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A TIONALE AND PLAN FOR FIELD DATA ACQUISITION REQUIRED FOR THE RATIONAL DESIGN AND EVALUATION OF SEISMIC AND ACOUSTIC CLASSIFYING SENSORS by Bob O. Bon Mobility and Environmental Systems Laboratory U.S. Army Engineer Waterway: Experiment Station P.O. Box 631, Vicksburg, Miss. 39180

Final Report



Present for Project Ahanager, Remotely Monitored Battlefield Sensor System, AMC Fort Monmouth, New Jersey 07703

Under Project IX764723DL73

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| 20. ABSTRACT (Continued). |
| targets and terrains, it is recognized that an adequate design will require signature data base representative of the spectrum of conditions under which the system is to operate. |
| This report presents a plan for assembling a data base for the develop ment and testing of two types of seismic and acoustic classifying sensors: a sensor for classifying single targets, and a sensor for classifying single targets in a multiple-target environment. The plan also (a) defines the targets to be used in the data collection program, (b) defines the test site conditions to be used in the data collection program and develops a method for relating test site conditions to worldwide environments, (c) estallishes a method for assembling a data base of realistic background noise signatures and (d) specifies the test procedures for signature acquisition from the var ious target classes. The report includes maps showing predicted worldwide performance of seismic and acoustic sensors and the rationale behind their formulation. |
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PREFACE

The work reported herein is a portion of a seismic research program conducted by the U. S. Army Engineer Waterways Experiment Station (WES) and sponsored by the Project Manager, Remotely Monitored Battlefield Surveillance System, U. S. Army Materiel Command, Fort Monmouth, New Jersey, under Project No. 1X764723DL73 entitled "Target Signature Data Base Study."

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The work was under the direct supervision of the Chief, Mobility and Environmental Systems Laboratory (MESL), Mr. W. G. Shockley, and the Chief, Environmental Systems Division (ESD), MESL, formerly Mr. W. E. Grabau and currently Mr. B. O. Benn, and under the joint supervision of the Chiefs of the Environmental Research and Environmental Characterization Branches, ESD, MESL, Messrs. J. R. Lundien and J. L. Decell, respectively. Personnel making significant contributions to the preparation of the report include Messrs. Decell, M. A. Zappi, P. A. Smith, M. M. Culpepper, L. E. Link, and Lundien. This report was compiled by Mr. Benn.

Director of WES during this work <u>and preparation</u> of the report was COL G. H. Hilt, CE. Technical Director was Mr. F. R. Brown.

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CONVERSION FACTORS, U. S. CUSTOMARY TO METRIC (SI) AND METRIC (SI) TC U. S. CUSTOMARY UNITS OF MEASUREMENT

Units of measurement used in this report can be converted as follows:

| Multiply | By | To Obtain | | |
|--------------------------------|----------------|------------------------------|--|--|
| U. S. Customary to Metric (SI) | | | | |
| feet | 0.3048 | uetres | | |
| miles | 1.6093 | kilometres | | |
| tons (short) | 0.90718 | metric tons | | |
| Metric (S | 51) to U. S. (| Customary | | |
| millimetres | 0.0394 | inches | | |
| centimetres | 0.3937 | inches | | |
| metres | 3.2808 | feet | | |
| kilometres | 0.6214 | miles (U. S. statute) | | |
| kilograms | 2.2046 | pounds (mass) | | |
| newtons per metre | 0.0685 | pounds (force) per feet | | |
| grams per cubic centimetre | 0.0361 | pounds (mass) per cubic inch | | |
| centimetres per second | 1.968 | feet per minute | | |
| metres per second | 2.237 | miles per hour | | |
| kilometres per hour | 0.6214 | miles per hour | | |
| kilogram-second-centimetre | 0.0270 | slugs-seconds-inches | | |

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RATIONALE AND PLAN FOR FIELD DATA ACQUISITION REQUIRED FOR THE RATIONAL DESIGN AND EVALUATION OF SEISMIC AND ACOUSTIC CLASSIFYING SENSORS

PART I: INTRODUCTION

Background

1. A major objective of the Project Manager, Remotely Monitored Battlefield Sensor System (REMBASS), is the development of a seismic or an acoustic sensor (or both) that can classify (at the sensor) targets, i.e. discriminate among helicopters, fixed-wing aircraft, tracked vehicles, wheeled vehicles, walking men, and background noise, in worldwide environments. The approach almost universally taken to design logic for classifying sensors uses measured signals from targets of interest. From these signals, features that can be consistently associiated with a particular target are sought by means of mulciple correlation techniques. It has been documented that the correlation techniques are strong tools for evaluating and correlating the discriminating features of specific target classes; however, the dependence on empirical data restricts the applicability of the desired design.

2. Experience has shown that seismic and acoustic signals are affected by a number of target and environmental variables, which often result in an inability of the sensor to associate signals collected under one set of conditions directly with signals collected under other conditions.¹ However, REMBASS sensors are intended to work satisfactorily under a large variety of target and terrain conditions, and it is recognized that an adequate design will be forthcoming only if seismic and acoustic signals representative of those that would be generated in the real world are used in the design data bases. From a simplistic viewpoint, it can be argued that a solution to the design problem rests in generating a data base of sufficient size and statistical representativeness that would permit, with existing data analysis techniques, the isolation

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of the features that are unaffected by the generation and propagation of the seismic and acoustic energy. More mature consideration of the large number of viriables involved brings the realization that literally thousands of empirical tests would be required to define the signature envelope for a given target class.² Still more tests would be required to establish that the synergistic effect of combining certain variables would not result in nearly identical signatures from two or more classes of targets.

3. In view of the problems associated with designing classifying sensors strictly on the basis of empirical data, it appears prudent to attempt to generate a design data base by using a balanced experimental and theoretical program. In this approach, well-controlled empirical tests are conducted in a spectrum of target and terrain conditions, thereby providing measured data for use as interpolation benchmarks. In the theoretical portion of the program, realistic simulation models are used to estimate how the signatures would vary (from benchmark to benchmark) if the various terrain and target factors were varied throughout the range of interest.

4. The simulation techniques required in a balanced theoretical and experimental program should be applied with the realization that there is no such thing as an "exact" theoretical description of a phenomenon, and, therefore, there would always be some uncertainty as to how representative of the total population of signatures a given signature is. In this report a systematic experimental program is proposed by the U. S. Army Engineer Waterways Experiment Station (WES) that is aimed at developing seismic and acoustic data bases of defined worldwide representativeness. The results of the program are intended to provide considerable signature data for use directly in the design of classifiers and also to verify simulation results so that as an adjunct an analytically generated data base can be used in the design process with confidence.

Purpose

5. The purpose of this report is to present a plan, and the rationale for its development, for assembling a data base for the development and testing of two types of seismic and acoustic classifying sensors:

- <u>a</u>. A sensor for use in a preliminary REMBASS. The sensor must be capable of classifying single targets in terrain and background noise conditions representative of worldwide conditions. This sensor is considered by REMBASS to be in engineering development.
- b. An advanced-development sensor that is capable of classifying single targets in a multiple-target environment.
 This sensor must also perform in worldwide environments.

Scope

6. The plan:

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- <u>a</u>. Defines the targets to be used in the data collection program.
- b. Defines the test site conditions to be used in the data collection program and develops a method of relating test site conditions to worldwide environments.
- <u>c</u>. Establishes a method of assembling a data base of realistic background noise signatures.
- d. Specifies the test procedures for signature acquisition from the various target classes.

7. The development of the plan required study of several factors that cause instability in seismic and acoustic signatures, i.e. target, terrain, and background noise factors that induce variations in the signatures. Part II of this report presents the rationale for selecting the targets to be used in the data collection program. Part III addresses the problems associated with signature variations induced by different terrain conditions. Included in this part of the report is a

terrain matrix, the elements of which form a realistic combination of the terrain factors that affect seismic and acoustic signatures. Also included is a description of the methods used to combine the terrain element data and published terrain maps into a prediction of how seismic and acoustic sensors would be expected to work worldwide. Part IV is devoted to the development of a theoretical and empirical scheme for establishing a background signature data base. Part V summarizes the data acquisition procedures and includes a list of the tests, test sites, and targets required to implement the plan.

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8. It is emphasized that this report is to be used in conjunction with Reference 3, i.e., the test sites, instrumentation used, and target conditions should be documented in accordance with Reference 3. For this reason, details concerning these aspects of the data collection program are treated only briefly in this report.

PART II: TARGET SELECTION

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9. A major complication that affects the quality of the data base available for the design of classifying sensors is the fact that the largest portion of existing seismic and acoustic signature data has been collected from U. S. vehicles. Implicit in this practice is the assumption that signatures from foreign and domestic vehicles (in the same class) are very similar; however, data to demonstrate this are scarce or nonexistent. There are only a limited number of foreign vehicles available to the U. S. development agencies, and, therefore, any comprehensive signature data collection program for REMBASS will have to make extensive (although not exclusive) use of the U. S. vehicles. For this reason, it is necessary to compare U. S. and foreign vehicles on the basis of the seismic and acoustic signatures they phoduce. This part of the report presents a list of U. S. targets (and a rationale for selecting them) to be used in the REMBASS Engineering Development and Advanced Development programs.

U. S. Versus Foreign Vehicles

10. Since the vehicle parameters that control seismic an! acoustic signatures (i.e. those vehicle parameters listed in Table 1) have been identified,¹ it seems reasonable to assume that the parameters could be used as a basis for selecting U. S. vehicles that would yield signatures similar to several types of foreign vehicles. An extensive literature survey 4^{-29} was undertaken to identify U. S. and foreign military vehicles and to assemble the relevant information (that listed i. Table 1) on them. The following major problems emerged early in the study:

 <u>a</u>. A large number of vehicle types are identified, many of which are modifications of the basic type. For example, Reference 4 lists three types of 5-ton,* 6x6 cargo truck,

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^{*} A table of factors for converting U. S. customary units of measurement to metric (SI) units and metric (SI) to U. S. customary units is given on page 4.

i.e. M54, M54A1, and M54A2. The M54 cargo truck has a spark-ignition engine, the M54A1 has a diesel compressionignition engine, and the M54A2 has a multifuel compressionignition engine. The different ignition systems will cause subtle differences in the seismic and acoustic signatures and therefore all types must be listed. However, other vehicle types have such modifications as hard cab versus canvas top, which would not change the signature of the vehicle. It was decided to inventory and list all the pertinent data on all vehicle types, including all modifications.

- b. A large number of U. S. vehicle types are experimental or prototype vehicles. It was decided to include all these vehicles in the inventory because some running prototypes exist. It was felt that prototypes can possibly be used in a field program if they are the only U. S. vehicles that produce signatures similar to important foreign vehicles.
- <u>c</u>. Complete data (listed in Table 1) exist for only a few U. S. and foreign vehicles. A single source of useful (but not complete) data was not readily available at WES or at any one Department of Defense (DOD) office. Therefore, various publications had to be ordered from a number of different sources. All material had not been received at this writing (July 1975).

11. The vehicle types identified are listed in Tables 2-9 as follows:

| ሞላክ1ላ | Vebtelo Class | Number of | |
|-------|----------------------------|----------------------|--|
| Table | venicie ciass | venicie Types Listed | |
| 2 | U. S. wheeled | 273 | |
| 3 | USSR wheeled | 146 | |
| 4 | U. S. tracked | 110 | |
| 5 | USSR tracked | 79 | |
| 6 | U. S. rotary-wing aircraft | 36 | |

| | | Number or | |
|-------|---------------------------|----------------------|--|
| Table | Vehicle Class | Vehicle Types Listed | |
| 7 | USSR rotary-wing aircraft | 13 | |
| 8 | U. S. fixed-wing aircraft | 104 | |
| 9 | USSR fixed-wing aircraft | 65 | |

Because of the large number of vehicles identified early in the study, the vehicle inventory does not include any vehicles manufactured prior to 1940 and also was restricted (with a few exceptions) to vehicles of U. S. and USSR manufacture.

Selection of Foreign Vehicle Analogs

Ground vehicles

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12. The large number of individual models listed for each country necessitated the comparison of the vehicle parameters by classifying the vehicles according to categories of some of the vehicle parameters listed in Table 1. As stated in paragraph 10c, all the data required were not available and a much abbreviated list of parameters had to be used. For many wheeled vehicles the following important parameters were available: weight, number of wheels, tire size, suspension type, horsepower, fuel type, and coolant type. However, only weight, horsepower, and coolant type were consistently available for many of the tracked vehicles. Each U. S. and each foreign vehicle (where sufficient data were available 4-29) was classified or grouped (by computer) according to the parameter categories listed in Table 10. Table 11 summarizes the results of the classification for the wheeled and tracked vehicles and presents groupings of U. S. vehicle types that can be expected to yield signatures similar to groupings of foreign vehicle types. Table 11 shows two categories of foreign vehicles, "Desired Foreign" and "Other Foreign." The desired foreign vehicles were those vehicles identified in Tables 3 and 5 that met the following criteria:

- <u>a</u>. The vehicle had to (potentially*) exist in significant numbers in Warsaw Pact countries; or if the vehicle was of new design, production had to have been initiated or was likely to be initiated.
- b. All weight classes (light, medium, and heavy) had to be represented in each vehicle class.

All the foreign vehicles that met the criteria above are listed in Table 12. Those foreign vehicles that did not meet the criteria, but could be classified (data were available), are listed in Table 11 as "Other Foreign" vehicles.

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13. In summary, the U. S. vehicles that should be used in the data collection program are those listed in Table 11 under the heading "Proposed U. S. Analog." It is emphasized that the listing does not always identify a specific U. S. vehicle as the proposed analog, but rather a group of U. S. vehicles. This specification was omitted deliberately to permit the final selection at the locality where the signature tests are run. The selection then can be rationally biased toward what is available at the test location.

14. Study of Tables 11 and 12 reveals that there is not a U.S. analog for all the desired foreign vehicles; i.e., no analogs were found for the following:

| Wheeled | Tracked |
|---------|---------|
| T-111 | Т54 |
| T-13C | Т55 |
| T-141 | т62 |
| OT-64 | M70 |
| ОТ-64 | |

Also no data are available for certain foreign vehicles; therefore, i. was impossible to determine whether or not there is a U. S. analog for the tracked M-1973 and M-1974. Based on the information summarized above, it appears prudent to:

* Data are not ava. lable to estimate the total number of vehicles of a given type. Estimates are made on the basis of TOE (Table of Organization and Equipment) allowances for the various military units.

a. Put highest priority on gathering data on those foreign vehicles that have no U. S. analogs.

- b. In all cases possible, collect signature data (concurrently) on the foreign vehicle and its U. S. analog to demonstrate that the U. S. analog actually generates a facsimile signature.
- <u>c</u>. Review and study existing DOD signature data to compare (where possible) signatures from U. S. analog vehicles and the corresponding foreign vehicles to demonstrate that the U. S analog actually generates a facsimile signature.
- d. Solicit from the Foreign Science Technology Center and other intelligence sources information on those vehicles identified as important but for which no descriptive data are available.

Aircraft

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15. Criteria similar to those stated in paragraph 12 for ground vehicles were applied to the foreign aircraft (Tables 7 and 9) to arrive at a listing of foreign (exclusively USSR) aircraft from which signatures are desired (Table 13). It should be noted that data on the number of any identified aircraft were not available; therefore, the listing in Table 13 should be considered tentative. As much of the target data identified in Reference 3 (Table 1) as was available was assembled for each foreign aircraft listed in Table 13, and the values of these parameters were compared by computer with the corresponding values for the U. S. aircraft. This analysis resulted in identification of USSR aircraft that could be considered analogous to a given U. S. aircraft. The characteristics of the U. S. aircraft are listed in Table 14 along with the corresponding data for as many of the desired aircraft as applicable. The U. S. aircraft (extracted from Table 14) that can be considered analogous to the foreign aircraft and should be used in the data collection program are:

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| Rotary-Wing | Fixed-Wing | |
|-------------|----------------|--|
| CH-46F | None available | |
| UH-IN | | |
| TH-57A | | |
| CH-3B | | |
| HH-IK | | |

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Study of Tables 13 and 14 reveals that a U. S. analog is not listed for every desired foreign aircraft, i.e., no analogs were "ound for the following aircraft:

| Rotary-Wing | Fixed-Wing |
|-------------|----------------|
| M1-12 · | Tu-22 |
| M1-10 | Tu-95 |
| Mi-6 | Tu-16 |
| Mi-4 | Be-12 |
| | Yak-25 |
| | M1G-25 |
| ` | MiG-21 |
| | An-22 |
| | 11-76 |
| | Tu-1 44 |

Also no data were available for certain foreign aircraft; therefore, it was impossible to determine whether there is a U. S. analog. These aircraft are:

| Rotary-Wing | Fixed-Wing |
|-------------|-----------------|
| Ka-15 | Tu-22 |
| Ka-22 | Tu-95 |
| Yak-24 | ' ſu-1 6 |
| | Be-12 |
| | Yak-25 |
| | MiG-25 |
| | MiG-21 |
| | An-22 |
| | I1- 76 |
| | Tu-144 |

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16. In summary, there appear to be few U. S. aircraft that can be assumed to generate seismic and acoustic signatures that would be facsimiles of signatures generated by USSR aircraft. It is emphasized that the results presented in paragraph 15 are based on incomplete data: therefore, the conclusions presented on the foreign aircraft from which signatures are desired (Table 13), as well as the list of foreign vehicle analogs (paragraph 15 and Table 14), should be considered tentative.

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PART III: TEST SITE REQUIREMENTS

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17. It is desired that REMBASS work satisfactorily any place in the world. It is generally recognized that there will inevitably be conditions under which the terrain will constrain the operation of the system, but the goal is to develop a system that is as terrain insensitive as possible. Experience with classifying sensors has emphasized that their performance was closely related to the terrain conditions on which the design data base was generated; therefore, it is important to know where in the spectrum of world terrain a given test condition lies. From a statistical standpoint, testing in all terrain conditions that affect neismic and acoustic signatures appears impossible; so the ability to generalize, i.e. extrapolate or interpolate the signals collected at a site, is as important as the data collection effort itself. The test sites recommended for use have been selected on the assumption that the data could be generalized by analytical methods. The racionale for establishing the test site requirements is developed in the following paragraphs.

Verrain Factor Considerations

18. Seismic signatures are normally more sensitive than acoustic signatures to environmental conditions, but exceptions do occur. For example, wind has both a direct effect on acoustic signatures (i.e., it could carry the sound away from the sensor) and an indirect effect (i.e., it could cause noise as it flows around vegetation), and thereby could obscure the acoustic signals. Also, soft soil conditions can cause a vehicle target to work harder, thereby increasing the engine noise; but at the same time, the soft soil would tend to decrease tire or track and hull noise. Because of this sensitivity of seismic signatures, the test site selection criteria are based primarily on seismic considerations, but documentation of site conditions should include all the terrain data (specified in Reference 3) needed to extrapolate both seismic and acoustic signatures to other terrains.

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19. The terrain factors that significantly influence the magnitude and frequency content of a generated seismic signal are:

- a. Ground surface rigidity (surface spring constant, N/m; and maximum deformation, m).
- b. Bulk properties (compression wave velocity, m/sec; shear wave velocity, m/sec; and bulk density, g/cm³).
- c. Depths to interfaces, m.

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- d. Surface roughness, rms elevation in cm (important only
- when it causes motion in the target mass; used primarily for vehicle targets and not walking-man targets).

These factors are discussed in the following paragraphs.

20. As a target moves along the ground surface, the material over which it moves will deform in a nonlinear manner. The amount of deformation can be estimated from load-deflection (plate-load) terms on the material.³⁰ The force the target applies to the ground with respect to time is related to these ground deformations, thus affecting the magnitude of the seismic signal generated by the target.

21. The properties of the various soil layers (i.e. compression wave velocity, shear wave velocity, bulk density, and thickness of each layer of material) affect to a great extent the coupling and propagation of the generated seismic signal. These parameters vary directly with the type of material present. Generally, a more rigid material will allow less coupling of the signal to the substratum, but will attenuate the signal to a lesser degree as it is propagated. Conversely, a softer material will allow more coupling of the signal energy, but will attenuate the propagated signal to a greater extent. In general, for a given surface soil condition, the shear wave velocity and depth of the first and second layers are good indicators of substratum rigidity and therefore, to a large extent, control the seismic responses from a given location. These factors used in conjunction with WES propagation models form the knystone for selecting the test site and relating the test results to worldwide conditions.

Terrain matrix

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22. To approximate the spectrum of terrain conditions that affect the generation and propagation of seismic signals, the normal range of variation for each of the terrain factors (paragraph 19) was defined, and a terrain matrix, elements of which are realistic combinacions of terrain factors, was compiled (Table 15). It was recognized that a matrix could not be designed that would account for every possible variation in terrain conditions that is known to exist in the world. For this reason, the following guidelines were followed in developing the terrain matrix:

- <u>a</u>. All elements of the matrix should be composites of terrain features that could most likely be found in the real world. The matrix elements selected should represent those conditions that would be likely to occur a significant percentage of the time.
- b. The matrix should contain combinations of factors that would result in the "best-case" and "worst-case" performances, and also combination of factors that would result in performances for several intermediate cases. Thus, the matrix should span the ranges of values that are possible in the world environment.

The derived terrain matrix (Table 15) contains 70 terrain elements. From a technical standpoint, it would be desirable to test the vehicles in real-world conditions that correspond to all 70 terrain elements; but for practical reasons, signature data will have to be obtained from much fewer locations. For this reason it is important to establish the relative significance of each element, i.e. areal extent and the degree to which each element affects the seismic signal.

Seismic response

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23. From previous studies (paragraph 21 and Reference 40) at WES, it has been shown that the shear wave velocities of the surface and subsurface soils strongly influence the generation and propagation of seismic energy. This fact suggests that seismic responses could be displayed in terms of shear wave velocity and thereby provide a rations.

means of grouping or further generalizing the elements listed in Table As Figure 1 displays the shear velocities for the various terrain matrix elements, i.e. top-layer-material shear wave velocity versus foundationmaterial shear wave velocity, along with the general descriptions of the materials commonly found with the various shear wave velocities (a more complete description of each element is given in Table 15). Each of the crosses in Figure 1 represents several elements in which the layer thicknesses are different (e.g., top layer is 0.25, 1.5, or 4.0 m thick). The values of shear wave velocities shown are presented to span the range of values found in nature (excluding hard, c. spetent rock); therefore, note that the top-layer-material shear wave velocity ranges to about 1200 m/sec. Top and foundation layers can be found that exhibit the full range shown; however, velocities in surface layers greater than about 600 m/sec are relatively uncommon.

24. To generalize the relative seismic response from each matrix element, seismic signatures predicted for the PT76 (USSR light tank) at a range of 300 m were analyzed (Figure 2) in terms of the maximum signal amplitude; i.e., if the particle velocity span (maximum positive peak to negative peak) of the seismic signature was between 0 and 0.2 x 10^{-3} cm/sec, the matrix element was considered to have poor seismic response; if the particle velocity was between 0.2 and 0.5 x 10^{-3} cm/sec, the seismic response was considered fair; and if the particle velocity was 0.5 x 10^{-3} cm/sec or greater, the seismic response was considered good.

25. Large amounts of seismic signature data have been collected by WES and other DOD agencies at sites in the following locations:

| | WES | Other DOD Agencies |
|------------------------|-----|-----------------------|
| Yuma, Arizona | Х | х |
| Vicksburg, Mississippi | Х | - |
| Fort Huachuca, Arizona | Х* | - |
| Panama Canal Zone | Х | Х |

*Data collected in both wet and dry seasons.

| | 1150 | Other DOD |
|--|------|-----------|
| | WES | Agencies |
| Fort Bragg, North Carolina | Х* | х |
| Eglin Air Force Base, Florida | Х | Х |
| Aberdeen Proving Ground, Maryland | х | X |
| Fort Wainwright, Alaska | х | - |
| Honeywell Proving Grounds, Minnesota | х | Х |
| Nellis Air Force Base, Nevada | Х | - |
| Fort Lewis, Washington | х | - |
| Puerto Rico | Х | - |
| West Germany | Х | - |
| Fort Carson, Colorado | Х | - |
| General Motors Proving Ground, Milford, Michigan | Х | Х |
| Fort Belvoir, Virgínia | Х | Х |
| | | |

* Data collected in both wet and dry seasons.

Figure 3 shows a plot of shear wave velocity for the top and foundation layers at all sites at which WES has collected data. Comparison of Figures 2 and 3 reveals that the bulk of the signature data have been collected at sites that have relatively good seismic responses. For this reason priority should be given to testing at sites that have relatively poor seismic responses, i.e. sites that have high shear wave velocities in their first and second layers.

Areal extent of the terrain elements

26. To arrive at an estimate of the relative occurrence of each of the terrain elements, they were correlated with published map information. As indicated in paragraph 19, the terrain factors in the matrix are quite specific; but the published information on the world's terrain conditions is normally thematic maps of physiography, agriculture (soil type and texture), lithology, etc. Correlation between the terrain matrix elements and the more general mapped data can be established in only a qualitative sense, and then only if several of the general terrain factors are combined and considered simultaneously.

• 27. The published maps were reviewed to determine (a) the types and quality of thematic maps available, (b) their scale and usefulness in meeting the required objectives, and (c) their immediate availability. Five thematic maps depicting regional associations of terrain characteristics (factor families) were selected: surface configuration, surface soil texture, subsurface lithology, state of ground (water table regimes), and vegetation (see Tables 16-20). These maps were regionally interpreted and adapted to provide the required input data for the compila-"tion (or superposition) of thematic maps of the world. A map scale of 1:50,000,000 was chosen as being the most compatible for the mapping task.

28. The five thematic maps were stacked manually to compile and produce a thematic factor complex map. This compilation process generated "unique" map units of the world that are characterized by an array of five separate terrain characteristics (factor families). A total of 1052 unique map units were thus identified (Plate 1). Table 21 is the legend for the factor complex map (Flate 1). The numbers in the legend under surface configuration, soils, lithology, etc., correspond to the category numbers identified in Tables 16-20. For example, map unit 1 (Table 21) is situated in a plain (Table 16, category 1), the soil is predominantly sand (Table 17, category 1), and the lithology is consolidated rock (Table 18, category 1), etc.

