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AMRL-TR-75-14

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DEVELOPMENT OF AN IMPROVED COMPUTER MODEL OF THE HUMAN BODY AND EXTREMITY DYNAMICS

*CALSPAN CORPORATION
BUFFALO, NEW YORK 14221*

JULY 1975

20090513 139

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FOR THE COMMANDER



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Director
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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AMRL-TR-75-14	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) DEVELOPMENT OF AN IMPROVED COMPUTER MODEL OF THE HUMAN BODY AND EXTREMITY DYNAMICS		5. TYPE OF REPORT & PERIOD COVERED Technical Report
		6. PERFORMING ORG. REPORT NUMBER Y11 series
7. AUTHOR(s) J. T. Fleck F. E. Butler		8. CONTRACT OR GRANT NUMBER(s) F33615-75-C-5002
9. PERFORMING ORGANIZATION NAME AND ADDRESS Calspan Corporation Buffalo, New York 14221		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 62202F, 7231-05-19
11. CONTROLLING OFFICE NAME AND ADDRESS Aerospace Medical Research Laboratory Aerospace Medical Division Wright-Patterson Air Force Base, Ohio 45433		12. REPORT DATE July 1975
		13. NUMBER OF PAGES 164
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) None
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES Phase III Calspan Three-Dimensional Crash Victim Model Simulation was sponsored by the National Highway Safety Administration, Dept. of Transportation. The ground work for the simulation was performed in Phases I and II, both jointly sponsored by NHTSA and the Motor Vehicle Manufacturers Association.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Computer Simulation - Three Dimension Dynamics Mathematical Model - Vehicle Crash Victims Harness Restraint System Aerodynamic Forces		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Three principal modifications; namely, an improved joint formulation, an improved belt restraint formulation and inclusion of aerodynamic forces, were incorporated into the Phase III Calspan Three-Dimensional Crash Victim Model Simulation.		

AD-A014816

PREFACE

This report describes the modifications which were incorporated into the Phase III* Calspan Three-Dimensional Crash Victim Simulation Program to satisfy current Air Force requirements.

Three principal modifications are:

1. Improved Joint Formulation
2. Improved Belt Formulation
3. Inclusion of Aerodynamic Forces.

The modifications have been made so that they may be used on the CDC6600 computer at the Mathematics and Analysis Branch of AMRL.

The research effort summarized in this report was performed for the Aerospace Medical Research Laboratory [FY8990] under Contract No. Calspan F33615-75-C-5002. Dr. John T. Fleck of the Computer Mathematics Department of Calspan served as principal investigator.

The authors wish to thank Ints Kaleps of the Aerospace Medical Research Laboratory for his suggestions and direction during the analytical development of the program.

*Phase III was sponsored by the National Highway Traffic Safety Administration, Department of Transportation. The ground work for the simulation was performed in Phases I and II, both jointly sponsored by NHTSA and the Motor Vehicle Manufacturers Association.

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Section 1

INTRODUCTION

The Calspan 3-D Crash Victim Simulation Model was originally developed to study human body dynamics associated with automobile accidents. The formulation, however, is quite general, giving it great versatility and making it applicable to many studies involving human body dynamics. Reference 1 contains a complete description of this model.

To fit the specific needs of the Mathematics and Analysis Branch (BBM) of the Aerospace Medical Research Laboratory (AMRL), three principal modifications have been made to the program. These are: an improved joint formulation, an improved belt restraint formulation and the inclusion of aerodynamic forces.

The modifications are described in the following sections.

Section 2

JOINT ALGORITHM

The joint routine, subroutine VISPR, which is in the Calspan 3-D Crash Victim Model, has been modified to provide the option of computing the flexure torque as a function of both the flexure angle (elevation) and azimuth angle.

NOMENCLATURE

D_m	3 x 3 direction cosine matrix specifying the orientation of segment m's local reference with respect to the inertial reference.
$T_{m,n}$	3 x 3 direction cosine matrix specifying the relative orientation of joint n's local reference with respect to the local reference of segment m.
T	3 x 3 direction cosine matrix specifying the relative orientation of joint's local reference systems, $T=I$, the identity matrix, is the equilibrium position.
T_{ij}	ij^{th} element of matrix T .
$r_{m,n}$	3 x 1 matrix (vector) specifying the location of joint n as measured in segment m's local reference.
x, y, z	used to designate axes of a right handed coordinate system
x_m, y_m, z_m	may be regarded as 3 x 1 matrix (vector) which is of unit magnitude and is orthogonal.

NOMENCLATURE (CONTINUED)

- θ flexure angle of joint.
- ψ torsion angle of joint.
- ϕ azimuth angle used to describe flexure torque asymmetrically.
- μ 3 x 1 matrix (vector) of unit magnitude used to designate axis of flexure.

Joint Routine

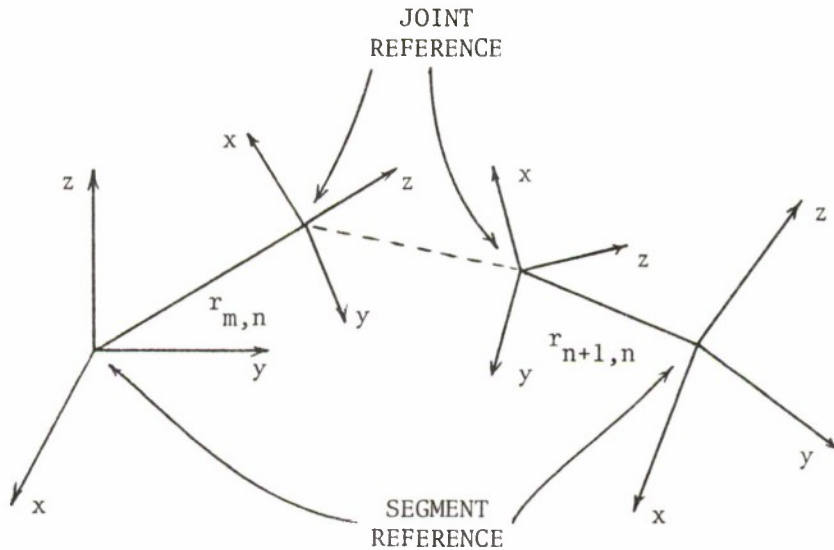


FIGURE 1 Joint Coordinate System

The position of joint n, which is fixed in segment m, is given by vector $r_{m,n}$ (see Figure 1). The orientation of the joint with respect to segment m's reference system is given by the direction cosine matrix $T_{m,n}$. The matrix $T_{m,n}$ is computed from the yaw (about Z), pitch (about Y), and roll (about X) angles, which are specified on input along with the vector $r_{m,n}$.

Joint n connects segments m and $n+1$. The vector $r_{n+1,n}$ and the matrix $T_{n+1,n}$ are determined from input as were $r_{m,n}$ and $T_{m,n}$.

For the relative orientation of the joint we have

$$T_{m,n}^T D_m = T_{n+1,n} D_{n+1}$$

$$T = T_{n+1,n} D_{n+1} (T_{m,n} D_m)^1$$

where D_m, D_{n+1} are the direction cosine matrices specifying the orientation of the segments and T is the direction cosine matrix specifying the relative orientation of the joint, and where A^1 is the transpose of A .

$T_{m,n}$ and $T_{n+1,n}$ are defined so that the equilibrium position of the joint occurs when $T=I$, the identity matrix.

Consider the following figure

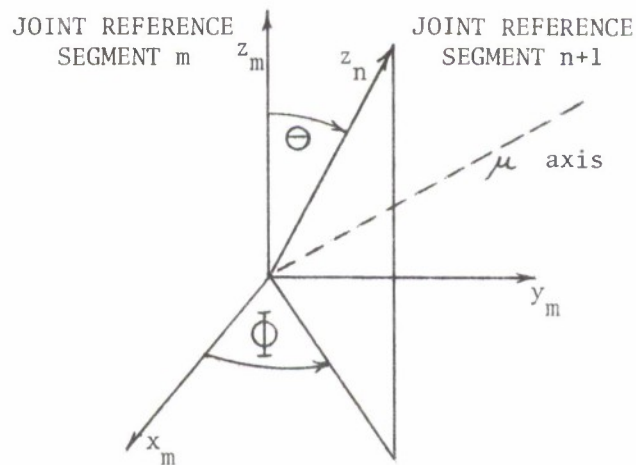


FIGURE 2 Joint Flexure

The angle, θ , between the Z axes of the joint reference systems is defined as the flexure angle of the joint. The angle, Φ , between the projection of Z_n in the $X_m Y_m$ plane and the X_m axis is defined as the azimuth angle. A twist (torsion) angle, ψ , may be defined as either a rotation about Z_m or a rotation about Z_n .

If the joint is pinned (hinge joint), the pin axis is taken as the Y axis, hence Y_m is parallel to Y_n for this pinned joint. In this case, $\bar{\Phi}$ may either be 0 or π .

Flexure

The axis of flexure, μ , may be computed as the vector cross product of Z_m and Z_n .

$$\text{That is } \mu = Z_m \otimes Z_n / |Z_m \otimes Z_n|.$$

Note that when $\theta=0$ or $\theta=\pi$, μ is undefined. The case $\theta=\pi$ will not be considered. We will assume that $0 < \theta < \pi$. That is, any flexure angle equal or greater than π will never occur.

The direction cosines of a vector in the direction of Z_n with respect to joint reference m are given by the third row of the matrix T (i.e. the third row of T is a unit vector in the Z_n direction.)

We have

$$\sin \theta \cos \bar{\Phi} = T_{31}$$

$$\sin \theta \sin \bar{\Phi} = T_{32}$$

$$\cos \theta = T_{33}$$

Hence

$$\theta = \cos^{-1} T_{33}$$

$$\bar{\Phi} = \tan^{-1} \left(\frac{T_{32}}{T_{31}} \right) \text{ if } \theta \neq 0$$

$$\mu = \begin{pmatrix} -T_{32} \\ T_{31} \\ 0 \end{pmatrix}$$

where T_{ij} is the i, j^{th} element of the matrix T.

Define the matrix T_{μ} which represents a rotation of θ about the axis μ . We have, in matrix form,*

$$T_{\mu} = \mu\mu^1 + (I - \mu\mu^1) \cos \theta - \sin \theta \mu \epsilon \theta$$

where $\mu \epsilon \theta$ is the matrix

$$\mu \epsilon \theta = \begin{pmatrix} 0 & -\mu_z & \mu_y \\ \mu_z & 0 & -\mu_x \\ -\mu_y & \mu_x & 0 \end{pmatrix}$$

In our case, $\mu_x = -T_{32}$, $\mu_y = T_{31}$ and $\mu_z = 0$.

We compute the restoring torque for flexure, $f(\theta, \bar{\Phi})$, as a function of the flexure angle, θ , and the azimuth, $\bar{\Phi}$. The torque, $+f(\theta, \bar{\Phi})\mu$, will be applied to segment m and the torque, $-f(\theta, \bar{\Phi})\mu$, will be applied to segment $n+1$. We assume that when $\theta = 0$, $f(\theta, \bar{\Phi}) = 0$, hence the fact that $\bar{\Phi}$ and μ are undefined in this case will be of no consequence.

Representation of Flexure Torque

We use the following approximation for the torque function $f(\theta, \bar{\Phi})$.

The function, $f(\theta, \bar{\Phi})$, is represented as a continuous or tabular function of θ for discrete values of $\bar{\Phi}$.

That is, $f(\theta, \bar{\Phi}_n) = g_n(\theta)$ $n=1, N$

and where $\bar{\Phi}_1 = -\pi$, $\bar{\Phi}_2, \dots, \bar{\Phi}_N, \bar{\Phi}_{N+1}$, ($\bar{\Phi}_{N+1} = \pi$), are equally spaced between $-\pi$ and π and it is assumed that $f(\theta, \pi) = f(\theta, -\pi)$ therefore $\bar{\Phi}_{N+1}$ is not required. (The range $-\pi$ to π is used to be consistent with the four quadrant arctan routines, which are used to evaluate $\bar{\Phi}$.)

* Reference 1, Volume 1, page 23.

The value of N will be restricted only by the storage one is willing to allocate and the computing time involved.

The function g_n may be defined as the m^{th} degree polynomial in $(\theta - \theta_0)$ or as a table. (They cannot be mixed, i.e. for a particular joint all g must be tabular or polynomial.)

In both cases, a deadband may be specified, i.e. a θ_{n_0} is given and $g_n(\theta) = 0$ if $\theta < \theta_{n_0}$.

For intermediate values of Φ (i.e., $\bar{\Phi}_n < \Phi < \bar{\Phi}_{n+1}$), we evaluate f for g_n and for g_{n+1} and linearly interpolate on Φ . The wrap around if $\Phi > \bar{\Phi}_N$ or $\Phi < \bar{\Phi}_1$ is treated consistently (i.e., interpolate between g_N and g_1 .)

Twist (Torsion)

When there is no flexure, i.e. $\theta = 0$, the twist γ is easily defined as the rotation about the Z_m axis. In this case

$$T = T_Z(\gamma) = \begin{pmatrix} \cos \gamma & \sin \gamma & 0 \\ -\sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

When θ is not equal to zero, we may think of first twisting about Z_m and then rotation about the axis μ

$$T = T_\mu(\theta) T_Z(\gamma)$$

or we may first rotate about μ and then twist about the resultant Z, i.e. Z_n .

$$T = T_Z(\gamma) T_\mu(\theta)$$

These definitions are equivalent and thus give a unique definition of the angle γ . To show this, we expand T as

$$T = T_Z(\mu \mu^1 + (I - \mu \mu^1) \cos \theta - \sin \theta \mu \theta)$$

and as

$$T = (\mu_1 \mu_1^1 + (I - \mu_1 \mu_1^1) \cos \theta - \sin \theta \mu_1 \theta) T_Z$$

where $\mu_1 = T_{Z_m} \mu$, i.e. the axis of rotation is fixed in the X_m, Y_m plane. Substituting for the value of μ_1 in the above expression shows the equivalence.

Although the angle ψ is well defined, it does not seem possible to uniquely define an axis, which may be used for the restoring torque. This problem exists because we are talking about a mathematical definition of twist and not a physical description of a joint.

The program has been coded to use the Z_m axis. The magnitude of the torque is computed by the standard spring function characteristics available in the program. This is done using subroutine EFUNCT.

The torque, q , is computed from the five parameters S_1, S_2, S_3, S_4 and S_5 by the following algorithms.

$$\text{If } \psi \leq S_5 \\ q = S_1 \psi$$

$$\text{If } \psi > S_5 \text{ an additional torque } q_s \text{ is computed as} \\ q_s = S_2(\psi - S_5)^2 + S_3(\psi - S_5)^3$$

$$\text{If } \dot{\psi} < 0 \text{ (unloading) } q_s \text{ is modified by } q_s = S_4 q_s \\ \text{(If } S_5 \text{ is equal to zero, } q_s \text{ is not computed but } q \text{ is modified by } S_4.)$$

For small values of $|\dot{\psi}|$, (10 radians/sec), the routine interpolates between the loading and unloading characteristics.

The total torque $q + q_s$ is returned as the function value.

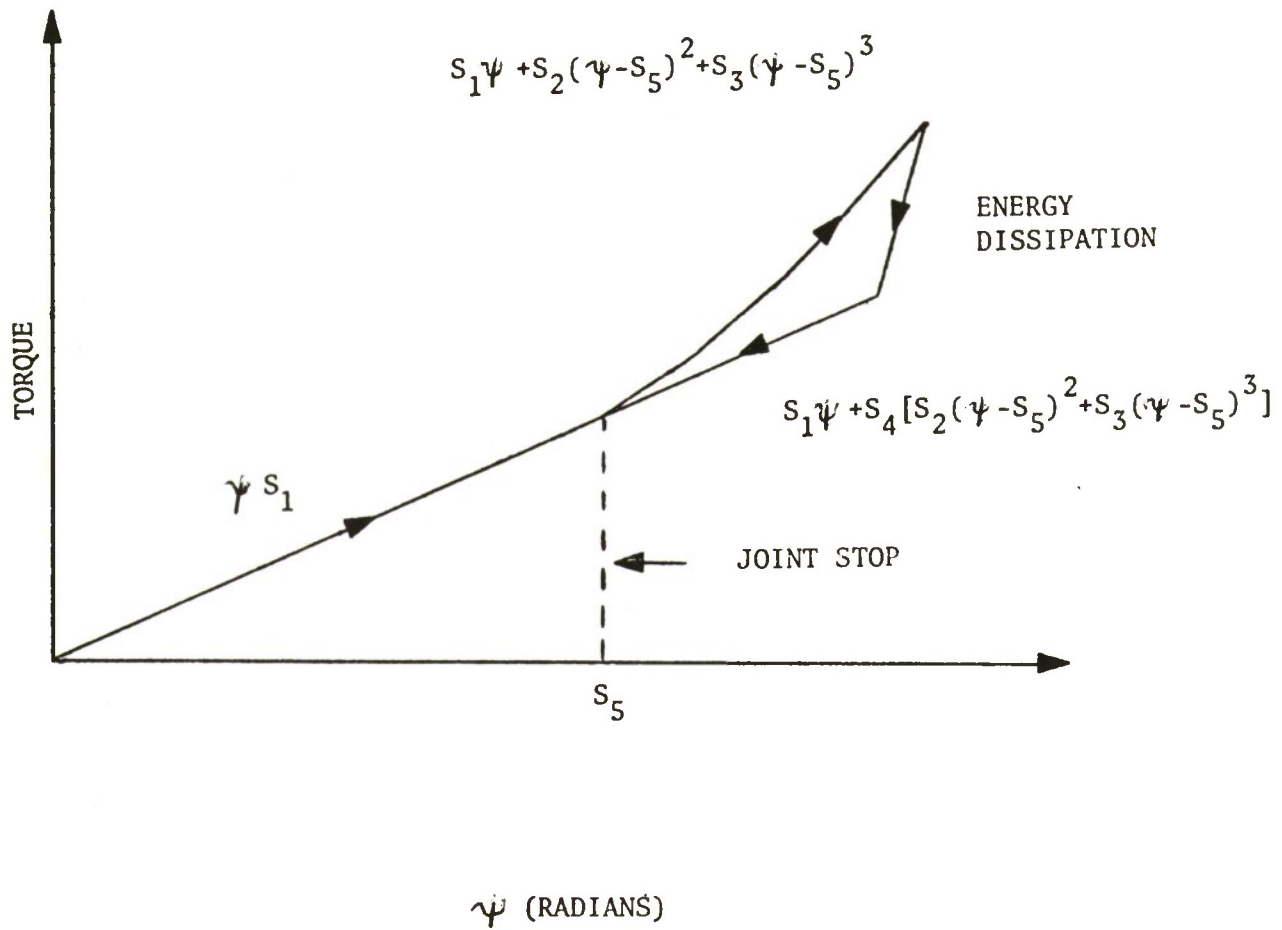
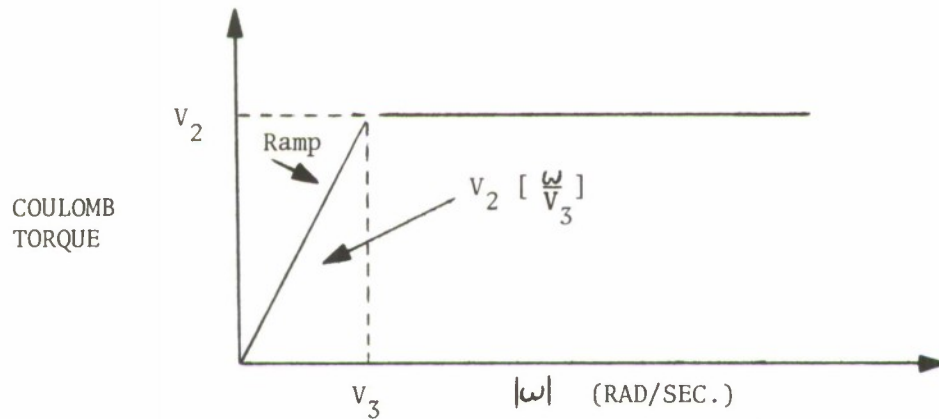


FIGURE 3 JOINT SPRING TORQUE

Viscous and Coulomb Torques

Let ω be the relative angular velocity. A torque is computed to oppose this velocity using the standard viscous function definition in the program. This is illustrated in Figure 4.



$$q/|\omega| = v_1 + v_2 / (\max(|\omega|, v_3))$$

ω is the relative angular velocity.

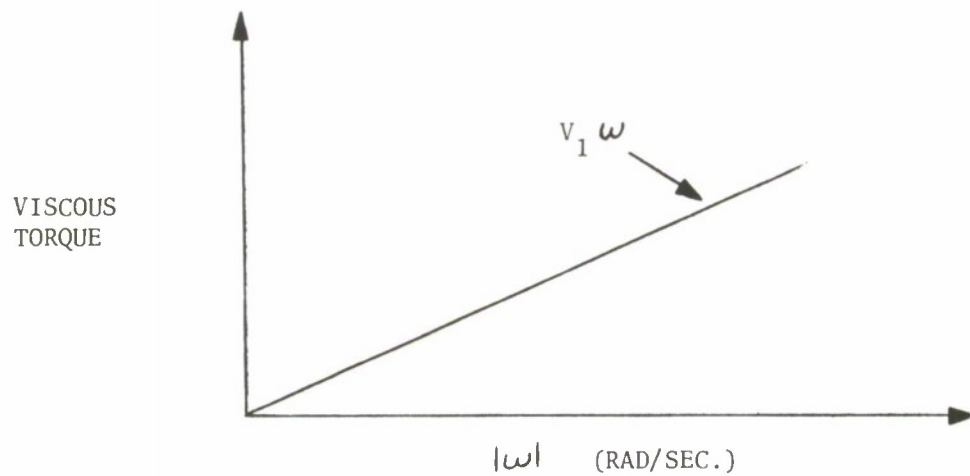


FIGURE 4 JOINT TORQUE DUE TO RELATIVE ANGULAR VELOCITY AT THE JOINT

Section 3

BELT ALGORITHM

The belt routine in Version III of the Calspan 3-D program is restricted to a simple belt passing around a single segment. Although several of these belts may be used, no provision for interaction of the belts was made.

To overcome this restriction and to satisfy the requirements of the current contract, an entirely new belt algorithm has been developed and incorporated into the program.

The current version of the algorithm assumes each belt lies essentially in a plane which may be described by a set of reference points rigidly attached to segments. Thus, its use should be restricted to harnesses (several belts connected at a common junction point) which constrain the segments involved from large relative motions.

The algorithm should lend itself to significant improvements in the modeling of harnesses.

The concept of a harness is introduced in this version of the program. A harness consists of from one to several belts. Each belt is defined as the set of straight line segments connecting prescribed reference points. One end of the belt is the anchor point and the other end the junction point. See Figure 5 below.

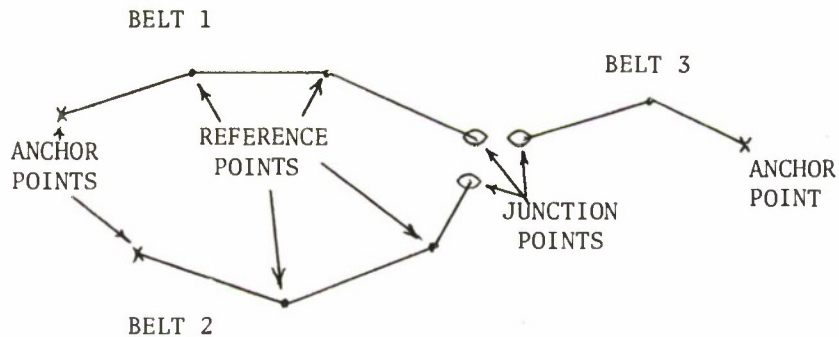


FIGURE 5 BELT HARNESS MODEL

Each reference point is fixed relative to a prescribed segment. An ellipsoid is assigned to each reference point. The ellipsoid is fixed to the same segment as the reference point. Ellipsoids associated with the anchor point and the junction point are ignored in the current version of the program hence may be specified as zero. The ellipsoid is used to determine an outward normal vector to the surface of the ellipsoid at the reference point. If the net force on the segment at this point has a positive component along this normal, the point will be ignored in computing the belt length. If no ellipsoid is specified for an interior point, this point will always be used in computing the belt length. For example, see Figure 6.

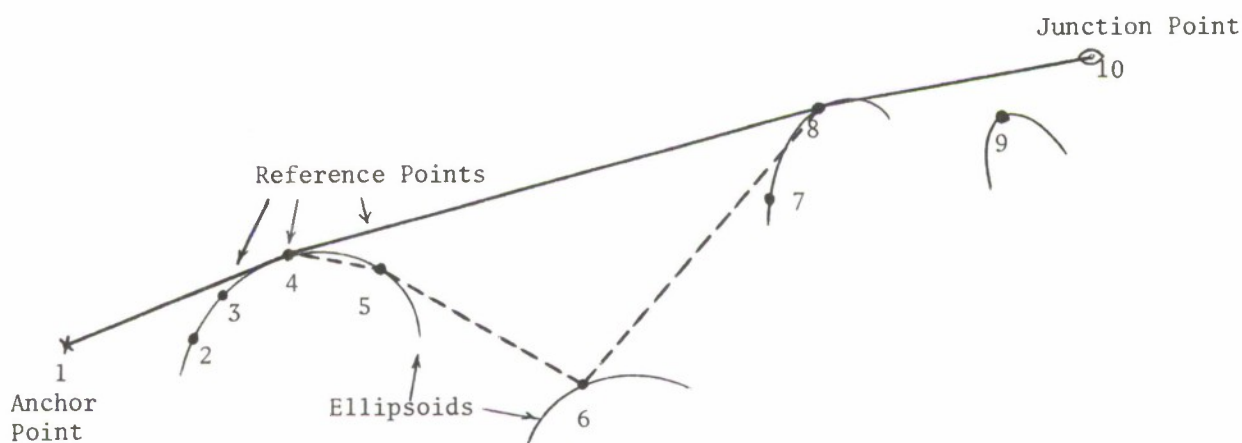


FIGURE 6 BELT LENGTH SPECIFICATION

In this example, the belt is defined by the 10 reference points illustrated. Ellipsoids associated with the interior points are represented by the curved lines. In the above configuration, the belt length would be computed as the sum of the length of the lines from 1 to 4, 4 to 8 and 8 to 10 as illustrated by the solid lines.

If no ellipsoid were specified for point 6, the belt would follow the dashed line, 1-4-5-6-8-10. The algorithm determines this belt configuration in the following manner:

1. The belt is first assumed to go from point 1 to point 2 to point 3.
2. The net force at point 2 (assuming constant tension) is found to be directed along the outward normal to the reference ellipsoid assigned to point 2 hence point 2 is dropped from consideration.
3. The belt is next assumed to go from point 1 to point 3 to point 4.
4. This is the same situation as was found in step 2 above hence point 3 is dropped.
5. The belt is next assumed to go from point 1 to point 4 to point 5.
6. The net force at point 4 is directed along the inward normal to the ellipsoid assigned to point 4 hence point 4 is accepted.
7. The belt is next assumed to go from point 4 (the last accepted point) to point 5 to point 6.
8. The net force at point 5 is found to be directed along the inward normal to the ellipsoid assigned to point 5 hence point 5 is accepted.
9. The belt is next assumed to go from point 5 to point 6 to point 7.
10. The net force at point 6 is found to be directed along the outward normal to the ellipsoid assigned to point 6 hence point 6 is dropped from consideration.
11. Point 5 was accepted because 4,5,6 were acceptable, since 6 is now rejected and the belt is assumed to go from 4 to 5 to 7.

This process is continued resulting in the following condensed steps.

12. 5 is rejected.
13. Try 4-7-8.
14. 7 rejected.
15. Try 4-8-9.
16. 8 accepted.
17. Try 8-9-10.
18. 9 rejected.
19. Since 10 is a junction point, the final belt is 1-4-8-10.

Computation of Belt Tension

The strain is computed as

$$\text{strain} = \frac{\text{calculated length} - \text{reference length}}{\text{reference length}}$$

The stress (tension) is computed by the standard force deflection routines available in the program using strain as the deflection parameter.

The current version of the program assumes that the tension is uniform in the belt.

Examples

The above technique provides considerable versatility in defining belt systems. For example:

SIMPLE LAP BELT

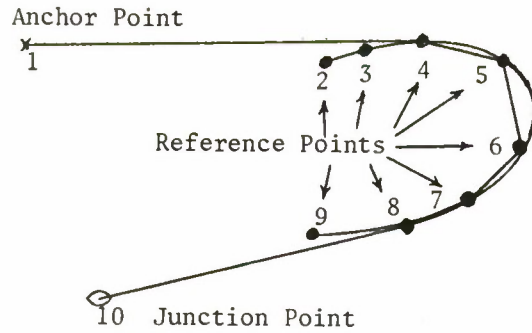


FIGURE 7 Simple Lap Belt Harness Configuration

Define a harness consisting of one belt. In this case, the junction point is actually an anchor point. All interior reference points are attached to the same segment and assigned the same reference ellipsoid.

SHOULDER BELT AND LAP BELT

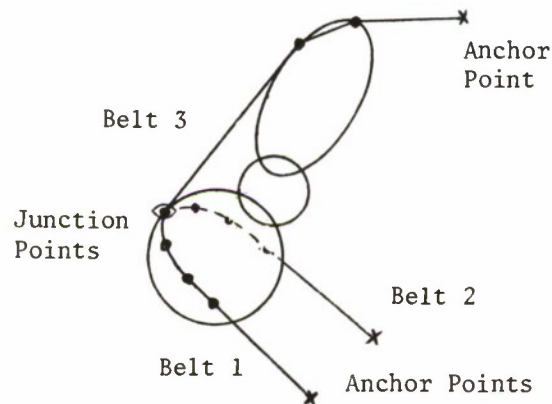


FIGURE 8 Shoulder Belt and Lap Belt Harness Configuration

Define a harness consisting of three belts with the junction points attached to a segment, which is disjoint (but need not be) from the body segments. This segment is assigned a mass and an inertia tensor and will move dynamically to achieve a force balance. (we recommend that the junction points all be located at the cg of the junction segment to prevent large angular accelerations.)

The Input Description of the program contains the details of inputting a belt system.

General Comments

Since there is no limitation (except storage) on the number of harnesses, belts or reference points, quite elaborate belt systems may be modeled.

The program is so written that it may be modified to include effects of belt friction and deformation of the surface at the reference points. For example, the reference points could be moved along the normal as a function of the normal force.

The belt is not constrained to lie in a plane. The algorithm, as illustrated in Figure 5, was designed on the assumption that the interior reference points lie essentially in a plane. Highly, non planar sets of points may produce unexpected results. No study has been made of this potential problem or of other unusual configurations that would cause the algorithm to fail.

The computation of frictional effects and deformation is complicated by the fact that a change in belt position or tension at one point affect all the points. Thus, the problem would require the use of techniques such as finite element methods. However, a first approximation to the effects of deformation could be made by holding the reference points fixed during the course of an integration step and at the completion of a successful integration step the points could be moved along the normal (as defined by the reference ellipsoid) as a function of the normal force computed from the current belt configuration. Alternately, the point could be moved in the direction of the net force. Storage has been allocated in the program to store a fixed reference point and a modified reference point. Perhaps the effects of friction could be approximated by allowing the modified reference point to move in a direction other than along the normal. Future study should consider these possibilities.

Section 4

AERODYNAMIC FORCES

Routines have been added to the program to allow the application of a specified force to any segment. The method allows any force to act on any segment. In addition, for each segment a boundary plane is specified and the force is not applied until the segment penetrates the boundary plane.

An aerodynamic pressure, a boundary plane, and an ellipsoid are associated with each segment for which it is desired to compute an aerodynamic force. The aerodynamic pressure, as a function of time, is inputted as tabular data.

As the ellipsoid penetrates the boundary plane, an estimate of the projected area normal to the pressure is made and the force and torque are computed and applied to the segment. For partial penetration, the force is applied at a point in the ellipsoid. At full penetration, the force is applied at the center of the ellipsoid.

MATHEMATICAL FORMULATION

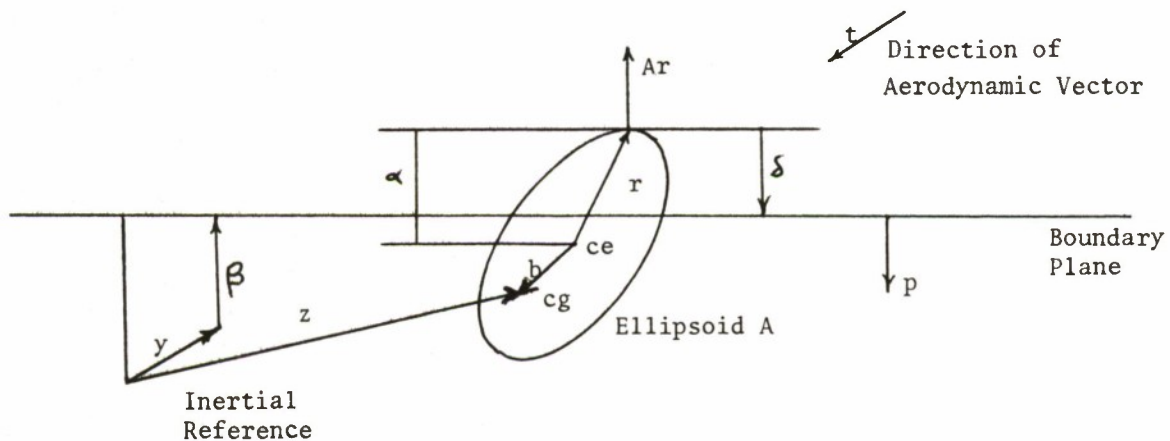


FIGURE 9 BOUNDARY PLANE PENETRATION BY ELLIPSOID

Let y location of reference point for plane
 z location of cg of segment
 b offset of center of ellipsoid from cg
 e penetration distance
 p unit vector describing outward normal to boundary plane
 r vector from center of ellipsoid to point of maximum penetration
 α distance from center of ellipsoid to point of maximum penetration
 t vector describing wind (force per unit area)
 A matrix defining the ellipsoid (a 3x3 positive definite matrix.)
 β distance of plane from its reference point

We have the following equations:

$$r \cdot Ar = 1 \quad \text{if } r \text{ is on the ellipsoid}$$

$$p \cdot r = -\alpha$$

$$p \cdot [z + b + r] = -\beta + S + p \cdot y$$

$$Ar \quad \text{vector normal to ellipsoid at } r.$$

At a given instant in time we know y, z, b, p, t and A .

In the computer program, the ellipsoid matrix is a given constant in the reference system of the segment. All quantities are first converted to this reference system for ease of computation.

COMPUTATION OF PENETRATION DISTANCE

If r goes to the point of maximum penetration, then

$$Ar = c p, \quad \text{where } c \text{ is some constant}$$

since $r \cdot Ar = 1$ if r is on the ellipsoid

$$r = c A^{-1} p$$

$$r \cdot Ar = c^2 p \cdot A^{-1} p = 1$$

then $c = 1 / \sqrt{p \cdot A^{-1} p}$

and $r = A^{-1} p / \sqrt{p \cdot A^{-1} p}$

The penetration distance \mathcal{S} may be computed as

$$\mathcal{S} = p \cdot [z + b + r - y] - \beta,$$

and α may be computed as

$$\alpha = p \cdot r = \sqrt{p \cdot A^{-1} p}$$

If \mathcal{S} is less than zero, no penetration has occurred.

If \mathcal{S} is greater than 2α the ellipsoid has fully penetrated the plane.

COMPUTATION OF PROJECTED AREA

If penetration has occurred, we must distinguish between three cases in the computation of the shadow (projected) area of the ellipsoid onto the plane.

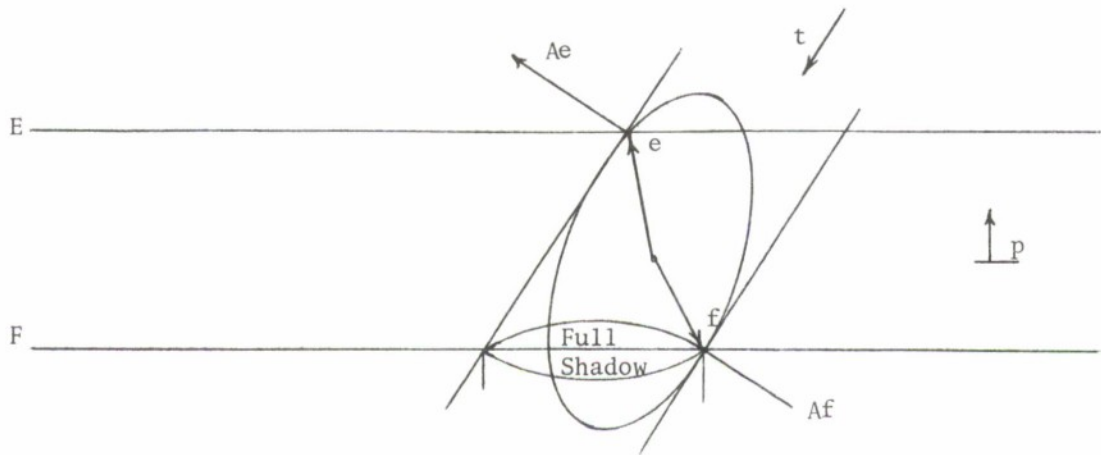


FIGURE 10 SHADOW (PROJECTED) AREA OF ELLIPSOID ONTO A PLANE

Consider the above figure where planes E and F are parallel to the boundary plane p and are such that at the points e and f which are on the ellipsoid and in the indicated planes we have $t \cdot Ae = 0$, $t \cdot Af = 0$ and the planes are positioned that $|p \cdot e|$ and $|p \cdot f|$ are at their maximum values (i.e. if the planes were moved further away from the center of the ellipsoid, no such points could be found.)

Consider the Three Cases

Case I The boundary plane is above plane E but still intersects the ellipsoid. In this case, the projected area is the area of the ellipsoid formed by the intersection with the plane p projected on a plane normal to t.

Case II The boundary plane is between planes E and F. This is a region where the projected area is made up of parts of two ellipses. One is the shadow ellipse and the other is the ellipse formed by the intersection of the ellipsoid and the plane p.

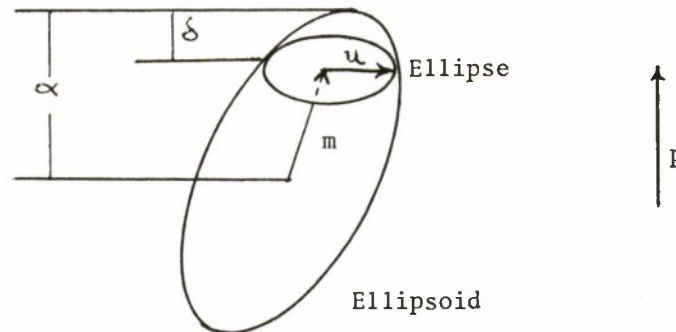
Case III The boundary plane is below plane F. In this case, the full shadow ellipse is produced and does not alter with the penetration distance or orientation of the boundary plane.

Computation in the Above Cases

It may be shown that

$$p \cdot e = (p \cdot A^{-1} p - (p \cdot t)^2 / t \cdot A t)^{1/2} = -p \cdot f$$

Case I This case exists when $\delta > 0$ and $\alpha > p \cdot e + \delta$



The center of the ellipse of intersection is at m where

$$m = (\alpha - \delta) A^{-1} p / p \cdot A^{-1} p$$

FIGURE 11 Intersection Ellipsoid

The equation of a point u on this ellipse is

$$u \cdot B u = 1$$

where u is measured from the center of the ellipse hence lies in the plane of intersection, and

$$B = (I - p p \cdot) A (I - p p \cdot) / (1 - m \cdot A m)$$

$$m \cdot A m = (\alpha - \delta)^2 / p \cdot A^{-1} p$$

The matrix B is singular (has a zero eigenvalue) but the product of the two non zero eigenvalues is the reciprocal of the square of the product of the major and minor axis of the ellipse. The area is the product of π times the product of the major and minor axes.

We have

$$P = \text{product of eigenvalues} = [(\text{tr}(B))^2 - \text{tr}(B^2)]/2$$

where $\text{tr}(B)$ is the trace (sum of diagonal elements) of the matrix B .

For a matrix such as B , the product of the eigenvalues can most readily be computed as the sum of the principle minors.

Hence,

$$\text{Area} = \pi (1 - m \cdot A_m) / p^{1/2}$$

The area normal to t is then equal to $|p \cdot t|$.

The point of force application will be taken as the center of the ellipse (i.e. $A_t m$)

Case III Full Shadow

This exists when $\delta > 0$ and $\delta > p \cdot e + \alpha = \alpha - p \cdot f$

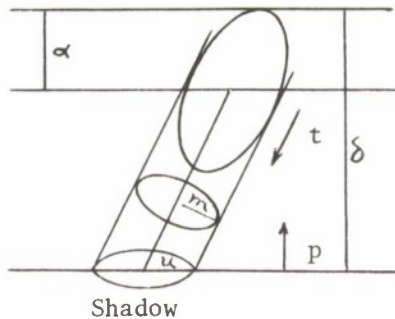


FIGURE 12 Full Shadow

At point u on the shadow ellipsoidal cone is measured from the center of the ellipse in a plane \perp to t .

$$u \cdot C u = 1$$

$$\text{where } C = A - A_t(A_t) \cdot / t \cdot A_t$$

The product p of the nonzero eigenvalues is the sum of the principle minors of C . The projected area is then $\text{Area} = \pi / p^{1/2}$

The force is applied at center of ellipsoid.

Case II Mixed Region

The exact calculation here is involved since it involves the computation of areas of partial ellipses. Since the method of aerodynamic force computation is only an approximation, we decided that it is reasonable to compute the projected area and the point of force application in the following manner:

1. Referring to Figure 9, if \mathcal{S} is less than zero, no penetration has occurred so no aerodynamic force will be applied.
2. If \mathcal{S} is positive, a scale factor is computed as (Figure 10)
$$\text{Scale} = (\alpha - \mathcal{S} + |p \cdot e|) / (\alpha + |p \cdot e|)$$

If scale is greater than one, no penetration has occurred ($\mathcal{S} < 0$).
If scale is less than zero, the ellipsoid has penetrated enough that Case III applies. In this case, scale is set to zero.
3. The full projected Area is computed by the formula in Case III
$$\text{Area} = \pi / p^{1/2}.$$

The effective area is computed as
$$\text{Effective Area} = (1 - \text{Scale}^2) * \text{Area}$$
4. The point of force application is computed as
$$q = \text{Scale} * r$$

where r is the vector from the center of the ellipsoid to the point of maximum penetration (see Figure 9.)
5. The aerodynamic force is computed by interpolating the given table of pressure for the proper time and multiplying this pressure by the Area.
6. The force and torque are then applied to the segment.

