

AD-A009 334

QUARTERLY TECHNICAL SUMMARY REPORT,  
OCTOBER - DECEMBER 1974, SEISMIC DATA ANALYSIS  
CENTER

R. A. Hartenberger

Teledyne Geotech

Prepared for:

Defense Advanced Research Projects  
Air Force Technical Applications Center

15 January 1975

DISTRIBUTED BY:

**NTIS**

National Technical Information Service  
U. S. DEPARTMENT OF COMMERCE

**Best  
Available  
Copy**

1

2

3

4

5

6

7

8

9

10

11

12

13

14

15

16

17

18

19

20

21

22

23

24

25

26

27

28

29

30

31

32

33

34

35

36

37

38

39

40

41

42

43

44

45

46

47

48

49

50

51

52

53

54

55

56

57

58

59

60

61

62

63

64

65

66

67

68

69

70

71

72

73

74

75

76

77

78

79

80

81

82

83

84

85

86

87

88

89

90

91

92

93

94

95

96

97

98

99

100

101

102

103

104

105

106

107

108

109

110

111

112

113

114

115

116

117

118

119

120

121

122

123

124

125

126

127

128

129

130

131

132

133

134

135

136

137

138

139

140

141

142

143

144

145

146

147

148

149

150

151

152

153

154

155

156

157

158

159

160

161

162

163

164

165

166

167

168

169

170

171

172

173

174

175

176

177

178

179

180

181

182

183

184

185

186

187

188

189

190

191

192

193

194

195

196

197

198

199

200

201

202

203

204

205

206

207

208

209

210

211

212

213

214

215

216

217

218

219

220

221

222

223

224

225

226

227

228

229

230

231

232

233

234

235

236

237

238

239

240

241

242

243

244

245

246

247

248

249

250

251

252

253

254

255

256

257

258

259

260

261

262

263

264

265

266

267

268

269

270

271

272

273

274

275

276

277

278

279

280

281

282

283

284

285

286

287

288

289

290

291

292

293

294

295

296

297

298

299

300

301

302

303

304

305

306

307

308

309

310

311

312

313

314

315

316

317

318

319

320

321

322

323

324

325

326

327

328

329

330

331

332

333

334

335

336

337

338

339

340

341

342

343

344

345

346

347

348

349

350

351

352

353

354

355

356

357

358

359

360

361

362

363

364

365

366

367

368

369

370

371

372

373

374

375

376

377

378

379

380

381

382

383

384

385

386

387

388

389

390

391

392

393

394

395

396

397

398

399

400

401

402

403

404

405

406

407

408

409

410

411

412

413

414

415

416

417

418

419

420

421

422

423

424

425

426

427

428

429

430

431

432

433

434

435

436

437

438

439

440

441

442

443

444

445

446

447

448

449

450

451

452

453

454

455

456

457

458

459

460

461

462

463

464

465

466

467

468

469

470

471

472

473

474

475

476

477

478

479

480

481

482

483

484

485

486

487

488

489

490

491

492

493

494

495

496

497

498

499

500

501

502

503

504

505

506

507

508

509

510

511

512

513

514

515

516

517

518

519

520

521

522

523

524

525

526

527

528

529

530

531

532

533

534

535

536

537

538

539

540

541

542

543

544

545

546

547

548

549

550

551

552

553

554

555

556

557

558

559

560

561

562

563

564

565

566

567

568

569

570

571

572

573

574

575

576

577

578

579

580

581

582

583

584

585

586

587

588

589

590

591

592

593

594

595

596

597

598

599

600

601

602

603

604

605

606

607

608

609

610

611

612

613

614

615

616

617

618

619

620

621

622

623

624

625

626

627

628

629

630

631

632

633

634

635

636

637

638

639

640

641

642

643

644

645

646

647

648

649

650

651

652

653

654

655

656

657

658

659

660

661

662

663

664

665

666

667

668

669

670

671

672

673

674

675

676

677

678

679

680

681

682

683

684

685

686

687

688

689

690

691

692

693

694

695

696

697

698

699

700

701

702

703

704

705

706

707

708

709

710

711

712

713

714

715

716

717

718

719

720

721

722

723

724

725

726

727

728

729

730

731

732

733

734

735

736

737

738

739

740

741

742

743

744

745

746

747

748

749

750

751

752

753

754

755

756

757

758

759

760

761

762

763

764

765

766

767

768

769

770

771

772

773

774

775

776

777

778

779

780

781

782

783

784

785

786

787

788

789

790

791

792

793

794

795

796

797

798

799

800

801

802

803

804

805

806

807

808

809

810

811

812

813

814

815

816

817

818

819

820

821

822

823

824

825

826

827

828

829

830

831

832

833

834

835

836

837

838

839

840

841

842

843

844

845

846

847

848

849

850

851

852

853

854

855

856

857

858

859

860

861

862

863

864

865

866

867

868

869

870

871

872

873

874

875

876

877

878

879

880

881

882

883

884

885

886

887

888

889

890

891

892

893

894

895

896

897

898

899

900

901

902

903

904

905

906

907

908

909

910

911

912

913

914

915

916

917

918

919

920

921

922

923

924

925

926

927

928

929

930

931

932

933

934

935

936

937

938

939

940

941

942

943

944

945

946

947

948

949

950

951

952

953

954

955

956

957

958

959

960

961

962

963

964

965

966

967

968

969

970

971

972

973

974

975

976

977

978

979

980

981

982

983

984

985

986

987

988

989

990

991

992

993

994

995

996

997

998

999

1000

1001

1002

1003

1004

1005

1006

1007

1008

1009

1010

1011

1012

1013

1014

1015

1016

1017

1018

1019

1020

1021

1022

1023

1024

1025

1026

1027

1028

1029

1030

