

MOST Project -3FG 0,1411 UNCLASSIFIED C014-44008 **CUP** Technical Memo Summary of Signal Processing Techniques for Conformal/Planar Array Sonar System (U) 8 ADA03172 7 March 1966 Contract NObsr 93022 680425-0260 Project Serial Number SS-048-00 Task 8189 65 (GE Requisition Number EH-88157) Prepared by 1976 NOV 5 General Electric Company W Heavy Military Electronics Division Syracuse, N.Y. spectr A DISTRIBUTION STATEMENT A Approved for public release; Prepared for Distribution Unlimited Navy Department Bureau of Ships U.S. Navy Electronics Laboratory San Diego, California of the United States within the maning of the This dogs defen mare Laws Title & U.S.C. / Section 793 and 79 mission of the revelation of its contents in a Espi tre uthorned person is prohibited by law. DOWNGRADED AT 3 YEAR INTERVALS: DECLASSIFIED AFTER 12 YEARS DOD DIR 5200.10 UNCLASSIFIED

14) C\$14-44\$\$ Technical Memo., Summary of Signal Processing Techniques 6 for Conformal/Planar Array Sonar System 7 Mar 66 Nobsr-93022 Project Serial Number 55-048-00 Task 8189 (GE Requisition Number EH-88157) T. Stark Prepared by General Electric Company Heavy Military Electronics Division Syracuse, N.Y. Prepared for Navy Department Bureau of Ships NOV 5 1976 U.S. Navy Electronics Laboratory San Diego, California This document contains information affecting the national defense of ites within the meaning of the Unit Espin Etio d 794. The r the ition of ۶, د contents in any an unauth zed person as prohibited iner DOWNGRADED AT 3 YEAR INTERVALS: DECLASSIFIED AFTER 12 YEARS DOD DIR 5200.10 UNICLASSIF MEIDENELAI 9510



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## Summary of Signal Processing Techniques

for

Conformal/Planar Array Sonar System (U)

## CONFORMAL/PLANAR ARRAY SONAR PROJECT

March 1966

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#### SECTION I

#### INTRODUCTION

This report covers work done on signal processing technique studies during the period from January 1, 1966 to February 28, 1966 on the Conformal/Planar Array Sonar Contract NObsr 93022. /

A previous report entitled "The First Cut Signal Processor for Conformal/ Planar Array Sonar System", <sup>1</sup> in which a feasible signal processing sub-system for the C/PAS System was recommended, contains much of the background material for the work reported here. In the course of this work various techniques were studied under the requirements imposed by the C/PAS System concept, se outfilled in references 2 and 3. Since the system concept presented in these references may be quite different from the system concept that is finally chosen it was deemed appropriate to review the technique studies that were previously made and to determine their range of applicibility in terms of signal bandwidth and number of beams to be processed.

Therefore, the purpose of the work reported here is to:

(1) Review the technique studies previously conducted to determine feasibility of these techniques for various combinations of signal bandwidth and number of beams. Specifically, bandwidths in the range of 50 to 200 cps for the wideband signals, 1 to 4 cps for the narrow band signal, and number of beams in the range of 100 to 1000 were assumed.

(2) Extend the studies previously conducted to include cost and size estimates for hardware implementations of the First Cut Signal Processing Sub-System, as well as for other techniques studied, as a function of signal bandwidth and number of beams.

(3) Identify critical components of the most promising techniques which require further detailed study and/or laboratory breadboard work in order to raise confidence level for application to the C/PAS System.

Section II contains a summary of the important features of the signal processing techniques which have been studied to date as well as a table showing requirements under which the studies were made. \_\_\_\_\_\_ TO PC, 2

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Section III summarizes the results of the studies of cost as a function of signal bandwidth and number of beams.

In Section IV critical parts of promising techniques are identified and recommendations for further study are given.

Sections V, VI and VII contain the details of the cost studies for the surface duct, narrowband bottom bounce, and wideband bottom bounce techniques.

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#### SECTION II

#### SUMMARY OF TECHNIQUE STUDIES

The purpose here is to summarize signal processing requirements as well as the important features of signal processing techniques that have been studied to date and to outline requirements and techniques for future study.

The requirements for technique studies are given in Table 2. In this table requirements 1, 2, 3 and 5 are the same as the requirements under which previous techniques were studied. A more detailed description of these requirements is to be found in the First Cut Signal Processor Report.<sup>(1)</sup> It is proposed that future signal processing techniques be studied under requirements 1, 2, 4, 5 and 6. This set of requirements differs from the first set in two ways. First, requirement 4 is substituted for requirement 3. These two requirements differ only in the variable pulse length part. Requirement 3 specifies that the processor have two switching functions, one switch having the capability of selecting the number of beams to be processed and the other having the capability of selecting one of a number of processor configurations which are designed to handle different pulse lengths. Under requirement 4 these two switching functions are eliminated. Therefore, each signal processing configuration studied under this requirement will only have the capability of processing a given number of beams and a particular signal. The reason for changing this requirement is that the particular combinations of number of beams and pulse lengths that should be designed into the signal processor should be chosen to be consistent with the C/PAS System Concept. Inputs from system studies are needed before these combinations can be selected. Until the time when such inputs are available, signal processing studies will be conducted under requirement 3 but keeping in mind that a requirement similar to requirement 4 may eventually be imposed.

Requirement 4 and 6 are nearly the same except for the application and the fact that the wideband processor is required to process only zero doppler targets while the surface duct processor is required to process targets in the doppler range +50 cps.

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Table 1 illustrates the categories under which technique studies conducted to date and future technique studies will be summarized. Even though a tentative selection of the techniques listed in this table has been made for the First Cut Signal Processor, all of the techniques listed are still considered to be candidates for the Experimental Ship System. The cascaded VICI technique which is described in detail in reference 4 has been eliminated from further consideration because of the large number of delay lines required and the cost relative to the VICI technique which is described in the First Cut Signal Processing Report. The dispersive network or delay line technique was considered for processing a linear FM pulse and has been eliminated from further consideration because of the difficulty of physically realizing large values of dispersion over a relatively small bandwidth. The requirements are prohibitive even for a signal bandwidth of 100 cps and a BT = 5. The requirement is increasingly severe with increase in signal BT product.

Further details of all of the signal processing techniques in Table 2 are given in the appropriate references at the end of this report.

During the period from March to June 1966, the study of signal processing techniques will continue. The techniques which will be studied are discussed in the paragraphs that follow.

<u>N-Bit Correlator</u> - This type of correlator will be studied for the wideband bottom bounce and the surface duct applications. The technique differs from the clipped correlator processor in the following ways: (1) The limiter is replaced by an A/D converter, (2) The time compressed digital words are D/A converted in order to achieve an analog correlation, (3) The storage requirements and the processor dynamic range both increase with increase in the number of bits, (4) The advantage of normalization obtained by hard limiting is lost.

<u>TIMAC</u> - This correlator will be studied for the wideband bottom bounce and surface duct applications. This is a one bit coding scheme that uses delta modulation in place of the polarity sampling done in the clipper correlator. Except for the method of coding it is substantially similar to a clipped correlator. The dynamic range of the device is related to the number of samples used in the correlation

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and the feedback characteristic used in the encoding. This technique appears to have the capability of accomplishing the equivalent of a multibit correlation with a concurrent saving in storage capacity.

<u>Reference Clipped Hetroline Correlator</u> - This technique will be studied for the wideband bottom bounce and surface duct applications. The concept here is that the reference signal be limited and the polarity samples stored in a recirculating memory without time compression. The clipped reference is used to correlate with the received analog signal. The reference storage requirements are considerably reduced in comparison to an analog correlator, but real time operation may still require a prohibitive amount of hardware.

<u>Analog Tapped Delay Line Processors</u> - For both the wideband bottom bounce and surface duct modes, tapped delay line processors are likely candidates for a variety of waveforms. It appears that magnetostructive delay lines probably up to 100 milliseconds are feasible, with reservations concerning dynamic range, spurious, and bandwidth limitations on this type of delay line.

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<u>Other digital processors</u> - To date a single digital processing technique was studied for the narrowband bottom bounce mode. It is intended here to study other digital techniques for this mode of operation as well as studying techniques for the wideband bottom bounce and surfact duct modes.

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13.	Feasibility	Feasible with high confidence (except detector)
12.	Coh/Noncoherent Flexibility	Switch post detection filters
11.	Stage of Development	Can be built with transistors
10.	Critical Components	High dynamic range detector
9.	Cabinets (225 beams)	1 1/2
8.	Cost (225 beams)	175K
7.	Dynamic Range	60 db
6.	Storage Requirement	None
5.	Sample Rate Per Beam	400 cps
4.	Output Signal Format	Time Multiplexed, Analog, Detected
3.	Input Signal Format	N Inputs on N Wires
2.	Requirement and Application	*2 2,5 - WBBB & SD
1.	Technique	Simple Pulse Processor BT = 1 T = 10 ms B = 100 cps

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TABLE 1

SUMMARY OF TECHNIQUE FEASIBILITY STUDY

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1.	Technique	VICI BT = 1, T = $1/2$ sec, B = 2 cps
2.	Requirement & Application	1, NBBB
3.	Input Signal Format	Time multiplexed beams (analog)
4.	Output Signal Format	Time sequence of doppler bins for each beam in sequence (analog)
5.	Sample Rate/Beam	136 cps
6.	Storage Requirement	Two 3676 usec Quartz delay lines
7.	Dynamic Range	60 db
8.	Cost (225 beams)	25 <b>K</b>
9.	Cabinets (225 beams)	1/4
10.	Critical Components	None
11.	Stage of Development	Applicable transistor hardware experience
12.	Coh/Noncoherent Flexibility	Not easily adaptable (needs further study)
13,	Feasibility	Feasible with high confidence
14.	Advantages	Cost, size, established technique
15.	Disadvantages	High output bandwidth

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TABLE 1 (CONT.)

SUMMARY OF TECHNIQUE FEASIBILITY STUDY

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1.	Technique	Digital Doppler Processor BT = 1, T = $1/2$ sec, B = 2 cps
2.	Requirement & Application	1, NBBB
3.	Input Signal Format	Time multiplexed beams (analog)
4.	Output Signal Format	Time sequence of doppler bins for each beam in sequence (digital)
5.	Sample Rate/Beam	I & Q channels 100 cps per channel
6.	Storage Requirement	271,000 bit magnetic core memory or 24 - 10 ms delay lines
7.	Dynamic Range	36 db (6 bit encoder)
8.	Cost (225 beams)	35К
9.	Cabinets (225 beams)	1/2
10.	Critical components	None
11.	Stage of Development	No hardware - concept verified by digital simulation.
12.	Coh/Noncoherent flexibility	Provisions are easily made
13.	Feasibility	Feasible - commerciably available components for required data rates.
14.	Advantages	Digital output, design flexibility, eventual implementation in micro- circuits
15.	Disadvantages	Cost & size, range and doppler splitting losses

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TABLE 1 (CONT.)

