

000260

AD A 031724

000260

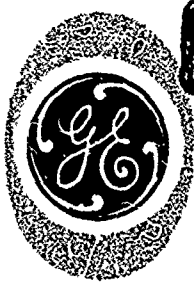
John

00V1B1

FL

MOST Project 3

(1)



OOVI LIBRARY COPY

TEMP

THE ITERATIVE
DETERMINATION
OF MODEL
PARAMETERS
BY NEWTON'S
METHOD

67TMP-64

GENERAL ELECTRIC COMPANY
SANTA BARBARA
CALIFORNIA

DDC
RECEIVED
NOV 2 1976
A

DISTRIBUTION STATEMENT A
Approved for public release;
Distribution Unlimited

Copy no. 17

THE ITERATIVE DETERMINATION OF MODEL
PARAMETERS BY NEWTON'S METHOD,

(10) Henry P. Kramer

(11) 67TMP-64

September 1967

(12) 15p.

Prepared for
Naval Ships System
Department of the Navy
Washington, D.C.

Contract No. N00024-67-C-1303

(15)

TEMPO
GENERAL ELECTRIC COMPANY
SANTA BARBARA, CALIFORNIA

346 420
bpg

RECEIVED BY	
WTS	Write Section <input checked="" type="checkbox"/>
SEC	Staff Section <input type="checkbox"/>
MANROBERTS	<input type="checkbox"/>
IDENTIFICATION	
BY <i>Allen on file</i>	
DISTRIBUTION/AVAILABILITY CODES	
Dist.	STAIL. ORG. OR SPECIAL
A	

THE ITERATIVE DETERMINATION OF MODEL PARAMETERS BY NEWTON'S METHOD

The problem that we would like to solve is to determine numbers a_1, a_2, \dots, a_N and $\Delta_1, \Delta_2, \dots, \Delta_N$ so that, with regard to an observation $e(t)$ and for unknown N , the equation

$$e(t) = \sum_{k=1}^N a_k s(t-\Delta_k) \quad (1)$$

is satisfied.

Let us define

$$y(t;x) = \sum_{k=1}^N x_k s(t-x_N + \Delta_k) - e(t). \quad (2)$$

In keeping with the spirit of Newton's method for finding the root of a function of one variable, we are looking for a vectorial increment δx such that

$$y(t;x+\delta x) = y(t;x) + \sum_{k=1}^{2N} \frac{\partial y}{\partial x_k} \delta x_k + \text{terms of higher order} = 0.$$

Thus we have an equation

$$\sum_{k=1}^{2N} \frac{\partial y}{\partial x_k} \delta x_k = -y(t;x) \quad (3)$$

from which to determine the incremental vector components δx_k . At this point it is important to recall that both members of Equation 3

are functions of t . In order to eliminate t and obtain $2N$ equations in $2N$ unknowns we could, for example, choose $2N$ values of t , t_1, t_2, \dots, t_{2N} and evaluate both members of Equation 3 at these t values. In a real situation this procedure has the drawback that the demands for accuracy placed on the values of y and its partial derivatives at the special t points would be too great. In the presence of noise (due to inaccuracies in measurement, in the model, round-off errors, etc.) the above method of creating $2N$ equations in the $2N$ unknowns should be rejected as being unstable.

Actually, however, this method is just one realization of a general method of deriving $2N$ equations in $2N$ unknowns from Equation 3. The general method postulates that $2N$ linear functionals be chosen $\gamma_1, \gamma_2, \dots, \gamma_{2N}$ and applied to both members of Equation 3. The result is then

$$\sum_{k=1}^{2N} \gamma_l \left(\frac{\partial y}{\partial x_k} \right) \delta x_k = -\gamma_l(y). \quad (l = 1, 2, \dots, 2N). \quad (4)$$

We now have a non-homogeneous linear system of equations in the unknown δx_k ($k = 1, 2, \dots, 2N$) and this system has a unique solution only if the matrix M with elements

$$M_{lk} = \gamma_l \left(\frac{\partial y}{\partial x_k} \right) \quad (5)$$

is non-singular and the vector g with elements

$$- \gamma_l(y) \quad (6)$$

does not vanish.

