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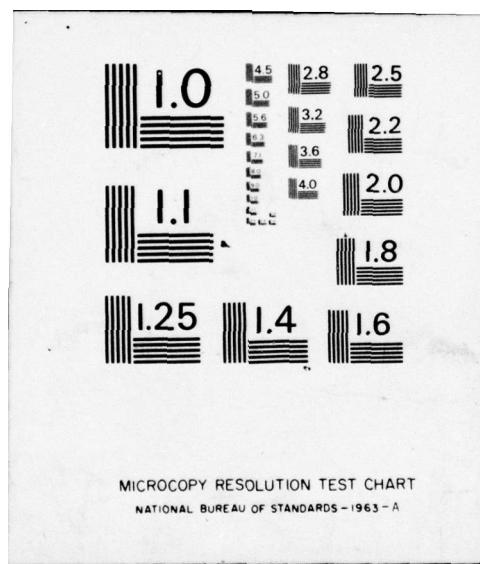
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REPORT NO. R-TR-76-018

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AIR DEFENSE ANALYSIS
THE INFLUENCE OF PARAMETRIC VARIATION
ON EFFECTIVENESS OF A SHORT RANGE
AIR DEFENSE SYSTEM
TECHNICAL REPORT

PREPARED BY
CHARLES S. HICKS, P.E.



JANUARY 1976



RESEARCH DIRECTORATE

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A performance analysis of a generic 30mm air defense gun system was undertaken to determine what factors influence effectiveness of such a system. A computer model that produces contours of constant kill probability vs range was employed. The significant results and conclusions are as follows: (1) A new effectiveness measure called Weighted Kill Area (WKA) was developed.		

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- (2) Curves were produced showing the influence of parameter changes on effectiveness.
- (3) High effectiveness can be achieved in two basically different ways.
- (4) A trade-off study is needed to determine which is the most cost effective way to get high effectiveness.
- (5) Several factors that influence effectiveness could not be covered within the scope of this study. They should be the object of further investigation. Among them are time-of-flight variation, improvements to the computer model, round lethality improvements, and correlations between biases and standard deviations on target position measurement.

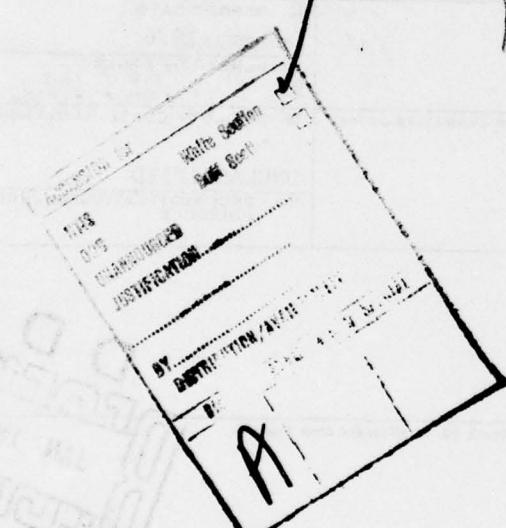


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1.0 INTRODUCTION

This report covers work done under the Automatic Cannon Technology program which is part of an ongoing effort to develop improved firepower to meet future tactical threats to Army field units.

1.1 Objectives

- a. Conduct parametric sensitivity analysis of short range air defense system concepts.
- b. Develop a data base from these analyses that will aid in formulating advanced air defense system configurations.
- c. Develop an effectiveness measure that is related to kill probability, and can be used to rate the effectiveness of competing systems and concepts.
- d. Determine the effectiveness of air defense gun systems designs that utilize the concept of high accuracy and low rate of fire.
- e. Determine possible parametric relationships that could help the designer and analyst define an effective air defense system.

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2.0 CONCLUSIONS AND RECOMMENDATIONS

2.1 Conclusions

2.1.1 The results of the parametric sensitivity analysis show that equally high effectiveness can be achieved by both very accurate, low-rate-of-fire gun systems and less accurate, high-rate-of-fire gun systems.

2.1.2 It is possible to achieve almost any reasonable value of effectiveness by employing a high enough rate of fire in a system with average biases and standard deviations, or conversely, employing a very low rate of fire in a system with zero biases and very small standard deviations.

2.1.3 Accurate low rate of fire systems tend to have high, narrow effectiveness peaks centered about a precise value of gun barrel dispersion. Increased biases and standard deviations broaden and reduce the peaks making effectiveness lower, but also less sensitive to changes in gun parameters.

2.1.4 The results of the study also indicate that biases and standard deviations on measurement of target position must be approximately equal to each other to achieve peak effectiveness in any given system.

2.1.5 The Weighted Kill Area (WKA) concept, developed as an adjunct to the ISO PK simulation, has proved to be a useful effectiveness measure for rating air defense system performance.

2.1.6 Finally, a data base has been developed and converted into a set of curves which indicate the relationship of the various gun system parameters to performance effectiveness. This will be an aid to the designer in developing advanced air defense system concepts.

2.2 Recommendations

2.2.1 It is recommended that a trade-off study be made to determine which is the most cost-effective approach to producing an effective system; the precision low-rate-of-fire system that is difficult to maintain and calibrate in the field, or the high-firing rate system that is easier to maintain and calibrate, but uses great quantities of ammunition.

2.2.2 Several other factors that influence air defense gun system effectiveness could not be investigated within the scope of this study. Any future air defense gun system effectiveness study should include these items:

- a. Develop modifications to ISO PK to improve its sensitivity to certain parameters, incorporate the WKA calculations, and develop a way to compute engagement Probability of Kill (P_K).
- b. Determine the influence of improved ammunition effectiveness; specifically the effects of increased round lethality and reduced time of flight.
- c. Determine the exact location and shape of the effectiveness peak of the low-rate-of-fire system and the effect on it of gun barrel dispersion and muzzle velocity variation.
- d. Investigate in greater detail the effect of gun pointing bias on effectiveness.
- e. Investigate in greater detail the influence on effectiveness, of biases and standard deviations on target position measurement.
- f. Investigate and try to develop improved methods for modeling advanced fire-control techniques using non-linear prediction against maneuvering targets.

3.0 DISCUSSION

3.1 Method of Approach

The simplest approach seemed to be to exercise one gun system through many variations, and using a proper measure of effectiveness determine what relationships exist. This approach required that a gun system representative of the state-of-the-art, and having reasonable growth potential, be chosen; that a proven and versatile simulation model be available; and that a useful means of measuring effectiveness be available or be developed. How each of these requirements was met is discussed in following sections.

3.1.1 Choice of gun system - The many recent air defense gun studies conducted under the Low Altitude Forward Area Air Defense System (LOFAADS) requirement influenced the choice of gun system used in this study. The choice is a 30mm system using improved GAU-8 ammunition, and having many of the performance characteristics appropriate to the Division Air Defense Study (DIVADS) and the Army Radar Gun Air Defense System (ARGADS) Required Operational Capability (ROC).

3.1.2 Choice of computer model - The choice of the computer simulation suitable for this study was influenced mainly by two requirements:

a. It had to be a general model that could reliably simulate a wide range of gun systems.

b. It had to be thoroughly "debugged" - in other words, a model on which enough experience has been gained that the results can be accepted with a high degree of confidence. Of the models available, ISO PK best fits these requirements. It is described in the following section:

3.1.2.1 Computer model description - ISO PK is a deterministic computer model employing a burst kill algorithm to evaluate the relative effectiveness of high-rate of fire air defense gun systems using burst fire modes. It simulates a one-gun-on-one-target encounter and plots the results of one burst independent of all other bursts at all points within a specified range of the gun. In this study, low-rate-of-fire modes are simulated by reducing the number of rounds in a burst to one, or a few. The burst kill algorithm that is used can be derived from its basic assumptions. Let:

AV be the vulnerable area of the target

BKP(t) be the burst kill probability function

(R_1, R_2) be the burst center coordinate

(X_1, X_2) be the projectile coordinate

n be the number of rounds per burst

where the coordinates are in "azimuth-like" and "elevation-like" coordinates in the plane perpendicular to the line-of-sight of the gun to the target.

Assume the X_1, X_2 are independently distributed where:

$$X_i \sim N(R_i, \sigma_{i+2}^2), i = 1, 2$$

Also assume that R_1, R_2 have a bivariate normal distribution with marginal distribution,

$$R_i \sim N(\mu_{i+2}, \sigma_{i+2}^2), i = 1, 2$$

and correlation ρ . The variances σ_1^2, σ_2^2 will result from the dispersion introduced by muzzle velocity variation and gun dynamics. The remaining errors are accounted for in the distribution of (R_1, R_2) .

For fixed t we have

$$BKP = E \left\{ \frac{nAV}{2\pi\sigma_1\sigma_2} e^{-\frac{1}{2\sigma_1^2 + 2\sigma_2^2}} \left(\frac{R_1^2}{\sigma_1^2} \frac{R_2^2}{\sigma_2^2} \right) (R_1, R_2) \right\}$$

The expected value can be solved in and expressed in matrix notation,

Let

$$V = \begin{bmatrix} \sigma_3^2 & \rho \sigma_3 \sigma_4 \\ \rho \sigma_3 \sigma_4 & \sigma_4^2 \end{bmatrix} \begin{bmatrix} \mu_3 \\ \mu_4 \end{bmatrix}$$

Now, there exists an orthonormal matrix P such that

$$P' V P \begin{bmatrix} 1 & 0 \\ -\frac{1}{\alpha_1} & 1 \\ \frac{\alpha_1}{\alpha_2} & 0 \\ 0 & \frac{1}{\alpha_2} \end{bmatrix} = K^2.$$

Set

$$A = K' P' \begin{bmatrix} 1 & 0 \\ -\frac{1}{\sigma_1^2} & 1 \\ \sigma_1 & 0 \\ 0 & -\frac{1}{\sigma_2^2} \end{bmatrix} PK.$$

Then

$$BKP = \frac{nAV}{2\pi\sigma_1\sigma_2 \left| I+A \right|^{\frac{1}{2}}} \exp \left\{ -\frac{1}{2} V' A \left[I - (I+A)^{-1} A \right] V \right\}$$

The output of the model is in the form of a plot of isometric lines of constant kill probability. The inputs to ISO PK consist of:

- a. Target and flight path data
- b. Target sensor data
- c. Gun and ammunition characteristics
- d. Output plot dimensions

The target flies straight and level at a constant velocity from right to left across the plot. The target speed and altitude can be specified, and a plot of ISO PK contours in a horizontal plane at that altitude, is produced.

The sensor input data consist of mean measurement errors and standard deviations on six parameters of target position: range, azimuth angle, elevation angle, and their respective rates.

The gun and ammunition input data are: mean muzzle velocity and its standard deviation, range vs. time-of-flight of the projectile, means and standard deviations of gun pointing errors, standard deviation of residual gun barrel dispersion, maximum tracking angle rates, maximum

achievable gun barrel elevation angle, and number of rounds fired in the burst.

By varying these inputs it is possible to optimize a system within constraints, such as computer model limitations or practical limitations on parameter values. The problem of determining when a system is "optimized" is a complex one which is discussed in the next section.

3.1.3 Choice of effectiveness measure - The amount of data generated during this study made it necessary to broadly categorize the systems into three groups as an aid to evaluating the results.

These three are defined strictly on the basis of input error budgets to the ISO PK model. In the conventional sense, category 1 systems could be called "super accurate." All system biases are zero, standard deviations on gun pointing are zero, or very small; and standard deviations in measured target position are zero, or very small. A category 1 system could be considered as beyond the present state-of-the-art, at least in some of its characteristics.

Category 2 systems are "accurate;" that is, biases and standard deviations are all quite small, but achievable at the limit of the present state-of-the-art.

Category 3 contains the "field systems." These have biases larger than necessary, indicating that the system requires calibration; large gun pointing sigmas, indicating perhaps the need for servo system maintenance; and large target sensor sigmas, which indicate a need for sensor tuning and maintenance, and so forth.

A criterion for ranking air defense gun systems according to effectiveness is difficult to choose because there are many possible definitions of effectiveness. Some definitions are too complex to be easily understood, and others are simple, but don't give a complete definition. What system analysts and decision makers desire is a measure of effectiveness that can be expressed as one number which describes the gun system's ability to defeat aerial threats - in other words, be related to Probability of Kill, (P_K). This is attractive because P_K best describes a gun's purpose. However, P_K varies with range, and used by itself, raises more questions than it answers. What P_K at what range best describes

effectiveness? Is a system that produces high P_K at short range coupled with low P_K at medium and long ranges more effective than a system that has medium P_K at short and medium ranges, with low P_K only at long range?

The answer may depend somewhat on the scenario, but it is difficult to subjectively compare ISO PK plots of several systems and rank them based on the several P_K 's and ranges that appear on each plot.

The measure of effectiveness developed during this project is a number related to P_K . It is called Weighted Kill Area and is in units of square kilometers. WKA is computed directly from the output plot of the ISO PK program. Reference to Figure 1 will help clarify the following description of how WKA is computed: The incremental areas contained between successive P_K contours are computed and multiplied by the P_K value of the outer contour in each case. All these areas are then summed and their total becomes the system WKA. A larger WKA value indicates greater effectiveness in killing targets. Each value of WKA applies to a particular gun system against a particular target. It changes appreciably if either gun system characteristics or target scenario (target size, speed, and altitude) are changed. The method appears to be a sensitive indicator of system effectiveness and easily produces relative rankings on groups of systems. The reader can check for himself the difficulty of evaluating gun systems by mentally ranking the four systems whose plots are shown in Figures 2 through 5. The WKA ranking of these systems is given in Appendix A along with the input data for each system.

A computer code (program) has been developed to make the WKA calculation and rank the systems in descending order. It assumes that the P_K contours are ellipses symmetrically disposed about the gun. In certain cases the contours depart from the elliptical shape, and to that extent the results are an approximation. Worthwhile improvements to this method of computing effectiveness could be made by developing a routine to calculate the actual area under the contours by subtracting the small area immediately surrounding the gun where in some cases target angular rates exceed gun slewing rates, and by incorporating the program into ISO PK as a subroutine.

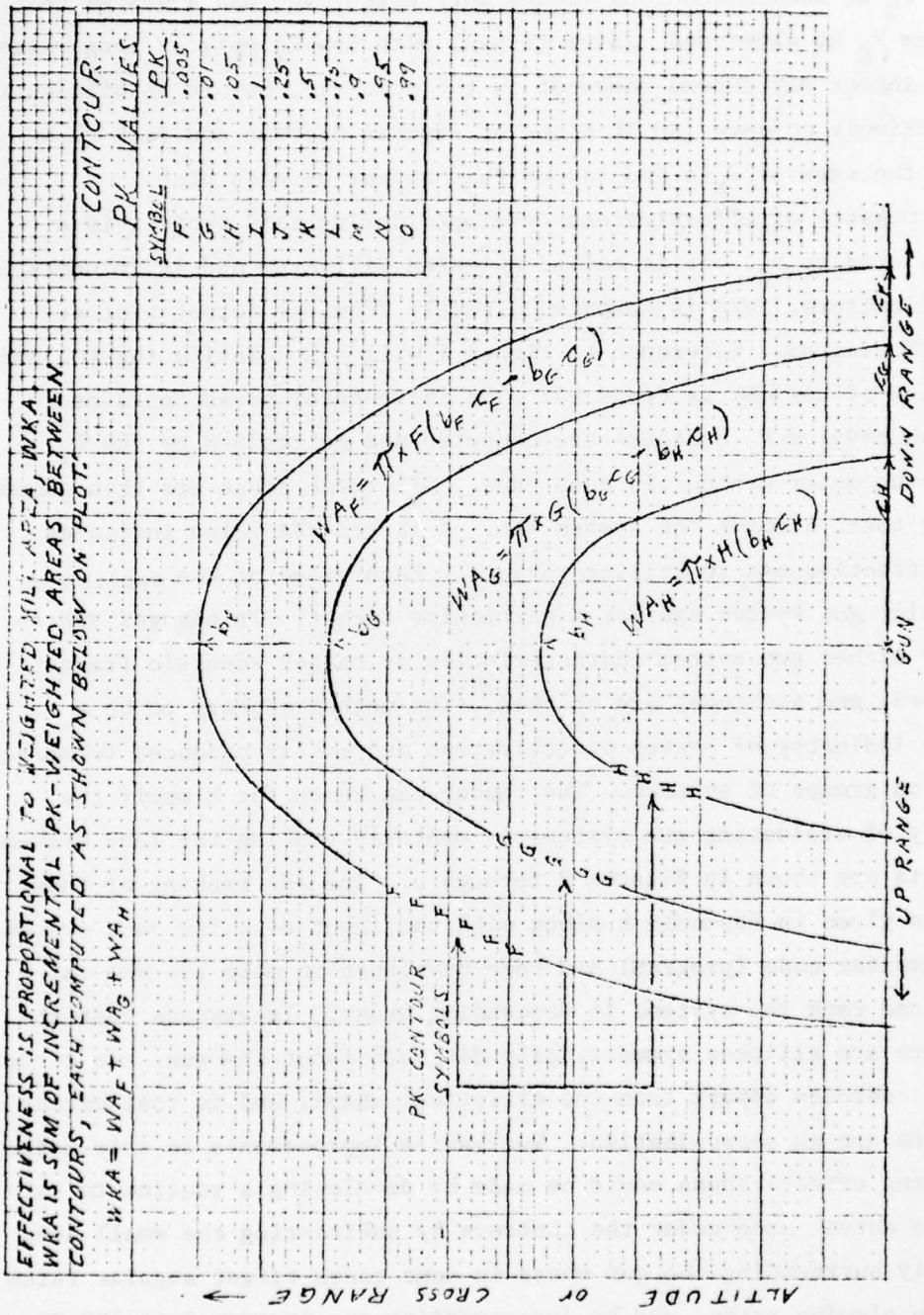


Figure 1 Computation of Effectiveness Measure, WKA

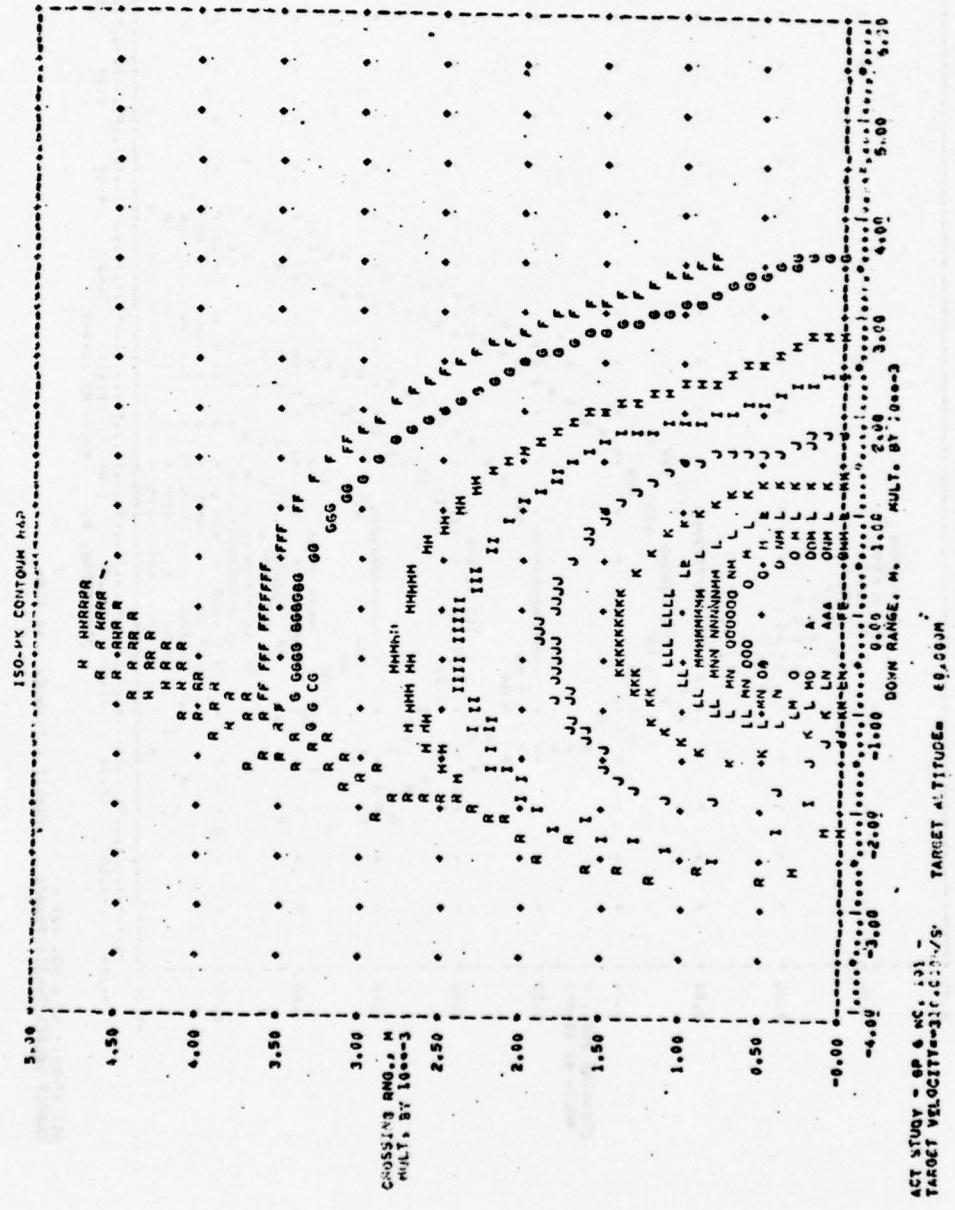


Figure 2 ISO PK Plot, System 101

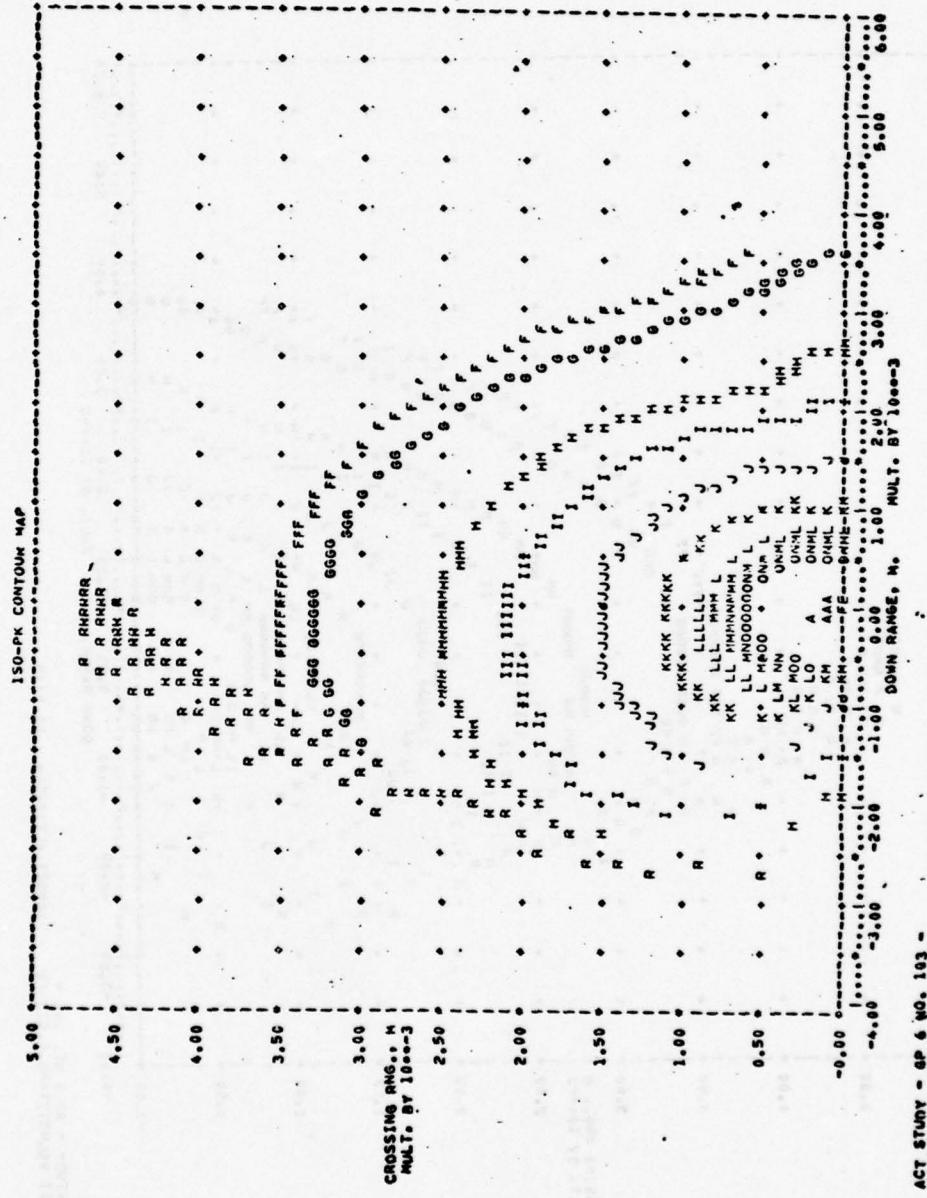
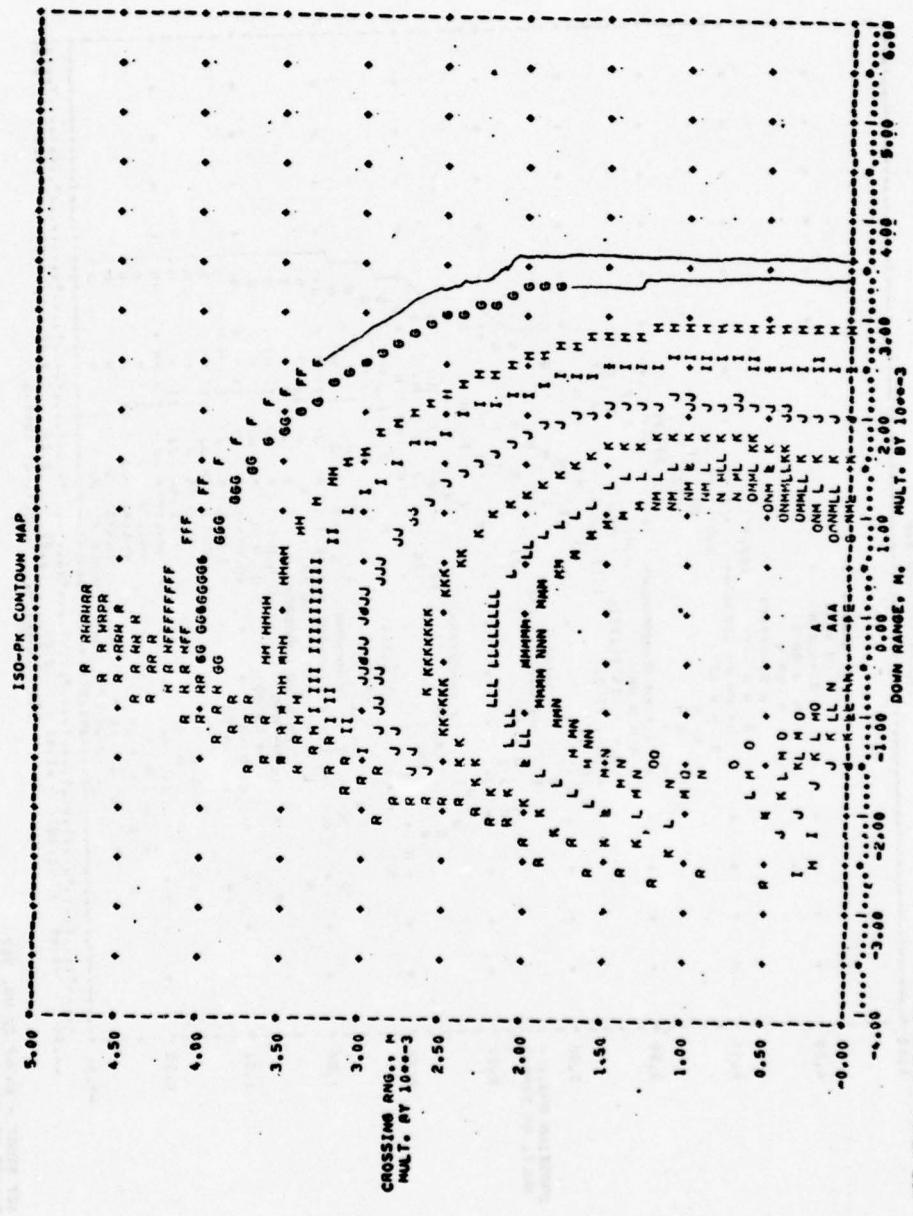


