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TURBULENT WAKES IN A STRATIFIED FLUID. PART II:
USER'S SUMMARY GUIDE TO "WAKE" COMPUTER PROGRAM

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<p>This document is a part of the final report on Contract N00014-72-C-0413 covering the period May 15, 1972, to June 30, 1974 and contains the user information needed to operate the WAKE program on the A.R.A.P. Digital Scientific Corporation META-4 computer system. Part I of this report summarizes the turbulent model derivation and verification, and the sensitivity of the wake collapse to changes in initial conditions.</p>		

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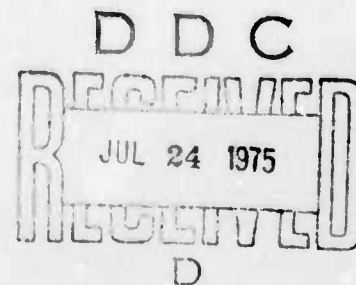


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1. INTRODUCTION

For the last two years A.R.A.P. has been developing a computer program capable of solving the three-dimensional steady flow problem of fluid motion in a stratified fluid. This work was accomplished in various stages, and is now assembled in one FORTRAN program called WAKE. This program resides on the A.R.A.P. computer system. This part of the final report summarizes the usage of WAKE and gives detailed explanations of its input requirements and output results. In Section 2 we briefly summarize the theoretical problem. In Section 3 we examine the numerical scheme used to solve the equations of motion. In Section 4 we detail the input/output specifications, including the structure of the important initial profile file. The Appendix gives a source listing of the entire WAKE program and its full subroutine complement. This guide is not intended as a full explanation of the WAKE program - only the FORTRAN listings can do that. Nor is it intended to demonstrate the conversion possibilities of WAKE to other computer facilities. Rather, with this guide a computer analyst unfamiliar with the WAKE program should be able to construct a needed set of initial profiles, grasp an overview of the numerical scheme and program structure, and produce suitably correct output from the A.R.A.P. computer facility in a fairly short period of time.

2. THE THEORETICAL PROBLEM

When a self-propelled body moves through a medium with a stratified density gradient, a wake is generated which expands behind the body as its potential energy increases. Far behind the body the potential and kinetic energies come into balance and the wake collapses. The heavier fluid, finding itself in a region of lighter background density, reestablishes the stable condition existing before passage of the body, but at the expense of the generation and transmission of internal gravity waves. The theoretical prediction of this complex physical problem has been the subject of a great deal of study. The intent of the A.R.A.P. approach is to model the generated turbulence by the technique of invariant second-order closure and to follow the buildup and collapse phase through two Brunt-Vaisala (B.V.) periods of fluid motion. A more detailed explanation of the derivation of the equations is presented in Part 1 of this final report (ref. 1). For completeness we here present the derived, modeled, approximated and normalized equations as they stand prior to numerical solution.

For the turbulence q^2 ($= \overline{u'u'} + \overline{v'v'} + \overline{w'w'}$):

$$\begin{aligned} \frac{Dq^2}{Dt} = & - \frac{2}{Fr^2} \overline{w'w'} - \frac{2q^2}{Re\lambda^2} + \frac{\partial}{\partial y} \left[\left(3v_c \frac{\overline{v'v'}}{q} \Lambda_y + \frac{1}{Re} \right) \frac{\partial q^2}{\partial y} \right] \\ & + \frac{\partial}{\partial z} \left[\left(3v_c \frac{\overline{w'w'}}{q} \Lambda_z + \frac{1}{Re} \right) \frac{\partial q^2}{\partial z} \right] - 2 \overline{u'u'}_k \frac{\partial u_i}{\partial x_k} \end{aligned} \quad (2.1)$$

For the perturbation density $\hat{\rho}$:

$$\frac{D\hat{\rho}}{Dt} = + \frac{Pr}{Re} \nabla^2 \hat{\rho} - \frac{\partial \overline{v' \rho'}}{\partial y} - \frac{\partial \overline{w' \rho'}}{\partial z} + w \quad (2.2)$$

For the mean velocities u , v , and w :

$$\frac{Du}{Dt} = + \frac{1}{Re} \nabla^2 u - \frac{\partial \overline{u' v'}}{\partial y} - \frac{\partial \overline{u' w'}}{\partial z} \quad (2.3)$$

$$\frac{Dv}{Dt} = - \frac{\partial \pi}{\partial y} + \frac{1}{Re} \nabla^2 v - \frac{\partial \overline{v' v'}}{\partial y} - \frac{\partial \overline{v' w'}}{\partial z} \quad (2.4)$$

$$\frac{Dw}{Dt} = - \frac{\partial \pi}{\partial z} + \frac{1}{Re} \nabla^2 w - \frac{\partial \overline{v' w'}}{\partial y} - \frac{\partial \overline{w' w'}}{\partial z} - \frac{\hat{\rho}}{Fr^2} \quad (2.5)$$

For the scale length Λ :

$$\begin{aligned} \frac{D\Lambda}{Dt} = v_c \frac{\partial}{\partial x_1} \left(q \Lambda \frac{\partial \Lambda}{\partial x_1} \right) - s_1 \frac{\Lambda}{q} \frac{\overline{u'_i u'_j}}{u'_i u'_j} \frac{\partial u_1}{\partial x_j} - s_2 v \frac{\Lambda}{\lambda^2} \\ - s_3 \delta_{31} \frac{\Lambda}{q} \frac{\overline{u'_i \rho'}}{Fr^2} - s_4 \frac{1}{q} \left(\frac{\partial q \Lambda}{\partial x_1} \right)^2 \end{aligned} \quad (2.6)$$

For perturbation pressure:

$$\begin{aligned} \nabla^2 \pi = - \frac{1}{Fr^2} \frac{\partial \hat{\rho}}{\partial z} - \frac{\partial^2 \overline{v' v'}}{\partial y^2} - 2 \frac{\partial^2 \overline{v' w'}}{\partial y \partial z} - \frac{\partial^2 \overline{w' w'}}{\partial z^2} \\ + 2 \frac{\partial v}{\partial y} \frac{\partial w}{\partial z} - 2 \frac{\partial v}{\partial z} \frac{\partial w}{\partial y} - \frac{\partial}{\partial x} \left(\frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right) \end{aligned} \quad (2.7)$$

For the turbulent correlations:

$$\begin{aligned}
 0 = & - \overline{u_i' u_k'} \frac{\partial u_j}{\partial x_k} - \overline{u_j' u_k'} \frac{\partial u_i}{\partial x_k} - \delta_{31} \frac{\overline{u_j' \rho'}}{Fr^2} - \delta_{3j} \frac{\overline{u_i' \rho'}}{Fr^2} \\
 & - \frac{q}{\Lambda} \left(\overline{u_i' u_j'} - \frac{\delta_{ij} q^2}{3} \right) - 2(b-f) \frac{q^3}{3\Lambda} \delta_{ij} \\
 0 = & - \overline{u_i' u_j'} \frac{\partial \rho}{\partial x_j} - \overline{u_j' \rho'} \frac{\partial u_i}{\partial x_j} - \delta_{31} \frac{\overline{\rho'^2}}{Fr^2} - \frac{Aq}{\Lambda} \overline{u_i' \rho'} \\
 0 = & - \overline{u_j' \rho'} \frac{\partial \rho}{\partial x_j} - sbq \frac{\overline{\rho'^2}}{\Lambda} \tag{2.8}
 \end{aligned}$$

A complete nomenclature may be found in Part 1. Restrictions and modifications, especially in regard to the Quasi-Equilibrium eqs. (2.8) for the turbulent correlations and the correction factor f , are also detailed in Part 1. The algebraic solution to eqs. (2.8), with the assumptions that the principle production gradients are in u and ρ , and density gradients in y are smaller than density gradients in z (for computation of f only) gives:

$$\begin{aligned}
 \overline{v'v'} &= \frac{1 - 2b + 2f}{3} q^2 \\
 \overline{v'w'_s} &= \frac{\overline{v'v'}}{c_1 Fr^2} \frac{\partial \hat{\rho}}{\partial y} & \overline{v'w'} &= \overline{v'w'_s} - \frac{q\Lambda}{3} \left(\frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right) \\
 \overline{v'\rho'} &= - \frac{Fr^2 q}{\Lambda} \overline{v'w'_s} \\
 \overline{u'v'} &= - \frac{\Lambda}{q} \left(\overline{v'v'} \frac{\partial u}{\partial y} + \overline{v'w'_s} \frac{\partial u}{\partial z} \right)
 \end{aligned}$$

$$\begin{aligned} \overline{w' \rho'} &= \frac{1}{c_2} \left[\frac{q}{\Lambda} \left(\overline{v' v'} \frac{\partial \rho}{\partial z} + \overline{v' w'} \frac{\partial \hat{\rho}}{\partial y} \right) - \frac{\overline{v' \rho'}}{bsFr^2} \frac{\partial \hat{\rho}}{\partial y} \right] \\ \overline{w' w'} &= \overline{v' v'} - \frac{2\Lambda}{qFr^2} \overline{w' \rho'} \\ \overline{u' u'} &= q^2 - \overline{v' v'} - \overline{w' w'} \\ \overline{\rho' \rho'} &= -\frac{\Lambda}{qbs} \left(\overline{v' \rho'} \frac{\partial \hat{\rho}}{\partial y} + \overline{w' \rho'} \frac{\partial \rho}{\partial z} \right) \\ \overline{u' \rho'} &= \frac{1}{c_1} \left[\frac{\partial \rho}{\partial z} \left(\overline{v' w'} \frac{\partial u}{\partial y} + \overline{w' w'} \frac{\partial u}{\partial z} \right) \right. \\ &\quad \left. - \frac{q}{\Lambda} \left(\overline{u' v'} \frac{\partial \hat{\rho}}{\partial y} + \overline{v' \rho'} \frac{\partial u}{\partial y} + \overline{w' \rho'} \frac{\partial u}{\partial z} \right) \right] \\ \overline{u' w'} &= -\frac{\Lambda}{q} \left[\frac{\overline{u' \rho'}}{Fr^2} + \overline{v' w'} \frac{\partial u}{\partial y} + \overline{w' w'} \frac{\partial u}{\partial z} \right] \end{aligned} \quad (2.9)$$

With

$$c_1 = \frac{Aq^2}{\Lambda^2} - \frac{1}{Fr^2} \frac{\partial \rho}{\partial z}$$

$$c_2 = \frac{1}{Fr^2} \left(1 + \frac{1}{bs} \right) \frac{\partial \rho}{\partial z} - c_1$$

$$f = b - \left(\frac{1-2b}{3} \right) \left\{ \frac{\Lambda^2}{q^2} \left(\frac{\partial u}{\partial y} \right)^2 - \frac{1}{c_1 c_2} \left(\frac{\partial u}{\partial z} \right)^2 \right.$$

$$\left. \left[\frac{A^2 q^2}{\Lambda^2} + \left(1 - \frac{A}{bs} \right) \frac{1}{Fr^2} \frac{\partial \rho}{\partial z} \right] - \frac{1}{c_2 Fr^2} \frac{\partial \rho}{\partial z} \right\}$$

and

$$\frac{\partial \rho}{\partial z} = \frac{\partial \hat{\rho}}{\partial z} + 1.$$

The solution procedure always involves the solution of eqs. (2.9) for the turbulent correlations and eq. (2.6) for the dynamic scale Λ . However, the solutions of the main variables q^2 , $\hat{\rho}$, u , v , w , and π are governed by the regime of interest. Thus, only q^2 , $\hat{\rho}$ and u are computed in a Phase I calculation where $Re_0 \lesssim 0.1$. Here $v = w = \pi = 0$ since the flow is far from collapse. In a Phase II calculation, we solve for q^2 , $\hat{\rho}$, v , w , and π , assuming that $u = 0$; we are here restricted to flows for which $|u_{\max}|/q_{\max} \lesssim 0.1$. When the flow situation does not fit either condition, we calculate all the variables q^2 , $\hat{\rho}$, u , v , w , and π in a Phase III calculation.

For the runs presented in Part I (ref. 1), we take our initial conditions on the main variables (when they are nonzero) to be those assembled in Table 2.1.

TABLE 2.1
 TABULATION OF NONZERO INITIAL CONDITIONS

$$r = (y^2 + z^2)^{1/2}$$

$$q^2: \quad q^2 = \begin{cases} \frac{0.0108}{(1+r^2)^2} & \text{swirl and lift-force} \\ 0.0108 \exp[-0.69 r^2] & \text{simple collapse} \end{cases}$$

$$\hat{p}: \quad \hat{p} = \begin{cases} z & z \leq 1 \\ z \exp[-2(r^2 - 1)] & z > 1 \end{cases}$$

$$u: \quad u = \begin{cases} 0.080 (1 - Cr^2) \exp[-Cr^2] & C = 3.125 \text{ momentumless} \\ -0.305 \exp[-5(r-0.2)^2] & \text{axial momentum} \end{cases}$$

$$v, w: \quad v = -\frac{Vz}{r} \quad v = \frac{(1 - \exp[-3r^2])(1.5 - r)^2}{15 r} \quad r \leq 1.5$$

$$w = \frac{Vy}{r} \quad w = 0 \quad r > 1.5$$

for swirl cases

$$v = \gamma z \left(\frac{1}{E_+} - \frac{1}{E_-} \right)$$

$$E_{\pm} = z^2 + (y \pm \ell)^2$$

$$w = \gamma \left(\frac{y-\ell}{E_-} - \frac{y+\ell}{E_+} \right)$$

$$\ell = 0.4$$

$$\gamma = \pm 0.0033$$

for trim-force cases

$$\pi: \quad \pi = 0 \text{ throughout}$$

3. THE NUMERICAL APPROACH

Equations (2.1)-(2.8) are solved in the two-dimensional y-z plane by recasting them in finite difference form and applying the ADI technique of Peaceman, Rachford and Douglas (refs. 2 and 3). In this method we construct a two-dimensional grid in the y and z directions and march in the x direction as we follow the flow development downstream of the initial conditions. In the y and z directions the first and second derivatives are approximated by centered differences (spacing is variable), while forward differences are used in x (ref. 4). Inputted tolerance parameters control the size and speed of the marching direction, and the spacing variability and intensity.

At the beginning of a new step in Δx (perhaps the start of the run itself), the program performs an implicit sweep in one direction in $\Delta x/2$ and then sweeps in the other direction in $\Delta x/2$ to complete the ADI procedure. The initial sweeping direction alternates with each full step to unbiased any solution near the edge of an expanding profile. These steps have used the current values of q^2 , \hat{r} , u , v , w , and π , together with the gross scale Λ to step forward in x. Although the main variables are coupled by eqs. (2.1)-(2.5) and (2.8), we choose to use current values wherever necessary to decouple the equations completely. Solutions at the next x are then swept to compute maximum values, maximum changes, and various integrals of interest, along with the updated scales Λ_y and Λ_z . The next step Δx_{new} is computed based on the changes taken by the present step in relation to the maximum change permitted. The profiles are then swept again to update the pressure forcing function - the right side of eq. (2.7), and to compute the algebraic turbulence via eq. (2.8).

WAKE then calls the pressure iteration subroutine. It works as a miniature WAKE program by adding a $-\partial\pi/\partial t$ term to the left side of eq. (2.7) and performing iterations in π stepping from the current solution to the next steady state estimate. Appropriate output routines are then called, followed by the necessary set of routines that inspect the curvatures in the y and z directions, readjusting the profile again per inputted tolerance criteria. A new step is then taken.

The mainline program is called WAKE. The Appendix of this report contains a complete listing of WAKE and its subroutines; in-house disk I/O routines and other straightforward assembler routines are not included. These routines control the monitoring of the disk files storing the large array of data necessary to execute the calculation.

It may be worthwhile to realize that the file record length is 24 words, broken into four sections of six words each. The first section contains TV(6), where TV(1) = $\partial u/\partial y$; TV(2) = $\partial u/\partial z$; TV(3) = $\partial\rho/\partial y$; TV(4) = $\partial\rho/\partial z$; TV(5) = F; and TV(6) = π . The second section holds XV(6) at the present step value; the third holds the intermediate (first-sweep) values of XV(6); and the fourth section holds the new step values of XV(6). Here XV(1) = q^2 , XV(2) = p ; XV(3) = u; XV(4) = v; XV(5) = w; and XV(6) = Λ .

4. INPUT CONTROL

Initialization of a WAKE run requires the generation of an initial profile file (giving the desired initial conditions to the desired variables) and the input of an appropriately punched deck of computer cards. The initial file must be formed in a way totally compatible with the sample generation program shown at the end of the Appendix. It must be structured as follows.

First word: the initial x position value.
 Second word: the number of points NY in the y direction and NZ in the z direction.
 Next NY words: the NY independent y values of the y direction mesh (monotonically increasing).
 Next NZ words: the NZ independent z values of the z direction mesh (monotonically increasing).
 Next NY*NZ words: the complete corresponding mesh values for the first initialized dependent variable. The file must contain these NY*NZ values in blocks of 10 y values at a time (for all z), until the last block contains enough values to reach NY. Thus, the blocks would be built as 10*NZ, 10*NZ, 5*NZ if NY=25.
 Next NY*NZ words: the second initialized variable.
 .
 .
 .
 Next word: - 1.0 to signal end-of-data.

With the disk buffering currently in operation, the file inversion program PBFFI must be called to invert the initial file four sectors at a time.

The input cards to the WAKE program (example copies are included in the Appendix) are as follows:

Card 1: INFLG, N, JOBE (3I4 format code). INFLG = 0 on a restart, = 1 on a start. N = 1 permits a new run to start before completing the current run; N = 0 does not. JOBE = value, the upper minute limit on current job execution time. If JOBE = 0, the program will not test for the job time.

Card 2: NRUNI, CMNT (I4, 19A4). If NRUNI = value, the current run is given this run number; if NRUNI = 0, the run number counter in the common file is updated by one. CMNT is a 19 element vector containing any desired comments (printed at the start of the run).

Card 3: NSTMX, NSTSI, XMIN, XMAX, DELX, MXHRS, LAMIN (2I4, 3F8.3, 2I4). NSTMX sets the maximum number of steps permitted for the run. NSTSI sets the initial step value, typically = 0. XMIN is the initial x value. XMAX is the maximum x value (the program terminates when reaching XMAX). DELX is the initial Δx spacing. MXHRS is the run time maximum hours (termination also). LAMIN = 0 signals a normal run with turbulence; LAMIN = 1 signals a run with laminar flow.

Card 4: MXRY, LYLFF, MXRZ, LZLFF (4I4). MXRY and MXRZ are the maximum number of mesh points possible in the y and z directions; the most possible currently is 40. LYLFF and LZLFF set the lower boundary flags, = 0 implies a free lower boundary; = - 1 implies a reflecting lower boundary.

Card 5: NRFV (14I4). NRFV (7,2) gives the reflection properties for the seven variables q^2 , \hat{p} , u, v, w, Λ , π across the two axes. The first seven integers give the variable properties across the z axis (+ to - y); the second seven give their properties for + to - z across the y axis. The integer entry is 0 if the variable is zero at the axis, and 1 if the slope of the variable is zero across the axis.

Card 6: VSCAV (5F8.3). VSCAV is a five element array giving the scaling factors for q^2 , $\hat{\rho}$, u , v , w ; typically = 1.0.

Card 7: VWTFV (5F8.3) is a five element array giving the weighting factors for q^2 , $\hat{\rho}$, u , v , w . Typically, weight = 1.0 is given to q^2 , $\hat{\rho}$ and u ; while = 0.0 is given to v and w (they do not control anything).

Card 8: ZEROV (7F8.3). ZEROV is a seven element array giving the edge values of q^2 , $\hat{\rho}$, u , v , w , Λ and π , where q^2 , u and π must = 0.0, but nonzero values are possible for $\hat{\rho}$, v and w . The edge value for Λ is formed internally within the program.

Card 9: EPSN, EPSX, EPSS, ECMN, ECMX (5F8.3). This card gives the run tolerances, and is used with the scaling and weighting factors to set running noise levels (EPSN times the appropriate VSCAV entry), maximum changes (EPSX), edge tolerances (EPSS), minimum curvature (ECMN), and maximum curvature (ECMX). Typically, EPSN = 0.001, EPSX = 0.05; EPSS = 0.001; ECMN = 0.02 and ECMX = 0.05.

Card 10: DXMAX, DXMIN, DXFMX, BUFAC, FCUR, DFFMN, DFFMX, DFRMX (8F8.3). This card sets the spacing in the three directions. In the marching direction x , DXMAX is the maximum step size permitted; DXMIN is the minimum size, = 0.00001; DXFMN is the maximum rate at which Δx can grow and the solution march downstream, = 1.5; BUFAC is the maximum factor (times EPSX) that a variable may change before the step size is reduced and the step tried again, = 2.0; FCUR multiplies ECMN and ECMX when curvatures require too many points, = 1.1; DFFMN is a minimum spacing factor (times the width of the profile) below which a point cannot be inserted, = 0.05; DFFMX is a maximum spacing factor above which a point must be added, = 0.05; and DFRMX is the optimum spacing ratio, traditionally set equal to 2.02.

Card 11: NIOLP, NIOPP, NFOLP, NTOPP, NTOLP, NSOLP, NIAAF, LOU (8I4). The first six parameters control printout as a function of the number of steps taken by the solution. Thus, if NIOLP = 5, every fifth step will generate an intermediate line printer record of x , Δx , Λ_y , Λ_z , maximum values of all variables, and integrals of potential and kinetic energies, and momentum. NIOPP generates intermediate disk storage; NFOLP causes a print of normalized mesh output along a specifically inputted y and z value; NTOPP generates a disk save of the total variable profiles; NTOLP causes a line print/plot of the variable profiles; and NSOLP yields a print of nonnoise turbulence to the line printer. NIAAF sets the frequency of profile readjustment, = 2 from stability considerations. LOU = -1 forces only a printer plot; = +1 forces only a number plot; = 0 permits both printer plot and full profile output to the line printer for every requested variable.

Card 12: XOUTV (10F8.3) gives specific x values at which total printouts and disk storage is requested (overrides the output control parameters on the previous card).

Card 13: NSTAT, NSTBC, NUFF, LIBUF, LFBUF, LTBUF, NSTPR, IDSV (14I4). NSTAT controls the solution configuration desired: NSTAT = 1 for the solution of q^2 , \hat{p} , u ; NSTAT = 2 for q^2 , \hat{p} , v , w , π ; and NSTAT = 3 for all variables. NSTBC prevents a backup and retry of a step for the initial number of steps (typically = 5) set by NSTBC. NUFF sets the smooth transition to an XOUTV value, = 4. LIBUF, LFBUF and LTBUF control intermediate, full, and total printouts on a backup (0 or 1). NSTPR is the number of steps in the pressure iteration loop, ≤ 5 . IDSV is an array of seven elements giving the disk storage switch for each of the seven variables (= 0 if the variable is not to be stored, as must be the case currently for Λ ; = 1 if the variable is to be stored for future plotting purposes).

Card 14: RE, G, PR, AS, A, B, BETA, C, S (9F8.3). This card gives the Reynolds number, (Froude number)⁻², Prandtl number, and turbulence model parameters currently set at AS = 2.5; A = 0.75; B = 0.125; BETA = 0.0; C = 0.1; S = 1.8.

Card 15: DC, U, RIS, DRDZ, SCALE, PCRIT, SCALM, SPORS, CPOR (9F8.3). DC = 0.3 is the diffusion coefficient; U is the free stream velocity = 1.0; RIS = 0.25 is the stability cutoff of the Richardson number; DRDZ is the constant background $\partial\rho_0/\partial z$. If DRDZ = 0.0, WAKE will read card 20. SCALE sets the initial value of the scale length. PCRIT = 0.005 is the value of the ratio of maximum change to maximum value below which the pressure iteration is said to converge (herewith, 0.5%). SCALM = 0.01 is the minimum scale length permitted. SPORS is the square of the distance to the wave-absorbing liner, normalized by Λ ; and CPOR is the strength of the liner itself. The liner strength increases exponentially with a power of $CPOR*(r^2 - SPORS)$.

Card 16: S1, S2, S5, S6, S7, S8, LSCAL (6F8.3, I4). The values of S1 - S8 set the constants in the dynamic scale equation. LSCAL = 0 means the scale equation is computed but does not influence the other variables. Currently, $s_3 = S5$; $s_4 = S6 = S7 = \frac{1}{2}S8$.

Card 17: QCUT, DIVP, DIVF, PNORM, PCUT, CMU, XFACT, XZERO, YOUT, ZOUT (10F8.3). QCUT = 0.001 is the factor times the current maximum value of q^2 that sets the computational noise level of q^2 . If a local value of q^2 is below $QCUT*q_{max}^2$, that point is not considered when constructing the various integrals of interest. Re^{-1} is given the value of CMU, not RE^{-1} , at points beyond a squared distance, normalized by Λ , greater than PCUT (= 40). This procedure is a further attempt to stabilize the solution. DIVP = 0.1 is the fraction of DXMAX setting the minimum value of the step size Δx entering the calculation for the corrective divergence effect, the last term in eq. (2.7).

When the program Δx_{new} is below $\text{DIVP} * \text{DXMAX}$, the divergence correction may overwhelm the physics taking place, typically during the first few steps of a run. $\text{DIVF} = 2.0$ is the accepted value given to the effectiveness of the divergence term, so that $\partial/\partial x \approx -u/2\Delta x_{\text{new}}$. $\text{PNORM} = 1.0$ normalizes the pressure step-size factors that yield the step-size in the pressure iteration (ref. 4). The pressure step is $\Delta t(1) = \text{PNORM} * (\text{YMAX}-\text{YMIN}) * (\text{ZMAX}-\text{ZMIN})/\text{PN}(1)$, where PN is (10.0, 30.0, 60.0, 100.0, 150.0). XFACT and XZERO give the rational distance downstream, so that $(X/D) = \text{XFACT} * X + \text{XZERO}$. Finally, YOUT and ZOUT are the values of y and z along which the full printout is computed for output display.

Card 18: FNAME (8A4) is the name of the disk files to be used during program execution, and are the working file (WAKWF), the gamma matrix file (WAKGM), the global intermediate save file (WAKGL) and the total profile plot save file (WAKPL). The common file (WAKCM) is entered into WAKE by a data statement.

Card 19: FILEN , ISTAT , ITYPE , LZMAX , LPRFL , IFULL (A4, A1, 5I4). This card controls the location of the initial profiles, and provides start conditions on various aspects of the WAKE program. When $\text{ITYPE} = -1$, FILEN is ignored and the initial profiles are sought in the entered profile plot file. When $\text{ITYPE} = 0$, FILEN gives the name of the file containing the initial profiles. For $\text{ITYPE} > 0$, these initial profiles are assumed to have been generated by the axisymmetric program JETMN . ISTAT is the counterpart of NSTAT and gives the run statistic for the initial profiles (1, 2 or 3). When $\text{LZMAX} = 0$ the program keeps track of the spread in Λ_z and prints and stores the running profiles at the first point of nonmonotonic behavior in Λ_z . Then $\text{LZMAX} = 1$ so that the procedure will not repeat. When $\text{LZMAX} = -1$, the scales Λ_y and Λ_z are fixed at the SCALM value entered on card 15. $\text{LPRFL} = -1$ is the standard operating mode of the pressure loop, and signals to the body of the WAKE program

that the iteration is complete. When LPRFL = 0 on initialization, the pressure iterations are performed prior to the first step DELX in q^2 , $\hat{\rho}$, u , v , w . IFULL = 1 forces a total printout to the line printer of the initial profiles; IFULL = 0 does not.