Section 5

REFERENCES

1. Fleck, J.T., Butler, F.E., and Vogel, S.L., "An Improved Three-Dimensional Computer Simulation of Motor Vehicle Crash Victim," Calspan Technical Report No. ZQ-5180-L-1, July 1974. Vol. I Engineering Manual, Vol. II Model Validation, Vol. III User's Manual, Vol. IV Programmer's Manual.
2. Bartz, J.A., "A Three-Dimensional Computer Simulation of a Motor Vehicle Crash Victim' Phase 1 Development of the Computer Program" Calspan Technical Report No. VJ-2978-U-1, July 1971.
3. Bartz, J.A., and Butler, F.E., "A Three-Dimensional Computer Simulation of a Motor Vehicle Crash Victim' Phase 2 Validation of the Model, "Calspan Technical Report No. VJ-2978-V-2, December 1972.

APPENDIX A

REV 12 12/19/74
INPUT DESCRIPTION FOR THE CALSPAN 3-D CRASH VICTIM SIMULATION PROGRAM
AS SUPPLIED TO WRIGHT PATTERSON A.F.B. (CONTRACT NO. F33615-75-C-5002)

NOTE: THIS REPORT IS SUPPLIED WITH 'I' IN COLUMN 1 FOR PAGE SKIP
CONTROL TO ALLOW FOR PRINTING ON VARIOUS COMPUTER SYSTEMS.

THE FOLLOWING SPECIAL SYMBOLS MAY DIFFER ON OTHER SYSTEMS:

"#" IS USED TO INDICATE "NOT EQUAL".
"<" IS USED TO INDICATE "LESS THAN".
">" IS USED TO INDICATE "GREATER THAN".
"|" IS USED TO INDICATE "ABSOLUTE VALUE".

ANY LINE WITH A "|" AT THE RIGHT INDICATES A CHANGE MADE TO THIS
INPUT DESCRIPTION INCLUDED IN CALSPAN REPORT NO. ZQ-5180-L-I ENTITLED
"AN IMPROVED THREE DIMENSIONAL COMPUTER SIMULATION OF MOTOR VEHICLE
CRASH VICTIMS" (JULY 1974).

OUTLINE OF INPUT TO THE PROGRAM :

- CARDS A - DATE AND RUN DESCRIPTION, UNITS OF INPUT AND OUTPUT,
CONTROL OF RESTART, INTEGRATOR AND OPTIONAL OUTPUT.
- CARDS B - PHYSICAL CHARACTERISTICS OF THE SEGMENTS AND JOINTS.
- CARDS C - DESCRIPTION OF THE VEHICLE MOTION.
- CARDS D - CONTACT PLANES, BELTS, AIR BAGS, CONTACT ELLIPSOIDS,
CONSTRAINTS, AND SYMMETRY OPTIONS.
- CARDS E - FUNCTIONS DEFINING FORCE-DEFLECTIONS, INERTIAL SPIKE,
ENERGY ABSORPTION FACTOR, AND FRICTION COEFFICIENTS.
- CARDS F - ALLOWED CONTACTS AMONG SEGMENTS, PLANES, BELTS, AIR BAGS
AND CONTACT ELLIPSOIDS.
- CARDS G - INITIAL ORIENTATIONS AND VELOCITIES OF THE SEGMENTS.
- CARDS H - CONTROL OF OUTPUT OF TIME HISTORY OF SELECTED SEGMENT
MOTIONS AND JOINT PARAMETERS.

A. MAIN PROGRAM INPUT

CARD A.1.A	FORMAT (3A4,2I4,F8.0)
DATE(1),I=1,3	DATE OF THE RUN (12 CHARACTERS).
IRSIN	RESTART INPUT UNIT NO. IF BLANK OR ZERO, ALL INPUT TO BE SUPPLIED ON CARDS A.3 TO CARDS H.7. IF NONZERO (SUGGESTED VALUE =4) INPUT WILL BE SUPPLIED FROM A PREVIOUS RESTART TAPE AND CARDS A.1.B,C AND A.2.
IRSOUT	RESTART OUTPUT UNIT NO. IF NONZERO (SUGGESTED VALUE =3) RECORDS WILL BE WRITTEN ON THIS OUTPUT UNIT FOR FUTURE RESTART RUNS. AN INITIAL RECORD CONTAINING ALL INPUT AND INITIALIZATION DATA WILL BE WRITTEN PLUS A TIME POINT RECORD AT EVERY TIME INTERVAL AS SPECIFIED BY DT ON CARD A.4.
RSTIME	RESTART TIME (SEC.) REQUIRED IF IRSIN # 0. SHOULD BE NONZERO AND AN INTEGER MULTIPLE OF DT ON CARD A.4. PROGRAM WILL READ RECORDS FROM THE PREVIOUS RESTART TAPE UP TO AND INCLUDING THIS TIME, MAKE CHANGES PER CARD A.2 AND CONTINUE OPERATION FROM THERE.
CARDS A.1.B - A.1.C	FORMAT (20A4/20A4)
COMENT(1),I=1,40	DESCRIPTION OF THE RUN (160 CHARACTERS ON TWO CARDS).

THESE CARDS REQUIRED ONLY IF IRSIN > 0 , IN WHICH CASE ALL OTHER INPUT AS SPECIFIED ON CARDS A.3 TO H.7 ARE BYPASSED. TWO SETS OF A.2 (EACH TERMINATED WITH A BLANK CARD) ARE REQUIRED. THE FIRST SET IS PROCESSED AFTER THE INITIAL INPUT RECORD IS READ FROM INPUT UNIT IRSIN AND, IF IRSOUT # 0, BEFORE THE INPUT RECORD IS WRITTEN ON OUTPUT UNIT IRSOUT. THE SECOND SET IS PROCESSED AFTER THE TIME POINT RECORD FOR TIME = RSTIME HAS BEEN READ AND, IF IRSOUT # 0, AFTER THE SAME RECORD IS WRITTEN ON OUTPUT UNIT IRSOUT, BUT BEFORE THE PROGRAM RESUMES OPERATION.

CARDS A.2.A - A.2.N FORMAT(A8, 4I4, 2(F8.0, I8, A8))

AVAR	ALPHANUMERIC NAME (LEFT ADJUSTED IN FIELD) OF VARIABLE TO BE REDEFINED FOR RESTART. PROGRAM IS CAPABLE OF CHANGING ANY VARIABLE IN THE LABELED COMMON BLOCKS AS USED AFTER ALL INITIALIZATION HAS BEEN PERFORMED. THE USER SHOULD ASCERTAIN THAT CHANGING THIS VARIABLE IS VALID FOR THE PROGRAM.
INDEX(I), I=1,3	THE ARRAY INDICES, IF ANY, OF THE VARIABLE. MUST AGREE IN NUMBER AND THE VALUES MUST BE LESS THAN OR EQUAL TO THE DIMENSIONS OF THE VARIABLE. BLANK OR ZERO FOR NO DIMENSION.
ITYPE	SUPPLY 1,2 OR 3 TO INDICATE THAT THE NEW VALUE IS TO BE REAL(RR), INTEGER(II) OR ALPHANUMERIC(AA). MUST AGREE WITH THE TYPE OF THE VARIABLE WITHIN THE PROGRAM.
RR, II OR AA	NEW VALUE OF THE VARIABLE AVAR TO BE SUPPLIED IN THE APPROPRIATE FIELD DETERMINED BY THE VALUE OF ITYPE.
RROLD, IIOLD OR AAOLD	THE PREVIOUS VALUE OF THE VARIABLE AVAR IN THE APPROPRIATE FIELD ACCORDING TO THE ITYPE VALUE. INTEGER OR ALPHANUMERIC DATA WILL BE TESTED EXACTLY, REAL DATA TO 5 SIGNIFICANT DIGITS. IF THE CURRENT VALUE IS DIFFERENT, THE PROGRAM WILL TERMINATE WITH AN ERROR MESSAGE. IF ZERO OR BLANK IS SUPPLIED, NO CHECK IS PERFORMED.

THESE A.2 CARDS WILL BE PROCESSED UNTIL A BLANK VALUE FOR AVAR IS ENCOUNTERED. NO FURTHER INPUT IS REQUIRED.

CARD A.3 FORMAT (3A4, 3F12.0)

 UNITL UNIT OF LENGTH (4 CHARACTERS)

 UNITM UNIT OF FORCE (MASS) (4 CHARACTERS)

 UNITT UNIT OF TIME (4 CHARACTERS).

NOTE : UNITL, UNITM AND UNITT SHOULD CORRESPOND TO THE USER'S INPUTS. THROUGHOUT THIS DESCRIPTION, INCHES, POUNDS AND SECONDS (IN,LBS,SEC) ARE USED AS SAMPLE UNITS.

 GRAVTY(I),I=1,3 THE X, Y AND Z COMPONENTS OF GRAVITY (IN/SEC**2).

CARD A.4 FORMAT (2I4, 4F8.0)

 NDINT NUMBER OF ITERATIONS FOR FINAL CONVERGENCE TEST OF THE INTEGRATOR SUBROUTINE DINT (MINIMUM VALUE = 2, SUGGESTED VALUE = 4).

 NSTEPS NUMBER OF INTEGRATION STEPS (OR OUTPUT TIME POINTS) FOR THE INTEGRATOR ROUTINE. MAY BE ZERO TO OBTAIN INITIAL CONDITIONS.

 DT MAIN PROGRAM TIME INTERVAL FOR INTEGRATOR ROUTINE OUTPUT (SEC). TOTAL TIME OF RUN WILL BE NSTEPS*DT SECONDS WITH MAIN PROGRAM TAPE 1, PRINTER PLOT AND OPTIONAL OUTPUT PRODUCED EVERY DT SECONDS.

 HO INITIAL INTEGRATOR STEP SIZE (SEC).

 HMAX MAXIMUM INTEGRATOR STEP SIZE (SEC). FOR BEST EFFICIENCY DT SHOULD BE AN INTEGRAL MULTIPLE OF HMAX AND HMAX A POWER OF TWO MULTIPLE OF HO. (SUGGESTED VALUE = 0.001 SEC.)

 HMIN MINIMUM INTEGRATOR STEP SIZE (SEC). IF A FIXED STEP SIZE IS DESIRED, SET HMIN GREATER THAN HMAX, AND STEP SIZE WILL DOUBLE FROM HO UNTIL HMAX IS ACHIEVED.

NPRT(I),I=1,40

AN ARRAY OF INDICATORS THAT CONTROL VARIOUS OPTIONAL DIAGNOSTIC OUTPUT FOR THE PROGRAM. A VALUE OF ZERO OR BLANK INDICATES NO OUTPUT FOR THAT PARTICULAR ITEM. IN GENERAL, A VALUE OF 1 MEANS THAT THE OUTPUT WILL BE PRODUCED EVERY TIME A PARTICULAR SUBROUTINE IS EXECUTED. HOWEVER, FOR ELEMENTS 1-6 THE VALUE INDICATES THE PRINT FREQUENCY, E.G., A VALUE OF 5 WILL PRODUCE OUTPUT EVERY 5TH EXECUTION OF THE SUBROUTINE. OUTPUT PRODUCED BY ELEMENTS 7-26 IS INTENDED FOR DIAGNOSTIC OR "CHECK OUT" PURPOSES AND IS NOT COMPLETELY LABELED. THE USER SHOULD CONSULT THE LISTING OF THE SUBROUTINE FOR A DESCRIPTION OF THE VARIABLES THAT ARE PRINTED.

THE NPRT ARRAY

ELEMENT NO.	SUBROUTINE	OUTPUT PRODUCED
1	MAIN	TAPE 1 OUTPUT
2	MAIN	ELTIME OUTPUT
3	MAIN	SUBROUTINE PRINT OUTPUT
4	NOT USED	
5	PRIPLT	Y-Z VIEW PRINTER PLOT
6	PRIPLT	X-Z VIEW PRINTER PLOT
7	BINPUT	HA, HB
8*	DAUX	IJK,RHS,C ARRAYS
9	DAUX	SUBROUTINE PRINT OUTPUT
10	IMPULS	DIAGNOSTIC OUTPUT
11	SETUP1	U2,V1 ARRAYS
12	VISPR	DIAGNOSTIC OUTPUT
13	PRIPLT	CJOINT ARRAY
14	WINDY	WIND FORCES
15	BELTG	DIAGNOSTIC OUTPUT
16	HBELT	HARNES-BELT FORCES
17	EDEPTH	DIAGNOSTIC OUTPUT
18	NOT USED	
19	NOT USED	
20	CHAIN	XCOMP,XVCOMP,SEGLP,SEGLV
21	AIRBAG	DIAGNOSTIC OUTPUT
22	AIRBG1	DIAGNOSTIC OUTPUT
23	AIRBG3	DIAGNOSTIC OUTPUT
24	UPDATE	ROLL-SLIDE TEST OUTPUT
25	DINT	CONVERGENCE TEST DATA
26	DINT	SUBROUTINE OUTPUT EVERY STEP

* A VALUE OF NPRT(8) = 2 WILL PRINT ARRAYS BEFORE AND AFTER THE FIRST CALL TO SUBROUTINE FSMSOL ONLY.

B. SUBROUTINE BINPUT

CARD B.1 FORMAT (2I6, 8X, 5A4)

NSEG THE NUMBER OF SEGMENTS (MAXIMUM = 20).
NOTE: THE VEHICLE AND GROUND WILL BE ASSIGNED
SEGMENT NUMBERS NSEG+1 AND NSEG+2.

NJNT THE NUMBER OF JOINTS (MAXIMUM = 21).
NOTE: NORMALLY NJNT = NSEG-1, BUT JOINT
NUMBERS NSEG AND NSEG+1 MAY BE USED TO
CONNECT THE VEHICLE AND THE GROUND TO
LOWER NUMBERED SEGMENTS.

BDYTTL(I),I=1,5 DESCRIPTION OF THE CRASH VICTIM
(20 CHARACTERS).

CARDS B.2.A - B.2.I FORMAT (A4, 1X, A1, 10F6.0)
(NSEG CARDS)

EACH CARD (I) FOR I = 1, NSEG WILL CONTAIN INPUT DATA FOR THE ITH
SEGMENT. THE SEGMENT IDENTIFYING NUMBERS (I) WILL BE REFERRED TO
ON LATER INPUT CARDS.

SEG(I) AN ABBREVIATION OF THE NOMENCLATURE
OF THE ITH SEGMENT (4 CHARACTERS).

CGS(I) THE PLOT SYMBOL OF THE SEGMENT C.G.
(1 CHARACTER).

W(I) THE WEIGHT OF THE SEGMENT (LBS).

PHI(J,I),J=1,3 THE PRINCIPAL MOMENTS OF INERTIA OF THE
SEGMENT ABOUT THE X, Y, AND Z
AXES OF THE SEGMENT (LBS-SEC**2-IN).
THERE ARE NO RESTRICTIONS ON THE VALUES OF
W(I) OR PHI(J,I), THEY MAY BE NEGATIVE OR
ZERO. IF ANY COMPONENT IS ZERO, IT IS
ASSUMED THAT THE SYSTEM IS SUITABLY CON-
STRAINED SO THAT THE SYSTEM MATRIX IS NON-
SINGULAR.

BD(J,I),J=1,3 THE X, Y, AND Z SEMIAXES OF THE
SEGMENT CONTACT ELLIPSOID (IN).

BD(J,I),J=4,6 THE LOCATION OF THE CENTER OF THE SEGMENT
CONTACT ELLIPSOID, WITH RESPECT TO THE
CENTER OF GRAVITY OF THE SEGMENT, IN THE
LOCAL BODY SEGMENT REFERENCE(IN). THESE
PRIMARY CONTACT ELLIPSOIDS ARE GIVEN THE
SAME IDENTIFYING NUMBER AS THE SEGMENT.
THEY MAY BE REDEFINED WITH AN ARBITRARY
ORIENTATION ON CARDS D.5.

CARDS B.3.A - B.3.J FORMAT (A4, 1X, A1, 2I4, 6F6.0/ 14X, 6F6.0)
 (2*NJNT CARDS - 2 CARDS FOR EACH JOINT)

EACH CARD (J) FOR J = 1, NJNT WILL CONTAIN INPUT DATA FOR THE JTH JOINT. THE JOINT IDENTIFYING NUMBERS (J) WILL BE REFERRED TO ON LATER INPUT CARDS.

JOINT(J) AN ABBREVIATION OF THE NOMENCLATURE OF THE JTH JOINT (4 CHARACTERS).

JS(J) PLOT SYMBOL OF THE JOINT LOCATION (1 CHARACTER).

JNT(J) MAGNITUDE INDICATES THE NUMBER OF THE SEGMENT THAT IS CONNECTED TO SEGMENT J+1 BY JOINT J. IF NEGATIVE, JOINT J IS ASSOCIATED WITH A FLEXIBLE ELEMENT. IF ZERO, SEGMENT J+1 IS THE REFERENCE SEGMENT OF ANOTHER BODY. (|JNT(J)| < J+1).

IPIN(J) 0 - THERE ARE TO BE NO CONSTRAINTS ON JOINT J.
 1 - JOINT J IS PINNED (HINGE).
 2 - JOINT J IS NOT PINNED (BALL AND SOCKET).
 4 - JOINT J IS AN EULER JOINT.
 NON-ZERO VALUES FOR IPIN MAY BE SUPPLIED AS POSITIVE OR NEGATIVE TO INDICATE THAT THE INITIAL CONDITION OF THE JOINT IS UNLOCKED (POSITIVE) OR UNLOCKED (NEGATIVE). THE INITIAL STATE OF AN EULER JOINT IS SET BY USE OF IPIN AS FOLLOWS

IPIN	IEULER	STATE
4	8	FREE
- 4	7	ALL AXES LOCKED
- 5	6	SPIN FREE, OTHERS LOCKED
- 6	5	NUTATION FREE, OTHERS LOCKED
- 7	4	PRECESSION FREE, OTHERS LOCKED
- 8	3	SPIN LOCKED, OTHERS FREE
- 9	2	NUTATION LOCKED, OTHERS FREE
-10	1	PRECESSION LOCKED, OTHERS FREE

(PRECESSION ABOUT Z
 NUTATION ABOUT RESULTANT X
 SPIN ABOUT RESULTANT Z)
 IF IPIN IS LESS THAN -3 PROGRAM WILL SET IEULER AS ABOVE AND THEN SET IPIN = -4.

SR(I,2*J-1),I=1,3 COORDINATES OF LOCATION OF JOINT J (IN.) IN THE LOCAL REFERENCE SYSTEM OF SEGMENT JNT(J).

SR(I,2*J),I=1,3 COORDINATES OF LOCATION OF JOINT J (IN.) IN THE LOCAL REFERENCE SYSTEM OF SEGMENT J+1.

FOLLOWING DATA IS ON 2ND CARD FOR EACH JOINT.

YPR1(I,J),I=1,3 THE YAW, PITCH AND ROLL ANGLES (DEGREES)
 SPECIFYING THE PRINCIPAL AXES OF JOINT J IN
 THE LOCAL REFERENCE SYSTEM OF SEGMENT JNT(J).
 YAW ABOUT Z AXIS
 PITCH ABOUT RESULTANT Y AXIS
 ROLL ABOUT RESULTANT X AXIS

YPR2(I,J),I=1,3 THE YAW, PITCH AND ROLL ANGLES (DEGREES)
 SPECIFYING THE PRINCIPAL AXES OF JOINT J IN
 THE LOCAL REFERENCE SYSTEM OF SEGMENT J+1.
 THE Z AXIS IS THE REFERENCE AXIS TO DEFINE
 FLEXURE. THE Y AXIS IS USED AS THE PIN AXIS
 EXCEPT FOR THE SPECIAL EULER JOINTS. THE XY
 PLANE IS USED FOR GLOBALGRAPHIC JOINTS WITH
 X AS THE REFERENCE AXIS.

CARDS B.4.A - B.4.J FORMAT (2 (4F6.0, F12.0))
(NJNT SETS OF CARDS, ONE FOR EACH JOINT J. IF |IPIN(J)| # 4,
EACH SET READS VALUES FOR 3*J-2 AND 3*J-1 ON ONE CARD ONLY.
IF |IPIN(J)| = 4 , JOINT J IS AN EULER JOINT AND A SECOND CARD
IS NECESSARY TO READ VALUES FOR 3*J)

SPRING(I,3*J-2), THE FLEXURAL SPRING CHARACTERISTICS FOR
I=1,5 JOINT J. IF J IS AN EULER JOINT, THE SPRING
CHARACTERISTICS ABOUT THE PRECESSION AXIS.
IF JOINTF(J) # 0 (ON CARD F.5.A), THESE
VALUES ARE NOT USED AND SHOULD BE ZERO.

SPRING(I,3*J-1), THE TORSIONAL SPRING CHARACTERISTICS FOR
I=1,5 JOINT J. IF J IS AN EULER JOINT, THE SPRING
CHARACTERISTICS ABOUT THE NUTATION AXIS.

SPRING(I,3*J), SECOND CARD OF EACH SET IS REQUIRED
I=1,5 ONLY IF J IS AN EULER JOINT, THE SPRING
CHARACTERISTICS ABOUT THE SPIN AXIS.

I=1 LINEAR SPRING COEFFICIENT
(IN-LBS/DEG).

I=2 QUADRATIC SPRING COEFFICIENT
(IN-LBS/DEG**2).

I=3 CUBIC SPRING COEFFICIENT
(IN-LBS/DEG**3).

I=4 ENERGY DISSIPATION COEFFICIENT
(DIMENSIONLESS).
A VALUE OF 1. SPECIFIES NO LOSS
A VALUE OF 0. SPECIFIES MAXIMUM LOSS

I=5 JOINT STOP LOCATION WITH RESPECT TO
THE CENTER OF SYMMETRY (DEG).
FOR A VALUE OF ZERO THE ROUTINE WILL USE ONLY
THE LINEAR SPRING COEFFICIENT AND WILL APPLY
THE ENERGY DISSIPATION FACTOR

CARDS B.5.A - B.5.J FORMAT(5F6.0, 18X, 2F6.0)
 (NJNT SETS OF CARDS, ONE FOR EACH JOINT J. IF |IPIN(J)| # 4,
 VALUES FOR 3*J-2 ARE ON ONE CARD ONLY. IF |IPIN(J)| = 4,
 J IS AN EULER JOINT AND VALUES FOR 3*J-1 AND 3*J ARE REQUIRED
 ON A SECOND AND THIRD CARD OF EACH SET.)

VISC(I,3*J-2), THE VISCOUS CHARACTERISTICS FOR JOINT J.
 I=1,7 IF J IS AN EULER JOINT, THE VISCOUS CHAR-
 ACTERISTICS ABOUT THE PRECESSION AXIS.

VISC(I,3*J-1), THE SECOND CARD OF EACH SET IS REQUIRED
 I=1,7 ONLY IF J IS AN EULER JOINT, THE VISCOUS
 CHARACTERISTICS ABOUT THE NUTATION AXIS.

VISC(I,3*J) THE THIRD CARD OF EACH SET IS REQUIRED
 I=1,7 ONLY IF J IS AN EULER JOINT, THE VISCOUS
 CHARACTERISTICS ABOUT THE SPIN AXIS.

- I=1 VISCOUS COEFFICIENT (IN-LB-SEC/DEG).
- I=2 COULOMB FRICTION COEFFICIENT (IN-LB).
- I=3 RELATIVE ANGULAR VELOCITY OF JOINT
 AT WHICH FULL COULOMB FRICTION IS
 APPLIED (DEG/SEC). MUST BE GREATER THAN 0.
- I=4 T1: THE MAXIMUM TORQUE (IN-LBS) ALLOWED FOR A
 LOCKED JOINT (OR EULER AXIS). IF EXCEEDED, THE
 JOINT WILL UNLOCK. IF T1 = 0, THE TEST WILL
 NOT BE PERFORMED.
- I=5 T2: THE MINIMUM TORQUE (IN-LBS)
 ALLOWED FOR JOINT J TO REMAIN UNLOCKED.
 IF T2 = 0, THE TEST WILL NOT BE PERFORMED.
- I=6 T3: THE MINIMUM ANGULAR VELOCITY (RAD/SEC)
 NECESSARY FOR JOINT J TO REMAIN UNLOCKED.
 IF T3 = 0, THE TEST WILL NOT BE PERFORMED.
- I=7 $E = (1+U)/2$ WHERE U IS THE CLASSICAL
 COEFFICIENT OF RESTITUTION TO BE USED FOR THE
 IMPULSE OPTION IF THE JOINT HITS THE JOINT
 STOP ($0 < E < 1$ OR $-1 < U < 1$). A VALUE OF $E = 0$
 MEANS THAT THE IMPULSE OPTION WILL NOT BE
 EXERCISED FOR THIS JOINT.

CARDS B.6.A - B.6.I
(NSEG CARDS)

FORMAT (12F6.0)

SGTEST(1,1,I)	MAGNITUDE TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (RAD/SEC).
SGTEST(2,1,I)	ABSOLUTE ERROR TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (RAD/SEC).
SGTEST(3,1,I)	RELATIVE ERROR TEST FOR THE ANGULAR VELOCITY OF SEGMENT NO. I (DIMENSIONLESS).
SGTEST(1,2,I) (2,2,I) (3,2,I)	SAME AS ABOVE, BUT FOR THE LINEAR VELOCITY OF SEGMENT NO. I (IN/SEC).
SGTEST(1,3,I) (2,3,I) (3,3,I)	SAME AS ABOVE, BUT FOR THE ANGULAR ACCELERATION OF SEGMENT NO. I (RAD/SEC**2).
SGTEST(1,4,I) (2,4,I) (3,4,I)	SAME AS ABOVE BUT FOR THE LINEAR ACCELERATION OF SEGMENT NO. I (IN/SEC**2).

THESE CONVERGENCE TESTS ARE PERFORMED IN SUBROUTINE DINT ON THE RESULTANT OF THE DERIVATIVE VECTORS. THE LINEAR VELOCITIES AND ACCELERATIONS ARE COMPUTED ONLY FOR REFERENCE SEGMENTS (I.E. SEGMENT NO. 1 AND THOSE SEGMENTS I WHERE $JNT(I-1) = 0$), THEREFORE ANY TEST NUMBERS SUPPLIED FOR LINEAR VELOCITIES AND ACCELERATIONS OF OTHER SEGMENTS WILL BE IGNORED. THE TESTS FOR CONVERGENCE ARE PERFORMED IN THE FOLLOWING ORDER :

- 1) IF THE MAGNITUDE TEST IS ZERO, NO TESTING IS DONE FOR THAT VARIABLE.
- 2) IF THE MAGNITUDE OF THE RESULTANT VECTOR IS LESS THAN THE MAGNITUDE TEST, THE ROUTINE HAS PASSED THE CONVERGENCE TEST FOR THAT VARIABLE.
- 3) IF THE ABSOLUTE ERROR TEST IS GREATER THAN ZERO, AND THE MAGNITUDE OF THE ABSOLUTE ERROR (DIFFERENCE BETWEEN THE PREDICTED AND COMPUTED VECTOR) IS LESS THAN THE ABSOLUTE ERROR TEST, THE ROUTINE HAS PASSED THE CONVERGENCE TEST FOR THAT VARIABLE.
- 4) IF THE RELATIVE ERROR OF THE MAGNITUDE OF THE ABSOLUTE ERROR COMPARED TO THE MAGNITUDE OF THE COMPUTED VECTOR IS GREATER THAN THE RELATIVE ERROR TEST, THE CONVERGENCE TEST HAS FAILED.

IF NFLX # 0, CARDS B.7 ARE REQUIRED. EACH FLEXIBLE ELEMENT AS DEFINED ON CARDS B.3 CONTAINS AT LEAST THREE CONNECTED SEGMENTS CONSISTING OF A REFERENCE SEGMENT, ONE OR MORE INTERIOR SEGMENTS AND A TERMINATING SEGMENT. EACH JOINT IN THE ELEMENT SHOULD HAVE A NEGATIVE VALUE FOR JNT, AND THE NUMBER OF INTERIOR SEGMENTS WILL BE ONE LESS THAN THE NUMBER OF NEGATIVE VALUES OF JNT FOR EACH ELEMENT. NFLX IS THE TOTAL NUMBER OF INTERIOR SEGMENTS OF ALL FLEXIBLE ELEMENTS.

CARD B.7.A FORMAT (18I4)

 NFX THE NUMBER OF INTERIOR SEGMENTS FOR WHICH HF ARRAYS ARE TO BE SUPPLIED.

 KNT(K),K=1,NFX THE INTERIOR SEGMENT IDENTIFICATION NUMBERS IN THE ORDER OF THE HF ARRAYS TO BE SUPPLIED. IF THE VALUES OF NFX AND KNT ARE NOT CONSISTENT WITH THE NEGATIVE VALUES OF JNT ON CARDS B.3 THE PROGRAM WILL TERMINATE WITH AN APPROPRIATE ERROR MESSAGE.

CARDS B.7.B - B.7.N FORMAT (12F6.0)
 (4*NFX CARDS, 4 CARDS FOR EACH SEGMENT IN THE ORDER AS THEY ARE DEFINED IN THE KNT VECTOR.)

(HF(I,J,K),J=1,12) THE COEFFICIENTS OF THE QUADRATIC FORM
 ,I=1,4 FUNCTION USED TO DEFINE THE ORIENTATION OF INTERIOR SEGMENT KNT(K) WITH RESPECT TO REFERENCE SEGMENT OF THE ELEMENT.

FORM THE COLUMN VECTOR V WITH FOUR COMPONENTS Y,P,R AND 1, WHERE Y,P,R ARE THE YAW, PITCH AND ROLL OF THE TERMINATING SEGMENT RELATIVE TO THE REFERENCE SEGMENT. LET H BE A SYMMETRIC 4X4 MATRIX SUCH THAT $F(V) = 1/2 V \cdot HV$ REPRESENTS A QUADRATIC SCALAR FUNCTION OF THE VARIABLES Y,P AND R IN RADIANS. THUS

 YAW OF SEGMENT KNT(K) = $1/2 V \cdot HF(I, J, K) V$
 PITCH OF SEGMENT KNT(K) = $1/2 V \cdot HF(I, J+4, K) V$
 ROLL OF SEGMENT KNT(K) = $1/2 V \cdot HF(I, J+8, K) V$ (I,J=1,4)

C. SUBROUTINE VINPUT

CARD C.1 FORMAT (20A4)
 VPSTTL(I),I=1,20 DESCRIPTION OF THE CRASH VEHICLE DECELERATION
 (80 CHARACTERS).

CARD C.2 FORMAT (8F6.0, I6, 2F6.0)
 ANGLE(I),I=1,3 FOR THE HALF SINE-WAVE DECELERATION
 (NATAB = 0) OR FOR THE UNIDIRECTIONAL
 DECELERATION TABULAR INPUT (NATAB > 0),
 ANGLE(1) AND ANGLE(2) REPRESENT THE
 AZIMUTH AND ELEVATION (OBLIQUE ANGLES)
 OF THE DIRECTION OF THE DECELERATION
 IMPULSE (DEG). ANGLE(3) IS NOT USED
 AND THE INITIAL YAW, PITCH AND ROLL
 OF THE VEHICLE ARE ASSUMED TO BE ZERO.
 FOR THE OMNIDIRECTIONAL TABULAR INPUT
 (NATAB < 0). THEY REPRESENT THE INITIAL
 YAW, PITCH AND ROLL OF THE VEHICLE (DEG).

 VIPS THE INITIAL VELOCITY OF THE CRASH VEHICLE.
 (IN/SEC - UNITS AS SPECIFIED ON CARD A.3)
 A NEGATIVE VALUE MAY BE SUPPLIED FOR NATAB=0
 TO INDICATE THAT THE VEHICLE WILL ACCELERATE
 FROM A VELOCITY OF ZERO TO |VIPS|.

 VTIME THE TIME DURATION OF THE DECELERATION
 IMPULSE (SEC). REQUIRED ONLY IF NATAB = 0.
 A VALUE OF ZERO IS NOT PERMITTED IF NATAB=0.

 XO(I),I=1,3 THE INITIAL X, Y, AND Z COORDINATES
 OF THE VEHICLE REFERENCE ORIGIN IN
 INERTIAL REFERENCE (IN).

 NATAB INTEGER NUMBER OF TIME POINTS FOR WHICH
 VEHICLE DECELERATION DATA IS TO BE SUPPLIED.
 THE ALGEBRAIC SIGN OF NATAB DETERMINES THE
 TYPE OF VEHICLE MOTION AS FOLLOWS:

 IF NATAB = 0, THE DIRECTION IMPULSE IS AN
 ANALYTICAL HALF-SINE WAVE FUNCTION THAT
 DECELERATES THE VEHICLE FROM AN INITIAL
 SPEED OF VMPH TO ZERO IN VTIME SECONDS.

 IF NATAB > 0, THE VEHICLE MOTION IS
 UNIDIRECTIONAL AND ONLY THE RESULTANT LINEAR
 DECELERATION IS INPUTTED IN TABULAR FORM ON
 CARDS C.3. (NATAB SHOULD BE ODD AND MAXIMUM
 VALUE IS 99.)

 IF NATAB < 0, THE VEHICLE MOTION IS ALSO
 ROTATIONAL, AND THE COMPONENTS OF BOTH
 LINEAR AND ANGULAR ACCELERATION ARE INPUTTED
 IN TABULAR FORM ON CARDS C.4. (MINIMUM
 VALUE OF NATAB IS -100.)

ATO THE BEGINNING TIME POINT FOR THE
DECELERATION TABLE INPUT (SEC).

ADT FIXED TIME INTERVAL FOR THE DECELERATION
TABLE INPUT (SEC).

CARDS C.3.A - C.3.N FORMAT (12F6.0)

THESE CARDS ARE REQUIRED ONLY IF NATAB > 0.

ATAB(I,I), I=1, NATAB THE NATAB VALUES OF DECELERATION
(G'S) FOR THE CRASH VEHICLE
FOR FIXED TIME INTERVALS

$T(I) = ATO + (I-1)*ADT$ FOR I=1, NATAB.

SUPPLY 12 VALUES PER CARD, USE AS MANY CARDS
AS NECESSARY. SINCE A SIMPSON'S INTEGRATION
IS USED TO COMPUTE VELOCITY AND POSITION,
THE VALUE OF NATAB MUST BE ODD. THE LAST
VALUE, ATAB(1, NATAB) WILL BE USED TO INTEGRATE
FOR ANY TIME GREATER THAN T(NATAB-1).

CARDS C.4.A - C.4.M FORMAT (10X, 6F10.0)

MATAB CARDS ARE REQUIRED ONLY IF NATAB < 0 (MATAB = -NATAB)

EACH CARD (I) WILL CONTAIN THE LINEAR AND ANGULAR ACCELERATIONS
FOR TIME $T(I) = ATO + (I-1)*ADT$ FOR I = 1, MATAB.

ATAB(J,I), J=1,3 THE VALUES OF THE X, Y AND Z COMPONENTS OF
LINEAR DECELERATION (G'S) FOR TIME POINT
T(I). THE PROGRAM WILL INTEGRATE FOR VELOCITY
AND POSITION BEYOND THE LAST TIME POINT
USING THE LAST VALUES SUPPLIED.

ATAB(J,I), J=4,6 THE VALUES OF THE COMPONENTS OF ANGULAR
ACCELERATION (DEG/SEC**2) FOR TIME POINT(I).
THE VALUES FOR THE LAST TIME POINT MUST BE
ZERO WHICH IS ASSUMED BY PROGRAM FOR
INTEGRATING BEYOND THE LAST TIME POINT.

D. SUBROUTINE SINPUT

CARD D.1	FORMAT (6I6)
NPL	THE NUMBER OF PLANES DESCRIBING A CONTACT PANEL OF THE VEHICLE (20 MAXIMUM).
NBLT	THE NUMBER OF BELTS USED TO RESTRAIN THE CRASH VICTIM (8 MAXIMUM).
NBAG	THE NUMBER OF AIR BAGS USED TO RESTRAIN THE CRASH VICTIM (5 MAXIMUM).
NELP	THE NUMBER OF CONTACT ELLIPSOIDS TO BE SUPPLIED ON CARDS D.5.
NQ	THE NUMBER OF CONSTRAINTS TO BE SUPPLIED ON CARDS D.6. EACH CONSTRAINT TYPE 5 WILL BE CONSIDERED AS TWO CONSTRAINTS REQUIRING TWO SETS OF CARDS (NOTE: THE PROGRAM WILL LATER INCREMENT NQ BY 1 FOR EACH $NF(1) = 0$ ON CARDS F.1.B AND F.3.B AND THE FINAL MAXIMUM ON NQ IS 12).
NSD	THE NUMBER OF SPRING DAMPERS TO BE SUPPLIED ON CARDS D.8 (20 MAXIMUM).

IF NPL # 0, NPL SETS OF D.2 ARE REQUIRED.

CARD D.2.A FORMAT (I4, 4X, 5A4)

J THE NUMBER IDENTIFYING THE PLANE,
 MUST BE INPUTTED AS SUCCESSIVE
 INTEGERS 1, 2, 3,...., NPL.

PLTTL(I,J),I=1,5 A 20 CHARACTER DESCRIPTION OF THE
 JTH PANEL.

CARDS D.2.B - D.2.D FORMAT (3F12.0)

P1(I),I=1,3 THE X,Y AND Z COORDINATES OF POINT P1 IN
 VEHICLE (OR SEGMENT TO WHICH PLANE IS
 ATTACHED) REFERENCE (IN).

P2(I),I=1,3 THE X,Y AND Z COORDINATES OF POINT P2 IN
 VEHICLE (OR SEGMENT TO WHICH PLANE IS
 ATTACHED) REFERENCE (IN).

P3(I),I=1,3 THE X,Y AND Z COORDINATES OF POINT P3 IN
 VEHICLE (OR SEGMENT TO WHICH PLANE IS
 ATTACHED) REFERENCE (IN).

WHERE P1, P2, AND P3 ARE 3 OF THE CORNERS OF A BOUNDED RECTANGULAR PLANE
SUCH THAT THE EDGE P1P2 IS 90 DEGREES CLOCKWISE (AS VIEWED FROM THE
EXTERNAL SURFACE) FROM THE EDGE P1P3.

IF NBLT # 0, NBLT SETS OF D.3 ARE REQUIRED.

CARD D.3.A

FORMAT (5A4)

BLTTTL(I,J),I=1,5 A 20 CHARACTER DESCRIPTION OF THE
JTH BELT.

CARD D.3.B

FORMAT (6F12.0)

BELT(I,J),I=1,3 X,Y, AND Z COORDINATES, IN VEHICLE (OR SEGMENT
TO WHICH BELT IS ANCHORED) REFERENCE, OF
ANCHOR POINT A FOR THE JTH BELT (IN).

BELT(I,J),I=4,6 X,Y, AND Z COORDINATES, IN VEHICLE (OR SEGMENT
TO WHICH BELT IS ANCHORED) REFERENCE, OF
ANCHOR POINT B FOR THE JTH BELT (IN).

NOTE: THE PROGRAM MUST PASS A PLANE THROUGH THE THREE POINTS, ANCHOR
POINT A, ANCHOR POINT B, AND A FIXED POINT ON THE CONTACTED BODY SEGMENT.
IF ANCHOR POINTS A AND B COINCIDE, THEY MUST BE SEPARATED SLIGHTLY FOR
INPUT SUCH THAT THE DESIRED BELT PLANE WILL BE DEFINED.

CARD D.3.C

FORMAT (5F12.0)

BELT(I,J),I=7,9 X, Y, AND Z COORDINATES, IN LOCAL BODY
SEGMENT REFERENCE (BUT WITH RESPECT TO
ELLIPSOID CENTER, NOT C.G.), OF THE
FIXED CONTACT POINT ON THE BODY
SEGMENT FOR THE JTH BELT (IN).

BELT(10,J) CURRENTLY NOT USED BY THE PROGRAM.

BELT(11,J) BELT SLACK (IN). THE SLACK, WHEN ADDED TO
THE INITIAL GEOMETRIC LENGTH, RESULTS IN
THE INITIAL BELT LENGTH. IF DESIRED, THE
INITIAL BELT LENGTH MAY BE INPUTTED AS A
NEGATIVE NUMBER AND THE PROGRAM WILL
COMPUTE THE SLACK.

IF NBAG # 0, NBAG SETS OF D.4 ARE REQUIRED BY
SUBROUTINE AIRBGI.

CARD D.4.A	FORMAT (5A4, I4)
BAGTTL(I,J),I=I,5	A 20 CHARACTER DESCRIPTION OF THE JTH AIR BAG.
NPANEL(J)	NUMBER OF VEHICLE CONTACT PANELS THAT ARE ALLOWED TO INTERACT WITH THE JTH AIR BAG (MAXIMUM = 4).
CARD D.4.B	FORMAT(6F12.0)
AB(I,J),I=I,3	THE X, Y AND Z SEMIAXES OF THE JTH AIR BAG WHEN FULLY INFLATED AND UNDEFORMED (IN).
BFA(I,J),I=1,3	THE X,Y AND Z COORDINATES OF THE CENTER OF THE AIR BAG CONTACT ELLIPSOID WITH RESPECT TO THE AIR BAG CENTER OF GRAVITY (IN).
CARD D.4.C	FORMAT (6F12.0)
YB,PB,RB	THE INITIAL ORIENTATION (YAW, PITCH, AND ROLL) OF THE JTH AIR BAG IN THE VEHICLE REFERENCE (DEG).
ZDEP(I,J),I=1,3	THE X, Y, AND Z COORDINATES OF THE DEPLOYMENT POINT OF THE JTH AIR BAG IN THE LOCAL REFERENCE OF THE 1ST PANEL ON CARD D.4.G (IN).
CARD D.4.D	FORMAT (6F12.0)
XBM(J)	WEIGHT OF AIR BAG MEMBRANE AND CONTENTS (LBS).
CYTD(J)	GAS SUPPLY ACTUATOR FIRING TIME AFTER THE START OF VEHICLE DECELERATION (SEC).
CYPA(J)	ATMOSPHERIC PRESSURE (PSIA).
CYSP(J)	INITIAL GAS SUPPLY PRESSURE (PSIG).
CYTO(J)	INITIAL GAS SUPPLY TEMPERATURE (DEG R).
CYVO(J)	GAS SUPPLY RESERVOIR VOLUME (IN**3).

CARD D.4.E

FORMAT (6F12.0)

CYCD(J) SONIC THROAT DISCHARGE COEFFICIENT
(DIMENSIONLESS).

CYK(J) RATIO OF SPECIFIC HEATS OF SUPPLY
GAS (DIMENSIONLESS).

CYR(J) SPECIFIC GAS CONSTANT (IN/DEG R).

CYAT(J) SONIC THROAT AREA (IN**2).

CYPV(J) VENT PRESSURE OF THE EXHAUST
ORIFICE (PSIG).

CYCDO(J) EXHAUST ORIFICE DISCHARGE
COEFFICIENT (DIMENSIONLESS).

CARD D.4.F

FORMAT (5F12.0)

CYAO(J) EXHAUST ORIFICE AREA (IN**2).

SPRK(J) SPRING CONSTANT OF A LINEAR SPRING
USED TO SIMULATE ATTACHMENT OF THE
BAG AT THE DEPLOYMENT POINT IN THE
VEHICLE (LB/IN).

VSCS(J) COEFFICIENT OF SLIDING FRICTION OF
THE AIR BAG (DIMENSIONLESS)

CK(J) PARAMETER USED TO STABILIZE AIR
BAG NUMERICAL INTEGRATION (SEC**-1).
SUGGESTED VALUE = 250.

