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AD 911384



Research and Development Technical Report
ECOM-0129-F

WATER ACTIVATED ZINC-SILVER OXIDE

PRIMARY BATTERY

FINAL REPORT

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By
C. C. BROWN

JUNE, 1973

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UNITED STATES ARMY ELECTRONICS COMMAND · FORT MONMOUTH, N.J.

CONTRACT DAAB07-71-C-0129

EAGLE-PICHER INDUSTRIES, INC.
Joplin, Missouri

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WATER ACTIVATED ZINC-SILVER OXIDE
PRIMARY BATTERY

FINAL REPORT

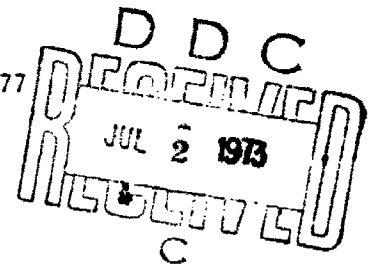
16 February 1971 to 15 March 1973

CONTRACT NO. DAAB07-71-C-0129

DA PROJECT NO. 1T0627 05A 0530277

Prepared by

C. C. Brown



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Couples Department
Electronics Division
Eagle-Picher Industries, Inc.
Joplin, Missouri

For

U. S. ARMY ELECTRONICS COMMAND, FORT MONMOUTH, N. J.

ABSTRACT

This report describes the design, development, manufacture and evaluation testing of a Zinc-Silver Oxide reserve battery in accordance with "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery". This includes a description of the design effort, the design, the test program, the test equipment and the test results. The evaluation testing showed compliance with the requirements of the technical guidelines.

FOREWORD

This work was performed for Power Sources Division, Electronics Components Laboratory, U.S. Army Electronics Command, Fort Monmouth, New Jersey, under Contract DAAB07-71-C-0129. This report is prepared in accordance with DDI423, Exhibit A under the above contract and is intended to describe the complete program.

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1.0 GENERAL

The work performed under this contract consisted of the design, development and fabrication of sixty (60) batteries as described in the following paragraphs and selection of thirty (30) of these units for test in accordance with 2-f of "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery" and Table I herein.

2.0 DESIGN FEATURES

2.1 Cell Design

The cell design effort was begun with the design approach described in Eagle-Picher proposal EPP-1170-474/DMH which was in turn based on an Eagle-Picher internally developed battery with performance characteristics similar to those required by this contract. The proposed design called for one (1) negative and two (2) positive plates in each cell. The area of each of these plates was 5.25 square inches and the total weight of positive material was 28.8 grams and of negative material was 23.6 grams. Cells were fabricated with this plate design and with two (2) layers of membrane separation on the positive plate and one (1) layer of absorbent separation on the negative plate. These cells, when tested, failed to yield the required capacity before the cutoff voltage was reached. When approximately half of the expected capacity was expended the voltage dropped noticeably to a lower level which was maintained for a short time then gradually decreased to the point of cutoff. These voltage characteristics can be seen in the curve of Figure 1.

These cells were disassembled and it was determined that the active material was not being completely utilized because the potassium hydroxide electrolyte was not being dispersed enough to completely activate the positive plates. In order to correct this cells were fabricated with a layer of absorbent separation between the positive plate and the membrane separation and other cells with no separation on the positive plate and with two (2) layers of both membrane and absorbent separation on the negative plate. Neither of these designs produced any significant improvement in the performance.

The next step was to fabricate cells with the same positive plate area and active material as the first design but only half the length of the first design. This produced a cell with four (4) positive and three (3) negative plates. Since the same weight plates were used as the original design, excess negative material was in the cell because three (3) plates were required to balance the four (4) positive plates. These cells produced the expected capacity, 8.9 ampere hours, at a voltage .05 to .08 VDC above that of the first design.

Cells were then fabricated using the shorter plate design but with lighter negative plates to provide the proper active material ratio, positive-to-negative. In order to fit the specified battery outline, these plates were shorter than the first half-length cells. These changes resulted in a design with six (6) positive and five (5) negative plates each of 1.69 square inches, producing a total negative area of 8.55 square inches and positive area of 10.12 square inches. The negative material weight is 21.0 grams for the five (5) plates

and the positive material weight is 30.35 grams for six (6) plates. These cells provided good voltage and capacity in excess of that required by the specification.

2.2 Case Design

The major controlling factor in the case design was the cell configuration which would meet the specified electrical requirements. Because a short multiple plate cell was required to achieve the required electrical performance, the orientation of the cells would have to be across the short dimension of the specified envelope. With this cell configuration, the method of activation must then be determined.

The cells will activate quicker from the end because the separation is open at the end allowing the water to flow directly in between the layers of separation and the plates. The short cell configuration described above fits into the specified envelope leaving room for the activation channel along one side and the connector on the end as shown in Figure 2. In order to prevent electrolyte leakage and allow escape of the gases generated during stand and discharge, porous teflon vent filters, also shown in Figure 2, were provided at both ends of the cells. This allows the gas to escape freely with the battery in any position since both vents could not be covered by electrolyte at the same time.

The first method of sealing tried was to provide a neoprene gasket, on all of the cells, which would be compressed by the cover which contained the vent filters. Leakage occurred around the neoprene gasket which was attributed to uneven compression of the gasket.

The next sealing method tried consisted of providing a common manifold which activated all cells, reference Figure 2. An expansion stopper is provided in the end of this manifold through which the water can be added. After completion of the activation, the stopper is then installed in the activation port to prevent electrolyte leakage. The gas generated after activation is vented through the porous teflon filters. This method worked well in sealing the unit. Although there was some free electrolyte left in the manifold during discharge, there was no leakage.

This case was fabricated from plastic (MIL-P-21105). The vibration and shock tests were performed on this case with no detrimental effects. The first batteries fabricated had the plate leads and intercell connectors on the end opposite the activation manifold. This resulted in shorting between the plates and the plate leads. The shorting was caused by insufficient clearance between the plates and the end of the cell case. On the other batteries fabricated, the intercell connections and plate leads were placed on the end next to the activation manifold where there was more head room. This type of fabrication prevented shorting of the plate lead wires.

3.0 BATTERY FABRICATION

The batteries were assembled in plastic cases (Figure 2) which were fabricated here in our plant. After formation of the positive plate strips, the plates were cut to size and wrapped with separator. The negative plates are cut to sized and wrapped with separator then placed alternately with the positive plates to make a cell. The cells are immediately inserted

into the case as they are assembled. After all the cells are placed into the case, the cover is installed and sealed in place. The cells are then interconnected and lead wires routed to the power output connector. The cell interconnections are then covered with potting. The top and bottom vent strips are then installed and sealed. The units are then painted and the labels and activation plug installed.

40 TEST PERFORMANCE

The test units were loaded as follows:

Section	Condition A		Condition B	
	2 min. Load 1	18 min. Load 2	Continuous Load	End Voltage
A ₁	(ohms) 6.76 ± 1%	(ohms) O.C.	(ohms) N/A	2.12
A ₂	14.2 ± 1%	291 ± 1%	28.75 ± 1%	10.0

The actual test setup was as shown in Figures 3 and 4.

The batteries were activated with water stabilized for 8 hours minimum at the same temperature as the battery except when the battery was below 40°F. Then the water was stabilized for 8 hours minimum at 40°F. The Immediate Discharge Tests were started five (5) minutes after the start of activation.

When specified, shock and vibration loads as follows were applied to the test unit:

Vibration: Sine, 0.06 in DA
 Sweep, 1 cpm from 10 to 55 to 10 cps
 Duration, 95 ± 5 min/axis, 3 axis

Shock: Average acceleration during first 3ms is 75 g's
 Peak acceleration, 125 to 175 g's
 One shock in each of 3 directions
 Three shocks total

The batteries were activated in accordance with the instructions attached to each battery which is as follows. The battery was removed from its protective packaging and held in the vertical position with

TABLE I

TEST PLAN

<u>TEST DESCRIPTION</u>	<u>LOAD CONDITION</u>	<u>SPECIMEN NUMBERS</u>
Immediate Discharge at 75°F	A	1 - 4
Immediate Discharge at 125°F		5 - 6
Immediate Discharge at 0°F		7 - 8
Immediate Discharge at -20°F		9 - 10
Discharge at 75°F following 7 days activated storage at 75°F		11 - 12
Discharge at 75°F following 100 hours activated storage at 125°F		13 - 14
Immediate Discharge at 75°F following exposure to mechanical vibration and shock		15 - 16
Immediate Discharge at 75°F while being exposed to mechanical shock		17 - 18
Immediate Discharge at 75°F while being exposed to vibration	A	19 - 20
Immediate Discharge at 75°F	B	21 - 22
Immediate Discharge at 125°F		23 - 24
Immediate Discharge at 0°F		25 - 26
Immediate Discharge at -20°F		27 - 28
Discharge at 75°F following 7 days activated storage at 75°F	B	29 - 30

the activation opening at the top (Ref. Figure 2). The unit was filled with water and held in that position for two (2) minutes, then the unit was filled again and rotated 180° so that the activation opening was at the bottom and held in that position two (2) minutes. The plug was then removed and the excess water poured out and the plug was again installed. All activations were completed in the five (5) minutes allowed.

5.0 TEST SUMMARY

Table II gives a summary of test results for the thirty (30) units tested. The low temperatures produced marginal results in the A₁ Section, when discharged at Condition A. This was especially noted at -20°F. This is probably due to the location of the cells being on the end of the battery and their load being open circuit 90% of the time, results in their temperature being lower than average temperature of the cells in the A₂ Section. The A₂ Section was marginal at 0°F and very poor at -20°F when discharged at Load Condition B. The only reason that could be determined for poor operation at Condition B loads was the difference in the rate.

Low capacity in the A₁ Section of Specimens 11, 14, 15 and 16 was experienced during original testing caused by a cell-to-cell short through a poor seal around the bottom vent opening as shown in Figure 5. This opening in the seal allowed zinc dendrites to form between the cells producing a high resistance short. This could be prevented on future batteries fabricated by placing individual vent patches over the bottom vents as shown in Figure 6.

This would not change the seal method but would permit inspection of each seal to verify that no voids are in the seal. This method was used on five (5) units which were tested to the original environments where the shorting occurred. There was no shorting in any of these units. The thirty (30) units delivered have the revised seals in accordance with Figure 6 .

