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COMPUTER AUTOMATED DESIGN OF SYSTEMS

Larry Paul Vines

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

Computer Automated Design of Systems

by

Larry Paul Vines

June 1976

Thesis Advisor:

George J. Thaler

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parameters. A parameter minimization routine is then used to minimize a specific cost function and to set the free parameters. A graphical output of the desired response and actual system response is then produced for comparison by the engineer.

Computer Automated Design
of
Systems

by

Larry Paul Vines
Lieutenant, United States Navy
B.S.E.E., Purdue University, 1970

Submitted in partial fulfillment of the
requirements for the degree of

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ABSTRACT

An automated digital computer technique of control system design is presented. The emphasis is on compensator design but the method is applicable to the design of any system with free parameters. Signal representation and system response are in the time domain.

The inputs required from the engineer are the system configuration, the desired output response and the free parameters. A parameter minimization routine is then used to minimize a specific cost function and to set the free parameters. A graphical output of the desired response and actual system response is then produced for comparison by the engineer.

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I. INTRODUCTION

The past two decades have been witness to an ever increasing use of the digital computer. Engineering usage and design are probably the most important justification for the large memory, high speed computers of today. Classes in computer application to engineering problems have become part of the established curricula at most universities. Numerous papers have appeared on the application of the computer to engineering problems [1] which until recently were unsolvable or at best required long, tedious procedures which gave only approximate solutions.

Control system engineering has relied increasingly on computer simulation of large scale systems to verify that design specifications have been met and to make modifications to a system even before producing a prototype. There are programs available to simulate virtually any electrical circuit, or control system, either in transfer function form or as a system of first order differential equations. Others draw the Bode, Nichols or Nyquist plots of open and closed loop systems. Some programs help design compensators which use an iterative method to achieve the desired frequency response [2] [3]. Researchers continue to better adapt the computer to engineering usage.

Catalapiedra [4] has used an iterative method to find the optimum reduced order model for large order systems. MacNamara [5] went even further and used an iterative method to find the optimum compensation for an aircraft autopilot. It would appear that these techniques could be extended and applied to the direct simulation and design of control

system circuits in the time domain.

The intent of this thesis was to develop a user oriented program which could simulate a wide variety of control systems and determine the values of the gains, poles and zeros necessary to produce a desired response. A convenient means of data card input was to be provided to specify (1) the control system which was to be optimized and (2) the desired response. A locally available function minimization routine (ECFLX) was to be used to optimize the simulated system's output.

To simulate the system which is to be optimized, transfer functions which are commonly encountered were reduced to first order linear differential equations. These equations were then programmed so that the transfer function blocks could be connected in an arbitrary fashion by data card input. Several common nonlinear transfer blocks were also provided. The program will simulate the system with the known parameters and then allow all unknown or adjustable parameters to be fixed by the computer optimization routine to achieve the desired response.

II. PROGRAM DEVELOPMENT AND IMPLEMENTATION

A. GENERAL

Any program which is to be of maximum benefit to the user must have a simple means of data input and an output which is easy to interpret and apply to the problem at hand. The input data should have a physical significance that does not lose its relevance through the programming of numerous equations. The program should be a readily usable tool and not a problem in itself. The intent of this thesis is to present such a program, Computer Automated Design of Systems (CADS), which is readily used for simulation with optimization of the output. Optimum in the sense that the output response of a given system configuration is as near the desired response as possible.

Most control system design starts with a proposed transfer function block schematic to achieve a desired time domain response. CADS has the common transfer functions built into the program and the input data can come directly from the proposed system schematic. The transfer blocks which are available for system simulation are presented in Table I. These blocks should be adequate, either separately or in various cascade combinations, to represent most control systems.

TYPE

CF

SYMBOL

EQUATION SOLVED

ELCCK

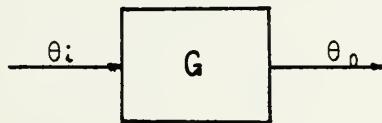
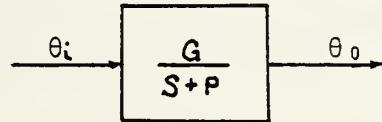
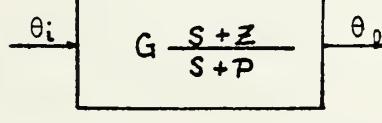
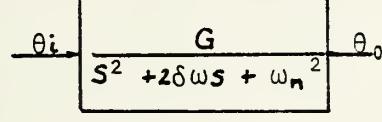
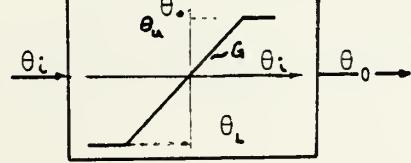
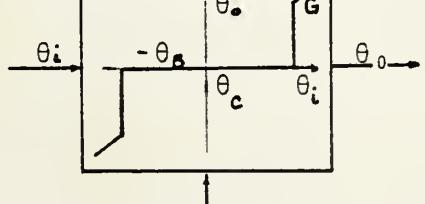
1		$\theta_0 = G\theta_i$
2		$\dot{\theta}_0 = -P\theta_0 + G\theta_i$
3		$\dot{\theta}_0 = -P\theta_0 + G(\dot{\theta}_i + Z\theta_i)$
4		$\ddot{\theta} = -2\delta\omega_n \dot{\theta}_0 - \omega_n^2 \theta_0 + G\theta$
5		$\theta_0 = G\theta_i \quad \theta_L \leq G\theta_0 \leq \theta_u$ $\theta_0 = \theta_u \quad \theta_u < G\theta_i$ $\theta_0 = \theta_L \quad G\theta_i < \theta_L$
6		$\theta_0 = 0 \quad \theta_c < \theta_B$ $\theta_0 = G\theta_i \quad \theta_c \geq \theta_B$

TABLE I Program Transfer Function Blocks

To use the program the engineer must know the system configuration in transfer block form and the desired second order output response. If other than a second order response is desired, this may be easily specified but requires some knowledge of how to input the desired response. CALS will take the transfer block system, connect it, compare the given system response to the desired response and set any free parameters to achieve the closest match possible of the system output to the desired response.

Figure 1 is representative of the type of system the program can simulate and optimize. In figure 1, the parameters of the numbered transfer function blocks are known or fixed by equipment limitations. Transfer blocks X, Y, and Z contain variable parameters which must be selected by the program to make the system output reproduce a desired output function as closely as possible.

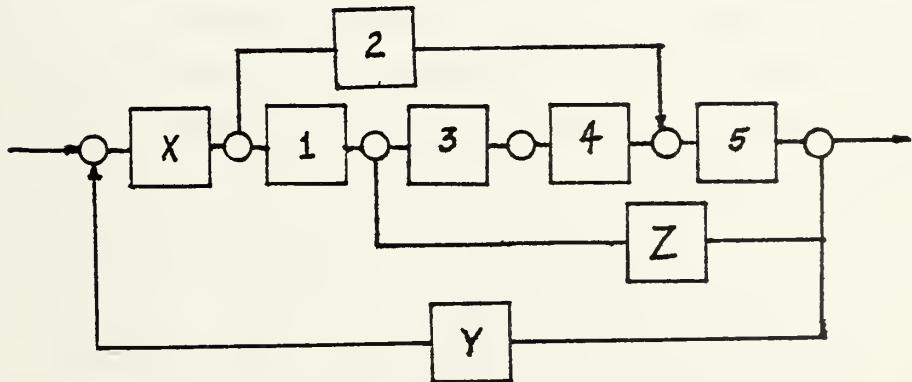


FIGURE 1 Typical System to be Optimized

E. MAIN PROGRAM

The MAIN program was developed to control the selection of the subfunctions used in the optimization process and to compute the desired response of the systems which were to be optimized. A second order step response is calculated from equation (I) as the desired response and stored in the array XDATA.

$$\theta_0 = \frac{G}{s^2 + 2\delta\omega_n s + \omega_n^2} u(t) \quad (I)$$

The MAIN is essentially a bookkeeping routine which controls the program execution. The subfunction operations it controls are defined in the following sections.

C. PLANT

The common simulation routines LISA, DSL, ECAP, CSMP and INTEG were investigated in an attempt to adapt them to the general problem specified above. These programs required either the input of the system's state variable equations, Laplace transform equations or the node-transfer function pair for each system simulated. These programs are useful for simulation if all of a system's parameters have been specified. However, each simulation is problem specific and these techniques are not readily integrated with other subfunction programs. A simulation subprogram which was capable of accepting data card input to simulate a wide variety of control systems and of working with other existing subprograms had to be developed.

Subfunction PLANT was developed to simulate the systems which were to be optimized. It provides the versatility necessary to simulate numerous system configurations and is capable of working with a minimization routine to optimize the variable parameters. The program reads the transfer function block connections from data cards. This data is then used to automatically set up the system equations in state variable format. These state variable equations are solved as first order, ordinary differential equations by the Runge-Kutta-Gill forth order method. The programming was done in Fortran IV and all calculations are in double precision. The capability of connecting the transfer function blocks in any configuration (feed forward, feedback, etc.) is possible with this program. Simulation flexibility is provided by having each block within the system capable of accepting an external forcing function.

1. Block Data Card

Several possible ways of inputting the data necessary to simulate arbitrary system configurations were investigated. A means of defining a system configuration directly from a block diagram schematic was chosen as the most preferable method. Using this approach, each data card was designed to be directly related to a transfer function of the system. This resulted in having direct access to the transfer function parameters for optimization.

To simulate the system, a data card is prepared for each transfer block in the schematic diagram. The data card contains a field of numbers which specify the block number, the type of transfer function contained within the block, the input node and the output node to which the block is connected and the values of any parameters associated with the transfer function. The general format of the data

cards used to input the system configuration is shown below.

1	11	20	40	60	(Column Number)
---	----	----	----	----	-----------------

ELKCCD=EEVV	G	P	Z		
-------------	---	---	---	--	--

Where:

CC = Position number of the block

D = Type of block (number)

EE = Input node number

VV = Output node number

G, P, and Z are parameters of the transfer function.

2. Block Connections

The number of transfer blocks in the system and the data cards associated with each of the blocks are read upon initial entry into the simulation routine. The program then connects the transfer function blocks in the proper order by comparing the input node number of a block to the output node number of every other block. Whenever these two numbers are equal, the blocks are known to be connected and a flag is set equal to 1.0. The flags are then used to identify the input drives to each block.

3. Drives

The input quantity to each block is called the DRIVE. The program was designed to allow for multiple inputs to the system being simulated. This flexibility was achieved by making the input to each block equal to the sum of the outputs of all blocks connected to the input node plus any external forcing function (DRVIN) feeding the transfer block. The input DRIVE to a block is determined as shown in equation (II).

$$\text{DRIVE}(i) = \sum \text{THA}(j) * \text{FLAG}(j,i) + \text{DRVIN}(i) \quad (\text{II})$$

$\text{THA}(j)$ is the output of block j . $\text{FLAG}(j,i)$ is 1.0 if block j is connected to block i and zero if it is not connected. $\text{DRVIN}(i)$ is any external forcing function specified by the user which drives block i . DRVINS must be inserted in subroutine ELANT as Fortran IV statements. The standard program has $\text{DRVIN}(1) = 1.0$ specified as a unit step input to the system. Problem III-E in the section Investigation of Program Performance demonstrates how multiple, time varying inputs are to be inserted in the program.

4. Standard Transfer Function Blocks

The transfer function blocks available for system simulation are shown in Table I. These blocks were selected because of their common usage in the modeling process. They were also found to be adequate either separately or in various cascade combinations to represent most control systems.

The transfer function equations for each type of block were written in state variable format and stored in an array named THA . The program reads a number from a block's data card which specifies the type of transfer function associated with the block. The system equations are then solved sequentially by selecting the type of equation associated with block number one, solving for its output and then sequencing to block number two, etc. The integral equations are solved by a modified RK4 fourth order method in the subfunction routines. Three integration routines were necessary to store the intermediate results obtained for those equations involving a double integration. The four subfunctions, RKLDE2 , RKLDE3 , CCPLX and RKDF4 are called by ELANT . RKLDE2 is used for the integration of a

type two block. RKLDE3 is used for integration of a type three block and to store intermediate quantities for subfunction CCPLX. CCPLX calls RKLDE3 and RKLDE4 for integration of a type four block.

No provision has been made for the input of initial conditions or the integrators. Therefore, the integrations must start at time equal zero. The user must specify the step size tc to be used for integration (DT) and the problem run time (TF). To conserve computer time DT should be made as large as possible. DT = TF/1000 is suggested as appropriate in most cases. Equally important is that TF be as small as possible. Use of the program has shown that letting TF be greater than the transient response time of the system is rarely justified. For preliminary analysis TF was kept to only slightly longer than the time of the first undershoot for second order dominant systems. Because of the complexity of subroutine PLANT a flow chart of PLANT has been included as Appendix B.

5. Parameters to be Optimized

The parameters of the system which are to be optimized by the minimization routine EOXPLO must be specified in PLANT. The minimization routine returns the trial values of the variable parameters to PLANT in an array labeled 'C'. Regular Fortran IV statements equate the variable parameters to the values in this array. If a pole-zero pair were to be optimized, the following statements would be inserted in PLANT: P(i) = C(1) and Z(i) = C(2). The location for the preceding statements is clearly indicated in the program listing for PLANT.

D. DESIRED RESPONSE (XDATA)

The criteria against which the system response will be compared will vary according to the application of the system. Since most design work on control systems is done on the basis of second order dominance, the program was written to provide a second order step response with adjustable δ , W_n and gain as the basic criteria against which the simulated system will be compared. The desired δ , W_n and gain are read in as input data. The step response is then computed in the main program by subfunction RKLDEC and stored in the array called XDATA. Any other time domain response may be specified by the user by removing the second order step response equations and replacing them with the equations of the desired response. An example is provided by problem III-E in Investigation of Program Performance. If the program is being used for simulation only and no data curve is desired, setting the input variable LEAP = 1 will cause the program to bypass the computation of the standard second order data equation.

E. COST FUNCTION (PERFORMANCE INDEX, PI)

The achieved system response is compared with the desired response and the difference is the error. The program searches for the parameter settings which will minimize this error. The cost function may be specified by the user to weight the system outputs as desired in subfunction FE. The default cost function of the program is

the integral error squared. $J = \int_0^{T^F} (\text{Err})^2 dt$. An example of a weighted cost function is presented in Section III.

F. MINIMIZATION ROUTINE

1. General

The free parameters are optimized to reduce the cost function by the complex method of M. J. Box.[6] Box's constrained optimization method has been programmed at the Naval Postgraduate School by R. R. Hilleary as a subroutine called ECXPLX. This subroutine will find the minimum of an arbitrary function (cost function) subject to arbitrary explicit constraints and for implicit constraints. Explicit constraints are defined as upper and lower bounds on the free parameters. Implicit constraints may be arbitrary functions of the free parameters (e.g. $P_1 P_2 < 178$).

Two function subprograms are used to evaluate the objective function and implicit constraints, FE and KE respectively. The method BOXPLX uses to search for the values of the free parameters which minimize the cost function is explained in the computer program listing.

2. Explicit/Implicit Constraints and Start Points

ECXPLX searches a feasibility region (n -dimensional space, where n = number of free parameters) defined by upper and lower bounds on the free parameters for a minimum cost function. The smaller the region defined by these boundaries, the more rapidly the program will converge to the optimum parameter settings. Good engineering judgement will be necessary to keep the feasibility region as small as

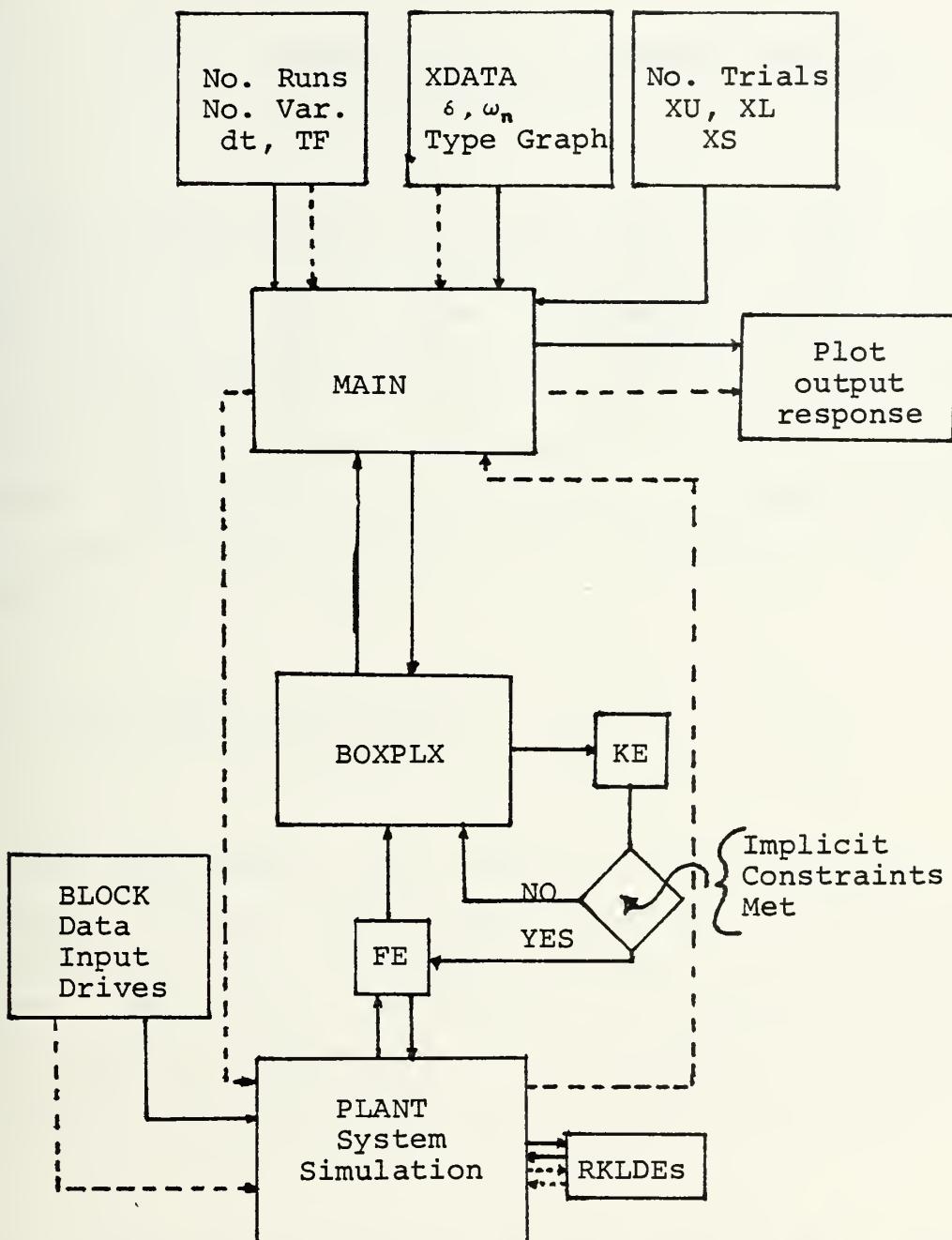
possible. The boundaries of the search region are read from data cards by the main program as the upper bound (XU) and the lower bound (XL) for each free parameter.

Implicit constraints may be any arbitrary function of the free parameter desired. If an implicit constraint such as the product of a pole-zero pair must be less than some number is to be evaluated, it must be supplied by the user to the subfunction KE. No implicit constraints were used in this thesis.

The starting values of the free parameters (XS) are read in by the MAIN from data cards. A good choice of starting values will dramatically reduce the time required for optimization. A preliminary root locus or Bode plot method of estimating the best values of the free variables should be accomplished whenever possible.

G. GRAPHICAL OUTPUT

Two subroutines were written to provide for the graphical output of the desired response and the best system response achieved by the optimization process. The user may select, by data card input, either subroutine PPIT which provides a high speed printer plot or subroutine PIC which provides a calcomp graph. Every fifth integration point stored in the arrays XDATA and THAOUT is plotted. Subroutines PPIT and PIC call the subroutines PLOTP and DRAW respectively. PLOTP and DRAW are standard plotting routines at the NES computer facility and are not a part of the simulation program. Figure 2 diagrams the information flow and data input to the program.



Optimization →
Simulation →

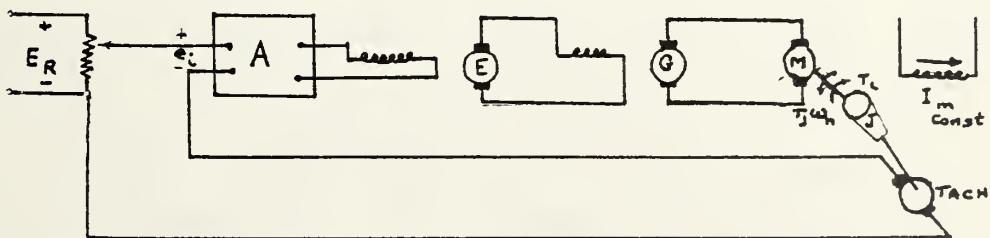
FIGURE 2 CADS Program Flow Chart

III. INVESTIGATION OF PROGRAM PERFORMANCE

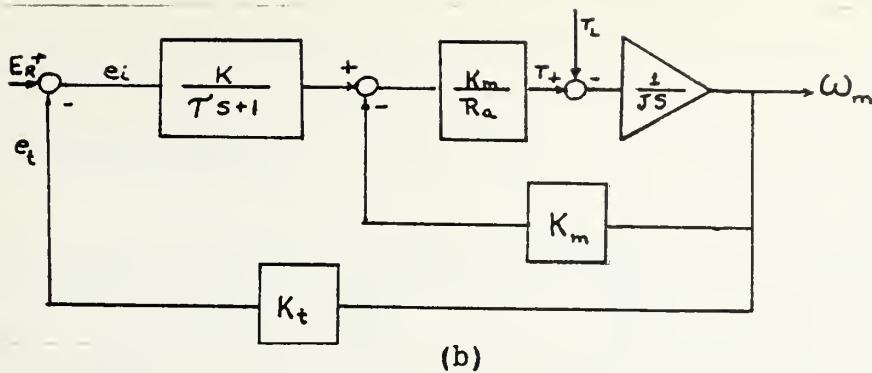
The example problems presented below were used to aid in the development of the optimization program. The order of difficulty of the problems progresses from a simple textbook single variable, single input system to a multivariable operational servo drive system which has multiple inputs and discrete level feedback. An example of how a schematic diagram representation of a system is prepared for input to the program is presented prior to considering the example problems.