1031

1032

1033

1034

1035

1036

1037

1038

1039

1040

1041

1042

1043

1044

1045

1046

1047

1048

1049

1050

1051

1052

1053

1054

1055

1056

1057

1058

1059

1060

1061

1062

1063

1064

1065

1066

1067

1068

1069

1070

1071

1072

1073

1074

1075

1076

1077

1078

1079

1080

1081

1082

1083

1084

1085

1086

1087

1088

1089

1090

1091

1092

1093

1094

1095

1096

1097

1098

1099

1100

1101

1102

1103

1104

1105

1106

1107

1108

1109

1110

1111

1112

1113

1114

1115

1116

1117

1118

1119

1120

1121

1122

1123

1124

1125

1126

1127

1128

1129

1130

1131

1132

1133

1134

1135

1136

1137

1138

1139

1140

1141

1142

1143

1144

1145

1146

1147

1148

1149

1150

1151

1152

1153

1154

1155

1156

1157

1158

1159

1160

1161

1162

1163

1164

1165

1166

1167

1168

1169

1170

1171

1172

1173

1174

1175

1176

1177

1178

1179

1180

1181

1182

1183

1184

1185

1186

1187

1188

1189

1190

1191

1192

1193

1194

1195

1196

1197

1198

1199

1200

1201

1202

1203

1204

1205

1206

1207

1208

1209

1210

1211

1212

1213

1214

1215

1216

1217

1218

1219

1220

1221

1222

1223

1224

1225

1226

1227

1228

1229

1230

1231

1232

1233

1234

1235

1236

1237

1238

1239

1240

1241

1242

1243

1244

1245

1246

1247

1248

1249

1250

1251

1252

1253

1254

1255

1256

1257

1258

1259

1260

1261

1262

1263

1264

1265

1266

1267

1268

1269

1270

1271

1272

1273

1274

1275

1276

1277

1278

1279

1280

1281

1282

1283

1284

1285

1286

1287

1288

1289

1290

1291

1292

1293

1294

1295

1296

1297

1298

1299

1300

1301

1302

1303

1304

1305

1306

1307

1308

1309

1310

1311

1312

1313

1314

1315

1316

1317

1318

1319

1320

1321

1322

1323

1324

1325

1326

1327

1328

1329

1330

1331

1332

1333

1334

1335

1336

1337

1338

1339

1340

1341

1342

1343

1344

1345

1346

1347

1348

1349

1350

1351

1352

1353

1354

1355

1356

1357

1358

1359

1360

1361

1362

1363

1364

1365

1366

1367

1368

1369

1370

1371

1372

1373

1374

1375

1376

1377

1378

1379

1380

1381

1382

1383

1384

1385

1386

1387

1388

1389

1390

1391

1392

1393

1394

1395

1396

1397

1398

1399

1400

1401

1402

1403

1404

1405

1406

1407

1408

1409

1410

1411

1412

1413

1414

1415

1416

1417

1418

1419

1420

1421

1422

1423

1424

1425

1426

1427

1428

1429

1430

1431

1432

1433

1434

1435

1436

1437

1438

1439

1440

1441

1442

1443

1444

1445

1446

1447

1448

1449

1450

1451

1452

1453

1454

1455

1456

1457

1458

1459

1460

1461

1462

1463

1464

1465

1466

1467

1468

1469

1470

1471

1472

1473

1474

1475

1476

1477

1478

1479

1480

1481

1482

1483

1484

1485

1486

1487

1488

1489

1490

1491

1492

1493

1494

1495

1496</

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1 REPORT NUMBER SDAC-TR-74-23	2 GOVT ACCESSION NO.	3 RECIPIENT'S CATALOG NUMBER AD-A009 334
4 TITLE (and Subtitle) SEISMIC DATA ANALYSIS CENTER QUARTERLY TECHNICAL SUMMARY REPORT, OCTOBER-DECEMBER 1974		5 TYPE OF REPORT & PERIOD COVERED Progress Report
		6 PERFORMING ORG. REPORT NUMBER
7 AUTHOR(s) Hartenberger, R. A.		8 CONTRACT OR GRANT NUMBER(s) F08606-74-C-0006
9 PERFORMING ORGANIZATION NAME AND ADDRESS Teledyne Geotech 314 Montgomery Street Alexandria, Virginia 22314		10 PROGRAM ELEMENT PROJECT, TASK AREA & WORK UNIT NUMBERS
11 CONTROLLING OFFICE NAME AND ADDRESS Defense Advanced Research Projects Agency Nuclear Monitoring Research Office 1400 Wilson Blvd. Arlington, Va. 22209		12 REPORT DATE 15 January 1975
		13 NUMBER OF PAGES 27
14 MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) VELA Seismological Center 312 Montgomery Street Alexandria, Virginia 22314		15 SECURITY CLASS. (of this report) Unclassified
		15a DECLASSIFICATION DOWNGRADING SCHEDULE
16 DISTRIBUTION STATEMENT (of this Report)  APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.		
17 DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18 SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) <p>This report summarizes the scientific work accomplished at the Seismic Data Analysis Center (SDAC) in the period October through December 1974.</p> <p>During the quarter, eight technical reports covering six subjects were approved for distribution to the government approved list. A letter to the editor of the Bulletin of the Seismological Society of America concerning secondary P wave arrivals was also approved for publication.</p>		

DD FORM 1473 1 JAN 73 EDITION OF 1 NOV 65 IS OBSOLETE

Reproduced by  
NATIONAL TECHNICAL  
INFORMATION SERVICE  
US Department of Commerce  
Springfield, VA. 22151

Unclassified  
SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

PRICES SUBJECT TO CHANGE

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

Three of the reports (TR-74-16, 17, and 18) describe our programming and processing experience with the ILLIAC IV computing system, while Report TR-74-4 describes a new source theory for complex earthquakes. Two reports are comparative in nature: the first, TR-74-5 compares LASA's Detection Processing System with that of NORSAR's; the second, TR-74-6 is an empirical comparison of the two-segment maximum likelihood frequency-wavenumber (f-k) spectra with the f-k spectra produced by beamforming in the frequency domain. Studies of average P and PKP codas and of an iterative beam processor are documented in Reports 305 and TR-73-7, respectively.