29. The terrain descriptions that identify the various terrain matrix elements (Table 15) were qualitatively correlated with the array of terrain characteristics obtained from the five thematic maps (Table 22). For example, terrain description 1.10 <u>could</u> exist in each terrain factor under which a 1 is entered in the first line of Table 22. A computer program was developed to associate the unique map units of the thematic factor complex map with all the possible terrain descriptions that could be associated with the various terrain matrix elements. Table 23 is a portion of the computer-generated key that identifies the terrain matrix element terrain description numbers associated with the unique map units of the thematic factor complex map.

30. On the basis of the shear wave velocity criteria shown in Figure 2, for both the surface and foundation materials, and the thick-ness of the surface layer, the terrain matrix elements were classified

into the seven categories of seismic response (Table 24). Using this classification scheme, each unique map unit of the thematic factor complex map, which had been previously correlated with the terrain matrix element terrain description numbers, was assigned to a category of seismic response, thus producing a world map that delineates areas of relative seismic response (Plate 2). It is emphasized that the map depicts the predominant seismic response of each area. Within each area delineated, the seismic response will vary because of local variation in terrain conditions that could not be identified at the mapping scale used. Study of Flate 2 illustrates two points:

- <u>a</u>. A significant portion of the world will exhibit fair to good seismic response (category 3); therefore, it can be assumed that seismic sensors can be designed to function adequately in a large portion of the land mass of the world.
- b. Figure 3 shows that relatively few tests have been conducted at sites that fall in category 3; therefore, additional signature data should be collected in these types of seismic-response areas. Also, significant portions of the world's land mass exhibit fair to poor seismic response, and extensive signature data should be collected in these areas also (categories 6 and 7).

Test Site Recommendations

31. In general, a spectrum of sites (based on their shear wave velocities) should be selected to span the range of variation found in nature. Because the bulk of available signature data has been collected in areas of relatively good seismic response, priority should be given to data collection at sites with top-layer shear wave velocities greater than about 400 m/sec. The foundation-material velocities should range from about 200 to 1600 m/sec. The sites should exhibit a variety of first-layer thicknesses. Since surface conditions affect seismic and acoustic signatures, tests should be conducted on a range of surface

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conditions; i.e., tests should be conducted on both smooth roads (goodquality gravel or pavement) and cross-country, and one site should have soil soft enough to result in extensive rutting. More specifically, the following tabulation can be used as a general guide to selecting sites.

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| Condi- tion | Top-Layer Shear Wave Velocity m/sec | Material Shear Wave Velocity m/sec | First- Layer Thick- ness m | Site Surface | Prior- ity |
|----------------|--|---|--|------------------------------|---------------|
| 1 | > 500 | 300 | >2.0 | Cross-country | 2 |
| 2 | >400 | >400 | N/A | Smooth road | 1 |
| 3 | >400 | >400 | N/A | Cross-country | 2 |
| 4 | >400 | >600 | <0.5 | Cross-country | 2 |
| 5 | > 400 | >600 | <0.5 | Smooth road | 1 |
| 6 | >400 | >600 | >1.0 | Cross-country or smooth road | 2 |
| 7 | >700 | >1000 | <0.5 | Cross-country | 2 |
| 8 | > 700 | >1000 | >1.0 | Cross-country or smooth road | 1 |
| 9 | < 200 | ≥200-<600 | <0.5 | Smooth road | 2 |
| 10 | < 200 | >600 | >0.5 | Smooth road | 3 |
| 11 | < 200 | >600 | >1.0 | Smooth road | 3 |
| 12 | >400 | >600 | <0.25 | Smooth road | 2 |
| 13 | <200 | >600 | >1.75 | Smooth road | 2 |
| 14 | <200 | < 600 | >1.0 | Smooth, soft surface (ex- | - 1 |

32. Other factors that must be considered in the selection include:

- a. Ease of access to the site.
- b. Vehicle logistic and security support.
- <u>c</u>. Weather conditions; for example, testing in Alaska in the winter would not be cost-effective.
- d. Background noise, cultural and natural.

No site will be optimum with respect to site and support conditions, and the selection should be biased toward the site conditions and priorities listed in paragraph 31. Also, specific sites used for collection of design data should be situated where the background noise is relatively quiet. Sites meeting almost all the criteria listed above can be found on government property at Yakima Firing Center, Yakima, Washington; Fort Hood, Texas; and test areas available at the WES, Vicksburg, Mississippi.

PART IV: BACKGROUND NOISE CONSIDERATIONS

33. One major complication in designing classifying sensors is the impossibility of incorporating a sufficient number of realistic background noise signatures into the design data base. A sensor must be designed to operate at any arbitrary point where the background noise is the result of a combination of various noise sources. The noise source will often be transitory (storms, highway and air traffic), but can be permanent (pumping stations, stream noise, etc.). Furthermore, the distance from the noise source will affect the resultant noise signature.

34. To attempt the collection of a sufficient number of background signatures that would constitute a statistically representative sample of the total population of background signatures is probably foolhardy. It appears much more feasible to collect data from a number of independent noise sources and combine them analytically by using seismic- and acoustic-signal propagation, models.

35. Figure 4 shows the five major steps required to develop a realistic background noise design data base: (a) catalog background noise sources, (b) obtain signatures from the various sources, (c) determine interrelation of sources, (d) compile a matrix of sources and their corresponding distances from arbitrary points in the world environments, and (e) superimpose signatures from sources by using WES propagation models. The following paragraphs discuss these steps in more detail.

Noise Sources

36. Independent noise sources are grouped into two categories: cultural and natural. Cultural background noises are those nontarget noises that are the result of man's presence or activities. Natural background noises are those nontarget noises that are the result of nature's activities. Table 25 is a tentative list of noise sources that are considered to be sufficiently independent (or unique) to yield representative signatures. The field data collection program should be directed toward measuring signatures from these sources. Measurement

duration should include at least one 24-hr cycle.

Map Study

37. In any geographic location of the world, at any selected point on the ground, at least one and probably more of the cultural noise sources listed in Table 25 will be encountered. In some large geographic areas, such as countries or segments of countries, there will be a certain mix of cultural sources that could be expected to occur at any given location. This may be due to such factors as the overall level of development, long-term cultural history, or primary commercial products (industrial, agricultural, etc.). One factor that would certainly affect the mix would be the proximity to the point source selected. That is, the larger the area (around a selected point) considered, the greater the probability that a large number of background noises will be encountered. Thus, to determine the probable mix to be encountered, the sampling points for a given geographic area must be not only randomly selected, but also sufficient in quantity to ensure a statistical representation within some desired confidence limits. In the case of a particular interest, the purely random aspects might be partially abandoned in the form of influencing the sampling locations so that they are representative of the range in variation of the contributing factors. For instance, in considering seismic signatures, such factors as soils, geology, vegetation, slope, etc., play a part in contributing to the resulting signature. Thus, it is desirable to select areas (on the basis of an analysis of the combination of these factors) that are representative of the range of variations existing. This was accomplished in West Germany. Figure 5 shows the locations of the 1:50,000 quadrangle areas that are deemed to be most representative of the range of variations that exist in the terrain factors mentioned above.

38. Within each 1:50,000 quadrangle selected for study the noise sources had to be sampled. The following paragraphs describe the procedures by giving an example using the Fulda quadrangle northeast of

Frankfurt. The geographic boundaries defining the quadrangle were used as the limits of consideration, and a random number generator was used to select 20 points within the sample quadrangle boundaries (see Figure 6). Each of these 20 points was plotted on the quadrangle and used as a reference in determining the mix of background noise sources that was encountered at various distance classes from the randomly selected points, i.e. 0-0.5, 0.5-1.0, and 1.0-2.0 km (see Figure 7). For each distance class, an inventory of the cultural background noise sources was made. The method lescribed above was applied universally to all 20 points (Universal Transverse Mercator Grid coordinates are listed in Table 26), which resulted in the inventory of noise sources listed in Table 27. This inventory shows the types and numbers of background noise sources encountered as a function of the distance from the sampling point. The numeric codes for the types of b. __cound noise sources are identified in Table 25.

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A Method of Compiling the Noise Signature Data Base

39. A terrain matrix element can be associated with each sampling point, thereby providing the necessary terrain data for using the WES propagation models to make a realistic composite signature for each sampling point. The composite signature is produced by associating each noise source identified (Table 25) with a random distance selected within the various distance ranges (0-0.5, 0.5-1.0, and 1.0-2.0 km), from the point at which the signature is desired. Then for each noise source identified, a measured signal (a facsimile of the noise source identified) is input to the propagation models and a new signal is c. lculated for the proper range. Once calculations are made for all the measured signals (i.e., these signals are propagated to the desired point), the signals are summed to make a composite background noise signal that is directly related to the real-world environment. The " immediate objective that emerges for the field sampling program is the collection of the background noise signatures for the noise sources listed in Table 25.

PART V: DATA COLLECTION PLAN

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40. As stated earlier, state-of-the-art techniques for correlating target signature features with the various vehicle classes require a signature data base representative of the total signature population. A rigorous definition of an adequate data base cannot be made at this time (July 1975) because information is not available to define the expected signature variation from a given vehicle type (i.e. the M113 type or the M151 type) nor the signature variation from a given vehicle class. Table 1 identifies the target variables, i.e. components of the ground (wheeled and tracked) and air (rotary-wing and fixed-wir.g) vehicles that are known to affect seismic and acoustic signatures to some degree. Table 1 contains a sufficient number of variables to suggest that there can be a great de/l of signature variation within a given target class. Furthermore, som' signature variations within a target type can be expected because of differences in manufacturer and because of the normal variations in mechanical performance caused by changes in parc tolerances with age (wear).

41. The design data base should have signatures that span the range of signature variations not only as a function of the various types of vehicles within a class, but also as a function of the environment within which the signature is generated. Data to define the signal variation associated with a target type and class should be generated with single targets. These data are intended to provide the required data for REMBASS engineering development, i.e. for the simpler singletarget classifiers. For a classifier capable of performing in a multiple-target environment (advanced-development classifiers), data must be generated to permit definition of the information extractable (about a single target) from signatures made up of two or more targets.

42. This part of the report describes a series of tests that will yield data critical to the definition of the seismic and acoustic signal variations within a target type and target class. Also, a plan is presented for the collection of seismic and acoustic response data

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from multiple targets such that an information extraction threshold (concerning a single vehicle) can be defined. Further, data collection from background noise sources (Table 25) is described.

Single-Target Data Acquisition

Signature variations from cargets of a single type

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43. Signature data collection programs are often conducted using only one vehicle to represent a vehicle type. Often, as in the case of foreign vehicles, only one vehicle is available; furthermore, excessive costs preclude use of more than one target type if U. S. vehicles are used. The danger exists, however, that a specific vehicle could have a discrepancy that generates a signature feature that could bias the design of the logic of a classifying sensor. During the production of a specific type of vehicle, production controls ensure that the component parts meet certain specifications. During assembly, these parts are connected, again within certain tolerances, into a working mechanical system.

44. The performance of this assembled system must also meet certain specified criteria, and it is probable that only slight signature variations will result from vehicle to vehicle, especially when the measurement being used considers the synergistic effect of the many slight variations, i.e., variations in one component may tend to compensate for variations in another. Certain vehicle components may tend to wear unevenly; therefore, old vehicles may produce more erratic or significantly different signatures than new ones.

45. To rigorously ascertain the signature variations for all the vehicle types of interest would be extremely costly and time-consuming. Some data, however, are badly needed to demonstrate that signatures from a single vehicle are representative of signatures from that vehicle type. The following paragraphs present a plan for determining signature variations in a specific target type. A set of tests to be conducted, in which lignatures are measured under controlled conditions, will be

described, and the data necessary for characterizing the target and terrain conditions will be specified. Targets

46. The tests will be restricted to types of vehicles within two target classes: wheeled and tracked vehicles. Based on the comparisons according to probable seismic and acoustic signatures (Table 11), and the resulting targets defined for use in the data collection program, the tests will use an M35Al wheeled vehicle and an M113 Armored Personnel Carrier tracked vehicle. The data to be collected and the test conditions specified will apply to both vehicles.

47. Three vehicles of each type should be selected at random from a large pool (more than 20) of vehicles whose overall condition is determined to be "reasonably representative of live conditions," e.g. have been readied for unit training by normal maintenance procedures. The selection of these vehicles, from those available for use at the test site, should be accomplished with a minimum of bias.

48. Once the vehicles have been selected, they should be inspected for major deficiencies such as a bad muffler, etc. If such deficiencies exist, the vehicle should be rejected and another vehicle selected. The vehicle data listed in Table 1 should be compiled for each vehicle type to provide data for predicting seismic and acoustic signatures. In addition, the overall condition of each test vehicle should be documented so that variations in signal characteristics can be related to variations in vehicle conditions. At one test site it would be desirable to obtain signatures from a vehicle (if a multifuel vehicle is available) using both diesel oil and gasoline to provide a basis for comparing the signatures of significance as related to fuel.

Test site conditions and layout

49. No special test site condition is specified for these tests. Therefore, any of the 14 terrain conditions recommended in paragraph 31 would be satisfactory. However, the tests should be repeated in at least two different areas, e.g. Yakima Firing Center, Fort Hood, or Mississippi (total of 12 vehicles, six from each class).

50. The general layout for these tests is shown in Figure 8.

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Three test conditions will be required: (a) a paved road; (b) a crosscountry condition, i.e., characterized by soil covered with some type of low vegetation; and (c) an obstacle course that is level except for an obstacle, wider than the vehicle, placed at the closest point of approach to the sensor and perpendicular to the direction of travel. The obstacle should have a semicircular cross section whose height (radius) is 20 cm and base (diameter) is 40 cm. Each of these test conditions should be situated in the same environmental setting.

51. The constant-speed section (see Figure 8) of each test lane will vary in length depending upon the terrain conditions and target being tested. This distance will be the result of a field decision subsequent to determination of the seismic response characteristics of the site. In the past, this distance has varied from less than 500 to about 2000 m for the M35A1 and the M113. The acceleration and deceleration sections of the course should be at least 100 m long, but for the faster test speeds, more than 100 m may be needed for the acceleration lane.

Conduct of tests

52. Each vehicle should be run at two constant speeds through the smooth paved-road course--10 km/hr and convoy speed. The vehicle should be accelerated and decelerated gradually up to and from the desired constant velocity. For the cross-country test course, the tests should be conducted in the same manner except for speeds. For this course, each vehicle should be run at 7.5 and 30 km/hr. For the obstacle course, each vehicle should be run at constant speeds of 5 and 12 km/hr. An event mark should be placed on the signature recording to indicate entrance into and exit from the constant speed zone, and at each 50-m interval throughout the test course. Recordings of seismic and acoustic signatures should be initiated in the acceleration lane and be continued until the vehicle comes to a stop in the deceleration lane.

Signature variations from targets of a single class

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53. As stated in paragraph 41, data to define the signature variations associated with a target class should be generated with

single targets. These variations result from differences in the vehicle types within the class in addition to differences resulting from travel mode of the target, site conditions, and range from target to sensor. Targets of interest for this data collection effort are: wheeled ground vehicles, tracked ground vehicles, rotary-wing aircraft, fixed-wing aircraft, men, and backgrounds. The U. S. ground vehicles selected as most desirable are listed in Table 11, and the desired aircraft are listed in Table 14 (note that no U. S. fixed-wing aircraft have been identified as analogous to Warsaw Pact aircraft). Walking-man targets, though not addressed in detail thus far in this report, are required and data should be collected from both single-map and squad targets (i.e. one, three, and seven men). Site req irements are recommended in paragraph 31. The following paragraphs discuss the test method and course layout for each target class.

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54. <u>Ground vehicles</u>. The test method and layout should be identical to those described in paragraph 52 and shown in Figure 8, respectively. Duplicate tests should be run for each vehicle referred to in paragraph 13 on both improved road, cross-country, and obstacle sites on as many of the test (terrain) conditions listed in paragraph 31 as possible. The wheeled vehicle data acquisition should be conducted first, starting with the lightest vehicle and proceeding to the heavlest. The tracked vehicle data acquisition should follow in a similar manner. This sequence will minimize the influence of previous vehicle runs (i.e. on the geometry of the test path) on the on-going tests and eliminate the wheeled vehicle reaction to track pad imprints in the ground. This is especially important on cross-country sites; in very soft soils separate test lanes should be selected for wheeled and tracked vehicles.

55. <u>Aircraft</u>. Signatures from aircraft are less sensitive to terrain conditions but are affected more by atmospheric conditions than are signatures from ground vehicles. In addition, aircraft travel mode affects the resulting signature appreciably. The test layout for acquisition of aircraft signatures should consist of positioning a single triaxis geophone in the ground at some convenient position and burying a second triaxis geophone near the first and covering it with a

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sufficient acoustical barrier to prevent direct coupling of acoustic waves to the geophone. The acoustical barrier should consist of a thickness (empirically determined) of sound-absorbing material such as fiberglass insulation. Both geophones should be positioned so that the axis of one of the horizontal geophones is oriented in the direction of the aircraft approach path for the tests. In addition to the geophones, an acoustic transducer should be located near the geophones to record the acoustic signatures of the targets. The aircraft test path should begin at a distance of 2 km from ground zero and proceed beyond ground zero for the same distance. .. should be noted that the test layout above can be aphriced by simply adding an acoustically protected triaxis geophone to the triaxis geophone-acoustic sensor array shown in Figure 8 (i.e. the array closest to the vehicle test path) and recording only the outputs from these three sensors. The aircraft test path would then parallel the vehicle test path and the vehicle test path could be used as a navigation aid by the aircraft pilots.

56. Duplicate tests should be run with the aircraft specified in Table 28. It is noteworthy that only rotary-wing aircraft are specified by name in this list. Fixed-wing aircraft (approximately three) should be included as they are determined to be applicable to the data-collection effort.

57. The travel modes for each aircraft should consist of horizontal flight at speeds one-half the normal cruising speed and at the normal cruising speed, at two heights above the ground of 150 to 750 m. In addition, signatures should be acquired for the aircraft descending from 750 m to approximately 50 m and ascending back to 750 m. The descent should begin at a position along the aircraft test path approximately 0.5 km from ground zero and terminate at ground zero. The ascent should begin at ground zero and be completed at a distance of 0.5 km from ground zero. The descent and ascent tests can be conducted as a single overpass; no touchdown is necessary.

58. The tests described above should be conducted in as many of the different subsurface conditions in paragraph 31 as possible so that the effect of terrain conditions can be completely evaluated. The
atmospheric conditions cannot be easily specified prior to testing, but should be thoroughly documented at the time the test is conducted. Walking-man target

59. The layout for acquisition of signatures from walking-man targets should be identical to that shown in Figure 8, except that only the response of the triaxis geophone and the acoustic sensor closest to the travel path should be recorded. The targets should consist of one, three, and seven men and the travel modes should include normal route walk and march step (marching in unison). Two walk paths should be used, the first emphasizing low signal levels having a closest point of approach (CPA) of 15 m and the second having a JPA of 5 m from the triaxis geophone. Each target should start at a position/100 m from the CPA point and proceed beyond the CPA 100 m on both walk paths. When a road is available, one walk path should be identical to the vehicle test paths on the road, and the other should parallel the road in natural terrain. The tests should be conducted in as many of the 14 conditions listed in paragraph 31 as possible.

Summary

60. Table 28 summarizes the targets, site conditions, and travel modes needed for the definition of the variations within target types and classes. A total of 1420 test runs are identified with 740 considered essential, 544 considered second priority, and 136 considered third priority. The first column (Table 28) shows that none of the target types for fixed-wing aircraft are listed. Further study is needed to define the U. S. aircraft that should be used in the data acquisition program.

Multiple-Target Signature Acquisition

61. An advanced-development (AD) sensor must be capable of classifying single targets in a multiple-target environment and in worldwide terrain environments. Data must be collected in these environments so that specifications for the design of AD sensors can be prepared. Unfortunately, multiple targets present special problems in an AD data collection program because the ranges of each vehicle to the sensor are restricted by the dynamic limits of recording system. If the recording limits are set so that a primary vehicle produces slightly below the maximum recordable signal, all secondary targets must be restricted in range so that the total combined signal level from all targets remains below the maximum. Thus, the choice in signal level dictates the nearest range at which secondary targets can approach the sensor. Also, a lower limit in signal amplitude is established by the noise level inherent in the recording process. A secondary target whose range increases to the point at which its signal falls below the noise level of the recorder does not produce usable information.

62. In summary, the combined signal strengths from all targets in a multiple-target data collection program must be restricted to the dynamic range of the recording system (i.e. above the noise level and below the recording saturation limit). For good analog recording systems, this dynamic range is restricted to approximately 30-40 dB, and for good digital recording systems, the dynamic range is restricted to approximately 50-60 dB. The dynamic range of the recorder can be shifted up or down to accommodate nearly all primary target requirements, but once it is set, the dynamic range then restricts the recordable signal level (and thus the range from target to sensor) of all secondary targets.

63. In the following paragraphs, a procedure is described in which the dynamic range of the recording system can be used to specify the ranges of both primary and secondary targets. Range relations

64. The variation in the seismic signal from a target as it travels along a given path is the result of a complex interaction of the target with the ground surface. Both the signal amplitude and frequency change as a function of range even if the ground parameters remain constant and the vehicle continues at the same speed. Data summarized from tests on good sites (Fort Bragg, North Carolina), poor sites (Fort Wainwright, Alaska), and computer study results suggest that an inversesquare relation can be used to estimate the relative sensor-to-target

ranges for the primary and secondary targets for the ranges of interest to REMBASS for both good and poor seismic sites. Thus, if the range (R) from target to sensor doubles, the signal amplitude is reduced approximately by a factor of four (for ground targets).

Target relations

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65. If only multiple targets of the same type were of interest, the $1/R^2$ relation could be used to set relations so that the dynamic range is not exceeded. Since targets of mixed types should be tested, a guide has been prepared to indicate relative amplitude between targets. In the tabulation below, the target seismic-signal amplitudes are normalized to the footstep-signal amplitudes (at the same range):

| | Normalized Amplitude |
|--------------------------|----------------------|
| Footstep | • 1 |
| Light wheeled vehicle (M | 10 |
| Heavy wheeled vehicle (M | 35) 20 |
| Light tracked vehicle (M | 113) 100 |
| Heavy tracked vehicle (M | 50A1) 150 |

66. The differences in signal amplitude shown in the tabulation above must be compensated for by a difference in range between the primary and secondary targets. Thus, if equal signal amplitudes are desired for a heavy tracked vehicle and a light wheeled vehicle for example, the heavy tracked vehicle must be run at a longer target-tosensor range than the light wheeled vehicle. The approximate range can be established by the $1/R^2$ relation as shown in the tabulation below.

Range for Secondary Target Amplitude to Equal Primary Target Amplitude

| | | Primary Tan | get at Range R ₁ | from Sensor | |
|--------------------------------|--|--|---|---|--|
| | Footstap | Light Wheeled M151 | Medium Wheelod M35 | Light Tracked M113 | lleavy Tracked <u>H60</u> |
| Footstep | $R_2 \sim R_1$ | $R_2 = R_1 / \sqrt{10}$ | $R_2 = R_1 / \sqrt{20}$ | $R_2 = R_1 / 10$ | $R_2 = R_1 / \sqrt{150}$ |
| Light Wheeled (M151) | $R_2 = \sqrt{10} R_1$ | $R_{2} = R_{1}$ | $R_2 = R_1/\sqrt{2}$ | $R_2 = R_1 / \sqrt{10}$ | $R_2 = R_1 / \sqrt{15}$ |
| Medium Wheeled (MJS) | $R_2 = \sqrt{20} R_1$ | $R_2 = \sqrt{2} R_1$ | $R_2 - R_1$ | $R_2 = \sqrt{0.2} R_1$ | $R_2 = \sqrt{2715} R$ |
| Light Tracked (N113) | $R_2 = 10 R_1$ | $R_2 - \sqrt{10} R_1$ | $R_2 = \sqrt{5} R_1$ | $R_2 - R_1$ | $R_2 = R_1 / \sqrt{1.5}$ |
| Heavy Tracked (M60) | $R_2 = \sqrt{150} R_1$ | P ₂ - 15 R ₁ | R ₂ - √7.5 R ₁ | $R_2 = \sqrt{1.5} R_1$ | R ₂ = R ₁ |
| | Fontstep Light Wheeled (M151) Medium Wheeled (M155) Light Tracked (M113) Heavy Tracked (M60) | Footstep Footstep $R_2 = R_1$ Light Wheeled (M151) Medium Wheeled (M35) Light Tracked (M113) R_2 = 10 R_1 Heavy Tracked (M60) $R_2 = \sqrt{150} R_1$ | Fontutep $R_2 = R_1$ $R_2 = R_1/\sqrt{10}$ Light Wheeled $R_2 = \sqrt{10} R_1$ $R_2 = R_1/\sqrt{10}$ Light Wheeled $R_2 = \sqrt{10} R_1$ $R_2 = R_1$ (M151) $R_2 = \sqrt{20} R_1$ $R_2 = \sqrt{2} R_1$ (M155) $R_2 = 10 R_1$ $R_2 = \sqrt{2} R_1$ Light Tracked $R_2 = 10 R_1$ $R_2 = \sqrt{10} R_1$ Heavy Tracked $R_2 = \sqrt{150} R_1$ $R_2 = \sqrt{15} R_1$ | Primary Target at Range R_1 Light Uncoled Medium Wheeled Missi Footstep Missi Missi Medium Missied Missi Footstep $R_2 = R_1$ $R_2 = R_1/\sqrt{10}$ $R_2 = R_1/\sqrt{20}$ Light Wheeled (Missi) $R_2 = \sqrt{10} R_1$ $R_2 = R_1/\sqrt{10}$ $R_2 = R_1/\sqrt{20}$ Light Wheeled (Missi) $R_2 = \sqrt{10} R_1$ $R_2 = R_1$ $R_2 = R_1/\sqrt{2}$ Medium Wheeled (Missi) $R_2 = \sqrt{20} R_1$ $R_2 = \sqrt{2} R_1$ $R_2 = R_1/\sqrt{2}$ Light Tracked (Missi) $R_2 = 10 R_1$ $R_2 = \sqrt{10} R_1$ $R_2 = \sqrt{5} R_1$ Heavy Tracked (M60) $R_2 = \sqrt{150} R_1$ $P_2 = \sqrt{15} R_1$ $R_2 = \sqrt{7.5} R_1$ | Primary Target at Range R ₁ from Sensor Light Wheeled Medium Light Tracked Footstep R ₂ = R ₁ R ₂ = R ₁ /./10 R ₂ = R ₁ /./20 R ₂ = R ₁ /10 Light Wheeled M13 M13 M113 Footstep R ₂ = R ₁ R ₂ = R ₁ /./10 R ₂ = R ₁ /./20 R ₂ = R ₁ /10 Light Wheeled (M151) R ₂ = ./10 R ₁ R ₂ = .R ₁ R ₂ = .R ₁ /./2 R ₂ = .R ₁ /./10 Medium Wheeled (M151) R ₂ = ./20 R ₁ |

Multiple-target test program

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67. Multiple-target signals are desirable as part of the AD design data bank because the unique combination of signal levels that can result from such tests may not be amenable to single-target processing techniques. Targets of interest for this data collection effort are: wheeled ground vehicles, tracked ground vehicles, men, rotary-wing aircraft, and fixed-wing aircraft. Three vehicles in each vehicle target class and one man should be used in the test program as summarized in Table 29. The site requirements, target travel modes, target combinations, and test iterations for the program are listed in Table 30. The site requirements were selected from those test conditions listed in paragraph 21.