SUMMARY OF TECHNIQUES FEASIBILITY STUDY

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1.	Technique	Clipper correlator BT = 8, T = 80 ms, B = 100 cps	
2.	Requirement & Application	2,5 WBBB and SD	
3.	Input Signal Format	Time multiplexed clipped beam inputs	
4.	Output Signal Format	Time sequence of correlation values for each beam in sequence	
5.	Sample Rate/Beam	200 срв	
6.	Storage Requirement	Two 500 µsec delay lines one 120 stage shift register	
7.	Dynamic Range		
8.	Cost (225 beams)	15K	
9.	Cabinets (225 beams)	1/4	
10.	Critical Components	None	
11.	Stage of Development	Applicable experience with SQS-26 correlator	
12.	Coh/Noncoherent Flexibility		
13.	Feasibility	Feasible with high confidence	
14.	Advantages	Cost & Size - normalized output, flexible with regard to signal coding	
15.	Disadvantages	Distortion due to limiting, output format requires demultiplexing	

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TABLE 1 (CONT)

SUMMARY OF TECHNIQUE FEASIBILITY STUDY

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1.	Technique	Scanned Filter BT = 1, T = $1/2$ , B = 2 cps
2.	Requirement & Application	1, NBBB
3.	Input Signal Format	Time multiplexed beams (analog)
4.	Output Signal Format	Time sequence of doppler bins for each beam in sequence (analog)
5.	Sample Rate/Beam	300 cps
6.	Storage Requirement	589,824 bit magnetic core memory
7.	Dynamic Range	48 db (8 bit encoder)
8.	Cost (225 beams)	125K
9.	Cabinets (225 beams)	2 1/2
10.	Critical Components	D/A Converter (8 bit, 7.66 Mc)
11.	Stage of Development	Applicable transistor hardware experience
12.	Coh/Noncoherent Flexibility	Switch predection filter
13.	Feasibility	Feasible with high confidence (D/A converter is a development item)
14.	Advantages	Easily adopted to shorter pulses, High dynamic range, Flexible memory
15.	Disadvantages	Requires A/D & D/A converters. cost and size range & frequency splitting losses.

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TABLE 1 (CONT.)

SUMMARY OF TECHNIQUE FEASIBILITY STUDY

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TABLE 2

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REQUIREMENT FOR C/PASS SIGNAL PROCESSING TECHNIQUE STUDIES

quirement Number	Requirement Application	+ 24	Type of Pulse	Pulse Length (T)	Bend- Width (B)	BT Product	Doppler Freq. Range	# Doppler Bins	Dynamic* Range	Coments
l	Marrow Band Bottom Bounce	225 Nominal 100-1000	5	1/2 sec nom 1/4 to 1 sec		г	100 cps	20	48-60 đb	Same as lst cut
2	Wide Band Bottom Bounce	225 Nominal 100-1000	CM	10 ms 5-100 ms	ᆌ	1	16-	ı	48-60 đb	Same as lst cut
3.	Wide Band Bottom Bounce	225 100-1000	NAT	Variable	100 cps	Variable 100 cps	100 cps	ı		Same as lst cut
4	Wide Band Bottom Bounce	225 100-1000	LFM or 100 ms Quadratic 10 ms - Phase Code 1/2 sec		100 cps 50-200 cps	5-50**	д	T	48-60 đb	
5.	Surface Duct	200 100-1000	B	10 ms 5-100 ms		ı	100 cps	100 cps No. Doppler Processing	48-60th	Same as Ist cut
6.	Surface Duct	200 100-1000	LFM or 100 ms Quadratic 10 ms- Phase Code 1/2 sec		100 cps 50- 200 cps	5-50**	100 cps		48-60 đb	

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NOTES: \* A dynamic range goal in the 48-60 db range appears desirable. However, techniques with lower dynamic range

should not be omitted from consideration on the basis of dynamic range alone.

\*\* This Requirement restricts the range of combinations of B and T

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#### SECTION III

#### SUMMARY OF CRITICAL COMPONENTS

As a result of the technique studies to date, a number of the more important critical components that might be required in the final C/PASS signal processing equipment have been identified. For the most part specifications on these parts are such that near state-of-the-art design techniques or hardware are required for their implementation. As such, more detailed study and/or laboratory breadboarding is required to increase confidence in feasibility.

A brief description of each of the critical components is given below, with recommendations for further work.

1

The Adaptive Reverberation Filter - As described in the First Cut Signal Processing report, this filter is a relatively sophisticated part of the Narrowband Bottom Bounce Processor. It presently appears desirable that this notch be capable of automatically adjusting its notch depth and center frequency as a function of reverberation amplitude and center frequency. In the present signal processing concept one reverberation notch is required in each beam channel. Cost and size estimates reveal that this single item is a major contribution to both the cost and size of the Narrowband Bottom Bounce Processor. In addition, it is felt that realistic performance predictions of such a filter can best be obtained using sea tapes and either a laboratory breadboard or a digital simulation of the filter. It is therefore recommended that a design study of this filter be initiated, and that a breadboard model using microminiature circuits wherever possible be constructed and tested in the laboratory.

<u>High Dynamic Range Envelope Detector</u> - A 60 db dynamic range design goal was established for the simple pulse processors to be used in both the Surface Duct and Wideband Bottom Bounce Modes. This requirement does not appear to be critical for any of the components except the envelope detector. Such a dynamic range even for the relatively narrow 100 cps signal bandwidth is near state-of-the-art. Since such a detector is needed for every beam in both wideband and surface duct modes it is not only desirable to obtain the best possible performance, but the

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design must be such that size, cost and power concumption are minimized. It is therefore recommended that laboratory work on improving the state-of-the-art of such a detector be continued.

Auto Gate High Power Amplifier - The preamplifier - delay line - post amplifier circuitry in the autogate for both the VICI and Scanned Filter processors will ultimately limit the dynamic range capability of this device. A 60 db dynamic range design goal on this device represents a near state-of-the-art or beyond state-of-the-art requirement for the VICI application. The requirement is perhaps more easily met for the scanned filter application since the bandwidth is somewhat lower. The dynamic range that can be achieved in this device is directly related to how hard the preamplifier can drive the delay line. It is estimated that to insure a 60 db dynamic range it is necessary that the preamplifier be designed to produce 70 volts into a 500% load over a 3 Mc video bandwidth. It is recommended that the required amplifier be designed, built, and tested.

D/A Converter for the Scanned Filter - The D/A converter for the Scanned Filter Processor described in the First Cut Signal Processing Report is required to make an 8 bit conversion at a 6.75 Mc rate. This represents a near state-of-the-art requirement and is the most critical component in the scanned filter processor. A D/A converter for a similar processor is presently being developed in house for the Naval Research Laboratory under Contract Nonr 4903-(00)X. The design goal for this D/A converter is to convert a 10 bit digital word at a 5 Mc rate. A paper design for this converter which utilizes integrated circuitry for the timing functions is completed and parts are on order. The present schedule calls for a completed product by August 1966. It is our intention to keep abreast of the progress on this development.

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#### SECTION IV

#### SUMMARY OF COST STUDIES

The cost study was conducted in order to show how the cost and size of processors described in The First Cut Signal Processing report<sup>(1)</sup> vary as a function of the number of beams to be processed, signal bandwidth, and signal BT product. The study serves several important functions. It establishes the order of magnitude of the signal processing problem for the C/PASS application and shows the important contributors to size and cost within the signal processing subsystem itself. Furthermore, cost and size versus number of beams and signal bandwidth provides an important input to system cost effectiveness trade-off studies.

Estimates of numbers of circuit boards, filters, power supplies and other components were made in order to calculate cost and number of cabinets required. The cost figures and number of cabinets were calculated on the basis of "good commercial practice" utilizing transistor design techniques. Very little consideration was given to integrated or microminiature circuits. The costs are for materials only, and do not include costs for development and design or for system testing.

The general procedure for cost estimating was to first examine each of the blocks of a functional block diagram in order to decide the make or buy question. Outside vendor items were costed using previous quotes on similar items as well as catalogue information. For those items which would be built in house, the functional blocks were broken down to  $2" \times 4"$  circuit board level. An estimate of the number of such circuit boards for each function was then made. It was assumed that the cost for parts plus the time required to assemble and test an average  $2" \times 4"$  circuit board would be \$100.

The sketch in Figure 1 illustrates a typical cabinet layout. The cabinet described has a frame 24" wide by 24" deep by 72" high. It has three drawers which contain the 2" x 4" circuit boards, power supplies and a blower. For the circuits built in house a packing density of 1500 2" x 4" circuit boards was assumed. Volume occupied by outside vendor items such as delay lines and magnetic core memories was estimated from previous quotes on similar items and catalogue information.

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The ranges of variation selected for number of beams & signal bandwidth are as shown below:

Processor	Number of Beams	Signal Bandwidth
Narrowband processor	100 to 1000	l cps to 4 cps
Wideband processor	100 to 1000	50 cps to 200 cps
Surface Duct Processor	100 to 1000	50 cps to 200 cps

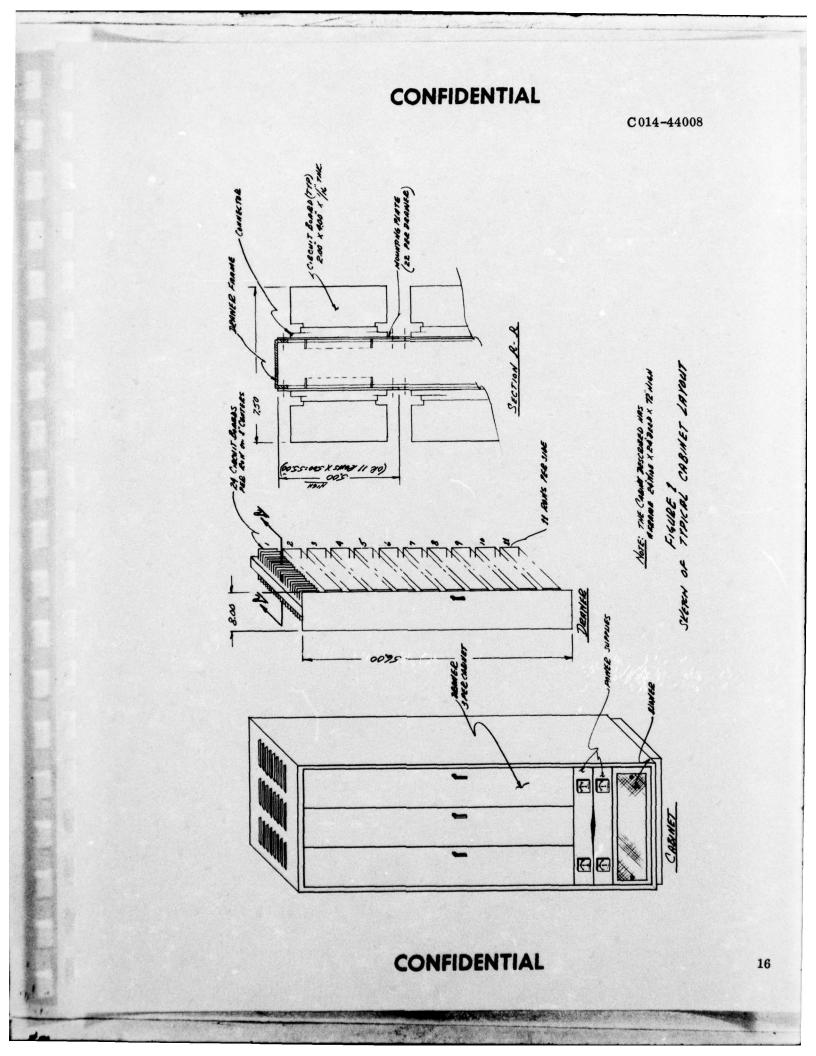
It is assumed that within the range of variations shown that the component cost does not change as a function of the number of identical components required.

