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SOURCE STUDIES IN THE NEAR- AND FAR-FIELD

SEMI-ANNUAL TECHNICAL REPORT NO. 5-PART A

1 MAY 1975 TO 30 NOVEMBER 1975

Prepared by  
Lawrence S. Turnbull, David Sun, James C. Batts,  
and Frode Ringdal

TEXAS INSTRUMENTS INCORPORATED  
Equipment Group  
Post Office Box 6015  
Dallas, Texas 75222

Contract No. F44620-73-C-0055  
Amount of Contract: \$393,369  
Beginning 23 April 1973  
Ending 31 August 1976

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Prepared for  
AIR FORCE OFFICE OF SCIENTIFIC RESEARCH

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Nuclear Monitoring Research Office  
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30 November 1975

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## ABSTRACT

Several continuing investigations of the seismic source using near- and far-field data are discussed. We completed our analysis of near-field acceleration data recorded at Bear Valley, California, by examining two small events which occurred on 7 February 1974 and 6 July 1974. The February event, using only spectral analysis, was found to have a moment of  $3 \times 10^{21}$  dyne-cm with an equivalent circular dislocation radius of 0.18 km<sup>2</sup>. Both spectral and time domain waveform fitting techniques were applied to the July event. The solutions using each method were in reasonable agreement, with a seismic moment in the range of 2 to  $4 \times 10^{21}$  dyne-cm over an equivalent dislocation radius of about 0.1 to 0.3 km<sup>2</sup>.

Using far-field surface wave data, two central California area earthquakes (22 June 1973 and 28 November 1974) were re-examined using two new earth models which were determined by McEvilly (1975) for the north-east and southwest side of the San Andreas fault. Several far-field solutions for the source mechanism were obtained by using various combinations of stations and earth models, including use of both structures at once for the first time. However, for the central California event of 28 November 1974, the mechanism which agreed closely with that obtained by other means used only those stations on the west side of the fault, with the southwest structure used in the spectral fit.

Theoretical first higher mode surface wave spectra were generated for a double couple source in a layered half space. Both Gutenberg-Bullen and Hamilton-Healy earth models were used. As with fundamental mode spectra, 'holes' were found almost exclusively for vertical strike-slip faults. Higher mode spectral levels in the 3 to 9 second period range were

found to be comparable with 15 to 50 second period fundamental mode spectra. Also, from the excitation of the earth models, greater amplitude higher mode signals from shallow events should occur from high velocity crustal source regions.

Preliminary results have been obtained for five large events which were a part of the Sinkiang, China earthquake swarm of August 1974. Both simple spectral and spectral ratio fitting methods were employed. The far-field solutions showed a consistent trend for these five events of shallow focal depth.

Finally, we concluded our examination of the scatter of the earthquake population in the  $M_s - m_b$  discriminant. Focusing on the body-wave magnitude estimate instead of the surface wave magnitude as in previous studies, we applied the maximum likelihood method of Ringdal (1975) in an attempt to improve the accuracy of the PDE bodywave magnitudes. Although the scatter of the population did not change significantly, the slope of the data set decreased approximately 0.25.

## ACKNOWLEDGMENTS

Mr. James Battis produced the analysis and wrote the text for Section II. Dr. David Sun generated major parts of Section III, including the computer program which utilizes two different earth models in fitting far-field spectra.

Section IV was a joint project with Frode Ringdal while this author visited NORSAR, and this section was written by Frode.

Mrs. Cherylann Saunders typed all of the text, prepared the majority of the figures and all of the tables.

*Lawrence S. Turnbull, Jr.*

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## SECTION I INTRODUCTION

In this report, we present a discussion of several continuing investigations of the seismic source from near- and far-field data. We complete our analysis of near-field acceleration data recorded at Bear Valley in Section II. Two rather small events ( $m_b$ 's of 3.0 and 3.2) that were recorded in 1974 (7 February and 6 July) were studied using both spectral methods and time domain waveform techniques.

Several studies using far-field surface wave data to determine source parameters are discussed in Section III. Two central California area earthquakes, 22 June 1973 and 28 November 1974, are re-examined using two new earth models by McEvelly (1975) for the northeast and southwest sides of the San Andreas fault. In particular, we examine the problem of fitting far-field surface wave spectra when the source region contains a major discontinuity. In this section, we continue our examination of theoretical first higher mode spectra for characteristics that would reflect source depth and structural dependence, such as 'holes' and amplitude level over a particular frequency range. Also in this section, we present a preliminary analysis of several events that occurred during an earthquake swarm in Sinkiang, China, in August 1974.

Finally, in Section IV, we conclude our examination of the scatter of the earthquake population in the  $M_s - m_b$  discriminant. Instead of focusing on the  $M_s$  determination as in our previous studies, we apply the maximum likelihood method of Ringdal (1975) in an attempt to improve the accuracy of the PDE bodywave magnitudes for our data base.

SECTION II  
ANALYSIS OF TWO SMALL BEAR VALLEY EVENTS

A. INTRODUCTION

Since the occurrence of a magnitude 4.2 earthquake in June of 1973 two additional events having potential for near-zone analysis have been recorded by stations of the University of California accelerometer array located along the Bear Valley segment of the San Andreas Fault. These events were a magnitude 3.0 earthquake which occurred on February 7, 1974 and one of magnitude 3.2 which was recorded on July 6, 1974. While being of significantly lower magnitudes than earthquakes previously studied in the near-field, accelerometer records of relatively high signal-to-noise ratios, probably accounted for by the shallow depths associated with these events, were obtained at a sufficient number of stations to warrant analysis to determine the source characteristics. As with the earlier June earthquake, (Turnbull and Battis, 1974), the intermediate-zone coverage of the July 6 earthquake, resulting in determinations of location and fault plane solution independent of near-field observations, along with the relatively wide azimuthal coverage in the near-field would provide a set of restrictions on any solution resulting from the Haskell moving dislocation source model. For this reason and as a test of the applicability of the Haskell earthquake source approximation to events of very low magnitude, the near-zone analysis concentrated on the July 6, 1974 earthquake.

The University of California Bear Valley accelerometer array is located approximately 30 km southeast of Hollister, California along a seismically active segment of the San Andreas Fault. In the vicinity of the array the main fault zone strikes to the northwest, separating two distinct crustal



structures. To the southwest of the fault lies a region of high velocity granite and metamorphic strata with lower velocity sedimentary rocks predominating in the northeastern block. Detailed crustal studies have been conducted for this region (McEvelly, personal communication, 1974; Aki and Lee, 1975; and Engdahl and Lee, 1975) which have indicated a structure of complex inhomogeneities within the fault zone. As the Haskell moving dislocation source model is a whole space representation, the velocity profile determined by McEvelly, as given in Table II-1, was used to evaluate two sets of 'whole-space' velocities for use with stations on each side of the fault. These velocities were obtained by using a weighted average of the velocity profile from the hypocentral depth to the surface with the weighting factors for each velocity being proportional to the thickness of its respective layer. These weighting factors and the whole-space velocities for each crust block are also given in Table II-1. It should be noted, however, that in the case of spectral evaluation of the source characteristics using Brune's model (1970), it was felt that the velocities of the layer containing the earthquake hypocenter under study were more appropriate for use in analysis.

In Figure II-1, the location of each station in the near-field array, as operational during the recording of the two events studied in this report is shown. Each site is equipped with a three component accelerometer. The dashed line in this figure represents the surface trend of the San Andreas Fault through Bear Valley. In an effort to improve the azimuthal coverage of events occurring close to the near-field array, several modifications in the network configuration have been made since the June 23, 1973 earthquake. Of primary importance is the shift of station 6 from the northeast to the southwestern side of the fault zone. This added a second station located on the higher velocity crustal material to the southwest which aids in evaluation of differences in signal character as a function of the receiver location relative to the fault.

TABLE II-1  
BEAR VALLEY VELOCITY MODEL

| Depth To Bottom Of Layer (km) | Weighting Factor | Southwest Structure     |                         | Northeast Structure     |                         |
|-------------------------------|------------------|-------------------------|-------------------------|-------------------------|-------------------------|
|                               |                  | V <sub>p</sub> (km/sec) | V <sub>s</sub> (km/sec) | V <sub>p</sub> (km/sec) | V <sub>s</sub> (km/sec) |
| 0.6                           | 0.09             | 4.25                    | 2.46                    | 2.38                    | 1.51                    |
| 2.5                           | 0.29             | 5.2                     | 3.0                     | 3.04                    | 1.76                    |
| 5.5                           | 0.45             | 6.34                    | 3.66                    | 5.88                    | 3.30                    |
| 10.0                          | 0.17             | 5.96                    | 3.45                    | 4.84                    | 2.80                    |
| Whole Space Model             |                  | 5.76                    | 3.32                    | 4.56                    | 2.60                    |

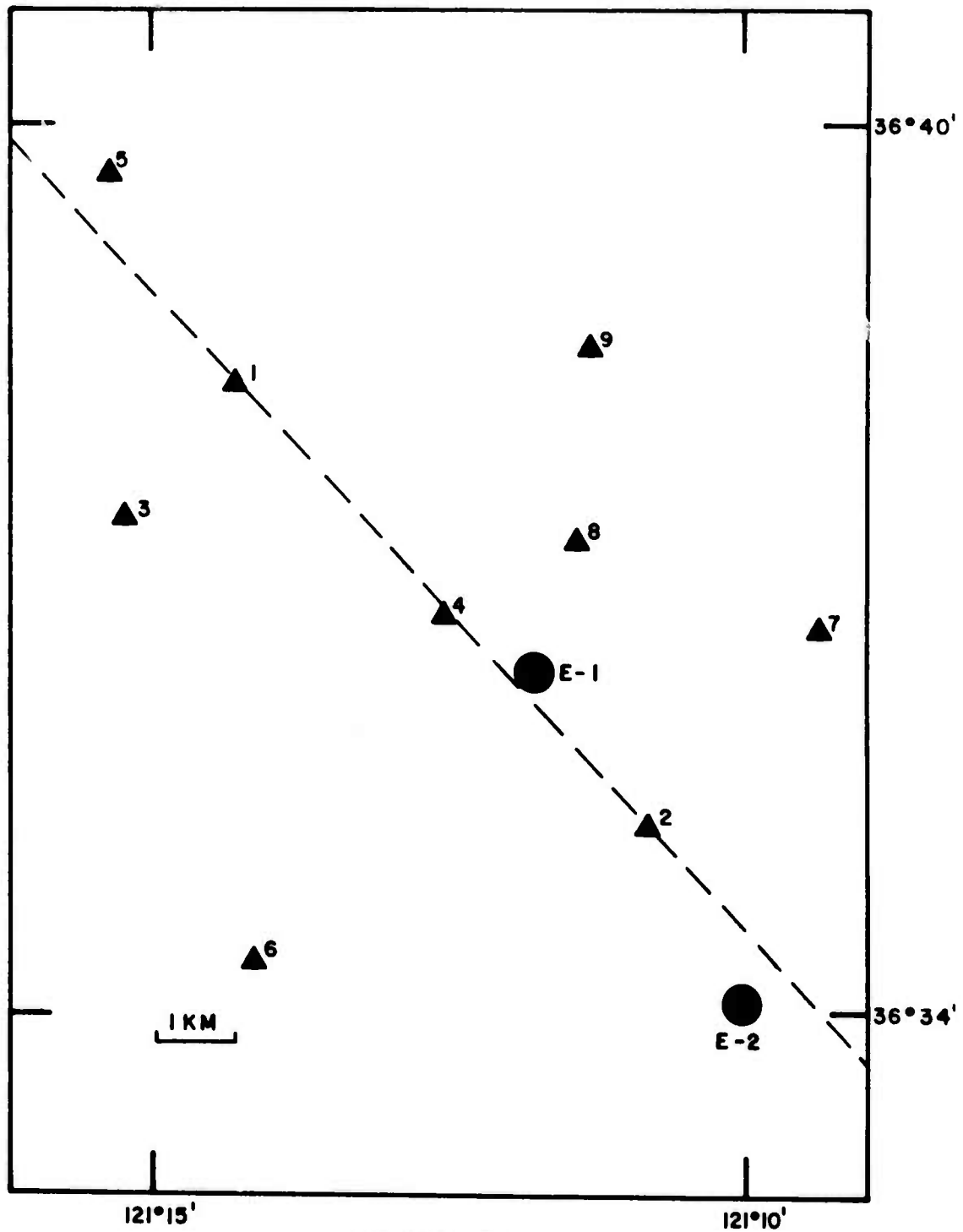


FIGURE II-1

MAP OF BEAR VALLEY ACCELEROMETER ARRAY SHOWING  
 EPICENTERS OF THE FEBRUARY 7, 1974 (E-1) AND  
 JULY 6, 1974 (E-2) EARTHQUAKES

For this report the source parameters of both the February and the July earthquakes were determined using spectral techniques. In addition, for reasons stated earlier, time domain waveform fitting was used with the July event. In the following sections the methods used in the analysis and the results of the analysis of each event is presented and the implications of these results are discussed in relation to an earlier examination of the June 22, 1973 Bear Valley event (Turnbull and Battis, 1974).

## B. EVALUATION OF SOURCE PARAMETERS

The techniques used to evaluate source parameters from near-zone data have been covered in detail by earlier reports (Turnbull and Battis, 1974; Turnbull, et al., 1975). However, to facilitate the understanding of the results presented here, a brief discussion of the two methods used in this report are given below.

Using Brune's source model (1970) it is possible to estimate the seismic moment,  $M_0$ , and a measure of the area of faulting,  $r$ , the equivalent circular dislocation radius, from the displacement amplitude spectrum of a given record of an earthquake. The equations giving these relationships are:

$$M_0 = 4\pi\rho\beta^3R\Omega_0 \quad (\text{II-1})$$

and

$$r = \left(\frac{7\pi}{4}\right)^{1/2} \beta/(2\pi f_c) \quad (\text{II-2})$$

where  $\rho$  is the material density,  $\beta$  the propagation velocity of the type of bodywave dominating the time gate used to calculate the spectra,  $R$  is the hypocenter to station distance, all supposedly known parameters, and  $\Omega_0$  is the low frequency spectral level and  $f_c$  is the corner frequency of the

spectra. In addition, other parameters of the source, such as stress drop, can be evaluated from this model.

In this study the acceleration amplitude spectrum of each component is calculated directly from the acceleration data as a preliminary step to evaluation of the associated displacement spectrum. Due to the superior noise suppression qualities of the maximum entropy spectral estimator over the discrete fast fourier transform (Turnbull, et al., 1975) the maximum entropy method is used for this step. The acceleration amplitude spectrum is then converted to a displacement spectrum by two subsequent divisions of the spectra by  $(2\pi f)$ . At this point all necessary information for the evaluation of the corner frequency and low frequency level for a given component is available.

The first division of the acceleration amplitude spectrum yields the velocity amplitude spectrum. The corner frequency of the displacement spectrum is the frequency of the peak value of the velocity amplitude spectrum. As noise in the acceleration spectrum will usually cause the extreme low frequency velocity amplitudes to blow up, these frequencies are neglected in evaluation of  $f_c$ . Given the value of  $f_c$  the low frequency level is then calculated as the average displacement spectral amplitude between the point at which the low frequency spectrum deviates from a slope of  $(2\pi f)^{-2}$  and the corner frequency.

To obtain the values used for evaluation of source parameters the information from the components of each site must be combined. In the case of  $\Omega_0$  this is done by resolving the individual component low frequency levels. In the case of corner frequency the intermediate value is selected. This would seem to be more rational than simple averaging as the latter may result in a value of  $f_c$  which could not be supported by the spectra. As was stated earlier, these values are then used in the equations of Brune's model to obtain estimates of the source parameters.

The second method of source characteristic evaluation used in this report is Haskell's moving dislocation model (Haskell, 1969). In this process the time domain acceleration traces are numerically integrated to yield velocity waveforms for each component of a station. As the Haskell model is a whole space representation, the complex structure of the P- and S-waves packets can not be simulated by this model. Thus, by some means a single period of the P- or S-wave must be isolated for each station to be used in the fitting process.

Using external information such as hypocenter locations and fault plane solutions to provide an initial case, theoretical waveforms for unit transverse and longitudinal dislocations of the fault plane are calculated for each station. At this point adjustments to fault length and width, rise time, and rupture velocity are made to produce theoretical pulse durations approximating those of the empirical waveforms. Again, restrictions such as spectral estimates of fault area are used to constrain the parameters. Following these adjustments least squared error combination of the two dislocations are calculated for fitting each station separately and as a group. The fault plane parameters of dip and strike are then perturbed to locate the minimum residual solution for each station and for all stations together. Once this set of solutions is determined the theoretical waveforms for each solution at every station is calculated. At this point a qualitative judgement on the 'goodness of fit' is made to determine which solution is accepted.

It should be noted that the least squares error combination for all stations taken as a whole may not necessarily be the best solution. This situation can result from such things as uncertainties in determining which pulses to fit for some of the stations or interference patterns effecting the empirical amplitudes. Under these circumstances the observer may select one of the solutions based on a single station as being a superior fit to the empirical waveforms.

### C. THE FEBRUARY 7, 1974 EARTHQUAKE

On February 7, 1974 an earthquake of local magnitude 3.0 occurred along the San Andreas Fault in Bear Valley, California and was recorded by three stations of the University of California accelerometer array. The epicenter of this event was located approximately 1.5 kms southeast of Station 4 of the array (McEvelly and Johnson, 1974). The location of this epicenter is shown in Figure 11-1 by the closed circle labeled E-1. The depth of the event was calculated to be 5.28 kms. Considering possible location errors and variations in the fault surface with depth it would appear that this event occurred on the main fault surface of the San Andreas Fault.

Probably due to the low magnitude of the earthquake, only the records of the three stations closest to the epicenter, Sites 2, 4, and 8, were of satisfactory quality for analysis. As an example of the records produced by this event the acceleration and derived velocity traces from Station 2 are displayed in Figures 11-2 and 11-3. It is apparent that the S-wave portion of the signal is dominated by a much higher frequency signal than in previously studied earthquakes (Turnbull and Battis, 1973; Turnbull and Battis, 1974). However, while the S-wave packet of the velocity waveforms examined heretofore tended to be dominated by a single pulse, it can be seen in Figure 11-3 this is not true for the February earthquake. As the isolation of a dominant pulse is essential to the successful application of the Haskell model it was decided to use only spectral methods to ascertain the earthquake source parameters of this event.

The acceleration, velocity and displacement normalized energy density spectra of the S-wave estimated by the maximum entropy method for the N45E component of Station 2 are shown in Figures 11-4 through 11-6. A highpass filter with a corner frequency of 0.8 Hz was applied to the acceleration data prior to evaluation of the spectra. In this case a spectral corner frequency of 6.0 Hz can be seen and the low frequency spectral level was

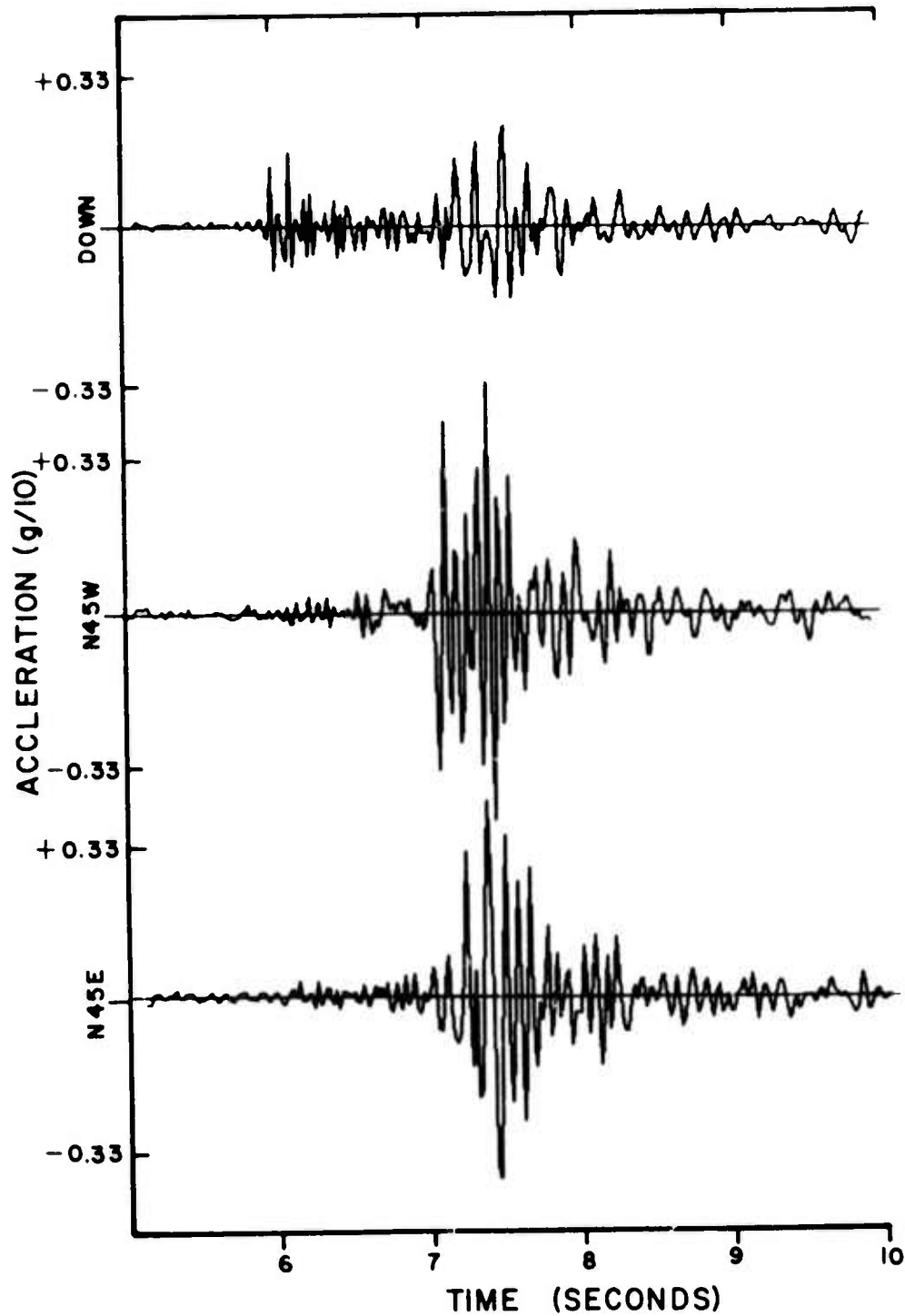


FIGURE II-2

ACCELEROGRAMS FROM STATION 2 OF THE  
FEBRUARY 7, 1974 EARTHQUAKE



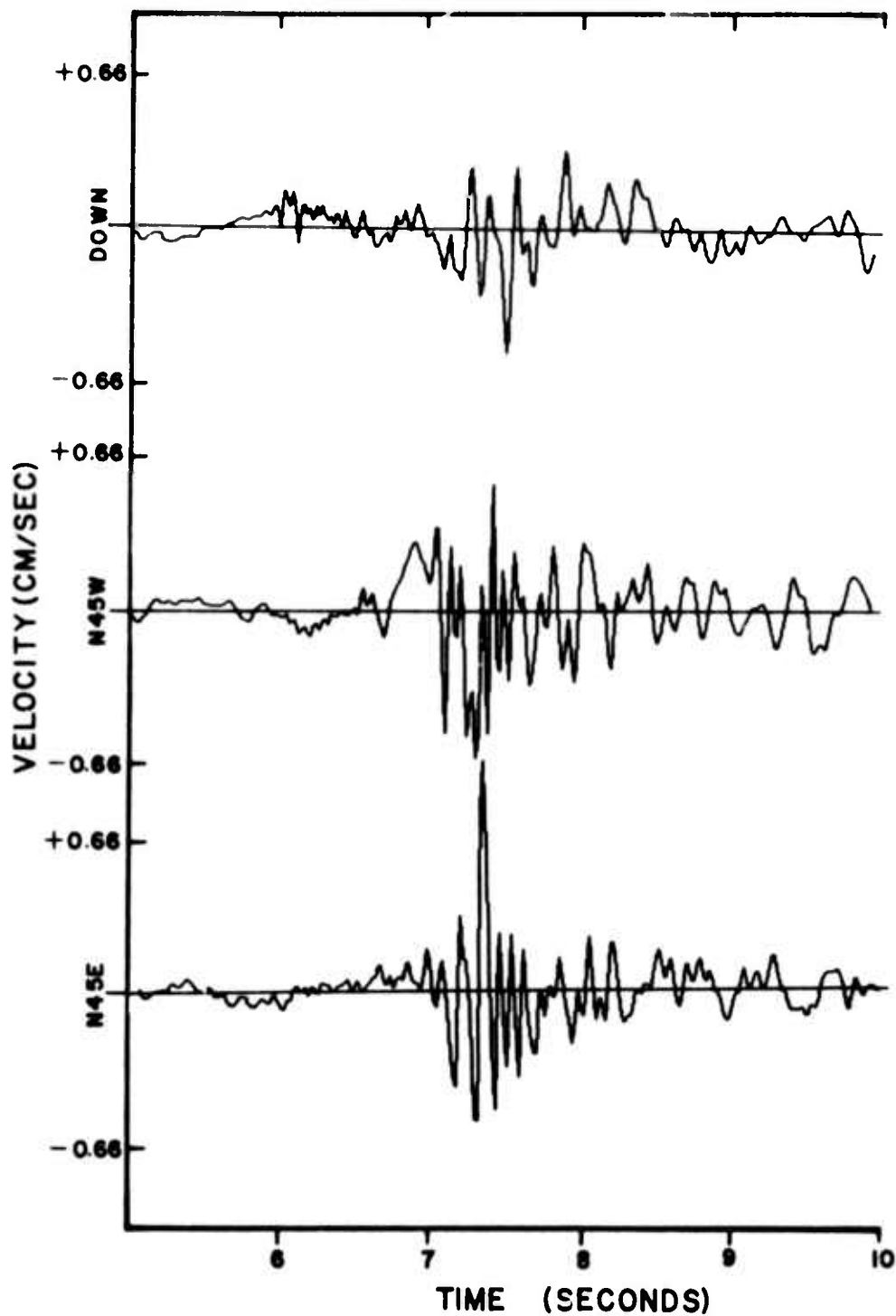
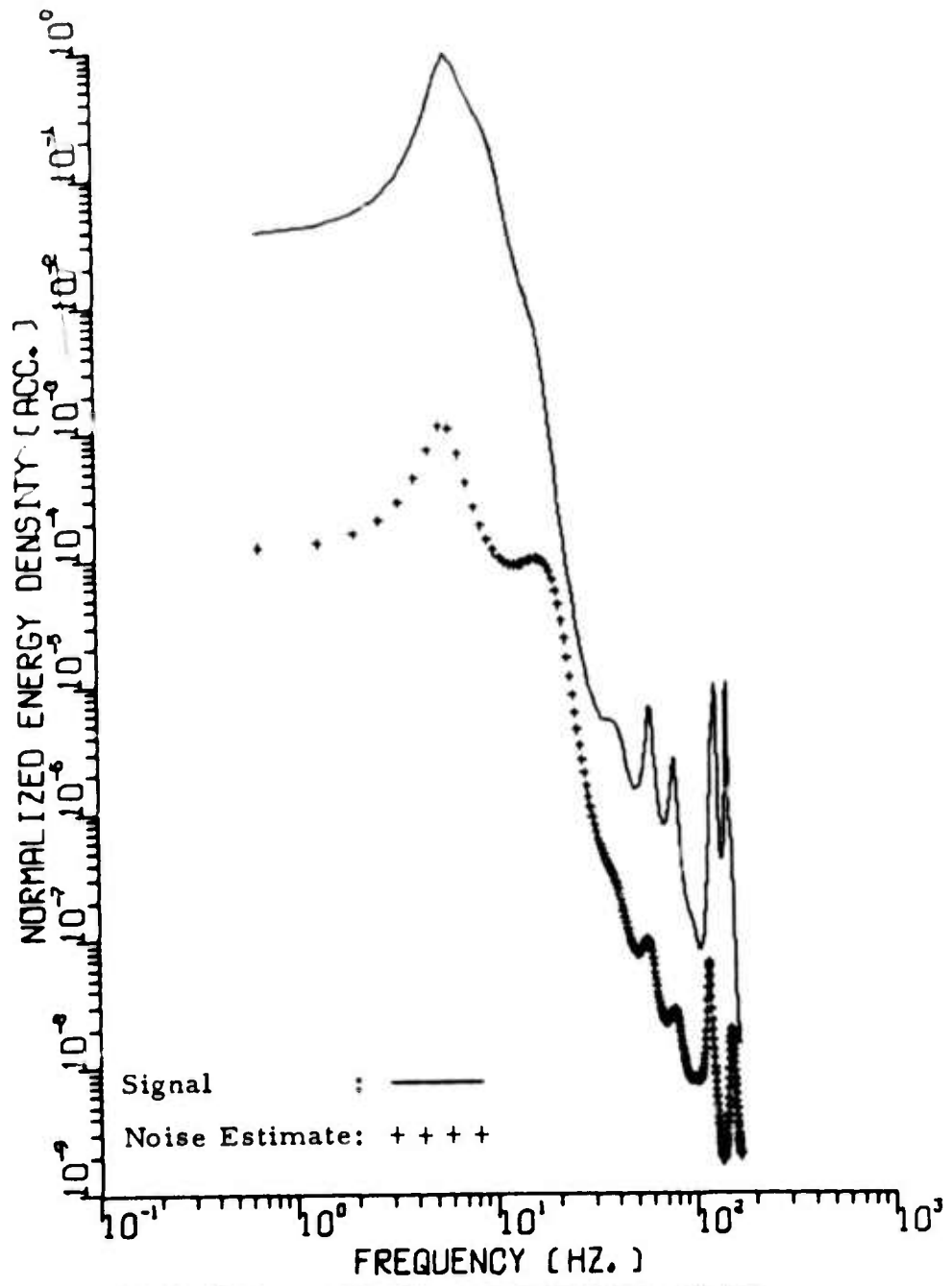


FIGURE II-3

DERIVED VELOCITY TRACES FROM STATION 2 OF  
THE FEBRUARY 7, 1974 EARTHQUAKE



2/7/74 - STAT 2 COMP NOISE / NOISE ESTIMATION COMP NOISE

FIGURE II-4

NORMALIZED ACCELERATION S-WAVE ENERGY DENSITY  
 SPECTRUM OF N45E COMPONENT OF STATION 2;  
 EARTHQUAKE OF FEBRUARY 7, 1974

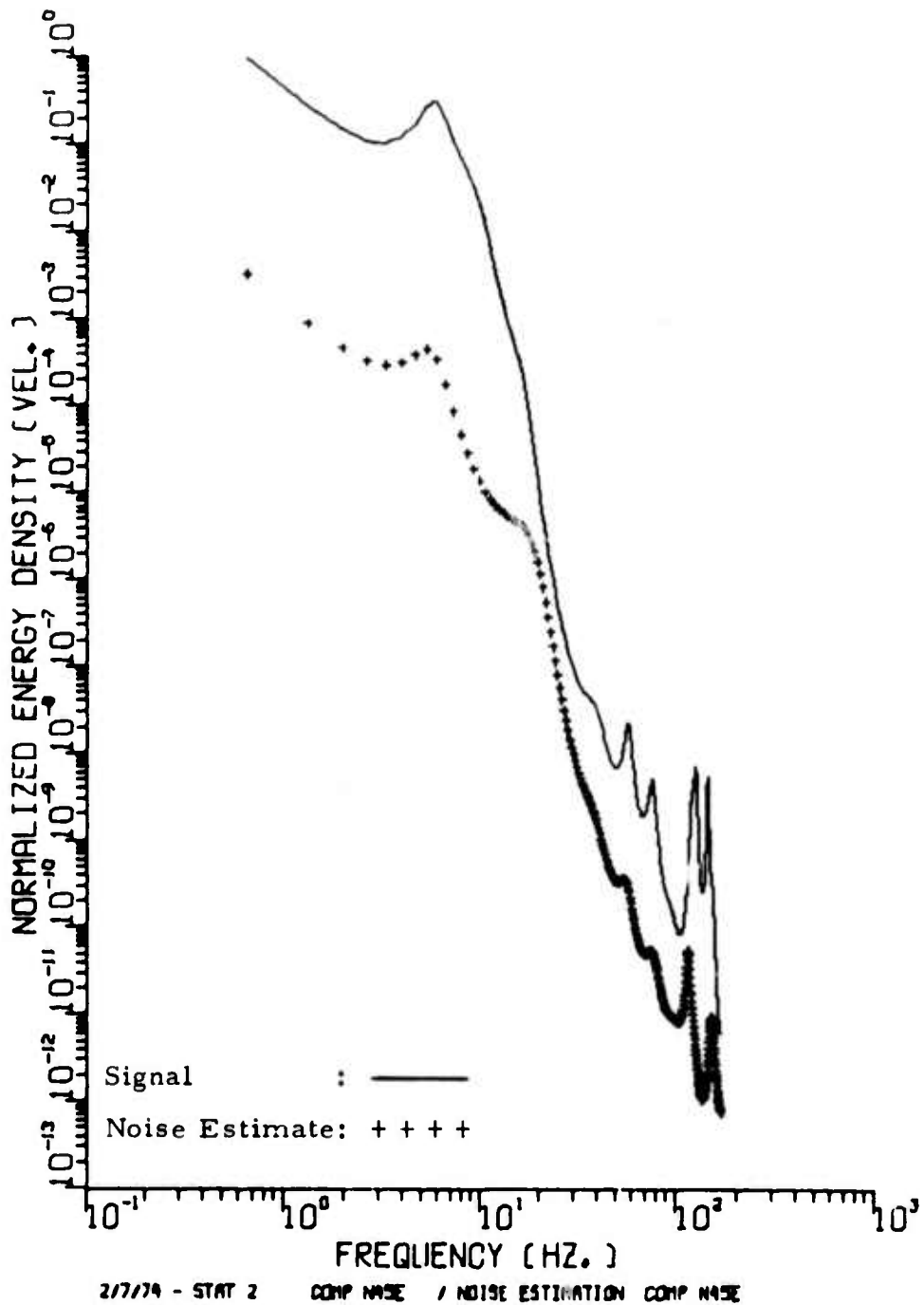


FIGURE II-5

NORMALIZED VELOCITY S-WAVE ENERGY DENSITY  
 SPECTRUM OF N45E COMPONENT OF STATION 2;  
 EARTHQUAKE OF FEBRUARY 7, 1974

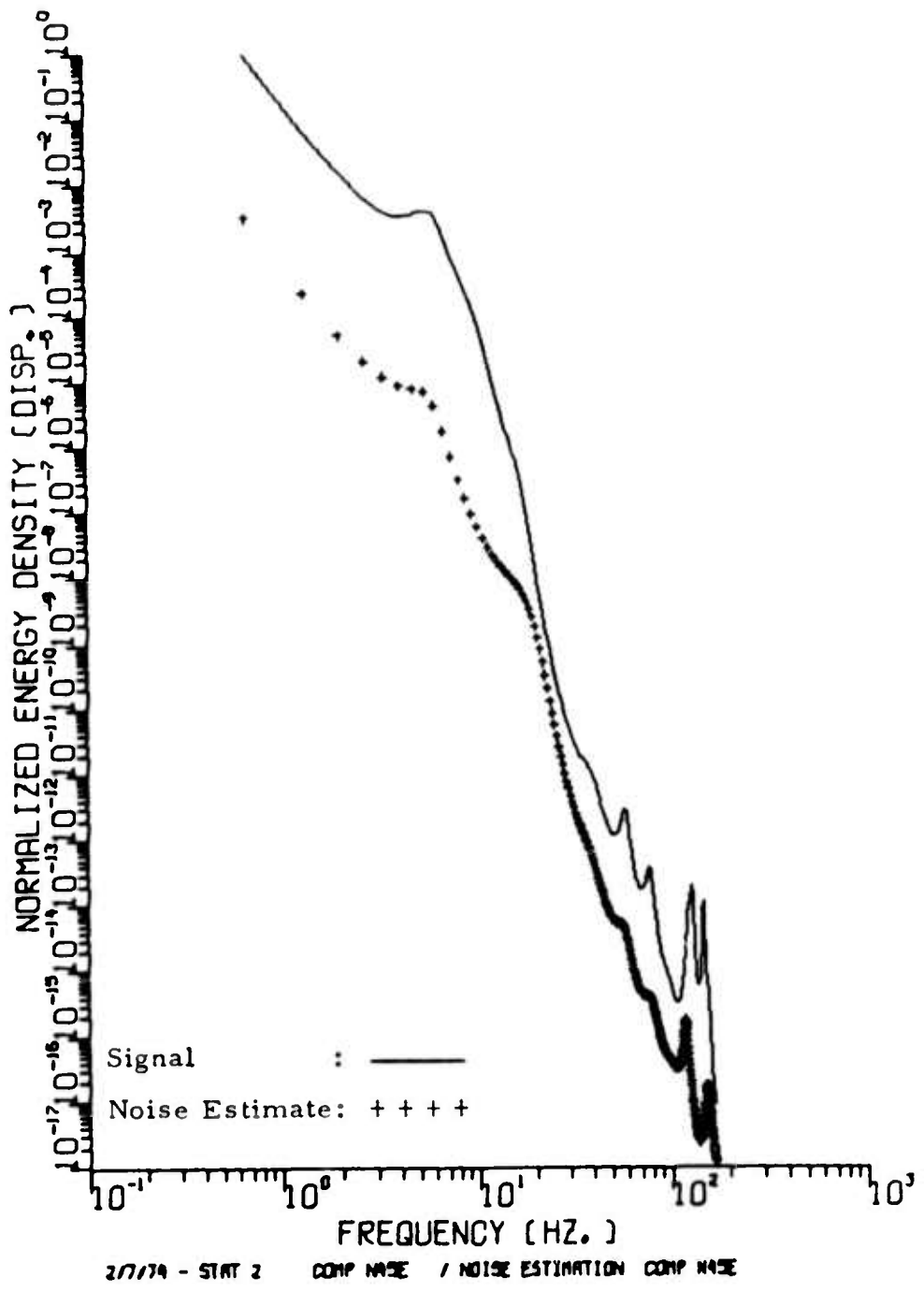


FIGURE II-6  
 NORMALIZED DISPLACEMENT S-WAVE ENERGY DENSITY  
 SPECTRUM OF N45E COMPONENT OF STATION 2;  
 EARTHQUAKE OF FEBRUARY 7, 1974

calculated as  $5.44 \times 10^{-2}$  cm·sec. Similar spectra were calculated for each of the other components recording the event.

