

AD/A-000 104

**MODIFICATION TO MATH MODEL FOR SMALL
INDEPENDENT ACTION FORCES (SIAF)**

TRW Systems Group

Prepared for:

**Advanced Research Projects Agency
Army Missile Command**

15 December 1973

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MODIFICATION TO MATH MODEL FOR
SMALL INDEPENDENT ACTION FORCES (SIAF)
FINAL REPORT

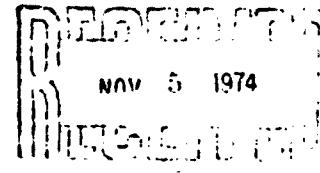
15 December 1973

Contract Number DAAH01-73-C-0914

D D C

REF ID: A621176

NOV 5 1974



Sponsored by:

U.S. Army Infantry School
Concepts and Studies Division ACN 13954

Supported by ARPA Funds

Technical Requirement Number 1816

Amount of Contract: \$187,003

Contract Dates: 25 May 1973 to 31 December 1973

Prepared by:

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The research was the responsibility of the U.S. Army Infantry School, ACN: 13954. It was supported by funds from the Defense Advanced Research Projects Agency of the Department of Defense. Fiscal aspects of the contract were monitored by the U.S. Army Missile Command.

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ACKNOWLEDGEMENTS

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The TRW Study Team wishes to acknowledge its appreciation to the Study Sponsor Representative, Major Ardeen R. Foss, U.S. Army Infantry School, to the Chairman of the Study Advisory Group, Colonel John E. McCleary, U.S. Army Infantry School, to his staff, and to the members and alternate members of the Study Advisory Group, for their guidance.

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MODIFICATION TO MATH MODEL FOR SMALL INDEPENDENT ACTION FORCES (SIAF) FINAL REPORT

INTRODUCTION

This document, prepared by TRW Systems Group, One Space Park, Redondo Beach, California, constitutes the final technical report on the "Modification to Math Model for SIAF" program. This program was conducted under ARPA/AMICOM Contract Number DAAH01-73-C-0914 during the period 25 May 1973 to 31 December 1973. The original study sponsor was the USACDC Systems Analysis Group. Shortly after the start of the work, cognizance was transferred to the U. S. Army Infantry School. The principal product of this program was a revision to a computerized simulation model of a SIAF operating in both reconnaissances and combat modes developed by TRW under previous ARPA contracts.

The SIAF simulation model is provided as computer software installed on the CDC 6500 computer at Fort Leavenworth, Kansas, and additions to and replacements for a six-volume User's Manual as follows:

Volume I-Model Description and Programming Guide (This Final Report serves as a forward to Volume I)

Volume II-Model Subroutines (Terrain, Weather, Targets)

Volume III-Model Subroutines (SIAF Function and Ancillary Routines)

Volume IV-Model Program Listing

Volume V-Combat Initialization Subroutines

Volume VI-Combat Execution Subroutines

These six volumes are to be considered as part of the final report.

This final report provides a background to the SIAF program, a brief description of the features of the integrated SIAF model, and a summary of the tasks performed during the current contract.

Section 2 of Volume I provides a more complete overview of the SIAF model. Full details of the individual submodels are provided in Volumes II through VI.

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BACKGROUND

In recognition of the increasing importance and complexity of small military patrols in low intensity guerilla warfare, ARPA activated the Small Independent Action Forces (SIAF) program in 1968. This continued project has as its ultimate objective the improvement of the operational effectiveness of SIAF units. One aspect of this objective has been the need to develop a rapid and economical means of measuring patrol effectiveness to permit the effects of postulated improvements or changes to be evaluated. Namely, a capability is required to

- ° Study effects of changes in equipment
- ° Establish tradeoffs for organization/equipment mixes
- ° Expose alternative doctrine options

In furtherance of this objective, ARPA has sponsored several types of research and development programs. These have included the collection of extensive field data on the various aspects of patrol operations in Southeast Asia, equipment development programs, field test programs, and a SIAF computer model simulation program by TRW Systems. The model is the subject of this report.

The SIAF simulation model has been developed by TRW Systems under seven successive programs. The first, under ARPA/AMICOM Contract DAAH01-70-C-0141 running from August 1969 to June 1970, was to determine the feasibility of structuring a SIAF model for use as an evaluation tool. The second, under ARPA/AMICOM Contract DAAH01-71-C-0100 running from August 1970 to August 1971 was to develop a computerized simulation of a SIAF patrol in a reconnaissance role. The primary effort was formulation and programming of the model itself. Volumes II and III of the SIAF Users Manual describe primarily the results of that effort.

The third TRW SIAF program was the SIAF External Fire Support Study, under ARPA/AMICOM Contract DAAH01-71-C-1115 running from May 1971 to May 1972. An output of that study was an External Fire Support Submodel that was incorporated into the SIAF Reconnaissance Model.

The fourth SIAF model development program provided for the development and programming of a fully computerized stochastic combat submodel

which provided dynamic deployment logic as well as fully simulated small arms fire. This work was performed under ARPA/AMICOM Contract DAAH01-72-C-0305 running from November 1971 to December 1972. The results were fully integrated with the previous SIAF Reconnaissance Model.

Two subsequent contracts, DAAH01-73-C-0222 and DAAH01-73-C-0257 which were performed in December 1972 and from March 1973 to July 1973, respectively, were used to reprogram the SIAF model to run on the CDC 6500 computer.

The final SIAF model development contract was used to modify the SIAF Model. This has been performed under Contract DAAH01-73-C-0914 from June 1973 to December 1973. The work performed is the subject of this report.

MODEL SUMMARY

The Small Independent Action Forces (SIAF) Model is a computer simulation intended for use in evaluating the effectiveness of alternative SIAF concepts. The model essentially accepts as input a military operations plan, such as would be prepared by a military commander in the field for an actual patrol operation, and simulates this operation on a computer. It considers both reconnaissance and combat missions. The SIAF Model simulates the interactions of the operations plan with the terrain, weather, and enemy situation. It considers a total mission from beginning to end. The output of the model is the effectiveness of the particular operation under consideration. During the simulation of activities and events which occur during SIAF operations, the model calculates statistics pertaining to movement, navigation, surveillance and detection, fire support, supply maintenance, human maintenance, communications, and casualties.

The model is checked out and is ready for use. It can be applied to a variety of problems involving the effectiveness of SIAF operations, such as the effects of postulated improvements and determination of performance capabilities of these type units. It can also be used to study the sensitivities with respect to numerous input variables.

Listed below are some of the features of the SIAF model compared to other models which might be used for the same purpose:

- 1) It simulates the entire mission from start to finish and is capable of considering up to 10-day missions. This differs from many existing models of patrol operation which consider only a partial mission segment. The functions of movement, navigation, surveillance and detection, fire support, supply maintenance, human maintenance and external communications and their interactions are explicitly considered in the model.
- 2) It includes a detailed and realistic treatment of terrain considering relief, vegetation, obstacles, cultural features and surface material. This differs from other existing models in that for this model relief is represented by a continuous surface, and vegetation is represented throughout the entire area of operations instead of just locally.
- 3) It has an explicit detailed treatment of visual detection considering instantaneous locations of each SIAF and target individual as well as light level, reflectivity and background.
- 4) It includes dynamic movement of the patrol and detailed target movement. The patrols can advance toward targets or can be made to move around them.
- 5) The suppressive effect of incoming fire is considered for both movement and outgoing fire.

The combat model has the following detailed features:

- 1) It considers the events and conditions just prior to entering combat as well as the combat itself. Thus allowing study of the effect of pre-combat conditions and of entry into and exit from combat.
- 2) It considers ambush, attack, defense and meeting engagements.
- 3) It is stochastic and considers the attributes of each man on both sides. It considers individual fire-target combinations.

- 4) It relates the progress and the outcome of combat operations to environmental variables such as terrain, weather, etc., as well as to the combat power on each side.
- 5) It allows a study of combat alone or combat in combination with reconnaissance and/or in combination with the complete SIAF mission.
- 6) It considers EFS and organic weapon combat.
- 7) It allows user-input to many of the variables and decision factors so as to study the effect of variations of these.

SUMMARY OF ACTIVITY

Technical Objective

The objective of Contract DAAH01-73-C-0914 "Modification to Math Model for Small Independent Action Forces", is to improve the capability and utility of the previously developed SIAF model.

Technical Requirements

This section discusses each of the requirements specified in Technical Requirement Number 1816, which is an attachment to the contract.

1.0 Digital Elevation Data - The SIAF model now has the capability to use digital elevation data from tapes provided by the Defense Mapping Agency. Using subroutines created by the Systems Analyses Group of USACDC, a TOPOCOM tape is unpacked and a disk file is created for the area of operations. This disk file contains elevation data at the maximum resolution. When the SIAF model is run, the elevation data is read from the disk at the desired resolution. Changes were made to the storage sequence for elevation data such that the area of operations can be of any dimensions. The USACDC supplied subroutines are described in Volume III, Sections 10.5 to 10.7 (MAPGEN, CONVERT, ROTATE).

1.1 Tape Supplied - The SIAF sample case was run using a TOPOCOM tape containing elevations from the northern half of map sheet 1755I. This area is part of the Hunter-Liggett Military Reservation near King City, California. The maximum resolution of the data is 12.7 meters.

1.2 Variable Terrain Resolution - The capability is provided for varying the terrain resolution when changing from a reconnaissance mode to a combat mode and vice versa. At the start of the model the elevation data is read from the disk according to reconnaissance resolution by Subroutine RCREAD (See Volume III, Section 10.9). When a combat decision is made, the reconnaissance data is saved on a temporary file while Subroutine CMREAD obtains from the original disk file the elevation data at combat resolution (See Volume III, Section 10.8). Due to the requirement for more storage at greater resolution, the area considered during combat is smaller than the entire area of operations. The center of the combat area is determined dynamically by considering the SIAF position, target position, projected deployment point, and projected engagement point. The best shaped rectangle for containing these points is selected. In case the boundary of this area is crossed during combat the combat area is shifted. This is done by Subroutine OUTSID (See Volume III, Section 10.10). When the simulation returns to a reconnaissance mode, the old elevation data is retrieved by Subroutine CONMIS (See Volume VI, Section 3.14)

2.0 Vegetation, Microrelief, and Soil Shapes - The Terrain Submodel has been reprogrammed to consider vegetation, microrelief, and surface features as polygons. These polygons are input as rectangles, circles, or triangles. Dominant classes are used to describe the area not covered by a polygon. (See Volume II, Section 2.1)

3.0 Antipersonnel Mines - Capability has been added to allow a pre-planned Claymore mine ambush. In the reconnaissance mode the SIAF moves to the mine deployment area and hand emplaces the mines. When a target comes within detection range, control is shifted to the Combat Submodel to consider detailed detection, movement, and lethality of the mines. (See Subroutine MINES in Volume VI, Section 3.18).

4.0 Dynamic Action/Reaction - Provisions have been made to allow dynamic actions and reactions of the two opposing forces in combat. The action is taken following detection of the adversary. When the target detects the attacker, it can either

- withdraw
- deploy in place
- open fire
- ignore the detection
- rotate the formation
- move to best deployment position

The desired option is a user input. If the attacker detects a change in the original status of the target, it can withdraw, change its deployment point, or exchange roles between the maneuver unit and the base of fire. The target then gets to react one more time to a subsequent detection of a change in the attacker's intent. This capability is described in Subroutines REACT and CREAT (See Volume VI, Sections 3.16 and 3.17).

5.0 Internal Communications - An internal communications submodel has been added to the SIAF Combat Model to introduce delay times for communications between maneuver units. Three messages were incorporated for use requiring internal communications. These are "break contact" "change deployment point", and "exchange roles between the base of fire and the moving maneuver unit". For each message an heirarchy of preferred communications means is input. These are selected from visual hand signals, aural communication, radio, smoke grenades, and sending a messenger. Additional messages could be easily added to this list. Internal communications are controlled by Subroutine IC (See Volume III, Section 8.2).

6.0 Hand Grenades - Hand grenades have been added as an alternative weapon for a firefight. Logic was developed such that hand grenades are used at short ranges when the firer is highly suppressed. Existing routines in the Fire Control and Lethality Submodel were expanded to cover the employment decision and the simulation of the lethality of hand grenades. (See Volume VI, Section 2)

7.0 External Fire Support - An extensive effort was undertaken to provide a stochastic, dynamic model of external fire support during combat. Subroutines EFSTIM (See Volume III, Section 5.3) computes the times of arrival of either artillery shells or bombs. This is based on the tactical situation and the input delay times associated with requesting fire

support. Subroutine EFS1 (See Volume III, Section 5.2) stochastically computes the effects of each burst. This is based on input range and deflection errors, ballistic dispersion errors, and lethality data. Provisions are included to adjust firing between volleys when an observer is present.

8.0 Model Demonstration and Validation - This requirement calls for the performance of test runs on the USACDC 6500 computer at Fort Leavenworth, Kansas. These test runs are to be selected from historical examples, field tests, or other appropriate sources. They are to be used to verify the predictive capabilities of the integrated reconnaissance and combat SIAF model. Considerable effort was undertaken to discover appropriate data sources to use for a test case. The SIAF model requires very specific inputs in terms of a detailed operations plan, a tape containing the elevation and vegetation data for the area of operations, the weather, and detailed information on the locations of the targets. In the Combat Model, the SIAF makes decisions based on input decision criteria. Although extensive data was collected by The Vertex Group of the Research Management Corporation on historical SIAF operations, the data requirements for a simulation were not met. In the area of field tests, it was found that the only appropriate field test was the reconnaissance test performed at Hunter-Liggett in 1971. This was previously simulated and the results are presented in Volume I, Section 6. It does not include any of the combat model.

The approach taken by TRW to satisfy this task was in two parts. The first is a detailed validation through an experimental field test of the line-of-sight prediction portion of the model. This was felt important because it is a key driver of the events in the model. For this purpose an experiment was performed at the Hunter-Liggett Military Reservation where line of sight distances were measured from known locations at various headings. This test was simulated using the appropriate portions of the SIAF model with the elevation data tape from the Defense Mapping Agency. Resolution was varied from 12.7, 25.4 and 50.8 meters between elevation points. Results were found to be very close for rolling terrain at the 12.7 meter resolution, with a fast decline in accuracy as resolu-

tion was lowered. The simulation was also performed using the ASARS technique of modelling relief. It was found that the SIAF technique was slightly more accurate at 12.7 meter resolution and that the ASARS technique did not give credible results at lesser resolutions. This test is described in Volume I, Section 8.

The second step in model verification is to present a detailed examination of a sample case. This case is to be demonstrated at the SIAF Executive Overview Meeting on 18 January 1974 at Fort Benning, Georgia. The presentation will show the decisions, events, actions, and results of the SIAF simulation for a typical scenario. A qualitative assessment is to be made by experienced SIAF personnel. The sample case is also presented in Volume I, Section 6.

9.0 Documentation - The documentation for the current contract is provided as augmentation to the documentation from previous contracts. The most recent version was published in December 1972. All routines that were added or modified are to be replaced or added as specified in the augmentation instructions. The result is an integrated whole.

10.0 Train Government Personnel - A training class is scheduled for the week of 14 January 1974 at Fort Benning, Georgia. This class will teach analysts and programmers to understand, use, and modify the SIAF model. The class sessions are to be videotaped and placed in the videotape library at the U.S. Army Infantry School.

11.0 Stop/Restart - Capability has been added to the model to allow several stop points. At the point in the model that the stop point is reached, all of the common blocks are copied onto a disk. The model can then be restarted from that point for later use. This allows playing the combat portion separately and running it many times without repeating the earlier portions of the mission. This is performed by Subroutine RESTRT (See Volume III, Section 10.4).

12.0 Integrated, Debugged Model - The additions to the SIAF Model have been fully integrated with the previous version. The model has been debugged and is operational. At the time of this writing, it is scheduled to be installed on the CDC 6500 computer at Fort Leavenworth, Kansas

within a few days. Since the previous version is currently installed, no difficulties are foreseen.

13.0 Model and Documentation Requirements - Standards for the model and the documentation have been fully followed from USACDC supplement 1 to AR-18-7 Appendix M.

This document, prepared under ARPA Contract DAAH01-73-C-0914, contains changes and additions to Volume I, of the SIAF System Model User's Manual, 15 December 1972; hence, these pages replace or augment appropriate pages of the above referenced document. Table I provides instructions for accomplishing these changes to Volume I. (The pages in this document appear in the order in which they are referenced in Table I. As shown in Table I, for example, Pages i through ix of this document replace Pages i through xiii of Volume I of the User's Manual dated 15 December 1972.

**Table I. Instructions for Changing and Augmenting Volume I, SIAF System
Model User's Manual, 15 December 1972 (Sheet 1)**

Page or Section	Replacement	Augmentation
Pages 1 through 12		Go in front of Volume I
Pages i through ix	Replace Pages i through xi11	
Page 1-1	Replaces Page 1-1	
Pages 2-1 through 2-84	Replaces Pages 2-1 through 2-80	
Pages 3-1 through 3-57	Replaces Pages 3-1 through 3-37	
Pages 4-1 through 4-17	Replaces Pages 4-1 through 4-15	
Pages 5-1 through 5-12	Replaces Pages 5-1 through 5-10	
Pages 6-137 through 6-221	Replaces 6-137 through 6-204	
Pages 8-1 through 8-3n	Replaces Page 8-1	
Page 9-1		Goes behind Page 8-30

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1.0 INTRODUCTION

The Small Independent Action Forces (SIAF) System Model User's Manual consists of six volumes. Volume I provides the information necessary to actually operate the model on the computer while Volumes II, III, V and VI provide the more detailed analysis and discussion of the subroutines.

Volumes II and III contain the reconnaissance routines developed under ARPA Contract DAAH01-71-C-0100 while Volumes V and VI are the combat routines developed under Contract DAAH01-72-C-0305. All of the volumes have been modified under Contract DAAH01-73-C-0914.

These volumes are as follows:

Volume I - Model Description and Programming Guide

Volume II - Reconnaissance Subroutines (Terrain, Weather, Targets)

Volume III - Reconnaissance Subroutines (SIAF Functions and Ancillary Routines)

Volume IV - Model Program Listing

Volume V - Combat Initialization Subroutines

Volume VI - Combat Execution Subroutines

The first volume contains general information concerning the use of the model. The first section contains a qualitative description of the model and associated subroutines. This is followed by sections which present alphabetical lists of the model input and output variables. Next, the model subroutines are presented and summarized (details of each subroutine are contained in Volumes II, III, V and VI). Finally, a sample case consisting in part of the simulation of a test conducted at Hunter Liggett Military Reservation and computer operating procedures are included.

2.0 PROGRAM DESCRIPTION

The SIAF system model is a computer simulation intended for use in evaluating the effectiveness of alternative SIAF concepts. This model essentially accepts as input a military operations plan, such as would be prepared by the military commander for an actual patrol operation, and simulates this operation in a computer environment. It considers a small independent action force which follows this operations plan, and considers both reconnaissance and combat missions. The SIAF model simulates the interaction of the operations plan with the terrain, weather, and enemy situation and considers a total mission from beginning to end. The output of the model is the effectiveness of the particular operation under consideration. During the simulation of the activities and events which occur during SIAF operations, the model calculates statistics pertaining to movement, navigation, surveillance and detection, fire support, supply maintenance, human maintenance, and communications. The specific objectives of this modeling effort were as follows:

- 1) Develop a methodology for modeling a SIAF patrol and implement the methodology.
- 2) Quantitatively measure the reconnaissance and combat effectiveness of alternative SIAF concepts.
- 3) Identify those variables which have the greatest impact on the overall effectiveness of SIAF.

2.1 SIAF MEASURES OF EFFECTIVENESS

In order to satisfy the objectives stated above, one of the first tasks that had to be performed was that of defining appropriate measures of effectiveness for SIAF since these are essentially the outputs of the model. For this purpose, experienced patrol leaders representing various military organizations were interviewed. Based upon these discussions, a list of measures of effectiveness was identified. Some of these measures are shown in Figure 2.1.

As an example of how these measures are applied to a SIAF problem, consider a situation where the user desires to compare the relative merits of two sensor systems, one of which is bulkier and requires a larger crew but is very reliable, versus less reliable equipment which is lighter and

- | | |
|--|---|
| <u>MOVEMENT MOE'S</u> | <u>FIRE SUPPORT MOE'S</u> |
| <ul style="list-style-type: none">● INSERTION SUCCESSES/ATTEMPTS● PATROL DURATION● DISTANCE TRAVELED | <ul style="list-style-type: none">● NUMBER OF SIAF CASUALTIES● NUMBER OF ENEMY CASUALTIES● NUMBER OF TIMES ENEMY IS HIT BY FIRE |
| <u>NAVIGATION MOE'S</u> | <u>SUPPLY MAINTENANCE</u> |
| <ul style="list-style-type: none">● NAVIGATION ACCURACY● TARGET LOCATION ERROR | <ul style="list-style-type: none">● PATROL WEIGHT● PERCENT SUPPLIES CONSUMED● PERCENT AMMUNITION EXPENDED |
| <u>SURVEILLANCE MOE'S</u> | <u>HUMAN MAINTENANCE</u> |
| <ul style="list-style-type: none">● NUMBER OF TARGETS DETECTED● NUMBER OF TARGETS IDENTIFIED● NUMBER OF TIMES SIAF IS DETECTED | <ul style="list-style-type: none">● HUMAN PERFORMANCE DEGRADATION |
| | <u>COMMUNICATION MOE'S</u> |
| | <ul style="list-style-type: none">● COMMUNICATION SUCCESSES/COMMUNICATION ATTEMPTS |

Figure 2.1. Typical SIAF Measures of Effectiveness

requires a smaller crew. For this purpose, measures such as detection per detection opportunity and man days per detection might be selected as being fundamental. Given such data, trade-offs are readily obtained providing useful guidance for research and development decision making. For examining and answering questions pertaining to engagement, the classical measures: casualties, exchange ratio (enemy casualties/SIAF casualties), and survivor ratio (SIAF survivors/enemy survivors) are computed. These measures are often used in the evaluation of competing patrol weapons mixes. Another possibility is that one might not be interested in casualties, per se, but in the number of times SIAF is able to direct fire on the enemy. This measure is also calculated by the model.

Ancillary statistics are intended to be of value for elucidation of cause and effect relationships. As a simple example in the use of these statistics, suppose that it is consistently found that battery life is a principal cause of communication failures. Given typical patrol durations and communication frequencies, a clear justification is available for a development effort aimed at extending power source endurance.

In summary, because of the requirement for the model to apply to general SIAF problems, a large number of measures and ancillary statistics are calculated and provided by the model. Application of the model requires that the user select from these data those statistics which pertain to the particular problem of interest. (Details of the model outputs are provided in Section 4.0 of this volume.)

2.2 MODEL APPROACH AND REQUIREMENTS

The approaches considered for the SIAF model included an analytical model, war gaming, and computer simulation. During this evaluation, a purely analytic model was discarded since it does not have the generality necessary to meet project requirements. War gaming is too slow and unwieldy for most SIAF purposes and is usually valuable only if copious resources and time are available. Field exercises and combat testing were also considered but were ruled out since, at times, conceptual systems must be studied by the decision maker. Simulation using analytical submodels was judged to combine the necessary generality and flexibility with acceptable speed and economy. The

computer simulation method allows for comparing alternative concepts (i. e., different mixes of personnel, material, and procedures) within a scenario of fixed conditions and assumptions. For the SIAF project, it constituted a clear first choice.

Once simulation was selected for developing the SIAF mathematical model, the next task was to prepare specifications for developing this model. The purpose of these specifications was to identify required model inputs, outputs, and submodels. To this end, it was recognized that the measures of effectiveness illustrated in Figure 2.1 depend upon five basic factors which are the terrain, weather, enemy situation, friendly situation in terms of units which support SIAF operations, and the specific SIAF operations plan being considered. Since the basic purpose of the model is to estimate the effectiveness of SIAF operations as a function of changes in these factors, they were essentially identified as inputs to the model. This is illustrated in Figure 2.2.

In identifying the submodel areas, a vigorous effort was made to develop a model which is as realistic as possible. To this end, it was recognized that in the real world a patrol leader prepares an operations plan before he starts the mission. In this operations plan, he considers the functions of movement, navigation, surveillance and detection, fire support, supply maintenance, human maintenance, communications, and command and control. In addition, these are the essential functions the patrol performs during the execution of the plan. Hence, these areas, in addition to terrain, weather, and enemy, were identified as the major areas for submodel development. (See Figure 2.3.)

Although submodels in each of these areas could conceivably be independently developed, a realistic simulation of patrol operation must also consider the interactions of the functions shown in Figure 2.3 with each other and the weather, terrain, and enemy situation. For example, the movement rate a patrol selects will be a function of the terrain and weather, pack weight, and fatigue of the patrol members. This will have an impact on the patrol duration, distance traveled, the visual detection capability of the patrol, and the possibility that the patrol is detected. That is, if the patrol moves rapidly over rough terrain, the patrol surveillance capability is decreased since more attention must be devoted to

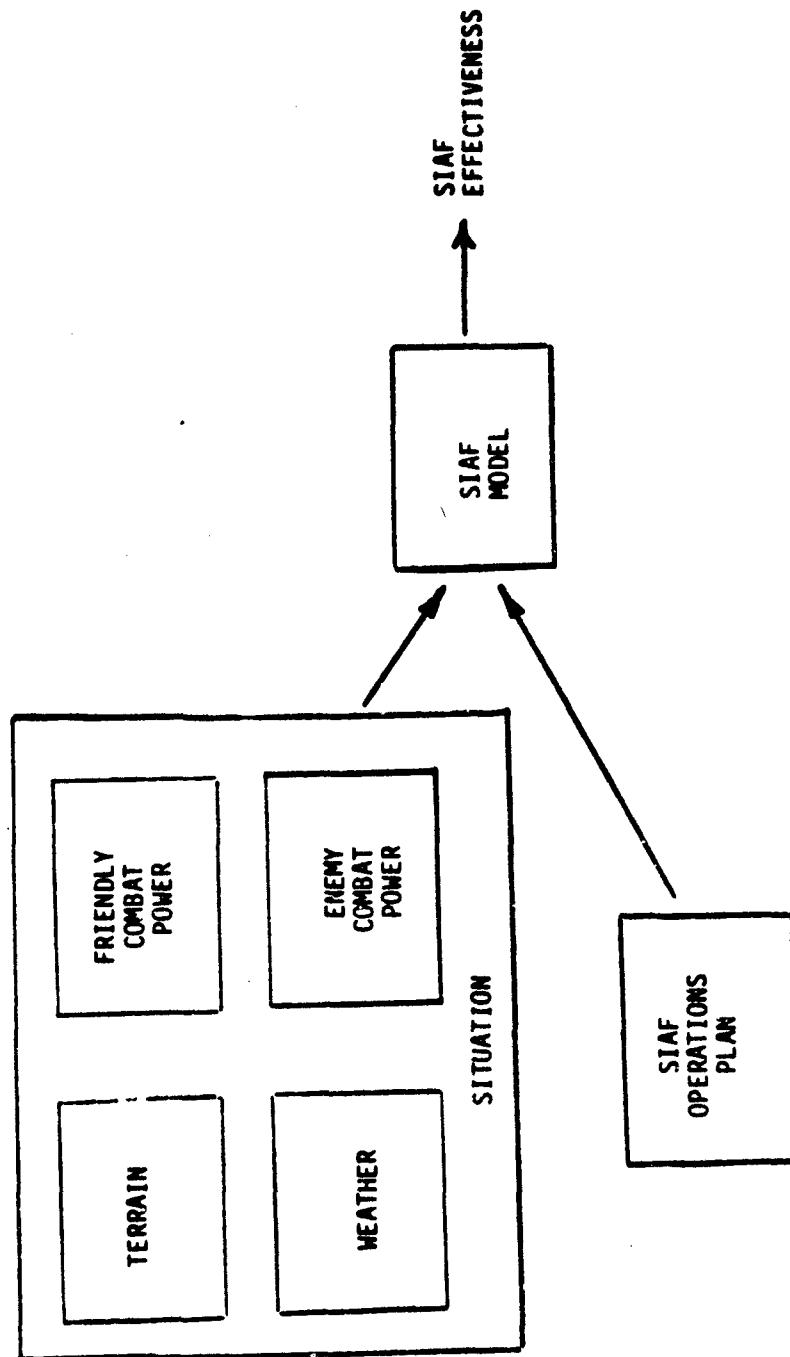


Figure 2.2, SIAF Model Overview

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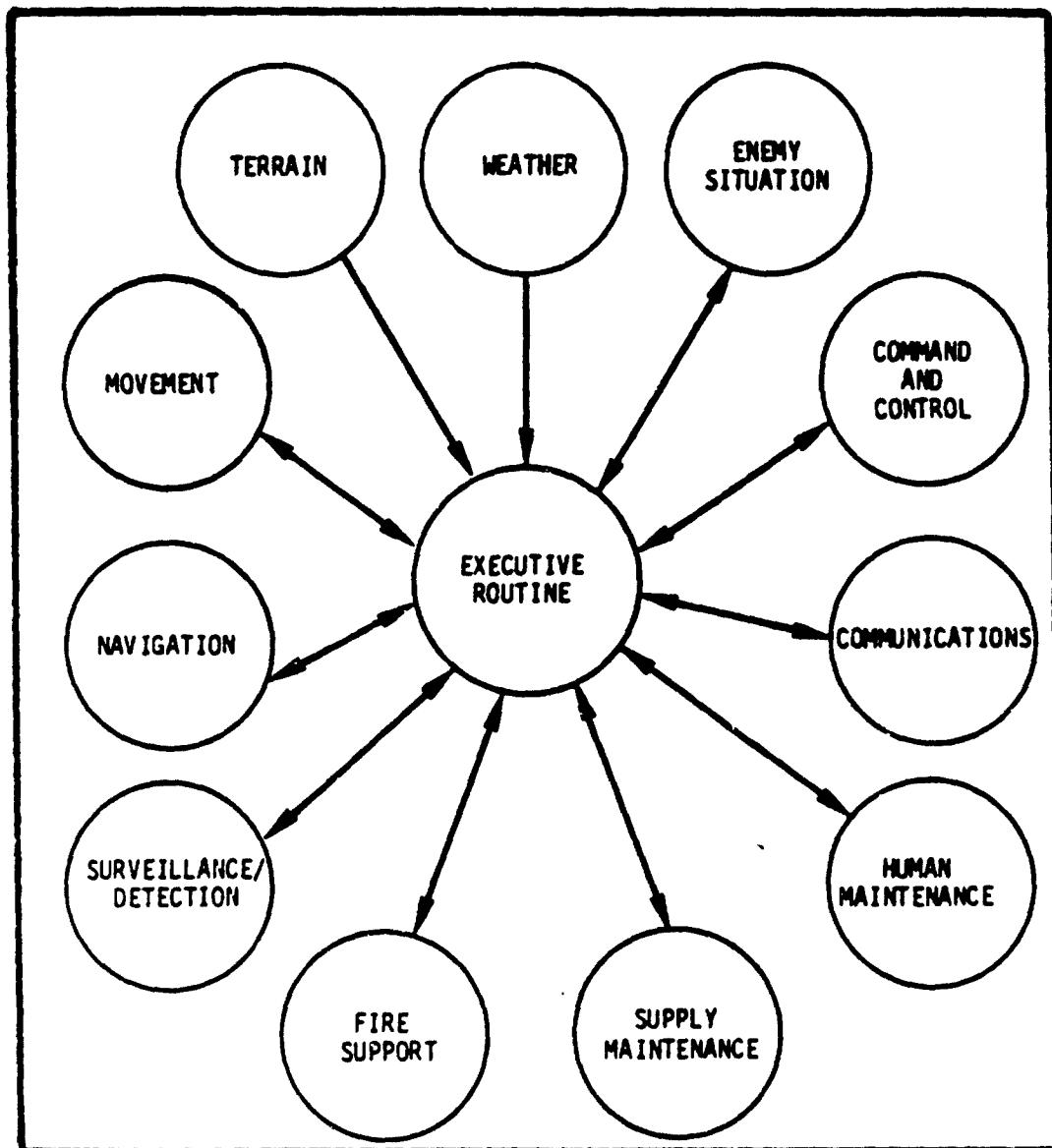


Figure 2.3, SIAF Model Elements

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movement and, consequently, less can be devoted to surveillance. In addition, movement is a cue for visual detection and, hence, increases the possibility of detection by the enemy. This patrol movement rate also influences the energy expenditure rate of the patrol and the food and water requirements which are functions of the temperature and humidity and which, in turn, influence subsequent patrol movement rates. These are examples of the complex interactions which are considered in this model. These interactions are extremely important since equipments and tactics which lead to improvements in some areas could possibly result in a decrease in effectiveness in other areas (see Figure 2.1).

2.3 THE EXECUTIVE ROUTINE

The performance of many of the functions identified previously depend upon physical environment parameters of terrain and weather; as such, these subroutines use this information as input data. The problem here is that the physical environment parameters change with the location of the patrol on a route such as that shown in Figure 2.4; however, the subroutines are constrained to accept only a single value for a particular variable. A simple solution to the problem is to time step the patrol through the route using small time intervals. The idea, of course, is that if the time intervals are sufficiently small, one can assume that the appropriate physical environment parameters are constant during this interval. This approach, however, was not selected since it was felt that this would result in excessive model running time. A time step of 30 seconds, for example, would result in 28,800 time intervals for a patrol with a 10-day mission. Also, visual detection probability changes drastically as a function of light level; hence, it is desirable to examine events on a shorter time interval basis during periods of sunrise and sunset.

The possibility of using a purely distance driven simulation was also considered. However, this approach is complicated by the fact that the patrol may conduct stationary reconnaissance operations for long periods of time and normally reports its position and status to the base on a periodic basis (a function of time). Also, some targets are of such a nature that they may enter and leave the simulation as a function of time,

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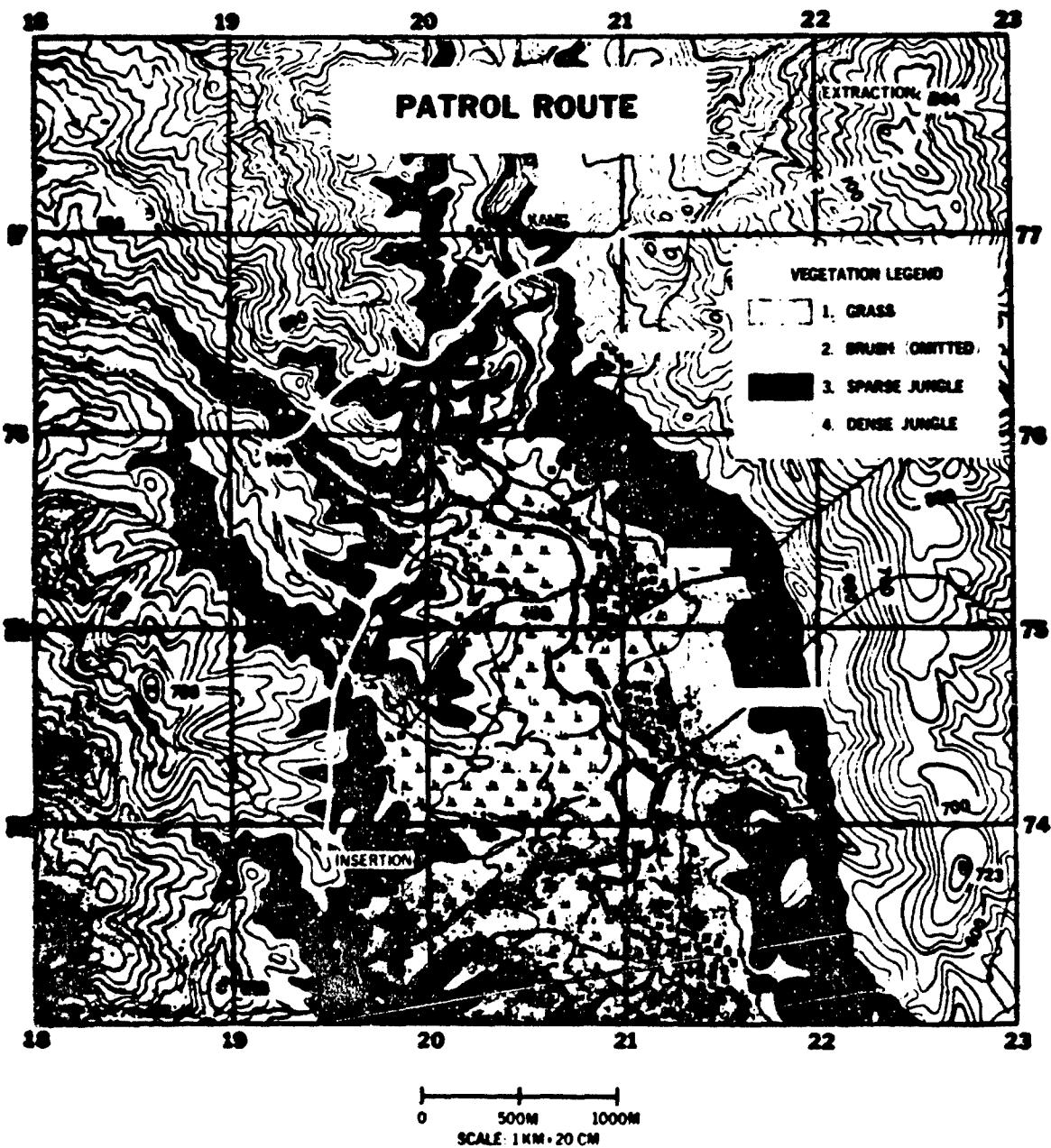


Figure 2.4, Patrol Route

further complicating the manner in which the model is driven. Likewise, a purely event driven simulation was discarded since events such as movement and surveillance and detection are continuously occurring in patrol operations.

The resulting executive routine essentially consists of a marriage of these ideas. The basis of the concept is a grid square approach for inputting digitized terrain data and is illustrated in Figure 2.5. With this approach, a map of the area of operations is divided into grid squares whose resolution is user input. The total area is assigned a vegetation class with exceptions to this as subareas (polygons), in the form of rectangles, circles, and triangles (user input) assigned to the total (see Volume II for discussion of the terrain model). Based upon the axis of advance of the patrol, a segment, defined as the distance of the first grid crossing, checkpoint, obstacle, or polygon crossing, whichever is smaller, is first generated as shown in Figure 2.5(b). The movement rate over this segment is next calculated and a segment time is computed. This segment time is then checked to see if any target movement or communication events are to occur within the segment. If so, the segment is redefined as the distance the patrol moves to the time that particular event is scheduled to occur. Once a segment is defined, statistics pertaining to the functions shown in Figure 2.3 are calculated and accumulated for the segment. After these calculations, another segment is generated and the process is continued until the last checkpoint is reached.

If the SIAF patrol is stationary, a time driver subroutine drives the model and uses criteria of light level and target movement for determining the time step. During periods where the light level is relatively constant and targets are beyond feasible detection ranges, the time interval selected is large. When light level changes rapidly the time step is automatically reduced to account for the change in visual detection capability which occurs in this situation. Again, statistics pertaining to the functions shown in Figure 2.3 are accumulated for each time segment.

In addition to the distance and time segments defined previously, a subset of these called mini-segments are also generated when detections are feasible. Figure 2.6 illustrates this concept which operates as follows: During a simulation of the mission, many of the targets in the area of operations are not feasible of being detected because of the distance between them and the SIAF patrol. For each segment, feasibility of

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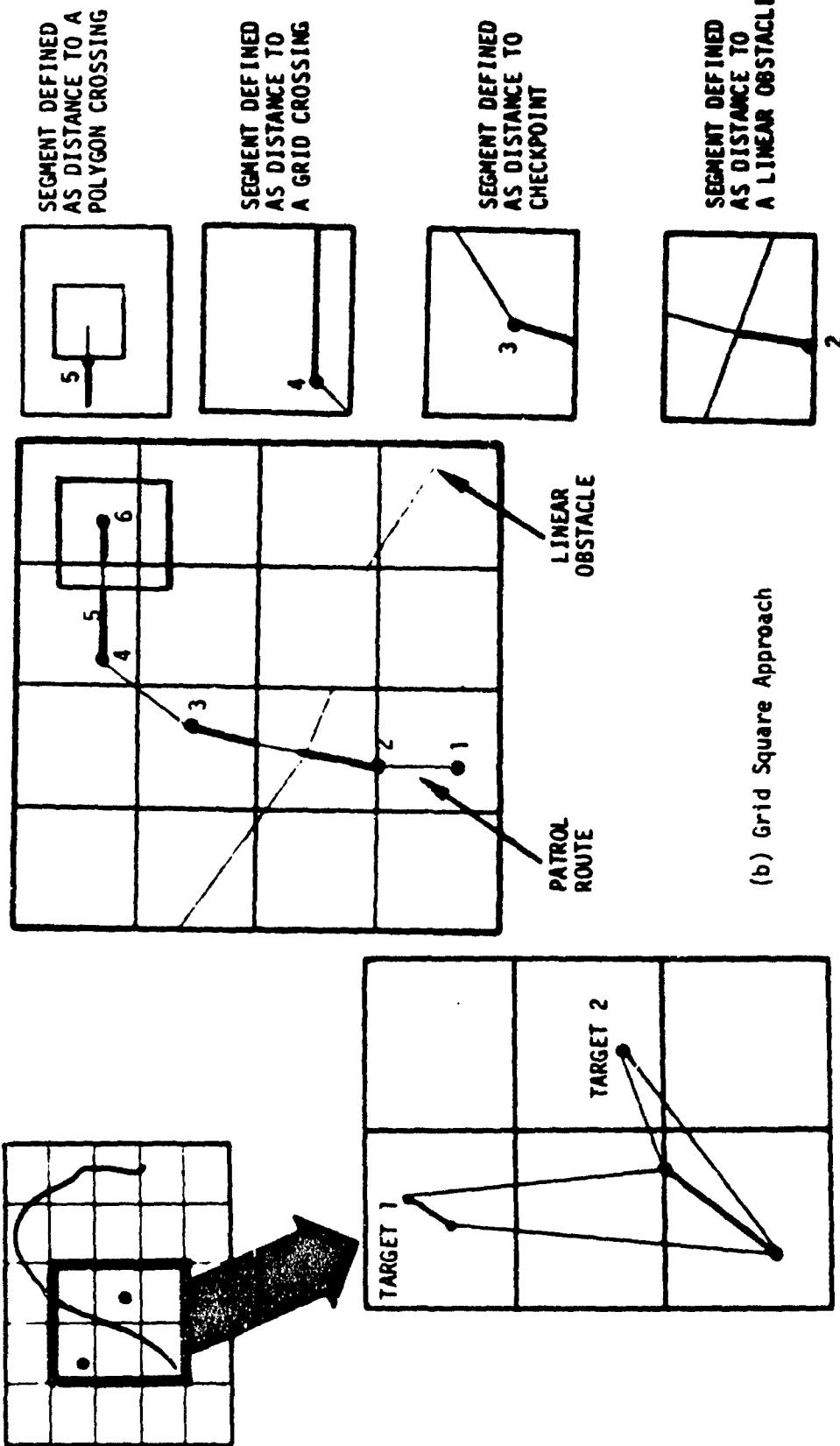


Figure 2.5, Generation of a Distance Segment

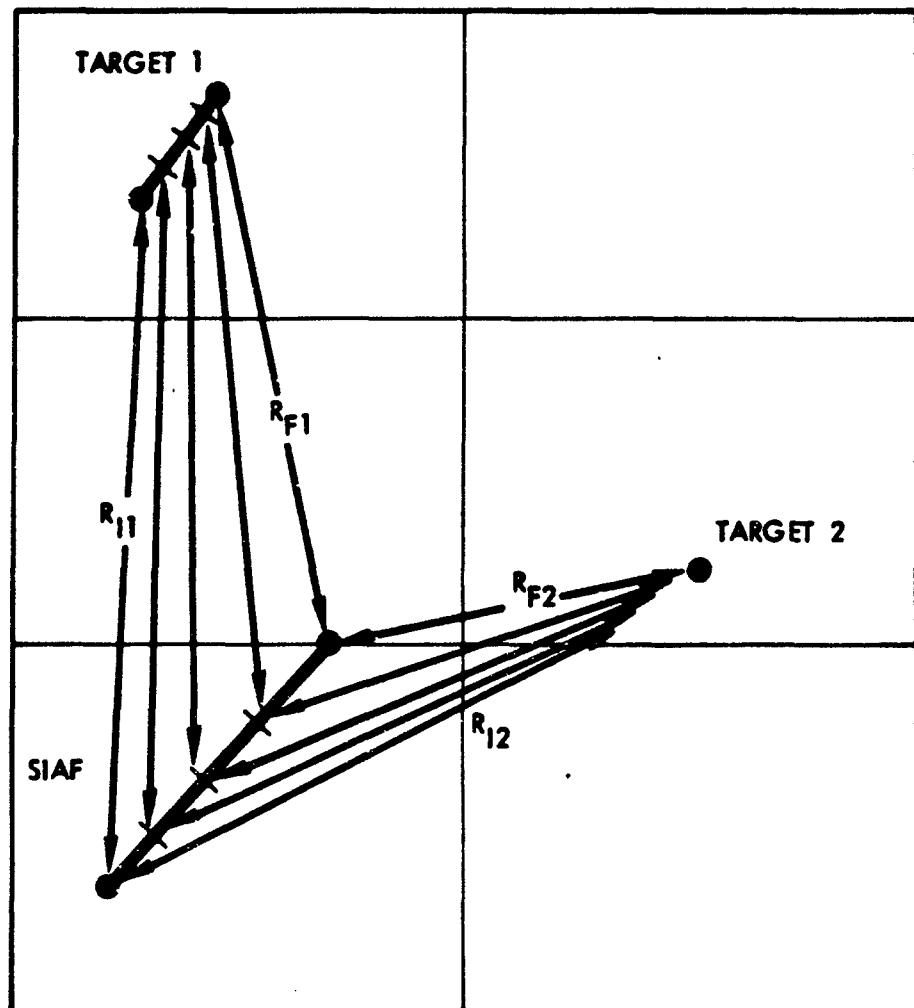


Figure 2.6, Illustration of Mini-Segments

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target detection is checked at the minimum range point and, if not feasible, the target is not considered during the next series of calculations. If feasible, on the other hand, the line of sight between SIAF and the target could change as a function of their relative positions in the segments. In this situation, both SIAF and target segments are divided into mini-segments. The length of the mini-segments are user input. In this situation, the program advances SIAF and each feasible target, a mini-segment at a time, and determines a detection verdict for each mini-segment. For this calculation two options are available: In the first of these, the centroid of the patrol and each target are examined to determine if line of sight exists. If so, then it is assumed that line of sight exists between all members of each group. The user also has the option of treating man-to-man intervisibility in which he can consider the relative location of each individual in both the patrol and target formations (see the Surveillance/Detection Submodel, Volume III, Section 4.0, for the details). This option accounts for the fact that some of the individuals in a particular group may not be visible by all members of the other group. Thus, the user can consider the patrol as one point or consider individuals as desired. These options essentially serve to automatically increase the resolution of the model when required and use less detail resolution when this is appropriate. All of these features serve to minimize the running time of the model and provide the user the option of selecting the resolution he desires.

2.4 SIAF SUBMODELS AND SUBROUTINES

In this section, each of the submodels shown in Figure 2.3 is summarized and the interactions among them are described. The subroutines described herein are listed in Section 5.0 of this volume for ease in referencing. Volumes II, III, V and VI contain detailed information concerning these submodels and subroutines.

2.4.1 SIAF Terrain Submodel

The purpose of the SIAF Terrain Submodel is to provide a representation of the terrain for use in line-of-sight and slope calculations,

and for considering factors such as the vegetation at various points in the area of operations as required by the other subroutines. This submodel considers the following factors:

- Relief
- Vegetation
- Obstacles and Cultural Features
- Micro-Relief
- Surface Materials

The manner in which these factors are treated in this submodel is summarized below.

Relief

The basic approach for treating relief is to divide the map into grids, whose size is a user input. The grid elevation data is obtained from a military "TOPOCOM" tape of the area of operations. The tape contains digitized elevation data of various areas and is of a high resolution. Thus, the elevation data represents the elevation at each corner of the grid square. Based upon these data, the model generates a hyperbolic surface between the points for each grid square. Figure 2.7 illustrates this surface for two grid squares. In order to explain and illustrate the results which are obtained with this approach, an ionic model of four grid squares was developed. Figure 2.8 is a photograph of this model. It illustrates the curved surface which is obtained from the four-corner input data.

As an example of the impact of various resolutions on the accuracy of the relief representation, a study was made using Army map sheet 1755 IV NE, Alder Peak California, 1:25,000. Figure 2.9 shows actual contours and the contours which result from this model using 100-meter resolution. These 100-meter data were obtained from a listing of an Army digitized terrain tape of the area. The Figure illustrates how much of the section of road can be observed from the observation post for both sets of contours; there is considerable error in the results obtained from the model when the 100-meter resolution is used. Figure 2.10 shows the same situation for 50-meter resolution. These illustrations show that accuracy

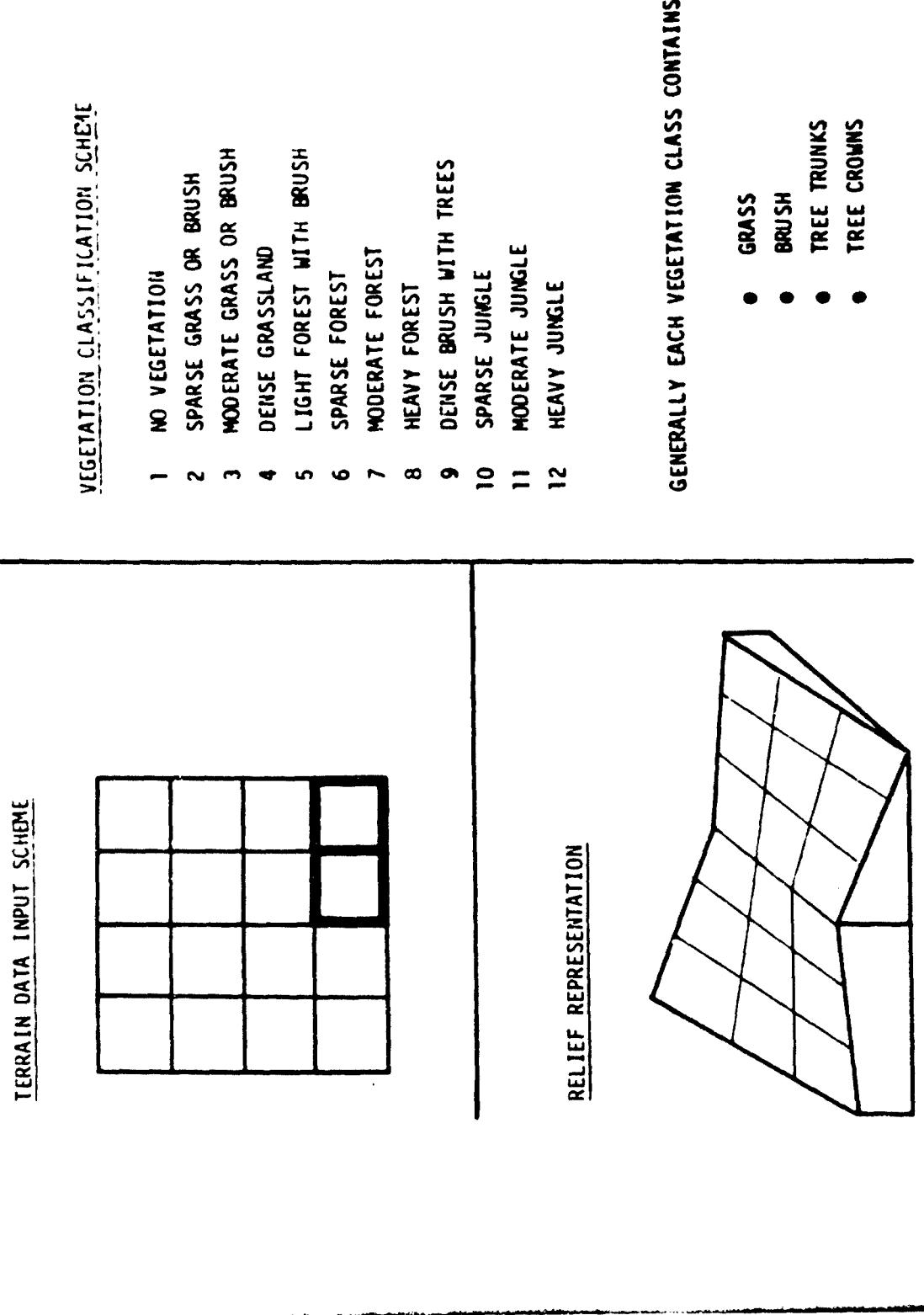


Figure 2.7, Terrain Model - Relief and Vegetation Summary

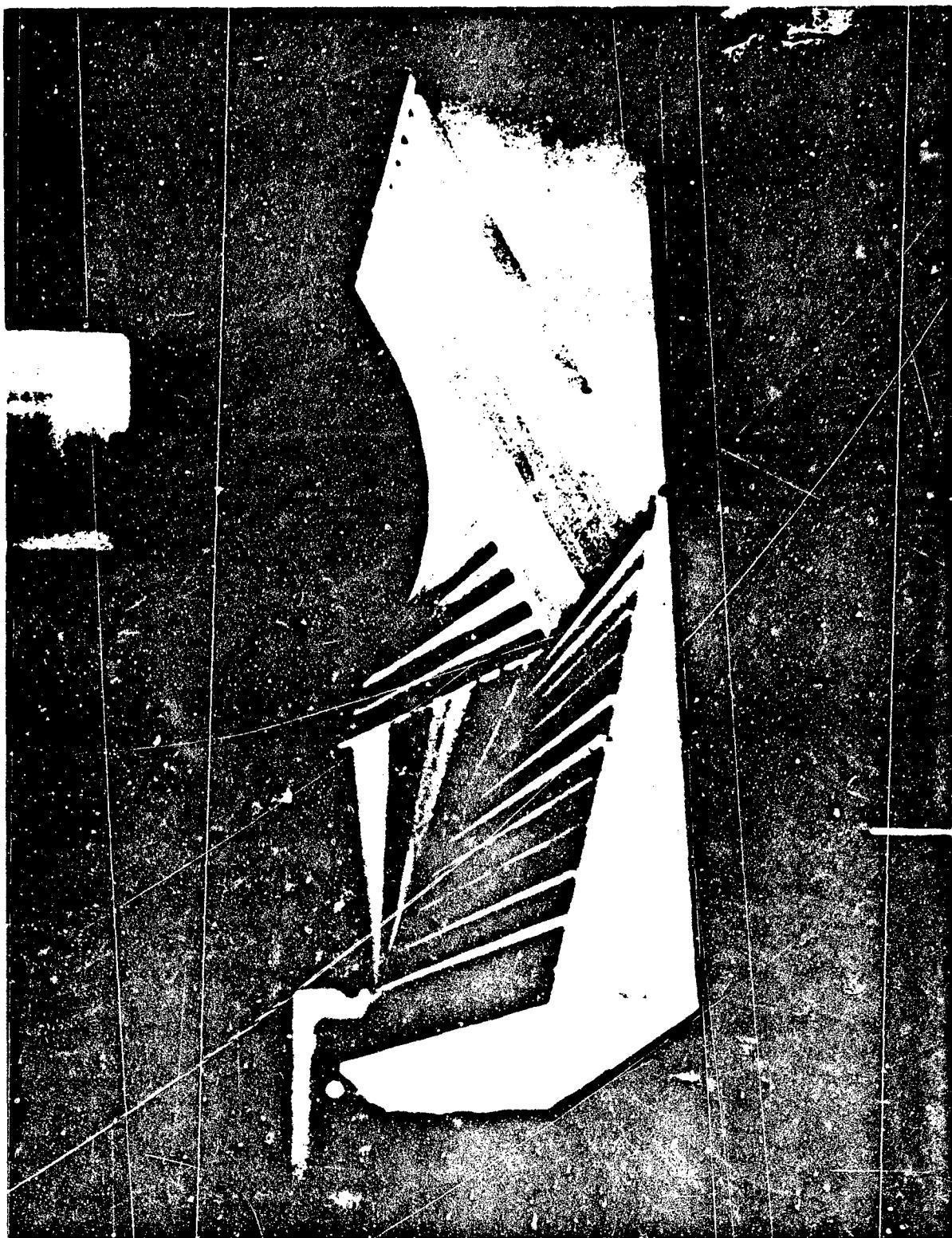


Figure 2.8, Photograph of an Iconic Model of the
SIAF Mathematical Terrain Model

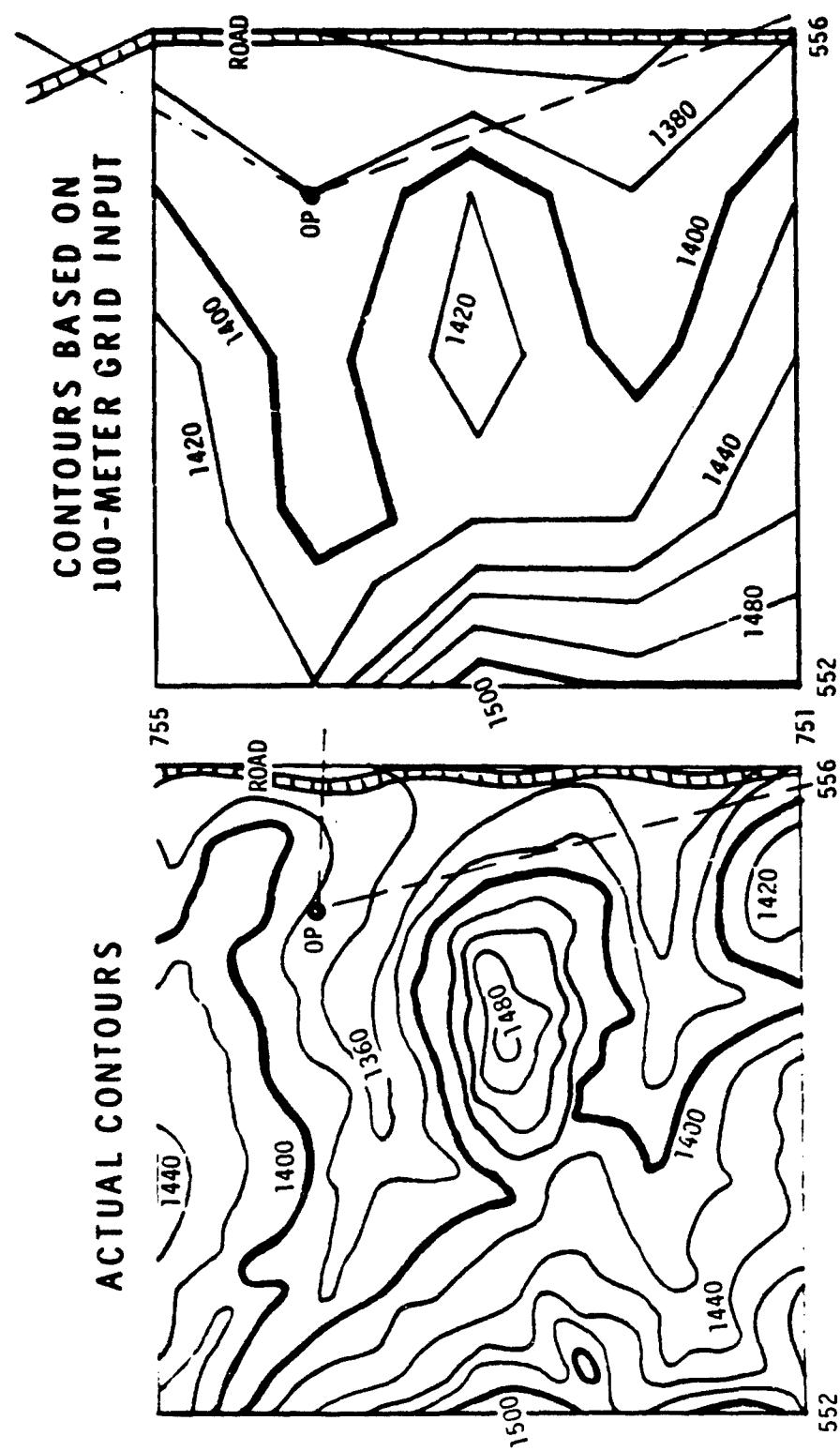


Figure 2.9, Comparison of 100-Meter Resolution Digitized Data with Map Contours

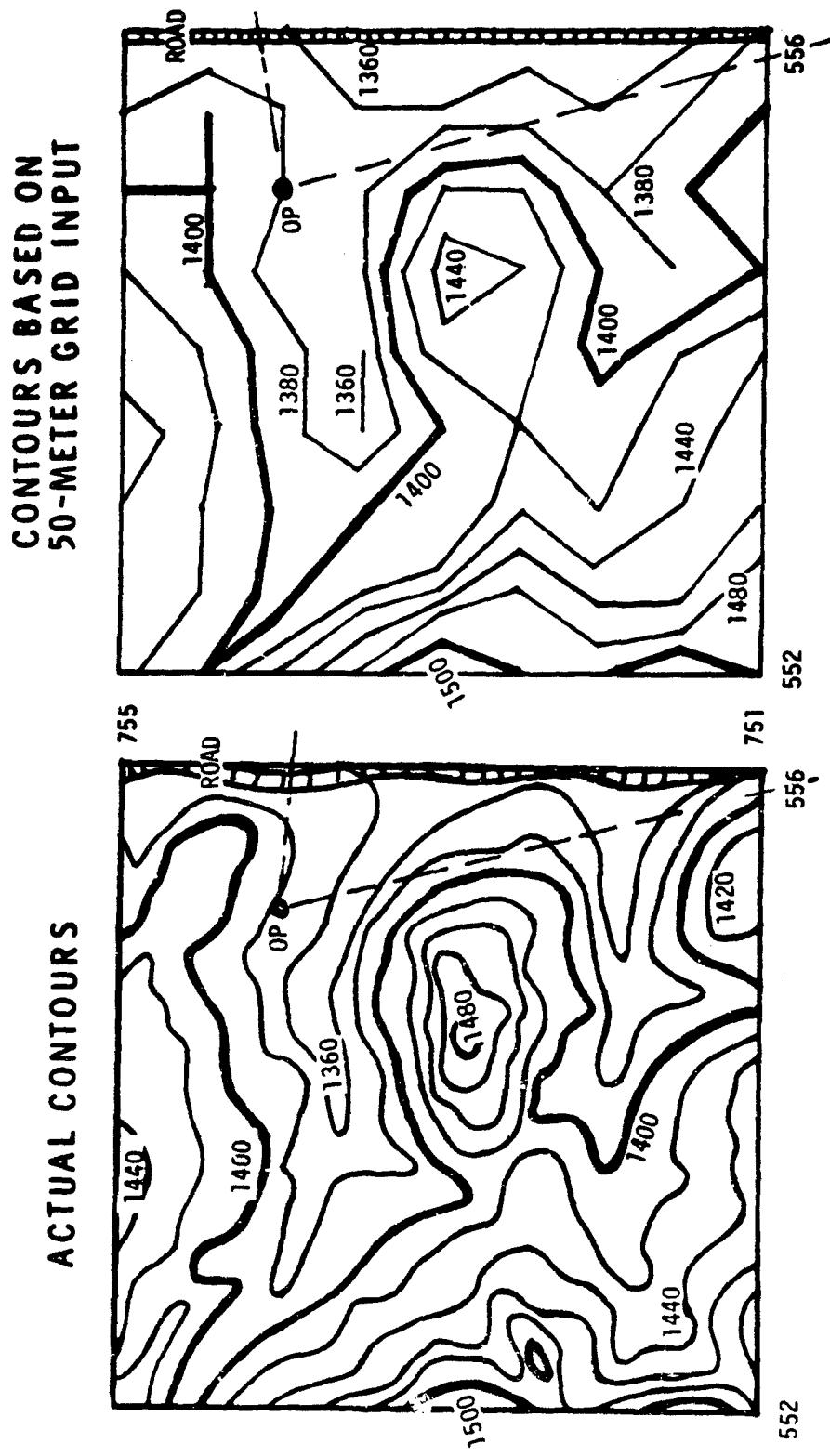


Figure 2.10, Comparison of 50-Meter Resolution
Manual Data with Map Contours

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of relief representation is considerably better with 50-meter resolution. It is interesting to note that the terrain for which this comparison was made is fairly rugged. Hence, the preceding analysis probably represents a worst-case situation.

Further comparison of the relief part of this model to field experiments is presented in Section 8.0 of this model.

Vegetation

The problem of appropriately modeling the vegetation factor of terrain for SIAF was approached in two steps. First, it was necessary to develop an appropriate vegetation classification scheme. Second, it was necessary to determine the manner in which this scheme could best be used, in conjunction with the relief portion of the Terrain Submodel.

The vegetation classes considered in this submodel are summarized in Figure 2.7. As shown in the figure, each class of vegetation consists of a certain amount of grass, brush, and trees. The features within each class are assumed to be distributed at random. To the total area for which elevation is input is assigned one number from 1 to 12 to represent the class (dominant) of vegetation to be found within the area. Exceptions to this are inputted as subareas in the form of triangles, circles, and rectangles and are also assigned a number from 1 to 12 and are used to represent subareas of vegetation other than the dominant within the total area.

In developing this classification scheme, an attempt was made to include consideration of the types of vegetation which might be found in various parts of the world. In addition, an attempt was also made to gather realistic data concerning the density and size of the vegetation features within each class. To this end, various references (indicated in Volume II) were studied. The data in these references were augmented by a field trip to Hunter Liggett Military Reservation where aerial photographs of the area were obtained and a ground survey was conducted.

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Figure 2.12, Class 5 Vegetation: Light Forest with Brush

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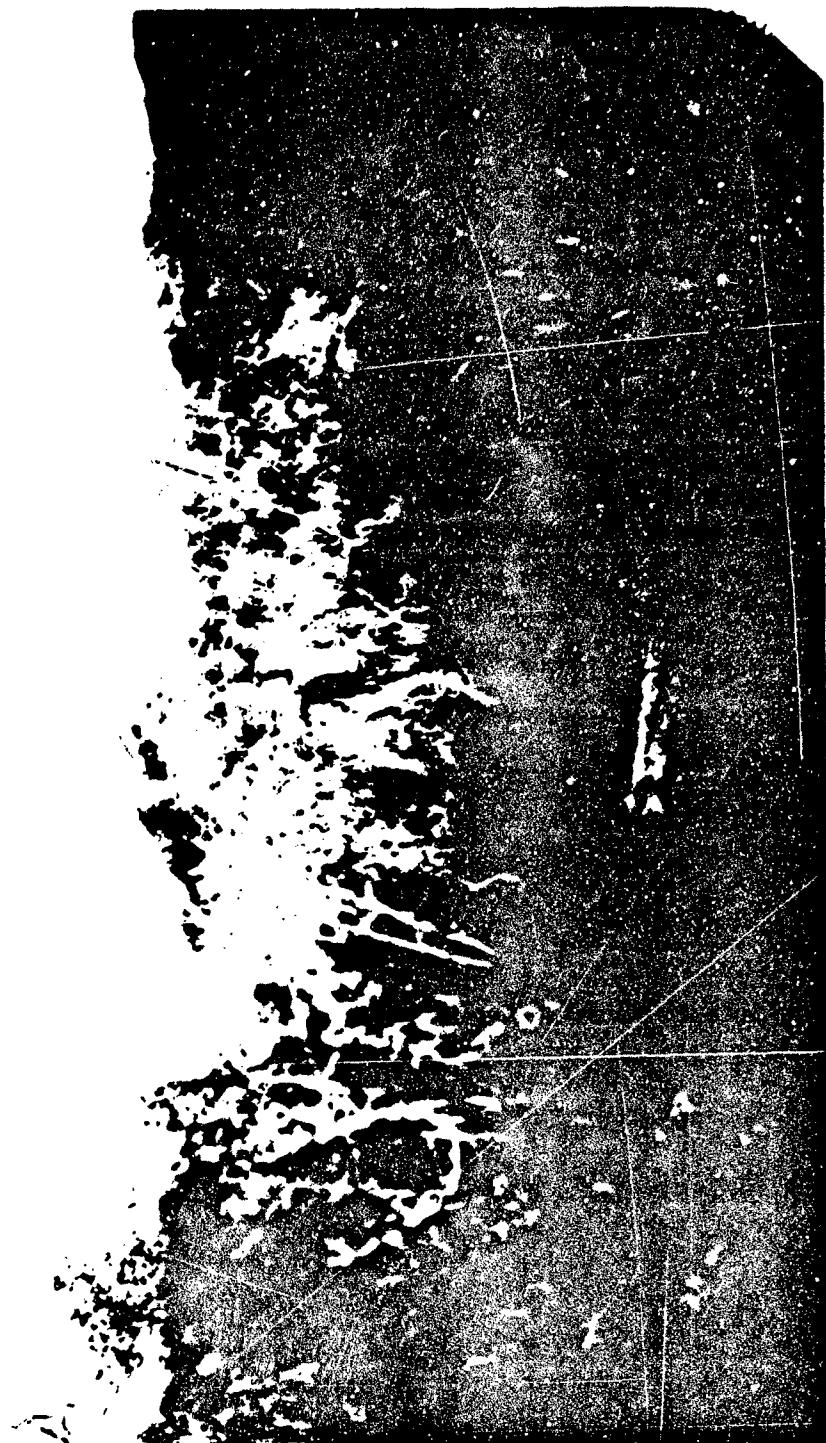


Figure 2.13, Class 3 Vegetation: Moderate Brush

Figure 2.11 presents one of these aerial photographs while Figure 2.12 provides a closeup view of the vegetation in the square of Figure 2.11. Figure 2.13 is a view of the vegetation in the area of the circle of Figure 2.11. The vegetation shown in the photograph of Figure 2.12 was subsequently defined as class 5, light forest with brush. Results of the ground survey indicated that there were approximately 63 features of brush per 50- by 50-meter square, each feature being approximately 2 meters wide and 3 meters high. In addition, the 42 trees in this area were judged to be an average of 10 meters high with 3-meter wide crowns. The vegetation shown in Figure 2.13 was found to be considerably different as might be expected from an inspection of Figure 2.11. This area was defined as class 3, moderate grass or brush, and was found to consist of 500 features of brush per 50-meter square. Each feature was judged to be a sphere with a diameter of approximately 1.5 meters.

As an example of the impact of the polygon (triangles, rectangles, and circles) overlay method of vegetation representation, Figure 2.14 shows the accuracy of realism that can be obtained through this method. As can be observed, considerable accuracy can be obtained.

Obstacles and Cultural Features

For the purposes of modeling, cultural features and obstacles are treated in the same manner as vegetation in that a polygon configuration resembling the feature or obstacle is overlaid on the area and is assigned a number which indicates the type of area obstacle. Cultural features such as roads, on the other hand, are input by means of straight line segments. Figure 2.15 summarizes obstacles and cultural features considered in this submodel and presents an example which illustrates the input procedure described above.

Surface Materials

The surface materials or soil classifications considered in this submodel are summarized in Figure 2.15. In preparing the inputs to the submodel, a dominant soil classification is assigned to the area of operations. Thus, if the area is considered to consist mainly of sand, then the number 2 would be associated with the area. Exceptions to this are input by a means of subareas in the form of circles, rectangles, and triangles illustrated in Figure 2.15. Thus, for example the shown, the cross-hatched area would consist of high plasticity silt (class 0) while the remainder of the area would have the dominant soil class (class 2).

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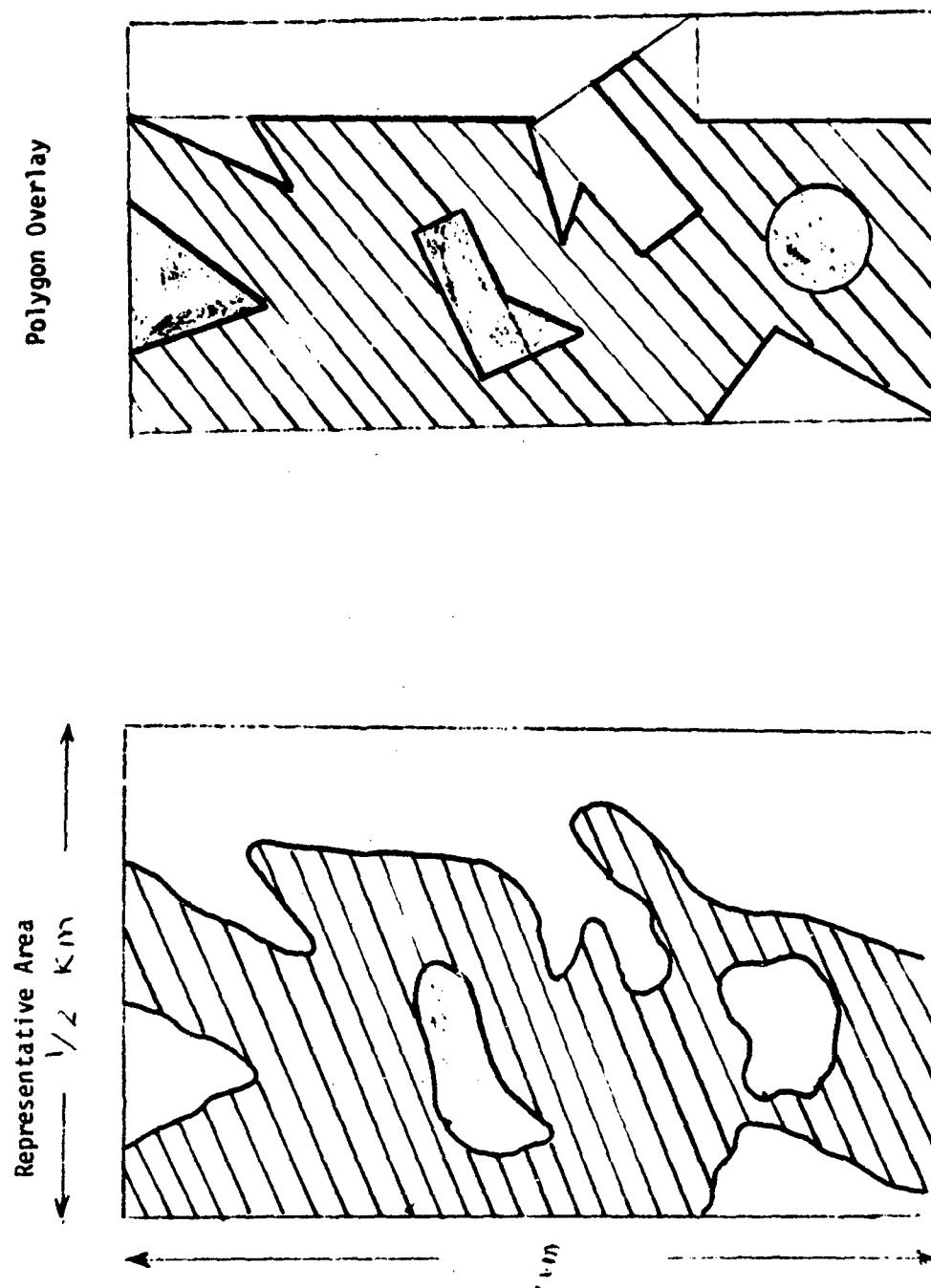


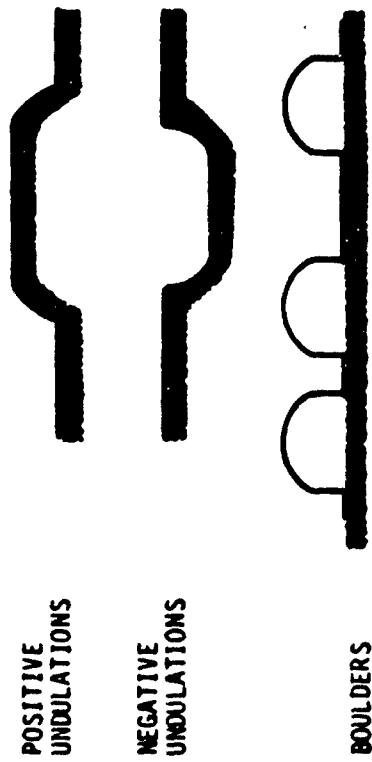
Figure 2.14. Effect of Polygon Overlay on Vegetation Representation

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MICRO RELIEF (5 CLASSES)



OBSTACLES AND CULTURAL FEATURES

AREA

LINEAR

- SWAMPS
- RIVER
- CULTIVATED LAND
- STREAM
- VILLAGES
- RAVINE
- DIKE
- CANAL
- CLIFF
- ROAD
- TRAIL
- LAKE BOUNDARIES

POLYGON BY EXCEPTION METHOD OF INPUTTING SOIL, MICRORELIEF AND VEGETATION

SOIL CLASSIFICATION

- 1 GRAVEL
- 2 SAND
- 3 CLAY - LOW PLASTICITY
- 4 CLAY - HIGH PLASTICITY
- 5 SILT - LOW PLASTICITY
- 6 SILT - HIGH PLASTICITY
- 7 PLOWED EARTH (SOFT)
- 8 FROZEN GROUND

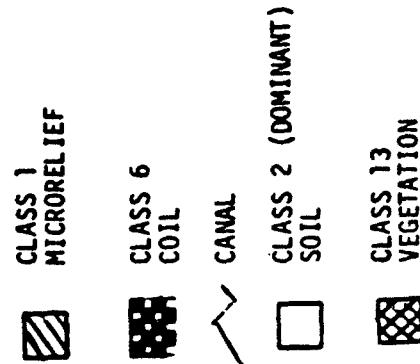
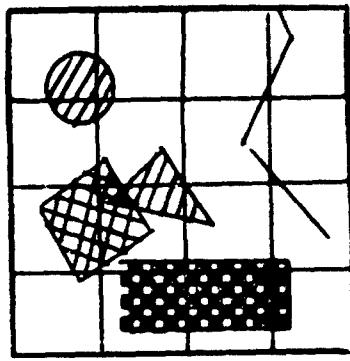


Figure 2.15. Terrain Model - Additional Factors Considered

Micro-Relief

In addition to the factors considered in the foregoing discussion, certain terrain irregularities must now be considered. Figure 2.16 photographically illustrates some of these irregularities that exist at the Hunter Liggett Military Reservation. These irregularities are called micro-relief for this model. Here, positive undulations, negative undulations, and boulders are considered. Each class of micro-relief consists of a combination of these features of varying densities and sizes. These features are assumed to be distributed randomly within an area; they are input by means of circles, rectangles and triangles as illustrated in Figure 2.15. Thus, the cross-hatched region, as shown in Figure 2.15, would consist of that class of micro-relief desired by the user while the remainder of the area of operations would consist of a dominant micro-relief class.

Summary

To illustrate how these factors of terrain are combined in the model, Figure 2.17, which presents a top view of six grid squares, was developed. A profile view of this situation is shown in Figure 2.18. A study of Figure 2.17 and 2.18 indicates that line of sight could be obstructed for a variety of reasons. For example, line of sight could be obstructed by relief, an obstacle, features of brush, crowns of trees, or trunks of trees. The relief and obstacle line-of-sight decision is essentially a deterministic one which is based upon the geometry of the situation while the line-of-sight verdict due to vegetation and micro-relief is a probabilistic one. Furthermore, this probabilistic verdict depends upon the relative location of the vegetation features and the micro-relief features with respect to the observer and the target. For example, features close to the observer tend to have a greater impact on concealment probability than do those further away. See Sections 2.5, 2.10, and 2.11 in Volume II for concealment analysis and description of equations.

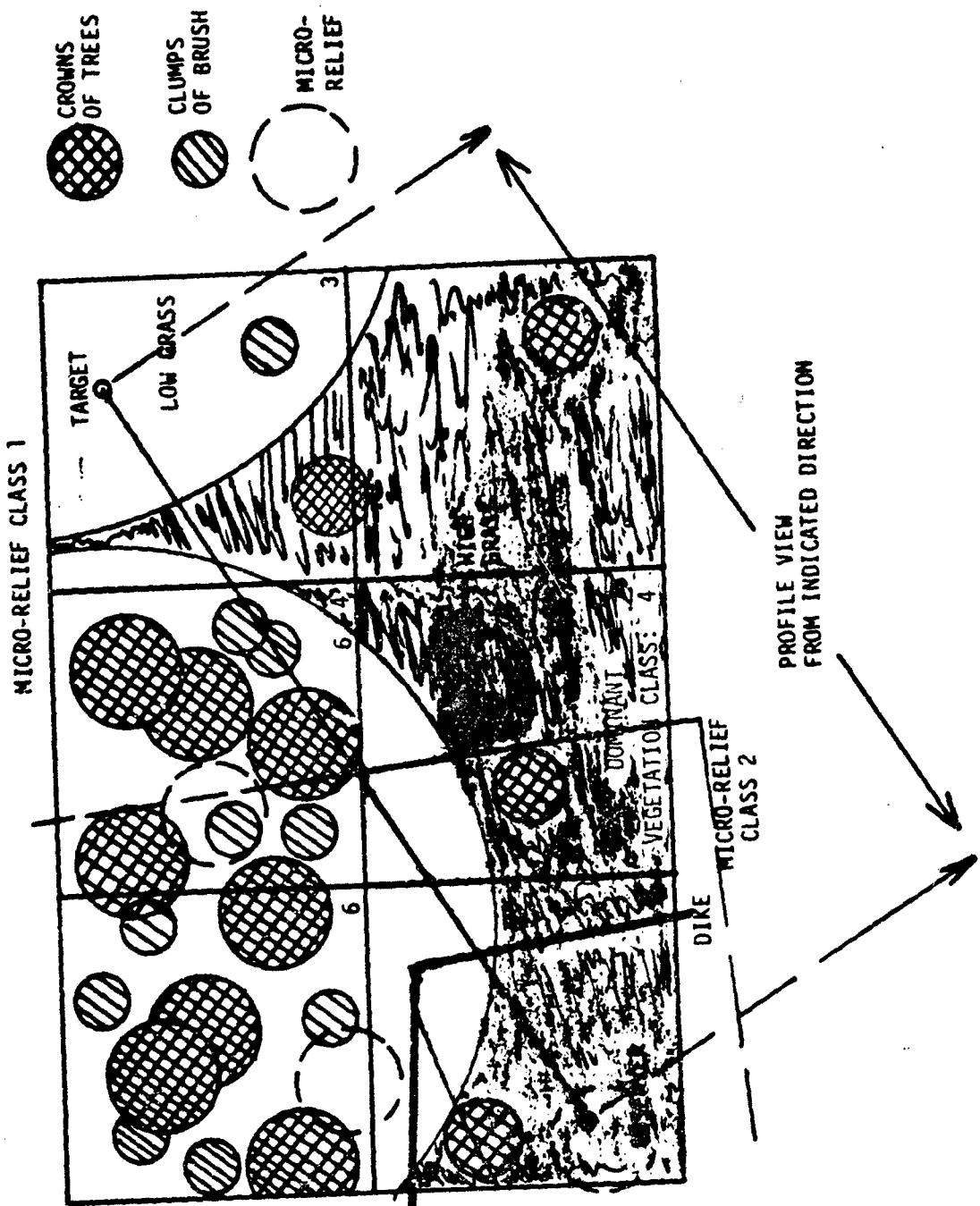
This total line-of-sight decision calculation is made by Subroutine TERCON which in turn calls eight other terrain subroutines as illustrated in Figure 2.19. Here, Subroutines MICSOL and MITFEA essentially determine if a target is on a micro-relief feature or on an obstacle such as a swamp. Both of these factors are used to adjust the height of the target.

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Figure 2.16. Micro-Relief Features



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Profile View from Indicated Direction

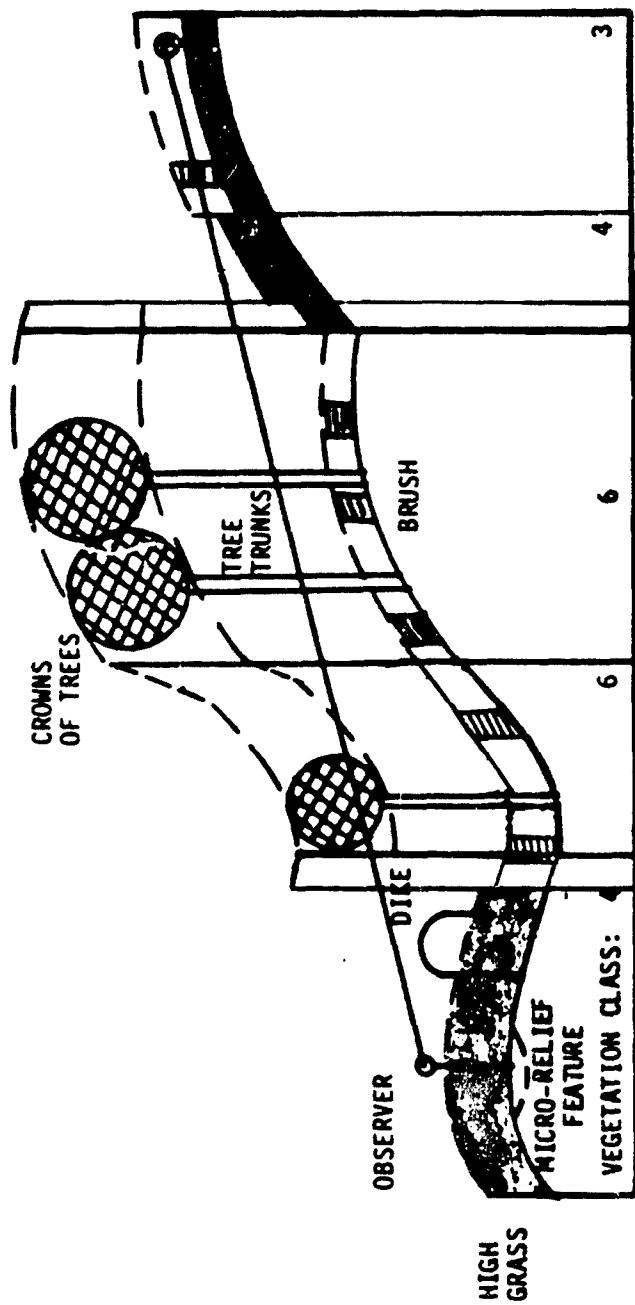


Figure 2.18, General Line-of-Sight Situation "profile View"

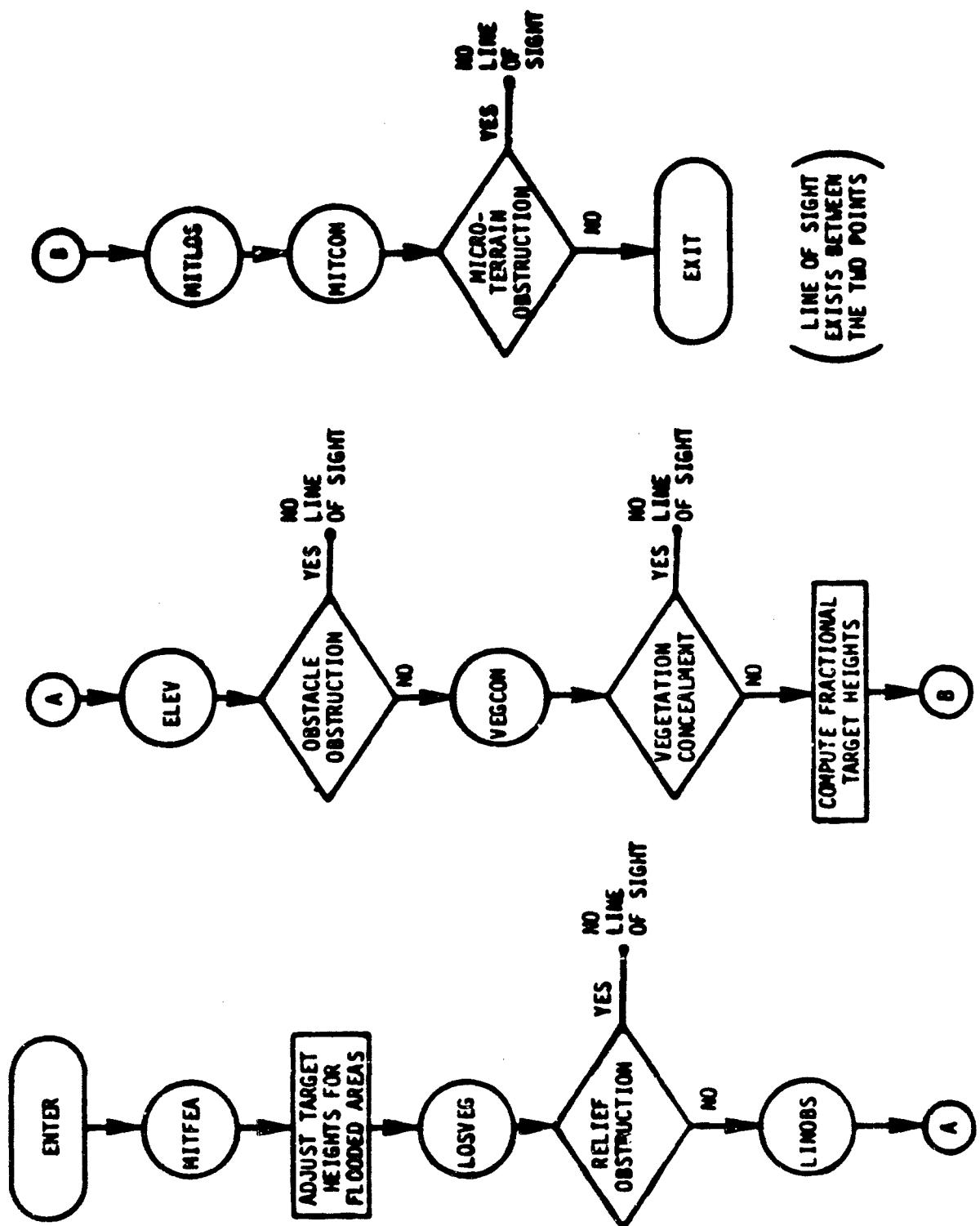


Figure 2.19, Terrain Concealment Subroutine (TERRCON)

appropriately. Next, Subroutine LOSVEG is called and determines if there is a relief intercept between the two points of interest. If so, a no-line-of-sight verdict is returned by the subroutine. If there is not a relief obstruction, Subroutines LINOBS and ELEV are next called. These subroutines essentially determine if there is an obstacle between the two points of interest and determine the elevation of the obstacle. Based upon these calculations, a check is made for an obstacle obstruction and a line-of-sight/no-line-of-sight verdict is again made as shown in Figure 2.19. If line of sight exists, then Subroutine VEGCON is called to check the vegetation concealment. As part of this calculation it could turn out that a target is partially concealed because of vegetation. If so, the area of the target visible is calculated. The final two subroutines, called MITLOS and MITCON, determine if there is a micro-relief obstruction between the two points of interest.

In summary, Subroutine TERCON determines if there is line of sight between any two points in the area of operations. The line-of-sight verdict is based upon an examination of relief, obstacles and cultural features, vegetation, and micro-relief which exists between the two points under consideration.

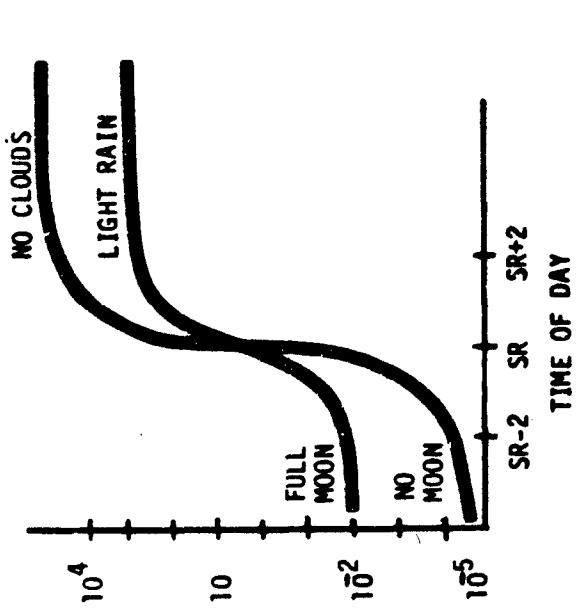
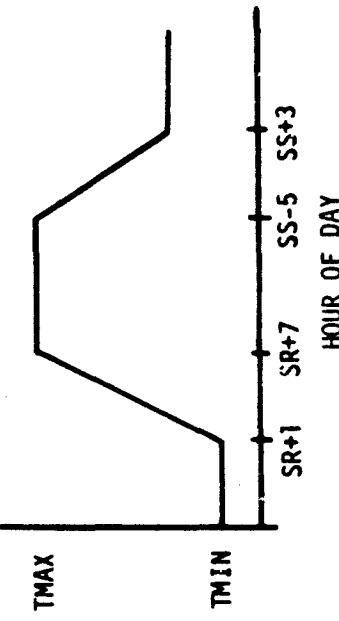
2.4.2 SIAF Weather Model

Figure 2.20 shows Weather Subroutine variables for weather classification, light level, temperature, and wind velocity. In the model, these variables are functions of time. When a subroutine needs a particular weather variable, the model simply examines the weather variables at the time in question and selects the appropriate values. The 11 classes of weather which vary from clear to heavy fog are input by the user as a function of time. Figure 2.21 is an example of the procedure to input variables for the Weather Subroutine.

