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ENGINE-FUEL LUBRICANT COMPATIBILITY TESTS ON MIL-L-2104C OILS USING ENGINE MODEL 6V53T AND HIGH SULFUR FUEL

E. A. Frame, et al

Southwest Research Instutite

Prepared for:

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September 1974

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# ENGINE-FUEL-LUBRICANT COMPATIBILITY TESTS ON MIL-L-2104C OILS USING ENGINE MODEL 6V53T AND HIGH SULFUR FUEL

INTERIM REPORT AFLRL NO. 26

> E. A. Frame S. J. Lestz A. A. Johnston



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U. S. Army Fuels and Lubricants Research Laboratory
Southwest Research Institute
San Antonio, Texas

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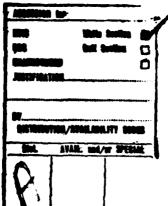
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	Earlier work in this program showed tha					
	cycle diesel engine model 6V53T when subject					
	test cycle, operating with a reference No. 2 die					
	the low-ash (0.93% wt.) lubricant REO 203 de					
	(1.75% wt.) lubricant REO 205 was judged bo					
	work, the use of high natural sulfur fuel (1.2%					
	and ring zone deposits with REO 205 lubrican	t, and increased cylinde	er liner wear and intake port plugging			
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with REO 203 lubricant. Based upon this performance with the two-cycle diesel engine, model 6V53T. A recommendation of the control of the control of the cycle diesel engine, model 6V53T.	e, the 1.2% natural sulfur fuel was judged incompatible commendation for additional engine testing is made.				



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## **FOREWORD**

The work reported herein was conducted at the U.S. Army Fuels and Lubricants Research Laboratory (USAFLRL), located at Southwest Research Institute, San Antonio, Texas, under Contract DAAK02-73-C-0221 during the period June 1973 through September 1973. The contract monitor was Mr. C. F. Schwarz, USA MERDC, Coating and Chemical Laboratory STSFB-GL, Aberdeen Proving Ground, Maryland. Project technical monitors were Messrs. M.E. LePera and T.C. Bowen, also of that office. Current contract monitor is Mi. F.W. Schaekel, USAMERDC, STSFB-GL, Ft. Belvoir, Virginia.

# **TABLE OF CONTENTS**

		Page
LIST	OF ILLUSTRATIONS	4
LIST	OF TABLES	4
١.	INTRODUCTION	5
II.	DETAILS OF . IE TEST	5
	A. Test Engine  B. Test Fuel  C. Test Lubricants  D. Test Technique	5 5 8 8
ш.	DISCUSSION	10
	Performance of DFM (High-Sulfur Fuel) and REO 205 Lubricant (High-Ash)—Test     No. 6     Performance of DFM (High-Sulfur Fuel) and REO 203 Lubricant (Low-Ash)—Test     No. 7     No. 7	11 16
IV.	CONCLUSIONS	17
V.	RECOMMENDATIONS	18
VI.	STATUS OF PROGRAM	18
VII.	ACKNOWLEDGEMENT	18
VIII.	REFERENCES	18
APPE	ENDICES	
<b>D</b>	1—Compatibility Test Procedure Wheeled—Vehicle Test Cycle 6V53T Engine	21 31 35 79 123

## LIST OF ILLUSTRATIONS

Figure		Page
1	M551 Armored Reconnaissance/Airborne Assault Vehicle—"Sheridan"	6
2	Diesel Engine Model 6V53T Test Facility	7
3	Damaged and Adjacent Exhaust Valves (Test No. 6)	12
	LIST OF TABLES	
Table		Page
1	6V53T Engine Characteristics	6
2	Analysis of Test Fuels	7
3	Comparison of Test Lubricant Property Data with MIL-L-2104C Requirements	8
4	6V53T Engine Operating Conditions	9
5	6V53T Compatibility Test Summary	10
6	Summary of Operating Data	11
7	Piston Ping Freedom	12
8	Piston Ring Groove Deposits Back of Groove: Percent Carbon Filling	12
9	Piston Groove - Inside Diameter Percent Ring Supporting Carbon	13
10	Piston "F" Rating Demerits	13
11	Piston Skirt Deposit Demerits	14
12	Cylinder Liner Scuffing Percent Total Ring-Travel Area Scuffed	14
13	Piston Ring Gap Change	15
14	Cylinder Liner Diameter Change	15
15	Test Fuel Analyses	16
16	Lubricant Analyses	17

## I. INTRODUCTION

The Department of Defense (DoD) must procure many different types of petroleum fuels to meet the requirements of its military ground, air, and marine equipment. Operation outside the continental United States increases the complexity of fuel logistics because of the wide geographical scatter of the U.S. military installations. Therefore, standardization of fuel requirements between the services and between allied countries has been a continuing subject of discussion and study. The problem of U.S. Army fuel standardization within the NATO complex has been primarily in the area of diesel fuel requirements; namely, the U.S. Army providing diesel fuels meeting VV-F-800a, DF1/DF2, whereas the other NATO countries have interchangeability agreements for using NATO F-54 which is similar to MIL-F-16884F. Both F-54 and MIL-F-16884F have specification limits that permit higher sulfur and higher distillation values (90%-EP); characteristics that may cause increased wear/deposition in two-cycle diesel engines within the military inventory. Prior to AMC permitting the use of a high-sulfur fuel in lieu of VV-F-800a, additional engine data were desired upon which a sound judgment could be made. To this end, it was decided to undertake the engine tests reported herein.

## II. DETAILS OF THE TEST

## A. Test Engine

The engine used in this program was the 6V53T, whose characteristics are shown in Table 1. End use for this engine is the M551-Sheridan, Armored Reconnaissance/Airborne Assault Vehicle, Full Tracked, 152mm; a picture of which is shown in Figure 1. The 6V53T engine was selected because it is typical of one family of two-cycle diesel engines found in today's Army, i.e., the 6V53, 3-53, 8V71T, and 12V71T engines that are used throughout the combat vehicle fleet. Specifically, this particular engine model was selected for two reasons: (1) considerable lubricant-engine compatibility data had been accumulated in this engine using MIL-L-2104C oils<sup>(2)</sup>, and (2) this is a highly stressed engine which is sensitive to variations in fuel and lubricant quality and composition.<sup>(3)</sup>

The laboratory test stand (Figure 2) consisted of a 400 hp Midwest absorption dynamometer, Eaton's Dynamatic control chassis, and a Hagen pneumatic load transmitting/indicating load system. Combustion air is drawn into the engine through a stack of four dry-type automotive air filters inside a fiberglass-lined 30-gallon barrel. Arctic anti-freeze (MIL-A-11755) used for jacket coolant is circulated by the engine centrifugal-type water pump, with the thermostat mechanically blocked open to provide normal operation flow restriction. The throttle (governor-rack control) is operated by an air-powered diaphragm. Blow-by is vented through the rocker cover breather cap to a blow-by meter and then drawn into the air barrel inlet with the combustion air, resulting in 100% blow-by recycle.

## B. Test Fuel

The hydrocarbon fuel was blended to generally conform to the specification limits of Military Specification MIL-F-16884F, diesel fuel, marine (D<sup>r</sup>M). The upper limit of sulfur (1%) and distillation end point (EP 725°F) were selected to assure that the fuel represented the most severe blend that might be found in the logistics system. Table 2 presents a comparison of the specification and procured fuel characteristics for the high-sulfur fuel (DFM) and the reference No. 2 diesel fuel, which is a nominal VV-F-800a<sup>(4)</sup> No. 2 diesel fuel conforming to the requirements established by Federal Test Method Standard 791B, Method 341.4;<sup>(5)</sup> and is a straight-run, mid-range natural sulfur fuel which is manufactured under closely controlled refinery operation to minimize compositional deviations. A single batch of this latter fuel was used to generate the engine-lubricant compatibility baseline data that are used for comparison in this program. As noted from Table 2, the sulfur level of the procured diesel marine (DFM) type fuel was higher than the specification limit by 0.2% weight, along with the distillation end point that was above

<sup>\*</sup>Superscript numbers in parentheses indicate references at end of report.

TABLE 1. 6V53T ENGINE CHARACTERISTICS

Engine type	Turbocharged, two-cycle compression ignition, direct injection uniflow scavenging
Weight, lb (Dry)	1092
Number of cylinders, arrangement	6, V
Displacement, cu. in.	318
Bore and stroke, in.	3-7/8 × 4-1/2
Cylinder block material	Aluminum, with cast iron liners
Rated brake horsepower	300 at 2800 rpm, at 60°F and 29.92 in. Hg
Maximum torque, lb-ft	615 at 2200 rpm
Compression ratio	17 to 1
Fuel system	Unit injectors (N 70, needle valve), primary and secondary engine filters
Governor	Limiting speed, double weight
Oil sump capacity, gal	5
Oil filter	Full-flow single filter
Oil cooling	Integral heat exchanger using 100% jacket-coolant flow
Piston description	
Material design	Cast iron, trunk type
Ring configuration	1-Fire ring (rectangular) 3-Compression rings (rectangular) 2-Oil rings
Oil spray cooled	Yes, from top of connecting rod



FIGURE 1. M551 ARMORED RECONNAISSANCE/ AIRBORNE ASSAULT VEHICLE—"SHERIDAN"

TABLE 2. ANALYSIS OF TEST FUELS

D	Ref N	o. 2 DF	MIL-F-16	884F (DFM)
Property	Test fuel	Specification <sup>a</sup>	Test fuel	Specification <sup>a</sup>
API gravity	33.2	Record	34.1	Record
Viscosity at 100°F, Cs	3.20	1.6-4.5	3.66	52.1-6.0
Flash point, °F	185	100 min	190	140 min
Cloud point, °F	+23	Record	+30	+ 10 max
Pour point, °F	+18	20 max	+10	0 max
Water and sediment	0.0	0.05 max	0	0.01 max
Carbon residue, %	0.10	0.20 max	0.14	0.20 max
Lamp sulfur, %	0.415	0.35 min	1.20	1.00 max
Acıd no.	0.108	Record	0.18	0.50 max
Aniline no., °F	145	Record	150	Record
Copper corrosion	1A	No. 2 max	ND	1 max
Distillation, °F	ŀ		ł	
IBP	410	Record	399	NR
10%	468	Record	447	NR
50%	519	500 min	533	Record
90%	603	600-640	679	675 max
EP	689	650-690	744	725 max
Cetane number	47b	40-45	50.5	47 min
Higher heating value,			i	
Btu/lb	19.550c	Record	18,960	NR
Accelerated stability.	ŕ	,	} '	
total insolubles, mg/				
100 mg	2.1	NR	1.50	2.5 max
Ash, % N:= Not determined. NR : Not required.	0.006	0.01 max	ND	NR

\*Section 4.1, Method 341.7, FTM Std. 791B. bCalculated Cetane Index.

\*\*Calculated higher value from gravity, viscosity, and distillation properties.

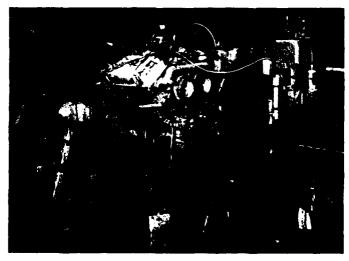


FIGURE 2. DIESEL ENGINE MODEL 6V53T TEST FACILITY

the desired limit by 19°F. Since this fuel procurement was not obtained from a normal refinery run, these deviations from the specification were permitted. The fuel was analyzed when received, between the first and second test and after the final engine run, to define changes in the fuel characteristics which might contribute or detract from the final engine deposit/wear results. These data are reported in the Program Detail Section.

## C. Test Lubricants

The two lubricants used in this program were furnished by the U.S. Army Coating and Chemical Laboratory (C&CL), designated REO 205 and REO 203.\* Both lubricants meet the requirements established in U.S. Military Specification MIL-L-2104C.<sup>(6)</sup> Comparison of property data of the oils with MIL-L-2104C requirements is presented in Table 3. These lubricants were selected for this program for three specific reasons: (1) both had been previously evaluated in the 6V53T diesel engine using the reference

TABLE 3. COMPARISON OF TEST LUBRICANT PROPERTY DATA WITH MIL-L-2104C REQUIREMENTS

Property	REO 205	REO 203	MIL-L-2104C
Gravity, API	27.3	27.4	Report
Flash point, °F	460	465	425 min
Viscosity, CST			
at 210°F	12.93	12.61	9.6-12.9
at 100°F	126.7	121.6	Report
Viscosity index	101	94	75 min
Pour point, °F	-5	-5	0 (max)
Carbon residue, %	1.69	1.19	Report
Sulfated ash, %	1.75	0.93	Report
Total acid no.	3.0	3.6	Report
Total base no.	12.5	5.4	Report
Additive, % wt			
Zn	0.093	0.093	Report
Ca	0.44	0.24	Report
Ba	Nil	Nil	Report

No. 2 diesel fuel, (2) they represent high- and low-ash additive package formulations similar to oils which may be procured by the military under MIL-L-2104C, and (3) the manufacturer of the 6V53T engine recommends use of a low-ash oil (1.00% wt maximum) with fuel having a sulfur content of up to 0.500% weight, and a high-ash oil (up to 1.50% wt) when using a high-sulfur fuel. REO 203 was formulated as a "Universal Oil" to meet the American Petroleum Institute (API) service classification CD/SE<sup>(7)</sup>, while REO 205 was formulated primarily to meet API classification, CD.

## D. Test Technique

A laboratory test technique, previously developed by the Army in cooperation with the Coordinating Research Council (CRC)<sup>(8)</sup>, was selected for the DFM program. This technique involves cyclic endurance testing of the vehicle engine on a laboratory dynamometer stand for 210 hr, which is designed to correlate with 20,000 miles field service for a tactical, wheeled vehicle. Compatibility of the engine-fuel-lubricant system is judged on: (1) the ability of the test engine to maintain performance throughout the cycle; (2) wear developed in engine components; (3) accumulation of fuel and lubricant related engine deposits; and (4) the physical and chemical condition of the lubricant as monitored throughout the test.

Even though the M551 is a full-track-laying vehicle, it was doubted that the wheeled-vehicle test cycle for the 6V53T engine would be used because of the prior experience (2,9,10) using this test cycle with the Military two-cycle diesel engine. Additionally, the data obtained using this cycle operating on reference No. 2 diesel fuel(2) provided a baseline for the DFM program. The details of the wheeled-vehicle

<sup>\*</sup>These lubricants were originally identified as CCL-L-758 and L-759 respectively.

compatibility test cycle, as applied to the 6V53T engine, are given in Appendix I. The procedure as shown reflects the comments and suggestions provided by the CRC Army Combat Engines Fuels and Lubricants Group. The substance of the CRC guidance is based on a group meeting held 24 August 1972 and is presented in Appendix II. The current procedure is essentially the same as the one used in References 2, 9, and 10, except that glycol coolant (arctic antifreeze, MIL-A-11755) was used in the current series of tests. A summary of the current test procedure is as follows:

- Clean, measure, and rebuild test engine using new cylinder liners, pistons, piston rings, connecting rod, and main bearing inserts, in accordance with standardized buildup procedures specified by appropriate Army Technical Manuals (11,12) or engine manufacturer bulletins. (13)
- Run-in the engine and perform full-load performance calibration using reference No. 2 DF.
- Flush fuel system and conduct full-load performance calibration using test fuel (DFM).
- Conduct compatibility endurance test; operating conditions are summarized in Table 4.
- Perform post-test full-load performance calibration.
- Disassemble, inspect, and rate in accordance with CRC Diesel Manual No. 5,(14) and remeasure
  engine.

Detailed baseline test data using reference No. 2 diesel fuel (Test Nos. two and three) were appended to the report of reference 2 and are not included in this report. Detailed test data for Test

**TABLE 4. 6V53T ENGINE OPERATING CONDITIONS** 

Parameter	Limits; or se	ttings, for	
rarameter	Power mode	Idle mode	
Speed, rpm Fuel flow	2800 + 20	650 + 10	
Typical, lb/min, (2 lb wt/time) Fuel/cycle, mm <sup>3</sup> Revolutions/2 lb	2.07 ± 0.07 67 69 2680 ± 50	(use 2 oz) 	
Time/2 lb Obs BHp output Jacket-out, 1-	0.965 + 0.035 282   300 180 + 2	- 100 ± 2	
Coolant & T. F. Oil sump. F. Fuel temp & filter, F.	8 12 250, max 90 + 5	2 - 3	
Fuel pressure, range, psi Compressor suction, clean filter, inches water	55 70 6.0 max	70 max	
Compressor suction, dirty filter, inches water Exhaust back pressure	12.0 max		
(after turbo), inches Hg Crankcase pressure, inches water Oil pressure, psi	2.3 6.0 max 32 min	5 min	
Blowby flow, CFH	1150 max	2 mm	
Test duration Oil drains Oil level checks and additions	210 hr None Every 1	4 hr	
Oil samples Airbox inspection	I very 1 None		

Nos. 6 and 7, using high-sulfur fuel (DFM), are found in Appendices III and IV. Each appendix includes the following information:

- (1) Summary of Buildup Measurements
- (2) Summary of Operating Data
  - Power performance before test

Date

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- Tabulated data for power mode, idle mode, and record of unscheduled shutdowns
- Plotted operating data
- Used-Lubricant Analyses
- Wear Measurements
- (5) Deposit Ratings and Parts Description (in accordance with CRC Rating Manual No. 5)
- Photographs of the "average" and "worst" cylinder assemblies from a deposit standpoint (designated by the CRC Army Combat Engines, Fuels, and Lubricants Performance Group)

Only summary and comparative data necessary to establish engine and lubricant performance are presented in the discussion section of the report (Tables 6 through 16 and Figure 3). Fo: detailed test data, the reader is referred to Appendices III and IV.

The CRC Combat Engines, Fuels, and Lubricants Group inspected the pistons, piston rings, cylinder liners, and connecting rod and main bearing inserts at the U.S. Army Fuels and Lubricants Research Laboratory on 14-15 February 1974. Appendix V contains a summary of the inspection results relevant to the fuel sulfur level and its compatibility with the 6V53T engine.

#### III. DISCUSSION

Four 6V53T engine-fuel-lubricant compatibility tests, using the 210-hr wheeled-rehicle test cycle, form the basis of the current program. A summary of the four tests is shown in Table 5. Note in Table 5

Test Engine codes stopping test no. completed no. hours Reference no. 2 diesel fuel (0.42%S) 20 Dec 72 6D36804-14 **REO 203** 210 Completed test 6D5084-4 **REO 205** 209.5 16 Jan 73 OK -(exhaust valve seat breakage in cylinder 2R) DFM (1.2%-S) 18 Jun 73 6D5084-6 **REO 205** 194 Power loss; burned 6 eah. valve-21.

**REO 203** 

196

TABLE 5. 6V53T COMPATIBILITY TEST SUMMARY

Oil

Test

Reason for

Rising crankcase pressure & blow-by

flow

that Test Nos. 2 and 3 provide the baseline data for comparison with the current high-sulfur fuel (DFM) test results (Tests 6 and 7).

# A. Performance of DFM (High-Sulfur Fuel) and REO 205 Lubricant (High-Ash)—Test No. 6

The first of the fill of the best insulations of the second of the secon

Engine operation was held within the desired performance envelope through 13 engine cycles, 182 hours (Table 6). During the fourteenth cycle, increasing exhaust temperature and power loss required test termination at 194 hours without obtaining a final power curve. The engine was disassembled and upon inspection of the valve train, a burned exhaust valve in cylinder No. 2 on the left bank was found. No damage to the cylinder, piston, or turbo-charger was noted, and all other cylinders appeared normal. Figure 3 shows the valve compared with a sister valve and valves from adjacent cylinders. Deposit and wear measurements were then completed on all engine parts required by the test plan.

Piston ring freedom (Table 7) was less than when using reference No. 2 diesel fuel. This lack of freedom was reflected in both piston ring groove deposits (Table 8) and piston ring groove supporting carbon (Table 9). However, when tests Nos. 3 and 6 are compared (Table 10), using the proposed CRC

TABLE 6. SUMMARY OF OPERATING DATA

				Power	mode			
•		REC	205		REC		203	
Parameters	DI	·M	Ref No. 2 DF		DFM		Ref No. 2 DF	
	Test	no. 6	Test	no. 3	Test	no. 7	Test r	10. 2
	Max	Avg	Max	Avg	Max	Avg	Max	Avg
Engine speed, rpm, 2800 ± 20	2800	2800	2800	2800	2800	2800	2800	2800
Load, lb	428	421	440	432	428	421	435	431
BHP, obs. (2800/4100) × load	292	288	300	297	292	287	297	294
Fuel/cycle, mm <sup>3</sup>	68.1	67.3	67.7	67.1	68.4	67.6	68.2	67.1
Fuel rate, lb/min	2.08	2.06	2.09	2.07	2.09	2.06	2.10	2.07
Oil consumption, lb/hr avg for		0.52	i -	0.49	-	0.52	-	0.66
test duration	194	hr	209	.5 hr	196	hr	21	0 hr
	T	emperati	ures, °F					
Jacket-in	171	170	174	172	174	170	176	172
Jacket-out, 180+5	182	181	184	181	186	181	184	181
Oil sump	238	237	236	234	240	236	246	238
Inlet air (compressor)	101	95	94	79	114	99	96	83
Airbox	287	282	281	270	300	290	304	291
Exhaust before turbo	1060	1050	1060	1035	1100	1070	1090	1060
Exhaust after turbo	900	880	900	860	930	900	920	885
Fuel at filter (secondary)	91	89	82	78	100	90	83	80
		Pressure	s	-				
Compressor suction, in. H, O	10.8	6.9	11.2	7.1	12.9	8.0	11.2	7.2
Compressor discharge, in. Hg	24.7	23.8	24.2	23.4	24.3	23.0	24.0	23.2
Blower discharge (airbox), in. Hg	36.7	35.7	38.7	37.0	37.7	35.8	38.5	37.0
Crankcase, dipstick tube, in. H, O	4.7	4.2	5.0	4.5	6.0	5.4	4.2	3.5
Exhaust before turbo, in. Hg	26.3	25.7	26.7	25.9	26.9	25.0	26.7	25.9
Exhaust after turbo, in. Hg	2.2	2.1	2.2	2.2	2.9	1.9	2.2	2.1
Oil gallery, psi	43	41.7	42.7	41.8	41.5	40.8	36.2	35.4
Fuel at filter, psi	72	69.8	74.5	73.6	71.0	69.6	72	72
Blow-by flow, cfh at 29,92 in. Hg			Į į			l	l	ļ
and 115°F	900	850	1100	1020	1030	910	900	790
Record of unscheduled shutdowns	No	ne	No	ne	N	o <u>ne</u>		a
a Repair oil leak at filter housing &	flush ma	in heat e	exchange	r 24 hou	rs total			

TABLE 7. PISTON RING FREEDOM

Ring		DFM			Ref No. 2	DF					
No.	Free	Cold stuck & pinched		Free	Cold stuck & pinched						
REO 205											
1	1 3 1 2 5 0 12										
2	5	0	1	6	0	0					
2	3 5 5	1	0	6	0	0					
4	6	0	0	6	0	0					
Total	19	2	3	23	0	1 <sup>a</sup>					
	REO 203										
1	6	0	0	6	0	0					
2	6	0	0	6	0	0					
3	6	0	0	6	0	0					
4	6	0	0	6	0	0					
Total	24	0	0	24	0	0					
<sup>a</sup> Valve	Failt	ıre			<u> </u>						

TABLE 8. PISTON RING GROOVE DEPOSITS BACK OF GROOVE: PERCENT CARBON FILLING

		DEN	4	Ref No. 2 DF		
Ring No.	Max	Avg	Avg (w/o Max)	Max	Avg	Avg (w/o max)
			REO 205			
1	100 <sup>a</sup> (3) <sup>b</sup>	5.8	15	100 <sup>a</sup>	21	6
2	100 <sup>a</sup> (1)	77	72	90	72	68
3	100 <sup>a</sup> (1)	27	12	40	19	15
4	10	2	1	3	1	<1
			REO 203			
1	3	1	1	15	7	5
1 2 3 4	85	63	59	75	70	69
3	2υ	12	11	5	4	3
4	0	0	0	0	0	0

 $^{a}$ Stuck = 100% volume fill.

bNumbers in parentheses indicate number stuck.