A. DATA INPUT, AN EXAMPLE

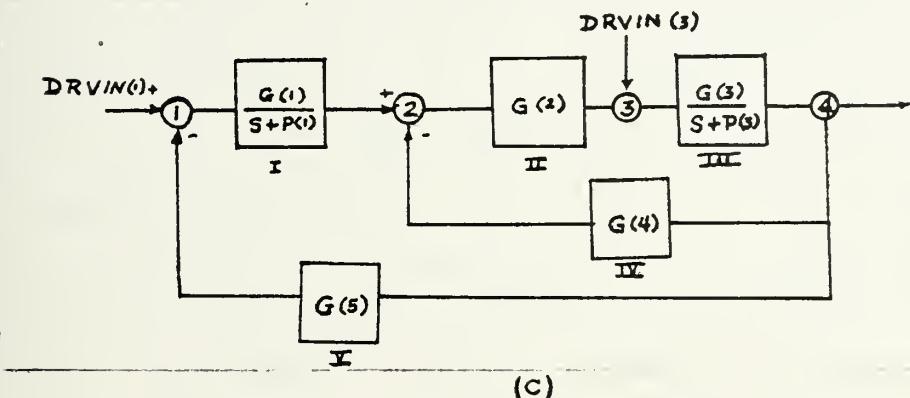
The Ward-Leonard drive system [7] shown schematically in Figure 3 (a) has two variable parameters. The gain of the amplifier and the tachometer feedback are available to adjust the system's response. To simulate the system a block diagram representation of the system is drawn as shown in Figure 3 (c) using the transfer blocks from Table I.



(a)



(b)



(c)

FIGURE 3 Ward - Leonard Speed Control System
Using Feedback. (A) Schematic Diagram
(B) Block Diagram (C) Block Diagram
Using CADS Blocks.

Where

$$G(1) = K/\tau \quad P(1) = 1/\tau$$

$$G(2) = Km/Ra$$

$$G(3) = 1/J \quad P(3) = 0$$

$$G(4) = -Km$$

$$G(5) = -Kt$$

$$DRVIN(1) = E_r$$

$$DRVIN(3) = -T_L$$

The nodes of the block diagram are then numbered sequentially 1, 2, ..., n. The blocks between the nodes are also numbered sequentially 1, 2, ..., N as shown in Figure 3 (c). Data cards (N) are then prepared for each block which specify the block number, type of block, the input node, the output node, and the parameters contained within the block. In Figure 3 (c), for example, block 1 is

a type two transfer block connected between nodes 1 and 2. The data card input for this block would be

BIK012=0102

K/τ

$1/\tau$

The program reads the data card input and connects the blocks by setting a FLAG = 1. whenever the input node number to a block is the same as the output node number of any other block. The input to a transfer block is then determined to be the sum of the outputs of all blocks connected to the input node plus any external forcing function driving the input node. The program has a unit step specified for DRVIN (1). If this is the only input to the system, no action is necessary on the part of the user. If other than a unit step input to the system is desired or if there are other external forcing functions such as DRVIN (3), they must be specified and placed within the body of the subroutine PLANT as Fortran IV statements. For the example shown in Figure 3 (c), a card with the equation

DRVIN(3) = f(T_L)

would have to be inserted preceding the drive equations. An example of how multiple, time varying drives are specified is given in section III. E.

When optimizing a system, some of the input quantities will be unknown or variables. These variables must also be assigned within subroutine PLANT. To optimize the variables K_1 and K_t of Figure 3 the following two statements would be inserted in PLANT:

G(1) = C(1)
G(5) = C(2)

where C(1) and C(2) are the variables which will be optimized by subroutine BOXPLX.

E. TACHOMETER FEEDBACK

The first optimization problem attempted was one which had an exact solution that can be found by algebraic methods. An instrument servo [8] with unity feedback and forward transfer function

$$G(S) = \frac{1000}{S(S+10)} \quad (\text{III})$$

was to be compensated with tachometer feedback as shown in Figure 4. The only specification for the system's performance of this single variable, second order system was the simple requirement that the closed loop roots have a $\delta = 0.7$.

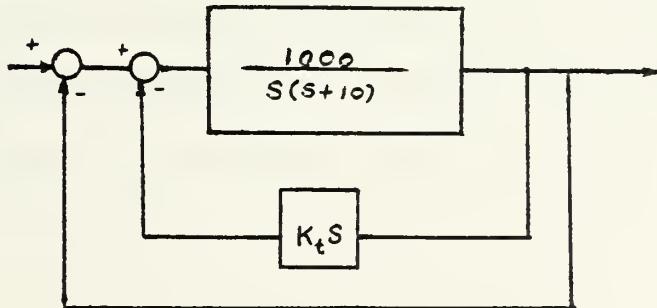


FIGURE 4 Tachometer Compensated System

The system shown in Figure 4 was redrawn as Figure 5 in order to achieve the tachometer feedback. The characteristic equation of the system shown in figure 5 is

$$s^2 + (10 + 10^3 \frac{K_t}{t} s + 10^3 = 0 \quad (\text{IV})$$

The required $K_t = 0.0343$ may be calculated from equation IV.

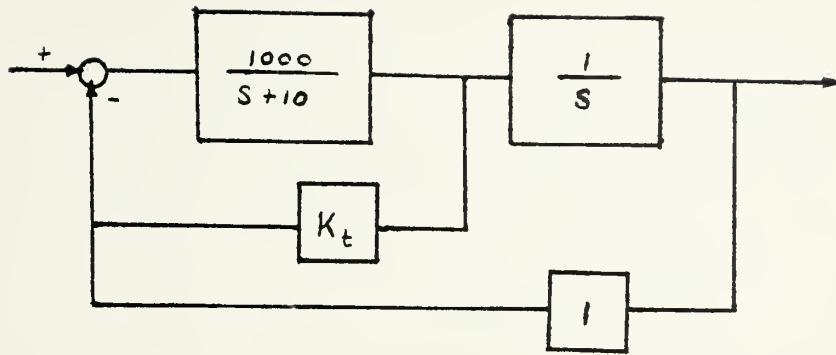


FIGURE 5 CADS Block Diagram of Tachometer System

CADS was programmed to optimize the system with the variable, K_t , specified to be between the limits $0.01 < K_t < 1.0$. The desired response was specified to be the standard second order step response for $\delta = 0.7$, $W_n = 1000$. CADS determined the optimum value for K_t to be $K_t = 0.0343$. Figure 6 shows the system's step response and the desired response are virtually superimposed.



FIGURE 6 CADS Compensated Tachometer Feedback System Response

The type one system, in the preceding example, allowed derivative feedback from the forward path without requiring a block which was capable of differentiation. One may encounter a type zero system or a system which cannot be configured to provide derivative feedback from the forward path. The possibility of providing a pseudo derivative feedback using a type three block was investigated for these cases.

A type three block with $Z = 0$ and $G = P$ is shown in Figure 7. If the pole is placed far out on the real axis, this block approximates derivative feedback.

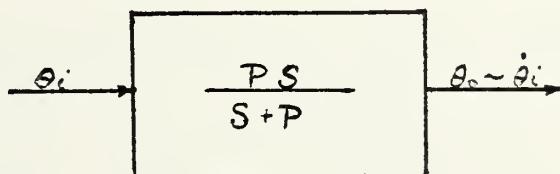


FIGURE 7 Type Three Block used for
Pseudo Tachometer Feedback

The effect of using this pseudo tachometer feedback on the complex roots of the closed loop system is negligible. It does add a real root at $P = -964$.

The system of Figure 5 was redrawn as shown in Figure 8 using the pseudo tachometer feedback.

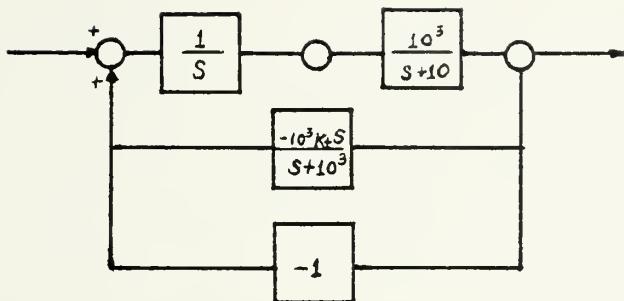


FIGURE 8 Pseudo Tachometer Feedback

The optimization program calculated $K_t = 0.0352$ for the above configuration. This gave a $\delta = 0.715$.

The system response and the desired response are shown in figure 9. The two responses are again nearly superimposed. This method of providing derivative feedback has the disadvantage of adding an integration step to the problem solution with the concomitant increase in problem solution time.



FIGURE 9 Pseudo Tachometer Compensated System's Response

C. CASCADE COMPENSATION

Having proven the feasibility of the program optimizing a single variable system where an exact solution was available, the next problem considered extending the problem scope to a third order plant with two variables. The unstable plant that was to be compensated is shown in Figure 10.

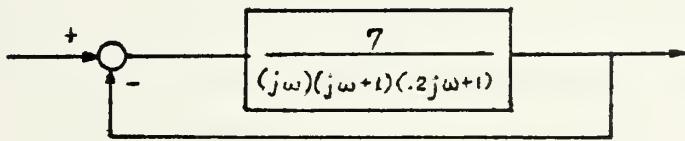


FIGURE 10 Third Order Plant to be Compensated

The plant was to be stabilized using a single section cascade compensator. The compensated plant was required to have $M_{PW} < 2$, without reducing the error coefficient. [8] The compensated system is shown in Figure 11. To keep the error coefficient constant, the compensator used was a simple lag network ($\tau_1 < \tau_2$).

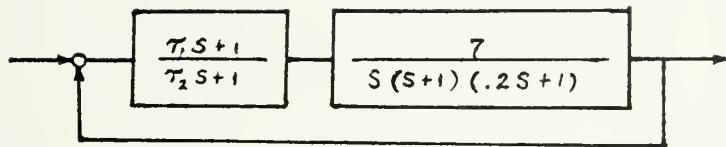


FIGURE 11 Lag Compensated System

A compensator which would meet the required specifications was calculated by conventional methods as a check on the program's performance. The Bode plot of the uncompensated and conventionally compensated system is shown in Figure 12. The values of τ_1 and τ_2 for Figure 11 which would meet the design requirements were determined to be $\tau_1 = 10$, $\tau_2 = 100$. The compensated system's response using these values for the compensator is shown in Figure 13.

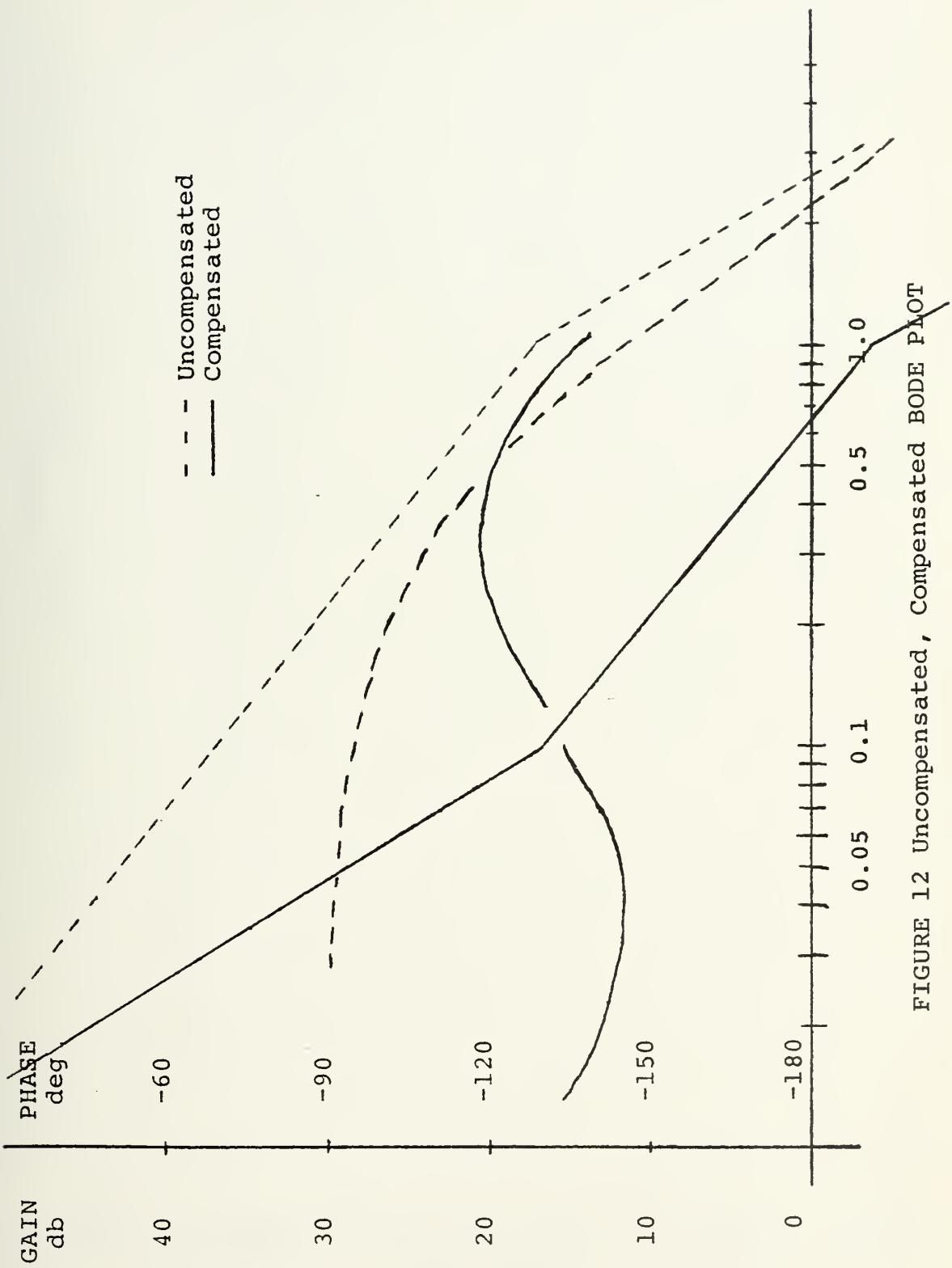


FIGURE 12 Uncompensated, Compensated BODE PLOT



FIGURE 13 Conventionally Compensated System Response

The compensated system was redrawn as shown in Figure 14 using the standard program transfer blocks available for system simulation.

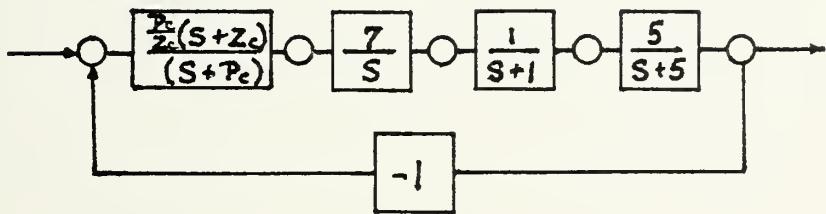


FIGURE 14 CADS Lag Compensated System

A standard second order response of $\delta = .3$, $W_n = 0.75$ was chosen as the desired response for the optimization program to match. The limits placed on the optimization program were $.001 < P_c < .1$ and $.01 < Z_c < 1$. Arbitrary values to begin optimization were specified as $P_{c0} = .01$ and $Z_{c0} = .1$ in the logarithmic centers of the search zones. CAES determined $T_1 = 8.078$ and $T_2 = 67.47$ as the optimum parameter settings. Figure 15 shows the desired response and the program compensated system response.

The response of the system compensated by CADS is more nearly the desired response than is the conventionally compensated system. One should remember that the specified response is for a true second order system whereas, the compensated system is forth order. Therefore, a perfect

match of desired versus actual responses could not be obtained.



FIGURE 15 CADS Compensated System Response

D. CASCADE LEAD COMPENSATION

The complexity of the next problem to be solved by CADS was extended to five free parameters. The plant shown in figure 16 was to be used to follow a unit amplitude sine-wave input of 200 rad/sec. The output amplitude was to be almost exactly the same as the input amplitude, and the output could not lag the input by more than 10° . Two sections of cascade compensation were to be used. [8]

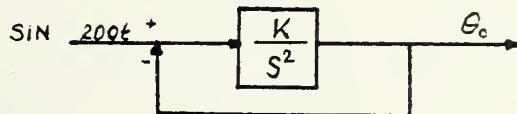


FIGURE 16 Plant for Lead Compensation

The specified requirements may be interpreted as an open loop gain > 15 db and a phase angle $\sim 90^\circ$ at $\omega_n = 200$ from a Nichols plot. A cut and try solution on a Nichols plot showed that a gain of 3×10^6 and two phase lead compensators with a double zero at $\zeta = 70$ and a double pole at $P = 700$ will satisfy the closed loop magnitude and phase requirements. Figure 17 shows the system response and desired response obtained for these values. The magnitude of the compensated system's response is 93% of the desired response and lags by 8.12° .

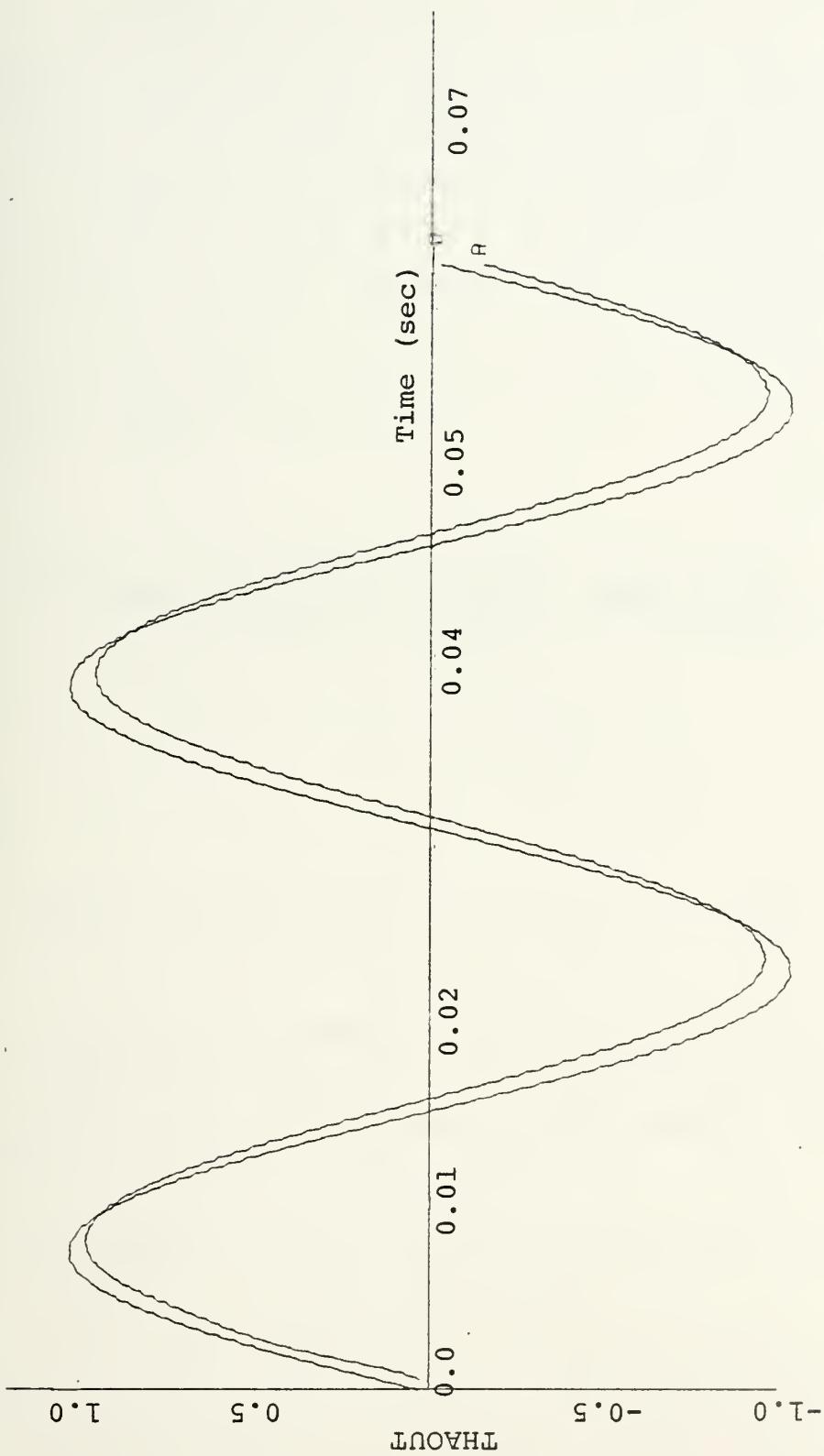


FIGURE 17 Conventional Lead Compensated System Response

The problem was then run on the optimization program with the block connections as shown in Figure 18. The free parameters were the poles and zeros of the compensators and the gain of the plant. The desired data curve of $XDATA = \sin(200t)$ was generated from the standard second order step response by setting $\delta = 0$, $W_n = 200$ and using $X(2)$ as the desired response. The initial search zone limits were specified as $600 < P_i < 800$, $60 < Z_i < 80$, $2.8 \times 10^6 < G(3) < 3.2 \times 10^6$.