The results of this analysis and the implied source characteristics are given in Table II-2. As would be expected for an event of this low magnitude, the seismic moments and dislocation radii are of low values. However, as this analysis does not consider factors such as attenuation, the corner frequencies given are lower bounds and thus the dislocation radii could be even smaller. However, attenuation should have only slight effect on  $\Omega_0$  and thus the estimated values of  $M_0$  are probably valid.

#### D. THE JULY 6, 1974 EARTHQUAKE

The July 6, 1974 earthquake was recorded by six stations of the Bear Valley accelerometer array. In addition this magnitude 3.2 earthquake was also recorded in the intermediate field which provided a hypocentral location and a fault plane solution for this event. The epicenter of this event is shown in Figure II-1 by the circle labeled E-2 (McEvelly and Johnson, 1974). A depth of 6.57 kms was determined for the hypocenter. Both the Haskell model and spectral estimates of the source characteristics were made for this event. The time domain process will be discussed first.

The accelerometer stations recording the event were Stations 2 and 4 which lie directly on the surface trace of the San Andreas, 3 and 6 which lie to the southeast of the fault and Sites 7 and 8 which are located on the lower velocity northeastern crustal block. The acceleration waveforms recorded at the various stations are of a highly complex nature and it is again difficult to pick what might be considered a dominant pulse for use in time domain waveform fitting in the velocity traces of most sites. As an example, the acceleration and velocity waves recorded at Stations 3, Figures II-7 and II-8, and 7, Figures II-9 and II-10, respectively are shown. In both cases the high variability of signal content from component to component make selection of a dominant pulse difficult.

TABLE II-2  
 S-WAVE SPECTRAL ESTIMATES OF SOURCE PARAMETERS  
 FEBRUARY 7, 1974 EARTHQUAKE

| Station | Component     | $f_c$ (Hz) | $\Omega_o$ (cm · sec × 10 <sup>-2</sup> ) | r (km) | $M_o$ (dyne · cm × 10 <sup>21</sup> ) |
|---------|---------------|------------|-------------------------------------------|--------|---------------------------------------|
| 2       | N45E          | 6.0        | 0.544                                     |        |                                       |
|         | N45W          | 9.3        | 0.198                                     |        |                                       |
|         | Vertical      | 6.67       | 0.117                                     |        |                                       |
|         | Total Spectra | 6.67       | 0.591                                     | 0.18   | 3.96                                  |
| 4       | N45E          | 8.67       | 0.0326                                    |        |                                       |
|         | N45W          | 9.33       | 0.0480                                    |        |                                       |
|         | Vertical      | 9.33       | 0.0470                                    |        |                                       |
|         | Total Spectra | 9.33       | 0.0747                                    | 0.13   | 0.47                                  |
| 8       | N45E          | 6.0        | 0.306                                     |        |                                       |
|         | N45W          | 6.0        | 0.363                                     |        |                                       |
|         | Vertical      | 6.0        | 0.119                                     |        |                                       |
|         | Total Spectra | 6.0        | 0.489                                     | 0.21   | 3.16                                  |

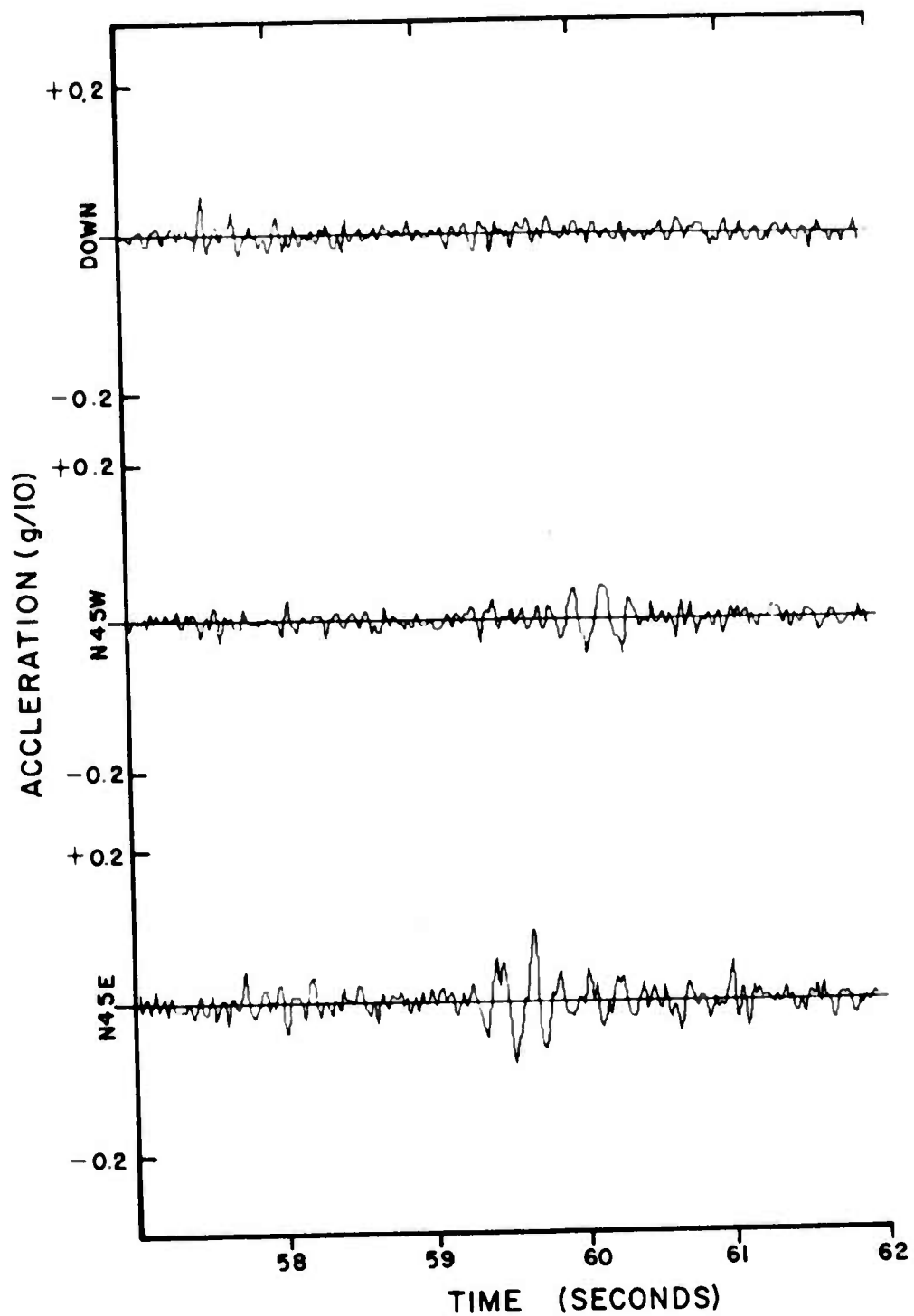


FIGURE II-7  
 ACCELEROGRAMS FROM STATION 3 FOR THE  
 JULY 6, 1974 EARTHQUAKE

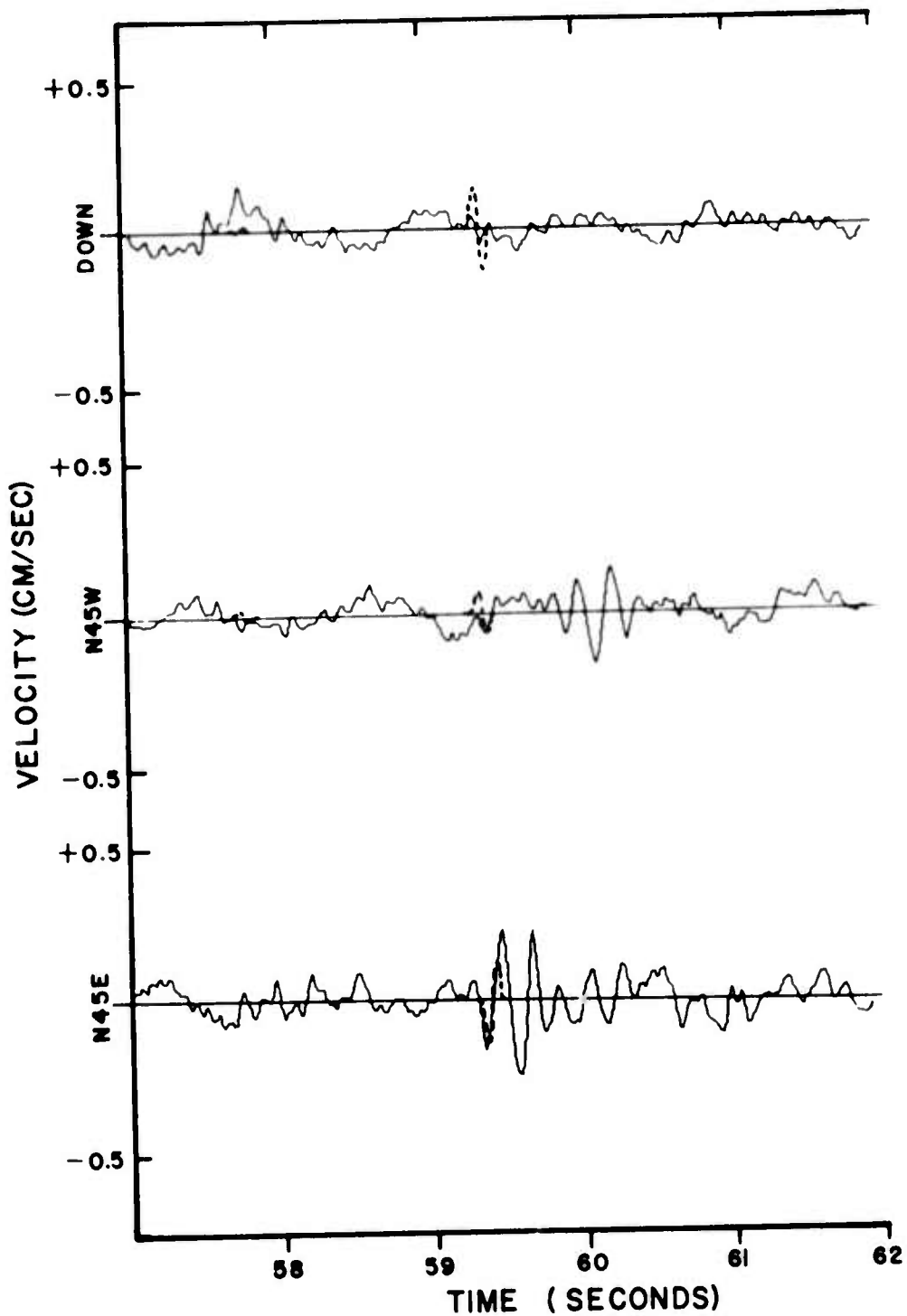


FIGURE II-8

DERIVED VELOCITY TRACES FROM STATION 3  
 FOR THE JULY 6, 1974 EARTHQUAKE  
 (DASHED LINE REPRESENTS HASKELL MODEL SOLUTION)



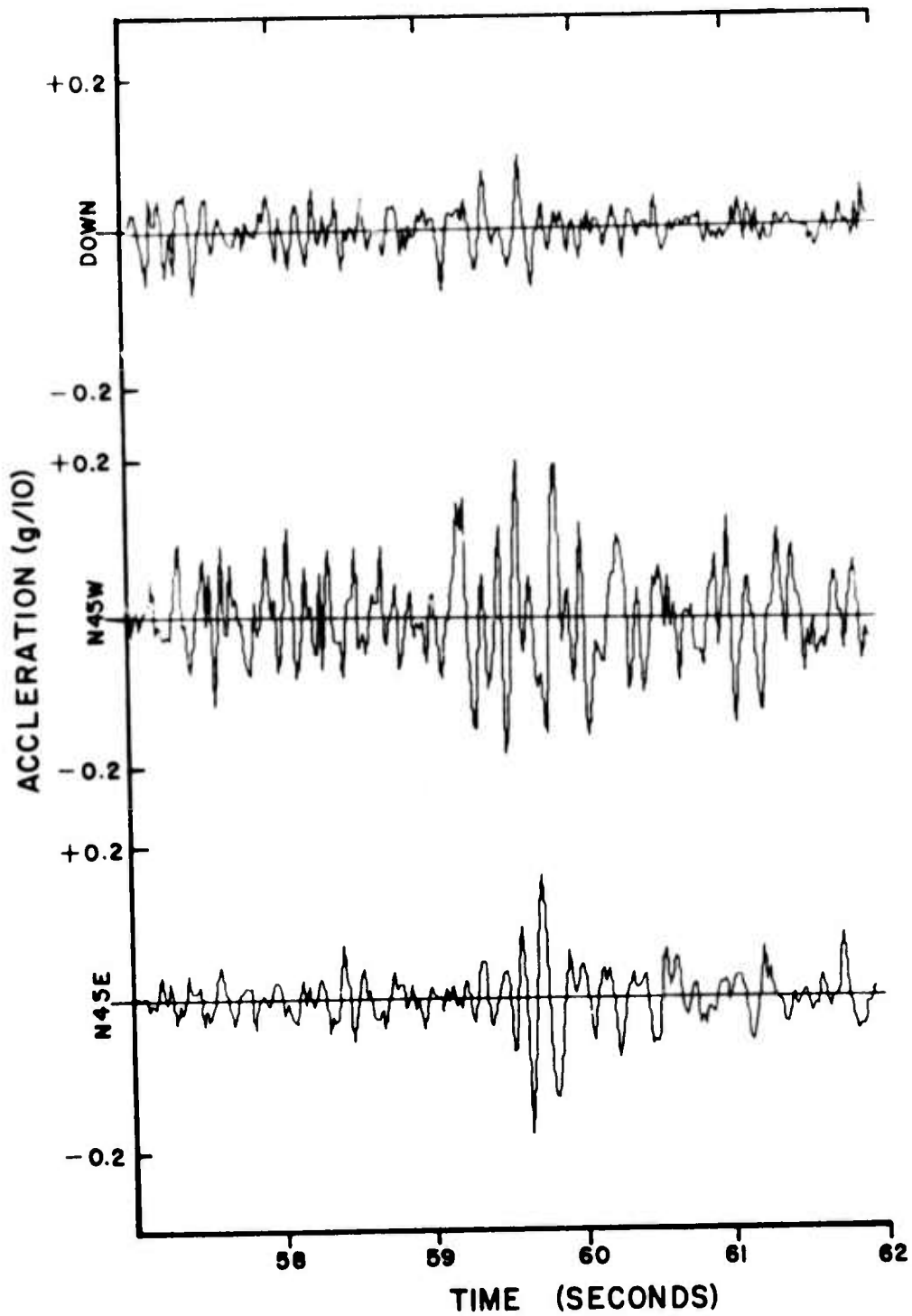


FIGURE II-9

ACCELEROGRAMS FROM STATION 7 FOR THE  
JULY 6, 1974 EARTHQUAKE

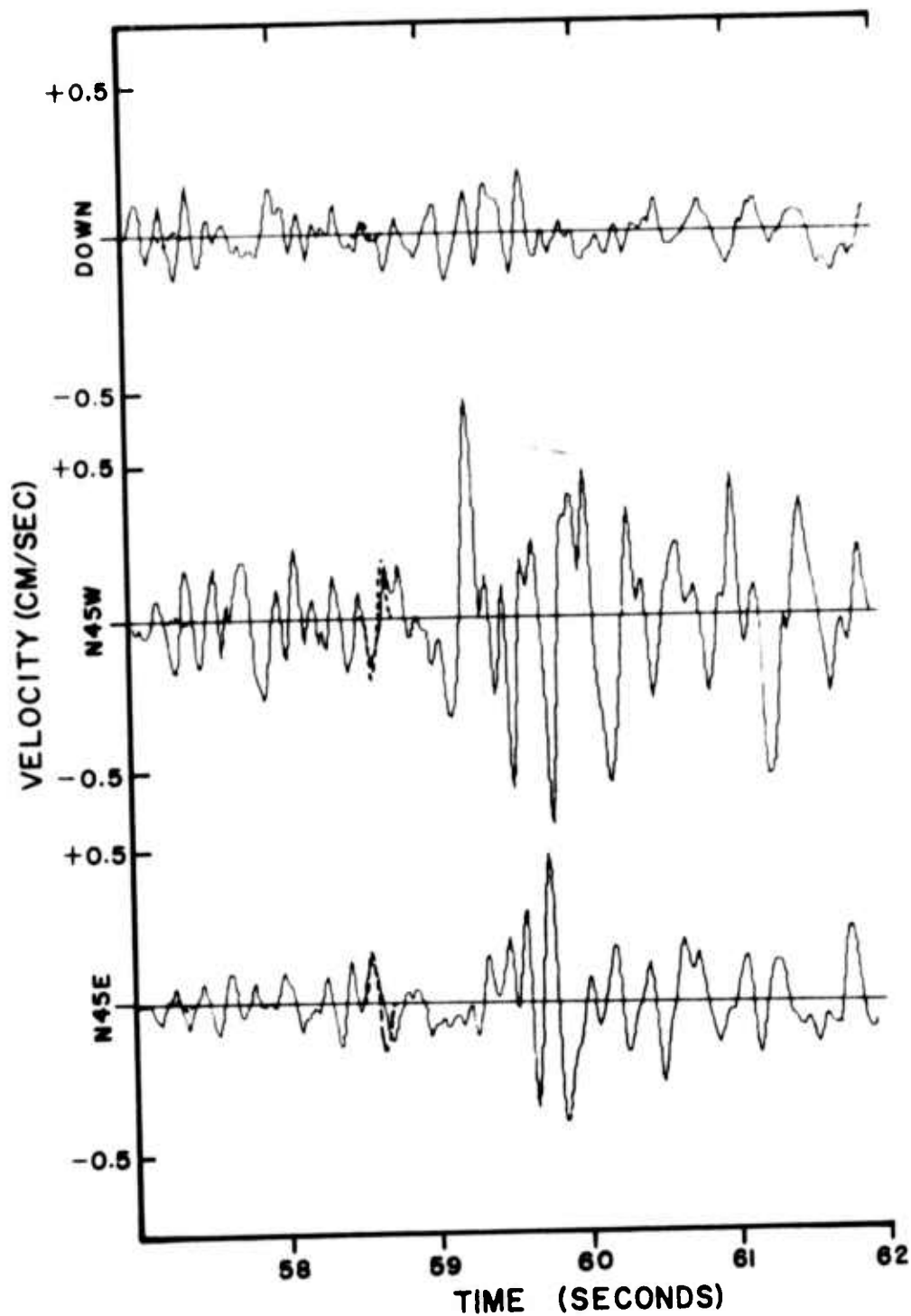


FIGURE II-10

DERIVED VELOCITY TRACES FROM STATION 7  
 FOR THE JULY 6, 1974 EARTHQUAKE  
 (DASHED LINE REPRESENTS HASKELL MODEL SOLUTION)

To overcome the difficulty, the whole space velocities calculated previously were used to determine approximate P- and S-wave arrival times. The velocity of the crustal block on which the station was located was used for each station. For Stations 2 and 4, those lying directly on the fault trace, times based on each model and an average velocity were used. As most stations recorded a strong P-arrival on at least one component, it was apparent that errors of as much as one second existed in these calculations. For this reason the dominant pulse used for fitting with the Haskell model was selected by using the S-P times to locate the approximate S-arrival time and then picking the nearest apparent dominant pulse.

As previously explained, once the pulses to be used in the fitting process are selected, unit dislocation waveforms for each station are calculated using as many external restrictions as possible. In this case the hypocentral location and a fault plane solution have been determined for the source from intermediate field data (McEvelly and Johnson, 1974). The fault plane solution defined a fault striking N40W and nearly vertical in dip. However, this was taken as the strike direction solely because it parallels the San Andreas surface trace in the vicinity of the epicenter. The auxiliary plane of N50E could also define the fault and thus both planes were used to produce theoretical waveforms by Haskell's source model.

Using least squared error fitting on the amplitudes of the selected pulses from all stations simultaneously and separately, the initial source structures were perturbed to produce 7 solutions defined by the minimum residual over all test cases for each set of fittings. Each solution was then used to produce theoretical waveforms at every station which were judged for overall 'goodness of fit'. Of these solutions for the July earthquake the one determined by waveform fitting at Site 6 separately was selected. At best, the quality of this fit can be considered marginal, in general being poorer than the fits shown in Figures II-8 and II-10 for Stations 3 and 7, respectively.

From Figures II-8 and II-10 it would appear that the modeled pulse duration is less than the observed indicating error in the calculated fault length, rise time or rupture velocity. At other stations the theoretical duration is closer to the observed value. However, this may indicate that these parameters are in error to some degree. The source parameters are given in Table II-3. That the Haskell model could not produce a satisfactory solution at all stations is probably the result of several problems which will be discussed later in this report.

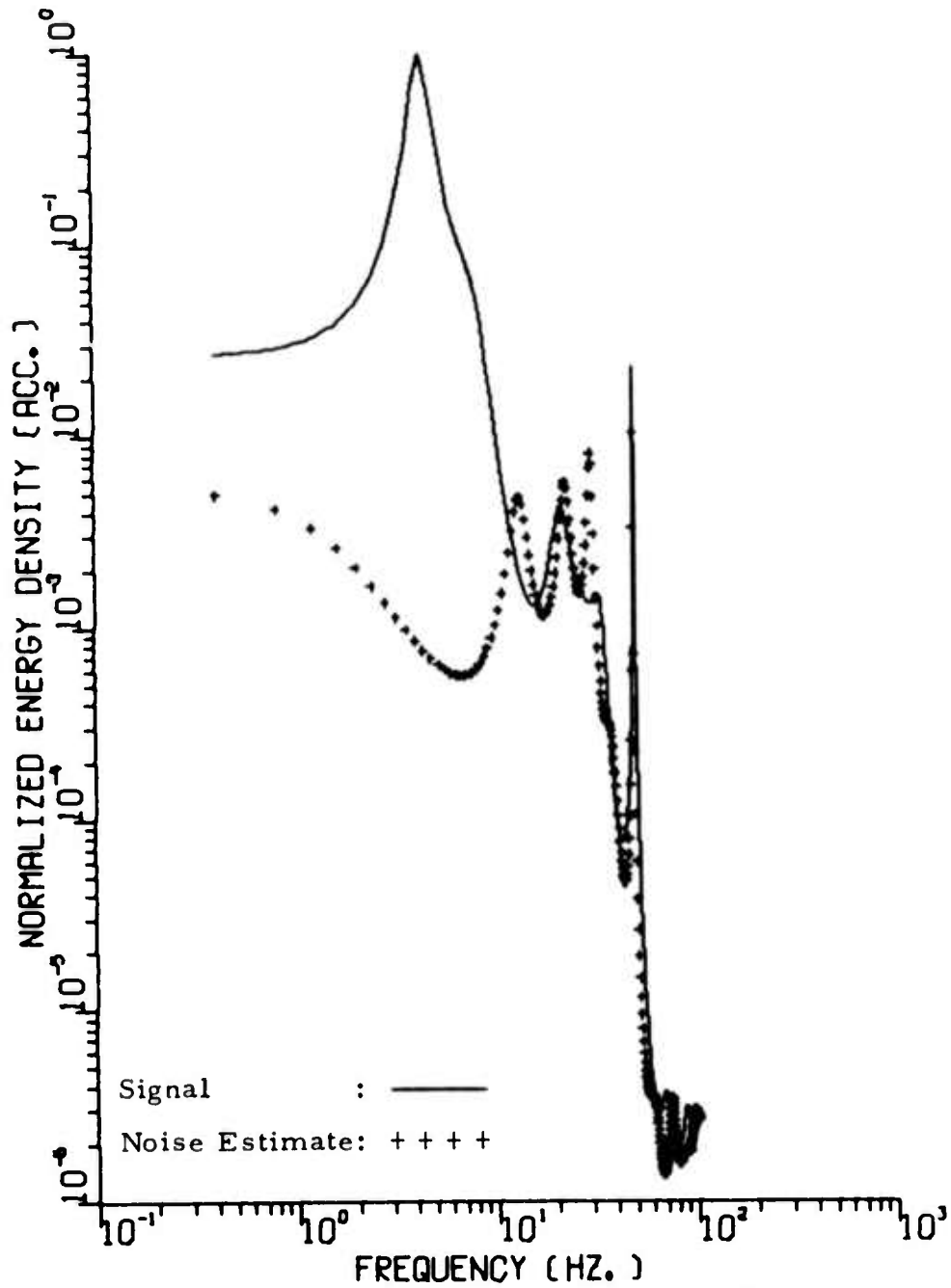
In addition to the time domain modeling of the earthquake source, spectral estimates of the source characteristics were also made for this event. As is apparent on consideration of the empirical velocity waveforms in Figures II-8 and II-10 the spectra calculated for each station are highly variable and no single set of spectra could be considered typical of this event. However, the S-wave spectra of the N45E component at Station 8 are shown in Figures II-11 to II-13. The corner frequency,  $f_c$ , for this component is somewhat lower than for other stations but appears as a well defined peak in the velocity spectra at about 4 Hz. The results for all stations are shown in Table II-4. As with the February earthquake the relatively high corner frequency, indicating small fault area, and low seismic moments calculated for this event are as expected from a low local magnitude earthquake.

