYSP(45,1), I=1,4)/4HC*, 4H
    23, 4H /, (RYSP(46,1), I=1,4)/4HC*, 4H /, (RYSP(47,1), I=1,4)/4HC*, 4H
    24, 4H /, (RYSP(48,1), I=1,4)/4HC*, 4H /, (RYSP(49,1), I=1,4)/4HC*, 4H
    25, 4H /, (RYSP(50,1), I=1,4)/4HC*, 4H /, (RYSP(51,1), I=1,4)/4HC*, 4H
    26, 4H /, (RYSP(52,1), I=1,4)/4HC*, 4H /, (RYSP(53,1), I=1,4)/4HC*, 4H
    27, 4H /, (RYSP(54,1), I=1,4)/4HC*, 4H /, (RYSP(55,1), I=1,4)/4HC*, 4H
    28, 4H /, (RYSP(56,1), I=1,4)/4HC*, 4H /, (RYSP(57,1), I=1,4)/4HC*, 4H
    29, 4H /, (RYSP(58,1), I=1,4)/4HC*, 4H /, (RYSP(59,1), I=1,4)/4HC*, 4H
    30, 4H /, (RYSP(60,1), I=1,4)/4HC*, 4H /, (RYSP(61,1), I=1,4)/4HC*, 4H
    31, 4H /, (RYSP(62,1), I=1,4)/4HC*, 4H /, (RYSP(63,1), I=1,4)/4HC*, 4H
    32, 4H /, (RYSP(64,1), I=1,4)/4HC*, 4H /, (RYSP(65,1), I=1,4)/4HC*, 4H
    33, 4H /, (RYSP(66,1), I=1,4)/4HC*, 4H /, (RYSP(67,1), I=1,4)/4HC*, 4H
    34, 4H /, (RYSP(68,1), I=1,4)/4HC*, 4H /, (RYSP(69,1), I=1,4)/4HC*, 4H
    35, 4H /, (RYSP(70,1), I=1,4)/4HC*, 4H /, (RYSP(71,1), I=1,4)/4HC*, 4H
    36, 4H /, (RYSP(72,1), I=1,4)/4HC*, 4H /, (RYSP(73,1), I=1,4)/4HC*, 4H
    37, 4H /, (RYSP(74,1), I=1,4)/4HC*, 4H /, (RYSP(75,1), I=1,4)/4HC*, 4H
    38, 4H /, (RYSP(76,1), I=1,4)/4HC*, 4H /, (RYSP(77,1), I=1,4)/4HC*, 4H
    39, 4H /, (RYSP(78,1), I=1,4)/4HC*, 4H /, (RYSP(79,1), I=1,4)/4HC*, 4H
    40, 4H /, (RYSP(80,1), I=1,4)/4HC*, 4H /, (RYSP(81,1), I=1,4)/4HC*, 4H
    41, 4H /, (RYSP(82,1), I=1,4)/4HC*, 4H /, (RYSP(83,1), I=1,4)/4HC*, 4H
    42, 4H /, (RYSP(84,1), I=1,4)/4HC*, 4H /, (RYSP(85,1), I=1,4)/4HC*, 4H
    43, 4H /, (RYSP(86,1), I=1,4)/4HC*, 4H /, (RYSP(87,1), I=1,4)/4HC*, 4H
    44, 4H /, (RYSP(88,1), I=1,4)/4HC*, 4H /, (RYSP(89,1), I=1,4)/4HC*, 4H
    45, 4H /, (RYSP(90,1), I=1,4)/4HC*, 4H /, (RYSP(91,1), I=1,4)/4HC*, 4H
    46, 4H /, (RYSP(92,1), I=1,4)/4HC*, 4H /, (RYSP(93,1), I=1,4)/4HC*, 4H
    47, 4H /, (RYSP(94,1), I=1,4)/4HC*, 4H /, (RYSP(95,1), I=1,4)/4HC*, 4H
    48, 4H /, (RYSP(96,1), I=1,4)/4HC*, 4H /, (RYSP(97,1), I=1,4)/4HC*, 4H
    49, 4H /, (RYSP(98,1), I=1,4)/4HC*, 4H /, (RYSP(99,1), I=1,4)/4HC*, 4H
    50, 4H /, (RYSP(100,1), I=1,4)/4HC*, 4H /, (RYSP(101,1), I=1,4)/4HC*, 4H
    51, 4H /, (RYSP(102,1), I=1,4)/4HC*, 4H /, (RYSP(103,1), I=1,4)/4HC*, 4H
    52, 4H /, (RYSP(104,1), I=1,4)/4HC*, 4H /, (RYSP(105,1), I=1,4)/4HC*, 4H
    53, 4H /, (RYSP(106,1), I=1,4)/4HC*, 4H /, (RYSP(107,1), I=1,4)/4HC*, 4H
    54, 4H /, (RYSP(108,1), I=1,4)/4HC*, 4H /, (RYSP(109,1), I=1,4)/4HC*, 4H
    55, 4H /, (RYSP(110,1), I=1,4)/4HC*, 4H /, (RYSP(111,1), I=1,4)/4HC*, 4H
    56, 4H /, (RYSP(112,1), I=1,4)/4HC*, 4H /, (RYSP(113,1), I=1,4)/4HC*, 4H
    57, 4H /, (RYSP(114,1), I=1,4)/4HC*, 4H /, (RYSP(115,1), I=1,4)/4HC*, 4H
    58, 4H /, (RYSP(116,1), I=1,4)/4HC*, 4H /, (RYSP(117,1), I=1,4)/4HC*, 4H
    59, 4H /, (RYSP(118,1), I=1,4)/4HC*, 4H /, (RYSP(119,1), I=1,4)/4HC*, 4H
    60, 4H /, (RYSP(120,1), I=1,4)/4HC*, 4H /, (RYSP(121,1), I=1,4)/4HC*, 4H
    61, 4H /, (RYSP(122,1), I=1,4)/4HC*, 4H /, (RYSP(123,1), I=1,4)/4HC*, 4H
    62, 4H /, (RYSP(124,1), I=1,4)/4HC*, 4H /, (RYSP(125,1), I=1,4)/4HC*, 4H
    63, 4H /, (RYSP(126,1), I=1,4)/4HC*, 4H /, (RYSP(127,1), I=1,4)/4HC*, 4H
    64, 4H /, (RYSP(128,1), I=1,4)/4HC*, 4H /, (RYSP(129,1), I=1,4)/4HC*, 4H
    65, 4H /, (RYSP(130,1), I=1,4)/4HC*, 4H /, (RYSP(131,1), I=1,4)/4HC*, 4H
    66, 4H /, (RYSP(132,1), I=1,4)/4HC*, 4H /, (RYSP(133,1), I=1,4)/4HC*, 4H
    67, 4H /, (RYSP(134,1), I=1,4)/4HC*, 4H /, (RYSP(135,1), I=1,4)/4HC*, 4H
    68, 4H /, (RYSP(136,1), I=1,4)/4HC*, 4H /, (RYSP(137,1), I=1,4)/4HC*, 4H
    69, 4H /, (RYSP(138,1), I=1,4)/4HC*, 4H /, (RYSP(139,1), I=1,4)/4HC*, 4H
    70, 4H /, (RYSP(140,1), I=1,4)/4HC*, 4H /, (RYSP(141,1), I=1,4)/4HC*, 4H
    71, 4H /, (RYSP(142,1), I=1,4)/4HC*, 4H /, (RYSP(143,1), I=1,4)/4HC*, 4H
    72, 4H /, (RYSP(144,1), I=1,4)/4HC*, 4H /, (RYSP(145,1), I=1,4)/4HC*, 4H
    73, 4H /, (RYSP(146,1), I=1,4)/4HC*, 4H /, (RYSP(147,1), I=1,4)/4HC*, 4H
    74, 4H /, (RYSP(148,1), I=1,4)/4HC*, 4H /, (RYSP(149,1), I=1,4)/4HC*, 4H
    75, 4H /, (RYSP(150,1), I=1,4)/4HC*, 4H /, (RYSP(151,1), I=1,4)/4HC*, 4H
    76, 4H /, (RYSP(152,1), I=1,4)/4HC*, 4H /, (RYSP(153,1), I=1,4)/4HC*, 4H
    77, 4H /, (RYSP(154,1), I=1,4)/4HC*, 4H /, (RYSP(155,1), I=1,4)/4HC*, 4H
    78, 4H /, (RYSP(156,1), I=1,4)/4HC*, 4H /, (RYSP(157,1), I=1,4)/4HC*, 4H
    79, 4H /, (RYSP(158,1), I=1,4)/4HC*, 4H /, (RYSP(159,1), I=1,4)/4HC*, 4H
    80, 4H /, (RYSP(160,1), I=1,4)/4HC*, 4H /, (RYSP(161,1), I=1,4)/4HC*, 4H
    81, 4H /, (RYSP(162,1), I=1,4)/4HC*, 4H /, (RYSP(163,1), I=1,4)/4HC*, 4H
    82, 4H /, (RYSP(164,1), I=1,4)/4HC*, 4H /, (RYSP(165,1), I=1,4)/4HC*, 4H
    83, 4H /, (RYSP(166,1), I=1,4)/4HC*, 4H /, (RYSP(167,1), I=1,4)/4HC*, 4H
    84, 4H /, (RYSP(168,1), I=1,4)/4HC*, 4H /, (RYSP(169,1), I=1,4)/4HC*, 4H
    85, 4H /, (RYSP(170,1), I=1,4)/4HC*, 4H /, (RYSP(171,1), I=1,4)/4HC*, 4H
    86, 4H /, (RYSP(172,1), I=1,4)/4HC*, 4H /, (RYSP(173,1), I=1,4)/4HC*, 4H
    87, 4H /, (RYSP(174,1), I=1,4)/4HC*, 4H /, (RYSP(175,1), I=1,4)/4HC*, 4H
    88, 4H /, (RYSP(176,1), I=1,4)/4HC*, 4H /, (RYSP(177,1), I=1,4)/4HC*, 4H
    89, 4H /, (RYSP(178,1), I=1,4)/4HC*, 4H /, (RYSP(179,1), I=1,4)/4HC*, 4H
    90, 4H /, (RYSP(180,1), I=1,4)/4HC*, 4H /, (RYSP(181,1), I=1,4)/4HC*, 4H
    91, 4H /, (RYSP(182,1), I=1,4)/4HC*, 4H /, (RYSP(183,1), I=1,4)/4HC*, 4H
    92, 4H /, (RYSP(184,1), I=1,4)/4HC*, 4H /, (RYSP(185,1), I=1,4)/4HC*, 4H
    93, 4H /, (RYSP(186,1), I=1,4)/4HC*, 4H /, (RYSP(187,1), I=1,4)/4HC*, 4H
    94, 4H /, (RYSP(188,1), I=1,4)/4HC*, 4H /, (RYSP(189,1), I=1,4)/4HC*, 4H
    95, 4H /, (RYSP(190,1), I=1,4)/4HC*, 4H /, (RYSP(191,1), I=1,4)/4HC*, 4H
    96, 4H /, (RYSP(192,1), I=1,4)/4HC*, 4H /, (RYSP(193,1), I=1,4)/4HC*, 4H
    97, 4H /, (RYSP(194,1), I=1,4)/4HC*, 4H /, (RYSP(195,1), I=1,4)/4HC*, 4H
    98, 4H /, (RYSP(196,1), I=1,4)/4HC*, 4H /, (RYSP(197,1), I=1,4)/4HC*, 4H
    99, 4H /, (RYSP(198,1), I=1,4)/4HC*, 4H /, (RYSP(199,1), I=1,4)/4HC*, 4H
    100, 4H /, (RYSP(200,1), I=1,4)/4HC*, 4H /, (RYSP(201,1), I=1,4)/4HC*, 4H
    101, 4H /, (RYSP(202,1), I=1,4)/4HC*, 4H /, (RYSP(203,1), I=1,4)/4HC*, 4H
    102, 4H /, (RYSP(204,1), I=1,4)/4HC*, 4H /, (RYSP(205,1), I=1,4)/4HC*, 4H
    103, 4H /, (RYSP(206,1), I=1,4)/4HC*, 4H /, (RYSP(207,1), I=1,4)/4HC*, 4H
    104, 4H /, (RYSP(208,1), I=1,4)/4HC*, 4H /, (RYSP(209,1), I=1,4)/4HC*, 4H
    105, 4H /, (RYSP(210,1), I=1,4)/4HC*, 4H /, (RYSP(211,1), I=1,4)/4HC*, 4H
    106, 4H /, (RYSP(212,1), I=1,4)/4HC*, 4H /, (RYSP(213,1), I=1,4)/4HC*, 4H
    107, 4H /, (RYSP(214,1), I=1,4)/4HC*, 4H /, (RYSP(215,1), I=1,4)/4HC*, 4H
    108, 4H /, (RYSP(216,1), I=1,4)/4HC*, 4H /, (RYSP(217,1), I=1,4)/4HC*, 4H
    109, 4H /, (RYSP(218,1), I=1,4)/4HC*, 4H /, (RYSP(219,1), I=1,4)/4HC*, 4H
    110, 4H /, (RYSP(220,1), I=1,4)/4HC*, 4H /, (RYSP(221,1), I=1,4)/4HC*, 4H
    111, 4H /, (RYSP(222,1), I=1,4)/4HC*, 4H /, (RYSP(223,1), I=1,4)/4HC*, 4H
    112, 4H /, (RYSP(224,1), I=1,4)/4HC*, 4H /, (RYSP(225,1), I=1,4)/4HC*, 4H
    113, 4H /, (RYSP(226,1), I=1,4)/4HC*, 4H /, (RYSP(227,1), I=1,4)/4HC*, 4H
    114, 4H /, (RYSP(228,1), I=1,4)/4HC*, 4H /, (RYSP(229,1), I=1,4)/4HC*, 4H
    115, 4H /, (RYSP(230,1), I=1,4)/4HC*, 4H /, (RYSP(231,1), I=1,4)/4HC*, 4H
    116, 4H /, (RYSP(232,1), I=1,4)/4HC*, 4H /, (RYSP(233,1), I=1,4)/4HC*, 4H
    117, 4H /, (RYSP(234,1), I=1,4)/4HC*, 4H /, (RYSP(235,1), I=1,4)/4HC*, 4H
    118, 4H /, (RYSP(236,1), I=1,4)/4HC*, 4H /, (RYSP(237,1), I=1,4)/4HC*, 4H
    119, 4H /, (RYSP(238,1), I=1,4)/4HC*, 4H /, (RYSP(239,1), I=1,4)/4HC*, 4H
    120, 4H /, (RYSP(240,1), I=1,4)/4HC*, 4H /, (RYSP(241,1), I=1,4)/4HC*, 4H
    121, 4H /, (RYSP(242,1), I=1,4)/4HC*, 4H /, (RYSP(243,1), I=1,4)/4HC*, 4H
    122, 4H /, (RYSP(244,1), I=1,4)/4HC*, 4H /, (RYSP(245,1), I=1,4)/4HC*, 4H
    123, 4H /, (RYSP(246,1), I=1,4)/4HC*, 4H /, (RYSP(247,1), I=1,4)/4HC*, 4H
    124, 4H /, (RYSP(248,1), I=1,4)/4HC*, 4H /, (RYSP(249,1), I=1,4)/4HC*, 4H
    125, 4H /, (RYSP(250,1), I=1,4)/4HC*, 4H /, (RYSP(251,1), I=1,4)/4HC*, 4H
    126, 4H /, (RYSP(252,1), I=1,4)/4HC*, 4H /, (RYSP(253,1), I=1,4)/4HC*, 4H
    127, 4H /, (RYSP(254,1), I=1,4)/4HC*, 4H /, (RYSP(255,1), I=1,4)/4HC*, 4H
    128, 4H /, (RYSP(256,1), I=1,4)/4HC*, 4H /, (RYSP(257,1), I=1,4)/4HC*, 4H
    129, 4H /, (RYSP(258,1), I=1,4)/4HC*, 4H /, (RYSP(259,1), I=1,4)/4HC*, 4H
    130, 4H /, (RYSP(260,1), I=1,4)/4HC*, 4H /, (RYSP(261,1), I=1,4)/4HC*, 4H
    131, 4H /, (RYSP(262,1), I=1,4)/4HC*, 4H /, (RYSP(263,1), I=1,4)/4HC*, 4H
    132, 4H /, (RYSP(264,1), I=1,4)/4HC*, 4H /, (RYSP(265,1), I=1,4)/4HC*, 4H
    133, 4H /, (RYSP(266,1), I=1,4)/4HC*, 4H /, (RYSP(267,1), I=1,4)/4HC*, 4H
    134, 4H /, (RYSP(268,1), I=1,4)/4HC*, 4H /, (RYSP(269,1), I=1,4)/4HC*, 4H
    135, 4H /, (RYSP(270,1), I=1,4)/4HC*, 4H /, (RYSP(271,1), I=1,4)/4HC*, 4H
    136, 4H /, (RYSP(272,1), I=1,4)/4HC*, 4H /, (RYSP(273,1), I=1,4)/4HC*, 4H
    137, 4H /, (RYSP(274,1), I=1,4)/4HC*, 4H /, (RYSP(275,1), I=1,4)/4HC*, 4H
    138, 4H /, (RYSP(276,1), I=1,4)/4HC*, 4H /, (RYSP(277,1), I=1,4)/4HC*, 4H
    139, 4H /, (RYSP(278,1), I=1,4)/4HC*, 4H /, (RYSP(279,1), I=1,4)/4HC*, 4H
    140, 4H /, (RYSP(280,1), I=1,4)/4HC*, 4H /, (RYSP(281,1), I=1,4)/4HC*, 4H
    141, 4H /, (RYSP(282,1), I=1,4)/4HC*, 4H /, (RYSP(283,1), I=1,4)/4HC*, 4H
    142, 4H /, (RYSP(284,1), I=1,4)/4HC*, 4H /, (RYSP(285,1), I=1,4)/4HC*, 4H
    143, 4H /, (RYSP(286,1), I=1,4)/4HC*, 4H /, (RYSP(287,1), I=1,4)/4HC*, 4H
    144, 4H /, (RYSP(288,1), I=1,4)/4HC*, 4H /, (RYSP(289,1), I=1,4)/4HC*, 4H
    145, 4H /, (RYSP(290,1), I=1,4)/4HC*, 4H /, (RYSP(291,1), I=1,4)/4HC*, 4H
    146, 4H /, (RYSP(292,1), I=1,4)/4HC*, 4H /, (RYSP(293,1), I=1,4)/4HC*, 4H
    147, 4H /, (RYSP(294,1), I=1,4)/4HC*, 4H /, (RYSP(295,1), I=1,4)/4HC*, 4H
    148, 4H /, (RYSP(296,1), I=1,4)/4HC*, 4H /, (RYSP(297,1), I=1,4)/4HC*, 4H
    149, 4H /, (RYSP(298,1), I=1,4)/4HC*, 4H /, (RYSP(299,1), I=1,4)/4HC*, 4H
    150, 4H /, (RYSP(300,1), I=1,4)/4HC*, 4H /, (RYSP(301,1), I=1,4)/4HC*, 4H
    151, 4H /, (RYSP(302,1), I=1,4)/4HC*, 4H /, (RYSP(303,1), I=1,4)/4HC*, 4H
    152, 4H /, (RYSP(304,1), I=1,4)/4HC*, 4H /, (RYSP(305,1), I=1,4)/4HC*, 4H
    153, 4H /, (RYSP(306,1), I=1,4)/4HC*, 4H /, (RYSP(307,1), I=1,4)/4HC*, 4H
    154, 4H /, (RYSP(308,1), I=1,4)/4HC*, 4H /, (RYSP(309,1), I=1,4)/4HC*, 4H
    155, 4H /, (RYSP(310,1), I=1,4)/4HC*, 4H /, (RYSP(311,1), I=1,4)/4HC*, 4H
    156, 4H /, (RYSP(312,1), I=1,4)/4HC*, 4H /, (RYSP(313,1), I=1,4)/4HC*, 4H
    157, 4H /, (RYSP(314,1), I=1,4)/4HC*, 4H /, (RYSP(315,1), I=1,4)/4HC*, 4H
    158, 4H /, (RYSP(316,1), I=1,4)/4HC*, 4H /, (RYSP(317,1), I=1,4)/4HC*, 4H
    159, 4H /, (RYSP(318,1), I=1,4)/4HC*, 4H /, (RYSP(319,1), I=1,4)/4HC*, 4H
    160, 4H /, (RYSP(320,1), I=1,4)/4HC*, 4H /, (RYSP(321,1), I=1,4)/4HC*, 4H
    161, 4H /, (RYSP(322,1), I=1,4)/4HC*, 4H /, (RYSP(323,1), I=1,4)/4HC*, 4H
    162, 4H /, (RYSP(324,1), I=1,4)/4HC*, 4H /, (RYSP(325,1), I=1,4)/4HC*, 4H
    163, 4H /, (RYSP(326,1), I=1,4)/4HC*, 4H /, (RYSP(327,1), I=1,4)/4HC*, 4H
    164, 4H /, (RYSP(328,1), I=1,4)/4HC*, 4H /, (RYSP(329,1), I=1,4)/4HC*, 4H
    165, 4H /, (RYSP(330,1), I=1,4)/4HC*, 4H /, (RYSP(331,1), I=1,4)/4HC*, 4H
    166, 4H /, (RYSP(332,1), I=1,4)/4HC*, 4H /, (RYSP(333,1), I=1,4)/4HC*, 4H
    167, 4H /, (RYSP(334,1), I=1,4)/4HC*, 4H /, (RYSP(335,1), I=1,4)/4HC*, 4H
    168, 4H /, (RYSP(336,1), I=1,4)/4HC*, 4H /, (RYSP(337,1), I=1,4)/4HC*, 4H
    169, 4H /, (RYSP(338,1), I=1,4)/4HC*, 4H /, (RYSP(339,1), I=1,4)/4HC*, 4H
    170, 4H /, (RYSP(340,1), I=1,4)/4HC*, 4H /, (RYSP(341,1), I=1,4)/4HC*, 4H
    171, 4H /, (RYSP(342,1), I=1,4)/4HC*, 4H /, (RYSP(343,1), I=1,4)/4HC*, 4H
    172, 4H /, (RYSP(344,1), I=1,4)/4HC*, 4H /, (RYSP(345,1), I=1,4)/4HC*, 4H
    173, 4H /, (RYSP(346,1), I=1,4)/4HC*, 4H /, (RYSP(347,1), I=1,4)/4HC*, 4H
    174, 4H /, (RYSP(348,1), I=1,4)/4HC*, 4H /, (RYSP(349,1), I=1,4)/4HC*, 4H
    175, 4H /, (RYSP(350,1), I=1,4)/4HC*, 4H /, (RYSP(351,1), I=1,4)/4HC*, 4H
    176, 4H /, (RYSP(352,1), I=1,4)/4HC*, 4H /, (RYSP(353,1), I=1,4)/4HC*, 4H
    177, 4H /, (RYSP(354,1), I=1,4)/4HC*, 4H /, (RYSP(355,1), I=1,4)/4HC*, 4H
    178, 4H /, (RYSP(356,1), I=1,4)/4HC*, 4H /, (RYSP(357,1), I=1,4)/4HC*, 4H
    179, 4H /, (RYSP(358,1), I=1,4)/4HC*, 4H /, (RYSP(359,1), I=1,4)/4HC*, 4H
    180, 4H /, (RYSP(360,1), I=1,4)/4HC*, 4H /, (RYSP(361,1), I=1,4)/4HC*, 4H
    181, 4H /, (RYSP(362,1), I=1,4)/4HC*, 4H /, (RYSP(363,1), I=1,4)/4HC*, 4H
    182, 4H /, (RYSP(364,1), I=1,4)/4HC*, 4H /, (RYSP(365,1), I=1,4)/4HC*, 4H
    183, 4H /, (RYSP(366,1), I=1,4)/4HC*, 4H /, (RYSP(367,1), I=1,4)/4HC*, 4H
    184, 4H /, (RYSP(368,1), I=1,4)/4HC*, 4H /, (RYSP(369,1), I=1,4)/4HC*, 4H
    185, 4H /, (RYSP(370,1), I=1,4)/4HC*, 4H /, (RYSP(371,1), I=1,4)/4HC*, 4H
    186, 4H /, (RYSP(372,1), I=1,4)/4HC*, 4H /, (RYSP(373,1), I=1,4)/4HC*, 4H
    187, 4H /, (RYSP(374,1), I=1,4)/4HC*, 4H /, (RYSP(375,1), I=1,4)/4HC*, 4H
    188, 4H /, (RYSP(376,1), I=1,4)/4HC*, 4H /, (RYSP(377,1), I=1,4)/4HC*, 4H
    189, 4H /, (RYSP(378,1), I=1,4)/4HC*, 4H /, (RYSP(379,1), I=1,4)/4HC*, 4H
    190, 4H /, (RYSP(380,1), I=1,4)/4HC*, 4H /, (RYSP(381,1), I=1,4)/4HC*, 4H
    191, 4H /, (RYSP(382,1), I=1,4)/4HC*, 4H /, (RYSP(383,1), I=1,4)/4HC*, 4H
    192, 4H /, (RYSP(384,1), I=1,4)/4HC*, 4H /, (RYSP(385,1), I=1,4)/4HC*, 4H
   
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55. DATA (PRSP(1,1),I=1,4)/4HC0 ,4H ,4H /,(PRSP(2,1),I=1
56. * ,4)/4HC0 ,4H ,4H ,4H /,(PRSP(3,1),I=1,4)/4HC2,4H ,4
57. * ,4H /,(PRSP(4,1),I=1,4)/4HC ,4H ,4H ,4H /,(PRSP
58. * (5,1),I=1,4)/4HC2 ,4H ,4H ,4H /,(PRSP(6,1),I=1,4)/4HC3
59. * ,4H ,4H ,4H /,(PRSP(7,1),I=1,4)/4HC4 ,4H ,4H ,4H
60. * /,(PRSP(8,1),I=1,4)/4HC5 ,4H ,4H ,4H /
61. DATA (TINP(1,1),I=1,8)/4H20 ,4HC02 ,4HC6 ,4H2 ,4HCLH ,4H2H ,4H
62. * ,4H /
63. DATA (POIS(1,1),I=1,8)/4HCLH ,4H2H ,4H ,4H ,4H ,4H
64. * ,4H /
65. DATA (FSS(1,1),I=1,5)/,125.,.261.,.012.,.130.,.00956/
66. DATA (FKFN(1,1),I=1,3)/12.,5,12.,5,0.,771/,(FKFN(1,1),I=1,3)/,65.,4.,
67. * ,4.,6.,5.,4.,5.,5.,5.,4.,/(FKFN(1,1),I=1,3)/0.,0.,0.,0.,0.,0.,/(FKFN(1,2),I=1,3)/
68. * ,2.,63724E+3.,3.,434485E+6.,5.,136124E+5.,/(FKFN(1,2),I=1,3)/,61910.,5.,
69. * ,69431.,3.,124440./,(FKFN(1,2),I=1,3)/0.,0.,0.,0.,0.,0.,/(FKFN(1,3),I
70. * ,=1,3)/1.,90E+5.,1.,59E+5.,4.,94E+7.,/(FKFN(1,3),I=1,3)/,6.,55E+4.,6.,55E+4.,
71. * ,1295E+5.,/(FKFN(1,3),I=1,3)/0.,0.,0.,0.,0.,0.,/(FKFN(1,4),I=1,3)/,0346A.,
72. * ,0015.,1.,5133.,/(FKFN(1,4),I=1,3)/,4175.,34.,4175.,34.,57175.,49.,/(FKFN(1,
73. * ,4),I=1,3)/,29.,29.,29.,29.,0.,0.,/(FKFN(1,5),I=1,3)/,74.,3.,493.,19610.,44.,/(F
74. * ,K0(1,5),I=1,3)/,451.,4.,451.,4.,110500.,0.,/(FKFN(1,5),I=1,3)/0.,0.,0.,0.,
75. * ,0.,/(FKFN(1,6),I=1,3)/,478.,14.,478.,14.,776.,017.,/(FKFN(1,6),I=1,3)/,3430A.,2
76. * ,3430B.,2.,34883.,6.,/(FKFN(1,6),I=1,3)/,617.,617.,0.,0.,/(FKFN(1,7),I=1,
77. * ,31/6.,89064E+5.,1.,31779E+7.,4.,41603E+4.,/(FKFN(1,7),I=1,3)/,101676.,95.,1
78. * ,01676.,95.,117282.,75.,/(FKFN(1,7),I=1,3)/,483.,833.,0.,0./
79. DATA (FKFN(1,8),I=1,3)/11.,0901.,208.,87.,0.,70045.,/(FKFN(1,8),I=1,3)/
80. * ,29386.,7.,29346.,7.,50640.,4.,/(FKFN(1,8),I=1,3)/0.,0.,0.,0.,0.,0./
81. DATA (PSIN(1,1),I=1,8)/1.,0.,1.,0.,1.,0.,1.,0.,1.,0.,0.,0.,0.,0.,0.,0.,0./
82. * ,2,1),I=1,8)/1.,0.,1.,0.,1.,0.,1.,0.,0.,0.,0.,0.,0.,0.,0.,0.,/(PSIN(1,3),I=1,8)/
83. * ,1.,0.,1.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,/(PSIN(1,2),I=1,8)/,151.32,26.05,
84. * ,216.,0.,93.,1145.,0.,0.,0.,0.,0.,0.,/(PSIN(1,2,2),I=1,8)/,46.,75.,166.,49,
85. * ,29.,87.,0.,1325.,44.,0.,0.,0.,0.,0.,0.,/(PSIN(1,3,2),I=1,8)/0.,0.,0.,0.,55A.,
86. * ,0.,0.,0.,53.,355.,0.,0.,0.,/(PSIN(1,1,3),I=1,8)/1.,0.,1.,0.,1.,0.,1.,0.,0.,0.,
87. * ,0.,0.,0.,0.,0.,/(PSIN(1,2,3),I=1,8)/1.,0.,1.,0.,1.,0.,1.,0.,0.,0.,0.,0.,0.,0./
88. DATA (PSIN(1,3,3),I=1,6)/1.,0.,1.,0.,1.,0.,1.,0.,0.,0.,0.,0.,0.,0.,0.,0./
89. * ,SID(1,2,4),I=1,8)/,0331.,.064.,.021.,.0058.,1.,0.,0.,0.,0.,0.,0.,/(PSIN(1,5),I=1
90. * ,4),I=1,8)/,0058.,.0058.,.0058.,.0058.,.0058.,.0058.,.0058.,.0058.,/(PSIN(1,2,5),I=1,8)
91. * ,/163.,87.,399.,3.,166.,5.,13.,12.,100.,0.,0.,0.,0.,0.,0.,/(PSIN(1,3,5),I=1,8)/0.,
92. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,/(PSIN(1,1,6),I=1,8)/,16.,61.,42.,25.,75
93. * ,69.,21.,8.,.1.,0.,0.,0.,0.,0.,0.,/(PSIN(1,2,6),I=1,8)/,16.,61.,42.,25.,75.,69.,21
94. * ,8.,.1.,0.,0.,0.,0.,0.,0.,/(PSIN(1,3,6),I=1,8)/0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
95. * ,8.,.1.,0.,0.,0.,0.,0.,0.,/(PSIN(1,1,3,6),I=1,8)/,0001.,0.,0.,0.,0.,0.,0.,0.,0.,
96. * ,0.,0.,/(PSIN(1,1,7),I=1,8)/,252.,67.,5018.,31.,054.,.0001.,0.,0.,0.,0.,0.,0.,0.,
97. * ,0.,/(PSIN(1,2,7),I=1,8)/,252.,67.,5018.,31.,054.,.0001.,0.,0.,0.,0.,0.,0.,0.,0.,
98. * ,SID(1,3,7),I=1,8)/,53.,681.,18.,786.,.059.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
99. DATA (PSIN(1,1,8),I=1,8)/,29.,41.,373.,6A.,0.,0.,1.,72.,.01.,2500.,0.,0.,0.,0.,0.,
100. * ,/(PSIN(1,2,8),I=1,8)/,88.,38.,20.,19.,13.,69.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
101. * ,/(PSIN(1,3,8),I=1,8)/,3.,0.,3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
102. DATA (FKKN(1,1),I=1,8)/3.,0.,3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
103. * ,2,1),I=1,8)/3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
104. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
105. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
106. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
107. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
108. * ,/(FKKN(1,1,3),I=1,8)/,3.,0.,3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
109. * ,I=1,8)/3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
110. * ,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
111. DATA BLK/4H

