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AFATL-TR-72-184

FEB 28 1973

MAR 27 1973

AUG 17 1973

VALIDATION AND EXPANSION
OF THE
FLOW ANGULARITY TECHNIQUE
FOR

PREDICTING STORE SEPARATION TRAJECTORIES

AIRCRAFT COMPATIBILITY AND WEAPONS FLIGHT DYNAMICS
BRANCH
PRODUCT ASSURANCE DIVISION

TECHNICAL REPORT AFATL-TR-72-184

SEPTEMBER 1972

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**Validation and Expansion
of the
Flow Angularity Technique
for
Predicting Store Separation Trajectories**

Stephen C. Korn, Captain, USAF

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FOREWORD

This report is based on a study performed at the Air Force Armament Laboratory from April through August 1972 as part of Project 2567, Task 02, Work Unit 014.

This technical report has been reviewed and is approved.


RANDALL L. FETTY, Colonel, USAF
Chief, Product Assurance Division

ABSTRACT

This report documents the external flow fields caused by various weapon configurations on the wing of an F-4 aircraft, verifies assumptions made in the flow angularity technique, and presents the documentation for the "Flow Angularity Computer Program" with example trajectories. The flow angularity program is presently capable of calculating the trajectories of stores off the inboard and outboard wing stations in either single, triple ejector rack, or multiple ejector rack configurations. The assumptions made in the flow angularity technique have been analyzed and generally validated as good approximations.

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LIST OF SYMBOLS AND ABBREVIATIONS

c.g.	Center of gravity
FS; BL, WL	Fuselage station, butt line, and water line of F-4C aircraft (feet)
MFS, MGL, MWL	Model fuselage station, butt line, and water line of F-4C 5% model aircraft (inches)
ν	Upwash angle (degrees)
α_p	Angle of attack of aircraft (degrees)

SECTION I

INTRODUCTION

The flow angularity technique for predicting store separation trajectories was originally documented in Reference (1), and this report is a follow-on to substantiate some of the assumptions made in that original report and to present the text of the "Flow Angularity Computer Program" (See Appendixes I to IV). The original "Flow Angularity Computer Program" was designed around the flow field of three M-117 bombs on a triple ejector rack (TER). In order to simulate the launches of stores from the different positions on the TER, certain scaling parameters were used to adjust the flow field. Since the publication of the original report, an additional wind tunnel test was conducted in which the flow field was surveyed for single ejector rack, TER, and a multiple ejector rack (MER) configurations. These additional flow fields enabled the evaluation of many of the scale factors used in the original program. The flow angularity program has been revised so it would accept data from these new flow fields.

The flow angularity program is presently being utilized at the Air Force Armament Laboratory for predicting trajectories of stores that have had new modifications, and stores that are new in design. The flow angularity program is also being used by the 6511 Test Group (TGEA) at El Centro, California, to determine safe launch conditions for their test vehicles.

SECTION II

DISCUSSION OF FLOW FIELD SURVEY TEST

A second flow field survey test (similar to that described in Reference 2) was conducted at Arnold Engineering and Development Center in March 1972. The test was conducted in order to measure the velocity vector components in the flow field beneath the wing of the F-4C aircraft at Mach number 0.85 and is documented in Reference 3. A conical-tip pressure probe was used to measure the velocity vectors beneath the wing with configuration combinations of pylons, ejector racks, (TER and MER) and stores (M-117, MK-81, and MK-84 bombs). The F-4 model and area surveyed are displayed in Figures 1 and 2.

As discussed in Reference (1), the flow angularity semi-empirical approach would only be cost effective if a flow field taken under one set of conditions could be used to predict trajectories of stores under many other launch conditions. Reference (1) built a rationale for using the flow field of three M-117 bombs for predicting trajectories for one, two, or three stores of any type on the TER at time of launch.

To test this theory, trajectories were calculated for M-117 bombs, SUU-51 bombs, and a tactical fighter attack flare. These trajectories were then compared with wind tunnel trajectories under the same conditions. It was found that all the trajectories had good trends and that the flow angularity method would be a useful tool in predicting store separation trajectories.

This second flow field test conducted in March 1972 had as objectives: to validate some assumptions made in the first report, to collect flow field data on the MER configurations on the outboard wing station, and to collect flow field data on large diameter stores on the inboard and outboard pylon stations. By validating the assumptions, very little additional flow field data would be needed for the F-4, F-15, and A-7 aircraft.

The first approximation that needed investigation was the use of the three bomb (TER) configuration flow field to predict the trajectories of stores from the shoulder stations of the TER. To investigate this approximation, the MK-81 and M-117 bombs were tested in configurations T3, T2, and T1 (See Figure 3). The velocity components measured during the test are given in Figures 4 to 24. The flow fields produced at the nose and tail of these bombs (for the TER configurations) are displayed in Figures 7(a), 7(b), 10(a), 10(b), 11(a), 11(b), 12(a), 12(b), 13(a), 13(b), 14(a), and 14(b). As can be seen, the flow pictures are similar for the three configurations, but some differences are present.

In order to investigate the effect that the differences in the flow field have on the trajectories, launches of the MK-81 from the T2 and T1

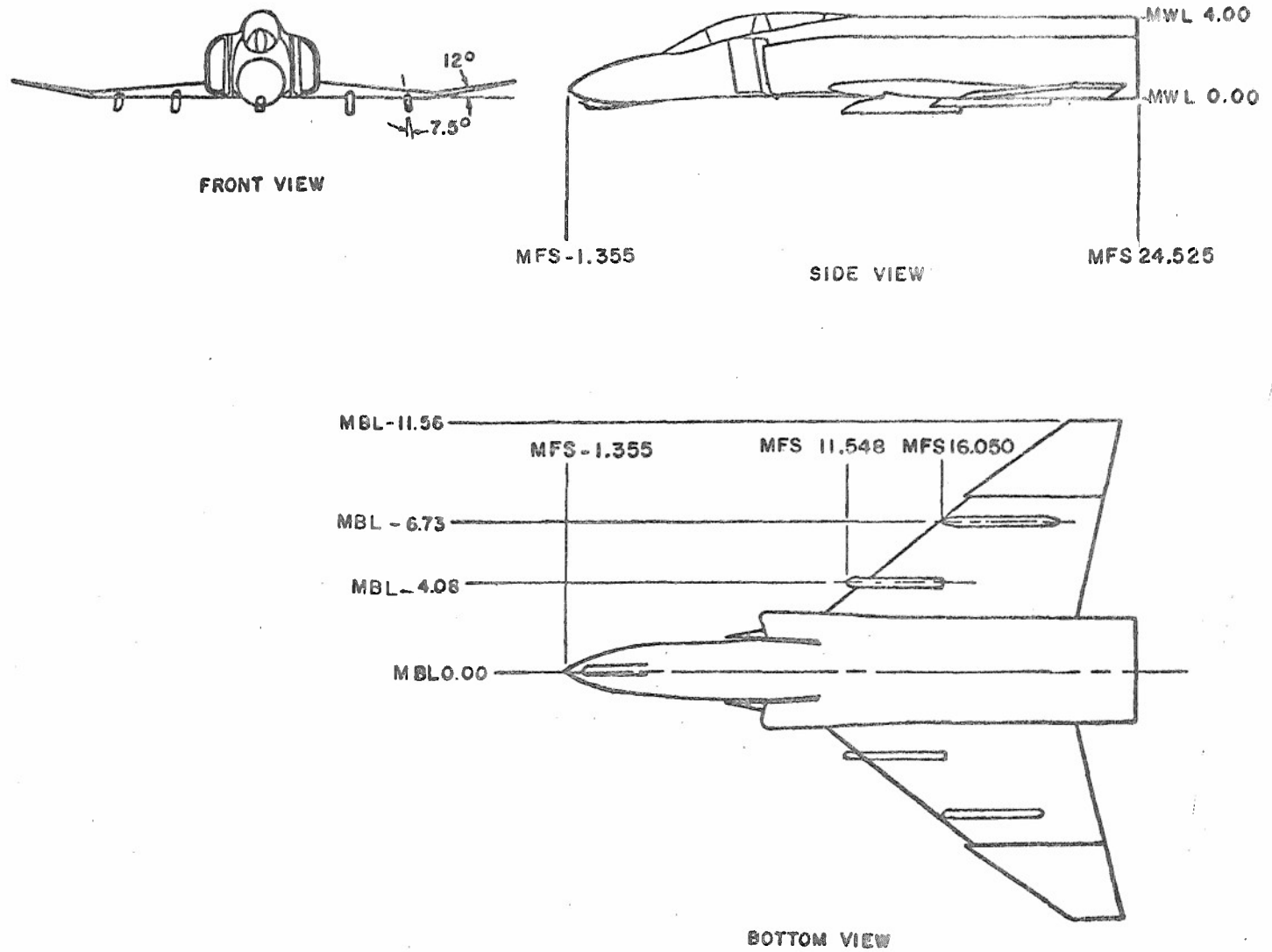
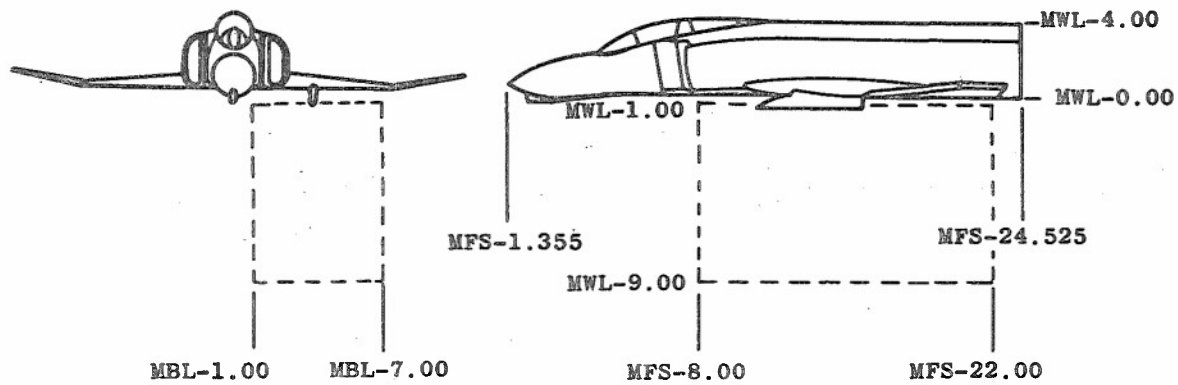
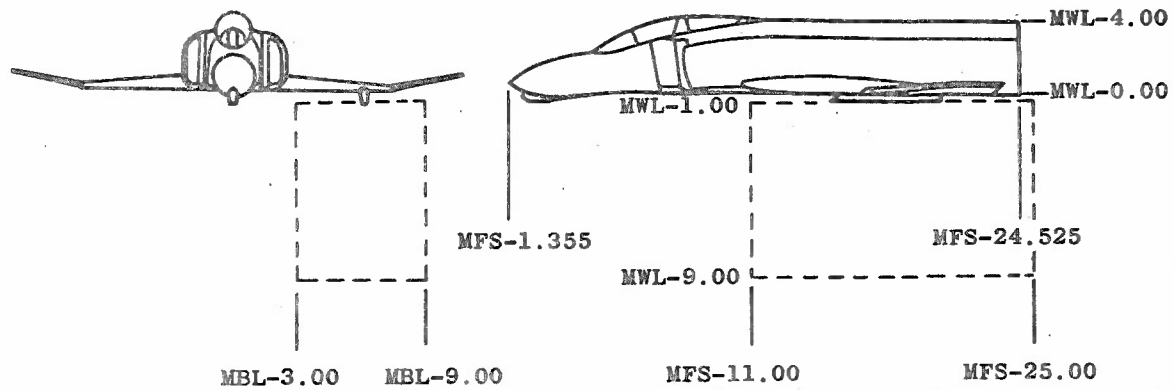


Figure 1. Sketch of the F-4C Parent-Aircraft Model Showing Pylon Locations



a. Region of Inboard Survey



b. Region of Outboard Survey

Figure 2. F-4C Parent Aircraft Showing Regions Surveyed

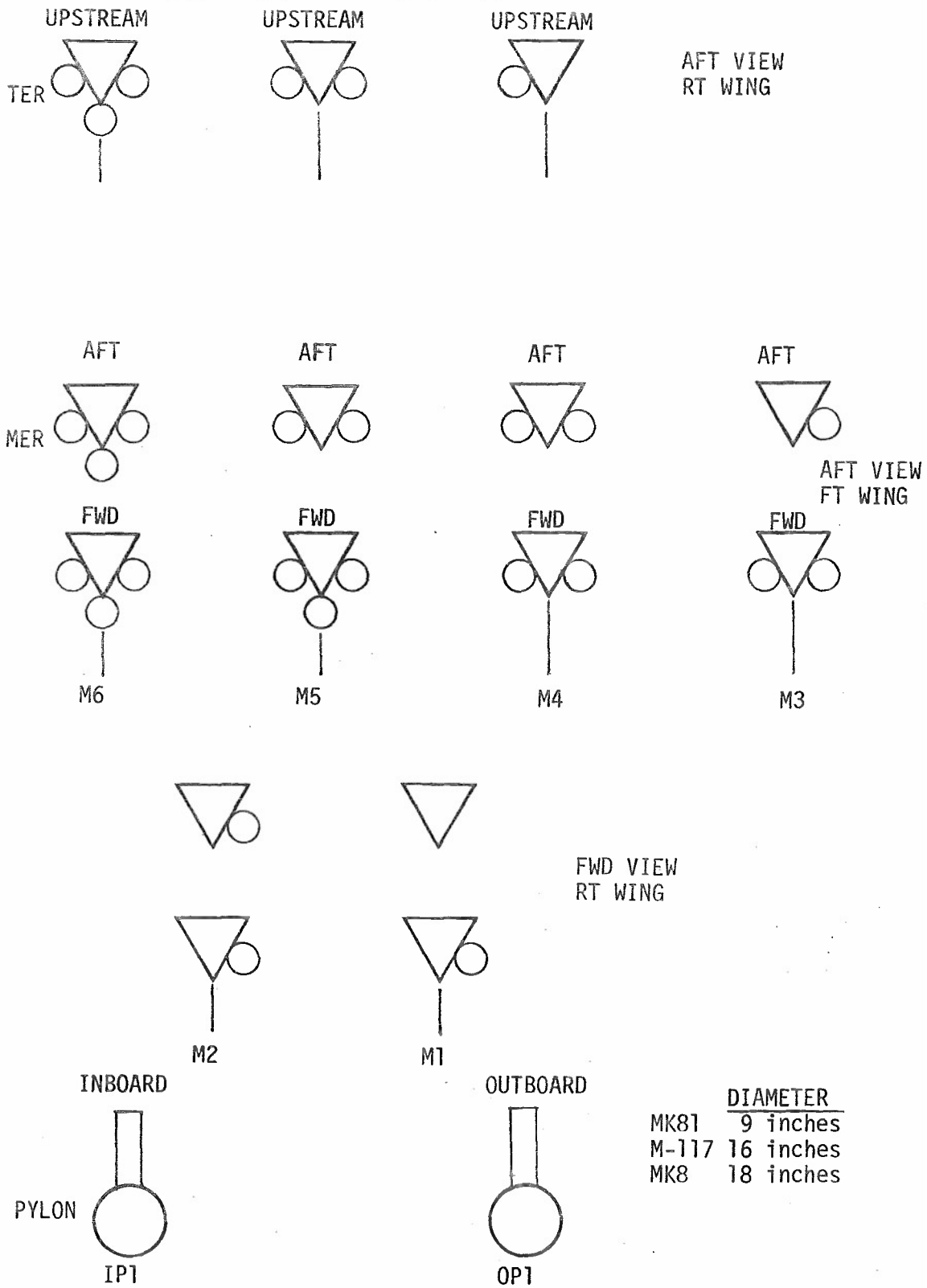
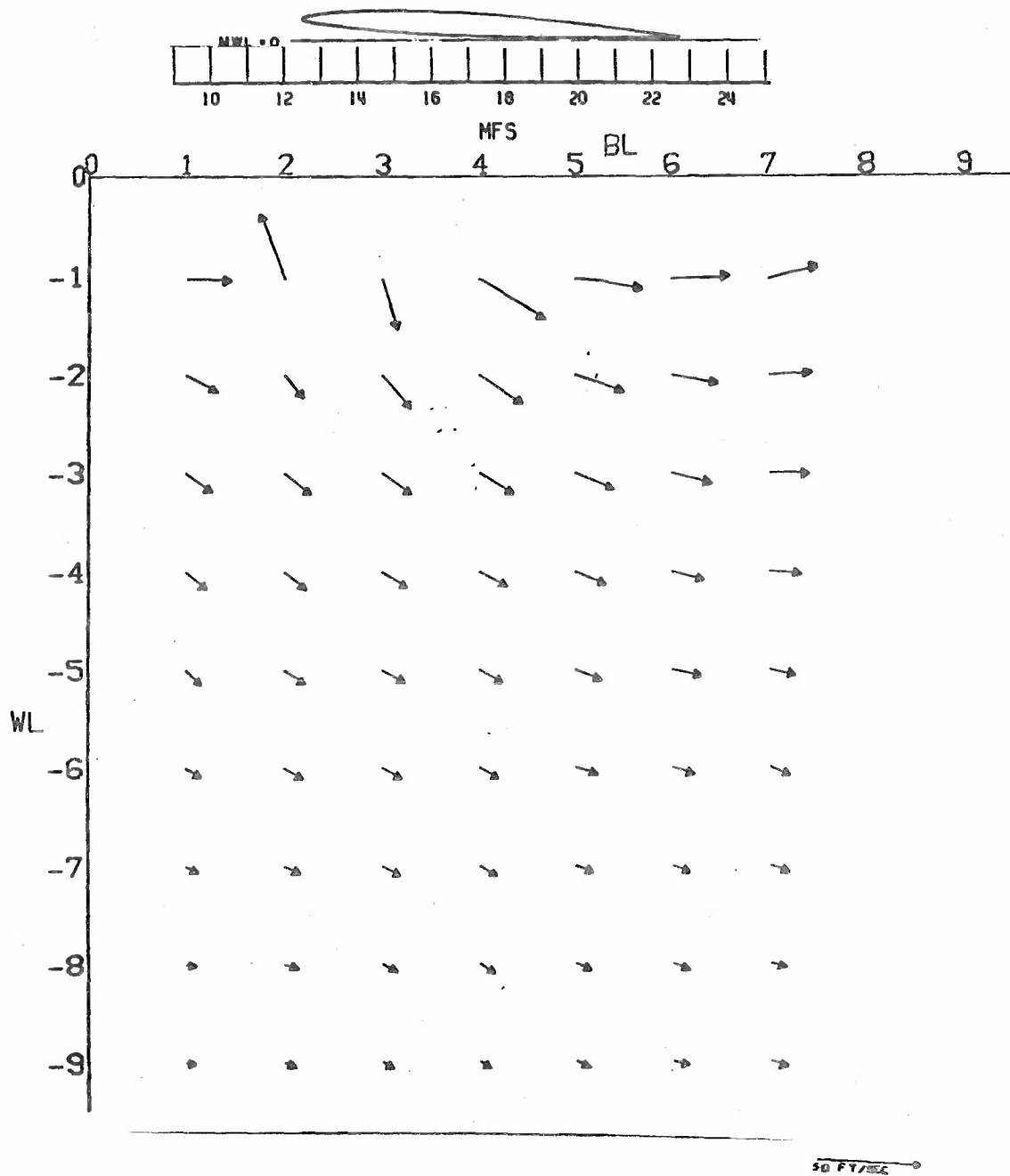
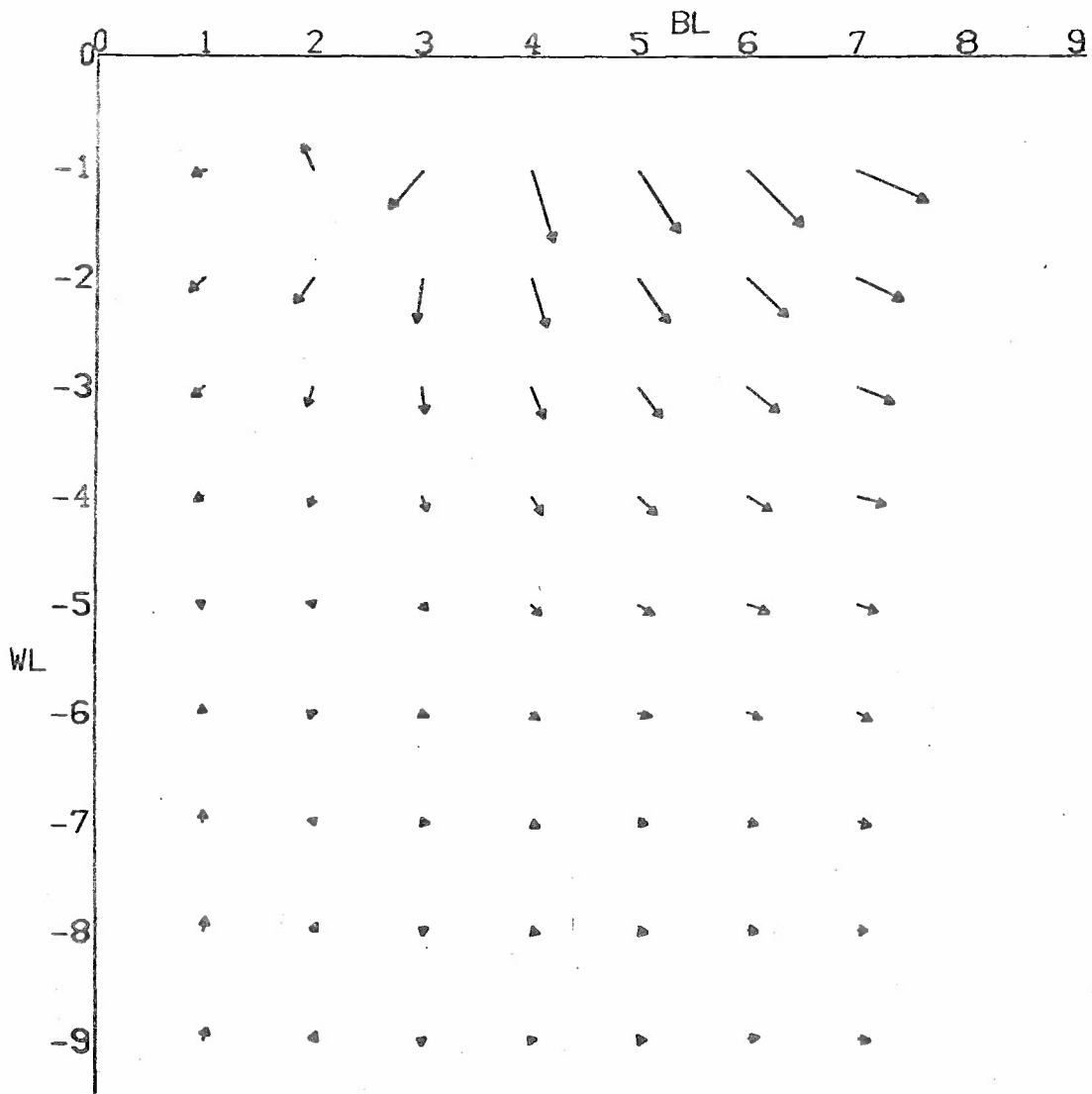