Figure 3 ISO PK Plot, System 103



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Figure 4 ISO PK Plot, System 358

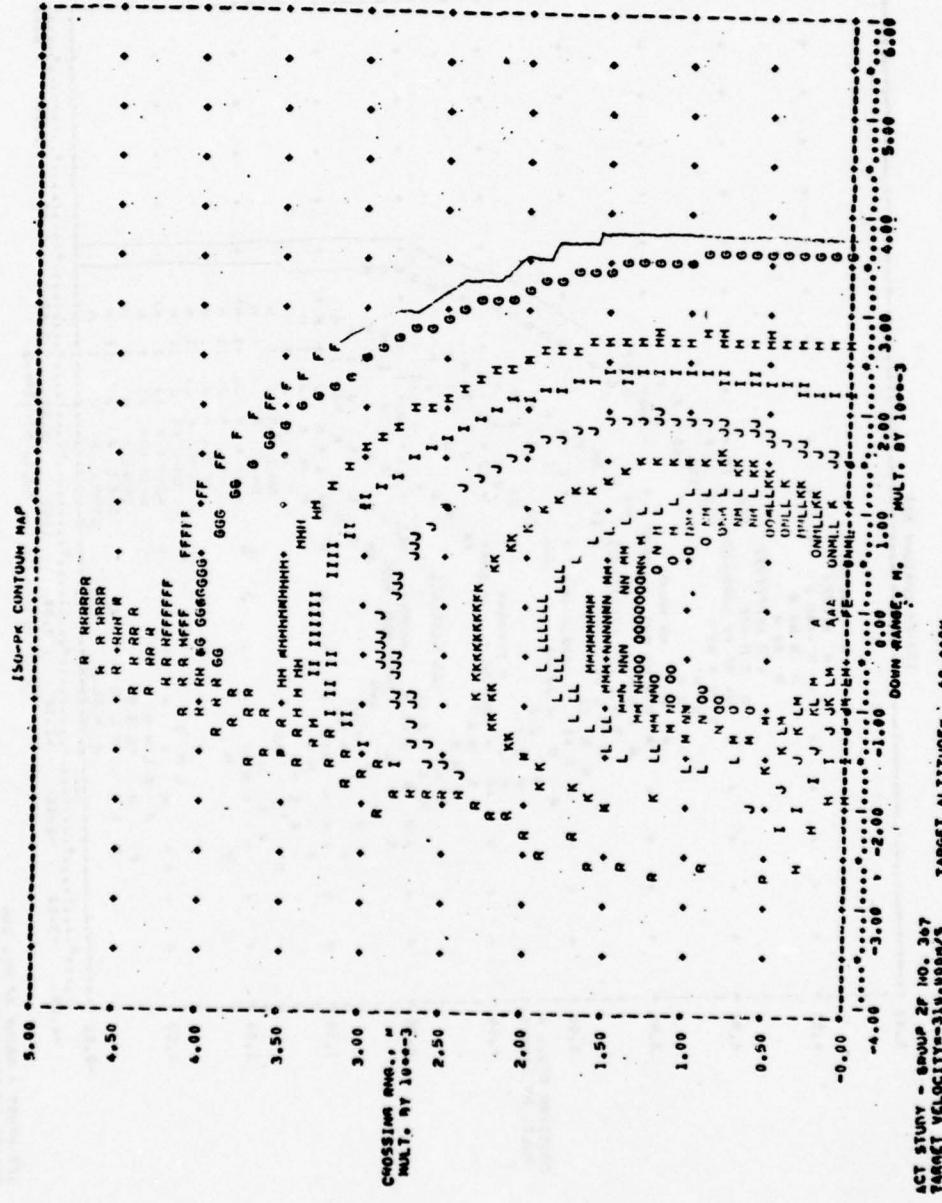


Figure 5 ISO PK Plot, System 367

3.2 Development of the Data Base

Thirty five gun and ammunition parameters, 20 target parameters and 10 to 15 plot parameters can be varied in the ISO PK model. This situation creates an unmanagable number of possible variations, therefore as many variables as possible, were eliminated from consideration. A constant plot size was adhered to throughout the study; the same target aircraft was used; and the same ammunition was used.

The parameters that were actually varied include the following:

- a. Standard deviation of muzzle velocity.
- b. Standard deviation of residual gun barrel dispersion in two axes.
- c. Number of rounds fired in a burst.
- d. Gun pointing bias in azimuth and elevation.
- e. Six biases (mean error) on sensor derived target position, (x, y, z, and their rates).
- f. Standard deviations of dynamic gun pointing error in azimuth and elevation at several slewing rates.
- g. Standard deviation of sensor derived target position (x, y, z, and their rates).

These parameters were judged to have the most influence on effectiveness. The others generally contribute to system effectiveness in a highly predictable, monotonic fashion, and therefore were fixed at "good design values."

Even with the number of variables reduced to a minimum in this fashion, computer runs were made on some 370 variants of the system. These runs were divided into groups; each group being an investigation of some particular aspect of the parametric correlations being discovered. There are about 30 groups, not all of which produced any useable information. The ones which did are reduced to plots and discussed in the next section. Appendix B contains the input data and output plot of the system ranked No. 1 in each plot group.

3.3 Discussion of Results

Group 1 was a special group of 26 runs designed to check out the ISO PK model limitations. When doing parameter studies, it is possible to cause an "underflow" or "overflow" in the PK algorithm by extreme variation

of input values and it is necessary to find these limits. Two limitations were found: Standard deviations of gun barrel dispersion equal to zero, and standard deviations of sensor-derived target position and rate equal to zero. These parameters are limited on the low side therefore, to small finite values. The minimum values of sensor sigmas (σ_R , σ_{AZ} , σ_{EL} , σ_R , σ_{AZ} , σ_{EL}) were arbitrarily set to the smallest values that would print out (.0001 meter, .0001 radian, etc). The program format could have been changed to print smaller values, but no additional information would be gained.

Some peculiarities were noted in the group 1 series about the influence of muzzle velocity variation and gun barrel dispersion on effectiveness, so this was investigated first. The results are given in Figures 6, 7, 8, and 9, in plots of effectiveness versus dispersion.

Figure 6 contains three plots of a category 1, or "super-accurate" system employing three different standard deviations of muzzle velocity. It is a very low rate of fire system, firing only one round per burst. Curves 2A and 2D show that a very high, sharp effectiveness peak can be achieved with a system using ammunition with a small standard deviation of muzzle velocity. However, the dispersion of such a system must be very precise and closely controlled. A small change in either direction drastically reduces effectiveness. The larger standard deviation of muzzle velocity used in curve 2B simply reduces effectiveness of this "super-accurate" system and moves the peak towards zero dispersion. It should be noted that the sigma muzzle velocity of curve 2B is probably a reasonable value for GAU-8 ammunition while the other two may be a little optimistic. Muzzle velocity variation is a factor not entirely under the control of the designer of a gun system. It is affected by such environmental factors as storage conditions, altitude, ambient temperature and so forth. Firing range data on existing ammunition indicates a possibly greater than 3-to-1 variation in sigma muzzle velocity simply due to differences in ambient temperature between a cool autumn day and a hot summer day.

Degradation of effectiveness due to factors not under the control of the designer and user, can be made up to a great extent by an increase

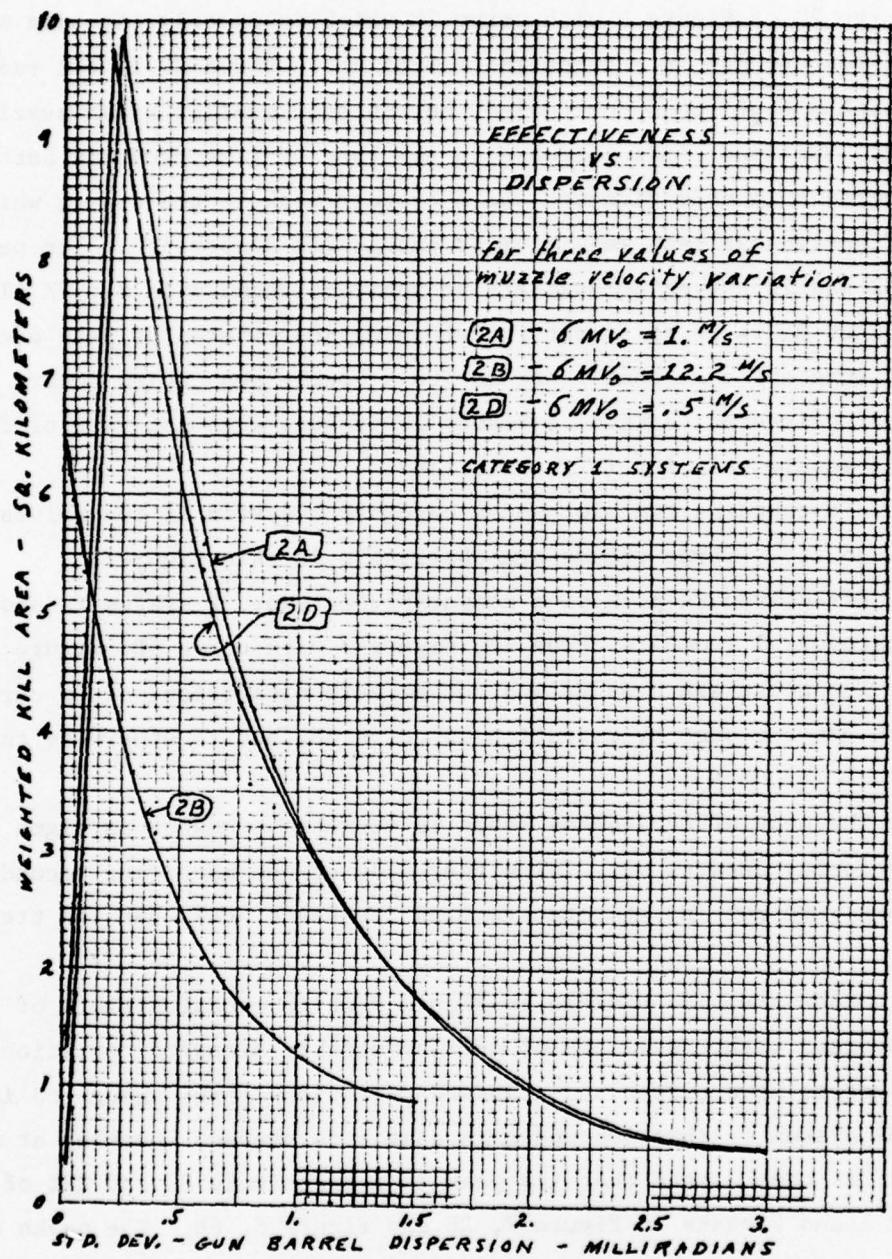


Figure 6 Effectiveness vs Dispersion at 3 values
of σ_{MV} . Category 1 Systems.

in the rate of fire. Figure 7 (note the change in vertical scale) compares curve 2D of Figure 6 with curve 2E which is exactly the same system, but with four rounds in a burst instead of one. Curve 2F is the same system with a four round burst also, but an even smaller sigma muzzle velocity. The four times increase in the rate of fire produces both a large increase in effectiveness and a broader peak in the curve, which makes effectiveness less sensitive to changes in dispersion. The peak of the 2E and 2F curves demonstrate an apparent anomaly in the PK algorithm that makes it difficult to determine just where the peak occurs. There is some evidence that there may be a double peak which occurs only at the effectiveness peaks of category 1 systems, with low rate of fire and small muzzle velocity (MV) variations.

Figure 8 contains two plots of a category 2 system at two values of muzzle velocity. Three trends are observable in this figure:

- (1) Effectiveness peak of a comparable category 2 system is about 27% of category 1 (compare curve 2E, Figure 7 with curve 6B, Figure 8).
- (2) The peaks are broader and not at zero dispersion, as in curve 2B, which has the same MV variation as curve 6B, but is otherwise category 1.
- (3) The peak effectiveness tends to decrease somewhat as sigma muzzle velocity departs very far either side of one meter per second; variations were not investigated to find the exact peak, but the trend is clear.

The trends are also visible in Figure 9 which contains plots of a category 3 systems with two values of muzzle velocity standard deviation. Category 3 systems have biases and standard deviations large enough to indicate that some system calibration and maintenance is needed. Looking at curve 9, Figure 9, it can be seen that its peak is respectively 6% and 22% of the category 1 and 2 peaks in Figure 7, 2E and Figure 8, 6B. The peaks also occur at successively larger standard deviations of gun barrel dispersion. The peak is at 0.25 milliradian for category 1 (Figure 6), about 0.45 milliradian for category 2 (Figure 8), and about 1.5 milliradians for category 3 (Figure 9). The peaks of the curves also get broader as the systems get less accurate. At the 50% of peak effectiveness level, the category 1

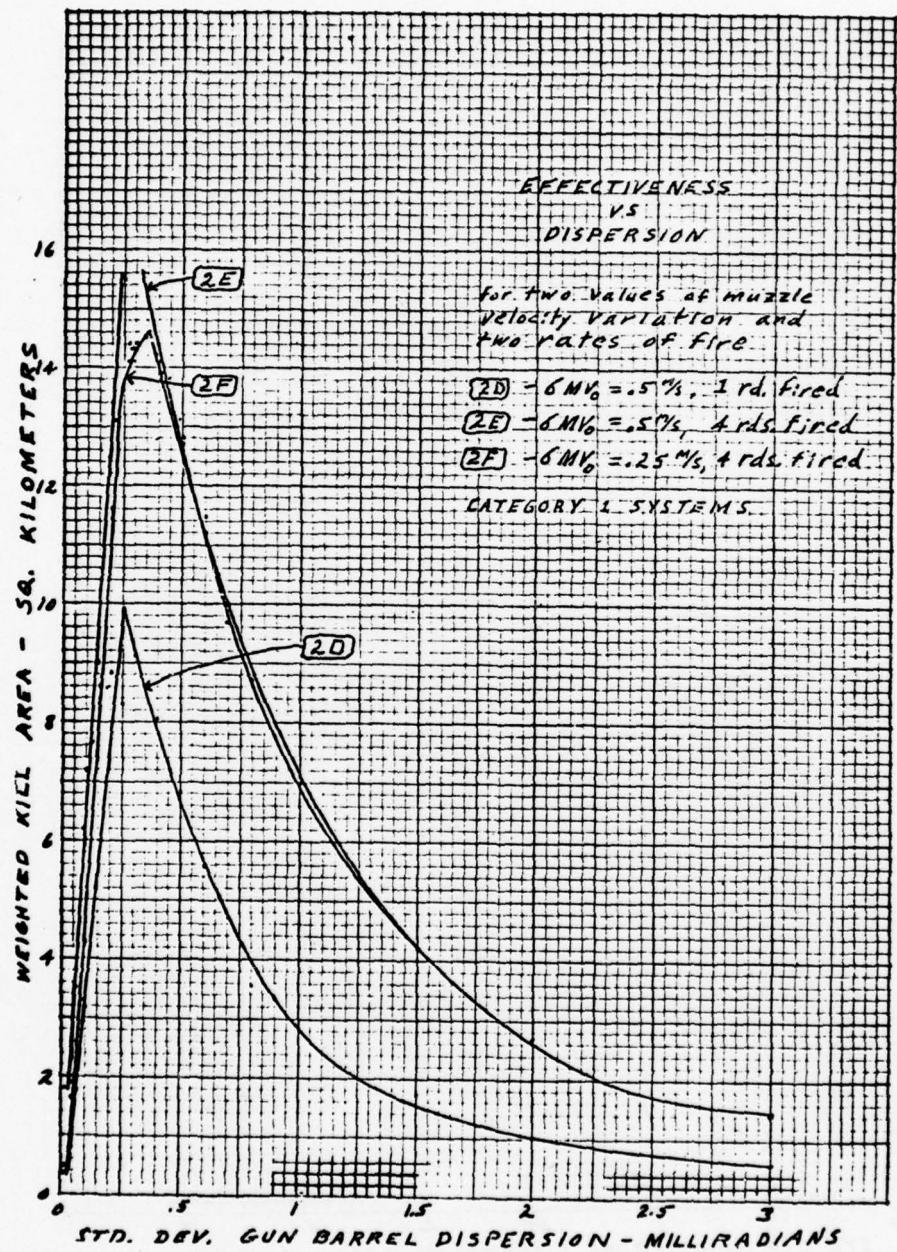


Figure 7 Effectiveness vs Dispersion at 2 rates
of fire. Category 1 Systems.

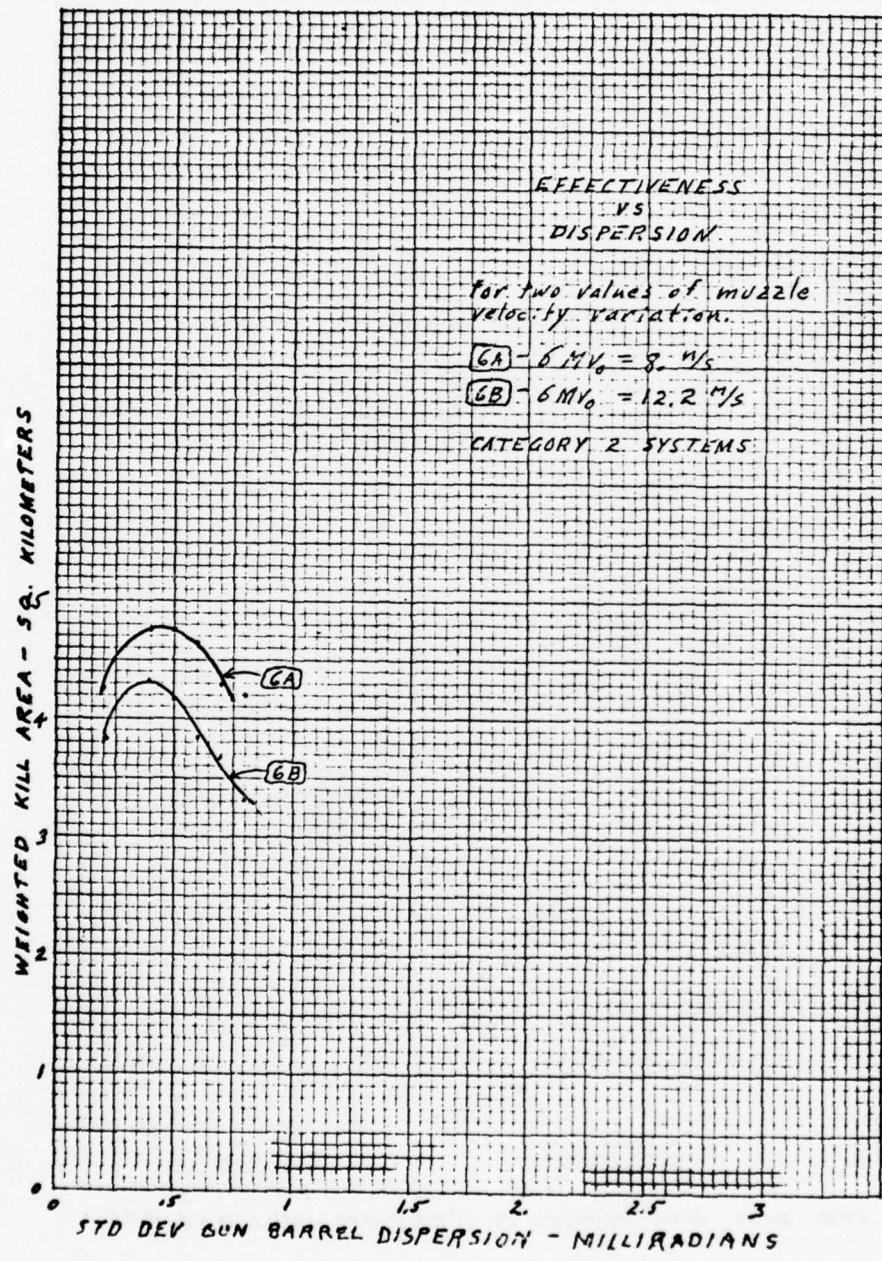


Figure 8 Effectiveness vs Dispersion at 2 values
of σMV . Category 2 systems.

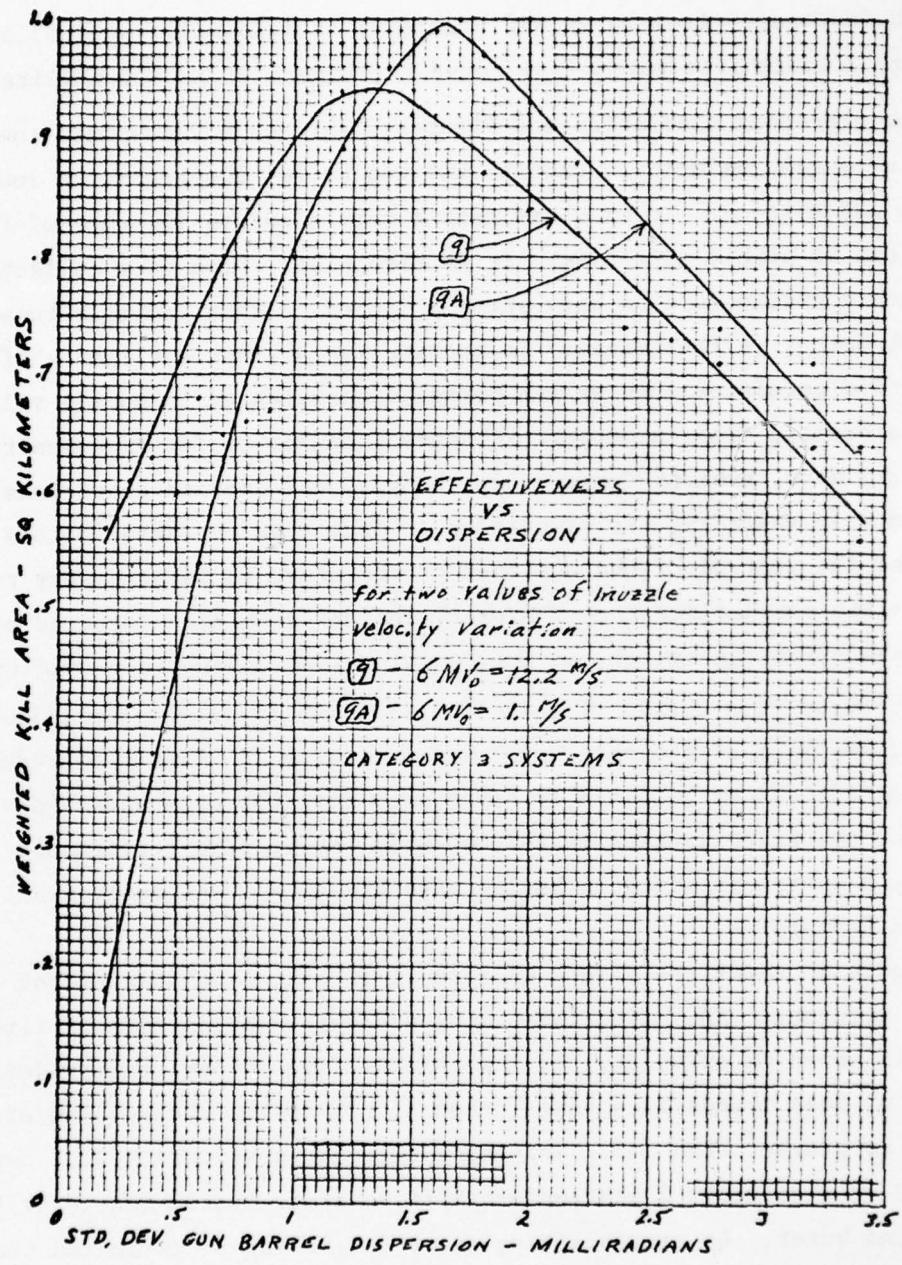


Figure 9 Effectiveness vs Dispersion at 2 values
of σ_{MV} . Category 3 Systems.

curve is approximatley 0.55 milliradian wide (Figure 6, curve 2D); category 2 width (estimated from curve 6B, Figure 8) is 1.25 milliradians; and category 3 width (estimated from curve 9A, Figure 9) is 3.5 milliradians.

The preceding discussion and Figures 6 through 9 illustrate the effect of muzzle velocity variation and gun barrel dispersion on low rate of fire gun systems. It is clear that a very accurate low-rate-of-fire system can be highly effective. It is also clear, from data collected, that such a system must be very sharply "tuned." When properly tuned, the peak output (effectiveness) is extremely high, but a slight shift in a sensitive parameter such as gun barrel dispersion or in muzzle velocity, causes a drastic drop in output. Changes from lot to lot in ammunition, gun barrel wear, ambient temperature changes, and storage consitions all affect muzzle velocity, and dispersion. Since some of these factors are not under the control of the designer or the user, it is necessary to consider the possibility that the precision and stability required of the low-rate-of-fire gun system can not be maintained under field conditions.

For example, a change of only -0.1 milliradian or +0.45 milliradian in the dispersion of the category 1 system (curve 2A, Figure 6) reduces its effectiveness by 50%, and if any biases develop, or standard deviations increase, the effectiveness is reduced still more. The performance of a category 1 system is based on having zero biases and extremely small standard deviations.

Figure 10 shows the effect of rate of fire as a substitute for extreme accuracy. The effectiveness of a category 1 low rate of fire system is shown in curve 2C. If low rate of fire is arbitrarily defined as four or less rounds in a burst, then such a system can have an effectiveness no greater than 9.5. This same effectiveness ($WKA = 9.5$) can be achieved by a category 2 state-of-the-art accurate system (curve 6) firing a 19 round burst. By extrapolating curve 5A, it can be estimated that a category 3 field system would need to fire a 160-round burst to have equal effectiveness.