TABLE II

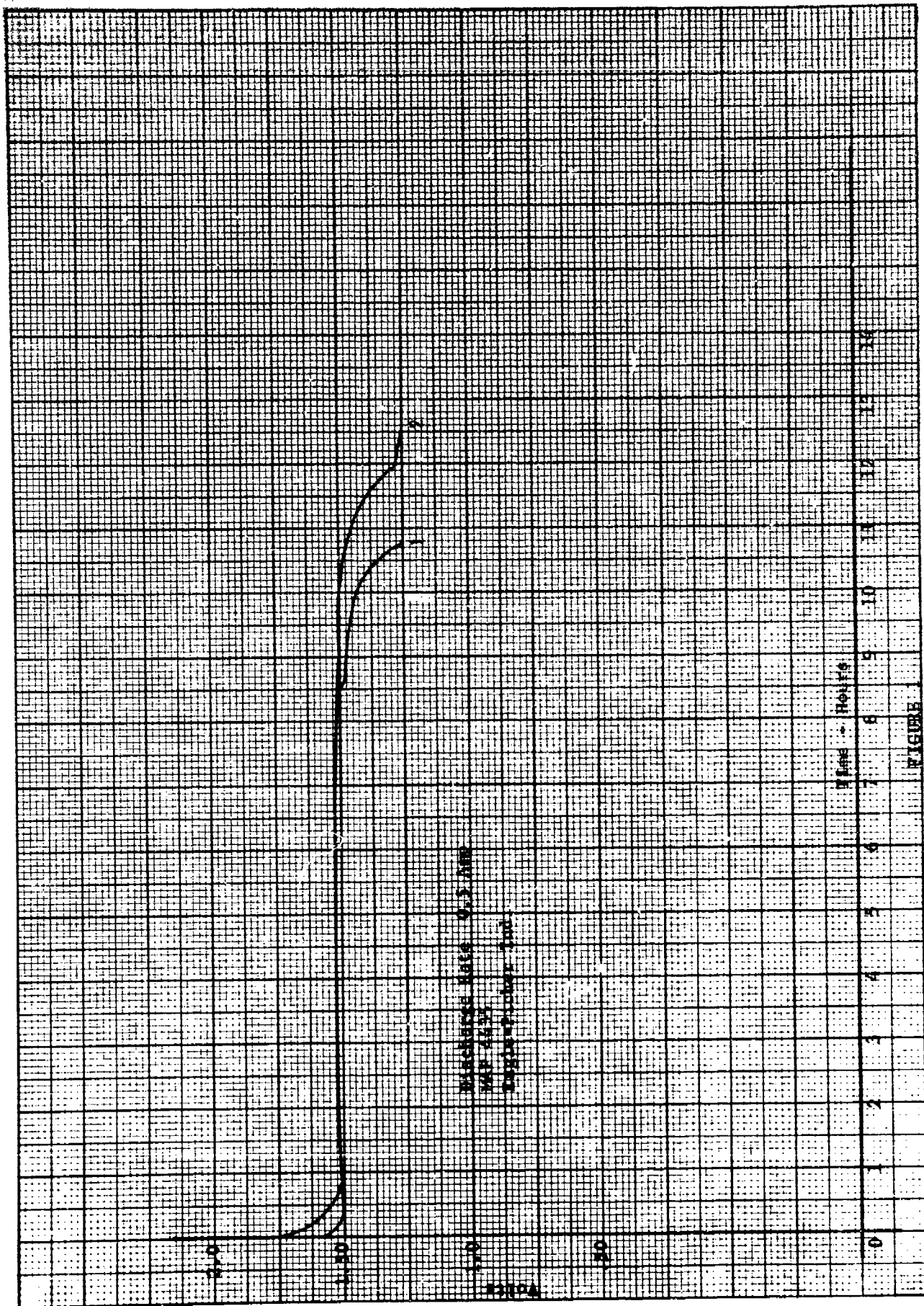
SUMMARY OF TEST RESULTS

SPEC. NO.	SERIAL NO.	TEST DESCRIPTION	A1 SECTION (HOURS)		A2 SECTION (HOURS)		TEST DATE	LOAD COND.
			Required	Results	Required	Results		
1	14	Immediate Discharge at 75°F	60	108	60	68	6/5/72	A
2	11	Immediate Discharge at 75°F	60	123	60	78	6/5/72	A
3	60	Immediate Discharge at 75°F	60	97	60	81	6/5/72	A
4	1	Immediate Discharge at 75°F	60	84	60	71	6/5/72	A
5	4	Immediate Discharge at 125°F	60	89	60	81	6/5/72	A
6	13	Immediate Discharge at 125°F	60	87	60	74	6/5/72	A
7	19	Immediate Discharge at 0°F	50	84	50	72	6/27/72	A
8	45	Immediate Discharge at 0°F	50	80	50	72	6/27/72	A
9	37	Immediate Discharge at -20°F	30*	69	30*	23	6/13/72	A
10	54	Immediate Discharge at -20°F	30*	52	30*	12	6/13/72	A
11	78	Discharge at 75°F following 7 day activated stand at 75°F	50	68	50	60	6/13/72	A
12	42	Discharge at 75°F following 7 day activated stand at 75°F	50	86	50	82	6/13/72	A
13	22	Discharge at 75°F following 100 hour activated stand at 125°F	50	62	50	75	6/13/72	A
14	47	Discharge at 75°F following 100 hour activated stand at 125°F	50	76	50	76	6/13/72	A
15	74	Immediate Discharge at 75°F following exposure to mechanical vibration and shock	60	90	60	79	6/19/72	A
16	24	Immediate Discharge at 75°F following exposure to mechanical vibration and shock	60	64	60	78	6/19/72	A
17	5	Immediate Discharge at 75°F while being exposed to mechanical shock	60	87	60	80	6/19/72	A
18	7	Immediate Discharge at 75°F while being exposed to mechanical shock	60	101	60	77	6/19/72	A
19	8	Immediate Discharge at 75°F while being exposed to vibration	60	103	60	79	6/19/72	A
20	34	Immediate Discharge at 75°F while being exposed to vibration	60	102	60	82	6/19/72	A
21	9	Immediate Discharge at 75°F	N/A	N/A	18	26:45	6/5/72	B
22	18	Immediate Discharge at 75°F	—	—	18	18	6/5/72	B
23	20	Immediate Discharge at 125°F	—	—	18	25	6/7/72	B
24	59	Immediate Discharge at 125°F	—	—	18	26	6/7/72	B
25	46	Immediate Discharge at 0°F	—	—	15	15:15	6/14/72	B
26	31	Immediate Discharge at 0°F	N/A	N/A	15	16:50	6/14/72	B

TABLE II (Continued)

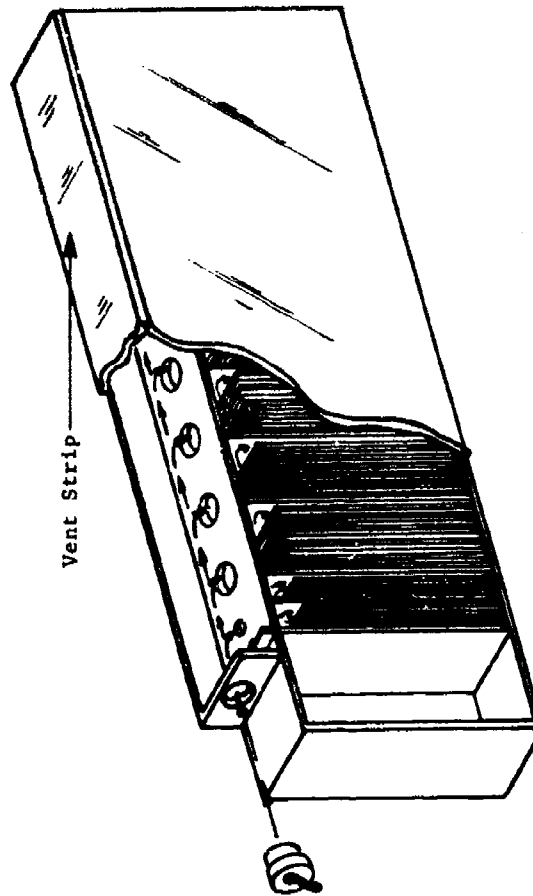
Spec. No.	Serial No.	Test Description	A ₁ SECTION (Hours)		A ₂ SECTION (Hours)		Test Date	Load Cond.
			Required	Results	Required	Results		
27	21	Immediate Discharge at -20°F	N/A	N/A	10*	5	6/13/72	B
28	53	Immediate Discharge at -20°F			10*	1	6/13/72	
29	35	Discharge at 75°F following 7 day activated stand at 75°F			15	23	6/7/72	
30	36	Discharge at 75°F following 7 day activated stand at 75°F	N/A	N/A	15	24	6/7/72	B

* -20°F Test is a Design Goal.



Maximum Rate of 0.5 MPH
 1000
 1000
 1000

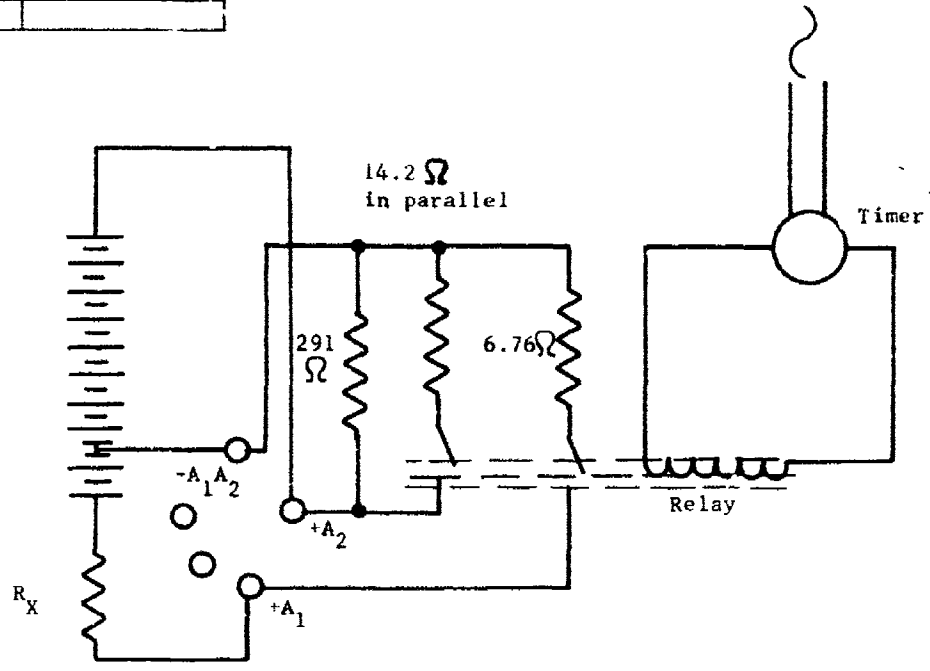
FIGURE



MAP 4435 ACTIVATION SYSTEM
AND ASSEMBLY LAYOUT

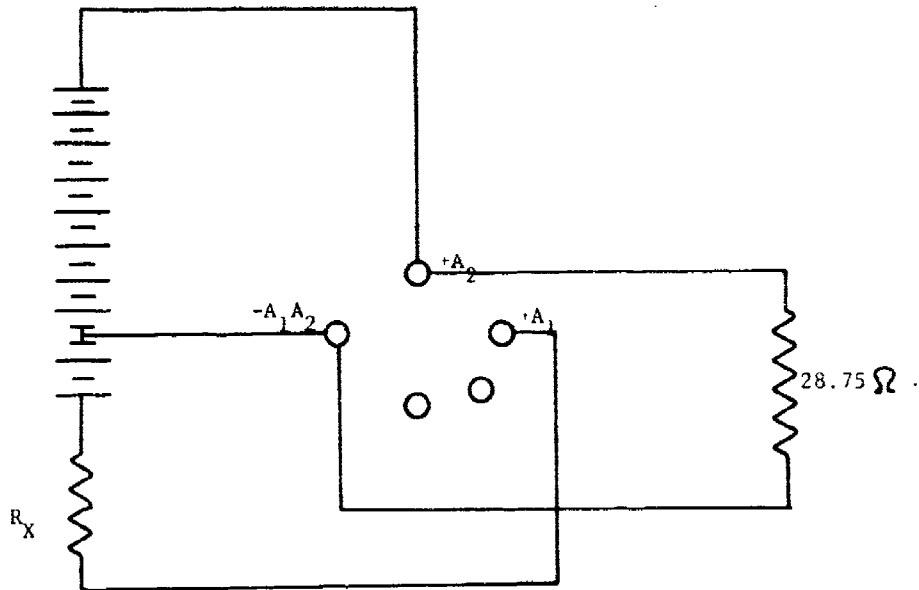
FIGURE 2

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED



UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES TOLERANCES: FRACTIONS \pm ANGLES \pm 3 PLACE DECIMALS $\pm .010$ 2 PLACE DECIMALS $\pm .03$	CONTRACT NO.		EAGLE PICHER INDUSTRIES, INC. COUPLES DEPARTMENT JOPLIN, MISSOURI		
	DATE _____		DISCHARGE SCHEMATIC LOAD CONDITION A		
	PREPARED	_____	SIZE	CODE IDENT NO.	DRAWING NO.
	CHECKED	_____	A	81855	FIGURE 3
ENGINEER	_____	SCALE	_____	SHEET	

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED



UNLESS OTHERWISE SPECIFIED
 DIMENSIONS ARE IN INCHES
 TOLERANCES: FRACTIONS \pm
 ANGLES \pm
 3 PLACE DECIMALS \pm .010
 2 PLACE DECIMALS \pm .03

CONTRACT NO. _____

DATE _____

PREPARED	
CHECKED	
ENGINEER	



EAGLE PICHER INDUSTRIES, INC.
 COUPLES DEPARTMENT
 JOPLIN, MISSOURI



DISCHARGE SCHEMATIC LOAD CONDITION B

SIZE

A

CODE IDENT NO.

81855

DRAWING NO.