Figure 3. Configurations

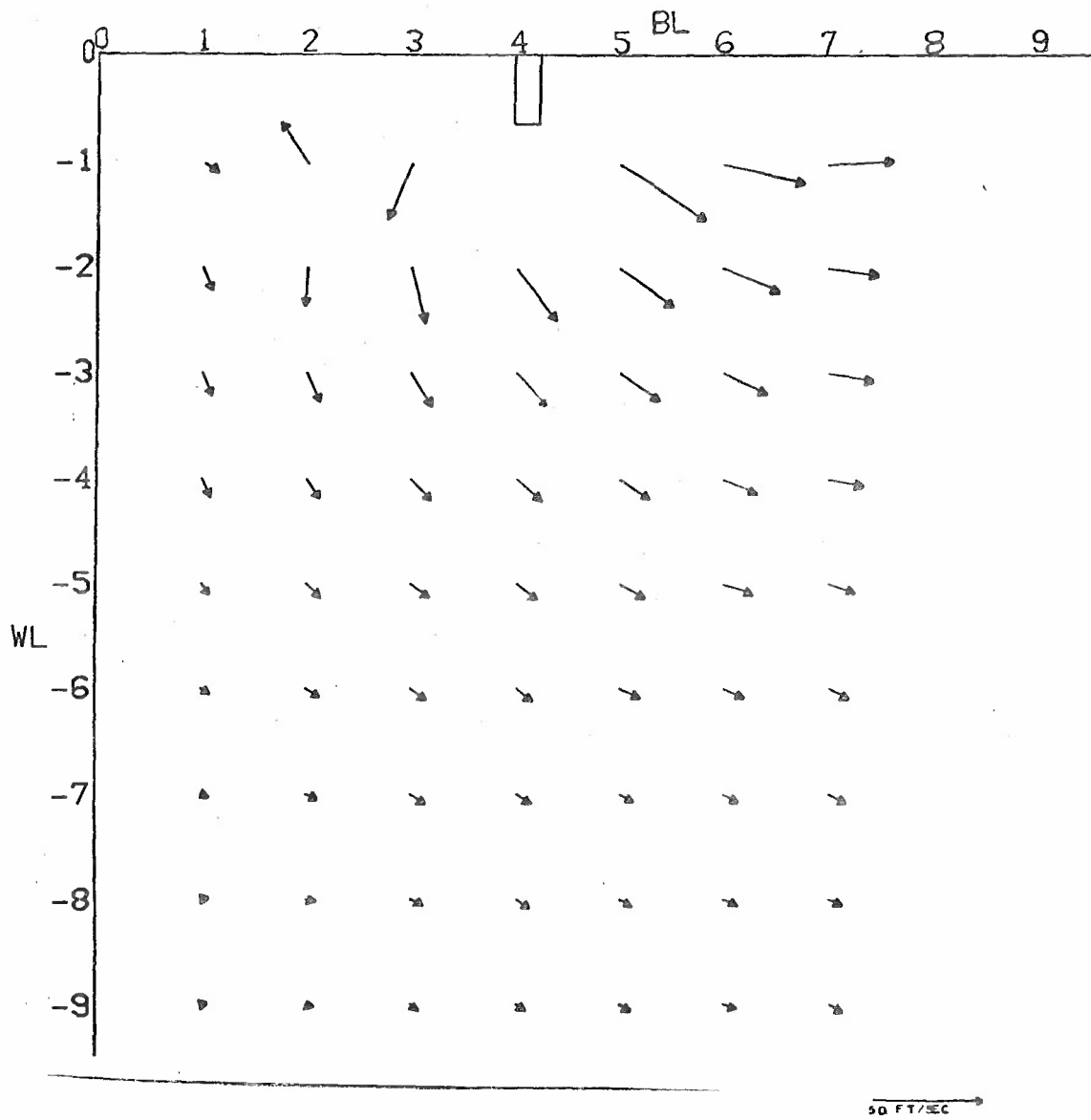
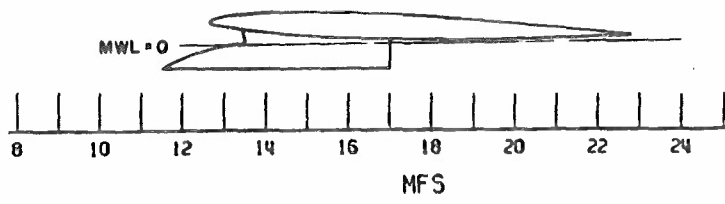


(a) $MFS = 12$

Figure 4. Effect of the Clean Wing on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

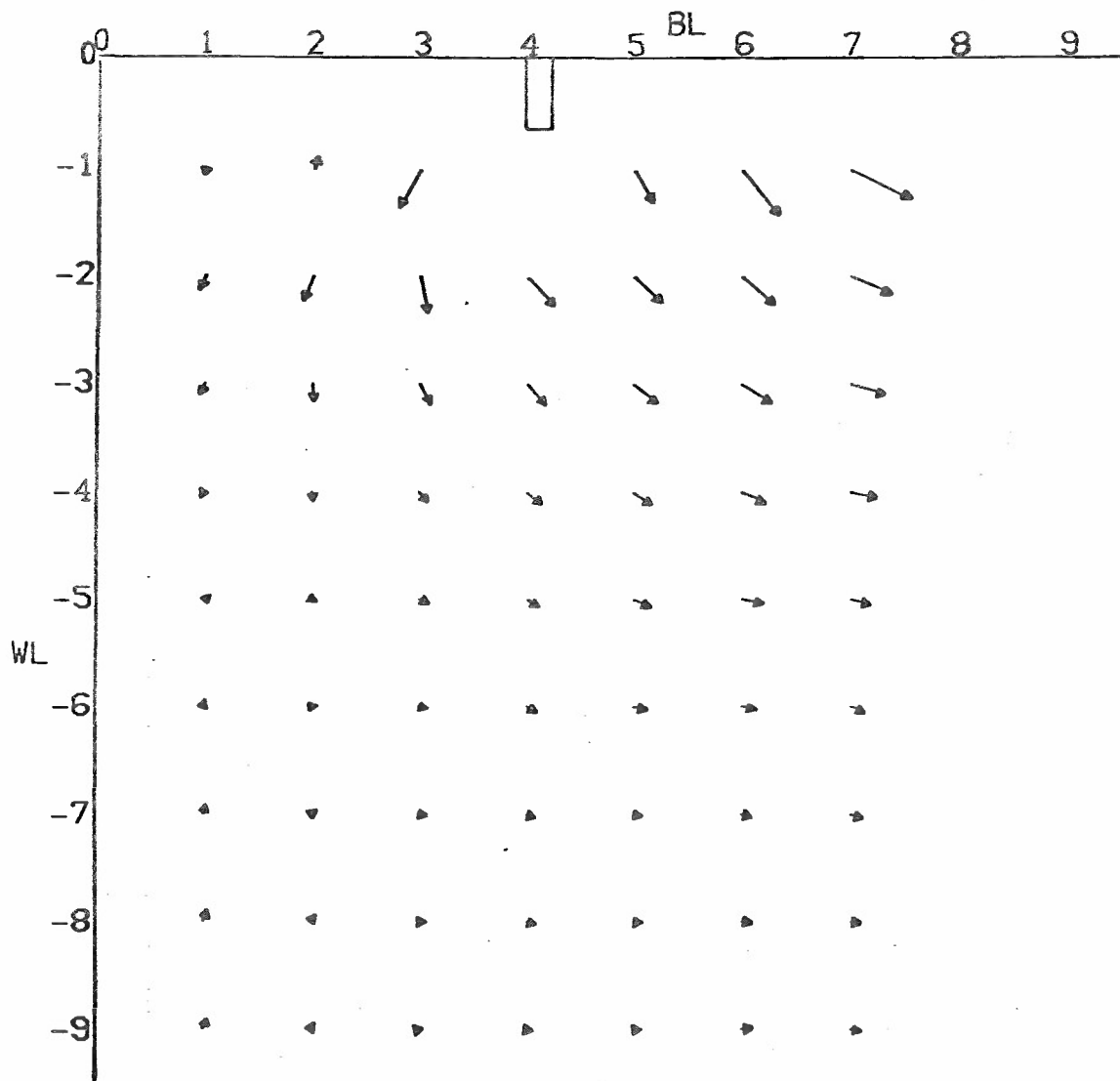


(b) MFS = 16
 Figure 4. Concluded



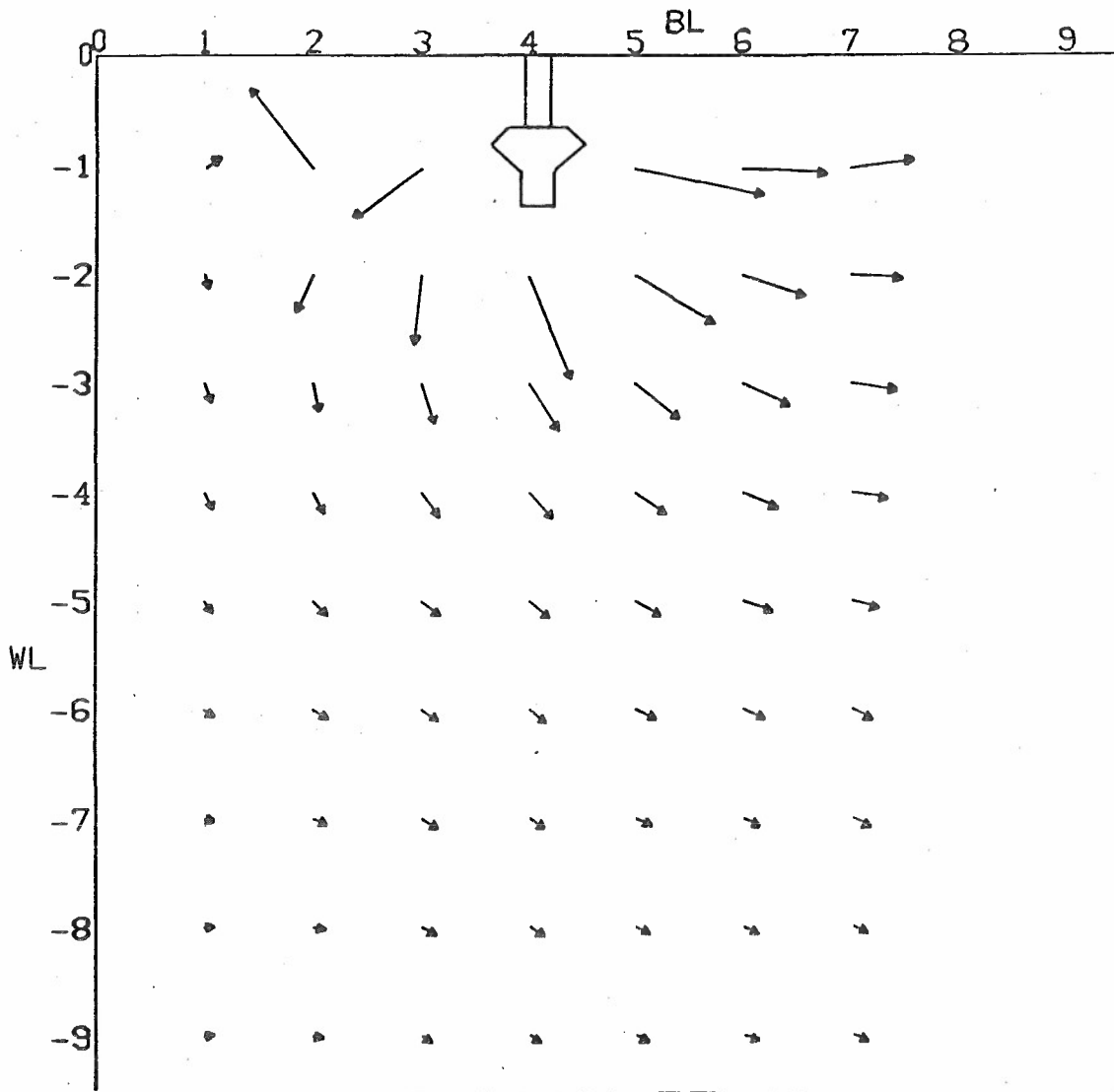
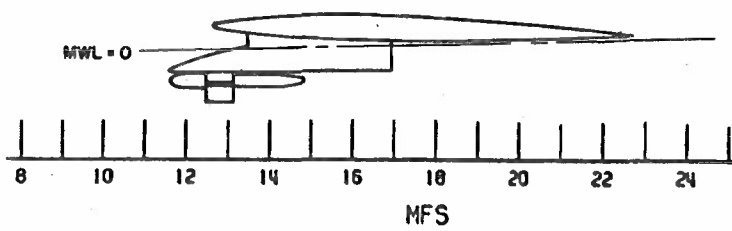
(a) MFS = 13

Figure 5. Effect of an Inboard Pylon on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