Reducing to the lowest possible rate of fire, a one-round burst, the category 1 system represented by curve 2C shows an effectiveness, WKA equal to 4.5. The category 2 system represented by curve 6 requires a

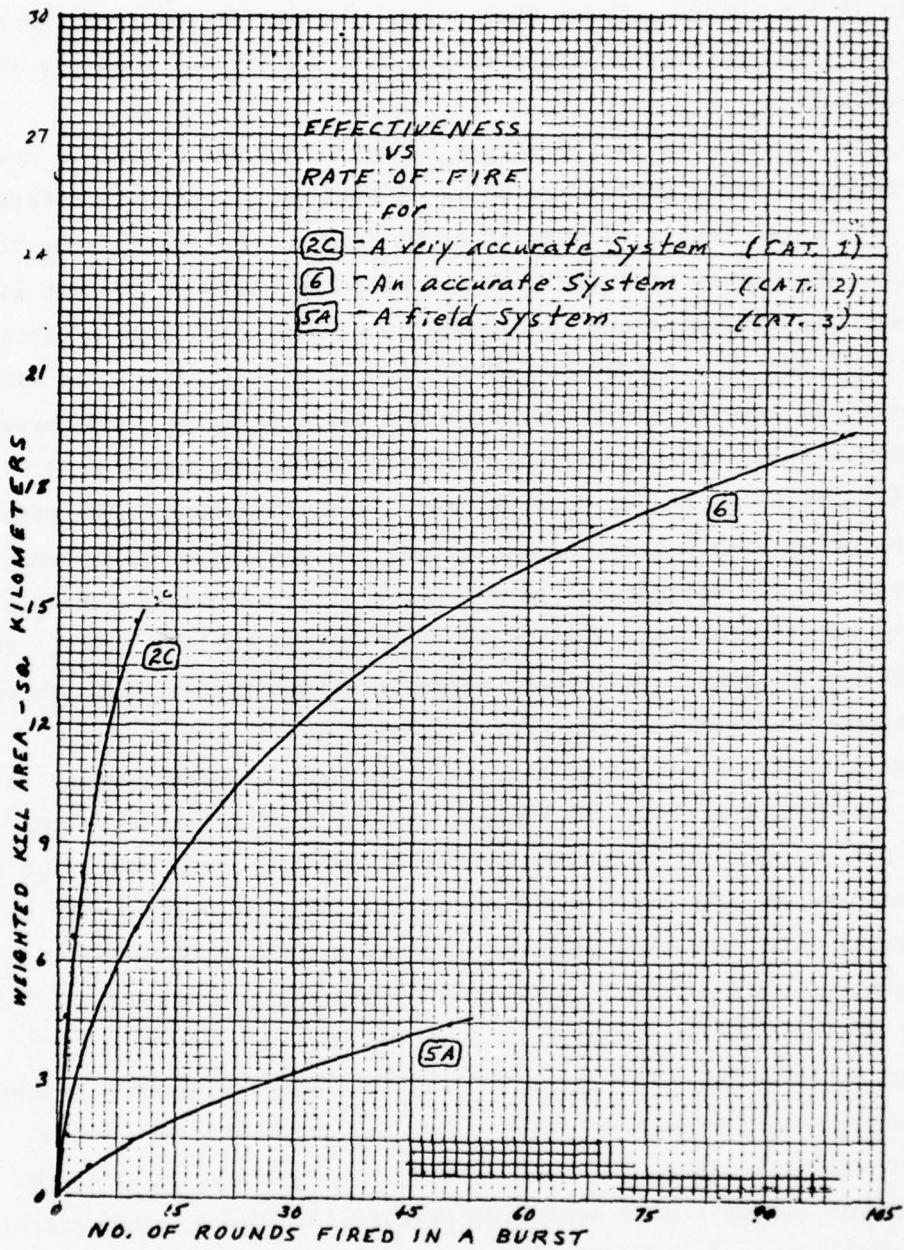


Figure 10 Effectiveness vs Rate of Fire.
Category 1, 2, and 3 Systems.

5 round burst for this effectiveness, and the category 3 (curve 5A) system requires a 50 round burst. A good assumption is that the burst duration is one second. Under that assumption all firing rates mentioned are well within the present state of the art, except for possibly the 160 round burst.

Figure 11 illustrates the strong effect of sensor biases on system effectiveness. Three curves are shown of what is basically a category 3 system with three levels of bias error on target location. Curve 9D represents the system with small biases near the state of the art limit. Gun barrel dispersion is the independent variable. The peak effectiveness is 1.74 WKA at a dispersion of about 0.75 milliradian. The system represented by curve 9 has biases that are twice as large, and curve 9C has biases 4 times as large. These peaks occur respectively at 0.87 WKA and 1.35 milliradian and at 0.25 WKA and 3.4 milliradians. The effect of gun pointing bias was not investigated. It was fixed at the very small value of 0.2 milliradian in all three of these curves. Basically, trends in this series were similar to those in the earlier plots. The more accurate systems have higher, narrower effectiveness peaks which occur at smaller values of gun barrel dispersion.

Figure 12 illustrates the monotonic decrease of effectiveness as the average standard deviations of dynamic gun pointing error increase. Dynamic gun pointing error varies with the tracking angle rate, and the points plotted in this curve are the averages of four such errors at four angular rates for each system. The curve shows a 50% reduction in the effectiveness of this category 2 system for an increase of less than one milliradian in dynamic gun pointing error.

Figures 13 through 17 are plots of effectiveness versus standard deviation of sensor-measured target range and angle errors. These plots are all of variants of a category 3 system, which explains the low values of effectiveness achieved. Figure 13 shows a broad effectiveness peak centered around 4 meters of range error standard deviation. It happens that the sensor range bias error for this series of system variants is also 4 meters, and this may account for the peak. However, further investigation of this aspect was beyond the scope of this study. It would require this series of model runs to be repeated a number of

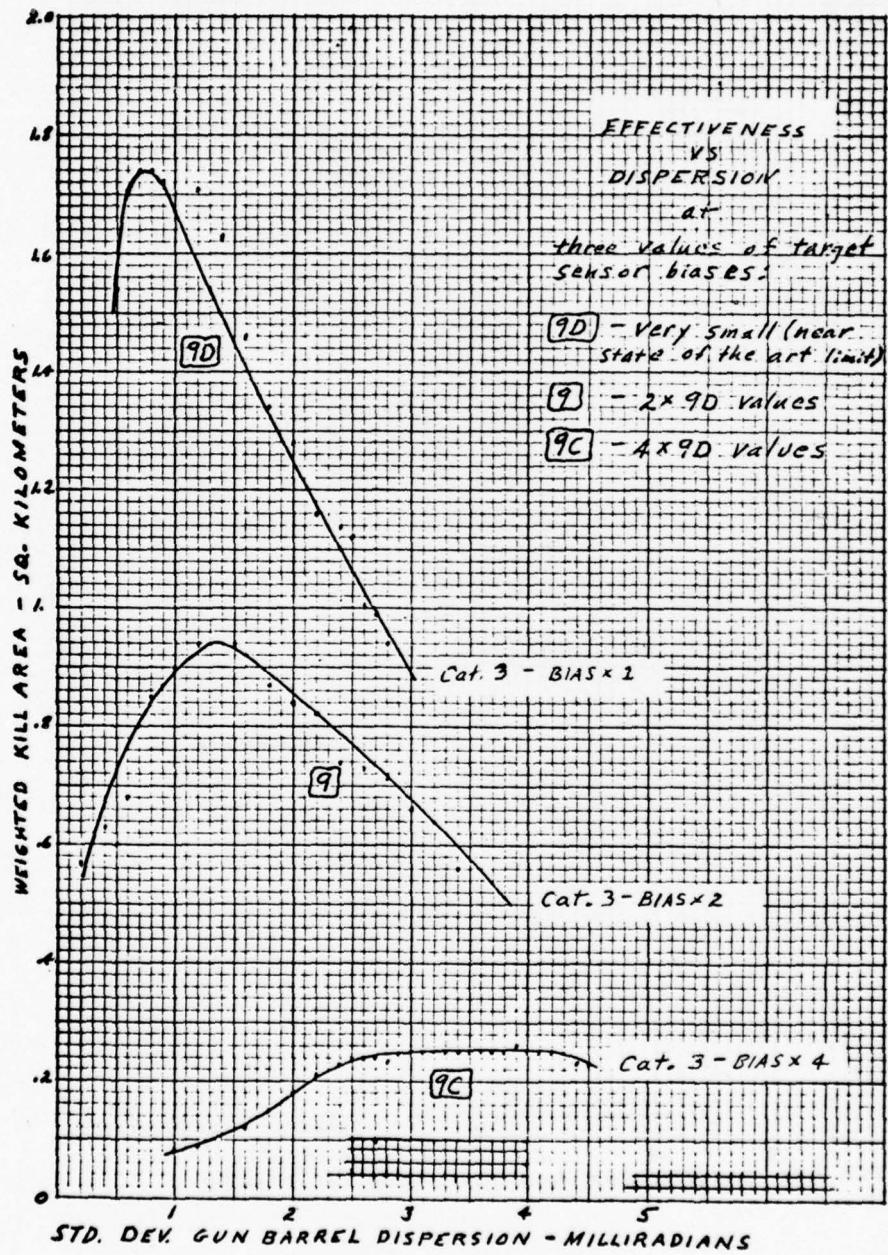


Figure 11 Effectiveness vs Dispersion at 3 values
of Sensor Bias. Category 3 Systems.

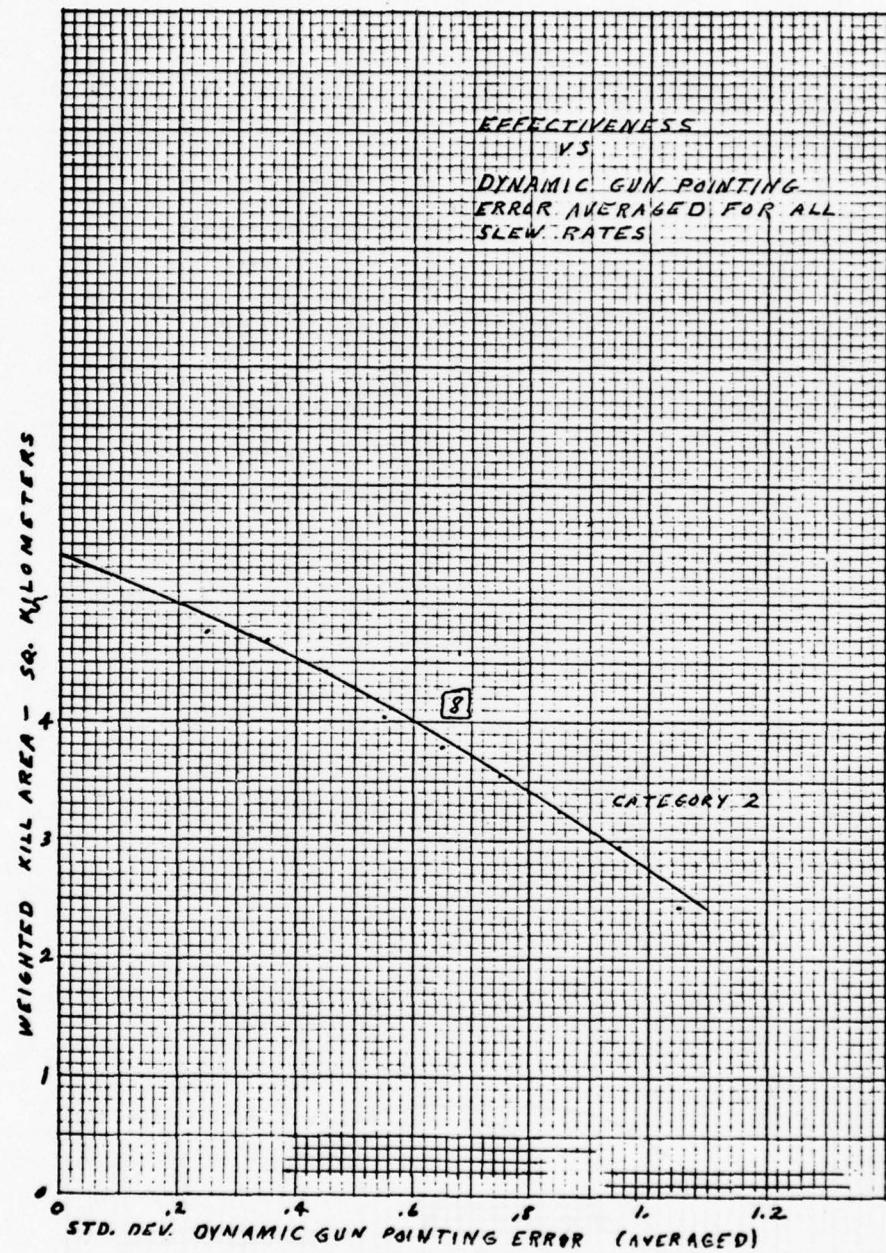


Figure 12 Effectiveness vs Dynamic Gun Pointing Error. Category 2 Systems.

times with different biases to determine the correlation between range bias and range standard deviation.

Figures 14, 15, and 16 which plot standard deviations of target angle, range rate, and angle rate against effectiveness, indicate that system effectiveness is not very sensitive to these parameter changes. Figure 15 indicates that system effectiveness is especially insensitive to standard deviations of range rate. This kind of result is not intuitively obvious, and the possibility that it may be due to a peculiarity in the burst kill algorithm employed to compute burst P_K needs to be investigated further. The method of computing Weighted Kill Area as the effectiveness measure, has been checked and does not seem to be contributing to the problem.

Figure 16 contains two plots of effectiveness against standard deviation of target angle rate, each plot representing a system with a different fixed value of standard deviation of target range rate measurement. Figure 15 showed that variation of σ_R had no appreciable influence on effectiveness. Figure 16 shows the influence of variation of σ_{AZ} and σ_{EL} at different values of σ_R . The results in Figure 16 show only a 10% change in effectiveness over the range of the plots, and the two plots are coincident until larger values of σ_{AZ} and σ_{EL} are reached. The divergence that does occur is small enough to be accounted for by round-off error, therefore it can be concluded that the effect of σ_R variation is negligible and the effect of σ_{AZ} and σ_{EL} variation is small over the range plotted, although a definite trend is established.

Figure 17 shows a plot of the square root of the sum of the squares (R.S.S.) of all six standard deviations of measured target range and angle (σ_R , σ_{AZ} , σ_{EL} , σ_R , σ_{AZ} , σ_{EL}) normalized to 1000 meters range. The normalizing is done at this range because it simplified the calculations and, fortuitously, the projectile flight time to 1000 meters is almost exactly one second. Therefore all normalized values convert to meters of offset at the target. It will be noted that the curve peaks broadly in terms of effectiveness when the R.S.S. total is about 5 meters. Coincidentally the R.S.S. of all of the six sensor biases normalized at this range is 5.1 meters. It is suggested that there is a correlation here,

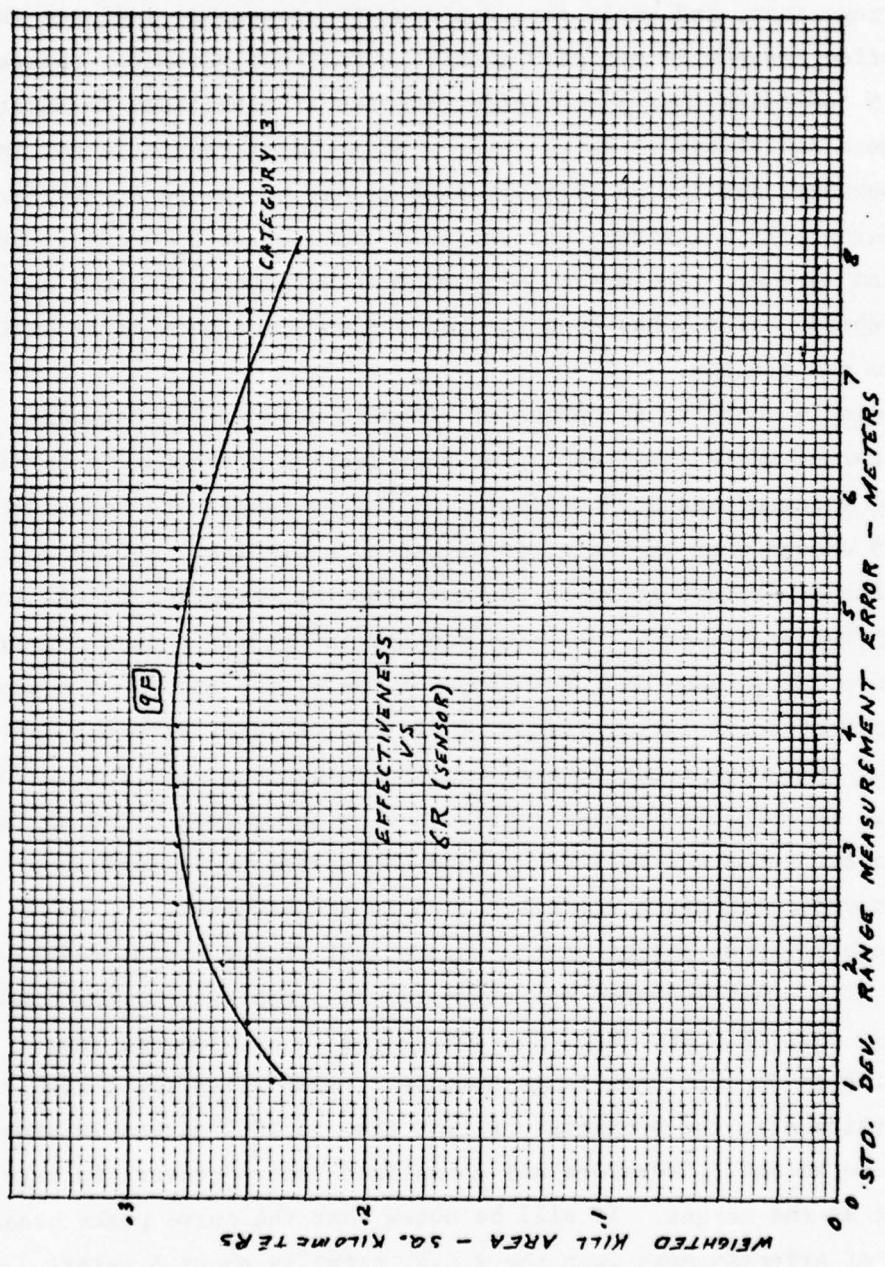


Figure 13 Effectiveness vs Sensor σR . Category 3 Systems.

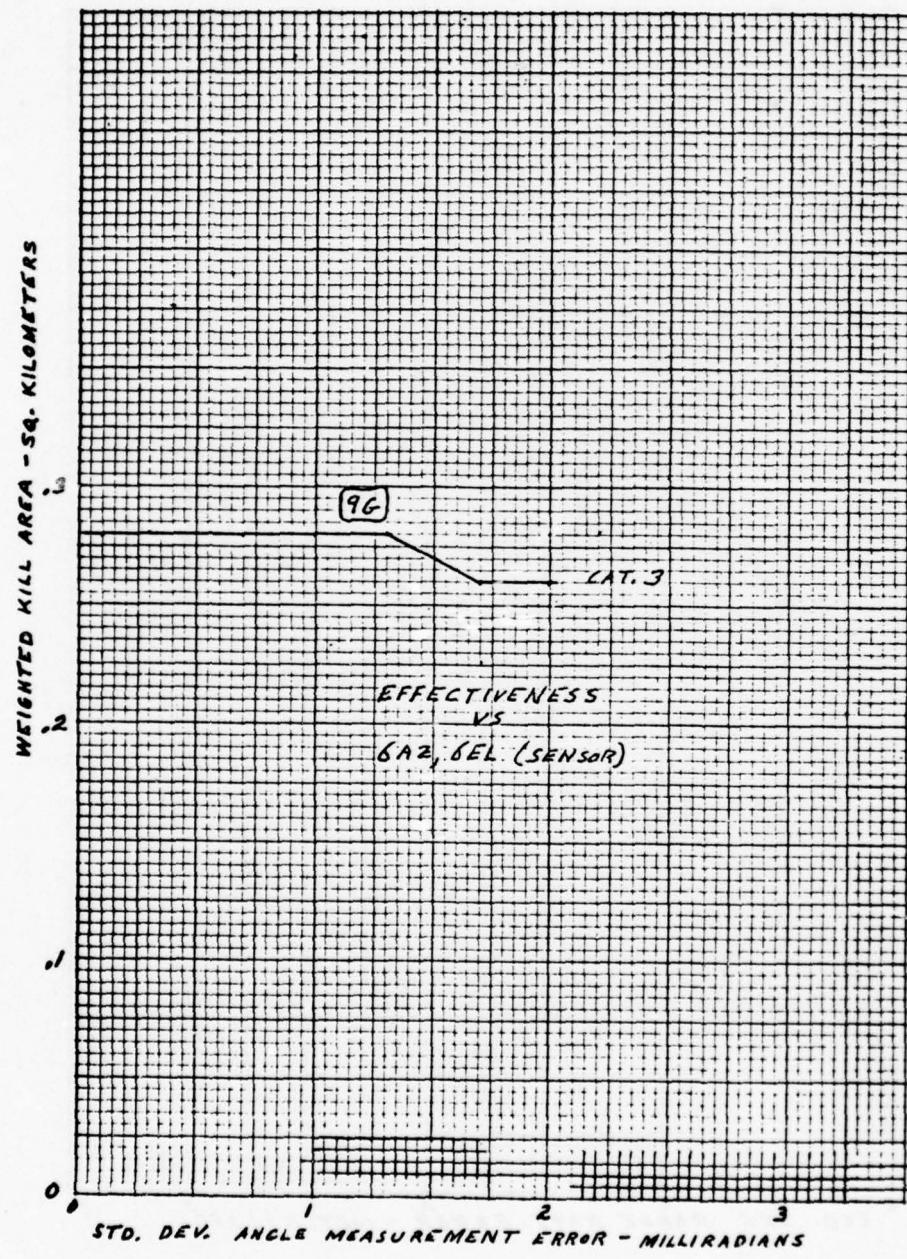


Figure 14 Effectiveness vs Sensor σ_{AZ} , σ_{EL} .
Category 3 Systems.

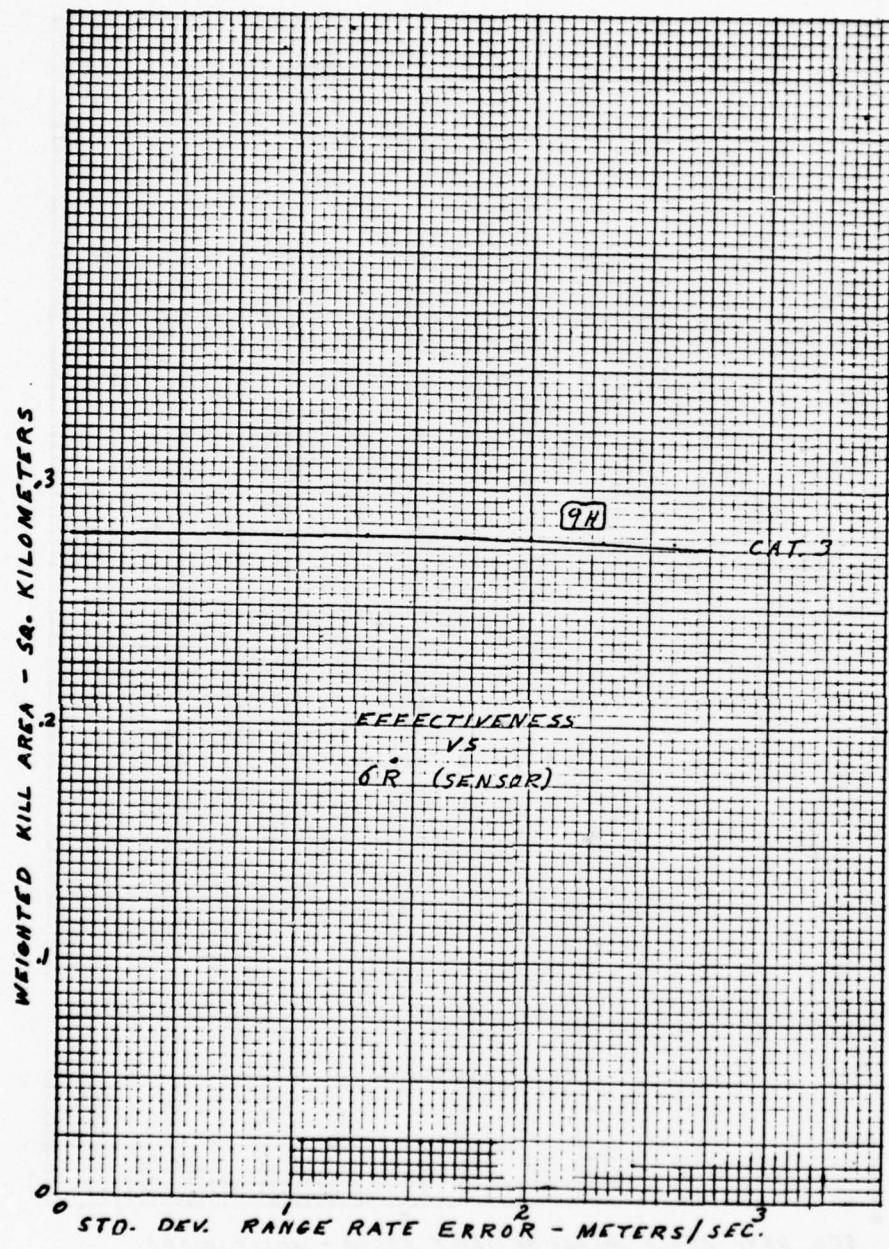


Figure 15 Effectiveness vs Sensor σ_R .
Category 3 Systems.