CMASS(J) MULTIPLIER TO INCREASE OR DECREASE
THE MASS OF THE AIR BAG TO ARTIFICIALLY
DAMPEN THE INTEGRATED AIR BAG MOTION.

NPANEL(J) SETS OF THE FOLLOWING TWO CARDS ARE REQUIRED TO DEFINE THE ELLIPSOIDS USED TO APPROXIMATE THE CONTACT PANELS FOR THE JTH AIR BAG. THE FIRST PANEL IS THE REACTION PANEL.

CARD D.4.G FORMAT (6F12.0)

B(I,K,J),I=1,3 X, Y, AND Z SEMIAXES FOR THE KTH
PANEL FOR THE JTH AIR BAG (IN).

BFB(I,K,J),I=1,3 THE LOCATION OF THE CENTER OF THE
PANEL ELLIPSOID WITH RESPECT TO ITS
CENTER OF GRAVITY (IN).

CARD D.4.H FORMAT (6F12.0)

ZR(I,K,J),I=1,3 X, Y, AND Z COORDINATES IN VEHICLE
REFERENCE OF THE CENTER OF GRAVITY
OF THE KTH PANEL OF THE JTH AIR BAG (IN).

YP,PP,RP THE ORIENTATION, YAW, PITCH, AND
ROLL OF THE KTH PANEL (DEG).

IF NHELP # 0, NHELP D.5 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

NOTE: NHELP IS THE NUMBER OF CONTACT ELLIPSOIDS TO BE SUPPLIED HERE, NOT THE NUMBER OF CONTACT ELLIPSOIDS IN THE PROGRAM. THE FIRST NSEG ELLIPSOIDS WERE SUPPLIED ON CARDS B.2.A - B.2.I WITH NO ANGULAR ROTATIONS. THEY MAY BE REPLACED HERE IF DESIRED.

CARDS D.5.A - D.5.J
(NHELP CARDS)

FORMAT (I6, 9F6.0)

M	CONTACT ELLIPSOID NUMBER. MAX = 24. IF M < NSEG + 1, DATA WILL REPLACE INPUT SUPPLIED ON CARDS B.2.A - B.2.I.
P1(I), I=1,3	THE X, Y, AND Z SEMIAXES OF THE CONTACT ELLIPSOID (IN).
P2(I), I=1,3	THE X, Y, AND Z COORDINATES OF THE ELLIPSOID OFFSET FROM THE SEGMENT CENTER OF GRAVITY.
P3(I), I=1,3	THE YAW, PITCH AND ROLL (DEGREES) OF THE CONTACT ELLIPSOID FROM THE PRINCIPAL AXIS OF THE SEGMENT.

IF NQ # 0, NQ D.6 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

CARDS D.6.A - D.6.J
(NQ CARDS)

FORMAT (3I6, 6F6.0)

KQTYPE(J)

TYPE NO. OF THE JTH CONSTRAINT

- 1: POINT SPECIFIED BY RK1 ON SEGMENT KQ1 WILL BE CONSTRAINED TO BE THE SAME AS THE POINT SPECIFIED BY RK2 ON SEGMENT KQ2.
- 2: POINT SPECIFIED BY RK1 ON SEGMENT KQ1 WILL BE CONSTRAINED TO REMAIN AT AN EQUAL DISTANCE ($D > 0$) FROM THE POINT SPECIFIED BY RK2 ON SEGMENT KQ2.
- 5: TENSION ELEMENT CONSTRAINT CONNECTING POINT RK1 ON SEGMENT KQ1 TO POINT RK2 ON SEGMENT KQ2 (REQUIRES TWO CARDS WITH KQTYPE, KQ1 AND KQ2 THE SAME ON BOTH).

KQ1(J)

SEGMENT IDENTIFICATION NUMBER OF THE 1ST SPECIFIED POINT.

KQ2(J)

SEGMENT IDENTIFICATION NUMBER OF THE 2ND SPECIFIED POINT.

RK1(I,J),I=1,3

COORDINATES OF SPECIFIED POINT ON SEGMENT KQ1 (IN). IF KQTYPE = 5, THE SECOND CARD WILL CONTAIN THE EFFECTIVE MASSES MA, MB AND MAB (LB.SEC**2/IN) IN PLACE OF RK1.

RK2(I,J),I=1,3

COORDINATES OF SPECIFIED POINT ON SEGMENT KQ2 (IN). IF KQTYPE = 5, THE SECOND CARD WILL CONTAIN THE SPRING CONSTANT K (LB/IN), THE VISCOUS DAMPING CONSTANT D (LB SEC/IN) AND THE REFERENCE LENGTH L (IN) IN PLACE OF RK2.

CARD D.7 IS ALWAYS REQUIRED. SUPPLY BLANK CARD FOR NORMAL 3D MOTION.

CARD D.7 FORMAT (18I4) IF NSEG>18, USE 2 CARDS.

NSYM(J),J=1,NSEG CONTROLS SYMMETRY OPTION OF BODY SEGMENTS
AS FOLLOWS :

NSYM(J) = 0 : NORMAL THREE DIMENSIONAL MOTION FOR BODY
SEGMENT J.

NSYM(J) = J : MOTION OF BODY SEGMENT J WILL BE RESTRICTED
TO THE X-Z PLANE WITH NO LATERAL MOTION,
HENCE IT WILL BE TWO DIMENSIONAL.

NSYM(J) = K : BODY SEGMENTS J AND K ARE TO REMAIN SYMMETRICAL
WITH NO LATERAL MOTION. THE MOTION OF EACH WILL
BE REPLACED WITH THEIR AVERAGE AND RESTRICTED
TO THE LOCAL X-Z PLANE. NSYM(K) MUST EQUAL J.

NSYM(J) = -K : BODY SEGMENTS J AND K ARE TO REMAIN MIRROR
SYMMETRICAL WITH RESPECT TO THE X-Z PLANE.
EQUAL BUT OPPOSITE LATERAL MOTION IS
PERMITTED. NSYM(K) MUST EQUAL -J.

NOTE : IN THE ABOVE SYMMETRY OPTIONS, THE USER MUST TAKE EXTREME
CARE THAT ALL INPUT WILL ALLOW THE SYMMETRY TO EXIST.

IF NSD # 0, NSD D.8 CARDS ARE REQUIRED BY SUBROUTINE SINPOT.

CARDS D.8.A - D.8.J FORMAT (2I3, IIF6.0)
(NSD CARDS)

MSDM(J) SEGMENT IDENTIFICATION NUMBERS (M AND N)
MSDN(J) TO WHICH THE JTH SPRING DAMPER IS ATTACHED.

APSDM(I,J),I=1,3 COORDINATES OF ATTACHMENT POINTS IN LOCAL
APSDN(I,J),I=1,3 SEGMENT REFERENCE ON SEGMENTS M AND N FOR
THE JTH SPRING DAMPER (IN.)

ASD(I,J),I=1,5 COEFFICIENTS OF QUADRATIC FUNCTIONS TO
I=1 : D0 (IN) COMPUTE THE SPRING FORCE (FS) AND THE
I=2 : A1 (LB/IN) VISCOUS FORCE (FD) FOR THE JTH SPRING
I=3 : A2 (LB/IN**2) DAMPER USING THE RELATIONSHIPS
I=4 : B1 (LB SEC/IN)
I=5 : B2 (LB SEC**2/IN**2)

$$FS = (D-D0) * (|A1| + A2 * |D-D0|)$$
$$FD = DV * (B1 + B2 * |DV|)$$

WHERE D AND DV ARE THE DISTANCE AND ITS TIME
DERIVATIVE BETWEEN THE POINTS APSDM AND APSDN.
IF A1 < 0. AND (D-D0) < 0.,
PROGRAM WILL SET FS= 0., I.E. THIS WILL ACT AS
TENSION ELEMENT.

E. SUBROUTINE CINPUT (FUNCTIONS INPUT)

THESE FUNCTIONS ARE REFERRED TO BY NUMBER IN THE NF ARRAYS REQUIRED ON CARDS F.1.B, F.2.B, F.3.B AND F.4.B. THEY ARE USED TO DEFINE THE FORCE DEFLECTION, INERTIAL SPIKE, R (ENERGY ABSORPTION) FACTOR, G (DEFLECTION) FACTOR AND FRICTION COEFFICIENT FUNCTIONS.

EACH FUNCTION MAY BE SUBDIVIDED, IF DESIRED, INTO TWO SEPARATE PARTS, F1 AND F2, WHERE

F1(D) IS DEFINED FOR $0 \leq D \leq |D1|$

F2(D) IS DEFINED FOR $|D1| \leq D \leq |D2|$.

IN ADDITION, EACH PART OF EACH FUNCTION MAY BE DEFINED IN EITHER OF THREE FUNCTIONAL FORMS: CONSTANT VALUE, TABULAR DATA, OR A FIFTH DEGREE POLYNOMIAL. THE EXISTENCE AND FORM OF EACH FUNCTION PART IS DETERMINED BY THE SUPPLIED VALUES OF D0, D1, AND D2 AS FOLLOWS:

F1	F2	D0	D1	D2
—	—	—	—	—
CONSTANT	-	0	0	F1 = D2
TABULAR	-	D0 .GE. 0	D1 .LT. 0	0
POLYNOMIAL	-	D0 .GE. 0	D1 .GT. 0	0
TABULAR	POLYNOMIAL	D0 .GE. 0	D1 .LT. 0	D2 .GT. 0
POLYNOMIAL	TABULAR	D0 .GE. 0	D1 .GT. 0	D2 .LT. 0
POLYNOMIAL	POLYNOMIAL	D0 .GE. 0	D1 .GT. 0	D2 .GT. 0

THE CONSTANT FORM IS APPLICABLE TO F1 ONLY BECAUSE THE ROUTINES ASSUME

IF $D > |D2|$ THEN $F(D) = F(|D2|)$ FOR $D2 \neq 0$ OR

IF $D > |D1|$ THEN $F(D) = F(|D1|)$ FOR $D2 = 0$.

THE CASE OF BOTH F1 AND F2 BEING TABULAR IS UNNECESSARY.

A MAXIMUM OF 50 FUNCTIONS MAY BE SUPPLIED TO THE PROGRAM. THESE FUNCTIONS MAY BE OF THE TYPES DESCRIBED ON EITHER CARDS E.1-E.4, CARDS E.6 OR CARDS E.7.

CARD E.1

I

FORMAT (I4, 4X, 5A4)

THE FUNCTION IDENTIFYING NUMBER. THESE NUMBERS NEED NOT BE SUPPLIED IN NUMERIC ORDER. IF THE SAME NUMBER IS USED MORE THAN ONCE, A WARNING WILL BE PRINTED AND THE LAST ONE SUPPLIED WILL BE USED. THE END OF THE FUNCTION INPUT IS INDICATED BY SUPPLYING A SINGLE CARD WITH I > 50.

KTITLE

A 20 CHARACTER ALPHANUMERIC TITLE DESCRIBING THE FUNCTION.

CARD E.2

FORMAT (5F12.0)

- D0 THE LOWER ABSCISSA VALUE OF THE FIRST PART OF THE FUNCTION, F1. D0 MUST BE NON-NEGATIVE (UNITS ARE IN. EXCEPT FOR THE BELT STRESS-STRAIN FUNCTIONS WHERE THEY ARE IN/IN).
- D1 THE MAGNITUDE OF D1 IS THE UPPER ABSCISSA VALUE OF F1 AND THE LOWER ABSCISSA VALUE OF F2, IF ANY. $D1 < 0$ INDICATES F1 IS TABULAR, $D1 > 0$ INDICATES F1 IS A POLYNOMIAL, AND $D1 = 0$ INDICATES $F1 = D2$, A CONSTANT.
- D2 IF $D1 = 0$, D2 IS THE CONSTANT VALUE OF F1. OTHERWISE, THE MAGNITUDE OF D2 IS THE UPPER ABSCISSA VALUE OF F2. IF $D2 = 0$, F2 IS NOT DEFINED; IF D2 IS NEGATIVE, F2 IS TABULAR; AND IF D2 IS POSITIVE, F2 IS A POLYNOMIAL.
- D3 IF THE FUNCTION IS TO BE USED FOR AN INERTIAL SPIKE, D3 REPRESENTS THE ABSCISSA VALUE FOR WHICH THE INERTIAL SPIKE IS TO BE IGNORED IF UNLOADING OCCURS AFTER DEFLECTION EXCEEDS D3. IF THE FUNCTION IS TO BE USED FOR A COEFFICIENT OF FRICTION, $D3 = (1+U)/2$ WHERE U IS THE COEFFICIENT OF RESTITUTION FOR THE IMPULSE OPTION ($0 < D3 < 1$ OR $-1 < U < +1$). A VALUE OF $D3 = 0$ MEANS THAT THE IMPULSE OPTION WILL NOT BE USED FOR THOSE CONTACTS USING THIS FUNCTION. WHEN THE GLOBALGRAPHIC OPTION IS USED, A FRICTION FUNCTION IS DEFINED AND THE VALUE OF D3 IS USED TO SPECIFY THE IMPULSE. (SEE CARD B.5.)
- D4 IF THE FUNCTION IS TO BE USED AS A FORCE DEFLECTION FUNCTION BY SUBROUTINE PLELP, $D4=RHO$, THE SCALAR THAT DETERMINES THE POINT OF FORCE APPLICATION. SUPPLY ZERO FOR POINT OF MAXIMUM PENETRATION, ONE FOR CENTER OF INTERSECTION ELLIPSE. IF USED AS THE FRICTION FUNCTION FOR A ROLL-SLIDE CONSTRAINT, D4 IS THE COEFFICIENT OF STATIC FRICTION TO BE USED FOR THE ROLL CONSTRAINT.

SUBROUTINE KINPUT (WIND FORCE AND JOINT RESTORING FORCE FUNCTIONS)

CARD E.5 IS ALWAYS REQUIRED AFTER THE END-OF-DATA CARD E.1 (I > 50).
MAY BE BLANK TO DESIGNATE NO FUNCTIONS ON CARDS E.6 OR E.7.

CARD E.5 FORMAT (2I6)

 NWINDF THE NUMBER OF WIND FORCE FUNCTIONS TO BE
 SUPPLIED ON CARDS E.6.A-E.6.N. MAY BE ZERO.

 NJNTF THE NUMBER OF JOINT RESTORING FORCE FUNCTIONS
 TO BE SUPPLIED ON CARDS E.7.A-E.7.N. MAY
 BE BLANK OR ZERO.

NWINDF SETS OF CARDS E.6.A - E.6.N ARE REQUIRED.

CARD E.6.A FORMAT (I4, 4X, 5A4)

 I,KTITLE SAME AS CARD E.1 EXCEPT THAT EACH FUNCTION
 NUMBER (I) MUST BE LESS THAN 51 AND MUST BE
 DISTINCT FROM THOSE SUPPLIED ON CARDS E.1.

CARD E.6.B FORMAT (5F12.0)

 DO,D1,D2,D3,D4 CURRENTLY NOT USED BY PROGRAM.

CARD E.6.C FORMAT (I6)

 NTMPTS THE NUMBER OF TIME POINTS OR CARDS REQUIRED
 TO DEFINE THIS FUNCTION ON CARDS E.6.D-E.6.N.

CARDS E.6.D - E.6.N FORMAT (4F12.0)

 (NTMPTS CARDS)

 T TIME (SEC.) SINCE INITIAL PENETRATION OF
 BOUNDARY PLANE. VALUES SHOULD BE IN ASCENDING
 ORDER WITH FIRST VALUE EQUAL TO ZERO.

 FX,FY,FZ THE X,Y AND Z COMPONENTS OF FORCE PER UNIT
 AREA (LBS./IN.**2) IN INERTIAL REFERENCE
 DUE TO THE WIND BLAST FORCE AT TIME T. THE
 PROGRAM WILL USE LINEAR INTERPOLATION ON T.
 IF LAST VALUE OF T IS EXCEEDED, THE LAST
 VALUES OF FX,FY AND FZ WILL BE USED.

NJNTF (FROM CARD E.5) SETS OF CARDS E.7.A - E.7.N ARE REQUIRED.

CARD E.7.A FORMAT (I4, 4X, 5A4)

I,KTITLE SAME AS CARD E.1 EXCEPT THAT EACH FUNCTION NUMBER (I) MUST BE LESS THAN 51 AND MUST BE DISTINCT FROM THOSE SUPPLIED ON CARDS E.1 OR CARDS E.6.A.

CARD E.7.B FORMAT (5F12.0)

D0,D1,D2,D3,D4 CURRENTLY NOT USED BY PROGRAM.

CARD E.7.C FORMAT (2I6)

NTHETA MAGNITUDE INDICATES THE NUMBER OF COLUMNS IN THE TWO DIMENSIONAL INPUT DATA MATRIX TO BE SUPPLIED ON CARDS E.7.D-E.7.N. THE MINIMUM VALUE IS 2. IF POSITIVE, THE NTHETA ENTRIES IN EACH ROW WILL BE TABULAR DATA FOR EQUALLY SPACED VALUES OF THE JOINT FLEXURE ANGLE (THETA) BETWEEN 0 AND 180 DEGREES. IF NEGATIVE, THE ENTRIES WILL REPRESENT THE COEFFICIENTS OF A (-NTHETA-1) ORDER POLYNOMIAL IN (THETA-THETA0)

NPHI NUMBER OF ROWS OF MATRIX OF DATA TO BE SUPPLIED ON CARDS E.7.D-E.7.N. EACH ROW REPRESENTS EQUALLY SPACED VALUES OF THE JOINT AZIMUTH ANGLE (PHI) BETWEEN -180 AND +180 DEGREES, BUT DOES NOT INCLUDE THE LAST ROW SINCE THE PROGRAM ASSUMES DATA FOR PHI(NPHI+1)=180 ARE THE SAME AS FOR PHI(1)=-180. MINIMUM = 1.

CARDS E.7.D - E.7.N FORMAT (5F12.0)
(NPHI SETS OF CARDS. USE EXTRA CARDS PER SET IF |NTHETA| > 5.)

THETA0 THE VALUE OF THE "DEAD BAND" ZONE FOR THIS VALUE OF PHI (DEGREES). IF THE FLEXURE ANGLE (THETA) IS LESS THAN THETA0, THE JOINT RESTORING FORCE WILL BE ZERO.

F(J),J=2,NTHETA FOR NTHETA POSITIVE, TABULAR VALUES OF THE JOINT RESTORING FORCE FOR FLEXURE ANGLES

$$\text{THETA}(J) = (J-1)*180/(\text{NTHETA}-1) \text{ DEGREES}$$

VALUES OF ZERO SHOULD BE SUPPLIED FOR THETA < THETA0.

FOR NTHETA NEGATIVE, THE COEFFICIENTS OF A POLYNOMIAL IN (THETA-THETA0) OF ORDER ONE LESS THAN THE MAGNITUDE OF NTHETA. F(J) IS THE COEFFICIENT OF (THETA-THETA0)**(J-1) WHERE (THETA-THETA0) IS EXPRESSED IN RADIANS. F(1) IS ASSUMED TO BE ZERO.

F. SUBROUTINE FINPUT (ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS)

IF NPL # 0, F.1 IS REQUIRED.

CARD F.1.A FORMAT (18I4) IF NPL>18, USE 2 CARDS.

MNPL(J),J=1,NPL FOR PLANE J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-PLANE CONTACT IS ALLOWED. NPL IS THE NUMBER OF PLANES FROM CARD D.1. THE VALUE OF ANY MNPL FOR PLANE J MAY BE ZERO AND THE MAXIMUM VALUE IS 5. HOWEVER IF IT IS REQUIRED TO HAVE MORE THAN 5 SEGMENTS CONTACT THE SAME PLANE, SET UP TWO OR MORE IDENTICAL PLANES AND PERMIT A MAXIMUM OF 5 SEGMENTS TO CONTACT EACH PLANE.

FOR EACH PLANE J, MNPL(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.1.B - F.1.N FORMAT (9I4)

NJ THE PLANE NUMBER FOR WHICH CONTACT IS ALLOWED. NJ MUST CORRESPOND TO J ABOVE. THERE MUST BE MNPL(J) CARDS WITH THIS SAME NJ. IF MNPL(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1) THE SEGMENT NUMBER TO WHICH PLANE J IS ATTACHED. IF VEHICLE, SUPPLY NSEG+1, IF GROUND, SUPPLY NSEG+2.

NS(2) THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A FOR WHICH CONTACT WITH THE NJTH PLANE IS ALLOWED.

NS(3) THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2).

- NF(1) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FORCE-DEFLECTION FUNCTION FOR THIS CONTACT. IF NF(1) = 0, A ROLLING - SLIDING CONSTRAINT OPTION WILL BE EXERCISED BY THE PROGRAM FOR THIS CONTACT WHICH DOES NOT REQUIRE NF(2), NF(3) OR NF(4) BUT DOES REQUIRE A FRICTION COEFFICIENT FUNCTION TO BE DEFINED BY NF(5). THE VALUE OF D3 ON CARD E.2 OF THIS FUNCTION SHOULD BE 0.5 (NON-ZERO TO ACTIVATE THE IMPULSE AND TO SET THE NORMAL COMPONENT OF RELATIVE VELOCITY TO ZERO AFTER THE IMPULSE HAS BEEN APPLIED). ALSO THE INITIAL POSITIONS ON CARDS G.2 MUST BE SUCH THAT CONTACT DOES NOT EXIST AT TIME = 0.
- NF(2) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE INERTIAL SPIKE FUNCTION FOR THIS CONTACT. IF NF(2) = 0, NO INERTIAL SPIKE EXISTS.
- NF(3) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE R (ENERGY-ABSORPTION) FACTOR FUNCTION. IF NF(3) = 0, A DEFAULT VALUE OF R = 1 IS ASSUMED.
- NF(4) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE G (DEFLECTION) FACTOR FUNCTION. IF NF(4) = 0, A DEFAULT VALUE OF G = 0 IS ASSUMED.
- NF(5) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FRICTION COEFFICIENT FUNCTION.

IF NBLT # 0, F.2 IS REQUIRED.

CARD F.2.A FORMAT (8I4)

MNBLT(J), J=1, NBLT FOR BELT J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-BELT INTERACTION IS ALLOWED. NBLT IS THE NUMBER OF BELTS FROM CARD D.1. EACH MNBLT MAY HAVE A VALUE OF 0 OR 1 ONLY.

FOR EACH BELT J, MNBLT(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.2.B - F.2.N FORMAT (9I4)

NJ THE BELT NUMBER TO BE CONTACTED, MUST CORRESPOND TO J ABOVE. THERE MUST BE MNBLT(J) CARDS WITH THE SAME NJ. IF MNBLT(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1) THE SEGMENT NUMBER TO WHICH BELT NJ IS ATTACHED. IF VEHICLE, SUPPLY NSEG+1, IF GROUND, SUPPLY NSEG+2.

NS(2) THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) FOR WHICH INTERACTION WITH THE NJTH BELT IS ALLOWED.

NS(3) THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2).

NF(1) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE THE FORCE-DEFLECTION FUNCTION FOR THIS CONTACT. THE ABSCISSA FOR THIS FUNCTION SHOULD BE STRAIN (IN/IN).

NF(I), I=2,4 SAME DEFINITION AS ON CARD F.1.B ABOVE.

NF(5) IF NON-ZERO, FULL BELT FRICTION IS ASSUMED, I.E., FORCES ARE COMPUTED FOR EACH HALF OF THE BELT SEPARATELY. IF ZERO, ZERO BELT FRICTION IS ASSUMED, I.E., BELT TENSION IS THE SAME AT BOTH BELT ANCHOR POINTS.

A BLANK F.3.A CARD IS REQUIRED FOR NO SEGMENT-SEGMENT CONTACTS.

CARD F.3.A FORMAT (18I4) IF NSEG>18, USE TWO CARDS.

MNSEG(J),J=1,NSEG FOR SEGMENT J, THE NUMBER OF SEGMENTS FOR WHICH SEGMENT-SEGMENT CONTACT IS ALLOWED. NSEG IS THE NUMBER OF SEGMENTS FROM CARD B.1. EACH SEGMENT CONTACT, A VERSUS B, MAY BE INPUTTED EITHER WAY EXCEPT WHERE AN INTERIOR CONTACT IS DESIRED (SEE NS(3)). ANY OR ALL VALUES OF MNSEG MAY BE ZERO. THE MAXIMUM VALUE FOR EACH MNSEG IS 5.

FOR EACH SEGMENT J, MNSEG(J) CARDS OF THE FOLLOWING MUST BE SUPPLIED.

CARDS F.3.B - F.3.N FORMAT (9I4)

NJ THE SEGMENT NUMBER TO BE CONTACTED, MUST CORRESPOND TO J ABOVE. THERE MUST BE MNSEG(J) CARDS WITH THIS SAME NJ. IF MNSEG(J) = 0, NO NJ = J SHOULD BE PRESENT.

NS(1) THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH SEGMENT NJ.

NS(2) THE SEGMENT NUMBER (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) FOR WHICH CONTACT WITH THE NJTH SEGMENT IS ALLOWED.

NS(3) THE NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH THE SEGMENT NS(2). IF NEGATIVE, AN INTERIOR CONTACT WILL BE ASSUMED WITH ELLIPSOID NS(1) INSIDE NS(3).

NF(I),I=1,5 SAME DEFINITIONS AS ON CARD F.1.B ABOVE.

IF NJNT > 0, F.4.A IS REQUIRED.
SUPPLY IGLOB=I FOR GLOBALGRAPHIC OPTION, OTHERWISE SUPPLY 0 OR BLANK

CARD F.4.A FORMAT (18I4) IF NJNT>18, USE TWO CARDS.

IGLOB(J),J=1,NJNT FOR EACH JOINT J, SUPPLY I FOR IGLOB(J) IF
IPIN(J) IS +3 OR -3 ON CARDS B.3.A - B.3.J;
OTHERWISE SUPPLY ZERO OR BLANK. ONE CARD
F.4.J MUST BE SUPPLIED BELOW FOR EACH J FOR
WHICH IGLOB(J) =I.

CARDS F.4.B - F.4.J FORMAT (9I4)

NJ THE IDENTIFICATION NUMBER FOR A GLOBALGRAPHIC
JOINT, MUST CORRESPOND TO J ABOVE AND CARDS
MUST BE SUPPLIED IN ASCENDING ORDER ON NJ.

NS(I),I=1,3 CURRENTLY NOT USED BY PROGRAM.

NF(1) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE
THE TORQUE-DEFLECTION FOR THIS GLOBALGRAPHIC
JOINT. THE ORDINATE FOR THIS FUNCTION SHOULD
BE TORQUE (IN. LB.) AND THE ABSCISSA IS THE
ANGULAR DEFLECTION (RADIAN) INTO THE STOP.

NF(2) THE FUNCTION NUMBER FROM CARD E.1 TO DEFINE
THE HERRON FORMULAS FOR T (JOINT STOP ANGLE
IN RADIAN) AND ITS DERIVATIVE TP WITH RES-
PECT TO PHI BOTH AS FUNCTIONS OF PHI (THE
JOINT ANGLE FROM THE REFERENCE AXIS IN RAD-
IAN). NORMALLY THEY WILL BE COMPUTED BY

$$T = P1 + SP*P2$$
$$TP = P1' + CP*P2 + SP*P2'$$

WHERE P1,P2 ARE THE 5TH DEGREE POLYNOMIAL
EVALUATIONS OF COS(PHI) USING THE
TWO POLYNOMIALS F1 AND F2 OBTAINED BY
SETTING BOTH D1,D2 > 0 ON CARD E.2;

P1',P2' ARE THEIR DERIVATIVES WITH
RESPECT TO PHI;

AND CP,SP ARE COS(PHI) AND SIN(PHI).

IF D1,D2 ARE NOT BOTH POSITIVE, T AND TP
WILL BE EVALUATED AS FUNCTIONS OF PHI IN
RADIAN (0 < PHI < 2*PI) AS SPECIFIED ON
CARDS E.1 - E.4 FOR FUNCTION NF(2).

SAME DEFINITIONS AS ON CARD F.I.B ABOVE

IF NJNT > 0, CARD F.5.A IS ALWAYS REQUIRED BUT MAY BE BLANK.

CARD F.5.A FORMAT (I8I4) USE TWO CARDS IF NJNT > I8.

JOINTF(J),J=I,NJNT FOR EACH JOINT (J), THE FUNCTION IDENTIFICATION NUMBER AS SUPPLIED ON CARDS E.7.A TO BE USED BY SUBROUTINE VISPR TO COMPUTE THE JOINT RESTORING FORCE BY FUNCTION FINTERP. IF ZERO, THE VALUES OF SPRING(1,3*J-2) AS SUPPLIED ON CARDS B.4.A WILL BE USED USING FUNCTION EJOINT.

IF NBAG # 0, NBAG CARDS OF THE FOLLOWING MUST BE SUPPLIED. SINCE THE AIR BAG ROUTINES DO NOT USE THE FORCE-DEFLECTION FUNCTIONS, THIS INPUT HAS DIFFERENT FORMATS THAN THE ABOVE ALLOWED CONTACTS.

CARDS F.6.A - F.6.N FORMAT (2I4, 20I2)

K THE AIR BAG NUMBER CORRESPONDING TO THE INDEX J UNDER CARDS D.4 ABOVE. K MUST BE IN NUMERIC ORDER K = 1 TO NBAG, WHERE NBAG IS THE NUMBER OF AIR BAGS DEFINED ON CARD D.I.

NK THE NUMBER OF SEGMENTS ALLOWED TO CONTACT THE KTH AIR BAG. THE MAXIMUM VALUE IS 10. IF NK = 0, THE REMAINDER OF THE CARD IS BLANK.

MBAG(2,I,K),
MBAG(3,I,K),I=1,NK THE SEGMENT NUMBERS (DETERMINED BY THE CARD NUMBER I UNDER CARD B.2.A) EACH FOLLOWED BY THE NUMBER OF THE ASSOCIATED CONTACT ELLIPSOID FOR WHICH CONTACT FORCES WITH THE KTH AIR BAG WILL BE COMPUTED.

CARD F.7.A IS ALWAYS REQUIRED. INSERT A BLANK CARD IF NO WIND FORCE CALCULATIONS ARE TO BE PERFORMED.

CARD F.7.A FORMAT (I8I4) USE TWO CARDS IF NSEG > 18.

MWSEG(1,J),J=1,NSEG FOR EACH SEGMENT J, SUPPLY ZERO IF NO WIND FORCE CALCULATIONS ARE TO BE PERFORMED. OTHERWISE, SUPPLY A VALUE OF ONE TO INDICATE WIND FORCES ARE TO BE PERFORMED.

SUPPLY CARD F.7.B FOR EACH SEGMENT (J) WHERE MWSEG(1,J) = 1.

CARD F.7.B FORMAT (5I4)

JJ THE SEGMENT IDENTIFICATION NUMBER FROM CARDS B.2.A FOR WHICH WIND FORCE CALCULATIONS ARE TO BE PERFORMED. MUST CORRESPOND TO J FROM CARD F.7.A AND BE SUPPLIED IN ASCENDING ORDER.

MWSEG(2,J) THE NUMBER OF THE CONTACT ELLIPSOID TO BE ASSOCIATED WITH SEGMENT NUMBER JJ.

MWSEG(3,J) THE SEGMENT IDENTIFICATION NUMBER (NSEG+1 FOR THE VEHICLE, NSEG+2 FOR THE GROUND) ASSOCIATED WITH PLANE NUMBER MWSEG (4,J).

MWSEG(4,J) THE PLANE IDENTIFICATION NUMBER FROM CARD D.2.A THROUGH WHICH IF SEGMENT J PASSES, WIND FORCE CALCULATIONS WILL BE PERFORMED.

MWSEG(5,J) THE FUNCTION NUMBER FROM CARD E.6.A FOR THE WIND FORCE FUNCTION TO BE USED.

F.8 SUBROUTINE HINPUT - CARD INPUT FOR HARNESS-BELT SYSTEMS.

CARD F.8.A IS ALWAYS REQUIRED. INSERT BLANK CARD IF NO HARNESS-BELT SYSTEMS ARE DESIRED.

CARD F.8.A FORMAT (6I4)

NHRNSS NUMBER OF HARNESS-BELT SYSTEMS TO BE
 SUPPLIED ON CARDS F.8.B-F.8.D. MAY BE ZERO
 OR BLANK. MAXIMUM VALUE = 5.

NBLTPH(I), NUMBER OF INDIVIDUAL BELTS FOR EACH HARNESS
 I=I,NHRNSS NO. I. MAY BE ZERO OR BLANK. MAXIMUM VALUE
 OF SUM OF ALL NBLTPH IS 20.

CARD F.8.A IS FOLLOWED BY NHRNSS SETS OF CARDS F.8.B - F.8.D.

CARD F.8.B FORMAT (18I4) USE TWO CARDS IF NBLTPH(I)>18.

NPTSPB(J), THE NUMBER OF REFERENCE POINTS INCLUDING
 J=I,NBLTPH(I) ANCHOR POINTS FOR BELT NO. J OF HARNESS
 NO. I. MAY BE ZERO OR BLANK. THE MAXIMUM
 VALUE OF THE SUM OF ALL NPTSPB FOR ALL
 HARNESS-BELT SYSTEMS IS 100.

EACH CARD F.8.B IS FOLLOWED BY NBLTPH(I) SETS OF CARDS F.8.C - F.8.D.

CARD F.8.C FORMAT (5I4, F12.6)

NFBLT(L, J), L=1,5 THE IDENTIFICATION NUMBERS OF THE 5 FUNCTIONS
 TO BE USED FOR BELT NO. J. THESE CORRESPOND
 TO I AS SUPPLIED ON CARDS E.1 OF THE FUNCTION
 DEFINITIONS. THESE FUNCTIONS ARE IDENTICAL TO
 THOSE DEFINED BY NF(I) - NF(5) ON CARDS F.2.B
 EXCEPT THAT THE COEFFICIENT OF FRICTION AS
 SPECIFIED BY NF(5) IS NOT CURRENTLY USED.

XLONG(J) BELT SLACK (IN). THE SLACK, WHEN ADDED TO
 THE INITIAL GEOMETRIC LENGTH, RESULTS IN
 THE INITIAL BELT LENGTH. IF DESIRED, THE
 INITIAL BELT LENGTH MAY BE SUPPLIED AS A
 NEGATIVE NUMBER AND THE PROGRAM WILL
 COMPUTE THE SLACK.

EACH CARD F.8.C IS FOLLOWED BY NPTSP8(J) CARDS F.8.D SPECIFYING THE REFERENCE POINTS (K) TO BE USED FOR BELT NO. J OF HARNESS NO. I.

CARD F.8.D

FORMAT (2I6, 3F12.6)

IBAR(1,K)

THE IDENTIFICATION NUMBER OF THE SEGMENT ASSOCIATED WITH REFERENCE POINT K.

IBAR(2,K)

THE IDENTIFICATION NUMBER OF THE CONTACT ELLIPSOID ASSOCIATED WITH POINT K. IF ZERO, PROGRAM WILL ASSUME BELT IS RIGIDLY ATTACHED TO THAT POINT (AS FOR ANCHOR POINTS ATTACHED TO THE VEHICLE).

BAR(L,K),L=1,3

THE X,Y AND Z COORDINATES OF REFERENCE POINT K IN THE LOCAL COORDINATE SYSTEM OF SEGMENT NO. IBAR(1,K). THE PROGRAM WILL ASSUME THAT BELT J WILL RUN THROUGH THE POINTS IN THE ORDER THEY ARE SUPPLIED. HOWEVER IF A CONTACT ELLIPSOID IS SPECIFIED BY IBAR(2,K) AND THE THE FORCES ARE SUCH AS TO PULL THE BELT AWAY FROM THE SURFACE, THIS POINT WILL BE IGNORED THAT TIME POINT.

G. SUBROUTINE INITIAL

CARD G.I FORMAT (3F10.0, 5I4)

 ZPLT(I),I=I,3 THE X, Y, AND Z PLOT COORDINATES
 (FOR SUBROUTINE PRIPLT) OF THE
 ORIGIN OF THE VEHICLE REFERENCE
 SYSTEM. 0 < X < 6I
 0 < Y < 6I
 0 < Z < I2I

 I1,J1,I2,J2 NOT USED BY THE CURRENT PROGRAM.

 I3 IF ZERO, SEGMENT AND ANGULAR VELOCITIES ARE
 NOT SUPPLIED ON THE FOLLOWING CARDS BUT ARE
 SET EQUAL TO THE INITIAL VEHICLE VELOCITY.
 IF I3 # 0, SEGLV AND WMGDEG MUST BE SUPPLIED.

ONE G.2 CARD MUST BE SUPPLIED FOR EACH REFERENCE SEGMENT (I.E.,
SEGMENT NO. 1 AND FOR EACH SEGMENT J+I WHERE JNT(J) = 0 ON CARDS
B.3) IN ASCENDING SEGMENT NUMBER SEQUENCE.

CARDS G.2.A - G.2.M FORMAT (6F10.0)

 SEGLP(I,J),I=I,3 THE INITIAL X, Y, AND Z COORDINATES OF THE
 JTH BODY SEGMENT IN INERTIAL REFERENCE (IN).

 SEGLV(I,J),I=I,3 THE INITIAL X, Y, AND Z COMPONENTS OF VELOCITY
 OF THE JTH BODY SEGMENT IN INERTIAL REFER-
 ENCE (IN/SEC). THESE FIELDS MAY BE LEFT BLANK
 IF I3 = 0 ON CARD G.1 IN WHICH CASE THE
 INITIAL VELOCITY OF THE VEHICLE WILL BE USED.

CARDS G.3.A - G.3.N FORMAT (6F10.0)
 (NSEG CARDS)

 YPR(I,J),I=I,3 THE INITIAL YAW, PITCH AND ROLL ANGLES OF
 THE JTH BODY SEGMENT (DEGREES).

NOTE: THE DIRECTION COSINE MATRICES OF THE BODY SEGMENTS ARE INITIALLY
COMPUTED BY ASSUMING THE ORDER OF THE ROTATING ANGLES IS REVERSED,
I.E., ROLL,PITCH,YAW.
(ROLL ABOUT X, PITCH ABOUT Y, AND YAW ABOUT Z.)

 WMGDEG(I,J),I=I,3 THE INITIAL COMPONENTS OF ANGULAR VELOCITY
 ABOUT THE LOCAL X,Y AND Z AXES OF THE JTH
 BODY SEGMENT (DEG/SEC). IF I3 = 0 ON CARD
 G.1, THE INITIAL ANGULAR VELOCITY OF THE
 VEHICLE WILL BE CONVERTED TO THE SEGMENT
 REFERENCE AND WILL BE USED.

H. SUBROUTINE HEDING

THIS SUBROUTINE PROVIDES INPUT TO CONTROL THE DESIRED TIME HISTORY OUTPUT OF SELECTED SEGMENT LINEAR AND ANGULAR ACCELERATIONS, VELOCITIES, AND DISPLACEMENTS, AND JOINT PARAMETERS.

H.1 SEGMENT LINEAR ACCELERATIONS (K = 1)

CARD H.1.A FORMAT (2I6, 3F12.6)

 NSG(K) THE NUMBER OF SELECTED POINTS ON
 THE VARIOUS BODY SEGMENTS FOR
 WHICH TIME HISTORIES ARE DESIRED.
 THE MAXIMUM VALUE FOR NSG(K) IS 20.
 IF NSG(K) IS 0, INSERT 2 BLANK CARDS.
 IF NSG(K) IS 1, A SINGLE BLANK CARD
 SHOULD FOLLOW CARD H.1.K.

 MSG(1,K) THE SEGMENT NUMBER AS DETERMINED
 BY INDEX I ON CARDS
 B.2.A - B.2.N OF THE FIRST POINT.

 XSG(I,1,K), I=1,3 THE X, Y, AND Z COORDINATES IN
 SEGMENT REFERENCE OF THE FIRST
 POINT (INCHES).

FOLLOWED BY NSG(K)-1 CARDS OF THE FOLLOWING (J = 2, NSG(K))

CARDS H.1.B - H.1.N FORMAT (I12, 3F12.6)

 MSG(J,K) SAME AS ABOVE BUT FOR THE JTH POINT.

 XSG(I,J,K), I=1,3 SAME AS ABOVE BUT FOR THE JTH POINT.

H.2 SEGMENT LINEAR VELOCITIES (K = 2)

CARDS H.2.A - H.2.N FORMAT (2I6, 3F12.6/(I12, 3F12.6))

 DESCRIPTION SAME AS FOR H.1.

H.3 SEGMENT LINEAR DISPLACEMENTS (K = 3)

CARDS H.3.A - H.3.N FORMAT (2I6, 3F12.6/(I12, 3F12.6))

 DESCRIPTION SAME AS FOR H.1.

H.4 SEGMENT ANGULAR ACCELERATIONS (K = 4)

CARD H.4

FORMAT (12I6/112, 3I6)

NSG(K)

THE NUMBER OF SELECTED BODY SEGMENTS FOR WHICH TIME HISTORIES ARE DESIRED. INSERT BLANK CARD IF NONE ARE DESIRED (NSEG MAXIMUM).

MSG(J,K),J=1,KSG
WHERE KSG=NSG(K)

THE SEGMENT NUMBERS AS DETERMINED BY INDEX I ON CARDS B.2.A - B.2.N. IF NSG(K) > 11, USE THE SECOND CARD, LEAVING THE FIRST FIELD OF 6 COLUMNS BLANK. IF NSG(K) = 11, A SECOND CARD, COMPLETELY BLANK, SHOULD FOLLOW THIS CARD.

H.5 SEGMENT ANGULAR VELOCITIES (K = 5)

CARD H.5

FORMAT (12I6/112, 3I6)

DESCRIPTION SAME AS FOR H.4.

H.6 SEGMENT ANGULAR DISPLACEMENTS (K = 6)

CARD H.6

FORMAT (12I6/112, 3I6)

DESCRIPTION SAME AS FOR H.4.

H.7 JOINT PARAMETERS (K = 7)

CARD H.7

FORMAT (12I6/112, 2I6)

NSG(K)

THE NUMBER OF SELECTED JOINTS FOR WHICH TIME HISTORIES ARE DESIRED. INSERT BLANK CARD IF NONE ARE DESIRED (NJNT MAXIMUM).

MSG(J,K),J=1,KSG
WHERE KSG=NSG(K)

THE JOINT NUMBERS AS DETERMINED BY INDEX J ON CARDS B.3.A - B.3.J. IF NSG(K) > 11, USE A SECOND CARD LEAVING THE FIRST FIELD OF 6 COLUMNS BLANK. IF NSG(K) = 11, A SECOND CARD, COMPLETELY BLANK, SHOULD FOLLOW THIS CARD.

APPENDIX B

The listing of 21 subroutines that follow represent the changes or additions that were made to the computer program contained in Volume IV, Programmer's Manual of Calspan Report No. ZQ-5180-L-1, "An Improved Three Dimensional Computer Simulation of Motor Vehicle Crash Victims," July 1974 to fulfill the requirements of Wright Patterson AFB Contract No. F33615-75-C-5002. Any subroutine not contained herein remains unchanged from the above mentioned report.

The following is a list of the included subroutines and a summary of the changes that have been made to them.