(b) MPS = 16

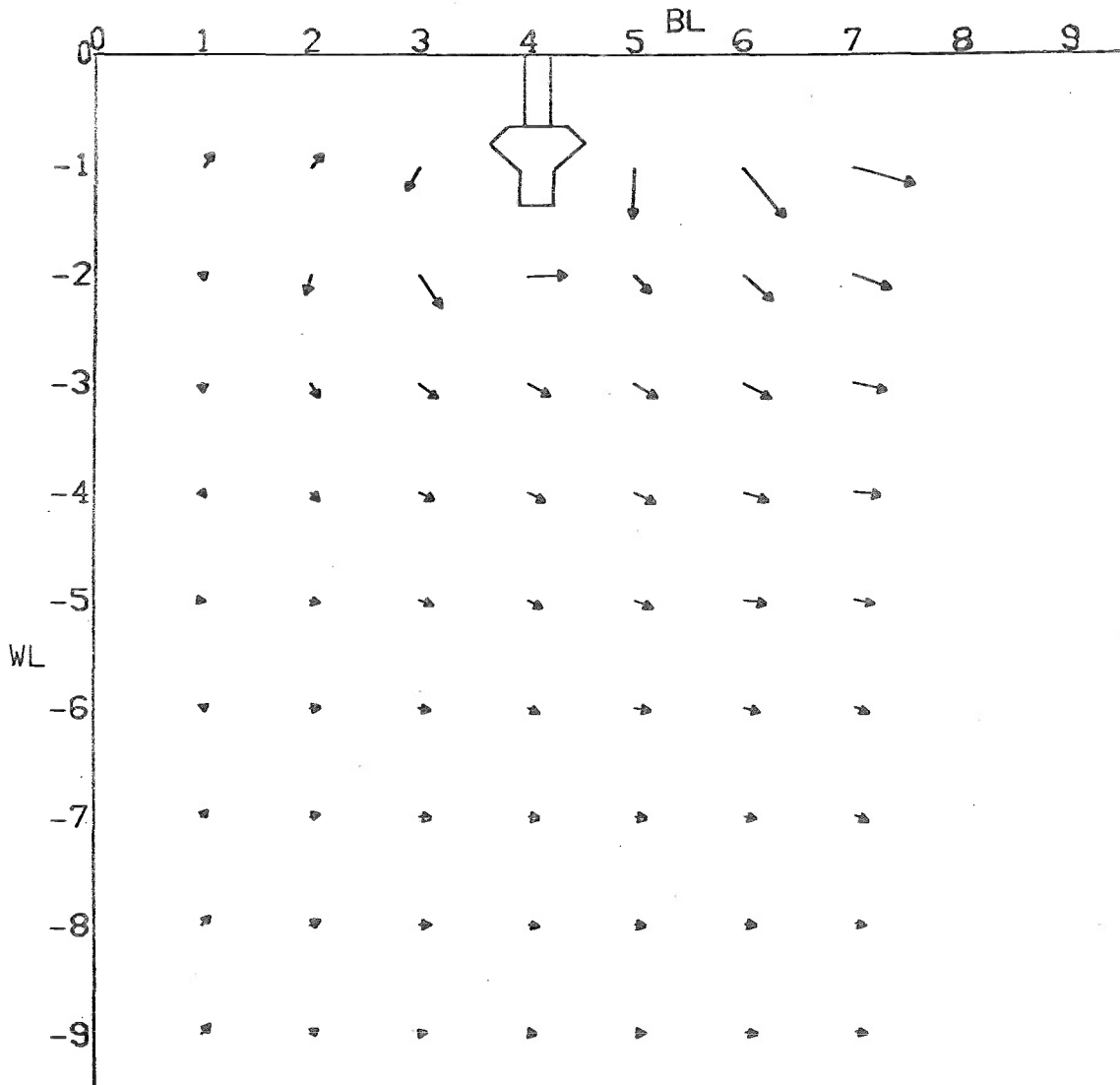
Figure 5. Concluded



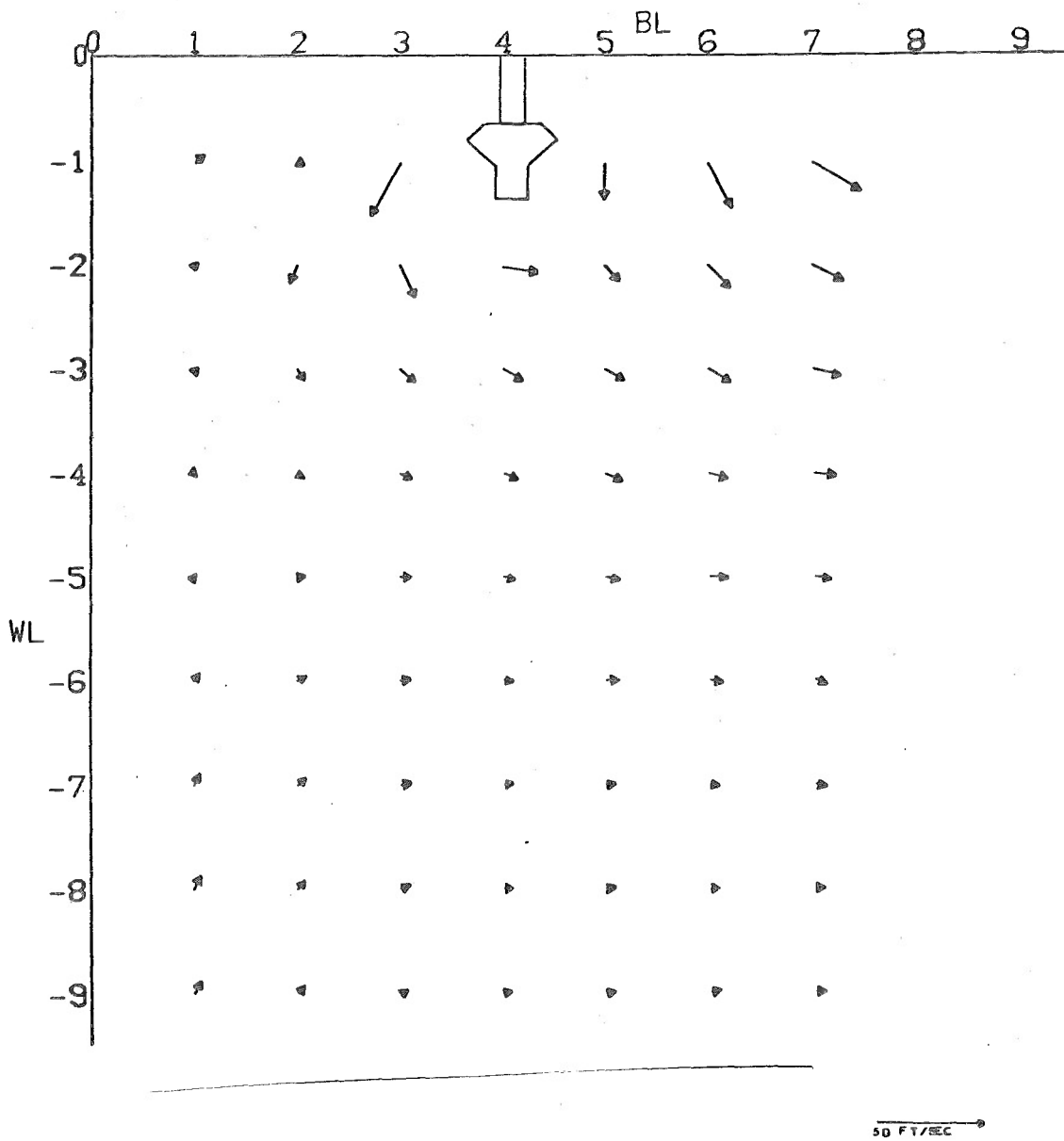
(a) MFS 12

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Figure 6. Effect of TER Rack on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

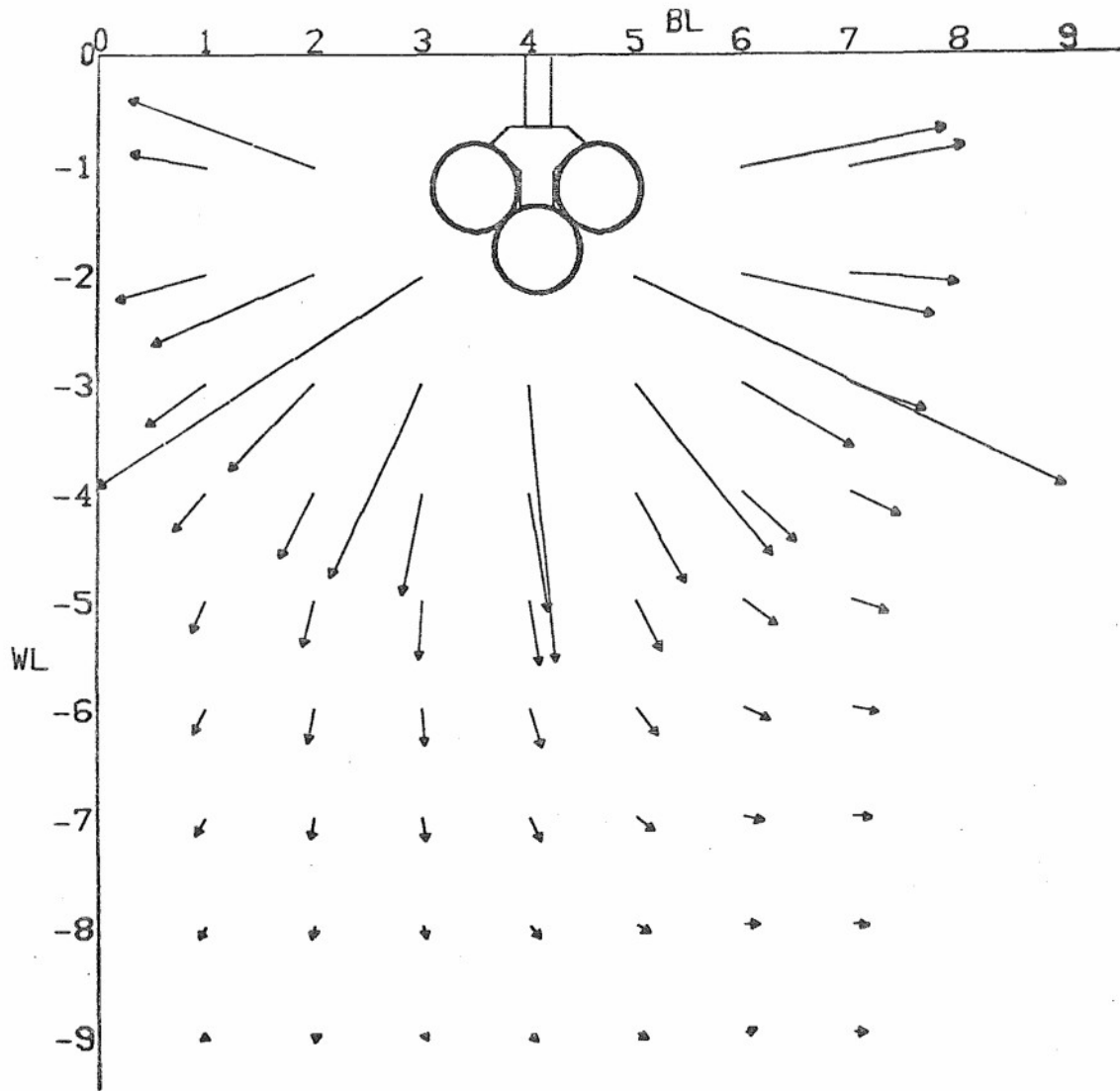
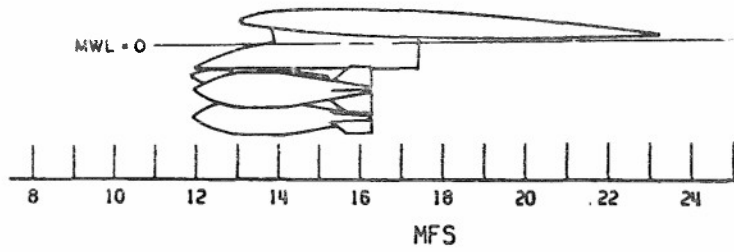


(b) MFS = 15
 Figure 6, Continued



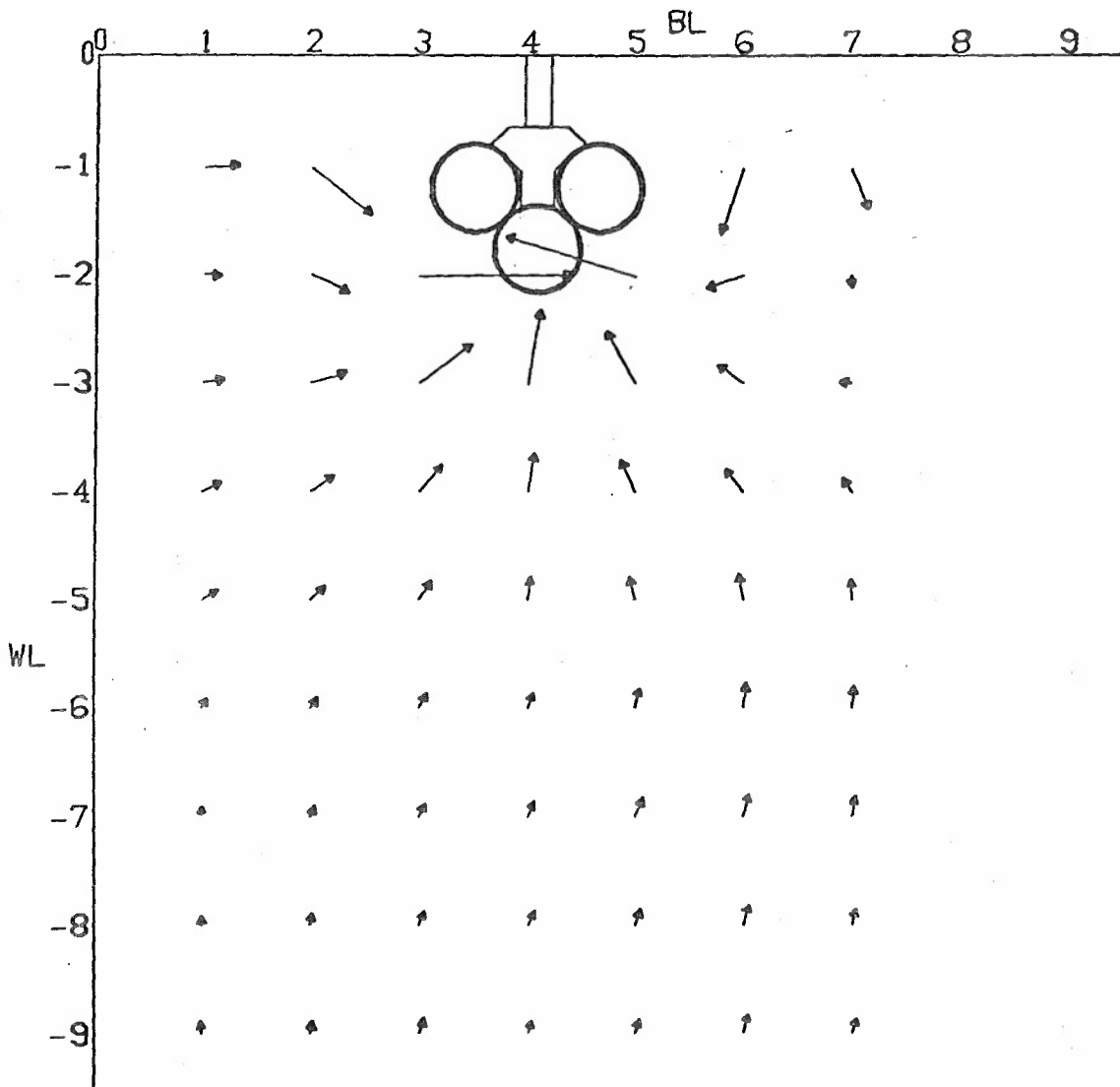
(c) $MFS = 16$

Figure 6, Concluded



(a) MFS = 12

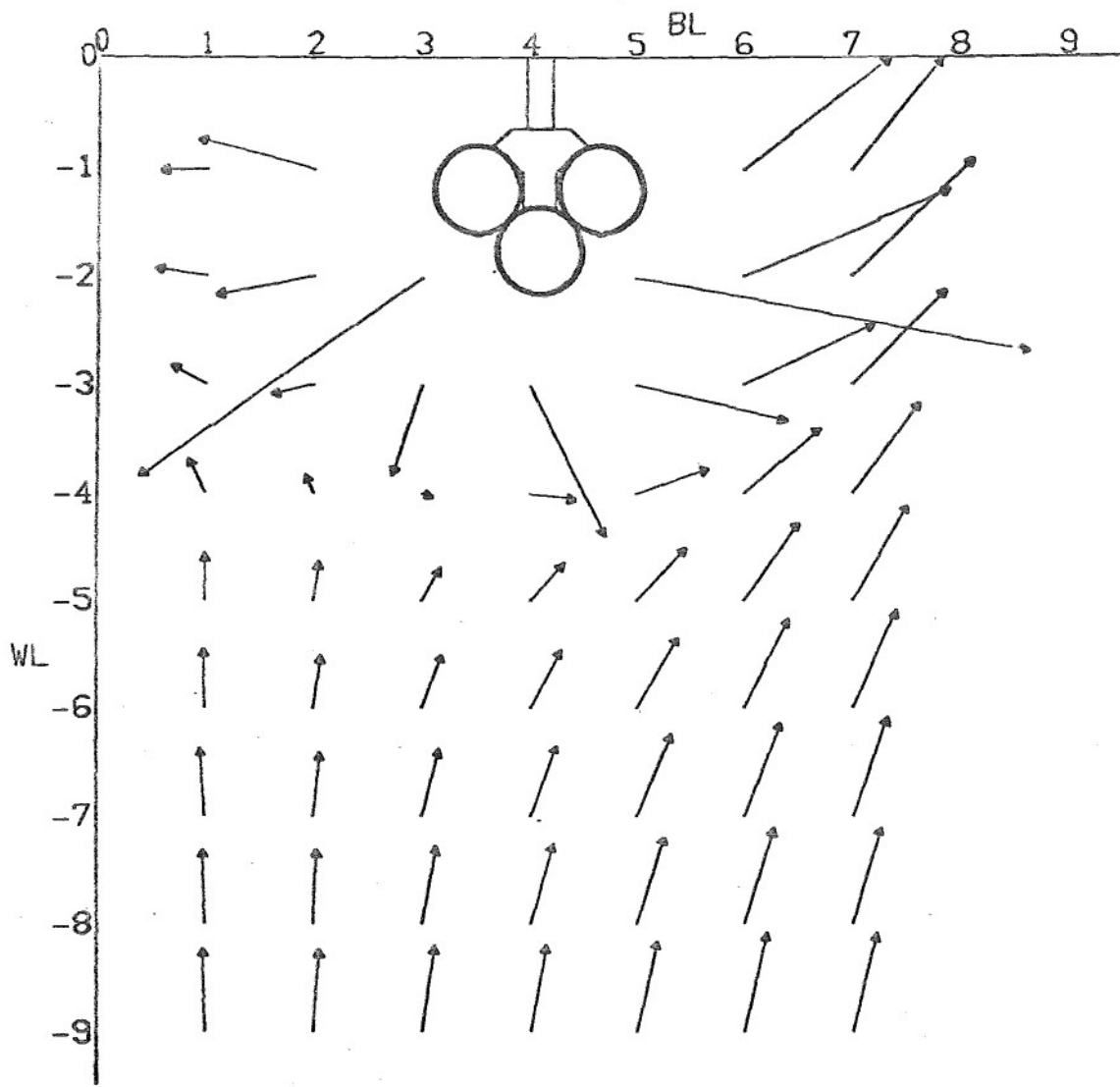
Figure 7. Effect of Three M-117 Bombs and TER on the Transverse Velocity Components of the Flow at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