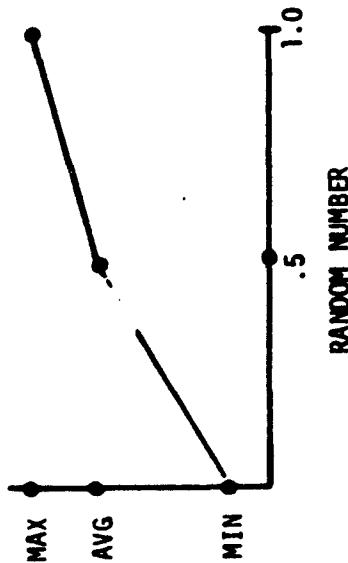
The light level data of Figure 2.20 (foot lamberts versus time) were obtained from Reference 1 and, as shown, varies rapidly near sunrise (SR) and sunset (SS). (Only sunrise is illustrated in the Figure since sunset is essentially the reverse of this.) The model also considers the interaction of these basic light level data with the weather in that the light level is degraded appropriately depending upon the weather conditions which exist at the time the light level is sampled.

WEATHER CLASSIFICATION SCHEME

- 1 VERY CLEAR
- 2 CLEAR
- 3 LIGHT OVERCAST
- 4 HEAVY OVERCAST
- 5 HAZE
- 6 LIGHT RAIN
- 7 MODERATE RAIN
- 8 HEAVY RAIN
- 9 LIGHT FOG/DUST
- 10 MODERATE FOG/DUST
- 11 HEAVY FOG/DUST

LIGHT LEVEL (FOOT LAMBERTS)TEMPERATURE
(TYPICAL CHARACTERISTIC)*

*Use local data for time scale.

WIND VELOCITY

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DAY	MOON RISE SET	MOON TYPE	TEMPERATURE MAX MIN	RELATIVE HUMIDITY MAX MIN	WIND VELOCITY (KNOTS)			WIND DIRECTION
					MIN	Avg	MAX	
01	1148	0156	1st Q.	78°F	30°F	98%	24%	0 2 7 360
02	1249	0235	"	84	32	98	16	0 0.25 2 330
03	1349	0307	"	78	32	99	18	0 0 0 0
04	1446	0335	"	60	41	99	45	0 1 8 320
05	1542	0400	"	59	32	99	46	0 2 8 060
06	1638	0423	"	68	26	99	27	0 3 12 090
07	1733	0446	"	66	32	98	32	0 5 18 250

Figure 2.21. Example Weather Input Values

The temperature curve was derived empirically from data collected at Los Angeles Civic Center and Hunter Liggett Military Reservation. Examination of these data revealed that the temperature begins to increase approximately one hour after sunrise (SR) and reaches its maximum value about seven hours after sunrise. Then it stays relatively constant with time, starts decreasing approximately five hours before sunset (SS), and reaches its minimum value at three hours after sunset. Based upon these observations, the temperature model shown in Figure 2.20 was constructed. The maximum and minimum temperatures and the time scale for any locality for each day of the operation would be input by the user; then the model will generate a curve as shown in the Figure. Relative humidity (not shown) is treated in a similar manner, but it decreases as temperature increases.

Finally, the maximum, average, and minimum wind velocity is input by the user, and a random number is drawn to determine the appropriate velocity. Wind direction is input as constant. This sample procedure essentially accounts for gusts. If a constant wind scenario is desired, the user can simulate this by equating the minimum, average, and maximum velocities.

2.4.3 Enemy Situation

Three options are provided in the model for treating the enemy. These are illustrated in Figure 2.22. As shown in the Figure, the user can have fixed enemy positions, can simulate an enemy movement in a random manner within a circular area of operations, or can simulate the enemy moving on a pre-planned path. For the random movement within a circle on the fixed targets, the user can either pre-select the initial positions of these targets or can have the computer select these positions at random. Targets such as trucks, personnel, and enemy caches are simulated by inputting appropriate target characteristics. Analyses and discussion of target movement are contained in Sections 4.1 and 4.3 of Volume II.

Subroutines pertaining to the SIAF functions are described next. These subroutines are exercised for each segment as discussed in Section 2.3.

2.4.4 Movement

This subroutine calculates the movement rate of the patrol to be consistent with maintaining good surveillance and detection capability. Figure 2.23 presents a simplified flow diagram of how this movement rate,

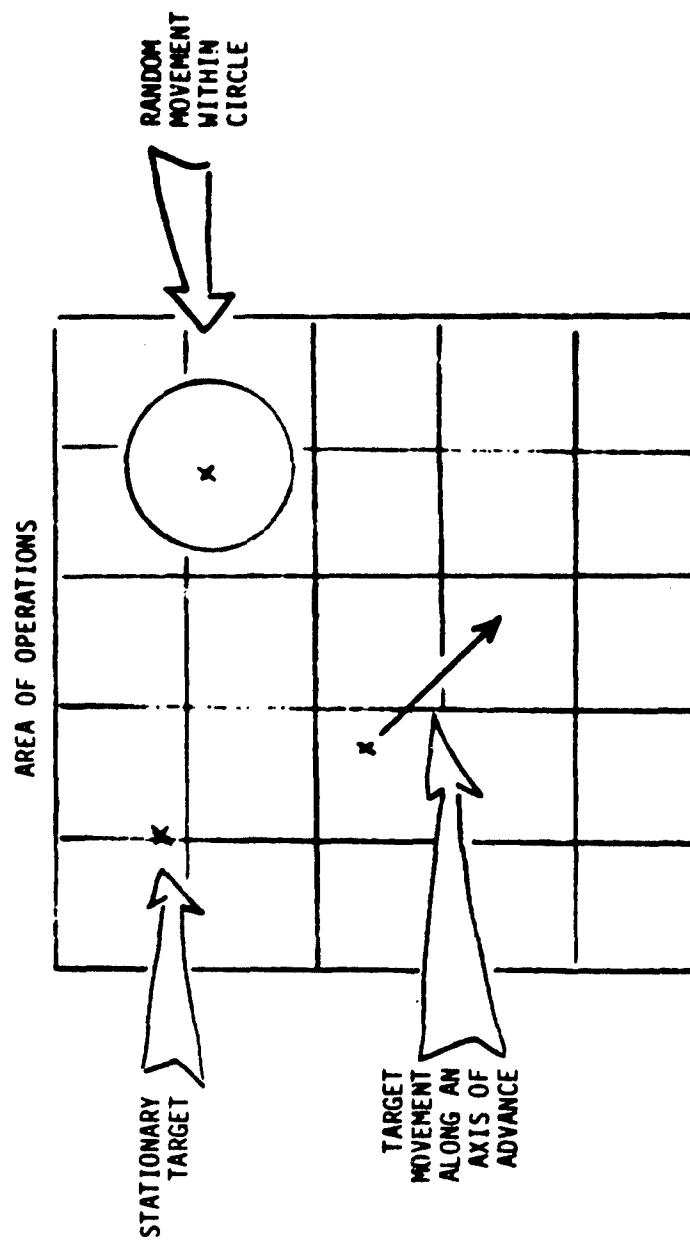
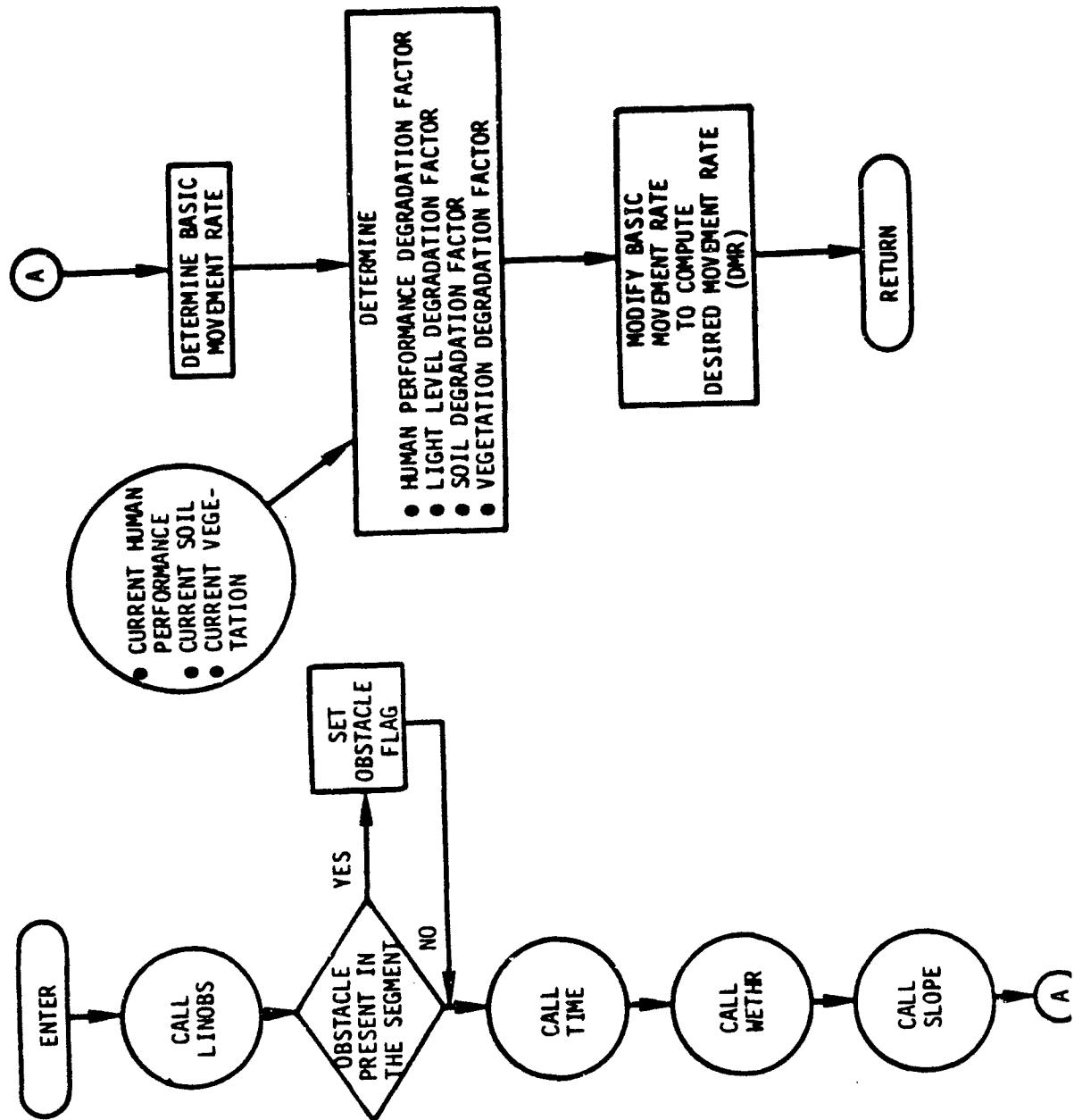


Figure 2.22. SIAF Model Threat Options



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called desired movement rate, is calculated. Upon entering this subroutine, a distance segment (see Figure 2.5), based upon the minimum of the distance to a checkpoint, terrain polygon crossing, or grid crossing, has already been calculated by a segment generator subroutine (see Volume III). The first check made in this subroutine is one to determine if the segment intersects a linear obstacle. For this purpose, Subroutine LINOBS is called and an appropriate flag is set if required. After this calculation, Subroutines Time, Weather, and Slope are called as shown in Figure 2.23, and a basic patrol movement rate is determined by means of a table look-up procedure. This movement rate is then modified to account for the current human performance level of the patrol, and the current soil and vegetation the patrol is moving through (these interactions among subroutines are illustrated by means of circles in Figure 2.23). The output of this subroutine is called the desired movement rate and is defined as that movement rate consistent with good surveillance and detection capability.

Although a desired patrol movement rate has been determined in the previous subroutine, it could turn out that time contingencies require that the patrol move faster than this rate. In order to determine an actual patrol movement rate, a movement command and control subroutine, illustrated in Figure 2.24, is used. As shown in the Figure, the checkpoints from the present patrol position to the end of the patrol route are first checked to determine if there is an arrival time constraint associated with any of them. If not, the actual movement rate is set equal to the desired movement rate. If a checkpoint has an associated arrival time, then the required movement rate, based upon the distance from the patrol to the checkpoint, and the remaining time is calculated. These calculations essentially simulate the commander's estimate of his required movement rate which he would obtain in a similar manner.

Since it is possible that this required movement rate could exceed certain human and physical, environmentally constrained limits, both critical and marginal movement rate limits are next calculated. This marginal movement rate limit is defined as the minimum of the desired movement rate and a 10 percent margin associated with a movement rate consistent with zero body heat storage. The critical movement rate is defined as the minimum of three times the desired movement rate (which is

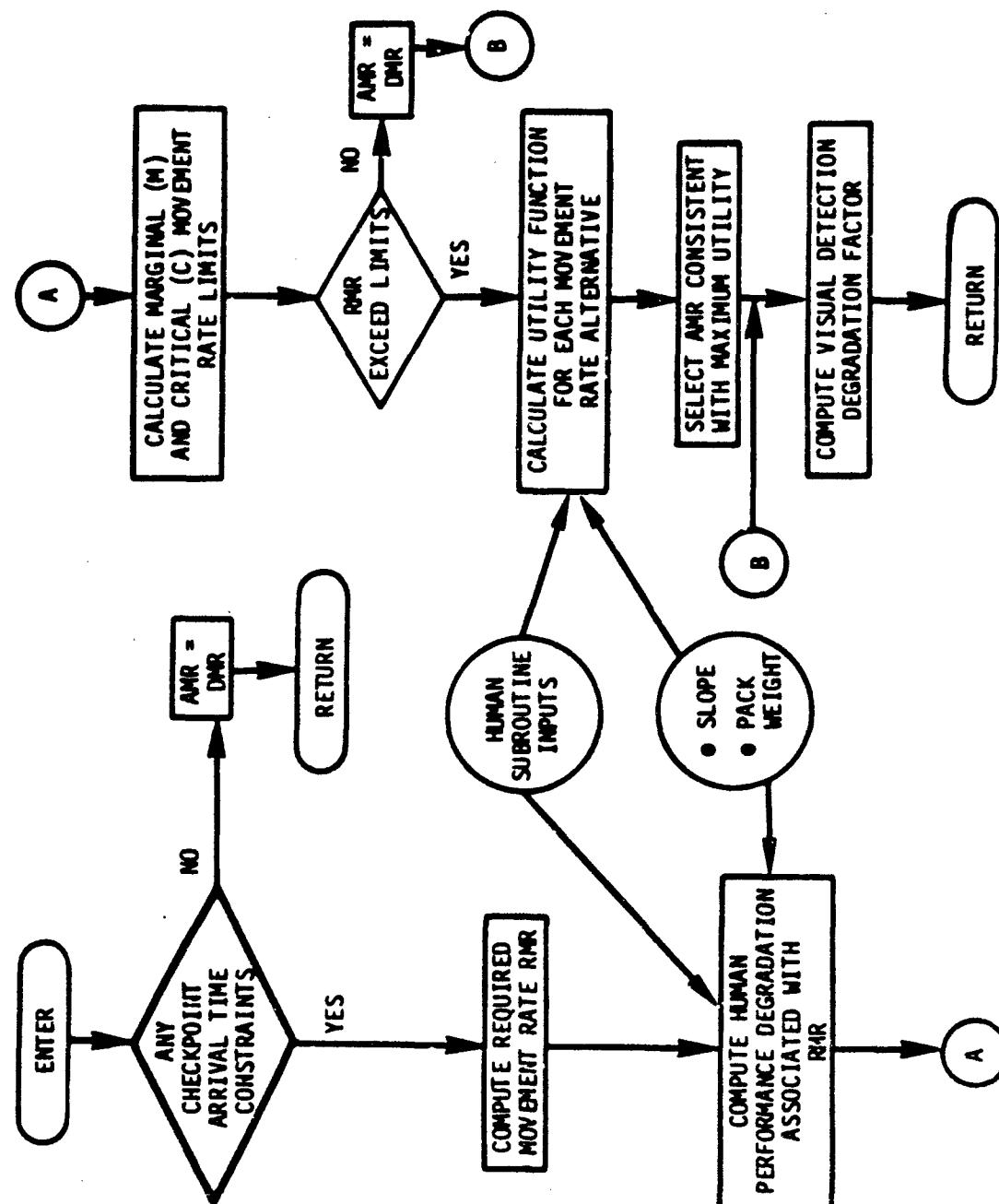


Figure 2-24 - Movement Command and Control Subroutine Iteration 1

estimated to be the nominal movement rate due to the terrain and weather) and that movement rate at which the body just maintains thermal equilibrium. As shown in Figure 2.24, these factors are functions of the current status of the patrol which is available in the communication block of the program. If the required movement rate is less than these limits, then the actual movement rate is set equal to the desired movement rate. If the required rate exceeds these limits, then the patrol leader must trade off his surveillance capability and time. For this purpose, weighting factors for each of these performance variables are provided as input, thus allowing the user the capability to consider alternative movement rate tactics. Based upon these input weighting factors, an actual patrol movement rate is selected and the visual performance degradation factor associated with this movement rate (used by the Visual Detection Subroutine) is calculated.

2.4.5 Navigation

The purpose of this subroutine is to determine the CEP of the patrol location. During the conduct of a mission, the patrol normally determines its location at the various checkpoints and reports its position to the base. However, if a target is detected or another contingency develops, the patrol may need to know its location at positions in between checkpoints. This location error is a function of the distance the patrol has traveled since it last updated its position. Figure 2.25 summarizes the calculations made in this subroutine which starts by computing the range and azimuth errors associated with navigation from the last checkpoint. These dead-reckoning errors are then combined with map, base, and recording errors, and a basic patrol CEP is calculated. Next, the user has the option of adjusting this calculated CEP in accordance with the specifications provided in Reference 2. Independent of these specifications, the patrol could improve its initial estimate of its location by map terrain association if the light level is favorable. This essentially adjusts the location estimate to account for readily identifiable terrain features which the patrol leader could use to more accurately determine his position. Finally, the user has the option of specifying certain patrol location equipment which aids the patrol in determining its position. If this equipment is specified, then the patrol location is adjusted, based upon the amount of

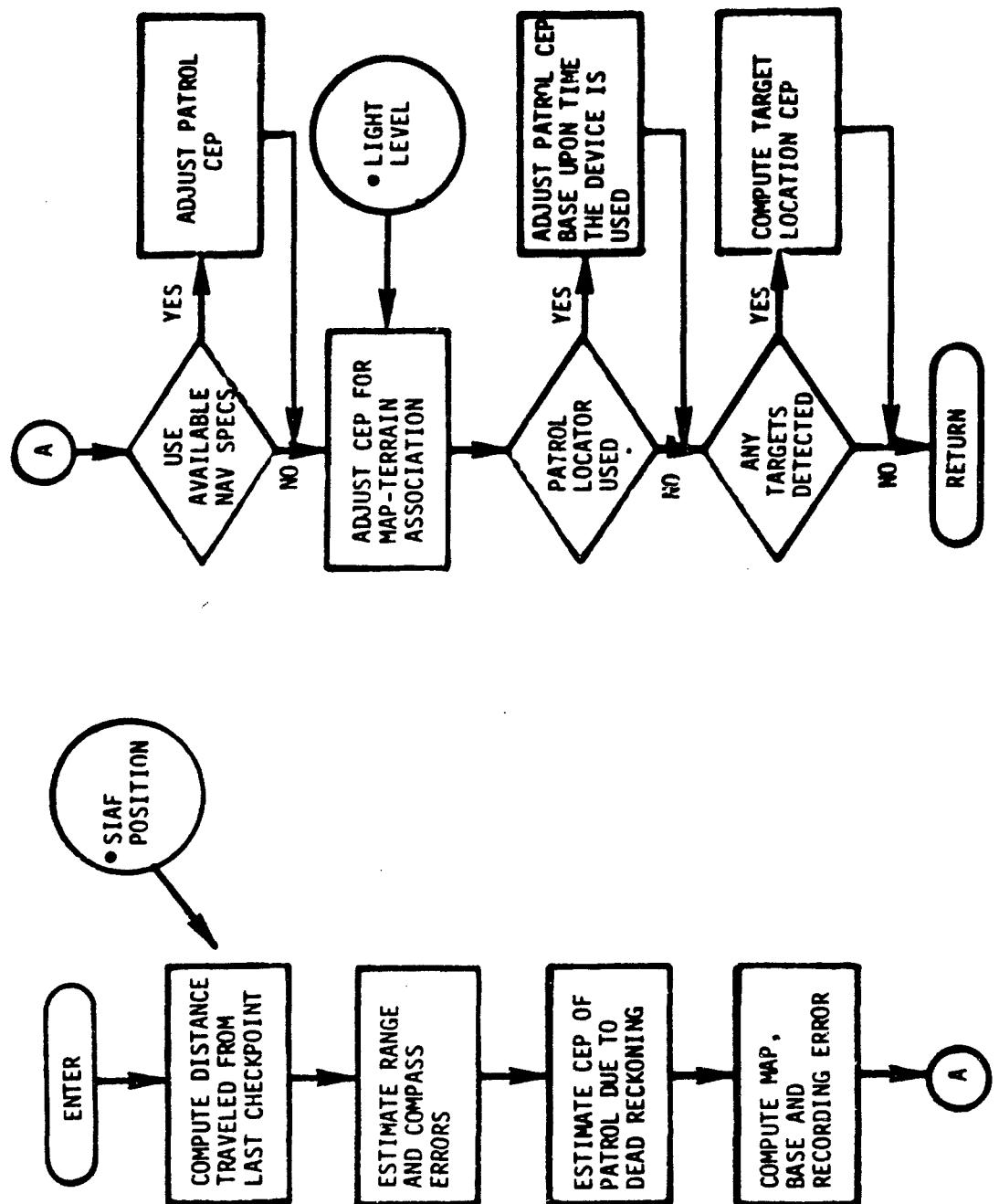


Figure 2.25, Navigation Subroutine (NAV)

time this equipment is used. These steps serve to determine a CEP of the patrol location. As shown in Figure 2.25, if a target is detected, this subroutine also calculates the CEP of the location of the target with respect to the patrol. This calculation is based upon considerations similar to those previously described.

2.4.6 Surveillance/Detection

Aural Detection

The purpose of this subroutine is to determine an aural detection verdict for SIAF against the targets in the area of operations and for the targets against SIAF. The aural detection capability of an individual depends upon the local background sound level and the sound level being made by the individual. The first calculation made in this subroutine, shown in Figure 2.26, is to determine the local aural background level for SIAF and for the targets. This background level is a function of the vegetation, time of day, and weather. Next, the source noise level for SIAF and the targets is computed. This source noise level depends upon the number of men in the unit, their disposition, and their present activity. If, for example, the patrol is moving through heavy vegetation, then its source noise level is considerably higher than it would be if the patrol were conducting a stationary reconnaissance. Based upon these two calculations, the sound level arriving at the listener is computed (considering range and vegetation attenuation) and is compared with the hearing threshold and the local background noise. If the threshold is exceeded, then the appropriate detection opportunity is stored in a vector for subsequent analysis by the Detect and Decision Subroutines.

Visual Detection

The Visual Detection Subroutine is illustrated in Figure 2.27. The purpose of this subroutine is to calculate probability of making a single glimpse, visual detection of targets that are feasible of being detected by SIAF, and for targets to detect SIAF. In this calculation, line of sight between SIAF and the targets is assumed. Hence, the calculation mainly considers light level for the detection computation. As shown in Figure 2.27, the first calculation is to determine the target reflectance, background reflectance, the light level at the target, and the light level

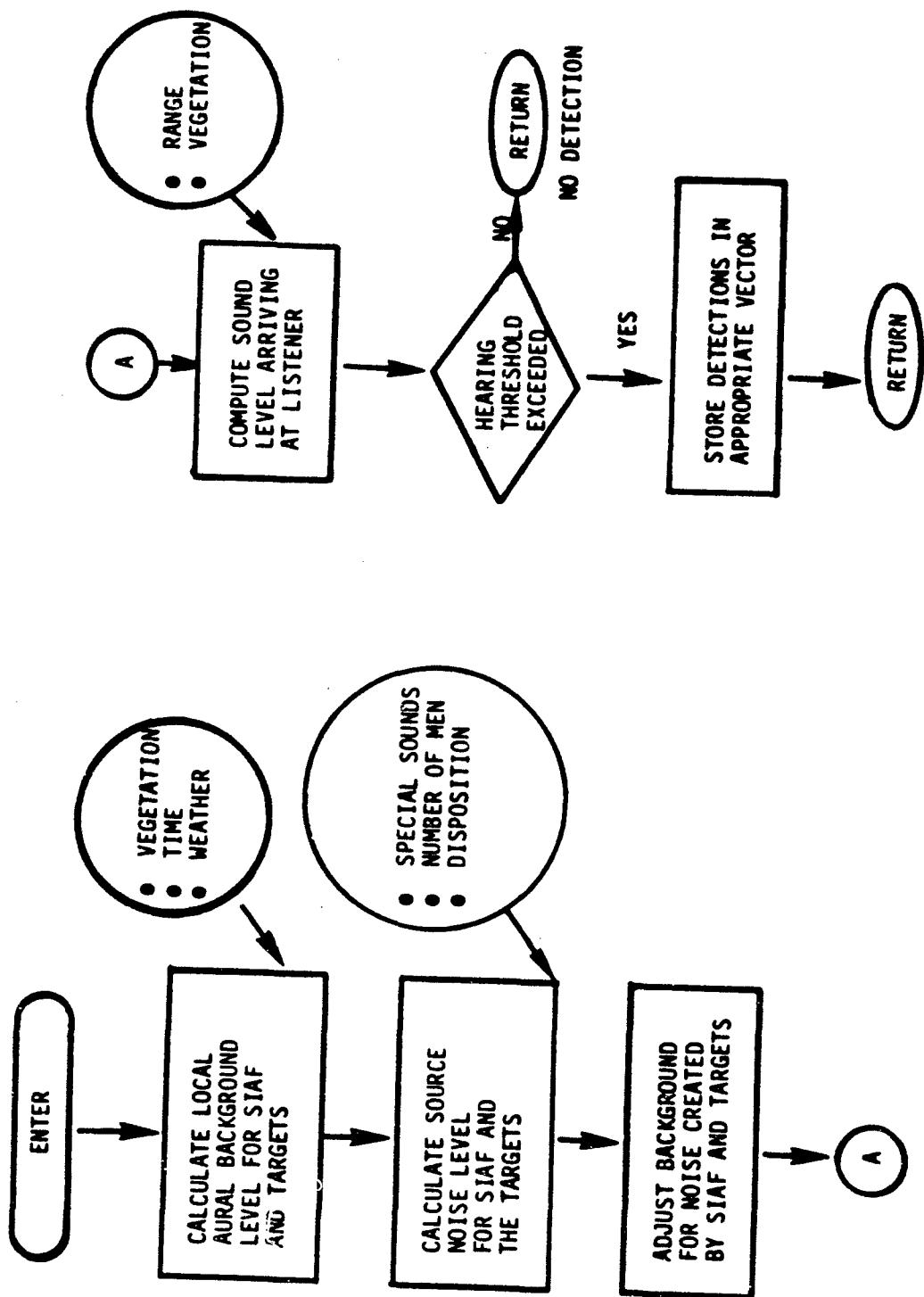


Figure 2.26, Aural Detection Subroutine (AURAL)

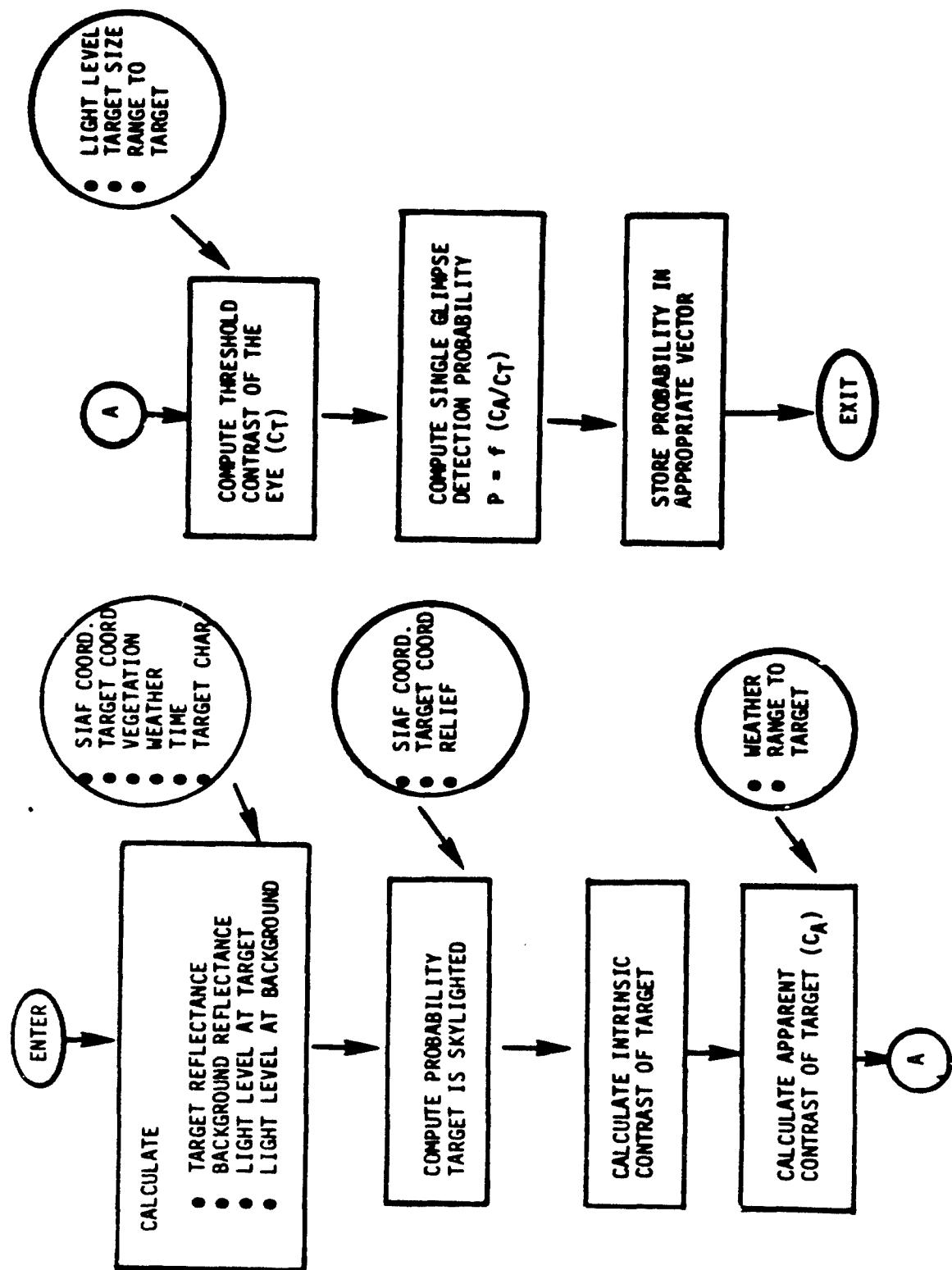


Figure 2.27, Visual Detection Subroutine (VISUAL)

of the background. Depending upon the location of SIAF and the particular target under consideration, there is a possibility that the target may be skylighted. The next calculation is then made using the Terrain Concealment Subroutine to determine background conditions, including skylighting. Based upon this information, the intrinsic contrast of the target is computed. This intrinsic contrast is essentially the ratio of the brightness of the target to the brightness of the background. Depending upon the range between SIAF and the target and the weather conditions, the contrast of the target as observed by the eye differs from the intrinsic contrast. This is called apparent contrast and is next calculated considering the factors mentioned above. The third contrast calculated in this subroutine is threshold contrast of the eye. As indicated in Figure 2.27, this threshold contrast is a function of the light level, target size, and the range to the target. The ratio of apparent contrast to threshold contrast is then used to determine a single glimpse detection probability. This probability is then stored in an appropriate vector as further indicated in Figure 2.27.

Detect

The described calculations serve to determine detection opportunities and are independent of line of sight. Subroutine Detect, illustrated in Figure 2.28, combines these calculations with the relief and vegetation and considers the physical location of SIAF and the target. As mentioned previously in Section 2.3, this detection calculation is made once for each mini-segment and can consider man-to-man detection if desired by the user. The first calculation made is to determine which patrol members are looking in the correct sector to potentially see the target. If, for example, no patrol members are viewing any targets, then detection is not feasible. For all feasible targets, Subroutines TERCON, AURAL, and VISUAL are next called. These subroutines essentially examine line of sight between SIAF and the target, sound levels made by SIAF and the target, and light level to determine whether detection or several detections can possibly occur in the mini-segment. Based upon this information and the time available, detection verdicts are calculated in a Monte Carlo fashion for SIAF and all detectable targets. The order and interval between detections is created to identify who sees who first and later is used in the decision model to determine simultaneous detection/counterdetection situations.

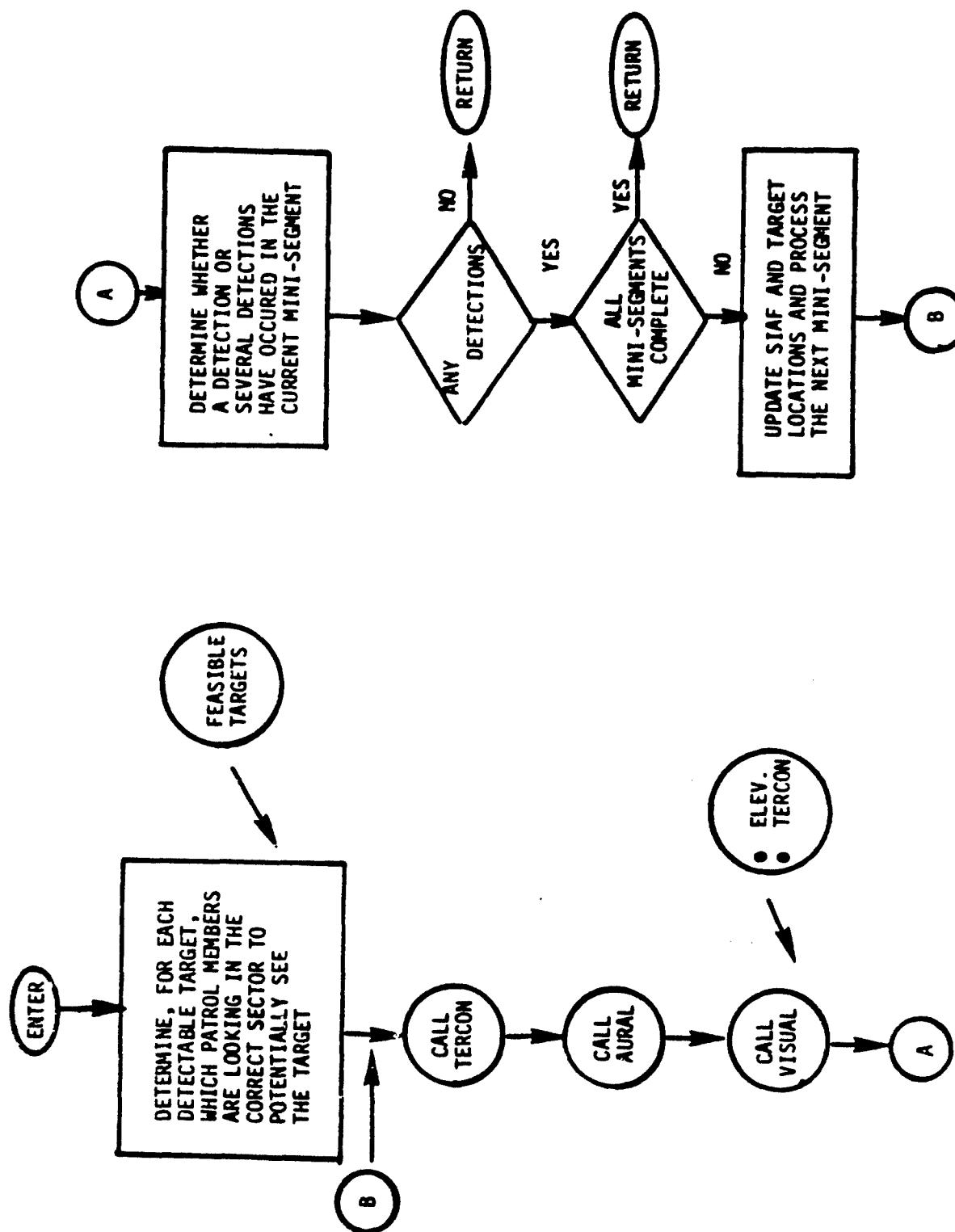


Figure 2.28, Detection Subroutine (DETECT)

2.4.7 Fire Support

If a patrol detects a target, it may elect to direct fire on the target, without engaging in a firefight depending upon the mission and the situation at the time of detection. For this purpose, an external fire support subroutine (EPS) is called by the Executive Routine. As shown in Figure 2.29, the user can select air, artillery, or manual gunfire for analysis. If air is selected, then the assumption is made that the target movement provides negligible error in ordnance delivery CEP. Because of the response time of artillery and naval guns, a moving target could introduce decreased accuracy in delivery CEP; hence, the user can examine this situation if desired. As shown in Figure 2.29, factors such as surprise and adjusted fire, target reaction to the first round hit, and the interactions of the effectiveness of the fire support mission with the patrol and target location errors are considered. If preliminary fire support is to be used prior to attacking a target, a detailed simulation of external fire support effectiveness is used. This is discussed in the Combat Submodel description.

2.4.8 Supply Maintenance

The Supply Maintenance Subroutine illustrated in Figure 2.30 is essentially a booking subroutine which increments and/or decrements the supply status of the patrol during each segment. As shown in the Figure, food, water, ammunition, and pack weight are incremented if the patrol was resupplied during the last segment and decremented for combat operation and for normal food and water consumption. The normal food and water consumption requirements are calculated in the Human Maintenance Subroutine which follows.

2.4.9 Human Maintenance

This subroutine computes food and water requirements for the patrol and calculates the current human performance degradation of the patrol. As illustrated in Figure 2.31, the current energy expenditure rate of the patrol members is first determined. This is based on the current patrol activity which includes rest, sleep, stationary reconnaissance activities, or movement. During movement, the energy expenditure rate is a function of the slope, pack weight, and movement rate, for which values are available to this subroutine via the communication block of the program. Once the energy expenditure rate is determined, the value of the segment time is used

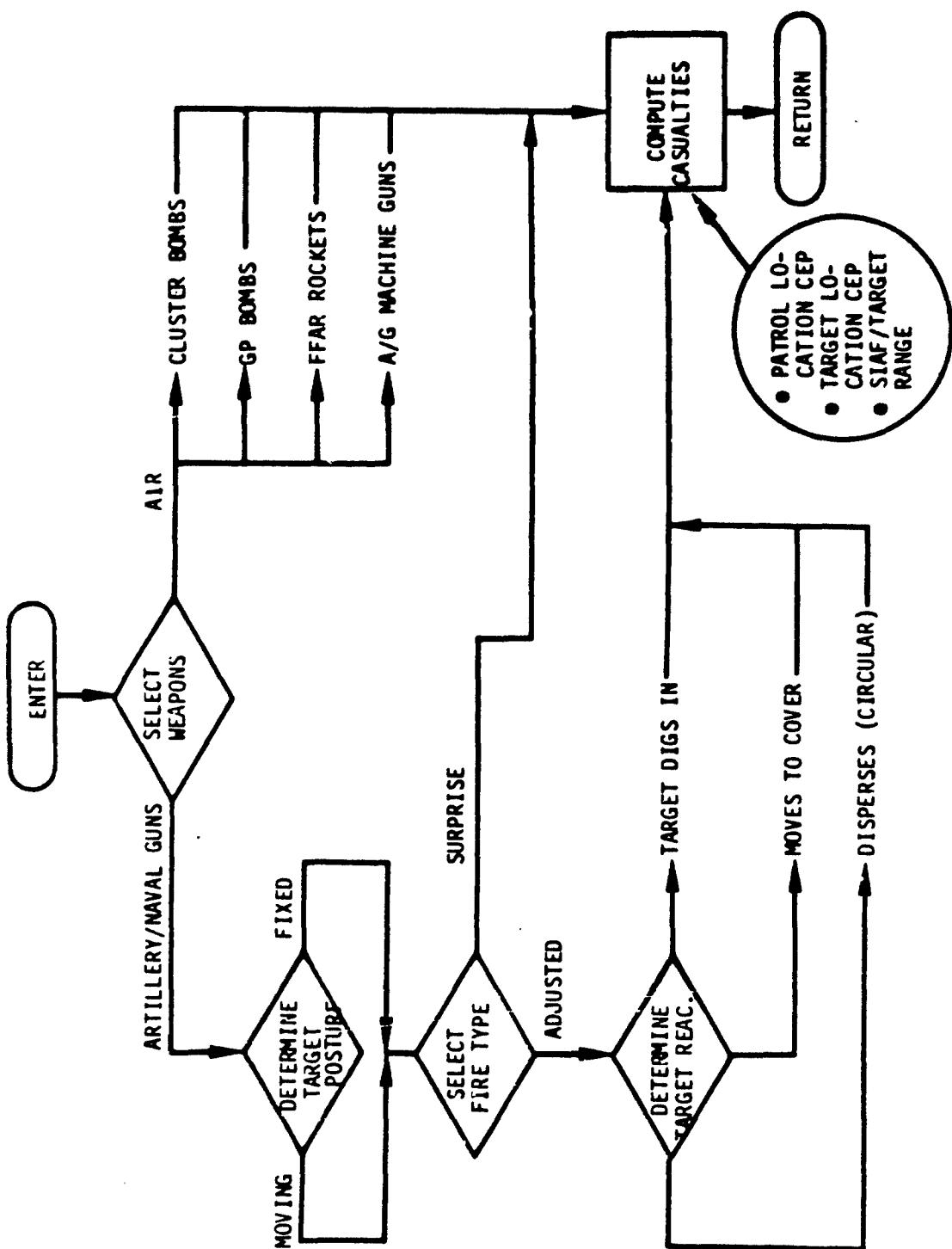


Figure 2.29, External Fire Support Subroutine (EFS)

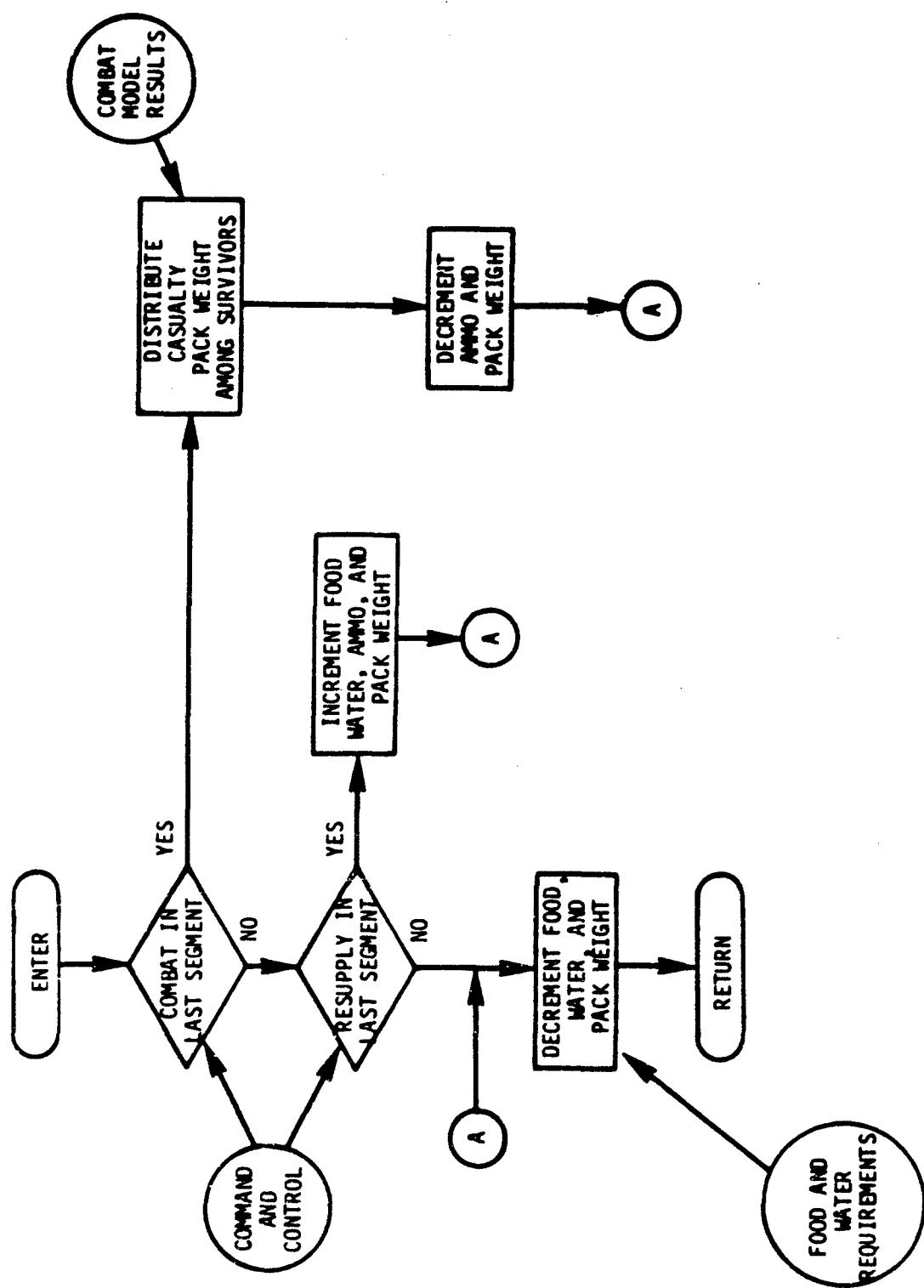


Figure 2.30. Supply Maintenance Subroutine (LOGIS)

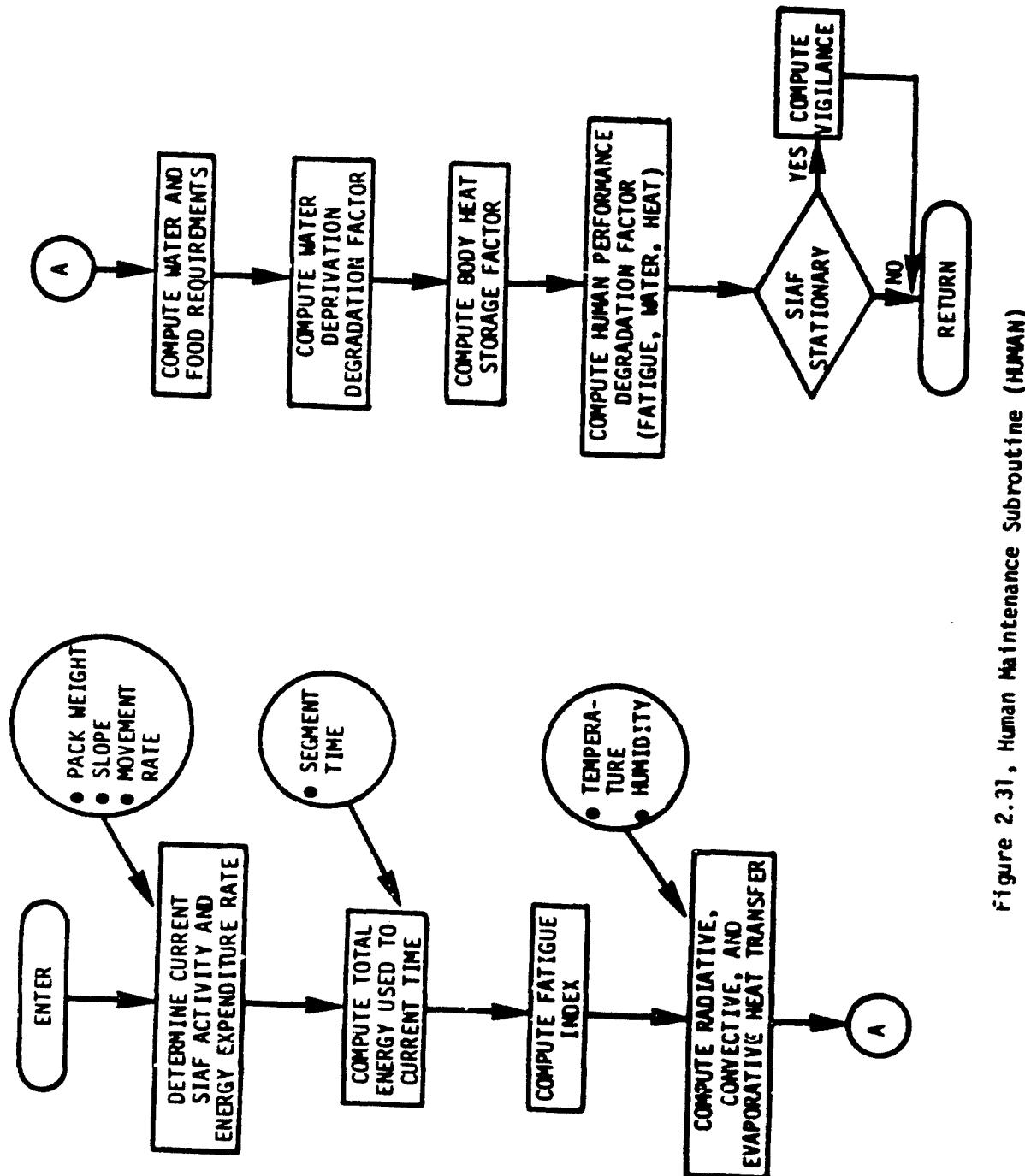


Figure 2.31, Human Maintenance Subroutine (HUMAN)

to compute energy expenditure and an associated fatigue index as shown in Figure 2.31. This energy expenditure is then used to compute the body heat lost through radiation, convection and evaporation. From this, food and water requirements and body heat storage are calculated. These factors are then combined and a human performance degradation factor is computed. This human performance degradation factor is the amount in percent by which the performance of patrol functions such as visual detection are degraded due to fatigue, body heat storage, and water deprivation. In addition, visual detection performance is influenced by a factor called vigilance which accounts for the decrease in the alertness of patrol members as a function of the time they have been conducting stationary reconnaissance operations. If the patrol is stationary, this calculation is also made as shown in Figure 2.31.

2.4.10 External Communications

The External Communications Subroutine shown in Figure 2.32 calculates an external communication verdict for the patrol on each communication attempt. First, the total ampere hours currently available to the patrol are computed to determine if the battery life is expended. If so, a no-communication verdict is returned by the subroutine. If power is available, then a power budget analysis is conducted; and vegetation, defraction, and space losses are computed. These calculations depend upon the current distance from the patrol to the base and the terrain between SIAF and the base. The results of this power budget are used to compute the signal-to-noise ratio at the receiver. This signal-to-noise ratio is then used to compute message intelligibility. As shown in Figure 2.32, the model simulates the actions of the patrol repeating the message until the intelligibility criteria (a user input) is satisfied. If the intelligibility criteria is not satisfied with N trials (N is a user input), then a no-communications verdict is returned by the subroutine. If the criteria is satisfied, then the communication is said to be successful.

2.4.11 Command and Control

The current SIAF command and control model consists of a movement command and control subroutine (described in Section 9.1) and a post detection decision subroutine (Section 9.2).

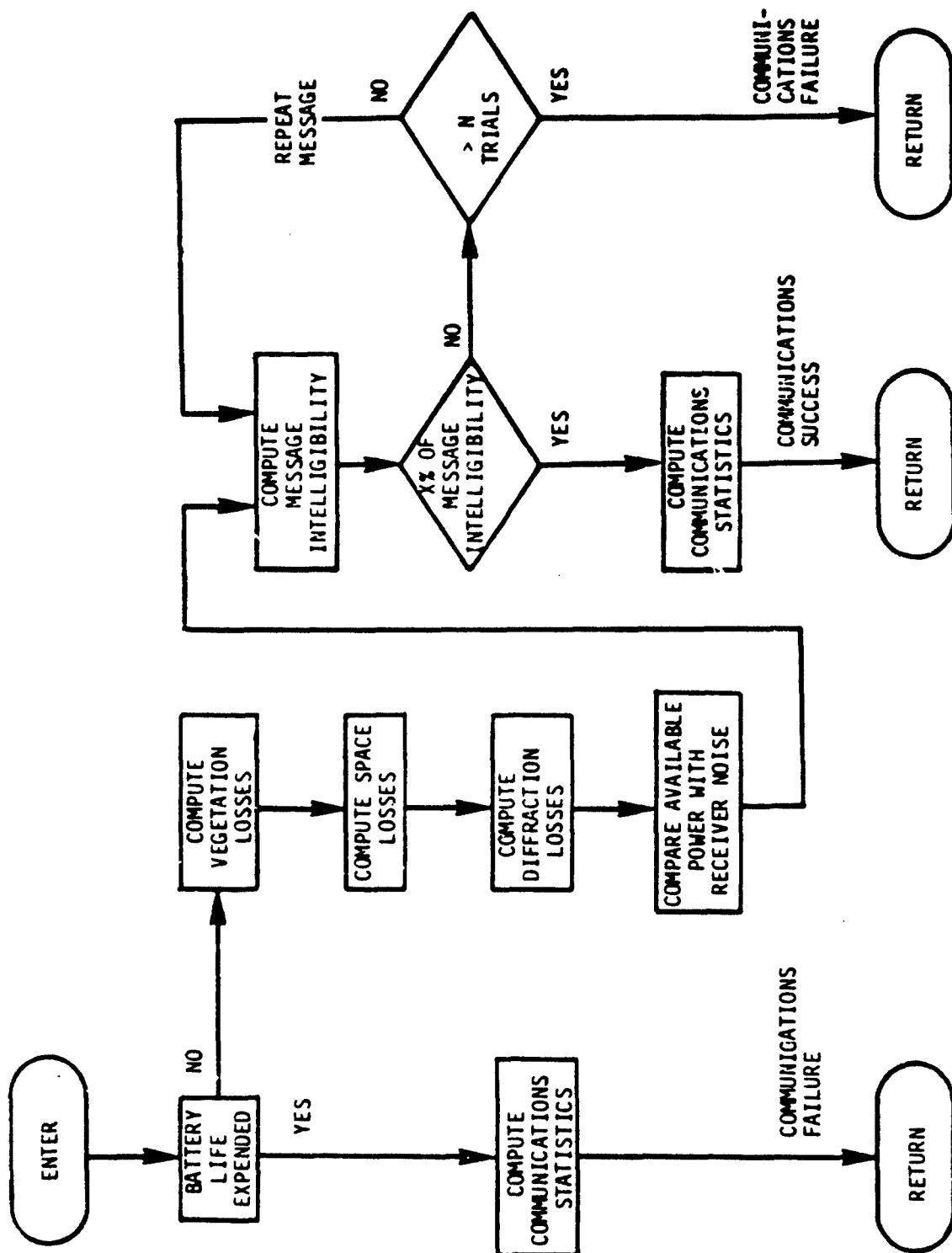


Figure 2.32, External Communications Subroutine (EXCOM)

With respect to patrol movement, the required movement rate which a patrol must sustain in order to arrive at a next checkpoint on time is compared with a desired movement rate that is consistent with being able to maintain good surveillance. If the required rate exceeds the desired rate, trade-offs are made between time and detection performance to select the most satisfactory movement rate for the patrol. The trade-off results can be controlled by adjusting input weighting factors.

In the post detection subroutine of Section 9.2, alternatives are provided which cause the patrol to move along a dynamic route toward the target to identify it or to move around the target to avoid it. Logic is also provided for calling external fire support on targets. Input variables are provided which allow the user the capability of exercising these model options (see Section 9.0 for details).

2.5 SIAF COMBAT SUBROUTINES

Thus far an overview of the reconnaissance model has been presented in previous sections. Once the SIAF patrol detects a target, however, it may decide to combat the target, and once the combat is completed the patrol may decide to continue the reconnaissance mission. The SIAF model considers these possibilities. In the following section an overview of the combat decision and execution subroutines are presented. (Details of these routines are described in Volumes V and VI.) Included is a description of the decision logic and decision optimization routines, and a discussion of the combat executive routine. Finally an overview of the withdrawal and the continue mission routine which allows the patrol to continue on its reconnaissance mission once the combat operating is completed, is presented.

2.5.1 Combat Decision Logic and Optimization Logic

In the SIAF reconnaissance model many detection and identification possibilities exist. For example, the SIAF patrol could possibly identify two targets simultaneously or several targets could identify and detect SIAF at the same time. Because of the complications involved in developing logic to model these situations, combat operations where more than one target is involved are not considered in the model. Instead if it turns out that several targets detect SIAF or SIAF has detected and identified several targets then a no combat decision is made and the SIAF patrol avoids the

targets. Considering the fact that SIAF normally operates as an independent force this is probably a reasonable simulation of what they would in fact do. That is, should they detect and identify more than one target they would probably avoid the target area.

Now consider the case in the simulation model where SIAF detects and identifies a single target. In this case if its mission is combat, the patrol must decide what kind of combat action to initiate. Here decision logic is necessary since it is impossible to determine exactly where the patrol will be and exactly what and where the target is when the detection occurs during the simulation. Hence this logic dynamically examines the current tactical situation and selects a course of action. The movement to contact and deployment decision logic shown in Figure 2.33 indicates that five courses of action are possible. The first course of action is that the patrol could call in external fire support on the target. The second alternative is that the patrol could deploy for ambush. This alternative, for example, would probably be selected if the target were moving toward the SIAF patrol. On the other hand the target may be moving in a direction away from the patrol or may be out of range of the patrol. In this case the SIAF patrol could decide to move to a deployment position and call for external fire support if available, before initiating the fire fight. Another alternative, even before a detection occurs, is to move to an ambush area to deploy Claymore mines. The fifth alternative, of course, is a no combat decision. The decision logic subroutines examine the current tactical situation and select one of these alternatives based on the following decision variables.

- 1) Mission (ambush, attack, or deploy Claymore mines)
- 2) Force ratio (i.e., the relative size of the target vs the size of the SIAF)
- 3) SIAF-target range
- 4) Direction of travel of the target
- 5) The terrain between the SIAF patrol and the target as to its effects on cover, concealment, and observability.

The decision logic is constructed so that the user can adjust the input data and choose different criteria for selecting a course of action. Thus the decision variables are examined, the tactical situation determined by the model and a combat option is dynamically selected.

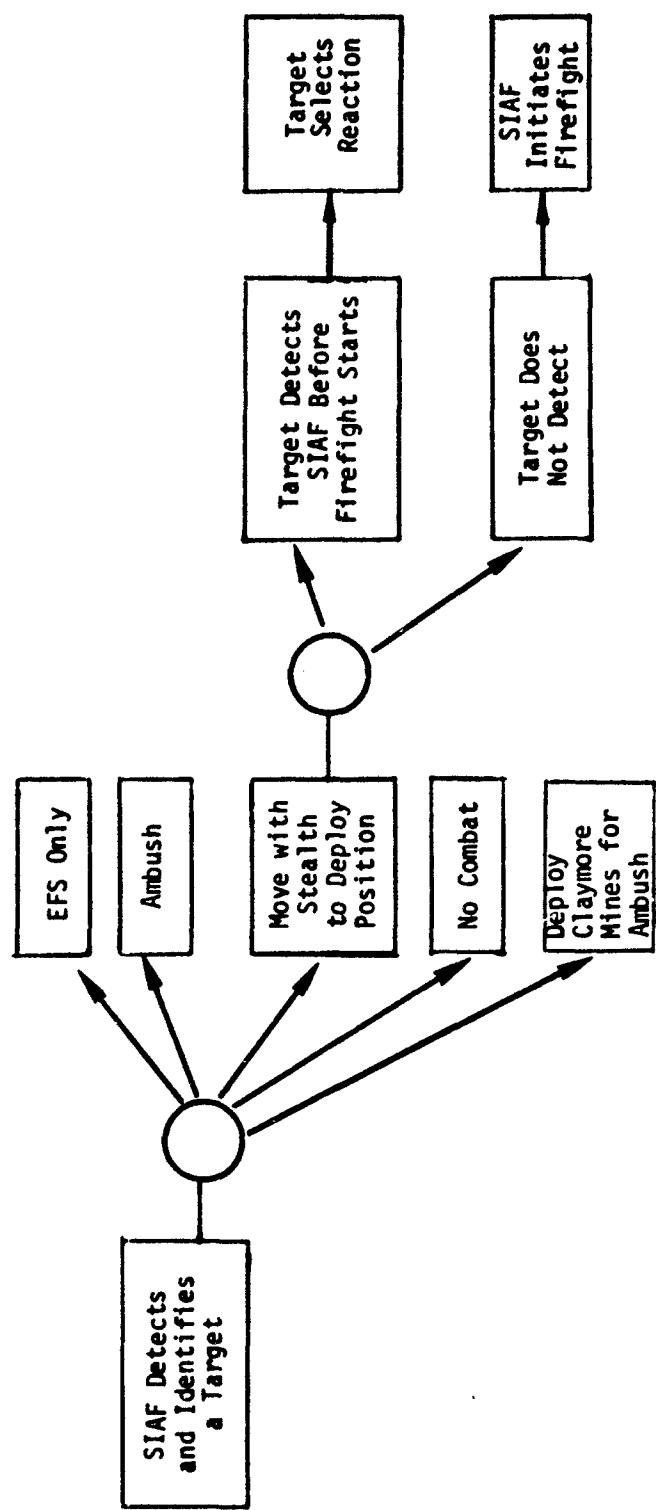


Figure 2.33, Movement to Contact and Deployment Logic

In the case of external fire support only the external fire support (EFS) subroutine is then called, external fire support simulated, and the patrol then makes a "continue the mission" decision and would probably, in this case, decide to return to continue the reconnaissance patrol. In the case where deployment is selected, optimization logic optimally selects the exact deployment position of each maneuver unit in the terrain. The most complicated situation evolves when the patrol decides to move to a deployment position. In this case the dynamic route selector routine (DROUTE) selects movement points based upon different movement criteria which again are user input. As shown in Figure 2.33 when the patrol is involved in this type of a movement the target could possibly detect the patrol before the fire fight occurs. In this event the target could react by moving, deploying, or opening fire. If, on the other hand, the target does not detect the patrol in movement to the deployment position, SIAF initiates the fire fight. If the target should move toward a better defensive position, the SIAF may reselect its deployment points or exchange roles between maneuver units and the base of fire. Thus, the combat decision and optimization logic provide a mechanism for the user to select various combat alternatives based upon the current tactical situation.

2.5.2 Combat Executive

In Section 2.3 the executive routine used to drive a reconnaissance model was described. In this section an overview of the executive routine used to drive the combat model is presented. In this regard two approaches for driving the combat executive routine were examined. The following section describes and compares these two approaches.

The first alternative shown in Figure 2.34 indicates that each man in this situation has a clock time, initial values of which are selected to be different based upon user input. The model selects the man with the smallest clock time and decides how much time is to be spent observing in an intelligence routine, and computes this amount of time (t_1' in the figure). Then movement and fire controller models decide if the man will move or fire. If he is to fire, for example, the fire controller model decides at whom he will fire and computes the firing time (t_2' in the figure). If communications are to occur the time required for communications are also computed. Finally casualty assessments are made. After these calculations are made the clock time for this particular individual examined

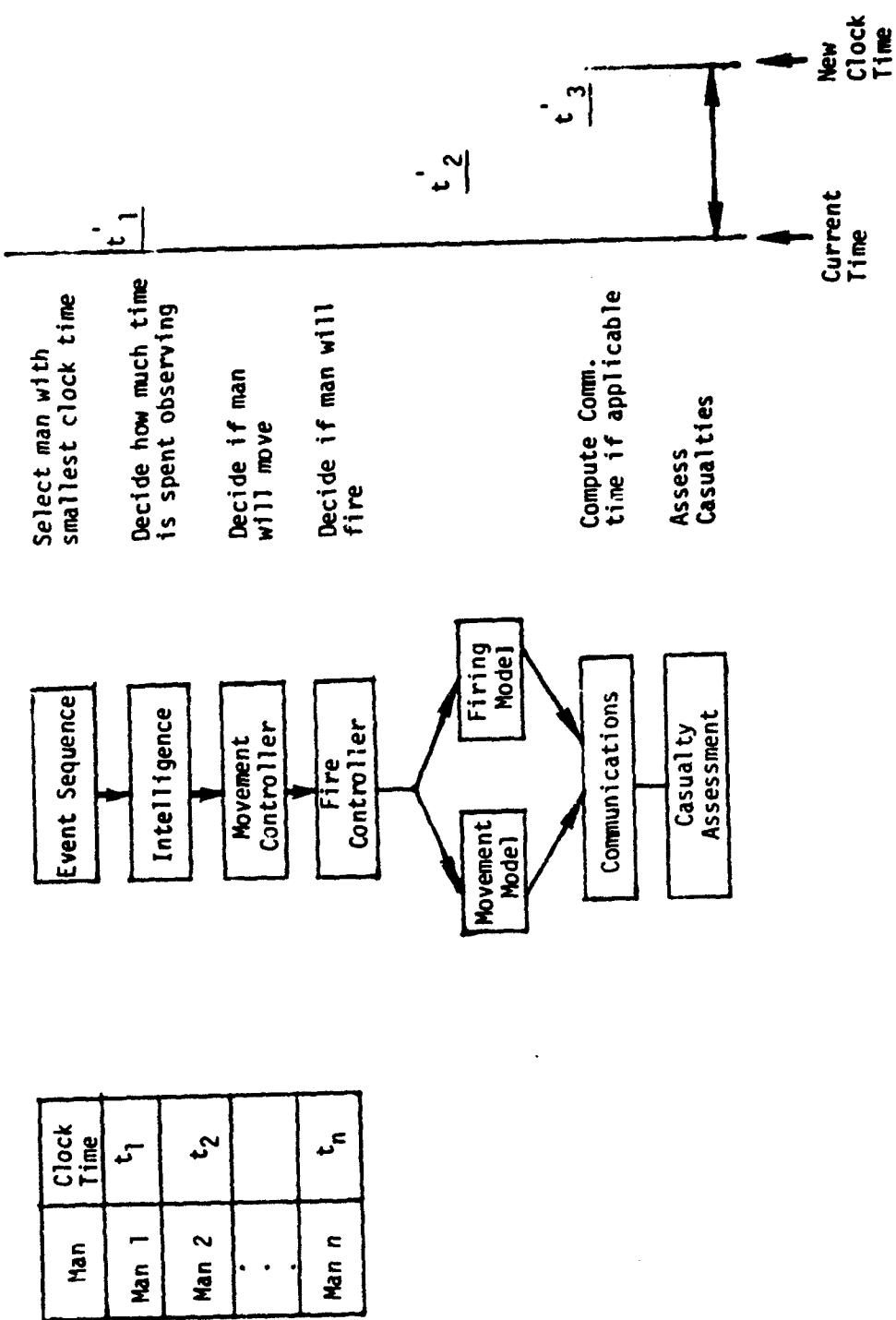


Figure 2.34, Alternative 1 to the Combat Executive

is advanced by the amount $t'_1 + t'_2 + t'_3$ and he is given a new clock time. The model then scans the list of men and clock times, picks out the minimum, and repeats the procedure. Thus, in alternative one, each man is individually cycled through functions that he is required to perform during combat and time is advanced in the fashion described above. This is the approach that is used in models such as DYNTACS and ASARS.

An alternative to this approach is presented in Figure 2.35. Here, instead of individually selecting each man and having a clock time associated with each man, only one clock time exists in the model. The event times in this case are movement, detection, casualty, EFS burst, and internal message reception. The executive routine computes the movement and detection event times for each individual for both the attacker and defender, and the casualty times of each individual for both the attacker and defender. It then scans this list of times together with any scheduled arrival of EFS and any scheduled reception of a message between maneuver units. It then selects the minimum time, and defines the corresponding event as the event which occurs in this particular segment of the model. Figure 2.35, for example, illustrates what would happen if the event were movement. In this case, all moving individuals would be moved an appropriate amount of ammunition, the clock time and the status of each man would be updated, and calculations would be repeated. Thus, instead of cycling through each man, this particular method examines the next event to occur for all men, advances the clock time based upon the minimum of these times, and updates the attributes of each man to what they would be at this time.

A comparison of these two approaches is shown in Figure 2.36 and here, three attributes were defined: running time, event accuracy, and capability to handle cumulative interactions. The comparison indicates that alternative one probably has a faster running time in most cases. However, arguments that alternative two could be faster are also possible to evolve. As far as event accuracy is concerned, alternative one could possibly neglect events which occur to other individuals during a given loop through the logic. The reason for this can be seen through a further examination of Figure 2.34 which shows that an individual could possibly become a casualty during the advance of his clock time. Thus, unless a time step variable is set to adjust the advance of

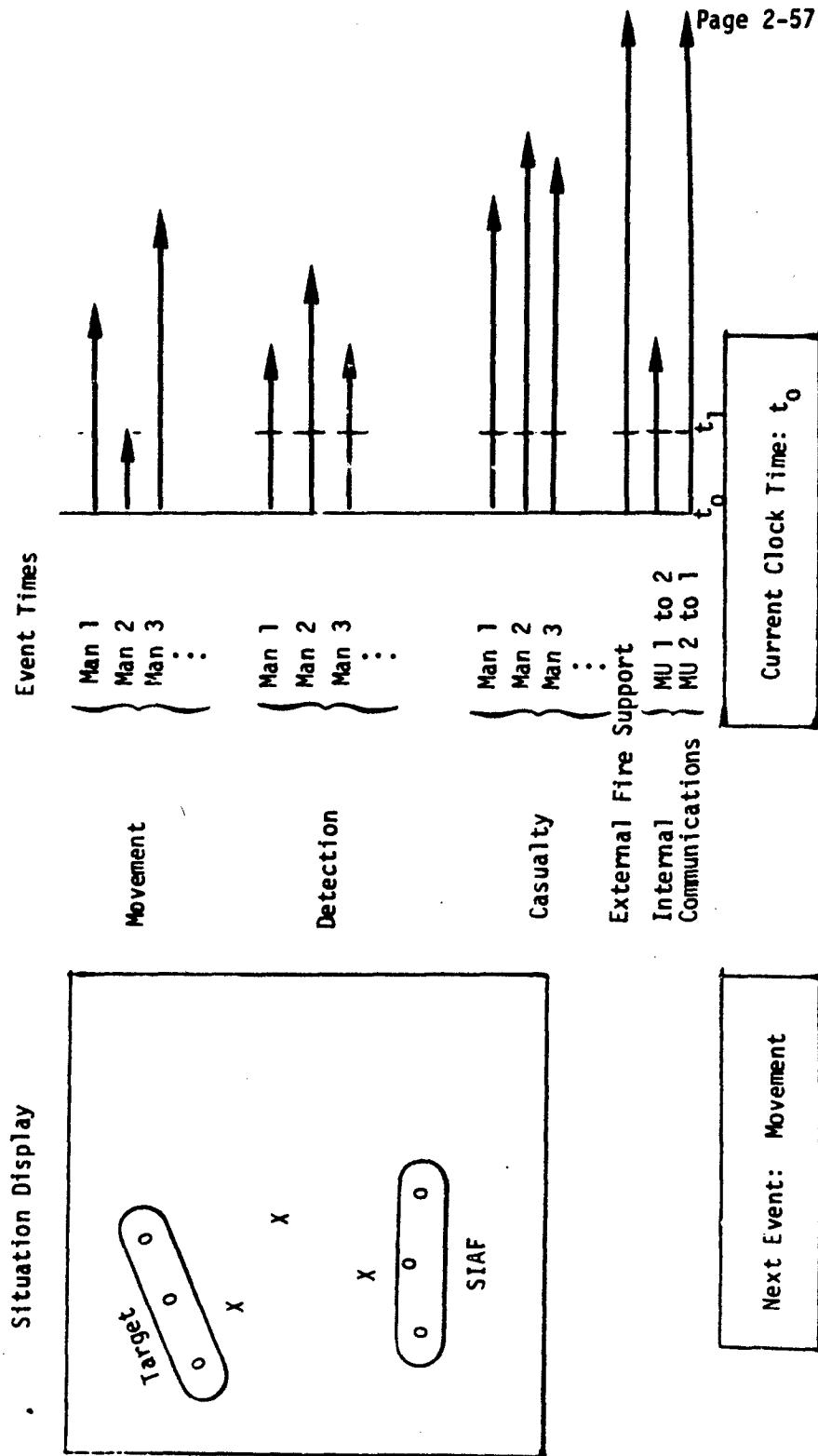


Figure 2.35, Alternative 2 to the Combat Executive (Sheet 1)

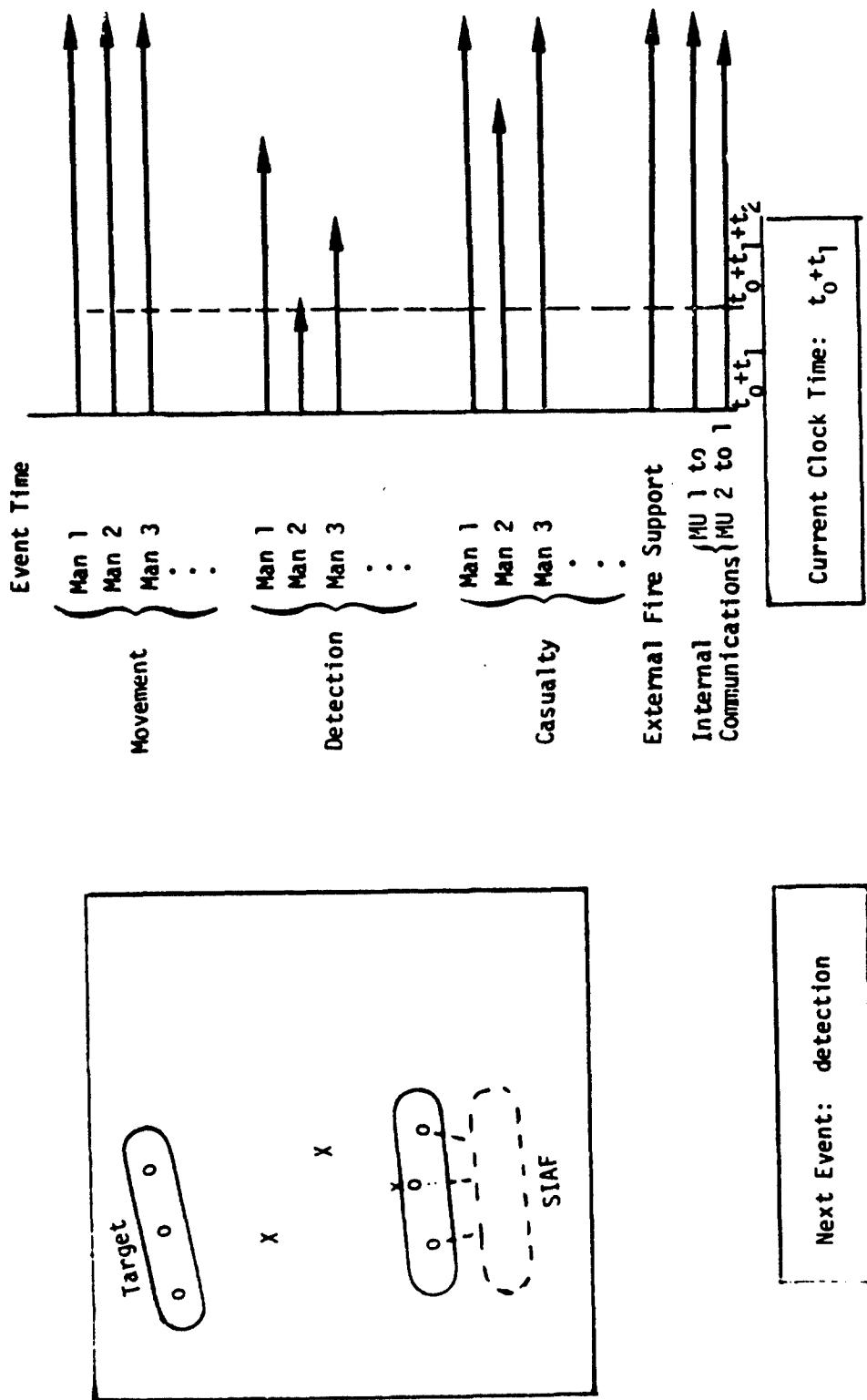


Figure 2.35, Alternative 2 to the Combat Executive (Sheet 2)

Attribute	Alternative 1	Alternative 2 SIAF Technique
Running time	Faster running time in most cases	Will normally run longer but could run faster than Alt. 1
Event Accuracy	Could neglect events which occur to other individuals during a given loop through the logic	Such events are not neglected since everyone is updated during each advance of the clock
Capacity to handle cumulative interaction	Suppression only considers one man firing at one and neglects simultaneous firing	Suppression includes the effect of many individuals firing at one (cumulative P_K table)

Figure 2.36. Comparison of Executive Alternatives

the clock, these types of events, which would tend to bias the results, could occur. With alternative two, such events are not neglected since the time of the first event for all individuals is first calculated and time is advanced in a fashion previously described. With respect to cumulative effects, alternative one neglects the fact that the suppression of an individual may be greater because three individuals may be firing at him rather than just one. Alternative two, on the other hand, can include these types of cumulative effects. As far as implementation goes, it is not clear that alternative one is superior to alternative two. Different logic is required for both alternatives, and a comparison is very difficult to make. Based upon the manner in which the reconnaissance model currently runs and an examination of these alternatives, alternative two was selected as the technique to be used for the SIAF combat model.

In summary, two executive routines are provided with the SIAF model. The first is the reconnaissance executive which operates in the manner described in Section 2.3. Once the detection and identification occurs the decision logic determines whether a combat action will occur. If a combat is to occur then the combat executive described above simulates this part of the mission. Once a combat mission is concluded and a decision is made to return to the reconnaissance operation, the reconnaissance executive routine described in Section 2.3 takes over and continues driving the model.

2.5.3 Data Structure and Manipulation

The SIAF combat model consists of a series of subroutines and an executive routine. The executive routine advances time in the manner previously described and calls individual subroutines to make various calculations. Interactions are considered and modeled by the subroutines which essentially update the attribute list of the target and SIAF shown in Figure 2.37. For example, ATT(1,1,1) is the fire team number of the first man in the attacker patrol. ATT(3,2,2) contains a value of the number of rounds remaining for man number 2 in the defender unit. The attribute matrix is a 25 x 20 x 2 matrix, and the attributes of each individual are changed by various subroutines depending upon the situation. For example, should movement occur then the current X and Y coordinates, attributes 7 and 8, of each individual involved in the movement are updated by the appropriate routine. Should a patrol member assume a different posture, then the height of the patrol member is

Z is the Patrol Identifier

- 1: Attacker
- 2: Defender

X is the Attribute of the Patrol Member

- 1: Team Number
- 2: Weapon Number
- 3: Current Ammunition Supply (Rounds)
- 4: Casualty Status
- 5: Firing Status
- 6: Current Suppression State
- 7: Current x Coordinate (Meters)
- 8: Current y Coordinate (Meters)
- 9: Next x Coordinate (Meters)
- 10: Next y Coordinate (Meters)
- 11: Height (Meters)
- 12: Width (Meters)
- 13: Current Posture
- 14: Moving Element
- 15: Maneuver Unit to Which the Element Belongs
- 16: Number of Rounds Remaining in Magazine
- 17: Function in Patrol
- 18: Movement Rate of Each Individual
- 19: Individual's Assignment
- 20: Initial Ammunition Supply
- 21: Weapon Type
- 22: Position in Fire Team
- 23: Secondary Weapon Number
- 24: Hand Grenade Supply
- 25: Signal Grenade Supply

ATT(X,Y,Z)

Y is the Patrol Member

1 2 3

20

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adjusted, attribute No. 11. Should his movement status change, for example, should he be in a suppression state where movement is not allowed, then the movement status attribute is changed. Attribute changes by one routine in turn effect other routines. For example, should the movement status change, the firing status would probably be different to allow the advancing unit to start moving again. Hence, the interactions between routines are essentially communicated to each of the routines through the attribute matrix. Naturally this is an oversimplification of the exact details of the model and is intended to be an overview to aid in understanding the details presented in Volumes V and VI.

2.5.4 Calculation of Movement Event Times

As previously described in Section 2.5.2 five events are defined in the executive: movement times, detection times, casualty times, communication arrival times, and EFS burst event times. This section describes the calculation of movement event times. Figure 2.36 illustrates this calculation and shows the SIAF team in a line formation moving from one objective point to the next objective point which in this case is the point generated by a dynamic route subroutine. The model starts by computing the objective point for each individual based upon its formation of the unit. For a line formation the objective points would be as shown in the figure. If the formation were a "V" or a wedge then subroutine FORMST would compute the appropriate objective points for each individual and load these values into the ATT matrix. Specifically, these values would be located in ATT 9 and 10, the next movement coordinates. Next, based upon the present location of each individual, this subroutine calculates segment lengths for each individual. As shown in the figure, the segment lengths for each individual could be different and the path each individual takes could be over different terrain; hence, the movement rate model described previously in the reconnaissance section is called and the movement rate of each individual over each segment is calculated. Next these movement rates are modified by the current suppression state which is stored in the ATT matrix. Finally, the segment lengths are divided by movement rates to compute the time at which each individual would reach its next objective point. Then the minimum of all these times is calculated and stored in a variable called STIME.

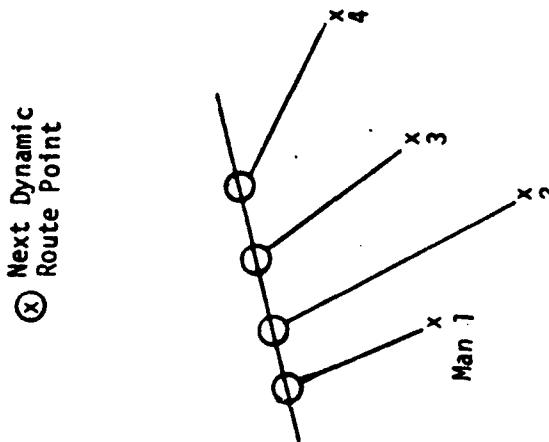
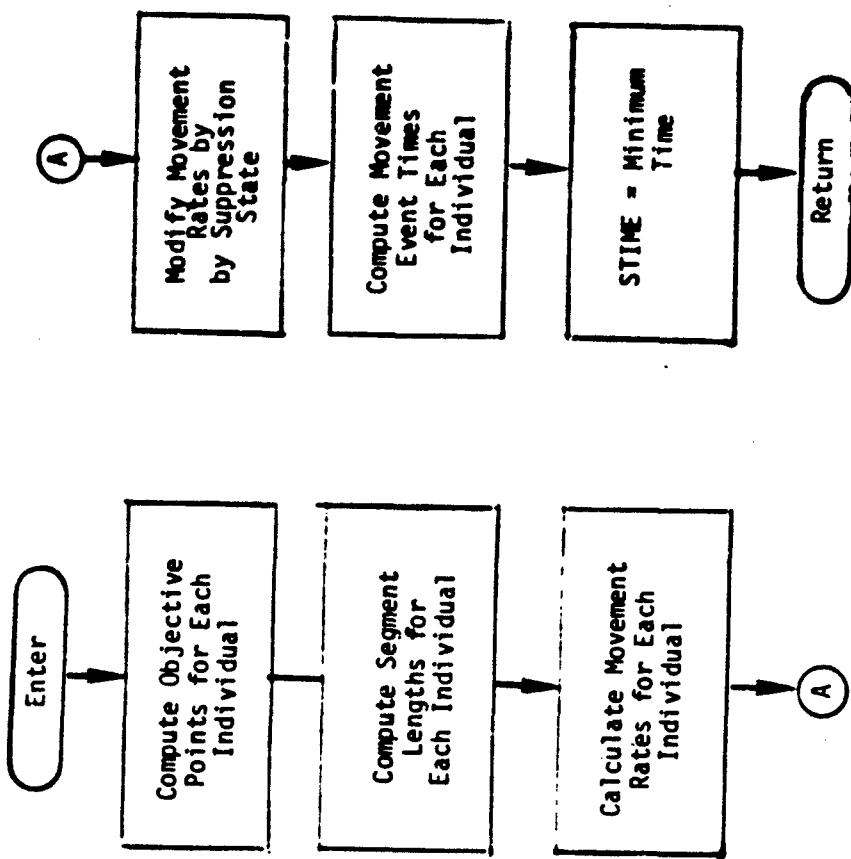


Figure 2.38. Calculation of Movement Event Times

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2.5.5 Calculation of Detection Event Times

The previous section described how movement event times are calculated. In this section the calculation of detection event times is described and illustrated in Figure 2.39. First a specific SIAF and target individual are selected. Here detection times are based upon individual detections on individuals, that is, if there are 20 members in a SIAF patrol and 20 members in a target then there are 400 calculations made. After a SIAF individual and target individual are selected the terrain routines are entered and calculations made to determine if line-of-sight exists. If line-of-sight does not exist a no-detection verdict is entered. If line-of-sight does exist and the target is firing then the target is declared detected and time of detection is stored in the array DTIME as shown in the figure. Here the value of DTIME is the current time plus the reaction time which is the time it takes the individual to react to the detection and either change his posture, firing option, movement rate, or change another of his attributes based upon this detection. As shown in the figure, if line-of-sight exists but the target is not firing then a visual detection subroutine is entered to calculate the visual detection time TT. This routine is similar to the routine used in the reconnaissance model described in Volume III. Based upon this calculation the matrix DTIME is again loaded. Finally, the DTIME plus a maximum time are compared with the current time to allow for considering the fact that an individual might have detected another individual 5 seconds ago and the detection may still be valid. As shown in the figure the variable MDET is set equal to TRUE or FALSE which indicates whether the detection did or did not occur. The model proceeds in this fashion until all individuals in the SIAF patrol and all individuals in the target have been examined for detection.

2.5.6 Calculation of Casualty Event Times

Figure 2.40 describes this calculation which starts with computing the assigned area of responsibility of each individual. From this information the next calculation essentially determines a figure of merit and determines firing assignments which will maximize this figure of merit. Thus, this calculation determines the optimum strategy for the

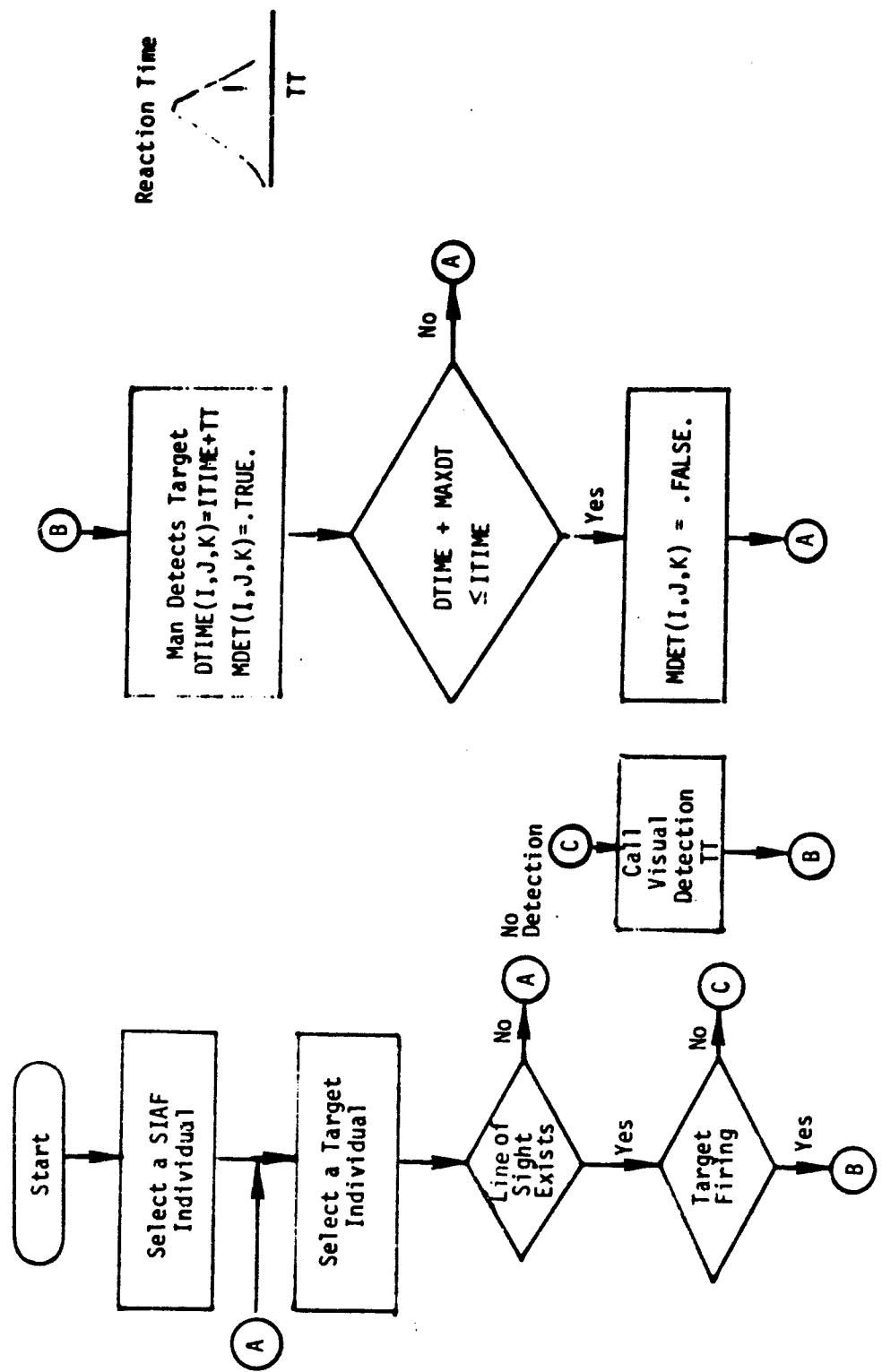


Figure 2.39. Calculation of Detection Events

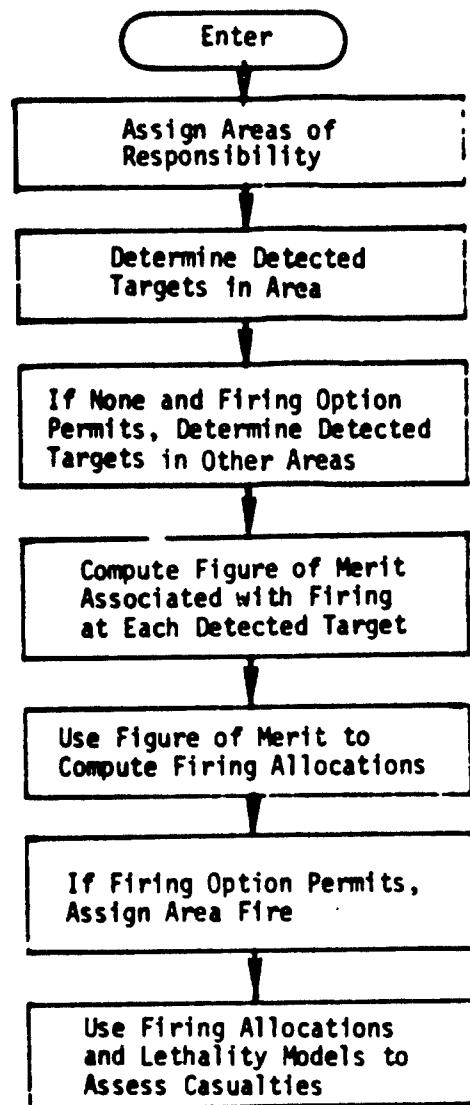


Figure 2.40, Calculation of Firing Events

target and SIAF patrol to use in firing. Based upon this optimum strategy, firing allocation and lethality models are entered to compute casualty times.