68. The following paragraphs briefly discuss the site layout and additional details of the test program. It is felt that the magnitude of the test program outlined is in the proper order; however, some deviations from the test plan are expected as the test program progresses because some of the data specified will become obviously redurdant. Also, omissions will surface as the data are analyzed.

69. <u>Test layout</u>. The general test layout for multiple targets is shown in Figure 9. For each test two targets should be used, a primary target and a secondary target. As can be seen from Table 29, in part of the tests the primary and secondary vehicles can be the same type of vehicle (e.g. two Mil3 vehicles), but for most of the tests they should be different and represent all combinations of the listed targets. Note that during the conduct of a test, both high-level signals and low-level signals will be recorded at the same time depending on the ranges from targets to sensor and the type of target involved. An alternate walk path (path 2 for the walking-man target) is shown in Figure 9 and should be used as a substitute for the primary target path on the test lane when a high-signal-level condition for footsteps is desired. The gain of (ach recording channel should be set so that the primary target signal falls at approximately half of the dynamic range of each sensor channel. The secondary target signal will vary about this reference for all

secondary target ranges (even though some channels will be saturated for part of the run). The target and range relations listed in paragraph 66 can be used as a guide in selecting secondary target positions which will permit the collection of secondary target signals within the dynamic range of the recording system.

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70. Ground vehicles. All ground vehicle paths include an acceleration section, a constant-speed section, and a deceleration section, as shown in Figure 9. For the primary target and the secondary target, each of the three sections should be at least 100 m long (for some speeds the acceleration and deceleration sections will have to be longer than 100 m). All accelerations and decelerations for each test should be synchronized as closely as possible so that the vehicles enter and leave the constant-speed sections together. Signal recording should be initiated at the beginning of the acceleration period and continue through to the end of the deceleration period. The constant-speed section for the primary vehicle should be centered about the zero CPA point (i.e. +50 m on either side of the zero marker), and the constantspeed section for the secondary vehicle should start at the 50-, 200-, 500-, 1000-, and 2000-m stakes on the test lane (i.e. D = 50, 200, 500, and 2000 m in Figure 9). Ground vehicle speeds for the tests are shown in Table 30. One exception to these guidelines is that for the test in which the primary and secondary vehicles are the same and the secondary target test range is 50 m. In this case, the constant-speed section should be extended until the combined signal amplitudes decrease to the noise level of the recording system. Secondary target signal amplitudes should remain within the dynamic range of the recorder (once set for the primary target). Any secondary target ranges that produce signal amplitudes larger than that from the primary target (i.e. for both the highsignal-level and low-signal-level conditions) should be elimidated; any secondary target ranges that produce signal amplitudes below the noise level of the recorder (i.e. for both the high-signal-level and lowsignal-level conditions) should also be eliminated. These ranges can be estimated from relations discussed in paragraphs 64 and 65 and verified in the field by setting the dynamic range for the primary vehicle and

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monitoring the signal levels from the secondary vehicle as it moves from CPA out to the maximum range.

71. <u>Walking-man target</u>. The paths for the walking-man target can be much shorter than those specified for the vehicle targets, but should take approximately the same travel time. For example, a vehicle traveling over a 100-m section at a constant speed of 10 km/hr and a man walking a 40-m section will require approximately the same travel time. Also, since the walking man can quickly repeat the primary target path (for both the high- and low-signal-level conditions) by merely reversing his direction of travel, the secondary target can continue its travel over the complete secondary path at a constant speed without stopping.

72. <u>Aircraft</u>. Because of the much higher travel speeds of aircraft than of ground targets and because of the difficulty in controlling aircraft position precisely, aircraft should be tested as secondary targets only for all aircraft-vehicle target combinations. Any ground target tested with an aircraft target should be considered the primary target and be positioned in the primary target constant-speed section during the test. Each test should consist of a single pass of the aircraft at a constant speed and altitude as the ground target travels over its primary target path at a constant speed. Aircraft speeds and altitudes should be as shown in Table 30; they are identical to those for the single-target tests (Table 28).

73. Multiple aircraft tests should be conducted in the same manner as for ground target tests when the primary and secondary targets are the same (see paragraph 70). The aircraft should be synchronized so that they pass the CPA at different altitudes at the same time going in opposite directions. The recording should be continued until the combined signal level decreases to the recording noise level for both the 40-m and 500-m sensors.

74. <u>Summary</u>. Table 30 summarizes the multiple-target test program. A total of 2952 test runs are identified and made up of various combinations of targets (fourth column of Table 30 and the target type and target combination matrix shown in Table 29), site conditions, and target travel modes.

Background Noise Signitures

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75. Background noise signatures should be collected: (a) on an opportunity basis during the conduct of the previously described tests or enroute to these test areas, or (b) using a small sensor and recorder package at specific isolated noise sources. Signatures should be obtained for all cultural noise sources listed in Table 25 and as many of the natural sources as possible. The sensor systems used should include one triaxis geophone and an acoustic sensor located at ranges of 50, 200, and 1000 m from the noise source. The terrain conditions at each noise measurement area should be described according to the procedures outlined in Reference 3. Noise should be measured for a continuous 10-min segment of each hour of a period of 24 continuous hours. An effort should be made to obtain noise data in more than one terrain condition (perhaps two) from as many of the sources as possible.

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Figure 6. Sample locations, Fulda quadrangle

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Figure 7. Sampling template for identifying a mix of background noise sources

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Figure 9. Test layout for multiple-target test program (not to scale)

Table 1

Target Characteristics that Affect Vehicle Seismic

and Acoustic Signatures

Wheeled Ground-Contact Vehicles

Weight (empty)

Payload

Number of wheels

Tire size(s)

Number of tire lugs per wheel

Tire pressure

fread depth (average)

Ground-contact area

Number of teeth in the axle gear in the final drive differential

Final drive differential gear ratio

Engine rpm versus vehicle speed curves for all gears. Vehicle should be loaded and run on level terrain at speeds up to 60 km/hr

Engine model

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(1) Horsepower

- (2) Number of cylinders
- (3) Number of cycles
- (4) Fuel type
- (5) Cooling type
- (6) Location of exhaust
- (7) Number of blades in cooling fan
- (8) Ratio of fan rpm to engine rpm

Suspension type, i.e. whether the vehicle has:

- (1) Independent suspension
- (2) No suspension, or any combination of independent and no suspension
- (3) Bogie, walking-beam, or any combination of independent, bogie, and walking-beam
- (4) Any combination of (1), (2), and (3)

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(Continued)

(Sheet 1 of 4)

Table 1 (Continued)

Wheeled Ground-Contact Vehicles (Continued)

Weight (kg) of unsprung mass, i.e. the weight of each wheel assembly. For a solid-axle suspension, use one-half weight of each axle assembly; for no suspension, use zero weight

Longitudinal distance(s) (cm) of each wheel center from the center of gravity

Static tire deflection at normal (or noted) tire pressure at combat load Pitch inertia (kg-sec²-cm) of sprung mass about center of gravity

Longitudinal distance(s) (cm) of driver from center of gravity

For each suspension unit (wheel assembly), complete suspension spring force-deflection relations from rebound to full bump

Tracked Ground-Contact Vehicles

Weight (empty)

Payload

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Track pitch

Track width

Truck condition, i.e., actual dimensions of track pads, number and location of broken shoes, etc.

Number of track pads on each side in contact with ground

Number of teeth on the track sprocket gear

Number of teeth in the axle gear in the final drive differential

Final drive differential gear ratio

Engine rpm versus vehicle speed curves for all gears. Vehicle should be loaded and run on level terrain at speeds up to 60 km/hr

Engine model

- (1) Horsepower
- (2) Number of cylinders
- (3) Number of cycles
- (4) Fuel type
- (5) Cooling type

(Continued)

(Sheet 2 of 4)

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Table 1 (Continued)

| | Tracked Ground-Contact Vehicles (Continued) |
|----------------------------|---|
| Engine model | (Continued) |
| (6) Numb | er of blades in the cooling fan |
| (7) Rati | o of fan rpm to engine rpm |
| Suspension t | ype, i.e. whether the vehicle has: |
| (1) Inde | pendent suspension |
| (2) No s susp | uspension, or any combination of independent and no ension |
| (3) Bogi and | e, walking-beam, or any combination of independent, bogie, walking-beam |
| (4) Any | combination of (1), (2), and (3) |
| Weight (kg) and one-ha | of unsprung mass, i.e., weight of the road wheel or bogic lf weight of the track |
| Longitudinal gravity | distance(s) (cm) of each wheel center from the center of |
| Pitch inerti | a (kg-sec ² -cm) of sprung mass about center of gravity |
| Longitudinal | distance(s) (cm) of driver from center of gravity |
| For each sus force-defl | pension unit (wheel assembly), complete suspension spring ection relations from rebound to full bump |
| For each sus both in jo | pension unit with damping, complete force-velocity relations unce and rebound |
| The length (beneath th | cm) along the leading portion of the track, measured from e leading road wheel to the foremost part of the track |
| The approach the leadin | angle (deg) (angle determined by a horizontal line beneath g road wheel and the leading force of the track) |
| Normal opera | ting track tension (static) |
| | 1 |
| | Rotary-Wing and Fixed Aircraft |

Payload

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Number of engines

(Continued)

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(Sheet 3 of 4)

Table 1 (Concluded)

Rotary-Wing and Fixed Aircraft (Continued)

Engine specifications:

- (1) Type, i.e. turbine or piston engine
- (2) Model

- (3) Horsepower
- (4) Number of cylinders
- (5) Fuel type
- (6) Type of cooling
- (7) Exnaust configuration and location
- (8) Number of fan blades

(Sheet 4 of 4)

| | | Nomenclature of U. S. Wheeled Vehicles |
|-----|--------|--|
| 1. | ML | 33. M43E1 |
| 2. | MLAL | 34. M43E2 |
| 3. | M6 | 35. M44 |
| 4. | M20 | 36. M44A1 |
| 5. | 1126 | 37. M44A2 |
| 6. | M26A1 | 38. M44C |
| 7. | M27 | 39. M45 |
| 8. | M27B1 | 40. M45A1 |
| 9. | M34 | 41. M45A2 |
| 10. | M35 | 42. M45A2G |
| 11. | M35A1 | 43. M45C |
| 12. | M35A2 | 44. M46 |
| 13. | M35A2C | 45. M46A1C |
| 14. | M36 | 46. M46A2C |
| 15. | M36A1 | 47. M46C |
| 15. | M36A2 | 48. M47 |
| 17. | M36C | 49. M48 |
| 18. | M37 | 50. M48A2 |
| 19. | M37B1 | 51. M49 |
| 20. | M38 | 52. M49A1C |
| 21. | M38A1 | 53. M49A2C |
| 22. | M38A1C | 54. M49C |
| 23. | M38A1D | 55. M50 |
| 24. | M39 | 56. M50A1 |
| 25. | M40 | 57. M50A2 |
| 26. | M40A2 | 58. M51 |
| 27. | M40A2C | 59. M51A1 |
| 28. | M40C | 60. M51A2 |
| 29. | M41 | 61. M52 |
| 30. | M42 | 62. M52A1 |
| 31. | M43 | 63. M52A2 |
| 32. | M43B1 | 64. M53 |
| | | |

Table 2

. M. (Continued)

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(Sheet 1 of 4)

Table 2 (Continued)

| 65. | M53B1 | 99. | M113A1 |
|-----|--------|------|---------|
| 66. | M54 | 100. | M114 |
| 67. | M54A1 | 101. | M121 |
| 68. | M54A1C | 102. | M123 |
| 69. | M54A2 | 103. | M123A1C |
| 70. | M54A2C | 104. | M123C |
| 71. | M55 | 105. | M123D |
| 72. | M55AL | 106. | XM123E2 |
| 73. | M55A2 | 107. | M125 |
| 74. | M56 | 108. | M125A1 |
| 75. | M56B1 | 109. | XM125E1 |
| 76. | M56C | 110. | M133 |
| 77. | M57 | 111. | M135 |
| 78. | M58 | 112. | M139 |
| 79. | N59 | 113. | M139C |
| 80. | M60 | 114. | XM142 |
| 81. | M61 | 115. | XM145 |
| 82. | M61A2 | 116. | XM147E3 |
| 83. | M62 | 117. | M151 |
| 84. | M63 | 118. | M151A1 |
| 85. | M63A2 | 119. | M151A1C |
| 86. | M63A2C | 120. | M151A2 |
| 87. | M63C | 121. | XM151 |
| 88. | M106 | 122. | XM151E1 |
| 89. | M107 | 123. | XM151E2 |
| 90. | M108 | 124. | XM157 |
| 91. | M109 | 125. | M170 |
| 92. | M109A1 | 126. | XM190 |
| 93. | M109A2 | 127. | XM191 |
| 94. | M109A3 | 128. | M201 |
| 95. | M109C | 129. | M201B1 |
| 9ó. | M1090 | 130. | M207 |
| 97. | M110 | 131. | M207C |
| 98. | м113 | 132. | XM207 |
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|------|---------|------|---------|
| 133. | M209 | 167. | M292A1 |
| 134. | M211 | 168. | M292A2 |
| 135. | M215 | 169. | M292A3 |
| 136. | M217 | 170. | M292A4 |
| 137. | M217C | 171. | M292A5 |
| 138. | M220 | 172. | M328A1 |
| 139. | M220C | 173. | M342 |
| 140. | M220D | 174. | M342A2 |
| 141. | M221 | 175. | XM342 |
| 142. | M222 | 176. | M343A2 |
| 143. | M246 | 177. | XM357 |
| 144. | M246A1 | 178. | XM375 |
| 145. | M246A2 | 179. | XM376 |
| 146. | M249 | 180. | XM377 |
| 147. | XM249 | 181. | XM381 |
| 148. | M250 | 182. | XM384 |
| 149. | XM250 | 183. | XM401 |
| 150. | M274 | 184. | XM408 |
| 151. | M274A1 | 185. | XM410 |
| 152. | M274A2 | 186. | M422 |
| 153. | M274A3 | 187. | M422A1 |
| 154. | M274A5 | 188. | M425 |
| 155. | M275 | 189. | M426 |
| 156. | M275A1 | 190. | M427 |
| 157. | M275A2 | 191. | XM434E1 |
| 158. | XM282 | 192. | XM434E2 |
| 159. | XM282E2 | 193. | XM437 |
| 160. | XM282E3 | 194. | XM437E1 |
| 161. | M291A1 | 195. | XM437E2 |
| 162. | M291ALD | 196. | XM438E2 |
| 163. | M291A2 | 197. | XM443 |
| 164. | M291A2C | 198. | XM453E1 |
| 165. | M291A2D | 199. | XM453E2 |
| 166. | M292 | 200. | XM453E3 |
| | | | |

(Continued)

See.

Table 2 (Continued)

(Sheet 3 of 4)

| | | Table 2 (Conc | luded) | | |
|-------------|---------|---------------|--------|------|---------|
| 201. | XM512 | 235. | M618 | 269. | M820A2 |
| 202. | XM512E1 | 236. | M619 | 270. | M821 |
| 203. | XM512E2 | 237. | M621 | 271. | M825 |
| 204. | XM512E3 | 238. | M622 | 272. | M1185A3 |
| 205. | XM512E4 | 239. | M623 | 273. | V-100 |
| 206. | XM520 | 240. | M624 | | |
| 207. | XM520E1 | 241. | M656 | | |
| 208. | XM521 | 242. | XM656 | | |
| 209. | XM523 | 243. | M708 | | |
| 210. | XM523E2 | 244. | M708A1 | | |
| !11. | XM531 | 245. | M711 | | |
| 212. | M535 | 246. | M715 | | |
| .13. | M543 | 247. | M718 | | |
| 214. | M543A1 | 248. | M718A1 | | |
| 215. | M543A2 | 249. | M724 | | |
| 16. | M548 | 250. | M725 | | |
| 17 . | M551 | 251. | M726 | | |
| 18. | M553 | 252. | M746 | | |
| 19. | XM554 | 253. | M748A1 | | |
| 20. | M559 | 254. | M751A1 | | |
| 21. | M561 | 255. | M757 | | |
| 22. | XM561 | 256. | M764 | | |
| 23. | M577 | 257. | XM791 | | |
| 24. | M578 | 258. | M792 | | |
| 25. | M602 | 259. | M813 | | |
| 26. | M607 | 260. | M813A1 | | |
| 27. | M609A1 | 261. | XM813 | | |
| 28. | M610 | 262. | M814 | | |
| 29. | M611 | 263. | M815 | | |
| 30. | M611C | 264. | M816 | | |
| 31. | M613 | 265. | M817 | | |
| 32. | M614 | 266. | M818 | | |
| 33. | M616 | 267. | M819 | | |
| 34. | M617 | 268. | M820 | | |

(Sheet 4 of 4)

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| Vehicle Code No. | Model No. |
|------------------|------------------|
| 1 | GAZ(UAZ)-69 |
| 2 | GAZ-62 |
| 3 | маг-205 |
| 4 | KRAZ-214 |
| 5 | ZIL-157 K |
| 6 | ZIL-583 |
| 7 | GAZ-56 |
| 8 | ZIL-164 |
| 9 | MAZ-502 |
| 10 | UAZ-450D |
| 11 | URAL-355M |
| 12 | ZIL-131 |
| 13 | URAL-375 |
| 14 | URAL-375D |
| 15 | KRAZ-222 |
| 16 | KRAZ-219 |
| 17 | KAZ-605 |
| 18 | GAZ-66 |
| 19 | MAZ-500A |
| 20 | UAZ-452D |
| 21 | GAZ-53F |
| 22 | MAZ-505 |
| 23 | ZAZ-971 |
| 24 | ZIL-135 |
| 25 | MAZ-535A |
| 26 | MAZ-543 |
| 27 | ZIL-E-167 |
| 28 | MAZ-514 |
| 29 | BELAZ-548 |
| 30 | TZ-200 |
| | (Continued) |

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Table 3

Nomenclature of USSR Wheeled Vehicles

(Sheet 1 of 5)

| Vehicle Code No. | Model No. |
|------------------|-------------|
| 31 | ATS-8-200 |
| 32 | ATSM-4-157 |
| 33 | ATZ-3-157 |
| 34 | ATZ-4-164 |
| 35 | UAZ-469 |
| 36 | ZAZ-969 |
| 37 | ZIL-133 |
| ~ 38 | BELAZ-540 |
| 39 | MOAZ-522 |
| 40 | UMZ-ZIL-151 |
| 41 | MAZ-503 |
| 42 | PSG-65/130 |
| 43 | KRAZ-255B |
| 44 | PSG-160 |
| 45 | GAZ~SAZ-53B |
| 46 | NAMI-076 |
| 47 · | TZ-63 |
| 48 | TZ-150 |
| 49 | ATSM-4-150 |
| 50 | ATZ-3-151 |
| 51 | MZ-51 |
| 52 | MZ-150 |
| 53 | MI-964 |
| 54 | ATZ-3.8-130 |
| 55 | ATS-26-355M |
| 56 | MAZ-200V |
| 57 | GAZ-63P |
| 58 | KRAZ-221 |
| 59 | GAZ-53P |
| 60 | ZIL-164AN |
| 61 | KAZ-606A |
| 62 | GAZ-51P |
| 63 | MAZ-537 |
| (Continue) | 4) |

Table 3 (Continued)

(Sheet 2 of 5)

า ในไม่แนะประเทศสาราส์หนึ่งให้หน้าสาราวิจารีการการการการการสาราส์สาราส์ที่สาราส์หน

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| Vehicle Code No. | Model No. |
|------------------|-------------------|
| 64 | ZIL-133V |
| 65 | KRAZ-258 |
| 66 | KAZ-608B |
| 67 | ZIL-137 |
| 68 | ZIL-131V |
| 69 | MAZ-529 |
| 70 | URAGAN-8 |
| 71 | ZIL-157KV |
| 72 | ZIL-130V1 |
| 73 | KAZ-608 |
| 74 | MAZ-504 |
| 75 | URAL-3778 |
| 76 | URAL-375S |
| 77 | GAZ-93A |
| 78 | KAZ-600AV |
| 79 | ZIL-MMZ-585L,585M |
| 80 | ZIL-MMZ-555 |
| 81 | 11 AZ-503A |
| 82 | GAZ-53B |
| 83 | KRAZ-256B |
| 84 | MAZ-525 |
| 85 | MAZ-530 |
| 86 | BELAZ-548A |
| 87 | GAZ-69 |
| 88 | GAZ-69A |
| 89 | GAZ-63 |
| 90 | GAZ-63A |
| 91 | MAZ-501 |
| 92 | ATS-51A |
| 93 | ATSPT-1.9 |
| 94 | AVV-2 |
| 95 | ATZ-2.2-51A |
| 96 | ATZ-3.8-53A |

Table 3 (Continued)

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(Sheet 3 of 5)

| e Code No. | Model No. |
|------------------|---------------|
| 97 | ATSM-4-157K |
| 98 | ATS-1.9-51A |
| 99 | ATS-2.6-355M |
| 100 | ATS-2.6-53F |
| 101 | ATS-2.9-53F |
| 102 | ATS-4.2-53A |
| L03 | ATS-4.2-130 |
| 104 | MZ-51M |
| 105 | ATSPT-1.7 |
| L06 [.] | ATSPT-1.9 |
| 107 | ATSPT-2.8 |
| 108 | ATSPT-5.6 |
| 109 | AVTS-1.7 |
| L10 | AVV-2 |
| 111 | S-9 56 |
| 112 | GAZ-67B |
| 113 | GAZ-46 |
| 114 | UAZ-450A |
| L15 | UAZ-452A,452E |
| L16 | KMAZ-5410 |
| 117 | KMAZ-5510 |
| 118 | KMAZ-53202 |
| 119 | UAZ-4510 |
| 120 | MAV (GAZ)-46 |
| 121 | BAV-485 |
| 122 | GAZ-51 |
| 123 | ZIL-150 |
| 124 | ZIL-151 |
| 125 | ZIL-137 |
| 126 | BTR-60P |
| 27 | BTR-152 |

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Table 3 (Continued)

(Continued)

(Sheet 4 of 5)

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| Vehicle Code No. | Model No. |
|------------------|------------------|
| 128 | BRDM SCOUT CAR |
| 129 | BRDM-2 SCOUT CAR |
| 130 | BM-14 |
| 131 | BM-21 |
| 132 | BRDM (SNAPPER) |
| 133 | BA 64 |
| 134 | BTJ -40 |
| 135 | BTR-152VI |
| 136 | BTR-60P |
| 137 | BRDM |
| [′] 138 | MAZ-535 |
| 139 | T-111 |
| 140 | T-138 |
| 141 | T-1141 |
| 142 | ARS-12/14 |
| 143 | DDA-53 |
| 144 | KRAZ-255 |
| 145 | от-64 |
| 146 | OT-65 |
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Table 3 (Concluded)

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(Sheet 5 of 5)

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| Vehicle Code No. | Model No. | |
|------------------|-----------------|--|
| 1 | т6 | |
| 2 | T23 | |
| 3 | T23E3 | |
| 4 | T25 | |
| 5 | T48 | |
| 6 | T 74 | |
| 7 | M3A3 (light) | |
| 8 | M3A3 | |
| 9 | M3A2 | |
| 10 | M3A3 (medium) | |
| 11 | M3A4 | |
| 12 | M3A5 | |
| 13 | M4 (full track) | |
| 14 | M8 | |
| 15 | M10 | |
| 16 | M48A1 | |
| 17 | M56 | |
| 18 | M60 | |
| 19 | M103 | |
| 20 | M2 | |
| 21 | M3 | |
| 22 | M4 (half track) | |
| 23 | LVT1 | |
| 24 | LVT2 | |
| 25 | LVTA2 | |
| 26 | LVTAL | |
| 27 | LVTA4 | |
| 28 | LVTA5 | |
| 29 | M29 | |
| 30 | M29C | |
| 31 | M76 | |
| (Continued) | | |

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Nomenclature of U. S. Tracked Vehicles

Table 4

(Sheet 1 of 4)

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| Vehicle Code Nc. | Model No. | |
|------------------|--------------------|--|
| 32 | M59 | |
| 33 | M75 | |
| 34 | T113E2, M113 | |
| 35 | MK4, LVT4 | |
| 36 | M51 | |
| 37 | M74 | |
| 38 | M88 | |
| 39 | M41 | |
| 40 | M41A1 | |
| 41 | M41A2 | |
| 42 | M41A3 | |
| 43 | M47 | |
| 44 | M48 | |
| 45 | M48C | |
| 46 | M48A2 | |
| 47 | M48A2C | |
| 48 | M5 | |
| 49 | M5-A1 | |
| 50 | M5-A2 | |
| 51 | M5-A3 | |
| 52 | M5-A4 | |
| 53 | MK5, LVTA-5 | |
| 54 | M24 | |
| 55 | M4A1 (w/75-mm gun) | |
| 56 | M4A3 (w/75-mm gun) | |
| 57 | T41E1 | |
| 58 | M4Al (w/76-mm gun) | |
| 59 | M4A3 (w/76-mm gun) | |
| 60 | M26 | |
| 61 | M26A1 | |
| 62 | M46 | |
| 63 | M46A1 | |
| | (Continued) | |
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Table 4 (Continued)