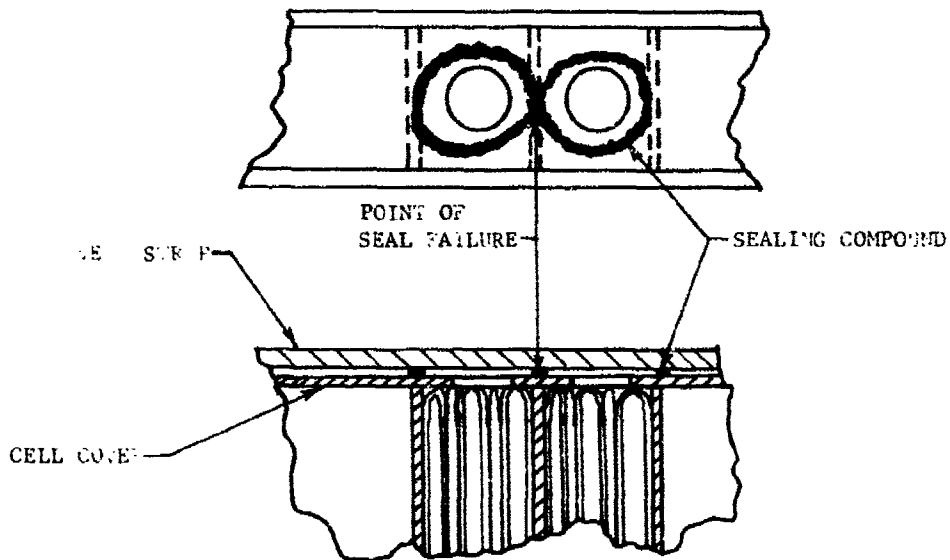
FIGURE 4

SCALE

SHEET

APPLICATION		REVISIONS			
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE	APPROVED

VENT STRIP NOT SHOWN ON TOP VIEW



UNLESS OTHERWISE SPECIFIED
DIMENSIONS ARE IN INCHES
TOLERANCES: FRACTIONS \pm
ANGLES \pm
3 PLACE DECIMALS \pm .010
2 PLACE DECIMALS \pm .03

CONTRACT NO.

DATE _____

PREPARED		
CHECKED		
ENGINEER		



EAGLE PICHER INDUSTRIES, INC.
COUPLES DEPARTMENT
JOPLIN, MISSOURI



ORIGINAL VENT SEAL

SIZE
A

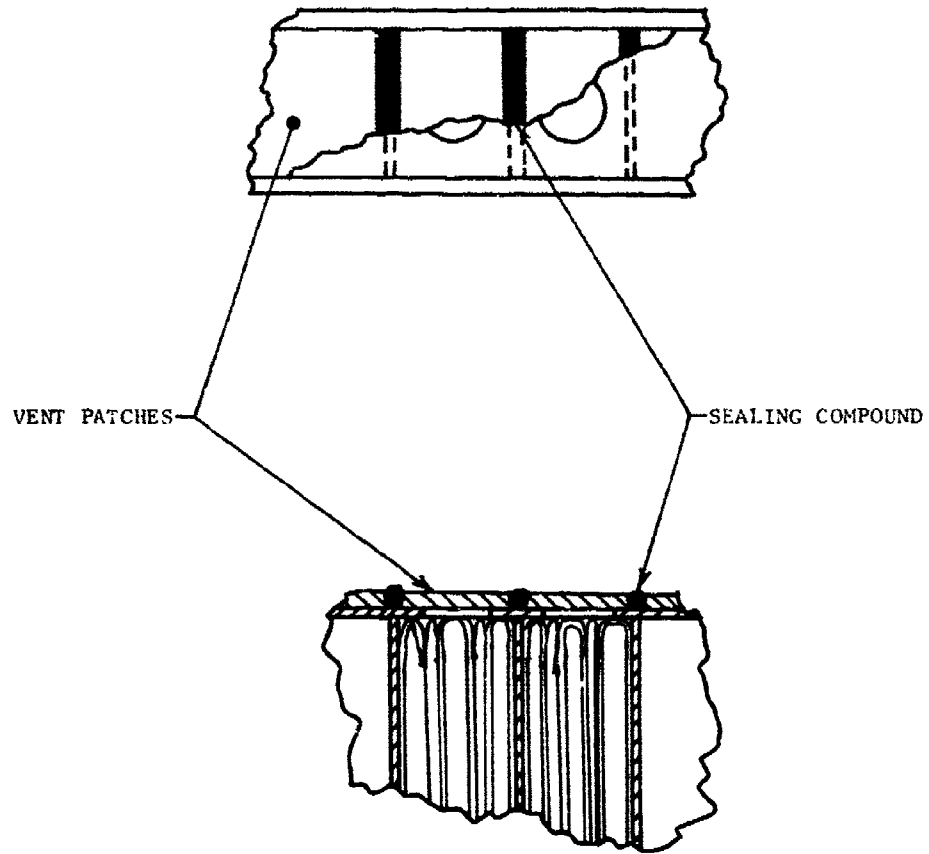
CODE IDENT NO.
81855

DRAWING NO.
FIGURE 5

SCALE N/A

SHEET

APPLICATION		REVISIONS		
NEXT ASSY	USED ON	LTR	DESCRIPTION	DATE APPROVED



UNLESS OTHERWISE SPECIFIED
 DIMENSIONS ARE IN INCHES
 TOLERANCES: FRACTIONS ±
 ANGLES ±
 3 PLACE DECIMALS ± .010
 2 PLACE DECIMALS ± .03

CONTRACT NO.



EAGLE PICHER INDUSTRIES, INC.
 COUPLES DEPARTMENT
 JOPLIN, MISSOURI



DATE _____

PREPARED		
CHECKED		
ENGINEER		

REVISED VENT SEAL

SIZE A	CODE IDENT NO. 81855	DRAWING NO. FIGURE 6
SCALE N/A		SHEET

APPENDIX I

TEST DATA

Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 75°F

Note: For clarity, load 1 surges are shown at 5 hr. intervals. Actual loading was a 2 min. Load 1, 18 min. Load 2 cycle.

Specimen No. 2, S/N 11

Date: June 5, 1972

Battery Output VDC

16

14

12

10

8

6

4

2

0

A₂ Section

A₁ Section

Discharge Time - Hours

10 20 30 40 50 60 70 80 90 100 110 120

Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 75°F

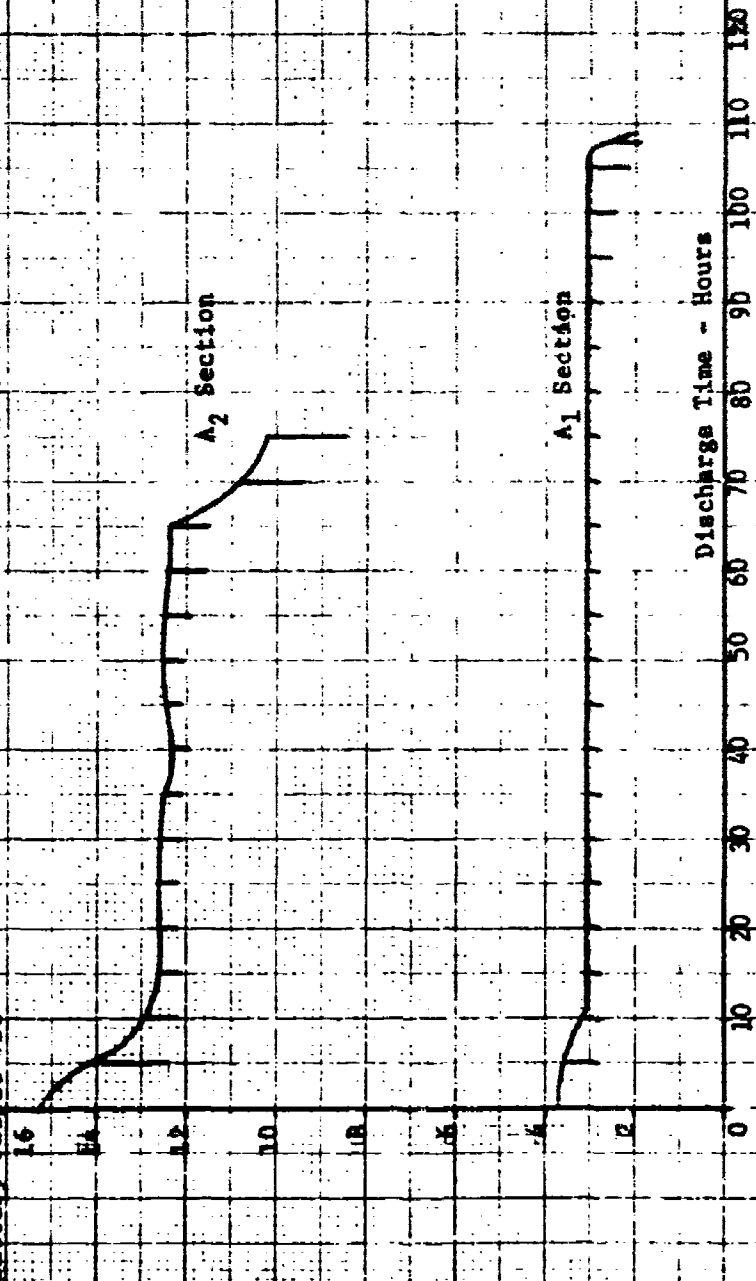
Note: For clarity, load 1 surges are shown at 1 hour intervals.

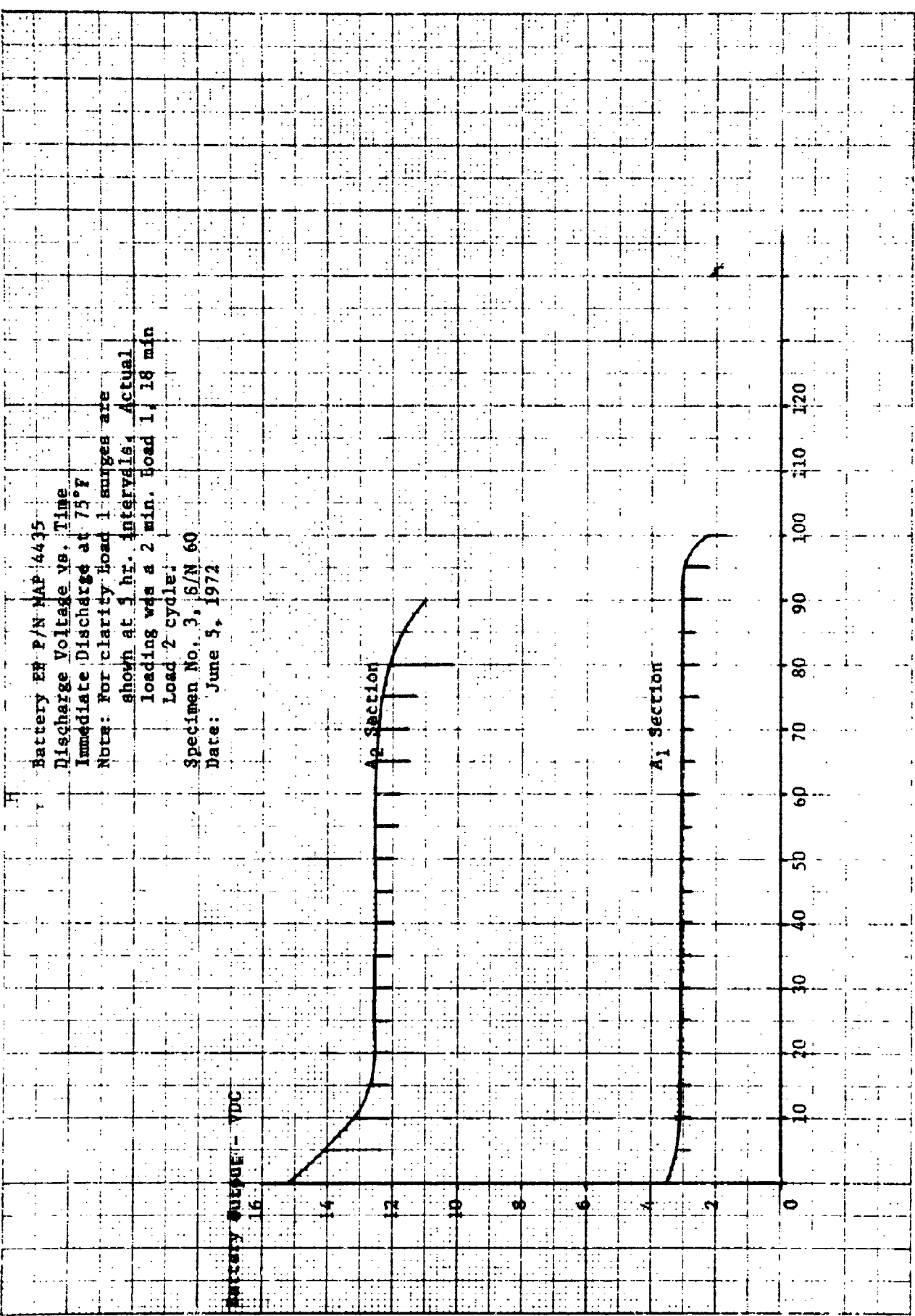
Actual loading was a 2 min. load 1
13 min load 2 cycles