It is necessary to say a word about the notion of a linear functional γ . γ associates with each member f of a class of functions a number $\gamma(f)$ in such a way that if f and g are any two functions in the class, α and β are any two numbers, and that if the function $\alpha f + \beta g$ also belongs to the class, then

$$\gamma(\alpha f + \beta g) = \alpha \gamma(f) + \beta \gamma(g).$$

If the class of functions consists of all those which are square integrable over the real axis, then by the celebrated Riesz-Fischer theorem* every bounded functional γ has the representation

$$\gamma(f) = \int_{-\infty}^{\infty} i(x) \overline{h_{\gamma}(x)} dx,$$

where h_{γ} is a square integrable function corresponding to the linear functional γ and the bar denotes complex conjugate.

After this brief digression let us return to Equation 4 to see how it can be used to approach a solution by iteration. Suppose at the n^{th} step an approximate solution Z^n has been calculated. To determine the next, hopefully improved, approximant Z^{n+1} , we set

$$\delta x^n = Z^{n+1} - Z^n$$

and let

$$M_{L^n} \equiv \gamma_{L^n} \left(\frac{\partial y}{\partial x_k} \right)^n \quad \text{and} \quad (7)$$

$$g_{L^n} \equiv -\gamma_{L^n}(y^n). \quad (8)$$

Then

$$M^n Z^{n+1} = M^n Z^n - g^n \quad (9)$$

and if M^n has an inverse, then

$$Z^{n+1} = Z^n - (M^n)^{-1} g^n. \quad (10)$$

It can be shown† that if the initial guess Z^0 is sufficiently close to a solution, then the sequence of approximants Z^0, Z^1, Z^2, \dots converges to the solution.

* Halmos, Paul P., Introduction to Hilbert Space, Chelsea Publishing Company, New York, 1951, p 31.

† Stern, M. L., "Sufficient conditions for the convergence of Newton's Method in complex Banach spaces", Proc. Amer. Math. Soc., vol 3, (1952) pp 858-863.

It is apparent that one of the major problems with the method is the selection of a good initial approximant Z^0 . Two methods have been devised to obtain approximate solutions for Equation 1. The first will be called the Fourier method. Taking the Fourier transform of both members of Equation 1, the result is

$$E(f) = \left(\sum_{k=1}^N a_k e^{-2\pi i f \Delta_k} \right) S(f). \quad (11)$$

This expression is, however, valid only for those frequencies for which $S(f)$ and $E(f)$ do not vanish, that is, only for the frequencies that lie in the common band in case s and consequently e are bandlimited. If in Equation 11 we divide both members by $S(f)$ and then take the inverse Fourier transform of the result, we obtain

$$d(t) = \sum_{k=1}^N a_k \int_{\Omega} e^{2\pi i f(t-\Delta_k)} df, \quad (12)$$

where Ω represents the pertinent band of frequencies.

If $\Omega = \left| f - \frac{w}{2} \leq f \leq \frac{w}{2} \right|$, then

$$d(t) = \sum_{k=1}^N a_k \frac{\sin \pi w(t-\Delta_k)}{\pi(t-\Delta_k)} \quad (13)$$

and the values of $\Delta_1, \Delta_2, \dots, \Delta_N$ can be estimated as the position of the maxima of $d(t)$. The values of a_1, a_2, \dots, a_N are approximated by the magnitudes of $d(t)$ at the observed maxima. The limit of resolution of this method is about $1/w$, i.e., if $\Delta_i - \Delta_{i+1} < 1/w$, then the corresponding two maxima will have moved together so as to yield only one maximum.

$$\text{If } \Omega = \left| f \right| - \frac{w}{4} - w_c \leq f \leq -w_c + \frac{w}{4}, w_c - \frac{w}{4} \leq f \leq w_c + \frac{w}{4} \Big|,$$

then

$$d(t) = \sum_{k=1}^N a_k \left\{ \frac{\sin \pi (2w_c + w/2)(t - \Delta_k) - \sin \pi (2w_c - w/2)(t - \Delta_k)}{\pi (t - \Delta_k)} \right\} \quad (14)$$

or

$$d(t) = 2 \sum_{k=1}^N a_k \cos 2\pi w_c (t - \Delta_k) \frac{\sin \pi w/2 (t - \Delta_k)}{\pi (t - \Delta_k)} \quad (15)$$

Again the same method for estimating the Δ 's and a 's can be used.

$$\text{If } \Omega = \left\{ f \mid w_c - \frac{w}{2} \leq f \leq w_c + \frac{w}{2} \right\},$$

then

$$d(t) = \sum_{k=1}^N a_k e^{2\pi i w_c (t - \Delta_k)} \frac{\sin \pi w (t - \Delta_k)}{\pi (t - \Delta_k)} \quad (16)$$

and the real part will again have maxima near the points $t = \Delta$ and the magnitudes of these maxima will be close to a_k .