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

1a

SDAC QUARTERLY TECHNICAL SUMMARY REPORT, OCTOBER-DECEMBER 1974

SEISMIC DATA ANALYSIS CENTER REPORT NO.: SDAC-TR-74-23

AFTAC Project No.: VELA VT/4709

Project Title: Seismic Data Analysis Center

ARPA Order No.: 1620

ARPA Program Code No.: 3F10

Name of Contractor: TELEDYNE GEOTECH

Contract No.: F08606-74-C-0006

Date of Contract: 01 July 1974

Amount of Contract: \$2,237,956

Contract Expiration Date: 30 June 1975

Project Manager: Royal A. Hartenberger  
(703) 836-3882

P. O. Box 334, Alexandria, Virginia 22314

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.

## ABSTRACT

This report summarizes the scientific work accomplished at the Seismic Data Analysis Center (SDAC) in the period October through December 1974.

During the quarter, eight technical reports covering six subjects were approved for distribution to the government approved list. A letter to the editor of the Bulletin of the Seismological Society of America concerning secondary P wave arrivals was also approved for publication.

Three of the reports (TR-74-16, 17, and 18) describe our programming and processing experience with the ILLIAC IV computing system, while Report TR-74-4 describes a new source theory for complex earthquakes. Two reports are comparative in nature: the first, TR-74-5 compares LASA's Detection Processing System with that of NORSAR's; the second, TR-74-6 is an empirical comparison of the two-segment maximum likelihood frequency-wavenumber (f-k) spectra with the f-k spectra produced by beamforming in the frequency domain. Studies of average P and PKP codas and of an iterative beam processor are documented in Reports 305 and TR-73-7, respectively.

## TABLE OF CONTENTS

	Page
ABSTRACT	
Average P and PKP Coda for Earthquakes (Report 305)	1
An Iterative Approximation to the Mixed-Signal Processor (TR-73-7)	2
A Source Theory for Complex Earthquakes (TR-74-4)	3
A Comparison of the LASA and NORSAR Short-Period Arrays (TR-74-5)	12
Comparison of Two Segment Maximum-Likelihood (TSML) Frequency Wavenumber Spectra with the Fast Beamed Frequency Wavenumber Spectra (FKPLOT) (TR-74-6)	13
A Study of the ILLIAC IV Computer for Seismic Data Processing (TR-74-16)	14
Computer Program Description (TR-74-17)	18
Computer Listings for ILLIAC IV Version of FKCOMB (TR-74-18)	19
P <sub>s</sub> and pP Phases from Seven Pahute Mesa Events	20

Average P and PKP Coda for Earthquakes (Report 305)

Our analysis of 418 small-event ( $m_b \leq 5.8$ ) seismograms recorded at 17 world-wide stations, and of 148 large-event ( $m_b$ ,  $M_s$  (NOS), or  $m_b$  from Pasadena or Berkeley  $\geq 7.0$ ) seismograms recorded at 8 worldwide stations and TFO indicates that coda shape is primarily a function of the arrival times and relative amplitudes of significant secondary arrivals. However, for times greater than 10 to 20 seconds into the coda, large-event codas are approximately 0.14  $m_b$  units greater in amplitude at any given time relative to their maxima, than the corresponding relative amplitude for small-event codas. This suggests that large events are, in fact, multiple events, with the nominal period of source activity for a given sequence estimated to be on the order of 1 to 2 minutes. Correspondingly, large events also tend to be emergent, displaying a 0.2 to 0.3  $m_b$  increase in amplitude between 5 and 30 seconds into the P-wave arrival over that observed in the first 5 seconds of the arrival. Because of their differences, large-event and small-event coda observations cannot be combined. At least two sets of coda observations are required (and are presented in the report) for coda prediction. The small-event codas are used to predict the codas for the San Fernando, California, earthquake of 9 February 1971, at 43 stations. With few exceptions, the observed coda lie within one standard deviation of the predicted coda.

An Iterative Approximation to the Mixed-Signal Processor (TR-73-7)

In this study we develop an iterative beam processor which in the limit is identical to the mixed-signal processor (Dean et. al., 1968). Assuming that two events arrive simultaneously at an array consisting of  $N$  sensors, the array is first beamed on one of the two epicenters to produce a signal estimate for this event ( $0$ 'th iteration). This signal estimate is then time-shifted and subtracted from each of the original  $N$  seismograms in an attempt to remove the signal from the original seismograms. The new set of records, each containing  $N$  stripped seismograms, is then beamed to produce a signal estimate for the second event. The signal estimate for the second event is now time-shifted, subtracted from the original  $N$  seismograms, and the stripped seismograms are rebeamed on the first event. The process is repeated until differences in successive signal estimates for the desired event fall below a predetermined threshold. The iterative-beam processor has great practical (and intuitive) appeal. For seven or more elements, the iterative process converges in a few iterations requiring only a few shift and sum operations per data point, while the equivalent mixed-signal (asymptotic maximum-likelihood) processor requires a convolution for each data point.

### A Source Theory for Complex Earthquakes (TR-74-4)

In this report we review several source theories including that of Haskell (1964) who developed a theory for the spectral distribution of the teleseismic compressional and shear radiation from long thin strike-slip or tensional earthquakes in a homogeneous infinite elastic space. He noted that the strike-slip earthquakes had a higher S/P (shear-to-compressional) energy ratio than was commonly observed, and speculated that most earthquakes have a small component of tensional faulting. He suggested that since tensional faults have a lower S/P ratio than do strike-slip earthquakes, a small portion of tensional cracking could dramatically alter the S/P ratio. Haskell also had some difficulty in matching the existing evidence on the ratio of short-period to long-period energy, and speculated that the fault surface might be "rough". This possibility he modeled in two ways: first, by allowing the ramp displacement function to be modulated by a sine wave, and second, by assuming that for high frequencies the fault acts as the sum of several small faults. Haskell's (1969) paper developed techniques for calculating the nearfield displacement from slip or tensional earthquakes.