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112. 5      MOVE=MM(1)
113.      IF (ITS) 50,10,50
114.      *16=0.
115.      *11=0.
116.      IF (K(R)) 40,40,15
117.      IF (IFC(N+1)-1) 25,20,25
118.      IF (1+.001-IF(N+1)) 25,25,30
119.      IFC(N+1)=-1
120.      VM(N+1)=0.
121.      DO 35 K=1,TS
122.      VM(N+1,K)=-TC(K,3)
123.      *11=-VM(N+1)
124.      *12=0.
125.      SUMA=0.
126.      DO 45 J=1,IS
127.      PROS(J)=0.
128.      SLAR(J)=0.
129.      *11=0.
130.      FLIQ=0.
131.      *11=0.
132.      *11=1
133.      *11=TIME
134.      *11=TIME
135.      *11=TIME
136.      *11=TIME
137.      *11=TIME
138.      *11=TIME
139.      *11=TIME
140.      *11=TIME
141.      *11=TIME
142.      *11=TIME
143.      *11=TIME
144.      *11=TIME
145.      *11=TIME
146.      *11=TIME
147.      *11=TIME
148.      *11=TIME
149.      *11=TIME
150.      *11=TIME
151.      *11=TIME
152.      *11=TIME
153.      *11=TIME
154.      *11=TIME
155.      *11=TIME
156.      *11=TIME
157.      *11=TIME
158.      *11=TIME
159.      *11=TIME
160.      *11=TIME
161.      *11=TIME
162.      *11=TIME
163.      *11=TIME
164.      *11=TIME
165.      *11=TIME
166.      *11=TIME
167.      *11=TIME
168.      *11=TIME

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THER0053
THER0054
THER0055
THER0056
THER0057
THER0058
THER0059
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THER0095
THER0096
THER0097
THER0098
THER0099
THER0100
THER0101
THER0102
THER0103
THER0104
THER0105
THER0106
THER0107
THER0108
THER0109

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165. GO TO 185
170. 36 125 K=1,IS
171. 6001=9001,60)*A(1)
172. IF (K=6) 125,120,125
173. 300(K)=S(A*(K)+0.01/EF(1)
174. 6005(6)=9005(6)+0.001
175. IF (K=6) 165,165,136
176. 30 125 K=1,IS
177. 300(K)=S(A*(K)+0.01/EF(1)
178. IF (K=6) 125,120,125
179. 6005(6)=9005(6)+0.001
180. IF (K=6) 165,165,136
181. IF (K=6) 125,120,125
182. IF (K=6) 165,165,136
183. IF (K=6) 125,120,125
184. IF (K=6) 165,165,136
185. IF (K=6) 125,120,125
186. IF (K=6) 165,165,136
187. IF (K=6) 125,120,125
188. IF (K=6) 165,165,136
189. IF (K=6) 125,120,125
190. IF (K=6) 165,165,136
191. IF (K=6) 125,120,125
192. IF (K=6) 165,165,136
193. IF (K=6) 125,120,125
194. IF (K=6) 165,165,136
195. IF (K=6) 125,120,125
196. IF (K=6) 165,165,136
197. IF (K=6) 125,120,125
198. IF (K=6) 165,165,136
199. IF (K=6) 125,120,125
200. IF (K=6) 165,165,136
201. IF (K=6) 125,120,125
202. IF (K=6) 165,165,136
203. IF (K=6) 125,120,125
204. IF (K=6) 165,165,136
205. IF (K=6) 125,120,125
206. IF (K=6) 165,165,136
207. IF (K=6) 125,120,125
208. IF (K=6) 165,165,136
209. IF (K=6) 125,120,125
210. IF (K=6) 165,165,136
211. IF (K=6) 125,120,125
212. IF (K=6) 165,165,136
213. IF (K=6) 125,120,125
214. IF (K=6) 165,165,136
215. IF (K=6) 125,120,125
216. IF (K=6) 165,165,136
217. IF (K=6) 125,120,125
218. IF (K=6) 165,165,136
219. IF (K=6) 125,120,125
220. IF (K=6) 165,165,136
221. IF (K=6) 125,120,125
222. IF (K=6) 165,165,136
223. IF (K=6) 125,120,125
224. IF (K=6) 165,165,136
225. IF (K=6) 125,120,125

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226. 315 AZ=P*1"
227. HCV=0
228. SURC=ROUIC
229. TAF=0
230. NUT=0
231. MS = 5
232. IF (KRR(9)-5) 335,411,411
233. 411 DO 607 N=1,A
234. DO 608 IZ=1,4
235. 608 IZ,M)=0.0
236. 408 IZ,M)=6.0
237. NRR(IZ,M)=1
238. 603 NRR(IZ,M)=1
239. DO 607 IZ=1,8
240. NPP(IZ,M)=1
241. PSI(IZ,M)=0.0
242. FKR(IZ,M)=0.0
243. FNAK(1,IZ,M)=ELLK
244. FNAK(1,IZ,M)=ELLK
245. 607 NPP(IZ,M)=1
246. 603 FOPFAT(8X,2A4,32H)SPECIES NOT FOUND IN THERMO DATA)
247. IF (KRR(81-4) 413,414,414
248. 414 I1=1
249. MR=3
250. IRY=1
251. C*****H2O+C==CO+H2*****
252. RMU(1,I1)=1.0
253. KRU(2,I1)=1.0
254. PFI(1,I1)=1.0
255. PMU(2,I1)=1.0
256. I1=2
257. GO TO 421
258. 413 IF (KPR(81-2) 416,415,416
259. 415 I1=1
260. MR=3
261. IPX=2
262. C*****CO2+C==2CO*****
263. 421 RMU(1,I1)=1.0
264. RMU(2,I1)=1.0
265. PMU(1,I1)=2.0
266. IF (MR .EQ. 1) GO TO 417
267. I1=3
268. GO TO 422
269. 416 I1=1
270. MR=1
271. IPX=3
272. C*****H2+2C==C2H2*****
273. 422 RMU(1,I1)=1.0
274. RMU(2,I1)=2.0
275. PMU(1,I1)=1.0
276. 417 DO 418 I=1,MS
277. SURC=FLOAT(I)
278. RMU(1,I+MR)=SUFC
279. 418 PMU(1,I+MR)=1.0
280. MT=MR+MS
281. NICK=KRR(4)
282. IF (KRR(71) 701,702,701

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THERM16R

[illegible]


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1. SURROUTINE KININ
2. DIMENSION KRA(10,33),WRA(3,33),7A(33),PRA(33),TFA(3),TS(15)
3.
4. C
5. REAL A(1),MEI(1),FFIN(1),TAU(10,10)
6. EQUIVALENCE (TFA(1),A(1)), (MEI(1),A(51)), (FFIN(1),A(101)),
7. 1(TAU(1),A(151))
8. DIMENSION TE(100),CIJ(100,3)
9. DIMENSION X(1),VLAM(100,1)
10.
11. C
12. COMMON
13. 1 FANOA(100),FANOE(100),RA(100,2),RC(100,2),
14. 2 RC(100,2),PE(100,2),FF(100,2),TU(100,2),VF(100),
15. 3 Y(100),WTN(100),VNU(100,10),EF(100),IFC(100),
16. 4 IP(100),CP(100),H(100),SK(100),TC(100),VLWK(100),
17. 5 E(100),LAMI(100),GARK(1,1)
18.
19. C
20. COMMON /PARAM1/ KINAKOUT,JGR,FOL,PAR,IOC,M,KFX(3),PR(10),TILE(3),
21. 1 TMIN,TMAX,VISC,PR(1)
22.
23. C
24. COMMON /PARAM2/ WM,SCH,RHO,VEL,N1,FF,FFA,TS,ISP,P,T,SIP,MJP,
25. 1 FL,EMI,FLIO,NQ,IFL,ISQ,KPALP,CPF,INF,TF,AA,TTS,
26. 2 IN,IL,IT,MCEE,HMELT,SELT,TMAX,TMIN,MELT,SUMN,
27. 3 SUP,LJC,HG,CPG,SVA,SVH,SVC,SVD,SUMC,MXC,SAI,
28. 4 VMACH,KRZ,SPJ,GAM,THI,MX,DACHI,HCH,MCV,TBT,
29. 5 IFRZ,FOAT,SP1,IXG,SVI,KKJ,IXC,IXG,SM1,NOATO,
30. 6 SAP,FEFF,WS,RV,CDF,VA,HOS,RUP,1,DUM2,EP,IFCJC,
31. 7 ISP2,ATG,VNU2,WL
32.
33. C
34. COMMON /ARRAYS/ # (16,16),B(16),N(3),XC(50),XG(50),ZKE(10),
35. 1 YLO(10),CMCLO(10),WALJP(10),EB(10),ALP(10),
36. 2 GAM,H(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
37. 3 IR(10),IOAT(10),KAT(10),UN(10,10),EPL(10)
38. EQUIVALENCE (TU(101),TF(1)), (VNU(1),CIJ(1))
39.
40. C
41. COMMON /KINETX/ NT,PKF(50),EAK(50),FKK(50),PMU(10,50),PMU(10,50),
42. 1 PMR(50),PKKK(50)
43.
44. C
45. EQUIVALENCE (B(1),X(1)), (GARK(1),VLAM(1))
46.
47. C
48. COMMON/CAPKIN/ KKK(10),ROUCH,NCC
49. COMMON/CONCRD/ Z,GARF,VR(3)
50. COMMON/STCPG/ PERCT,STPFR,CPEF
51. DATA (TFA(1),I=1, 8)/500.,1000.,1500.,2000.,2500.,3000.,3500.,
52. 14000./
53. DATA (TSA(1),I=1,15)/1200.,1400.,1600.,1800.,2000.,2200.,2400.,
54. 12600.,2600.,3000.,3200.,3400.,3600.,3800.,4000./
55. DATA KTF,KTS/R,15/
56. NCC=NCC+1
57.
58. 5 IF (NCC-1) 315,10,315
59.
60. 10 HEAD (KIN,360) KKK(2,PR,ZE,PC,POUCH,GARF,TILE
61. IF (KKK(1)-8) 20,15,20
62.
63. 15 KR(1)=8
64. GO TO 355
65.
66. 20 IF (KKK(4) .LT. 8) GO TO 33
67. READ(KIN,32) PERCT

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KIN10001
KIN10002
KIN10003
KIN10004
KIN10005
KIN10006
KIN10007
KIN10008
KIN10009
KIN10010
KIN10011
KIN10012
KIN10013
KIN10014
KIN10015
KIN10016
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KIN10041
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KIN10043
KIN10044
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KIN10046
KIN10047
KIN10048
KIN10049
KIN10050
KIN10051

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55. 32 FOR CAT(510,0)
56. STPR=700000000
57. CPER=1.-STPR
58. IF (KPK(5)-2) 40,25,40
59. 25 KTF=0
60. 30 KTF=KTF+1
61. KTF (KIN,355) TFA(KTF)
62. IF (TFA(KTF)) 50,55,30
63. KTF=KTF+1
64. IF (KPK(5)-2) 60,45,60
65. KTS=0
66. 30 KTS=KTS+1
67. KTF (KIN,355) TSA(KTS)
68. IF (TSA(KTS)) 50,55,50
69. KTS=KTS+1
70. KTF(7)=KPK(10)
71. KTF(4)=KPK(5)-1
72. KTF(6)=0
73. IF (KPK(9)) 70,65,70
74. KTF(10)=0
75. 60 TO 75
76. KTF(10)=1
77. IF (KPK(8)) 85,60,65
78. KTF(3,1)=1
79. 60 TO 90
80. KTF(3,1)=KPK(4)
81. KTF(3,1)=0
82. KTF(3,1)=1
83. IF (KPK(5)-4) 100,95,100
84. KTF(3)=0
85. KTF(3,1)=1
86. KTF(3,1)=1
87. 60 TO 115
88. IF (KPK(5)-4) 115,105,110
89. KTF(3)=0
90. 60 TO 115
91. KTF(3,1)=KPK(2)
92. KTF(3,1)=1
93. KTF(4,1)=0
94. KTF(4,1)=0
95. KTF(4,1)=0
96. KTF(4,1)=0
97. 60 TO 120
98. KTF(4,1)=KPK(6)
99. KTF(4,1)=KPK(7)
100. KTF(4,1)=KPK(8)
101. KTF(4,1)=KPK(9)
102. KTF(4,1)=KPK(10)
103. KTF(4,1)=KPK(11)
104. KTF(4,1)=KPK(12)
105. KTF(4,1)=KPK(13)
106. KTF(4,1)=KPK(14)
107. KTF(4,1)=KPK(15)
108. KTF(4,1)=KPK(16)
109. KTF(4,1)=KPK(17)
110. KTF(4,1)=KPK(18)
111. 60 TO 215

112.	140	IF (KRR(1)-2) 145,145,170	KINI0117	*COR
113.	145	KRA(5,1)=0	KINI0118	*-12
114.		KRA(1,2)=0	KINI0119	
115.		KRA(2,2)=0	KINI0120	
116.		KRA(3,2)=0	KINI0121	
117.		KRA(4,2)=0	KINI0122	
118.		KRA(5,2)=0	KINI0123	
119.		KRA(9,2)=0	KINI0124	
120.		ZA(2)=0.0	KINI0125	
121.		KRA(2)=0.0	KINI0126	
122.		IF (KRR(1)-2) 155,150,155	KINI0127	
123.	150	KRA(5,2)=5	KINI0128	
124.	155	ICT=2		
125.		GO TO 215	KINI0141	
126.	170	IF (KRR(1)-3) 150,175,190	KINI0142	
127.	175	KRA(5,1)=2	KINI0143	
128.		KRA(1,2)=3	KINI0144	
129.		KRA(2,2)=0	KINI0145	
130.		KRA(3,2)=0	KINI0146	
131.		KRA(4,2)=0	KINI0147	
132.		KRA(5,2)=1	KINI0148	
133.		KRA(9,2)=0	KINI0149	
134.		ZA(2)=0.0	KINI0150	
135.		KRA(2)=2E	KINI0151	
136.		ICT=2		
137.		GO TO 215	KINI0164	*COR
138.	190	KRA(5,1)=2	KINI0165	*-12
139.		KRA(1,2)=3	KINI0166	
140.		KRA(2,2)=0	KINI0167	
141.		KRA(3,2)=0	KINI0168	
142.		KRA(4,2)=0	KINI0169	
143.		KRA(5,2)=1	KINI0170	
144.		KRA(9,2)=0	KINI0171	
145.		ZA(2)=0.0	KINI0172	
146.		KRA(2)=2E	KINI0173	
147.		KRA(1,3)=4	KINI0174	
148.		KRA(2,3)=0	KINI0175	
149.		KRA(3,2)=0	KINI0176	
150.		KRA(4,3)=0	KINI0177	
151.		KRA(5,3)=0	KINI0178	
152.		KRA(9,3)=0	KINI0179	
153.		ZA(2)=0.0	KINI0180	
154.		KRA(3)=0.0	KINI0181	
155.	195	IF (KRR(1)-5) 200,195,200	KINI0182	
156.	200	KRA(5,3)=3	KINI0183	
157.	205	ICT=3		
158.		GO 220 1=1,ICT	KINI0196	*COR
159.	220	KRA(10,1)=0	KINI0197	*-12
160.		IF (KRR(5)) 225,235,225	KINI0198	
161.	225	ICT=ICT+1	KINI0199	
162.		ICT=ICT+KTF	KINI0200	
163.		GO 230 1=0,ICT,ICT	KINI0201	
164.		KRA(1,1)=0	KINI0202	
165.		KRA(2,1)=0	KINI0203	
166.		KRA(3,1)=0	KINI0204	
167.		KRA(4,1)=0	KINI0205	
168.		KRA(5,1)=0	KINI0206	

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169. KRA(9,I)=0
170. ZAT(1)=TFA(T-UCT)
171. PRA(1)=0.0
172. CONTINUE
173. KRA(3,NC1)=KPKSS
174. NC1=NC12+1
175. NC14=NC12+K15
176. GO TO 240
177. NC13=NC1+1
178. NC14=NC1+K15
179. IF (KRA(6)) 245,240,245
180. NC15=NC13+1
181. DO 250 I=NC13,NC15
182. KPA(1,I)=0
183. KRA(2,I)=0
184. KRA(3,I)=0
185. KPA(4,I)=0
186. KRA(5,I)=0
187. KRA(9,I)=0
188. ZAT(1)=500.0
189. PRA(1)=0.0
190. KPA(2,I)=1.0F-19
191. CONTINUE
192. IF (KRA(5)) 260,245,260
193. KPA(3,NC13)=KPKSS
194. KPA(4,NC15)=2
195. ZAT(NC15)=1000.0
196. NC13=NC13+2
197. NC14=NC14+2
198. DO 275 I=NC13,NC16
199. KRA(1,I)=0
200. KRA(2,I)=0
201. KPA(3,I)=0
202. KPA(4,I)=2
203. KPA(5,I)=0
204. ZAT(1)=TSA(T-F(C13+1))
205. PRA(1)=0.0
206. IF (KRA(8)-1) 265,265,270
207. KRA(9,I)=0
208. GO TO 275
209. KRA(9,I)=4
210. CONTINUE
211. IF (KRA(8)-1) 285,285,280
212. KRA(9,NC14)=6
213. NC13=NC14+1
214. CONTINUE
215. IF (PC) 285,215,295
216. DO 305 I=1,NC13
217. KPA(3,I)=1
218. DO 300 J=1,10
219. KPA(4,J)=KPA(4,J)-1
220. ZAT(1)=ZAT(1)-1
221. PRA(8)=PRA(8)-1
222. KPA(1,I)=KPA(1,I)-1
223. KPA(2,I)=KPA(2,I)-1
224. KPA(5,I)=KPA(5,I)-1
225. DO 310 I=1,10

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KIN10207
KIN10208
KIN10209
KIN10210
KIN10211
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KIN10219
KIN10220
KIN10221
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KIN10229
KIN10230
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KIN10232
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KIN10256
KIN10257
KIN10258
KIN10259
KIN10260
KIN10261
KIN10262
KIN10263

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226. KRA(1,1)=KRA(1,2)
227. KRA(1,2)=2
228. KRA(2,2)=0
229. KRA(3,2)=0
230. ZA(2)=0.0
231. KRA(5,1)=0
232. ZA(1)=7
233. PRA(1)=PC
234. NCT3=CT3+1
235. IF (NCT3-UCT3) 325,320,320
236. NCC=0
237. GO TO 5
238. NO 330 I=1,10
239. KRA(1)=KRA(1,NCC)
240. CONTINUE
241. Z=ZA(NCC)
242. PF=PR(NCC)
243. PRA(1)=KRA(1,NCC)
244. KRA(2)=KRA(2,NCC)
245. KRA(3)=KRA(3,NCC)
246. IF (KRA(4)) 355,355,335
247. DO 345 I=1,PF,N
248. IF ((IFC(1)/3)*delta-IFC(1)) 340,345,340
249. NS=I-1
250. GO TO 350
251. CONTINUE
252. GO TO 355
253. VN(NS+1)=VN(NS+1)
254. TFC(NS+1)=TFC(NS+1)
255. TFC(NS+1)=TFC(NS+1)
256. VTC(NS+1)=VTC(NS+1)
257. FARGO(NS+1)=FARGO(NS+1)
258. FARGO(NS+1)=FARGO(NS+1)
259. N=NS
260. RETURN
261. C
262. FORMAT (J0I1,6F10.5,2A4,A2)
263. FORMAT (F10.5)
264. END

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KIN10264
KIN10265
KIN10266
KIN10267
KIN10268
KIN10269
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KIN10271
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KIN10275
KIN10276
KIN10277
KIN10278
KIN10279
KIN10280
KIN10281
KIN10282
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KIN10290
KIN10291
KIN10292
KIN10293
KIN10294
KIN10295
KIN10296
KIN10297
KIN10298
KIN10299
KIN10300
KIN10301
KIN10302

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1. C SUBROUTINE ZTIME
2.
3. REAL NELA(1),NEIR(1),FEIN(1),TAU(10,10)
4. EQUIVALENCE (NELA(1),A(1)), (FEIN(1),A(5)), (FEIR(1),A(10)),
5. 1(TAU(1),A(15))
6. DIMENSION YF(100),CJ(100,1)
7. DIMENSION X(1),VLAP(10,1)
8.
9. C
10. CCFRCH FANOA(100),FAFOR(100),RU(10,2),PC(130,2),
11. 1 R(100,2),RE(100,2),PE(100,2),TU(100,2),VN(100),
12. 2 Y(100),CTN(100),VNU(100,30),FF(100),IEC(100),
13. 3 IP(100),CP(100),M(100),Sd(155),TC(100),VLNK(100),
14. 4 E(100),LAMI(100),GAPK(1,1)
15.
16. C COMMON /PARA*1/ KTN,KOUT,JAN,WOL,JAP,IPC,P,KKX(3),KR(10),TILF(3),
17. 1 TMIN,TMAX,VISC,PR(1)
18.
19. C COMMON /PARA*2/ WP,SCH,RHO,VFL,R1,REF,FFA,IS,ISP,P,T,SIF,MTP,
20. 1 FL,FNL,FLIO,NO,IEL,ISPO,KRALP,CPE,TRF,TER,AA,ITS,
21. 2 IM,LL,IT,MODE,HMELT,SMELT,TMAX,TMTN,MELT,SUMN,
22. 3 SUPL,JC,HG,C6G,SVA,SVR,SVC,SVN,SURC,NXC,SAI,
23. 4 VMACH,KRZ2,SP1,GAR,THI,RX,INCHT,HCH,NCU,INT,
24. 5 IPZ,POAT,SRI,IXG,SVI,KKJ,TAC,DXG,SHI,MOATO,
25. 6 SA2,FFE,KS,RV,CME,VA,POS,DUM1,DUM2,EP,TEC,IC,
26. 7 ISP2,MTG,VMUP,WTL
27.
28. C COMMON /APRAYS/ A(16,16),R(16),W(3),XC(50),XC(50),ZKF(10),
29. 1 TLO(10),DMCLO(10),WALJP(10),FR(10),ALPI(10),
30. 2 GAPH(10),GAMF(10),TO(10,3),TX(10,3),WAT(10),
31. 3 LP(10),IOAT(10),KAT(10),DUM(10,10),FRL(10)
32.
33. C EQUIVALENCE (TU(10),TE(1)), (VNU(1),CJ(1))
34.
35. C COMMON /KINETX/ MT,FKF(50),EAP(50),FKK(50),PNU(10,50),KMU(10,50),
36. 1 PMR(50),PKKK(50)
37.
38. C EQUIVALENCE (B(1),X(1)), (GAPK(1),VLAP(1))
39.
40. C COMMON/ACE1/GAPEX,PEFN,PCH,ACHSQ,SQNAK,XP
41.
42. C COMMON /DIFFER/ IC(11),ALPT(10),C(10),SORCF(2),RA(2),IR(10),
43. 1 II,KK,J,VINT,VINT,JAT(10),LJM(10,10),FANA(10),
44. 2 FARB(10),KPHAT2)
45.
46. C DIMENSION ATA(10),ATR(10),ATC(10)
47. EQUIVALENCE (TO(1),ATA(1)), (TO(11),ATR(1)), (TO(21),ATC(1))
48.
49. C COMMON/CAPKIN/ KPK(10),ROUCH,NCC
50. COMMON/CONCHO/ Z,GAMER,WR(3)
51. CALL FTIME
52. NFE=0
53. TIMIN=300.
54. TIMAX=20000.
55. Z=0.0
56. PR=0.0

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55. KKJ=0
56. PSV=P
57. JI=0
58. IF (ITS + 1) 5,10,5
59. GAMEX=0.6666667
60. W(1)=1.0
61. W(2)=0.
62. W(3)=0.
63. W(4)=0.
64. W(5)=1
65. NCV=0
66. NOAT=0
67. WP=20.
68. T=3000.
69. HIP=0.
70. STD=0.
71. KR(10)=0
72. ITS=0
73. TDC=1
74. KRALP=0
75. KKJ=0
76. WS=1.0
77. KRA=KR(8)
78. KRQ=KR(4)
79. CALL KIRIN
80. KX(1)=KR(P)
81. WRITE (ROUT,290) TILE,KR
82. KR(8)=0
83. KRZ=0
84. TET=501.
85. KR(4)=KR(4)-1
86. IF (KR(4)) 20,15,15
87. IF (KR(6)) 25,25,20
88. KR(6)=KR(6)-1
89. 25 IF (KR(7)) 35,35,20
90. KR(7)=KR(7)-1+1
91. 35 IF (ABS(W(1)) + ARSLUP(2)) + ABS(WR(3)) 45,45,40
92. 40 W(1)=WR(1)
93. W(2)=WR(2)
94. W(3)=WR(3)
95. KRALP=1
96. CONTINUE
97. IF (KR(1) - 5) 55,50,55
98. 50 KR(1)=0
99. KR(P)=1
100. MOVE=KR(1)
101. KRALP=KRALP+IABS(KR8-KR(P))+IABS(KR4-KR(4))
102. SVA=0.
103. SVP=0.
104. TEZ=0
105. IF (MOVE - 5) 65,60,65
106. STOP
107. IF (GAMER) 70,95,70
108. 70 GAMF=SIGN(AFAXI,IABS(GAMER),0.0001),GAMER
109. IF (KR(3)) 80,80,75
110. 75 IF (KR(3)-9) 90,80,90
111. 80 J=1

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ZIP10055
ZIP10056
ZIP10057
ZIP10058
ZIP10059
ZIP10060
ZIP10061
ZIP10062
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ZIP10064
ZIP10065
ZIP10066
ZIP10067

ZIP10069
ZIP10070
ZIP10071
ZIP10072
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ZIP10096
ZIP10097
ZIP10098
ZIP10099
ZIP10100
ZIP10101
ZIP10102
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ZIP10104
ZIP10105
ZIP10106
ZIP10107
ZIP10108
ZIP10109
ZIP10110
ZIP10111

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112.      DO 85 IK=1,4
113.      EF(J)=EF(I)**(GAFER/GAFEX)
114.      J=J+1
115.      85 GAFEX=GAFEX
116.      95 IF (Z) 120,100,120
117.      100 IF (MOBE-q) 105,155,270
118.      105 IF (MOBE-3) 270,110,270
119.      110 IF (PR(S)) 270,270,115
120.      115 SIP=EXP
121.      60 TO 270
122.      120 IF (RCOE - 1) 125,125,140
123.      125 IF (T) 130,135,135
124.      130 T=T
125.      135 IFZ=1
126.      135 COTTIME
127.      60 TO 270
128.      140 IF (MOBE - 2) 270,255,145
129.      145 IF (MOBE-4) 260,150,260
130.      150 T=7
131.      155 MOBE=2
132.      155 KKE=-1
133.      155 KKE(5)=X0(P(5),1)
134.      155 K(1)=2
135.      155 PRAC (R10,245) KVI,UR,HTP,PSB,PRCK,SAI,PR1
136.      155 PHOR=-9999.
137.      155 KPI=-9999.
138.      155 IF (UR) 165,170,160
139.      155 SVI=UR
140.      155 60 TO 170
141.      155 SVI=SVI
142.      170 IF (HTP) 175,140,175
143.      175 HCH=HTP/1.6
144.      140 IF (KSO) 185,200,185
145.      185 IF (KSR + 9999.) 190,165,190
146.      190 SVI=KSR/1.6
147.      60 TO 266
148.      195 SVI=HTP
149.      200 IF (PRCK) 210,215,205
150.      205 SVI=PRCK
151.      60 TO 215
152.      210 SP1=KHC
153.      215 IF (PR1) 225,230,220
154.      220 SVI=PR1
155.      60 TO 236
156.      225 SP1=P
157.      230 60 TO (235,240,245), KVI
158.      235 SVI=SGRI (HCH - SP1) * 9010P.)
159.      60 TO 250
160.      240 HCH=SP1+SVI/9010P.*SVI
161.      60 TO 250
162.      245 SHI=HCH-SVI/9010P.*SVI
163.      250 SAI=SAI/57.29577
164.      SVA=(1.3146 * SH1 + SVI * COS(SAI))**2./9010P.
165.      SVA=SVA**2./1.9869
166.      SVC=(SVI * COS(SAI))**2./9010P.+SHI
167.      SV7=SP1+SVB/(1.3146 * SH1)
168.