1. SUBROUTINE CINPUT: Statement numbers have been renumbered for readability and previous version has been subdivided into new SUBROUTINE CINPUT and SUBROUTINE FINPUT. Calls to new subroutines KINPUT and HINPUT have been added.
2. SUBROUTINE CONTCT: Card No.'s 140-160 and 780-1050 have been added to control the calling of SUBROUTINE WINDY and SUBROUTINE HBELT.
3. SUBROUTINE DINT: Card No.'s 530 and 2150-2170 have been modified to simplify program logic and are equivalent to previous version.
4. SUBROUTINE ELTIME: Card No.'s 210 and 220 have been modified to include SUBROUTINE WINDY and SUBROUTINE HBELT for N=35 and 36.
5. FUNCTION EVALFD: Extensive modifications have been made to accommodate abscissas that exceed the range of tabular function definitions.
6. SUBROUTINE FINPUT: New subroutine that is actually the second half of previous SUBROUTINE CINPUT that controlled the input specifying allowed contacts between body segments with vehicle panels, belts, airbags and other body segments. New code has been inserted at card no.'s 2100-2280 for new input card F.5 defining joint functions to be used. Old input cards F.5 have been renamed F.6 and new code has been inserted at card no.'s 2540-2800 for input cards F.7 controlling the new wind force calculations.

APPENDIX B (Continued)

7. SUBROUTINE FLXSEG: Card No.'s 130 and 140 have been interchanged to properly control the call to SUBROUTINE ELTIME.
8. FUNCTION FNTERP: New subroutine that computes the restoring torque of a joint by double linear interpolation on the flexure angle (θ) and azimuth angle (ϕ).
9. SUBROUTINE HBELT: New subroutine that computes the forces and torques of individual belt sections of the harness-belt systems.
10. SUBROUTINE HINPUT: New subroutine that controls the input of cards F.8.A-F.8.D containing the setup and control of the harness-belt system.
11. SUBROUTINE IMPULS: Card No.'s 1810 and 1820 have been modified to properly control call to SUBROUTINE ELTIME.
12. SUBROUTINE KINPUT: New subroutine that controls the input of cards E.5, E.6 and E.7 containing the definitions of the wind force and joint restoring force functions.
13. SUBROUTINE OUTPUT: Card No.'s 1280-1300 have been modified to print the joint angles in degrees for the new joint functions.
14. SUBROUTINE PLELP: Comments in card no.'s 50 and 60 have been corrected.
15. SUBROUTINE RSTART: Card No.'s 630-640, 1480-1580, 1630-1640, 1770, 1890, 1970, 2060, 2150, 2170-2180, 2930 and 4410-4620 have been modified or added to insert JOINTF in COMMON/DESCRP/ and to include COMMON/HARNESS/ and COMMON/KALEPS/.
16. SUBROUTINE SEARCH: Several additions and modifications have been made to accommodate the changes made to SUBROUTINE RSTART.

APPENDIX B (Continued)

17. SUBROUTINE UPDATE: Card No.'s 360-370, 1020-1210 have been added to call SUBROUTINE UPDFDC for each belt of harness-belt systems and card no. 2400 has been modified to set initial state of rolling-sliding constraint.
18. SUBROUTINE VEHPOS: Card No.'s 410-440 and 1100-1110 have been modified to extrapolate beyond last entry in vehicle position input tables.
19. SUBROUTINE VINPUT: Card No.'s 560, 600 and 750-810 have been modified to permit input of negative VIPS on input card C.2 and delete the restriction that the last acceleration on card C.3 be zero.
20. SUBROUTINE VISPR: Card No.'s 190, 310, 560-570, 600-870, 930, 1090-1100, 1190-1230, 1350-1410, 1450, 1470-1480, 1500, 1560, 1580, 1650-1670, 1800, 1830-1840, 1990-2000 and 2020 have been added or modified to include the necessary logic for the new joint functions.
21. SUBROUTINE WINDY: New subroutine that computes the forces and torques of a wind blast acting on specified body segments.

	SUBROUTINE CINPUT	CINPC010
C		REV 12 12/18/74CINPG020
C	CONTROLS THE CARD INPUT OF THE FORCE-DEFLECTION, INERTIAL SPIKE,	CINPG030
C	R FACTOR, G FACTOR AND FRICTION COEFFICIENT FUNCTION DEFINITIONS	CINPG040
C		CINPG050
	IMPLICIT REAL*B(A-H,O-Z)	CINPG060
	COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	CINPG070
	COMMON/TEMPVS/JTITL(5,51),NF(5),NS(3),KTITL(31)	CINPG080
	REAL JTITL,KTITL	CINPG090
	IS = 0	CINPG100
	DO 10 I = 1,50	CINPG110
10	NTI(I) = 0	CINPG120
	J1 = 1	CINPG130
C		CINPG140
C	INPUT CARD E.1 - FUNCTION NO. AND TITLE, IF NO. > 50 SKIP OUT.	CINPG150
C		CINPG160
11	READ (5,12) I,(KTITL(J),J = 1,5)	CINPG170
12	FORMAT (I4,4X,5A4)	CINPG180
	IF (I.GT.50) GO TO 30	CINPG190
	DO 13 J = 1,5	CINPG200
13	JTITL(J,I) = KTITL(J)	CINPG210
C		CINPG220
C	HAS FUNCTION NO. BEEN ALREADY USED?	CINPG230
C		CINPG240
	IF (NTI(I).NE.0) WRITE(6,14) I	CINPG250
14	FORMAT('0 FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BE	CINPG260
	*REPLACED BY NEXT FUNCTION')	CINPG270
	NTI(I) = J1	CINPG280
	J2 = J1+4	CINPG290
C		CINPG300
C	INPUT CARD E.2	CINPG310
C		CINPG320
	READ (5,15) (TAB(J),J = J1,J2)	CINPG330
15	FORMAT (6F12.0)	CINPG340
	IS = 1-IS	CINPG350
	IF (IS.EQ.0) WRITE (6,16)	CINPG360
16	FORMAT(/////)	CINPG370
	WRITE (6,17) IS,I,(JTITL(J,I),J=1,5),I,NTI(I),(TAB(J),J=J1,J2)	CINPG380
17	FORMAT(I1,'FUNCTION NO.',I4,4X,5A4,20X,'NTI(' ,I2,') =',I5,45X	CINPG390
	* 'CARDS E'//10X,'D0',13X,'D1',13X,'D2',13X,'D3',13X,'D4'/5F15.4//)	CINPG400
	DO = TAB(J1)	CINPG410
	D1 = TAB(J1+1)	CINPG420
	D2 = TAB(J1+2)	CINPG430
	J1 = J2+1	CINPG440
	IF (D1) 22,18,20	CINPG450
C		CINPG460
C	FUNCTION IS CONSTANT D2 FOR ALL D.	CINPG470
C		CINPG480
18	WRITE (6,19) D2	CINPG490
19	FORMAT(7X,'FUNCTION IS CONSTANT',F12.6)	CINPG500

C	GO TO 11	CINP0510
C	5TH ORDER POLYNOMIAL ... 1ST FUNCTION	CINP0520
C	INPUT CARD E.3	CINP0530
C		CINP0540
C		CINP0550
	20 J2 = J1+5	CINP0560
	READ(5,15)(TAB(J),J = J1,J2)	CINP0570
	WRITE(6,21) (TAB(J),J = J1,J2)	CINP0580
	21 FORMAT(7X,'FIRST PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINP0590
	* 8X,'A0',13X,'A1',13X,'A2',13X,'A3',13X,'A4',13X,'A5',13X/C	CINP0600
	* 6F15.6//)	CINP0610
	J1 = J2+1	CINP0620
	GO TO 25	CINP0630
C	TABLE LOAD ... 1ST FUNCTION	CINP0640
C	INPUT CARDS E.4.A-E.4.N	CINP0650
C		CINP0660
C		CINP0670
	22 READ(5,23) NPI	CINP0680
	23 FORMAT (12I6)	CINP0690
	TAB(J1) = NPI	CINP0700
	J1 = J1+1	CINP0710
	J2 = J1+2*NPI-1	CINP0720
	READ(5,15)(TAB(J),J = J1,J2)	CINP0730
	WRITE (6,24) NPI, (TAB(J) ,J = J1, J2)	CINP0740
	24 FORMAT(7X,'FIRST PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINP0750
	* 8X,'D',16X,'F(D)' /(F15.6,F15.4))	CINP0760
	J1 = J2+1	CINP0770
C		CINP0780
C	CHECK FOR SECOND FUNCTION	CINP0790
C		CINP0800
	25 IF(D2) 28,11,26	CINP0810
C		CINP0820
C	SECOND FUNCTION ... 5TH ORDER POLYNOMIAL	CINP0830
C	INPUT CARD E.3	CINP0840
C		CINP0850
	26 J2 = J1+5	CINP0860
	READ(5,15)(TAB(J),J = J1,J2)	CINP0870
	WRITE (6,27) (TAB(J),J = J1,J2)	CINP0880
	27 FORMAT(7X,'SECOND PART OF FUNCTION - 5TH DEGREE POLYNOMIAL'//	CINP0890
	* 8X,'B0',13X,'B1',13X,'B2',13X,'B3',13X,'B4',13X,'B5',13X/C	CINP0900
	* 6F15.6//)	CINP0910
	J1 = J2+1	CINP0920
	GO TO 11	CINP0930
C		CINP0940
C	SECOND FUNCTION ... TABLE LOAD	CINP0950
C	INPUT CARDS E.4.A-E.4.N	CINP0960
C		CINP0970
	28 READ(5,23) NPI	CINP0980
	TAB(J1) = NPI	CINP0990
	J1 = J1+1	CINP1000

J2 = J1+2*NPI-1	CINP1010
READ(5,15)(TAB(J),J = J1,J2)	CINP1020
WRITE(6,29) NPI, (TAB(J), J = J1,J2)	CINP1030
29 FORMAT(7X,'SECOND PART OF FUNCTION - ',I4,' TABULAR POINTS'//	CINP1040
* 8X,'D',16X,'F(D)' / (F15.6,F15.4))	CINP1050
J1 = J2+1	CINP1060
GO TO 11	CINP1070
30 MXTB1 = J1-1	CINP1080
CALL KINPUT	CINP1090
CALL FINPUT	CINP1100
CALL HINPUT	CINP1110
RETURN	CINP1120
END	CINP1130

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SUBROUTINE CONTACT                                CONT0010
C                                                    REV 12 12/19/74CONT0020
C CONTROLS THE CALLING OF SUBROUTINES REQUIRED TO COMPUTE THOSE CONT0030
C EXTERNAL FORCES AND TORQUES ACTING ON THE BODY SEGMENTS. CONT0040
C                                                    CONT0050
IMPLICIT REAL*8 (A-H,O-Z)                        CONT0060
COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40) CONT0070
COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6), CONT0080
*           MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6), CONT0090
*           NTPL(5,20),NTBLT(5,8),NTSEG(5,22) CONT0100
COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20), CONT0110
*           NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21) CONT0120
COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NT1(50),NTAB(500),TAB(2000) CONT0130
COMMON/KALEPS/WTIME(30),IWIND(30),MWSEG(5,22) CONT0140
COMMON/HRNESS/ BAR(6,100) , XLONG(20), IBAR(2,100), NTHRNS(20), CONT0150
*           NHRNSS, NBLTPH(5), NFBLT(5,20), NPTSPB(20) CONT0160
CALL ELTIME(1,12)                                CONT0170
NPSF = 0                                           CONT0180
NBSF = 0                                           CONT0190
NSSF = 0                                           CONT0200
IF (NPL.LE.0) GO TO 21                            CONT0210
C                                                    CONT0220
C CALL PLELP ROUTINE FOR EACH ALLOWED PLANE-SEGMENT CONTACT. CONT0230
C                                                    CONT0240
DO 20 J=1,NPL                                     CONT0250
IF (MNPL(J).EQ.0) GO TO 20                        CONT0260
KPL = MNPL(J)                                     CONT0270
DO 19 I=1,KPL                                     CONT0280
NPSF = NPSF+1                                     CONT0290
M1 = MPL(1,1,J)                                   CONT0300
M2 = MPL(2,1,J)                                   CONT0310
M3 = MPL(3,I,J)                                   CONT0320
NT = NTPL(I,J)                                    CONT0330
JT = NTAB(NT)                                     CONT0340
TAB(JT) = 0.0                                     CONT0350
19 CALL PLELP(M2,M3,M1,J,NT)                       CONT0360
20 CONTINUE                                       CONT0370
21 IF(NBLT.LE.0) GO TO 41                          CONT0380
C                                                    CONT0390
C CALL BELTRT ROUTINE FOR EACH ALLOWED BELT-SEGMENT CONTACT. CONT0400
C                                                    CONT0410
DO 30 J=1,NBLT                                    CONT0420
IF (MNBLT(J).EQ.0) GO TO 30                       CONT0430
KBLT = MNBLT(J)                                   CONT0440
DO 29 I=1,KBLT                                    CONT0450
NBSF = NBSF+1                                     CONT0460
M1 = MBLT(1,I,J)                                  CONT0470
M2 = MBLT(2,1,J)                                  CONT0480
M3 = MBLT(3,I,J)                                  CONT0490
NT = NTBLT(1,J)                                   CONT0500

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	JT = NTAB(NT)	CONT0510
	TAB(JT) = 0.0	CONT0520
	NF = NTAB(NT+5)	CONT0530
	IF (NF.NE.0) JT = NTAB(NT+6)	CONT0540
	IF (NF.NE.0) TAB(JT) = 0.0	CONT0550
	29 CALL BELTRT(M2,M3,M1,J,NT)	CONT0560
	30 CONTINUE	CONT0570
C		CONT0580
C	CALL SEGSEG ROUTINE FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	CONT0590
C		CONT0600
	41 DO 50 J=1,NSEG	CONT0610
	IF (MNSEG(J).EQ.0) GO TO 50	CONT0620
	KSEG = MNSEG(J)	CONT0630
	DO 49 I=1,KSEG	CONT0640
	NSSF = NSSF+1	CONT0650
	M1 = MSEG(1,I,J)	CONT0660
	M2 = MSEG(2,I,J)	CONT0670
	M3 = MSEG(3,I,J)	CONT0680
	NT = NTSEG(I,J)	CONT0690
	JT = NTAB(NT)	CONT0700
	TAB(JT) = 0.0	CONT0710
	49 CALL SEGSEG(J,M1,M2,M3,NT)	CONT0720
	50 CONTINUE	CONT0730
C		CONT0740
C	CALL AIRBAG ROUTINE FOR ALLOWED BAG-SEGMENT CONTACTS, IF ANY.	CONT0750
C		CONT0760
	IF (NBAG.NE.0) CALL AIRBAG	CONT0770
C		CONT0780
C	CALL WINDY ROUTINE FOR WIND FORCES ON EACH SEGMENT.	CONT0790
C		CONT0800
	DO 60 J=1,NSEG	CONT0810
	IF (MWSEG(1,J).EQ.0) GO TO 60	CONT0820
	M1 = MWSEG(2,J)	CONT0830
	M2 = MWSEG(3,J)	CONT0840
	M3 = MWSEG(4,J)	CONT0850
	NT = MWSEG(5,J)	CONT0860
	CALL WINDY (J,M1,M2,M3,NT)	CONT0870
	60 CONTINUE	CONT0880
C		CONT0890
C	CALL HBELT ROUTINE FOR EACH HARNESS-BELT SYSTEM.	CONT0900
C		CONT0910
	IF (NHRNSS.LE.0) GO TO 99	CONT0920
	J1 = 1	CONT0930
	K1 = 1	CONT0940
	DO 70 I=1,NHRNSS	CONT0950
	IF (NBLTPH(I).LE.0) GO TO 70	CONT0960
	J2 = J1 + NBLTPH(I) - 1	CONT0970
	DO 69 J=J1,J2	CONT0980
	IF (NPTSPB(J).LE.0) GO TO 69	CONT0990
	K2 = K1 + NPTSPB(J) - 1	CONT1000

```
CALL HBELT(NPTSPB(J),IBAR(1,K1),BAR(1,K1),NTHRNS(J),XLONG(J))    CONT1010
K1 = K2+1                                                            CONT1020
69 CONTINUE                                                         CONT1030
J1 = J2+1                                                            CONT1040
70 CONTINUE                                                         CONT1050
99 CALL ELTIME(2,12)                                               CONT1060
RETURN                                                             CONT1070
END                                                                  CONT1080
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SUBROUTINE DINT(IN,N,DTPR,HO,HMAX,HMIN,/T/,X,DER,NOINT)          OINT0010
                                                                    REV 12 10/25/74D OINT0020
EXECUTIVE ROUTINE USED FOR PERFORMING AN INTEGRATION            OINT0030
STEP BETWEEN PRINT TIME POINTS.                                OINT0040
                                                                    OINT0050
ARGUMENTS                                                       OINT0060
  IN: INTEGRATION STEP NUMBER                                   DINT0070
  N: NO OF VARIABLES TO BE SUPPLIED AS INPUT TO ROUTINE       OINT0080
      OR COMPUTED BY SUBROUTINE PDAUX WHEN K=0 (MAX=120).      OINT0090
  DTPR: PRINT TIME INTERVAL DESIRED                            DINT0100
  HO: INITIAL INTEGRATION STEP SIZE                            OINT0110
  HMAX: MAXIMUM INTEGRATION STEP SIZE                          DINT0120
  HMIN: MINIMUM STEP SIZE                                       OINT0130
  T: TIME                                                         DINT0140
  X: ARRAY OF STATE VARIABLES                                   DINT0150
  DER: ARRAY OF DERIVATIVES OF STATE VARIABLES                DINT0160
  NOINT: NUMBER OF ESTIMATES OF INTEGRATION PARAMETERS         OINT0170
      TO BE MADE AT THE END OF ANY INTERMEDIATE TIME STEP.    DINT0180
                                                                    OINT0190
IMPLICIT REAL*8 (A-H,O-Z)                                       DINT0200
COMMON/CONTRL/ NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40) OINT0210
COMMON/INTEST/ SGTEST(3,4,22),XTEST(264)                       DINT0220
COMMON/CNSNTS/ PI, RADIANT,G,THIRD,EPS1,EPS4,EPS6,EPS8,       OINT0230
*           EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3) OINT0240
COMMON/COINT/ E(3,120),F(5,120),GG(5,120),Y(5,120),U(5,120) DINT0250
*           ,H,HPRINT,TSAVE,TPRINT,TSTART,ICNT,IDBL,IFLAG     DINT0260
DIMENSION      X(120),DER(120)                                  DINT0270
                                                                    DINT0280
                                                                    DINT0290
CALL ELTIME(1,3)                                                OINT0300
  IF (IN.NE.0) GO TO 3                                           DINT0310
                                                                    DINT0320
FIRST TIME IN ROUTINE, PERFORM INITIALIZATION STEP .          DINT0330
                                                                    OINT0340
H = HO                                                            DINT0350
HPRINT = H                                                        OINT0360
  IDBL=3                                                           DINT0370
  ICNT = 0                                                         OINT0380
  TPRINT = T                                                       OINT0390
CALL OUTPUT(0)                                                    OINT0400
K = 0                                                              DINT0410
CALL PDAUX(X,DER,N,K)                                             DINT0420
IF (N.GT.120) WRITE (6,9) N                                       DINT0430
9 FORMAT('0 NUMBER OF VARIABLES IN SUBROUTINE DINT IS',I6,      DINT0440
*       ' AND EXCEEDS THE ARRAY SIZES OF 120. PROGRAM TERMINATED.')

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	F(4,I) = 0.	DINT0510
	1 F(5,I) = 0.	DINT0520
	GO TO 65	DINT0530
C		DINT0540
C	START OF NEW PRINT POINT INTERVAL.	DINT0550
C		DINT0560
	3 TPRINT = TPRINT+DTPR	DINT0570
	H = HPRINT	DINT0580
C		DINT0590
C	ENTRY TO ADVANCE INTEGRATDR.	DINT0600
C		DINT0610
	4 K = 1	DINT0620
	CALL UPDATE(K)	DINT0630
	IF (K.EQ.1) GO TO 2	DINT0640
C		DINT0650
C	RECALL PDAUX FOR IMPULSE IF K = -1	DINT0660
C		DINT0670
	IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT0680
	CALL PDAUX(X,DER,N,K)	DINT0690
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT0700
	H = H0	DINT0710
	ICNT = 0	DINT0720
	K = 1	DINT0730
	DO 6 I=1,N	DINT0740
	F(1,I) = X(I)	DINT0750
	F(2,I) = DER(I)	DINT0760
	F(3,I) = 0.0	DINT0770
	F(4,I) = 0.0	DINT0780
	6 F(5,I) = 0.0	DINT0790
	2 HPRINT = H	DINT0800
	IF (T+H+EPS8.GE.TPRINT) H = TPRINT-T	DINT0810
C		DINT0820
C	ENTRY TO BACKUP INTEGRATDR, CONVERGENCE TEST FAILED.	DINT0830
C		DINT0840
	5 D1 = 0.5*H	DINT0850
	D12=D1+D1	DINT0860
	D123=H-D1	DINT0870
	TSTART=T	DINT0880
	T=TSTART+D1	DINT0890
	DO 10 I=1,N	DINT0900
	DO 10 J=1,5	DINT0910
	U(J,I)=0.	DINT0920
	Y(J,I)=0.	DINT0930
	10 GG(J,I) = F(J,I)	DINT0940
	CALL DZP(N,X,GG,E,D1,1)	DINT0950
	IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT0960
	CALL PDAUX(X,DER,N,K)	DINT0970
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT0980
	DD 20 I=1,N	DINT0990
	W=X(I)-GG(1,I)	DINT1000

Z=DER(I)-GG(2,I)	DINT1010
Y(1,I)=Y(1,I)+W	DINT1020
Y(2,I)=Y(2,I)+Z	DINT1030
Y(3,I)=Y(3,I)+W**2	DINT1040
Y(4,I)=Y(4,I)+Z*W	DINT1050
20 GG(2,I)=DER(I)	DINT1060
CALL DZP(N,X,GG,E,D1,0)	DINT1070
K = 2	DINT1080
IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT1090
CALL PDAUX(X,DER,N,K)	DINT1100
IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1110
T=TSTART+H	DINT1120
H1 = EPS1/H	DINT1130
DO 30 I=1,N	DINT1140
GG(2,I)=F(2,I)	DINT1150
W=X(I)-GG(1,I)	DINT1160
Z=DER(I)-GG(2,I)	DINT1170
Y(1,I)=Y(1,I)+W	DINT1180
Y(2,I)=Y(2,I)+Z	DINT1190
Y(3,I)=Y(3,I)+W**2	DINT1200
Y(4,I)=Y(4,I)+Z*W	DINT1210
Y(5,I)=Y(3,I)-.5*Y(1,I)**2	DINT1220
U(5,I)=Y(4,I)-.5*Y(1,I)*Y(2,I)	DINT1230
Z=0.	DINT1240
IF(Y(5,I).NE.0.)Z=U(5,I)/Y(5,I)	DINT1250
IF (Z.GT.H1) Z = H1	DINT1260
GG(5,I)=Z	DINT1270
ZYZ = (Y(2,I)-Z*Y(1,I))/D1Z	DINT1280
GG(4,I) = 0.5*GG(4,I)	DINT1290
30 GG(3,I) = ZYZ - D1*GG(4,I)	DINT1300
CALL DZP(N,X,GG,E,H ,1)	DINT1310
K = 3	DINT1320
IF (NPRT(26).NE.0) CALL OUTPUT(0)	DINT1330
CALL PDAUX(X,DER,N,K)	DINT1340
IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1350
DO 44 L=1,NDINT	DINT1360
ZL=L	DINT1370
ZH=ZL*H	DINT1380
DO 40 I=1,N	DINT1390
W=X(I)-GG(1,I)	DINT1400
Z=DER(I)-GG(2,I)	DINT1410
IF (DABS(W).LT.EPS24) W=0.0	DINT1420
IF (DABS(Z).LT.EPS24) Z=0.0	DINT1430
U(1,I)=U(1,I)+W	DINT1440
U(2,I)=U(2,I)+Z	DINT1450
U(3,I)=U(3,I)+W**2	DINT1460
U(4,I)=U(4,I)+W*Z	DINT1470
Z=GG(5,I)	DINT1480
IF(L.EQ.1)GO TO 35	DINT1490
Z=0.	DINT1500

	FX=Y(5,I)+U(3,I)-U(1,I)**2/ZL	DINT1510
	IF (FX.NE.0.)Z=(U(5,I)+U(4,I)-U(1,I)*U(2,I)/ZL)/FX	DINT1520
	IF (Z.GT.H1) Z = H1	DINT1530
35	GG(5,I)=Z	DINT1540
	W=(Y(2,I)-Z*Y(1,I))/D12	DINT1550
	Z=(U(2,I)-Z*U(1,I))/ZH	DINT1560
	GG(3,I)=(H*W-D1*Z)/D123	DINT1570
40	GG(4,I)=(Z-W)/D123	DINT1580
	M=1	DINT1590
	IF (L.EQ.1)M=0	DINT1600
	CALL DZP(N,X,GG,E,H,M)	DINT1610
	IF (L.EQ.NDINT.OR.NPRT(26).NE.0) CALL OUTPUT(0)	DINT1620
	IF (L.EQ.NDINT) K = 4	DINT1630
	CALL PDAUX(X,DER,M,K)	DINT1640
44	IF (L.NE.NDINT.AND.NPRT(26).NE.0) CALL OUTPUT(1)	DINT1650
C		DINT1660
C	TEST FOR CONVERGENCE	DINT1670
C		DINT1680
	IF (K.LT.0) GO TO 47	DINT1690
	DO 46 II=1,N,3	DINT1700
	IF (XTEST(II).LE.0.0) GO TO 46	DINT1710
	TE = 0.0	DINT1720
	TT = 0.0	DINT1730
	I2 = II+2	DINT1740
	DO 45 I=II,I2	DINT1750
	Z=GG(5,I)*(X(I)-GG(1,I))+GG(2,I)+H*(GG(3,I)+H*GG(4,I))	DINT1760
	TE = TE+(DER(I)-Z)**2	DINT1770
45	TT = TT+DER(I)**2	DINT1780
	IF (NPRT(25).NE.0) WRITE (6,48) T,II,TT,TE,(XTEST(I),I=II,I2)	DINT1790
	IF (TT.LT.XTEST(II)) GO TO 46	DINT1800
	IF (XTEST(II+1).GT.0.0 .AND. TE.LT.XTEST(II+1)) GO TO 46	DINT1810
	IF (TE.GE.XTEST(II+2)*TT) GO TO 47	DINT1820
46	CONTINUE	DINT1830
C		DINT1840
C	CONVERGENCE SUCCESSFUL	DINT1850
C		DINT1860
	GO TO 60	DINT1870
C		DINT1880
C	CONVERGENCE FAILED, TEST TO DIVIDE H.	DINT1890
C		DINT1900
47	IF (NPRT(25).EQ.0) WRITE (6,48) T,II,TT,TE,(XTEST(I),I=II,I2)	DINT1910
48	FORMAT('0 DINT CONV. TEST',F10.6,I6,5G16.8)	DINT1920
	WRITE (6,49) T,H	DINT1930
49	FORMAT('0 TEST FAILED AT TIME =',F10.6,' FOR H =',F10.6)	DINT1940
	ICNT = 0	DINT1950
	IF (H.LE.HMIN) GO TO 61	DINT1960
	IF (NPRT(26).NE.0) CALL OUTPUT(1)	DINT1970
	T = T-H	DINT1980
	H = H*0.5	DINT1990
	K = 2	DINT2000

GO TO 5	DINT2010
60 IF (H.GT.0.74*HPRINT) ICNT = ICNT+1	DINT2020
61 DO 63 I=1,N	DINT2030
F(1,I) = X(I)	DINT2040
F(2,I) = DER(I)	DINT2050
F(3,I) = GG(3,I) +2.0*H*GG(4,I)	DINT2060
F(4,I) = GG(4,I)	DINT2070
63 F(5,I) = GG(5,I)	DINT2080
IF(ICNT.LT.IDBL) GO TO 65	DINT2090
ICNT = 0	DINT2100
H = H*2.0	DINT2110
IF (H.GT.HMAX) H=HMAX	DINT2120
HPRINT = 2.0*HPRINT	DINT2130
IF (HPRINT.GT.HMAX) HPRINT = HMAX	DINT2140
65 CALL UPDATE(2)	DINT2150
CALL OUTPUT(1)	DINT2160
IF (TPRINT-T.GE.EPS8) GO TO 4	DINT2170
CALL ELTIME(2,3)	DINT2180
RETURN	DINT2190
END	DINT2200

<pre> C 30 MTOUT = LTIME(1) NDIFF = MTOUT-MTIN(N) MTIN(N) = -1 IF (NDIFF.EQ.0) GO TO 32 NT(N) = NT(N) + NDIFF DO 31 I=1,40 IF (MTIN(I).NE.-1) MTIN(1) = MTIN(I) + NDIFF 31 CONTINUE 32 GO TO 99 C C SUBSEQUENT CALLS FROM MAIN PROGRAM, PRINT SUMMARY TABLE. C 40 NTSUM = LTIME(1) NT(1) = NTSUM - MTIN(1) TIME = FLOAT(NTSUM)/100.0 WRITE (6,41) TIME 41 FORMAT('1 ELAPSED CPU TIME =',F10.2,' SECONDS'// * ' SUB CALLS TIME % '//) PCSUM = 0.0 NTSUM = 0 DO 42 I=1,NSUB J = IND(I) PC = FLOAT(NT(J))/TIME PCSUM = PCSUM + PC NTSUM = NTSUM + NT(J) 42 WRITE (6,43) SUB(J),NC(J),NT(J),PC 43 FORMAT(A10,2I10,F10.2) WRITE (6,44) NTSUM,PCSUM 44 FORMAT('0TOTAL',14X,I10,F10.2) 99 RETURN END </pre>	<pre> ELTI0510 ELTI0520 ELTI0530 ELTI0540 ELTI0550 ELTI0560 ELTI0570 ELTI0580 ELTI0590 ELTI0600 ELTI0610 ELTI0620 ELTI0630 ELTI0640 ELTI0650 ELTI0660 ELTI0670 ELTI0680 ELTI0690 ELTI0700 ELTI0710 ELTI0720 ELTI0730 ELTI0740 ELTI0750 ELTI0760 ELTI0770 ELTI0780 ELTI0790 ELTI0800 ELTI0810 ELTI0820 </pre>
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C      DOUBLE PRECISION FUNCTION EVALFD (D,N,L)                               EVAL0010
C      REV 10 09/26/74EVAL0020
C      EVALUATE FUNCTION THAT IS DEFINED AT LOCATION N OF TAB ARRAY          EVAL0030
C      FOR ABSCISSA VALUE D.  EVALUATES DERIVATIVE, FUNCTION OR INTEGRAL    EVAL0040
C      AS L EQUALS 0, 1, OR 2.  TAB ARRAY IS DEFINED AS FOLLOWS:           EVAL0050
C      TAB(N)      - D0 (D0 MUST BE NON-NEGATIVE)                           EVAL0060
C      TAB(N+1)    - D1 (F1 DEFINED FOR D0 < D < D1)                       EVAL0070
C      TAB(N+2)    - D2 (F2 DEFINED FOR D1 < D < D2)                       EVAL0080
C      TAB(N+3)    - (NOT CURRENTLY USED)                                   EVAL0090
C      TAB(N+4)    - (NOT CURRENTLY USED)                                   EVAL0100
C      TAB(N+5)    - START OF DEFINITION OF 1ST PART OF FUNCTION (F1)      EVAL0110
C      WHICH IS FOLLOWED BY DEFINITION OF 2ND PART OF FUNCTION (F2),      EVAL0120
C      IF ANY.                                                             EVAL0130
C      2ND PART OF FUNCTION EXISTS IF D2 IS NON-ZERO.                       EVAL0140
C      SIGN OF D1 DETERMINES FORM OF DEFINITION FOR 1ST PART OF          EVAL0150
C      THE FUNCTION.                                                       EVAL0160
C      EVAL0170
C      D1 ZERO INDICATES THAT FUNCTION IS CONSTANT D2 FOR ALL D.          EVAL0180
C      EVAL0190
C      D1 POSITIVE INDICATES THAT TAB(N+5)-TAB(N+10) CONTAINS             EVAL0200
C      A0,A1,...A5.  THE COEFFICIENTS OF A 5TH ORDER POLYNOMIAL.          EVAL0210
C      EVAL0220
C      D1 NEGATIVE INDICATES THAT TAB(N+5) CONTAINS NP (REAL)             EVAL0230
C      FOLLOWED BY D(1), F(1), D(2), F(2) ..., D(NP), F(NP)               EVAL0240
C      EVAL0250
C      WARNING- TABULAR FUNCTION MUST BE DEFINED FOR WHOLE RANGE,         EVAL0260
C      THAT IS, FROM D0 TO D1 INCLUSIVE,OR D1 TO D2 INCLUSIVE.           EVAL0270
C      EVAL0280
C      EVAL0290
C      SIMILARLY, THE SIGN OF D2 (IF NON-ZERO) DETERMINES FORM OF        EVAL0300
C      DEFINITION OF 2ND PART OF FUNCTION, IF ANY.                        EVAL0310
C      EVAL0320
C      EVAL0330
C      IF D < D0                                FUNCTION = 0                EVAL0340
C      IF D > |D1|  AND  D2=0                      FUNCTION = F1(|D1|)         EVAL0350
C      IF D > |D2|  AND  D2#0                      FUNCTION = F2(|D2|)         EVAL0360
C      EVAL0370
C      IMPLICIT REAL*8(A-H,O-Z)                                             EVAL0380
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)   EVAL0390
C      F = 0.0                                                                EVAL0400
C      IOUTR = 0                                                                EVAL0410
C      D0 = TAB(N)                                                            EVAL0420
C      IF (D.LT.D0) GO TO 40                                                    EVAL0430
C      D1 = TAB(N+1)                                                            EVAL0440
C      D2 = TAB(N+2)                                                            EVAL0450
C      IF (D1.NE.0.0) GO TO 26                                                 EVAL0460
C      IF (L-1) 40,24,25                                                       EVAL0470
C 24 F = D2                                                                    EVAL0480
C      GO TO 40                                                                EVAL0490
C 25 F= (D-D0)*D2                                                              EVAL0500

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	GO TO 40	EVAL0510
C		EVAL0520
C	COMPUTE INDEX OF F1 DEFINITION	EVAL0530
C		EVAL0540
	26 NP = N+5	EVAL0550
	IF (L.EQ.2) GO TO 41	EVAL0560
C		EVAL0570
C	DERIVATIVES AND FUNCTIONS HERE, INTEGRALS HAVE OTHER LOGIC	EVAL0580
C		EVAL0590
	IF (D.LT.DABS(D1)) GO TO 31	EVAL0600
	IF (D2.NE.0.0) GO TO 32	EVAL0610
C		EVAL0620
C	D .GE. D1 , D2 = 0	EVAL0630
C		EVAL0640
	30 IF (D1.LE.0.0) GO TO 33	EVAL0650
C		EVAL0660
C	IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVAL0670
C	IOUTR.EQ.0 INDICATES D.LE. D1 . COMPUTE POLY DERIVATIVE	EVAL0680
C		EVAL0690
	IF (D.GT.DABS(D1)) IOUTR = 1	EVAL0700
	X = D1	EVAL0710
	GO TO 37	EVAL0720
C		EVAL0730
C	D0 < D < D1	EVAL0740
C		EVAL0750
	31 IF (D1.LT.0.0) GO TO 35	EVAL0760
	X = D	EVAL0770
	GO TO 37	EVAL0780
C		EVAL0790
C	D .GE. D1 , D2 NON-ZERO, USE F2	EVAL0800
C		EVAL0810
	32 MP = 6	EVAL0820
C		EVAL0830
C	COMPUTE INDEX OF F2 DEFINITION	EVAL0840
C		EVAL0850
	IF (D1.LT.0.0) MP = 2.0 * TAB(NP)+1.0	EVAL0860
	NP = NP+MP	EVAL0870
	IF (D.LT.DABS(D2)) GO TO 34	EVAL0880
29	IF (D2.LT.0.0) GO TO 33	EVAL0890
C		EVAL0900
C	IOUTR.EQ.1 INDICATES D BEYOND RANGE. DERIVATIVE = 0.	EVAL0910
C	IOUTR.EQ.0 INDICATES D.LE. D2 . COMPUTE POLY DERIVATIVE	EVAL0920
C		EVAL0930
	IF (D.GT.DABS(D2)) IOUTR = 1	EVAL0940
C		EVAL0950
C	D .GE. D2 (POSITIVE), EVALUATE F2 FOR D2	EVAL0960
C		EVAL0970
	X = D2	EVAL0980
	GO TO 37	EVAL0990
C		EVAL1000

C	D EXCEEDS TABULAR DEFINITION, SET F = F(NP)	EVAL1010
C	IF TABLE DEFINITION EXTENDS BEYOND RANGE, USE TABLE VALUES	EVAL1020
C		EVAL1030
	33 MB = TAB(NP)	EVAL1040
	NB = NP+MB+MB	EVAL1050
	IF (D .LE. TAB(NB-1)) GO TO 35	EVAL1060
	IF (L.EQ.1) F=TAB(NB)	EVAL1070
	GO TO 40	EVAL1080
C		EVAL1090
C	D1 .LE. D < D2	EVAL1100
C		EVAL1110
	34 IF (D2.LT.0.0) GO TO 35	EVAL1120
	X = D	EVAL1130
	GO TO 37	EVAL1140
C		EVAL1150
C	EVALUATE F FROM TABULAR DEFINITION	EVAL1160
C		EVAL1170
	35 MB = TAB(NP)	EVAL1180
	K1 = NP+3	EVAL1190
	K2 = NP+MB+MB	EVAL1200
	DO 36 K=K1,K2,2	EVAL1210
	IF (D.GT.TAB(K)) GO TO 36	EVAL1220
	IF (L-1) 28,27,40	EVAL1230
C		EVAL1240
C	EVALUATE DERIVATIVE FROM TABLE	EVAL1250
C		EVAL1260
	28 F = (TAB(K+1)-TAB(K-1))/(TAB(K)-TAB(K-2))	EVAL1270
	GO TO 40	EVAL1280
C		EVAL1290
C	EVALUATE FUNCTION FROM TABLE	EVAL1300
C		EVAL1310
	27 R2 = TAB(K)-TAB(K-2)	EVAL1320
	R1 = (D-TAB(K-2))/R2	EVAL1330
	R2 = (TAB(K)-D)/R2	EVAL1340
	F = R1*TAB(K+1)+R2*TAB(K-1)	EVAL1350
	GO TO 40	EVAL1360
	36 CONTINUE	EVAL1370
	IF (L.EQ.1) F = TAB(K2)	EVAL1380
	GO TO 40	EVAL1390
	37 IF (IOUTR.EQ.1 .AND. L.EQ.0) GO TO 40	EVAL1400
	IF (L-1) 38,39,40	EVAL1410
C		EVAL1420
C	EVALUATE DERIVATIVE OF 5TH DEGREE POLYNOMIAL	EVAL1430
C		EVAL1440
	38 F = TAB(NP+1)+X*(2.0*TAB(NP+2)+X*(3.0*TAB(NP+3)+X*(4.0*TAB(NP+4)+	EVAL1450
	* X*5.0*TAB(NP+5)))	EVAL1460
	GO TO 40	EVAL1470
C		EVAL1480
C	EVALUATE 5TH DEGREE POLYNOMIAL	EVAL1490
C		EVAL1500

	39 F =	TAB(NP) + X*(TAB(NP+1)+X*(TAB(NP+2)	EVAL1510
	*	+X*(TAB(NP+3)+X*(TAB(NP+4)+X*TAB(NP+5))))	EVAL1520
		GO TO 40	EVAL1530
C			EVAL1540
C	L=2:	COMPUTE INTEGRAL OF FUNCTION FROM D0 TO D.	EVAL1550
C			EVAL1560
	41 IF (D.EQ.D0) GO TO 40		EVAL1570
		X0 = D0	EVAL1580
		X1 = D1	EVAL1590
		DO 50 I=1,2	EVAL1600
		IF (X1) 43,49,42	EVAL1610
	42 A0 =	TAB(NP)	EVAL1620
		A1 = TAB(NP+1)/2.0	EVAL1630
		A2 = TAB(NP+2)/3.0	EVAL1640
		A3 = TAB(NP+3)/4.0	EVAL1650
		A4 = TAB(NP+4)/5.0	EVAL1660
		A5 = TAB(NP+5)/6.0	EVAL1670
		NP = NP+6	EVAL1680
		X = X0	EVAL1690
		IF (X.NE.0.0) F=F-X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVAL1700
		X = DMIN1(D,X1)	EVAL1710
		IF (X.NE.0.0) F=F+X*(A0+X*(A1+X*(A2+X*(A3+X*(A4+X*A5))))	EVAL1720
		IF(D.LE.X1) GO TO 40	EVAL1730
		IF(I.EQ.1.AND.D2.NE.0.0) GO TO 49	EVAL1740
C			EVAL1750
C	NOTE -	NP WAS UPDATED NP=NP+6 BEFORE THIS, READY FOR SECOND PASS	EVAL1760
C			EVAL1770
	F = F +	(D-X1)*(TAB(NP-6)+X1*(TAB(NP-5)+X1*(TAB(NP-4)	EVAL1780
	*	+X1*(TAB(NP-3)+X1*(TAB(NP-2)+X1*TAB(NP-1))))	EVAL1790
		GO TO 40	EVAL1800
	43 MB =	TAB(NP)	EVAL1810
		K1 = NP+3	EVAL1820
		K2 = NP+MB+MB	EVAL1830
		NP = K2+1	EVAL1840
		DL = DMIN1(D,DABS(X1))	EVAL1850
	DU 44	K=K1,K2,2	EVAL1860
		IF (X0.GE.TAB(K)) GO TO 44	EVAL1870
		Z1 = DMAX1(X0,TAB(K-2))	EVAL1880
		Z2 = DMIN1(DL,TAB(K))	EVAL1890
		FYX = TAB(K-1)*TAB(K) - TAB(K+1)*TAB(K-2)	EVAL1900
		FY = TAB(K+1) - TAB(K-1)	EVAL1910
		F = F +(FYX + 0.5*FY*(Z1+Z2)) *(Z2-Z1)/ (TAB(K)-TAB(K-2))	EVAL1920
		IF (Z2.NE.DL) GO TO 44	EVAL1930
		IF(I.EQ.1.AND.D2.NE.0.0) GO TO 49	EVAL1940
		IF(Z2. EQ. D) GO TO 40	EVAL1950
		F = F +(D-Z2)*(FYX+Z2*FY)/ (TAB(K)-TAB(K-2))	EVAL1960
		GO TO 40	EVAL1970
	44	CONTINUE	EVAL1980
	49	X0 = DABS(D1)	EVAL1990
	50	X1 = D2	EVAL2000

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40 EVALFD = F  
RETURN  
END
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EVAL2010  
EVAL2020  
EVAL2030
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SUBROUTINE FINPUT                                FINPG010
C                                                    REV 12 12/18/74FINPG020
C CONTROLS CARD INPUT SPECIFYING THE ALLOWED CONTACTS OF THE CRASH FINPG030
C VICTIM BODY SEGMENTS WITH VEHICLE PANELS, BELTS, AIRBAGS AND OTHERFINPG040
C BODY SEGMENTS ALONG WITH THE ASSOCIATED FUNCTIONS TO BE USED FOR FINPG050
C EACH CONTACT.                                FINPG060
C ALSO SETS UP TABLES TO CONTROL TIME HISTORY INFORMATION FOR FINPG070
C EACH FUNCTION FOR EACH ALLOWED CONTACT.        FINPG080
C                                                    FINPG090
IMPLICIT REAL*8(A-H,D-Z)                        FINPG100
COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40) FINPG110
COMMON/JBARTZ/ MNPL( 20),MNBLT( 8),MNSEG( 22),MNBAG( 6),    FINPG120
*           MPL(3,5,20),MBLT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),  FINPG130
*           NTPL(5,20),NTBLT(5,8),NTSEG(5,22)                FINPG140
COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000) FINPG150
COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)FINPG160
*           ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JOINT(21)      FINPG170
*           ,CGS(21),JS(21)                                  FINPG180
REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT  FINPG190
LOGICAL*1 CGS,JS                                           FINPG200
COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24) FINPG210
*           ,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12) FINPG220
*           ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)          FINPG230
*           ,NQ,KQ1(12),KQ2(12),KQTYPE(12)                 FINPG240
COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)  FINPG250
*           ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)    FINPG260
*           ,VISC(7,63),JNT(21),IPIN(21),MS,ISING(22)     FINPG270
*           ,IGLOB(21),JOINTF(21)                          FINPG280
COMMON/CEULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGD(3,21),  FINPG290
*           FE(3,21),TQE(3,31),CONST(3,21)                FINPG300
COMMON/KALEPS/WTIME(30),IWIND(30),MWSEG(5,22)             FINPG310
COMMON/TEMPVS/JTITLE(5,51),NF(5),NS(3),KTITLE(31)        FINPG320
REAL BLANK /' /',JTITLE,KTITLE                          FINPG330
REAL SURFCE(2,3) /' PL', 'ANE ', ' BE', 'LT ', ' SEG', 'MENT' /  FINPG340
MXNTI = 50                                                FINPG350
J1 = MXTB1+1                                             FINPG360
C                                                    FINPG370
C INPUT ALLOWED CONTACTS AND FUNCTIONS BY REF. NO.        FINPG380
C                                                    FINPG390
NT = 1                                                    FINPG400
WRITE (6,31)                                             FINPG410
31 FORMAT('1 ALLOWED CONTACTS AND ASSOCIATED FUNCTIONS')  FINPG420
DO 61 I=1,4                                             FINPG430
IJK = 0                                                 FINPG440
GO TO (32,34,35,36),I                                  FINPG450
32 IF (NPL.LE.0) GO TO 61                               FINPG460
C                                                    FINPG470
C INPUT NO. OF SEGMENTS TO CONTACT EACH PLANE.          FINPG480
C INPUT CARD F.1.A                                       FINPG490
C                                                    FINPG500

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	READ (5,33) (MNPL(J),J=1,NPL)	FINP0510
33	FORMAT(18I4)	FINP0520
	NJJ = NPL	FINP0530
	GO TO 37	FINP0540
34	IF (NBLT.LE.0) GO TO 61	FINP0550
C		FINP0560
C	INPUT NO. OF SEGMENTS TO CONTACT EACH BELT.	FINP0570
C	INPUT CARD F.2.A	FINP0580
C		FINP0590
	READ (5,33) (MNBLT(J),J=1,NBLT)	FINP0600
	NJJ = NBLT	FINP0610
	GO TO 37	FINP0620
35	IF (NSEG.LE.0) GO TO 61	FINP0630
C		FINP0640
C	INPUT NO. OF SEGMENTS TO CONTACT EACH SEGMENT.	FINP0650
C	INPUT CARD F.3.A	FINP0660
C		FINP0670
	READ (5,33) (MNSEG(J),J=1,NSEG)	FINP0680
	NJJ = NSEG	FINP0690
	GO TO 37	FINP0700
36	IF (NJNT.LE.0) GO TO 61	FINP0710
C		FINP0720
C	INPUT CARD F.4.A	FINP0730
C	SUPPLY IGLOB(J)=1 FOR EACH GLOBALGRAPHIC JOINT J=1,NJNT	FINP0740
C		FINP0750
	READ (5,33) (IGLOB(J),J=1,NJNT)	FINP0760
	NJJ = NJNT	FINP0770
C		FINP0780
C	START OF LOOP TO READ CONTACTS FOR PLANES (I=1), BELTS (I=2),	FINP0790
C	SEGMENTS (I=3) AND FUNCTIONS FOR GLOBALGRAPHIC JOINTS (I=4).	FINP0800
C		FINP0810
37	DO 60 J=1,NJJ	FINP0820
	IF (I.EQ.1) NK = MNPL(J)	FINP0830
	IF (I.EQ.2) NK = MNBLT(J)	FINP0840
	IF (I.EQ.3) NK = MNSEG(J)	FINP0850
	IF (I.EQ.4) NK = IGLOB(J)	FINP0860
	IF (NK.LE.0) GO TO 60	FINP0870
	DO 59 K=1,NK	FINP0880
	IF (IJK.EQ.0) WRITE (6,38) I	FINP0890
38	FORMAT('0',119X,'CARDS F.',I1)	FINP0900
	IF (IJK.EQ.0 .AND. I.NE.4) WRITE (6,39) SURFCE(1,I),SURFCE(2,I)	FINP0910
39	FORMAT('0',3X,2A4,8X,'SEGMENT',2X,'FORCE DEFLECTION',6X,'INERTIAL	FINP0920
	*SPIKE',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF.')	FINP0930
	IF (IJK.EQ.0 .AND. I.EQ.4) WRITE (6,40)	FINP0940
40	FORMAT('0',5X,'JOINT (GLOBALGRAPHIC)',2X,'TORQUE DEFLECTION',6X,'HF	FINP0950
	*ERRON FORMULA',10X,'R FACTOR',13X,'G FACTOR',10X,'FRICTION COEF.')	FINP0960
	IJK = 1	FINP0970
C		FINP0980
C	INPUT CONTACT SURFACE NO., SEGMENT NO., AND FUNCTION NOS.	FINP0990
C	INPUT CARD F.(I).(K)	FINP1000

C	READ (5,33) NJ,NS,NF	FINP1010
	WRITE (6,41) NJ,NS,NF	FINP1020
41	FORMAT('0',I7,'-',I3,I11,'-',I3,I8,4I21)	FINP1030
	IF (NJ.NE.J) WRITE (6,42)	FINP1040
42	FORMAT(' FINPUT INPUT ERROR. PROGRAM TERMINATED.')	FINP1050
	IF (NJ.NE.J) STOP	FINP1060
	NLT = 1	FINP1070
	DO 43 JJ = 1,31	FINP1080
43	KTITLE(JJ) = BLANK	FINP1090
	GO TO (44,46,48,49),I	FINP1100
C		FINP1110
C	PLACE SEGMENT NO. AND INDEX TO NTAB ARRAY INTO M- AND NT- ARRAYS.	FINP1120
C		FINP1130
44	MPL(1,K,J) = NS(1)	FINP1140
	MPL(2,K,J) = NS(2)	FINP1150
	MPL(3,K,J) = NS(3)	FINP1160
	NTPL(K,J) = NT	FINP1170
	DO 45 JJ = 1,5	FINP1180
45	KTITLE(JJ) = PLTTL (JJ,J)	FINP1190
	GO TO 50	FINP1200
46	MBLT(1,K,J) = NS(1)	FINP1210
	MBLT(2,K,J) = NS(2)	FINP1220
	MBLT(3,K,J) = NS(3)	FINP1230
	NTBLT(K,J) = NT	FINP1240
	DO 47 JJ = 1,5	FINP1250
47	KTITLE(JJ) = BLTTTL (JJ,J)	FINP1260
C		FINP1270
C	SET UP TWO TABLES FOR FULL BELT FRICTION	FINP1280
C		FINP1290
	IF (NF(5).NE.0) NLT = 2	FINP1300
	GO TO 50	FINP1310
48	MSEG(1,K,J) = NS(1)	FINP1320
	MSEG(2,K,J) = NS(2)	FINP1330
	MSEG(3,K,J) = NS(3)	FINP1340
	NTSEG(K,J) = NT	FINP1350
	KTITLE (3) = SEG(J)	FINP1360
	GO TO 50	FINP1370
C		FINP1380
C	NOTE: GLOBALGRAPHIC JOINT WILL SAVE NT IN IGLOB ARRAY	FINP1390
C		FINP1400
49	IGLOB(J) = NT	FINP1410
	KTITLE(2) = JOINT(J)	FINP1420
C		FINP1430
C	SET UP POINTERS TO TAB ARRAY IN NTAB ARRAY.	FINP1440
C		FINP1450
50	NFJ = NS(2)	FINP1460
	IF (NFJ.GT.0) KTITLE(6) = SEG(NFJ)	FINP1470
	DO 52 JJ = 1,5	FINP1480
	IF (NF(JJ).LE.0) GO TO 52	FINP1490
		FINP1500