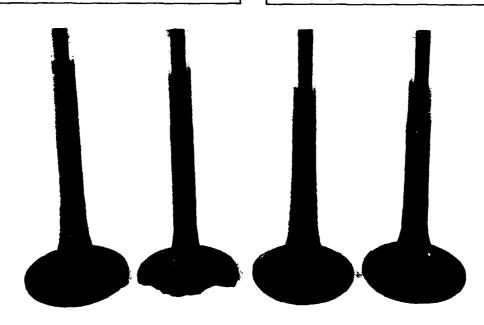


FIGURE 3. DAMAGED AND ADJACENT EXHAUST VALVES (Test No. 6)

"F"-rating method<sup>(15)</sup>, the total 6-cylinder demerit deposit rating was slightly less (cleaner) when DFM fuel was used. This is because the "F"-rating method does not include cylinders with stuck rings in calculating the deposit ratings. Thus, test No. 6, with several stuck rings, gave a cleaner rating using this method. In all cases, ring No. 1 is the top ring, also referred to as the fire ring. Piston skirt deposits (Table 11) were essentially the same as those formed when using the reference fuel. Intake port deposits were found to be twice the level (3% vs 1.5%) of that observed in the test using reference fuel.

Wear was generally the opposite of the deposit trend; i.e., cylinder liner scuffing (Table 12), piston ring gap change (Table 13), and cylinder liner diameter change (Table 14) decreased when using the DFM instead of the reference No. 2 diesel fuel.

## TABLE 9. PISTON GROOVE-INSIDE DIAMETER PERCENT RING SUPPORTING CARBON

Position		DFM		Ref	No. 2 D	F
Position	Мах	Avg	Avg (w/o max)	Max	Avg	Avg (w/o max
			REO 205			
			Ring no. 1			
Thrust	100a(3)b	50	0	1002(1)	17	0
Rear	100a(3)	57	13	100a(1)	17	0
Antithrust	100a(3)	57	13	100a(1)	17	0
Front	1002(3)	53	7	100ª(1)	17	0
			Ring no. 2			
Thrust	100 <sup>a</sup> (1)	49	39	100	49	24
Rear	100a(1)	68	51	90	42	32
Antithrust	100a(1)	76	52	100	64	56
Front	100a(1)	62	43	100	57	48
			REO 203			
			Ring no. 1			
Thrust	0	0	0	0	0	0
Rear	0	0	0	0	0	0
Antithrust	0	0	0	0	0	0
Front	0	0	0	0	0	0
			Ring no. 2			
Thrust	90	63	50	80	36	27
Rear	85	52	45	60	18	9
Antithrust	100	58	49	100	49	39
Front	90	37	26	70	38	31

## TABLE 10. PISTON "F" RATING<sup>2</sup> DEMERITS

	REO 205		REO 203	
1117 Yr	DFM	Ref no. 2 DI-	DEM	Ref no. 2 DF
"F"Demerit		Test no	/Test hr	
	6/194	3/209.5	7/196	2/210
Minimum cylinder	80b	160°	133	131
Maximum cylinder	280	210	189	168
Average cylinder	175	197	148	150
Total cylinder	1048	1183	890	899

aProposed CRC F-Rating Method for Total Demerits (0 = Clean)-Location Factor not used; Piston Skirt Demerit not included. bFire rings not removed from cyls 1R, 1L, 3L, & 3L Top C/R, otherwise min was 187.

<sup>&</sup>lt;sup>C</sup>Fire ring not removed from cyl 2R, otherwise min was 198.

TABLE 11. PISTON SKIRT DEPOSIT DEMERITS

		DI	·M	Ref no. 2		. 2 DF
Position	Max	Avg	Avg (w/o max)	Max	Avg	Avg (w/o max)
			REO 205			
Thrust	4.2	3.5	3.3	4.8	4.4	4.3
Antithrust	4.2	3.7	3.6	5.0	4.4	4.3
Avg T & AT		3.6	3.5		4.4	4.3
			REO 203			
Thrust	4.1	4.0	3.9	4.5	4.2	4.1
Antithrust	4.1	3.9	3.8	3.8	3.6	3.6
Avg T & AT	1	4.0	3.9	-	3.9	3.9

TABLE 12. CYLINDER LINER SCUFFING PERCENT COMPRESSION RING-TRAVEL AREA SCUFFED

	Ĭ	DF	M		Ref n	o. 2 DF
Area scuffed	Max	Avg	Avg (w/o max)	Max	Avg	Avg (w/o max)
		R	EO 205			
Thrust	35	13	9	40	15	10
Antithrust	25	13	10	40	12	7
Total area	25	13	10	40	14	8
Glazed deposits	60	44	41	55	31	29
Lacquered deposits	35	28	23	15	9	8
REO 203						
Thrust	30	13	10	15	5	3
Antithrust	30	14	11	5	2	2
Total area	25	14	11	8.5	4	3
Glazed deposits	70	54	51	25	19	13
Lacquer deposits	35	2.3	21	12	9	9

Fuel analyses following completion of the test (Table 15 dated 18 June 1973) provide no indication of major fuel degradation, even though the fuel injection system recycles approximately 50% of the fuel back to the storage tank. This causes the fuel to undergo a cyclic heating to approximately 160°F with cooling to 80°F.

Final oil analyses (Table 16) were comparable to the results obtained on the oil when using reference No. 2 diesel fuel. Origin of the tin (33 ppm) is not known and reexamination of the engine did not clarify this point.

Overall, the use of the DFM appeared to increase ring zone and combustion chamber deposits, an expected result due to the fuel's high distillation end-point. The piston ring surfaces had undergone severe attack, due most likely to the high-sulfur content of the fuel, and apparently the oil could not inhibit this action. However, cylinder liner wear, oil degradation, scuffing, etc., were well controlled by the high-ash oil additive package, especially when considering that the fuel was on the extreme side of the specification.

TABLE 13. PISTON RING GAP CHANGE

D:		DFM			Ref no. 2	DF
Ring No.	Max	Avg	Avg (w/o max)	Max	Avg	Avg (w/o max)
			REO 20.	5		
Į a	0.008	0.007	0.007	0.010	0.005	0.003
2b	0.004	0.003	0.003	0.007	0.005	0.005
зb	0.004	0.003	0.002	0.010	0.006	0.005
4	0.003	0.002	0.002	0.012	0.005	0.004
5-7	0.014	0.010	0.009	0.036	0.015	0.011
REO 203						
1	0.021	0.013	0.012	0.003	0.002	0.002
2	0.005	0.004	0.004	0.003	0.002	0.002
2	0.006	0.004	0.003	0.004	0.002	0.002
4	ባ.006	0,004	0.004	0.004	0.002	0.002
5 - 7	0.016	0.013	0.012	0.010	0.007	0.006
		not include		<u> </u>		

TABLE 14. CYLINDER LINER DIAMETER CHANGE

		DFM			Ref no. 2	Dł
Location	Max	Avg	Avg (w/o max)	Max	Avg	Avg (w/o max)
			REO 205			
		Per	pendicular to	Crank		
Тор	0.0016	0.0012	0.0011	0.0053	0.0025	0,0020
Middle	0.0007	0.0004	0.0004	0.0011	0.0010	0.0010
Bottom	0.0003	0.0002	0.0001	0.0007	0.0004	0.0003
		F	arallel to Cra	nk		
Тор	0.0010	0.0005	0.0004	0.0010	0.0006	0.0005
Middle	0.0008	0.0002	0.0001	0.0011	0.0006	0.0005
Bottom	0.0003	0.0001	0.0001	0.0006	0.0003	0.0002
			REO 203			
		Per	pendicular to	Crank		
Тор	0.0036	0.0026	0.0020	0.0011	0.0008	0.0007
Middle	0.0013	0.0011	0.0010	0.0009	0.0007	0.0007
Bottom	0.0009	0.0007	0.0007	0.0003	0.0002	0.0002
		F	arallel to Crai	nk		
Тор	0.0015	0.0007	0.0006	0.0007	0.0004	0.0004
Middle	0.0011	0.0006	0.0005	0.0004	0.0003	0,0002
Bottom	0.0005	0.0003	0.0003	0.0010	0.0003	0.0002

TABLE 15.

Property		DFM	
· · · openty	5/24/73	6/18/73	8/6/73
API gravity, deg	34.1	33.6	33.7
Viscosity at 100°F, cs	3.66	3.78	3.78
Flash point, °F	190	-	180
Cloud point, °F	+36	-	+33
Pour point, °F	+10	-	+28
Water + sediment	Water=0	Water=0	] _
ſ	Sed=Trace	Sed=Trace	Í -
Carbon residue %	0.14	0.12	0.21
Sulfur %	1.21	1.205	1.21
Acid no.	0.18	0.21	0.19
Aniline point, "F	150	150	148.6
Distillation, °F			1 10.0
1BP	399	402	382
10%	447	448	454
50%	533	532	538
90%	679	686	677
EP	744	736	753
Accelerated gum			
mg/100 mg Gross heating value	1.5	0.6	1.2
Btu/lb	18,960	_	

## B. Performance of DFM (High-Sulfur Fuel) and REO 203 Lubricant (Low-Ash)— Test No. 7

Engine operation remained within the desired performance envelope through 13 engine cycles (Table 6) as in Test No. 6; then, crankcase pressure began increasing. At the completion of the fourteenth cycle (196 hours), crankcase pressure and blow-by flow rate approached the maximum allowable limits. Experience<sup>(2,3)</sup> had shown that rising crankcase pressure and blow-by flow rate are generally indicative of pending severe piston scuffing and piston/liner seizure. Therefore, to assure engine integrity, the test was terminated, and no attempt was made to run the final power curve.

The engine was disassembled, and deposit/wear measurements were made. Generally ring freedom and deposition (Tables 7, 8, 9 and 11) showed little or no change from the rating levels recorded when using the reference fuel. The piston deposit ratings obtained using the "F" rating method (Table 10) confirmed the similar deposition severity of test No. 2 and No. 7. However, intake port deposits increased significantly from one percent restriction in the test using reference fuel to 9% restriction in the test using DFM.

In the cases of cylinder liner scuffing, piston ring gap change, and cylinder liner wear (Tables 12, 13 and 14), all areas showed major increases over the test using reference fuel, and in most cases the wear rates reached levels comparable to those using REO 205 lubricant and reference fuel. Of major significance, the fire-ring gap increased to a level over twice that experienced with REO 205 and the reference fuel (Table 13, ring No. 1). This wear was the reason for increased crankcase pressure.

Fuel analyses (Table 15, dated 6 August 1973) accomplished after the completion of Test No. 7 showed no significant changes from the as-received condition. Lubricant analyses compared favorably with the test results using reference fuel (Table 16).

Overall, the use of DFM with REO 203 showed increased wear, but no increased deposit formation except for intake port plugging. Again, as in Test No. 6, piston ring surface deterioration was extreme, and the oil formulation appeared to be unable to inhibit the deterioration. Based on close examination of the engine, the remaining 14-hour cycle of the test might have been completed without major engine component failure.

TABLE 16. LUBRICANT ANALYSES

	F	EO 205	R	EO 203	
Properties	DFM	Ref no. 2 DF	DFM	Ref no. 2 DF	
	194 hrs	209.5 hrs	196 hrs	210 hrs	
		Viscosity, cs, 100	r <sub>F</sub>		
Start	126.7	126.7	121.6	121.6	
End	136.5	147.1	137.8	130.1	
Δ	9.8	20.4	16.2	8.5	
		Viscosity, cs, 210	°F		
Start	12.93	12.93	12.61	12.61	
End	13.74	14.42	13.73	13.33	
Δ	0.81	1.49	1.12	0.72	
		Total acid no.			
Start	3.0	3.0	3.6	3.6	
End	4.0	4.9	4.5	4.4	
Δ	1.0	1.9	0.9	0.8	
Total base no.					
Start	12.5	12.5	5.4	5.4	
End	10.9	12.2	3.8	5.6	
Δ	~1.6	0.3	~1.6	0.2	
		Carbon residue,	76		
Start	1.69	1.69	1.19	1.19	
End	2.55	2.56	1.85	1.66	
Δ	0.86	0.87	0.66	0.47	
		Sulfated ash, %			
Start	1.75	1.75	0.93	0.93	
End	2.17	2.27	1.03	1.08	
Δ	0.42	0.52	0.10	0.15	
	Me	tals, ppm, end of	test		
Iron	136	151	183	54	
Tin	33	0	0	0	
Lead	20	24	29	10	
Chromium	0	0	10	2	

## IV. CONCLUSIONS

- Marine Diesel Fuel (DFM, 1.2% sulfur) is judged incompatible for use with the current family
  of military two-cycle diesel engines.
- Use of DFM produces engine deterioration resulting in reduced performance, and possible increased maintenance, and reduction in engine life.
- The combination of high-ash lubricant (REO 205) and reference No. 2 diesel fuel produces borderline acceptable engine compatibility. Use of DFM with REO 205 produces major increases in ring sticking and ring face distress over an otherwise borderline acceptable performance.

The combination of low-ash lubricant (REO 203) and reference No. 2 diesel fuel produces the
desired high-level fuel-lubricant-engine compatibility; however, use of DFM with REO 203
produces significant increases in engine wear, ring face distress, and intake port plugging.

## V. RECOMMENDATIONS

As a result of recent meetings on interchangeability of diesel fuels, USAMC and allied nations have established a maximum allowable sulfur content of 0.7% for diesel fuel. Such a fuel (designated NATO F-54) should be evaluated in a similar manner as the tests reported herein. These tests would provide a set of data for fuels of intermediate sulfur content, which should help in defining the overall effects of fuel sulfur content on two-cycle diesel engine performance.

## **VI. STATUS OF PROGRAM**

During the period from September, 1972, through July, 1974, 13 6V53T engine/lubricant/fuel compatibility tests were conducted at USAFLRL. In tests 1 through 5, MIL-L-2104C lubricants REO 203 and REO 205 were run once each and REO 204 three times, using the 210-hr wheeled-vehicle test cycle with the reference No. 2 diesel fuel (0.42% natural sulfur). This work was reported in an interim report (AFLRL No. 29).

Tests 6 (REO 205) and 7 (REO 203), run on the 210-hr wheeled-vehicle cycle using DFM fuel (1.2% natural sulfur), are covered in this report.

Another interim report (AFLRL No. 37) covering tests 8, 9, and 10 is under preparation and will be published as soon as possible. Tests 8 (REO 203) and 9 (REO 205) were run on the 240-hr tracked-vehicle cycle using reference No. 2 diesel fuel. In test 10 another MIL-L-2104C lubricant (CCL-L-734) was run on the 210-hr wheeled-vehiclee cycle using reference No. 2 diesel fuel (0.42% natural sulfur).

Test 11 (REO 203) and tests 12 and 13 (both REO 205) were run on the 210-hr wheeled-vehicle cycle using a fuel with 0.70% natural sulfur which nominally met NATO F-54 requirements. The report of these tests is in preparation.

A final report will be issued covering all 13 6V53T engine compatibility tests in which the fuels, lubricants, and test cycle effects will be discussed. Also, this final report will tie in the results of the recent AVDS-1790-2A engine compatibility tests using the same MIL-L-2104C lubricants and reference No. 2 diesel fuel.

## VII. ACKNOWLEDGEMENT

The authors wish to acknowledge the assistance provided by Messrs. M.E. LePera and T.C. Bowen, project technical monitors at USA MERDC, STSFB-GL, and Mr. F.W. Schaekel of that office for his critical review, and to the engine and chemical laboratory staff at USAFLRL. Special recognition is made of Mr. D. C. Babcock, who took the special photographs, and Mr. J. L. Simpson who provided the necessary expert deposit rating assistance required in this program.

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# APPENDIX I

COMPATIBILITY TEST PROCEDURE WHEELED--VEHICLE TEST CYCLE 6V53T ENGINE

## COMPATIBILITY TEST PROCEDURE WHEELED-VEHICLE TEST CYCLE 6V53T ENGINE

## I. Pretest Inspection

A pretest inspection will be made to ascertain the condition of the engine prior to test. During the inspection, initial measurement of engine components listed in Table I will be made. Components found to be out of new or service limits will be replaced. The engine will be fitted with new connecting rod and main bearings, new cylinder liners, and new piston and piston ring sets. Parts such as the oil pan, cylinder heads, valves, cylinder block passages, and heat exchangers will be cleaned. Standardized build-up procedures specified by the appropriate Army Technical Manual/Engine Manufacturer (9, 10) will be used. During rebuild, the engine will be fitted with appropriate temperature and pressure sensing devices to measure the following:

## Temperatures:

Exhaust (before and after turbocharger)
Intake Air (before turbocharger)
Oil
Main gallery
Sump
Coolant (to and from engine)
Fuel (to engine)

## Pressures:

Exhaust (before and after turbocharger)
Intake Air (before and after turbocharger)
Airbox
Fuel (to injector pump)
Oil (Main gallery)
Crankcase

## Flows:

Fuel Blowby

## Table 1

## Wear Data Evaluation

The following engine components are gauged before and after the test. Data are evaluated on change during test.

Crankshaft end play.

Cylinder Bores--Parallel and perpendicular to crankshaft at the top, middle and bottom.

Piston--Parallel and perpendicular to wrist pin at the top and bottom.

Piston Rings--Gap and side clearance.

Piston Pins and Bushings.

Connecting Rod Bearings -- Position A, B and C.

Connecting Rod Journals.

Main Bearings -- Position A, B and C.

Main Bearing Journals.

Valve Clearance.

## Engine Ratings (Deposits/Condition)

CRC Diesel Rating Manual used to rate following components.

**Pistons** 

Rings

Ring Grooves

Lands

Skirt

Undercrown

Valves

Tappets, Cams and Rocker Arms

Cylinders

Bearings

Mai.

Connecting Rod

General engine -- rust and sludge

## II. Engine Break-In

An engine break-in will be conducted using the provided test lubricant and the following cycle:

Engine Speed, rpm	Load, Obs BHp	Time, min.
1800	30	15
2200	130	30
2500	200	30
2800	225	30

## III. Full Load Performance Determination --

Immediately following the break-in conduct a full load performance determination consisting of measuring engine torque, brake horsepower and brake specific fuel consumption at 200 rpm intervals between engine speeds of 1800 and 2800 rpm at full throttle. Change oil and filter after power curve.

## IV. Compatibility Endurance Test\*

The compatibility endurance test consists of repeating the endurance cycle for \* days without interruption for \* hours of engine operation. During test, the engine is to be operated using arctic anti-freeze as the coolant. Coolant temperatures must be maintained within ±5°F of the listed value; and, the idle temperature must be obtained within 10 minutes after starting each idle portion of the cycle. Coolant will be used to control the oil temperature which shall not exceed 250°F. The fuel is to be held within 5°F of the intake air (to turbocharger) temperature by use of an external water to fuel heat exchanger.

## Wheeled Vehicle-Endurance Cycle

Period	Time, hrs.	Load, %	Speed, rpm	Coolant Temp., °F
1	2	100	2800 ± 20	180
2	1	0	$650 \pm 25$	100
3	2	100	2800	180
4	1	0	650	100
5	2	100	2800	180
6	1	0	650	100
7	2	100	2800	180
8	1	0	650	100
9	2	100	2800	180
10	10		Shutdown	

<sup>\*</sup> Wheeled Vehicle Cycle = 15 days for 210 hours operation

- Notes: 1. Coolant temperature refers to jacket outlet. The thermostat is blocked open.
  - 2. Anti-Freeze used as coolant; MIL-A-11755C, A-1, 15 October 1971.
  - 2. Temperature reduced to 100°F within 10 minutes after idle runs start.
  - 4. Temperature limits, ± 5°F.
  - 5. Maximum allowable oil sump temperature, 250°F.
  - 6. No oil drains during wheeled-vehicle test cycle.
  - 7. Oil Samples:

Wheeled-Vehicle Cycle

- a. One-half pint sample every 14 hours -- 12 total
- b. 1 pint sample every 70 hours -- 3 total
- 8. Makeup oil; add to full mark on sight glass; weight oil in.
- 9. At the start of each day's operation during the wheeled vehicle cycle, run at idle for 5 minutes and then proceed directly to full rack power at 2800 RPM.
- 10. At end of day's operation, idle the engine for 5 minutes (without resetting jacket coolant controller), and take oil sample prior to shutdown.
- 11. Take complete log sheet readings at the end of the 2 hour power phases, and at the end of the idle phases.

Fresh test oil will be placed in the engine at the start of the endurance test; and there will be no forced oil additions. Make-up oil shall be added, as required only in one-quart increments during the shutdown periods. Records of all oil additions must be maintained. Oil samples are to be taken after each day of engine operation as shown in Table II. The sampling method consists of installing a tap in the oil cooler inlet or oil gallery and taking the sample just prior to shutdown. The sample line must be flushed before taking each sample (return all flush oil to the crankcase). Specific operating limits for the 6V53T are given in Table III for the wheeled-vehicle cycle.

New and Used Oil Sampling and Analysis Schedule-Wheeled Vehicle Cycle TABLE II.

Large volume sample (16 oz.) Small volume sample (8 oz.) Indicates analysis to be performed. Substitute for Cr for AVDS-1790 engine. X Indicates a....,

\* Substitute for Cr for AVD

\*\* Analyze for 6V53T only.

Table III. Wheeled Vehicle Test Cycle

# Operating Condition

# Limits; or settings, for

	Power Phas	e Idle Phase
Speed, rpm	2800 ± 20	$650 \pm 10$
Fuel Flow		
Typical, lb/min, (2 lb wt/time)	$2.07 \pm .07$	(use 2 oz)
Fuel/cycle, mm <sup>3</sup>	67 - 69	~
Revolutions/2 lb	$2680 \pm 50$	-
Time/2 lb	$0.965 \pm .035$	-
Obs BHp output	282 - 300	~
Jacket-out, °F	$180 \pm 2$	$100 \pm 2$
Coolant AT, F	8 - 12	2 - 3
Oil Sump, °F	250, max	~
Fuel Temp & Filter	$90 \pm 5$	-
Fuel Pressure, range	55 - 70	70 max
Compressor Suction, clean		
filter, inches water	6.0 max	-
Compressor Suction, dirty		
filter, inches water	12.0 max	-
Exhaust Back Pressure		
(after turbo), inches Hg	2.3 max	-
Crankcase Pressure	6.0 max	•
Oil Pressure, minimum	32 psi	5 <b>ps</b> i
Blowby Flow, CFH	1150 max	-
Test Duration		210 Hrs
Oil Drains		None
Oil Level Checks and Additions		Every 14 Hrs
Oil Samples		Every 14 Hrs
Airbox Inspection		None

## V. Full Load Performance Determination --

Immediately following the final endurance cycle a full load performance determination will be made. The determination is the same as in Sec. III.