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(Sheet 2 of 4)

| Table 4 (Continued) | | |
|---------------------|----------------------------|--|
| Vehicle Code No. | Modal No. | |
| 64 | M4 (full track) | |
| 65 | M4A3 $(w/105-mm howitzer)$ | |
| 66 | M45 | |
| 67 | M8E2 | |
| 68 | M4 | |
| 69 | M4A1 | |
| 70 | M4C | |
| 71 | M4AJ.C | |
| 72 | м6 | |
| 73 | T18E1 | |
| 74 | M32 | |
| 75 | м39 | |
| 76 | M2A1 | |
| 77 | M16 | |
| 78 | M15A1 | |
| 79 | M19AL | |
| 80 | M18 | |
| 81 | М36 | |
| 82 | M36B1 | |
| 83 | M36B2 | |
| 84 | M7 | |
| 85 | M7B1 | |
| 86 | M37 | |
| 87 | r106 | |
| 88 | M40 | |
| 89 | M41 | |
| 90 | M43 | |
| 91 | T46E1 | |
| 92 | M3A1 | |
| 93 | M4AL | |
| 94 | M21 | |
| 95 | T16 | |
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| Vehicle Code No. | Model No. |
|------------------|-----------|
| 96 | M60A1 |
| 97 | M48A3 |
| 98 · | M551 |
| 99 | M114A1 |
| 100 | M113A1 |
| 101 | LVTP-7 |
| 102 | M42 |
| 103 | M110 |
| 104 | M55 |
| 105 | M107 |
| 106 | M109 |
| 107 | M53 |
| 108 | M44 |
| 109 | M108 |
| 110 | M52 |

Table 4 (Concluded)

(Sheet 4 of 4)

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| | | _ |
|------------------|-------------------|---|
| Vehicle Code No. | Model No. | |
| 1 | T54, T55 | |
| 2 | T-62 | |
| 3 | BTR | |
| 4 | M-1967 | |
| 5 | 2SU-57/2 | |
| 6 | ZSU-23/4 | |
| 7 | BM-24 | |
| 8 | BTU | |
| 9 | BAT/M | |
| 10 | MTU-54 | |
| 11 | Mineclearing Tank | |
| 12 | K-61 | |
| 13 | PTS/M | |
| 14 | GAZ-47 | |
| 15 | GAZ-71 | |
| 16 | K-61 | |
| 17 | PTS | |
| 18 | GT-T | |
| 19 | V-1, VITYAZ | |
| 20 | AT-L | |
| 21 | AT-S | |
| 22 | ATS-59 | |
| 23 | AT-T | |
| 24 | т-34 | |
| 25 | T-54-T | |
| 26 | JSU-T-B | |
| 27 | JSU-TE | |
| 28 | т-54А | |
| 29 | JS-3 | |
| 30 | T10-M | |
| 31 | PT76 | |
| | (Continued) | |

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| Table | 5 |
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Nomenclature of USSR Tracked Vehicles

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(Sheet 1 of 3)

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| Vehicle Code No. | Model No. |
|------------------|--------------|
| 32 | т54 |
| 33 | SU-37 |
| 34 | SU85 |
| 35 | SU-100 |
| 36 | JSU-122 |
| 37 | JSU-152 |
| 38 | T60 |
| 39 | T70 |
| 40 | KW11 |
| 41 | JS-Z |
| 42 | ASU-57 |
| 43 | ASU-85 |
| 44 | ZSU-57-2 |
| 45 | ZSU-23-4 |
| 46 | BTR-50PK |
| 47 , | BTR-40 |
| 48 | M1967 |
| 49 | AT-P |
| 50 | GAS-47 |
| 51 | T-80 |
| 52 | PT-76 |
| 53 | PT-85 |
| 54 | T-34/76 |
| 55 | T-34/85 |
| 56 | T -44 |
| 57 | T-54 |
| 58 | T-55 |
| 59 | T-62 |
| 60 | T-100 |
| 61 | KV |
| 62 | KV85 |
| 63 · | JSI, II, III |
| (Cor | ntinued) |

Table 5 (Continued)

(Sheet 2 of 3)

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| Vehicle Code No. | Model No. |
|------------------|-----------------|
| 64 | T-10 |
| 65 | SU-76 |
| 66 | SU-122 |
| 67 | SU-152 |
| 68 | BMP-76PB |
| 69 | V-1, VITYAZ |
| 70 | Carrier Penguin |
| 71 | Carrier Utility |
| 72 | GT-SM |
| 73 | GAZ-71 |
| 74 | M-1970 |
| 75 | OT-62B |
| 76 | M-70 |
| 77 | M-1973 |
| 78 | M-1974 |
| 79 | 0 T -62C |

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Table 5 (Concluded)

(Sheet 3 of 3)

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| Table 6 |) |
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| Vehicle Code No. | Model No. |
|------------------|-----------|
| 1 | UH-1F |
| 2 | нн-1к |
| 3 . | UH-1L |
| 4 | UH-1H |
| 5 | UH1N |
| 6 | AH-1G |
| 7 | TH-1L |
| 8 | OH-13S |
| 9 | AH-1J |
| 10 | TH-13J |
| 11 | TH-57A |
| 12 | OH-58A |
| 13 | QH-50D |
| 14 | TH-55A |
| 15 | OH-6A |
| 16 | НИ-43В |
| 17 | HH-43F |
| 18 | UH-2C |
| 19 | HH-2D |
| 20 | SH-2D |
| 21 | HH-2C |
| 22 | SH-2F |
| 23 | CH-3B |
| 24 | SH-3D |
| 25 | CH-3E |
| 26 | HH-52A |
| 27 | CH-54A |
| 28 | CH-54B |
| 29 | CH-53A |
| 30 | НН-53С |
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Nomenclature of U. S. Rotary-Wing Aircraft

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| Table 6 | (Concluded) |
|---------|-------------|
|---------|-------------|

| Vehicle Code No. | Model No. |
|------------------|-----------|
| 31 | CH-53D |
| 32 | RH-53D |
| 33 | CH-46F |
| 34 | CH-47C |
| 35 | CH-34C |
| 36 | OH-23D |

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|--|--------------|--|
| Code | Design: :ion | NATO Code Name |
| 1 | V-12(Mi-12) | Homer |
| 2 | Mi-10 | Harke |
| 3 | Mi-8 | Hip |
| 4 | Mi6 | Hook |
| 5 | MI-4 | Hound |
| 6 | Mi-2 | Hoplite |
| 7 | Ka-26 | Hoodlum |
| 8 | Ka-25K | Hormone |
| 9 | Ka~20 | Harp |
| 10 | Ka-18 | Hog |
| | Yak-24 | |
| 12 | Ka-15 | Hen |
| 12 | v=_72 | |
| 22 | NG-22 | |

Table 7

Nomenclature of USSR Rotary-Wing Aircraft

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| Nomenclature of U. | S. Fixed-Wing Aircraft | |
|--------------------|------------------------|---|
| | | _ |
| Vehicle Code No. | Model No. | |
| 1 | АЗВ | |
| 2 | A-4F | |
| 3 | A-4M | |
| · 4 | A-6A | |
| 5 | A-7D | |
| 6 | A-7E | |
| 7 | AV-8A | |
| 8 | A-37B | |
| 9 | A-10 | |
| 10 | B-52F | |
| 11 | B-52G | |
| 12 | B-52H | |
| 13 | B-66D | |
| 14 | FB-111A | |
| 15 | B-1 | |
| 16 | F-101B | |
| 17 | F-102A | |
| 18 | F-104C | |
| 19 | F-104G | |
| 20 | F-105D | |
| 21 | F-106A | |
| 22 | F-111F | |
| 23 | F-4J | |
| 24 | F-4E | |
| 25 | F-5A/B | |
| 26 | F-5E | |
| 27 | F-8J | |
| 28 | XFV-12A | |
| 29 | F-14A | |
| 30 | F-15A | |
| (Con | tinued) | |

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Table 8

(Sheet 1 of 4)

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| • | Table 8 (Conti | nued) |
|------------------|----------------|----------|
| | | |
| Vehicle Code No. | Mo | odel No. |
| 31 | | P-530 |
| 32 | | YF-16 |
| 33 | | YF-17 |
| 34 | | WU/U-2 |
| 35 | | SR-71 |
| 36 | | RF-46 |
| 37 | | RA-5C |
| 38 | | RB-57F |
| 39 | | 0-1G |
| 40 | | 0-2A |
| 41 | | OV-1A |
| 42 | | OV-10A |
| 43 | | Y0-3A |
| 44 | | P-2H |
| 45 | | P-3C |
| . 46 | | S-2E |
| 47 | | S-3A |
| 48 | | E-1B |
| 49 | | E-2B |
| 50 | | E-3A |
| 51 | | E-4A |
| 52 | | C-121G |
| 53 | | C-130B |
| 54 | | C-130E |
| 55 | | нс-130н |
| 56 | | C-131E |
| 57 | | KC-135A |
| 58 | | VC-137C |
| 59 | | C-140A |
| . 60 | | C-141A |
| 61 | | C-1A |
| | (Continued) | |

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(Sheet 2 of 4)

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| Vehicle Code No. | Model No. |
|------------------|--------------|
| .62 | C2A |
| 63 | C-7A |
| 64 | C-8A |
| 65 | C-5À |
| 66 | VC-6B |
| . 67 | C-9A |
| 68 | C-9B |
| 69 | T-2C |
| 70 | T-28D |
| 71 | T-29D |
| 72 | T-33A |
| 73 | т-34в |
| 74 | т-37в |
| 75 | T-38A |
| 76 | T-39A |
| 77 | T-41A |
| 78 | T-42A |
| 79 | TC-4C |
| 80 | T-43A |
| 81 | U-1A |
| 82 | U-3B |
| 83 | U-4B |
| 84 | U-5A |
| 85 | U-6A |
| 86 | U-7A |
| 87 | U-8D |
| . 83 | U-8F |
| 89 | U-10D |
| 90 | U-11A |
| 91 | HU-16A/E |
| 92 | U-17A |
| | (Continued) |

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Table 8 (Continued)

(Sheet 3 of 4)

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| Vehicle Code No. | Model No. | |
|------------------|-----------------|--|
| 93 | U-21A | |
| 94 | U-21F | |
| 95 | AU-23A | |
| 96 | AU-24A | |
| 97 | ҮС-119 К | |
| 98 | AC-119K | |
| 99 | A-6E | |
| 100 | VC-11A | |
| 101 | X-24B | |
| 102 | YE-5 | |
| 103 | U-9C | |
| 104 | U-21A | |

Table 8 (Concluded)

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| | Nomenclature of USSR Fixed-Wing | Aircraft |
|---------|---------------------------------|----------------|
| Code | Designation | NATO Code Name |
| L | TU-22 | Blinder |
| 2 | TU-? | Backfire |
| 3 | N-4 | Bison |
| , -+ | Tu-95 | Bear |
| 5 | Tu-16 | Badger |
| 6 | 11-28 | Beagle |
| 7 | Yak-28 | Brewer |
| 8 | Be-10 | Mallow |
| 9 | Be-12 | Mail |
| 10 | Yak-? | Mandrake |
| 11 | Yak-25 | Mangrove |
| 12 | MiG-25 | Voxbat |
| 13 | MiG-25 | |
| 14 | MiG-25 | |
| 15 | MiG-23 | Flogger |
| 16 | MiG-? | Faithless |
| 17 | MiG-? | Flipper |
| 18 | MiC-21 | Fishbed G |
| 19 | MiG-21 | Fishbed F/J/K |
| 20 | MiG-21 | Fishbed D/H |
| 、 21 | MiG-21 | Fishbed C |
| 22 | MiG-19 | Farmer |
| 23 | ri1G-17 | Fresco |
| 24 | Su-J.1 | Flagon A |
| 25 | Su-? | Flagon B |
| 26 | Su-? | Fitter B |
| 27 | Su-7 | Fitter |
| 28 | Su- 9 | Fishpot |
| 29 | Tu-29 P | Fiddler |
| 30 | Yak-? | Freehand |
| 31 | Yak-23P | Firebar |
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Sim Scieles

| CodeDesignationNATO Code Name32An-26Coke33An-24VCoke34An-22Coka35An-14Clod36An-12Cub37An-10Cat38M-1539Be-30Cuff40I1-8641I1-62Classic43I1-62M200Classic44I1-18VCoot45I1-14Crate46I1-14NCrate47I1-12Coach48Tu-154ACareless50Tu-144Charger51Tu-134Crusty52Tu-134ACrusty53Tu-104ACaael A56Tu-104BCaael A57Yak-40Coding58Yak-40MCoding59Yak-33Martis61Yak-30Magnum62Yak-18764AN-10Janes | · | | |
|---|------------|------------------|----------------|
| 32 An-26 Coke 33 An-24V Coke 34 An-22 Coka 35 An-14 Clod 36 An-12 Cub 37 An-10 Cat 38 M-15 39 Be-30 Cuff 40 I1-86 41 I1-76 Cadid 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-14N Crate 46 I1-14N Crate 47 I1-12 Coach 48 Tu-154A Careless 50 Tu-144 Charger 51 Tu-134A Crusty 52 Tu-104A Camel A 53 Tu-104A Camel A 56 Tu-104B Cading 57 Yak-40 Coding 58 Yak-40M Coding 57 Yak-32 Martis 58 Yak-34 Ma | Code | Designation | NATO Code Name |
| 33An-24VCoke34An-22Coke35An-14Clod36An-12Cub37An-10Cat38M-1539Be-30Cuff40II-8641II-76Candid42II-62Classic43II-62M200Classic44I1-18VCoot45I1-14Crate46I1-14MCrate47I1-12Coach48Tu-154ACareless50Tu-144Charger51Tu-134Crusty52Tu-134Crusty53Tu-104ACakel A56Tu-104BCamel B57Yak-40Coding58Yak-32Mantis61Yak-33Max62Yak-18764AN-10Janes | 32 | An-26 | Coke |
| 34 An-22 Coke 35 An-14 Clod 36 An-12 Cub 37 An-10 Cat 38 M-15 39 Be-30 Cuff 40 I1-86 41 I1-76 Candid 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-18V Coot 45 I1-14 Crate 46 I1-14M Crate 47 I1-12 Coach 48 Tu-154A Careless 49 Tu-154A Careless 50 Tu-134 Crusty 51 Tu-134 Crusty 52 Tu-104A Camel A 55 Tu-104B Camel A 56 Tu-104B Camel A 56 Tu-104B Cadel B 57 Yak-40 Coding 58 Yak-32 Mantis 59 Yak-18T | 33 | An-24V | Coke |
| 35 An-14 Clod 36 An-12 Cub 37 An-10 Cat 38 N-15 39 Be-30 Cuff 40 I1-86 41 I1-76 Candid 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-18V Coot 45 I1-14 Crate 46 I1-14N Crate 47 I1-12 Coach 48 Tu-154 Careless 49 Tu-154 Careless 50 Tu-134 Crusty 51 Tu-134 Crusty 52 Tu-104A Camel A 53 Tu-104A Camel A 56 Tu-104B Cading 57 Yak-40 Coding 58 Yak-32 Mantis 51 Yak-30 Magnum 52 Yak-187 50 Yak-32 M | 34 | An-22 | Coke |
| 36 An-12 Cub 37 An-10 Cat 38 M-15 39 Be-30 Cuff 40 I1-86 41 I1-76 Candid 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-18V Coot 45 I1-14 Crate 46 I1-14N Crate 47 I1-12 Coach 48 Tu-154 Careless 49 Tu-144 Charger 50 Tu-144 Crusty 51 Tu-134A Crusty 52 Tu-134A Crusty 53 Tu-144 Cleat 54 Tu-144 Cleat 55 Tu-144 Cookpot 54 Tu-144 Cleat 55 Tu-144 Cleat 56 Tu-144 Cleat 56 Tu-104A Camel A 56 Tu-104B Camel A 56 | 35 | An-14 | Clod |
| 37An-10Cat38N-1539Be-30Cuff4011-864111-76Candid4211-62Classic4311-62M200Classic4411-18VCoot4511-14Crate4611-14MCrate4711-12Coach48Tu-154ACareless50Tu-144Charger51Tu-134ACrusty52Tu-134ACowpot54Tu-104ACamel A55Tu-104ACamel A56Tu-104BCamel B57Yak-40Coding58Yak-40MCoding59Yak-32Mantis61Yak-30Magnum62Yak-18764AN-10Janes | 36 | An-12 | Cub |
| 38 N-15 39 Be-30 Cuff 40 I1-86 41 I1-76 Candid 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-18V Coot 45 I1-14 Crate 46 I1-14N Crate 47 I1-12 Coach 48 Tu-154 Careless 50 Tu-154A Charger 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-104A Camel A 55 Tu-104A Canel A 56 Tu-104B Cading 57 Yak-40 Coding 58 Yak-32 Mantis 59 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-187 64 AN-10 Janes | 37 | An-10 | Cat |
| 39 Be-30 Cuff 40 11-86 41 11-76 Candid 42 11-62 Classic 43 11-62M200 Classic 44 11-18V Coot 45 11-14 Crate 46 11-14M Crate 47 11-12 Coach 48 Tu-154 Careless 49 Tu-154A Careless 50 Tu-144 Charger 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-104A Charger 55 Tu-104A Cauel A 56 Tu-104B Cauel A 57 Yak-40 Coding 58 Yak-18T 30 Yak-32 Mantis 61 Yak-330 Magnum 62 Yak-187 64 AN-10 Janes | 38 | M-15 | |
| 4011-864111-76Candid4211-62Classic4311-62M200Classic4411-18VCoot4511-14MCrate4611-14MCrate4711-12Coach48Tu-154Careless49Tu-144Charger50Tu-144Charger51Tu-134Crusty52Tu-134ACrusty53Tu-144Cleat54Tu-104ACauel A55Tu-104ACauel A56Tu-104BCauel A57Yak-40Coding58Yak-32Mantis61Yak-18764AN-10Janes | 39 | Be-30 | Cuff |
| 41I1-76Candid42I1-62Classic43I1-62M200Classic44I1-18VCoot45I1-14Crate46I1-14MCrate47I1-12Coach48Tu-154Careless49Tu-144Charger50Tu-134Crusty52Tu-134ACrusty53Tu-124Cookpot54Tu-104ACamel A55Tu-104ACamel A56Tu-104BCading57Yak-40Coding58Yak-32Mantis61Yak-30Magnum62Yak-18764AN-10Janes | 40 | 11- 86 | |
| 42 I1-62 Classic 43 I1-62M200 Classic 44 I1-18V Coot 45 I1-14 Crate 46 I1-14M Crate 47 I1-12 Coach 48 Tu-154 Careless 49 Tu-154A Careless 50 Tu-134 Crusty 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-144 Cleat 54 Tu-144 Cleat 55 Tu-144 Cookpot 54 Tu-144 Cleat 55 Tu-144 Cleat 54 Tu-144 Cleat 55 Tu-104A Cauel A 56 Tu-104B Cauel A 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-183 Max 63 Yak-183? | 41 | I1 -76 | Candid |
| 43I1-62M200Classic44I1-18VCoot45I1-14Crate46I1-14MCrate47I1-12Coach48Tu-154Careless49Tu-154ACareless50Tu-134ACharger51Tu-124Cookpot52Tu-134ACrusty53Tu-144Cleat54Tu-114Cleat55Tu-104ACauel A56Tu-104BCading57Yak-40Coding58Yak-18T60Yak-32Mantis61Yak-18AMaxu62Yak-18AMaxu63Yak-18Y64AN-10Janes | 42 | I1-62 | Classic |
| 44I1-18VCoot45I1-14Crate46I1-14MCrate47I1-12Coach48Tu-154Careless49Tu-154ACareless50Tu-134Charger51Tu-134ACrusty52Tu-134ACrusty53Tu-124Cookpot54Tu-104ACleat55Tu-104ACamel A56Tu-104BCamel B57Yak-40Coding58Yak-18T30Yak-32Mantis61Yak-18AMax62Yak-18AMax63Yak-18Y64AN-10Janes | 43 | 11-62M200 | Classic |
| 45I1-14Crate46I1-14MCrate47I1-12Coach48Tu-154Careless49Tu-154ACareless50Tu-144Charger51Tu-134ACrusty52Tu-124Cookpot54Tu-104ACleat55Tu-104ACamel A56Tu-104BCamel A57Yak-40Coding58Yak-40MCoding59Yak-18T30Yak-32Mantis61Yak-18AMax62Yak-18AMax63Yak-18Y64AN-10Janes | 44 | I1-18V | Coot |
| 46 11-14M Crate 47 11-12 Coach 48 Tu-154A Careless 49 Tu-154A Careless 50 Tu-144 Charger 51 Tu-134A Crusty 52 Tu-134A Cookpot 53 Tu-124 Cookpot 54 Tu-104A Cleat 55 Tu-104A Camel A 56 Tu-104B Cading 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-182 Magnum 62 Yak-182 64 AN-10 Janes | 45 | I1-14 | Crate |
| 47I1-12Coach48Tu-154Careless49Tu-154ACareless50Tu-144Charger51Tu-134Crusty52Tu-134ACrusty53Tu-114Cleat54Tu-104ACamel A55Tu-104BCading57Yak-40Coding58Yak-18T30Yak-32Mantis61Yak-183Max62Yak-18364AN-10Janes | 46 | 11-14 M | Crate |
| 48 Tu-154 Careless 49 Tu-154A Careless 50 Tu-144 Charger 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-114 Cleat 55 Tu-104A Camel A 56 Tu-104B Cading 57 Yak-40M Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-18A Max 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 47 | 11-12 | Coach |
| 49 Tu-154A Caraless 50 Tu-144 Charger 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-104A Cleat 55 Tu-104A Camel A 56 Tu-104B Cadel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-18A Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 48 | Tu-154 | Careless |
| 50 Tu-144 Charger 51 Tu-134A Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-114 Cleat 55 Tu-104A Camel A 56 Tu-104B Cadel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 49 | Tu-154A | Careless |
| 51 Tu-134 Crusty 52 Tu-134A Crusty 53 Tu-124 Cookpot 54 Tu-114 Cleat 55 Tu-104A Camel A 56 Tu-104B Camel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-18A Max 62 Yak-18? 64 AN-10 Janes | 50 | Tu-144 | Charger |
| 52 Tu-134A Grusty 53 Tu-124 Gookpot 54 Tu-114 Cleat 55 Tu-104A Gamel A 56 Tu-104B Gamel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-18A Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 51 | Tu-134 | Crusty |
| 53 Tu-124 Cookpot 54 Tu-114 Cleat 55 Tu-104A Camel A 56 Tu-104B Camel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18X Max 63 Yak-18? 64 AN-10 Janes | 52 | Tu-134A | Crusty |
| 54 Tu-114 Cleat 55 Tu-104Λ Camel A 56 Tu-104B Camel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18X Max 63 Yak-18? 64 ΛΝ-10 Janes | 53 | Tu-124 | Cookpot |
| 55 Tu-104Λ Camel A 56 Tu-104B Camel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-18A Max 62 Yak-18? 63 Yak-18? 64 ΛΝ-10 Janes | 54 | Tu-114 | Cleat |
| 56 Tu-104B Camel B 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18X 63 Yak-18Y 64 AN-10 Janes | 55 | $Tu-104\Lambda$ | Camel A |
| 57 Yak-40 Coding 58 Yak-40M Coding 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18X Max 63 Yak-18? 64 AN-10 Janes | 56 | Tu-104B | Camel B |
| 58 Yak-40M Coding 59 Yak-18T 50 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 57 | Yak-40 | Coding |
| 59 Yak-18T 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 58 | Yak-40M | Coding |
| 30 Yak-32 Mantis 61 Yak-30 Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 59 | Yak-18T | |
| 61 Yak-30 Magnum 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | <u>ن</u> 0 | Yak-32 | Mantis |
| 62 Yak-18A Max 63 Yak-18? 64 AN-10 Janes | 61 | Yak-30 | Magnum |
| 63 Yak-18? 64 AN-10 Janes | 62 | Yak-18A | Max |
| 64 AN-10 Janes | 63 | Yak-18? | |
| | 64 | AN-10 | Janes |
| 65 BE-30 Janes | 65 | BE-30 | Janes |

Table 9 (Concluded)

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Table 10

Vehicle Parameter Codes

Wheeled Vehicles

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Weight, kg

| Class | Class Range |
|-------|-----------------------|
| 3 | 0-2 000 |
| 2 | >2 000-4000 |
| 3 | >40 00-5500 |
| 4 | >5500-8000 |
| 5 | >8000-10,000 |
| 6 | >10.000 |

Number of Wheels Per Side

| <u>Class</u> | No. of Wheels Per Side |
|--------------|------------------------|
| 1 | 2 |
| 2 | 3 |
| 3 | 4 |
| | |

<u>Tire Size</u>

<u>Class</u> 1

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Suspension

| Class | Туре | |
|-------|----------------------------|--|
| 1 | Semielliptical (IS) | |
| | Timken-Detroit #2034 | |
| | Timken-Detroit SFD-375-A-1 | |
| | Semielliptical; inverted | |
| | Hotchkies Drive; 10871261 | |
| | Bogie Model SWD-321 | |
| | Bogie Model SWD-322 | |
| | Bogie Model GMC | |
| | Leaf springs | |
| | Bogie Model FWD (Spel) | |
| | Bogie Model SFD 4600 | |
| | | |

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| Class | Туре |
|--------------|------------------------------------|
| | Bogie Model Rockwell STD |
| | Bogie Model KENW BM 2150-1 |
| 2 | Civil |
| 3 | Air shock absorbers, double acting |
| 4 | Torsion bar |
| 5 | Solid mount walking beam |
| 6 | No suspension |
| | Horsepower |
| <u>Class</u> | |
| 1 | All |
| | Fuel Type |
| <u>Class</u> | Type Fuel |
| 1 | Gasoline |
| 2 | Diesel |
| 3 | Multifuel |
| <u>c</u> | Coolant Type |
| Class | Type Cooling |
| 1 | Air |
| 2 | Liquid |

(Continued)

(Sheet 2 of 3)

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Table 10 (Concluded)

Tracked Vehicles

Weight, kg

| Class | Class Range |
|-------|-----------------|
| 1 | 0- -9999 |
| 2 | 10,000-19,999 |
| 3 | 20,000-29,999 |
| 4 | 30,000-39,999 |
| 5 | >40,000 |

Horsepower

| <u>Class</u> | Class Range |
|--------------|-------------|
| 1 | 0-400 |
| 2 | >400 |

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Fuel Type

| <u>Class</u> | Type Fuel |
|--------------|-----------|
| 1 | Gasoline |
| 2 | Diesel |
| 3 | Multifuel |

มสมบัตร เองประกันของเป็นไฟส์ อาจไฟกันประสุดิจตัว อย่างสามหรือไปได้ที่ <mark>ไม่สุดกระจำหนังการการใหญ่ไปสุดจากไฟ ไป</mark>สม

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Comparison of U. S. and Foreign Vehicles

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| 541 |
| 11 |
| 80 |
| 75 |
| 82 |
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| 1,53 |
| 1,54 |
| 1,67 |
| 1,85 |
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Duals considered as one wheel.