2.5.7 Calculation of Internal Communication Event Times

One of the events considered is the reception of a communication from another maneuver unit within the patrol. This would occur after deployment when units are divided into moving maneuver units and a base of fire. In this case it may be necessary to communicate decisions such as break contact, change deployment points, or exchange roles between the moving units and the base of fire. The latter two would be in response to a reaction of the target such as a change in its route or deployment. Several options are available to provide communications. These are by visual hand signals, aural commands, radio, smoke grenades and by sending a messenger. For each type of message, the model has a preference order for attempting communication. These are dependent on the tactical situation. The internal communications routines, called by IC, determine whether or not the communication will be successfully received and interpreted, and they determine the delay time until the message can be implemented. The delay time becomes an event time because the result affects further progress of the combat, including firing, detection and movement status.

2.5.8 Calculation of External Fire Support Event Times

The fifth event considered is an External Fire Support (EFS) event. This is defined as the arrival of a burst, either a volley of artillery or the weapons dropped in a single pass of a close air support aircraft. EFS is a scheduled event but its execution depends on the tactical situation. It is used preparatory to an attack mission. Upon identification of the target, the aimpoint is communicated and a schedule of arrivals is determined. If the target has not counterdetected the SIAF, then the arrivals are scheduled such that they are finished at the same time that the target reaches the minimum safe distance from the target. If this is the case, but the target subsequently counterdetects the SIAF, an immediate open fire command is sent and the schedule of arrivals is adjusted

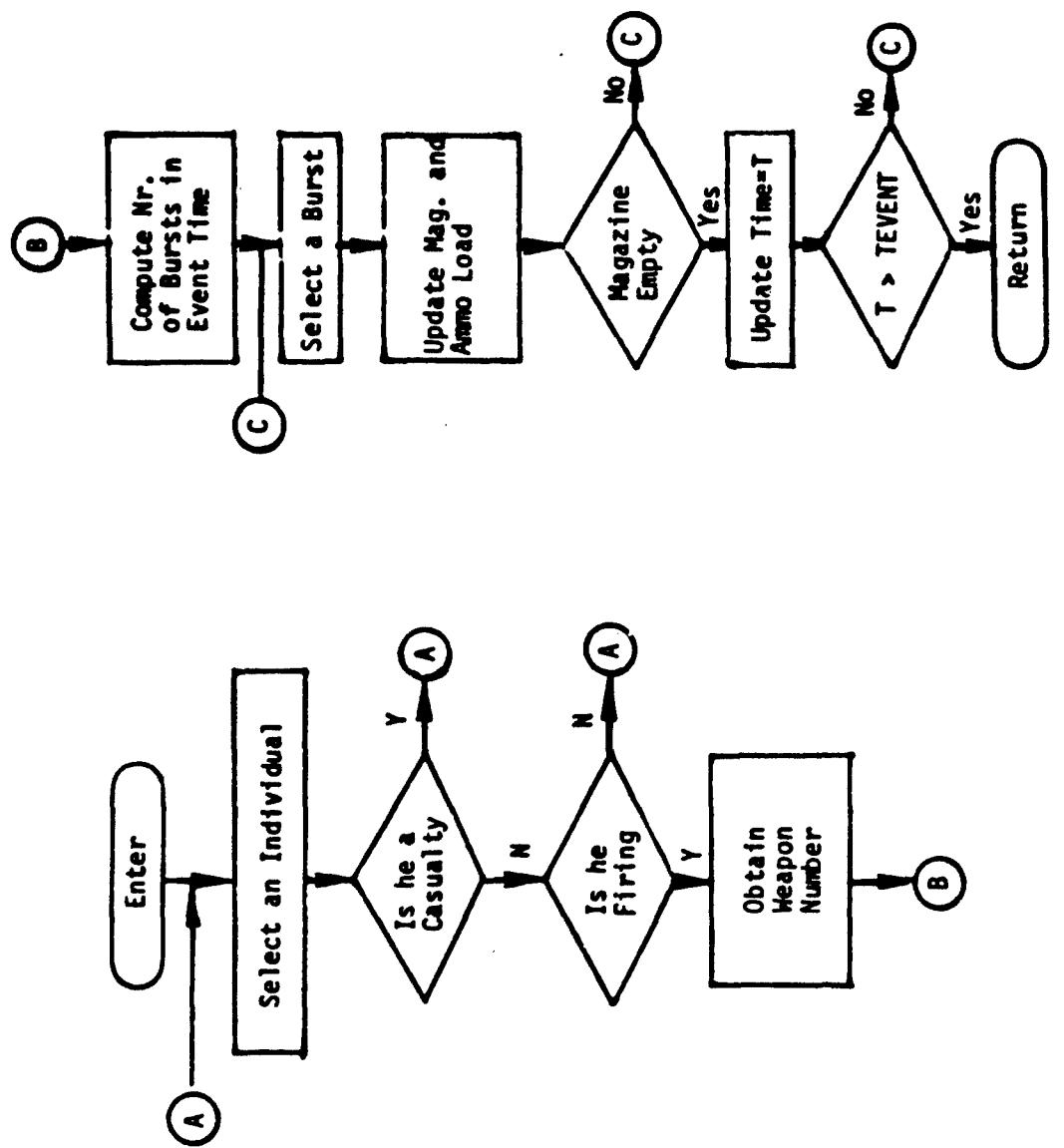


Figure 2.41, Ammunition Update Subroutine (AMMOUNP)

to start after a delay due to communications and time of flight. If the target has counterdetected the SIAF at the time of the original request, the delay time also includes time to make aiming calculations and to aim the weapons.

If external fire support is the next event, then Subroutine EFS1 is entered to compute the casualties due to each bomb or shell. This is done by considering aim point errors due to the inability of the SIAF to exactly determine the grid coordinates of the target. This includes both navigation errors and target location estimation errors. Also considered is the ballistic dispersion error. Once the aimpoint is determined (stochastically), the distance of each individual is determined and compared to the lethality data for the weapon. The attribute table is updated to account for any casualties.

Once these times are calculated the next event to occur be it movement, detection, casualty, EFS, or internal communication can be computed. If, for example, it is a movement event then the individuals are moved by updating the ATT matrix. If the next event is a detection event the corresponding logic is entered which will modify the movement rates and firing options based upon these detections. If, on the other hand, the next event was a casualty event then the appropriate element in the ATT matrix are updated to indicate that the individual has become a casualty. After these series of calculations are made the ammunition update, weapon substitution, break contact, and withdrawal routines are entered as appropriate. These routines are described in the next sections.

2.5.9 Ammunition Update

The purpose of this subroutine is to update the ammunition of each individual based upon the current elapsed time and the firing scheme. This routine is described in Figure 2.41 which shows that the first calculation is to select an individual. Next, the question is asked, "is he a casualty?" If so, his ammunition is not updated since he could not have been firing. Hence, another individual is selected and the calculations proceed. If he is not a casualty and if he is firing then his weapon number is obtained from the ATT matrix and the number of bursts in the current event time are computed for this particular weapon and particular

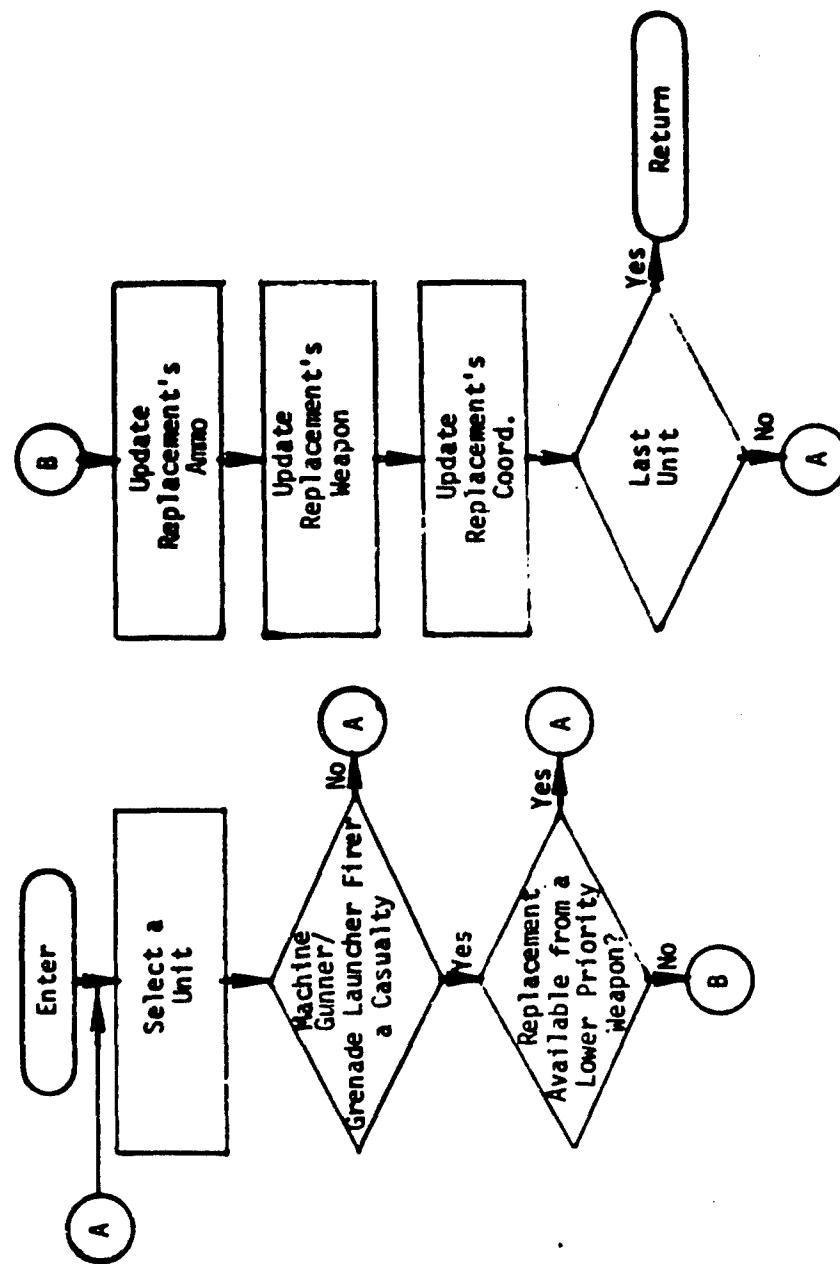


Figure 2.42, Weapon Substitution Subroutine (WSUBS)

Table 2-1. Firing Options

	Firing Options				
	0	1	2	3	4
Fire at detected targets in area of responsibility		X	X	X	X
If none, fire at any detected targets				X	X
If none, conduct area fire into area of responsibility			X		X
Don't fire	X	X		X	

Table 2-2, Firing Options for the Base of Fire and the Maneuver Unit

		Maneuver Unit							
		Base of Fire							
		SSMU	0	1	2	3	4	5	6
SSBF		Firing Option	0	0	0	0	0	2	2
0	0		1	1	1	1	4	2	2
1	1		1	1	1	4	2	2	
2	1		1	1	1	4	2	2	
3	1		1	1	1	4	2	2	
4	1		1	1	1	4	2	2	
5	2		2	2	2	2	2	2	
6	2		2	2	2	2	2	2	

SSBF = Suppression State for the Base of Fire

SSMU = Suppression State for the Maneuver Unit

firing rate of the individual. It could turn out that during the event time the magazine of the weapon became empty. Hence, the next series of calculations determines whether this occurred. If the magazine does become empty reloading time is entered into the calculation and modifies the number of rounds that the individual expended during the last event. If the magazine did not become empty, then number of rounds are computed based upon the event time and firing rate of the weapon. These calculations are done for each individual and the subroutine returns when all individuals have been examined.

2.5.10 Weapon Substitution

If an individual becomes a casualty (major wound or death) in a particular event, it could turn out that the patrol operations plan is to have another individual take over his weapon. This normally occurs in a case of team weapons like grenade launchers, and machine guns. If the machine gunner is hit a patrol member who fires a rifle or grenade launcher will take over his weapon. An attempt to replace him with a rifleman is made first. If the man who is hit fires a grenade launcher an attempt is made to replace him with a rifleman only. Subroutine WSUBS provides the logic implementing this strategy. Figure 2.42 illustrates the calculations made. First, a unit is selected and here the assumption is that intra-unit weapon substitution is not allowed. That is, weapon substitution is only allowed within a particular unit. After a unit is selected the question is asked if the gunner who is a casualty fires a machine gun or a grenade launcher. If not, another unit is selected and this unit selection process continues until the number of units in a patrol and target are exhausted. If the patrol member under consideration is a casualty and is either a machine gunner or fires a grenade launcher and an appropriate replacement can be found then the ammunition of the replacement is updated, his weapon is switched and his next movement coordinates are changed. These calculations continue until all units have been examined for weapon substitution. (Note: If the user does not desire to play weapon substitution, this subroutine can be bypassed by appropriately adjusting the input variables. This is described further in Volume VI, Subroutine WSUBS.)

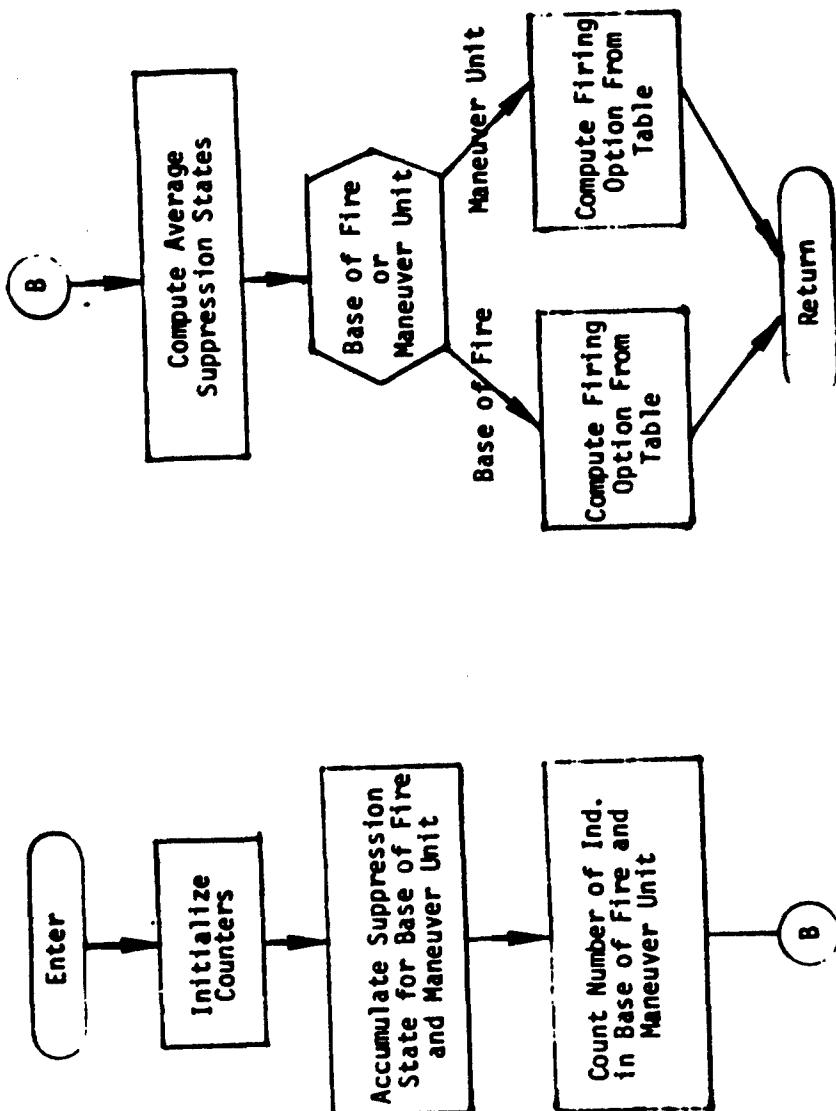


Figure 2.43, Firing Option Subroutine (FIREOP)

Table 2-3, Logic for Breaking Contact

Break Variable	Definition	Criteria
Firepower	$FP = \frac{\text{Firepower of Target}}{\text{Firepower of SIATF}}$	Break if $FP > FP_{Max}$
Casualty Fraction	$CF = \frac{\text{SIATF Casualties}}{\text{SIATF Force Size}}$	Break if $CF > CF_{Max}$
Time	$T = \text{Elapsed time of the firefight}$	Break if $T > T_{lim}$
Loss of Key Personnel	$L_i = 1$ if the PL is hit $L_i = 2$ if the PL and APL are hit	Break if $L_i = j$ ($j = 1$ or 2)
SIATF - Target Range	$R = \text{Minimum Distance Between SIATF and Target}$	Break if $R < R_{lim}$
Ammunition	$A = \text{Average Number of Rounds Remaining (per troop)}$	Break if $A < A_{lim}$

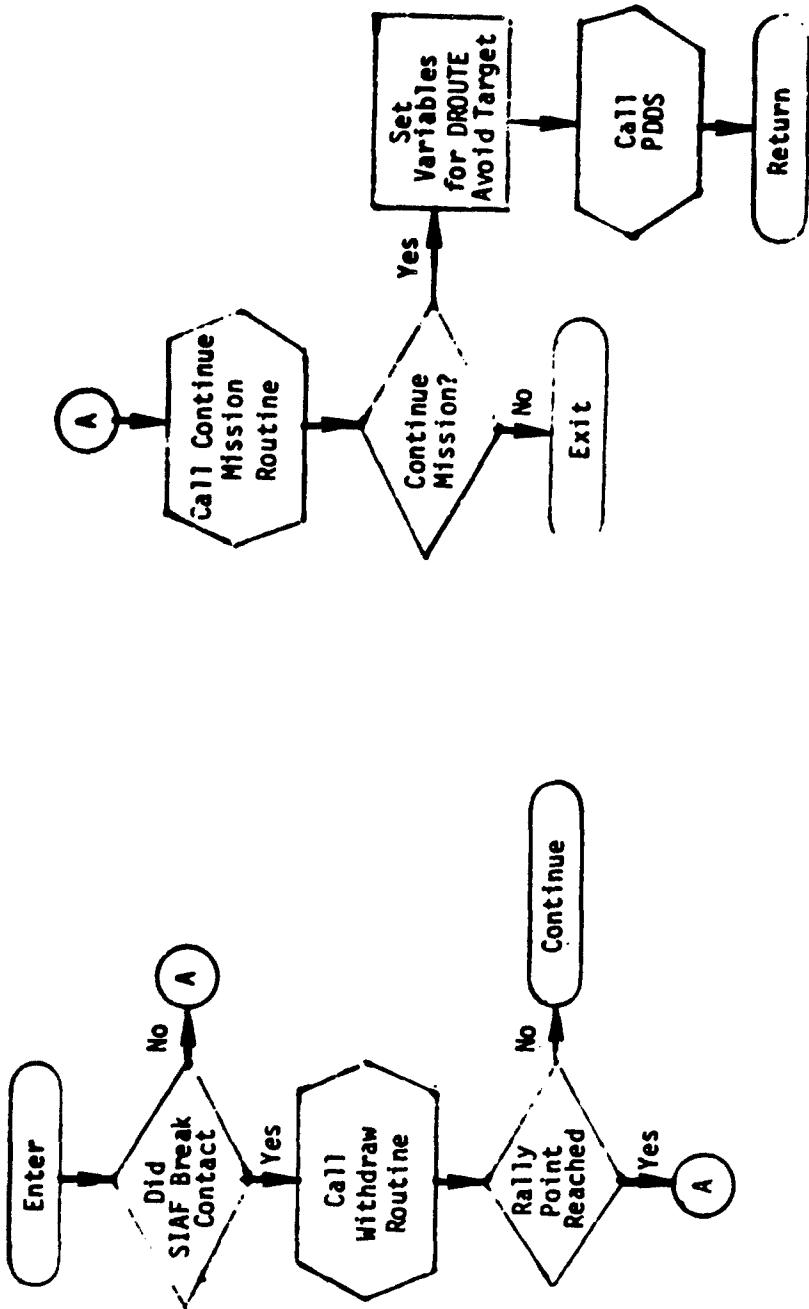


Figure 2.44, Logic For Continuing Reconnaissance After Combat

2.5.11 Firing Options

This particular section describes and presents an overview of how firing options are changed dynamically throughout the conduct of the simulation. Table 2-1 shows the firing options considered in the model. For example, Firing Option 0 is simply "don't fire". Firing Option 1 says, "fire if targets are in your area of responsibility. If none, then don't fire". Option 2 says "fire if detected targets are in area of responsibility. If none, then conduct area fire in area of responsibility." Options 3 and 4 are similar and can be examined by studying Table 2-1. Table 2-2 shows the firing options of both the base of fire and maneuver unit and here the numbers correspond to the options previously described in Table 2-1. For the base of fire, the firing option is a function of their own suppression state and the suppression state of the maneuver unit since their mission is to support the advance of the maneuver unit. The firing options of the maneuver unit on the other hand is a function of their own suppression state only. As an example, Table 2-2 shows that if the maneuver unit in suppression state 0 through 3 their firing option is 0, that is "don't fire". If they are in suppression state 4, 5, or 6, however, their firing option is firing option 2 which states fire at detected targets in area of responsibility. Hence, the firing options can be changed for the base of fire and the maneuver unit by user input data depending upon which particular strategy the user wishes to simulate.

Figure 2.43 shows how this logic is implemented in subroutine FIREOP. When the subroutine is entered counters are initialized and the suppression state for all individuals in the base of fire and maneuver unit is accumulated. Next the number of individuals in the base of fire and maneuver units are counted and the average suppression state of each of these units is computed. Table 2-2 is entered and the appropriate firing option computed by means of table look-up. In this fashion the firing options of both the base of fire and maneuver unit are dynamically adjusted throughout the execution of the combat mission.

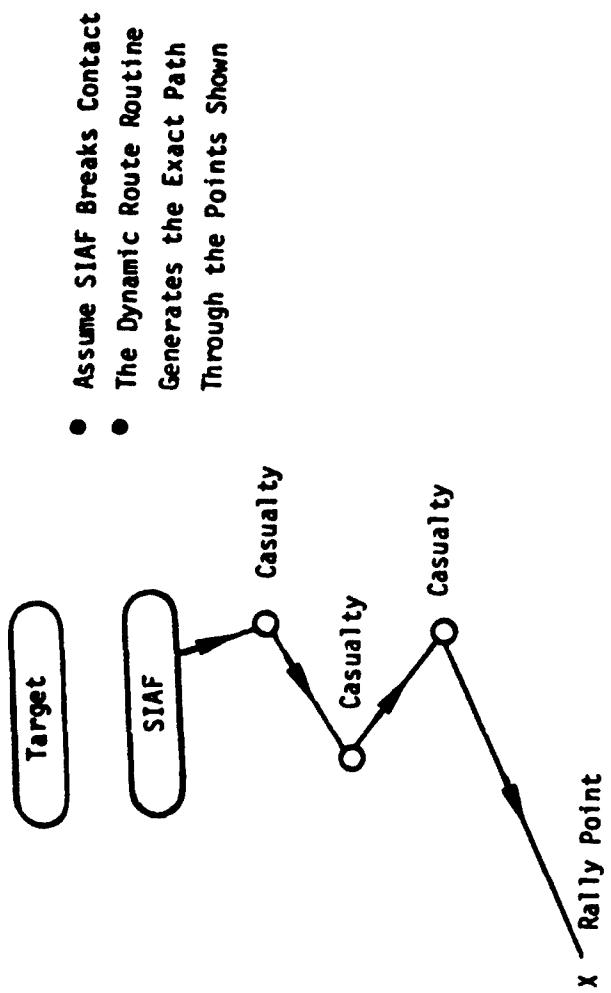


Figure 2.45, Illustration of Withdrawal Model

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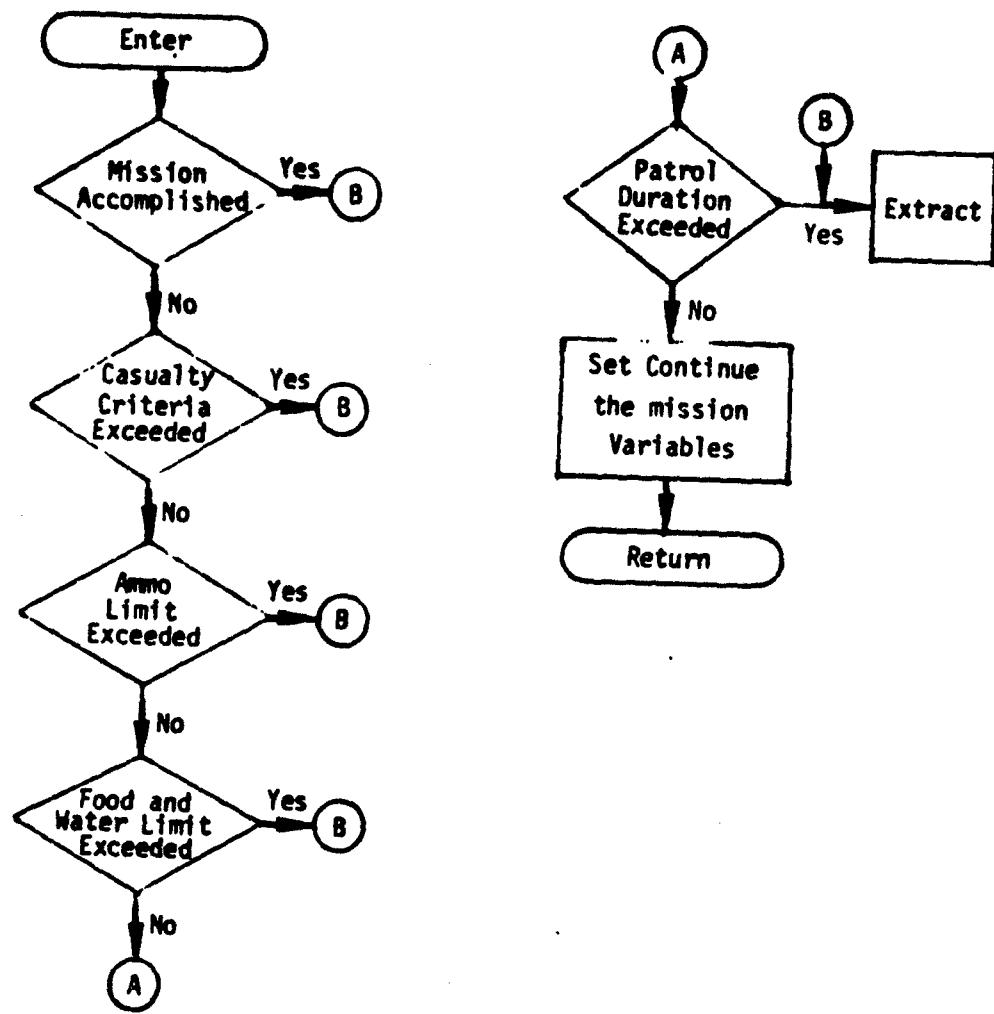


Figure 2.46, Continue The Mission Subroutine

This firer also has the option of firing his normally assigned weapon or throwing a handgrenade. Dependent upon the figure of merit calculated for both his normally assigned weapon and a handgrenade, for the situation that the firer under consideration is in, a decision is made as to which weapon to utilize. The handgrenade is basically used at short ranges under high suppression.

2.5.12 Mines

A SIAF patrol has the capability of Claymore mine ambush. Figure 2.46A depicts a typical mine field deployment. The user specifies a Claymore mine ambush intent by inputting the required inputs, and upon the enemy patrol reaching the most lethal point in the field (middlemost) the mines are detonated. The cumulative probability of kill of all mines in the field upon each target element is computed and the cumulative probability is Monte Carloed for each target individually to determine if the target suffered a minor wound (hit), major wound, or death. Figure 2-46-B shows how this logic is implemented in Subroutine MINES.

2.5.13 Break Contract

In each loop of the simulation, logic for breaking contact is entered if a break contact event is to occur and if so, a determination is made as to which side breaks contact. The break variables described in Table 2-3 are fire power, casualty fraction, time, loss of key personnel, SIAF-target range and ammunition. The criteria for breaking contact are adjusted by means of user input for both the SIAF patrol and for the target. For example, if the user wishes to implement a strategy whereby the SIAF patrol breaks contact after their ammunition reaches 30% of the initial load they implement this strategy by appropriately adjusting the ammunition limit variable shown in the table. The other criteria shown in the table are used in a similar manner. The break contact logic implements a break contact decision if any of the criteria are satisfied.

2.5.14 Withdraw

Figures 2.44 through 2.46 describe how we model a situation where SIAF returns to its reconnaissance mission after the combat operation has been completed. As seen from Figure 2.44, this routine is entered once the proper break contact variable has been set. The first question asked

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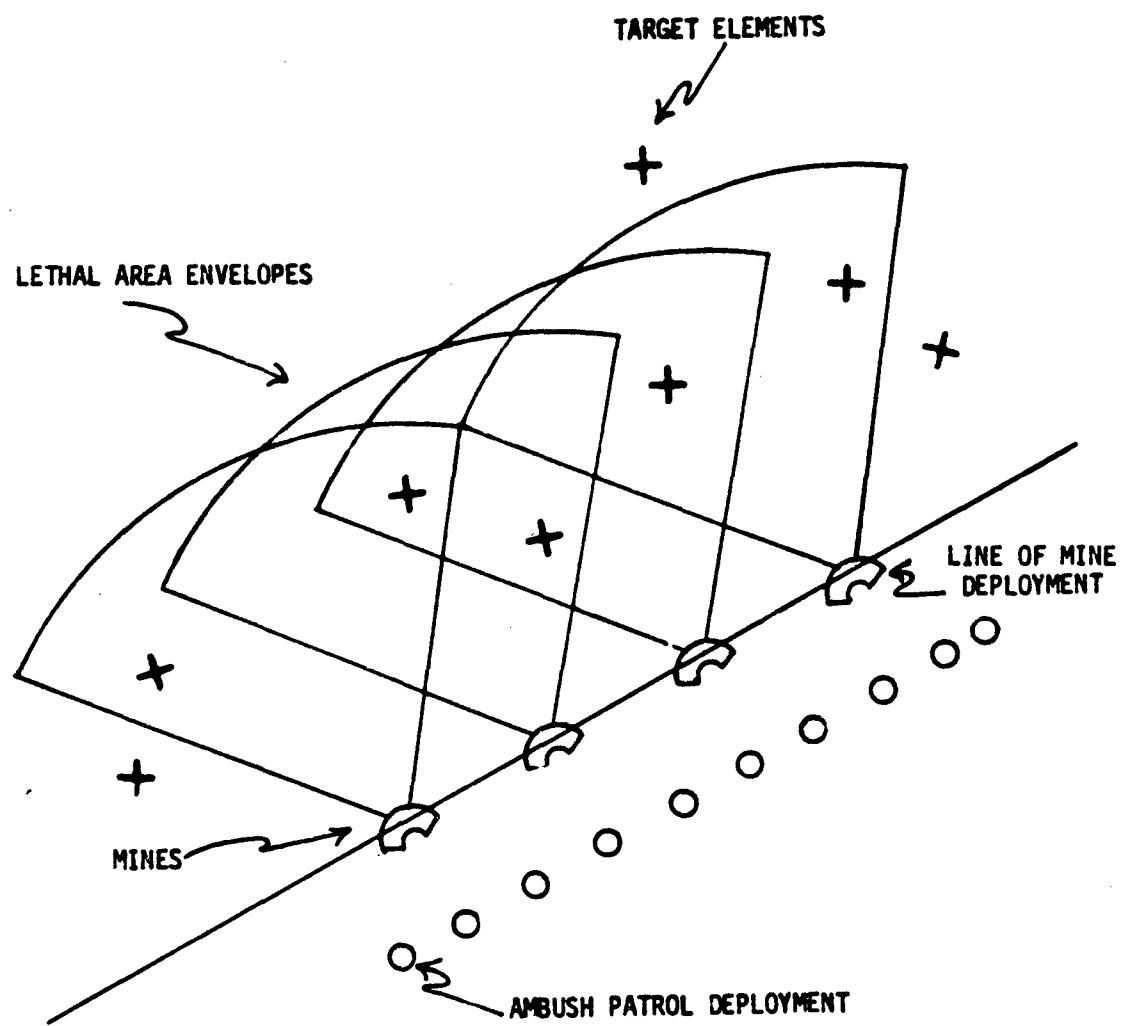


Figure 2.46A Typical Minefield Deployment

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USER INPUT:

NUMBER OF MINES
LENGTH OF FIELD
ANGLE OF DEPLOYMENT
CENTER OF FIELD

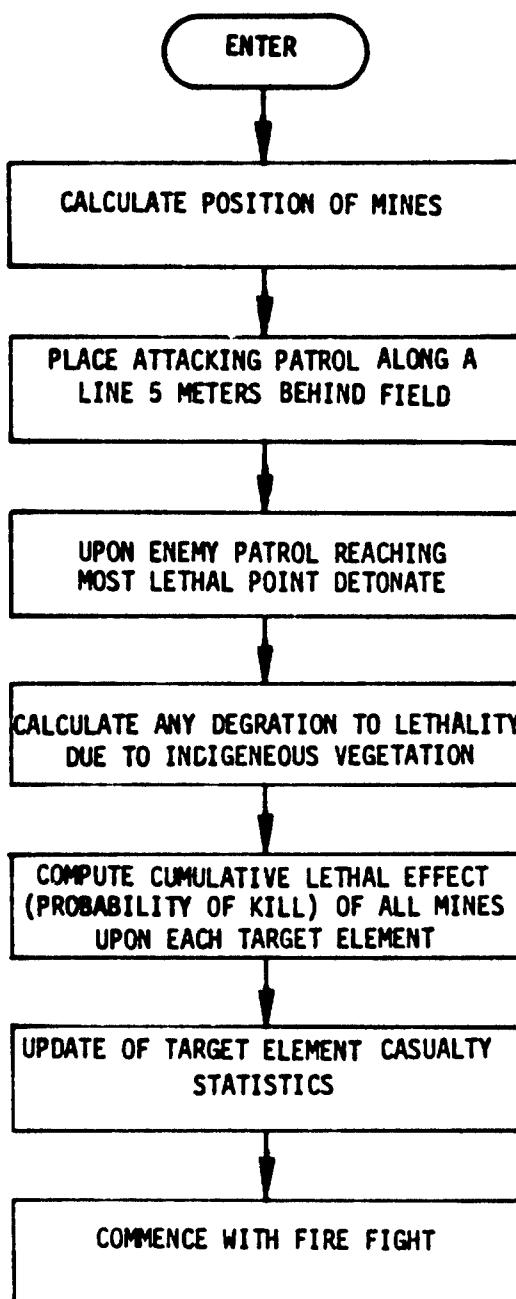


Figure 2.46B, Logic Diagram (MINES)

is, "did SIAF break contact?". If not, then no withdrawal is required for the SIAF unit and the continue-the-mission subroutine described in Figure 2-46 is entered. If SIAF did decide to break contact, then a withdrawal routine is entered. This withdrawal routine calculates the major withdrawal objective points for the patrol. Next, the withdrawal is simulated until the rally point is reached. Once the rally point is reached, the continue-the-mission decision subroutine is entered and if the decision is to continue the mission, then dynamic route variables are set up to avoid the target and get the patrol back to the planned route.

Figure 2.45 illustrates the withdrawal model which forces the patrol to pass through points where a casualty has occurred to the rally point. As indicated in Figure 2.45 the dynamic route subroutine is called to generate the exact route through the casualty locations to the rally point.

2.5.15 Continue the Mission

Once the rally point is reached, the continue-the-mission subroutine shown in Figure 2.46 simulates the patrol leader's decision to extract or go back to the planned route. This decision is based upon the variables shown which are mission objective, casualty criteria, ammunition limits, food and water limits, and patrol duration limits. By adjusting these limits which are user input values, the user can select the criteria he wishes to use in simulating the decision to continue the mission or extract. If a continue-the-mission decision is reached, dynamic route variables are set and subroutine PDDS (see Volume III) is called to generate the route back to the planned path. If the decision is to extract then the model terminates and variables are initiated for the next replication.

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2.5.16 Summary of Attacker and Defender Options

Prior to a detection occurring, the SIAF Reconnaissance Model simulates the SIAF mission as discussed in Section 2.4. Once a detection and identification is made (either by SIAF or by the target), the party making the detection and identification becomes the attacker and the other party becomes the defender.

As discussed in Section 2.5.1, the attacker will select one of five options, viz, 1) EES only, 2) ambush, 3) move with stealth to attack, 4) deploy for ambush with mines, 5) no combat. Meanwhile, the defender, having not yet detected, continues to move along his preplanned route. If the attacker selects options 2 or 3, a deployment point is computed and the dynamic route routine generates the attacker's route between his present position and the deployment point. If the defender detects the attacker before the attacker initiates the firefight, then the defender initiates the firefight or selects an alternative course of action to protect its position.

Once the firefight commences, the defender remains stationary unless he decides to break contact. If the target decides to break contact, the engagement is considered complete and SIAF decides whether to continue its mission. However, if SIAF decides to break contact, the withdrawal is simulated until the rally point is reached, at which point SIAF decides whether to continue its mission, in which case the SIAF Reconnaissance Model is again employed to simulate the remainder of the mission.

2.5.17 Summary of Model Capacities

This section summarizes the current capacities of the model. A summary of computer requirements is given in Sections 7.1 and 7.2 of this volume.

- Maximum number of men on each side = 20
- Maximum number of different weapons = 20
- Maximum number of different grenade launches = 10
- Maximum grid of terrain elevation points = 1366
- Maximum number of targets = 20
- Maximum number of preplanned route points for each target = 20
- Maximum number of preplanned SIAF route points = 100
- Maximum number of helicopter landing points = 5
- Maximum number of weather changes = 100
- Maximum length of simulated patrol = 10 days

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3.0 MODEL INPUT

The model input data consists of users inputs, data base, and elevation data. The elevation data is taken directly from digital TOPOCOM tapes from the Defense Mapping Agency. When a particular area of operations is desired, a set of subroutines is used to generate a file of elevation data which can be permanently stored. This file can then be accessed at the start of each run as long as the area of operations remains the same. This file contains elevation data at the maximum resolution (or minimum separation). The model then reads from this file to obtain data for the required resolution. The maximum elevation points at any one time is 8196.

The remaining data inputs are read via NAMELIST card input. In general, the namelist card input has been organized into categories of data base (NAML1), user input (NAML2), target oriented user inputs, (NAML3), and combat oriented user inputs (NAML4). Table 3.1 contains a complete list and definition of all of the required input variables. This table is organized by first presenting user inputs, (those variables specific to a situation) and then presenting the data base. (Variables whose values are unlikely to change from run to run). Within these categories the data is organized by categories according to the use of the variables. For example, all of the required inputs to describe the targets are found together.

The variables in the data base are further described by default values which are current best estimates. These need only be changed if better data become available.

Table 3.2 contains a cross reference to Table 3.1. Here all variables from the namelists are presented in alphabetical order with the sheet number of the corresponding location in Table 3.1. It is felt that this method of presentation allows the user to better understand the meaning of a variable because he is able to see its definition in the context of other variables with which it is associated.

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USER INPUT

SET UP

JSTART Starting point within run if RESTRT feature is used (See Volume III, Section 10.4)

JSTOP Termination point within run if STOP feature is to be used for later RESTRT.

NCOPY Number of copies of summary output desired

MAXCAS Number of cases

MAXREP Number of replications

ICOMBF Bypass combat flag

= 0 reconnaissance only
= 1 combat model included

IX1, IX2 Initial Random numbers (see Subroutine MAIN).

TERRAIN

THEATA

Angle between the X axis SIAF computer coordinate system and military grids degrees

VH X coordinate of origin of SIAF computer coordinate 4-digit military grid

VK Y coordinate of origin of SIAF computer coordinate 4-digit military grid

Table 3-1, Namelist Inputs (Sheet 1)

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TERRAIN (Continued)

COMPRES	Combat resolution for elevation array (Distance between grid lines)	meters (12.7)
RECRRES	Reconnaissance resolution for elevation array (Distance between grid lines)	meters (50.8)
RESMAX	Maximum resolution available for elevation array	meters (12.7)
IXMAT	Number of scan lines in input Z matrix (output from MAPGEN) (See Vol. III, Section 10.5)	-
IYMAT	Number of elevation points per scan line	-
IDOMST	Dominant soil type	-
DOMWT	Dominant class of micro-relief	-
DOMV	Dominant class of vegetation	-
NOB	Total number of linear obstacles	-
NRVP	Total number of vegetation polygons	-
NRMT	Total number of micro-relief polygons	-
NRST	Total number of soil polygons	-
LNR1	The integer number designating the first linear obstacle	-
VEGI	The integer number designating the first vegetation polygon	-
SOIL1	The integer number designating the first micro-relief polygon	-

Table 3-1, Namelist Inputs (Sheet 2)

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TERRAIN (Continued)

MICR1
The integer number designating the first soil
polygon

I0B(L)

Linear obstacle type; for L=1,2,3,...,NOB

where I0B(L) =

- 1 if linear obstacle L is a river
- 2 if linear obstacle L is a stream
- 3 if linear obstacle L is a ravine
- 4 if linear obstacle L is a dike
- 5 if linear obstacle L is a canal
- 6 if linear obstacle L is a cliff
- 7 if linear obstacle L is a road
- 8 if linear obstacle L is a trail
- 9 if linear obstacle L is a lake or reservoir

ITRC(L)

Geometry of Lth polygon, where

- 1 if Lth polygon is a triangle
- 2 if Lth polygon is a rectangle
- 3 if Lth polygon is a circle

for L=1,2,3,..., NRVP+NRMP+NRSOIL

(XOB{I,L},
YOB{I,L});

Coordinates of start point of segment I of
obstacle L, for L=1,2,...,NOB, and 1-1,2,...,
(NC0(L)+1) or coordinates describing the
geometry of the Lth polygon

NC0(L)

Number of line segments comprising linear
obstacle L, for L=1,2,3,...,NOB

ICL(L)

Class of the Lth polygon, for L=1,2,...,NRVP+
NRMP+NRSOIL

Table 3-1, Namelist Inputs (Sheet 3)

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NAVIGATION DEVICES

PPLS Portable Position Location System. If such a device is carried by SIAF, PPLS=1, if not carried by SIAF, set PPLS=0.

SCALE

TBUR Set TBUR=0 if it is impracticable to use PPLS or if sufficient time is not available. TBUR=1 if sufficient time is available only for a "quick" navigation fix. (2 min. after aircraft arrival, CEP=150.) TBUR=2 if sufficient time (15 min.) is available for an accurate navigational fix (CEP=60 meters).

SPEC

Map Scale Special Case. Allows override of HumRRO SIAF navigation specs. Input revised limit on standard deviation of distance between actual SIAF location and believed SIAF location. (HumRRO nav. specs. are used if SPEC is input as zero.)

Table 3-1, namelist Inputs (Sheet 4)

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SIAF INPUTS

DESCRIPTION

	Average height of a SIAF element	- meters
SC(1)	Average width of a SIAF element	- meters
SC(2)	Number of men in the SIAF patrol	- meters
SC(4)	Average visual reflectivity of a SIAF element	- dB
SC(5)	Hearing threshold for a SIAF member	- dB
SC(6)		

{ 0 if a vegetation class dependent formation is to be used for SIAF
1 if specific formation number 1 is to be used for SIAF
2 if specific formation number 2 is to be used for SIAF
5 if specific formation number 5 is to be used for SIAF

IFS } For Reconnaissance
(See DETECT)

(See FORMATIONS)

OPERATIONS PLAN

XBASE	X coordinate of base.	- 4-digit military grid
YBASE	Y coordinate of base	- 4-digit military grid
ITZERO	Time mission starts from base.	- days, hrs., min., sec.

Table 3-1. Namelist Inputs (Sheet 5)

SIAF INPUTS (Continued)

ITMAX	Limiting value on patrol time duration (used as temporary checkout input)	- days, hrs, min, sec.
<u>INSERTION</u>		
MODE	Insertion vehicle description (1 = helo, 2 = truck, 3 = boat, 4 = fixed wing).	
TDEBK(MODE)	Average time to debark, for M = insertion travel mode.	- days, hrs, min, sec.
VELM(MODE)	Average velocity of the insertion travel mode over the terrain from base to insertion point.	- meters/sec
TPREP	Time necessary to complete prep firing (i.e., - seconds time enemy has to move toward primary landing zone).	
NLZ	Number of landing zones	
XLZ(I)	X coordinate of the I th landing zone.	- 4-digit military grid
YLZ(I)	Y coordinate of the I th landing zone	- 4-digit military grid
PLZ(IZ)	Radius of landing zone IZ	- meters
NDECOV	Number of alternate landing zones (sequentially numbered) that are used for deceptive landings in addition to the actual landing zone attempt at the primary site. This dilutes the enemy in the area of actual landing. This number must be less than or equal to (NLZ-1).	

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Table 3-1, Namelist Inputs (Sheet 6)

SIAF INPUTS (Continued)

ISEN	$\begin{cases} 0 & \text{if LZ sensors are not used before landing attempt} \\ 1 & \text{if LZ sensors are used before landing attempt} \end{cases}$	
ISENLZ	Number of LZ's seeded with sensors (seeding proceeds sequentially starting with the primary LZ)	
HLZ	Time before landing that sensors are monitored.	- seconds
NSENS	Number of sensors in each LZ (each individual LZ has the same number of sensors)	
ENRG	Range within which the enemy may engage the SIAF upon attempting insertion	- meters
	<u>ROUTE</u>	
NPLAN(IZ)	Number of coordinate points for the planned route for insertion IZ	
XPLAN(IP,IZ)	X axis of the IP th checkpoint of the planned route when the insertion is made at point IZ.	- 4-digit military grid
YPLAN(IP,IZ)	Y axis of the IP th checkpoint of the planned route when the insertion is made at point IZ.	- 4-digit military grid
ITARR(IP,IZ)	Planned arrival time at checkpoint IP when insertion is made at point IZ (equals zero if this time is not pertinent).	- days, hrs., min., sec.
ITSTAY(IP,IZ)	Mission elapsed time to remain at non-movement point of IP th checkpoint for insertion point IZ.	- days, hrs., min., sec.

Table 3-1. SIAF Inputs (Sheet 7)

SIAF INPUTS (Continued)

ISTAY(IP,I2)	$\begin{cases} 0 & \text{if route checkpoint IP for insertion point I2 is not a non-movement point} \\ 1 & \text{if route checkpoint IP for insertion point I2 is a non-movement point} \end{cases}$	Planned departure time from checkpoint IP for insertion point I2. - days, hrs, min, sec.
ITMOV(IP,I2)		
NTAR	<u>TARGET INPUTS</u>	
NFIX	Total number of targets	
	Number of targets located specifically by user. (Others located randomly)	
ITST(IT)	Time when target IT is created in the model. - days, hrs, min, sec.	
ITSTOP(IT)	Time when target IT is eliminated from the model. - days, hrs, min, sec.	
IDET(IT)	$\begin{cases} 1 & \text{if target IT is to be considered on an element-to-element basis} \\ 0 & \text{otherwise} \end{cases}$	<u>MOVEMENT</u>
IMV(IT)	$\begin{cases} 1 & \text{target IT is fixed} \\ 2 & \text{target IT moves at random} \\ 3 & \text{target IT moves according to a time and checkpoint plan} \end{cases}$	

Table 3-1. Namelist Inputs (Sheet 8)

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TARGET INPUTS (Continued)
Movement (Cont'd.)

For IMV = 2 or 3 supply =

FRCMVD(IT)	Fraction of the time target IT is moving during the day
FRCMVN(IT)	Fraction of the time target IT is moving during the night
RANMAX(IT)	Maximum range target IT can travel. (Random only) - meters
TVEL(IT)	Velocity of the IT th target. (0 if not a manned target) - meters/sec.

IF IMV = 3 also add

IMP(IT)	Number of movement periods for target IT.
ITIMS(IL,IT)	The time that target IT initiates movement - days, hrs, min, sec. period IL.
GOALTX(IL,IT)	The X coordinate of the goal point for movement period IL of target IT.
GOALTY(IL,IT)	The Y coordinate of the goal point for movement period IL of target IT.
TC(1,IT)	The X starting coordinate for the IT th target (0 if random).
TC(2,IT)	The Y starting coordinate for the IT th target (0 if random).

Table 3-1. NameList Inputs (Sheet 9)

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TARGET INPUTS (Continued)

	<u>CHARACTERISTICS</u>	
TC(3,IT)	The average height of an element of target IT.	- meters
TC(4,IT)	The average width of an element of target IT.	- meters
TC(5,IT)	The number of fire teams making up target IT.	
TC(6,IT)	The number of elements making up target IT.	
TC(7,IT)	The average visual reflectivity of an element of target IT.	
TC(8, IT)	The average 1.06 micron reflectivity of an element of target IT (for laser designation).	
TC(9,IT)	The hearing threshold for a member of target IT.	- dB
		<u>FORMATION</u>
IFT(IT)	0 if a vegetation class dependent formation is to be used 1 if a specific formation for target IT is to be used (e.g., a fixed set of buildings)	{ For Reconnaissance (See DETECT)}
FORMAT(I,J,IT)	The locations within a target for a special formation of each of the J elements for target IT	

Table 3-1. Namelist Inputs (Sheet 10)

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TARGET INPUTS (Continued)
Formation (Cont'd)

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	Where: $I = 1$ is the X location of element J relative to the $J - 1$ element $I = 2$ is the Y location of element J relative to the $J - 1$ element (only used if $IFT(1T) = 1$)	
	For Renaissance (See UTECT)	
<u>NSTP(1T)</u>	<u>Number of special sound track periods of target 1T</u>	
<u>ISOFF(1K,1T)</u>	<u>The time when the IK^{th} sound period stops operating for target 1T</u>	- days, hrs, min, sec.
<u>ISON(1K,1T)</u>	<u>The time when the IK^{th} sound period starts to operate for target 1T</u>	- days, hrs, min, sec.
<u>SOUND(1K,1T)</u>	<u>Sound level for IK^{th} sound period for target 1T.</u>	- dB

Table 3-1. /ame list Inputs (Sheet 11)

TARGET INPUTS (Continued)

DETECTION

RCMAX(IT)

The range between a target IT and SIAF which describes the distance beyond which detailed detection computations are not desired.

RCMIN(IT)

The range between a target IT and SIAF that always requires detailed detection computations without first checking feasibility.
(See TARGET.)

POST DETECTION

0 if target IT is to be eliminated upon detection

- { 1 if SIAF should proceed toward target IT in order to identify the target given that it cannot be identified at detection
2 if SIAF should call external fire support against target IT after advancing for identification
3 if SIAF should avoid target IT upon first detection of target IT.
(See PDDS)

KREC(IT)

Table 3-1. Namelist Inputs (Sheet 12)

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<u>TARGET INPUTS (Continued)</u>	<u>EXTERNAL FIRE SUPPORT</u>	<u>(This Section For EFS Only Attack)</u>
IFSUP(IT)	$\begin{cases} 0 & \text{no external fire support available} \\ 1 & \text{artillery support available - Also used for combat} \\ 2 & \text{air support available} \end{cases}$	
	<u>Artillery</u>	
IFADJ(IT)	$\begin{cases} 0 & \text{if fire without adjustment} \\ 1 & \text{if fire with adjustment} \end{cases}$	
	<u>ITACT</u>	$\begin{cases} 1 & \text{if target digs in in-place} \\ 2 & \text{if target expands circularly (if IFADJ(IT) = 1)} \\ 3 & \text{if target moves to cover} \end{cases}$
		<u>Close Air Support</u>
IAMG(IT)	$\begin{cases} 1 & \text{if air/ground machine guns are used} \\ 0 & \text{if air/ground machine guns are not used} \end{cases}$	
ICBOM(IT)	$\begin{cases} 1 & \text{if cluster bombs are used} \\ 0 & \text{if CBU's are not used} \end{cases}$	
IGBOM(IT)	$\begin{cases} 1 & \text{if general purpose bombs are used} \\ 0 & \text{if general purpose bombs are not used} \end{cases}$	
IFAR(IT)	$\begin{cases} 1 & \text{if folding fin A/C rockets are used} \\ 0 & \text{if FFAR's are not used} \end{cases}$	

Table 3-1. Namelist Inputs (Sheet 13)

TARGET INPUTS (Continued)

	<u>If Using Cluster Bombs</u>	
FMCB1(IT)	Lethal area of CBU bomblet versus first pass personnel posture	- square
FMCB2(IT)	Lethal area of CBU bomblet versus second and subsequent pass personnel posture	- square
NCB(IT)	Number of ordnance delivering passes, CBU	
	<u>If Using General Purpose Bombs</u>	
FMGPB(IT)	Mean area effectiveness (GP) - personnel posture	
	<u>If Using Rockets</u>	
FMA1(IT)	Lethal area of rockets versus second and subsequent passes personnel posture	- square meters
FMA2(IT)	Lethal area of rockets versus second and subsequent passes personnel posture	- square meters
	<u>If Using Machine Guns</u>	
NGF(IT)	Number of rounds of machine gun fire	
VAX(IT)	Personnel vulnerable area to MG projectiles.	- square meters

Table 3-1, Namelist Inputs (Sheet 14)

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WEATHER INFORMATION

TSR	Time of sunrise	days, hrs., min., sec
TSS	Time of sunset	days, hrs., min., sec
NWCL(I,1)	Time at which weather class changes	days, hrs., min., sec
NWCL(I,2)	New weather class commencing at time NWCL(I,1)	
WDAY(I,J)	Daily weather information	
	I: Day of the patrol.	
	J: 1 = time of moonrise	hrs., min
	2 = time of moonset	hrs., min
	3 = type of moon	
	Type 0 = New Moon	*F
	Type 1 = 1/4 Moon	*F
	Type 2 = 1/2 Moon	x
	Type 3 = Full moon	x
	4 = Maximum temperature	*F
	5 = Minimum temperature	*F
	6 = Maximum relative humidity	x
	7 = Minimum relative humidity	x
	8 = Minimum wind velocity	kts
	9 = Average wind velocity	kts
	10 = Maximum wind velocity	kts
	11 - Direction wind is coming from	Compass bearing
		0 - 360°

Table 3-1, Namelist Inputs (Sheet 15)

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<u>COMBAT INPUTS</u>	
	<u>HUMAN</u>
XMU	Mean human reaction time to detection
SSIG	Standard deviation of human reaction time to detections
UNKCON	Factor to compute area of uncertainty of target position as a function of the elapsed time since the target was last seen.
VELNOM (I,K)	Nominal velocity, moving normally I = 1, or moving at top speed I = 2, where K = 1 for attackers, K - 2 for defenders. Meters/Seconds
FHCR	Fraction of height below which subject is said to be not standing
FHPR	Fraction of height below which subject is said to be prone.
XMAXDT	Elapsed time from last detection after which target position becomes unknown.
MAXDT	Maximum time after which previous detections lose their value
<u>FIRING</u>	
DELTA	Increment by which firing allocations are varied in the point fire allocation model (See FALFC)
AIMMX (K)	Contains maximum aiming time; K = 1 attacker, K - 2 defender
FTAPB (K)	Contains fraction of time between bursts spent aiming; K - 1 attacker, K - 2 defender
DTEFS	Maximum probable delay of EFS after EFS is called
HFR	Height above terrain cutoff for firing

Table 3-1, Namelist Inputs (Sheet 16)

Firing (Cont'd)

DF(I,J)

Firing rate degradation factor when the fraction of ammunition remaining is of index I; J - 1 for point-fire weapons, J - 2 for area-fire weapons

FORMATIONS (For Combat Only; See FORMS)

IPERM(J,M)

Contains the positions of a fire team. J indicates the fire team number and M indicates the particular permutation of fire team positions within their maneuver unit. (M = 1, 2, 3, 4, or 5).

IFORFT (J)

The formation type to be used by the individual within a fire team. Examples: = 1 column, = 2 wedge, = 3 vee, = 5 echelon right, - 6 echelon left; where J, - 1 for stealth, J = 2 for fire and movement, J = 3 for assault, J = 4 for pursuit, J = 5 for withdrawal, J = 6 for stopped.

IFORMT(J)

The formation type for fire teams within maneuver units (same as for IFORFT).

FORFTX (K,J)

The relative X location of the Kth position within fire team formation J

FORFTY (K,J)

The relative Y location of the Kth position within fire team formation J

FORMUX(I,J)

The relative X location of the Ith fire team in maneuver unit formation J

FORMUY(I,J)

The relative Y location of the Ith fire team in maneuver unit formation J

FORSF(X)

The relative spacing in the X direction of the patrol element from the fire team leader of fire team formation type J

Table 3-1, Namelist Inputs (Sheet 17)

Formations (Cont'd)		Notes
FORSFY(J)	The relative spacing in the Y direction of the patrol element from the fire team leader of fire team formation type J	
FORSMX(J)	The relative spacing in the X direction of the fire team in position from the leader of the maneuver unit in formation	
FORSMY(J)	The relative spacing in the Y direction of the fire team in position from the leader of the maneuver unit in formation type J	
	<u>FIRING ALLOCATION</u>	
COLMIN(K)	Contains minimum fraction of fire power directed against each detected target; K = 1 defender, K = 2 attacker	
WPWT(I,J)	Contains weapon weighting factor for firing allocation	
	J = 1 - attacker applies to defender's weapons	
	2 - defender applies to attacker's weapons	
	I = 1 - semi-automatic weapon	
	2 - automatic weapon	
	3 - grenade launcher	
ARSMN(K)	Contains minimum length of each man's area of responsibility; K = 1 attacker, K = 2 defender	
ARSPI(K)	Contains fractional overlap of each man's area of responsibility; 1 attacker, 2 defender	
FDGFAC(K)	Contains lateral distance on each side of right-most and left-most targets for defending total area of responsibility; K = 1 defender, K = 2 attacker	

Table 3-1. Namelist Inputs (Sheet 18)

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<u>DEPLOYMENT CRITERIA</u> (See DL0GIC)		
RAMB	Ambush range between deployment point and engagement point	Meters
RAMIN	Minimum admissible value of RA (see subroutine DL0G5)	Meters
RATT	Attack range between deployment point and engagement point	Meters
REFS	Minimum admissible distance between the subject patrol and object patrol for calling EFS.	Meters
ROBS	Maximum admissible distance between the subject patrol and the engagement point to use detailed terrain information (See DL0G7)	Meters
RSP	Approximate distance desired between trial deployment points	Meters
RZ	Maximum admissible ratio of line-of-sight cut-off distance to range to observed target for adequate cover due to line-of-sight obstruction	
I0REC	1 - SIAF to be the subject patrol 2 - target to be the subject patrol	In case of standoff only.
IPURSU(J)	= 0 if the maneuver unit is not to pursue the defender in the withdrawal mode past the last attacker objective point (presently not used).	
GSAPRR	Approximate spacing desired between rows and between columns of predeployment movement area array. (See DL0G8)	Meters
NSECT	Number of angular increments (through π radians) subtended by the circular array of trial deployment points about a stationary object patrol	

Table 3-1. Name list Inputs (Sheet 19)

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Deployment Criteria (Cont'd)

CADM	Minimum admissible value of ADM, where ADM is the average merit value of trial points set in predeployment movement area ($0 \leq CADM \leq 1$). (See LOGIC)	
FRAMB	Minimum admissible force ratio for ambush	
FRATT	Minimum admissible force ratio for attack	
GMAX	Maximum admissible slope from deployment point to engagement point for engagement	
CC1 CC2 CC3	Percentage thresholds, to be used jointly, with PPI, PP5, for determining adequate cover, concealment, and observation (see subroutine CC0).	
CLASS(J,K)	0 if micro-relief Class J and vegetation Class K are deemed jointly admissible for a deployment point (See DL067). 1 if micro-relief Class J and vegetation Class K are deemed joint conditionally admissible 2 if micro-relief Class J and vegetation Class K are deemed joint inadmissible	
DTDAMB	Minimum deployment time required for ambush	Seconds
DTDATT	Minimum deployment time required for attack	Seconds
DTENGPM	Maximum admissible time for object patrol to move to engagement point	Seconds
DTPURM	Maximum admissible time for subject patrol to move to deployment point.	Seconds

Table 3-1. Namelist Inputs (Sheet 20)

Deployment Criteria (Cont'd)

PP1	Probability thresholds, to be used jointly with CC2, CC3, for determining adequate cover, concealment and observation (see subroutine CC0).
Q1	Coefficients, non-negative and summing to 1, used to determine the merit value of a point in the movement area (See subroutine CC0).
Q2	
Q3	
	FIRING OPTIONS (See FIREOP)
FOTB(I,J,K)	Firing options for the base of fire where I - the average suppression state of the base of fire, J - the average suppression state of the unit they are supporting, and K - 1 for attackers, K - 2 for defenders.
FOTM(J,K)	Firing options for the unit being supported by the base of fire where J is the average suppression state of the unit and K - 1 for attackers, K - 2 for defenders
	SUPPRESSION
DJUST (J,K)	Defines suppression state J as a function of P _{HIT} per minute; K - 1 defender, K - 2 attacker (See SUPN)
SUFAC(I,J)	Contains degradation factors J each suppression state (I); J - 1 firing rate; J - 2 aiming accuracy; J = 3 moving; J = 4 hand grenades
	WITHDRAWAL
NSECTR	Number of angular increments (through a half arc of 60°) between middle trial point and extreme trial point (use to select a rally point). (See RPT)

Table 3-1. NameList Inputs (Sheet 21)

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Withdrawal (Cont'd)	
DWDR	Radius of circular array of trial points for withdrawing to rally point
CARFR	Maximum allowable value of the ratio: $\frac{\text{number of casualties carried}}{\text{number of members carrying}}$
C1	Maximum admissible ratio of current food per man to initial food for extraction
C2	Maximum admissible ratio of current water per man to initial water per man for extraction
LDAYS	Minimum admissible number of days elapsed for extraction
	<u>DEFENDER REACTION (See Subroutine REACT)</u>
KDEFOP	Defender option index (after detecting attacker) 1 Withdraw at top speed 2 Deploy in place 3 Start firing in place 4 Ignore detection 5 Rotate formation and stop 6 Deploy with stealth to new point

Table 3-1, Namelist Inputs (Sheet 22)

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ATTRIBUTES

XATT(I,J,K)

Personnel attributes I for each man J, K = 1 for attackers
 $K = IT + 1$ for defenders, where IT is the target number 1-4

I: Is the attribute of the Patrol Member

1 Team number

2 Weapon number (See WTS In Weapon Supply DATA BASE)

3 Current ammunition supply (rounds)

4 Casualty status: 0 = not a casualty

1 = minor wound

2 = major wound

3 = dead

5 Firing status: 0 = not firing

1 = area fire

2 = point fire

6 Current suppression state

7 Current X coordinate (meters)

8 Current Y coordinate (meters)

9 Next X coordinate (meters)

10 Next Y coordinate (meters)

11 Height (meters)

12 Width (meters)

13 Current posture: 1 = standing

2 = crouching

3 = prone

14 Moving Status (0 = stopped, 1 = moving

normally, 2 = moving at top speed)

15 Maneuver unit to which the element belongs

16 Number of rounds remaining in magazine

17 Function in Patrol: 1 = Patrol Leader

2 = Asst. Patrol Leader

3 = Machine Gunner

4 = Grenade Launcher

5 = Rifleman

18 Movement rate of each individual

Table 3-1, Name List Inputs (Sheet 23)

Attributes (Cont'd)

- 19 Individual's assignment: 1 = if in base of fire
2 = if in maneuver unit
- 20 Initial ammunition supply
- 21 Weapon type: 1 = point fire
2 = area fire
- 22 Position in fire team
- 23 Secondary weapon carried: 13 = Hand Grenade
0 = None
- 24 Hand Grenade Supply
- 25 Smoke Grenade Supply

VATT(I,J,K)

Maneuver unit attributes I for each maneuver unit J, K = 1
for attackers, K = IT + 1 for defenders, where IT is the
target number 1-4

- I: 1 = Movement type, loads MOVTYP
- 2 = Number of fire teams in the maneuver unit
- 3 = Index M used to specify which of the particular
permutation used to assign fire teams to their
positions within their maneuver unit
- 4 = Number of patrol member acting as leader of
the maneuver unit. Loads KPEN
- 5 = Maneuver Unit assignment, Loads IBF
- 1 = base of fire
- 0 = moving

Table 3-1, Namelist Inputs (Sheet 24)

ZATT(I,K)

- ATTRIBUTES (on :NL :J)
- Attacker defender attribute I, K = 1 for S1:M, K = IT + 1
for target IT, where IT is the target number 1-4
- I:
- 1 = Number of maneuver units in the patrol
 - 2 = Patrol mission. Loads MISS
 - 3 = Availability of external fire support to patrol;
 - 0 = not available
 - 1 = available. Loads EFSA
 - 4 = Patrol member number of patrol leader. Loads NPL
 - 5 = Patrol member number of assistant patrol leader.
Loads NAPL
 - 6 = Relative weight factor assigned to semi-automatic weapons in defining firepower for the attacking patrol. Loads SCEMI(1)
 - 7 = Relative weight factor assigned to semi-automatic weapons in defining firepower for the defending patrol. Loads CSEMI(2)
 - 8 = Relative weight factor assigned to automatic weapons in defining firepower for the attacking patrol. Loads CAUTO(1)
 - 9 = Relative weight factor assigned to automatic weapons in defining firepower for the defending patrol. Loads CAUTO(2)
 - 10 = Relative weight factor assigned to grenades in defining firepower for the attacking patrol.
Loads CGREN(1)
 - 11 = Relative weight factor assigned to grenades in defining firepower for the defending patrol.
Loads CGREN(2)
 - 12 = Firepower ratio which if exceeded will result in a break contact decision for defenders. Loads FPMAX(1)
 - 13 = Firepower ratio which if exceeded will result in a break contact decision for attackers. Loads FPMAX(2)

Table 3-1. Namelist Inputs (Sheet 25)

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ATTRIBUTES (CONTINUED)

- 14 = Maximum number of rounds per man which will result in a break contact decision for attacking patrol. Loads RLIN(1)
- 15 = Maximum number of rounds per man which will result in a break contact decision for defending patrol. Loads RLIN(2)
- 16 = Casualty fraction which it exceeded will result in a break contact decision for attacking patrol. Loads CFMAX(1).
- 17 = Casualty fraction which if exceeded will result in a break contact decision for defending patrol. Loads CFMAX(2)
- 18 = Value of the loss of key personnel (see definition of L(K)) which will result in a break contact decision for attackers. Load LKP(1)
- 19 = Value of the loss of key personnel (see definition of L(K)) which will result in a break contact decision for defenders. Load LKP(2)
- 20 = Elapsed engagement time which will result in a break contact decision for attacking patrol. Loads TLIN(1)
- 21 = Elapsed engagement time which will result in a break contact decision for defending patrol. Loads TLIN(2)
- 22 = Range between units which will result in a break by defending patrol. Loads DISTL
- 23 = Orientation angle of patrol configuration if stationary, as required by subroutine FORMST

Table 3-1, Namelist Inputs (Sheet 26)

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XLAAN (I,J)	WEAPON	Contains lethal areas for grenade Type J
	1 = 1	Lethal area for minor wound - target position 1 = standing
	2	Lethal area for minor wound - target position 2 = crouching
	3	Lethal area for minor wound - target position 3 = prone
	4	Lethal area for major wound - target position 1 = standing
	5	Lethal area for major wound - target position 2 = crouching
	6	Lethal area for major wound - target position 3 = prone
	7	Lethal area for death wound - target position 1 = standing
	8	Lethal area for death wound - target position 2 = crouching
	9	Lethal area for death wound - target position 3 = prone

Table 3-1. Name list Inputs (Sheet 27)

WCHAR(I,J)

WEAPONS (Continued)
 Weapon characteristics I for each weapon number J.

1	Maximum range (meters)
2	Minimum range (meters)
3	Rounds per trigger pull - point fire
4	Actual firing rate - point fire (trigger pulls/min)
5	Rounds per trigger pull - area fire
6	Actual firing rate-area fire (trigger pulls/min)
7	P given hit indicator (or value)
8	Air error indicator
9	σX_1 (mils) used if aim error indicator is zero
10	σY_1 (mils)
11	σX_2 (mils)
12	σY_2 (mils)
13	μX_3 (mils)
14	μY_3 (mils)
15	σX_3 (mils)
16	σY_3 (mils)
17	Distance between aimpoints - area fire (meters)
18	Maximum number of aimpoints in area of responsibility - area fire
19	Minimum number of aimpoints in area of responsibility - area fire
20	Vertical aimpoint above ground level for area fire (meters)
21	Lethal area indicator (= 0 except for grenades)
22	Weapon type for area assignment (1 = semi-automatic, 2 = automatic, 3 = grenades)
23	Weapon type for firing allocating weight factors (1 = semi-automatic, 2 = automatic, 3 = grenades)
24	Weapon magazine capacity (rounds)
25	Loading time (Seconds)

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Table 3-1, Name list Inputs (Sheet 28)

MINES

NBR	= Number of mines deployed by Subject Patrol
LGTH	= Length of mine field (meters)
XCENT YCENT	= Coordinates of the centroid of the mine field deployment line segment. (line along which mines are deployed). (Map Coordinates)
TAK	= Angle that the mine field deployment lines makes with the X-axis. Positive counterclockwise
XLAAM (I, LAIC)	= Lethal area for mines. See table XLAAM, Volume IV
LAIC	= Lethal area indication for mines. Points to appropriate lethal area column for mines in table XLAAM
XENGA YENGA	= Coordinates of engagement point (Map Coordinates)
<u>EXTERNAL FIRE SUPPORT</u> (For Combat Model)	
T1	= The time to make a request for EFS plus aiming calculation time, and time for flight of the shells
T2	= The time to communicate open fire request plus the time of the flight of the shells given that attack has been previously planned
T3	= The time delay between each volley of shells
SAFDIS	* The safe-distance radius between the SIAF and target for an EFS attack

Table 3-1. Namelist Inputs (Sheet 29)

External Fire Support (Cont'd)

NVOLLEY = The total number of volleys in the EFS attack

SIGMDIS = The error due to ballistic dispersion expressed as the standard deviation.

JARTL = Variable whose value (1, 2, 3, 4, 5, 6) specifies which type of artillery or air support is used:

- 1 = 4.2 inch mortar
- 2 = 155 MM Howitzer
- 3 = 105 MM Howitzer
- 4 = 175 MM Gun
- 5 = 8 inch Howitzer
- 6 = Air support

MAEE (Z,J) Lethal radius of selected ammo against Posture (Z) for kill level J
 J=1 death, J=2 major wound, J=3 minor wound.

NSUPP = Suppression state assigned to enemy patrol after completion of the first volley of EFS

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
IPOS	Total number of different personnel postures in set		
SEGMIN	Minimum segment length for which a segment is considered negligibly small	meters	0.1
DSTEP	The maximum step size to be used in a mini-segment. The highest velocity moving feasible target will define the time step size to use for detailed	meters	10.

Table 3-1, Namelist Inputs (Sheet 30)

Data Base Set Up (Cont'd)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
DSTEP	detection to assure, at most, a step size of DSTEP for any target or for SIAF (the value must be > 0)	meters	
MAXDIS	Maximum distance patrol can move in any event time	Meters	
FORMS(I,J,IFS)	FORMATION (Reconnaissance Only) The location within a SIAF patrol for each of the elements J for each type of special formation IFS (used by Subroutine DETECT when man-to-man detection is desired)	meters	
	where: I = 1 is the X location of element J relative to the J = 1 element I - 2 is the Y location of element J relative to the J = 1 element		
BSAREA	Body surface area	square ft	20.
CONCAP	Convective capacity content	BTU/lb ⁰ F	0.0735
CPRAT (L)	Energy expenditure rate for type L check point (rest, recon, sleep, etc. - subroutine HUMAN)	meters	See Subroutine HUMAN

Table 3-1, Namelist Inputs (Sheet 31)

Human Maintenance (Cont'd)

SIGFFR	Heat transfer constant: $\sigma * F_{ae} * f_r$	BTU/ft ² hr (°R) ⁴	0.1103×10^8
where			
σ	= Stephen-Boltzman constant		
F_{ae}	= Shape emissivity factor		
f_r	= Radiation area factor		
RHOH	Air density	1bs/cu ft	0.075
P	Barometric pressure	mm Hg	760.
To	Base film temperature, absolute	F	536.
P0	Standard pressure	mm Hg	760.
RPE	Vapor resistance, air	in. of air	0.24
RPG	Vapor resistance, garments	in. of air	0.50
XMAX	Maximum SIAF personnel energy expenditure rate(BTU/hr)		

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Table 3-1, Namelist Inputs (Sheet 32)

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HUMAN MAINTENANCE (cont.)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
FHRAT(L)	Food consumption energy expenditure rate for type L checkpoint (rest, recon, sleep, etc. - see Subroutine HUMAN).	BTU/hr	See Subroutine LOGIS
LAMDAE	Heat of vaporization	BTU/lb	1080.
STS	Skin temperature	°F	95.
PS	Vapor Pressure at skin	in. Hg	42.
<u>TERRAIN</u>			
SL1	Limiting value on terrain surface quadratic coefficient - a value close to zero indicates the terrain surface is approximately linear	5×10^4	
SL2	Limiting value of slope differences	0.06	
DMT(I,K)	Density of micro-relief feature of type K (positive undulations, negative undulations, boulders) in micro-relief class I ($I=1,\dots,5$).	number/acre	See Subroutine MICROT
RHOI(II,U)	Density of vegetation features type U (1=grass, 2=brush, 3-tree trunk, 4-tree crown) in vegetation class II.	number/acre	See Subroutine VEGCOM
RMAX(II,U)	Range at which a target has unity probability of being completely concealed by vegetation features of type U in class II.	meters	See NAMELIST

Table 3-1, Namelist Inputs (Sheet 33)

TERRAIN (Cont.)			
<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
RMTMAX(I,L)	Range at which a target has unity probability of being completely concealed by micro-relief features of type L (1=positive undulations, 2=negative undulations, 3=bulldozers) in micro-relief class I (see Subroutine MICROT).	meters	See Subroutine MICROT
W(I,U)	Width of vegetation features of type U (1=grass, 2=brush, 3=tree trunks, 4=tree crowns) in vegetation class I (see Subroutine VEGCON).	meters	See Subroutine VEGCON
WLT(L,K)	Width of micro-relief feature of type K (1=positive undulations, 2=negative undulations, 3=bulldozers) in micro-relief class L (see Subroutine MICROT)	meters	See Subroutine MICROT
DSW11	Water depth in vegetation class 13 - sparse swamp.	meters	1.0
DSW12	Water depth in vegetation class 14 - dense swamp.	meters	1.0
DRICE	Water depth in vegetation class 16 - rice field	meters	0.3
H(I,U)	Height above surface of vegetation features (1=grass, 2=brush, 3=tree trunks, 4=crowns of trees) for vegetation class I (I=1,...,16).	meters	See Subroutine VEGCON

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Table 3-1. Namelist Inputs (Sheet 34)

TERRAIN (cont.)			
<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
HB(J)	Height of obstacle of type J for J=1,...,9 (see Subroutine TERCON).	meters	See Subroutine TERCON
HMT(I,K)	Height of a micro-relief feature of type K (positive undulations, negative undulations, boulders) in micro-relief class I (I=1,...,5).	meters	See Subroutine MICRO1
AQXMAX	The maximum X coordinate at the boundary of the area of operations.	meters	7200.
AQYMAX	The maximum Y coordinate at the boundary of the area of operations.	meters	2400.
REF(II,J)	The effective background reflectance for vegetation class II where		See Subroutine VISUAL
	1 is with a downward look angle		
	2 is with a nearly parallel look angle		
	3 is with an upward look angle		
XLP(II)	The fractional light penetration of vegetation class II		See Light Penetration Subroutine (Volume II, Section 3.2)
VEGC(3,II)	The formation type for moving in the vegetation class II (1-file; 2-column; 3-diamond) (Reconnaissance Only)	meters	See DETECT
VEGC(1,II)	The formation spacing parameter for the vegetation class II (Reconnaissance Only)	meters	See DETECT

Table 3-1. Namelist Inputs (Sheet 35)

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<u>Symbol</u>	<u>NAVIGATION</u> (See NAV Subroutine)	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
SGMTAB	Sigma, Map Terrain Association, Best. For the area of SIAF operation this value represents the standard deviation of the best (minimum) distances within which SIAF can determine its location at any point on its route (except a check-point) by Map Terrain Association, provided that visibility and flight level are adequate (i.e., ALL = ALLB, VISM = VISMB).		meters	50.
SGMTAW	Sigma, Map Terrain Association, Worst. Analogous to SGMTAB, but for poor visibility (VISM = VISMW, ALL = ALLW). This term represents the limit on position location by map terrain association.		meters	200.
VISMB	Meteorological Visibility, Best. Visibility (VISM) at which the surrounding terrain features can be seen and identified in sufficient detail to allow the SIAF location to be determined (by Map Terrain Association) to approximately the distance given by the one sigma value of SGMTAB.		meters	13.
VISMW	Meteorological Visibility, Worst. Similar to VISMB described above, but for the "worst" visibility. If VISM = VISMW then SGMTA = SGMTAW. If VISM < VISMW then SIAF location cannot be determined by Map Terrain Association.		meters	300.

Table 3-1. Namelist Inputs (Sheet 36)

NAVIGATION (cont.)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
ALLW	The "worst" value of Ambient Light Level (ALL) for Map Terrain Association. If ALL > ALLW then SIAF location cannot be determined by Map Terrain Association.	ft. Lambert	4×10^3
ITACOS	Average time necessary to get an air craft on-site if PPLS is to be used	seconds	900.
ALLB	The "best" value of Ambient Light Level (ALL) for map-terrain-association (i.e., that value of ALL at which SIAF location can be determined to approximately SCMTAB provided that visibility is good). If ALL > ALLB then it is assumed that ALL > ALLB.	ft. Lambert	5×10^3
PMC	Point-on-map Error (Constant Component). Error associated with putting the believed SIAF location on the map as a point (25 meters suggested for 1:50,000 map; other map scales are automatically converted internally).	meters	25.
PNR	Point-on-map Error (component that increases with range traveled). (25 meters for 1:50,000 map; other values converted internally).	meters	25.
RC	Range Error Constant. Average error associated with estimating range traveled (by pace count), expressed as % of distance traveled since last checkpoint.		4.

Table 3-1. Namelist Inputs (Sheet 37)

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<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
RCTAR	Range Error Constant Target Estimate. Average error (σ) associated with visual estimation of the range to a sighted target, expressed as % of estimated range.		10.
BE	Base Error. (σ_{BE}). Average distance between SIAF location and exact center of checkpoint location when SIAF believes it is at checkpoint.	meters	25.
AA	Average compass reading error (assume more than one compass reading is taken for mission leg).	degrees	1.85
AEQ	Effect of special equipment on estimating average compass reading error.	degrees	0.
ATTAR	Angle error, target estimate. Average compass reading error of bearing to target.	degrees	4.
GR	Grid Reading Error. Introduced by translating the point on the map into eight-digit grid readings (25 meters for 1:50,000 map; other values converted).	meters	25.
ATTER	Effect of terrain on estimating average compass reading error.	degrees	0.

Table 3-1. Name list Inputs (Sheet 38)

NAVIGATION (cont.).

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
RTER	Effect of terrain on estimating range traveled.		0.
REQ	Effect of special equipment on estimating range traveled.		0.
ITDRPM	Average time for SIAF to determine its position by dead reckoning, put point on map, and read eight digit grid coordinates.	seconds	60.
ITMTA	Average time necessary to attempt position location by map-terrain association with good light and visibility, given general area by dead reckoning.	seconds	120.
ITMTAR	Average time necessary to estimate range and bearing of target visually detected.	seconds	30.
ITPLSA	Average time for an accurate (CEP = 60 meters) navigational fix by PPLS once A/C is on site.	seconds	120.
ITPLSQ	Average time for a "quick" navigational fix (CEP = 150 meters) by PPLS once A/C is on site.	seconds	900.
<u>MOVEMENT RATE</u>			
VTRP	Typical SIAF movement rate. (See Subroutine MVRATE)		.3 meters per second
TMR(I,J)	Movement rates for night (J=1) and day (J=2) over terrain slopes satisfying for various slope values I	km/hr	See Subroutine MVRATE

Table 3-1, Name list Inputs (Sheet 39)

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MOVEMENT RATE (Cont'd)			
<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
TMR(1,3)	Slope limits defining movement rate as a step function		See Subroutine MVRATE
VEGF(I)	Movement rate degradation factor for vegetation class I ($I = 1, \dots, 16$).		See Subroutine MVRATE
SOILF(I,J)	Movement rate degradation factor for soil type J (see Subroutine SOIL), for wet conditions ($I=1$) and dry conditions ($I=2$).		See Subroutine MVRATE
ALIM(I,J)	Night and day limits of ambient light level for a movement rate degradation (lower limit $I=1$, upper limit $I=2$, night $J=1$, day $J=2$).	ft lamberts	See Subroutine MVRATE
ALLF(I,J)	Movement rate degradation factor for night ($J=1$), and day ($J=2$) for various values ($I=1, 2, 3$; see Subroutine MVRATE) of ambient light level.		See Subroutine MVRATE
VEGC(2,II)	The speed adjustment factor for the vegetation class II (integer). (Used by target Only)		See MOVET

Table 3-1. Name list Inputs (Sheet 40)

Movement Rate (Cont'd)				
	<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
WDC		Weighting factor associated with detection for critical movement problem		
WDM		Weighting factor associated with detection for marginal movement problem		
WTC		Weighting factor associated with time for critical movement problem		
WTM		Weighting factor associated with time for marginal movement problem		
		AURAL DETECTION		
	ATTEN(J)	The attenuation coefficient for sound passing through solid growth of feature type J. This will be modified by growth density in the subroutine (1=grass, 2=brush, 3=tree trunk, 4=tree crown).	dB/meter	See Subroutine AURAL
	VEGC(4,II)	The background noise level for vegetation class II in the daytime.	dB	See Subroutine AURAL
	VEGC(5,II)	The background noise for vegetation class II in the nighttime.	dB	See Subroutine AURAL
	VEGC(6,II)	The noise generated by one man moving in vegetation class II.	dB	See Subroutine AURAL
	VEGC(7,II)	The noise generated by one man not MOVING IN VEGETATION class II.	dB	See Subroutine AURAL
	VEGC(8,II)	The incremental wind background noise for vegetation class II.	dB/knot	See Subroutine AURAL

Table 3-1, Name list Inputs (Sheet 41)

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<u>Symbol</u>	<u>DETECTION</u> (See Subroutine DETECT)	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
ANGID	Angular subtense required for identification of a target	minutes of arc		12.
CRECOG	Contrast ratio required for recognition of a target.			1.
DBACK	Distance behind target considered for background calculations.	meters		50.
TDMIN	Time interval in which detections can be considered simultaneous.	seconds		
WR	Fractional target width required to be visible for target recognition.			0.5
SECT (I,IND,1)	Sector of scan for the case of both patrols moving or both patrols stopped, where I=1 for the angular left bound for the sector of responsibility for the current sector index IND (IND=1,2,3,4), and I=2 is the angular right bound.			See DETECT
SECT (I,IND,2)	Sector of scan for the case of stationary observer and moving target where I and IND are as above. This variable is an adjustment to the scan sector due to peripheral vision being able to pick up targets at a much wider angle from forward than is nominal for a fixed target (see Subroutine DETECT).			See DETECT

Table 3-1, Name list Inputs (Sheet 42)

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<u>Symbol</u>	<u>Definition</u> (See Subroutine DETECT)	<u>Units</u>	<u>Default Value</u>
ANGID	Angular subtense required for identification of a target	minutes of arc	12.
CRECOG	Contrast ratio required for recognition of a target.		1.
DBACK	Distance behind target considered for background calculations.	meters	50.
TDMIN	Time interval in which detections can be considered simultaneous.	seconds	
WR	Fractional target width required to be visible for target recognition.		0.5
SECT (I,IND,1)	Sector of scan for the case of both patrols moving or both patrols stopped, where I=1 for the angular left bound for the sector of responsibility for the current sector index IND (IND=1, 2, 3, 4), and I=2 is the angular right bound.		See DETECT
SECT (I,IND,2)	Sector of scan for the case of stationary observer and moving target where I and IND are as above. This variable is an adjustment to the scan sector due to peripheral vision being able to pick up targets at a much wider angle from forward than is nominal for a fixed target (see Subroutine DETECT).		See DETECT

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Table 3-1, Name list Inputs (Sheet 42)

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<u>Symbol</u>	<u>Definition</u>	<u>Units</u>	<u>Default Value</u>
ISECT(J)	Sector of primary surveillance responsibility for member J of a patrol (forward sector=1, left side=2, right side=3, rear sect=r4).		1, 2, 3, 4, 1, 2
<u>WEATHER</u>			
IDTIME	Time interval preceding current time during which rain is considered to cause a current wet soil condition	hours	1.0
VISLUM(I,1)	Meteorological visibility at sea level for weather class I (see Subroutine WETHR).	meters	See Subroutine WETHR
VISLUM(I,J)	Illumination of the sky for weather class I, where J=2 for daylight; J=3 for sunrise; 4: sunset; 5: night, no moon; 6: night, quarter moon; 7: night, half moon; 8: night, full moon.	ft Lambert	See Subroutine WETHR

Table 3-1, Name list Inputs (Sheet 43)

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<u>AMMUTAB (K)</u>	<u>SUPPLY</u>	<u>Weight of ammunition for type K weapon</u>	<u>lbs/round</u>
K	<u>WEAPON</u>		
1.	M-14(SA6)	.080	
2.	M-14A1	.080	
3.	M-60MG	.080	
4.	M-16(SA)	.040	
5.	M-16(A)	.040	
6.	Stoner MG	.040	
7.	M-79 GL	.600	
8.	XM-148 RGL	.600	
9.	AK-47	.070	
10.	AK-47(A)	.070	
11.	RPD Lt. MG	.070	
12.	SGM Hvy. MG	.070	
13.	M26 A1	1.0	
14.	M18 A1	3.5	
15.	Stoner MG 1:14	.040	
16.	AAI SPIW(SA)	.029	
17.	AAI SPIW(A)	.029	
18.	AAI SPIW MG	.033	
19.	17. with 11.2 Gr Flechette	.032	
20.	0.17 Cal(A)	.037	

Table 3-1, Namelist Inputs (Sheet 44)

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<u>FOOD SUPPLY</u>	
PEQUIP	Total weight of patrol equipment carried pounds
EQUIP	Initial weight of equipment carried per man pounds
H2O	Initial amount of water carried per man pounds
RH2O	Total weight of resupply water pounds
FOOD	Initial amount of food carried per man pounds
RFOOD	Total weight of resupply food pounds
<u>WEAPON SUPPLY</u>	
SAMU(K)	Number of rounds of ammo carried by SIAF for weapon type K.
RAMU(K)	Total number of resupply ammo rounds for weapon type K.
RMINES	Number of resupply mines.
NMINES	Total number of mines carried by SIAF
RHANDG	Number of resupply hand grenades.
NHANDG	Total number of hand grenades carried by SIAF
NSWT	Number of SIAF weapon types
WTS(K)	K th SIAF weapon type

Table 3-1. Namelist Inputs (Sheet 45)

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WEAPON SUPPLY (cont.)

- 1 - M-14 (SA6)
- 2 - M-14A1
- 3 - M-60MG
- 4 - M-16 (SA)
- 5 - M-16(A)
- 6 - Stoner MG
- 7 - M-79 GL
- 8 - XM-148 RGL
- 9 - AK-47
- 10 - AK-47 (A)
- 11 - RPD Lt. MG
- 12 - SGM Hvy. MG
- 13 - M26 A1
- 14 - M18 A1
- 15 - Stoner MG 1:14
- 16 - AAI SPIW (SA)
- 17 - AAISPIW (A)
- 18 - AAI SPIW MG
- 19 - 17. with 11.2 Gr Flechette
- 20 - 0.17 Cal (A)

Table 3-1. Namelist Inputs (Sheet 46)

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COMMUNICATION

TUSE	Average external communication message duration	minutes
XDBINS	Sound level increase during attempt of external communication	dB
ICPER	Length of communications period	hours
FREQ	Transmitter frequency of the patrol radio	-
PT	Transmitter output power	mw
TPWWR	Transmission power requirements	amps
RPWWR	Reception power requirements	amps
RNF	Receiver noise figure	dB
BETA	Receiver bandwidth	Kilocycles
BLIFE	Battery life for single radio (assuming a 9:1 ratio of receiving time to transmitting time)	Hours
NBAT	Number of batteries carried per radio.	
NRAD	Total number of radios carried by SIAF	

Table 3-1, Namelist Inputs (Sheet 47)

DYNAMIC ROUTE (See Subroutine DROUTE)

IDELA	0 if point A,B,C,D, or E is to be deleted 1 if point A,B,C,D, or E is not deleted	
IDELB		
IDELC		
IDELD		
IDELF		
RAVOID	Radial distance from XAVOID. YAVOID with which all grid points are to be deleted (enter 0 if no such position).	meters
XAVOID	X coordinate of position for deletion of grid points	
YAVOID	Y coordinate of position for deletion of grid points	
RAVODD	Radial distance from XAVODD. YAVODD within which all grid points are to be deleted (enter 0 if no such position - second position).	meters
XAVODD	X coordinate of second position for deletion of grid points	
YAVODD	Y coordinate of second position for deletion of grid points	
GSAPRX	Approximate desired grid points spacing	
GSAPXX	Approximate desired spacing for second stage grid (LFL0BJ = 1, I_GRID = 1)	meters

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Table 3-1. Namelist Inputs (Sheet 48)

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Dynamic Route (Cont'd)

DSA	First significant range from enemy position XPPT, YPPT; enter only if DYWT (9,MI) ≠ 0
DSAA	First significant range from position XPPTT, YPPTT; enter only if DYWT (8,MI) ≠ 0
DMOR	Second significant range from enemy position XPPT, YPPT, enter only if DYWT (9,MI) ≠ 0
DMORR	Second significant range from position XPPTT, YPPTT; enter only if DYWT (8,MI) ≠ 0
RFSA	Risk factor associated with DSAA.
RFMOR	Risk factor associated with DMOR
RFMORR	Risk or benefit factor associated with DMORR
RFSA	Risk factor associated with DSA
NPAR	Number of parameters considered in the determination of path utility
DYWT(IPAR,MI)	Weight Factors for Assumed Missions; relative importance of parameter IPAR
MI:	Mission Situation

- 1 = Reconnaissance - detect and identify suspected enemy but avoid encounter
- 2 = Reconnaissance - avoid enemy and proceed as fast as possible
- 3 = Combat
 - avoid detection and identification by the enemy

Table 3-1, Namelist Inputs (Sheet 49)

Dynamic Route (Cont'd)

- IPAR:**
- 1 = Movement Time
 - 2 = SIAF Detects Enemy
 - 3 = SIAF identifies enemy
 - 4 = Energy detects SIAF
 - 5 = Enemy identifies SIAF
 - 6 = SIAF cover
 - 7 = SIAF Concealment
 - 8 = Distance from Energy (2) **
 - 9 = Distance from Energy (1) **

** The enemy locations can be used; however, the ninth parameter calculation refers to the same enemy position as the calculation of detection, identification, cover, and concealment.

CBDYWT (IPAR, ICB) The weight associated with parameter IPAR while movement type ICB is in progress (Same definition as DYWT above; used for combat)

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Table 3-1, Namelist Inputs (Sheet 50)

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EXTERNAL FIRE SUPPORT (for EFS Only Mission)

JNF	Total number of firings
AIRC	1 - If FFAR's are helicopter launched 0 - If FFAR's are fixed wing aircraft launched
IPREP	0 Don't use prep fire 1 Use LZ prep fire (prep fire assumed only on the primary LZ)
PL	CBU bomblet pattern length
PW	CBU bomblet pattern width
MLANG	Mean launch angle of MG firing
MLRANG	Mean launch range of MG firing
LANGLE	Launch angle of FFAR salvo
LRANGE	Launch range of FFAR salvo
MAE (i)	Lethal area of selected ammo versus personnel in posture (i)
F(i,j)	Fraction of personnel in posture (i) for each firing
TBISTR	System delay time before first round or volley is delivered after fire request
TBRNDS	System delay time between subsequent rounds/volleys

Table 3-1. Namelist Inputs (Sheet 51)

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EXTERNAL FIRE SUPPORT (cont.)