Card 20: ZL, DRDZH (2F8.3). When DRDZ = 0.0 on card 15, card 20 is read. Above $z = 0.0$ and below $z = ZL$, the background density gradient is set to DRDZH. For $ZL < z < 0.0$, $DRDZ = -10^{-6}$.

With the reading of these twenty cards, WAKE will begin computation. Beside the intermediate output described above, several integrals and functional values are printed every step by the pressure iteration and WAKSC subroutines. The heading above each value is chosen to give a quick identification of that value. The normalized divergence error indicates the closeness to which our calculation is maintaining $\nabla \cdot \bar{v} = 0$. The various kinetic and potential energy components give an indication of energy distribution within and outside the turbulent wake. The printout "error" of the pressure iteration should be disregarded since the pressure iteration scheme currently in use has evolved beyond the usefulness of "error". Otherwise, printout in WAKOT is explained when it is printed. The plot file is stored in the same manner that the initial profile file is constructed, only with multiple values of x , one set of data following the other.

The switches on the META-4 console permit on-going changes to the output scheme presented above. The switches used here are:

- 0: terminates a run during the pressure iteration loop
- 1: forces an intermediate line printer output
- 2: forces a full line printer output at YOUT and ZOUT
- 3: forces a total line printer output
- 4: forces an intermediate printout to the disk file

- 5: forces a total printout to the disk file
- 6: forces a total line printer output of the turbulence distributions
- 7: forces a printer picture of the main variables
- 13: terminates a run after a step in Δx (including the pressure iteration) has been completed
- 14: prints the full reflection vector on run initialization

There is, of course, no substitute for the actual program language. A copy of the FORTRAN logic is presented in the Appendix. The potential user must be warned that the weak link in the program is the capacity of the pressure iteration loop to maintain a consistent pressure solution behind the running solution of q^2 , $\hat{\rho}$, u , v and w . The cross velocities v and w will react rapidly to a degenerating pressure field, but they react slowly to a build-up of the density field prior to collapse. The WAKE program runs slowly on the A.R.A.P. facility; a 24 hour run is standard when trying to extend collapse dynamics to one B.V. Since this program is a "one-man" operation, extreme care must be taken in the input of the data cards. Internal data consistency checks are simply not there.

5. REFERENCES

1. Lewellen, W. S., M. Teske and Coleman duP. Donaldson: "Turbulent Wakes in a Stratified Fluid," Part I, A.R.A.P. Report No. 226, 1974.
2. von Rosenberg, D. U.: Methods for the Numerical Solution of Partial Differential Equations, Elsevier Press (1969), p. 87.
3. Roache, P. J.: Computational Fluid Dynamics, Hermosa Publishers (1972), p. 180-185, 194-195.
4. Sullivan, R. D.: "A Program to Compute the Behavior of a Three-Dimensional Turbulent Vortex," ARL TR 74-0009 (1974), p. 15.
5. Carnahan, B., H. A. Luther and J. O. Wilkes: Applied Numerical Methods, Wiley and Sons (1969), pp. 452-453, 508.

APPENDIX

This Appendix contains the FORTRAN listing of the complete WAKE program as programmed at A.R.A.P. The first listing is the mainline WAKE followed by the listing of common, followed by the called subroutines in alphabetical order. WAKE consumes all 32 K of core storage, requiring every subroutine called by the mainline to be Located, and subroutines within these routines (particularly WAKMY and WAKMZ) to be Scaled. Data and program storage would push beyond 200 K on a larger machine.

The last program in the Appendix gives a sample indication of the structure of a FORTRAN program generating the initial profile file. Following this program is a listing of an example input deck.


```
WAKE.S(0105)
*IOCS(2501 READER,1403 PRINTER)
**WAKE - STRATIFIED SUBMARINE WAKE MAINLINE
C
C THIS IS THE STRATIFIED SUBMARINE WAKE MAINLINE
C
*COPY (CMWAK)
C
C INITIATE THE RUN
C
    CALL WAKIN
    IF (LSTFL) 20,20,8
C
C INTEGRATE THE EQUATIONS
C
5    GO TO (7,6),NSS
6    CALL WAKSZ
    GO TO (10,7),NSS
7    CALL WAKSY
    GO TO (6,10),NSS
C
C INITIALIZE THE PROFILES
C
8    CALL WAKPI
C
C COMPUTE AUXILIARY QUANTITIES
C
10   CALL WAKAC
C
C CHECK SOLUTION VALUES
C
20   CALL WAKAL
    IF (LMLFL) 22,30,5
C
C COMPUTE THE SUPEREQUILIBRIUM VALUES
C
22   CALL WAKSC
    IF (NSTAT-1) 24,30,24
C
C COMPUTE PRESSURE SOLUTION
C
24   CALL WAKPC
C
C OUTPUT RUN RESULTS
C
30   CALL WAKPP
    CALL WAKOT
    IF (LMLFL) 40,20,20
C
C AUTOPOINT ADJUST PROFILES
C
40   IF (LIAAF) 50,20,50
50   IEND=NRST+JEND-1
    CALL WAKAA(D2DZM,ZOLDV,ZNEWV,NRNZV,NRST,IEND,MXRZ,LZFAF,NPNZ,
1    LZLFF,2)
    CALL WAKAA(D2DYM,YOLDV,YNEWV,NRNYV,NYPS,NYPE,MXRY,LYFAF,NPNY,
1    LYLFF,1)
    IF (LFCUR) 30,60,30
60   CALL WAKAZ
```

A-2

GO TO 20

END

CART 10 0105 DB ADDR 3080 DB CNT 0078

CMWAK.S(0105)

DIMENSION ZMV(20),ZV(20),ZPV(20)

C

COMMON IOLAY,IYPSN,NMOVE,NK,JOBE,NOUT,BUFR(1284),BUFS(1284)
 COMMON NWR,NWWZF,NPISN,NCOMT,NWVEC,IBOT,ITOP
 COMMON NPUS,JZ,JY,LZFAF,LYFAF,LIAAF,NMAT,NVAR,NVART,NMK
 COMMON LIOLF,LLOPF,LFOLF,LTOPF,LTOLF,LSOLF,LSTFL,LMLFL
 COMMON LTRNF,LBURF,LPKRF,LUVCF,LOVFF,LFCUR,JERR
 COMMON YM,Y,YP,FMU,XK,CVV,BBETA,HBETA,BBS,Q,DXI,CWS,SCAL
 COMMON ZNEWV(40),YNEWV(40),NRNZV(40),NRNYV(40),NPNZ,NPNY
 COMMON IROWT,IROWA,IROWR,IROWG,MOOD,IMAPV(4),JSTAT

C

COMMON ZM,IYPSM,IYPEM,XMMV(6),XMYV(6),XMPV(6)
 COMMON Z,IYPS,IYPE,XZMV(6),XV(6),XZPV(6)
 COMMON ZP,IYPSP,IYPEP,XPMV(6),XPYV(6),XPPV(6)
 COMMON TZMV(6),TV(6),TZPV(6),TPYV(6),TMYV(6)
 COMMON AV(6),GM(16),KOWB(18,40,3),KOWG(16,40)
 COMMON XMAT(6),YMAT(6),ZMAT(6),DVEC(24)
 COMMON ZA,IVECA,IVECB,IRFV(6,4)
 COMMON SLNID(3),GAMID(3),GLOID(3),PLTID(3),COMID(3)

C

COMMON NSTMX,NSTST,XMIN,XMAX,NG,NP,NSS,NRUN,KLOK(6)
 COMMON NYPS,NYPE,PXKY,NRST,JEND,MXRZ,LSCAL,LENDF,DIFFMN,CMU
 COMMON EPSN,EP SX,EPSS,ECMN,ECMX,VSCAV(5),VWTFV(5)
 COMMON DXMAX,DXMIN,DXFMX,BUFAC,DIFFMX,DFRMX,DXSAV,X,XP,FCUR
 COMMON NPTS,NIULP,NIOPP,NFOLP,NTOPP,NTOLP,NSOLP,NSTPK,LPRFL
 COMMON NIAAF,NSTAI,NSTBC,NUFF,LIBUF,LFBUF,LTBUF
 COMMON XOUTV(10),YOLDV(40),ZOLDV(40),IYPSV(40),IYPEV(40)
 COMMON KE,G,PR,DC,AS,S,A,B,BETA,C,U,RIS,DRUZ,PCRIT,SCALM
 COMMON LAMIN,MXHS,LOUT,LZMAX,DX,CVS,D2DYM(40),D2DZM(40)
 COMMON EPSXV(5),EPSSV(5),ECMXV(5),XMOM,XPE,XKE,TURBX(10)
 COMMON FMAXV(7),YMAXV(7),ZMAXV(7),TMAXV(7),GMAXV(7)
 COMMON DEPST,DEPSI,SPORS,CPOR,PNORM,PCUT,QCUT,DIVP,DIVF
 COMMON S1,S2,S5,S6,S7,S8,XFACT,XZERO,SCALE,YSCAL,ZSCAL
 COMMON ZEROV(7),NKFV(7,2),IDSV(7),LDRDZ,DRDZL,DRDZH
 COMMON CMNT(19),FNAME(8),LYLFF,LZLFF,YOUT,ZOUT,SPACR(10)

C

EQUIVALENCE (ZMV(1),ZM),(ZV(1),Z),(ZPV(1),ZP)

CART ID 0105 DB ADDR 4340 DB CNT 004A

WAKAA,S(0105)

**WAKAA - STRATIFIED SUBMARINE WAKE, AUTOPOINT ADJUST PROFILES
SUBROUTINE WAKAA(D2DM,FOLDV,FNEWV,NRNV,ISTR,IEND,MXP,LFAF,NPN,
1 LFLFF,LL)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM DETERMINES THE NEW SET OF POINTS
C NEEDED TO SATISFY ERKOK TOLERANCES

C

DIMENSION D2DM(40),FOLDV(40),FNEWV(40),NRNV(40),JPOS(2)

*COPY (CMWAK)

C

DATA JPOS/1HY,1HZ/

C

1000 FORMAT(/,33H CURVATURE TOLERANCES RELAXED IN ,A1,E15.5)

C

IOLAY=11

FNEWV(1)=FOLDV(ISTR-1)

NRNV(1)=ISTR-1

DFMIN=OFFMN*(FOLDV(IEND+1)+FOLDV(ISTR-1))

DFMAX=OFFMX*(FOLDV(IEND+1)-FOLDV(ISTR-1))

ISTRX=ISTR+LFLFF

RATIO=ECMX/ECMN

FCURV=1.0

C

C FORWARD PASS TO DETERMINE NEW PROFILE POINTS

C

100 JN=1

DFNEW=1.0E10

DO 128 J=ISTRX,IEND

F=FOLDV(J)

FP=FOLDV(J+1)

IF (J-ISTR) 1101,1102,1102

1101

FM=F+FP

GO TO 1104

1102

FM=FOLDV(J-1)

1104

DFM=F-FM

DFP=FP-F

DFT=DFM+DFP

I=NRNV(JN)

IF (J-ISTR) 123,1106,1106

1106

IF (I) 120,120,111

111

IF (I+1-J) 120,112,112

112

DFNEW=1.0E10

IF (JN-1) 114,114,113

113

DFNEW=FNEWV(JN)-FNEWV(JN-1)

114

IF (DFT-DFMAX) 1145,1145,116

1145

IF (DFT*DFT*D2DM(J)*RATIO-FCURV) 115,115,116

115

IF (DFT/DFNEW-DFRMX) 126,126,116

116

IF (DFM/DFNEW-DFRMX) 117,117,119

117

IF (DFM-DFMAX) 118,118,119

118

IF (DFM*DFM*D2DM(J)-FCURV) 120,120,119

119

IF (DFM-DFMIN) 120,1195,1195

1195

JN=JN+1

CALL WAKOJ(D2DM(J-1),D2DM(J),DFM,DFNEW)

FNEWV(JN)=FM+DFM

NRNV(JN)=0

120

JN=JN+1

FNEWV(JN)=F

NRNV(JN)=J

```

DFNEW=FNEWV(JN)-FNEWV(JN-1)
IF (DFP/DFNEW-DFRFX) 123,123,125
123 IF (DFP-DFMAX) 124,124,125
124 IF (DFP*DFP*O2DM(J)-FCURV) 126,126,125
125 IF (DFP-DFMIN) 126,1255,1255
1255 JN=JN+1
CALL WAKDS(O2DM(J),O2DM(J+1),DFP,DFNEW)
FNEWV(JN)=F+DFP
NRNV(JN)=0
126 IF (JN+4-MXP) 128,160,160
126 CONTINUE
JN=JN+1
FNEWV(JN)=FOLDV(IEND+1)
NRNV(JN)=IEND+1

C
C BACKWARD PASS OF NEW POINTS TO SATISFY RATIO CRITERION
C
JS=0
130 JP=JN+JS
FP=FNEWV(JN)
FNEWV(JP)=FP
NRNV(JP)=NRNV(JN)
DO 141 J=3,JN
I=JN+2-J
F=FNEWV(I)
NR=NRNV(I)
JP=JP-1
IF (JS) 132,132,131
131 FNEWV(JP)=F
NRNV(JP)=NR
132 FM=FNEWV(I-1)
DFP=FP-F
DFM=F-FM
IF (DFM/DFP-DFRFX) 140,140,134
134 NRM=NRNV(I-1)
IF (NR*NRM) 140,140,135
135 DFO=DFM
CALL WAKDS(O2DM(NR),O2DM(NRM),DFO,DFP)
FO=F-DFO
IF (NR-NRM-2) 137,136,137
136 NR=NR-1
F=FOLDV(NR)
IF (ABS(F-FO)-DFM/DFRFX) 138,138,137
137 NR=0
F=FO
138 JP=JP-1
IF (JS) 140,140,139
139 FNEWV(JP)=F
NRNV(JP)=NR
140 FP=F
141 CONTINUE
C
C CHECK FOR POINTS ADDED TO SATISFY RATIO CRITERION
C
IF (JS) 142,142,150
142 JS=2-JP
IF (JN+JS+4-MXP) 143,143,160
143 IF (JS) 150,150,130
C

```

C CHECK WHETHER PROFILE MUST BE REORGANIZED

C

```
150  LFAF=0
      NR=IISTR-1
      JN=JN+JS
      DO 156 J=1,JN
      NKN=NRNV(J)
      IF (NRN-NR) 151,155,151
151  LFAF=1
      GO TO 1565
155  NR=NR+1
156  CONTINUE
1565  NPN=JN
      IF (FCURV-1.0) 158,158,157
157  WRITE (NOUT,1000) JPOS(LL),FCURV
158  RETURN
```

C

C MAXIMUM POINTS EXCEEDED ON AUTOPOINT ADJUSTMENT

C

```
160  FCURV=FCURV*FCUR
      IF (FCURV-1.0E10) 100,180,180
180  LFCUR=LL
      RETURN
      END
CART ID 0105  DB ADDR 2E50  DB CNT 011A
```

WAKAC.S(0105)

**WAKAC - STRATIFIED SUBMARINE WAKE, AUXILIARY CALCULATIONS
SUBROUTINE WAKAC

C
C THIS SUBROUTINE IN THE WAKE PROGRAM PERFORMS A NUMBER OF TASKS
C AUXILIARY TO THE SOLUTION OF THE SYSTEM OF EQUATIONS
C
C 1) COMPUTES MAXIMUM ABSOLUTE VALUE FOR EACH VARIABLE AND Y AND Z
C LOCATIONS OF SAME, MAXIMUM STEP CHANGE OF VARIABLES, AND
C MAXIMUM X DERIVATIVES
C
C 2) COMPUTES FOR EACH Z ROW THE MAXIMUM SECOND DERIVATIVE
C WITH RESPECT TO Z FOR ALL Y
C
C 3) COMPUTES FOR EACH Y COLUMN THE MAXIMUM SECOND DERIVATIVE
C WITH RESPECT TO Y FOR ALL Z
C
C 4) CONSTRUCTS THE MESH VALUE PRINTOUT
C
C 5) COMPUTES THE APPROPRIATE LENGTH SCALES

DIMENSION VALUE(40),TOTAL(7,40,2),PSIV(40)

*COPY (CMWAK)

EQUIVALENCE (TOTAL(1,1,1),ROWG(1,1)),(VALUE(1),NRNZV(2))
EQUIVALENCE (PSIV(1),ZNEWV(1)),(GM(1),TKE),(GM(2),VKE)
EQUIVALENCE (GM(3),RPE),(GM(4),WPE),(GM(5),WKE)
EQUIVALENCE (GM(6),AREA),(GM(7),PSIM),(GM(8),XLIFT)

C
C ZERO PERTINENT VARIABLES
C

IOLAY=5
MOOD=1
LFL=NPTSN-NSTST
PLANE=1.0/FLOAT(LYLFF+2)/FLOAT(LZLFF+2)
XMUM=0.0
XPE=0.0
TKE=0.0
VKE=0.0
RPE=0.0
WPE=0.0
WKE=0.0
AREA=0.0
PSIM=0.0
XLIFT=0.0
CALL SFVFL(0.0,PSIV,MXRY)
CALL SFVFL(0.0,FMAXV,4*NVART)
DO 40 I=1,2
DO 35 JY=1,40
CALL SFVMV(ZEROV,TOTAL(1,JY,I),NVART)

35

CONTINUE

40

CONTINUE

CALL SFVFL(0.0,D2UYM,40)

CALL SFVFL(0.0,D2UZM,40)

CALL WAKSE(ECMX,ECMXV)

NYPSX=NYPS+LYLFF

DO 50 JY=NYPSX,NYPE

IF (YOUT-YOLDV(JY)) 60,55,45

45

IF (YOUT-YOLDV(JY+1)) 55,50,50

50

CONTINUE

```

55   RATY=(YOUT-YOLDV(JY))/(YOLDV(JY+1)-YOLDV(JY))
C
C   INITIALIZE FOR PASSING THROUGH PROFILE
C
60   IROWA=2
      IROWR=4
      IF (LSTFL) 96,96,95
95   IROWR=2
96   NRSTX=NRST+LZLFF
      NREND=NRST+JEND-1
      NPOS=NRST-1
      CALL WAKRR(NRST-1,ZV)
      CALL WAKRR(NRST,ZPV)
      DO 250 NR=NRST,NKEND
      PSIH=0.0

C
C   READ THREE SURROUNDING ROWS AND TEST FOR SELECTED Z IN DOMAIN
C
      IF (NR-NRST) 104,105,103
103  NPOS=NR
      CALL SFVMV(Z,ZM,NWWZF)
      CALL WAKMR(2,1)
      CALL SFVMV(ZP,Z,NWWZF)
      CALL WAKMR(3,2)
      CALL WAKRR(NR+1,ZPV)
      GO TO 105
104  ZM=Z+Z-ZP
105  DZM=Z-ZM
      DZP=ZP-Z
      DZT=ZP-ZM
      LYFAF=0
      IF (ZOUT-ZM) 107,1065,106
106  IF (ZOUT-Z) 1065,107,107
1065 LYFAF=1
      RATZ=(ZOUT-ZM)/(Z-ZM)

C
C   STEP THROUGH ALL Y POINTS COMPUTING AUXILIARY QUANTITIES
C
107  Y=YOLDV(IYPS-1)
      YP=YOLDV(IYPS)
      CALL WAKMP(IROWR,NR+1,IYPS-1,XPYV,1)
      CALL WAKMP(IROWR,NR,IYPS-1,XV,1)
      IF (NR-NRST) 108,109,109
108  CALL WAKRF(XPYV,XMYV,2)
      GO TO 110
109  CALL WAKMP(IROWR,NR-1,IYPS-1,XMYV,1)
110  IYPSX=IYPS+LYLFF
      IF (LFL) 112,112,111
111  CALL WAKMP(IROWA,NR,IYPS-1,AV,1)
112  CALL WAKMP(IROWR,NR+1,IYPS,XPPV,1)
      CALL WAKMP(IROWR,NR,IYPS,XZPV,1)
      IF (NR-NRST) 113,114,114
113  CALL WAKRF(XPPV,XMPV,2)
      GO TO 115
114  CALL WAKMP(IROWR,NR-1,IYPS,XMPV,1)
115  DO 200 JY=IYPSX,IYPE
      IF (JY-IYPS) 116,117,117
116  CALL WAKRF(XPPV,XPMV,1)
      CALL WAKRF(XZPV,XZMV,1)

```



```

CALL WAKRF(XMPV,XPMV,1)
YM=Y+Y-YP
GO TO 130
117 IF (LFL) 120,120,119
119 CALL WAKMP(IROWA,NR,JY,AV,1)
120 CALL SFVMV(XPYV,XPMV,NMOVE)
CALL SFVMV(XV,XZMV,NMOVE)
CALL SFVMV(XMYV,XMMV,NMOVE)
YM=Y
Y=YP
YP=YOLDV(JY+1)
CALL WAKMP(IROWR,NR+1,JY+1,XPPV,1)
CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
IF (NR-NRST) 125,128,128
125 CALL WAKRF(XPPV,XMPV,2)
GO TO 130
128 CALL WAKMP(IROWR,NR-1,JY+1,XMPV,1)
130 DYM=Y-YM
DYP=YP-Y
DYT=YP-YM

C
C PERFORM AUXILIARY COMPUTATIONS FOR EACH VARIABLE
C
DO 145 I=1,NWVEC
IF (LFL) 1406,1406,1402
1402 TEM=ABS(XV(I)-AV(I))
IF (TEM-TMAXV(1)) 1406,1406,1403
1403 TMAXV(I)=TEM
1406 TEM=ABS(XV(I))
IF (TEM-FMAXV(1)) 142,142,1407
1407 FMAXV(I)=TEM
YMAXV(I)=Y
ZMAXV(I)=Z
IF (I-1) 1408,1408,142
1408 NKL=NR
JYL=JY
142 IF (LIAAF) 143,145,143
143 IF (I-NVAR) 144,144,145
144 D2DY=((XZPV(I)-XV(I))/DYP-(XV(I)-XZMV(I))/DYM)/DYT/ECMXV(I)
D2DZ=((XPYV(I)-XV(I))/DZP-(XV(I)-XMYV(I))/DZM)/DZT/ECMXV(I)
TEM=ABS(D2DY)
IF (TEM-D2DYM(JY)) 1447,1447,1446
1446 D2DYM(JY)=TEM
1447 TEM=ABS(D2DZ)
IF (TEM-D2DZM(NR)) 145,145,1448
1448 D2DZM(NR)=TEM
145 CONTINUE
C
C STORE MESH OUTPUT VALUES
C
IF (LYFAF) 1515,1515,150
150 DO 151 I=1,NWVEC
TOTAL(I,JY,1)=XMYV(I)+RATZ*(XV(I)-XMYV(I))
151 CONTINUE
1515 IF (YOUT-YM) 155,153,152
152 IF (YOUT-Y) 155,155,155
153 DO 154 I=1,NWVEC
TOTAL(I,NR,2)=XZMV(I)+RATY*(XV(I)-XZMV(I))
154 CONTINUE

```

```

155 IF (JY-JYL) 158,156,158
156 VALUE(NR)=XV(1)
C
C COMPUTATION OF INTEGRALS
C
158 CALL WAKLL(TEM,1)
IF (TEM) 200,159,200
159 SUMF=PLANE*DYI*DZI
LZFAF=0
IF (NR-NRST) 1591,1592,1592
1591 SUMF=0.5*SUMF
LZFAF=1
1592 IF (JY-NYPS) 1593,1594,1594
1593 SUMF=0.5*SUMF
LZFAF=1
1594 XMOM=XMOM+XV(3)*(U+XV(3))*SUMF
TKE=TKE+XV(1)*(U+XV(3))*SUMF
TEM=(XV(4)-ZEROV(4))**2+(XV(5)-ZEROV(5))**2
TEM=(XV(3)*XV(3)+TEM)*(U+XV(3))*SUMF
RPE=RPE+XV(2)*XV(2)*SUMF
VKE=VKE+TEM
XLIFT=XLIFT+(XV(5)-ZEROV(5))*SUMF
IF (XV(1)-QCUT*FMAXV(1)) 162,162,161
161 XPE=XPE+XV(2)*Z*SUMF
AREA=AREA+SUMF
GO TO 165
162 WKE=WKE+TEM
TEM=XV(2)*XV(2)*SUMF
XPE=XPE+TEM/2.0
WPE=WPE+TEM
165 IF (LZFAF) 200,166,200
166 PSIH=PSIH+0.5*DYM*(XV(5)+XZMV(5)-2.0*ZEROV(5))
PSIV(JY)=PSIV(JY)+0.5*DZM*(XV(4)+XMYV(4)-2.0*ZEROV(4))
TEM=0.5*(PSIV(JY)-PSIH)
IF (ABS(TEM)-ABS(PSIM)) 200,200,167
167 PSIM=TEM
200 CONTINUE
250 CONTINUE
TKE=TKE/2.0
VKE=VKE/2.0
WKE=WKE/2.0
XKE=TKE+VKE
XLIFT=-XLIFT
RPE=G*RPE/2.0
WPE=G*WPE/2.0
XPE=G*XPE
C
C COMPUTATION OF GROSS SCALE LAMBDA S
C
NPOS=NRL
CALL WAKRR(NRL,ZV)
Y=YULDV(JYL)
XV(1)=FMAXV(1)
TEM=XV(1)/4.0
IYPSX=JYL+1
LFL=0
DO 260 JY=IYPSX,IYPE
XMYV(1)=XV(1)
YM=Y

```

```
CALL WAKMP(IROWR,NRL,JY,XV,1)
Y=YOLDV(JY)
IF (TEM-XV(1)) 256,252,252
252 IF (LFL) 260,254,260
254 YP=YM+(Y-YM)*(XMYV(1)-TEM)/(XMYV(1)-XV(1))
LFL=1
GO TO 260
256 LFL=0
260 CONTINUE
EPSSV(3)=2.0*C*(YP-YOUT)
NRSTX=NRL+1
LFL=0
DO 280 NR=NRSTX,NKEND
IF (TEM-VALUE(NR)) 276,272,272
272 IF (LFL) 280,274,280
274 ZP=ZOLDV(NR-1)+(ZOLDV(NR)-ZOLDV(NR-1))*(VALUE(NR-1)-TEM)/
1 (VALUE(NR-1)-VALUE(NR))
LFL=1
GO TO 280
276 LFL=0
280 CONTINUE
EPSSV(1)=2.0*C*(ZP-ZOUT)
RETURN
END
CART ID 0105 DB ADDR 4390 DB CNT 0206
```

A-12

WAKAL,S(0105)

**WAKAL - STRATIFIED SUBMARINE WAKE. AUXILIARY LOOP FOR EXECUTION
SUBROUTINE WAKAL

C

C THIS SUBROUTINE IN THE WAKE PROGRAM EXAMINES SOLUTION VALUES

C

*COPY (CMWAK)

C

DATA JMSGF,JMSGR,JMSG8,JMSG6/2HST,2HRS,2HBU,2HOK/

C

1000 FORMAT(/ /47H FULL OUTPUT AT FIRST LOCAL MAXIMUM OF Z LAMBDA)

1001 FORMAT(/ /35H DX LESS THAN MINIMUM ALLOWED VALUE)

C

C CHECK RUN POSITION

C

IOLAY=6

IF (LMLFL) 100,100,122

100

XP=X

NPTSN=NPTS

IF (LSTFL) 102,101,102

101

NPTSN=NPTS+1

XP=X+DX

102

CALL WAKFS(NIAAF,LIAAF)

LIOLF=0

CALL WAKFS(NIOLP,LIOLF)

CALL WAKFS(NIOPP,LIOPF)

CALL WAKFS(NFOLP,LFOLF)

CALL WAKFS(NTOPP,LTOPF)

CALL WAKFS(NIULP,LTULF)

CALL WAKFS(NSOLP,LSOLF)

