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**A NEW THERMODYNAMIC PARAMETER TO
PREDICT FORMATION OF SOLID SOLUTION OR
INTERMETALLIC PHASES IN HIGH ENTROPY
ALLOYS (POSTPRINT)**

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A new thermodynamic parameter to predict formation of solid solution or intermetallic phases in high entropy alloys



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A simple thermodynamic criterion is proposed to predict the presence or absence of equilibrium intermetallic phases in a high entropy alloy at a given temperature T . The criterion was verified using 45 currently available HEAs, for which equilibrium phases and respective annealing temperature are reported. The present model shows good correlation with experiment and gives an improved ability to predict formation of solid solution and intermetallic phases compared to earlier models.

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1. Introduction

Since the first reports of high entropy alloys (HEAs), a number of attempts have been made to predict phase formation in these alloys, in particular to predict compositions, which would favor formation of solid solution phases. The formation of disordered solid solution phases in HEAs was initially suggested to be governed by high entropy of mixing of alloying elements in these phases [1,2]:

$$\Delta S_{\text{mix}} = -R \sum c_i \ln c_i \quad (1)$$

Here R is the gas constant and c_i is the atomic fraction of element i . Indeed, the high value of ΔS_{mix} may reduce the Gibbs free energy, ΔG_{mix} , of the solid solution (SS) below that of competing intermetallic (IM) phases. However, in spite of having high ΔS_{mix} values, many HEAs are multi-phase and can also contain IM phases. For example, Otto et al. [3] studied the effects of entropy and enthalpy on phase formation in 5-component equimolar alloys. They started from a single-phase solid solution CoCrFeMnNi HEA [4] and made 5 other alloys by substituting Co, Cr, Fe or Ni, one element at a time, with, respectively, Ti, Mo or V, V and Cu. Although ΔS_{mix} was the same, the modified alloys contained multiple SS and/or IM phases. Thermodynamic analysis showed that formation of multiple phases was consistent with minimization of the total Gibbs free energy,

which includes both entropy and enthalpy contributions. It was concluded that ΔS_{mix} stabilizes single-phase SS microstructures in rare cases. In many cases, the entropy effect is insufficient to counteract the driving forces that favor formation of secondary phases based on strongly interacting component pairs.

Several additional semi-empirical criteria for predicting solid solution phase formation in HEAs were introduced recently [5–9]. Similar to Hume-Rothery rules for binary substitutional solid solutions [10], these criteria focus on the differences of the atomic sizes (δr), electronegativities ($\delta \chi$), and valence electron concentrations (VEC) of the alloying elements. Additionally, the enthalpy of mixing (ΔH_{mix}) and a parameter Ω were also used to develop criteria for the stability of SS, IM and/or amorphous phases in as-cast HEAs [11].

Zhang et al. [5] were the first who identified the importance of δr and ΔH_{mix} in the formation of SS, IM, SS + IM, or even amorphous phases, in as-cast HEAs. These parameters are calculated using the following equations:

$$\delta r = \sqrt{\sum c_i (1 - r_i/\bar{r})^2} \cdot 100\% \quad (2)$$

$$\Delta H_{\text{mix}} = \sum_{i < j} 4H_{ij}c_i c_j \quad (3)$$

Here r_i and c_i are atomic radius and atomic fraction of element i ; $\bar{r} = \sum c_i r_i$ is the average atomic radius; and H_{ij} is an enthalpy of mixing of elements i and j , which values are calculated by using

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Miedema's model as given in Ref. [12].

Statistical analysis of existing experimental data for HEAs produced by casting revealed that SS phases can be present if $\delta r < 6.2\%$ and $-12 \text{ kJ/mol} < \Delta H_{\text{mix}} < 5 \text{ kJ/mol}$, while IM phases can be present in HEAs for which $\delta r > 3\%$ and $\Delta H_{\text{mix}} < 0 \text{ kJ/mol}$ [5,13]. HEAs with $\delta r > 6.2\%$ and $-40 \text{ kJ/mol} < \Delta H_{\text{mix}} < -12 \text{ kJ/mol}$ can contain amorphous phases. The ΔH_{mix} range for IM HEAs overlaps with the ΔH_{mix} ranges for SS and amorphous HEAs. Therefore, the ΔH_{mix} parameter cannot be used for the separation of SS and IM HEAs, but it can be used to predict whether SS or amorphous phase would form. Such selectivity of ΔH_{mix} can be easily understood because ΔH_{mix} is a characteristic of disordered phases, to which SS and amorphous phases belong, while the enthalpy of formation ΔH_{IM} should be used for IM phases, which is different from ΔH_{mix} .