NN(J)	Number of rounds in each firing	
NROP	Number of ordnance delivery passes, GP	
NRS1P	Number of rockets launched - first pass	
NRS2P	Number of rockets launched - second and subsequent passes	
NCB1P	Number of CBU bomblets delivered, first pass	
NCB2P	Number of CBU bomblets delivered, second and all subsequent passes	
NGPB	Number of GP bombs delivered	
RPA	Artillery range probable error (also used for combat)	meters
RPECBU	CBU delivery error - range	meters
RPEGPB	GP delivery error - range	meters
DPE	Artillery deflection probable error(also used for combat)	meters
DPECBU	CBU delivery error - deflection	meters
DPEGPB	GP delivery error - deflection	meters

Table 3-1. Namelist Inputs (Sheet 52)

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**Table 3.2, Alphabetical Cross Reference
for Namelist Input Variables**

Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.
AA	38	CONCAP	31	ENRNG	7
AEQ	38	CPRAT	31	EQUIP	45
AIMMX	16	CRECOG	42	F	51
AIRC	51	C1	22	FDGFAC	18
ALIM	40	C2	22	FHCR	16
ALLB	37	DBACK	42	FHPR	16
ALLF	40	DELTA	16	FMA1	14
ALLW	37	DF	17	FMA2	14
AMWTAB	44	DMOR	49	FMCB1	14
ANGID	42	DMORR	49	FMCB2	14
ARSMN	18	DMT	33	FMGPB	14
ARSPI	18	DOMMT	2	FOOD	45
AOXMAX	35	DOMV	2	FORFTX	17
AOYMAX	35	DPE	52	FORFTY	17
ATER	38	DPECBU	52	FORMS	31
ATTAR	38	DPEGPB	52	FORMT	10
ATTEN	41	DRICE	34	FORMUX	17
BE	38	DSA	49	FORMUY	17
BETA	47	DSAA	49	FORSFX	17
BLIFE	47	DSTEP	30	FORSFY	18
BSAREA	31	DSUST	21	FORSMX	18
CADM	20	DSW11	34	FORSMY	18
CARFP	22	DSW12	34	FOTB	21
CBDYWT	50	DTDAMB	20	FOTM	21
CC1	20	DTDATT	20	FRAMB	20
CC2	20	DTEFS	16	FRATT	20
CC3	20	DTENG	20	FRCMVD	9
CLASS	20	DTPURM	20	FRCMVN	9
COLMIN	18	DWDR	22	FREQ	47
COMRES	2	DYWT	49	FTAPB	16

Table 3.2, Alphabetical Cross Reference
for Namelist Input Variables (cont.)

Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.
FWRAT	33	IFORMT	17	ITSTOP	8
GMAX	20	IFS	5	ITZERO	5
GOALTX	9	IFSUP	13	IXMAT	2
GOALTY	9	IFT	10	IX1	1
GR	38	IGBOM	13	IX2	1
GSAPRR	19	IMV	8	IYMAT	2
GSAPRX	48	IOB	3	JARTL	30
GSAPXX	48	IPERM	17	JNF	51
H	34	IPOS	30	JSTART	1
HB	35	IPREP	51	JSTOP	1
HFR	16	IPURSU	19	KDEFOP	22
HMT	35	ISECT	43	KREC	12
HLZ	7	ISEN	7	LAMDAE	33
H2O	45	ISENLZ	7	ANGLE	51
IAMG	13	ISOFF	11	LDAYS	22
ICBOM	13	ISSON	11	LGTH	29
ICL	3	ISTAY	8	LNRI	2
ICOMBF	1	ITACOS	37	LRANGE	51
ICPER	47	ITACT	13	MAE	51
IDEA1	48	ITARIV	7	MAEE	30
IDELB	48	ITDRPM	39	MAXCAS	1
IDELC	48	ITIMS	9	MAXDIS	31
IDELD	48	ITMAX	6	MAXDT	16
IDELE	48	ITMOV	8	MAXREP	1
IDET	8	ITNTA	39	MICR1	3
IDTIM	43	ITNTAR	39	MLANGL	51
IDIREC	19	ITPLSA	39	MLRANG	51
IDOMST	2	ITPLSQ	39	MODE	6
IFADJ	13	ITRC	3	NBAT	47
IFAR	13	ITST	8	NBR	29
IFORFT	17	ITSTAY	7	NCB	14

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Table 3.2, Alphabetical Cross Reference
for Namelist Input Variables (cont.)

Variable	Sheet 3.1 Sheet No.	Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.
NCB1P	52	NWCL	15	REF	35
NCB2P	52	P	32	REFS	19
NCO	3	PEQUIP	45	REQ	39
NCOPY	1	PL	51	RESMAX	2
NDECOY	6	PMC	37	RFMOR	49
NFIX	8	PMR	37	RFMORR	49
NGF	14	PO	32	RFOOD	45
NGPB	52	PPLS	4	RFSA	49
NHANDG	45	PP1	21	RFSAA	49
NLZ	6	PP2	21	RHANDG	45
NMINES	45	PP3	21	RHOH	32
NMP	9	PP4	21	RHOI	33
NN	52	PP5	21	RH20	45
NOB	2	PS	33	RLZ	6
NPAR	48	PT	47	RMAX	33
NPLAN	7	PW	51	RMINES	45
NRAD	47	Q1	21	RMTMAX	34
NRMT	2	Q2	21	RNF	47
NROP	52	Q3	21	ROBS	19
NRST	2	RAMB	19	RPA	52
NRS1P	52	RAMU	45	RPE	32
NRS2P	52	RAMIN	19	RPECBU	52
NRVP	2	RANMAX	9	RPEGPB	52
NSECT	19	RATT	19	RPG	32
NSECTR	21	RAVODD	48	RPOWR	47
NSENS	7	RAVOID	48	RSP	19
NSTP	11	RC	37	RTER	39
NSUPP	30	RCTAR	38	RZ	19
NSWT	45	RCMAX	12	SAFDIS	29
NTAR	8	RCMIN	12	SAMU	45
NVOLLEY	30	RECRES	2	SC	5

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Table 3.2, Alphabetical Cross Reference
for Namelist input Variables (cont.)

Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.	Variable	Table 3.1 Sheet No.
SCALE	4	T0	32	XBASE	5
SECT	42	T1	29	XCENT	29
SEGMIN	30	T2	29	XDBINS	47
SGMTAB	36	T3	29	XENGA	29
SGMTAW	36	UNKCON	16	XLAAW	27
SIGFFR	32	VAX	14	XLP	35
SIGMDIS	30	VEGC	35,40,41	XLZ	6
SL1	33	VEGF	40	XMAXDT	16
SL2	33	VEG1	2	XMMAX	32
SOILF	40	VELM	6	XMU	16
SOIL1	2	VELNOM	16	XOB	3
SOUNDT	11	VH	1	XPLAN	7
SPEC	4	VISLUM	43	YATT	24
SSIG	16	VISMB	36	YAVODD	48
STS	33	VISMW	36	YAVOID	48
SUFAC	21	VK	1	YBASE	5
TAK	29	VTYP	39	YCENT	29
TBRNDS	51	W	34	YENGA	29
TBUR	4	WCHAR	28	YLZ	6
TB1STR	51	WDAY	15	YOB	3
TC	9	WDC	41	YPLAN	7
TDEBK	6	WDM	41	ZATT	25
TDMIN	42	WMT	34		
THEATA	1	WPWT	18		
TMR	39	WR	42		
TPOWR	47	WTC	41		
TPREP	6	WTM	41		
TSR	15	WTS	45		
TSS	15	XATT	23		
TUSE	47	XAVODD	48		
TVEL	9	XAVOID	48		

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4.0 MODEL OUTPUTS

4.1 RECONNAISSANCE MODEL OUTPUTS

The reconnaissance model output variables are defined in Table 4-1, and are listed according to the order in which they appear in the model output format. The method used to calculate these variables is described in subroutines SISTAT and SIWRT of Volume IV.

4.2 COMBAT MODEL OUTPUTS

The combat model output variables are defined in Table 4-2. In the model, these variables are printed out during each even time thus giving the user a time history of the events which took place during the combat operation.

Table 4-1. Model Output Variables (Sheet 1)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
IVOR(IT,1)	The number of visual detections of target IT by SIAF.	
SDET SR(IT,1)	The visual detection success ratio of target IT by SIAF.	
SSTVDR(IT,1)	The mean visual detection range of target IT by SIAF.	meters
SSSTD(IT,1)	The standard deviation of the visual detection range of target IT by SIAF.	meters
SISTVD(IT,1)	Mean time of detection of target IT by SIAF.	days, hrs, min
SSISIV(1T,1)	Standard deviation of the time of detection of target IT by SIAF.	days, hrs, min
IAOR(1T)	Number of aural detection cues associated with the visual detection of target IT.	
IIVOR(1T,1)	Number of identifications of target IT by SIAF.	
SIDS R(1T,1)	Identification success ratio of target IT by SIAF.	
SSTRR(1T,1)	Mean identification range of target IT by SIAF.	meters
SSSTRR(1T,1)	Standard deviation of the identification range of target IT by SIAF.	meters
SISTR(1T,1)	Mean time of identification of target IT by SIAF	days, hrs, min
SSISTR(1T,1)	Standard deviation of the time of identification of target IT by SIAF.	days, hrs, min
IIAOR(1T,1)	Number of aural detections of target IT by SIAF.	

Table 4-1. Model Output Variables (Sheet 2)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SAURSR(IT,1)	Aural detection success ratio of target IT by SIAF.	meters
SSTADR(IT,1)	Mean aural detection range of target IT by SIAF.	meters
SSSTDAD(IT,1)	Standard deviation of the aural detection range of target IT by SIAF.	meters
SISTAD(IT,1)	Mean time of an aural detection of target IT by SIAF.	days,hrs,min
SSISTA(IT,1)	Standard deviation of the time of an aural detection of target IT by SIAF.	days,hrs,min
SCEPTA(IT)	The mean target location CEP of target IT.	meters
SSCEPT(IT)	Standard deviation of the target location CEP of target IT.	meters
IVOR(IT,2)	The number of visual detections of SIAF by target IT.	
SDETSR(IT,2)	Visual detection success ratio of SIAF by target IT.	
SSTVDR(IT,2)	Mean visual detection range of SIAF by target IT.	meters
SSSTVD(IT,2)	Standard deviation of the visual detection range of SIAF by target IT.	meters
SISTVD(IT,2)	Mean time of detection of SIAF by target IT.	days,hrs,min
SSISITV(IT,2)	Standard deviation of the time of detection of SIAF by target IT.	
IIVOR(IT,2)	Number of identifications of SIAF by target IT.	

Table 4-1. Model Output Variables (Sheet 3)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SIDSR (IT,2)	Identification success ratio of SIAF by target IT.	meters
SSTRR (IT,2)	Mean identification range of SIAF by target IT.	meters
SSSTRR (IT,2)	Standard deviation of the identification range of SIAF by target IT.	meters
SISRTT (IT,2)	Mean time of identification of SIAF by target IT.	days,hrs,min
SSISTR (IT,2)	Standard deviation of the time of identification of SIAF by target IT.	days,hrs,min
IIAOR (IT,2)	Number of aural detections of SIAF by target IT.	
SAURSR (IT,2)	Aural detection success ratio of SIAF by target IT.	
SSTADR (IT,2)	Mean aural detection range of SIAF by target IT.	meters
SSSTAD (IT,2)	Standard deviation of the aural detection range of SIAF by target IT.	meters
SISTAD (IT,2)	Mean time of an aural detection of SIAF by target IT.	days,hrs,min
SSISTA (IT,2)	Standard deviation of the time of an aural detection of SIAF by target IT.	days,hrs,min
SLSR (IT,1)	Percent of the time target IT is not detected by SIAF due to a relief intercept.	
SLOSV (IT,1)	Percent of the time target IT is not detected by SIAF due to a vegetation intercept.	

Table 4-1. Model Output Variables (Sheet 4)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SLOSD(IT,1)	Percent of the time target IT is not detected by SIAF due to insufficient range or light.	km/hr
SLOST(IT,1)	Percent of the time target IT is not detected by SIAF due to insufficient time.	km/hr
SLOSR(IT,2)	Percent of the time SIAF is not detected by target IT due to a relief intercept.	days,hrs,min
SLOSV(IT,2)	Percent of the time SIAF is not detected by target IT due to a vegetation intercept.	days,hrs,min
SLOSD(IT,2)	Percent of the time SIAF is not detected by target IT due to insufficient range or light.	km
SLOST(IT,2)	Percent of the time SIAF is not detected by target IT due to insufficient time.	km
SMVEL	Mean movement rate of the SIAF patrol.	km/hr
SSVEL	Standard deviation of the movement rate of the SIAF patrol.	km/hr
STIME	Mean patrol duration.	days,hrs,min
SSTIME	Standard deviation of the patrol duration.	days,hrs,min
SPATDI	Mean distance traveled by the SIAF patrol.	km
SSPATD	Standard deviation of the distance traveled by the SIAF patrol.	km
SYEL(1)	Patrol velocity histogram. This vector consists of 12 elements. In each element, the percent of time the patrol is moving is stored in increments of 0.2 of a kilometer per hour.	km

Table 4-1, Model Output Variables (Sheet 5)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SCEPM	The mean patrol location CEP at checkpoints.	meters
SSDCEP	Standard deviation of the patrol location CEP at checkpoints.	meters
SITNAV	Mean time for the patrol to determine its location.	minutes
SSDIT	Standard deviation of the time for the patrol to determine its location.	minutes
SATTEM	Mean number of communication attempts.	
SSATTE	Standard deviation of the number of communication attempts.	
SSUCRA	Mean communication success ratio of the patrol.	
SSSUCR	Standard deviation of the communication success ratio of the patrol.	
SAPCAD	The percent of the communication power loss due to relief for communication failures.	
SAPCAF	The percent of the communication power loss due to vegetation for communication failures.	
SAPCAS	The percent of the communication power loss due to range for communication failures.	
STTIME	The mean time the communication receiver of the patrol is on.	days,hrs,min
SSTTIM	Standard deviation of the time the communication receiver of the patrol is on.	days,hrs,min
STTUSE	The mean time the transmitter of the patrol communication equipment was on.	days,hrs,min

Table 4-1, Model Output Variables (Sheet 6)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SSTTUS	Standard deviation of the time the transmitter of the patrol communication equipment was on.	days, hrs, min
AMPHR	Ampere hours available at the beginning of the patrol.	amp hrs
SAMPHR	Mean ampere hours used by the communication equipment during the patrol.	amp hrs
SSAMPH	Standard deviation of the ampere hours used by the communication equipment during the patrol.	amp hrs
FOOD	Amount of food carried per patrol member at the beginning of the mission.	lbs/man
H2O	Amount of water carried per patrol member at the beginning of the mission.	lbs/man
XP2	Amount of ammunition carried per patrol member at the beginning of the mission.	lbs/man
XP3	Amount of ordnance other than ammunition carried per patrol member at the beginning of the mission.	lbs/man
SFOODA	Mean amount of food carried by each patrol member at the end of the patrol.	lbs/man
SSF00D	Standard deviation of the amount of food carried by each patrol member at the end of the patrol.	lbs/man
SH20A	Mean amount of water carried by each patrol member at the end of the patrol.	lbs/man
SSH20A	Standard deviation of the amount of water carried by each patrol member at the end of the patrol.	lbs/man

Table 4-1, Model Output Variables (Sheet 7)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SPAK1	Mean amount of ammunition carried by each patrol member at the end of the patrol.	lbs/man
SSPAK2	Standard deviation of the amount of ammunition carried by each patrol member at the end of the patrol.	lbs/man
SPAK3	Mean amount of ordnance other than ammunition carried by each patrol member at the end of the patrol.	lbs/man
SSPAK3	Standard deviation of amount of ordnance other than ammunition carried by each patrol member at the end of the patrol.	lbs/man
SPDEGL	The mean human performance degradation at the end of the patrol.	
SSPDEG	Standard deviation of human performance degradation at the end of the patrol.	
SPDMAX	The mean of the maximum human performance degradation experienced by the patrol during the mission.	
SSPDMA	The standard deviation of the maximum human performance degradation experienced by the patrol during the mission.	
SPDMIN	The mean of the minimum human performance degradation experienced by the patrol during the mission.	
SSPDMI	The standard deviation of the minimum human performance degradation experienced by the patrol during the mission.	
SPDAVG	The mean of the average human performance degradation experienced by the patrol during the mission.	

Table 4-1. Model Output Variables (Sheet 8)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
SSPDAV	The standard deviation of the average human performance degradation experienced by the patrol during the mission.	BTU
SSIGEN	The mean of the energy expended per patrol member at the end of the patrol.	BTU
SSIGE	The standard deviation of energy expended per patrol member at the end of the patrol.	BTU
SSGMAX	The mean of the maximum energy expended per patrol member during the mission.	BTU
SSGMMA	The standard deviation of the maximum energy expended per patrol member during the mission.	BTU
SSGMIN	The mean of the minimum energy expended per patrol member during the mission.	BTU
SSGMI	The standard deviation of the minimum energy expended per patrol member during the mission.	BTU
SSGAVG	The mean of the average energy expended per patrol member during the mission.	BTU
SSGAV	The standard deviation of the average energy expended per patrol member during the mission.	BTU
PDPLOT(1)	A vector in which is stored a time history of human performance degradation for the mission.	

Table 4-1, Model Output Variables (Sheet 9)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
HIPLOT(I)	A vector of times associated with the human performance values in PDPLOT.	
JJTIME(I)	A vector in which is stored the arrival time of SJAF at the checkpoints.	
AAALL(I)	The vector in which is stored a time history of the light level.	
KKTIME(I)	A vector of times associated with the light level data.	

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Table 4-2, Combat Outputs (Sheet 1)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
ATT(1,J,K)	Fire team number of man J; K = 1 for attackers and K = 2 for defenders.	-
ATT(2,J,K)	Weapon number of man J; K = 1 for attackers and K = 2 for defenders.	-
ATT(3,J,K)	Current ammunition supply of man J; K = 1 for attackers and K = 2 for defenders.	rounds
ATT(4,J,K)	Casualty status of man J; K = 1 for attackers and K = 2 for defenders. 0 = not a casualty; 1 = minor wound; 2 = major wound; 3 = dead.	-
ATT(5,J,K)	Firing status of man J; K = 1 for attackers and K = 2 for defenders. 0 = not firing; 1 = area fire; 2 = point fire.	-
ATT(6,J,K)	Current suppression state of man J; K = 1 for attackers and K = 2 for defenders.	-
ATT(7,J,K)	Current X coordinate of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(8,J,K)	Current Y coordinate of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(9,J,K)	Next X coordinate of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(10,J,K)	Next Y coordinate of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(11,J,K)	Height of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(12,J,K)	Width of man J; K = 1 for attackers and K = 2 for defenders	meters

Table 4-2. Combat Outputs (Sheet 2)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
ATT(13,J,K)	Current posture of man J; K = 1 for attackers and K = 2 for defenders.	meters
ATT(14,J,K)	Moving status of man J; K = 1 for attackers and K = 2 for defenders. 0 = stopped; 1 = moving normally; 2 = moving at top speed.	
ATT(15,J,K)	Maneuver unit of man J; K = 1 for attackers and K = 2 for defenders.	
ATT(16,J,K)	Number of rounds remaining in magazine of the weapon of man J; K = 1 for attackers and K = 2 for defenders.	
ATT(17,J,K)	Function of man J in the patrol; K = 1 for attackers and K = 2 for defenders. 1 = patrol leader; 2 = assistant patrol leader; 3 = machine gunner; 4 = grenadier; 5 = riflename.	meters/ seconds
ATT(18,J,K)	Movement rate of man J; K = 1 for attackers and K = 2 for defenders.	
ATT(19,J,K)	Man J's maneuver unit; K = 1 for attackers and K = 2 for defenders.	
ATT(20,J,K)	Initial ammunition supply of man J; K = 1 for attackers and K = 2 for defenders.	
ATT(21,J,K)	Man J's weapon type; K = 1 for attackers and K = 2 for defenders. 1 = point fire; 2 = area fire.	
ATT(22,J,K)	Position of man J in fire team; K = 1 for attackers and K = 2 for defenders.	
ATT(23,J,K)	Weapon number of secondary weapon carried by man J; K = 1 for attackers and K = 2 for defenders. 0 = none; 13 = hand grenade.	
ATT(24,J,K)	Supply of hand grenades for man J; K = 1 for attackers and K = 2 for defenders.	
ATT(25,J,K)	Supply of signal grenades carried by man J; K = 1 for attackers and K = 2 for defenders.	

Table 4-2, Combat Outputs (Sheet 3)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
ALPHA(J)	Orientation angle SIAF member J moves to the next point during the current time event.	radians
TIMCAS	Time of the next casualty event.	seconds
TIMDET(K)	Time of the next detection event, K = 1 for attackers, K = 2 for defenders.	seconds
IBRK(K)	0 if patrol K does not break contact; 1 if patrol K breaks contact. K = 1 for attackers and K = 2 for defenders.	
IBVAR(J,K)	K = 1 for attackers and K = 2 for defenders. J = 1,2,...,6 (defined below).	
IBVAR(1,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to lack of adequate firepower.	
IBVAR(2,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to lack of adequate ammunition.	
IBVAR(3,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to the high casualty fraction.	
IBVAR(4,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to the loss of key personnel.	
IBVAR(5,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to excessive elapsed time of the fire fight.	
IBVAR(6,K)	0 if the decision is to continue the fire fight; 1 if the decision is to break contact due to the excessively close range of the fire fight.	
IBVAR(6,1)	IBVAR(6,1) is always zero.	

Table 4-2. Combat Outputs (Sheet 4)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
IEXTR(1)	{= 0 Continue. = 1 Extract: all targets have been recognized.	
IEXTR(2)	{= 0 Continue. = 1 Extract: lack of adequate firepower.	
IEXTR(3)	{= 0 Continue. = 1 Extract: lack of adequate ammunition.	
IEXTR(4)	{= 0 Continue. = 1 Extract: high casualty fraction.	
IEXTR(5)	{= 0 Continue. = 1 Extract: inadequate food.	
IEXTR(6)	{= 0 Continue. = 1 Extract: inadequate water.	
IEXTR(7)	{= 0 Continue. = 1 Extract: time duration exceeded.	
INDCAS	Side that sustains next casualty.	
JEXTR	{= 0 Continue the mission. = 1 Extract.	
JGO	= 0 Combat decision is to avoid engagement. = 1 To conduct an EFs operation. = 2 Decision is to ambush. = 3 Decision is to attack. = 4 Decision is to deploy Claymore mines for ambush.	

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Table 4-2. Combat Outputs (Sheet 5)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
JSP	= 1 if SIAF is the subject patrol (attackers). = 2 if the target is the subject patrol.	
STIME	Time to the next movement event.	seconds
NTYPEC	Type of casualty sustained.	
NUMCAS	Number of the man sustaining the next casualty.	
SLENG(J)	Length traveled by SIAF man J during the current time event.	
TIMEFF	Elapsed time of the fight.	seconds
XYBRK	X-Y coordinates of the break point.	meters
XYDEPL	X-Y coordinates of the deployment point.	meters
XYENG	X-Y coordinates of the engagement point.	meters
XYRALY	X-Y coordinates of the rally point.	meters

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Table 4-2, Combat Outputs (Sheet 6)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
EFSTIME(L)	Time vector containing times of scheduled arrivals of external fire support burst events.	seconds
AIMPTXY	X-Y coordinates of external fire support bursts.	meters
XMINES(M)	X-Y coordinates of the deployment of the M th mine in a Claymore minefield.	meters
TMINES	Time until target arrives in Claymore minefield.	seconds
TAKOP	Target's direction of movement.	radians
ICOMFT	1 if firing is being conducted; 0 before and after firing	
MOVINF(IUN)	Movement information flag maneuver unit IUN. 0 = if a new check point is needed. 1 = if the current check point is still in effect.	
IGA(IUN)	Current check point for maneuver unit IUN.	
NGA(IUN)	Total check points for maneuver unit IUN until the next objective point.	
XYGA(I,IUN)	X-Y coordinates of check point I for maneuver unit IUN	meters
INRPA(IUN)		
IMP(A,IUN)	Current objective point for maneuver unit IUN.	

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Table 4-2, Combat Outputs (Sheet 7)

<u>Symbol</u>	<u>Definition</u>	<u>Units</u>
NARP (IUN)	Total number of objective points for maneuver unit IUN.	
XYARP(N,IUN)	X-Y coordinates of N th objective point for maneuver unit IUN.	meters
KKK	Maneuver unit that last arrived at a check point.	

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5.0 SUBROUTINES

The SIAF model subroutines are presented in Table 5-1 and a brief summary of their function is presented in Table 5-2. The elevation data handling subroutines are presented in Table 5-3. This information is provided as an overview of the SIAF model subroutines. Details concerning the purpose, description, inputs, outputs, flow chart, and programming information are presented in Volumes II, III, V, and VI.

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Table 5-1. SIAF Models and Associated Subroutines (Sheet 1)

<u>TERRAIN (RECON)</u>	<u>TARGET</u>	<u>NAVIGATION</u>	<u>COMMUNICATIONS</u>
LOSVEG	TARMOV	NAV	EXCOM
VEGCON	TARGEN		IC
MICSLOL	MOVEV	SURVEILLANCE/ DETECTION	ICGRE
MITFEA			ICMSG
MITLOS			ICLOS
MITCON			ICRAD
ELEV			ICAUR
SLOPE			
LINOBGS	CASEIN	STRACK	<u>COMMAND AND CONTROL</u>
TERCON	REPIN	VISUAL	
	RESTART	DETECT	
			PODS
		<u>SUPPLY MAINTENANCE</u>	<u>ELEVATION DATA HANDLING</u>
		LOGIS	
WETHR		INSERT	
		SEGGEN	
		TMDRVR	<u>HUMAN MAINTENANCE</u>
		MVRATE	
	LOGIS	DRROUTE	

Table 5-1. SIAF Models and Associated Subroutines (Sheet 2)

<u>DECISION LOGIC</u>	<u>OPTIMIZATION LOGIC</u>	<u>FIRE CONTROL/LETHALITY</u>	<u>COMBAT FUNCTIONS AND C²</u>
MISGEN	OLOGIC	KILL	CHAIN
CC0	OLOG4	LGTH	MOVPLN
DLOGIC	OLOG6	ARAS	MOVRV
DLOG1	OLOG7	PKBRP	FORMAT
DLOG2	OLOG8	FALOC	POSTURE
DLOG3	OLOG9	PTPTPK	DTBCFR
DLOG4	OLOG10	ARPTPK	FIRATE
DLOG5		ARPTI	AMMOUP
DLOG6		SI	FIREOP
DLOG7		PKH	WSUBS
DLOG8		SUPH	BREAK
DLOG9		NEXTC	RPT
DLOG10		PCONCL	WDR
DLOG11		PEQTN	ETERNAL FIRE SUPPORT
	EFCAS		COMMIS
			REPT
		EFS	REACT
		EFS1	CREACT
		EFSTIM	MINES
			FIRINT
			EFSMIN

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Table 5-2. SIAF Subroutines and Their Function (Sheet 1)

<u>TERRAIN</u>	
LOSVEG	- Computes line-of-sight limit due to vegetation and relief
VEGCON	- Computes vegetation concealment
MITFEA	- Determines if a target is on a micro-relief feature
MITLOS	- Computes line-of-sight limit due to micro-relief
MITCON	- Computes micro-relief concealment
ELEV	- Calculates elevation of a particular terrain coordinate
SLOPE	- Calculates slope between two points in the A0
LINOBS	- Determines if there is an obstacle, or vegetation, micro-relief, or soil polygons between two points
TERCON	- Integrates terrain subroutines into one package
MICSOL	- Determines micro-relief, vegetation, and soil type about a particular terrain coordinate
<u>WEATHER</u>	
WETHR	- Computes ambient light level, meteorological visibility, temperature, humidity, wind velocity, and rain/no rain verdict
<u>TARGET</u>	
TARMOV	- Moves targets during the insertion operation
TARGEN	- Places targets on the map
MOVET	- Moves targets in accordance with the scenario during non-insertion operations

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Table 5-2, SIAF Subroutines and Their Function (Sheet 2)

ANCILLARY AND DATA HANDLING

- | | |
|----------------|---|
| MAIN | - Provides logic to drive the SIAF model |
| CASEIN | - Converts military coordinates to computer coordinates and converts all times to seconds |
| REPIN | - Initializes subroutine variables to proper values at the start of a new replication |
| RESTART | - Provides for model execution to start and stop at preset points |

MOVEMENT

- | | |
|---------------|--|
| INSERT | - Simulates an insertion operation |
| SEGGEN | - Generates SIAF movement segment |
| TMDRVR | - Computes time interval for driving the model if the segment length is zero |
| MVRATE | - Computes nominal patrol velocity and actual velocity based upon mission and time constraints |
| DROUTE | - Computes check points for dynamic movement |

NAVIGATION

- | | |
|------------|--|
| NAV | - Computes patrol location CEP and target location CEP if detection(s) have occurred |
|------------|--|

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Table 5-2. SIAF Subroutines and Their Function (Sheet 3)

SURVEILLANCE/DETECTION

TARGET	- Eliminates infeasible targets from detection calculations
AURAL	- Determines aural detection verdict
STRACK	- Simulates special sound effects such as truck tailgate noise
VISUAL	- Determines visual detection verdict
DETECT	- Integrates detection subroutines into one package

EXTERNAL FIRE SUPPORT (EFS)

EFS	- Computes results of external fire support when EFS only mode is used
EFSI	- Simulates the effects of external fire support in combat mode
EFSTIM	- Computes the event times for external fire support bursts
EFCAS	- Determines which members sustained casualties from external fire support

SUPPLY MAINTENANCE

LOGIS	- Updates available patrol food, water, and ammunition
-------	--

HUMAN MAINTENANCE

HUMAN	- Computes required food and water depending upon work performed and computes human performance degradation due to fatigue, body water loss, and body heat storage
-------	--

Table 5-2, SIAF Subroutines and Their Function (Sheet 4)

<u>OPTIMIZATION LOGIC</u>	
OL06C	- Provides an optimum array of objective points for attacking maneuver unit routes for ambush or attack
OL064	- Assigns the nominal attack configuration based upon the tactical situation and patrol mission
OL066	- Determines whether the observed patrol configuration is linear or perimeter and - in case of linear - the axes of maximum and minimum dispersion of position
OL067	- Sets an array of trial points over which to search for an optimum deployment point for the case in which the defenders are moving to within engagement range
OL068	- Sets an array of trial points over which to search for an optimum deployment point for the case in which the defenders are moving and the attackers must move to within engagement range of the line of movement of the defenders
OL069	- Sets an array of trial points over which to search for an optimum deployment point for the case in which the defenders are stationary
OL0610	- Selects an optimum deployment point from an array of trial points set by OL067, 8, or 9

<u>COMMUNICATIONS</u>	
EXCOM	- Calculates external communications statistics and updates battery supply
IC	- Integrates the fire IC subroutines and decides whether internal communications is available between maneuver units
ICGFE	- Checks and updates the maneuver leaders supply of signal grenades
ICMSG	- Selects a messenger

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Table 5-2. SIAF Subroutines and Their Function (Sheet 5)

COMMUNICATIONS (cont.)

- | | | |
|-------|---|---|
| ICLOS | - | Determines whether line-of-sight exists between two maneuver unit leaders |
| ICRAD | - | Determines whether two maneuver units can communicate using radios |
| ICAUR | - | Determines whether a receiver can detect an aural message |

COMMAND AND CONTROL

- | | | |
|------|---|---|
| PDDS | - | Determines detection verdict(s) from the possible detection possibilities |
|------|---|---|

Table 5-2. SIAF Subroutines and Their Function (Sheet 6)

<u>TERRAIN (COMBAT)</u>	
JETERR	- Determines whether the line of sight from the observer to the observed is obstructed by macro-relief, and if it is not, computes probabilities of cover and concealment (head to head, head to foot, foot to head, and foot to foot). - Computes the probabilities of no cover and of complete cover for observer-target and target-observer.
PCOVER	- Computes the probabilities of no concealment and of complete concealment for observer-target and target-observer.
PCONCL	- Computes the probabilities of complete obstruction of observer and target and the probabilities of no obstruction of observer and target.
PEQTN	-

<u>DECISION LOGIC</u>	
MISGEN	- Coordinates combat initialization and combat execution.
CC0	- Evaluates cover, concealment, and observation of an observer's position with respect to the observed's position.
DLOGIC	- Simulates engagement-avoid decision and defines General Combat.
DLOG1	- Reads detection and identification statistics and specifies two patrols-- one to be a potential attacker and the other a potential defender.
DLOG2	- Determines whether a patrol is sufficiently remote from an enemy patrol to call for external fire support.
DLOG3	- Determines whether the latest possible deployment time would occur before sunrise or the earliest after sunset.
DLOG4	- Determines whether the relative movement of the two patrols would allow adequate time for the attacking patrol to move to deployment and then to deploy. Determines all reachable deployment points.
DLOG5	- Searches for the nearest admissible deployment point for the case of a moving enemy patrol where the enemy patrol's line of movement is not within engagement range of the attacking patrol.

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Table 5-2. SIAF Subroutines and Their Function (Sheet 7)

DECISION LOGIC (Cont'd)

- DL066 - Searches for the nearest admissible deployment point for the case of a moving enemy patrol where the enemy patrol's line of movement is within engagement range of the attacking patrol
- DL067 - Tests a trial deployment point for terrain admissibility
- DL068 - Tests a pre-deployment movement area for sufficient protectiveness
- DL069 - Evaluates protectiveness for movement at a trial point in an array over a pre-deployment movement area
- DL060 - Searches for the nearest admissible deployment point for the case of a stationary enemy patrol
- DL061 - Computes the SIAF velocity vector for SIAF on either a planned route or a dynamic route for the case in which SIAF is a potential defender

FIRE CONTROL/LETHALITY

- | | |
|--------|--|
| KILL | - Controls the operation of the remaining fire control/lethality subroutines |
| LETH | - Allocates point fire weapons, assigns area fire as appropriate
- hand grenades as appropriate |
| ARAS | - Computes the area of responsibility for each firer and computes which targets are in each area of responsibility |
| PKBRP | - Computes a figure of merit for alternative firing strategies |
| FALOC | - Computes the optimum point fire allocations for all firers in the point fire mode |
| NEXTC | - Computes casualty data for the next attacker and defender casualty |
| PTPTPK | - Computes kill probability for each firer using a rifle or machine gun |
| ARPTPK | - Computes kill probability for each firer using a grenade launcher |
| S1 | - Computes the total single shot delivery error for each weapon type |
| PKH | - Computes the probability of kill given a hit |
| SUPN | - Computes individual suppression states |

Table 5-2, SIAF Subroutines and Their Function (Sheet 8)

COMBAT FUNCTIONS AND C²

MAIN	- Provides logic to drive the combat model.
MOVPLN	- Generates dynamic route points between unit movement objective points.
MOVDRV	- Computes movement rates and movement event times.
FORMST	- Computes coordinates of individuals for various formations.
POSTURE	- Computes the posture of each individual.
FIRATE	- Computes firing rate of each individual based upon the ammunition remaining.
AMROUP	- Updates ammunition in the magazine and total ammunition remaining for each individual.
FIREOP	- Computes the firing option of each unit based upon the current suppression state of the unit.
WSUBS	- Provides logic for weapon substitution.
BREAK	- Provides logic for breaking contact.
RPT	- Computes withdrawal points for defending unit.
WDR	- Computes withdrawal points for attacking unit.
COMMIS	- Computes a continue the mission decision for SIAF after the combat operation has been completed.
REACT	- Provides six defender reaction options after detection but before fire-fight
CREATECT	- Permits attacking unit to revise its plan before attack is initiated
MINES	- Provides for a Claymore Mine ambush
FIRIHT	- Initiates fire-fight between an attacking and a defending unit
EFSMIN	- Updates the EFS event times

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Table 5-3. SIAF Elevation Data Handling (Sheet 1)

ELEVATION DATA HANDLING

CONVERT	- Produces FORTRAN - compatible tapes from Defense Mapping Agency (TOPOCOM) Digital Topographic Tapes
MAPGEN	- Selects and/or thins terrain elevation data for the area of operation
ROTATES	- Provides for rotation and change of interval distance between elevation points at a map area output from MAPGEN
CMREAD	- Loads a selected section of the available map area into computer memory
REREAD	- Condenses the input area elevations in computer memory

6.0 SAMPLE CASE

Sections 6.1 through 6.4 describe a test case which illustrates the use of the reconnaissance model while Sections 6.5 and 6.6 present a combat model test case.

As part of the SIAF program, a model verification plan was developed and a test using actual patrols was conducted. Concurrent with the test, the SIAF System Model was exercised for the purpose of simulation, this test and providing data for comparison purposes. This section presents a sample case based upon the test scenario. Included is a qualitative description of the test, a description of the model input data consisting of terrain, weather, the SIAF operations plan, and the enemy situation, and a description of the outputs of the model.

6.1 QUALITATIVE DESCRIPTION OF THE TEST PROGRAM

The field test was conducted at the Hunter Liggett Military Reservation located near King City, California, a facility of the Combat Developments Command Experimentation Command headquartered at Fort Ord, California (Monterey). The test exercise was conducted in a relatively rugged and remote valley which is also a part of Los Padres National Forest. Figure 6.1 is a photograph of a map of the area of operations which represents a geographic area of approximately 17 square kilometers. The patrol mission-scenario (including an aggressor scenario) was developed by the test conductor employing inputs from the test team members. The mission was basically one of reconnaissance which consisted of surveillance of a road suspected of being an enemy supply route, by a SIAF patrol moving primarily at night along the high ground on one side of the valley. Combat was not entered or simulated and live ammunition was not carried.

As shown by Figure 6.1, the distance between the projected insertion and extraction points is approximately 6-1/4 kilometers; however, the route between checkpoints and projected patrol bases is not a straight line nor did the patrols follow a simple point-to-point route. The actual route traveled by each patrol was approximately 9 kilometers long.

Each patrol spent two days in an objective area near the center of the route. This area contained several OP's and bases among which the patrol moved. Aggressor activity existed in the area, some of which was along the roads. For experimental purposes, this area was instrumented to determine exact positions and ranges of detection between the SIAF patrols and the aggressor.



Figure 6.1, SIAF Area of Operations
Showing Patrol Checkpoints

The 5 1/2 day mission was performed by each of 20 patrol teams provided by the 3 participating services:

Army Special Forces	10 teams
U. S. Marine Corps	5 teams
U. S. Navy Seals	5 teams

Each six-man SIAF patrol team was given the same mission, checkpoints, and basing areas, and was exposed to the same aggressor scenario. Patrols moved primarily at night. During the day the patrols established bases from which they monitored the primary road or conducted related reconnaissance and surveillance activities. The sample case described herein (referenced as scenario 1) treats only the first of these patrol missions.

6.2 GENERATION OF BINARY TAPE 8

As described in Section 3.0, Binary Tape 8 is generated from card input. Because of the requirement to duplicate the test situation as closely as possible, detailed terrain and vegetation data were first gathered. This section describes that task.

As previously described in Section 2 4.1, the terrain resolution study for the Hunter Liggett area indicated a substantial increase in accuracy with 50-meter resolution as compared with that obtained for 100-meter resolution. Since the objective of the Hunter Liggett test was to validate the SIAF model, it was considered necessary to use 50-meter resolution. Since the only available digitized data were 100-meter resolution, a decision was made to input the elevation data for the area of operations shown in Figure 6.1 by hand. For this purpose, the map shown in Figure 6.1 was enlarged and a 50-meter grid was overlayed on the map. Then elevation data associated with each corner point of the grid were recorded on computer input sheets. The resulting 7,105 points took approximately two weeks to record. A namelist printout of these resulting data is shown in Figure 6.2. These data, which were used to generate Binary Tape 8, are in feet since the map used for this purpose (Reference 3) contained elevation information in these units. Data were subsequently converted to meters in the computer program.

It should be pointed out that Army digitized terrain tapes of various areas of the world exist. These tapes obviate the necessity of inputting

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Figure 6.2, Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 1)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 2)

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Figure 6.2. NameList Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 3)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 4)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 5)

Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 6)

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Figure 6.2. NameList Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 7)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation(V) Data (Sheet 8)

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Figure 6.2. NameList Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 9)

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Figure 6.2, Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 10)

1140,	1160,	1180,	1200,	1210,	1300,	1350,	1450,	1400,	1380,
1360,	1400,	1400,	1200,	1200,	1300,	1220,	1170,	1150,	1150,
1880,	1840,	1600,	1230,	1230,	1210,	1160,	1160,	1460,	1400,
1350,	1280,	1190,	1160,	1150,	1150,	1140,	1140,	1140,	1200,
1200,	1190,	1160,	1150,	1220,	1300,	1400,	1420,	1400,	1140,
1150,	1160,	1150,	1220,	1400,	1400,	1400,	1420,	1440,	1370,
1360,	1400,	1400,	1400,	1400,	1400,	1300,	1300,	1260,	1260,
1860,	1780,	1760,	1760,	1720,	1630,	1550,	1510,	1450,	1400,
1360,	1320,	1300,	1200,	1200,	1200,	1200,	1160,	1220,	1220,
1390,	1360,	1320,	1200,	1200,	1200,	1200,	1240,	1280,	1260,
1180,	1180,	1160,	1150,	1150,	1140,	1140,	1140,	1140,	1140,
1140,	1160,	1160,	1180,	1220,	1300,	1360,	1400,	1380,	1360,
1360,	1380,	1400,	1400,	1400,	1400,	1300,	1220,	1270,	1400,
1840,	1780,	1720,	1670,	1650,	1600,	1540,	1460,	1440,	1380,
1350,	1360,	1400,	1400,	1400,	1400,	1400,	1400,	1400,	1220,
1780,	1780,	1720,	1640,	1640,	1600,	1570,	1530,	1500,	1440,
1400,	1360,	1340,	1270,	1270,	1200,	1200,	1180,	1220,	1200,
1180,	1200,	1160,	1160,	1160,	1160,	1160,	1160,	1160,	1340,
1140,	1160,	1180,	1200,	1200,	1300,	1340,	1320,	1320,	1320,
1340,	1360,	1380,	1400,	1400,	1380,	1380,	1300,	1250,	1260,
1710,	1780,	1730,	1730,	1650,	1650,	1570,	1520,	1490,	1410,
1380,	1360,	1320,	1280,	1280,	1240,	1200,	1200,	1240,	1240,
1210,	1160,	1160,	1160,	1160,	1160,	1160,	1160,	1140,	1140,
1140,	1140,	1180,	1180,	1220,	1220,	1280,	1350,	1380,	1320,
1350,	1370,	1400,	1400,	1400,	1400,	1310,	1240,	1200,	1140,
1680,	1720,	1740,	1660,	1660,	1600,	1560,	1500,	1460,	1390,
1400,	1400,	1370,	1340,	1340,	1290,	1230,	1200,	1240,	1240,
1220,	1160,	1160,	1170,	1170,	1160,	1160,	1160,	1160,	1160,
1160,	1160,	1200,	1230,	1230,	1300,	1320,	1350,	1360,	1300,
1320,	1340,	1360,	1400,	1400,	1360,	1320,	1200,	1120,	1120,
1720,	1700,	1660,	1610,	1610,	1600,	1540,	1480,	1400,	1420,
1440,	1400,	1380,	1370,	1370,	1290,	1220,	1230,	1260,	1260,
1460,	1420,	1370,	1350,	1200,	1160,	1160,	1160,	1260,	1240,
1220,	1210,	1180,	1200,	1200,	1180,	1180,	1160,	1160,	1160,
1170,	1180,	1200,	1230,	1230,	1280,	1340,	1320,	1300,	1310,
1320,	1340,	1360,	1400,	1400,	1300,	1240,	1180,	1160,	1100,

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Figure 6.2. Marxist Printout of Sample Case Elevation (Z) and Vegetation (Y) Data (Sheet 11)

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Figure 6.2. Nautical Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 12)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 13)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 14)

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Figure 6.2. Hemelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 15).

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Figure 6.2. Nautical Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 16)

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Figure 6.2. Hemelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 17)

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Figure 6.2. NameList Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 18)

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Figure 6.2, Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 19)

1700., 1660., 1740., 1760., 1520., 1700., 1520., 1560., 2*1580.	1640., 1620., 1530., 1700., 1550., 1630., 1630., 1350.	1265., 1290., 1300., 1240., 1200., 1200., 1620., 241000.	1560., 1540., 1510., 1450., 1450., 1450., 2*1300., 1200.	3*2120., 1810., 1770., 1680., 1640., 2*1600., 1620., 2140., 2050., 1980.	1380., 1810., 1770., 1680., 1640., 2*1600., 1620., 1600., 1630., 1660.	4*1660., 1275., 1260., 1340., 1420., 1450., 1560., 1530., 1450., 1550.	2*1550., 1500., 1420., 1540., 1270., 1260., 1240., 1170., 1170.	3*2150., 2*2100., 2200., 2240., 2140., 2040., 1960.	1880., 1820., 1770., 1750., 1650., 1620., 1540., 1660., 1680., 1720.	**1720., 1740., 1720., 1680., 1630., 1580., 1510., 1420., 1340.	1280., 1250., 1330., 1380., 1340., 1460., 1500., 1430., 1480., 1550.	1480., 1520., 1450., 1380., 1320., 1260., 1200., 1180., 1160., 1160.	2*2150., 2100., 2150., 2160., 2200., 2220., 2100., 2040., 1960.	1860., 1840., 1810., 1770., 1680., 1620., 1690., 1700., 1730., 1750.	3*1800., 1280., 1440., 2*1300., 1400., 1330., 1230., 1240., 1430., 1400., 1440., 1420.	1440., 1460., 1460., 2140., 2200., 2230., 2260., 2220., 2100., 2020., 1960.	1940., 1470., 1800., 1770., 1720., 1630., 1700., 1760., 1780., 1800.	1820., 1840., 1815., 1750., 1670., 1630., 1520., 1460., 1400., 1330.	1300., 1240., 1240., 1260., 1290., 1360., 1420., 1380., 1300., 1370.	2*1400., 1330., 1260., 1260., 1240., 1220., 1200., 1160., 1140.	3*2140., 2220., 2*2260., 2180., 2100., 2020., 1970.	1980., 1900., 1860., 1820., 1810., 1750., 1700., 1790., 2*1840.	1880., 1440., 1860., 1800., 1720., 1600., 1570., 1520., 1470., 1400.	1290., 1260., 1240., 1290., 2*1320., 1350., 1280., 1300., 1330.	1340., 1340., 1320., 2*1760., 1230., 1190., 1160., 1140.	3*2160., 2210., 2240., 2260., 2160., 2060., 2000., 1960.	1900., 1880., 1850., 1830., 1810., 1740., 1780., 1840., 1900., 1900.	1820., 1770., 1730., 1630., 1620., 1540., 1460., 1380., 1330., 1295.	1260., 1220., 1270., 1300., 1240., 1260., 1240., 2*1260., 1170., 1170.	1280., 3*1400., 1240., 1240., 1240., 1150., 1150., 1160., 1160., 1170.	4*2200., 2260., 2200., 2160., 2050., 1980., 1940., 1900., 1940., 1900.	1940., 1900., 1860., 3*1800., 1690., 1580., 1500., 1440., 1400., 1360., 1360., 1300.	2*1800., 1760., 1690., 1580., 1500., 1440., 1400., 1360., 1360., 1300.	1280., 1265., 1240., 4*1200., 1200., 1150., 1150., 1160., 1170.	1260., 3*1300., 1300., 1300., 1280., 2220., 2100., 2040., 2030., 2000.	4*2240., 2280., 2220., 2100., 2040., 2040., 2030., 2000.	2000., 1950., 1860., 1800., 1920., 2*1900., 1960., 1940., 1880.	1760., 1460., 2*1760., 1600., 1530., 1450., 1400., 1400., 1380., 1360.
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Figure 6.2. Namelist Printout of Simple Case Elevation (Z) and Vegetation (V) Data (Sheet 20)

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Figure 6.2. Namelist Printout of Sample Case Elevation (Z) and Vegetation (V) Data (Sheet 21)

terrain data by hand as was done for this sample case, and normal use of the model for various SIAF studies would probably not require as extensive an effort as was undertaken for this project.

As with relief, considerably more effort than normally required was taken to input vegetation data since the objective of the simulation was to duplicate as best as possible the test situation. As described in Section 2.4.1, a vegetation survey of the Hunter Liggett area was conducted for the purpose of obtaining input data for this simulation. During this survey, aerial photographs of the area were obtained, a ground survey was conducted, and the vegetation in the area was categorized according to the classification scheme shown in Figure 2.7. From this information, the vegetation data for the 50-meter grid square resolution were recorded on computer input sheets. The last part of Figure 6.2 shows namelist printout of these data from which Tape 8 was generated. Because of the difficulties of correlating the aerial photograph with the map, this exercise took approximately three weeks; however, normal use of the model would require a far less extensive effort. In fact, with the aid of the namelist input the vegetation of the entire area could be input with one card if the user desired to specify a constant vegetation class for the area.

6.3 USER INPUT AND DATA BASE

Values corresponding to the variables of Tables 3-1 and 3-2 are presented in Figure 6.3. The data base in NAML1 consists of the first three pages of this Figure. The user inputs with the exception of the target data are in NAML2 which starts on the third page of Figure 6.3, while the target data (NAML3) starts on the seventh page of Figure 6.3. The user input for the sample case has been organized alphabetically so there is a one-to-one correspondence between this sample case and the inputs described in Section 3.0.

In order to exercise the dynamic route and external fire support options of the model, this sample case was organized as follows: For targets 1 and 2, the decision rule used was for SIAF to move toward these targets in an attempt to identify them. Once targets were identified, external fire support was to be called on the targets. For targets 3 and 4, the decision rule was to avoid these targets, if detected, by moving around them. For

Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 1)

LINIAN	=	3.0
ITPLSA	=	3.0
IPLESQ	=	1.023
LAMUAE	=	1.0670.
NPAN=30		
P	=	79.30.
PNC	=	25.0
PNK	=	25.0
PQ	=	79.30.
PS	=	42.0
RK	=	4.0
RC TAK	=	10.0
RREF	=	0.3
REU	=	0.0
RHULL	=	0.0
RNGL	=	0.0
RMAX	=	100.0
RMIN	=	100.0
RMINMAX	=	2.0
RPE	=	0.44
RPG	=	0.5
RTER	=	0.1
SECT	=	2.0000.
SEGMIN	=	1.1
SIGNAO	=	0.0
SUMTAN	=	2.00.
SIGFTK	=	0.00302.
SLI:	=	0.0005.
SLC	=	0.05.
SOLIF	=	0.8
SPS	=	95.0
T0	=	5.000
TAD	=	0.1

1000-0000-00-00

Page 1

Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 2)

VUL	=	15.0	1.0	3.0	3.500	10.00	0.00	1.00	0.005	3.0	33.0	20.0
		20.0	31.0	6.5	20.00	32.0	0.00	32.0	1.00	2.0	30.0	20.0
		6.0	9.7	3.0	31.0	20.0	37.0	32.0	0.21	2.0	0.90	2.0
		33.0	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2
		2.0	1	0.32	1.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		4.3	0	2.0	1	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		7.5	0	0.7	2.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		2.0	0	2.0	0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		1.0	0.20	2.0	2.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		2.0	0	2.0	0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		1.5	0	0.32	1.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		2.0	0	2.0	0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		2.0	0	2.0	0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		2.0	0	0.32	1.0	2.0	0.0	2.0	0.0	0.0	0.0	0.0
		6.0	0	4.5	0	6.0	0.0	6.0	0.0	0.0	0.0	0.0
		2.0	0	0.92	1.0	4.0	0.0	4.0	0.0	0.0	0.0	0.0
		35.0	0	0.16	0.0	34.0	0.0	34.0	0.0	0.0	0.0	0.0
YEUR	=	1.0	0.35	0.7	0.4	0.92	0.0	0.7	0.62	1.0	0.20	1.0
		0.3	0.2	0.2	0.2	0.2	0.0	0.2	0.0	0.3	0.2	0.2
VISLUM	=	49000.0	15000.0	13000.0	10000.0	2000.0	500.0	300.0	50.0	0.0	0.0	0.0
		10000.0	5000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0	1000.0
		2.0	4.0	1.0	1.0	0.1	0.1	0.1	0.1	0.1	0.1	0.1
		2.0	0.001	0	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002
		2.0	0	0.01	0	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005	0.0005
		2.0	0	0.004	0	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002	0.0002
		2.0	0	0.008	0	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
VISMU	=	13.0	0	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002
VISHA	=	20.0	0.1	0	0	0	0	0	0	0	0	0
		W	=	1.0	0.0	1.0	0.0	1.0	0.0	1.0	0.0	1.0
		4*	0.0	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		4*	0.0	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		4*	0.0	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		4*	0.0	3.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		ALP	=	3.0	1.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
				0.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0	0.0
		6ENU										

LOGICAL
BETA = 40.0
BLIFE = 100.0
DMUX = 0.0
DMUXT = 1.0

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Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 3)

Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 3)

Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 4)

CMDIT = 1,
DPE = 100.,
Y2A=Y2A
USMA=U0.0

EJUIP = 0.,
EshNu = 2.0.

F = 1.0,
FUDU = 13.47,

FUMMS=2.280.,
FUKMT=2.140*0.0

FATU = 50.0,
G3APRX=20.0

G3APXX=200.0

HL2=3600.0

H2U = 36.991,

ICPER = 3000,

IUTLA=1,
IUTLD=1,

IDELC=1,
IUELD=1,

IDLEL=1,
IUMST = 3,

IPADJ = 1.1,49**0,

IPS=0,
IFSUP = 5101,

IFT=51*01,

IPJS = 1,
IPKEP = 0.,

ISLEN = 24H
IIS = 4H

ISEN = 0.,

ISENL2=0,

ISTAY = 01,2231,7,5031,7,2931,31021,91,1,31021,91,3,1,203,6,232,10,0,

ISTAY(1,01) = 03,1,131417,1,1 = 2*3, 131417,1,1 = 3,

ISTAY(2,11) = 3,1,131417,1,1 = 200,

ITAI = 1,3*2,47*1,

ITAKIV = 01170000,2*0,01220000,2*0,02220000,2*0,03030000,

2*0,03220000,03220115,290,032*0000,04000000,04220000,

0422C115,2900,04240000,0,05060000,06020000,06060000,06060000,2*0,

06060000,0,0

ITMAX = 64002155,

ITNUV(1,01) = 01170000,2*0,01220000,2*0,02220000,2*0,03030000,

33140000,2*0,03220000,03220115,290,04040000,04210000,

04220000,04220115,290,05040000,0,05190000,06020000,

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NAMELIST PRINTOUT OF SAMPLE CASE USER INPUT (SHEET 5)	
ITM	= 1
ITM1	= 1
ITM2	= 1
ITM3	= 1
ITM4	= 1
ITM5	= 1
ITM6	= 1
ITM7	= 1
ITM8	= 1
ITM9	= 1
ITM10	= 1
ITM11	= 1
ITM12	= 1
ITM13	= 1
ITM14	= 1
ITM15	= 1
ITM16	= 1
ITM17	= 1
ITM18	= 1
ITM19	= 1
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ITM506	= 1
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ITM508	= 1
ITM509	= 1
ITM510	= 1

Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 6)

Figure 6.3, Memelist Printout of Sample Case User Input (Sheet 7)

Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 9)

Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 11)