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| U. S. besited Mailog Unset Foreign Real Interest Mailog Total Foreign Total Foreign <thtotal Foreign Total Foreign</thtotal | Proposed | | | | No. of | Wheels | | | | £,, ○] | |
|--|-----------------|--------------------|------------------|--------------|----------|-------------|-----------|--------------|-------|----------|--------|
| Minelad (Continued) Minelad (Continued) GAT-53Y 2,950 6 2 7,50-20 Semielliptic 80 Gas GAT-93H 3,000 6 2 7,50-20 Semielliptic 80 Gas GAT-63H 3,300 4 2 10.00-18 70 | U. S. Analog | Desired Foreign | Other Foreign | Weight kg | Total | rer Side | Tire Size | Suspension | power | Туре | Type |
| CAVE-537 2,950 6 2 8.25-20 Semielliptic 80 Gas Liquid GAVE-63A 3,440 4 2 7.000 6 2 7.50-20 70 </td <td></td> <td></td> <td></td> <td></td> <td>Wheeled</td> <td>(Contin</td> <td>ued)</td> <td></td> <td></td> <td></td> <td></td> | | | | | Wheeled | (Contin | ued) | | | | |
| $ \begin{array}{cccccc} & & & & & & & & & & & & & & & & $ | | | GAZ-53F | 2,950 | 9 | . ∾ | 8.25-20 | Semielliptic | 80 | Gas | Liquid |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | GAZ-93A | 3,000 | Ś | 2 | 7.50-20 | | 20 | | |
| $ \begin{array}{llllllllllllllllllllllllllllllllllll$ | | | GAZ-63 | 3,200 | t, | ŝ | 10.00-18 | | 70 | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | URAL-355M | 3,360 | 9 | Q | 8.25-20 | | 95 | | |
| $ \begin{array}{llllllllllllllllllllllllllllllllllll$ | | | GAZ-63A | 3,440 | † | ଧ | 10.00-18 | | 70 | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | GAZ-SAZ-53B | 3,750 | † | ~ | 8.25-20 | | 115 | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | GAZ-53B | 3,750 | 9 | 2 | 8.25-20 | | 115 | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | TZ-63 | 3,890 | t, | ~≀ | 9.75-18 | | 70 | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | KAZ-608 | 1,000 | 9 | CJ | 9.00-20 | | 150 | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | GAZ-51P | 2,485 | υī | m | 7.50-20 | | 70 | | |
| AVV-2 $7,50-20$ 70 $M46C$ $MV-2$ $2,900$ 6 2 $7,50-20$ 115 $M46C$ $MTZ-2.2-5LA$ $2,900$ 6 2 $7,50-20$ 116 $M35$ $5,570$ 10 3 $9,00-20$ 1146 $M19$ $M49$ $M49$ 10 3 $9,00-20$ 1146 $M49C$ $M55$ 10 3 $9,00-20$ 1146 $M35A1$ $6,118$ 10 3 $9,00-20$ 1146 $M49C$ $M49C$ $6,123$ 10 3 $9,00-20$ 1146 $M56$ $M56$ 10 3 $9,00-20$ 1146 $M217$ $M217$ 10 3 $9,00-20$ 1146 $M26A2$ $M264$ 10 3 $9,00-20$ 1146 $M217$ $M217$ 10 3 $9,00-20$ 1146 $M26A2$ $M264$ 10 3 $9,00-20$ 1146 $M26A2$ $M264$ 10 3 $9,00-20$ 1146 | | | GAZ-62 | 2,570 | ţ, | CJ | 11.00-16 | | 80 | | |
| M46C ATZ-2.2-51A 2,904 6 2 7.50-20 115 M211 5,570 10 3 9.00-20 146 M35A1 M35A1 6,078 10 3 9.00-20 146 M35A1 M35A1 M35A1 6,078 10 3 9.00-20 146 M36A M35A1 6,078 10 3 9.00-20 146 M36A M35A1 6,118 10 3 9.00-20 146 M36A M35A2 6,118 10 3 9.00-20 146 M36A M36A 3 9.00-20 146 146 M36A M217 5,504 10 3 9.00-20 146 M36A1 M36A1 M36A1 3 9.00-20 146 146 M36A2 6,564 10 3 9.00-20 146 146 M36A2 M36A1 3 9.00-20 146 146 146 146 146 146 146 146 146 146 146 | | | AVV-2 | 2,900 | ţ, | 2 | 7.50-20 | | 70 | | |
| M46C 5,570 10 3 9.00-20 146 M35A1 M35A1 M211 5,653 10 3 9.00-20 146 M35A1 M35A1 M35A1 M35A1 10 3 9.00-20 146 M49C M36 M36 10 3 9.00-20 146 M49C M36 M36 10 3 9.00-20 146 M36 M217 0 3 9.00-20 146 M217 M217 3 9.00-20 146 145 M36 M216 3 9.00-20 146 145 M217 M217 M216 3 9.00-20 145 M36 M216 M21 M216 10 3 9.00-20 | | | ATZ-2.2-51A | 2,904 | 9 | N | 7.50-20 | | 115 | | |
| M211 M211 M211 M211 M211 M211 M214 M214 | M46C | | | 5,570 | 10 | ቦገ | 9.00-20 | | 146 | | |
| M211 5,973 10 3 9.00-20 145 M35A1 M35A1 6,078 10 3 9.00-20 146 M35A1 M49 6,118 10 3 9.00-20 146 M49 M36 6,118 10 3 9.00-20 146 M49 M36 6,118 10 3 9.00-20 146 M36 M35A2C 6,123 10 3 9.00-20 146 M35A2C M35A2 6,126 10 3 9.00-20 146 M35A2C M35A2 M35A2 100 3 9.00-20 146 M35A1 M217 6,578 10 3 9.00-20 145 M217 M217 5,666 10 3 9.00-20 145 M215 M216 10 3 9.00-20 145 M215 M216 10 3 9.00-20 145 M36A1 6,626 10 3 9.00-20 145 M36A2 6,626 10 <td>M35</td> <td></td> <td></td> <td>5,653</td> <td>10</td> <td>m</td> <td>9.00-20</td> <td></td> <td>146</td> <td></td> <td></td> | M35 | | | 5,653 | 10 | m | 9.00-20 | | 146 | | |
| M35A1 6,078 10 3 9.00-20 146 M49C M49C 10 3 9.00-20 146 M49C M49C 6,118 10 3 9.00-20 146 M36 M35A2 M35A2 10 3 9.00-20 146 M35A2 M35A2 0.020 10 3 9.00-20 146 M35A2 M35A2 0.022 146 146 146 M217 M59 0 3 9.00-20 146 M217 M517 10 3 9.00-20 146 M217 M217 0 9.00-20 146 145 M217 M217 3 9.00-20 146 145 M217 M215 10 3 9.00-20 145 M217 M216 10 3 9.00-20 146 M217 M215 10 3 9.00-20 145 M36A1 M36A2 3 9.00-20 145 145 | MZII | | | 5,973 | IO | m | 9.00-20 | | 145 | | |
| M49 M49 M49C M49C M49C M49C M46 6,118 10 3 9.00-20 146 M35 6,123 10 3 9.00-20 146 M35 6,196 10 3 9.00-20 146 M35A2C 6,196 10 3 9.00-20 146 M35A2C 6,504 10 3 9.00-20 146 M217 6,504 10 3 9.00-20 145 M217 6,5504 10 3 9.00-20 145 M217 M217 6,558 10 3 9.00-20 145 M217 M216 10 3 9.00-20 145 145 M2642 10 3 9.00-20 145 145< | M35A1 | | | 6.078 | 10 | m | 9.00-20 | | 146 | <u> </u> | |
| M49C 0.118 10 3 9.00-20 146 M36 6,123 10 3 9.00-20 146 M35A2C 6,196 10 3 9.00-20 146 M59 6,504 10 3 9.00-20 146 M217 6,504 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,626 10 3 9.00-20 145 M217 0.020 145 145 145 M26A1 6,626 10 3 9.00-20 146 | 0 TN | | | 6,118 | 10 | ო | 9.00-20 | | 146 | | |
| M36 M36 10 3 9.00-20 146 M35A2C 6,196 10 3 9.00-20 146 M59 6,372 10 3 9.00-20 146 M59 6,504 10 3 9.00-20 145 M217 6,504 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,626 10 3 9.00-20 145 M217 6,626 10 3 9.00-20 145 M36A1 6,626 10 3 9.00-20 146 | M49C | | | 6,118 | 10 | m | 9.00-20 | | 146 | | |
| M35A2C 6,196 10 3 9.00-20 146 M59 6,372 10 3 9.00-20 146 M517 6,504 10 3 9.00-20 145 M217 6,504 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,626 10 3 9.00-20 145 M36A1 6,626 10 3 9.00-20 146 | M36 | | | 6,123 | IO | m | 9.00-20 | | 146 | | |
| MS9 6,372 10 9.00-20 146 MS17 6,504 10 3 9.00-20 145 M217 6,554 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,558 10 3 9.00-20 145 M217 6,626 10 3 9.00-20 146 M36A1 6,626 10 3 9.00-20 146 | M35A2C | | | 6,196 | JO | m | 9.00-20 | | 146 | | |
| M217 6,504 10 3 9.00-20 145 M217c 6,558 10 3 9.00-20 145 M215 6,558 10 3 9.00-20 145 M215 6,558 10 3 9.00-20 145 M26A1 6,626 10 3 9.00-20 146 M36A2 6,626 10 3 9.00-20 146 | M59 | | | 6,372 | 10 | ٦ | 9.00-20 | | 146 | <u> </u> | |
| M217c 6,504 10 3 9.00-20 145 M217c 6,558 10 3 9.00-20 145 M26A1 6,626 10 3 9.00-20 146 M36A2 6,626 10 3 9.00-20 146 | MZIT | | | 6,504 | TO | ŝ | 9.00-20 | | 145 | | |
| M215 6,558 10 3 9.00-20 145 M36A1 6,626 10 3 9.00-20 146 M36A2 6,626 10 3 9.00-20 146 | M217C | | | 6.504 | 10 | m | 9.00-20 | | 145 | | |
| M36A1 6,626 10 3 9.00-20 146 1 M36A2 6,626 10 3 9.00-20 146 | NO15 | | | 6,558 | IO | m | 9.00-20 | | 145 | | |
| M36A2 6,626 10 3 9.00-20 T 146 T T | M36A1 | | | 6,626 | 10 | m | 9.00-20 | | 146 | | |
| | M36A2 | | | 6,626 | 10 | m | 9.00-20 | * | 146 | - | • |

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| | Coclant | adkt | | Liguid | | | | | | | | | | | | | | | | | | | | | | ~~~ | | + |
|----------|--------------|------------|---------|-----------------|---------|----------|----------|----------|----------|-------------|---------|---------|---------|----------|---------|-----------|----------|-----------|----------|----------|---------|------------|----------|-------------|-----------|-----------|-----------|------------|
| | Fuel | TYPE | | Gas | | | | | • | Multi | | | | + | Gas | | <u> </u> | | : | | | | | | | | | + |
| | Horse- | power | | 146 | 146 | 224 | 224 | 224 | 224 | 140 | 140 | 140 | 140 | 210 | 92 | 112 | 112 | 109 1 | 150 | 150 | 220 | 104 | 220 | 104 | 180 | 180 | 180 | 92 |
| | | ouspension | | Semielliptic | | • | | | | | | | | | | | | | | | | | | | | | | - |
| | | Tre Size | ied) | <u>9</u> .00-20 | 9.00-20 | 11.00-20 | 14.00-20 | 11.00-20 | 11.00-20 | 9.00-20 | 9.00-20 | 9.00-20 | 9.00-20 | 11.00-20 | 8.25-20 | 12.00-18 | 12.00-18 | 12.00-18 | 12.00-20 | 12.00-20 | 9.00-20 | 12.00-18 | 9.00-20 | 12.00-18 | 21.00-28 | 14.00-20 | 14.00-20 | 8.25-20 |
| Wheels | Per | Slae | (Contin | m | m | m | m | m | m | (۲) | Υ | ŝ | m | m | m | ŝ | m | m | m | m | m | m | ε | ŝ | m | m | m | ŕ |
| No. of | - - - | Total | Theeled | 10 | 10 | 10 | 9 | 10 | 01 | 0 r | 01 | ΟŢ | 10 | JO | 10 | 9 | 9 | 9 | 9 | 9 | 10 | 9 | 10 | 9 | 9 | 9 | 9 | 10 |
| | Weight | КĜ | 14 | 6,726 | 6,887 | 7,613 | 7,631 | 7,661 | 7,874 | 6,404 | 6, 404 | 6,633 | 6,633 | 7,720 | 5,580 | 5,700 | 5,800 | 6,135 | 6,460 | 6,225 | 6,200 | 6,250 | 6,350 | 6,700 | 6,800 | 6,830 | 7,500 | 7.625 |
| | Other | Foreign | | | | | | | | | | | | | | | | | | | ZIL-133 | ATSM-4-157 | ZIL-133V | ATZ-3-157 | ZIL-E-167 | URAL-377S | URAL-375S | 17-211-151 |
| | Desireā - | Foreign | | | | | | | | | | | | | ZII-151 | ZIL-157KV | ZIL-157K | ARS-12/14 | ZIL-131 | ZIL-131V | | | | | | | | |
| Proposeá | ц. s. | Anelog | | M36C | M50 | M40 | M39 | M40A2 | T9W | M50Al | M50A2 | M-SALC | M4 9A2C | MÉLAZ | | | | | | | | | | | | | | |

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| Proposed | | | 110:22+ | No. of | Wheels | | | 0 0 1 1 1 1 | لم, لع ا | Coolant |
|-----------------|--------------------|------------------|----------|--------|---------|-----------|--------------|----------------------------|-------------|--------------|
| C. J. Analog | Pestrea Foreign | ouner Foreign | Kg Kg | Total | Side | Tire Size | Suspension | power | Type | Type |
| | | | | Wheled | (Contin | leà) | | | | |
| | | ATZ-3-151 | 6,700 | 10 | m | 8.25-20 | Semielliptic | 92 | Gas | Liquid |
| ié 30 | | | 8,161 | TO | m | 12.00-20 | | 224 | - | |
| I63 | | | 8,263 | IO | ŝ | 11.00-20 | | 224 | | |
| 141 | | | 8,672 | IO | m | 14.00-20 | | 724 | | |
| <u>п</u> 08 | | | 8,788 | TO | m | 9.00-20 | | 146 | • | |
| 16342C | | | 8,060 | 10 | m | 12.00-20 | | 210 | Multi | |
| 52A2 | | | 8,092 | 0.1 | m | 11.00-20 | | 210 | | . |
| 163A2 | | | 8,123 | 10 | m | 11.00-20 | | 210 | | |
| CT OA2C | | | 8,640 | TO | m | 11.00-20 | | 210 | | |
| th OC | | | 8,686 | 10 | ŝ | 11.00-20 | | 210 | | |
| 54A2 | | | 8,915 | JO | m | 11.00-20 | | 210 | | |
| 813 | | | 9,736 | 10 | m | 11.00-20 | | 250 | | |
| 5142 | | | 9,942 | 10 | m | 11.00-20 | | 210 | * | |
| L. | BTR-152V1 | | 8,119 | 9 | m | 12.00-18 | | 0TT | Gas | |
| | BTR-152 | | 8,368 | Ś | m | 12.00-18 | | 110 | | |
| | URAL-375 | | 8,400 | 6 | ς (| 14.00-20 | | 180 | | |
| | | URAL-375D | 8,400 | 9 | ŝ | 14.00-20 | | 180 | * | |
| | | MAZ-514 | 8,700 | IO | m | 11.00-22 | | 180 | Diesel | |
| | | KRAZ-258 | 9,680 | IO | m | 12.00-20 | | 240 | Diesel | |
| 125 | | | 14,765 | 10 | m | 14.00-24 | | 297 | Gas | |
| | KRAZ-214 | | 12,300 | 9 | m | 15.00-20 | | 205 | Diesel | |
| | KRAZ-255B | | 11,950 | 9 | m | 15.00-20 | | 240 | | |
| | KRAZ-256B | | 11,400 | 10 | m | 12.00-20 | * | 215 | | |
| | | NAMI-076 | 19,000 | 6 | m | | - | ļ | | |
| | | KRAZ-219 | 11,300 | IO | m | 12.00-20 | Semielliptic | 180 | | |
| | | KRAZ-222 | 12,200 | 10 | m | 12.00-20 | Semielliptic | 180 | • | * |
| -100 | | | 7,370 | 7† | 2 | No data | No data | 191 | Gas | No data |
| | | | • | (Con | tinued) | | | | | |
| | | | | | | | | | (Sheet | 4 OI 0) |

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| se- Fuel Coolant er Type Type | |) Diesel Liquid) Gas Liquid) Gas Liquid | |) Gas Liquid | o Gas Air 5 Gas Liquid |) Gas/ diesel | 9 Gas/ | diesel | t Gas |) Diesel Liquid | D No data | D No data | D No data | D Liquid | | · · · · · · · · · · · · · · · · · · · | | | | | |
|------------------------------------|----------------|--|---------|--------------|----------------------------------|------------------|-----------------|--------|--------|------------------|-------------|-----------|-----------|----------|--------|---------------------------------------|--------|---------|--------|----------|--|
| Hors Suspension powe | | No data 100 Semielliptic 140 Semielliptic 80 | | Not used 160 | | 300 | 500 | | | 58 | 13(| 28(| 58(| 540 | 300 | 30 | 58(| 540 | | 1 | |
| Tire Size | nued) | 12.00-18 13.00-18 9.75-18 | | N/A | | | | | | | | | | | | | | | | * | |
| No. of Wheels Per Total Side | Wheeled (Conti | ש מיט די בי | Tracked | Not used | | | | | | | | | | | | | | | | | |
| Weight kg | | 5,535 6,930 4,808 | | 3,467 | 5 , 500 3 , 350 | 15,276 | 10 . 670 | | 10,600 | 10,069 10,069 | 0 548 | 10.000 | 10,000 | 14,500 | 15,000 | 16,390 | 14,000 | 14,000 | 14,000 | 12,500 | |
| Other Foreign | | | | | | | | | | | | | | | | | | | | BMP-2 | |
| sed 3. Desired 3. Foreign | | 0T-65 BRDM-2 BTR-1:0 | | | ASII- 57 | | | | ٩ | 796 IM | . гух | | RMP-76PB | BTR-50PK | 0T-62B | 0T-62C | PT-76 | ZSU23-4 | ASU-85 | | |
| Propos U. S Analo | | | | 911W | M76 | M551 | 51 LM | | M132 | JJCW | | | | | | | | | | | |

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Table 11 (Concluded)

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| Proposed II S | Decired | 0+ 7 2 4 2 4 | + Y + F - 11 | IIO. Of | Wheels | | | , Horse | [ອາເສ | Coolant |
|------------------|----------|-----------------|---------------------------|---------|---------|-----------|------------|------------|--------|---------|
| Analog | Foreign | Foreign | 2 19 19 19 19 | Intel | Side | Tire Size | Suspension | power | Type | Type |
| | | | | Tracked | (Cantin | ueá) | | | | |
| 0017 | | | 21,274 | lot u | seà | N/A | itte trea | 240 | Diesel | Liquid |
| 515 | | | 27,324 | | | | | 105 | | |
| 0111 | | | 25,740 | | | | | 1405 1 | _ | |
| ME 05 | | | 20,636 | | | | | 40万 | | |
| 60 IN | | | 23,082 | | | | | 405 | | ••• |
| | eu-85 | | 29,600 | | | | | 500 | _, · | |
| | ZSU-57-2 | | 28,100 | | | | - <u>-</u> | 520 | | |
| | 50-100 | | 31,600 | | | | | 005 | | |
| | | N36B2 | 29,900 | | | | | U L | | * |
| XLBAIE2 | | | 45 , 760 | | | | | 750 | | £≛r |
| 1100 1100 | | | 44,580 | | | | | 750 | | Air |
| | 1-10 | | 50,000 | | | | | 700 | | Liquid |
| | | J3-2 | 46,300 | | | | | 650 | | Liquid |
| | | JS-3 | 45 , 800 | | | | | 650 | | Liquid |
| | | · | EO 000 | + | | - | - | ς ΥςΩ | + | Lionid |

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State of the state

| Wheeled Vehicles | Tracked Vehicles |
|------------------------|------------------|
| Trucks | APC |
| ZAZ-971 | |
| ZIL-157K/157KV | M1967 |
| JRAL-375 | K61 |
| JAZ/GAZ-69 | M1 970 |
| GAZ-66 | BMP-76PB |
| JAZ-63 | BTR-50PK |
| ZIL-1.30V1 | OT-62B |
| ZTL-J.31/131V | OT-62C |
| ZIL -151 | |
| ľ-111 | Tanks |
| r-141 | |
| I-138 | PT-76 |
| JAZ-450D | T54 or T55 |
| ARS-12/14 | т62 |
| KRAZ-214/255/255B/256B | T10 |
| | М7О |
| APC | • |
| | Weapons |
| BTR-152 | |
| BTR-60P | ASU-57 |
| BRDM-2 | ASU-85 |
| BTR-152V1 | SU-85 |
| BTR-40 | SU-100 |
| OT-65 | ZSU-23-4 |
| 07-64 | ZSU~57-2 |
| | M1974 |
| | M1 073 |

| | | | Table | e 12 | | | |
|---------|--------|----------|-------|-------|------------|-----|--------|
| Roreign | Ground | Vehicles | from | Which | Signatures | 970 | Destre |

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eastration

| Rotary-Wing | Fixed-Wing |
|-------------|----------------|
| Mi-8 | Tu-22 |
| Mi-2 | Tu- 95 |
| Ka-18 | Tu-16 |
| Ка-25К | Be-12 |
| Ka-26 | Yak-2 5 |
| Mi-12 | MiG-25 |
| Mi-10 | MiG-21 |
| Mi-6 | An-22 |
| Mi-4 | 1-7 6 |
| Ka-15 | Tu-144 |
| Ka-22 | |
| Yak-24 | |

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Table 13 Foreign Aircraft from Which Signatures are Desired

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| | | Compar | ison of U. | S. and Fo | reign Airc | raft | | | |
|--------------------------------------|--|-------------------------------------|---|---------------------------------------|---|--------------------------------------|--|-------------------------------------|---|
| Proposed U.S. Analog CH-46F | Desired Foreign Aircraft Mi-8 | Proposed U.S. Analog UH-IN | Desired Foreign Aircraft <u>Mi-Z</u> | Proposed U. S. Analog TH-57A | Desired Foreign Aircraft Ka-18 | Proposed U. S. Analog CH-3B | Desired Foreign Aircraft Ka-25K | Proposed U.S. Analog HR-IK | Desired Foreign Aircraft Ka-26 |
| | | | Ro | tary-Wing | | | | | |
| 6044 | 6,816 | 2517 | 2424 | 695 | | 4393 | 4400 | 2349 | 2085 |
| | 4,000 | | 800 | | | | 2000 | 1759 | 1065 |

| | | T | ble | 14 | | |
|------------|----|----|-----|-----|---------|----------|
| Comparison | of | υ, | 8. | and | Foreign | Aircraft |

ade a la finista carra la marca da marchiter de la construcción de la construcción de la construcción de la con

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| Wt, empty, kg | 6044 | 6,816 | 2517 | 2424 | 695 | | 4323 | 4400 | 2349 | 2085 |
|---------------|---------|---------|---------|---------|---------|------|---------|---------|---------|--------|
| Payload, kg | | 4,000 | | 800 | | | | 2000 | 1759 | 1065 |
| No. rotors | 2 | l | 1 | l | 1 | 2 | l | 2 | 1 | 2 |
| No. engines | 2 | 2 | 2 | 2 | 1 | 1 | 2 . | 2 | l | 2 |
| Horsepower | 1400 | 1,500 | 900 | 437 | | - | 1400 | 900 | 1400 | 325 |
| Type engine | Turbine | Turbine | Turbine | Turbine | Turbine | ~- | Turbine | Turbine | Turbine | Piston |
| Wt, gross, kg | 9360 ` | 11,880 | 4725 | 3750 | 1305 | 1300 | 9225 | 7045 | 3825 | 2970 |
| | | ı | | | | | | | | |

| | | | | USSR | | | |
|---------------|---------|---------|---------|-------------|-------|-------|--------|
| | Mi-12 | Mi-10 | Mi-6 | <u>Mi-4</u> | Ka-15 | Ka-22 | Yak-24 |
| | | | Rotary- | Wing | | | |
| Wt, empty, kg | | 27,300 | 27,240 | | | | |
| Payload, kg | 30,000 | 15,000 | 12,000 | 1,740 | | | |
| No. rotors | 2 | 1 | 1 | 1 | 2 | 2 | 2 |
| No. engines | 4 | 2 | 2 | 1 | - | | |
| Horsepower | 6,500 | 5,500 | 5,500 | 1,700 | | | |
| Type engine | Turbine | Turbine | Turbine | Piston | | | |
| Wu, gross, kg | 103,950 | 43,113 | 42,170 | 38,220 | | | 15,874 |
| | | | | | | | |

| | | | | | | ISSR | | | | |
|---------------|------------|--------------------------|-------------------|-------------------|---------------------|---------------------|---------------------|-------------|-------------|--------------|
| | 1 Tu-22 | <u>1</u> <u>Tu-95</u> | 5 <u>Tu-16</u> | 9 <u>Be-12</u> | 11 <u>Yak-25</u> | 12 <u>M10-25</u> | 18 <u>M1G-21</u> | 34 An-22 | 41 11-76 | 50 Tu-144 |
| | | | | Ē | ixed-Wing | | | | | |
| Wt, gross, kg | 78,750 | 148,500 | 67,500 | 31,500 | 13,500 | 28,030 | 7650 | 225,000 | 159,300 | 177,750 |
| No. engines | 2 | 4 | 2 | 2 | 2 | 2 | 1 | 4 | 14 | 14 |
| Thrust, kg | 11,700 | | 8,775 | | 3,375 | | 5400 | | 11,385 | 17,361 |
| llorsepower | | 12,000 | | 4,000 | | | | 15,000 | | |