The second method, based on correlation, can also be used for obtaining first estimates. Let us multiply both members of Equation 1 by $s(t-z)$ and integrate over all values of the variable t . We can then write

$$R_{s, \epsilon}(z) = \sum_{k=1}^N a_k R_{s, s}(z - \Delta_k), \quad (17)$$

where

$$R_{f, g}(z) \equiv \int_{-\infty}^{\infty} f(t-z) g(t) dt \quad (18)$$

If the Δ_k are sufficiently separated, i.e., by more than $1/w$, then the position of the maxima of $R_{s, \epsilon}(z)$ provides first estimates for $\Delta_1, \Delta_2, \dots, \Delta_N$ and the magnitudes of the maxima divided by $R_{s, s}(0)$ provide estimates for a_1, a_2, \dots, a_N .

Having found first estimates of $\Delta_1, \Delta_2, \dots, \Delta_N$ and a_1, a_2, \dots, a_N , we must now seek to improve them by iteration. The requirements for a good iterative method are:

1. Improvement of resolution. If one maximum actually corresponds to two separate components, the method should be able to resolve the two components.
2. If some secondary maxima have been confounded with primary maxima the iterative method should be capable of eliminating them.
3. Finally, an improvement in accuracy in the evaluation of $\Delta_1, \dots, \Delta_N$ should result from the application of the method.

Once the initial estimates have been made we turn to Newton's method for their improvement. To this end we must choose functionals $\gamma_1, \dots, \gamma_{2N}$.

Let

$$\gamma_i(f) = \int_{-\infty}^{\infty} f(t) \varepsilon(t - x_{i+N}) dt$$

and

$$\gamma_{i+N}(f) = \int_{-\infty}^{\infty} f(t) \{-x_i s'(t - x_{i+N})\} dt,$$

where s' denotes the derivative of s . The matrix M^R , defined by Equation 7, takes the form

$$M_{L+K}^R = \int_{-\infty}^{\infty} s(t - x_K^R) s(t - x_L^R) dt$$

$$M_{L+NK}^R = \int_{-\infty}^{\infty} s(t - x_K^R) \{-x_L^R s'(t - x_L^R)\} dt$$

$$M_{L+N}^R = \int_{-\infty}^{\infty} \{-x_K^R s'(t-x_{K+N}^R)\} s(t-x_{L+N}^R) dt$$

$$M_{L+N, K+N}^R = \int_{-\infty}^{\infty} \{-x_K^R s'(t-x_{K+N}^R)\} \{-x_L^R s'(t-x_{L+N}^R)\} dt$$

for $L = 1, 2, \dots, N$ and $K = 1, 2, \dots, N$.

Using the notion of convolution or correlation we can write the above matrix elements more conveniently as

$$M_{L, K}^R = R_{s, s}(x_{K+N}^R - x_{L+N}^R)$$

$$M_{L+N, K}^R = -x_L^R R_{s, s'}(x_{K+N}^R - x_{L+N}^R)$$

$$M_{L, K+N}^R = -x_K^R R_{s', s}(x_{K+N}^R - x_{L+N}^R)$$

$$M_{L+N, K+N}^R = x_K^R x_L^R R_{s', s'}(x_{K+N}^R - x_{L+N}^R)$$

for $L = 1, 2, \dots, N$ and $K = 1, 2, \dots, N$.