## VI. Engine Inspection and Lubricant Deposit Ratings

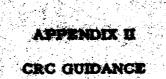
After completion of the final performance determination, the engine will be disassembled for inspection, measurements and deposit ratings. Measurement of the components listed in Table I will be made; and, other loaded components will be inspected reporting their condition. Engine parts will be rated for lubricant deposits and displayed for inspection by members of the Coordinating Research Council's, Motor Army Combat Engine Fuels and Lubricants Performance Group.

## VII. Test Oils

Lubricants to be tested are being furnished by U.S. Army Mobility Equipment Research and Development Cent r, Coating and Chemical Laboratory (C&CL).

## VIII. Test Fuel

Diesel fuel to be used is designated reference no. 2 diesel fuel, and it is approved by C&CL according to the requirements set forth in Section 4.1, Method 341, FTM Standard 791B.



## CRC GUIDANCE

During a meeting held 24 August 1972, the following test modifications were proposed by the CRC Army Combat Engine Fuels and Lubricants Group:

- 1. Engine Buildup Standardized buildup procedures specified by the appropriate Army Technical Manual/Engine Manufacturer should be used. It was the group's opinion that specialized buildup, such as would be used in strickly lubricant evaluation programs, could possibly cloud the original intent of the compatibility tests by imposing unrealistic engine environments for the oils. Review of the standardized procedures indicate that sufficient data for evaluating wear performance will be generated using these procedures. Only one exception to standard measurements will be made in that ring proudness will be measured using a simple V-block fixture.
- 2. Engine Rebuild Parts Engine components such as ring sets and bearings used for rebuilding a specific engine should be from a single supplier. Use of a single manufacturers parts will assist in limiting variation in results.
- 3. <u>Used Oil Analyses</u> The following analyses will be performed on 60,120,180, and 240 hour AVDS-1790 samples and 70, 140, and 210 hour 6V53T samples:

Analysis	Method
Viscosity (100°F & 210°F)	D445
TAN	D664
TBN	D2876
Insolubles (Pentane & Benzene)	D893 (Procedure A & B)
Gravity	D287
Flash Point	D92
Sulfated Ash	D872
IR	(to be determined)
Additive Content (Zn,Ca,Ba)	Atomic Absorption
Elemental Analysis	•
AVDS-1790 (Sn,Fe,Cu,Pb,Al & Mo)	Atomic Absorption
6V53T (Na, Fe, Cu, Pb, Al, Cr & Sr	

In the event abnormal results are obtained, additional analyses of the remaining samples will be performed.

- 4. Endurance Cycle AVDS 1790 Tests The 2 hours shutdown period is to be lengthened to 4-hours. It is felt that this would assist in control by allowing repetitive operation on a daily basis rather than the scheduled 22-hours cycle.
- 5. 6V53T Endurance Cycle Immediately following the last 2-hours of full load operation, the engine will be idled for 5-minutes prior to shutdown. This is to avoid a hot-shutdown which could over stress the engine.
- 6. 6V53T Coolant Arctic antifreeze meeting Specification MIL-A-11755C will be used as coolant. This will standardize the coolant and provide additional stressing of the lubricant.

# APPENDEX III

Test Number 6

Fuel: MIL-F-16884 (DFM)
Oil: REO 205, CCL-L-758
Engine No.: 6D5084-6

Test Hours: 194

Date Completed: 18 June 1973

TABLE 1 6V53T 6D5084-6 BUILD-UP ENGINE MEASUREMENTS

			Inches	
Measurements	Min.	Max.	Avg.	Specified Limits (1)
Crankshaft main bearing				
clearance	.0043	.0057	.0050	.0070 max.
Campbaft bearing alexander				
Camshaft bearing clearance Left cam	.0060	.0068	.0064	.0080 max.
Right cam	.0055	.0069	.0061	.0080 max.
Connecting rod bearing				
clearance	.0017	.0030	.0025	.0016~.0046
		· -		
Crankshaft end-play	.006	.006	.006	.004011
Oil pump				
Between rotors	.003	.003	.003	.004011
Outer rotor/housing	.0015	.0015	.0015	.0010035
Cylinder liner block bore				
Taper	.0000	.0005		.0015 max.
Out-of-round	.0000		.0007	.0015 max.
Inside diameter	4.3575	4.3591	4.3582	4.3595 max.
Cylinder liners (installed	.)			/2)
Taper	.0000	.0012	.0006	.002 max. $\binom{(2)}{(2)}$
Out-of-round	.0000			.003 max. (2)
Inside diameter	3.8756	3.8776	3.8766	3.8752-3.8767
Piston to liner fit	.0066	.0086	.0078	.00600095
Piston Diameter	3.8683	3.8692	3.8688	3.8669-3.8691
Rine winn				
Fire ring End gap	.30	.35	.33	.020046
Side clearance	.004	.004	.004	.003006
#1 Compression ring	0.24	0.40	225	
End gap Side clearance	.024 .007	.042	.035	.020046
Side Clediance	.007	.009	.008	.007010
#2 & #3 Compression rings				
End gap	.028	.044	.034	.020046
Side clearance	.006	.007	.007	.005008
Oil rings				
End gap	.018	.024	.020	.010025
Side clearance	.003	.010	.004	.00150055

<sup>(1)</sup> Limits on new parts unless maximum wear limit specified.(2) Wear limits with new liners in a used block.

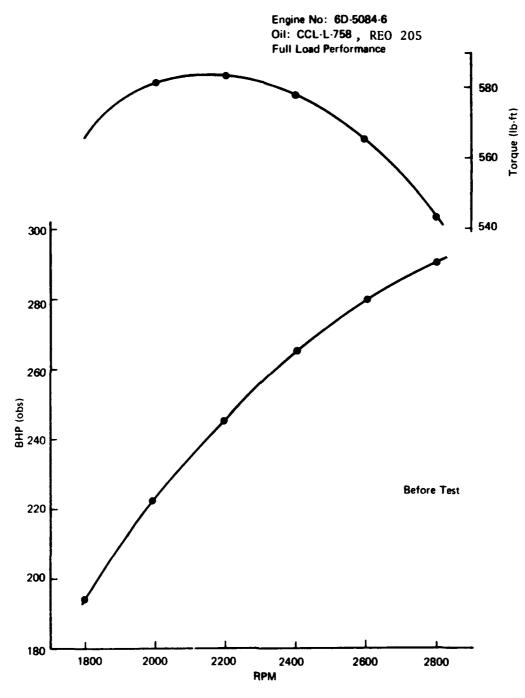


FIGURE 1

TABLE 2
SUMMARY OF OPERATING DATA

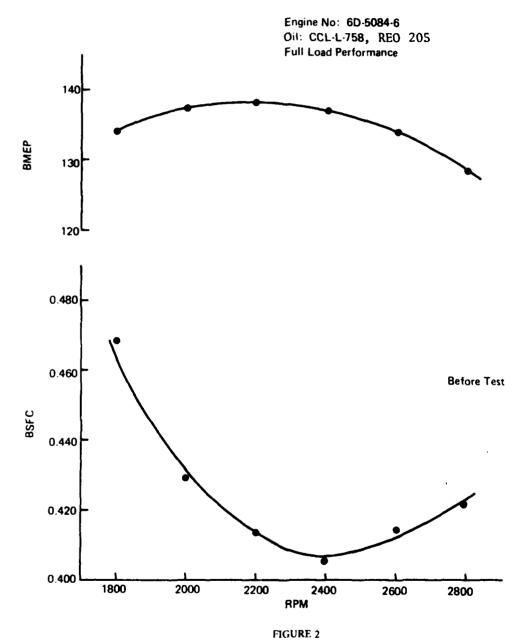
Engine Test No. 6D5084-6

Oil Code CCL-L-758 (REO 205)

Engine speed, rpm, 2800±20/ 650±10  Load, 1bs BHp, obs. (2800/4100) x load Fuel/cycle, mm³ Fuel rate, lb/min Oil consumption, (lb/hr Avg for 194 Hrs)  Temperatures, OF  Jacket-in Jacket-out 180±5/100±2 Inlet air (compressor) Airbox Lxhaust before turbo Exhaust after turbo Fuel at filter (secondary)  Pressures  Compressor suction, in. H20 Compressor discharge in. Hg Blower discharge (airbox), in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust before turbo, in. Hg Ex		Po	wer Mode		Idle Mode
650±10 Load, lbs BHp, obs. (2800/4100) x load Fuel/cycle, mm³ Fuel rate, lb/min Oil consumption, (lb/hr Avg for 194 Hrs)  Temperatures, OF  Jacket-in Jacket-out 180±5/100±2 Inlet air (compressor) Airbox Lxhaust before turbo Exhaust after turbo Fuel at filter (secondary)  Pressures  Compressor suction, in. H20 Compressor discharge in. Hg Exhaust before turbo, in. Hg Crankcase, dipstick tube in. H20 Exhaust after turbo, in. Hg Exhaust after turbo,		Min.	Max.	Avg.	Avg.
Load, lbs BHp, obs. (2800/4100) x load BHp, obs. (2800/4100) x load Fuel/cycle, mm <sup>3</sup> Fuel rate, lb/min Oil consumption, (lb/hr Avg for 194 Hrs)  Temperatures, OF  Jacket-in Jacket-out 180±5/100±2 Inlet air (compressor) Airbox Airbox Airbox BHower discharge in. Hg Blower discharge (airbox), in. Hg Crankcase, dipstick tube in. Hg Exhaust after turbo, in. Hg Exhaust after, psi Evaluate Isource, Iso		2800	2800	2800	650
BHp, obs. (2800/4100) x load Fuel/cycle, mm <sup>3</sup> Fuel rate, lb/min Oil consumption, (lb/hr Avg for 194 Hrs)  Temperatures, OF  Jacket-in Jacket-out 180±5/100±2 Inlet air (compressor) Airbox Lxhaust before turbo Exhaust after turbo Fuel at filter (secondary)  Pressures  Compressor discharge in. Hg Blower discharge (airbox), in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Crankcase, dipstick tube in. H <sub>2</sub> 0 Exhaust after turbo, in. Hg Exhaust after turbo, in. Hg Exhaust after turbo, i		3 <b>54</b>	428	421	-
Fuel/cycle, mm <sup>3</sup> Fuel rate, lb/min Oil consumption, (lb/hr Avg for 194 Hrs)  Temperatures, OF  Jacket-in Jacket-out 180±5/100±2 Jipe 182 Jipe 181 Jipe 182 Jipe 182 Jipe 183		242	292	288	-
Oil consumption, (lb/hr Avg for 194 Hrs) 0.52  Temperatures, OF  Jacket-in		66.2	68.1	67.3	-
Temperatures, OF  Jacket-in 168 171 170  Jacket-out 180±5/100±2 179 182 181 101  Oil sump 235 238 237 121  Inlet air (compressor) 90 101 95  Airbox 276 287 282  Lxhaust before turbo 1020 1060 1050  Exhaust after turbo 500 900 880  Fuel at filter (secondary) 84 91 89  Pressures  Compressor suction, in. H <sub>2</sub> 0 6.4 10.8 6.9  Compressor discharge in. Hg 22.8 24.7 23.8 -  Blower discharge (airbox), in. Hg 34.6 36.7 35.7 -  Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 -  Exhaust before turbo, in. Hg 24.5 26.3 25.7  Exhaust after turbo, in. Hg 1.9 2.2 2.1 -  Oil gallery, psi 40.5 43 41.7 26.8  Blowby flow, cfh at 29.92	Fuel rate, lb/min	1.96	2.08	2.06	
Temperatures, OF  Jacket-in					
Jacket-in       168       171       170         Jacket-out 180±5/100±2       179       182       181       101         Oil sump       235       238       237       121         Inlet air (compressor)       90       101       95         Airbox       276       287       282         Lxhaust before turbo       1020       1060       1050         Exhaust after turbo       500       900       880         Fuel at filter (secondary)       84       91       89         Pressures         Compressor suction, in. H <sub>2</sub> 0       6.4       10.8       6.9         Compressor discharge in. Hg       22.8       24.7       23.8       -         Blower discharge (airbox),       34.6       36.7       35.7       -         Crankcase, dipstick tube       3.9       4.7       4.2       -         Exhaust before turbo, in. Hg       24.5       26.3       25.7         Exhaust after turbo, in. Hg       1.9       2.2       2.1       -         Oil gallery, psi       40.5       43       41.7       26.8         Fuel at filter, psi       66       72       69.8	for 194 Hrs)	_	-	0.52	
Jacket-in       168       171       170         Jacket-out 180±5/100±2       179       182       181       101         Oil sump       235       238       237       121         Inlet air (compressor)       90       101       95         Airbox       276       287       282         Lxhaust before turbo       1020       1060       1050         Exhaust after turbo       500       900       880         Fuel at filter (secondary)       84       91       89         Pressures         Compressor suction, in. H <sub>2</sub> 0       6.4       10.8       6.9         Compressor discharge in. Hg       22.8       24.7       23.8       -         Blower discharge (airbox),       34.6       36.7       35.7       -         Crankcase, dipstick tube       3.9       4.7       4.2       -         Exhaust before turbo, in. Hg       24.5       26.3       25.7         Exhaust after turbo, in. Hg       1.9       2.2       2.1       -         Oil gallery, psi       40.5       43       41.7       26.8         Fuel at filter, psi       66       72       69.8	Temperatures, OF				
Jacket-out 180±5/100±2 179 182 181 101 Oil sump 235 238 237 121 Inlet air (compressor) 90 101 95 Airbox 276 287 282 Lxhaust before turbo 1020 1060 1050 Exhaust after turbo 500 900 880 Fuel at filter (secondary) 84 91 89  Pressures  Compressor suction, in. H <sub>2</sub> 0 6.4 10.8 6.9 Compressor discharge in. Hg 22.8 24.7 23.8 - Blower discharge (airbox), in. Hg 34.6 36.7 35.7 - Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 - Exhaust before turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Blowby flow, cfh at 29.92		168	171	170	
Oil sump					101
Inlet air (compressor)  Airbox  276  287  282  Lxhaust before turbo  Exhaust after turbo  Fuel at filter (secondary)  Pressures  Compressor suction, in. H <sub>2</sub> 0  Compressor discharge in. Hg  Blower discharge (airbox), in. Hg  Crankcase, dipstick tube in. H <sub>2</sub> 0  Exhaust before turbo, in. Hg  Oil gallery, psi  Fuel at filter, psi  Blowby flow, cfh at 29.92					
Airbox					
Exhaust after turbo 500 900 880 Fuel at filter (secondary) 84 91 89  Pressures  Compressor suction, in. H <sub>2</sub> 0 6.4 10.8 6.9 Compressor discharge in. Hg 22.8 24.7 23.8 - Blower discharge (airbox), in. Hg 34.6 36.7 35.7 -  Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 - Exhaust before turbo, in. Hg 24.5 26.3 25.7 Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92		276	287	282	
Pressures       Secondary	Lxhaust before turbo	1020	1060	1050	
Pressures  Compressor suction, in. H <sub>2</sub> 0 6.4 10.8 6.9  Compressor discharge in. Hg 22.8 24.7 23.8 -  Blower discharge (airbox),    in. Hg 34.6 36.7 35.7 -  Crankcase, dipstick tube    in. H <sub>2</sub> 0 3.9 4.7 4.2 -  Exhaust before turbo, in. Hg 24.5 26.3 25.7  Exhaust after turbo, in. Hg 1.9 2.2 2.1 -  Oil gallery, psi 40.5 43 41.7 26.8  Fuel at filter, psi 66 72 69.8	Exhaust after turbo	500	900	880	
Compressor suction, in. H <sub>2</sub> 0 6.4 10.8 6.9 Compressor discharge in. Hg 22.8 24.7 23.8 - Blower discharge (airbox), in. Hg 34.6 36.7 35.7 - Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 - Exhaust before turbo, in. Hg 24.5 26.3 25.7 Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92	Fuel at filter (secondary)	84	91	89	
Compressor discharge in. Hg 22.8 24.7 23.8 - Blower discharge (airbox), in. Hg 34.6 36.7 35.7 - Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 - Exhaust before turbo, in. Hg 24.5 26.3 25.7 Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8	Pressures				
Compressor discharge in. Hg	Compressor suction, in. H <sub>2</sub> 0	6.4	10.8	6.9	
in. Hg 34.6 36.7 35.7 - Crankcase, dipstick tube in. H <sub>2</sub> 0 3.9 4.7 4.2 - Exhaust before turbo, in. Hg 24.5 26.3 25.7 Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92	Compressor discharge in. Hg	22.8	24.7	23.8	-
Crankcase, dipstick tube in. H <sub>2</sub> 0  Exhaust before turbo, in. Hg  Oil gallery, psi Fuel at filter, psi  Crankcase, dipstick tube 3.9  4.7  4.2  - 26.3  25.7  1.9  2.2  2.1  - 40.5  41.7  26.8  Blowby flow, cfh at 29.92		24.6	26 7	25 7	
in. $H_20$ 3.9 4.7 4.2 - Exhaust before turbo, in. $Hg$ 24.5 26.3 25.7 Exhaust after turbo, in. $Hg$ 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8		34.0	30.7	35.7	_
Exhaust before turbo, in. Hg 24.5 26.3 25.7  Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8  Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92		3 0	47	4 2	_
Exhaust after turbo, in. Hg 1.9 2.2 2.1 - Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92					-
Oil gallery, psi 40.5 43 41.7 26.8 Fuel at filter, psi 66 72 69.8 Blowby flow, cfh at 29.92					-
Fuel at filter, psi 66 72 69.8  Blowby flow, cfh at 29.92					26.8
Blowby flow, cfh at 29.92					20.5
	<del>-</del>		. —		
in no ano iliye //OU MOU 870 🗢	in. Hg and 115°F	780	900	850	-

### Unscheduled Shutdowns

At 30 hours: Repaired flexible exhaust pipe, lost 20 minutes At 194 hours: Stopped due to power loss. Test terminated.



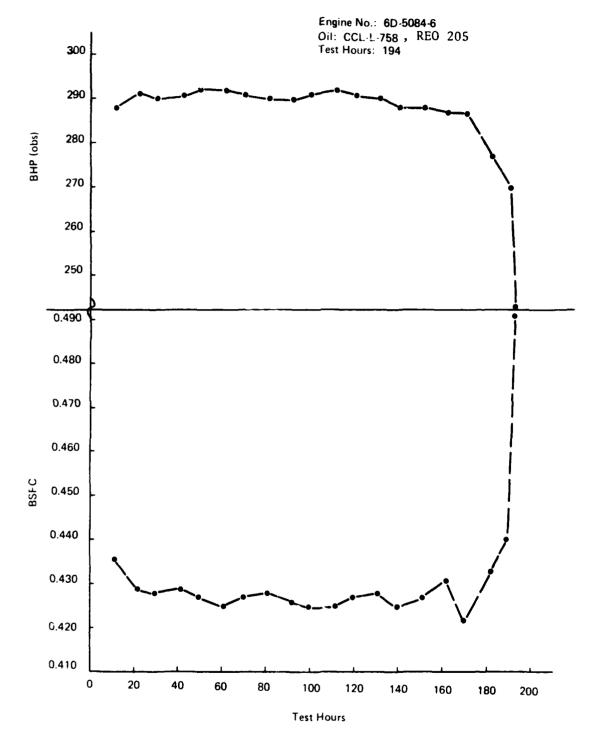
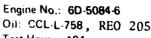


FIGURE 3



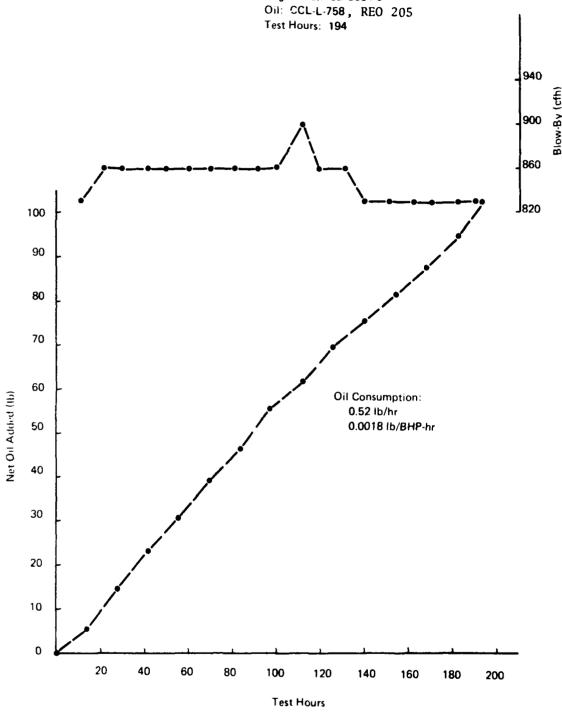


FIGURE 4

TABLE 3 LUBRICANT ANALYSES 6V53T - bD5084-6

Oil: CCL-L-758 REC 205

Property	New Oil	42	70	98	140	168	194
K. Vis, Cs, 100 K. Vis, Cs, 210 V-I	12.93 101	136.34 13.70 106	140.76 14.02 105	138.72 13.77 103	145.07 14.44 106	146.19 14.32 106	136.53 13.74 105
TAN (D664) TBN (D2896) Insolubles (D893),9 Pentane A		3.59 11.98 0.07	3.85 11.39		4.32		
Benzene A Pentane B Benzene B	0.04		0.08 0.06 0.24 0.18	0.10 0.06 0.20 0.15	0.06 0.29	0.07	0.10 0.09 0.33 0.24
Gravity <sup>O</sup> API (D287) Pour (D97), <sup>O</sup> F Carbon Residue	27.3 -5	N.D. N.D.	N.D.	N.D.	N.D.	N.D.	26.0 -5
(D524),% Flash Pt.(D92), OF S. Ash, % (D872)	1.69 460 1.75	450	460	460	455	460	2.55 455 2.17
Metals PPM, A.A.							
Na Cu Cr Pb Sn Fe Al I.R. Trace No.	212 0 0 6.5 0 7 0	188 5.5 0 10 31.5 65 0 246	200 5.5 0 15 41.5 78 2.5 247	175 6.5 0 16 37.5 76 3.5 248	213 6.0 0 18 38.5 101 3.5 249	218 5.8 0 18 34.5 108 4.0 250	218 5.8 0 20 33 136 3.5 251