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ZIP10112
ZIP10113
ZIP10114
ZIP10115
ZIP10116
ZIP10117
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P=SVN
GO TO 270
HIP=Z
GO TO 270
STP=Z
TF (SIP + 9999.) 270,265,270
STP=SCH
SCHAK=0.
PSV=PCH
TF (PR) 275,265,260
KKJ=1
ACFSG=PR*F
GAME=GAME-1.0
PR=PSV*(1.+GAME/2.*SCHAK)/(1.+GAME/2.*ACHSK)**((GAM/GAME)
KR(5)=1
P=PR
AASP=WM
RETURN
C
290 FORMAT (1H19X35HGRAPHITE SURFACE KINETICS (GASKET) 2A4.A2.5X1011)
295 FORMAT (11.F9.4,5F10.4)
END

ZIP10169
ZIP10170
ZIP10171
ZIP10172
ZIP10173
ZIP10174
ZIP10175
ZIP10176
ZIP10177
ZIP10178
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ZIP10180
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SURROUTINE AFM4T
REAL NFIA(1),NFIB(1),FFIN(1),TAU(10,10)
EQUIVALENCE (NFIA(1),A(1)), (NFIB(1),A(51)), (FFIN(1),A(101)),
1(TAU(1),A(151))
DIMENSION TF(180),CIJ(180,1)
DIMENSION X(1),VLAM(180,1)

COMMON
1 FMOA(180),FAMOR(180),RB(180,2),RC(180,2),
2 RO(180,2),RE(180,2),RF(180,2),TU(180,2),VN(180),
3 Y(180),WTM(180),VNU(180,10),FF(180),IFC(180),
4 IP(180),CP(180),H(180),SH(180),TC(180),VLNK(180),
5 E(180),LAMT(180),GAPK(1,1)

COMMON /PARAM1/ KIN,KOUT,JAN,MOL,NAB,IOC,N,KKX(3),KR(10),TILE(3),
1 TTMIN,TTMAX,VISC,PR(1)

COMMON /PARAM2/ WM,SCH,RHO,VEL,B1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
1 EL,ENL,FLIR,HQ,IFL,ISPG,KRALP,CPF,TRE,IER,AA,ITS,
2 IN,IL,IT,MODE,HMELT,SMELT,TMAX,TMIN,MELT,SUMN,
3 SUML,JC,HG,CPG,SVA,SVP,SVC,SVD,SUMC,NXC,SA1,
4 VMACH,KRZZ,SP1,GAM,THI,FX,DMCHI,HCH,NCV,TBT,
5 IFRZ,NOAT,SRI,IXG,SV1,KKJ,IXC,NXG,SH1,NOATO,
6 SA2,FFF,WS,RV,CHF,VA,HOS,DUM1,DUM2,EP,IFCJC,
7 ISP2,WTG,VMU2,WTL

COMMON /APRAYS/ A(16,16),H(16),W(3),XC(50),XG(50),ZKE(10),
1 TLO(10),DMCLO(10),WALPJ(10),EB(10),ALP(10),
2 GAMH(10),GAPK(10),TO(10,3),TK(10,3),WAT(10),
3 IP(10),IOAT(10),KAT(10),UM(10,10),ERL(10)
EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))

COMMON /KINETX/ MT,FKE(50),EAK(50),EXK(50),PNU(10,50),PUU(10,50),
1 PMR(50),PKKK(50)

EQUIVALENCE (R(1),X(1)), (GAPK(1),VLAM(1))

COMMON /DIFFER/ IR(11),FNU(10),PNUS(10),SLAM(10),RE(10),RY(10),
1 INC(10),JJ(10),SLB(16),SLA(16,16)

IF TRYING TO PUSH THROUGH TMIN OR TMAX -- REINVERT AND DT TO ZERO
IF (ITS-NCV-1) 5,5,10
DTU=1000.
DTD=DTU.
TTMIN=300.
TTMAX=20000.
CONTINUE
X1=X(1)
IF (T - TMIN) 15,15,20
IF (X(1)) 95,30,20
IF (T - TMAX) 30,25,25
IF (X(1)) 30,30,95
IF NEW COMPENSED HAS NEG CORRECTION, DELET AFTER REINVERT
IF (IFP) 45,65,35

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*COR
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55. 35 IF (VN(IREF)) 40,40,65
56. 40 IF (X(ITER) + 1.E-30) 45,65,65
57. 45 IF (IREF-N) 55,55,50
58. 50 JC=0
59. 55 CALL SWAP (A,R,SLA,SLR)
60. 60 DO 60 I=1,ISPO
61. 61 A(I,IER)=0.
62. 62 A(ITER,I)=0.
63. 63 A(ITER,IER)=1.E30
64. 64 R(ITER)=-0.1
65. 65 IF (COUNT) 175,190,190
66. 66 IF S.E. ERROR AND CORRECTION ON T OF CONFLICTING SIGN,REINVERT
67. 67 IF (MODE - 1) 160,70,165
68. 68 IF (X(1) + R1) 55,75,75
69. 69 ON S.F. IF DELTA LN T .GT. .9 REINVERT NO 01 IF F1 AND ENL ARE SAME
70. 70 IF (ABS(X(1)) - 0.9) 165,165,40
71. 71 IF (F1 - 0.02) 85,90,90
72. 72 IF (F1 - 100.) 165,90,50
73. 73 NOFE=0
74. 74 REINVERT
75. 75 CALL SWAP (A,R,SLA,SLR)
76. 76 IF CONVERGED EXCEPT FOR T ON H OR S OPTIONS -- NON CONVERGENT
77. 77 IF (MODE - 1) 155,105,100
78. 78 IF (F1 + 100. * ENL - 1.E - 4) 205,205,155
79. 79 ON S.F. OPTION RESULT IN CONFLICTING FROM/CORRECTION OR T PUSH
80. 80 IF OTHER BALANCES RELATIVELY GOOD, SET T TO TMIN/TMAX AS PER ERROR
81. 81 AND GO TO THERE (IF T ALREADY THERE - NONCONVERGE) ELSE LT TO ZERO
82. 82 IF (ABS(R1) - 100. * (F1 + ENL)) 155,110,110
83. 83 TMIN=AMAX1(TMIN,-DTU,300.)
84. 84 TMAX=AMIN1(TMAX,DTU,20000.)
85. 85 IF (X1+R1) 115,155,145
86. 86 IF (R1) 120,120,130
87. 87 IF (T-TMIN) 200,200,125
88. 88 T=AMAX1(TMIN,T-DTU)
89. 89 TMAX=T
90. 90 DTU=DTU/2.
91. 91 GO TO 195
92. 92 IF (T-TMAX) 135,200,200
93. 93 T=AMIN1(TMAX,T+DTU)
94. 94 TMIN=T
95. 95 DTU=DTU/2.
96. 96 IF (ABS(T - TF(JC)) - .001) 140,195,195
97. 97 JFC(JC)=1
98. 98 VN(JC)=1.F-3/WTN(JC)*WTG
99. 99 Y(JC)=0.
100. 100 GO TO 195
101. 101 IF (T-TMIN) 200,200,150
102. 102 IF (T-TMAX) 155,200,200
103. 103 Y(1)=0.
104. 104 MODE=0
105. 105 TMIN=TMIN
106. 106 TMAX=TMAX
107. 107 IN=IN-1
108. 108 IL=2
109. 109 GO TO 190
110. 110 Y(1)=0.
111. 115 IF (X(2) + 1.) 170,210,210

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AFMA0112
AFMA0113
AFMA0114
AFMA0115
AFMA0116
AFMA0117
AFMA0118
AFMA0119
AFMA0120
AFMA0121
AFMA0122
AFMA0123
AFMA0124
AFMA0125
AFMA0126
AFMA0127
AFMA0128
AFMA0129
AFMA0130
AFMA0131
AFMA0132

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1. SURROUTINF ALPST
2. COMMON/ACF1/GAMEX,REFM,PCH,ACHSQ,SQPAK,SXP
3.
4. REAL NFIA(1),NFIR(1),FFIN(1),TAU(10,10)
5. EQUIVALENCE (NFIA(1),A(1)), (NFIR(1),A(51)), (FFIN(1),A(101)),
6. 1(TAU(1),A(151))
7. DIMENSION TF(180),CIJ(180,1)
8. DIMENSION X(1),VLAM(180,1)
9.
10. COMMON
11. 1 FAMOA(180),FAMOB(180),RR(180,2),RC(180,2),
12. 2 RD(180,2),RE(180,2),RF(180,2),TU(180,2),VM(180),
13. 3 Y(180),WTM(180),VNU(180,10),FF(180),IFC(180),
14. 4 IP(180),CP(180),H(180),SB(180),TC(180),VLNK(180),
15. 5 E(180),LAMI(180),GAMK(1,1)
16.
17. COMMON /PARAM1/ KIN,KOUT,JAN,MOL,NAR,IDC,N,KXX(3),KR(10),TILE(3),
18. 1 TTMIN,TTMAX,VISC,PR(1)
19.
20. COMMON /PARAM2/ WM,SCH,RHO,VEL,R1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
21. 1 EL,ENL,FLIR,NQ,IFL,ISQ,KRALP,CP,IRE,IER,AA,ITS,
22. 2 IN,IL,IT,MODE,MWELT,SMELT,TMAX,TMIN,MELT,SUMN,
23. 3 SUML,JC,HG,CPG,SVA,SVR,SVC,SVD,SUMC,NXC,SAI,
24. 4 VMACH,KRZZ,SP1,GAM,THI,MX,DMCHI,HCH,NCV,TRT,
25. 5 IFR2,NOAT,SR1,IXG,SV1,KKJ,IXC,IXG,SH1,NOATO,
26. 6 SA2,FFF,WS,RV,CMF,VA,HOS,DUM1,DUM2,EP,IFCJC,
27. 7 ISP2,WTG,VMU2,NTL
28.
29. COMMON /ARRAYS/ A(16,16),B(16,16),W(3),XC(50),XG(50),ZKE(10),
30. 1 TLO(10),DMCLO(10),VALUP(10),ER(10),ALP(10),
31. 2 GAMH(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
32. 3 IR(10),IOAT(10),KAT(10),UP(10,10),EBL(10)
33. EQUIVALENCE (TU(181),TF(1)), (VNU(1),CIJ(1))
34.
35. COMMON /KINETX/ MT,EAK(50),EXK(50),PMU(10,50),RMU(10,50),
36. 1 PHR(50),PKKK(50)
37.
38. COMMON /FOURVALENCE (P(1),X(1)), (GAMK(1),VLAM(1))
39.
40. COMMON /DIFFER/ IC(1),ALPT(10),C(10),SORCE(P),RA(2),IM(10),
41. 1 IT,KK,J,VIT,YINT,JAT(10),LIP(10,10),FAKA(10),
42. 2 FAMB(10),KFHA(2)
43.
44. DIMENSION ATA(10),ATR(10),ATC(10)
45. EQUIVALENCE (TG(1),ATA(1)), (TG(11),ATR(1)), (TG(21),ATC(1))
46.
47. DATA REFD,FFAD/4HREFM,4HFFA /
48. DATA IS,Ic,I7/2H ,2H*1,2H*W/
49. TEMAX=20000.
50. IF (KR(3) - 7) 5,10,10
51. IF (NEF) 145,145,20
52. TGF=NEF
53. READ (17H,475) NEF
54. NEF=NEF+INF
55. INF=INF+1

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55. READ (KIN,455) (MFI(I),MFT(I),FFI(I),I=1,MF,MEF)
56. KIN(3)=9-KIN(2)
57. IF (MFI(MF) - MFT(MEF)) 20,15,20
58. TFMAX=FFI(MF)
59. GO TO 30
60. 1MFE=1
61. IF (MFI(1) - MFT(1)) 30,25,30
62. TFMAX=FFI(1)
63. JL=0
64. DO 50 I=1,MF
65. IF (MFI(I)-MFT(I)) 40,35,40
66. MFI=FFI(I)
67. JL=JL+1
68. GO TO 50
69. IF (MFI-MFT(I)) 50,45,50
70. MFI=FFI(I)
71. JL=JL+1
72. CONTINUE
73. IF (JL) 80,30,55
74. DO 75 J=1,M
75. FFI(J)=1.F+10
76. IF (MFI(J)-.01) 75,75,60
77. IF (MFI(J)) 65,70,65
78. IF (IABS(MFI(J))-1) 75,70,75
79. FFI(J)=(MFI(J)/MFI)*MFI*(MFI*GAPEX)
80. CONTINUE
81. WRITE (KOUT,460) MFI,FFI
82. IF (MFI-JL) 145,145,80
83. J=1
84. WRITE (KOUT,460)
85. MFI=JL+1
86. DO 140 I=1,MFI
87. I=1
88. I1=15
89. I2=15
90. I3=15
91. I4=15
92. IF (I4-I) 85,85,105
93. IF (MFI(J)) 90,105,90
94. IF (IABS(MFI(J)) - 3) 95,105,95
95. IF (TFMAX - 20000.) 100,105,105
96. TFI(J)=TFMAX
97. I=0
98. GO TO 125
99. IF (MFI(I) - FANOA(J)) 135,110,135
100. IF (MFI(I) - FANOB(J)) 135,115,135
101. IF (MFI(I) - 100.) 130,120,120
102. TFI(J)=MFI(I)+MFI(I),TFMAX)
103. WRITE (KOUT,465) FANOA(J),FANOB(J),TF(J),I1,I2
104. I1=I6
105. I2=I7
106. GO TO 135
107. FFI(J)=FFI(I)
108. WRITE (KOUT,470) MFI(I),MFT(I),MFI(I),I1,I3,I4
109. FFI(J)=FFI(J)*GAPEX
110. I3=I6
111. I4=I7

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ALPS0055
 ALPS0056
 ALPS0057
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 ALPS0059
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 ALPS0070
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 ALPS0109
 ALPS0110
 ALPS0111

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112.      135      I=I+1
113.      IF (I - NFF) 105,105,140
114.      J=J+1
115.      NFF=0
116.      VS=1.0
117.      IF (KR(6)) 165,150,150
118.      W(1)=0.
119.      IF (KR(4)) 160,160,155
120.      IF (KR(4) - 3) 170,160,170
121.      W(1)=1.0
122.      GO TO 170
123.      VS=V(1)+V(2)+K(3)
124.      MOAT=MOAT
125.      MOAT=0
126.      NUP=0.
127.      DO 230 K=1,IS
128.      ALPH=(W(1) * TK(K,1) + W(2) * TK(K,2) + W(3) * TK(K,3))/VS
129.      IF (ALPH) 175,175,230
130.      IF (KAT(K)-99) 185,180,185
131.      IF (K(6)) 230,225,225
132.      IF (KR(6)) 225,190,205
133.      IF (TK(K,1)) 195,195,230
134.      IF (KR(8)) 225,225,206
135.      IF (TK(K,3)) 225,225,230
136.      IF (MOAT) 220,220,210
137.      DO 215 KK=1,MOATG
138.      IF (LOAT(KK) - K) 215,225,215
139.      CONTINUE
140.      CONTINUE
141.      GO TO 230
142.      MOAT=MOAT+1
143.      SUM1=SUM1-ALPH
144.      LOAT(MOAT)=K
145.      CONTINUE
146.      VS=VS*(1. + DIM1)
147.      DO 235 K=1,IS
148.      GAMF(K)=0.
149.      ALPH(K)=(W(1) * TQ(K,1) + W(2) * TQ(K,2) + W(3) * TQ(K,3))/VS
150.      TEST=1.0
151.      IF (KR(6)) 315,245,240
152.      STOP 222
153.      C SURFACE MASS BALANCE PACKAGE GOFS HERE
154.      IF (KR(4) - 2) 290,250,290
155.      IF (NCV+KR(3)) 255,255,330
156.      PMU2=0.
157.      KR(4)=1
158.      DO 265 K=1,IS
159.      IF (WTM(K)-1.0) 265,260,260
160.      VA=VN(K)/FF(K)
161.      ZKF(K)=VA
162.      PMU2=PMU2+VA*WTM(K)
163.      CONTINUE
164.      J=ISP
165.      DO 280 IK=ISP,N
166.      IF (WTM(IK)-1.0) 280,270,270
167.      VA=VN(IK)/FF(IK)
168.      PMU2=PMU2+VA*WTM(IK)

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169.			NO 275 K=1,IS	ALPS0169
170.	275		ZKE(K)=ZKF(K)+VA*VNU(J,K)	ALPS0170
171.	280		J=J+1	ALPS0171
172.			NO 285 K=1,IS	ALPS0172
173.	285		ZKE(K)=ZKF(K)/PMU2	ALPS0173
174.	290		NO 310 I=1,IS	ALPS0174
175.			K=IR(I)	ALPS0175
176.	295		IF (KAT(I)-99) 295,300,295	ALPS0176
177.	300		IF (W(1)) 305,305,310	ALPS0177
178.			ALP(K)=0.	ALPS0178
179.			GO TO 310	ALPS0179
180.	305		ALP(K)=ALP(K)+ZKF(K)	ALPS0180
181.	310		CONTINUE	ALPS0181
182.			TEST=1.*W(2)+W(3)	ALPS0182
183.	315		NO 320 K=1,IS	ALPS0183
184.	320		TEST=TEST-ALP(K)*WTM(K)	ALPS0184
185.			IF (ARS(TEST) - .001) 335,335,325	ALPS0185
186.	325		WRITE (KOUT,485) . W	ALPS0186
187.			STOP	ALPS0187
188.	330		WRITE (KOUT,490)	ALPS0188
189.			STOP	ALPS0189
190.	335		IF (KR(3)) 340,340,400	ALPS0190
191.	340		IF (NOAT0) 400,400,345	ALPS0191
192.	C		REINITIALIZE SPECIES	ALPS0192
193.	345		PIH=P/10.	ALPS0193
194.			PIH=ALOG(PIN)	ALPS0194
195.			J=1	ALPS0195
196.			NO 395 IK=1,N	ALPS0196
197.			IF (IFC(J) + 1) 350,395,360	ALPS0197
198.	350		IFC(J)=IFC(J)+3	ALPS0198
199.			IF (J - IS) 370,370,355	ALPS0199
200.	355		YC=0.	ALPS0200
201.			GO TO 375	ALPS0201
202.	360		IF (IFC(J) - 1) 355,395,365	ALPS0202
203.	365		IFC(J)=IFC(J)-3	ALPS0203
204.	370		YC=PIH	ALPS0204
205.	375		IF (IFC(J)) 385,390,380	ALPS0205
206.	380		IFC(J)=1	ALPS0206
207.	385		VN(J)=0.	ALPS0207
208.			V(J)=YC	ALPS0208
209.			GO TO 395	ALPS0209
210.	390		VN(J)=PIN	ALPS0210
211.			V(J)=PIH	ALPS0211
212.	395		J=J+1	ALPS0212
213.	400		IF (NOAT) 450,450,405	ALPS0213
214.	405		J=1	ALPS0214
215.			NO 430 IK=1,N	ALPS0215
216.			IF (NOAT - J) 425,410,410	ALPS0216
217.	410		NO 420 L=1,NOAT	ALPS0217
218.			K=IOAT(L)	ALPS0218
219.			LAMT=LAMT(J)/2*(K - 1)	ALPS0219
220.			LAMT=LAMT-(LAMT / 2)*2	ALPS0220
221.			IF (LAMT) 415,420,415	ALPS0221
222.	415		VN(J)=0.	ALPS0222
223.			IFC(J)=IFC(J)-3	ALPS0223
224.			GO TO 430	ALPS0224
225.	420		CONTINUE	ALPS0225

```

226. 425 CONTINUE
227. 430 J=J+1
228. 435 IF (NOAT - 1) 445,435,435
229. 440 DO 440 L=1,NOAT
230. 445 K=10AT/L)
231. 450 J=IR(K)
232. 455 IFC(J)=IFC(J)+6
233. 460 CONTINUE
234. 465 RETURN
235. C
236. 455 FORMAT (2A4,F12.5,2A4,F12.5,2A4,F12.5)
237. 460 FORMAT (2A4, UPDATE OF DIFFUSION FACTORS/10X,7ASPECTSYLADIFFUSION)
238. 465 10N FACTOR)
239. 470 FORMAT (11X2A4,6XF10.3,2A2)
240. 475 FORMAT (11X2A4,6XF10.5,2A2)
241. 480 FORMAT (13X,5F6.5,F6.4)
242. 485 FORMAT (/5X54HALL GASEOUS DIFFUSION FACTORS RECALCULATED AS (MOL.%ALPS0242
243. 11/F7.3,3H)*F6.3//)
244. 490 FORMAT (/// 5X54HALL MASS BALANCE INITIATION, CHECK . . . /
245. 1 10X74H1, REARRANGEMENT OF ELEMENTS BETWEEN ENDF AND WALL SOLUTIONALPS0245
246. 2NS (KX12).G1.0) /10X2A42, COMPONENT MASS FRACTION ( XE12.4,11H) MOALPS0246
247. 3T EQUAT/16X71H10 ZERO FOR UNDEFINED COMPONENT (ALL ZERO GRAM-ATOMIALPS0247
248. 4C-WEIGHTS PER GRAM) )
249. 490 FORMAT (////5X75H10 VAL TO EDGE COMPOSITION AVAILABLE BECAUSE LAST ALPS0249
250. 1SOLUTION HAS NOT CONVERGED OR/11X73H10 FIRST GUESSES HAVE BEEN IALPS0250
251. 2INTRODUCED IN INPUT SUBROUTINE (KX(3)=1 TO 4) )
252. END

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ALPS0226
ALPS0227
ALPS0228
ALPS0229
ALPS0230
ALPS0231
ALPS0232
ALPS0233
ALPS0234
ALPS0235
ALPS0236
ALPS0237
ALPS0238
ALPS0239
ALPS0240
ALPS0241
ALPS0242
ALPS0243
ALPS0244
ALPS0245
ALPS0246
ALPS0247
ALPS0248
ALPS0249
ALPS0250
ALPS0251
ALPS0252


```

1. C
2. REAL MFIAT(1),MFIH(1),FFTH(1),TAU(10,10)
3. EQUIVALENCE (MFIAT(1),A(1)), (MFIH(1),A(5)), (FFTH(1),A(10)),
4. 1(TAU(1),A(15))
5. DIMENSION TE(100),CIJ(100,1)
6. DIMENSION X(1),VLAM(100,1)
7. C
8. COMMON
9. FAMOA(100),FAMOB(100),RR(100,2),RC(100,2),
10. RQ(100,2),PE(100,2),PE(100,2),TU(100,2),VH(100),
11. Y(100),WTH(100),VUH(100,10),FF(100),IEF(100),
12. IP(100),CP(100),H(100),SC(100),TC(100),VLAM(100),
13. E(100),LANT(100),GAMP(1,1)
14. C
15. COMMON /PARAM1/ KTH,KOUT,JAN,NOL,DAE,IGC,G,KKK(3),PH(10),TTLF(3),
16. TTHIN,TTNAX,VISC,PH(1)
17. C
18. COMMON /PARAM2/ WM,SCHEARHO,VFL,H1,MFF,FFA,TS,ISP,P,T,SIF,HIP,
19. FL,ENL,FLTQ,NG,IFL,ISHQ,KRALP,CFE,IRF,IFR,AA,ITS,
20. IN,IL,IT,MDF,HMELT,SMELT,IMAX,IMIN,MELT,SUMN,
21. SIML,JG,HG,CPG,SVA,SVD,SVC,SVM,SUMC,NXC,SAT,
22. VMACH,KRZ2,SP1,GAP,THI,MX,DNCHT,ACH,NCV,TRT,
23. IFRZ,MOAT,SRI,IXG,SVI,KKJ,IX,NXG,SH1,MOATO,
24. SAZ,FFF,WS,RV,CMF,VA,HOS,DUM1,DUM2,EP,IFCUC,
25. ISP2,WTG,VHU2,WL
26. C
27. COMMON /APRAYS/ A(16,16),H(16),W(3),YC(50),XG(50),ZKE(10),
28. TLO(10),DNCLG(10),SWAI,JP(10),FER(10),ALPI(10),
29. GAMB(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
30. IP(10),IOAT(10),KAT(10),UM(10,10),FRL(10)
31. EQUIVALENCE (TU(10),TE(1)), (VUH(1),CIJ(1))
32. C
33. COMMON /KINETX/ MT,FKF(50),EKK(50),PMU(10,50),PMU(10,50),
34. PMP(50),PKKK(50)
35. C
36. EQUIVALENCE (B(1),X(1)), (GAMP(1),VLAM(1))
37. C
38. COMMON /DIFFER/ IC(11),ALPT(10),C(10),SORCE(P),RA(2),IM(10),
39. II,KK,J,VINT,VINT,JAT(10),LIF(10,10),FAMA(10),
40. FAMB(10),KPHK(2)
41. C
42. DIMENSION ATA(10),ATR(10),ATC(10)
43. EQUIVALENCE (TR(1),ATA(1)), (TG(11),ATB(1)), (TR(21),ATC(1))
44. C
45. IF (J - IS) 10,10,15
46. 10 JM=J-1
47. WRITE (KOUT,190) JM,IS,(FAMOA(1),FAMOB(1),I=1,JM)
48. WRITE (KOUT,195) (FAMOA(I),FAMOB(I),I=ISP,N)
49. STOP
50. DO 25 L=2,IS
51. JM=ISP-L
52. INJ=IN(JM + 1)
53. IF (JM - 1) 30,20,20
54. 20 DO 25 K=1,JM

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*COR
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55. UGH=TAU(IPJ,K)
56. DO 25 I=1,IS
57.   IM(I,K)=UM(I,K)-UGH*UM(I,JM + 1)
58.   CONTINUE
59.   DO 50 I=1,IS
60.     IM(I,I)
61.     IF (IM(I - 1) 40.50,40
62.     DO 45 K=1,IS
63.       VSUM(K,IM)
64.       UPRK,IM)=UM(K,I)
65.       UM(K,I)=V
66.       IM(I)=IM(IM(I))
67.       IM(IM(I))=IM(I)
68.       GO TO 35
69.     CONTINUE
70.   C -----ELEMENT -- BASE GAS CORRESPONDENCE
71.   C INITIALIZE ROW AND COLUMN SUMS
72.   TG=IS
73.   DO 55 I=1,IS
74.     IM(I)=1
75.     IC(I)=1
76.     C EVALUATE INITIAL SUMS
77.     LA=0
78.     DO 70 J=1,IS
79.       DO 65 J=1,IS
80.         LAMT=LAMIC(J)/LAMB
81.         IF (I,J)=LMT-(LAMY / 2)*2
82.         IF (I,J)=LMT-(LAMY / 2)*2
83.         IC(J)=IC(J)+1
84.         IM(I)=IM(I)+1
85.       CONTINUE
86.       LAMC=LAMC+LAMB
87.       C CHECK FOR ZEROS
88.       T2=0
89.       DO 165 I=1,IS
90.         IF (IC(I) - T2) 120,95,120
91.         DO 50 J=1,IS
92.         IF (LIM(J,I)) 95,90,95
93.         CONTINUE
94.         IC(I)=J
95.         IM(J)=I
96.         LIM(J,I)=0
97.         DO 115 K=1,IS
98.         IF (LIM(K,I)) 100,105,100
99.         IC(K)=IC(K)+1
100.        LIM(J,K)=0
101.        IF (LIM(K,I)) 110,115,110
102.        LIM(K,I)=0
103.        IM(K)=IM(K)+1
104.        CONTINUE
105.        GO TO 170
106.        IF (IM(I) - T2) 165,125,165
107.        DO 135 J=1,IS
108.        IF (LIM(I,J)) 130,135,130
109.        IC(J)=J
110.        IM(J)=I
111.        LIM(I,J)=0

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BELC0055
 BELC0056
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 BELC0111

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112.      GO TO 140
113.      CONTINUE
114.      DO 160 K=1,IS
115.      IF (LTP(K,J)) 145,150,145
116.      F(K)=F(K)-1
117.      LTP(K,J)=0
118.      IF (LTP(I,K)) 155,160,155
119.      LTP(I,K)=0
120.      TC(K)=IC(K)-1
121.      CONTINUE
122.      GO TO 170
123.      CONTINUE
124.      IZ=IZ+1
125.      GO TO 20
126.      J=IS+1
127.      IF (IS) 175,175,75
128.      DO 180 I=1,IS
129.      K=1+L(I)
130.      F(K)=F(K)+1
131.      F(K)=F(K)+1
132.      WRITE (MOUT,200) (I,ATC(I)),I=1,IS
133.      WRITE (MOUT,205) (F(K),I)=1,IS
134.      DO 185 I=1,IS
135.      DO 185 I=1,IS
136.      TC(I)=0
137.      GO 185 K=1,IS
138.      TC(I)=TC(I)+L(I)*UP(I,K)+TC(K,I)
139.      RETURN
140.      C
141.      FORMAT (///150, ONLY FOLLOWING 13,230 CASE SPECIES FOUND FOR 13,
142.      1 54 ELEMENTS/(2X2004))
143.      FORMAT (//304 OTHER SPECIES CONSIDERED VERF/(2X2004))
144.      145  FORMAT (//X,04ELEMENTS,7X,1504/(20X,15/4))
145.      200  FORMAT (//X,1204SE SPECIES,3X,5(204,4X)/(20X,5(204,4X)))
146.      205  .
147.      END

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1. SUBROUTINE CRECT (NCE)
2. DIMENSION DY(1),DYA(1)
3.
4. REAL NFA(1),NFB(1),FFIN(1),TAU(10,10)
5. EQUIVALENCE (NFA(1),A(1)), NFB(1),A(5)), (FFIN(1),A(10)),
6. 1(TAU(1),A(15))
7. DIMENSION TF(100),CLJ(100,1)
8. DIMENSION X(1),VLA(100,1)
9.
10. COMMON /PARA01/ FAKOR(100),RP(100,2),RC(100,2),
11. RC(100,2),PE(100,2),PE(100,2),VM(100),
12. Y(100),XFB(100),VM(100,10),FF(100),TEC(100),
13. IP(100),CF(100),H(100),SA(100),IC(100),VLOR(100),
14. E(100),LAP(100),GAPK(1,1)
15.
16. COMMON /PARA02/ KTO,KOUT,JOH,POL,NAP,TEC,P,KKY(3),VR(10),TILE(3),
17. TMIN,TMAX,VISC,PK(1)
18.
19. COMMON /PARA03/ RP,SGH,RHO,VLA(10),DEF,FEA,IS,ISP,P,T,STF,HP,
20. EL,EML,FLIG,NO,TEL,ISQ,KHALP,CPE,TRF,TER,AA,ITS,
21. IP,IT,IT,MODE,HMELT,SELT,TRAX,TRIM,MEI,T,SUMN,
22. SUFF,JC,HG,CDE,SVA,SVR,SVC,SVD,SUMC,NXC,SAL,
23. VACH,KPZZ,SP1,GAM,DTT,EX,OFCHT,UCH,NCV,TRT,
24. IENZ,NDAT,CRI,1XG,SVI,MKJ,XC,XG,SHI,NDATO,
25. SA2,FEF,MS,RV,CME,VA,HOS,DUU1,DUM2,FP,IFCJC,
26. ISP2,VTG,VMU2,NTL
27.
28. COMMON /ARRAYS/ A(16,16),P(16),N(3),VC(50),XG(50),ZKE(10),
29. TIC(10),DMCLO(10),VALJP(10),FR(10),ALP(10),
30. GAPH(10),GAPF(10),TG(10,3),TK(10,3),WAT(10),
31. IR(10),IOTAT(10),KAT(10),UR(10,10),EAL(10)
32.
33. EQUIVALENCE (TIC(1),TE(1)), (VMU(1),CIJ(1))
34.
35. COMMON /KINETX/ MT,FKE(50),EAK(50),EXK(50),PMU(10,50),PMU(10,50),
36. POK(50),PKK(50)
37.
38. EQUIVALENCE (R(1),X(1)), (GAPK(1),VLA(1))
39.
40. COMMON /DIFFER/ IG(1),FMI(10),PMUS(10),SLAM(10),PE(10),MY(10),
41. IRC(10),JJ(10),SLR(16),SLA(16,16)
42.
43. EQUIVALENCE (A(1),DY(1),DYA(1))
44.
45. N1=1
46. N=IR(1)
47. NTL=0,
48. VTC=0,
49. DMF2=0,
50. T=1
51. IT=NR(R)+N
52. DO 130 JK=1,IM
53. DYTEC=DFDY(TK)
54. IF (DYTEC) 10,5,10
55. IF (IFC(1)) 150,50,120
56. IF (IFC(1)) 90,15,115