#### E. DISCUSSION OF RESULTS

While the general levels of seismic moments calculated for both the February and July earthquakes are reasonable when compared to the seismic moments and local magnitudes of other events studied from the near-zone, as shown in Figure II-14, it is apparent that a high level of variation in spectrally determined seismic moment exists between stations of the near-field array for each event. While this is in part accounted for by variations in the seismic source radiation patterns, a comparison of results studied in

TABLE II-3  
 BEAR VALLEY EARTHQUAKE OF JULY 6, 1974  
 HASKELL SOURCE MODEL SOLUTION

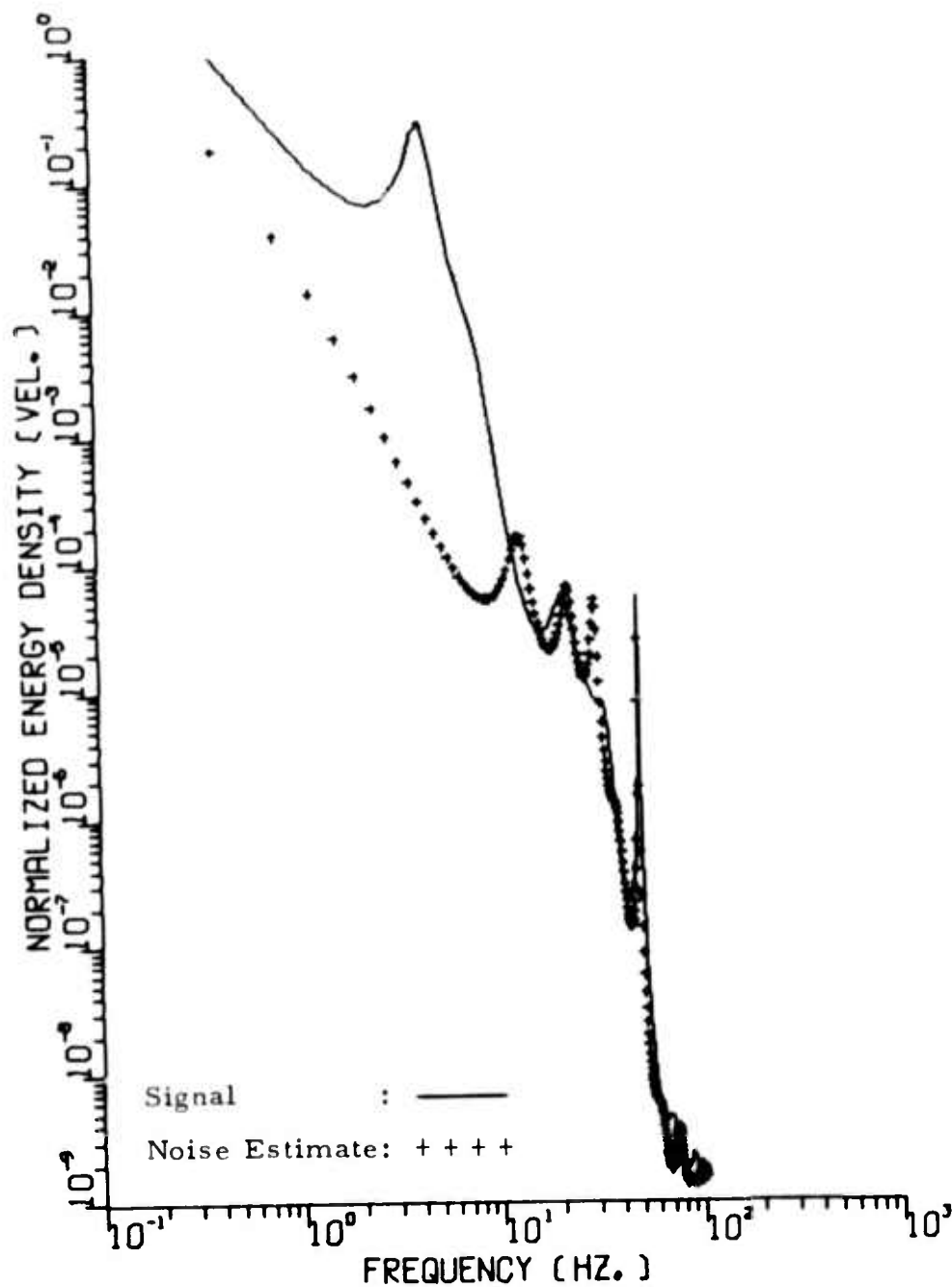
|                   |   |                                      |                             |
|-------------------|---|--------------------------------------|-----------------------------|
| Epicenter         | : | 36°34.1'N                            |                             |
| Depth             | : | 121°10.1'W                           |                             |
| Velocities        | : | Southwest Crustal Stations:          | $V_p = 5.76 \text{ km/sec}$ |
|                   |   |                                      | $V_s = 3.32 \text{ km/sec}$ |
|                   |   | Northeast Crustal Stations:          | $V_p = 4.56 \text{ km/sec}$ |
|                   |   |                                      | $V_s = 2.60 \text{ km/sec}$ |
| Strike Angle      | : | N40W                                 |                             |
| Dip Angle         | : | 80° to NE                            |                             |
| Fault Dimensions: |   | Length = 0.18 km                     |                             |
|                   |   | Width = 0.18 km                      |                             |
| Rise Time         | : | 0.02 sec                             |                             |
| Rupture Velocity  | : | 2.5 km/sec                           |                             |
| Dislocations      | : | Strike-Slip:                         | 6.24 cm                     |
|                   |   | Dip-Slip :                           | 5.84 cm                     |
| Seismic Moment    | : | $8.3 \times 10^{20} \text{ dyne cm}$ |                             |



7/6/74 - STAT 8 COMP MADE / NOISE ESTIMATION COMP MADE

FIGURE II-11

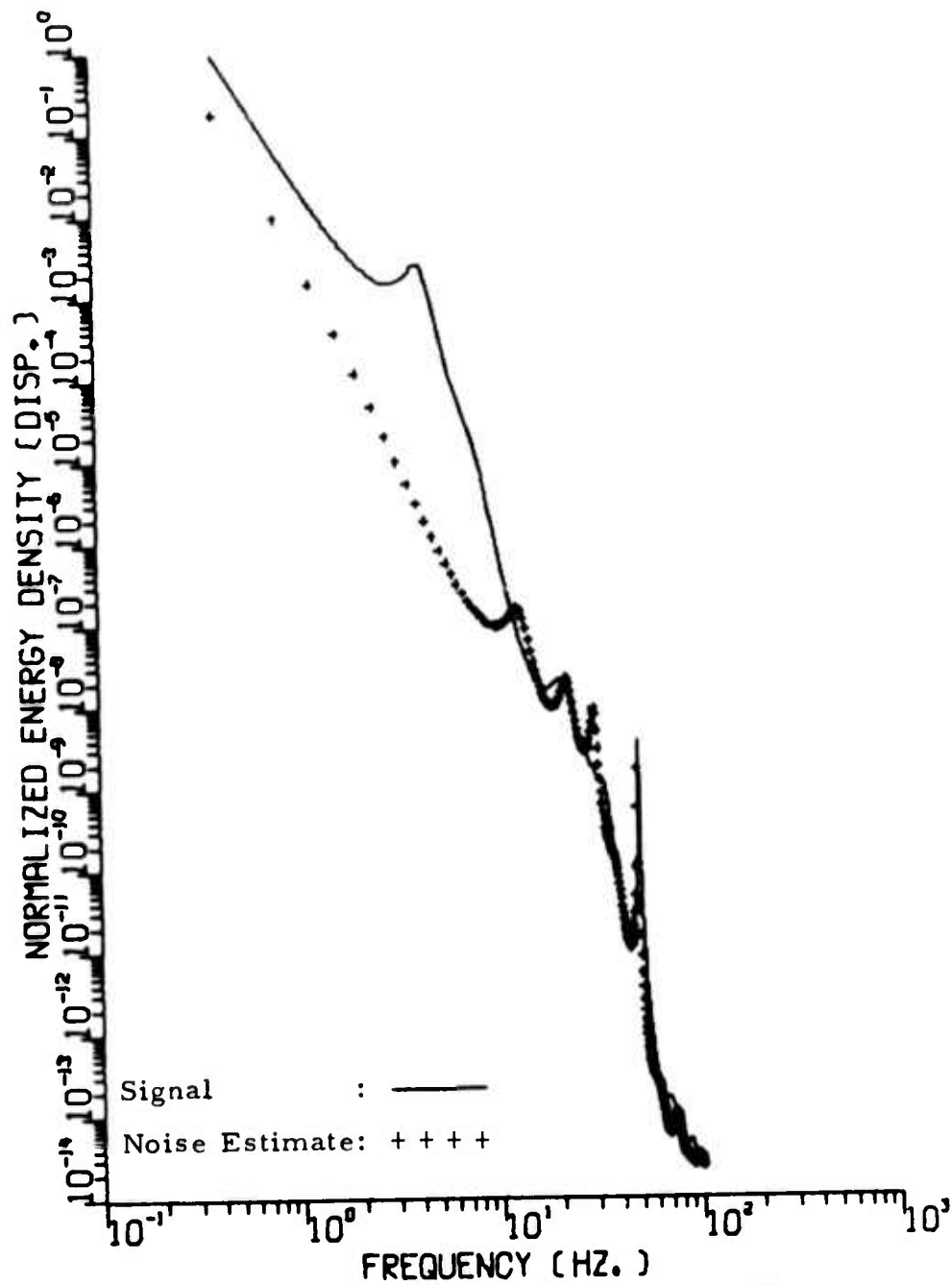
NORMALIZED ACCELERATION S-WAVE ENERGY DENSITY  
SPECTRUM FOR N45E COMPONENT OF STATION 8;  
EARTHQUAKE OF JULY 6, 1974



7/6/74 - STAT 8 COMP MADE / NOISE ESTIMATION COMP MADE

FIGURE II-12

NORMALIZED VELOCITY S-WAVE ENERGY DENSITY  
SPECTRUM FOR N45E COMPONENT OF STATION 8;  
EARTHQUAKE OF JULY 6, 1974



7/6/74 - STMT 8 COMP WAVE / NOISE ESTIMATION COMP WAVE

FIGURE II-13

NORMALIZED DISPLACEMENT S-WAVE ENERGY DENSITY  
 SPECTRUM FOR N45E COMPONENT OF STATION 8;  
 EARTHQUAKE OF JULY 6, 1974



TABLE II-4  
 S-WAVE SPECTRAL ESTIMATES OF SOURCE PARAMETERS  
 JULY 6, 1974 EARTHQUAKE

| Station | Component     | $f_c$ (Hz) | $\Omega_0$ (cm · sec × 10 <sup>-2</sup> ) | r (km) | $M_0$ (dyne · cm × 10 <sup>21</sup> ) |
|---------|---------------|------------|-------------------------------------------|--------|---------------------------------------|
| 2       | N45E          | 8.4        | 0.25                                      | 0.17   | 4.4                                   |
|         | N45W          | 6.0        | 0.41                                      |        |                                       |
|         | Vertical      | 7.6        | 0.06                                      |        |                                       |
|         | Total Spectra | 7.6        | 0.48                                      |        |                                       |
| 3       | N45E          | 4.0        | 0.24                                      | 0.29   | 4.4                                   |
|         | N45W          | 4.4        | 0.12                                      |        |                                       |
|         | Vertical      | ?          | 0.01                                      |        |                                       |
|         | Total Spectra | 4.4        | 0.27                                      |        |                                       |
| 4       | N45E          | 5.6        | 0.12                                      | 0.23   | 2.1                                   |
|         | N45W          | 6.4        | 0.09                                      |        |                                       |
|         | Vertical      | 5.2        | 0.08                                      |        |                                       |
|         | Total Spectra | 5.6        | 0.17                                      |        |                                       |
| 6       | N45E          | 11.2       | 0.02                                      | 0.20   | 1.2                                   |
|         | N45W          | 6.4        | 0.06                                      |        |                                       |
|         | Vertical      | 4.8        | 0.08                                      |        |                                       |
|         | Total Spectra | 6.4        | 0.10                                      |        |                                       |
| 7       | N45E          | 5.4        | 0.20                                      | 0.24   | 3.1                                   |
|         | N45W          | 8.4        | 0.13                                      |        |                                       |
|         | Vertical      | 5.2        | 0.13                                      |        |                                       |
|         | Total Spectra | 5.4        | 0.27                                      |        |                                       |
| 8       | N45E          | 4.4        | 0.62                                      | 0.29   | 9.0                                   |
|         | N45W          | 4.0        | 0.37                                      |        |                                       |
|         | Vertical      | 6.8        | 0.06                                      |        |                                       |
|         | Total Spectra | 4.4        | 0.72                                      |        |                                       |

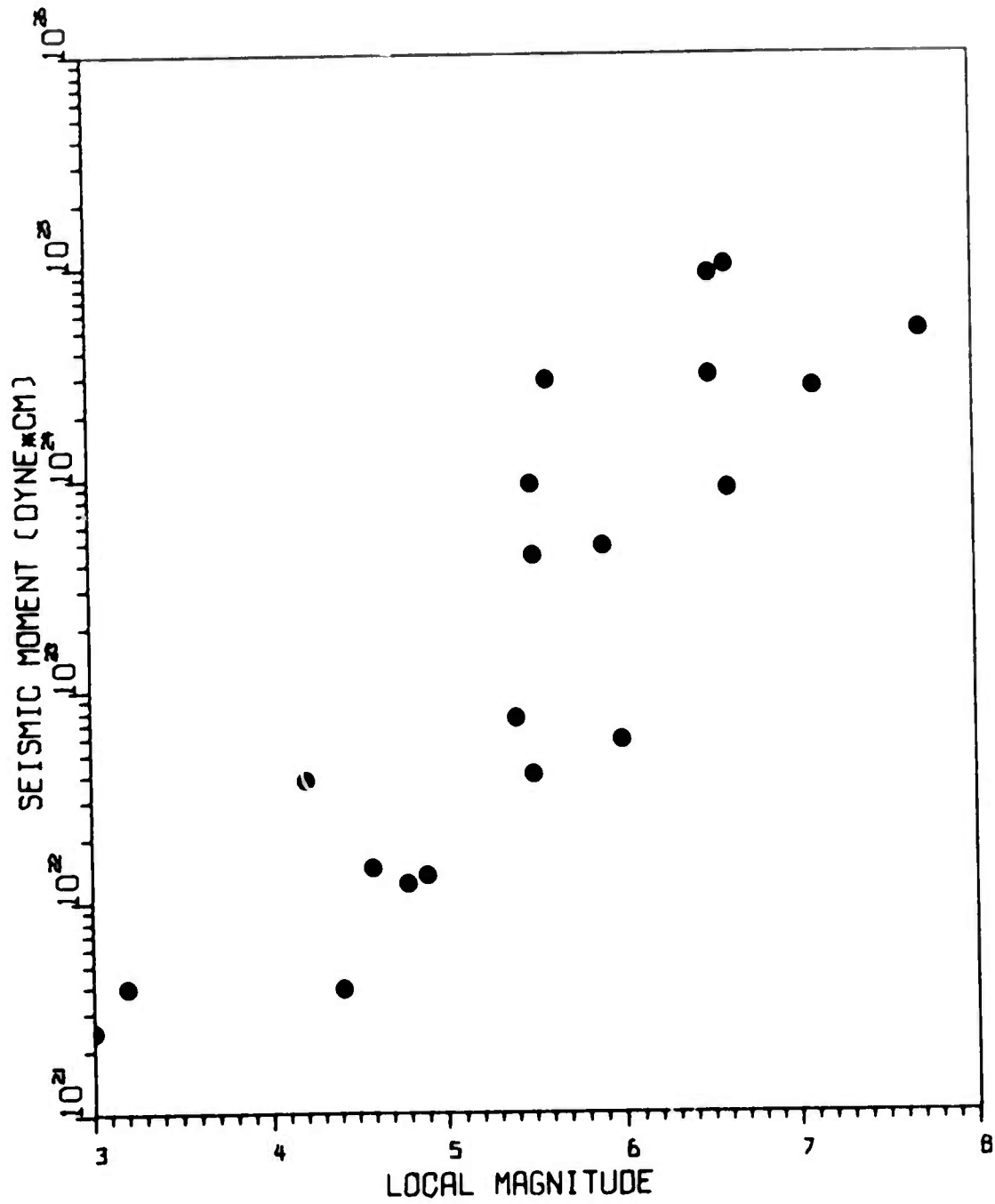


FIGURE II-14  
 OBSERVED LOCAL MAGNITUDES VERSUS NEAR-FIELD  
 SPECTRAL SEISMIC MOMENTS

this report and of the June 22, 1973 Bear Valley earthquake (Turnbull, et al., 1975; Turnbull et al., 1974b) indicate that the transmission and site effects may be more important in causing these variations.

In Table II-5 the seismic moments calculated by spectral means for the three Bear Valley earthquakes are shown for each station recording an event. It would appear from this data that the seismic moment found at each site is dependent on location of the site. The average moment for Stations 7 and 8, which are located to the northeast of the San Andreas Fault, tend to be higher than for Stations 2 and 4 which lie on the fault and Stations 3 and 6, which lie to the southwest, seem to have the lowest moments. McEvelly and Johnson (1974) have found a similar correlation between seismic moment for a given event and site location. Based on their data they find a factor of between 3 and 4 difference between stations to the southwest and to the northeast of the fault with the stations on the fault having a seismic moment intermediate between these stations. In addition, however, it would appear from Table II-5 that even for stations on the same structure significant variations occur. This can be seen in the consistent lower moment estimate at Station 4 as compared to Station 2.

Systematic variations in the acceleration amplitudes, as indicated by the variations in seismic moment, can explain the difficulty of the Haskell model to fit the July 6, 1974 earthquake. First, using multiple station fitting, it is apparent that one is attempting to find the fault whose radiation pattern can model the empirical amplitude pattern. However, if the empirical data is significantly altered by means external to the source, as appears to be the case at Bear Valley, then it is highly unlikely that a source model can reproduce these effects with a 'reasonable' earthquake source. Secondly, the complexities of the structure produce anomalous phases which reduce the dominance of any single pulse in the empirical wavetrain. Under these conditions it is highly unlikely that the same arrival will be selected at

TABLE II-5  
SEISMIC MOMENTS FOR EACH EVENT AT BEAR VALLEY  
AS CALCULATED AT EACH STATION

|           | 6/22/73              | 2/7/74               | 7/6/74               |
|-----------|----------------------|----------------------|----------------------|
| Station 2 | $1.8 \times 10^{22}$ | $4.0 \times 10^{21}$ | $4.4 \times 10^{21}$ |
| Station 3 | --                   | --                   | $4.4 \times 10^{21}$ |
| Station 4 | $6.5 \times 10^{21}$ | $4.7 \times 10^{20}$ | $2.1 \times 10^{21}$ |
| Station 6 | --                   | --                   | $1.2 \times 10^{21}$ |
| Station 7 | $5.4 \times 10^{22}$ | --                   | $3.1 \times 10^{21}$ |
| Station 8 | $7.5 \times 10^{22}$ | $3.2 \times 10^{21}$ | $9 \times 10^{21}$   |

all stations used in the fitting process. This in turn results in incorrect phase and amplitude relations between the stations making a 'good fit' within such restrictions as the fault plane solution nearly impossible. Thus, it can be concluded that the failure of the Haskell model in this case is not failure of the source model but rather of its inability to cope with transmission effects.

It is also possible that these transmission or site effects can explain the apparent disagreement of seismic moments calculated for the June 22, 1973 earthquake from near, intermediate, and far-field data. Using Haskell's model a seismic moment of  $1.2 \times 10^{23}$  dyne·cm was calculated for this event. However, moments of much lower magnitude were found in the intermediate and far-field. Smith (1973) calculated an intermediate zone moment of  $2 \times 10^{22}$  dyne·cm while the best far-field estimates ranged between 0.7 and  $2 \times 10^{22}$  dyne·cm (D. Sun, personal communication, 1975). If one assumes that the variations of amplitude result from site amplifications for stations on the fault and to the northeast of it, then using McEvelly and Johnson's correction factor, the recorded amplitudes of Stations 7 and 8 should be reduced by a factor of about 3.5. Reducing these amplitudes will reduce the modeled dislocations and seismic moment an equal amount. Thus a seismic moment of  $3.4 \times 10^{22}$  dyne·cm would be obtained, in much better agreement with the intermediate and far-field results for this earthquake.

## SECTION III FAR-FIELD SOURCE STUDIES

### A. INTRODUCTION

For the past several months, the examination of far-field spectra for source characteristics has been conducted along several lines of investigation. The investigation of two California earthquakes (22 June 1973 and 28 November 1974) using far-field surface wave data has been extended from the last study (Turnbull, et al., 1975). In Subsection B, we discuss the effect a new source region structure (McEvelly, 1975) would have on the source mechanism solution. The investigation of theoretical higher mode spectra has also been continued, with comprehensive spectral displays produced and analyzed for two different representative earth structures in Subsection C. Finally, in Subsection D, we present preliminary results on the investigation of a swarm of earthquakes that occurred in Sinkiang, China in 1974.

### B. CONTINUED EVALUATION OF THE FAR-FIELD SOURCE MECHANISM FOR TWO CALIFORNIA EARTHQUAKES

In previous work (Turnbull, et al., 1975), it was felt that one of the limitations to the far-field solutions for these events was knowledge of the source region structure. From a field survey conducted by McEvelly (1975), we were able to obtain better structure estimates for both sides of the San Andreas fault in the Bear Valley region. This structure is listed in Table III-1, with the dispersion curves for both sides of the fault displayed in Appendix A. The major difference between the structure on each side of the fault, of course, is the higher velocity layers in the structure on the southwest side.

TABLE III-1  
BEAR VALLEY REGION STRUCTURE (McEVILLY, 1975)

| Depth<br>h                                                                                                                                             | Layer<br>Thickness<br>$\Delta h$ | Northeast Side of Fault |       |       | Southwest Side of Fault |       |       |
|--------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------|-------------------------|-------|-------|-------------------------|-------|-------|
|                                                                                                                                                        |                                  | $\rho$                  | $V_p$ | $V_s$ | $\rho$                  | $V_p$ | $V_s$ |
| 0.6                                                                                                                                                    | 0.6                              | 2.0                     | 2.38  | 1.51  | 2.7                     | 4.25  | 2.46  |
| 2.5                                                                                                                                                    | 1.9                              | 2.1                     | 3.04  | 1.76  | 2.7                     | 5.2   | 3.0   |
| 5.5                                                                                                                                                    | 3.0                              | 2.7                     | 5.88  | 3.30  | 2.74                    | 6.34  | 3.66  |
| 10.0                                                                                                                                                   | 4.5                              | 2.75                    | 4.84  | 2.80  | 2.74                    | 5.96  | 3.45  |
| 15.5                                                                                                                                                   | 5.5                              | 2.75                    | 4.98  | 2.88  | 2.8                     | 6.94  | 4.0   |
| 19.3                                                                                                                                                   | 3.8                              | 2.8                     | 6.02  | 3.48  | 2.8                     | 6.67  | 3.86  |
| 21.0                                                                                                                                                   | 1.7                              | 2.9                     | 6.55  | 3.79  | 3.0                     | 6.55  | 3.78  |
| 25.0                                                                                                                                                   | 4.0                              | 3.0                     | 6.86  | 3.97  | 3.0                     | 6.55  | 3.78  |
| 50.0                                                                                                                                                   | 25.0                             | 3.32                    | 8.2   | 4.65  | 3.32                    | 8.2   | 4.65  |
| <div style="display: flex; justify-content: space-between;"> <span>↓</span> <span>Merge With Gutenberg-Bullen Earth Model</span> <span>↓</span> </div> |                                  |                         |       |       |                         |       |       |

Another way to determine the impact the structural differences have on the observed spectra is to generate theoretical spectra using a source imbedded in these structures. Using the bodywave source mechanisms for these two events, spectral variation with respect to depth and radiation patterns of a particular depth were generated. The two source mechanisms are listed below in Table III-2.

TABLE III-2  
SOURCE PARAMETERS FOR THE TWO CALIFORNIA EVENTS

| Event Description           | Depth - h<br>(km) | Dip - $\delta$<br>(deg) | Slip - $\lambda$<br>(deg) | Strike - $\theta$<br>N (deg) E |
|-----------------------------|-------------------|-------------------------|---------------------------|--------------------------------|
| Bear Valley 6-22-73         | 10.25             | 70                      | 30                        | 135                            |
| Central California 11-28-74 | 4                 | 90                      | 0                         | 35                             |

These spectra and radiation patterns are displayed for both events in Appendix B. The major conclusions that can be drawn from comparisons between the two structural responses are:

- From the displays of Rayleigh and Love wave amplitude spectra as a function of depth we see that, for the appropriate source depth, and for both events, the spectral levels for the northeast structure are approximately an order of magnitude higher than those levels generated by the southwest side.
- From the Rayleigh and Love wave radiation patterns for both events generated at 20 seconds period, we see that the patterns have shapes that are structure dependent as well as having different spectral levels.



With these structural properties firmly in mind, we attempted to 'fit' the observed spectra in the same manner as in previous analysis of these events (Turnbull, et al., 1975). The stations available for the Bear Valley event of 22 June 1973 are displayed in Figure III-1, with the Rayleigh wave traces used from OGD and ALQ, and the Love wave trace from LASA. In the spectral fitting process, no absolute minimum residual was observed, but a solution was obtained by picking the local minimum residual. Because the stations lie to the east of the fault, the northeast structure was used. The solution was found to be close to the bodywave mechanism, with a depth of 6 km, dip of  $80^{\circ}$ , slip of  $0^{\circ}$ , strike of  $N175^{\circ}E$ , and a seismic moment of  $0.9 \times 10^{22}$  dyne-cm. This moment is about an order of magnitude less than that obtained by fitting near-field acceleration data, and approximately the same as that obtained previously using the HelMBERGER structure.

Analysis of the central California event of 28 November 1974 presented a more complex situation. The stations available are displayed in Figure III-2, with the Rayleigh wave traces used from NORSAR, TLO, ALPA, ZLP, and KIP, and the Love wave trace from LASA. With stations on both sides of the fault, a problem arises as to which source region structure is appropriate. An exhaustive approach was applied to this situation, with solutions obtained by using the northeast model only, the southwest model only, and for the first time, a combination of the two structures. The solutions obtained for the different combinations of stations and structures based on the minimum residual criteria and the distribution of minimum residual criteria are given in Tables III-3 and III-4, respectively. All of the solutions yield a similar source mechanism; a vertical strike-slip fault with a strike direction of  $N45^{\circ}E$ . This agrees very well with the bodywave solution. However, except for the solution obtained by fitting the three stations in the west with the southwest model, all of the focal depth estimates were too deep.

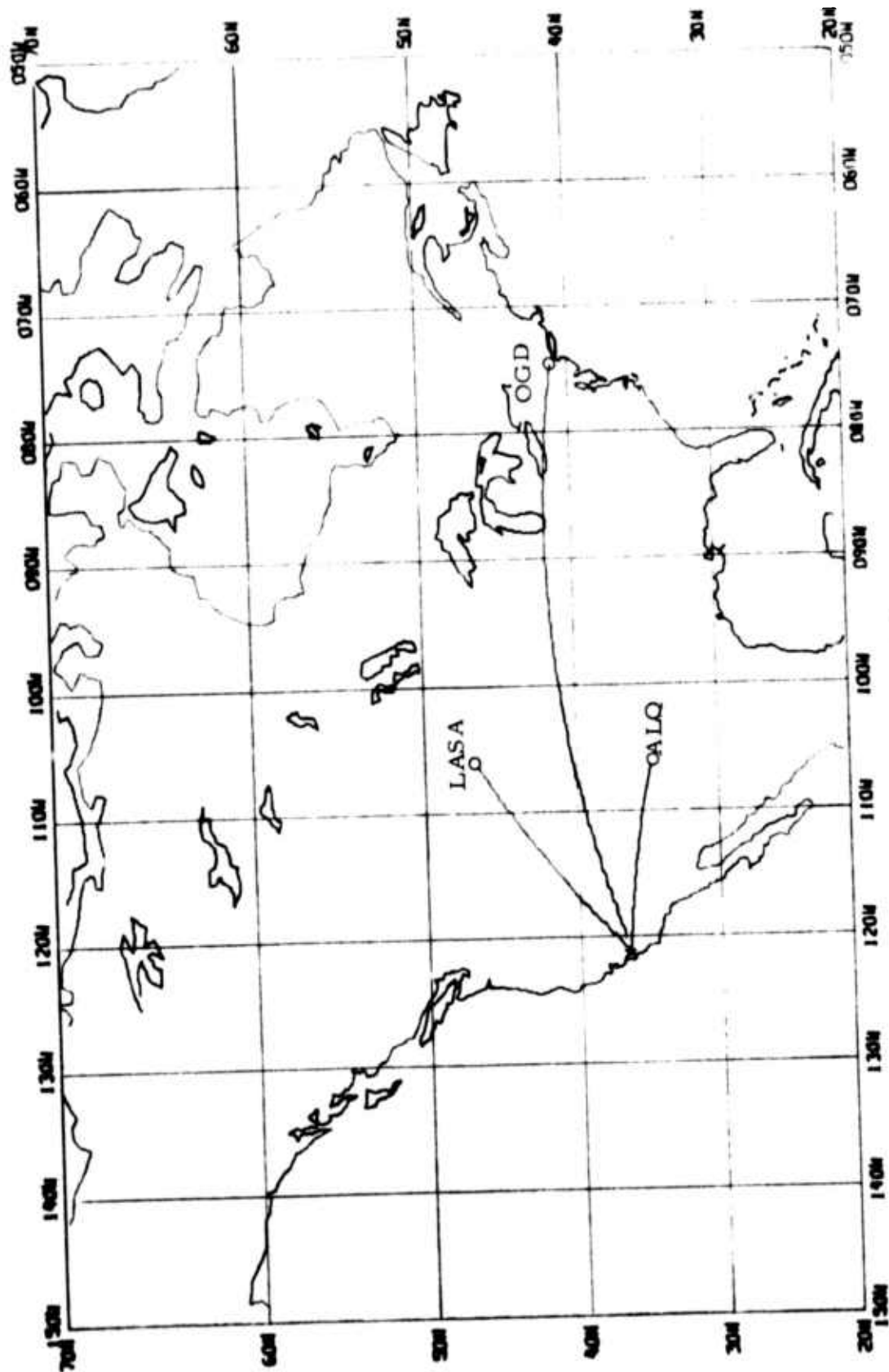


FIGURE III-1  
 TRAVEL PATHS TO THE AVAILABLE STATIONS FOR THE  
 JUNE 22, 1973 EARTHQUAKE

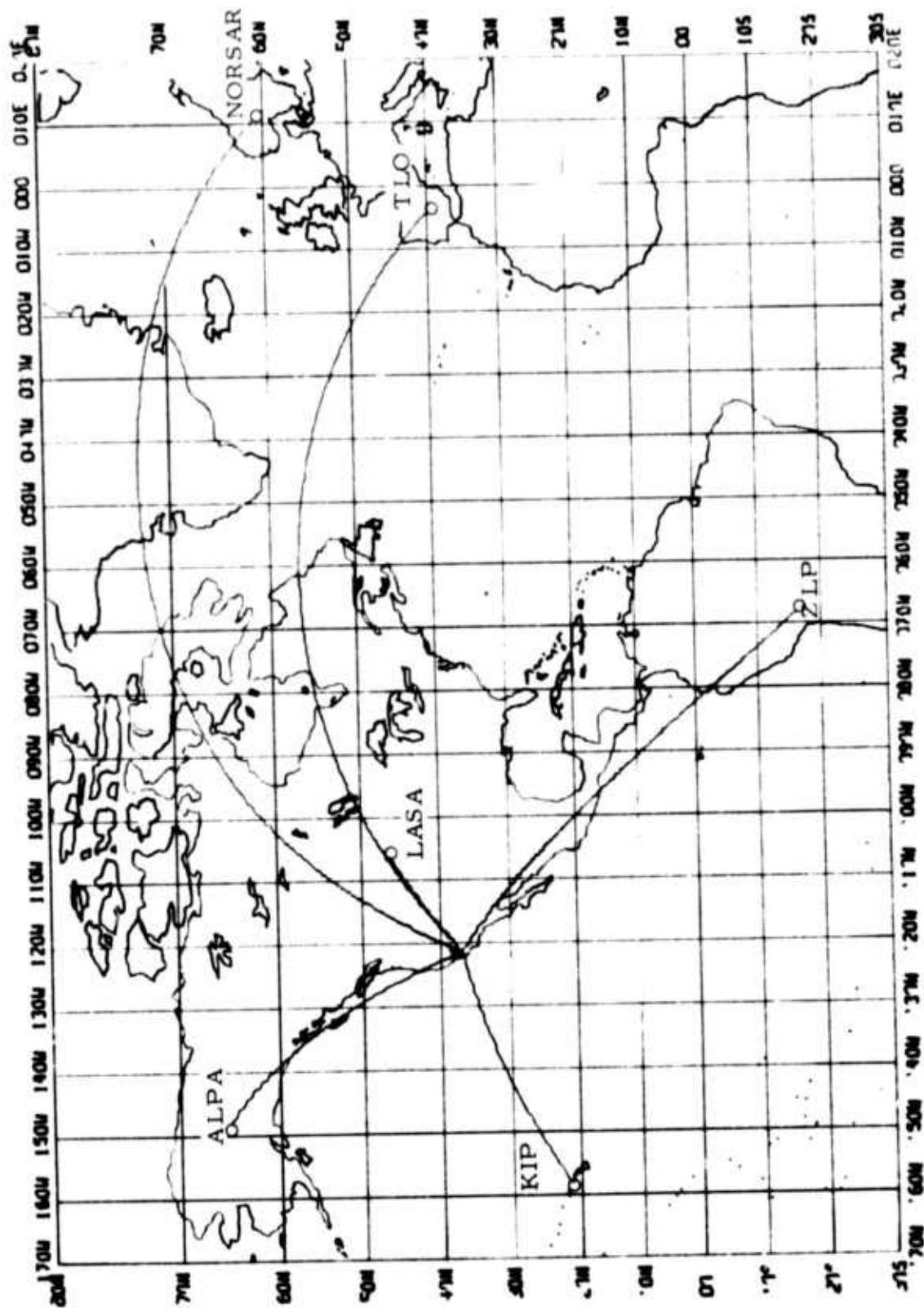


FIGURE III-2  
 TRAVEL PATHS TO THE AVAILABLE STATIONS FOR THE  
 NOVEMBER 28, 1974 EARTHQUAKE

TABLE III-3  
 ESTIMATIONS OF SOURCE PARAMETERS FOR THE CENTRAL CALIFORNIA  
 EVENT OBTAINED BY AMPLITUDE SPECTRAL FITTING BASED ON  
 MINIMUM-RESIDUAL CRITERION

| Structure      | Stations Used          | Optimal Solution |                                 |                                   |                                     |                        | Moment<br>$10^{25}$ dyne-cm |
|----------------|------------------------|------------------|---------------------------------|-----------------------------------|-------------------------------------|------------------------|-----------------------------|
|                |                        | Depth<br>h (km)  | Dip angle<br>$\delta$ (degrees) | Slip Angle<br>$\lambda$ (degrees) | Strike<br>N $\theta$ <sup>o</sup> E |                        |                             |
| Southwest Only | ALPA<br>ZLP<br>KIP     | 6                | 80                              | 30                                | 135                                 | $0.530 \times 10^{-1}$ |                             |
| Southwest Only | ALPA<br>LASA<br>NORSAR | 37.5             | 90                              | 0                                 | 40<br>130                           | 0.232                  |                             |
| Southwest Only | All Stations           | 37.5             | 80                              | 0                                 | 45                                  | 0.226                  |                             |
| Northeast Only | LASA<br>NORSAR<br>TLO  | 27.5             | 80                              | 0                                 | 125                                 | 0.111                  |                             |
| Northeast Only | ALPA<br>LASA<br>NORSAR | 27.5             | 80                              | 0                                 | 60                                  | 0.113                  |                             |
| Northeast Only | All Stations           | 27.5             | 90                              | 0                                 | 40<br>130                           | 0.104                  |                             |
| Both           | All Stations           | 27.5             | 80                              | 0                                 | 60                                  | 0.115                  |                             |

TABLE III-4

ESTIMATIONS OF SOURCE PARAMETERS FOR THE CENTRAL CALIFORNIA  
EVENT OBTAINED BY AMPLITUDE SPECTRAL FITTING BASED ON  
DISTRIBUTION-OF-MINIMUM-RESIDUAL CRITERION

| Structure      | Stations Used          | Source Parameters |              |                          |              |                            |              |                          |              |                |              |
|----------------|------------------------|-------------------|--------------|--------------------------|--------------|----------------------------|--------------|--------------------------|--------------|----------------|--------------|
|                |                        | Depth h (km)      |              | Dip Angle $\delta^\circ$ |              | Slip Angle $\lambda^\circ$ |              | Strike $N\theta^\circ E$ |              | Probable Range | % Confidence |
|                |                        | Probable Range    | % Confidence | Probable Range           | % Confidence | Probable Range             | % Confidence | Probable Range           | % Confidence |                |              |
| Southwest Only | ALPA<br>ZLP<br>KIP     | 4.5-10.25         | 78           | 60-90                    | 79           | -30, 0, 30                 | 78           | 15-45<br>110-140         | 38<br>48     |                |              |
| Southwest Only | ALPA<br>LASA<br>NORSAR | 32.5-42.0         | 89           | 80-90                    | 100          | 0                          | 100          | 35-50<br>125-140         | 48<br>48     |                |              |
| Southwest Only | All Stations           | 32.5-42.0         | 70           | 80-90                    | 100          | 0                          | 100          | 40-50<br>130-140         | 51<br>32     |                |              |
| Northeast Only | LASA<br>NORSAR<br>TLO  | 23.0-37.5         | 89           | 70-90                    | 84           | 0                          | 75           | 25-55<br>115-145         | 45<br>44     |                |              |
| Northeast Only | ALPA<br>LASA<br>NORSAR | 23.0-37.5         | 78           | 80-90                    | 98           | 0                          | 100          | 55-65<br>145-155         | 54<br>46     |                |              |
| Northeast Only | All Stations           | 23.0-37.5         | 88           | 80-90                    | 79           | 0                          | 100          | 30-60<br>120-150         | 42<br>42     |                |              |
| Both           | All Stations           | 23.0-37.5         | 79           | 80-90                    | 89           | 0                          | 100          | 55-65<br>145-155         | 46<br>46     |                |              |

From the above analysis, we have reached the following conclusions:

- Fitting the surface wave spectra with one earth model using stations on both sides of the fault neglects the effect of the medium discontinuity. One possible way to correct for this discontinuity would be to make the appropriate travel path correction. This problem will be examined in future studies.
- Fitting the surface wave spectra with two earth models would seem to be a reasonable approach, if we consider the effect of the discontinuity as a difference in the source excitation. One problem in this approach is, however, that the combination of the two earth models for simulating both sides of the fault actually neglects the possible physical complexity of the source due to the discontinuity.
- At the present time, we have no solution to the above problems. Since the location of this event is definitely on the west side of the San Andreas fault, the far-field solution obtained by using the three stations to the west of the fault with the southwest earth model should be considered a good estimate.