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Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 12)

```

    INV(25)= 0.000000000000000E+000  FCMVN(25)= 7442.0  7443.0  7444.0  7445.0
    FCMVN(25)= 7446.0  7447.0  7448.0  7449.0
    FCMVN(25)= 7450.0  7451.0  7452.0  7453.0
    FCMVN(25)= 7454.0  7455.0  7456.0  7457.0
    FCMVN(25)= 7458.0  7459.0  7460.0  7461.0
    FCMVN(25)= 7462.0  7463.0  7464.0  7465.0
    FCMVN(25)= 7466.0  7467.0  7468.0  7469.0
    FCMVN(25)= 7470.0  7471.0  7472.0  7473.0
    FCMVN(25)= 7474.0  7475.0  7476.0  7477.0
    FCMVN(25)= 7478.0  7479.0  7480.0  7481.0
    FCMVN(25)= 7482.0  7483.0  7484.0  7485.0
    FCMVN(25)= 7486.0  7487.0  7488.0  7489.0
    FCMVN(25)= 7490.0  7491.0  7492.0  7493.0
    FCMVN(25)= 7494.0  7495.0  7496.0  7497.0
    FCMVN(25)= 7498.0  7499.0  7500.0  7501.0
    FCMVN(25)= 7502.0  7503.0  7504.0  7505.0
    FCMVN(25)= 7506.0  7507.0  7508.0  7509.0
    FCMVN(25)= 7510.0  7511.0  7512.0  7513.0
    FCMVN(25)= 7514.0  7515.0  7516.0  7517.0
    FCMVN(25)= 7518.0  7519.0  7520.0  7521.0
    FCMVN(25)= 7522.0  7523.0  7524.0  7525.0
    FCMVN(25)= 7526.0  7527.0  7528.0  7529.0
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    FCMVN(25)= 7534.0  7535.0  7536.0  7537.0
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Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 13)

Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 14)

Figure 6.3. Numblist Printout of Sample Case User Input (Sheet 15)

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Figure 6.3, Namelist Printout of Sample Case User Input (Sheet 16)

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Figure 6.3. Namelist Printout of Sample Case User Input (Sheet 17)

targets 5 through 51, no dynamic movement was used. Instead, once detected, these targets were removed from the simulation and subsequent identification was not attempted.

6.4 MODEL INPUTS

The outputs of the model consist of detail and summary printout. Detail printout presented in Figure 6.4 begins with some target transformations and then shows the X and Y coordinates of the SIAF location, the target currently being considered under the dynamic route option, and the current time in seconds. The second page of Figure 6.4, for example, indicates that IDTAR equals zero. Thus, there are no targets currently being considered for the dynamic route option at the simulation time shown. The third page of Figure 6.4 indicates that the dynamic route option was taken by the patrol at the time shown. Subsequent printout reveals that the patrol was moving toward the first target in an attempt to identify it. Finally, the fifth page of Figure 6.4 shows the result of an external fire support mission which was called on target number 2 and later on target number 1. This detail printout continues and presents a time history of a portion of the operation by showing when a dynamic route is used, the results of the external fire support missions, and the location of the patrol throughout the entire mission.

Summary printout of the simulation of the mission for all 51 targets is presented in Figure 6.5. Table 6-1 presents a brief description of these targets. For this summary printout, the dynamic route option described above was not used; hence, KREC(IT) was set equal to zero for all targets.

Included in Figure 6.5 are statistics pertaining to visual detection, target identification, aural detection, target location, movement, navigation, communications, supply maintenance, and human maintenance. As an example of the correlation of these results with the physical situation, Figures 6.6 and 6.7 are presented. Figure 6.6 shows the first six targets in the vicinity of the star cluster turn while Figure 6.7 shows the time line diagram associated with these targets.

A study of these Figures and Page 1 of the output data of Figure 6.5 reveals that for 5 replications, targets 1 through 3 were never visually detected by SIAF while targets 4 through 6 were always detected. Page 37

of the output reveals that the reasons for no detection on target 1 were primarily due to vegetation while targets 2 and 3 were always masked by relief. The aural detection statistics of Page 10 of Figure 6.5 indicate that targets 1, 2, and 5 were always detected by SIAF while target 4 (8 personnel) was not. Aural detection of targets 3 and 6 was not feasible.

With respect to detections of SIAF. Page 19 of Figure 6.5 indicates that target 4 (8 personnel) visually detected SIAF once in 5 replications while Page 28 reveals no aural detections of SIAF by the enemy.

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Figure 6.4, Detailed Computer Output (Sheet 1)

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Figure 6.4, Detailed Computer Output (Sheet 2)

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Figure 6.4, Detailed Computer Output (Sheet 3)

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Figure 6.4. Detailed Computer Output (Sheet 4)

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Figure 6.4, Detailed Computer Output (Sheet 5)

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Figure 6.4, Detailed Computer Output (Sheet 6)

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Figure 6.4, Detailed Computer Output (Sheet 7)

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Figure 6.4, Detailed Computer Output (Sheet 8)

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Figure 6.4. Detailed Computer Output (Sheet 9)

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Figure 6.4, Detailed Computer Output (Sheet 10)

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Figure 6.4, Detailed Computer Output (Sheet 11)

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Figure 6.4. Detailed Computer Output (Sheet 12)

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Figure 6.4, Detailed Computer Output (Sheet 13)

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Figure 6.4, Detailed Computer Output (Sheet 14)

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Figure 6.4, Detailed Computer Output (Sheet 15)

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Figure 6.4, Detailed Computer Output (Sheet 16)

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Figure 6.4, Detailed Computer Output (Sheet 17)

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Figure 6.4. Detailed Computer Output (Sheet 18)

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Figure 6.4, Detailed Computer Output (Sheet 19)

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Page 6-63

Figure 6.4. Detailed Computer Output (Sheet 20)

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Page 6-64

Figure 6.4, Detailed Computer Output (Sheet 21)

16905-6003-94-00

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Figure 6.4, Detailed Computer Output (Sheet 22)

1995-0002-20-00

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Figure 6.4, Detailed Computer Output (Sheet 23)

10000-0000-10-00

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Figure 6.4, Detailed Computer Output (Sheet 24)

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Figure 6.4, Detailed Computer Output (Sheet 25)

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Figure 6.4, Detailed Computer Output (Sheet 26)

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XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	455448
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	453468
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	423229
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	45576
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	455200
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	453091
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	453724
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	453981
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	424362
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	457103
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	457201
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	45704
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	429362
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	429966
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	45732
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	457923
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	45724
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	459125
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	457720
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	463327
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	480901
XSIAF, YSIAF, IOTAK, ITIME	883.023	3907.076	0	465032
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	462633
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	463461
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	46432
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	465233
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	46001
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	463632
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	463033
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	47101
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	471632
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	473433
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	475201
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	47532
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	477123
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	475501
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	482401
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	482522
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	484323
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	465001
XSIAF, YSIAF, IUTAK, ITIME	883.023	3907.076	0	469601

Figure 6.4, Detailed Computer Output (Sheet 27)

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Figure 6.4. Detailed Computer Output (Sheet 28)

Figure 6.4, Detailed Computer Output (Sheet 29)

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XSTAR, YSTAR, JULAN, 01, 01	675.336	461.0.473	2	22901
XSTAR, YSTAR, JULAN, 01, 01	676.336	461.0.473	2	22902
XSTAR, YSTAR, JULAN, 01, 01	673.476	469.3.373	2	22903
XSTAR, YSTAR, JULAN, 01, 01	672.136	469.3.373	0	22904
XSTAR, YSTAR, JULAN, 01, 01	672.326	469.3.373	0	22905
XSTAR, YSTAR, JULAN, 01, 01	672.326	469.2.372	0	22906
XSTAR, YSTAR, JULAN, 01, 01	671.596	469.3.373	0	22907
XSTAR, YSTAR, JULAN, 01, 01	671.596	469.3.373	0	22908
XSTAR, YSTAR, JULAN, 01, 01	670.136	469.3.373	0	22909
XSTAR, YSTAR, JULAN, 01, 01	669.136	469.3.373	0	22910
XSTAR, YSTAR, JULAN, 01, 01	669.136	469.3.373	0	22911
XSTAR, YSTAR, JULAN, 01, 01	667.326	469.3.373	0	22912
XSTAR, YSTAR, JULAN, 01, 01	667.326	469.3.373	0	22913
XSTAR, YSTAR, JULAN, 01, 01	666.136	469.3.373	0	22914
XSTAR, YSTAR, JULAN, 01, 01	666.136	469.3.373	0	22915
XSTAR, YSTAR, JULAN, 01, 01	665.136	469.3.373	0	22916
XSTAR, YSTAR, JULAN, 01, 01	665.136	469.3.373	0	22917
XSTAR, YSTAR, JULAN, 01, 01	663.716	469.3.373	0	22918
XSTAR, YSTAR, JULAN, 01, 01	663.716	469.3.373	0	22919
XSTAR, YSTAR, JULAN, 01, 01	662.136	469.3.373	0	22920
XSTAR, YSTAR, JULAN, 01, 01	662.136	469.3.373	0	22921
XSTAR, YSTAR, JULAN, 01, 01	660.136	469.3.373	0	22922
XSTAR, YSTAR, JULAN, 01, 01	660.136	469.3.373	0	22923
XSTAR, YSTAR, JULAN, 01, 01	659.136	469.3.373	0	22924
XSTAR, YSTAR, JULAN, 01, 01	658.136	469.3.373	0	22925
XSTAR, YSTAR, JULAN, 01, 01	656.136	469.3.373	0	22926
XSTAR, YSTAR, JULAN, 01, 01	656.136	469.3.373	0	22927
XSTAR, YSTAR, JULAN, 01, 01	655.136	469.3.373	0	22928
XSTAR, YSTAR, JULAN, 01, 01	653.716	469.3.373	0	22929
XSTAR, YSTAR, JULAN, 01, 01	653.716	469.3.373	0	22930
XSTAR, YSTAR, JULAN, 01, 01	652.136	469.3.373	0	22931
XSTAR, YSTAR, JULAN, 01, 01	652.136	469.3.373	0	22932
XSTAR, YSTAR, JULAN, 01, 01	650.136	469.3.373	0	22933
XSTAR, YSTAR, JULAN, 01, 01	649.136	469.3.373	0	22934
XSTAR, YSTAR, JULAN, 01, 01	648.136	469.3.373	0	22935
XSTAR, YSTAR, JULAN, 01, 01	647.136	469.3.373	0	22936
XSTAR, YSTAR, JULAN, 01, 01	646.136	469.3.373	0	22937
XSTAR, YSTAR, JULAN, 01, 01	645.136	469.3.373	0	22938
XSTAR, YSTAR, JULAN, 01, 01	644.136	469.3.373	0	22939
XSTAR, YSTAR, JULAN, 01, 01	643.716	469.3.373	0	22940
XSTAR, YSTAR, JULAN, 01, 01	643.716	469.3.373	0	22941
XSTAR, YSTAR, JULAN, 01, 01	642.136	469.3.373	0	22942
XSTAR, YSTAR, JULAN, 01, 01	641.136	469.3.373	0	22943
XSTAR, YSTAR, JULAN, 01, 01	640.136	469.3.373	0	22944

Figure 6.4, Detailed Computer Output (Sheet 30)

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Figure 6.4, Detailed Computer Output (Sheet 31)

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Figure 6.4, Detailed Computer Output (Sheet 32)

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Figure 6.4. Detailed Computer Output (Sheet 33)

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Figure 6.4, Detailed Computer Output (Sheet 34)

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Figure 6.4. Detailed Computer Output (Sheet 35)

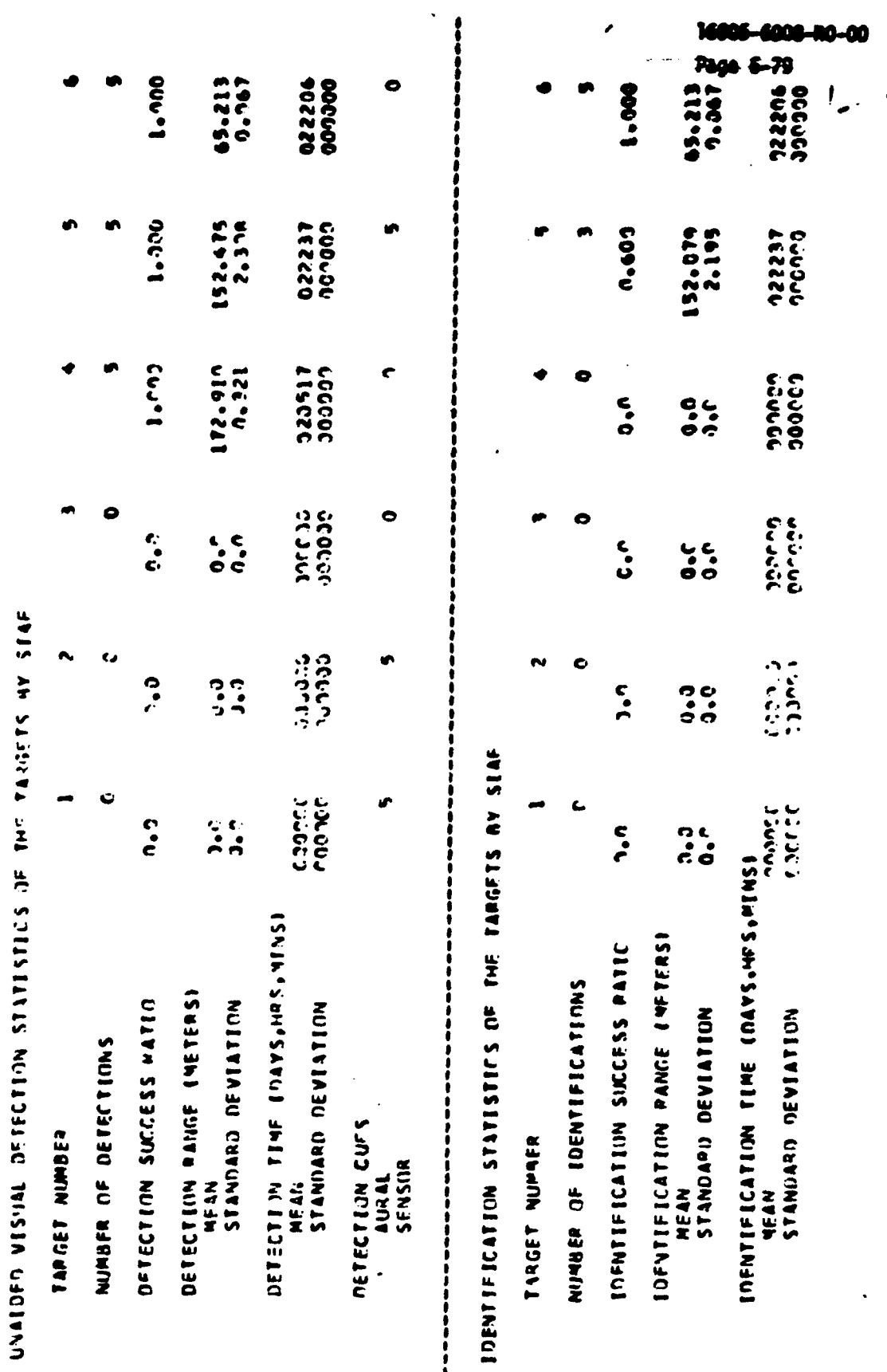


Figure 6.5. SAE specifies several areas of safety in addition to the main areas of safety.

INVENTIFICATION STATISTICS OF THE INVENTORS BY SIAF

CHILD VISUAL DEFECTS AND STATISTICS OF THE TARGETS IN SIAE

Figure 6.5. SIGHT SURVEILLANCE STATISTICS (PAGE 2)
HUNTING LIGHTER SCENARIOS

Figure 6.5. SIAF SURVEILLANCE STATISTICS (PAGE 3)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	13	14	15	16	17	18
NUMBER OF DETECTIONS	0	0	0	0	0	0
DETECTION SUCCESS RATIO	0.0	0.0	0.000	0.0	0.0	0.000
DETECTION RANGE (METERS)						
MEAN	0.0	1C39.449	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.626	0.0	0.0	0.0	0.023
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
STANDARD DEVIATION	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
DETECTION CUES						
AURAL	0	5	0	0	5	0
SENSOR						

IDENTIFICATION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	13	14	15	16	17	18
NUMBER OF IDENTIFICATIONS	0	0	0	0	0	0
IDENTIFICATION SUCCESS RATIO	0.0	0.011	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)						
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)						
MEAN	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
STANDARD DEVIATION	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

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IDENTIFICATION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	IDENTIFICATION STATISTICS OF THE TARGETS BY STAFF										10000-0000-0000-0000
	NUMBER OF DETECTIONS	C	DETECTION SUCCESS RATIO (WEFTPS)	DETECTION RANGE (METERS)	MEAN	STANDARD DEVIATION	DETECTION CUES	AURAL	SENSOR	0	
25	25	26	27	28	0.0	0.0	0	0	0	0	042216
26	26	27	28	29	0.0	0.0	0	0	0	0	042204
27	27	28	29	30	0.0	0.0	0	0	0	0	042200
28	28	29	30	31	0.0	0.0	0	0	0	0	042200
29	29	30	31	32	0.0	0.0	0	0	0	0	042200
30	30	31	32	33	0.0	0.0	0	0	0	0	042200
31	31	32	33	34	0.0	0.0	0	0	0	0	042200
32	32	33	34	35	0.0	0.0	0	0	0	0	042200
33	33	34	35	36	0.0	0.0	0	0	0	0	042200
34	34	35	36	37	0.0	0.0	0	0	0	0	042200
35	35	36	37	38	0.0	0.0	0	0	0	0	042200
36	36	37	38	39	0.0	0.0	0	0	0	0	042200
37	37	38	39	40	0.0	0.0	0	0	0	0	042200
38	38	39	40	41	0.0	0.0	0	0	0	0	042200
39	39	40	41	42	0.0	0.0	0	0	0	0	042200
40	40	41	42	43	0.0	0.0	0	0	0	0	042200
41	41	42	43	44	0.0	0.0	0	0	0	0	042200
42	42	43	44	45	0.0	0.0	0	0	0	0	042200
43	43	44	45	46	0.0	0.0	0	0	0	0	042200
44	44	45	46	47	0.0	0.0	0	0	0	0	042200
45	45	46	47	48	0.0	0.0	0	0	0	0	042200
46	46	47	48	49	0.0	0.0	0	0	0	0	042200
47	47	48	49	50	0.0	0.0	0	0	0	0	042200
48	48	49	50	51	0.0	0.0	0	0	0	0	042200
49	49	50	51	52	0.0	0.0	0	0	0	0	042200
50	50	51	52	53	0.0	0.0	0	0	0	0	042200
51	51	52	53	54	0.0	0.0	0	0	0	0	042200
52	52	53	54	55	0.0	0.0	0	0	0	0	042200
53	53	54	55	56	0.0	0.0	0	0	0	0	042200
54	54	55	56	57	0.0	0.0	0	0	0	0	042200
55	55	56	57	58	0.0	0.0	0	0	0	0	042200
56	56	57	58	59	0.0	0.0	0	0	0	0	042200
57	57	58	59	60	0.0	0.0	0	0	0	0	042200
58	58	59	60	61	0.0	0.0	0	0	0	0	042200
59	59	60	61	62	0.0	0.0	0	0	0	0	042200
60	60	61	62	63	0.0	0.0	0	0	0	0	042200
61	61	62	63	64	0.0	0.0	0	0	0	0	042200
62	62	63	64	65	0.0	0.0	0	0	0	0	042200
63	63	64	65	66	0.0	0.0	0	0	0	0	042200
64	64	65	66	67	0.0	0.0	0	0	0	0	042200
65	65	66	67	68	0.0	0.0	0	0	0	0	042200
66	66	67	68	69	0.0	0.0	0	0	0	0	042200
67	67	68	69	70	0.0	0.0	0	0	0	0	042200
68	68	69	70	71	0.0	0.0	0	0	0	0	042200
69	69	70	71	72	0.0	0.0	0	0	0	0	042200
70	70	71	72	73	0.0	0.0	0	0	0	0	042200
71	71	72	73	74	0.0	0.0	0	0	0	0	042200
72	72	73	74	75	0.0	0.0	0	0	0	0	042200
73	73	74	75	76	0.0	0.0	0	0	0	0	042200
74	74	75	76	77	0.0	0.0	0	0	0	0	042200
75	75	76	77	78	0.0	0.0	0	0	0	0	042200
76	76	77	78	79	0.0	0.0	0	0	0	0	042200
77	77	78	79	80	0.0	0.0	0	0	0	0	042200
78	78	79	80	81	0.0	0.0	0	0	0	0	042200
79	79	80	81	82	0.0	0.0	0	0	0	0	042200
80	80	81	82	83	0.0	0.0	0	0	0	0	042200
81	81	82	83	84	0.0	0.0	0	0	0	0	042200
82	82	83	84	85	0.0	0.0	0	0	0	0	042200
83	83	84	85	86	0.0	0.0	0	0	0	0	042200
84	84	85	86	87	0.0	0.0	0	0	0	0	042200
85	85	86	87	88	0.0	0.0	0	0	0	0	042200
86	86	87	88	89	0.0	0.0	0	0	0	0	042200
87	87	88	89	90	0.0	0.0	0	0	0	0	042200
88	88	89	90	91	0.0	0.0	0	0	0	0	042200
89	89	90	91	92	0.0	0.0	0	0	0	0	042200
90	90	91	92	93	0.0	0.0	0	0	0	0	042200
91	91	92	93	94	0.0	0.0	0	0	0	0	042200
92	92	93	94	95	0.0	0.0	0	0	0	0	042200
93	93	94	95	96	0.0	0.0	0	0	0	0	042200
94	94	95	96	97	0.0	0.0	0	0	0	0	042200
95	95	96	97	98	0.0	0.0	0	0	0	0	042200
96	96	97	98	99	0.0	0.0	0	0	0	0	042200
97	97	98	99	100	0.0	0.0	0	0	0	0	042200
98	98	99	100	101	0.0	0.0	0	0	0	0	042200
99	99	100	101	102	0.0	0.0	0	0	0	0	042200
100	100	101	102	103	0.0	0.0	0	0	0	0	042200
101	101	102	103	104	0.0	0.0	0	0	0	0	042200
102	102	103	104	105	0.0	0.0	0	0	0	0	042200
103	103	104	105	106	0.0	0.0	0	0	0	0	042200
104	104	105	106	107	0.0	0.0	0	0	0	0	042200
105	105	106	107	108	0.0	0.0	0	0	0	0	042200
106	106	107	108	109	0.0	0.0	0	0	0	0	042200
107	107	108	109	110	0.0	0.0	0	0	0	0	042200
108	108	109	110	111	0.0	0.0	0	0	0	0	042200
109	109	110	111	112	0.0	0.0	0	0	0	0	042200
110	110	111	112	113	0.0	0.0	0	0	0	0	042200
111	111	112	113	114	0.0	0.0	0	0	0	0	042200
112	112	113	114	115	0.0	0.0	0	0	0	0	042200
113	113	114	115	116	0.0	0.0	0	0	0	0	042200
114	114	115	116	117	0.0	0.0	0	0	0	0	042200
115	115	116	117	118	0.0	0.0	0	0	0	0	042200
116	116	117	118	119	0.0	0.0	0	0	0	0	042200
117	117	118	119	120	0.0	0.0	0	0	0	0	042200
118	118	119	120	121	0.0	0.0	0	0	0	0	042200
119	119	120	121	122	0.0	0.0	0	0	0	0	042200
120	120	121	122	123	0.0	0.0	0	0	0	0	042200
121	121	122	123	124	0.0	0.0	0	0	0	0	042200
122	122	123	124	125	0.0	0.0	0	0	0	0	042200
123	123	124	125	126	0.0	0.0	0	0	0	0	042200
124	124	125	126	127	0.0	0.0	0	0	0	0	042200
125	125	126	127	128	0.0	0.0	0	0	0	0	042200
126	126	127	128	129	0.0	0.0	0	0	0	0	042200
127	127	128	129	130	0.0	0.0	0	0	0	0	042200
128	128	129	130	131	0.0	0.0	0	0	0	0	042200
129	129	130	131	132	0.0	0.0	0	0	0	0	042200
130	130	131	132	133	0.0	0.0	0	0	0	0	042200
131	131	132	133	134	0.0	0.0	0	0	0	0	042200
132	132	133	134	135	0.0	0.0	0	0	0	0	042200
133	133	134	135	136	0.0	0.0	0	0	0	0	042200
134	134	135	136	137	0.0	0.0	0	0	0	0	042200
135	135	136	137	138	0.0	0.0	0	0	0	0	042200
136	136	137	138	139	0.0	0.0	0	0	0	0	042200
137	137	138	139	140	0.0	0.0	0	0	0	0	042200
138	138	139	140	141	0.0	0.0	0	0	0	0	042200
139	139	140	141	142	0.0	0.0	0	0	0	0	042200
140	140	141	142	143	0.0	0.0	0	0	0	0	042200
141	141	142	143	144	0.0	0.0	0	0	0	0	042200
142	142	143	144	145	0.0	0.0	0	0	0	0	042200
143	143	144	145	146	0.0	0.0	0	0	0	0	042200
144	144	145	146	147	0.0	0.0	0	0	0	0	042200
145	145	146	147	148	0.0	0.0	0	0	0	0	042200
146	146	147	148	149	0.0	0.0	0	0	0	0	042200
147	147	148	149	150	0.0	0.0	0	0	0	0	042200
148	148	149	150	151	0.0	0.0	0	0	0	0	042200
149	149	150	151	152	0.0	0.0	0	0	0	0	042200
150	150	151	152	153	0.0	0.0	0	0	0	0	042200
151	151	152	153	154	0.0	0.0	0	0	0	0	042200
152	152	153	154	155	0.0						

UNUSUAL DECISION STATISTICS OF THE TWO-PIECE HYBRID

Figure 6.5. SIAS SURVEILLANCE STATISTICS (PAGE 5)
MUNICIPALITY SURVEILLANCE STATISTICS (PAGE 5)

TARGET NUMBER	NUMBER OF IDENTIFICATIONS	IDENTIFICATION STATISTICS OF THE TARGETS BY SENSOR			
		AURAL	OPTICAL	MICROPHONE	TELESCOPIC
37	6	0.0	0.0	0.0	0.0
38	6	0.0	0.0	0.0	0.0
39	6	0.0	0.0	0.0	0.0
40	6	0.0	0.0	0.0	0.0
41	6	0.0	0.0	0.0	0.0
42	6	0.0	0.0	0.0	0.0
43	6	0.0	0.0	0.0	0.0
44	6	0.0	0.0	0.0	0.0
45	6	0.0	0.0	0.0	0.0
46	6	0.0	0.0	0.0	0.0
47	6	0.0	0.0	0.0	0.0
48	6	0.0	0.0	0.0	0.0
49	6	0.0	0.0	0.0	0.0
50	6	0.0	0.0	0.0	0.0
51	6	0.0	0.0	0.0	0.0
52	6	0.0	0.0	0.0	0.0
53	6	0.0	0.0	0.0	0.0
54	6	0.0	0.0	0.0	0.0
55	6	0.0	0.0	0.0	0.0
56	6	0.0	0.0	0.0	0.0
57	6	0.0	0.0	0.0	0.0
58	6	0.0	0.0	0.0	0.0
59	6	0.0	0.0	0.0	0.0
60	6	0.0	0.0	0.0	0.0
61	6	0.0	0.0	0.0	0.0
62	6	0.0	0.0	0.0	0.0

Figure 6.5. Aural, visual, microphone, telescopic identification statistics of the targets in Table 71.

UNAIDED VISUAL DETECTION STATISTICS OF THE TARGETS IN TABLE 71

NUMBER OF DETECTIONS

DETECTION SUCCESS RATE

DETECTION TIME (DAYS, HRS, MINS)

STANDARD DEVIATION

MEAN

SIGNATURE DEVIATION

DETECTION RANGE (METERS)

DETECTION CUES

SENSOR

AURAL

OPTICAL

MICROPHONE

TELESCOPIC

Figure 2-2, STAFF SURVEILLANCE STATISTICS PAGE 21
 UNARMED TARGETS BY STAFF IDENTIFICATION

UNARMED VISUAL DETECTION STATISTICS OF THE TARGETS BY STAFF					
TARGET NUMBER	43	44	45	46	47
NUMBER OF DETECTIONS	5	5	5	5	5
DETECTION SUCCESS RATIO	1.000	1.000	1.000	1.000	1.000
DETECTION RANGE (METERS)	2560.214	13320.244	3140.893	3340.067	3340.614
MEAN	10.374	6.0	6.0	6.0	6.0
STANDARD DEVIATION	0.767	0.767	0.752	0.782	0.824
DETECTION TIME (DAYS, HRS, MINS)	060945	061641	062113	070013	075555
MEAN	000000	000000	000000	000000	000000
STANDARD DEVIATION	000000	000000	000000	000000	000000
DETECTION CUFFS	5	5	5	5	5
AURAL SENSOR	5	5	5	5	5

IDENTIFICATION STATISTICS OF THE TARGETS BY STAFF

IDENTIFICATION STATISTICS OF THE TARGETS BY STAFF					
TARGET NUMBER	43	44	45	46	47
NUMBER OF IDENTIFICATIONS	5	5	5	5	5
IDENTIFICATION SUCCESS RATIO	1.000	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)	2560.214	10.3	5.0	5.0	5.0
MEAN	10.374	10.3	5.0	5.0	5.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)	000000	000000	000000	000000	000000
MEAN	000000	000000	000000	000000	000000
STANDARD DEVIATION	000000	000000	000000	000000	000000

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Figure 6.5. SIAM SUBJECTIVE STATISTICS (PAGE 9)
 1. NUMBER OF TARGETS
 2. DETECTION SCENARIO 1
 3. IDENTIFICATION SCENARIO 1
 4. APPLICATIONS

UNAIRED VISUAL DETECTION STATISTICS OF THE TARGETS BY SIAP

TARGET NUMBER	40	50	51
NUMBER OF DETECTIONS	6	6	3
DETECTION SUCCESS RATIO	1.000	1.000	0.667
DETECTION RANGE (METERS)			
MEAN	119.722	736.549	736.549
STANDARD DEVIATION	7.669	20.247	6.017
DETECTION TIME (DAYS, HRS, MINS)			
MEAN	0.70640	0.70643	0.70643
STANDARD DEVIATION	0.00000	0.00000	0.00000
DETECTION CUES			
AURAL	0	0	0
SENSOR			

IDENTIFICATION STATISTICS OF THE TARGETS BY SIAP

TARGET NUMBER	40	50	51
NUMBER OF IDENTIFICATIONS	5	3	0
IDENTIFICATION SUCCESS RATIO	1.000	0.000	0.000
IDENTIFICATION RANGE (METERS)			
MEAN	119.722	100	0.0
STANDARD DEVIATION	7.669	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)			
MEAN	0.70640	0.70643	0.70643
STANDARD DEVIATION	0.00000	0.00000	0.00000

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Figure 6.2. AERIAL DETECTION STATISTICS (PAGE 10)
 NIGHT LIGHT SURVEY
 5 REPETITIONS

AERIAL DETECTION STATISTICS OF THE TARGETS BY STAF

TARGET NUMBER	1	2	3	4	5	6
NUMBER OF DETECTIONS	5	5	6	6	5	0
DETECTION SUCCESS RATIO	1.000	1.000	0.6	0.6	1.000	0.0
DETECTION RANGE (METERS)						
MEAN	344.181	242.831	60.0	0.0	311.824	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	012157	012200	000000	000000	022139	000000
STANDARD DEVIATION	000000	000000	000000	000000	000000	000000

TARGET LOCATION STATISTICS

TARGET NUMBER	1	2	3	4	5	6
TARGET LOCATION CEP (METERS)						
MEAN	0.0	0.0	24.861	21.923	9.376	0.310
STANDARD DEVIATION	0.0	0.0	0.046	0.337		

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AIRRAL DETECTION STATISTICS FOR THE TARGETS IN STAF

TARGET NUMBER	7	8	9	10	11	12
NUMBER OF DETECTIONS	5	5	6	9	5	0
DETECTION SUCCESS RATIO	1.00	1.00	1.00	1.00	1.00	0.00
DETECTION RANGE (METERS)						
MEAN	423.070	190.7	80.7	0.0	392.972	0.0
STANDARD DEVIATION	20.5	70.7	80.7	0.0	6.0	0.0
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	130221	130221	130221	000000	010851	000000
STANDARD DEVIATION	000000	000000	000000	AC0000	AC0000	000000

TARGET LOCATION STATISTICS

TARGET NUMBER	7	8	9	10	11	12
TARGET LOCATION CEP (METERS)						
MEAN	0.0	0.0	0.0	74.077	0.0	169.272
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0

ANALYSIS OF DATA FOR THE 16905-6008-R0-00 ACTIVITY

DETECTION AND TARGET LOCATIONS

TARGET NUMBER	DETECTION COUNTS			DETECTION TIME (DAYS, HRS, MINS)			TARGET LOCATION CEP (METERS)		
	MEAN	STANDARD DEVIATION	NUMBER OF DETECTIONS	MEAN	STANDARD DEVIATION	NUMBER	MEAN	STANDARD DEVIATION	NUMBER
13	1.6	1.5	14	0.0	0.0	5	2.0	1.0	13
14	1.6	1.5	15	0.0	0.0	6	2.0	1.0	14
15	1.6	1.6	16	0.0	0.0	6	2.0	1.0	15
16	1.6	1.7	17	0.0	0.0	6	2.0	1.0	16
17	1.6	1.7	18	0.0	0.0	6	2.0	1.0	17
18	1.6	1.8	19	0.0	0.0	6	2.0	1.0	18
19	1.6	1.8	20	0.0	0.0	6	2.0	1.0	19
20	1.6	1.8	21	0.0	0.0	6	2.0	1.0	20
21	1.6	1.8	22	0.0	0.0	6	2.0	1.0	21
22	1.6	1.8	23	0.0	0.0	6	2.0	1.0	22
23	1.6	1.8	24	0.0	0.0	6	2.0	1.0	23
24	1.6	1.8	25	0.0	0.0	6	2.0	1.0	24
25	1.6	1.8	26	0.0	0.0	6	2.0	1.0	25
26	1.6	1.8	27	0.0	0.0	6	2.0	1.0	26
27	1.6	1.8	28	0.0	0.0	6	2.0	1.0	27
28	1.6	1.8	29	0.0	0.0	6	2.0	1.0	28
29	1.6	1.8	30	0.0	0.0	6	2.0	1.0	29
30	1.6	1.8	31	0.0	0.0	6	2.0	1.0	30
31	1.6	1.8	32	0.0	0.0	6	2.0	1.0	31
32	1.6	1.8	33	0.0	0.0	6	2.0	1.0	32
33	1.6	1.8	34	0.0	0.0	6	2.0	1.0	33
34	1.6	1.8	35	0.0	0.0	6	2.0	1.0	34
35	1.6	1.8	36	0.0	0.0	6	2.0	1.0	35
36	1.6	1.8	37	0.0	0.0	6	2.0	1.0	36
37	1.6	1.8	38	0.0	0.0	6	2.0	1.0	37
38	1.6	1.8	39	0.0	0.0	6	2.0	1.0	38
39	1.6	1.8	40	0.0	0.0	6	2.0	1.0	39
40	1.6	1.8	41	0.0	0.0	6	2.0	1.0	40
41	1.6	1.8	42	0.0	0.0	6	2.0	1.0	41
42	1.6	1.8	43	0.0	0.0	6	2.0	1.0	42
43	1.6	1.8	44	0.0	0.0	6	2.0	1.0	43
44	1.6	1.8	45	0.0	0.0	6	2.0	1.0	44
45	1.6	1.8	46	0.0	0.0	6	2.0	1.0	45
46	1.6	1.8	47	0.0	0.0	6	2.0	1.0	46
47	1.6	1.8	48	0.0	0.0	6	2.0	1.0	47
48	1.6	1.8	49	0.0	0.0	6	2.0	1.0	48
49	1.6	1.8	50	0.0	0.0	6	2.0	1.0	49
50	1.6	1.8	51	0.0	0.0	6	2.0	1.0	50
51	1.6	1.8	52	0.0	0.0	6	2.0	1.0	51
52	1.6	1.8	53	0.0	0.0	6	2.0	1.0	52
53	1.6	1.8	54	0.0	0.0	6	2.0	1.0	53
54	1.6	1.8	55	0.0	0.0	6	2.0	1.0	54
55	1.6	1.8	56	0.0	0.0	6	2.0	1.0	55
56	1.6	1.8	57	0.0	0.0	6	2.0	1.0	56
57	1.6	1.8	58	0.0	0.0	6	2.0	1.0	57
58	1.6	1.8	59	0.0	0.0	6	2.0	1.0	58
59	1.6	1.8	60	0.0	0.0	6	2.0	1.0	59
60	1.6	1.8	61	0.0	0.0	6	2.0	1.0	60
61	1.6	1.8	62	0.0	0.0	6	2.0	1.0	61
62	1.6	1.8	63	0.0	0.0	6	2.0	1.0	62
63	1.6	1.8	64	0.0	0.0	6	2.0	1.0	63
64	1.6	1.8	65	0.0	0.0	6	2.0	1.0	64
65	1.6	1.8	66	0.0	0.0	6	2.0	1.0	65
66	1.6	1.8	67	0.0	0.0	6	2.0	1.0	66
67	1.6	1.8	68	0.0	0.0	6	2.0	1.0	67
68	1.6	1.8	69	0.0	0.0	6	2.0	1.0	68
69	1.6	1.8	70	0.0	0.0	6	2.0	1.0	69
70	1.6	1.8	71	0.0	0.0	6	2.0	1.0	70
71	1.6	1.8	72	0.0	0.0	6	2.0	1.0	71
72	1.6	1.8	73	0.0	0.0	6	2.0	1.0	72
73	1.6	1.8	74	0.0	0.0	6	2.0	1.0	73
74	1.6	1.8	75	0.0	0.0	6	2.0	1.0	74
75	1.6	1.8	76	0.0	0.0	6	2.0	1.0	75
76	1.6	1.8	77	0.0	0.0	6	2.0	1.0	76
77	1.6	1.8	78	0.0	0.0	6	2.0	1.0	77
78	1.6	1.8	79	0.0	0.0	6	2.0	1.0	78
79	1.6	1.8	80	0.0	0.0	6	2.0	1.0	79
80	1.6	1.8	81	0.0	0.0	6	2.0	1.0	80
81	1.6	1.8	82	0.0	0.0	6	2.0	1.0	81
82	1.6	1.8	83	0.0	0.0	6	2.0	1.0	82
83	1.6	1.8	84	0.0	0.0	6	2.0	1.0	83
84	1.6	1.8	85	0.0	0.0	6	2.0	1.0	84
85	1.6	1.8	86	0.0	0.0	6	2.0	1.0	85
86	1.6	1.8	87	0.0	0.0	6	2.0	1.0	86
87	1.6	1.8	88	0.0	0.0	6	2.0	1.0	87
88	1.6	1.8	89	0.0	0.0	6	2.0	1.0	88
89	1.6	1.8	90	0.0	0.0	6	2.0	1.0	89
90	1.6	1.8	91	0.0	0.0	6	2.0	1.0	90
91	1.6	1.8	92	0.0	0.0	6	2.0	1.0	91
92	1.6	1.8	93	0.0	0.0	6	2.0	1.0	92
93	1.6	1.8	94	0.0	0.0	6	2.0	1.0	93
94	1.6	1.8	95	0.0	0.0	6	2.0	1.0	94
95	1.6	1.8	96	0.0	0.0	6	2.0	1.0	95
96	1.6	1.8	97	0.0	0.0	6	2.0	1.0	96
97	1.6	1.8	98	0.0	0.0	6	2.0	1.0	97
98	1.6	1.8	99	0.0	0.0	6	2.0	1.0	98
99	1.6	1.8	100	0.0	0.0	6	2.0	1.0	99
100	1.6	1.8	101	0.0	0.0	6	2.0	1.0	100
101	1.6	1.8	102	0.0	0.0	6	2.0	1.0	101
102	1.6	1.8	103	0.0	0.0	6	2.0	1.0	102
103	1.6	1.8	104	0.0	0.0	6	2.0	1.0	103
104	1.6	1.8	105	0.0	0.0	6	2.0	1.0	104
105	1.6	1.8	106	0.0	0.0	6	2.0	1.0	105
106	1.6	1.8	107	0.0	0.0	6	2.0	1.0	106
107	1.6	1.8	108	0.0	0.0	6	2.0	1.0	107
108	1.6	1.8	109	0.0	0.0	6	2.0	1.0	108
109	1.6	1.8	110	0.0	0.0	6	2.0	1.0	109
110	1.6	1.8	111	0.0	0.0	6	2.0	1.0	110
111	1.6	1.8	112	0.0	0.0	6	2.0	1.0	111
112	1.6	1.8	113	0.0	0.0	6	2.0	1.0	112
113	1.6	1.8	114	0.0	0.0	6	2.0	1.0	113
114	1.6	1.8	115	0.0	0.0	6	2.0	1.0	114
115	1.6	1.8	116	0.0	0.0	6	2.0	1.0	115
116	1.6	1.8	117	0.0	0.0	6	2.0	1.0	116
117	1.6	1.8	118	0.0	0.0	6	2.0	1.0	117
118	1.6	1.8	119	0.0	0.0	6	2.0	1.0	118
119	1.6	1.8	120	0.0	0.0	6	2.0	1.0	119
120	1.6	1.8	121	0.0	0.0	6	2.0	1.0	120
121	1.6	1.8	122	0.0	0.0	6	2.0	1.0	121
122	1.6	1.8	123	0.0	0.0	6	2.0	1.0	122
123	1.6	1.8	124	0.0	0.0	6	2.0	1.0	123
124	1.6	1.8	125	0.0	0.0	6	2.0	1.0	124
125	1.6	1.8	126	0.0	0.0	6	2.0	1.0	125
126	1.6	1.8	127	0.0	0.0	6	2.0	1.0	126
127	1.6	1.8	128	0.0	0.0	6	2.0	1.0	127
128	1.6	1.8	129	0.0	0.0	6	2.0	1.0	128
129	1.6	1.8	130	0.0	0.0	6	2.0	1.0	129
130	1.6	1.8	131	0.0	0.0	6	2.0	1.0	130
131	1.6	1.8	132	0.0	0.0	6	2.0	1.0	131
132	1.6	1.8	133	0.0	0.0	6	2.0	1.0	132
133	1.6	1.8	134	0.0	0.0	6	2.0	1.0	133
134	1.6	1.8	135	0.0	0.0	6	2.0	1.0	134
135	1.6	1.8	136	0.0	0.0	6	2.0	1.0	135
136	1.6	1.8	137	0.0	0.0	6	2.0	1.0	136
137	1.6	1.8	138	0.0	0.0	6	2.0	1.0	137
138	1.6	1.8	139	0.0	0.0	6	2.0	1.0	138
139	1.6	1.8	140	0.0	0.0	6	2.0	1.0	139
140	1.6	1.8	141	0.0	0.0	6	2.0	1.0	140
141	1.6	1.8	142	0.0	0.0	6	2.0	1.0	141
142	1.6	1.8	143	0.0	0.0	6	2.0	1.0	142
143	1.6	1.8	144	0.0	0.0	6	2.0	1.0	143
144	1.6								

ANNUAL SURVEILLANCE STATISTICS (PAGE 12)
MAY 1978
5 REPLICATES

ANNUAL DETECTION STATISTICS OF THE TARGETS BY STAFF

TARGET NUMBER	19	20	21	22	23	24
NUMBER OF DETECTIONS	0	0	0	0	0	0
DETECTION SUCCESS RATIO	0.0	0.000	0.0	0.0	0.0	0.0
DETECTION RANGE (METERS)	0.0	27.000	0.0	0.0	0.0	0.0
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)	000000	000000	000000	000000	000000	000000
MEAN	000000	000000	000000	000000	000000	000000
STANDARD DEVIATION	000000	000000	000000	000000	000000	000000

TARGET LOCATION STATISTICS

TARGET NUMBER	19	20	21	22	23	24
TARGET LOCATION CEP (METERS)	5.095	5.095	0.0	0.487	6.329	72.065
MEAN	1.033	0.0	0.0	0.0	0.453	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0

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2. AURAL DETECTION STATISTICS (PAGE 16)
INTER-LINEGET SCENARIO 1
REPLICATIONS

AURAL DETECTION STATISTICS OF THF TARGETS BY SIAF

TARGET NUMBER	25	26	27	28	29	30
NUMBER OF DETECTIONS	0	0	0	0	0	0
DETECTION SUCCESS RATIO	0.0	0.0	0.0	0.000	0.0	0.0
DETECTION RANGE (METERS)						
MEAN	0.0	0.0	0.0	446.849	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	8.559	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	00000.00000	00000.00000	00000.00000	04221.8	000000	000000
STANDARD DEVIATION	00000.00000	00000.00000	00000.00000		000000	000000

TARGET LOCATION STATISTICS

TARGET NUMBER	25	26	27	28	29	30
TARGET LOCATION CEP (METERS)						
MEAN	22.011	0.0	29.577	6.591	0.0	0.0
STANDARD DEVIATION	0.0	0.0	27.384	0.0	0.0	0.0

Figure 6.5. SIAF SURVEILLANCE STATISTICS (PAGE 15)
MUNIER LIGGETT SCENARIO 1
SIAF'S REPLICATIONS

AURAL DETECTION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	31	32	33	34	35	36
NUMBER OF DETECTIONS	4	0	0	0	6	5
DETECTION SUCCESS RATIO	1.000	0.0	0.0	0.0	1.000	1.000
DETECTION RANGE (METERS)						
MEAN	27.909	0.0	0.0	0.0	301.201	263.412
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)	050554 000000	000000 000000	000000 000000	000000 000000	052114 000000	000000 000000
MEAN						
STANDARD DEVIATION						

TARGET NUMBER	31	32	33	34	35	36
TARGET LOCATION CEP (METERS)	4.537 1.261	0.1 0.0	6.489 0.0	5.744 0.261	31.116 0.489	36.438 0.011
MEAN						
STANDARD DEVIATION						

HUNTER LIGGETT SCENARIOS STATISTICS (PAGE 16)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

AURAL DETECTION STATISTICS IF THE TARGETS BY SIAF

TARGET NUMBER	37	38	39	40	41	42
NUMBER OF DETECTIONS	6	0	0	0	0	5
DETECTION SUCCESS RATIO	0.0	0.0	0.0	0.0	0.0	1.000
DETECTION RANGE (METERS)						
MEAN	2.0	0.0	0.0	0.0	0.0	369.338
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	34.106
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	0.00000	0.00000	0.00000	0.00000	0.00000	0.00215
STANDARD DEVIATION	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000

TARGET LOCATION STATISTICS

TARGET NUMBER	37	38	39	40	41	42
TARGET LOCATION CEP (METERS)						
MEAN	19.649	0.0	0.0	0.0	0.0	37.123
STANDARD DEVIATION	0.021	0.0	0.0	0.0	0.0	0.0164

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Figure 6.5. SIAR SURVEILLANCE STATISTICS (PAGE 17)
HUNTER BUGGET SCENARIO 1
5 REPLICATIONS

AURAL DETECTION STATISTICS OF THE TARGETS BY SIAR

TARGET NUMBER	43	44	45	46	47	48
NUMBER OF DETECTIONS	5	0	5	5	5	5
DETECTION SUCCESS RATIO	1.000	0.0	1.000	1.000	1.000	1.000
DETECTION RANGE (METERS)						
MEAN	374.015	2.0	394.064	466.796	470.139	418.854
STANDARD DEVIATION	22.622	0.0	8.192	41.378	34.697	36.359
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	060845	000000	061643	062112	070012	070554
STANDARD DEVIATION	000000	000000	000000	000000	000000	000000

TARGET LOCATION STATISTICS						
TARGET NUMBER	43	44	45	46	47	48
TARGET LOCATION CEP (METERS)						
MEAN	36.810	192.413	48.151	48.161	48.116	48.191
STANDARD DEVIATION	0.198	0.0	0.110	0.115	0.112	0.118

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Figure 6.5. SIAR SURVEILLANCE STATISTICS (PAGE 18)
HUNTER LIGGETT SCENARIO I
5 REPLICATIONS

AIRAL DETECTION STATISTICS FOR THE TARGETS BY SIAR

TARGET NUMBER	49	50	51
NUMBER OF DETECTIONS	0	0	0
DETECTION SUCCESS RATIO	0.0	0.0	0.0
DETECTION RANGE (METERS)	0.0	0.0	0.0
MEAN	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)	000000 000000	000000 000000	000000 000000
MEAN	000000	000000	000000
STANDARD DEVIATION	000000	000000	000000

TARGET LOCATION STATISTICS

TARGET NUMBER	49	50	51
TARGET LOCATION CEP (METERS)	17.214 0.096	105.901 0.057	105.904 0.072
MEAN	17.214	105.901	105.904
STANDARD DEVIATION	0.096		0.057

Figure 6.5, TARGET SURVEILLANCE STATISTICS (PAGE 16)
HUNTER LIGGETT SCENARIO 1
S REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	1	2	3	4	5
NUMBER OF DETECTIONS	0	0	0	1	0
DETECTION SUCCESS RATIO	0.0	0.0	0.0	0.200	0.0
DETECTION RANGE (METERS)	0.0	0.0	0.0	172.478	0.0
MEAN STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)	-00000.0	00000.0	00000.0	020517	00000.0
MEAN STANDARD DEVIATION	-00000.0	00000.0	00000.0	00000.0	00000.0
DETECTION CUES	0	0	0	0	0
AURAL					
SENSOR					

IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	1	2	3	4	5
NUMBER OF IDENTIFICATIONS	0	0	0	0	0
IDENTIFICATION SUCCESS RATIO	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)	0.0	0.0	0.0	0.0	0.0
MEAN STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)	00000.0	00000.0	00000.0	00000.0	00000.0
MEAN STANDARD DEVIATION	00000.0	00000.0	00000.0	00000.0	00000.0

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Figure 3.3. TARGET SURVEILLANCE STATISTICS (PAGE 2 of
HUNTER LIGGETT SCENARIOS)
5 REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	7	8	9	10	11	12
NUMBER OF DETECTIONS	0	3	0	0	0	3
DETECTION SUCCESS RATIO	1.0	1.0	0.0	0.0	0.0	0.0
DETECTION RANGE (METERS)						
MEAN	0.0	3.0	0.0	0.0	0.0	1036.898
STANDARD DEVIATION	0.0	2.0	0.0	0.0	0.0	2.441
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	0000000	0000000	0000000	0000000	0000000	0000000
STANDARD DEVIATION	0000000	0000000	0000000	0000000	0000000	0000000
DETECTION-CUES						
AURAL	0	0	0	0	0	0
SENSOR						

IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	7	8	9	10	11	12
NUMBER OF IDENTIFICATIONS	0	0	0	0	0	0
IDENTIFICATION SUCCESS RATIO	0.0	1.0	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)						
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)						
MEAN	0000000	0000000	0000000	0000000	0000000	0000000
STANDARD DEVIATION	0000000	0000000	0000000	0000000	0000000	0000000

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FIGURE 1. TABLE OF SENSITIVITIES OF STATISTICS (PAGE 21)
HURTELLIGETTS SCENARIOS

UNILINEAR VISUAL DEFFECTIVENESS STATISTICS ARE BIASED BY THE TARGETS

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TARGET NUMBER	IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS		
	MEAN NUMBER OF IDENTIFICATIONS	STANDARD DEVIATION	IDENTIFICATION TIME (DAYS, HRS, MINS)
19	20	21	22
20	21	22	23
21	22	23	24
22	23	24	
23	24		
24			

TARGET NUMBER	UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS		
	MEAN NUMBER OF DETECTIONS	STANDARD DEVIATION	DETECTION TIME (DAYS, HRS, MINS)
19	3	0	0.600
20	3	0	0.600
21	3	0	0.600
22	3	0	0.600
23	3	0	0.600
24	3	0	0.600

TARGET NUMBER	UNAIDED AUDITORY DETECTION STATISTICS OF SIAF BY THE TARGETS		
	MEAN NUMBER OF DETECTIONS	STANDARD DEVIATION	DETECTION TIME (DAYS, HRS, MINS)
19	0	0	0.000
20	0	0	0.000
21	0	0	0.000
22	0	0	0.000
23	0	0	0.000
24	0	0	0.000

Figure 5-1. TABLE 1. SURVEILLANCE STATISTICS (PAGE 22)
UNAIDED VISUAL DETECTION (PAGE 22)
AUDITORY DETECTION SCENARIO 1
4 REPLICATIONS

REPORT NO. 1, TEST 1, IDENTIFICATION STATISTICS (PAGE 2/3)
NUMBER OF IDENTIFICATIONS SECURED = 1
NUMBER OF IDENTIFICATIONS PUBLICATIONS

UNAIRED VISUAL DETECTION STATISTICS OF STAR BY THE TARGETS

TARGET NUMBER	25	26	27	28	29	30
NUMBER OF DETECTIONS	0	4	0	0	4	0
DETECTION SUCCESS RATIO	0.0	0.900	0.0	0.0	0.800	0.0
DETECTION RANGE (METERS)	0.0	172.107	0.0	0.0	3.600	0.0
MEAN	0.0	85.050	0.0	0.0	6.600	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)	0000000	00133	0000000	0000000	002205	0000000
MEAN	0000000	0000000	0000000	0000000	0000000	0000000
STANDARD DEVIATION	0000000	0000000	0000000	0000000	0000000	0000000
DETECTION CUFFS	0	0	0	0	0	0
AURAL	0	0	0	0	0	0
SENSOR	0	0	0	0	0	0

IDENTIFICATION STATISTICS OF STAR BY THE TARGETS

TARGET NUMBER	25	26	27	28	29	30
NUMBER OF IDENTIFICATIONS	0	0	0	0	4	0
IDENTIFICATION SUCCESS RATIO	0.0	0.0	0.0	0.0	1.000	0.0
IDENTIFICATION RANGE (METERS)	0.0	0.0	0.0	0.0	0.0	0.0
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS, HRS, MINS)	0000000	0000000	0000000	0000000	002205	0000000
MEAN	0000000	0000000	0000000	0000000	0000000	0000000
STANDARD DEVIATION	0000000	0000000	0000000	0000000	0000000	0000000

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Figure 6.5, TARGET SURVEILLANCE STATISTICS (PAGE 24)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	31	32	33	34	35	36
NUMBER OF DETECTIONS	1	0	0	0	0	0
DETECTION SUCCESS RATIO	0.250	0.0	0.0	0.0	0.0	0.0
DETECTION RANGE (METERS)	25.007	2.0	0.0	0.0	0.0	0.0
MEAN	25.0	2.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS,HRS,MINS)	050054 000000	030000 020000	300000 000000	000000 000000	000000 000000	000000 000000
MEAN	050054 000000	030000 020000	300000 000000	000000 000000	000000 000000	000000 000000
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION GUES AURAL SENSOR	0	0	0	0	0	0

IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	31	32	33	34	35	36
NUMBER OF IDENTIFICATIONS	1	0	0	0	0	0
IDENTIFICATION SUCCESS RATIO	1.000	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)	25.007 0.0	2.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
MEAN	25.0 0.0	2.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0	0.0 0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS,HRS,MINS)	050054 000000	030000 020000	300000 000000	000000 000000	000000 000000	000000 000000
MEAN	050054 000000	030000 020000	300000 000000	000000 000000	000000 000000	000000 000000
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0

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Figure 6.5, TARGET SURVEILLANCE STATISTICS (PAGE 26)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	43	44	45	46	47	48
NUMBER OF DETECTIONS	3	0	0	0	0	1
DETECTION SUCCESS RATIO	0.666	0.0	0.0	0.0	0.0	0.200
DETECTION RANGE (METERS)						
MEAN	255.577	7.0	0.0	0.0	0.0	335.355
STANDARD DEVIATION	1.525	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS,HRS,MIN)						
MEAN	060845	000000	000000	000000	000000	070555
STANDARD DEVIATION	000000	000000	000000	000000	000000	000000
DETECTION CUES						
AURAL	0	0	0	0	0	0
SENSOR						

IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	43	44	45	46	47	48
NUMBER OF IDENTIFICATIONS	0	0	0	0	0	0
IDENTIFICATION SUCCESS RATIO	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION RANGE (METERS)						
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
IDENTIFICATION TIME (DAYS,HRS,MIN)						
MEAN	000000	000000	000000	000000	000000	000000
STANDARD DEVIATION	000000	000000	000000	000000	000000	000000

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Figure 6.5, TARGET SURVEILLANCE ST. STICS (PAGE 27)
 HUNTER LIGGETT SCENARIO 1
 5 REPLICATES

UNAIDED VISUAL DETECTION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	49	50	51
NUMBER OF DETECTIONS	5	5	5
DETECTION SUCCESS RATIO	1.000	1.000	1.000
DETECTION RANGE (METERS)			
MEAN	119.722	736.548	736.548
STANDARD DEVIATION	0.669	0.047	0.047
DETECTION TIME (DAYS,HRS,MINS)			
MEAN	070640	070643	070643
STANDARD DEVIATION	000000	000000	000000
DETECTION CUES			
AURAL	0	0	0
SENSOR			

IDENTIFICATION STATISTICS OF SIAF BY THE TARGETS

TARGET NUMBER	49	50	51
NUMBER OF IDENTIFICATIONS	5	5	0
IDENTIFICATION SUCCESS RATIO	1.000	0.0	0.0
IDENTIFICATION RANGE (METERS)			
MEAN	119.722	0.0	0.0
STANDARD DEVIATION	0.669	0.0	0.0
IDENTIFICATION TIME (DAYS,HRS,MINS)			
MEAN	070640	070640	000000
STANDARD DEVIATION	000000	000000	000000

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Figure 6-3. TARGET SURVEILLANCE STATISTICS (PAGE 23)
HUNTER LIGGETT SCENARIO 1
5 APPLICATIONS

AUDIT DETECTION STATISTICS OF STAFF BY THE TARGETS

TARGET NUMBER	1	2	3	4	5	6
NUMBER OF DETECTIONS	0	0	0	0	0	0
DETECTION SUCCESS RATIO	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION RANGE (METERS)						
MEAN	0.0	0.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	3.0	3.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	000000 000000	000000 000000	000000 000000	000000 000000	000000 000000	000000 000000
STANDARD DEVIATION						

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Figure 5.5. TARGET SURVEILLANCE STATISTICS (PAGE 20)
HUNTER LOGGED SCENARIO 1
5 REPLICATIONS

ANNUAL DETERMINATION STATISTICS OF STAFF BY TIME TARGETS

TARGET NUMBER	NUMBER OF DETECTIONS		DETECTION SUCCESS RATIO		DETECTION RANGE (METERS)		DETECTION TIME (DAYS, HRS, MINS)	
	MEAN	STANDARD DEVIATION	MEAN	STANDARD DEVIATION	MEAN	STANDARD DEVIATION	MEAN	STANDARD DEVIATION
11	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
10	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
9	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
8	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
7	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
6	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
5	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
4	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
3	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
2	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
1	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
0	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000
12	6	0.0	0.0	0.0	0.0	0.0	0.00000	0.00000

FIGURE 1. AIRPORT SURVEILLANCE STATISTICS (PAGE 3 OF 3)
BY TARGET NUMBER SCENARIO 1
5 REPLICATES

AIRPORT DETECTION STATISTICS BY SIZE OF THE TARGETS

TARGET NUMBER	13	14	15	16	17	18
NUMBER OF DETECTIONS	6	3	0	0	0	0
DETECTION SUCCESS RATIO	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION RANGE (METERS)						
MEAN	0.0	3.0	0.0	0.0	0.0	0.0
STANDARD DEVIATION	0.0	0.0	0.0	0.0	0.0	0.0
DETECTION TIME (DAYS, HRS, MINS)						
MEAN	00000.0	00000.0	00000.0	00000.0	00000.0	00000.0
STANDARD DEVIATION	00000.0	00000.0	00000.0	00000.0	00000.0	00000.0

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Figure 6.5. TARGET SURVEILLANCE STATISTICS (PAGE 32)
HUNTER LIGGET SCENARIOS
S. REPLICATIONS

AUGUSTAL DEFECTICION: STATISTICS OF THE INFLUENZA

TARGET NUMBER	NUMBER OF DETECTIONS	DETECTION SUCCESS RATE	MEAN DETECTION RANGE (METERS)	DETECTION TIME (DAYS,IRS,MINS)		STANDARD DEVIATION	MEAN DEVIATION
				DETECTION	STANDARD DEVIATION		
26	25	0	0.0	0.0	0.0	0.00000	0.00000
27	26	0	0.0	0.0	0.0	0.00000	0.00000
28	29	0	0.0	0.0	0.0	0.00000	0.00000
29	29	0	0.0	0.0	0.0	0.00000	0.00000
30	30	0	0.0	0.0	0.0	0.00000	0.00000

Figure 6.5. TARGET SURVEILLANCE STATISTICS (PAGE 331)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

TARGET NUMBER	NUMBER OF DETECTIONS	DETECTION SUCCESS RATE	MEAN RANGE (METERS)	DETECTION TIME (DAYS, HRS, MINS)		STANDARD DEVIATION
				MEAN	STANDARD DEVIATION	
31	0	0.0	0.0	0.0	0.0	0.00000
32	0	0.0	0.0	0.0	0.0	0.00000
33	0	0.0	0.0	0.0	0.0	0.00000
34	0	0.0	0.0	0.0	0.0	0.00000
35	0	0.0	0.0	0.0	0.0	0.00000
36	0	0.0	0.0	0.0	0.0	0.00000
37	0	0.0	0.0	0.0	0.0	0.00000
38	0	0.0	0.0	0.0	0.0	0.00000
39	0	0.0	0.0	0.0	0.0	0.00000
40	0	0.0	0.0	0.0	0.0	0.00000
41	0	0.0	0.0	0.0	0.0	0.00000
42	0	0.0	0.0	0.0	0.0	0.00000
43	0	0.0	0.0	0.0	0.0	0.00000
44	0	0.0	0.0	0.0	0.0	0.00000
45	0	0.0	0.0	0.0	0.0	0.00000
46	0	0.0	0.0	0.0	0.0	0.00000
47	0	0.0	0.0	0.0	0.0	0.00000
48	0	0.0	0.0	0.0	0.0	0.00000
49	0	0.0	0.0	0.0	0.0	0.00000
50	0	0.0	0.0	0.0	0.0	0.00000
51	0	0.0	0.0	0.0	0.0	0.00000
52	0	0.0	0.0	0.0	0.0	0.00000
53	0	0.0	0.0	0.0	0.0	0.00000
54	0	0.0	0.0	0.0	0.0	0.00000
55	0	0.0	0.0	0.0	0.0	0.00000
56	0	0.0	0.0	0.0	0.0	0.00000
57	0	0.0	0.0	0.0	0.0	0.00000
58	0	0.0	0.0	0.0	0.0	0.00000
59	0	0.0	0.0	0.0	0.0	0.00000
60	0	0.0	0.0	0.0	0.0	0.00000
61	0	0.0	0.0	0.0	0.0	0.00000
62	0	0.0	0.0	0.0	0.0	0.00000
63	0	0.0	0.0	0.0	0.0	0.00000
64	0	0.0	0.0	0.0	0.0	0.00000
65	0	0.0	0.0	0.0	0.0	0.00000
66	0	0.0	0.0	0.0	0.0	0.00000
67	0	0.0	0.0	0.0	0.0	0.00000
68	0	0.0	0.0	0.0	0.0	0.00000
69	0	0.0	0.0	0.0	0.0	0.00000
70	0	0.0	0.0	0.0	0.0	0.00000
71	0	0.0	0.0	0.0	0.0	0.00000
72	0	0.0	0.0	0.0	0.0	0.00000
73	0	0.0	0.0	0.0	0.0	0.00000
74	0	0.0	0.0	0.0	0.0	0.00000
75	0	0.0	0.0	0.0	0.0	0.00000
76	0	0.0	0.0	0.0	0.0	0.00000
77	0	0.0	0.0	0.0	0.0	0.00000
78	0	0.0	0.0	0.0	0.0	0.00000
79	0	0.0	0.0	0.0	0.0	0.00000
80	0	0.0	0.0	0.0	0.0	0.00000
81	0	0.0	0.0	0.0	0.0	0.00000
82	0	0.0	0.0	0.0	0.0	0.00000
83	0	0.0	0.0	0.0	0.0	0.00000
84	0	0.0	0.0	0.0	0.0	0.00000
85	0	0.0	0.0	0.0	0.0	0.00000
86	0	0.0	0.0	0.0	0.0	0.00000
87	0	0.0	0.0	0.0	0.0	0.00000
88	0	0.0	0.0	0.0	0.0	0.00000
89	0	0.0	0.0	0.0	0.0	0.00000
90	0	0.0	0.0	0.0	0.0	0.00000
91	0	0.0	0.0	0.0	0.0	0.00000
92	0	0.0	0.0	0.0	0.0	0.00000
93	0	0.0	0.0	0.0	0.0	0.00000
94	0	0.0	0.0	0.0	0.0	0.00000
95	0	0.0	0.0	0.0	0.0	0.00000
96	0	0.0	0.0	0.0	0.0	0.00000
97	0	0.0	0.0	0.0	0.0	0.00000
98	0	0.0	0.0	0.0	0.0	0.00000
99	0	0.0	0.0	0.0	0.0	0.00000
100	0	0.0	0.0	0.0	0.0	0.00000

Figure 6.5. TARGET SURVEILLANCE STATISTICS (PAGE 36)
MONTE CARLO SCENARIO 1
5 REPLICATIONS

AURAL DETECTION STATISTICS OF SIAF AT THE TARGETS

TARGET NUMBER	NUMBER OF DETECTIONS	DETECTION SUCCESS RATIO			MEAN STANDARD DEVIATION	DETECTION TIME (DAYS, HRS, MINS)	- MEAN STANDARD DEVIATION
		MEAN RANGE (METERS)	STANDARD DEVIATION	MEAN			
37	36	0.0	0.0	0.0	0.0	000000 000000	000000 000000
38	39	0.0	0.0	0.0	0.0	000000 000000	000000 000000
39	40	0.0	0.0	0.0	0.0	000000 000000	000000 000000
40	41	0.0	0.0	0.0	0.0	000000 000000	000000 000000
41	42	0.0	0.0	0.0	0.0	000000 000000	000000 000000
42	43	0.0	0.0	0.0	0.0	000000 000000	000000 000000
43	44	0.0	0.0	0.0	0.0	000000 000000	000000 000000
44	45	0.0	0.0	0.0	0.0	000000 000000	000000 000000
45	46	0.0	0.0	0.0	0.0	000000 000000	000000 000000
46	47	0.0	0.0	0.0	0.0	000000 000000	000000 000000
47	48	0.0	0.0	0.0	0.0	000000 000000	000000 000000
48	49	0.0	0.0	0.0	0.0	000000 000000	000000 000000
49	50	0.0	0.0	0.0	0.0	000000 000000	000000 000000
50	51	0.0	0.0	0.0	0.0	000000 000000	000000 000000
51	52	0.0	0.0	0.0	0.0	000000 000000	000000 000000
52	53	0.0	0.0	0.0	0.0	000000 000000	000000 000000
53	54	0.0	0.0	0.0	0.0	000000 000000	000000 000000
54	55	0.0	0.0	0.0	0.0	000000 000000	000000 000000
55	56	0.0	0.0	0.0	0.0	000000 000000	000000 000000
56	57	0.0	0.0	0.0	0.0	000000 000000	000000 000000
57	58	0.0	0.0	0.0	0.0	000000 000000	000000 000000
58	59	0.0	0.0	0.0	0.0	000000 000000	000000 000000
59	60	0.0	0.0	0.0	0.0	000000 000000	000000 000000
60	61	0.0	0.0	0.0	0.0	000000 000000	000000 000000
61	62	0.0	0.0	0.0	0.0	000000 000000	000000 000000
62	63	0.0	0.0	0.0	0.0	000000 000000	000000 000000
63	64	0.0	0.0	0.0	0.0	000000 000000	000000 000000
64	65	0.0	0.0	0.0	0.0	000000 000000	000000 000000
65	66	0.0	0.0	0.0	0.0	000000 000000	000000 000000
66	67	0.0	0.0	0.0	0.0	000000 000000	000000 000000
67	68	0.0	0.0	0.0	0.0	000000 000000	000000 000000
68	69	0.0	0.0	0.0	0.0	000000 000000	000000 000000
69	70	0.0	0.0	0.0	0.0	000000 000000	000000 000000
70	71	0.0	0.0	0.0	0.0	000000 000000	000000 000000
71	72	0.0	0.0	0.0	0.0	000000 000000	000000 000000
72	73	0.0	0.0	0.0	0.0	000000 000000	000000 000000
73	74	0.0	0.0	0.0	0.0	000000 000000	000000 000000
74	75	0.0	0.0	0.0	0.0	000000 000000	000000 000000
75	76	0.0	0.0	0.0	0.0	000000 000000	000000 000000
76	77	0.0	0.0	0.0	0.0	000000 000000	000000 000000
77	78	0.0	0.0	0.0	0.0	000000 000000	000000 000000
78	79	0.0	0.0	0.0	0.0	000000 000000	000000 000000
79	80	0.0	0.0	0.0	0.0	000000 000000	000000 000000
80	81	0.0	0.0	0.0	0.0	000000 000000	000000 000000
81	82	0.0	0.0	0.0	0.0	000000 000000	000000 000000
82	83	0.0	0.0	0.0	0.0	000000 000000	000000 000000
83	84	0.0	0.0	0.0	0.0	000000 000000	000000 000000
84	85	0.0	0.0	0.0	0.0	000000 000000	000000 000000
85	86	0.0	0.0	0.0	0.0	000000 000000	000000 000000
86	87	0.0	0.0	0.0	0.0	000000 000000	000000 000000
87	88	0.0	0.0	0.0	0.0	000000 000000	000000 000000
88	89	0.0	0.0	0.0	0.0	000000 000000	000000 000000
89	90	0.0	0.0	0.0	0.0	000000 000000	000000 000000
90	91	0.0	0.0	0.0	0.0	000000 000000	000000 000000
91	92	0.0	0.0	0.0	0.0	000000 000000	000000 000000
92	93	0.0	0.0	0.0	0.0	000000 000000	000000 000000
93	94	0.0	0.0	0.0	0.0	000000 000000	000000 000000
94	95	0.0	0.0	0.0	0.0	000000 000000	000000 000000
95	96	0.0	0.0	0.0	0.0	000000 000000	000000 000000
96	97	0.0	0.0	0.0	0.0	000000 000000	000000 000000
97	98	0.0	0.0	0.0	0.0	000000 000000	000000 000000
98	99	0.0	0.0	0.0	0.0	000000 000000	000000 000000
99	100	0.0	0.0	0.0	0.0	000000 000000	000000 000000

Figure 6-5. TABLE I SURVEILLANCE STATISTICS (PAGE 33)
MUNIFR LIGGETT SCENARIOS, REPLICATIONS

TARGET NUMBER	NUMBER OF DETECTIONS	DEFECTIVE SUCCESSION RATIO	MEAN		STANDARD DEVIATION		DETECTION TIME (DAYS, HRS, MINS)	
			0.0	0.0	0.0	0.0	0.0	0.0
43	65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
44	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
45	65	0.0	0.0	0.0	0.0	0.0	0.0	0.0
46	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
47	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
49	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
51	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
52	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
53	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
55	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
56	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
57	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
58	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
59	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
61	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
62	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
63	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
64	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
65	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
66	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
67	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
68	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
69	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
72	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
73	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
74	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
75	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
76	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
77	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
78	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
79	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
81	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
82	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
83	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
84	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
86	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
87	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
88	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
89	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
91	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
92	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
93	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
94	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
95	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
96	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
97	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
98	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
99	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100	66	0.0	0.0	0.0	0.0	0.0	0.0	0.0

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CALORIES OF DETECTED SNAKES (PINEY ISLAND)

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CAUSES OF NO DETECTION FOR TARGETS (PERCENT)	INSUFFICIENT TIME	RANGE AND LIGHT LEVEL	MASKING BY VECTAIIIS	MASKING BY BELIEF	TARGET NUMBER	CAUSES OF NO DETECTION FOR STAFF (PERCENT)
0.0	19.032	93.948	0.0	0.0	2	1.0
0.0	0.0	0.0	0.0	0.0	1	0.0
0.0	0.0	0.0	0.0	0.0	0	0.0

1. *Digitized by Google*

Figure 6.5. STAFF/TARGET SURVEILLANCE STATISTICS (PAGE 39)
HUNTING LIGHT SCENARIOS
5 REPLICATIONS

CAUSES OF NO DETECTION FOR STAFF (PERCENT)						
TARGET NUMBER	13	14	15	16	17	18
MASKING BY RELIEF	0.0	33.969	14.167	0.0	78.750	61.431
MASKING BY VEGETATION	0.0	63.262	66.667	0.0	21.250	36.392
RANGE AND LIGHT LEVEL	0.0	3.0	2.500	0.0	0.0	1.000
INSUFFICIENT TIME	0.0	2.769	16.667	0.0	0.0	1.000

CAUSES OF NO DETECTION FOR TARGETS (PERCENT)						
TARGET NUMBER	13	14	15	16	17	18
MASKING BY RELIEF	0.0	33.969	14.050	0.0	74.110	61.335
MASKING BY VEGETATION	0.0	63.262	66.110	0.0	20.000	36.335
RANGE AND LIGHT LEVEL	0.0	2.769	4.959	0.0	5.002	1.007
INSUFFICIENT TIME	0.0	0.0	14.876	0.0	0.0	1.242

Figure 6.5. STAFF/TARGET SURVEILLANCE STATISTICS (PAGE 43)
 HUNTER LIGGETT SCENARIO I
 5 REPLICATIONS

CAUSES OF NO DETECTION FOR STAFF (PERCENT)					
TARGET NUMBER	19	20	21	22	23
MASKING BY RELIEF	0.0	52.795	0.0	0.0	90.270
MASKING BY VEGETATION	100.000	40.373	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.0	74.305
INSUFFICIENT TIME	0.0	5.832	0.0	100.000	0.0
CAUSES OF NO DETECTION FOR TARGETS (PERCENT)					
TARGET NUMBER	19	20	21	22	23
MASKING BY RELIEF	0.0	53.125	0.0	0.0	89.041
MASKING BY VEGETATION	90.196	40.625	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	9.804	3.125	0.0	100.000	0.0
INSUFFICIENT TIME	0.0	3.125	0.0	0.0	4.311

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Figure 6.5. STAFF/TARGET SURVEILLANCE STATISTICS (PAGE 41)
 MUNI TEP LIGHT SCENARIO 1
 5 REPLICATES

CAUSES OF NO DETECTION FROM STAFF (PERCENT)					
TARGET NUMBER	25	26	27	28	29
MASKING BY RELIEF	23.136	46.156	35.494	37.122	0.0
MASKING BY VEGETATION	71.722	27.473	59.395	50.204	90.933
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.409	2.332
INSUFFICIENT TIME	5.141	26.374	5.161	12.265	6.736

CAUSES OF NO DETECTION FOR TARGETS (PERCENT)					
TARGET NUMBER	25	26	27	28	29
MASKING BY RELIEF	23.136	47.721	32.164	32.946	0.0
MASKING BY VEGETATION	71.722	28.409	53.001	44.957	91.645
RANGE AND LIGHT LEVEL	6.499	0.0	14.035	22.279	2.350
INSUFFICIENT TIME	0.643	23.864	0.0	0.218	36.364

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Figure 5. STAFF/TARGET SURVEILLANCE STATISTICS (PAGE 42)
 HUNTER / GUYETT SCENARIO I
 5 APPLICATIONS

CAUSES OF NO DETECTION FOR STAFF (PERCENT)

TARGET NUMBER	31	32	33	34	35	36
MASKING BY RELIEF	52.147	0.0	0.0	91.549	89.286	11.697
MASKING BY VEGETATION	39.877	0.0	0.0	0.0	7.143	83.482
RANGE AND LIGHT LEVEL	3.067	0.0	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	4.908	0.0	100.000	8.451	3.571	4.911

CAUSES OF NO DETECTION FOR TARGETS (PERCENT)

TARGET NUMBER	31	32	33	34	35	36
MASKING BY RELIEF	50.595	0.0	0.0	85.526	87.549	11.314
MASKING BY VEGETATION	38.690	0.0	0.0	0.0	7.004	81.375
RANGE AND LIGHT LEVEL	2.976	0.0	100.000	0.0	5.447	7.311
INSUFFICIENT TIME	7.738	0.0	0.0	-14.674	0.0	0.0

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Figure 6.5. SIAF/TARGET SURVEILLANCE STATISTICS (PAGE 43)
HUNTER LIGGETT SCENARIO 1
5 REPLICATIONS

CAUSES OF NO DETECTION FOR SIAF (PERCENT)						
	37	38	39	40	41	42
TARGET NUMBER	0.0	9.563	2.489	0.0	100.000	96.270
MASKING BY RELIEF	100.000	99.617	97.511	100.000	0.0	3.722
MASKING BY VEGETATION	0.0	0.0	0.0	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	1.923	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	0.0	0.0	0.0	0.0	0.0	0.0

CAUSES OF NO DETECTION FOR TARGETS (PERCENT)						
	37	38	39	40	41	42
TARGET NUMBER	0.0	9.153	2.489	0.0	100.000	93.046
MASKING BY RELIEF	100.000	85.752	97.511	100.000	0.0	3.597
MASKING BY VEGETATION	0.0	5.098	0.0	0.0	0.0	2.398
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	0.0	0.0	0.0	0.0	0.0	0.959

Figure 5.5. STAF/TARIF SURVEILLANCE STATISTICS (PAGE 44)
 WINTER LIGGETT SCENARIO 1
 5 APPLICATIONS

CAUSES OF NON DETECTION FOR STAF (PERCENT)

TARGET NUMBER	43	44	45	46	47	48
MASKING BY RELIEF	95.875	0.0	100.000	100.000	100.000	100.000
MASKING BY VEGETATION	3.125	0.0	0.0	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	0.0	0.0	0.0	0.0	0.0	0.0

CAUSES OF NON DETECTION FOR TARGETS (PERCENT)

TARGET NUMBER	43	44	45	46	47	48
MASKING BY RELIEF	95.473	0.0	98.000	98.000	98.000	98.394
MASKING BY VEGETATION	3.112	0.0	0.0	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	100.000	0.0	2.000	2.000	0.0
INSUFFICIENT TIME	0.415	0.0	2.000	0.0	0.0	1.606

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Figure 6-2. Effectiveness of target detection methods (page 65)

CAUSES OF INDETECTION FOR CLASSIFICATIONS		TARGET NUMBER		TARGET NUMBER	
		49	51	49	51
MASKING BY RELIEF	0.0	0.0	0.0	0.0	0.0
MASKING BY VEGETATION	0.0	0.0	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	0.0	0.0	0.0	0.0	0.0
CAUSES OF INDETECTION FOR TARGETS (PREDICT)		TARGET NUMBER		TARGET NUMBER	
		49	50	50	51
MASKING BY RELIEF	0.0	0.0	0.0	0.0	0.0
MASKING BY VEGETATION	0.0	0.0	0.0	0.0	0.0
RANGE AND LIGHT LEVEL	0.0	0.0	0.0	0.0	0.0
INSUFFICIENT TIME	0.0	0.0	0.0	0.0	0.0

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DATA PROCESSING STATISTICS (PVT) - 61
PATROL DURATION SUMMARY

MOVEMENT RATE (KM/HR)	
MEAN	6.964
STANDARD DEVIATION	0.324
PATROL DURATION (DAYS, HRS, MINS)	
MEAN	0.71053
STANDARD DEVIATION	0.00033
DISTANCE TRAVELED (KM)	
MEAN	9.022
STANDARD DEVIATION	0.003
MOVEMENT RATE HISTOGRAM (KM/HR)	
PERCENT TIME BETWEEN 0.1 - 0.200 KM/HR =	0.004
PERCENT TIME BETWEEN 0.200 - 0.400 KM/HR =	0.0
PERCENT TIME BETWEEN 0.400 - 0.600 KM/HR =	0.009
PERCENT TIME BETWEEN 0.600 - 0.800 KM/HR =	0.018
PERCENT TIME BETWEEN 0.800 - 1.000 KM/HR =	0.457
PERCENT TIME BETWEEN 1.000 - 1.200 KM/HR =	0.101
PERCENT TIME BETWEEN 1.200 - 1.400 KM/HR =	0.038
PERCENT TIME BETWEEN 1.400 - 1.600 KM/HR =	0.137
PERCENT TIME BETWEEN 1.600 - 1.800 KM/HR =	0.004
PERCENT TIME BETWEEN 1.800 - 2.000 KM/HR =	0.030
PERCENT TIME BETWEEN 2.000 - 2.200 KM/HR =	0.002
PERCENT TIME BETWEEN 2.200 - 2.400 KM/HR =	0.101

FIGURE 6.5. SIAF NAVIGATION STATISTICS (PAGE 47)
INTERLIGGETT SCENARIO 1
5 REPLICATIONS

PATROL CEP AT CHECKPOINTS (METERS)

MEAN	31.621
STANDARD DEVIATION	8.442

TIME TO DETERMINE LOCATION (MIN)

MEAN	0.810
STANDARD DEVIATION	0.0

SIAF INSERTION STATISTICS

INSERTION ATTEMPTS

NUMBER OF SUCCESSFUL INSERTIONS

NUMBER OF INSERTIONS AT PRIMARY LZ

NUMBER OF INSERTIONS AT SEC. LZS

INSERTION TIME (DAYS, HRS, MINS)

011700

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EXTERNAL COMMUNICATIONS

ATTEMPTS
MEAN 176.000
STANDARD DEVIATION 0.0

COMMUNICATION SUCCESS RATIO
MEAN C. 827
STANDARD DEVIATION 0.034

AVERAGE POWER LOSSES FOR COMMON FAILURES (PERCENT)
ATTENUATION DUE TO RELIEF 10.952
ATTENUATION DUE TO VEGETATION 1.019
ATTENUATION DUE TO RANGE 88.037

TOTAL TIME RECEIVING (DAYS, HRS, MINS)
MEAN 000.000
STANDARD DEVIATION 000.000

TOTAL TIME TRANSMITTING (DAYS, HRS, MINS)
MEAN 000.300
STANDARD DEVIATION 000.017

AMPERE HRS AVAILABLE 138.000

AMPERE HRS USED
MEAN 79.817
STANDARD DEVIATION C.097

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SUPPLY MAINTENANCE - STATISTICS		
TOTAL WEIGHT CARRIED (LBS/MAN)	MEAN	65.053
	STANDARD DEVIATION	0.0
FOOD (LBS/MAN)	MEAN	6.520
	STANDARD DEVIATION	0.0
WATER (LRS/MAN)	MEAN	8.019
	STANDARD DEVIATION	0.0
AMMO (LBS/MAN)	MEAN	0.0
	STANDARD DEVIATION	0.0
OTHER ORDNANCE (LBS/MAN)	MEAN	2.250
	STANDARD DEVIATION	0.0

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TIME, DEG.	PERP. DEG.	TIME	STANDBY POSITION	MEAN POSITION	STANDARD DEVIATION	TIME OF APPROXIMATION (ESTIMATE APPROXIMATE POSITION ONCE)
022132	0.0009	021931	0.01	0.0	0.0	020933
022131	0.0006	021931	0.0111	0.0111	0.0111	020933
022130	0.0003	021931	0.0121	0.0121	0.0121	020933
022129	0.0002	021931	0.0131	0.0131	0.0131	020933
022128	0.0001	021931	0.0141	0.0141	0.0141	020933
022127	0.0000	021931	0.0151	0.0151	0.0151	020933

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LIGHT LEVEL IF LAMPERESI AND SAMPLE TIME (DAYS, HRS, MIN)

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TIME	LEVEL	SAMPLE TIME	LIGHT LEVEL
0.01800	1.00E-01	0.01800	0.01800
0.01933	2.0E-02	0.01933	0.01933
0.02067	3.0E-02	0.02067	0.02067
0.02200	4.0E-02	0.02200	0.02200
0.02333	5.0E-02	0.02333	0.02333
0.02467	6.0E-02	0.02467	0.02467
0.02600	7.0E-02	0.02600	0.02600
0.02733	8.0E-02	0.02733	0.02733
0.02867	9.0E-02	0.02867	0.02867
0.03000	1.00E-01	0.03000	0.03000
0.03133	1.10E-01	0.03133	0.03133
0.03267	1.20E-01	0.03267	0.03267
0.03400	1.30E-01	0.03400	0.03400
0.03533	1.40E-01	0.03533	0.03533
0.03667	1.50E-01	0.03667	0.03667
0.03800	1.60E-01	0.03800	0.03800
0.03933	1.70E-01	0.03933	0.03933
0.04067	1.80E-01	0.04067	0.04067
0.04200	1.90E-01	0.04200	0.04200
0.04333	2.00E-01	0.04333	0.04333
0.04467	2.10E-01	0.04467	0.04467
0.04600	2.20E-01	0.04600	0.04600
0.04733	2.30E-01	0.04733	0.04733
0.04867	2.40E-01	0.04867	0.04867
0.05000	2.50E-01	0.05000	0.05000
0.05133	2.60E-01	0.05133	0.05133
0.05267	2.70E-01	0.05267	0.05267
0.05400	2.80E-01	0.05400	0.05400
0.05533	2.90E-01	0.05533	0.05533
0.05667	3.00E-01	0.05667	0.05667
0.05800	3.10E-01	0.05800	0.05800
0.05933	3.20E-01	0.05933	0.05933
0.06067	3.30E-01	0.06067	0.06067
0.06200	3.40E-01	0.06200	0.06200
0.06333	3.50E-01	0.06333	0.06333
0.06467	3.60E-01	0.06467	0.06467
0.06600	3.70E-01	0.06600	0.06600
0.06733	3.80E-01	0.06733	0.06733
0.06867	3.90E-01	0.06867	0.06867
0.07000	4.00E-01	0.07000	0.07000
0.07133	4.10E-01	0.07133	0.07133
0.07267	4.20E-01	0.07267	0.07267
0.07400	4.30E-01	0.07400	0.07400
0.07533	4.40E-01	0.07533	0.07533
0.07667	4.50E-01	0.07667	0.07667
0.07800	4.60E-01	0.07800	0.07800
0.07933	4.70E-01	0.07933	0.07933
0.08067	4.80E-01	0.08067	0.08067
0.08200	4.90E-01	0.08200	0.08200
0.08333	5.00E-01	0.08333	0.08333
0.08467	5.10E-01	0.08467	0.08467
0.08600	5.20E-01	0.08600	0.08600
0.08733	5.30E-01	0.08733	0.08733
0.08867	5.40E-01	0.08867	0.08867
0.09000	5.50E-01	0.09000	0.09000
0.09133	5.60E-01	0.09133	0.09133
0.09267	5.70E-01	0.09267	0.09267
0.09400	5.80E-01	0.09400	0.09400
0.09533	5.90E-01	0.09533	0.09533
0.09667	6.00E-01	0.09667	0.09667
0.09800	6.10E-01	0.09800	0.09800
0.09933	6.20E-01	0.09933	0.09933
0.10067	6.30E-01	0.10067	0.10067
0.10200	6.40E-01	0.10200	0.10200
0.10333	6.50E-01	0.10333	0.10333
0.10467	6.60E-01	0.10467	0.10467
0.10600	6.70E-01	0.10600	0.10600
0.10733	6.80E-01	0.10733	0.10733
0.10867	6.90E-01	0.10867	0.10867
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0.11133	7.10E-01	0.11133	0.11133
0.11267	7.20E-01	0.11267	0.11267
0.11400	7.30E-01	0.11400	0.11400
0.11533	7.40E-01	0.11533	0.11533
0.11667	7.50E-01	0.11667	0.11667
0.11800	7.60E-01	0.11800	0.11800
0.11933	7.70E-01	0.11933	0.11933
0.12067	7.80E-01	0.12067	0.12067
0.12200	7.90E-01	0.12200	0.12200
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0.12467	8.10E-01	0.12467	0.12467
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0.12867	8.40E-01	0.12867	0.12867
0.13000	8.50E-01	0.13000	0.13000
0.13133	8.60E-01	0.13133	0.13133
0.13267	8.70E-01	0.13267	0.13267
0.13400	8.80E-01	0.13400	0.13400
0.13533	8.90E-01	0.13533	0.13533
0.13667	9.00E-01	0.13667	0.13667
0.13800	9.10E-01	0.13800	0.13800
0.13933	9.20E-01	0.13933	0.13933
0.14067	9.30E-01	0.14067	0.14067
0.14200	9.40E-01	0.14200	0.14200
0.14333	9.50E-01	0.14333	0.14333
0.14467	9.60E-01	0.14467	0.14467
0.14600	9.70E-01	0.14600	0.14600
0.14733	9.80E-01	0.14733	0.14733
0.14867	9.90E-01	0.14867	0.14867
0.15000	1.00E-00	0.15000	0.15000
0.15133	1.00E-00	0.15133	0.15133
0.15267	1.00E-00	0.15267	0.15267
0.15400	1.00E-00	0.15400	0.15400
0.15533	1.00E-00	0.15533	0.15533
0.15667	1.00E-00	0.15667	0.15667
0.15800	1.00E-00	0.15800	0.15800
0.15933	1.00E-00	0.15933	0.15933
0.16067	1.00E-00	0.16067	0.16067
0.16200	1.00E-00	0.16200	0.16200
0.16333	1.00E-00	0.16333	0.16333
0.16467	1.00E-00	0.16467	0.16467
0.16600	1.00E-00	0.16600	0.16600
0.16733	1.00E-00	0.16733	0.16733
0.16867	1.00E-00	0.16867	0.16867
0.17000	1.00E-00	0.17000	0.17000
0.17133	1.00E-00	0.17133	0.17133
0.17267	1.00E-00	0.17267	0.17267
0.17400	1.00E-00	0.17400	0.17400
0.17533	1.00E-00	0.17533	0.17533
0.17667	1.00E-00	0.17667	0.17667
0.17800	1.00E-00	0.17800	0.17800
0.17933	1.00E-00	0.17933	0.17933
0.18067	1.00E-00	0.18067	0.18067
0.18200	1.00E-00	0.18200	0.18200
0.18333	1.00E-00	0.18333	0.18333
0.18467	1.00E-00	0.18467	0.18467
0.18600	1.00E-00	0.18600	0.18600
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0.19800	1.00E-00	0.19800	0.19800
0.19933	1.00E-00	0.19933	0.19933
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0.20200	1.00E-00	0.20200	0.20200
0.20333	1.00E-00	0.20333	0.20333
0.20467	1.00E-00	0.20467	0.20467
0.20600	1.00E-00	0.20600	0.20600
0.20733	1.00E-00	0.20733	0.20733
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0.21000	1.00E-00	0.21000	0.21000
0.21133	1.00E-00	0.21133	0.21133
0.21267	1.00E-00	0.21267	0.21267
0.21400	1.00E-00	0.21400	0.21400
0.21533	1.00E-00	0.21533	0.21533
0.21667	1.00E-00	0.21667	0.21667
0.21800	1.00E-00	0.21800	0.21800
0.21933	1.00E-00	0.21933	0.21933
0.22067	1.00E-00	0.22067	0.22067
0.22200	1.00E-00	0.22200	0.22200
0.22333	1.00E-00	0.22333	0.22333
0.22467	1.00E-00	0.22467	0.22467
0.22600	1.00E-00	0.22600	0.22600
0.22733	1.00E-00	0.22733	0.22733
0.22867	1.00E-00	0.22867	0.22867
0.23000	1.00E-00	0.23000	0.23000
0.23133	1.00E-00	0.23133	0.23133
0.23267	1.00E-00	0.23267	0.23267
0.23400	1.00E-00	0.23400	0.23400
0.23533	1.00E-00	0.23533	0.23533
0.23667	1.00E-00	0.23667	0.23667
0.23800	1.00E-00	0.23800	0.23800
0.23933	1.00E-00	0.23933	0.23933
0.24067	1.00E-00	0.24067	0.24067
0.24200	1.00E-00	0.24200	0.24200
0.24333	1.00E-00	0.24333	0.24333
0.24467	1.00E-00	0.24467	0.24467
0.24600	1.00E-00	0.24600	0.24600
0.24733	1.00E-00	0.24733	0.24733
0.24867	1.00E-00	0.24867	0.24867
0.25000	1.00E-00	0.25000	0.25000
0.25133	1.00E-00	0.25133	0.25133
0.25267	1.00E-00	0.25267	0.25267
0.25400	1.00E-00	0.25400	0.25400
0.25533	1.00E-00	0.25533	0.25533
0.25667	1.00E-00	0.25667	0.25667
0.25800	1.00E-00	0.25800	0.25800
0.25933	1.00E-00	0.25933	0.25933
0.26067	1.00E-00	0.26067	0.26067
0.26200	1.00E-00	0.26200	0.26200
0.26333	1.00E-00	0.26333	0.26333
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0.26600	1.00E-00	0.26600	0.26600
0.26733	1.00E-00	0.26733	0.26733
0.26867	1.00E-00	0.26867	0.26867
0.27000	1.00E-00	0.27000	0.27000
0.27133	1.00E-00	0.27133	0.27133
0.27267	1.00E-00	0.27267	0.27267
0.27400	1.00E-00	0.27400	0.27400
0.27533	1.00E-00	0.27533	0.27533
0.27667	1.00E-00	0.27667	0.27667
0.27800	1.00E-00	0.27800	0.27800
0.27933	1.00E-00	0.27933	0.27933
0.28067	1.00E-00	0.28067	0.28067
0.28200	1.00E-00	0.28200	0.28200
0.28333	1.00E-00	0.28333	0.28333
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0.28733	1.00E-00	0.28733	0.28733
0.28867	1.00E-00	0.28867	0.28867
0.29000	1.00E-00	0.29000	0.29000
0.29133	1.00E-00	0.29133	0.29133
0.29267	1.00E-00	0.29267	0.29267
0.29400	1.00E-00	0.29400	0.29400
0.29533	1.00E-00	0.29533	0.29533
0.29667	1.00E-00	0.29667	0.29667
0.29800	1.00E-00	0.29800	0.29800
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0.30200	1.00E-00	0.30200	0.30200
0.30333	1.00E-00	0.30333	0.30333
0.30467	1.00E-00	0.30467	0.30467
0.30600	1.00E-00	0.30600	0.30600
0.30733	1.00E-00	0.30733	0.30733
0.30867	1.00E-00	0.30867	0.30867
0.31000	1.00E-00	0.31000	0.31000
0.31133	1.00E-00	0.31133	0.31133
0.31267	1.00E-00	0.31267	0.31267
0.31400	1.00E-00	0.31400	0.31400
0.31533	1.00E-00	0.31533	0.31533
0.31667	1.00E-00	0.31667	0.31667
0.31800	1.00E-00	0.31800	0.31800
0.31933	1.00E-00	0.31933	0.31933
0.32067	1.00E-00	0.32067	0.32067
0.32200	1.00E-00		

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5 REPLICATIONS

LIGHT LEVEL	SAMPLE TIME	1.00E-04	3.00E-04	9.00E-04	9.00E-04	9.00E-04
	052000	C52040	052100	052200	052300	052400
LIGHT LEVEL	8.00E-04	1.00E-03	1.00E-03	1.00E-03	1.00E-03	1.00E-03
SAMPLE TIME	060100	060200	060214	060300	060400	060500
LIGHT LEVEL	4.70E-01	1.21E-02	1.07E-03	1.07E-03	1.00E-04	1.00E-04
SAMPLE TIME	060600	060700	060800	060900	061000	061100
LIGHT LEVEL	1.00E-04	1.00E-04	1.00E-04	1.00E-04	1.00E-04	1.00E-04
SAMPLE TIME	061113	061123	061137	061200	061300	061400
LIGHT LEVEL	1.00E-04	1.00E-04	1.62E-03	5.15E-01	1.91E-01	1.00E-03
SAMPLE TIME	061500	061600	061700	061800	061900	062000
LIGHT LEVEL	1.00E-03	1.00E-03	1.00E-03	1.00E-03	1.00E-03	1.00E-03
SAMPLE TIME	062100	062200	062300	070000	070100	070200
LIGHT LEVEL	1.00E-03	1.00E-03	6.92E-04	7.62E-01	8.58E-01	1.31E-02
SAMPLE TIME	070300	070400	070500	070600	070442	070700
LIGHT LEVEL	1.00E-03	1.00E-03	070900			

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Table 6-1, Target Number System (Sheet 1)

- WATER CAN EVENT - DAY 01
 - 1 - TRUCK (ROUND TRIP)
 - 2 - MEN + WATER CANS
 - 3 - LIT CIGARETTES
- AMMO CARRIERS - DAY 02
 - 4 - MEN
- STAR CLUSTER EVENT - DAY 02
 - 5 - TRUCK (ROUND TRIP)
 - 6 - FLARE (COLUMN)
- TRUCK/AMMO EVENT - DAY 03
 - 7 - TRUCK + TAILGATE BANGING
 - 8 - LIT CIGARETTES
- SMOKE AT SUNRISE EVENT - DAY 03
 - 9 - MEN
 - 10 - SMOKE COLUMN
- RADAR ANTENNA DISASSEMBLY - DAY 03
 - 11 - TRUCK (ROUND TRIP)
 - 12 - MEN
 - 13 - CIGARETTE SMOKE (COLUMN)
- RADAR ANTENNA ASSEMBLY - DAY 03
 - 14 - TRUCK (ROUND TRIP)
 - 15 - MEN
 - 16 - CIGARETTE SMOKE (COLUMN)
- SECURITY PATROL (A-LOOPS) - DAY 03
 - 17 - TRUCK (DELIVERY)
 - 18 - PATROL THROUGH LOOPS
- MUDFLAP CARRIERS - DAY 04
 - 19 - TRUCK (DELIVERY)
 - 20 - PATROL THROUGH LOOPS (C-TRAIL)
- AGGRESSOR TENT
 - 21 - TWO PATROLS LEAVING
 - 22 - LIT CIGARETTE
 - 23 - CROW'S NEST PATROL (A74)
 - 24 - TWO TRUCKS (PICK-UP)

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Table 6-1, Target Setting System (Sheet 2)

- EXECUTE WEAPON EVENTS DAY 04
 - 25 - TRUCK (DELIVERY)
 - 26 - PATROL
- SECURITY PATROL (A-LOOPS) - DAY 04
 - 27 - TRUCK (DELIVERY)
 - 29 - PATROL (A-1 TO A-41)
 - 30 - PATROL (A-49 TO A-62)
- * • WATER CAN EVENT - DAY 04
 - 28 - TRUCK (ROUND TRIP)
- NOODLE CARRIERS - DAY 05
 - 31 - PATROL (C-LOOPS)
 - 32 - TWO PATROLS LEAVING AGGRESSOR TENT
 - 33 - LIT CIGARETTE
 - 34 - CROW'S NEST PATROL
 - 35 - TWO TRUCKS (PICK-UP)
- * • STAR CLUSTER EVENT - DAY 05
 - 36 - TRUCK (ROUND TRIP)
 - 37 - FLARE
- HE PAD EVENT - DAY 06
 - 38 - TRUCK (ROUND TRIP)
 - 39 - MEN
 - 40 - STROBE LIGHT
 - 41 - LANDING LIGHTS
- * • PASSING TRUCKS - DAY 06
 - 42 - AMMO TRUCK
 - 43 - RADAR DISASSEMBLY TRUCK
- LASER EXERCISE - DAY 06
 - 44 - BEACON
- * • PASSING TRUCKS - DAY 06 AND 07
 - 45 - RADAR ASSEMBLY TRUCK
 - 46 - LOOP PATROL TRUCK
 - 47 - NOODLE CARRIER TRUCK
 - 48 - TWO TRUCKS FOR PICK-UP
- ROAD PATROL EVENT - DAY 07
 - 49 - TRUCK (ONE-WAY)
 - 50 - PATROL
 - 51 - CIGARETTE SMOKE (COLUMN)

* EVENTS PLANNED FOR A SECOND PATROL IN THE TEST, THAT PRESENT DETECTION OPPORTUNITIES FOR THE FIRST PATROL.

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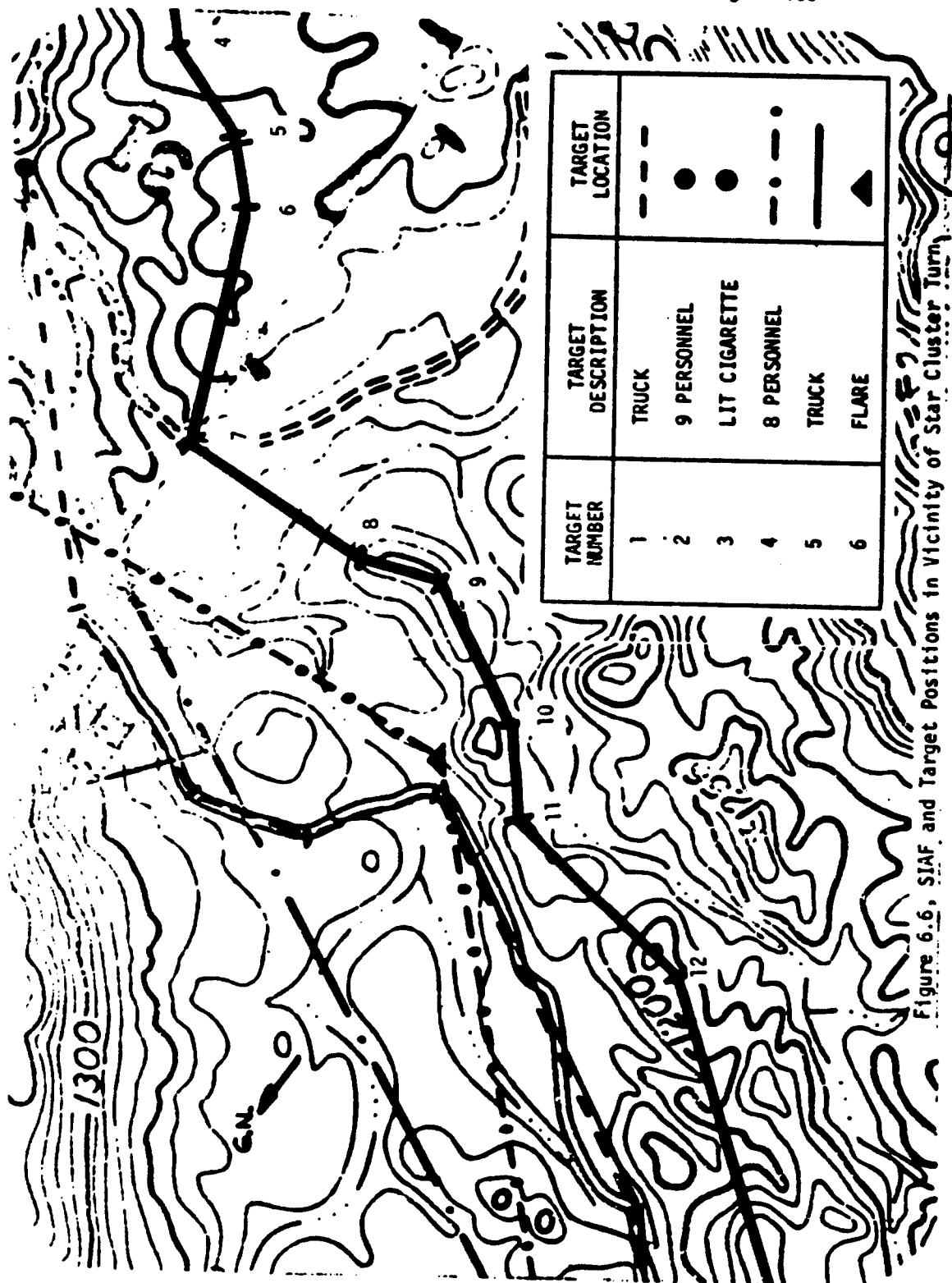


Figure 6-6, SIAF and Target Positions in Vicinity of Star Cluster Turn

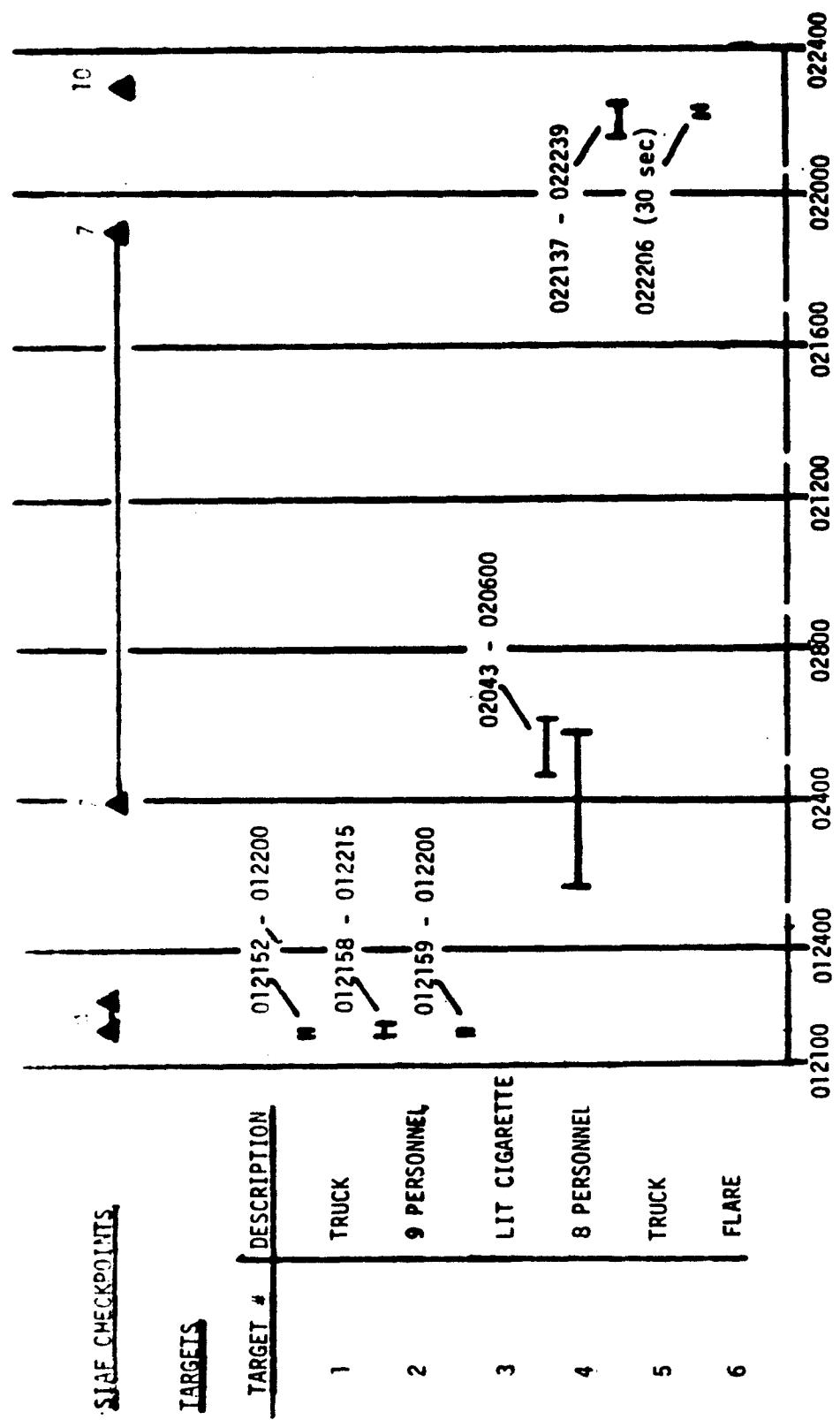


Figure 6.7. Timeline Diagram for Selected Portion of the Scenario

6.5 USER INPUT FOR THE COMBAT MODEL SAMPLE CASE

As an example of the operation of the integrated reconnaissance and combat model including the additions made in the modification contract, the following case is presented. Figure 6.8 shows the namelist input used for this case. The area of operations is taken from the Hunter Liggett Military Reservation. The scenario calls for a SIAF patrol of eight men on an ambush mission. They are moving in the dry El Piojo Creek bed at 0800. The scenario is diagrammed in Figure 6.9. The target starts on the other side of an 80 foot hill approximately 600 meters away. The target is a six-man patrol and is heading on a collision course with the SIAF.

6.6 OUTPUTS FOR THE COMBAT MODEL SAMPLE CASE

The outputs of the model, shown in Figure 6.10, consist of detail and summary printout. The detailed printout begins with the location of the target and of the SIAF. Two lines of printout are generated by the Reconnaissance model at the end of each segment. This gives the positions, a detection verdict, the time, and the reason for no line of sight.

At 17 minutes into the mission, the SIAF detects the target. This is shown by point 1 on Figure 6.9. It is in an area of both vegetation and microrelief. The output then shows the generation of a dynamic route to seek recognition of the target. The grid plot shows the selected grid points for the dynamic route. One minute later, the SIAF identifies the target. The range is 264 meters. This is shown by point 2 on Figure 6.9 for both the SIAF and target. At this point, a dynamic route is generated to return to the original route should that be the decision of the SIAF.

The action selected by the decision logic submodel is to continue to ambush. A preliminary deployment point and engagement point is selected which is the first admissible point. The optimization logic then selects deployment points for both a base of fire and a moving maneuver unit. These are shown by the pair of points labelled number 3 at the edge of the wooded area. The projected engagement point for the target is also shown. The optimization logic also determines an assault point close to the target.

At this point in the simulation, the terrain resolution is shifted from 50.8 meters to 12.7 meters for greater accuracy in the line of sight calculations. The individual attributes are then printed for both patrols

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at the start of combat. The next computation is the generation of dynamic routes for the attacker maneuver units to the deployment points.

The combat model through its executive routine, CMAIN, then assumes control of the simulation. This is driven by the first occurrence of a detection, arrival at the checkpoint (generated by dynamic route routine), casualty, or 20 seconds if nothing else happens. For other missions, it considers also the arrival of an external fire support burst and the detonation of Claymore mines. For this case, the first few events are individual detections by SIAF members of target members. More detections could be occurring, but only one is printed per patrol at each event interval. Here the locations of the maneuver unit leaders are also printed. The next two events are arrivals at the intermediate dynamic route points. This process continues until both maneuver units have arrived at their deployment points. At this time, they stop. A dynamic route is generated for the moving maneuver unit to get to the assault point, but movement does not begin on this leg for an ambush until the firefight has begun. The model continues to print detection events for the attacker of the defender while the defender is moving to the engagement point.

When the defender arrives at the engagement point, the SIAF opens fire and a casualty event occurs within 2 seconds. As shown in the printout, the casualty is defender number 5 who sustains a minor wound. The next event is another casualty. This time defender 2 sustains a major wound. The elapsed time of the firefight is 3.3 seconds. The attribute tables for both patrols are then printed as they are after either a major wound or death. At this time, the defender decides to withdraw and selects a direction 180° opposite to which it was moving. The break decision was due to the high number of casualties.

At the five second point, defender number 3 is killed. The break decision printout is repeated for information purposes, but no new action is taken. The next event is a major wound for defender 1 at 6.2 seconds. At 7.8 seconds, defender 6 is killed and at 9.7 seconds, defender 4 is killed. At this point all defenders have been killed or wounded. The SIAF stops firing and the moving maneuver unit reaches the first checkpoint on its assault route.

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At 30 seconds, however, the SIAF decides to break due to an elapsed time criterion. A rally point is selected on the opposite side of the hill and the SIAF begins moving. After arriving at the rally point, the patrol decides to continue the reconnaissance mission. The final attributes are printed and control is returned to the Reconnaissance Model. At this time, the elevation data at the 50.8 meter resolution is retrieved. The SIAF then completes its operations plan and is extracted. Summary statistics for the mission are then printed.

6.7 EXAMPLE USING EXTERNAL FIRE SUPPORT

The same case was run using external fire support in preparation for the firefight. The same inputs were used except the mission was changed to attack. The same deployment and engagement points were selected, but this time a volley of artillery shells arrived soon after the request. Figure 6.12 shows the detailed output from there on. First the burst points are printed and then the attributes after the burst. The next event is a casualty inflicted by the SIAF who open fire after the first volley. The next events are arrivals of more volleys of artillery. Again the target decides to break in the opposite direction. The attacker decides to break due to the elapsed time criterion.

6.8 EXAMPLE USING CLAYMORE MINES

For this case, the mission was switched to an ambush using Claymore mines. As shown in Figure 6.13, the mines were deployed just inside the edge of the wooded area. The SIAF was deployed in the woods and was not detected by the target. When the target reached the most vulnerable area with respect to the mines, they were detonated and all of the target personnel were killed. Control then returned to the Reconnaissance model after the withdrawal. The detailed output is shown in Figure 6.14.

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SNA4L1	=	1.85.
AA	=	0..
AEO	=	0..
ALIM	=	30001.. 3..001.. 10..0.. 100..
ALLB	=	5000..
ALLF	=	75.. 241.. 0.75.. 201..
ALLW	=	3036..
ANGIO	=	12..
AOXMAX	=	2400..
AOYMAX	=	7200..
AMWTAB	=	360.08.. 340.04.. 280.6.. 460.07.. 1.0.3.1.0.06.200.0249.
ATER	=	0..
ATTAR	=	4..
ATTEN	=	0.03.. 0.09.. 0.15.. 0.12..
BE	=	25..
BSAREA	=	20..
COMRES=15..	=	
CONCAP	=	0.0735..
CPRAT	=	1700.. -700.. 600.. -1200.. -550.. -50.. -600..
CRFCOG	=	1..
DACK	=	150..
DMT	=	0.. 25.. 75.. 25.. 260.. 75.. 900.. 1000.. 600..
DRICE	=	0.3..
DSTEP	=	20..
DSW11	=	1..
DSW12=1..	=	
DYMT=1..1..3..3..-1..1..1..0..-1..0..0..-2..0..1..1..50..0..2..-3..4..0..1	=	
FWRAT	=	300.. 500.. 003.. 400.. 450.. 350.. 337..
GR	=	25..
H	=	0.. 1.. 1.5.. 3.. 8*0.. 0.5.. 2*0.. 0.7..
		450.. 3.. 251.. 3.. 25.. 353.. 252.. 4.. 0..
		440.. 2.. 25.. 5.. 4.. 1.. 75.. 11.. 16.. 0.. 3.. 2.. 0..
		4*3.. 10.. 12.. 15.. 20.. 15.. 18.. 24.. 30.. 3.. 5.. 2.. 0..
HR	=	-1.. -0.5.. -4.. 1.8.. -0.8.. 4.. 2.. 2*0..
HMT	=	0.. -3.25.. 2*-J.5.. 2*J.. 3.25.. 0.5.. 5*J.. 0.25.. 1..
IDT1M	=	1..
ISECT11=1..2..3..4..1..2..3..1..4..1..2..1..3..1..2..3..4..1..1..2..3..4..1..2..3..	=	
ITACNS	=	900..
ITDRP4	=	60..
ITDTRA	=	120..
ITNTAK	=	30..

Figure 6.8. Combat Sample Case Narrative Inputs

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NPARTS	=	900.
TP150	=	120.
IHWAT	=	350.
IVMAT	=	301.
LAMDAF	=	1000..
NPARTS	=	9.
P	=	760..
PNC	=	25..
PHR	=	25..
PO	=	760..
PJ	=	42..
RC	=	4..
RCTAR	=	10..
RECREES	=	50..
REF	=	0..3.. 0..3.. J..13.. 0..13.. 4..0..3.. 4..0..0..9.. J..17.. 0..15.. 2..0..2..
		2..0..3.. 2..0..13.. 3..0..35.. 0..3.. 4..0..0..9.. 0..17.. 2..15.. 2..0..2..
		3..0..1.. 2..0..13.. 0..0..4.. 0..0..3.. 3..0..0..2.. 1.. 0..0..6.. 0..2.. 1..,
REQ	=	0..
RESMAX	=	12..7..
RHOH	=	0..075..
RHOI	=	0.. 500.. 667.. 120.. 4..0.. 18.. 2..0.. 5..
		4..0.. 135.. 250.. 500.. 0.. 1200.. 250.. 500.. 1000.. 20.. 1000..
		50.. 0.. 4..0.. 70.. 140.. 300.. 600.. 30.. 200.. 350.. 600.. 0..
		100.. 260.. 4..0.. 70.. 140.. 300.. 600.. 30.. 200.. 350.. 600.. 0..
		100.. 2..0.. 100.. 36.. 72.. 36.. 100.. 10.. 32.. 16.. 10.. 50.. 2..10..
RMAX	=	100.. 36.. 20.. 10.. 8..100.. 10.. 2..100.. 10..
		4..0..100.. 75.. 30.. 12.. 1.. 12.. 1.. 18.. 1.. 10.. 100.. 80..
		2..10..0.. 0..
RMAX	=	200.. 100.. 50.. 2..20.. 100.. 50.. 5..200.. 150.. 50..
RPE	=	0..24..
RPG	=	0..5..
RTFR	=	0..
SECT	=	5..9..0..785..0..7d5.. 2..35.. 3..93.. 5..64.. 2..35.. 3..93..
		4..72.. 1..57.. 0.. 2..3..1..4.. 0.. 1..37.. 4..72..
SEGMIN	=	1..
SGMTAB	=	50..
SGMTAB	=	203..
SIGFFR	=	3..0..0..0..0..0..0..1103..
SL1	=	0..0..0..5..
SL2	=	0..0..5..
SNILF	=	0..d.. .45.. .8.. .75.. .1.. .02.. .6.. .5.. .6.. 3..01.. 4..9..9..

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SIS	= 95.
TAR	= 536.
	- .1. .25. .5. .75. 1.. 1.25. .301.5. 1.15. .8. .5. .35.
	- .15. .05. .35. .25. .2. .5. 1.. 1.5. .20. .5. .303.0. .2.3.
	- 1.6. 1.. .7. .3. .1. .38.35. - 1.6. - 1.4. - 1.2. - 1.. -.8.
	- .6. - 4. - 2. 0.. .2. .9. .6. .0. 1.. 1.2. 1.4. 1.6. 1.8.
VEGC	= 15.
	- 1.5. 1.. 3. .35. .30. .55. .30. .0.5. 10. .0.85. 3. .35. .28.
	- 56. .31. .0.5.
	- .0.7. 3.. 31.. 26.. 51.. 32.. 0.5. 2.. 0.40. 2.. 30.. 25.. 58..
	- 33.. 0.5.
	- .5. .0.85. .3. .29. .24. .36. .33. .0.45. .18. .0.80. .3. .28.
	- 23. .59. .33. .0.4.
	- 7.5. .0.7. 2.. 27. .22. .37. .32. .0.35. .7.5. 0.65. 2.. 25.
	- 20. .55. .30.. 0.3.
	- 1.. J.20. 2.. 25. .9. 20.. 60.. 36.. 3.2. 2.. 0.43. 2.. 28..
	- 23. .56. .32.. 0.3.
	- 1.3. .0.30. 1.. 27. .22. .38. .33. .0.25. 1.. 0.2. 1.. 25..
	- 20.. 60.. 34.. 0.2.
	- 2.. 0.3. 1.. 30.. 25.. 62.. 35.. 0.5. 1.. 0.2. 1.. 28.. 29..
	- 63.. 35.. 34..
	- 2.. .9. 3.. 40.. 35.. 57.. 32.. 0.4. 10.. 0.2.. 0.. 40..
	- 35.. 61.. 34.. 0.5.
VEGF	= 1.
	- .05. .7. .4. .0.85. .0.8. .7. .0.65. .2. .0.4. .3. .2.
	- .3. .2. .9. .2.
VISLUM	= 4000.
	- 15000.. 13000.. 10000.. 2000.. 500.. 300.. 50..
	- 10000.. 5000.. 100.. 100.. 100.. 500.. 100.. 10..
	- 240.. 10.. 1.. 1.. 5.. 1.. 0.. 1.. 244.. 1.. 0.. 0.. 0.. 0.. 0..
	- 280.0001. 0.00008. 0.00002. 0.00002. 0.00008. 0.00005. 0.00002. 0.00001.
	- 280.001. 0.00008. 0.00002. 0.00008. 0.00005. 0.00002. 0.00001.
	- 280.004. 0.0003. 0.008. 0.003. 0.002. 0.006. 0.004.
	- 280.01. 0.008. 0.002. 0.008. 0.005. 0.002. 0.001.
VISM	= 13.
VISMW	= 300..
VIVP=3.	
	- 0.. 1.. 1.5. 10.. 80.. 20.. 280.. 50..
	- 480.. 2.. 241.. 0.. 42.. 1.. 2.. 10.. 3..
	- 480.. 380.. 0.3. 0.45. 0.2. 200.. 0.62. 0.. 0.5. 20..
	- 480.. 3.. 3.5.. 4.. 4.5.. 2.. 4.. 6.5.. 5.. 0.. 2.. 2*3..
WAT	= 0.. 5.. 4.. 240.. 5.. 40.. 50.. 0.. 2.. 2*3..
MR	= 0.5.
XLP	= 381.. 0.95. 0.9. 0.55. 3.15. 0.01. 0.5. 0.25. 0.1. 1.. 0.75.
	- 0.95. 1..

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SNAME2	= 40..
BETA	= 100..
BLIFE	= 100..
DDDA=0..	
DDDB=0..	
DDDC=0..	
DDDA7	= 2..
DDDV	= 1..
DPE	= 10..
DSA=0..	
DSAA=0..	
EQUIP	= 0..
EMANC	= 0..
F11.11	= 1..
FOOD	= 13.47..
FORMS	= 200..0..
FORM1	= 800..0..
FREQ	= 50..
GSAPRJ	= 20..
GSAPXX	= 20..
ML2	= 36.00..
M20	= 26.96..
ICL(1)	= 5.3.5..
ICPER	= 3600..
IDELA=1..	
IDEB=1..	
IDELC=1..	
IDELD=1..	
IDELF=1..	
LOOMST	= 3..
IFADJ	= 20..0..
IFSD=0..	
IFSUP	= 20..0..
IFSUP(1)	= 1..
IDR=560..	
IFT=20..0..	
IP05	= 1..
IPREP	= 0..
ISEN	= J..
ISFNL7=0..	
ISTAY(1..1)=3*0..1..	
ITARIV(1..1)=4..7..	

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ITAC1	51.352.1691.
ITMAX	=01000000.
ITMOV(1,1)	=3*0.01083700.
ITAC(1)	=1,2,1
IVSTAV(1,1)	=3*0.0002000.
ITZERO	= 01000000.
IX1	= 334432395.
IX2	= 363975447.
JSTART	=0.
JSTOP	=0.
JWF	=1.
LNRL	=0.
KREC(1)	=3*1.
MAE(1)	=400..
MAXCAS	= 1.
MAXREP	=1.
NICKI	=1.
MODE	= 1.
NOAT	=2.
NC0(1)	=3,4,3.
NCOPV	=1.
NOECOV	= 0.
NFTX	= 1.
NHANOG	=0.
NL2	= 1.
NAMES	=0.
NN(1)	=36.
NOB	= 0.
NP LAN(1)	=7.
NRAD	= 1.
NRMT	= 2.
NRST	= 0.
NRVP	=1.
NSENS	=0.
NSWT	= 1.
NTAR	=1.
NWCL(1,1)	= 010800. 012000. 020630. 021600. 022000. 030400. 050630. 050900. 051600. 052000. 060630. 060900. 061600. 062000.
070630. 070900. 100300.	
NWCL(1,2)	= 2, 1, 5, 1, 2, 1, 3, 1, 5, 1, 2, 1, 3, 1, 2, 1, 1.
PEQUIP	=313.46.
PPLS	= 0..

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S S Y E R I S	
RAMU	= 40..
RAV000	= 0..
RAV010	= 0..
RFM000	= 0..
RFM001	= 0..
RFM002	= 0..
RFSA0	= 5..
RFSA1	= 5..
RW20	= 0..
RW21	= 1..
RZ211	= 50..
RNINES	= 0..
RNF	= 10..
RPA	= 25..
RPOUR	= 0.6..
SANU	= 400..
SC(1)	= 1.7..
SC(2)	= 0.5..
SC(3)	= 1..
SC(4)	= 0..
SC(5)	= 0.04..
SC(6)	= 32..
SCALE	= 50000..
SOIL1	= 0..
SPEC	= 0..
TBLSTR	= 60..
TBRNDS	= 30..
TBUR	= 0..
TDEAK	= 400..
TOMIN	= 10..
THEATA	= 0..
TPWRA	= 1.5..
TPREP	= 0..
TSR	= 0554..
TSS	= 1829..
TUSE	= 0.5..
VECI	= 3..
VELM	= 4*100..
VH	= 6302..
VK	= 7146..
MDAY	= 0360.. 0716.. 3760.. 0649.. 0946.. 1346.. 4*1148.. 2045.. 2159..

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2310., 2350., 0014., 0110., 4*156., 5*0., 5*1., 73., 79., 69., 63.,
72., 75., 4*78., 51., 56., 51., 47., 48., 5*52., 98., 97., 98., 85.,
98., 99., 4*98., 20., 23., 40., 22., 20., 26., 4*24., 104., 20., 100.,
3., 4., 2., 5*1., 8., 5., 12., 15., 8., 5*6., 3*300., 300., 190.,
3*360..

MDC = 0..

NDN = 0..

WTC = 1..

HTH = 1..

HTS = 4., 3*0..

YAVODD=0..

XAVOID=0..

XBASE =6345..

XLZ(1) = 6455..

XOBINS = 40..

XMMAX = 6000..

XMB(1,1)=6419.5.6424.5.6419.5.

XOB(1,2)=6417.5.6417.5.50..

XOB(1,3)=6419.5.6424.5.6419.5.

XPLAN(1,1)=6451..6447..6427..6418.6.6427..6447..6451..

YAVODD=0..

YAVOID=0..

YBASE =7240..

YLZ(1) = 7284..

YOB(1,1)=7306..7318.5.7318..5,

YOB(1,2)=7318.5.7321..

YOB(1,3)=7306..7318.5.7318..5,

YPLAN(1,1)=7296..7311..7319..7319..7311..7296..

SNAML3

IDET =20*0..

TVEL=20*0..SUJUND=100*0..NNP=2*0..NSTP=20*3..

IMV(1)= 3. RANMAX(1)= 4000.. FRCMVN(1)= 1..

TVEL(1)= 0.3. NNP(1)= 1.. ITS(1)= 3108000. ITS(1)= 3200000.

ITIM(1,1)= 01081600.01092000.

GOALX(1,1)=6442..

GOALY(1,1)=7341..

TC(1,1)=6392..7301..1.7..5.1..6..0..32..

NSIP(1)= 1.. ISSUN(1,1)= 01080000. 01221500..

ISSOFF(1,1)= 02080000. 0122210..

RCHW(1)= 200.. REWAX(1)= 1500..

SOUND(1,1)= 90.. 43..

6

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CADW	= .4.
CARFA	= .5.
CI	= .3.
CS	= .3.
CC1	= .90..
CC2	= .90..
CC3	= .50..
CLASS	= 2.2.1.1.1. 2.2.1.1.1. 1.1.1.1.1. 0.0.0.0.0. 0.0.0.0.0.
OTEF5	= 300..
OTENGH	= 3600..
OTDAM	= 150..
OTDATR	= 120..
OTFNS	= 300..
OTPUNK	= 3600..
ONDR	= 300..
FRAMS	= 7.
FRAFF	= .9.
GMAX	= .3.
GSAPAR	= 50..
IDIREC	= 1.
IPERH1	= 1.
LDAYS	= 4..
NSECTY	= 6.
NSECTR	= 3.
PPI	= .1.
PP2	= .3.
PP3	= .3.
PP4	= .5.
PP5	= .95.
Q1	= .33.
Q2	= .33.
Q3	= .34.
RAMB	= 100..
RAMIN	= .6.
RATT	= 100..
RFFS	= 500..
RURS	= 600..
RSP	= 10..
RZ	= .5.

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(4)

SAFDIS=15.;
JARTL=1.
MAFE(1)=14..12.6.11.3.9.0.11.3.9.0.0.0.0.
NSUPP=1.
SIGMDIS=15..
KDEFOP=4..

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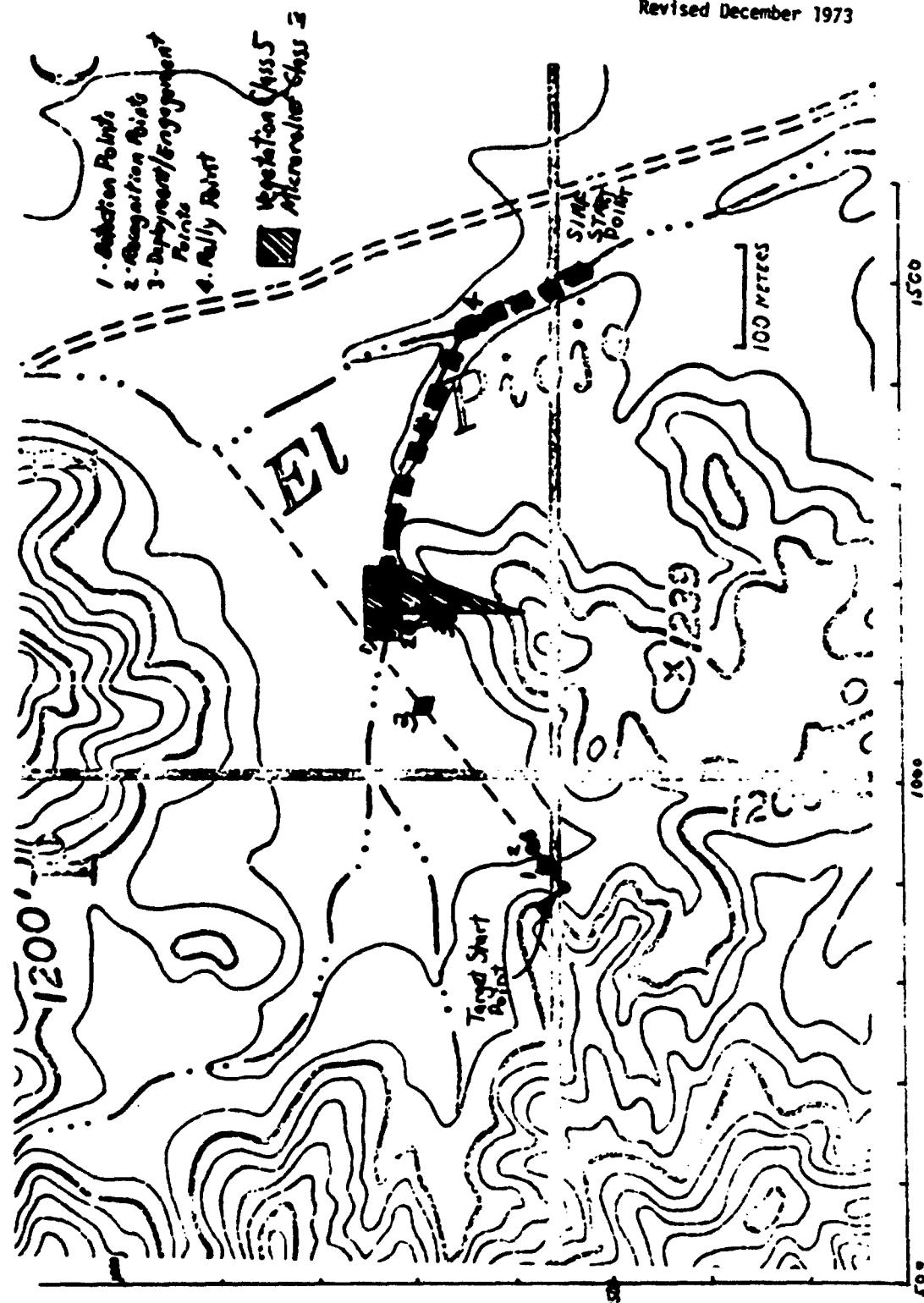


Figure 6.9. Sample Case Diagram

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ESTABLISHING A FINAL SENSE OF STABILITY IN THE TEENS

Figure 6.10. Sample Case Output

TARGET DETECTED DYNAMIC ROUTE TO SCREEN RECOGNITION
R,V COORDINATES IN EACH MOVEMENT FOR THE 1144-1444 THIS MU.

X,MN	V,MN	Y,MN
1168.39	1732.00	
1143.08	1703.92	
1147.39	1693.54	
1131.69	1683.16	
1126.39	1657.08	
1100.31	1662.39	
1084.62	1652.00	
1068.93	1621.62	
1053.24	1631.24	
1037.54	1620.85	
1021.85	160.47	
1006.16	1600.09	
984.78	1563.82	
960.47	1525.31	
959.09	1508.96	
943.39	1558.25	
917.32	1563.82	

STATISTICS ON ABOVE DYNAMIC ROUTE
NUMBER OF POINTS IN THE ROUTE : 17

SIAF POSITION: X - 1167.82 Y - 1727.20	TARGET DETECTED: YES	TIME: 0455-01	ROUTE: 1144-1444
SIAF DETECTS TARGET NO. 1 USUALLY	TARGET DEFECTED: YES	TIME: 0455-01	ROUTE: 1144-1444
SIAF POSITION: X - 1163.08 Y - 1703.92	TARGET DEFECTED: YES	TIME: 0455-01	ROUTE: 1144-1444
SIAF DETECTS TARGET NO. 1 USUALLY	TARGET DEFECTED: YES	TIME: 0455-01	ROUTE: 1144-1444
SIAF RECOGNIZED TARGET NO. 1 AT X - 1163.08 Y - 1703.92 THE RECOGNITION RANGE IS 26.8			

DYNAMIC ROUTE TO RETURN TO XXI WHICH PI UP DIGITAL QUOTE IN DISTRI

X,Y COORDINATES IN EACH MOVEMENT FOR THE LEADS OF THIS MU.

X,CY	Y,VY	PI
1163.08	1703.42	
1165.04	1705.22	
1167.00	1706.22	
1168.96	1707.42	
1170.92	1709.12	
1171.26	1710.75	
1171.59	1712.36	
1171.92	1714.01	
1172.25	1715.64	
1172.58	1717.26	
1172.91	1718.89	
1173.25	1720.52	
1173.58	1722.15	
1172.28	1724.12	
117C.98	1726.C8	
1165.68	1728.04	
1168.39	1730.00	

STATISTICS ON ABOVE DYNAMIC ROUTE
NUMBER OF POINTS IN THE ROUTE : 17

MISSION IS -- AMASH OR AVOID

THE COURSE OF ACTION FOR STAB TO TAKE :

STAF DECIDES TO CHT. ON TO AMASH

SIAF IS TO BE THE SUBJECT PATROL

ENGAGEMENT POINT X = 1177.1343 Y = 1702.3624

FOR MANEUVER UNIT NUMBER 1, 010, IT COMPUTES APPROXIMATE PATH

1164 1173 174C
1691 1662 1677

FOR MANEUVER UNIT NUMBER 2, IT ALSO COMPUTES APPROXIMATE PATH

116C 1177
171E 1682

ENGAGEMENT POINT 1177.04 1692.15
A 128.8V EFFECT ANGLE HAS BEEN SET AT X= 220.60V, LEVEL 0.0
RESOLUTION HAS BEEN CHANGED TO 0.1M PER LEVEL OF 12.7 METERS

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PATROL MEMBER STATISTICS BEFORE COMBAT

ATTACKER PATROL:

PATROL MEMBER

	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER									
WEAPON TYPE	M-16(SA)	M-16(SA)	M-16(SA)	M-16(A1)	M-16(G)	M-16(SA)	M-16(SA)	M-16(SA)	0
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	0
CASUALTY STATUS	NU	NU	NU	NU	NU	NU	NU	NU	0
PIRING STATUS	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	0
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METERS)	1160.48	1163.89	1163.89	1163.89	1165.72	1165.72	1166.12	1166.65	0.00
CURRENT Y (METERS)	1716.14	1691.46	1711.61	1720.43	1727.62	1724.86	1696.44	1693.63	0.00
NEXT X (METERS)	0.30	0.03	0.00	0.00	0.30	0.30	0.30	0.30	0.00
NEXT Y (METERS)	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.00
HEIGHT (METERS)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WEIGHT (METERS)	.50	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	0.00
MOVING STATUS	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	0.00
MANEUVER UNIT	1	2	2	2	2	2	2	2	0
ROUNDS REMAIN (MAUL)	0	0	0	0	0	0	0	0	0
FUNCTION IN PATROL	P.L.	A.P.L.	KIPLIFEL MAN	M.GUNNER	G-1 GUNNER	G-1 GUNNER	RIFLEMAN	RIFLEMAN	0
MOVEMENT RATE (M/S/SEC)	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.41	0.00
INDIV. ASSIGNMENT	HARVE FR.	AD. UVIT HASE FU.	HASE FR.	DASE FR.	HASE FR.	DASE FR.	P. UNIT	P. UNIT	0.00
INITIAL (4TH) SUPPLY	100	100	100	100	100	100	100	100	0
WEAPON TYPE	APR-A	APR-A	APR-A	APR-A	APR-A	APR-A	APR-A	APR-A	0
POSIT. IN FIRE TEAM	1	1	1	1	1	1	1	1	0
SECONDARY WEAPON AVAIL	HO. GREN.	HO. GREN.	HO. GREN.	HO. GREN.	HO. GREN.	HO. GREN.	HO. GREN.	HO. GREN.	0
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	2	2	2	2	2	2	2	0

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DYNAMIC ROUTE FOR ATTACKER MU¹
X,Y COORDINATES ON EACH MOVEMENT FOR THE LEADER OF THIS MU.
XCYN YDYN
1163.89 1691.46
1168.58 1677.16
1173.28 1662.86
STATISTICS ON ABOVE DYNAMIC ROUTE
NUMBER OF POINTS IN THE PICTURE : 3

DYNAMIC ROUTE FOR ATTACKER MU²
X,Y COORDINATES ON EACH MOVEMENT FOR THE LEADER OF THIS MU.
XCYN YDYN
1166.48 1715.14
1166.03 1649.29
1177.19 1682.44
STATISTICS ON ARC OF DYNAMIC ROUTE
NUMBER OF POINTS IN THE ROUTE : 7

Time Recitation: F.P.

TIME HRS. MIN. SEC. X Y

		POSITION (ATTACKER)		EVENT	
TIME	HRS. MIN. SEC.	X	Y		
POSITION OF ATTACKER MU 1	X- 1164.79	Y- 1688.72			
POSITION OF ATTACKER MU 2	X- 1162.32	Y- 1712.42			
POSITION OF DEFENDER MU 1	X- 934.69	Y- 1577.75			
1 8 18 31	1164.79	1588.72	DETECTION	ATTACKER MEMBERS: 4 DETECTS DEFENDER MEMBER: 2	
POSITION OF ATTACKER MU 1	X- 1165.69	Y- 1685.97			
POSITION OF ATTACKER MU 2	X- 1163.61	Y- 1709.83			
POSITION OF DEFENDER MU 1	X- 937.03	Y- 1579.63			
1 8 18 41	1165.69	1685.97	DETECTION	ATTACKER MEMBERS: 7 DETECTS DEFENDER MEMBER: 1	
POSITION OF ATTACKER MU 1	X- 1166.59	Y- 1683.23			
POSITION OF ATTACKER MU 2	X- 1164.89	Y- 1707.24			
POSITION OF DEFENDER MU 1	X- 937.38	Y- 1581.50			
1 8 19 51	1166.59	1683.23	DETECTION	ATTACKER MEMBERS: 4 DETECTS DEFENDER MEMBER: 6	
POSITION OF ATTACKER MU 1	X- 1167.49	Y- 1683.48			
POSITION OF ATTACKER MU 2	X- 1166.17	Y- 1704.65			
POSITION OF DEFENDER MU 1	X- 941.72	Y- 1583.38			
1 8 19 1	1167.49	1680.48	DETECTION	ATTACKER MEMBER: 8 DETECTS DEFENDER MEMBER: 6	
POSITION OF ATTACKER MU 1	X- 1167.90	Y- 1679.05			
POSITION OF ATTACKER MU 2	X- 1166.86	Y- 1703.30			
POSITION OF DEFENDER MU 1	X- 942.94	Y- 1584.36			
1 8 19 0	1167.95	1679.35	MOVEMENT	ATTACKER MU 1 WILL MOVE 1.51 METERS AT AN ANGLE OF -71	
1 8 19 6	1166.86	1703.30	MOVEMENT	ATTACKER MU 2 WILL MOVE 1.51 METERS AT AN ANGLE OF -6	
POSITION OF ATTACKER MU 1	X- 1168.57	Y- 1677.19			
POSITION OF ATTACKER MU 2	X- 1167.71	Y- 1701.55			
POSITION OF DEFENDER MU 1	X- 944.53	Y- 1585.62			
1 8 19 12	1168.57	1677.19	MOVEMENT	ATTACKER MU 1 WILL MOVE 1.96 METERS AT AN ANGLE OF -71	
1 8 19 12	1167.71	1701.55	MOVEMENT	ATTACKER MU 2 WILL MOVE 1.96 METERS AT AN ANGLE OF -6	
POSITION OF ATTACKER MU 1	X- 1169.47	Y- 1674.44			
POSITION OF ATTACKER MU 2	X- 1159.00	Y- 1698.96			
POSITION OF DEFENDER MU 1	X- 943.07	Y- 1587.50			
1 8 19 22	1169.47	1674.44	DETECTION	ATTACKER MEMBERS: 3 DETECTS DEFENDER MEMBER: 5	
POSITION OF ATTACKER MU 1	X- 1170.38	Y- 1671.7C			
POSITION OF ATTACKER MU 2	X- 1170.28	Y- 1695.17			

POSITION OF DEFENDER MU 1		POSITION OF DEFENDER MU 2		DETECTION		ATTACKER MEMBER: 6 DETECTS DEFENDER MEMBER: 4	
1	19	32	1170.38	1671.70	1590.37		
POSITION OF ATTACKER MU 1	X- 1171.28	Y- 1666.95					
POSITION OF ATTACKER MU 2	X- 1171.56	Y- 1693.78					
POSITION OF DEFENDER MU 1	X- 951.32	Y- 1591.23					
POSITION OF ATTACKER MU 1	X- 1171.28	Y- 1666.95	DETECTION	ATTACKER MEMBER: 3 DETECTS DEFENDER MEMBER: 1			
POSITION OF ATTACKER MU 2	X- 1172.18	Y- 1666.21					
POSITION OF DEFENDER MU 1	X- 953.90	Y- 1593.12					
1	19	52	1172.18	1666.21	DETECTION	ATTACKER MEMBER: 7 DETECTS DEFENDER MEMBER: 4	
POSITION OF ATTACKER MU 1	X- 1173.08	Y- 1663.47					
POSITION OF ATTACKER MU 2	X- 1174.13	Y- 1688.61					
POSITION OF DEFENDER MU 1	X- 956.24	Y- 1594.99					
1	20	2	1173.08	1663.47	DETECTION	ATTACKER MEMBER: 4 DETECTS DEFENDER MEMBER: 5	
POSITION OF ATTACKER MU 1	X- 1173.13	Y- 1663.31					
POSITION OF ATTACKER MU 2	X- 1176.20	Y- 1688.46					
POSITION OF DEFENDER MU 1	X- 956.32	Y- 1595.06					
1	6	20	2	1173.13	1663.31	MOVEMENT	ATTACKER MU 1 WILL MOVE .10 METERS AT AN ANGLE OF -7°
1	8	20	2	1174.20	1668.46	MOVEMENT	ATTACKER MU 2 WILL MOVE .10 METERS AT AN ANGLE OF -6°

DYNAMIC ROUTE FOR ATTACKER MU 1
X,Y COORDINATES ON EACH MOVEMENT FOR THE LEADER OF THIS MU.

X,Y,MN

Y,DW

1173.13 1663.31

1156.54 1663.93

1139.94 1668.59

1125.98 1687.83

1109.39 1690.47

109C15 1676.51

109C15 1676.51

STATISTICS ON ABOVE DYNAMIC ROUTE
 NUMBER OF POINTS IN THE ROUTE : 6

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31

POSITION OF ATTACKER MU 2 X- 1175.49 Y- 1685.87

POSITION OF DEFENDER MU 1 X- 958.67 Y- 1296.93

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31 DETECTION ATTACKER MEMBER: 6 DETECTS DEFENDER MEMBER: 6

POSITION OF ATTACKER MU 2 X- 1173.13 Y- 1663.31

POSITION OF DEFENDER MU 1 X- 960.68 Y- 1298.54

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31 MOVE MENT

ATTACKER MU 1 WILL MOVE 0.00 METERS AT AN ANGLE OF -71

POSITION OF DEFENDER MU 1 X- 1177.04 Y- 1682.74

POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1682.74

POSITION OF DEFENDER MU 1 X- 963.02 Y- 1600.42

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31

POSITION OF DEFENDER MU 1 X- 965.36 Y- 1602.29

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31 DETECTION ATTACKER MEMBER: 4 DETECTS DEFENDER MEMBER: 6

POSITION OF ATTACKER MU 2 X- 1173.13 Y- 1663.31

POSITION OF DEFENDER MU 1 X- 970.00 Y- 1606.04

POSITION OF DEFENDER MU 2 X- 967.71 Y- 1604.17

POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31 DETECTION ATTACKER MEMBER: 1 DETECTS DEFENDER MEMBER: 6

POSITION OF ATTACKER MU 2 X- 1173.13 Y- 1663.31

POSITION OF DEFENDER MU 1 X- 1063.31 Y- 1663.31 DETECTION ATTACKER MEMBER: 1 DETECTS DEFENDER MEMBER: 6

POSITION OF ATTACKER MU 2 X- 1173.13 Y- 1663.31

POSITION OF DEFENDER MU 1 X- 1177.04 Y- 1682.74

POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1682.74

POSITION OF DEFENDER MU 1 X- 972.39 Y- 1607.91

POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1682.74

POSITION OF DEFENDER MU 1 X- 1173.13 Y- 1663.31 DETECTION ATTACKER MEMBER: 7 DETECTS DEFENDER MEMBER: 2

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POSITION OF ATTACKER MU 1 X- 1173•13 V- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 974•73 V- 1609•79
POSITION OF DEFENDER MU 2 X- 1173•13 1663•31 DETECTION
ATTACKER MEMBER: 2 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 977•08 V- 1611•66
POSITION OF DEFENDER MU 2 X- 1173•13 1663•31 DETECTION
ATTACKER MEMBER: 3 DEFENDERS MEMBER: 1
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•76
POSITION OF DEFENDER MU 1 X- 979•42 V- 1613•54
POSITION OF DEFENDER MU 2 X- 1177•04 V- 1682•76
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31 DETECTION
ATTACKER MEMBER: 5 DEFENDERS MEMBER: 6
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31 DETECTION
ATTACKER MEMBER: 5 DEFENDERS MEMBER: 6
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31 DETECTION
ATTACKER MEMBER: 5 DEFENDERS MEMBER: 6
POSITION OF DEFENDER MU 1 X- 981•76 V- 1615•41
POSITION OF DEFENDER MU 2 X- 1177•04 V- 1682•76
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31 DETECTION
ATTACKER MEMBER: 7 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 1 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 984•10 V- 1617•28
POSITION OF DEFENDER MU 2 X- 1177•04 V- 1682•74
POSITION OF ATTACKER MU 1 X- 1173•13 1663•31 DETECTION
ATTACKER MEMBER: 8 DEFENDERS MEMBER: 5
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 986•45 V- 1619•16
POSITION OF DEFENDER MU 2 X- 1177•04 1663•31 DETECTION
ATTACKER MEMBER: 3 DEFENDERS MEMBER: 1
POSITION OF ATTACKER MU 1 X- 1173•13 V- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 991•13 V- 1621•91
POSITION OF DEFENDER MU 2 X- 1177•04 1663•31 DETECTION
ATTACKER MEMBER: 6 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 993•49 V- 1621•91
POSITION OF DEFENDER MU 2 X- 1177•04 1663•31 DETECTION
ATTACKER MEMBER: 3 DEFENDERS MEMBER: 1
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 995•49 V- 1621•91
POSITION OF DEFENDER MU 2 X- 1177•04 1663•31 DETECTION
ATTACKER MEMBER: 4 DEFENDERS MEMBER: 1
POSITION OF ATTACKER MU 1 X- 1173•13 Y- 1663•31
POSITION OF ATTACKER MU 2 X- 1177•04 V- 1682•74
POSITION OF DEFENDER MU 1 X- 997•49 V- 1621•91
POSITION OF DEFENDER MU 2 X- 1177•04 1663•31 DETECTION
ATTACKER MEMBER: 4 DEFENDERS MEMBER: 1

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POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1024.87	Y-	1649.89	
1 8 24 54 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 2 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1027.21	Y-	1651.77	
1 6 25 6 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 3 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	
POSITION OF DEFENDER MU 1 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1029.95	Y-	1653.64	
1 8 25 16 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 3 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1031.09	Y-	1655.52	
1 6 25 24 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 3 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1034.09	Y-	1657.39	
1 6 25 34 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 7 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1037.05	Y-	1659.64	
1 6 25 46 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 3 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1039.39	Y-	1661.91	
1 6 25 56 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 3 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1041.73	Y-	1663.39	
1 6 26 16 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 4 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1046.08	Y-	1665.26	
1 6 26 20 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 4 DEFENDERS MEMBER: 3
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	
POSITION OF DEFENDER MU 1 X-	1045.07	Y-	1667.12	
1 6 26 23 POSITION OF ATTACKER MU 1 X-	1173.13	Y-	1663.31	DETECTION
POSITION OF DEFENDER MU 1 X-	1173.13	Y-	1663.31	ATTACKER MEMBER: 4 DEFENDERS MEMBER: 4
POSITION OF ATTACKER MU 2 X-	1177.06	Y-	1662.74	

POSITION OF DEFENDER MU 1 X- 1043.76 Y- 1009.01		ATTACKER MEMBER: 3 DETECTS DEFENDER MEMBER: 3	
1 6 26 30	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1051.10 Y- 1670.86			
1 6 26 40	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1053.45 Y- 1672.76			
1 6 26 56	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1055.79 Y- 1676.63			
1 6 27 6	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1058.13 Y- 1676.31			
1 6 27 16	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1060.47 Y- 1676.36			
1 6 27 26	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1062.01 Y- 1666.29			
1 6 27 36	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1063.16 Y- 1666.13			
1 6 27 46	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1067.50 Y- 1664.00			
1 6 27 56	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1069.84 Y- 1665.86			
1 6 28 5	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1662.74			
POSITION OF DEFENDER MU 1 X- 1072.19 Y- 1687.75			
1 6 28 16	1173.13 1663.31	DETECTION	
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31			

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POSITION OF ATTACKER MU 1 X- 1173.12 Y- 1662.31
POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1692.74
POSITION OF DEFENDER MU 1 X- 1674.53 Y- 1689.52
1 8 2 9 11 12 13 1683.31 0177.C11A
POSITION OF ATTACKER MU 1 X- 1173.13 Y- 1663.31
POSITION OF ATTACKER MU 2 X- 1177.06 Y- 1682.76
POSITION OF DEFENDER MU 1 X- 1674.07 Y- 1689.57

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1 DEFENDER 6 28 29 CASUALTY EVENT
THE NUMBER OF THE CASUALTY MEMBER IS : 5
THE TYPE OF CASUALTY IS : W.I.N.D.
TIME(SEC) THAT OPERATION HAS BEEN UNDER WAY: 1.8720
POSITION : X- 1175.13 Y- 1655.31
POSITION OF ATTACKER : X- 1172.37 Y- 1663.43
POSITION OF DEFENDER : X- 1177.05 Y- 1662.74
POSITION OF DEFENDER : X- 1075.30 Y- 1690.24

1 DEFENDER 8 28 29 CASUALTY EVENT
THE NUMBER OF THE CASUALTY MEMBER IS : 2
THE TYPE OF CASUALTY IS : W.I.N.D.
TIME(SEC) THAT OPERATION HAS BEEN UNDER WAY: 3.2854
POSITION : X- 1172.37 Y- 1663.43

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DEFENSE POSITION	WEAPON TYPE	1	2	3	4	DEFENSE POSITION	WEAPON TYPE	1	2	3	4
CURRENT AMMO SUPPLY	AT-47	AT-47	AT-47	AT-47	AT-47	CURRENT AMMO SUPPLY	AT-47	AT-47	AT-47	AT-47	AT-47
CASUALTY STATUS	100	100	100	100	100	CASUALTY STATUS	100	100	100	100	100
FIRING STATUS	ARMED	ARMED	ARMED	ARMED	ARMED	FIRING STATUS	ARMED	ARMED	ARMED	ARMED	ARMED
SUPPRESSIVE SUPPORT	0.00	0.00	0.00	0.00	0.00	SUPPRESSIVE SUPPORT	0.00	0.00	0.00	0.00	0.00
CURRENT X (METERS)	1072.18	1078.42	1089.55	1094.55	1098.42	CURRENT X (METERS)	1072.18	1078.42	1089.55	1094.55	1098.42
CURRENT Y (METERS)	1070.14	1086.49	1098.55	1104.55	1109.55	CURRENT Y (METERS)	1070.14	1086.49	1098.55	1104.55	1109.55
NEXT X (METERS)	1070.14	1086.49	1098.55	1104.55	1109.55	NEXT X (METERS)	1070.14	1086.49	1098.55	1104.55	1109.55
NEXT Y (METERS)	1070.00	1086.00	1098.00	1104.00	1109.00	NEXT Y (METERS)	1070.00	1086.00	1098.00	1104.00	1109.00
HEIGHT (METERS)	1070.00	1086.00	1098.00	1104.00	1109.00	HEIGHT (METERS)	1070.00	1086.00	1098.00	1104.00	1109.00
WIDTH (METERS)	0.50	0.50	0.50	0.50	0.50	WIDTH (METERS)	0.50	0.50	0.50	0.50	0.50
CURRENT PICTURE	STANDBY	STANDBY	STANDBY	STANDBY	STANDBY	CURRENT PICTURE	STANDBY	STANDBY	STANDBY	STANDBY	STANDBY
MOVING STATUS	UPPERED	UPPERED	UPPERED	UPPERED	UPPERED	MOVING STATUS	UPPERED	UPPERED	UPPERED	UPPERED	UPPERED
MANEUVER UNIT	1	1	1	1	1	MANEUVER UNIT	1	1	1	1	1
ROUNDS REMAIN (WAD)	20	20	20	20	20	ROUNDS REMAIN (WAD)	20	20	20	20	20
MOVEMENT RATE (M/S)	0.00	0.00	0.00	0.00	0.00	MOVEMENT RATE (M/S)	0.00	0.00	0.00	0.00	0.00
INDIV. ASSIGNMENT	0.00	0.00	0.00	0.00	0.00	INDIV. ASSIGNMENT	0.00	0.00	0.00	0.00	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	INITIAL AMMO SUPPLY	100	100	100	100	100
WEAPON TYPE	AT-47	AT-47	AT-47	AT-47	AT-47	WEAPON TYPE	AT-47	AT-47	AT-47	AT-47	AT-47
POSITION IN FIRST TIER	1	1	1	1	1	POSITION IN FIRST TIER	1	1	1	1	1
SECONDARY WEAPONS AVAILABILITY	0.00	0.00	0.00	0.00	0.00	SECONDARY WEAPONS AVAILABILITY	0.00	0.00	0.00	0.00	0.00
NO. OF HANDED GRENADE	0	0	0	0	0	NO. OF HANDED GRENADE	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	NO. OF SMOKE GRENADE	0	0	0	0	0

BREAK DECISION: DEFENDER BREAKS CONTACT WITH THE ENEMY CASUALTY RATE AT 3.6103

DEFENDER BREAKS	ATTACKER POSITION	ATTACKER POSITION	ATTACKER POSITION	ATTACKER POSITION
WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL
WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL
WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL
WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL	WITARAWAHL

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1 2.9 2.9 USUALTY EVENT
DEFENDER PAY 4 JL SUSTAINS THE NEXT CASUALTY
THE NUMBER OF THE CASUALTY IS 4851 3
THE TYPE OF CASUALTY IS : DEATH
TIME(SEC) THAT COUNTER UPDATING HAS BEEN UNDERTAKEN : 00.0625
POSITION : X- 1171.53 Y- 1663.56

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DEFENDER PATROL	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER									
WEAPON TYPE	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47
CURRENT AMMO SUPPLY	99	100	99	100	99	100	99	100	99
CASUALTY STATUS	NO. KILLED	NO. WOUNDED	NO. KILLED						
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSSION STATUS	0	0	0	0	0	0	0	0	0
CURRENT X (METERS)	1074.93	1072.18	1078.35	1058.68	1081.18	1071.81	1063.81	1071.81	1063.81
CURRENT Y (METERS)	1664.46	1694.14	1696.34	1697.75	1662.14	1693.65	1662.14	1693.65	1662.14
NEXT X (METERS)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT Y (METERS)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEIGHT	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
CURRENT POSTURE	TRUCK	PHONE	PHONE	PHONE	PHONE	PHONE	PHONE	PHONE	PHONE
MOVING STATUS	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	1	1	1	1	1	1	1	1	1
ROUNDS REPAIRED (MAG.)	14	20	19	23	20	19	23	20	19
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT PATTERN (M/S SEC)	30	30	30	30	30	30	30	30	30
INDIV. ASSIGNMENT	BASE FA.	BASE FA.	BASE FA.						
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AK-4	AK-4	AK-4	AK-4	AK-4	AK-4	AK-4	AK-4	AK-4
POSITION IN FIRE TEAM	1	2	3	4	5	6	7	8	9
SECONDARY WEAPONS	AVI	AVI	AVI	AVI	AVI	AVI	AVI	AVI	AVI
NO. OF HAND GRENADES	0	0	0	0	0	0	0	0	0
NO. OF SHOTGUN SHELLS	0	0	0	0	0	0	0	0	0

AREAK DECISION : DEFENDER PATROL BREAKS CONTACT WITH HIGH CASUALTY FACTION
 POSITION OF ATTACKER : X- 1170.9; Y- 1654.6A
 POSITION OF ATTACKER : X- 1177.0; Y- 1652.7A
 POSITION OF DEFENDER : X- 1170.1; Y- 1651.7C
 POSITION OF DEFENDER : X- 1170.1; Y- 1651.7C

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1. *Classification of Casualty*
2. *Differences between Casualty and Non-Casualty*
3. *The Relation of Casualty to the Casualty Index*
4. *Types of Casualty*
5. *Classification of Casualty*
6. *Classification of Casualty*
7. *Classification of Casualty*

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ATTACKER TEAM CASUALTY SUSTAINED

ATTACKER PATROL:	PATROL NUMBER								
	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER									
WEAPON TYPE	4-16(SA)	4-16(SA)	4-16(SA)	M-16(A)	M-79	GL	4-16(SA)	M-16(SA)	1
CURRENT AMMO SUPPLY	36	36	89	89	2	36	96	96	0
CASUALTY STATUS	NC	NC	NU	NU	ND	ND	NC	NU	0
FIRING STATUS	POINT	POINT	POINT	POINT	POINT	POINT	POINT	POINT	0
SUPPRESSION STATE	0	0	0	0	5	5	0	0	0
CURRENT X (METERS)	1177.06	1170.82	1176.36	1177.57	1175.73	1178.16	1169.56	1172.22	0.00
CURRENT Y (METERS)	1662.74	1663.68	1678.44	1687.50	1676.72	1692.39	1658.60	1668.31	0.00
NEXT X (METERS)	1177.19	1156.54	1176.73	1177.67	1176.22	1176.16	1158.23	1158.87	0.00
NEXT Y (METERS)	1662.44	1665.95	1677.46	1687.61	1672.48	1692.39	1661.26	1670.66	0.00
HEIGHT (METERS)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METERS)	*2.0	*5.0	*5.0	*5.0	*5.0	*5.0	*5.0	*5.0	0.00
CURRENT PCSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	0.00
MOVING STATUS	STOPPED	HALT	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	0.00
MANEUVER UNIT	2	1	2	2	2	2	1	1	0
ROUNDS REMAIN (AGS)	16	16	16	16	16	16	16	16	16
PRODUCTION RATE IN PATRUL	P.L.	A.P.L.	K.IFLEMAN	K.GUNNER	G.R.I.NCH.	RIFLEMAN	RIFLEMAN	RIFLEMAN	0
MOVEMENT RATE (M/SEC)	0.30	0.34	0.30	0.00	0.00	0.00	0.54	0.56	0.00
INDIV. ASSIGNMENT	BASE F9	M. UNIT	BASE FR.	BASE FR.	BASE FA.	BASE FA.	P. UNIT	M. UNIT	0
INITIAL APMD SUPPLY	130	100	100	100	100	100	100	100	0
WEAPON TYPE	AREA	AREA	AREA	4FA	AREA	AREA	AREA	AREA	0
POSIT. IN FIRE TEAM	1	1	2	3	4	5	2	3	0
SECONDARY WEAPON AVI	H. GREEN	H. GREEN	H. GREEN	H. GREEN	H. GREEN	H. GREEN	H. GREEN	H. GREEN	0
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	2	3	0	0	0	0	0	0

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DEFENSE STATUS	1	2	3	4	5	6	7	8	9	10	11	12	13	14
FIRE TEAM NUMBER	4	1	4	1	4	1	4	1	4	1	4	1	4	1
WEAPON TYPE	AK-47													
CURRENT AMMO SUPPLY	99	220	133	98	133	103	133	103	133	103	133	103	133	103
CASUALTY STATUS	MAINTAINING POSITION													
FIRING STATUS	N/A													
SUPPRESSION STATUS	100%+5.2	100%+1.6	100%+0.5	100%+3.7	100%+0.5	100%+3.7	100%+0.5	100%+3.7	100%+0.5	100%+3.7	100%+0.5	100%+3.7	100%+0.5	100%+3.7
CURRENT X (METERS)	1080.70	1090.14	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50
CURRENT Y (METERS)	1070.70	1070.14	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50
NEXT X (METERS)	1080.70	1090.14	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50	1080.36	1090.50
NEXT Y (METERS)	1070.70	1070.14	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50	1070.36	1070.50
HEIGHT (METERS)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METERS)	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20	1.20
CURRENT POSITION	PHONE													
MOVING STATUS	STOPPED													
MANEUVER UNIT	1	1	1	1	1	1	1	1	1	1	1	1	1	1
ROUNDS REMAIN (MAG.)	19	20	20	18	20	20	18	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN											
MOVEMENT RATE (M/S EC)	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30	.30
INITIAL ASSIGNMENT	BASE F-4													
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA													
POSIT. IN FIRE TEAM	1	2	3	4	5	6	7	8	9	10	11	12	13	14
SECONDARY WEAPON AVAIL	NONE													
NO. OF PANG GRENADE	0	0	0	0	0	0	0	0	0	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	0	0	0	0	0	0	0	0	0

BREAK DECISION : DIFFERENCE BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

AREAS OF CLASH & DEFENSE BREAKS CONTACT DUE TO HIGH CASUALTY FRACTION

POSITION OF ATTACKER : 1 X- 1070.57 Y- 1063.91

POSITION OF ATTacker : 2 X- 1077.0 Y- 1062.74

POSITION OF DEFENDER : 4 X- 1074.62 Y- 1064.70

1. H-2A CASUALTY REPORT
DEFINITION: PATIENT SUSTAINS THE NEXT CASUALTY
THE NUMBER OF THE CASUALTY REPORT IS: 0
THE TYPE IS: SURVIVOR
TIME(SPECIFIC) THAT THIS INCIDENT HAS BEEN UNDERTAKEN: 10.0000
POSITION: X- 1154.97 Y- 166.01

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ATTACHMENT:

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1 24 42 CASUALTY EVENT
DEFENDER PART OF SUSTAINING THE PART CASUALTY
THE NUMBER OF CASUALTY IS : 4
THE TYPE OF CASUALTY IS : RECAP
TIME(S) THAT COMBAT ACTION HAS BEEN UNDERTAKEN
POSITION : X- 116.36 Y- 166.57 9.6705

ATTACKER TABLE AFTER CASUALTY SUSTAINED

ATTACKER PATROL:	1	2	3	4	5	6	7	8	9
PATROL MEMBER:	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1
WEAPON TYPE	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI	P-161 SAI
CURRENT AMMO SUPPLY	94	94	94	94	94	94	94	94	94
CASUALTY STATUS	NO	NO	NO	NO	NO	NO	NO	NO	NO
BATTALION STATUS	POINT	POINT	POINT	POINT	POINT	POINT	POINT	POINT	POINT
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1177.04	1168.94	1176.36	1177.57	1179.73	1176.16	1167.70	1170.35	1170.35
CURRENT Y (METER)	1682.74	1663.97	1676.44	1687.56	1676.72	1692.36	1659.03	1660.57	1660.57
NEXT X (METER)	1177.19	1156.54	1176.70	1177.67	1176.22	1176.16	1159.20	1154.87	1154.87
NEXT Y (METER)	1682.44	1665.95	1677.46	1687.41	1672.44	1612.29	1661.24	1670.66	1670.66
WEIGHT (MEGTON)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND
Moving Status	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	2	1	2	2	2	2	2	1	1
ROUNDS REPAIR (MG.C.1)	14	14	14	14	2	0	14	14	14
FUNCTION IN PATROL	P.L.	A.P.-L.	AIRFIELD	H. GUNNER	G.R. LMG	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	0.00	0.54	0.00	0.00	0.00	0.00	0.54	0.54	0.54
INDIV. ASSIGNMENT	BASE FR.	%	UNIT BASE FR.	BASE FR.	BASE FR.	BASE FR.	UNIT	UNIT	UNIT
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	2	3	4	5	6	7	8	9
SECONDARY WEAPON AVAIL	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	4
NO. OF SMOKE GRENADE	2	2	0	0	0	0	0	0	0

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DEFENDER PATROL

PATROL MEMBER

FIRE TEAM NUMBER	1	WEAPONS TYPE	AK-47	CURRENT AMMO SUPPLY	100	CASUALTY STATUS	QA. WOUND	FIRING POSITION	MA. SIGHTING	SUPPRESSION STATE	NUT	CURRENT X (METERS)	1074.62	NEXT X (METERS)	1099.70	NEXT Y (METERS)	1099.16	HEIGHT (METERS)	1.70	WIDTH (METERS)	.50	CURRENT POSTURE	PRONE	Moving STATUS	STOPPED	MOVEMENT RATE (M/S)	.15	MANEUVER UNIT	P.L.	FUNCTION IN PATROL	A.P.L. RIFLEMAN	WEAPON TYPE	A.P.L. RIFLEMAN	SECONDARY WEAPON AVI	None	NO. OF HMG GRENADE	0	NO. OF SMOKE GRENADE	0
DEFENDER PATROL	1	WEAPONS TYPE	AK-47	CURRENT AMMO SUPPLY	100	CASUALTY STATUS	DEAD	FIRING POSITION	MA. SIGHTING	SUPPRESSION STATE	NOT HOT	CURRENT X (METERS)	1074.62	NEXT X (METERS)	1099.70	NEXT Y (METERS)	1099.16	HEIGHT (METERS)	1.70	WIDTH (METERS)	.50	CURRENT POSTURE	PRONE	Moving STATUS	STOPPED	MOVEMENT RATE (M/S)	.15	MANEUVER UNIT	P.L.	FUNCTION IN PATROL	A.P.L. RIFLEMAN	WEAPON TYPE	A.P.L. RIFLEMAN	SECONDARY WEAPON AVI	None	NO. OF HMG GRENADE	0	NO. OF SMOKE GRENADE	0
ATTACKER PATROL	1	WEAPONS TYPE	AK-47	CURRENT AMMO SUPPLY	100	CASUALTY STATUS	DEAD	FIRING POSITION	MA. SIGHTING	SUPPRESSION STATE	NOT HOT	CURRENT X (METERS)	1074.62	NEXT X (METERS)	1099.70	NEXT Y (METERS)	1099.16	HEIGHT (METERS)	1.70	WIDTH (METERS)	.50	CURRENT POSTURE	PRONE	Moving STATUS	STOPPED	MOVEMENT RATE (M/S)	.15	MANEUVER UNIT	P.L.	FUNCTION IN PATROL	A.P.L. RIFLEMAN	WEAPON TYPE	A.P.L. RIFLEMAN	SECONDARY WEAPON AVI	None	NO. OF HMG GRENADE	0	NO. OF SMOKE GRENADE	0
ATTACKER PATROL	2	WEAPONS TYPE	AK-47	CURRENT AMMO SUPPLY	100	CASUALTY STATUS	DEAD	FIRING POSITION	MA. SIGHTING	SUPPRESSION STATE	NOT HOT	CURRENT X (METERS)	1074.62	NEXT X (METERS)	1099.70	NEXT Y (METERS)	1099.16	HEIGHT (METERS)	1.70	WIDTH (METERS)	.50	CURRENT POSTURE	PRONE	Moving STATUS	STOPPED	MOVEMENT RATE (M/S)	.15	MANEUVER UNIT	P.L.	FUNCTION IN PATROL	A.P.L. RIFLEMAN	WEAPON TYPE	A.P.L. RIFLEMAN	SECONDARY WEAPON AVI	None	NO. OF HMG GRENADE	0	NO. OF SMOKE GRENADE	0
ATTACKER PATROL	3	WEAPONS TYPE	AK-47	CURRENT AMMO SUPPLY	100	CASUALTY STATUS	DEAD	FIRING POSITION	MA. SIGHTING	SUPPRESSION STATE	NOT HOT	CURRENT X (METERS)	1074.62	NEXT X (METERS)	1099.70	NEXT Y (METERS)	1099.16	HEIGHT (METERS)	1.70	WIDTH (METERS)	.50	CURRENT POSTURE	PRONE	Moving STATUS	STOPPED	MOVEMENT RATE (M/S)	.15	MANEUVER UNIT	P.L.	FUNCTION IN PATROL	A.P.L. RIFLEMAN	WEAPON TYPE	A.P.L. RIFLEMAN	SECONDARY WEAPON AVI	None	NO. OF HMG GRENADE	0	NO. OF SMOKE GRENADE	0

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO HIGH CASUALTY FRACTION

POSITION OF ATTACKER PATROL X- 1159.33 Y- 1665.50
 POSITION OF ATTACKER PATROL 2 X- 1177.04 Y- 1622.74
 POSITION OF DEFENDER PATROL 1 X- 1074.62 Y- 1689.70
 POSITION OF DEFENDER PATROL 2 X- 1074.62 Y- 1689.70
 POSITION OF DEFENDER PATROL 3 X- 1074.62 Y- 1689.70
 ATTACKER MU 1 WILL MOVE 9.75 METERS AT AN ANGLE OF 171°
 ATTACKER MU 2 WILL MOVE 3.00 METERS AT AN ANGLE OF -63°

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BREAK DECISION 1: DEFENDER BREAKS CONTACT DUE TO INADEQUATE FIREPOWER

POSITION OF ATTACKER MU 1 X- 1159.33 Y- 1665.50

POSITION OF ATTACKER MU 2 X- 1177.04 Y- 1682.74

POSITION OF DEFENDER MU 1 X- 1074.62 Y- 1689.70

POSITION OF DEFENDER MU 3 X- 1072.19 Y- 1694.14

1 8 29 NO EVENTS IN 20 SECONDS.

BREAK DECISION 2: ATTACKER BREAKS CONTACT DUE TO EXCESSIVE ELAPSED TIME(FIGHT)

BREAK DECISION 3: DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

BREAK DECISION 4: DEFENDER BREAKS CONTACT DUE TO HIGH CASUALTY FRACTION

IC FOR BREAK CONTACT-AVAILABLE SIEF RALLY POINT 1400 2427
ATTACKER WITHDRAWAL ROUTE 5 1159.33 1460.24

1665.50 1626.89

ATTACKER WITHDRAWAL ROUTE 5 1177.04 1466.74

1682.74 1626.89

POSITION OF ATTACKER MU 2 X- 1165.12 Y- 1679.25

POSITION OF DEFENDER MU 1 X- 1074.00 Y- 1689.70

1 8 33 46 1451.55 1628.73 PROJEC MENT

1 8 33 46 1450.22 1620.13 PROJEC MENT

RESOLUTION AND CONTINUATION OF THE PREVIOUS PHASE LEVEL 16
DECISION 5: CONTINUE THE PREVIOUS PHASE. AFTER WHICH OPERATOR IS COMPUTED:
MISSION: TRAINING: CURRENT ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY:
CURRENT ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY:
CURREN ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY: PREVIOUS ACTIVITY:
PATTERN: PATTERN: PATTERN: PATTERN: PATTERN:

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PATROL WEAPONS STATISTICS AFTER COMBAT

ATTACKER PATROL:

	PATROL MEMBER					
	1	2	3	4	5	6
FIRE TEAM NUMBER						
WEAPON TYPE	M-16(SA)	M-16(SA)	M-16(SA)	M-16(A)	M-16(SA)	M-16(SA)
CURRENT AMMO SUPPLY	94	94	94	82	0	0
CASUALTY STATUS	NU	NU	NU	NU	NU	NU
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0
CURRENT X (METER)	1466.22	1451.55	1465.41	1466.79	1465.95	1467.40
NEXT X (METER)	1626.89	1628.73	1621.90	1631.07	1617.03	1636.96
NEXT Y (METER)	1466.24	1466.24	1465.41	1467.07	1464.59	1623.47
HEIGHT (METER)	1626.69	1626.89	1621.96	1631.62	1617.02	1636.75
WIDTH (METER)	1.70	1.70	1.70	1.70	1.70	1.70
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND
MOVING STATUS	TUP SP.	TUP SP.	TUP SP.	TUP SP.	TUP SP.	TUP SP.
MANEUVER UNIT	2	1	2	2	2	2
ROUNDS REMAIN (MAG.)	14	14	14	14	14	14
PROJECTILES IN PATROL	P.L.	A.P.L.	A.I.R.	GUNNER	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	1.08	1.08	1.08	1.08	1.08	1.08
INDIV. ASSIGNMENT	BASE FR.	N. UNIT	GAGE	G. GUNNER	N. RIFLEMAN	N. RIFLEMAN
INITIAL AMMO SUPPLY	100	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	1	2	3	4	5
SECONDARY WEAPON AVI	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE
NO. OF HAND GRENADE	4	4	4	4	4	4
NO. OF SMOKE GRENADE	2	1	0	0	0	0

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DEFENDER PAYLOAD:		PATROL MEMBERS			
		1	2	3	4
FIREFTEAM NUMBER		1	1	1	1
WEAPON TYPE	AK-47	AK-47	AK-47	AK-47	AK-47
CURRENT AMMO SUPPLY	99	100	98	100	100
CASUALTY STATUS	PA. INJURED	PA. INJURED	DFAD	WI. WOUNDED	DFAD
FLYING STATUS	NOT FLY	NOT FLY	NOT FLY	NOT FLY	NOT FLY
SUPPRESSIVE STATE	0	0	0	0	0
CURRENT X (METER)	1074.62	1072.18	1073.05	1067.34	1066.03
CURRENT Y (METER)	1659.70	1656.14	1656.04	1656.85	1622.04
NEXT X (METER)	0.00	0.00	0.00	0.00	0.00
NEXT Y (METER)	0.00	0.00	0.00	0.00	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70
WIDTH (METER)	.50	.50	.50	.50	.50
CURRENT PC STURE	PRONE	PRONE	PRONE	PRONE	STAND
MOVING STATUS	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	1	1	1	1	1
ROUND'S REMAIN (MAG.1)	19	20	20	18	20
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	.30	.30	.30	.30	.30
TACTICAL ASSIGNMENT	BASE FA.	BASE FA.	BASE FA.	BASE FA.	BASE FA.
INITIAL AMMO SUPPLY	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA
POSITION IN FIRE TEAM	1	2	3	4	5
SECONDARY WEAPON AVI	NONE	NONE	NONE	NONE	NONE
NO. OF HMG GRENADE	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0

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SIAF POSITION: X - 1456.51 Y - 1625.3 TARGET DETECTED: NO TIME: DAYS-01 HOURS-09 MINUTES-01
XSTAR = 932 YSTAR = 1576 LOS = 1
SIAF DETECTS TARGET NO. 1 VISUALLY
SIAF POSITION: X - 1470.05 Y - 1574.83 TARGET DETECTED: NO TIME: DAYS-01 HOURS-09 MINUTES-01
XSTAR = 932 YSTAR = 1576 LOS = 1
SIAF DETECTS TARGET NO. 1 VISUALLY
SIAF POSITION: X - 1473.20 Y - 1563.00 TARGET DETECTED: NC TIME: DAYS-01 HOURS-09 MINUTES-01
XSTAR = 932 YSTAR = 1576 LOS = 1

SIAF POSITION: X - 1483.60 Y - 1524.00 TARGET DETECTED: NJ TIME: DAYS-01 HOURS-09 MINUTES-01
XSTAR = 932 YSTAR = 1576 LOS = 1
SIAF DETECTS TARGET NO. 1 VISUALLY
SIAF POSITION: X - 1490.00 Y - 1500.00 TARGET DETECTED: NC TIME: DAYS-01 HOURS-09 MINUTES-01
XSTAR = 932 YSTAR = 1576 LOS = 1

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TILDE MCVEHAN AT PLOT FIVE SIX

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SIAF SURVEILLANCE STATISTICS (PAGE 1)
HUNTER LIQUET SCENARIO 1
1 REPLICATIONS

UNAIDED VISUAL DETECTION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	1
NUMBER OF DETECTIONS	1
DETECTION SUCCESS RATIO	1.000
DETECTION RANGE (METERS)	
MEAN	301.064
STANDARD DEVIATION	0.000
DETECTION TIME (DAYS, HRS, MINS)	
MEAN	010.817
STANDARD DEVIATION	000.000
DETECTION CUES	
AURAL	0
SENSOR	

IDENTIFICATION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	1
NUMBER OF IDENTIFICATIONS	1
IDENTIFICATION SUCCESS RATIO	1.000
IDENTIFICATION RANGE (METERS)	
MEAN	263.878
STANDARD DEVIATION	0.000
IDENTIFICATION TIME (DAYS, HRS, MINS)	
MEAN	010.817
STANDARD DEVIATION	000.000

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SIAF SURVEILLANCE STATISTICS (PAGE 2)

HUNTER LIGUETT SCENARIO 1

1 REPLICATIONS

AURAL DETECTION STATISTICS OF THE TARGETS BY SIAF

TARGET NUMBER	1
NUMBER OF DETECTIONS	0
DETECTION SUCCESS RATIO	0.000

DETECTION RANGE (METERS)

MEAN	0.000
STANDARD DEVIATION	0.000

DETECTION TIME (DAYS, HRS, MINS)

MEAN	000.000
STANDARD DEVIATION	000.000

TARGET LOCATION STATISTICS

TARGET NUMBER	1
TARGET LOCATION (ECEF METERS)	43.287
MEAN	43.287

STANDARD DEVIATION

STAFF/TARGET SURVEILLANCE STATISTICS (PAGE 5)
HUNTER LIGGETT SCÉNARIO 1
1 REPLICATIONS

CAUSES OF NO DETECTION FOR STAFF (PERCENT)

TARGET NUMBER	1
MASKING BY RELIEF	90.000
MASKING BY VEGETATION	10.000
RANGE AND LIGHT LEVEL	0.000
INSUFFICIENT TIME	0.000

CAUSES OF NO DETECTION FOR TARGETS (PERCENT)

TARGET NUMBER	1
MASKING BY RELIEF	90.000
MASKING BY VEGETATION	10.000
RANGE AND LIGHT LEVEL	0.000
INSUFFICIENT TIME	0.000

SIAF MOVEMENT STATISTICS (PAGE 6)
HUNTER INTELLIGENT SCENARIO I
1 REPPLICATIONS

MOVEMENT RATE (KM/HR)	
MEAN	1.645
STANDARD DEVIATION	.0164
PATROL DURATION (DAY SIM TIME)	
MEAN	0109.06
STANDARD DEVIATION	.000000
DISTANCE TRAVELED (KM)	
MEAN	1.356
STANDARD DEVIATION	0.000
MOVEMENT RATE = HISTOGRAM (KM/HR)	
PERCENT TIME BETWEEN	0.000 - 200 KM/HR = 0.000
PERCENT TIME BETWEEN	200 - 400 KM/HR = 0.000
PERCENT TIME BETWEEN	400 - 600 KM/HR = 0.000
PERCENT TIME BETWEEN	600 - 800 KM/HR = 0.000
PERCENT TIME BETWEEN	800 - 1,000 KM/HR = 0.000
PERCENT TIME BETWEEN	1,000 - 1,200 KM/HR = 0.000
PERCENT TIME BETWEEN	1,200 - 1,400 KM/HR = 0.000
PERCENT TIME BETWEEN	1,400 - 1,600 KM/HR = 0.595
PERCENT TIME BETWEEN	1,600 - 1,800 KM/HR = .081
PERCENT TIME BETWEEN	1,800 - 2,000 KM/HR = .323
PERCENT TIME BETWEEN	2,000 - 2,200 KM/HR = .000
PERCENT TIME BETWEEN	2,200 - 2,400 KM/HR = 0.000
PERCENT TIME BETWEEN	2,400 - 2,600 KM/HR = 0.000

SIAF NAVIGATION STATISTICS (PAGE 7)

HUNTER LIGGETT SCENARIO

1 REPLICATIONS

PATROL CEP AT CHECKPOINT 14 (METERS)

MEAN	41.515
STANDARD DEVIATION	12.09

TIME TO DETERMINE LOCATION (MIN)

MEAN	7.50
STANDARD DEVIATION	0.00

SIAF INSERTION STATISTICS

INSERTION ATTEMPTS

NUMBER OF SUCCESSFUL INSERTIONS	NUMBER OF INSERTIONS AT PRIMARY LL	NUMBER OF INSERTIONS AT SEC. LL	INSERTION TIME (DAYS, HRS, MINS)
1	1	0	000800

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STAR COMMUNICATION STATISTICS (RAUSE - 4) HUNTER LIGGETT SCENARIO I 1 REPLICATIONS

EXTRACRITICAL COMMUNICATIONS

ATTENUATION		STANDARD DEVIATION		1.000		0.000	
COMMUNICATION SUCCESS RATE		STANDARD DEVIATION		1.000		0.000	
AVERAGE PC/P LOSSES FOR COMM FAILURE		PERCENT		0.000		0.000	
ATTENAUATION DUE TO RELIEF	0.000	ATTENAUATION DUE TO VEGETATION	0.000	ATTENAUATION DUE TO RANGE	0.000	ATTENAUATION DUE TO RANGE	0.000
TOTAL TIME RECEIVING (DAYS, HOURS, MINUTES)		0000050		0000000		0000000	
TOTAL TIME TRANSMITTING (DAYS, HOURS, MINUTES)		0000001		0000000		0000000	
AMPERE HOURS AVAILABLE		130.000		0.000		0.000	
AMPERE HOURS USE		510		0.000		0.000	

SIAS HUMAN MAINTENANCE STATISTICS PAGE 101
 HUMAN PERFORMANCE SCENARIO I
 1 REPLICATIONS

	BEGINNING	END	MAX	MIN	AVERAGE
HUMAN PERFORMANCE DEGRADATION	0.0	0.004	0.004	0.000	0.002
MEAN	0.0	0.000	0.003	0.000	0.000
STANDARD DEVIATION	0.0	0.000	0.004	0.000	0.002
ENERGY EXPENDED (BTU)					
MEAN	0.0	846.215	846.215	0.000	442.342
STANDARD DEVIATION	0.0	0.000	0.030	0.000	0.000
TIME HISTORY OF HUMAN PERFORMANCE DEGRADATION (FIRST REPLICATION ONLY)					
TIME	010801	010801			
PERF. DEG.	.300				

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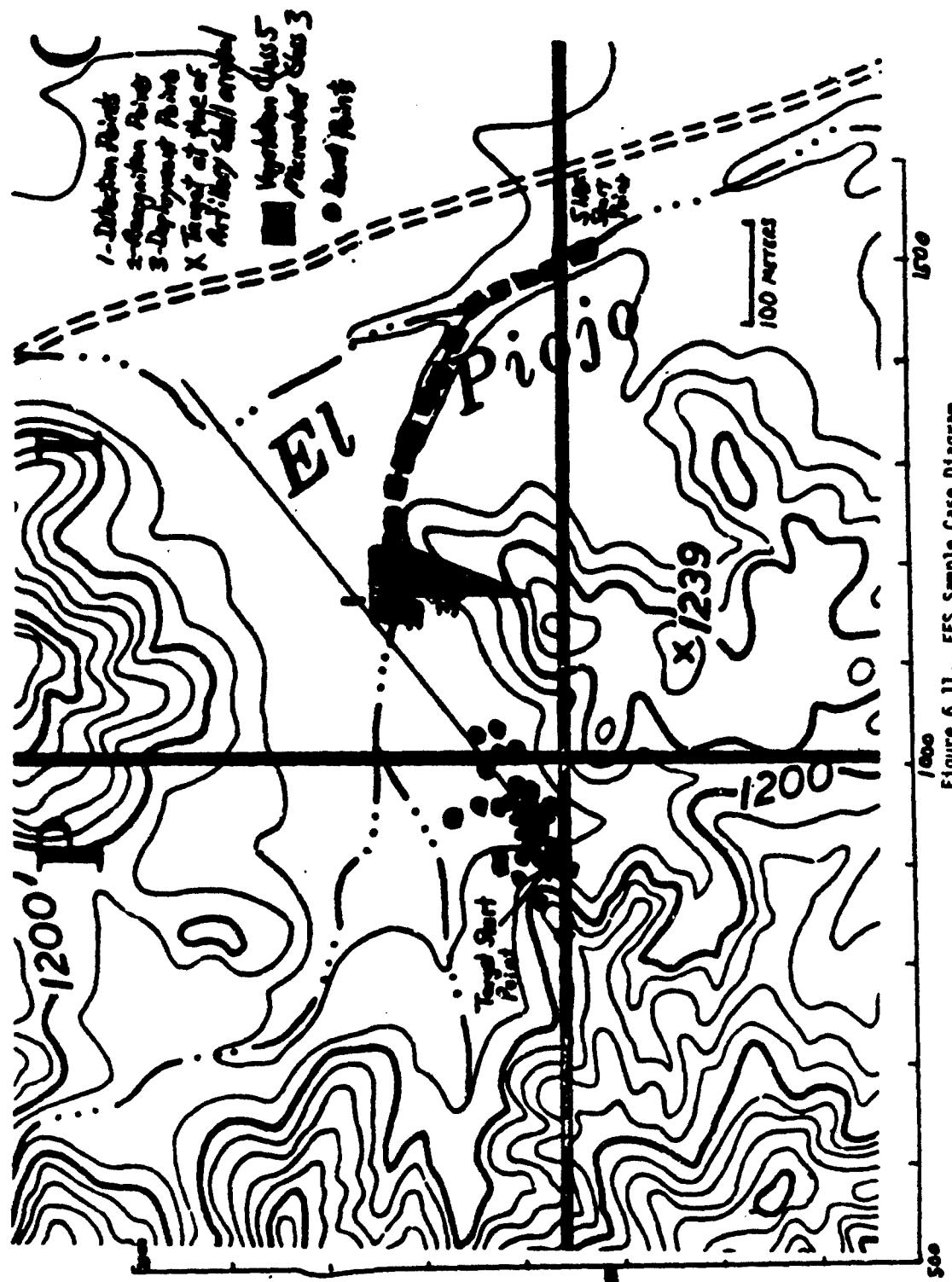


Figure 6.11. EFS Sample Case Diagram

Best Available Copy

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X-Y COORDINATES OF EXPENDABLE SUPPORT BURST POINTS
X = 828.97 Y = 1623.07
X = 831.63 Y = 1623.07
X = 834.41 Y = 1623.07
X = 897.41 Y = 1539.96
X = 967.97 Y = 1598.93
POSITION OF ATTACKER MU 1 X= 1169.38 Y= 1674.72
POSITION OF ATTACKER MU 2 X= 1168.87 Y= 1699.22
POSITION OF DEFENDER MU 1 X= 946.64 Y= 1587.31

Figure 6.12. EFS Sample Case Output

1 4 19 21

ATTACKER PATROL:

ATTACKER PATROL:

ATTACKER PATROL:

PATROL AREA:

FIRE TEAM NUMBER	WEAPON TYPE	H-101(SA)	H-101(SA)	H-101(SA)	H-101(SA)	H-79 Gd	H-101(SA)	H-101(SA)	H-101(SA)
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	YU	NO	NO	NO	NO	NO	NO	NO	NO
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1166.87	1169.38	1170.21	1168.16	1172.06	1167.23	1170.76	1167.91	0.00
CURRENT Y (METER)	1699.22	1674.72	1695.77	1701.65	1691.26	1704.74	1670.04	1674.50	0.00
HEIGHT X (METER)	1177.19	1175.28	1176.70	1177.67	1176.22	1178.16	1171.82	1174.74	0.00
HEIGHT Y (METER)	1662.44	1662.86	1677.46	1687.41	1672.48	1692.39	1658.08	1667.64	0.00
WEIGHT (KG)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
GUNNERS (METER)	.50	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	0.00
MOVING STATUS	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	0.00
MANEUVER UNIT	2	1	2	2	2	2	2	1	0
AMMO'S REMAIN (MG.)	20	20	20	20	20	20	20	20	0
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	M.GUNNER	GR.LINCH.	RIFLEMAN	RIFLEMAN	RIFLEMAN	0.00
MOVEMENT RATE (M/SEC)	.29	.29	.29	.29	.29	.29	.29	.29	0.00
INDIV. ASSIGNMENT	BASE FR.	M. UNIT	BASE FR.	BASE FR.	BASE FR.	M. UNIT	M. UNIT	M. UNIT	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	0
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	0
POSIT. IN FIRE TEAM	1	1	2	3	4	5	2	3	0
SECONDARY WEAPON AVI	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	0
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	2	0	0	0	0	0	0	0

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OFFENDER PAYLOAD		PATROL MEMBER		SCENE SURVEYOR	
PLATE TEAM NUMBER	WEAPON TYPE	PLATE TEAM NUMBER	WEAPON TYPE	SCENE SURVEYOR	SCENE SURVEYOR
CURRENT AMMO SUPPLY	AK-47	AK-47	AK-47	AK-47	AK-47
CASUALTY STATUS	100	100	100	100	100
FIRING STATUS	MI + HOUND MA. MOUND	NO	DEAD	NO	MA. WOUND
SUPPRESSION STATE	NOT	NOT	NOT	NOT	NOT
CURRENT X (METER)	946.64	941.41	949.76	938.28	941.41
CURRENT Y (METER)	1587.31	1569.53	1583.41	1579.50	1589.53
MEMENT X (METER)	0.00	0.00	0.00	0.00	0.00
MEMENT Y (METER)	0.00	0.00	0.00	0.00	0.00
HEIGHT	1.70	1.70	1.70	1.70	1.70
WIDTH	.50	.50	.50	.50	.50
CURRENT POSTURE	PRONE	PRONE	PRONE	PRONE	PRONE
MOVING STATUS	NORMAL	STOPPED	NORMAL	STOPPED	NORMAL
MANEUVER UNIT	1	1	1	1	1
RODOS REMAIN TRACCS	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	.30	.30	.30	.30	.30
INITIAL AMMO SUPPLY	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA
POSSN. IN FIRE TEAM	1	2	3	4	5
SECONDARY WEAPON AVI	None	None	None	None	None
NO OF HAND GUNS/PISTOL	0	0	0	0	0
SCENE SURVEYOR	None	None	None	None	None

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

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1. 4 19 21 CASUALTY EVENT
DEFENDED PATROL SUSTAINS THE NAT CASUALTY
THE NUMBER OF THE CASUALTY MEMBER IS : 5
THE TYPE OF CASUALTY IS : PAJ. WIND
TIME(SEC) THAT COMBAT OPERATION HAS BEEN UNDERWAY: 9.7322
POSITION : X- 1169.45 Y- 1674.52

ATTRIBLIE TABLE AFTER CASUALTY SUSTAINED

ATTACKER PATCHES:

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DEFENDER PATROL:

	1	2	3	4	5	6	7	8	9
<u>FIRE TEAM NUMBER</u>	1	1	1	1	1	1	1	1	1
<u>WEAPON TYPE</u>	AK-47								
<u>CURRENT AMMO SUPPLY</u>	100	100	100	100	100	100	100	100	100
<u>CASUALTY STATUS</u>	P1-FIJND MA-WOUNDED								
<u>FIRING STATUS</u>	NUT								
<u>SUPPRESSIVE SUPPORT</u>	0	0	0	0	0	0	0	0	0
<u>CURRENT X (METERS)</u>	946.47	947.47	949.59	938.28	932.71	941.61	941.61	941.61	941.61
<u>CURRENT Y (METERS)</u>	1567.17	1589.53	1583.27	1593.43	1579.37	1589.53	1589.53	1589.53	1589.53
<u>NEXT X (METERS)</u>	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
<u>NEXT Y (METERS)</u>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
<u>HEIGHT (METERS)</u>	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
<u>WIDTH (METERS)</u>	.50	.50	.50	.50	.50	.50	.50	.50	.50
<u>CURRENT POSTURE</u>	PRONE								
<u>MOVING STATUS</u>	TOP SP.	STOPPED	TOP SP.	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
<u>MANEUVER UNIT</u>	1	1	1	1	1	1	1	1	1
<u>ROUNDS REPAIR (MAG.)</u>	20	20	20	20	20	20	20	20	20
<u>FRAGMENT IN PATROL</u>	P.L.	A.P.L.	RIFLEMAN						
<u>MOVEMENT RATE (M/S EC)</u>	.30	.30	.30	.30	.30	.30	.30	.30	.30
<u>INDIV. ASSIGNMENT</u>	EASF FR.								
<u>INITIAL AMMO SUPPLY</u>	100	100	100	100	100	100	100	100	100
<u>WEAPON TYPE</u>	AREA								
<u>POSIT. IN FIRE TEAM</u>	1	2	3	4	5	6	7	8	9
<u>SECONDARY WEAPON AVAILABILITY</u>	None								
<u>NO. OF HAND GRENADE</u>	0	0	0	0	0	0	0	0	0
<u>NO. OF SMOKE GRENADE</u>	0	0	0	0	0	0	0	0	0

- BREAK DECISION : DEFEND - BREAKS CONTACT ETC TO LACK OF APPROPRIATE EQUIPMENT
BREAK DECISION : DEFEND - BREAKS - CONTACT ETC TO HIGH CASUALTY RATES

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X-Y COORDINATES OF EXTERNAL FIRE SUPPORT BURST PNTS	
X =	965.92
X =	1014.78
X =	1034.45
X =	1002.17
POSITION OF ATTACKER MU 1	X- 1170.35 V- 1671.77
POSITION OF ATTACKER MU 2	X- 1170.24 V- 1696.44
POSITION OF DEFENDER MU 1	X- 944.12 V- 1585.30

1 8 19 31

ATTRIBUTES AFTER EFS BURST

ATTACKER PATROL:

	1	2	3	4	5	6	7	8	9
	PATROL MEMBER								
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1
WEAPON TYPE	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)	H-161(SA)
CURRENT AMMO SUPPLY	99	99	99	99	99	99	99	99	99
CASUALTY STATUS	NO	NO	NO	NO	NO	NO	NO	NO	NO
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1170.24	1170.35	1171.24	1169.89	1172.73	1169.28	1171.03	1169.49	0.00
CURRENT Y (METER)	1696.44	1671.77	1692.95	1699.97	1688.23	1702.42	1666.95	1676.82	0.00
HEAT X (METER)	1177.19	1173.28	1176.70	1177.67	1176.22	1176.16	1171.82	1174.74	0.00
HEAT Y (METER)	1682.44	1642.86	1677.46	1687.41	1672.48	1692.39	1658.08	1667.64	0.00
WEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WEIGHT (METER)	.50	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND
MOVING STATUS	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL
MANEUVER UNIT	2	1	2	2	2	2	1	1	0
OUNDS REMAIN (MAC-10)	19	19	19	17	19	19	19	19	0
FUNCTION IN PATROL	P.L.	A.P.L.	PIPLERMAN	H.GUNNER	GADINCH.	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	.29	.29	.29	.29	.29	.29	.29	.29	.00
INDIV. ASSIGNMENT BASE FR.	K.	UNIT	BASE	FR.	BASE	FR.	BASE	FR.	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	0.00
WEAPON TYPE	ARE	ARE	ARE	ARE	ARE	ARE	ARE	ARE	0.00
POSIT. IN FIRE TEAM	1	1	2	3	4	5	2	3	0
SECONDARY WEAPON AVI	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	H. GREN.	0
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	2	0	0	0	0	0	0	0

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DEFENDER PATROL:	PATROL MEMBER									
	1	2	3	4	5	6	7	8	9	1
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1	1
WEAPON TYPE	AK-47									
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	PI. WOUNDED MAJ. WOUNDED									
FIRING STATUS	NOT									
SUPPRESSION STATE	1	1	1	1	1	1	1	1	1	1
CURRENT X (METER)	944.12	941.41	947.25	938.28	952.71	941.61	941.61	941.61	941.61	941.61
CURRENT Y (METER)	1585.30	1589.53	1581.40	1593.43	1579.37	1589.53	1589.53	1589.53	1589.53	1589.53
NEXT X (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT Y (METER)	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50
CURRENT POSTURE	PRONE									
MOVING STATUS	TOP SP.	STOPPED	TOP SP.	STOPPED						
MANEUVER UNIT	1	1	1	1	1	1	1	1	1	1
ROUND'S REMAIN (H.A.G.)	20	20	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN							
MOVEMENT RATE (M/SEC)	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0
TADIV. ASSIGNMENT	BASE FR.									
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA									
POSTY. IN FIRE TEAM	1	2	3	4	5	6	7	8	9	10
SECONDARY WEAPON AVI	NONE									
NO. OF HAND GRENADE	0	0	0	0	0	0	0	0	0	0
NUC. OF SIGHT GRENADE	0	0	0	0	0	0	0	0	0	0

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO HIGH CASUALTY FRACITION

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X-Y COORDINATES OF EXTERVAL FIRE SUPPORT GUNSI POINTS

X =	880.46	Y =	1575.04
X =	933.84	Y =	1610.04
X =	949.34	Y =	1571.41
X =	993.72	Y =	1619.40
POSITION OF ATTACKER MU 1	X -	1171.25	Y - 1669.03
POSITION OF ATTACKER MU 2	X -	1171.53	Y - 1693.85
POSITION OF DEFENDER MU 1	X -	941.70	Y - 1583.43

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1 - 8 1G 4!
 ATTRIBUTES AFTER FS DURST

ATTACKER PATROL:	1	2	3	4	5	6	7	8	9	1
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1	0
WEAPON TYPE	M-16(SAI)									
CURRENT AMMO SUPPLY	99	99	99	97	97	99	99	99	99	0
CASUALTY STATUS	NO									
FIRING STATUS	NOT									
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0	3
CURRENT X (METER)	1171.53	1171.25	1172.21	1171.49	1173.36	1171.20	1171.29	1170.90	1170.90	0.00
CURRENT Y (METER)	1693.85	1669.33	1690.13	1696.67	1685.41	1700.26	1664.07	1674.31	1674.31	0.00
NEXT X (METER)	1177.19	1173.28	1176.70	1177.67	1176.22	1178.16	1171.82	1174.74	1174.74	0.00
NEXT Y (METER)	1682.44	1662.86	1677.46	1687.01	1672.48	1692.39	1658.08	1667.64	1667.64	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WIDTH (METER)	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	0.00
CURRENT POSTURE	STAND	0.00								
MOVING STATUS	NORMAL	0.00								
MANEUVER UNIT	2	1	2	2	2	2	2	1	1	0
ROUNDS REMAIN (MAG.)	19	19	19	17	19	19	19	19	19	0
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	M.GUNNER	G.R.	L.NCH.	RIFLEMAN	RIFLEMAN	RIFLEMAN	
MOVEMENT RATE (M/SEC)	*2.9	*2.9	*2.9	*2.9	*2.9	*2.9	*2.9	*2.9	*2.9	0.00
INDIV. ASSIGNMENT	BASE FR.	M. UNIT	BASE FR.	M. BASE	FR.	M. BASE	FR.	M. P. UNIT	M. UNIT	
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	0
WEAPON TYPE	AREA									
POSIT. IN FIRE TEAM	1	1	2	3	4	5	6	3	3	0
SECONDARY WEAPON AVAILABILITY	H. GRENADE									
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	2	2	0	0	0	0	0	0	0

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DEFENDER PATROL		PATROL MEMBER								
		1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER		1	1	1	1	1	1	1	1	1
WEAPON TYPE	AK-47									
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	PI. WOUNDED MA. WOUNDED PI. WOUNDED									
FIRING STATUS	NOT									
SUPPRESSION STATE	1	1	1	1	1	1	1	1	1	1
CURRENT X (METERS)	941.78	941.41	944.91	938.28	952.71	941.41	941.41	941.41	941.41	941.41
NEXT X (METERS)	1583.43	1589.53	1574.52	1593.43	1579.37	1589.53	1589.53	1589.53	1589.53	1589.53
NEXT Y (METERS)	-0.30	-0.30	0.00	-0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEIGHT (METERS)	-0.30	-0.30	0.00	-0.00	0.00	0.00	0.00	0.00	0.00	0.00
WIDTH (METERS)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
CURRENT POSTURE	PRONE									
MOVING STATUS	TOP SP.	STOPPED								
MANEUVER UNIT	1	1	1	1	1	1	1	1	1	1
ROUNDS REPAIR (WAG.)	20	20	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.I.	A.P.L.	RIFLEMAN							
MOVEMENT RATE(M/SFC)	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0
INDIV. ASSIGNMENT	HASE FR.									
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA									
POSITION IN FIRE TEAM	1	2	3	4	5	6	7	8	9	10
SECONDARY WEAPON AVI	NO. OF HAND GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE	NO. OF SMOKE GRENADE

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER
BREAK DECISION : NOT NEEDED BREAKS CONTACT DUE TO HIGH CASUALTY RATE

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X-Y COORDINATES OF INTERJET & IRF SUPPORT BURST POINTS

X =	868.01	Y =	1267.50
X =	936.91	Y =	1003.22
X =	959.04	Y =	1262.42
X =	1004.12	Y =	1602.83
POSITION OF ATTACKER MU 1		X-	1172.19
POSITION OF ATTACKER MU 2		X-	1172.01
POSITION OF DEFENDER MU 1		X-	939.64
		Y-	1691.27
		Y-	1581.55

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ATTRIBUTES AFTER EFS HUST

ATTACHED PATROL:

	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	0
WEAPON TYPE	M-16(SAI)	1							
CURRENT AMMO SUPPLY	99	99	99	99	99	99	99	99	0
CASUALTY STATUS	NO	0							
FIRING STATUS	NOT	0							
SUPPRESSION STATE	3	0	3	0	0	0	0	0	0
CURRENT X (METERS)	1172.41	1172.15	1173.17	1173.09	1173.98	1173.11	1173.54	1173.34	0.00
CURRENT Y (METERS)	1691.21	1688.28	1687.41	1684.27	1682.59	1686.00	1681.19	1671.81	0.00
NEXT X (METERS)	1177.19	1175.18	1176.70	1177.67	1176.22	1176.25	1171.82	1176.74	0.00
NEXT Y (METERS)	1682.44	1682.86	1687.46	1687.61	1682.48	1682.38	1686.98	1687.64	0.00
HEIGHT (METERS)	1.7	0	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WIDTH (METERS)	.5	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	0.00							
MOVING STATUS	NORMAL	0.00							
MANEUVER UNIT	2	1	2	2	2	2	2	2	0
ROUNDS REMAIN (MAC)	19	19	19	17	19	19	19	19	0
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	P.GUNNER	G.R.D.M.	RIFLEMAN	RIFLEMAN	RIFLEMAN	0
MOVEMENT RATE(M/SEC)	.29	.29	.29	.29	.29	.29	.29	.29	0.00
INDIV. ASSIGNMENT	BASE PR	M. UNIT	BASE FR	BASE FR	BASE FR	M. UNIT	M. UNIT	M. UNIT	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	0
WEAPON TYPE	AREA	0							
POSIT. IN FIRE TEAM	1	1	3	4	4	4	4	4	0
SECONDARY WEAPON AVI	H. GREY	0							
NO. OF HAND GRENADE	4	4	2	0	3	0	0	0	0
NO. OF SMOKE GRENADE									

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DEFENDER PATROL:

PATROL MEMBER:

	1	2	3	4	5	6	7	8	9	10
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1	1
WEAPON TYPE	AK-47									
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	MI. WOUNDED	MA. WOUNDED	MI. WOUNDED	MA. WOUNDED						
FIRING STATUS	NOT									
SUPPRESSION STATE	1	1	1	1	1	1	1	1	1	1
CURRENT X (METER)	939.4	941.41	942.56	938.28	952.71	941.41	941.41	941.41	941.41	941.41
CURRENT Y (METER)	1581.5	1581.53	1577.65	1593.43	1579.37	1589.53	0.03	0.03	0.03	0.03
NEXT X (METER)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NEXT Y (METER)	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HEIGHT (METER)	1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7	1.7
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50
CURRENT POSTURE	PRONE									
MOVING STATUS	TOP SP.	STOPPED	TOP SP.	STOPPED						
MANEUVER UNIT	1	1	1	1	1	1	1	1	1	1
ROUNDS REMAIN (WAG.)	20	20	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P.L.	P.I.G.E.M.	RIFLEMAN						
MOVEMENT RATE (M/SEC)	.3	.3	.3	.3	.3	.3	.3	.3	.3	.3
INITIV. ASSIGNMENT	BASE FR.									
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA									
POSTY. IN FIRE TEAM	1	2	3	4	5	6	7	8	9	10
SECONDARY WEAPON AVAILABILITY	NONE									
NO. OF HAND GRENADE	0	0	0	0	0	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	0	0	0	0	0

BREAK DECISION: ATTACKER BREAKS CONTACT DUE TO EXCESSIVE ELAPSED TIME (FIGHT)

BREAK DECISION: DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

BREAK DECISION: U-FENEFIC BREAKS CONTACT DUE TO HIGH CASUALTY RATIO
 IC FOR BREAK CONTACT - AVAILABLE SIAF RALLY POINT 1670.9603 1644.5587
 ATTACKER WITHDRAWAL RALLY POINT

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ATTRIBUTES AFTR EFS BUST

ATTACKER PATROL:

	1	2	3	4	5	6	7	8	9
PATROL MEMBERS									
FIRE TEAM NUMBER	M-16(SA)	1	1	1	1	1	1	1	0
WEAPON TYPE	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)
CURRENT AMMO SUPPLY	99	99	99	99	99	99	99	99	99
CASUALTY STATUS	ND	ND	ND	ND	ND	ND	ND	ND	ND
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1183.54	1182.97	1183.64	1183.63	1184.70	1183.58	1182.36	1183.15	0.00
CURRENT Y (METER)	1689.73	1665.65	1695.83	1692.81	1681.00	1694.67	1660.56	1671.15	0.00
NEXT X (METER)	1470.96	1476.44	1470.41	1471.51	1469.86	1471.68	1470.41	1471.51	0.00
NEXT Y (METER)	1648.66	1646.64	1643.63	1653.63	1638.72	1650.60	1643.69	1653.63	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND
MOVING STATUS	TOP SP.	TOP SP.	TOP SP.	TOP SP.	TOP SP.	TOP SP.	TOP SP.	TOP SP.	TOP SP.
MANEUVER UNIT	2	1	2	2	2	2	2	1	1
ROUNDS REMAIN (MAG.)	13	19	19	17	19	19	19	19	0
FUNCTION IN PATROL	P.O.L.	A.P.L.	AIRFIELD GUNNER G.R.4INCH. AIRFIELD RIFLEMAN RIFLEMAN						
MOVEMENT RATE(M/SEC)	1.06	1.06	1.06	1.06	1.06	1.06	1.06	1.06	0.00
INCIV. ASSIGNMENT	BASE FR.	M. UNIT	BASE FR.	BASE FR.	BASE FR.	P. UNIT	M. UNIT	M. UNIT	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	0
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	1	2	3	4	5	2	3	0
SECONDARY WEAPON AVI	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE	M. GRENADE
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	1	0	0	0	0	0	0	0

DEFENDER PATROL	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER									
WEAPON TYPE	AK-47								
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	WOUNDED								
FIRING STATUS	NLT								
SUPPRESSION STATE	1	1	1	1	1	1	1	1	1
CURRENT X (METERS)	937.10	940.41	940.22	938.28	932.71	941.41	941.41	940.33	940.00
CURRENT Y (METERS)	1579.68	1584.53	1575.77	1593.43	1579.37	1589.53	1589.53	1580.00	1580.00
NEXT X (METERS)	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT Y (METERS)	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30
HEIGHT (METERS)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METERS)	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
CURRENT POSTURE	PRONE	PRUNE	PACIFIC	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE
MOVING STATUS	TIP SP.	STOPPED	TIP SP.	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	1	1	1	1	1	1	1	1	1
ROUNDS REMAIN (MAG.)	20	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.I.L.	A.P.L.	RIFLEMAN						
MOVEMENT RATE (M/SEC)	•30	•30	•30	•30	•30	•30	•30	•30	•30
INDIV. ASSIGNMENT	BASE FR.								
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA								
POSIT. IN FIRE TEAM	1	2	3	4	5	6	7	8	9
SECONDARY WEAPON AVI	N/NF	N/CME							
NO. OF HAND GRENADE	0	0	0	0	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	0	0	0	0

POSITION OF ATTACKER MU 1	X-	1201.35	Y-	1664.56	TIME TO SECUDS.
POSITION OF ATTACKER MU 2	X-	1201.77	Y-	1687.13	MU 1 X- 1222.93 Y- 1663.29
POSITION OF DEFENDER MU 1	X-	932.41	Y-	1575.93	MU 2 X- 1242.00 Y- 1694.52
POSITION OF DEFENDER MU 2	X-	927.73	Y-	1572.18	MU 1 X- 927.73 Y- 1572.18

1 8 20 41 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1244.61 Y- 1664.01

POSITION OF ATTAKER MU 2 X- 1241.45 Y- 1681.46

POSITION OF DEFENDER MU 1 X- 923.04 Y- 1568.43

1 8 21 1 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1266.24 Y- 1660.73

POSITION OF ATTACKER MU 2 X- 1262.90 Y- 1678.39

POSITION OF DEFENDER MU 1 X- 918.30 Y- 1564.68

1 8 21 21 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1287.87 Y- 1659.46

POSITION OF ATTACKER MU 2 X- 1284.34 Y- 1675.33

POSITION OF DEFENDER MU 1 X- 913.67 Y- 1560.94

1 8 21 41 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1309.50 Y- 1658.18

POSITION OF ATTACKER MU 2 X- 1305.79 Y- 1672.26

POSITION OF DEFENDER MU 1 X- 908.99 Y- 1557.19

1 8 22 1 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1331.13 Y- 1656.91

POSITION OF ATTACKER MU 2 X- 1327.24 Y- 1669.20

POSITION OF DEFENDER MU 1 X- 904.30 Y- 1553.44

1 8 22 21 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1352.76 Y- 1655.63

POSITION OF ATTACKER MU 2 X- 1348.69 Y- 1666.13

POSITION OF DEFENDER MU 1 X- 899.62 Y- 1549.69

1 8 22 41 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1374.39 Y- 1654.35

POSITION OF ATTACKER MU 2 X- 1370.14 Y- 1663.06

POSITION OF DEFENDER MU 1 X- 694.93 Y- 1545.94

1 8 23 1 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1390.01 Y- 1653.08

POSITION OF ATTACKER MU 2 X- 1391.59 Y- 1660.00

POSITION OF DEFENDER MU 1 X- 890.24 Y- 1542.20

1 8 23 21 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1417.64 Y- 1621.8C

POSITION OF ATTACKER MU 2 X- 1413.06 Y- 1656.93
 POSITION OF DEFENDER MU 1 X- 1405.56 Y- 1538.43

1 8 23 41 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1439.27 Y- 1650.53

POSITION OF ATTACKER MU 2 X- 1434.69 Y- 1653.87

POSITION OF DEFENDER MU 1 X- 1534.70 Y- 1530.95

1 8 24 1 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1460.90 Y- 1649.25

POSITION OF ATTACKER MU 2 X- 1455.93 Y- 1650.80

POSITION OF DEFENDER MU 1 X- 1516.19 Y- 1530.95

1 8 24 21 NO EVENTS IN 20 SECONDS.

POSITION OF ATTACKER MU 1 X- 1470.96 Y- 1646.66

POSITION OF ATTACKER MU 2 X- 1465.51 Y- 1649.38

POSITION OF DEFENDER MU 1 X- 1529.21 Y- 1529.21

1 8 24 3.0 1476.96 1648.66 MOVE MENT

ATTACKER MU 1 WILL MOVE 10.08 METERS AT AN ANGLE OF 1649.38 MOVE MENT

ATTACKER MU 2 WILL MOVE 10.08 METERS AT AN ANGLE OF 1529.21 MOVE MENT

RESOLUTION HAS BEEN CHANGED BACK TO THE RECOGNITION LEVEL OF 50.8 METERS

DECISION ON CONTINUATION OF RECONNAISSANCE MISSION AFTER COMBAT OPERATION IS COMPLETED :

MISSION DECISION : CONTINUE

CURRENT AMOUNT OF FOOD REMAINING PER MAN(B) : 13.4442

CURRENT AMOUNT OF WATER REMAINING PER MAN(B) : 6.9334

PATROL DURATION (DAYS) : 1

SIAF DETECTS TARGET NO. 1 VISUALLY

SIAF RECOGNIZED TARGET NO. 1 AT X- 1470.96 Y- 1648.66 THE RECOGNITION RANGE IS 543.51

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PATROL MEMBER STATISTICS AFTER COMBAT

ATTACKER PATROL:

	1	2	3	4	5	6	7	8	9
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1	1
WEAPON TYPE	4-1C(SA)	4-1C(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)
CURRENT AMMO SUPPLY	99	99	99	99	99	99	99	99	99
CASUALTY STATUS	NC	NO	NJ	NO	NJ	NO	NJ	NO	NO
FIRING STATUS	NOT	NOT							
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1465.41	1470.96	1466.10	1466.46	1466.86	1466.63	1470.35	1470.87	0.00
CURRENT Y (METER)	1549.30	1548.66	1544.32	1554.31	1539.16	1559.31	1643.69	1653.85	0.00
NEXT X (METER)	1470.96	1470.96	1470.41	1471.21	1469.86	1472.06	1470.41	1471.51	0.00
NEXT Y (METER)	1548.66	1548.00	1643.69	1653.93	1638.72	1658.60	1653.69	1653.63	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	0.00
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50	0.00
CURRENT POSTURE	STAND	STAND							
ROVING STATUS	TOP SP.	TOP SP.							
MANEUVER UNIT	2	1	2	2	2	2	2	1	0
ROUNDS PER MAIN (MAG.)	19	19	19	17	19	19	19	19	0
FUNCTION IN PATROL	P.L.	A.P.L.	RIFLEMAN	H.GUNNER	G.R.LNCH.	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/SEC)	1.08	1.08	1.08	1.08	1.08	1.08	1.08	1.08	0.00
INDIV. ASSIGNMENT	BASE FR.	M. UNIT	BASE FR.	BASE FR.	BASE FR.	M. UNIT	M. UNIT	M. UNIT	0.00
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	0
WEAPON TYPE	AK4A	AREA	ARFA						
POSIT. IN FIRE TEAM	1	1	2	3	4	5	2	3	0
SECONDARY WEAPON AVAILABILITY	H. GRENADE	0							
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4	0
NO. OF SMOKE GRENADE	2	1	0	0	0	0	0	0	2

DEFENDER PATROL:		PATROL MEMBER											
		1	2	3	4	5	6	7	8	9	10	11	12
FIRE TEAM NUMBER		1	1	1	1	1	1	1	1	1	1	1	1
WEAPON TYPE	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	PT. WOUNDED	MA. WOUNDED	MI. WOUNDED	DEAD	MA. WOUNDED								
FIRING STATUS	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT	NUT
SUPPRESSION STATUS	0	0	0	0	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	374.01	941.41	877.13	338.28	932.71	941.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00
CURRENT Y (METER)	1529.21	1589.53	1525.30	1593.43	1579.37	1589.53	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT X (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT Y (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEIGHT (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50	.50
CURRENT POSITION	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE	PRONE
MOVING STATUS	TOP SP.	STOPPED	TOP SP.	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	1	1	1	1	1	1	1	1	1	1	1	1	1
ROUNDS REPAINT (MAG.)	20	20	20	20	20	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P. L.	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN	RIFLEMAN
MOVEMENT RATE (M/S EC)	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0	*3.0
INDIV. ASSIGNMENT	BASE	BASE	FR.	BASE	FR.	BASE	FR.	BASE	FR.	BASE	FR.	BASE	FR.
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	2	3	4	5	6	7	8	9	10	11	12	13
SECONDARY WEAPON AVI	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE
NO. OF HAND GRENADE	0	0	0	0	0	0	0	0	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	0	0	0	0	0	0	0	0

SIAF POSITION: X- 1430.95 Y- 1625.60	TARGET DETECTED: YES	TIME: DAYS-10 HOURS-08 MINUTES-26
XSTAR = 932 VSTAR = 1576 LJS = 1		
SIAF DETECTS TARGET NO. 1 VISUALLY		
SIAF POSITION: X- 1422.40 Y- 1620.67	TARGET DETECTED: YES	TIME: DAYS-01 HOURS-03 MINUTES-27
XSTAR = 932 VSTAR = 1575 LJS = 1		
SIAF DETECTS TARGET NO. 1 VISUALLY		
SIAF POSITION: X- 1371.60 Y- 1591.40	TARGET DETECTED: YES	TIME: DAYS-01 HOURS-03 MINUTES-29
XSTAR = 932 VSTAR = 1576 LJS = 1		
SIAF DETECTS TARGET NO. 1 VISUALLY		

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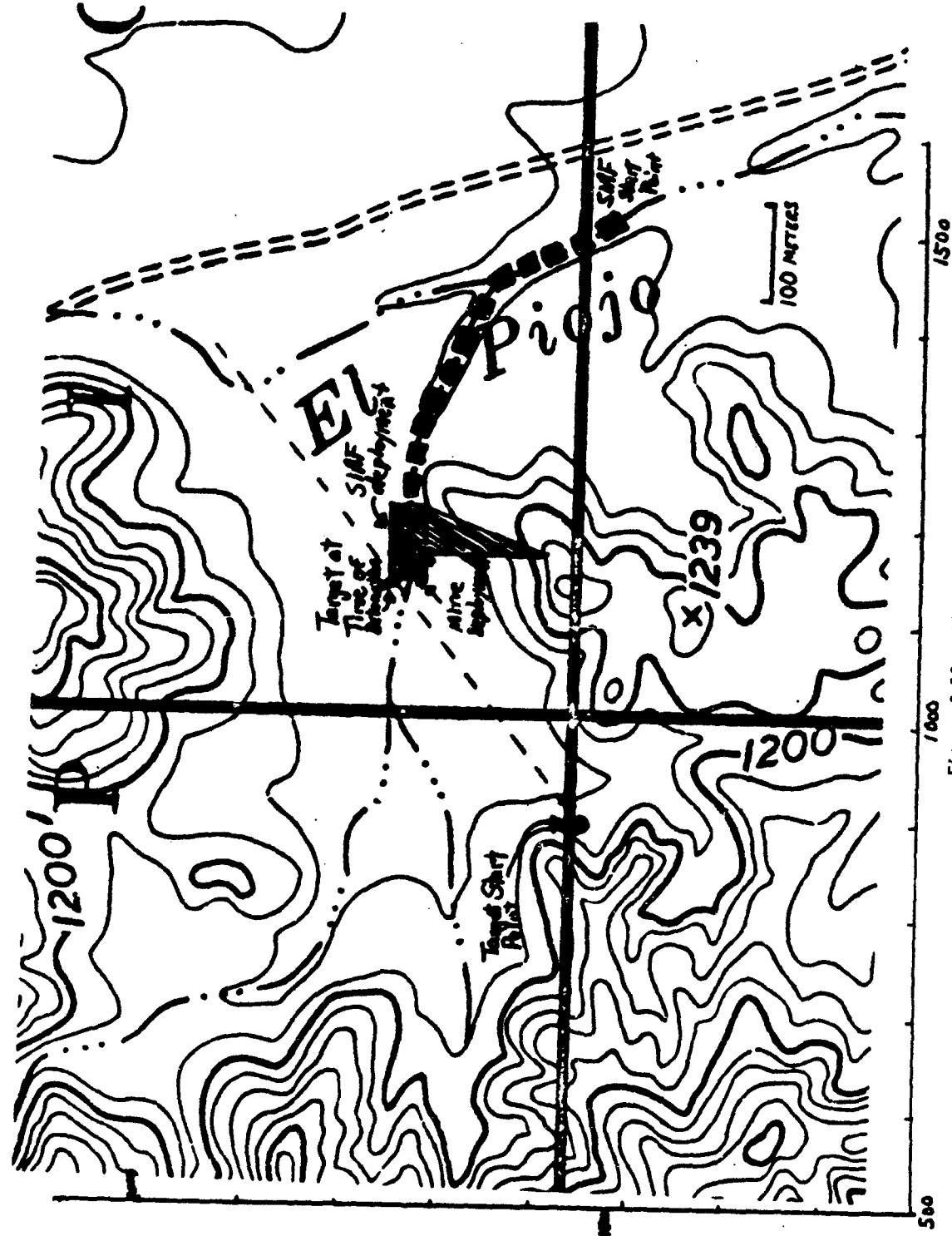


Figure 6.13. Claymore Mines Sample Case Diagram

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ATTRIBUTES AFTER DEPLOYMENT OF CLAYMORE MINES

ATTACKER PATROL:		PATROL MEMBER		
		1	2	3
FIRE TEAM NUMBER		1	1	1
WEAPON TYPE	M-16(SA)	M-16(SA)	M-16(SA)	M-16(SA)
CURRENT AMMO SUPPLY	100	100	100	100
CASUALTY STATUS	NO	NO	NO	NO
FIRING STATUS	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0
CURRENT X (METER)	1157.41	1160.93	1163.66	1166.78
CURRENT Y (METER)	1716.73	1719.22	1721.72	1724.22
NEXT X (METER)	0.00	0.00	0.00	0.00
NEXT Y (METER)	0.30	0.00	0.00	0.00
WEIGHT (METER)	1.70	1.70	1.70	1.70
WIDTH (METER)	.50	.50	.50	.50
CURRENT POSITION	CRUCH	CRUCH	CRUCH	CRUCH
MOVING STATUS	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	2	1	2	2
ROUNDS REMAIN (MAG.)	20	20	20	20
FUNCTION IN PATROL	P.L.	A.P.L. RIFLEMAN M. GUNNER S.G. LMG. RIFLEMAN		
MOVEMENT RATE (M/SEC)	0.00	0.00	0.00	0.00
INDIV. ASSIGNMENT	BASE FR.	M. UNIT BASE FR.	BASE FR.	M. UNIT
INITIAL AMMO SUPPLY	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	1	2	3
SECONDARY WEAPON AVAIL	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE
NO. OF HAND GRENADE	4	4	4	4
NO. OF SMOKE GRENADE	2	2	0	0

Figure 6-14. Combat Outputs for Claymore Mines Sample Case

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DEFENDER PAGE

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DEPLOYMENT OF CLAYMORE MINES	
X MINE	1154.23
X MINE	1166.00
X MINE	1177.71
Y MINE	1120.63
Y MINE	1130.00
Y MINE	1139.37

ATTACKER PATROL:		PATROL MEMBERS						
	1	2	3	4	5	6	7	8
FIRE TEAM NUMBER	1	1	1	1	1	1	1	1
WEAPON TYPE	H-1675361	H-1675361	H-1675361	H-1675361	H-1675361	H-1675361	H-1675361	H-1675361
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100
ASSAULT STATUS	NO	NO	NO	NO	NO	NO	NO	NO
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0	0	0
CURRENT X (METERS)	1197.41	1160.53	1163.46	1166.78	1169.90	1173.03	1176.15	1179.27
CURRENT Y (METERS)	1716.73	1719.22	1721.72	1724.22	1726.72	1729.22	1731.72	1734.22
NEXT X (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
NEXT Y (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
METRIC (METER)	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH (METER)	.50	.50	.50	.50	.50	.50	.50	.50
CURRENT POSITION	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND
MOVING STATUS	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED	STOPPED
MANEUVER UNIT	2	1	2	2	2	2	1	0
ROUNDS REMAIN (MAG.)	20	20	20	20	20	20	20	20
FUNCTION IN PATROL	P.L.	A.S.L.	RIFLEMAN	R.GUNNER	GUNNER	RIFLEMAN	RIFLEMAN	RIFLEMAN
Movement Rate (m/sec)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
INDIV. ASSIGNMENT	BASE FR.	M. UNIT	BASE FR.	M. UNIT	BASE FR.	M. UNIT	M. UNIT	M. UNIT
INITIAL AMMO SUPPLY	130	100	100	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA
POSIT. IN FIRE TEAM	1	1	2	2	2	2	2	2
SECONDARY WEAPON AVAIL	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE	H. GRENADE
NO. OF HAND GRENADE	4	4	4	4	4	4	4	4
NO. OF SMOKE GRENADE	2	2	0	0	0	0	0	0

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DEFENDER PATROL		PATROL MEMBER							
		1	2	3	4	5	6	7	8
FIRE TEAM NUMBER		1	1	1	1	1	1	1	1
WEAPON TYPE	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47	AK-47
CURRENT AMMO SUPPLY	100	100	100	100	100	100	100	100	100
CASUALTY STATUS	DEAD	DEAD	DEAD	DEAD	DEAD	DEAD	DEAD	DEAD	DEAD
FIRING STATUS	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT	NOT
SUPPRESSION STATE	0	0	0	0	0	0	0	0	0
CURRENT X (METER)	1150.00	1166.96	1133.12	1143.75	1156.25	1146.86	0.00	0.00	0.00
CURRENT Y (METER)	1750.00	1753.90	1746.10	1757.81	1742.19	1753.90	0.00	0.00	0.00
VECT X (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
VECT Y (METER)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
HEIGHT	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70	1.70
WIDTH	.50	.50	.50	.50	.50	.50	.50	.50	.50
CURRENT POSTURE	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND	STAND
MOVING STATUS	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL	NORMAL
MANEUVER UNIT	1	1	1	1	1	1	1	1	1
ROUNDS REMAIN (MAG.)	20	20	20	20	20	20	20	20	20
Movement Rate(m/sec)	.30	.30	.30	.30	.30	.30	.30	.30	.30
TADIV. ASSIGNMENT	BASE FR.	BASE FR.	BASE FR.	BASE FR.	BASE FR.	BASE FR.	BASE FR.	BASE FR.	BASE FR.
INITIAL AMMO SUPPLY	100	100	100	100	100	100	100	100	100
WEAPON TYPE	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA	AREA
P/SIT. IN FIRE TEAM	1	2	3	4	5	6	6	6	6
SECONDARY WEAPON AVL	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE	NONE
NO. OF HAND GRENADE	3	0	0	0	0	0	0	0	0
NO. OF SMOKE GRENADE	0	0	0	0	0	0	0	0	0

POSITION OF ATTACKER MU 1 X- 1163.53 Y- 1719.22
 POSITION OF ATTACKER MU 2 X- 1157.41 Y- 1716.73
 POSITION OF DEFENDER MU 1 X- 1150.00 Y- 1750.00

1 10 17 51 TIME OF MINS DETONATION

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE FIREPOWER

BREAK DECISION : DEFENDER BREAKS CONTACT DUE TO LACK OF ADEQUATE AMMUNITION

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7.0 OPERATING PROCEDURES

This section describes the operating procedures in terms of hardware requirements, software requirements, overlay structure of the model, and sample deck setup.

7.1 HARDWARE REQUIREMENTS

- CDC 6000 series digital computer
- SCOPE operating system
- FORTRAN EXTENDED source program compiler(FTN)
- COMPASS assembler
- Tape drive for input of topocom tape
- 232K of octal 60-bit words central memory
- Temporary and short-term storage devices (i.e., disk or tape)
- Standard system file configuration for input data and object program modules.

7.2 SOFTWARE REQUIREMENTS

- FORTRAN unit 1 is used for reading namelist input data. This data consists of NAML1, NAML2, NAML3, and NAML4. File NLINP is referenced to this unit.
- FORTRAN unit 2 is used for temporary storage. At the beginning of the model the packed reconnaissance elevations are stored here. After the return of a combat operation this unit is read to restore reconnaissance elevation data. File PAKZ is referenced to this unit.
- FORTRAN unit 5 is used for standard input. File INPUT is referenced to this unit.
- FORTRAN unit 6 is used for standard output. File OUTPUT is referenced to this unit.
- FORTRAN unit 7 is used for temporary storage. When a start/stop point is reached, the common blocks are dumped or read from this unit, so that the model can be started or stopped at specific points. File START is referenced to this unit.
- FORTRAN unit 8 is used for reading elevation input data. This file is a direct output of topocom programs, MAPGEN or ROTATE. File ZINP is referenced to this unit.

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- FORTRAN unit 9 is used for intermediate storage. The common block STATS is updated on this unit for each replication of the model. File STATS is referenced to this unit.
- Most of the COMMON blocks used by the SIAF program are defined in the following computer pages 1 through 47 of Figure 7.1. These blocks were generated by the BLKGEN program described in Appendix A of this volume. Using these COMMON blocks the SPECIN program defined in Appendix B of this volume, punched out the DIMENSION and EQUIVALENCE statements for all subroutines requiring any variable pertaining to the COMMON blocks.
- To facilitate finding a location of a common variable, Figure 7.2 gives an alphabetical list of all variables in these commons. Furthermore, their location in that block and the block name are given along with its dimension if the variable is an array.

7.3 OVERLAY STRUCTURE

- Figure 7.3 is a chart overview of the overlay structure organization. Within each overlay block the overlay level is given and the subroutine and programs are listed alphabetically, along with the size of the model with that overlay.

7.4 SAMPLE DECK SET-UPS

- Figures 7.4 - 7.6 are listings of card decks that would be required to create the model from tape starting from scratch and end up with an execution of the sample case.
- Figure 7.4, when submitted, will create or copy from the SIAF tape, all source cards and store them on permanent disk files.
- Now, execution of Figure 7.5 will compile all these source cards and create the object modules required for loading. These also are stored on permanent disk files.
- Figure 7.6 takes the generated object modules along with the required input files and executes the sample case.

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7.5 INSTALLATION

- The SIAF program as described above was installed and runs on a CDC 6500 digital computer at the USACDC Data Processing Installation, at Fort Leavenworth, Kansas.

CURRENT COMMON IS -- MASTER COMMON LISTING

COMMON/DATABASE/DATABASE(625)

CURRENT BLOCK IS DATA(624) 6241 6242

VARIABLE	COMMON IS DIMENSION	POSITION	TYPE	DESCRIPTION
ATTEN	4	1		
DSW11		5		
DSW12		6		
DRICE	7			
DMT		3, 3	6	
H		16, 4	23	
HD		3	97	
HMT		5, 3	36	
ISELECT		29	111	
RHO		16, 4	131	
QMTMAX		5, 3	195	
RMAX		16, 4	210	
REF		16, 3	274	
SECT		2, 4, 2	122	
VECC		3, 16	338	
VISLUM		6, 3	466	
W		16, 4	530	
WMT		5, 1	534	
XLP	16	16	609	

Figure 7.1. Master Common Listings (Sheet 1)

CURRENT COMMON IS - - - - - MASTER COMMON LISTING

COMMON/DATAB2/DATAB2(100)

CURRENT BLOCK IS DATAB2 (96)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ALIN		2,2	1	
ALLF		3,2	5	
SL1			11	
SL2			12	
SOILF		2,6	13	
TMR		16,3	29	
VEGF		16	AJ	

Figure 7.1. Master Common Listings (Sheet 2)

CURRENT COMMON IS -
CURRENT COMMON IS COMMON/DLOCAL/DGLOBAL (100)

CURRENT BLOCK IS DGLOBAL (100)

MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ALPHA1	1	1	ADM	
ALPHA2	2	2	ADM	
BETA	3	3	ADM	
DSOROP	4	4	ADM	
DSENG	5	5	ADM	
DSPUR	6	6	ADM	
DTDEPL	7	7	ADM	
DTENG	8	8	ADM	
DTPUR	9	9	ADM	
DTWATL	10	10	ADM	
ICOUNT	11	11	ADM	
IDARK	12	12	ADM	
IFLAG	13	13	ADM	
IPOSE	14	14	ADM	
ISET	15	15	ADM	
ISTOFF	16	16	ADM	
ISUIT	17	17	ADM	
ITAREN	18	18	ADM	
JGO	19	19	ADM	
JSP	20	20	ADM	
JFACT	21	21	ADM	
KFACT	22	22	ADM	
MENOP	23	23	ADM	
	24	24	ADM	
	25	25	ADM	

Figure 7.1. Master Common Listings (Sheet 2)

CURRENT BLOCK IS GLOBAL (100)

PAGE

MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
MENSP		26		
NGS		27		
NHMIN		28		
PHI		29		
PURVEL		30		
R		31		
RADV1		32		
RADV2		33		
RC		34		
RS		35		
SF		36		
SVATM		37		
TACKOP		38		
VADM		39		
VCEAL		40		
VCOV		41		
VELOP		42		
V OBS		43		
X1		44		
X2		45		
WA		46		
WB		47		
XDEPL		48		
XICIR		49		
XOP		50		
XSP		51		
YDEPL		52		
YICIR		53		
YOP		54		
YSP		55		
ZENG		56		
ZENG		57		

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Figure 7.1. Master Common Listings (Sheet 4)

CURRENT BLOCK IS 0 LOGOUT (1001)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ZOEPL		58		
ZENG		59		
ZETA		60		
IR		61		
MGS		62		
GS		63		
OLXDEP		64		
OLYDEP		65		
OLWULX		66		
OLVULY		67		
OLVEL		68		
OLTACK		69		
ISTU		70		
BLANK1		71		
IHAN		72		
JMAN		73		
IFFSID		74		
KDEFOP		75		
ISTART		76		
XDEFOP		77		
YDEFOP		78		
TARV		79		
IFFF		80		
ISTALL		81		

Figure 7.1, Master Common Listings (Sheet 5)

CURRENT COMMON IS --
COMMON/OLOCIN/OLOCIN(150)
CURRENT BLOCK IS OLOCIN (150)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
GADM		1		
CC1		2		
CC2		3		
CC3		4		
CLASS	5,16	5		
OTDAMB		85		
OTDAAT		86		
OTEF5		87		
OTENGH		88		
OTPURN		89		
EFSA		90		
FRAM8		91		
FRATT		92		
GMAX		93		
IDIREC		94		
IDUM1		95		
IDUM2		96		
VISS		97		
NSECT		98		
PP1		99		
PP2		100		
PP3		101		
PP4		102		
Q1		103		
Q2		104		

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Figure 7.1. Master Common Listings (Sheet 6)

CURRENT BLOCK IS DLOGIN (1501)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
Q3		105		
RAMB		106		
RAMIN		107		
RATT		108		
REFS		109		
ROBS		110		
RSP		111		
RZ		112		
PS		113		
GSAPRQ		114		

Figure 7.1, Master Common Listings (Sheet 7)

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CURRENT COMMON IS --
MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
A		1		
		4,204		

CURRENT BLOCK IS COMMON (\$16)

Figure 7.1. Master Common Listings (Sheet 8)

MASTER COMMON LISTING

CURRENT COMMON IS --
COMMON/COMM81/COMM81(715)
CURRENT BLOCK IS COMM81 (711)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
AC	164	1		
ALL		65		
ATAR		66		
ASTAFA		67		
CC		68		
CT		69		
CR		70		
CLL		71		
CR2	212	72		
D	204	76		
DRINS		250		
DRINT		251		
DBSPEC		252		
EOUT	204	302		
FTREL		306		
FOHREL		507		
G1OUT		508		
	204			

Figure 7.1. Master Common Listings (Sheet 9)

CURRENT COMMON IS COMM/COMM82/COMM82(6451).CMTR1(320)
CURRENT BLOCK IS COMM82 (6421)

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MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
G2OUT	1	204		
G3OUT		205		
HS		409		
HT		410		
IOE		411		
ISAD		412		
ITAD		413		
IDAY		414		
ISPRIT		415		
I2		416		
ITIME		417		
ILZAVL		5		
ITVEG		20		
IGEN		423		
IMP		443		
IFIRST		463		
ISV3		20		
ITVO		483		
IAT		503		
IAS		504		
INC		505		
IDEFS		506		
IFYPE		507		
IT		508		
ITGRIO		526		
		546		
		549		

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Figure 7.1. Master Common Listings (Sheet 10)

CURRENT BLOCK IS COMM2 1 6421

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
IP		550		
IVOL		551		
ISIP	20	552		
JIT		572		
KEY		573		
LZFAQ	20	574		
LFLAG	20	575		
MHQ	5	614		
MS		615		
MT		616		
NUI		620		
NOCH	20	621		
NDAY		622		
		642		

Figure 7.1. Master Common Listings (Sheet 11)

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CURRENT BLOCK IS CMTARI (320) *****
MASTER COMMON LISTING PAGE 12

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ITARG	20,5	1		
IAOR	20,2	101		
IVOR	20,2	141		
ICH	20	181		
ISA	20	201		
ISV	20	221		
ITA	20	241		
ITV	20	261		
IRFCOG	20,2	281		

Figure 7.1. Master Common Listings (Sheet 12)

MASTER COMMON LISTING

卷之三

CURRENT BACK COMMUNICATED BY CMMB 3/20/01 • CHTARZ2 (1901)

DANCE

三

VARIABLE	POSITION	TYPE	DESCRIPTION
	POSITION	TYPE	DESCRIPTION
NOETEC	1		
NSEC	2		
PAIR	3		
PALL	4		
PALLB	5		
PHONE	6		
PHONEB	7		
PSKY	8		
PGSKY	9		
PSCP	10		
POEGL	12		
R	14		
RLOSS	15		
RS	16		
RT	17		
RN	18		
RH	19		
SNUN	20		
SEGL	21		
SEGLCT	22		
STIME	23		
SGENDX	24		
SGENDY	25		
STSTART	26		
TZ	27		

Figure 7.1. Master Common Listings (Sheet 13)

CURRENT BLOCK IS COMMON (681)

MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
TARVEL				
TNUM		111		
THS		112		
HT		113		
ISTART		114		
		115		
THETA	20	116		
TH		136		
TEMP		137		
TOETS		20		
ISAVE	20,2	138		
VISH		198		
VIGLEV		199		
VOEG	200			
HV		201		
WS		202		
WT		203		
WD		204		
XB	5,20	205		
XLZ	5	305		
XS		310		
XT		311		
XTAR	20	312		
X2		312		
XDYNOL	10	333		
YB	5,20	343		
YLZ	5	443		
YS		449		
YT		449		
YTAR	20	450		
YZ		470		
YDYNOL	10	471		
ZZ		481		

Figure 7.1. Master Common Listings (Sheet 14).

CURRENT BLOCK IS CNTAR2 [1001] MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
RAWLZ	20,5	1		

Figure 7.1. Master Common Listings (Sheet 15)

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MASTER COMMON LISTING

CURRENT COMMON IS COMM/COMM/COMM44(295)
CURRENT BLOCK IS COMM44 (292)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
INSTANT	20,2	1		
ISTR1	20,2	41		
ISTR2	20,2	51		
ISTIVOL	20,2	71		
STAGR	20,2	121		
STRR	20,2	161		
STUD?	20,2	201		
SC4	20,1	241		
TC6	20	262		
CEPPAT	20	262		
CEPTAR		263		
CEPPH		263		
CEPPSS		264		
CEPPS		265		
ITNAV		286		
ITNAVS		287		
ITNVS		288		
ITNAVM		219		
NNAV		290		
SOCPEP		291		
SOITNV		232		

Figure 7.1. Master Common Listings (Sheet 16)

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MASTER COMMON LISTING

CURRENT COMMON IS --
COMMON/COMM35(COMM35(50),COMM35(500),COMM35(5000),COMM35(1000))

CURRENT BLOCK IS COMM35(50)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
AMR		1		
CS		2		
FM1		2		
FM2		4		
ROBUST		5		
IST		6		
VBAR		7		
VEL		8		
XAMR		9		
NOCOM		21		
MREP		22		
PCINT		23		
SUCRAT		24		
TAMPHR		25		
TPCADO		26		
TPCAF		27		
TPCAS		28		
TTIME		29		
TTUSE		30		
APCAO		31		
APCAF		32		
APGAS		33		
ATTEMP		14		
DF1		15		
DF2		16		
		37		

Figure 7.1. Master Common Listings (Sheet 17)

CURRENT BLOCK IS COMM85 (50)

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MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
F		38		
I80EAD		39		
ICON		40		
IP04R		41		
ICON		42		
COMM		43		
IP0WRT		44		
ICPER		45		
IXST		46		
HH		47		
PAT		48		
D1		49		
D2		50		

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Figure 7.1. Master Common Listings (Sheet 18)

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CURRENT BLOCK IS COMMS (5001)

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MASTER COMMON LINES

VARIABLE DIMENSION POSITION TYPE

DESCRIPTION

AAAAA 900 1

Figure 7.1. Master Common Lines (Sheet 10)

CURRENT BLOCK IS COMMONS | 5J01

MASTER COMMON LISTING
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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
KKTIME	500	1		

ANSWERED BY COMPUTER

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Figure 7.1. Master Common Listings (Sheet 20)

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PAGE

CURRENT BLOCK IS COMMES 1 3001 MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
JUTIME		160	1	

Figure 7.1. Master Common Listings (Sheet 2)

MASTER COMMON LISTING

CURRENT COMMON IS --
CURRENT COMMON/LINSIG/LINSIG (3403)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
LMT	1			
DOMV	2			
ETA	1			
FLAMDA	4			
SAM	3,20	5		
ICL	50	65		
II	204,5	115		
ISI		1135		
IRP	50	1136		
AND		1136		
LNR1		1197		
LSVA		1198		
MICR1		1199		
NY2		1190		
NY3		1191		
NRSCL		1192		
NRSP		1193		
NUYFG	264	1194		
SOTL		1390		
VECC		1399		
VEC2		1400		
XBAR		1401		
XOB	1000	1422		
YBAR		2402		
YOB	1000	2403		

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Figure 7.1, Master Common Listings (Sheet 22)

MASTER COMMON LISTING

CURRENT COMMON IS --

COMMON/MISC01/MISC01(300)

CURRENT BLOCK IS MISC01 1 2431

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VARIABLE DIMENSION POSITION TYPE DESCRIPTION

AMPHRA	1		
AMUN	2		
AMUTAB	21		
BSAREA	27		
CLAVNN	28		
CONCAP	29		
CPRAT	7		
EQUIP	37		
EXOEGI	38		
FINDEX	39		
FOOD	60		
FOODA	61		
FOOOD	62		
FOODU	63		
FWRAT	7		
H20	51		
H20A	52		
H200	53		
H20F0	54		
H20U	55		
HANDGM	56		
HIPLOT	57		
ICNT	107		
ICOMB	108		
IOVFL	109		

Figure 7.1. Master Common Listings (Sheet 21)

CURRENT BLOCK IS MISCB1 (243)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
INREP		110		
INREP1		111		
INREP2		112		
IREONE		113		
IRESUP		114		
ISCN		115		
ITMUL1		116		
ITIMPR		122		
KK		123		
LAMDAE		124		
MAXREQ		125		
MMAX		126		
NCOPY		127		
NHANDG		128		
NHGA		129		
NHU		130		
NLFLAG		131		
NMA		132		
NMINES		133		
NNHJ		134		
NSWT		135		
P		136		
PU		137		
PAKWT		138		
PAKWT2		139		
PAKWT3		140		
PAKWT4		141		
PATRON		142		
POAVG		143		
POMAX		144		
POMIN		145		
POPLOT		146		
		50		
		167		

Figure 7.1. Master Common Listings (Sheet 24)

CURRENT BLOCK IS MISCB1 (243) MASTER COMMON LISTING

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VARIABLE	DEFINITION	POSITION	TYPE	OPTION
POTOT		137		
PEQUIP		198		
RAMU		199		
RFOOD		203		
RH20		204		
RHANDC		205		
RHOMH		206		
RMINES		207		
RPE		208		
RPC		209		
RTIME		210		
SAMU		211		
SAMUTE		215		
SGANG		219		
SGMAX		220		
SGMIN		221		
SGT01		222		
SIGENG		223		
SIEGR		224		
SIGFFR		225		
SIS		226		
T		227		
TAMUN		228		
TEQUIP		229		
THEYS		230		
WT		231		
WTS		232		
XP2		236		
XPI		240		
XP4KMT		241		
PS		242		
		243		

Figure 7-1. Master Common Listings (Sheet 25)

CURRENT COMMON IS ---
MASTER COMMON LISTING

CURRENT BLOCK IS OBSTAB (S1) :.....

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
HSIG		1		
HTAU		2		
PSL		3		
HSIG		4		
HTAU		5		
XSIG		6		
XTAU		7		
XSTAR2	20	8		
YSIG		9		
YTAU		10		
YSTAR2	20	11		
YSIAF		12		
ZSIG		13		
ZTAU		14		

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Figure 7.1, Master Common Listings (sheet 26)

Figure 7.1. Master Common Listings (Sheet 27)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
L030	20.2	1		
L031	20.2	61		
L032	20.2	61		
L033	20.2	61		

MASTER COMMON LISTING

CURRENT COMMON IS --

CURRENT BLOCK IS OUTS11 / 1281

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CURRENT COMMON IS --
COMMON/TARINT/TARINT(1205)
CURRENT BLOCK IS TARINT (- 201)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
XGOAL	20	1		
YGOAL	20	21		
ISTART	20	41		
YCHNG	20	61		
ISAA	20	81		
ITAA	20	101		
ISVV	20	121		
ITVV	20	141		
IANCHS	20	161		
IANCHT	20	181		

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Figure 7.1. Master Common Listings (Sheet 28)

CURRENT COMMON IS COMMON/MISCB2/MISCB21500)
CURRENT BLOCK IS MISCB2 (4971 2222)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
DMORQ		1		
DMORR		2		
JSA		3		
OSAA		4		
DWNT	9,1	5		
IOELA		5		
IOELB		12		
IOELC		33		
IOELD		14		
IOELE		35		
IOV		16		
IGEFBK		17		
IGRIO		18		
JCOMAX		39		
JCOMXX		40		
JCS		41		
JCSS		42		
JROMAX		43		
JROMXX		44		
JRS		45		
JRSS		46		
KREC		47		
LFLQD	20	48		
ML		68		
MI		59		
MII		70		

Figure 7.1. Master Common Listings (Sheet 22).

Figure 7.1. Master Common Listings (Sheet 30)

CURRENT BLOCK IS MISCH2 (6971) MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
NIOV		71		
NPAR		72		
RV000		73		
RAUDIO		74		
RFMOR		75		
RFMORR		76		
RFSA		77		
RFSAI		78		
VIP		79		
XAV000		80		
XAVOID		81		
MAX		200		
XEE		282		
XEE		292		
YAV000		297		
YAVOID		298		
YDYN		299		
YPP1		31		
YPP1		439		
YPP1		440		
YPP1		441		
YPP1		442		
YPP1		443		
YPP1		444		
YPP1		445		
YPP1		446		
YPP1		447		
NONC		448		
INSTC		449		
GSPAX		450		
GSPDX		451		
ASA		452		
ASA		453		

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CURRENT COMMON IS -

COMMON/USIB01/USIB01(110), USIB01(200)

CURRENT BLOCK IS USIB01

PAGE 1

MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ANGIO		1		
AOXMAX		2		
AOYMAX		3		
CNT	20	4		
CRECOG		24		
DBACK		25		
DOMHT		26		
ORNT	20	27		
DSTEP		47		
DRST	20	48		
ENRNG		58		
FRCMVO		20		
FRCNVM		20		

Figure 7.1. Master Common Listings (Sheet 31)

CURRENT BLOCK IS USTAR1	4	2001	MASTER COMMON LISTING	PAGE	32
VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION	
GOALTX	10,20	1			

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Figure 7.1. Master Common Listings (Sheet 32)

MASTER COMMON LISTING

CURRENT COMMON IS --
 COMMON/USIB02/USIB02(550), USTAR2(200)
 CURRENT BLOCK IS USIB02 (550)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
MLZ	1	10		
I08	2	30		
ISENLZ	5	50		
IPREP	6	50		
IMOV	9	50		
IMV	20	100,5		
ITMOV				
ITMAX				

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Figure 7.1. Master Common Listings (Sheet 33)

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CURRENT BLOCK TS USFAR2	1	2001	MASTER COMMON LISTING	PAGE	34
VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION	
GOALTY	10,20	1			

Figure 7.1. Master Common Listings (Sheet 34)

CURRENT COMMON IS -

MASTER & COMMON LISTING

CURRENT BLOCK IS USIB03 (261),
COMMON/USIB03/USIB03(261),USIB03(261),USIB03(261)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
IDE1	20	5,20		
ISSOFF	20	5,20		
ISSON	20	5,20		
ITSTP	20	5,20		
ITSI	20	5,20		
ITZERO	261			

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Figure 7.1. Master Common Listings (Sheet 35)

Figure 7.1. Master Common Listings (Sheet 36)

CURRENT BLOCK IS USRARS (200) *****
MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
			1	
			10,20	ITIMS

10000-0000-00-00
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CURRENT COMMON IS --
COMMON/USIB04/USIB04(S00)
CURRENT BLOCK IS USIB04 (S00)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ISTAV	100,5	1		

Figure 7.1. Master Common Listings (Sheet 37)

Figure 7.1. Master Common Listings (Sheet 38)

CURRENT COMMON IS --	COMMON/USIB05/USIB05(500)	MASTER COMMON LISTING		PAGE 38		
CURRENT BLOCK IS USIB05 (500) :::::		VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
		ITSTAV		100,5	1	

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CURRENT COMMON IS ---
COMMON/USI806/USI806(500)
CURRENT BLOCK IS USI806 (500)

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
ITARIV	100,5	1		

Figure 7.1. Master Common Listings (Sheet 39)

CURRENT COMMON IS --
COMMON/US1007/US1007(4001),USTAR(300)

CURRENT BLOCK IS US1007 (476)

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
IDOMST		1		
KRECOL		2		
MODE		3		
NOB		4		
MCO	5	5		
NRMT		6		
NSENS		7		
NLZ		8		
NDECOY		9		
NTAR		10		
NFTX		11		
NMP	20	12		
NSTP	20	13		
NNCL	100,2	14		
NPLAN	5	15		
NRST		256		
RANMAX	20	261		
RSEN		262		
RLZ	5	262		
RCHIN	20	263		
RCMAX	20	264		
SC	6	265		
SEGMIN		320		
TZERO		334		
TOEBK	4	335		
		336		

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Figure 7.1. Master Common Listings (Sheet 40)

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MASTERS COMMON LISTING
RECEIPT OF 15 HOURS

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
TIPREP	LEVEL	20	NUMBER	
TOMIN	LEVEL	340	NUMBER	
ISR	LEVEL	361	NUMBER	
ISS	LEVEL	362	NUMBER	
VELM	LEVEL	363	NUMBER	
		364	NUMBER	10.11
		365	NUMBER	366
		366	NUMBER	478

Figure 7.1. Master Canon Listings (Sheet 41)

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CURRENT BLOCK IS USTAR4 (300) *****

MASTER COMMON LISTING

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
TC	10,20	1		
SOUND1	5,20	201		

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Figure 7.1, Master Common Listings (Sheet 42)

CURRENT COMMON IS -
COMMON/USI808/USI808(10).USTARS(1000)
CURRENT BLOCK IS USI808 (6)

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1000-0000-10-00
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MASTER COMMON LISTING

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
XBASE				1
YBASE				2
X1FREN				3
X2FREN				4
Y1FREN				5
Y2FREN				6

Figure 7.1. Master Common Listings (Sheet 43)

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MASTER COMMON LISTINGS			
CURRENT BLOCK IS USRARS (1000)	POSITION	TYPE	DESCRIPTION
VARIABLE DIMENSION			
XPLAN	100.5	1	
YPLAN	100.5	503	

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Figure 7.1. Master Common Listings (Sheet 44)

MASTER COMMON LISTING			
CURRENT COMMON IS --	CURRENT DIMENSION	POSITION	TYPE
CURRENT BLOCK IS USI010 { 31)			
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VARIABLE	DIMENSION	POSITION	DESCRIPTION
ALLB		1	
ALLW		2	
ATTAR		3	
A		4	
ATER		5	
AFQ		6	
BE		7	
GR		8	
ITDRPH		9	
ITWMTA		10	
ITWTAR		11	
ITACOS		12	
ITPLSQ		13	
ITPLSA		14	
PMC		15	
PMS		16	
PPLS		17	
RC		18	
RCTAR		19	
RTER		20	
REQ		21	
SCALE		22	
SPEC		23	
SIGNTAB		24	
SGMTAB		25	

Figure 7.1. Master Common Listings (Sheet 45)

Figure 7.1. Master Canon Listings (Sheet 46)

MASTER COMMON LISTING			
CURRENT BLOCK IS US1010 (311	VISIBLE DIMENSION	POSITION	TYPE
			DESCRIPTION
	TOUR	26	
	INERTIA	27	
	VH	28	
	VK	29	
	VISMM	30	
	VISMG	31	

MASTER COMMON LISTING

CURRENT COMMON IS USIB11 (17)

CURRENT CLOCK IS USIB11 (17)

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VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
IOTIM		1		
MDC		2		
MDH		3		
NTC		4		
NTW		5		
MAXREP		6		
NBAT		7		
NRAD		8		
PT		9		
RNF		10		
RPOWR		11		
IPONR		12		
TUSE		13		
XOBINS		14		
BETA		15		
BLIFE		16		
FREQ		17		

Figure 7.1. Master Common Listings (Sheet 47)

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COMMON REFERENCES IN ALTERNATIVE AREA			
VARIABLE COMMON	NAME	PSM	SIZE
ALM1	1	1	900
ADM	1	1	1616
AC	1	1	2
ALH	1	5	2
ALF	1	5	2
ALM1	65	65	2
ALM2	2	2	2
ALM3	2	2	2
AMH	1	1	2
AMH1	1	1	2
AMH2	1	1	2
AMH3	1	1	2
AMH4	1	1	2
AMH5	1	1	2
AMH6	1	1	2
AMH7	1	1	2
AMH8	1	1	2
AMH9	1	1	2
AMH10	1	1	2
AMH11	1	1	2
AMH12	1	1	2
AMH13	1	1	2
AMH14	1	1	2
AMH15	1	1	2
AMH16	1	1	2
AMH17	1	1	2
AMH18	1	1	2
AMH19	1	1	2
AMH20	1	1	2
AMH21	1	1	2
AMH22	1	1	2
AMH23	1	1	2
AMH24	1	1	2
AMH25	1	1	2
AMH26	1	1	2
AMH27	1	1	2
AMH28	1	1	2
AMH29	1	1	2
AMH30	1	1	2
AMH31	1	1	2
AMH32	1	1	2
AMH33	1	1	2
AMH34	1	1	2
AMH35	1	1	2
AMH36	1	1	2
AMH37	1	1	2
AMH38	1	1	2
AMH39	1	1	2
AMH40	1	1	2
AMH41	1	1	2
AMH42	1	1	2
AMH43	1	1	2
AMH44	1	1	2
AMH45	1	1	2
AMH46	1	1	2
AMH47	1	1	2
AMH48	1	1	2
AMH49	1	1	2
AMH50	1	1	2
AMH51	1	1	2
AMH52	1	1	2
AMH53	1	1	2
AMH54	1	1	2
AMH55	1	1	2
AMH56	1	1	2
AMH57	1	1	2
AMH58	1	1	2
AMH59	1	1	2
AMH60	1	1	2
AMH61	1	1	2
AMH62	1	1	2
AMH63	1	1	2
AMH64	1	1	2
AMH65	1	1	2
AMH66	1	1	2
AMH67	1	1	2
AMH68	1	1	2
AMH69	1	1	2
AMH70	1	1	2
AMH71	1	1	2
AMH72	1	1	2
AMH73	1	1	2
AMH74	1	1	2
AMH75	1	1	2
AMH76	1	1	2
AMH77	1	1	2
AMH78	1	1	2
AMH79	1	1	2
AMH80	1	1	2
AMH81	1	1	2
AMH82	1	1	2
AMH83	1	1	2
AMH84	1	1	2
AMH85	1	1	2
AMH86	1	1	2
AMH87	1	1	2
AMH88	1	1	2
AMH89	1	1	2
AMH90	1	1	2
AMH91	1	1	2
AMH92	1	1	2
AMH93	1	1	2
AMH94	1	1	2
AMH95	1	1	2
AMH96	1	1	2
AMH97	1	1	2
AMH98	1	1	2
AMH99	1	1	2
AMH100	1	1	2
AMH101	1	1	2
AMH102	1	1	2
AMH103	1	1	2
AMH104	1	1	2
AMH105	1	1	2
AMH106	1	1	2
AMH107	1	1	2
AMH108	1	1	2
AMH109	1	1	2
AMH110	1	1	2
AMH111	1	1	2
AMH112	1	1	2
AMH113	1	1	2
AMH114	1	1	2
AMH115	1	1	2
AMH116	1	1	2
AMH117	1	1	2
AMH118	1	1	2
AMH119	1	1	2
AMH120	1	1	2
AMH121	1	1	2
AMH122	1	1	2
AMH123	1	1	2
AMH124	1	1	2
AMH125	1	1	2
AMH126	1	1	2
AMH127	1	1	2
AMH128	1	1	2
AMH129	1	1	2
AMH130	1	1	2
AMH131	1	1	2
AMH132	1	1	2
AMH133	1	1	2
AMH134	1	1	2
AMH135	1	1	2
AMH136	1	1	2
AMH137	1	1	2
AMH138	1	1	2
AMH139	1	1	2
AMH140	1	1	2
AMH141	1	1	2
AMH142	1	1	2
AMH143	1	1	2
AMH144	1	1	2
AMH145	1	1	2
AMH146	1	1	2
AMH147	1	1	2
AMH148	1	1	2
AMH149	1	1	2
AMH150	1	1	2
AMH151	1	1	2
AMH152	1	1	2
AMH153	1	1	2
AMH154	1	1	2
AMH155	1	1	2
AMH156	1	1	2
AMH157	1	1	2
AMH158	1	1	2
AMH159	1	1	2
AMH160	1	1	2
AMH161	1	1	2
AMH162	1	1	2
AMH163	1	1	2
AMH164	1	1	2
AMH165	1	1	2
AMH166	1	1	2
AMH167	1	1	2
AMH168	1	1	2
AMH169	1	1	2
AMH170	1	1	2
AMH171	1	1	2
AMH172	1	1	2
AMH173	1	1	2
AMH174	1	1	2
AMH175	1	1	2
AMH176	1	1	2
AMH177	1	1	2
AMH178	1	1	2
AMH179	1	1	2
AMH180	1	1	2
AMH181	1	1	2
AMH182	1	1	2
AMH183	1	1	2
AMH184	1	1	2
AMH185	1	1	2
AMH186	1	1	2
AMH187	1	1	2
AMH188	1	1	2
AMH189	1	1	2
AMH190	1	1	2
AMH191	1	1	2
AMH192	1	1	2
AMH193	1	1	2
AMH194	1	1	2
AMH195	1	1	2
AMH196	1	1	2
AMH197	1	1	2
AMH198	1	1	2
AMH199	1	1	2
AMH200	1	1	2
AMH201	1	1	2
AMH202	1	1	2
AMH203	1	1	2
AMH204	1	1	2
AMH205	1	1	2
AMH206	1	1	2
AMH207	1	1	2
AMH208	1	1	2
AMH209	1	1	2
AMH210	1	1	2
AMH211	1	1	2
AMH212	1	1	2
AMH213	1	1	2
AMH214	1	1	2
AMH215	1	1	2
AMH216	1	1	2
AMH217	1	1	2
AMH218	1	1	2
AMH219	1	1	2
AMH220	1	1	2
AMH221	1	1	2
AMH222	1	1	2
AMH223	1	1	2
AMH224	1	1	2
AMH225	1	1	2
AMH226	1	1	2
AMH227	1	1	2
AMH228	1	1	2
AMH229	1	1	2
AMH230	1	1	2
AMH231	1	1	2
AMH232	1	1	2
AMH233	1	1	2
AMH234	1	1	2
AMH235	1	1	2
AMH236	1	1	2
AMH237	1	1	2
AMH238	1	1	2
AMH239	1	1	2
AMH240	1	1	2
AMH241	1	1	2
AMH242	1	1	2
AMH243	1	1	2
AMH244	1	1	2
AMH245	1	1	2
AMH246	1	1	2
AMH247	1	1	2
AMH248	1	1	2
AMH249	1	1	2
AMH250	1	1	2
AMH251	1	1	2
AMH252	1	1	2
AMH253	1	1	2
AMH254	1	1	2
AMH255	1	1	2
AMH256	1	1	2
AMH257	1	1	2
AMH258	1	1	2
AMH259	1	1	2
AMH260	1	1	2
AMH261	1	1	2
AMH262	1	1	2
AMH263	1	1	2
AMH264	1	1	2
AMH265	1	1	2
AMH266	1	1	2
AMH267	1	1	2
AMH268	1	1	2
AMH269	1	1	2
AMH270	1	1	2
AMH271	1	1	2
AMH272	1	1	2
AMH273	1	1	2
AMH274	1	1	2
AMH275	1	1	2
AMH276	1	1	2
AMH277	1	1	2
AMH278	1	1	2
AMH279	1	1	2
AMH280	1	1	2
AMH281	1	1	2
AMH282	1	1	2
AMH283	1	1	2
AMH284	1	1	2
AMH285	1	1	2
AMH286	1	1	2
AMH287	1	1	2
AMH288	1	1	2
AMH289	1	1	2
AMH290	1	1	2
AMH291	1	1	2
AMH292	1	1	2
AMH293	1	1	2
AMH294	1	1	2
AMH295	1	1	2
AMH296	1	1	2
AMH297	1	1	2
AMH298	1	1	2
AMH299	1	1	2
AMH300	1	1	2
AMH301	1	1	2
AMH302	1	1	2
AMH303	1	1	2
AMH304	1	1	2
AMH305	1	1	2
AMH306	1	1	2
AMH307	1	1	2
AMH308	1	1	2
AMH309	1	1	2
AMH310	1	1	2
AMH311	1	1	2
AMH312	1	1	2
AMH313	1	1	2
AMH314	1	1	2
AMH315	1	1	2
AMH316	1	1	2
AMH317	1	1	2
AMH318	1	1	2
AMH319	1	1	2
AMH320	1	1	2
AMH321	1	1	2
AMH322	1	1	2
AMH323	1	1	2
AMH324	1	1	2
AMH325	1	1	2
AMH326	1	1	2
AMH327	1	1	2
AMH328	1	1	2
AMH329	1	1	2
AMH330	1	1	2
AMH331	1	1	2
AMH332	1	1	2
AMH333	1	1	2
AMH334</td			

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSN	SIZE	DEFINITION
CEPTRAR	CEPTRAR	263	20	
CLASS	CLASS	5	5,16	
CLAYMM	CLAYMM	26		
CLL	CLL	71		
CLMT	CLMT	1		
CNT	CNT	4	20	
COMMO	COMMO	43		
CONCAP	CONCAP	29		
CPRT1	CPRT1	38	7	
CREC06	CREC06	24		
CR2	CR2	72	2,2	
CR	CR	79		
CS	CS	2		
CT	CT	69		
DBACK	DBACK	25		
DBINS	DBINS	260		
DBIN1	DBIN1	281		
DBSPEC	DBSPEC	282	20	
DR1	DR1	36		
DR2	DR2	37		
DHORR	DHORR	2		
DHOR	DHOR	-	1	
DNT	DNT	-	1	
DOMMT	DOMMT	26		
DONY	DONY	2		
OSAA	OSAA	2	3	
OSDOP	OSDOP	6		
DRICE	DRICE	7		
DSENG	DSENG	7		
DRHT	DRHT	27		
DTDAMS	DTDAMS	65		
DTDATI	DTDATI	66		
DTDEPL	DTDEPL	6		
DRST	DRST	48		
OTERS	OTERS	67		
OTENG4	OTENG4	68		

Figure 7-2. Cross-reference of Common Variables (Sheet 2)

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COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE NAME	COMMON PSN	DIMENSION SIZE 1	DEFINITION	BLOCK NAME
BYENG	10			DLGCBL
DSPUR	6			USI1801
DSTEP	47			DLGCBL
DSW11	5			DATA80
DSW12	6			DATA80
DPURM	9			DLGCBL
DPUR	11			DLGCBL
DWAIT	12			MISC82
DWTI	5			COMM85
D1	49			COMM85
D2	50			COMM85
D	76			COMM81
EFSA	90			DLGCBN
ENRG	68			USI1801
EOUT	302			COMM31
ETA	3			LINSIG
EQUIP	37			MISC81
EXEGET	34			MISC81
FLANDA	4			LINSIG
FINDEX	39			MISC81
FM1	4			COMM85
FM2	5			COMM85
FRAFB	91			DLGCBN
FRAFT	92			MISC81
F000A	41			MISC81
F000D	42			MISC81
F000U	43			MISC81
F00D	40			MISC81
FRCMVD	69			USI1801
FRCMVN	69			COMM31
FTHREL	506			MISC81
FWRAT	44			COMM81
FURREL	507			COMM85
F	38			LINSIG
GAM	5			DLGCBN
GMAX	93			USTARI
GOALTX	1			
		204		10,20

Figure 7-2, Cross-reference of Common Variables (Sheet 3)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	COMMON PSN	SIZE	DEFINITION
GOALTY		1	10,20	
GSAPOXX	GSAPOXX	114		
GSAPOXX	GSAPOXX	194		
GS	GS	63	204	
GROUT	GROUT	588	204	
G2OUT	G2OUT	1	204	
G3OUT	G3OUT	285	204	
HANDGM	HANDGM	56	9	
HB	HB	87	9	
HH	HH	47		
HLZ	HLZ	1		
HMT	HMT	96		
HIAU	HIAU	2		
HSIG	HSIG	1		
HIPLOT	HIPLOT	57	50	
HS	HS	409		
HI	HI	410		
H20A	H20A	52		
H200	H200	53		
H2000	H2000	54		
H2000	H2000	56		
H20U	H20U	55		
H20	H20	51		
H	H	23	16,4	
IDDEAD	IDDEAD	39		
IDARK	IDARK	14		
IDAY	IDAY	414		
IANCHS	IANCHS	161	20	
IANCHT	IANCHT	101	20	
IAOR	IAOR	101	20,2	
IAS	IAS	506		
IAT	IAT	505		
ICH	ICH	101	20	
IDELA	IDELA	32		
IDELB	IDELB	33		
IDELC	IDELC	34		
IDELO	IDELO	35		

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Figure 7-2. Cross-reference of Common Variables (Sheet 4)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSN	SIZE	DEFINITION	BLOCK	NAME
IODEL		36			MISCB2	
IODETS		500	20		COMM82	
IODET		1	20		USIB33	
IODE		411			COMM82	
ICL		65			LINSIG	
ICNT		107			MISCB1	
ICOMB		108			MISCB1	
ICOM		40			COMMS	
ICOUNT		13			DLOGBL	
ICPER		45			COMMS	
IDIREC		94			DLOGIN	
IOOMSI		1			USIB07	
IOUM1		95			DLOGIN	
IOUM2		96			DLOGIN	
IFFF		80			DLOGBL	
IOVFL		109			MISCB1	
IFFSTD		74			DLOGBL	
IOYOL		551			COMM82	
IOV		37			MISCB2	
IFIRST		403	20		COMM82	
IGEN		443	20		COMM82	
IGETBK		38			MISCB2	
IFLAGS		15			DLOGBL	
ICRID		39			MISCB2	
IMAN		72			DLOGBL	
II		115	204,5		LINSIG	
IOBST		6			COMMS	
IOB		2		5	USIB02	
ILZAVL		416	5		COMM82	
IMOV		10	20		USIB02	
IMP		463	20		COMM82	
IMV		30	20		USIB02	
INREP1		111			MISCB1	
INREP2		112			MISCB1	
INREP		113			MISCB1	
LSAA		61	20		TARINT	
ISAD		412			COMM82	

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Figure 7-2. Cross-reference of Common Variables (Sheet 5)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSW	DIMENSION SIZE	DEFINITION	BLOCK NAME
ISA	201		20		CYCLE
IPOSE	16				GLOBAL
IPORT	4				COMMON
IPWR	14				COMMON
ITAA	101		20		TARGET
ITAO	413				COMMON
IPREP	9				USING
IRECDS	201		20,2		COMMON
ITAREN	20				CHARACTER
ITANG	1		20,5		GLOBAL
ITARIV	1		100,5		CHARACTER
IREONE	111				MISC01
IRESUP	114		7		MISC02
ISCEIN	113		7		CHARACTER
ITA	241		20		DATA00
ISECT1	111		20		USING01
ISEMLZ	6				USING02
ISEN	7				GLOBAL
ISET	17				COMMON
IP	550				COMMON
ICON	92				COMMON
IGRID0	569				COMMON
ITWUA	122				GLOBAL
ITIME	617				COMMON
ITIMEQ	123				GLOBAL
ITIMS	1		10,20		TARGET
ITSOFF	21		5,20		USING04
ISSON	121		5,20		GLOBAL
ISTADT	1		20,2		COMMON
INSTALL	81				COMMON
ISTART	76				GLOBAL
ISTART1	11		20		TARGET
ISTAY	1		100,5		USING04
ISTUFF	18				GLOBAL
ISTP	552		20		COMMON
ISTR1	61		20,2		GLOBAL
ISTRU	70				GLOBAL

Figure 7-2. Cross-reference of Common Variables (Sheet 6)

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COMMON VARIABLES IN ALPHABETICAL ORDER			
VARIABLE NAME	COMMON NAME	DIMENSION SIZE	DEFINITION
I8V01	I8V	20,2	
I8T	I8T	7	
ISU1	ISU1	115	
ISVO	ISVO	503	
ISVV	ISVV	121	20
ISV	ISV	221	20
ITMAX	ITMAX	550	
ITNOV	ITNOV	50	100,5
ITNAV	ITNAV	289	
ITNAVS	ITNAVS	287	
ITNAV	ITNAV	286	
ITNUSS	ITNUSS	288	
ITRC	ITRC	1136	50
ITSTAY	ITSTAY	1	100,5
ITSTC	ITSTC	496	
ITSTOP	ITSTOP	241	20
ITSTR1	ITSTR1	415	
ITST	ITST	221	20
ITVO	ITVO	504	
ITVEG	ITVEG	423	20
ITVV	ITVV	141	20
ITV	ITV	261	20
ITYPE	ITYPE	526	20
ITZERO	ITZERO	261	
INC	INC	507	
IT	IT	546	
ITV02	ITV02	141	20,2
ITSI	ITSI	46	
IT2	IT2	416	
JCOMAX	JCOMAX	40	
JCOMXX	JCOMXX	41	
JCSS	JCSS	43	
JCS	JCS	42	
JCO	JCO	21	
JMAN	JMAN	73	

Figure 7-2. Cross-reference of Common Variables (Sheet 1)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSN	DIMENSION	SIZE	DEFINITION	BLOCK NAME
JIT	JITIME	572	1	100		COMM82
JTACT		1	23			DLOG81
JROMAX	JROMAXX	44				MISC82
JROMXX		45				MISC82
JRSS	JRSS	67				MISC82
JRS	JSP	46				MISC82
JSP	KDEFOP	22				DLOGBL
KDEFOP	KEY	75				DLOGBL
KEY	KKTIME	573	1	500		COMM82
KKTIME	KWD	1				COMM85
KWD	KK	1186				LINSIG
KK	KTACT	124	24			MISC81
KTACT	KREC	2				US1807
KREC	KRECOL	48	20			MISC82
KRECOL	LAMDAE	125				MISC81
LAMDAE	LFLAG	594	20			COMM82
LFLAG	LFLOGJ	68				MISC82
LFLOGJ	LNRI	1187				LINSIG
LNRI	LLSD	1				OUTS11
LLSD	LOSR	41				OUTS11
LOSR	LOST	61				OUTS11
LOST	LOSSY	101				OUTS11
LOSSY	LSVS	1188				LINSIG
LSVS	LZTAR	574	20			COMM82
LZTAR	MAXREQ	126				DLOGBL
MAXREQ	MENOP	1				MISC82
MENOP	MENSP	25	20			DLOGBL
MENSP	MICR1	26	20			DLOGBL
MICR1	MGS	1189	62			MISC81
MGS	MII	62	70			OUTS11
MII	MISS	70	97			OUTS11
MISS	MMAX	97	127			OUTS11
MMAX	MNB	127	614			COMM82
MNB	MI	614	69			MISC82
MI	MODE	69	3			US1807

Figure 7-2... Cross-reference of Common Variables (Sheet A)

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Figure 7-2. Cross-reference of Common Variables (Sheet 9)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	DIMENSION	SIZE	DEFINITION
WAVP	WAVP	1193	1193	WAVE PACKET
NSTP	NSTP	36	20	NUMBER OF STEPS
MSUT	MSUT	136	136	NUMBER OF STEPS
LINS16	LINS16	1196	1196	NUMBER OF STEPS
UDEV1	UDEV1	65	65	NUMBER OF STEPS
OLVEXP	OLVEXP	65	65	NUMBER OF STEPS
OLVEXL	OLVEXL	65	65	NUMBER OF STEPS
OLVEXR	OLVEXR	65	65	NUMBER OF STEPS
PAIR	PAIR	3	3	CORRELATION COEFFICIENT
PDAVG	PDAVG	14	14	AVERAGE POSITION
PAKNT2	PAKNT2	143	143	NUMBER OF PAKETS
PAKNT3	PAKNT3	141	141	NUMBER OF PAKETS
PAKNT4	PAKNT4	142	142	NUMBER OF PAKETS
PAKNT5	PAKNT5	139	139	NUMBER OF PAKETS
PALB	PALB	5	5	NUMBER OF PAKETS
PALL	PALL	4	4	NUMBER OF PAKETS
PATDIS	PATDIS	43	43	NUMBER OF PAKETS
PATRON	PATRON	143	143	NUMBER OF PAKETS
PCINT	PCINT	24	24	NUMBER OF PAKETS
PDEGL	PDEGL	14	14	NUMBER OF PAKETS
POMAX	POMAX	145	145	NUMBER OF PAKETS
PEQUIP	PEQUIP	196	196	NUMBER OF PAKETS
PHI	PHI	29	29	NUMBER OF PAKETS
POPLOT	POPLOT	147	147	NUMBER OF PAKETS
PHONE8	PHONE8	7	7	NUMBER OF PAKETS
PHONE6	PHONE6	6	6	NUMBER OF PAKETS
PP1	PP1	99	99	NUMBER OF PAKETS
PP2	PP2	100	100	NUMBER OF PAKETS
PP3	PP3	101	101	NUMBER OF PAKETS
PSGP	PSGP	12	12	NUMBER OF PAKETS
PSGSKY	PSGSKY	10	10	NUMBER OF PAKETS

Figure 7-2. Cross-reference of Common Variables (Sheet 10)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSN	SIZE	DEFINITION	BLOCK NAME	COMMON NAME
PSKY		0	3		COMM1	
PSL		3	3			
PS	PURVEL	243				
PA		30				
PS	P	136				
P1		113				
P2		104				
P3		105				
RADW1	RADW1	32			DLOGIN	DLOGIN
RADW2	RADW2	33			DLOGIN	DLOGIN
RAMB	RAMB	106			DLOGIN	DLOGIN
RAMIN	RAMIN	107			DLOGIN	DLOGIN
RAMU	RAMU	199	4		MISC81	MISC81
RANL2	RANL2	1	20,5		CMTAR2	CMTAR2
RANMAX	RANMAX	262	20		USIB07	USIB07
RATT	RATT	106			DLOGIN	DLOGIN
RAVODD	RAVODD	73			MISC81	MISC81
RAVOID	RAVOID	74			DLOGBL	DLOGBL
RCMAX	RCMAX	306	23		MISC82	MISC82
RCMIN	RCMIN	203	20		MISC82	MISC82
REFS	REFS	109			USIB07	USIB07
REF	REF	274	16,3		DLOGIN	DLOGIN
RHANDG	RHANDG	205			DATA88	DATA88
RC	RC	34			MISC81	MISC81
RFMORR	RFMORR	76			DATA88	DATA88
RFMOR	RFMOR	75			MISC81	MISC81
RF000	RF000	203			DATA88	DATA88
RFSA	RFSA	74			MISC82	MISC82
RFSA	RFSA	77			MISC82	MISC82
RHOH	RHOH	206			MISC81	MISC81
RHO	RHO	131	16,4		DATA88	DATA88
RH20	RH20	204			MISC81	MISC81
RMAX	RMAX	210	16,4		DATA88	DATA88
RH	RH	83			COMM83	COMM83
RLLOSS	RLLOSS	79			COMM83	COMM83

Figure 7-2. Cross-reference of Common Variables (Sheet 11)

COMMON VARIANCES IN ALPHABETICAL ORDER

Figure 7-2. Cross-referencce of Common Variables (Sheet 12)

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Figure 7-2, Cross-reference of Common Variables (Sheet 13)

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	DEFINITION	SIZE	DIMENSION	BLOCK NAME
SU2			12		
SOILF			13	2,6	
SOIL			1396		
SNUM			64		
SOUND1			201	5,20	
SIADR			121	20,2	
SUGRAT			25		
SITIME			106	20,2	
STRR			161	20,2	
SISTR1			109		
SIS			226		
SYVDR			201	20,2	
TACKOP			36		
TAMPHR			26		
TAMUN			229		
TARVEL			111		
TARY			79		
TOEBK			336	4	
TOETS			138	20	
TOMIN			361		
TC6			242	2,1	
TC			1	10,20	
TEMP			137		
TERUDP			230		
THI			116	20	
THETA			116		
THETS			231		
THS			113		
THR			136		
TPCAD			29		
TPCAF			27		
TPCAS			26		
TNUM			112		
TSAVE			150	20,2	
TPREP			340		

74

US1807

COMM83

COMM84

COMM85

COMM86

COMM87

COMM88

COMM89

COMM90

COMM91

COMM92

COMM93

COMM94

COMM95

COMM96

COMM97

COMM98

COMM99

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COMM07

COMM08

COMM09

COMM0A

COMM0B

COMM0C

COMM0D

COMM0E

COMM0F

COMM0G

COMM0H

COMM0I

COMM0J

COMM0K

COMM0L

COMM0M

COMM0N

COMM0O

COMM0P

COMM0Q

COMM0R

COMM0S

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COMM0U

COMM0V

COMM0W

COMM0X

COMM0Y

COMM0Z

COMM0A

COMM0B

COMM0C

COMM0D

COMM0E

COMM0F

COMM0G

COMM0H

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COMM0J

COMM0K

COMM0L

COMM0M

COMM0N

COMM0O

COMM0P

COMM0Q

COMM0R

COMM0S

COMM0T

COMM0U

COMM0V

COMM0W

COMM0X

COMM0Y

COMM0Z

COMM0A

COMM0B

COMM0C

COMM0D

COMM0E

COMM0F

COMM0G

COMM0H

COMM0I

COMM0J

COMM0K

COMM0L

COMM0M

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COMM0Q

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COMM0V

COMM0W

COMM0X

COMM0Y

COMM0Z

COMM0A

COMM0B

COMM0C

COMM0D

COMM0E

COMM0F

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COMM0J

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COMM0L

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COMM0R

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COMM0T

COMM0U

COMM0V

COMM0W

COMM0X

COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE NAME	COMMON NAME	PSN	SIZE	DEFINITION	BLOCK NAME
TTIME		30			COMM85
TSR		362			USIB07
TSS		363			USIB07
TSTART		115			USIB07
TVEL		341	20		COMM83
TTUSE		31			USIB07
TZERO		335			COMM85
TZ		110			USIB07
TO		226			COMM83
T		227			MISCB1
VBAR		6			COMM85
VADM		39			DLOGBL
VCEAL		40			DLOGBL
VCHNG		61	27		DLOGBL
VDEG		203			TARINT
VCOV		41			COMM83
VEGC		338			DLOGBL
VEGC		1399	6,16		DATAB8
VEGF		83			LINSIG
VEG1		1400			DATAB8
VELH		364			LINSIG
VELOP		42			USIB07
VEL		9	12		DLOGBL
VIGLEV		199			COMM83
VISLUM		466			DLOGBL
VISM		198			MISCB2
VOBS		43			USIB07
VTYP		79			DLOGBL
WDAY		368	10,11		COMM83
WA		46			DATAB8
WB		47			OBSTAR
WD		204			OBSTAR
WT		594			OBSTAR
WTAU		5	5,3		USIB07
WSIG		4			MISCB1
WR		478			
WTS		236			

Figure 7-2. Cross-reference of Common Variables (Sheet 14)

SIAF,T100,MT1.
TASK,TN=SIAF,TA=13954,OS=ATDSOPF,TR=TS.
REQUEST,SIAFO0,*AM.
REQUEST,SIAFO1,*AM.
REQUEST,SIAFO2,*AM.
REQUEST,SIAFO3,*AM.
REQUEST,SIAFO4,*AM.
REQUEST,SIAFO5,*AM.
REQUEST,SIAFO6,*AM.
REQUEST,SIAFO7,*AM.
REQUEST,SIAFO8,*AM.
REQUEST,BTPKS,*AM.
REQUEST,NLINP,*AM.
REQUEST,ZINP,*AM.
REQUEST,CONVRT,*AM.
REQUEST,MAPGEN,*AM.
REQUEST,ROTATE,*AM.
VSN,SIAF=0000.
REQUEST,SIAF,*HY.
COPYBR,SIAF,SIAFO0.
COPYBR,SIAF,BTPKS
COPYBR,SIAF,SIAFO1.
COPYBR,SIAF,SIAFO2.
COPYBR,SIAF,SIAFO3.
COPYBR,SIAF,SIAFO4.
COPYBR,SIAF,SIAFO5.
COPYBR,SIAF,SIAFO6.
COPYBR,SIAF,SIAFO7.
COPYBR,SIAF,SIAFO8.

Figure 7.4, Creation of Source Files (Sheet 1)