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*COR
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55. 15 IF (IP(I)) 20,45,20
56. 20 IF (M - IK) 25,30,25
57. 25 IF (KOF) 45,45,35
58. 30 M1=M1+1
59. 35 M=IR(M1)
60. 35 VP(I)=VN(I)*(1. + DYI)
61. 40 IF (VN(I)) 45,45,40
62. 40 Y(I)=ALOG(VN(I))
63. 40 GO TO 50
64. 45 Y(I)=Y(I)+DYI
65. 45 VP(I)=EXP(Y(I))
66. 50 VA=VTF(I)*VN(I)
67. 60 WIG=WTG+VA
68. 60 DU*2=DUP2+VA/FF(I)
69. 65 TF (IK - IS) 55,55,65
70. 55 PHUS(I)=VA(I)
71. 70 IF (KR(6)) 130,60,60
72. 60 SLAM(I)=VN(I)/FF(I)
73. 70 GO TO 130
74. 65 DO 75 K=1,IS
75. 75 VA=VN(I)*K*VP(I)
76. 75 IF (KR(6)) 75,76,75
77. 70 SLAM(K)=SLAM(K)+VA/FF(I)
78. 75 PHUS(K)=PAUS(K)+VA
79. 75 IF (KR(6)) 130,130,80
80. 80 DO 85 K=1,IS
81. 85 SLAM(K)=SLAM(K)+VN(I)*VLA(I)*K
82. C NON-PRESENT BASE CORRECTIONS AND TESTS
83. 90 Y(I)=Y(I)+DYI
84. 95 IF (Y(I)) 130,95,95
85. 95 IF (IFC(I) + 1) 130,100,100
86. 100 IF (KR(6)) 110,105,105
87. 105 IF (T - TF(I) + .001) 130,110,110
88. 110 Y(I)=0.
89. 110 IFC(I)=+1
90. 90 GO TO 130
91. 115 VN(I)=VA(I)+DYI
92. 92 IF (VN(I)) 125,125,120
93. 120 VTI=VTI+VN(I)*VIN(I)
94. 94 GO TO 130
95. 125 VN(I)=0.
96. 96 IFC(I)=-1
97. 130 I=I+1
98. 98 IF (KR(6)) 145,135,145
99. 135 FFF=VTC/DUP2
100. 100 DO 140 I=1,IS
101. 140 SLAM(I)=SLAM(I)*FFF
102. 145 RETURN
103. END

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CREC0055
CREC0056
CREC0057
CREC0058
CREC0059
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CREC0090
CREC0091
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CREC0095
CREC0096
CREC0097
CREC0098
CREC0099
CREC0100
CREC0101
CREC0102
CREC0103

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112.      R1=R(1)
113.      IF (KR(9)) 110,110,105
114.      CALL KINFT
115.      MOP=1
116.      IF (KR(7) - 1) 125,120,115
117.      I00=-2
118.      WRITE (KOUT,215) (I,I=1,IS)
119.      UP1F (KOUT,210) YTS,T,AA,FL,FUL,CHE,(E(1),I=1,IS)
120.      IF (IIS) 45,40,130
121.      I1=IIS
122.      IF (IIS-67) 140,135,140
123.      KR(7)=9
124.      I00=-2
125.      IF (IIS-70) 155,155,145
126.      NCV=1
127.      KR(7)=4
128.      I00=-2
129.      IIS=-1
130.      GO TO 45
131.      CALL SWAP (SLA,SLP,A,H)
132.      ICT=10
133.      DUM1=0.
134.      I01=100
135.      DO 170 I=1,IS
136.      IF (IFC(I) - 1) 170,170,165
137.      A(I + 2,I + 2)=1.E+10
138.      CONTINUE
139.      I00=101
140.      CALL PERAY (TR,A(7),I1) 0,ROIL) 0,1,0,100)
141.      ICT=ICT-1
142.      IF (ICT) 190,175,175
143.      IF (I00) 190,140,140
144.      CALL AFAT
145.      GO TO (140,145,145,145), I0
146.      CALL SCALE (M01)
147.      CALL CRECT (M01)
148.      IF (CMF - 1.E-12) 130,190,205
149.      IF (ICV) 190,200,195
150.      CALL SWAP (A,B,SLA,SLP)
151.      GO TO 145
152.      NCV=1
153.      GO TO 45
154.      IF (KR(7) - 1) 65,145,60
155.      C
210.      FORMAT (/41X,14,F0.2,1P4E10.2/(10I0F12.5))
215.      FORMAT (10I,40Z,40Z,1TC TEEF  PAFS+MET F04IL FR  MAFSAI FR  SCALF
1      /16(13.70 F4S.0L1))
156.      END

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GASK0112
GASK0113
GASK0114
GASK0115
GASK0116
GASK0117
GASK0118
GASK0119
GASK0120
GASK0121
GASK0122
GASK0123
GASK0124
GASK0125
GASK0126
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GASK0159


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1.      C      COMMON /PARAM1/ KTN,KNTY,JAN,MOL,NAF,IPC,N,KKX(3),KR(10),TITLE(1),
2.      REAL N(10),N(10),N(10),N(10),N(10),N(10),N(10),N(10),N(10),N(10),
3.      EQUIVALENCE (N(10),N(10)), (N(10),N(10)), (N(10),N(10)), (N(10),N(10)),
4.      1020(1),N(10))
5.      DIMENSION TF(180),CIJ(180,1)
6.      COMPLEX X(1),Y(1),Z(1),W(1)
7.      C
8.      COMMON /PARAM2/ FAKOAI(180),FAKOB(180),KR(180,2),RC(180,2),
9.      1      RD(180,2),RE(180,2),RF(180,2),TG(180,2),VN(180),
10.     2      Y(180),WTH(180),VNU(180,10),FF(180),IFC(180),
11.     3      IP(180),CP(180),M(180),SH(180),TC(180),VLNK(180),
12.     4      E(180),LANT(180),GAPK(1,1)
13.     C
14.     COMMON /PARAM3/ KTN,KNTY,JAN,MOL,NAF,IPC,N,KKX(3),KR(10),TITLE(1),
15.     1      TTPIN,TTMAX,VISC,PR(1)
16.     C
17.     COMMON /PARAM4/ W,SCH,RHO,VFL,B1,NFF,FFA,IS,ISP,P,T,SIP,HIP,
18.     1      EL,ENL,FLIQ,MQ,IFL,ISPC,KKALP,CPF,IRE,IER,AA,ITS,
19.     2      IN,IL,IT,PODE,HMELT,SMELT,TMAX,TMIN,MELT,SUMN,
20.     3      SUML,JC,MG,CPG,SVA,SVR,SVC,SVD,SUMC,NXC,SAL,
21.     4      VNA,CH,KRZ2,SP1,GAH,THI,MA,PRCHI,HCH,NCV,TBT,
22.     5      IFPZ,NOAT,SRI,IXG,SVI,MKJ,IXC,NKG,SHI,NCATO,
23.     6      SA2,FFF,WS,RV,CNF,VA,HOS,DUM1,DUM2,EP,IFCJC,
24.     7      ISP2,WT6,VNU2,WTL
25.     C
26.     COMMON /PARAM5/ A(16,16),B(16),X(13),XC(50),XG(50),ZKE(10),
27.     1      TLO(10),CPCLC(10),WALJP(10),FER(10),ALP(10),
28.     2      GAMH(10),GAMF(10),TO(10,3),TK(10,3),NAT(10),
29.     3      IR(10),IOAT(10),KAT(10),UM(10,10),FBL(10)
30.     EQUIVALENCE (U(10),T(1)), (VNU(1),CIJ(1))
31.     C
32.     COMMON /PARAM6/ MT,FKE(50),EAK(50),FYK(50),PMU(10,50),RMU(10,50),
33.     1      PFR(50),PKKK(50)
34.     C
35.     EQUIVALENCE (B(1),X(1)), (GAMK(1),VLAM(1))
36.     C
37.     COMMON /DIFFER/ IR(11),FNU(10),PMUS(10),SLAM(10),RE(10),BY(10),
38.     1      IHC(10),JU(10),SLR(16),SLA(16,16)
39.     C
40.     WSSE=AS
41.     DO 5 I=1,IS
42.     5      IBC(I)=IFC(I)
43.     IF (KR(6)) 40,15,10
44.     USSE=AMIN1((1),C,)+AMIN1(W(2),0,)+AMIN1(W(3),0,0)
45.     US=W(1)+V(2)+W(3)
46.     GO TO 20
47.     15      CONTINUE
48.     IF (ITS) 25,40,40
49.     DO 35 I=1,IS
50.     35      IF (IBC(I)-1) 35,30,35
51.     30      IFC(I)=-1
52.     35      CONTINUE
53.     RV=VISC-XTN / WT6
54.

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55. IF (KR(7) - 1) 60.45,50
56. IF (ITS) 40.55,60
57. WRITE (KOUT,325) FFF,WL,WIG,AA,PV,ALP,PNUS,SLAM
58. KR(7)=KR(7)-1
59. IF (KR(7) - 1) 60.55,60
60. WRITE (KOUT,330) (I,I=1,IS)
61. C INITIALIZE
62. EL=0.
63. CP6=0.
64. EP=P
65. CFF=0.
66. JC=0
67. JCS=0
68. TSPQ=IS+2
69. R(1)=0.
70. R(2)=0.
71. A(1,1)=0.
72. A(1,2)=0.
73. A(2,1)=0.
74. A(2,2)=0.
75. C ----INITIALIZE CONTRIBUTION OF MOST SIGNIFICANT SPECIES IN EACH
76. DO 65 I=1,IS
77. ER(I)=0.
78. E(I)=AA*ALP(I)
79. TSP2=TSPQ
80. C -- - MAIN PASE SPECIES LOOP
81. DO 315 IK=1,IS
82. I=2-IND(IK)
83. IF (KAT(IK)-99) 75,70,75
84. DUS(I-2)=0.
85. C ZERO MATRIX
86. DO 80 K=1,TSPQ
87. AK,IJ=0.
88. IF (ITS) 100,85,100
89. C NORMALIZE ON PRESSURE ON FIRST PASS
90. VN(I-2)=VN(I-2)/SUMH
91. ERL(I-2)=0.
92. IF (INC(I-2)) 100,90,95
93. Y(I-2)=Y(I-2)-SUML
94. GO TO 100
95. IF (SUMC.NE. 0.0) VN(I-2)=VN(I-2)/SUMC
96. IF (SUMC.EQ. 0.0) VN(I-2)=0.0
97. C INITIALIZE SOME MORE
98. R(I)=0.
99. A(I,1)=0.
100. IP(I-2)=0.
101. C SET FLAG INDICATING SIGNIFICANCE OF SPECIES IN MASS
102. C BALANCE(S) AND INCREMENT COUNT ON SIGNIFICANT SPECIES
103. IF (VN(I-2) - ERL(I-2)) 110,110,105
104. IP(I-2)=1
105. C TREAT PASE SPECIES CONTAINING BUT NOT REPRESENTING NON-PRESENT
106. C ELEMENTS IN SAME MANNER AS NON-PRESENT COMPENSED SPECIES
107. IF (INC(I-2)+1) 315,115,115
108. IF (INC(I-2)) 170,205,120
109. A(I,I)=1.
110. VA=VN(I-2)
111. IF (IABS(JAC(I-2)-3)-1) 125,270,130

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112. 125 A(2,I)=1.0
113. GO TO 270
114. 130 IF (EAI - 2) - APS(VA)) 135,140,140
115. 135 EAI - 2)=ABS(VA)
116. 140 TH1 - 2)=J-2
117. 145 F(I - 2)=F(I - 2)-VA
118. 150 IF (K(6)) 145,150,150
119. 155 DO 155 K=1,IS
120. 160 A(2,I)=EAI*(I-2)*(PIQS(K)/LTG+GANE(K))
121. 165 A(I,I)=A(I,I)+1.
122. 170 YPNE=AXI(TFII,TF(I - 2))
123. 175 IF (T - TF(I - 2) + .001) 165,165,170
124. 180 A(I,I)=1.0E+10
125. 185 F(I - 2)=VM(I - 2)*1.001E+10
126. 190 VMIE=0
127. 195 IF (K(6)-1) 175,180,175
128. 175 IF (K(6)) 270,270,140
129. 180 IF (TF(I - 2) + .001 - T) 315,185,185
130. 185 IF (JC) 195,195,190
131. 190 IF (Y(I-2)-QJC) 315,315,195
132. 195 KJCEY(I-2)
133. JCS=JC
134. TMAX=TF(I - 2)
135. JC=I-2
136. TFCJC=TFC(I-2)
137. 200 A(I,JCS+2)=0.
138. A(I,I)=1.0
139. R(I)=QJC
140. GO TO 315
141. C ----GAS PHASE
142. 205 VA=VM(I - 2)
143. PFE=CPG+VA*CP(I - 2)
144. A(I,I)=VA
145. EP=EP-VA
146. 210 IF (KAT(I)-49) 210,265,210
147. 215 DO 220 K=1,IS
148. 220 A(K+2,I)=GAP(I-2,K) + GAP(K) * H(T-2))*VA
149. A(I,I)=A(I,I)+VA*V
150. DUE=OUT(T - 2)/NTG*WTL/KTC+VA
151. DO 235 K=1,IS
152. 235 IF (F(I,K) - ABS(F(I,K) + 2,T)) 225,230,230
153. 230 F(I,K)=ABS(F(I,K) + 2,T))
154. T(I,K)=T-2
155. F(I,K)=F(I,K)-A(I,K + 2,I)
156. 235 A(K + 2,I)=A(K + 2,I)+DUE*2*PIQS(I)
157. GO TO 270
158. DUE1=VTH(I - 2)/NTG+VA
159. DUE2=WTL/KTC*DUE1
160. IF (K(4)) 245,245,250
161. F(I,I)=0.
162. VA=VM + 1.)*VA
163. GO TO 255
164. DUE1=DUE1*(I) - FFE / FFE(I - 2))
165. 250

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169.      VA=(PV + FFF / FF(I - 2))*VA
170.      GO TO 260 N=1,IS
171.      A(I + 2,1)=EXP(1*SI*AN(X)+CUM2*PHUS(X)
172.      A(I,1)=A(I,1)+VA
173.      F(I - 2) = A(I,1)+VA
174.      F(I - 2)=I-2
175.      F(I - 2)=F(I - 2)-1/6
176.      IF (CUM2 - 2) 310,290,275
177.      IF (F(I-2)) 315,265,260
178.      HOS=SE(I - 2)
179.      GO TO 295
180.      HOS=SE(I - 2)-1.5625*Y(I - 2)-1.5625
181.      GO TO 300
182.      HOS=H(I - 2)
183.      IF (F(I-2)) 315,300,295
184.      A(I,1)=HOS
185.      GO TO 305
186.      A(I,1)=HOS*Y(I - 2)
187.      A(I,2)=A(I,2)+HOS*Y(I - 2)
188.      CFF=CFF+CP(I - 2)*Y(I - 2)
189.      CONTINUE
190.      GO TO 1=1,IS
191.      RE(I)=F(I)
192.      AY(I)=Y(I)
193.      RETURN
194.
195.      C
196.      FORMAT (32H FFF,PTI,PTG,AA,RV/ALP/PHUS/SLAP/1X+E12.5/(1X10F12.5))
197.      FORMAT (10I,40X,40HITS TEMP PRES&MVT EQUIL FR MASRAI FR SCALF&NAT10195
198.      1 /101T5,7H MASRAI))
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1.  SUBROUTINE FALZ
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4.  REAL MFIAC(1),MFEI(1),EFFI(1),TMAU(1,10)
5.  EQUIVALENCE (MFIAC(1),A(1)), (MFEI(1),A(3)), (EFFI(1),A(101)),
6.  TMAU(1),A(151))
7.  DIMENSION TFI(150),CIJ(180,1)
8.  DIMENSION X(1),VNU(180,1)
9.
10. COMMON /PARAM1/ FAFGA(180),FAFOR(180),KR(180,2),RE(180,2),
11. RU(180,2),REI(80,2),PF(180,2),TU(180,2),VN(180),
12. Y(180),VTM(180),VNU(180,10),FF(180),IFC(180),
13. YI(180),CP(180),H(180),SB(180),TC(180),VLNK(180),
14. FI(180),LAMI(180),GAEK(1,1)
15.
16. COMMON /PARAM2/ KIN,KOUT,JAM,MOL,NAR,IDC,N,KKX(3),KR(10),TITLE(3),
17. TTMIN,TTMAX,VISC,PAR(1)
18.
19. COMMON /PARAM3/ NM,SCH,RHO,VEL,H1,HFF,FFA,IS,ISP,P,T,SIP,HIP,
20. EL,ENL,FLIQ,NG,IFL,ISPG,KKALP,CPF,IRE,IER,IAA,ITS,
21. IN,IL,IT,MODE,HMELT,SMELT,TMAX,TMIN,WELT,SUMN,
22. SUML,JC,H6,CPG,SVA,SVA,SVC,SVD,SUMC,NXC,SAL,
23. VMACH,KRZ2,SP1,GAM,THI,MX,DMCHT,HCH,NCV,TAT,
24. IPRZ,MOAT,SRI,IXG,SV1,KKJ,IXC,NXG,SW1,MOATO,
25. SA2,FFAWS,RV,CMF,VA,HOS,LUH1,DUM2,EP,IFCJC,
26. ISP2,ATG,VAL2,WT
27.
28. COMMON /ARRAYS/ AT(16),R(16),W(3),XC(50),XG(50),ZKF(10),
29. TIO(10),DMCLO(10),WALJP(10),EB(10),ALP(10),
30. GAM(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
31. IR(10),TOAT(10),KAT(10),UM(10,10),EBL(10)
32.
33. EQUIVALENCE (TU(183),TF(1)), (VNU(1),CIJ(1))
34.
35. COMMON /KINELIX/ MT,FKE(50),EAK(50),FXK(50),PMU(10,50),RMU(10,50),
36. PWR(50),PKKK(50)
37.
38. EQUIVALENCE (B(1),X(1)), (GANK(1),VLAM(1))
39.
40. COMMON /DIFFER/ TF(11),PMU(10),PNUS(10),SLAM(10),BE(10),BY(10),
41. TFC(10),JJC(10),SLB(16),SLA(16,16)
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55. IF (IFC(J)) 70.345.105
56. IF (IFC(J)+1) 345.30.30
57. IF (ITS) 50.35.50
58. VA(J)=VN(J)/SUMC
59. IF (IFC(J)) 50.45.40
60. IF (SUMC .EQ. 0.0) VN(J)=VN(J)/SUMC
61. IF (SUMC .EQ. 0.0) VN(J)=0.0
62. GO TO 50
63. V(J)=Y(J)-SUMC
64. F(J)=V(LK(J))-Y(J)
65. DO 65 I=1,IS
66. IF (IFC(I)) 60.60.55
67. FNU(I)=0.
68. GO TO 45
69. FNU(I)=VN(I)*(J,I)
70. E(J)=E(J)+FNU(I)*V(I)
71. CONTINUE
72. EAP=ABS(E(J))
73. IF (IFC(J)) 70.250.105
74. COMPENSED SPECIES
75. FAB=E(J)
76. IF (KR(I)) 45.75.75
77. IF (1-IF(J)*.001) 80.85.85
78. FAB=0.
79. IF (KR(5)) 195.195.205
80. IF (E(J) - EER) 195.195.90
81. FFP=E(J)
82. IF (IFP) 95.95.100
83. ISPO=ISPO+1
84. IF=ISPO
85. IF=IFN
86. IF=IK
87. GO TO 110
88. ISPO=ISPO+1
89. IF=ISPO
90. WT=0.
91. IF (KR(5)) 120.115.115
92. TMIN=MAX1(TE(J),TMIN)
93. WTR=WTN(J)/WTG
94. DO 125 I=1,ISPO
95. A(I,IF)=0.
96. A(TE,I)=0.
97. DO 140 K=1,IS
98. PUN1=VNU(J,K)
99. IF (IFC(K)-1) 130.130.140
100. VA=0.001*V(K)
101. A(K+2,IC)=PUN1-WTR*(PNU(K) +GAMF(K)*WTG)
102. KF(K)=KE(K)-VA
103. IF (ABS(VA) - ER(K)) 140.140.135
104. ED(K)=ABS(VA)
105. TS(K)=IK
106. CONTINUE
107. K=TE-ISP2
108. IF (IK=0) 165.165.145
109. JK(K)=JC
110. A(TE)=Y(JC)
111. IF (JC-IS) 155.155.150

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112.	150	ATF(J)=TC(JC)	WAT20111
113.		RTF(J)=JC	WAT20112
114.	155	FFJ=Z(JF)	WAT20113
115.		IF (H(JC) 375,375,160	WAT20114
116.	160	FA=AS(FA)	WAT20115
117.		GO TO 375	WAT20116
118.	165	AKO=J	WAT20117
119.		ATF(J)=TC(J)	WAT20118
120.		RTF(J)=JC	WAT20119
121.	170	IF (T+COI-TC(J)) 175,175,170	WAT20120
122.		IF (K(J)) 190,190,200	WAT20121
123.	175	IF (K(J) - 1) 180,185,186	WAT20122
124.	180	IF (K(J)) 190,185,185	WAT20123
125.	185	ATF(J)=1,0+10	WAT20124
126.		RTF(J)=1/6(J)+J,0(J)+10	WAT20125
127.	190	DOF=0	WAT20126
128.		IF (K(J) - 2) 195,195,240	WAT20127
129.	195	IF (K(J) - 1) 375,300,375	WAT20128
130.	200	IF (T-TC(J)-COI) 205,205,220	WAT20129
131.	205	IF (JC) 215,215,210	WAT20130
132.	210	IF (K(J)-COI) 365,365,215	WAT20131
133.	215	FA=0(J)	WAT20132
134.		JC=IF	WAT20133
135.		TC(J)=TC(JC)	WAT20134
136.		TA=TC(J)	WAT20135
137.	220	IF (K(J)) 225,225,220	WAT20136
138.		IF (K(J)-2) 365,225,210	WAT20137
139.	225	K(J)=JC	WAT20138
140.		DO 230 K=1,15	WAT20139
141.	230	ATF(J+2)=TC(JC)	WAT20140
142.		RTF(J)=TC(J)	WAT20141
143.		GO TO 365	WAT20142
144.	235	HOS=H(J)	WAT20143
145.		GO TO 345	WAT20144
146.	240	HOS=H(J)	WAT20145
147.	245	ATF(J)=HOS	WAT20146
148.		ATF(J)=ATF(J)-VL(J)*HOS	WAT20147
149.		CPE=CPFC(J)*H(J)	WAT20148
150.		GO TO 375	WAT20149
151.	C	605 PLAS SPEC DS	WAT20150
152.	250	IF (J)=0	WAT20151
153.		IF (V(J)) 255,375,255	WAT20152
154.	255	TC=0	WAT20153
155.		CPE=CPFC(J)*H(J)	WAT20154
156.		IF (K(J)) 265,260,265	WAT20155
157.	260	FFJ=FF(J)	WAT20156
158.	265	RTF(J)=TC(J)*H(J)	WAT20157
159.		DO 270 K=1,11	WAT20158
160.		IF (K(J)) 270,270,285	WAT20159
161.	270	IF (K(J)) 275,275,290	WAT20160
162.	275	DOF=0	WAT20161
163.		FFJ=1,0	WAT20162
164.		GO TO 285	WAT20163
165.	280	RTF(J)=TC(J)-FF(J)	WAT20164
166.	285	GO 290 RTF(J)	WAT20165
167.		TC=TC(K)	WAT20166
168.		VA=V(J)-2*ATF(J)	WAT20167

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169. IF (KAT(K1)-99) 260,305,290
170. IF (K0(F1) 305,306,295
171. VA=VA+V*VF(J)*VF(J,I - 2) + G*VF(I - 2) * u(J)
172. VF(I - 2)=VF(I - 2)-VA
173. ACSV=ACSV(VA)
174. VA=VA+P*VF(I - 2)*VF(I - 2)
175. GO TO 310
176. VF=VA+VF(J)
177. VA=VA+VA*VF
178. VF(I - 2)=VF(I - 2)-VA
179. ACSV=ACSV(VA)
180. VA=VA+VA*VF(I - 2)*VF(I - 2)+P*VF(I - 2)
181. GO TO 310
182. VF(I - 2)=VF(I - 2)-VA
183. ACSV=ACSV(VA)
184. IF (ACSV - FUL(I - 2)) 320,320,315
185. I=I+1
186. IF (ACSV - FUL(I - 2)) 330,330,325
187. IF (ACSV(VI) - FUL(I - 2)) 340,340,330
188. FUL(I - 2)=ACSV
189. I=I - 2=I
190. DO 345 K=1,ISF2
191. A(I,K)=A(I,K)+V*VF(I,K - 2)
192. P(I)=P(I)-V*VF(I)
193. A(I,1)=A(I,1)-V*VF(I)
194. A(I,1)=A(I,1)+VF(I)*FNU(I - 2)
195. CTIME=CTIME+VF(I)*FNU(I - 2)
196. IF (IC) 375,375,345
197. FP=FP-VF(I)
198. F(I)=1
199. F(I)=R(I)-V*VF(I)*F(I)
200. A(I,1)=A(I,1)-VF(I)*F(I)
201. IF (MOIE - 2) 370,350,355
202. HOS=H(I)*VF(I)
203. GO TO 360
204. HOS=VH(I)*(SF(I) - 1.9669 * Y(I) - 1.9669)
205. DO 365 I=1,ISF2
206. A(I,1)=HOS*FNU(I - 2)+A(I,1)
207. A(I,2)=A(I,2)-HOS
208. A(I,1)=A(I,1)-HOS*VF(I)
209. P(I)=P(I)-HOS*VF(I)
210. CPF=CPF+VH(I)*P(I)
211. IF (FL - FAP) 380,385,345
212. FI=EP
213. J=J+1
214. CONTINUE
215. RETURN
216. FIC

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112. 115 DO 160 IF=TSF3,JSPG
113. IV=IV+1
114. IF (IV - 1) 140,140,120
115. C REDUCE NEW ROW BY PREVIOUS ROWS
116. 120 DO 135 J=2,IV
117. K=I(J - 1)
118. OTV=ATF(K + 2)
119. IF (OTV) 125,135,125
120. ATF(K + 2)=0.
121. JP=J+ISP
122. DO 130 K=3,ISP2
123. ATF(K)=ATF(K)+OTV*ATF(K)
124. CONTINUE
125. C SECK VALID NOT-2E00 ELEMENT
126. 140 DO 150 J=IV,IS
127. K=I(J)
128. IF (ABS(ATF(K + 2)) - .01) 150,150,145
129. IF (IFC(K)) 153,155,150
130. CONTINUE
131. C SINGULAR CONDENSED SET
132. GO TO 165
133. I(J)=I(IV)
134. I(IV)=K
135. OTV=ATF(K + 2)
136. ATF(K + 2)=1.
137. C NORMALIZE NEW ROW
138. DO 160 J=3,ISP2
139. ATF(J)=ATF(J)/IV
140. C COMPLETES FLJOR LOOP=NON SINGULAR
141. GO TO 85
142. C EXTRACT COEFFICIENTS ON SINGULAR SET=POORASE
143. DO 170 J=2,IV
144. K=I(J - 1)
145. AR(J - 1)=ATF(K + 2)
146. AR(IV)=1.
147. C EXTRACT COEFFICIENTS ON SINGULAR SET - BASE
148. DO 185 K=1,IS
149. IF (IFC(K)) 185,185,175
150. IF (ABS(ATF(K + 2)) - .01) 185,185,180
151. IV=IV+1
152. AR(IV)=ATF(K + 2)
153. J(IV)=K
154. CONTINUE
155. C ISOLATE NEW CONDENSED CANDIDATE
156. DO 195 J=1,IV
157. K=J(J)
158. IF (VA(K)) 190,190,195
159. JZ=J
160. KZEK
161. GO TO 200
162. CONTINUE
163. STOP
164. C WHO MUST GO TO ALLOW ENTRY OF NEW CANDIDATE
165. 200 TEST=-1.0F10
166. JX=0
167. DO 220 J=1,IV
168. IF (ABS(AT(J))-.01) 220,220,205

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169. 205 DUM1=AR(J2)/AR(J)
170. IF (DUM1) 210,220,220
171. K=J(J)
172. DUM1=DUM1+VN(K)
173. IF (DUM1 - TEST) 220,220,215
174. TEST=DUM1
175. JX=J
176. KX=K
177. CONTINUE
178. IF (AR(JX) .NE. 0.0) TEST=VN(KX)/AR(JX)
179. IF (AR(JX) .EQ. 0.0) TEST=0.0
180. C DOES NEW CANDIDATE ENTER
181. IF (E(K2) - E(KX)) 85,85,225
182. C YES
183. 225 GO TO 230 J=J+1
184. K=J(J)
185. VN(K)=VN(K)-TEST*AR(J)
186. KR(7)=KR(7)+1
187. VN(KX)=0.
188. KZ=KX
189. JZ=JX
190. GO TO A5
191. C FLTMINATE TERMS CORRESPONDING TO PRESENT RASF CONDENSED
192. DO 250 K=1,IS
193. IF (IFC(K)) 250,250,240
194. 240 GO 245 IE=ISP3,ISP4
195. 245 A(IE,K + 2)=0.
196. CONTINUE
197. IF (J2) 270,270,255
198. C FLY MATRIX TO YIELD SHALL NEG CORRECTION ON ELIMINATED SPECIES
199. IF (KX - IS) 265,265,260
200. KZ=JZ+IS
201. A(KZ + 2,KZ + 2)=1.E+15
202. R(KZ + 2)=1.E+10
203. CONTINUE
204. R(2)=EP+R(2)
205. IF (MODF - 1) 310,290,280
206. IF (ABS(EHS / A(1,1)) - .0001) 310,310,320
207. 285 IF (ABS(R(1)) - 1.E - 4) 310,310,320
208. IF (IFCJC) 295,285,305
209. 295 IF (JC - TRJ) 305,305,300
210. GO TO 285
211. MODE=0
212. TMIN=TTSL
213. TMAX=TTMAX
214. GO TO 285
215. 310 IF (FI - 1.E - 4) 315,315,320
216. 315 IF (FOL - 1.E - 5) 335,335,320
217. 320 IV=ISP2
218. IL=1
219. IF (MODE) 325,325,330
220. 325 IF=ISP2-1
221. IL=2
222. X(1)=0.
223. 330 RETURN
224. 335 IF (MY(9)) 340,340,330
225. 340 TKE=-2

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'A130225
'A130226

GO TO 30
END

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227.

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1. SUBROUTINE PROPS
2. DIMENSION T(1), RHO(1), C(PAR(1)), SC(1), CAPC(1)
3. DIMENSION ZA(10), ZT(10), VK(10), VI(10)
4. COMMON/ACF1/GAMF1,REF1,PCF,ACHS,SCNAC,SXF
5.
6. REAL A(1),REF1(1),FEF1(1),TAU(10,10)
7. EQUIVALENCE (DEF1A(1),A(1)), (DEF1(1),A(5)), (FEF1(1),A(10)),
8. TAU(1),A(10))
9. DIMENSION TE(10),CTJ(10,1)
10. DIMENSION X(1),VLN(10,1)
11.
12. COMMON FCF1A(10),FAF1A(10),REF1(10,2),RC(10,2),
13. RC1(10,2),FE(10,2),SC(10,2),T(10,2),VM(10),
14. Y(10),CTJ(10),VM(10),FE(10),IFC(10),
15. IP(10),CP(10),H(10),SC(10),TC(10),VLN(10),
16. F(10),LMT(10),GAMP(1,1)
17.
18. COMMON /PAF1A/ KTN,KOUT,JAN,NOL,NAR,IDC,N,KKX(3),KF(10),TILF(3),
19. TTMIN,TTMAX,VISC,PR(1)
20.
21. COMMON /PAS1A/2/ WM,SCN,RHO,VEL,R1,REF,FEA,TS,ISP,P,1,SIP,MIP,
22. FL,ENL,FL10,10,IFL,ISP,G,KFALP,CPE,IFE,IER,AA,TTT,
23. IN,IL,IT,MOFE,MPFELT,SUELI,TAX,TMID,MELT,SUMN,
24. SUML,JP,HG,CPE,SVA,SVC,SVD,SUMC,FXC,SAT,
25. VMACH,KOZZ,SP1,GA,TH,IX,DMCHT,HCH,KCV,TH,
26. IER2,IGAT,CR1,IXG,SV1,PKJ,IXC,XXG,SH1,IGATO,
27. S12,FEF,KS,RY,CNF,VA,HOS,DMW1,NUM2,EP,IFCJC,
28. ISP2,ATG,VNU2,ATL
29.
30. COMMON /APRAYS/ A(16,16),P(16),W(3),XC(50),XG(50),ZKE(10),
31. T(10),DMCLO(10),UAL,JP(10),FR(10),ALP(10),
32. GAVH(10),GAMF(10),TG(10,3),TK(10,3),WAT(10),
33. IR(10),IOAT(10),KAT(10),UM(10,10),FBL(10)
34. EQUIVALENCE (NUC(1),TE(1)), (VNU(1),C(1))
35.
36. COMMON /MTFEX/ MT,FKE(50),FAK(50),FKK(50),PRU(10,50),PMU(10,50),
37. PMR(50),PKKK(50)
38.
39. EQUIVALENCE (P(1),X(1)), (GAMK(1),VIAP(1))
40.
41. COMMON /DIFFER/ IR(11),FRU(10),PRUS(10),SLAM(10),RE(10),RY(10),
42. IPC(10),JU(10),SLB(16),SLA(16,16)
43.
44. ALF=A(2,1)/A(1,1)
45. CSP=1./A(1,1)*AA
46. IF (MODE - 3) 5,10,5
47. CSP=CSP/T
48. RETAS=P(A(2,2) - A(1,2) / A(1,1) * A(2,1))-1.
49. GAMP=1.-ALF
50. GAMP=1./11.*RETA-1.9869/AA*GAMP/CSP*GAMP*P
51. IF (NR(5)) 15,20,15
52. GAMP=GAMP
53. ITS=-1
54. HMY=0.