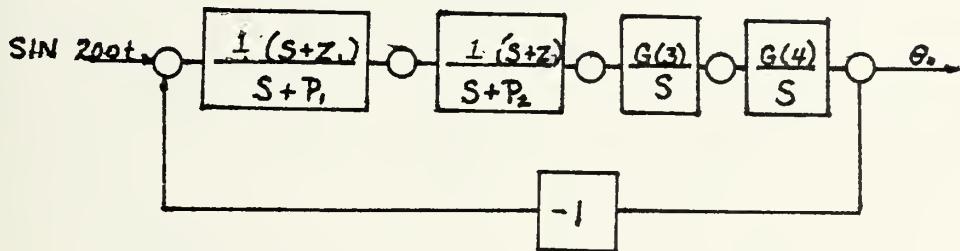


FIGURE 18 CADS Block Diagram for Lead Compensation

The optimization program solution went to the lower limits for both poles and the upper limits for both the zeros and the gain. The limits of the search zones were relaxed to $500 < P_i < 600$, $80 < Z_i < 90$ and $3.2 \times 10^6 < G(3) < 3.4 \times 10^6$. The program again placed the free variables on the limits of $P_i = 500$, $Z_i = 90$, and $G(3) = 3.4 \times 10^6$. The system and desired response for these values is shown in Figure 19. The system magnitude and phase are much closer to the desired output response than the response of the conventionally designed compensator.

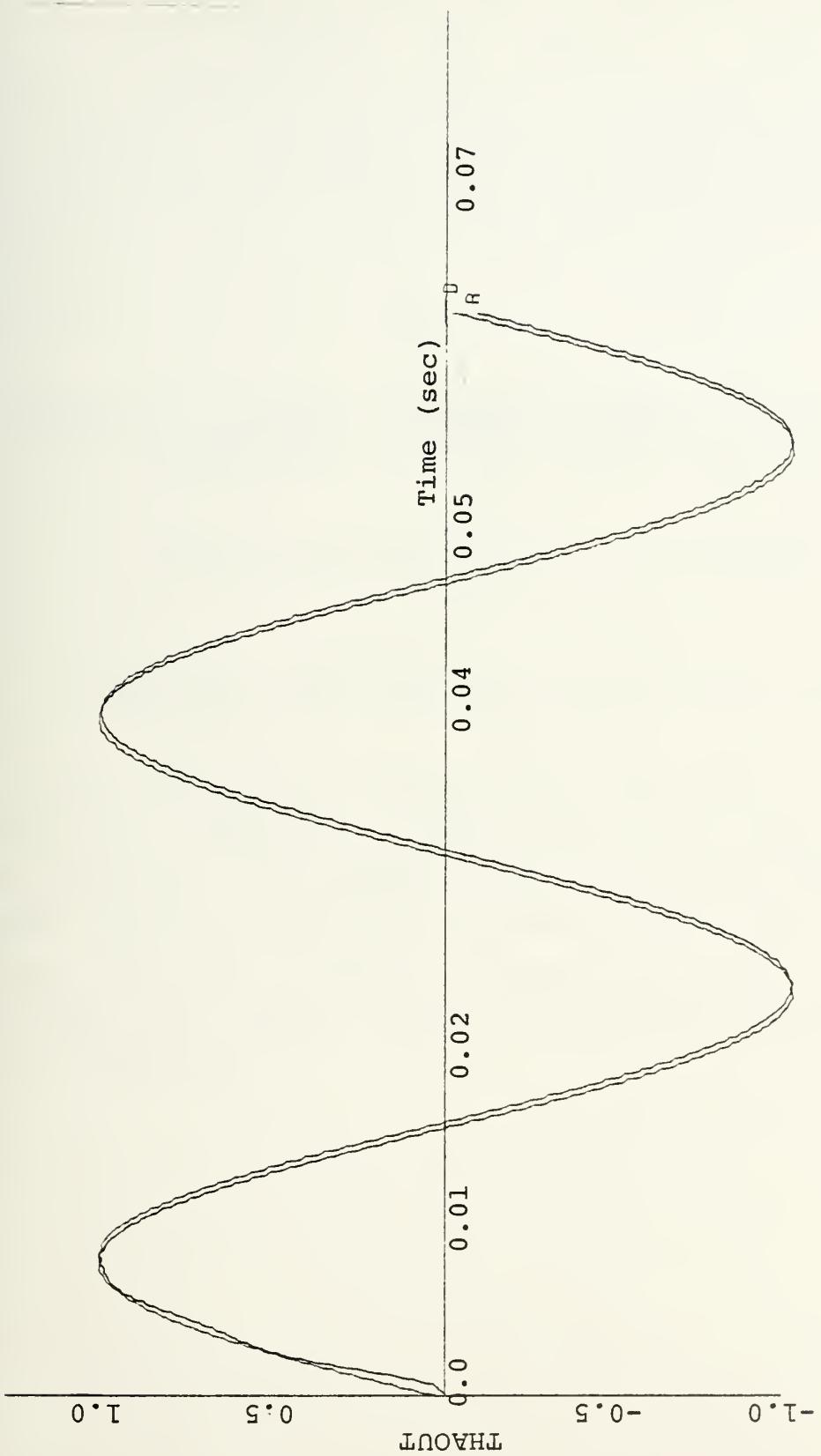


FIGURE 19 CADS Lead Compensated System Response

The phase difference is only 4.33° . Continued relaxation of the boundaries produced the compensated system shown in Figure 20. Figure 21 is a plot of the system's response for these values. The system's response is improved in that it lags the input by only 3.46° and the magnitude is essentially the same as the input magnitude.

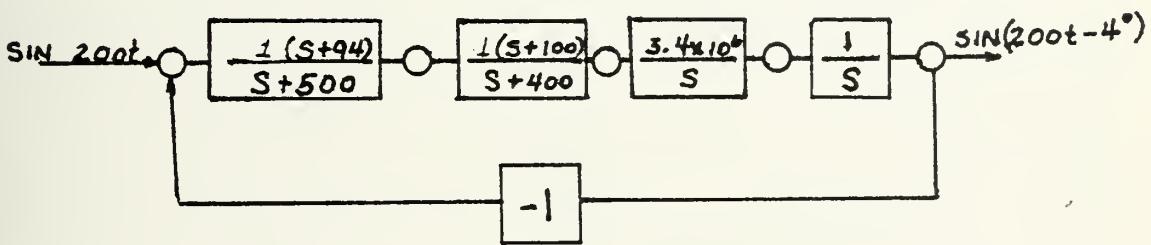


FIGURE 20 CADS Compensated System Block Diagram

The optimization program was activated at $T = 0$ although the problem specifications were for the steady state response. The problem was rerun with the optimization process started after the transient had died out. The same values for the optimum compensator were obtained. Apparently the small initial transient did not effect the problem solution.

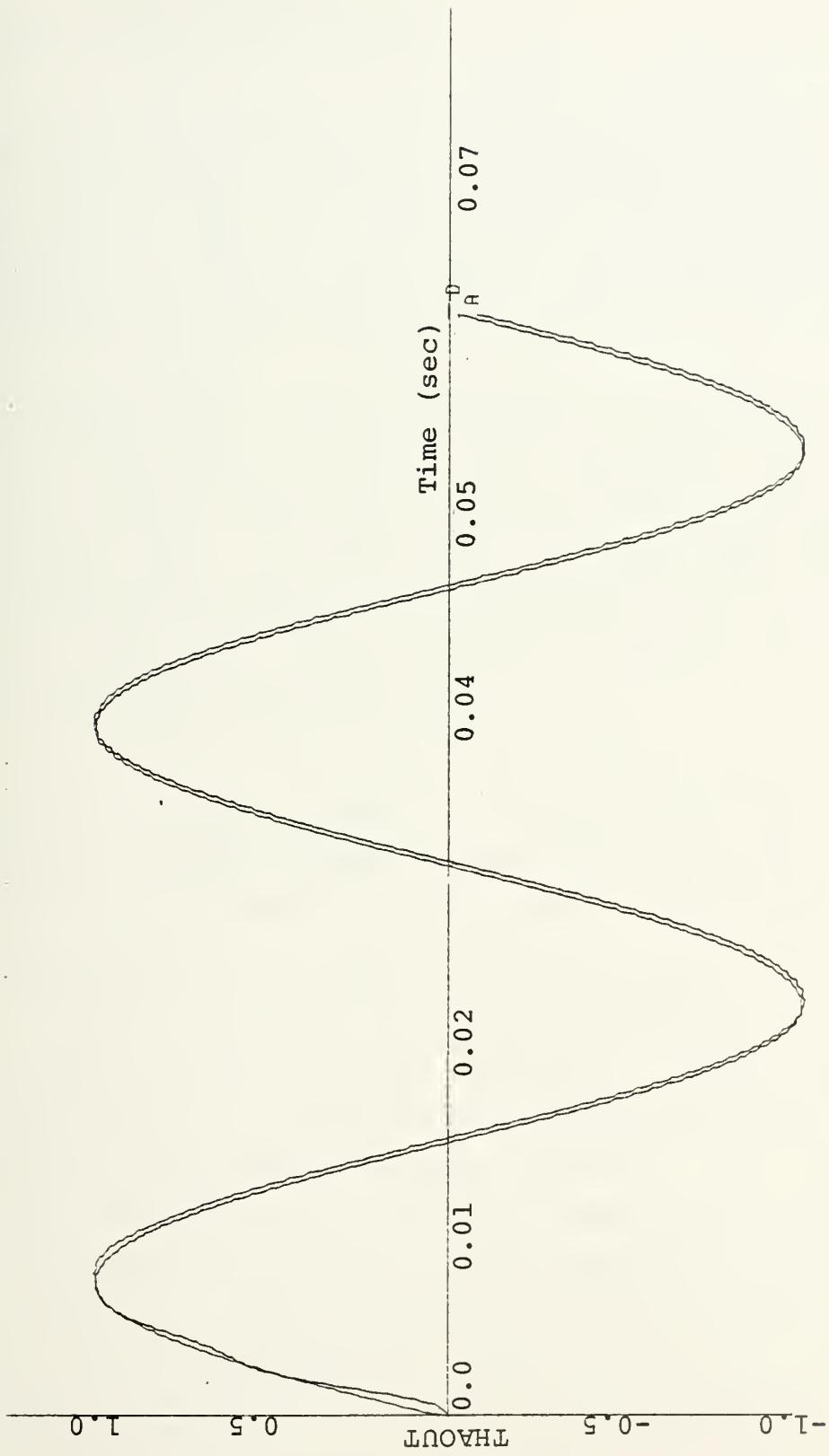


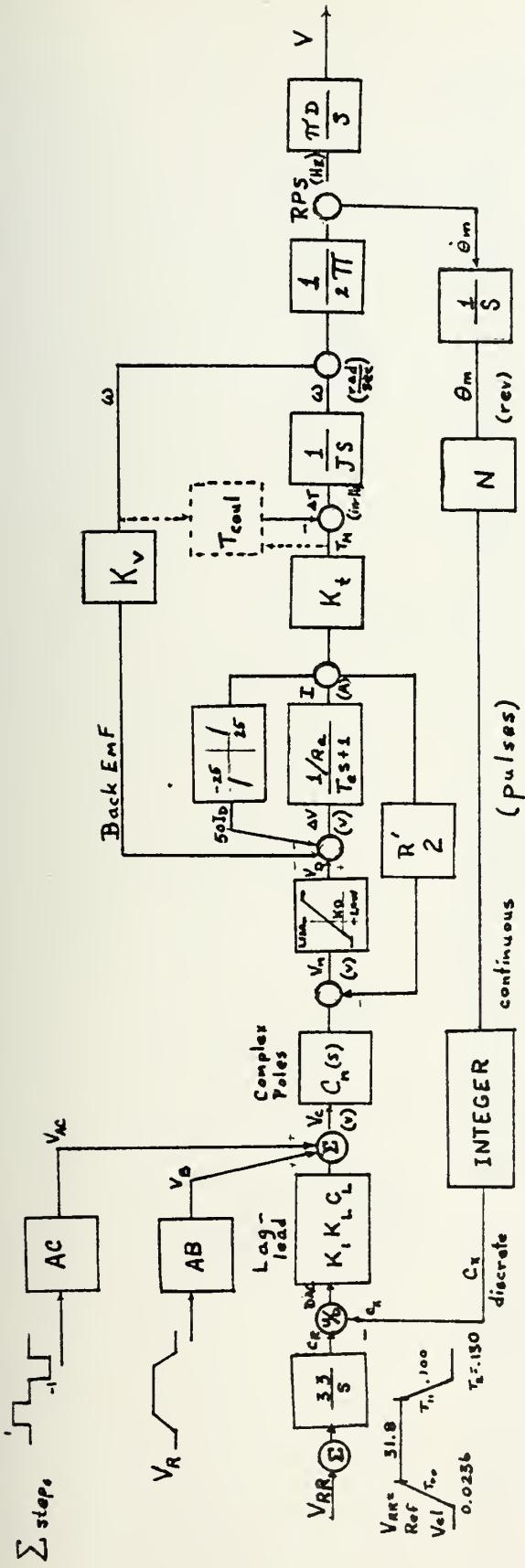
FIGURE 21 CADS Relaxed Boundary System Response

E. SERVO SYSTEM COMPENSATION

The foregoing examples of the simulation - optimization program were simple examples which could obviously be quickly solved with the standard cut and try methods. A more complex and challenging example of program usage is presented by the system shown in Figure 22.

The system is an operational servo drive mechanism with multiple inputs and discrete level feedback. This highly nonlinear system's output was to follow the input as closely as possible and in steady state ($t \geq 75\text{ms}$) there was to be very little noise ripple. The free parameters of the system are the poles and zeros of the compensator, C_L , and the poles of the noise suppressor C_n .

To simulate and optimize the system it was redrawn using the available program blocks as shown in Figure 23. During simulation it was found that the current limiter for I_D was not needed because $|I_D| < 25\text{ A}$ and the limiter was removed to decrease program run time. The desired response (XDATA) was written as a set of three equations. These equations were then used to replace the second order step response equations in the standard program. DRVIN(1), (4) and (5) were also written as a set of equations and placed in subroutine PLANT. The discrete level feedback to block two was achieved by making DRVIN(2) = INTGER(THA(12)). These changes to the main program and PLANT were all that were necessary to simulate this system. The implementation of these changes to the program is shown on pages 80 and 81.



$$\begin{aligned}
 AC &= \frac{AJR_a}{K_t K_D} \\
 AB &= \frac{K_V}{r K_D} \\
 A &= \frac{1}{2} \frac{V_p^2}{X_a} \\
 X_a &= \frac{3}{8} \text{ in.} \\
 V_p &= 31.8 \text{ (in/sec)} \\
 V_R &= A * \sum \text{Ramps}
 \end{aligned}$$

$$\begin{aligned}
 C_L(s) &= \frac{(1+s/50)^2}{(1+s/20)(1+s/500)} \\
 C_n(s) &= \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \\
 \zeta &= 0.5, \omega_n = 1300 \\
 T_c &= 2.425 \text{ (lb)} \\
 T_e &= \frac{L}{R_a}
 \end{aligned}$$

$$\begin{aligned}
 K_1 &= 1.6 \\
 K_L &= 3.48 \\
 K_D &= 2 \\
 L &= 50(\mu H) \\
 J &= 0.0016 \text{ (in.lb.sec}^2\text{)} \\
 r &= \frac{(mD)/g}{2\pi} \\
 K_T &= 0.765 \text{ (in/lb)} \\
 R_a &= 0.5 \text{ (ohm)} \\
 \omega &= 50(\mu H)
 \end{aligned}$$

FIGURE 22 Servo Drive Mechanism, Original Compensation

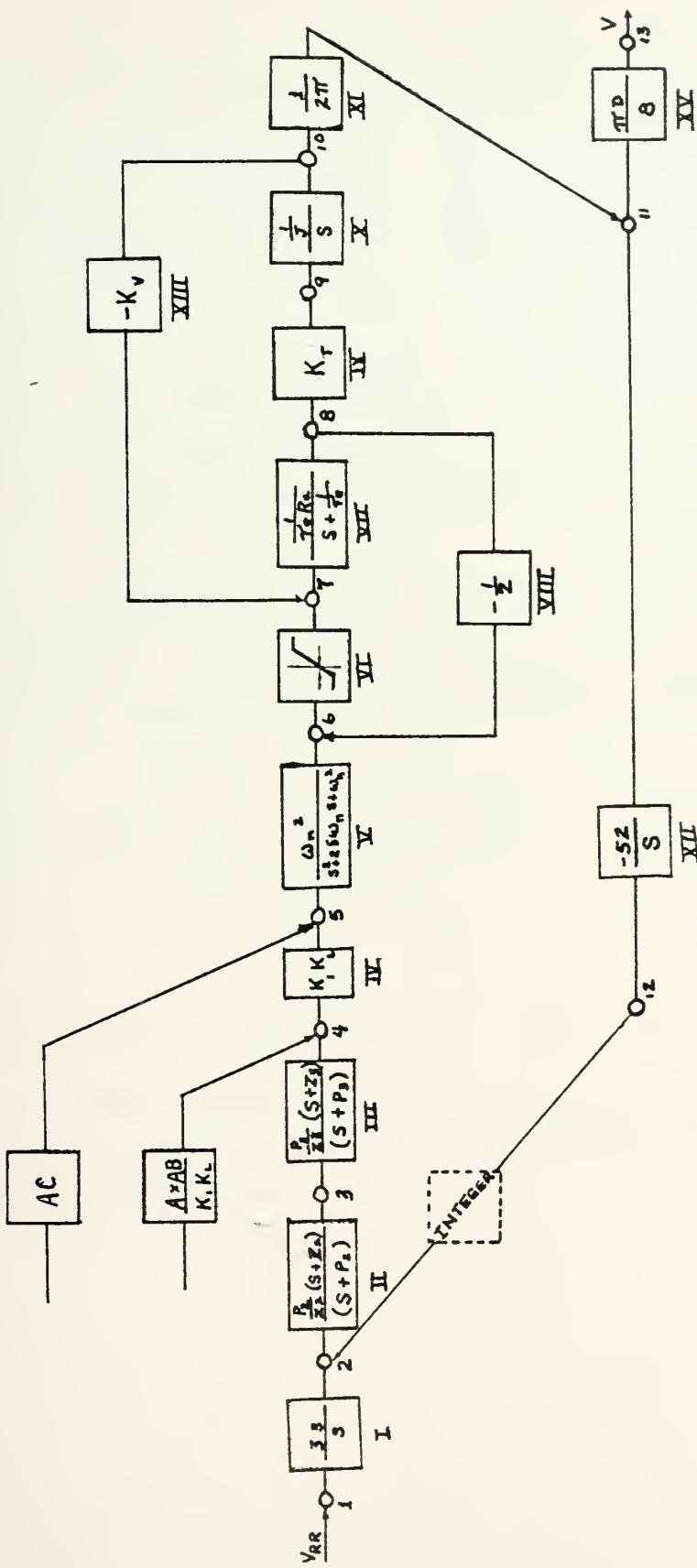


FIGURE 23 CADS Diagram of Servo Drive Mechanism

The system optimization was initially broken into two parts. This was to reduce the number of variables that were to be optimized per run and to obtain near optimum starting values for the free parameters. The above steps were taken in an effort to decrease the computer time required for a solution. The first run was to optimize the compensator, C_L , independent of the noise suppressor. The second optimization run was to select values for the noise suppressor, C_N . The rationale behind this separation was that the two circuits perform different functions and should therefore be initially separable in their effects on the system. The final optimization run was to be made with all free parameters available to the program for optimization. The search zone centered on the values found above.

Figure 24 shows the response for the system as originally compensated. The optimization run to set the values for C_L resulted in $Z_1 = 43.5$, $P_1 = 21.0$, $Z_2 = 47.5$, $F_2 = 592.0$. Figure 25 shows the simulation of the system using these values. The initial velocity overshoot has been reduced and the average velocity after the transient appears more equally distributed above and below the desired velocity.