In Haskell (1966) he extended the idea of a modulated ramp displacement function to a stochastic displacement function. The ensemble of displacement functions was characterized by the average autocorrelation of the ensemble. This average autocorrelation led them to an average spectrum. Haskell chose the autocorrelation function to be similar to that of the sine-wave modulated ramp function in his 1964 paper, except that it had no periodic factor, and satisfied an integral constraint resulting from the fact that the earthquake must begin and end in a state of static equilibrium.

The displacement spectrum resulting from this autocorrelation behaved at high frequencies like  $\omega^{-3}$  (the spectrum resulting from the modulated ramp function was asymptotic as  $\omega^{-4}$ ). Aki (1967) showed that an  $\omega^{-3}$  asymptote leads to predictions for the shape of the  $M_s - m_b$  curve in disagreement with observation, and chose a different ensemble autocorrelation function which yielded an asymptotic slope of  $\omega^{-2}$ . (Aki's particular choice of an autocorrelation does not satisfy Haskell's criterion that the earthquake begin

and end in a state of static equilibrium. However, a different autocorrelation function, which would satisfy the equilibrium criteria, could be selected which would still result in an  $\omega^{-2}$  asymptotic slope.)

Savage (1966) extended Haskell's 1964 nonstatistical theory to handle the case of a dislocation nucleating at a point in the fault plane and spreading circularly to the boundaries of an elliptical fault. (Haskell (1964) had assumed that the fault started on a line across the width of a narrow fault and propagated down the length of the fault). Savage showed that while the simple ramp displacement function yielded a displacement spectrum asymptotic as  $\omega^{-2}$  in Haskell's initial line dislocation model; it resulted in an  $\omega^{-3}$  asymptote when the more realistic initial point dislocation was assumed. This, he showed, was due to the fact that the radiating surface grew quadratically with time instead of linearly. This  $\omega^{-3}$  asymptote was corroborated by Molnar, et. al. (1973) for cases in which the fault rupture velocity is less than the shear velocity.

Brune (1970) presented a shear wave source theory which brought together in a physically reasonable way several important concepts. He made plausible the idea that until influences from the ends of the fault were felt, the fault displacement after cracking would be a ramp function proportional to  $\frac{\sigma t}{\mu}$ , where  $\sigma$  is the stress and  $\mu$  is the shear modulus. Assuming then, in effect, that the entire fault began to radiate at once, the characteristic period for the radiated shear energy became  $L/\beta$ , where  $L$  is the fault length and  $\beta$  is the shear velocity. Brune's shear wave displacement spectrum decayed asymptotically as  $\omega^{-2}$ . This slope was not strictly speaking derived, but simply followed from his assumed form for the far-field solution which he chose to be in agreement with the result for an instantaneous stress pulse applied to the interior of a spherical surface (see Bullen, 1963). This, of course, is not necessarily a good model of a growing displacement nucleating at a point on the surface of a plane or spherical surface. (The fact that Bullen [1963] and Randall [1966] found corner frequencies proportional to  $L/\beta$  for shear and  $L/\alpha$  for compressional motion reflects the fact that their source was assumed to act instantaneously, and not the fact that the source was distributed over a volume instead of a surface, as suggested by Molnar et al. [1973]).

In his 1970 paper Brune introduced the concept of partial stress drop,  $\sigma_p$ , and showed that it could lead to a spectral slope of  $-1$  somewhere between zero frequency where the displacement spectrum is flat, and asymptotic frequencies where an exponent of  $-2$  obtains. Savage (1972) and others have pointed out that for a long thin fault one must expect  $\sigma_p \propto W/L$  where  $W$  is the fault width due to binding of the fault at the sides.

Contemporaneous with his theoretical paper, Brune and a number of co-workers analyzed signals from many earthquakes and tried to interpret them in its light: see, for example, Trifunac and Brune (1970), Wyss (1970), Wyss and Brune (1971), Wyss and Hanks (1972), Hanks and Wyss (1972), Molnar and Wyss (1972), and Wyss and Molnar (1972). One of the most interesting findings of these analyses is that the P wave corner frequency is higher than the S wave corner frequency. Hanks and Wyss (1972) attempted to explain this fact by replacing  $\beta$  in Brune's (1970) theory of  $\alpha$ , the compressional wave velocity, and appealing to the concept of characteristic wavelength. They pointed out, however, that there was not theoretical foundation for these procedures. Indeed Savage (1972) pointed out that the more precise theories of Haskell (1964) and Savage (1966) predict approximately equal corner frequencies for P and S waves, due to the fact that the corner frequencies are dominated by the duration of faulting, so long as that time is greater than  $L/\beta$ , and not by the length of the fault per se.

Molnar, Tucker, and Brune (1973) have reported that the P wave corner frequency is higher than that of the S wave corner for 144 aftershocks of the San Fernando February 9, 1971, earthquake. They also show by an exact solution, following Savage (1966), that the P-corner is higher than the S-corner if the strain is released instantaneously over the entire surface of a circular disk. On the other hand, if the dislocation propagates at about 0.5 times the S wave velocity then they find that the two corner frequencies are about equal. This result is in agreement with the studies of Haskell (1964) and Savage (1966, 1972).