```

NFJ = NF(JJ)
DO 51 KK = 1,5
KJ = 5*JJ+KK+1
51 KTITLE(KJ) = JTITLE(KK,NFJ)
52 CONTINUE
WRITE (6,53) KTITLE
53 FORMAT(1X,5A4,1X,A4,5(1X,5A4))
DO 58 NL = 1,NLT
NTAB(NT) = J1
NT = NT+1
DO 56 L=1,5
NX = NF(L)
NTAB(NT) = 0
IF (NX.EQ.0) GO TO 55
NTAB(NT) = NTI(NX)
IF (NTI(NX).NE.0) GO TO 56
WRITE(6,54) NX
54 FORMAT ('0 FUNCTION NO.',I4,' HAS NOT BEEN DEFINED. PROGRAM TERMINIF
*NATED.')
```

FINP1510
FINP1520
FINP1530
FINP1540
FINP1550
FINP1560
FINP1570
FINP1580
FINP1590
FINP1600
FINP1610
FINP1620
FINP1630
FINP1640
FINP1650
FINP1660
FINP1670
FINP1680
FINP1690
FINP1700
FINP1710
FINP1720
FINP1730
FINP1740
FINP1750
FINP1760
FINP1770
FINP1780
FINP1790
FINP1800
FINP1810
FINP1820
FINP1830
FINP1840
FINP1850
FINP1860
FINP1870
FINP1880
FINP1890
FINP1900
FINP1910
FINP1920
FINP1930
FINP1940
FINP1950
FINP1960
FINP1970
FINP1980
FINP1990
FINP2000

```

55 IF (L.NE.1) GO TO 56

IF FORCE DEFLECTION FUNCTION NO. IS ZERO,
SET UP FOR ROLLING CONSTRAINT

NQ = NQ+1
NTAB(NT) = -NQ
KQTYPE(NQ) = -4
KQ1(NQ) = NS(2)
KQ2(NQ) = NS(1)
IF (I.NE.3) GO TO 56
KQ1(NQ) = J
KQ2(NQ) = NS(2)
56 NT = NT+1

INITIALIZE TAB ARRAY TO ZERO EXCEPT FOR DMAX, DINER, FDMAX.

J2 = J1+19
DO 57 JJ=J1,J2
57 TAB(JJ) = 0.0
NX = NTAB(NT-5)
IF (NX.LT.0) GO TO 58
TAB(J1+8) = DABS(TAB(NX+1))
IF (TAB(NX+2).NE.0.0) TAB(J1+8) = DABS(TAB(NX+2))
TAB(J1+10) = EVALFD(TAB(J1+8),NX,1)
NX = NTAB(NT-4)
IF (NX.LE.0) GO TO 58
TAB(J1+9) = DABS(TAB(NX+1))
IF (TAB(NX+2).NE.0.0) TAB(J1+9) = DABS(TAB(NX+2))
58 J1 = J2+1
```

59	CONTINUE	FINP2010
60	CONTINUE	FINP2020
61	CONTINUE	FINP2030
	MXNT8 = NT-I	FINP2040
	MXTB2 = J1-1	FINP2050
	IF (MXTB2.GT.2000) WRITE (6,62) MXTB2	FINP2060
62	FORMAT('O ERROR IN SUBROUTINE FINPUT, SIZE OF TAB ARRAY =',I8//	FINP2070
	* ' PROGRAM TERMINATED')	FINP2080
	IF (MXTB2.GT.2000) STOP	FINP2090
C		FINP2100
C	INPUT CARD F.5 - JOINT FUNCTIONS TO BE USED.	FINP2110
C		FINP2120
	IF (NJNT.LE.0) GO TO 81	FINP2130
	READ (5,33) (JOINTF(J),J=I,NJNT)	FINP2140
	IJK = 0	FINP2150
	DO 80 J=1,NJNT	FINP2160
	IF (JOINTF(J).EQ.0) GO TO 80	FINP2170
	IF (IJK.EQ.0) WRITE (6,77)	FINP2180
77	FORMAT('1',119X,'CARD F.5'/	FINP2190
	* ' THE FOLLOWING JOINT RESTORING FORCE FUNCTIONS AS DEFINED	FINP2200
	*ON CARDS E.7 WILL BE USED.'//4X,'JOINT',10X,'FUNCTION'//)	FINP2210
	JF = JOINTF(J)	FINP2220
	IJK = 1	FINP2230
	WRITE (6,78) J,JOINT(J),JF,(JTITLE(I,JF),I=1,5)	FINP2240
78	FORMAT(I6,'-',A4,I10,'-',5A4)	FINP2250
	IF (NTI(JF).EQ.0) WRITE (6,42)	FINP2260
	IF (NTI(JF).EQ.0) STOP	FINP2270
80	CONTINUE	FINP2280
C		FINP2290
C	INPUT CONTACT SEGMENTS FOR AIRBAG, IF ANY.	FINP2300
C		FINP2310
81	IF (NBAG.LE.0) GO TO 69	FINP2320
	IJK = 0	FINP2330
	DO 68 J=1,NBAG	FINP2340
C		FINP2350
C	INPUT CARD F.6.(J)	FINP2360
C		FINP2370
	READ (5,63) K,NK,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINP2380
63	FORMAT(2I4,20I2)	FINP2390
	MNBAG(J) = NK	FINP2400
	IF (NK.EQ.0) GO TO 68	FINP2410
	IF (IJK.EQ.0) WRITE (6,64)	FINP2420
64	FORMAT(///5X,'AIRBAG',4X,'VS.',4X,'SEGMENTS',90X,'CARDS F.6')	FINP2430
	IF (K.NE.J) WRITE (6,42)	FINP2440
	IF (K.NE.J) STOP	FINP2450
	WRITE (6,65) J,(MBAG(2,I,J),MBAG(3,I,J),I=1,NK)	FINP2460
65	FORMAT('O NO.',I2,12X,I0(I3,'-',I3))	FINP2470
	DO 66 I=1,NK	FINP2480
	K = MBAG(2,I,J)	FINP2490
66	KTITLE(I) = SEG(K)	FINP2500

	WRITE (6,67) (BAGTTL(I,J),I=1,5),(KTITLE(I),I=1,NK)	FINP2510
	67 FORMAT(1X,5A4,10(3X,A4))	FINP2520
	68 CONTINUE	FINP2530
C		FINP2540
C	INPUT CARDS F.7.A-F.7.B FOR SUBROUTINE WINDY.	FINP2550
C		FINP2560
	69 READ (5,33) (MWSEG(1,J),J=1,NSEG)	FINP2570
	IPAGE = 0	FINP2580
	DO 73 J=1,NSEG	FINP2590
	IWIND(J) = 0	FINP2600
	WTIME(J) = 0.0	FINP2610
	IF (MWSEG(1,J).EQ.0) GO TO 73	FINP2620
	IF (IPAGE.EQ.0) WRITE (6,70)	FINP2630
	70 FORMAT('1 SEGMENT WIND FORCES',99X,'CARDS F.7'//	FINP2640
	* ' SEGMENT-ELLIPSOID SEGMENT-PLANE',	FINP2650
	* 17X,'WIND FORCE FUNCTION')	FINP2660
	IPAGE = 1	FINP2670
	READ (5,33) (MWSEG(I,J),I=1,5)	FINP2680
	WRITE (6,71) (MWSEG(I,J),I=1,5)	FINP2690
	71 FORMAT('0',I7,' -',I3,I14,' -',I3,I30)	FINP2700
	IF (MWSEG(1,J).NE.J) WRITE (6,42)	FINP2710
	IF (MWSEG(1,J).NE.J) STOP	FINP2720
	M3 = MWSEG(3,J)	FINP2730
	M4 = MWSEG(4,J)	FINP2740
	M5 = MWSEG(5,J)	FINP2750
	WRITE (6,72) SEG(J),SEG(M3),(PLTTL(I,M4),I=1,5)	FINP2760
	* , (JTITLE(I,M5),I=1,5)	FINP2770
	72 FORMAT(5X,A4,15X,A4,'-',5A4,2X,5A4)	FINP2780
	73 CONTINUE	FINP2790
	RETURN	FINP2800
	END	FINP2810


```

SUBROUTINE FLXSEG
C
IMPLICIT REAL*8(A-H,O-Z)
COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
*      ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8),NFLX
COMMON/CNSNTS/ PI, RADIANG,THIRD, EPS1, EPS4, EPS6, EPS8,
*      EPS12, EPS15, EPS20, EPS24, UNITL, UNITM, UNITT, GRAVTY(3)
COMMON/TEMPVS/ TT(3,3), THN(4), CN1(3,3), CN(3,3), WNM1(3),
*      THND(4), PTD(3), WCSN(3), RHSN(3), RHS1(3),
*      RHS2(3), GF(3,4), GC(3,3), CGC(3,3), THA(3),
*      THAD(3), THADEG(3), DN2N1(3,3), RMG(3)
IF (NFLX.EQ.0) GO TO 99
CALL ELTIME(1,34)
IFX = 1
11 N1 = NFLEX(1,IFX)
N3 = NFLEX(3,IFX)
CALL DOTT(D(1,1,N3),D(1,1,N1),TT,3,3,3)
THN(1) = DATAN2(TT(1,2),TT(1,1))
THN(2) = -DARSIN(TT(1,3))
THN(3) = DATAN2(TT(2,3),TT(3,3))
THN(4) = 1.0
CT22 = 1.0-TT(1,3)**2
CT2 = DSQRT(CT22)
ST2 = -TT(1,3)
CT1 = TT(1,1)/CT2
ST1 = TT(1,2)/CT2
CN1(1,1) = -TT(1,1)*TT(1,3)/CT22
CN1(1,2) = -TT(1,2)*TT(1,3)/CT22
CN1(1,3) = 1.0
CN1(2,1) = -ST1
CN1(2,2) = CT1
CN1(2,3) = 0.0
CN1(3,1) = TT(1,1)/CT22
CN1(3,2) = TT(1,2)/CT22
CN1(3,3) = 0.0
CALL DOT(TT,WMEG(1,N3),WNM1,3,1,3)
DO 12 I=1,3
12 WNM1(I) = WNM1(I) - WMEG(I,N1)
CALL MAT(CN1,WNM1,THND,3,3,1,3,3,3)
THND(4) = 0.0
CALL CROSS(WMEG(1,N1),WNM1,WCSN)
RHSN(1) = ( (-THND(1)*ST1*ST2 + THND(2)*CT1/CT2)*WNM1(1)
*      +( THND(1)*CT1*ST2 + THND(2)*ST1/CT2)*WNM1(2) )/CT2
RHSN(2) = -THND(1)*(CT1*WNM1(1) + ST1*WNM1(2))
RHSN(3) = ( (-THND(1)*ST1 + THND(2)*CT1*ST2/CT2)*WNM1(1)
*      +( THND(1)*CT1 + THND(2)*ST1*ST2/CT2)*WNM1(2) )/CT2
13 N2 = NFLEX(2,IFX)
M = 0
DO 15 I=1,3

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REV 12 10/25/74
FLXS0010
FLXS0020
FLXS0030
FLXS0040
FLXS0050
FLXS0060
FLXS0070
FLXS0080
FLXS0090
FLXS0100
FLXS0110
FLXS0120
FLXS0130
FLXS0140
FLXS0150
FLXS0160
FLXS0170
FLXS0180
FLXS0190
FLXS0200
FLXS0210
FLXS0220
FLXS0230
FLXS0240
FLXS0250
FLXS0260
FLXS0270
FLXS0280
FLXS0290
FLXS0300
FLXS0310
FLXS0320
FLXS0330
FLXS0340
FLXS0350
FLXS0360
FLXS0370
FLXS0380
FLXS0390
FLXS0400
FLXS0410
FLXS0420
FLXS0430
FLXS0440
FLXS0450
FLXS0460
FLXS0470
FLXS0480
FLXS0490
FLXS0500

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RHS1(2) = RHS1(2) + THAD(1)*(CN(1,2)*RHS2(2)+CN(2,2)*CSC*RHS2(3)) FLXS1010
*          + THAD(2)*CN(1,2)*CSS*RHS2(3) FLXS1020
RHS1(3) = RHS1(3) - THAD(2)*CSC*RHS2(3) FLXS1030
CALL MAT(GF, RHSN, RHS2, 3,3,1,3,3,3) FLXS1040
M = 1 FLXS1050
DO 30 I=1,3 FLXS1060
CALL MAT(HF(1,M,IFX), THND, PTD, 3,3,1,4,3,3) FLXS1070
RHS2(I) = RHS2(I) + XDY(PTD,CN1,WNM1) FLXS1080
30 M = M+4 FLXS1090
CALL MAT(CN, RHS2, PTD, 3,3,1,3,3,3) FLXS1100
DO 35 I=1,3 FLXS1110
35 RHS1(I) = RHS1(I) + PTD(I) FLXS1120
CALL DOT(D(1,1,N1),RHS1,V4(1,IFX),3,1,3) FLXS1130
IF (IFX.EQ.NFLX) GO TO 98 FLXS1140
IFX = IFX+1 FLXS1150
IF (NFLEX(1,IFX).EQ.N1 .AND. NFLEX(3,IFX).EQ.N3) GO TO 13 FLXS1160
GO TO 11 FLXS1170
98 CALL ELTIME(2,34) FLXS1180
99 RETURN FLXS1190
END FLXS1200

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C      DOUBLE PRECISION FUNCTION FINTERP(THETA,PHI,NT)                                FNT00010
C      REV 12 12/06/74 FNT00020
C      COMPUTES THE RESTORING TORQUE OF A JOINT AS A FUNCTION OF THE                FNT00030
C      FLEXURE ANGLE (THETA) AND THE AZIMUTH ANGLE (PHI) AS DEFINED BY             FNT00040
C      FUNCTION NO. NT                                                              FNT00050
C      ASSUMES 0 < THETA < PI                                                       FNT00060
C      -PI < PHI < PI                                                                FNT00070
C      DATA IN TAB ARRAY CONTAINS NTHETA,NPHI FOLLOWED BY                         FNT00080
C      TWO DIMENSIONAL ARRAY OF FUNCTIONAL VALUES (NTHETA > 0)                   FNT00090
C      OR POLYNOMIAL COEFFICIENTS (NTHETA < 0) FOR EQUALLY                         FNT00100
C      SPACED VALUES OF PHI.                                                       FNT00110
C      THETA(I) = (I-1)*PI/(NTHETA-1) FOR I=1,NTHETA                             FNT00120
C      PHI(J) = -PI + (J-1)*2*PI/NPHI FOR J=1,NPHI                               FNT00130
C      F(THETA,PHI) = F(THETA,-PI)                                                 FNT00140
C      SUBROUTINE EVALUATES G1(THETA) = F(THETA,PHI(J) )                          FNT00150
C      G2(THETA) = F(THETA,PHI(J+1))                                               FNT00160
C      FOR PHI(J) < PHI < PHI(J+1)                                                 FNT00170
C      BY LINEAR INTERPOLATION OR POLYNOMIAL EVALUATION AND THEN LINEAR           FNT00180
C      INTERPOLATES BETWEEN G1 AND G2 TO OBTAIN F(THETA,PHI).                     FNT00190
C      IF F < 0, F IS SET TO ZERO, THEREFORE A DEAD BAND IS OBTAINED              FNT00200
C      BY NEGATIVE VALUES IN THE TABLE.                                          FNT00210
C      IMPLICIT REAL*8 (A-H,O-Z)                                                  FNT00220
C      COMMON/CNSNTS/ PI,RADIAN,G,THIRD,EPS1,EPS4,EPS6,EPS8,                       FNT00230
C      * EPS12,EPS15,EPS20,EPS24,UN1TL,UNITM,UNITT,GRAVTY(3) FNT00240
C      COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NT1(50),NTAB(500),TAB(2000) FNT00250
C      IERROR = 0                                                                    FNT00260
C      IF (PHI.LT.-PI) IERROR = 1                                                    FNT00270
C      IF (PHI.GT. PI) IERROR = 2                                                    FNT00280
C      IF (THETA.LT.0.0) IERROR = 3                                                  FNT00290
C      IF (THETA.GT.PI) IERROR = 4                                                  FNT00300
C      IF (IERROR.NE.0) WRITE (6,11) IERROR,THETA,PHI,NT                          FNT00310
11 FORMAT('0 IMPROPER ARGUMENTS TO FUNCTION FINTERP. ERROR CODE =',I4/           FNT00320
C      * '0 THETA =',G25.15, ' PHI =',G25.15,' NT =',I6)                          FNT00330
C      IF (IERROR.NE.0) STOP                                                         FNT00340
C      NF = NT1(NT) + 5                                                             FNT00350
C      NTHETA = TAB(NF)                                                             FNT00360
C      NPHI = TAB(NF+1)                                                             FNT00370
C      DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR PHI.                       FNT00380
C      XNP = (PHI+PI)/(2.0*PI)*TAB(NF+1)                                           FNT00390
C      NP1 = XNP                                                                     FNT00400
C      NP2 = NP1+1                                                                    FNT00410
C      IF (NP2.GE.NPHI) NP2 = 0                                                       FNT00420
C      RP2 = XNP - DFLOAT(NP1)                                                       FNT00430
C      RP1 = 1.0 - RP2                                                               FNT00440

```

	NTH = IABS(NTHETA)	FNTE0510
	IP1 = NF+1+NP1*NTH	FNTE0520
	IP2 = NF+1+NP2*NTH	FNTE0530
C		FNTE0540
C	DETERMINE INDEX AND INTERPOLATION PARAMETERS FOR THETA.	FNTE0550
C		FNTE0560
	IF (NTHETA.LT.0) GO TO 20	FNTE0570
	XNT = THETA/PI*(TAB(NF)-1.0)	FNTE0580
	NT1 = XNT	FNTE0590
	RT2 = XNT - DFLOAT(NT1)	FNTE0600
	RT1 = 1.0 - RT2	FNTE0610
	IT1 = IP1 + NT1	FNTE0620
	IT2 = IP2 + NT1	FNTE0630
	G1 = RT1*TAB(IT1+1) + RT2*TAB(IT1+2)	FNTE0640
	G2 = RT1*TAB(IT2+1) + RT2*TAB(IT2+2)	FNTE0650
	GO TO 23	FNTE0660
C		FNTE0670
C	COMPUTE FOR POLYNOMIALS IN THETA FOR FIXED PHI.	FNTE0680
C		FNTE0690
	20 NPOLY = -NTHETA-1	FNTE0700
	IT1 = IP1 + NPOLY + 2	FNTE0710
	IT2 = IP2 + NPOLY + 2	FNTE0720
	THETA1 = THETA - TAB(IP1+1)	FNTE0730
	THETA2 = THETA - TAB(IP2+1)	FNTE0740
	G1 = 0.0	FNTE0750
	G2 = 0.0	FNTE0760
	DO 21 I=1, NPOLY	FNTE0770
	IT1 = IT1-1	FNTE0780
	IT2 = IT2-1	FNTE0790
	G1 = THETA1*(TAB(IT1)+G1)	FNTE0800
	21 G2 = THETA2*(TAB(IT2)+G2)	FNTE0810
	23 FNTERP = RP1*G1 + RP2*G2	FNTE0820
	IF (FNTERP.LT.0.0) FNTERP = 0.0	FNTE0830
	RETURN	FNTE0840
	END	FNTE0850


```

      IF (MM.EQ.0)      GO TO 20
      DO 14 J=1,3
14  T2(J) = BAR(J+3,JJ) - BD(J+3,MM)
      CALL MAT(BD(7,MM),T2,T3,3,3,1,3,3,3)
      CALL DOT(D(1,1,KK),T3,ZNR,3,1,3)
      DPR = 0.0
      DO 15 J=1,3
15  DPR = DPR + ZNR(J)*(ZY(J,LL)/DS(LL) - ZY(J,LL-1)/DS(LL-1))
      IF (DPR.LT.0.0)  GO TO 20
C
C  POSITIVE DPR INDICATES BELT IS PULLING AWAY FROM POINT JJ. REMOVE
C  POINT FROM FUTURE CONSIDERATION AND DECREASE LL - NO. OF LENGTHS.
C
      LL = LL-1
      GO TO 12
20  JF(LL+1) = K
C
C  COMPUTE XLG - TOTAL LENGTH OF THE LL BELT SECTIONS.
C
      XLG = 0.0
      DO 30 L=1,LL
30  XLG = XLG + DS(L)
C
C  NEGATIVE XLONG INDICATES INITIAL SLACK IN BELT.
C
      IF (XLONG.LT.0.0) XLONG = XLG-XLONG
C
C  COMPUTE FRC - TOTAL FORCE OF BELT AND APPLY IT TO ALL SEGMENTS.
C
      STRAIN = (XLG-XLONG)/XLONG
      FRC = FRCDFL(STRAIN,NT,1)
      IF (FRC.LE.0.0)  GO TO 99
      IF (NPRT(16).NE.0) WRITE (6,31) TIME,XLG,STRAIN,FRC,LL
31  FORMAT('0 SUB HBELT',F13.6,3G18.7,16)
      DO 40 L=1,LL
      L1 = JF(L)
      L2 = JF(L+1)
      K1 = IBAR(1,L1)
      K2 = IBAR(1,L2)
      CALL MAT(D(1,1,K1),ZY(1,L),T4,3,3,1,3,3,3)
      CALL MAT(D(1,1,K2),ZY(1,L),T5,3,3,1,3,3,3)
      CALL CROSS(BAR(4,L1),T4,T6)
      CALL CROSS(BAR(4,L2),T5,T7)
      FR = FRC/DS(L)
      IF (NPRT(16).NE.0) WRITE (6,32) L1,K1,K2,DS(L),FR,(ZY(J,L),J=1,3)
32  FORMAT(6X,316,5G18.7)
      DO 40 J=1,3
      U1(J,K1) = U1(J,K1) + FR*ZY(J,L)
      U2(J,K1) = U2(J,K1) + FR*T6(J)
      U1(J,K2) = U1(J,K2) - FR*ZY(J,L)

```