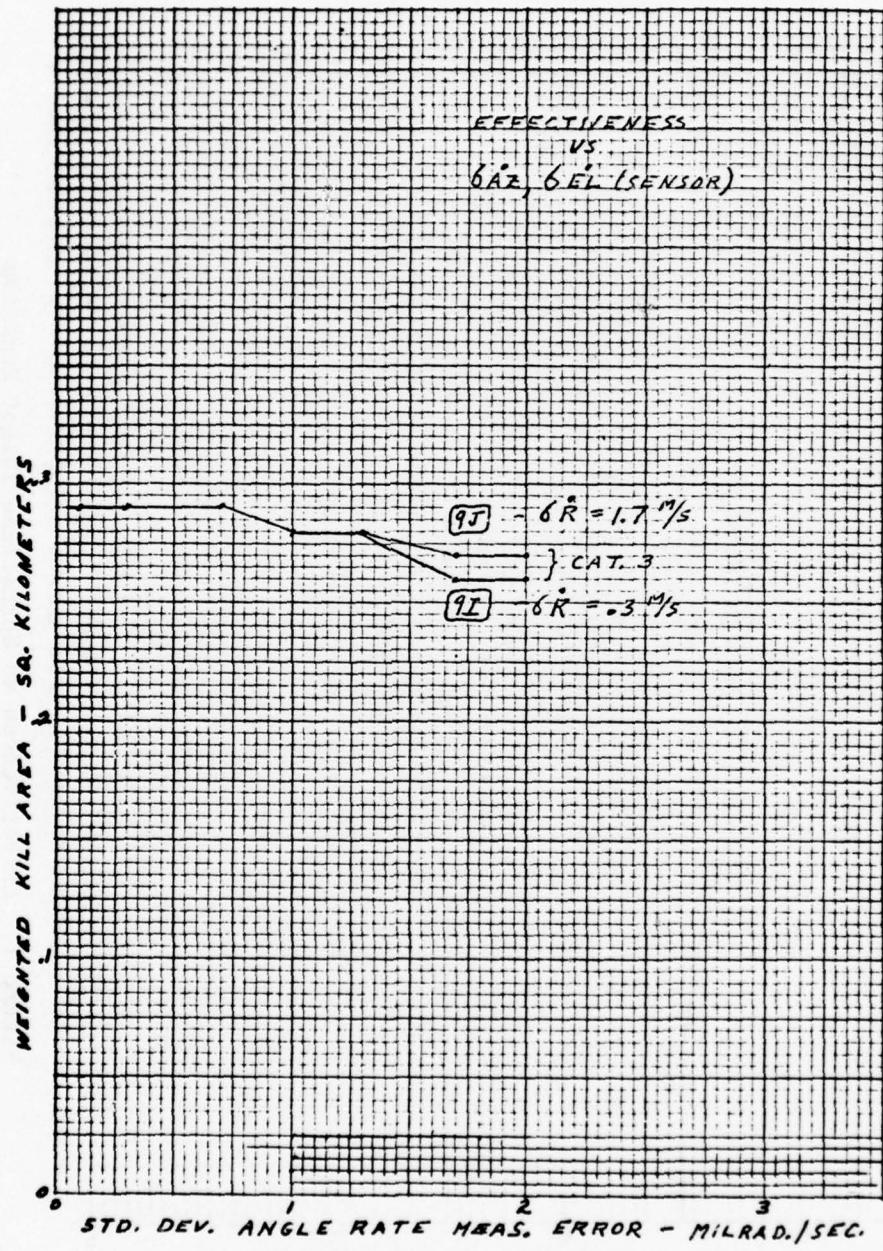


Figure 16 Effectiveness vs Sensor σ_{AZ} , σ_{EL} .
Category 3 Systems.

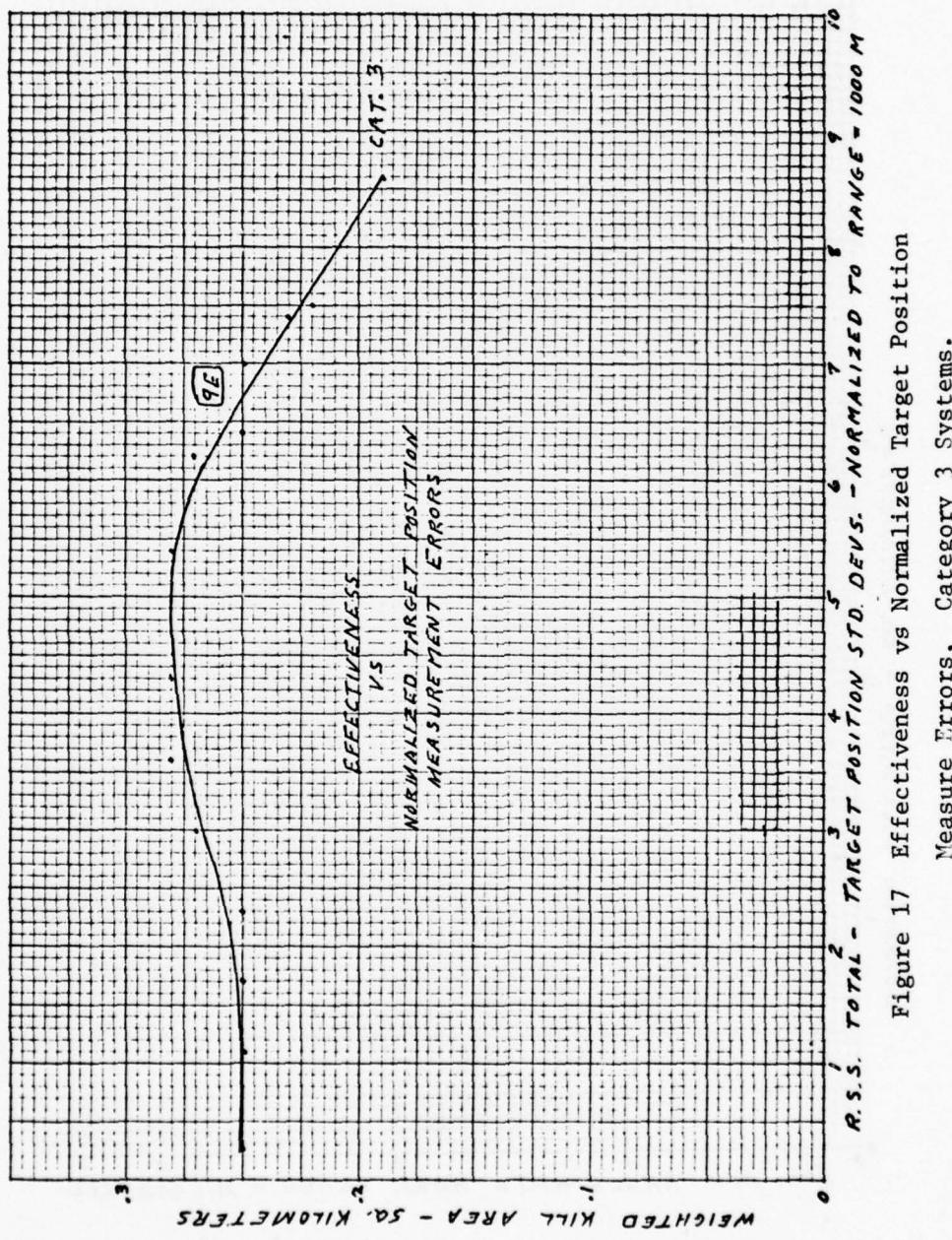


Figure 17 Effectiveness vs Normalized Target Position
 Measure Errors. Category 3 Systems.

that can be proved or disproved by making another series of computer runs in which controlled variations in bias are also made. The values of biases in this series were:

R = 4 meters, AZ = 2 milliradians, EL = 2 milliradians, R = 0.8 meter/sec., AZ = 0.8 milliradians/sec., EL = 0.8 milliradians/sec.

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A.0 APPENDIX A - WKA RANKING AND SYSTEM DATA FOR FIGURES 2, 3, 4, & 5

The four system illustrated in Figures 2 through 5 have the following WKA ratings in decending order:

Fig. 4, System 358 WKA = 14.505

Fig. 5, System 367 WKA = 11.473

Fig. 2, System 101 WKA = 6.801

Fig. 3, System 103 WKA = 4.880

The input data sheets for these systems are given on the following pages of this section.

GADESS ISO - PK CONTOUR PROGRAM --- MARCH 1973
 ACT STUDY - GP & NO. 101 - C.HICKS 11/18/74

CALIBER TYPE 2
 MUZZLE VELOCITY, M/S 1220.00
 STD. DEV. OF MUZZLE VELOCITY, M/S 12.2000
 STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD. 0.000600
 STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD. 0.000600
 MAXIMUM ELEVATION, RAD. 1.4400
 MAXIMUM ELEVATION RATE, RAD./SEC. 1.20
 MAXIMUM AZIMUTH RATE, RAD./SEC. 1.20
 AVERAGE SYSTEM REACTION TIME, SEC. 0.0
 ROUNDS PER PULSE 10.
 MAXIMUM EFFECTIVE RANGE, METERS 6000.
 RANGE, M. = 3500.0000 TIME OF FLIGHT, SECs. = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT FL. RATE, R/S STD DEV OF EL. ERROR, R
 1 0.0 0.0001
 2 0.120 0.0001
 3 0.600 0.0001
 4 1.200 0.0003

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R
 1 0.0 0.0001
 2 0.120 0.0001
 3 0.600 0.0001
 4 1.200 0.0003

MEAN MEASUREMENT ERRORS XM(I)

RANGE, M. 0.50000
 AZIMUTH, RAD. 0.00010
 ELEVATION, RAD. 0.00010
 RANGE RATE, M/S 0.20000
 AZ. RATE, RAD/S 0.00010
 EL. RATE, RAD/S 0.00010

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
0.50	0.0	0.0	0.0	0.0	0.0
AZIMUTH	0.0001	0.0	0.0	0.0	0.0
ELEVATION	0.0	0.0001	0.0	0.0	0.0
R. RATE	0.0	0.0	0.200	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0001

CHARACTER	H	K	L	M	N	O	
F	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
G	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
H	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
I	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
J	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
K	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
L	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
M	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
N	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500
O	0.0050	0.0100	0.0500	0.1000	0.2500	0.5000	0.7500

GADS ISO - PK CONTOUR PROGRAM --- MARCH 1973
 ACT STUNY - GP 6 NO. 103 -
 C.HICKS 11/18/74

CALIBER TYPE

MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-COMP. OF RES. GUN DISP., RAD.
 STD. DEV. OF Y-COMP. OF RES. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 ROUNDS PER BURST

RANGE, M. = 3500.0000 TIME OF FLIGHT, SECs. = 6000.
 DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION BIAS, RAD.= 0.0

POINT FL. RATE, R/S STD DEV OF EL. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

BALLISTIC COEFFICIENT, K-BAR = 0.2057

	CONTINUOUS	DISCRETE
1	0.00000	0.00000
2	0.00000	0.00000
3	0.00000	0.00000
4	0.00000	0.00000

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH BIAS, RAD.= 0.0

	CONTINUOUS	DISCRETE
1	0.00000	0.00000
2	0.00000	0.00000
3	0.00000	0.00000
4	0.00000	0.00000

SENSOR ERRORS
 MEAN MEASURENT ERRORS XM(1)

	CONTINUOUS	DISCRETE
1	0.00000	0.00000
2	0.00000	0.00000
3	0.00000	0.00000
4	0.00000	0.00000

MASK F
 FL. RATE ON DATA F
 AZ. RATE T
 INSUF. TIME T
 OUT OF BURST D

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELFV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.0	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0	0.0
R. RATE	0.0	0.0	0.0001	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0001

GAUSSIAN CONTROL PROGRAM --- MARCH 1973

ACT STUDY - GROUP 2F NO. 3511

C.MYCKS 04/18/75

CALIBRE TYPE
 MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-CUM-P. OF RES. GUN DISP., RAD.
 STD. DEV. OF Y-CUM-P. OF RES. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 ROADS PER FURST
 MAXIMUM EFFECTIVE RANGE, METERS
 RANGE, $R = 3500 \cdot 0000$

TIME OF FLIGHT, SECS. = 7.0000
 RIAS, RAD. = 0.0
 POINT EL. RATE, R/S STD DEV OF EL. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

MEAN MEASUREMENT ERRORS XM(I)

RANGE, M	0.0
AZI. AUTH. RAD.	0.0
ELEVATION, RAD	0.0
RANGE RATE, 1/S	0.0
AZ. RATE, RAD/S	0.0
EL. RATE, RAD/S	0.0

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
0.00	0.0	0.0	0.0	0.0	0.0
AZI.UTH	0.0	0.0001	0.0	0.0	0.0
ELEVATN	0.0	0.0001	0.0	0.0	0.0
R. RATE	0.0	0.0001	0.0	0.0	0.0
AZ. RATE	0.0	0.0001	0.0	0.0001	0.0
EL. RATE	0.0	0.0001	0.0	0.0001	0.0001

G A U E S I S O - P R O C E S S O R D A T A D R A F T

ACT STUDY - GEORGE 2F 10. 367

M A N U C H 1 9 7 3

C. M T C K S 0 4 / 1 M / 7 5

CALIBER TYPE:

MUZZLE VELOCITY, ft/s
 STD. DEV. OF MUZZLE VELOCITY, ft/s
 STD. DEV. OF X-UP, OF AZ. UP, OF DISP., GUN DISP., RAD.
 STD. DEV. OF Y-COMP., OF AZ. S., GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 MAXIMUM EFFECTIVE RANGE, METERS
 ROUNDS PER PULSE, = 3500. 0000

TIME OF FLIGHT, SECS. = 7.0000
 HIAS, RAD. = 0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT FL. RATE, P/S STD. DEV. OF EL. ERROR, R

1	0.0	0.0
2	0.120	0.0
3	0.600	0.0
4	1.200	0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, P/S STD. DEV. OF AZ. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

SENSOR ERRORS
 MEAN MEASUREMENT ERRORS, MM

H A N D E L E M
 AZI-MUTH, RAD.
 E L F I V A T I O N , R A D .
 H A N D E L E R A T E , 1 / S
 AZ. RATE, RAD/S
 EL. RATE, RAD/S

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

P A R A M E T E R	A Z I M U T H	E L E V .	R A T E	A Z . R A T E	E L . R A T E
R A N G E	0.00	0.0	0.0	0.0	0.0
A Z I M U T H	0.0	0.0001	0.0	0.0	0.0
E L E V A T I O N ,	0.0	0.0	0.0001	0.0	0.0
R . RATE	0.0	0.0	0.000	0.0	0.0
A Z . RATE	0.0	0.0	0.0001	0.0	0.0
E L . RATE	0.0	0.0	0.0	0.0001	0.0

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B.O APPENDIX B - CHARACTERISTICS OF THE TOP RANKED SYSTEMS IN EACH DATA BASE GROUP

Following is a list of the No. 1 ranked system for each of the groups plotted in Figures 6 through 17. ISO PK plots and input data for each of these systems are given on the following pages.

	<u>SYSTEM NO.</u>	<u>CATEGORY</u>	<u>WKA VALUE</u>	<u>PAGES</u>
<u>Fig. 6</u>				
GP2A	288	1	9.76	B-3,4
GP2B	286	1	6.17	B-5,6
GP2D	314	1	9.42	B-7,8
<u>Fig. 7</u>				
GP2D	314	1	9.42	B-7,8
GP2E	341	1	15.60	B-9,10
GP2F	359	1	14.57	B-11,12
<u>Fig. 8</u>				
GP6A	87	2	4.77	B-13,14
GP6B	89	2	4.32	B-15,16
<u>Fig. 9</u>				
GP9	146	3	.939	B-17,18
GP9A	186	3	.997	B-19,20
<u>Fig. 10</u>				
GP2C	57	1	14.68	B-21,22
GP5A	83	3	4.43	B-23,24
GP6	102	2	19.38	B-25,26
<u>Fig. 11</u>				
GP9	146	3	.939	B-17,18
GP9C	220	3	.260	B-27,28
GP9D	206	3	1.74	B-29,30
<u>Fig. 12</u>				
GP8	289	2	4.98	B-31,32
<u>Fig. 13</u>				
GP9F	243	3	.285	B-33,34

	<u>SYSTEM NO.</u>	<u>CATEGORY</u>	<u>WKA VALUE</u>	<u>PAGES</u>
<u>Fig. 14</u>				
GP9C	250	3	.285	B-35, 36
<u>Fig. 15</u>				
GP9H	252	3	.285	B-37, 38
<u>Fig. 16</u>				
GP9I	263	3	.291	B-39, 40
GP9J	272	3	.291	B-41, 42
<u>Fig. 17</u>				
GP9E	233	3	.280	B-43, 44

SADES ISO - PK CONTOUR PROGRAM --- MARCH 1973

ACT STUDY - GROUP 2A NO. 2AA

C.MTRS 03/12/75

CALIBER TYPE

MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.
 STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 ROUNDS PER PUPST

MAXIMUM EFFECTIVE RANGE, METERS

TIME OF FLIGHT, SECs.

RANGE, M. #3500.0000

2

1220.00
 1.0000
 0.00200
 0.00200
 1.400
 1.20
 1.20
 0.0

BALLISTIC COEFFICIENT, K-BAP = 0.2057

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION

POINT EL. RATE, R/S STD DEV OF EL. ERROR, R

1	0.0	0.0
2	0.120	0.0
3	0.600	0.0
4	1.200	0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH

POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

1	0.0	0.0
2	0.120	0.0
3	0.600	0.0
4	1.200	0.0

MEAN MEASUREMENT ERRORS XM(I)

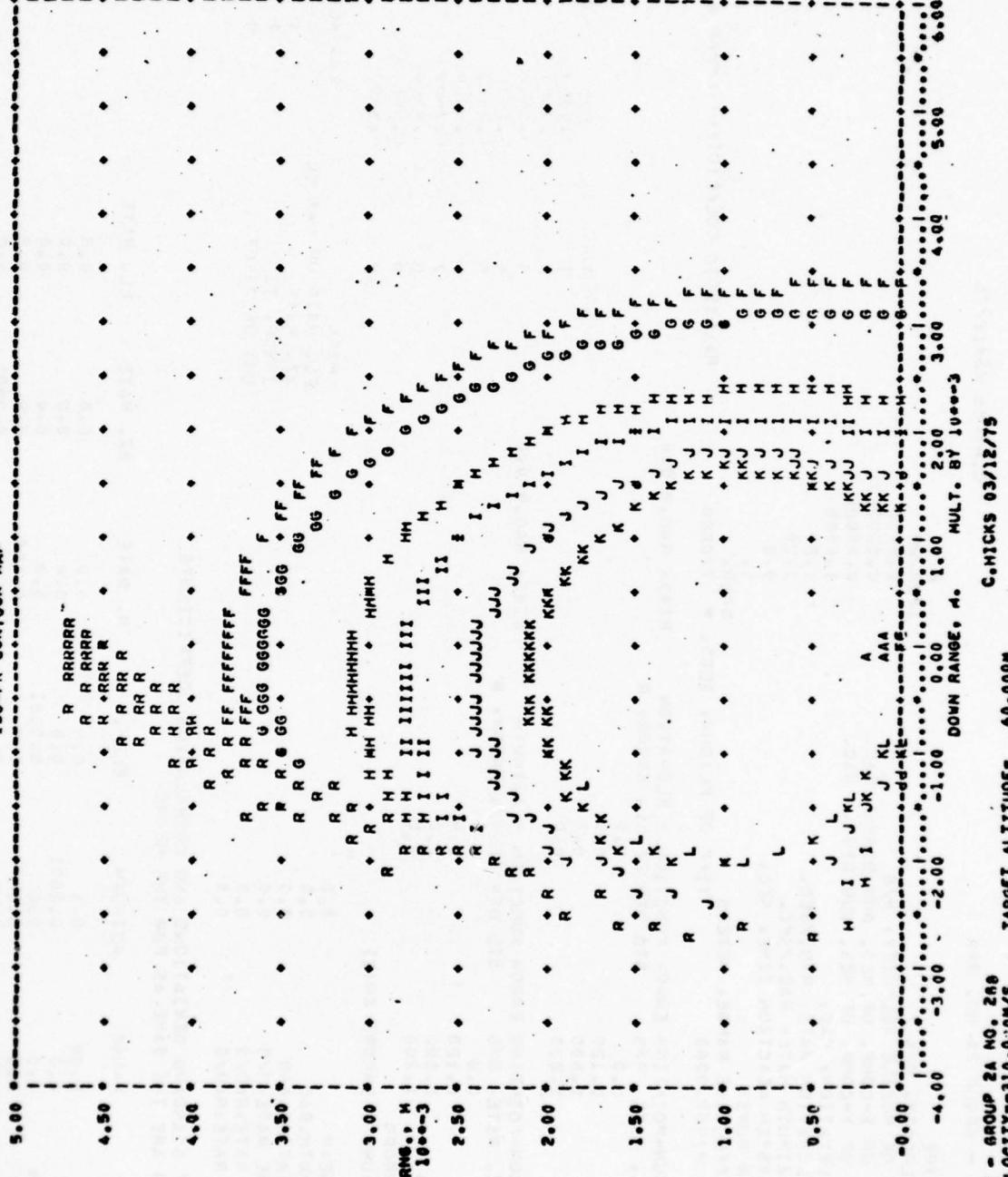
RANGE, M	0.0
AZIMUTH, RAD	0.0
ELEVATION, RAD	0.0
RANGE RATE, M/S	0.0
AZ. RATE, RAD/S	0.0
EL. RATE, RAD/S	0.0

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

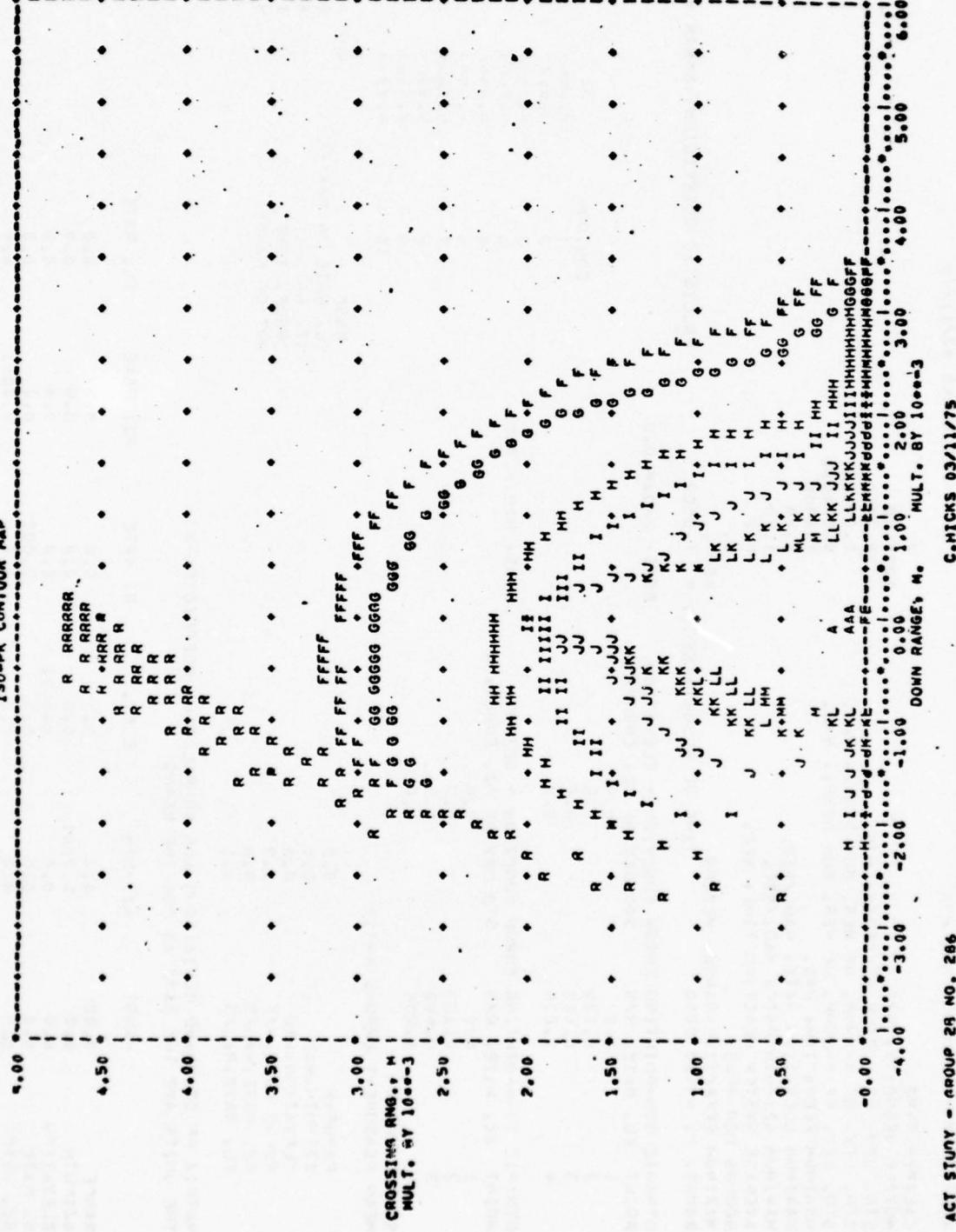
	RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.00	0.0	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0	0.0	0.0
R. RATE	0.0	0.0	0.0001	0.0	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0	0.0001
EL. RATE	0.0	0.0	0.0	0.0	0.0001	0.0001

	MARK	CHARACTER
1	PX	F
2	PP	S
3	PP	H
4	PP	I
5	PP	J
6	PP	K
7	PP	L
8	PP	M
9	PP	N
10	PP	O

ISO-PK CONTOUR MAP



ISO-PK CONTOUR MAP



GAUSSIAN DISTRIBUTION OF MEASUREMENTS

ACT STUDY - GRAPHIC 20-0, 11a

CONTINUATION 04/10/75

CALCULATED TYPE

MUZZLE VELOCITY, ft/s
 STD. DEV. OF MUZZLE VELOCITY, ft/s
 STD. DEV. OF X-COMP. OF ITS, GRAD. RATE, RAD.
 STD. DEV. OF Y-COMP. OF ITS, GRAD. RATE, RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 ROUNDS PER MINUTE
 MAXIMUM EFFECTIVE RANGE, FEET
 RANGE, " = 3500.0000

TIME OF FLIGHT, SECs. = 7.0000

BIAS, RAD. = 0.0

POINT FL. RATE, ft/s STD. DEV. OF FL. RATE, RAD.

POINT	FL. RATE, ft/s	STD. DEV. OF FL. RATE, RAD.
1	0.6	0.0
2	0.120	0.0
3	0.600	0.0
4	1.200	0.0

DYNAMIC GUN-POINTING ERROR FUNCTION = ELEVATION

POINT AZ. RATE, ft/s STD. DEV. OF AZ. ERROR, RAD.