At intermediate dislocation velocities the results of Savage (1974) show the importance of the operational definition of corner frequency. Savage (1974) shows that if the corner frequency is defined as the intersection of the

high frequency displacement asymptote with the horizontal low-frequency asymptote, then if  $v$ , the dislocation velocity, is close to the shear wave velocity the P wave corner will be substantially higher than the S wave corner. On the other hand, examination of Savage's Figures 1 and 2 shows that for the same cases the P wave corner will be on the order of only 20% higher than the S wave corner if the corners are taken as the 6dB (1.2 amplitude) points on the displacement amplitude spectrum. The identical conclusions can be obtained by examination of Figure 6 in Molnar et al. (1973). In fact, one sees there the special dangers of the asymptotic definition of corner frequencies in that for  $v=\alpha$ , where  $\alpha$  is the compressional wave velocity, the intersection definition gives  $f_p < f_s$  for  $\theta=85^\circ$ , an observation point near the plane of the fault. This result is easily verified from Savage's (1974) figures, and one may see also that for the 6dB corners,  $f_p > f_s$ . These results suggest that the 6dB corner determination is more reliable than determination by the intersection of asymptotes. It is probably just as "objective" as the intersection of asymptotes method, and is certainly not as severely affected by incorrect values of  $Q$ , a serious problem with the latter method as pointed out by Thatcher and Hanks (1973).

We show in this paper that another explanation of the  $f_p > f_s$  paradox may be found by further development of Haskell's (1964, 1966, 1972) ideas that a substantial amount of tensional faulting accompanies many strike-slip or dip-slip earthquakes, and that many earthquakes are accompanied by smaller earthquakes. There is substantial evidence for this point of view in the literature. Wyss and Brune (1967) concluded that the 28 March 1964 Alaskan earthquake ruptured in a series of events; initially propagating in various azimuthal directions from the epicenter, then after a period of about 44 seconds propagating steadily to the West. They also concluded that other large earthquakes are similar in character. Trifunac and Brune (1970) found that the Imperial Valley earthquakes could be regarded as a series of earthquakes initiated along a strike-slip fault in accordance with  $v/\beta \approx .5-.6$ . Kamb et al. (1971) show that the pattern of near-surface faulting for the San Fernando earthquake was very complicated, and Jungels and Frazier (1973) conclude that this complexity must be taken into account in order to satisfactorily interpret the static displacement observations. One might speculate

that if the near-surface faulting is complicated, so too must be the deeper faulting. Jungels and Frazier also require changes in dip for the fault plane. Bolt (1972) analyzed the Pacoima Dam strong motion records for the San Fernando earthquake and concluded that several "bursts" of high frequency energy were received from remote epicenters on the fault plane. Mikumo (1973) discusses the substantial field evidence for flexures in the San Fernando fault plane before adopting a plane surface for his theoretical model. Murray (1973) has concluded that the main Parkfield earthquake consisted of two separate earthquakes on two branches of the San Andreas.

It seems, in fact, that almost every carefully investigated earthquake reveals first-order departures from a plane slip fault. This, of course, is not surprising given the inhomogeneities of the real earth. Tensional sub-earthquakes must also be expected. Although a homogeneous substance may fail in shear, one must expect zones of weakness in an inhomogeneous material to "pull apart", thus introducing a tensional component to an earthquake. Alternatively, if a fault plane is curved and strike-slip movement occurs, one expects some separation on the curves.

The above remarks are not meant to deny that the best initial approximation to almost all earthquakes is slip on a plane. This is strongly implied by the numerous successful studies of long-period radiation from earthquakes based on the double-couple model. However, one might reasonably expect the high-frequency displacement spectrum asymptotes to be severely affected by small tensional sub-earthquakes.

Another puzzling contradiction between theory and observation has been the apparent S/P amplitude ratio, as observed on velocity or acceleration seismograms, of about 3/1, whereas theory, e.g. Haskell (1964), predicts a ratio closer to 10 or 20 to 1. The possibility that observations are affected by unknown variations in Q between S and P waves somewhat confuses the issue. The most reliable data is presumably that from closest in, and Trifunac and Brune (1970) show strong-motion seismograms where the ratio for the 1940 Imperial Valley subearthquakes vary between 10/1 and 1/1 with a mean around 3/1. The first six minutes of aftershocks of the February 9, 1971 San Fernando Earthquake as recorded at the Pacoima Dam strong motion instrument

also give a mean ratio of about 3/1, as we show in the original report. As pointed out by Haskell (1964), this paradox could be resolved if much of the energy around the corner frequency came from tensional faulting for which the theoretical amplitude ratio is about 3/1.

Among the important observations which a successful source theory should address are those which have grown out of the efforts to discriminate earthquakes from underground explosions. The amplitude of twenty-second Rayleigh waves plotted versus the amplitude of one-second compressional waves is known to be an excellent discriminant; see for example Evernden et al. (1969, 1971) and Marshall and Basham (1972). One of Aki's (1967) chief motivations in changing from Haskell's (1966)  $\omega^{-3}$  model to an  $\omega^{-2}$  model was that the latter is in much better agreement with existing  $M_s-m_b$  data. On the other hand, the "spread" in observed  $M_s-m_b$  plots is much greater than can be accounted for by sampling, measurement, and propagation errors; and therefore any single line in  $M_s-m_b$  space, such as the  $\omega^{-2}$  model cannot adequately explain the data. Examples of especially discordant earthquakes that look like explosions with respect to this discriminant may be found in Landers (1972) and Der (1973). Douglas et al. (1973a) have shown that a substantial amount of this discrepancy may be explained by assuming that the earthquakes are dip-slip with a dip of  $45^\circ$ . This fault-plane orientation has a radiation pattern maximum for the teleseismic P radiation. Douglas et al. and Gilvert (1973) have also shown that even for point sources the average shallow shearing earthquakes will separate from explosions by approximately 0.5-1.0 magnitude units. A possible physical explanation is that if one first matches the P wave amplitudes, then for the earthquake there is ten times the compressional wave amplitude emitted as shear waves. If shear waves are about as efficiently converted to Rayleigh waves at the free surface as are the compressional waves and if the earthquake is "shallow" with respect to the Rayleigh wavelength, then one expects about ten times the Rayleigh wave from an earthquake as from an explosion of equal  $m_b$ . The same argument then suggests that for tensional earthquakes one would have only about three times the Rayleigh wave amplitude.