```
40 U2(J,K2) = U2(J,K2) - FR*T7(J)
99 CALL ELTIME(2,36)
RETURN
END
```

```
HBEL1010
HBEL1020
HBEL1030
HBEL1040
```



```

*          ' REFERENCE LENGTH =',G16.8///                                HINP0510
*          ' HARNESS BELT POINT SEGMENT ELLIPSOID ',                    HINP0520
*          9X,'REFERENCE POINT' /                                        HINP0530
*          3X,'NO.',5X,'NO.',3X,'NO.',5X,'NO.',5X,'NO.',6X,          HINP0540
*          6X,'X',9X,'Y',9X,'Z',3X / )                                  HINP0550
C                                                                 HINP0560
C          CHANGE SIGN OF XLONG FOR INITIAL CALL TO HBELT.              HINP0570
C                                                                 HINP0580
C          XLONG(J) = -XLONG(J)                                         HINP0590
C                                                                 HINP0600
C          SET UP POINTERS IN NTAB AND INITIAL VALUES OF TAB FOR BELT J HINP0610
C          AS WAS DONE FOR OTHER CONTACTS IN SUBROUTINE FINPUT.        HINP0620
C                                                                 HINP0630
C          NTHRNS(J) = NT                                               HINP0640
C          NTAB(NT) = JJ1                                               HINP0650
C          NT = NT+1                                                    HINP0660
C          DO 17 L=1,5                                                  HINP0670
C          NTAB(NT) = 0                                                 HINP0680
C          NX = NFBLT(L,J)                                              HINP0690
C          IF (NX.EQ.0) GO TO 17                                         HINP0700
C          NTAB(NT) = NTI(NX)                                           HINP0710
C          IF (NTI(NX).GT.0) GO TO 17                                    HINP0720
C          WRITE (6,16) NX                                              HINP0730
16 FORMAT('O FUNCTION NO.',I4,' HAS NOT BEEN DEFINED.',              HINP0740
*          ' PROGRAM TERMINATED.')                                       HINP0750
C          STOP                                                         HINP0760
17 NT = NT+1                                                            HINP0770
   JJ2 = JJ1+19                                                         HINP0780
   DO 18 JJ=JJ1,JJ2                                                    HINP0790
18 TAB(JJ) = 0.0                                                        HINP0800
   NX = NTAB(NT-5)                                                     HINP0810
   IF (NX.LT.0) GO TO 19                                               HINP0820
   TAB(JJ1+8) = DABS(TAB(NX+1))                                         HINP0830
   IF (TAB(NX+2).NE.0.0) TAB(JJ1+8) = DABS(TAB(NX+2))                 HINP0840
   TAB(JJ1+10) = EVALFD(TAB(JJ1+8),NX,1)                               HINP0850
   NX = NTAB(NT-4)                                                     HINP0860
   IF (NX.LE.0) GO TO 19                                               HINP0870
   TAB(JJ1+9) = DABS(TAB(NX+1))                                         HINP0880
   IF (TAB(NX+2).NE.0.0) TAB(JJ1+9) = DABS(TAB(NX+2))                 HINP0890
19 JJ1 = JJ2+1                                                         HINP0900
   K2 = K1 + NPTSPB(J) - 1                                             HINP0910
   DO 70 K=K1,K2                                                       HINP0920
C                                                                 HINP0930
C          INPUT CARD F.8.D                                             HINP0940
C                                                                 HINP0950
C          READ (5,21)          (IBAR(L,K),L=1,2),(BAR(L,K),L=1,3)     HINP0960
C          WRITE (6,22) I,J,K,(IBAR(L,K),L=1,2),(BAR(L,K),L=1,3)     HINP0970
21 FORMAT(2I6,3F12.6)                                                 HINP0980
22 FORMAT(I5,I8,I6,2I8,7X,3F10.3)                                       HINP0990
C          DO 23 L=1,3                                                  HINP1000

```

23	BAR(L+3,K) = BAR(L,K)	HINP1010
70	CONTINUE	HINP1020
	K1 = K2+1	HINP1030
80	CONTINUE	HINP1040
	J1 = J2+1	HINP1050
90	CONTINUE	HINP1060
	MXNTB = NT-1	HINP1070
	MXTB2 = JJ1-1	HINP1080
	IF (MXTB2.GT.2000) WRITE (6,62) MXTB2	HINP1090
62	FORMAT('O ERROR IN SUBROUTINE HINPUT, SIZE OF TAB ARRAY =',I8//	HINP1100
	* ' PROGRAM TERMINATED.')	HINP1110
	IF (MXTB2.GT.2000) STOP	HINP1120
99	RETURN	HINP1130
	END	HINP1140

	CALL DAUX(0)	IMPUG510
29	IF (NQ.LE.0) GO TO 31	IMPUG520
	DO 30 J=1,NQ	IMPUG530
	DO 30 I=1,3	IMPUG540
30	V3(I,J) = 0.0	IMPUG550
31	DO 32 J=1,NSEG	IMPUG560
	DO 32 I=1,3	IMPUG570
	U1(I,J) = 0.0	IMPUG580
32	U2(I,J) = 0.0	IMPUG590
	IF (NJNT.LE.0) GO TO 21	IMPUG600
	DO 33 J=1,NJNT	IMPUG610
	DO 33 I=1,3	IMPUG620
	V1(I,J) = 0.0	IMPUG630
33	V2(I,J) = 0.0	IMPUG640
21	IF (NFLX.EQ.0) GO TO 23	IMPUG650
	DO 22 J=1,NFLX	IMPUG660
	DO 22 I=1,3	IMPUG670
22	V4(I,J) = 0.0	IMPUG680
C		IMPUG690
C	REPLACE CALLS TO CONTACT AND VISPR WITH SINGLE CALL	IMPUG700
C	AT FIRST CONTACT IF NOT CONSTRAINT.	IMPUG710
C		IMPUG720
23	IF (I1.NE.1) GO TO 34	IMPUG730
	NT = NTPL(I2,I3)	IMPUG740
	M1 = MPL(1,I2,I3)	IMPUG750
	M2 = MPL(2,I2,I3)	IMPUG760
	M3 = MPL(3,I2,I3)	IMPUG770
	CALL PLELP(M2,M3,M1,I3,NT)	IMPUG780
	IF (NTAB(NT+1).LT.0) GO TO 37	IMPUG790
	K1 = M2	IMPUG800
	K2 = M1	IMPUG810
	GO TO 39	IMPUG820
34	IF (I1.NE.3) GO TO 35	IMPUG830
	NT = NTSEG(I2,I3)	IMPUG840
	M1 = MSEG(1,I2,I3)	IMPUG850
	M2 = MSEG(2,I2,I3)	IMPUG860
	M3 = MSEG(3,I2,I3)	IMPUG870
	CALL SEGSEG(I3,M1,M2,M3,NT)	IMPUG880
	IF (NTAB(NT+1).LT.0) GO TO 37	IMPUG890
	K1 = I3	IMPUG900
	K2 = M2	IMPUG910
	GO TO 39	IMPUG920
35	IF (I1.NE.4) WRITE (6,36) I1,I2,I3	IMPUG930
36	FORMAT('% IMPROPER ARGUMENTS TO SUBROUTINE IMPULS'/	IMPUG940
	* ' ARGUMENTS = ', 3I6 /	IMPUG950
	* ' PROGRAM TERMINATED')	IMPUG960
	IF (I1.NE.4) STOP	IMPUG970
C		IMPUG980
C	RECALL VISPR FOR JOINT STOP.	IMPUG990
C		IMPUG1000

	IF (IABS(IPIN(I3)).NE.4) GO TO 25	IMPU1010
	CALL EJOINT(I2,I3)	IMPU1020
	GO TO 26	IMPU1030
25	CALL VISPR(I2,I3)	IMPU1040
26	K1 = IABS(JNT(I3))	IMPU1050
	K2 = I3+1	IMPU1060
	GO TO 39	IMPU1070
C		IMPU1080
C	SET UP SPECIAL U1,U2 FOR FIRST CONTACT OF CGNSTRANT.	IMPU1090
C		IMPU1100
37	KQ = -NTAB(NT+1)	IMPU1110
	KQTEST = 1	IMPU1120
	KQTYPE(KQ) = -IABS(KQTYPE(KQ))	IMPU1130
	K1 = KQ1(KQ)	IMPU1140
	K2 = KQ2(KQ)	IMPU1150
	IF (K1.GT.NSEG) GO TO 38	IMPU1160
	CALL MAT(A13(1,1,2*KQ-1),QQ(1,KQ),U1(1,K1),3,3,1,3,3,3)	IMPU1170
	CALL MAT(A23(1,1,2*KQ-1),QQ(1,KQ),U2(1,K1),3,3,1,3,3,3)	IMPU1180
38	IF (K2.GT.NSEG) GO TO 39	IMPU1190
	CALL MAT(A13(1,1,2*KQ),QQ(1,KQ),U1(1,K2),3,3,1,3,3,3)	IMPU1200
	CALL MAT(A23(1,1,2*KQ),QQ(1,KQ),U2(1,K2),3,3,1,3,3,3)	IMPU1210
C		IMPU1220
C	FINAL SETUP OF U1 AND U2	IMPU1230
C		IMPU1240
39	DO 40 J=1,NSEG	IMPU1250
	DO 40 I=1,3	IMPU1260
	U1(I,J) = U1(I,J)*RW(J)	IMPU1270
40	U2(I,J) = U2(I,J)*RPHI(I,J)	IMPU1280
	DO 41 I=1,3	IMPU1290
	SEGLA(I,NVEH) = 0.0	IMPU1300
41	WMEGD(I,NVEH) = 0.0	IMPU1310
	CALL DAUX(I)	IMPU1320
	IF (KQTEST.EQ.1) KQTYPE(KQ) = IABS(KQTYPE(KQ))	IMPU1330
	IF (NPRT(10).NE.0) CALL PRINT(6HPREIMP)	IMPU1340
	IF (I1.GT.3) GO TO 51	IMPU1350
	IF (NPRT(10).NE.0) WRITE (6,42) R11,R21	IMPU1360
42	FORMAT ('0'/(6G20.8))	IMPU1370
	CALL CROSS(WMEG (1,K1),R11(1),TEMP)	IMPU1380
	CALL DOT(D(1,1,K1),TEMP,DWR1(1),3,1,3)	IMPU1390
	CALL CROSS(WMEG (1,K2),R21(1),TEMP)	IMPU1400
	CALL DOT(D(1,1,K2),TEMP,DWR2(1),3,1,3)	IMPU1410
	CALL CROSS(WMEGD(1,K1),R1I(1),TEMP)	IMPU1420
	CALL DOT(D(1,1,K1),TEMP,DWR3(1),3,1,3)	IMPU1430
	CALL CROSS(WMEGD(1,K2),R2I(1),TEMP)	IMPU1440
	CALL DOT(D(1,1,K2),TEMP,DWR4(1),3,1,3)	IMPU1450
	TVREL = 0.0	IMPU1460
	TDV = 0.0	IMPU1470
	DO 50 I=1,3	IMPU1480
	VREL(I) = SEGLV(1,K1)+DWR1(I) - SEGLV(I,K2)-DWR2(I)	IMPU1490
	DV (I) = SEGLA(I,K1)+DWR3(I) - SEGLA(I,K2)-DWR4(I)	IMPU1500

	TVREL = TVREL + TTI(I)*VREL(I)	IMPU1510
50	TDV = TDV + TTI(I)*DV (I)	IMPU1520
	GO TO 53	IMPU1530
51	CALL DOT(D(1,1,K1),WMEG (1,K1),DWR1(1),3,1,3)	IMPU1540
	CALL DOT(D(1,1,K2),WMEG (1,K2),DWR2(1),3,1,3)	IMPU1550
	CALL DOT(D(1,1,K1),WMEGD(1,K1),DWR3(1),3,1,3)	IMPU1560
	CALL DOT(D(1,1,K2),WMEGD(1,K2),DWR4(1),3,1,3)	IMPU1570
	TVREL = 0.0	IMPU1580
	TDV = 0.0	IMPU1590
	DO 52 I=1,3	IMPU1600
	VREL(I) = DWR1(I) - DWR2(I)	IMPU1610
	DV (I) = DWR3(I) - DWR4(I)	IMPU1620
	TVREL = TVREL + TTI(I)*VREL(I)	IMPU1630
52	TDV = TDV + TTI(I)*DV (I)	IMPU1640
53	ALPHA = 0.0	IMPU1650
C		IMPU1660
C	NOTE: CREST IS SUPPLIED AS (1+E)/2 WHERE E IS THE CLASSICAL	IMPU1670
C	COEFFICIENT OF RESTITUTION BUT WITH A RANGE OF -1 TO +1.	IMPU1680
C	CREST HAS A RANGE OF 0 TO +1 WHERE 0 (E=-1) REPRESENTS NO IMPULSE.	IMPU1690
C		IMPU1700
	IF (TDV.NE.0.0) ALPHA = -2.0*CREST*TVREL/TDV	IMPU1710
	IF (NPRT(10).NE.0) WRITE (6,42) DWR1,DWR2,DWR3,DWR4,	IMPU1720
	* TT1,VREL,DV,	IMPU1730
	* TVREL,TDV,CREST,ALPHA	IMPU1740
	DO 60 J=1,NSEG	IMPU1750
	DO 60 i=1,3	IMPU1760
	SEGLV(I,J) = SEGLV(I,J) + ALPHA*SEGLA(I,J)	IMPU1770
60	WMEG (I,J) = WMEG (I,J) + ALPHA*WMEGD(I,J)	IMPU1780
	CALL OUTPUT(1)	IMPU1790
	CALL PRINT(6HIMPULS)	IMPU1800
	CALL ELTIME(2,27)	IMPU1810
99	RETURN	IMPU1820
	END	IMPU1830

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SUBROUTINE KINPUT                                     KINP0010
C                                                     REV 12 12/11/74KINP0020
C PERFORMS THE FOLLOWING CARD INPUT AFTER CARDS E.1-E.4 (SUBROUTINE KINP0030
C CINPUT) AND BEFORE CARDS F.I-F.5 (SUBROUTINE FINPUT). KINP0040
C   CARD E.5 - NWINDF: NO. OF WIND FORCE FUNCTIONS ON CARDS E.6 KINP0050
C   - NJNTF : NO. OF JOINT FORCE FUNCTIONS ON CARDS E.7 KINP0060
C   CARDS E.6 - DEFINITIONS OF WIND FORCE FUNCTIONS KINP0070
C   CARDS E.7 - DEFINITIONS OF JOINT RESTORING FORCE FUNCTIONS KINP0080
C                                                     KINP0090
C   IMPLICIT REAL*8(A-H,O-Z) KINP0100
C   COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000) KINP0110
C   COMMON/TEMPVS/JTITL(5,5I),NF(5),NS(3),KTITL(31),TH(50) KINP0120
C NOTE: TEMPVS IS SHARED HERE WITH SUBROUTINES CINPUT AND FINPUT. KINP0130
C REAL BLANK/' ',JTITL,KTITL KINP0140
C COMMON/CNSNTS/ PI, RADIANS,G,THIRD,EPS1,EPS4,EPS6,EPS8, KINP0150
C * EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVITY(3)KINP0160
C                                                     KINP0170
C INPUT CARD E.5 - NWINDF AND NJNTF KINP0180
C                                                     KINP0190
C READ (5,11) NWINDF,NJNTF KINP0200
I1 FORMAT(2I6) KINP0210
   JI = MXTB1+1 KINP0220
   IF (NWINDF.LE.0) GO TO 3I KINP0230
   DO 30 K=I,NWINDF KINP0240
C                                                     KINP0250
C INPUT CARD E.6.A - FUNCTION NO. AND TITLE KINP0260
C                                                     KINP0270
C READ (5,12) I,(KTITL(J),J=1,5) KINP0280
I2 FORMAT(I4,4X,5A4) KINP0290
   WRITE (6,13) I,(KTITL(J),J=1,5),I,J1 KINP0300
I3 FORMAT('1 WIND FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') =', KINP0310
   * I5,43X,'CARDS E.6'//) KINP0320
   IF (I.LE.0.OR.I.GT.50) WRITE (6,I4) KINP0330
I4 FORMAT('0 IMPROPER FUNCTION NO. PROGRAM TERMINATED.') KINP0340
   IF (I.LE.0.OR.I.GT.50) STOP KINP0350
   IF (NTI(I).NE.0) WRITE (6,15) I KINP0360
I5 FORMAT('0 FUNCTION NO.',I4,' HAS ALREADY BEEN INPUTTED AND WILL BE KINP0370
   * REPLACED BY THIS FUNCTION.') KINP0380
   NTI(I) = J1 KINP0390
   DO I6 J=I,5 KINP0400
I6 JTITL(J,I) = KTITL(J) KINP0410
   J2 = JI+4 KINP0420
C                                                     KINP0430
C INPUT CARD E.6.B - DO THRU D4 (FOR NOW A BLANK CARD) KINP0440
C                                                     KINP0450
C READ (5,I7) (TAB(J),J=J1,J2) KINP0460
C WRITE (6,18) (TAB(J),J=J1,J2) KINP0470
I7 FORMAT(6F12.0) KINP0480
I8 FORMAT(10X,'D0',13X,'D1',13X,'D2',13X,'D3',13X,'D4'/5F15.4//) KINP0490
   J1 = J2+1 KINP0500

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C		KINP0510
C	INPUT CARD E.6.C - NTMPTS	KINP0520
C		KINP0530
	READ (5,11) NTMPTS	KINP0540
	WRITE (6,19) NTMPTS	KINP0550
	19 FORMAT('0 WIND FORCE TABLES FOR ',I6,' TIME POINTS.'//	KINP0560
	* 11X,'T',14X,'FX(T)',15X,'FY(T)',15X,'FZ(T)' /)	KINP0570
	TAB(J1) = NTMPTS	KINP0580
	J1 = J1+1	KINP0590
	J2 = J1+4*NTMPTS-1	KINP0600
C		KINP0610
C	INPUT CARDS E.6.D-E.6.N - NTMPTS CARDS OF T,FX(T),FY(T),FZ(T)	KINP0620
C		KINP0630
	READ (5,20) (TAB(J),J=J1,J2)	KINP0640
	WRITE (6,21) (TAB(J),J=J1,J2)	KINP0650
	20 FORMAT(4F12.0)	KINP0660
	21 FORMAT(3X,F12.6,3G20.6)	KINP0670
	J1 = J2+1	KINP0680
	30 CONTINUE	KINP0690
	31 IF (NJNTF.LE.0) GO TO 51	KINP0700
	DO 50 K=1,NJNTF	KINP0710
C		KINP0720
C	INPUT CARD E.7.A - FUNCTION NO. AND TITLE	KINP0730
C		KINP0740
	READ (5,12) I,(KTITLE(J),J=1,5)	KINP0750
	WRITE (6,32) I,(KTITLE(J),J=1,5),I,J1	KINP0760
	32 FORMAT('1 JOINT FORCE FUNCTION NO.',I4,4X,5A4,10X,'NTI(',I2,') =',	KINP0770
	* I5,42X,'CARDS E.7'//)	KINP0780
	IF (I.LE.0.OR.1.GT.50) WRITE (6,14)	KINP0790
	IF (I.LE.0.OR.1.GT.50) STOP	KINP0800
	IF (NTI(I).NE.0) WRITE (6,15) I	KINP0810
	NTI(I) = J1	KINP0820
	DO 33 J=1,5	KINP0830
	33 JTITLE(J,I) = KTITLE(J)	KINP0840
C		KINP0850
C	INPUT CARD E.7.B - D0,D1,D2,D3,D4 (FOR NOW A BLANK CARD).	KINP0860
C		KINP0870
	J2 = J1+4	KINP0880
	READ (5,17) (TAB(J),J=J1,J2)	KINP0890
	WRITE (6,18) (TAB(J),J=J1,J2)	KINP0900
	J1 = J2+1	KINP0910
C		KINP0920
C	INPUT CARD E.7.C - NTHETA,NPHI	KINP0930
C		KINP0940
	READ (5,11) NTHETA,NPHI	KINP0950
	TAB(J1) = NTHETA	KINP0960
	TAB(J1+1) = NPHI	KINP0970
	J1 = J1+2	KINP0980
	IF (NTHETA.LT.0) GO TO 38	KINP0990
	DO 35 J=1,NTHETA	KINP1000


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35 TH(J) = DFLOAT(J-1)*180.0/DFLOAT(NTHETA-1) KINP1010
WRITE (6,36) NTHETA,NPH1,(TH(J),J=2,NTHETA) KINP1020
36 FORMAT('0 FUNCTION IS TABULAR FOR' ,13,' X',13,' VALUES OF THETA AKINP1030
*ND PHI'//30X,'THETA'/5X,'PHI',5X,'THETA0',F16.3,4F20.3/ KINP1040
* (15X,5F20.3)) KINP1050
37 FORMAT(F9.2,F10.3,5G20.7/(19X,5G20.7)) KINP1060
GO TO 40 KINP1070
38 NPOLY = -NTHETA -1 KINP1080
WRITE (6,39) NPOLY,NPH1,(BLANK,J,J=1,NPOLY) KINP1090
39 FORMAT('0 FUNCTION IS COEFFICIENTS OF' ,13,' ORDER POLYNOMIALS IN KINP1100
*(THETA-THETA0) FOR',13,' VALUES OF PHI.'// KINP1110
* 27X,'COEFFICIENTS OF (THETA-THETA0)**N'/ KINP1120
* 5X,'PHI',5X,'THETA0',7X,5(A4,'N =' ,12,11X)/(26X,A4,'N =' ,12,11X,KINP1130
* A4,'N =' ,12,11X,A4,'N =' ,12,11X,A4,'N =' ,12,11X,A4,'N =' ,12) ) KINP1140
40 WRITE (6,21) KINP1150
DO 49 I=1,NPH1 KINP1160
PHIDEG = DFLOAT(I-1)*360.0/DFLOAT(NPH1) - 180.0 KINP1170
C KINP1180
C INPUT CARDS E.7.D - E.7.N NPH1 SETS WITH NTHETA ITEMS PER SET. KINP1190
C EACH SET I IS FOR PHI(I) = -180 +(I-1)*360/NPH1 DEGREES AND KINP1200
C ASSUMES DATA FOR PHI(NPHI+1) = 180 IS SAME AS PHI(I) = -180. KINP1210
C KINP1220
J2 = J1 + IABS(NTHETA) -1 KINP1230
READ (5,17) (TAB(J),J=J1,J2) KINP1240
WRITE (6,37) PHIDEG,(TAB(J),J=J1,J2) KINP1250
IF (NTHETA.LT.0) TAB(J1) = TAB(J1)*RADIAN KINP1260
IF (NTHETA.LT.0) GO TO 49 KINP1270
C KINP1280
C FOR TABULAR DATA, FILL IN ZERO VALUES WITH INTERPOLATED NEGATIVE KINP1290
C VALUES. OVERWRITE VALUE IN FIRST COLUMN (SUPPLIED AS THETA0) WITH KINP1300
C VALUE FOR THETA = 0 AND ALL OTHER ZERO VALUES. KINP1310
C KINP1320
THETA0 = TAB(J1) KINP1330
IF (THETA0.EQ.0.0) GO TO 49 KINP1340
JJ = THETA0*DFLOAT(NTHETA-1)/180.0 + 1.0 + EPS6 KINP1350
JJ1 = J1+JJ KINP1360
IERROR = 0 KINP1370
IF (JJ1.GT.J2) IERROR = 1 KINP1380
IF (TAB(JJ1).LE.0.0) IERROR = 2 KINP1390
IF (IERROR.NE.0) GO TO 46 KINP1400
DO 45 J=1,JJ KINP1410
J1J = J1+J-1 KINP1420
IF (J.NE.1.AND.TAB(J1J).GT.0.0) IERROR = 3 KINP1430
45 TAB(J1J) = TAB(JJ1)*(TH(J)-THETA0)/(TH(JJ+1)-THETA0) KINP1440
46 IF (IERROR.NE.0) WRITE (6,47) IERROR KINP1450
47 FORMAT('0 INPUT ERROR. INCONSISTENT VALUE OF THETA0. IERROR =' ,12,KINP1460
* ' PROGRAM TERMINATED.') KINP1470
IF (IERROR.NE.0) STOP KINP1480
49 J1 = J2+1 KINP1490
50 CONTINUE KINP1500

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51 MXTB1 = J1-1
RETURN
END

KINP1510
KINP1520
KINP1530

C	LINES = LINES+1	OUTPUT510
	IF (MOD(LINES,LPP).NE.1) GO TO 51	OUTPUT520
	CALL HEDING(LINES,LPP,MPSF,MBSF,MSSF)	OUTPUT530
C		OUTPUT540
C	PRINT LINE OF DATA FOR THIS TIME POINT ON EACH OUTPUT UNIT (NT).	OUTPUT550
C		OUTPUT560
	51 USEC = 1000.0*TIME	OUTPUT570
	NT = 2L	OUTPUT580
C		OUTPUT590
C	COMPUTE AND PRINT DATA FOR 7 TYPES OF OUTPUT ABOVE	OUTPUT600
C		OUTPUT610
	DO 68 K=1,7	OUTPUT620
	IF (NSG(K).LE.0) GO TO 68	OUTPUT630
	KSG = NSG(K)	OUTPUT640
	J3 = 3	OUTPUT650
	IF (K.EQ.7) J3 = 2	OUTPUT660
	DO 67 J1=1,KSG,J3	OUTPUT670
	J2 = MIN0(J1+J3-1,KSG)	OUTPUT680
	NT = NT+1	OUTPUT690
	DO 66 J=J1,J2	OUTPUT700
	L = MSG(J,K)	OUTPUT710
	GO TO (52,54,56,59,61,64,65),K	OUTPUT720
C		OUTPUT730
C	1. SEGMENT LINEAR ACCELERATIONS IN LOCAL REFERENCE	OUTPUT740
C		OUTPUT750
	52 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)	OUTPUT760
	CALL CROSS (WMEG(1,L),T1,T2)	OUTPUT770
	CALL CROSS (WMEGD(1,L),XSG(1,J,K),T3)	OUTPUT780
	CALL MAT(D(1,1,L),SEGLA(1,L),T4,3,3,1,3,3,3)	OUTPUT790
	DO 53 I=1,3	OUTPUT800
	53 ACC(I,J) = (T4(I)+T3(I)+T2(I))/G	OUTPUT810
	GO TO 63	OUTPUT820
C		OUTPUT830
C	2. SEGMENT LINEAR VELOCITIES IN VEHICLE REFERENCE	OUTPUT840
C		OUTPUT850
	54 CALL CROSS (WMEG(1,L),XSG(1,J,K),T1)	OUTPUT860
	CALL DOT(D(1,1,L),T1,T2,3,1,3)	OUTPUT870
	DO 55 I=1,3	OUTPUT880
	55 T3(I) = SEGLV(I,L)+T2(I)-XVCOMP(I)	OUTPUT890
	GO TO 58	OUTPUT900
C		OUTPUT910
C	3. SEGMENT LINEAR DISPLACEMENTS IN VEHICLE REFERENCE	OUTPUT920
C		OUTPUT930
	56 CALL DOT(D(1,1,L),XSG(1,J,K),T1,3,1,3)	OUTPUT940
	DO 57 I=1,3	OUTPUT950
	57 T3(I) = SEGLP(I,L)+T1(I)-XCOMP(I)	OUTPUT960
	58 CALL MAT (DVEH,T3,ACC(1,J),3,3,1,3,3,6)	OUTPUT970
	GO TO 63	OUTPUT980
C		OUTPUT990
		OUTPUT1000

C	4. SEGMENT ANGULAR ACCELERATIONS IN LOCAL REFERENCE	OUTP1010
C		OUTP1020
	59 DO 60 I=1,3	OUTP1030
	60 ACC(I,J) = WMEGD(I,L)/(2.0*PI)	OUTP1040
	GO TO 63	OUTP1050
C		OUTP1060
C	5. SEGMENT ANGULAR VELOCITIES IN VEHICLE REFERENCE	OUTP1070
C		OUTP1080
	61 CALL DOT (D(1,1,L),WMEG(1,L),T1,3,1,3)	OUTP1090
	CALL MAT (DVEH,T1,T2,3,3,1,3,3,3)	OUTP1100
	DO 62 I=1,3	OUTP1110
	62 ACC(I,J) = (T2(I)-VMEG(I))/(2.0*PI)	OUTP1120
	63 ACC(4,J) = DSQRT(ACC(1,J)**2+ACC(2,J)**2+ACC(3,J)**2)	OUTP1130
	GO TO 66	OUTP1140
C		OUTP1150
C	6. SEGMENT ANGULAR DISPLACEMENTS IN VEHICLE REFERENCE	OUTP1160
C		OUTP1170
	64 CALL DOT (D(1,1,L),DVEH,T1,3,3,3)	OUTP1180
	CALL YPRDEG(T1,ACC(1,J))	OUTP1190
	TRACE = 0.5*(T1(1)+T2(2)+T3(3)-1.0)	OUTP1200
	IF (TRACE.GT. 1.0) TRACE = 1.0	OUTP1210
	IF (TRACE.LT.-1.0) TRACE = -1.0	OUTP1220
	ACC(4,J) = DARCOS(TRACE)/RADIAN	OUTP1230
	GO TO 66	OUTP1240
C		OUTP1250
C	7. JOINT PARAMETERS	OUTP1260
C		OUTP1270
	65 ACC(1,J) = PRJNT(1,L)/RADIAN	OUTP1280
	ACC(2,J) = PRJNT(2,L)/RADIAN	OUTP1290
	ACC(3,J) = PRJNT(3,L)	OUTP1300
	ACC(4,J) = PRJNT(4,L)	OUTP1310
	ACC(5,J) = PRJNT(5,L)	OUTP1320
	ACC(6,J) = PRJNT(6,L)	OUTP1330
	66 CONTINUE	OUTP1340
	IF (K.LE.6) WRITE (NT,121) USEC,((ACC(I,J),I=1,4),J=J1,J2)	OUTP1350
	121 FORMAT(F9.3,3(3X,4F9.2))	OUTP1360
	67 IF (K.EQ.7) WRITE (NT,123) USEC,((ACC(I,J),I=1,6),J=J1,J2)	OUTP1370
	123 FORMAT(F9.3,2(2X,0P2F7.2,1P4D11.4))	OUTP1380
	68 CONTINUE	OUTP1390
C		OUTP1400
C	PRINT PLANE FORCES	OUTP1410
C		OUTP1420
	IF (MPSF.EQ.0) GO TO 77	OUTP1430
	DO 76 J1=1,MPSF,2	OUTP1440
	J2 = MIN0(J1+1,MPSF)	OUTP1450
	NT = NT+1	OUTP1460
	76 WRITE (NT,129) USEC,((PSF(I,J),I=1,7),J=J1,J2)	OUTP1470
	129 FORMAT(F9.3,2(F9.3,3F9.2,3F8.2))	OUTP1480
C		OUTP1490
C	PRINT BELT FORCES	OUTP1500

C	77 IF (MBSF.EQ.0) GO TO 79	OUTP1510
	DO 78 J1=1,MBSF,2	OUTP1520
	J2 = MINO(J1+1,MBSF)	OUTP1530
	NT = NT+1	OUTP1540
	78 WRITE (NT,135) USEC,((BSF(I,J),I=1,4),J=J1,J2)	OUTP1550
	135 FORMAT(F9.3,4(F15.6,F12.2,3X))	OUTP1560
C		OUTP1570
C	PRINT SEGMENT CONTACT FORCES	OUTP1580
C		OUTP1590
	79 IF (MSSF.EQ.0) GO TO 81	OUTP1600
	DO 80 J=1,MSSF	OUTP1610
	NT = NT+1	OUTP1620
	80 WRITE (NT,37) USEC,((SSF(I,J),I=1,10)	OUTP1630
	37 FORMAT(2F9.3,3F9.2,3F8.2,2X,3F8.2)	OUTP1640
C		OUTP1650
C	PRINT AIRBAG FORCES	OUTP1660
C		OUTP1670
	81 IF (NBAG.EQ.0) GO TO 91	OUTP1680
	K1 = 1	OUTP1690
	DO 83 J=1,NBAG	OUTP1700
	IF (MNBAG(J).EQ.0) GO TO 83	OUTP1710
	KBAG = MNBAG(J)+NPANEL(J)+5	OUTP1720
	DO 82 J1=1,KBAG,4	OUTP1730
	J2 = MINO(J1+3,KBAG)	OUTP1740
	K2 = K1+J2-J1	OUTP1750
	NT = NT+1	OUTP1760
	WRITE (NT,21) USEC,((BAGSF(I,K),I=1,3),K=K1,K2)	OUTP1770
	21 FORMAT(F9.3,4(3X,3F9.2))	OUTP1780
	82 K1 = K2+1	OUTP1790
	83 CONTINUE	OUTP1800
	91 CONTINUE	OUTP1810
C		OUTP1820
	CALL ELTIME(2,8)	OUTP1830
	RETURN	OUTP1840
	END	OUTP1850
		OUTP1860

	SUBROUTINE PLELP(M,MM,N,NN,NT)	PLEL0010
		REV 12 11/25/74
C	COMPUTES FORCES (WHICH ARE ADDED TO U1 ARRAY)	PLEL0020
C	AND TORQUES (WHICH ARE ADDED TO U2 ARRAY)	PLEL0030
C	OF ELLIPSOID (MM) ATTACHED TO BODY SEGMENT (M)	PLEL0040
C	INTERSECTING PLANE (NN) ATTACHED TO SEGMENT (N).	PLEL0050
C		PLEL0060
	IMPLICIT REAL *8(A-H,O-Z)	PLEL0070
	COMMON/TABLES/MXNT1,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)	PLEL0080
	COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)	PLEL0090
	*,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)	PLEL0100
	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),	PLEL0110
	* NPSF,NBSF,NSSF,NBSGF,NPANEL(6),PRJNT(6,21)	PLEL0120
	COMMON/CNTRSF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)	PLEL0130
	COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),B31(3,3,24),B32(3,3,24)	PLEL0140
	*,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12)	PLEL0150
	* ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)	PLEL0160
	* ,NQ,KQ1(12),KQ2(12),KQTYPE(12)	PLEL0170
	COMMON/TEMPVS/DMNT(3,3),TEMP(3,3),B(3,3),XMN(3),RLN(3),XMM(3),	PLEL0180
	* TM(3),R(3),RM(3),DMNWN(3),RLM(3),RN(3),VMN(3),VR(3),	PLEL0190
	* WMN(3),WCM(3),WCN(3),VREL(3),FFM(3),FR(3),TQM(3),	PLEL0200
	* TQN(3),TQNT(3),T(3),H(3),T1(3),T2(3),RMD(3),RND(3),	PLEL0210
	* TD(3),TT4(3,4),TT5(3,4),T3(3),T4(3),P,AMR,FM,CF,	PLEL0220
	* VRT,VRTS,TF,MCF,NCF	PLEL0230
	CALL ELTIME(1,21)	PLEL0240
		PLEL0250
C	COMPUTE PENETRATION DISTANCE, IF NEGATIVE, RETURN.	PLEL0260
C		PLEL0270
C	CALL DOT(D(1,1,M),D(1,1,N),DMNT,3,3,3)	PLEL0280
	DO 10 I=1,3	PLEL0290
	10 XMN(I) = SEGLP(I,M) - SEGLP(I,N)	PLEL0300
	CALL MAT(D(1,1,M),XMN,XMM,3,3,1,3,3,3)	PLEL0310
	CALL MAT(DMNT,PL(1,NN),TM,3,3,1,3,3,3)	PLEL0320
	BET = PL(4,NN)	PLEL0330
	DO 11 I=1,3	PLEL0340
	11 BET = BET - TM(I)*(BD(I+3,MM)+XMM(I))	PLEL0350
	CALL MAT(BD(16,MM),TM,RM,3,3,1,3,3,3)	PLEL0360
	BTS = TM(1)*RM(1) + TM(2)*RM(2) + TM(3)*RM(3)	PLEL0370
	BTE = -DSQRT(BTS)	PLEL0380
	P = BET - BTE	PLEL0390
	MCF = NTAB(NT+1)	PLEL0400
	NCF = -MCF	PLEL0410
	IF (NCF.GT.0) CFQQ(NCF) = -999.	PLEL0420
	IF (P.LE.0.0) GO TO 99	PLEL0430
C		PLEL0440
C	IF COMPLETE PENETRATION, RETURN	PLEL0450
C		PLEL0460
C	IF (BET+BTE.GT.0.0) GO TO 99	PLEL0470
C		PLEL0480
C	COMPUTE TG - THE POINT IN SEGMENT REFERENCE AT WHICH THE CONTACT	PLEL0490
C		PLEL0500


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C          FORCES ARE TO BE APPLIED WHICH LIES ON THE SCALED PLEL0510
C          LINE BETWEEN THE POINT OF MAXIMUM PENETRATION (RHO=0) PLEL0520
C          AND THE CENTER OF THE INTERSECTION ELLIPSE (RHO=1). PLEL0530
C          AND TEMP - THE SAME POINT IN VEHICLE REFERENCE. PLEL0540
C PLEL0550
RHO = 0.0 PLEL0560
IF (MCF.GT.0) RHO = TAB(MCF+4) PLEL0570
BETE = (1.0+RHO*P/BTE)/BTE PLEL0580
AMR = -1.0/BTE PLEL0590
DO 13 I=1,3 PLEL0600
RM(I) = BETE*RM(I) PLEL0610
RLM(I) = RM(I) + BD(I+3,MM) PLEL0620
13 RN(I) = RLM(I) + XMM(I) PLEL0630
CALL DOT(DMNT,RN,RLN,3,1,3) PLEL0640
C PLEL0650
C IF BOUNDARY PLANE IS GIVEN, COMPUTE DISTANCE FROM POINT TO PLANE, PLEL0660
C IF NEGATIVE OR > LIMIT, RETURN. PLEL0670
C PLEL0680
DO 14 I=8,13,5 PLEL0690
IF (PL(I+4,NN).LE.0.0) GO TO 14 PLEL0700
DIST = RLN(1)*PL(I,NN) PLEL0710
* + RLN(2)*PL(I+1,NN) PLEL0720
* + RLN(3)*PL(I+2,NN) - PL(I+3,NN) PLEL0730
IF (DIST.LE.0.0 .OR. DIST.GT.PL(I+4,NN)) GO TO 99 PLEL0740
14 CONTINUE PLEL0750
CALL PLSEGF(M,N,NT) PLEL0760
IF (MCF.LT.0) GO TO 30 PLEL0770
C PLEL0780
C STORE RESULTS FOR OUTPUT ROUTINE. PLEL0790
C PLEL0800
PSF(1,NPSF) = P PLEL0810
PSF(2,NPSF) = FM PLEL0820
PSF(3,NPSF) = FM*CF PLEL0830
IF (VRT.EQ.1.0) PSF(3,NPSF) = FM*CF*VRTS PLEL0840
PSF(4,NPSF) = TF PLEL0850
DO 24 I=1,3 PLEL0860
24 PSF(I+4,NPSF) = RLN(I) PLEL0870
GO TO 99 PLEL0880
30 PSF(1,NPSF) = P PLEL0890
DO 31 I=1,3 PLEL0900
PSF(I+1,NPSF) = T(I) PLEL0910
31 PSF(I+4,NPSF) = RLN(I) PLEL0920
CALL CROSS(WMN,TM,T1) PLEL0930
CALL MAT(BD(16,MM),T1,T2,3,3,1,3,3,3) PLEL0940
TMT = TM(1)*T2(1) + TM(2)*T2(2) + TM(3)*T2(3) PLEL0950
TMT = TMT/BTE PLEL0960
DO 32 I=1,3 PLEL0970
32 RMD(I) = (T2(I)-TMT*RM(I))*BETE PLEL0980
CALL CROSS(DMNWN,VREL,T1) PLEL0990
CALL CROSS(WMN,RMD,T3) PLEL1000

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CALL DOT(D(1,1,M),T3,RQQ(1,NCF),3,1,3)
SQQ(NCF) = 0.0
DO 36 I=1,3
36 SQQ(NCF) = SQQ(NCF) + TM(I)*(T3(I)+2.0*T1(I))
99 CALL ELTIME(2,21)
RETURN
END
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PLEL1010
PLEL1020
PLEL1030
PLEL1040
PLEL1050
PLEL1060
PLEL1070
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SUBROUTINE RSTART(IF,IT)
C
C THE FIVE FUNCTIONS OF SUBROUTINE RSTART ARE:
C   1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.
C   2. WRITE INPUT & INITIALIZATION RECORD UNTO NEW RESTART TAPE.
C   3. READ TIME POINT RECORD FROM OLD RESTART TAPE.
C   4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.
C   5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.
C
C IMPLICIT REAL*8(A-H,O-Z)
C
C ALL LABELED COMMON BLOCKS ARE INCLUDED HERE
C TO GIVE A COMPLETE SET FOR REFERENCE
C 1
COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
DIMENSION IC1(49)
EQUIVALENCE (IC1(1),NSEG)
C 2
COMMON/CNTRF/ PL(17,20),GAB(8,3),BELT(20,8),TPTS(6,8),BD(24,25)
DIMENSION RC2(1172)
EQUIVALENCE (RC2(1),PL(1,1))
C 3
COMMON/VPOSTN/ TIME,X0(3),XDOTO(3),XCOMP(3),XVCOMP(3),AX(3),
* ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,
* NATAB,NACLR,DVEH(3,3),VMEG(3),VMEGD(3),XACOMP(3),
* THET(3),ZPLT(3)
DIMENSION RC3(1527),RC3A(1511),IC3(2),RC3B(18)
EQUIVALENCE (RC3(1),TIME),(RC3A(1),AX(1)),
* (IC3(1),NATAB),(RC3B(1),DVEH(1,1))
C 4
COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
* ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
DIMENSION RC4(660)
EQUIVALENCE (RC4(1),D(1,1,1))
C 5
COMMON/CMATRX/V1(3,21),V2(3,21),V3(3,12),B12(3,3,42),A22(3,3,42)
* ,F(3,21),TQ(3,21),WJ(21)
DIMENSION RC5A(918),RC5B(147)
EQUIVALENCE (RC5A(1),V1(1,1)),(RC5B(1),F(1,1))
C 6
COMMON /ABDATA/ ABC(3,5), ZA(3,5), DA(3,3,5), BFA(3,5)
* ,BCGV(3,5),BMEG(3,5)
DIMENSION RC6(120)
EQUIVALENCE (RC6(1),ABC(1,1))
C 7
COMMON/TITLES/ DATE(3),COMENT(40),VPSTTL(20),BDYTTL(5),BLTTTL(5,8)
* ,PLTTL(5,20),BAGTTL(5,6),SEG(22),JOINT(21)
* ,CGS(21),JS(21)
REAL DATE,COMENT,VPSTTL,BDYTTL,BLTTTL,PLTTL,BAGTTL,SEG,JOINT
LOGICAL*1 CGS,JS

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RSTA0010
REV 12 12/19/74RSTA0020
RSTA0030
RSTA0040
RSTA0050
RSTA0060
RSTA0070
RSTA0080
RSTA0090
RSTA0100
RSTA0110
RSTA0120
RSTA0130
RSTA0140
RSTA0150
RSTA0160
RSTA0170
RSTA0180
RSTA0190
RSTA0200
RSTA0210
RSTA0220
RSTA0230
RSTA0240
RSTA0250
RSTA0260
RSTA0270
RSTA0280
RSTA0290
RSTA0300
RSTA0310
RSTA0320
RSTA0330
RSTA0340
RSTA0350
RSTA0360
RSTA0370
RSTA0380
RSTA0390
RSTA0400
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RSTA0420
RSTA0430
RSTA0440
RSTA0450
RSTA0460
RSTA0470
RSTA0480
RSTA0490
RSTA0500

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	REAL RC7,RC7A,XDTE,XCMENT	RSTA0510
	DIMENSION RC7(238),RC7A(281),XDTE(3),XCMENT(40)	RSTA0520
	EQUIVALENCE (RC7(1),VPSTTL(1)),(RC7A(1),DATE(1))	RSTA0530
C 8	COMMON/CNSNTS/ PI, RADIANG,THIRD, EPS1, EPS4, EPS6, EPS8,	RSTA0540
	* EPS12, EPS15, EPS20, EPS24, UNITL, UNITM, UNITT, GRAVITY(3)	RSTA0550
	DIMENSION RC8(18)	RSTA0560
	EQUIVALENCE (RC8(1),PI)	RSTA0570
C 9	COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)	RSTA0580
	* ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)	RSTA0590
	* ,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22)	RSTA0600
	* ,IGLOB(21),JOINTF(21)	RSTA0610
	DIMENSION RC9(1688),IC9(107)	RSTA0620
	EQUIVALENCE (RC9(1),PHI(1,1)),(IC9(1),JNT(1))	RSTA0630
C 10	COMMON/JBARTZ/ MNPL(20),MN8LT(8),MNSEG(22),MN8AG(6),	RSTA0640
	* MPL(3,5,20),M8LT(3,5,8),MSEG(3,5,22),MBAG(3,10,6),	RSTA0650
	* NTPL(5,20),NT8LT(5,8),NTSEG(5,22)	RSTA0660
	DIMENSION IC10(1236)	RSTA0670
	EQUIVALENCE (IC10(1),MNPL(1))	RSTA0680
C 11	COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),	RSTA0690
	* NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)	RSTA0700
	DIMENSION RC11(480),IC11(4),RC11A(126)	RSTA0710
	EQUIVALENCE (RC11(1),PSF(1,1)),(IC11(1),NPSF),	RSTA0720
	* (RC11A(1),PRJNT(1,1))	RSTA0730
C 12	COMMON/INTEST/ SGTEST(3,4,22),XTEST(3,88)	RSTA0740
	DIMENSION RC12(528)	RSTA0750
	EQUIVALENCE (RC12(1),SGTEST(1,1,1))	RSTA0760
C 13	COMMON/CSTRNT/A13(3,3,24),A23(3,3,24),831(3,3,24),B32(3,3,24)	RSTA0770
	* ,HHT(3,3,12),RK1(3,12),RK2(3,12),QQ(3,12),TQQ(3,12)	RSTA0780
	* ,RQQ(3,12),HQQ(3,12),SQQ(12),CFQQ(12)	RSTA0790
	* ,NQ,KQ1(12),KQ2(12),KQTYPE(12)	RSTA0800
	DIMENSION RC13(72),IC13(37),RC13A(1212),RC13H(348)	RSTA0810
	EQUIVALENCE (RC13(1),RK1(1,1)),(IC13(1),NQ),(RC13A(1),A13(1,1,1))	RSTA0820
	* ,(RC13H(1),HHT(1,1,1))	RSTA0830
C 14	COMMON/TABLES/MXNTI,MXNTB,MXT81,MXT82,NTI(50),NTA8(500),TAB(2000)	RSTA0840
	DIMENSION IC14(554)	RSTA0850
	EQUIVALENCE (IC14(1),MXNTI)	RSTA0860
C 15	COMMON/COMAIN/VAR(120),DER(120),DT,HC,HMAX,HMIN,RSTIME,	RSTA0870
	* ISTEP,NSTEPS,NDINT,NEQ,IRSI,IRSOUT	RSTA0880
	DIMENSION RC15(245),IC15(6)	RSTA0890
	EQUIVALENCE (RC15(1),VAR(1)),(IC15(1),ISTEP)	RSTA0900
C 16	COMMON/CDINT/ E(3,120),FF(5,120),GG(5,120),Y(5,120),U(5,120)	RSTA0910
		RSTA0920
		RSTA0930
		RSTA0940
		RSTA0950
		RSTA0960
		RSTA0970
		RSTA0980
		RSTA0990
		RSTA1000

	* ,H,HPRINT,TSAVE,TPRINT,TSTART,ICNT,IDBL,IFLAG	RSTA1010
C	NOTE: FF REPLACES F FROM SUBROUTINE DINT.	RSTA1020
	DIMENSION RC16(2765),IC16(3)	RSTA1030
	EQUIVALENCE (RC16(1),E(1,1)),(IC16(1),ICNT)	RSTA1040
C 17	COMMON/DAMPER/APSDM(3,20),APSON(3,20),ASD(5,20),	RSTA1050
	* NSO,MSDM(20),MSON(20)	RSTA1060
	DIMENSION RC17(220),IC17(41)	RSTA1070
	EQUIVALENCE (RC17(1),APSDM(1,1)),(IC17(1),NSO)	RSTA1080
C 18	COMMON/CEULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGO(3,21),	RSTA1090
	* FE(3,21),TQE(3,21),CONST(3,21)	RSTA1100
	DIMENSION RC18(504)	RSTA1110
	EQUIVALENCE (RC18(1),HIR(1,1,1))	RSTA1120
C 19	COMMON/TEMPVI/ TT1(3),R11(3),R2I(3),CREST,JSTOP(4,2,21)	RSTA1130
	DIMENSION RC19(10),IC19(168)	RSTA1140
	EQUIVALENCE (RC19(1),TTI(1)),(IC19(1),JSTOP(1,1,1))	RSTA1150
C 20	COMMON /WJONES/	RSTA1160
	* FORCE(3,5),TORA(3,5),XBM(5),ZOE(3,5),VBAGG(5),VSCS(5),	RSTA1170
	* BPHI(3,5),DBR(3,3,5),DPVCTR(3,5),DEPLOY(3,5),AB(3,5),SPRK(5),	RSTA1180
	* CYTD(5),CYP(5),CYSP(5),CYT0(5),	RSTA1190
	* CYVO(5),CYCO(5),CYK(5),CYR(5),CYAT(5),CYPV(5),CYCDO(5),	RSTA1200
	* CYAO(5),CYP0(5),CYSS(5),CYLO(5),CYC(5),CYRHO(5),CYVMAX(5),	RSTA1210
	* CYORFC(5),CYRHO(5),CYT(5),CYP(5),CYMIN(5),CYMOUT(5),	RSTA1220
	* BAGPV(5),PD(5),VBAG(5),VOLBP(5),SWITCH(5),1FULL(6),	RSTA1230
	* TMP(18),TMP1(3),A(3,3),PF(3),TORQ(3),	RSTA1240
	* TQB(3,10),FRB(3,10),VOL(10),OELF(3),	RSTA1250
	* B(9,4,5),ZB(3,4,5),ZR(3,4,5),BFB(9,4,5),DRR(9,4,5),	RSTA1260
	* DB(9,4,5),PCGV(3,4,5),PMEG(3,4,5),VOLP(4,5),FRA(3,4),PREVT	RSTA1270
	* ,CK(5),CMASS(5)	RSTA1280
	DIMENSION RC20A(30),RC20B(235),RC20C(50),RC20D(109),RC20E(180),	RSTA1290
	* RC20F(60),RC20G(420),RC20H(320),RC20I(10)	RSTA1300