POINT	AZ. RATE, ft/s	STD. DEV. OF AZ. ERROR, RAD.
1	0.0	0.0
2	0.120	0.0
3	0.600	0.0
4	1.200	0.0

MEAN MEASUREMENT ERRORS $\lambda^{(1)}$ MEAN MEASUREMENT ERRORS $\lambda^{(2)}$

RANGE, RAD. RATE, RAD. RATE

AZIMUTH, RAD. RATE, RAD. RATE

ELEVATION, RAD. RATE, RAD. RATE

PITCH, RAD. RATE, RAD. RATE

AZ. RATE, RAD. RATE, RAD. RATE

EL. RATE, RAD. RATE, RAD. RATE

MEAN MEASUREMENT ERRORS $\lambda^{(3)}$ MEAN MEASUREMENT ERRORS $\lambda^{(4)}$

RANGE, RAD. RATE, RAD. RATE

AZIMUTH, RAD. RATE, RAD. RATE

ELEVATION, RAD. RATE, RAD. RATE

PITCH, RAD. RATE, RAD. RATE

AZ. RATE, RAD. RATE, RAD. RATE

EL. RATE, RAD. RATE, RAD. RATE

MEAN MEASUREMENT ERRORS $\lambda^{(5)}$ MEAN MEASUREMENT ERRORS $\lambda^{(6)}$

RANGE, RAD. RATE, RAD. RATE

AZIMUTH, RAD. RATE, RAD. RATE

ELEVATION, RAD. RATE, RAD. RATE

PITCH, RAD. RATE, RAD. RATE

AZ. RATE, RAD. RATE, RAD. RATE

EL. RATE, RAD. RATE, RAD. RATE

MEAN MEASUREMENT ERRORS $\lambda^{(7)}$ MEAN MEASUREMENT ERRORS $\lambda^{(8)}$

RANGE, RAD. RATE, RAD. RATE

AZIMUTH, RAD. RATE, RAD. RATE

ELEVATION, RAD. RATE, RAD. RATE

PITCH, RAD. RATE, RAD. RATE

AZ. RATE, RAD. RATE, RAD. RATE

EL. RATE, RAD. RATE, RAD. RATE

MEAN MEASUREMENT ERRORS $\lambda^{(9)}$ MEAN MEASUREMENT ERRORS $\lambda^{(10)}$

RANGE, RAD. RATE, RAD. RATE

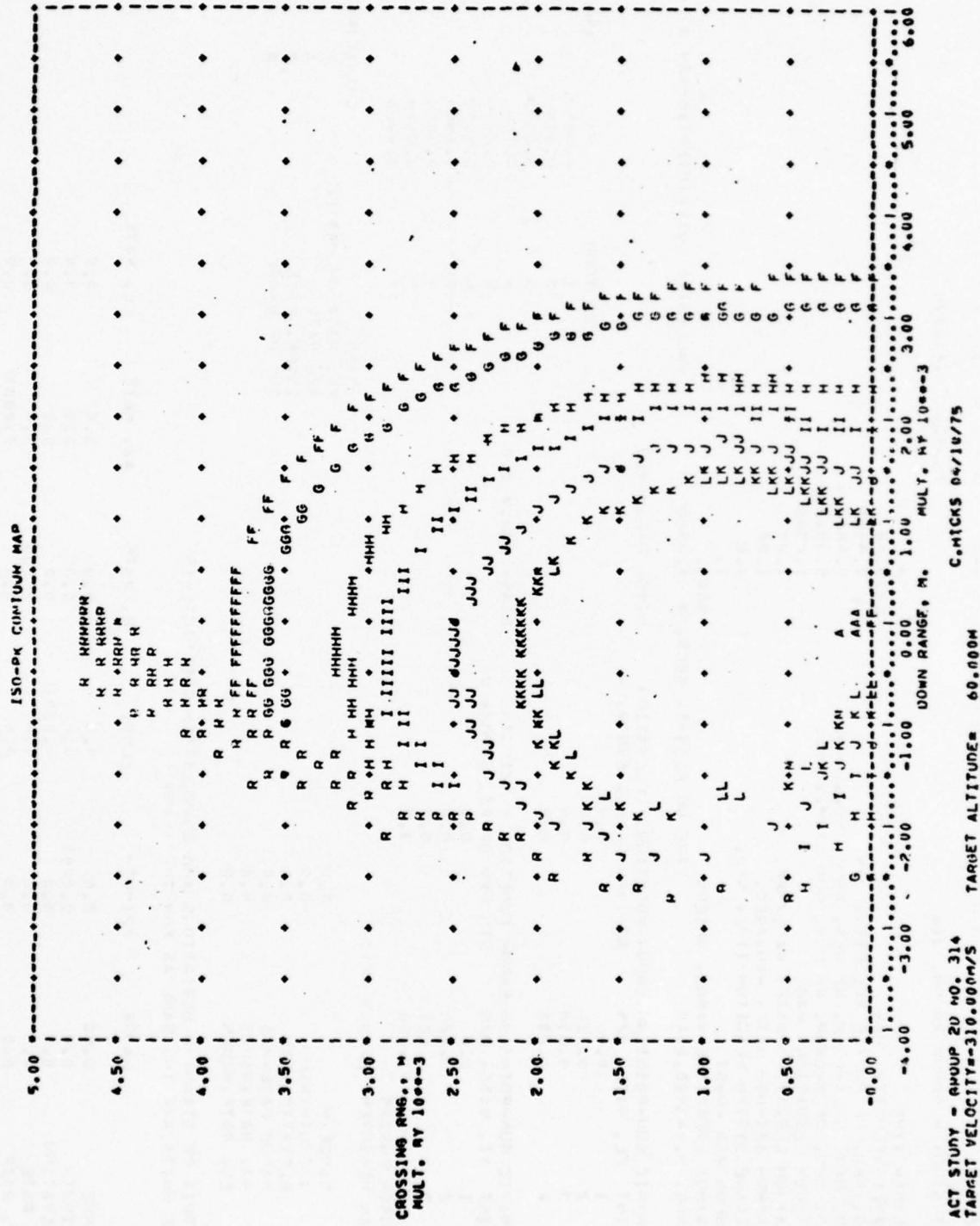
AZIMUTH, RAD. RATE, RAD. RATE

ELEVATION, RAD. RATE, RAD. RATE

PITCH, RAD. RATE, RAD. RATE

AZ. RATE, RAD. RATE, RAD. RATE

EL. RATE, RAD. RATE, RAD. RATE



GAUNTSTON CORNELL GUNNAR
ACT STUDY - SPURS 2000-141

CONTINUATION

CALCULATED TYPE

PURSE VELOCITY, ft/s
STD. DEV. OF PURSE VELOCITY, ft/s
STD. DEV. OF X-COMP. OF VES. STD. DEV. OF Y-COMP. OF VES. STD. DEV. OF Z-COMP. OF VES.
MAXIMUM ELEVATION, RAD.
MAXIMUM AZIMUTH RATE, RAD./SEC.
AVERAGE SYSTEM EJECTION TIME, SEC.
ROUND OFF PUSHTIME, SEC.

MAXIMUM EFFECTIVE RANGE, NM = 3500.0000
RANGE, NM = 3500.0000

DYNAMIC GUN-POLARITIES EJECT FUNCTION = ELEVATION,
POINT FL. RATE, ft/s

STD. DEV. OF EL. EJECTION, °

POINT	FL. RATE,	ELEV.	EL. EJECTION,	CONTR.	COEFF.
1	0.0	0.0	0.0	1	1.000
2	0.120	0.0	0.0	2	0.100
3	0.000	0.0	0.0	3	0.000
4	1.200	0.0	0.0	4	1.000

DYNAMIC GUN-POLARITIES EJECT FUNCTION = AZIMUTH,
POINT AZ. RATE, RAD. STD. DEV. OF AZ. EJECTION, R
1 0.0 0.0
2 0.120 0.0
3 0.500 0.0
4 1.200 0.0

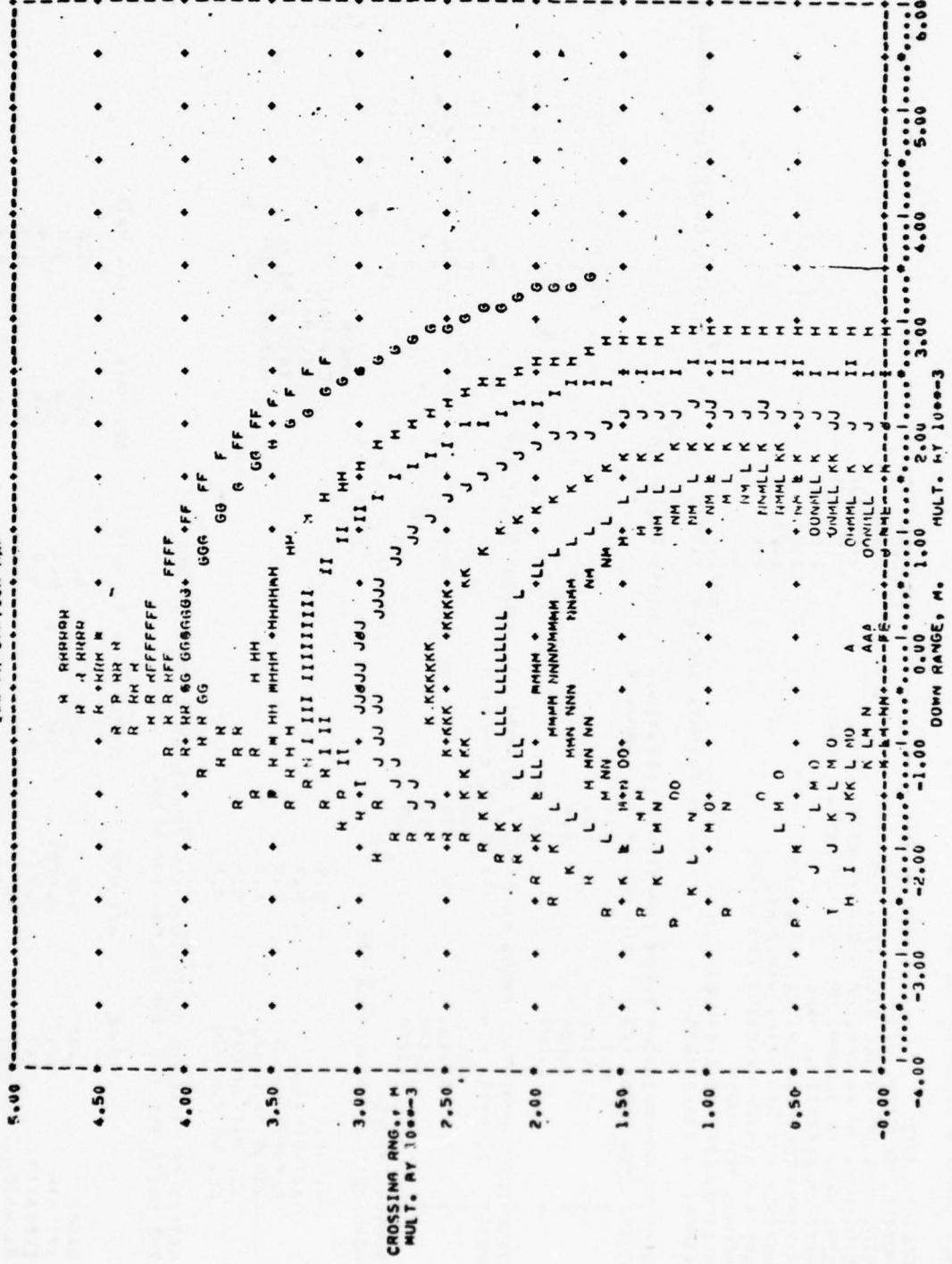
MEAN MEASUREMENT ERRORS X(1)

RAD. SEFT.
AZIMUTH RATE,
ELEVATION, RAD.
EL. RATE, RAD.
AZ. RATE, RAD.
EL. RATE, RAD.

MATRIX OF STANDARD DEVIATIONS AND CORRELATING COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

EL. RATE	AZ. RATE	ELEV.	EL. RATE	AZ. RATE	ELEV.
0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000
0.000	0.000	0.000	0.000	0.000	0.000

150-PK COUNT MAP



ACT STUDY - 6900222E NO. 341
TA90ET VELOCITY=-310.000/S

CHICKS 04/11/79

卷之三

A D E S T S O - P R C C O N T O U R P R O G R A M --- M A R C H 1 9 7 3
 CT STURY - CHUH 2F (4) . 359

C.HICKS 04/18/75

ALIEN TYPE

 UZZLE VELOCITY, M/S
 TD. DEV. OF MUZZLE VELOCITY, '4/S
 TD. DEV. OF X-COMP. OF RGS. GUN DISP., RAD.
 TD. DEV. OF Y-COMP. OF RGS. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.

VEEAGE SYSTEM REACTION TIME, SEC.

ORDS PER HINST

MAXIMUM EFFECTIVE RANGE, METERS

ANGLE, M. =3500.0000

TIME OF FLIGHT, SECs. = 6000.

RIAS, RAD.= 0.0

QINT EL. RATE, '4/S STD DEV OF EL. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION

QINT AZ. RATE, '4/S STD DEV OF AZ. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

BIAS, RAD.= 0.0

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH

QINT AZ. RATE, '4/S STD DEV OF AZ. ERROR, R
 1 0.0 0.0
 2 0.120 0.0
 3 0.600 0.0
 4 1.200 0.0

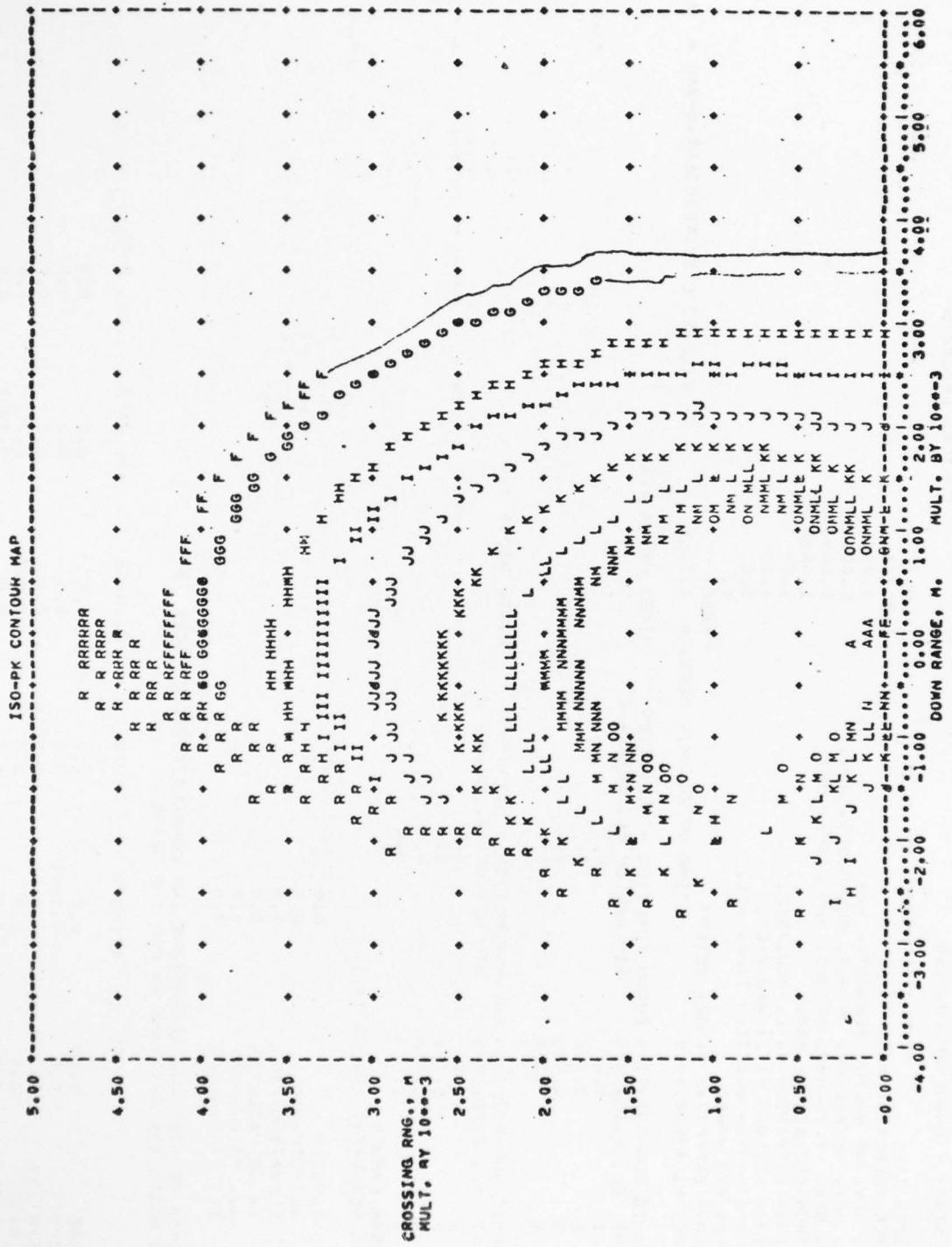
BIAS, RAD.= 0.0

ENSUR ERRORS
 EACH MEASUREMENT ERRORS X(1)

RANGE,M	AZIMUTH	ELEV.
0.0	0.0	0.0
AZMUTH,RAD	0.0	
ELEVATION,RAD	0.0	
RAISE RATE,'4/S	0.0	
AZ. RATE,RADS	0.0	
EL. RATE,RADS	0.0	

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0001	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0001
0.0	0.0	0.0	0.0	0.0	0.0



GADESS ISO - PK CONTOUR PROGRAM ---- MARCH 1973
 ACT STUNY - GP 6 NO. 87 - C.HICKS 11/14/74

CALIBER TYPE
 MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-COMP. OF RES. GUN DISP., RAD.
 STD. DEV. OF Y-COMP. OF RES. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 MAXIMUM EFFECTIVE RANGE, METERS
 RANGE, M. = 3500.0000

TIME OF FLIGHT, SECS. # 6000.
 # 7.00000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT FL. RATE, R/S STD DEV OF EL. ERROR, R

1	0.0	0.0002
2	0.120	0.0002
3	0.600	0.0002
4	1.200	0.0005

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

1	0.0	0.0002
2	0.120	0.0002
3	0.600	0.0002
4	1.200	0.0005

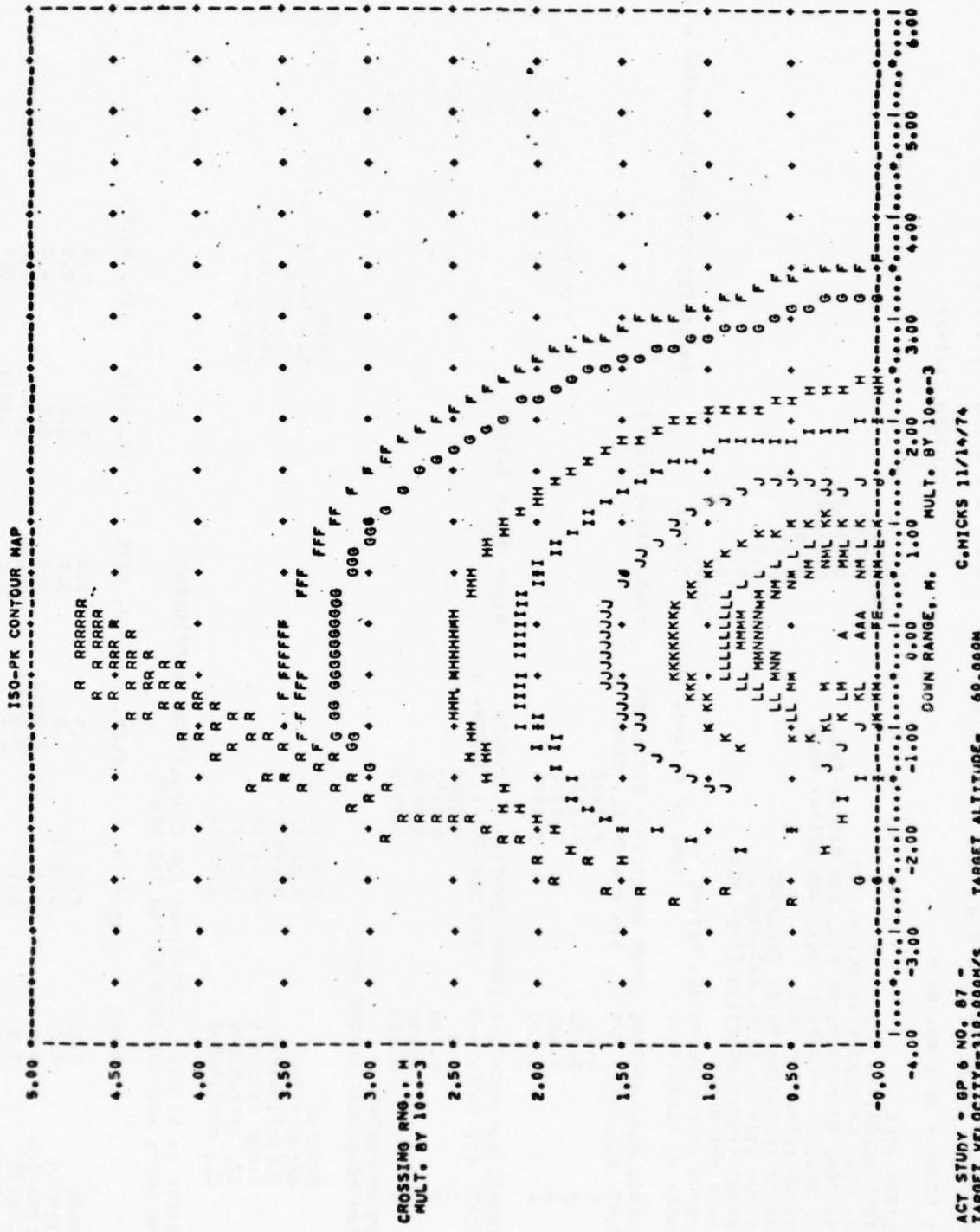
SENSOR FATORS
 MEAN MEASURENT ERRORS XM(I)

RANGE, M
 AZIMUTH, RAD
 ELEVATION, RAD
 RANGE RATE, M/S
 AZ. RATE, RAD/S
 EL. RATE, RAD/S

MASK
 EL. RATE, 0.0
 AZ. RATE, 0.0
 INSUF. T 1/2
 OUT OF RADI, 0

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
0.50	0.0	0.0	0.0	0.0	0.0
0.0	0.0001	0.0	0.0001	0.0	0.0
0.0	0.0	0.0	0.0001	0.0	0.0
0.0	0.0	0.0	0.0	0.200	0.0
0.0	0.0	0.0	0.0	0.0	0.0001
0.0	0.0	0.0	0.0	0.0	0.0001



6 A D E S I S O - P K C O N T O U R P R O G R A M --- M A R C H 1 9 7 3
C.MTCKS 11/14/74

A C T S T U D Y - G P 6 N O . 8 9 -

CALIBER TYPE

2

MUZZLE VELOCITY, M/S
STD. DEV. OF MUZZLE VELOCITY, M/S
STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.
STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.
MAXIMUM ELEVATION, RAD.
MAXIMUM ELEVATION RATE, RAD./SEC.
MAXIMUM AZIMUTH RATE, RAD./SEC.

AVERAGE SYSTEM REFRACTION TIME, SEC.

ROUNDS PER BURST

MAXIMUM EFFECTIVE RANGE, METERS

RANGE, M. = 3500.0000 TIME OF FLIGHT, SECs. = 6000.

BALLISTIC COEFFICIENT, K-BAR = 0.2057

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
POINT FL. RATE, R/S STD DEV OF EL. ERROR, R

1 0.0 0.0002
2 0.120 0.0002
3 0.600 0.0002
4 1.200 0.0005

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

1 0.0 0.0002
2 0.120 0.0002
3 0.600 0.0002
4 1.200 0.0005

SENSOR ERRORS

MEAN MEASUREMENT ERRORS XM(I)

RANGE, M	0.50000
AZIMUTH, RAD	0.00010
ELFVATION, RAD	0.00010
RANGE RATE, M/S	0.20000
AZ. RATE, RAD/S	0.00010
EL. RATE, RAD/S	0.00010

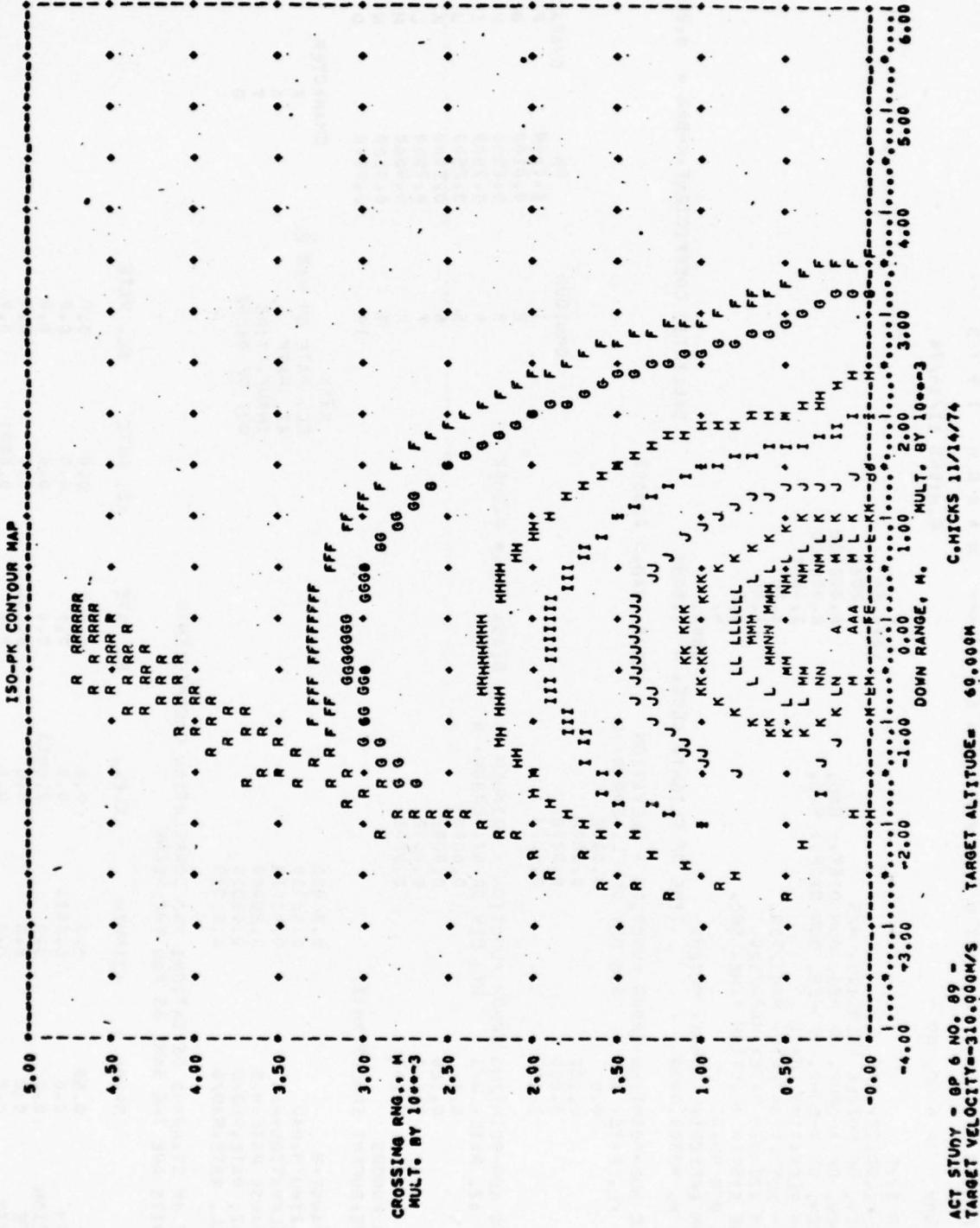
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.50	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0	0.0
R. RATE	0.0	0.0	0.0	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0001	0.0

CHARACTER	F
CHARACTER	G
CHARACTER	H
CHARACTER	I
CHARACTER	J
CHARACTER	K
CHARACTER	L
CHARACTER	M
CHARACTER	N
CHARACTER	O

MASK	EL. RATE OR MAX EL
MASK	AZ. RATE
MASK	INSUF. TIME
MASK	OUT OF RANGE

CHARACTER	F
CHARACTER	A
CHARACTER	T
CHARACTER	R



GADE'S ISU-PK CONTOUR PROGRAM --- MARCH 1973

ACT STUNY - GROUP 9 NO. 140

C.MICAS 01/10/75

CALIBER TYPE

MUZZLE VELOCITY, M/S

STD. DEV. OF MUZZLE VELOCITY, M/S

STD. DEV. OF X-COMP. OF RES. GUN DISP. RAD.

STD. DEV. OF Y-COMP. OF RES. GUN DISP. RAD.

MAXIMUM ELEVATION, RAD.

MAXIMUM ELEVATION RATE, RAD./SEC.