Trying to separate SS and IM phase fields, Yang and Zhang [6] proposed a parameter Ω , which contains both ΔS_{mix} , and ΔH_{mix} , and is calculated as:

$$\Omega = T_m \Delta S_{\text{mix}} / |\Delta H_{\text{mix}}| \quad (4)$$

Here $T_m = \sum c_i T_{mi}$ and T_{mi} is the melting point of element i . Only SS phases are found in as-cast HEAs for which $\Omega \geq 1.1$ and $\delta r < 3.6\%$. SS and IM HEAs share the space of $3.6\% \leq \delta r < 6.6\%$ and $1.1 \leq \Omega \leq 10$, while at $\Omega > 10$ only SS HEAs are identified. Most of the IM alloys have $\delta r \geq 6.6\%$ and $1 \leq \Omega \leq 2$, and metallic glasses have $\delta r \geq 5\%$ and $\Omega \leq 2$ [6].

These empirical criteria for phase selection were developed and tested using as-cast HEAs, which often contain non-equilibrium phases. Wang et al. [14] have recently evaluated these criteria to predict formation of equilibrium SS or IM phases in well homogenized and annealed HEAs. Using a limited number of data (27 alloys) available in the literature at that time, Wang et al. [14] found that the ΔH_{mix} and δr ranges for HEAs with only SS phases after annealing narrowed significantly. Annealed HEAs with FCC and BCC solid solutions had $\Delta H_{\text{mix}} > -7.5 \text{ kJ/mol}$ and $\delta r < 3.3\%$, while as-cast SS HEAs had $\Delta H_{\text{mix}} > -12.5 \text{ kJ/mol}$ and $\delta r < 6.2\%$. Annealed HEAs with intermetallic compounds appeared at $\Delta H_{\text{mix}} < -7.5 \text{ kJ/mol}$ and $\delta r > 3.3\%$. However, three Al-containing HEAs that were identified as BCC structures had ΔH_{mix} between -17 and -10 kJ/mol and δr between 5 and 6%, which are typical for IM HEAs. They suggested that the Al-containing HEAs probably have a B2 phase. However, ΔH_{mix} and δr are characteristics of the alloy composition only and are not affected by alloy processing. Therefore, narrowing the $\Delta H_{\text{mix}} - \delta r$ range for the SS HEAs after annealing may indicate that IM phases formed after annealing in other HEAs, which were solid solutions after casting, or this can just be due to much smaller number of the assessed alloys.

While the effect of δr on the formation of SS or IM phases can be understood from Hume-Rothery rules, the influence of ΔH_{mix} and/or Ω values on the phase selection is not so clear. The authors who derived these criteria [5,6,11,15] state that phase selection among different phases is determined by the competition between ΔH_{mix} and $T\Delta S_{\text{mix}}$. However this statement is thermodynamically incorrect, because these terms are not in competition, but rather work together to reduce the Gibbs free energy of the SS phase.

Troparevsky et al. [16] (2015) proposed a model that, through the use of high-throughput computation of the enthalpies of formation of binary compounds, seemed to predict single-phase SS equiatomic HEAs. The stability of the competing SS and IM phases was analyzed by comparing the contributions to the Gibbs free energy from only mixing entropy ($-T\Delta S_{\text{mix}}$) for SS alloys and from only the enthalpy of formation ($\Delta H_{ij}^{\text{IM}}$) for the ordered binary compounds. Thus they assumed that $\Delta H_{\text{mix}} = 0$ and $\Delta S_{\text{IM}} = 0$, which is generally incorrect as ΔH_{mix} can be very negative in some cases and ΔS_{IM} can be comparable with ΔS_{mix} in ordered structures

in which the number of alloying elements is higher than the number of sublattices. Troparevsky et al. also assumed that an HEA will have a single SS phase at a temperature T if $\Delta H_{ij}^{\text{IM}}$ values for any binary system present in the alloy are above $-T\Delta S_{\text{mix}}$. According to their model, among the currently developed non-refractory HEAs only those consisting of Co, Cr, Fe, Mn and/or Ni are truly single-phase solid solutions, while other alloys should form multiple phases during annealing at $T_{\text{cr}} = 0.55 T_m$. The conclusion may be correct for equiatomic alloys, however, many non-equiatomic HEAs containing other elements than listed above also retain their single-phase SS structure after annealing (see Table 1). Using their approach, Troparevsky et al. provided a list of new HEAs, which should be single-phase solid solutions, to guide experimental searches. In addition to the combinations of 5 elements listed above, these alloys can also contain such elements as Ir, Os, Rh, Pd, Ru, Pt, – all are very expensive.