	EQUIVALENCE (RC20A(1),FORCE(1,1)),(RC20B(1),XBM(1)),	RSTA1310
	* (RC20C(1),CYRHO(1)),(RC20D(1),TMP(1)),	RSTA1320
	* (RC20E(1),B(1,1,1)),(RC20F(1),ZB(1,1,1)),	RSTA1330
	* (RC20G(1),ZR(1,1,1)),(RC20H(1),DB(1,1,1)),	RSTA1340
	* (RC20I(1),CK(1))	RSTA1350
C 21	COMMON/RSAVE/ XSG(3,20,3),NSG(7),MSG(20,7)	RSTA1360
	DIMENSION RC21(180),IC21(147)	RSTA1370
	EQUIVALENCE (RC21(1),XSG(1,1,1)),(IC21(1),NSG(1))	RSTA1380
C 22	COMMON/FLXBLE/ HF(4,12,8),B42(3,3,24),V4(3,8),NFLEX(3,8),NFLX	RSTA1390
	DIMENSION RC22(624),IC22(25)	RSTA1400
	EQUIVALENCE (RC22(1),HF(1,1,1)),(IC22(1),NFLEX(1,1))	RSTA1410
C 23	COMMON/HRNESS/ BAR(6,100),XLONG(20),IBAR(2,100),NTHRNS(20),	RSTA1420
	* NHRNSS, NBLTPH(5),NFB(5,20),NPTSPB(20)	RSTA1430
		RSTA1440
		RSTA1450
		RSTA1460
		RSTA1470
		RSTA1480
		RSTA1490
		RSTA1500

	DIMENSION RC23(620) , IC23(346)	RSTA1510
	EQUIVALENCE (RC23(1),BAR(1,1)) , (IC23(1),IBAR(1,1))	RSTA1520
C 24	COMMON/KALEPS/ WTIME(30),IWIND(30),MWSEG(5,22)	RSTA1530
	DIMENSION RC24(30) , IC24(140)	RSTA1540
	EQUIVALENCE (RC24(1),WTIME(1)) , (IC24(1),IWIND(1))	RSTA1550
C	DIMENSION COMMON(24)	RSTA1560
	DATA COMMON /8HCONTRL ,8HCNTRSRF ,8HVPOSTN ,8HSGMNTS ,	RSTA1570
	* 8HCMATRIX ,8HABDATA ,8HTITLES ,8HCNSNTS ,	RSTA1580
	* 8HDESCRP ,8HJBARTZ ,8HFORCES ,8HINTEST ,	RSTA1590
	* 8HCSTRNT ,8HTABLES ,8HCOMAIN ,8HCDINT ,	RSTA1600
	* 8HDAMPER ,8HCEULER ,8HTEMPVI ,8HWJONES ,	RSTA1610
	* 8HRSAVE ,8HFLXBLE ,8HHRNESS ,8HKALEPS /	RSTA1620
	REAL AOLD4,AAOLD4	RSTA1630
	DATA BLANK/8H /	RSTA1640
	DIMENSION INDEX(3)	RSTA1650
	CALL ELTIME(1,25)	RSTA1660
	GO TO (100,200,300,400,500),IF	RSTA1670
C		RSTA1680
C	1. READ INPUT & INITIALIZATION RECORD FROM OLD RESTART TAPE.	RSTA1690
C		RSTA1700
	100 READ (IT) IC1,PL,BD,X0,XDOT0,RC3A,NATAB,ZPLT,NSYM,XDTE,XCMNT,	RSTA1710
	* RC7,CGS,JS,RC8,RC9,JNT,IC10,NPANEL,SGTEST,RC13,IC13,	RSTA1720
	* IC14,DT,HC,HMAX,HMIN,NSTEPS,NDINT,RC17,IC17,IEULER,	RSTA1730
	* RC20B,IFULL,RC20E,RC20G,RC20I,RC21,IC21,NS,ISING	RSTA1740
	* ,HF,NFLEX,NFLX,IC19,IGLOB,JOINTF,RC23,IC23,RC24,IC24	RSTA1750
	WRITE (6,I01) IT,XDTE,XCMNT	RSTA1760
	101 FORMAT('0 INPUT DATA HAS BEEN READ IN FROM UNIT NO.',I4//	RSTA1770
	* 10X,3A4//10X,20A4/10X,20A4)	RSTA1780
	GO TO 999	RSTA1790
C		RSTA1800
C	2. WRITE INPUT & INITIALIZATION RECORD ONTO NEW RESTART TAPE.	RSTA1810
C		RSTA1820
	200 WRITE (IT) IC1,PL,BD,X0,XDOT0,RC3A,NATAB,ZPLT,NSYM,DATE,COMENT,	RSTA1830
	* RC7,CGS,JS,RC8,RC9,JNT,IC10,NPANEL,SGTEST,RC13,IC13,	RSTA1840
	* IC14,DT,HC,HMAX,HMIN,NSTEPS,NDINT,RC17,IC17,IEULER,	RSTA1850
	* RC20B,IFULL,RC20E,RC20G,RC20I,RC21,IC21,NS,ISING	RSTA1860
	* ,HF,NFLEX,NFLX,IC19,IGLOB,JOINTF,RC23,IC23,RC24,IC24	RSTA1870
	GO TO 999	RSTA1880
		RSTA1890
C		RSTA1900
C	3. READ TIME POINT RECORD FROM OLD RESTART TAPE.	RSTA1910
C		RSTA1920
	300 READ (IT) TIME,BELT,TPTS,XCOMP,XVCOMP,RC3B,RC4,RC5B,RC6,IPIN,RC11	RSTA1930
	* ,IC11,PRJNT,TAB,RC16,IC16,RC20A,RC20C,IFULL,RC20H,PREVTR	RSTA1940
	* ,RC21,IC21,VAR,DER,NEQ,XTEST,V4,ICI9,RC13H,KQTYPE	RSTA1950
	* ,IEULER,RC23,WTIME,IWIND	RSTA1960
	CALL OUTPUT(1)	RSTA1970
	GO TO 999	RSTA1980
C		RSTA1990
		RSTA2000

C	5. WRITE TIME POINT RECORD ONTO NEW RESTART TAPE.	RSTA2010
C		RSTA2020
	500 WRITE (IT) TIME,BELT,TPTS,XCOMP,XVCOMP,RC3B,RC4,RC5B,RC6,IPIN,RC11	RSTA2030
	* ,IC11,PRJNT,TAB,RC16,IC16,RC20A,RC20C,IFULL,RC20H,PREVTR	RSTA2040
	* ,RC21,IC21,VAR,DER,NEQ,XTEST,V4,IC19,RC13H,KQTYPE	RSTA2050
	* ,IEULER,RC23,WTIME,IWIND	RSTA2060
	GO TO 999	RSTA2070
C		RSTA2080
C	4. READ NEW INPUT DATA FROM INPUT STREAM FOR RESTART.	RSTA2090
C		RSTA2100
	400 READ (5,401) AVAR,INDEX,ITYPE,RR,II,AA,RROLD,IIOLD,AAOLD	RSTA2110
	401 FORMAT(A8,4I4,2(F8.0,I8,A8))	RSTA2120
	CALL SEARCH(AVAR,INDEX,NCOM,ITEM)	RSTA2130
	IF (NCOM.LE.0) GO TO 490	RSTA2140
	IF (NCOM.GT.24) GO TO 999	RSTA2150
	IF (ITYPE.GT.3) GO TO 490	RSTA2160
	GO TO (1, 2, 3, 4, 5, 6, 7, 8, 9,10,11,12,	RSTA2170
	* 13,14,15,16,17,18,19,20,21,22,23,24),NCOM	RSTA2180
C	COMMON /CONTRL/	RSTA2190
	1 IF (ITEM.GT.49) GO TO 490	RSTA2200
	IF (ITYPE.NE.2) GO TO 490	RSTA2210
	IOLD = IC1(ITEM)	RSTA2220
	IC1(ITEM) = II	RSTA2230
	GO TO 494	RSTA2240
C	COMMON /CNTSRF/	RSTA2250
	2 IF (ITEM.GT.1172) GO TO 490	RSTA2260
	IF (ITYPE.NE.1) GO TO 490	RSTA2270
	ROLD = RC2(ITEM)	RSTA2280
	RC2(ITEM) = RR	RSTA2290
	GO TO 492	RSTA2300
C	COMMON /VPOSTN/	RSTA2310
	3 IF (ITEM.GT.1527) GO TO 402	RSTA2320
	IF (NTYPE.NE.1) GO TO 490	RSTA2330
	ROLD = RC3(ITEM)	RSTA2340
	RC3(ITEM) = RR	RSTA2350
	GO TO 492	RSTA2360
	402 IF (ITEM.GT.1529) GO TO 403	RSTA2370
	IF (NTYPE.NE.2) GO TO 490	RSTA2380
	IOLD = IC3(ITEM-1527)	RSTA2390
	IC3(ITEM-1527) = II	RSTA2400
	GO TO 494	RSTA2410
	403 IF (ITEM.GT.1553) GO TO 490	RSTA2420
	IF (NTYPE.NE.1) GO TO 490	RSTA2430
	ROLD = RC3B(ITEM-1529)	RSTA2440
	RC3B(ITEM-1529) = RR	RSTA2450
	GO TO 492	RSTA2460
C	COMMON /SGMNTS/	RSTA2470
	4 IF (ITEM.GT.660) GO TO 404	RSTA2480
	IF (ITYPE.NE.1) GO TO 490	RSTA2490
	ROLD = RC4(ITEM)	RSTA2500

	RC4(ITEM) = RR	RSTA2510
	GO TO 492	RSTA2520
404	IF (ITEM.GT.682) GO TO 490	RSTA2530
	IF (ITYPE.NE.1) GO TO 490	RSTA2540
	IOLD = NSYM(ITEM-660)	RSTA2550
	NSYM(ITEM-660) = II	RSTA2560
	GO TO 494	RSTA2570
C	COMMON /CMATRIX/	RSTA2580
5	IF (ITEM.GT.1065) GO TO 490	RSTA2590
	IF (ITYPE.NE.1) GO TO 490	RSTA2600
	ROLD = RC5A(ITEM)	RSTA2610
	RC5A(ITEM) = RR	RSTA2620
	GO TO 492	RSTA2630
C	COMMON /ABDATA/	RSTA2640
6	IF (ITEM.GT.120) GO TO 490	RSTA2650
	IF (ITYPE.NE.1) GO TO 490	RSTA2660
	ROLD = RC6(ITEM)	RSTA2670
	RC6(ITEM) = RR	RSTA2680
	GO TO 492	RSTA2690
C	COMMON /TITLES/ NOTE: NO PROVISION FOR CGS OR JS.	RSTA2700
7	IF (ITEM.GT.281) GO TO 490	RSTA2710
	IF (ITYPE.NE.3) GO TO 490	RSTA2720
	AOLD = RC7A(ITEM)	RSTA2730
	RC7A(ITEM) = AA	RSTA2740
	GO TO 496	RSTA2750
C	COMMON /CNSNTS/	RSTA2760
8	IF (ITEM.GT.15) GO TO 408	RSTA2770
	IF (ITEM.LE.12) GO TO 408	RSTA2780
	IF (ITYPE.NE.3) GO TO 490	RSTA2790
	AOLD = RC8(ITEM)	RSTA2800
	RC8(ITEM) = AA	RSTA2810
	GO TO 496	RSTA2820
408	IF (ITYPE.NE.1) GO TO 490	RSTA2830
	ROLD = RC8(ITEM)	RSTA2840
	RC8(ITEM) = RR	RSTA2850
	GO TO 492	RSTA2860
C	COMMON /DESCRP/	RSTA2870
9	IF (ITEM.GT.1688) GO TO 409	RSTA2880
	IF (ITYPE.NE.1) GO TO 490	RSTA2890
	ROLD = RC9(ITEM)	RSTA2900
	RC9(ITEM) = RR	RSTA2910
	GO TO 492	RSTA2920
409	IF (ITEM.GT.1795) GO TO 490	RSTA2930
	IF (ITYPE.NE.2) GO TO 490	RSTA2940
	IOLD = IC9(ITEM-1688)	RSTA2950
	IC9(ITEM-1688) = II	RSTA2960
	GO TO 494	RSTA2970
C	COMMON /JBARTZ/	RSTA2980
10	IF (ITEM.GT.1236) GO TO 490	RSTA2990
	IF (ITYPE.NE.2) GO TO 490	RSTA3000

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        IOLD = IC10(ITEM)
        IC10(ITEM) = II
        GO TO 494
C      COMMON /FORCES/
11     IF (ITEM.GT.480) GO TO 411
        IF (NTYPE.NE.1) GO TO 490
        ROLD = RC11(ITEM)
        RC11(ITEM) = RR
        GO TO 492
411    IF (ITEM.GT.490) GO TO 412
        IF (NTYPE.NE.2) GO TO 490
        IOLD = IC11(ITEM-480)
        IC11(ITEM-480) = II
        GO TO 494
412    IF (ITEM.GT.616) GO TO 490
        IF (NTYPE.NE.1) GO TO 490
        ROLD = RC11A(ITEM-490)
        RC11A(ITEM-490) = RR
        GO TO 492
C      COMMON /INTEST/
12     IF (ITEM.GT.528 ) GO TO 490
        IF (ITYPE.NE.1) GO TO 490
        ROLD = RC12(ITEM)
        RC12(ITEM) = RR
        GO TO 492
C      COMMON /CSTRNT/
13     IF (ITEM.GT.1212) GO TO 413
        IF (ITYPE.NE.1) GO TO 490
        ROLD = RC13A(ITEM)
        RC13A(ITEM) = RR
        GO TO 492
413    IF (ITEM.GT.1249) GO TO 490
        IF (ITYPE.NE.2) GO TO 490
        IOLD = IC13(ITEM-1212)
        IC13(ITEM-1212) = II
        GO TO 494
C      COMMON /TABLES/
14     IF (ITEM.GT.554 ) GO TO 414
        IF (ITYPE.NE.2) GO TO 490
        IOLD = IC14(ITEM)
        IC14(ITEM) = II
        GO TO 494
414    IF (ITEM.GT.2554) GO TO 490
        IF (ITYPE.NE.1) GO TO 490
        ROLD = TAB(ITEM-554)
        TAB(ITEM-554) = RR
        GO TO 492
C      COMMON /COMAIN/
15     IF (ITEM.GT.245 ) GO TO 415
        IF (ITYPE.NE.1) GO TO 490

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RSTA3480
RSTA3490
RSTA3500

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        ROLD = RC15(ITEM)
        RC15(ITEM) = RR
        GO TO 492
415 IF (ITEM.GT.251 ) GO TO 490
    IF (IYPE.NE.2)   GO TO 490
    IOLD = IC15(ITEM-245)
    IC15(ITEM-245) = II
    GO TO 494
C     COMMON /CDINT /
    16 IF (ITEM.GT.2765) GO TO 416
    IF (IYPE.NE.1)   GO TO 490
    ROLD = RC16(ITEM)
    RC16(ITEM) = RR
    GO TO 492
416 IF (ITEM.GT.2768) GO TO 490
    IF (IYPE.NE.2)   GO TO 490
    IOLD = IC16(ITEM-2765)
    IC16(ITEM-2765) = II
    GO TO 494
C     COMMON /DAMPER/
    17 IF (ITEM.GT.220 ) GO TO 417
    IF (IYPE.NE.1)   GO TO 490
    ROLD = RC17(ITEM)
    RC17(ITEM) = RR
    GO TO 492
417 IF (ITEM.GT.261 ) GO TO 490
    IF (IYPE.NE.2)   GO TO 490
    IOLD = IC17(ITEM-220)
    IC17(ITEM-220) = II
    GO TO 494
C     COMMON /CEULER/
    18 IF (ITEM.GT.22 ) GO TO 418
    IF (IYPE.NE.2)   GO TO 490
    IOLD = IEULER(ITEM)
    IEULER(ITEM) = II
    GO TO 494
418 IF (ITEM.GT.526 ) GO TO 490
    IF (IYPE.NE.1)   GO TO 490
    ROLD = RC18(ITEM-22)
    RC18(ITEM-22) = RR
    GO TO 492
C     COMMON /TEMPVI/
    19 IF (ITEM.GT.10 ) GO TO 419
    IF (IYPE.NE.1)   GO TO 490
    ROLD = RC19(ITEM)
    RC19(ITEM) = RR
    GO TO 492
419 IF (ITEM.GT.178 ) GO TO 490
    IF (IYPE.NE.2)   GO TO 490
    IOLD = IC19(ITEM-10)

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RSTA3510
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RSTA3980
RSTA3990
RSTA4000

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	IC16(ITEM-10) = II	RSTA4010
	GO TO 494	RSTA4020
C	COMMON /WJONES/	RSTA4030
20	IF (ITEM.GT.315) GO TO 420	RSTA4040
	IF (ITYPE.NE.1) GO TO 490	RSTA4050
	ROLD = RC20A(ITEM)	RSTA4060
	RC20A(ITEM) = RR	RSTA4070
	GO TO 492	RSTA4080
420	IF (ITEM.GT.321) GO TO 320	RSTA4090
	IF (ITYPE.NE.2) GO TO 490	RSTA4100
	IOLD = IFULL(ITEM-315)	RSTA4110
	IFULL(ITEM-315) = II	RSTA4120
	GO TO 494	RSTA4130
320	IF (ITEM.GT.1433) GO TO 490	RSTA4140
	IF (ITYPE.NE.1) GO TO 490	RSTA4150
	ROLO = RC200(ITEM-321)	RSTA4160
	RC200(ITEM-321) = RR	RSTA4170
	GO TO 492	RSTA4180
C	COMMON /RSAVE/	RSTA4190
21	IF (ITEM.GT.180) GO TO 421	RSTA4200
	IF (ITYPE.NE.1) GO TO 490	RSTA4210
	ROLO = RC21(ITEM)	RSTA4220
	RC21(ITEM) = RR	RSTA4230
	GO TO 492	RSTA4240
421	IF (ITEM.GT.327) GO TO 490	RSTA4250
	IF (ITYPE.NE.2) GO TO 490	RSTA4260
	IOLD = IC21(ITEM-180)	RSTA4270
	IC21(ITEM-180) = II	RSTA4280
	GO TO 494	RSTA4290
C	COMMON /FLXBLE/	RSTA4300
22	IF (ITEM.GT.624) GO TO 422	RSTA4310
	IF (ITYPE.NE.1) GO TO 490	RSTA4320
	ROLD = RC22(ITEM)	RSTA4330
	RC22(ITEM) = RR	RSTA4340
	GO TO 492	RSTA4350
422	IF (ITEM.GT.649) GO TO 490	RSTA4360
	IF (ITYPE.NE.2) GO TO 490	RSTA4370
	IOLD = IC22(ITEM-624)	RSTA4380
	IC22(ITEM-624) = II	RSTA4390
	GO TO 494	RSTA4400
C	COMMON/HRNESS/	RSTA4410
23	IF (ITEM.GT.620) GO TO 423	RSTA4420
	IF (ITYPE.NE.1) GO TO 490	RSTA4430
	ROLO = RC23(ITEM)	RSTA4440
	RC23(ITEM) = RR	RSTA4450
	GO TO 492	RSTA4460
423	IF (ITEM.GT.966) GO TO 490	RSTA4470
	IF (ITYPE.NE.2) GO TO 490	RSTA4480
	IOLD = IC23(ITEM-620)	RSTA4490
	IC23(ITEM-620) = II	RSTA4500

<pre> GO TO 494 C COMMON/KALEPS/ 24 IF (ITEM.GT.30) GO TO 424 IF (ITYPE.NE.1) GO TO 490 ROLD = RC24(ITEM) RC24(ITEM) = RR GO TO 492 424 IF (ITEM.GT.170) GO TO 490 IF (ITYPE.NE.2) GO TO 490 IOLD = IC24(ITEM-30) IC24(ITEM-30) = II GO TO 494 C C ERROR MESSAGE - TERMINATE PROGRAM. C 490 WRITE (6,491) AVAR,INDEX,NCOM,ITEM,ITYPE,RR,II,AA 491 FORMAT('0 SUBROUTINE RSTART INPUT ERROR'// * ' AVAR= ',A8,'INDEX=',I4,' NCOM=',I6,' ITEM=',I6, * ' ITYPE=',I6,' RR=',G15.8,' II=',I8,' AA= ',A8// * ' PROGRAM IS BEING TERMINATED.') STOP C C PRINT MESSAGE FOR REAL VARIABLES. C 492 WRITE (6,493) AVAR,INDEX,COMMON(NCOM),ROLD,RR 493 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/', * ' HAS BEEN CHANGED FROM ',G15.8,' TO ',G15.8) IF (RROLD.EQ.0.0) GO TO 400 IF (DABS(RROLD-ROLD).LE.0.0001*RROLD) GO TO 400 WRITE (6,383) RROLD 383 FORMAT(' INPUT VALUE FOR RROLD WAS ',G15.8//) GO TO 490 C C PRINT MESSAGE FOR INTEGER VARIABLES. C 494 WRITE (6,495) AVAR,INDEX,COMMON(NCOM),IOLD,II 495 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/', * ' HAS BEEN CHANGED FROM ', I8,' TO ', I8) IF (IIOLD.EQ.0) GO TO 400 IF (IOLD.EQ.IIOLD) GO TO 400 WRITE (6,385) IIOLD 385 FORMAT(' INPUT VALUE FOR IIOLD WAS ',I8//) GO TO 490 C C PRINT MESSAGE FOR ALPHANUMERIC VARIABLES. C 496 WRITE (6,497) AVAR,INDEX,COMMON(NCOM),AOLD,AA 497 FORMAT('0',A6,'(',I4,',',I4,',',I4,') OF COMMON',A6,'/', * ' HAS BEEN CHANGED FROM ', A8,' TO ', A8) IF (AOLD.EQ.BLANK) GO TO 400 </pre>	<pre> RSTA4510 RSTA4520 RSTA4530 RSTA4540 RSTA4550 RSTA4560 RSTA4570 RSTA4580 RSTA4590 RSTA4600 RSTA4610 RSTA4620 RSTA4630 RSTA4640 RSTA4650 RSTA4660 RSTA4670 RSTA4680 RSTA4690 RSTA4700 RSTA4710 RSTA4720 RSTA4730 RSTA4740 RSTA4750 RSTA4760 RSTA4770 RSTA4780 RSTA4790 RSTA4800 RSTA4810 RSTA4820 RSTA4830 RSTA4840 RSTA4850 RSTA4860 RSTA4870 RSTA4880 RSTA4890 RSTA4900 RSTA4910 RSTA4920 RSTA4930 RSTA4940 RSTA4950 RSTA4960 RSTA4970 RSTA4980 RSTA4990 RSTA5000 </pre>
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AAOLD4 = AAOLD
AOLD4 = AOLD
IF (AOLD4.EQ.AAOLD4) GO TO 400
WRITE (6,387) AAOLD
387 FORMAT(' INPUT VALUE FOR AAOLD WAS ',A8//)
GO TO 490
999 CALL ELTIME(2,25)
RETURN
END
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RSTA5010
RSTA5020
RSTA5030
RSTA5040
RSTA5050
RSTA5060
RSTA5070
RSTA5080
RSTA5090
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*          3,22,0 , 3,22,0 , 3,22,0 , 22,0,0 /
C
C 5 COMMON/CMATRX/
C
  DIMENSION C5 ( 8) , NC5 ( 24)
  EQUIVALENCE (C5 (1),BVAR( 46)) , (NC5 (1),NDIM(1, 46))
  DATA C5 / 8HV1 ,8HV2 ,8HV3 ,8HB12 ,8HA22 ,
*           8HF ,8HTQ ,8HWJ /
  DATA NC5 / 3,21,0 , 3,21,0 , 3,12,0 , 3,3,42 , 3,3,42 ,
*           3,21,0 , 3,21,0 , 21,0,0 /
C
C 6 COMMON/ABDATA/
C
  DIMENSION C6 ( 6) , NC6 ( 18)
  EQUIVALENCE (C6 (1),BVAR( 54)) , (NC6 (1),NDIM(1, 54))
  DATA C6 / 8HABC ,8HZA ,8HDA ,8HBFA ,8HBGCV ,
*           8HBMEG /
  DATA NC6 / 3,5,0 , 3,5,0 , 3,3,5 , 3,5,0 , 3,5,0 ,
*           3,5,0 /
C
C 7 COMMON/TITLES/
C
  DIMENSION C7 ( 11) , NC7 ( 33)
  EQUIVALENCE (C7 (1),BVAR( 60)) , (NC7 (1),NDIM(1, 60))
  DATA C7 / 8HDATE ,8HCOMENT ,8HVPSTTL ,8HBDYTTL ,8HBLTTTL ,
*           8HPLTTL ,8HBAGTTL ,8HSEG ,8HJOINT ,8HCGS ,
*           8HJS /
  DATA NC7 / 3,0,0 , 40,0,0 , 20,0,0 , 5,0,0 , 5,8,0 ,
*           5,20,0 , 5,6,0 , 22,0,0 , 21,0,0 , 22,0,0 ,
*           21,0,0 /
C
C 8 COMMON/CNSNTS/
C
  DIMENSION C8 ( 16) , NC8 ( 48)
  EQUIVALENCE (C8 (1),BVAR( 71)) , (NC8 (1),NDIM(1, 71))
  DATA C8 / 8HPI ,8HRADIAN ,8HG ,8HTHIRD ,8HEPS1 ,
*           8HEPS4 ,8HEPS6 ,8HEPS8 ,8HEPS12 ,8HEPS15 ,
*           8HEPS20 ,8HEPS24 ,8HUNITL ,8HUNITM ,8HUNITT ,
*           8HGRAVITY /
  DATA NC8 / 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*           0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*           0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 ,
*           3,0,0 /
C
C 9 COMMON/DESCRP/
C
  DIMENSION C9 ( 16) , NC9 ( 48)
  EQUIVALENCE (C9 (1),BVAR( 87)) , (NC9 (1),NDIM(1, 87))
  DATA C9 / 8HPI ,8HW ,8HSR ,8HHA ,8HMB ,
*           8HHT ,8HRPHI ,8HRW ,8HSPRING ,8HVISC ,

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*          8HJNT      ,8HIPIN      ,8HNS      ,8HISING      ,8HIGLOB      , SEAR1010
*          8HJOINTF /                               SEAR1020
DATA NC9 / 3,22,0 , 22,0,0 , 3,42,0 , 3,42,0 , 3,42,0 , SEAR1030
*          3,3,42 , 3,22,0 , 22,0,0 , 5,63,0 , 7,63,0 , SEAR1040
*          21,0,0 , 21,0,0 , 0,0,0 , 22,0,0 , 21,0,0 , SEAR1050
*          21,0,0 /                               SEAR1060
C                               SEAR1070
C 10 COMMON/JBARTZ/                               SEAR1080
C                               SEAR1090
      DIMENSION C10( 11) , NC10( 33)              SEAR1100
      EQUIVALENCE (C10(1),BVAR(103)) , (NC10(1),NDIM(1,103)) SEAR1110
      DATA C10/ 8HMNPL ,8HMNBLT ,8HMNSEG ,8HMNBAG ,8HMPL , SEAR1120
*          8HMBLT ,8HMSEG ,8HMBAG ,8HNTPL ,8HNTBLT , SEAR1130
*          8HNTSEG /                               SEAR1140
      DATA NC10/ 20,0,0 , 8,0,0 , 22,0,0 , 6,0,0 , 3,5,20 , SEAR1150
*          3,5,8 , 3,5,22 , 3,10,6 , 5,20,0 , 5,8,0 , SEAR1160
*          5,22,0 /                               SEAR1170
C                               SEAR1180
C 11 COMMON/FORCES/                               SEAR1190
C                               SEAR1200
      DIMENSION C11( 10) , NC11( 30)              SEAR1210
      EQUIVALENCE (C11(1),BVAR(114)) , (NC11(1),NDIM(1,114)) SEAR1220
      DATA C11/ 8HPSF ,8HBSF ,8HSSF ,8HBAGSF ,8HNPSF , SEAR1230
*          8HNBSF ,8HNSSF ,8HNBGSF ,8HNPNEL ,8HPRJNT / SEAR1240
      DATA NC11/ 7,20,0 , 4,20,0 , 10,20,0 , 3,20,0 , 0,0,0 , SEAR1250
*          0,0,0 , 0,0,0 , 0,0,0 , 6,0,0 , 6,21,0 / SEAR1260
C                               SEAR1270
C 12 COMMON/INTEST/                               SEAR1280
C                               SEAR1290
      DIMENSION C12( 2) , NC12( 6)                SEAR1300
      EQUIVALENCE (C12(1),BVAR(124)) , (NC12(1),NDIM(1,124)) SEAR1310
      DATA C12/ 8HSGTEST ,8HXTEST /              SEAR1320
      DATA NC12/ 3,4,22 , 3,88,0 /              SEAR1330
C                               SEAR1340
C 13 COMMON/CSTRNT/                               SEAR1350
C                               SEAR1360
      DIMENSION C13( 17) , NC13( 51)              SEAR1370
      EQUIVALENCE (C13(1),BVAR(126)) , (NC13(1),NDIM(1,126)) SEAR1380
      DATA C13/ 8HA13 ,8HA23 ,8HB31 ,8HB32 ,8HHHT , SEAR1390
*          8HRK1 ,8HRK2 ,8HQQ ,8HTQQ ,8HRQQ , SEAR1400
*          8HHQQ ,8HSQQ ,8HCFQQ ,8HNQ ,8HKQ1 , SEAR1410
*          8HKQ2 ,8HKQTYPE /                      SEAR1420
      DATA NC13/ 3,3,24 , 3,3,24 , 3,3,24 , 3,3,24 , 3,3,12 , SEAR1430
*          3,12,0 , 3,12,0 , 3,12,0 , 3,12,0 , 3,12,0 , SEAR1440
*          3,12,0 , 12,0,0 , 12,0,0 , 0,0,0 , 12,0,0 , SEAR1450
*          12,0,0 , 12,0,0 /                      SEAR1460
C                               SEAR1470
C 14 COMMON/TABLES/                               SEAR1480
C                               SEAR1490
      DIMENSION C14( 7) , NC14( 21)              SEAR1500

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EQUIVALENCE (C14(1),8VAR(143)) , (NC14(1),NDIM(1,143))
DATA C14/ 8HMXNTI ,8HMXNT8 ,8HMXT81 ,8HMXT82 ,8HNTI , SEAR1510
*      8HNTA8 ,8HTA8 / SEAR1520
DATA NC14/ 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 50,0,0 , SEAR1530
*      500,0,0 , 2000,0,0/ SEAR1540
C SEAR1550
C 15 COMMON/COMAIN/ SEAR1560
C SEAR1570
DIMENSION C15( 13) , NC15( 39) SEAR1580
EQUIVALENCE (C15(1),8VAR(150)) , (NC15(1),NDIM(1,150)) SEAR1590
DATA C15/ 8HVAR ,8HDER ,8HDT ,8HHO ,8HHMAX , SEAR1600
*      8HMIN ,8HRSTIME ,8H1STEP ,8HNSTEPS ,8HNDINT , SEAR1610
*      8HNEQ ,8HIRSIN ,8HIRSOUT / SEAR1620
DATA NC15/ 120,0,0 , 120,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , SEAR1630
*      0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , SEAR1640
*      0,0,0 , 0,0,0 , 0,0,0 / SEAR1650
C SEAR1660
C 16 COMMON/CDINT / SEAR1670
C SEAR1680
DIMENSION C16( 13) , NC16( 39) SEAR1690
EQUIVALENCE (C16(1),8VAR(163)) , (NC16(1),NDIM(1,163)) SEAR1700
DATA C16/ 8HE ,8HFF ,8HGG ,8HY ,8HU , SEAR1710
*      8HH ,8HHPRINT ,8HTSAVE ,8HTPRINT ,8HTSTART , SEAR1720
*      8HICNT ,8HIDBL ,8HIFLAG / SEAR1730
DATA NC16/ 3,120,0 , 5,120,0 , 5,120,0 , 5,120,0 , 5,120,0 , SEAR1740
*      0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , 0,0,0 , SEAR1750
*      0,0,0 , 0,0,0 , 0,0,0 / SEAR1760
C SEAR1770
C 17 COMMON/DAMPER/ SEAR1780
C SEAR1790
DIMENSION C17( 6) , NC17( 18) SEAR1800
EQUIVALENCE (C17(1),8VAR(176)) , (NC17(1),NDIM(1,176)) SEAR1810
DATA C17/ 8HAPSDM ,8HAPSDN ,8HASD ,8HNSD ,8HMSDM , SEAR1820
*      8HMSDN / SEAR1830
DATA NC17/ 3,20,0 , 3,20,0 , 5,20,0 , 0,0,0 , 20,0,0 , SEAR1840
*      20,0,0 / SEAR1850
C SEAR1860
C 18 COMMON/CEULER/ SEAR1870
C SEAR1880
DIMENSION C18( 7) , NC18( 21) SEAR1890
EQUIVALENCE (C18(1),8VAR(182)) , (NC18(1),NDIM(1,182)) SEAR1900
DATA C18/ 8HIEULER ,8HHIR ,8HANG ,8HANGD ,8HFE , SEAR1910
*      8HTQE ,8HCONST / SEAR1920
DATA NC18/ 22,0,0 , 3,3,21 , 3,21,0 , 3,21,0 , 3,21,0 , SEAR1930
*      3,21,0 , 3,21,0 / SEAR1940
C SEAR1950
C 19 COMMON/TEMPVI/ SEAR1960
C SEAR1970
DIMENSION C19( 5) , NC19( 15) SEAR1980
EQUIVALENCE (C19(1),8VAR(189)) , (NC19(1),NDIM(1,189)) SEAR1990
SEAR2000

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	DATA C19/ 8HTT1	,8HR11	,8HR21	,8HCREST	,8HJSTOP	/	SEAR2010
	DATA NC19/ 3,0,0	, 3,0,0	, 3,0,0	, 0,0,0	, 4,2,21	/	SEAR2020
C							SEAR2030
C 20	COMMON/WJONES/						SEAR2040
C							SEAR2050
	DIMENSION C20(64)	, NC20(192)					SEAR2060
	EQUIVALENCE (C20(1),8VAR(194))	, (NC20(1),ND1M(1,194))					SEAR2070
	DATA C20/ 8HFORCE	,8HTORA	,8HX8M	,8HZDEP	,8HV8AGG	,	SEAR2080
*	8HVSCS	,8H8PH1	,8HD8R	,8HDPVCTR	,8HDEPLOY	,	SEAR2090
*	8HAB	,8HSPRK	,8HCYTD	,8HCYPA	,8HCYSP	,	SEAR2100
*	8HCYTO	,8HCYVC	,8HCYCD	,8HCYK	,8HCYR	,	SEAR2110
*	8HCYAT	,8HCYPV	,8HCYCD0	,8HCYAO	,8HCYPO	,	SEAR2120
*	8HCYSS	,8HCYLO	,8HCYC	,8HCYRHO0	,8HCYVMAX	,	SEAR2130
*	8HCYORFC	,8HCYRHO	,8HCYT	,8HCYP	,8HCYMIN	,	SEAR2140
*	8HCYMOUT	,8H8AGPV	,8HPD	,8HVBAG	,8HVOL8P	,	SEAR2150
*	8HSWITCH	,8H1FULL	,8HTMP	,8HTMP1	,8HA	,	SEAR2160
*	8HPF	,8HTORQ	,8HTQ8	,8HFR8	,8HVOL	,	SEAR2170
*	8HDELf	,8H8	,8HZ8	,8HZR	,8HBF8	,	SEAR2180
*	8HDRR	,8HD8	,8HPCGV	,8HPMEG	,8HVOLP	,	SEAR2190
*	8HFRA	,8HPREVT	,8HCK	,8HCMAS5	/		SEAR2200
	DATA NC20/ 3,5,0	, 3,5,0	, 5,0,0	, 3,5,0	, 5,0,0	,	SEAR2210
*	5,0,0	, 3,5,0	, 3,3,5	, 3,5,0	, 3,5,0	,	SEAR2220
*	3,5,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2230
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2240
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2250
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2260
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2270
*	5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	, 5,0,0	,	SEAR2280
*	5,0,0	, 6,0,0	, 18,0,0	, 3,0,0	, 3,3,0	,	SEAR2290
*	3,0,0	, 3,0,0	, 3,10,0	, 3,10,0	, 10,0,0	,	SEAR2300
*	3,0,0	, 9,4,5	, 3,4,5	, 3,4,5	, 9,4,5	,	SEAR2310
*	9,4,5	, 9,4,5	, 3,4,5	, 3,4,5	, 4,5,0	,	SEAR2320
*	3,4,0	, 0,0,0	, 5,0,0	, 5,0,0	/		SEAR2330
C							SEAR2340
C 21	COMMON/RSAVE/						SEAR2350
C							SEAR2360
	DIMENSION C21(3)	, NC21(9)					SEAR2370
	EQUIVALENCE (C21(1),8VAR(258))	, (NC21(1),ND1M(1,258))					SEAR2380
	DATA C21/ 8HXSG	,8HNSG	,8HMSG	/			SEAR2390
	DATA NC21/ 3,20,3	, 7,0,0	, 20,7,0	/			SEAR2400
C							SEAR2410
C 22	COMMON/FLXBLE/						SEAR2420
C							SEAR2430
	DIMENSION C22(5)	, NC22(15)					SEAR2440
	EQUIVALENCE (C22(1),8VAR(261))	, (NC22(1),ND1M(1,261))					SEAR2450
	DATA C22/ 8HHF	,8HB42	,8HV4	,8HNFLEX	,8HNFLX	/	SEAR2460
	DATA NC22/ 4,12,8	, 3,3,24	, 3,8,0	, 3,8,0	, 0,0,0	/	SEAR2470
C							SEAR2480
C 23	COMMON/HRNESS/						SEAR2490
	DIMENSION C23(8)	, NC23(24)					SEAR2500


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EQUIVALENCE (C23(1),BVAR(266)) , (NC23(1),NDIM(1,266)) SEAR2510
DATA C23/ 8H8AR ,8HXLONG ,8HIBAR ,8HNTHRNS ,8HNHRNSS , SEAR2520
* 8HNB LTPH ,8HNFBLT ,8HNPTSPB / SEAR2530
DATA NC23/ 6,100,0 , 20,0,0 , 2,100,0 , 20,0,0 , 0,0,0 , SEAR2540
* 5,0,0 , 5,20,0 , 20,0,0 / SEAR2550
C SEAR2560
C 24 COMMON/KALEPS/ SEAR2570
DIMENSION C24( 4) , NC24( 12) SEAR2580
EQUIVALENCE (C24(1),BVAR(274)) , (NC24(1),NDIM(1,274)) SEAR2590
DATA C24/ 8HWTIME ,8HIWIND ,8HMWSEG / SEAR2600
DATA NC24/ 30,0,0 , 30,0,0 , 5,22,0 / SEAR2610
NCOM = 50 SEAR2620
IF (AVAR.EQ.BLANK) GO TO 99 SEAR2630
C SEAR2640
C SEARCH FOR VARIABLE NO. IV. SEAR2650
C SEAR2660
NCOM = C SEAR2670
DO 10 IV=1,NVAR SEAR2680
IF (AVAR.EQ.BVAR(IV)) GO TO 12 SEAR2690
10 CONTINUE SEAR2700
GO TO 99 SEAR2710
C SEAR2720
C SEARCH FOR COMMON NO. IC. SEAR2730
C SEAR2740
12 DO 20 IC=1,KOM SEAR2750
IF (IV.GE.KOUNT(IC).AND.IV.LT.KOUNT(IC+1)) GO TO 22 SEAR2760
20 CONTINUE SEAR2770
GO TO 99 SEAR2780
C SEAR2790
C COMPUTE ITEM NO. FOR VARIABLE IV IN COMMON IC. SEAR2800
C SEAR2810
22 K1 = KOUNT(IC) SEAR2820
K2 = IV-1 SEAR2830
ITEM = 1 SEAR2840
IF (K1.EQ.IV) GO TO 25 SEAR2850
DO 24 K=K1,K2 SEAR2860
NI = 1 SEAR2870
DO 23 I=1,3 SEAR2880
IF (NDIM(I,K).NE.0) NI=NI*NDIM(I,K) SEAR2890
23 CONTINUE SEAR2900
24 ITEM = ITEM+NI SEAR2910
25 DO 26 I=1,3 SEAR2920
IF (INDEX(I).EQ.0 .AND. NDIM(I,IV).NE.0) GO TO 99 SEAR2930
IF (NDIM(I,IV).EQ.0 .AND. INDEX(I).GT.1) GO TO 99 SEAR2940
NJ(I) = MAX0(INDEX(I)-1,0) SEAR2950
NK(I) = MAX0(NDIM(I,IV),1) SEAR2960
IF (NJ(I).GE.NK(I)) GO TO 99 SEAR2970
26 CONTINUE SEAR2980
ITEM = ITEM+NJ(1)+NJ(2)*NK(1)+NJ(3)*NK(2)*NK(1) SEAR2990
NCOM = IC SEAR3000

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99 RETURN
END

SEAR3010
SEAR3020

C		UPDA0510
C	CALL UPDFDC FOR EACH ALLOWED PLANE-SEGMENT CONTACT.	UPDA0520
C		UPDA0530
	NPSF = 0	UPDA0540
	DO 11 J = 1,NPL	UPDA0550
	NK = MNPL(J)	UPDA0560
	IF (NK.LE.0) GO TO 11	UPDA0570
	DO 10 K = 1, NK	UPDA0580
	NPSF = NPSF+1	UPDA0590
	NT = NTPL(K,J)	UPDA0600
	NF = NTAB(NT+5)	UPDA0610
	CALL UPDFDC(NT)	UPDA0620
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 10	UPDA0630
	CALL IMPULS(1,K,J)	UPDA0640
	I = -1	UPDA0650
	10 CONTINUE	UPDA0660
	11 CONTINUE	UPDA0670
	12 IF (NBLT.LE.0) GO TO 15	UPDA0680
C		UPDA0690
C	CALL UPDFDC FOR EACH ALLOWED BELT-SEGMENT CONTACT.	UPDA0700
C		UPDA0710
	DO 14 J = 1,NBLT	UPDA0720
	NK = MNBLT(J)	UPDA0730
	IF (NK.LE.0) GO TO 14	UPDA0740
	DO 13 K = 1,NK	UPDA0750
	NT = NTBLT(K,J)	UPDA0760
	NF = NTAB(NT+5)	UPDA0770
	NT6 = NT+6	UPDA0780
	CALL UPDFDC(NT)	UPDA0790
C		UPDA0800
C	AND FOR 2ND FUNCTION, IF FULL BELT FRICTION.	UPDA0810
C		UPDA0820
	13 IF (NF.NE.0) CALL UPDFDC(NT6)	UPDA0830
	14 CONTINUE	UPDA0840
C		UPDA0850
C	CALL UPDFDC FOR EACH ALLOWED SEGMENT-SEGMENT CONTACT.	UPDA0860
C		UPDA0870
	15 NSSF = 0	UPDA0880
	DO 17 J=1,NSEG	UPDA0890
	NK = MNSEG(J)	UPDA0900
	IF (NK.LE.0) GO TO 17	UPDA0910
	DO 16 K = 1,NK	UPDA0920
	NSSF = NSSF+1	UPDA0930
	NT = NTSEG(K,J)	UPDA0940
	NF = NTAB(NT+5)	UPDA0950
	CALL UPDFDC(NT)	UPDA0960
	IF (NT.GT.0.OR.TAB(NF+3).EQ.0.0) GO TO 16	UPDA0970
	CALL IMPULS(3,K,J)	UPDA0980
	I = -1	UPDA0990
	16 CONTINUE	UPDA1000

17	CONTINUE	UPDA1010
	IF (NHRNSS.LE.0) GO TO 71	UPDA1020
C		UPDA1030
C	CALL UPDFDC FOR EACH BELT OF HARNESS-BELT SYSTEMS.	UPDA1040
C		UPDA1050
	J1 = 1	UPDA1060
	K1 = 1	UPDA1070
	DO 70 I1=1,NHRNSS	UPDA1080
	IF (NBLTPH(II).LE.0) GO TO 70	UPDA1090
	J2 = J1 + NBLTPH(II) - 1	UPDA1100
	DO 69 J=J1,J2	UPDA1110
	IF (NPTSPB(J).LE.0) GO TO 69	UPDA1120
	K2 = K1 + NPTSPB(J) - 1	UPDA1130
	NT = NTHRNS(J)	UPDA1140
	NF = NTAB(NT+5)	UPDA1150
	CALL UPDFDC(NT)	UPDA1160
	K1 = K2+1	UPDA1170
69	CONTINUE	UPDA1180
	J1 = J2+1	UPDA1190
70	CONTINUE	UPDA1200
71	IF (NJNT.LE.0) GO TO 39	UPDA1210
C		UPDA1220
C	CHECK FOR IMPULSE ON JOINT STOPS	UPDA1230
C	TO BE CALLED IF IN JOINT STOP (JSTOP(1)=1) THIS TIME STEP	UPDA1240
C	BUT NOT IN IN JOINT STOP (JSTOP(2)=0) AT PREVIOUS TIME.	UPDA1250
C		UPDA1260
	DO 20 K=1,NJNT	UPDA1270
	IF (JNT(K).EQ.0) GO TO 20	UPDA1280
	IF (IABS(IPIN(K)).NE.4 .AND. VISC(7,3*K-2).EQ.0.0) GO TO 19	UPDA1290
	DO 18 J=1,3	UPDA1300
	K3J = 3*K-3+J	UPDA1310
	IF (IABS(IPIN(K)).NE.4) K3J=3*K-2	UPDA1320
	IF (IABS(IPIN(K)).EQ.4 .AND. VISC(7,K3J).EQ.0.0) GO TO 18	UPDA1330
	IF (JSTOP(J,1,K).NE.1.OR.JSTOP(J,2,K).NE.0) GO TO 18	UPDA1340
	CALL IMPULS(4,J,K)	UPDA1350
	I = -1	UPDA1360
18	JSTOP(J,2,K) = JSTOP(J,1,K)	UPDA1370
19	IF (IGLOB(K).EQ.0) GO TO 20	UPDA1380
	NT = IGLOB(K)	UPDA1390
	MT = NTAB(NT+5)	UPDA1400
	CALL UPDFDC(NT)	UPDA1410
	IF (TAB(MT+3).EQ.0.0) GO TO 20	UPDA1420
	IF (JSTOP(4,1,K).NE.1.OR.JSTOP(4,2,K).NE.0) GO TO 20	UPDA1430
	CALL IMPULS(4,4,K)	UPDA1440
	I = -1	UPDA1450
20	JSTOP(4,2,K) = JSTOP(4,1,K)	UPDA1460
C		UPDA1470
C	TEST TO LOCK OR UNLOCK JOINTS	UPDA1480
C		UPDA1490
C		UPDA1500

C	CONDITIONS TO CHANGE SIGN OF IPIN(J)	UPDA1510
C		UPDA1520
C		UPDA1530
C	PINNED UNPINNED	UPDA1540
C	LOCKED (-1) H.TQ > T1 (-2) TQ > T1	UPDA1550
C		UPDA1560
C	UNLOCKED (+1) H.TQ < T2 (+2) TQ < T2	UPDA1570
C	OR OR	UPDA1580
C	WJ < T3 WJ < T3	UPDA1590
C		UPDA1600
C	DO 30 J=1,NJNT	UPDA1610
C	IF (IABS(IPIN(J)).EQ.4) GO TO 30	UPDA1620
C	IF (IPIN(J)) 21,30,22	UPDA1630
C	21 T1 = VISC(4,3*J-2)	UPDA1640
C	IF (T1.EQ.0.0) GO TO 30	UPDA1650
C	IF (IPIN(J).LE.-2) TQM = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)	UPDA1660
C	IF (IPIN(J).EQ.-1) TQM = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))	UPDA1670
C	IF (TQM-T1) 30,30,29	UPDA1680
C	22 T2 = VISC(5,3*J-2)	UPDA1690
C	IF (T2.EQ.0.0) GO TO 23	UPDA1700
C	IF (IPIN(J).GE.2) TQM = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)	UPDA1710
C	IF (IPIN(J).EQ. 1) TQM = DABS(XDY(HB(1,2*J),D(1,1,J+1),TQ(1,J)))	UPDA1720
C	IF (TQM-T2) 28,30,30	UPDA1730
C	23 T3 = VISC(6,3*J-2)	UPDA1740
C	IF (T3.EQ.0.0) GO TO 30	UPDA1750
C	IF (WJ(J)-T3) 28,30,30	UPDA1760
C	28 CALL IMPLS2(0,J,HB(1,2*J))	UPDA1770
C	1 = -1	UPDA1780
C	29 IPIN(J) = -IPIN(J)	UPDA1790
C	30 CONTINUE	UPDA1800
C		UPDA1810
C	TEST TO LOCK OR UNLOCK EULER JOINTS AXES.	UPDA1820
C	USE SAME TEST AS ABOVE BUT ON EACH AXIS SERARATELY.	UPDA1830
C		UPDA1840
C	IF LOCK(IEULER,K) IS NEGATIVE, AXIS K IS LOCKED;	UPDA1850
C	TO UNLOCK AXIS SET IEULER TO -LOCK(IEULER,K).	UPDA1860
C		UPDA1870
C	IF LOCK(IEULER,K) IS POSITIVE, AXIS K IS UNLOCKED;	UPDA1880
C	TO LOCK AXIS SET IEULER TO LOCK(IEULER,K).	UPDA1890
C		UPDA1900
C	DO 60 J=1,NJNT	UPDA1910
C	IF (IABS(IPIN(J)).NE.4) GO TO 60	UPDA1920
C	IEULER = IEULER(J)	UPDA1930
C	CALL DOT(HIR(1,1,J),TQ(1,J),TQTEST,3,1,3)	UPDA1940
C	DO 55 K=1,3	UPDA1950
C	K3J = 3*J-3+K	UPDA1960
C	NLOCK = LOCK(JEULER,K)	UPDA1970
C	IF (NLOCK.GT.0) GO TO 52	UPDA1980
C	IF (VISC(4,K3J).EQ.0.0) GO TO 55	UPDA1990
C	IF (DABS(TQTEST(K)).GT.VISC(4,K3J)) JEULER = -NLOCK	UPDA2000
C	GO TO 55	

52	IF (VISC(5,K3J).EQ.0.0) GO TO 53	UPDA2010
	IF (DABS(TQTEST(K)).LT.VISC(5,K3J)) JEULER = NLOCK	UPDA2020
	GO TO 55	UPDA2030
53	IF (VISC(6,K3J).EQ.0.0) GO TO 55	UPDA2040
	IF (DABS(ANGD(K,J)).LT.VISC(6,K3J)) JEULER = NLOCK	UPDA2050
55	CONTINUE	UPDA2060
	IF (JEULER.EQ.IEULER(J)) GO TO 60	UPDA2070
	IF (JEULER.EQ.8) GO TO 59	UPDA2080
	MODE = -1	UPDA2090
	K = JEULER	UPDA2100
	IF (K.LE.3) GO TO 57	UPDA2110
	MODE = 1	UPDA2120
	K = K-3	UPDA2130
	IF (K.GT.3) MODE=0	UPDA2140
57	IEULER(J) = 8	UPDA2150
	IPIN(J) = 4	UPDA2160
	CALL IMPLS2(MODE,J,HIR(1,K,J))	UPDA2170
	I = -1	UPDA2180
59	IEULER(J) = JEULER	UPDA2190
	IPIN(J) = 4	UPDA2200
	IF (IEULER(J).NE.8) IPIN(J) = -4	UPDA2210
60	CONTINUE	UPDA2220
C		UPDA2230
39	IF (NQ.LE.0) GO TO 99	UPDA2240
	DO 40 K=1,NQ	UPDA2250
	IF (KQTYPE(K).LT.3) GO TO 40	UPDA2260
	IF (KQTYPE(K).GT.4) GO TO 40	UPDA2270
	IF (CFQQ(K).LT.0.0) KQTYPE(K) = -KQTYPE(K)	UPDA2280
	IF (CFQQ(K).LT.0.0) GO TO 42	UPDA2290
C		UPDA2300
C	TEST IF ROLLING CONSTRAINT SHOULD BE SLIDING AND VICE VERSA.	UPDA2310
C		UPDA2320
	QN = -XDY(TQQ(1,K),HHT(1,1,K),QQ(1,K))	UPDA2330
	IF (NPRT(24).NE.0) WRITE (6,41) KQTYPE(K),KQ1(K),KQ2(K),	UPDA2340
	* (RK1(11,K),I1=1,3),(RK2(11,K),I1=1,3),	UPDA2350
	* ((HHT(11,J,K),J=1,3),I1=1,3),	UPDA2360
	* (QQ(11,K),I1=1,3),(TQQ(11,K),I1=1,3),(RQQ(11,K),I1=1,3),	UPDA2370
	* (HQQ(11,K),I1=1,3),SQQ(K),CFQQ(K),QN	UPDA2380
41	FORMAT('0 UPDATE ROLL-SLIDE TEST'/(2X,9G14.6))	UPDA2390
	IF (QN.LT.0.0) KQTYPE(K) = -4	UPDA2400
	IF (QN.LT.0.0) GO TO 42	UPDA2410
	QDOTQ = QQ(1,K)**2 + QQ(2,K)**2 + QQ(3,K)**2	UPDA2420
	QT = DSQRT(QDOTQ-QN**2)	UPDA2430
	IF (KQTYPE(K).EQ.3 .AND. QT.LE.CFQQ(K)*QN) GO TO 40	UPDA2440
	IF (KQTYPE(K).EQ.4 .AND. QT.GE.0.9*CFQQ(K)*QN) GO TO 40	UPDA2450
	KQTYPE(K) = 7-KQTYPE(K)	UPDA2460
42	CALL OUTPUT(C)	UPDA2470
	CALL SETUP2	UPDA2480
	CALL DAUX(K)	UPDA2490
	CALL OUTPUT(1)	UPDA2500