N.D. - Not Determined

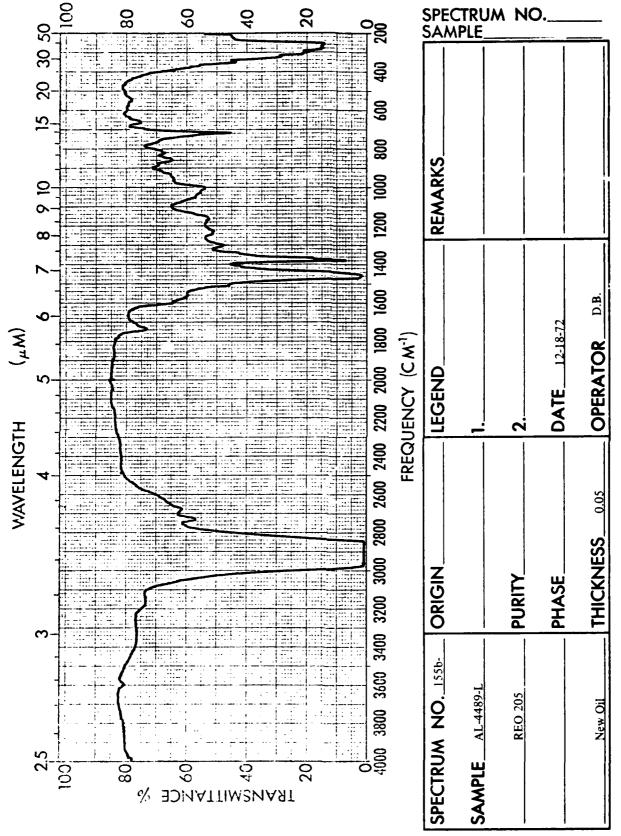
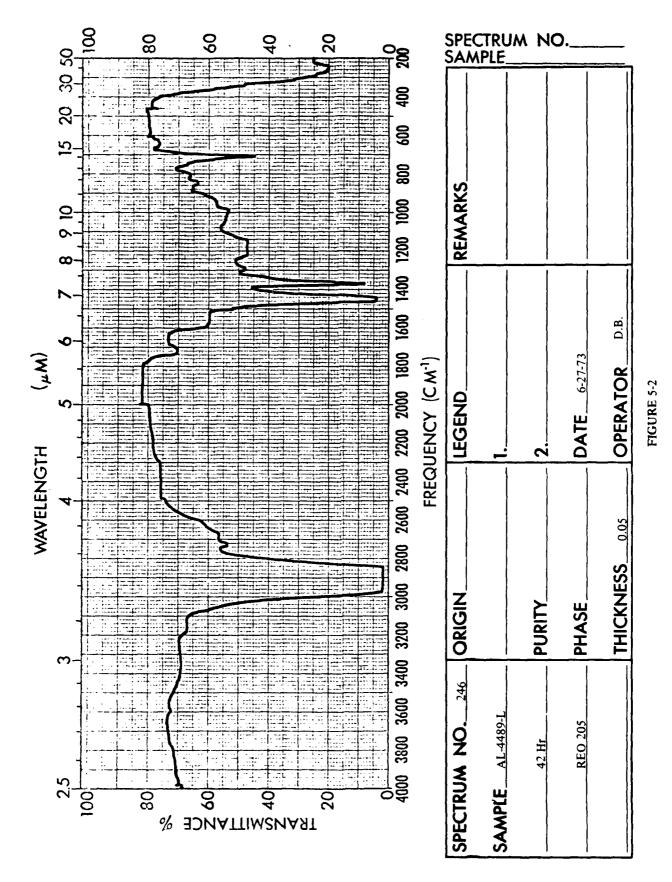


FIGURE 5-1



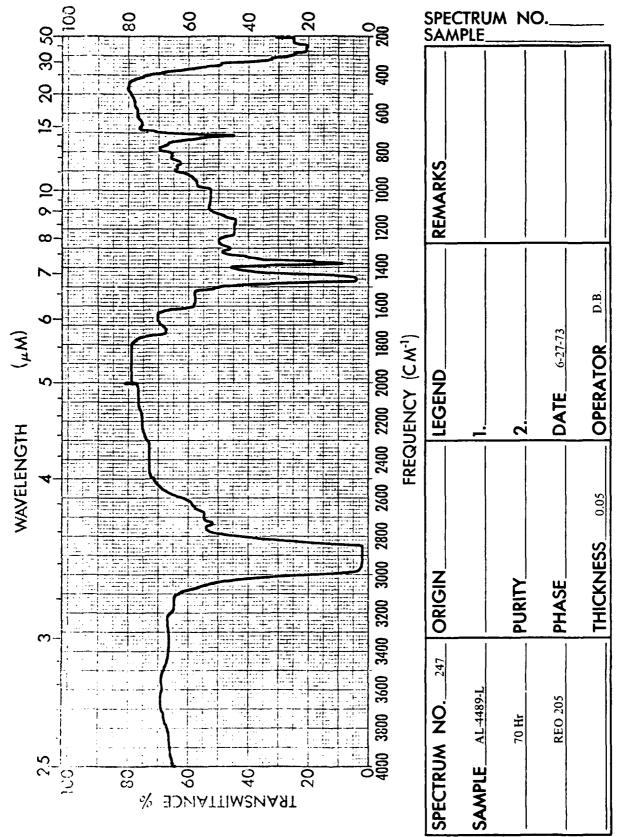


FIGURE 5-3

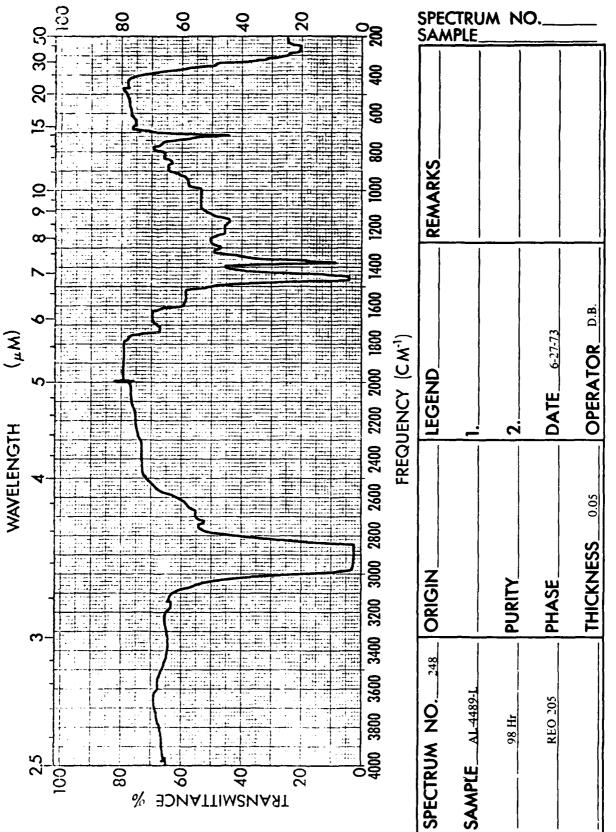


FIGURE 5-4

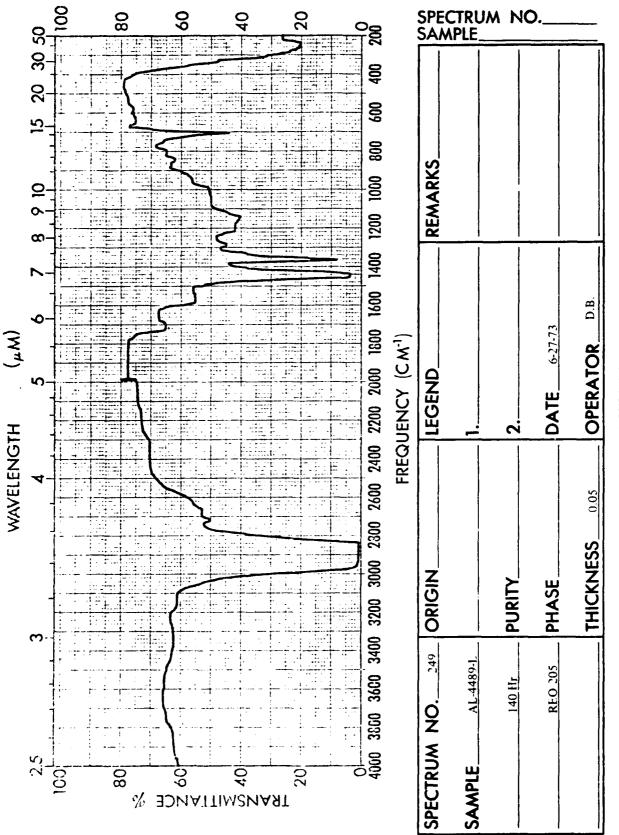


FIGURE 5-5

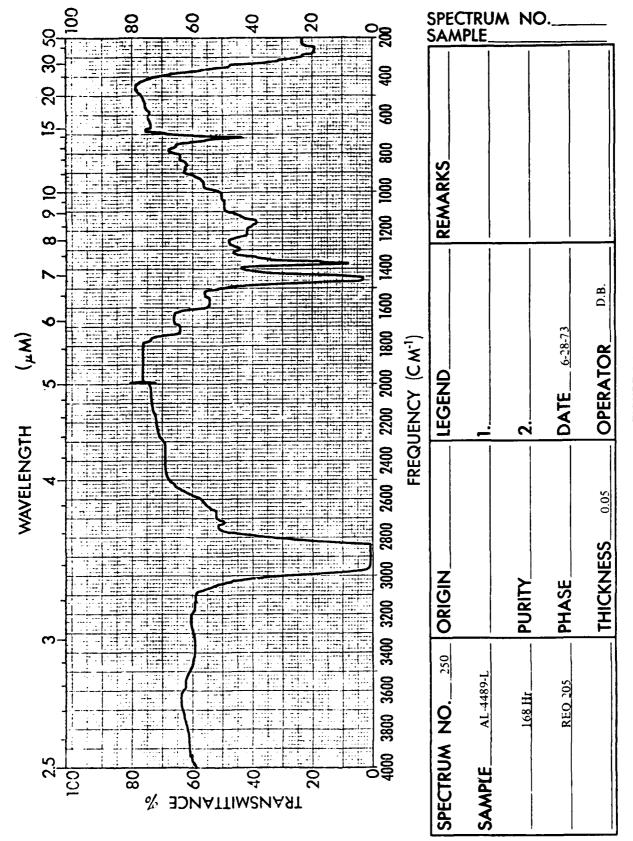
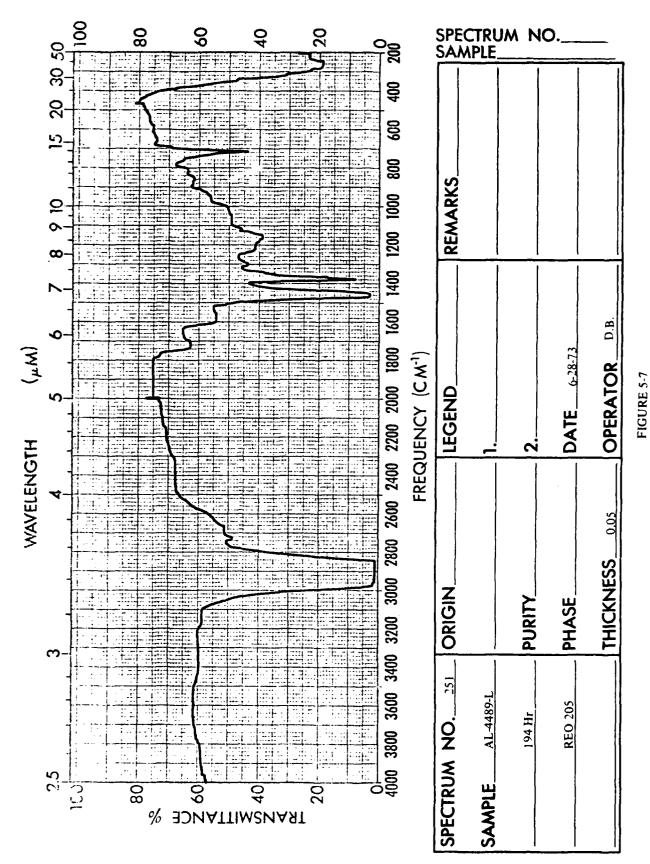


FIGURE 5-6



### WEAR MEASUREMENTS

(INCHES)

TABLE 4-1

### ENGINE NO. 6D5084-6

OIL: CCL-L-758, REO 205 Hrs. 194

			Pisto	n Ring (	Gap		
Piston No.	1	2	3	4	5	6	7
lL Before	0.033	0.035	0.037	0.044	0.024	0.020	0.020
After	Stuck	.038	.038	.046	.038	.028	.028
Change	-	.003	.001	.002	.014	.008	.008
2L Before	0.030	0.030	0.028	0.028	0.022	0.018	0.018
After	.038	.033	.030	.029	-	.028	.028
Change	.008	.003	.002	.001	-	.010	.010
3L Before	0.035	0.042	0.029	0.029	0.022	0.020	0.022
After	Stuck	Stuck	Sluggish	.032	.035	.030	.032
Change	-	-	- 33	.003	.013	.010	.010
lR Before	0.035	0.024	0.040	0.043	0.022	0.018	0.018
After	Stuck	.028	.044	.045	.033	.025	.025
Change	-	.004	.004	.002	.011	.007	.007
2R Before	0.032	0.041	0.044	0.028	0.022	0.018	0.018
After	.038	.043	.048	.030	.034	.025	.025
Change	.006	.002	.004	.002	.012	.007	.007
3R Before	0.035	0.040	0.028	0.029	0.020	0.018	0.018
After	.042	.043	.030	.032	.033	.025	.025
Change	.007	.003	.002	.003	.013	.007	.007

TABLE 4-2
ENGINE NO. 6D5084-6
OIL: CCL-L-758, REO 205
Hrs. 194

Cylinder Liner Perpendicular to Crankshaft Parallel to Crankshaft Middle Bottom Top Middle Cylinder No. Top **Bottom** lL Before 3.8777 3.8776 3.8776 3.8767 3.8777 3.8767 3.8786 3.8783 3.8775 3.8766 3.8775 3.8768 After .0009 .0007 -.0001 -.0001 -.0002 .0001 Change 2L Before 3.8761 3.8772 3.8764 3.8758 3.8768 3.8770 3.8777 3.8763 After 3.8768 3.8764 3.8767 3.8768 .0005 -.0001 .0006 -.0001 -.0002 Change .0007 3.8761 3L Before 3.8764 3.8771 3.8776 3.8775 3.8771 3.8780 3.8771 3.8764 3.8773 3.8775 3.8774 After .0016 .0000 .0003 -.0003 .0000 .0003 Change lR Before 3.8758 3.8765 3.8766 3.8759 3.8771 3.8765 After 3.8772 3.8768 3.8767 3.8769 3.8772 3.8765 .0001 .0010 .0001 .0000 Change .0014 .0u03 3.8756 3.8764 2R Before 3.8760 3.8770 3.8758 3.8766 3.8774 3.8759 3.8758 3.8772 After 3.8771 3.8767 .0011 .0004 .0001 .0002 .0008 .0001 Change 3.8773 3.8768 3.8762 3.8771 3.8768 3R Before 3.8761 3.8776 3.8779 3.8770 3.8770 3.8768 3.8770 After Change .0015 .0006 .0002 .0008 -.0001 .0000

### TABLE 4-3 ENGINE NO. 6D-5084-6 OIL: CCL-L-758, REO 205 Hrs. 194

Cylinder No.	Piston O.D.
lL Before	3.8692
After	3.8682
Change	.0010
2L Before	3.8692
After	3.8677
Change	.0015
3L Before	3.8690
After	3.8680
Change	.0010
lR Before	3.8685
After	3.8668
Change	.0017
2R Before	3.8683
After	3.8668
Change	.0015
3R Before	3.8685
After	3.8670
Change	.0015

### TABLE 4-4 ENGINE NO. 6D5084-6 OIL: CCL-L-758, REO 205 Hrs. 194

		Main Bear:	ing Journal	Main Be	earing
Nu	mber	AA	ВВ	F	R
1	Before	3.4992	3.4994	3.5048	3.5049
	After	3.4992	3.4994	3.5052	3.5052
	Change	.0000	.0000	.0004	.0003
2	Before	3.4995	3.4990	3.5038	3.5039
	After	3.4991	3.4989	3.5046	3.5045
	Change	.0004	.0001	.0008	.0006
3	Before	3.4992	3.4993	3.5047	3.5048
	After	3.4991	3.4992	3.5050	3.5048
	Change	.0001	.0001	.0003	.0000
4	Before	3.4993	3.4992	3.5038	3.5037
	After	3.4990	3.4990	3.5038	3.5038
	Change	.0003	.0002	.0000	.0001

			Crankshaft	Thrust Washer	S
Nu	mber		2	3	4
Α	Before	.1204	.1199	.1207	.1198
	After	.1204	.1199	.1207	.1198
	Change	.0000	.0000	.0000	.0000
В	Before	.1208	.1205	.1202	.1203
	After	.1208	.1204	.1200	.1203
	Change	.0000	.0001	.0002	.0000

### Exhaust Valve Clearances

Before Test,	All .024" to .026"	
Before Test (a) After Test	All .024" to .026"	
	(Except 2L = approx010"	<b>'</b> )

(a) - at 193 hours when fuel injectors changed.

TABLE 4-5
ENGINE NO. 6D5084-6
OIL: CCL-L-758, REO 205
Hrs. 194

	Rod Beari	ng Journal	Rod Be	earing
Cylinder No.	AA	BB	F	R
lL Before	2.7492	2.7495	2.7512	2.7515
After	2.7490	2.7490	2.7516	2.7516
Change	.0002	.0005	.0004	.0001
2L Before	2.7490	2.7490	2.7516	2.7518
After	2.7489	2.7489	2.7521	2.7520
Change	.0001	.0001	.0005	.0002
3L Before	2.7490	2.7492	2.7518	2.7520
After	2.7486	2.7489	2.7520	2.7523
Change	.0004	.0003	.0002	.0003
lR Before	2.7496	2.7493	2.7520	2.7515
After	2.7492	2.7492	2.7522	2.7520
Change	.0004	.0001	.0002	.0005
2R Before	2.7491	2.7490	2.7518	2.7518
After	2.7489	2.7487	2.7521	2.7520
Change	.0002	.0003	.0003	.0002
3R Before	2.7490	2.7490	2.7515	2.7515
After	2.7488	2.7486	2.7520	2.7515
Change	.0002	.0004	.0005	.0000

TABLE 5-1

RING STICKING

Date 9 July 1973	Observer J. Simpson
6D5084-6	CCL-L-758 (REO 205)
Engine Model 6V53T Serial No.	Fuel MIL-F-16884 (DFM) (AL-4669-F)Lubricant

	3R (A	Free	Free	Free	Free
-	2R	Free	Free	Free	Free
	H.	100% Hot Stuck	Free	Free	Free
Piston Number	3r (w)	100% Hot Stuck	270 <sup>o</sup> Hot Stuck	Cold Pinched	Free
	21	Free	Free	Free	Free
	11	Cold Pinched	Free	Free	Free
	Ring No.				

Indicate by letter—Free or Sluggish, or by number and letter—percent Pinched (cold stuck) or percent Hot stuck (Pages 6 and 7 of Manual).

(A) and (W) indicate average and worst from deposit standpoint.

the second se

### TABLE 5-2

RING DEPOSITS

, , , , , , , , ,	2 - 2 8 4 - 2
100AH - 100AH	1 1
70AH 30-7 100AH	30-7
*	
- 60-3 -	
- 70-3 -	
- 60-3 -	60-3

See pages 4, 36 and 37 of Manual. Areas previously rated for carbon, rate 0 for lacquer

\* Ring not removed from piston (see page 1).
(1) 20CH, 40BH, 40AH
(2) 30CH, 30BH, 40AH

TABLE 5-3

### RING FACE CONDITION

Date 9 July 1973 Observer J. Simpson Serial No. 6D5084-6 Lubricant CCL-L-758 (REO 205) Fuel MIL-F-16884 (DFM) (AL-4669-F) 6V53T Engine Model

			Cylinder Number	mber		
	11	31	3٢	1R	2R	38
First Ring (1)	(1) Normal Wear	Heavy Wear	Excessive Excessive Excessive Wear Wear	Excessive Wear	Excessive Wear	Excessive Wear
Second Ring (1)		<u></u>				
Third Ring						
Fourth Ring (1)						
Oil Ring Slots—% Open	100	100	100	100	100	100

Pages 1 and 2 and 59 through 65 of Manual.

(1) Chrome on ring faces is severely stressed. Individual rings displayed some or all of the following:

Storing, scuffing, ridging, cracking, checking, and pitting.

TABLE 5-4

### PISTON SURFACE DEPOSITS

Date 9 July 1973	Observer J. Simpson	
6D5084-6	CCL-L-758	(REO 205)
Serial No.	Lubricant	
Engine Model 6V53T	Fuel_MIL-F-16884 (DFM) (AL-4669-F)	

65 ASC 10csc 100-3 38 3.0 3.7 25DA 20CA 60BA 60BH 40AH 35AH 40BH **60AH** 40BH 55AH 15AH 15-6 40-4 20-3 3.5 3.8 100-3 10DA 55CA 35BSC 35DA 65ASC 2R 75BH 25AH SOAH 70BH 30AH 45BH 30-8 40AH 15-5 65AHC 80CA 15aSC 25BA 5DA 100-3 10CA 3.4 4.2 --N/A--80BH 20AH 45BH Piston Number 60ВН 40АН **40BH 60AH** 30CA 20CSH 30BA 20AHC 2-6 100-3 3.2 3.6 ಕ 30DS 60CA LOAA 20BH 80AH 60ВН 35AH 85BH 15AH 10BH 60AH 45-6 20-4 65AH 10-6 1 100-3 25BA 75AM 4.2 3.5 7 80AHC 15BA 5CA 20AH<sub>45-9</sub>35AH 35-5 70BH 50BH 50AH 30AH 25BH 100-3 20BA 80AA 40AHC 30CA 30BA 3.6 3.3 **60BH** 40AH **70BH** 30AH 40BH 60AH Combustion Chamber\* A Anti-Thrust က 8 Top A Thrust Under Head \* A Relief Areas \* A Skirts\* A Lands

Lacquer-Pages 4, 36, 37 of Manual.

\*Carbon and Ash: Use Volume Factor (Pages 5 and 40 through 47) Indicate H, M, or S (Page 5)

\* The letter A in last position designates an ash deposit.

1

TABLE 5-5

### PISTON RING GROOVE DEPOSITS

Date 9 July 1973 Observer J. Simpson Engine Model 6V53T Serial No. 6D5084-6 Fuel MIL-F-16884 (DFM) (AL-4669-FLubricant CCL-L-758

(REO 205)

							Cylinder Number	Number					
			11	<b>1</b> 2			ઝ		R.	7	2R	38	_
		CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO
	-	*		100AH	,	#	ı	*		10AH	90-7	15AH	85-7
Ton of Grows	2	40AH	60-3	20AH	80-4	*	1	1	100-7	25AH	75-5	65AH	35-5
	က	1	100-3	ł	100-3	*		ı				SAH	95-5
	4	1	100-3	L	100-3	40AH	60-5	١	100-4	1	100-4	1	100-5
	-	#	-	25	1	4	1	4	1	15	ı	5	1
Section of Group	2	80	1	75	ı	*	-	45	-	5/	ı	85	
	က	Н	١	10	ı	*	1	10	1	ST	-	25	1
	4	1	ı	2	-	10		1	1	1	ı	2	ı
	-	*		-	100-5	*	1	*	•	10 <b>A</b> H	90-5	,	100-4
Bottome of Green	2	20AH	80-4	•	100-3	*	ı	25AH	75-5	•	100-3	,	100-4
	က	•	100-3	-	100-3	*	•	1	100-4	•	100-3	'	100-4
	4	ı	100-3	1	100-3	1	100-4	•	100-4	-	100-3	ı	100-4
Drain Holes—% Blocked	p		0		0		0		0		0		0

Lacquer: Pages 4, 36, and 37

\*Carbon and Ash: Use Volume Factor (Pages 5 and 40 through 47) Indicate H, M, or S (Page 5)

tCarbon and Ash: Indicate Percent Filled and H, M, or S (Page 5)

\* Ring not removed from piston (see page 1) + % volume fill

. dan Pene baise.