50 FT/SEC

(b) $\alpha_p = 0.3$, $MFS = 16$

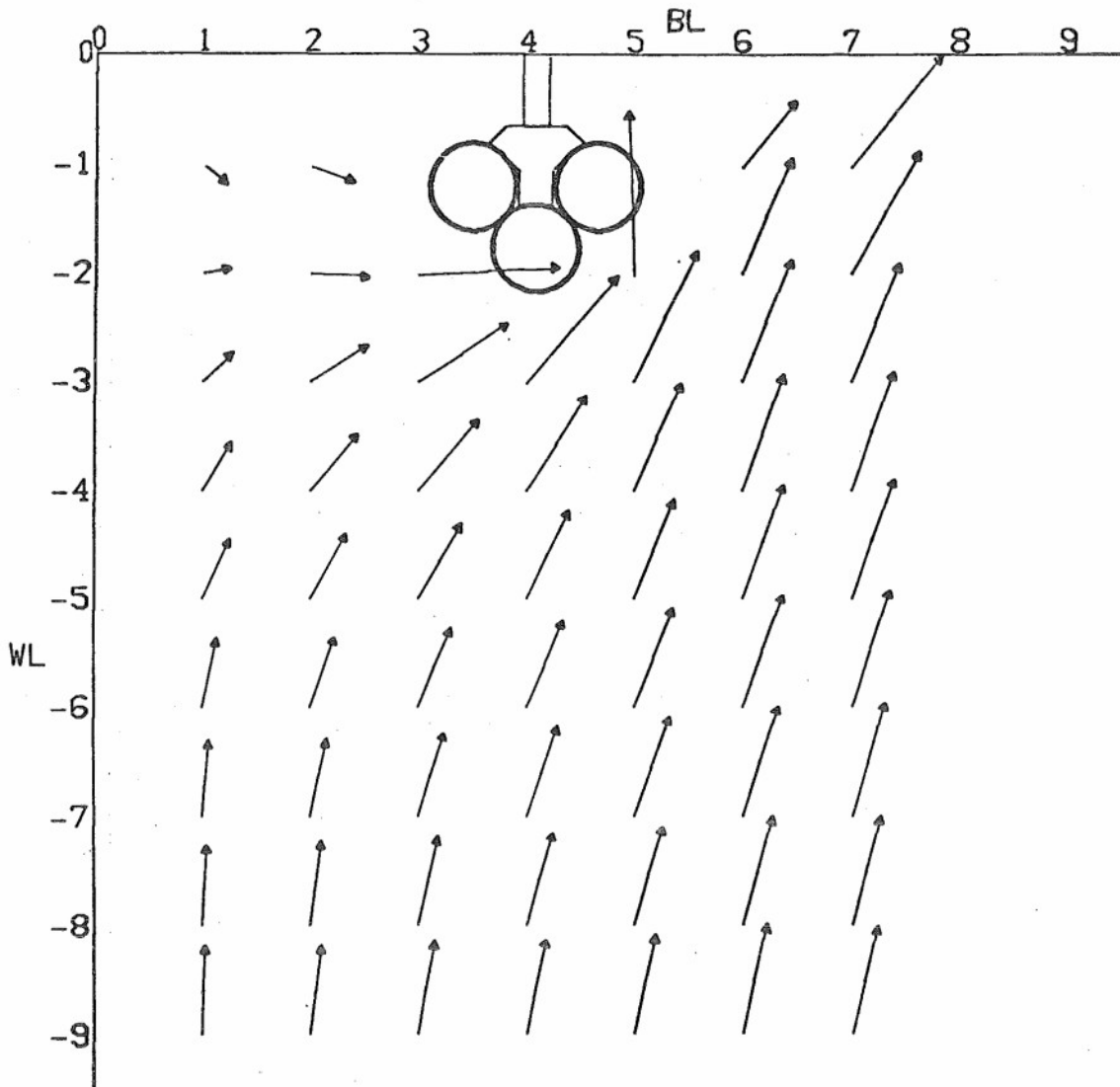
Figure 7, Continued



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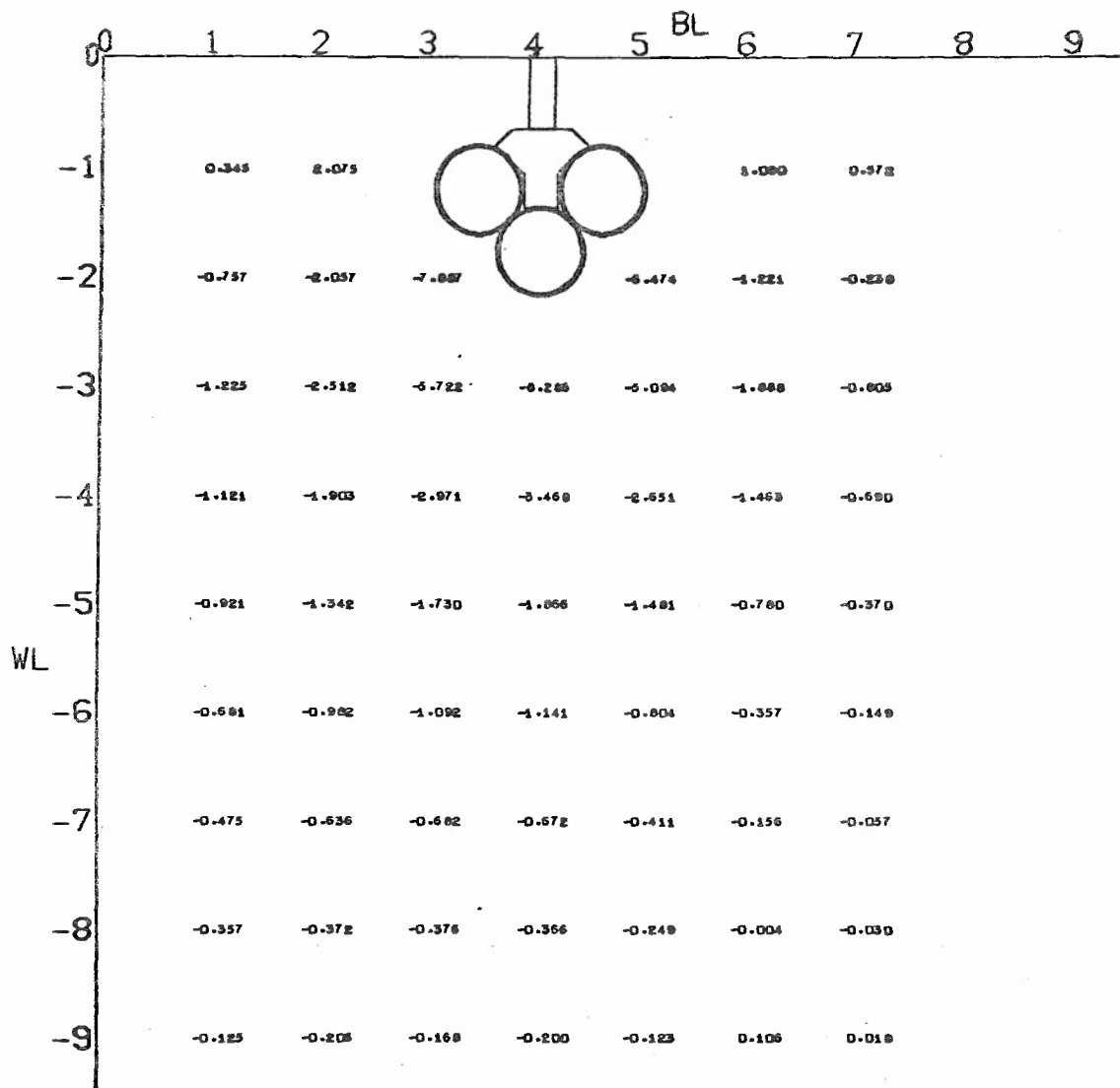
(c) $\alpha_p = 3,3$, MFS = 12

Figure 7, Continued



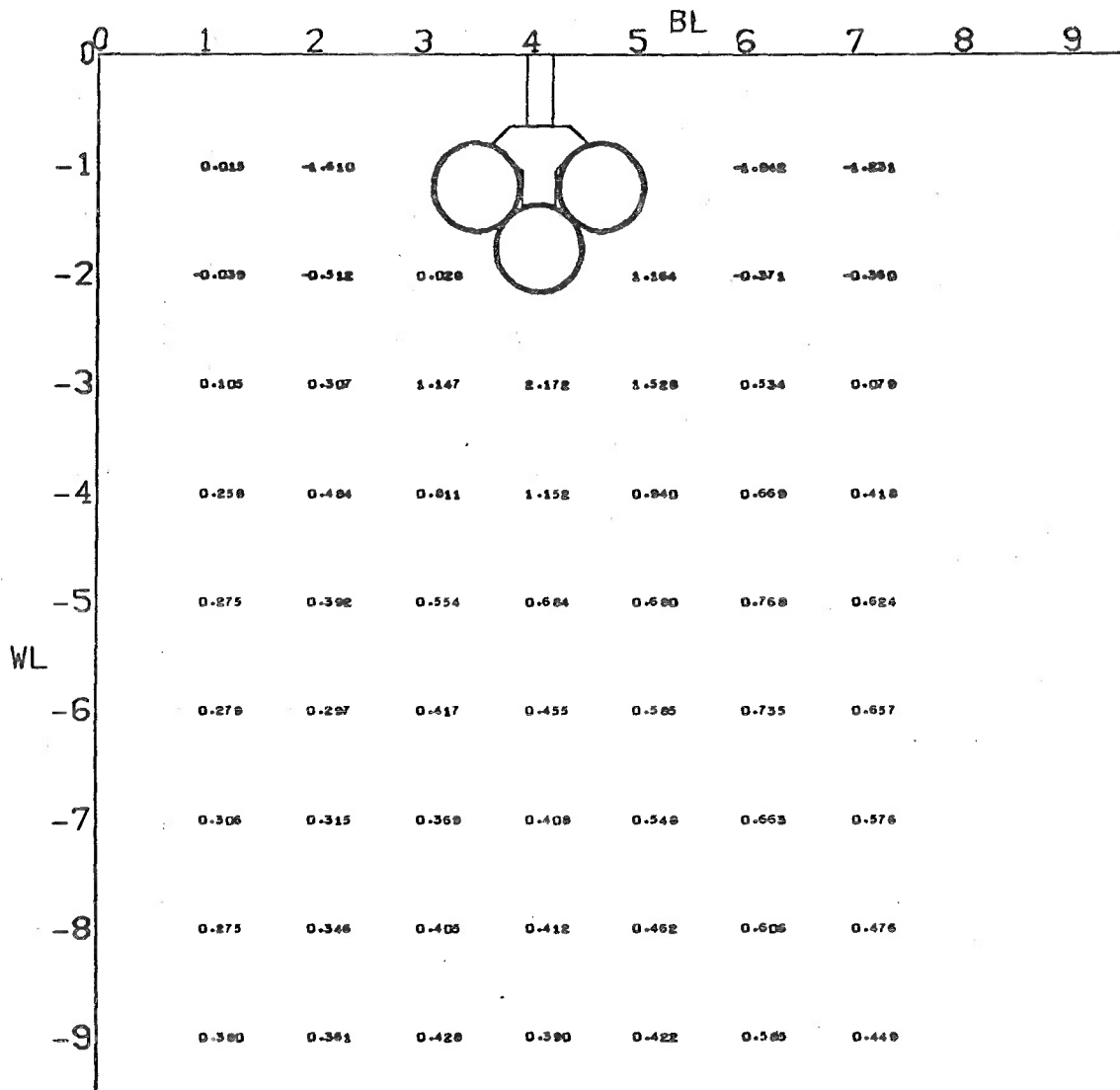
(d) $\alpha_p = 3.3$, $MFS = 16$

Figure 7. Concluded



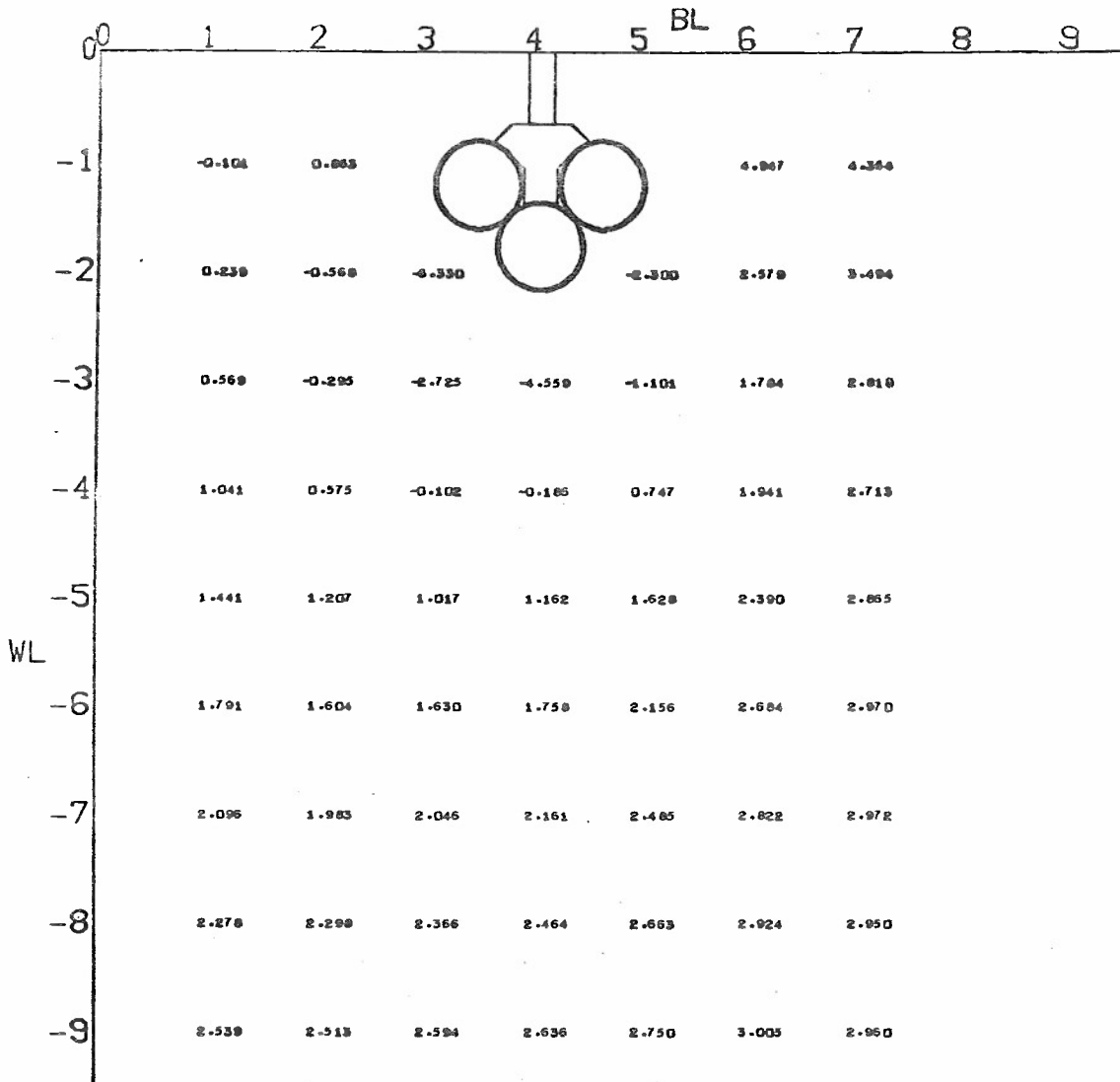
(a) MFS = 12

Figure 8. Effect of Three M-117 Bombs and TER on the Flow Angle Formed by the z Component of Velocity and the Total Velocity Vector at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



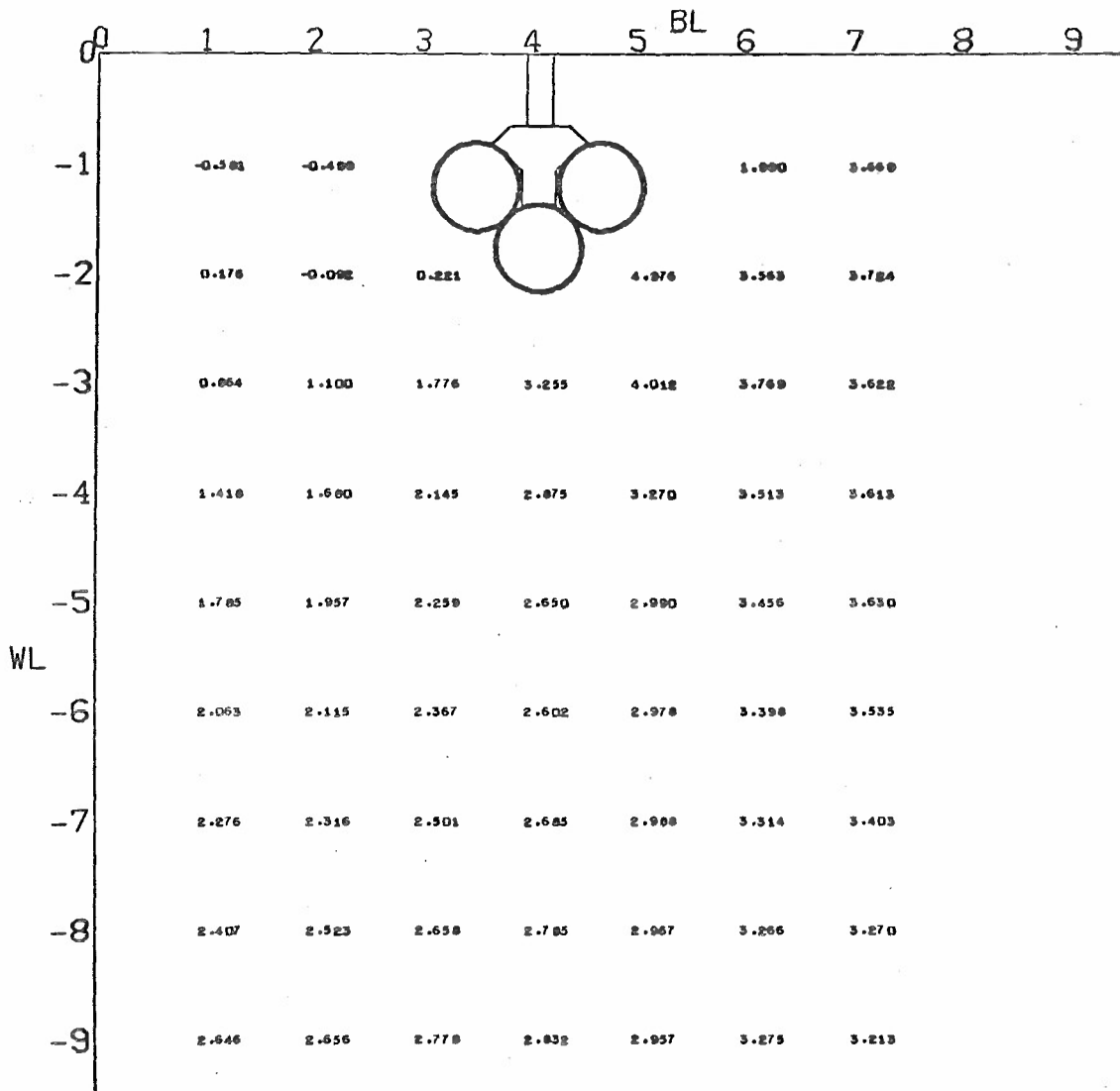
(b) $MFS = 16$

Figure 8. Concluded



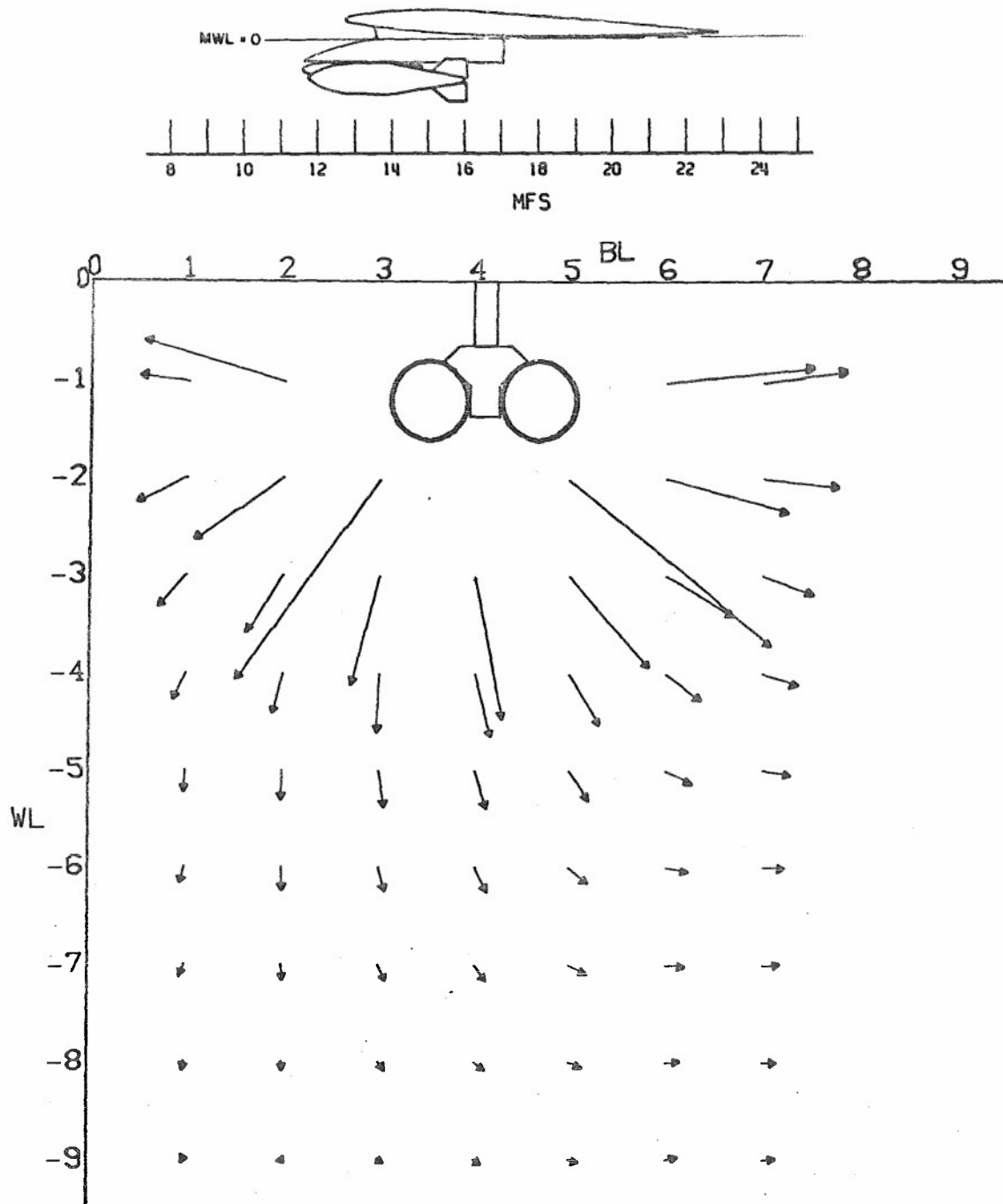
(a) MFS = 12

Figure 9. Effect of Three M-117 Bombs and TER on the Flow Angle Formed by the z Component of Velocity and Total Velocity Vector at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 3.3$