JSTAT=JMSGF

IF (LSTFL) 103,110,105

103

IF (LPRFL) 104,170,170

104

LIOLF=1

LIOPF=0

LFOLF=0

LTULF=0

LTOPF=0

LSOLF=0

JSTAT=JMSGR

GO TO 170

105

LIOLF=1

LFOLF=1

LTOLF=IYPSN

LSOLF=0

LIOPF=NIOPP

LTOPF=NTOPP

LIAAF=NIAAF

GO TO 164

C

C SET UP FOR NEXT STEP

C

110

CALL WAKSE(EPSS,EPSSV)

CALL WAKSE(EPSX,EPSXV)

JSTAT=JMSG6

DXSAV=DX

DO 114 IXBRK=1,10

XBRK=XOUTV(IXBRK)

IF (X-XBRK) 112,114,114

```

112 DO 1122 I=1,NUFF
    TEM=FLOAT(I)
    IF (X+TEM*DX-XBRK) 1122,1124,1124
1122 CONTINUE
    GO TO 114
1124 DX=(XBRK-X)/TEM
    IF (I-1) 1126,113,1126
1126 XP=X+DX
    GO TO 116
113 XP=XBRK
1135 LIOLF=1
    LFOLF=1
    LIOLF=1
    LSOLF=1
    LIOPF=NIOPP
    LTCPF=NTOPP
    IF (LTRNF) 119,116,119
114 CONTINUE
116 IF (XP-XMAX) 118,117,117
117 LTRNF=1
    LENDF=1
    GO TO 1135
118 IF (NPTSN-NSTMX) 119,117,117
119 DXI=2.0/DX
C
C INITIALIZE FOR CURRENT INTEGRATION STEP
C
    LMLFL=1
    IF (LBURF) 120,120,121
120 NSS=3-NSS
121 RETURN
122 LMLFL=0
    IF (LPKRF) 190,124,190
C
C ERROR CHECK
C
124 CALL DVCHK(ISW)
    GO TO (1241,1242),ISW
1241 LDVCF=1
    LIOLF=1
1242 CALL OVERF(ISW)
    GO TO (1243,1244,1244),ISW
1243 LOVFF=1
    LIOLF=1
1244 IF (LDVCF+LOVFF) 175,130,175
C
C CHECK FOR BACKUP AND DETERMINE NEW DX
C
130 LBURF=0
    DO 136 I=1,NVAR
    IF (TMAXV(I)-EPSXV(I)*BUFAC) 136,136,135
135 IF (NPTSN-NSTBC) 136,136,1355
1355 LBURF=I
136 CONTINUE
    DXN=DXSAV*ABS(DXFMX)
    DO 162 I=1,NVAR
    VMAX=GMAXV(I)
    IF (LBURF) 144,142,144
142 TEM=FMAXV(I)

```

```
      IF (TEM-VMAX) 1435,1435,143
143  GMAXV(I)=TEM
1435 VMAX=TEM
144  IF (VWTFV(I)) 162,162,145
145  IF (VMAX-VSCAV(I)*EPSN) 1455,146,146
1455 VMAX=VSCAV(I)*EPSN
146  AERR=ABS(EPSX)
      IF (EPSX) 147,148,148
147  AERR=AERR*VSCAV(I)
      GO TO 149
148  AERR=AERR*VMAX
149  AERR=AERR/VWTFV(I)
      TEM=TMAXV(I)/DX
      IF (TEM) 151,162,151
151  DXX=AERR/TEM
      IF (DXX) 162,162,160
160  IF (DXX-DXN) 161,162,162
161  DXN=DXX
162  CONTINUE
      DX=DXN
      IF (DX-UXMIN) 1620,1621,1621
1620 LIOLF=1
      LTRNF=1
      WRITE (NOUT,1001)
      GO TO 190
1621 IF (DXFMX) 163,1623,1622
1622 IF (DX-DXMAX) 163,163,1623
1623 DX=DXMAX
163  IF (LBUFR) 1630,164,1630
1630 JSTAT=JMSGB
      LTRNF=1
      IF (UXSAV-DX*DXFMX) 1631,1632,1632
1631 DX=UXSAV/DXFMX
1632 LIOLF=0
      LFOLF=0
      LTOLF=0
      LSOLF=0
      LIOPF=0
      LTOPF=0
      IF (LIBUF) 1633,1634,1633
1633 LIOLF=1
1634 IF (LFBUF) 1635,1636,1635
1635 LFOLF=1
1636 IF (LTBUF) 1637,1638,1637
1637 LTOLF=1
1638 IF (LIBUF+LFBUF+LTBUF) 190,101,190
C
C SUCCESSFUL INTEGRATION STEP
C
164  IF (LZMAX) 1646,1642,165
1642 IF (EPSSV(1)-ZSCAL) 1644,165,165
1644 LZMAX=1
      LIOLF=1
      LFOLF=1
      LTOLF=1
      LIOPF=NIOPP
      LTOPF=NTOPP
      WRITE (NOUT,1000)
      GO TO 165
```

```
1646 EPSSV(1)=SCALM
      EPSSV(3)=SCALM
165  ZSCAL=EPSSV(1)
      YSCAL=EPSSV(3)
      CALL SFVMV(FMAXV,GMAXV,NWVEC)
170  LMLF1=-1
175  CALL WAKCS(1,L1OLF)
      CALL WAKCS(2,LFOLF)
      CALL WAKCS(3,LTOLF)
      CALL WAKCS(4,L1OPF)
      CALL WAKCS(5,LTOPF)
      CALL WAKCS(6,LSOLF)
190  CALL WAKCS(0,LTRNF)
      CALL WAKCS(13,LTRNF)
      RETURN
      END
CART ID 0105  DB ADDR 5880  DB CNT 0180
```

```

WAKAY.S(0105)
**WAKAY - STRATIFIED SUBMARINE WAKE, AUTOPOINT ADJUST Y
  SUBROUTINE WAKAY(NRX)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM REORGANIZES A ROW
C
  DIMENSION IYPNV(40)
*COPY (CMWAK)
  EQUIVALENCE (YOLDV(1),IYPNV(2))
C
C MAKE WORKING COPY OF NRNYV
C
  NPOS=NRX
  CALL WAKRR(NRX,ZV)
  IF (IYPS) 160,160,100
100  IYS=0
  DO 108 IY=1,NPNY
  I=NRNYV(IY)
  IF (I) 106,106,101
101  IF (IYS) 102,102,104
102  IF (I-IYPS) 104,103,103
103  IYS=IY
104  IF (IYPE-I) 106,105,105
105  IYE=IY
106  IYPNV(IY)=I
108  CONTINUE
C
C CHECK FOR MID-POINT ADDED ON EITHER END
C
  IF (IYS-1) 114,114,111
111  IF (NRNYV(IYS)-IYPS) 114,112,114
112  IF (NRNYV(IYS-1)) 113,113,114
113  IYS=IYS-1
114  IF (IYE-NPNY) 115,120,120
115  IF (NRNYV(IYE)-IYPE) 120,116,120
116  IF (NRNYV(IYE+1)) 117,117,120
117  IYE=IYE+1
C
C CHECK WHETHER NRX ROW IS VOIDED BY ADJUSTMENT
C
120  IF (IYS-IYE) 121,121,1201
1201  IF (IYE-1) 121,121,1203
1203  IYS=IYE
C
C FORWARD REORGANIZATION PASS
C
121  JYM=0
  IYS=MMAX(1,IYS-1)
  IYE=MMIN(NPNY,IYE+1)
  DO 150 IY=IYS,IYE
  JYT=NYPY+IY-2
  JYF=IYPNV(IY)
  I=IY
122  I=I+1
  IF (I-NPNY) 123,123,124
123  JYP=IYPNV(I)
  IF (JYP) 122,122,125
124  JYP=10000
125  IF (JYF) 126,126,132

```



```
126 IF (JYT-JYM) 150,150,127
127 IF (JYT-JYP) 128,150,150
128 CALL WAKIY(JYM,JY1,JYP,IY)
    GO TO 148
132 IF (JYT-JYF) 133,148,142
133 IF (JYT-JYM) 134,134,145
134 JYM=JYF
    GO TO 150
142 IF (JYT-JYP) 145,150,150
145 CALL SFVMV(ROWB(1,JYF,2),ROWB(1,JYT,2),NMOVE)
148 IYPNV(IY)=-JYT
    JYM=JYT
150 CONTINUE
C
C BACKWARD REORGANIZATION PASS
C
    DO 154 JY=IYS,IYE
    JYT=NYPS+IYS+IYE-JY-2
    IY=IYS+IYE-JY
    JYF=IYPNV(IY)
    IF (JYF) 154,151,152
151 JYM=IABS(IYPNV(IY-1))
    JYP=IABS(IYPNV(IY+1))
    CALL WAKIY(JYM,JY1,JYP,IY)
    GO TO 153
152 CALL SFVMV(ROWB(1,JYF,2),ROWB(1,JYT,2),NMOVE)
153 IYPNV(IY)=-JYT
154 CONTINUE
    IYPS=NYPS+IYS-1
    IYPE=NYPS+IYE-3
160 CALL WAKWR(NRX,ZV)
    RETURN
    END
CART ID 0105 DB ADDR 3200 DB CNT 0086
```

WAKAZ,S(0105)

**WAKAZ - STRATIFIED SUBMARINE WAKE, AUTOPOINT ADJUST Z
SUBROUTINE WAKAZC
C THIS SUBROUTINE IN THE WAKE PROGRAM REORGANIZES THE SOLUTION FILEC
*COPY (CMWAK)C
C CHECK PROFILE SHIFTC
IOLAY=12
MOOD=-1
IF (LZLFF) 101,102,102
101 NRSTN=2
GO TO 108
102 NRSTN=(MXRZ-NPNZ)/2+2
IF (NRST+(JEND-1)/2-MXRZ/2) 107,108,107
107 LZFAF=1
108 IF (LYLFF) 111,112,112
111 NYPSN=2
GO TO 118
112 NYPSN=(MXRY-NPNY)/2+2
IF (NYPS+(NYPE-NYPS)/2-MXRY/2) 117,118,117
117 LYFAF=1
118 IF (LYFAF) 1181,119,1181C
C SOLUTION PROFILE MUST BE REORGANIZED IN Y DIRECTIONC
1181 NYPS=NYPSN
NYPE=NYPS+NPNY-3
DO 1185 JZ=1,NPNZ
NRF=NRNZV(JZ)
IF (NRF) 1185,1185,1182
1182 CALL WAKAY(NRF)
1185 CONTINUE
DO 1188 I=1,NPNY
JZ=NYPS+I-2
YOLDV(JZ)=YNEWV(I)
1188 CONTINUE
119 IF (LZFAF) 120,160,120C
C SOLUTION PROFILE MUST BE REORGANIZED IN Z DIRECTIONC
120 NRST=NRSTN
JEND=NPNZ-2
C
C FORWARD REORGANIZATION PASSC
NRM=0
DO 150 JZ=1,NPNZ
NRT=NRST+JZ-2
NRF=NRNZV(JZ)
J=JZ
122 J=J+1
IF (J-NPNZ) 123,123,124
123 NRP=NRNZV(J)
IF (NRP) 122,122,125
124 NRP=10000
125 IF (NRF) 126,126,132

```
126 IF (NRT-NKM) 150,150,127
127 IF (NRT-NKP) 126,150,150
128 CALL WAKIZ(NRM,NRT,NKP,JZ)
GO TO 148
132 IF (NRT-NRF) 133,148,142
133 IF (NRT-NRM) 134,134,145
134 NKM=NRF
GO TO 150
142 IF (NRT-NKP) 145,150,150
145 NPOS=NRF
CALL WAKRR(NRF,ZV)
NPOS=NRT
CALL WAKWR(NRT,ZV)
148 NRNZV(JZ)=-NRT
NRM=NRT
150 CONTINUE
C
C BACKWARD REORGANIZATION PASS
C
DO 154 JZ=1,NPNZ
NKT=NRST+NPZ-JZ-1
IZ=NPZ+1-JZ
NKF=NRNZV(IZ)
IF (NRF) 154,151,152
151 NKM=IABS(NRNZV(IZ-1))
NKP=IABS(NRNZV(IZ+1))
CALL WAKIZ(NKM,NRT,NKP,IZ)
GO TO 153
152 NPOS=NKF
CALL WAKRR(NKF,ZV)
NPOS=NRT
CALL WAKWR(NRT,ZV)
153 NRNZV(IZ)=-NRT
154 CONTINUE
DO 156 I=1,NPNZ
JZ=NRST+I-2
ZULDV(JZ)=ZNEWV(I)
156 CONTINUE
160 RETURN
END
CAKT ID 0105 DB ADDR 2F70 DB CNT 00C4
```

WAKCL.S(0105)

**WAKCL - STRATIFIED SUBMARINE WAKE, COMPUTE LENGTH SCALES
SUBROUTINE WAKCL(XXV,FTEM)

C
C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES THE VERTICAL AND
C SCALE LENGTHS BY COMPARISON WITH THE RICHARDSON LENGTH
C

DIMENSION XXV(6)

*COPY (CMWAK)

C

SCAL=ZSCAL

IF (FTEM) 103,140,103

103 TEM=SQRT(RIS*ABS(XXV(1))/FTEM)/G)

IF (SCAL-TEM) 140,140,110

110 SCAL=TEM

IF (SCAL-SCALM) 120,130,130

120 SCAL=SCALM

130 SCAL=SQRT(ABS(SCAL*ZSCAL))

140 IF (LSCAL) 150,160,150

150 SCALE=XXV(6)

RETURN

160 SCALE=2.0*YSCAL*YSCAL*SCAL/(YSCAL*YSCAL+SCAL*SCAL)

RETURN

END

CART 10 0105 DB ADDR 3A90 DB CNT 002E

WAKCS.S(0105)

**WAKCS - STRATIFIED SUBMARINE WAKE, CHECK DATA SWITCH
SUBROUTINE WAKCS(LL,LFL)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM CHECKS THE LL DATA SWITCH
C FOR POSSIBLE OUTPUT TO LINE PRINTER OR DISK FILE

C

*COPY (CMWAK)

C

CALL DATSW(LL,ISW)

GO TO (10,20),ISW

10 LFL=1

LIOLF=1

20 RETURN

END

CART 10 0105 DB ADDR 2UE0 DB CNT 001C

WAKDG.S(0105)

**WAKDG - STRATIFIED SUBMARINE WAKE, DETERMINE DENSITY GRADIENT
SUBROUTINE WAKDG(ZPOS)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM DETERMINES THE BACKGROUND
C DENSITY GRADIENT WHERE APPLICABLE

C

*COPY (CMWAK)

C

IF (LORDZ) 10,100,10
10 IF (ZPOS) 20,30,30
20 IF (ZPOS-DRDZL) 30,50,25
25 DRDZ=-0.000001
RETURN
30 DRDZ=DRDZH
100 RETURN
END

CART 10 0105 DB ADDR 45A0 DB CNT 0020

WAKDS.S(0105)

**WAKUS - STRATIFIED SUBMARINE WAKE, OBTAIN DELTA SPACING RATIO
SUBROUTINE WAKDS(CURVM,CURVP,DF,DFO)

C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES A NEW DF AS SOME
C FRACTION OF THE OLD SO AS TO BALANCE THE THREE-POINT PROFILE

C
*COPY (CMWAK)

C
DFRM=0.99*DFRMA
IF (CURVP) 190,191,190
190 TEMB=SQRT(CURVM/CURVP)
IF (TEMB-DFRM) 192,192,191
191 TEMB=DFRM
GO TO 194
192 TEMA=1.0/DFRM
IF (TEMB-TEMA) 193,194,194
193 TEMB=TEMA
194 DF=DF/(1.0+TEMB)
IF (DF/DFO-DFRM) 196,196,195
195 DF=DFO*DFRM
196 RETURN
END
CARD 10 0105 DB ADDR 2700 DB CNT 002C

WAKEC,S(0105)
**WAKEC - STRATIFIED SUBMARINE WAKE, EDGE CONDITION CHECK
SUBROUTINE WAKEC(LFL)

C
C THIS SUBROUTINE IN THE WAKE PROGRAM TURNS THE IMPLICIT UPSWEEP
C AND CHECKS FOR SATISFACTION OF THE BOUNDARY EDGE CONDITION
C

*COPY (CMWAK)

C

```
LFL=1
CALL SFVMV(AV,XMAT,NWVEC)
DO 100 I=1,NWVEC
XMAT(I)=XMAT(I)-GM(I)*ZEROV(I)
100 CONTINUE
DO 110 I=1,NVAR
IF (ABS(XMAT(I)-ZEROV(I))-EPSSV(I)) 110,110,120
110 CONTINUE
CALL SFVMV(XMAT,AV,NWVEC)
CALL WAKMP(IROWA,NR,JY,AV,2)
RETURN
120 LFL=0
RETURN
END
```

CART ID 0105 DB ADDR 4310 DB CNT 002C

WAKFS.S(0105)

**WAKFS - STRATIFIED SUBMARINE WAKE, FLAG SET
SUBROUTINE WAKFS(NPP,LFL)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM SETS THE OUTPUT FLAGS

C

*COPY (CMWAK)

C

LFL=0

IF (NPP) 102,102,100

100 IF (MOD(NPTSN,NPP)) 102,101,102

101 LFL=1

LIOLF=1

102 RETURN

END

CAKT ID 0105 DB ADDR 2E00 DB CNT 001C

WAKIN,S(0105)

**WAKIN - STRATIFIED SUBMARINE WAKE, INPUT CARDS AND START RUN
SUBROUTINE WAKIN

C

C THIS SUBROUTINE IN THE WAKE PROGRAM STARTS THE RUN
C

DIMENSION ETID(3),LFLAG(6),COMN(2),FILEN(2),FILID(3)
DIMENSION IDATE(4),JVCHV(5),FTID(3),HSCAL(2)

*COPY (CMWAK)

EQUIVALENCE (LTRNF,LFLAG(1)),(AV(1),FILID(1))

C

DATA COMN/4HWAKC,1HM/,JERRX/2H /,BLANK/4H /
DATA HSCAL/3HOFF,3HUN /
DATA JVCHV/2HQW,2HRU,2HU ,2HV ,2HW /

C

1000 FORMAT(18I4)
1001 FORMAT(7(A4,A1,3X))
1002 FORMAT(I4,19A4)
1003 FORMAT(2I4,3F8.3,2I4)
1004 FORMAT(6F8.3,I4)
1005 FORMAT(10F8.3)
1020 FORMAT(A4,A1,5I5)
2000 FORMAT(1H0,A4,A1,26H CANNOT BE FOUND OR OPENED)
2002 FORMAT(44H0JOB ABCRT - WAKE PROGRAM IS IN RESTART MODE)
2006 FORMAT(45H1ARAP STRATIFIED SUBMARINE WAKE PROGRAM ,19A4,
1 7H RUN ,14)
2007 FORMAT(12HORUN RESTART,11X,4A2)
2008 FORMAT(10HORUN START,13X,4A2)
2009 FORMAT(20HORUN SPECIAL RESTART,3X,4A2)
2010 FORMAT(/3X,9HMAX STEPS,3X,10HSTART STEP,4X,5HMIN X,7X,5HMAX X,
1 4X,10HINITIAL DX,4X,7HMAX HRS,4X,8HLAM FLAG/
2 I8,112,4X,3E12.4,I8,I12)
2011 FORMAT(/2X,10HMAX Y SIZE,2X,10HLOW Y FLAG,2X,10HMAX Z SIZE,2X,
1 10HLOW Z FLAG/I8,4I12)
2012 FORMAT(12X,7E12.4)
2013 FORMAT(14HOSCALE FACTORS,4X,5(A2,10X))
2014 FORMAT(15HOWEIGHT FACTORS,3X,5(A2,10X))
2015 FORMAT(/3X,9HNOISE MIN,2X,10HMAX CHANGE,2X,10HEGE TOLER,3X,
1 8HMIN CURV,4X,8HMAX CURV/5E12.4)
2016 FORMAT(/4X,6HMAX DX,6X,6HMIN DX,5X,9HDX FACTOR,3X,9HBU FACTOR,
1 5X,4HCURV,4X,9HMIN SPACE,3X,9HMAX SPACE,5X,5HRATIO/8E12.4)
2017 FORMAT(15HOUTPUT CONTROL,4X,9HINT PRINT,3X,8HINT DISK,3X,
1 10HFULL PRINT,2X,10HTOTAL DISK,2X,11HTOTAL PRINT,2X,8HSE PRINT,
2 3X,11HAUTO ADJUST,3X,7HPICTURE/12X,8I12)
2018 FORMAT(12H0X OUTPUT AT,10E12.4)
2022 FORMAT(/6X,2HKE,10X,1HG,11X,2HPR,8X,7HSMALL A,7X,1HA,11X,1HB,
1 10X,4HBETA,9X,1HC,11X,1HS/9E12.4)
2023 FORMAT(/6X,2HDC,10X,1HU,11X,3HRI*,8X,4HORDZ,8X,5HSCALE,4X,
1 10HPRES ERROR,3X,9HMIN SCALE,4X,7HSPOR SQ,6X,4HCPOR/9E12.4)
2024 FORMAT(/6X,2HS1,10X,2HS2,10X,2HS5,10X,2HS6,10X,2HS7,10X,2HS8,
1 6X,9HSCALE EQN/6E12.4,5X,A3)
2025 FORMAT(15HOSOLUTION FILES,4X,7HWORKING,4X,5HGAMMA,5X,6HGLOBAL,
1 4X,4HPLOT,6X,6HCOMMUN/20X,7(A4,A1,5X))
2031 FORMAT(18HOREFLECTION VECTOR,2X,14I6)
2032 FORMAT(12HOEDGE VALUES,6X,5(A2,10X),2HSL,10X,2HP)
2033 FORMAT(14H0CONTROL FLAGS,5X,9HTYPE STAT,4X,8HSTART-UP,5X,
1 5HBREAK,6X,6HBU INT,6X,7HBU FULL,5X,8HBU TOTAL,4X,8HITERATES,
2 4X,16HDISK SAVE VECTOR/12X,7I12,9X,7I2)
2034 FORMAT(17H0START CONDITIONS,3X,4HNAME,6X,5HVALUE,5X,6HOPTION,

```

1 4X,6HLAMBDA,3X,8HPRESSURE,3X,6HOUTPUT/20X,A4,A1,I9,4I10)
2035 FORMAT(12H00RDZ CHANGE,2E12.4)
2040 FORMAT(/3X,8HQ CUTOFF,3X,10HDIVG PCENT,3X,9HDIVG FACT,4X,
1 6HP NORM,5X,8HS CUTOFF,4X,9HCUTOFF MU,3X,8HX FACTOR,5X,
2 6HX ZERO,5X,8HY OUTPUT,4X,8HZ OUTPUT/10E12.4)

```

```

C
C RUN INITIALIZATION
C

```

```

IOLAY=1
CALL IIBFR(2,BUFR)
CALL LETLI(ETID,BUFR)
CALL IIBFR(2,BUFS)
CALL LETLI(FTID,BUFS)
NCOMT=419
NWWZF=2
NWR=24
NMR=18
NMOVE=12
NMAI=16
NINU=8
NOUT=5
NVAR=5
NWVEC=6
NVART=7
IROWT=1
IROWG=6
IMAPV(1)=1
IMAPV(2)=7
IMAPV(3)=13
IMAPV(4)=19
CALL GDATE(IDATE)

```

```

C
C OPEN COMMON SAVE DISK FILE AND READ IN CONTENTS
C

```

```

L=1
CALL LETLU(COMID,2,BUFR,ETID,COMN(1),-1,2,N)
IF (N) 5,20,5
5 CALL SFVMV(COMN,FNAME,2)
10 WRITE (NOUT,2000) FNAME(L),FNAME(L+1)
CALL EXIT
20 NRX=1
CALL PBFDR(COMID,NRX,NCOMT,NSTST)

```

```

C
C READ INITIAL INPUT CARD
C

```

```

READ (NINU,1000) INFLG,N,JOBE
LSTFL=1
INFLG=INFLG-1
IF (INFLG) 110,115,120
110 LSTFL=-1
NSTST=NPTS
GO TO 1211
115 IF (LENDF) 118,116,118
116 IF (N) 118,117,118
117 WRITE (NOUT,2002)
CALL EXIT
118 LENDF=0

```

```

C
C READ REMAINING INPUT CARDS

```

```

C
120  READ (NINU,1002) NRUNI,CMNT
      READ (NINU,1003) NSTMX,NSTSI,XMIN,XMAX,DELX,MXHRS,LAMIN
      READ (NINU,1000) MXRY,LYLFF,MXRZ,LZLFF
      READ (NINU,1000) NRVV
      READ (NINU,1005) VSCAV
      READ (NINU,1005) VWTFV
      READ (NINU,1005) ZEKUV
      READ (NINU,1005) LPSN,EPSX,EPSS,ECMN,ECMX
      READ (NINU,1005) DXMAX,DXMIN,DXFMX,BUFAC,FCUR,OFFMN,OFFMX,DFRMX
      READ (NINU,1000) NIOLP,NIOPP,NFOLP,NTOPP,NTOLP,NSOLP,NIAAF,LOJT
      READ (NINU,1005) XOUTV
      READ (NINU,1000) NSTAT,NSTBC,NUFF,LIBUF,LFBUF,LTBUF,NSTPR,IDSV
      READ (NINU,1005) KE,G,PR,AS,A,B,BETA,C,S
      READ (NINU,1005) DC,U,R1S,DRDZ,SCALE,PCRIT,SCALM,SPORS,CPOK
      READ (NINU,1004) S1,S2,S5,S6,S7,S8,LSCAL
      READ (NINU,1005) WCUT,DIVP,DIVF,PNORM,PCUT,CMU,XFACT,XZERO,
1  YOUT,ZOUT
      READ (NINU,1001) FNAME

```

```

C
C OPEN REMAINING BASIC DISK FILES

```

```

C
1211  L=1
      CALL LETLU(SLNID,2,BUFS,FTID,FNAME(1),-1,2*NWR,N)
      IF (N) 10,1212,10
1212  L=3
      CALL LETLU(GAMID,2,BUFR,ETID,FNAME(3),-1,2*NMAT,N)
      IF (N) 10,1213,10

```

```

C
C OPEN GLOBAL DISK FILE AND PROFILE DISK FILE

```

```

C
1213  IF (NIOPP) 1215,1215,1214
1214  L=5
      CALL LETLU(GLOID,2,BUFR,ETID,FNAME(5),-1,2,N)
      IF (N) 10,1216,10
1215  CALL SFVFL(BLANK,FNAME(5),2)
1216  IF (NTOPP) 1218,1218,1217
1217  L=7
      CALL LETLU(PLTID,2,BUFR,ETID,FNAME(7),-1,2,N)
      IF (N) 10,122,10
1218  CALL SFVFL(BLANK,FNAME(7),2)
122   IF (INFLG) 144,123,1224
C
C SPECIAL RESTART WITH CURRENT WORKING FILE (NEW COMMON DATA)

```

```

C
1224  NSTST=NPTS
      LSTFL=-1
      GO TO 142
C
C PROFILE INPUT INITIALIZATION

```

```

C
123   NSTST=NSTSI
      NPTS=NSTST
      IF (NRUNI) 125,125,124
124   NRUN=NRUNI-1
125   NRUN=NRUN+1
      IKWR=2
      ZSCAL=SCALE
      YSCAL=SCALE