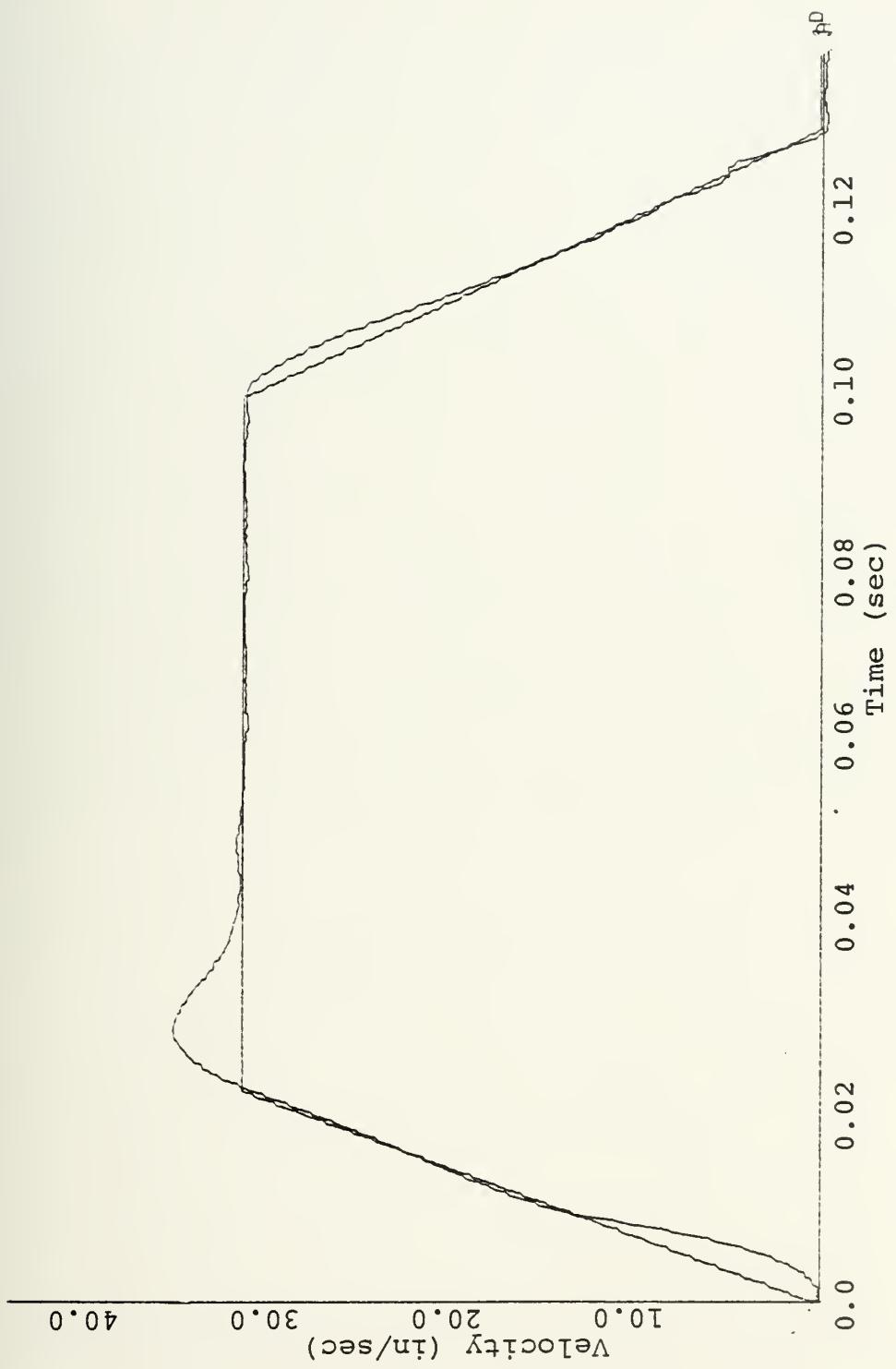


FIGURE 24 Original Servo System Response

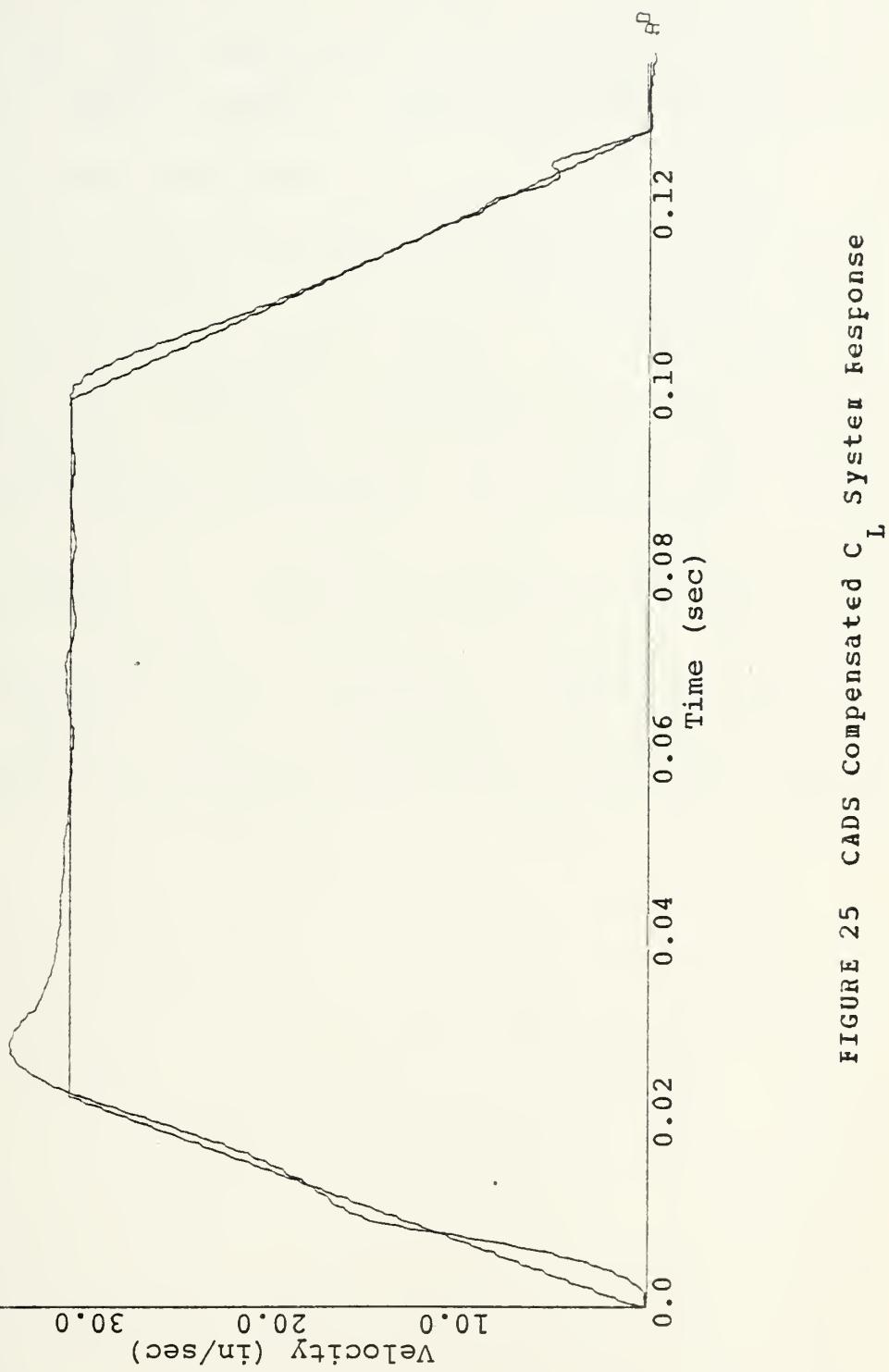


FIGURE 25 CADS Compensated C_L System Response

The initial optimization run for setting the values of the noise suppressor used the same cost function which had been used for all previous optimization runs

$$J = \int_{\text{N}} \text{Err}^2 dt.$$

This resulted in $\delta = 0.2$ (lower bound), and $W_n = 1500$ (upper bound). Figure 26 shows the result of using this cost function was to further decrease the overshoot. However, it allowed larger switching or noise transients as a result of weighting large transient errors more than the lesser noise jitter. To overcome this problem, the cost function was changed to $J = \int |Err| * t * dt$. This was to weight the steady state errors more heavily than the transient errors. Using this cost function the values set by the optimization program were $\delta = .2$ and $W_n = 1430$.

The damping factor, δ , was again placed on the lower limit. The initial overshoot was still improved over the original system's response but the switching transients were not improved over the previous optimization trial. The results of the simulation run using these values is shown in Figure 27.

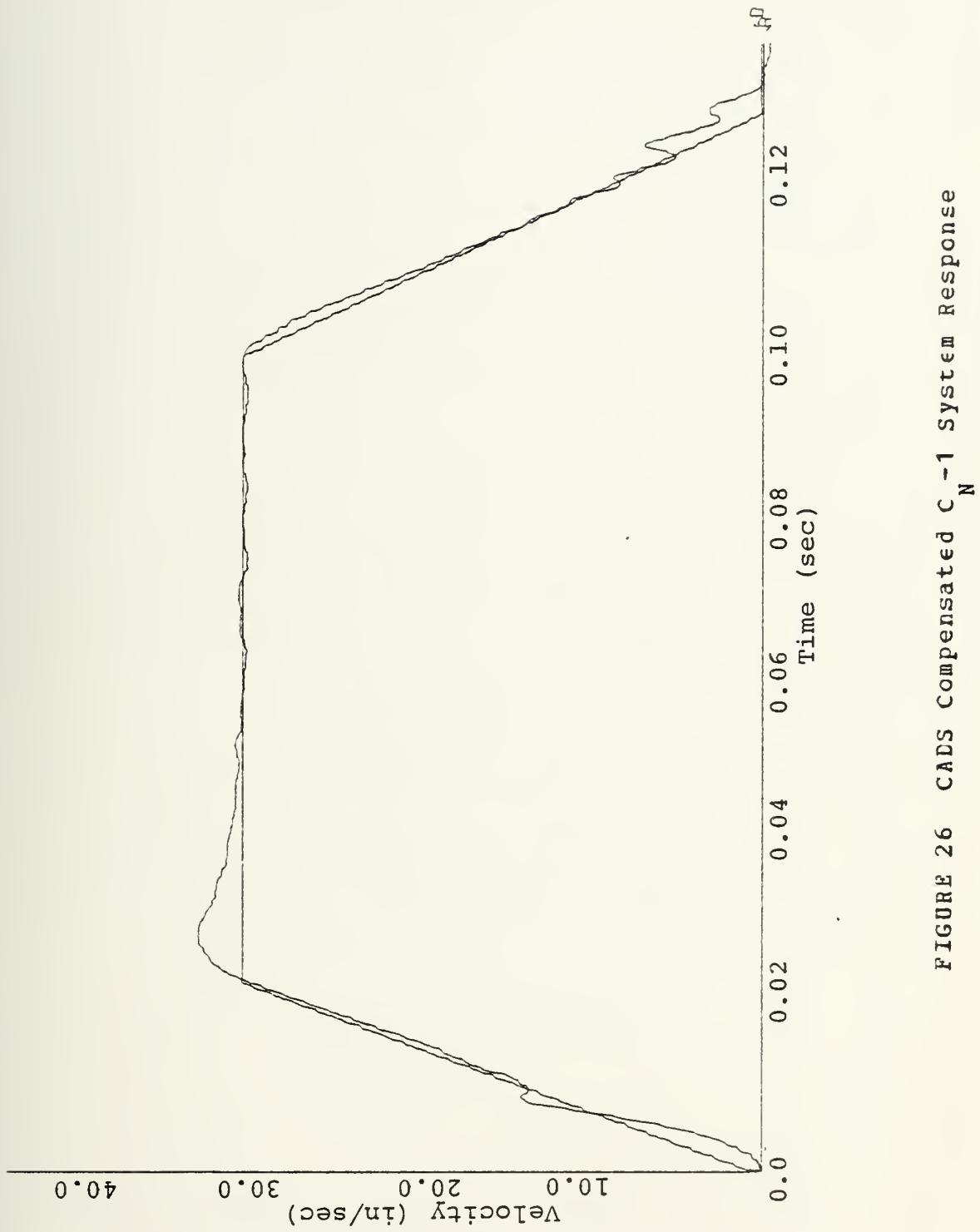


FIGURE 26 CADS Compensated C-1 System Response
_N

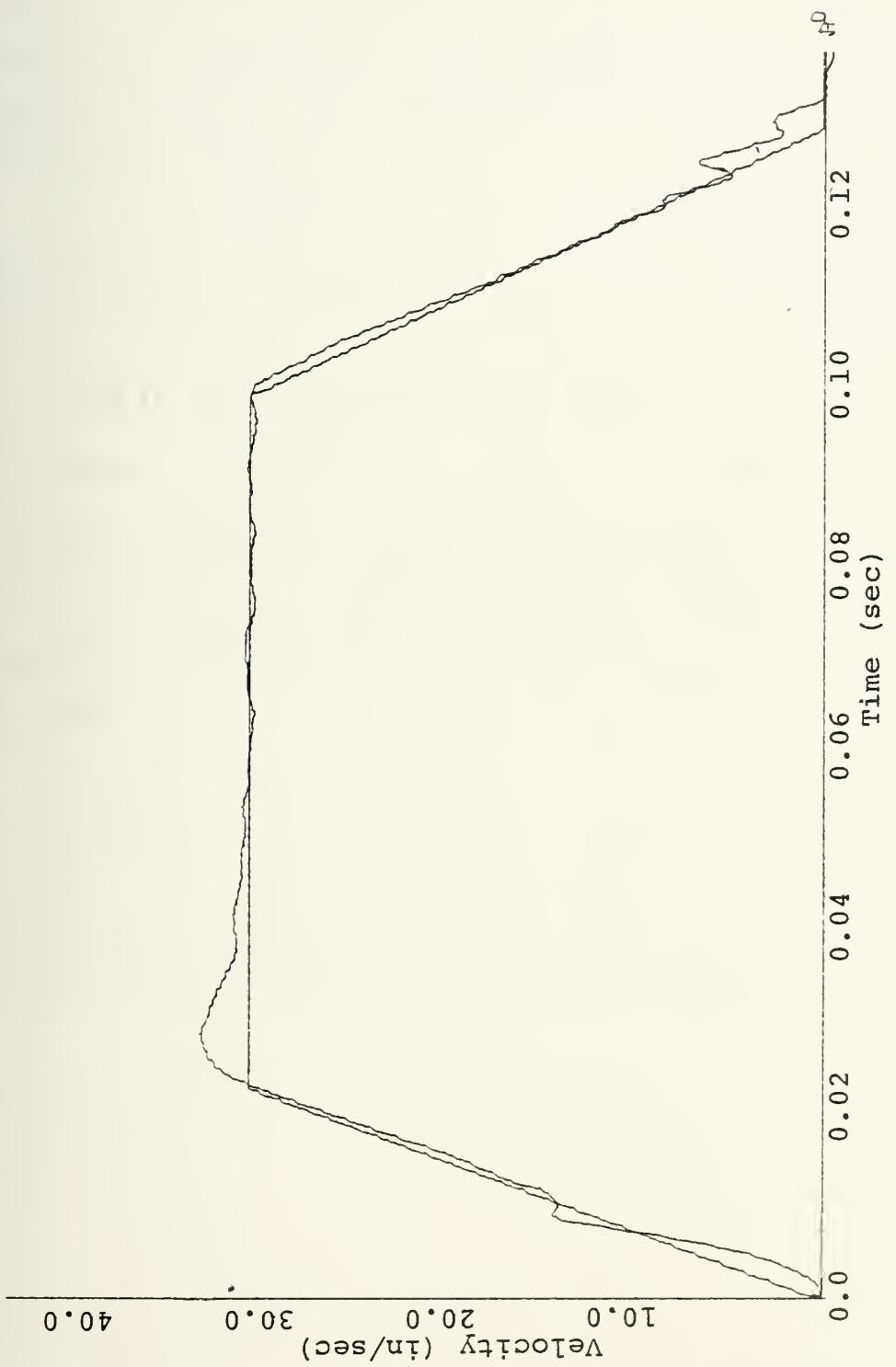


FIGURE 27 CADS Compensated C-2 System Response
N_H

A final optimization run was made with all six variables free. The performance index was changed to the weighted cost function shown in equation V. The weighting factor was computed to equally weight the start up transient and the steady state responses in an effort to reduce the switching transients.

$$\begin{aligned} J &= \int |Err| dt & 0.0 \leq T \leq 0.045 \\ J &= \int 4.14 * |Err| dt & 0.045 < t \leq TF \end{aligned} \quad (V)$$

The optimum compensator values established by CADS were $P_2 = 27.1$, $Z_2 = 52.5$, $P_3 = 521.$, $Z_3 = 48.1$, $\delta = 0.32$ and $W_n = 1268$. Figure 28 shows the fully compensated system's response. The initial overshoot has been reduced and the average velocity in steady state is closer to the desired value than the original system's response. However, the transient error on shut off is still present. Table II. summarizes the results of the optimization of the servo system.

The CPU time required for the optimization process was not decreased by splitting the problem into two separate parts. The time required for each optimization run on the individual compensators was the same as the time required to optimize the complete system with six variables.

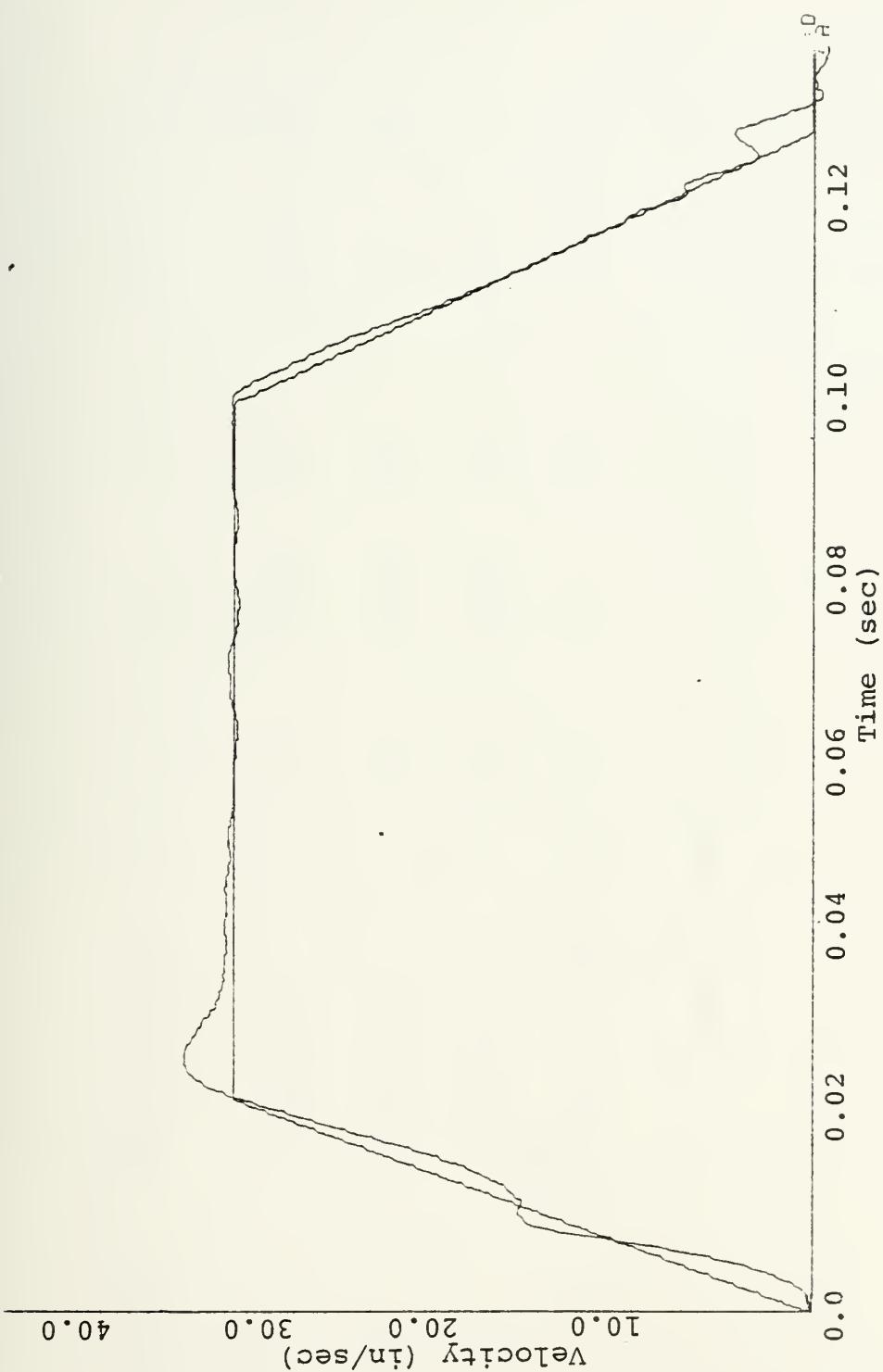


FIGURE 28 CADS Optimized System Response

Compensator	Cost Function	P_2	Z_2	P_3	Z_3	δ	w_n
C _{original}		20.	50.	500.	50.	0.5	1300
C_I	$\int_{\text{Err}^2 dt}$	21.	43.45	592	47.47	0.5	1300
C_N	$\int_{\text{Err}^2 dt}$	21.	43.45	592	47.47	0.2	1500.
C_I, C_N	$\int_{0.045}^{0.047} \text{Err} * t dt$ $\int_{0.045}^{0.047} \text{Err} dt + 4.14 \int_{0.045}^{0.047} \text{Err} dt$	21.	43.45	592	47.47	0.2	1430.

TABLE II Summary of Servo Drive Optimization

This problem has presented an excellent example of the necessity to carefully select the cost function which will measure the system's performance. Defining a performance index which will weight the more objectionable characteristics of a system's response so that they are eliminated or reduced becomes difficult as the system's complexity increases. The performance index, $J = \int (Err)^2 dt$, was not adequate in its treatment of the noise and switching transients for the above problem. The other performance indexes used were also marginal in their effects upon parameter optimization. Although the cost function was reduced to a mathematically correct minimum, the system's performance was not the best that could be achieved. The system's performance was only optimum due to the definition of the cost function. The system was simulated using the compensator values determined from the last optimization run with the exception of δ which was increased to $\delta = 0.5$. This simulation was made based upon engineering judgment of the effects of varying δ . Figure 29 shows that this change in the damping factor produced a system response which was nearer the desired response than any of the previous runs.