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55. CAPC(1)=1.
56. I1=1
57. WM=AA/P
58. IS=IS-1
59. TT(1)=T*1.8
60. RHO(1)=AA/(1.3146 * T)
61. CBRK(1)=CPF
62. ASTR=1.15
63. FORM NECESSARY SUMMATIONS
64. PKU2=0.
65. CPTIL=0.
66. HTIL=0.
67. HTZ=0.
68. PKU2=0.
69. PKU1=0.
70. TKU3=0.
71. CGG=0.
72. CGGPR=0.
73. IER=0
74. IF=0
75. DO 55 K=1,15
76. WK(K)=0.
77. ZK(K)=0.
78. IF (WAT(K)-0.1) 25,30,30
79. IF=K
80. IF (IFC(K)) 35,40,45
81. IF (KR(6)) 40,55,55
82. IF (WTK(K)-0.1) 50,50,45
83. 45 ZK(K)=VN(K)/EF(K)
84. 50 WK(K)=VN(K)
85. 55 CONTINUE
86. I=1
87. DO 85 IK=1,N
88. IF (WTK(I)-0.1) 60,75,75
89. IF=IK
90. ME=H(I)
91. WTE=VTK(I)
92. CPE=CP(I)
93. H(I)=0.
94. WTK(I)=0.
95. CP(I)=0.
96. IF (IK-IS) 85,85,65
97. DO 70 K=1,15
98. WK(K)=WK(K)+V(I)*V(I)*T,4
99. GO TO 85
100. 75 IF (IFC(I)) 85,80,85
101. 80 PKU1=PKU1+V(I)*EF(I)*.01/.66/ME X
102. I=I+1
103. V(I)=PKU1/P
104. PKU5=0.
105. PKU6=0.
106. WZ=1.385
107. WD=1.2*ASTR/PMU1
108. WZ=WD7/PMU1-PM2
109. WU=0.284*WZ
110. W05=0.32*WZ/PMU1
111. WD=WD4/PMU1+0.5

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C
25. IF (WAT(K)-0.1) 25,30,30
30. IF (IFC(K)) 35,40,45
35. IF (KR(6)) 40,55,55
40. IF (WTK(K)-0.1) 50,50,45
45. ZK(K)=VN(K)/EF(K)
50. WK(K)=VN(K)
55. CONTINUE
60. IF (WTK(I)-0.1) 60,75,75
65. IF=IK
70. WK(K)=WK(K)+V(I)*V(I)*T,4
75. IF (IFC(I)) 85,80,85
80. PKU1=PKU1+V(I)*EF(I)*.01/.66/ME X
85. I=I+1

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112. I=1
113. DO 165 I=1,N
114. IF (IFC(I)) 165,95,90
115. IF (K0(6)) 95,165,165
116. IF (WTM(I)-0.1) 165,100,100
117. VA=VA*(I)/EFF(I)
118. IF (IFR) 130,150,105
119. IF (IK-IS) 110,110,115
120. CEJ=CEJ*(I,I)
121. GO TO 125
122. CEJ=0.
123. DO 120 K=1,IS
124. CEJ=CEJ+VNU(I,K)*CIJ(IF,K)
125. HTI=HTI-CEJ*HE
126. CP(I)=CP(I)-CEJ*CPH
127. WT(I)=WT(I)-CEJ*WTE
128. VC=VA*HTI*(I)
129. P*G2=PHI2+VU
130. HT2=HT2+VA*HT(I)
131. IF (IK-IS) 145,145,135
132. DO 140 K=1,IS
133. VK(K)=VK(K)+VNU(I)*VNU(I,K)
134. VK(K)=ZK(K)+VA*VNU(I,K)
135. FFT=FF(I)
136. IF (IFC(I)) 155,150,155
137. FFT=FF(I)*(1./60*FX)
138. VA=VN(I)/FFI
139. VU=VA*VNU(I)
140. VC=VN(I)*EFFI
141. PH2=PH2+VU
142. T*U3=1.0/3+VA
143. CFTI=VA*CP(I)*CFTI
144. HTI=HTI+VA*HT(I)
145. CPG=CPG+VU(I)*CP(I)
146. H*U5=H*U5+VU(I)*H(I)
147. A*U5=A*U5+VA/(PH2 -VC * W07 )
148. P*U6=P*U6+VA/(1.04 -VC * X08 )
149. IF (IFC(I)) 165,160,165
150. CPGH=CPGH+VU(I)*CP(I)
151. T*U4
152. V*U5=A*U5/AA
153. V*U6=(PH2 + CFTI / 1.9060 - 2.5 * T*U3)/P
154. PH2=PH2/P
155. V*U3=1.0/3+PH2
156. HT2=HT2/PH2*1.0
157. DO 170 K=1,IS
158. VK(K)=VK(K)/AA*W07(K)
159. ZK(K)=ZK(K)/PH2*W07(K)
160. WT(I)=0.
161. VT(I)=0.
162. DO 175 K=1,IS
163. VT(I)=VT(I)+CIJ(K,T)*VK(K)/WTM(K)*WAT(I)
164. ZI(I)=ZI(I)+CIJ(K,T)*ZK(K)/WTM(K)*WAT(I)
165. CPG=CPG/AA
166. CPH=CPH/AA
167. H*U5=H*U5/AA
168.

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169. CPTIL=CPTIL/PMU2
170. HTIL=HTIL/PMU2*1.8
171. OMEGA=1.07/(1 + 106.7)*0.159
172. OMEGA=9.16F-AT/PSORT(T)/OMEGA
173. VU=KHO(T)*OMEGA*VNU1
174. TCOND=KHO(T)*OMEGA*VNU6/VNU1*1.069
175. SC(1)=VNU5/VNU2*%K
176. PR(T)=CPA*PR/VNU6*VNU5/1.946*%JM
177. IF (KKJ) 205,205,180
178. GAME=GAME-1.0
179. SCMAK=(HCH-HK%)/GA*1.0065/T*%K
180. PSP=((1-6GAPE/2)*SQMAK)/(1+.6GAPE/2)*ACHSG))*((CAM/GAPE)
181. IF (ABS(PSP-1.0)-1.E-4) 200,200,185
182. IF (KKJ-10) 190,190,195
183. P=P*PSP
184. AA=P*%P
185. KKJ=KKJ+1
186. ITSEIT
187. GO TO 240
188. NCV=1
189. KKJ=0
190. IF (PCV) 215,215,210
191. WRITE (KOUT,255) TILF
192. GO TO 225
193. IF (KK(101/2 + KP(7) + KP(2) + PR(3)) 225,225,220
194. WRITE (KOUT,250) TILF
195. IF (K(61)) 226,227,227
196. WRITE (KOUT,245) CP6,CSP,ALF,RETA,6AMP
197. GO TO 229
198. WRITE (KOUT,228) CPG
199. FORMAT(10X,11H CP-FROZEN= ,F12.5)
200. CONTINUE
201. VU12=VNU1*VNU2
202. IF (KKX(1)-4) 235,235,235
203. HML=HML*1.8
204. PUNCH 260. HML, TT, WM, CSP, ALF, VNU, PR
205. CONTINUE
206. WRITE (KOUT,265) TT,VNU,TCND,DRAR,PR,SC,VNU1,VNU2,WM,HTIL,CPTIL
207. 1 ,HTZ
208. WRITE (KOUT,275) GAMEX,(KAT(J),J=1,IS)
209. WRITE (KOUT,270) (VI(J),J=1,IS)
210. WRITE (KOUT,270) (ZI(J),J=1,IS)
211. RETURN
212. C
213. FORMAT (/27H DERIVATIVE PROPERTY OUTPUT,/,57H CP-FROZEN CP-EQUILIPROPN20A
214. 1L DLM/FLAT DLM/CLIP GAMMA,/,5E12.5)
215. FORMAT (14,11X,45HGRAPHITE SURFACE KINETICS (GASKET) SOLUTION 5X PROPN210
216. 1 2A4,A2//)
217. FORMAT (4H1-----FOLLOWING OUTPUT NON-CONVERGENT-----PROPN212
218. 1-- 2A4,A2//)
219. FORMAT (6F12.5,F8.4)
220. FORMAT (/54H PROPERTY ROUTINE OUTPUT IN LR-MASS,FT-SEC,BTH,AND DEPROPN215
221. 1C-R /67H TEMP VISC COND DRAR
222. 2 SC/6E12.5,/,57H MU1 MU2 MOL.WT
223. 3L CPTIL,XSHHTIL,/,6E12.5)
224. FORMAT (1X10E12.5)
225. FORMAT (/54H ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . ,PROPN220

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227.

1 . . 9H (CA4FA =Ff.3.1H)/1X10(4XI3.5X1)
END

PK0P0221
PK0P0222

[illegible]

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55.      TRC(J)=TRC(J - 1)
56.      TRC(J - 1)=JA
57.      K=1
58.      GO TO 20
59.      IR(J)=1000
60.      CONTINUE
61.      IF (K) 25,25,5
62.      TRC(J5 + 1)=10000
63.      M=TRC(J)
64.      M1=1
65.      L=TS+2
66.      L=0
67.      LL=1
68.      LIP=M+K*(2)
69.      DO 240 IK=1,LL
70.      I=1+1
71.      IF (IK - IS) 30,30,45
72.      SLAN(I)=0.
73.      TRC(I)=IFC(I)
74.      PMS(I)=0.
75.      IF (IK(I) - 1) 35,35,75
76.      DYI=X(I + 2)
77.      IF (IFC(I) + 1) 275,40,40
78.      IF (IFC(I)) 205,95,230
79.      IF (IFC(I) + 1) 75,50,50
80.      IF (IFC(I)) 70,55,45
81.      VA=E(I)-T(I)*Y(I)
82.      DO 65 J=1,JS
83.      IF (IRC(J)) 60,60,65
84.      VA=VA+VNU(I,J)*X(J + 2)
85.      CONTINUE
86.      DYI=VA
87.      GO TO 95
88.      IF (IK - TRC) 75,60,75
89.      DYI=0.
90.      GO TO 275
91.      IFC(I)=1
92.      DYI=X(IER)
93.      GO TO 230
94.      I=I+1
95.      IF (L - IER) 90,85,90
96.      DYI=X(I)
97.      GO TO 230
98.      DATG=D+TR+V(I)*DYI*WTM(I)
99.      IF (IP(I)) 100,195,100
100.      IF (IK - N) 105,145,105
101.      IF (V(I) - NUMP) 110,140,140
102.      IF (NOF) 195,195,115
103.      IF (DYI) 120,275,125
104.      IF (V(I) / RUMP - .9999995 - CMF * DYI) 275,275,130
105.      IF (V(I) / RUMP - 1. - CMF * DYI) 135,275,275
106.      CMF=(V(I) / RUMP - .9999995)/DYI
107.      GO TO 275
108.      CMF=(RUMP / V(I) - 1.)/DYI
109.      GO TO 275
110.      IF (NOF) 175,175,150
111.      M1=M1+1

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SCAL0110
SCAL0111

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112. M=IR(M1)
113. IF (DY1) 155,275,160
114. IF (DY1 * CMF + .999) 165,275,275
115. IF (DY1 * CMF - 9.) 275,275,170
116. CMF=-.999/DY1
117. GO TO 275
118. CMF=9./DY1
119. GO TO 275
120. IF (DY1 * CMF - 2.303) 180,190,190
121. IF (DY1 * CMF + 6.909) 185,275,275
122. CMF=-6.909/DY1
123. GO TO 275
124. CMF=2.303/DY1
125. GO TO 275
126. IF (Y(I) - RULP + ARS(DY1) * CMF) 275,200,200
127. CMF=-Y(I) - RULP/ARS(DY1)
128. GO TO 275
129. NON-PRESENT BASE
130. IF (KR(6)) 215,210,210
131. IF (T - TE(I) + .001) 275,215,215
132. IF (Y(I) + CMF * DY1 - 0.1) 275,220,220
133. DUM1=(.1 - Y(I))/DY1
134. IF (DUM1 - .001) 275,275,225
135. CMF=DUM1
136. GO TO 275
137. DWTL=DWTL+DY1*WTF(I)
138. IF (DY1) 235,275,250
139. IF (VW(I)) 250,250,240
140. IF (VW(I) + DY1 * CMF) 245,250,250
141. CMF=-VW(I)/DY1+1.00001
142. IF (KR(6)) 265,255,255
143. CLIP=ARS(CLIP/WTF(I))
144. IF (ARS(CMF * DY1) - CLIP) 275,275,260
145. CMF=CLIP/ARS(DY1)
146. GO TO 275
147. IF (ARS(CMF * DY1) - P) 275,275,270
148. CMF=P/ARS(DY1)
149. CMF(I)=CMF
150. DY(IK)=DY1
151. IF (KR(6)) 290,285,285
152. RUL=ARMAX(1.1,RV/2.)
153. CMF=ARMAX(CMF,WTF / ARS(ABS(DWTL - DWTG / WTE * WTL) / RVL - DWTG))
154. IF (KR(7)-1) 300,300,295
155. NO=1
156. WRITE (KOUT,350) (FARNG(J),VW(J),Y(J),DYA(J,LL),CMFF(J),F(J),IFC(J),J=1,NO)
157. IF (J=1,NO)
158. WRITE (KOUT,360) (FR(I),I=1,IS)
159. WRITE (KOUT,360) (X(I),I=1,IS)
160. WRITE (KOUT,355) (TR(I),I=1,IS)
161. CONTINUE
162. IF (X(I)) 305,345,305
163. X1=X(I)*C*F
164. ARX=ARS(X(I))
165. IF (ARS(X1) - .5) 315,315,310
166. CMF=.5/ARY
167. X1=CMF*X(I)
168.

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SCAL0112
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169. 315 IF (X1) 325,345,320
170. 320 TP=TMAX
171. X1=ATM1(.2,X1)
172. GO TO 330
173. 325 TP=TM10
174. X1=AMAX1(-0.2,X1)
175. 330 OTR=(TM - T)/(TP * X1)
176. IF (OTR - 1.) 335,340,340
177. 335 CPE=OTR*C-F
178. T=TP
179. GO TO 345
180. T=T/(1. - X1)
181. 345 AA=AA*EXP(CMF * X(2))
182. RETURN
183. C
184. -350 FORMAT (1X2(1X2H0.9X1HY8Y2H0Y7X5HSCAL E7X1)H4X5H1FC 1P)/(1X40,5E
185. 1 10,3,13,12,1X,44,5E10,3,13,12))
186. 355 FORMAT (10I5)
187. 360 FORMAT (8F12.4)
188. END
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SCAL0188

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SECTION 3

SAMPLE PROBLEMS

Presented in this section are three sample problems which were run on a Univac 1108 digital computer. An attempt was made to utilize almost all of the options available in the GASKET2 program. For each sample problem, the following is presented:

- A brief description of the nature of the problem and solution
- A listing of the input data deck
- A few typical pages of the program output

Sample Problem 1

In this problem, ablation rates at the throat of a rocket nozzle are calculated. The propellant gases are comprised of seven elements, including both hydrogen and oxygen. The surface material option of ATJ bulk graphite is used. The program options which utilize built-in physical data are selected; hence, only 10 cards of input data are required for the complete sequence of calculations. The ideal chamber conditions (propellant flame temperature of 3764°K, ideal pressure of 68.02 atm) are input. After redefining the elemental set to include the fictitious element "GRAPHITE," subsequent calculations performed by the program include determination of the actual chamber state (54.42 atm) and an isentropic expansion to the throat (unity Mach no.). The frozen edge state is computed for the built-in array of eight temperatures, and the surface ablation rate is computed for the built-in array of fifteen surface temperatures.

Listing of Input

1.	3005110600	3764.	54.42	-1.0	68.02	0.969	0.
2.	7						
3.	1	HYDROGEN	1.008	3.3192			
4.	4	BERYLLIUM	9.012	1.4265			
5.	6	CARBON	12.011	0.9236		1.0	
6.	7	NITROGEN	14.007	0.8342			
7.	8	OXYGEN	16.0	1.9161			
8.	9	FLUORINE	19.0	0.8680			
9.	17	CHLORINE	35.453	0.4012			
10.	8						

Sample Problem 1 Output

GRAPHITE SURFACE KINETICS (GASKET) PROG. 1

0110000+00

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00500	.0330797	.0000000
4	BERYLLIUM	9.01200	.0142129	.0000000
6	CARBON	12.01100	.0092023	.0000000
7	NITROGEN	14.00700	.0063215	.0000000
8	OXYGEN	16.00000	.0190910	.0000000
9	FLUORINE	19.00000	.0086483	.0000000
17	CHLORINE	35.45300	.0039973	.0000000
106	GRAPHITE	12.01100	.0000000	.0032570

ELEMENTS	HYDROGEN	BERYLLIUM	CARBON	NITROGEN	OXYGEN
	FLUORINE	CHLORINE	GRAPHITE		

BASE SPECIES	H2	BE	CO2	CCLH	H2O
	PH	CLH	C*		

Sample Problem 1 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROB. 1

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DLNW/DLNT	DLNW/DLNP	GAMMA
.49545+00	.12580+01	-.57602+00	.35229+01	.11334+01

PROPERTY ROUTINE OUTPUT IN

TEMP	VISS	COND	DBAR	PR	SC
.67752+04	.61615+04	.75106+04	.23259+03	.51461+00	.72427+00
MU1	MU2	POL.WT	HTIL	CPTIL	HTIL*
.77603+00	.20648+02	.25599+02	.42582+04	.86999+00	.23844+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER (GAMEX = .667)

1	4	6	7	9	17	104
.33335+01	.12809+00	.11053+00	.11656+00	.30546+00	.16432+00	.00000
.89675+01	.69022+01	.13622+00	.14390+00	.23118+00	.14498+00	.00000

SOLUTION TIMES

ITERATIONS = 32

TIME = 9.2A7 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS =	.21215+00
TEMP = 6775.2000 DEG R.	= 3764.0000 DEG K.
PRESS =	68.02000 ATM

ENTHALPY - BTU/LRM	GAS	CONDENSED	COMPOSITE
ENTROPY - BTU/LRM DEG R	.24931+03	-.54624+04	-.78736+03
DENSITY - LRM/FT3	.24060+01	.15349+01	.25855+01
MOLECULAR WEIGHT	.29030+00	.35189+00	.35189+00
	21.114	25.0120	25.5946

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.28681-02	H2	.51374+00	H2O	.52155+01	CO	.00000
FM	.26427-01	BE	.37865-02	CCL4	.85119+07	C2H2	.31456+07
C	.12442-04	C2	.66064+10	C3	.21189+12	C4	.84802+18
C2BE	.74619+09	HECL	.37108+02	HECLF	.36218+01	3ECL2	.82985+02
REF2	.40610-01	HEMO	.66279+02	HEM2	.19498+03	3EH2O2	.36210+02
BE2CL4	.35445+07	HE2O2	.27032+03	HE3O3	.24759+03	HE4O4	.85633+04
BE6O6	.20125+06	CCL	.36754+08	CCLF0	.54481+09	CCLF3	.79560+17
CCL3F	.43880+17	CCL4	.12540+17	CF	.21456+07	CF4	.44796+08
CF2O	.42082+09	CF3	.70361+14	CF4	.41132+17	CH	.10493+06
CHCL2F	.86493+14	CHCL3	.47047+14	CHFO	.79573+07	CHF3	.44654+14
CHNO	.95549+06	CHO	.45571+04	CH2	.57441+07	CH2CLF	.24644+11
CH2F2	.10232+11	CH2O	.27401+05	CH3	.44354+06	CH3CL	.10870+08
CH4	.97096+07	CN	.24543+05	C2F2	.14879+15	C2F4	.28364+22
C2H4O	.19663+14	C2H2	.24440+09	C3O2	.41003+10	C4H2	.75546+17
CLF	.84849+07	CLF03	.60026+24	CLF3	.87612+21	CLH0	.17413+05
ClO	.15244+05	ClO2	.89297+11	CL2O	.85230+11	F	.11110+03
FN	.68111+08	FNO	.10759+08	FO	.39131+08	F2O	.52961+15
H	.69679+01	HN	.40321+04	HO	.38114+02	H2N	.24586+04
H3N	.18218+04	HNF2	.45197+11	N	.27902+04	NO	.36568+03
N2O	.58770+07	N2O3	.10572+15	N2O4	.28330+21	N2O5	.17632+25
O3	.22818+11	CCL2F2	.72649+17	CCL0	.51757+05	CF0	.14886+06
FN02	.41704+14	CLN02	.41138+13	F2N	.62872+13	FN03	.19497+20
BEH	.17145+04	HN02	.20359+08	HN03	.18560+13	RE2O	.10682+02
HO2	.12061+06	NO3	.47587+14	CF4O	.84379+23	CCL2	.82626+10
F2N2	.42902+17	H2N2	.28486+08	RE2F2O	.17103+01	CH2	.88652+09
CLF5	.11751+36	HEH	.65441+15	FO2	.24159+11	C2H	.12570+07
C2CL4	.12864+20	C2CL6	.28053+30	C2HF	.67411+11	C2CL2	.17562+12
CHCL	.40746+08	CHF	.35408+08	C2F3N	.17697+19	F3N0	.16489+24
CL2	.30764+05	N2	.10623+00	O2	.14692+04	CNO	.14911+06
C2H3	.71395+10	C2H6	.84166+14	C3H	.61907+11	C3H2	.56004+12
C3H4	.45045+14	C3H5	.20283+13	C4H	.34384+14	C4H2	.57922+15
CL4H4N04*	.00000	HEW2O2*	.00000	HE*	.00000	HEO*	.17912+00
BE3N2*	.00000	BECL2*	.00000	HEF2*	.00000		

Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROP. 1      2000200+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLNM/DLNT      DLNM/DLNP      GAMMA
.49506+00      .13039+01      -.60504+00      .36699-01      .11327+01

PROPERTY ROUTINE OUTPUT IN LB-MASS,FT,SEC,RTU,AND DEG-R
TEMP      VISC      COND      DBAR      PR      SC
.67212+04      .61287-04      .74620-04      .28689-03      .31494+00      .72426+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.77499+00      .20619+02      .25514+02      .43013+04      .A6896+00      .24063+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      2      3      4      5      6      7      8      9      10      11      12      13      14      15      16      17      18      19      20
.33335-01      .12809+00      .11053+00      .11656+00      .30546+00      .16432+00      .14172+00      .00000
.89982-01      .69338-01      .13601+00      .1436A+00      .23836+00      .17807+00      .14496+00      .00000

SOLUTION TIMES
ITERATIONS = 3      TIME = 1.249 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .21195+00
TEMP = 6721.2491 DEG R. = 3734.0273 DEG K.      PRESS = 54.42000 ATM

ENTHALPY - BTU/LBM      GAS      CONDENSED      COMPOSITE
.29254+03      -.58969+04      -.78736+03
ENTROPY - BTU/LBM DEG R      .2A272+01      .15297+01      .26009+01
DENSITY - LBM/FT3      .23351+00      .282A6+00      .25.5143
MOLECULAR WEIGHT      21.0627      25.0120      25.5143

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES)....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
C02      .291A3-02      H2      .31040+00      H2O      .32357-01      C*      .00000      CLH      .40019-01
FH      .26414-01      BE      .40393-02      CCLN      .67381-07      CO      .23178+00      CLM2      .19219-07
C      .10445-06      C2      .43A31-10      C3      .1154A-12      C4      .35696-18      C5      .31440-21
C2BE      .49368-09      BECL      .37338-02      HECLF      .3572A-01      HECL2      .A1426-02      REF      .44293-01
REF2      .40808-01      REMO      .6727A-02      REM2      .17333-03      REMO4      .375A2-02      REO      .27294-03
RE2CL4      .27308-07      HE2O2      .243A6-03      RE3O3      .27990-03      HE3O5      .35546-05
BE6O6      .23314-06      CCL      .28A17-0A      CCLFO      .46249-09      CCL2O      .19074-09
CCL3F      .269A8-17      CCL4      .770A2-1A      CF      .17226-07      CFH      .33543-0A      CF2      .A9300-10
CF2O      .33469-09      CF3      .47004-14      CF4      .25784-17      CH      .A1195-07      CHCLF2      .60000-14
CHCL2F      .541A4-14      CHCL3      .29411-14      CHF0      .63030-07      CHF3      .27583-14      CHN      .39842-04
CHNO      .75218-06      CHO      .38831-04      CH2      .42021-07      CH2CLF      .1A030-11      CH2CL2      .23708-11
CH2F2      .643A3-12      CH2O      .21617-05      CH3      .30546-06      CH3CL      .64674-09      CH3F      .14695-09
CH4      .62909-07      CN      .19843-05      C2F2      .10752-15      C2F4      .13399-22      C2H4      .118A0-10
C2HNO      .97335-15      C2N2      .14962-09      C3O2      .25290-10      C4H2      .28097-17      CL      .620A3-02
CLF      .79011-07      CLFO3      .47634-24      CLF3      .58176-21      CLHO      .16440-05      CLNO      .16589-07
CLO      .15549-05      CLO2      .86633-11      CL2O      .76640-11      F      .11359-03      FHO      .12099-07
FN      .59609-0A      FNO      .97331-09      FO      .37407-08      F2O      .43854-15      F3N      .16507-19
H      .73024-01      HN      .36701-04      HO      .40034-02      H2      .25088-04      H2O2      .50087-07
H3N      .14492-04      H4N2      .27351-11      N      .27506-04      NO      .3A019-03      NO2      .94613-0A
N2O      .54463-07      N2O3      .88768-16      N2O4      .22938-21      N2O5      .13586-25      O      .54542-03
O3      .23779-11      CCL2F2      .44727-05      CFC      .12598-06      C2F6      .26A43-20
FNO2      .36221-14      CLNO2      .36384-13      F2H      .48535-13      FNO3      .15578-20      HNO      .76643-06
HEN      .15949-04      HNO2      .186A9-0A      HNO3      .14144-13      AF2O      .11155-02      HNO2      .79529-33
HO2      .12141-06      NO3      .44848-14      CF4O      .44198-23      CCL2      .60609-10      CCL3      .10845-13
F2N2      .29146-17      H2N2      .21249-08      HE2F2O      .16646-01      CN2      .63233-09      C2O      .17887-07
CLF5      .55342-37      HEH      .50405-15      FO2      .22464-11      C2H      .A1308-0A      C2N      .60477-09
C2CL4      .62617-21      C2CL6      .10766-30      C2HF      .34A15-11      C2CL2      .10515-12      C2HCL      .92043-10
CHCL      .29571-08      CHF      .26186-0A      C2F3H      .A5421-20      F3HO      .11A94-24      F2      .27915-10
CL2      .29698-05      N2      .10589+00      O2      .22352-04      CNO      .12322-06      N3      .66642-09
C2H3      .38503-10      Z2H6      .34929-14      C3H      .31964-11      C3H2      .26160-12      C3H3      .42033-13
C3H4      .17873-14      C3H5      .72244-14      C4H      .15952-14      C4+2      .21827-15      CLH4H*      .00000
CLH4NO4*      .00000      BEH2O2*      .00000      HE*      .00000      9EO*      .17798+00      CRE2*      .00000
RE3N2*      .00000      BECL2*      .00000      REF2*      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASSET) PHON, 1      500100+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN  CP-EQUIL  DLNM/DLNT  DLNM/DLNP  GAMMA
.49587+00  .12511+01  -.54367+00  .31434+01  .11302+01

PROPERTY ROUTINE OUTPUT IN  LH=MASS,FT,SEC+RTU,ATM  OFG=R      SC
TEMP      VISC      CORR      DBAR      PH      SC
.63793+04  .5922+04  .7322+04  .49482+03  .39575+00  .72433+00
MU1      MU2      MUL*WT      HTIL      CPTIL      HTIL*
.77413+00  .20594+02  .25606+02  .3A464+04  .A7149+00  .20679+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . . (GAMEX = .667)
      1      4      6      7      8      9      17      106
.33335-01  .12809+00  .11053+00  .11656+00  .30866+00  .16432+00  .14172+00  .00000
.91019-01  .65809-01  .13771+00  .14546+00  .23345+00  .17956+00  .14659+00  .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = 2.331 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .22523+00
TEMP = 6379.3015 OFG H. = 3544.0564 OFG K.      PRESS = 31.47837 ATM

ENTHALPY - RTU/LHM      GAS      CONDENSED      COMPOSITE
.72630+02      -.61156+04      -.10649+04
ENTROPY - RTU/LHM DEG K      .29496+01      .14963+01      .26004+01
DENSITY - LBM/FT3      .14230+00      .25.0120      .17436+00
MOLECULAR WEIGHT      21.0621      25.0120      25.8059

ABOVE ARE STATIC PROPERTIES      K-KINETIC = .27759+03 HTU/LHM
VEL. = .3724+04 FT/SEC      FLUX = .84496+03 LHM/FT2SEC      MACH = 1.00004