```

```

ZEROV(6)=2.0*SCALE
X=XMIN
IF (DELX) 130,130,129
129 DX=DELX
130 READ (NINU,1020) FILEN,LZFAF,LYFAF,LZMAX,LPRFL,IYPSN
IF (LYFAF) 134,131,131
131 CALL LETLU(FILID,2,BUFR,ETID,FILEN(1),-1,2,N)
IF (N) 132,140,132
132 WRITE (NOUT,2000) FILEN
CALL EXIT
134 CALL SFVMV(FNAME(7),FILEN,2)
C
C INITIALIZE FIXED PARAMETERS
C
140 NSS=1
LIAAF=1
DEPST=0.0
DEPSI=0.0
DXSAV=0.0
142 DO 143 I=1,6,2
KLOK(I)=0
143 CONTINUE
LDRUZ=0
IF (DRUZ) 144,1435,144
1435 LDRDZ=1
READ (NINU,1005) DRUZL,DROZH
144 LSOLF=0
DO 145 I=1,6
LFLAG(I)=0
145 CONTINUE
JERR=JERRX
FMU=1.0/RE
XK=PR/RE
BBETA=1.0+2.0*B*BETA
HBETA=1.5*BBETA
BBS=1.0+BBETA/B/S
CVV=(1.0-2.0*B*(1.0-BETA))/3.0/BBETA
C
C REFLECTION PROPERTY CONDITION CONSTRUCTION
C
DO 155 L=1,2
DO 151 I=1,NWVEC
IRFV(I,L)=NRFV(I,L)
151 CONTINUE
DO 153 I=2,3
DO 152 K=1,2
N=2*(3-I)+K
IRFV(N,L+2)=IABS(1-NRFV(I,L))-IABS(L-K)
152 CONTINUE
153 CONTINUE
DO 154 N=5,NWVEC
IRFV(N,L+2)=NRFV(7,L)
154 CONTINUE
155 CONTINUE
CALL DATSW(14,ISW)
GO TO (160,200),ISW
160 WRITE (NOUT,1000) IRFV
C
C OUTPUT RUN PARAMETERS

```

```
C
200  WRITE (NOUT,2006) CMNT,NRUN
      IF (INFLG) 201,202,203
201  WRITE (NOUT,2007) IDATE
      GO TO 204
202  WRITE (NOUT,2008) IDATE
      GO TO 204
203  WRITE (NOUT,2009) IDATE
204  WRITE (NOUT,2010) NSTMX,NSTST,XMIN,XMAX,DX,MXHRS,LAMIN
      WRITE (NOUT,2011) MXRY,LYLFF,MXRZ,LZLFF
      WRITE (NOUT,2031) NMFV
      WRITE (NOUT,2013) JVCHV
      WRITE (NOUT,2012) VSCAV
      WRITE (NOUT,2014) JVCHV
      WRITE (NOUT,2012) VWTFV
      WRITE (NOUT,2032) JVCHV
      WRITE (NOUT,2012) ZEKOV
      WRITE (NOUT,2015) EPSN,EPSX,EPSS,ECMN,ECMX
      WRITE (NOUT,2016) DXMAX,DXMIN,DXFMX,BUFAC,FCUR,DFFMN,DFFMX,DFRMX
      WRITE (NOUT,2017) NIOLP,NIOPP,NFOLP,NTOPP,NTOLP,NSOLP,NIAAF,LOUT
      WRITE (NOUT,2018) XUUTV
      WRITE (NOUT,2033) NSTAT,NSTBC,NUFF,LIBUF,LFBUF,LTBUF,NSTPR,IDSV
      WRITE (NOUT,2022) RE,G,PR,AS,A,B,BETA,C,S
      WRITE (NOUT,2023) DC,U,RIS,DRDZ,SCALE,PCRT,SCALM,SPORS,CPOR
      WRITE (NOUT,2024) S1,S2,S5,S6,S7,S8,HSCAL(LSCAL+1)
      WRITE (NOUT,2040) QCUT,DIVP,DIVF,PNORM,PCUT,CMU,XFACT,XZERO,
1  YOUT,ZOUT
      WRITE (NOUT,2025) FNAME,COMN
      IF (INFLG) 210,205,210
205  WRITE (NOUT,2034) FILEN,LZFAP,LYFAP,LZMAX,LPRFL,IYPSN
210  IF (LDRDZ) 215,220,215
215  WRITE (NOUT,2035) DRUZL,DRDZH
C
C  START RUN EXECUTION
C
220  LMLFL=-1
      NPTSN=NPTS
      RETURN
      END
CART 10 0105  DB ADDR 5570  DB CNT 0224
```

```
WAKIY.S(0105)
**WAKIY - STRATIFIEDED SUBMARINE WAKE, INSERT A Y POINT
  SUBROUTINE WAKIY(JYM,JYT,JYP,IY)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM INSERTS
C A Y POINT BETWEEN TWO EXISTING ROW POINTS
C
*COPY (CMWAK)
C
  RATY=(YNEWV(IY)-YNEWV(IY-1))/(YNEWV(IY+1)-YNEWV(IY-1))
  DO 102 I=1,2
    CALL WAKMP(I,NPOS,JYM,XZMV,1)
    CALL WAKMP(1,NPOS,JYP,XZPV,1)
    DO 101 J=1,NWVEC
      XV(J)=XZMV(J)+RATY*(XZPV(J)-XZMV(J))
101  CONTINUE
    CALL WAKMP(I,NPOS,JYT,XV,2)
102  CONTINUE
  RETURN
  END
CAKT 10 0105  DB ADDR 2CC0  DB CNT 0026
```

```

WAKIZ.S(0105)
**WAKIZ - STRATIFIED SUBMARINE WAKE, INSERT A Z ROW
  SUBROUTINE WAKIZ(NRM,NKT,NRP,IZ)

```

```

C
C THIS SUBROUTINE IN THE WAKE PROGRAM INSERTS
C A Z ROW BETWEEN TWO EXISTING ROWS
C

```

```

*COPY (CMWAK)

```

```

C
C FILL MINUS AND PLUS ROWS IN BUFFER
C

```

```

      NPOS=NRM+1
      CALL WAKRR(NRM,ZMV)
      NPOS=NRP-1
      CALL WAKRR(NRP,ZPV)
      Z=ZNEWV(IZ)
      RATZ=(Z-ZM)/(ZP-ZM)
      IF (IYPSM*IYPSP) 10,10,20
10     IYPS=MMAX(IYPSM,IYPSP)
      GO TO 30
20     IYPS=MMIN(IYPSM,IYPSP)
30     IYPE=MMAX(IYPEM,IYPEP)
      IYPSX=IYPS+LYLFF

```

```

C
C INTERPOLATE FOR NRT ROW
C

```

```

      NPOS=NRT
      DO 114 JY=IYPSX,IYPE
      DO 112 I=1,2
      CALL WAKMP(I,NRT-1,JY,XMYV,1)
      CALL WAKMP(I,NRT+1,JY,XPYV,1)
      DO 111 J=1,NWVEC
      XV(J)=XMYV(J)+RATZ*(XPYV(J)-XMYV(J))
111    CONTINUE
      CALL WAKMP(I,NRT,JY,XV,2)
112    CONTINUE
114    CONTINUE
      CALL WAKWR(NRT,ZV)
      RETURN
      END

```

```

CART ID 0105 DB ADDR 2CF0 DB CNT 004E

```



```
WAKLL.S(0105)
**WAKLL - STRATIFIED SUBMARINE WAKE, LINER LOCATION CALCULATION
  SUBROUTINE WAKLL(TEM,LFL)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM DETERMINES WHETHER THE LINER
C HAS BEEN REACHED AND SETS THE COEFFICIENT APPROPRIATELY
C
*COPY (CMWAK)
C
  TEM=0.0
  RR=Y*Y/YSCAL/YSCAL+Z*Z/ZSCAL/ZSCAL
  IF (RR-SPORS) 100,100,10
10  TEMM=CPOR*(RR-SPORS)
  GO TO (20,30),LFL
20  TEM=0.5*(EXP(TEMM)+EXP(-TEMM))-1.0
  RETURN
30  TEM=Y*(XV(4)-ZEROV(4))/YSCAL/YSCAL+Z*(XV(5)-ZEROV(5))/ZSCAL/ZSCAL
  TEM=CPOR*TEM*(EXP(TEMM)-EXP(-TEMM))
100 RETURN
  ENC
CART ID 0105  DB ADDR 2E20  DB CNT 0026
```

WAKMG,S(0105)

**WAKMG - STRATIFIED SUBMARINE WAKE, MOVE GAMMA ROW
SUBROUTINE WAKMG(NRX,ZPOS,LFL)

C
C THIS SUBROUTINE IN THE WAKE PROGRAM MOVES THE GAMMA MATRIX ROW
C BETWEEN THE ROW BUFFER AND DISK FILE
C

DIMENSION ZPOS(2)

*COPY (CMWAK)

C

DATA JERRX/2HMG/

C

IF (NRX) 100,100,10

10 IF (NRX-MXRZ) 20,20,100

20 CALL SFVMV(ZPOS,ZA,NWWZF)

IYPSX=IVECA+LYLFF

LL=NMAT*(IVECB-IYPSX+1)

NRXX=(NRX-1)*MXRY+IYPSX

GO TO (30,40),LFL

30 CALL PBFDR(GAMID,NRXX,LL,ROWG(1,IYPSX))

RETURN

40 CALL PBFOW(GAMID,NRXX,LL,ROWG(1,IYPSX))

RETURN

100 JERR=JERRX

RETURN

END

CART ID 0105 DB ADDR 2060 DB CNT 0032

```
WAKMP.S(0105)
**WAKMP - STRATIFIED SUBMARINE WAKE, MOVE A POINT
   SUBROUTINE WAKMP(IMAP,NRZ,NRY,VEC,LFL)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM MOVES SELECTED POINT
C INFORMATION BETWEEN THE ROW OR GAMMA BUFFER AND VEC
C
   DIMENSION VEC(2)
*COPY (CMWAK)
C
   DATA JERRX/2HMP/
C
   J=NRZ-NPOS+2
   IF (J) 200,200,10
  10  IF (J-3) 20,20,200
  20  IF (IMAP-5) 60,200,30
  30  GO TO (40,50),LFL
  40  CALL SFVMV(ROWG(1,NRY),VEC,NMAT)
      RETURN
  50  CALL SFVMV(VEC,ROWG(1,NRY),NMAT)
      RETURN
  60  NRXX=IMAPV(IMAP)
      IF (IMAP-3) 90,70,80
  70  IF (MOUD) 90,80,200
  80  NRXX=NRXX-NWVEC
  90  GO TO (100,110),LFL
 100  CALL SFVMV(ROWB(NRXX,NRY,J),VEC,NWVEC)
      RETURN
 110  CALL SFVMV(VEC,ROWB(NRXX,NRY,J),NWVEC)
      RETURN
 200  JERR=JERRX
      RETURN
      END
CART ID 0105 DB ADDR 2U40 DB CNT 0040
```

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WAKMR.S(0105)

**WAKMR - STRATIFIED SUBMARINE WAKE, MOVE A BUFFER ROW
SUBROUTINE WAKMR(NRF,NRT)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM MOVES THE CONTENTS OF THE
C ROW BUFFER FROM ROW NRF TO ROW NRT

C

*COPY (CMWAK)

C

DO 100 I=1,MXRY

CALL SFVMV(ROWB(1,I,NRF),ROWB(1,I,NRT),NMR)

100 CONTINUE

RETURN

END

CART ID 0105 DB ADDR 2040 DB CNT 001A

```

WAKMV.S(0105)
**WAKMV - STRATIFIED SUBMARINE WAKE, SUPEREQUILIBRIUM MATRIX VALUES
SUBROUTINE WAKMV(XXV,TTV,T)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES THE SUPEREQUILIBRIUM
C MATRIX VALUES NEEDED FOR THE IMPLICIT UPSWEEP CALCULATION
C
DIMENSION XXV(6),TTV(6),T(10)
*COPY (CMWAK)
C
IF (XXV(1)) 100,100,101
100 CALL SFVFL(0.0,T,10)
CVS=0.0
CWS=0.0
RETURN
101 Q=SQRT(XXV(1))
FTEM=TTV(4)+DRDZ
CALL WAKCL(XXV,FTEM)
IF (LAMIN) 100,102,100
102 BQL=BBETA*Q/SCALE
C1=A*BQL*Q/SCALE-G*FTEM
C2=BBS*G*FTEM-C1
TEM=TTV(1)*TTV(1)*SCALE/Q/BQL-BBETA*G*FTEM/C2
1 -TTV(2)*TTV(2)*BBETA*(G*FTEM*(1.0-A/B/S)+A*A*XXV(1)
2 /SCALE/SCALE)/C1/C2
CVS=CVV+(B-CVV*TEM)/(HBETA+TEM)
CALL WAKTC(CVS,1.0,IVECA)
CVW=CVS/C1
C4=CVW*G*TTV(3)
T(7)=-BQL*CVW*XXV(1)
C3=CVS*DRDZ+C4*BBS*TTV(3)
T(4)=CVS*XXV(1)*BQL/C2
T(3)=C3*BQL/C2
CWS=CVS-2.0*G*(C3+CVS*TTV(4))/C2
CALL WAKTC(CWS,1.0-CVS,IVECB)
DUR=(FTEM*CWS*XXV(1)+C4*TTV(3)*XXV(1)
1 -BQL*(T(3)*XXV(1)+T(4)*TTV(4)))/C1
T(2)=- (G*DUR+CWS*XXV(1))/BQL
T(6)=-CVS*XXV(1)/BQL
T(5)=-C4*TTV(2)/BQL
CUR=(FTEM*C4*TTV(1)+TTV(3)*TTV(1)*CVS*(1.0
1 +BQL*BQL/C1))/C1
T(1)=- (G*CUR+C4*TTV(1))/BQL
T(8)=CVS
T(9)=CWS
T(10)=C4
RETURN
END
CART ID 0105 DB ADDR 41C0 DB CNT 005E

```

WAKMY.S(0105)

**WAKMY - STRATIFIED SUBMARINE WAKE, Y IMPLICIT MATRIX COEFFICIENTS
SUBROUTINE WAKMY

C
C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES THE X,Y,Z AND D MATRIX
C COEFFICIENTS FOR THE Y IMPLICIT UPSWEEP
C

DIMENSION T(10,5)

*COPY (CMWAK)

EQUIVALENCE (T(1,1),ZNEWV(1))

C

FPRZ(ARGM,ARG,ARGP)=FZM*(ARGM+FZS*ARG-FZR*ARGP)

FPRY(ARGM,ARG,ARGP)=FYM*(ARGM+FYS*ARG-FYR*ARGP)

SPRZ(ARGM,ARG,ARGP)=SZM*ARGM+SZ*ARG+SZP*ARGP

SPRY(ARGM,ARG,ARGP)=SYM*ARGM+SY*ARG+SYP*ARGP

C

C COMPUTE SPACING FACTORS
C

DZM=Z-ZM

DZP=ZP-Z

DZT=DZM+DZP

FZM=-DZP/DZM/DZT

FZP=DZM/DZP/DZT

FZ=-FZM-FZP

TEM=DZM/DZP

FZR=TEM*TEM

FZS=FZR-1.0

SZM=2.0/DZM/DZT

SZP=2.0/DZP/DZT

SZ=-SZM-SZP

C

DYM=Y-YM

DYP=YP-Y

DYT=DYM+DYP

FYM=-DYP/DYM/DYT

FYP=DYM/DYP/DYT

FY=-FYM-FYP

TEM=DYM/DYP

FYR=TEM*TEM

FYS=FYR-1.0

SYM=2.0/DYM/DYT

SYP=2.0/DYP/DYT

SY=-SYM-SYP

C

CALL SFVFL(0.0,XMAT,NWVEC)

CALL SFVFL(1.0,YMAT,NWVEC)

CALL SFVFL(0.0,ZMAT,NMOVE)

C

C COMPUTE MULTIPLICATIVE FACTORS
C

CALL WAKDG(ZM)

CALL WAKMV(XMYV,TMYV,T(1,5))

CALL WAKDG(ZP)

CALL WAKMV(XPYV,TPYV,T(1,4))

CALL WAKDG(Z)

CALL WAKMV(XZMV,TZMV,T(1,3))

CALL WAKMV(XZPV,TZPV,T(1,2))

CALL WAKMV(XV,TV,T(1,1))

TMU=FMU

```

IF (SPORS) 40,40,20
20 TEM=Y*Y/YSCAL/YSCAL+Z*Z/ZSCAL/ZSCAL
   IF (TEM-PCUT) 40,40,30
30 TMU=CMU
40 CL=2.0*(AS*TMU/SCALE+B*Q)/SCALE
C
C COMPUTE DERIVATIVE FACTORS
C
   DXX=DXI*(U+XV(3))
   CALL WAKLL(TEMK,1)
   ADM=FYM*XZMV(4)
   AD=FY*XV(4)
   ADP=FYP*XZPV(4)
   SL=SCALE/3.0
   FQY=FPRY(SQRT(XZMV(1)),Q,SQRT(XZPV(1)))
   FQZ=FPRZ(SQRT(XMYV(1)),Q,SQRT(XPYV(1)))
   FKZ=FPRZ(XMYV(1),XV(1),XPYV(1))
   FRZ=FPRZ(XMYV(2),XV(2),XPYV(2))
   FUY=FPRY(XZMV(3),XV(3),XZPV(3))
   FUZ=FPRZ(XMYV(3),XV(3),XPYV(3))
   FVY=FPRY(XZMV(4),XV(4),XZPV(4))
   FVZ=FPRZ(XMYV(4),XV(4),XPYV(4))
   FWY=FPRY(XZMV(5),XV(5),XZPV(5))
   FWZ=FPRZ(XMYV(5),XV(5),XPYV(5))
   FLY=FPRY(XZMV(6),XV(6),XZPV(6))
   FLZ=FPRZ(XMYV(6),XV(6),XPYV(6))
   SPLY=3.0*DC*YSCAL*CVS*Q+TMU
   FPLY=3.0*DC*YSCAL*CVS*FQY
   SPLZ=3.0*DC*SCAL*CWS*Q+TMU
   FPLZ=3.0*DC*SCAL*CWS*FQZ
   PROM=FUY*T(5,1)+FUZ*T(1,1)+FVY*T(8,1)+(FWY+FVZ)*T(10,1)+FWZ*T(9,1)
   PROP=FUY*FUY*T(6,1)+FUZ*FUZ*T(2,1)-Q*SCALE*(FWY+FVZ)**2/3.0
C
C COMPUTE MATRIX ELEMENTS FOR QQ
C
   TEMD=SPLZ*SPRZ(XMYV(1),XV(1),XPYV(1))+FPLZ*FKZ
   TEMC=FPRZ(XMYV(1)*XMYV(5),XV(1)*XV(5),XPYV(1)*XPYV(5))
   XMAT(1)=-SPLY*SYM-FPLY*FYM+ADM
   YMAT(1)=DXX-SPLY*SY-FPLY*FY+AD+CL+2.0*(PROM+G*T(3,1))
   ZMAT(1)=-SPLY*SYP-FPLY*FYP+ADP
   DVEC(1)=DXX*XV(1)-2.0*(PROP+G*FRZ*T(4,1))+TEMD-TEMC
C
C COMPUTE MATRIX ELEMENTS FOR RHO
C
   TEMM=T(7,1)-XK
   TEMP=FPRY(T(7,3),T(7,1),T(7,2))
   TEMD=(T(4,1)-XK)*SPRZ(XMYV(2),XV(2),XPYV(2))
1  +FPRZ(T(4,5),T(4,1),T(4,4))*FRZ
   TEMQ=FPRZ(T(3,5)*XMYV(1),T(3,1)*XV(1),T(3,4)*XPYV(1))
   TEMC=FPRZ(XMYV(2)*XMYV(5),XV(2)*XV(5),XPYV(2)*XPYV(5))
   XMAT(2)=TEMM*SYM+TEMP*FYM+ADM
   YMAT(2)=DXX+TEMM*SY+TEMP*FY+AD
   ZMAT(2)=TEMM*SYP+TEMP*FYP+ADP
   DVEC(2)=DXX*XV(2)-TEMD-TEMQ-DRDZ*XV(5)-TEMC
   IF (NSTAT-2) 50,60,50
C
C COMPUTE MATRIX ELEMENTS FOR U
C
50 TEMM=T(6,1)-TMU

```

```

TEMP=FPRY(T(6,3),T(6,1),T(6,2))
TEMQ=(T(2,1)-TMU)*SPRZ(XMYV(3),XV(3),XPYV(3))
1 +FPRZ(T(2,5),T(2,1),T(2,4))*FUZ
TEMQ=FPRY(T(5,3)*XZMV(1),T(5,1)*XV(1),T(5,2)*XZPV(1))
1 +FPRZ(T(1,5)*XMYV(1),T(1,1)*XV(1),T(1,4)*XPYV(1))
TEMC=FPRZ(XMYV(3)*XMYV(5),XV(3)*XV(5),XPYV(3)*XPYV(5))
XMAT(3)=TEMM*SYM+TEMP*FYM+ADM
YMAT(3)=DXX+TEMM*SY+TEMP*FY+AD
ZMAT(3)=TEMM*SYP+TEMP*FYP+ADP
DVEC(3)=DXX*XV(3)-TEMQ-TEMQ-TEMC
IF (NSTAT-2) 70,60,60

C
C COMPUTE MATRIX ELEMENTS FOR V
C
60 TEMD=Q*SL*FPRZ(FPRY(XMMV(5),XMYV(5),XMPV(5)),FWY,
1 FPRY(XPMV(5),XPYV(5),XPPV(5)))
TEMQ=FPRY(T(8,3)*XZMV(1),T(8,1)*XV(1),T(8,2)*XZPV(1))
1 +FPRZ(T(10,5)*XMYV(1),T(10,1)*XV(1),T(10,4)*XPYV(1))
TEMC=FPRZ(XMYV(4)*XMYV(5),XV(4)*XV(5),XPYV(4)*XPYV(5))
XMAT(4)=-TMU*SYM+ADM
YMAT(4)=DXX-TMU*SY+AD+TEMK
ZMAT(4)=-TMU*SYP+ADP
DVEC(4)=DXX*XV(4)+TMU*SPRZ(XMYV(4),XV(4),XPYV(4))
1 +TEMQ-FPRY(TZMV(6),TV(6),TZPV(6))-TEMQ+TEMK*ZEROV(4)
2 +Q*SL*SPRZ(XMYV(4),XV(4),XPYV(4))+SL*FQZ*(FWY+FVZ)-TEMC

C
C COMPUTE MATRIX ELEMENTS FOR W
C
TEMD=Q*SL*FPRY(FPRZ(XMMV(4),XZMV(4),XPMV(4)),FVZ,
1 FPRZ(XMPV(4),XZPV(4),XPPV(4)))
TEMQ=FPRY(T(10,3)*XZMV(1),T(10,1)*XV(1),T(10,2)*XZPV(1))
1 +FPRZ(T(9,5)*XMYV(1),T(9,1)*XV(1),T(9,4)*XPYV(1))
TEMC=FPRZ(XMYV(5)*XMYV(5),XV(5)*XV(5),XPYV(5)*XPYV(5))
XMAT(5)=-TMU*SYM+ADM-SL*(Q*SYM+FQY*FYM)
YMAT(5)=DXX-TMU*SY+AD+TEMK-SL*(Q*SY+FQY*FY)
ZMAT(5)=-TMU*SYP+ADP-SL*(Q*SYP+FQY*FYP)
DVEC(5)=DXX*XV(5)+TMU*SPRZ(XMYV(5),XV(5),XPYV(5))
1 +TEMQ-FPRZ(TMYV(6),TV(6),TPYV(6))-TEMQ+TEMK*ZEROV(5)
2 +SL*FQY*FVZ-G*XV(2)-TEMC

C
C COMPUTE MATRIX ELEMENTS FOR SCALE
C
70 IF (XV(1)-QCUT*FMAXV(1)) 80,80,90
80 DVEC(6)=2.0*SCALE
GO TO 100
90 TEMD=SPLZ*SPRZ(XMYV(6),XV(6),XPYV(6))+FPLZ*FLZ
TEMC=FPRZ(XMYV(6)*XMYV(5),XV(6)*XV(5),XPYV(6)*XPYV(5))
XMAT(6)=XMAT(1)
YMAT(6)=DXX-SPLY*SY-FPLY*FY+AD
1 +S1*(PROM+PROP/XV(1))+S2*CL/2.0+S5*G*(T(3,1)+T(4,1))*FRZ/XV(1))
2 +S7*XV(6)*(FQY*FWY+FQZ*FWZ)/Q+S8*(FQY*FLY+FQZ*FLZ)
ZMAT(6)=ZMAT(1)
DVEC(6)=DXX*XV(6)+TEMD-S6*Q*(FLY*FLY+FLZ*FLZ)-TEMC

C
C LOWER BOUNDARY CONDITION CHECK
C
100 IF (JY-2) 200,110,105
105 IF (JY-IYPSN) 300,300,500
110 IF (LYLFF) 500,300,300

```



```
200  DO 220 I=1,NWVEC  
      TEM=1.0  
      IF (IRFV(I,1)) 205,205,210  
205  TEM=-1.0  
210  ZMAT(I)=ZMAT(I)+TEM*XMAT(I)  
220  CONTINUE  
      GO TO 400  
300  DO 320 I=1,NWVEC  
      DVEC(I)=DVEC(I)-XMAT(I)*ZEROV(I)  
320  CONTINUE  
400  CALL SFVFL(0.0,XMAT,NWVEC)  
500  RETURN  
      END  
CART ID 0105  DB ADDR 45C0  DB CNT 017A
```

WAKMZ,S(0105)

**WAKMZ - STRATIFIED SUBMARINE WAKE, Z IMPLICIT MATRIX COEFFICIENTS
SUBROUTINE WAKMZ

C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES THE X,Y,Z AND D MATRIX
C COEFFICIENTS FOR THE Z IMPLICIT UPSWEEP

C DIMENSION T(10,5)

*COPY (CMWAK)
EQUIVALENCE (T(1,1),ZNEWV(1))

C FPRZ(ARGM,ARG,ARGP)=FZM*(ARGM+FZS*ARG-FZR*ARGP)
C FPRY(ARGM,ARG,ARGP)=FYM*(ARGM+FYS*ARG-FYR*ARGP)
C SPKZ(ARGM,ARG,ARGP)=SZM*ARGM+SZ*ARG+SZP*ARGP
C SPRY(ARGM,ARG,ARGP)=SYM*ARGM+SY*ARG+SYP*ARGP

C COMPUTE SPACING FACTORS

C DZM=Z-ZM
C DZP=ZP-Z
C DZT=DZM+DZP
C FZM=-DZP/DZM/DZT
C FZP=DZM/DZP/DZT
C FZ=-FZM-FZP
C TEM=DZM/DZP
C FZR=TEM*TEM
C FZS=FZR-1.0
C SZM=2.0/DZM/DZT
C SZP=2.0/DZP/DZT
C SZ=-SZM-SZP

C DYM=Y-YM
C DYP=YP-Y
C DYT=DYM+DYP
C FYM=-DYP/DYM/DYT
C FYP=DYM/DYP/DYT
C FY=-FYM-FYP
C TEM=DYM/DYP
C FYR=TEM*TEM
C FYS=FYR-1.0
C SYM=2.0/DYM/DYT
C SYP=2.0/DYP/DYT
C SY=-SYM-SYP

C CALL SFVFL(0.0,XMAT,NWVEC)
C CALL SFVFL(1.0,YMAT,NWVEC)
C CALL SFVFL(0.0,ZMAT,NMOVE)