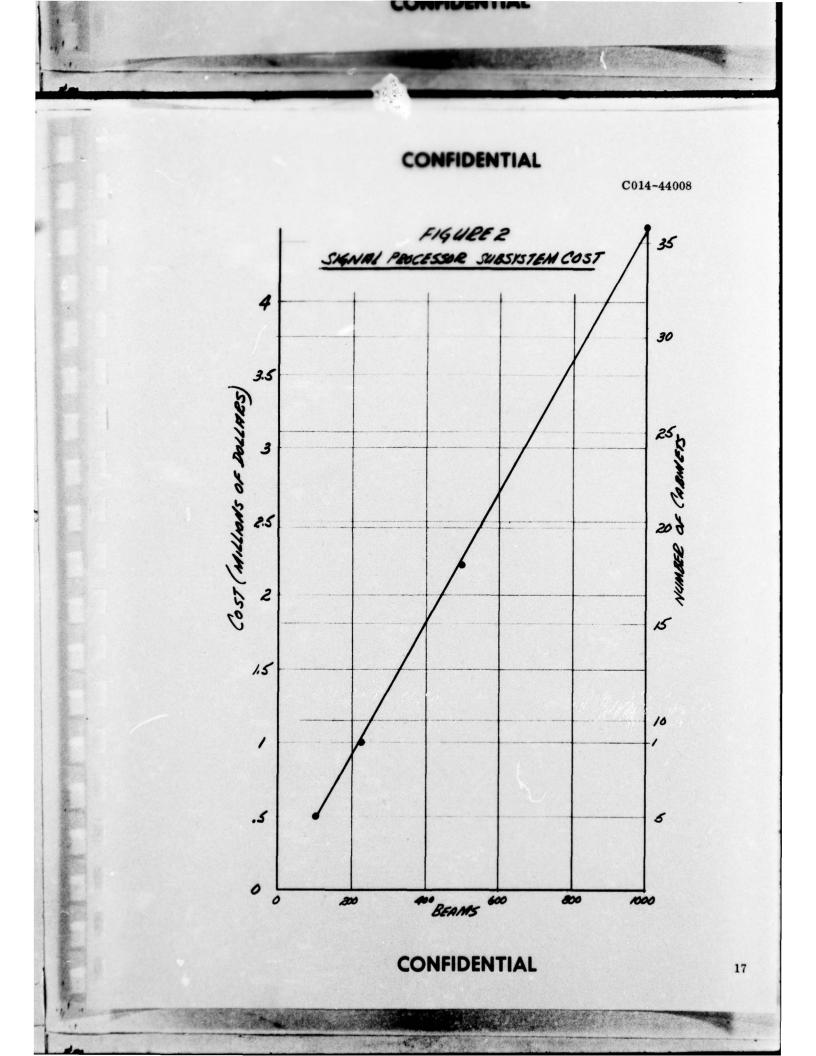
Since both the number of components and the cost per component can only be approximated at this time, the total cost and size figures are at best order of magnitude estimates. However, the relative cost and size as a function of signal bandwidth and number of beams should be more accurate.

Table 3 summarizes signal processor subsystem cost. The center column in this table represents cost for the First Cut Signal Processor for a narrowband bottom bounce pulse width of 1/2 sec, and wideband bottom bounce and surface duct signal bandwidth equal to 100 cps. The column on the left represents similar processor cost except that the narrowband pulse width is 1/4 sec, and the wideband and surface duct bandwidth is 50 cps. The third column is for a narrowband pulse width of 1 sec, and wideband and surface duct bandwidth of 200 cps. As shown in this table the total signal processor cost does not vary appreciably for change in signal parameters.

The table also serves to show that the predominant costs are in the narrowband preprocessor and the simple pulse processor.

Figure 2 shows the First Cut Signal Processor costs as a function of number of beams, all other parameters of the First Cut Processor being constant.





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225 Beams	<sup>1</sup> / <sub>↓</sub> sec width WB -	lse Length WB Band- 50 cps BT = 8 ndwidth cps	$\frac{-1}{2} \sec \theta$ width BT = 8	ndwidth	NB Pulse Length/Sec WB Bandwidth 200 cps WB BT = 8 SD Bandwidth = 200 cps	
	Cost	Cabinets	Cost	Cabients	Cost	Cabinets
NB Preprocessor	\$450K	3	\$450K	3	\$450K	3
Scanned Filter & Auto Gate	90K	2 <sup>1</sup> / <sub>2</sub>	125 <b>K</b>	2 <sup>1</sup> / <sub>2</sub>	180K	2 <sup>1</sup> / <sub>2</sub>
Wideband Mode Selector	200 <b>K</b>	<u>1</u> 2	100K	1 2	100K	1/2
Wideband Clipper Correlator	12K	1	16 <b>K</b>	1 4	25K	1/2
Wideband Simple Pulse Processor	110K	1	llok	l	llok	1
Surface Duct SP Processor	180K	11/2	180 <b>K</b>	1 <u>1</u> 2	180K	1 <u>1</u> 2
TOTAL	942 <b>K</b>	8.75	981 <b>K</b>	8.75	1,045K	9

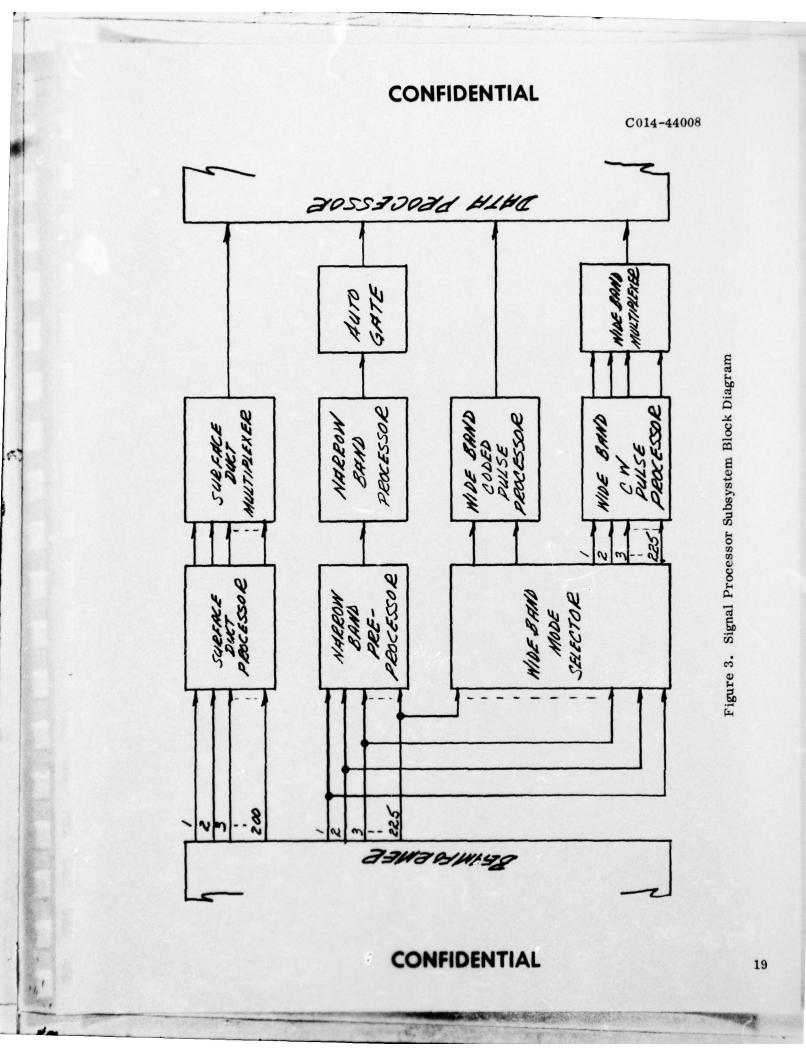
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## TABLE 3

SIGNAL PROCESSOR SUBSYSTEM COST

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#### SECTION V

## THE SURFACE DUCT PROCESSOR

A block diagram of the surface duct processor is shown in Figure 5. The 200 parrallel channel simple pulse processor shown corresponds to the system requirement assumed for the First Cut Signal Processor. It is assumed for costing purposes that this same configuration would be used for any combination of signal bandwidth within the range of 50 to 200 cps and number of beams in the range 100 to 1000. The First Cut Processor was designed for a 10 ms pulse and a sampling rate per beam of 400 cps was chosen as being adequate. In order to process 200 beams the time multiplexers in this case must operate at a 400 x 200 = 80 Kc rate which is well within the state-of-the-art and within the maximum data rate which is acceptable to the data processor. For the worst case situation of a 5 millisecond pulse and 1000 beams and a sampling rate of 800 cps per beam, the output data rate for this processor will be 800 x 1000 = 800 Kc. This data rate, although within the state-of-the-art is probably too high to be acceptable to the data processor. Therefore, if a processor were to be built for this case an implementation using four identical processors each capable of processing 250 beams would probably be used. However, the multiplexer cost also varies as a function of the number of beams, therefore the material costs would not be affected appreciably by this kind of implementation change.

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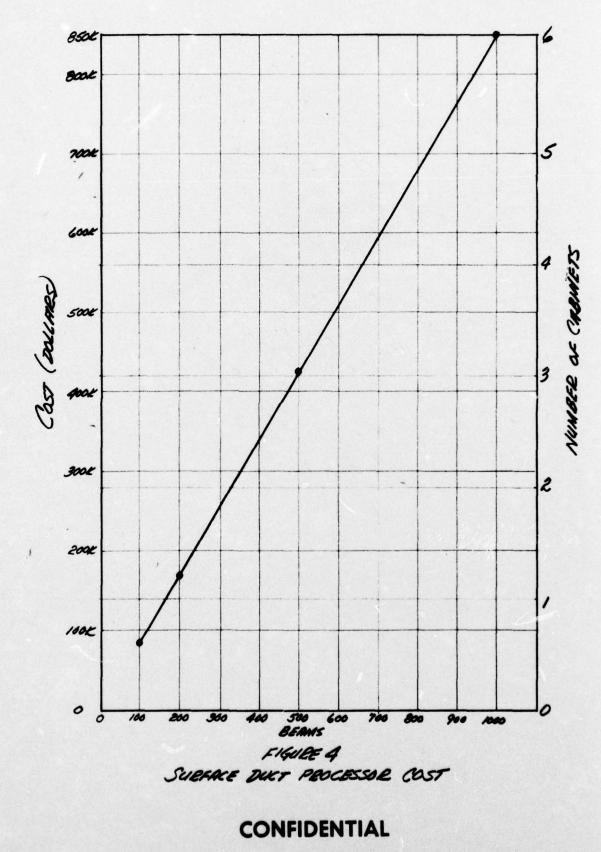
For a particular number of beams within the 100 - 1000 range the processor material cost is not affected by a change in bandwidth from 50 cps to 200 cps.

Table 4 shows the cost estimate and number of cabinets as a function of number of beams for each of the blocks in Figure 5. The data presented in Table 4 was used to plot Figure 4 which shows cost and number of cabinets as a function of the number of beams to be processed.

Costs for this processor were based on the assumption that most of the equipment would be built in house. The total cost figures are therefore strongly influenced by the assumption that an average circuit board which would comprise one filter (for instance) would cost about \$100 for materials, assembly and test.