#### C. CONTINUED EXAMINATION OF THE THEORETICAL HIGHER MODE SPECTRA

Continuing with our examination of theoretical first higher mode Rayleigh and Love wave spectra, double couple sources were placed at three representative depths (4, 30, and 50 km) in a Gutenberg-Bullen earth model and a Hamilton-Healy earth model. Variations of the spectra with respect to dip, slip, and strike were examined (see Appendix C). We can summarize the properties of this spectra as follows:

- Regardless of the structure, the only consistent 'holes' in the spectra occur for Rayleigh waves generated by a vertical strike-slip source mechanism. In particular, for the Gutenberg-Bullen structure, two 'holes' appeared for this source mechanism placed 30 km deep at 9 and 20 seconds period.
- The level of first higher mode spectra is approximately an order of magnitude less than that of the fundamental mode spectra over the same frequency range (15 to 40 seconds period). The higher mode spectra over the 3 to 15 second period range is, however, approximately the same level as the fundamental mode 15 to 40 second spectra.
- For the Gutenberg-Bullen structure, the first higher mode spectra drops off rapidly for periods greater than 9 seconds, especially for Love waves. This drop-off is even more severe for the Hamilton-Healy structure, starting at 6 seconds period. This is a direct result of the lower velocity material in the upper crust of the Hamilton-Healy model. Therefore, we should expect to observe higher modes with greater regularity from thick high velocity source region crustal structures using presently installed instrumentation.

#### D. ANALYSIS OF THE SINKIANG, CHINA EARTHQUAKE SWARM OF AUGUST 1974

During most of the month of August and the early part of September 1974, a major earthquake swarm of over 300 recorded events occurred in Sinkiang, China. The location of the swarm is shown by the boxed area in Figure III-3. (This map was part of an earlier study by Turnbull, et al., 1974a). The number and magnitude of these events as a function of date is shown in Figure III-4.

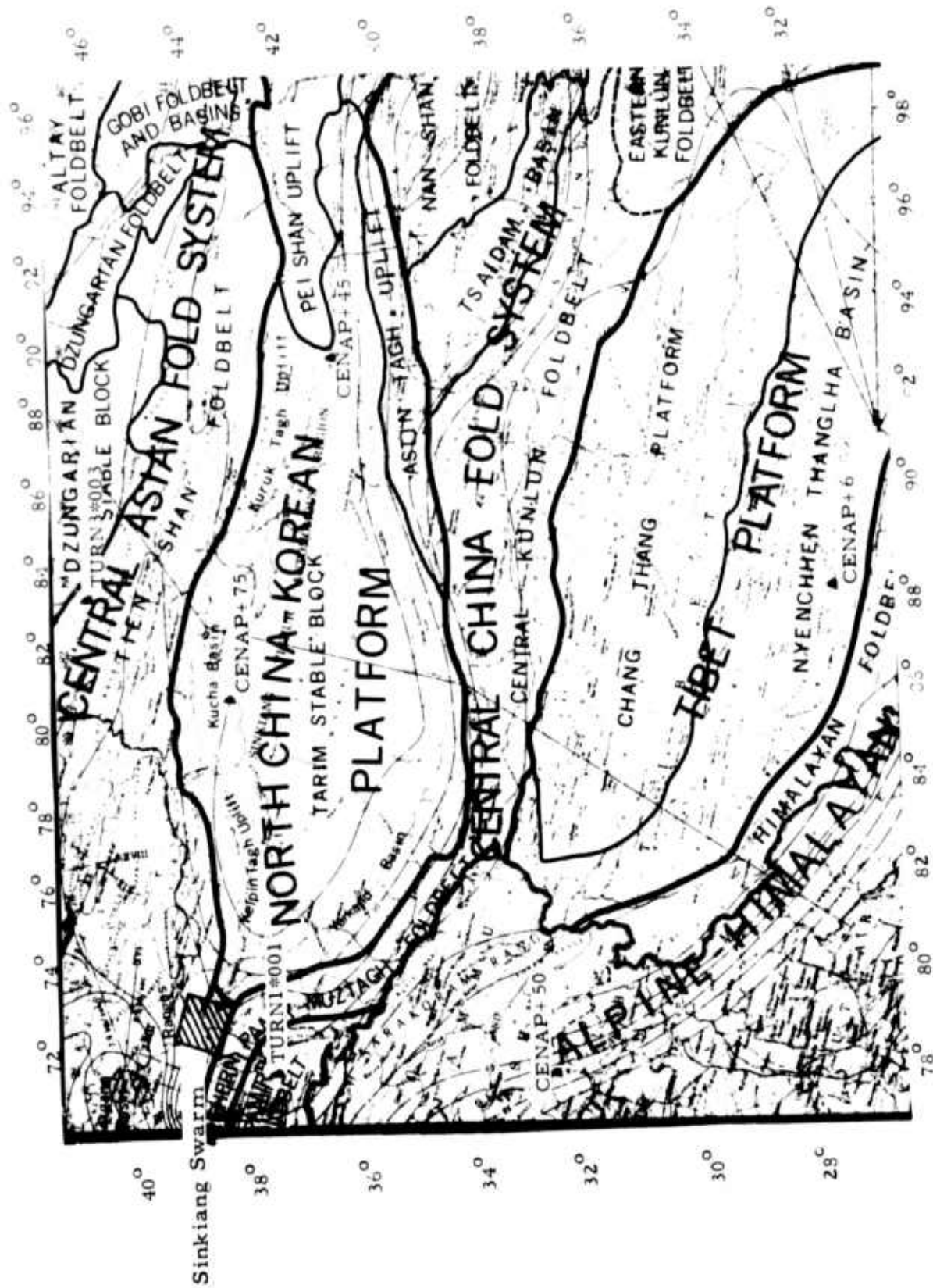


FIGURE III-3

LOCATION OF SINKIANG, CHINA SWARM OF AUGUST, 1974 - (BOXED AREA)



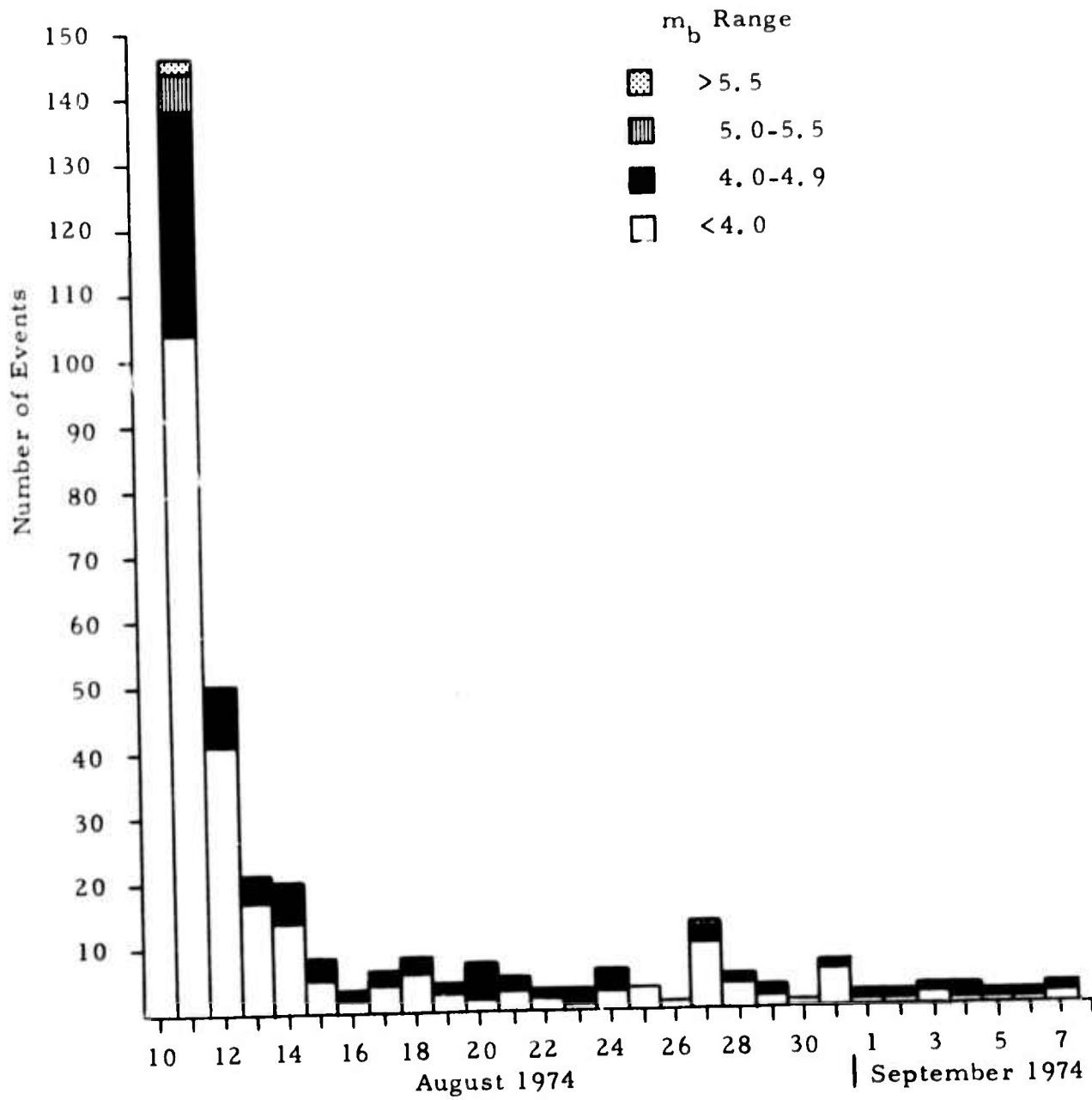


FIGURE III-4  
 THE NUMBER AND MAGNITUDE CHRONOLOGY OF THE  
 RECORDED EVENTS OF THE SINKIANG EARTHQUAKE  
 SWARM OF AUGUST 1974

This swarm was chosen for intensive analysis because of the following reasons:

- The opportunity to analyze a large number of events from a small region - investigate the repeatability of source mechanism from event to event and local tectonics.
- The possibility of using a master event or events with spectral ratios to measure path effects.
- The opportunity to determine effective attenuation by eliminating radiation pattern effects (knowing the source mechanism) and by two station path corrections (in the instances where they occur).

Preliminary analysis of five of these events have consistently yielded shallow source depths in the 4 to 10 km range. The source mechanism details, though, have not followed a particular trend at this point of the study. A more detailed analysis of this swarm will be presented in the next report.

SECTION IV  
THE  $M_s - m_b$  RELATIONSHIP

In previous work by Turnbull et al. (1974b, 1975) the  $M_s - m_b$  discriminant was investigated with the objective of reducing the scatter of the earthquake population. Several methods were tried to achieve such a reduction; all of them designed to modify in various ways the  $M_s$  determinations at individual single stations of the VLPE network, and assess the impact on network magnitude measurements. However, no significant reduction of the  $M_s - m_b$  scatter was observed.

In this report we focus upon the  $m_b$  determination, and apply the maximum likelihood method of Ringdal (1975) in an attempt to improve the accuracy of the PDE bodywave magnitudes for our data base. The basic idea is that PDE magnitudes of small events tend to be biased high, because only a few stations (with particularly favorable radiation patterns) report such events, and network magnitudes are therefore obtained by averaging over a set of stations that is not representative of the whole network. By taking into account the estimated noise levels at the non-detecting stations, this magnitude bias can partly be compensated for. Our model is as follows:

- For large events, the typical number of PDE stations that report a bodywave magnitude is assumed to be at least  $N_0$  (where  $N_0$  is a number to be estimated)
- For a given event, the number  $N$  of stations that actually report a magnitude is compared to  $N_0$ . If  $N \geq N_0$ , it is assumed that essentially all PDE stations detected the event. If  $N < N_0$ , we assume that, for each of  $(N_0 - N)$  stations, the magnitude was less than a certain threshold value  $m$ .

- The threshold values  $m$  at each station are assumed to be independently sampled from a normal distribution  $m \sim N(m_o, \sigma_o^2)$
- The world-wide magnitude values of the event are assumed to follow a normal distribution  $N(\mu, \sigma_S^2)$ ; where the parameter  $\mu$  denotes the true magnitude of the event.

The likelihood function (Ringdal, 1975) becomes; for

$N < N_o$  :

$$L(\mu) = \prod_{i=1}^N \frac{1}{\sigma_S} \cdot \phi \left( \frac{m_i - \mu}{\sigma_S} \right) \cdot \left[ \Phi \left( \frac{m_o - \mu}{\sqrt{\sigma_S^2 + \sigma_o^2}} \right) \right]^{N_o - N} \quad (IV-1)$$

where the  $m_i$  denote the magnitude measured at the detecting stations, and where  $\phi$  and  $\Phi$  are the standard normal density and distribution functions, respectively. An estimate of  $\mu$  is then obtained by numerical maximization of (IV-1).

In order to do this, it is necessary to have available realistic estimates of the parameters  $\sigma_S, m_o, \sigma_o, N_o$ ; besides the observed quantities  $N$  and  $\{m_i; i = 1, \dots, N\}$ . Studies by Evernden (1969) of the noise levels of some of the better WWSSN stations seem to indicate values of  $m_o = 5.0$  and  $\sigma_o = 0.2$  as realistic estimates. Veith and Clawson (1972) found  $\sigma_S = 0.4$  to be representative of the WWSSN network. From studies of PDE bulletins, we have found a value of  $N_o = 25$  as a reasonable estimate of the number of stations expected to report magnitudes of large Eurasian events.

Figure IV-1 shows the theoretical bias  $(\bar{m} - \mu)$  between the average magnitude  $\bar{m}$  (over the  $N$  detecting stations) and the true magnitude  $\mu$  as a function of the ratio  $N/N_o$  and for various values of  $(\bar{m} - m_o)$ . Equation (IV-1) has been used to compute these bias values. Note that the only assumed parameter values in Figure IV-1 are  $\sigma_S = 0.4$  and  $\sigma_o = 0.2$ ;

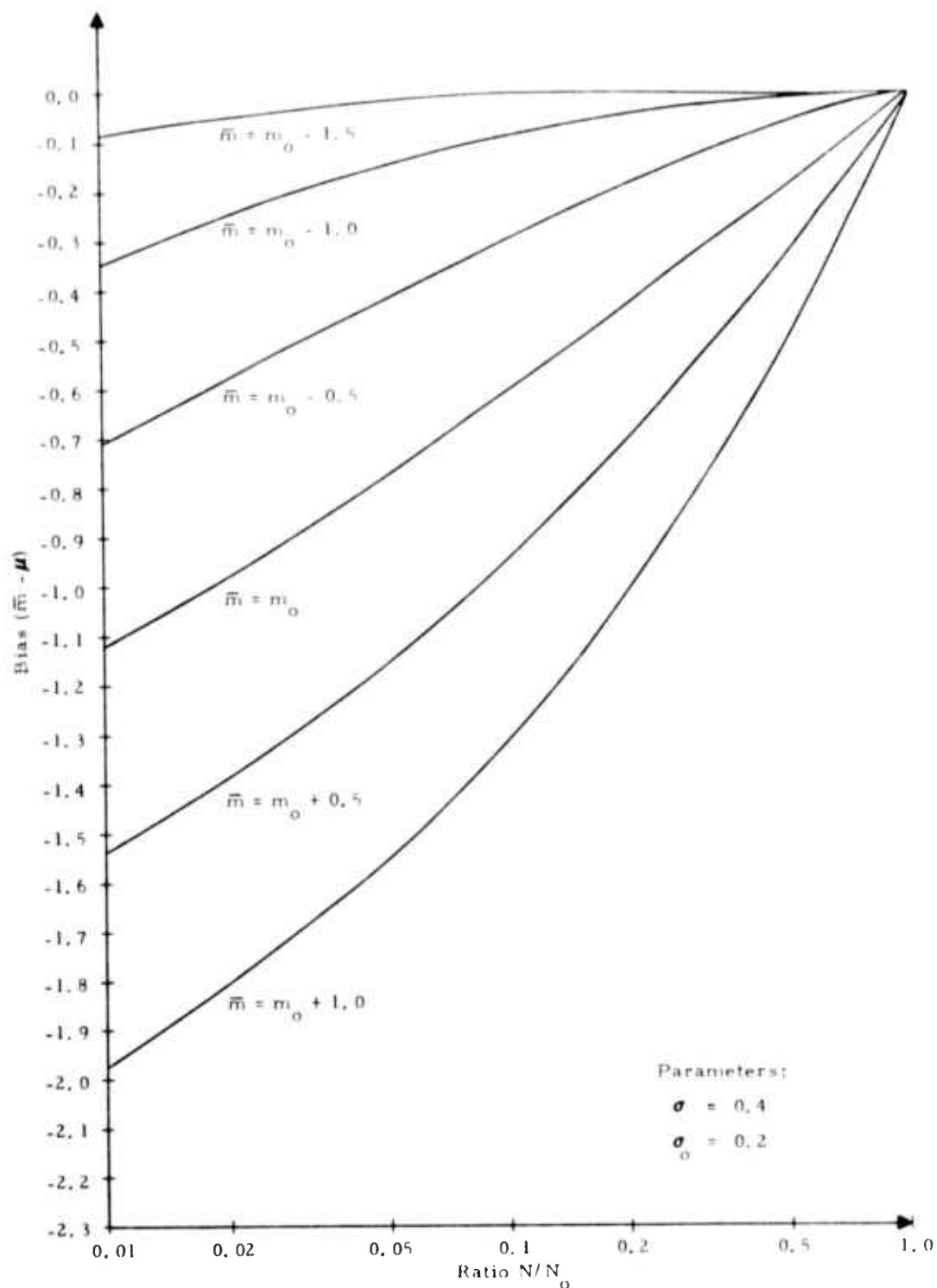


FIGURE IV-1

EXPECTED BIAS OF CONVENTIONAL MAGNITUDE  $\bar{m}$  RELATIVE TO TRUE MAGNITUDE  $\mu$  FOR A HYPOTHETICAL NETWORK AS A FUNCTION OF THE PERCENTAGE OF DETECTING STATIONS

hence the graphs can also be applied to networks with different parameter values  $N_o$  and  $m_o$  than used here.

Table IV-1 lists the events in the data set along with certain event parameters. Among those are the NORSAR and PDE reported  $m_b$  values; the number  $N$  of PDE station magnitudes available, and the maximum likelihood PDE magnitudes from the preceding model. Figures IV-2 and IV-3 plot NORSAR magnitudes versus PDE standard  $m_b$  and PDE maximum likelihood (M-L)  $m_b$ , respectively. It is seen that the latter case produces a linear trend with a slope close to 1.00, while Figure IV-2 exhibits the network magnitude bias effect for small events, and produces a more horizontal slope of about 0.8. The conclusion is that the maximum likelihood  $m_b$  values are more consistent estimates of  $\mu$  than the standard PDE  $m_b$  for our data set.

In order to see if the use of maximum likelihood  $m_b$  values would reduce the scatter in the  $M_s - m_b$  population, VLPE  $M_s$  was plotted against PDE  $m_b$  (Figure IV-4) and against PDE(M-L)  $m_b$  (Figure IV-5). The straight line of each figure is a least squares orthogonal fit, and the orthogonal standard deviation  $\sigma$  has been computed together with the slope  $\alpha$  and intercept  $\beta$  of the estimated functional relationship:

$$M_s = \alpha \cdot m_b + \beta \quad (IV-2)$$

We note that the value of  $\sigma$  does not decrease when PDE  $m_b$ 's are replaced by maximum likelihood estimates; on the contrary, a slight increase is found (from 0.238 to 0.262). However, the slope  $\alpha$  is much steeper in the first case (1.54 versus 1.23), hence the values of  $\sigma$  are not directly compatible. (For example, an estimation method that assigned identical  $m_b$  values to all events would produce a vertical slope with  $\sigma = 0$ ; hence, a low value of  $\sigma$  does not necessarily imply improved estimation techniques.)

TABLE IV-1  
 EVENT PARAMETERS OF EURASIAN DATA BASE  
 (PAGE 1 OF 3)

| Event Number | Number Of PDE Stations | PDE (M-L) $m_p$ | PDE $m_p$ | NORSAR $m_p$ | VLPE Station - $M_s$ Values |     |     |     |     |     |     |     |     |     |     | ALPA $M_s$ | NORSAR $M_s$ |     |     |
|--------------|------------------------|-----------------|-----------|--------------|-----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------|--------------|-----|-----|
|              |                        |                 |           |              | 1                           | 2   | 3   | 4   | 5   | 6   | 7   | 8   | 9   | 10  | 11  |            |              |     |     |
| 31           | 9                      | 4.7             | 5.0       | 4.6          | 0.0                         | 4.2 | 5.9 | 4.1 | 0.0 | 4.8 | 4.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.7 | 4.3 |
| 36           | 12                     | 4.7             | 4.9       | 4.6          | 0.0                         | 3.9 | 0.0 | 3.3 | 0.0 | 3.5 | 4.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.0 | 4.2 |
| 37           | 2                      | 4.3             | 4.8       | 4.3          | 0.0                         | 4.1 | 0.0 | 4.5 | 0.0 | 4.3 | 4.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.3 | 4.2 |
| 39           | 22                     | 5.2             | 5.3       | 5.1          | 0.0                         | 5.0 | 0.0 | 4.9 | 0.0 | 5.4 | 5.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.8 | 5.2 |
| 43           | 9                      | 4.5             | 4.7       | 4.7          | 0.0                         | 3.2 | 3.6 | 3.7 | 0.0 | 3.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.0 | 3.6 |
| 62           | 1                      | 4.1             | 4.6       | 4.6          | 0.0                         | 4.0 | 0.0 | 0.0 | 0.0 | 3.8 | 4.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.6 | 0.0 |
| 73           | 1                      | 4.4             | 5.9       | 4.2          | 0.0                         | 4.2 | 3.9 | 3.8 | 0.0 | 4.0 | 4.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.0 | 3.9 |
| 87           | 7                      | 4.4             | 4.6       | 4.2          | 0.0                         | 3.4 | 3.5 | 3.6 | 0.0 | 3.6 | 3.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.3 | 3.3 |
| 88           | 14                     | 4.9             | 5.1       | 5.0          | 0.0                         | 3.9 | 4.4 | 4.4 | 0.0 | 4.5 | 4.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.3 | 0.0 |
| 89           | 2                      | 4.1             | 4.5       | 4.4          | 0.0                         | 3.5 | 4.4 | 4.3 | 0.0 | 4.0 | 4.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.1 | 4.1 |
| 95           | 11                     | 4.9             | 5.2       | 4.9          | 0.0                         | 3.9 | 4.8 | 0.0 | 0.0 | 4.1 | 3.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 0.0 | 0.0 |
| 112          | 28                     | 5.7             | 5.7       | 5.7          | 0.0                         | 4.4 | 5.1 | 5.1 | 0.0 | 4.8 | 5.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.8 | 0.0 |
| 123          | 10                     | 4.5             | 4.6       | 3.9          | 0.0                         | 4.0 | 3.6 | 4.1 | 0.0 | 3.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.9 | 3.9 |
| 134          | 28                     | 5.4             | 5.4       | 5.2          | 0.0                         | 0.0 | 4.7 | 0.0 | 0.0 | 4.8 | 5.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 0.0 | 0.0 |
| 294          | 23                     | 5.2             | 5.2       | 4.6          | 0.0                         | 4.1 | 4.5 | 4.2 | 0.0 | 5.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 4.6 | 4.8 |
| 341          | 9                      | 5.0             | 5.4       | 5.2          | 5.1                         | 0.0 | 0.0 | 0.0 | 0.0 | 5.3 | 0.0 | 0.0 | 5.6 | 4.4 | 0.0 | 0.0        | 0.0          | 3.8 | 0.0 |
| 472          | 17                     | 5.1             | 5.2       | 4.4          | 3.8                         | 0.0 | 0.0 | 4.0 | 0.0 | 4.0 | 0.0 | 0.0 | 4.1 | 0.0 | 0.0 | 0.0        | 0.0          | 0.0 | 4.0 |
| 505          | 22                     | 5.2             | 5.3       | 5.2          | 3.9                         | 0.0 | 0.0 | 3.7 | 0.0 | 4.7 | 0.0 | 0.0 | 4.6 | 3.3 | 0.0 | 0.0        | 0.0          | 4.1 | 4.2 |
| 605          | 10                     | 4.9             | 5.1       | 4.5          | 0.0                         | 0.0 | 0.0 | 4.3 | 0.0 | 4.3 | 0.0 | 0.0 | 4.3 | 0.0 | 0.0 | 0.0        | 0.0          | 0.0 | 5.0 |
| 611          | 8                      | 4.7             | 5.0       | 4.4          | 0.0                         | 0.0 | 0.0 | 4.4 | 0.0 | 4.2 | 0.0 | 0.0 | 4.2 | 0.0 | 0.0 | 0.0        | 0.0          | 0.0 | 0.0 |

TABLE IV - 1  
 EVENT PARAMETERS OF EURASIAN DATA BASE  
 (PAGE 2 OF 3)

| Event Number | Number Of PDF Stations | PDE (M-L) | PDE $m_p$ | NORSAR $m_p$ | VLPE Station - $M_s$ Values |     |     |     |     |     |     |     |     |     |     | ALPA $M_s$ | NORSAR $M_s$ |     |     |
|--------------|------------------------|-----------|-----------|--------------|-----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------|--------------|-----|-----|
|              |                        |           |           |              | 1                           | 2   | 3   | 4   | 5   | 6   | 7   | 8   | 9   | 10  | 11  |            |              |     |     |
| 653          | 16                     | 5.0       | 5.2       | 5.1          | 4.2                         | 0.0 | 0.0 | 0.0 | 3.9 | 4.3 | 0.0 | 0.0 | 0.0 | 4.1 | 0.0 | 0.0        | 0.0          | 4.0 | 4.2 |
| 710          | 7                      | 4.4       | 4.5       | 4.5          | 0.0                         | 3.9 | 0.0 | 0.0 | 0.0 | 0.0 | 4.2 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0        | 0.0          | 3.5 | 3.8 |
| 711          | 11                     | 5.0       | 5.4       | 5.0          | 0.0                         | 4.6 | 0.0 | 0.0 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 | 4.2 | 0.0 | 0.0        | 0.0          | 4.2 | 4.7 |
| 716          | 19                     | 5.4       | 5.5       | 4.8          | 0.0                         | 4.6 | 0.0 | 0.0 | 0.0 | 0.0 | 5.7 | 0.0 | 0.0 | 5.0 | 0.0 | 0.0        | 0.0          | 4.5 | 0.0 |
| 744          | 26                     | 5.7       | 5.7       | 5.2          | 5.7                         | 5.6 | 0.0 | 0.0 | 0.0 | 0.0 | 5.5 | 0.0 | 0.0 | 5.5 | 0.0 | 4.9        | 0.0          | 4.9 | 5.9 |
| 775          | 17                     | 5.2       | 5.4       | 5.3          | 0.0                         | 5.2 | 0.0 | 0.0 | 0.0 | 0.0 | 4.9 | 0.0 | 0.0 | 4.9 | 0.0 | 5.4        | 0.0          | 5.0 | 0.0 |
| 776          | 5                      | 4.5       | 4.8       | 4.8          | 0.0                         | 3.8 | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0        | 0.0          | 3.7 | 0.0 |
| 799          | 35                     | 6.0       | 6.0       | 5.8          | 0.0                         | 6.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.8 | 0.0 | 5.8        | 0.0          | 5.4 | 5.7 |
| 818          | 26                     | 5.7       | 5.7       | 5.6          | 4.4                         | 4.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.8 | 0.0 | 0.0        | 0.0          | 0.0 | 0.0 |
| 825          | 3                      | 4.3       | 4.7       | 4.6          | 4.2                         | 4.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.4 | 0.0 | 4.1        | 0.0          | 0.0 | 0.0 |
| 828          | 12                     | 5.3       | 5.7       | 5.6          | 5.3                         | 6.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 5.8 | 0.0 | 5.8        | 0.0          | 5.5 | 5.8 |
| 837          | 7                      | 4.6       | 4.9       | 4.7          | 3.8                         | 3.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 4.0        | 0.0          | 3.4 | 0.0 |
| 859          | 54                     | 5.7       | 5.7       | 5.3          | 5.0                         | 5.4 | 0.0 | 0.0 | 0.0 | 5.1 | 5.2 | 0.0 | 0.0 | 5.2 | 0.0 | 0.0        | 5.3          | 5.3 | 5.2 |
| 881          | 14                     | 5.0       | 5.2       | 5.1          | 0.0                         | 3.6 | 0.0 | 0.0 | 0.0 | 3.6 | 3.8 | 0.0 | 0.0 | 3.8 | 0.0 | 0.0        | 4.2          | 3.5 | 3.8 |
| 890          | 30                     | 5.3       | 5.3       | 4.8          | 0.0                         | 4.8 | 0.0 | 0.0 | 0.0 | 0.0 | 5.2 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0        | 5.5          | 4.6 | 5.1 |
| 897          | 13                     | 4.8       | 5.0       | 4.5          | 0.0                         | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 | 4.3 | 0.0 | 0.0 | 3.9 | 0.0 | 4.0        | 0.0          | 3.6 | 4.1 |
| 929          | 10                     | 4.8       | 5.1       | 4.7          | 0.0                         | 4.2 | 0.0 | 0.0 | 0.0 | 0.0 | 4.6 | 0.0 | 0.0 | 4.0 | 0.0 | 3.9        | 3.5          | 0.0 | 4.5 |
| 937          | 18                     | 5.1       | 5.2       | 4.2          | 0.0                         | 4.3 | 0.0 | 0.0 | 0.0 | 0.0 | 4.0 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0        | 4.5          | 3.9 | 4.0 |
| 946          | 4                      | 4.2       | 4.3       | 4.1          | 0.0                         | 3.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0        | 0.0          | 3.4 | 3.4 |
| 950          | 2                      | 4.3       | 4.9       | 4.2          | 0.0                         | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.1 | 0.0 | 0.0 | 3.8 | 0.0 | 3.9        | 0.0          | 0.0 | 4.0 |



TABLE IV-1  
 EVENT PARAMETERS OF EURASIAN DATA BASE  
 (PAGE 3 OF 3)

| Event Number | Number Of PDE Stations | PDE (M-L)<br>$m_p$ | PDE $m_p$ | NORSAR $m_p$ | VLPE Station - $M_s$ Values |     |     |     |     |     |     |     |     |     |     | ALPA $M_s$ | NORSAR $M_s$ |     |
|--------------|------------------------|--------------------|-----------|--------------|-----------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------------|--------------|-----|
|              |                        |                    |           |              | 1                           | 2   | 3   | 4   | 5   | 6   | 7   | 8   | 9   | 10  | 11  |            |              |     |
| 956          | 8                      | 4.4                | 4.5       | 4.1          | 0.0                         | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.4 | 0.0 | 4.5 | 4.2 | 4.1 | 0.0        | 4.2          | 4.3 |
| 965          | 8                      | 4.6                | 4.8       | 4.6          | 0.0                         | 0.0 | 0.0 | 0.0 | 0.0 | 3.9 | 0.0 | 4.1 | 3.5 | 0.0 | 0.0 | 3.2        | 3.5          | 4.2 |
| 966          | 17                     | 5.1                | 5.2       | 4.8          | 0.0                         | 0.0 | 0.0 | 0.0 | 3.8 | 4.1 | 0.0 | 4.2 | 0.0 | 4.3 | 4.3 | 4.3        | 4.1          | 0.0 |
| 1039         | 25                     | 6.1                | 6.1       | 6.3          | 5.5                         | 0.0 | 0.0 | 0.0 | 5.7 | 5.3 | 0.0 | 5.9 | 5.6 | 5.0 | 5.7 | 5.5        | 5.7          | 5.5 |
| 1065         | 6                      | 4.4                | 4.6       | 4.6          | 0.0                         | 4.1 | 0.0 | 0.0 | 3.4 | 4.3 | 0.0 | 0.0 | 3.9 | 0.0 | 4.0 | 4.3        | 0.0          | 4.3 |
| 1080         | 9                      | 4.6                | 4.8       | 4.5          | 3.9                         | 4.2 | 0.0 | 0.0 | 3.8 | 4.2 | 0.0 | 4.3 | 0.0 | 0.0 | 0.0 | 0.0        | 3.5          | 4.5 |
| 1083         | 40                     | 5.7                | 5.7       | 5.3          | 4.8                         | 5.3 | 0.0 | 0.0 | 3.8 | 5.3 | 0.0 | 5.0 | 5.1 | 4.3 | 5.2 | 4.9        | 4.9          | 5.3 |
| 1085         | 56                     | 6.1                | 6.1       | 5.7          | 5.4                         | 5.8 | 0.0 | 0.0 | 4.6 | 5.9 | 0.0 | 5.9 | 5.7 | 4.8 | 5.6 | 5.7        | 6.0          | 6.0 |
| 1132         | 24                     | 5.5                | 5.5       | 5.2          | 5.5                         | 5.3 | 0.0 | 0.0 | 0.0 | 5.9 | 0.0 | 0.0 | 0.0 | 4.8 | 5.4 | 0.0        | 0.0          | 0.0 |
| 1166         | 15                     | 5.0                | 5.2       | 5.4          | 4.2                         | 4.9 | 0.0 | 4.7 | 0.0 | 0.0 | 3.3 | 4.7 | 0.0 | 0.0 | 4.4 | 4.3        | 4.7          | 4.7 |
| 1172         | 23                     | 5.4                | 5.4       | 5.8          | 3.4                         | 4.7 | 0.0 | 5.0 | 0.0 | 4.3 | 4.5 | 4.7 | 0.0 | 4.2 | 0.0 | 5.2        | 0.0          | 0.0 |
| 1180         | 19                     | 5.2                | 5.3       | 5.6          | 0.0                         | 5.0 | 0.0 | 4.8 | 0.0 | 4.8 | 4.8 | 4.7 | 0.0 | 0.0 | 0.0 | 4.4        | 4.4          | 0.0 |