```
SKIPF,SIAF,9.  
COPYBR,SIAF,NLINP.  
COPYBR,SIAF,ZINP.  
COPYBR,SIAF,CONVRT.  
COPYBR,SIAF,MAPGEN.  
COPYBR,SIAF,ROTATE.  
CATALOG,SIAF00,SIAF00,ID=SIAF,RP=100,CY=1.  
CATALOG,BTPKS,BTPKS,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF01,SIAF01,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF02,SIAF02,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF03,SIAF03,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF04,SIAF04,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF05,SIAF05,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF06,SIAF06,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF07,SIAF07,ID=SIAF,RP=100,CY=1.  
CATALOG,SIAF08,SIAF08,ID=SIAF,RP=100,CY=1.  
CATALOG,NLINP,NLINP,ID=SIAF,RP=100,CY=1.  
CATALOG,ZINP,ZINP,ID=SIAF,RP=100,CY=1.  
CATALOG,CONVRT,CONVRT,ID=SIAF,RP=100,CY=1.  
CATALOG,MAPGEN,MAPGEN,ID=SIAF,RP=100,CY=1.  
CATALOG,ROTATE,ROTATE,ID=SIAF,RP=100,CY=1.  
EOR  
EOI
```

Figure 7.4, Creation of Source Files (Sheet 2)

SIAF,T400.
TASK,TN=SIAF,TA=13954,OS=ATDSDPF,TR=TS.
REQUEST,NVBFT0,*AM.
REQUEST,NVBFT1,*AM.
REQUEST,NVBFT2,*AM.
REQUEST,NVBFT3,*AM.
REQUEST,NVBFT4,*AM.
REQUEST,NVBFT5,*AM.
REQUEST,NVBFT6,*AM.
REQUEST,NVBFT7,*AM.
REQUEST,NVBFT8,*AM.
ATTACH,SIAF00,SIAF00,ID=SIAF.
ATTACH,BTPKS.BTPKS,ID=SIAF.
ATTACH,SIAF01,SIAF01,ID=SIAF.
ATTACH,SIAF02,SIAF02,ID=SIAF.
ATTACH,SIAF03,SIAF03,ID=SIAF.
ATTACH,SIAF04,SIAF04,ID=SIAF.
ATTACH,SIAF05,SIAF05,ID=SIAF.
ATTACH,SIAF06,SIAF06,ID=SIAF.
ATTACH,SIAF07,SIAF07,ID=SIAF.
ATTACH,SIAF08,SIAF08,ID=SIAF.
FTN,I=SIAF00,B=NVBFT0.
COMPASS,I=BTPKS,B=NVBFT0.

Figure 7.5, Creation of Object Files (Sheet 1)