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BERNES	BEAMS FILTER	766	OVER	TER	ENVE	SOL	-07	PASS	OVERLOAD ENVELOPE LO-PASS TOTAL CHOINETS TOTAL	CHON	YERS	707AL
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00/	300	30K	100 1/04	1/05	200	ZOK	00/	ZOL	200 20K 100 410K 700 42K	42K	1/2	AZL
200	600 60K	60K	800	ZOK	400	AOK	200	ZOK	000%	4.18		141K
500	1500	isok	200	SOL	000/	1000 100K	500	Sok	500 50K 3500 10.3K	10.3K	21/2 3435	360.35
1000	3000	Jook	1000	yant	2000	EDOK	0001	YOOK	100K 2000 200K 1000 100K 7000 20.6K	20.65	μ	7072

TIME MULTIPLIZER COST

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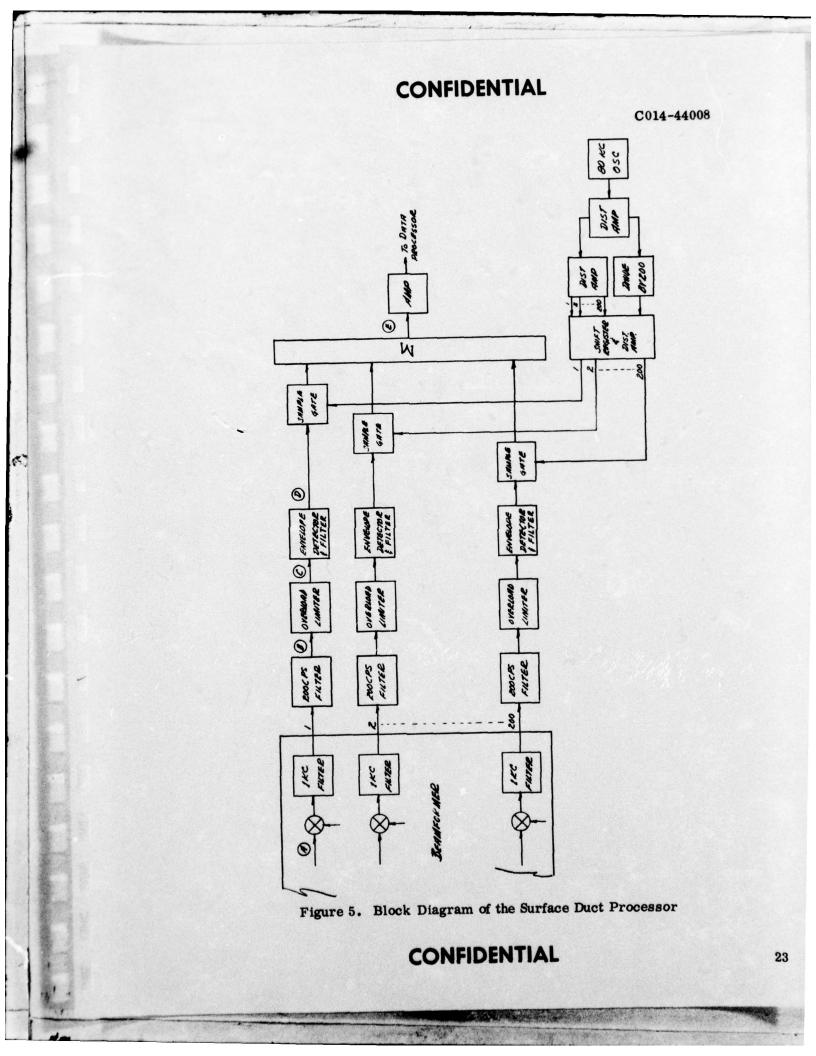
REAK THOMAGE	The	K	Kare	Y		CILLINED DOWE	DOWER	166	707.92		CRBINETS TOTAL	78101
Participa		**				~~~			00000	1.3		cas/
NUMBER	dates cho	COST	<b>ZMADS</b>	Cast	RIMAS	rest	<b>ZAMES</b>	ast 1	<b>MUDE</b>	Cast A	ANASC .	F CAR.
		1.00					·	1.00	~	1		
`	0	1.36	-	00/	`	8	,	100/	~		1	
01	9	1.3K	01	×	N	800		100	61	1	1	1
00/	Ņ	2.8K	00/	10K	9	600	-	100/	122	. +6	1/8	13.9¢
200	27	475K	-	æ	11	1.1%	~	00/	239	.8K	-	26,352
200	53	IK	500	SOK	27	2.7%	`	100	593	2.0K	2	65.8K
1000	123	20.5K	1000	100K	52	s.er	`	100	1176	418	1	129.754

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JURFACE DUET PROCESSOR CAST

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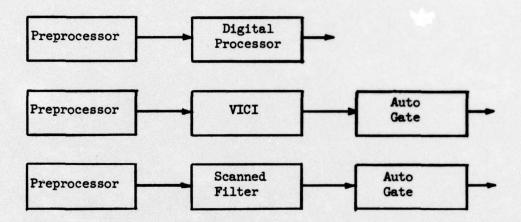
#### SECTION VI

#### THE NARROW BAND PROCESSOR

## A. INTRODUCTION

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Three Narrowband Processors were considered in the First Cut Signal Processing report. The major components of each is shown in the sketch below



Even though there are minor functional differences in the preprocessors for the three cases shown, the costs for any particular combination of pulse length and number of beams in the ranges considered are nearly the same. Therefore, for costing purposes the scanned filter preprocessor was costed in detail and the same cost figures were used for the other two preprocessors.

In all cases the general procedure for costing was to select particular combinations of number of beams and pulse width and to decide on system configurations for each of the combinations. The case of the digital VICI illustrates the procedure. Here pulse lengths of 1/4, 1/2 and 1 second and numbers of beams of 125, 250, 500 and 1000 were chosen in order to define twelve system configurations. For each system a judgement was made concerning whether to make a particular part more complex with increase in number of beams and/or pulse length or to split the function into two less complex parts.

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#### B. THE NARROWBAND PREPROCESSOR

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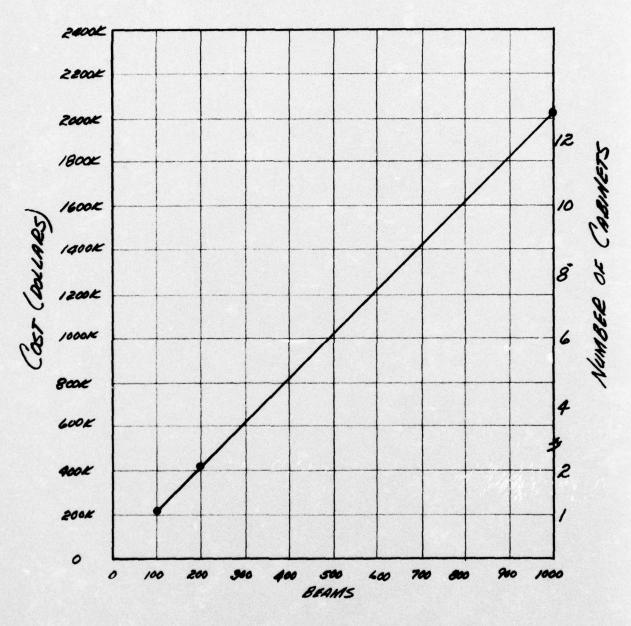
A block diagram of the preprocessor for the Scanned Filter is shown in Figure 7. The 225 channel case shown corresponds to the system requirement assumed for the First Cut Signal Processor. The requirements on individual components of the preprocessor do not change appreciably with change of signal pulse length in the range 1/4 to 1 sec. consequently the cost figures are independent of pulse length. The input filter, reverberation notch, range gate and sampling gate requirements are independent of the number of beams. However, the bandwidth of the gate generating circuitry and the multiplexer output bandwidth increases with increase in number of beams, therefore, in actual implementation a judgement would be required to determine for any particular application whether a single high bandwidth multiplexer or two or more lower bandwidth multiplexers should be used. It was assumed that this judgement would result in two or more multiplexers of the same or lower bandwidth as that required for the First Cut configuration. Therefore, number of components for the multiplexing and gate generating circuitry were assumed to vary linearly with number of beams. Since component costs were considered to be independent of number of identical components, the preprocessor costs are a linear function of the number of beams.

Table 5 summarizes the cost and number of cabinet estimates for each of the blocks in Figure 7. The data in Table 5 was used to plot Figure 6 which shows cost and number of cabinets as a function of number of beams to be processed.

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FIGUBE 6

SCANNED FILTER PRE PROCESSOR

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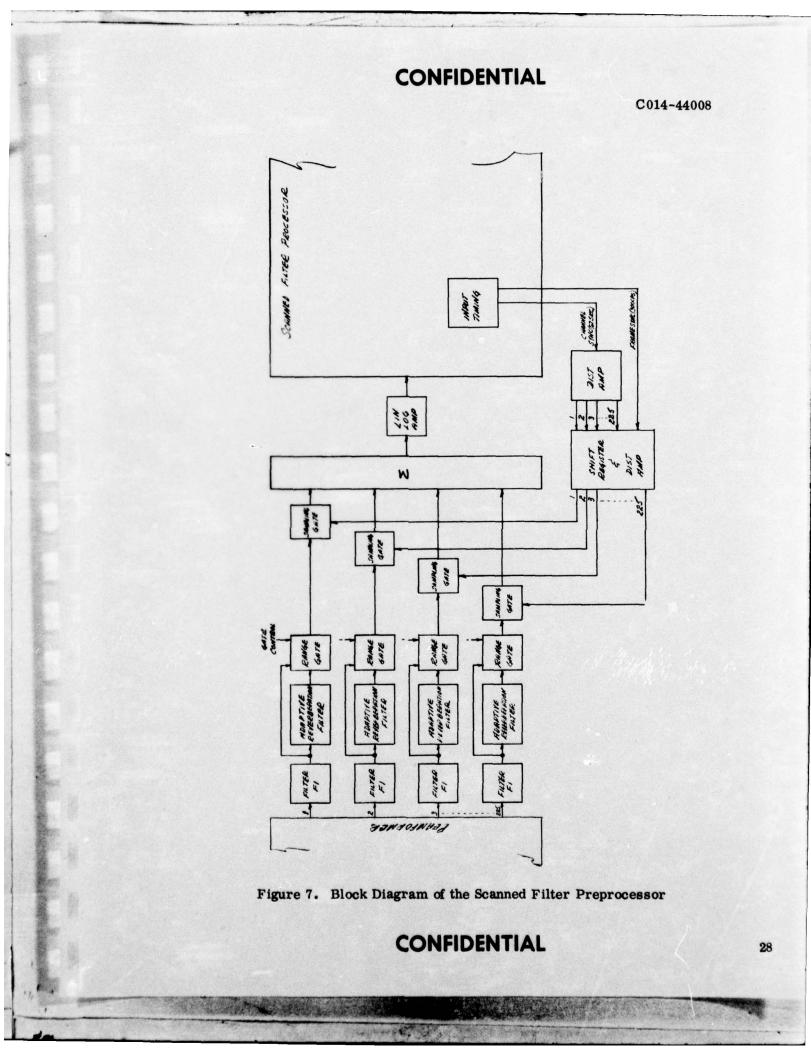
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# SCANNED FILTER PREPERESSOR

CON	IFI	DENTIAL
Park Cast	I CAN'S	#208.4K
SUMMER BANGE & DOG AMP. DUR CABINETS COST	7 NUME	40 2021 4,94 14 20814 300 2038 10.24 21/2 44.94 300 20128 51.34 121/2 2077
CAB	CAST	75'75 76'75 76'75
TOTAL	T IBINGED	202/ 20128 20138
AMP	1200	905 305 305
507	T BURENS COSI	~ ~ ~
LE É CATE	COST	10K 20K
SAMP	- Buens Cosi	600 100 1.1K 200 5.2K 1000
MER	Casr	12:5 111 111
Sum	BINEDS	sz 52
FILTER REACTIVE	asr	<b>2.8</b> 200 201 1700 1704 6 600 100 101 1352 400 402 3400 3402 11 112 200 2012 2032 2002 2002 17000 1.701 52 5.22 1000 1002
RUM	RINK	100 15 <b>28</b> 200 201 1700 200 27 1354 400 406 3400 1000 123 2332 200 2004 1700
160	cast bu	3012 704 702
FIL	BUNDE	200 400 2000
	COST	2.8K 175K 125K
BEANS TIMING	ANADIS	15 15
BEANS	Aintee	002 002
CON	IFII	DENTIAL

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#### C. THE SCANNED FILTER AND AUTOGATE

The Scanned Filter and Auto Gate block diagrams for the 225 beam, 1/2 sec pulse requirement are shown in Figures 9 and 10. Twelve different Scanned Filter and Auto Gate processor configurations were studied in order to calculate costs. In general the designs of individual functions in these block diagrams were not appreciably changed with changes in number of beams and pulse length. Instead the number of identical functions required increases.

Tables 6 and 7 summarize the cost estimates made for the twelve scanned filter configurations studied and the Auto Gate. As can be seen from these tables the largest single cost item is the Magnetic Core memory.

The memory price for each configuration was costed on the basis of costs shown in the table below.