MAXIMUM AZIMUTH RATE, RAD./SEC.

AVERAGE SYSTEM REACTION TIME, SEC.

ROLLS OPEN HUMST

MAXIMUM EFFECTIVE RANGE, METERS

RANGE, M. = 3500,000

TIME OF FLIGHT, SECS. = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION POINT EL. RATE, R/S STD. DEV. OF EL. ERROR, R

1 0.0 0.0010

2 0.120 0.0010

3 0.600 0.0010

4 1.200 0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, R

1 0.0 0.0010

2 0.120 0.0010

3 0.600 0.0010

4 1.200 0.0020

SENSOR ERRORS

MEAN MEASUREMENT ERRORS XM(I)

RANGE, M 2.00000

AZIMUTH, RAD. 0.0010

EL. ELEVATION, RAD. 0.0010

HATUE RATE, R/S 0.40000

AZ. RATE, RAD/S 0.0040

EL. RATE, RAD/S 0.0040

RANGE 0.00 0.0 0.0

AZIMUTH 0.0 0.0001

ELEVATION 0.0 0.0 0.0

R. RATE 0.0 0.0 0.0

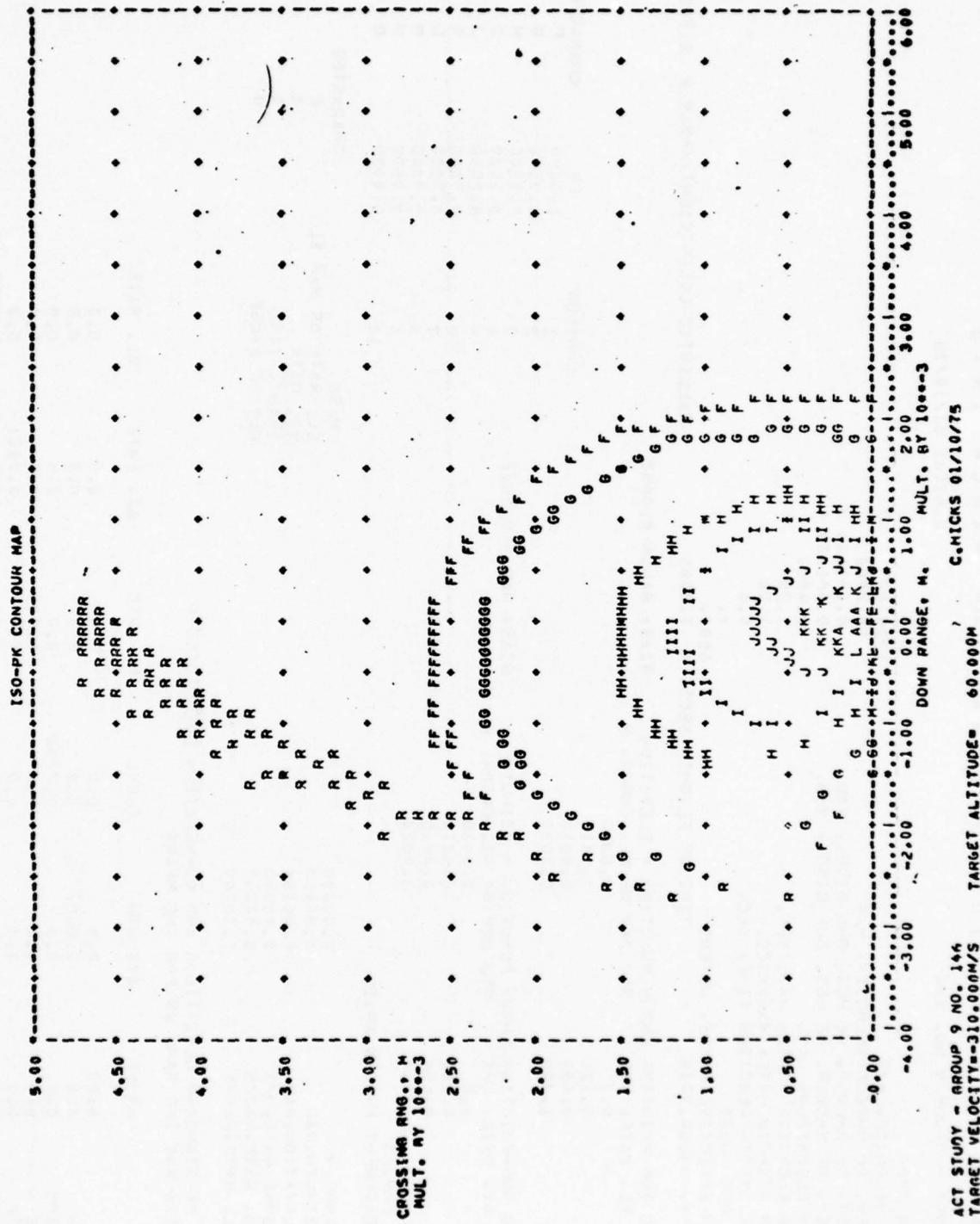
AZ. RATE 0.0 0.0 0.0

EL. RATE 0.0 0.0 0.0

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.00	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0	0.0
R. RATE	0.0	0.0	0.0001	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0001

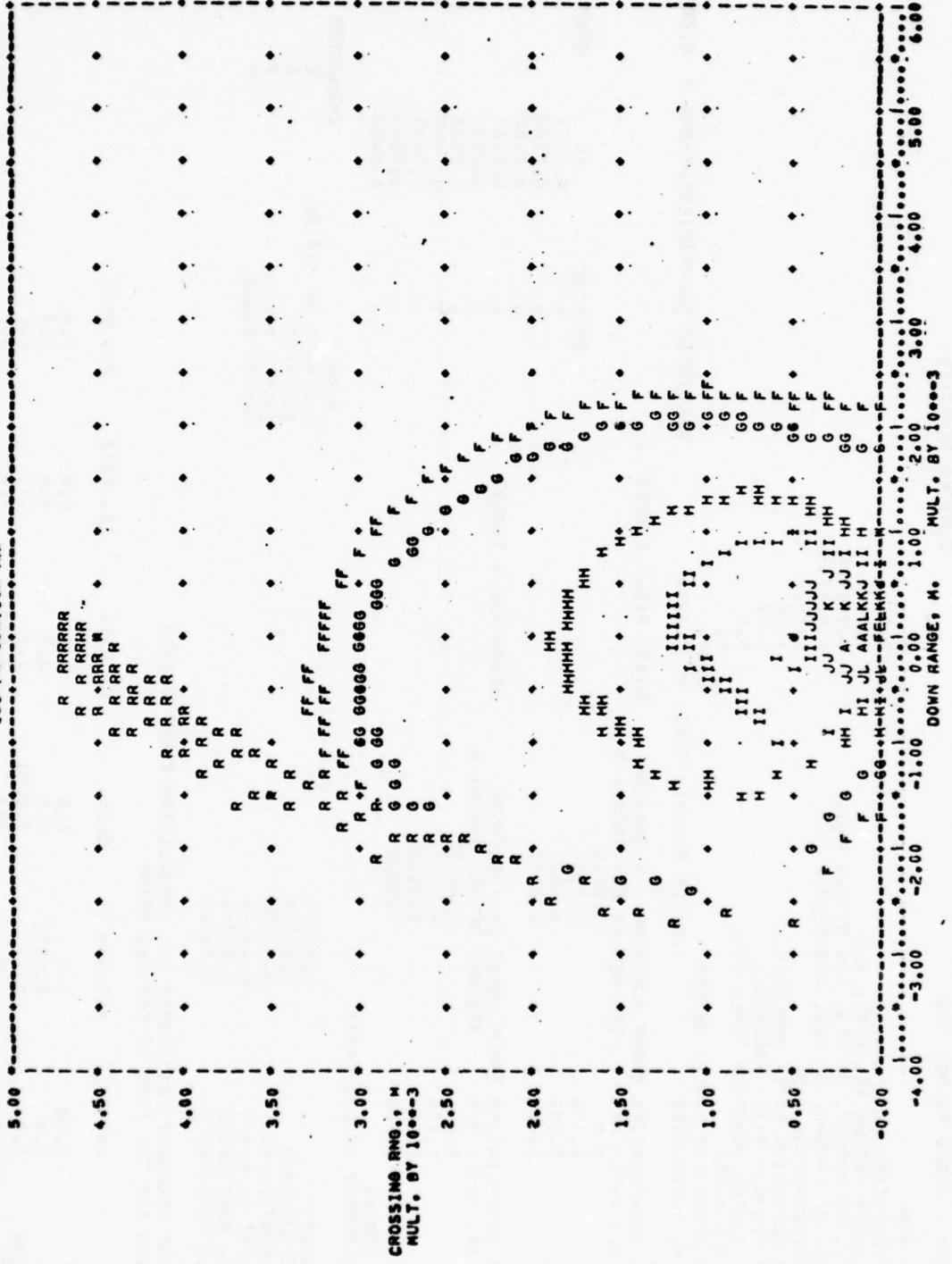
MASK	CHARACTER	MASK	CHARACTER
EL. RATE OR MAX EL	E	EL. RATE	E
AZ. RATE	A	AZ. RATE	A
INSUF. TIME	T	TIME	T
OUT OF RANGE	R	OUT OF RANGE	R



GADES 150 - PK CONTOUR PROGRAM -- MARCH 1973
 ACT STUNY - GROUP 9A NO. 1A6 C.HICKS 01/15/75

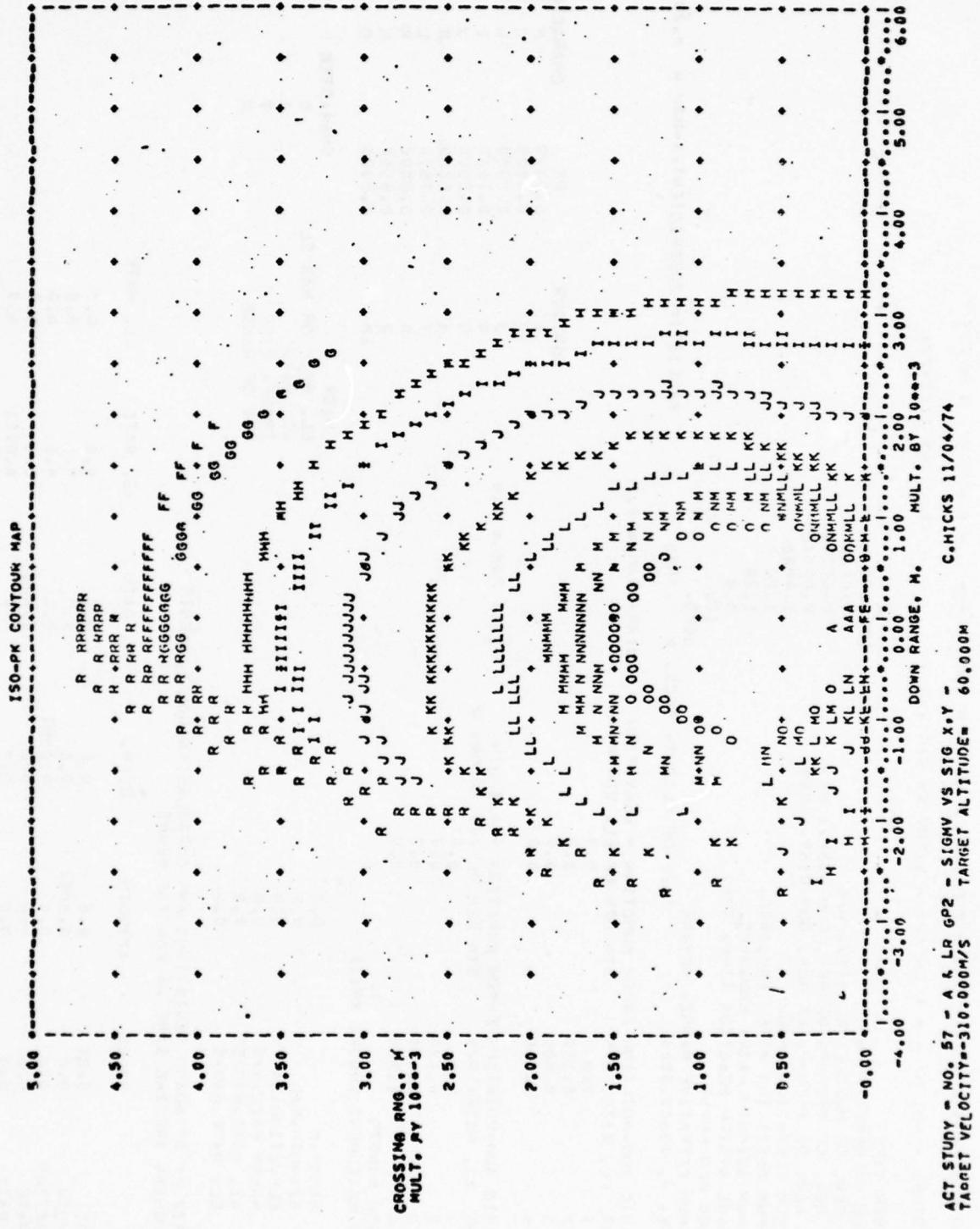
CALIBER TYPE	MUZZLE VELOCITY, M/S	TIME OF FLIGHT, SECs.	BIAS, RAD.	BALLISTIC COEFFICIENT, K-BAR
	1220.00	6000.	0.0000	0.2057
STD. DEV. OF MUZZLE VELOCITY, M/S	1.0000			
STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.	0.001700			
STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.	0.001700			
MAXIMUM ELEVATION, RAD.	1.4000			
MAXIMUM ELEVATION RATE, RAD./SEC.	1.20			
MAXIMUM AZIMUTH RATE, RAD./SEC.	1.20			
AVERAGE SYSTEM REACTION TIME, SEC.	0.0			
ROUNDS PER BURST	4.			
MAXIMUM EFFECTIVE RANGE, METERS	6000.			
RANGE, M. = 3500.0000		7.00000		
DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION	POINT EL. RATE, R/S	STD DEV OF EL. ERROR, R	BIAS, RAD.	0.0002
1	0.0	0.0010		
2	0.120	0.0010		
3	0.600	0.0010		
4	1.200	0.0020		
DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH	POINT AZ. RATE, R/S	STD DEV OF AZ. ERROR, R	BIAS, RAD.	0.0002
1	0.0	0.0010		
2	0.120	0.0010		
3	0.600	0.0010		
4	1.200	0.0020		
SENSOR FROPS				
MEAN MEASURENt ERRORS XM(1)				
RANGE, M.	2.00000			
AZIMUTH, RAD	0.00100			
ELEVATION, RAD	0.00100			
RANGE RATE, M/S	0.40000			
AZ. RATE, RAD/S	0.00040			
EL. RATE, RAD/S	0.00040			
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS	THE UNITS ARE THE SAME AS FOR THE MEANS			
RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE
RANGE	0.00	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0
R. RATE	0.0	0.0	0.0001	0.0
AZ. RATE	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0001	0.0

ISO-PK CONTOUR MAP



840ES150 - PK CONTINUOUS PROGRAM --- MARCH 1473
 ACT STUDY - NO. 57 - A R LR GMP - SIGMV VS STG vs Y -
 C.MTCKS 11/04/74

CALIBER TYPE	MUZZLE VELOCITY, M/S	1220.00	CHARACTER	PK
STD. DEV. OF MUZZLE VELOCITY, M/S		1.0000	CHARACTER	F
STD. DEV. OF X-COMP. OF HES. GUN DTSP., RAD.		0.000700	CHARACTER	G
STD. DEV. OF Y-COMP. OF HES. GUN DTSP., RAD.		0.000700	CHARACTER	H
MAXIMUM ELEVATION, RAD.		1.4400	CHARACTER	I
MAXIMUM ELEVATION RATE, RAD./SEC.		1.20	CHARACTER	J
MAXIMUM AZIMUTH RATE, RAD./SEC.		1.20	CHARACTER	K
AVERAGE SYSTEM REACTION TIME, SEC.		0.0	CHARACTER	L
ROUNDS PER QUIRST		1.0.	CHARACTER	M
MAXIMUM EFFECTIVE RANGE, METERS		6000.	CHARACTER	N
RANGE, M. = 3500.0000	TIME OF FLIGHT, SECS.	= 7.0000	CHARACTER	O
DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION		BIAS, RAD.= 0.0	CHARACTER	P
POTNT FL. RATE, R/S	STN DFV OF EL. ERRO, R		CHARACTER	Q
1	0.0	0.0	CHARACTER	R
2	0.120	0.0	CHARACTER	S
3	0.600	0.0	CHARACTER	T
4	1.200	0.0	CHARACTER	U
DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH		BIAS, RAD.= 0.0	CHARACTER	V
POTNT AZ. RATE, P/S	STN DEV OF AZ. ERROR, R		CHARACTER	W
1	0.0	0.0	CHARACTER	X
2	0.120	0.0	CHARACTER	Y
3	0.600	0.0	CHARACTER	Z
4	1.200	1.0	CHARACTER	A
SENSOR ERRORS			CHARACTER	B
MEAN MEASUREMENT ERRORS XM(I)			CHARACTER	C
RANGE, M.	0.0		CHARACTER	E
AZIMUTH, RAD.	0.0		CHARACTER	F
ELFVATION, RAD.	0.0		CHARACTER	A
RANGE RATE, M/S	0.0		CHARACTER	T
AZ. RATE, RAD/S	0.0		CHARACTER	R
EL. RATE, RAD/S	0.0		CHARACTER	S
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS				
THE UNITS ARE THE SAME AS FOR THE MEANS				
RANGE	AZIMUTH	ELFV.	R. RATE	EL. RATE
0.00	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0
ELFVATION	0.0	0.0	0.0001	0.0
R. RATE	0.0	0.0	0.0001	0.0
AZ. RATE	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0001	0.0



GAUSSIAN CONDITIONAL PROBABILITY --- MARCH 1974

ACT STUDY - GP 5 NO. HJ - STA OFV.

C. PITCHS 11/04/74

CALIBER TYPE

MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-COMP. OF GUN DISP., RAD.
 STD. DEV. OF Y-COMP. OF GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM ANGULAR RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 RADIUS OF CURVATURE, METERS
 MAXIMUM EFFECTIVE RANGE, METERS
 RANGE, M. = 3500.0000

TIME OF FLIGHT, SECS. = 7.0000

HALLISITIC COEFFICIENT, HAK = 0.2057

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT FL. RATE, R/S STD. DEV. OF EL. ERROR, R
 1 0.0 0.0015
 2 0.120 0.0015
 3 0.600 0.0020
 4 1.200 0.0030

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, R
 1 0.0 0.0015
 2 0.120 0.0015
 3 0.600 0.0020
 4 1.200 0.0030

MEAN MEASUREMENT ERRORS, MM(1)

RANGE, M
 AZIMUTH, RAD
 ELEVATION, RAD
 RANGE RATE, M/S
 AZ. RATE, RAD/S
 EL. RATE, RAD/S

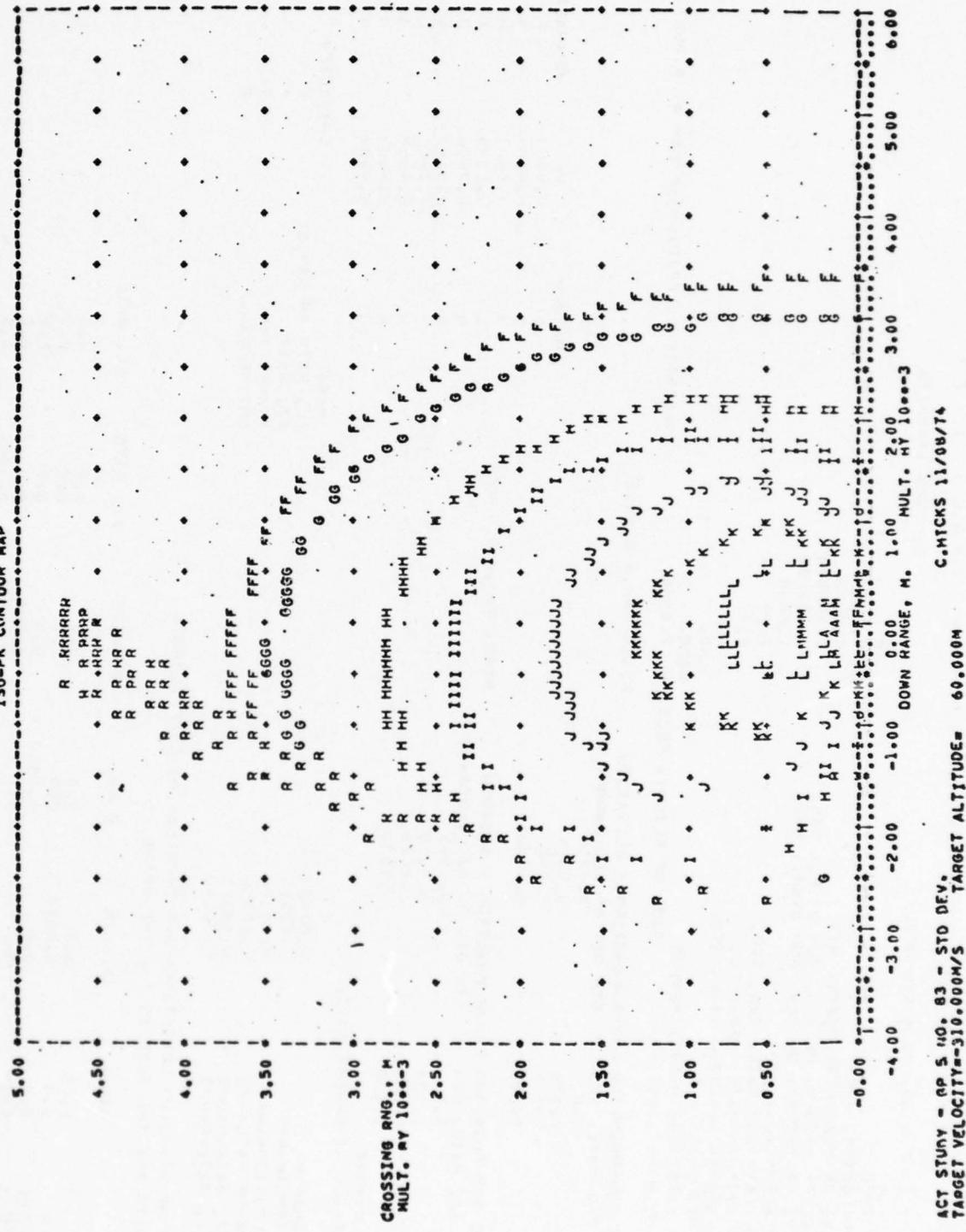
2.00000
 0.00100
 0.00100
 0.40000
 0.00040
 0.00040

CHARACTER
 F
 A
 T
 R

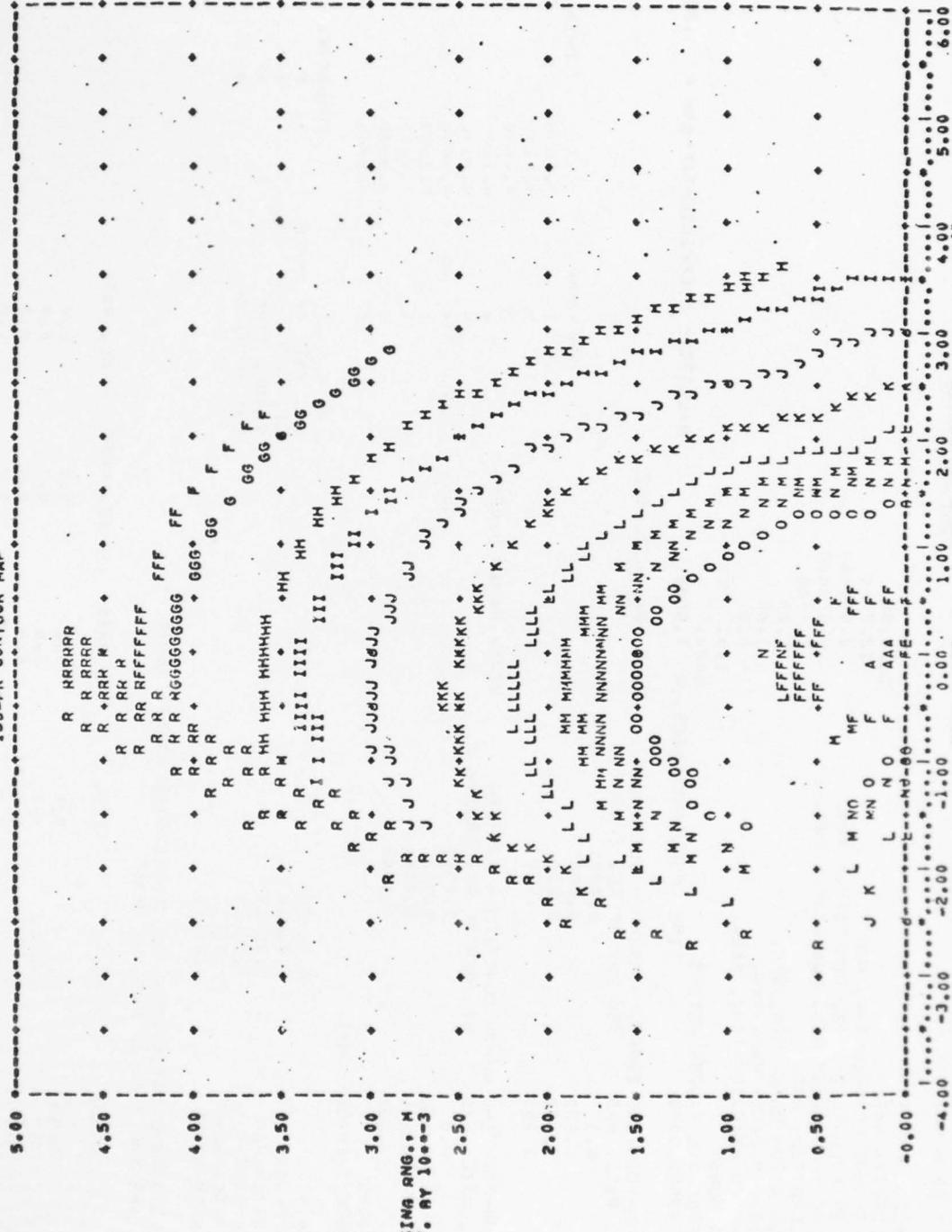
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	EL.FV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.50	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0010	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0010	0.0	0.0
R. RATE	0.0	0.0	0.0	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0005

ISO-PK CONTOUR MAP



ISO-PK CONTOUR MAP



ACT STUDY = OP 6 NO. 102
TIME = 00:00:00.000M/S

TARGET ALTITUDE = 60.000M

C.HICKS 11/19/74

GADES 150 - PK CONTOUR PROGRAM --- MARCH 1973

ACT STUDY - GROUP 9C NO. 220 C.MICKS 01/29/75

CALIBER TYPE

MUZZLE VELOCITY, M/S

STD. DEV. OF MUZZLE VELOCITY, M/S

STD. DEV. OF X-COMP. OF RES. GUN DISP., RAD.

STD. DEV. OF Y-COMP. OF RES. GUN DISP., RAD.

MAXIMUM ELEVATION, RAD.

MAXIMUM ELEVATION RATE, RAD./SEC.