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .27318-02      H2      .32262+00      H2O      .30764+01      C#      .00000
FH      .26684+01      HE      .29799+02      CCLH      .36403+07      CO      .23449+00
C      .49832-07      C2      .12001-10      C3      .24174+13      C4      .51448+19
C2RE      .16436-09      HECL      .28715+02      HECLF      .37215+01      HECL2      .81873-02
HEF2      .44390-01      HEHO      .48529+02      HEH2      .10469+03      HEH2O2      .30026-02
HE2CL4      .15897-07      HE2C2      .19662+03      HEF3O3      .24291+03      HE4O4      .88306+04
RE6O6      .23615-06      CCL      .11200+08      CCLF3O      .25637+09      CCLF3      .14808+17
CCL3F      .75742-18      CCL4      .21567+18      CF      .15868+08      CF#      .37747-10
CF2O      .17744+09      CF3      .10443+14      CF4      .82064+18      CH      .51811-07
CHCL2F      .18370-14      CHCL3      .10163+14      CHEFO      .35444+07      CHE3      .94948+15
CHNO      .43530+06      CHO      .23341+04      CH2      .18336+07      CH2CLF      .71700+12
CH2F2      .25524+12      CH2O      .13182+05      CH3      .15837+06      CH3CL      .34490+09
CH4      .36865-07      CN      .10136+05      C2F2      .25193+16      C2F4      .21301+23
C2H4O      .25111-15      C2N2      .57503+10      C3O2      .41461+11      CH#2      .47399+18
CLF      .44974+07      CLF#3      .47909+25      FIF3      .83535+22      CL#O      .99812+06
CLO      .84962-06      CLO2      .27124+11      CL2O      .27719+11      F      .78547+04
FN      .23708+08      FNO      .38823+09      FO      .14624+08      F2H      .90912+16
H      .65694+01      HN      .20948+04      HO      .29439+02      H2N      .15136+04
H3N      .97000+05      H4N2      .81142+12      N      .15777+04      NO      .25032+03
N2O      .27127+07      N2O3      .14671+14      N2O4      .23465+22      N2O5      .81268+27
O3      .62527+12      CCL2F2      .12848+17      E2#      .12414+13      FCL      .65594+07
FNO2      .88244+15      CLN#2      .10025+13      E2#      .12414+13      FNO3      .17591+21
REN      .76398+05      HNO2      .72431+09      H#O3      .38992+14      HE2O      .70420+03
H#O2      .53615-07      H2N2      .99771+15      C#4O      .65570+24      CCL2      .23277+10
F2N2      .53440+18      H2#2      .48877+09      HE2F3O      .15761+03      C#2      .22592+09
CLF5      .18459+38      HE4      .69606+14      F#2      .60519+12      C2#      .51929+08
C2CL4      .12229+21      C2CL6      .10149+11      C2HF      .13129+11      C2CL2      .34554+13
CHCL      .11644+08      CHF      .10842+04      C2F3#      .16422+20      F3NO      .11447+25
CL2      .21579+05      F2      .10770+00      O2      .13016+04      C#O      .58038+07
C2H3      .12922+10      C2H6      .99422+15      C3#      .92580+12      C3+2      .65852+13
C3H4      .43219+15      C3#5      .14449+14      C4#      .30223+15      C4#2      .43396+16
CLHNO4#      .00000      EEM2O2#      .00000      HE#      .00000      HE#O      .14966+00
RESN2#      .00000      HECL2#      .00000      HEF2#      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROR. 1      00000000000

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLHP/DLHP      DLHP/DLHP      GAMMA
.36603+00      .49852+02      -.43601+01      .49949+01      .99459+00

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT. SEC. RTU. AND DEG-R
TEMP      VISC      COFO      DBAR      PR      SC
.90000+03      .16292-04      .15778-04      .17653-04      .50751+00      .72433+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.77413+00      .20596+02      .25806+02      -.52830+03      .48840+00      -.13648+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      4      6      7      8      9      17      104
.33335-01      .12809+00      .11053+00      .11656+00      .50546+00      .16432+00      .14172+00      .00000
.91019-01      .65809+01      .15771+00      .14544+00      .23385+00      .17954+00      .14659+00      .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = .414 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT
MASS CONDENSED/MASS GAS = .22523+00
TEMP = 900.0000 DEG K. = 500.0000 DEG K.      PRESS = 31.47837 ATM

ENTHALPY - RTU/LHM      GAS      CONDENSED      COMPOSITE
-4.22911+04      -.10178+05      -.37409+04
ENTROPY - RTU/LHM DEG R      .29345+01      .29797+00      .17153+01
DENSITY - LBM/FT3      .10687+01      .12359+01      .12359+01
MOLECULAR WEIGHT      21.0621      25.0120      25.8059

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .2731A-02      H2      .32264+00      H2O      .30265-01      CO      .00000      CLH      .41121-01
C      .26684-01      HE      .29748-02      CCLN      .36303-07      CO      .23469+00      C2H2      .88519-08
C2H2      .42812-07      C2      .12001-10      C3      .28174-13      C4      .51448-19      C5      .36090-22
C2H4      .16436-09      HECL      .28718-02      HECLF      .37213-01      4ECL2      .81873-02      HEE      .38901-01
HEF2      .44390-01      BEHO      .48529-02      FEH2      .10869-03      4F+2O2      .30026-02      FEO      .16679-03
HE2CL4      .15897-07      HE2O2      .19662-03      FE3O4      .24291-03      4E+O4      .88306-04      RE5O4      .33307-05
HE4O6      .23615-06      CCL      .11200-08      CCLFO      .25637-09      CCLF3      .14808-17      CCL2O      .94859-10
CCL3F      .75742-18      CCL4      .21869-18      CF      .73674-08      CFH      .15664-08      CF2      .37747-10
CF2O      .17754-09      CF3      .14443-14      CF4      .42068-18      CH      .31811-07      CHCLF2      .20569-14
CHCL2F      .18370-14      CHCL3      .10163-14      CHF3      .35446-07      CH4      .94948-15      CH2CLF      .26279-04
CHNO      .43530-06      CHD      .23341-04      CH2      .18436-07      CH3CL      .34490-09      CH3F      .67572-10
CH2F2      .25524-12      CH2O      .15182-05      CH3      .15837-06      C2F4      .21301-23      C2H4      .44993-11
CH4      .36865-07      CH      .10136-05      C2F2      .25193-16      C4H2      .47399-18      CL      .55665-02
C2H4O      .25131-14      C2H2      .57403-10      C3O2      .91461-11      C4H2      .99812-06      CLNO      .73927-08
CLF      .44978-07      CLF3      .47909-25      CL2O      .27719-11      F      .78547-04      FHO      .57663-08
CLO      .84982-06      CLO2      .27128-11      CL2O      .18429-08      F2O      .98912-16      F3N      .26601-20
FN      .23708-04      FNO      .38823-09      HO      .29434-02      4F2O      .15136-04      H2O2      .39910-08
H      .65694-01      HN      .20448-04      N      .15777-04      V2O5      .41268-27      O      .35128-03
H3N      .97000-05      H4N2      .81192-12      N2O4      .23865-22      CFO      .65594-07      C2F6      .24885-31
N2O      .27127-07      N2O3      .14471-16      CCLO      .26841-05      F2O      .17391-21      H4O      .34649-06
O3      .62527-12      CCL2F2      .12844-17      F2N      .12418-13      H2O      .70920-03      F4N2      .34641-34
FNO2      .88244-18      CLNO2      .10023-13      HNO3      .49920-14      CCL2      .23277-10      CCL3      .35735-14
FEN      .76398-05      HNO2      .72831-09      NO3      .99771-15      FE2O      .22592-09      C2O      .71995-08
H2O      .53835-07      H2N2      .68778-09      F2O2      .46319-12      C2H      .31928-08      C2HCL      .20189-09
F2N2      .53840-14      BEH      .69606-16      C2HF      .13129-11      F2O      .34558-13      F2HCL      .16380-10
CLF3      .18469-38      C2CL6      .10169-11      C2F3H      .16422-20      F3O      .11447-25      F2      .10373-10
C2CL4      .12224-21      CHL      .10942-08      O2      .13016-04      CNO      .65038-07      N3      .24373-09
CL2      .21579-05      C2H6      .99522-15      C3H      .92460-12      C3H2      .65852-13      C3H3      .10447-13
C2H3      .12922-10      C3H5      .14499-14      C4H      .30223-15      C4H2      .43396-16      CLH4*      .00000
CLH4N4*      .00000      BE42O2*      .00000      HE*      .00000      BEO*      .14966+00      CRE2*      .00000
HE3N2*      .00000      BECL2*      .00000      HEF2*      .00000

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Sample Problem 1 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) PROC. 1      0003000+00
CP-FROZEN= .36624+00

PROPERTY ROUTINE OUTPUT IN LB-MASS,FT,SEC,RTU,AND DEG-R
TEMP      VISC      COND      DBAR      PR      SC
.90000+03 .16355-04 .99522+05 .17653-04 .60185+00 .72464+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.94288+00 .25172+02 .26508+02 -.36450+04 .43371+00 -.37859+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      1      2      3      4      5      6      7      8      9      10
.71313-01 .87637-01 .11139+00 .13714+00 .22999+00 .20646+00 .15608+00 .00000
.91019-01 .65809-01 .13771+00 .14546+00 .23385+00 .17956+00 .14659+00 .00000

SOLUTION TIMES
ITFRATIONS = 34      TIME = 9.753 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS AT: GRAPHITE
MASS TRANSFER COEFFICIENT ROUGH = .96900+00
RHO V WALL/RHOE DE CM = .10000-16 BPRIME = .00000

STATE ADJACENT TO THE SURFACE . . .
TEMP = 900.0000 DEG R = 500.0000 DEG K      PRESS = 31.47837 ATM

      GAS      CONDENSED      COMPOSITE
ENTHALPY - RTU/LBM      -.41003+04      .00000      -.41003+04
ENTROPY - BTU/LBM DEG R      .14084+01      .00000      .00000
DENSITY - LBM/FT3      .12695+01      .00000      .12695+01
MOLECULAR WEIGHT      26.5080      .0000      26.5080

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = BPRIME CONDENSED ) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .23277-07      H2      .56440-01      H2O      .26938+00      C*      .00000      CLH      .11182+00
FH      .27636-03      HE      .00000      CCLN      .75120-27      CO      .34549-10      C2H2      .12954-27
C      .00000      C2      .00000      C3      .00000      C4      .00000      C5      .00000
C2RE      .00000      RECL      .15712-13      HFCLF      .43118-02      RECL2      .28301-03      REF      .72840-27
REF2      .14155+00      REHO      .24712-31      REM2      .97115-54      HFH2O2      .14283-03      REO      .00000
BE2CL4      .10721-08      BE2O2      .00000      RF3O3      .63335-25      RF4O4      .92324-17      RE5O5      .21536-10
BE6O6      .14516-01      CCL      .00000      CCLFO      .67369-25      CCLF3      .00000      CCL2O      .23793-25
CCL3F      .00000      CCL4      .00000      CF      .00000      CFN      .15286-37      CF2      .00000
CF2O      .18187-24      CF3      .00000      CF4      .00000      CH      .00000      CHCLF2      .45249-31
CHCL2F      .22641-30      CHCL3      .27769-28      CHFO      .15828-19      CHF3      .14261-30      CHN      .38271-16
CHNO      .44346-17      CHD      .32711-28      CH2      .00000      CH2CLF      .43060-22      CH2CL2      .31835-18
CH2F2      .64381-24      CH2O      .30833-15      CH3      .14482-19      CH3CL      .76154-09      CH3F      .89693-15
CH4      .24588+00      CN      .00000      C2F2      .00000      C2F4      .00000      C2H4      .32929-15
C2H4O      .13713-30      C2N2      .64819-17      C3O2      .00000      C4N2      .00000      CL      .92420-21
CLF      .21185-36      CLF03      .00000      CLF3      .00000      CLH0      .10898-25      CLN0      .00000
CLO      .00000      CLO2      .00000      CL2O      .00000      F      .18740-37      FHO      .00000
FN      .00000      FNO      .00000      FO      .00000      F2O      .00000      F3N      .00000
H      .29398-21      HN      .34121-15      H0      .12689-26      H2N      .58404-20      H2O2      .15944-36
H3N      .42508-01      H4N2      .15408-21      H      .00000      VO      .60951-32      H02      .00000
N2O      .23507-35      N2O3      .00000      N2O4      .00000      N2O5      .00000      O      .00000
O3      .00000      CCL2F2      .00000      C2N2      .17024-37      CF0      .00000
FN02      .00000      CLN02      .00000      F2N      .00000      FN03      .00000      C2F6      .00000
REN      .00000      HN02      .00000      HN03      .00000      RE2O      .00000      H4N2      .98354-36
H02      .00000      N03      .00000      CF4O      .00000      CCL2      .00000      F4N2      .00000
F2N2      .00000      H2N2      .31209-28      BE2F2O      .00000      CCL2      .00000      C2O      .00000
CLF5      .00000      BE4      .00000      F02      .00000      CN2      .00000      C2N      .00000
C2CL4      .00000      C2CL6      .00000      C2HF      .00000      C2CL3      .00000      C2HCL      .24659-36
CHCL      .00000      CHF      .00000      C2F3N      .00000      F3N0      .07000      F2      .00000
CL2      .11230-20      N2      .10851+00      O2      .00000      CNO      .00000      N3      .00000
C2H3      .86439-35      C2H6      .20206-06      C3H      .00000      C3H2      .00000      C3H3      .00000
C3H4      .73722-31      C3H5      .28923-26      C4H      .00000      C4H2      .00000

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Sample Problem 1 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) PROB. 1

5002000+40

6 6

CP-FROZEN= .41587+00

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, ATU, AND DFG-R
 TEMP VISC COND DGR PR SC
 .25200+04 .32185-04 .33969-04 .97419-04 .39403+00 .72449+00
 MU1 MU2 MOL.WT HTIL CPTIL HTIL*
 .80934+00 .21579+02 .23272+02 -.12491+04 .75158+00 -.17734+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPX = .667)
 1 6 7 8 9 17 106
 .39722-01 .81106-01 .13133+00 .13745+00 .23048+00 .20404+00 .17147+00 .00000
 .90963-01 .65695-01 .13893+00 .14526+00 .23553+00 .17927+00 .14635+00 .00000

SOLUTION TIMES
 ITERATIONS = 8 TIME = 5.121 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS ATJ GRAPHITE
 MASS TRANSFER COEFFICIENT RHO CM = .96900+00
 RHO V WALL/RHOE UE CM = .14042-02 RPRIME = .14042-02

STATE ADJACENT TO THE SURFACE . . .
 TEMP = 2420.0000 DEG R = 1400.0000 DEG K PRESS = 31.47857 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY = BTU/LBM	-.24804+04	.00000	-.24804+04
ENTROPY = BTU/LBM DEG R	.22753+01	.00000	.00000
DENSITY = LBM/FT3	.39404+00	.00000	.39404+00
MOLECULAR WEIGHT	23.2721	.0000	23.2721

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
 (MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE (UE CM)) . . .
 1= .49822-04 2= .67044-04 3= .12046-11 4= .24574-19 5= .11522-21
 6= .30147-21 7= .27480-26 8= .26413-28

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
 1= .27438+01 2= .27438+01 3= .75284+01 4= .27438+01 5= .75284+01
 6= .20656+02 7= .20442+02 8= .19474+00

CHEMICAL STATE ADJACENT TO THE SURFACE
 (MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
 (MOLE FR FOR CONDENSED = RPRIME CONDENSED) . . .

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.85921-02	H2	.38445+00	H2O	.30121-01	C*	.00000	CLH	.33103-01
PH	.39627-02	BE	.46478-13	CCLN	.17192-09	CO	.23852+00	C2H2	.15142-06
C	.36925-20	C2	.31321-23	CA	.74905-22	C4	.24869-28	C5	.13041-28
C2H6	.31974-19	HECL	.37022-09	HECLF	.47444+01	HECL2	.12952-01	HEF	.75549-07
HEF2	.74927-01	HEHO	.15085-04	HEH2	.84046-10	HEH2O	.22544-02	HFO	.17640-15
BE2CL4	.67036-07	BE2O2	.14076-12	BE3O3	.47439-07	BE4O4	.60434-05	HE5O5	.57045-04
BE6O6	.38201-02	CCL	.44444-14	CCLFO	.45752-12	CCLFA	.27107-22	CCL2O	.60625-12
CCL3F	.24804-22	CCL4	.23116-22	CF	.15439-17	CFH	.22236-13	CF2	.46445-17
CF2O	.61283-12	CF3	.31722-22	CF4	.25451-22	CH	.14714-17	CHCLF2	.61564-17
CHCL2F	.14021-16	CHCL3	.49242-16	CHFO	.24971-14	CHF3	.32045-17	CHN	.37644-04
CHNO	.25429-08	CHO	.93430-08	CH2	.73062-13	CH2CLF	.52464-12	CH2CL2	.92022-11
CH2F2	.47337-13	CH2O	.25500-05	CH3	.24142-06	CH3CL	.52715-06	CH3F	.31217-08
CH4	.73102-02	CH	.25181-12	C2F2	.62044-25	C2F4	.44047-31	C2H4	.13545-05
C2H4O	.25441-13	C2F2	.74447-11	C3O2	.60514-11	C4H2	.67244-18	CL	.44544-07
CLF	.28423-14	CLFO3	.00000	CLFA	.00000	CLHO	.17927-11	CLNO	.40521-17
CLO	.43749-16	CLO2	.16245-27	CL2O	.15744-23	F	.72122-13	FHO	.95043-18
FN	.38846-21	FNO	.14545-20	FO	.61591-24	F2O	.21925-36	FNN	.00000
H	.53855-06	HN	.52442-12	HO	.80142-09	H2N	.43551-08	H2O2	.11415-15
H3N	.22196-03	H4H2	.64144-14	F	.23443-15	NO	.40605-11	NO2	.22003-20
H2O	.48229-14	H2O3	.56012-34	H2O4	.00000	N2O5	.00000	O	.10360-14
O3	.16403-32	CCL2F2	.22278-22	CCLO	.11786-08	CFO	.11241-12	CF4	.44041-38
FN02	.38048-31	CLNO2	.61906-28	F24	.72493-29	FAO3	.00000	HNO	.44163-14
BEH	.81119-14	HN02	.12122-14	HN03	.15244-24	HE2O	.54114-14	FAH2	.00000
HO2	.76146-19	NO3	.76544-14	CF4O	.44046-18	CCL2	.33734-17	CCL4	.11915-19
F2N2	.26453-34	H2N2	.20224-13	HE2F2O	.21678-01	CF2	.46774-17	C2O	.69201-14
CLF5	.00000	BEH	.00000	FO2	.62441-11	C2H	.13944-12	C3N	.80212-16
C2CL4	.20215-24	C2CL6	.93260-17	C2HF	.26451-15	C2CL2	.24070-16	C2HCL	.47193-11
CHCL	.25239-15	CHF	.27044-15	C2F3N	.52410-25	F3H	.00000	F2	.54023-25
CL2	.77717-10	N2	.11405-00	O2	.34436-16	CH	.27460-13	N3	.66649-19
C2H3	.30471-10	C2H4	.73444-04	C3H	.27704-14	C3H2	.13457-13	CH4	.26247-11
C3H4	.14646-09	C3H5	.57432-08	C4H	.20547-17	C4H2	.34442-14		

Sample Problem 1 Output (Concluded)

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GRAPHITE SURFACE KINETICS (GASKET) PROB. 1      5002000+00      6 6

CP-FROZEN= .52269+00

PROPERTY ROUTINE OUTPUT IN LB-MASS,FT+SEC+RTU+AND OFG-H
TEMP      VISC      COND      DBAR      PR      SC
.72000+04 .64280+04 .66452+04 .55595+03 .50561+00 .72553+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL+
.87984+00 .23487+02 .24810+02 .84810+04 .73985+00 .69927+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASF) = .667)
1      2      3      4      5      6      7      8      9      10      11      12      13      14      15      16      17      18      19      20
.34442-01 .34894-01 .55762+00 .75109+01 .12072+00 .95579+01 .81641-01 .00000
.59850-01 .34231-01 .53805+00 .77487-01 .12461+00 .98065+01 .72704-01 .00000

SOLUTION TIMES
ITERATIONS = 6      TIME = 4.693 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS ATJ GRAPHITE
MASS TRANSFER COEFFICIENT ROUN = .96900+00
RHO V WALL/RHOE UE CM = .90496+00 BPRIME = .90496+00

STATE ADJACENT TO THE SURFACE . . .
TEMP = 7199.9999 DEG R = 4000.0000 DEG K      PRESS = 31.47837 ATM

ENTHALPY = BTU/LBM      GAS      CONDENSED      COMPOSITE
.58476+04      .00000      .45476+04
ENTROPY = BTU/LBM DEG R      .24015+01      .00000      .00000
DENSITY = LBM/FT3      .14852+00      .00000      .14852+00
MOLECULAR WEIGHT      24.8099      .0000      24.8099

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM) . . .
1= .68928-08 2= .50169-08 3= .31663-01 4= .10204-02 5= .56004-02
6= .10715-02 7= .14080-03 8= .24100-05

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .12717+01 2= .12717+01 3= .16173+01 4= .12717+01 5= .16173+01
6= .20564+01 7= .26157+01 8= .33264+01

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = BPRIME CONDENSED ) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .40920-06      H2      .14220+00      H2O      .26537-05      C#      .00000
FH      .23877-01      FE      .68840+02      CCLN      .11922-03      CO      .18706+00
C      .16619-02      C2      .17498-02      C3      .81174+02      C4      .74222+04
C2H6      .52947-02      BECL      .29082-02      HCLF      .13700-01      HECL2      .21961-02
BEF2      .21516-01      HFNO      .69443-06      HFH2      .50970-04      3FH2O2      .20260+00
HE2CL4      .11603-08      HF2O2      .47866-11      HF3O3      .17855-15      HE4O4      .31693+20
BE6O6      .19430-31      CCL      .23411-04      CCLFO      .30144+09      CCLF3      .20419+17
CCL3F      .54822-14      CCL4      .10582-14      CF      .18453-03      CFH      .10499+04
CF2O      .30941-09      CF3      .37664-10      CF4      .14679-13      CH      .51956+03
CHCL2F      .67811-11      CHCL3      .24704-11      CHFO      .28027-07      CHF3      .70992+11
CHNO      .14881-06      CHO      .22842-04      CH2      .68656-06      CH2CLF      .14420+08
CH2F2      .76764-09      CH2O      .46237-06      CH3      .19064+03      CH3CL      .22271+05
CH4      .12706-04      CHN      .77914-02      C2F2      .20741-08      C2H4      .27694+15
C2H4O      .13140-12      C2H2      .41630-05      C3O2      .27134+07      C4H2      .51145+04
CLF      .18686-06      CLF3      .37722-14      CLF3      .39304+20      CLHO      .30383+09
CLO      .84935-09      CLO2      .14854-17      CL2O      .53655-14      F      .43851+03
FN      .14854-07      FNO      .37945-12      FO      .47587-11      F2O      .84752+18
H      .10666+00      HI      .30843-04      HO      .11849+05      4H      .73866-05
H3N      .13402+05      H3N2      .89843-13      H      .60870+04      JO      .11125+06
N2O      .73472-11      N2O3      .11633-26      F2O4      .84252+36      42O5      .00000
O3      .16508-21      CCL2F2      .13176-13      CCLO      .33296+05      CFO      .16610+06
FNO2      .41029-21      CLNO2      .23826-20      F2H      .14381-12      FNO3      .71199+31
BEN      .15094-04      HNO2      .61988-16      HNO3      .15354+24      HE2O      .12312+06
H2O      .10567-13      NO3      .12518-24      CF4O      .12314+22      CCL2      .24126+06
F2N2      .44303-17      H2F2      .31478-09      3E2F2O      .57605+06      CN2      .12552+05
CLF5      .11706-35      HEH      .25768-14      FO2      .71634+18      2H      .78099+01
C2CL4      .20610-14      C2CL6      .20847-24      C2HF      .33483+04      C2CL2      .77916+06
CHCL      .68925-04      CHF      .10444+04      C2F3H      .61728+13      FMO      .19937+27
CL2      .34953-05      N2      .37622-01      O2      .36844+11      CNO      .83820+07
C2H3      .63328-04      C2H6      .37495-09      CH      .68832+01      C3H2      .25206+02
C3H4      .25480-04      C3H5      .48875-05      CH4      .88971-01      C4H2      .43112+02

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Sample Problem 2

The shockwave option of GASKET is utilized in this problem. The surface material is made of 15% SiC/PG. The boundary layer edge state is specified as the stagnation condition behind a normal shock wave with an upstream Mach number of two. The shock is assumed to exist in the divergent section of a nozzle and, thus, conditions upstream of the shock are calculated via an isentropic expansion from input ideal chamber conditions. Since the edge gases contain both hydrogen and oxygen, all three kinetically-controlled surface reactions are possible. Two temperatures are input for both the frozen edge and surface temperature arrays. Finally, the diffusion factors are updated for 16 selected species.

Listing of Input

1.	5094220400	3901.	40.81	-2.0	68.02	0.463	0.0	PROP. 2
2.	.15							
3.	1000.							
4.	1500.							
5.								
6.	1200.							
7.	1400.							
8.								
9.	6							
10.	1 HYDROGEN	1.008	3.2219					
11.	6 CARBON	12.011	.56490		1.0			
12.	7 NITROGEN	14.008	.5366					
13.	8 OXYGEN	16.0	2.2486					
14.	13 ALUMINUM	26.98	1.013					
15.	17 CHLORINE	35.453	.5398					
16.	1	0.0	-9999.		0.0			
17.	16							
18.	C	0.69100CH	0.74920CH4		0.93570CH		1.02670	
19.	CO	1.01700CO2	1.29140C2H2		1.17460H		0.30180	
20.	H2	0.38930H2O	0.77490N		0.74930NO		0.99810	
21.	N2	1.026200	0.7397002		1.00000C2		1.02530	
22.	8							

Sample Problem 2 Output

GRAPHITE SURFACE KINETICS (GASKET) PROB. 2 0110000*J0

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00800	.0322205	.0000000
6	CARBON	12.01100	.0052493	.0000000
7	NITROGEN	14.00800	.0053663	.0000000
8	OXYGEN	16.00000	.0224271	.0000000
13	ALUMINUM	26.98000	.0101305	.0000000
17	CHLORINE	35.45300	.0053983	.0000000
14	SILICON	28.09000	.0000000	.0037407
106	GRAPHITE	12.01100	.0000000	.0745088

ELEMENTS	HYDROGEN CHLORINE	CARBON SILICON	NITROGEN GRAPHITE	OXYGEN	ALUMINUM
BASE SPECIES	H2 CLH	CO2 CH3CL3S	ALN C*	H2O	AL

Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET) SOLUTION          PROB. 2

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLNM/DLWT      DLNM/DLHP      GAMMA
.42289+00      .12704+01      -.81279+00      .49323+01      .11173+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT-SEC, RTU, AND DEG-R
TEMP      WISC      COND      UBAR      PR      SC
.70218+04      .62950+04      .84839+04      .24681+03      .20753+00      .72419+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.73200+00      .19437+02      .33303+02      .65193+04      .96142+00      .43301+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .667)
      6      7      8      13      14      106
.32478+01      .67853+01      .75170+01      .35979+00      .27332+00      .19134+00      .00000      .00000
.11322+00      .11673+00      .12994+00      .26974+00      .46727+01      .20364+00      .00000      .00000

SOLUTION TIMES
ITERATIONS = 27          TIME = 5.727 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72922+00
TEMP = 7021.8000 DEG R. = 3901.0000 DEG K.      PRESS = 68.02000 ATM

ENTHALPY = BTU/LBM      GAS      CONDENSED      COMPOSITE
.19521+04      .45284+04      -.78073+03
ENTROPY = HTU/LBM DEG R      .20114+01      .48044+00      .72097+01
DENSITY = LBM/FT3      .25544+00      101.9600      .44172+00
MOLECULAR WEIGHT      19.2588      101.9600      31.3027

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
C02      .34049+02      H2      .32612+00      H2O      .10142+00      C*      .00000      CLH      .10317+00
AL      .34049+02      ALN      .62793+06      CH3CL3S      .00000      C*      .14134+00      C2H2      .21043+08
C      .61816+07      C2      .27773+11      C3      .05550+14      C4      .61009+20      C5      .15053+23
CAL      .15823+08      ALCL      .30440+01      ALCL0      .57887+02      ALCL2      .10091+01      ALCL4      .16885+03
ALH      .47985+03      ALH02      .26119+02      AL0      .22285+02      AL2CL6      .23514+10      AL20      .14059+02
AL202      .13163+04      CCL      .40185+08      CCLN      .54882+07      CCL20      .13645+08      CCL4      .16480+16
CH      .46292+07      CHCL3      .21843+13      CHN      .12377+04      CH00      .71144+06      CH0      .43111+04
CH2      .20564+07      CH2CL2      .62869+11      CH20      .22208+05      CH3      .12179+06      CH3CL      .65644+09
CH4      .21208+07      CH4      .81008+06      C2H4      .13280+11      C2H40      .40575+15      C2N2      .14714+10
C302      .67075+11      CH42S1      .00000      CH42      .24948+19      CL      .19093+01      CLH0      .18083+04
CLH3S1      .00000      CLN0      .20144+06      CL0      .19467+04      CL02      .46439+09      CLS1      .00000
CL2H2S1      .00000      CL20      .30342+09      CL2S1      .00000      CL3HS1      .00000      CL4S1      .00000
H      .92093+01      HN      .54434+04      H0      .16302+01      H51      .00000      H2N      .13589+04
H202      .78294+06      H3N      .16734+04      H4N2      .46761+11      H4S1      .00000      H      .43874+04
N0      .14889+02      N02      .14505+06      N51      .00000      H20      .22032+06      H203      .65235+14
N204      .67070+19      N205      .16845+22      0      .26379+02      CS1      .00000      C2S1      .00000
O3      .17671+04      S1      .00000      S12      .00000      S13      .00000      CCL0      .12090+02
CLN02      .17850+11      HN0      .34743+05      HN02      .28477+07      HN03      .10030+11      ALH0      .30329+04
H02      .20316+05      N03      .31540+12      CCL2      .19426+09      CCL3      .89640+13      H2N2      .31542+08
CN2      .28294+09      C20      .67827+08      C2H      .10781+08      CS1      .00000      CS12      .00000
C2N      .80606+10      C2S1      .00000      S12      .00000      C2CL4      .41566+20      C2CL6      .66177+29
AL02      .30844+03      C2CL2      .68407+13      C2HCL      .27460+10      CHCL      .38211+08      CL3S1      .00000
CL2      .24563+04      N2      .48527+01      02      .32099+03      CND      .14687+06      N3      .19382+08
C2H3      .50618+11      C2H6      .42556+15      C3H      .10492+12      C3H2      .10796+13      C3H4      .16381+14
C3H4      .66570+16      C3H5      .29253+15      C4H      .20492+16      C4H2      .28295+17      ALCL0*      .00000
CS1*      .00000      CLH40*      .00000      CLH40*      .00000      ALCL1*      .00000      ALN*      .00000
AL205S1*      .00000      C3AL4*      .00000      S4S1*      .00000      AL*      .00000      AL203*      .13774+08
O2S1*      .00000      S1*      .00000      ALA013S*      .00000

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Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) PROR. 2 2000200+00

DERIVATIVE PROPERTY OUTPUT
 CP-FROZEN CP-EQUIL DLNM/DLNT ULNM/DLNP GAMMA
 .42237+00 .13866+01 -.90234+00 .53735-01 .11154+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, RTU, AND DFG-R
 TEMP VISC COND DBAR PR SC
 .68843+04 .62125-04 .83769-04 .39809-03 .20738+00 .72416+00
 MU1 MU2 MOL.WT HTIL CPTIL HTIL*
 .72854+00 .19343+02 .32992+02 .66964+04 .96181+00 .44251+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)

1	6	7	8	13	17	14	106
.32478-01	.67853-01	.75171-01	.35979+00	.27332+00	.19138+00	.00000	.00000
.11334+00	.11629+00	.12945+00	.28969+00	.67757-01	.28347+00	.00000	.00000

SOLUTION TIMES
 ITERATIONS = 4 TIME = 1.144 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72521+00
 TEMP = 6884.3399 DEG R. = 3824.6333 DEG K. PRESS = 40.81000 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LBM	.14709+04	-.44570+04	-.78073+03
ENTROPY - BTU/LBM DEG R	.29646+01	.97375+00	.21277+01
DENSITY - LBM/FT3	.15522+00		.26779+00
MOLECULAR WEIGHT	19.1235	101.9600	32.9921