Memory Capacity	Cost/bit	Total Cost
2048 bits	\$.24/bit	\$ 35K
4096 bits	\$.18/bit	\$ 52K
8192 bits	\$.15/bit	\$ 87K
16384 bits	\$.12/bit	\$140K

In order to facilitate presentation of the memory cost in Table 6 the total memory cost figures were broken up into \$5,000 units. The number of memory units required for each configuration was then inserted in the Table.

Figure 8 shows a plot of Scanned Filter costs as a function of number of beams for the three pulse widths considered.

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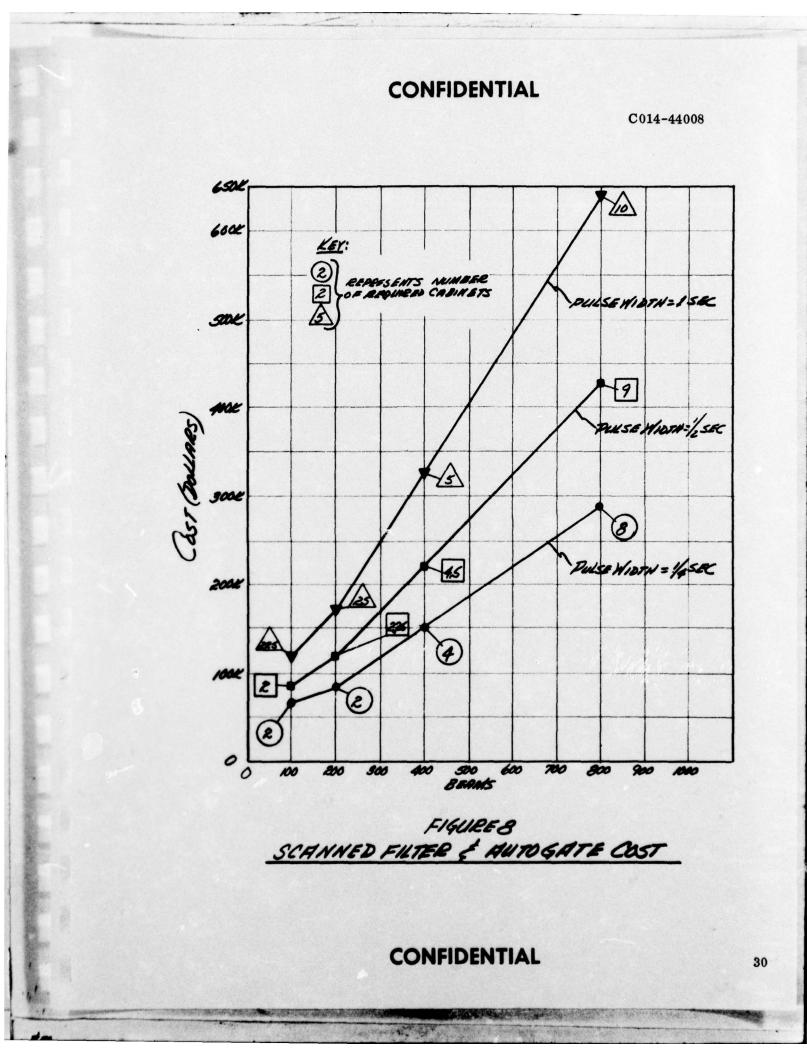


TABLE 6

SCANNED FILTER & AUTO GATE COST

						NUMBER	OF P	NUMBER OF MODULES REQ.	REQ.					COST
	No. Beams		100	Γ		200	Γ		100	Γ		800		PER
	Pulse Length (Sec)	1/1	1/2	-	1/1	1/2	-	1/1	1/2	-	1/4	1/2	-	
+	Analog Sample and Hold Analog/Digital Converter Temporary Data Storage Buffer Registers Partial Memory Word Selection Gates	, r	1	F I	-	1	н	~	N	N	ŧ	4	4	4.00K 7.00K 0.72K 2.16K
5. 5. 6. 7. 10. 11. 12. 12. 12. 12. 12. 12. 12. 12. 12	Imput Timing Load Address Buffer Registers Load Address Generator Load/Unload Address Selection Gates Load/Unload System Control Unload Address Generator Load/Unload Timing System Clock Generator	1	1	F	г	1	н	1	1	н	I	F	T I	1.08K 1.35K 3.60K 0.54K 1.08K 1.80K 1.80K
13.	Memory Register	7	10	71	P	17	28	21	35	56	42	70	211	5.00K
14. 15.	Output Memory Word Conversion Digital/Analog Converter	l	ı	1	1	1	ı	2	8	2	4	ŧ	•	1.44K 3.00K
16. 17. 19. 29. 21. 23. 24.	Signal Spectrum Bandpass Filter Video Drive Amplifier Balanced Mixer Marrow Bandpass Pre-Detection IF Filter IF Amplifier Linear Envelope Detector Linear Envelope Detector Low Pass Post-Detection Filter Peak Detection and Hold Circuit Oscillator Drive Amplifier	1	ı	1	ı	ı	Г	8	N	N	æ	÷	4	0.20K 0.10K 0.25K 0.20K 0.40K 0.20K 0.20K 0.25K
25. 26. 27.	Voltage Controlled Step Scan Osciliator Digital Step Scan Generator Filter Delay Compensation	1	1	1	1	1	1	1	ı	1	ı	I	I	0.50K 0.90K
28.	Auto Gate	1	1	1	ı	1	1	2	2	2	4	#	ŧ	3.00%

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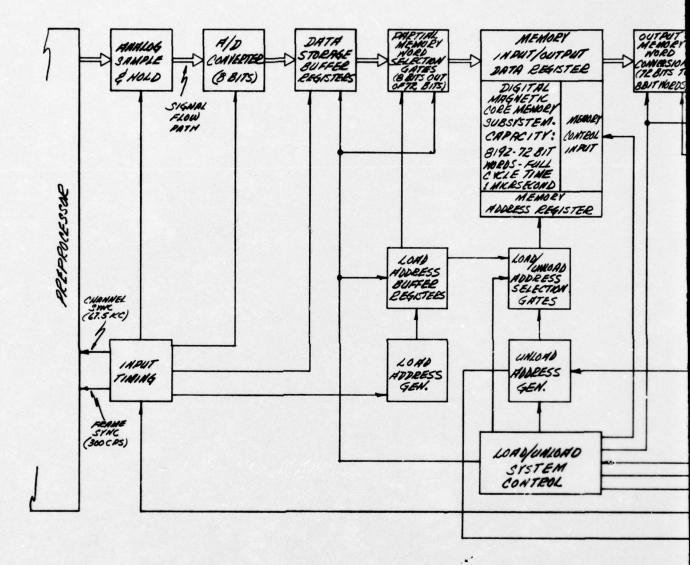
Tapped Delay Line	\$1,000
Delay Line & Associated Circuits	1,300
Distribution Amplifier	300
Gain Controlled Amplifier	300
Comparator	300
Summer	200
Gate Generator	200
Gate	100 \$3,700

TABLE 7

AUTO GATE COST

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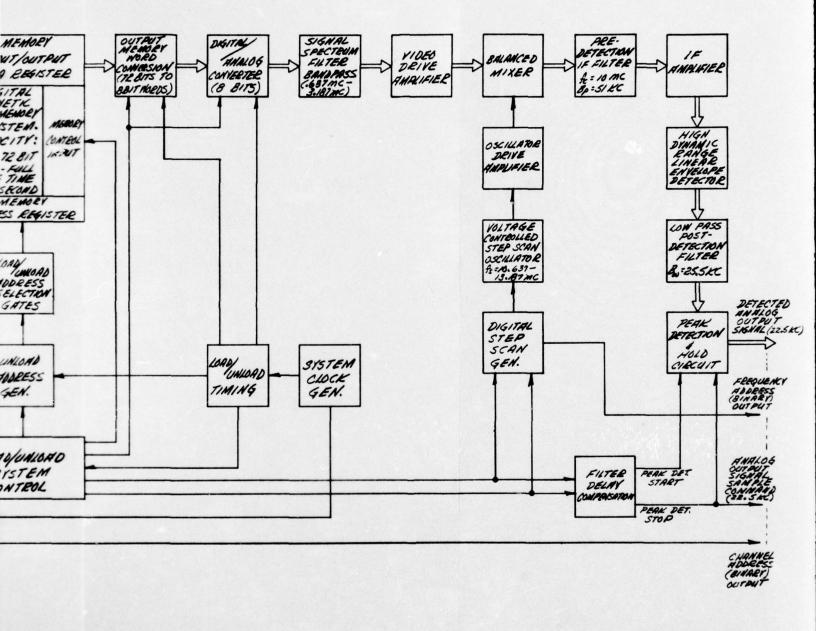
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Figure 9. Detailed Block Diagram of the Scanned Filter

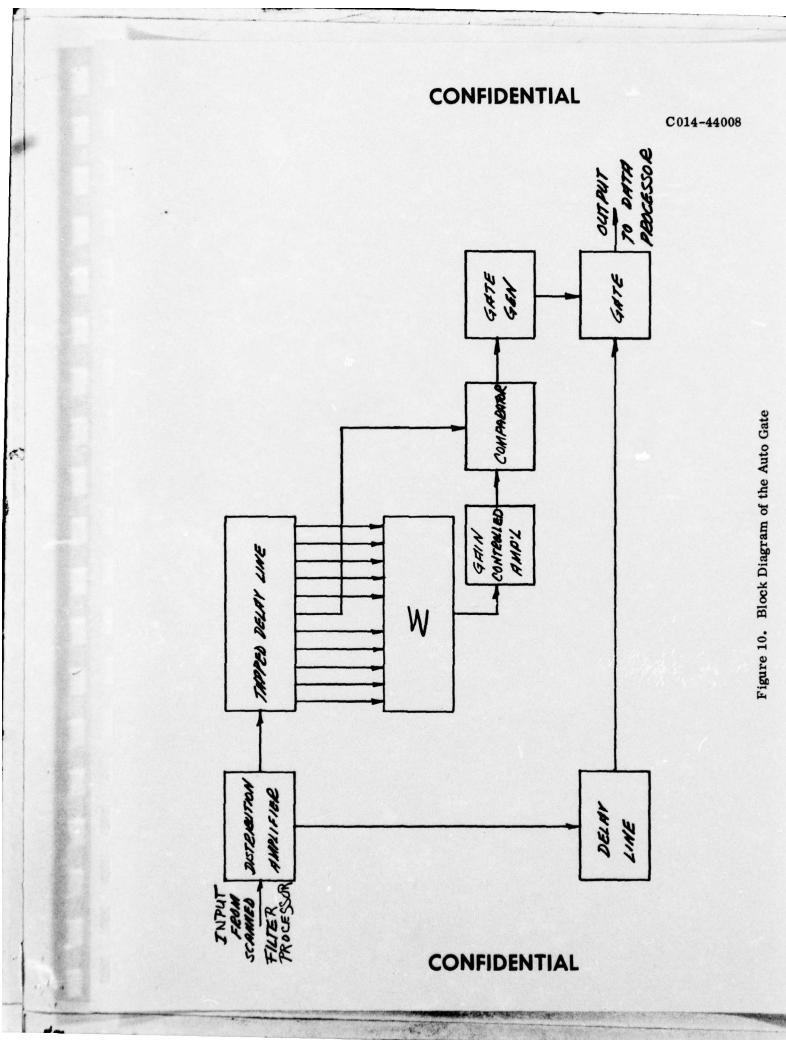
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#### D. THE VICI PROCESSOR AND AUTO GATE

A block diagram of the VICI processor is shown in Figure 13. This same configuration would be used for any combination of pulse length within the range 1/4to 1 sec and number of beams in the range 100 to 1000. However, in cases where a given combination of pulse length and number of beams is beyond the capabilities of a single VICI, two or more VICI's are required in parallel.