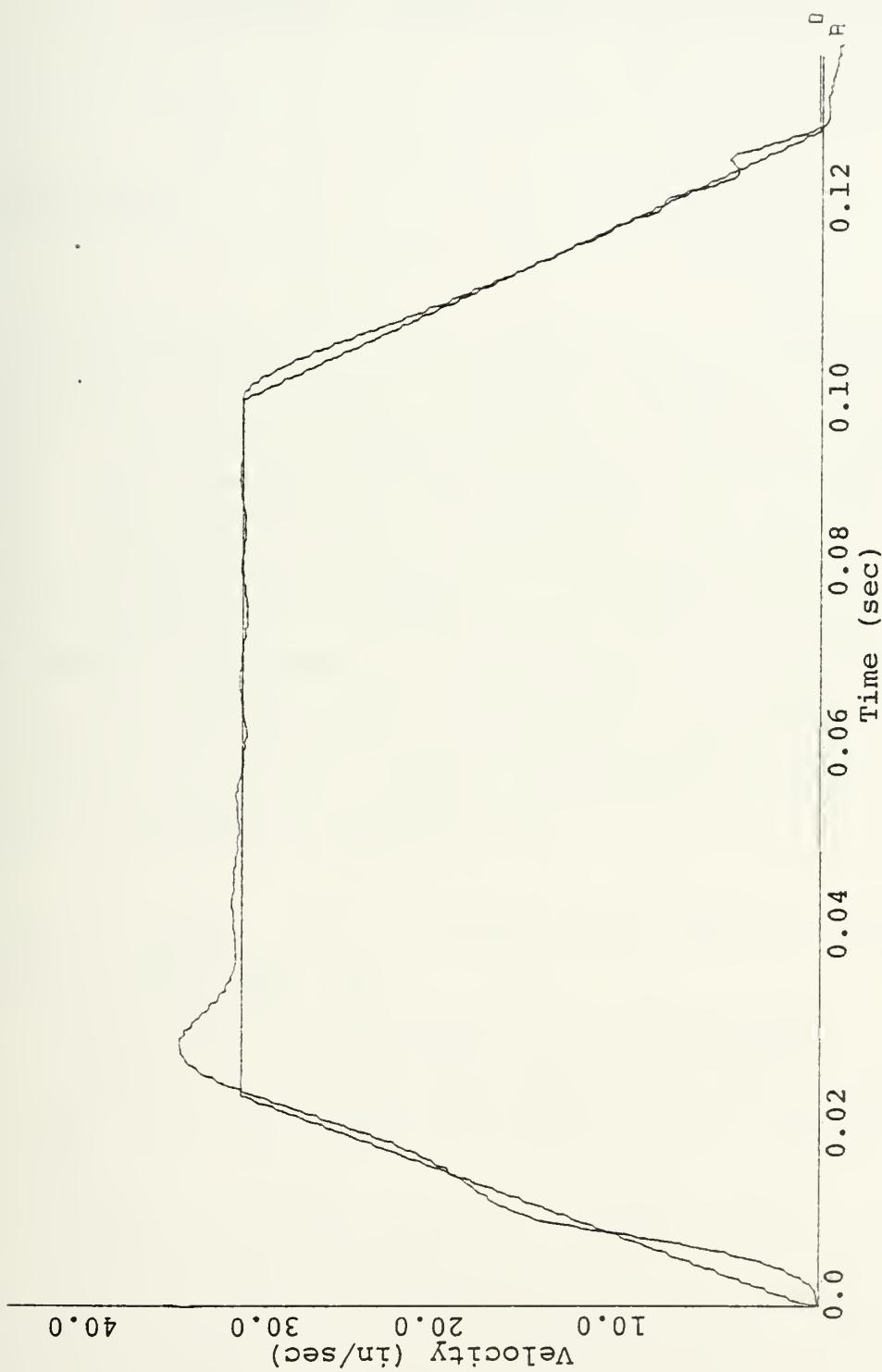


FIGURE 29 Servo System Response, CADS Values with $\delta = 0.5$

IV. DISCUSSION, CONCLUSIONS AND RECOMMENDATIONS

A. DISCUSSION

The objective of this thesis was to investigate the feasibility of developing a computer program which would optimize a variety of control systems' responses in the time domain. The program developed during the investigation proves that time domain optimization of control system responses is not only feasible but desirable due to the readily interpretable results of the optimization process. CALS requires approximately 200K bytes of computer core when the high speed printer plot is used for graphical display of the output and 230K when outputting calcomp graphs. These core requirements are a maximum and could be reduced by more careful, professional programming.

The computer time required for CALS to arrive at a solution is dependent upon

- (1) the order of the system being simulated,
- (2) the area of the search zone determined by the upper and lower bounds on the variable parameters and
- (3) the nearness of the starting guess to the optimum parameter values.

Every trial value of a parameter selected by FOXPLX requires a complete simulation of the system in order to evaluate the system's response and compare it with the desired response. The program run time is therefore, $T_{Run} = \text{the number of trials} \times \text{system simulation time}$. A high order system may

require twenty seconds of CPU time for simulation. If 300 trials are required to determine the optimum parameter values, the total CPU time would be 100 minutes.

Example Problem	Lower Bound	Starting Guess	Upper Bound	Number of Trials	CPU Time Required
	III	XL	XS	XU	
b (pseudo)	-300	-34.3	-3	55	7min03sec
c	.001 .01	.01 .1	0.1 1.0	225 225	24min53sec 24min53sec
d	400 400 90 90 3.4×10^6	450 450 95 95 3.5×10^6	500 500 100 100 3.5×10^6	2,000	68min
e	10 40 400 .3 1150	20 50 500 .5 1300	30 60 600 .55 1400	230	4hr

Table III

Table III presents a summary of the search zones and times required to obtain a solution for some of the problems considered in this thesis. The amount of CPU time required for a solution, especially for problem III-E, may seem excessive. However, there are several considerations which should be made prior to arriving at this conclusion.

- (1) The equations of the system do not have to be written, programmed nor debugged if the system's

component transfer functions are known.

(2) Time domain requirements do not have to be translated into frequency domain specifications for system simulation and design.

(3) A systematic search is carried out to obtain the optimum parameter settings. This assures that with valid bounds on the variables an acceptable solution will be obtained with the first optimization attempt.

The time required to perform the above steps in the design process by conventional means may result in many more hours of CPU time than if the program CADS were used from the beginning of the design process.

Several means of reducing the computer time required for optimization were previously outlined in section II. The most significant reduction is obtained by keeping the number of integrations required for system simulation to a minimum. Block diagram reduction of the system should be accomplished whenever possible. The example of the Ward Lechner drive system shown on page 26 can be reduced to the simple system shown in Figure 30 by block diagram reduction.

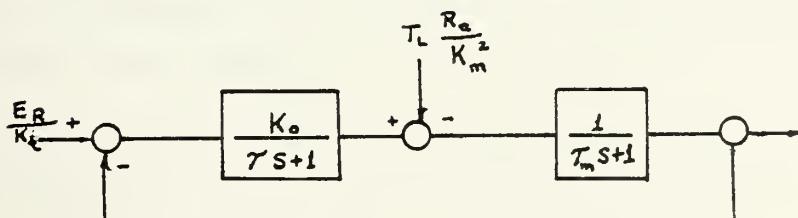


FIGURE 30 Block Reduced Ward-Lechner Drive

Section III.E. showed the effect of using different cost functions to measure the quality of the optimized response. Although the integral error squared criteria is often used to judge a system's performance, the user should carefully consider how to best define a cost function which will properly penalize deviations of the system response from the desired response. A small error ($\text{err} < 1$) squared becomes even smaller. If all the errors are small, the IES is a valid cost function but if the system response involves large and small errors a weighted cost function will have to be used. One method of arriving at a properly weighted cost function is to simulate the system using first estimates of the variable parameters and recording the sum of the errors over the different portions of the response. A ratio of the errors can then be used to arrive at proper weighting factors for each time section of the response.

BOXFIX will continue the optimization process, working in the seventh significant digit until it can no longer reduce the cost function. Often an acceptable solution for the system parameters has been found long before the cost function has been reduced to its minimum. A judicious use of CADS may be made by evaluating the system response after ten to fifteen minutes of run time to see if an acceptable solution has been found.

B. CONCLUSIONS

Time domain optimization using the CADS program is a simple, straight forward process which does not require an in-depth analysis of the system being optimized. Economic use of CPU times does dictate that intelligent starting values and bounds be placed on the variable parameters which are to be optimized.

The program is a readily usable tool for simulation without optimization. It is competitive with, if not superior to, other common simulation routines when simulating typical control systems. This feature alone is expected to bring the program into common usage.

C. RECOMMENDATIONS FOR FUTURE WORK

- (1) All integral calculations performed during this investigation were done in double precision for increased accuracy of the system response. The possibility of using single precision calculations should be investigated to decrease core requirements.
- (2) The ability to begin the optimization process at some time greater than zero should be provided. This will necessitate modification of the data input cards and block equations so that initial conditions can be entered.
- (3) The program presently requires that external forcing functions (DEViNs) and the variables which are to be optimized be specified by Fortran IV statements placed within the body of the program. A method of reading these specifications from data card input should be developed so that the user will not have to "shuffle" cards in the program deck.
- (4) The graphical output of CADS was all that was necessary for the investigations conducted in this thesis but a provision for numerical output of selected responses should be provided for detailed analysis.
- (5) The feasibility of reducing the number of significant digits BCKPLX uses should be studied as a means of reducing optimization time. Also some criteria might be developed to reject a system's response before TF is reached if it is determined to be unacceptable.

(6) A method of automatically relaxing the boundaries on the variables being optimized when they go to their limits should be developed.

(7) The standard cost function provided and all user developed cost functions should be normalized. This would permit a more direct and easier comparison of a system's "goodness" when several different integration step sizes or run times have been used in the optimization process.

APPENDIX A

Block Data Card Format

| 1 | 11 | 20 | 40 | 60

BLKCCD=EEVV G P Z

CC = POSITION NUMBER OF THE BLOCK
D = TYPE OF BLOCK (NUMBER)
EE = INPUT NODE NUMBER
VV = OUTPUT NODE NUMBER
G = VALUE OF GAIN
P = VALUE OF THE POLE*
Z = VALUE OF THE ZERO*

* For block type 4, θ is read into the P location and ω_n is read into the Z position.

* For block type 5, θ_u is read into the P position and θ_l is read into the Z position.

* For block type 6, θ_c is read into the P position and θ_e is read into the Z position.

EXAMPLES

G

BLKC11=0102 10.

G P

BLKC12=0304 1. 5.

G P Z

BLKC13=0405 1. 10. 5.

	G	δ	ω_N
B1K104=1006	200.	.2	14.14
	G	θ_u	$-\theta_L$
B1K115=1207	10.	20.	-5.
	G	θ_c	θ_B
B1K126=0708	1.	3.	10.

*See Table I.

APPENDIX B

Plant Flow Chart

FUNCTION PLANT (C)

```
CIMENSION G(25), P(25), Z(25), FLAG(25,25), CM
G(25), THACLT(25), CMGDOT(25), DRVIN(25),
NFI(25), IR(25), IV(25), X2(25), X2D0T(25),
CRIVE(25), THA(25), IC(25), ID(25), IE(25),
THACLT(3001), XDATA(3001), C(25)
```

```
REAL *8THACLT
```

```
REAL *8XDATA
```

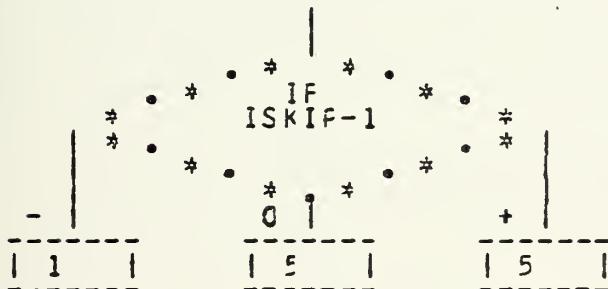
```
REAL *8THA, THACLT, T, DT, CRIVE, CMG, CMGDOT, DRVIN, TF
```

```
REAL *8F1, F2
```

```
REAL *8X2, X2DCT
```

```
CCMMCN T, CT, TF, THACLT, XDATA, M3, ICCNT, NEG, ISKIP, ITF
```

FOR OPT RUNS, INFILEIT READ STATEMENTS AFTER READING



1

```
| ISKIP=2 |
```

```
***READ (5,24) N, ISET
```

INITIALIZE COUNTERS

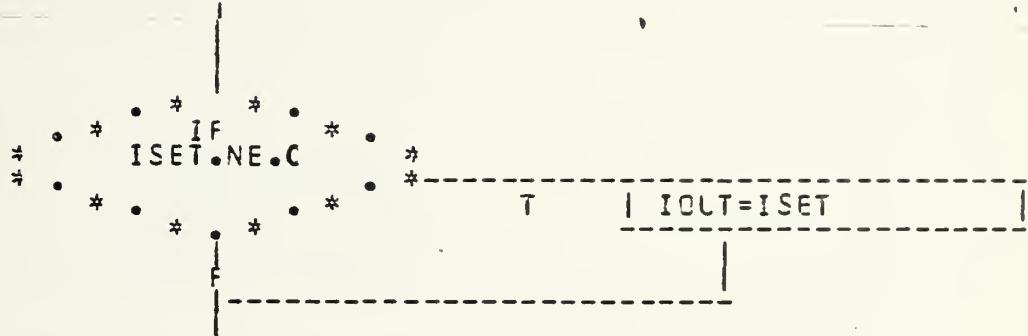
```

    ICUT = C
    IVCLT = C
    F1 = CT
    F2 = C.500*F1
    N11 = C
    N55 = C
    N66 = C
    ICK = Z=N
  
```

READ INPUT DATA

```
+-----+
+ DC +
+ I=1,N +
+-----+
|  
***READ (5,25) IC(I),ID(I),IE(I),IV(I),G(I),P(I),Z(I)  
|  
SET TFACT = CLTPLT OF LAST BLOCK  
|  
+-----+
+ * . * IF * . *
+ * (IV(I)-IVCLT).LE.0 *
+ * . * . * . *
+ * . * . * . *
+-----+ T | 2 |  
F  
+-----+
| IVCLT=IV(I)
| ICLT =IC(I)
+-----+  
2 +-----+
+ * . * IF * . *
+ * ID(I).EG.1 * . *
+ * . * . * . *
+ * . * . * . *
+-----+ T | N11=N11+1 |
F  
+-----+
+ * . * IF * . *
+ * ID(I).EG.5 * . *
+ * . * . * . *
+-----+ T | N55=N55+1 |
F  
+-----+
+ * . * IF * . *
+ * ID(I).EG.6 * . *
+ * . * . * . *
+-----+ T | N66=N66+1 |
F  
+-----+
3 +-----+
***WRITE (6,26) IC(I),ID(I),IE(I),IV(I),G(I),P(I),Z(I)
```

SET THACLT = SPECIFIED THETA, IF ANY

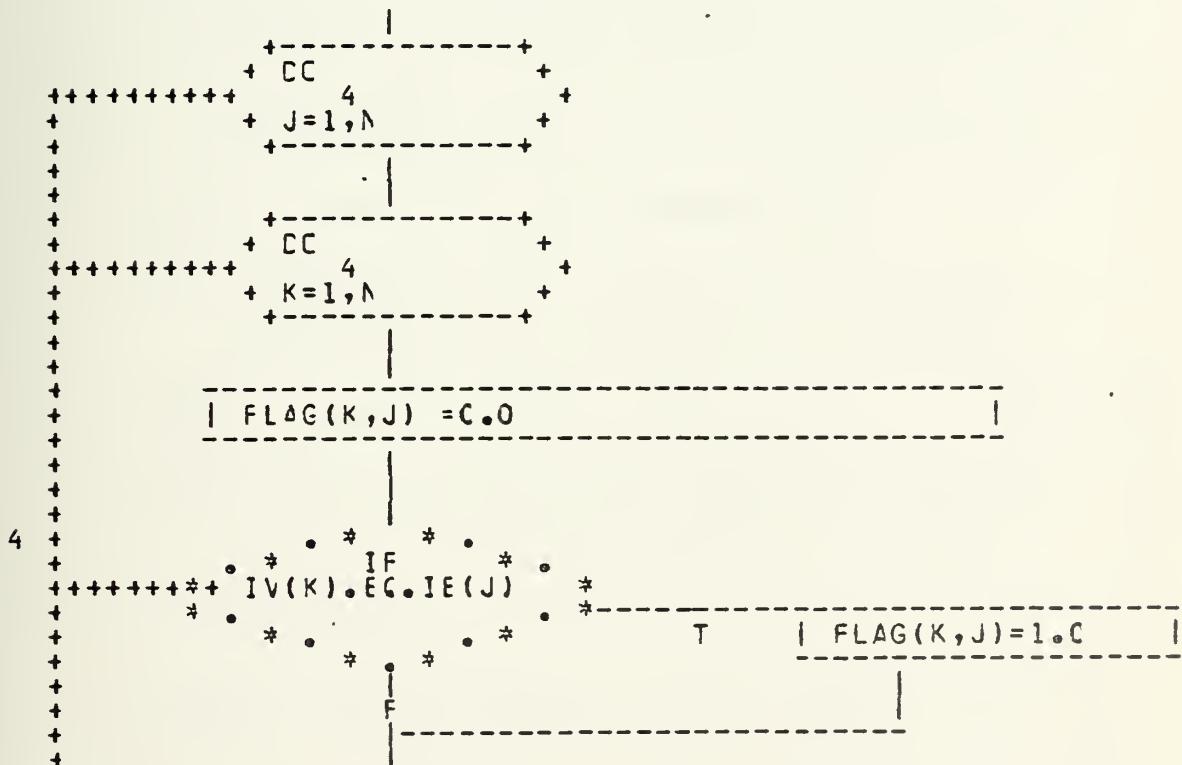


***WRITE (6,27) ICUT

```
| N11 = 4*N11
| N55 = 4*N55
| N66 = 4*N66
| NEC = N-1
```

SCAN FCR INPLTS

CONNECT SYSTEM BY SETTING FLAG=1. FOR CONNECTED BLKS



TAKE BLK TYPE AND SOLVE EQUATIONS ONE BY ONE

CLEARING CLT REGISTERS AND INITIALIZING COUNTERS

```
5 +-----+
+ ICLR=1,N +
+-----+
| TFA(ICLR) =0.00
| THACGT(ICLF) =0.00
| CMG(ICLR) =0.00
| CMGDOT(ICLR) =0.00
| CFVIN(ICLR) =0.00
| X2(ICLR) =0.00
+-----+
6 | X2DCT(ICLR) =0.00
| =0.000
+-----+
```

NR'S CONTROL ENTRY POINT IN INTEGRATION SUBROUTINES

```
+-----+
| NR2 =1
| NR3 =1
| NR4 =1
+-----+
```

M3 CONTROLS WHICH BLOCK EQUATION IS BEING SOLVED

```
+-----+
| M3 =0
+-----+
```

ICCNT IS USED TO CONTROL PROGRAM FLOW

```
+-----+
| ICCNT=0
+-----+
```

IWAIT IS USED TO CONTROL TIME. TIME IS STEPPED EVERY
FIRST AND THIRD PASS THRU INTEGRATION ROUTINES

```
+-----+
| IWAIT=0
| IT =0
+-----+
```

ILAST'S CONTROL PROGRAM DATA AND PROGRAM EXIT

```
+-----+
| ILAST=0
| IELAST =0
| IELAST =0
+-----+
```

SPECIFY ANY PARAMETERS TO BE OPTIMIZED HERE

EG. $F(1)=C(2)$, $Z(1)=C(1)$,

SET DRIVES FOR INFITS

7
+-----+
+ DC +
+ MDRV=1,N +
+-----+
| CRVIN(1) =1.
| DRIVE(MDRV) =0.00
+-----+
+ DC +
+ M=1,N +
+-----+
8 | DRIVE(MDRV) =CRVIN(MDRV)+TRA(M)
| #FLAG(M,MDFV)
+-----+
9 | DRIVE(MDRV) =CRVIN(MDRV)+DRIVE(MDRV)
+-----+
10 | M2 =M2+1
+-----+

PICK TYPE EGN TO SOLVE

* * . * * . *
* . * IF * . *
* . * IWAIT.EG.0 * . * T | T=T+H2
* . * . * . * . *
* . * . * . * . *
* . * IF * . * T | 11
* . * IEG(M2).EG.1 * . *
* . * . * . * . *
* . * . * . * . *

* * * IF
* * * ID(M₂).EC.2 * *
* * * T | 12 |
F
* * * IF
* * * ID(M₂).EC.3 * *
* * * T | 13 |
F
* * * IF
* * * ID(M₂).EC.4 * *
* * * T | 14 |
F
* * * IF
* * * ID(M₂).EC.5 * *
* * * T | 15 |
F
* * * IF
* * * ID(M₂).EC.6 * *
* * * T | 16 |

***WRITE (6,28)

STCF

START SCLUTICA

TYPE ONE EQUATIONS

SOLVES THACLT = G*THAIN

11

```
|-----|  
| THA(M3) = G(M3)*CRIVE(M3)  
| IWAIT=IWAIT+1  
| ILAST=ILAST+1  
|-----|  
|-----|  
| * * * IF * * *  
| * (ILAST.EC.N11).AND.(ICGNT.EC.NEQ)  
| * * * * * * * T | 21 |  
| * * * * * * *  
| F  
|-----|  
| 18 |
```

TYPE TWO EQUNS

SOLVES THACLT/THAIN = G/(S + P)

12

```
|-----|  
| THADOT(M3) = -P(M3)*THA(M3)+G(M3)  
| *CRIVE(M3)  
| S = RKLCE2(THA,THADOT,NR2)  
| IWAIT=IWAIT+1  
|-----|  
|-----|  
| * * * IF * * *  
| * S-1.0 * * *  
| * * * * * * *  
| C |  
| + |  
|-----|  
| 17 | | 18 | | 21 |  
|-----|
```

TYPE THREE EQUNS

SOLVES THACLT/THAIN = G*(S + Z)/(S + P)

13

```
|-----|  
| CMGDOT(M3) = -P(M3)*CMG(M3)+G(M3)  
| *CRIVE(M3)  
|-----|  
|-----|
```

S=RKLDE3(CMG,CMGDCT,NR3)

THA(M3) = (Z(M3)-F(M3))*OMG(M3)
+G(M3)*DRIVE(M3)
IWAIT=IWAIT+1

IF S-1.0
0 +
17 18 21

TYPE FCLR EQU.