Table 5-5a

	STANDARD COMPUTATION SHEET FOR PISTON RATING	
TEST PROCEDURE 6V53T	RATER J, Simpson DATE 9 July 1973	PIST(
TEST HOURS 194	LABORATORY TEST NUMBER 6D5084-6 (Test No. 6)	
TEST LABORATORY AFLRE	STAND NO. 5 ENGINE NO. 6D5084	ļ
LUBRICANT REG 205	FUEL MIL-P-16884 (DFM)	Q N

ON NO.

EST	TEST LABORATORY AFLRE	API.RI.															
UBA		HY THE	ST	STAND NO. 5		ENGIN	ENGINE NO.	6D5084									
	LUBRICANT	RE0 205	FUEL		7	884 (1	EM)	1	1	 		کا	10. 1 GR	OOVE.	NO. 1 GROOVE, VOLUME-%	1E-%	
												<u> </u>	PISTO	NWTD	PISTON WTD. RATING	ی	165.25
	├—		GRC	GROOVES							1	LANDS				3	E.P.
DEPOSIT TYPE	SIT DEPOSIT	NO. 1	NO. 2	-	NO. 3	ž	NO. 4	NO. 1		S	NO. 2	S.	5.3	ž	NO. 4	5	CROWN
		AREAS DEMENITAREAS	TAREA-% DEMER	TAREA.	% DEMERIT	AREA-%	DEMERIT	AREA-% DE	MERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA.K	SEMERIT
I	HC 1.00	**	80 80.00	1	1.00	1	1.00										
Ž	MHC 0.75																
	MC 0.50																
887	LC 0.25							60 1	15.00	2	17.50	40	10.00				
	VLC 0 15							40	6.00	30	4.50	9	9.00	20	3.00		
L	CARBON		80.00		1.00	1.	1.00	21.00	٥	22.	22.00	19	19.00	ď	3.00		
6	BL 0.100			09	6.00									45	4.50		
ö	DB1L 0.075					80	6.00										
<b>▼</b>	NL 0.050													35	1.75		
)	2 LAL 0.025															100	2.50
ځ	AL 0.010																
<u>«</u>	RL 0.001																
	LACQUER RATING		-		6.00	6.	6.00	-			<u> </u>	Ĺ	1	9	6.25	2.	2.50
CLEAN	AN 0																
2	ZONAL RATING							,									
<b>∀</b> 201	LOCATION FACTOR			ļ													
MEIG	WEIGHTED RATING		80.00	_	7.00	7.	7.00	21.00	0	22.00	00	19	19.00	6	9.25	1	2.50

WEIGHTED TOTAL DEPOSITS

\*\*Pinched ring not removed

Table 5-5b

PISTON NO. 2L.	NO. 1 GROOVE, VOLUME-%	PISTON WTD* RATING 187.13
STANDARD COMPUTATION SHEET FOR PISTON RATING RATER J. SIMPSON DATE 9 July 1973 LABORATORY TEST NUMBER 65084-6 (Test NO. 5) STAND NO. 5 ENGINE NO. 655084	FUEL MIL-P-16884 (DPM)	
TEST PROCEDURE 6V53T TEST HOURS 194 TEST LABORATORY AFIRE	LUBRICANT RED 205	

						GROOVES	VES							-	AND					
Disposit occoper	3	100												֭֭֭֭֭֭֭֭֓֞֜֜֜֜֜֜֜֡֡	202				<u>3</u>	JER.
	ີ ເ	. E	Š	-	Z	10. 2	Ž	NO. 3	Ŏ.	4.	- O		Ž	NO. 2	Ž	NO.3	Š	7.4	S.	CROMIN
	, ,		AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA-%	DEMERIT	AREA-%	AREAN DEMENTAREAN DEMENITAREAN	AREA.K	DEMERIT	AREA-%	DEMERIT	AREA.X	DEMERIT	AREAS	DEMERIT
HC 1.80			25	25.00	75	75.00	01	10.00	2	2.00										
MHC 0.75		ð.																		
MC 0.50	(C)	0																		
LC 0.25	1	2									70	17.50	50	12.50	25	6.25				
VLC 0.15	-	9									õ	4.50	20	7.50	65	9.75	35	5.25		
CARSON	至雪		25	25.00	75	5.00	10	10.00	7	2.00	22	22.00	20.	20.00		16.00	5.	5.25		
BL 0.100	-	8														$\prod$				
DB1L 0.075	0	75							9	4.5							45	3.38		
AL 0.0	0,	0.060													10	0.50	2	1.00		
LAL 0.0	0	0.025											L						3.	1
<b>₩</b>	<b>9</b>	0.010																	3	25.30
RL 0.0	_	100.0																		
LACOUER		<b></b>	i	-				!				1		!	6	0.50	4.	4.38	2.	2.50
CLEAN 0																				
ZONAL RATING	_	MG																		
LOCATION FACTOR		TOR					!													
WEIGHTED RATING		DMI	25.	25.00	, 25	2.00	់ ព	10.00	9	6.50	22	22.00	20.00	8	16	16.50	σ	9.63	1	2 50
0.000								1							;   	7	;	, , ,		3

Table 5-5c

	PISTON NO 3E			NO. 1 GROOVE, VOLUME-%	
STANDARD COMPUTATION SHEET FOR PISTON RATING	RATER J. Simpson DATE 9 July 1973	LABORATORY TEST NUMBER 605084-6 (Test No. 6)	STAND NO. 2 ENGINE NO. 6D5084	FUEL MIL-F-16884 (DFM)	
	TEST PROCEDURE 6V53T	TEST HOURS 194	TEST LABORATORY ACTION	LUBRICANT REO 205	

														PISIC		PISTON WID. RATING	_ _	80.71
				GRO	GROOVES							4	LANDS					INDER
TYPE	E FACTOR	NO. 1	2	NO. 2	ž	NO. 3	NO. 4	. 4	NO.	-	Ž	NO. 2	ž	NO. W	Š	+	5	CROWN
		AREAS DEMENTAREAS DEMENITAREAS DEMENIT AREAS DEMENIT	TAREA	X DEMERIT	AREA.X	DEMERIT	AREA.%	DEMERIT	AREA%	DEMERIT	AREA-%	TAREA % DEMERITAREA % DEMERITAREA % DEMERITAREA % DEMERITAREA % DEMERIT	AREA.X	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMERI
¥	C 1.00	**	*		**		10	10.00										
Ż	MHC 0.75																	
í.	MC 0.50		 															
884	LC 0.25								ž	200	9	15,00	y a	21 25	9	53 6		
	VLC 0.15								8	1.20	35	5.25	15	2.25	9	9.0		
	CARBON RATING						្ត	10.00	و ا	6.20	8	20.25	7	23.50	11.50	50		
8	L 0.100														۶	00		
8	DBrL 0.075						45	3.38			5	0.38			3	3		
83	L 0.050			L														
סח נפר	NL 0.025																8	2.50
<b>&gt;</b> ∧C	AL 0.010																	
<u>ا</u>	L 0.001																	
	LACQUER RATING						l m	3.38		į	] 。	0.38			] ~i	3.00	2.	2.50
CLEAN	W 0																	
¥02	ZONAL RATING																	
LOCA	LOCATION FACTOR																	
WEIG	WEIGHTED RATING				! !		13.	13.38	9	6.20	20.63	63	23	23.50	14.50	50	2.50	000

<sup>•</sup>WEIGHTED TOTAL DEPOSITS

\*\*Stuck rings - not removed

Table 5-5d

						ST	ANDA	AD COA	PUTA	STANDARD COMPUTATION SHEET FOR PISTON RATING	EET F	OR PIST	NO RV	TING					
# # #	TEST PROCEITEST HOURS	TEST PROCEDURE 194 TEST HOURS 194 TEST LABORATORY	<b>w</b>	V53T AFLRL		RAT LAB	RATER LABORATO STAND NO	RATER J. Simpson LABORATORY TEST NUMBER. STAND NO 5 ENGINE NO	ST NUM	ABER	DATE 6D5084 6D5084	DATE 9 July 1973 6D5084-6 (Test No. 6D5084	y 1973 est No	9	E .	PISTON NO		18	
1	LUBRICANT	ANT	REO 205			FUE	MI	FUEL MIL-F-16884 (DFM)	184 (DI	(M)						NO. 1 GROOVE, VOLUM	TOOVE	VOLU	₹
Į														į	L	PISTO	PISTON WTD. RATIN	RAT	Įž
					!	GROOVES	VES							۲	LANDS				$\vdash$
	TYPE	FACTOR	Š.	-	ž	NO. 2	ž	NO. 3	Ž	NO. 4	NO.	-	ž	NO. 2	ž	NO.3	ž	¥0.4	7
			AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	EA% DEWERITAREA% DEMERITAREA% DEMERIT AREA% DEWERITAREA% DEWERITAREA% DEWERITAREA% DEWERIT AREA% DEWERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA.X	DEMERIT	AREA.%	DEMERI	<del>∤ }</del>
	Ę	1.00	*		45	45.00	10	10.00	7	1.00									+-
	MHC	0.75																	┿
NO	<b>∑</b>	0.50																	+-
₽AA	ပ	0.25									9	15.00	80	20.00	40	10.00	45	11 25	+
<u> </u>	VIC VIC	0.15									40	6.00		3.00		9.00	Ĺ	6.00	+-
	₩ س	CARBON			45	45.00	21	10.00		1.00	12	21.00	23	23.00		19.00		17.25	+-
	<b>B</b>	0.100					10	1.00	20	2.00									+
	987	0.075																	+
83	4	0.060															15	0.75	<del>-</del>
סח	IAL I	0.025																	┿
<u>DA.</u>	₹ >>	0.010																	+-
1	اي	0.001																	┿
	5°	LACQUER						_			i					] ;	)	0.75	+
L																			_

AREA-% DEMERIT

CROWN

2.50

100

2.50

2.50

18.00

19.00

23.00

21.00

3.00

11.00

45.00

2.00

1.0

142.50

WEIGHTED TOTAL "EPOSITS

WEIGHTED RATING LOCATION FACTOR ZONAL RATING

CLEAN

\*\*Stuck ring not removed

Table 5-5e

1973 PISTON NO.			NO 1 GROOV	
RATER J. SImpson DATE 9 July 1973	LABORATORY TEST NUMBER 6D5084-6 (Test No. 6)	STAND NO. 5 ENGINE NO. 605084	FUFL MIL-F-16884 (DFM)	
TEST PROCEDURE 6053T	FEST HOURS 194	TEST LABORATORY AFTRE	LIRRICANT REO 205	

Ŋ	LUBRICANT		REO 205			FUEL	- }	MIL-F-16884 (DFM)	884 (D	FM)	1				Z	NO. 1 GROOVE, VOLUME-%	OOVE,	VOLUE	AE-%	l
							,	ļ	!				i	ļ	<u></u>	PISTO	PISTON WTD. RATING	RATIN	2	280.51
L						GROOVES	VES							۲	LANDS				3	UNDER-
30	DEPOSIT	PEPOSIT	NO.	1	NO. 2	). 2	ž	NO. 3	NO.	•	NO. 1	-	N	NO. 2	Ž	NO. 3	Ŏ.	4	5	CROWN
-			AREA-% DEMERIT AREA-% DE	JEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA-%	MERITAREAS DEMERIT AREAS DEMERITAREAS DEMERITAREAS DEMERITAREAS DEMERITAREAS DEMERITAREAS DEMERITAREAS DEMERIT	AREA-%	DEMERIT	AREA.%	DEMERIT	AREA.%	DEMER
	ž	1.00	15	15.00	75	75.00	15	15.00	1	1.00										
	MHC	0.75																		
NÓ	¥	0.50																		
88/	ಲ್	0.25									70	17.50	75	18.75	45	11.25				
/ጋ	VLC	0.15									30	4.50	25	3.75	20	7.50	15	2.25		
	32	CARBON	15.	15.00	75	75.00	15	15.00	1	1.00	22.	22.00		22.50	77	18.75				
	BL	0.100															10	1.00		
	ספיר	0.075							20	1.50					2	0.38	15	1.13		
83	AL	0.060															40	2.00		
no	LAL OUI	0.025															20	0.50	001	2.50
<b>DA</b>	₹	0.010																		
<u>1</u>	RL	0.001																		
	LAC RA	LACQUER RATING		ţ	i		i 		1	1.50	-	•		ļ.		0.38	4	4.63	2.	2.50
Ö	CLEAN	0																		
	ZONAL RATING	RATING																		
ت	OCATION	LOCATION FACTOR																		
*	EIGHTEL	WEIGHTED RATING	15.00	00	75.00	.00	15	15.00	2,	2.50	22.00	00	22.50	50	15	19.13	6.88	88	2.	2.50

WEIGHTED RATING 15.00
•WEIGHTED TOTAL DEPOSITS

Table 5-5f

TON RATING Y 1973 PISTON NO. 3R (Test No. 6)	NO. 1 GROOVE, VOLUME-%	PISTON WTD* RATING 193.26	] :	NO 2 NO 3 NO 4 CROWN	EMERIT AREA & DEMERIT AREA & DEMERIT AR				60 15.00 40 10.00	40 6.00 55 8.25 35 5.25	21.00 18.25 5.25	45 4.50	5 0.38 15 1.13	5 0.25	100 2.50	_		0.38 5.88 2.50				21.00 18.63 11.13 2.50
DATE 9 July 197 6D5084-6 (Test 6D5084	ſ			NO. 1	AREA & DEMERIT				40 10.00	00.6 09	19.00							-				19.00
Simpson TEST NUMBER ENGINE NO	MIL-F-16884 (DFM)			4.0N	AREA-% DEMERIT	2 2.00					2.00		20 1.50					1.50				3.50
J. Sir	MIL-P-		VES	NO. 3	AREA'S DEMERIT	25 25.00					25.00	20 2.00						2.00				27.00
STAND RATER_ LABORA STAND N	FUEL.		GROOVES	NO. 2	AREA-MOEMERIT	85 85.00					85.00											85.00
E 6053T 194 RY AFLRE	REO 205			NO. 1	AREA-% DEMERIT	5 5.00					5.00	5 0.50						0.50				5.50
TEST PROCEDURE 194 TEST HOURS 194 TEST LABORATORY	LUBRICANT				I YPE FACTOR	HC 1.88	MHC 0.75	MC 0.50	רכ 0.25	VLC 0.15	CARBON	BL 0.100	DB1L 0.075	AL 0.050	LAL 0.025	VLAL 0.010	RL 0.001	LACQUER	CLEAN 0	ZONAL RATING	LOCATION FACTOR	WEIGHTED RATING
	3		L_	6				NO	BAA	2				EB	סח	<b>∑</b> ∀′			٥		ئا	لځ

TABLE 5-6

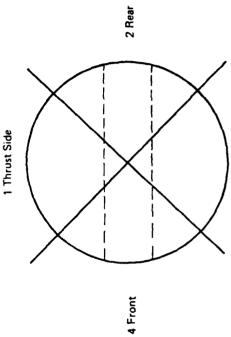
# PISTON GROOVE INSIDE DIAMETER-% RING SUPPORTING CARBON

Date 9 July 1973 Observer J. Simpson 6D5084-6 CCL-L-758 (REO 205) Serial No. MIL-F-16884 (DFM) (AL-4669-F) Engine Model 6V53T Fuel MIL-F-168

				Piston	Piston Number		
Piston Ring	Quadrant	11	21	31	18	2R	38
	1	a +	0	+ م	+ Q	0	0
•	2	a +	40	+ .a	+ q	0	0
-	3	ъ +	40	+ م	+ Q	0	0
	4	а +	20	+ q	+ Q	0	0
	-	15	09	+ Q	0	09	09
ć	2	20	7.0	+ Q	25	90	100
7	3	75	70	+ Q	10	100	100
	4	100	70	+ ,a	80	10	10

+ Ring not removed from piston (see page 1)

a - cold pinch b - hot stuck



3 Anti-Thrust Side

TABLE 5-7

PISTON SURFACE CONDITION

Date 9 July 1973	Observer J. Simpson
605084-6	CCL-L-758 (REO 205)
Serial No.	Lubricant
Engine Model 6V53T	MIL-F-16884 (DFM) (AL-469-F)

			Piston Number	Vumber		
	16	21	3L	18	2R	38
Top Land				1		
			T PUI TON	•		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
Skirt	20% Scuffing	1% Scored 5% Light Scuffing	10% Scuffing	20% Scuffing	58	20%
				7	500	SCULLING
Piston Pin						
			Normal-+			

Pages 1 through 2 and 59 through 65 of Manual.

TABLE 5-8

### **VALVE DEPOSITS**

9 July 1973 Date 9 July 197 Observer J. Simpson (REO 205) 6D5084-6 CCL-L-758 Lubricant Serial No. (AL-4669-F) Engine Model 6V53T Fuel MIL-F-16884 (DFM)

\*Carbon and Ash: Use Volume Factor Technique (Pages 5 and 40 through 47 of Manual). tUse Chart, Page 21—Indicate H, M, or S (Page 5). Lacquer: Pages 4, 36 and 37.

(1) The head of one exhaust valve was broken (burned ?)

TABLE 5-9

**EXHAUST VALVE SURFACE CONDITIONS** 

Engine Model 6V53T		Serial No.	6D5084-6		Date	Date 9 July 1973
Fuel MIL-F-16884 (DFM)		Lubricant	CCL-L-758 (REO 205)	REO 205)	Observer	Observer J. Simpson
(AL-4669-F)	F)					
	11	21	31	18	2R	38
Freeness in Guide	Free	Free	Free	Free	Free	Free
Head	 	(1)	Normal			
Face	(2)	(1)	(2)	(2)	(2)	(2)
Seat		8	Normal			
Stem			Normal			
Тір			Normal			

See Pages 1, 2, 16 through 23, and 54 through 65 of Manual.

- (1) Broken or burned one valve only(2) Evidence of leakage

TABLE 5-10

TAPPETS, CAMS, AND ROCKER ARMS

Engine Model 6V5	6V53T		Serial No.	19	6D5084-6		Date 9 Tuly 1973	1973
Fuel MIL-F-16	5884 (E	MIL-F-16884 (DFM)	1 1		CCL-L-758		Observer J.	Observer J. Simpson
	<b>4</b> )	L-4669-F	_		(REO 205)	_		
					Cylinder Number	100		
			11	21	31	18	2R	38
Tannat Danasis		-NI						
apper Deposit		EXH.			Not Bated			
		2			Not Bated			
Tappet Surface Condition	tion	INT						
		ЕХН			Not Rated			1 1 1 1
Cam Lobes	seqo				Normal		Normal	
	i	INI						
	<u>a</u>	EXH			Not Rated			
		INT						
Hocker Arms	guinsua	ЕХН			Not Rated		11	
	3	L L						
	Share	EXH	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		A +CN			
					ווטר זומים			

Lacquer: Pages 4, 36 and 37 of Manual See Pages 1, 2, 16 through 23, and 54 through 65.

TABLE 5-11

# CYLINDER LINERS AND CYLINDER HEADS

		changes.
	% Lacquer 25 10 25 30 35 35 28 28	3Rand humidity changes.
9 July 1973 J. Simpson	% Total       % Glazed       %         7.5       55       4.5         4.5       45       45         25       40       35         17.5       35       5         5       60       44         13       44       44         1Percent scuffed in compression ring travel area.	2R
5084-6 Date 9 J -L-758 Observer J (REO 205) Cy, inder Liner Scuffing Percent of Total Ring Travel Area (1)	% Total Area Scuffed 7.5 4.5 25 17.5 17.5 13 (1) Percent scuffed in	1R due to
GG CCI	Percent Scuffed  ust Anti-Thrust  3 12  6 3  6 3  6 25  0 25  0 15  3 13	31d
Serial NoLubricant	Percent Thrust 3	2L
6V53T 16884 (DFM) (AL-4669-F)	Percent Port Restriction	1L
Engine Model 6V53T Fuel MIJF-16884	Cylinder Number Res 1L 2L 3L 3R 2R 3R Average	MC SC SC SC Not rated, too m

Carbon and Ash: Use Volume Factor Pages 5 and 40 through 47 Indicate H, M, or S
Lacquer: Use Pages 4, 36, and 37
For Surface Condition—See Pages 1, 2, 16 through 23 and 54 through 65

TABLE 5-12

SURFACE CONDITION

Engine Model 6V53T Fuei MIL-F-16884 (A)	3T 84 (DFM) (AL-4669-F)	Serial No.	0	6D5084-6 CL-L-758 (REO 205)		Date 9 July 1973 Observer J. Simpsion	ly 1973 Simpsion
Bearing No.	-	2	8	4			
Main – Bearing		-NORMAL W	-NORMAL WITH LIGHT PITTING-	PITTING-			
-Journal	1	NORMAL,	/AI				
Rod-Bearing	11	2L	31.	1R	2R	3R	
-Journal				NORMAL WEAR			
Piston Pin				NORMAL			
Bushing				NORMAL			

Note surface condition. See pages 1, 2, 16 through 23 and 54 through 65 of Manual.

TABLE 5-13

## SLUDGE DEPOSITS

Engine Fuel	Engine Model 5V53T Serial No. 6I	Serial No. 6D5084-6 Date 9 July 1973 Lubricant CCL-L-758 Observer J. Simpson
1	-699	(REO 205)
		Rating
	Connecting Rods	Clean
	Rocker Arm Covers	0.5
	Top Deck	0.5
	Push Rod Covers	1
	Push Rod Chamber	-
	Timing Gear Cover	•
	Oil Pan	0.5

See pages 5 and 40 to 47 of Manual.

Oil Screen

Clean

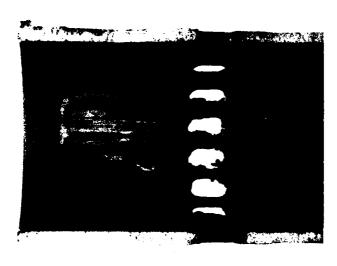
Use CRC Volume Factor Technique.