Specimen No. 1, S/N 14

Date: June 5, 1972

Battery Output - VDC





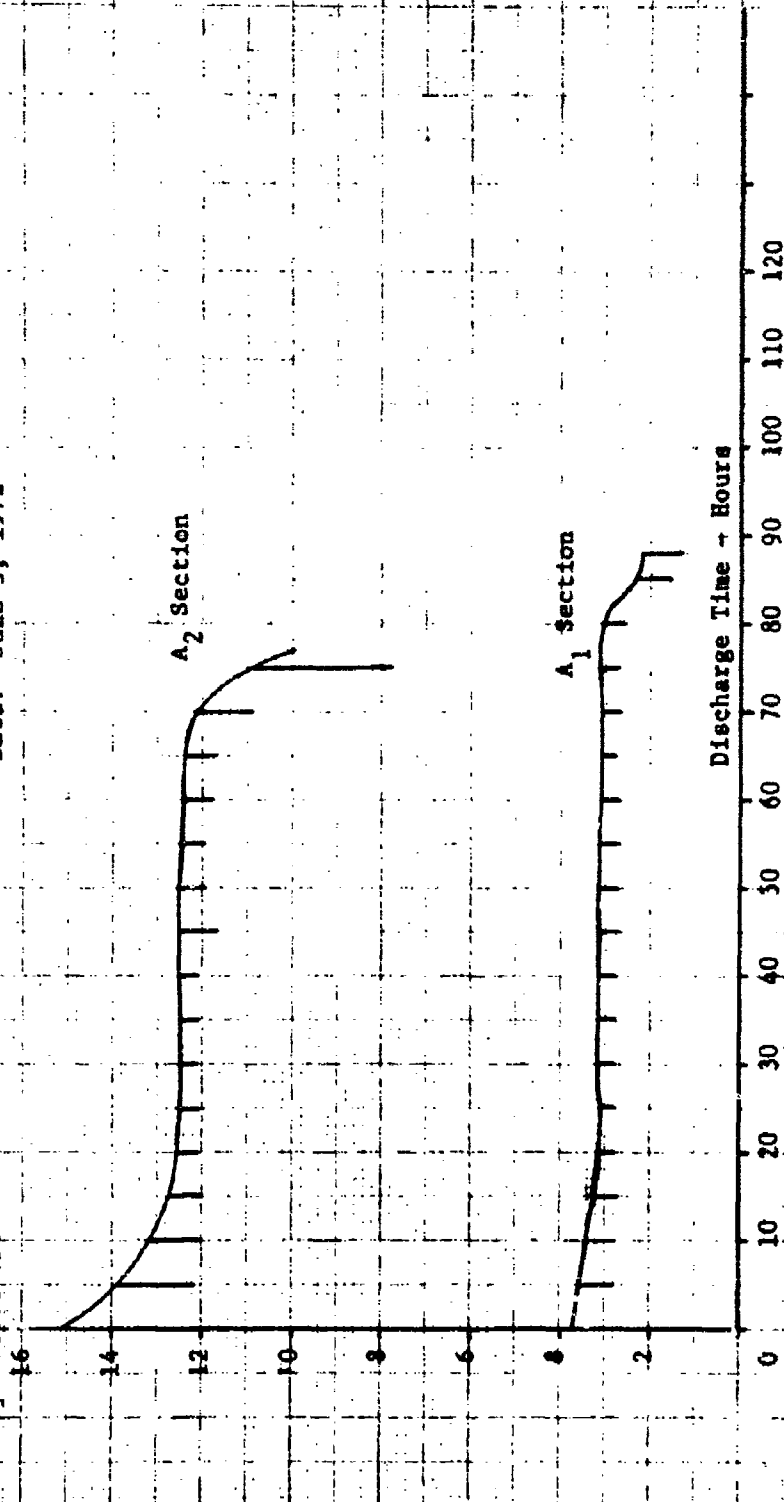
Battery ER P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 75°F
Note: For clarity load surges are
shown at 1 hr. intervals. Actual
loading was a 2 min. load 1, 18 min
load 2 cycle.
Specimen No. 3, 18/N 60
Date: June 5, 1972

Battery EP P/N MAP-4435
Discharge Voltage vs. Time
Immediate Discharge at 75°F

Note: For clarity, Load 1 surges are shown at 5 hr. intervals. Actual loading was a 2 min Load 1, 18 min Load 2.

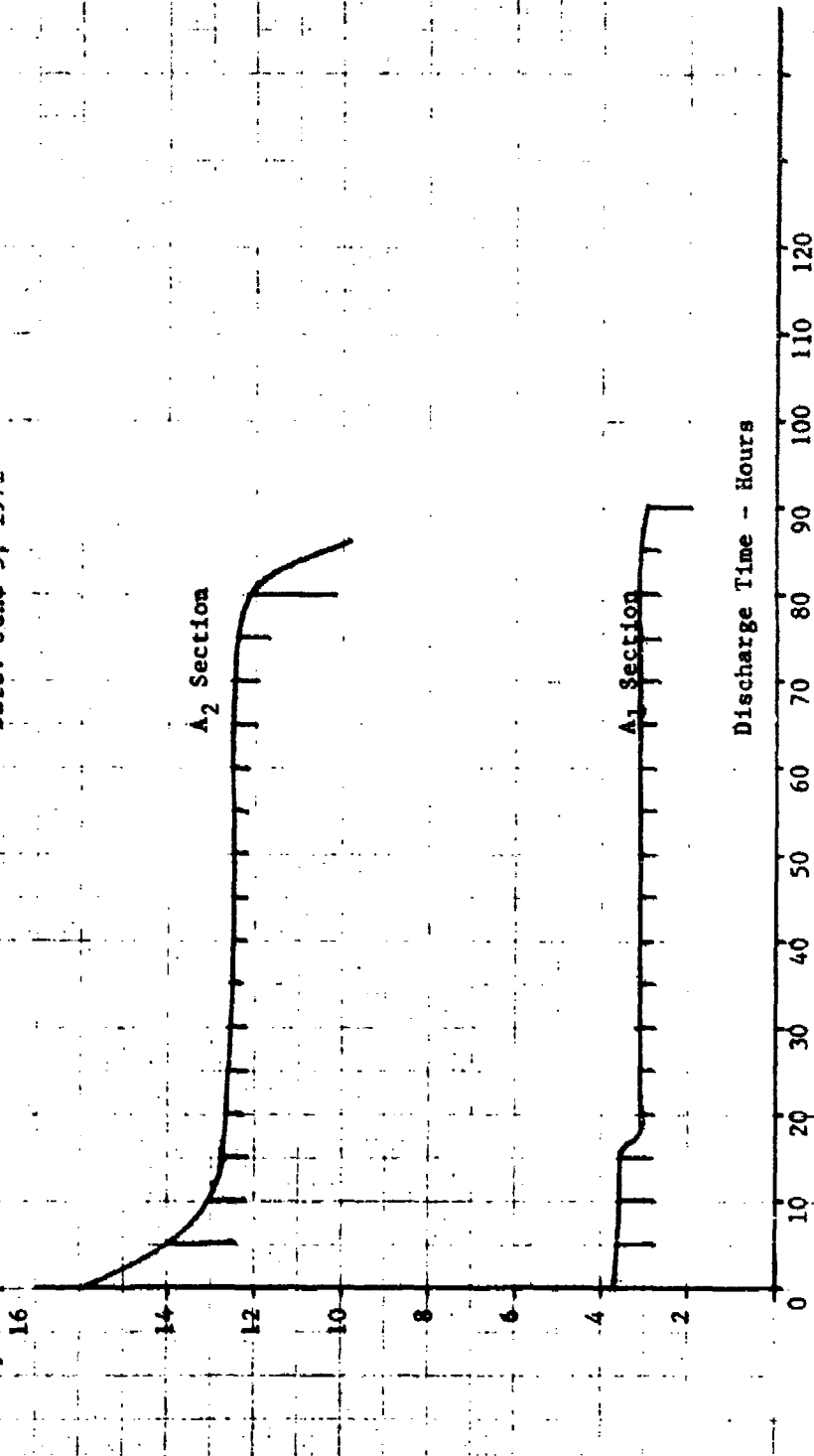
Specimen No. 4, S/N 1
Date: June 5, 1972

Battery Output-VDC



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 125°F
Note: For clarity, Load 1 surges are
shown at 5 hr. intervals. Actual
loading was a 2 min. Load 1, 18 min.
Load 2, cycle.
Specimen No. 5, S/N 4
Date: June 5, 1972

Battery Output - VDC



Battery EP P/N MAP 4435

Discharge Voltage vs. Time

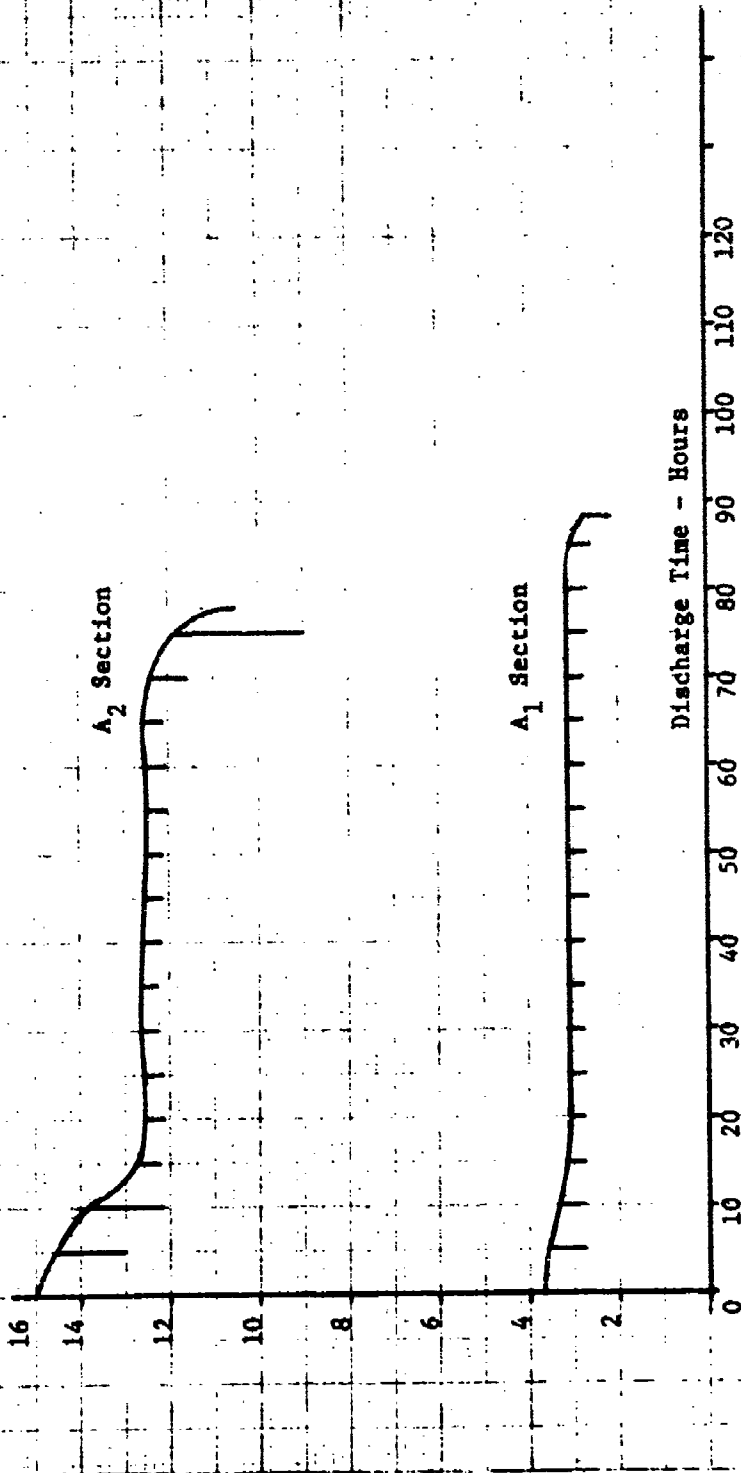
Immediate Discharge at 125°F

Note: For clarity, Load 1 surges are shown at 5 hr. intervals. Actual loading was a 2 min, Load 1, 18 min, Load 2, cycle.