(b) MFS = 16

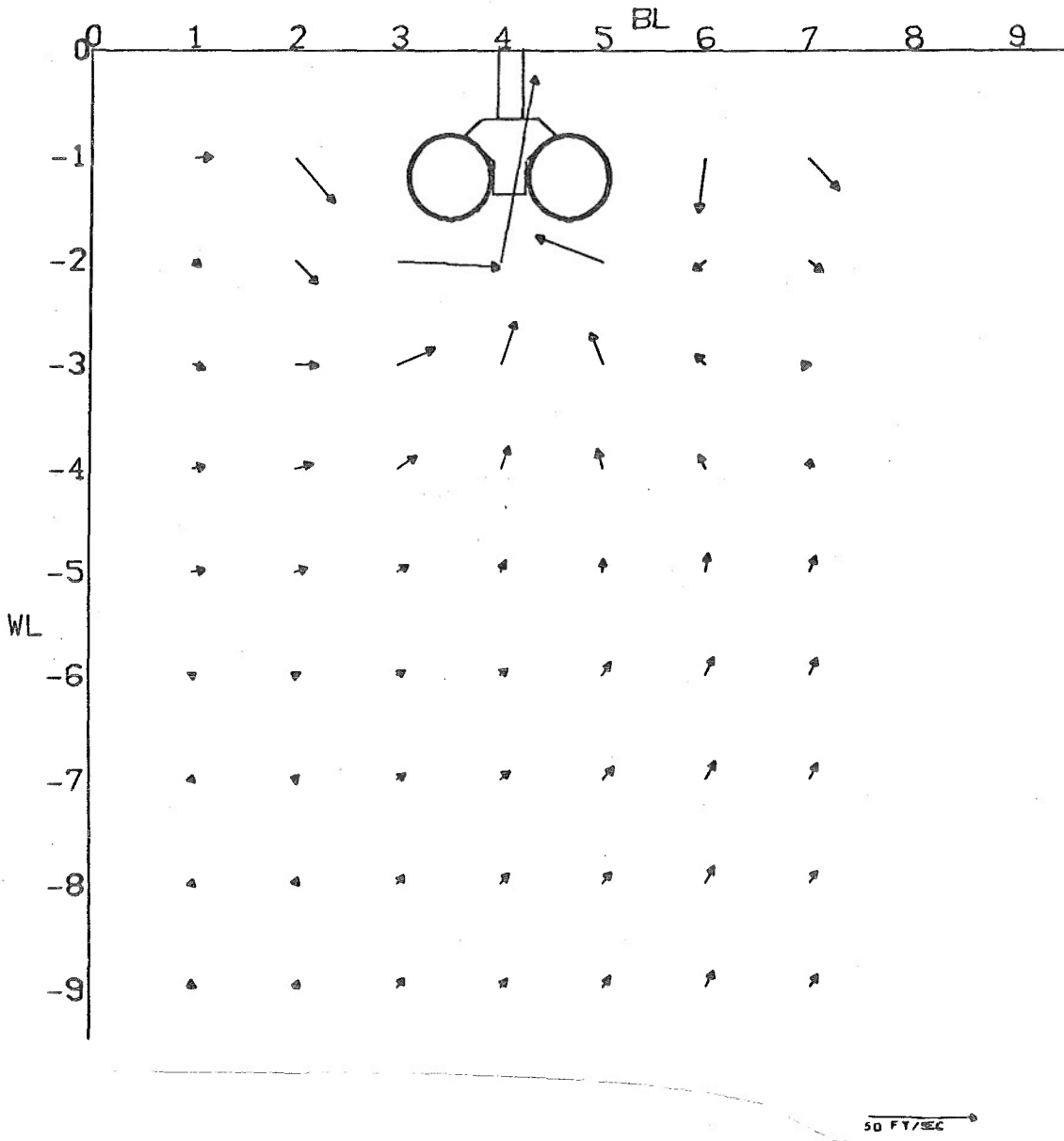
Figure 9. Concluded



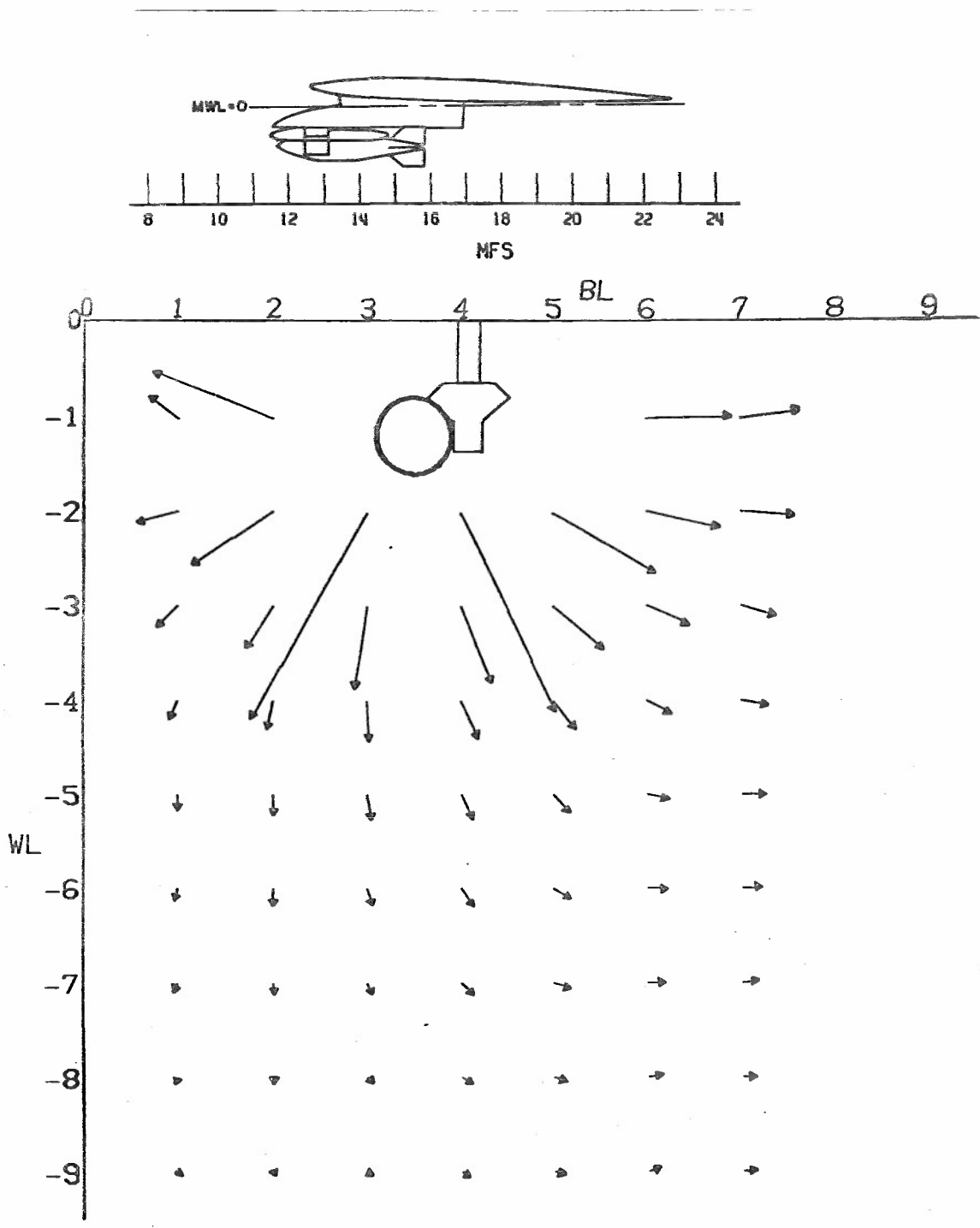
(a) MFS = 12

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Figure 10. Effect of Two M-117 Bombs and TER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

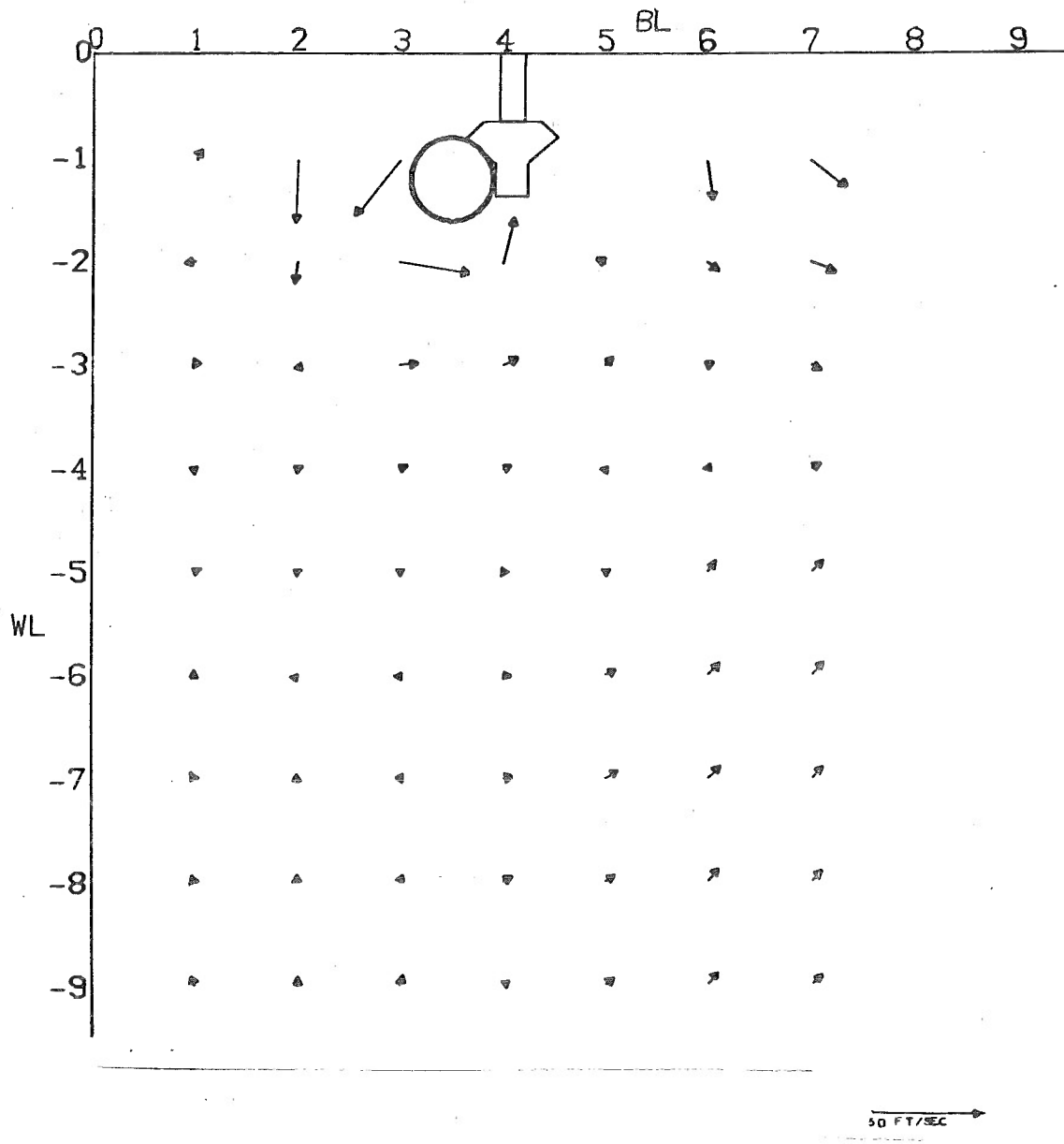


(b) MFS = 16
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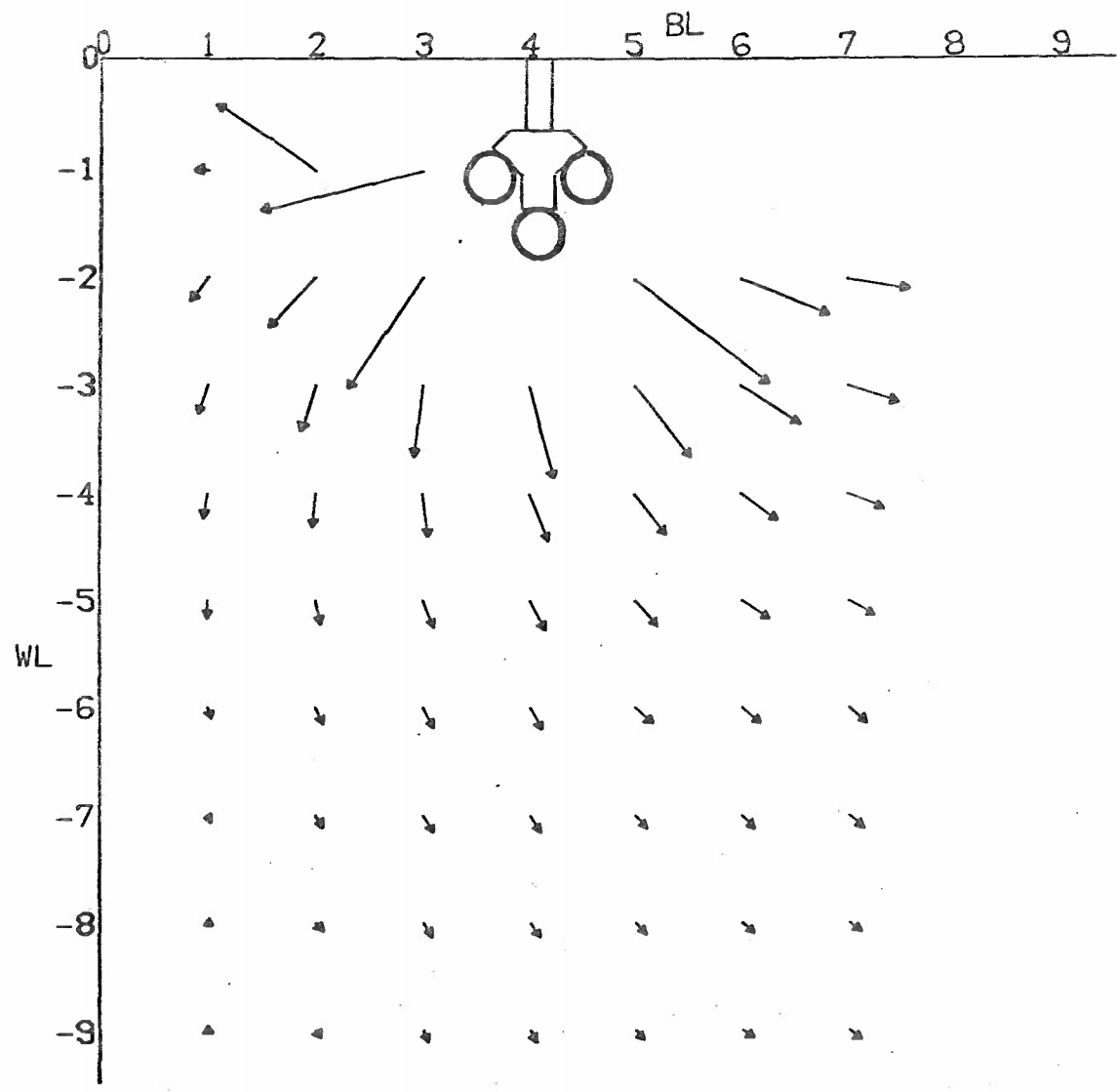
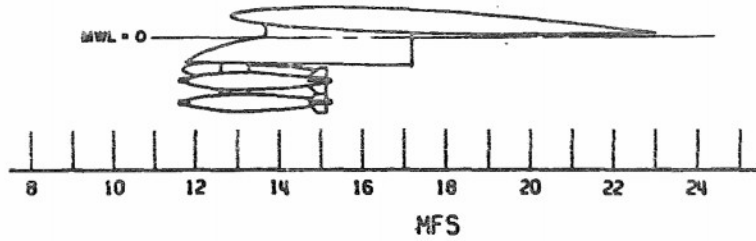


(a) MFS = 12

Figure 11. Effect of one M-117 Bomb and TER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