MAXIMUM AZIMUTH RATE, RAD./SEC.

AVERAGE SYSTEM REACTION TIME, SEC.

ROUNDS PER PULSE

MAXIMUM EFFECTIVE RANGE, METERS

RANGE, M. = 350.0000 TIME OF FLIGHT, SECS. = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION

POINT EL. RATE, R/S STD DEV OF EL. ERROR, R

1 0.0 0.0010

2 0.120 0.0010

3 0.600 0.0010

4 1.200 0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH

POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

1 0.0 0.0010

2 0.120 0.0010

3 0.600 0.0010

4 1.200 0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - BIAS, RAD.= 0.0002

POINT EL. RATE, R/S STD DEV OF EL. ERROR, R

1 0.0 0.0010

2 0.120 0.0010

3 0.600 0.0010

4 1.200 0.0020

MEAN MEASUREMENT ERRORS XM(1)

RANGE, M

AZIMUTH, RAD

ELEVATION, RAD

RANGE RATE, M/S

AZ. RATE, RAD/S

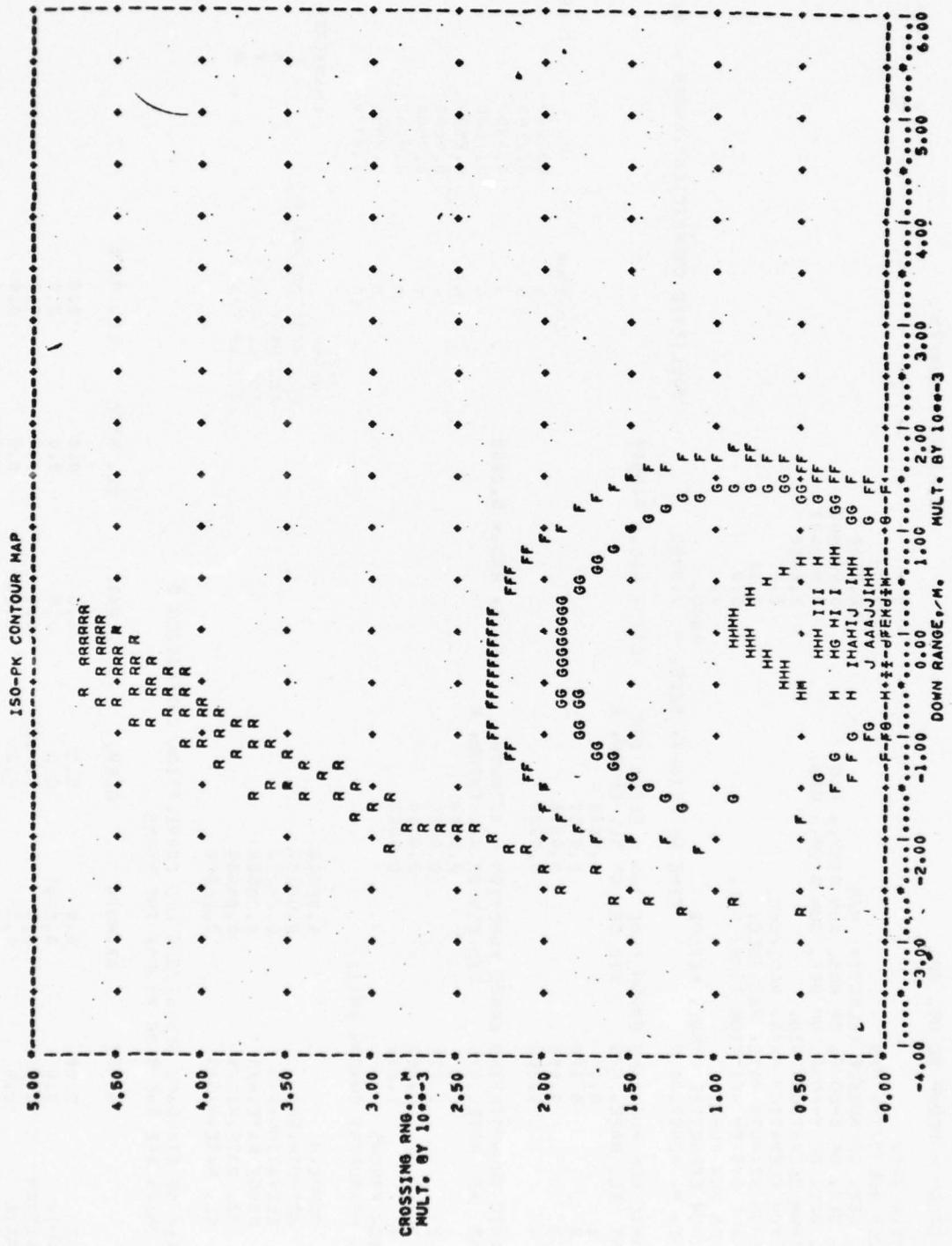
EL. RATE, RAD/S

4.00000
0.00200
0.00200
0.00000
0.00080
0.00080

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS

THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
RANGE	0.00	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.001	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.001	0.0	0.0
R. RATE	0.0	0.0	0.0	0.000	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0001



GADESS 150 - PK CONTOUR PROGRAM --- MARCH 1973
 ACT STUDY - GROUP 9D NO. 206 C.HICKS 01/15/75

CALIBER TYPE

MUZZLE VELOCITY, M/S

1220.00

12.2000

STD. DEV. OF MUZZLE VELOCITY, M/S

0.000800

STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.

0.000800

STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.

0.000800

MAXIMUM ELEVATION, RAD.

1.4800

MAXIMUM ELEVATION RATE, RAD./SEC.

1.20

MAXIMUM AZIMUTH RATE, RAD./SEC.

1.20

AVERAGE SYSTEM REACTION TIME, SEC.

0.0

MAXIMUM EFFECTIVE RANGE, METERS

6000.

TIME OF FLIGHT, SECS. = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION POINT EL. RATE, R/S STD DEV OF EL. ERROR, R

0.0010

0.0010

0.0010

0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

0.0010

0.0010

0.0010

0.0020

MEAN MEASUREMENT ERRORS XM(1)

RANGE, M

1.00000

AZIMUTH, RAD

0.00050

ELEVATION, RAD

0.00050

RANGE RATE, M/S

0.20000

AZ. RATE, RAD/S

0.00020

EL. RATE, RAD/S

0.00020

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS

THE UNITS ARE THE SAME AS FOR THE MEANS

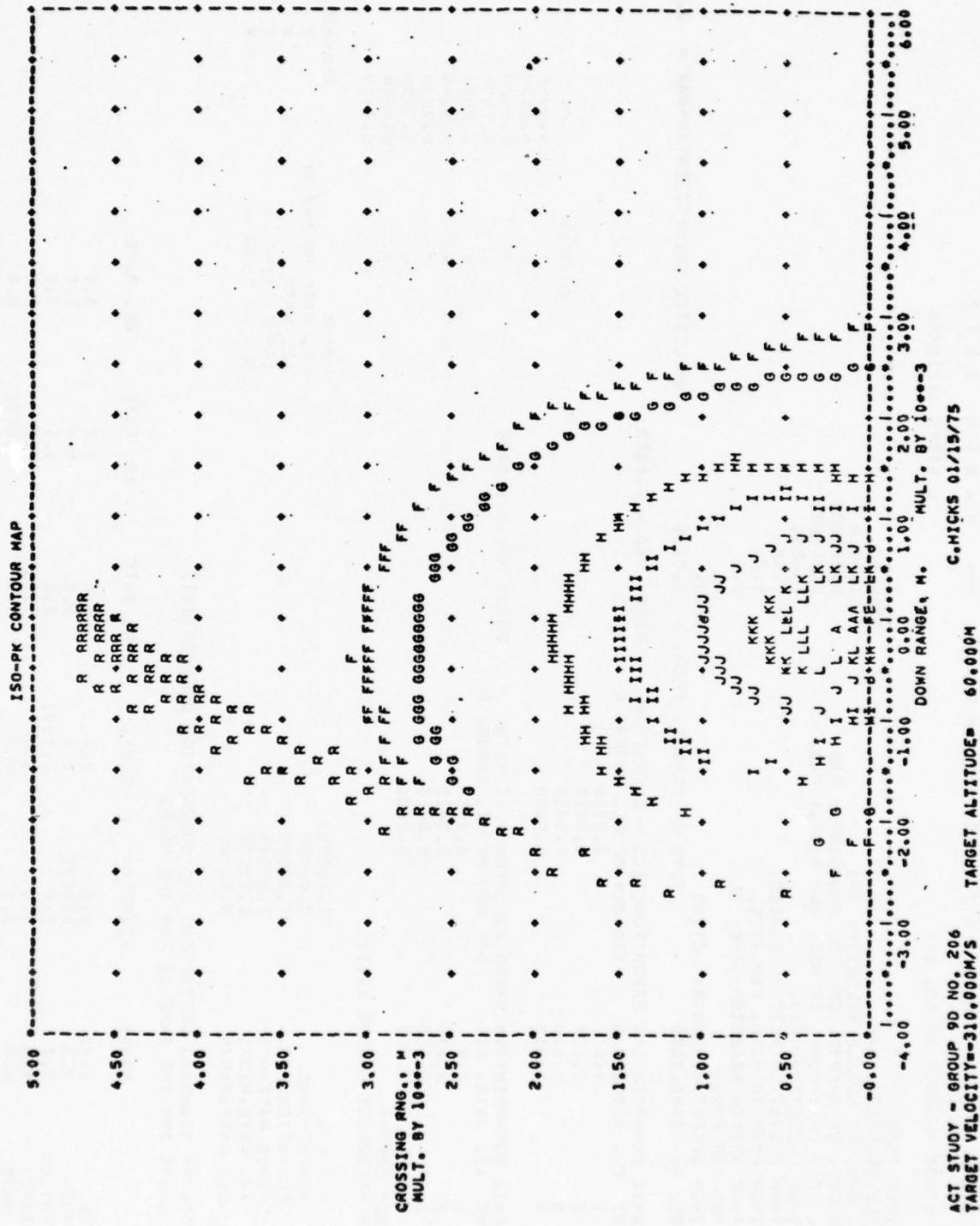
RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
0.00	0.0	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0001	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0001	0.0	0.0
R RATE	0.0	0.0	0.0	0.0	0.0
AZ. RATE	0.0	0.0	0.0	0.0001	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0001

BALLISTIC COEFFICIENT, K-BAR = 0.2057

CHARACTER	PX	0.0050
CHARACTER	F	0.0100
CHARACTER	F	0.0200
CHARACTER	F	0.0400
CHARACTER	F	0.0800
CHARACTER	F	0.1600
CHARACTER	F	0.3200
CHARACTER	F	0.6400
CHARACTER	F	0.7500
CHARACTER	F	0.9000
CHARACTER	F	0.9500
CHARACTER	F	0.9900

MASK

FL. RATE ON MAX EL.	E
AZ. RATE	A
INSUF. TIME	F
OUT OF RANGE	R



G A N D E S I S O - P R C C O N T R O L P R O G R A M --- M A R C H 1 9 7 3

A C T S T U D Y - R P N 4 1 1 . 2 0 9 C . H I C K S 0 4 / U 7 4

CALIBER TYPE: 2

MUZZLE VELOCITY, M/S: 1220.00

STD. DEV. OF MUZZLE VELOCITY, M/S: 0.00000

STD. DEV. OF X-COMP. OF GUN DISP., RAD.: 0.000400

STD. DEV. OF Y-COMP. OF GUN DISP., RAD.: 0.000400

MAXIMUM ELEVATION, RAD.: 1.4400

MAXIMUM ELEVATION RATE, RAD./SEC.: 1.20

MAXIMUM AZIMUTH RATE, RAD./SEC.: 1.20

AVERAGE SYSTEM REACTION TIME, SEC.: 0.0

ROUNDS PER BURST: 4.

MAXIMUM EFFECTIVE RANGE, METERS: 6000.

RANGE, M.: =3500.000 TIME OF FLIGHT, SECS.: = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION POINT FL. RATE, R/S: BIASS, RAD.= 0.0002

POINT	FL. RATE, R/S	STD. DEV. OF EL. ERROR, R
1	0.0	0.0001
2	0.120	0.0001
3	0.600	0.0001
4	1.200	0.0003

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH POINT AZ. RATE, M/S: BIASS, RAD.= 0.0002

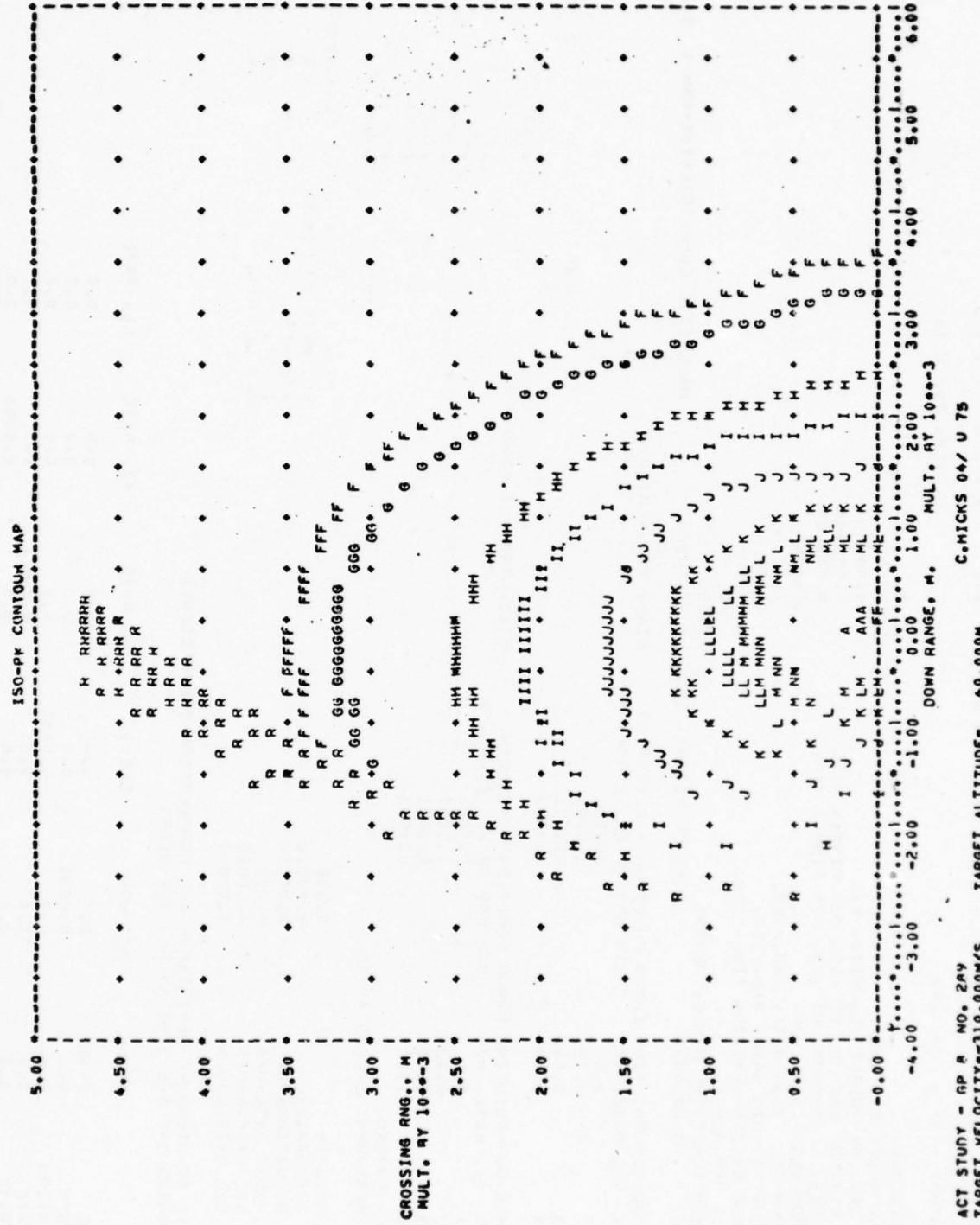
POINT	AZ. RATE, M/S	STD. DEV. OF AZ. ERROR, R
1	0.0	0.0001
2	0.120	0.0001
3	0.600	0.0001
4	1.200	0.0003

SENSOR ERRORS MEAN MEASUREMENT ERRORS X(1)

RANGE, M.	AZIMUTH, RAD.	ELEV., RAD.	EL. RATE, RAD./SEC.
0.500	0.00010	0.00010	0.00010
0.0	0.00010	0.00010	0.00010
0.200	0.00010	0.00010	0.00010
0.0	0.00010	0.00010	0.00010
0.0	0.00010	0.00010	0.00010

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	EL. RATE	AZ. RATE	EL. RATE
0.50	0.0	0.0	0.0	0.0	0.0
0.0	0.0001	0.0	0.0	0.0	0.0
0.0	0.0	0.0001	0.0	0.0	0.0
0.0	0.0	0.0	0.200	0.0	0.0
0.0	0.0	0.0	0.0	0.0001	0.0
0.0	0.0	0.0	0.0	0.0	0.0001



ACT STUDY - GP # NO. 2A4
TARGET 1 VELOCITY = 310.000M/S

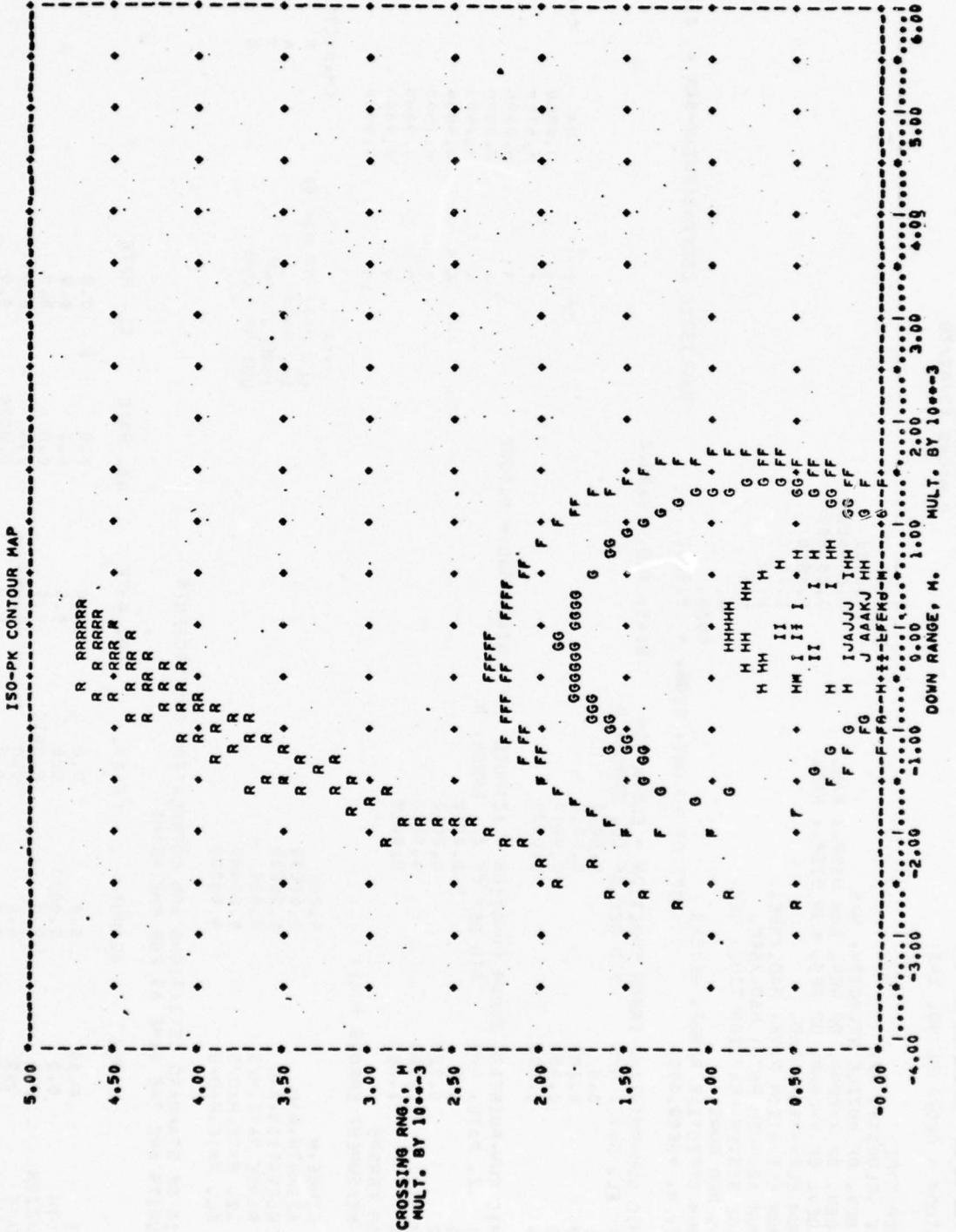
TARGET ALTITUDE = 60.000M

C.HICKS 04/ U 75

GADES 150-PK CONTOUR PROGRAM --- MARCH 1973
 ACT STUDY - GROUP 9E NO. 243

C.HICKS 02/07/75

CALIBER TYPE	2								
NUZZLE VELOCITY, M/S	1220.00								
STD. DEV. OF MUZZLE VELOCITY, M/S	12.2000								
STD. DEV. OF X-COMP. OF RES. GUN DISP., RAD.	0.003400								
STD. DEV. OF Y-COMP. OF RES. GUN DISP., RAD.	0.003400								
MAXIMUM ELEVATION, RAD.	1.4A00								
MAXIMUM ELEVATION RATE, RAD./SEC.	1.20								
MAXIMUM AZIMUTH RATE, RAD./SEC.	1.20								
AVERAGE SYSTEM REACTION TIME, SEC.	0.0								
ROUNDS PER BURST	4.								
MAXIMUM EFFECTIVE RANGE, METERS	6000.								
PARSE, M. = 3500.0000	TIME OF FLIGHT, SECS. = 7.0000								
DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION									
POINT EL. RATE, R/S		STD DEV OF EL. ERROR, R							
1	0.0	0.0010							
2	0.120	0.0010							
3	0.600	0.0010							
4	1.200	0.0020							
DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH									
POINT AZ. RATE, R/S		STD DEV OF AZ. ERROR, R							
1	0.0	0.0010							
2	0.120	0.0010							
3	0.600	0.0010							
4	1.200	0.0020							
SENSOR ERRORS									
MEAN MEASUREN ^T ERRORS XM(1)									
RANGE, M	4.000								
AZIMUTH, RAD	0.00200								
ELEVATION, RAD	0.00200								
RANGE RATE, M/S	0.800								
AZ. RATE, RAD/S	0.00080								
EL. RATE, RAD/S	0.00080								
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS									
THE UNITS ARE THE SAME AS FOR THE MEANS									
RANGE	4.00	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE			
AZIMUTH	0.0	0.0	0.0	0.0	0.0	0.0			
ELEVATION	0.0	0.0010	0.0	0.0	0.0	0.0			
R. RATE	0.0	0.0	0.0010	0.0	0.0	0.0			
AZ. RATE	0.0	0.0	0.0	1.000	0.0	0.0			
EL. RATE	0.0	0.0	0.0	0.0	0.0010	0.0			



GADES 150 - PK COUNTDOWN PROGRAM --- LAUNCH 1973

ACT STUDY - GROUP 96 NO. 250

C.HICKS 02/19/75

CALIBER TYPE

MUZZLE VELOCITY, M/S
 STD. DEV. OF MUZZLE VELOCITY, M/S
 STD. DEV. OF X-COMP. OF RES. GUN DISP., RAD.
 STD. DEV. OF Y-COMP. OF RES. GUN DISP., RAD.
 MAXIMUM ELEVATION, RAD.
 MAXIMUM ELEVATION RATE, RAD./SEC.
 MAXIMUM AZIMUTH RATE, RAD./SEC.
 AVERAGE SYSTEM REACTION TIME, SEC.
 ROUNDS PER FUSIL
 MAXIMUM EFFECTIVE RANGE, METERS

RANGE, M. = 3500.0000 TIME OF FLIGHT, SECs. = 7.00000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
 POINT FL. RATE, K/S STD DEV OF EL. ERROR, R

1	0.0	0.0010
2	0.120	0.0010
3	0.600	0.0010
4	1.200	0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
 POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R

1	0.0	0.0010
2	0.120	0.0010
3	0.600	0.0010
4	1.200	0.0020

SENSOR ERRORS

MEAN MEASURMENT ERRORS XM(1)

RANGE, M.
 AZIMUTH, RAU
 ELEVATION, RAU
 RANGE RATE, M/S
 AZ. RATE, RAU/S
 EL. RATE, RAU/S

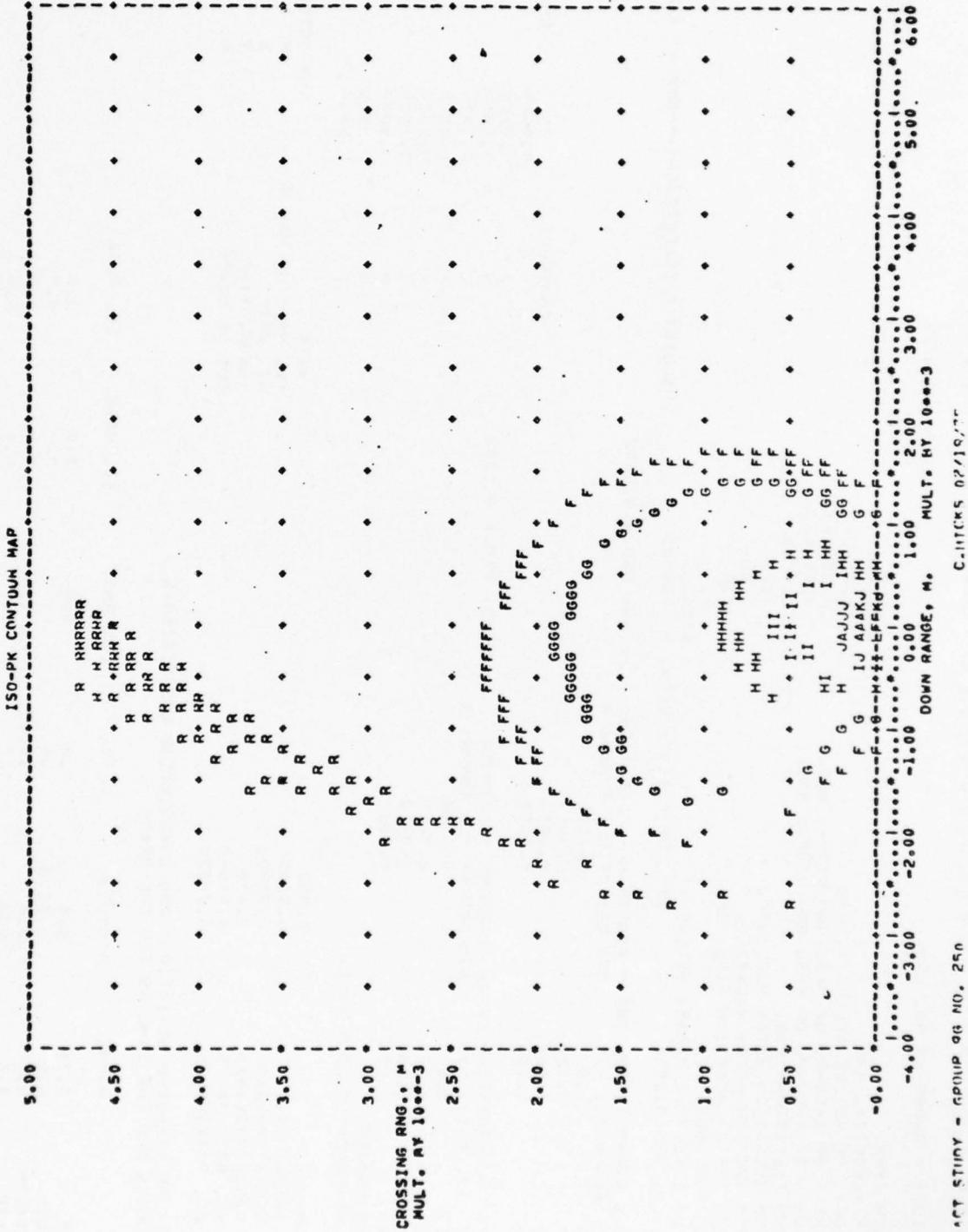
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
 THE UNITS ARE THE SAME AS FOR THE MFANS

RANGE	AZIMUTH	ELEV.	RAU	AZ. RATE	EL. RATE
RANGE	3.75	0.0	0.0	0.0	0.0
AZIMUTH	0.0	0.0003	0.0	0.0	0.0
ELEVATION	0.0	0.0	0.0003	0.0	0.0
RA. RATE	0.0	0.0	0.0	1.000	0.0
AZ. RATE	0.0	0.0	0.0	0.0	0.0
EL. RATE	0.0	0.0	0.0	0.0	0.0010

HALLISTIC COEFFICIENT, K-BAH = 0.2057

CHARACTER	PK	F
1	0.0040	0.0100
2	0.0500	0.0500
3	0.1000	0.1000
4	0.1500	0.1500
5	0.2000	0.2000
6	0.2500	0.2500
7	0.3000	0.3000
8	0.3500	0.3500
9	0.4000	0.4000
10	0.4500	0.4500

CHARACTER	FL.	AZ.	EL.
?	0.0500	0.0500	0.0500
H	0.1000	0.1000	0.1000
I	0.1500	0.1500	0.1500
J	0.2000	0.2000	0.2000
K	0.2500	0.2500	0.2500
L	0.3000	0.3000	0.3000
M	0.3500	0.3500	0.3500
N	0.4000	0.4000	0.4000
O	0.4500	0.4500	0.4500



GAUSSIAN - P.R. CONTOUR PROGRAM --- MARCH 1973

ACT STUDY - GROUP 96 NO. 25?