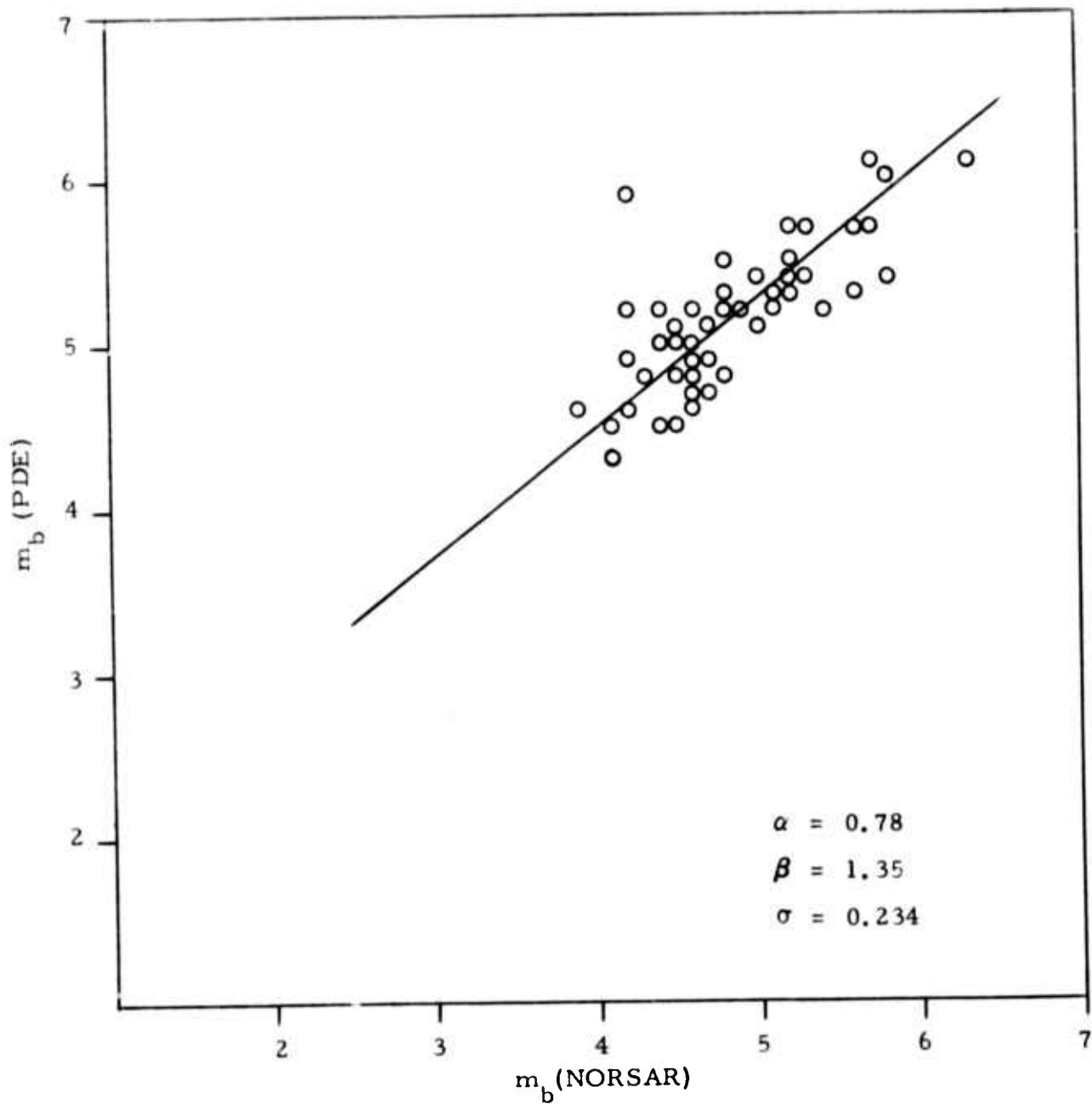


FIGURE IV-2  
 NORSAR  $m_b$  VERSUS PDE  $m_b$

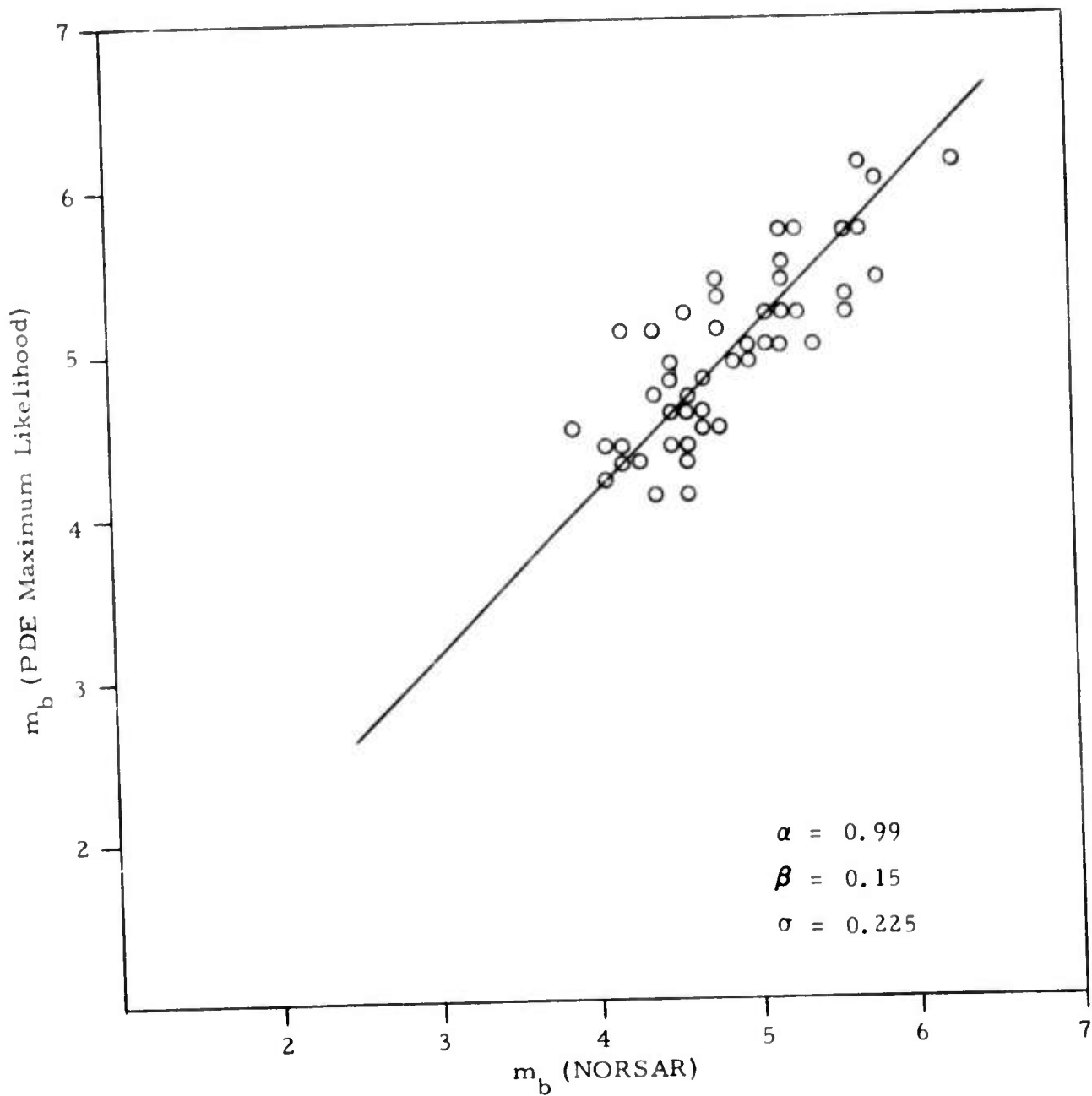


FIGURE IV-3  
 NORSAR  $m_b$  VERSUS PDE MAXIMUM LIKELIHOOD  $m_b$

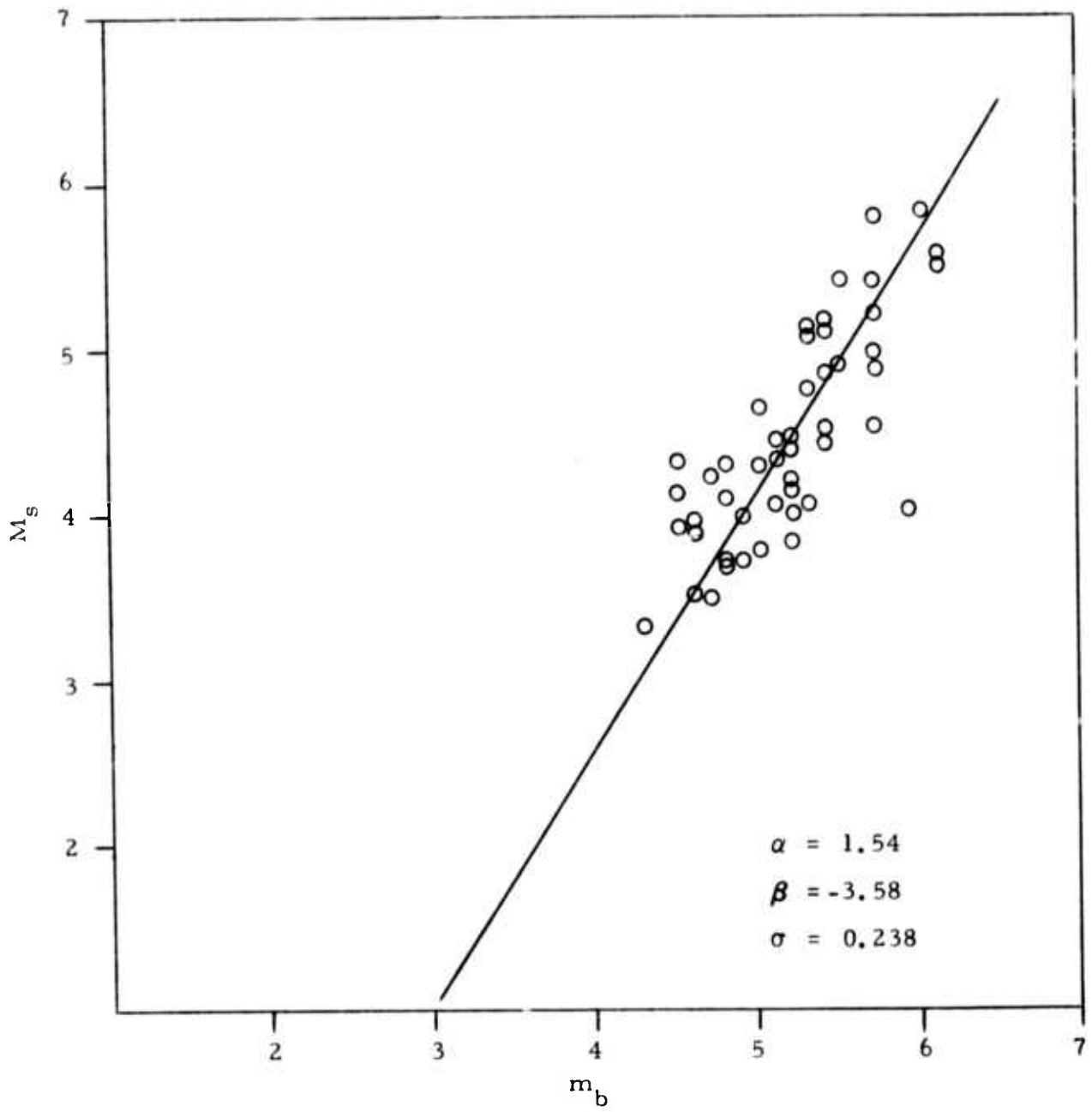


FIGURE IV-4  
PDE  $m_b$  VERSUS VLPE  $M_s$

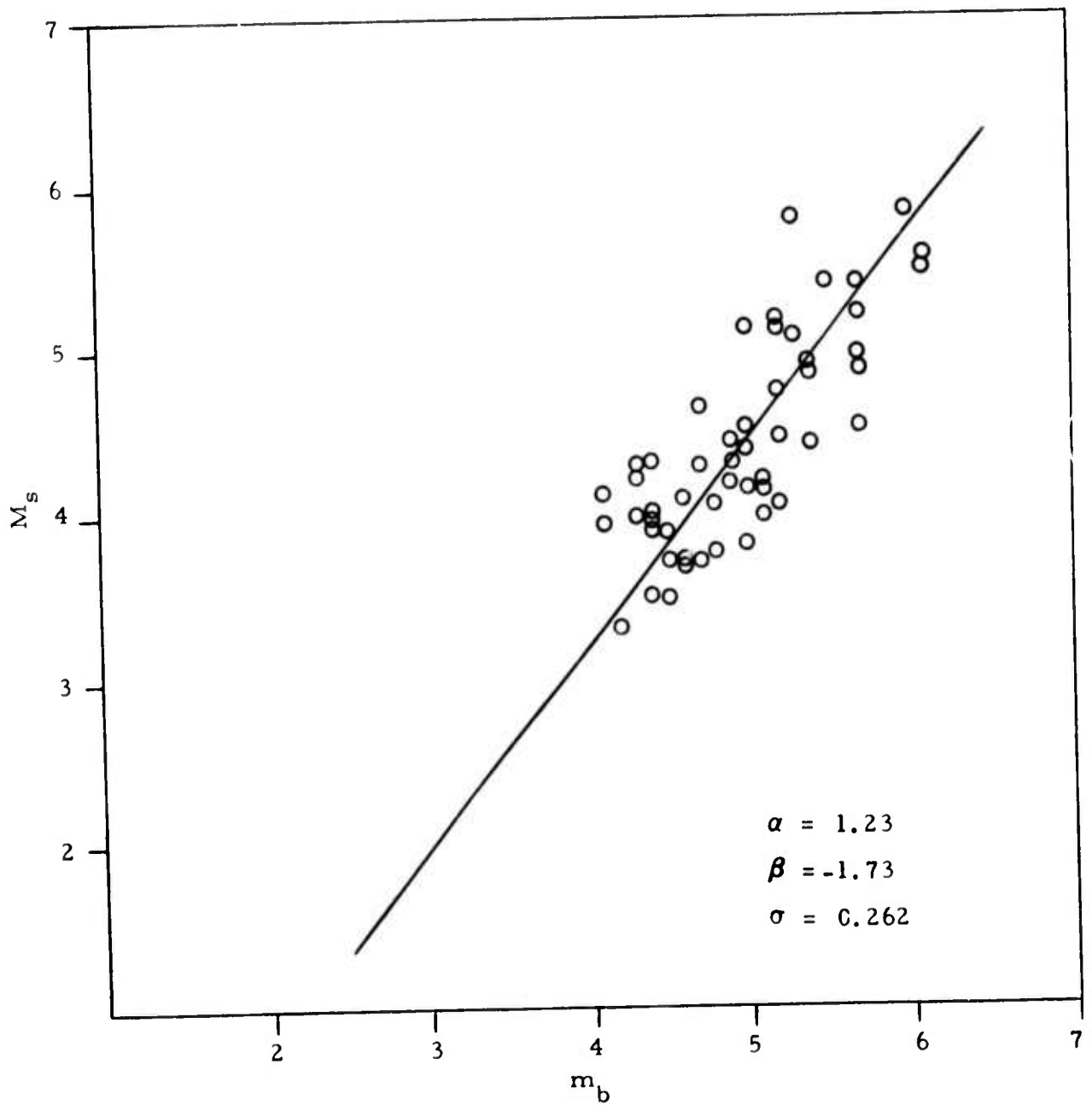


FIGURE IV-5  
 MAXIMUM LIKELIHOOD PDE  $m_b$  VERSUS VLPE  $M_s$

In order to examine more closely the variations of the  $M_s - m_b$  slope as a function of estimation techniques of  $M_s$  and  $m_b$ , a total of nine cases were run based on the given event population. In each case, the  $M_s$  values estimated by either VLPE (averaging), ALPA or NORSAR were combined with the  $m_b$  values of NORSAR, PDE, and PDE(M-L). The results are summarized in Table IV-2. The following points are noteworthy:

- Four of the runs produce a virtually identical slope ( $\alpha \approx 1.37$ ). These are precisely those four runs that combine 'consistent'  $M_s$  and  $m_b$  values, i. e., values free of network bias effects. (NORSAR or ALPA  $M_s$  versus NORSAR or PDE(M-L)  $m_b$ .)
- A consistently high value of the slope (1.66 or 1.64) is found when PDE  $m_b$  is plotted against a consistent  $M_s$ .
- A consistently low value of  $\alpha$  (1.23 or 1.24) results when VLPE  $M_s$  is plotted against a consistent  $m_b$ .
- When PDE  $m_b$  is plotted against VLPE  $M_s$ ,  $\alpha$  is again high, showing that the network bias effects in PDE magnitudes dominate those of VLPE.

Hence, the behavior of the computed slope agrees well with what could be expected from network bias consideration, and it appears that the most accurate linear functional relationship between  $M_s$  and  $m_b$  for the given data set (ranging in  $m_b$  values from about 4.0 to 6.0) has a slope of approximately 1.4.

Considering closer the four cases of consistent slope estimates, it is interesting to note that the value of  $\sigma$  is lower when using PDE(M-L)  $m_b$  versus either ALPA or NORSAR  $M_s$  compared to when NORSAR  $m_b$  is used ( $\sigma \approx 0.26$  versus  $\sigma \approx 0.31$ ). It would be interesting to compare PDE(M-L)  $m_b$  to the VLPE-ALPA-NORSAR combined network with the network bias reduced

TABLE IV-2  
 RELATIONSHIP  $M_s - m_b$  FOR VARIOUS COMBINATIONS OF  
 $M_s$  AND  $m_b$  MEASUREMENT PROCEDURES

| $m_b$                     | $M_s$  | Number*<br>Of Points<br>NP | Slope<br>$\alpha$ | Intercept<br>$\beta$ | $\sigma$<br>Orthogonal | $\sigma$<br>( $M_s/m_b$ ) |
|---------------------------|--------|----------------------------|-------------------|----------------------|------------------------|---------------------------|
| PDE                       | VLPE   | 52                         | 1.54              | -3.58                | 0.238                  | 0.437                     |
|                           | ALPA   | 41                         | 1.66              | -4.33                | 0.253                  | 0.490                     |
|                           | NORSAR | 35                         | 1.64              | -3.95                | 0.276                  | 0.530                     |
| PDE<br>Maximum Likelihood | VLPE   | 52                         | 1.23              | -1.73                | 0.262                  | 0.415                     |
|                           | ALPA   | 41                         | 1.37              | -2.57                | 0.257                  | 0.436                     |
|                           | NORSAR | 35                         | 1.37              | -2.25                | 0.259                  | 0.439                     |
| NORSAR                    | VLPE   | 52                         | 1.24              | -1.67                | 0.309                  | 0.492                     |
|                           | ALPA   | 41                         | 1.37              | -2.48                | 0.321                  | 0.544                     |
|                           | NORSAR | 35                         | 1.39              | -2.14                | 0.305                  | 0.522                     |

\* The missing data points (NP < 52) are due to lack of available data for NORSAR or ALPA  $M_s$  for some events, and not due to nondetection at these stations.

by maximum likelihood processing; however, we have not been able to do this, mostly because of the lack of reliable VLPE data for some stations.



SECTION V  
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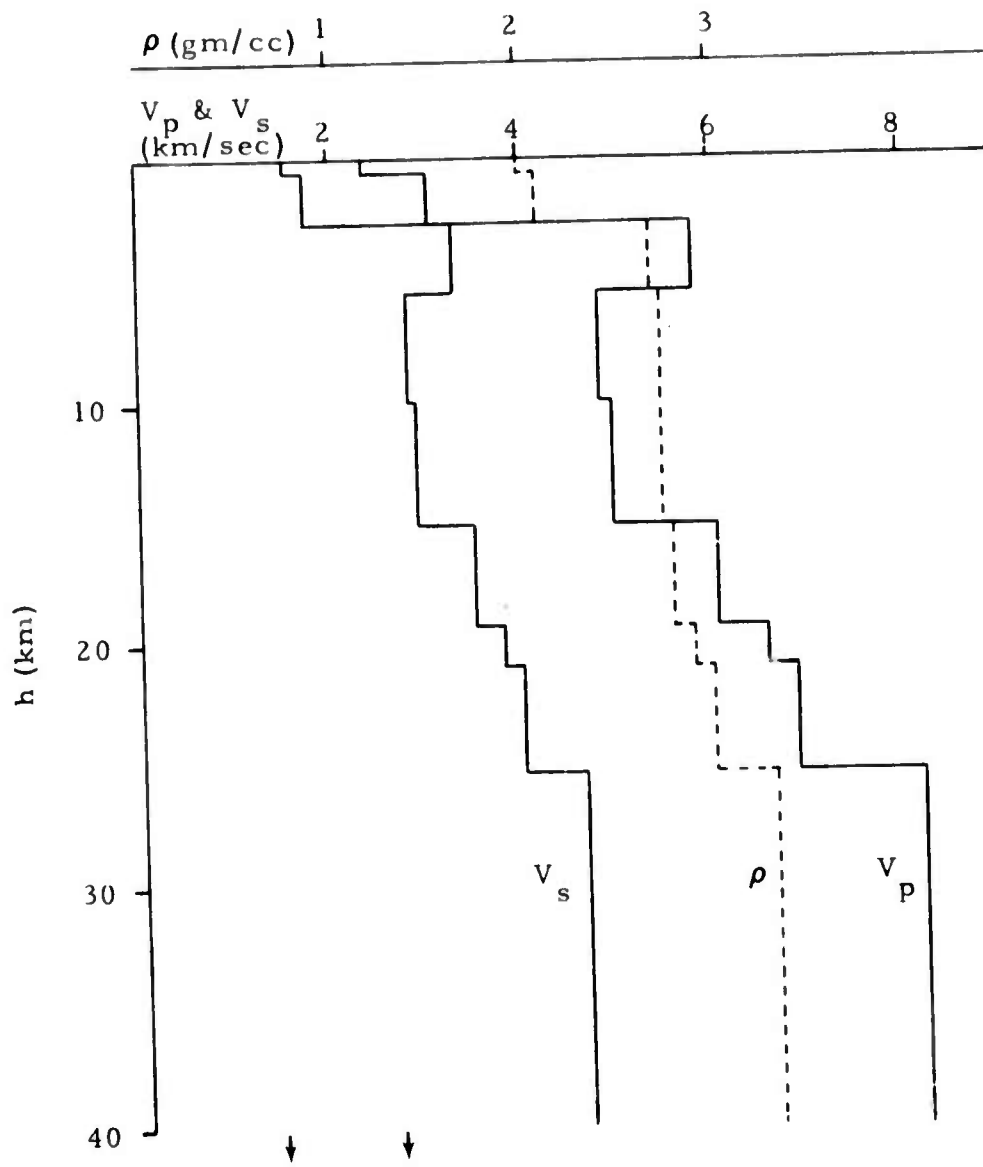
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APPENDIX A  
DISPERSIVE CHARACTERISTICS OF THE  
BEAR VALLEY STRUCTURE

Using the velocity profile obtained by McEvelly (1975), dispersion curves were generated for the structures representing both sides of the fault. Figure A-1 shows the velocity-density profile for the northeast side, and the associated Rayleigh and Love wave dispersion curves are displayed in Figure A-2. Similarly, the velocity-density profile and associated dispersion curves are given in Figures A-3 and A-4, respectively.

The major difference between these structures is the higher velocity material on the southwest side of the fault. This is reflected in the dispersion curves, with higher group and phase velocities between 10 and 30 seconds period for the southwest structure.



Same as Gutenberg-Bullen Earth Model

FIGURE A-1  
BEAR VALLEY STRUCTURE - NORTHEAST  
SIDE OF FAULT

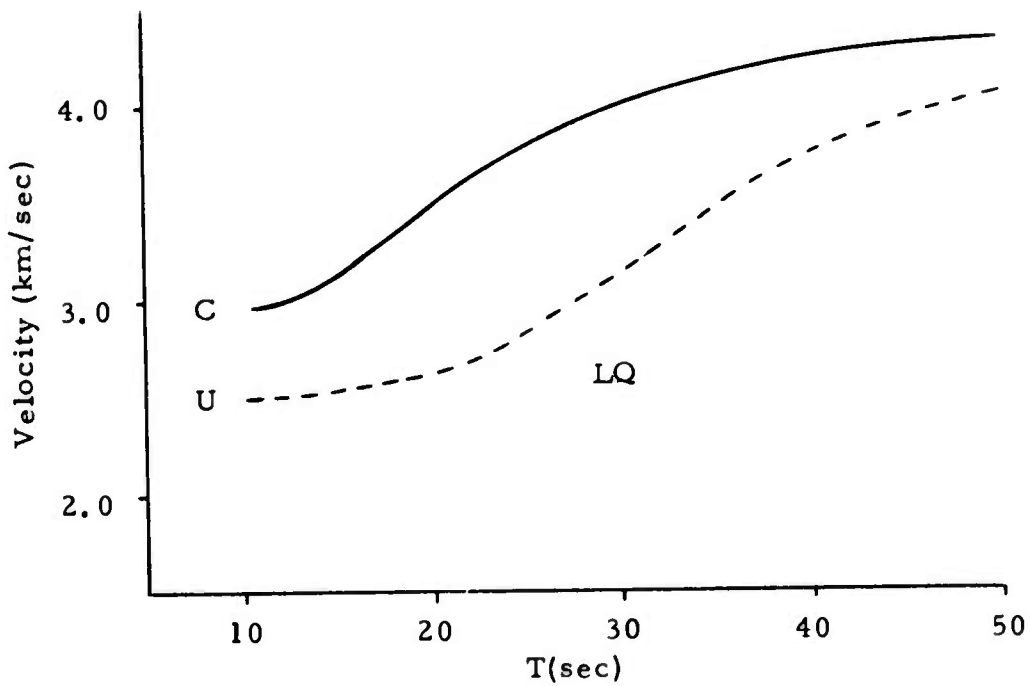
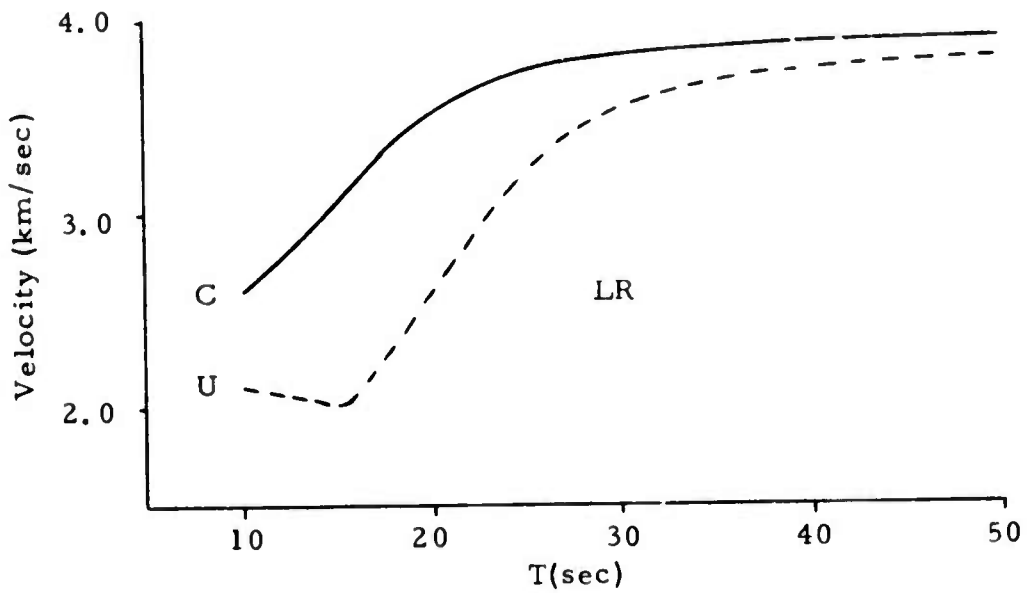
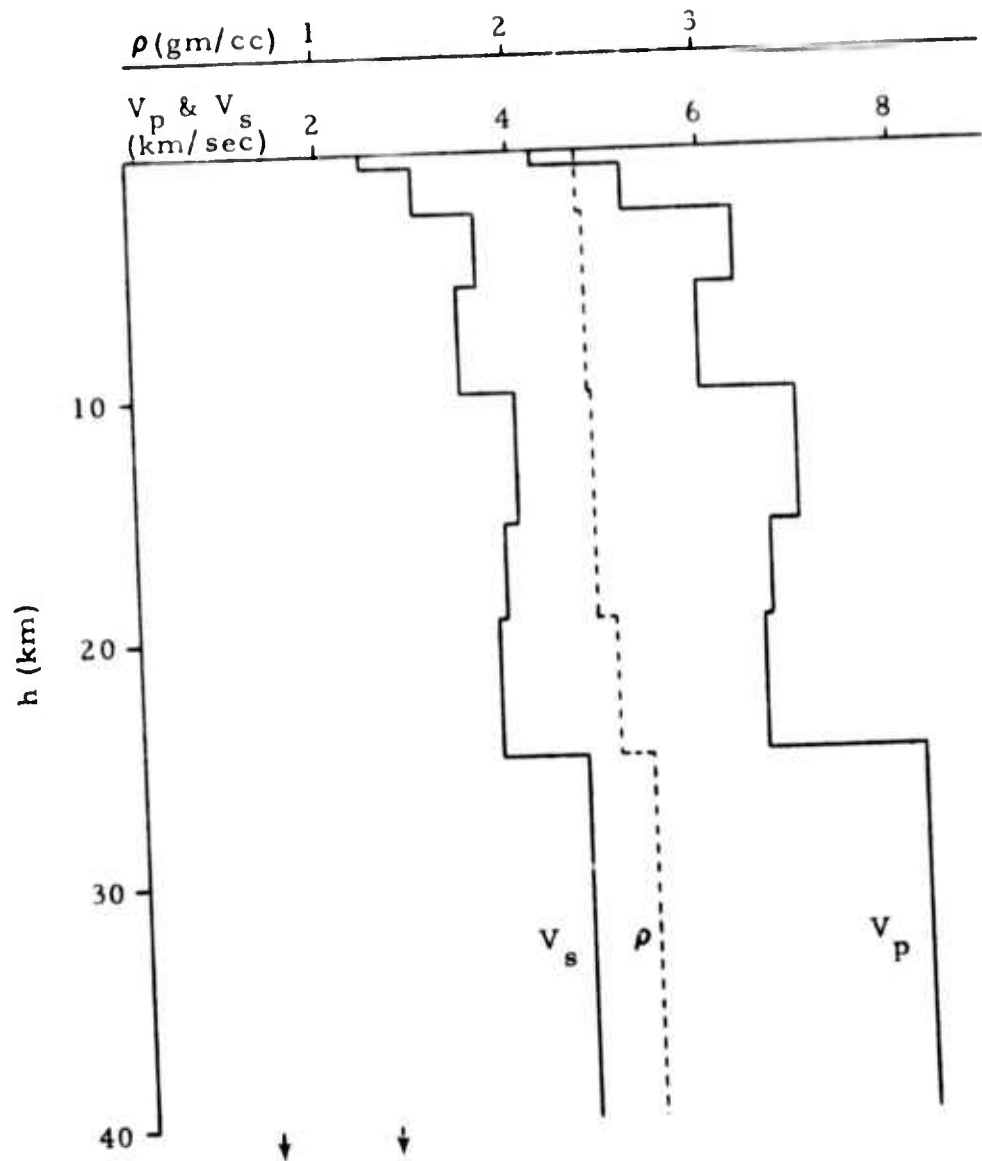


FIGURE A-2  
 RAYLEIGH AND LOVE WAVE DISPERSION  
 FOR BEAR VALLEY STRUCTURE  
 (NORTHEAST SIDE OF FAULT)



Same as Gutenberg-Bullen Earth Model

FIGURE A-3  
 BEAR VALLEY STRUCTURE - SOUTHWEST  
 SIDE OF FAULT

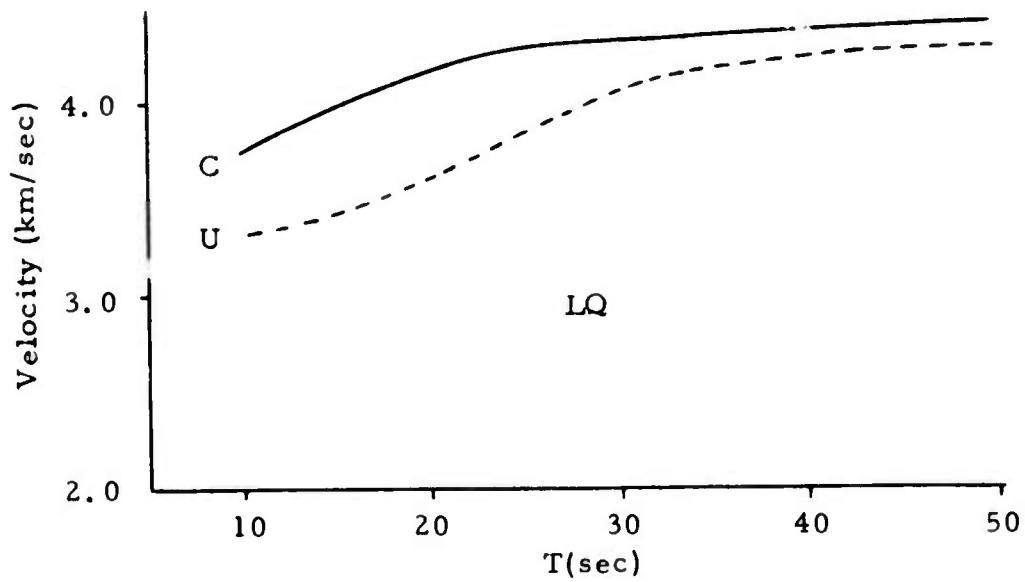
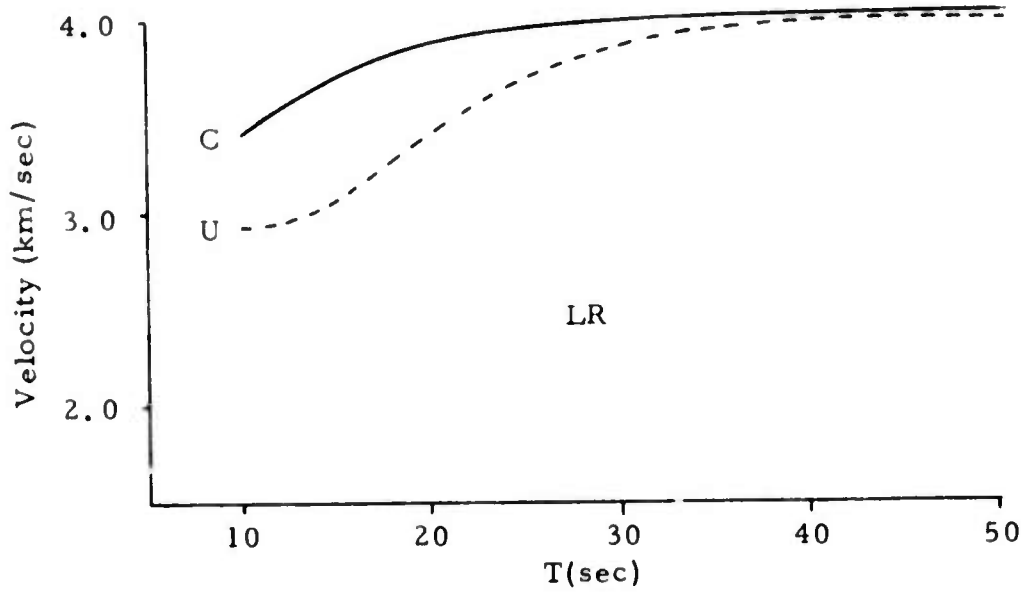


FIGURE A-4  
 RAYLEIGH AND LOVE WAVE DISPERSION  
 FOR BEAR VALLEY STRUCTURE  
 (SOUTHWEST SIDE OF FAULT)



APPENDIX B  
SPECTRAL RESPONSE OF THE  
BEAR VALLEY STRUCTURE

Theoretical spectra were generated for each event using the Bear Valley structures as described in Appendix A. Of particular interest were changes in spectral shape and level. For the Bear Valley event of 22 June 1973, Figures B-1a and B-1b give the Rayleigh and Love wave amplitude spectra as a function of depth for the northeast structure, while Figures B-2a and B-2b give similar spectra for the southwest structure. Figures B-3a and B-3b show the Rayleigh and Love wave radiation patterns at 20 and 30 seconds period for the northeast structure, and Figures B-4a and B-4b give the patterns for the southwest structure.