Anglin (1971) plotted complexity versus third moment of the observed spectrum for earthquakes and explosions and found good separation. In general

there is no physical explanation for the separation, and until one is presented, the weaknesses and limitations of the discriminant cannot be convincingly discussed. In this report we give a plausible explanation of Anglin's results by assuming that the more complex the earthquake, the more small earthquakes there are accompanying it. (A complicating point in this discussion is the idea developed by Douglas et al. (1973b) that complexity may be due to arrivals along separate low and high-Q paths.)

In this report we find that the high-frequency asymptotes of earthquakes can vary between  $\omega^{-3}$  for simple earthquakes to  $\omega^{-1.5}$ , where the exponent is restrained only by the requirement for finite radiated energy (von Seggern and Blandford [1972] present evidence that the asymptote for explosions is  $\omega^{-2}$ ). We find that in the case of complicated earthquakes mixing shear and tensional sub-earthquakes, any monotonically decreasing displacement spectral shape can be attained. Savage (1972) has made much the same point, saying "the spectrum of the incoherent radiation could mask the  $\omega^{-3}$  asymptotic behavior". This implies that short-period discriminants may be very unreliable in practice. However, with knowledge of the underlying mechanism it may be possible to suitably constrain the combinations of discriminants, regionalize the earthquakes, and make short period discriminants predictable and reliable.

In the original report, we develop and apply the theory, make some comparisons with previous theoretical results, and compare some results with observation.

In summary, we have developed a theory which accounts for the observed separation between  $M_s:m_b$  lines for earthquakes and explosions, and also explains the robustness of the discriminant despite wide ranges in earthquake ( $M_s-m_b$ ) values. This wide range is explained as being due to the existence of both simple and complex earthquakes. One also sees that the difference ( $M_s-m_b$ ) can be a good discriminant even though the slope of the earthquake  $M_s:m_b$  line is not 1.0.

The fact that P/S ratios are closer to 0.3 than to 0.03 as classically predicted, together with the observations of higher P than S corner frequency, have been shown to be related phenomena and explainable in terms of tensional subearthquakes.

A tentative explanation has been given for the success of the complexity-third moment of frequency discriminant (we might note that this discriminant is vulnerable to evasion techniques).

The results suggest that the projected intersection of the earthquake and explosion populations suggested by the data of several workers, e.g. Marshall and Basham (1972), would not occur if data at lower magnitudes were obtained. Aside from displacement overshoot, the only method for obtaining convergence of the populations would be for small events to preferentially draw relaxation energy from small source regions as in the theory of Archambeau (1968). This possibility lies outside the scope of the present theory. Mean  $M_s : m_b$  regression lines appear to be somewhat lacking in physical significance. The fact that some theoretical justification can be obtained for short-period discriminants suggests that they may be relied upon in non-evasion situations if carefully regionalized and if care is taken to select paths unaffected by P wave multipathing.

Further research should aim at deciding if tensional subearthquakes really exist or are only a theoretical abstraction. Field, experimental, and numerical work should all have a place.

Investigation of the displacement time history near the front of the crack is important to see if on the time scale of interest teleseismically (or regionally for earthquake damage studies) the initial velocity is discontinuous as Brune (1970) suggested and as we have assumed. Brune (1973) has presented some experimental evidence to the contrary, but it is not completely clear that wave energy from regions of earlier movement has not slightly distorted the measurements. This question is, of course, crucial because the discontinuity in the displacement time history governs the far-field high-frequency asymptote, and any slope substantially different from  $\omega^{-3}$  would require major changes in the theory.

The study of the distribution of subearthquakes is also crucial. We have assumed a delta function here; perhaps a distribution similar to that for earthquakes could be shown to be reasonable and tested. Again, both mapping of faults in the field and experimental measurements are needed.

Although we do not expect our basic results to change, it is important to replace Haskell's original solution for the simple earthquake by an exact solution for a fully two-dimensional fault plane surface for both slip and tensional earthquakes. Here Savage's (1974) lead could be followed.

As a final point, Aki (1967) and others have pointed out that for large events  $m_b$  is not a satisfactory measure of the total 1.0 Hz energy in the signal. A suitable measure suggested by Aki is the maximum amplitude in the P coda times the "length" of the coda raised to some power between 0.5 and 1.0.

### A Comparison of the LASA and NORSAR Short-Period Arrays (TR-74-5)

This study compares the LASA and NORSAR short-period arrays in terms of their detection processing systems and their event summaries, for data recorded during a period of 40 days from 15 February to 25 March 1972. An overview of the worldwide surveillance performance of the combined LASA-NORSAR systems is also given.

There are two signal detection algorithms in the LASA and NORSAR Detection Processors (DP). The first algorithm checks successive signal-to-noise ratio threshold crossings by computing and comparing Short Time Averages (STA) and Long Time Averages (LTA). The second algorithm checks in successive tests the consistency of the azimuths and velocities of the arriving signal. This study showed that many of LASA/SAAC LTA measurements in the first algorithm may include part of the signal, thus lowering the reported signal-to-noise ratio. The LTA measurements in the NORSAR DP system do not include any part of the arriving signals.

Either LASA or NORSAR confirmed 73% of the events on the NOAA PDE (Preliminary Detection of Epicenters) list over the data period, and 37% were confirmed by both arrays. The LASA alone reported 56% of the events on PDE list, and NORSAR alone reported 53%.