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.66546-02	H2	.31914+00	H2O	.98954-01	C*	.00000	CLH	.10119+00
AL	.38011-02	ALN	.50642-06	CH3CL3S	.00000	CO	.17968+00	C2H2	.74198-09
C	.42776-07	C2	.34498-11	C3	.15450-14	C4	.97545-21	C5	.15381-24
CAL	.91928-09	ALCL	.31646-01	ALCLO	.60040-02	ALCL2	.47705-02	ALCL3	.12395-03
ALH	.42844-03	ALH02	.26300-02	ALO	.24446-02	AL2CLA	.79259-11	AL2O	.14617-02
AL2O2	.13715-04	CCL	.23072-08	CCL4	.32720-07	CCL2O	.74694-09	CCL4	.50571-17
CH	.26478-07	CHCL3	.71824-14	CH4	.72273-05	CH4O	.41045-06	CH4O	.29746-04
CH2	.10254-07	CH2CL2	.21424-11	CH2O	.12917-05	CH3	.54189-07	CH3CL	.24218-09
CH4	.83002-08	CH4	.51440-06	C2H4	.30748-12	C2H4O	.84772-16	C2H2	.49727-11
C3O2	.22951-11	C4H2S1	.00000	C4H2	.35153-20	CL	.21254-01	CLH0	.15154-04
CLH3S1	.00000	CL4O	.15142-06	CL0	.18806-04	CL02	.38063-09	CLS1	.00000
CL2H2S1	.00000	CL2O	.21360-09	CL2S1	.00000	CL3HS1	.00000	CL4S1	.00000
H	.10200+00	H4	.43880-04	H0	.17379-01	H51	.00000	H2N	.22965-04
H2O2	.60506-06	H3N	.99507-05	H4N2	.14790-11	H4S1	.00000	N	.41830-04
N0	.15441-02	N02	.13285-06	SI	.00000	N2O	.17530-06	N2O3	.37517-14
N2O4	.33807-19	N2O5	.72549-23	O	.31989-02	OS1	.00000	O2S1	.00000
O3	.16687-09	SI	.00000	SI2	.00000	SI3	.00000	CLO	.83900-05
CLN02	.11848-11	H4O	.27487-05	H4O2	.21334-07	H4O3	.65512-12	ALH0	.30315-02
H02	.18717-05	N03	.23774-12	CCL2	.93704-10	CCL3	.34541-13	H2N2	.16010-08
CN2	.13420-09	C2O	.33490-08	C2H	.42842-09	CS1	.00000	CS12	.00000
C2N	.30556-10	C2S1	.00000	NS12	.00000	C2CL4	.77890-21	C2CLA	.68114-30
AL02	.34069-03	C2CL2	.28164-13	C2HCL	.92984-11	CHCL	.18481-08	CL3S1	.00000
CL2	.21420-04	N2	.87684-01	O2	.38878-03	CNO	.93847-07	NS	.60613-09
C2H3	.13349-11	C2H6	.63183-16	C3H	.31154-13	C3H2	.21307-14	CSH3	.26940-15
C3H4	.91207-17	C3H5	.31438-16	C4H	.30331-17	C4H2	.31891-18	ALCLO*	.00000
CS1*	.00000	CLH4N*	.00000	CLH4H04*	.00000	ALCL3*	.00000	ALN*	.00000
AL2O5S1*	.00000	C3AL4*	.00000	N4S13*	.00000	AL*	.00000	AL2O3*	.13672+00
O2S1*	.00000	SI*	.00000	AL6O13S*	.00000				

Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET)  PROB. 2  5000100*00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN  CP-EQUIL  DLNM/DLNT  DLNM/DLNP  GAMMA
.92267+00  .11508+01  -.62810+00  .33430-01  .11111+01

PROPERTY ROUTINE OUTPUT IN  LB-MASS.FT*SEC*BTU*AND DEG-R
TEMP  VISC  COND  DBAR  PR  SC
.58395+04  .55713-04  .77229-04  .22498-02  .19013+00  .72459+00
MU1  MU2  MOL.WT  HTIL  CPTIL  HTIL*
.71314+00  .18914+02  .34303+02  .54259+04  .98836+00  .35344+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)
      6      7      8      13      17      14      106
.32478-01  .67853-01  .75170-01  .35979+00  .27332+00  .19138+00  .00000  .00000
.12227+00  .12477+00  .13877+00  .26677+00  .35429-01  .31199+00  .00000  .00000

SOLUTION TIMES
ITERATIONS = 8  TIME = 2.154 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT
MASS CONDENSED/MASS GAS = .88144+00
TEMP = 5839.4862 DEG R. = 3244.1602 DEG K.  PRESS = 5.49583 ATM

ENTHALPY - BTU/LBM  GAS  CONDENSED  COMPOSITE
.14629+04  .49298+04  .15324+04
ENTROPY - BTU/LBM DEG R  .31944+01  .91785+00  .21277+01
DENSITY - LBM/FT3  .21492+01  .44203+01
MOLECULAR WEIGHT  18.2305  101.9600  34.3033

ABOVE ARE STATIC PROPERTIES  N-KINETIC = .75168+03 BTU/LBM
VEL. = .6134+04 FT/SEC  FLUX = .27115+03 LBM/FT2SEC  MACH = 2.00009

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES)....
SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.
CO2  .57216-02  H2  .35496+00  H2O  .83429+01  C*  .00000  CLM  .13076+00
AL  .10219-02  ALN  .28250-07  CH3CL3S  .00000  CO  .18806+00  C2H2  .34405-10
C  .22047-04  C2  .36849-13  C3  .86103-17  C4  .75224-24  C5  .42889-28
CAL  .13454-10  ALCL  .19183-01  ALCLO  .81966-02  ALCL2  .59746-02  ALCL3  .91144-04
ALH  .66549-04  ALH2  .73142-03  ALH3  .45774-03  AL2CL6  .87286-12  AL2O  .22585-03
AL2O2  .16610-05  CCL  .10738-09  CCLN  .34864-08  CCL2O  .87612-10  CCL4  .97907-19
CH  .10625-08  CHCL3  .23164+15  CHN  .14237-05  CH2O  .55778-07  CH3  .45080-08
CH2  .52156-09  CH2CL2  .10849-12  CH2O  .20662-06  C2H4O  .50464-18  CH3CL  .17694-10
CH4  .87956-09  CN  .49273-07  C2H4  .60120-14  C2H4O  .50464-18  C2H2  .12991-12
C3O2  .52186-13  C4H2SI  .00000  C4H2  .36796-23  CL  .19782-01  CLH2  .35802-05
CLH3SI  .00000  CLN2  .14008-07  CL2  .36828-05  CL2  .12846-10  CLSI  .00000
CL2H2SI  .00000  CL2O  .11589-10  CL2SI  .00000  CL3H3SI  .00000  CL4SI  .00000
H  .80459-01  HN  .70494-05  HO  .74131-02  HSI  .00000  H2N  .39376-05
H2O2  .47484-07  H3N  .21441-05  H4N2  .18131-13  H4SI  .00000  H2N  .76693-05
NO  .46806-03  NO2  .99751-08  NSI  .00000  N2O  .19283-07  N2O3  .00000
N2O4  .26890-22  N2O5  .10035-26  O  .10040-02  O3  .00000  O2SI  .00000
O3  .31641-11  SI  .00000  SI2  .00000  SI3  .00000  CCL2  .16998-05
CLN2  .23702-13  HNO  .31141-06  HNO2  .11069-08  HNO3  .78013-14  ALMO  .10207-02
HO2  .16208-06  NO3  .23454-14  CCL2  .44799-11  CCL3  .10606-14  H2N2  .74808-10
CN2  .36106-11  C2O  .13467-09  C2H  .13260-10  CSI  .00000  CSI2  .00000
C2N  .55699-12  C2SI  .00000  NSI2  .00000  C2CL4  .35771-23  C2CL6  .33426-33
AL2O  .49744-04  C2CL2  .61986-15  C2HCL  .31046-12  CHCL  .79986-10  CL3SI  .00000
CL2  .10691-04  N2  .91795-01  O2  .93117-04  CNO  .73102-08  N3  .20733-10
C2H3  .19746-13  C2H6  .39104-18  C3H  .27295-15  C3H2  .10612-16  C3H3  .11610-17
C3H4  .31700-19  C3H5  .53164-19  C4H  .51075-20  C4H2  .56120-21  ALCL0*  .00000
CSI*  .00000  CLH4O*  .00000  CLH4O*  .00000  ALCL3*  .00000  ALN*  .00000
AL2O5SI*  .00000  C3AL4*  .00000  N4SI3*  .00000  AL*  .00000  AL2O3*  .15764+00
O2SI*  .00000  SI*  .00000  AL6O13S*  .00000

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Sample Problem 2 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASKET)  PROGR. 2  4000300+00

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN  CP-EQUIL  DLNM/DLNT  DLNM/DLNP  GAMMA
.42208+00  .14694+01  -.95479+00  .55542-01  .11133+01

PROPERTY ROUTINE OUTPUT IN  LB-MASS,FT,SEC,RTU,AND DEG-R
TEMP      VISC      COND      DBAR      PH      SC
.66873+04  .60935-04  .82537-04  .67562-03  .20531+00  .72416+00
MU1       MU2      MOL.WT    HTIL      CPTIL    HTIL*
.72372+00  .19211+02  .32842+02  .67796+04  .96604+00  .44566+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .667)
      1      6      7      8      13      17      14      106
.32478-01  .67453-01  .75171-01  .35979+00  .27332+00  .19138+00  .00000  .00000
.11435+00  .11673+00  .12993+00  .28765+00  .65560-01  .28578+00  .00000  .00000

SOLUTION TIMES
ITERATIONS = 6  TIME = 1.642 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .73616+00  PRESS = 22.91442 ATM
TEMP = 6687.2614 DEG R. = 3715.1452 DEG K.

ENTHALPY - RTU/LBM      GAS      CONDENSED      COMPOSITE
.32478-01  .19543+04  -.46420+04  -.84259+03
ENTROPY - BTU/LBM DEG R  .30291+01  .96388+00  .21534+01
DENSITY - LBM/FT3      .84753-01  .15409+00  .15409+00
MOLECULAR WEIGHT      18.9163  101.9600  32.8417

VEL2 = .1760+04 FT/SEC  MACH2 = .52408  THETA 2 = .000000 DEG
ABOVE ARE STATIC CONDITIONS DOWNSTREAM OF THE SHOCK FOR ...
VEL1 = .613+04 FT/SEC  H1-STATIC = -.153+04 RTU/LBM  H-TOT = -.781+03 RTU/LBM
P1 = 5.49553 ATM  RH01 = .44203-01 LBM/FT3  THETA 1 = .000000 DEG

STATIC CHEMICAL STATE (MOLE FR.=MOLECULES/TOTAL GAS PHASE MOLECULES)...
SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.  SPECIES  MOLE FR.
CO2      .65572-02  H2       .31644+00  H2O      .95764-01  C*       .000000  CLH*     .10146+00
AL       .58066-02  ALN      .34344+04  CH3CL3S .000000  CO       .17894+00  C2H2     .24640-09
C        .25328-07  C2       .11828+11  C3       .36136-15  C4       .12391-21  C5       .12456-25
CAL      .42995-09  ALCL     .31215-01  ALCLU    .53265-02  ALCL2    .75948-02  ALCL3    .93504-04
ALH      .34166-03  ALH2     .24153-02  ALU      .25390-02  AL2CL6   .27008-11  AL2O     .13289-02
AL2O2    .12234-04  CCL      .11578-08  CCLN     .16876-07  CCL2O    .38431-09  CCL4     .14001-17
CH       .13112-07  CHCL3    .21492-14  CHN      .40859-05  CH*O     .22341-06  CHO      .19150+04
CH2      .46012-08  CH2CL2   .72125-12  CH2O     .71645-06  CH3      .22819-07  CH3CL    .86541-10
CH4      .31908-08  CH4      .29621-06  C2H4     .67417-13  C2H*O    .15619-16  C2H2     .15312-11
C3O2     .70543-12  C4H2SI   .000000  C4H2     .36169-21  CL       .25150-03  CLMO     .11745-04
CLH3SI   .000000  CLN2     .10243-06  CL2SI    .000000  CL2      .24139-09  CLSI     .000000
CL2H2SI  .000000  CL2O     .12447-09  CL2SI    .000000  CL3H2SI  .000000  CL4SI    .000000
H        .10940+00  HN       .31434-04  HO       .17240-01  HSI      .000000  H2N      .14683-04
H2O2     .40442-06  H3N      .57443-05  H4O2     .40745-12  H4SI     .000000  H4N      .35563-04
NO       .14605-02  NO2      .10217-06  HSI      .000000  H2O      .12316-06  H2O3     .15545-14
N2O4     .11272-19  N2O5     .18577-23  O        .34610-02  O3       .000000  O2SI     .000000
O3       .11910-04  SI       .000000  S12      .000000  S13      .000000  CLO      .54905-05
CLN02    .63045-12  HNO      .19269-05  HNO2     .14443-07  HNO3     .33111-12  AL*O     .28044-02
H2       .14622-05  NO3      .13378-12  CCL2     .40636-10  CCL3     .11994-13  H2N2     .72596-09
CN2      .55106-10  C2O      .14718-08  C2H       .15315-09  CCL4     .000000  CS12     .000000
CPN      .14102-10  C2SI     .000000  CPH      .000000  C2CL4    .12619-21  C2CL6    .57432-31
AL2O     .32283-03  C2CL2    .81011-14  C2HCL    .24981-11  CHCL     .79824-09  CL3SI    .000000
CL2      .16137-04  N2       .67341-01  O2       .41144-03  CNO      .53474-07  N3       .30164-09
C2H3     .32188-12  C2H6     .86408-17  C3H      .68220-14  C3H2     .36974-15  C3H3     .39846-16
C3H4     .11337-17  C3H5     .30216-17  C4H      .38134-18  C4H2     .35184-19  AL*LO*   .000000
CSI*     .000000  CLH4H*   .000000  CLH4H*O* .000000  ALCL3*   .000000  ALN*     .000000
AL2O5SI* .000000  C3AL4*   .000000  H4SI3*   .000000  AL*       .000000  AL2O3*   .13648+00
O2SI*    .000000  SI*       .000000  AL6O13S* .000000

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Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROB. 2

DERIVATIVE PROPERTY OUTPUT
 CP-FROZEN CP-EQUIL DLNM/DLNT DLNM/DLNP GAMMA
 .42198+00 .14901+01 -.97911+00 .57415-01 .11137+01

PROPERTY ROUTINE OUTPUT IN LB-MASS.FT-SEC+RTU+AND DFG-R
 TEMP VISC COND DBAR PR SC
 .67695+04 .61431-04 .82941-04 .59241-03 .20701+00 .72413+00
 MU1 MU2 MOL.WT HTIL CPTIL HTIL*
 .72531+00 .19255+02 .32735+02 .68589+04 .96296+00 .45142+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)

1	6	7	8	13	17	14	106
.32478-01	.67853-01	.75171-01	.35479+00	.27332+00	.19138+00	.00000	.00000
.11354+00	.11600+00	.12912+00	.28951+00	.48365-01	.28346+00	.00000	.00000

SOLUTION TIMES
 ITERATIONS = 3 TIME = .954 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72300+00
 TEMP = 6769.4843 DEG R. = 3760.8246 DEG K. PRESS = 26.66895 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LHM	.19907+04	-.46140+04	-.78073+03
ENTROPY - BTU/LHM DEG R	.48105+01	.96803+00	.21534+01
DENSITY - LBM/FT3	.10248+00		.17658+00
MOLECULAR WEIGHT	18.9990	101.9600	32.7352

ABOVE ARE ISENTROPIC STAGNATION CONDITIONS DOWNSTREAM OF THE SHOCK FOR . . .
 VEL1 = .613+04 FT/SEC H1-STATIC = -.153+04 BTU/LHM H-TOT = -.781+03 BTU/LHM
 P1 = 5.49553 ATM RH01 = .44203-01 LBM/FT3 THETA 1 = .000000 DEG

ISEN. STAG. CHEMICAL STATE (MOLE FR.=MOLECULES / TOTAL GAS PHASE MOLECULES)..

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.66244+02	H2	.31844+00	H2O	.96757-01	C*	.00000	CLH	.99440-01
AL	.41177-02	ALN	.41753-06	CH3CL3K	.00000	CO	.17827+00	C2H2	.31299+09
C	.31162-07	C2	.16515-11	C3	.53108-15	C4	.21174-21	C5	.23125-25
CAL	.57655-09	ALCL	.32058-01	ALCL0	.61418-02	ALCL2	.77738-02	ALCL3	.95705-04
ALH	.38606-03	CLL	.14413-04	CLLN	.19762-07	CLL20	.35038-11	AL20	.18492-02
AL202	.13972-04	CLL02	.28195-02	CLL0	.19762-07	CLL20	.35038-11	CLL4	.18492-02
CH	.16502-07	CHCL3	.28403-14	CHN	.46268-05	CHN0	.25955-06	CH0	.21769-04
CH2	.57256-04	CH2CL2	.90902-12	CH20	.42266-06	CH3	.27665-07	CH3CL	.10615-09
CH4	.38123-08	CN	.35097-06	C2H4	.91729-13	C2H40	.25097-16	C2H2	.20210-11
CO2	.94123-12	C4H2SI	.00000	C4H2	.61212-21	CL	.25115-01	CLH0	.12975-04
CLH3SI	.00000	CLN0	.12044-06	CL0	.18052-04	CL02	.31630-09	CLSI	.00000
CL2H2SI	.00000	CL20	.15714-09	CL2SI	.00000	CL3H4C1	.00000	CL4SI	.00000
H	.11054+00	HN	.38137-04	HO	.18184-01	HSI	.00000	H2N	.16675-04
H2O2	.44268-06	H3N	.64423-05	H4H2	.56497-12	H4SI	.00000	N	.39880-04
NO	.13772-07	N02	.12161-06	NSI	.00000	N20	.14360-06	I203	.25112-14
N204	.18551-19	N205	.34535-23	O	.37092-02	OSI	.00000	O2SI	.00000
O3	.15521-09	SI	.00000	SI2	.00000	SI3	.00000	CLC0	.61645-05
CLN02	.82745-12	H40	.22406-05	HN02	.16411-07	HN03	.45079-12	ALH0	.30063-02
H02	.17225-05	N03	.18353-12	CLL2	.50754-10	CLL3	.15528-13	H2N2	.90840-09
CN2	.71735-10	C20	.18641-08	C2H	.19863-09	CS1	.00000	CS12	.00000
C2N	.13594-10	C2SI	.00000	NSI2	.00000	C2CL4	.19282-21	C2CL6	.17071-30
AL02	.36435-03	C2CL2	.10809+13	C2HCL	.37568-11	CHCL	.10042-08	CL3SI	.00000
CL2	.19006-04	N2	.86440-01	O2	.44450-03	CND	.54444-15	N3	.38342-09
C2H3	.44419-12	C2H6	.12457-16	C3H	.47754-14	C3H2	.55444-15	C3H3	.60615-16
C3H4	.17612-17	C3H5	.49637-17	C4H	.62057-18	C4H2	.57383-19	ALCLO*	.00000
CS1*	.00000	CLH4N*	.00000	CLH4N0*	.00000	ALCLH*	.00000	ALN*	.00000
AL205SI*	.00000	C3AL4*	.00000	H4SI3*	.00000	AL*	.00000	AL203*	.13472+00
O2SI*	.00000	SI*	.00000	AL60135*	.00000				

Sample Problem 2 Output (Continued)

GRAPHITE SURFACE KINETICS (GASNET) PROR. 2 0090000000
UPDATE OF DIFFUSION FACTORS

SPECIES	DIFFUSION FACTOR
CO2	1.29140
H2	.36930
H2O	.77490
CO	1.01700
CPH2	1.17460
C	.69180
C2	1.02930
CH	.74920
CH4	.93570
CN	1.02670
H	.30160
N	.74930
NO	.99810
O	.73970
N2	1.02620
O2	1.00000

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DNH/DLIT	DLNH/DLNP	CAPMA
.35736+00	.10551+02	-.39322+01	.90604+01	.94911+00

PROPERTY ROUTINE OUTPUT IN LH-MASS, FT, SEC, RTU, AND DEG-K

TEMP	VISC	COND	UHAR	PR	SC
.14000+04	.23573-04	.22113-04	.65800-04	.24968+00	.72409+00
MU1	MU2	POL.WT	MTIL	PTIL	HTIL
.76380+00	.18628+02	.32735+02	.13115+04	.64736+00	.50277+03

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER, . . . (GAMES = .667)

1	6	7	8	13	17	14	104
.32478+01	.67853+01	.75171+01	.35474+00	.27332+00	.14134+00	.00000	.00000
.96237+01	.11406+00	.13071+00	.29634+00	.45249+01	.24731+00	.00000	.00000

SOLUTION TIMES

ITERATIONS = 3 TIME = .443 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .72300+00
TEMP = 1400.0000 DEG K. PRESS = 26.66495 ATP

	GAS	CONDENSED	COMPOSITE
ENTHALPY - RTU/LHM	-.25724+03	-.67346+04	-.29774+04
ENTROPY - RTU/LHM DEG K	.24231+01	.42230+00	.15335+01
DENSITY - LHM/FT3	.38543+00		.66409+00
MOLECULAR WEIGHT	14.9440	101.9600	32.7352

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.66244+02	H2	.31444+00	H2O	.96757+01	C	.00000	CLH	.99440+01
AL	.41177+02	ALH	.41753+06	CH3CL3S	.00000	CO	.17427+00	CPH2	.31299+09
C	.31162+07	C2	.16415+11	C3	.53108+15	C4	.21172+21	C5	.23176+25
CAL	.57645+09	ALCL	.52059+01	ALCL0	.61418+02	ALCL2	.77738+02	ALCL4	.95705+04
ALH	.38466+03	ALH02	.26145+02	ALO	.24040+02	AL2CL6	.32038+11	AL20	.14925+02
AL202	.13972+04	CCL	.14413+08	CCLH	.14762+07	CCL20	.45073+09	CCL4	.18820+17
CH	.16502+07	CHCL3	.28403+14	CH4	.44268+05	CH40	.25955+06	CH0	.21769+04
CH2	.57256+08	CH2CL2	.90402+12	CH20	.42266+06	CH3	.27463+07	CH3CL	.10615+09
CH4	.38123+08	CH	.35057+06	C2H4	.91729+13	C2H40	.23097+16	CPH2	.20210+11
C302	.94123+12	CH4PST	.00000	C4H2	.41212+21	CL	.23113+01	CLH0	.12976+04
CLH3SI	.00000	CLH0	.12094+04	CL0	.14052+04	CL02	.31630+09	LLSI	.00000
CLH2ST	.00000	CL20	.15714+09	CL2SI	.00000	CL3HST	.00000	CL3ST	.00000
H	.11044+00	HN	.26137+04	H0	.14144+01	HSI	.00000	H2N	.16678+04
H202	.48268+06	H3N	.44423+05	H4H2	.76497+12	H4SI	.00000	H	.39800+04
NO	.15772+03	N02	.12161+04	SI	.00000	N20	.14364+06	N20S	.23112+14
N204	.18551+14	N205	.34435+23	O	.37092+02	OSI	.00000	O2SI	.00000
O3	.15591+09	SI	.00000	SI2	.00000	SI3	.00000	CCLO	.61653+05
CLH02	.82745+12	HNO	.22406+05	H402	.14511+07	HNO3	.45079+12	ALH0	.30043+02
H02	.17225+05	N03	.18353+12	CCL2	.40754+10	CCL3	.15528+13	H2N2	.90810+09
CN2	.71735+10	C20	.14461+08	C2H	.14463+09	CSI	.00000	CS12	.00000
C2H	.13594+10	C2SI	.00000	CS12	.00000	C2CL4	.19282+21	C2CL6	.10207+30
AL02	.36435+03	C2CL2	.10409+13	C2HCL	.37564+11	CHCL	.10042+04	CL3ST	.00000
CL2	.19006+04	N2	.46990+01	O2	.44950+03	CL0	.64254+07	N3	.38342+09
CLH3	.44419+12	C2H4	.12457+16	C3H	.97754+14	C3H2	.55444+15	CSH3	.60643+16
C3H4	.17612+17	C3H5	.49639+17	C4H	.42057+18	C4H2	.47383+19	ALCL04	.00000
CSI	.00000	CLH4N	.00000	CLH4N04	.00000	ALCL14	.00000	ALN4	.00000
AL205SI	.00000	C3AL4	.00000	N4SI3	.00000	AL	.00000	AL203	.13472+00
O2SI	.00000	SI	.00000	AL6013S	.00000				

Sample Problem 2 Output (Continued)

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CP-PROZEM = .37638+00

PROPERTY ROUTINE OUTPUT IN LB-PASS, FT, SEC, HTU, AND DFG-H
TEMP      VISC      COND      DPAR      PR      SC
.81688+00 .28888+00 .25662+00 .49088+00 .39318+00 .72437+00
MU      MU2      MOL.WT      HTIL      CPTIL      HTILO
.03997+00 .20538+02 .25888+02 -.11818+04 .64087+00 -.15330+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAPEX = .647)
      1      6      7      8      13      17      19      106
.00045+01 .10165+00 .11071+00 .24012+00 .98337+01 .40033+00 .40674+05 .00000
.96235+01 .11809+00 .13073+00 .24633+00 .49295+01 .24731+00 .46902+05 .00000

SOLUTION TIMES
ITERATIONS = 29      TIME = 4.449 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS SIC/PG
MASS TRANSFER COEFFICIENT ROUGH = .46300+00
RHO V WALL/RHOE UE CM = .44639+04 HF KINE = .44639+04

STATE ADJACENT TO THE SURFACE . . .
TEMP = 2160.0000 DEG R = 1200.0000 DEG K      PRESS = 26.66895 ATM

      GAS      COMPENSED      COMPOSITE
ENTHALPY - RTU/LBM      -.15525+04      .00000      -.15525+04
ENTROPY - RTU/LBM DEG R      .20017+01      .00000      .00000
DENSITY - LBM/FT3      .43759+00      .00000      .43759+00
MOLECULAR WEIGHT      25.8842      .0000      25.8842

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOF UE CM) . . .
1= .39581+04 2= .27801+05 3= .21308+10 4= .21079+23 5= .16877+26
6= .66781+26 7= .60427+32 8= .50836+34

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .32088+01 2= .32088+01 3= .10816+02 4= .32088+01 5= .10816+02
6= .35572+02 7= .42073+04 8= .55184+06

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
(MOLE FR FOR CONDENSED = RPRIME CONDENSED) . . .