For the central California event of 28 November 1974, Figures B-5a and B-5b give the Rayleigh and Love wave amplitude spectra as a function of depth for the northeast structure, while Figures B-6a and B-6b give similar spectra for the southwest structure. Figures B-7a and B-7b show the Rayleigh and Love wave radiation patterns at 20 and 30 seconds period for the northeast structure, and Figures B-8a and B-8b give the patterns for the southwest structure.

1-DPH/BEV/622/NE

DOUBLE COUPLE

DIP ANGLE= 70.0

SLIP ANGLE= 30.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LR-AMP

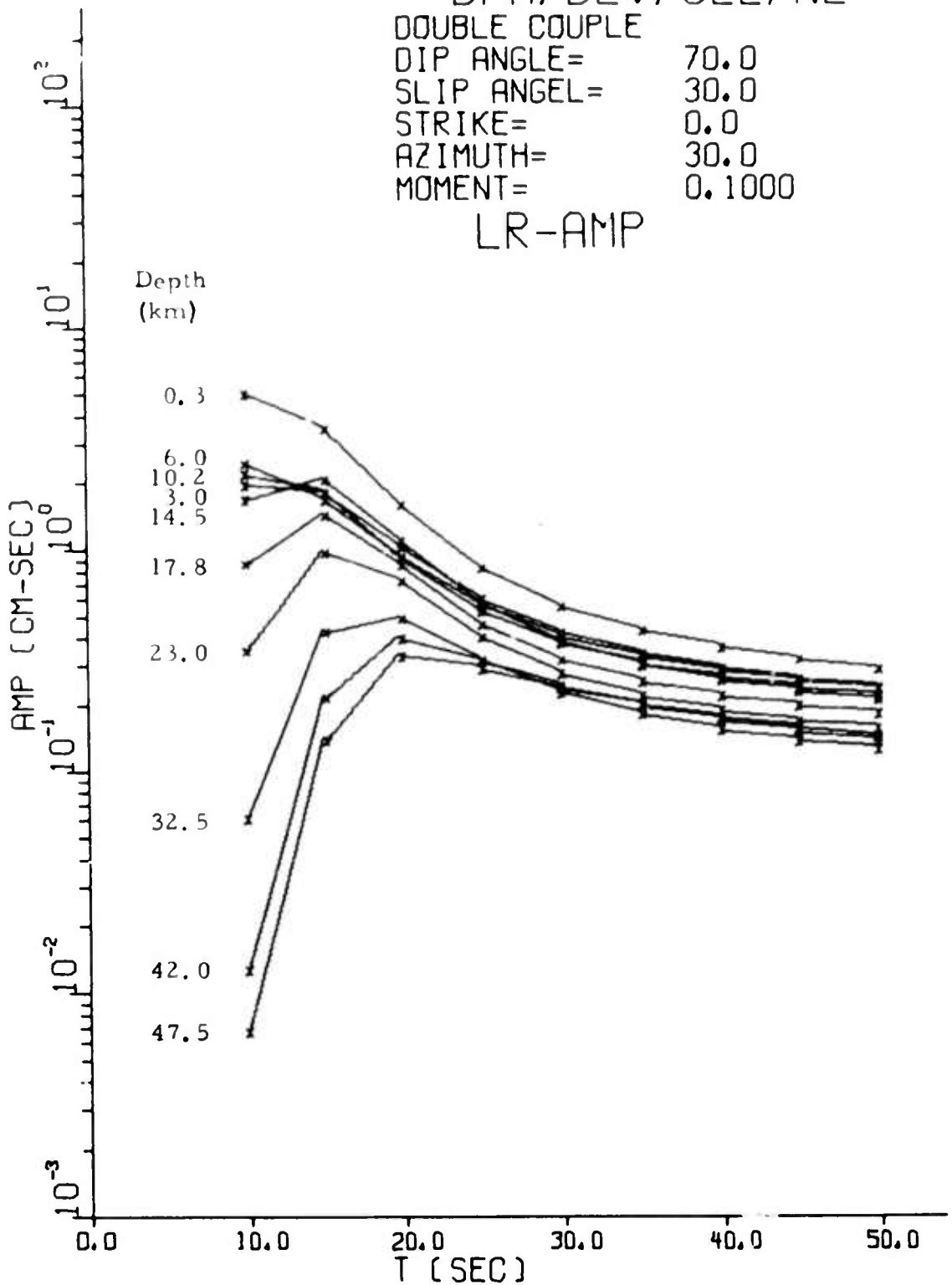


FIGURE B-1a

FUNDAMENTAL MODE RAYLEIGH WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 22 JUNE 1973 BEAR VALLEY EVENT IN THE NORTHEAST STRUCTURE

V-DPH/BEV/622/NE

DOUBLE COUPLE

DIP ANGLE= 70.0

SLIP ANGLE= 30.0

STRIK = 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LQ-AMP

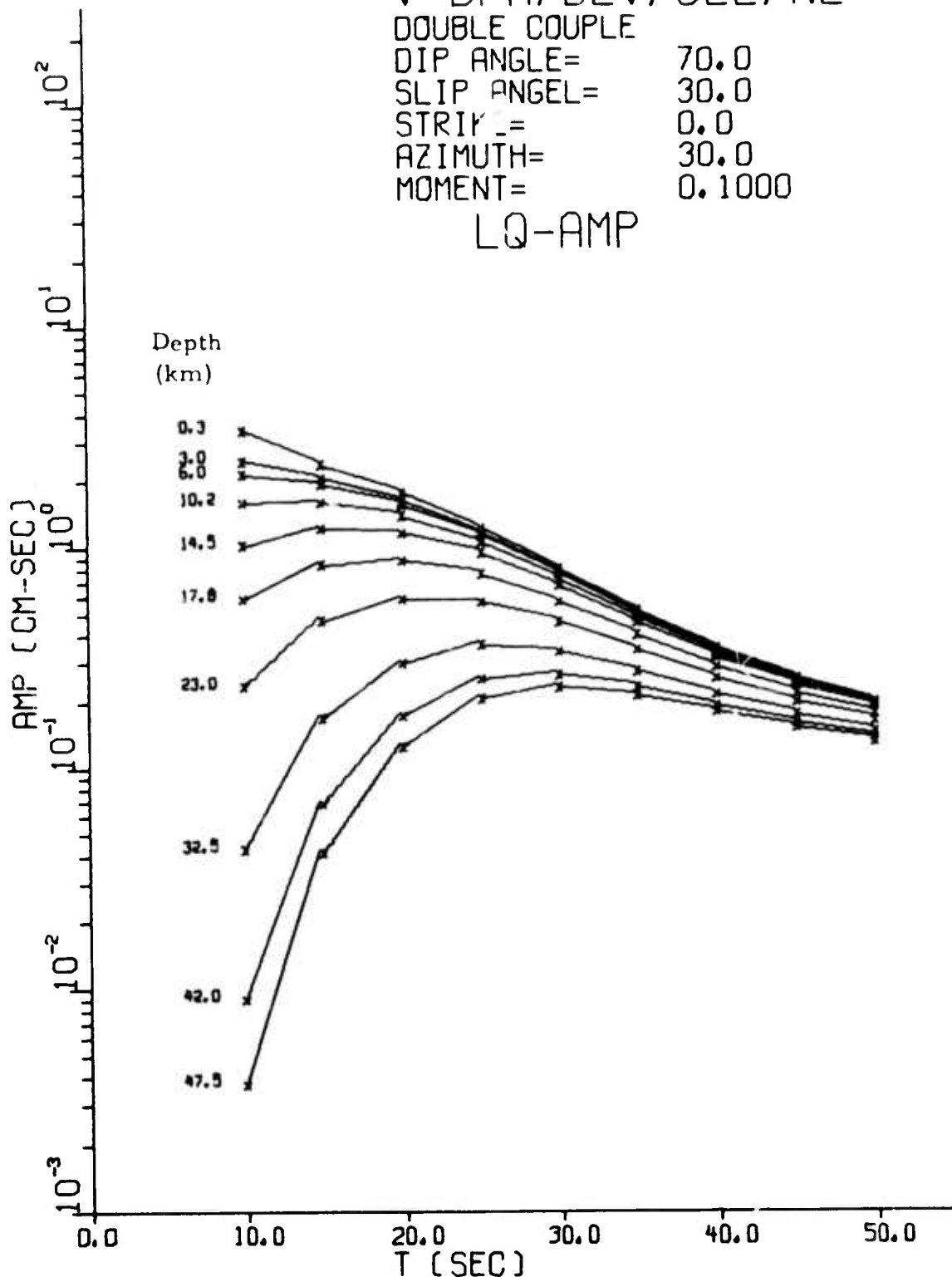


FIGURE B-1b

FUNDAMENTAL MODE LOVE WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 22 JUNE 1973 BEAR VALLEY EVENT IN THE NORTHEAST STRUCTURE

V-DPH/BEV/622/SW

DOUBLE COUPLE

DIP ANGLE= 70.0

SLIP ANGLE= 30.0

STRIKE= 0.7

AZIMUTH= 30.0

MOMENT= 0.1000

LR-AMP

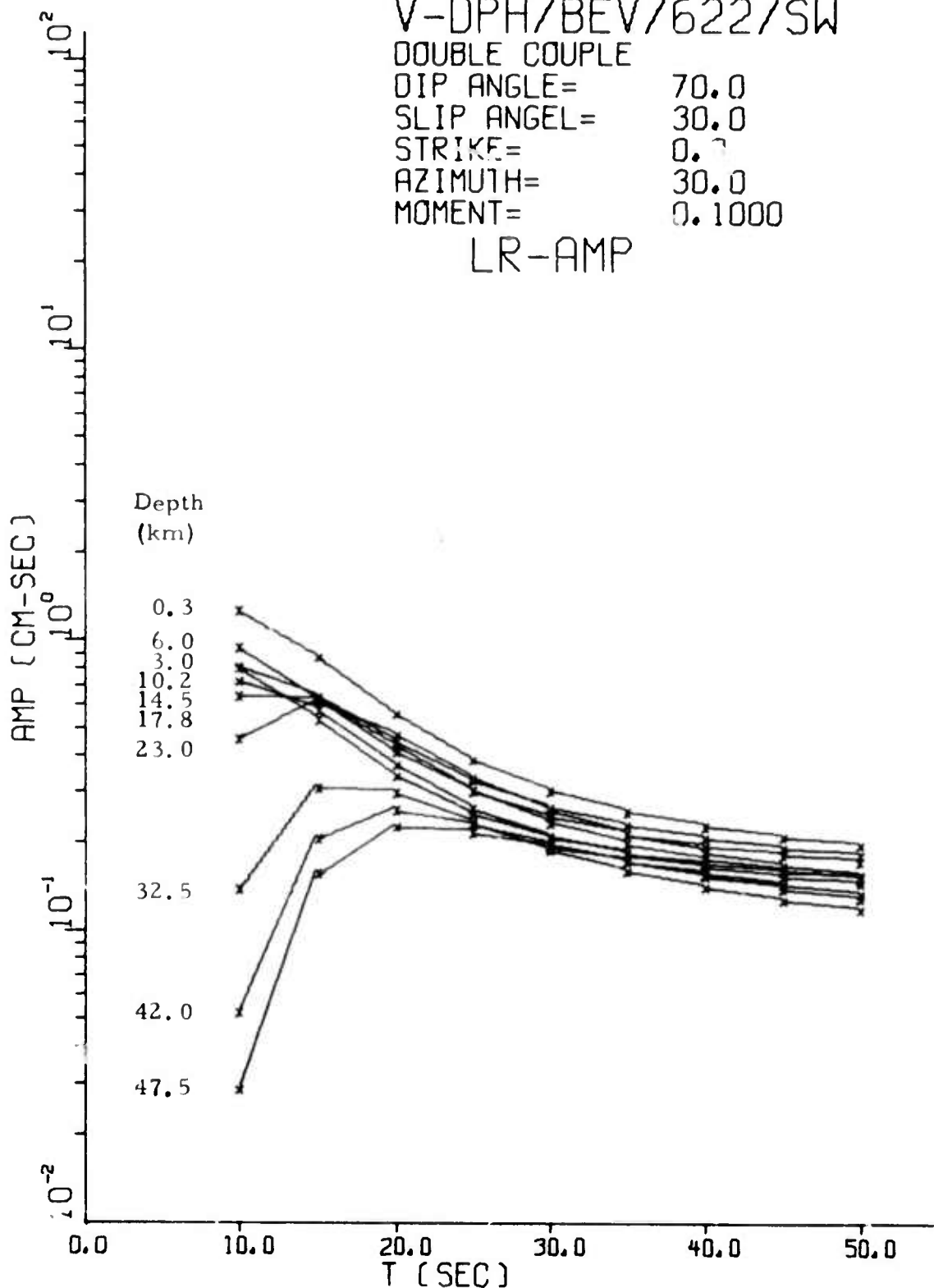


FIGURE B-2a

FUNDAMENTAL MODE RAYLEIGH WAVE SPECTRA USING THE  
SOURCE MECHANISM OF THE 22 JUNE 1973 BEAR VALLEY  
EVENT IN THE SOUTHWEST STRUCTURE

V-DPH/BEV/622/SW

DOUBLE COUPLE

DIP ANGLE= 70.0

SLIP ANGEL= 30.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LQ-AMP

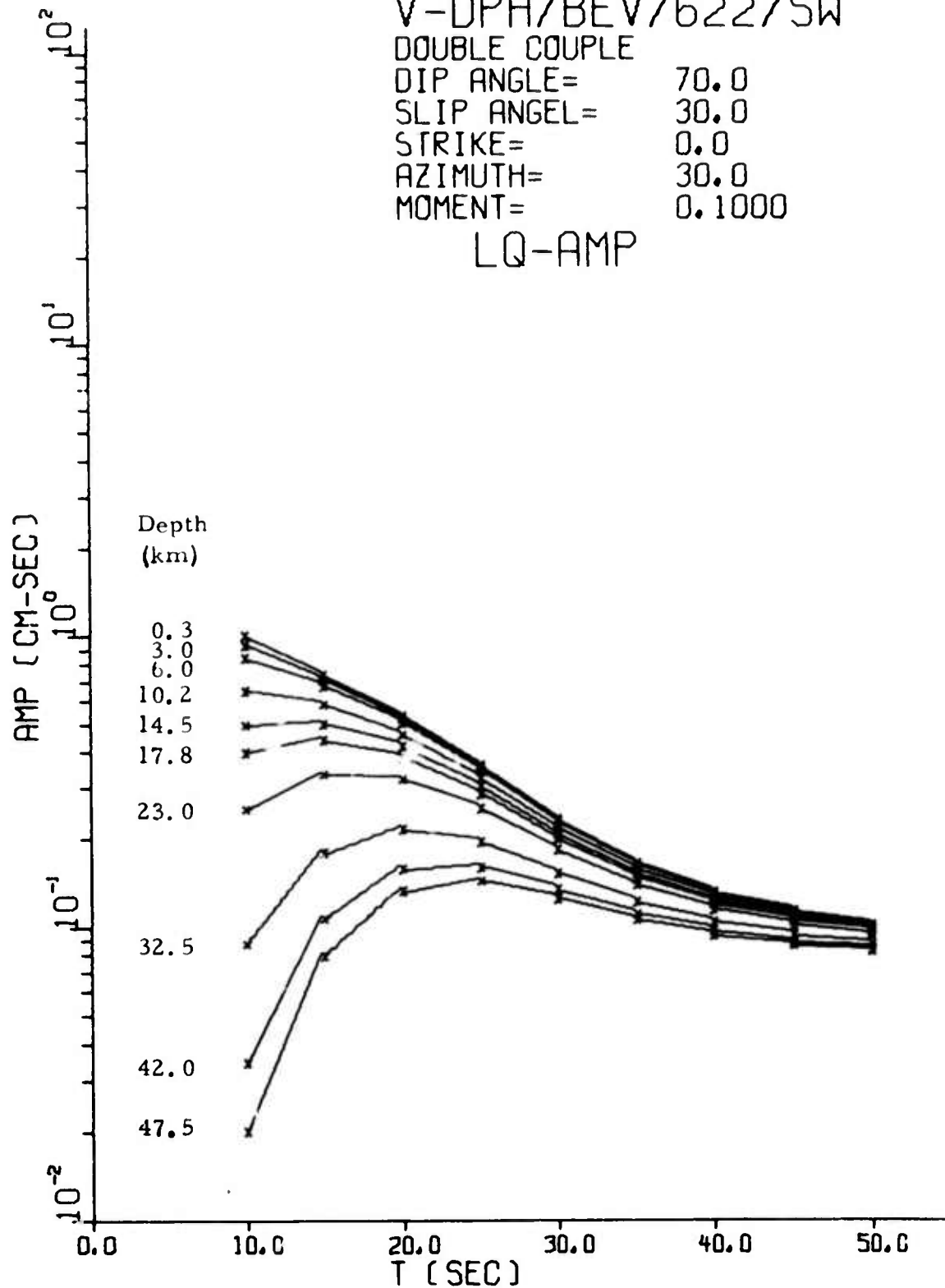
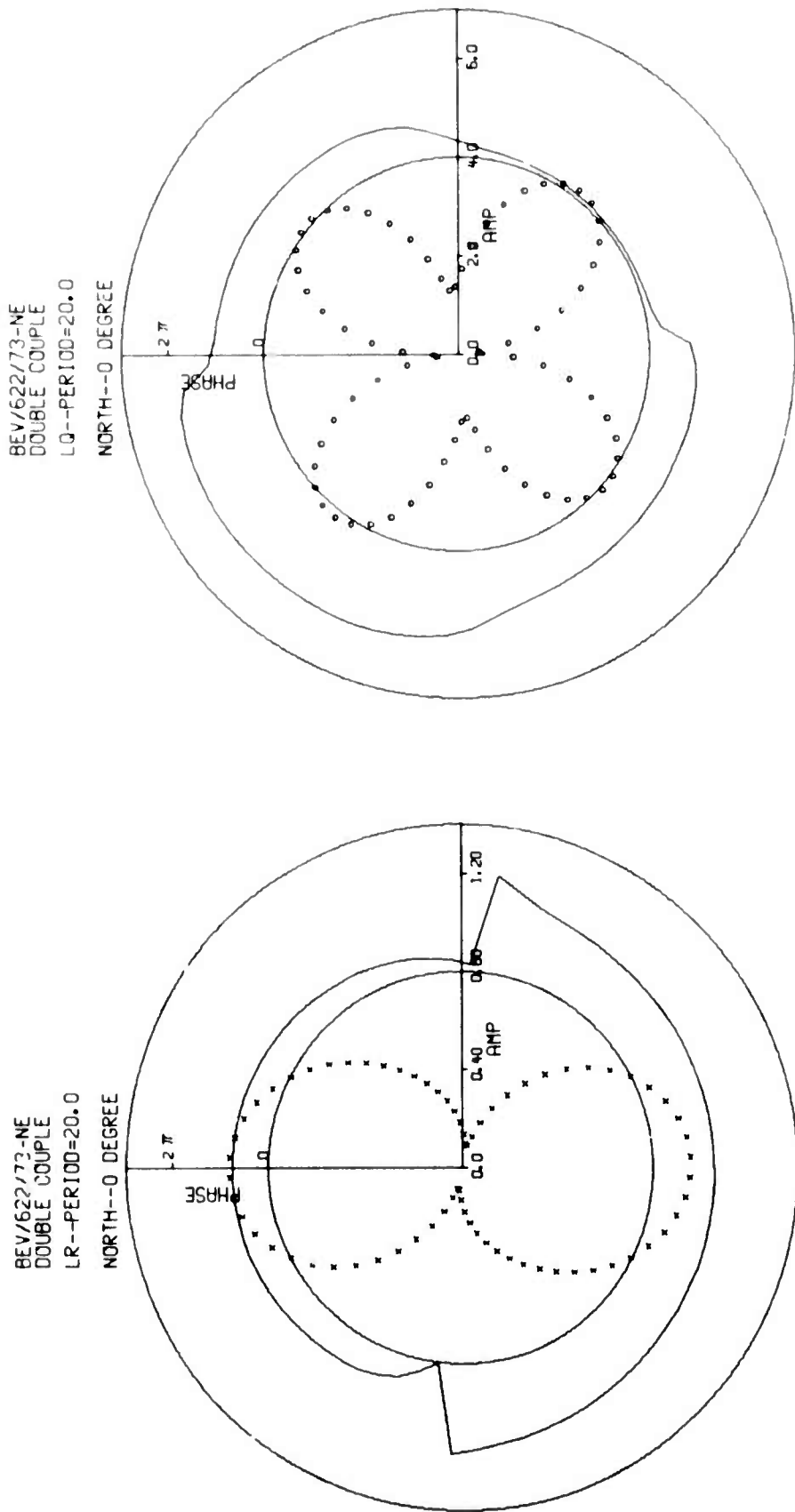


FIGURE B-2b

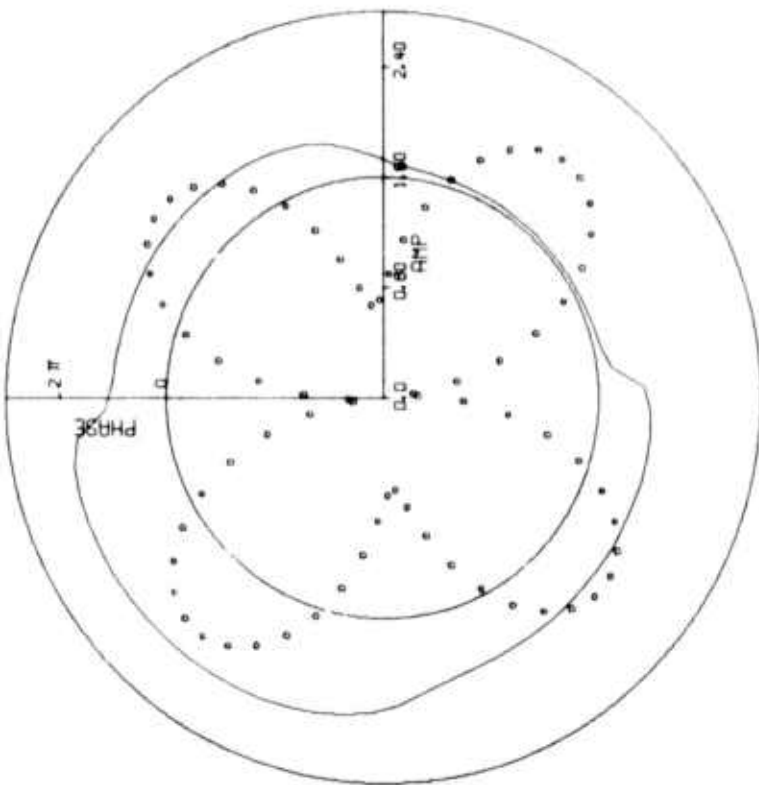
FUNDAMENTAL MODE LOVE WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 22 JUNE 1973 BEAR VALLEY EVENT IN THE SOUTHWEST STRUCTURE



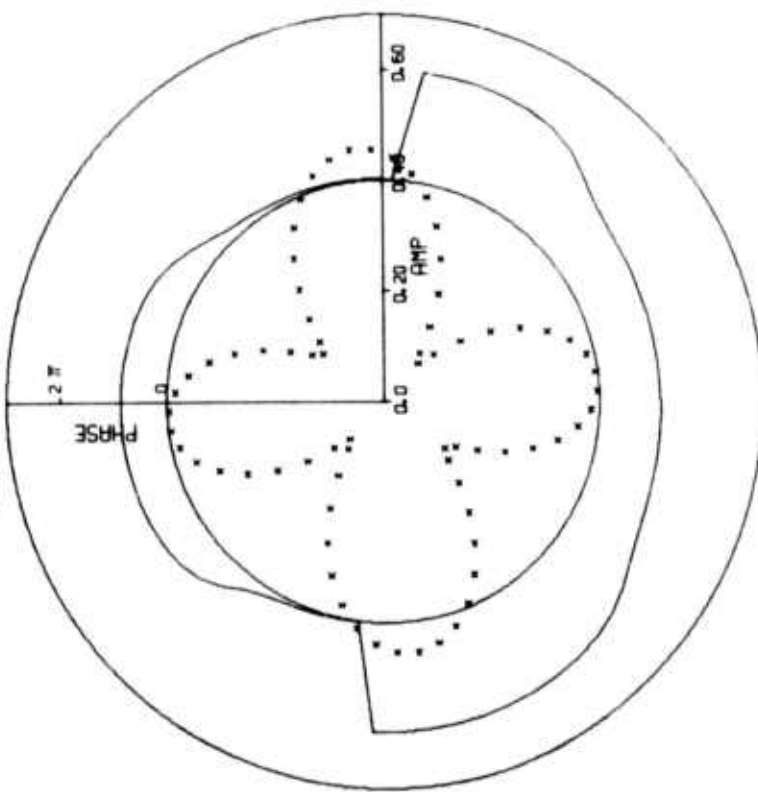
B-6

FIGURE B-3a  
FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
(T = 20 SECONDS) USING THE SOURCE MECHANISM OF THE  
22 JUNE 1973 BEAR VALLEY EVENT IN THE  
NORTHEAST STRUCTURE

BEV/622/73-NE  
 DOUBLE COUPLE  
 LQ--PERIOD=30.0  
 NORTH--0 DEGREE



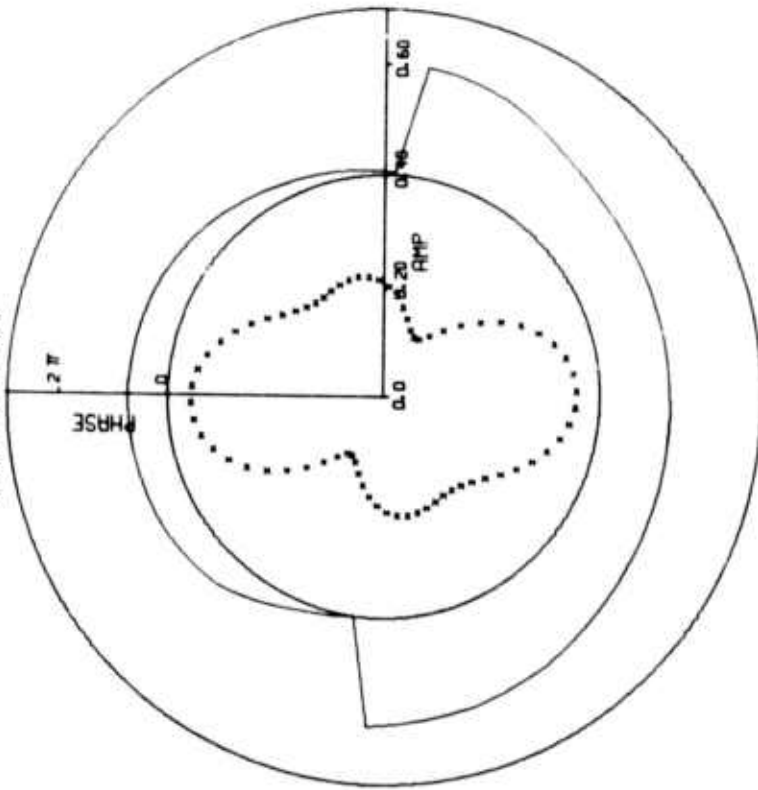
BEV/622/73-NE  
 DOUBLE COUPLE  
 LR--PERIOD=30.0  
 NORTH--0 DEGREE



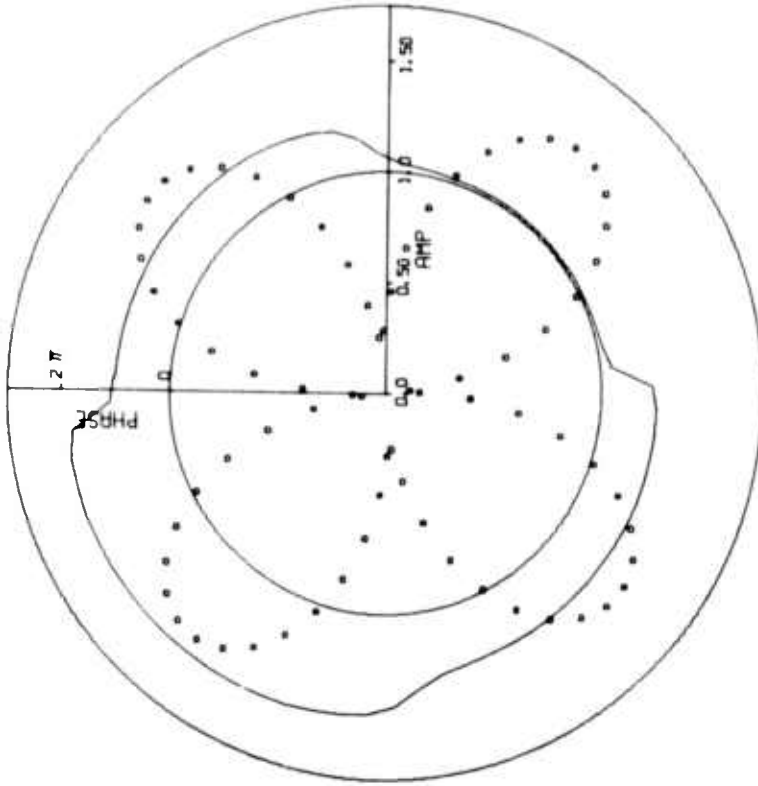
B-7

FIGURE B-3b  
 FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
 (T = 30 SECONDS) USING THE SOURCE MECHANISM OF THE  
 22 JUNE 1973 BEAR VALLEY EVENT IN THE  
 NORTHEAST STRUCTURE