SCLVES THACLT/THAIN = G/(S**2 + 2*DELTA*WN*S + WN**2)

14

V =CCFLX(F,Z,G,DRIVE,X2,CMG,NR4)
THA(M3) =CMG(M3)
IWAIT=IWAIT+1

IF V-1.
0 +
17 18 21

TYPE FIVE EQU

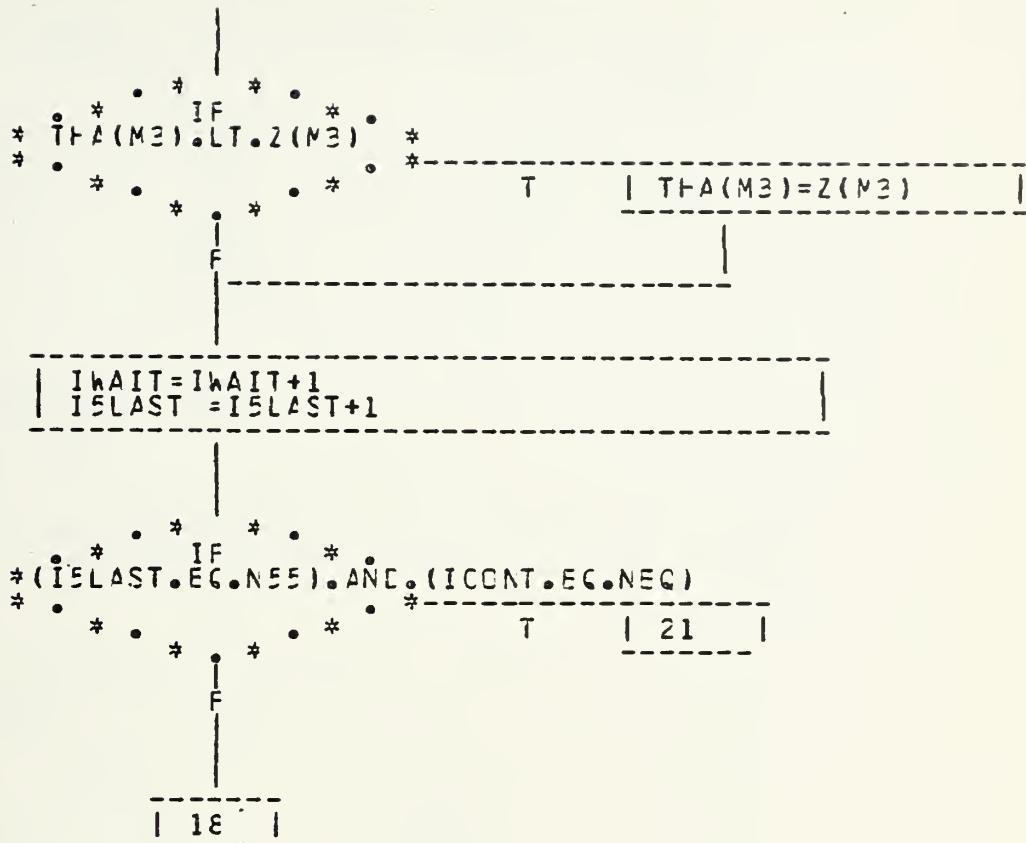
SCLVES THAOLT = G*THAIN FOR /G*THAIN/ < SAT LIMITS

15

THA(M3) =G(M3)*DRIVE(M3)

IF THA(M3).GT.F(M3)
THA(M3)=P(M3)

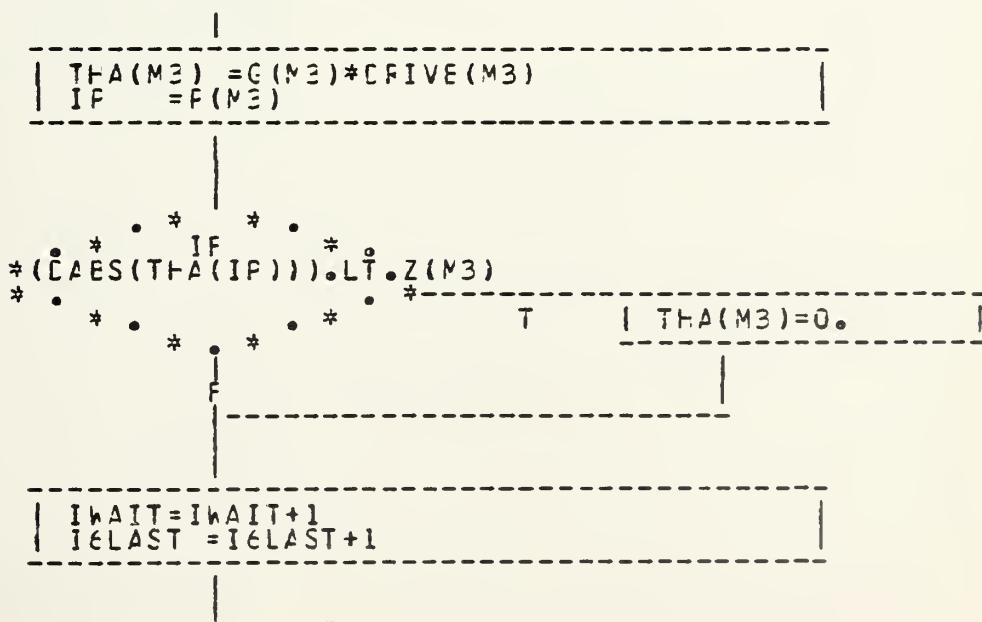
F



• TYPE SIX ECNS

SCLVES THAOLT = G*THAIN FCR CNT REF > C Z BCUND

16



```

* (IELAST.EC.NEE) . AND. (ICONT.EC.NEG)
*          *          *          *          *
*          *          *          *          *          T   | 21 |
*          *          *          *          *
*          F
*          |
*          18

```

17 ***WRITE (6,29)

STCF

18 | ICCNT=ICCNT+1

```

*          *          *          *          *
*          *          *          *          *          IF
*          *          *          *          *          ICCNT-N
*          *          *          *          *          *
*          *          *          *          *          0
*          *          *          *          *          +
*          10      | 19      | 20

```

CNE PASS HAS BEEN MADE FOR EACH EGN. INCREMENT

```

| NR2 = NR2+1
| NR3 = NR3+1
| NR4 = NR4+1
| N2 = C
| ICCNT=0

```

```

*          *          *          *          *
*          *          *          *          *          IF
*          *          *          *          *          IWAIT.EQ.ICK
*          *          *          *          *          *
*          *          *          *          *          T   | IWAIT=0 |
*          *          *          *          *
*          F
*          |
*          7

```

20 ***WRITE (6,30)

STCF

CATA CCOLLECTION FCINT. DATA IS RECORDED AT END OF
COMPLETE TIME STEP(CT)

21

```
| IT = IT+1
| THACUT(IT) = THA(IOLUT)
```

TEST FOR END OF FLN

```
IF T-TF < 0
  22
  22
  23
```

RESET COUNTERS FOR NEXT PASS THRU EQUATIONS

22

```
NR2 = 1
NR3 = 1
NR4 = 1
N2 = 0
ICCNT = 0
IWAIT = 0
ILAST = 0
ISLAST = 0
IELAST = 0
```

23

```
| FLANT=1.
```

RETURN

```
24  FCFORMAT (I2,2X,I2)
25  FCFORMAT (3X,I2,I1,1X,2I2,8X,3E20.7)
26  FCFORMAT (/,5H ELK ,I2,I1,2H =,2I2,6X,3E20.7)
27  FCFORMAT (//,2X,'THETA CUT IS THA(',I2,')')
28  FORMAT (4CH *** EGN SWITCH CONTROL DID NOT WORK)
29  FCFORMAT (2CH INTEGRATION TRUELE)
30  FCFORMAT (5EH ERROR IN INTERGATION. ATTEMPTED TO
      INTEG. MORE THAN N-EGN)
```

END

```

C DECK MODIFIED FOR PROBLEM III-E.
C MODIFICATIONS TO MAIN
C CALCULATE STANDARD SECUND ORDER SYSTEM RESPONSE FOR EXPLOS DATA
C  $X_{LEAP} = -2*E*WN*XD - WN**2*X + DRV$ 
C
C ILEATA = 0
C X(1) = 0.00
C
C C NOT COMPUTE DATA CURVE IF LEAP = 1
C IF (LEAP.EQ.1) GO TO 5
C X(2) = 0.00
C NT = 0
C T = T+DT
C
C 181 IF(T.GE.0.13) GO TO 1812
C IF(T.GE.0.1) GO TO 1812
C IF(T.GE.0.0236) GO TO 1812
C IF(T=1.247*4*DT) GO TO 1811
C
C 1811 X(1)=31.8
C C T0 1814
C X(1)=31.8-10600.* (T-0.1)
C 1812 C T0 1814
C ILEATA=ILEATA+1
C
C 1814 XLEATA(ILDATA)=X(1)
C ILETA(T-TF)181183.102
C NEW HAVE STANDARD VALUES
C 1E3 CONTINUE WITH PROB
C
C MODIFICATIONS TO PLANT
C
C 7 CC S MCRV=1,N
C CFVIN(1)*S GO HERE IF FUNCTIONS CF TIME
C
C 8888 THA12=THA(12)
C INERV=INT(THA12)
C CFVIN(2)=FLOAT(INERV)
C IF(IWAIT.EC.0) T=T+H2
C IF(T.GE.0.13) GO TO 1122
C IF(T.GE.0.01) GO TO 1123
C IF(T.GE.0.0236) GO TO 1124
C CFVIN(1)=1247.46*T
C
C 1290
C 1300
C 1310
C 1320

```

```

1124 CC T0 1125
      CFVIN(1)=31.8
1125 CC T0 1125
      CFVIN(1)=31.8-1060.* (T-0.1)
1126 CC T0 1125
      CFVIN(1)=0.0
1127 CC T0 1126
      CFVIN(1)=LT*0.02361 GC T0 1126
      IF(T*GT*0.1) GO T0 1127
1128 CC T0 1128
      CFVIN(5)=2.809
1129 CC T0 1129
      CFVIN(5)=0.131 GO T0 1128
1130 CC T0 1129
      CFVIN(5)=-2.809
1131 CC T0 1129
      CFVIN(5)=0.
1132 CC T0 1130
      CFVIN(4)=0.02361 GO T0 1130
      IF(T*GT*0.1) GO T0 1131
1133 CC T0 1132
      CFVIN(4)=41.6522*T
1134 CC T0 1132
      CFVIN(4)=0.131 GO T0 1133
      IF(T*GT*0.131) GO T0 1133
      CFVIN(4)=0.5839+32.7578*(0.1-T)
1135 CC T0 1132
      CFVIN(4)=0.
1136 CC T0 1132
      CFVIN(4)=0.
C   DRIVE(MCRV) = 0.00
C   CC E M=1,N
C   DRIVE(MCRV) = DRIVE(MDRV)+THA(M)*FLAG(M,MCRV)
C   S DRIVE(MCRV) = DRVIN(MDRV)+DRIVE(MCRV)
C

```

EXEC FOR TCLG, REGION • GO=200K

//FCRT•SYNDD*****

COMPUTER AUTOMATED DESIGN OF SYSTEMS
(CADS)

BY
LARRY PAUL VINES
LIEUTENANT USN

1 APRIL 76

THIS PROGRAM WILL SIMULATE/OPTIMIZE CONTROL SYSTEMS AND CIRCUITS.
THE INPUT DATA WHICH IS TO BE OPTIMIZED TRANSFERRED ARECTIONS WHICH
ARE LOCATED ONLY IN THE SYSTEM. THESE FUNCTIONS ARE CONNECTED DIFFERENTLY
TO EACH OTHER. THESE FUNCTIONS COULD BE CONNECTED IN A RANDOM ARBITRARY
FASHION FROM THE DATA CARD PROVIDED. THESE FUNCTIONS COULD BE
TRANSFERRED BLOCK BY BLOCK. MOST CONTROL SYSTEMS WHICH WILL
ACEQUATE TO A SIDE VARIETY OF CONTROL SYSTEMS CAN EASILY
ALSO WORK WITH THE KNOWN SYSTEM PARAMETERS TO BE SET BY THE
USER. ALL UNKNOWN OR ADJUSTABLE PARAMETERS TO ACHIEVE THE DESIRED RESPONSE.
INITIALIZATION ROUTINE (BOXPLX) A GRAPHICAL OUTPUT OF THE DESIRED RESPONSE AND ACTUAL SYSTEM
RESPONSE IS THEN PROVIDED.

DESCRIPTION OF PARAMETERS

NRNS = NUMBER OF RUNS TO BE MADE. NRUNS = 1 WHEN OPTIMIZING.

NV = NUMBER OF VARIABLES BOXPLX WILL SET.

NAV = NUMBER OF ALX VARIABLES DEFINED.

LEAF = 0 COMPUTES STANDARD SECOND ORDER STEF RESPONSE FOR
DATA CURVE
= 1 SKIPS SECOND ORDER DATA EQUATION

NFR = FREQUENCY OF OUTPUT FROM BOXPLX FOR DIAGNOSTIC PURPOSES.
(NPR = 25, 50, 100 IS RECOMMENDED)

```

* * * * * NTA = NUMBER OF TRAILS ALLOWED BY BOXPLX FCR A SOLUTION.
* * * * * IFLCT = OPTIONAL PRINTER PLCT CF SCULATION. = 0 NC PLOT.
* * * * * ICRAW = OPTIONAL CALCOMP GRAPH CF SCULATION.
* * * * * ICPLOT = OPTIONAL PLOT = 0 NC PLOT
* * * * * ** C ONLY ONE PLOT OPTION MAY BE USED AT A TIME. IFCAW REQUIRES
* * * * * A / EXEC CLGP CONTROL CARD AND 230K REGION.

* * * * * T = TIME INITIAL CONDITION. MUST BE ZERO. IS RECOMMENDED.
* * * * * CT = STEP SIZE FOR INTEGRATION. TF/1000. IS RECOMMENDED.
* * * * * TF = FINAL PROBLEM TIME.

* * * * * CELTA = CAMPING FACTOR
* * * * * WNA = NATURAL FREQUENCY
* * * * * BETTA = GAIN FACTOR
* * * * * FCR STANDARD 2ND ORDER DATA CURVE

* * * * * XS(I) = STARTING GUESS
* * * * * XL(I) = UPPER BOUND FOR VARIABLE PARAMETERS TO BE SET BY
* * * * * XL(I) = LOWER BOUND THE MINIMIZATION ROUTINE
* * * * * N = NUMBER OF TRANSFER FUNCTION BLOCKS CONNECTED.
* * * * * ISET = OUTPUT VARIABLE TO BE OPTIMIZED/PLOTTED
* * * * * CELTA = DEFAULT VARIABLE PLOTTED IS HIGHEST NUMBERED NODE VAR.

* * * * * DESCRIPTION OF BLOCK TRANSFER FUNCTIONS

* * * * * ELKCCD=EEVV G P/DELTA/UL/REF 2/W/L/BLND
* * * * * CC = NUMBER OF BLOCK IN SYSTEM CONFIGURATION (IE. ELK NUMBER 1)
* * * * * C = TYPE OF TRANSFER FUNCTION BLOCK.
* * * * * EF = INPUT NODE NUMBER
* * * * * VV = OUTPUT NODE NUMBER
* * * * * E = GAIN OF BLOCK
* * * * * F = FCLE OF BLOCK TRANSFER FUNCTION
* * * * * CELTA = CAMPING FACTOR FOR COMPLEX TRANSFER BLOCK (TYPE 4)

```

```

*** LL = UPPER LIMIT FOR LIMIT BLOCK (TYPE 5)
*** REF = REFERENCE FOR DEAD ZONE BLOCK (TYPE 6)
*** Z = ZERO FOR BLOCK TRANSFER FUNCTION
*** WN = NATURAL FREQUENCY FOR COMPLEX BLOCK (TYPE 4)
*** LL = LOWER LIMIT FOR LIMIT BLOCK (TYPE 5)
*** ECIND = MAGNITUDE OF DEAD ZONE (TYPE 6)
*** C(1) = AUXILIARY VARIABLES (USED IN BOXPLX)
*** CFVIN(I) = EXTERNAL FORCING INPUTS

```

DATA CARD FORMATS

```

CARD 1 NRUNS (II)
CARD 2 NV,NAV,LEAP,NPR,NTA,IPRCT,ICRAW (7I5)
CARD 3 T,DT,TF (3F10.5)
CARD 4 DELTA, WN, BETA (3F10.5)
STARTING GUESS AND LIMIT CARDS (USED ONLY WHEN OPTIMIZING)
XS(I) N(E15.7,5X) N MAX = 25
XU(I)
XL(I)

CARD 5 N,ISET (12,2X,12)
CARD 6 BLK(I2,I1=I2,I2,8X,2E20.7)
AS MANY CARDS AS THERE ARE BLOCKS CONNECTED
..... TWO TITLE CARDS ARE REQUIRED IF CALCNP PLCTS
..... ARE TO BE OUTPUT (CC1 1-4E)

```

```

DIMENSION XS(25), XL(25), XU(25)
DIMENSION X(2), XDT(2)

```

```

950
960
970
980
990
1000
1010
1020
1030
1040
1050
1060
1070
1080
1090
1100
1110
1120
1130
1140
1150
1160
1170
1180
1190
1200
1201
1202
1203
1204
1205
1206
1207
1208
1209
1210
1211
1212
1213
1214
1215
1216
1217
1218
1219
1220
1221
1222
1223
1224
1225
1226
1227
1228
1229
1230
1231
1232
1233
1234
1235
1236
1237

```

```

C1 VEN SICN THAOUT (3001) , XDATA(3001)
REAL *8 XDATA
REAL *8 THAOUT
REAL *8 X, XDOT, T, TF, CT
COMMON T, DT, TF, THAOUT, XDATA, M3, ICCNT, NEQ, ISKIP, ITF
EXFLX. THE MULTIPLE RUN OPTION SHOULD NOT BE USED WHEN EMPLOYING
TIME BECOMES EXCESSIVE. USE ONLY FOR PLANT - DATA RUNS

READ (5,12) NRUNS
READ/WRITE CONTROL DATA

CC C111 I RUN=1,NRUNS
READ (5,13) NV,NAV,LEAP,NPRINT,IPLOT,IDRAW
WRITE (6,14) NV,NAV,LEAP,NPRINT,IPLOT,IDRAW
READ (5,15) T,DT,TF
WRITE (6,16) T,DT,TF
READ (5,17) DELTA,W,BETA
WRITE (6,17) DELTA,W,BETA

READ/WRITE SEARCH BOUNDS IF OPTIMIZING
IF (NV .EQ. 0) GO TO 1
SET LIMITS
STARTING GUESS
READ (5,18) (XS(I),I=1,NV)
LEFFER BCUNE
READ (5,18) (XU(I),I=1,NV)
LCWER BCUNC
READ (5,18) (XL(I),I=1,NV)
WRITE (6,15) (XS(I),I=1,NV)
WRITE (6,16) (XU(I),I=1,NV)
WRITE (6,17) (XL(I),I=1,NV)
WRITE (6,18) (XL(I),I=1,NV)
WRITE (6,19) (XL(I),I=1,NV)
WRITE (6,20) (XL(I),I=1,NV)
WRITE (6,21) (XS(I),I=1,NV)
WRITE (6,22) (XU(I),I=1,NV)
WRITE (6,23) (XL(I),I=1,NV)
WRITE (6,24) (XL(I),I=1,NV)
WRITE (6,25) (XL(I),I=1,NV)
1 CCNTINUE
1 CF = TF/DT
1 IF = ICF
1 IF (ICP .GT. 4500) IDP=4500

```

PLCT EVERY FIFTH DATA POINT

NNFLT = 0.2*IDP

R = 1./2.

IF = 0
ISKIP = 0

CALCULATE STANDARD SECOND ORDER SYSTEM RESPONSE FOR BOXFLS DATA

```
I[DATA = 0
X(1) = 0.00
C C NCT COMPUTE DATA CURVE IF LEAF = 1
IF (LEAF.EQ.1) GO TO 5
X(2) = 0.00
N1 = 0
XCC(T(1)) = X(2)
2 XCC(T(2)) = -2.*DELTA*WN*X(2)-WN**2*X(1)+BETA
S = RKLCEQ(2,X,XDOT,T,DT,NT)
IF (S-1) 2,4
= WRITE(6,23)
= STCP
C 4 I[DATA = I[DATA+1
X(I[DATA) = X(1)
C C TEST FOR END OF COMPUTATION
IF (T-TF) 2,5
5 NCH HAVE STANDARD VALUES
CONTINUE WITH PROG
SET DATA CURVE = 0. IF NOT PLOTTING
IF (LEAF.EQ.0) GO TO 7
C C C C
6 I=14500
I[DATA = I[DATA+1
T= T+DT
X(I[DATA) = X(1)
IF (T-TF) 6,7,7
7 CONTINUE
C C CALL PLANT TO SIMULATE THE SYSTEM
```

```

C   7 IF (NV.EC.0) PL = PLANT(1.)
C   C IF OPTIMIZING, CALL BCXPLX AND WRITE OPTIMIZED VALUES
C   CALL BOXPLX (NV,NAV,NPR,NTA,R,XS,IP,XU,XL,YMN,IER)
C   WRITE (6,24) (XS(I),I=1,NV)
C   WRITE (6,25) YMN,IER
C
C   FCT SYSTEM RESPONSE
C
C   8 IF (IFLCT.EC.0) GO TO 5
C   WRITE (6,26)
C   CALL FPFL (XDATA,THAOUT,DT,NPLT,IP)
C   GOTO 11
C
C   5 IF (ICRAN.EQ.0) GO TO 10
C   CALL PIC (XDATA,THACUT,DT,NPLT,IP)
C   GOTO 11
C
C   10 WRITE (6,27) IRUN
C
C   11 WRITE (6,28) IRUN
C
C   12 STCP
C
C   13 FCRNAT (715)
C   14 FCRNAT (//,2X,'NV = ',15,2X,'NAV = ',15,2X,'LEAP = ',11,2X,'NFR =
C   15 FCRNAT ('NTA = ',15)
C   16 FCRNAT ('/2X*T(0)=','F7.3',2X,'CT=','F10.5',2X,'TF=','F10.5')
C   17 FCRNAT ('/2X*DELT=','F10.5',2X,'HN=','F10.5',2X,'BETA=','F10.5')
C   18 FCRNAT (4,15,75X)
C   19 FCRNAT (//,2X:'STARTING GUESS')
C   20 FCRNAT (//,2X,'5(E15.75X))')
C
C   21 FCRNAT (//,2X:'UPPER BCUNDS')
C   22 FCRNAT (//,2X:'LOWER BCUNDS')
C   23 FCRNAT (5X,'ID NCT DO STANDARD EGN PROPERLY STOPED INT')
C   24 FCRNAT (//,2X,'THE XS(I) ARE ','5(E15.75X)')
C   25 FCRNAT (//,2X,'FUNCTION VALLE IS ','E15.75X')
C   26 FCRNAT ('-1')
C   27 FCRNAT ('/,* NO PLOTS, CALLED FCR * *')
C   28 FCRNAT (//,2X,'*** RUN ,11,CCNFLETE ***')
C
C   END
C
C   KE EVALUATES IMPLICIT CONSTRAINTS ON BOXPLX VARIABLES
C   FLACTIGN KE (C)
C   CINNSIGN C (25)
C