      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
COP      .40874+01      H2      .42502+00      H2O      .15115+00      CO      .00000      CLM      .10230+01
AL      .27935+14      ALN      .20846+21      CH3CL3S      .21331+09      CO      .15525+00      C2M2      .47424+08
C      .12600+24      C2      .13441+20      C3      .47686+27      C4      .11707+34      C5      .52747+35
CAL      .78428+24      ALCL      .57363+06      ALCLC      .15427+05      ALCL2      .97485+03      ALCL3      .88782+01
ALM      .35048+13      ALM2      .74113+06      AL      .10322+14      AL2CL6      .22790+02      AL2O      .77191+11
AL2O2      .28495+12      CCL      .21445+23      CLCV      .11774+11      CCl2O      .62767+14      CCL4      .98809+27
CM      .38662+21      CMCL3      .42540+19      CM4      .46410+05      CM4O      .12279+06      CM4O      .66837+09
CM2      .28693+15      CH2CL2      .12754+12      CM2O      .18406+05      CM3      .38078+07      CM3CL      .11247+06
CM4      .22542+01      CM      .43416+15      CM4O      .56033+06      CM4O      .56880+14      CM4O      .56047+13
C3O2      .26131+12      CM2S1      .21327+15      CM4O2      .12867+21      CL      .53377+09      CLM      .62041+13
CLM3S1      .13848+05      CLN      .14844+19      CLU      .92421+19      CL2      .47399+31      CLS1      .31085+14
CL2M2S1      .47949+07      CL2O      .23441+27      CL2S1      .11430+07      CL3M2      .39019+07      CL4S1      .56891+06
H      .24800+07      H2      .40799+14      H2O      .67477+10      H2S1      .53950+16      H2N      .40544+09
H2O2      .16346+16      H3N      .44847+03      H4O2      .14564+14      H4S1      .72323+10      H      .24938+18
NO      .14021+12      NO2      .23467+22      S1      .11081+16      S2O      .14621+16      S2O3      .00000
N2O4      .00000      N2O5      .00000      O      .42029+17      OS1      .25232+05      O2S1      .42141+09
O3      .53704+36      SI      .98640+18      S12      .14701+26      S18      .31254+32      CCLN      .22529+10
CLM2O      .50891+31      H2O      .15747+15      H4O2      .62473+20      H4O3      .22184+30      ALMO      .15982+06
H2O2      .11399+20      NO3      .58541+37      CCL2      .97581+21      CCL3      .75063+24      H2M2      .86176+15
CM2      .37940+20      C2O      .12163+16      CM4      .12495+15      CS1      .11571+27      CS12      .29665+24
C2M      .18942+19      C2S1      .66610+23      S12      .21422+21      C2CL4      .11728+29      C2CL6      .00000
AL2O      .38095+15      C2CL2      .38320+20      CMCL      .12442+13      CMCL      .11958+18      CL3S1      .93370+07
CL2      .32313+12      H2      .10206+00      O2      .76456+18      CM      .33204+15      H3      .12775+21
CM3      .50928+12      C2M4      .27511+05      CM4      .95214+18      CM2      .14913+16      CM3      .19846+13
CM4      .77345+11      C3H5      .58512+09      CM4      .10440+21      CM4      .23952+17

```

Sample Problem 2 Output (Concluded)

GRAPHITE SURFACE KINETICS (GASNET) PRON. 2 5002000000

CP-PROZEN = .3033+00

PROPERTY ROUTINE OUTPUT IN LR-MASS,FT,SEC,RTU,AND DEG-R
 TEMP VISC COND DHAR PP SC
 .25200+04 .29698-24 .29248-04 .11494+03 .34617+00 .72471+00
 MU1 MU2 MOL.WT HTIL CPTEL HTILO
 .02010+00 .20169+02 .24940+02 -.75174+03 .70007+00 -.10046+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASER = .647)
 1 6 7 8 13 17 19 106
 .07025-01 .10298+00 .11222+00 .24211+00 .98046-01 .34687+00 .15452-04 .106
 .96221-01 .11032+00 .11064+00 .29824+00 .49246-01 .24720+00 .35444-04 .00000

SOLUTION TIMES
 ITERATIONS = 11 TIME = 3.675 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS SIC/PG
 MASS TRANSFER COEFFICIENT ROULK = .46300+00
 RHO V WALL/RHOE UE CM = .33747-03 RHPHPL = .33747-03

STATE ADJACENT TO THE SURFACE . . .
 TEMP = 2520.0000 DEG R ± 1400.0000 HLG K PRESS = 26.66895 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LHM	-.11133+04	.00000	-.11133+04
ENTROPY - RTU/LHM DEG R	.20449+01	.00000	.00000
DENSITY - LBM/FT3	.36139+00		.36139+00
MOLECULAR WEIGHT	24.9401	.0000	24.9401

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHOE UE CM) . . .
 1 = .53828-05 2 = .14741-04 3 = .54105+00 4 = .76104-14 5 = .27709-21
 6 = .66291-21 7 = .50441-26 8 = .55636-28

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES

1 = .16744+02 2 = .14744+02 3 = .20184+03 4 = .16744+02 5 = .21144+03
 6 = .07324+04 7 = .14939+02 8 = .37005+00

CHEMICAL STATE ADJACENT TO THE SURFACE

(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
 (MOLE FR FOR CONDENSED = WHOLE CONDENSED) . . .

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
CO2	.26499-01	H2	.44432+00	H2O	.13404+00	CO	.00000	CLH	.14444-01
AL	.67449-11	ALA	.23031-17	CH3CLAS	.64415-11	CO	.16533+00	CPH2	.46001-08
C	.71227-21	C2	.94749-24	C3	.37354-24	CH	.20434-31	C5	.17944-32
CAL	.61001-28	ALCI	.33044-04	ALCLD	.44475-04	ALC12	.72441-02	ALCL4	.62370-01
ALH	.32045-10	ALHD2	.21947-04	ALU	.24444-11	ALPCL4	.40464-04	AL20	.17444-07
AL202	.40241-04	UCL	.30451-20	CLCLH	.44461-11	CL120	.54444-13	CL4	.51245-25
CH	.37341-14	CHCL3	.32716-18	CH4	.61437-05	CH10	.16705-06	CHD	.71245-08
CH2	.13542-13	CH2CL2	.14431-12	CH20	.14100-05	CH3	.44150-07	CH3CL	.31441-07
CH4	.13046-02	CH	.41420-13	CPH4	.44772-07	CPH4D	.24137-14	CPH2	.18349-12
CSO2	.50614-12	CH42SI	.72444-20	CH42	.41444-21	CL	.17607-07	CLMO	.27349-11
CLH3SI	.74722-04	CLH10	.34414-17	CLU	.64414-14	CLU2	.11459-26	CLSI	.44140-12
CLH2SI	.29144-07	CL20	.40444-24	CL2SI	.43279-07	CL3H4SI	.14744-07	CL4SI	.77219-07
H	.62462-06	H1	.24724-12	HD	.37417-14	H4SI	.14444-13	H2H	.42444-08
H2O2	.21420-14	H4H	.21444-03	H442	.24414-14	H4SI	.17645-09	H	.25922-15
NO	.16646-10	NO2	.36302-19	SI	.37474-14	20	.17002-14	N2O3	.32049-34
N2O4	.00000	N2O5	.00000	O	.44271-14	O	.31438-04	O2SI	.44944-08
O3	.12666-30	SI	.10747-14	SI2	.24424-22	SI3	.13743-27	CLLO	.24444-09
CLH2O2	.33434-27	H4O	.19742-13	H4O2	.14434-17	H4O3	.44422-27	ALHO	.74411-05
H2	.14327-17	H4O3	.40143-32	CL2	.64744-14	CL3	.40422-22	H2H2	.17045-13
CH2	.66443-14	C20	.67402-15	C24	.43177-14	CS1	.17052-23	CS12	.34522-21
C2H	.21770-17	C2SI	.20116-20	4412	.17772-14	C2L14	.73178-24	C2CL4	.00000
ALD2	.62443-12	442	.44425-19	CLHCL	.47444-13	CHCL	.17645-16	CL3SI	.40011-07
CL2	.98244-11	42	.44745-01	OP	.74645-13	CH1	.17645-13	12	.54247-19
C2H3	.90474-12	C2H4	.20440-07	CSH	.14412-16	CH2	.44412-16	CH4	.12412-13
C3H4	.70245-12	C3H5	.27040-10	CH1	.16474-20	CH42	.24144-17		

Sample Problem 3

In this problem, all options which require the input of thermophysical properties are utilized. The surface material option of carbon/carbon 901 is used. The edge thermodynamic state (2805.81°K and 12.778 atm) is input directly. Diffusion factors for 16 selected species are input. Preexponential factors, activation energies, and temperature exponents are input for each of the eight possible kinetically controlled reactions, and inhibiting coefficients are input only for the three oxidation reactions. Finally, two frozen-edge temperatures and two surface temperatures are input to be used in lieu of the corresponding built-in temperature arrays.

Listing of Input

	1	0037223400	2804.61	12.778	0.0	0.0	0.246	U.	PRGN. 5
	2.	1000.							
	3.	1500.							
	4.								
	5.	1200.							
	6.	1400.							
	7.								
	8.	5							
	9.	1 HYDROGEN	1.008	3.6732					
	10.	6 CARBON	12.011	1.8865		1.0			
	11.	7 NITROGEN	14.007	1.2430					
	12.	8 OXYGEN	16.000	3.6376					
	13.	9 FLUORINE	19.000	0.022683					
	14.	16							
	15.	C	0.49180CH	0.74920CH4	0.93570CN			1.02670	
	16.	CO	1.61700C02	1.29140C2H2	1.17460H			0.30180	
	17.	H2	0.48930H2O	0.77490N	0.7493JNO			0.99810	
	18.	H2	1.02620G	0.73970O2	1.00000C2			1.02530	
	19.	-1 6 2	8 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/61				C02	
	20.	-940539+5	366362+5	130735+2	733664-3-754525+6	79A849+2	500.	2500.1	-0.C02
	21.	-940539+5	365616+5	142661+2	269831-3-233974+5	79B583+2	2500.	6000.1	-0.C02
	22.	-2 1 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/61				H2	
	23.	-996 0+0	212685+5	626264+1	934668-3 610915+5	484856+2	500.	2500.1	-0.H2
	24.	-996 0+0	212227+5	800304+1	362 19-3-186878+7	484694+2	2500.	6000.1	-0.H2
	25.	-2 1 1	6 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/61				H2O	
	26.	-577479+5	303899+5	847497+1	183253-2-305370+6	68A879+2	500.	2500.1	-0.H2O
	27.	-577479+5	302499+5	132 A+2	213126-3-481992+7	68A3P5+2	2500.	6000.1	-0.H2O
	28.	-1 6 1	6 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/61				CC	
	29.	-264169+5	224202+5	779944+1	441449-3-262 21+6	653523+2	500.	2500.1	-0.CO
	30.	-264169+5	223740+5	866947+1	665971-4-155174+6	653761+2	2500.	6000.1	-0.CO
	31.	-1106 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/61				C*	
	32.	-0 0+0	144476+5	550350+1	240 14-3-559635+6	121418+2	500.	2500.2	-0.C*
	33.	-0 0+0	144197+5	526395+1	216128-3 13132E+7	121316+2	2500.	6000.2	-0.C*
	34.	-1 17 1	1 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	9/64				CLH	
	35.	-220529+5	219473+5	705542+1	710907-3-136296+6	623935+2	500.	2500.1	-0.CLH
	36.	-220529+5	218861+5	863263+1	128215-3-964314+6	623719+2	2500.	6000.1	-0.CLH
	37.	-1 9 1	0 1 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	12/68				FH	
	38.	-651399+5	211211+5	641313+1	828856-3 240795+5	587192+2	500.	2500.1	-0.FH
	39.	-651399+5	210707+5	855858+1	138134-3-254239+7	587 11+2	2500.	6000.1	-0.FH
	40.	-1 13 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	12/65				AL	
	41.	779999+5	134785+5	491880+1	303529-4 233929+5	508505+2	500.	2500.1	-0.AL
	42.	779999+5	134527+5	362 42+1	277499-3 427534+7	508413+2	2500.	6000.1	-0.AL
	43.	-1 13 1	7 0 0 0 0 0 0 0 0 0 0 0 0 0 JNAF TAPE 7/71	3/67				ALN	
	44.	104 0+6	239 70+5	883244+1	131622-3-197554+6	703673+2	500.	2500.1	-0.ALN
	45.	104							

153

155

[illegible]

157

397.	1 13 2 17 1 9	U 0 0 0 0 0 0 0	OJANAF TAPE 7/71 9/64	ALCL2F
398.	-18A599+6	524770+5	197633+2	40A103-4-3A5568+6 11A120+3 500. 2500.1
399.	-18A599+6	524717+5	198479+2	366848-5-333708+6 11A113+3 2500. 6000.1
400.	1 13 1 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/69	ALF
401.	-633999+5	240411+5	887470+1	116104-3-161923+6 713971+2 500. 2500.1
402.	-633999+5	240372+5	889563+1	989A96-4-25324A+5 713957+2 2500. 6000.1
403.	1 13 1 9 1 3	0 0 0 0 0 0 0	OJANAF TAPE 7/71 3/64	ALFO
404.	-140199+6	387 28+5	147308+2	647977-4-490235+6 A77 21+2 500. 2500.1
405.	-140199+6	386943+5	148629+2	620618-5-399958+6 876941+2 2500. 6000.1
406.	1 13 2 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 9/64	ALF2
407.	-164999+6	364104+5	137529+2	589260-4-361521+6 935 50+2 500. 2500.1
408.	-164999+6	364 26+5	138732+2	557732-5-279841+6 935 23+2 2500. 6000.1
409.	1 13 3 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	ALF3
410.	-289 34+6	517593+5	196134+2	961594-4-593177+6 10A750+3 500. 2500.1
411.	-289 34+6	51746A+5	198119+2	8A9909-5-47048A+6 10A746+3 2500. 6000.1
412.	2 13 6 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	AL2F4
413.	-629449+6	113740+6	432161+2	186920-3-136338+7 185892+3 500. 2500.1
414.	-629449+6	113715+6	435993+2	176772-4-111393+7 1A58A3+3 2500. 6000.1
415.	1 6 1 17 1 9	1 A 0 0 0 0 0	OJANAF TAPE 7/71 6/61	CCLFO
416.	-01999+6	49931A+5	187407+2	408800-3-939527+6 106163+3 500. 2500.1
417.	-101999+6	49A819+5	196342+2	34642A-4-709 93+6 106145+3 2500. 6000.1
418.	1 6 1 17 3 9	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/69	CCLF3
419.	-169199+6	654737+5	250 18+2	307306-3-125579+7 120684+3 500. 2500.1
420.	-169199+6	654342+5	256454+2	279824-4-913396+6 120670+3 2500. 6000.1
421.	1 6 2 17 2 9	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	CCL2F2
422.	-117499+6	662599+5	252480+2	216872-3-105405+7 125637+3 500. 2500.1
423.	-117499+6	662319+5	25699A+2	198840-4-799570+6 125628+3 2500. 6000.1
424.	1 6 3 17 1 9	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	CCL3F
425.	-689999+5	670140+5	254612+2	13A2A0-3-A52234+6 12A914+3 500. 2500.1
426.	-689999+5	669969+5	257474+2	127695-4-679417+6 12A908+3 2500. 6000.1
427.	1 6 1 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	CF
428.	609939+5	234870+5	660711+1	20A914-3-266925+6 701371+2 500. 2500.1
429.	609999+5	234657+5	843A15+1	1A7354-3 112597+7 701296+2 2500. 6000.1
430.	1 6 1 9 1 7	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/69	CFN
431.	959999+4	370A24+5	13443A+2	512571-3-5A9919+6 8364A9+2 500. 2500.1
432.	959999+4	37023A+5	146279+2	409 1-4-614166+6 836282+2 2500. 6000.1
433.	1 6 1 9 1 8	0 0 0 0 0 0 0	OJANAF TAPE 7/71 12/65	CF0
434.	-409999+5	34E5A0+5	129144+2	35A914-3-624512+6 873417+2 500. 2500.1
435.	-409999+5	34A145+5	137 35+2	304924-4-437467+6 873263+2 2500. 6000.1
436.	1 6 2 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/70	CF2
437.	-434999+5	35397A+5	133694+2	212426-3-618773+6 860687+2 500. 2500.1
438.	-434999+5	354 19+5	117 A3+2	640 47-3 308590+7 A60701+2 2500. 6000.1
439.	1 6 2 9 1 A	0 0 0 0 0 0 0	OJANAF TAPE 7/71 12/69	CF20
440.	-152699+6	491412+5	184618+2	509401-3-112766+7 100635+3 500. 2500.1
441.	-152699+6	490790+5	1957A5+2	435420-4-826862+6 100513+3 2500. 6000.1
442.	1 6 3 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/69	CF3
443.	-112399+6	499352+5	190341+2	307225-3-106 A9+7 103108+3 500. 2500.1
444.	-112399+6	499459+5	196861+2	27626A-4-735969+6 103 95+3 2500. 6000.1
445.	1 6 4 9 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 6/69	CF4
446.	-223 39+6	646124+5	247199+2	413699-3-146A42+7 113647+3 500. 2500.1
447.	-223 39+6	645596+5	255832+2	372280-4-103623+7 11362A+3 2500. 6000.1
448.	2 6 0 0 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 12/69	C2
449.	200223+6	247256+5	766724+1	754223-3 187666+6 685755+2 500. 2500.1
450.	200223+6	246A60+5	843612+1	447170-3 2423A5+6 685615+2 2500. 6000.1
451.	3 6 0 0 0 0	0 0 0 0 0 0 0	OJANAF TAPE 7/71 12/69	C3
452.	195999+6	310530+5	102229+2	100665-2-445919+6 A12712+2 500. 2500.1
453.	195999+6	306869+5	125242+2	230548-3-270248+7 A12476+2 2500. 6000.1

Sample Problem 3 Output

GRAPHITE SURFACE KINETICS (GASKET) PROG. 3

0130000*00

RELATIVE ELEMENTAL COMPOSITIONS, ATOMIC WTS/UNIT MASS

AT.NO.	ELEMENT	ATOMIC WT	EDGE GAS	SURFACE
1	HYDROGEN	1.00800	.0367511	.0000000
6	CARBON	12.01100	.0166646	.0000000
7	NITROGEN	14.00700	.0124297	.0000000
8	OXYGEN	16.00000	.0363751	.0000000
9	FLUORINE	19.00000	.0002268	.0000000
106	GRAPHITE	12.01100	.0000000	.0632570

ELEMENTS	HYDROGEN	CARBON	NITROGEN	OXYGEN	FLUORINE
	GRAPHITE				

BASE SPECIES	H2	CO2	N2	H2O	FH
	C*				

UPDATE OF DIFFUSION FACTORS

SPECIES	DIFFUSION FACTOR
CO2	1.29140
H2	.38930
H2O	.77490
N2	1.02620
CO	1.01700
C	.69180
CH	.74920
CH4	.93570
CN	1.02670
C2H2	1.17460
H	.30160
N	.74930
NO	.99810
O	.73970
O2	1.00000
C2	1.02530

Sample Problem 3 Output (Continued)

GRAPHITE SURFACE KINETICS (GASNET) PROC. 3

5002700040

6 6

CD=PROZEN = .40642+00

PROPERTY ROUTINE OUTPUT IN LH=MASS,FT,SEC,HTU,AREA,IF=H
 TEMP VISC COND DENS TR SC
 .00200+00 .32202+04 .21946+04 .20799+03 .59990+00 .72560+00
 MU1 MU2 POL,WT HTL CPVTL PTLA
 .91000+00 .24522+02 .74222+02 -.22304+04 .65100+00 -.22777+04

ELEMENTAL X AND Z MASS FRACTIONS BY ATOMIC NUMBER (BAREN = .667)
 1 6 7 8 9 10A
 .34707-01 .20209+00 .16974+00 .30842+00 .42026+04 .00000
 .00037-01 .10074+00 .16924+00 .34775+00 .46136+02 .00000

SOLUTION TIMES
 ITERATIONS = 9 TIME = 2.00A SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
 MASS TRANSFER COEFFICIENT HOCUP = .24400+00
 AND V WALL/RHCE UE CM = .36549+00 RPHIME = .36509+05

STATE ADJACENT TO THE SURFACE
 TEMP = 2920.0000 DEG R = 1400.0000 DEG K PRESS = 12.7700 ATM

	GAS	CONDENSED	COMPOSITE
ENTHALPY - BTU/LBM	-.23210+04	.00000	-.23210+04
ENTROPY - BTU/LBM DEG R	.22778+01	.00000	.00000
DENSITY - LBM/FT3	.17234+00		.17234+00
MOLECULAR WEIGHT	24.0277	.0000	24.0277

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS

(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHCE UE CM) . . .
 1a .20622-11 2a .20394-10 3a .62277-15 4a .14100-10 5a .52247-21
 6a .12444-20 7a .11020-25 8a .10443-27

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES

1a .20444+03 2a .20444+03 3a .41413+05 4a .20444+03 5a .41413+05
 6a .39606+07 7a .34961+02 8a .33290+00

CHEMICAL STATE ADJACENT TO THE SURFACE

(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES)
 (MOLE FR FOR CONDENSED = RPHIME CONDENSED)

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
COS	.20660+00	M2	.13763+00	N2O	.20701+00	C6	.00000	FM	.54917-02
N2	.15006+00	CO	.21270+00	C	.12225-21	HO	.20168-07	N03	.27003-29
CH	.24604-19	CH4	.34500-06	CHNO	.62813+07	CHD	.31555-08	CH2	.34602-15
CH2O	.32602-04	CH3	.43417-09	CH4	.49644-05	CN	.60089-10	CNO	.19360-13
CH2 NCN	.02424-19	C2H	.23449-16	C2H2	.46792-11	C2H4	.12399-10	C2HNO	.50602-17
C2H	.26030-19	C2H2	.18655-14	C2O	.42104-14	C3O2	.26190-13	C4H	.62090-25
C2H2	.41220-22	C4H2	.20810-25	H	.50230-06	HN	.36064-12	MNO	.90543-13
MNO2 TR	.60216-14	MNO3	.20508-24	HO2	.51714-16	M2H	.11257-08	M2N2	.38256-14
N2O2	.30374-13	H3N	.21726-04	M4N2	.10715-15	V	.42360-15	NO	.19767-09
N02	.20066-17	N2O	.17162-13	N2O3	.14489-31	O	.68069-13	O2	.60927-13
C2H6	.96498-12	C2H3	.73364-15	C3H	.62367-20	C3H2	.11281-19	C3H3	.05090-10
C3H4	.17992-16	C3H5	.26672-15	F2	.29367-24	CHF	.50361-17	CHFO	.14526-08
CHF3	.13191-18	CH2F2	.49591-15	CH3F	.63194-11	C2F2	.60764-28	C2F3H	.94375-20
C2F4	.95265-34	C2HF	.65967-14	F	.26389-12	CFH	.35534-16	FF	.10407-20
FWO	.10522-18	FWO2	.74180-20	FWO3	.00000	FO	.60793-22	FO2	.16645-27
FWN	.20079-20	FWN2 TR	.76466-34	FO	.32145-14	F3H	.34429-33	F3NO	.00000
CF	.77779-19	CFN	.79470-15	CFU	.14415-12	CF2	.33902-18	CF2O	.12005-11
CF3	.34321-23	CF4	.41522-23	C2	.13842-26	C1	.43170-27	C4	.19044-35
CS	.14004-37								

Sample Problem 3 Output (Continued)

GRAPHITE SURFACE KINETICS (GASKET) SOLUTION

PROG. 3

DERIVATIVE PROPERTY OUTPUT

CP-FROZEN	CP-EQUIL	DLNM/DLMT	DLHM/DLHP	GAMMA
.46249+00	.65564+00	-.99470-01	.44135-02	.11752+01

PROPERTY ROUTINE OUTPUT IN LB-MASS, FT, SEC, BTU, AND DEG-R

TEMP	VISC	CONU	UHAR	PR	SC
.50505+04	.51724-04	.39360-04	.76050-03	.60777+00	.72573+00
MU1	MU2	MOL.WT	HTIL	CPTIL	HTIL*
.90353+00	.24443+02	.23866+02	-.76863+03	.54365+00	-.90189+03

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GAMEX = .667)

1	6	7	8	9	106
.37025-01	.20256+00	.17410+00	.38200+00	.43097-02	.00000
.49537-01	.18874+00	.16429+00	.58775+00	.46436-02	.00000

SOLUTION TIMES

ITERATIONS = 38

TIME = 13.699 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .00000
 TEMP = 5050.4579 DEG R. = 2805.4100 DEG K. PRESS = 12.77800 ATM

ENTHALPY - BTU/LHM	GAS	CONDENSED	COMPOSITE
	-.10389+04	.00000	-.10389+04
ENTROPY - BTU/LHM DEG R	.26582+01	.00000	.26582+01
DENSITY - LBM/FT3	.82678-01		.82678-01
MOLECULAR WEIGHT	23.8660	.0000	23.8660

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.	SPECIES	MOLE FR.
C02	.12957+00	H2	.10109+00	H2O	.32744+00	C*	.00000	FW	.54117-02
N2	.14795+00	CO	.27292+00	C	.77738-11	H0	.67376-02	N03	.39440-13
CH	.61978-11	CH*	.22775-06	CH10	.11414-06	CH0	.24462-05	CH2	.83245-11
CH20	.20104-06	CH3	.23200-09	CH4	.13789-09	CH	.17571-08	CH0	.39465-08
CN2	.18493-12	C2H	.81423-13	C2H2	.69146-12	C2H4	.22745-15	C2H40	.10719-14
C2H	.48730-14	C2H2	.88703-14	C20	.94466-11	C302	.53113-13	C4H	.29314-23
CHH2	.72762-24	CH42	.17134-25	H	.73962-02	H0	.66530-06	H40	.38493-06
HNO2	.11660-07	H403	.34432-12	H02	.53589-06	H2N	.84655-06	H2N2	.22739-10
H202	.30976-06	H41	.12701-05	H4H2	.46335-14	N	.39010-06	N0	.74492-03
N02	.70996-07	H20	.58228-07	H203	.37731-15	O	.31381-03	O2	.41419-03
C2H6	.21207-19	C2H5	.26796-15	C3H	.62186-18	C3H2	.29627-19	C3H3	.58945-20
C3H4	.27923-21	C3H5	.48241-21	F2	.01304-14	CHF	.24473-12	CHF0	.24447-08
CHF3	.12704-18	CH2F2	.72442-16	CH3F	.54603-13	C2F2	.33636-22	C2F3H	.28234-26
C2F4	.39976-30	C2HF	.13616-16	F	.17095-05	F40	.11542-08	FN	.87972-11
FNO	.87045-10	FNO2	.94423-15	F403	.20093-21	F0	.42544-10	F02	.32441-12
F2N	.57401-17	F2H2	.11121-21	F20	.23175-18	F3H	.95160-25	F3N0	.17392-29
CF	.16741-11	CF*	.17162-11	CF	.24658-08	CF2	.61495-14	CF20	.75542-11
CF3	.72827-19	CF4	.42456-22	C2	.34436-16	C3	.55451-20	C4	.88845-28
C5	.24395-32								

Sample Problem 3 Output (Continued)

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GRAPHITE SURFACE KINETICS (GASNET) PROR. 3      0000000000

DERIVATIVE PROPERTY OUTPUT
CP-FROZEN      CP-EQUIL      DLNM/DLNT      DLNM/DLNP      G6HFA
.38462+00      .19183+01      -.27575+00      .44135+02      .10709+01

PROPERTY ROUTINE OUTPUT IN LB-MASS.FT.SEC.RTU.AND DEG-R
TEMP      VISC      COND      DHAN      PR      SC
.18000+04      .26207-04      .16470-04      .15753-03      .61201+00      .72573+00
MU1      MU2      MOL.WT      HTIL      CPTIL      HTIL*
.90353+00      .24443+02      .23866+02      -.24210+04      .44749+00      -.24385+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GANEY = .667)
      1      6      7      8      9      106
.37025-01      .20256+00      .17410+00      .58200+00      .43097-02      .00000
.49537-01      .18874+00      .16929+00      .58775+00      .46836+02      .00000

SOLUTION TIMES
ITERATIONS = 38      TIME = .252 SEC.

CLOSED SYSTEM EQUILIBRIUM SOLUTION OUTPUT

MASS CONDENSED/MASS GAS = .00000
TEMP = 1800.0000 DEG K. = 1000.0000 DEG K.      PRESS = 12.77400 ATM

ENTHALPY - RTU/LBM      GAS      CONDENSED      COMPOSITE
-.24353+04      .00000      -.24353+04
ENTROPY - BTU/LBM DEG K      .22222+01      .00000      .22222+01
DENSITY - LBM/FT3      .25186+00      .0000      .25186+00
MOLECULAR WEIGHT      25.8660      .0000      25.8660

CHEMICAL STATE (MOLE FR. = MOLECULES / TOTAL GAS PHASE MOLECULES).....

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .12957+00      H2      .10109+00      H2O      .15274+00      C4      .00000      PH      .54117-02
N2      .14795+00      CO      .27242+00      C      .77738-11      H0      .00000      F0      .39443-13
CH      .61978-11      CH4      .262775-06      CH3O      .11414-06      CH0      .24462-05      CH2      .63245-11
CH2O      .20108-06      CH3      .25200-09      CH4      .13784-04      CH      .17571-08      CH0      .39465-08
CN2      .18443-12      C2H      .01523-13      C2H2      .69146-12      C2H4      .22785-15      C2H4O      .10715-18
C2N      .48730-14      C2N2      .69703-14      C2O      .94466-11      C3O2      .51115-13      C4H      .29314-23
C4H2      .72782-24      C4H2      .17314-25      H      .74462-02      H4      .44530-06      H2O      .38495-06
HN02      .11660-07      HN03      .24432-12      H02      .55449-06      H2H      .22789-10
H2O2      .30976-06      H3O      .12701-05      H4H2      .64335-14      V      .39010-06      H2N2      .74442-03
N02      .70996-07      N2O      .58224-07      N2O3      .77731-15      O      .31351-03      O2      .41419-03
C2H6      .21207-19      C2H3      .25746-15      C3H      .62186-14      C3+2      .29627-19      C3H3      .58945-20
C3H4      .27923-21      C3H5      .48241-21      F2      .41304-14      CHF      .24473-12      CHF0      .28647-08
CHF3      .12704-18      CH2F2      .72442-16      CH3F      .44603-13      C2F2      .35638-22      C2F34      .24234-26
C2F4      .39976-30      C2HF      .13-16-16      F      .17095-05      FH0      .11542-08      F4      .87972-11
FNO      .87085-10      FNC2      .44423-15      FNO3      .20043-21      FO      .42544-10      FO2      .32441-12
F2N      .57401-17      F2H2      .11121-21      F2O      .23175-14      F3H      .39160-25      F3NO      .17392-29
CF      .16741-11      CF4      .17162-11      F0      .24459-08      CF2      .41495-14      CF2O      .75542-11
CF3      .72827-19      CF4      .42446-22      C2      .34436-14      C3      .54451-20      C4      .64445-28
CS      .24345-32

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Sample Problem 3 Output (Concluded)

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CO-FROZEN = .5430E+00

PROPERTY ROUTINE OUTPUT IN LG-PASS,RT-SEC,PTO-APP DEG-K
TEMP      VISC      CORR      DENS      EN      SE
.2160E+04 .2695E-04 .1940E-04 .1654E-03 .5705E+00 .725E+00
MU1      MU2      MOL WT      ITTL      DTTL      ITTL
.9236E+00 .2450E+02 .2416E+02 .2412E+04 .4777E+00 .2454E+04

ELEMENTAL K AND Z MASS FRACTIONS BY ATOMIC NUMBER . . . (GASEX = .667)
      1      2      3      4      5      6      7      8      9      10
.3368E-01 .2030E+00 .1660E+00 .5411E+00 .4156E-02 .000000 .000000 .000000 .000000 .000000
.4953E-01 .1847E+00 .1692E+00 .5477E+00 .4663E-02 .000000 .000000 .000000 .000000 .000000

SOLUTION TIMES
ITERATIONS = 9          TIME = 2.474 SEC.

OPEN SYSTEM CHEMICAL KINETICS SOLUTION OUTPUT

SURFACE IS PC 901
MASS TRANSFER COEFFICIENT HMOX = .2460E+00
RHO V WALL/RHCE DE CM = .744E-12  PRIME = .744E-12

STATE ADJACENT TO THE SURFACE . . .
TEMP = 2160.0000 DEG K  PRESS = 12.77E+00 ATM

      GAS      CONDENSED      COMPOSITE
ENTHALPY = BTU/LBM      -2.2405E+04      .000000      -2.2405E+04
ENTROPY = BTU/LBM DEG K .2183E+01      .000000      .2183E+01
DENSITY = LBM/FT3      .2040E+00      .000000      .2040E+00
MOLECULAR WEIGHT      25.1859      .000000      25.1859

NET FORWARD RATE OF KINETICALLY CONTROLLED REACTIONS
(MOLES OF REACTION / UNIT SURFACE AREA / TIME / RHO DE CM) . . .
1= .3414E-14  2= .5493E-13  3= .6283E-14  4= .5508E-23  5= .3492E-25
6= .1293E-25  7= .1147E-31  8= .9612E-34

RATIO OF FORWARD TO REVERSE KINETICALLY CONTROLLED PRODUCTION RATES
1= .2814E+02  2= .2814E+02  3= .7919E+03  4= .2814E+02  5= .1125E+02
6= .4163E+02  7= .3692E-04  8= .3093E-06

CHEMICAL STATE ADJACENT TO THE SURFACE
(MOLE FR FOR GASES = MOLECULES / TOTAL GAS MOLECULES )
(MOLE FR FOR CONDENSED = GRIFF CONDENSED) . . .

SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.      SPECIES      MOLE FR.
CO2      .2394E+00      H2      .1522E+00      H2O      .2654E+00      CO      .000000      CO2      .5512E-02
N2      .1510E+00      CO      .1860E+00      C      .5078E-25      H2O      .2481E-09      CO      .1204E-34
CH      .3904E-22      CH4      .3944E-06      CH2O      .5119E-07      CH2O      .5311E-09      CH2      .1201E-16
CH2O      .3756E-04      CH4      .5220E-09      C4H      .1E-23E-03      C4H      .4015E-16      C4H      .3341E-15
C2H      .6565E-21      C2H      .1449E-17      C2H2      .2320E-10      C2H4      .4711E-09      C2H4      .2339E-16
C2N      .4544E-21      C2H2      .1152E-14      C2H      .1649E-17      C4H2      .2489E-13      C4H      .1705E-25
C4H2      .1604E-21      C4H2      .3554E-25      H      .2144E-07      H      .2469E-14      H2O      .5637E-15
HNO2 TR      .1092E-18      H2O3      .1907E-24      H2O2      .2369E-19      H2O2      .1223E-09      H2N2      .2184E-15
H2O2      .1410E-14      H3E      .560E-04      H4O2      .6347E-16      V      .4447E-14      CO      .1274E-11
N2O      .1012E-20      N2O      .1205E-15      O2O3      .3747E-17      O      .4301E-16      O2      .3834E-16
C2H6      .3959E-09      C2H3      .1072E-14      C3H      .1512E-20      C3H2      .8502E-20      C3H3      .4477E-17
C3H4      .7606E-15      C3H5      .2364E-13      F2      .1E-12E-27      CH4      .1101E-14      CH4      .1172E-08
CHF3      .1440E-14      CH2F2      .1E-07E-14      F2O3F      .4454E-10      C2F2      .7428E-30      C2F3N      .3725E-28
C2F4      .6994E-35      C2HF      .1144E-14      F      .1457E-14      FNO      .1129E-13      FN      .5359E-24
FNO      .1171E-21      FNO2      .3470E-32      F2O3      .000000      F2O      .5527E-26      F2O      .1402E-32
F2N      .5552E-32      F2N2 TR      .7761E-34      F2O      .000000      F3N      .000000      F3NO      .000000
CF      .2784E-21      CF4      .6347E-14      CF2O      .4454E-14      CF2      .1201E-19      CF2O      .6915E-12
CF3      .1355E-24      CF4      .2222E-24      C2      .4544E-10      C4      .1549E-29      C4      .5336E-18
C5      .000000

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