C COMPUTE MULTIPLICATIVE FACTORS

C CALL WAKDG(ZM)
C CALL WAKMV(XMYV,TMYV,T(1,5))
C CALL WAKDG(ZP)
C CALL WAKMV(XPYV,TPYV,T(1,4))
C CALL WAKDG(Z)
C CALL WAKMV(XZMV,TZMV,T(1,3))
C CALL WAKMV(XZPV,TZPV,T(1,2))
C CALL WAKMV(XV,TV,T(1,1))
C TMU=FMU

```

IF (SPORS) 40,40,20
20 TEM=Y*Y/YSCAL/YSCAL+Z*Z/ZSCAL/ZSCAL
IF (TEM-PCUT) 40,40,30
30 TMU=CMU
40 CL=2.0*(AS*TMU/SCALE+B*Q)/SCALE
C
C COMPUTE DERIVATIVE FACTORS
C
DXX=DXI*(U+XV(5))
CALL WAKLL(TEMK,1)
ADM=FZM*XMYV(5)
AD=FZ*XV(5)
ADP=FZP*XPYV(5)
SL=SCALE/3.0
FQY=FPRY(SQRT(XZMV(1)),Q,SQRT(XZPV(1)))
FQZ=FPRZ(SQRT(XMYV(1)),Q,SQRT(XPYV(1)))
FKY=FPRY(XZMV(1),XV(1),XZPV(1))
FRY=FPRY(XZMV(2),XV(2),XZPV(2))
FRZ=FPRZ(XMYV(2),XV(2),XPYV(2))
FUY=FPRY(XZMV(3),XV(3),XZPV(3))
FUZ=FPRZ(XMYV(3),XV(3),XPYV(3))
FVY=FPRY(XZMV(4),XV(4),XZPV(4))
FVZ=FPRZ(XMYV(4),XV(4),XPYV(4))
FWY=FPRY(XZMV(5),XV(5),XZPV(5))
FWZ=FPRZ(XMYV(5),XV(5),XPYV(5))
FLY=FPRY(XZMV(6),XV(6),XZPV(6))
FLZ=FPRZ(XMYV(6),XV(6),XPYV(6))
SPLY=3.0*DC*YSCAL*CVS*Q+TMU
FPLY=3.0*DC*YSCAL*CVS*FQY
SPLZ=3.0*DC*SCAL*CWS*Q+TMU
FPLZ=3.0*DC*SCAL*CWS*FQZ
PROM=FUY*T(5,1)+FUZ*T(1,1)+FVY*T(8,1)+(FWY+FVZ)*T(10,1)+FWZ*T(9,1)
PROP=FUY*FUY*T(6,1)+FUZ*FUZ*T(2,1)-Q*SCALE*(FWY+FVZ)**2/3.0
C
C COMPUTE MATRIX ELEMENTS FOR QQ
C
TEMD=SPLY*SPRY(XZMV(1),XV(1),XZPV(1))+FPLY*FKY
TEMC=FPRY(XZMV(1)*XZMV(4),XV(1)*XV(4),XZPV(1)*XZPV(4))
XMAT(1)=-SPLZ*SZM-FPLZ FZM+ADM
YMAT(1)=DXX-SPLZ*SZ-FPLZ*FZ+AD+CL+2.0*(PROM+G*T(3,1))
ZMAT(1)=-SPLZ*SZP-FPLZ*FZP+ADP
DVEC(1)=DXX*XV(1)-2.0*(PROP+G*FRZ*T(4,1))+TEMD-TEMC
C
C COMPUTE MATRIX ELEMENTS FOR RHO
C
TEMM=T(4,1)-XK
TEMP=FPRZ(T(4,5),T(4,1),T(4,4))
TEMD=(T(7,1)-XK)*SPRY(XZMV(2),XV(2),XZPV(2))
1 +FPRY(T(7,3),T(7,1),T(7,2))*FRY
TEMQ=FPRZ(T(3,5)*XMYV(1),T(3,1)*XV(1),T(3,4)*XPYV(1))
TEMC=FPRY(XZMV(2)*XZMV(4),XV(2)*XV(4),XZPV(2)*XZPV(4))
XMAT(2)=TEMM*SZM+TEMP*FZM+ADM
YMAT(2)=DXX+TEMM*SZ+TEMP*FZ+AD
ZMAT(2)=TEMM*SZP+TEMP*FZP+ADP
DVEC(2)=DXX*XV(2)-TEMD-TEMQ-DRDZ*XV(5)-TEMC
IF (NSTAT-2) 50,60,50
C
C COMPUTE MATRIX ELEMENTS FOR U
C

```

```

50  TEMM=T(2,1)-TMU
    TEMP=FPRZ(T(2,5),T(2,1),T(2,4))
    TEMD=(T(6,1)-TMU)*SPRY(XZMV(3),XV(3),XZPV(3))
1   +FPRY(T(6,3),T(6,1),T(6,2))*FUJ
    TEMQ=FPRY(T(5,3)*XZMV(1),T(5,1)*XV(1),T(5,2)*XZPV(1))
1   +FPRZ(T(1,5)*XMYV(1),T(1,1)*XV(1),T(1,4)*XPYV(1))
    TEMC=FPRY(XZMV(3)*XZMV(4),XV(3)*XV(4),XZPV(3)*XZPV(4))
    XMAT(3)=TEMM*SZM+TEMP*FZM+ADM
    YMAT(3)=DXX+TEMM*SZ+TEMP*FZ+AD
    ZMAT(3)=TEMM*SZP+TEMP*FZP+ADP
    DVEC(3)=DXX*XV(3)-TEMD-TEMQ-TEMC
    IF (NSTAT-2) 70,60,60

C
C  COMPUTE MATRIX ELEMENTS FOR V
C
60  TEMD=Q*SL*FPRZ(FPRY(XMMV(5),XMYV(5),XMPV(5)),FWY,
1   FPRY(XPMV(5),XPYV(5),XPPV(5)))
    TEMQ=FPRY(T(8,3)*XZMV(1),T(8,1)*XV(1),T(8,2)*XZPV(1))
1   +FPRZ(T(10,5)*XMYV(1),T(10,1)*XV(1),T(10,4)*XPYV(1))
    TEMC=FPRY(XZMV(4)*XZMV(4),XV(4)*XV(4),XZPV(4)*XZPV(4))
    XMAT(4)=-TMU*SZM+ADM-SL*(Q*SZM+FQZ*FZM)
    YMAT(4)=DXX-TMU*SZ+AD+TEMK-SL*(Q*SZ+FQZ*FZ)
    ZMAT(4)=-TMU*SZP+ADP-SL*(Q*SZP+FQZ*FZP)
    DVEC(4)=DXX*XV(4)+TMU*SPRY(XZMV(4),XV(4),XZPV(4))
1   +TEMD-FPRY(TZMV(6),TV(6),TZPV(6))-TEMQ+TEMK*ZEROV(4)
2   +SL*FQZ*FWY-TEMC

C
C  COMPUTE MATRIX ELEMENTS FOR W
C
    TEMD=Q*SL*FPRY(FPRZ(XMMV(4),XZMV(4),XPMV(4)),FVZ,
1   FPRZ(XMPV(4),XZPV(4),XPPV(4)))
    TEMQ=FPRY(T(10,3)*XZMV(1),T(10,1)*XV(1),T(10,2)*XZPV(1))
1   +FPRZ(T(9,5)*XMYV(1),T(9,1)*XV(1),T(9,4)*XPYV(1))
    TEMC=FPRY(XZMV(5)*XZMV(4),XV(5)*XV(4),XZPV(5)*XZPV(4))
    XMAT(5)=-TMU*SZM+ADM
    YMAT(5)=DXX-TMU*SZ+AD+TEMK
    ZMAT(5)=-TMU*SZP+ADP
    DVEC(5)=DXX*XV(5)+TMU*SPRY(XZMV(5),XV(5),XZPV(5))
1   +TEMD-FPRZ(TMYV(6),TV(6),TPYV(6))-TEMQ+TEMK*ZEROV(5)
2   +Q*SL*SPRY(XZMV(5),XV(5),XZPV(5))+SL*FQY*(FWY+FVZ)-G*XV(2)-TEMC

C
C  COMPUTE MATRIX ELEMENTS FOR SCALE
C
70  IF (XV(1)-QCUT*FMAXV(1)) 80,80,90
80  DVEC(6)=2.0*SCALE
    GO TO 100
90  TEMD=SPLY*SPRY(XZMV(6),XV(6),XZPV(6))+FPLY*FLY
    TEMC=FPRY(XZMV(6)*XZMV(4),XV(6)*XV(4),XZPV(6)*XZPV(4))
    XMAT(6)=XMAT(1)
    YMAT(6)=DXX-SPLZ*SZ+PLZ*FZ+AD
1   +S1*(PROM+PROP/XV(1))+S2*CL/2.0+S5*G*(T(3,1)+T(4,1))*FRZ/XV(1))
2   +S7*XV(6)*(FQY*FWY+FQZ*FLZ)/Q+S8*(FQY*FLY+FQZ*FLZ)
    ZMAT(6)=ZMAT(1)
    DVEC(6)=DXX*XV(6)+TEMD-S6*Q*(FLY*FLY+FLZ*FLZ)-TEMC

C
C  LOWER BOUNDARY CONDITION CHECK
C
100 IF (JZ-1) 200,110,102
102 IF (JY-IYPSM) 104,500,106

```

```
104 IF (JY-1) 500,500,300
106 IF (JY-IYPEM) 500,500,300
110 IF (LZLFF) 500,300,300
200 DO 220 I=1,NWVEC
      TEM=1.0
      IF (IRFV(I,2)) 205,205,210
205 TEM=-1.0
210 ZMAT(I)=ZMAT(I)+TEM*XMAT(I)
220 CONTINUE
      GO TO 400
300 DO 320 I=1,NWVEC
      DVEC(I)=DVEC(I)-XMAT(I)*ZEROV(I)
320 CONTINUE
400 CALL SFVFL(0.0,XMAT,NWVEC)
500 RETURN
      END
CART ID 0105 DB ADDR 4740 DB CNT 0180
```

WAKOT,S(C105)

**WAKOT - STRATIFIED SUBMARINE WAKE, OUTPUT THE RESULTS
SUBROUTINE WAKOT

C

C THIS SUBROUTINE IN THE WAKE PROGRAM OUTPUTS THE RESULTS

C

DIMENSION JVCHV(7),JPOS(2),PBUF(880),KLOCK(6),HDSV(2,2)
DIMENSION TOTAL(7,40,2),OVEC(33),DBUF(440),NN(40),MM(40),HNUL(2)

*COPY (CMWAK)

EQUIVALENCE (TOTAL(1,1,1),ROWG(1,1))
EQUIVALENCE (PBUF(1),ROWB(1,1,3)),(PBUF(441),DBUF(1))
EQUIVALENCE (NN(1),NRNZV(1)),(MM(1),NRNYV(1))

C

DATA JPOS/1HY,1HZ/,JERRX/2H /,HNUL/4H ,4HNUL/
DATA JVCHV/2HQG,2HRU,2HU ,2HV ,2HW ,2HSL,2HP /
DATA HDSV/4H ,4H ,4H(STO,4HRED)/

C

1000 FORMAT(/6X,24HFULL PROFILE OUTPUT FOR ,A2,1X,2A4,1X,A4)

1001 FORMAT(1H)

1003 FORMAT(/7X,5HZ Y,10E12.4)

1004 FORMAT(/6X,23HMESH PROFILE OUTPUT AT ,A1,2H = ,E12.4//

1 7X,A1,7(10X,A2))

1010 FORMAT(/6X,32HTURBULENCE PROFILE OUTPUT AT Z = ,E12.4//

1 7X,1HY,10X,2HUV,10X,2HUW,10X,2HVV,10X,2HUR,10X,2HVR,10X,2HWR,
2 10X,2HRR,10X,2HUU,10X,2HVV,10X,2HWW/)

1015 FORMAT(/6X,8HX POINTS,9X,1HX,13X,2HDX,10X,

1 8HY SPREAD,7X,8HY POINTS,7X,8HZ SPREAD,7X,
2 8HZ POINTS,9X,3HX/U,11X,3HB V/I10,4X,3E15.5,
3 19,6X,E15.5,19,6X,2E14.5)

1021 FORMAT(/6X,6HSTATUS,7X,8HZ LAMBDA,7X,8HR LAMBDA,

1 7X,8HY LAMBDA,7X,8HMOMENTUM,
2 7X,8HP ENERGY,7X,8HK ENERGY,14X,12HELAPSED TIME/
3 6X,A4,4X,6E15.5,8X,12,5H HRS ,12,5H MIN ,12,4H SEC)

1036 FORMAT(/14X,7(10X,A2))

1037 FORMAT(18H MAXIMUM VALUE ,7E12.4)

1038 FORMAT(18H Y LOCATION ,7E12.4)

1039 FORMAT(18H Z LOCATION ,7E12.4)

1040 FORMAT(18H MAXIMUM CHANGE ,7E12.4)

1041 FORMAT(18H GLOBAL MAXIMUM ,7E12.4)

1045 FORMAT(/18X,2HUV,10X,2HUW,10X,2HVV,10X,2HUR,10X,2HVR,10X,2HWR,

1 10X,2HRR,10X,2HUU,10X,2HVV,10X,2HWW/12H MAXIMUMS ,10E12.4)

1049 FORMAT(/6X,6HSTATUS,8X,8HX POINTS,9X,1HX/6X,A4,I14,E19.5)

2000 FORMAT(/19H BACKUP NEEDED FOR ,A2)

2001 FORMAT(/26H DIVIDE CHECK HAS OCCURRED)

2002 FORMAT(/22H OVERFLOW HAS OCCURRED)

2003 FORMAT(/33H SOLUTION HAS SPREAD TOO FAST IN ,A1,5X,4I6)

2005 FORMAT(/22H RUN SUSPENDED AT X = ,E12.5,5X,11HX POINTS = ,I3,

1 5X,6HNPS = ,I3,5X,6HNPS = ,I3)

2006 FORMAT(/48H MAXIMUM POINTS EXCEEDED ON AUTOPOINT ADJUST IN ,A1)

2007 FORMAT(/22H GLOBAL FILE IS FILLED)

2008 FORMAT(/20H PLOT FILE IS FILLED)

2009 FORMAT(/4H WAK,A2,19H ERROR HAS OCCURRED)

2010 FORMAT(/20H TOTAL ELAPSED TIME ,12,5H HRS ,12,5H MIN ,12,4H SEC)

2011 FORMAT(/49H TOTAL PROFILES STORED AT THIS X ON THE PLOT FILE)

2012 FORMAT(/26H MAXIMUM RUN TIME EXCEEDED)

2031 FORMAT(11E12.4)

2032 FORMAT(E12.4,12X,9E12.4)

2033 FORMAT(E12.4,24X,8E12.4)

2034 FORMAT(E12.4,36X,7E12.4)

```

2035 FORMAT(E12.4,48X,6E12.4)
2036 FORMAT(E12.4,60X,5E12.4)
2037 FORMAT(E12.4,72X,4E12.4)
2038 FORMAT(E12.4,84X,3E12.4)
2039 FORMAT(E12.4,96X,2E12.4)
2040 FORMAT(E12.4,108X,E12.4)

```

C

C CHECK FOR ERRORS

C

```

IOLAY=10
MOOD=1
NRSTX=NRST-1
NREND=NRST+JEND
NZP=JEND+2
NYPSX=NYPS-1
NYPEX=NYPE+1
NYP=NYPE-NYPS+3
LTRNF=LTRNF+LOVCF+LOVFF+LPKRF+LFCUR
IF (LBUF) 105,105,100
100 WRITE (NOUT,2000) JVCHV(LBUF)
105 IF (JERR-JERRX) 106,107,106
106 WRITE (NOUT,2009) JERR
LTRNF=1
107 IF (LTRNF) 110,200,110
110 IF (LOVCF) 120,130,120
120 WRITE (NOUT,2001)
130 IF (LOVFF) 140,150,140
140 WRITE (NOUT,2002)
150 IF (LPKRF) 160,190,160
160 WRITE (NOUT,2003) JPOS(LPKRF),NYPS,NYPE,NRST,JEND
190 IF (LFCUR) 195,200,195
195 WRITE (NOUT,2006) JPOS(LFCUR)
200 IF (LPRFL) 205,900,900

```

C

C CHECK FOR INTERMEDIATE PRINTOUT TO LINE PRINTER

C

```

205 IF (LIOLF) 210,300,210
210 CALL CLOCK(1,KLOCK)
Y=YOLDV(NYPEX)-YOLDV(NYPSX)
Z=ZOLDV(NREND)-ZOLDV(NRSTX)
YP=XFACT*XP+XZERO
ZP=YP*SQRT(G)/3.1416
WRITE (NOUT,1021) JSTAT,(EPSSV(I),I=1,3),XMOM,XPE,XKE,
1 (KLOCK(I),I=1,6,2)
WRITE (NOUT,1015) NPTSN,XP,DX,Y,NYP,Z,NZP,YP,ZP
WRITE (NOUT,1045) TURBX
WRITE (NOUT,1036) JVCHV
WRITE (NOUT,1001)
WRITE (NOUT,1037) FMAXV
WRITE (NOUT,1038) YMAXV
WRITE (NOUT,1039) ZMAXV
WRITE (NOUT,1040) TMAXV
WRITE (NOUT,1041) GMAXV

```

C

C CHECK FOR INTERMEDIATE PRINTOUT TO GLOBAL DISK FILE

C

```

300 IF (LIOPF) 310,400,310
310 NRX=33
IF (NCFRL(GLOID,NG,NRX+1)) 320,330,330

```

A-48

```
320 LTRNF=1
    WRITE (NOUT,2007)
    GO TO 400
330 OVEC(1)=XP
    CALL SFVMV(YSCAL,OVEC(2),2)
    CALL SFVMV(XMOM,OVEC(4),20)
    CALL SFVMV(GM,OVEC(24),8)
    OVEC(32)=GM(11)
    OVEC(33)=DEPST
    CALL PBFOW(GLOID,NG,NRX,OVEC)
    NRX=NG
    CALL PBFOW(GLOID,NRX,1,-1.0)
C
C CHECK FOR MESH PRINTOUT TO LINE PRINTER
C
400 IF (LFOLF) 404,450,404
404 WRITE (NOUT,1049) JSTAT,NP1SN,XP
    DO 409 I=1,NVART
    IF (FMAXV(I)) 409,409,405
405 DO 406 JY=NYP1SX,NYP1EX
    TOTAL(I,JY,1)=TOTAL(I,JY,1)/FMAXV(I)
406 CONTINUE
    DO 407 JZ=NRSTX,NKEND
    TOTAL(I,JZ,2)=TOTAL(I,JZ,2)/FMAXV(I)
407 CONTINUE
409 CONTINUE
    ZM=EPSSV(1)/2.0/C
    YM=EPSSV(3)/2.0/C
    WRITE (NOUT,1004) JPOS(2),ZOUT,JPOS(1),JVCHV
    WRITE (NOUT,1001)
    DO 410 JY=NYP1SX,NYP1EX
    Y=YOLDV(JY)/YM
    WRITE (NOUT,2031) Y,(TOTAL(I,JY,1),I=1,NVART)
410 CONTINUE
    WRITE (NOUT,1004) JPOS(1),YOUT,JPOS(2),JVCHV
    WRITE (NOUT,1001)
    DO 420 JZ=NRSTX,NKEND
    Z=ZOLDV(JZ)/ZM
    WRITE (NOUT,2031) Z,(TOTAL(I,JZ,2),I=1,NVART)
420 CONTINUE
```

```
C
C CHECK FOR TOTAL TURBULENCE PRINTOUT TO LINE PRINTER
C
450 IF (LSOLF) 460,500,460
460 IF (LAMIN) 500,461,500
461 WRITE (NOUT,1049) JSTAT,NP1SN,XP
    GMAX=1.0E-06*FMAXV(1)
    DO 480 JZ=NRSTX,NKEND
    IYPS=IYPSV(JZ)
    IYPE=IYPEV(JZ)
    IF (IYPS) 480,480,462
462 IYPSX=IYPS+LYLFF
    CALL WAKMG(JZ,ZV,1)
    IYS=0
    DO 468 JY=IYPSX,IYPE
    DO 465 I=1,10
    IF (ABS(ROWG(I,JY))-GMAX) 465,465,466
465 CONTINUE
    GO TO 468
```



```

466 IYE=JY
    IF (IYS) 468,467,468
467 IYS=JY
468 CONTINUE
    IF (IYS) 469,480,469
469 WRITE (NOUT,1010) ZOLDV(JZ)
    DO 470 JY=IYS,IYE
    WRITE (NOUT,2031) YOLDV(JY),(ROWG(1,JY),I=1,10)
470 CONTINUE
480 CONTINUE
C
C CHECK FOR TOTAL PRINTOUT TO PROFILE DISK FILE
C
500 IF (LTOPF) 510,600,510
510 IVECA=NYP
    IVECB=NZP
    J=0
    DO 515 I=1,NVART
    J=J+IDSV(I)
515 CONTINUE
    NRX=J*IVECA*IVECB+IVECA+IVECB+3
    IF (NDFRL(PLTID,NP,NRX)) 520,530,530
520 LTRNF=1
    LTOPF=0
    WRITE (NOUT,2008)
    GO TO 600
530 ZA=XP
    CALL PBFDW(PLTID,NP,2,ZA)
    CALL PBFDW(PLTID,NP,IVECA,YOLDV(NYPSX))
    CALL PBFDW(PLTID,NP,IVECB,ZOLDV(NRSTX))
    WRITE (NOUT,2011)
    GO TO 601
C
C CHECK FOR TOTAL PRINTOUT TO LINE PRINTER
C
600 IF (LTOLF) 601,700,601
601 IKOWR=2
    IF (LEURF) 604,604,603
603 IKOWR=4
604 IF (LTOLF) 608,610,608
606 WRITE (NOUT,1049) JSTAT,NPTSN,XP
610 DO 680 IVAR=1,NVART
    CALL SFVFL(ZEROV(IVAR),PBUF,880)
    K=1
    GMAX=GMAXV(IVAR)
    JVAR=IVAR
    IF (IVAR-NVART) 612,611,611
611 JVAR=6
    IKOWR=IKOWT
612 GO TO (6125,6125,6121,6122,6122,6125,6122),IVAR
6121 IF (NSTAT-2) 6125,680,6125
6122 IF (NSTAT-1) 6125,680,6125
6125 IF (LTOLF) 613,614,613
613 IF (GMAX) 6132,6132,6135
6132 K=2
6135 I=MMIN(1,LTOPF)*IDSV(IVAR)+1
    WRITE (NOUT,1000) JVCHV(IVAR),(HDSV(J,I),J=1,2),HNUL(K)
614 DO 670 IYP=1,NYP,10
    IYPSX=NYPSX+IYP-1

```

```

IYPEX=MMIN(IYPSX+9,NYPEX)
N=IYPEX-IYPSX+1
K=N+1
NZP=440/K*K
IF (LTOLF) 616,618,616
616 IF (GMAX) 618,618,6165
6165 WRITE (NOUT,1003) (YOLDV(I),I=IYPSX,IYPEX)
WRITE (NOUT,1001)
618 I=0
J=0
L=0
DO 650 NR=NRSTX,NREND
NPOS=NR
I=I+1
CALL WAKRR(NR,ZV)
PBUF(I)=Z
IF (NR-NRST) 6181,6183,6184
6181 IF (LZLFF) 6187,6182,6182
6182 IYPS=IYPSV(NR+1)
IYPE=IYPEV(NR+1)
GO TO 619
6183 IF (LZLFF) 6186,6187,6187
6184 IF (NR-NREND) 6186,6185,6185
6185 IYPS=IYPSV(NR-1)
IYPE=IYPEV(NR-1)
GO TO 619
6186 IYPS=MMIN(IYPS,IYPSV(NR-1))
IYPE=MMAX(IYPE,IYPEV(NR-1))
IF (NR-NREND+1) 6187,619,619
6187 IYPS=MMIN(IYPS,IYPSV(NR+1))
IYPE=MMAX(IYPE,IYPEV(NR+1))
619 L=L+1
NN(L)=0
MM(L)=1
DO 640 JY=IYPSX,IYPEX
I=I+1
J=J+1
IF (JY-IYPS+1) 6195,630,620
6195 MM(L)=MM(L)+1
GO TO 640
620 IF (JY-IYPE-1) 630,630,621
621 I=I+IYPEX-JY
J=J+IYPEX-JY
GO TO 641
630 CALL WAKMP(IROWR,NR,JY,XV,1)
PBUF(I)=XV(JVAR)
DBUF(J)=XV(JVAR)
NN(L)=NN(L)+1
640 CONTINUE
641 IF (I-NZP) 6415,642,642
6415 IF (NR-NREND) 650,642,642
642 I=I/K
IF (LTOPF) 6432,6438,6432
6432 IF (IDSV(IVAR)) 6434,6436,6434
6434 CALL PBFOW(PLTID,NP,J,DBUF)
6436 IF (LTOLF) 6438,646,6438
6438 IF (GMAX) 646,646,644
644 DO 645 JZ=1,I
IF (NN(JZ)) 645,645,6440

```

```

6440  J=MM(JZ)
      L=(JZ-1)*K+1
      JS=L+J
      JE=JS+NN(JZ)-1
      GO TO (6441,6442,6443,6444,6445,6446,6447,6448,6449,6450),J
6441  WRITE (NOUT,2031) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6442  WRITE (NOUT,2032) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6443  WRITE (NOUT,2033) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6444  WRITE (NOUT,2034) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6445  WRITE (NOUT,2035) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6446  WRITE (NOUT,2036) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6447  WRITE (NOUT,2037) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6448  WRITE (NOUT,2038) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6449  WRITE (NOUT,2039) PBUF(L),(PBUF(J),J=JS,JE)
      GO TO 645
6450  WRITE (NOUT,2040) PBUF(L),(PBUF(J),J=JS,JE)
645   CONTINUE
646   I=0
      J=0
      L=0
      CALL SFVFL(ZEROV(IVAR),PBUF,880)
650   CONTINUE
670   CONTINUE
680   CONTINUE
      IF (LTOPF) 690,700,690
690   NRX=NP
      CALL PBFDW(PLTID,NRX,1,-1.0)
C
C   WRITE COMPLETED SOLUTION FOR NEXT INTEGRATION STEP (WAKSC)
C
700   IF (LMLFL) 702,800,800
702   NPTS=NPTSN
      X=XP
      IF (LSTFL) 705,710,705
705   LSTFL=0
710   NRX=1
      CALL PBFDW(COMID,NRX,NCOMT,NSTST)
C
C   SET UP FOR RETURN OR END
C
800   IF (LTRNF) 900,850,900
850   N=1
      GO TO 910
860   IF (KLOCK(1)-MXHRS) 870,880,880
870   IF (JOB) 875,875,872
872   IF (JS-JOB) 875,900,900
875   RETURN
880   WRITE (NOUT,2012)
900   N=2
      JS=NG/160+MMIN(1,NIUPP)
      JE=NP/160+MMIN(1,NTUPP)

```

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```
910  WRITE (NOUT,2005) XP,NPTSN,JS,JE
      CALL CLOCK(1,KLOCK)
      JS=KLOCK(3)
      DO 924 I=1,6,2
      J=6-I
      K=J-2
      JE=KLOK(J)+KLOCK(J)
      IF (K) 923,923,921
921  IF (JE-59) 923,923,922
922  JE=JE-60
      KLOCK(K)=KLOCK(K)+1
923  KLOCK(J)=JE
924  CONTINUE
      GO TO (860,930),N
930  DO 932 I=1,6,2
      KLOK(I)=KLOCK(I)
932  CONTINUE
      WRITE (NOUT,2010) (KLOK(I),I=1,6,2)
      NRX=1
      CALL PBFOW(COMID,NRX,NCOMT,NSTST)
      CALL CLBFR(BUFR)
      CALL CLBFR(BUFS)
      CALL EXIT
      END
CART ID 0105  DB ADDR 5270  DB CNT 02F2
```