```

C NC IMPLICIT CONSTRAINTS

```
      KEE = 0
      RETURN
END

C   COMPUTES THE ERRCR FUNCTION (PERFORMANCE INDEX) FOR BOXPLX
FUNCTION FFE(C)
DIMENSION THAOUT(3001), XDATA(3001), C(25)
REAL *8 XDATA, THAOUT, ET, T, DIFF, PI
C
C NNON T, DT, TF, THAOUT, XDATA, M3, ICNT, NEQ, ISKIP, ITF
T=ACUT(1)=0.D0
C1FF=0.D0
FI = PLANT(C)
PL = PLANT(C)

CC 1 I=1,ITF
C1FF=XDATA(I)-THAOUT(I)
1 FI = PI+DIFF*I*2

C   VALUE OF PI
FFE=PI
RETURN
END

C   FUNCTION PLANT SIMULATES THE SYSTEM
FUNCTION PLANT(C)
DIMENSION G(25), P(25), Z(25), DRIVE(25), I(25) ON
1C(25), THAOUT(25), CMGDC(25), CRVIN(25), IC(25), IE(25)
2NF(25), TIR(25), IV(25), X2DOT(25), THAOUT(3001), XDATA(300
1) C(25)
REAL #8 T, ACUT
REAL *8 XDATA
REAL *8 TA, THADOT, T, DT, DRIVE, CMG, CMGDC, CRVIN, TF
REAL *8 I, T2
REAL *8 X2, X2DOT
C
C NNON T, DT, TF, THAOUT, XDATA, M3, ICNT, NEQ, ISKIP, ITF
C
C   FOR OPTIMIZATION RUNS INHIBIT READ STATEMENTS AFTER READING
1 IF (ISKIP-1) 1,5,5
1 ISKIP=2
1 REAL (5,24) N, ISET
C   INITIALIZE COUNTERS
```

```

ICLT = 0
IVLT = 0
ID = 0.5D0*H1
N11 = 0
N15 = 0
TCK = 2*N

```

```

*** READ INPUT DATA ***
COMPLEX BLOCK TYPE 44 READS DELTA IN FROM P FIELD AND
WANIS READ IN Z FIELD
SATURATION BLOCK TYPE 55 READS PLLS SAT LEVEL IN FRCM P FIELD AND
SEGMENT LEVEL FROM 2 FIELD
ZONE BLOCK TYPE 6 READS CONTROL REF FROM P FIELD AND
ZONE BOUND FRCM 2 FIELD

```

```

EE 2 1=1 N
READ (5,25) IC(I), ID(I), IE(I), IV(I), G(I), P(I), Z(I)
SET THACUT = OUTPUT OF LAST BLOCK
IF ((IV(I)-IVOUT).LE.0) GO TO 2
IF (IC(I)-IC(I)) .EQ. 1) N11=N11+1
IF (IC(I)-IC(I)).EQ. 5) N55=N55+1
IF (IC(I)-IC(I)).EQ. 6) N66=N66+1
2

```

```

EE 2 1=1 N
WRITE (6,26) IC(I), ID(I), IE(I), IV(I), G(I), P(I), Z(I)

SET THACUT = SPECIFIED THETA, IF ANY
IF (ISET.NE.0) IOUT=ISET
WRITE (6,27) IOUT
N11 = 4*N11
N55 = 4*N55
N66 = 4*N66
*** SHOULD NOW HAVE INPUT DATA AVAILABLE IN C,D,E,V ***
NEC = N-1
*** SCAN FOR INPUTS ***

```

```

CCCCCCCCCCCC CCCC CCCCC CCCCC CCCCC

```

CONNECT UP SYSTEM BY SETTING FLAG=1. IF BLOCKS ARE CONNECTED

```
CC 4 J=1,N  
CC 4 K=1,N  
FLAG(K,J)=0.0  
IF (IV(K).EQ.IE(J)) FLAG(K,J)=1.0  
  
***NOW MUST TAKE TYPE OF BLK AND GO TO EGS FOR SOLUTION***  
CLEARING OUT REGISTERS AND INITIALIZING COUNTERS  
  
= FF6 IC(LR)=1,N  
= FF7 ACOT(IC(LR))=0.00  
= FF8 CLR(IC(LR))=0.00  
= FF9 GELOT(IC(LR))=0.00  
= FF10 FVIN(IC(LR))=0.00  
= FF11 XZ(IC(LR))=0.00  
= FF12 XCOT(IC(LR))=0.00  
  
T = C.000  
NFS CONTROL ENTRY POINT IN INTEGRATION SUBROUTINES(RKLDCE'S)  
NFS = 1  
NFS = 1  
NFS = 1  
  
NFS CONTROLS WHICH BLOCK EQUATION IS BEING SOLVED  
N2 = 0  
ICNT IS USED TO CONTROL PROGRAM FLOW  
ICNT = 0  
WAIT IS USED TO CONTROL TIME. TIME IS STEPPED EVERY FIRST AND  
THIRD PASS THRU INTEGRATION ROUTINES  
WAIT = 0  
LAST'S CONTROL PROGRAM DATA AND PROGRAM EXIT
```

```

11700
11800
11900
12000
12100
12200
12300
12400
12500
12600
12700
12800
12900
13000
13100
13200
13300
13400
13500
13600
13700
13800
13900
14000
14100
14200
14300
14400
14500
14600
14700
14800
14900
15000
15100
15200
15300
15400
15500
15600
15700
15800
15900
16000
16100
16200

SPECIFY ANY PARAMETERS TO BE OPTIMIZED
EC. P(1)=C(2), Z(1)=C(1),
*** INSERT NV VARIABLE SPECIFICATIONS HERE ***
C(2)=C(1)

***SET DRIVES FOR INPUTS***
CFVIN(1)=1.

7 EC S MCRV=1,N
CFVIN(1)*S GO HERE IF FUNCTIONS CF TIME
DRIVE(MCRV) = 0.D0

CC 8 N=1,N
8 DRIVE(MCRV) = DRIVE(MCRV)+T*A(M)*FLAG(M,MCRV)
S DRIVE(MCRV) = DRVIN(MCRV)+DRIVE(MCRV)

10 N2 = N3+1

FICK TYPE EQN TO SOLVE
IF ((WAIT*EQ*0) T = T+H2
IF ((IC(N2)*EQ*1) GC T0 11
IF ((IC(N3)*EQ*2) GC T0 12
IF ((IC(N3)*EQ*3) GC T0 13
IF ((IC(N3)*EQ*4) GC T0 14
IF ((IC(N3)*EQ*5) GC T0 15
IF ((IC(N3)*EQ*6) GC T0 16
WRITE(6,28)
STCP

***START SCLUTION***
TYPE ONE EQUATIONS
SCLUTES THACUT = G*THAIN
11 T^A(N3) = G(M3)*DRIVE(M3)
11 WAIT = IWAIT+1

```

```

LAST = LAST +1
IF ((LAST.EQ.N11).AND.(ICONT.EC.NEQ)) GO TO 21
GC TO 1E

TYPE TWO ECNS
SCLVES THAOUT/THAIN = G/(S + P)
C
12 THACOT(M3) = -P(M3)*THA(M3)+G(M3)*DRIVE(M3)
S = RKLCE2(THA,THADCT,NR2)
IF WAIT = IWAIT+1
IF (S-1.0) 17,18,21

TYPE THREE EQNS
SCLVES THAOUT/THAIN = G*(S + Z)/(S + P)
C
13 CMGDOT(M3) = -P(M3)*OMG(M3)+G(M3)*DRIVE(M3)
S = RKLCE3(OMG,OMGDC,NR3)
THA(M3) = (Z(M3)-F(M3))*OMG(M3)+G(M3)*DRIVE(M3)
IF WAIT = IWAIT+1
IF (S-1.0) 17,18,21

TYPE FOUR EQNS
SCLVES THAOUT/THAIN = G/(S**2 + 2*DELT*A*N*S + WN**2)
C
14 V = CCP LX(P,Z(G,DRIVE,X2,OMG,NR4))
THA(M3) = CMG(M3)
IF WAIT = IWAIT+1
IF (V-1.0) 17,18,21

TYPE FIVE EQNS
SCLVES THAOUT = G*THAIN FOR /G*THAIN/ < SATURATION LIMITS
C
15 THA(M3) = G(M3)*DRIVE(M3)
IF ((THA(M3)*GT.P(M3)) THA(M3)=P(M3))
IF ((THA(M3)*LT.Z(M3)) THA(M3)=Z(M3))
IF WAIT = IWAIT+1
IF (ELAST = 15LAST+1
IF ((LAST.EQ.N55).AND.(ICONT.EC.NEQ))) GO TO 21
GC TO 1E

TYPE SIX ECNS
SCLVES THAOUT = G*THAIN FCR CONTROL REF > BOUND DEAD SPACE
C
16 THA(M3) = G(M3)*DRIVE(M3)
IF = P(M3)
IF ((CAES(THA(IP)).LT.Z(M3)) THA(M3)=0.
IF WAIT = IWAIT+1

```

```

16 LAST = 16LAST.EQ.N66).AND.(ICCNT.EQ.NEQ)) GC TC 21
17 IF(ICTP .EQ. 18)
18 ICCNT = ICCNT+1
19 IF((ICONT-N) 10,19,20
C    CNE PASS HAS BEEN MADE FOR EACH ECH. GO TO NEXT STEP INCREMENT
C
1: NF2 = NF2+1
2: NF3 = NF3+1
3: NF4 = NF4+1
4: NF5 = 0
5: IF((IWAIT.EQ.ICK) IWAIT=0
6: CC TO 7
C
20 WRITE(6,30)
STCP
C
C DATA COLLECTION PCINT. DATA IS RECORDED AT END OF COMPLETE
TIME STEP(DT)
C
21 IT = IT+1
IF(ACT(IT) = THA(IOUT))
TEST FOR END OF RUN
IF((T-TF) .GT. 22,23
RESET COUNTERS FOR NEXT PASS THRU EQUATIONS
C
22 NF2 = 1
NF3 = 1
NF4 = 1
NF5 = 0
ICCNT = 0
LAST = 0
LAST = 0
LAST = 0
CONT = 0
CONT = 0
CONT = 1.
RETURN
C
24 FCBRN((12,2X,12,1X,212,8X,3E20,7)
25 FCBRN((3X,12,11,1X,212,8X,3E20,7)
26 FCBRN((/5H,BLK,12,11,2H=1212;EX,3E20,7)
27 FCBRN((/,2X,THETA,CUT IS THA(,12,1,7)

```

```

2E FCFMAT (40H *** EGN SWITCH CONTROL DID NOT WORK ***)
2S FCFMAT (20H INTEGRATION TROUBLE)
3D FCFMAT (58H ERROR IN INTERGATION. ATTEMPTED TO INTEG. MORE THAN N-
1 EGN)
ENC

```

```

FORTTRAN 4 VERSION OFRUNGE-KUTTA-GILL ROUTINE
X,XDOT,T,DOT, ARE IN DOUBLE PRECISION
NMAX N=25

```

```

FUNCTION RKLDSEQ(N,X,XDOT,T,DT,NT)
DIMENSION X(1),XDOT(1),C(1),C(25),H

```

```

C      NT = NT + 1
CC     TO (1,2,3,4),NT

```

```

1      H1 = DT
      H2 = H1 * 0.5DD0
      H3 = H1 * 2.0DD0

```

```

      C(1) = 1./C(0)
      C(2) = 0.5C(0)

```

```

      T = T + H2
      CC TO 5

```

```

2      A = 0.2528932188134525
CC TO 5

```

```

3      A = 1.7071067811865475
      T = T + H2
      CC TO 5

```

```

4      C(4) = X(1) + H6*XDOT(1) - Q(1)/2.E0
      X(1) = 0
      RKLDSEQ = 2.
      CC TO 6

```

```

5      C(5) = 1./N
      X(1) = C(1) + A*(C(1)*XDOT(1)-Q(1))
      C(2) = H3*A*XDOT(1) + (1./H0 - 3.*C(0)*A)*Q(1)
      RKLDSEQ = 1.

```

```

C      RETURN
ENC

```

```

FORTTRAN 4 VERSION OFRUNGE-KUTTA-GILL ROUTINE

```

2640
10

**X, XCOT, T, DT, ARE IN DOUBLE PRECISION
N=25**

```

C   1  H2 = H1*0.5DD
C   2  H2 = H1*2.0DD
C   3  H2 = H1/6.0DD
C   4  S(M3) = 0.0D0
C   5  A = C*5E0
C   6  GC 10 5

C   7  A = 0.2928932188134525
C   8  GC 10 5

C   9  X(M3) = X(M3)+H6*XDOT(M3)-Q(M3)/Z.DD
C  10 RKLDE3 = 1.EC.NEQ  RKLDE3=2.
C  11 IF (ICONT.EC.NEQ)
C  12   GC 10 6
C  13   X(M3) = X(M3)+A*(ET*XDQT(M3)-Q(M3))
C  14   S(M3) = H3*A*XDQT(M3)+(1.D0-3.D0*A)*Q(M3)
C  15   RKLDE3 = 1.
C  16   RETURN
C  17 END

C   18 FUNCTION COMPLEX
C   19 THIS FUNCTION IS USED TO COMPUTE THE RESPONSE OF A COMPLEX
C   20 TRANSFER FUNCTION (G/(S.*2 + 2*E*k*S + k**2)) OF A COMPLEX
C   21 FUNCTION CCPLEX (P,Z,G,CRIVE,X2,CNG,NR4)
C   22 DIMENSION CMG(1),P(1),Z(1),X2,CNG,NR4
C   23 DIMENSION THADOUT(3001),XDATA(3001)
C   24 REAL *8 CNG,CMDOT,CRIVE,X2,X2DGT,T,DT
C   25 REAL *8 ET,F
C   26 CMNCF,T,DT,TF,THADOUT,XDATA,M3,ICNT,NEQ,ISKIP,ITF
C   27 CMGDOT(M3) = X2(M3)
C   28 SS = RKLDE3(CMG,CMGDOT,NR4)
C   29 X2DCT(M3) = -2.*P(M3)*Z(M3)*X2(M3)-Z(M3)+C(M3)*CRIVE(M3)
C   30 1)
C   31 SSS = RKLDE4(X2,X2DCT,NR4)
C   32 CCLFX = SSS
C   33 RETURN

```

ENC
 C THIS FUNCTION WORKS ONLY WITH COMPLEX ROUTINE
 C

```

FUNCTION RKLDE4 (X,XDOT,NR4)
CIVENSICN X(1) XDDOT(1), XCCT(1), GC(25)
DIVENSICN THAOUT(3001), XDATA(3001)
REAL *8 THACUT, XDATA
REAL *8 X1 XDOT, T, DT, CC, H1, H2, H3, HC
CCVNCN T, DT, TF, THAOUT, XDATA, M3, ICOUNT, NEQ, ISKIP, ITF

C GC TO (1,2,3,4), NR4
1 H1 = CT
H2 = H1*0.5D0
H3 = H1*2.0D0
H4 = H1/6.0D0
GC(M3) = 0.0D0
A = 0.5D0
GC TO 5

C 2 A = 0.28932188134525
C 3 GC TO 5
      A = 1.7071067811865475

C 4 X(M3) = X(M3)+H6*XDOT(M3)-QC(M3)/2.D0
      RKLDE4 = 1.0C.NEQ) RKLDE4=2.
      IF (ICONT.EC.NEQ) RKLDE4=2.
      GC TO 6

C 5 X(M3) = X(M3)+A*(CT*XDDOT(M3)-QC(M3))
      GC(M3) = H3*A*XDDOT(M3)+(1.D0-3.CD4A)*QC(M3)
      RKLDE4 = 1.

C 6 RETURN
ENC

C SLEROUTINE PIC (XDATA,THAOUT,DT,NPPLT,IDF)
C THIS ROUTINE PLOTS THE SYSTEM AND DESIRED RESPONSES IN-OUT EBUFFERS
C REQUIRES APPROXIMATELY 28K FOR STORAGE AND
C CIVENSICN XX(900), YY(500), WW(500)
C DIVENSICN TX(4), TY(4)
C REAL *8 XDATA(501), THAOUT(501), TITLE(112), CT
C REAL *8 LABC/

```

```
REAL *4LABA/'TITLE' ,LABC/' D '
READ (5,2) TITLE
      TITLE IS ON TWO CARDS AND MUST HAVE YOUR ID
      AND GRAPH-TITLE IN COL 1-48.
```

```
T STEP = 5.0*DT
J = 0.
BIGX = 0.
BIGY = 0.
SMAX = 0.
SMLY = 0.

CC   I=1,IIDP,5
J=J+1
XX(J)=T
YY(J)=XDATA(I)
XX(J)=THAOUT(I)
XX(C)=YY(J)
TMAX=WK(J)=AMAX1(XD,TH)
YMIN=AMIN1(XD,TH)
XMAX=AMAX1(BIGX,X)
IF(BIGX>LT,X)BIGX=X
IF(BIGY>LT,YMAX)BIGY=YMAX
IF(SMLY>GT,YMIN)SMLY=YMIN
T=T+STEP
1  CCNTINUE

T X(1) = 0.
T X(2) = 0.
T X(3) = 0.
T X(4) = 0.
T Y(1) = BIGX
T Y(2) = SMLY
T Y(3) = 0.
T Y(4) = 0.

FLCT SYSTEM RESPONSE
SYMBL 'A' IS ACTUAL RESPONSE, SYMBL 'D' IS DESIRED DATA RESPONSE
CALL ERRAW (4, TX,TY,1,1,LABC,TITLE,G,0,0,0,0,0,0,0,0,L)
CALL ERRAW (NPPLT,XX,WW,2,0,LABA,TITLE,0,0,0,0,0,0,0,0,0,L)
FLCT DESIRED RESPONSE
```


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SAGE

CALL BOXPLX (NV,NAV,NPR,NTA,R,XS,IP,XU,XL,YMN,IER)

DESCRIPTION OF PARAMETERS

NV AN INTEGER INPUT DEFINING THE NUMBER OF INDEPENDENT VARIABLES OF THE OBJECTIVE FUNCTION TO BE MINIMIZED.
NOTE: MAXIMUM NV + NAV IS PRESENTLY 50. MAXIMUM NV IS 25. IF THESE LIMITS MUST BE EXCEEDED, PUNCH A SOURCE STATEMENT.

NAV AN INTEGER INPUT DEFINING THE NUMBER OF AUXILIARY VARIABLES THE USER WISHES TO DEFINE FOR HIS OWN CONVENIENCE. IT IS TYPICALLY THE NUMBER OF VARIOUS CONSTRAINTS. IF THIS CONSTRIANT IS NOT USED AS AN AUXILIARY VARIABLE, THE OPTITIONAL OUTPUT FEATURE OF BOXPLEX CAN BE USED TO OBSERVE THE VALUES OF THE CONSTRAINTS AS THE USED ALGORITHM PROGRESSES. IF USED, NAV SHOULD BE EVALUATED IN FUNCTION KEY (DEFINED BELOW). NAV MAY BE ZERO.

NPR INPUT INTEGER CONTROLLING THE FREQUENCY OF OUTPUT DESIRED FOR DIAGNOSTIC PURPOSES. IF NPR = 0, NO OUTPUT WILL BE PRODUCED BY BOXPLEX. OTHERWISE, CURRENT COMPLEXITY OF THEIR CENTERED TRIAL WILL BE COMPUTED AFTER EACH NPR PERMISSIBLE TRIALS. THE NUMBER OF TOTAL TRIALS, NUMBER OF FEASIBLE TRIALS, NUMBER OF CONSTRAINTS, NUMBER OF FUNCTIONS ARE INCLUDED IN THE OUTPUT. ADDITIONALLY, WHEN NPR = GT. 0, THE SAME INFORMATION WILL BE OUTPUT:

- 1) IF THE INITIAL POINT IS NOT FEASIBLE
- 2) AFTER THE FIRST COMPLETE COMPLEXITY GENERATED TRIAL,
- 3) IF A FEASIBLE VERTEX CANNOT BE FOUND AT SOME TRIAL,
- 4) IF THE OBJECTIVE FUNCTION VALUE OF A VERTEX CANNOT BE MADE NO-LARGER-THAN-1.
- 5) IF THE LIMIT ON TRIALS (NTA) IS REACHED AND
- 6) WHEN THE OBJECTIVE FUNCTION HAS BEEN CHANGED FOR 2*NV TRIALS, INDICATING A LOCAL MINIMUM HAS BEEN FOUND.

IF THE USER WISHES TO TRACE THE PROGRESS OF A SOLUTION, A CHOICE OF NPR = 25, 50 OR 100 IS RECOMMENDED.

NTA INTEGER INPUT OF LIMIT ON THE NUMBER OF TRIALS ALLOWED

IN THE CALCULATION. IF THE USER INPUTS DATA LINE 0, A DEFALUT VALUE OF 2000 IS USED WHEN THIS LINE IS REACHED. CONTROL RETURNS TO THE CALLING PROGRAM WITH THE BEST ATTAINED OBJECTIVE FUNCTION VALUE IN YMN, AND THE BEST ATTAINED SOLUTION PCINT IN XS.

R A REAL NUMBER INPUT TO DEFINE THE FIRST RANGE NUMBER USED IN DEVELOPING THE INITIAL COMPLEX OF 2*NV VERTICES. (0. GT. R LT. 1.) IF R IS NOT WITHIN THESE BOUNDS, IT WILL BE REPLACED BY 1./2..

XS INPUT REAL ARRAY DIMENSIONED AT LEAST NV+NAV. THE FIRST NV MUST CONTAIN A FEASIBLE ORIGIN FOR STARTING THE FCN- CALCULATION. THE LAST NAV NEED NOT BE INITIALIZED. RETURN FROM BOXPLX THE FIRST NV ELEMENTS OF THE ARRAY COUNTAIN THE COORDINATE OF THE MINIMUM OBJECTIVE FUNCTION, AND THE REMAINING NAV (NAV - NV) ELEMENTS CONTAIN THE VALUES OF THE CORRESPONDING AUXILIARY VARIABLES.

IP INTEGER INPUT FOR OPTIONAL INTEGER PROGRAMMING. IF IP=1, THE VALUES OF THE INDEPENDENT VARIABLES WILL BE REPLACED WITH INTEGER VALUES (STILL STORED AS REAL*4).