1.1. A simple thermodynamic criterion for SS or IM phase formation

In this paper we propose a new approach for the phase selection, which takes into account both enthalpy and entropy terms of the competing phases. The main assumption in this approach is that ΔH_{mix} and ΔH_{IM} are related. Both terms can be calculated by summing bond energies between first-neighbor atom pairs and thus some relationship between these terms should exist. The entropy of formation, ΔS_{IM} , of binary and/or ternary compounds is close to zero. However, it can be high in multi-component compounds that have more constituents than sublattices and/or have a large solubility range, although ΔS_{IM} should not be higher than ΔS_{mix} . For example, using the sublattice model for configurational entropy [17], it can be shown that ΔS_{IM} of $(A,B)_1(C,D,E)_3$ compound is $0.997R$, where R is the gas constant. This is more than 60% of ΔS_{mix} of a 5-component equiatomic SS HEA. As the first approximation, we assume linear relationships between ΔH_{IM} and ΔH_{mix} , and between ΔS_{IM} and ΔS_{mix} for HEAs with negative values of ΔH_{mix} :

$$\Delta H_{\text{IM}} = \kappa_1 \cdot \Delta H_{\text{mix}} \text{ and } \Delta S_{\text{IM}} = \kappa_2 \cdot \Delta S_{\text{mix}} \quad (5)$$

where $\kappa_1 > 1$ and $0 \leq \kappa_2 < 1$. The thermodynamic condition for the formation of a SS phase at a temperature T is:

$$\Delta H_{\text{mix}} - T\Delta S_{\text{mix}} < \Delta H_{\text{IM}} - T\Delta S_{\text{IM}} \quad (6)$$

Combining Eqs. (5) and (6) results:

$$\kappa_1 = \frac{\Delta H_{\text{IM}}}{\Delta H_{\text{mix}}} < -\frac{T\Delta S_{\text{mix}}}{\Delta H_{\text{mix}}}(1 - \kappa_2) + 1 \equiv \kappa_1^{\text{cr}}(T) \quad (7)$$

Equation (7) indicates that a SS phase with given ΔS_{mix} and ΔH_{mix} values ($\Delta H_{\text{mix}} < 0$) is thermodynamically preferable at a temperature T , if the $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$ ratio (i.e. κ_1) for any competing IM phase is below the critical value $\kappa_1^{\text{cr}}(T) = T\Delta S_{\text{mix}}/|\Delta H_{\text{mix}}|(1 - \kappa_2) + 1$. It can be seen that κ_1^{cr} increases with a decrease in $|\Delta H_{\text{mix}}|$ and an increase in the level of ordering of an intermetallic phase. Thus the condition for suppression of IM phases at a temperature T is:

$$\kappa_1^{\text{cr}}(T) > \Delta H_{\text{IM}}/\Delta H_{\text{mix}} \quad (8)$$

Table 1 shows 45 HEAs, including 27 alloys analyzed by Wang et al. [14], for which information about phase contents in the annealed condition, as well as the annealing temperature, is available. We calculated δr , ΔH_{mix} , ΔH_{IM} , $\Omega(T_A)$, $\kappa_1^{\text{cr}}(T_m)$ and $\kappa_1^{\text{cr}}(T_A)$ parameters for these alloys (T_A is the absolute annealing temperature) and compared how well these parameters can predict phases at a given annealing temperature. ΔH_{IM} values were calculated

Table 1
Phases in several HEAs after annealing at a temperature T_A . Calculated parameters discussed in the paper are also shown.