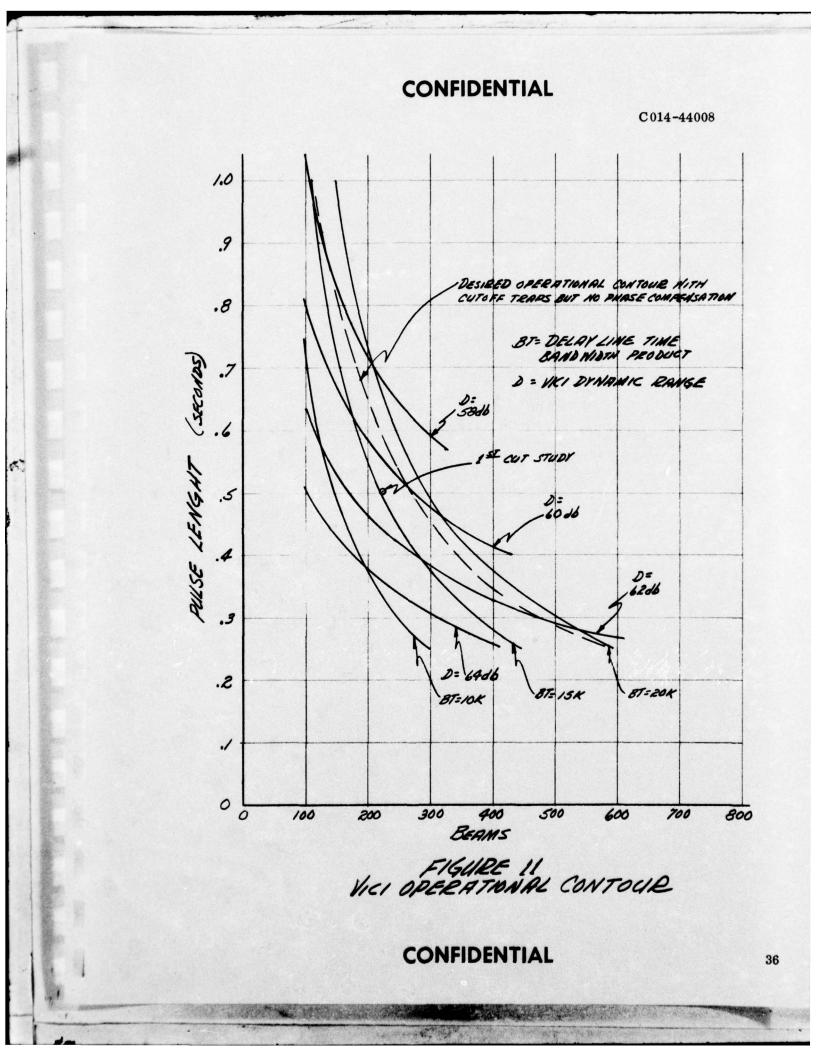
Figure 11 shows the trade-off that must be considered in choosing a VICI for a particular pulse length and number of beams. A point on this curve represents the desired operating point in terms of pulse length and number of beams. The lines of constant BT product show the time-bandwidth requirement on the VICI delay line and the lines of constant dynamic range shows the performance to be expected from the processor. The dashed line represents the desired operation contour.

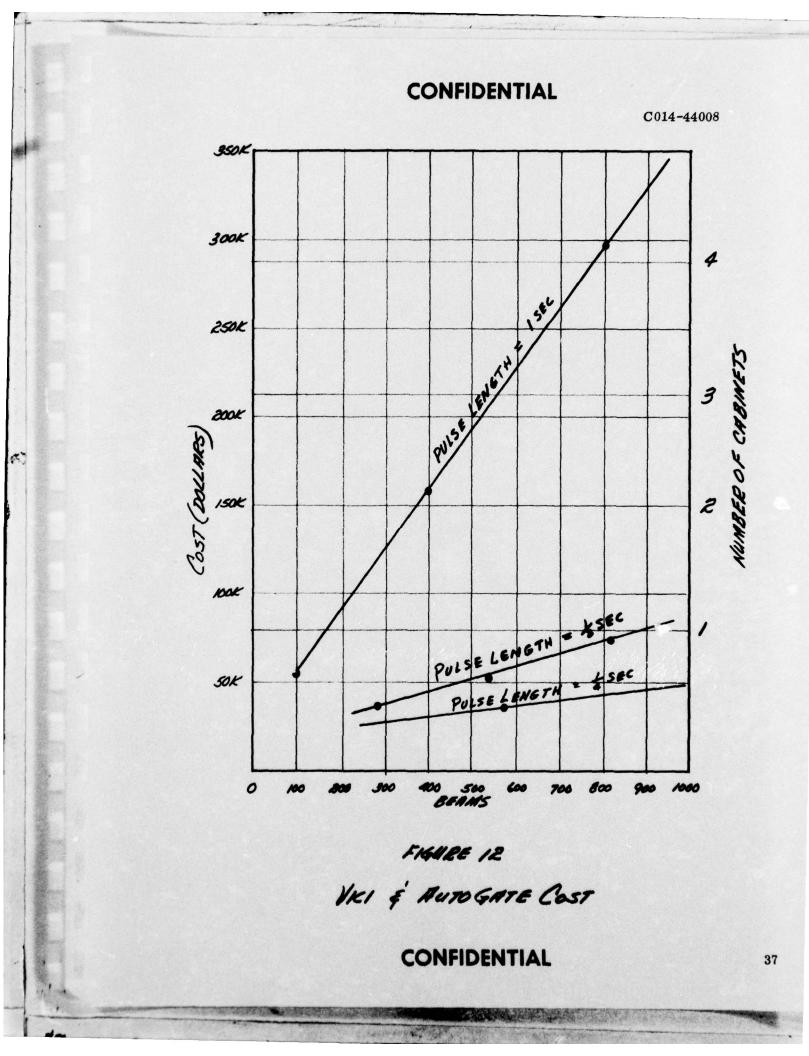
If we were to choose an operating point to the right of the dashed line, the time bandwidth requirement for the delay line begins to get excessive, such that design problems increase very rapidly. In fact BT products in the range 20 to 25 are pushing the quartz delay line state-of-the-art. Therefore an operating point too far to the right of the operational contour represents a requirement that is beyond the state-of-the-art for a single VICI. If we pick an operating point to the left of the dashed curve the VICI design problems become less severe. However, an operating point too far to the left indicated that the full capacity of the VICI is not being used.

Table 8 shows the cost break down for a single VICI. This table used in conjunction with Figure 11 to determine the number of VICI's required for a particular pulse width allows one to calculate cost versus number of beams. In order to estimate number of cabinets it was assumed that four VICI processors can be packaged in a single cabinet.

Figure 12 shows a plot of the resulting cost and number of cabinets as a function of number of beams for several pulse lenghts.

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(2)	Delay Lines	\$7,000
(2)	Delay Line Drivers	400
(2)	Post Delay Amplifiers	200
	Upshifter & L.O.	1,200
	Downshifter & L.O.	1,200
	AGC Control	1,500
	f <sub>s</sub> Gen. & Phase Det.	1,500
	Variable Gain	100
	T.P. Gain & Summer	200
*	Cabinet, Power Supplies & Misc.	1,000 \$14,300

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TABLE 8 VICI COST

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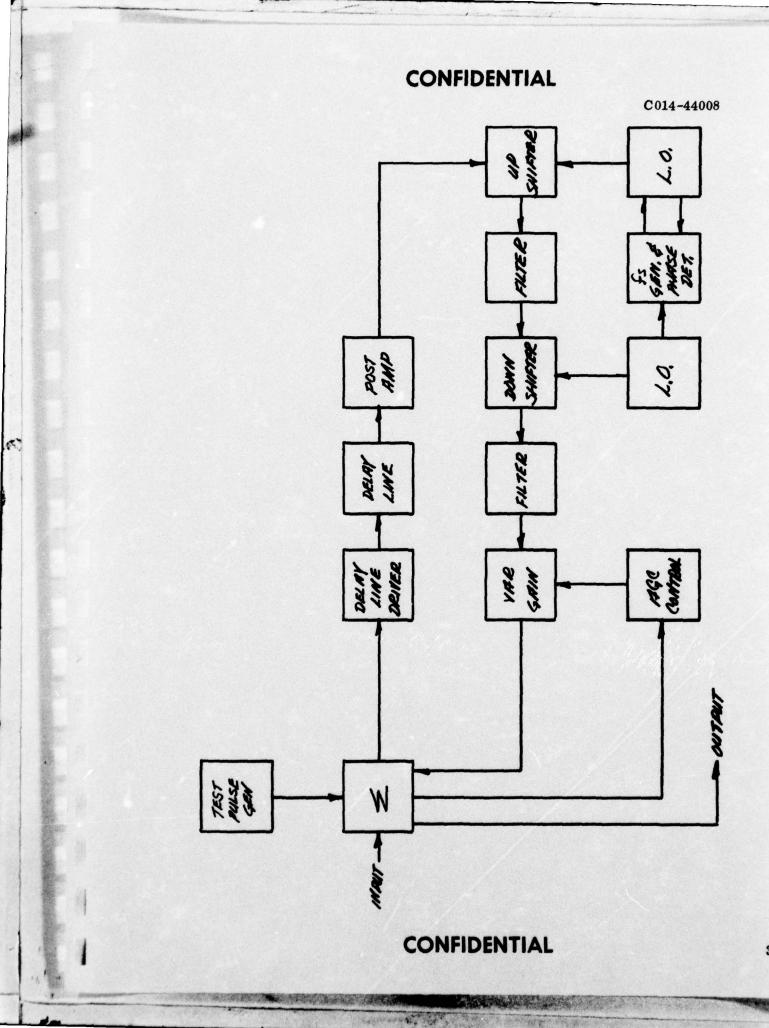


Figure 13. VICI Block Diagram

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#### E. THE DIGITAL DOPPLER PROCESSOR

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The basic Digital Doppler Processor costed here is described in a memo entitled "Application of a Digital Signal Processor to the Planar Array Sonar".<sup>(5)</sup> A block diagram for the 225 beam, 1/2 sec pulse requirement is shown in Figure 15.

As described in the introduction to this Section, twelve different configurations covering the desired ranges of pulse length and number of beams were studied in order to estimate cost and number of cabinets required.

Table 9 shows a cost break down referenced to the block diagram in Figure 15.

Table 10 shows some of the important system parameters for each of the configurations costed.

A plot of cost and number of cabinets as a function of number of beams for several pulse lengths is given in Figure 14.