XU A REAL ARRAY DIMENSIONED AT LEAST NV INPUTTING THE UPPER BOUND ON EACH INDEPENDENT VARIABLE? (EACH EXPPLICIT CCN- CONSTRAINT). INPUT VALUES ARE SLIGHTLY ALTERED BY EXPLX.

XL A REAL ARRAY DIMENSIONED AT LEAST NV INPUTTING THE LOWER BOUND ON EACH INDEPENDENT VARIABLE? (EACH EXPPLICIT CCN- CONSTRAINT). INPUT VALUES ARE SLIGHTLY ALTERED BY EXPLX. (EACH EXPPLICIT CCN- VALUES IF NONE ARE GIVEN) AND XL WHICH ARE PRACTICALLY ABOVE OR BELOW THE SPECIFIED SOLUTION. INPUT VALUES ARE SLIGHTLY ALTERED BY BOXFLX.

YMN THIS OUTPUT IS THE VALUE (REAL*4) OF THE OBJECTIVE FUNCTION, CORRESPONDING TO THE SOLUTION POINT OUTPUT IN XS.

IER INTEGER ERROR RETURN TO BE INTERRUPTED FCN RETURN FROM BOXPLX. IER WILL BE ONE OF THE FOLLOWING:

=-1 CANNOT FIND FEASIBLE VERTEX OR RESTART (SEE "METHODS BELOW").
=0 FUNCTION VALUE UNCHANGED FOR N. TRIALS. (WHERE N=6*NV+10) THIS UNFEASIBLE VERTEX DEVELOP A LONGER-TERM PARAMETER.
=1 CANNOT DEVELOP A FEASIBLE VERTEX.
=2 CANNOT REACH (N+1) EXITED.
=3 LIMIT ON TRIALS REACHED. (N+1) EXITED.
NOTE: VALID RESULTS MAY BE RETURNED IN ANY OF THE

ABOVE CASES.

EXAMPLE OF USAGE

THIS EXAMPLE MINIMIZES THE OBJECTIVE FUNCTION SHOWN IN THE EXTERNAL FUNCTION $F(X)$. THERE ARE TWO INDEPENDENT VARIABLES $X(1)$ & $X(2)$ AND TWO CONSTRAINT FUNCTIONS (SEE $X(3)$ & $X(4)$) WHICH ARE EVALUATED AS AUXILIARY VARIABLES $E(X)$.

EINEN STICH X5(4) : X1(2) : X1(2)

```

STARTING GUESS
X(1) = 1.0
X(2) = 0.5
LPERLIMITS(1) = 6.0
LPERLIMITS(2) = 6.0
LCXL(1) = 0.0
LCXL(2) = 0.0

```

```

CALL BCXPLX (NV$NAV,NPRINTA,R$IP,XU,XL,YMN,IER)
WRITE(6,1) ((XS(I),I=1,4)YMN,IER)
1 FORMAT ('//','THE POINT IS LOCATED AT (XS(I)=',I4,E13.7,5X),
11//, ' AND THE FUNCTION VALUE IS ',E13.7,IER = ,I5)
STOP
END

```

```

FUNCTION KE(X)
EVALUATE CONSTRAINTS. SET KE=0 IF NO IMPLICIT CONSTRAINT IS
VIOLATED, OR SET KE=1 IF ANY IMPLICIT CONSTRAINT IS VIOLATED.
CINNENSIK X(4)

```

```

KE = 0
XF(3) = X1 + 1.732051*X2
XF(4) = X1*LT.0 OR X2*(3) .GT. 0.0
X(4) = X1*1.732051-X2

```

```

1 IF (X(4) •GE• 0.) RETURN
1 KE = 1
END

FUNCTION FE(X)
DIMENSION X(4)
THIS IS THE OBJECTIVE FUNCT
FE = -(X(2)**3*(9.-(X(1)-
END

```

NETTUNO

IF AN INITIAL COMPLEX IS ESTABLISHED, THE BASIC COMPUTATION IS INITIATED. THESE INSTRUCTIONS FINE THE CURRENT VERTEXES, WHICH ARE THE CORRESPONDING VERTEXES. THE LARGE STATIONARY VERTICES ARE REPLACED BY THE VECTORS OF ALL THE VERTICES. THE OBJECTIVE FUNCTION IS COMPUTED AS A VECTOR IN- SPACES, ITS OVER-REFLECTION IS OBTAINED BY THE FACTOR 1/3, AND THE LENGTH OF THE VECTOR IS INCREASED. THE VERTICES ARE THEN RELOCATED, AND THE PROCESS IS REPEATED UNTIL THE VERTICES ARE NO LONGER CHANGED.

WHEN AN OVER-REFLECTION IS NOT FEASIBLE CR REMAINS WORST, IT IS CONSIDERED NOT-PERMISSIBLE AND IS DISPLACED HALFWAY

THE CENTROID AFTER FIFTH ATTEMPT IS MADE BY REFLECTING THE PRESENT POSITION OF THE VERTEX, AND OVER-REFLECTING THE CURRENT POSITION. THIS PROCESS IS REPEATED UNTIL THE POSITION IS FEASIBLE. A RESTART FOR A RESTART IS ALSO MADE WITH NO SIGNIFICANT IMPROVEMENT.

IT IS RECOMMENDED THAT THE USER READ THE REFERENCE FOR FURTHER USEFUL INFORMATION. IT SHOULD BE NOTED THAT THE ALGORITHM DEFINED THERE HAS BEEN ALTERED TO FIND THE CONSTRAINED MINIMUM, RATHER THAN THE MAXIMUM.

FENARKS

NOTE: NO NON-LINEAR PROGRAMMING ALGORITHM CAN GUARANTEE THAT THE ANSWER FOUND IS THE GLOBAL MINIMUM RATHER THAN JUST A LOCAL MINIMUM. HOWEVER, ACCORDING TO REF², THE COMPLEX NETWORK HAS AN ADVANTAGE IN THAT IT TENDS TO FIND THE GLOBAL MINIMUM MORE FREQUENTLY THAN MANY OTHER NON-LINEAR PROGRAMMING ALGORITHMS.

IT SHOULD BE NOTED THAT THE AUXILIARY VARIABLE CAN ALSO BE USED TO DEAL WITH PRECISELY CONSTRAINED CONSTRAINTS. ANY EQUALITY CONSTRAINT INVOLVED IN THE SET OF INDEPENDENT VARIABLES IS USUALLY INVOLVED IN AN INDEPENDENT VARIABLE WHICH IS NOT TRULY CONSTRAINED. THE GENERAL RULE IS THAT A GIVEN VARIABLE CAN ACCESSES ONE OR MORE OF THE SET OF NAV AUXILIARY VARIABLES. THE GIVING OF THE INDEPENDENT VARIABLE CAN RESTRICT THE NUMBER OF THE SET OF NAV AUXILIARY VARIABLES WHICH CAN ACCESSES IT.

ROUTINES AND FUNCTIONS REQUIRED

SUBROUTINE 'BOUT' AND FUNCTION 'FBV' ARE INTEGRAL PARTS OF THE COMPLEX PACKAGE.

THE SECOND FUNCTION THE USER MUST PROVIDE EVALUATES THE OBJECTIVE FUNCTION. IT IS CALLED $FE(x)$ AS SPECIFIED IN THE EXAM-
PLE ABOVE AND FE MUST BE SET TO THE VALUE OF THE OBJECTIVE
FUNCTION CORRESPONDING TO CURRENT VALUES OF THE NV INDEPENDENCE
VARIABLES IN ARRAY x .

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EFGRAMMER

R.R. HILLEARY 1/1966
REVISED FOR SYSTEM 360 4/1967
CORRECTED 1/1965
REVISED/EXTENDED BY L.NOLAN/F.HILLEARY 2/1975

```
SLEEPGUTINE BOXPLX (NV,NAV,NPR,NTZ,RZ,XS,IF,EU,BL,YM%,IER)
DIMENSION V(50,50), FUN(50), SUM(25), CEN(25), XS(NV), EU(NV), BL(NV)
```

$5 \cdot 10^{-6}$

1

106

```

C      N1 = 0          TOTAL VARS, EXPLICIT PLUS IMPLICIT
C      NFT = 0          CURRENT TRIAL NC.
C      NFTS = 0          CURRENT NO. OF PERMISSIBLE TRIALS
C      NFTS = 0          CURRENT NO. OF TIMES F HAS BEEN ALMOST UNCHANGED
C      C      CHECK FEASIBILITY OF START POINT
C
C      CC 4  I=1:NV
C      VT = XS(I)
C      IF (BL(I)*LE.VT) GO TO 1
C      I = -1
C      VT = BL(I)
C      CC TC 2
C      IF (EU(I)*GE.VT) GO TO 2
C      I = I
C      VT = EU(I)
C      IF (NPR.GT.0) WRITE (6,49) I
C      2  VT(I) = VT
C      CEN(I) = VT
C      IF (IP.EQ.1) GO TO 4
C      BL(I) = BL(I)+AMAX1(EP,EP*AES(BL(I)))
C      BL(I) = BL(I)-AMAX1(EP,EP*AES(BL(I)))
C      SLM(I) = VT
C
C      NCE = 1          NUMBER OF CONSTRAINT EVALUATIONS
C      I = 1
C      IF (KE(V(1,1).EQ.0) GO TO 5
C      IF (NPR.LE.0) GO TO 12
C      WRITE(6,50)
C      GE TO 12
C      ENFE = 1
C
C      C      NUMBER OF VERTICES (K) = 2 TIMES NC. OF VARIABLES.
C      K = 2*NV
C      C      NUMBER OF DISPLACEMENTS ALLOWED.
C      KLIN = 5*NV+10

```

C NUMBER OF CONSECUTIVE TRIALS WITH UNCHANGED FE TC TERMINATE.

ACT = NLIM+NV
ALPHA = 1.2
FK = K
FKV = FK-1
BETA = ALPHA+1.

BXFX3560
BXFX3580
BXFX3590
BXFX3600
BXFX3610
BXFX3620
BXFX3630
BXFX3640
BXFX3650
BXFX3660
BXFX3670
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BXFX3950
BXFX3960
BXFX3970
BXFX3980
BXFX3990
BXFX4000
BXFX4010
BXFX4020
BXFX4030

C INSURE SEED OF RANDCM NUMBER GENERATOR IS CCC.

ICF = R*1.E7
IF (MOD(IQR,2).EQ.0) ICR=IQR+101

C FUN(1) = FE(V(1,1), UP INITIAL VERTICES

YLN = FUN(1)
FLN = 1.
FLNGLD = FUN(1)

CC 15 I=2,K

LINT = 0

7 LINT = LINT+1
LINT = 0

C EN CALCULATION IF FEASIBLE CENTROID CANNOT BE FOUND.
IF (LINT.GE.NLIM) GO TO 11

CC E J=1,NV

C RANGE NUMBER GENERATOR (RANGU)

ICR = ICR*65535
IF (ICR.LT.0) IQR = IQR+2147483647+1

RCX = ICR
RCX = RCX*4656613E-9

V(J,I) = BL(J)+RQX*(BL(J)-BL(V(J,I))
IF (IP.EQ.1) V(J,I)=AINT((V(J,I)+.5))

8 CONTINUE

CC 10 L=1:NIN

NCE = NCE+1
IF (KE(V(1,1)).EQ.0) GO TO 13

CC S J=1:NV

YI = *5*(V(J,1)+CEN(J))
IF (IP.EQ.1) VT = AINT(VT+.5)

V(J,I) = VT

S CONTINUE

10 CONTINUE

```

C 11 IF(E(1).NE.0) GO TO 12
C   WRITE(*,11) I
C   CALL BCUT(NT,NPT,NFE,NCE,NV,NVT,V,I,FUN,CEN,I)
C 12 IER = -1
C   EC TO 4 E

C 13 CC 14 J=1 NV
C   SLM(J) = SUM(J)/FI
C 14 CEN(J) = SLM(J)/FI

C TRY TO ASSURE FEASIBLE CENTROID FOR STARTING.
C   NCE = NCE+1
C   IF (KE(CEN).NE.0) GO TO 7
C   NFE = NFE+1
C   FUN(I) = FE(V(1,I))
C 15 CONTINUE

C END CF LOOP SETTING CF INITIAL COMPLEX.
C   IF (NPROLE.0) GO TO 17
C   CALL BOLT(NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,CEN,0)
C   FIND THE WORST VERTEX, THE 'J' TH.
C   J = 1

C CC 16 I=2 K
C   IF (FUN(J).GE.FUN(I)) GC TO 16
C   J = I
C 16 CONTINUE

C EASIC LCCF. ELIMINATE EACH WORST VERTEX IN TURN. IT MUST BECOME
C AC LONGER WORST, NOT MERELY IMPROVED. FIND NEXT-TO-WORST VERTEX,
C THE 'JN' TH ONE.
C   JN = 1
C   IF (J.EC.1) JN = 2
C 17 JN = 1

C CC 18 I=1 K
C   IF (I.EC.J) GC TO 18
C   IF (FUN(JN).GE.FUN(I)) GO TO 18
C   JN = I
C 18 CONTINUE

C   LIMIT = NUMBER OF MOVES DURING THIS TRIAL TOWARD THE CENTRIC
C   DEL = 70 FUNCTION VALUE.
C   LIMIT = 1
C   COMPLETE CENTROID AND COVER REFLECT WORST VERTEX.

```



```

GC TO 42
26 NFE = NFE+1
      FTRY = FE(V(1,J))

C TEST TO SEE IF FUNCTION VALUE HAS ACT CHANGED.
C AFC = ABS(FUNTRY-FUNOLD)
C AVX = AMAX(ABS(EP*FUNOLD),EP)

C ACTIVATE THE FOLLOWING TWO STATEMENTS FOR DIAGNOSTIC PURPOSES ONLY.
C
C      WRITE(6,55) J,AFO,AMX,FUNTRY,FUNOLD,FUN(J),FUN(N),NTFS,K
C 55 FCFNAUT(1X,13.6E15.7,215)
C      IF(AFO-NTFS+1) GO TO 27
C      NTFS = NTFS+1
C      IF(NTFS.LT.NCT) GO TO 28
C      IER = 0
C      IF(INP.LE.0) GO TO 42
C      WRITE(6,53) K
C      GC TO 42
C 27 NTFS = 0

C IS THE NEW VERTEX NO LONGER WORST?
C 28 IF(FUNTRY.LT.FUN(JN)) GO TO 34

C TRIAL VERTEX IS STILL WORST; ADJUST TOWARD CENTROID THROUGH THE
C EVERY KTH TIME, OVER-REFLECT THE OFFENDING VERTEX
C EEST VERTEX
C LINT = LINT+1
C IF(MCC(CLINT,KV).NE.0) GO TO 30
C CALL FBV(K,FUN,M)
C
C 29 I=1,IV
C     VT = BEITA*(V(I,M))-ALPHA*V(I,J)
C     IF((IP.EQ.1) .AND. VT = AINT(VT+.5))
C     V(I,J) = AMAX(VT,BU(I)),BL(I))
C
C GC TO 32
C
C 30 CC = 1 I=1,IV
C     VT = 5*(CEN(I)+V(I,J))
C     IF(IP.EQ.1) VT = AINT(VT+.5)
C     V(I,J) = VT
C 31 CONTINUE
C
C 32 IF(LINT.LT.NLIM) GC TO 33
C
C CANNOT MAKE THE JTH VERTEX NO LONGER WORST BY DISPLACING TOWARD

```

C THE CENTROID OR BY OVER-REFLECTING THRU THE BEST VERTEX.
 1 IF $\frac{I}{N} = \frac{2}{2}$ WRITE (6,52) NT,J
 2 IF $\frac{I}{N} = \frac{4}{2}$ WRITE (6,52) NT,J
 3 IF $\frac{I}{N} = \frac{NT+1}{TC}$
 C SUCCESS: WE HAVE A REPLACEMENT FOR VERTEX J.
 24 FUN(J) = FLNTRY
 FUN(LC) = FLNTRY
 NFT = NFT+1
 C EVERY 100TH PERMISSIBLE TRIAL, RECOMPUTE CENTROID SUMMATION TC
 /VCIC CREEPING ERROR
 4 IF (MC(MCC(NPT,1000).NE.0)) GO TC 37
 C
 CC 26 I=1 NV
 SUM(I) = 0.
 C CC 25 N=1 K
 SUM(I) = SUM(I)+V(I,N)
 C CEN(I) = SUM(I)/FK
 C CENTINUE
 C LC = 0
 GC TO 35
 C CC 28 I=1 NV
 SUM(I) = SUM(I)+V(I,J)
 C LC = J
 C CC 29 IF (NPR*LE.0) GO TC 40
 IF (MC(NFT,NPR).NE.0) GO TO 40
 C CALL BCUT (NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,CEN,LC)
 C HAS THE MAX. NUMBER OF TRIALS BEEN REACHED WITH CUT CONVERGENCE?
 4C IF (NT.GT.NTA) GO TO 41
 C NEXT-TC-WCRST VERTEX NOW BECOMES WCRST.
 J = JN
 CC TC 17
 41 IF (NPR*GT.0) WRITE (6,54)

```

C COLLECT CR POINT FOR ALL ENDINGS• FEASIBLE VERTEX•
C CANNOT DEVELOP A NO-LONGER-WORST VERTEX. IER = 1
C FUNCTION VALUE UNCHANGED FOR K TRIALS. IER = 0
C LIMIT ON TRIALS REACHED. IER = 2
C CANNOT FIND FEASIBLE VERTEX AT START. IER = -1
C
C FIND BEST VERTEX•
CALL FBV (K,FUN,M)
IF (IER.GE.3) GO TO 44
C
C RESTART IF THIS IS THE FIRST TRY.
CR IF THIS IS THE FIRST TRY.
IF (NPR.LE.0) GO TO 42
WRITE (*,55) (M,YMN,FUN(M))
55 FORMAT (6X,M,YMN,FUN(M))
42 IF (FUN(CM).GE.YMN) GO TO 47
IF (ABS(FUN(N)-YMN).LE.AMAX1(EP,EF*YMN)) GO TO 47
C GIVE IT ANOTHER TRY UNLESS LIMIT ON TRIALS REACHED.
44 FUN = FUN(CM)
FLN(I) = FLN(M)
C
45 IF (I = 1, NV
CEH(I) = V(I,M)
SN(I) = V(I,M)
V(I,1) = V(I,M)
C
46 IF (I = 1, NVT
XS(I) = V(I,M)
C
47 IF (IER.LT.3) GO TO 6
IF (NPR.LE.0) GO TO 48
CALL BCUT(NT,NPT,NFE,NCE,NV,NVT,V,K,FUN,V(1,M),-1)
C
48 RETURN
C
49 FORMAT (50H INDEX AND DIRECTION CF OUTLYING VARIABLE AT START 15)
50 FORMAT (50H IMPLICIT CONSTRAINT VIOLATED AT START CEAD END )
51 FORMAT (0CANNOT FIND FEASIBLE!,14,TH VERTEX OR CENTEROID AT START )
52 10 FORMAT (10H OR WORST TRIAL 14 54H CANNOT FIND FEASIBLE VERTEX WHICH IS N8XPX63400
53 10 LNCER (40H LIMITATION HAS BEEN ALREADY UNCHANGED FOR 15,7+ TRIALS)
54 FCNAT (40H TRIAL 14 15X, REST VERTEX WHICH IS N8XPX63800
55 FCNAT (27H LIMITATION EXCEEDED. ) E8XPX63500
56 FCNAT (0H BEST VERTEX IS NO.,13, CLD MIN WAS 0 ,E15.7,
57 10 NEW MIN IS E15.7)
58 FCNAT (0MIN OBJECTIVE FUNCTION IS 0 ,E15.7)

```

```

      ENE
      SELET RECOUTINE FBV (K, FUN, N)
      CIMSICHINE FUN(50)
      N = 1
      1  CCONTINUE
      CRETURN
      ENEC URCTINE BOUT (NT,NPT,NFE,NCE,NV,NVT,V,K,FN,C,IK)
      CIMSICHINE V(50,50), FN(50), C(25)
      WRITE (C,4) NT,NPT,NFE,NCE
      CCC 1 I=1,K
      WRITE (C,5) FN(I),(V(J,I)), J=1,NV)
      IF (NVT.LE.NV) GO TC 1
      NVF = NV+1
      WRITE (C,6) (V(J,I)), J=NVP,NVT)
      1  CCONTINUE
      CIF (IK.NE.0) GO TO 2
      CWRITE (6,7) (C(I),I=1,NV)
      RETRN
      2  IF (IK.GE.0) GO TO 2
      WRITE (6,8) (C(I),I=1,NV)
      RETRN
      2  WRITE (6,9) IK, (C(I),I=1,NV)
      RETRN
      C4  FCRMAT ('ONG.TOTAL TRIALS = '15,4X,154X, FEASIBLE TRIALS = '154X, CONSTRAINTS = '154X, EVALUATION = '154X, INDEPENDENT VARIABLES = '154X, DEPENDENT VARIABLES = '154X, FUNCTION VALUE = '6X, FUNCTION CONSTRAINTS = '6X, IMPLICIT CONSTRAINTS = '6X, CENTROR ('1H,E16.7'2X,7E14.7)/(21X,7E14.7) )
      2  CFCRMAT ('21X,7E14.7)
      2  CFCRMAT ('10FCENTROID 11X,7E14.7/(21X,7E14.7))
      2  CFCRMAT ('0 BESTVERTEX,7X,7E14.7/(21X,7E14.7))
      2  CFCRMAT ('OCENTROID LESS VX,12,2X,7E14.7/(21X,7E14.7))
      ENC
      /* CARE GOES HERE
      //GC.SYSIN EC */
      C*** THE FOLLOWING CARDS ARE THE DATA DECK FOR PROBLEM III-B.
      C*** THAT FEEDBACK COMPENSATION.

```

C	1	0.1	0.0002	1 1000 1
		0.6	31.628	0.22
		0.7	1000.	1000.
		0.0346		
		-0.0346		
		-0.0350		
		0.4		
		BLK 12=C1C2		
		BLK 22=C2C3		
		BLK 21=C3C1		
		BLK 11=C0C0		

10.

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