A direct comparison of LASA and NORSAR Event Summaries shows that 72% of the NORSAR published events are within LASA's surveillance range. Of these in-the-range events, 70% were confirmed by LASA. Of the unconfirmed events 11% were due to system failures, and 7% were unconfirmed by DP. Similarly, 78% of the LASA published events were within NORSAR's surveillance range. Among these in-the-range events, 38% were confirmed by NORSAR. Of the unconfirmed events 5% were due to system failures, and 45% were unconfirmed by DP. The higher percentage of NORSAR DP unconfirmed events is due partly to the high background noise of the array.

Although we do not estimate the detection thresholds of the arrays in this report, we note that the average noise on the LASA beams is about a factor of two lower than that of NORSAR. Therefore, LASA's detection threshold would be ~0.3 magnitude units lower than NORSAR's, if average signal losses were the same at both sites.

Comparison of Two Segment Maximum-Likelihood (TSML) Frequency Wavenumber Spectra with the Fast Beamed Frequency Wavenumber Spectra (FKPLOT) (TR-74-6)

The empirical comparison of the two segment maximum likelihood f-k spectra with the fast frequency domain beam f-k spectra (FKCOMB, FKPLOT) shows that the latter is more suitable for the separation of multiple signals if the amplitudes of the signals differ considerably. This advantage of the beaming process is attributed primarily to the stripping procedure, which has not been developed for the maximum likelihood spectra. The maximum likelihood f-k spectra, on the other hand, are less sensitive to the array response and easier to interpret, especially if the array used contains only a few elements, since the sidelobes of the array response are more confusing on the FKCOMB output of this case. Both processes require a good signal to noise ratio ( $\sim 2$ ) for successful application.

Composited recordings of long period Rayleigh waves recorded at LASA were utilized for the comparison using various subarray configurations and signal and noise levels.

A Study of the ILLIAC IV Computer for Seismic Data Processing (TR-74-16)

This is the first report in a series of three which pertain to our experience with the ILLIAC IV computing system. The purpose of this study was to determine the suitability of the ILLIAC computer for processing seismic data. We have done this by looking at the computing requirements of each of several algorithms; and then, by comparing these requirements with the characteristics of the ILLIAC, we investigated the feasibility of programming each of the algorithms on the ILLIAC. Finally, the procedure FKCOMB was actually coded for the ILLIAC and the program has been tested and run. FKCOMB is a long-period seismic signal analysis procedure, which is important in calculating discriminants between earthquakes and nuclear explosions; it may become an integral part of data processing on the Seismic Network. FKCOMB was chosen for this experiment because the large amount of processor time required prohibits its use in-house. Also, known results are available with which to compare the ILLIAC version.

The ILLIAC computer consists of a control unit, 64 arithmetic units or processing elements (PE), 128K 64-bit words of core, and  $10^9$  bits of disk storage. The 64 PE's execute instructions in lock step; i.e., they all execute the same instruction simultaneously. It is in this respect that the ILLIAC departs from conventional computer architecture.

The control unit decodes instructions and executes instructions for program control. It has 24-bit integer arithmetic hardware to calculate indices and addresses. There are four general purpose accumulators and a 64-word fast access memory in the CU, which also has access to all 128K of core and initiates transfers between core and disk.

The primary computational resource of the ILLIAC is the array of 64 processing elements. Each has complete arithmetic capabilities and can perform  $2 \times 10^6$  multiplications per second. The capacity of all 64 PE's is about  $10^8$  multiplications per second. Each PE has access only to 2K of core, and has only limited capability to communicate with other PE's. Control within a PE consists of the ability programatically to disable selected PE's. When disabled, a PE's memory is protected and cannot be altered by the PE, though all other facets of instruction are performed.

The ILLIAC disk is the primary storage device. It consists of 13 head-per-track disks and two disk controllers. Together the disks hold approximately  $10^9$  bits. Transfers between core and disk are initiated by the ILLIAC control unit and occur in blocks or pages of 1024 words. The transfer rate is about  $10^9$  bits per second. Access time to any record on disk is 40 milliseconds or less. The disk can be loaded from the Tenex file system prior to program execution and unloaded after program termination. The layout of data to the ILLIAC disk is under user control and should be arranged to minimize access times during program execution.

The 64 processing elements provide the ability to perform vector arithmetic operations on 64 data elements simultaneously. Program logic generally requires that selected PE's be disabled to avoid redundant calculations if all 64 processing units are not required. In general, program execution time is decreased if disabling of PE's is avoided.

ILLIAC is able to perform approximately 100 million operations (i.e., a multiplication, addition, etc.) per second. Any procedure which requires fewer than 100 billion operations would have a running time of under 10 minutes. The setup time for an ILLIAC job is large enough to make such a run impractical. Thus, algorithms requiring very few computations or the use of a small data base with any algorithm are unsuitable for ILLIAC processing.

We conclude from this study that the ILLIAC computer when programmed to perform seismic processing on large data bases can be a valuable tool in the development of seismic event detection and discrimination procedures. It is feasible to implement some existing algorithms on the ILLIAC which are not currently used to process large data bases, or some algorithms which are proposed but not tested due to a lack of computing power. Our experience with one algorithm (FKCOMB) which is representative of seismic analysis programs shows that a major benefit of the ILLIAC to seismic processing is its ability to operate in parallel on sixty-four different data streams, thereby reducing the time required to process large data bases. Efficiently arranging these data streams for the processing element memories is an important consideration for designing any seismic algorithms for the ILLIAC.

It is feasible to program ILLIAC to perform the algorithms reviewed in this study: convolution-recursive filtering, PHILTRE, matched filtering, beamforming, and maximum likelihood  $f-k$  estimation. Since a major factor in programming any of these algorithms is the data arrangement in core, a more detailed study of the data configurations for these algorithms would be needed to optimize the use of the computing power of ILLIAC. One algorithm (FKCOMB) was studied in detail and implemented on ILLIAC IV. Data editing schemes were devised for FKCOMB which can be used with appropriate modifications for all the seismological algorithms we reviewed.