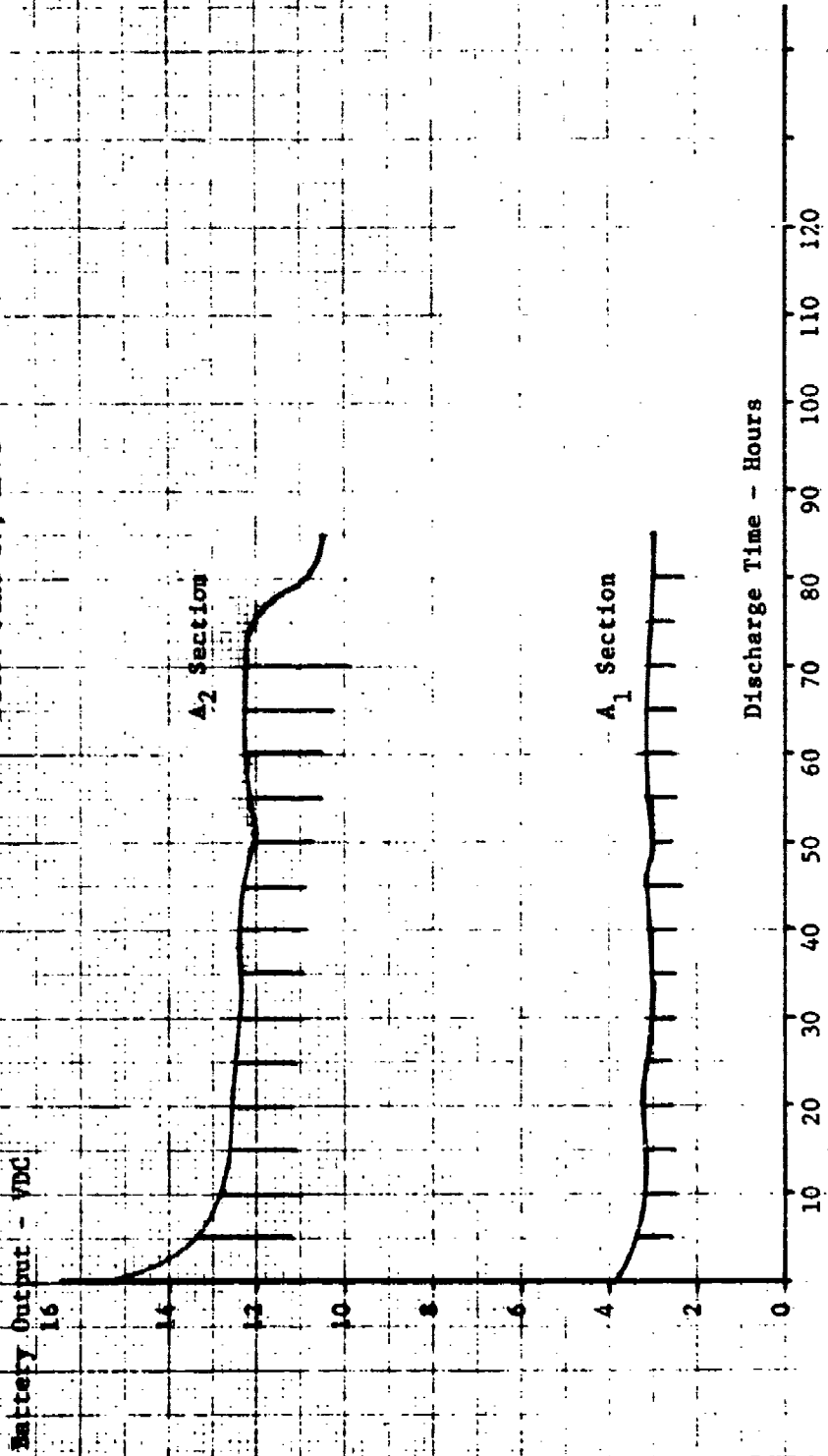
Specimen No. 6, S/N 13

Date: June 5, 1972

Battery Output - VDC



Battery EF P/N MAP4435
 Discharge Voltage vs. Time
 Immediate Discharge at 0°F
 Note: For clarity, Load 1 surges are shown
 at 5 hr. intervals. Actual loading was
 2 min. Load 1, 18 min. Load 2 cycles
 Specimen No 7, S/N 19
 Date: June 27, 1972



Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Immediate Discharge at 0°F

Note: For clarity, Load 1 surges are shown at 1 hr. intervals. Actual loading was a 2 min. Load 1, 18 min. Load 2 cycle

Specimen No. 8, S/M-43

Date: June 27, 1972

Battery Output-VDC

16

14

12

10

8

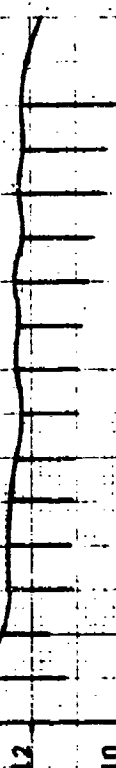
6

4

2

0

A₂ Section



A₁ Section



Discharge Time - Hours

120

110

100

90

80

70

60

50

40

30

20

10

BATTERY EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at $\sim 20^{\circ}$

Note: For clarity, Load 1 surges are shown
at 5 hr. intervals. Actual loading was
a 2 min. load 1; 16 min. load 2 cycle.

Specimen No. 9, S/N 37
Date: June 13, 1972

Battery Output-Vdc

1.8

1.6

1.4

1.2

1.0

0.8

0.6

0.4

0.2

0

A₂ Section

A₁ Section

Discharge Time - Hours

120

110

100

90

80

70

60

50

40

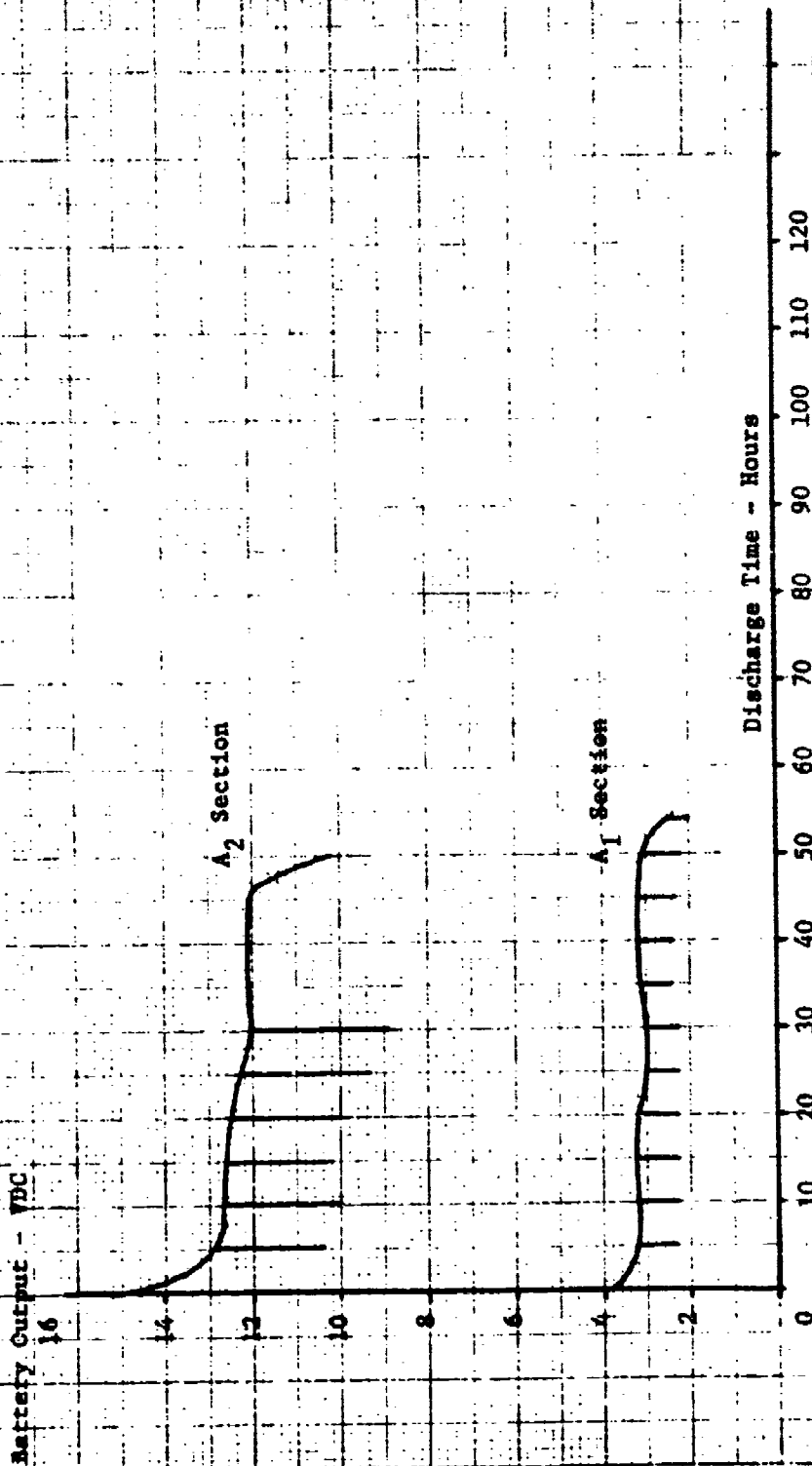
30

20

10

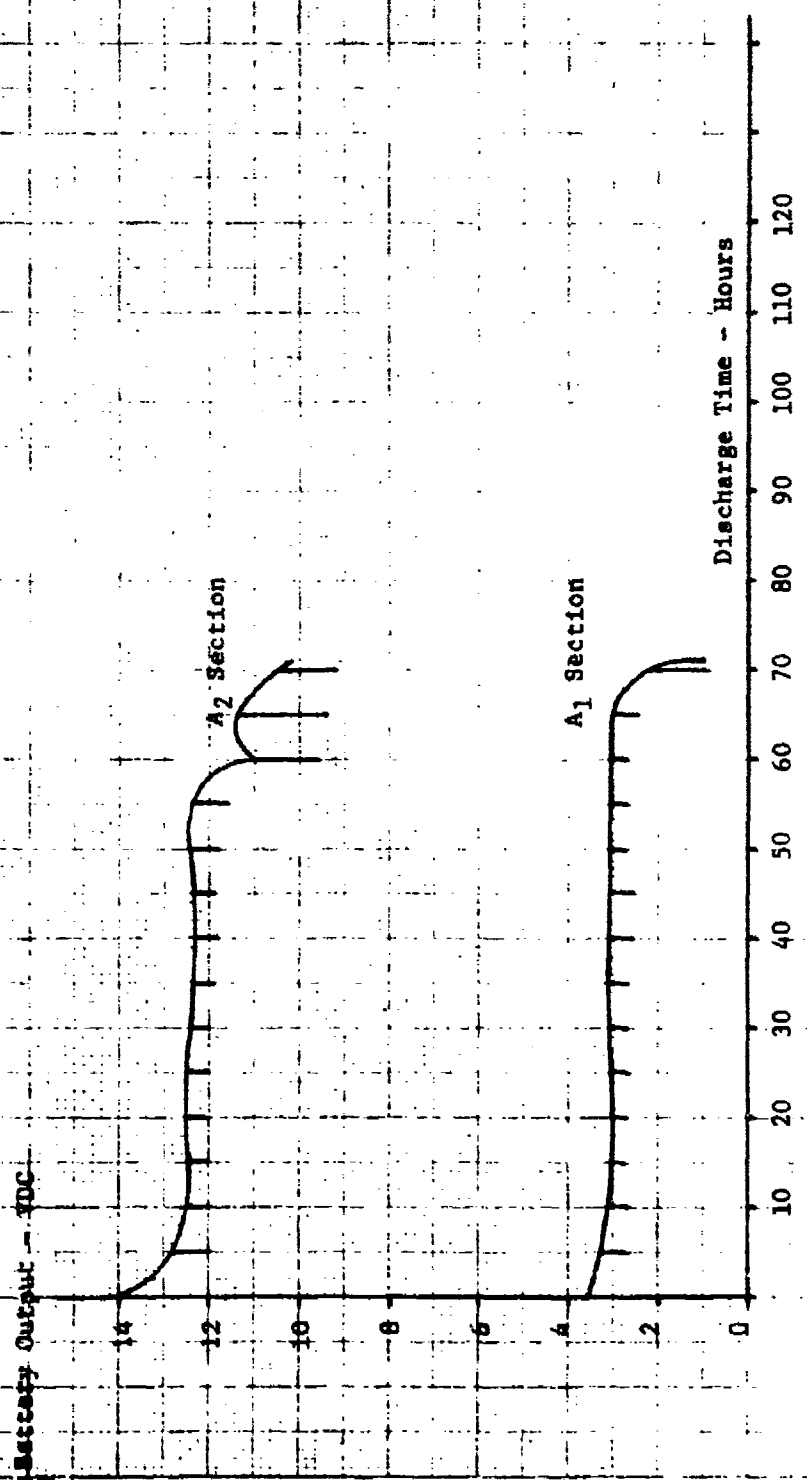
0

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at -20°F
Note: For clarity, Load 1 surges are shown
at 5 hrs. Actual loading was a 2 min.
Load 1, 16 min. Load 2 cycle
Specimen No. 10, S/N 54
Date June 13, 1972