```

WAKPC,S(0105)
**WAKPC - STRATIFIED SUBMARINE WAKE, PRESSURE CALCULATION
SUBROUTINE WAKPC
C
C THIS SUBROUTINE IN THE WAKE PROGRAM CONTROLS THE SOLUTION
C FOR THE PRESSURE BY THE POISSON EQUATION
C
C DIMENSION TOTAL(7,40,2),PN(5),VALUE(40,2)
*COPY (CMWAK)
EQUIVALENCE (TOTAL(1,1,1),ROWG(1,1)),(MM,EPSXV(1))
EQUIVALENCE (ERROR,GM(12)),(GM(10),DUI),(GM(9),DLI)
EQUIVALENCE (VALUE(1,1),ROWG(1,36))
C
C DATA PN/10.,30.,60.,100.,150./
C
1000 FORMAT(/6X,6HSTATUS,7X,9HXX POINTS,6X,9HMAX VALUE,6X,
1 10HMAX CHANGE,8X,3HDXX,11X,5HERROR/8X,2HPR: I14,5X,4E15.5)
2010 FORMAT(/41H PROGRAM EXIT DURING PRESSURE COMPUTATION)
C
C CHECK RUN POSITION
C
C IOLAY=8
IF (LSTFL) 50,105,100
50 LSTFL=LPRFL
IF (LSTFL) 310,85,85
85 MPTS=MM
DXX=EPSXV(2)
GO TO 109
100 IF (LPRFL) 310,105,105
105 MPTS=0
NREND=NRST+JEND
Y=YOLDV(NYPE+1)-YOLDV(NYPS-1)
Z=ZOLDV(NKEND)-ZOLDV(NRST-1)
DXX=PNORM*Y*Z/PN(1)
109 LPRFL=-1
MOOD=0
IBOT=1
ITOP=MXRY
LYFAF=0
CALL SFVMV(ZEROV,XPPV,NWVEC)
CALL SFVFL(0.0,ZEROV,NWVEC)
IF (LFOLF) 1090,110,1090
1090 NYPSX=NYPS+LYLFF
DO 1094 JY=NYPSX,NYPE
IF (YOUT-YOLDV(JY)) 110,1096,1092
1092 IF (YOUT-YOLDV(JY+1)) 1096,1094,1094
1094 CONTINUE
1096 LYFAF=JY
RATY=(YOUT-YOLDV(JY))/(YOLDV(JY+1)-YOLDV(JY))
CALL SFVFL(0.0,VALUE,80)
C
C INITIALIZE FOR NEXT INTEGRATION STEP
C
110 CALL DATSW(0,ISW)
GO TO (111,114),ISW
111 WRITE (NOUT,2010)
MM=MPTS
EPSXV(2)=DXX
LPRFL=LSTFL

```

```

      X=XP
      NPTS=NPTSN
      GO TO 300
114   DXI=2.0/DXX
      FMAXV(7)=0.0
      TMAXV(7)=0.0
      DUI=0.0
      DLI=0.0
      MPTS=MPTS+1
      CALL WAKPZ

C
C   DETERMINE NEW DXX FOR PRESSURE SOLUTION
C
      DXXO=DXX
      IF (MPTS-NSTPR) 127,170,170
127   DXX=DXX*PN(MPTS)/PN(MPTS+1)
C
C   SUCCESSFUL INTEGRATION STEP
C
170   ERROR=SQRT(DUI/DLI)/DXXO
      WRITE (NOUT,1000) MPTS,FMAXV(7),TMAXV(7),DXXO,ERROR
      IF (MPTS-1) 172,172,171
171   IF (TMAXV(7)-TEM) 172,172,180
172   TEM=TMAXV(7)
      IF (MPTS-NSTPR) 175,180,180
175   IF (TMAXV(7)/FMAXV(7)-PCRIT) 180,180,110
180   IF (LFOLF) 210,290,210
210   NRSTX=NRST+LZLFF
      NREND=NRST+JEND-1
      DO 230 NR=NRSTX,NKEND
      IF (ZOUT-ZOLDV(NR)) 265,240,220
220   IF (ZOUT-ZOLDV(NR+1)) 240,230,230
230   CONTINUE
240   RATZ=(ZOUT-ZOLDV(NR))/(ZOLDV(NR+1)-ZOLDV(NR))
      NPOS=NR
      CALL WAKRR(NR,ZV)
      CALL WAKRR(NR+1,ZPV)
      IYPSX=IYPS+LYLFF
      DO 260 JY=IYPSX,IYPE
      CALL WAKMP(IROWT,NR,JY,XV,1)
      CALL WAKMP(IROWT,NR+1,JY,XPYV,1)
      TOTAL(7,JY,1)=XV(6)+RATZ*(XPYV(6)-XV(6))
260   CONTINUE
265   IF (LYFAF) 290,290,270
270   DO 280 NR=NRSTX,NKEND
      TOTAL(7,NR,2)=VALUE(NR,1)+RATY*(VALUE(NR,2)-VALUE(NR,1))
280   CONTINUE
290   GMAXV(7)=FMAXV(7)
300   CALL SFVMV(XPPV,ZERUV,NWVEC)
310   RETURN
      END
CART ID 0105  DB ADDR 5A00  DB CNT 000A

```

```

WAKPI,S(0105)
**WAKPI - STRATIFIED SUBMARINE WAKE, PROFILE INITIALIZATION
SUBROUTINE WAKPI
C
C THIS SUBROUTINE IN THE WAKE PROGRAM INITIALIZES
C THE WORKING FILE WITH
C
C 1) KNOWN JET PLOT FILE RESULTS FOR AXISYMMETRIC FLOW
C
C 2) KNOWN STRATIFIED WAKE PLOT FILE RESULTS FOR SPECIAL RESTART
C
C 3) GIVEN PRESSURE DISTRIBUTIONS FOR POISSONS EQUATION
C
C DIMENSION FILID(3),RBUF(6,40),RR(16),JTOP(2)
*COPY (CMWAK)
EQUIVALENCE (RBUF(1,1),ROWG(1,1)),(AV(1),FILID(1))
EQUIVALENCE (JTOP(2),ZNEWV(2)),(RR(1),GM(1))
C
1000 FORMAT(/24H IMPROPER INITIALIZATION,4I5)
C
IOLAY=4
CALL SFVFL(0.0,GMAXV,NVART)
MOOD=-1
IF (LYFAF) 210,200,50
C
C FIND APPROPRIATE JET PROFILES TO INITIALIZE NSTAT = 1
C
50 NR=2
NVARI=3
100 NP=NR-1
CALL PBFDR(FILID,NP,LZFAF,ZNEWV)
ITOP=JTOP(1)
NR=NP+ITOP*LYFAF
CALL PBFDR(FILID,NR,1,XP)
IF (XP) 103,102,102
102 IF (XP-X) 100,100,103
103 NR=1
X=ZNEWV(1)
CALL SFVFL(0.0,XV,NVAR)
XV(6)=SCALE
IBOT=MMIN(MXRZY/(LYLFF+2),MXRZ/(LZLFF+2))
NSK=ITOP/IBOT+1
JO=0
NY=0
DO 120 J=1,ITOP,NSK
NY=NY+1
NP=NP+(J-JO-1)*LYFAF
JO=J
CALL PBFDR(FILID,NP,LYFAF,RR)
RBUF(1,NY)=RR(5)+RR(6)+RR(7)
RBUF(2,NY)=0.0
RBUF(3,NY)=RR(3)
RBUF(4,NY)=RR(1)
DO 115 I=1,NVARI
TEM=ABS(RBUF(I,NY))
IF (TEM-GMAXV(1)) 115,115,114
114 GMAXV(I)=TEM
115 CONTINUE
IF (J-ITOP) 116,120,120

```

```

116 IF (J+NSK-ITOP) 120,120,118
118 J=ITOP-NSK
120 CONTINUE
    CALL WAKSE(EPSS,EPSSV)
122 CALL SFVFL(0.0,RBUF(1,NY),NVARI)
    DO 125 I=1,NVARI
    IF (ABS(RBUF(I,NY-1))-EPSSV(I)) 125,125,126
125 CONTINUE
    NY=NY-1
    GO TO 122
126 IF (LZLFF) 1262,1264,1264
1262 NRST=2
    NRSTX=1
    JEND=NY-2
    GO TO 1266
1264 NRST=(MXRZ+1)/2-NY+2
    NRSTX=MXRZ/2
    JEND=NY+NY-3
1266 IF (LYLFF) 1268,1270,1270
1268 NYPS=2
    NYPSX=1
    NYPE=NY-1
    GO TO 127
1270 NYPS=(MXRY+1)/2-NY+2
    NYPSX=MXRY/2
    NYPE=NYPS+NY+NY-4
127 IF (JEND) 129,129,1275
1275 IF (NRST-2) 129,128,128
128 IF (NYPS-NYPE) 1285,129,129
1285 IF (NYPS-2) 129,130,130
129 WRITE (NOUT,1000) NYPS,NYPE,NRST,JEND
    CALL EXIT
C
C CONSTRUCT AXISYMMETRIC WORKING FILE
C
130 DO 180 JZ=1,NY
    NR=NRSTX+JZ-1
    NPOS=NR
    Z=RBUF(4,JZ)
    IF (JZ-NY) 132,131,131
131 IYPS=0
    IYPE=0
    GO TO 170
132 J=JZ
    IYPS=NYPSX-LYLFF
    DO 160 JY=1,NY
    J=J-1
    NRY=NYPSX+JY-1
    Y=RBUF(4,JY)
    IF (JZ-1) 133,133,133
133 YOLDV(NRY)=Y
    IF (LYLFF) 135,134,134
134 IY=NYPSX-JY+1
    YOLDV(IY)=-Y
135 R=SQR(Y*Y+Z*Z)
140 J=J+1
    IF (JY-NY) 141,165,165
141 IF (R-RBUF(4,J+1)) 142,142,140
142 RATR=(R-RBUF(4,J))/(RBUF(4,J+1)-RBUF(4,J))

```



```
CALL SFVMV(RBUF(1,J),XZMV,NVARI)
CALL SFVMV(RBUF(1,J+1),XZPV,NVARI)
IVAR=0
DO 146 I=1,NVARI
XV(I)=XZMV(I)+RATR*(XZPV(I)-XZMV(I))
IF (ABS(XV(I))-EPSSV(I)) 145,145,146
145 IVAR=IVAR+1
146 CONTINUE
IF (IVAR-NVARI) 150,165,165
150 CALL WAKMP(IROWR,NR,NRY,XV,2)
IF (LYLFF) 160,151,151
151 IF (JY-1) 160,160,152
152 IY=NYP SX-JY+1
CALL WAKMP(IROWR,NR,IY,XV,2)
IYPS=IYPS-1
160 CONTINUE
165 IYPE=NRY-1
170 CALL WAKWR(NR,ZV)
IF (LZLFF) 180,171,171
171 IF (JZ-1) 180,180,172
172 NR=NRSTX-JZ+1
NPOS=NR
Z=-Z
CALL WAKWR(NR,ZV)
180 CONTINUE
GO TO 250
C
C FIND APPROPRIATE SPECIAL RESTART PROFILES
C
200 CALL WAKSR(FILID)
GO TO 250
210 CALL WAKSR(PLTID)
250 NP=1
NG=1
RETURN
END
CART ID 0105 DB ADDR 3AC0 DB CNT 0132
```

WAKPM,S(0105)

**WAKPM - STRATIFIED SUBMARINE WAKE, PRESSURE MANIPULATIONS
SUBROUTINE WAKPM(LFL)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM PERFORMS VALUE MANIPULATIONS
C ON THE UPSWEEP AND DOWNSWEEP OF THE PRESSURE IMPLICIT SOLUTION
C

DIMENSION VALUE(40,2)

*COPY (CMWAK)

EQUIVALENCE (GM(10),DUI),(GM(9),DLI)

EQUIVALENCE (VALUE(1,1),ROWG(1,36))

C

SPRZ(ARGM,ARG,ARGP)=SZM*ARGM+SZ*ARG+SZP*ARGP

SPRY(ARGM,ARG,ARGP)=SYM*ARGM+SY*ARG+SYP*ARGP

C

GO TO (100,200),LFL

C

C MATRIX UPSWEEP CALCULATIONS
C

100

DZM=Z-ZM

DZP=ZP-Z

DZT=DZM+DZP

SZM=2.0/DZM/DZT

SZP=2.0/DZP/DZT

SZ=-SZM-SZP

DYM=Y-YM

DYP=YP-Y

DYT=DYM+DYP

SYM=2.0/DYM/DYT

SYP=2.0/DYP/DYT

SY=-SYM-SYP

GO TO (110,120),LZFAF

C

110

XMAT(1)=-SYM

YMAT(1)=DXI-SY

ZMAT(1)=-SYP

DVEC(1)=DXI*XV(6)+SPRZ(XMYV(6),XV(6),XPYV(6))-TV(5)

IF (JY-2) 1105,112,111

1105

TEM=FLOAT(IRFV(6,3))

GO TO 122

111

IF (JY-IYPSN) 123,123,130

112

IF (LYLFF) 130,123,123

C

120

XMAT(1)=-SZM

YMAT(1)=DXI-SZ

ZMAT(1)=-SZP

DVEC(1)=DXI*XV(6)+SPRY(XZMV(6),XV(6),XZPV(6))-TV(5)

IF (JZ-1) 1205,1215,1208

1205

TEM=FLOAT(IRFV(6,4))

GO TO 122

1208

IF (JY-IYPSM) 1209,130,121

1209

IF (JY-1) 130,130,123

121

IF (JY-IYPEM) 130,130,123

1215

IF (LZLFF) 130,123,123

C

122

ZMAT(1)=ZMAT(1)+(2.0*TEM-1.0)*XMAT(1)

123

XMAT(1)=0.0

C

130

TEM=1.0/(YMAT(1)-XMAT(1)*AV(1))

```

AV(1)=TEM*ZMAT(1)
AV(6)=TEM*(DVEC(1)-XMAT(1)*AV(6))
CALL WAKMP(IROWA,NR,JY,AV,2)
RETURN

```

```

C
C MATRIX DOWNSWEEP CALCULATIONS (WAKPY)
C

```

```

200 CALL WAKMP(IROWA,NR,JY,XV,1)
XV(6)=XV(6)-XV(1)*AV(6)
AV(6)=XV(6)
CALL WAKMP(IROWT,NR,JY,TV,1)
TEM=ABS(AV(6))
IF (TEM-FMAXV(7)) 230,230,220
220 FMAXV(7)=TEM
YMAXV(7)=YOLDV(JY)
ZMAXV(7)=ZOLDV(NR)
230 TEM=ABS(AV(6)-TV(6))
Y=YOLDV(JY)
Z=ZOLDV(NR)
DY=YOLDV(JY+1)-Y
IF (JY-1) 233,233,232
232 DY=DY+Y-YOLDV(JY-1)
233 DZ=ZOLDV(NR+1)-Z
IF (NR-1) 235,235,234
234 DZ=DZ+Z-ZOLDV(NR-1)
235 DUI=DUI+TEM*TEM*DY*DZ
DLI=DLI+TV(5)*TV(5)*DY*DZ
IF (TEM-TMAXV(7)) 250,250,240
240 TMAXV(7)=TEM
250 TV(6)=AV(6)
CALL WAKMP(IROWT,NR,JY,TV,2)
IF (LYFAF) 260,260,252
252 IF (JY-LYFAF) 260,254,256
254 VALUE(NR,1)=TV(6)
RETURN
256 IF (JY-LYFAF+1) 260,258,260
258 VALUE(NR,2)=TV(6)
260 RETURN
END

```

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CAKT 1D 0105 DB ADDR 4240 DB CNT 00C2

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A-60

WAKPP.S(0105)

**WAKPP - STRATIFIED SUBMARINE WAKE, PRINTER PLOTTER ROUTINE
SUBROUTINE WAKPP

C
C THIS SUBROUTINE IN THE WAKE PROGRAM SCANS THE WORKING FILE
C AND CONSTRUCTS A POINT PLOT FOR THE PRINTER

C
C DIMENSION II(21),JVEC(101)
C DIMENSION XVEC(40),JVCHV(7),JSCAL(101)
*COPY (CMWAK)
C EQUIVALENCE (JVEC(2),YNEWV(1)),(XVEC(1),ZNEWV(1))

C
C DATA IH/1H-/,IV/1HI/,IO/1H0/
C DATA II/1HM,1HM,1M ,1H8,1H ,1H6,1H ,1H4,1H ,1H2,1H ,1H1,1H .
1 1H3,1H ,1H5,1H ,1H7,1H ,1HP,1HP/
C DATA JVCHV/2HQ0,2HRO,2HU ,2HV ,2HW ,2HSL,2HP /

C
1005 FORMAT(1H1)
1010 FORMAT(18H PRINTER PLOT FOR ,A2,5X,11HX POINTS = ,I3,5X,4HX = ,
1 E11.5,5X,16HABS MAX VALUE = ,E11.5,5X,13HEDGE VALUE = ,E12.5)
1020 FORMAT(20X,101A1)
1040 FORMAT(12H0PERCENT MAX,3X,6H90/100,5X,5H70/80,5X,5H50/60,5X,
1 5H30/40,5X,5H10/20,5X,4H1/-1,5X,7H-10/-20,3X,7H-30/-40,3X,
2 7H-50/-60,3X,7H-70/-80,2X,8H-90/-100/12H NOTATION ,5X,1HP,
3 10X,1H7,9X,1H5,9X,1H3,9X,1H1,8X,1H0,10X,1H2,9X,1H4,9X,1H6,9X,
4 1H8,8X,1HM/)
1050 FORMAT(E18.5,1X,103A1)
1060 FORMAT(19X,103A1)
1070 FORMAT(6X,6E20.5)
1080 FORMAT(5X,1HZ,13X,103A1)
1090 FORMAT(/70X,1HY)

C
C INITIALIZE PLOT VALUES

C
C IOLAY=9
C IF (LPRFL) 10,350,350
10 IF (LTOLF) 15,20,15
15 IF (LOUT) 20,50,30
20 CALL DATSW(7,ISW)
GO TO (50,350),ISW
30 CALL DATSW(3,ISW)
GO TO (50,40),ISW
40 LTOLF=0
50 MOOD=1
NY=101
NZ=51
NYPSX=NYPS-1
NYPEX=NYPE+1
NRSTX=NRST-1
NREND=NRST+JEND

C
C SET UP AXES AND NOTATION

C
C YMIN=YOLDV(NYPSX)
C YMAX=YOLDV(NYPEX)
C ZMIN=ZOLDV(NRSTX)
C ZMAX=ZOLDV(NREND)
C DY=(YMAX-YMIN)/FLOAT(NY-1)
C DZ=(ZMAX-ZMIN)/FLOAT(NZ-1)

```

DO 80 I=1,6
YMAT(I)=YMIN+20.0*FLOAT(I-1)*DY
ZMAT(I)=ZMIN+10.0*FLOAT(I-1)*DZ
80 CONTINUE
K=19
DO 90 I=1,NY
K=K+1
IF (K-20) 84,82,82
82 K=0
JSCAL(I)=IV
GO TO 90
84 JSCAL(I)=IH
90 CONTINUE
C
C LOOP THROUGH FILE FOR EACH VARIABLE
C
IKOWR=2
IF (LBUF) 92,94,92
92 IKOWR=4
94 WRITE (NOUT,1005)
DO 300 IVAR=1,NVART
FMAX=FMAXV(IVAR)
FMIN=1.0E-04*FMAX
IF (FMAX) 300,300,100
100 JVAR=IVAR
IF (IVAR-NVART) 102,101,101
101 JVAR=6
IROWR=IROWT
102 WRITE (NOUT,1010) JVCHV(IVAR),NPTSN,XP,FMAX,ZEROV(IVAR)
WRITE (NOUT,1040)
WRITE (NOUT,1020) JSCAL
KS=9
IS=7
NS=NZ/2+1
NR=NREND-1
NPOS=NR
CALL WAKRR(NR+1,ZPV)
NPOS=NR+1
CALL WAKRR(NR,ZMV)
C
C LOCATE EVERY DESIRED Z VALUE
C
DO 250 IZ=1,NZ
JZ=NZ-IZ+1
Z=ZMIN+FLOAT(JZ-1)*DZ
105 IF (Z-ZP) 107,110,106
106 Z=ZP
GO TO 110
107 IF (Z-ZM) 108,110,110
108 IF (NR-NRSTX) 1095,1095,109
109 NR=NR-1
CALL WAKMR(1,3)
CALL SFVMV(ZM,ZP,NWWZF)
NPOS=NR+1
CALL WAKRR(NR,ZMV)
GO TO 105
1095 Z=ZM
C
C INTERPOLATE FOR PARAMETER VALUES

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```

C
110  RATZ=(Z-ZM)/(ZP-ZM)
      DO 115 JY=NYPSX,NYPEX
      CALL WAKMP(IROWR,NR,JY,XMYV,1)
      CALL WAKMP(IROWR,NR+2,JY,XPYV,1)
      XVEC(JY)=XMYV(JVAR)+RATZ*(XPYV(JVAR)-XMYV(JVAR))
115  CONTINUE
C
C EXPAND TO FILL PLOT ARRAY
C
      K=NYPSX
      DO 160 JY=1,NY
      Y=YMIN+FLOAT(JY-1)*UY
116  IF (Y-YOLDV(K)) 119,120,117
117  IF (Y-YOLDV(K+1)) 120,120,118
118  K=K+1
      IF (K-NYPEX) 116,119,119
119  TEM=XVEC(K)
      GO TO 121
120  RATY=(Y-YOLDV(K))/(YOLDV(K+1)-YOLDV(K))
      TEM=XVEC(K)+RATY*(XVEC(K+1)-XVEC(K))
C
C CHECK AND INSERT POINT VALUES
C
121  I=IFIX(10.0*TEM/FMAX)
      JVEC(JY)=II(I+11)
      IF (I) 160,122,160
122  I=IFIX(100.0*TEM/FMAX)
      IF (I) 160,124,160
124  IF (ABS(TEM)-FMIN) 160,126,126
126  JVEC(JY)=I0
160  CONTINUE
C
C PRINT TO PRINTER
C
      KS=KS+1
      IF (KS-10) 204,202,202
202  KS=0
      IS=IS-1
      WRITE (NOUT,1050) ZMAT(IS),IH,JVEC,IH
      GO TO 250
204  IF (JZ-NS) 208,206,208
206  WRITE (NOUT,1080) IV,JVEC,IV
      GO TO 250
208  WRITE (NOUT,1060) IV,JVEC,IV
250  CONTINUE
      WRITE (NOUT,1020) JSCAL
      WRITE (NOUT,1070) (YMAT(I),I=1,6)
      WRITE (NOUT,1090)
300  CONTINUE
350  RETURN
      END
CART ID 0105 DB ADDR 48C0 DB CNT 0152

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WAKPY.S(0105)
**WAKPY - STRATIFIED SUBMARINE WAKE, PRESSURE STEP IN Y
  SUBROUTINE WAKPY
C
C THIS SUBROUTINE IN THE WAKE PROGRAM MAKES A STEP OF DELTA XX/2
C WITH 2 DERIVATIVES EVALUATED AT THE PRESENT XX POINT
C
*COPY (CMWAK)
C
C INITIALIZE COMPUTATION
C
  IYPSN=IYPS
  IYPEN=IYPE
C
C INITIALIZE FOR THE Y DIRECTION AND SWEEP
C
  Y=YOLDV(IYPSN-1)
  YP=YOLDV(IYPSN)
  CALL WAKMP(IROWR,NR+1,IYPSN-1,XPYV,1)
  CALL WAKMP(IROWR,NR,IYPSN-1,XV,1)
  CALL WAKMP(IROWT,NR,IYPSN-1,TV,1)
  IF (JZ) 1081,1081,1082
1081 CALL WAKRF(XPYV,XMYV,4)
  GO TO 1083
1082 CALL WAKMP(IROWR,NR-1,IYPSN-1,XMYV,1)
1083 CALL WAKMP(IROWR,NR,IYPSN,XZPV,1)
  JY=IYPSN-1
  IF (LYLFF) 109,110,110
109 CALL WAKRF(XZPV,XZMV,3)
  YM=Y+Y-YP
  GO TO 120
C
C UPWARD PASS
C
110 JY=JY+1
  CALL SFVMV(XV,XZMV,NMOVE)
  CALL WAKMP(IROWT,NR,JY,TV,1)
  YM=Y
  Y=YP
  YP=YOLDV(JY+1)
  CALL WAKMP(IROWR,NR+1,JY,XPYV,1)
  IF (JZ) 116,116,118
116 CALL WAKRF(XPYV,XMYV,4)
  GO TO 119
118 CALL WAKMP(IROWR,NR-1,JY,XMYV,1)
119 CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
C
C CALCULATE MATRIX COEFFICIENTS AND INVERT FOR GAMMA AND AV
C
120 CALL WAKPM(1)
  IF (JY-IYPEN) 110,125,125
C
C UPPER BOUNDARY CONDITION
C
125 TV(6)=AV(6)
  CALL WAKMP(IROWT,NR,JY,TV,2)
C
C INITIALIZE FOR DOWNWARD PASS
C

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```
IYPEN=JY
IYPEX=IYPEN-1
IYPSX=IYPSN+LYLFF
IF (IYPSX-IYPEN) 150,156,156
150 DO 151 IY=IYPSX,IYPEX
    JY=IYPEX+IYPSX-IY
    CALL WAKPM(2)
151 CONTINUE
C
C ROW SWEEP COMPLETED
C
156 IYPS=IYPSN
    IYPE=IYPEN
    CALL WAKWR(NR,ZV)
    RETURN
    END
CART ID 0105 DB ADDR 3230 DB CNT 0094
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WAKPZ.S(0105)
**WAKPZ - STRATIFIED SUBMARINE WAKE, PRESSURE STEP IN Z
  SUBROUTINE WAKPZ
C
C THIS SUBROUTINE IN THE WAKE PROGRAM MAKES A STEP OF DELTA XX/2
C WITH Y DERIVATIVES EVALUATED AT THE PRESENT XX POINT
C
*COPY (CMWAK)
C
C INITIALIZE COMPUTATION
C
      LZFAF=2
      IROWR=1
      IROWA=3
      NRSTN=NRST
      JENDN=JEND
      NR=NRSTN-1
      NPOS=NR
      CALL WAKRR(NR,ZV)
      CALL WAKRR(NR+1,ZPV)
      JZ=0
      IF (LZLFF) 101,1015,1015
101  ZM=Z+Z-ZP
      IYPEM=IYPEP
      IYPSM=IYPS
      GO TO 110
1015 NR=NRSTN
102  JZ=JZ+1
      NPOS=NR
      CALL SFVMV(Z,ZM,NWWZF)
      CALL WAKMR(2,1)
      CALL SFVMV(ZP,Z,NWWZF)
      CALL WAKMR(3,2)
      CALL WAKRR(NR+1,ZPV)
C
C INITIALIZE FOR THE Y DIRECTION AND SWEEP
C
110  Y=YOLDV(IYPS-1)
      YP=YOLDV(IYPS)
      CALL WAKMP(IROWR,NR+1,IYPS-1,XPYV,1)
      CALL WAKMP(IROWR,NR,IYPS-1,XV,1)
      CALL WAKMP(IROWT,NR,IYPS-1,TV,1)
      IF (JZ) 111,111,1115
111  CALL WAKRF(XPYV,XMYV,4)
      GO TO 112
1115 CALL WAKMP(IROWR,NR-1,IYPS-1,XMYV,1)
112  IYPSX=IYPS+LYLFF
      IF (JZ) 1126,1126,1125
1125 CALL WAKMP(IROWA,NR-1,IYPS-1,AV,1)
1126 CALL WAKMP(IROWR,NR,IYPS,XZPV,1)
      DO 145 JY=IYPSX,IYPE
      IF (JY-IYPS) 114,1142,1142
114  CALL WAKRF(XZPV,XZMV,3)
      YM=Y+Y-YP
      GO TO 120
1142 IF (JZ) 1145,1145,1144
1144 CALL WAKMP(IROWA,NR-1,JY,AV,1)
1145 CALL SFVMV(XV,XZMV,NMOVE)
      CALL WAKMP(IROWT,NR,JY,TV,1)