Two independent uses for ILLIAC are suggested. First, FKCOMB and other algorithms now used selectively could be run routinely on larger data bases to better provide the services they already give on conventional machines. Second, experimental methods impractical to test via conventional machines could be tested on ILLIAC. The experience of implementing FKCOMB illustrates that the design and coding of new algorithms for ILLIAC is not significantly more difficult than for serial machines. The only phase not experimentally explored by this effort are the operational problems of manipulating the large amounts of data involved in routine processing of long and short period data on ILLIAC.

To maximize efficiency, the time consumed executing analysis algorithms should be significantly greater than the time required for data editing. A combination of algorithms such as matched filtering and FKCOMB require an order of magnitude more processing time on a given memory load than FKCOMB alone, and would thereby utilize ILLIAC more efficiently.

The following points represent our findings in developing FKCOMB software on the ILLIAC.

1. Faster and more reliable network file transfer between I4-Tenex and other hosts such as UCLA, Ames, TSS and SDAC would expedite the programming and use of the ILLIAC system.

2. There is no clear preference between CFD and GLYPNIR indicated by our experiences. The possibility of implementing CFD at SDAC or upgrading service at UCLA should be investigated, and an experiment made in the use of GLYPNIR before any long range decision is made.

3. Software debugging aids presently available for ILLIAC programming are minimal. Additional debugging aids would lessen the task of ILLIAC programming. User implementation of such aids on the SDAC host is feasible though at the cost of considerable effort.

4. We estimate that the time and effort required to design and code an ILLIAC program is no more than twice that required for a conventional machine. Due to the fact that ILLIAC is not fully operational at present and the necessity to handle the large amounts of data inherent in the use of an ultrafast machine, the time and effort required currently to debug an ILLIAC program may be as much as four times that required for a conventional machine.

5. Routine processing of 24 hours of long-period seismic data is not feasible at present due to the restricted availability of the ILLIAC processor and the inability at the system to handle the large amounts of data efficiently.

### Computer Program Description (TR-74-17)

In this second ILLIAC IV report we describe a preliminary version of a long period array processing package designed around the FKCOMB algorithm for use on the ILLIAC IV computer. FKCOMB is a general-purpose array-processing program that uses frequency-wavenumber analysis to produce a bulletin which lists signal detections and various statistics for each detection. Two data editing and reformatting modules prepare the seismic data for FKCOMB and can be modified for use with other seismic algorithms. Preliminary reformatting of the seismic data is performed by DEM1. The data is edited and fast fourier transformed by DEM2.

The input parameters required for operating these programs and their subroutines are described in this document.

Computer Listings for ILLIAC IV Version of FKCOMB (TR-74-18)

This is the third report in a series of three published at the Seismic Data Analysis Center in 1974, which describe our studies of and programming experience with the ILLIAC IV computer. The present report is a computer listing of the ILLIAC IV version of a scientific program called FKCOMB. The main program, FKCOMB, and two data-editing and formatting modules, DEM1 and DEM2 were written in Computational Fluid Dynamics Code (CFD); some subroutines were written in ASK code.

Letter to the Editor of BSSA

P<sub>s</sub> and pP Phases from Seven Pahute Mesa Events

Springer (1974) observed what he thought to be secondary P-wave arrivals in teleseismic records for Pahute Mesa explosions. It was hypothesized that these arrivals may be associated with a spall-closure source (Eisler and Chilton, 1964). Spectral analysis of the P-wave arrivals for seven Pahute Mesa explosions suggests that the secondary phase due to spall closure, P<sub>s</sub>, may be present in the records for two of the events studied.

The method we used to determine the existence of secondary p arrivals (pP or P<sub>s</sub>) for a given event involves the analysis of null patterns in the P-wave spectra which may result from interference of the types pP-P and P<sub>s</sub>-P. Analysis details are given by Cohen (1970) and Cohen et al. (1972).

Analysis of the records for seven Pahute Mesa events as recorded at five LRSM stations (HN-ME, KC-MO, PG-BC, RK-ON, and SV3QB) and two observatories (CPO and WMO) shows that the average P-wave spectra for two events, Knickerbocker and Rex, exhibit spectral-null patterns which may be interpreted as deriving from interference of the type P<sub>s</sub>-P; that is, the null frequencies f<sub>n</sub> are apparently related as follows:

$$f_n = [(2n+1)/2] \Delta f, n=0,1,2,3,\dots,$$

where  $\Delta f = 1/\tau$ , and  $\tau$  is the P<sub>s</sub>-P delay time. The spectra for the five remaining events display nulls which appear related to pP-p interference; here:

$$f_n = n\Delta f, n=0,1,2,3,\dots,$$

where  $\Delta f=1/\tau$ , and  $\tau$  is the pP-P delay time. The relationships between null frequencies f<sub>n</sub> and integers n for the seven events examined are given in the original letter.

Springer (1974) was able to obtain both pP-P and P<sub>s</sub>-P delay time estimates for a given event because he used records taken near ground surface zero. Our results, however, indicate that at teleseismic distances, either pP or P<sub>s</sub>, but not both, may appear as predominant secondary arrivals. That the spectra have been smoothed by averaging over a 0.15 Hz window cannot account for our inability to resolve nulls which may be associated with P<sub>s</sub>-P interference,

for even at delay times on the order of 3 seconds, the attenuation of spectral undulations produced by smoothing is only about 3 db. Rather, it is suggested that for events for which a spall is well developed, the surface-reflected phase pP, as observed at teleseismic distances, will be weak. The reason for this is that if a spall develops, energy in the pP phase is trapped above the spall, and is subsequently released as  $P_s$ . If the spall is small or nonexistent, of course, only pP may be observed.