BEV/622/73-SH  
 DOUBLE COUPLE  
 LR--PERIOD=20.0  
 NORTH--0 DEGREE



BEV/622/73-SW  
 DOUBLE COUPLE  
 LR--PERIOD=20.0  
 NORTH--0 DEGREE

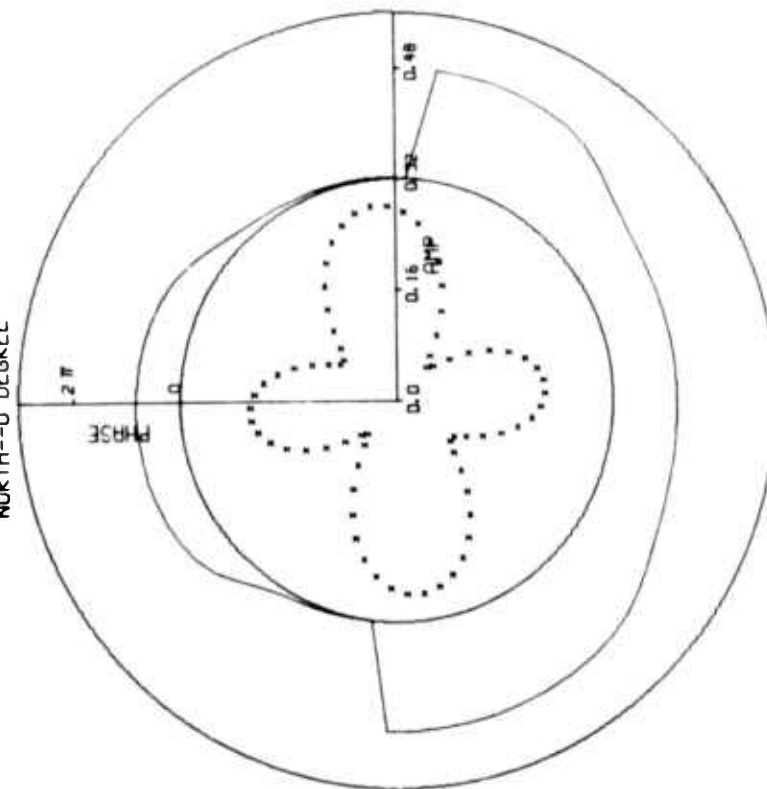


B-8

FIGURE B-4a  
 FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
 (T = 20 SECONDS) USING THE SOURCE MECHANISM OF THE  
 22 JUNE 1973 BEAR VALLEY EVENT IN THE  
 SOUTHWEST STRUCTURE



BEV/622/73-SW  
 DOUBLE COUPLE  
 LR--PERIOD=30.0  
 NORTH--0 DEGREE



BEV/622/73-SW  
 DOUBLE COUPLE  
 LG--PERIOD=30.0  
 NORTH--0 DEGREE

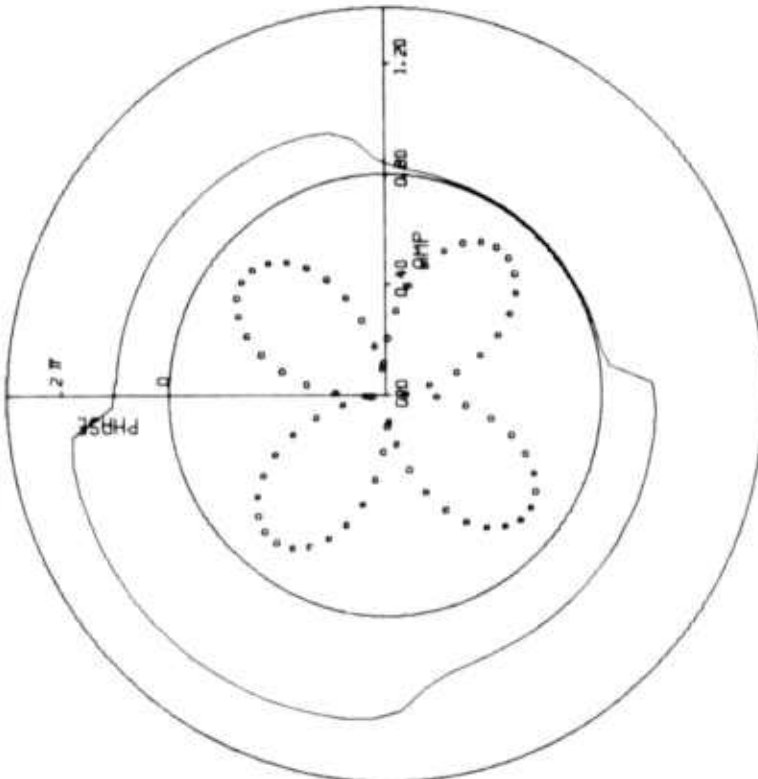


FIGURE B-4b  
 FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
 (T = 30 SECONDS) USING THE SOURCE MECHANISM OF THE  
 22 JUNE 1973 BEAR VALLEY EVENT IN THE  
 SOUTHWEST STRUCTURE

V-DPH/CCA/332/NE

DOUBLE COUPLE

DIP ANGLE= 90.0

SLIP ANGLE= 0.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LR-AMP

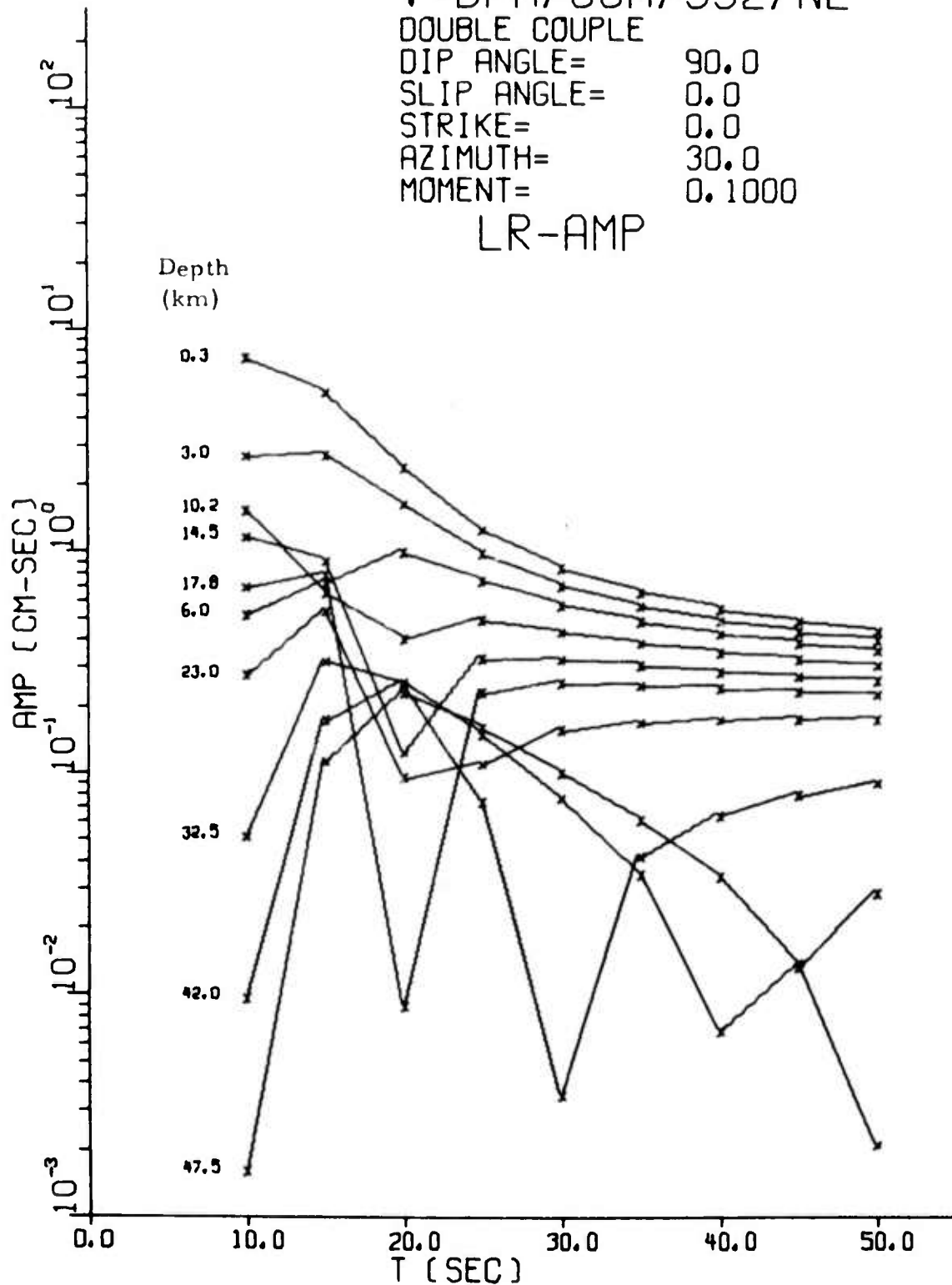


FIGURE B-5a

FUNDAMENTAL MODE RAYLEIGH WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT IN THE NORTHEAST STRUCTURE

V-DPH/CCA/332/NE

DOUBLE COUPLE

DIP ANGLE= 90.0

SLIP ANGLE= 0.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LQ-AMP

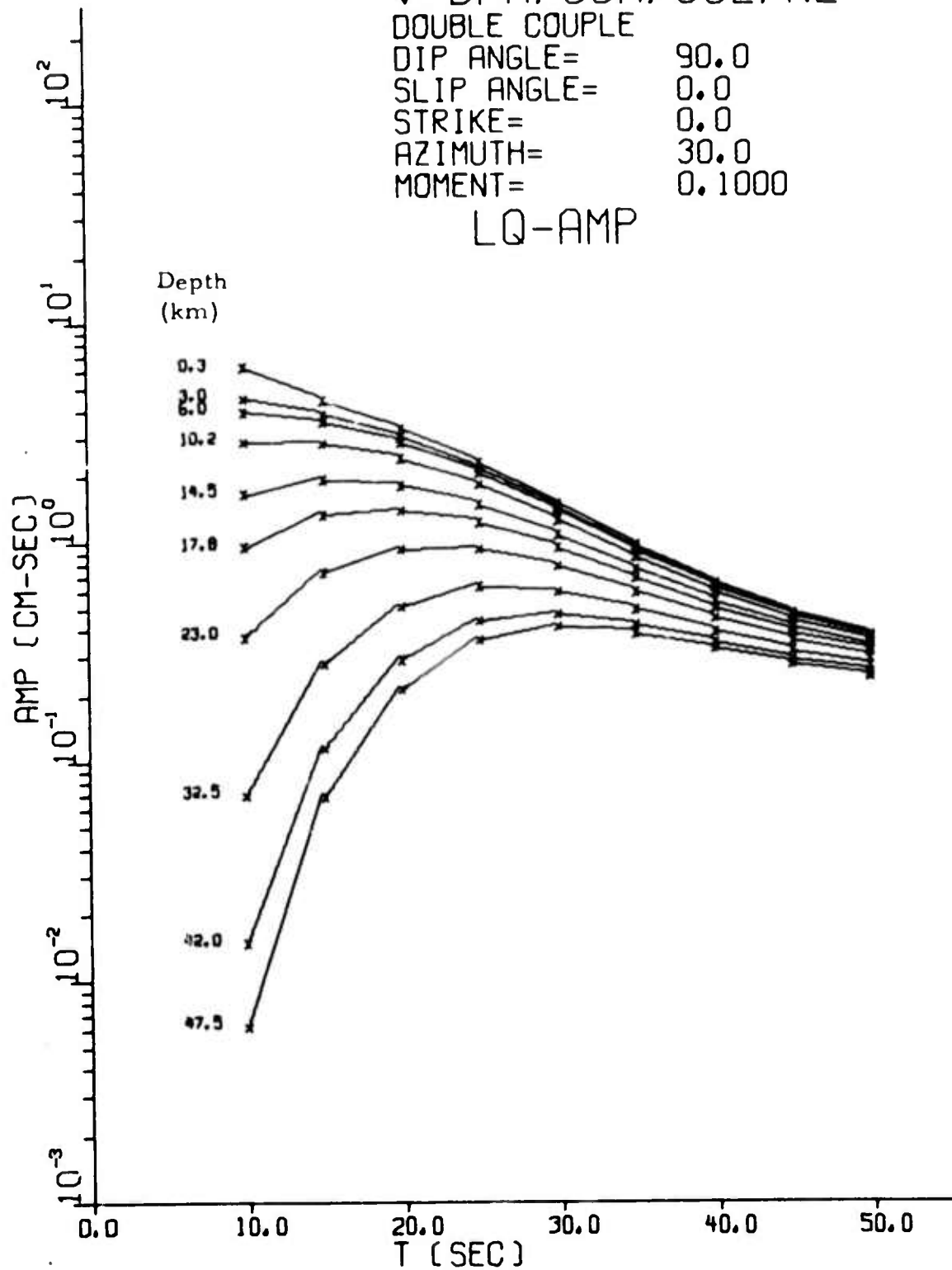


FIGURE B-5b

FUNDAMENTAL MODE LOVE WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT IN THE NORTHEAST STRUCTURE

V-DPH/CCA/332/SW

DOUBLE COUPLE

DIP ANGLE= 90.0

SLIP ANGLE= 0.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LR-AMP

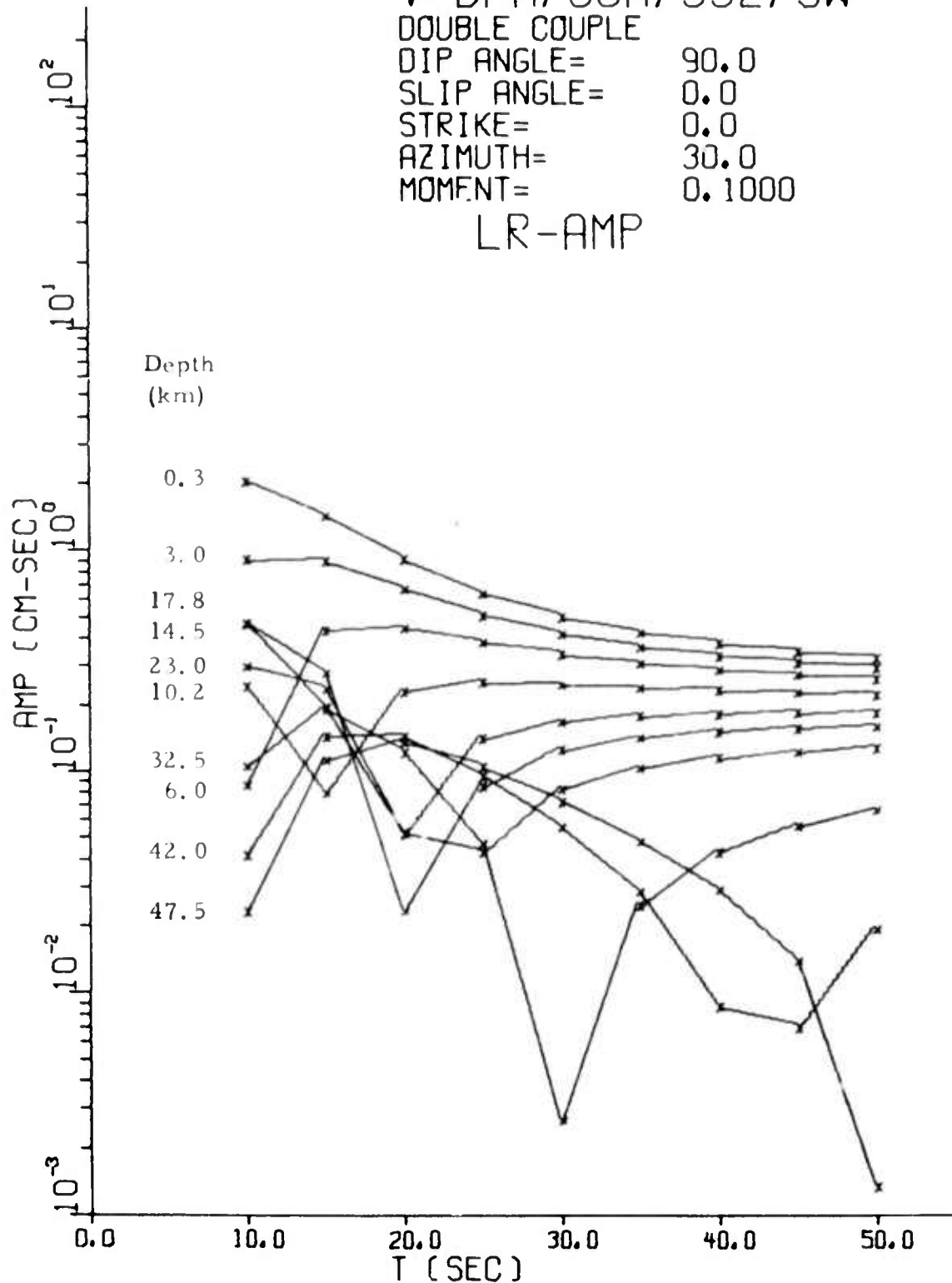


FIGURE B-6a

FUNDAMENTAL MODE RAYLEIGH WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT IN THE SOUTHWEST STRUCTURE

V-DPH/CCA/332/SW

DOUBLE COUPLE

DIP ANGLE= 90.0

SLIP ANGLE= 0.0

STRIKE= 0.0

AZIMUTH= 30.0

MOMENT= 0.1000

LQ-AMP

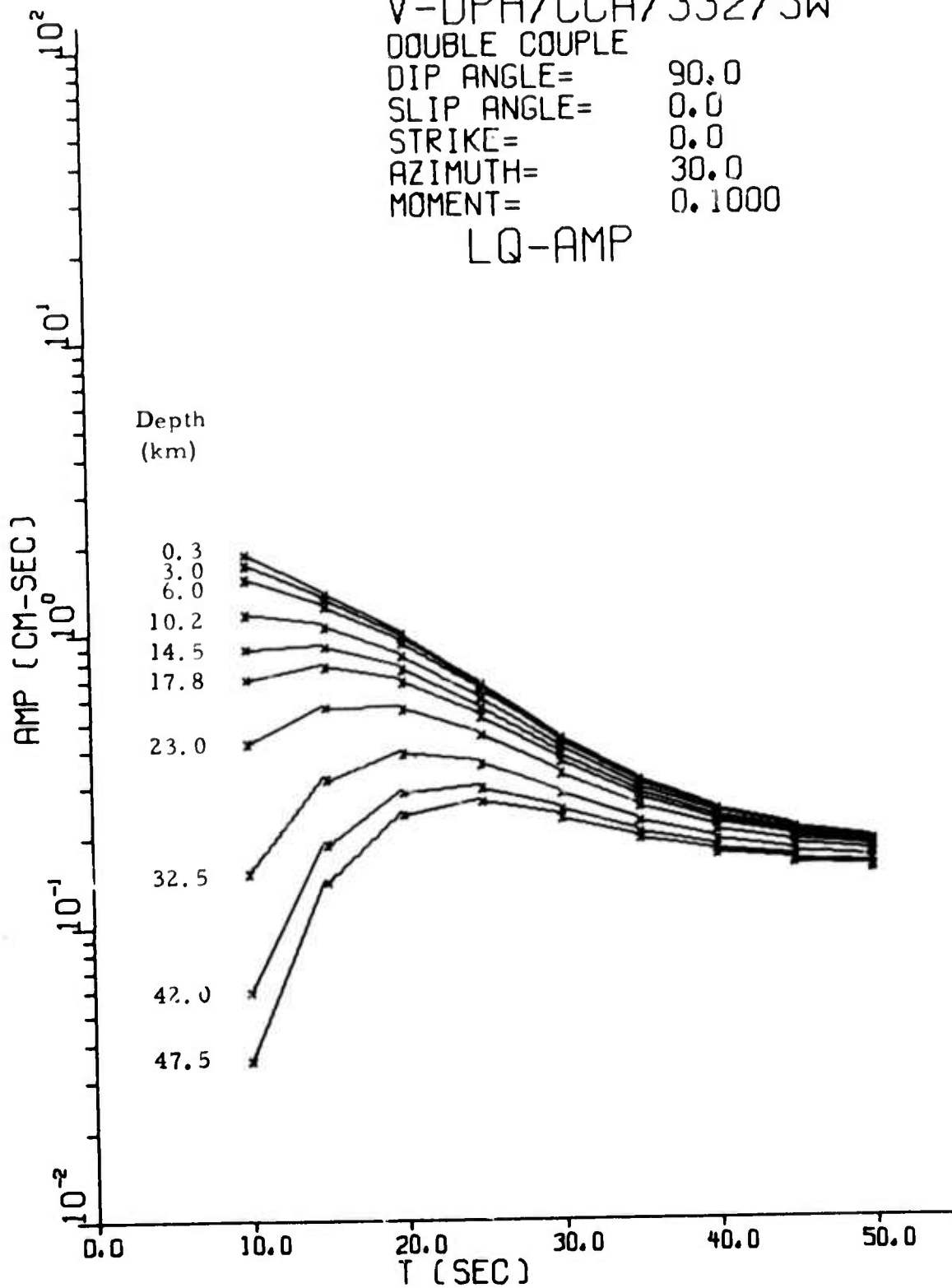


FIGURE B-6b

FUNDAMENTAL MODE LOVE WAVE SPECTRA USING THE SOURCE MECHANISM OF THE 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT IN THE SOUTHWEST STRUCTURE

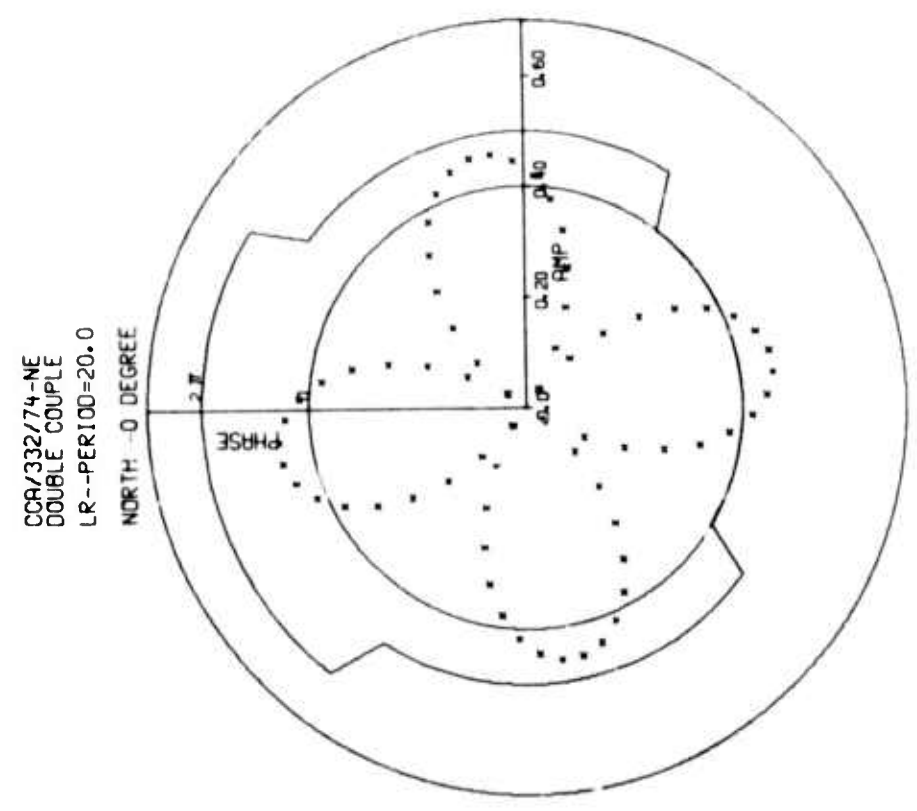
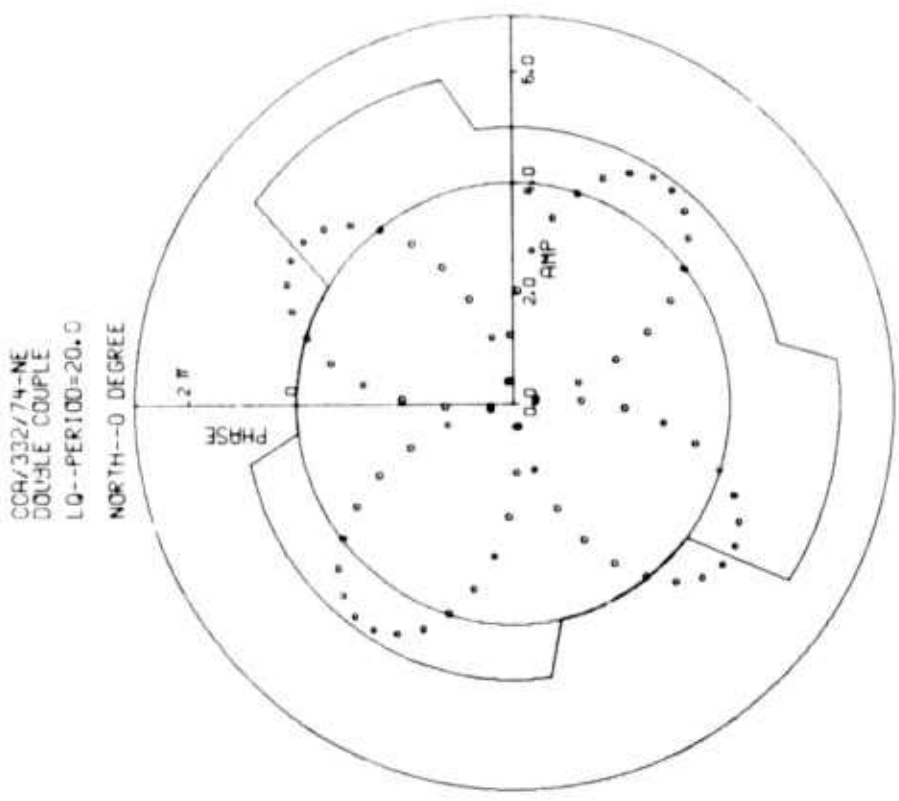


FIGURE B-7a  
FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
(T = 20 SECONDS) USING THE SOURCE MECHANISM OF THE  
28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT  
IN THE NORTHEAST STRUCTURE

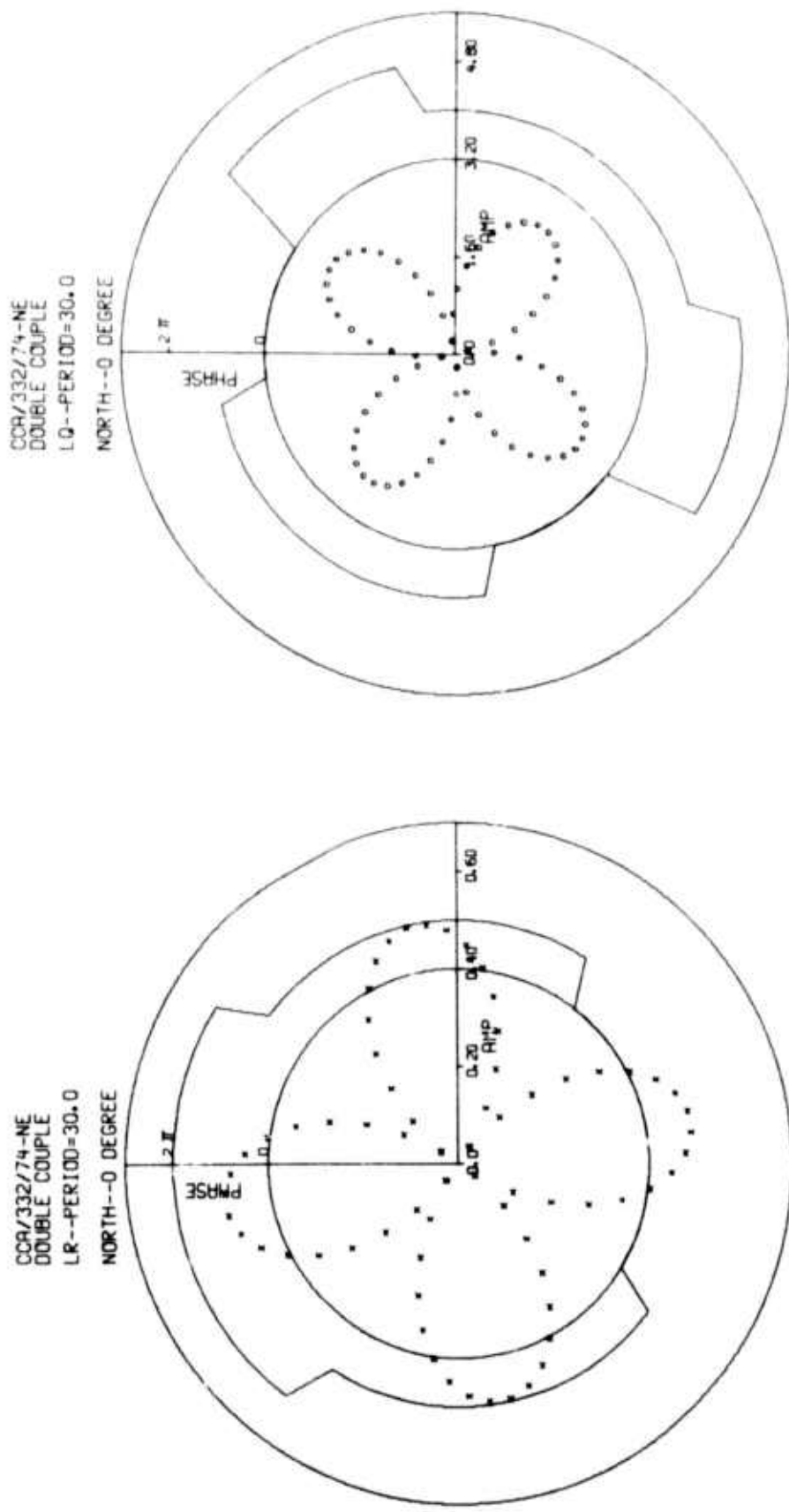


FIGURE B-7b  
 FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
 (T = 30 SECONDS) USING THE SOURCE MECHANISM OF THE  
 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT  
 IN THE NORTHEAST STRUCTURE

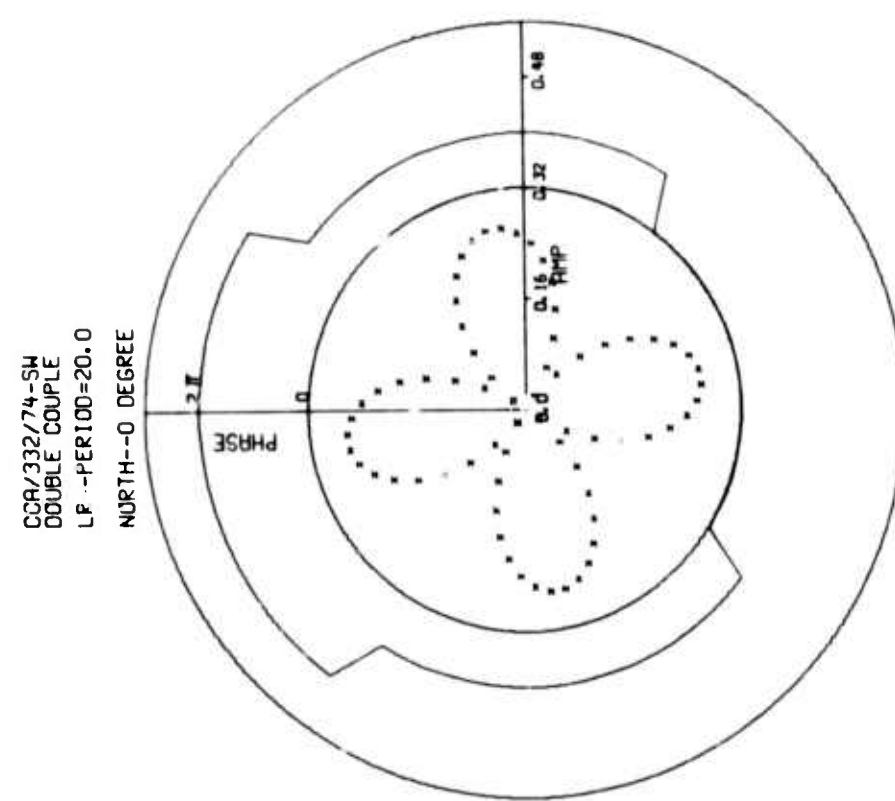
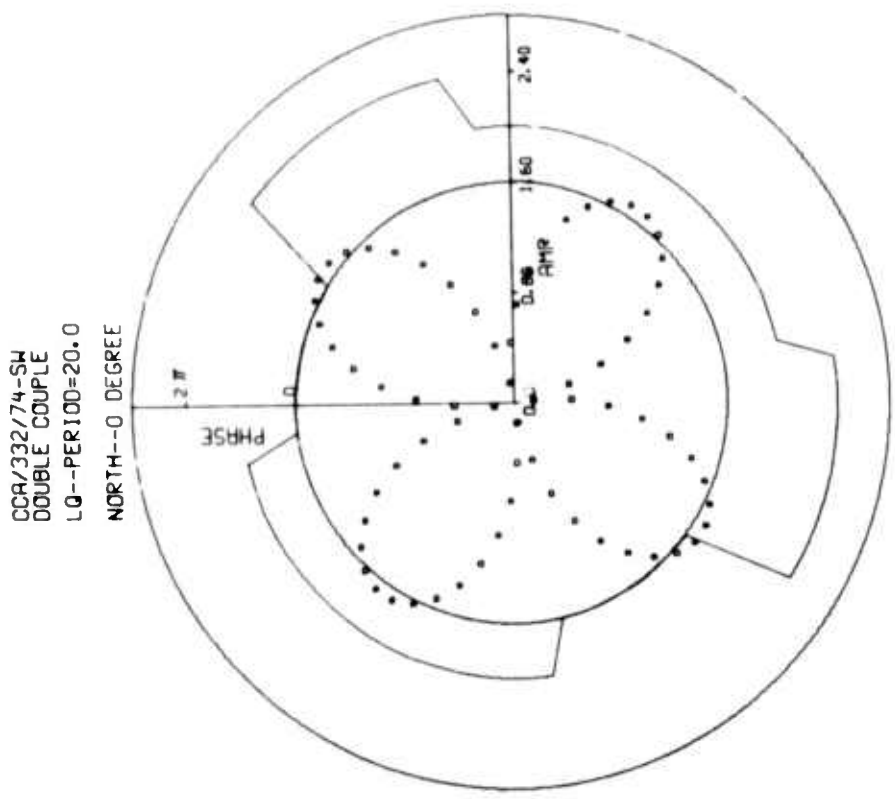