```
FTN,I=SIAF01,B=NVBFT1.  
FTN,I=SIAF02,B=NVBFT2.  
FTN,I=SIAF03,B=NVBFT3.  
FTN,I=SIAF04,B=NVBFT4.  
FTN,I=SIAF05,B=NVBFT5.  
FTN,I=SIAF06,B=NVBFT6.  
FTN,I=SIAF07,B=NVBFT7.  
FTN,I=SIAF08,B=NVBFT8.  
CATALOG,NVRFT0,NVBFT0,ID=SIAF,CY=1.  
CATALOG,NVBFT1,NVBFT1,ID=SIAF,CY=1.  
CATALOG,NVBFT2,NVBFT2,ID=SIAF,CY=1.  
CATALOG,NVBFT3,NVBFT3,ID=SIAF,CY=1.  
CATALOG,NVBFT4,NVBFT4,ID=SIAF,CY=1.  
CATALOG,NVBFT5,NVBFT5,ID=SIAF,CY=1.  
CATALOG,NVBFT6,NVBFT6,ID=SIAF,CY=1.  
CATALOG,NVBFT7,NVBFT7,ID=SIAF,CY=1.  
CATALOG,NVBFT8,NVBFT8,ID=SIAF,CY=1.  
EOI  
EOI
```

Figure 7.5, Creation of Object Files (Sheet 2)

SIAF,T700.
TASK,TN=SIAF,TA=13954,OS=ATDSDPF,TR=TS.
ATTACH,NVBFT0,NVBFT0,ID=SIAF.
ATTACH,NVBFT1,NVBFT1,ID=SIAF.
ATTACH,NVBFT2,NVBFT2,ID=SIAF.
ATTACH,NVBFT3,NVBFT3,ID=SIAF.
ATTACH,NVBFT4,NVBFT4,ID=SIAF.
ATTACH,NVBFT5,NVBFT5,ID=SIAF.
ATTACH,NVBFT6,NVBFT6,ID=SIAF.
ATTACH,NVBFT7,NVBFT7,ID=SIAF.
ATTACH,NVBFT8,NVBFT8,ID=SIAF.
ATTACH,NLINP,NLINP,ID=SIAF.
ATTACH,ZINP,ZINP,ID=SIAF.
RFL,150000.
LOAD,NVBFT0.
LOAD,NVBFT1.
LOAD,NVBFT2.
LOAD,NVBFT3.
LOAD,NVBFT4.
LOAD,NVBFT5.
LOAD,NVBFT6.
LOAD,NVBFT7.
LOAD,NVBFT8.

Figure 7.6, Execution of Model (Sheet 1)

NOGO
RFL,232000.
MNALPH.
EXIT.
DMP,232000.
EOR
\$NAML1

(REVISIONS TO NAMELIST NAML1)
SEND

\$NAML2
(REVISIONS TO NAMELIST NAML2)
SEND

\$NAML3
(REVISIONS TO NAMELIST NAML3)
SEND

\$NAML4
(REVISIONS TO NAMELIST NAML4)
SEND

EOR
EOI

Figure 7.6, Execution of Model (Sheet 2)

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8.0 SIAF RELIEF MODEL VALIDATION

8.1 PURPOSE

The purpose of this discussion is to describe the method and results of simulating line of sight experiments to demonstrate the validity of: 1) the line of sight calculations; and 2) the mathematical concept of macro-relief representation in the SIAF Terrain Submodel. The raw data used in the simulation was taken from field measurements at nine different locations in the Hunter-Liggett Military Reservation. The experiment measures line of sight data with respect to macro-relief only; the effects due to vegetation and micro-relief features are neglected.

8.2 HUNTER-LIGGETT FIELD EXPERIMENT

8.2.1 Purpose

The primary purpose of the field experiment was to gather actual line of sight data concerning terrain macro-relief. The line of sight experiments were conducted at nine locations within the map section shown in Figure 8.1.

8.2.2 Equipment

The experiments required three pieces of equipment. A compass was used to determine direction, a one-hundred meter rope, graduated in five meter intervals was used to measure surface distance, and a pair of walkie-talkies was used to relay information.

8.2.3 Methodology:

The typical procedure undertaken is depicted in Figure 8.2. An observer would stand at an easily identifiable point (i.e., landmarks, roads, peaks, saddlepoints, etc.) with a compass and walkie-talkie. One end of the hundred-meter rope is held by the observer. Another individual, designated as the "target", moves away from the observer holding the other end of the rope. The target is also equipped with a walkie-talkie. The target continues to walk away from the stationary observer, until only the target's head is visible (to the observer) due to the interruption of the line of sight by the ground. The observer and target are in radio communication, so that the location of the target at the time of line of sight interruption is established accurately.

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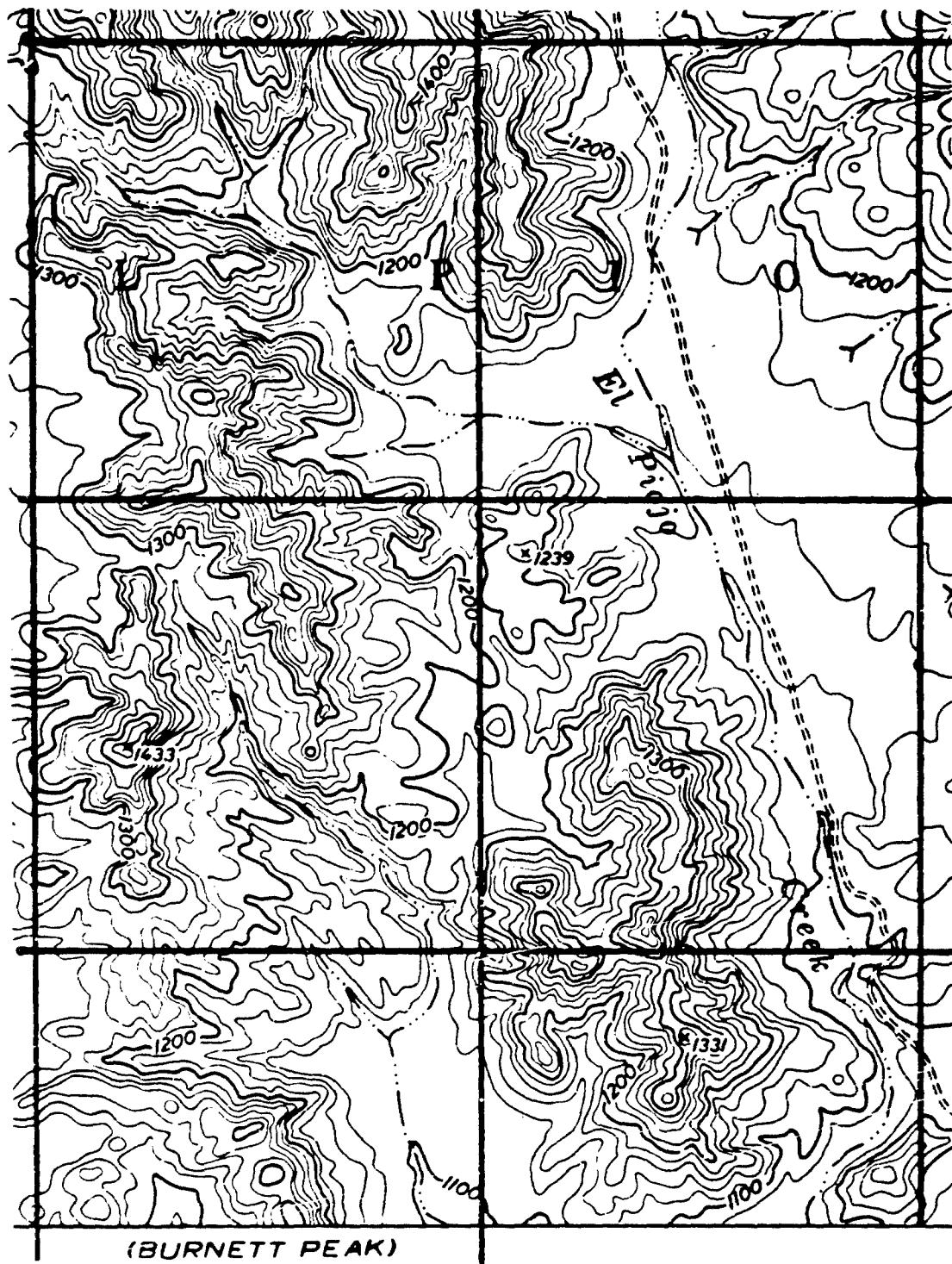


Figure 8.1, Hunter-Liggett Test Area

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Figure 8.2, LOS Experimental 1 Procedure

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The procedure was repeated at approximately every fifteen degrees of arc, at which time a third individual would record the heading, and the "surface distance" between the observer and target. By "surface distance" we mean the distance traced out by the rope over the curvature of the ground. This is to be distinguished from the "range distance," which is the distance between observer and target when the line of sight is projected onto the grid plane of zero altitude. See Figure 8.3 for the distinction. This procedure continued over a three hundred and sixty degree sweep about the observer, whenever the terrain permitted.

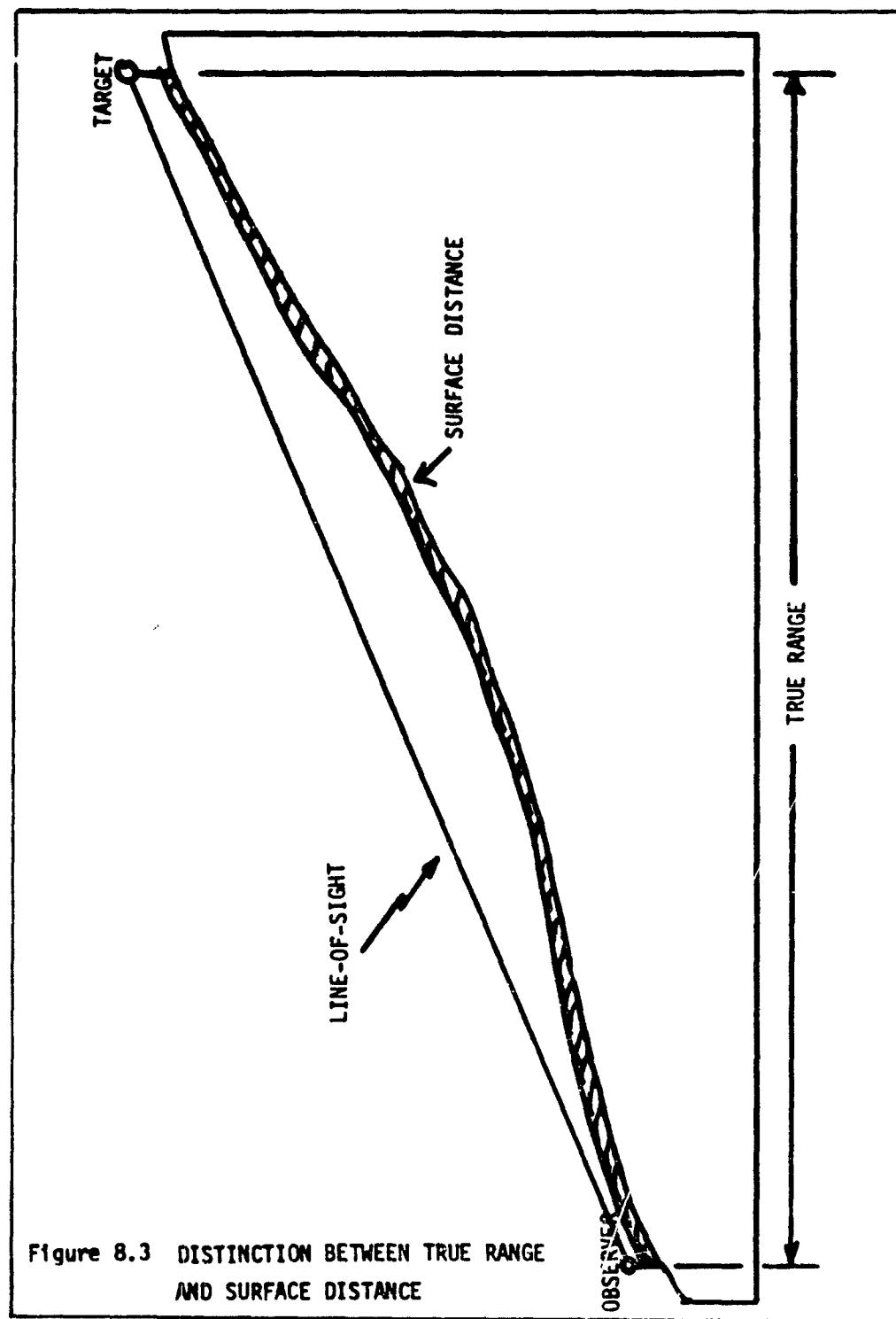
Line of sight data was collected at nine different locations. At each site, several direction headings and the corresponding surface distances were recorded. The nine locations are shown in Figure 8.1, and the experimental data is displayed in Figure 8.4.

8.2.4 Field Measurement Errors

In conducting an experiment of this type, four sources of error are inherent and must be taken into consideration using the data for validation purposes.

- Location Error: Exact determination of the observer's position (grid coordinates) is impossible. Minimizing the effects of this type of error was achieved basically by choosing observer positions near relief landmarks such as roads, peaks, saddle-points, and intersections.
- Compass Error: Compass readings are subject to errors due to alignment, sighting, and reading errors. An additional error source is in the estimation of magnetic north with respect to grid north. It is estimated that the combined effects of such errors amounts to $\pm 2^{\circ}$ error.
- Linear Measurement Error: All distances recorded on a map are given for a grid plane (of zero altitude) normal to any given elevation. The experiment, however, was conducted around sloping, hilly areas. Thus, the measured distance between the observer and target is the sloping surface ("slant") distance, and will be in error as a function of the distance and the difference in elevation between them. An approximation

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	POINT 1	POINT 2	POINT 3	POINT 4	POINT 5	POINT 6	POINT 7	POINT 8	POINT 9
MEAS 1	25m, 40°	71m, 85°	26m, 10°	31m, 5°	27m, 30°	67m, 115°	145m, 216°	65m, 100°	139m, 51°
MEAS 2	71m, 115°	15m, 25°	29m, 20°	31m, 15°	29m, 65°	63m, 125°	145m, 223°	60m, 115°	104m, 81°
MEAS 3	50m, 300°	23m, 355°	26m, 55°	35m, 30°	28m, 104°	61m, 140°	172m, 229°	67m, 136°	106m, 94°
MEAS 4									
MEAS 5									
MEAS 6									
MEAS 7									
MEAS 8									
MEAS 9									
MEAS 10									
MEAS 11									
MEAS 12									
MEAS 13									
MEAS 14									
MEAS 15									
MEAS 16									
MEAS 17									

Figure 8.4. Field Data (Hunter Liggett)

of this type of error is given by $D_E = D_M - D_M \cos(\theta)$, where D_E is the error in the distance measurement, D_M is the actual measured distance, and θ is the angle of elevation between observer and the target.

- Vegetation: As stated earlier, the intent of the experiment was to validate the SIAF model using line of sight verdicts with respect to macro-relief only. The effects of vegetation on line of sight were ignored. However, the presence of grass, sometimes several feet in height, could have introduced error into the measurements. This type of error is dependent on the density and height of the grass. The distance at which the line of sight is lost tends to be less in the presence of grass than otherwise. The effect of this error was minimized by choosing observer locations having very little vegetation (grass having negligible height) whenever possible.

8.3 ELEMENTS OF SIAF MODEL USED IN VALIDATION

8.3.1 Mathematical Representation at Macro-Relief in SIAF Model

The SIAF model utilizes a grid concept to describe macro-relief. Within each grid square a continuous surface is mathematically represented by a quadratic surface weighting all four corner elevation points. A region under consideration is assumed to be sufficiently small, so that effects due to earth's curvature are neglected, (i.e., a flat earth assumption is made, allowing use to use surface altitudes given by topographical maps). At each grid point, the earth's surface is specified by its altitude. Altitude data is available for grid resolutions as fine as 12.7 meters. The surface at nongrid points are determined as a weighted average of the four altitudes at the corner points of the grid square in which the point lies.

Consider Figure 8.5. Grid lines are defined by

$$x_j = (j-1)\Delta x$$
$$y_k = (k-1)\Delta y$$

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where Δx and Δy are grid square dimensions. The j, k^{th} rectangle is bounded by the grid lines $\{x=x_j, y=y_k, x=x_{j+1}, y=y_{k+1}\}$. The surface within the j, k^{th} grid square, as shown in Figure 8.5, is determined in the following manner where $z_{j,k}, z_{j,k+1}, z_{j+1,k}$ and $z_{j+1,k+1}$ are the input

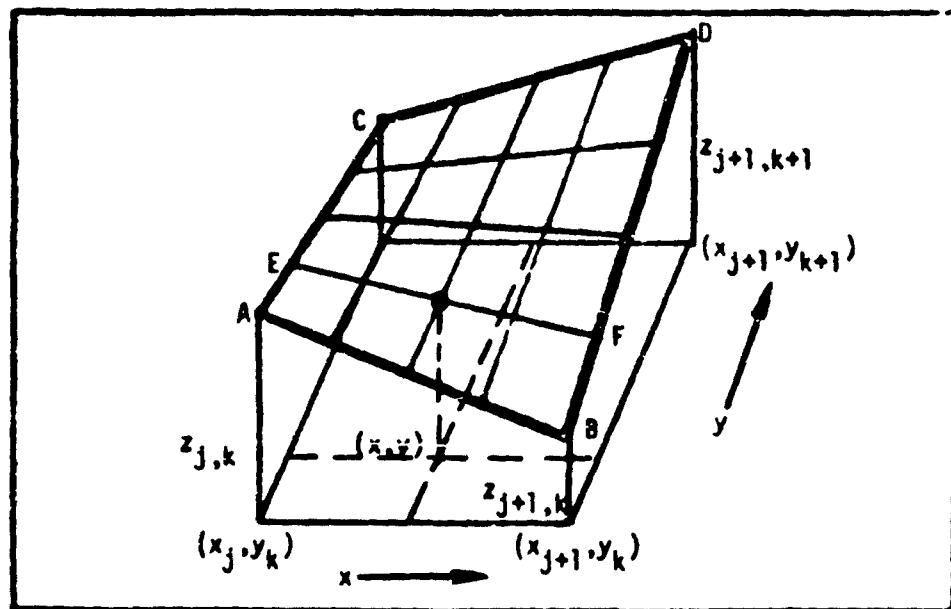


Figure 8.5, Surface Within j, k^{th} Rectangle

altitudes of the four corner points:

$$\text{Altitude on Line AB: } z_k(x) = \left[z_{j,k} + \frac{x-x_j}{x_{j+1}-x_j} (z_{j+1,k} - z_{j,k}) \right]$$

$$\text{Altitude on Line CD: } z_{k+1}(x) = \left[z_{j,k+1} + \frac{x-x_j}{x_{j+1}-x_j} (z_{j+1,k+1} - z_{j,k+1}) \right]$$

Altitude on Line EF (weighted average):

$$z(x,y) = \left\{ z_k(x) + \frac{y-y_k}{y_{k+1}-y_k} [z_{k+1}(x) - z_k(x)] \right\}$$

8.3.2 SIAF Subroutines Used

The subroutine LOSVEG is responsible for the line of sight calculations in the SIAF model. This subroutine is called by the subroutine DETERR. DETERR calculates intervisibility between any pair of points on the terrain for prone and upright positions of both the observer and the target. This intervisibility is characterized in terms of line of sight obstructions and various probabilities of cover and concealment. Cover and concealment are provided by micro-relief features and vegetation. Since the purpose of the field experiment was to consider macro-relief only, the line of sight experiments were performed in areas characterized by little or negligible amounts of micro-relief objects and vegetation. Thus the effects of cover and concealment on intervisibility are neglected in the simulation, and DETERR was modified to do this. Furthermore, for each pair of points on the terrain locating the observer and target, four lines of sight are considered by the subroutine DETERR.

- 1) "Head to head", i.e., observer and observed both upright.
- 2) "Head to foot", i.e., observer upright and observed prone.
- 3) "Foot to head", i.e., observer prone and observed upright.
- 4) "Foot to foot", i.e., observer and observed both prone.

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Since the field experiments considered only "head to head" lines of sight, DETERR was modified such that the simulation considered only that case.

The primary purpose of LOSVEG is to determine if the line of sight between an observer and target is obstructed by the intervening land surface (macro-relief). It accomplishes this by projecting the line of sight onto a grid plane (of zero altitude). Every intersection of the line of sight with horizontal and vertical grid crossings partitions the line of sight into segments. The subroutine checks for line of sight interruptions within or at the end-point of a given segment. This is done segment by segment, beginning with the segment containing the observer's position, until the line of sight is interrupted. If no interruption occurs the fraction of target height and the fraction of observer height covered by macro-relief is calculated; the routine continues on to compute cumulative distance through vegetation. It checks to see whether the cumulative distances through certain vegetation feature types is great enough to cause concealment of the target. This cumulative vegetation check, however, is of no concern to this test.

Detailed documentation and flow charts of LOSVEG and DETERR can be found in Volumes II and V respectively of the SIAF Users Manual.

8.4 COMPUTER SIMULATION OF FIELD TEST

The subroutines discussed above were modified and inserted into a program designed to simulate the line of sight experiments conducted at Hunter Liggett. The program considers only macro-relief features; it also takes into account several of the error sources which were inherent in the field experiments.

8.4.1 Simulation Methodology

The basic simulation procedure tries to model the actual experimental procedure conducted in the field. A given observer's position (grid coordinates on a topographic map) is determined as accurately as possible. Based on this determination, the program reads in all the elevation data in a square area centered about this point. The area is 444.5 grid points (using 12.7 meter resolution).

As in the actual experiments, the target is programmed to move away from the observer in a fixed direction. The target steps off increments of 3.175 meters away from observer. Every step increment initiates a call to subroutine DETERR, which in turn, calls LOSVEG to determine if a "head-to-head" line of sight exists. If it does the target takes another step of 3.175 meters away from the observer. The line of sight routine is called again. The procedure is repeated as long as the line of sight exists. This continues until either the line of sight no longer exists due to macro-relief obstruction, or the target has stepped off so many increments away from the observer that elevation data is no longer available for line of sight calculations. In the latter case, the distance between the observer and the target for which line of sight remains uninterrupted by macro-relief is considered to be unlimited.

Once the line of sight is obstructed, the target is programmed to move towards the observer. The step increment is reduced by half to 1.5875 meters. Again, each step increment initiates a call to the appropriate subroutines giving a line of sight verdict. The target is programmed to continue the inward movement until an uninterrupted line of sight is established again. As soon as the line of sight has been re-established, the target begins moving away from the observer once more. Now the step increments are made smaller ($1.5875 \div 2$). As before, each step gives rise to a line of sight verdict. The target continues moving away from the observer until the line of sight is interrupted by macro-relief again. At this instance, the range between the observer and target is recorded. In addition, the ranges between the observer and the line of sight intersections with grid crossings are recorded. These distances are needed to form an approximation of the actual surface between the observer and target. In short the simulation obtains data to approximate the surface distance by pinpointing the target's exact location (in a forward and backward manner) at the instant of line of sight obstruction.

The surface distance approximation is required because LOSVEG projects all lines of sight onto a grid plane of zero altitude, and computes all distances on this plane. Naturally, for extremely undulating relief, the linear range computed would be a poor approximation of the actual surface

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distance measured at Hunter Liggett. Figure 8.6 illustrates the estimation procedure. The distance between two successive grid crossings is computed. This is done for the C^{th} grid line by subtracting $D(C)$ from $D(C+1)$. The elevations at points where the line of sight intersect the two grid crossings are computed also ($ZZZ(C+1)$, and $ZZZ(C)$). The difference in elevation at these two points can be computed by subtracting $ZZZ(C)$ from $ZZZ(C+1)$. The surface distance from the C^{th} line is the length of the hypotenuse of the right triangle having sides $|D(C+1)-D(C)|$ and $|ZZZ(C+1)-ZZZ(C)|$. The estimation procedure is repeated for all grid squares having intersections with the line of sight; the results are summed to produce the surface distance from observer to target.

8.4.2 A Measure for Evaluating Validity

A comparison is made between the actual surface distance measured in the field and the estimated surface distance produced by the simulation. The absolute value of the difference between the actual and simulated surface distances is computed. This difference provides a measure for evaluating the credibility of:

- 1) the line of sight calculations and
- 2) the mathematical representation of macro-relief.

Specifically, a difference that approaches zero indicates that the simulation is producing reasonable results. However, a very small difference, or a difference of zero should not be interpreted as evidence of complete validity. It merely reflects that the line of sight algorithm, and the mathematical model for relief give reasonable estimates of the true situation.

8.4.3 Error Adjustments

Recall that the raw data from the field experiments was subject to four basic types of error. One such error involved inaccuracies in pin-pointing the exact location of the observer on a topographical map. A pencil point on a map of scale 1:50000, can be in error by as much as 20 meters. Furthermore, the exact location of the target is in doubt, not only due to the uncertainties in the observer's location, but due to

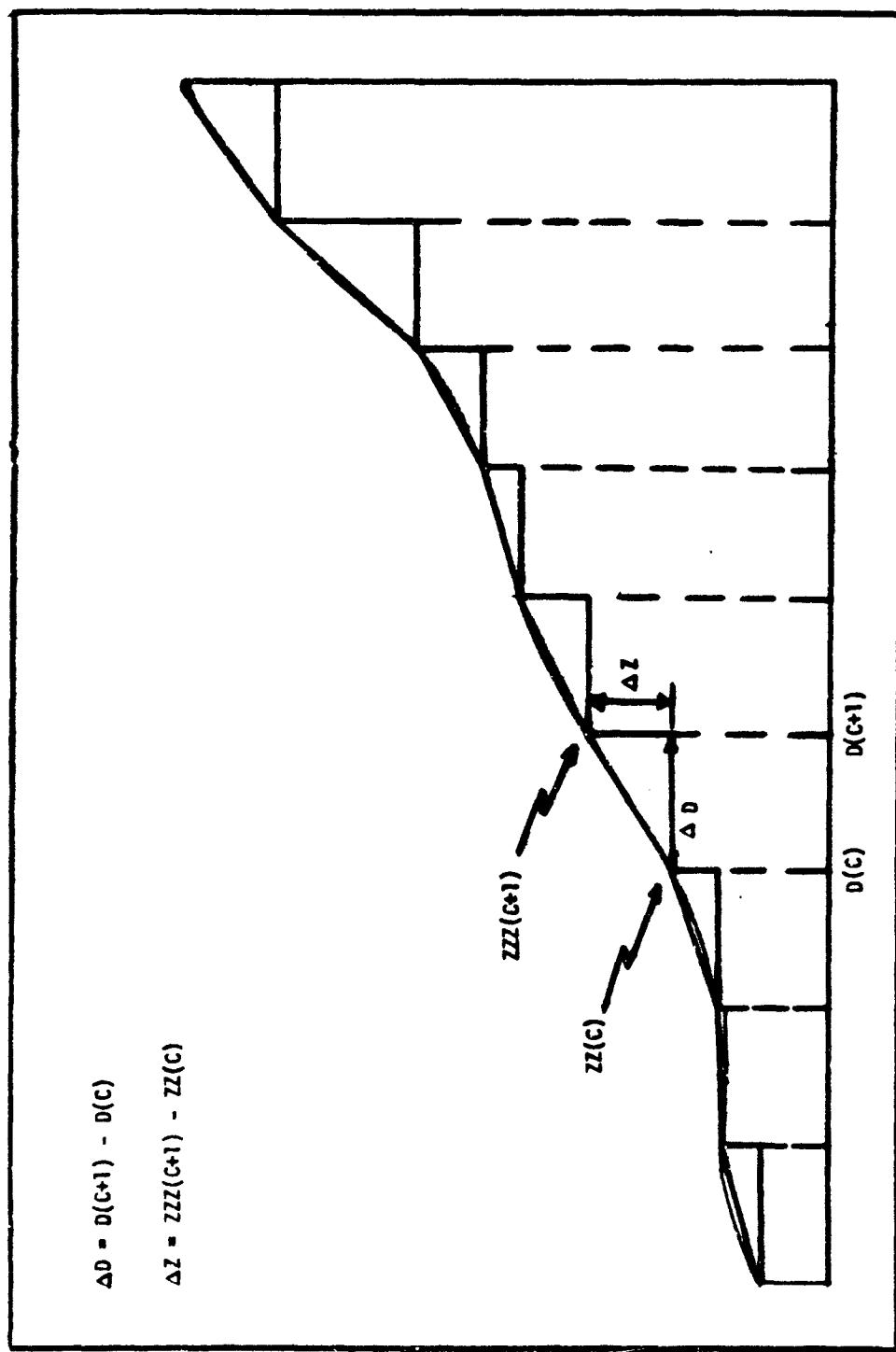


Figure 8.6 ESTIMATION OF SURFACE DISTANCE

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compass errors. The computer simulation attempts to correct such errors by:

- 1) considering a set of observer locations; and
- 2) slightly perturbing the angle of direction which locates the target relative to the observer.

Instead of investigating one possible observer location, the simulation considers a set of possible locations. Thirty-six equally spaced points within a 12.7 by 12.7 square area are analyzed. Each point is 2.54 meters apart. Thus, the input for "observer location" is not given by a pair of coordinates denoting a single point; it is given by a small grid area enclosing the most likely observer location. See Figure 8.7. This technique removes the guesswork involved with measuring map coordinates (by hand with a ruler), and places more emphasis on locating the observer's position relative to his immediate macro-relief environment.

At every observer location at Hunter Liggett, line of sight data was gathered in several different directions. The recorded angle (relative to magnetic north), for a given direction will be designated the "base angle." This angle contains small uncertainties due to compass reading errors. The simulation attempts to eliminate these uncertainties by perturbing the base angle slightly ($\pm 1^\circ$ and $\pm 2^\circ$). Thus, five different line of sight determinations are performed for a given direction:

- 1) the base angle determination;
- 2) base angle $+2^\circ$;
- 3) base angle $+1^\circ$;
- 4) base angle -1° ; and
- 5) base angle -2° .

In each case, the absolute value of the difference between actual and simulated surface distance is computed. The angle resulting in the smallest difference is chosen as the new "base angle" for that given direction. The same procedure is applied to each of the several other directions recorded at the experiment site.

In most instances, the simulation examined only three recorded directions at each experiment site. These three directions were chosen arbitrarily, but remained the same for each of the thirty-six points at

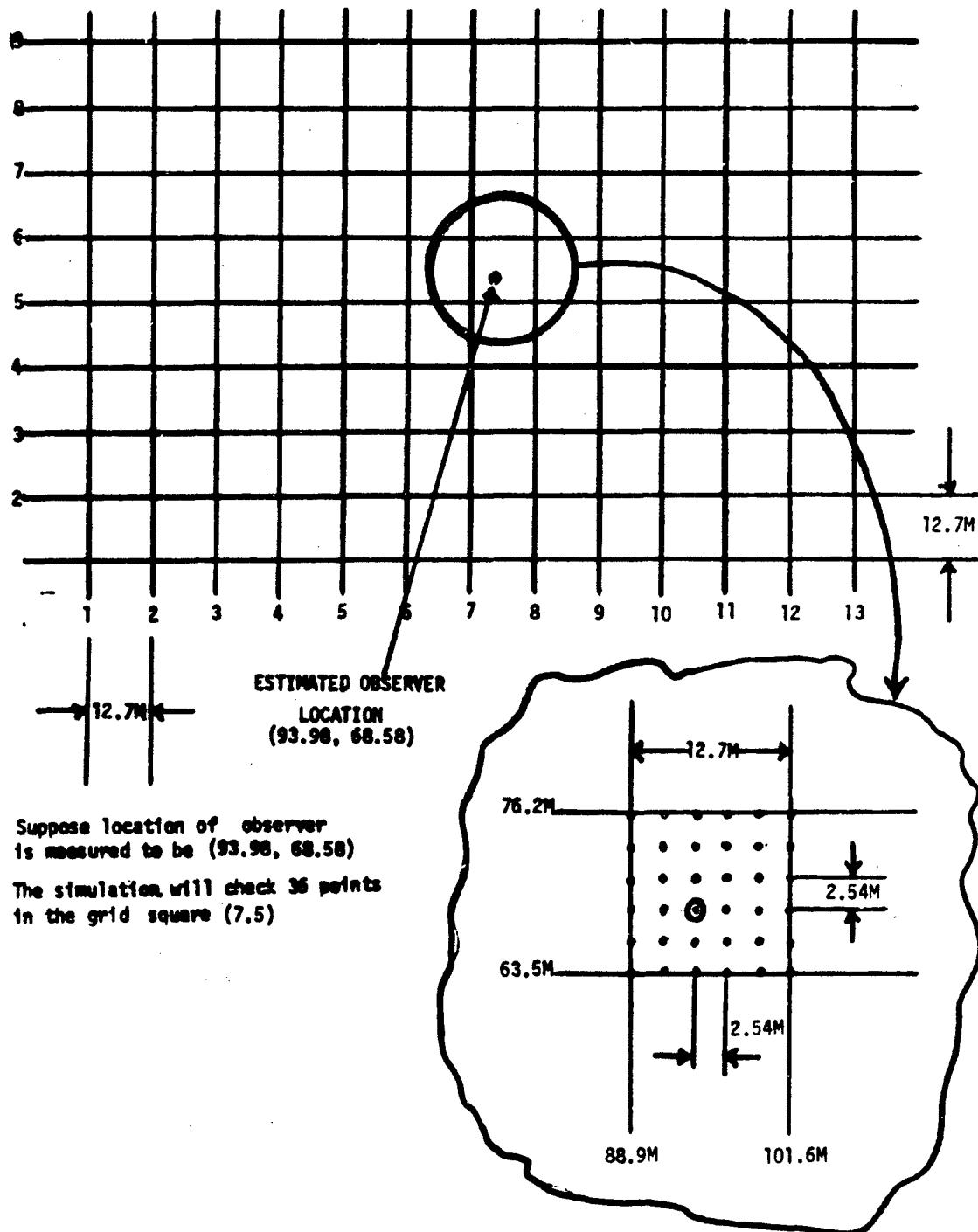


Figure 8.7 GRID OR OBSERVER LOCATION

a given location. Computer costs involved with examining more than three directions were prohibitive: the simulation considers thirty-six points. If three directions are examined, then fifteen line of sight experiments are performed (3×5). Thus there are $36 \times 15 = 360$ line of sight experiments performed for one location at Hunter Liggett.

8.4.4 Overall Measure of Validity

Recall that the absolute difference provided a measure of validity for a line of sight experiment conducted in one direction. But for each point, three different directions were analyzed. Thus a summary statistic, measuring the accuracy of line of sight calculations for all three directions, was needed.

The root mean square of the difference in each direction was chosen to measure the accuracy of all line of sight calculations at a given point. Specifically, the quantity measuring overall validity for line of sight calculations in all directions is given by:

$$\sqrt{\frac{\sum_{I=1}^N (D_A(I) - D_C(I))^2}{N}}, \text{ where } D_A(I) \text{ is the actual}$$

surface distance in the I^{th} direction, $D_C(I)$ is calculated surface distance in the I^{th} direction, and N is the number of directions analyzed ($N=3$ in this simulation). Thus every one of the thirty-six possible points under consideration has associated with it, a root mean square difference. This number reflects the accuracy of the simulation experiments at each of these points. The location of the point having the least root mean square difference is chosen to represent the actual position of the observer in the field experiment.

8.4.5 Simulation Using Different Resolutions

The simulations were conducted using three grid size resolutions. The initial simulation was done with elevation data available at grid points 12.7 meters apart. This was the finest resolution of elevation data available; hence this resolution was used to locate the actual

positions of the observer at the experiment sites. Having established these locations, the simulation was performed using coarser resolution: elevation data points 25.4 and 50.8 meters apart respectively. The simulation procedure using cruder resolution is exactly the same as described above, except that it no longer examines the set of thirty-six possible points for an actual location (it uses the actual locations derived from the initial simulation, thus avoiding a great deal of processing).

8.5 ANALYSIS OF SIMULATION RESULTS.

The root mean square (of differences between actual and simulated surface distance in all line of sight directions examined for a given experiment site at Hunter Liggett) provides a measure for evaluating the validity of the line of sight routines and macro-relief representation. Figure 8.8 gives these measures for all nine Hunter Liggett experiment sites, at the various resolutions used in the simulation. Figure 8.9 presents the simulation results broken down into individual line of sight experiments. The overall root mean square difference is given on this figure also.

As Figure 8.8 indicates, the simulation performed under 12.7 meter resolution produce very credible results. The results using 25.4 and 50.8 meter resolution are credible, but not as sharp. The reason for this is that the line of sight interruption distances measured are relatively short (i.e., with respect to the length of the side of the grid squares). Many of the line of sight obstruction distances measured at Hunter Liggett were less than 100 meters in length. These short distances do not affect the simulation when the resolution is very fine (i.e., 12.7 meter resolution), but as the resolution becomes coarser, the simulation results are more inaccurate. It must be stressed that this happens only when simulation is attempted over very short lines of sight using very coarse resolution. The inaccuracies appear in the form of large root mean square differences. Coarse resolution should be used in line of sight determinations when the observer and target are over 200 meters away.

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SITE	12.7 METERS RESOLUTION		25.4 METERS RESOLUTION		50.8 METERS RESOLUTION	
	ROOT MEAN SQUARE	PERCENT	ROOT MEAN SQUARE	PERCENT	ROOT MEAN SQUARE	PERCENT
1	5.9M	10.6	8.2M	42.7	67.8M	107.0
2	1.7M	3.3	18.6M	50.0	11.5M	43.0
3	1.6M	4.0	4.7M	40.6	*	100.
4	0.3M	0.5	4.7M	12.3	39.0M	107.2
5	2.1M	5.0	24.6M	82.8	38.9M	105.9
6	2.7M	4.6	10.0M	13.7	31.0M	52.8
7	8.1M	4.9	40.1M	25.9	67.7M	62.9
8	9.1M	9.7	16.0M	19.7	39.6M	71.8
9	3.0M	1.7	22.6M	12.1	48.1M	52.3

* UNLIMITED LINE OF SIGHT (i.e., TARGET HAS STEPPED OFF SO MANY INCREMENTS FROM OBSERVER THAT ELEVATION DATA IS NO LONGER AVAILABLE FOR LOS CALCULATIONS). FIGURE 8.10 ILLUSTRATES HOW THIS CAN HAPPEN.

FIGURE 8.8 ROOT MEAN SQUARE ERROR AT DIFFERENT RESOLUTIONS

SITE	RESOLUTION	DIRECTION 1		DIRECTION 2		DIRECTION 3		ROOT MEAN SQUARE
		MEASURED DISTANCE	ERROR	MEASURED DISTANCE	ERROR	MEASURED DISTANCE	ERROR	
1	12.7		1.8		6.3		7.8	5.9
	25.4	25.	*	71.	6.8	50.	9.3	8.2
	50.8		*		25.3		92.	67.8
2	12.7		1.9		2.2		-9	1.7
	25.4	71.	-8.2	68.	25.	23.	*	18.6
	50.8		-15.6		4.6		*	11.5
3	12.7		.9		-4		-2.6	1.6
	25.4	26.	*	29.	1.1	36.	6.5	4.7
	50.8		*		*		*	*
4	12.7		.0		-3		.3	0.3
	25.4	36.	-6.8	29.	3.2	47.	-3.0	4.7
	50.8		*		50.1		-23.0	39.0
5	12.7		-3.6		.0		.7	2.1
	25.4	27.	*	28.	30.6	42.5	-16.6	24.6
	50.8		*		56.		9.0	38.9

*Unlimited Line of Sight (i.e., target has stepped off so many increments from observer that elevation data is no longer available for LOS calculations). Figure 8.10 illustrates how this can happen.

Error = $D_C(I) - D_A(I)$ where $D_C(I)$ is the calculated surface distance in the I^{th} direction and $D_A(I)$ is the actual measured surface distance in the I^{th} direction.

Figure 8.9. Detailed Simulation Results (Sheet 1)
 (ALL MEASUREMENTS IN METERS)

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SITE	RESOLUTION	DIRECTION 1		DIRECTION 2		DIRECTION 3		ROOT MEAN SQUARE
		MEASURED DISTANCE	ERROR	MEASURED DISTANCE	ERROR	MEASURED DISTANCE	ERROR	
6	12.7	61.	-1.8	61.	-3.7	49.	-2.4	2.7
	25.4		-14.5		-9.3		1.0	10.0
	50.8		-33.5		-35.8		-21.9	31.0
7	12.7	145.	11.8	145.	5.3	172.	-6.2	8.1
	25.4		30.0		50.8		27.0	40.1
	50.8		43.3		65.4		*	67.7
8	12.7	67.	-10.6	68.	-11.8	57.	.0	9.1
	25.4		-10.1		-24.0		9.5	16.0
	50.8		*		38.0		41.2	39.6
9	12.7	139.	.6	118.	5.1	152.	.5	3.0
	25.4		-12.9		-1.1		40.	22.6
	50.8		-67.4		9.8		*	48.1

*Unlimited line of sight (i.e., target has stepped off so many increments from observer that elevation data is no longer available for LOS calculations). Figure 8.10 illustrates how this can happen.

Error = $D_C(I) - D_A(I)$ where $D_C(I)$ is the calculated surface distance in the I^{th} direction and $D_A(I)$ is the actual measured surface distance in the I^{th} direction.

Figure 8.9, Detailed Simulation Results (Sheet 2)

(ALL MEASUREMENTS IN METERS)

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Figure 8.10 demonstrates what can happen when line of sight calculations are conducted over a short distance using various resolutions. An observer and target, both of height 1.8 meters, stand 12 meters apart. Macro-relief described with 12.7 meter resolution indicates a line of sight interruption at approximately 6.7 meters from the observer. However, no such line of sight interruption occurs when describing macro-relief with 25.4 or 50.8 meter resolution. The figure shows that the hump at about 6.7 meters from the observer is not modeled when describing macro-relief using the cruder resolutions. This explains why some of the root mean square differences are so large when the simulation was run using 25.4 and 50.8 resolution (recall that the target keeps moving away from the observer until a verdict of obstruction is given).

The simulation results particularly those obtained when using the 12.7 meter resolution demonstrate that the SIAF line of sight routine and the SIAF representation of macro-relief are "reasonable". Furthermore, line of sight calculations are sensitive to resolution when the distance between observer and target is small (i.e., less than 100 meters). For the reason, the SIAF concept of switching resolution (using less resolution in the Reconnaissance Mode when long distances are involved; and finer resolution in the Combat Mode when shorter distances are involved, and more detailed computation are required) appears well founded.

8.6 SUMMARY

Line of sight data was collected at nine different locations at the Hunter Liggett Military Reservation. At each location, line of sight experiments were conducted in several different directions. Inherent errors in compass reading and in locating positions on a topographical map required the simulation to consider a set of possible locations and to vary the directions between observer and target. The initial simulation examines a set of thirty-six equally spaced (2.54 meters apart) points enclosed in a 12.7 by 12.7 meter grid square. Each of the thirty-six points are analyzed as follows. Three arbitrary experimental directions were chosen. Each direction is perturbed by $\pm 1^\circ$ and $\pm 2^\circ$, so that five line of sight verdicts are obtained. The verdict which offers the minimum

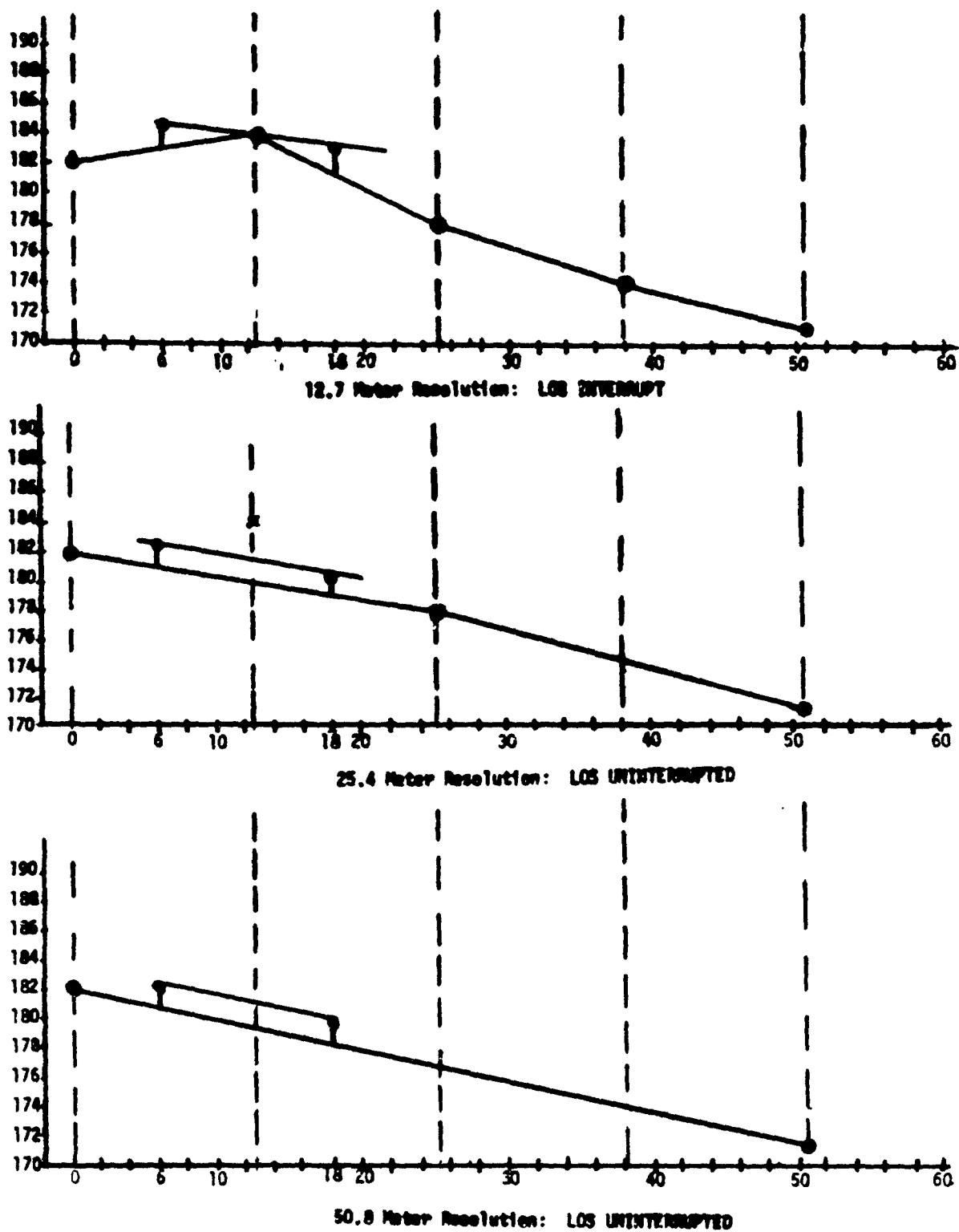


Figure 8.10 LOS VERDICT USING DIFFERENT RESOLUTIONS

difference between actual and computed surface distance determines the base angle for that direction. Thus each direction has associated with it, a measure of how accurate the simulation was. The root mean square of these individual differences gives an over measure of how accurate the simulation of the field experiment was at that point. The root mean square difference is given by:

$$\sqrt{\frac{\sum_{I=1}^N \{D_A(I) - D_C(I)\}^2}{N}}$$

where $D_A(I)$ is the actual surface distance, $D_C(I)$ is the computed surface distance, and N is the number of directions analyzed.

The initial simulation examines thirty-six possible points for a given experiment location, thus producing thirty-six root mean square differences. The location of the point having smallest root mean square is considered the site where the line of sight experiment actually took place. All nine experiment sites at Hunter Liggett were determined by the above procedure.

The simulation was repeated using resolutions of 25.4 and 50.8 meters. The same procedure was applied, except the observer positions are inputted (from initial simulation) instead of calculated.

The results of the simulation demonstrate that the SIAF line of sight calculations and the SIAF model of macro-relief are valid. Also, when the distance between observer and target is small (i.e., less than 100 meters), the line of sight calculations are dependent on resolution.

8.7 COMPARISON WITH ASARS BATTLE MODEL

Macro-relief models usually employ a grid square concept in which elevation data is known at four corners of each grid. The elevation at points lying between these data points are represented by an interpolated value using the known data points. Different methods are used to obtain these interpolated values. As mentioned before, the STAF model uses a continuous

surface representation within a grid square based on the four surrounding grid points. A less complex method uses two intersecting triangular planes within a grid square to obtain interpolated values. This scheme is used in the ASARS model. The simulation experiment was done utilizing both representations of macro-relief; the results were compared.

8.7.1 ASARS Methodology

ASARS macro-relief is modeled by specifying two triangular planes within a grid square. The planes are defined by specifying a diagonal within the grid square (a positive diagonal if it connects the lower left corner with the upper right corner; a negative diagonal if it connects the upper left corner with the lower right corner). The orientation of the diagonal is the same for all grid squares under consideration. Positive diagonals were used in the simulation.

The line of sight subroutine in the ASARS model is basically a series of comparisons. The line of sight between the observer and the target is projected onto a grid plane (of zero altitude) and partitioned into a set of segments. The endpoints of these segments are defined by the intersection of the line of sight with horizontal and vertical grid crossings and with diagonals. Initially, the horizontal distance between observer and target, and the vertical difference in elevation between the top of the observer and the top of the target are computed. These quantities are used to compute the tangent of the angle subtended by the line of sight and a horizontal line parallel to the grid plane at the top of the observer. This tangent value is designated "TANLIM".

The line of sight routine proceeds as follows: the elevation of the ground surface at an endpoint of a segment is referenced. The horizontal range from the observer to the endpoint is computed. These quantities are used to compute the tangent of the angle subtended by the line extending from the top of the observer to the ground surface at that endpoint, and the horizontal line parallel to the grid plane at the observer's height. Call this quantity "TAN". Figure 8.12 illustrates the above procedure. A comparison is made between TANLIM and TAN, to determine the line of sight verdict: If TAN is greater than or equal to TANLIM, the line of sight is interrupted at that endpoint. Otherwise, the line of sight exists and the

SITE	RESOLUTION	DIRECTION 1			DIRECTION 2			DIRECTION 3				
		MEAS. DIST.	SIAF ERROR	ASARS ERROR	MEAS. DIST.	SIAF ERROR	ASARS ERROR	MEAS. DIST.	SIAF ERROR	ASARS R.M.S.	SIAF R.M.S.	ASARS R.M.S.
1	12.7	25.	1.8	1.4	71.	6.3	5.3	50.	7.8	*	5.9	3.9
	25.4		*	*		6.8	*		9.3	94.9	8.2	94.9
	50.8		*	*		26.3	*		92.	189.2	67.8	189.2
2	12.7	71.	1.9	.9	65.	2.2	-2.7	23.	-.9	1.6	1.7	1.9
	25.4		-8.2	-3.0		25.	-172.0		*	*	18.6	121.8
	50.8		-15.6	175.3		4.5	171.0		*	*	11.5	173.2
3	12.7	26.	.9	15.	29.	-.4	5.8	36.	-2.6	9.8	1.6	10.9
	25.4		*	131.6		1.1	*		6.5	*	4.7	131.6
	50.8		*	69.7		..	*		*	*	*	69.7
4	12.7	35.	.0	7.0	29.	-.3	-6.1	47.	.3	.5	.3	5.4
	25.4		-6.8	182.7		3.2	201.4		-3.0	179.1	4.7	188.0
	50.8		*	*		50.1	201.5		-23.0	178.4	39.0	190.3
5	12.7	27.	-3.6	-2.4	28.	.0	-4.7	42.5	.7	-10.2	2.1	6.6
	25.4		*	*		30.6	*		-16.6	*	24.6	131.6
	50.8		*	*		55.	104.8		9.0	170.7	38.9	141.6

* UNLIMITED LINE OF SIGHT (i.e., TARGET HAS STEPPED OFF SO MANY INCREMENTS FROM OBSERVER THAT ELEVATION DATA IS NO LONGER AVAILABLE FOR LOS CALCULATIONS). FIGURE 8.10 ILLUSTRATES HOW THIS CAN HAPPEN.

ERROR = $D_C(I) - D_A(I)$ WHERE $D_C(I)$ IS THE CALCULATED SURFACE DISTANCE IN THE I^{TH} DIRECTION AND $D_A(I)$ IS THE ACTUAL MEASURED SURFACE DISTANCE IN THE I^{TH} DIRECTION.

FIGURE 8.11 SIAF AND ASARS SIMULATION RESULTS (SHEET 1)
(ALL MEASUREMENTS IN METERS)

SITE	RESOLUTION	DIRECTION 1			DIRECTION 2			DIRECTION 3				
		MEAS. DIST.	SIAF ERRONE UR	ASARS ERRONE UR	MEAS. DIST.	SIAF ERRONE UR	ASARS ERRONE UR	MEAS. DIST.	SIAF ERRONE UR	ASARS R.H.S. R.M.S		
6	12.7	61.	-1.0	-8.3	61.	-3.7	-23.6	49.	-2.0	-23.8	2.7	20.6
	25.4		-14.5	32.5		-9.3	31.1		1.0	98.9	10.0	62.7
	50.8		33.5	39.3		35.8	360.7		-21.9	*	31.0	330.
7	12.7	148.	11.8	-38.7	148.	8.3	-37.3	172.	-5.2	*	8.1	36.5
	25.4		39.0	112.9		38.8	20.9		27.0	26.7	40.1	68.1
	50.8		43.3	38.2		38.4	66.4		*	29.2	67.7	68.0
8	12.7	67.	-10.5	2.8	69.	-11.8	15.5	57.	*	*	9.1	11.1
	25.4		-10.1	21.9		-24.0	*		9.5	64.2	16.0	39.2
	50.8		*	48.1		38.0	38.0		41.2	22.7	39.6	120.
9	12.7	139.	.6	50.	118.	5.1	*	152.	.5	51.0	3.0	55.7
	25.4		-12.9	30.3		-1.1	43.4		40.	*	22.6	137.0
	50.8		-67.4	212.		9.8	144.3		*	*	40.1	181.3

* UNLIMITED LINE OF SIGHT (I.e., TARGET HAS STEPPED OFF SO MANY INCREMENTS FROM OBSERVER THAT ELEVATION DATA IS NO LONGER AVAILABLE FOR LOS CALCULATIONS). FIGURE 8.10 ILLUSTRATES HOW THIS CAN HAPPEN.

ERROR = $D_C(U) - D_A(I)$ WHERE $D_C(I)$ IS THE CALCULATED SURFACE DISTANCE IN THE I^{TH} DIRECTION AND $D_A(I)$ IS THE ACTUAL MEASURED SURFACE DISTANCE IN THE I^{TH} DIRECTION

FIGURE 8.11 SIAF AND ASARS SIMULATION RESULTS (SHEET 2)

(ALL MEASUREMENTS IN METERS)

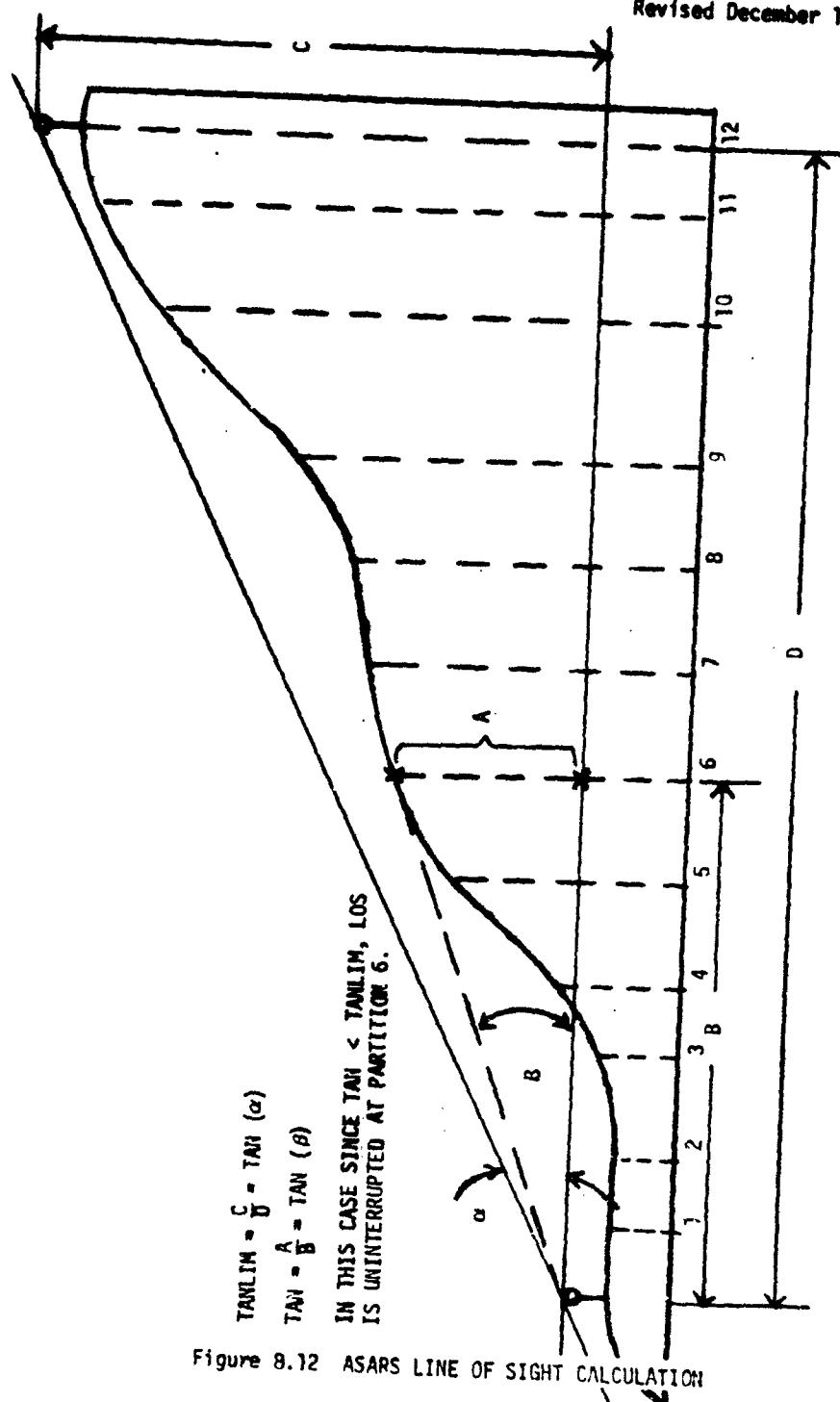


Figure 8.12 ASARS LINE OF SIGHT CALCULATION

procedure is repeated at the next endpoint.

The above procedure starts at the observer position and continues toward the target, until line of sight interruption occurs. If no interruption occurs, the fraction of target height covered by intervening macro-relief is computed.

The ASARS method of representing macro-relief along with the ASARS line of sight routine were inserted into the simulation program. Appropriate minor modifications in the simulation program were made to accommodate the change. Otherwise, the exact methodology used in the SIAF macro-relief simulation was followed for the ASARS simulation.

8.7.2 Comparison

The simulation results using the ASARS macro-relief model did not compare as well as those of the SIAF simulation. The ASARS simulation produced credible results at 12.7 meters resolution. As figure 8.11 indicates, the SIAF results at this resolution were generally better than those returned by the ASARS method (though in some instances the ASARS method gave better approximations). At coarser resolutions (25.4 and 50.8 meters), the SIAF results were significantly better. In almost every instance, the SIAF simulation gave smaller errors, and thus smaller root mean square differences. Also, the ASARS simulation produced more instances where erroneous "unlimited" lines of sight were given (see figure 8.10 for explanation).

The large root mean square differences at the coarser resolutions may be attributed to the less accurate scheme for approximating macro-relief. Interpolated values in the SIAF model use data from all four surrounding grid points, whereas the ASARS model use only three of the four data points available. In addition, the ASARS relief model has the disadvantage that the choice of which grid square diagonal to use in forming the two triangular planes must be held constant throughout the entire gridded area under consideration. This disadvantage results in a loss of realism (this method does not give a unique representation of relief). A situation depicted in figure 8.13 illustrates this disadvantage. In both case 1 and case 2, the same set of four data points is input. Suppose case 2 is the desired approximation (ridge), but because positive diagonals (lower left corner to upper right corner) was the established choice of diagonal orientation, we

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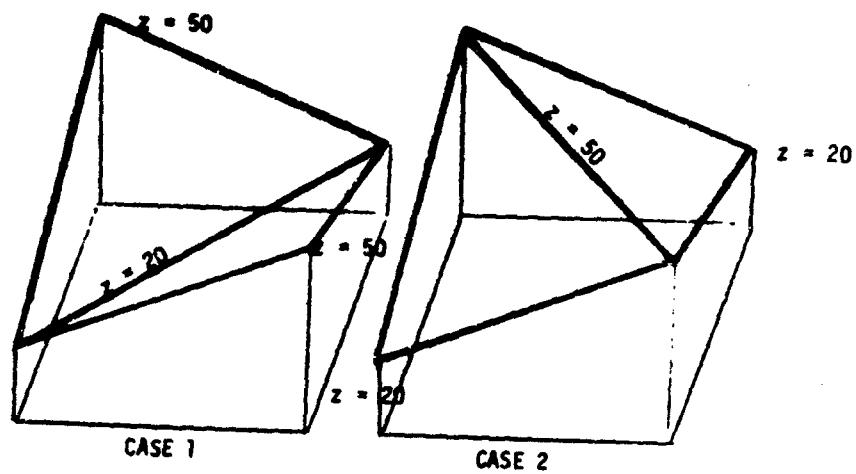


Figure 8.13 Non-Unique Terrain Surface Representation

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obtained an inaccurate representation (ravine). Clearly, the two surfaces resulting are quite different depending on the choice of diagonals. Thus, in comparison, it appears that the two-triangular-plane method of ASARS requires a smaller grid size to represent macro-relief to the same resolution as the four-point continuous surface scheme of SIAF.

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9.0 REFERENCES

1. S. Q. Duntley, et al, "Visibility," Applied Optics, Volume 3, Number 5, May 1964.
2. "Training for SIAF, Program Description Number 1: Land Navigation," HumRRO Division 4.
3. Army Map Sheets, Numbers 1755 IV NE, 1755 I NW, 1755 IV SE, and 1755 I SW, for Alder Peak, California, 1:25,000.
4. TRW Systems Group, "SIAF Model Development, Validation, and Implementation Final Report," 16905-6012-R0-00.

APPENDICES

Included herein are Appendix A, Block Data Generator Program and Appendix B, Specification Statement Punch Program (SPECPN) User's Guide.

These Appendices describe two computer programs which were originally written for the IBM 7094. These programs have recently been modified to run on the IBM 360, and in the process an additional change has been made.

The main external difference in the programs is that BLKGEN no longer punches a BLOCK DATA subprogram which must be input to SPECPN. The necessary information is written on tape and is read back directly into the necessary COMMON blocks for SPECPN. This eliminates the need for two separate passes through the machine, since the two programs can be run as one single program. They can, however, be run as separate phases if necessary, using a previously generated tape as input to SPECPN.

The conversion to the 360 was handled in this manner for several reasons:

1. It eliminated the need for unnecessary card handling associated with a punched BLOCK DATA.
2. It eliminated the need for two separate passes through the machine, since there is no need to compile a BLOCK DATA subprogram, and thus improved turnaround.
3. It improved the running time of the program by eliminating the punching of the BLOCK DATA.

The inputs to both BLKGEN and SPECPN remain unchanged from those described in Appendix A and Appendix B. The 360 version can thus be run using existing decks with no modifications. However, since the programs have been combined utilizing a short driver, an additional control card is necessary to specify whether BLKGEN, SPECPN, or both are to be executed. This control card must precede all other data. Card column 1 is punched non-zero if it is desired to execute BLKGEN; card column 2 is punched non-zero if it is desired to execute SPECPN.

The appropriate column is punched zero or left blank if it is desired to skip execution of either program. The standard input decks follow this card, with no separation between BLKGEN and SPECPN inputs, if both are being run. The output will be identical to that of the 7094 version, with the exception of a punched BLOCK DATA.

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APPENDIX A
BLOCK DATA GENERATOR PROGRAM
(BLKGEN)
User's Guide

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I. History:

Because many large programs use COMMON quite extensively, it has become a common practice to set up all the variables of a program, equate them to blocks, and put all the blocks in a COMMON array. In order to use the variables in a subroutine, one would have to write COMMON, DIMENSION, and EQUIVALENCE cards for each variable. It soon became apparent that it would be desirable to be able to generate these COMMON, DIMENSION, and EQUIVALENCE statements by some external means. The Specification Statement Punch Program (SPECUPN)¹ fulfills this desirability, but it requires a rather complicated BLOCK DATA sub-program to be written by the user to describe all the variables in COMMON.

The BLKGEN program was written to generate this BLOCK DATA sub-program from input cards which are easily written and changed. The combination of the BLKGEN and SPECUPN programs allow an easy way to create and update a master COMMON of blocks and variables. By using these two programs, it should be fairly easy for one to generate the COMMON, DIMENSION, and EQUIVALENCE cards for each subroutine.

II. Usage:

For a picture of the organization and the usage of the BLKGEN and SPECIN programs, look at Section V. It can be seen that the usage of the two programs requires two passes on the computer. On the first pass, the master input cards are input to the BLKGEN program. The output of the BLKGEN program is the BLOCK DATA sub-program punched on cards. The BLOCK DATA sub-program is input with the variable names for each subroutine to the SPECIN program on the second pass. The second pass output are the COMMON, DIMENSION, and EQUIVALENCE cards which are directly placed into the respective subroutines.

Since the specific usage of the SPECIN program is given in the SPECIN User's Guide, the only additional required information is the format of the input cards to the BLKGEN program. There are nine different cards accepted as input to the BLKGEN program, and each is described below:

1. IDENT Card:

The IDENT card is always the first card input to a run. The word IDENT starts in c.c. 1 and the number of cards that are to follow the IDENT card to describe the job is punched in c.c. 30. If c.c. 30 contains a 3, then there are three cards which contain information describing a run.

Example:

c.c. 1 10 c.c. 30
IDENT 70 1

THIS IS A SAMPLE RUN

The information punched on the card(s) following IDENT appears as comments in the BLOCK DATA program generated by BLKGEN. Columns 1 - 71 may be used for the comments cards.

2. PROGRAMMER Card:

The PROGRAMMER card simply contains identification information concerning the programmer, and it is always the second control card in a run following IDENT and the comment cards specified by IDENT. The word PROGRAMMER starts in c.c. 1, and the programmer's name follows immediately after (one space is skipped). Up to 24 characters may be used for the PROGRAMMER name.

Example:

c.c. 1

c.c. 12

PROGRAMMER

J. Gerry Purdy

3. DATE Card:

The DATE card must always be the third control card in any run. The word DATE starts in c.c. 1, followed by a blank, followed by the date.

Example:

c.c. 1

c.c. 7

DATE

November, 1966

Following the IDENT, PROGRAMMER, and DATE control cards are the cards which actually describe the COMMON blocks of the user's program. Each COMMON block is described separately in the following way:

- a) The actual cards which define the COMMON block of interest are presented to BLKGEN.
- b) Each master variable name of interest from the above defined COMMON block is denoted followed by a series of control cards identifying the variables within the master variable, their dimension, and their relative position within the block.
- c) After all master variables have been described a signal is given (ENDCOM) and the next COMMON block is defined. Following the last COMMON block definition a signal is given (ENDJOB) terminating the job. Each control card will now be described.

4. COMMON Card:

The COMMON control card must be the first card of each COMMON set. The number of cards that are to follow is placed in c.c. 30. What follows is the card or cards which define the COMMON block exactly as they would be punched for the user's program.

Example:

c.c. 1	c.c. 30
--------	---------

COMMON	2
--------	---

COMMON/VSTR/BLK(50), B(6), 30(36)
c (..)

In this example, cards are used to define the COMMON block VSTR. BLXGEN constructs a card image of these COMMON statements and places it in the FMT array in the output BLOCK DATA cards for processing by SPECPN.

Only 1 COMMON block name (e.g. VSTR) may be defined per use of COMMON. Subsequent COMMON entries would be used if the user has more than 1 COMMON block in his program. Blank or labeled COMMON blocks are acceptable. A maximum of 9 cards may be used for each COMMON block definition.

5. M Card:

The M card identifies the block name under the current COMMON. The M is placed in c.c. 1, the block name (up to 6 characters) starts in c.c. 10, and the description of the block (up to 24 characters) starts in c.c. 40.

Example:

c.c. 1	c.c. 10	c.c. 40
--------	---------	---------

M	BLK1	FLOATING CONSTANTS
---	------	--------------------

Sets of M and subsequent V cards may be repeated for each block in the current COMMON. The order in which the blocks are processed from the COMMON cards is arbitrary and the descriptions given starting in c.c. 40 are optional.

6. V Card:

The V card is the variable card and contains information about the variable which is contained within the current block. The V is in c.c. 1, the variable name (up to 6 characters) starts in c.c. 10, the dimension, if any, ends in c.c. 30, and the description of the variable (up to 24 characters) starts in c.c. 40, (optional). Singly dimensioned variables are indicated by placing a "1" or blank in c.c. 30.

Example:

c.c. 1 c.c. 10 c.c. 30 c.c. 40
V CGMR 10 GM RATIO OF E, M, S, V, M, S, J, TO EARTH.

7. JUMP Card:

The JUMP card allows spaces to be skipped in the current block for perhaps future expansion. The word JUMP begins in c.c. 1 and the number of spaces to be skipped ends in c.c. 30.

Example:

c.c. 1 c.c. 30
JUMP ↓
 20

The above card would cause a "hole" of 20 cells to be made in the current COMMON block.

8. ENDCOM Card:

The ENDCOM Card is simply a signal to the program that the current COMMON block is finished. The ENDCOM starts in c.c. 1.

Example:

c.c. 1
ENDCOM

Following the ENDCOM card is either a new COMMON card or the ENDJOB card.

9. ENDJOB Card:

The ENDJOB card is simply a signal to the program that the inputs are finished. It is always the last card in a job.

Example:

c.c. 1
ENDJOB

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III. Sample Inputs:

On the following pages is a listing of a sample set of input cards to the BLKGEN program. No labeled COMMON was used in this case, although both labeled and blank COMMON will work.

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COMMON VARIABLES IN ALPHABETICAL ORDER

VARIABLE	COMMON NAME	PSN	SIZE	DEFINITION	BLOCK NAME
NS		202	4		COMM83
WT		232			MISC81
WT		203			COMM83
WV		201			COMM83
W1		44			COMM83
W2		45			DLOGBL
WBAR		530	16,4		DATABB
XBASE		1401			LINSIG
XAMR		1			USIBBB
XAVODD		21			COMMBS
XAVOID		60			MISC82
XDEFOP		81			MISC82
XDEPL		77			DLOGBL
XDEPL		48			DLOGBL
XEE		203			MISC82
XB		205	5,20		COMM83
XDYNOL		333	1		COMM83
XDYN		82	200		MISC82
XENG		56			DLOGBL
XE		262			MISC82
XICIR		49			COMMBS
XGOAL		1			DLOGBL
XLP		609	20		TARINT
XPAKWT		242	16		DATABB
XOB		1402	1000		MISC81
XLZ		305	5		LINSIG
XOP		50			COMM83
XPLAN		50			DLOGBL
XPPTT		1			USTARS
XPPT		205	103,5		MISC82
XPPT		264			MISC82
XSTAR2		8	20		OBSTAB
XSTAR		312	21		COMM83
XTAU		7			OBSTAB
XP2		240			MISC81
XP3		241			MISC81
XSIAF		28			OBSTAB
XSIG		6			OBSTAB

Figure 7-2, Cross-reference of Common Variables (Sheet 16)

Figure 7-2. Cross-reference of Common Variables (Sheet 16)

COMMON VARIABLES IN ALPHABETICAL ORDER			
VARIABLE	COMMON NAME	COMMON DIMENSION	DEFINITION
V2FREN	ZDEPL	6	
ZENG	ZENGL	5	
ZTAU	ZTAU	6	
ZETA	ZETA	6	
ZSIG	ZSIG	2	
ZDEPL	ZDEPL	5	
PSN	PSN	5	
NAME	NAME	1	
BLOCK	NAME	1	
US1000	US1000	1	
01681	01681	1	
01682	01682	1	
01683	01683	1	
085148	085148	1	
085149	085149	1	
COMM83	COMM83	1	
OBSTAB	OBSTAB	1	

Figure 7-2. Cross-reference of Common Variables (Sheet 17)

Figure 7.3, Overlay Structure (1 Page)

THIS IS A FORTRAN IV
PROGRAMMER J. GERRY ANDREY
DATE NOVEMBER, 1966

PROGRAM TO GENERATE COMMON,
CONSTANTS FOR THE ISP PROGRAM.

COMMON	BLK1	4	BLK1 (125), BLK2 (50), BLK3 (100), BLK4 (50)	
1. BLK5 (50), BLK6 (200), BLK7 (200), BLK8 (500), BLK9 (75)				
2. BLK10(200), BLK11(200), BLK12(50), BLK13(50), BLK14(200)				
3. BLK15(300)				
BLK1				
CAE				
CBE				
CELLIP				
CMU				
CWE				
CGMR	10			
RCB	10			
CERAU				
CFTER				
CIN1				
CIN2				
COUT1				
COUT2				
CLIGHT				
CNMER				
CKMER				
CSOLC				
CDAYMN	12			
CDEG				
CJD50				
CPI2				
CPI				
C2PI				
CHMAX				
CHMIN				
CYMIN				
CTRMI				
CTRMR				
CER				
RASHE				

FLOATING POINT CONSTANTS
EQUATORIAL RADIUS OF EARTH
POLAR RADIUS OF EARTH
ELLIPTICITY OF EARTH
GRAVITATION CONSTANT OF EARTH
ROTATIONAL RATE OF EARTH
GM RATIO OF E.M.S.V.M.J.S TO EARTH
RADIUS OF E.M.S.V.M.J.S TO EARTH
EARTH RADII PER ASTRONOMICAL UNIT
FEET PER EARTH RADII
INITIAL CONDITION INPUT PER EARTH RADII
INITIAL CONDITION TIME PER MINUTE
TERMINAL CONDITION OUTPUT PER EARTH RADII
TERM. COND. OUTPUT TIME PER MINUTE
SPEED OF LIGHT
NAUTICAL MILES PER EARTH RADII
KILOMETERS PER EARTH RADII
SOLAR CONSTANT (WATTS/METER SQ.)
DAYS PER MONTH IN NON-LEAP YEAR
DEGREES PER RADIAN
JULIAN DATE OF JANUARY 1, 1950
PI/2
PI
2*PI
MAXIMUM STEPSIZE FOR TRAJ
MINIMUM STEPSIZE FOR TRAJ
AUXILIARY PARAMETER FOR TRAJ
TERM USED TO CAL. RADIUS OF EARTH
TERM USED TO CAL. RADIUS OF EARTH
ERROR BOUND FOR TRAJ
IMPACT PARAMETER FOR TRAJ

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CRASH	11.0	MIN. TEST ALTITUDE FOR TRAJ
CHFACT	11.0-CELLIP1	11.0-CELLIP1*2
CFAC12	11.0-CELLIP1	DESIRED ACCURACY IN TOF
ACRACY	FIXED POINT CONSTANTS	SYSTEM OUTPUT UNIT
BLK2	SYSTEM INPUT UNIT	UNIT FOR TRAJECTORY OUTPUT
KOUI	UNIT FOR INPUT TAPE	UNIT FOR EPHemeris TAPE
KIN	FOR INTR2	
XTRAJ		MASTER BODY FLAGS FOR EARTH CENTER
KIPEIN		MASTER BODY FLAGS FOR SUN CENTER
KEPHEW		MASTER BODY FLAGS FOR OTHER BODY CENTER
KERNO	10	FLOAT. PT. INPUTS
IBFGEM	10	EPOCH TIME (MIN. FROM 0 HOURS)
IBFGS	10	JULIAN DATE OF 0 HOURS EPOCH DAY
IBFGOB	10	RT. ASCEN. OF GREEN. 0 HR. EPOCH DAY
BLK3		EPOCH YEAR MINUS 1960
TEPOCH		EPOCH MONTH NUMBER
TJDATE		EPOCH DAY NUMBER
TALTAG		EPOCH HOUR
DYEAR		EPOCH MINUTE
DMONTH		EPOCH SECONDS AND FRACTIONS
DDAY		TYPE OF INITIAL CONDITIONS INPUT
DHOUR		DAY SINCE JAN. 1, 1950 TO EPOCH DAY
DMIN		CARTESIAN POS. AND VEL. AT EPOCH
DSEC		POLAR POS. AND VEL. AT EPOCH
DTYPE		INITIAL CONDITIONS INPUT
DBASE		RT. ASC. OF ICONS X AXIS
THOMX	6	CDA/2M LFT.*54/SLUG!
THOMP	6	DRAG VARIATION
TICOND	10	TYPE DRAG VAR. 1=1 PER.10 ³ SECULAR
RANGLE		DRAG ATNOS. MODEL
CDAD2W		AREA OF CRAFT FOR RAD. PRESSURE (MPA)
CK		MAS. OF CRAFT FOR RAD. PRESS. (KILO.)
CKSLCT		INITIAL STEPSIZE FOR INTEGRATION
CDRAGW		INPUT COVARIANCE MATRIX
DAREA		POWERED FLIGHT INPUTS (ASPOF)
DMASS		FLAG TO SET UP TRACING THRU EXECUTION
TSTEP	21	FACTOR TO MUL. TOF FOR NEW ESTIMATE
COVAR	10	
POWFLT		
TRACE		
BPRIM		

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MAX POINT INPUTS	50	POINT OF INPUT ICONDS	50
EQUINOX OF OUTPUT TRAJECTORY PRINT			
INITIAL CENTRAL BODY			
MAXIMUM NO. OF ITERATIONS	50	NO. OF VARIATIONAL EQUATIONS	50
MASTER POINTERS AND FLAGS			
SEARCH FLAG. 0 IF SEARCH IS ON			
OVERRIDE FLAG. 0NE. 0 TO PRINT ON SRCH,			
FLAG SET IN SEGIN FOR 1ST TIME THRU SLECT			
WORKING STORAGE			
CURRENT MU		RADIUS OF CURRENT CENTRAL BODY	
RCCB		TEMPORARY STORAGE	
TEMP	50	RADIUS OF TARGET CENTRAL BODY	
RTC B		OUTPUT VECTOR FROM TDCA	
DCAOUT		VALUE OF JULIAN DATE FOR CURRENT TIME	
TNOWJD	6	INIT. VAR. EQ. MEAN OF 50	
VEPOCH	36	TIME TO INTEGRATE TO IN TRAJ	
TG		TRAJECTORY STORAGE	
BLK7		RADIUS FROM CENTRAL BODY TO PROBE	
TR		TR**2	
TR2		TR**3	
TR3		TR**5	
TR5		TR**7	
TR7		COSINE LAMDA (CURRENT VEH. LAT.)	
COLA		SINE LAMDA (CURRENT VEH. LAT.)	
SILA		VELOCITY OF PROBE REL. TO ROT. EARTH	
TV		MAGNITUDE OF TV	
TVA		COEFF. IN DIURNAL DRAG VARIATION	
TDON		SEMI-MINOR AXIS OF CURRENT CERAL BODY	
CRSHB		PERT. ACEL. DUE TO POTEN. OF CCB.	3
TPOT		PERT. ACEL. DUE TO OTHER BODIES	3
TBPERT		PERT. ACEL. DUE TO RAD. PRESSURE	3
TRPRES		PERT. ACEL. DUE TO THRUST	3
ATHRST		PERT. ACEL. DUE TO ATMOSPHERIC DRAG	3
TDrag		POST. EFFECTS TO CAL. 2ND DER. OF V. EQ.	9
PMAT		VEL. EFFECTS TO CAL. 2ND DER. OF V. EQ.	9
VMAT		FLAG. 0 TO NOT CAL. V EQ.	
FLVE		FLAG. 0NE. 0 WHEN CCB IMPACTED IN TRAJ	
TCRASH		ESTIMATE PERIGEE ALT. FOR TRAJ	
PRAILT			

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V	SKIP	EQ. 0 TO EVAL. V. EQ. PRED. ONLY
V	SCALE	VALUE OF K IN K*EVAL. FOR TDCA
V	TICRT	ICONDS. CARTESIAN, MEAN QF 50
V	PSENUM	CURRENT PHASE NUMBER
V	BSETME	BASE TIME FOR PHASE DELTA T. T S
V	TALEA	FLAG, NON-ZERO FOR RAD. PRES. SCALE.
V	XN	30
V	XNDOT	30
V	TEMPTG	EPHEMERIS POSITIONS
V	TLASTM	EPHEMERIS VELOCITIES
V	STORTG	TEMPORARY VALUE OF TG IN SELECT
V	TLASIP	LAST T IN MASTER DELTA T. T LIST
V	TSEC	STORAGE OF TEMP TG
V	COLA	LAST T IN PHASE DELTA T. T LIST
V	SILA	FOR INTPL. SEC. FROM 1950 (PSEUDO D.P.)
V	COPH	COS(CURRENT VEH. LONGITUDE)
V	SIPH	SIN(CURRENT VEH. LONGITUDE)
V	CSALF	COS(CURRENT VEH. LATITUDE)
V	SNALF	SIN(CURRENT VEH. LATITUDE)
V	TRJPR	COS(CURRENT VEH. RIGHT ASCENSION)
V	BLK8	SIN(CURRENT VEH. RIGHT ASCENSION)
V	TLIST	FLAG, NON-ZERO FOR PRINT. IN TRAJ
N	BLK9	INTEGRATION INPUT
V	TRAJX	INTEGRATION INPUT LIST?
N	BLK10	INTEGRATION OUTPUT
V	CEJ	INTEGRATION OUTPUT LIST!
V	CEC	EARTH-MOON HARMONICS
V	CES	EARTH ZONAL HARMONICS J1,J2,...,J12
V	CNJ	EARTH SECTORAL-TESSELLAR HAR. S11...S66
V	CHC	EARTH SECTORAL-TESSELLAR HAR. S11...S66
V	CMS	MOON ZONAL HARMONICS J1,J2,...,J12
V	FJ	MOON SECTORAL-TESSELLAR HAR. S11...S66
V	C	CURRENT ZONALS BEING USED IN GPERT
V	S	CURRENT SECT.-TESS. BEING USED IN GPERT
V	BLK11	CURRENT SECT.-TESS. BEING USED IN GPERT
V	TIMES	TIMES FOR ALL PROCESSED TIMES
N	BLK12	ALL PROCESSED TIMES
V	ICCB	FIXED WORKING STORAGE
V	IOC8	CURRENT CENTRAL BODY
V	INC8	PREVIOUS CENTRAL BODY
V	NEOP	NEW CENTRAL BODY
V		STARTING POST. OF PHASE SHIFT T IN TIMES

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V	NHC	NOT 1	NOT 1. OF TUR IN TIMES
V	NUJ	NOT 1	STARTING POST. OF MID-COURSE T S IN TIMES
V	NSPT	NSPT	START. POSI. OF JULIAN DATE 1 S IN TIMES
V	NPDT	NPDT	START. POST. OF MASTER D T S IN TIMES
V	ITCB	ITCB	START. POST. OF SPECIAL PRT. T S IN TIMES
V	NPHTSE	NPHTSE	START. POST. OF PHASE D T S IN TIMES
V	NXTPHS	NXTPHS	VALUE OF TARGET CENTRAL BODY FOR TDCA
V	JPHSNO	JPHSNO	START. PSN. OF CURRENT PHASE IN LIST
V	JTYPE	JTYPE	START. PSN. OF NEXT PHASE
V	JFINCD	JFINCD	PSN. OF PHASE NO. IN CURRENT PHASE
V	JTCB	JTCB	PSN. OF PHASE TYPE IN CURRENT PHASE
V	JCCB	JCCB	PSN. OF FINAL CONDITION IN CURRENT PHASE
V	JRPPRS	JRPPRS	PSN. OF TARGET CENT. BODY IN CURR. PHASE
V	JDELT	JDELT	PSN. OF CURRENT CENT. BODY IN CURR. PHASE
V	BLK13	BLK13	PSN. OF RAD. PRES. FLAG IN CURR. PHASE
M	N1	N1	PSN. OF DELTA T FLAG IN CURRENT PHASE
M	N2	N2	FIXED TRAJECTORY STORAGE
M	N3	N3	DÉGRÉE OF HIGHEST ZONAL HARMONICS
V	NOPT	NOPT	DÉGRÉE OF HIGHEST SECTORAL HARMONICS
V	ITMNUIS	ITMNUIS	DÉGRÉE OF HIGHEST TESSERAL HARMONICS
V	IPHSE	IPHSE	OPTION FLAG FOR ROTAT
V	IQUIT	IQUIT	FLAG, •NE. 0 FOR FIRST PRE-EPOCH TIME
V	IPRTFG	IPRTFG	FLAG, •NE. 0 1ST TIME THRU PHASE
V	!TPTM	!TPTM	FLAG, •NE. 0 WHEN ALL TIMES PROCESSED
V	IBFLGS	IBFLGS	FLAG, •NE. 0 TO PRINT AFTER INTEG.
V	IQUAD	IQUAD	TYPE OF TIME RETURNED FROM SELECT
V	IBPRIM	IBPRIM	FLAGS FOR BODIES EFFECTS THIS PHASE
V	IMAX	IMAX	FLAG FOR DESIRED QUADRANT IN TDCA
V	ISLECT	ISLECT	FLAG FOR 1ST TIME LESS THAN ACCURACY
V	IRUNOT	IRUNOT	MAXIMUM LOOPS THRU TDCA
V	IWKFLG	IWKFLG	FLAG FOR SELECT SET IN PHASE
V	INTRX	INTRX	FLAG SET IN PHASE FOR SELECT
V	NVEL	NVEL	FLAG RETURNED FROM INTR2 FOR ERRORS
V	NRRR	NRRR	FLAG FOR INTPL. INTR3•••JP.A.V=0.P ONLY
V	BLK14	BLK14	FLAG. NON-ZERO FOR FXD. SIP. R-K IN TRAJ
V	PHASES	PHASES	PHASE LIST STORAGE
V	BLK15	BLK15	CONTAINS ALL PHASES TO BE PROCESSED
V	ICOND	ICOND	INPUT STORAGE BUFFER
V	ITYPE	ITYPE	INITIAL CONDITIONS
V	1	1	COORD. TYPE OF ICONGS
V	200	10	

SITIME	25
MCTIME	25
JDTIME	25
STYPE	10
TARGET	1
TRMCON	10
DELTMR	1C
DELSRH	10
PHASE	1
PYTYPE	1
FINCON	5
FINBOD	1
CURBOD	1
RPRESS	1
PDELTT	50
ENDJOB	1
ENDCOM	

SPECIAL INPUT TIMES

MIDCOURSE TIMES

JULIAN DATE TIMES

SEARCH VARIABLES

TARGET BODY FOR SEARCH

TERM CONDITIONS FOR SEARCH

BOUNDS FOR TERMINAL CONDITIONS

BOUNDS FOR SEARCH VARIABLES

PHASE I. D. NUMBER (.LT. 99999.0)

PHASE TYPE

PHASE FINAL CONDITIONS

PHASE TARGET CENTRAL BODY

CURRENT CENTRAL BODY

FLAG FOR RADIATION PRESSURE

PHASE DELTA T, + LIST

END JOB FLAG

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IV. Sample Output:

On the following pages is a listing of the outputs of the BLKGEN program.

PAGE

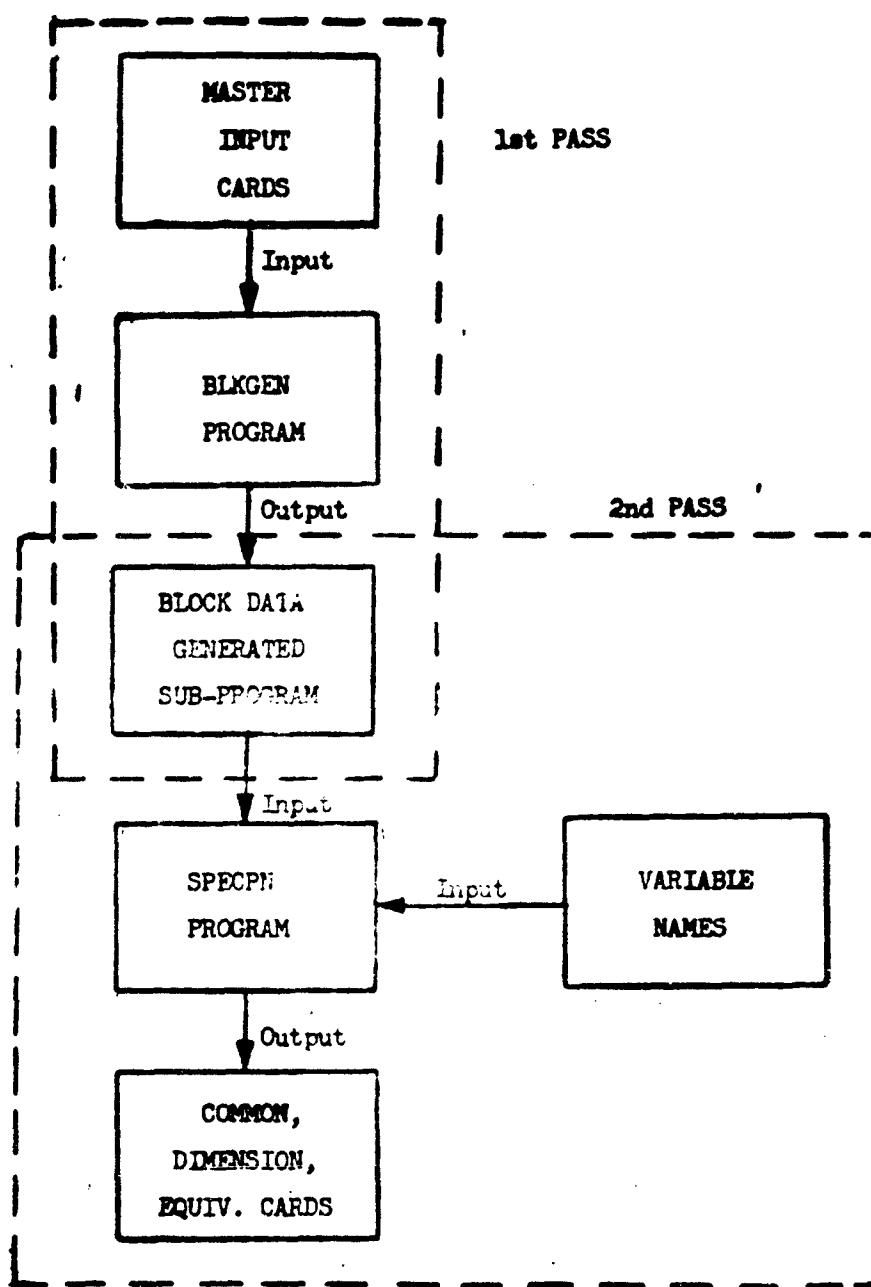
MASTER COMMON LISTINGS

CURRENT COMMAND IS --

CURRENT	BLK1	BLK1 (125), BLK2 (50), BLK3 (150), BLK4 (50)
1, BLKS (5,), BLK5 (200), BLK7 (200), BLK8 (50), BLK9 (75)		
2, BLK10 (200), BLK11 (200), BLK12 (50), BLK13 (50), BLK14 (200)		
3, BLK15 (30,)		

CURRENT BLOCK IS BLK1 (C1 FLOATING POINT CONSTANTS

VARIABLE	DIMENSION	POSITION	TYPE	DESCRIPTION
LAT		1		EQUATORIAL RADIUS OF EARTH
COL		2		SOLAR RADIUS OF EARTH
CEELIP		3		ELLIPRICITY OF EARTH
CNU		4		GRAVITATION CONSTANT OF EARTH
CWE		5		ROTATIONAL RATE OF EARTH
C3MK		15		GA RATE OF EARTH, M.J.S TO EARTH
KUB		16		RADIUS OF EARTH, M.J.S TO EARTH
GERAU		17		EARTH RADIUS PER ASTROMONICAL UNIT
GFTER		27		FEET PER EARTH RADIUS
LINIR		28		INITIAL LUNITUDE PER EARTH RADIUS
LIN2R		29		INITIAL LONGITUDE TIME PER MINUTE
OUT1		30		TERMINAL CONDITION OUTPUT PER EARTH RADIUS
OUT2		31		TERM. LUN. OUTPUT TIME PER MINUTE
CLIGHT		32		SPEED OF LIGHT
CNMEK		33		NAUTICAL MILES PER EARTH RADII
UKMEK		34		KILOMETERS PER EARTH RADII
CSULC		35		SOLAR CONSTANT (WATTS/METER SQ)
COAHR		36		DAYS PER MONTH IN NON-LEAP YEAR
CUEG		48		DEGREES PER RADIAN

V. Organization and Usage of BLKGEN and SPECPN Flow Chart:

VI. References:

1. Specification Statement Punch Program (SPECUPN) User's Guide,
A. J. DeSalvio and J. Rau, September 15, 1966, CIRC Report
Number 3127.21-01.

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APPENDIX B

SPECIFICATION STATEMENT PUNCH PROGRAM
(SPECPN)
User's Guide

SPECIN USERS GUIDE

The SPECIN (SPECification statement PInch) program was written to aid the FORTRAN programmer in his preparation of COMMON, DIMENSION, and EQUIVALENCE statements. It was designed primarily for programs which use the philosophy of master COMMON blocks and EQUIVALENCE variables e.g.

COMMON/COMMON/BLK1 (100), BLK2 (5000)
EQUIVALENCE (BLK1 (26), VAL1), (BLK2 (63), VAR2)

In this example only the variables VAR1, VAL2 are needed from the 100 cell block BLK1 and the 5000 cell block BLK2. Using EQUIVALENCE statements to identify only those variables actually used in a subroutine significantly reduces the card volume for a subroutine and the size of the symbol table necessary at compile time. This technique is opposed to the standard one of stringing out the actual COMMON variable names in the COMMON statement e.g.

COMMON/COMMON/ A, B, C(3), D, E, F(16), G(2), VAR1

To use SPECIN one must supply input in two forms. First, a BLOCK DATA subprogram must be prepared containing all of the master COMMON blocks including a complete list of each variable in COMMON, EQUIVALENCE numbers, and EQUIV1 and EQUIV2. This BLOCK DATA subprogram is then compiled and submitted as part of the SPECIN run. When the COMMON map changes, the BLOCK DATA subprogram must never be altered again. The second input to SPECIN is data cards specifying by subroutine those variables defined in COMMON. These variables may be in blank COMMON or any of the labeled COMMON blocks defined in the BLOCK DATA subprogram. The output from SPECIN is the COMMON, DIMENSION, and EQUIVALENCE statements necessary for each subroutine.

The advantages of using SPECPN are several:

- a) The format of the punched cards is uniform. This makes the program listing neat and easy to read.
- b) Once the BLOCK DATA subprogram has been verified for accuracy, the worry of mis-equivalencing a COMMON variable is ended.
- c) If significant changes are made in the COMMON map of a large scale program such that the equivalence numbers are disturbed, only the BLOCK DATA subprogram need be re-keypunched. The data cards used with the old COMMON may be re-submitted with SPECPN to recover all the COMMON, DIMENSION, and EQUIVALENCE statements for the new COMMON map.

BLOCK DATA Input to SPECPN

The BLOCK DATA subprogram must contain the following four labeled COMMON blocks:

COMMON/ISIZE/ISIZE
COMMON/BLK /BLK(I)
COMMON/FMT /FMT(J)
COMMON/XMCOM/XMCOM(ISIZE)

COMMON/ISIZE/ISIZE

ISIZE is an integer which defines the size of XMCOM. ISIZE will be $3 * N$, where N is the total number of COMMON variables defined in the user's program.

COMMON/BLK /BLK(I)

BLK is a dimensioned array which contains the name of each master COMMON block in BCD. The order of the names within BLK is arbitrary.

If the following COMMON statements appeared in the user's program:

COMMON/ /BLK1(100), BLK2(5000)
COMMON/COMA/ABLK1(50), ABLK2(25), ABLK3(500)

the master COMMON block names BLK1, BLK2, ABLK1, ABLK2, ABLK3 must appear in BLK , left adjusted, in BCD. For example:

```
COMMON /BLK/BLK(5)
DATA (BLK(I),I=1,5) /6HABLK2 ,6HBLK1 ,6HABLK3 ,
16HBLK2 ,6HABLK1 /
```

could be used to define /BLK/ for this program. The labeled COMMON block names, i.e. COMA, are not specified within BLK.

COMMON / FMT / FMT(J)

FMT is a dimensioned array defining the COMMON statements that appear in the user's program. All the information in FMT is in BCD. Since the format of a COMMON statement is so arbitrary (is it blank COMMON, or labeled COMMON; how many variables etc.) and the elements of the card so variable, the user is required to store in FMT the actual FORMAT statement that would cause the COMMON statements defined in the users program to be punched. For example; the COMMON card

```
COMMON /COMNAM / BLK1(100), BLK2(5000)
```

could be punched with the following statements

```
* WRITE (12, 901)
901  FORMAT(6X,34H(COMN/COMNAM/BLK1(100),BLK2(5000))
```

What goes into the array FMT is exactly what the compiler would generate in core at location #12: the BCD equivalent of what follows the word FORMAT, each character from "(" to the terminating ")" inclusive. In this example:

```
COMMON /FMT/FMT(7)
DATA (FMT(I),I=1,7)           /6H(6X,34,6HHCOMMO,
16HN/COMN,6HAN/BLK,+H(100),6H,dLK2(+,6H5000))/
```

would be used to load the array FMT. Each COMMON statement is specified in the above manner, in any order within FMT. If the final BCD word for a given format is not a full 6 characters, fill out the word with blanks following the ")" since each "FORMAT" must begin in a new word within FMT.

```
COMMON/XMCOM/XMCOM(131E)
```

XMCOM is an N x 3 array stored singly subscripted by rows. (N is the total number of COMMON variables in the user's program). In column 1 of XMCOM is placed the name of each COMMON variable, left adjusted, in BCD. Column 2 of XMCOM contains integer code words of the form I * 10000 + J. I is the entry in BLK which identifies the master COMMON block name appropriate for this variable. J is the equivalence number of the given variable within the master COMMON block. Column 3 of XMCOM contains integer code words of the form

$K = 10000 + L$. L is the dimension of the given variable. (Non-dimensioned variables are indicated with $L = 1$) K is the entry in FMT of the first word of the "FORMAT" statement which identifies the COMMON statement containing the given master COMMON block name. A sample XMCOM will now be constructed from the following COMMON map:

```
COMMON//BLK1(24)
COMMON//COMA//ABLK1(50)
EQUIVALENCE          (BLK1 ( 1),CAE ),(BLK1 ( 2),TEMP )
1,(BLK1 ( 12),CBE ),(BLK1 ( 13),CDAYMN)
DIMENSION TEMP(10).CDAYMN(12)
EQUIVALENCE          (ABL1 ( 1),NPR ),(ABL1 ( 2),NDPR )
1,(ABL1 ( 3),MATRIX)
DIMENSION MATRIX(48)
```

To compute ISIZE, we simply count the number of COMMON variables:
CAE, TEMP, CBE, CDAYMN, NPR, NDPR, MATRIX... 7

ISIZE: $3 * 7 = 21$

COMMON//ISIZE//ISIZE

DATA ISIZE /21/

The entries in BLK will be the master COMMON block names:

BLK1, ABLK1

COMMON / BLK / BLK(2)

DATA (BLK(I), I = 2) / 6HBLK1 , 6HABL1 /

The FMT array would be constructed from the following FORMAT statements:

```
FORMAT(6X,,1HCOMMON//BLK1(24))
FORMAT(6X,,1HCOMMON//COMA//ABL1(50))
COMMON//FMT//FMT(1)
DATA (FMT(I),I=1,4)/
16H(6X,16,6HCOMMON,6HN//BLK,6H(24))/
DATA (FMT(I),I=5,9)/
16H(6X,21+6H COMMON,6HN//COMA,6H//ABL1,6H(50)) /
```

XCOMMON would look as follows:

```
COMMON/XCOMMON/XCOMMON(21)
EQUIVALENCE (XCOMMON,IXCOMMON)
DIMENSION IXCOMMON(21)
DATA (XCOMMON()),I= 1,21) /
16HCAE  • 10001, 100C1,
26HTEMP • 10002, 10010,
36HCBE  • 10012, 10001,
46HCDAYMN, 10013, 10012,
56HNPR  • 20001, 50001,
66HNDPR • 20002, 50002,
76HMATRIX, 200C3, 50048/
    ↑   ↑   ↑   ↑   ↑
    ①   ②   ③   ④   ⑤
```

- ① VARIABLE NAME
- ② BLK ENTRY
- ③ EQUIVALENCE NO.
- ④ FMT ENTRY
- ⑤ DIMENSION

For compatibility with the G.E. computer, XCOMMON should be set

up as follows:

```
DATA (XCOMMON()),I= 1,21,3) /6HCAE ,6HTEMP ,6HCBE ,6HCDAYMN
1,6HNPR ,6HNDPR ,6HMATRIX/
DATA ((IXCOMMON(),IXCOMMON(I-1)),I= 2,20,3) /
1 10001, 10001,
2 10002, 10010,
3 10012, 10001,
4 10013, 10012,
5 20001, 50001,
6 20002, 50002,
7 200C3, 50048/
```

DATA CARD Input to SPECPN

The BLOCK DATA subroutine described above contains the complete definition of each COMMON block in the users program. The remaining inputs to SPECPN are a series of fixed format data cards describing the individual COMMON variables defined in each subroutine in the users program. The data cards have the following format:

For each subroutine:

Card 1

Contains the subroutine name in columns 1 - 6.
 This card serves to identify the routine which
 the punched and printed output from SPECPN belongs.
 The name punched in cc 1 - 6 may be any combination
 of alphanumeric characters except ENDSUB or ENDJOB.

Card 2-(N - 1) Contains the COMMON variable names, punched up to 12 per card, in columns 1 - 6, 7 - 12, 13 - 18, etc. The variable names must be left adjusted in each field.

Card N Contains ENDSUB in columns 1 - 6. The entry ENDSUB indicates to SPECPN that all the variables for this subroutine have been entered. Columns 7 - 72 of this card are ignored.

The above series of cards are repeated for as many subroutines as desired. Following the final ENDSUB card must be placed a card with ENDJOB to indicate the end of the input data. See figure 1 and appendix for an example of the deck set-up and data card samples.

Output from SPECPN

SPECPN delivers both printed and punched output. The first block of printed output will be the XMCOM array after having been algebraically sorted about column 1. For each subroutine name card in the data deck, a message is printed stating:

THE FOLLOWING CARDS ARE FOR SUBROUTINE XXXXX

This card is also punched. Next will be the EQUIVALENCE, DIMENSION, and COMMON cards, in that order. Continuation cards are indicated with an E in column 6 for EQUIVALENCE and a D in column 6 for DIMENSION. A card image is printed and punched. In the event that a variable is requested in the data deck that does not appear in XMCOM, the following error message is printed only:

ERROR - XXXXX NOT IN XMCOM.

Operating Notes

One point that should be noted is the flexibility which results from the use of the FMT array in the BLOCK DATA subprogram. As was explained above, SPECPN simply executes a WRITE (12, FMT(I)) in order to punch the Ith COMMON statement. In theory then, the user can direct

SPECPS to punch any card, in any arbitrary format for any arbitrary subroutine. For instance the user could place in FMT the necessary control characters to cause comments cards to be punched before or after COMMON statements, which define the variables in that COMMON block. Another use of FMT might be to include DIMENSION card images for those variables which are multi-dimensioned in the user's program since there is no provision in XMCOM for indicating such.

This could be accomplished as follows:

- a) Place in FMT(J) the FORMAT statement that would cause the desired DIMENSION statement to be punched.
- b) In the appropriate column 3 entry in XMCOM, set the dimension of the multi-dimensioned variable to 1.
- c) Instead of pointing to the COMMON card image in FMT for this variable, point to the DIMENSION card image, J.
- d) Be sure that another variable in the subroutine list does point to the proper COMMON card image.

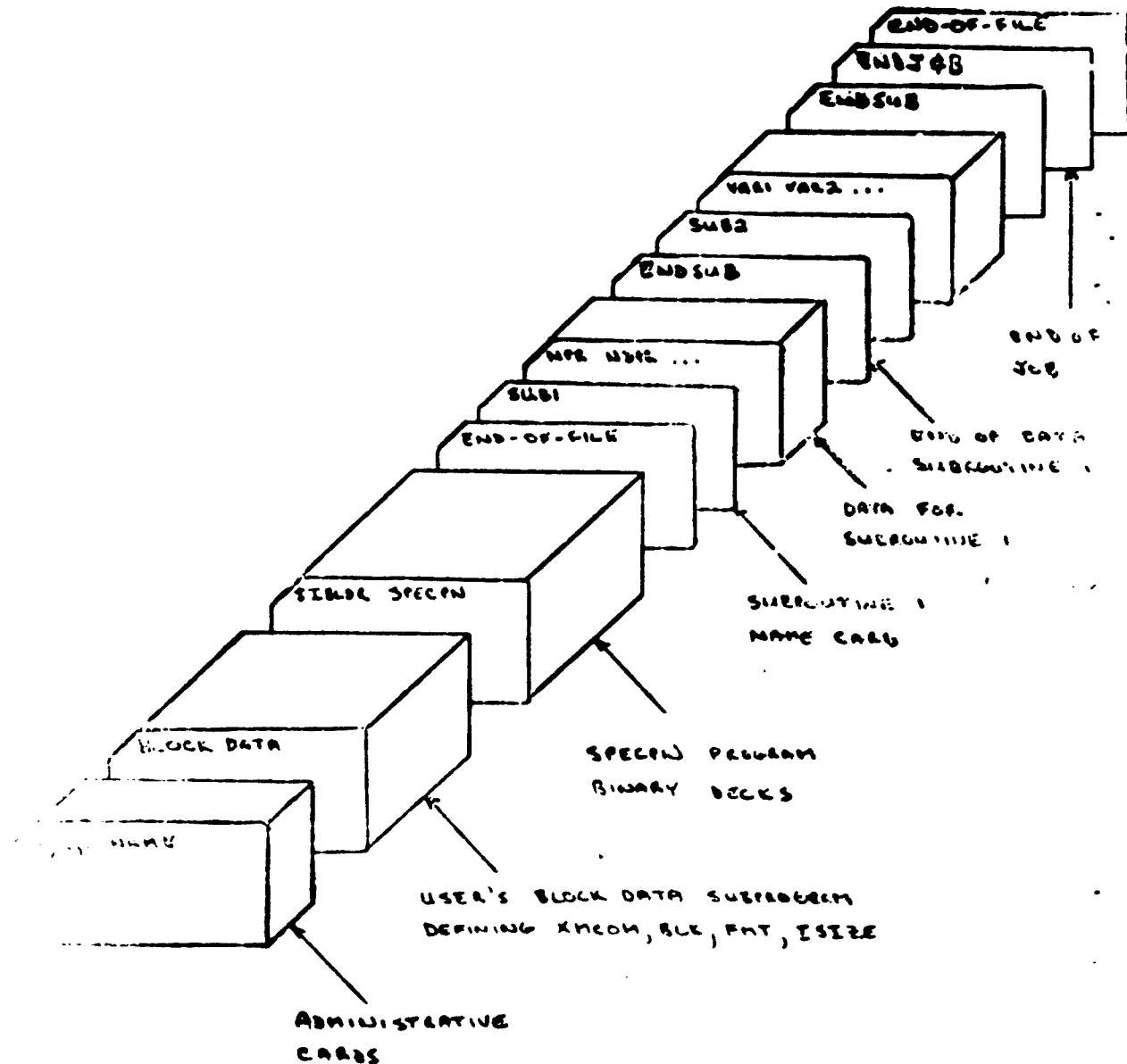
Setting the dimension to 1 will suppress the punching of a standard DIMENSION card.

To aid the spot checking of EQUIVALENCE variables it is a good practice to list the variables in ascending EQUIVALENCE order on the data cards for each subroutine. If it is desired to obtain EQUIVALENCE cards by master COMMON block, that is, have SPECIN start with a new EQUIVALENCE card for each new master COMMON block, it is only necessary to book up the variables by COMMON block within a subroutine and submit each set under the name of the same subroutine. The fact that the subroutine name is repeated within the data deck is immaterial since it is used only for identification of the output.

The following restrictions should be observed when running SPECIN:

- a) The total size of XMCOM + BLK + FMT must not exceed 22,753₁₀ cells. This is based on the SPECIN version currently in use on the 7094.

- b) Do not use a subroutine card with ENDSUB or ENDJOB in columns 1 - 6. These variables may appear on a data card providing they are not placed in columns 1 - 6.
- c) No variable name may be repeated in XMCOM.
- d) When operating on the 7094, a PUNCH card should be included in the administrative cards if more than 500 punched cards are expected or if it is desired to have the punched cards listed and/or interpreted.



SPECN DECE SETUP - FIGURE 1.

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The following page is an example of the data card
input to SPECPN

FIRST	CAC	ACT	DIP	KLT	FADK	ZOT	NPR	BUM	NON	ONK	MP	TNS
	KNT			THUMP	DRV	XUFK	INT	UHP		ORs		KKK
	MOUNT	DNR	DOG	MLT	BLKK						CK	
	ONTL	GGGG	DGN		K2Y	FLY	FADK	ZXA	AAD	LAVA	LO	
	NNN	AROUSEUNV	UVW		SPOT						CDM	
	KNOLW	ANT										
ENDSUB												
SECOND	CDAYNNASB	DNK	SPOT	KLT	INT	FADK	ZOT	FLY	NON	NP	BLKK	
	CBE	DALP	CAT	UMP	XOLT	KZY	DRV	NDPR	FDP	AHLT	JOB	
	KJJ	DNR	CK	TORB	DIP	AAD	RTS	OPT				
	DOT	ACT	KKK	BBNFK	ORB	CNTP	CHOM	AGGG	LAVA	ZXA	KNT	
	XUFK	ER	ZMPT	MOUSE	CELLIPABAL	<CO	CDEM	RPL	EUM	DUG	DAB	
	OINK	XUFK	DGN	BOND	TNS	DDP	RTS	CHOM	KLRS	NNN	2NK	
	XOLT	KQO	ONK	BLKK	FLY	RTS	SYCL	LVAE	ZAPT	ATHU	MAP	
	CK	MP	KK	BHFK	ACT	RTS	RTS	ECND	PPJ	SPR	UZ	
ENDSUB								CUM	NPF	AER	DAYNTAS	
THIRD	CELLIPCOAYMNKKK		FLY									
ENDSUB												
FOURTH	ACT	JOB										
ENDSUB												
FIFTH	CAT											
ENDSUB												
SIXTH	XUFK											
ENDSUB												
SIX	KQQ	FLY	DOT	DIP	ABAB	DNK	ZOT	KKK	DRV			
ENDSUB												
ENDJOB												

CELLIP

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**The following pages illustrate the punch card
output from SPECPN**

E•(IM2A 1 4)•DIP 1•(BLK6 1 19)•KL1 1•BLK3 1 43)•AC1
 E•(ITJA 1 6)•ZOT 1•(BLK2 1 11)•PR 1•BLK6 1 11)•FACK
 E•(COLB 1 26)•NON 1•(COLB 1 4)•CNK 1•TRAJ 1 6)•MP
 E•(TRAJ 1 1)•INS 1•(BLK3 1 6)•KN1 1•BLK3 1 24)•THUMP
 E•(BLK6 1 11)•KKK 1•(BLK6 1 16)•JNR 1•BLK4 1 11)•QOG
 E•(IM2A 1 2)•DRV 1•(BLK5 1 5)•XUFK 1•(BLK5 1 2)•INT
 E•(BLKS 1 1)•UWP 1•(BLK4 1 6)•ORG 1•(BLK6 1 17)•CK
 E•(COLB 1 24)•ONIL 1•(TRAJ 1 3)•GGG 1•(DOPLR 1 1)•DGN
 E•(DOPLR 1 21)•MLT 1•(BLK7 1 11)•BLKK 1•(COLB 1 25)•NNN
 E•(COLB 1 8)•UVW 1•(COLB 1 6)•UVW 1•(BLK3 1 2)•KZY
 E•(DOPLR 1 11)•FLY 1•(BLK4 1 11)•FADK 1•(BLK3 1 5)•ZXAX
 E•(BLK3 1 26)•SPOT 1•(BLK2 1 3)•AAAD 1•(DCPLR 1 8)•LAVA
 E•(BLK2 1 1)•CDM 1
 DIMENSION DIP 1 6)•ZOT 1 4)•KKK 1 6)•DRV 1 2)
 D•XUFK 1 6)•UVW 1 8)•FLY 1 2)•AAAD 1 3)
 COMMON /BLK1(110),BLK2(6),TJA(2)
 COMMON /BLAH/MZA(26),BLK3(9),BLK4(1),BLKS(21),BLK6(19),COLB(26)
 1,BLK7(1),
 COMMON /SHIPPO/TRAJ(6),DOPLR(12)

C THE FOLLOWING CARDS ARE FOR SUBROUTINE SECOND EQUIVALENCE
 E•(IM2A 1 10)•DNK 1•(BLK3 1 10)•CDAYMN1•(BLK2 1 6)•ABAB
 E•(BLKS 1 21)•LNT 1•(BLK4 1 26)•SPT 1•(BLK6 1 19)•KLT
 E•(DOPLR 1 11)•FLY 1•(COLB 1 11)•FADK 1•(TJA 1 6)•ZOT
 E•(BLK7 1 1)•BLKK 1•(BLK1 1 26)•NQN 1•(TJA 1 6)•MP
 E•(BLK4 1 2)•CAT 1•(BLK5 1 11)•U? 1•(BLK6 1 2)•DALP
 E•(BLK3 1 21)•KZY 1•(M2A 1 21)•DRV 1•(BLK2 1 2)•NDPR
 E•(COLB 1 21)•CPT 1•(TRAJ 1 21)•FCP 1•(DOPLR 1 3)•JOD
 E•(DOPLR 1 4)•KJJ 1•(BLK6 1 18)•JNR 1•(BLK4 1 9)•ORB
 E•(IM2A 1 4)•DIP 1•(BLK2 1 3)•AAAD 1•(COLB 1 7)•RTS
 E•(DOPLR 1 8)•LAVA 1•(BLK3 1 5)•2XA 1•(BLK3 1 6)•KNT
 E•(BLK3 1 10)•DFT 1•(BLK3 1 23)•ACT 1•(BLK6 1 3)•ERFK
 E•(BLK4 1 9)•ORB 1•(TJA 1 3)•CN?P 1•(BLK1 1 4)•CGNOM
 E•(COLB 1 8)•UVW 1•(M2A 1 1)•NPP 1•(BLK6 1 1)•BUTI
 E•(BLK4 1 11)•DOG 1•(BLK2 1 3)•DAB 1•(BLK6 1 5)•XUFK
 E•(BLK6 1 4)•ZMPT 1•(BLK4 1 8)•HOUSE 1•(BLK1 1 3)•CELLIP
 E•(BLK2 1 6)•ABAB 1•(COLB 1 17)•KCO 1•(TJA 1 1)•CAEM
 E•(BLK3 1 11)•CDE 1•(BLB 1 22)•KLSS 1•(COLB 1 25)•NIN
 E•(COLB 1 4)•GMK 1•(S?G 1 3)•XUFK 1•(DCPLR 1 1)•DGN

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E•(DOPLR { 9)•BUND 1•(TRAJ { 1)•TNS 1•(CULE { 7)•KIS 1
      DIMENSION ASAE { 3)•DNK { 3)•ZOT { 4)•FLY { 2)
      D•CAT { 6)•DRY { 2)•KJJ { 2)•DUE { 6)•AAU { 3)
      D•DOT { 3)•CGNOM { 6)•UWV { 8)•XUFK { 6)•ABAB { 3)
      D•KGG { 2)•XUFK { 6)•
      EQUIVALENCE (COL2 { 23)•SIGL 1•(BLK3 { 24)•THUMP 1
      E•(BLK6 { 2)•XULT 1•(COL3 { 17)•KOC 1•(COLB { 4)•UNK 1
      E•(BLK7 { 1)•BLKK 1•(DOPLR { 1)•FLY { 1)•DGN 1
      E•(DOPLR { 2)•HLT { 1)•BLK2 { 1)•DOT { 1)•SOND 1
      E•(BLK2 { 1)•NPR { 1)•MZA { 4)•DIP { 1)•BLK6 { 17)•CK 1
      E•(BLK3 { 6)•MP { 1)•BLK6 { 1)•KKK { 1)•BNFK 1
      E•(BLK3 { 23)•ACT { 1)•BLK3 { 25)•DUMP { 1)•BLK3 { 13)•LOT 1
      E•(BLK3 { 1)•CDM { 1)•MZA { 1)•NPP { 1)•BLK2 { 6)•ABAB 1
      E•(BLK1 { 10)•CDAYMN1•(TRAJ { 1)•TNS { 1)•
      DIMENSION KQQ { 2)•FLY { 2)•DOT { 3)•DIP { 3)•
      D•KKK { 6)•LOT { 10)•ABAB { 3)
      COMMON //BLK1(10)•BLK2(8)•TJA(2)
      COMMON/BLAH/MZA(26),BLK3(9),BLK4(11),BLK5(21),BLK6(19),COLB(26)
      COMMON/HIPPO/TRAJ(6)•DOPLR(12)
      C THE FOLLOWING CARDS ARE FOR SUBROUTINE THIRD
      EQUIVALENCE (BLK1 { 3)•CELLP1•(BLK1 { 10)•CDAYMN1
      E•(BLK6 { 11)•KKK 1•(DOPLR { 11)•FLY { 10)•LAND 1
      DIMENSION KKK { 6)•FLY { 2)
      COMMON //BLK1(10)•BLK2(8)•TJA(2)
      COMMON/BLAH/MZA(26),BLK3(9),BLK4(11),BLK5(21),BLK6(19),COLB(26)
      1•BLK7(1)
      COMMON/HIPPO/TRAJ(6)•DOPLR(12)
      C THE FOLLOWING CARDS ARE FOR SUBROUTINE FOURTH
      EQUIVALENCE (BLK3 { 23)•ACT { 1)•DOPLR { 3)•JOS 1
      COMMON/BLK3(9)•BLK4(11)•BLK5(21)•BLK6(19)•COLB(26)
      1•BLK7(1)
      COMMON/HIPPO/TRAJ(6)•DOPLR(12)
      C THE FOLLOWING CARDS ARE FOR SUBROUTINE FIFTH
      EQUIVALENCE (BLK4 { 2)•CAT { 6)•
      DIMENSION CAT { 6)•
      COMMON/BLAH/MZA(26),BLK3(9),BLK4(11),BLK5(21),BLK6(19),COLB(26)
      1•BLK7(1)
      C THE FOLLOWING CARDS ARE FOR SUBROUTINE SIXTH
      EQUIVALENCE TEEG { 5)•XUFK { 6)•TOLKI { 3)•CELLP1
      DIMENSION XUFK { 6)
    
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1,BLK1
1,COMMON //BLK1(10),BLK2(11),BLK3(12)
C THE FOLLOWING CARDS ARE FOR SUBROUTINE SIX
EQUIVALENCE (COLB 1 17)KOO 1,DOPLR 1 11,FLY 1
E,(BLK3 1 10)DOT 1,(MZA 1 6)DIP 1,ABAB 1
E,(MZA 1 10)DNK 1,(TJA 1 6)BLK2 1 6,ABAB 1
E,(MZA 1 2)DRV 1
DIMENSION KOO 1 2,FLY 1 2,DOT 1 2,DDIP 1
D,ABAB 1 5,DNK 1 3,20T 1 4,KKK 1 6,DRV 1
COMMON /BLAH/MZA(126),BLK3(19),BLK4(11),BLK5(21),BLK6(18),COLB(126)
1,BLK7(11)
COMMON /HIPPO/TRAJ(6),DOPLR(12)
COMMON //BLK1(10),BLK2(8),TJA(2)

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