Figure 6-1

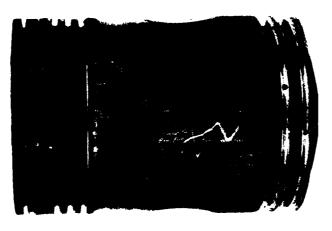
TEST 6

194 HRS

OIL CODE CCL-L-758 (REO 205)



3 Right Thrust A



3 Right Thrust A

Figure 6-2

TEST 6

194 HRS

OIL CODE CCL-L-758 (REO 205)

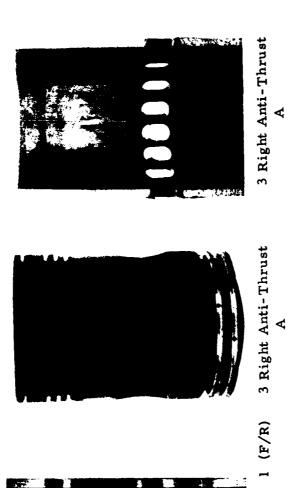
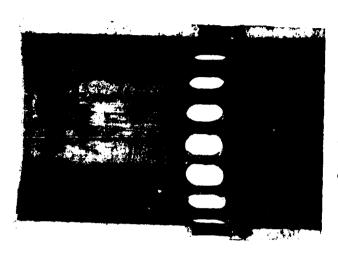


Figure 6-3

TEST 6

194 HRS

OIL CODE CCL-L-758 (REO 205)



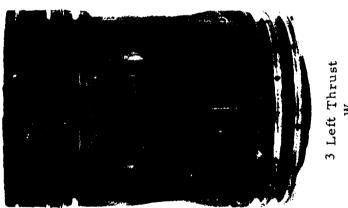
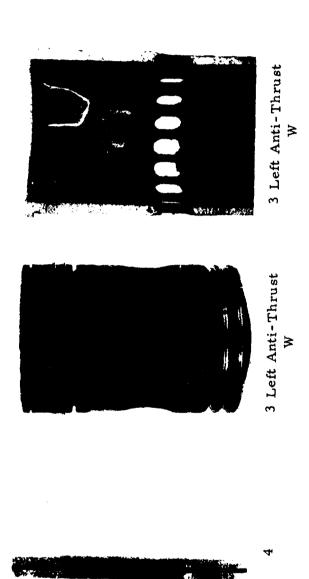


Figure 6-4

TEST 6

194 HRS

OIL CODE CCL-L-758 (REO 205)



## APPENDIX IV

Test Number 7 Fuel: MIL-F-16884 (DFM)

OII: REO 203, CCL-L-759

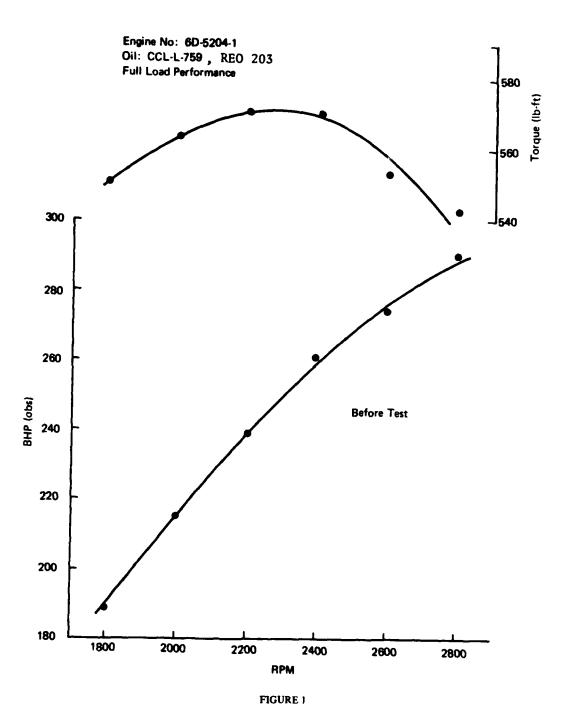
Engine No.: 6D5204-1 Test Hours: 196

Date Completed: 6 August 1973

TABLE 1 6V53T 6D5204-1 BUILD-UP ENGINE MEASUREMENTS

			Inches	(1)
Measurements	Min.	Max.	Avg.	Specified Limits (1)
Crankshaft main bearing				
clearance	.0035	.0050	.0043	.0070 max.
Camshaft bearing clearance				
Left cam	.0051	.0064	.0057	.0080 max.
Right cam	.0055	. 0065	.0062	.0080 max.
Connecting rod bearing				
clearance	.0018	.0037	.0025	.00160046
Crankshaft end-play	.007	.007	.007	.004011
Oil pump				
Between rotors	.005	.005	.005	.004011
Outer rotor/housing	.0025	.0025	.0025	.0010035
Cylinder liner block bore				
Taper	.0000	.0004	.0002	.0015 max.
Out-of-round	.0000	.0005	.0002	.0015 max.
Inside diameter	4.3564	4.3578	4.3571	4.3595 max.
Cylinder liners (installed)				002 may (2)
Taper	.0000	.0016	.0005	.002 max. (2)
Out-of-round	.0000	.0014	.0004	
Inside diameter	3.8755	3.8776	3.8764	3.8752-3.8767
Piston to liner fit	.0072	.0088	.0079	.00600095
Piston Diameter	3.8679	3.8690	3.8686	3.8669-3.8691
Fire ring				
End gap	.024	.038	.031	.020046
Side clearance	.003	.004	.004	.003006
#1 Compression ring				
End gap	.024	.032	.028	.020046
Side clearance	.007	.008	.008	.007010
#2 & #3 Compression rings				
End gap	.025	.040	.031	.020046
Side clearance	.006	.007	.006	.005008
Oil rings				
End gap	.018	.026	.022	.010025
Side clearance	.002	.004	.003	.00150055

<sup>(1)</sup> Limits on new parts unless maximum wear limit specified.
(2) Wear limits with new liners in a used block.



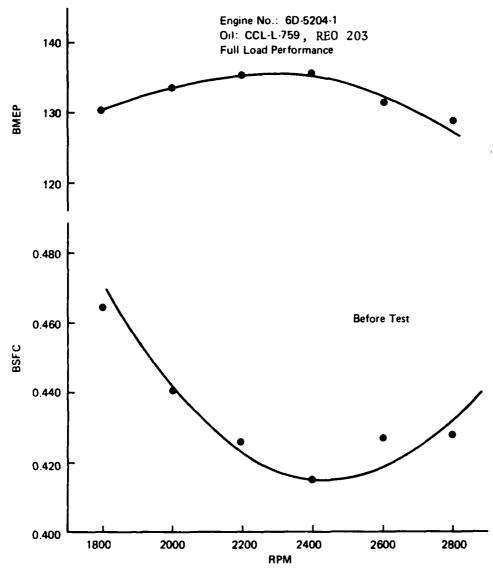


FIGURE 2

TABLE 2
SUMMARY OF OPERATING DATA

Engine Test No. 6D5204-1

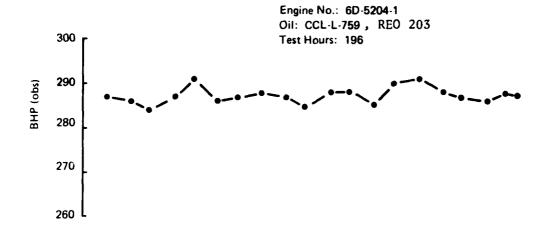
Oil Code CCL-L-759 REO 203

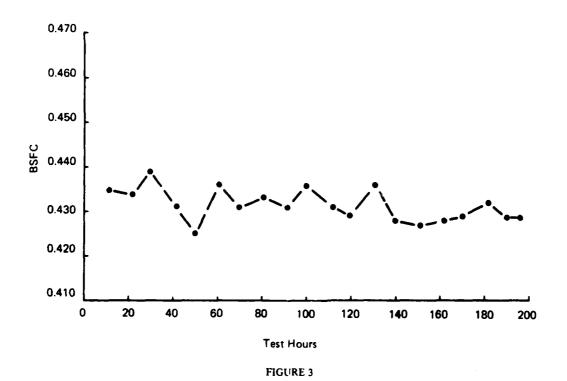
	Po	wer Mode		Idle Mode
	Min.	Max.	Avg.	Avg.
Engine speed, rpm, 2800±20/				
650±10	2800	2800	2800	640
Load, lbs.	412	428	421 .	
BHp, obs. (2800.4100) x load	281	292	287	
Fuel cycle, mm <sup>3</sup> ,	65.9	68.4	67.6	
Fuel rate, lb/min	2.0	1 2.09	2.06	
Oil consumption, (lb/hr Avg				
for 196 Hrs)			0.52	
Temperatures, OF				
Jacket-in	168	174	170	
Jacket-out 180±5/100±2	170	186	181	98
Oil sump	232	240	236	121
Inlet air (compressor)	78	114	99	
Airbox	272	300	290	
Exhaust before turbo	1020	1100	1070	
Exhaust after turbo	860	930	900	
Fuel at filter (secondary)	85	100	90	
Pressures				
Compressor suction, in. H <sub>2</sub> 0	6.6	12.9	8.0	
Compressor discharge in. Hg	21.0	24.3	23.0	
Blower discharge (airbox), in.Hg	34.0		35.8	
Crankcase, dipstick tube in. H <sub>2</sub> 0	4.9		5.4	
Exhaust before turbo, in. Hg	23.8		25.0	
Exhaust after turbo, in. Hg	1.6	2.9	1.9	
Oil gallery, psi	40.0	41.5		26
Fuel at filter, psi	67.5	71.0	69.6	
Blowby flow, cfh at 29.92 in.				
Hg and 115°F	830	1030	910	

## Unscheduled Shutdowns

At 137 Hrs: Repair auxiliary oil cooler water line - Lost 30 minutes.

At 196 Hrs: Test terminated due to high crankcase pressure.





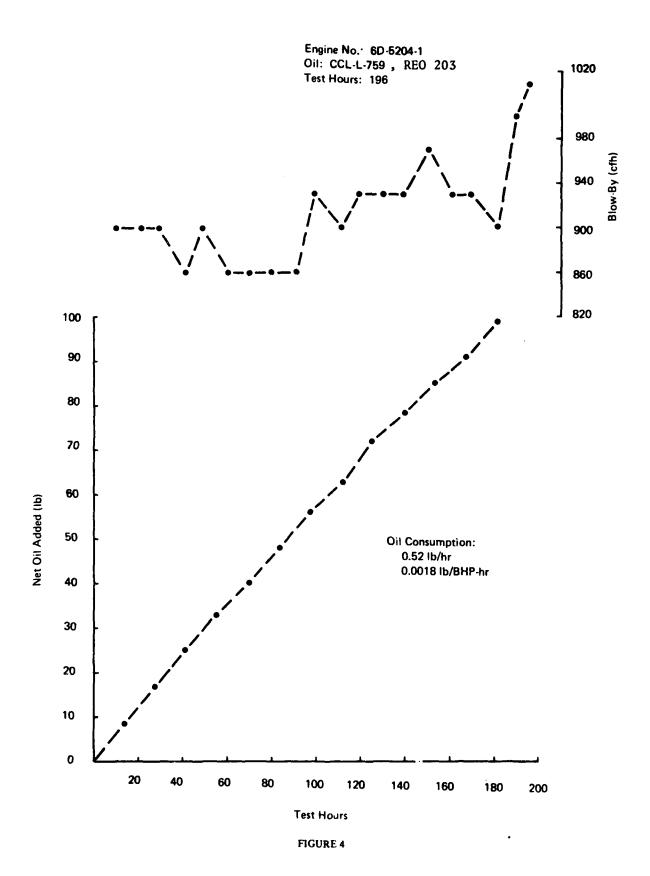
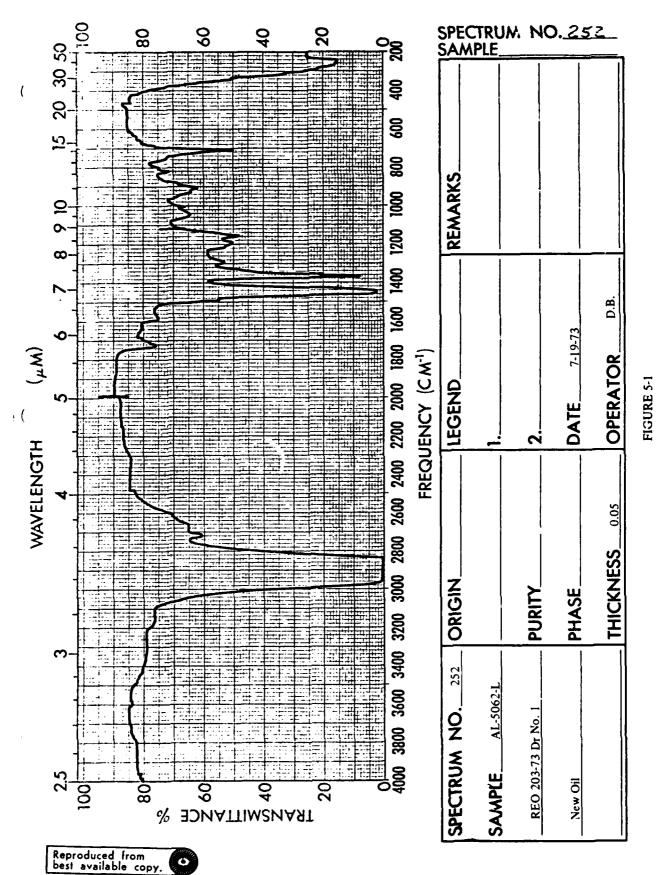


TABLE 3
LUBRICANT ANALYSES
6V53T - 6D5204-1
Oil: CCL-L-759 REO 203

	New	t		Test H	lours		
Property	<u> 0il</u>	42	70	98	140	168	196
K. Vis, Cs, 100	121.60	128.76	132.52	134.69	136.07	137.37	137.83
K. Vis, Cs, 210	12.61	13.00	13.24	13.38	13.54	13.58	137.03
V-I	94	103	102	102	103	103	104
TAN (D664)	3.6	3.01	4.22	3.59	4.48	3.69	4.48
TBN (D2896)	5.4	2.66	3.68	2.95	3.84		3.84
Insolubles (D893). 9	<b>s</b>						
Pentane A	N.D.		0.04	0.05	0.05	0.06	0.05
Benzene A	N.D.	0.03	0.03	0.05	0.04	0.05	0.05
Pentane B	N.D.	0.14	0.21	0.30	0.22	0.43	0.32
Benzene B	N.D.	0.24	0.18	0.28	0.17	0.35	0.26
Gravity OAPI (D287)	27.5	N.D.	N.D.	N.D.	N.D.	N.D.	26.4
Pour (D97), OF	<b>-</b> 5	N.D.	N.D.	N.D.	N.D.	N.D.	+5
Carbon Residue							
(D524),%	1.19		N.D.	N.D.	N.D.	N.D.	1.85
Flash Pt. (D92), F	465	473	476	470	477	470	479
S. Ash (D872),%	0.93	1.05	1.06	1.11	1.05	1.13	1.03
Metals PPM, A.A.							
Na	40	45	48	50	50	51	52
Cu	N.D.	8	9	9	8	10	10
Cr	N.D.	4	6	8	8	9	10
Pb	N.D.	28	26	26	29	27	29
Sn	N.D.	0	0	0	0.	0	0
Fe	N.D.	74	102	132	155	163	183
Al	N.D.	0	0	0	0	0	0
I.R. Trace No.	252	308	309	310	311	312	313

N.D. - Not Determined



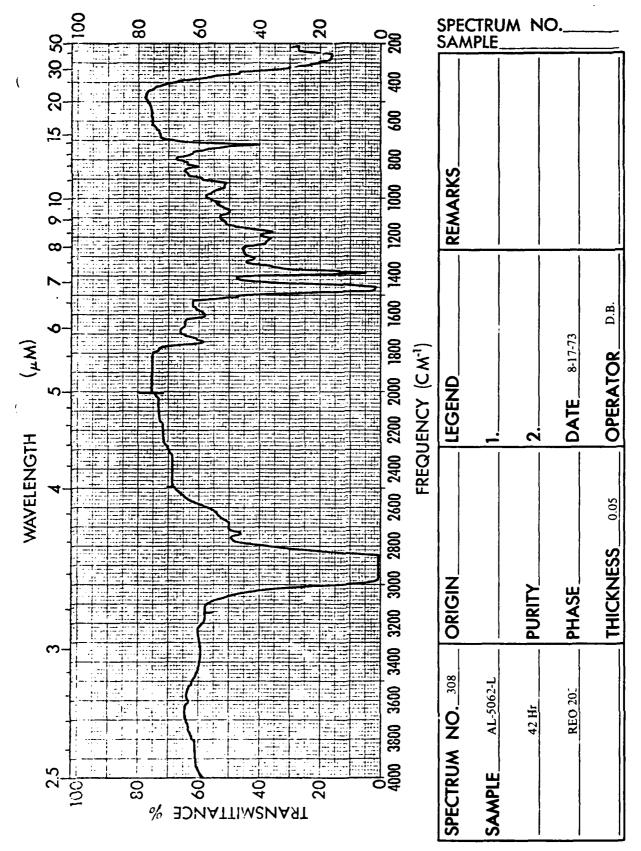


FIGURE 5-2

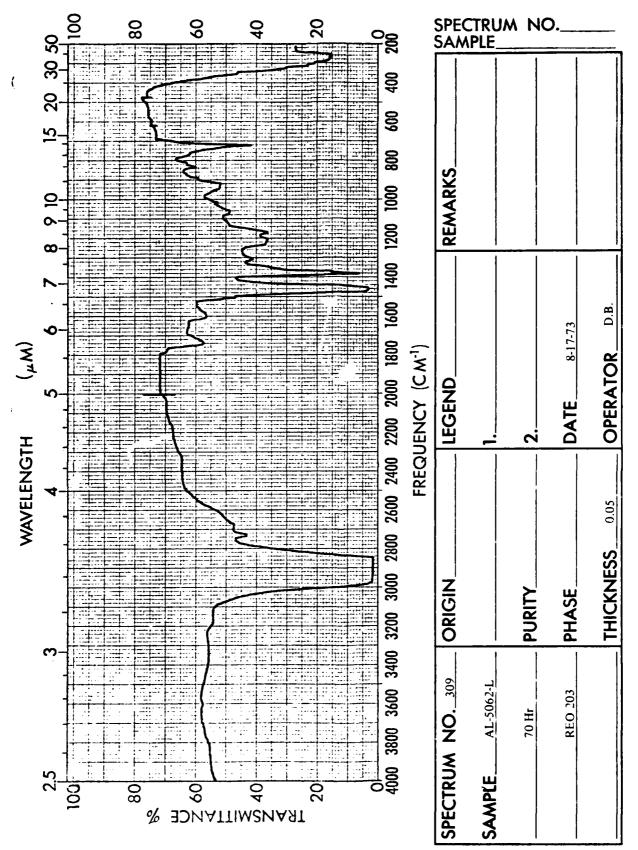


FIGURE 5-3

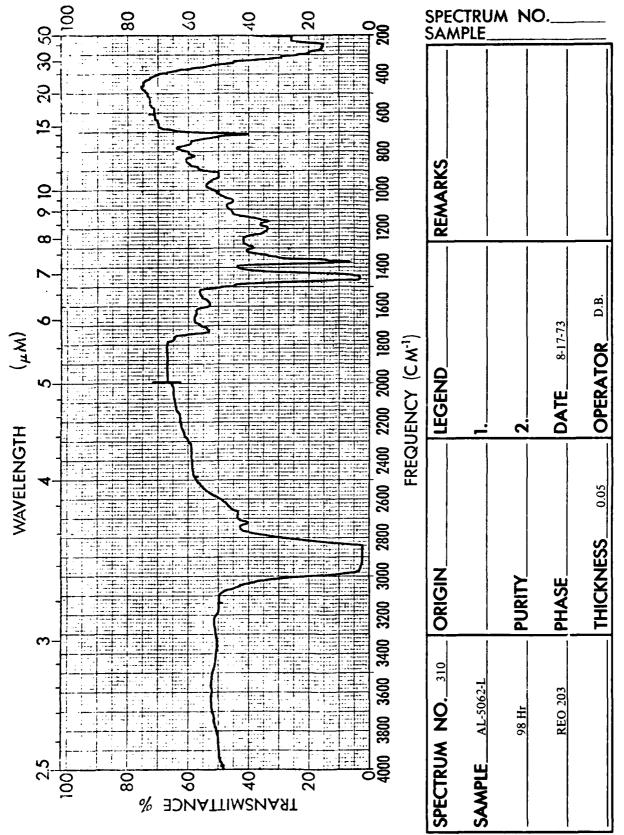


FIGURE 5-4

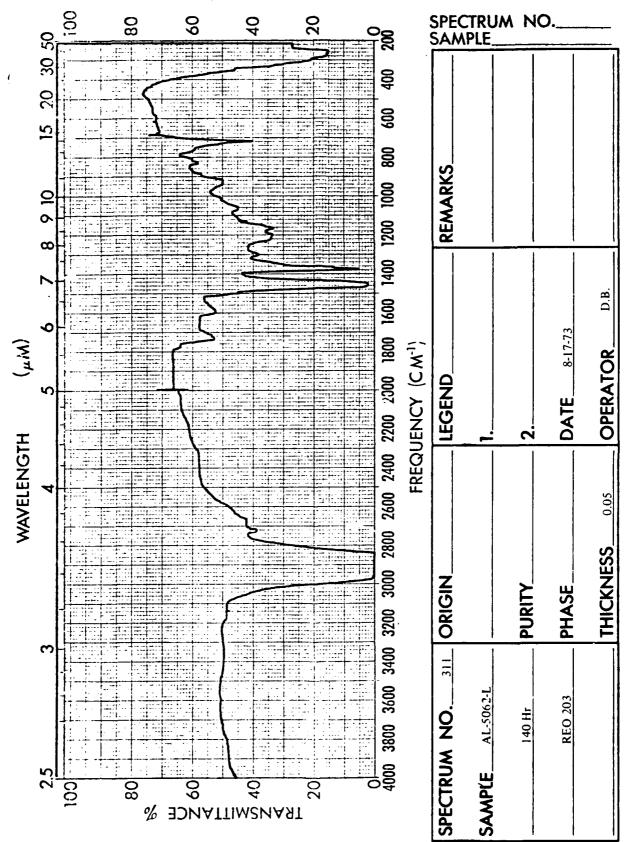
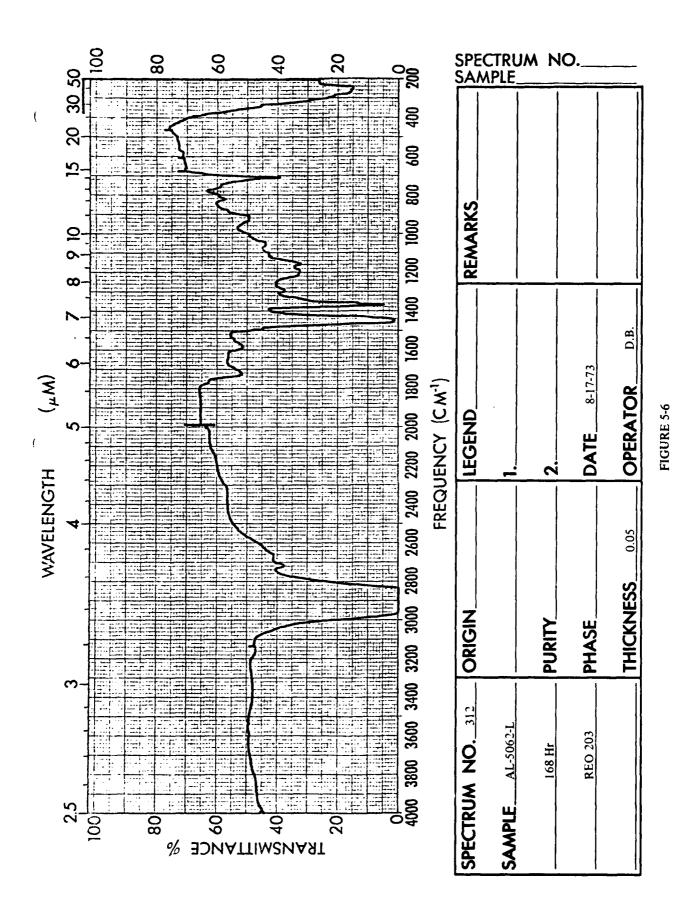