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Table 15

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Terrain Matrix

| 1. | | | c. Ko. Gualitative Terrain Descriptors | 1.10 Recently cultivated (loosened) top soil overlying moist loam 1.20 Recently cultivated (loosened) top soil overlying slightly sandy or gravelly soft clay 1.30 Loose cohesionless top soil overlying dry sand 1.40 Organic saturated clay overlying slightly sandy or gravelly soft clay | 2.10 Recently cultivated (loosened) top soil overlying moist sandy or gravelly loam 2.20 Recently cultivated (loosened) top soil overlying medium clay 2.30 Loose cohesionless top soil overlying dry gravel 2.40 Organic saturated clay overlying medium clay | 3.10 Recently cultivated (loosened) top soil overlying heavy gravely clay (till) 3.20 Loose cohesionless top soil overlying moist medium gravel 3.30 Organic saturated clay overlying vet medium dense sand 3.40 Organic saturated clay overlying heavy gravelly clay (till) | <pre>6 4.10 Recently cultivated (loosened) top soil overlying dense soil with high water table 4.20 Organic saturated clay overlying frozen silty or clayey loam 4.30 Organic saturated clay overlying deuse soil with high water table</pre> | |
|--------------------------|-------------|-----------|---|--|---|---|---|-----------|
| 11 | First | Leyer | H DESS | 0.25 4.0 | 0.25 1.5 4.0 | 0.25 4.0 | 0.29 4.0 | (P |
| of Top Laye Matarial | TTTT 122 BU | ; | Bulk Density c/cm3 | 1.60/1.70 1.60/1.70 1.60/1.70 | 1.60/2.00 1.60/2.00 1.60/2.00 | 1.60/2.05 1.60/2.05 1.60/2.05 | 1.60/1.80 1.60/1.80 1.60/1.80 | (Continue |
| steristics soundation | HOTABATAO | Shear | Welocity Welocity | 75/125 75/125 75/125 | 75/275 75/275 75/275 | 75/4:00 75/4:00 | 75/550 75/550 75/550 | |
| Citarad | | Compres- | sion Wave Velocity | 150/300 150/300 150/300 | 150/680 150/680 150/680 | 150/1450 150/1450 150/1450 | 150/2000 150/2000 150/2000 | |
| i of | 111 | Foughness | rms Elevation | 5.08 5.08 5.08 | 5.08 5.08 5.08 | 5.08 5.08 5.08 | 5.08 5.08 5.08 | |
| eristics | Y | Maximum | Spring Travel | 0.1 | 0.1 0.1 | 0.1 0.1 | 1.0 1.0 | |
| Charact | Rigidit | | Spring Constant v/- | $\frac{1}{100}$ | 0.775 × 10 ⁷ 0.775 × 10 ⁷ 0.775 × 10 ⁷ | 0.775 × 10 ⁷ 0.775 × 10 ⁷ 0.775 × 10 ⁷ | 0.775 × 10 ⁷ 0.775 × 10 ⁷ 0.775 × 10 ⁷ | |
| | | | Terrain Matrix | M N N | ov vi te | r- co o r | 11 11 | |

(Sheet 1 of 7)

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| | | | | | Qualitative Terrain Descriptors | Recently cultivated (loosened) top soil overlying | hard clay Loose cohesionless top soil overlying dense sand | and gravel Loose cohesionless top soil overlying weathered | rock | organic saturated cirdy overlying tense sam and | Organic saturated clay overlying cemented soil Organic saturated clay overlying vesthered rock | Organic saturated clay overlying hard clay | | Organic saturated clay overlying competent un- | | Organic material (pear) overlying dense sand and | gravel | Organic meterial (reat) overstand resident of | | Jense loam overlying weathered rock | | Dry loose gravel Medium sand | Moist sandy or silty clay |
|-------------|--------------|----------------|-----------|-----------|---------------------------------|---|---|---|-------------------------|---|---|--|-------------------------|--|-------------------------|--|--|---|------------------------|-------------------------------------|------------------------|---------------------------------|---------------------------|
| | | | | | No. | 5.10 | 5.20 | 5.30 | | 0#** | 5.5 8.8 | 2.70 | _ | (0.10) | _ | (6.11 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 27.0 | | | ~ | 7.20 | 1.30 |
| | | First | Layer | Thick- | HI HI | | | 0.25 | 1.5 | ħ.0 | _ | | 0.25 | т•5 • Т | 00.4 | 0.25 | 1.5 | 0°† | 0.25 | 1-5 | 0.4 | 10.0 | |
| | of Top Layer | Acertal | | Bulk | R/CB3 | | | 1.60/2.10 | 1.60/2.10 | 1.60/2.10 | | | 1.60/2.50 | 1.60/2.50 | 1.60/2.50 | 1.30/2.10 | 1.30/2.10 | 1.30/2.10 | 1.80/2.10 | 1.80/2.10 | 1.80/2.10 | 1.70 | • |
| ain Matrix | teristics of | oundation | Shear | Wave | m/sec | | | 75/750 | 75/750 | 75/750 | | | 15/1500 | 75/1500 | 75/1500 | 6 0/750 | 60/750 | 60/750 | 200/150 | 200/750 | 200/750 | × X | |
| sed in Terr | Charac | 2 | Compres- | sion Wave | Welocity | | | 150/2000 | 150/2000 | 150/2000 | | | 150/3500 | 150/3500 | 150/3500 | 200/2000 | 200/2000 | 200/2000 | 1+00/2000 | 400/2000 | 4:00/2000 | 655 | |
| Factors / | ٩ | | Roughness | SEL | Elevation cm | | | 5.08 | 5.08 | 5.08 | | | 5.08 | 5.08 | 5.08 | 1.20 | 1.20 | 1.20 | 3.81 | 3.81 | 3.81 | 3.05 | |
| Terrair | eristics | e Materia v | Maximu | Spring | Travel | | | 0.1 | 0.1 | 1.0 | | | 1.0 | 0.1 | 0.1 | 0.26 | 0-50 | 0-50 | 60 .0 | 60.0 | 60 • 0 | 0.075 | 1 |
| | Charact | Surfac | | Spring | Constant N/m | | | 0.775 × 10 ⁷ | 0.775 × 10 ⁷ | 0.775'× 10 ⁷ | | | 0.775 × 10 ⁷ | 0.775 × 10 ⁷ | 0.775 × 10 ⁷ | 0.36 × 10 ⁷ | 0.94 × 10 ⁶ | 0.94 × 10 ⁶ | 1.45 × 10 ¹ | 1.45×10^7 | 1.45 × 10 ⁷ | 101 ~ 22 0 | ** * **** |
| | | | | Terrain | Matrix Element | | | ET | 17 | 15 | , | | 16 | 71 | 1.8 | 61 | ଛ | ដ | ន | ស | 5 | X | 0 |

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| | 1 | | | | | o. Qualitative Terrain Descriptors | .10 Dry loose gravel overlying moist medium gravel .20 Dry loose gravel overlying heavy gravelly clay | (tiil) .30 Medium sand overlying wet medium-leuse sand | .40 Medium sand overlying moist medium gravel 50 Medium sand availation beams meanedly of at (1411) | | dense sand .70 Moist sandy or silty clay overlying heavy gravelly clay (till) | .10 Dry loose gravel overlying frozen silty or clayey loam | .20 Dry loose gravel overlying dense cohesionless soil with high water table | .30 Medium sand overlying frozen silty or clayey loam | .*•• Meulum samu overlying gense conceloniess soil VICA high water table | .50 Moist sandy or silty clay overlying frozen silty | or clayey loam .60 Moist sandy or silty clay overlying dense cohesionless soil with high water table |
|-------------|-------------|------------|-------|-----------------------|-----------|------------------------------------|--|---|--|--|---|---|---|---|---|--|--|
| | | | 41 | الد بر | l va | × | 88 | 2 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | Ĵ | 6 | 0 | ة ة ~ | | ō. | Ď |
| | er | | Firs | Thic | nes | | ډ | 0.2 | 1.5 | 0. .1 | | | 0 | 1.5 | ю. т | | |
| | of Tcp Lay | Material | | Bulk | Density | R/CE | | 1.79/2.05 | 1.70/2.05 | 1.70/2.05 | | | 1.70/1.80 | 1.70/1.80 | 1.70/1.80 | | |
| rain Matri | cteristics | Foundation | | Sh ear Wave | Velocity | <u>II sec</u> | | 260/400 | 260/400 | 260/400 | | | 260/550 | 260/550 | 260/550 | | |
| ised in Ter | Chara | | | Compres- sion Wave | Velocity | n'sec | | 655/1450 | 655/1450 | 655/1 ⁴ 50 | | | 655/2000 | 655/2000 | 655/2000 | | |
| n Factors | of | e. | | kougnness ras | Elevation | 6 | | 3.05 | 3.05 | 3.05 | | | 3-05 | 3-05 | 3.05 | | |
| Terrai | ucteristics | ace Materi | ity . | Spring | Travel | н | | 0.075 | 0.075 | 0.075 | | | 0-075 | 0.075 | 0.075 | | |
| | Chars | Surf | Rigio | Spring | Constant | 12/m | | 2.33 × 10 ⁷ | 2.33 × 10 ⁷ | 2.33 × 10 ⁷ | | | 2.33 × 10 ⁷ | 2.33 × 10 ⁷ | 2-33 × 10 ⁷ | | |
| | | | | Ter. Jin | Matrix | Element | | 26 | 27 | 28 | | | 8 | 30 | ц | | |

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| | | | | Qualitative Terrain Descriptors | Dry loose gravel overlying dense sand and gravel Dry louse gravel overlying cemented soil Dry loose gravel overlying weathered rock Dry loose gravel overlying hard clay Medium sand overlying dense sard and gravel Medium sand overlying ventheret soil. Medium sand overlying vesthered rock Medium sand overlying hard clay Medium sand overlying hard clay Medium sand overlying hard clay Medium sand overlying hard clay Medium sand overlying hard clay | Moist sandy or silty clay overlying cemented soil Moist sandy or silty clay overlying veathered rock Moist sandy or silty clay overlying hard clay | Dry loose gravel rværlying poorly consolidated calcareous silt or clay (aarl) Dry loose gravel overlying sandy consolidated gravel (conglomerate) Medium sand overlying poorly consolidated cal- careous silt or clay (marl) Medium sand overlying sandy consolidated gravel (conglomerate) Moist sandy or silty clay overlying poorly con- solidated gravel (conglomerate) Moist sandy or silty clay overlying sandy con- solidated gravel (conglomerate) | Dry loose gravel overlying competent unveathered rock Medium sand overlying competent unveathered rock Moist sandy or silty clay overlying competent un- veethered rock | |
|-------------|---------------------------|----------------|-----------------------|---------------------------------|--|--|---|---|------------|
| | | | | No. | 10.10 10.20 10.30 10.40 10.60 10.60 10.80 | 10.91 10.92 10.93 | 11.10 11.30 11.50 11.50 | 12.10 12.20 12.30 | |
| | 7 | First | Thick- ness | Ħ | 0.25 1.50 4.00 | | 0.25 1.50 4.00 | 0.25 1.50 { | (1 |
| | of Top Layer Material | | Bulk Density | g/cm ³ | 01.2/07.1 01.2/07.1 | | 1.70/2.30 1.70/2.30 1.70/2.30 | 1.70/2.50 1.73/2.53 1.70/2.55 | (Continued |
| ain Matrix | cteristics Coundation | Shear | Wave Velocity | m/sec | 260/750 260/750 260/750 | | 260/1100 260/1100 22/1100 | 260/1500 260/1500 260/1500 | |
| sed in Terr | Charad | - verumoj | sion Wave Velocity | m/sec | 655/2000 655/2000 655/2000 | | 655/2750 655/2750 655/2750 | 655/3500 655/3500 655/3500 | |
| n ractors U | of | Roughness | rms Elevation | 빙 | 3.05 3.05 3.05 | | 3.05 3.05 3.05 | 3.05 3.05 3.05 | |
| lerrai | cteristics ace Materia | îty Marîmim | Spring Travel | Ħ | 0.075 0.075 0.075 | | 0.075 0.075 0.075 | 0.075 0.075 0.075 | |
| | Chara | higid. | Spring Constant | <u>и/н</u> | 2.33 × 10 ⁷ 2.33 × 10 ⁷ 2.33 × 10 ⁷ | | 2.33 × 10 ⁷ 2.33 × 10 ⁷ 2.33 × 10 ⁷ | 2.33×10^{7} 2.33 × 10 ⁷ 2.33 × 10 ⁷ 2.53 × 10 ⁷ | |
| | | | Terrein Matriz | Element | 37 33 35 | | 35 37 | 38 39 4:0 | |

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| | | | Qualitative Terrain Descriptors | Wet medium dense sand Moist medium gr yel Heavy gravelly clay (till) | Wet medium dense sand overlying frozen silty or clayey loam Wet medium dense sand overlying dense cohesionless soil with high water table | Moist medium gravel overlying frozen slity of clayey loam | Moist medium graver overlying works and soil with high water table Heavy gravelly clay (till) overlying frozen silty | or ciayey loam Heavy gravelly clay (till) overlying dense cohesicnless soil with high water table | Wet medium dense sand overlying dense sand and | gravel Wet medium dense sand overlying cemented scil Wet medium dense sand overlying vesthered rock Wet medium dense sand overlying hari cley Meit medium gravel overlying dense sand and | gravel by Moist medium gravel overlying cemented soil voist medium gravel overlying veathered rock | Moist medium gravel overlying hard clay Heavy gravelly clay (till) overlying dense sand | and gravel Heavy gravelly clay (till) overlying cemented soil 2 Heavy gravelly clay (till) overlying vesthered | rock 3 Heavy gravelly clay (till) overlying herd clay | (Sheet 5 of 7) |
|------------|---------------------------------------|--------------|--------------------------------------|--|--|--|--|---|--|---|--|--|--|--|----------------|
| | | | No. | (13.10 13.20 13.30 | 14.10 14.20 | 14.30 | 02.41 | 14.60 | 15.10 | 15.20 15.30 15.40 | | - 51 - 12 - 12 - 12 - 12 - 12 - 12 - 12 - 1 | 15.91 | 15.9 | • |
| | r/ 7: | Layer | ness | 10.0L | | 0.25 | D. 4 | | | | 0.25 | 0.4.0 | | | ued) |
| | of Top Laye [aterial | ; | burk Density g/cm ³ | 1.90 | | 1.90/1.80 | 00.1/06.1 08.1/06.1 | | | | 1.90/2.10 1.90/2.10 | 1.90/2.10 | | | (Contin |
| is. Matrix | eristics of h | Shear | Wave Velocity m/sec | 100 | | 400/550 | 400/550 400/550 | | | | 1,00/750 | 100/120 | | | |
| anna ta | Character For | Compres- | sion Wave Velocity m/sec | 1450 | | 1450/2000 | 1450/2000 1450/2000 | | | | 1450/2000 | 1450/2000 | | | |
| | n ractors us of al | Roughness | ras Elevation cm | 1.90 | | 1.90 | 1.90 1.90 | | | | 1.90 | 1.90 1.90 | | | |
| | <u>Terral</u> eristics e Materi | y Maximun | Spring Travel m | 0.05 | | 0.05 | 0.05 J.05 | | | | 0.05 | 0.05 0.05 | | | |
| | Charact Surfac | Figidit | Spring Constant N/m | 5.43 × 10 ⁷ | | 5.43 × 10 ⁷ | 5.43×10^7 5.43×10^7 | | | | 5.43 × 10 ⁷ | 5.43 × 10' 5.43 × 10 ⁷ | | | |
| | | | Terrain Matrix El cent | I ¹ | | F2 | тт гт | | | | 45 | 54 F1 F1 | | | |

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| | | | | | | | Qualitative Terrain Descriptors | Wet medium sand overlying competent unveathered | rock | Moist medium gravel overlying competent urveathered rock | Heavy gravely clay (till) overlying competent unvestived rock | Frozen silty or clayey loam Dense cohesionless soil with high water table | Frozen silty or clayey loam overlying poorly con- | Frozen silty or clayer loam overlying sandy con- | solidated gravel (conglomerate) | Dense conesionless soil With high water table overlying sandy consolidated gravel (conglomerate) | Frozen silty or clayey loam overlying competent | unweathered rock Dense cohesionless soil with high water table | overlying unvesthered rock | Dense sand and gravel Cemented residual soil Hard clay Weathered rock |
|-------------|--------------|-------------|---------|-----------|-----------|-----------|---------------------------------|---|------------|---|--|--|---|--|---------------------------------|--|---|---|----------------------------|--|
| | | | | | | | No. | 01.91 | | 16.20 | 15.30 | 17.10 17.20 | /18.10 | 18.20 | | 05.01 | 01.01 | 10.20 | | 20.10 20.30 20.40 |
| | - | | First | Layer | Thick- | ness | Ħ | | 0.25 | 1.50 < | 1.00 | 10.0 | | 0.25 | 1.50 < | h.00 | 0.25 (| 1.50 | ₽.00 | 10.0 |
| | of Top Layer | faterial | | | Bulk | Density | g/cm ³ | | 1.90/2.50 | 1.90/2.50 | 1.90/2.50 | 1.80 | | 1.80/2.30 | 1.80/2.30 | 1.80/2.30 | 1.80/2.50 | 1.80/2.50 | 1.80/2.50 | 2.10 |
| ain Matrix | teristics : | oundation ! | | Shear | Wave | Velocity | m/sec | | 400/1500 | 4:00/1500 | 1400/1500 | 550 | | 250/1100 | 250/1100 | 00TT/0 <u>5</u> 5 | 550/1500 | 550/1500 | 550/1500 | 75C |
| sed in Terr | Charac | 4 | | Compres- | sion Wave | Velocity | m/sec | | 1450/3500 | 1450/3500 | 1450/3500 | 2000 | | 2000/2750 | 2000/2750 | 2000/2750 | 2000/3500 | 2000/3500 | 2000/3500 | 2000 |
| n Factors U | of | 81 . | | Roughiess | SILLI | Elevation | B | | 1.90 | 1.90 | 1,90 | 2.54 | | 2.54 | 2.54 | 2.54 | 2.54 | 2.54 | 2.54 | 3.81 |
| Terraí | eristics | e Materi | y | Muximum | Spring | Travel | Ħ | | 0.05 | 0.05 | 0.05 | 0.025 | | 0.025 | 0.025 | 0.025 | 0.025 | 0.025 | 0.027 | 0.03 |
| | Charact | Surfac | Rigidit | | Spring | Constant | <u>м/т</u> | ٢ | 5.43 × 10' | 5.43 × 10 ⁷ | 5.43 × 10 ⁷ | 10.85 × 10 ⁷ | | 10.85×10^{7} | 10.85×10^{T} | 10.85 × 10 ⁷ | 10.85 × 10 ⁷ | 10.85 × 10 ⁷ | 10.85 × 10 ⁷ | 8.14 × 10 ⁷ |
| | | | | | Terrain | Matrix | Element | | 49 1 | 6 1 | 50 | Σ | | 52 | 53 | Ţ. | 55 | 56 | 57 | 58 |

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Table 15 (Concluded)

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e adviced with a second of the Hickory desired with

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| | | | | Qualitative Terrain Descriptors | Dense sand and gravel overlying frozen silty or | Dense sand and gravel overlying dense cohesionless | soil with high water table Cemented soil overlying frozen silty or clayey | | Cemented soil overlying dense consionless soil with high water table | Hard clay overlying frozen silty or clayey loam Hard clay overlying dense cohesionless soil with high water table | Dense sand and gravel overlying competent un- | veatnered rock Cemented residual soil overlying competent un- | weathered rock | Hard clay overlying competent unweathered rock Weathered rock overlying competent unweathered rock | Hard cemented clay (hardpan) | Boulder till Compact cobbly and bould ery material Moderately haid shale or sandstone | Competent slightly weathered rock | Solid or massive ice (Ice cap) | Ice overlying dense sand and gravel | Ice overlying vesthered rock | | |
|-------------|-------------------------|---------|-----------------------|---------------------------------|---|--|--|------------------------|---|---|---|--|----------------|--|------------------------------|--|-----------------------------------|--------------------------------|-------------------------------------|------------------------------|------------------------|----------------|
| | 1 | | | No. | 01.12 | 21.20 | 21.30 | | 21.40 | 21.50 | (22.10 | 22.20 | | 22.40 | 23.10 | 23.20 23.40 23.40 | 24.00 | 25.00 | 26.10 | 26.20 | | |
| | r/ | First | Layer Thick- | Dess | | | 0.25 | 1.50 | h.00 | | | 0.25 | 1.50 | ¹⁴ .00 | _ | 10.00 | 10.00 | 10.00 | 0.25 | 1.50 ¢ | h.00 | |
| | of Top Laye Material | | Bulk | Density g/cm ³ | | | 2.10/1.80 | 2.10/1.80 | 2.10/1.80 | | | 2.10/2.50 | 2.10/2.50 | 2.10/2.50 | | 2.00 | 2.40 | 1.00 | 1.0/2.10 | 1.0/2.10 | 1.0/2.10 | |
| ain Matrix | teristics oundation | | Shear Wave | Velocity #/sec | | | 750/550 | 750/550 | 750/550 | | | 750/1500 | 750/1500 | 750/1500 | | 006 | 1200 | 1900 | 1900/750 | 1900/750 | 1900/750 | |
| sed in Terr | Charac | | Compres- sion Wave | Velocity m/sec | | | 2000/2000 | 2000/2000 | 2000/2000 | | | 2000/3500 | 2000/3500 | 2000/3500 | | 5400 | 3200 | 3700 | 3700/2000 | 3700/2000 | 3700/2000 | |
| Factors U | of J | | Roughness rms | Elevation cm | | | 3.81 | 3.81 | 3.81 | | | 3.81 | 3.81 | 3.81 | | 3.18 | 4 . μ5 | 1.20 | 1.20 | 1.20 | 1.20 | .: |
| Terrair | eristics e Materia | v | Maximum Spring | Travel | | | 0.03 | 0.03 | 0.03 | | | 0.03 | 0.03 | 0.03 | | 0.020 | 0.005* | 0.005 | 0.005 | 0.005 | 0.005 | pavement |
| | Charact Surfac | Rigidit | Sprinz | Constant N/m | | t | 8.14 × 10 ⁷ | 8.14 × 10 ¹ | 8.14 × 10 ⁷ | | ł | 8.14 × 10 ¹ | S.14 × 10 | 8.14 × 10 ⁷ | | 12.40 × 10 ⁷ | $1.8 \times 10^{10^{H}}$ | 1.8 × 10 ¹⁰ | 1.8 × 10 ¹⁰ | 1.8 × 10 ¹⁰ | 1.8 × 10 ^{-U} | surface; not a |
| | | | Terrain | Matrix Element | | | 59 | 60 | 61 | | | 62 | 63 | 61 | | 65 | 99 | 67 | 68 | 69 | 70 | Rock E |

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| Table 16 | ŝ |
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| | | | Slope |
|----|--|-------|------------------|
| | | Range | Areal Occurrence |
| | Category | . , | |
| 1. | Plains (generally level) | < 10 | >90 |
| | | > 30 | < 10 |
| 2. | Plains (Undulating or rolling) | < 10 | 50-90 |
| | | > 30 | < 10 |
| 3. | Tablelands and plateaus** | < 10 | 50-90 |
| | | > 30 | 10-25 |
| 4. | Plains and hills or mountains complex † | < 10 | 50-90 |
| | | >30 | 10-25 |
| 5. | Hi 11s | < 10 | < 50 |
| | | >30 | 10-50 |
| 6. | Mountains | < 10 | < 25 |
| | | >30 | >50 |

* Sampled from Peterence 31.

>* deather steped occur at higher elevations. Patter planet seem at lower elevations.

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| Table | 1 | 7 |
|-------|---|---|
|-------|---|---|

Surface Soil Categories*

| <u> </u> | Surface Soil Texture** (Upper 15 cm) | Range in Sand | n Composition Silt | on (2) [†] <u>Clay</u> |
|----------|---|------------------|-----------------------|------------------------------------|
| 1. | Sand ⁺⁺ | 85-100 | 0-15 | 0-1 0 |
| 2. | Sand and loam | | | |
| 3 | Sand and clay | | | |
| 4. | Sand and organic material | | | |
| 5. | Sand and bare area | | | |
| 6. | Loam | 23-52 | 28-50 | 7-27 |
| 7. | Loam and silt | | | |
| 8. | Loam and clay | | | |
| 9. | Loam and organic material | | | |
| 10. | Loam and bare area | | | |
| 11. | Silt | 0-20 | 80-100 | 0-12 |
| 12. | Silt and clay | | | |
| 13. | Clay | 0-45 | 0-40 | 40-100 |
| 14. | Clay and bare area | | | |
| 15. | Organic material | | | |
| 15. | Bare area‡ | | | |

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* Adapted from Reference 32.

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** Where two scil categories are identified means that two textures or conditions are extensive in the area mapped; the second texture or condition is of equal or lesser areal extent than the first.

+ Adapted from Reference 33.

++ Includes particles coarser than sand (e.g. gravel).

+ Areas generally devoid of soil.