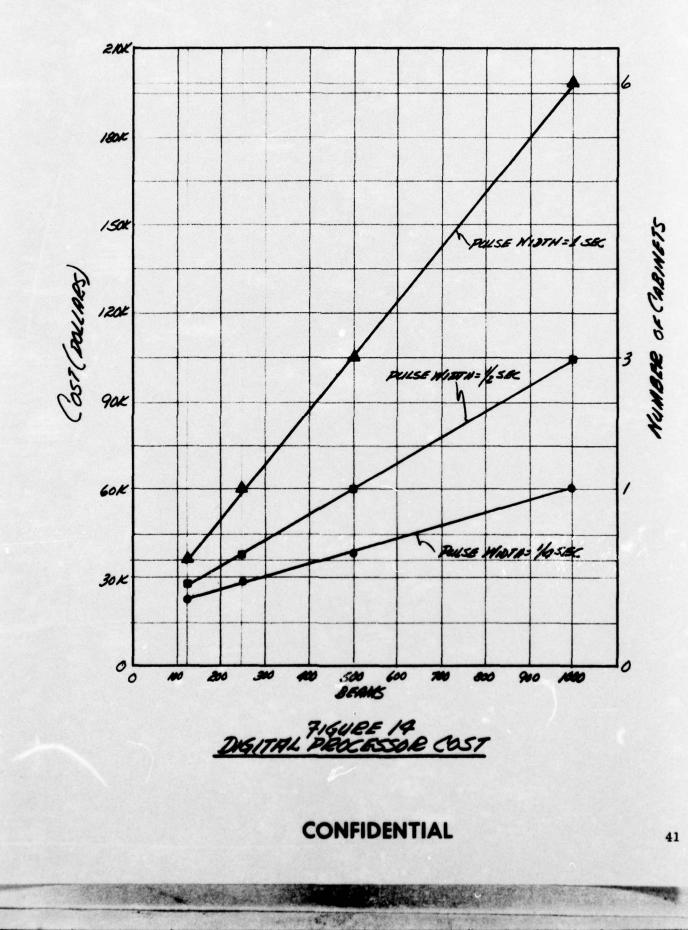
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A BEANS		125			250			500			1000	
PULSE LANOTH (SBC)	1/1	1/2	-	1/1	1/2	T	1/1	1/2	1	1/1	1/2	F
1. STNC. DET.	\$ 1.5	1.5	1.5	2.0	2.0	2.0	2.5	2.5	2.5	3.0	3.0	3.0
3. SAMPLE & ROLD	1.0.	11.0	1.0	0.5	5.0	5.0	1.0	1.0	1.0	1.0	1.0	1.0
4. A/D CONVERTER	* * •	4.0	0.4	0.0	0.0	5.0	0.0	6.0	6.0	8.0	8.0	8.0
6. MULTIPLIER QUAD.	\$ 2.0	2.5	3.0	2.5	3.0	0.0	3.0	6.0	12.0	6.0	12.0	54.0
7. CORE INTEG. STORE	\$20.0	30.0	10.0	30.0	10.04	80.0	10.0	80.0	1.2	80.0	160.0	320.0
9. MAGNITUDE PROC.	\$ 5.0	5.2	.0.	5.2	0.0	3.2		3.2	3.4	3.2	3.4	
10. WEIGHT. MULT.	\$ 1.0	1.1	1.3	11	1.3	5.6	1.3	5.6	5.2	5.6	5.2	10.4
11. WEIGHT STORE 12. RECIRC. STORE	\$ 0.5	0.2	0.2	0.5	0.2	1.4.0	0.5	8.0	1.4	0.4	1.1	1.6
	\$ 0.6	1.2	2.5	0.8	1.5	2.0	1.0	3.0	10.01	2.0	0.9	20.0
14. DIGITAL CLOCK	\$ 1.5	0.0	0.0	5.0	0.0	0.2	3.0	0.0	0.91	0.5	0.6	30.0
	\$ 2.5	8.8	3.0	8.8	3.0	0.4	3.0	0.4	6.0	4.0	6.0	10.0
Less items 14,15,16	\$32.8	14.7	57.5	45.7	57.8	106.7	58.8	106.1	203.6	107.7	202.1	396.5
Less items 14,15,16 & 7	\$15.8	19.2	25.5	20.2	25.8	42.7	26.8	42.1	75.6	43.7	1.47	140.5
Sub-Total Items 14,15,16	\$ 6.5	8.3	0.11	8.3	0.11	17.5	0.11	17.5	30.0	17.5	30.0	58.0
Total (less item 7)	\$22.3	27.5	36.5	38.5	36.8	60.2	37.8	9.65	105.6	61.2	1.401	198.5
		1	1	1	1	1	1	1	1		1	

TABLE 9

1

# DIGITAL PROCESSOR COST (IN THOUSANDS OF DOLLARS)

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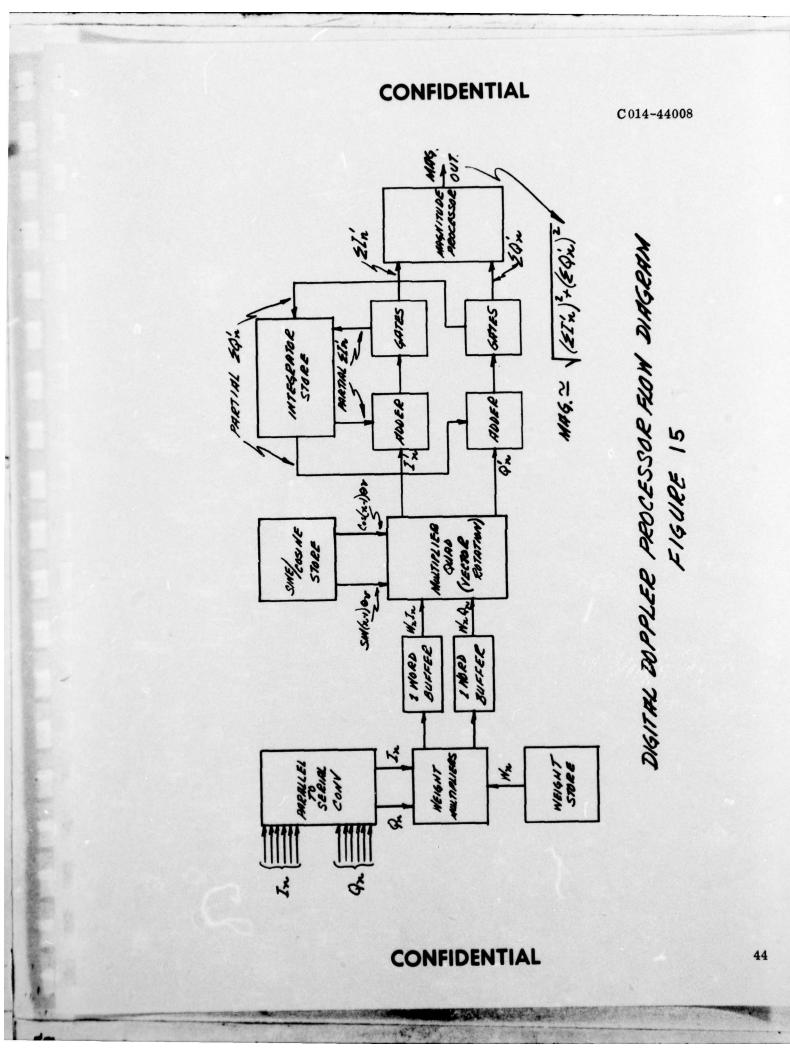
NO. BEAMS	125	250	500	1000
Pulse Length (Sec)	1/4 <sup>1</sup> / <sub>2</sub> 1	1/2 1	1 <u>1</u> 121	1 1 1 1
Input Word Rate Kc	12 Kc	24 Kc	48 Kc	96 Kc
Processor Word Rate Mc	0.29 0.58 1.15	0.58 1.15 2.30	1.15 2.30 4.60	2.30 4.60 9.22
Number of Quads	1 1 1	1 1 2	124	2 4 8
Quad Bit Rate (Mc)	3.5 6.9 13.8	6.9 13.8 13.8	13.8 13.8 13.8	13.8 13.8 13.8
Integrator Store (#12 bit words)	6 <b>K 12K 24K</b>	12K 24K 48K	24K 48K 96K	48 <b>K</b> 96K 192K

#### TABLE 10

DIGITAL PROCESSOR PARAMETERS

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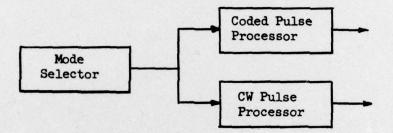
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#### SECTION VII

#### THE WIDEBAND PROCESSOR

#### A. INTRODUCTION

A block diagram showing the major components of the wideband processor is shown below.



For the range of signal bandwidths from 50 - 200 cps and BT products of 1 to 12, the coded pulse processor costs vary as a function of bandwidth, BT product and number of beams. The mode selector and CW pulse processor costs vary only as a function of number of beams. The wideband CW pulse processor is identical to the surface duct processor except for the input filter which is contained in the mode selector. Since the CW pulse processor costs are detailed in Section V, only the mode selector and coded pulse processor costs will be presented here.

The technique for handling more beams, higher BT products and larger bandwidths for the Mode Selector and the Coded Pulse processor is to add parallel functions rather than making functions more sophisticated.

#### B. THE MODE SELECTOR

A detailed block diagram of the Mode Selector is shown in Figure 17. Component costs and number of 2" x 4" circuit boards for various numbers of beams referenced to this figure are shown in Table 11.

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The resulting Mode Selector costs and number of cabinets as a function of number of beams are plotted in Figure 16.

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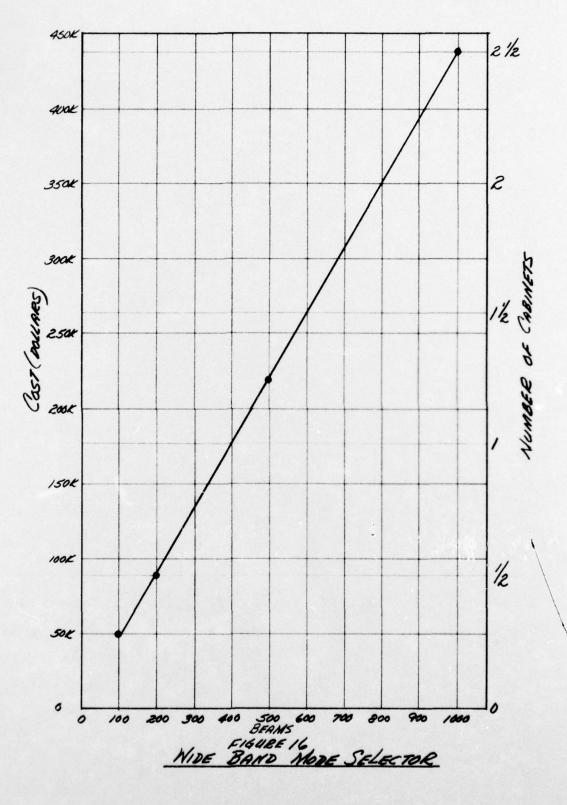
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	J.K	5	X	V	31	N
	1014	80AED	1/4 44.9%	88.3SK	21222	×38.26
	SUMMER TOTAL CABINETS TOTAL	ST BOREDS COST BOREDS COST BORDS COST NUMBER COST NUMBER COST NUMBER	1/4	12	1 1/4 212.2K	212 438.264
k	CABI	Cast	10K	2.06	6.15	
e cos.	TOTAL BURUS	NUMBER	326	643 2.0K	2.6K 1590 6.1K	5.2K 3180 12.2K
NIDE BAND MODE SELECTOR COST	YEE	rest	* 600	1.1%	2.6K	5.24
E SEL	SUMA	BABS	e	2	26	32
MOD	LIMITER	(1957	Par .	AOK	100%	2005
DAND	- Alwin	BARRESS	00/	200	200	200K 1000 200K
WIDE .	RAP	Cast	20%	40K	7001	BOX
	DIST AMP	BUREDS	200	400	000/	5000
	46	is cast	3.36 200	5.25K 400	10AESK 1000	20.85K 2000
	TIMIT	BARK	20	32	64	128
	BEAM TIMING	NUMBER	00/	200	500	0001

TABLE !!