```
CALL PRINT(6HUPDATE)
I = -1
40 CONTINUE
99 CALL ELTIME(2,7)
RETURN
END
```

```
UPDA2510
UPDA2520
UPDA2530
UPDA2540
UPDA2550
UPDA2560
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SUBROUTINE VEHPOS                                REV 12 12/16/74
C
C COMPUTE COMPONENTS OF VEHICLE POSITION AND MOTION AS A FUNCTION OF TIME USING DATA AND TABLES PRODUCED BY SUBROUTINE VINPUT.
C
C IMPLICIT REAL*8 (A-H,O-Z)
COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
COMMON/SGMNTS/O(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
*      ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
COMMON/VPOSTN/ TIME,XO(3),XDOTO(3),XCOMP(3),XVCOMP(3),AX(3),
*      ANGLE(3),VMPH,VTIME,ATAB(15,100),ATO,ADT,OMEGA,
*      NATAB,NACL,R,DVEH(3,3),VMEG(3),VMEGO(3),XACOMP(3),
*      THET(3),ZPLT(3)
COMMON/CNSNTS/ PI, RADIAN,G,THIRO,EPS1,EPS4,EPS6,EPS8,
*      EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVTY(3)
DIMENSION AC(3)
DATA TLAST/-100000.0/
T = TIME
IF(NATAB.NE.0) GO TO 20

C HALF-SINE WAVE DECELERATION
C
C IF(T.GT.VTIME) T=VTIME
WT = OMEGA*T
CWT1 = OCOS(WT)-1.0
SWT = OSIN(WT)
DO 10 I=1,3
AW = AX(I)*OMEGA
XACOMP(I) = -AW*OMEGA*SWT
XCOMP(I) = AX(I)*SWT + 1*(XDOTO(I)-AW)+XO(I)
10 XVCOMP(I) = AW*CWT1 + XDOTO(I)
GO TO 99
20 IF (NATAB.LT.0) GO TO 30

C UNIDIRECTIONAL DECELERATION
C
C IF (T.LT.VTIME) GO TO 21
C
C TIME POINT EXCEEDS TABLE, EXTRAPOLATE.
C
DLT = T-VTIME
ACO = ATAB(1,NATAB)
AC(1) = ATAB(2,NATAB) + G*ACO*DLT
AC(2) = ATAB(3,NATAB) + AC(1)*DLT + 0.5*G*ACO*DLT**2
GO TO 25

C USE QUADRATIC INTERPOLATION FROM TABLES FOR CURRENT VALUE OF TIME TO BE CONSISTENT WITH SIMPSON INTEGRATION OF TABLES.
C
21 J= 0.5*(T-ATO)/ADT +1.0

```

XK = T/ADT -DFLOAT(2*J-1)	VEHP0510
X1 = XK+1.0	VEHP0520
X2 = XK**2-XK+1.0	VEHP0530
X3 = XK-1.0	VEHP0540
UNITS = -G	VEHP0550
DO 23 I=1,2	VEHP0560
T1 = (ATAB(I,2*J-1)-2.0*ATAB(I,2*J)+ATAB(I,2*J+1))/6.0	VEHP0570
T2 = (ATAB(I,2*J+1)-ATAB(I,2*J-1))/4.0	VEHP0580
T3 = ATAB(I,2*J)	VEHP0590
AC(I) = ATAB(I+I,2*J-1)+ADT*X1*(X2*T1+X3*T2+T3)*UNITS	VEHP0600
23 UNITS = 1.0	VEHP0610
ACC = 0.5*XK*X3*ATAB(1,2*J-1)	VEHP0620
* - X3*X1*ATAB(1,2*J)	VEHP0630
* + 0.5*XK*X1*ATAB(1,2*J+1)	VEHP0640
C	VEHP0650
C	VEHP0660
C	VEHP0670
25 DO 29 I=1,3	VEHP0680
XACOMP(I) = -G*AX(I)*ACC	VEHP0690
XVCOMP(I) = AX(I)*AC(1)	VEHP0700
29 XCOMP(I) = XG(I)+AX(I)*AC(2)	VEHP0710
GO TO 99	VEHP0720
C	VEHP0730
C	VEHP0740
C	VEHP0750
30 IF (TIME.EQ.TLAST) GO TO 99	VEHP0760
DLTA = TIME-TLAST	VEHP0770
IF (TLAST.EQ.-100000.0) DLTA = 0.0	VEHP0780
TLAST = TIME	VEHP0790
J = (TIME-ATO)/ADT+1.0	VEHP0800
IF (J.GE.-NATAB) GO TO 32	VEHP0810
C	VEHP0820
C	VEHP0830
C	VEHP0840
C	VEHP0850
TJ = ATO + DFLOAT(J-1)*ADT	VEHP0860
DLT = TIME-TJ	VEHP0870
DO 31 I=1,3	VEHP0880
AL2 = (ATAB(I,J+1)-ATAB(I,J))*DLT/ADT*G	VEHP0890
AL1 = G*ATAB(I,J)	VEHP0900
XACOMP(I) = -AL1-AL2	VEHP0910
AL2 = 0.5*AL2	VEHP0920
XVCOMP(I) = ATAB(I+3,J)-DLT*(AL1+AL2)	VEHP0930
XCOMP(I) = ATAB(I+6,J)+DLT*(ATAB(I+3,J)-DLT*(0.5*AL1+AL2/3.0))	VEHP0940
AA2 = (ATAB(I+9,J+1)-ATAB(I+9,J))*RADIAN/ADT	VEHP0950
THET(I) = DLTA*(VMEG(I)+DLTA*(0.5*VMEGD(I)+DLTA*AA2/6.0))	VEHP0960
AA2 = AA2 * DLT	VEHP0970
AA1 = ATAB(I+9,J)*RADIAN	VEHP0980
VMEGD(I) = AA1 + AA2	VEHP0990
31 VMEG(I) = ATAB(I+12,J)*RADIAN + DLT*(AA1+0.5*AA2)	VEHP1000

	GO TO 34	VEHP1010
C		VEHP1020
C	TIME POINT EXCEEDS TABLE, EXTRAPOLATE.	VEHP1030
C		VEHP1040
	32 J = - NATAB	VEHP1050
	TJ = ATO + DFLOAT(J-1)*ADT	VEHP1060
	DLT = TIME-TJ	VEHP1070
	DO 33 I=1,3	VEHP1080
	XACOMP(1) = ATAB(I,J)*G	VEHP1090
	XVCOMP(I) = ATAB(I+3,J) +G*ATAB(I,J)*DLT	VEHP1100
	XCOMP (I) = ATAB(I+6,J) +ATAB(I+3,J)*DLT + 0.5*G*ATAB(I,J)*DLT**2	VEHP1110
	VMEGD(I) = 0.0	VEHP1120
	VMEG (I) = ATAB(I+12,J)*RADIAN	VEHP1130
	33 THET (I) = DLTA*VMEG(I)	VEHP1140
C		VEHP1150
C	UPDATE DIRECTION COSINE MATRIX OF VEHICLE.	VEHP1160
C		VEHP1170
	34 CALL DSETD(DVEH,THET,THT)	VEHP1180
C		VEHP1190
C	STORE VEHICLE DATA INTO NVEH SEGMENT DATA.	VEHP1200
C		VEHP1210
	99 DO 42 I=1,3	VEHP1220
	DO 41 J=1,3	VEHP1230
	41 D(I,J,NVEH) = DVEH(I,J)	VEHP1240
	SEGLP(I,NVEH) = XCOMP(1)	VEHP1250
	SEGLV(I,NVEH) = XVCOMP(I)	VEHP1260
	SEGLA(1,NVEH) = XACOMP(1)	VEHP1270
	WMEG (1,NVEH) = VMEG (I)	VEHP1280
	42 WMEGD(I,NVEH) = VMEGD(I)	VEHP1290
	RETURN	VEHP1300
	END	VEHP1310

C		VINPC510
C	HALF-SINE WAVE DECELERATION	VINPC520
C		VINPC530
	DMEGA = PI/VTIME	VINPC540
	AT = 0.5*VIPS/DMEGA	VINPC550
	IF (VIPS.LT.0.0) VIPS = 0.0	VINPC560
	DD 12 I=1,3	VINPC570
	XDDT0(I) = VIPS*AX(I)	VINPC580
12	AX(I) = AT*AX(I)	VINPC590
	WRITE (6,I3) VIPS,UN1TL,UN1TT,ANGLE,VTIME,UN1TT	VINPC600
13	FORMAT('0 PASSENGER COMPARTMENT DISPLACEMENT HISTORY'/	VINPC610
	* ' ANALYTICAL HALF-SINE WAVE DECELERATION'/	VINPC620
	* ' VG=',F8.3,1X,A4,'/',A4,' OBLIQUE ANGLES =',3F7.2,	VINPC630
	* ' DEGREES, TIME DURATION =',F7.3,1X,A4//)	VINPC640
	GD TO 4I	VINPC650
20	IF (NATAB.LT.0) GO TO 50	VINPC660
C		VINPC670
C	FDR UNIDIRECTIONAL VEHICLE MOTION	VINPC680
C	READ LINEAR DECELERATION TABLES FROM CARDS C.3	VINPC690
C		VINPC700
	READ (5,2I) (ATAB(I,I),I=1,NATAB)	VINPC710
21	FORMAT (I2F6.0)	VINPC720
C		VINPC730
C	EXTEND TABLE IF NECESSARY SUCH THAT NATAB IS ODD AND	VINPC740
C	LAST ENTRY NEED NOT BE ZERD. IF TABLE SIZE IS EXCEEDED ON TIME,	VINPC750
C	VALUE OF LAST ENTRY WILL BE USED.	VINPC760
C		VINPC770
	IF (MOD(NATAB,2).EQ.1) GO TO 23	VINPC780
	ATAB(1,NATAB+1) = ATAB(I,NATAB)	VINPC790
	NATAB = NATAB+1	VINPC800
23	VTIME = ADT * DFLOAT(NATAB-1)	VINPC810
C		VINPC820
C	USING SIMPSON'S INTEGRATION, COMPUTE VELDCITY AND DISPLACEMENT	VINPC830
C	TABLE FOR NATAB EQUALLY SPACED (ADT) TIME PDINTS.	VINPC840
C	FOR I=1,NATAB	VINPC850
C	ATAB(I,I) = LINEAR DECELERATION (G'S)	VINPC860
C	ATAB(2,I) = LINEAR VELOCITY (L UNITS/T UNITS)	VINPC870
C	ATAB(3,I) = LINEAR DISPLACEMENT (L UNITS)	VINPC880
C		VINPC890
	ATAB(2,1) = VIPS	VINPC900
	ATAB(3,1) = 0.0	VINPC910
	DA1 = ADT/3.0	VINPC920
	DA2 = ADT/12.0	VINPC930
	UNITS = -G	VINPC940
	DO 30 J=2,3	VINPC950
	DO 25 I=2,NATAB,2	VINPC960
	F1 = ATAB(J-1,I-1) * UNITS	VINPC970
	F2 = ATAB(J-1,I) * UNITS	VINPC980
	F3 = ATAB(J-1,I+1) * UNITS	VINPC990
	ATAB(J,I) = ATAB(J,I-1) + DA2*(5.0*F1+8.0*F2-F3)	VINP1000

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25 ATAB(J,I+1) = ATAB(J,I-1) + DA1*( F1+4.0*F2+F3)          VINP1010
30 UNITS = 1.0                                               VINP1020
C
C PRINT TABLES                                             VINP1030
C
WRITE (6,36) (UNITL,UNITT,UNITL,I=1,2)                     VINP1050
36 FORMAT('C UNIDIRECTIONAL VEHICLE POSITION TABLES'//      VINP1060
* 2(' TIME ACC VELOCITY POSITION ')/                       VINP1070
* 2(' (MILLESEC) (G) (' ,A4,'/',' ,A4,')',5X,'(' ,A4,')')//) VINP1080
DO 40 J=1,50                                               VINP1090
IF (J.GT.NATAB) GO TO 40                                   VINP1100
T1 = (AT0 + DFLOAT(J-1)*ADT)*1000.0                       VINP1110
IF (J+50.LE.NATAB) GO TO 38                               VINP1120
WRITE (6,37) T1,(ATAB(I,J),I=1,3)                         VINP1130
37 FORMAT(2(F11.5,F10.2,F13.4,F13.5,3X))                  VINP1140
GO TO 40                                                   VINP1150
38 T2 = (AT0 + DFLOAT(J+49)*ADT)*1000.0                  VINP1160
WRITE (6,37) T1,(ATAB(I,J),I=1,3),T2,(ATAB(I,J+50),I=1,3) VINP1170
40 CONTINUE                                               VINP1180
C
C INITIALIZATION                                           VINP1190
C
DO 35 I=1,3                                               VINP1200
35 XDOT0(I)= VIPS*AX(I)                                    VINP1210
41 DO 43 I=1,3                                            VINP1220
DO 42 J=1,3                                               VINP1230
42 DVEH(1,J) = 0.0                                        VINP1240
DVEH(I,I) = 1.0                                           VINP1250
VMEGD(I) = 0.0                                           VINP1260
43 VMEG(I) = 0.0                                         VINP1270
GO TO 99                                                  VINP1280
C
C FOR OMNIDIRECTIONAL (6 DEGREES OF FREEDOM) VEHICLE MOTION VINP1290
C READ LINEAR DECELERATION AND AUGULAR ACCELERATION TABLES VINP1300
C FROM CARDS C.4.                                         VINP1310
C
50 MATAB = -NATAB                                         VINP1320
READ(5,51) ((ATAB(I,J),I=1,3),(ATAB(1,J),I=10,12),J=1,MATAB) VINP1330
51 FORMAT(10X,6F10.0)                                     VINP1340
DO 60 J=1,MATAB                                           VINP1350
IF (MOD(J,50).NE.1) GO TO 53                              VINP1360
C
C PRINT PAGE HEADING AT START OF EACH 50 TIME POINTS.     VINP1370
C
IF (J.NE.1) WRITE (6,44)                                  VINP1380
44 FORMAT('1')                                             VINP1390
IPAGE = (J-1)/50 + 1                                       VINP1400
WRITE (6,52) IPAGE,UNITL,UNITT,UNITL,UNITT               VINP1410
52 FORMAT('O ROTATING VEHICLE LINEAR TIME HISTORY',      VINP1420
* 67X,'PAGE NO.',I3//)                                     VINP1430
VINP1440
VINP1450
VINP1460
VINP1470
VINP1480
VINP1490
VINP1500

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*          4X,'TIME',12X,'LINEAR DECELERATIONS (G'S)',          VINP1510
*          10X,'LINEAR VELOCITIES ('A4','/','A4,')',          VINP1520
*          11X,'LINEAR DISPLACEMENTS ('A4,')' /              VINP1530
$          3X,'('A4,')',3(11X,'X',11X,'Y',11X,'Z',3X) / )    VINP1540
53 IF (J.GT.1) GO TO 57                                       VINP1550
C                                                                 VINP1560
C   INTEGRATION INITIALIZATION FOR TIME = 0.                   VINP1570
C                                                                 VINP1580
DO 54 I=1,3                                                    VINP1590
  ATAB(I+6,J) = X0(I)                                          VINP1600
  ATAB(I+12,J) = 0.0                                          VINP1610
54 THET(I) = ANGLE(I)*RADIAN                                   VINP1620
  CALL DRCYPR(DVEH,ANGLE,3,2,1)                               VINP1630
  DO 55 I=1,3                                                  VINP1640
    XDOT0(I) = VIPS*DVEH(1,I)                                 VINP1650
55 ATAB(I+3,J) = XDOT0(I)                                     VINP1660
    GO TO 59                                                   VINP1670
57 DO 58 I=1,3                                                VINP1680
C                                                                 VINP1690
C   INTEGRATE LINEAR VELOCITY AND DISPLACEMENT.               VINP1700
C                                                                 VINP1710
  ATAB(I+3,J) = ATAB(I+3,J-1)-G*ADT/2.0*(ATAB(I,J-1)+ATAB(I,J)) VINP1720
58 ATAB(I+6,J) = ATAB(I+6,J-1)                                VINP1730
  *   +ADT*(ATAB(I+3,J-1)-G*ADT/6.0*(2.0*ATAB(I,J-1)+ATAB(I,J))) VINP1740
59 T1 = (A0 + DFLOAT(J-1)*ADT)                                VINP1750
60 WRITE(6,61) T1,(ATAB(I,J),I=1,9)                          VINP1760
61 FORMAT(F9.5,3(3X,3F12.3))                                  VINP1770
  DO 70 J=1,MATAB                                             VINP1780
    IF(MOD(J,50).NE.1) GO TO 63                               VINP1790
C                                                                 VINP1800
C   PRINT PAGE HEADING AT START OF EACH 50 TIME POINTS.     VINP1810
C                                                                 VINP1820
  IPAGE = (J-1)/50+1                                          VINP1830
  WRITE (6,62) IPAGE,UNITT,UNITT,UNITT                       VINP1840
62 FORMAT('1 ROTATING VEHICLE ANGULAR TIME HISTORY',          VINP1850
*        66X,'PAGE NO.',I3//                                  VINP1860
*        4X,'TIME', 6X,'ANGULAR ACCELERATIONS (DEG/'A4, '**2)', VINP1870
*        10X,'ANGULAR VELOCITIES (DEG/'A4,')',              VINP1880
*        11X,'ANGULAR DISPLACEMENTS (DEG)' /               VINP1890
*        3X,'('A4,')',2(11X,'X',11X,'Y',11X,'Z',3X),       VINP1900
*        10X,'YAW',8X,'PITCH',8X,'ROLL' /)                  VINP1910
63 IF(J.EQ.1) GO TO 65                                       VINP1920
C                                                                 VINP1930
C   INTEGRATE ANGULAR VELOCITY AND DISPLACEMENT.             VINP1940
C                                                                 VINP1950
DO 64 I=1,3                                                    VINP1960
  ATAB(I+12,J) = ATAB(I+12,J-1)+(ATAB(I+9,J-1)+ATAB(I+9,J))*ADT/2.0 VINP1970
64 THET(I) = ADT*(ATAB(I+12,J-1)+(2.0*ATAB(I+9,J-1)+ATAB(I+9,J))*ADT VINP1980
  */6.0)*RADIAN                                              VINP1990
  CALL DSETD(DVEH,THET,THI)                                   VINP2000

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65	CALL YPRDEG(DVEH,THET)	VINP2010
	T1 = (ATO + DFLOAT(J-1)*ADT)	VINP2020
70	WRITE (6,71) T1,(ATAB(1,J),1=10,15),THET	VINP2030
71	FORMAT(F9.5,3(3X,3F12.3))	VINP2040
C		VINP2050
C	PROGRAM INITIALIZATION FOR TIME = 0.	VINP2060
C		VINP2070
	CALL DRCYPR (DVEH,ANGLE,3,2,1)	VINP2080
	DO 72 I=1,3	VINP2090
	VMEG(I) = ATAB(I+12,1)*RADIAN	VINP2100
72	VMEGD(I) = ATAB(I+9 ,1)*RADIAN	VINP2110
C		VINP2120
C	SET UP SEGMENT DATA FOR GROUND.	VINP2130
C		VINP2140
99	NVEH = NSEG+1	VINP2150
	NGRND = NVEH+1	VINP2160
	SEG(NVEH) = VEH	VINP2170
	SEG(NGRND) = GRND	VINP2180
	IF (NVEH -1.GT.NJNT) JNT (NVEH -1) = 0	VINP2190
	IF (NVEH -1.GT.NJNT) IPIN(NVEH -1) = 0	VINP2200
	IF (NGRND-1.GT.NJNT) JNT (NGRND-1) = 0	VINP2210
	IF (NGRND-1.GT.NJNT) IPIN(NGRND-1) = 0	VINP2220
	DO 82 I=1,3	VINP2230
	DO 81 J=1,3	VINP2240
81	D(I,J,NGRND) = 0.0	VINP2250
	D(I,I,NGRND) = 1.0	VINP2260
	SEGLP(1,NGRND) = 0.0	VINP2270
	SEGLA(I,NGRND) = 0.0	VINP2280
	SEGLV(I,NGRND) = 0.0	VINP2290
	WMEG (I,NGRND) = 0.0	VINP2300
82	WMEGD(I,NGRND) = 0.0	VINP2310
	DO 83 J=NVEH,NGRND	VINP2320
	W(J) = 0.0	VINP2330
	RW(J) = 0.0	VINP2340
	DO 83 I=1,3	VINP2350
	PHI(I,J) = 0.0	VINP2360
83	RPHI(I,J) = 0.0	VINP2370
	RETURN	VINP2380
	END	VINP2390

```

C          SUBROUTINE VISPR(IJ,NJ)
C
C          COMPUTES VISCOS AND SPRING TORQUES AT THE JOINTS
C          AND ADDS THEM TO THE U2 ARRAY.
C
C          ARGUMENTS:
C          NJ = 0 - REGULAR COMPUTATION FOR ALL JOINTS
C          # 0 - COMPUTE ONLY FOR JOINT NJ IMPULSE
C
C          IJ = 1 IMPULSE FOR FLEXURE ONLY
C          = 2 IMPULSE FOR TORSION ONLY
C          = 4 IMPULSE FOR GLOBALGRAPHIC ONLY
C
C          IMPLICIT REAL*8 (A-H,O-Z)
C          COMMON/CONTRL/NSEG,NJNT,NS3,NJ3,NPL,NBLT,NBAG,NVEH,NGRND,NPRT(40)
C          COMMON/DESCRP/ PHI(3,22),W(22),SR(3,42),HA(3,42),HB(3,42)
C          *           ,HT(3,3,42),RPHI(3,22),RW(22),SPRING(5,63)
C          *           ,VISC(7,63),JNT(21),IPIN(21),NS,ISING(22)
C          *           ,IGLOB(21),JOINTF(21)
C          COMMON/SGMNTS/D(3,3,22),WMEG(3,22),WMEGD(3,22),U1(3,22),U2(3,22)
C          *           ,SEGLP(3,22),SEGLV(3,22),SEGLA(3,22),NSYM(22)
C          COMMON/FORCES/PSF(7,20),BSF(4,20),SSF(10,20),BAGSF(3,20),
C          *           NPSF,NBSF,NSSF,NBGSF,NPANEL(6),PRJNT(6,21)
C          COMMON/CMATRX/V1(3,21),V2(3,21),V3(3,12),B12(3,3,42),A22(3,3,42)
C          *           ,F(3,21),TQ(3,21),WJ(21)
C          COMMON/EULER/ IEULER(22),HIR(3,3,21),ANG(3,21),ANGD(3,21),
C          *           FE(3,21),TQE(3,31),CONST(3,21)
C          COMMON/TABLES/MXNTI,MXNTB,MXTB1,MXTB2,NTI(50),NTAB(500),TAB(2000)
C          COMMON/TEMPVS/T1(3),T2(3),T3(3),T4(3),T5(3),T6(3),T7(3),T8(3)
C          *           ,T9(3),HAD,HBD,WIJM,CV,CSA,CSB,WIJ(3),ANGL(3),TQC
C          *           ,THETO,THETOP,DH1(3,3),DH2(3,3),HD3(3,3),CC(3)
C          COMMON/TEMPVI/ TTI(3),R1I(3),R2I(3),CREST,JSTOP(4,2,21)
C          COMMON/CNSNTS/ PI, RADIANG,THIRD,EPS1,EPS4,EPS6,EPS8,
C          *           EPS12,EPS15,EPS20,EPS24,UNITL,UNITM,UNITT,GRAVTY(3)
C          COMMON /VPOSTN/ TIME
C          IF (NJNT.LE.0) GO TO 99
C          CALL ELTIME(1,13)
C          IF (NPRT(12).NE.0) WRITE (6,11) TIME
11  FORMAT('1 VISPR COMPUTATIONS FOR TIME =',F12.6)
C          J1 = 1
C          J2 = NJNT
C          IF (NJ.EQ.0) GO TO 13
C          J1 = NJ
C          J2 = NJ
13  DO 90 J=J1,J2
C          DO 12 L=1,3
12  TQ(L,J) = 0.0
C          WJ(J) = 0.0
C
C          DO NOT COMPUTE TORQUES FOR NULL, LOCKED OR EULER JOINTS.

```


C		VISP0510
	I = IABS(JNT(J))	VISP0520
	IF (I.LE.0) GO TO 90	VISP0530
	IF (IPIN(J).LT.0 .OR. IPIN(J).GT.3) GO TO 90	VISP0540
C		VISP0550
C	ZERO T1-T9 ARRAYS, VARIABLES HAD,HBD,WIJM,CV,CSA, AND CS8,	VISP0560
C	WIJ AND ANGL ARRAYS AND VARIABLES TQC,THETO AND THETOP.	VISP0570
C		VISP0580
	DO 10 L=1,42	VISP0590
10	TI(L) = 0.0	VISP0600
	CALL DOT(D(1,1,I),HT(I,I,2*J-1),DH1,3,3,3)	VISP0610
	CALL DOT(D(1,1,J+1),HT(1,I,2*J),DH2,3,3,3)	VISP0620
	CALL DOT(DH1,DH2,HD3,3,3,3)	VISP0630
C		VISP0640
C	NOTE: THIS VERSION CORRESPONDS TO OLDER VERSIONS AS FOLLOWS:	VISP0650
C		VISP0660
C	(HT) = ((HC) (H8) (HA))	VISP0670
C		VISP0680
C	(DH1) = ((A) (T2) (TI))	VISP0690
C		VISP0700
C	(DH2) = ((B) (T5) (T4))	VISP0710
C		VISP0720
C	WHERE A = T2 X T1	VISP0730
C	B = T5 X T4	VISP0740
C		VISP0750
C	(A.B A.T5 A.T4)	VISP0760
C	(HD3) = (T2.B T2.T5 T2.T4)	VISP0770
C	(T1.B T1.T5 T1.T4)	VISP0780
C		VISP0790
	HAD = HD3(3,3)	VISP0800
	IF (HAD.GT. 1.0) HAD = 1.0	VISP0810
	IF (HAD.LT.-1.0) HAD = -1.0	VISP0820
	ANGL(1) = DARCOS(HAD)	VISP0830
	ANGL(2) = 0.0	VISP0840
	IF (HD3(2,3).NE.0.0 .OR. HD3(I,3).NE.0.0)	VISP0850
*	ANGL(2) = DATAN2(HD3(2,3),HD3(1,3))	VISP0860
	CSAP = 0.0	VISP0870
	IF (NJ.NE.0.AND.IJ.EQ.4) GO TO 27	VISP0880
C		VISP0890
C	CONVERT TO INERTIAL REFERENCE SYSTEM	VISP0900
C	T3= D(I)*WMEG(I) T6=D(J+1)*WMEG(J+1)	VISP0910
C		VISP0920
C	HAD = COS TA = HD3(3,3)	VISP0930
C	WIJ = T3-T6	VISP0940
C	WJ = WIJ	VISP0950
C		VISP0960
	DO 20 L=1,3	VISP0970
	DO 15 M=1,3	VISP0980
	T3(L) = T3(L)+ D(M,L,I)* WMEG(M,I)	VISP0990
15	T6(L) = T6(L)+ D(M,L,J+1)* WMEG(M,J+I)	VISP1000

	WIJ(L)= T3(L)-T6(L)	VISP1010
20	WIJM = WIJM + WIJ(L)**2	VISP1020
	WIJM = DSQRT(WIJM)	VISP1030
	WJ(J) = WIJM	VISP1040
C		VISP1050
C	T7 = T1 X T4	VISP1060
C	HAC = T7	VISP1070
C		VISP1080
	CALL CROSS (DH1(1,3),DH2(1,3),T7)	VISP1090
	HAC = DSQRT((1.0-HAD)*(1.0+HAD))	VISP1100
C		VISP1110
C	COMPUTE CV, THE MAGNITUDE OF VISCOUS AND COULOMB TORQUE/WIJM	VISP1120
C	RA = -SGN TA DOT = WIJ.T7	VISP1130
C	AND CSA, THE MAGNITUDE OF FLEXURE TORQUE/HAC	VISP1140
C		VISP1150
	CV = VISCOS(WIJM,VISC(1,3*J-2))	VISP1160
	CREST = VISC(7,3*J-2)	VISP1170
	RA = WIJ(1)*T7(1)+WIJ(2)*T7(2)+WIJ(3)*T7(3)	VISP1180
	JSTP = 0	VISP1190
	IF (JOINTF(J).EQ.0) CSA = EFUNCT(ANGL(1),RA,SPRING(1,3*J-2),JSTP)	VISP1200
	IF (JOINTF(J).NE.0) CSA = FENTERP(ANGL(1),ANGL(2),JOINTF(J))	VISP1210
	CSAP = CSA	VISP1220
	IF (HAC.NE.0.0) CSA = CSA/HAC	VISP1230
	IF (NJ.EQ.0) JSTOP(1,1,J) = JSTP	VISP1240
	IF (IP1N(J).EQ.1) GO TO 34	VISP1250
C		VISP1260
C	FOR UNPINNED FREE JOINTS	VISP1270
C	CONVERT TO INERTIAL REFERENCE SYSTEM	VISP1280
C	T2 = D(I)**HB(NJ) T5 = D(J+1)**HB(MJ)	VISP1290
C		VISP1300
C	T8 = T2 X T5	VISP1310
C	HBD = COS TB = T2.T5	VISP1320
C	HBC = T8	VISP1330
C		VISP1340
	ANGL(3) = DATAN2(HD3(2,1)-HD3(1,2),HD3(2,2)+HD3(1,1))	VISP1350
C		VISP1360
C	RB = -SGN TB DOT = WIJ.T8	VISP1370
C	COMPUTE CSB, THE MAGNITUDE OF TORSIONAL TORQUE.	VISP1380
C		VISP1390
	RB = WIJ(1)*DH2(1,3) + WIJ(2)*DH2(2,3) + WIJ(3)*DH2(3,3)	VISP1400
	CSB = EFUNCT(ANGL(3),RB,SPRING(1,3*J-1),JSTP)	VISP1410
	IF (NJ.EQ.0) JSTOP(2,1,J) = JSTP	VISP1420
	IF (NJ.GT.0) GO TO 34	VISP1430
C		VISP1440
C	COMPUTE EFFECT OF GLOBALGRAPHIC JOINT STOP	VISP1450
C		VISP1460
27	IF (IGLOB(J).EQ.0) GO TO 34	VISP1470
	IF (DABS(HAD).GT.1.0-EPS6) GO TO 34	VISP1480
	NT = IGLOB(J)	VISP1490
	CALL HERRON(HD3(1,3),NTAB(NT+1),THETO,THETOP)	VISP1500

	JSTOP(4,1,J) = 0	VISP1510
	IF (ANGL(1).LE.THETG) GO TO 34	VISP1520
	JSTOP(4,1,J) = 1	VISP1530
	MT = NTAB(NT+5)	VISP1540
	CREST = TAB(MT+3)	VISP1550
	STH2 = 1.0-HAD**2	VISP1560
	STH = DSQRT(STH2)	VISP1570
	CTH = HAD/STH	VISP1580
	CST = DSQRT(STH2+THETOP**2)	VISP1590
	DR = (ANGL(1)-THETG)*STH/CST	VISP1600
	LT = NTAB(NT)	VISP1610
	TAB(LT) = DR	VISP1620
	TQF = FRCDL(DR,NT,1)	VISP1630
	TQC = TQF/CST	VISP1640
	CC(1) = -HD3(2,3) + HD3(1,3)*CTH*THETG	VISP1650
	CC(2) = HD3(1,3) + HD3(2,3)*CTH*THETG	VISP1660
	CC(3) = -STH*THETG	VISP1670
	DO 28 L=1,3	VISP1680
	28 T9(L) = CC(1)*DH1(L,1) + CC(2)*DH1(L,2) + CC(3)*DH1(L,3)	VISP1690
C		VISP1700
C	COMPUTE TOTAL TORQUE IN INERTIAL REFERENCE BY	VISP1710
C	TQ = -CV*WIJ + CSA*T7 + CSB*T8 + TQC*T9	VISP1720
C		VISP1730
	34 IF (NJ.EQ.0) GO TO 36	VISP1740
	CV = 0.0	VISP1750
	IF (IJ.NE.1) CSA = 0.0	VISP1760
	IF (IJ.NE.2) CSB = 0.0	VISP1770
	IF (IJ.NE.4) TQC = 0.0	VISP1780
	36 DO 37 L=1,3	VISP1790
	TQ(L,J) = -CV*WIJ(L) + CSA*T7(L) + CSB*DH2(L,3) + TQC*T9(L)	VISP1800
	37 TTI(L) = TQ(L,J)	VISP1810
	IF (NPRT(12).NE.0) WRITE (6,39)	VISP1820
	* J, CV, CSA, CSB, TQC, HAD, HAC, HBC, RA, RB,	VISP1830
	* HD3, WIJ, T7, T9,	VISP1840
	* (TQ(L,J), L=1,3)	VISP1850
	39 FORMAT(I4, 1P9D14.6/(4X, 9D14.6))	VISP1860
C		VISP1870
C	ADD TORQUE CONVERTED TO LOCAL REFERENCE BY	VISP1880
C	U2I = U2I + DI*TQ	VISP1890
C	U2J = U2J - DJ*TQ	VISP1900
C		VISP1910
	DO 40 L=1,3	VISP1920
	DO 40 M=1,3	VISP1930
	U2(L,I) = U2(L,I) + D(L,M,I)*TQ(M,J)	VISP1940
	40 U2(L,J+1) = U2(L,J+1) - D(L,M,J+1)*TQ(M,J)	VISP1950
C		VISP1960
C	STORE DATA FOR OUTPUT ROUTINE INTO PRJNT ARRAY.	VISP1970
C		VISP1980
	PRJNT(1,J) = ANGL(1)	VISP1990
	PRJNT(2,J) = ANGL(3)	VISP2000

```
PRJNT(3,J) = CSAP
PRJNT(4,J) = CSB
PRJNT(5,J) = CV*WIJM
PRJNT(6,J) = DSQRT(TQ(1,J)**2+TQ(2,J)**2+TQ(3,J)**2)
90 CONTINUE
CALL ELTIME(2,13)
99 RETURN
END
```

```
VISP2010
VISP2020
VISP2030
VISP2040
VISP2050
VISP2060
VISP2070
VISP2080
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```

NENTRY = TAB(KT+5)
KI = K1+10
K2 = 4*NENTRY + KT+2
IF (NENTRY.EQ.1) GO TO 31
DO 30 K=K1,K2,4
IF (FTIME.GT.TAB(K)) GO TO 30
KK = K
R1 = (TAB(K)-FTIME)/(TAB(K)-TAB(K-4))
GO TO 32
30 CONTINUE
31 KK = K2
R1 = 0.0
32 R2 = 1.0 - R1
DO 33 I=1,3
K= KK+I
33 FT(I) = R2*TAB(K) + R1*TAB(K-4)

C
C
C
COMPUTE PRESENTED AREA TO WIND FORCE.

CALL MAT(D(I,I,M),FT,FF,3,3,1,3,3,3)
CALL MAT(BD(7,MM),FF,AF,3,3,1,3,3,3)
FAF = FF(I)*AF(1) + FF(2)*AF(2) + FF(3)*AF(3)
IF (FAF.LE.0.0) GO TO 99
TF = TM(1)*FF(I) + TM(2)*FF(2) + TM(3)*FF(3)
BREF = DSQRT(BTS-TF*TF/FAF)
SCALE = (-BET+BREF)/(-BTE+BREF)
IF (SCALE.GE.1.0) GO TO 99
IF (SCALE.LT.0.0) SCALE = 0.0
TRACER = (BD( 7,MM)-AF(1)**2/FAF)*(BD(I1,MM)-AF(2)**2/FAF)
*      + (BD( 7,MM)-AF(1)**2/FAF)*(BD(I5,MM)-AF(3)**2/FAF)
*      + (BD(11,MM)-AF(2)**2/FAF)*(BD(15,MM)-AF(3)**2/FAF)
*      - (BD( 8,MM)-AF(1)*AF(2)/FAF)**2
*      - (BD( 9,MM)-AF(1)*AF(3)/FAF)**2
*      - (BD(12,MM)-AF(2)*AF(3)/FAF)**2
AREA = (I.0-SCALE**2) * PI / DSQRT(TRACER)

C
C
C
ADD FORCE AND TORQUES TO U1 AND U2 ARRAYS FOR SEGMENT M.

SCALE = SCALE/BTE
DO 36 I=1,3
RLM(I) = RM(I)*SCALE + BD(I+3,MM)
FT (I) = FT(I)*AREA
36 FF (I) = FF(I)*AREA
CALL CROSS (RLM,FF,TQM)
DO 39 I=1,3
UI(I,M) = U1(I,M) + FT(I)
39 U2(I,M) = U2(I,M) + TQM(I)
IF (NPRT(14).NE.0) WRITE (6,41) TIME,M,P,AREA,FT,TQM
41 FORMAT (' WIND FORCE',F14.6,I6,2F10.3,3X,3F12.5,3X,3F12.5)
99 CALL ELTIME (2,35)

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```

WIND0510
WIND0520
WIND0530
WIND0540
WIND0550
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WIND0990
WIND1000

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