Subsurface Lithologic Categories*

| | Rock Category | Rock Types |
|----|---------------------|---|
| 1. | Consolidated rock | Igneous and metamorphic rocks, well- consolidated sedimentary rocks, mixed or intermingled rock types |
| 2. | Unconsolidated rock | Weakly consolidated or unconsolidated sedi- mentary rocks |
| 3. | Alluvium | Restricted to detrital deposits of streams |
| 4. | Ice cap | Frozen material plus ice blocks |

* Adapted from Reference 34.

| | Water-Table Regime | Description | | | |
|------------|------------------------|--|--|--|--|
| 1. | Permafrost | Includes areas of continuous permafrost, where very little land is unfrozen; and areas of discontinuous permafrost, where scattered patches of unfrozen land occur | | | |
| ٺ . | High water table | High-water-table conditions can be ex- pected most of the year. Water table generally <5 m deep | | | |
| 3. | Water Table fluctuates | Water-table conditions cannot be pre- dicted with any degree of accuracy | | | |
| 4. | low water table . | Low-water-table conditions can be ex- pected most of the year. Water table generally >5 m deep | | | |
| 5. | Rock a ice | Ice caps and rocky areas where water- table conditions are not considered significant | | | |

Table 19 State-of-Ground Categories*

* Adapted from References 32 and 35...

| | | | Average Plant | | | |
|-----|--------------------------------------|---------------------|--------------------------|------------------|--|--|
| | Category * | | Height, m** | Coverage, %t | | |
| 1. | Needleleaf forest | | 15.0 - 35.0 | 75-100 | | |
| 2. | Broadleaf forest | | 15.0 - 35.0 | 75-100 | | |
| 3. | Mixed needleleaf and broadlea | 15.0 - 35.0 | 75-100 | | | |
| 4. | Montane forest | | 2.0 - 10.0 | 50-100 | | |
| 5. | Savanna | Woody: Nonwoody: | 5.0 - 10.0 0.5 - 2.0 | 50-100 75-100 | | |
| 6. | Forest and grassland | Woody: Nonwoody: | 10.0 - 15.0 0.5 - 1.0 | 25-50 50-100 | | |
| 7. | Woodland and scrubland | | 2.0 - 5.0 | 50-100 | | |
| 8. | Tundra and alpine | | 0.1 - 2.0 | 50-100 | | |
| 9. | Grassland | | 0.2 - 1.0 | 50-100 | | |
| 10. | Semidesert scrub and desert | | 0.2 - 5.0 | >0-50 | | |
| 11. | Barren | | | - | | |
| 12. | 2. Commercial grain and horticulture | | 0.5 - 2.0 | 50-100 | | |
| 13. | . Commercial plantation | | 2.0 - 15.0 | 50-100 | | |

| | j | 20 | | | |
|------------|------------|------|----------|-----------------|--|
| Vegetation | Categories | with | Selected | Characteristics | |

(infinite)

* Adapted from Reference 36.

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** Average height of plants in the main vegetation layer.

+ Area of ground covered by vegetation.
| Map Unite | Surface Configuration | Solls | Lithology | State of Ground | 'Vegetation | Map Unit | Surface Configuration | Soils | Lithology | State of Ground | Vegetation | Map Unit | Surface Configuration | Soils | Lichology | State of Ground | Vegetation |
|--|-----------------------|---|---|--|--|--|-----------------------|--|--|--|---|---|--|--|---|---|--|
| $\begin{array}{c} 1 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 20 \\ 21 \\ 22 \\ 23 \\ 31 \\ 13 \\ 22 \\ 33 \\ 34 \\ 35 \\ 15 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 1$ | | 103 01 02 02 02 02 02 02 02 02 02 02 02 02 02 02 02 02 <td>111111222222222333111112222222222222222</td> <td>E35 344441233444434434441111222333344444</td> <td>Contemporary Contemporary Conte</td> <td>54 55 59 60 12 34 55 59 60 62 63 64 56 67 89 71 73 74 57 77 78 79 80 82 83 84 856 87 88 88</td> <td></td> <td>CS O6 O6<</td> <td>JT 1111111111122222222222222222222222222</td> <td>35 22233333344445112222233333444444422</td> <td>334 05 09 10 23 5 10 <td< td=""><td>H H H 107 108 109 108 109 110 111 112 113 113 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141</td><td>"SS 11111111111111111111111111111111111</td><td>08 09 09<</td><td>HT 22222222222222333333111122322232223333</td><td>115 1122333334442223344113311112323333333</td><td>33A1 092 020 000 122 000 000 122 000 122 000 122 000 122 000 122 000 122 000 122 000</td></td<></td> | 111111222222222333111112222222222222222 | E35 344441233444434434441111222333344444 | Contemporary Conte | 54 55 59 60 12 34 55 59 60 62 63 64 56 67 89 71 73 74 57 77 78 79 80 82 83 84 856 87 88 88 | | CS O6 O6< | JT 1111111111122222222222222222222222222 | 35 22233333344445112222233333444444422 | 334 05 09 10 23 5 10 <td< td=""><td>H H H 107 108 109 108 109 110 111 112 113 113 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141</td><td>"SS 11111111111111111111111111111111111</td><td>08 09 09<</td><td>HT 22222222222222333333111122322232223333</td><td>115 1122333334442223344113311112323333333</td><td>33A1 092 020 000 122 000 000 122 000 122 000 122 000 122 000 122 000 122 000 122 000</td></td<> | H H H 107 108 109 108 109 110 111 112 113 113 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 | "SS 11111111111111111111111111111111111 | 08 09 09< | HT 22222222222222333333111122322232223333 | 115 1122333334442223344113311112323333333 | 33A1 092 020 000 122 000 000 122 000 122 000 122 000 122 000 122 000 122 000 122 000 |
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| 162 | 2 | 01 | 1 | 4 | 09 | 215 | 2 | 02 | 2 | 3 | 07 | 268 | 2 | 05 | 2 | 2 | 01 |
| 163 | 2 | 01 | 1 | 4 | 10 | 216 | 2 | 02 | 2 | 3 | 09 | 269 | 2 | 06 | 2 | 2 | 02 |
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| 166 | 2 | 01 | 2 | 3 | 02 | 219 | 2 | 02 | 2 | 4 | 05 | 272 | 2 | 06 | 2 | 2 | 12 |
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| 174 | 2 | 01 | 2 | 4 | 08 | 227 | 2 | 02 | 3 | 4 | 07 | 280 | 2 | 06 | 2 | 3 | 00 |
| 175 | 2 | 01 | 2 | 4 | 09 | 228 | 2 | 03 | 1 | 3 | 05 | 281 | 2 | 06 | 2 | 3 | 12 |
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| 178 | 2 | 01 | 2 | 4 | 12 | 231 | 2 | 03 | ĩ | 4 | 05 | 284 | 2 | 06 | 2 | Å | 05 |
| 170 | 2 | 0. | 2 | Ś | 09 | 232 | | 03 | ĩ | 7 | 10 | 285 | - | 06 | 5 | 4 | ã |
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| 184 | 2 | 01 | 3 | 4 | 09 | 237 | 2 | 04 | 2 | 1 | 01 | 290 | 2 | 06 | 3 | 2 | 02 |
| 185 | 2 | 01 | 3 | 4 | 10 | 238 | 2 | 04 | 2 | 1 | 02 | 291 | 2 | 06 | 3 | 2 | 12 |
| 186 | 2 | 01 | 3 | 4 | 11 | 239 | 、2 | 04 | 2 | 1 | 08 | 292 | 2 | 06 | 3 | 3 | 02 |
| 187 | 2 | 01 | 3 | 4 | 12 | 240 | 2 | 04 | 2 | 3 | 01 | 293 | 2 | 06 | 3 | 3 | 09 |
| 188 | 2 | 02 | 1 | 1 | 01 | 241 | 2 | 04 | 3 | 2 | 02 | 294 | 2 | 06 | 3 | 3 | 12 |
| 189 | 2 | 02 | 1. | 1 | 02 | 242 | 2 | 05 | 1 | 4 | 09 | 295 | 2 | 06 | 3 | 3 | 13 |
| 190 | 2 | 02 | 1 | 1 | 08 | 243 | 2 | 05 | 1 | 4 | 10 | 296 | 2 | 06 | 3 | Ä | 12 |
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| 192 | 2 | 02 | 1 | 5 | 05 | 240 | 4 | 00 | 1 | 1 | 02 | 301 | 4 | 07 | - | 4 | 09 |
| 196 | 2 | 02 | 1 | 3 | 07 | 249 | 2 | 06 | 1 | 1 | 05 | 302 | 2 | 07 | 1 | 4 | 12 |
| 197 | 4 | 02 | 1 | 3 | 12 | 250 | 2 | 06 | 1 | 1 | 80 | 303 | 2 | 07 | 2 | 2 | 01 |
| 198 | 2 | 02 | 1 | - 4 | 02 | 251 | 2 | 06 | 1 | 2 | 02 | 304 | 2 | 07 | 2 | 3 | 01 |
| 199 | 2 | 02 | •• | 4 | 05 | 252 | 2 | 06 | 1 | 2 | 05 | 305 | 2 | 07 | 2 | 3 | 03 |
| 200 | 2 | 02 | 1 | 4 | 07 | 253 | 2 | 06 | 1 | 2 | 09 | 306 | 2 | 07 | 2 | - 4 | 09 |
| 201 | 2 | 02 | 1 | 4 | 09 | 254 | 2 | 06 | 1 | 3 | 01 | 307 | 2 | 07 | 2 | 4 | 12 |
| 202 | 2 | 02 | 1 | 4 | 10 | 255 | 2 | 06 | 1 | 3 | 02 | 308 | 2 | 08 | 1 | 1 | 01 |
| 203 | 2 | 02 | 2 | 1 | C1 | 256 | 2 | 06 | ī | ñ | 03 | 309 | 2 | 08 | 1 | 1 | 08 |
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| 211 | 2 | 02 | 2 | 3 | 01 | 264 | 2 | 06 | 1 | 4 | 07 | 317 | 2 | 08 | 1 | 3 | 07 |
| 212 | 2 | 02 | 2 | 3 | 02 | 265 | 2 | 06 | 1 | 4 | 09 | 318 | 2 | - 08 | 1 | 3 | 08 |

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องนั้น มากกะ และสำหรับข้างก่องในสมให้แข่งประสิทธิศกับการก่อนี้ทางและสมไห้เป็นหลังได้

| Mart. Unite | Sui Ince Configuration | Sotta | Ltchology | State of Ground | Veretion | May Und C | Surface Configuration | Soils | Lithology | State of Ground | Vezation | Map Unit | Surface Configuration | Soils | Lithology | State of Ground | Vegetation |
|---|---|--|---|--|---|--|---|--|---|---|--|--|-----------------------|--|--|---|--|
| $\begin{array}{c} \textbf{319} \\ \textbf{320} \\ \textbf{322} \\ \textbf{322} \\ \textbf{322} \\ \textbf{322} \\ \textbf{322} \\ \textbf{323} \\ \textbf{323} \\ \textbf{333} \\ \textbf{33445} \\ \textbf{34567} \\ \textbf{3353} \\ \textbf{35567} \\ \textbf{3567} \\ \textbf{35661} \\ \textbf{35667} \\ \textbf{35677} \\ \textbf{35667} \\ \textbf{35677} \\ \textbf{35777} \\ \textbf{357777} \\ \textbf{357777} \\ \textbf{35777} \\ \textbf{35777} \\ \textbf{35777} \\ \textbf{357777} \\ \textbf$ | 222222222222222222222222222222222222222 | 08 09 09 09 09 09 | 1 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 | 333444444441111222233333333334444422334411113511522332 | 09 12 13 01 02 07 09 10 12 10 00 12 00 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 09 12 00 00 00 12 00 00 12 00 00 00 00 12 00 00 00 00 00 00 00 00 00 00 00 00 00 | 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 399 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 419 420 421 422 422 | 222222222222222222222222222222222222222 | 11 12 13 13 13 13 13 13 13 13 13 13 | 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 3 3 3 1 1 2 2 1 1 1 1 | 3323134422233334442233323344445445543543344444444 | 03 12 09 09 01 02 05 07 02 05 00 02 05 07 02 00 00 00 00 00 00 00 00 00 00 00 00 | $\begin{array}{c} 425\\ 426\\ 427\\ 428\\ 429\\ 430\\ 431\\ 432\\ 433\\ 434\\ 435\\ 436\\ 437\\ 438\\ 439\\ 440\\ 444\\ 443\\ 444\\ 444\\ 444\\ 445\\ 444\\ 445\\ 446\\ 447\\ 448\\ 449\\ 455\\ 455\\ 455\\ 455\\ 455\\ 455\\ 455$ | 。 | $\begin{array}{c} 02\\ 02\\ 02\\ 02\\ 02\\ 02\\ 03\\ 03\\ 04\\ 05\\ 06\\ 06\\ 06\\ 06\\ 06\\ 06\\ 06\\ 06\\ 06\\ 06$ | 1111121111112111111111111111111111222222 | 4444443443344111122333333344444444533333444444243334444 | 04 05 07 09 10 05 02 50 25 02 50 02 05 0 02 05 0 02 05 00 0 02 05 0 02 05 0 0 0 0 |
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| Map Unite | Surface Configuration | Satts | Lichology | State of Ground | Vegetation | Map Unit | Surface Configuration | Soils | Lithology | State of Ground | Vegetation | Map Unit | Surface Contiguration | Soils | Lithology | State of Ground | Vegetation |
| Ima 7890123488345678890123456789011234567890012334567890012334565555555555555555555555555555555555 | ms 3333333333333333333444444444444444444 | 08 03 08 09 09 10 11 13 13 13 13 13 15 01< | 77 22211111121111111111111111222222223311 | 2;;] 3441151134344411333344444445333444444413 | C3A 0270 0270 0880 122245 000 | Solution Solution Solution Solution< | INS 444444444444444444444444444444444444 | 105 02 03 03 03 03 03 03 03 05 05 05 05 05 05 05 05 05 05 05 05 06 | JFI 1122222222231111122211111111112222111111 | etg 4433334444434444444433444444444444444 | $\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array}\\ \end{array}\\ \end{array} \\ 10 \\ 12 \\ 02 \\ 05 \\ 12 \\ 04 \\ 05 \\ 10 \\ 02 \\ 04 \\ 07 \\ 10 \\ 02 \\ 04 \\ 07 \\ 10 \\ 05 \\ 07 \\ 10 \\ 05 \\ 00 \\ 10 \\ 05 \\ 00 \\ 10 \\ 05 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 10 \\ 00 \\ 00 \\ 10 \\ 00 \\ 00 \\ 00 \\ 00 \\ 10 \\ 00 \\ 00 \\ 00 \\ 10 \\ 0 \\ 0 \\ 0$ | IED S84 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 6004 605 6006 607 6010 612 611 6112 612 616 617 618 619 620 621 621 622 623 | 1115 4444444444444444444444444444444444 | 100 06 08 | III 11112222222222222222222222222222222 | tts 4444223333344444444444422333334444442337 | δgA 09 101 112 200 02 04 05 07 010 011 02 03 04 05 06 07 08 010 12 02 04 05 07 012 02 02 04 05 07 012 02 02 04 05 07 102 02 04 05 07 102 12 02 04 05 07 102 12 02 04 05 07 102 12 12 02 04 05 07 102 12 12 02 04 05 07 102 12 12 02 04 05 07 10 12 12 02 04 05 07 10 12 12 02 04 05 07 10 12 12 04 05 07 10 12 12 04 05 07 10 |
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| Map Vat e | Surface Configuration | Soila | Litiology | State of Ground | Vegetation | Map Brite | Surface Configuration | Sotts | Lit thology | State of Stouid | Vegatation | Aan. | Unic | Surface Configuration | Solls | Lichology | state of Ground | Vegetation |
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| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | Mat. Vist i | Surface Configuration | Solls | LILIOIOGY | Scate of Ground | Vegetation | Map Unic | Surface Configuration | Sofis | Lithology | State of Ground | Vegotation | Kap Unic | rface Configuration | sti | -1thology | Stare of Ground | Vegetation |
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Table 21 (Concluded)

| May Unde | Surface Configuration | Solis | Lithulogy | State of Ground | Vegetation | Man Unic | Surface Configuration | Sofis | Lithology | State of Ground | Vegetation | Map Unit | Surface Configuration | Soils | Lithology | State of Ground | Vegetation |
|--|---|---|---|--|---|--|------------------------|---|--|--|--|-------------|-----------------------|-------|-----------|-----------------|------------|
| 955 956 957 958 960 961 962 963 966 965 966 967 968 967 973 974 975 977 978 977 978 977 978 979 981 985 987 988 982 983 985 988 989 990 991 992 993 994 995 998 999 995 997 998 999 997 1000 1001 1006 1007 | 660666666666666666666666666666666666666 | 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 08 09 09 09 09 09 09 09 09 09 09 09 09 10 10 10 10 13 13 13 13 | 11111222222222222222333311111122222111111 | 4455522333333333444442234411223311133233333332233442123344 | 12 13 01 102 12 02 04 05 06 07 08 12 02 05 06 07 08 12 02 02 02 12 02 02 02 12 02 02 02 03 00 08 01 08 01 08 01 08 02 03 01 08 01 02 02 02 03 00 03 02 03 02 03 02 03 00 03 02 03 00 03 02 02 03 00 03 00 03 00 03 00 00 00 00 00 00 | 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 1040 1041 1042 1043 1044 1044 1045 1044 1045 1046 1047 1052 | ********************** | 133333344444555556666%%666666666666666666 | 1222223311:22111222111111111111111111222333444 | 4133342233331334131233444444444555555235245155 | 058120822224248122282818110257801121257781111111118811 | | | | | | |

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Table 22

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Matrix Element Terrain Da rithtors Associated With Inematic Factors Used To Compile 'actor Complex Mar of the World

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| | 3 | Barren | 0 | 0 | н | ٥ | 0 | 0 | ы | • | 0 | • | 0 | 0 | 0 | 9 | 0 | 0 | ч | н |
| | ន | 5 Desert Scrub 5 Devert | 0 | 0 | н | 0 | 0 | 0 | щ | • | 0 | н | 0 | Ö | ç | G | 0 | ٥ | ы | н |
| | 6 | bnalesar0 | • | o | 0 | н | 0 | 0 | 0 | H | 0 | н | ы | H | o | 7 | н | ٥ | 0 | н |
| ø | 80 | anigiA AigiA | 0 | 0 | ٥ | 0 | 0 | 0 | 0 | 0 | ¢ | н | Ċ | 0 | 0 | 0 | 0 | o | н | ы |
| tatio | 01 | Serubland & | 0 | 0 | н | o | 0 | 0 | н | 0 | 0 | н | 0 | 0 | 0 | 0 | 0 | ø | ч | н |
| Vege | 90 | 3 Jaerol Donleenvo | 0 | c | o | н | 0 | 0 | 0 | н | ¢ | -1 | ы | Ч | 0 | н | н | 0 | o | o |
| | 3 | annava3 | c | ç | 0 | 0 | 0 | 0 | c | 0 | 0 | н | Ċ | 0 | 0 | 0 | c | 0 | 0 | 0 |
| | 94 | Montane | 0 | o | 0 | 0 | 0 | • | 0 | 0 | 0 | н | • | с) | 0 | 0 | • | • | ¢ | • |
| | 55 | Mixed Fornet | 0 | • | 0 | ч | 0 | 0 | 0 | н | ٩ | н | ы | ٦ | 0 | ч | ы | c | 0 | • |
| | C2 | Broadleaf Forest | 0 | J | ٥ | н | ۰ | 0 | 0 | н | 0 | н | н | н | 0 | м | н | 0 | c | 0 |
| | 5 | lsalaibaaN Porest | 0 | 0 | 0 | н | o | • | Ö | н | 0 | н | г | н | ۰ | н | н | • | 0 | • |
| | ۳, | Rock of Ice | Ö | Q | 0 | 0 | o | ٥ | 0 | 0 | Ċ | 0 | • | 0 | 0 | 0 | 0 | 0 | S | • |
| tound | 4 | Low Water Table | 0 | н | ч | 0 | 0 | 0 | ч | 0 | 0 | 0 | 0 | • | 0 | 0 | 0 | н | -1 | н |
| of C | e | Mater Table Badauseult | ы | ы | • | 0 | ч | н | ۰ | 0 | ы | н | 0 | 0 | o | 0 | 0 | ч | н | ч |
| State | 5 | High Water Table | 1 | н | 0 | н | ы | н | 0 | ы | ч | н | ы | ч | ч | Ċ | ы | 0 | • | 0 |
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| ttolog | М | Unconsolidated Bock | 0 | 7 | ы | ы | 0 | н | г | ы | н | н | н | ٦ | ч | н | н | н | н | - |
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| | 12 | Bare Area | 0 | o | 0 | ئ | 0 | 0 | 0 | • | ¢ | ç | • | o | 0 | o | c | c | c | o |
| | ື່ມ | Material Material | 0 | ŝ | 0 | c | 0 | c | o | 0 | 0 | 0 | 0 | o | ø | 0 | • | 0 | r, | o |
| | 71 | Clay & Bare | Ċ | н | ٥ | ١Ħ | • | н | • | ч | ы | ى | -1 | н | +1 | щ | н | Ч | 0 | 0 |
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| ter. | 3 | Loam & Bare | ч | o | • | 0 | н | 0 | c | • | ¢ | 0 | 0 | 0 | н | 0 | 0 | 0 | o | o |
| re (u | 60 | Organic Matecial | н | 0 | 0 | 0 | ч | 0 | 0 | o | 0 | 0 | 0 | • | . 1 | ю | 0 | 0 | ¢ | 0 |
| 1110 | 88 | Loan & Clay | ы | н | 0 | н | Ħ | н | 0 | н | н | 0 | | н | н | ч | السو | ч | 0 | 0 |
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| ur fa | 8 | mao.l | н | o | 0 | 0 | н | 0 | 0 | 0 | Ċ | 0 | 0 | 0 | н | 0 | 0 | 7 | 0 | 0 |
| 5 | 6 | Sand & Bare | 0 | 0 | н | 0 | 0 | 0 | н | · ` | 0 | ч | 0 | c | н | <i>с</i> . | 0 | ¢ | -1 | |
| 203 | 04 | Sand 6 Organic Internet | 0 | 0 | ч | 0 | 0 | 0 | н | 0 | o | м | 0 | • | • 1 | 0 | 0 | 0 | ч | н |
| | E0 2 | Sand & Clay | 0 | н | н | н | 0 | н | н | ч | н | н | н | ٣ | н | ٦ | ч | ч | м | ы |
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| 1.10.4.1 | 4 | Plains & Hills or Mts Complex | н | н | -4 | -4 | 1 | ч | ч | ч | F-1 | | н | | ы | ч | н | н | ы | н |
| ، مدارز د | 5 | Tablalandr & Plateaus | н | н | ы | ы | н | ч | г | н | ч | . - | 7 | | н | •-1 | •-4 | ы | г | ы |
| | 17 | Rolling Prains | ч | н | ы | н | н | ч | н | T | F | н | ч | | н | н | ч | ч | ч | н |
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| | | Terrain | I.I. | 1.2 | Г.1 Г.1 | 1.4 | 2.1 | 2.2 | 2.3 | 2.4 | 3.1 | 3.2 | 3.3 | 3.4 | 4.1 | 4.2 | 4.3 | 5.1 | 5.2 | 5.3 |

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| wner 11 cm) | 10 11 12 13 14 15 16 | Bara & Bara Sile & Clay Clay & Bara Clay & Bara Diagante Di Diagante Di Diagante Di Diagante Diagante Diagante | C 1 1 C O C O | | 0 1 1 1 0 0 | 0011100 | T 0 T 0 0 T | 0 0 0 0 0 0 0 0 | 0 0 0 0 0 0 0 | LILL L O O ⁱ O | 1111 1 0 0 ⁰ 0 | 0 5 0 1 1 1 0 0 | 0011100 | 0 0 0 0 0 0 0 0 | | | 1000101 | 0 0 0 1 1 1 0 0 | 01111.000 | 0 1.1 1 0 0 0 | 1000101 | 1000101 | (¢ m 2) |
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| rface fexture (unser 15 cm) | 06 07 38 09 10 11 12 13 14 15 16 | Loam Loam 6 SLIC Loam 6 Clay Loam 6 Clay SLIC 6 Clay SLIC 6 Clay Clay Clay Clay Clay Clay Clay Clay | 010 0 0110 0 00 | 0000 0 0000 0 000 | 0 1 1 0 0 1 T I 0 0 ¹ | 0010001000 | 0 0 0 1 0 0 1 0 0 0 1 | 0 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 ₁ 00111111100 | LIL L LLLL L 0 0'0 | 001000100000000000000000000000000000000 | 00100010000 | 000 0 0 0 0 0 0 0 0 | 0 1 1 0 0 1 1 1 0 0 1 | 001 0 0011 1 6 6 1 | 0000 0 1000 1 0 1 1 | 0.011100010100 | 011 0 0111 1.0 0 0 | 5 1 1 0 0 1.1 1 1 0 0 0 | 0 0 0 0 1 0 0 0 1 0 1 1 | | (tan |
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Table 22 (Continued)

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Table 23

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Printout of Thematic Map Legend and Corresponding Terrain Matrix Elements