But

$$\frac{\partial R_{s, s}(\tau)}{\partial \tau} = - \int_{-\infty}^{\infty} s'(t-\tau) s(t) dt = -R_{s', s}(\tau)$$

and

$$\frac{\partial^2 R_{s, s}(\tau)}{\partial \tau^2} = \int_{-\infty}^{\infty} s'(t-\tau) s'(t) dt = R_{s', s'}(\tau).$$

Therefore,

$$\begin{aligned}
 M_{L,K}^R &= R_{s,s}(\tau) \Big|_{\tau = (x_K^R - x_L^R)} \\
 M_{L+N,K}^R &= x_L^R \frac{\partial R_{s,s}}{\partial \tau} \Big|_{\tau = (x_K^R - x_{L+N}^R)} \\
 M_{L,K+N}^R &= x_K^R \frac{\partial R_{s,s}}{\partial \tau} \Big|_{\tau = -(x_{K+N}^R - x_L^R)} \\
 M_{L+N,K+N}^R &= x_K^R x_L^R \frac{\partial^2 R_{s,s}}{\partial \tau^2} \Big|_{\tau = (x_{K+N}^R - x_{L+N}^R)}
 \end{aligned} \tag{19}$$

for $L = 1, 2, \dots, N$ $K = 1, 2, \dots, N$ $K = 1, 2, \dots, N$

The vector g^R whose components are given by Equation 8 takes the form

$$\begin{aligned}
 g_L^R &= \int_{-\infty}^{\infty} e(t) s(t - x_L^R) dt = R_{s,\varepsilon}(x_L^R) \\
 g_{L+N}^R &= \int_{-\infty}^{\infty} e(t) \{ -x_L^R s'(t - x_{L+N}^R) \} dt = x_L^R \frac{\partial R_{s,\varepsilon}}{\partial \tau} \Big|_{\tau = x_{L+N}^R}
 \end{aligned} \tag{20}$$

Equations 19 and 20 show that the only data that we require for the application of Newton's method are the correlation functions $R_{s,s}$ and $R_{s,\varepsilon}$. If these are furnished by observation, numerical differentiation will yield the remaining matrix and vector elements.

In the course of iteration it is necessary to update the matrix M and the vector g at each step. This, however, is very easily done since it involves no more than a table look up of the values of functions and their derivatives at new values of their arguments.

To test the ideas presented above by means of an example, the choice was made of

$$S(t) = \frac{\sin(\pi t)}{(\pi t)}.$$

This choice is motivated not only by the desire to generate a test, but also by the notion that upon transformation by the Fourier method Equation 1 takes the form of Equation 13 which is the same as that of Equation 1 when the above choice is made. Therefore, with this choice we can proceed to solve Equation 13 directly by Newton's method.

To determine the matrix elements consider

$$R_{s,s}(\tau) = \int_{-\infty}^{\infty} \frac{\sin \pi(t-\tau)}{\pi(t-\tau)} \frac{\sin \pi t}{\pi t} dt$$

$$= \int_{-\infty}^{\infty} e^{2\pi i f \tau} \left| X(f) \right|^2 df = \frac{\sin \pi \tau}{\pi \tau},$$

where $X(f) = 1$ for $-1/2 \leq f \leq 1/2$ and $X(f) = 0$ for $|f| > 1/2$.

$$\frac{\partial R_{s,s}}{\partial \tau} = \pi \frac{x \cos x - \sin x}{x^2} \Big|_{x = \pi \tau}$$

$$\frac{\partial^2 R_{s,s}}{\partial \tau^2} = \frac{\pi^2}{x^4} \left[-2x^2 \cos x + x(2-x^2) \sin x \right] \Big|_{x = \pi \tau}$$

A program (listed in the Appendix) was written to carry the calculations through numerically. Tests were performed on a weighted sum of delayed and truncated replicas of six $\pi t / \pi t$. Then tests showed that convergence, when it occurred, was rapid. We had numerical difficulties in high dimensions because of the many matrix inversions involved. The program was, however, able to resolve two pulses that were separated by 0.2, that is, by 0.2 of the normal resolution limit.

In order to facilitate decisions as to the best value of N , the mean square difference between the function e and its approximant was calculated and that solution was adopted as the final one which had a number of components yielding the smallest mean square difference.

A possible improvement might be had by evaluating the gradient of y , i.e., $\{ \partial y / \partial x_i \}$, at some point other than the last approximant to the zero. Work to realize this idea is going on at present and will be reported subsequently.

CONCLUSION

A method for solving the functional equation

$$e(t) = \sum_{k=1}^N a_k s(t - \Delta_k)$$

is presented. The method adapts the idea of Newton's method to the case at hand which differs from the classical situation in that the functions whose zeroes are sought are themselves elements of a function space. To illustrate the method a program was written that demonstrated a marked improvement in resolution for pulses of the form $\sin(\pi t) / (\pi t)$. One of the drawbacks of the method is that initial guesses have to be close to the actual solution. Another difficulty arises from the fact that since N is unknown, solution must be attempted with various values of N .