Material	T_A (K) [refs.]	Phases at T_A	δr	ΔH_{mix} (kJ/mol)	ΔH_{IM} (kJ/mol)	Ω (T_A)	κ_1^{CT} (T_A)	$\frac{\Delta H_{\text{IM}}}{\Delta H_{\text{mix}}}$
Al _{0.25} CoCrFeNi	1273 [18]	FCC	3.15	-6.78	-14.19	2.39	1.95	2.09
Al _{0.3} CoCr ₂ FeNi	973 [19]	BCC + FCC + σ	3.09	-7.03	-11.39	1.70	1.68	1.62
Al _{0.3} CoCrFeNi	1173 [20]	FCC + B2	3.33	-7.30	-15.76	2.06	1.82	2.16
Al _{0.3} CrFe _{1.5} MnNi _{0.5}	973 [19]	BCC + FCC + σ	3.13	-5.53	-13.49	2.17	1.87	2.44
Al _{0.3} NbTa _{0.8} Ti _{1.4} V _{0.2} Zr _{1.3}	1473 [21]	BCC	4.80	-6.34	-5.62	2.42	1.97	0.89
Al _{0.3} NbTaTi _{1.4} Zr _{1.3}	1473 [21]	BCC + BCC	4.35	-4.43	-6.26	4.20	2.68	1.41
Al _{0.4} CoCrFeMnNiV	973 [19]	σ	3.54	-11.96	-22.56	1.29	1.52	1.89
Al _{0.4} Hf _{0.6} NbTaTiZr	1473 [22]	BCC	4.25	-9.04	-9.25	1.92	1.77	1.02
Al _{0.5} CoCrCuFeNi	973 [23]	BCC + FCC + IM	3.60	-3.40	-12.87	4.21	2.68	3.79
Al _{0.5} CrFeNiTiV	973 [19]	IMs	4.77	-19.85	-35.52	0.59	1.24	1.79
Al _{0.5} CrMnFe _{1.5} Ni _{0.5}	973 [19]	BCC + σ	3.56	-7.29	-17.30	1.69	1.68	2.37
Al _{0.5} NbTa _{0.8} Ti _{1.5} V _{0.2} Zr	1473 [21]	BCC + BCC	4.77	-12.06	-11.94	1.36	1.54	0.99
Al _{0.8} CrFe _{1.5} MnNi _{0.5}	973 [19]	BCC/B2	4.00	-9.36	-21.78	1.34	1.54	2.33
Al _{1.17} CoCrFeNi	973 [18]	BCC + B2	4.90	-13.13	-33.68	0.99	1.40	2.56
Al _{1.5} CrFe _{1.5} MnNi _{0.5}	1273 [19]	BCC/B2	4.54	-12.39	-28.27	1.32	1.53	2.28
Al ₂ CoCrFeNi	973 [18]	BCC + B2	5.38	-15.48	-41.14	0.82	1.33	2.66
AlCo _{0.5} Cr _{0.5} Fe _{0.5} MnNiV	973 [19]	BCC/B2	4.25	-21.42	-36.20	0.72	1.29	1.69
AlCo _{0.5} Cr _{0.5} Fe _{0.5} MnNiV _{0.5}	973 [19]	BCC/B2	4.42	-20.89	-35.70	0.73	1.29	1.71
AlCo _{1.5} Cr ₂ Fe _{1.5} Mn ₂ NiV	973 [19]	σ	3.76	-11.74	-22.88	1.31	1.52	1.95
AlMo _{0.5} NbTa _{0.5} TiZr	1673 [22]	BCC + BCC	4.76	-23.76	-25.96	0.84	1.33	1.09
AlNb _{1.5} Ta _{0.5} Ti _{1.5} Zr _{0.5}	1673 [21]	BCC	3.99	-15.04	-21.93	1.39	1.56	1.46
Co _{0.5} CrFeMn _{1.5} Ni	973 [19]	FCC + σ	2.29	-4.03	-7.89	3.12	2.25	1.96
Co _{1.5} Cr _{0.5} FeMn _{0.5} Ni	973 [19]	FCC	2.08	-3.49	-6.26	3.53	2.41	1.80
CoCr _{0.75} FeMn _{0.75} Ni	973 [19]	FCC	2.23	-4.08	-6.83	3.17	2.27	1.68
CoCr _{1.25} FeMn _{0.25} Ni	973 [19]	FCC	1.98	-4.13	-5.43	2.97	2.19	1.31
CoCr ₂ FeNi	1273 [19]	FCC	1.89	-4.45	-3.77	3.17	2.27	0.85
CoCrCuFeMn	1123 [3]	FCC + FCC	2.30	4.18	1.13	3.60	2.44	0.27
CoCrFe _{0.5} Mn _{0.5} Ni _{1.5}	973 [19]	FCC	2.11	-4.89	-6.23	2.52	2.01	1.27
CoCrFeMnNi	1273 [3]	FCC	2.30	-4.19	-6.89	4.06	2.63	1.64
CoCrFeNi	573 [24]	FCC	1.72	-3.78	-5.09	1.75	1.7	1.35
CoCrFeNiTi _{0.5}	973 [25]	FCC + IM	4.12	-11.59	-19.37	1.10	1.44	1.67
CoCrMnNiV	973 [3]	FCC + IM	2.87	-9.18	-17.18	1.42	1.57	1.87
CoFeMnMoNi	973 [3]	FCC + IM	4.25	-3.98	-16.63	3.27	2.31	4.17
CoFeMnNiV	973 [3]	FCC + IM	3.02	-8.86	-18.74	1.47	1.59	2.11
CrFe _{1.5} MnNi _{0.5}	973 [19]	FCC + σ	2.02	-2.13	-6.12	5.03	3.01	2.88
CrFeMnNiTi	973 [3]	BCC + FCC + IM	4.48	-13.23	-28.61	0.98	1.39	2.16
CrMo _{0.5} NbTa _{0.5} TiZr	1473 [26]	BCC + BCC + IM	6.79	-6.89	-12.28	2.53	1.51	1.78
CrNbTiVZr	1473 [27]	BCC + IM	7.17	-4.70	-9.17	4.19	1.84	1.95
CrNbTiZr	1473 [27]	BCC + IM	7.13	-5.25	-12.37	3.23	1.65	2.36
Cu _{0.5} CoCrFeNi	1273 [28]	FCC	1.63	0.51	-1.92	32.58	14.03	-3.73
HfNbTaTiZr	1473 [29]	BCC	3.93	2.66	2.36	7.42	3.97	0.89
MoNbTaVW	1673 [30]	BCC	5.70	-4.69	-14.45	4.78	2.91	3.08
MoNbTaV	1673 [31]	BCC	5.37	-6.63	-12.88	2.91	2.16	1.94
NbTiV ₂ Zr	1473 [27]	BCC + BCC + BCC	6.50	-1.14	1.08	14.36	6.74	-0.95
NbTiVZr	1473 [27]	BCC	6.13	-0.18	1.52	97.02	39.81	-8.68