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| | 11.48 12 | | 11 21 11 | 21.11 21 | 12.10 14 | | 11.51 11 | 10.68 10 | 11.34 74 | | 18.68 18 | 7.110 7 | 11.11.11 | 18. 4H 18 | 7.24 14 | 10,00 | | | | 12.28 | | | | | | 9.40 13 | | | 8.50 11 | 8.58 14 | 7.28 . | 11.80 11 | | 11.74 10 | 18,78 14 11,78 14 | | | | | | 61 8¥*6 |
| | 11.20 | 12.21 | | | | | 1.51 | e 10.58 | 0 14.90 | | | | 0 1 u . H 0 | 8 14.58 | | 11.68 | 0 10.10 | 12.20 | 8 12.23 | 11.45 | 0 14.10 | | | | | | : | | | | 1 0.13 | 11./6 | | 11.61 | 91.19 | | | | | | E+•# # |
| s | 21 37 18.7 | 74 11 .4 | | 24 14 1 | 1.8.42 | | 4.4 EC | 39 8.4 | | | 2.8 82 2.8 82 | 3.6 5.2 | 1.01 10./ | 4.8 65 | 31 5.2 | 2.81 45 | 74 12.2 | 70 11.4 | 74 11.6 | 14 10.7 | 19 17.1 | 14 17.1 | | | | 1.1 8.3 | ; ; ; | | | 1.1 | 21 5.3 | 58 18.6 | | 51 11-5 | | | 2 S #2 | | | | |
| TERAAM DESculetue | 10.70 12. 5.JR 18. | 5. 38 19. | , 14 18. 1 | 9.18 4. | J. 78 R. | 21.41 | J.78 B. | | 11.54 11. | 1.39 7. | | | 11.50 11. | 3.78 8. | 1.34 2. | 5.24 7. | 4.14 1B. | 6.14 10. | 6.14 18. | 5.39 4. | 0.38 14. | 9.35 14. | | | 12 02.12 | 3.24 6. | 21.24 21. | | | 1.28 | 3.28 5. | 11.15 14. | 20.24 | 6.13 B. | A.13 7. | 6.13 16. | 1.38 2. | | | 71.40 | 3,74 4. |
| VEGETATION | 5 r | | 2: | | . • | • | ~ | ~ | s i | | £ | | | 2 | 11 | 12 | | | ŝ | \$ | - | ~ ` | • • | c | • | 2 | • | n, • | | • • | - | | | ~ | • | • | • | • | • • | ł | - |
| STATE OF GRUUND | | • | • • | • | •~ | | - | - | 4 | Ŧ | | | | n | - | • | -7 | • | 4 | 4 | - | | | - • | • | Ň | | ~ • | | | | | | 4 | • | • | • | • | r n | ŀ | • |
| L I ThØI 047 | - | | | - ~ | | • | ~ | 2 | ~ : | 2 | | . ~ | | -, | - | ſ | | - | - | | ~ | ~ 1 | ~ • | . • | | ~ | | ~ 1 | | | • | | | 2 | ~ | ~ | ~ | • | • • | | ۰ |
| 50115 | | - | -1 - | | . | | - | - | - | - | - | · _ | | - | - | ľ | ~ | • | ~ | N | ~ | ~ 1 | | . • | 4 | ~ | | N (| •• | . • | . N | | | ~ | • | ~ | ~ | • | ~ ~ | ł | ~ |
| SURFACE CONFICII+ PATION | | - | -1 - | | • •• | • | - | - | - | - | - | | | • | - | - | - | | | - | | | | - • | • | - | | | - • | • • | | • | | - | | - | -1 | • | | | - |
| NAP UNIT | - ~ | . | . | • | • | | * | ¢ | 2 | 11 | 12 | : 2 | | : | 1 | 16 | 11 | : : | 19 | 24 | 22 | 22 | | | | ** | | 14 | : | | 17 | 1 | | 32 | 2 | * | ŝ | | | | # 10 |

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Table 24

Seismic Response Ranking of the Terrain Matrix Elements

| Predicted Selsmic Response - Class 14 | T | 2 | ٣ | 4 | 5 | Ŷ | 7 |
|--|---|-------------------|--|---|-------------------------------------|---|---|
| Terrain Descriptor Number | 1.10-1.20-1.30-1.40-2.10-2.20-2.30-2.40 3.10-3.20-3.30-3.40-4.10-4.20-4.30-5.10 5.20-5.30-5.40-5.50-5.60-5.70-6.10-6.11 6.12 | 12.10-12.20-12.30 | 6.13-6.14-8.10-8.20-8.30-8.46-8.50-8.60 8.70-9.10-9.20-9.30-9.40-9.50-9.60-10.10 10.20-10.30-10.40-10.50-10.60-10.70-10.80-10.10 10.91-10.92-10.93-11.10-11.20-11.30-11.40-11.50 11.60 | 7.10-7.20-7.30-14.10-14.20-14.30-14.40-14.50 14.60 | 21.10-21.20-21.30-21.40-21.56-21.60 | 15.10-15.20-15.30-15.40-15.50-15.60-15.70-15.80 15.90-15.91-15.92-15.93-16.10-16.20-16.30-19.10 19.20 | 13.10-13.20-13.30-17.10-17.20-18.10-18.20-18.30 20.10-20.20-20.30-20.40-22.10-22.20-22.30-22.40 23.10-23.20-23.30-23.40-24.00-25.00-26.10-26.20 |

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| | Cultural | | Natural |
|-----|----------------------------------|------|------------------------|
| 1. | Urban áreas | 1N. | Rain |
| 2. | Railroads | 2N. | Sleet |
| 3. | Airports | ЗМ. | Hail |
| 4. | Marine traffic | 4N. | Wind |
| 5. | Interstate highways | 5N. | Stream |
| 6. | Principal highways | 6N. | Rivers and wave action |
| 7. | Secondary roads | 7N. | Thunder and lightning |
| 8. | Mines (underground and open pit) | 8N. | Earth tremors |
| 9. | Factories | 9N. | Rock cracking |
| 10. | Generating stations | 10N. | Animal noise |
| 11. | Agriculture operations | 11N. | Dust storms and/or |
| 12. | Construction operations | | |
| 13. | High-voltage transmission lines | | |
| 14. | Pipe lines | | |
| 15. | Lock or dan | | |
| 16. | Campsite | | |
| 17. | Wells | | |
| 18. | Windmills | | |
| 19. | Drawbridges | | |
| 20. | Impact areas | | |
| 21. | Cantonement areas | | |
| 22. | Schools and institutions | | |
| 23. | Logging activities | | |
| 24. | Pumping stations | | |

| Tab | le | 25 |
|-----|----|----|
| Tab | le | 25 |

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| Tal | ble | 26 |
|-----|-----|----|
|-----|-----|----|

Military Grid Coordinates of Sampling Points

Map: Fulda

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Series: M 745 No. L5524

Contra a distance interesting sections

Scale: 1:50,000

| | <u>Military Grid</u> | | | | | | |
|------------|----------------------|----------|--|--|--|--|--|
| Sample No. | <u>x</u> | <u>y</u> | | | | | |
| 1 | 4889 | 9466 | | | | | |
| 2 | 6488 | 8715 | | | | | |
| 3 | 6285 | 9669 | | | | | |
| 4 | 4982 | 9266 | | | | | |
| 5 | 6290 | 9380 | | | | | |
| 6 | 5654 | 9698 | | | | | |
| 7 | 6415 | 0355 | | | | | |
| 8 | 5536 | 0545 | | | | | |
| 9 | 5538 | 9114 | | | | | |
| 10 | 5631 | 9834 | | | | | |
| 11 | 5601 | 0189 | | | | | |
| 12 | 5384 | 9770 | | | | | |
| 13 | 4935 | 9103 | | | | | |
| 14 | 6539 | 9597 | | | | | |
| 15 | 6992 | 9527 | | | | | |
| 16 | 4845 | 9895 | | | | | |
| 17 | 4985 | 0432 | | | | | |
| 18 | 5486 | 0045 | | | | | |
| 19 | 5683 | 9820 | | | | | |
| 20 | 6888 | 0080 | | | | | |
| | | | | | | | |

| | | | Distance from Sampling Point, km | | | | | | | | |
|--------------|--------------|----------|----------------------------------|--------|------------|----------------|--|--|--|--|--|
| - | 0 | - 0.5 | 0.5 | - 1.0 | 1.0 | - 2.0 | | | | | |
| <u>Point</u> | <u>Typ</u> e | Number | Type | Number | Type | Number | | | | | |
| 1 | 1 | 2 | 6 | 2 | 1 | 2 | | | | | |
| | 2 | 1 | 7 | 1.4 | 2 | 1 | | | | | |
| | 6 | 2 | 16 | 1 | 7 | 31 | | | | | |
| | 7 | 5 | 15 | 1 | 13 | 1 | | | | | |
| | 11 | 1 | 11 | 1 | 18 | 1 | | | | | |
| | 5N | 5 | | | 16 | 1 | | | | | |
| | 6N | 1 | | | 24 | 1 | | | | | |
| | 15 | 1 | | | 11 | 1 | | | | | |
| | | | | | 22 | 1 | | | | | |
| 2 | 1 | 1 | 1 | 1 | 1 | 3 | | | | | |
| - | 7 | 5 | 6 | 1 | 7 | 28 | | | | | |
| | 11 | ĩ | 7 | 6 | 8 | 1 | | | | | |
| | 5N | 1 | 8 | 1 | 11 | 1 | | | | | |
| | <i>د</i> | | 11 | 1 | | | | | | | |
| | | <u> </u> | | 3 | . <u> </u> | 1 | | | | | |
| 3 | 7 | 6 | 11 | | 7 | 23 | | | | | |
| | 11 | 1 | 5N | 1 | 11 | 1 | | | | | |
| | <u> </u> | 1 | 211 | - | 13 | 1 | | | | | |
| | 5 | * | | | 17 | 1 | | | | | |
| | | | | | 18 | 1 | | | | | |
| | | | | | 5N | $\overline{2}$ | | | | | |
| | | | | | | | | | | | |
| 4 | 7 | 4 | 2 | 1 | 1 | 3 | | | | | |
| | 11 | 1 | 5 | 1 | 6 | 1 | | | | | |
| | 5N | 2 | 6 | 2 | 7 | 29 | | | | | |
| | 15 | 1 | 13 | 1 | 16 | 1 | | | | | |
| | | - | 15 | 4 | 18 | 1 | | | | | |
| | | | 6N | 1 | 5N | 5 | | | | | |
| | | | 11 | 1 | 6N | 1 | | | | | |
| | | | 7 | 7 | 15 | 1 | | | | | |
| | | | - | | 8 | 1 | | | | | |
| | | , | | 、 | 11 | 1 | | | | | |
| | | () | Continued |) | | | | | | | |
| | | | | | | (Sheet | | | | | |

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และระ และร่งการแหน่ง แต่แต่ประทัศษที่ประทัศ การและที่ประเป็นให้มายที่ให้เป็นได้ได้เรียงไม่มีการเรียงไม่มายไม่เห

| | | 1 | fable | 27 | | | |
|------------|--------|------|-------|---------|----|-------------|---|
| Backgrcund | Noise | Sour | ces, | Number | of | Occurrences | 2 |
| and | Distar | nces | from | Samplin | ng | Points | |

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| | 0 | | Distance | e from Sam | pling Point, km | | | | | |
|----------|------------------------------|------------------|--------------------------------|----------------------------------|--------------------------------------|-----------------------------------|--|--|--|--|
| Sampling | | - 0.5 | <u> </u> | <u>- 1.0</u> | | - 2.0 | | | | |
| 5 | <u>1ype</u> 7 11 5N | 5 1 1 | 1 7 16 13 15 11 | 2 12 1 1 1 1 1 | 1ype 1 6 7 11 | Number 2 1 43 1 | | | | |
| 6 | 7 11 15 | 6 1 1 | 7 11 13 5N | 11 1 1 1 | 1 7 11 15 17 | 2 38 1 1 1 | | | | |
| 7 | 7 11 5N | 5 1 1 | 7 11 17 | 11 1 1 | 1 2 7 16 11 | 4 1 39 1 1 | | | | |
| 8 | 1 7 11 5N | 1 7 1 1 | 7 11 5N | 10 1 1 | 1 2 7 6N 18 11 | 2 1 21 1 1 1 | | | | |
| 9 | 7 11 | 6 1 | 1 2 6 7 11 5N | 1 1 16 1 2 | 1 7 15 24 5N 6N 11 | 3 45 26 1 7 2 1 | | | | |
| | | (| Continued | 1) | 16 | 1 (Sheet 2 | | | | |

อดีสารกระโรสและสารกรไม้มาและสารกระสารสารกรีบสารกรีบสารกรณ์ให้สารกรีบสารกรณ์สารกระสารกระสารกระสารกระสารกระสารกร

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| | | | Distance | e from San | pling Po | oint, km |
|-------|--------------------------------|----------------------------|---------------------|-------------------|--|---------------------------------------|
| C | <u> </u> | - 0.5 | 0.5 | - 1.0 | 1.0 | - 2.0 |
| Point | Type | Number | Type | Number | Type | Number |
| 10 | 7 11 | 8 1 | 1 7 | 2 17 | 6 7 11 | 1 47 |
| | 5N | 2 | 11 5N | 1 3 | 13 17 5N 6N | 1 1 4 1 |
| 11 | 1 7 11 5N 15 | 1 9 1 1 | 7 11 15 8 | 11 1 1 | 1 2 7 16 8 11 17 5N 6N | 2 1 38 1 1 1 3 2 |
| 12 | 1 7 11 5N | 1 6 1 2 | 7 11 13 5N | 12 1 1 1 | 1 5 7 8 13 11 17 5N | 4 1 38 1 1 1 8 |
| 13 | 1 7 5N 6N 18 11 | 1 6 1 1 1 1 | 6 7 16 11 | 1 14 1 1 | 1 7 11 15 16 13 | 2 54 1 3 2 1 |

(Continued)

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(Sheet 3 of 5)

Lever Marsh and

| | | | Distanc | e from Sau | pling Po | oint, km |
|-------------------|--------------|---------------------------------------|---------|------------|----------|----------|
| . | 0 . | - 0.5 | 0.5 | - 1.0 | _1.0 | - 2.0 |
| Sampling Point | Type | Number | Туре | Number | Туре | Number |
| 14 | 1 | 1 | 6 | 1 | 1 | 2 |
| | 7 | 6 | 7 | 14 | 7 | 54 |
| | 5N | 1 | 16 | 1 | 15 | 3 |
| | 6 • • | _ | | _ | 11 | 1 |
| | 6N | 1 | 11 | 1 | 16 | 2 |
| | 11 | 1 | | | 13 | 1 |
| | | ـــــــــــــــــــــــــــــــــــــ | | | | |
| 15 | 7 | 5 | 6 | 1 | 1 | 1 |
| | 11 | · 1 | 7 | 15 | 6 | ī |
| | | | 11 | 1 | • | - |
| | 5N | 1 | 17 | 1 | 7 | 29 |
| | | • | 8 | 1 | 11 | 1 |
| | | | 5N | 2 | 17 | 1 |
| | | | | | 15 | 1 |
| | | | | | 5N | 6 |
| 16 | 1 | 1 | 7 | 10 | | |
| 10 | 2 | 1 | 16 | 2 | 9 | 1 |
| | 6 | 1 | 5N | 2 | 11 | ĩ |
| | 7 | 6 | 6N | 2 | 15 | ĩ |
| | 16 | 1 | 9 | 1 | 17 | 1 |
| | | | 1.1 | 1 | 16 | 3 |
| | | | | | 5N | 5 |
| | | | | | 7 | 40 |
| 17 | 5 | 1 | | 1 | 1 | |
| ±/ | 6 | 1 | 7 | 15 | 2 | 1 |
| | 7 | 7 | 11 | 1 | 7 | 32 |
| | 5N | 1 | 5N | 1 | 11 | 1 |
| | 11 | 1 | | | 13 | 1 |
| | | | | | 5N | 2 |
| | | | | | 9 | 1 |

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Table 27 (Continued)

(Continued)

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(Sheet 4 of 5)

| | 0 - | - 0.5 | Distance | from Sam | pling Po | pint, km |
|-------------------|---------------------------|-----------------------|---------------------|------------------|---|---------------------------------------|
| Sampling Point | Туре | Number | <u>Type</u> | Number | Type | Number |
| 18 | 7 17 11 5N 6N | 6 2 1 1 1 | 7 6 11 | 13 1 1 | 1 7 11 17 15 8 5N 6N 13 | 7 36 1 2 1 5 1 1 |
| 19 | 7 11 | 8 1 | 7 11 17 5N | 8 1 1 2 | 1 6 7 13 11 17 5N | 3 1 35 1 1 1 6 |
| 20 | 7 11 5N | 7 1 1 | 7 11 5N | 12 1 2 | 1 6 7 2 11 17 5N | 1 40 1 1 2 5 |

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(Sheet 5 of 5)

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Table 28

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Summary of the Single Target Test Program

Engineering Development (ED) Tests

| Remarks | Three vehicles are specified. One vehi- cle can be the same as used to determine signature variation with a target class (see above). | Smooth road, cross- country, and obstacle course is required at all locations for these tests. |
|---------------------------------|---|--|
| Number t Runs íty 3 | I | 1 |
| f Tes Prior | 8 | 8 |
| L of 1 | JI | 21 |
| No. Itei tfoi | о Ч ц | и и и и и |
| Target Travel Mode | hin a Target Type 10/km/hr and con- voy speed on road 7.5 and 30.0 km/hi for cross-country 5.0 and 12.0 km/hi for obstacle | 10 km/hr and c. u- voy speed on road 7.5 and 30.0 km/hr for cross-country 5.0 and 12.0 km/hr for obstacle |
| Prior- ity | ation Wit | |
| Terrain Site* Condition Code | vari es 3,8,13** | a 3,8,13** |
| Target Class | Wheeled vehicle type M35Al, three vehicl | Tracked vehicle type Mll3 three vehicles |

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(Continued)

* Terrain site condition codes correspond to conditions identified in paragraph 31. ** Tests to be run on cross-country, smooth road, and obstacle course.

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Table 28 (Concluded)

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2.2

| Target Class | Terrain Site Condition Code | Prior- ity | Target Travel Mode | No. of Itera- tions | Total N of Test Priori | fumber Runs ty 3 | Remarks |
|-----------------------------------|--|---------------|--|---------------------------|------------------------------|---------------------------|---------------------------------------|
| | Variat | ion Wit | hin a Target Class | | | | |
| Wheeled wehicle type M170 | 2,5,8,14 | 1 | 10 km/hr and con- | | | | Priority based on site |
| C/TH M35A1 M381 | 1,3,4,6,7,9, 12,13 | 7 | voy speed for road sites. 7.5 and 30.0 km/hr | 2 | 128 256 | 64 | conditions. |
| .4622 M813 M125 VIOU | 10.11 | Ċ | for cross-country sites | I | | | |
| Tracked vehicle type | | | | | | | |
| M113 M60 M551 | 2,5,8,14 1,3,4,6,7,9,12,13 10,11 | ном | Same as for wheeled vehicles. | 2 | 48 96 | 54 | Priority based on site conditions. |
| Rotary-wing aircraft CH46F | | | Altitude: 150 and | 6 | 18u - | I | |
| CHIN TH57A | 8,13,14 | | 750 m; speeds: 0.5 and 1.0 crufsin | 90 | | | |
| СН 3В Ні: IK | | | speed horfzontal flight; decending and ascending. | ı | | | |
| Fixed-wing afrcraft | | | | | | | |
| Three types; to be determined. | 8,13,14 | | Altitude 500 and 1500 m; speeds: 0.5 and 1.0 cruisin speed horizontal flight only. | 8 | - 21 | ł | |
| Walking-man targets | | | | | | | |
| One man Three men Seven men | 2,5,8,14 1,3,4,6,7,9,12,13 10.11 | цим | Route and march step 5- and 15-m CPA walk marks | 2 | 96 192 | 48 F | riority based on site onditions. |

| Table 29 |
|----------|
|----------|

Target Types and Targe: Combination Codes for Multiple-

Target Signature Acquisition

k

| | · · · | | Primary Targe | ts | |
|-----------------------------------|---------------------------------------|--------------------------------|------------------------------------|-----------------------------------|--------------------------------|
| Secondary Targets | Wheeled Vehicles <u>3 Types</u> | Tracked Vehicles 3 Types | Rotary-Wing Aircraft 3 Types | Fixed-Wing Aircraft 3 Types | Walking Man <u>l Man</u> |
| Wheeled vehicles (3 types) | 1* | 2 | 3 | 4 | 5 |
| Tracked ventcles (3 types) | | 6 | 7 | 8 | 9 |
| Rotary-wing aircraft (3 types) | | | 10 | 11 | 12 |
| Fixed-wing aircraft (3 types) | | | | 13 | 14 |

| | Talget Types | | | | | | | |
|------------------------------|---------------------|-------------------------|------------------------|--|--|--|--|--|
| Wh ee led Vehicles | Tracked Vehicles | Rotary-Wing Aircraft | Fixed-Wing Aircraft | | | | | |
| M170 | M113 | UH IN | | | | | | |
| M35A1 | M551 | TH57A | To be determined | | | | | |
| M125 | M60A1 | ннік | | | | | | |

* Numbers refer to target combination codes used in Table 30.

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Table 30

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Summary of the Multiple-Signature Acquisition Test Program

Advanced Development (AD) Tests

• }••!

| Remzrks | Site surface can be cross-country or smooth road | Site surface can be cross-country or smoth road | Site surface can be cross-country or smooth road | | Site surface can be cross-country or smooth roaú | |
|--|---|---|---|--|---|-------------|
| Tota []] Test <u>Runs</u> | 108 | 108 | | 432 | | |
| Iterations | 7 | 7 | | 8 | | |
| Target** Combinations | On . | σ | | б, | | |
| Target Travel Modes | Cross-country at 7.5 and 30 km/hr or Road at 10 km/hr and convoy speed | Cross-country at 7.5 and 30 km/hr or Road at 10 km/hr and convoy speed | Wheeled vehicles: Cross-country at 7.5 and 30 km/hr or Smooth road at 10 km/hr and convoy speed | Rotary-wing aircraft: Altitudes of 150, 750 m; speeds of 0.5 and 1.0 cruising speed, horizontal flight | Wheeled vehicles: Cross-country at 7.5 and 30 km/hr or Smooth road at 10 km/hr and convoy speed | (Continued) |
| Terrain Site Conditions Code* | 5, 8, 13 | 5, 8, 13 | 5, 8, 13 | | 5, 8, 13 | |
| Targe•s (Coded from Matrix in Table 29) | Ч | 2 | m | | 4 | |

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Table 30 (Continued)

| Remarks | · | Site surface can be cross-country or smooth road | | Site surface can be cross-country or smooth road | Site surface can be cross-country or smooth road | |
|--|---|---|--|---|---|------------|
| Total Test Runs | 432 | | 144 | 108 | | |
| Iterations | 8 | | 7 | 7 | | |
| Target Combinations | 6 | | ζ ή | σ | | ~ |
| Target Travel Modes | Fixed-wing aircraft: Altitudes of 500 and 1506 m; speeds of 0.5 and 1.0 cruising speed, horizontal flight | Wheeled vehicles: Cross-country at 7.5 and 30 km/hr or Smooth road at 10 km/hr and convoy speed | Walking-man: One man, normal walk, march step; two walk paths (near, far) | Cross-country at 7.5 and 30 km/hr or E3ad at 10 km/hr and convoy speed | Tracked ventcle: Cross-country at 7.5 and 30 km/hr or Road at 10 km/hr and convoy speed | (Continued |
| Terrain Site Conditions Code | | 5, 8, 13 | | 5, 8, 13 | 5, 8, 13 | |
| Targets (Coded from Matrix in Table 29) | | Ś | | అ | 7 | |

(Sheet 2 of 4)

Table 30 (Continued)

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| | Remarks | | | | | | | | (Sheet 3 of 4) |
|------------------------------|------------------------|---|--------------------------------|---|--------------------------------|--|--|-------------|----------------|
| Total | Test. Runs | 432 | 432 | | 36 | | 144 | | |
| | Iterations | 7 | 2 | | 2 | | Ν | | |
| | Target Combinations | σ | 6 | | ũ | | ũ | | |
| | larget Travel Modes | Rotary-Wing aircraft: Altitudes of 150, 750 m; speeds of 0.5, and 1.0 cruising speed, horiz- ontal flight | Tracked vehicles: Same as 6 | Fixed-wing aircraft: Altitudes of 500, 1500 m; speeds cf 0.5, and 1.0 cruising speed, horizon- tal flight | Tracked vehicles: Same as 6 | Walking-man: One man, normal route walk, one walk path (far) | Rotary-wing aircraft: Altitudes of 150, 750 r; speeds of 0.5 and 1.0 cruising speed, horiz- ortal flight | (Continued) | |
| Terr ai n Site | Conditions Code | 5, 8, 13 | 5 , 8, 13 | | 5, 8, 13 | | Ś | | |
| Targets (Coded from | Table 29) | t. | œ | | 6 | | 10 | | |

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Table 30 (Concluded)

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| | Remarks | | | | | | | |
|---|--|-------------------------------------|--|-------------------------------------|--|--|------------------------------------|--|
| The second se | Total Test. Kuns | 288 | | 72 | | 144 | 72 | 2952 |
| | Iterations | 7 | | 2 | | 7 | 2 | Total |
| | Target Combinations | 6 | | £ | | σ | Э | |
| | Target Travel Modes | Rotary-wing aircraft: Same as 10 | Fixed-Wing aircraft: Altitudes of 500, 1500 m; speeds of 0.5 and 1.0 cruising speed, horiz- ontal flight | Rotary-wing aircraft: Same as 10 | Walking-man: Oue man, normal routc walk, one walk path (far) | Fixed-wing aircraft: Altitudes of 500, 1500 m; speeds of 0.5 and 1.0 cruising speed, horiz- ontal flight | Fixed-wing afroraft: Same as 13 | Walking-man: One man, normal route walk, one welk path (far) |
| | Terrain Site Conditions Code | 2 | | 5, 8, 13 | | Ŋ | 5, 8, 13 | |
| | Targets (Coded from Matrix in Table 29) | 11 | | 12 | | 13 | 14 | |

(Sheet 4 of 4)

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In accordance with ER 70-2-3, paragraph 6c(1)(b), dated 15 February 1973, a facsimile catalog card in Library of Congress format is reproduced below.

Benn, Bob O

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Rationale and plan for field data acquisition required for the rational design and evaluation of seismic and acoustic classifying sensors, by Bob O. Benn. Vicksburg, U. S. Army Engineer Waterways Experiment Station, 1975. 1 v. (various pagings) illus. 27 cm. (U. S. Waterways Experiment Station. Miscellaneous paper M-75-10) Prepared for Project Manager, Remotely Monitored Battlefield Sensor System, AMC, Fort Monmouth, New Jersey, under Project 1X764723DL73. Includes bibliography.

 Acoustic waves.
Remote sensing.
Remotely monitored battlefield surveillance system.
Seismic waves.
Sensors.
Target classification.
U. S. Army Materiel Command.
(Series: U. S. Waterways Experiment Station, Vicksburg, Miss.
Miscellaneous paper M-75-10) TA7.W34m no.M-75-10