FIGURE 5-5



oz

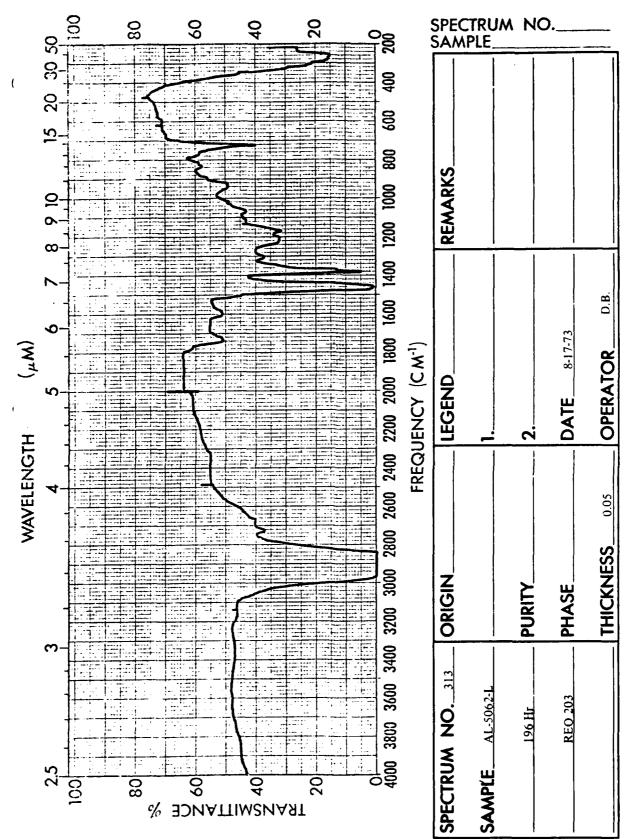


FIGURE 5-7

## WEAR MEASUREMENTS

(INCHES)

## TABLE 4-1

ENGINE NUMBER 6D 5204-1 OIL: CCL-L-759, REO 203

Hrs: 196

			Pi	ston Rin	g Gap		
Piston No.	1	2	3	4	5	6	7
lL Before	0.038	0.030	0.032	0.032	0.022	0.022	0.022
After	.049	.034	.034	.035	.030	.035	.033
Change	.011	.004	.002	.003	.008	.013	.011
2L Before	0.024	0.024	0.030	0.028	0.026	0.024	0.024
After	.045	.028	.033	.032	.042	.034	.034
Change	.021	.004	.003	.004	.016	.010	.010
3L Before	0.028	0.027	0.025	0.025	0.024	0.018	0.020
After	.042	.032	.031	.030	.038	.034	.030
Change	.014	.005	.006	.005	.014	.016	.010
lR Before	0.035	0.028	0.025	0.040	0.025	0.020	0.020
After	.042	.032	.030	.044	.040	.035	.033
Change	.007	.004	.005	.004	.015	.015	.013
2R Before	0.030	0.029	0.036	0.029	0.022	0.024	0.024
After	.044	.034	.041	.035	_	.040	.040
Change	.014	.005	.005	.006	_	.016	.016
3R Before	0.028	0.032	0.033	0.034	0.024	0.018	0.018
After	.040	0.035	.035	.036	.035	.028	.028
Change	.012	.003	.002	.002	.011	.010	.010

## TABLE 4-2 ENGINE NO. 6D5204-1 OIL: CCL-L-759, REO 203 Hrs: 196

				Cylind	er Liner		
		Perpendic	ular to	Crankshaft	Paralle.	l to Cra	nkshaft
Cyli	nder No	Top	Middle	Bottom	Top	Middle	Bottom
		<del></del>					
lL B	efore	3.8760	3.8770	3.8771	3.8768	3.8769	3.8767
A:	fter	3.8779	3.8782	3.8780	3.8772	3.8772	3.8763
C	hange	.0019	.0012	.0009	.0004	.0003	0004
	_						
2L B	efore	3.8762	3.8771	3.8767	3.8766	3.8770	3.8766
A:	fter	3.8781	3.8784	3.8776	3.8769	3.8773	3.8768
C	hange	.0019	.0013	.0009	.0003	.0003	.0002
3L B	efore	3.8765	3.8769	3.8763	3.8761	3.8767	3.8761
A:	fter	3.8798	3.8777	3.8771	3.8768	3.8774	3.8759
C	hange	.0033	.0008	.0008	.0007	.0007	0002
1R B	efore	3.8755	3.8765	3.8764	3.8760	3.8760	3.8762
A:	fter	3.8791	3.8775	3.8771	3.8765	3.8771	3.8766
C	hange	.0036	.0010	.0007	.0005	.0011	.0004
2R B	efore	3.8774	3.8775	3.8767	3.8760	3.8776	3.8775
A:	fter	3.8790	3.8785	3.8771	3.8775	3.8781	3.8780
C	hange	.0016	.0010	.0004	.0015	.0005	.0005
							_
	efore	3.8761	3.8770	3.8755	3.8751	3.8770	3.8768
	fter	3.8775	3.8782	3.8762	3.8770	3.8775	3.8769
C	hange	.0014	.0012	.0007	.0009	.0005	.0001

## TABLE 4-3 ENGINE NO. 6D-5204-1 OIL: CCL-L-759, REO 203 Hrs. 196

Cylinder No.	Piston O. D.
lL Before	3.8685
After	3.8679
Change	.0006
2L Before	3.8690
After	3.8675
Change	.0015
3L Before	3.8689
After	3.8672
Change	.0017
lR Before	3.8679
After	3.8669
Change	.0010
2R Before	3.8688
After	3.8674
Change	.0014
3R Before	3.8682
After	3.8669
Change	.0013

TABLE 4-4
ENGINE NO. 6D-5204-1
OIL: CCL-L-759, REO 203

Hrs.	196
nrs.	100

		Main Beari	ng Journal	Main Be	aring
Nu	mber	AA	BB	F	R
1	Before	3.4996	3.4995	3.5032	3.5031
	After	3.4992	3.4993	3.5033	3.5031
	Change	.0004	.0002	.0001	.0000
2	Before	3.4995	3.4995	3.5039	3.5038
	After	3.4992	3.4993	3.5039	3.5041
	Change	.0003	.0002	.0000	.0003
3	Before	3.4994	3.4993	3.5043	3.5042
	After	3.4992	3.4992	3.5044	3.5048
	Change	.0002	.0001	.0001	.0006
4	Before	3.4997	3.4995	3.5040	3.5042
-	After	3.4994	3.4994	3.5048	3.5048
	Change	.0003	.0001	.0008	.0006
			Crankshaft I	hrust Washe	rs
Nii	mber	1	2	3	4

		Crankshaft Thrust Washers					
Nu	mber	1	2	3	4		
A	Before	.1202	.1208	.1201	.1209		
	After	.1202	.1208	.1200	.1204		
	Change	.0000	.0000	.0001	.0005		
В	Before	.1198	.1202	.1207	.1205		
	After	.1186	.1202	.1207	.1204		
	Change	.0012	.0000	.0000	.0001		

## Exhaust Valve Clearances

Before Test - All .024" to .026" After Test - Not Recorded

TABLE 4-5
ENGINE NO. 6D-5204-1
OIL: CCL-L-759, REO 203
Hrs. 196

	Rod Bearin	g Journal	Rod Be	aring
Cylinder No.	AA	ВВ	F	R
lL Before	2.7497	2.7495	2.7518	2.7519
After	2.7496	2.7495	2.7518	2.7522
Change	.0001	.0000	.0000	.0003
2L Before	2.7492	2.7491	2.7522	2.7528
After	2.7493	2.7493	2.7529	2.7532
Change	0001	0002	.0007	.0004
3L Before	2.7492	2.7493	2.7522	2.7523
After	2.7492	2.7493	2.7529	2.7530
Change	.0000	.0000	.0007	.0007
lR Before	2.7495	2.7494	2.7515	2.7515
After	2.7491	2.7494	2.7523	2.7523
Change	.0004	.0000	.0008	.0008
2R Before	2.7493	2.7493	2.7518	2.7511
After	2.7492	2,7492	2.7525	2.7520
Change	.0001	.0001	.0007	.0009
3R Before	2.7490	2.7493	2.7514	2.7520
After	2.7490	2.7491	2.7519	2.7525
Change	.0000	.0002	.0005	.0005
···		•		

TABLE 5-1

## RING STICKING

Date 20 Aug 1973	Observer J. Simpson
B	Lubricant CCL-L-759 (REO 203)
	Fuel MIL-F-16884 (DFM)

	3R (W)	Free	Free	Free	Free
•	2R	Free	Free	Free	Free
	18	Free	Free	Free	Free
Piston Number	31	Free	Free	Free	Free
	2L (A)	Free	Free	Free	Free
	11	Free	Free	Free	Free
	Ring No.	<b>-</b> _	2	ю	4

Indicate by letter—Free or Sluggish, or by number and letter—percent Pinched (cold stuck) or percent Hot stuck (Pages 6 and 7 of Manual).

(A) and (W) denote average and worst from deposit standpoint.

TABLE 5-2

## RING DEPOSITS

Date 20 Aug 1973	Observer J. Simpson
. 6D-5204-1	1 CCL-L-759 (REO 203)
Serial No.	_Lubricant
del 6V53T	IL-F-16884 (DFM)

Cylin	Cylinder Number	jr.	11	_1	2F		<b>٦</b> ٤	_	_	18	2R	or	38	æ
			CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO
Piston	Тор	1	55AH	45-6	30AH	70-5	20 <b>AH</b>	9-08	SAH	80-6	10AH	(3)	,	100-6
Ring		2	60AH	40-6	45AH	(2)	75AH	<b>\$=</b> 8 <del>1</del>	30AH	65-3	65AH	30-6	,	25-4 70-6
		3	-	100-4	•	25-5 35-3	•	100-5	,	80-3		100-5		90-3
		4	•	90-3	-	40-3	1	75-3	ı	65-3	,	80-4		5=5 60-4
	<u> </u>	-	SOAH	5-7	95AH	2-7	100AH	-	80AH	20-9	70AH	30-6	100AH	
		2	15BH 85AH	-	45BH 55AH	_	20BH 80AH	ı	45BH 55AH	1	80BH 20AH	1	50BH 50AH	,
	,	3	100AH	_	100AH	_	100AH	1	100AH	•	100AH	ı	100AH	ı
		4	-	100-8	70AH	30-8	-	100-7	ı	100-6	50 <b>A</b> H	20-7	,	100-7
	Bottom	1	-	(1)	exe _	(I) excessive	~ e	(1)	-	70-4	SAH	$\Xi$		(1)
		2	-	(1)	_	5-9	~	20-3	-	5-5	5AH	30-3	'	20-3
		3	-	20-3	,	60-3	-	60-3	_	60-3	_	100-3	-	80-3
		4	<u> </u>	50-4	,	30-3		70-3	-	60-3	,	70-3	,	60-4

See pages 4, 36 and 37 of Manual. Areas previously rated for carbon, rate 0 for lacquer

Worn thru chrome 20-9, 20-4, 15-2 40-6, 30-5, 20-4 365 TABLE 5-3

RING FACE CONDITION

20 Aug 1973	Observer J. Simpson
rial No. 6D-5204-1	Junicant CCL-L-759 (REG 203)
Engine Model 6V53T	Fuel MIL-F-16884

			Cylinder Number	mber		
	7	ಸ	31	<b>1</b> R	2R	38
First Ring	(2) Mod Otherwise Satis- factory	HeavyWear HeavyWearExcessive HeavyPart PartChip- &(1) Lt Wear (2) Lpping ing(2) Lt (2) ModAmt	HeavyWear PartChip- ing(2)Lt	HeavyWear & (1) Lt (2) ModAmt	Excessive Wear	Excessive
Second Ring	(2) Mod Otherwise Satisfac- tory	(1) Wed vy per 1 de post 1	(4) Lt Heavy Chrome Wear	Excessive Chrome displacem (4) Beave	Excessive (5) Heavy of the Enry (3) Heavy	(5) Lt (4) Mod PartChin
Third Ring	(4) Mod	(4) Mod Blowby Streaks	(4) Mod	(5) Mod (5) Heav (4) Heavy (4) Mod	(5) Heavy (4) Mod	(4) Heavy
Fourth Ring	(5) Lt (4) Mod	(4) Mod	(4) Mod	(5) Mod (4) Mod	(5) Mod (5) Lt (4) Heavy (4) Mod	(5) Lt (4) Mod
Oil Ring Slots—% Open	100	100	100	100	100	100

Pages 1 and 2 and 59 through 65 of Manual.

- Scuffing Chrome Cracking
- 3 6 6 6
- Burning Carbon Cutting Chrome Displacement (cast iron visible) though ring does not display heavy wear.

TABLE 54

## PISTON SURFACE DEPOSITS

Serial No. 6D-5204-1 Date 20 Aug 1973 Lubricant CCL-L-759 (REO 203abserver J. SImpson Engine Model 6V53T Fuel MIL-F-16884

				Piston	Piston Number		
		11	2۲	31	18	2R	3R
		10 CSA	40 CSA	30 DŞA	52-9	5 CSA	25-9
	Top*	90 AS	e0-5 <b>*</b>	70-5	75-5	75-9	75-5*
		10 CSA	5 CSA	20 CSA	5 CSA	3 CSA	100 ASA
Combustion Chamber	Chamber*	90 AS	40 ASA	30 ASA	95 ASA	97 ASA	
			55 AS	50 AS			
Under Head	•_	100-3	100-3	100-3	100-3	100-3	100-3
Skirts*	Thrust	3.9	4.1	4.0	3.9	4.1	4.1
	Anti-Thrust	4.1	3.9	3.8	4.1	3.8	3.8
A 7:1:0	•		l	*1*			
neller Areas	9	C L	. T.	1. C T.	.1	C I	r <sub>1</sub>
	-	80AH	85AH	80 AH	55AH	85AH	65AH
1	2	40BH 60AH	I .	30вн 5-4 65 <b>а</b> н	55BH 45AH	45BH 5-5	85ВН 15АН
<u> </u>	င	35BH 65AH	25BH 5-7 70AH	20BH 10-9 50BH 65AH 5-6 50AH	50ВН 50АН	25BH 15-4 60AH 15-4	50BH 5-5
, ,	4	10-9 - 15-6 75-4	зоан 15-9 15-5	5-9 - 95-4	5AH 25-7 70-4	5BH 5-5 30AH 60-4	25-9 15AH 10-5 50-3

Lacquer—Pages 4, 36, 37 of Manual.
\*Carbon and Ash: Use Volume Factor (Pages 5 and 40 through 47)
Indicate H, M, or S (Page 5)

\*Non Carbonacous Fuel Deposit +CSA - C-depth, S-soft, A-ash type deposit

TABLE 5-5

and the second of the second o

## PISTON RING GROOVE DEPOSITS

Date 20 Aug 73
Observer J. Simpson Serial No. 6D-5204-1 Lubricant CCL-L-759 Fuel MIL-F-16884 Engine Model 6V53T

(REO 203)

							Cylinder Number	Number					
		-	11	7.			ઝ		18	2	2R	33	
		CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACQ
	-	,	100-8	ı	100-5	15АН	70-5		100-5		15-9 85-6		30-9
T	2	1	10-9 10-6	30AH	5-9 65-4	40AH	10-9	,	100-4		10-9 90-5	45AH	10-9 10-6 35-4
3000 TO 000	3	1	100-4	1	100-4	-	100-4	1	100-4	ı	40-5 60-4	•	20-5
	4	1	100-4	1	100-4	_	100-4	_	100-4	_	100-4	-	100-4
4:	٦,	1	100-6	•	9-001	1	-	3	_	-	100-6	-	9-001
Back of Groom	2	55	1	50	-	55	1	80	-	25	•	58	-
	က	15	ı	Э	, I	8	•	13	-	15	ì	20	-
	4	1	100-4	_	20-6 80-4	_	100-4	-	100-4	-	100-4	-	100-4
	1	-	15-9 85-4	_	60-5 40-4	-	50-5 50-4	10 <b>A</b> H	10-9 80-7	1	30 <b>-6</b> 70-5	•	60-6 40-5
90	2	15AH	5-7 80-4	20 <b>A</b> H	20-8 60-4	10 <b>A</b> H	5-9 85-4	15AH	20-9 65-5	20 <b>A</b> H	80-4	ı	100-4
	3	•	100-4	-	25-6 75-4	-	100-4	•	100-4	1	100-4	ı	100-4
	4	•	100-4	-	100-4	•	100-4	1	100-4	B	100-4	•	100-4
Drain Holes - % Blocked	þ	0		0		0		0		0		0	

Lacquer: Pages 4, 36, and 37

\*Carbon and Ash: Use Volume Factor (Pages 5 and 40 through 47) Indicate H, M, or S (Page 5) †Carbon and Ash: Indicate Percent Filled and H, M, or S (Page 5)

\* % Volume Fill

Table 5-5a

TEST PROCEDURE   6V53T   STANDARD COMPUTATION SHEET FOR PISTON RATING   PISTON NO. 1L	PISTON NO. 1L	NO. 1 GRC JVE, VOLUME-%	PISTON WTD* RATING 143.58	UNDER.	NO. 3 NO. 4 CROWN	LOEMERIT AREA SOEMERIT AREA SOEMERIT				8.75	00.6	
NO. 1	SNI NE			LANDS		EA-% DEMERIT AREA.				10.00	9.00	
NO. 1		ı			NO. 1	AREA-% DEMERITAR		-		4	1.20	+
NO. 1		84 (DFM)			NO. 4	AREA-S DEMERIT						+
NO. 1	ANDARD COM	MIL-F-168		VES	NO. 3	AREA-% DEMERIT	15 15.00					
TORY AFLAL  196  TORY AFLAL  NO. 1  AREAN DEWENT  1 1.00	۲۱۱ ۳.72	FUEL		GROC	NO. 2	AREA-% DEMERIT	55 55.00					
TEST PROCEDURE TEST HOURS TEST LABORATOI LUBRICANT TYPE FACTOR HC 1.00 MHC 0.75 MHC 0.75 C HC 0.25 C VLC 0.15	6V53T 196 3Y AFLRL	NEO 203			NO. 1	AREA-% DEMERIT	1 1.00					
TEST PF TEST LA LUBRIC TYPE TYPE TYPE CARBON MC CARBON M	OCEDURE JURS	ANT	*				1.00		0.50	0.25	0.15	
	TEST PR TEST HC TEST LA	LUBRIC			TYPE		ž	MHC		- 1	S VLC	

				1						
LACQUER	7E8	9.00		10.00	5.25	2.00	1	ļ	5.88	2.50
CLEAN	0									
ZONAL BATIMG	LING									-
LOCATION FACTOR	1CTOR									
WEIGHTED RATING	ATING	10.00	55.00	25.00	5.25	3.20	19.00	17 75	00 2	6
							2	2,11	3.00	7.30
WEIGHTED	20.0	WEIGHTED TOTAL DEPOSITS								

2.50

100

9.1 1.13 3.75

17.75

19.00

1.20

2.00

20

10.00

2

9.00

8

LACOUER AL O.025
RL O.001

0.050 0.075 BL 0.100

DBrL

15.00

55.00

1.00

CARBON

0.75 4.50

2 8

15 2

75

Table 5-5b

			;			S	ANDA	RD CON	STANDARD COMPUTATION SHEET FOR PISTON RATING	NO SE	EET FL	JR PIST	ON RA	INC						
1	STPR	<b><i>TEST PROCEDURE</i></b>	-	Trecyo		RAT	RATER	J. Simpson	nosc		DATE 20	20 Aug	20 Aug 1973		PIS	PISTON NO.		2L		
7	TEST HOURS.	JURS	ST			LAB	ORATC	LABORATORY TEST NUMBER	ST NUM	- 1	605204	-1 (Te	(Test No.	5	} •					
7	ST LA	TEST LABORATORY AFLRE	RY A	FLRL		STAI	STAND NO. 5		ENGINE NO.	E NO.	<b>6D5204</b>									
7	LUBRICANT	ANT	5	203		FUEL -	X	MIL-F-16884 (DFM)	884 (D	FM)	1				Ž	0. 1 GR	OOVE,	NO. 1 GROOVE, VOLUME-%	AE-%	
1																PISTO	V WTD	PISTON WTD. RATING	ي	133.3
						GROC	GROOVES							1	LANDS					INDER
	DEPOSIT TYPE	FACTOR	NO.	7. 1	S	NO. 2	ž	NO. 3	NO. 4	4.	Ş	-	N O	2	NO. 3	m	Š	*	55	CROWN
			AREA-%	AREA-% DEMERITAL	AREA-%	DEMERIT	AREA-%	REA % DEMERITAREA % DEMERIT AREA % DEMERITAREA % DEMERITAREA % DEMERITAREA % DEMERITAREA % DEMERITAREA % DEMERITAREA %	AREA %	DEMERIT	AREA-%	DEMERIT	AREAS	DEMERIT	AREA-%C	JEMERIT	AREA.%	DEMERIT	AREA.%	OF MER.
	Ę	8.	4	4.00	li	50.00	3	3.00												
	MHC	0.75																T		
NO	<u>ပ</u> ွ	0.50																		
BAA	ပ	0.25											45	11.25	25	6.25				
<u>'</u>	VLC VLC	0.15									85	12.75	55	8.25	20	10.50	30	4.50		
	ته وت	CARBON RATING	7	4.00	20	20.00		3.00	1		12	12.75	19.50	50	16	16.75		4.50		
	B	0.100									15	1.50					15	1.50		
	08r		9	4.50			40	3.00	20	1.50							15	1.13		
EB.	4						20	1.00	88	4.00					2	0.25	64	2.00		
no:	181 00:																		80.7	2.50
)A	₹	0.010																		
	7	0.001																		
l	5€	LACQUER	,	4.50	1		4	4.00	5.	5.50	1.	1.50	,			0.25	4	4.63		2.50
<u> </u>	CLEAN	0																		
	ZONAL	ZONAL RATING											1				1			
ات	OCATIO	LOCATION FACTOR																		
<u>₹</u>	EIGHTE	WEIGHTED RATING	Ψ	8.50	50	50.00	7	7.00	5.	5.50	14.	14.25	19.50	25	17	17.00	0	0 13		2 50
	1	TOT GUARANTE		02:0000													`		"	2

\*WEIGHTED TOTAL DEPOSITS

Table 5-5c

	1		12	Т		T		T	Т	Τ	Т	T-	Т	T	-
			138.71	INDER	CROWN	DENE									
		AE.%	ក្		55	AREA-%									
	ы	VOLU	RATIN		4	DEMERIT					4.50	4.50	1.50	1.13	
	). 3I.	OOVE,	WTD		Š	AREA-%					2	4	15	15	-
	PISTON NO.	NO. 1 GROOVE, VOLUME-%	PISTON WTD. RATING		6	EMERIT				5.00	9.75	14.75	1.00	0.38	-
	PIST	ž		LANDS	NO. 3	AREA-XD				20	65	7 7	10	u.	-
LING	2			3	2	- NDEMENITAREA N DEMERIT AREA NDEMERITAREA NOEMERITAREA NOEMERITAREA NDEMERITAREA NDEMERITAREA NDEMERITAREA NDEMERIT				7.50	9.75	55			•
ON RA	1973 No.				NO. 2	NEA XO				8	65	17.25			•
R PIST	20 Aug				_	EMERIT/					12.00	8	2.00		•
STANDARD COMPUTATION SHEET FOR PISTON RATING	RATER J. Simpson DATE 20 Aug 1973 LABORATORY TEST NUMBER 6D5204-1 (Test No. STAND NO. 5 ENGINE NO. 6D5204				S.	AREA-%		-			8	12.00	20		•
HS NO	SER 60	£			4	EMERIT									
UTATI	on T NUMI NGINE	34 (DF			NO. 4	REA-%D				i		'			-
COM	J. Simpson DATE 4TORY TEST NUMBER 6D5204 NO. 5 ENGINE NO. 6D5204	-F-168			9	EMERIT	8.00		-	-		8	6.50		
INDAR	RATER J. Sin LABORATORY 1 STAND NO. 5	- 1		VES	NO. 3	REA-% 0	8					8.00	65		
ST/	RATE LABO STAN	FUEL_		GROOVES	2	EMERIT	55.0					8			
					NO. 2	AREA-%	55					55.00			
	티티	203		i	-	EWERIT	1.00					1.00	4.00		
	6V53	KEO 203			NO. 1	AREA-% DEMERIT AREA	10					1.	40		
	rest procedure 6V53T Fest Hours 196 Fest Laboratory Aftre	<b> </b>			FACTOR		1.00	0.75	0.50	0.25	0.15	CARBON RATING	0.100	0.075	
	TEST PROCEDU TEST HOURS TEST LABORAT	.UBRICANT			UEPOSIT   I		ž	MHC	ည	CC	۸۲c	CAR	BL BL	DBrL	
	TES1 TES1 TES1	LUB			) Z Z			_≥	' 1	38 A				٥	
															•

2.50

100

2.00

40

0.20

4

5.00

100

2.50

4.63

1.38

0.20

2.00

5.00

6.50

4.00

LACQUER RATING

0.010

EACOUER !