using equation similar to Eq. (3) and the enthalpy of formation values $\Delta H_{ij}^{\text{IM}}$ for binary intermetallics reported in Ref. [16]:

$$\Delta H_{\text{IM}} = \sum_{i < j} 4H_{ij}^{\text{IM}} c_i c_j \quad (9)$$

κ_1^{CT} was calculated for a partially ordered condition of an IM phase ($\kappa_2 = 0.6$). $\Omega(T_A)$ was calculated using Eq. (4) in which T_A was used instead of T_m .

The ΔH_{mix} vs. δr , $\Omega(T_A)$ vs. δr and $\kappa_1^{\text{CT}}(T_A)$ vs. $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$ plots for the annealed alloys are shown in Fig. 1(a), (b) and (c), respectively. It can be seen that HEAs with the FCC crystal structures are well separated from IM HEAs with the use of ΔH_{mix} and δr parameters. Six out of seven of them fall within a top left rectangle (Fig. 1a) identified by Wang et al. [14] ($-7.5 < \Delta H_{\text{mix}} < 5$ kJ/mol, $\delta r < 3.3\%$) and one is slightly beyond of this rectangle (at $\Delta H_{\text{mix}} = -6.8$ kJ/mol and $\delta r = 3.47\%$). All alloys containing IM phases have $\Delta H_{\text{mix}} < -6.8$ kJ/mol and $\delta r > 3.47\%$. However SS HEAs consisting of BCC phases have ΔH_{mix} and δr values, which are common to both FCC and IM alloys. Thus ($\Delta H_{\text{mix}} - \delta r$) criterion does not work for HEAs containing BCC phases. The Ω criterion does not work at all (see Fig. 1b): The analyzed SS and IM alloys fall in the

same range of Ω and FCC HEAs are separated from all other alloys on the $\Omega(T_A) - \delta r$ plot by atomic size difference only. This observation supports our statement that ΔS_{mix} and ΔH_{mix} terms from which Ω is derived are not competing with each other but represent the same state of a SS phase.