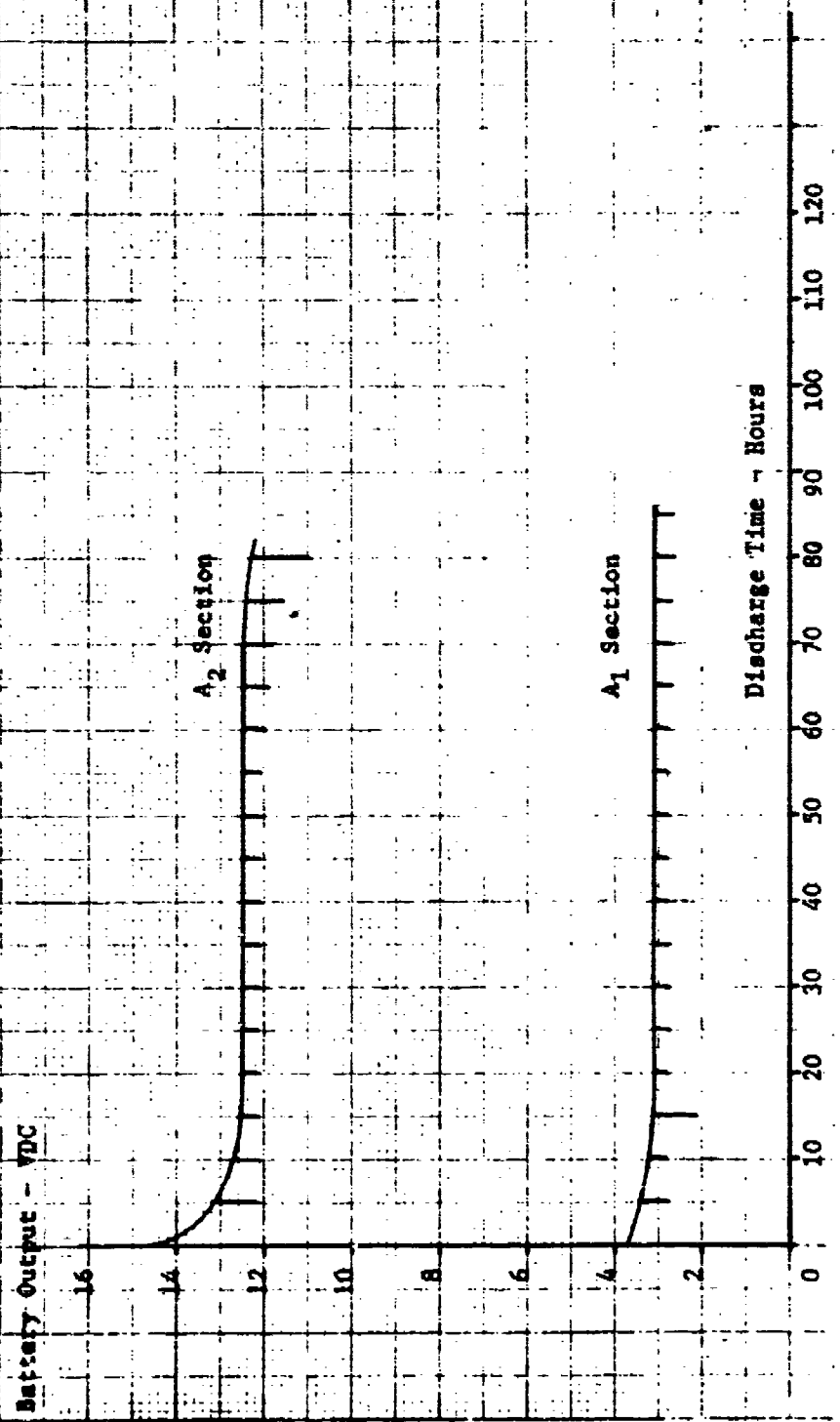


5561 25 4 4-5000 200 304

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Discharge at 75V after 7 day stand at 75^oF
Note: For clarity, Load 1 surges are shown
at 3 hr. intervals. Actual loading was
a 2 min. load 1, 18 min. load 2 cycle.
Specimen No. 11, S/N 78
Date: February 27, 1973



Battery EP P/N MAP 4435
 Discharge Voltage vs. Time
 Discharge at 75°F after 7-day stand at 75°F
 Note: For clarity, load 1 surges are shown at
 5 hr. intervals. Actual loading was a
 2-min. load-1, 18 min. load-2 cycle
 Specimen No. 12, S/N 42
 Date: June 13, 1972



Battery EP P/N 4435

Discharge Voltage vs. Time

Discharge at 75% after 100 hr; ended at 125%

Note: For clarity, Load 1 surges are shown at

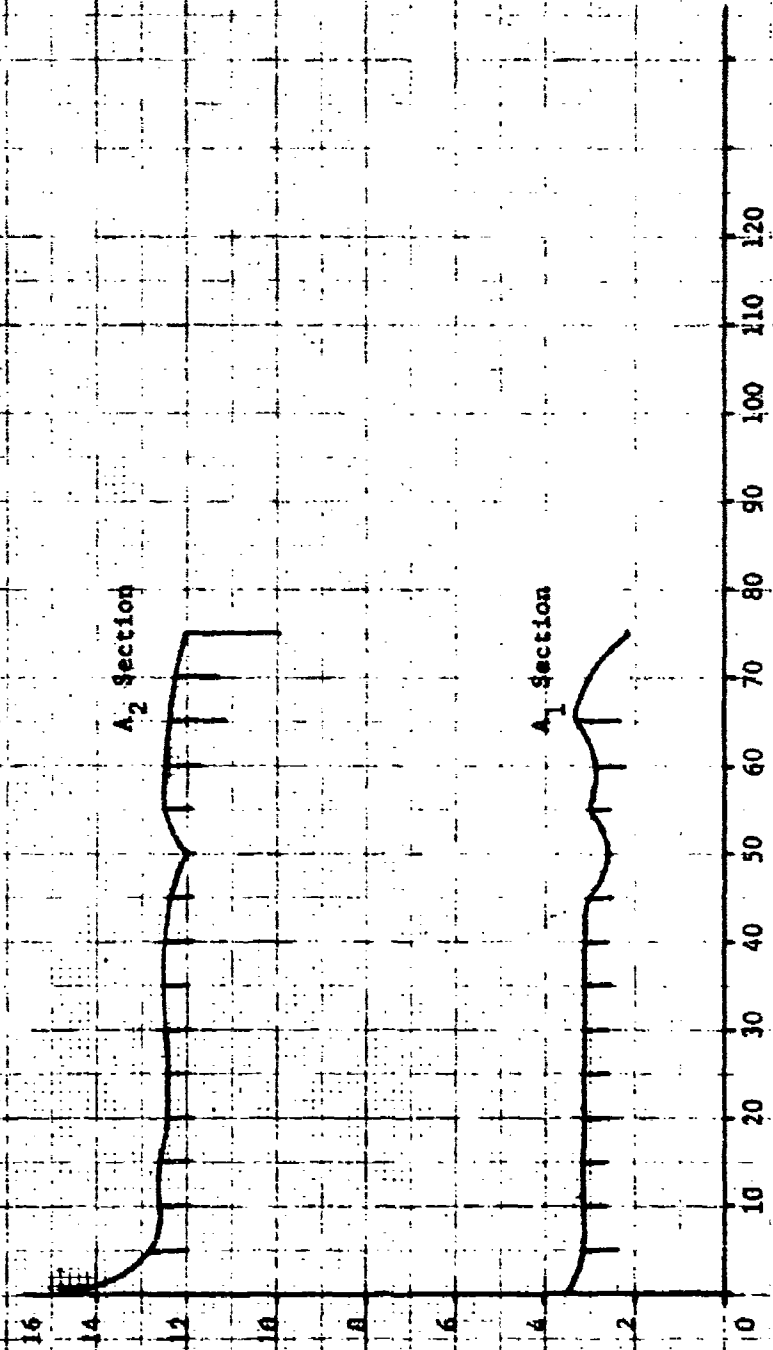
5 hr. interval. Actual loading was 4 2 min.

Load 1 10 min. Load 2 cycle.

Specimen No. 13, S/N 22

Date: June 13, 1972

Battery Output - VDC



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Discharge at 75V after 100 hr stand at 100V
Note: For clarity, Load 1 surges are shown at
5 hr. intervals. Actual loading was a
2 min. Load 1, 18 min Load 2 cycle

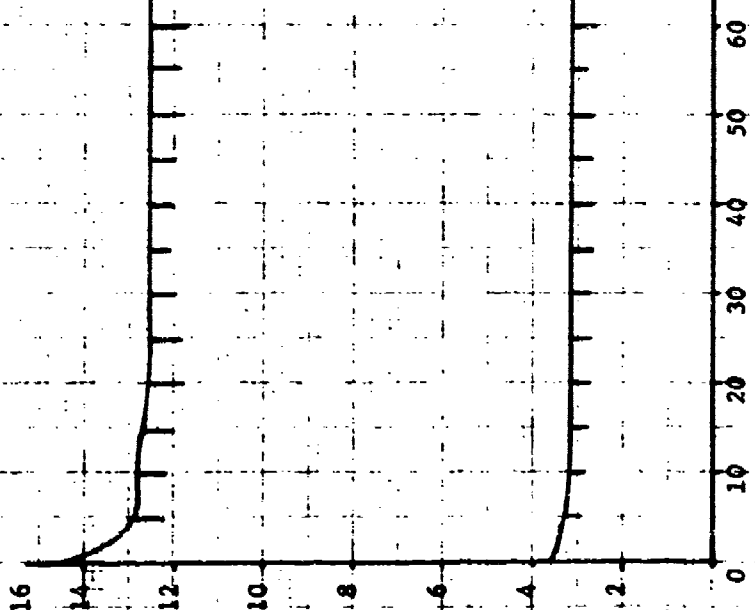
Specimen No. 14, D/N 47
Date: October 16, 1972