APPENDIX

IT-1 0:18 SB MON 09/05/67

```

1 FILE K-R
10 DIM E(256)
20 DIM M(20,20),W(20,20),F(20,1),Q(20,1),A(10),D(10)
25 READ TO,A0,B0,B
30 FOR I=1 TO TO\READ FILE 1,E(I)\NEXT I
40 P1=3.1415927
60 FOR S=1 TO 100\INPUT T1,L2
70 T=2*T1
110 FOR I=1 TO T1\INPUT A(I),D(I)\NEXT I
120 FOR LI =1 TO L2
130 MAT M=ZER(T,T)
140 MAT W=ZER(T,T)
150 MAT Q=ZER(T,1)
200 MAT F=ZER(T,1)
210 FOR J=1 TO T1\FOR I=1 TO TO
220 A1=P1*(A0*I-B0-D(J))
230 IF ABS(A1)<=.000001 THEN 270
240 F(J,1)=F(J,1)+E(I)*SIN(A1)/(A1*B)
250 F(T1+J,1)=F(T1+J,1)-E(I)*P1*(A1*COS(A1)-SIN(A1))/(A1*2)
260 GO TO 280
270 F(J,1)=F(J,1)+E(I)/B
280 NEXT I
285 F(T1+J,1)=A(J)*F(T1+J,1)
290 NEXT J
295 MAT F=(A0)*F
300 FOR I=1 TO T1
310 FOR J=1 TO T1
320 K=P1*(D(J)-D(I))
325 IF ABS(K)<=.00001 THEN 400
330 M(I,J)=SIN(K)/(K*B)
340 M(T1+I,T1+J)=A(I)*A(J)*(P1*2)*B*(2*K*COS(K)+((K*2)-2)*SIN(K))/(K*3)
350 M(I,T1+J)=P1*A(J)*(K*COS(K)-SIN(K))/(K*2)
380 GO TO 490
400 M(I,J)=1/B
410 M(T1+I,T1+J)=A(I)*A(J)*B*(P1*2)/3
420 M(I,T1+J)=0
430 M(T1+I,J)=0
490 NEXT J\NEXT I
495 FOR I=1 TO T1\FOR J=1 TO T1\M(I+T1,J)=M(J,T1+I)
496 NEXT J\NEXT I
497 FOR I=1 TO T1\FOR J=1 TO T1\IF ABS(M(I,J))>=10 E-11 THEN 500
498 M(I,J)=0\NEXT J\NEXT I
500 MAT W=INV(M)
510 MAT Q=W*F
520 FOR J=1 TO T1
530 A(J)=Q(J,1)
540 D(J)=D(J)+Q(T1+J,1)
550 NEXT J
560 NEXT LI
600 FOR I=1 TO T1
610 PRINT I;A(I);D(I)
620 NEXT I
630 NEXT S
700 DATA 100,.1,5,1
9999 END

```

UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R&D		
(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)		
1. ORIGINATING ACTIVITY (Corporate author) General Electric, TEMPJ 816 State Street Santa Barbara, California		2a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED
		2b. GROUP
3. REPORT TITLE THE ITERATIVE DETERMINATION OF MODEL PARAMETERS BY NEWTON'S METHOD		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates)		
5. AUTHOR(S) (Last name, first name, initial) Kramer, Henry P.		
6. REPORT DATE September 1967	7a. TOTAL NO. OF PAGES 12	7b. NO. OF REFS
8a. CONTRACT OR GRANT NO. N00024-67-C-1303	8b. ORIGINATOR'S REPORT NUMBER(S) 67TMP-64	
8c. PROJECT NO.	8d. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
10. AVAILABILITY/LIMITATION NOTICES		<div style="border: 1px solid black; padding: 5px;"> DISTRIBUTION STATEMENT A Approved for public release; Distribution Unlimited </div>
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Naval Ships System Dept. of the Navy Washington, D. C.
13. ABSTRACT <p>The principle of Newton's method for determining a zero of a function has been adopted to the problem of determining parameters a_1, a_2, \dots, a_n such that $y(t; a_1, a_2, \dots, a_n) = 0$ for almost all values of t. The method has been applied to the solution of a particular equation. Methods for determining initial guesses are also presented.</p>		

DD FORM 1473
1 JAN 64UNCLASSIFIED
Security Classification

UNCLASSIFIED

Security Classification

14	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	Functional equations iteration Newton's method						

INSTRUCTIONS

1. ORIGINATING ACTIVITY: Enter the name and address of the contractor, subcontractor, grantee, Department of Defense activity or other organization (*corporate author*) issuing the report.