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      YM=Y
      Y=YP
      YP=YOLDV(JY+1)
      CALL WAKMP(IROWR,NR+1,JY,XPYV,1)
      IF (JZ) 1148,1148,1149
1148  CALL WAKRF(XPYV,XMYV,4)
      GO TO 119
1149  CALL WAKMP(IROWR,NR-1,JY,XMYV,1)
119   CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
C
C   CALCULATE MATRIX COEFFICIENTS AND INVERT FOR GAMMA AND AV
C
120  CALL WAKPM(1)
145  CONTINUE
      IF (JZ-JENDN+1) 146,147,147
146  CALL WAKWR(NR,ZV)
147  NR=NR+1
      IF (JZ-JENDN) 102,150,150
C
C   INITIALIZE FOR DOWNWARD PASS
C
150  NR=NR-1
      JENDN=JZ
      IZEND=JENDN-LZLFF-1
      LZFAF=1
      IROWR=3
      IROWA=4
      DO 154 IZ=1,IZEND
      IYEND=IYPE-IYPS-LYLFF+1
      DO 1508 IY=1,IYEND
      JY=IYPE-IY+1
      IF (JY-IYPEM) 1502,1502,1508
1502  IF (JY-IYPSM) 1503,1506,1506
1503  IF (IYPSM-2) 1506,1506,1508
1506  CALL WAKMP(IROWR,NR,JY,AV,1)
      CALL WAKMP(IROWR,NR-1,JY,XV,1)
      XV(6)=XV(6)-XV(1)*AV(6)
      CALL WAKMP(IROWR,NR-1,JY,XV,2)
1508  CONTINUE
C
C   ROW SWEEP COMPLETED
C
      CALL WAKPY
      NR=NR-1
      NPOS=NR
      JZ=JZ-1
      CALL SFVMV(Z,ZP,NWWZF)
      CALL WAKMR(2,3)
      CALL SFVMV(ZM,Z,NWWZF)
      CALL WAKMR(1,2)
      IF (IZ-IZEND) 153,152,152
152  IF (LZLFF) 154,153,153
153  CALL WAKRR(NR-1,ZMV)
154  CONTINUE
      IF (JZ) 156,156,158
156  ZM=Z+Z-ZP
      IYPEM=IYPEP
      IYPSM=IYPS
158  CALL WAKPY

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JEND=JENDN
NRST=NRSTN
RETURN
END

CART ID 0105 DB ADDR 3130 DB CNT 00F2

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WAKRF,S(0105)
**WAKRF - STRATIFIED SUBMARINE WAKE, REFLECT A POINT
  SUBROUTINE WAKRF(TEMA,TEMB,LFL)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM PROVIDES REFLECTION
C
  DIMENSION TEMA(6),TEMB(6)
*COPY (CMWAK)
C
  CALL SFVMV(TEMA,TEMB,NWVEC)
  DO 100 I=1,NWVEC
  IF (IRFV(I,LFL)) 100,50,100
50  TEMB(I)=-TEMB(I)
  GO TO (60,60,100,100),LFL
60  TEMB(I)=TEMB(I)+2.0*ZEROV(I)
100 CONTINUE
  RETURN
  END
CART ID 0105 DB ADDR 4A20 DB CNT 0022
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WAKRR,S(0105)
**WAKRR - STRATIFIED SUBMARINE WAKE, READ A Z BUFFER ROW
SUBROUTINE WAKR (NRX,ZPOS)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM READS A Z ROW AND
C FILLS THE ROW BUFFER AT THE NRX POSITION FOR ALL Y
C
C DIMENSION ZPOS(2),RECB(24)
*COPY (CMWAK)
EQUIVALENCE (RECB(1),DVEC(1))
C
DATA JERRX/2HRR/
C
C FILL ZPOS WITH IYPS AND IYPE VALUES
C
IF (NRX) 300,300,10
10 IF (NRX-MXRZ) 20,20,300
20 ZA=ZOLDV(NRX)
IVECA=IYPSV(NRX)
IVECB=IYPEV(NRX)
CALL SFVMV(ZA,ZPOS,NWWZF)
C
C LOCATE NRX POSITION IN ROW BUFFER ARRAY
C
J=NRX-NPOS+2
IF (J) 300,300,30
30 IF (J-3) 40,40,300
40 IF (IVECA) 45,45,50
45 IYPSX=1
GO TO 140
50 IYPSX=IVECA+LYLFF
IF (IYPSX-1) 90,90,60
60 IYPEX=IYPSX-1
C
C FILL BUFFER ROW WITH LEADING ZEROS
C
DO 80 I=1,IYPEX
CALL SFVFL(0.0,ROWB(1,I,J),NWVEC)
CALL SFVMV(ZEKOV,KOWB(7,I,J),NWVEC)
CALL SFVMV(ZEKOV,KOWB(13,I,J),NWVEC)
80 CONTINUE
90 IYPEX=IVECB
C
C FILL BUFFER ROW WITH NRX INFORMATION
C
NRXX=(NRX-1)*MXRY+IYPSX
DO 130 I=IYPSX,IYPEX
CALL PBFDR(SLNID,NRXX,NWR,RECB)
CALL SFVMV(RECB(1),KOWB(1,I,J),NWVEC)
IF (MOOU) 105,110,115
105 CALL SFVMV(RECB(7),KOWB(7,I,J),NMOVE)
GO TO 130
110 CALL SFVMV(RECB(13),KOWB(7,I,J),NMOVE)
GO TO 130
115 CALL SFVMV(RECB(7),KOWB(7,I,J),NWVEC)
CALL SFVMV(RECB(19),KOWB(13,I,J),NWVEC)
130 CONTINUE
IYPSX=IYPEX+1
IF (IYPSX-MXRY) 140,140,160

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C  
C FILL BUFFER ROW WITH TRAILING ZEROES  
C  
140 DO 150 I=IYPSX,MXRY  
      CALL SFVFL(0.0,ROWB(1,I,J),NWVEC)  
      CALL SFVMV(ZEROV,ROWB(7,I,J),NWVEC)  
      CALL SFVMV(ZEROV,ROWB(13,I,J),NWVEC)  
150 CONTINUE  
160 RETURN  
300 JERR=JERRX  
      RETURN  
      END  
CART ID 0105 DB ADDR 4A50 DB CNT 008C
```

WAKSC.S(0105)
 **WAKSC - STRATIFIED SUBMARINE WAKE, SUPEREQUILIBRIUM CALCULATIONS
 SUBROUTINE WAKSC

C THIS SUBROUTINE IN THE WAKE PROGRAM COMPUTES THE AUXILIARY
 C TURBULENCE VIA SUPEREQUILIBRIUM THEORY

C 1) FOR THE RIGHT HAND SIDE OF POISSONS EQUATION

C 2) FOR DU/DY, DU/DZ, DRHO/DY AND DRHO/DZ

C 3) FOR TURBULENCE OUTPUT TO THE LINE PRINTER

C DIMENSION TURB(10),TOTAL(560)

*COPY (CMWAK)
 EQUIVALENCE (TURB(1),YMAT(1)),(DIVT,GM(11))
 EQUIVALENCE (FF,GM(13)),(FT,GM(14))

C 1000 FORMAT(//36H SUPEREQUILIBRIUM ERROR HAS OCCURRED,2I5,3E15.5)

1001 FORMAT(//42H SUPEREQUILIBRIUM CORRECTION TO ZERO NOISE,I4,
 1 14H TIMES AT STEP,I4)

1002 FORMAT(//16X,7HTURB KE,8X,7HMEAN KE,8X,7HRHO*RHO,6X,
 1 11HRHO*RHO OUT,4X,11HMEAN KE OUT,8X,4HAREA,
 2 9X,7HPSI MAX,6X,11HDISSIPATION/10X,8E15.5)

1003 FORMAT(1H0,15X,7HF TOTAL,9X,5HF MAX,8X,8HF CHANGE,7X,
 1 10HDIVG ERROR,7X,4HLIFT/10X,5E15.5)

1004 FORMAT(//37H TURBULENCE CORRECTION FOR MAX BOUNDS,2I5,
 1 8H AT STEP,I4)

C FPRZ(ARGM,ARG,ARGP)=FZM*(ARGM+FZS*ARG-FZR*ARGP)
 FPRY(ARGM,ARG,ARGP)=FYM*(ARGM+FYS*ARG-FYR*ARGP)
 SPRZ(ARGM,ARG,ARGP)=SZM*ARGM+SZ*ARG+SZP*ARGP
 SPRY(ARGM,ARG,ARGP)=SYM*ARGM+SY*ARG+SYP*ARGP

C ZERO PERTINENT VARIABLES

C IOLAY=7
 IF (LSTFL) 300,50,50
 50 MOOD=1
 LFL=0
 LVV=0
 LWW=0
 LZFAF=0
 PLANE=1.0/FLOAT(LYLFF+2)/FLOAT(LZLFF+2)
 DEPSN=0.0
 AREA=0.0
 DIVT=0.0
 CVS=0.0
 XFI=0.0
 FF=0.0
 FT=0.0
 CALL SFVFL(0.0,TURBX,10)
 CALL SFVMV(ROWG,TOTAL,560)
 SCMX=4.0*YSCAL*YSCAL*ZSCAL/(YSCAL*YSCAL+ZSCAL*ZSCAL)
 ZEROV(6)=SCMX
 FMAXV(6)=SCMX

C INITIALIZE FOR PASSING THROUGH PROFILE

C

```

      IROWA=2
      IROWR=4
      IF (LSTFL) 96,96,95
95     IROWR=2
96     NRSTX=NRST+LZLFF
      NREND=NRST+JEND-1
      NPOS=NRST-1
      CALL WAKRR(NRST-1,ZV)
      CALL WAKRR(NRST,ZPV)
      DO 250 NR=NRSTX,NREND
C
C   READ THREE SURROUNDING ROWS AND TEST FOR SELECTED Z IN DOMAIN
C
      IF (NR-NRST) 104,103,103
103    NPOS=NR
      CALL SFVMV(Z,ZM,NWWZF)
      CALL WAKMR(2,1)
      CALL SFVMV(ZP,Z,NWWZF)
      CALL WAKMR(3,2)
      CALL WAKRR(NR+1,ZPV)
      GO TO 105
104    ZM=Z+Z-ZP
105    DZM=Z-ZM
      DZP=ZP-Z
      DZT=ZP-ZM
      CALL WAKDG(Z)
C
C   STEP THROUGH ALL Y POINTS COMPUTING AUXILIARY QUANTITIES
C
      Y=YOLDV(IYPS-1)
      YP=YOLDV(IYPS)
      CALL WAKMP(IROWR,NR+1,IYPS-1,XPYV,1)
      CALL WAKMP(IROWR,NR,IYPS-1,XV,1)
      IF (NR-NRST) 108,109,109
108    CALL WAKRF(XPYV,XMYV,2)
      GO TO 110
109    CALL WAKMP(IROWR,NR-1,IYPS-1,XMYV,1)
110    IYPSX=IYPS+LYLFF
      CALL WAKMP(IROWT,NR,IYPS-1,TV,1)
      CALL WAKMP(IROWR,NR+1,IYPS,XPPV,1)
      CALL WAKMP(IROWR,NR,IYPS,XZPV,1)
      IF (NR-NRST) 113,114,114
113    CALL WAKRF(XPPV,XMPV,2)
      GO TO 115
114    CALL WAKMP(IROWR,NR-1,IYPS,XMPV,1)
115    DO 200 JY=IYPSX,IYPE
      IF (JY-IYPS) 116,117,117
116    CALL WAKRF(XPPV,XPMV,1)
      CALL WAKRF(XZPV,XZMV,1)
      CALL WAKRF(XMPV,XMMV,1)
      YM=Y+Y-YP
      GO TO 130
117    CALL WAKMP(IROWT,NR,JY,TV,1)
      CALL SFVMV(XPYV,XPMV,NMOVE)
      CALL SFVMV(XV,XZMV,NMOVE)
      CALL SFVMV(XMYV,XPMV,NMOVE)
      YM=Y
      Y=YP
      YP=YOLDV(JY+1)

```



```

CALL WAKMP(IROWR,NR+1,JY+1,XPPV,1)
CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
IF (NR=NRST) 125,128,128
125 CALL WAKRF(XPPV,XMPV,2)
GO TO 130
128 CALL WAKMP(IROWR,NR-1,JY+1,XMPV,1)
130 DYM=Y-YM
UYP=YP-Y
DYT=YP-YM

C
C COMPUTE SPACING FACTORS
C
FZM=-DZP/DZM/DZT
FZP=DZM/DZP/DZT
FZ=-FZM-FZP
TEM=DZM/DZP
FZR=TEM*TEM
FZS=FZR-1.0
SZM=2.0/DZM/DZT
SZP=2.0/DZP/DZT
SZ=-SZM-SZP

C
FYM=-DYP/DYM/DYT
FYP=DYM/DYP/DYT
FY=-FYM-FYP
TEM=DYM/DYP
FYK=TEM*TEM
FYS=FYK-1.0
SYM=2.0/DYM/DYT
SYP=2.0/DYP/DYT
SY=-SYM-SYP

C
C CHECK APPROPRIATE DENOMINATOR VALUES
C
IF (XV(1)) 135,141,141
135 XV(1)=0.0
LFL=LFL+1
141 Q=SQRT(XV(1))
FRZ=FPRZ(XMYV(2),XV(2),XPYV(2))
FTEM=FRZ+URDZ
CALL WAKCL(XV,FTEM)
IF (XV(6)-SCALM) 1410,1411,1411
1410 XV(6)=SCALM
1411 IF (XV(6)-SCMX) 1420,1420,1412
1412 XV(6)=SCMX
1420 IF (LAMIN) 142,143,142
142 Q=0.0
GO TO 150
143 BQL=BBETA*Q/SCALE
C1=A*BQL*Q/SCALE-G*FTEM
C2=BBS*G*FTEM-C1
IF (C1*C2) 150,144,150
144 IF (Q) 145,150,145
145 WRITE (NOUT,1000) NR,JY,XV(1),C1,C2
LTRNF=1
RETURN

C
C COMPUTE DERIVATIVES AND RIGHT HAND SIDE
C

```

```

150  FRY=FPRY(XZMV(2),XV(2),XZPV(2))
      FUZ=FPRZ(XMYV(3),XV(3),XPYV(3))
      FUY=FPRY(XZMV(3),XV(3),XZPV(3))
      TV(1)=FUY
      TV(2)=FUZ
      TV(3)=FRY
      TV(4)=FRZ
      IF (Q) 153,153,152
152  TEM=FUY*FUY*SCALE/Q/BQL-BBETA*G*FTEM/C2
      1 -FUZ*FUZ*BBETA*(G*FTEM*(1.0-A/B/S)+A*A*XV(1)/SCALE/SCALE)/C1/C2
      CTEM=CVV+(B-CVV*TEM)/(HBETA+TEM)
      CALL WAKTC(CTEM,1.0,LVV)
153  IF (NSTAT-1) 1540,1535,1540
1535 TV(5)=0.0
      TV(6)=0.0
      FVZ=0.0
      FWY=0.0
      GO TO 160
1540 TEMF=TV(5)
      CALL WAKLL(TEMK,2)
      IF (Q) 154,154,155
154  CTEM=0.0
      TEM=0.0
      TEMC=0.0
      GO TO 156
155  C3=CTEM*(DROZ+G*BBS*FRY*FRY/C1)
      TEM=2.0*CTEM*G*FRY*FPRZ(FPRY(XMMV(1),XMYV(1),XMPV(1)),
      1 FPRY(XZMV(1),XV(1),XZPV(1)),FPRY(XPMV(1),XPYV(1),XPPV(1)))/C1
      TEMC=CTEM-2.0*G*(C3+CTEM*FRZ)/C2
      CALL WAKTC(TEMC,1.0-CTEM,LWW)
      TEMC=TEMC*SPRZ(XMYV(1),XV(1),XPYV(1))
156  FVY=FPRY(XZMV(4),XV(4),XZPV(4))
      FVZ=FPRZ(XMYV(4),XV(4),XPYV(4))
      FWY=FPRY(XZMV(5),XV(5),XZPV(5))
      FWZ=FPRZ(XMYV(5),XV(5),XPYV(5))
      TEMA=2.0*FVZ*FWY
      TEMB=2.0*FVY*FWZ
      TV(5)=-TEMC-CTEM*SPRY(XZMV(1),XV(1),XZPV(1))-TEM-TEMA+TEMB-G*FRZ
      DXX=DX
      IF (DXX-DIVP*DXMAX) 157,158,158
157  DXX=DIVP*DXMAX
158  DXX=DIVF*DXX
      TV(5)=TV(5)+U*(FVY+FWZ)/DXX-TEMK
160  CALL WAKMP(IROWT,NR,JY,TV,2)
C
C  WRITE COMPLETED SOLUTION FOR NEXT INTEGRATION STEP
C
      CALL WAKMP(IROWA,NR,JY,XV,2)
C
C  COMPUTE RICHARDSON SCALE LENGTH COMPARISON
C
      IF (YOUT-YM) 170,161,1605
1605 IF (YOUT-Y) 161,170,170
161  IF (LZFAF) 170,162,170
162  IF (4.0*XV(1)-FMAXV(1)) 163,163,170
163  CWS=ABS(FTEM)
      LZ .F=1
C
C  COMPUTE SUPEREQUILIBRIUM TURBULENCE VALUES

```

```

C
170 IF (Q) 171,171,172
171 CALL SFVFL(0.0,TURB,10)
GO TO 176

C
C ORDER - UV UW VW UR VR WR RR UU VV WW
C
172 TURB(9)=CTEM*XV(1)
TURB(3)=TURB(9)*G*FKY/C1
TURB(5)=-BQL*TURB(3)/G
TURB(1)=- (TURB(9)*FUY+TURB(3)*FUZ)/BQL
TURB(6)=(BQL*(TURB(9)*FTEM+TURB(3)*FRY)
1 -TURB(5)*BBETA*G*FKY/B/S)/C2
TURB(10)=TURB(9)-2.0*G*TURB(6)/BQL
CALL WAKTC(TURB(10),XV(1)-TURB(9),I)
TURB(8)=XV(1)-TURB(9)-TURB(10)
TURB(7)=-SCALE*(TURB(5)*FRY+TURB(6)*FTEM)/Q/B/S
TURB(4)=(FTEM*(TURB(3)*FUY+TURB(10)*FUZ)
1 -BQL*(TURB(1)*FRY+TURB(5)*FUY+TURB(6)*FUZ))/C1
TURB(2)=- (G*TURB(4)+TURB(3)*FUY+TURB(10)*FUZ)/BQL
TURB(3)=TURB(3)-G*SCALE*(FWY+FWZ)/3.0
DO 174 I=1,10
IF (ABS(TURB(I))-ABS(TURBX(I))) 174,174,173
173 TURBX(I)=TURB(I)
174 CONTINUE
IF (CTEM-CVS) 176,176,175
175 CVS=CTEM
176 IF (LSOLF) 178,180,178
178 CALL WAKMP(IROWG,NR,JY,TURB,2)
C
C COMPUTATION OF INTEGRALS
C
180 SUMF=PLANE*DT*OZ1
IF (NR-NRST) 181,182,182
181 SUMF=0.5*SUMF
182 IF (JY-NYPS) 183,184,184
183 SUMF=0.5*SUMF
184 DEPSN=DEPSN+G*XV(1)*SUMF/SCALE
IF (NSTAT-1) 185,200,185
185 XFI=XFI+TV(5)*SUMF
AREA=AREA+SUMF
TEM=FVY+FWZ
DIVT=DIVT+TEM*TEM
IF (ABS(TV(5))-ABS(FF)) 187,187,186
186 FF=TV(5)
187 TEM=ABS(TV(5)-TEMF)
IF (TEM-FT) 200,200,188
188 FT=TEM
200 CONTINUE
CALL WAKWR(NR,ZV)
IF (LSOLF) 205,250,205
205 CALL WAKMG(NR,ZV,2)
250 CONTINUE
CALL SFVMV(TOTAL,ROWG,560)
C
C COMPUTE AND PRINT PERTINENT INTEGRALS
C
EPSSV(2)=SQRT(RIS*FMAXV(1)/G/CWS)/2.0
IF (LVV+LWW) 252,252,251

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251 WRITE (NOUT,1004) LVV,LWW,NPTSN
252 IF (LFL) 260,260,255
255 WRITE (NOUT,1001) LFL,NPTSN
260 DEPST=DEPST+0.5*DXSAV*(DEPSI+DEPSN)*B
    DEPSI=DEPSN
    WRITE (NOUT,1002) (GM(I),I=1,7),DEPST
    IF (NSTAT-1) 270,300,270
270 IF (FMAXV(4)*FMAXV(5)) 271,272,271
271 DIVT=DIVT*YSCAL*ZSCAL/(AREA*FMAXV(4)*FMAXV(5))
272 WRITE (NOUT,1003) XFI,FF,FI,DIVT,GM(8)
300 RETURN
    END
CANT ID 0105 DB ADDR 4AEO DB CNT 0264
```

```
WAKSE,S(0105)
**WAKSE - STRATIFIED SUBMARINE WAKE, SET EPSILON CRITERION
  SUBROUTINE WAKSE(EPS,EPVS)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM TRANSFERS EPS TO EPVS
C
  DIMENSION EPVS(5)
*COPY (CMWAK)
C
  DO 110 I=1,NVAR
    TEM=1.0E10
    VWTF=VWTFV(I)
    IF (VWTF) 108,108,100
100  VMAX=GMAXV(I)
    VSCA=VSCAV(I)
    IF (VMAX-VSCA*EPSN) 101,102,102
101  VMAX=VSCA*EPSN
102  IF (EPS) 103,104,104
103  TEM=-EPS*VSCA
    GO TO 106
104  TEM=EPS*VMAX
106  TEM=TEM/VWTF
108  EPVS(I)=TEM
110  CONTINUE
    RETURN
  END
CART ID 0105  DB ADDR 2730  DB CNT 0032
```

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WAKSR.S(0105)
**WAKSR - STRATIFIED SUBMARINE WAKE, SPECIAL RESTART PROFILES
  SUBROUTINE WAKSR(FILID)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM LOCATES A SET OF
C SPECIAL RESTART PROFILES AND INITIALIZES THE WORKING FILE
C
  DIMENSION FILID(3),RBUF(6,40),IBUF(40),IVEC(3)
*COPY (CMWAK)
  EQUIVALENCE (RBUF(1,1),ROWG(1,1)),(IBUF(2),ROWG(1,16))
C
  DATA IVEC/3,5,6/
C
1000  FORMAT(/25H IMPROPER SPECIAL RESTART,4I5)
C
C LOCATE PROPER X RECORD
C
  NR=2
  K=IVEC(LZFAP)
210  NP=NR-1
  CALL PBFDR(FILID,NP,2,ZA)
  NY=IVECA
  NZ=IVECB
  NR=NP+NY+NZ+K*NY*NZ
  CALL PBFDR(FILID,NR,1,XP)
  IF (XP) 215,212,212
212  IF (XP-X) 210,210,215
215  X=ZA
  IF (LZLFF) 2151,2152,2152
2151 NRST=2
  GO TO 2153
2152 NRST=(MXRZ-NZ)/2+2
2153 JEND=NZ-2
  IF (LYLFF) 2154,2155,2155
2154 NYPS=2
  GO TO 2156
2155 NYPS=(MXRY-NY)/2+2
2156 NYPE=NY+NYPS-3
  IF (JEND) 218,218,2160
2160 IF (NRST-2) 218,2165,2165
2165 IF (NYPS-NYPE) 2170,218,218
2170 IF (NYPS-2) 218,220,220
218  WRITE (NOUT,1000) NYPS,NYPE,NRST,JEND
  CALL EXIT
220  CALL PBFDR(FILID,NP,NY,YOLDV(NYPS-1))
  CALL PBFDR(FILID,NP,NZ,ZOLDV(NRST-1))
C
C BUILD WORKING FILE FROM SPECIAL RESTART PROFILES
C
  CALL SFVFL(0.0,TV,NWVEC)
  DO 250 JZ=1,NZ
  DO 2200 JY=1,40
  IBUF(JY)=0
  CALL SFVMV(ZEROV,RBUF(1,JY),NVAR)
  RBUF(6,JY)=ZEROV(7)
2200 CONTINUE
  DO 230 IVAR=1,NWVEC
  JVAR=IVAR
  KVAR=IVAR
```

```

GO TO (221,221,2202,2204,2204,2203),IVAR
2202 IF (NSTAT-2) 2207,230,2207
2203 KVAR=KVAR+1
2204 IF (NSTAT-1) 2206,230,2206
2206 IF (LZFAP-2) 230,2208,2208
2207 IF (LZFAP-2) 221,230,221
2208 JVAR=JVAR+LZFAP-3
221 NR=NP+(JVAR-1)*NY*NZ
DU 225 JY=1,NY,10
I=JY/10+1
J=10*(I-1)
NR1=MMIN(10,NY-J)
NRXX=NR+NR1*(JZ-1)+J*NZ
CALL PBFDR(FILID,NRXX,NRY,TURBX)
DU 224 I=1,NRY
J=J+1
RBUF(IVAR,J)=TURBX(I)
TEM=ABS(RBUF(IVAR,J))
IF (ABS(RBUF(IVAR,J))-ZEROV(KVAR))-1.0E-04) 2214,2214,2215
2214 IBUF(J)=IBUF(J)+1
2215 IF (TEM-GMAXV(KVAR)) 224,224,222
222 GMAXV(KVAR)=TEM
224 CONTINUE
225 CONTINUE
230 CONTINUE
NR=NRST+JZ-2
NPOS=NR
Z=ZOLDV(NR)
IYPS=0
IYPE=0
DO 240 NRY=1,NY
JY=NYPN+NR-2
IF (IYPS) 231,231,233
231 IF (IBUF(NRY)-K) 232,240,240
232 IYPS=MMAX(2,JY)
233 IF (IBUF(NRY)-K) 234,241,241
234 IF (NSTAT-1) 235,236,235
235 TV(6)=RBUF(6,NRY)
CALL WAKMP(IROWT,NR,JY,TV,2)
236 RBUF(6,NRY)=SCALE
CALL WAKMP(IROWR,NR,JY,RBUF(1,NRY),2)
240 CONTINUE
IF (IYPS) 242,242,218
241 IYPE=JY-1
242 CALL WAKWR(NR,ZV)
250 CONTINUE
RETURN
END
CART ID 0105 DB ADDR 57A0 DB CNT 0004

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WAKSY,S(0105)

**WAKSY - STRATIFIED SUBMARINE WAKE, STEP SOLUTION IN Y
SUBROUTINE WAKSY

C
C THIS SUBROUTINE IN THE WAKE PROGRAM MAKES A STEP OF DELTA X/2
C WITH Z DERIVATIVES EVALUATED AT THE PRESENT X POINT

C
*COPY (CMWAK)

C
C INITIALIZE COMPUTATION

C
IOLAY=3
GO TO (10,20),NSS
10 IROWA=3
IKOWR=2
MOOD=-1
LPKRF=0
GO TO 30
20 IROWA=4
IKOWR=3
MOOD=0
IF (LPKRF) 180,30,180
30 NR=NRST-1
NPOS=NR
CALL WAKRR(NR,ZV)
CALL WAKRR(NR+1,ZPV)
JENDX=JEND
IF (LZLFF) 100,102,102
100 JENDX=JEND+1
ZM=Z+Z-ZP
IYPEM=IYPEP
IYPSM=IYPSP
102 DO 157 JZ=1,JENDX
JZN=JZ+LZLFF
IF (JZN) 104,104,104
103 NR=NR+1
NPOS=NR
CALL SFVMV(Z,ZM,NWWZF)
CALL WAKMR(2,1)
CALL SFVMV(ZP,Z,NWWZF)
CALL WAKMR(3,2)
CALL WAKRR(NR+1,ZPV)
104 IYPSN=IYPS
IYPEN=IYPE
IBOT=IYPS+LYLFF
ITOP=IYPE
C
C INITIALIZE FOR THE Y DIRECTION AND SWEEP
C
106 Y=YOLDV(IYPSN-1)
YP=YOLDV(IYPSN)
CALL WAKMP(IROWR,NR+1,IYPSN-1,XPYV,1)
CALL WAKMP(IROWT,NR+1,IYPSN-1,TPYV,1)
CALL WAKMP(IROWR,NR,IYPSN-1,XV,1)
CALL WAKMP(IROWT,NR,IYPSN-1,TV,1)
IF (JZN) 1081,1081,1082
1081 CALL WAKRF(XPYV,XPYV,2)
CALL WAKRF(TPYV,TMYV,4)
GO TO 1083