When $\kappa_1^{\text{CT}}(T_A)$ are plotted versus $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$, clear separation of SS alloys from IM-containing alloys can be seen (Fig. 1c). To visualize this, a dashed line corresponding to the condition $\kappa_1^{\text{CT}}(T_A) = \Delta H_{\text{IM}}/\Delta H_{\text{mix}}$ is also shown in Fig. 1c. Almost all SS alloys, except two with a BCC structure, fall above the dashed line ($\kappa_1^{\text{CT}}(T_A)$ for SS alloys are above $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$) and almost all IM-containing HEAs fall below this line ($\kappa_1^{\text{CT}}(T_A)$ for these alloys are below $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$). This analysis indicates that the κ_1^{CT} parameter has an improved ability to predict the presence or absence of equilibrium IM phases in HEAs at a given annealing temperature than δr , ΔH_{mix} and/or Ω parameters. However, the κ_1^{CT} parameter cannot predict what types of solid solution phases (FCC, BCC or HCP) will form. Other criteria should be used to estimate this.

2. Conclusions

A simple thermodynamic criterion ($\kappa_1^{\text{CT}}(T)$ vs. $\Delta H_{\text{IM}}/\Delta H_{\text{mix}}$) is

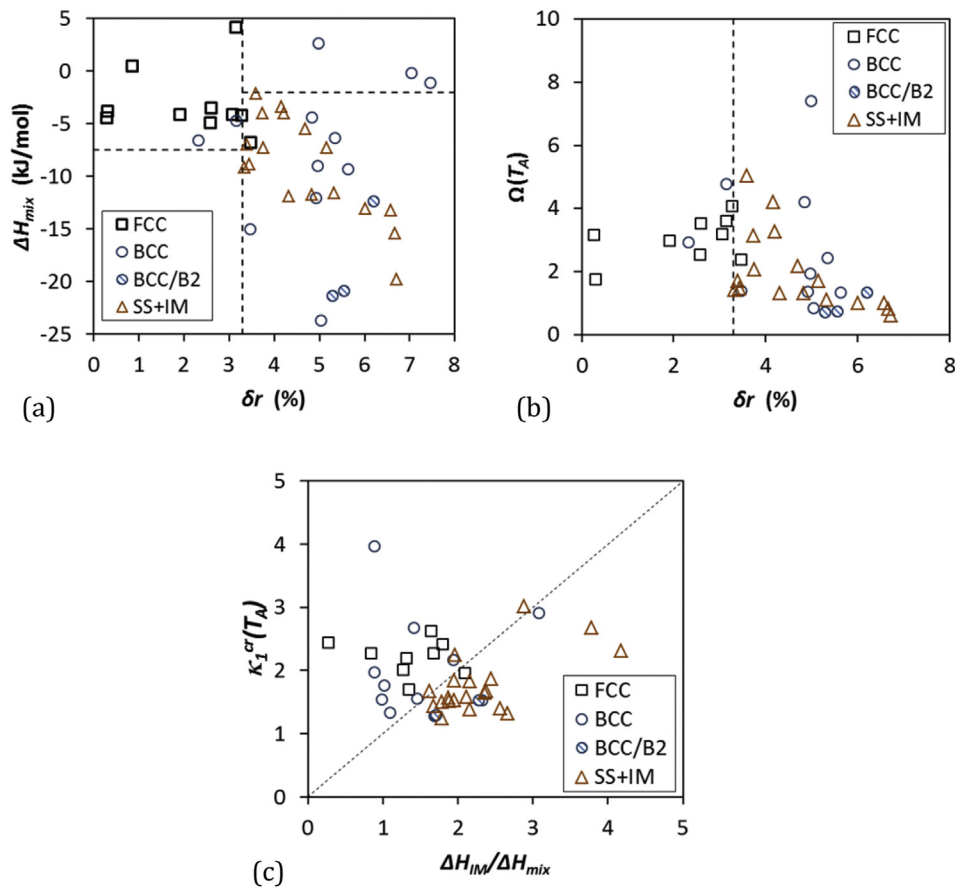


Fig. 1. (a) The $\Delta H_{mix} - \delta r$, (b) $\Omega(T_A) - \delta r$ and (c) $\kappa_1^{cr}(T_A) - \Delta H_{IM}/\Delta H_{mix}$ plots for annealed HEAs with different phase contents after annealing.

proposed to predict what types of equilibrium phases (solid solutions or intermetallics) are present in a high entropy alloy at a given temperature T . The criterion was verified using 45 currently available HEAs and showed good correlation with experiment. It is shown that the new criterion gives an improved ability to predict whether solid solution or intermetallic phases will form at a given temperature compared to earlier δr vs ΔH_{mix} or δr vs Ω criteria.

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