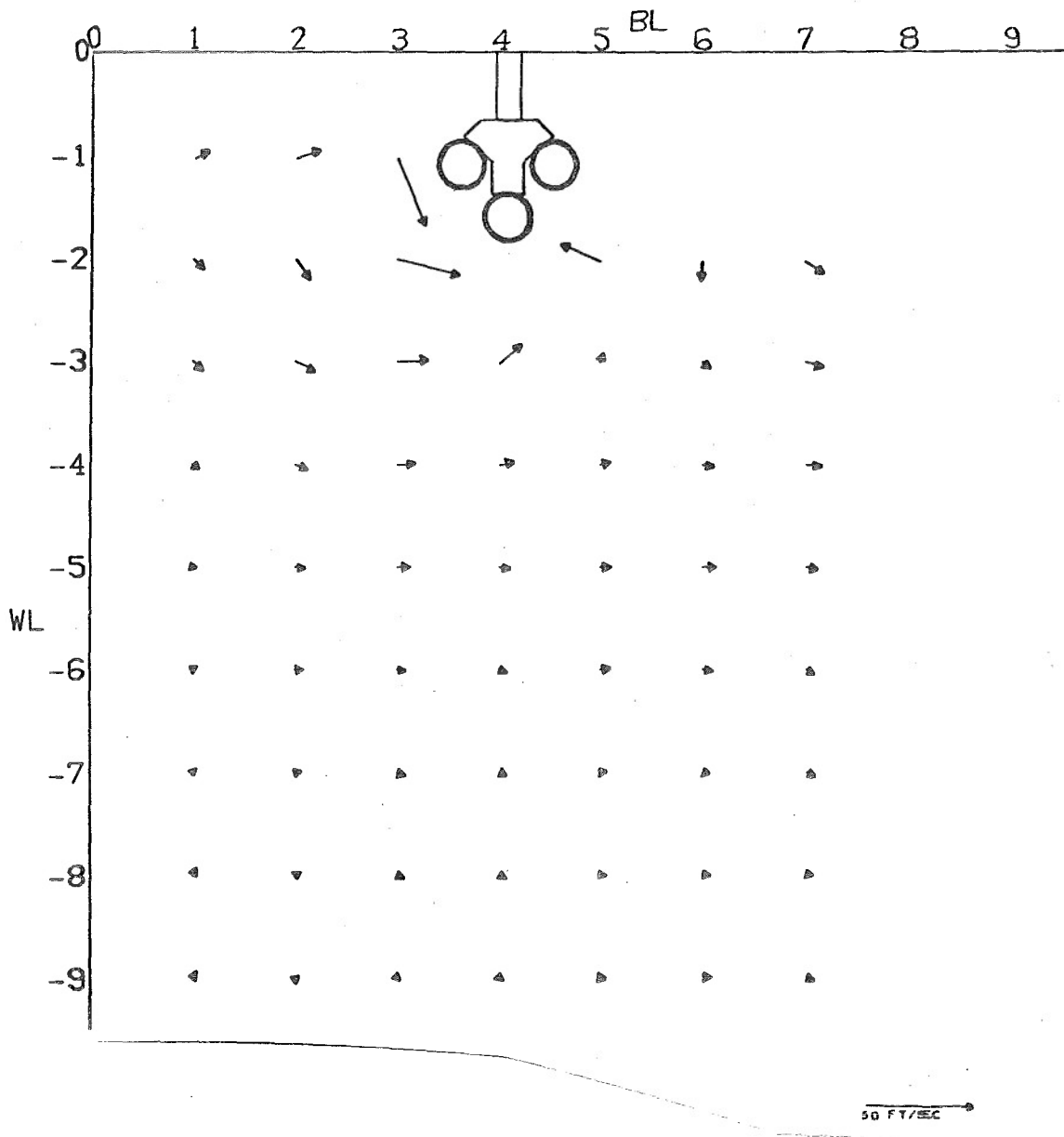
(b) MFS = 16
 Figure 11. Concluded



(a) $\alpha_p = 0.3$, MFS = 12

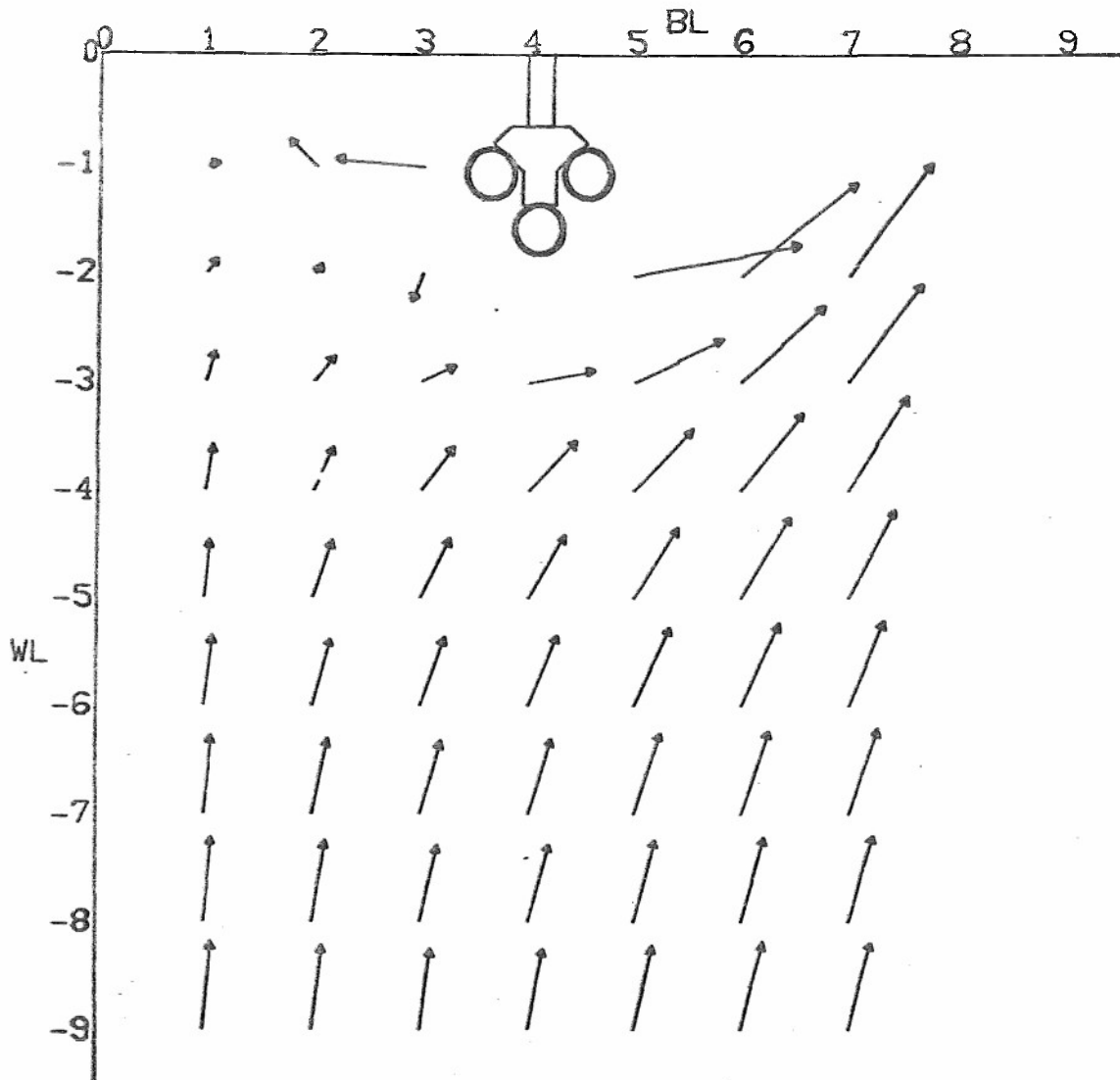
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Figure 12. Effect of Three MK-81 Bombs and TER on the Transverse Velocity Components of the Flow Field $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



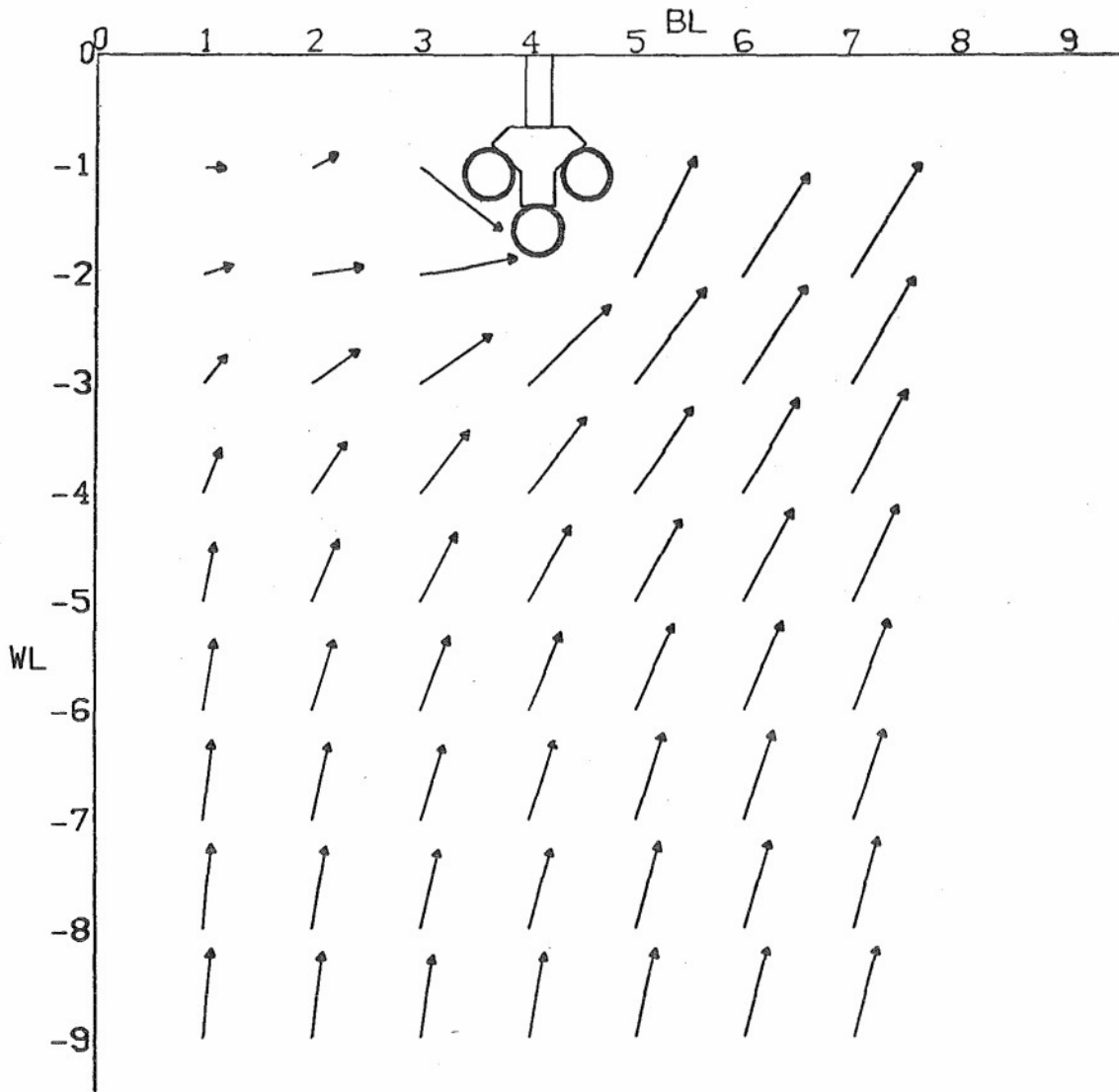
(b) $\alpha_p = 0.3$, MFS = 15

Figure 12. Continued



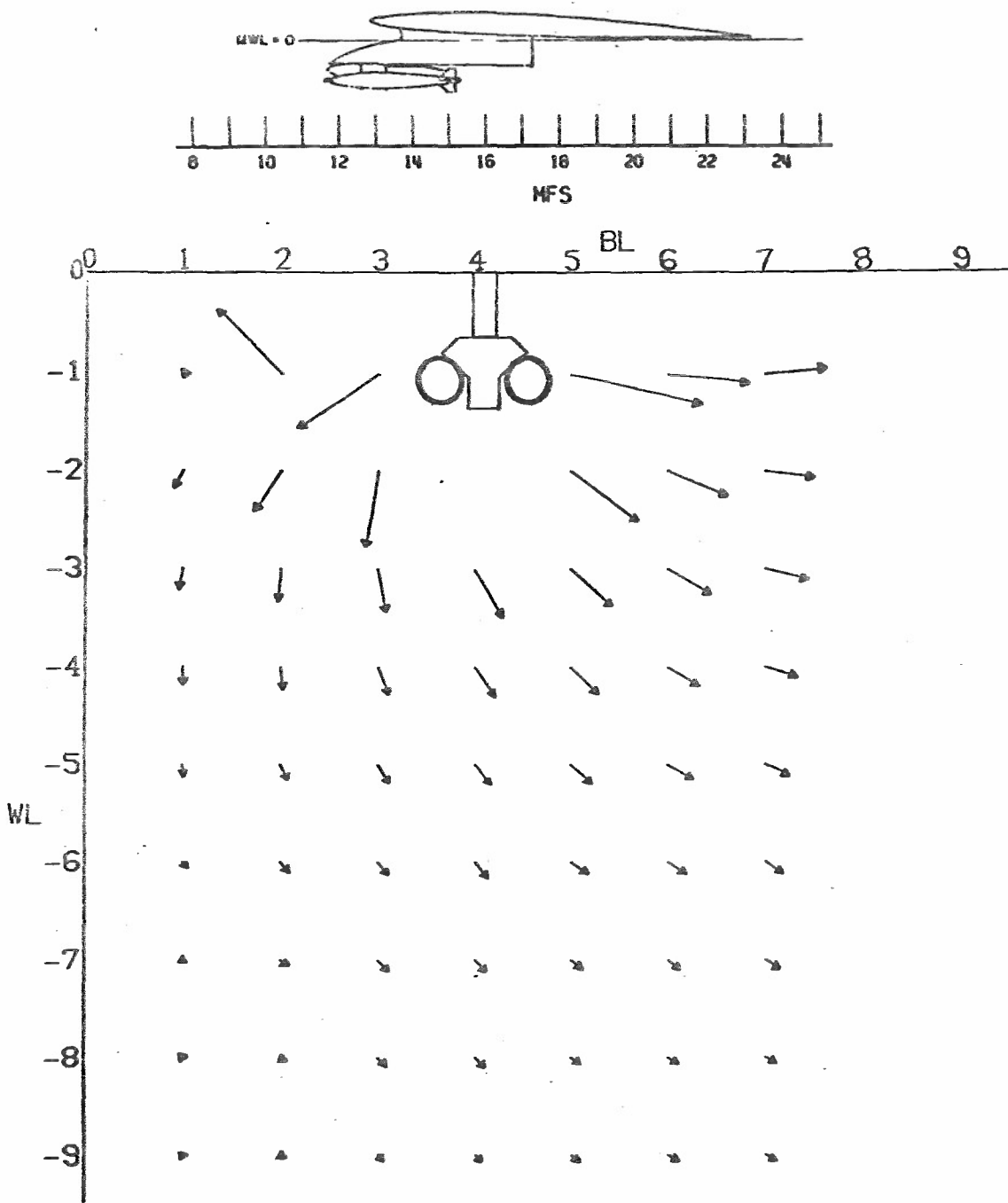
(c) $\alpha_p = 3.3$, MFS = 12

Figure 12, Continued



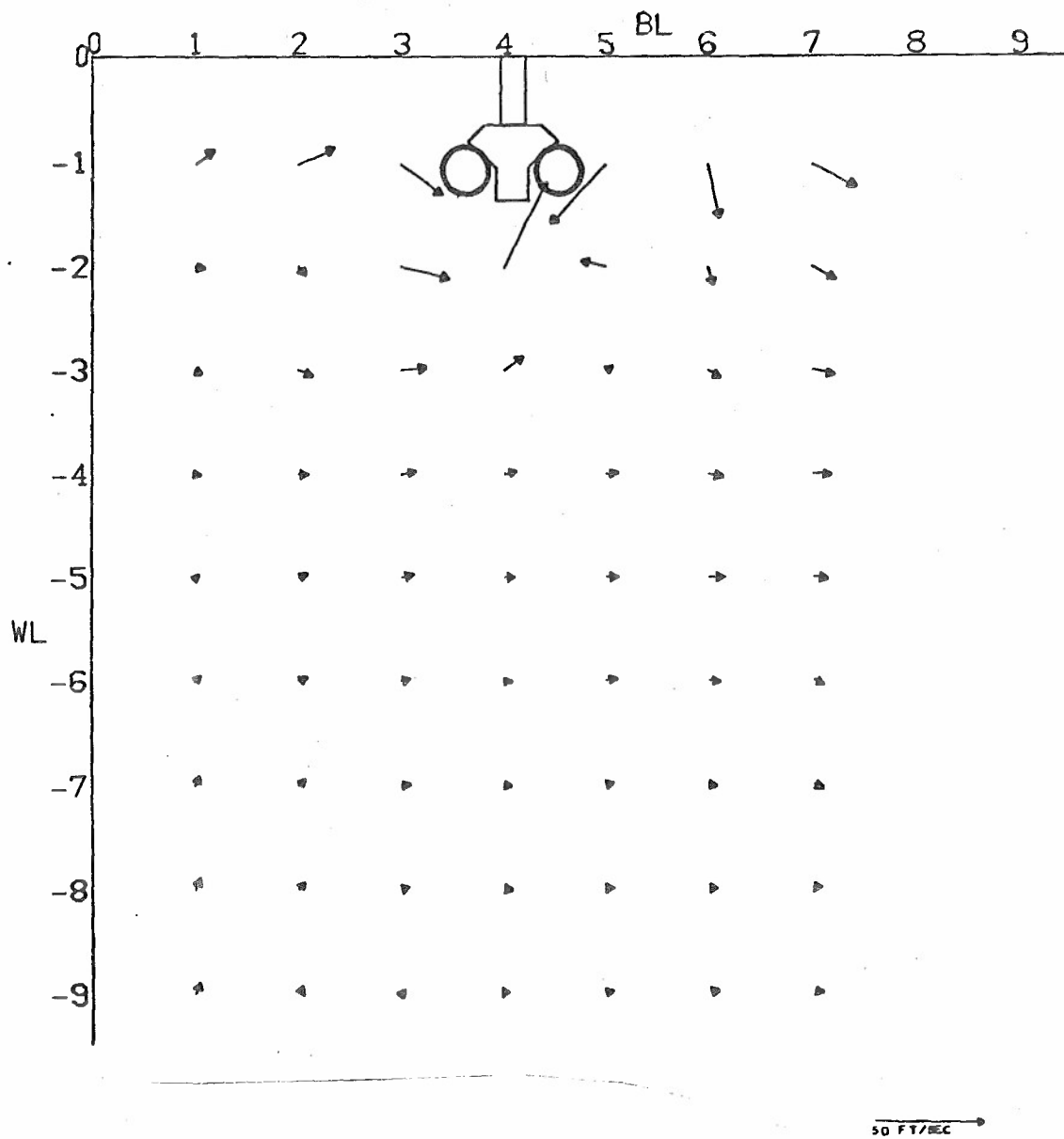
(d) $\alpha_p = 3.3$, MPS = 15

Figure 12. Concluded



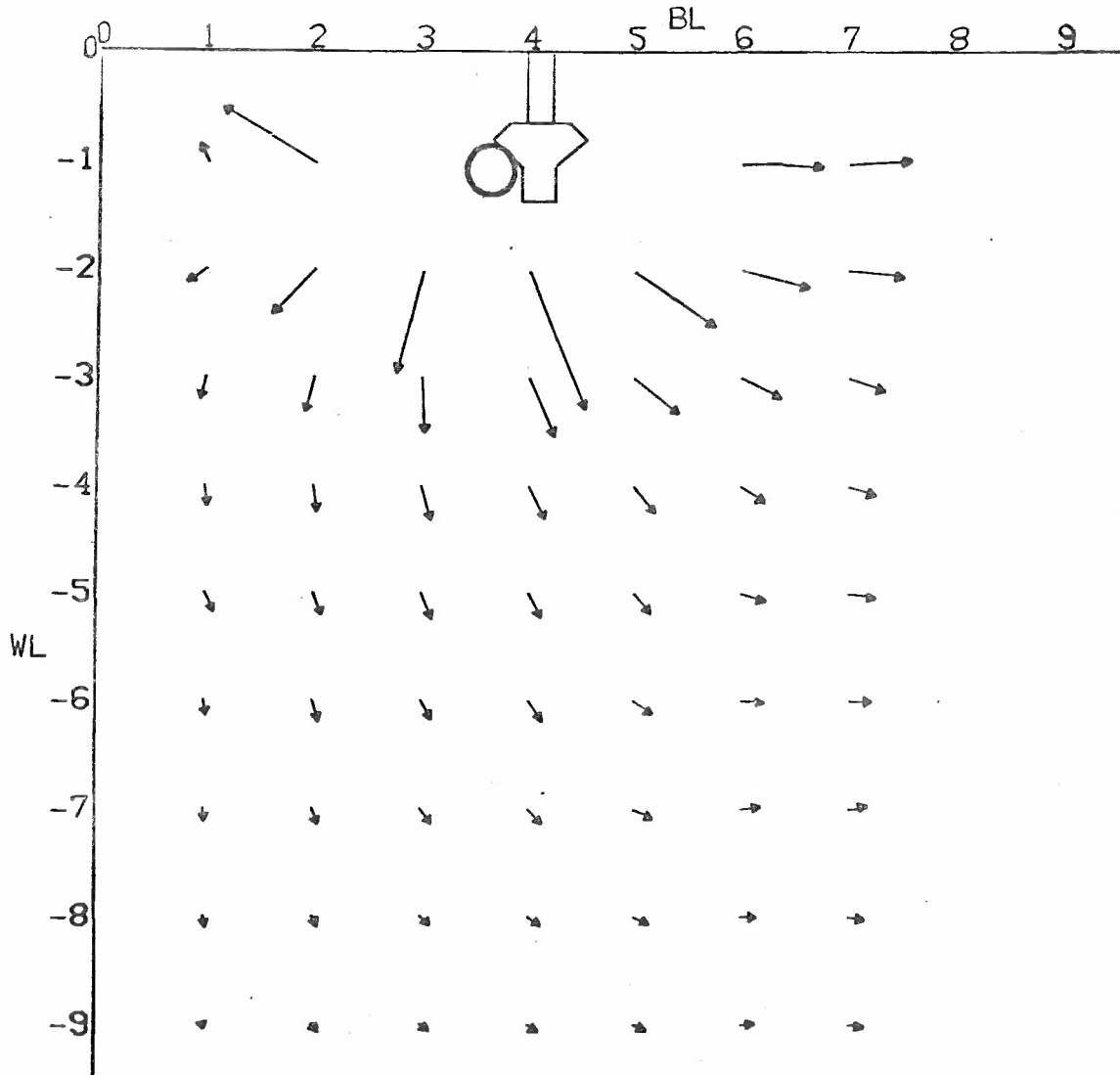
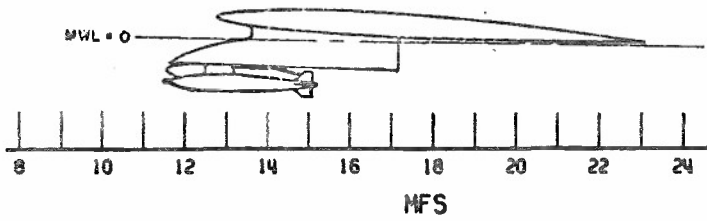
(a) MFS = 12