FIGURE B-8a  
 FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
 (T = 20 SECONDS) USING THE SOURCE MECHANISM OF THE  
 28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT  
 IN THE SOUTHWEST STRUCTURE



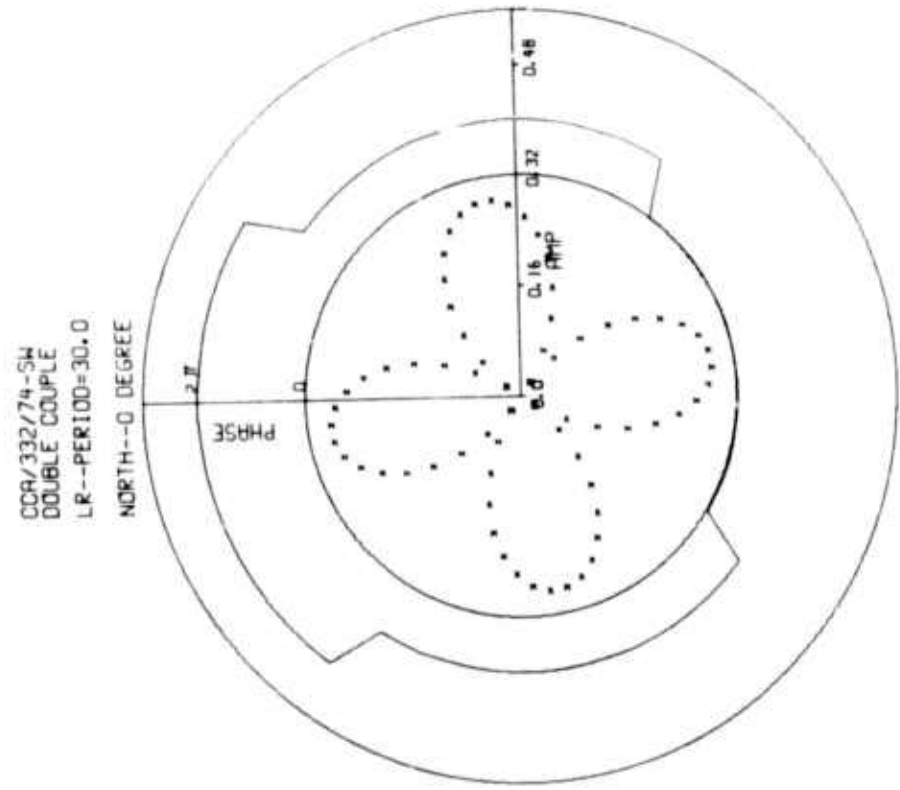
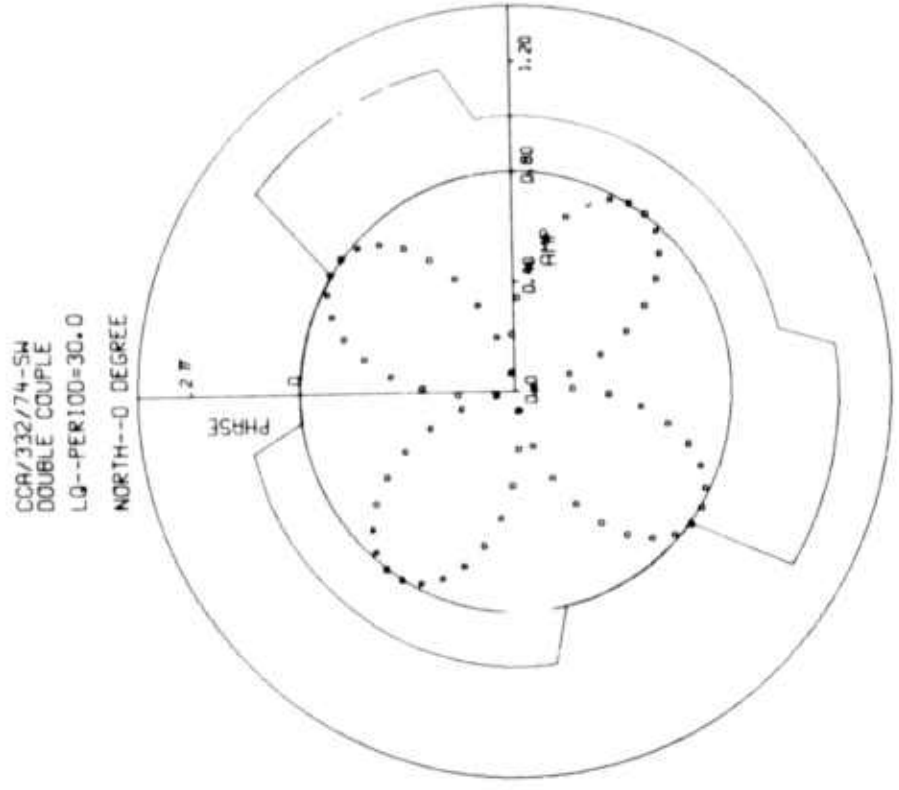


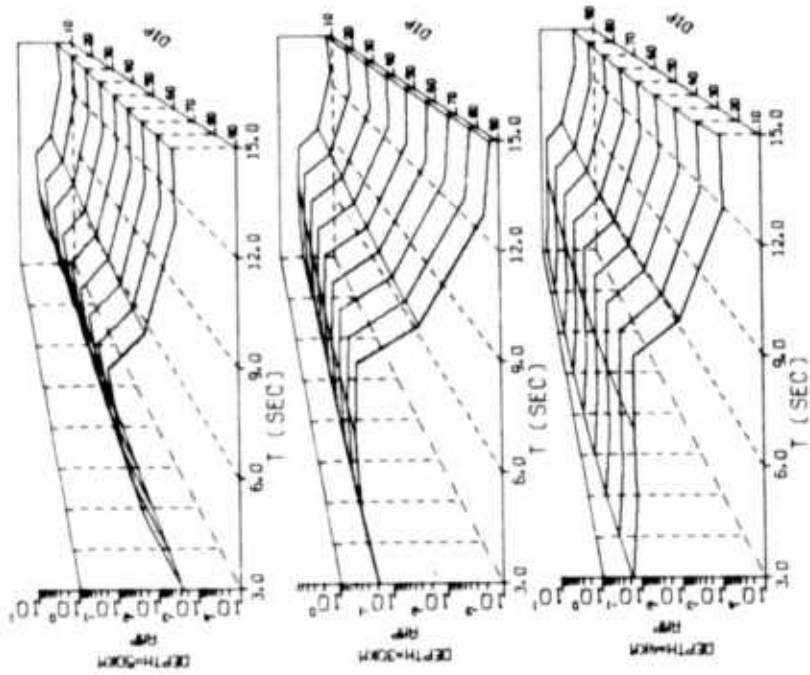
FIGURE B-8b  
FUNDAMENTAL MODE RAYLEIGH AND LOVE WAVE RADIATION  
(T = 30 SECONDS) USING THE SOURCE MECHANISM OF THE  
28 NOVEMBER 1974 CENTRAL CALIFORNIA EVENT  
IN THE SOUTHWEST STRUCTURE

APPENDIX C  
THEORETICAL FIRST HIGHER MODE  
SURFACE WAVE SPECTRA

As in previous work (Turnbull, et al., 1975), theoretical first higher mode Rayleigh and Love wave spectra were generated using the Harkrider (1964) formulation of a double couple source in a layered half space. Our objective is to identify any special spectral characteristics (such as shape or amplitude level) that would be useful in determining source depth or structure in the source region.

Figures C-1a through C-1d display the variation of dip, slip, and strike for first higher mode Rayleigh and Love waves over the period range of 3 to 15 seconds and for three representative source depths in a Gutenberg-Bullen earth model. Using the Hamilton-Healy earth model, the effect of dip angle variation is displayed over the same period range and for three source depths in Figure C-2. Finally, in Figure C-3, higher mode surface wave spectra over the period range of 15 to 40 seconds with dip angle variation is shown for three source depths in a Gutenberg-Bullen earth model.

GB-1ST HIGH / LOVE  
 DOUBLE-COUPLE = 0.0  
 SLIP ANGLE = 0.0  
 STRIKE = 0.0  
 MOMENT = 0.10  
 AZIMUTH = 30.0



GB-1ST HIGH/RAYLEIGH  
 DOUBLE-COUPLE = 0.0  
 SLIP ANGLE = 0.0  
 STRIKE = 0.0  
 MOMENT = 0.10  
 AZIMUTH = 30.0

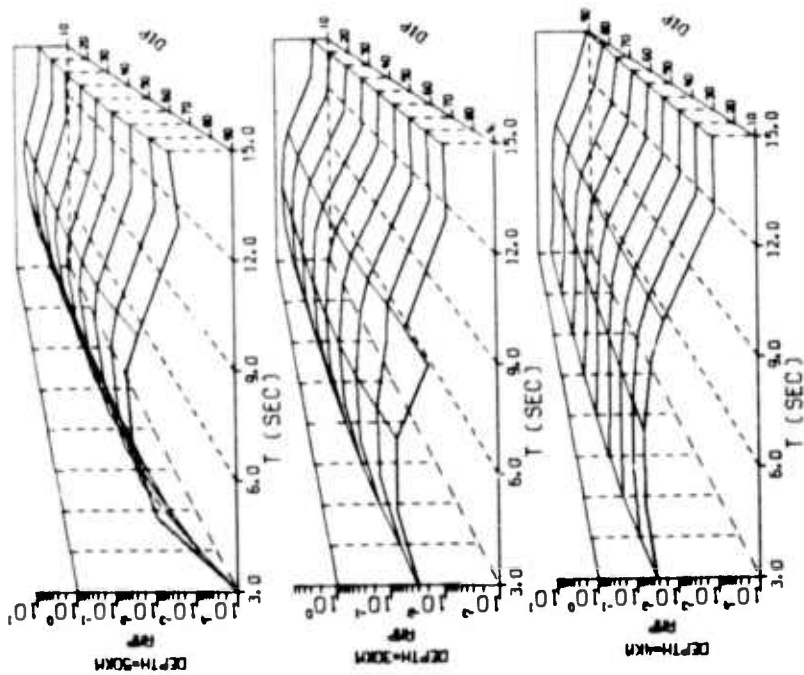


FIGURE C-1a  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A GUTENBERG-BULLEN EARTH MODEL:  
 Period Range 3 to 15 Seconds, Dip ( $\delta$ ) = Variable, Slip ( $\lambda$ ) =  $0^\circ$ , Strike ( $\theta$ ) =  $0^\circ$

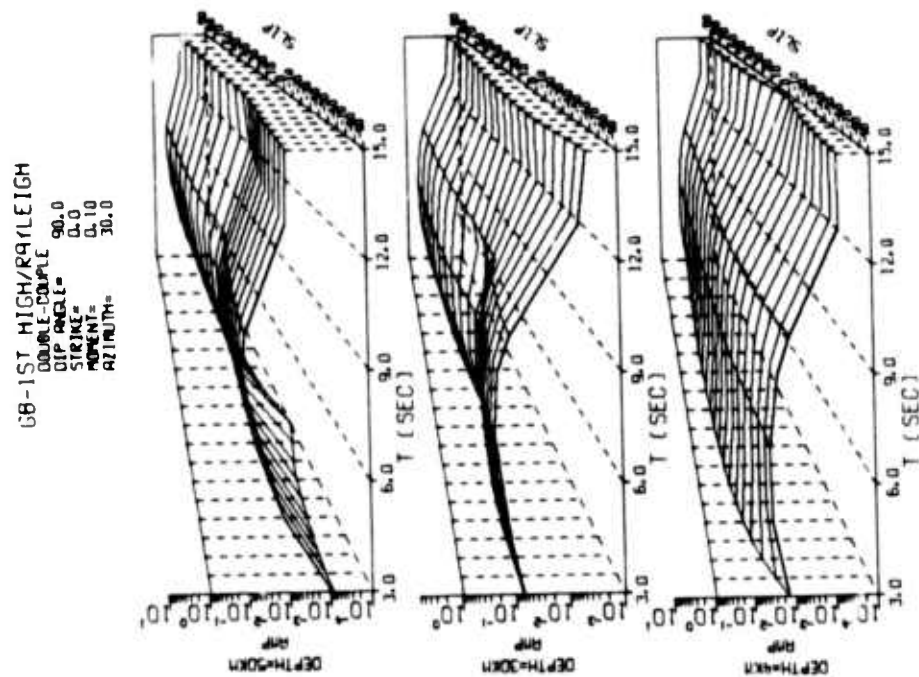
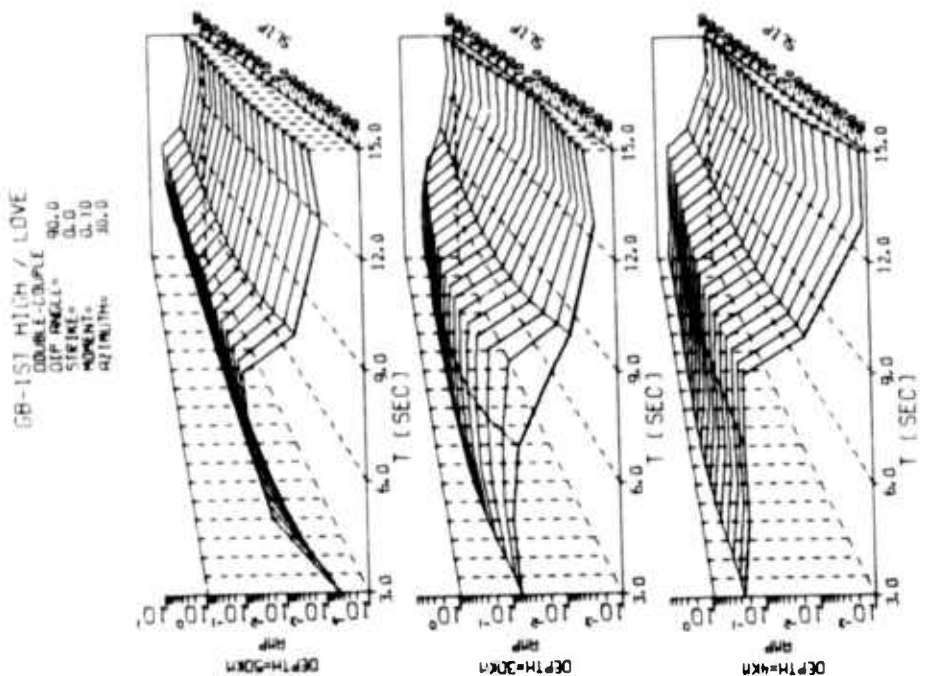
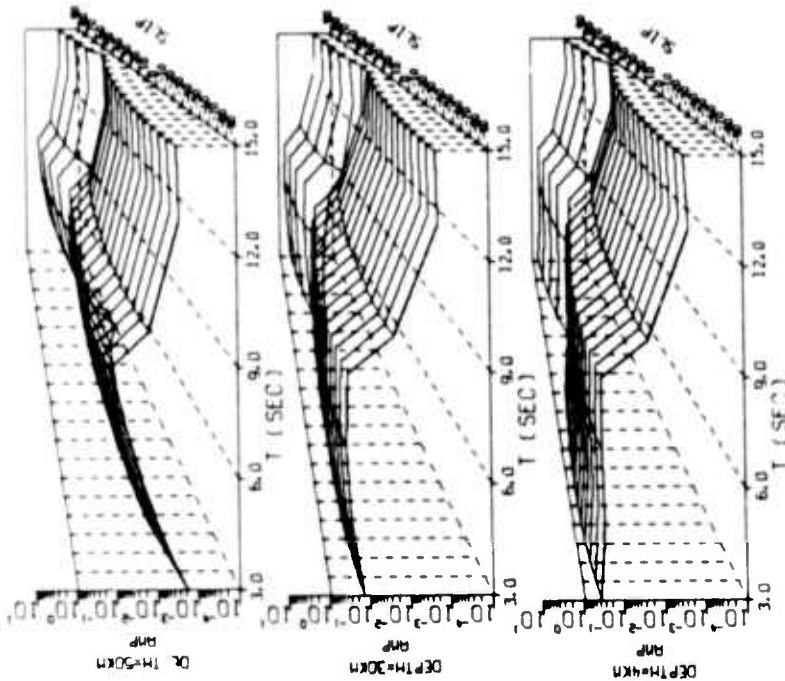


FIGURE C-1b  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A GUTENBERG-BULLEN EARTH MODEL:  
 Period Range 3 to 15 Seconds, Dip ( $\delta$ ) = 90°, Slip ( $\lambda$ ) = Variable, Strike ( $\theta$ ) = 0°

GB-1ST HIGH / LOVE  
 DOUBLE-COUPLE  
 DIP ANGLE = 60.0  
 STRIKE = 0.0  
 AZIMUTH = 30.0



GB-1ST HIGH/RAYLEIGH  
 DOUBLE-COUPLE  
 DIP ANGLE = 60.0  
 STRIKE = 0.0  
 AZIMUTH = 30.0

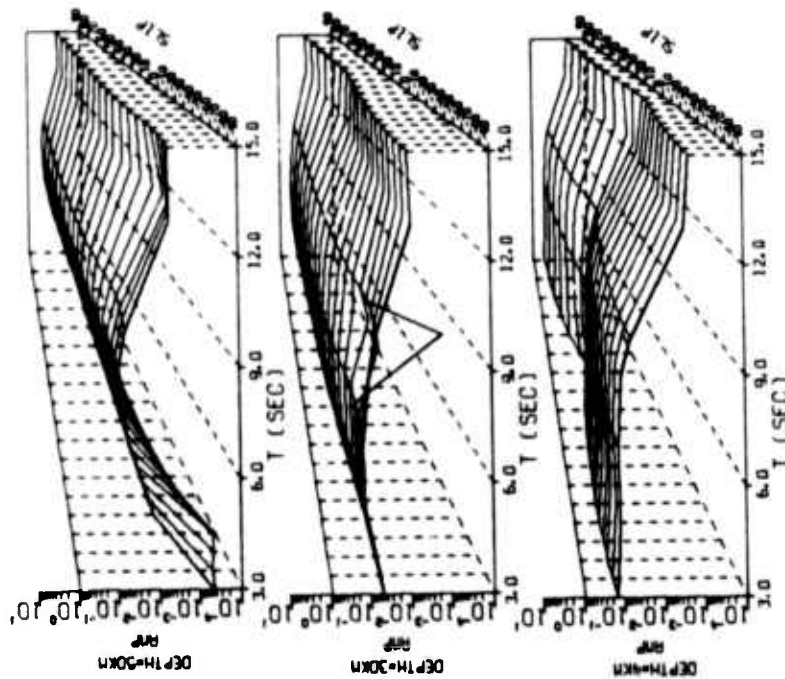
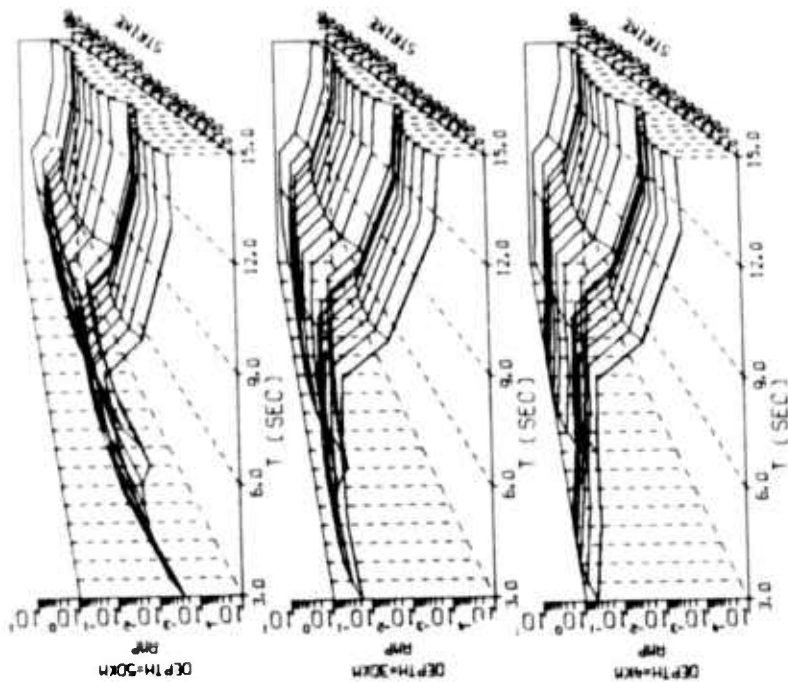


FIGURE C-1c  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A GUTENBERG-BULLEN EARTH MODE L:  
 Period Range 3 to 15 Seconds, Dip ( $\delta$ ) = 60°, Slip ( $\lambda$ ) = Variable, Strike ( $\theta$ ) = 0°

GB-1ST HIGH / LOVE  
 DOUBLE-COUPLE 90.0  
 DIP ANGLE 90.0  
 SLIP ANGLE 0.10  
 MOMENTS 30.0  
 AZIMUTH 0



GB-1ST HIGH/RAYLEIGH  
 DOUBLE-COUPLE 90.0  
 DIP ANGLE 90.0  
 SLIP ANGLE 0.10  
 MOMENTS 30.0  
 AZIMUTH 0

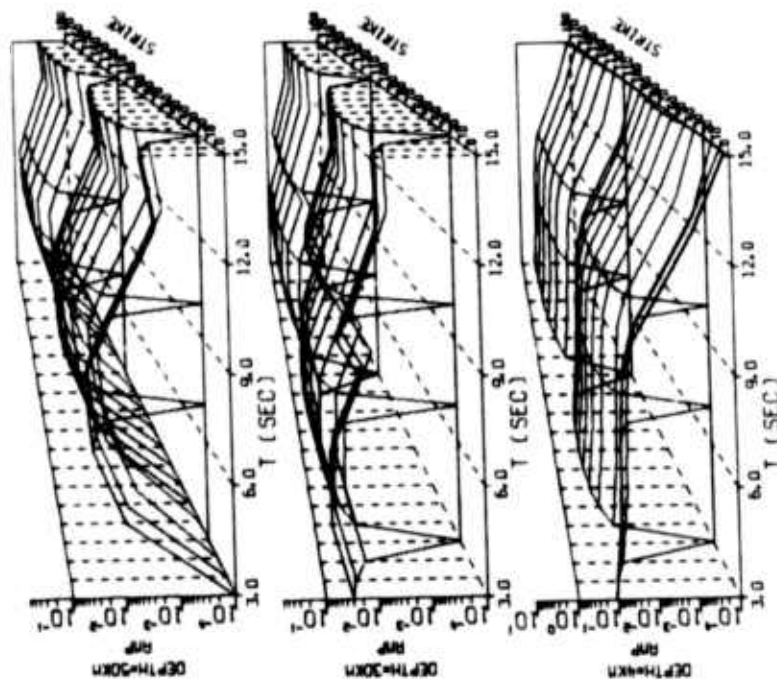
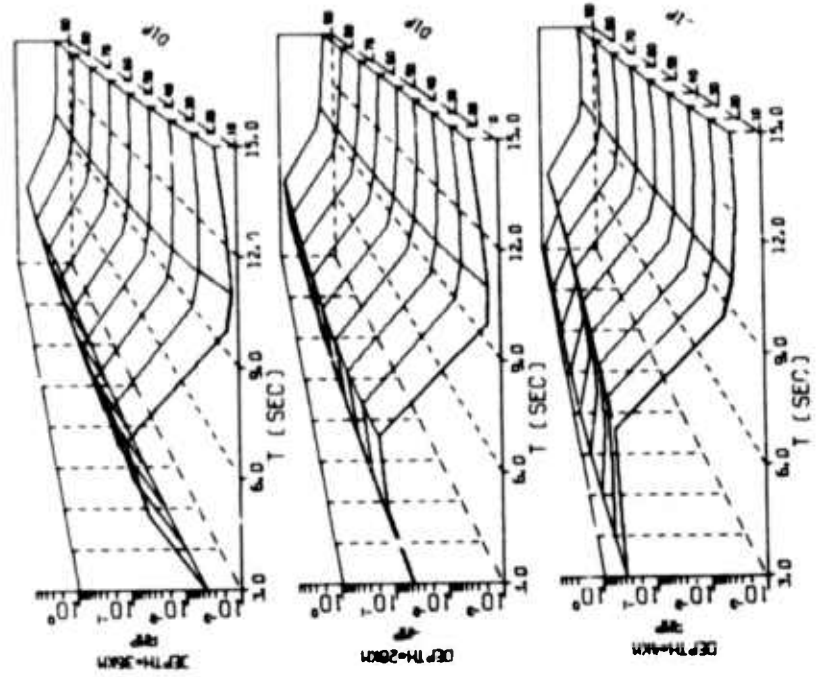


FIGURE C-1d  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A GUTENBERG-BULLEN EARTH MODEL:  
 Period Range 3 to 15 Seconds, Dip ( $\delta$ ) = 90°, Slip ( $\lambda$ ) = 0°, Strike ( $\theta$ ) = Variable

MH-1ST HIGH/LOVE  
 DOUBLE COUPLE 0.0  
 SLIP ANGLE 0.0  
 STRIKE 0.10  
 MOMENT 0.10  
 AZIMUTH 30.0



MH-1ST HIGH/RAYLEIGH  
 DOUBLE COUPLE 0.0  
 SLIP ANGLE 0.0  
 STRIKE 0.10  
 MOMENT 0.10  
 AZIMUTH 30.0

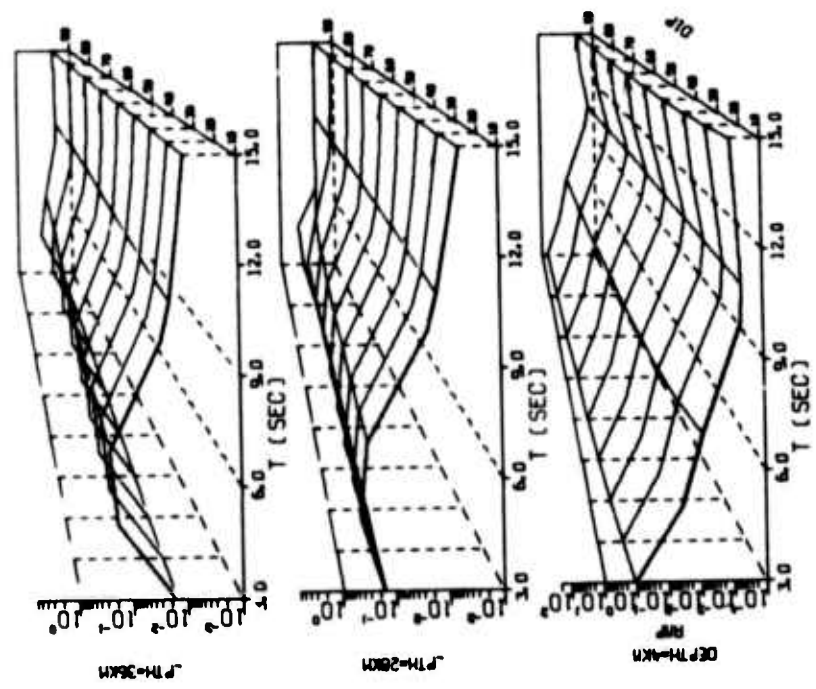


FIGURE C-2  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A HAMILTON-HEALY EARTH MODEL:  
 Period Range 3 to 15 Seconds, Dip ( $\delta$ ) = Variable, Slip ( $\lambda$ ) =  $0^\circ$ , Strike ( $\theta$ ) =  $0^\circ$

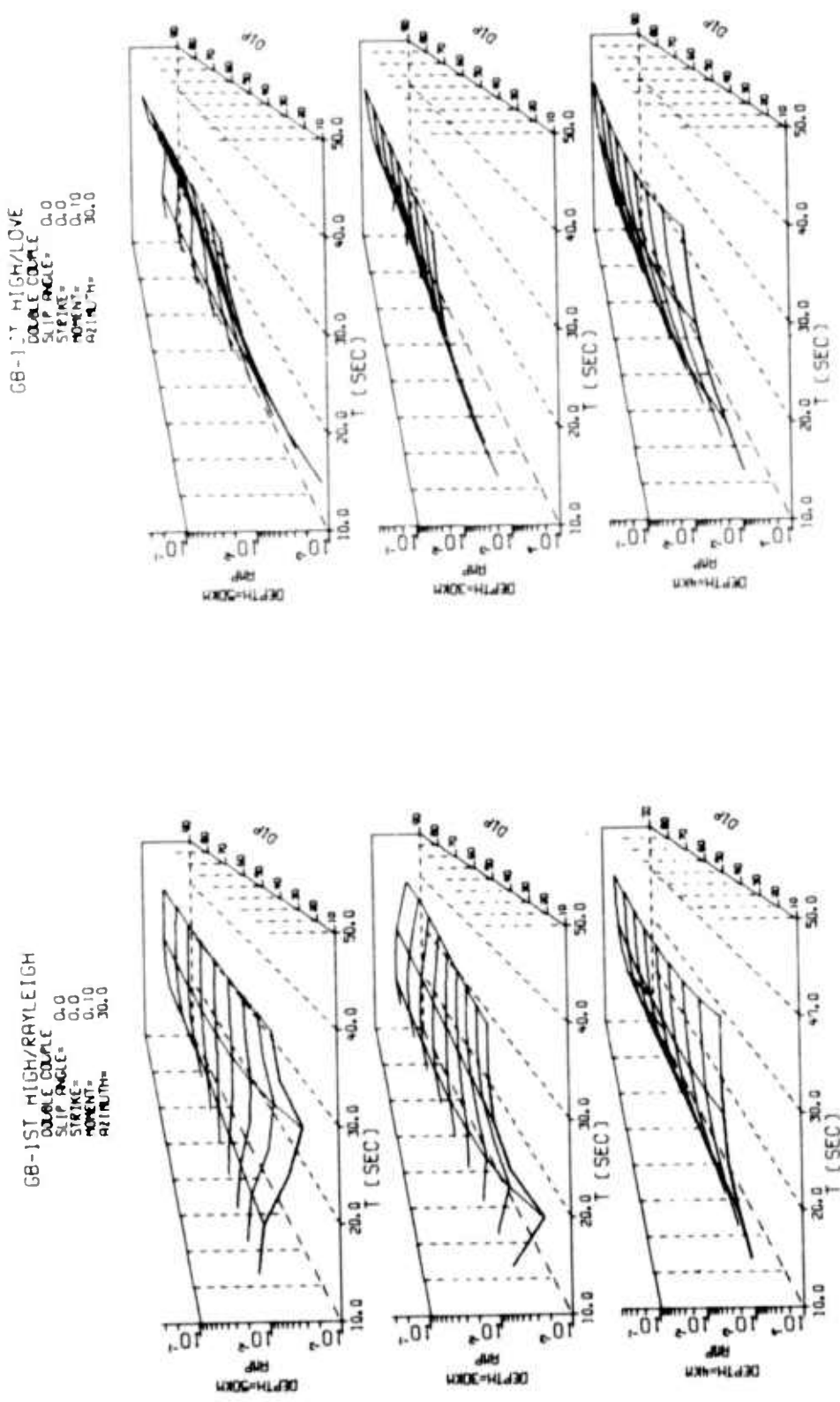


FIGURE C-3  
 THEORETICAL FIRST HIGHER MODE RAYLEIGH AND LOVE WAVE SPECTRA  
 FOR THREE SOURCE DEPTHS IN A GUTENBERG-BULLEN EARTH MODEL:  
 Period Range 15 to 40 Seconds, Dip ( $\delta$ ) = Variable, Slip ( $\lambda$ ) =  $0^\circ$ , Strike ( $\theta$ ) =  $0^\circ$



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| 20 ABSTRACT (Continue on reverse side if necessary and identify by block number) Several continuing investigations of the seismic source using near- and far-field data are discussed. We completed our analysis of near-field acceleration data recorded at Bear Valley, California, by examining two small events which occurred on 7 February 1974 and 6 July 1974. The February event, using only spectral analysis, was found to have a moment of $3 \times 10^{21}$ dyne-cm with an equivalent circular dislocation radius of 0.18 km <sup>2</sup> . Both spectral and time domain waveform fitting techniques were |                      |                                                                                      |  |

20. continued

applied to the July event. The solutions using each method were in reasonable agreement, with a seismic moment in the range of 2 to 4 x 10<sup>21</sup> dyne-cm over an equivalent dislocation radius of about 0.1 to 0.3 km<sup>2</sup>. 10 July 21st POWER  
1  
x 50 cm

Using far-field surface wave data, two central California area earthquakes (22 June 1973 and 28 November 1974) were re-examined using two new earth models which were determined by McEvelly (1975) for the northeast and southwest side of the San Andreas fault. Several far-field solutions for the source mechanism were obtained by using various combinations of stations and earth models, including use of both structures at once for the first time. However, for the central California event of 28 November 1974, the mechanism which agreed closely with that obtained by other means used only those stations on the west side of the fault, with the southwest structure used in the spectral fit. ←

Theoretical first higher mode surface wave spectra were generated for a double couple source in a layered half space. Both Gutenberg-Bullen and Hamilton-Healy earth models were used. As with fundamental mode spectra, 'holes' were found almost exclusively for vertical strike-slip faults. Higher mode spectral levels in the 3 to 9 second period range were found to be comparable with 15 to 50 second period fundamental mode spectra. Also, from the excitation of the earth models, greater amplitude higher mode signals from shallow events should occur from high velocity crustal source regions.

Preliminary results have been obtained for five large events which were a part of the Sinkiang, China earthquake swarm of August 1974. Both simple spectral and spectral ratio fitting methods were employed. The far-field solutions showed a consistent trend for these five events of shallow focal depth.

Finally, we concluded our examination of the scatter of the earthquake population in the  $M_s - m_b$  discriminant. Focusing on the bodywave magnitude estimate instead of the surface wave magnitude as in previous studies, we applied the maximum likelihood method of Ringdal (1975) in an attempt to improve the accuracy of the PDE bodywave magnitudes. Although the scatter of the population did not change significantly, the slope of the data set decreased approximately 0.25.