Battery Output - VDC

A₂ Section

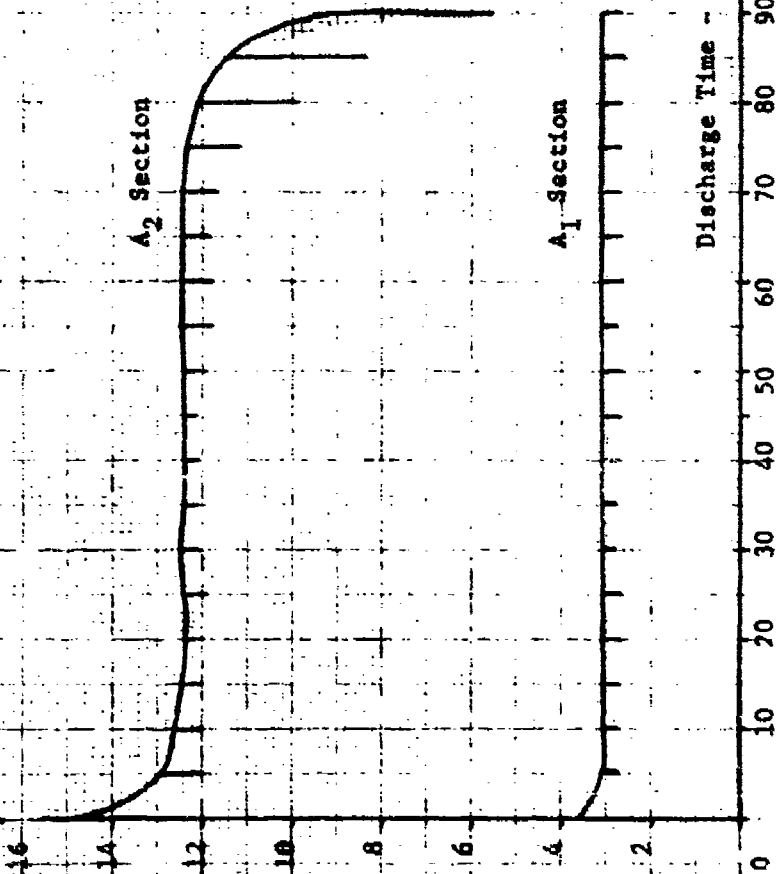
A₁ Section

Discharge Time - Hours



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 75°F. after Vibration and Shock
Note: For clarity, Load 1 surges are shown at 15 hr.
intervals, Actual loading was 2 1/2 min. Load 1
18 min. Load 2.
Specimen No. 15, S/N 74
Date: February 26, 1973

Battery Output - VDC



Battery EP P/N MAP 4435

Recharge Voltage vs. Time

Immediate Discharge at 75°F after Vibration and Shock

Note: For clarity, Load 1 surges are shown at 5 hr.

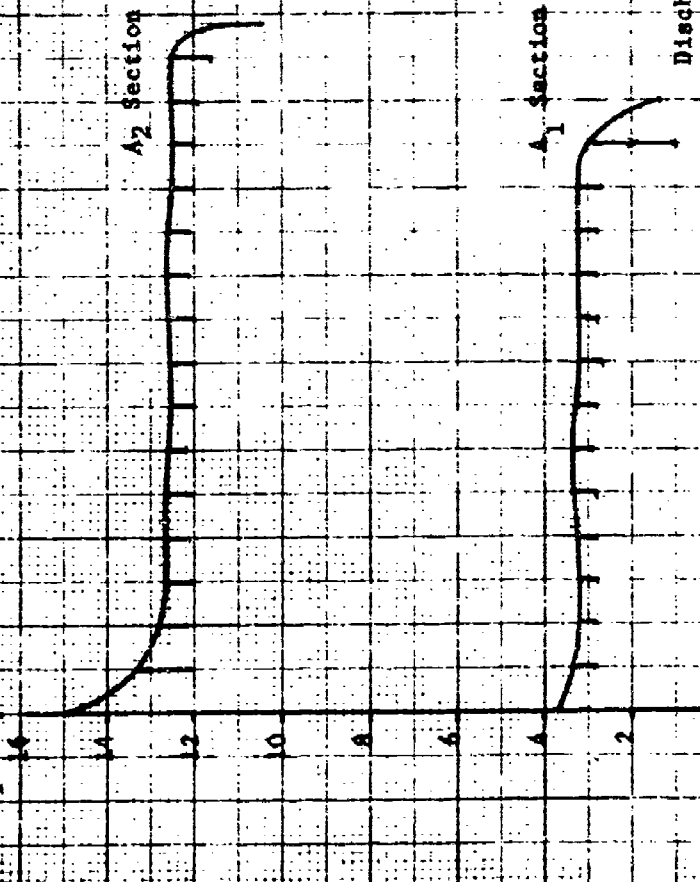
intervals. Actual loading was a 2-min. load at

18 min. Load 2 cycle.

Specimen No. 16, S/N 24

Date: October 17, 1952

Battery Output - VDC



Discharge Time - Hours

Battery EP/F/N MAP 443b

Discharge Voltage vs. Time

Immediate Discharge during Mechanical Shock

Note: For clarity, Load 1 surges are shown at

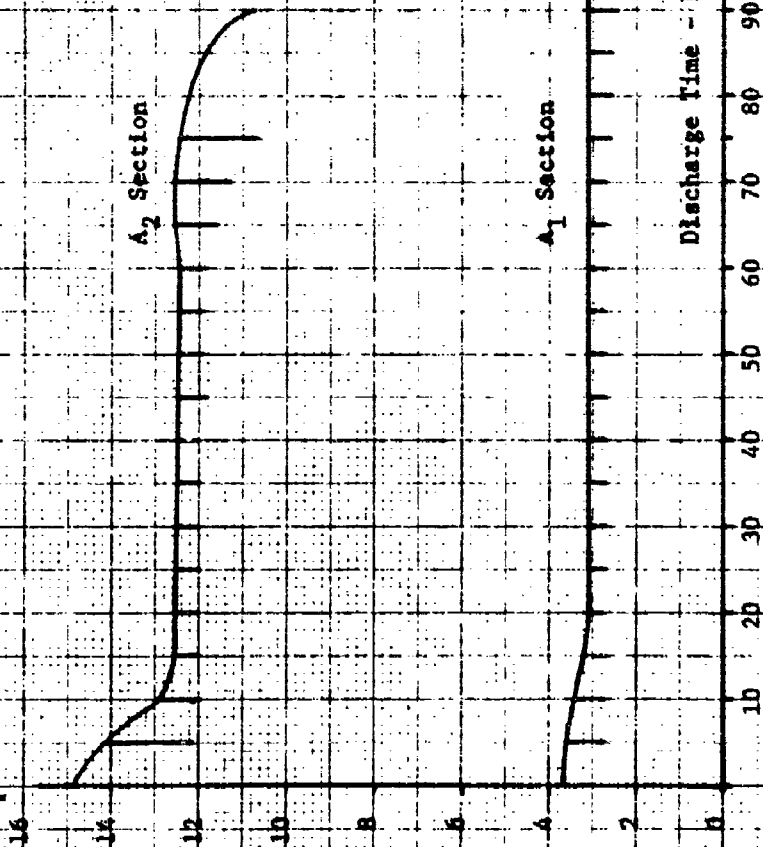
5 hr intervals. Actual loading was

2 min. Load 1, 10 min. Load 2 cycle.

Specimen No. 18, S/N 7

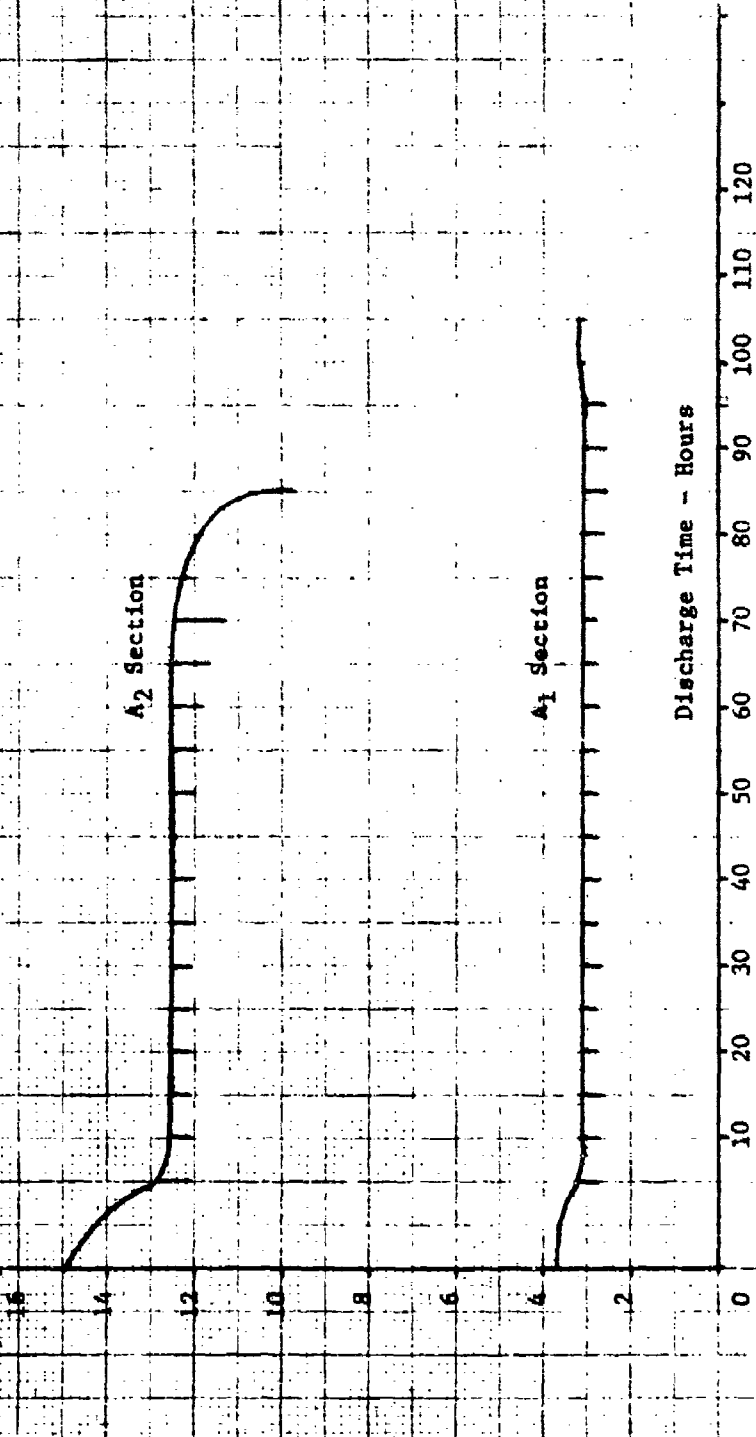
Date: June-19, 1972

Battery Output - VDC



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge during Vibration
Note: For clarity, Load 1 surges are shown at
5 hr. intervals. Actual loading was a
2 min. Load-1, 18 min. Load 2 cycle.
Specimen No. 19, S/N 8
Date: June 19, 1972

Battery Output - VDC



Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge during Vibration
Note: For clarity, Load 1 surges are
shown at 5 min. intervals. Actual
loading was a 2 min. Load 1, 18
min. Load 2 cycle.
Specimen No. 20; S/N 34
Date: June 19, 1972