Figure 13. Effect of Two MK-81 Bombs and TER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



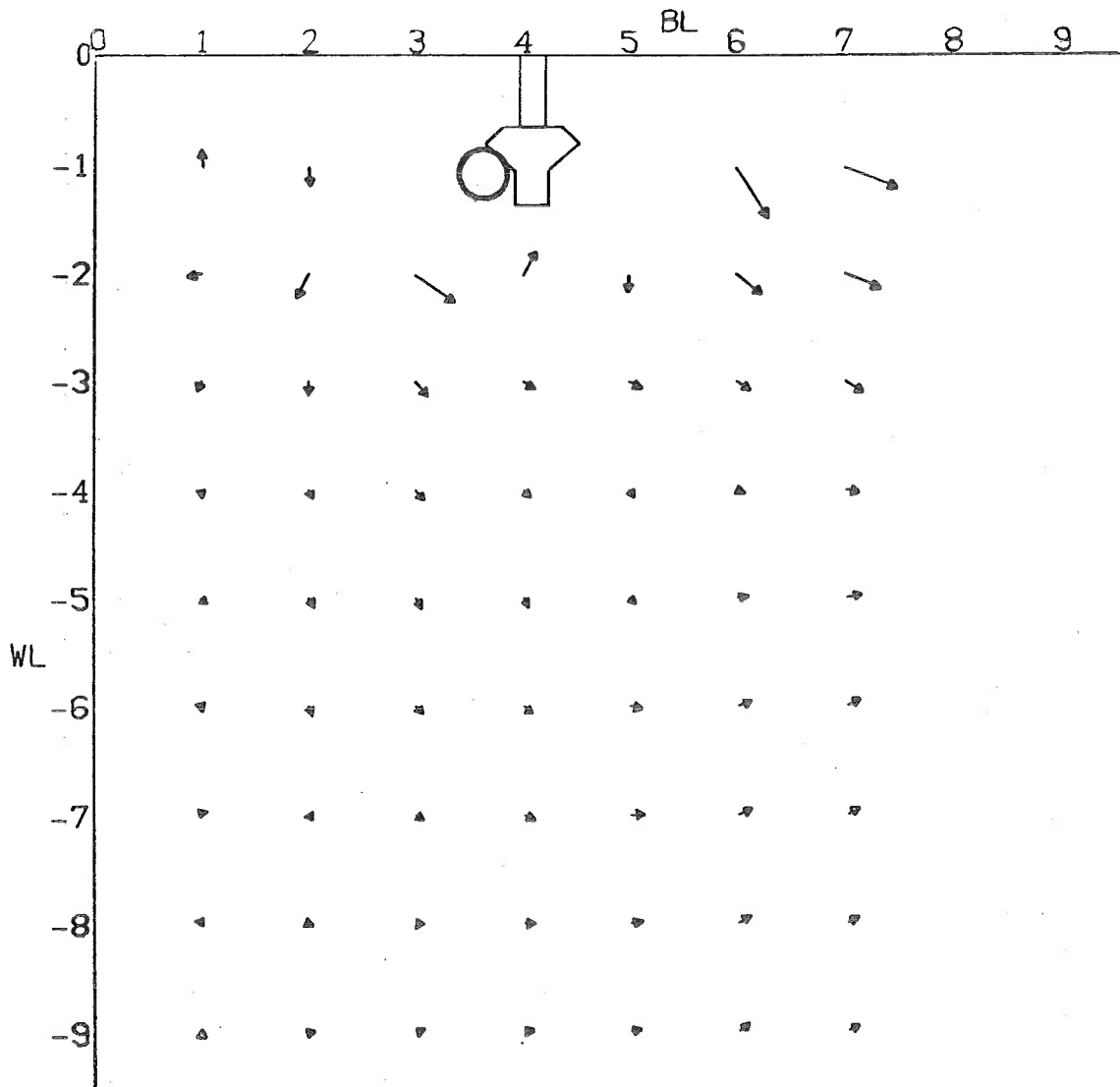
(b) MFS = 15

Figure 13. Concluded



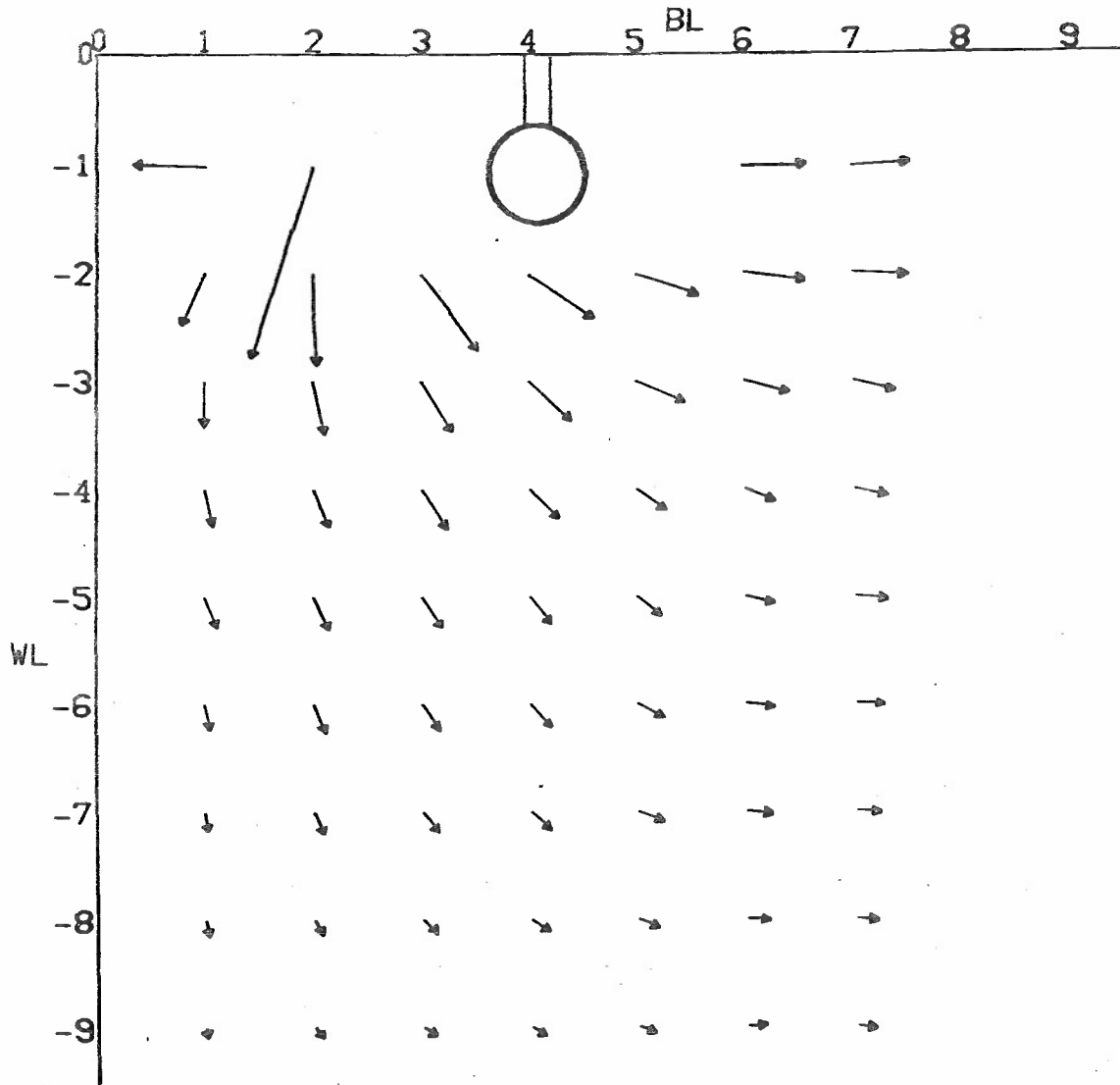
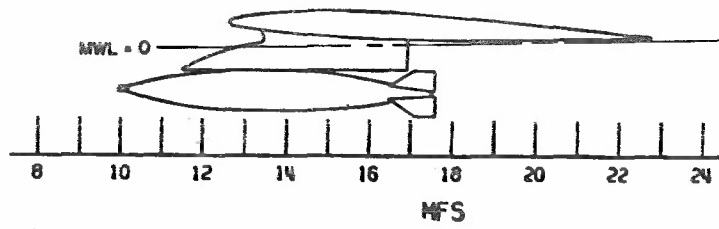
(a) MFS = 12

Figure 14. Effect of One MK-81 Bomb and TER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



(b) MFS = 15

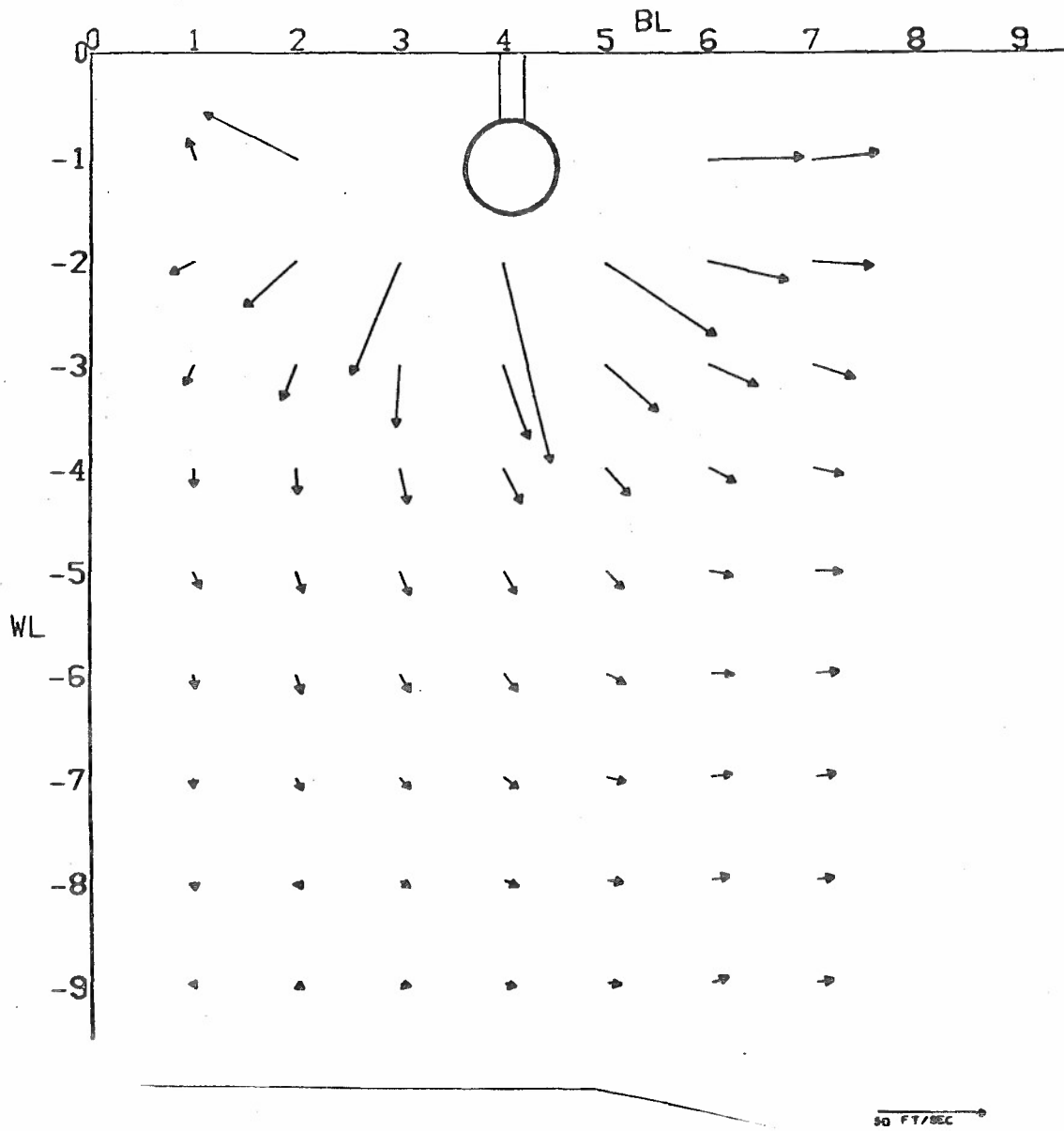
Figure 14. Concluded



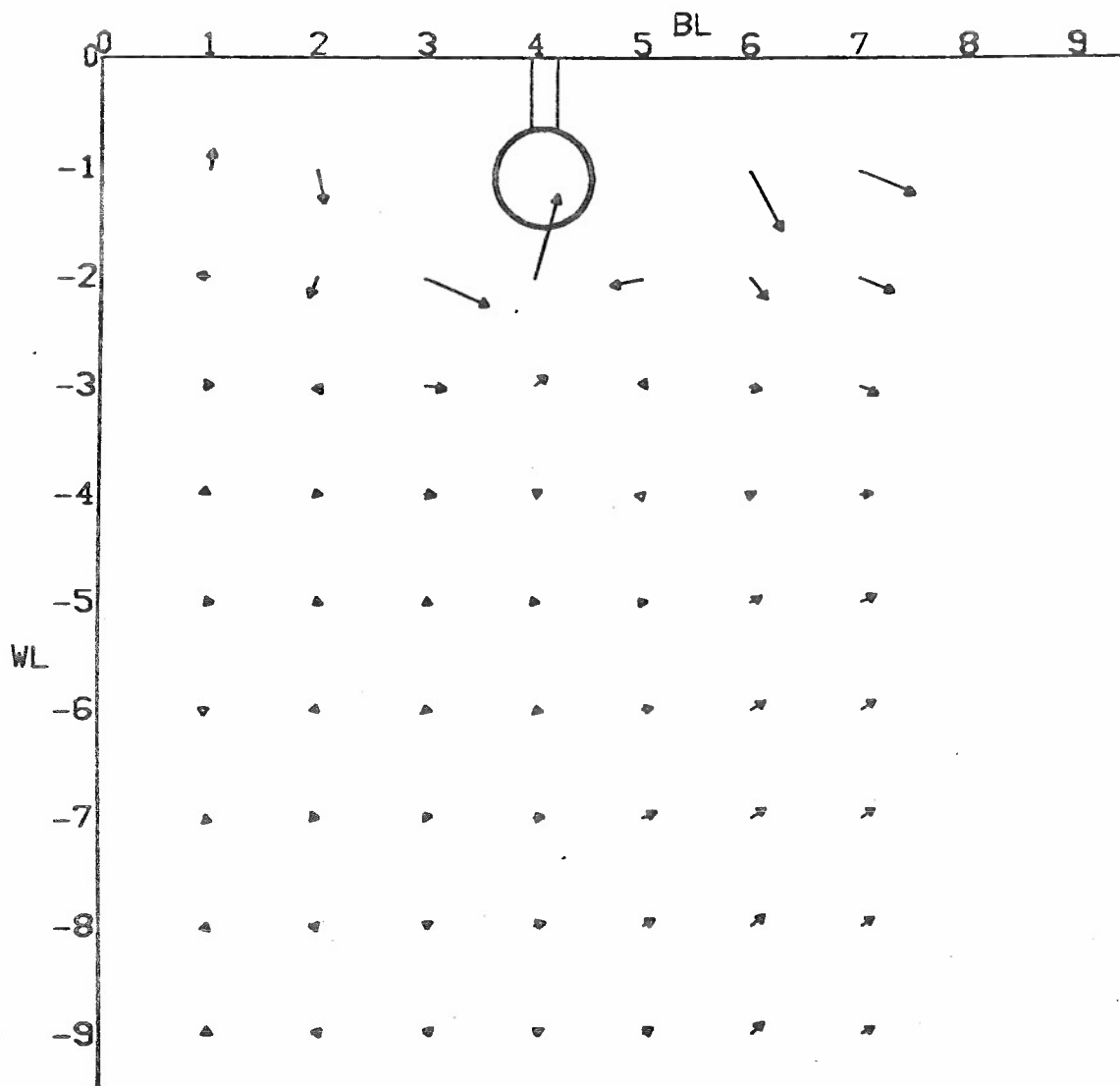
(a) $\alpha_p = 0.3$, MFS = 10

50 FT/SEC →

Figure 15. Effect of one MK-84 Bomb and Inboard Pylon on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