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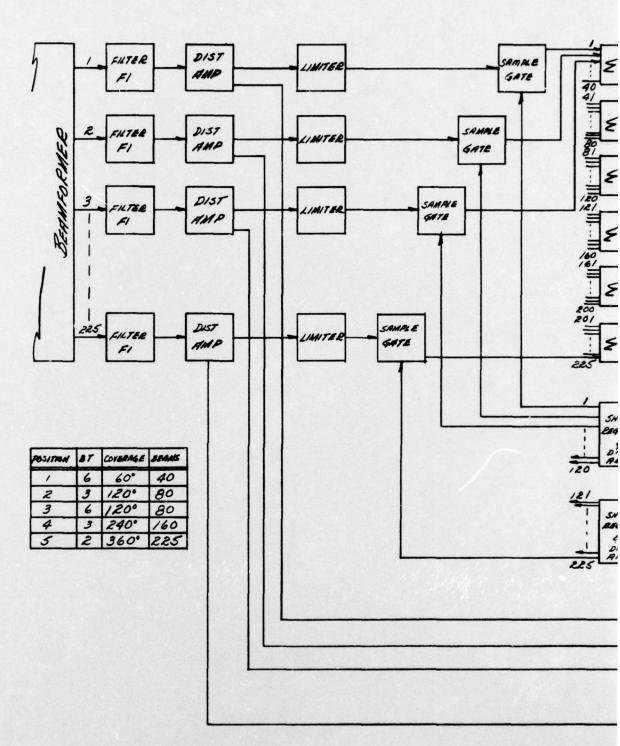
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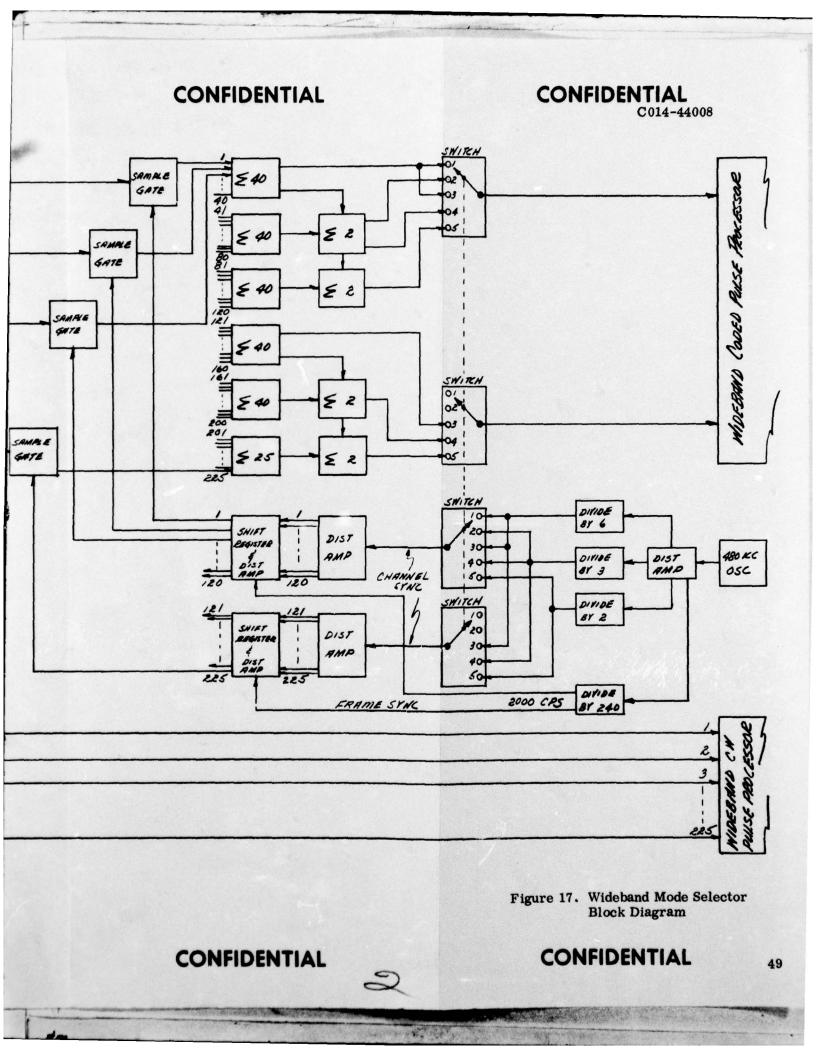
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#### C. THE CLIPPER CORRELATOR PROCESSOR

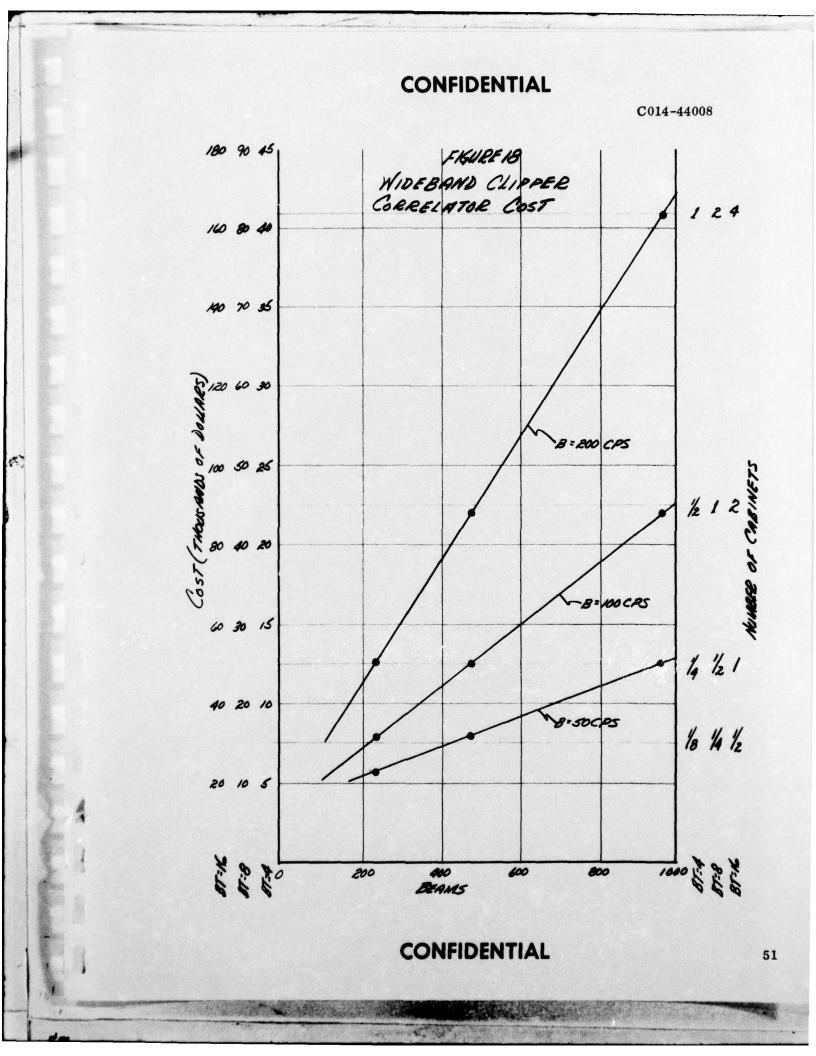
A block diagram of the clipper correlator processor is shown in Figure 19. The configuration shown meets the requirements assumed for the First Cut Signal Processor.

The First Cut Processor had the flexibility of choosing several different combinations of signal pulse length and number of beams for a 100 cps bandwidth coded pulse. In view of the fact that the clipper correlator configuration varies as a function not only of bandwidth and number of beams but also as a function of BT product it was decided to eliminate the switching flexibility for the purposes of costing.

Therefore, a number of processor configurations were studied, each configuration defined by pulse width, BT product, and number of beams to be processed. Table 12 shows the various combinations that were considered and specifies the number of "basic processors" needed for each configuration. Table 13 shows the "basic processor" cost with reference to Figure 19.

Curves of cost as a function of number of beams, BT product and Bandwidth were derived from Tables 12 and 13 and are presented in Figure 18.

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f = 2000 s 4800 bit ca		NO.	OF	"BASI	C" CLI	PPER CO	ORRELAT	OR PR	OCESSO	RS	•	
BT (For E	= 50 cps)	2	4	8	12	16	24	32	36	40	48	56
BT (For B	= 100 cps)		2	4	6	8	12	16	18	20	24	28
BT (For B	= 200 cps)			2	3	4	6	8	9	10	12	14
	80						1				2	
	160				l		2		3		4	
	240			1		2	3	4		5	6	7
Number of	320				2		4		6		8	
Beams	400						5				10	
	480		l	2	3	4	6	8	9	10	12	14
	560						7				14	
	640				4		8		12		16	
	720			3		6	9	12		15	18	21
	800				5		10		15		20	
	960	l	2	Ц.	6	8	12	16	18	20	24	28

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TABLE 12

CLIPPER CORRELATOR REQUIREMENTS

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#### Functions that are invarient as processors are added

	Boards	Cost
Limiter and Gate	4	\$ 400
Shift Register	3	1,000
Mixer	l	100
40 MHz Oscillator and Distribution Amplifier		850
9.6 MHz Oscillator and Distribution Amplifier		850
		\$3,200

Functions that are duplicated as processors are added

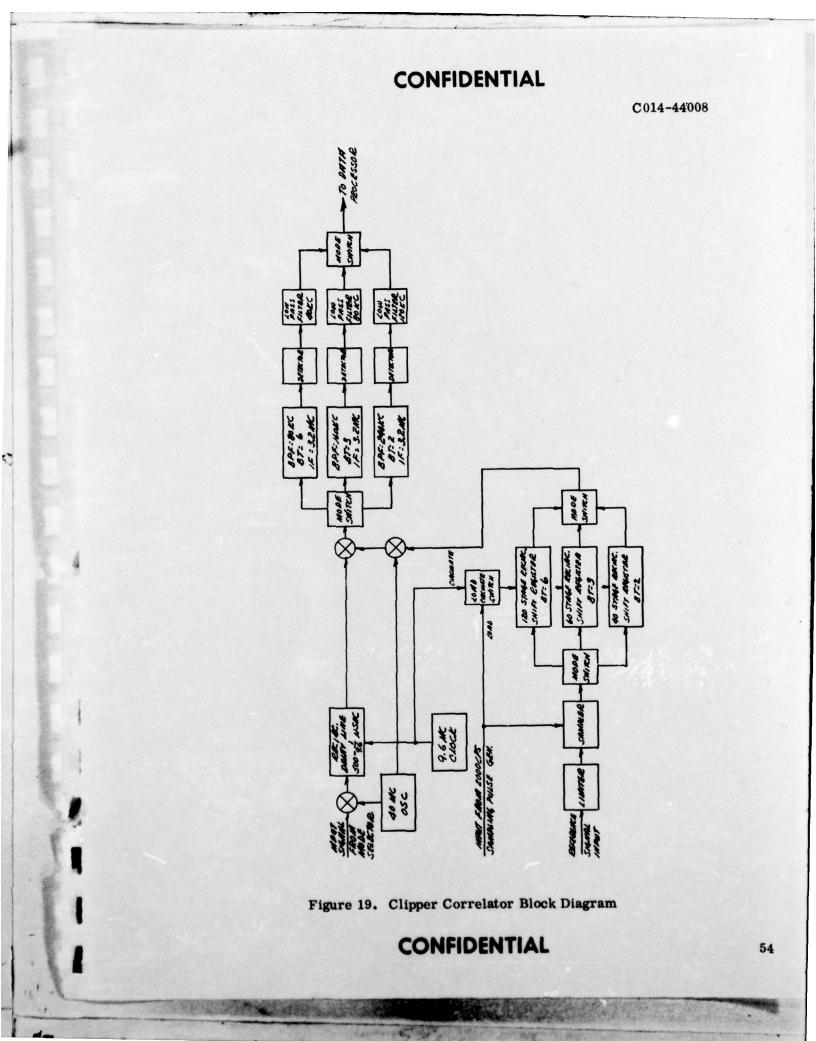
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		Boards	Co	ost
(2)	Mixers	2	\$ 2	200
	Output Amplifier	ı	נ	.00
	Bandpass Filter		נ	.00
	Envelope Detector	2	2	200
	Low Pass Filter	l	ı	.00
	Delay Line & Associated Circuitry		3,5	00
	Cabinet, Power Supplies, Misc.		5	00

TABLE 13

BASIC CLIPPER CORRELATOR COST

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#### REFERENCES

- "The First-Cut Signal Processor for Conformal/Planar Array Sonar System", 20 December 1965, Contract NObsr 93022, Task 8189.
- 2.a. "Interim Report Active Systems Analysis for Planar Array Sonar", 30 April 1965, Contract NObsr 93022.
  - b. "Addendum to Interim Report Active System Analysis for Planar Array Sonar", 30 April 1965, Contract NObsr 93022.
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