Battery Output - VDC

16

14

12

10

8

6

4

2

0

A2 Section

A1 Section

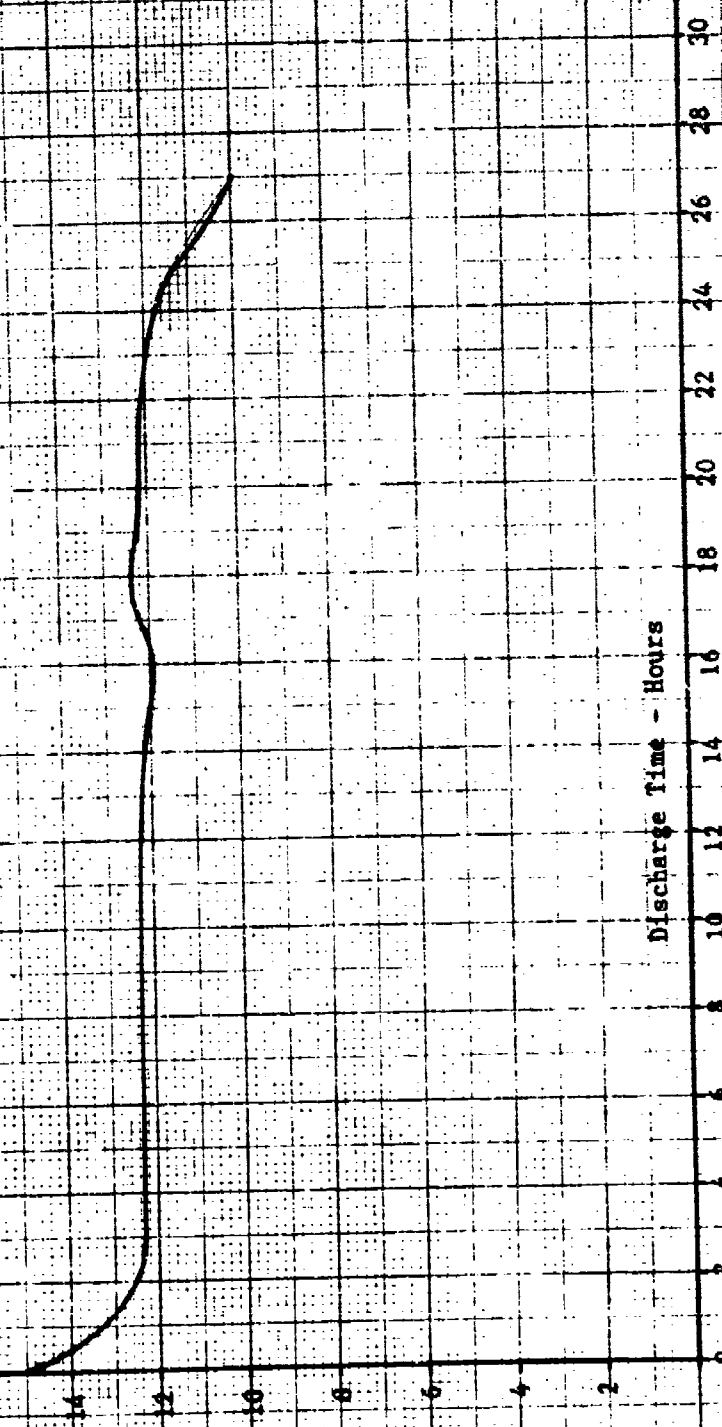
Discharge Time - Hours

10 20 30 40 50 60 70 80 90 100 110 120

ESEI 3A FORM 21 OF GEX 01
1 1/2 IN DIA
ON ORDER & JETTED
K&E

Battery EP P/N MAP 4435
Discharge Voltage Vd: 7.1mV
Immediate Discharge at 75mV
Specimen No. 21, IS/N 9
Date: June 5, 1972

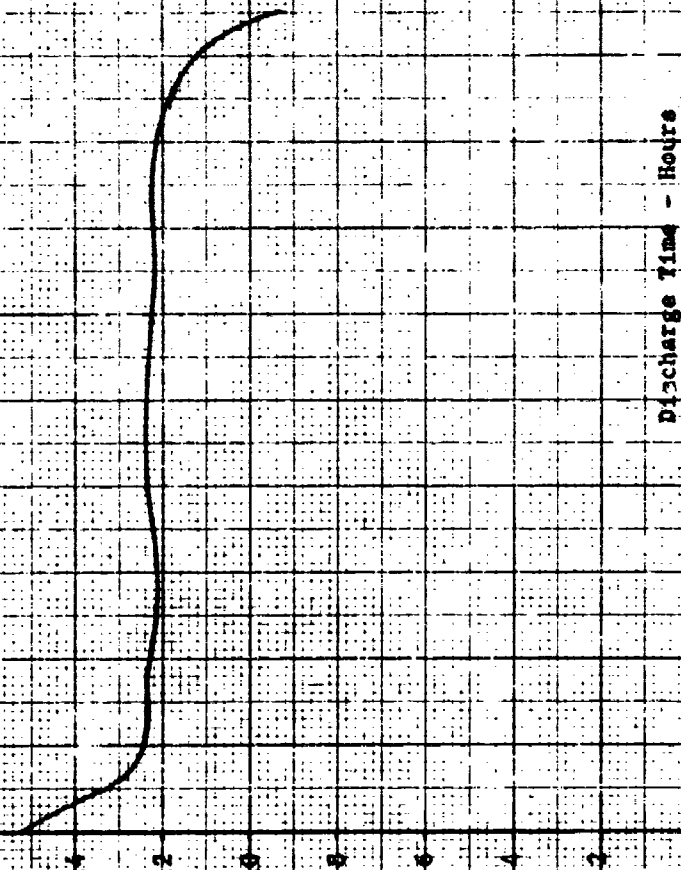
Battery Output - mV



Discharge Time - Hours

Battery HP P/N MAP 4433
Discharge Voltage vs. Time
Immediate Discharge at 75°F
Specimen No. 22, S/A 18
Date June 5, 1972

Battery Output - VDC



Discharge Time - Hours

Battery EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 125°F
Specimen No. 24, S/N 59
Date: June 7, 1972

Battery Output - VDC

16
12
8
4
0

Discharge Time - Hours

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30

K&E

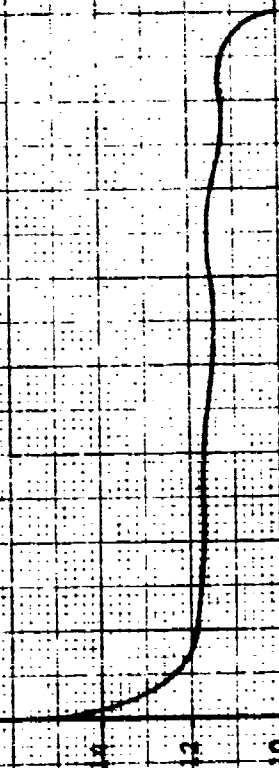
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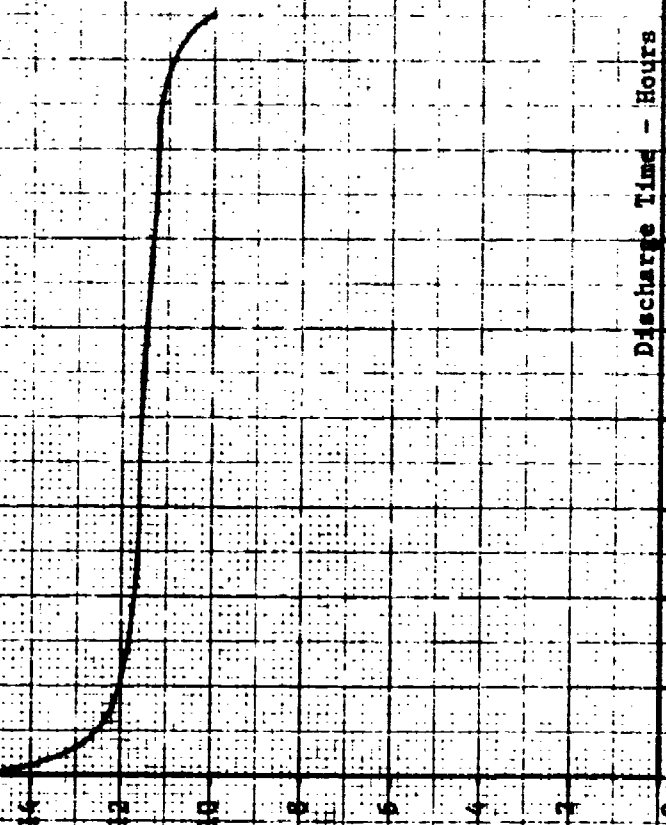
Battery 2F 7/N MAF 4454
Discharge Voltage vs. Time
Immediate Discharge at 0°F
Specimen No. 25, 87N 71
Date: March 8, 1973

AGENCY QUOTE - YDC



BATTERY EP P/N MAP 4435
Discharge Voltage vs. Time
Immediate Discharge at 0°F
Specimen No. 26, S/N 31
Date: June 14, 1972

Battery Output 1998



Battery EP P/N MAP 4435

Discharge Voltage vs. Time

Discharge at 75% after 7 day stand at 70°F

Specimen No. 29, S/W 05

Date: June 14, 1972

Battery Voltage - VDC

1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0

Discharge time - Hours

0

2

4

6

8

10

12

14

16

18

20

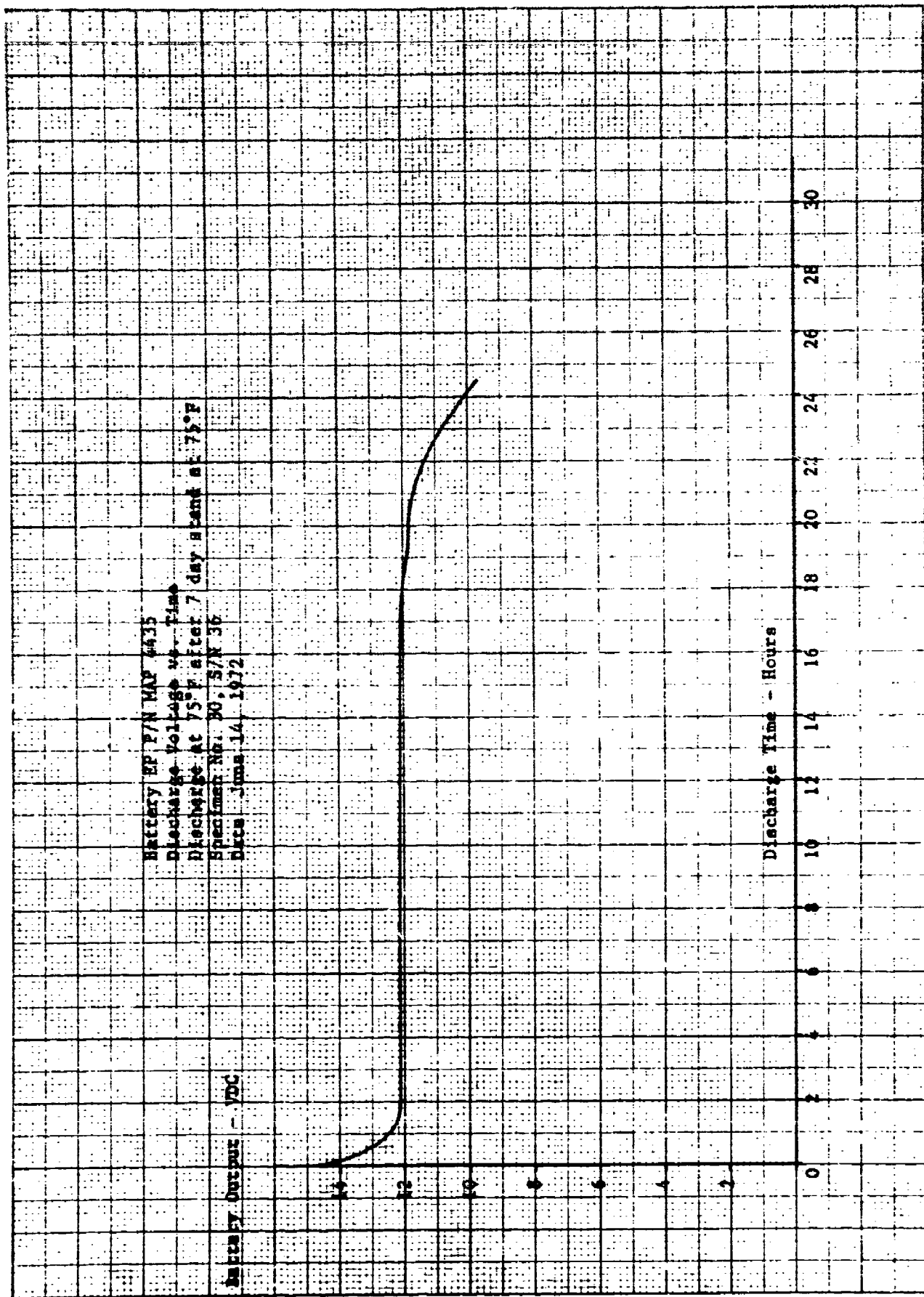
22

24

26

28

30



BATTERY EP P/N MAP 4435
Discharge Voltage vs. Time
Discharge at 75°F after 7 day stand at 75°F
Specimen No. 30, S/N 36
Date June 14, 1972

Energy Output - YOC

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13. ABSTRACT This report describes the design, development, manufacture and evaluation testing of a Zinc-Silver Oxide reserve battery in accordance with "Technical Guidelines for Water Activated Zinc-Silver Oxide Battery". This includes a description of the design effort, the design, the test program, the test equipment and the test results. The evaluation testing showed compliance with the requirements of the technical guidelines.			

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