```

1082 CALL WAKMP(IROWR,NR-1,IYPSN-1,XMYV,1)
      CALL WAKMP(IROWT,NR-1,IYPSN-1,TMYV,1)
1083 CALL WAKMP(IROWR,NR+1,IYPSN,XPPV,1)
      CALL WAKMP(IROWR,NR,IYPSN,XZPV,1)
      CALL WAKMP(IROWT,NR,IYPSN,TZPV,1)
      IF (JZN) 1087,1087,1088
1087 CALL WAKRF(XPPV,XMPV,2)
      GO TO 1089
1088 CALL WAKMP(IROWR,NR-1,IYPSN,XMPV,1)
1089 JY=IYPSN-1
      IF (LYLFF) 109,110,110
109  CALL WAKRF(XPPV,XPMV,1)
      CALL WAKRF(XZPV,XZMV,1)
      CALL WAKRF(XMPV,XMMV,1)
      CALL WAKRF(TZPV,TZMV,3)
      YM=Y+Y-YP
      GO TO 120
C
C   UPWARD PASS
C
110  JY=JY+1
      CALL SFVMV(XPYV,XPMV,NMOVE)
      CALL SFVMV(XV,XZMV,NMOVE)
      CALL SFVMV(XMYV,XMMV,NMOVE)
      CALL SFVMV(TV,TZMV,NMOVE)
      YM=Y
      Y=YP
      YP=YOLDV(JY+1)
      CALL WAKMP(IROWT,NR+1,JY,TPYV,1)
      IF (JZN) 112,112,113
112  CALL WAKRF(TPYV,TMYV,4)
      GO TO 114
113  CALL WAKMP(IROWT,NR-1,JY,TMYV,1)
114  CALL WAKMP(IROWR,NR+1,JY+1,XPPV,1)
      CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
      CALL WAKMP(IROWT,NR,JY+1,TZPV,1)
      IF (JZN) 116,116,118
116  CALL WAKRF(XPPV,XMPV,2)
      GO TO 120
118  CALL WAKMP(IROWR,NR-1,JY+1,XMPV,1)
C
C   CALCULATE MATRIX COEFFICIENTS AND INVERT FOR GAMMA AND AV
C
120  CALL WAKMY
      DO 125 I=1,NWVEC
          TEM=1.0/(YMAT(I)-XMAT(I)*GM(I))
          GM(I)=TEM*ZMAT(I)
          AV(I)=TEM*(D'EC(I)-XMAT(I)*AV(I))
125  CONTINUE
      CALL WAKMP(IROWA,NR,JY,AV,2)
      CALL WAKMP(IROWG,NR,JY,GM,2)
      IF (JY-IYPEN) 110,130,130
C
C   UPPER BOUNDARY CONDITION
C
130  CALL WAKEC(I)
      IF (I) 131,140,131
131  IYPEN=JY
      GO TO 150

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```

C
C ADD POINTS TO THE RIGHT SIDE WHERE NEEDED
C
140 IF (JY+2-MXRY) 141,141,170
141 IF (JY-NYPE) 110,148,148
148 YOLDV(JY+2)=YP+DFKMX*(YP-Y)
GO TO 110

C
C INITIALIZE FOR DOWNWARD PASS
C
150 IYPEX=IYPEN-1
IYPSX=IYPSN+LYLFF
IF (IYPSX-IYPEN) 1500,1515,1515
1500 DO 151 IY=IYPSX,IYPEX
JY=IYPEX+IYPSX-IY
CALL WAKMP(IROWA,NR,JY,XV,1)
CALL WAKMP(IROWG,NR,JY,GM,1)
DO 1507 I=1,NWVEC
XV(I)=XV(I)-GM(I)*AV(I)
1507 CONTINUE
CALL SFVMV(XV,AV,NWVEC)
CALL WAKMP(IROWA,NR,JY,AV,2)
151 CONTINUE
1515 IF (LYLFF) 156,152,152

C
C LOWER BOUNDARY CONDITION
C
152 DO 154 I=1,NVAR
IF (ABS(AV(I)-ZEROV(I))-EPSSV(I)) 154,154,160
154 CONTINUE

C
C RETURN TO MAINLINE
C
156 IYPS=MMAX(2,IYPSN)
IYPE=IYPEN
NYPS=MMIN(NYPS,IYPS)
NYPE=MMAX(NYPE,IYPE)
CALL WAKWR(NR,ZV)
157 CONTINUE

C
C MONOTONICITY CHECK TO ZERO VALUES
C
NRSTX=NRST+LZLFF
NREND=NRST+JENU-1
IF (LYLFF) 1585,1570,1570
1570 I=0
LL=LZLFF
IYPS=LZLFF*(MXRY-NYPS)+MXRY
DO 1580 JZ=NRSTX,NREND
IF (LL) 1571,1574,1574
1571 IF (IYPSV(JZ)-IYPS) 1572,1580,1579
1572 I=1
IYPE=IYPS-1
IYPS=IYPSV(JZ)
DO 1573 JY=IYPS,IYPE
CALL WAKWZ(JZ-1,JY)
1573 CONTINUE
IYPSV(JZ-1)=IYPS
GO TO 1580

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```

1574 IF (IYPSV(JZ)-NYPS) 1578,1578,1575
1575 IF (IYPSV(JZ)-IYPS) 1579,1580,1576
1576 I=1
      IYPE=IYPSV(JZ)-1
      DO 1577 JY=IYPS,IYPE
      CALL WAKWZ(JZ,JY)
1577 CONTINUE
      IYPSV(JZ)=IYPS
      GO TO 1580
1578 LL=-1
1579 IYPS=IYPSV(JZ)
1580 CONTINUE
      IF (I) 1585,1585,1570
1585 I=0
      LL=LZLFF
      IYPE=LZLFF*(1-NYPE)+1
      DO 1595 JZ=NRSTX,NREND
      IF (LL) 1586,1589,1589
1586 IF (IYPEV(JZ)-IYPE) 1594,1595,1587
1587 I=1
      IYPS=IYPE+1
      IYPE=IYPEV(JZ)
      DO 1588 JY=IYPS,IYPE
      CALL WAKWZ(JZ-1,JY)
1588 CONTINUE
      IYPEV(JZ-1)=IYPE
      GO TO 1595
1589 IF (IYPEV(JZ)-NYPE) 1590,1593,1593
1590 IF (IYPEV(JZ)-IYPE) 1591,1595,1594
1591 I=1
      IYPS=IYPEV(JZ)+1
      DO 1592 JY=IYPS,IYPE
      CALL WAKWZ(JZ,JY)
1592 CONTINUE
      IYPEV(JZ)=IYPE
      GO TO 1595
1593 LL=-1
1594 IYPE=IYPEV(JZ)
1595 CONTINUE
      IF (I) 180,180,1585
C
C ADD POINTS TO THE LEFT SIDE WHERE NEEDED
C
160 IF (IYPSN-2) 170,170,161
161 IYPSN=IYPSN-1
      IF (IYPSN-NYPS) 162,106,106
162 YOLDV(IYPSN-1)=YOLDV(IYPSN)-DFRMX*(YOLDV(IYPSN+1)-YOLDV(IYPSN))
      GO TO 106
C
C REDUCTION OF NUMBER OF POINTS REQUIRED
C
170 LPKRF=1
180 RETURN
      END
CAKT ID 0105 DB ADDR 4050 DB CNT 01CC

```

WAKSZ.S(0105)

**WAKSZ - STRATIFIED SUBMARINE WAKE, STEP SOLUTION IN Z
 SUBROUTINE WAKSZ

C
 C THIS SUBROUTINE IN THE WAKE PROGRAM MAKES A STEP OF DELTA X/2
 C WITH Y DERIVATIVES EVALUATED AT THE PRESENT X POINT
 C

*COPY (CMWAK)

C
 C INITIALIZE COMPUTATION
 C

```

      IOLAY=2
      GO TO (20,10),NSS
10     IKOWA=3
      IKOWR=2
      MOOD=-1
      LPKRF=0
      GO TO 30
20     IKOWA=4
      IKOWR=3
      MOOD=0
      IF (LPKRF) 180,30,180
30     NRSTN=NRST
      JENDN=JEND
100    NR=NRSTN-1
      NPOS=NR
      CALL WAKRR(NR,ZV)
      IBOT=IYPS+LYLFF
      ITOP=IYPE
      CALL WAKRR(NR+1,ZPV)
      IBOTP=IYPS+LYLFF
      ITOPP=IYPEP
      JZ=0
      IF (LZLFF) 101,1015,1015
101    ZM=Z+Z-ZP
      IYPEM=IYPEP
      IYPSM=IYPS
      GO TO 110
1015   NR=NRSTN
102    JZ=JZ+1
      NPOS=NR
      CALL SFVMV(Z,ZM,NWWZF)
      CALL WAKMR(2,1)
      CALL SFVMV(ZP,Z,NWWZF)
      CALL WAKMR(3,2)
      IBOT=IBOTP
      ITOP=ITOPP
      IF (JZ-JENDN) 104,104,106
104    CALL WAKRR(NR+1,ZPV)
      IBOTP=IYPS+LYLFF
      ITOPP=IYPEP
      GO TO 110
106    IYPS=0
      IYPE=0
      ZP=Z+DFRMX*(Z-ZM)
      ZOLDV(NR+1)=ZP
      IYPSV(NR+1)=0
      IYPEV(NR+1)=0
      IBOTP=0

```

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      ITOPP=0
C
C INITIALIZE FOR THE Y DIRECTION AND SWEEP
C
110  Y=YOLDV(IYPS-1)
      YP=YOLDV(IYPS)
      CALL WAKMP(IROWR,NR+1,IYPS-1,XPYV,1)
      CALL WAKMP(IROWT,NR+1,IYPS-1,TPYV,1)
      CALL WAKMP(IROWR,NR,IYPS-1,XV,1)
      CALL WAKMP(IROWT,NR,IYPS-1,TV,1)
      IF (JZ) 111,111,1115
111  CALL WAKRF(XPYV,XMYV,2)
      CALL WAKRF(TPYV,TMYV,4)
      GO TO 112
1115 CALL WAKMP(IROWR,NR-1,IYPS-1,XMYV,1)
      CALL WAKMP(IROWT,NR-1,IYPS-1,TMYV,1)
112  IYPSX=IYPS+LYLFF
      IF (JZ) 1126,1126,1125
1125 CALL WAKMP(IROWA,NR-1,IYPS-1,AV,1)
      CALL WAKMP(IROWG,NR-1,IYPS-1,GM,1)
1126 CALL WAKMP(IROWR,NR+1,IYPS,XPPV,1)
      CALL WAKMP(IROWR,NR,IYPS,XZPV,1)
      CALL WAKMP(IROWT,NR,IYPS,TZPV,1)
      IF (JZ) 113,113,1135
113  CALL WAKRF(XPPV,XMPV,2)
      GO TO 114
1135 CALL WAKMP(IROWR,NR-1,IYPS,XMPV,1)
114  LZERF=0
      IYPSN=MXRY+LYLFF*(MXRY-2)
      IYPEN=1
      DO 145 JY=IYPSX,IYPE
      IF (JY-IYPS) 1141,1142,1142
1141 CALL WAKRF(XPPV,XPMV,1)
      CALL WAKRF(XZPV,XZMV,1)
      CALL WAKRF(XMPV,XMMV,1)
      CALL WAKRF(TZPV,TZMV,3)
      YM=Y+Y-YP
      GO TO 120
1142 IF (JZ) 1145,1145,1144
1144 CALL WAKMP(IROWA,NR-1,JY,AV,1)
      CALL WAKMP(IROWG,NR-1,JY,GM,1)
1145 CALL SFVMV(XPYV,XPMV,NMOVE)
      CALL SFVMV(XV,XZMV,NMOVE)
      CALL SFVMV(XMYV,XMMV,NMOVE)
      CALL SFVMV(TV,TZMV,NMOVE)
      YM=Y
      Y=YP
      YP=YOLDV(JY+1)
      CALL WAKMP(IROWT,NR+1,JY,TPYV,1)
      IF (JZ) 1146,1146,1147
1146 CALL WAKRF(TPYV,TMYV,4)
      GO TO 1148
1147 CALL WAKMP(IROWT,NR-1,JY,TMYV,1)
1148 CALL WAKMP(IROWR,NR+1,JY+1,XPPV,1)
      CALL WAKMP(IROWR,NR,JY+1,XZPV,1)
      CALL WAKMP(IROWT,NR,JY+1,TZPV,1)
      IF (JZ) 1149,1149,1150
1149 CALL WAKRF(XPPV,XMPV,2)
      GO TO 120

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```

1150 CALL WAKMP(IROWR,NR-1,JY+1,XMPV,1)
C
C CALCULATE MATRIX COEFFICIENTS AND INVERT FOR GAMMA AND AV
C
120 CALL WAKMZ
DO 125 I=1,NWVEC
TEM=1.0/(YMAT(I)-XMAT(I)*GM(I))
GM(I)=TEM*ZMAT(I)
AV(I)=TEM*(OVEC(I)-XMAT(I)*AV(I))
125 CONTINUE
CALL WAKMP(IROWA,NR,JY,AV,2)
CALL WAKMP(IROWG,NR,JY,GM,2)
IF (JZ-JENDN) 129,130,130

C
C UPPER BOUNDARY CONDITION
C
129 IF (JY-IYPSN) 1291,1292,1292
1291 IF (IYPSN-2) 145,145,130
1292 IF (JY-IYPEP) 145,145,130
130 CALL WAKEC(I)
IF (I) 145,132,145
132 IF (JZ-JENDN) 134,133,133
133 LZERF=1
134 IYPSN=MMIN(JY,IYPSN)
IYPSN=MMA(2,IYPSN)
IYPEN=MMA(JY,IYPEN)
IF (JZ+2-MXRZ) 145,170,170

C
C OUTPUT CURRENT ROW TO DISK
C
145 CONTINUE
CALL WAKWR(NR,ZV)
CALL WAKMG(NR,ZV,2)
IF (JZ-JENDN) 147,146,146
146 IF (LZERF) 1465,150,1465
1465 IYPSN=IYPSN
GO TO 1485

C
C ADD POINTS TO THE LEFT SIDE WHERE NEEDED
C
147 IF (IYPSN-IYPSN) 1475,148,148
1475 IYPSN=IYPSN
C
C ADD POINTS TO THE RIGHT SIDE WHERE NEEDED
C
148 IF (IYPEN-IYPEP) 149,149,1485
1485 IYPEP=IYPEN
149 NR=NR+1
GO TO 102

C
C INITIALIZE FOR DOWNWARD PASS
C
150 NR=NR-1
JENDN=JZ
IZEND=JENDN-LZLFF-1
DO 154 IZ=1,IZEND
NPOS=NR
CALL SFVMV(Z,ZP,NWZCF)
CALL WAKMR(2,3)

```

```

CALL WAKRR(NR,ZV)
CALL WAKMG(NR,ZV,1)
IBOT=IYPS+LYLFF
ITOP=IYPE
IYPSN=MXRY+LYLFF*(MXRY-2)
IYPEN=1
IYEND=IYPEP-IYPS-LYLFF+1
DO 1508 IY=1,IYEND
JY=IYPEP-IY+1
CALL WAKMP(IROWA,NR+1,JY,AV,1)
CALL WAKMP(IROWA,NR,JY,XV,1)
IF (JY-IYPE) 1500,1500,1502
1500 IF (JY-IYPS) 1501,1506,1506
1501 IF (IYPS-2) 1506,1506,1502
1502 DO 1503 I=1,NVAR
IF (ABS(AV(I)-ZEROV(I))-EPSSV(I)) 1503,1503,1505
1503 CONTINUE
GO TO 1508
1505 IYPSN=MMIN(JY,IYPSN)
IYPSN=MMA(2,IYPSN)
IYPEN=MMA(JY,IYPEN)
GO TO 1508
1506 CALL WAKMP(IROWG,NR,JY,GM,1)
DO 1507 I=1,NWVEC
XV(I)=XV(I)-GM(I)*AV(I)
1507 CONTINUE
CALL WAKMP(IROWA,NR,JY,XV,2)
1508 CONTINUE
C
C ADD POINTS TO THE LEFT SIDE WHERE NEEDED
C
IF (IYPSN-IYPS) 1515,152,152
1515 IYPS=IYPSN
C
C ADD POINTS TO THE RIGHT SIDE WHERE NEEDED
C
152 IF (IYPEN-IYPE) 153,153,1525
1525 IYPE=IYPEN
153 CALL WAKWR(NR,ZV)
NR=NR-1
154 CONTINUE
C
C LOWER BOUNDARY CONDITION
C
IF (LZLFF) 1545,1545,1545
1545 NR=NR+1
LZERF=0
IYPSN=MXRY+LYLFF*(MXRY-2)
IYPEN=1
IYEND=IYPE-IYPS-LYLFF+1
DO 155 IY=1,IYEND
JY=IYPE-IY+1
CALL WAKMP(IROWA,NR,JY,AV,1)
DO 1546 I=1,NVAR
IF (ABS(AV(I)-ZEROV(I))-EPSSV(I)) 1546,1546,1547
1546 CONTINUE
GO TO 155
1547 IYPSN=MMIN(JY,IYPSN)
IYPSN=MMA(2,IYPSN)

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      IYPEN=MMAX(JY,IYPEN)
      LZERF=1
155   CONTINUE
      IF (LZERF) 160,156,160
C
C   RETURN TO MAINLINE
C
156   JEND=JENDN
      NRST=NRSTN
      RETURN
C
C   NEW LOWER ROW REQUIRED
C
160   IF (NRSTN-2) 170,170,161
161   NRSTN=NRSTN-1
      JENDN=JENDN+1
      CALL WAKRK(NR-1,ZMV)
      IBOT=0
      ITOP=0
      IYPSM=IYPSN
      IYPEM=IYPEN
      CALL WAKWR(NR-1,ZMV)
      ZOLDV(NRSTN-1)=ZM-DFRMX*(Z-ZM)
      IYPSV(NRSTN-1)=0
      IYPEV(NRSTN-1)=0
      GO TO 100
C
C   REDUCTION OF NUMBER OF POINTS REQUIRED
C
170   LPKRF=2
180   RETURN
      END
CART 10 0105  DB ADDR 4F20  DB CNT 0216
```


WAKTC.S(0105)

**WAKTC - STRATIFIED SUBMARINE WAKE, TURBULENCE CHECK FOR MIN/MAX VALUES
SUBROUTINE WAKTC(TEMM,TMAX,LFL)

C

C THIS SUBROUTINE IN THE WAKE PROGRAM CHECKS THAT VV AND WW SATISFY
C RATIONAL BOUNDS ON THEIR BEHAVIOR IN AN UNSTABLE DENSITY GRADIENT

C

*COPY (CMWAK)

C

IF (TEMM) 10,100,20
10 TEMM=0.0
GO TO 40
20 IF (TEMM-TMAX) 100,100,30
30 TEMM=TMAX
40 LFL=LFL+1
100 RETURN
END

CART 1D 0105 DB ADDR 4220 DB CNT 0020

```

WAKWR,S(0105)
**WAKWR - STRATIFIED SUBMARINE WAKE, WRITE A Z BUFFER ROW
SUBROUTINE WAKWR(NRX,ZPOS)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM WRITES A Z ROW AND
C FLUSHES THE ROW BUFFER AT THE NRX POSITION FOR ALL Y
C
C DIMENSION ZPOS(2),RECB(24)
*COPY (CMWAK)
EQUIVALENCE (RECB(1),DVEC(1))
C
C DATA JERRX/2HWR/
C
C WRITE IYPS AND IYPE VALUES BACK FROM ZPOS
C
C IF (NRX) 300,300,10
10 IF (NRX-MXRZ) 20,20,300
20 CALL SFVMV(ZPOS,ZA,NWWZF)
ZOLDV(NRX)=ZA
IYPSV(NRX)=IVECA
IYPEV(NRX)=IVECB
C
C LOCATE NRX POSITION IN ROW BUFFER ARRAY
C
C J=NRX-NPOS+2
IF (J) 300,300,30
30 IF (J-3) 40,40,300
40 IF (IVECA) 150,150,50
50 IYPSX=IVECA+LYLFF
IYPEX=IVECB
C
C WRITE NRX INFORMATION FROM BUFFER ROW
C
NRXX=(NRX-1)*MXRY+IYPSX
DO 130 I=IYPSX,IYPEX
CALL PBFDR(SLNID,NRXX,NWR,RECB)
CALL SFVMV(ROWB(1,I,J),RECB(1),NWVEC)
IF (MOOD) 105,110,115
105 CALL SFVMV(ROWB(7,1,J),RECB(7),NMOVE)
GO TO 120
110 CALL SFVMV(ROWB(7,I,J),RECB(13),NMOVE)
IF (I-IBOT) 112,111,111
111 IF (I-ITOP) 120,120,112
112 CALL SFVMV(ZERUV,RECB(7),NWVEC)
GO TO 120
115 CALL SFVMV(ROWB(7,I,J),RECB(7),NWVEC)
CALL SFVMV(ROWB(13,1,J),RECB(19),NWVEC)
120 NRXX=NRXX-1
CALL PFDW(SLNID,NRXX,NWR,RECB)
130 CONTINUE
150 RETURN
300 JERR=JERRX
RETURN
END
CART ID 0105 DB ADDR 3040 DB CNT 006A

```

```
WAKWZ,S(0105)
**WAKWZ - STRATIFIED SUBMARINE WAKE, WRITE A ZERO POINT
  SUBROUTINE WAKWZ(NRZ,NKY)
C
C THIS SUBROUTINE IN THE WAKE PROGRAM WRITES
C A ZERO POINT TO THE WORKING FILE
C
  DIMENSION RECB(24)
*COPY (CMWAK)
  EQUIVALENCE (RECB(1),DVEC(1))
C
  DATA JERRX/2HWZ/
C
  IF (NRZ) 100,100,10
10  IF (NRZ-MXRZ) 20,20,100
20  NRXX=(NRZ-1)*MXRY+NKY
  CALL SFVFL(0.0,RECB,NWVEC)
  DO 30 I=7,NWR,NWVEC
  CALL SFVMV(ZEROV,RECB(I),NWVEC)
30  CONTINUE
  CALL PBFOW(SLNID,NRXX,NWR,RECB)
  RETURN
100 JERR=JERRX
  RETURN
  END
CART ID 0105 DB ADDR 5140 DB CNT 0030
```

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WAKTM.S(0101)
*IOCS(2501 READER,DISK)
**INITIALIZATION PROGRAM FOR FULL PLANE SWIRL IN WAKE PROGRAM
  DEFINE FILE 1(32000,2,U,NR)
  DIMENSION YOLDV(40),ZOLDV(40),VEC(40)
  NINU=8
  READ (NINU,1000) NY
1000  FORMAT(I4)
  READ (NINU,1001) (YOLDV(JY),JY=1,NY)
1001  FORMAT(E12.4)
  RS=.4
  RV=1.5
  NZ=NY+NY-1
  DO 10 JY=1,NY
  IY=NY-JY+1
  IZ=NZ-JY+1
  YOLDV(IY)=RS*YOLDV(IY)
  ZOLDV(JY)=-YOLDV(IY)
  ZOLDV(IZ)=-ZOLDV(JY)
10  CONTINUE
  NY=NZ
  CALL SFVMV(ZOLDV,YOLDV,NY)
  RMAX=ZOLDV(NZ)
  NR=1
  RR=0.0
  WRITE (1,NR) RR
  WRITE (1,NR) NY,NZ,(YOLDV(JY),JY=1,NY),(ZOLDV(JZ),JZ=1,NZ)
  DO 100 I=1,6
  DO 90 JY=1,NY,10
  IY=MMIN(JY+9,NY)
  DO 80 JZ=1,NZ
  CALL SFVFL(0.0,VEC,40)
  Z=ZOLDV(JZ)
  IF (JZ-1) 70,70,30
30  IF (JZ-NZ) 40,70,70
40  DO 60 J=JY,IY
  Y=YOLDV(J)
  IF (J-1) 60,60,42
42  IF (J-NY) 45,60,60
45  R=SQRT(Y*Y+Z*Z)
  IF (R-RMAX) 46,60,60
46  GO TO (51,60,52,54,54,60),I
51  RR=(Z*Z+Y*Y)/RS/RS
  VEC(J)=.0108/(1.0+RR/6.25)**2
  GO TO 60
52  RR=0.5*(Z*Z+Y*Y)/RS/RS
  VEC(J)=0.080*(1.0-RR)*EXP(-RR)
  GO TO 60
54  RR=3.0*(Y*Y+Z*Z)
  IF (R) 60,60,55
55  IF (R-RV) 555,60,60
555  VEL=(1.0-EXP(-RR))*(RV-R)**2/R/15.0
  IF (I-4) 56,56,57
56  VEC(J)=-VEL*Z/R
  GO TO 60
57  VEC(J)=VEL*Y/R
60  CONTINUE
70  WRITE (1,NR) (VEC(J),J=JY,IY)
80  CONTINUE

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```
90 CONTINUE  
100 CONTINUE  
    RR=-1.0  
    WRITE (1, NR) RR  
    CALL EXIT  
    END  
CART 10 0101  DB ADDR 5410  DB CNT 0080
```



FORTRAN Coding Form

GX28-7327-6 U/M 050**
Printed in U.S.A.

PROGRAM PROGRAMMER	DATE	PUNCHING INSTRUCTIONS	GRAPHIC PUNCH	PAGE OF	CARD ELECTRO NUMBER*
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STATEMENT NUMBER	FORTRAN STATEMENT	IDENTIFICATION SEQUENCE
1	10	
2	FULL PLANE SWIRL WITH AXIAL VELOCITY AT FR = 10	
3	0.0 50.8 0	
4	0 40 0	
5	1 1 0 1 1 0 1 1	
6	.0001	
7	.5	
8	.0	
9	.001	
10	.63	
11	1 0 10 500 20 0 2 0	
12	19.4 50.8	
13	3 5 4 1 0 0 5	
14	3.68E+07.01	
15	.3 1. .25	
16	-.35 -.6	
17	.001 .1	
18	WAKWF WAKGM WAKGL WAKPL	
19	3 -1 1 0 1	

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**Number of forms per pad may vary slightly

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