0.00

占

0.080 0.025 2.50

9.13

16.13

17.45

14.00

2.00

14.50

55.00

5.00

LOCATION FACTOR WEIGHTED RATING

ZONAL RATING

CLEAN 0

\*WEIGHTED TOTAL DEPOSITS

Table 5-5d

CRC DIESEL RATING SYSTEM

2.50

WEIGHTED TOTAL DEPOSITS

Table 5-5e

The state of the s

## CRC DIESEL RATING SYSTEM

	STANDARD COMPUTATION SHE . FOR PISTON RATING	
TEST PROCEDURE 6V53T	RATER J. Simpson DATE 20 Aug 1973	PISTON NO. 2R
TEST HOURS 196	LABORATORY TEST NUMBER 605204-1 (Test No. 7)	
TEST LABORATORY AFTER	STAND NO. 5 ENGINE NO. 605204	
LUBRICANT REO 203	FUEL MIL-F-16884 (DPM)	NO. 1 GROOVE, VOLUME-%
		PISTON WTO* RATING

																1010			,	
																200	OMN	FISION WID HATING	۔۔۔	133.38
						GRO	GROOVES							Y.	LANDS				3	ER.
- O	DEPOSIT	DEPOSIT	NO.	). 1	ž	NO. 2	ž	NO. 3	N O	NO. 4	NO.	-	NO. 2	7	Š	NO. 3	Š	7.4	S.	CROWN
•			AREA.%	AREA-% DEMERITAREA	AREA-%	DEMERIT	AREA-%	L* DEMERITAREA * DEMERIT AREA * DEMERITAREA * DEMERITAREA * DEMERITAREA * DEMERITAREA * DEMERITAREA * DEMERIT	AREA.%	DEMERIT	AREA-%	DEMERIT	AREA.%	SEMERIT	AREA-%	DEMERIT	AREA-%	DEMERIT	AREA%	DEMERIT
	ž	1.00	~	3.00	55	55.00	15	1.50												
	MHC	0.75																		
NO	Š	0.50																		
88/	2	0.25											45	11.25	25	6.25	2	1,25		
	VLC	0.15									85	12.75	20	7.50	09	9.00	30	4.50		
	\$₹	CARBON RATING	E.	3.00	55	55.00	1	1.50	3		12.75	75	18.75	75	15	15.25	2	5.75		
	18	0.100	09	00.9							15	1.50								
	DBrL	0.075					40	3.00												
8	AL	0.050					20	1.00	25	1.25			5	0.25	15	0.75	65	3.25		
no	ם ראר	0.025							75	1.88									100	2.50
OV.	₹ V	0.010																		
	RL	0.001																		
	<b>LA</b>	LACQUER RATING	9	00.9	,		4	4.00	3	3.13	1.	1.50	o	0.25		0.75	m	3.25	7	2.50
ರ	CLEAN	0																		
	ZONAL	ZONAL RATING																		
3	CATION	LOCATION FACTOR																		
*	EIGHTEE	WEIGHTED RATING	5	9.00	55	55.00	5	5.50	m	3.13	14.25	25	19.00	00	16	16.00	6	9.00	2	2.50

Table 5-5f

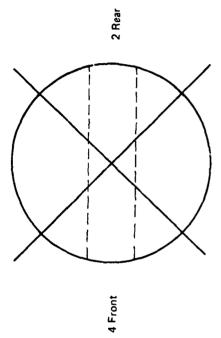
	8	160.38	UNDER.	CROWN	REA'S CEMERIT										100 2.50			2.50				2.50	
38	NO. 1 GROOVE, VOLUME-%	PISTON WTD. RATING		4.0	A-X DEMERITA					15 2.25	2.25	25 2.50		10 0.50	50 1.25			4.25				6.50	
PISTON NO	NO. 1 GROO	PISTON W	•	NO. 3	L'S DEMERIT ARI				50 12.50	45 6.75	19.25	2		5 0.25				0.25				19.50	
			LANDS	NO. 2	A-% DEMERITAREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT AREA-% DEMERIT				85 21.25 5	15 2.25 4	23.50							1				23.50	
STANDARD COMPUTATION SHEET FOR PISTON RATING ATER J. Simpson DATE 20 Aug 1973 ABORATORY TEST NUMBER 6D5204-1 (Test No. 7) AND NO. 5 ENGINE NO. 6D5204				NO. 1	EA-% DEMERITARE				8	65 9.75 1	9.75		35 2.63					2.63				12.38	
J. Simpson DATE  ORY TEST NUMBER 605204  O. 5 ENGINE NO. 605204	(DFM)			NO. 4	A-X DEMERIT AR						,			100 5.00				5.00				5.00	
STANDARD COMPUTATION S  PATER J. Simpson  LABORATORY TEST NUMBER.  STAND NO. 5 ENGINE NO.	MIL-F-1688			NO. 3	V% DEMERIT ARI	0 20.00					20.00	2.00		10				2.00				25.00	
STAND FATER_ LABORA STAND N	FUEL		GROOVES	NO. 2	% DEMERITARE	85.00 20					85.00	20										85.00	
3T RL	203			1	ARSA.% DEMERIT AREA.	1.00 85					1.00	00.6						9.00			10.00		OSITS
6V53T DURE 196 ATORY AFLRE	REO			DEPOSIT NO.		70	5	92	<b>S</b> C	15		0.100	0.075	0.050	0.025	0.010	0.001	-		SM S	:TOR		TOTAL DEP
6V53T TEST PROCEDURE 196 TEST HOURS 196 TEST LABORATORY AFIRE	LUBRICANT			DEPOSIT DEP		HC 1.00	MHC 0.75	S MC 0.50	(RE C 0.25	O VLC 0.15	CARBON	BL 0.1	DB1L 0.0	ı ł	¥	1		LACQUER	CLEAN 0	ZONAL RATING	LOCATION FACTOR	WEIGHTED RATING	WEIGHTED TOTAL DEPOSITS

TABLE 5-6

PISTON GROOVE INSIDE DIAMETER-% RING SUPPORTING CARBON

Date 20 Aug 73	
6D-5204-1 CCL-L-759 (REO 203)	
Serial No. 6D-5204-1 Lubricant CCL-L-759	
ngine Model 6V53T uel MIL-F-16884	

				Piston	Piston Number		
Piston Ring	Quadrant	11	2L	31	H.	2R	38
	_	0	0	0	0	0	c
-	2	0	0	0	0	0	0
_	3	0	0	c			
	*	0	0	C	2 0		
	-	25	90	30	65	0 6	
c	2	10	85	40	75	30	8 2
٧	3	75	40	80	25	7.5	
	4	25	25	15	40	25	06



1 Thrust Side

3 Anti-Thrust Side

TABLE 5-7

### PISTON SURFACE CONDITION

Date 20 Aug 73 Observer J. Simpson
Serial No. 6D-5204-1 Lubricant CCL-L-759 (REC 203)
Engine Model 6V53T Fuel MIL-F-16884

			Piston Number	lumber		
	1-	21	31	181	2R	38
Top Land			NORMAL	TT		
Skirt	10% Lt Scuffing	10% Lt Scuffing	15% Lt 20% Lt Scuffing Scuffing	1	15% Lt Scuffing	5% Lt Scuffing
Piston Pin				ŢŢ		

Pages 1 through 2 and 59 through 65 of Manual.

TABLE 5-8

### **VALVE DEPOSITS**

Date 20 Aug 73	Observer J. Simpson
6D-5204-1	CCL-L-759 (REO 203)
Serial No.	Lubricant
Engine Model 6V53T	Fuel MIL-F-16884

							Cylinder	Cylinder Number					
		_	11	3L		31	ب	18	or.	2	2R	38	~
		CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LACO	CARB	LARO
,	N.									$\perp$			
Head.	EX H	100-BHA		60-BHA 40 AH		60-BHA 40 AH		75-BHA 25 AH		55-BHA		5-AHA	
ı	Ī												
Face	EXH			Norma	l, with	signs	of slig	ot leak	ige on	Normal, with signs of slight leakage on some valves	lves		
	INI												
Tulipt	ЕХН					0.5	0.5 DEMERIT						
	INT												
Stem	EXH				1	0.5	0.5 DEMERIT-	1					

\*Carbon and Ash: Use Volume Factor Technique (Pages 5 and 40 through 47 of Manual). tUse Chart, Page 21—Indicate H, M, or S (Page 5). Lacquer: Pages 4, 36 and 37.

TABLE 5-9

**EXHAUST VALVE SURFACE CONDITIONS** 

Date 20 Aug 73	Observer J. Simpson
Serial No. 6D-5204-1	Lubricant CCL-L-759 (REO 203)
Engine Model 6V53T	Fuel MIL-F-16884

	11	25	ઝ	1R	2R	38
Freeness in Guide	Free	Free	Free	Free	Free	Free
Неэд			NOR	NORMAL		
Face			NOR	NORMAL		
Seat			NOR	NORMAL		
Stem			NOR	NORWAL		
Тір			NOR	NORMAL		8 9 9 9

See Pages 1, 2, 16 through 23, and 54 through 65 of Manual.

TABLE 5-10

## TAPPETS, CAMS, AND ROCKER ARMS

Date 20 Aug 73	Observer J. Simpson
erial No. 6D-5204-1	ubricant CCL-L-759 (REO 203)
Engine Model 6V53T	Fuel MIL-F-16884

					Cylinder Number	Der			
			11	31	31	18	2R	38	
		INT							П
rapper Deposit		EXH				RATED	NOT RATED		
		<u>S</u>			TON	RATED	NOT RATED		Г
Tannet Surface Condition	ion	INT							
		ЕХН			TON	RATED	NOT RATED		
Cam Lobes	sago				NOR	(AL	NORWAL		
		TNI							Ι.
	ē	ЕХН			TON	RATED	NOT RATED		T
,,-		Ī							T .
Rocker Arms	Burshing	ЕХН			NOT RATED	RATED			
	,	INT							Γ.
	Ters T	EXH			NOT RATED	RATED			Г

Lacquer: Pages 4, 36 and 37 of Manual See Pages 1, 2, 16 through 23, and 54 through 65.

TABLE 5-11

# CYLINDER LINERS AND CYLINDER HEADS

	% Lacquer 15 25 25 20 30 35 23	35 - 50
Date 20 Aug 73 Observer J. Simpson Scuffing 1 Travel Area (1)	% Glazed 30 50 50 65 70 60 54	2R 25 - -
203)  Cylinder Liner Scuffing Percent of Total Ring Travel A	Anti-Thrust Area Scuffed % (Anti-Thrust Area Scuffed % (Anti-Thrust B 9 5 5 6 6 18 6 18 5 6 6 15 17.5 11.5 6 11.5 6 11.5 6 11.5 6 11.5	1R 35
Serial No. 6D-5204-1 Lubricant CCL-L-759 (REO 203) Cylin	Percent Scuffed  rust Anti-Thrust  2 1 2 1 10 8 30 6 20 30 10 25 8 15 8 15 13 14	3L 20 - - 40
Serial No	Percent Thrust 2 2 30 30 20 10 10 113	35 - 40
3T 884	Percent Port Restriction 1 2 2 2 7 7 44 44	50 50
Engine Model 6V53T Fuel MIL-F-16884	Cylinder Number Re 1L 2L 3L 3R 2R 3R Average Cylinder Head Deposits	* 5 8 8

Carbon and Ash: Use Volume Factor Pages 5 and 40 through 47 indicate H, M, or S
Lacquer: Use Pages 4, 36, and 37
For Surface Condition—See Pages 1, 2, 16 through 23 and 54 through 65

SURFACE CONDITION TABLE 5-12

Date 20 Aug 73	Observer J. Simpson
6p-5204-1	CCL-L-759 (REO 203)
Serial No.	Lubricant _
Engine Model 6V53T	Fuel MIL-F-16884

Bearing No.	-	2	က	4	
Main-Bearing	Fatigue in of check-ing of	Fatigue as #1 & Lt Wiping	Fatigue in Fatigue Small amt Lt Wiping of check- Lt Wiping ment Embedment	Lt Wiping & Small Amt of Embedment	
-Journal	tinish			NORMAL	
Rod-Bearing	11	2L	31.	1R NORMAL	
-Journal				NORMAL	
Piston Pin				NORMAL	•
Bushing				NORMAL	* *

Note surface condition. See pages 1, 2, 16 through 23 and 54 through 65 of Manual.

TABLE 5-13

SLUDGE DEPOSITS

Date 20 Aug 73	Observer J. Simpson	
Serial No. 6D-5204-1	Lubricant CCL-L-759	(REO 203)
Engine Model 6V53T	Fuel MIL-F-16884	

Connecting Rods
Connecting Rods
Rocker Arm Covers

Top Deck
Push Rod Covers

Timing Gear Cover
Oil Pan
Oil Screen
Connecting Rating
Clean
Clean

See pages 5 and 40 to 47 of Manual.

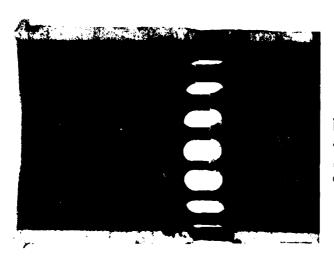
Use CRC Volume Factor Technique.

Figure 6-1

TEST 7

196 HRS

OIL CODE CCL-L-759 (REO 203)





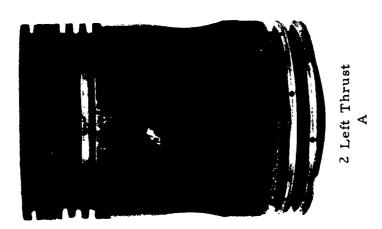


Figure 6-2

TEST 7

196 HRS

OIL CODE CCL-L-759 (REO 203)

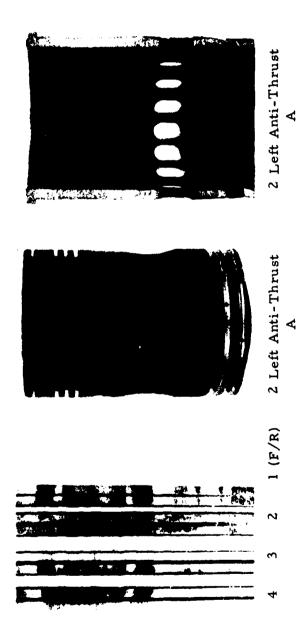
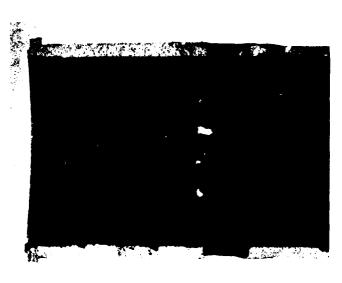


Figure 6-3

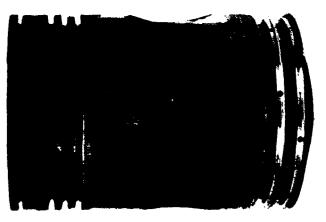
TEST 7

196 HRS

OIL CODE CCL-L-759 (REO 203)



3 Right Thrust W



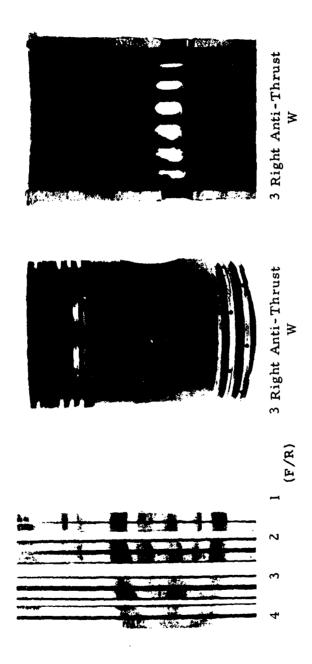
3 Right Thrust W

Figure 6-4

TEST 7

196 HRS

OIL CODE CCL-L-759 (REO 203)



### APPENDIX V

CRC Army Combat Engine Fuels and Lubricants Group Inspection Results

On 14-15 February 1974, this CRC group met at USAFLRL to inspect critical test engine parts from 6V53T engine-lubricant compatibility test numbers 6, 7, 8, 9 and 10. Participants in this inspection are shown in the attached table. The details of this meeting are presented in the CRC official minutes. However, the following is a summary of the group's specific and general conclusions with regard to the effect of fuel type (DFM vs No. 2 Ref. DF) on overall engine performance (Test Nos. 6 and 7 vs. 2 and 3:

Specific engine areas:

### a) Piston Deposits and Ring Sticking

Using the high sulfur fuel and CCL-L-759 oil, there was an overall increase in the deposit level. With the CCL-L-758 oil, there was an overall increase in the deposit level with occurrence of ring sticking.

As a result, it was concluded that the high sulfur fuel had a marked adverse effect on engine-fuel-lubricant compatibility in the piston area.

### b) Piston Ring Condition

The high sulfur DMF fuel significantly increased test severity with respect to ring face condition, ring wear, and ring sticking and pinching as judged by comparing Tests 6 and 7 to Tests 2 and 3.

### c) Cylinder Liners

The high sulfur fuel appeared to give an increase in liner deposits (both lacquer and port plugging). Scuffing,

glazing and wear data showed no consistent fuel related trend with oil CCL-L-758. These three parameters all increased with high sulfur fuel on CCL-L-759.

### d) Cylinder Heads

Messrs. Crosthwait and Crowe reported that, based on ratings, all oils except CCL-L-758 appeared compatible with the fuels, engine, and test cycles. The test on CCL-L-758 using high sulfur fuel showed exhaust valve distress with one broken valve and valve seat. Since this failure was similar to that observed with the low sulfur fuel test on this oil, it was suggested that analysis of valve faces and valve seat inserts be considered to determine if corrosion fatigue might be involved.

Specific engine area performance, summarized in table form, is shown as follows:

Wheeled Cycle Test Fuel\*

shown as follows:		wnee	ted CACTE	<u>rest</u> F	uel *
	Fuel =	No.	2 Ref DF	DF	· -
Performance Area	Lube =	758	759	758	759
Piston Ring Gap Increase		ND	LS	ND	MS
Cylinder Liner Wear		ND	LS	ND	MS
Ring Freedom		LS	ND	ND	ND
% Ring Groove Fill		ND	ND	ND	ND
% Ring Support Carbon		ND	LS	ND	MS
Piston Skirt Demerit		ND	ND	ND	ND
Cylinder Liner Scuff		ND	LS	ND	MS
Used Oil (Final) Wear Meta	als	ND	LS	ND	MS

<sup>\*</sup>Fiel: The high sulfur fuel (DFM) was more severe.

ND - No difference

MS - More severe

LS - Less severe

### General Conclusions (Fuel Sulfur Effect (Tests 2, 7 and 3,6))

The high sulfur fuel was more severe than the low sulfur fuel.

- Deposit Control and Ring Freedom: The high sulfur fuel caused more ring sticking with the high ash oil (758) than with the low sulfur fuel. In other deposit areas, there appeared to be no fuel/sulfur effect. With the low ash oil (759), the only significant change was that port plugging increased with the high sulfur fuel.
- Wear Control: With the high ash oil (758), there was no change in wear level between the two fuels. With the low ash oil (759) there was an increase in wear level when the high sulfur fuel was used, and it was about equal to the wear level of the high ash oil using either fuel.

### CRC INSPECTION PARTICIPANTS AT USAFLRL

### 14-15 February 1974

### Name

### Connection

٠٠.	Α.	McLain, Chairman	Caterpillar Tractor Company
*D.	c.	Bardy	Lubrizol Corporation
*P.	A.	Bennett	Rohm and Haas Company
T.	c.	Bowen	U. S. Army Mobility Equipment Research
			and Development Center (CCL)
*P.	I.	Brown	Chevron Research Company
D.	С.	Carlson	Shell Development Company
T.	D.	Cook	Automotive Research Associates
		Crosthwait	Mobil Research and Development Corp.
*J.	R.	Crowe	Mack Trucks, Inc.
*J.	Р.	Graham	PARAMINS Technology Division, Exxon
			Chemical Co.
*S.	J.	Lestz	U. S. Army Fuels and Lubricants
			Research Laboratory
		Nelson	Coordinating Research Council, Inc.
ŧС.	F.	Schwarz	U. S. Army Mobility Equipment Research
			and Development Center (CCL)
J.	L.	Simpson	U. S. Army Fuels and Lubricants
		(1)	Research Laboratory
		Sommer (1)	Detroit Diesel Allison Division, GMC
		Thurston	Koppers Company, Inc.
G.	W.	Wilkins	Sun Oil Company
*H.	L.	Wittek	List-Rosen-Wittek Associates, Inc.

<sup>\*</sup>Member, CRC-Diesel Army Combat Engine Fuels and Lubricants Group %Project Officer

<sup>(1)</sup> Representing \*J. G. Brandes