C.HICKS 02/14/75

CALIBER TYPE
MUZZLE VELOCITY, M/S
STD. DEV. OF MUZZLE VELOCITY, M/S
STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.
STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.
MAXIMUM ELEVATION, RAD.
MAXIMUM ELEVATION RATE, RAD./SEC.
MAXIMUM AZIMUTH RATE, RAD./SEC.
AVERAGE SYSTEM REACTION TIME, SEC.
ROUNDS PER RUST
MAXIMUM EFFECTIVE RANGE, METERS
RANGE, M. = 3500.0000 TIME OF FLIGHT, SECS. = 7.0000

DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION
POINT EL. RATE, R/S STD DEV OF EL. ERROR, R
1 0.0 0.0010
2 0.120 0.0010
3 0.600 0.0010
4 1.200 0.0020

DYNAMIC GUN-POINTING ERROR FUNCTION - AZIMUTH
POINT AZ. RATE, R/S STD DEV OF AZ. ERROR, R
1 0.0 0.0010
2 0.120 0.0010
3 0.600 0.0010
4 1.200 0.0020

SENSOR ERRORS

MEAN MEASUREMENT ERRORS XM(I)

RANGE, M.
AZIMUTH, RAD.
ELEVATION, RAD.

RANGE RATE, M/S
AZ. RATE, RAD/S
EL. RATE, RAD/S

R. RATE
AZ. RATE
EL. RATE

2 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

3 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

4 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

5 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

6 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

7 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

8 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

9 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

10 1220.00
12.2000
0.003400
0.003400
1.4000
1.2000
1.20
0.0
4.00

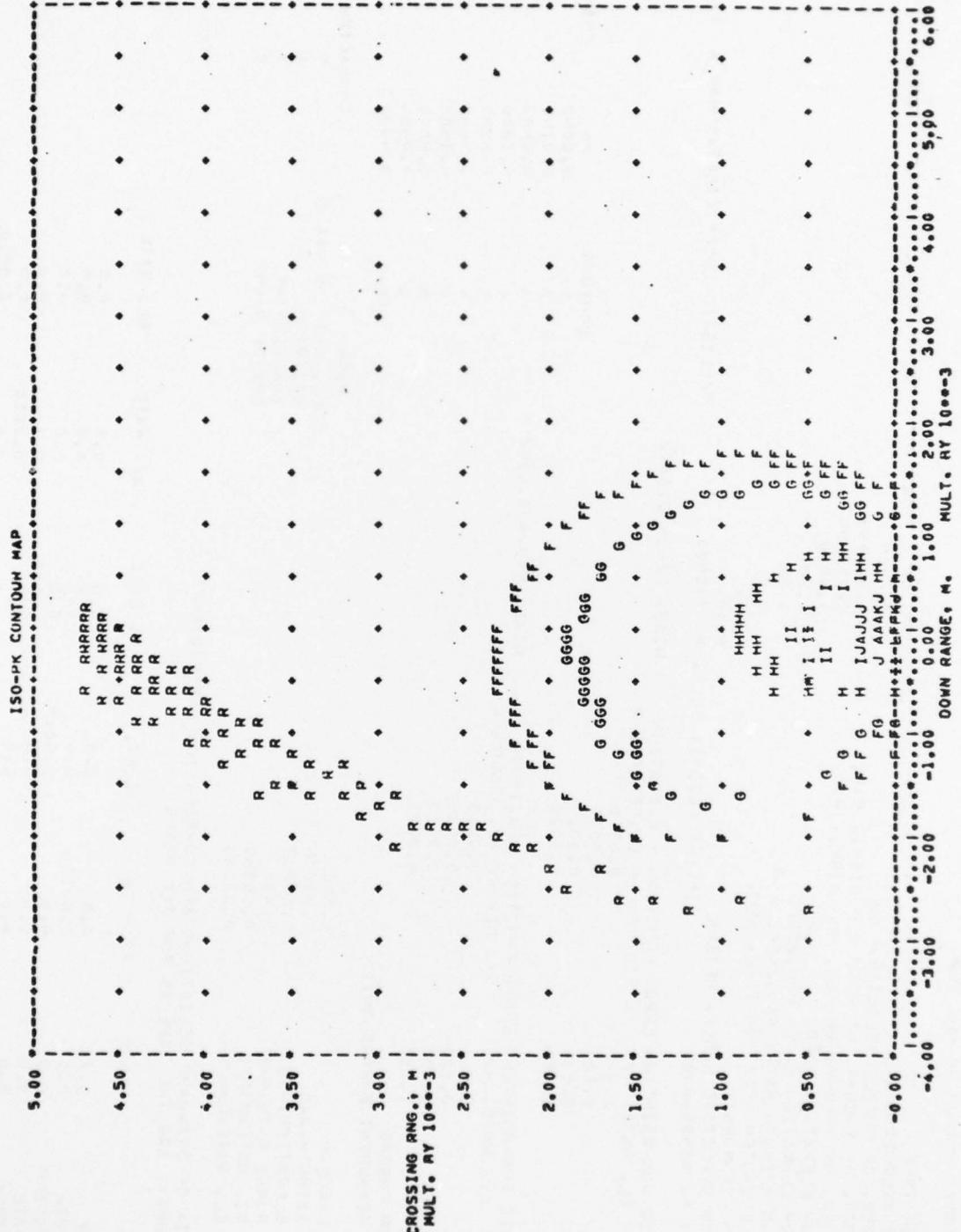
CHARACTERISTICS

MASK
EL. RATE OR MAX EL.
AZ. RATE
INSUF. TIME
OUT OF RANGE

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS

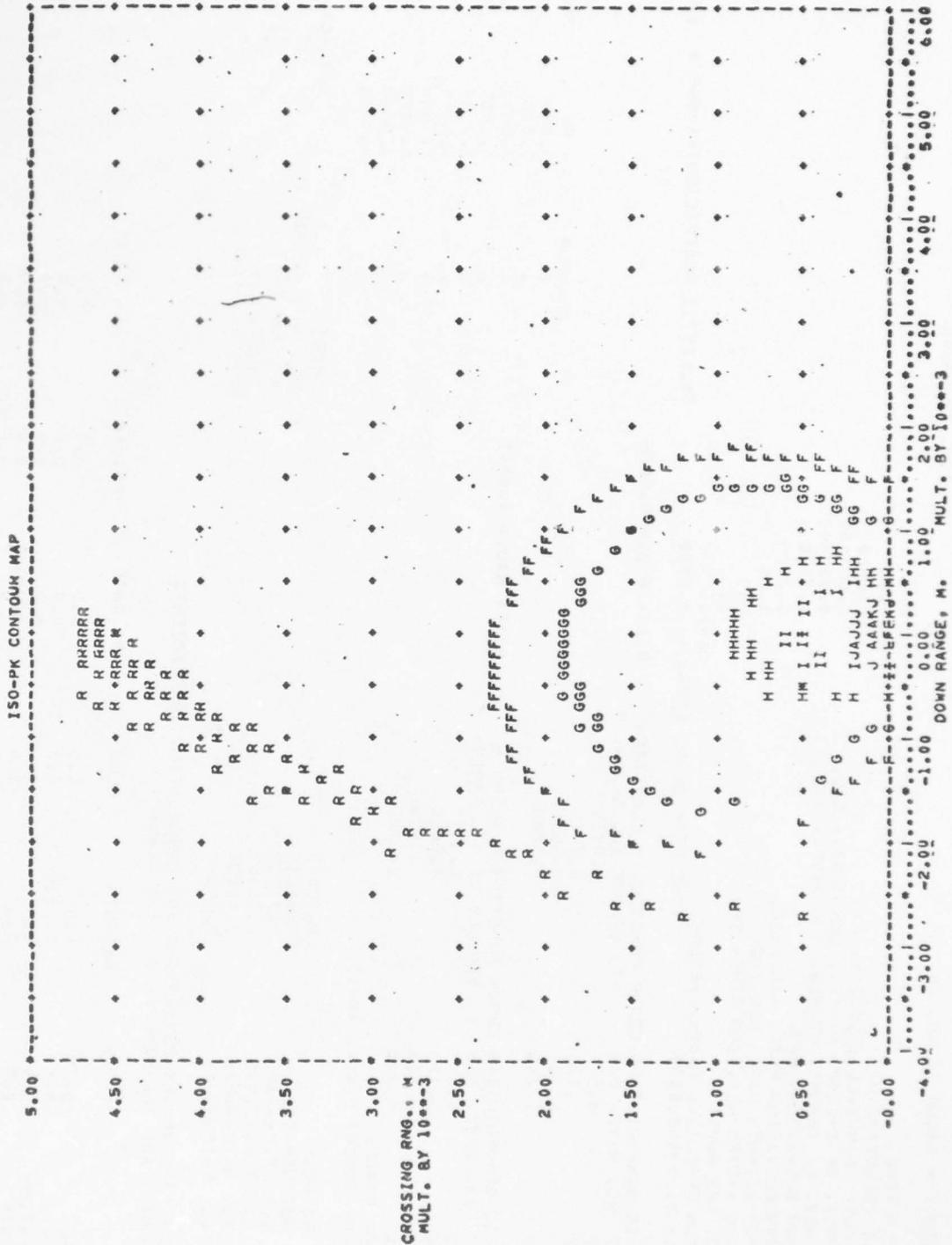
THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	P. RATE	AZ. RATE	EL. RATE
3.75	0.0	0.0	0.0	0.0	0.0
0.0	0.0010	0.0	0.0	0.0	0.0
0.0	0.0	0.0010	0.0	0.0	0.0
0.0	0.0	0.0	1.000	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0



G A U E S I S U - P K C O N T O U R P R O G R A M M A R C H 1 9 7 3
 ACT STUDY - GROUP 94 NO. 263

CALIBER TYPE	2	CHARACTER			
MUZZLE VELOCITY, M/S	1220.00				
STD. DEV. OF MUZZLE VELOCITY, M/S	12.2000				
STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.	0.003400				
STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.	0.003400				
MAXIMUM ELEVATION, RAD.	1.4900				
MAXIMUM ELEVATION RATE, RAD./SEC.	1.20				
MAXIMUM AZIMUTH RATE, RAD./SEC.	1.20				
AVERAGE SYSTEM REACTION TIME, SEC.	0.0				
ROU-D'S PER RURST	4.				
MAXIMUM EFFECTIVE RANGE, METERS	6000.				
RANGE, " = 3500.0000	TIME OF FLIGHT, SECS. = 7.0000	BALLISTIC COEFFICIENT, K-BAR = 0.2057			
DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION	BIAS, RAD.= 0.0002	CHARACTER			
POINT EL. RATE, R/S	STD DEV OF EL. ERROR, R				
1 0.0	0.0010	CONTOUR			
2 0.120	0.0010	1 6.0046			
3 0.600	0.0010	2 0.0160			
4 1.200	0.0020	3 0.0200			
SENSEUR ERRORS		4 0.1000			
MEAN MEASUREMENT ERRORS XM(I)		5 0.2500			
RANGE, M	4.00000	K			
AZIMUTH, RAD	0.00200	L			
ELEVATION, RAD	0.00200	M			
RANGE RATE, M/S	0.00000	N			
AZ. RATE, RAD/S	0.000080	O			
EL. RATE, RAD/S	0.000080	P			
MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS		CHARACTER			
THE UNITS ARE THE SAME AS FOR THE MEANS					
RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
3.75	0.0	0.0	0.0	0.0	0.0
0.0	0.0010	0.0	0.0	0.0	0.0
0.0	0.0	0.0010	0.0	0.0	0.0
0.0	0.0	0.0	0.300	0.0	0.0
0.0	0.0	0.0	0.0	0.0001	0.0
0.0	0.0	0.0	0.0	0.0	0.0001



GADGETS - GROUP 4.1 (II). P72

ACT STUDY - GROUP 4.1 (II). P72

CONTINUATION

CALC'DR TYPE

MUZZLE VELOCITY, M/S

STD. DEV. OF 100/LF VELOCITY, M/S

STD. DEV. OF X-COMP. OF 100/LF VELOCITY, M/S

STD. DEV. OF Y-COMP. OF 100/LF VELOCITY, M/S

MAXIMUM ELEVATION, DEG.

MAXIMUM AZIMUTH RATE, DEG./SEC.

AVERAGE SYSTEM REACTION TIME, SEC.

ROUNDS PER PULSE

MAXIMUM EFFECTIVE RANGE, MILES

RANGE, MILES = 3500.0000

TIME OF FLIGHT, SECS. = 7.0000

DYNAMIC GUN-PULSES, EXPONENTIAL FUNCTION - ELEVATION
POINT FL. RATE, R/S STD. DEV. OF EL. ERROR, R

1 0.0 0.010

2 0.120 0.010

3 0.200 0.010

4 0.200 0.020

DYNAMIC GUN-PULSES, EXPONENTIAL FUNCTION - AZIMUTH

POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, R

1 0.0 0.010

2 0.120 0.010

3 0.200 0.010

4 0.200 0.020

SENSORS, CHAMBERS

MEAN MEASUREMENT ERRORS X(1)

HATF, HATF

AZ. HATF, HATF

EL. HATF, HATF

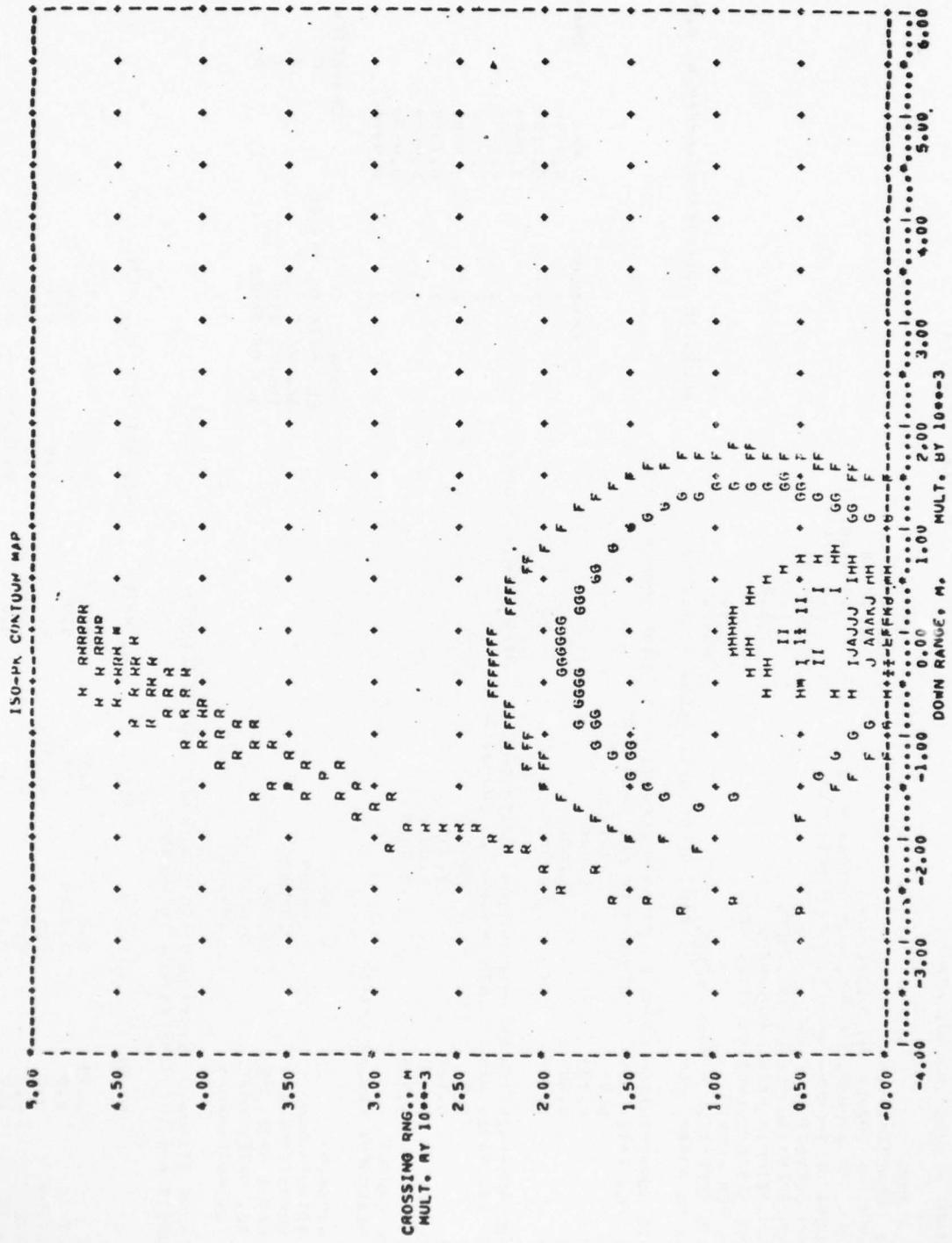
HATF, HATF

AZ. HATF, HATF

EL. HATF, HATF

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

HATF	AZIMUTH	ELEV.	R. HATF	AZ. HATF	EL. HATF
1.000	0.000	0.000	0.000	0.000	0.000
0.000	1.000	0.000	0.000	0.000	0.000
0.000	0.000	1.000	0.000	0.000	0.000
0.000	0.000	0.000	1.000	0.000	0.000
0.000	0.000	0.000	0.000	1.000	0.000
0.000	0.000	0.000	0.000	0.000	1.000



GADDESS - PRC CONTROL PROGRAM ---- MARCH 1973

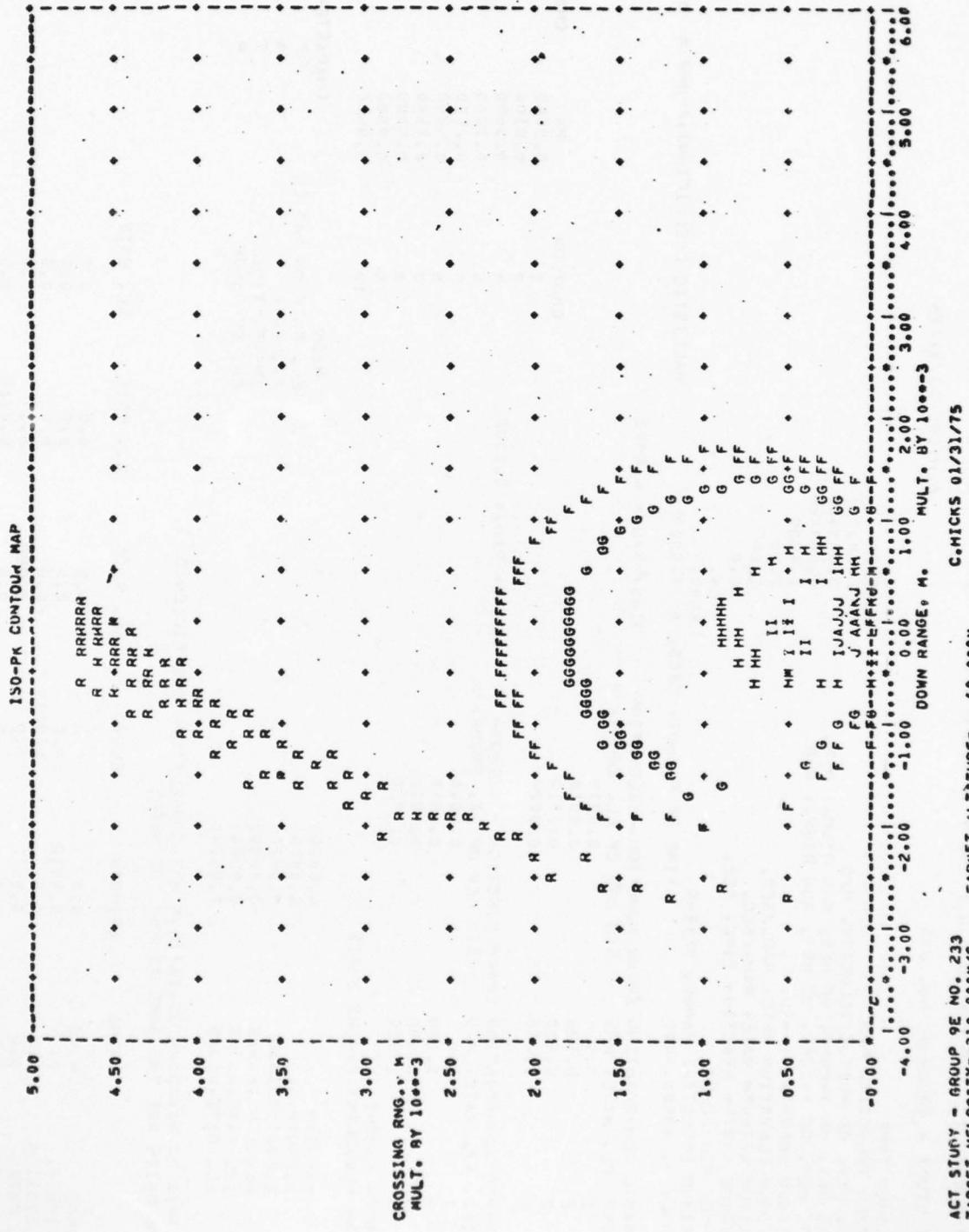
ACT STUDY - GROUP 9C NO. 233

C.HICKS 01/31/75

CALIBER TYPE		MUZZLE VELOCITY, M/S		STD. DEV. OF MUZZLE VELOCITY, " / S		STD. DEV. OF X-COMP. OF HES. GUN DISP., RAD.		STD. DEV. OF Y-COMP. OF HES. GUN DISP., RAD.		MAXIMUM ELEVATION, RAD.		MAXIMUM ELEVATION RATE, RAD./SEC.		MAXIMUM AZIMUTH RATE, RAD./SEC.		AVERAGE SYSTEM REACTION TIME, SEC.		MAXIMUM EFFECTIVE RANGE, METERS		TIME OF FLIGHT, SECS. = 7.0000		BALLISTIC COEFFICIENT, K-BAR = 0.2057	
POINT FL. RATE, R/S	STD. DEV. OF EL. ERROR, RAD.	1220.00	2	12.2000	12.2000	0.003400	0.003400	0.003400	0.003400	1.4000	1.4000	1.20	1.20	1.20	1.20	0.0	0.0	6000.	4.	CHARACTER	F		
1	0.0	0.0	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	10	CHARACTER	F			
2	0.120	0.120	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	10	CHARACTER	F			
3	0.600	0.600	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	10	CHARACTER	F			
4	1.200	1.200	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	10	CHARACTER	F			
DYNAMIC GUN-POINTING ERROR FUNCTION - ELEVATION		BIAS, RAD.= 0.0002		POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, RAD.		BIAS, RAD.= 0.0002		POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, RAD.		BIAS, RAD.= 0.0002		POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, RAD.		BIAS, RAD.= 0.0002		POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, RAD.		BIAS, RAD.= 0.0002		POINT AZ. RATE, R/S STD. DEV. OF AZ. ERROR, RAD.			
1	0.0	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	MASK	F			
2	0.120	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	CHARACTER	A			
3	0.600	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	0.0010	0.0	0.0010	0.0010	0.0	0.0	0.0010	0.0010	CHARACTER	T			
4	1.200	0.0020	0.0020	0.0	0.0020	0.0020	0.0	0.0	0.0020	0.0020	0.0020	0.0	0.0020	0.0020	0.0	0.0	0.0020	0.0020	CHARACTER	R			
SENSOR FREQUENCIES		MEAN MEASUREMENT ERRORS XM(I)		RANGE		AZIMUTH		ELEV.		R. RATE		AZ. RATE		EL. RATE		RANGE		AZIMUTH		ELEV.		R. RATE	
RANGE, M/S		AZIMUTH, RAD.		ELEVATION, RAD.		EL. RATE, RAD./SEC.		AZ. RATE, RAD./SEC.		EL. RATE, RAD./SEC.		AZ. RATE, RAD./SEC.		EL. RATE, RAD./SEC.		RANGE		AZIMUTH		ELEV.		R. RATE	
4.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.00	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

MATRIX OF STANDARD DEVIATIONS AND CORRELATION COEFFICIENTS
THE UNITS ARE THE SAME AS FOR THE MEANS

RANGE	AZIMUTH	ELEV.	R. RATE	AZ. RATE	EL. RATE
4.00	0.0	0.0	0.0	0.0	0.0
0.0	0.0010	0.0	0.0	0.0	0.0
0.0	0.0	0.0010	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0000	0.0
0.0	0.0	0.0	0.0	0.0000	0.0
0.0	0.0	0.0	0.0	0.0000	0.0
0.0	0.0	0.0	0.0	0.0000	0.0



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