2a. REPORT SECURITY CLASSIFICATION: Enter the overall security classification of the report. Indicate whether "Restricted Data" is included. Marking is to be in accordance with appropriate security regulations.

2b. GROUP: Automatic downgrading is specified in DoD Directive 5200.10 and Armed Forces Industrial Manual. Enter the group number. Also, when applicable, show that optional markings have been used for Group 3 and Group 4 as authorized.

3. REPORT TITLE: Enter the complete report title in all capital letters. Titles in all cases should be unclassified. If a meaningful title cannot be selected without classification, show title classification in all capitals in parenthesis immediately following the title.

4. DESCRIPTIVE NOTES: If appropriate, enter the type of report, e.g., interim, progress, summary, annual, or final. Give the inclusive dates when a specific reporting period is covered.

5. AUTHOR(S): Enter the name(s) of author(s) as shown on or in the report. Enter last name, first name, middle initial. If military, show rank and branch of service. The name of the principal author is an absolute minimum requirement.

6. REPORT DATE: Enter the date of the report as day, month, year, or month, year. If more than one date appears on the report, use date of publication.

7a. TOTAL NUMBER OF PAGES: The total page count should follow normal pagination procedures, i.e., enter the number of pages containing information.

7b. NUMBER OF REFERENCES: Enter the total number of references cited in the report.

8a. CONTRACT OR GRANT NUMBER: If appropriate, enter the applicable number of the contract or grant under which the report was written.

8b, 8c, & 8d. PROJECT NUMBER: Enter the appropriate military department identification, such as project number, subproject number, system numbers, task number, etc.

9a. ORIGINATOR'S REPORT NUMBER(S): Enter the official report number by which the document will be identified and controlled by the originating activity. This number must be unique to this report.

9b. OTHER REPORT NUMBER(S): If the report has been assigned any other report numbers (*either by the originator or by the sponsor*), also enter this number(s).

10. AVAILABILITY/LIMITATION NOTICES: Enter any limitations on further dissemination of the report, other than those imposed by security classification, using standard statements such as:

- (1) "Qualified requesters may obtain copies of this report from DDC."
- (2) "Foreign announcement and dissemination of this report by DDC is not authorized."
- (3) "U. S. Government agencies may obtain copies of this report directly from DDC. Other qualified DDC users shall request through _____."
- (4) "U. S. military agencies may obtain copies of this report directly from DDC. Other qualified users shall request through _____."
- (5) "All distribution of this report is controlled. Qualified DDC users shall request through _____."

If the report has been furnished to the Office of Technical Services, Department of Commerce, for sale to the public, indicate this fact and enter the price, if known.

11. SUPPLEMENTARY NOTES: Use for additional explanatory notes.

12. SPONSORING MILITARY ACTIVITY: Enter the name of the departmental project office or laboratory sponsoring (*paying for*) the research and development. Include address.

13. ABSTRACT: Enter an abstract giving a brief and factual summary of the document indicative of the report, even though it may also appear elsewhere in the body of the technical report. If additional space is required, a continuation sheet shall be attached.

It is highly desirable that the abstract of classified reports be unclassified. Each paragraph of the abstract shall end with an indication of the military security classification of the information in the paragraph, represented as (TS), (S), (C), or (U).

There is no limitation on the length of the abstract. However, the suggested length is from 150 to 225 words.

14. KEY WORDS: Key words are technically meaningful terms or short phrases that characterize a report and may be used as index entries for cataloging the report. Key words must be selected so that no security classification is required. Identifiers, such as equipment model designation, trade name, military project code name, geographic location, may be used as key words but will be followed by an indication of technical context. The assignment of links, rules, and weights is optional.

UNCLASSIFIED

Security Classification