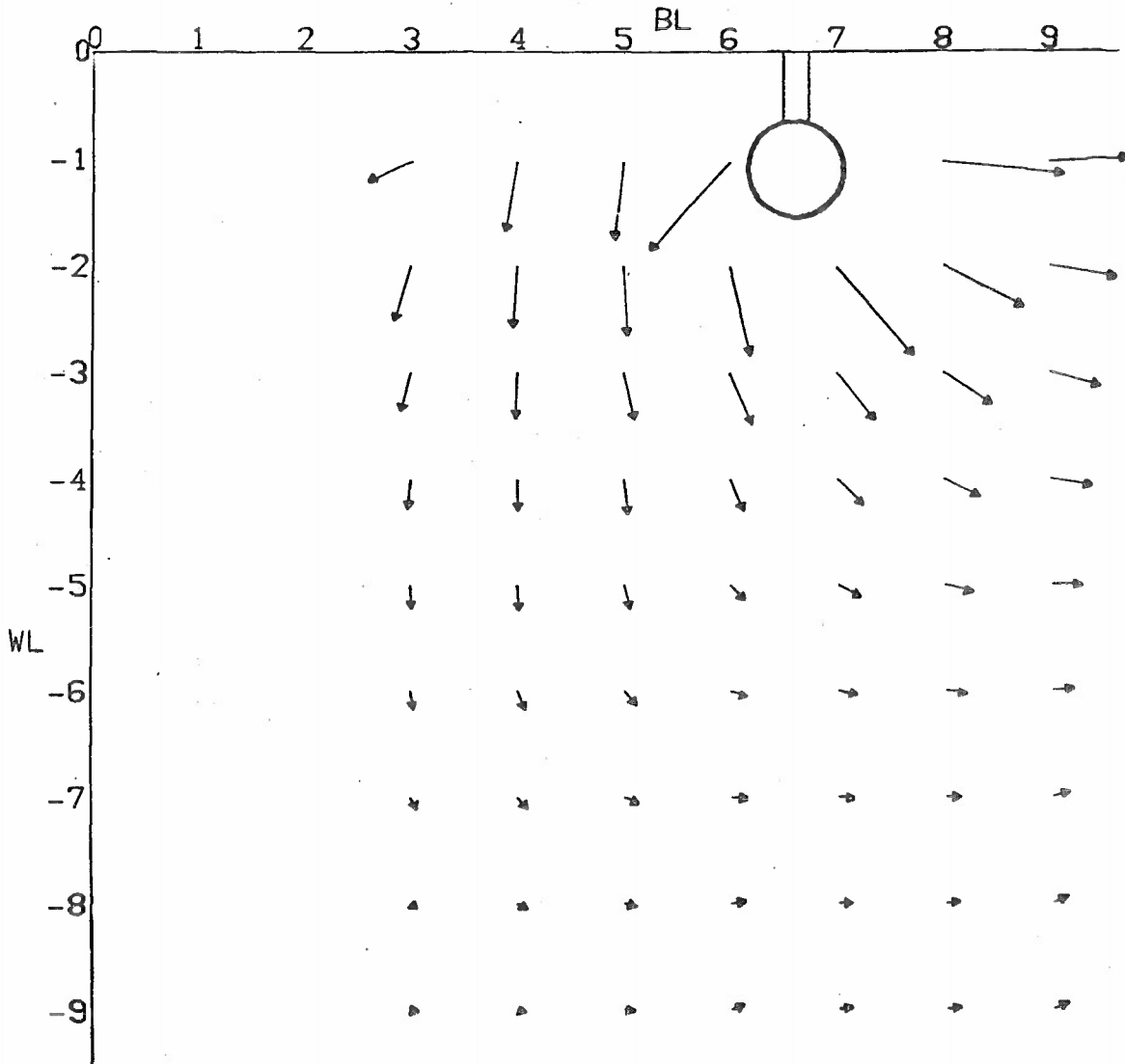
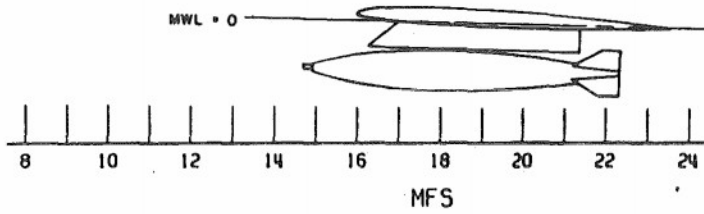


(b) MFS = 12
 Figure 15. Continued



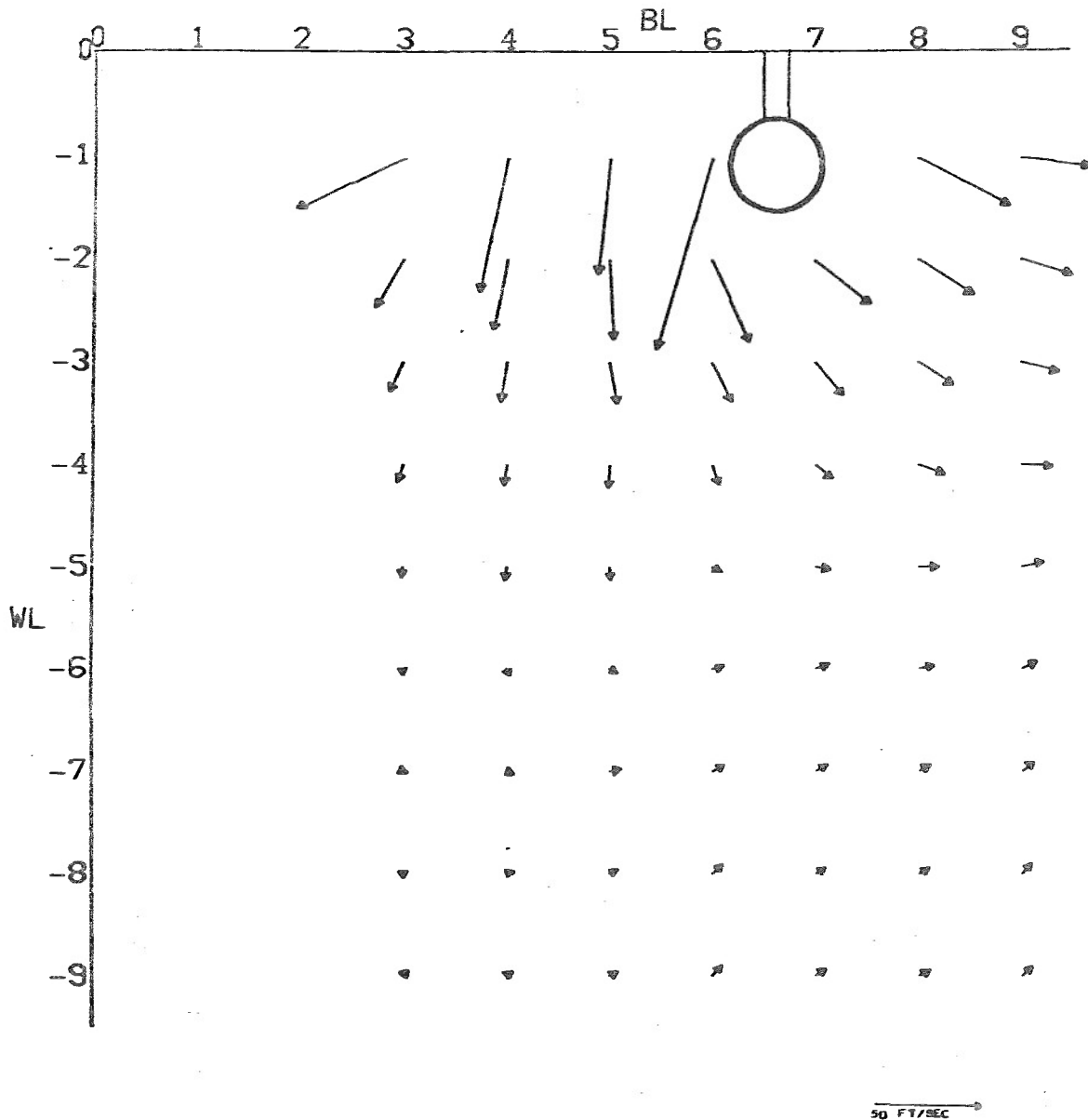
(c) MFS = 17

Figure 15. Concluded



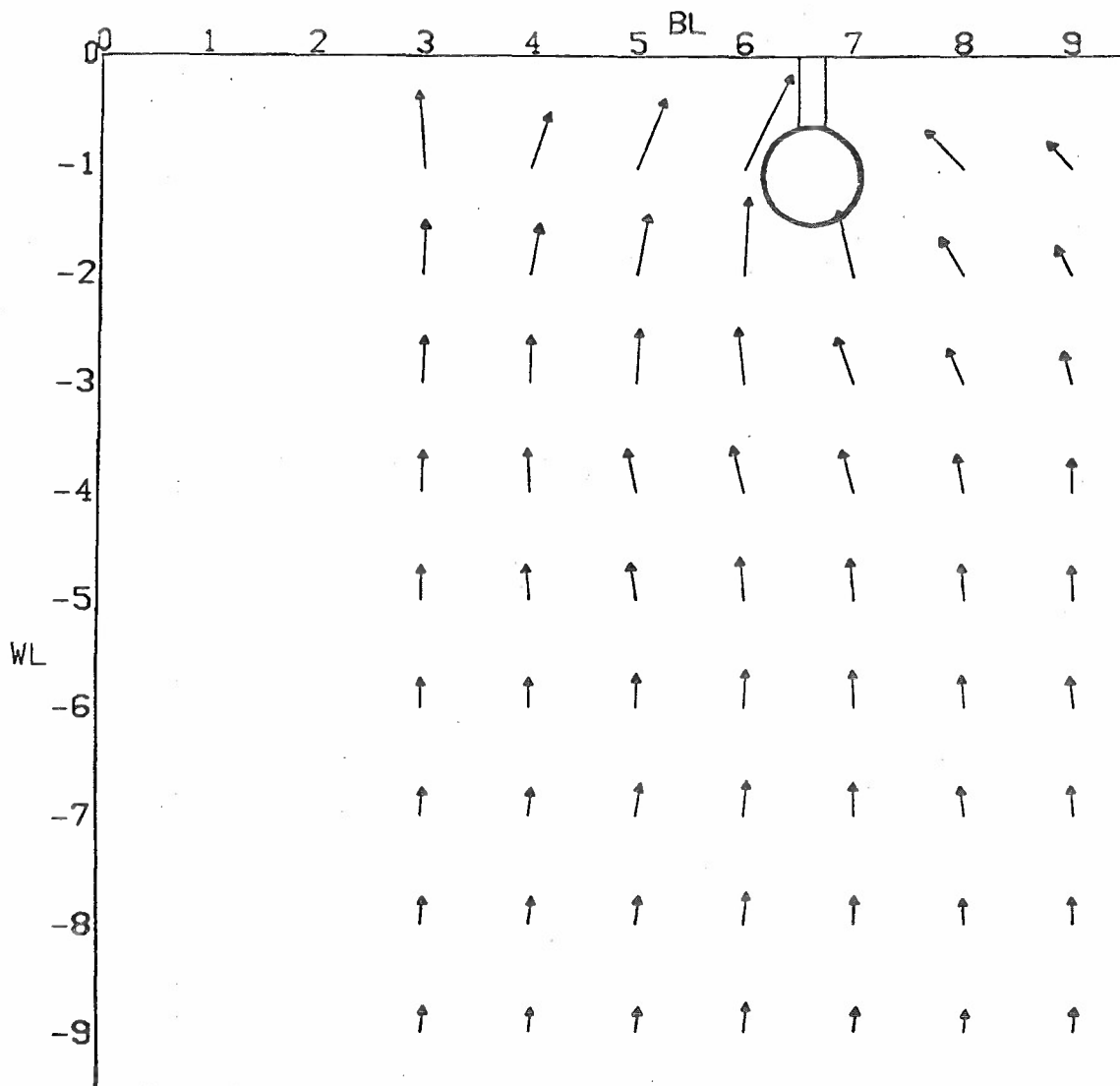
(a) MFS 15

Figure 16. Effect of One MK-84 Bomb and Outboard Pylon on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



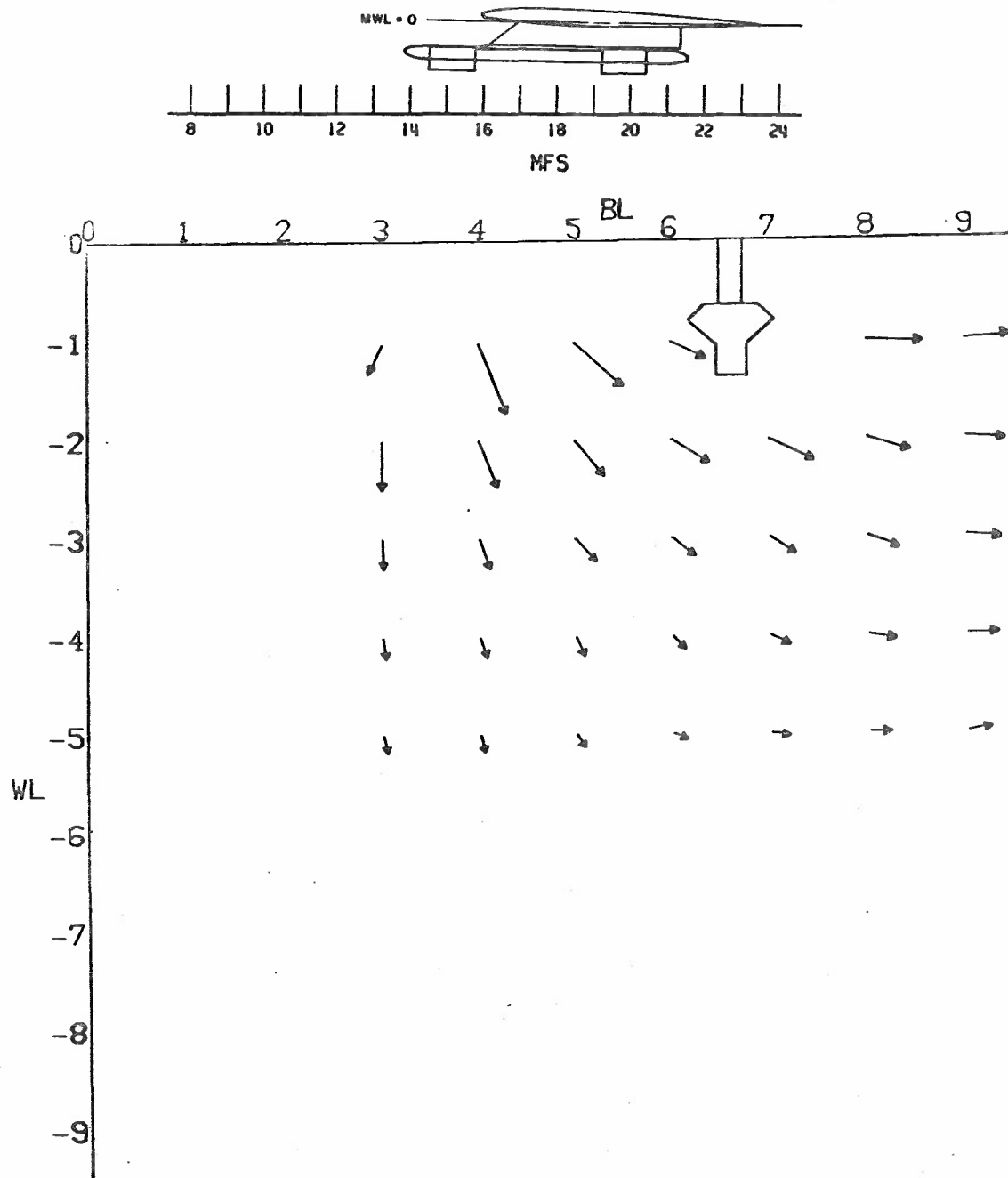
(b) MFS 17

Figure 16. Continued



(c) MFS = 22

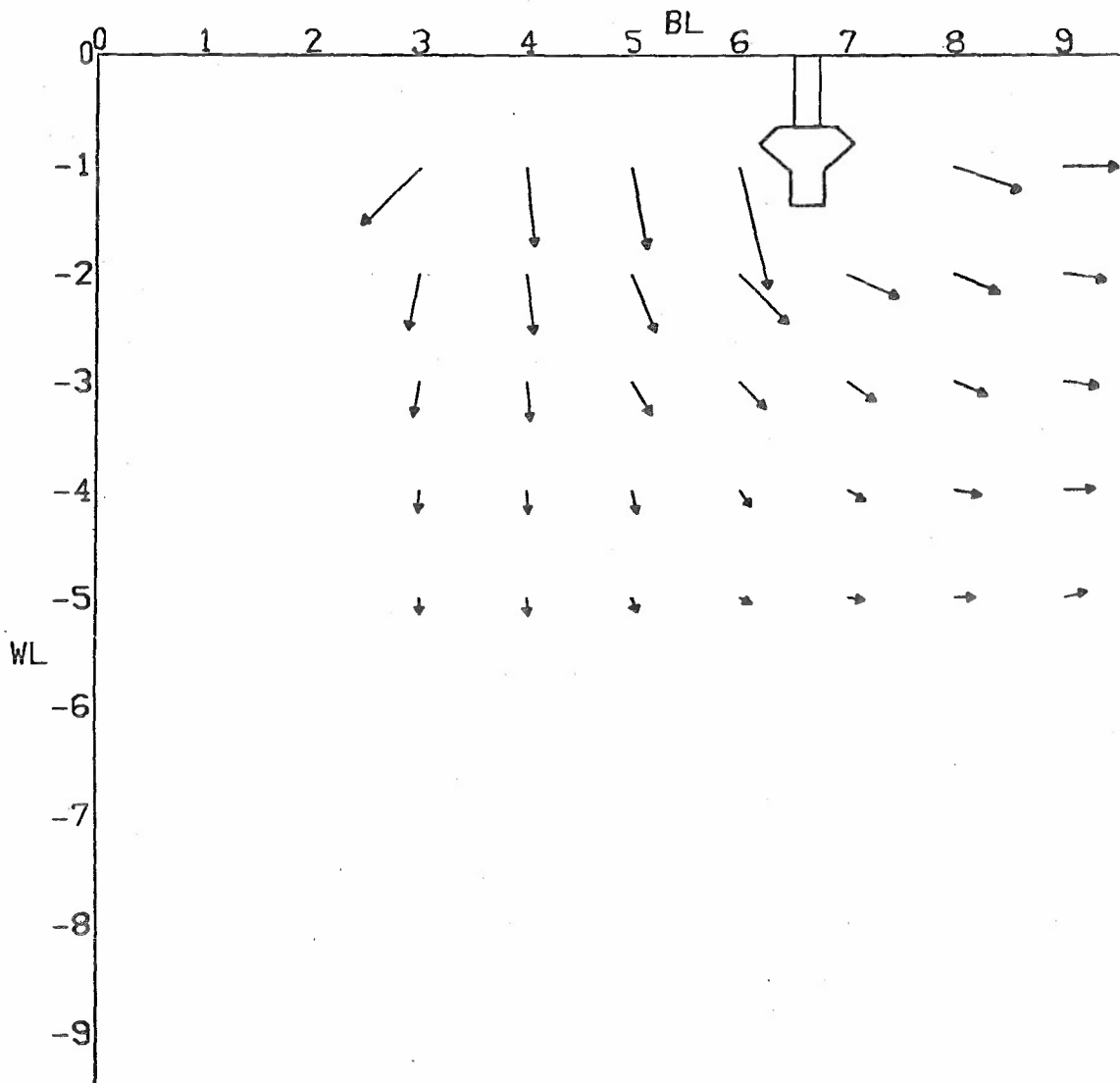
Figure 16. Concluded



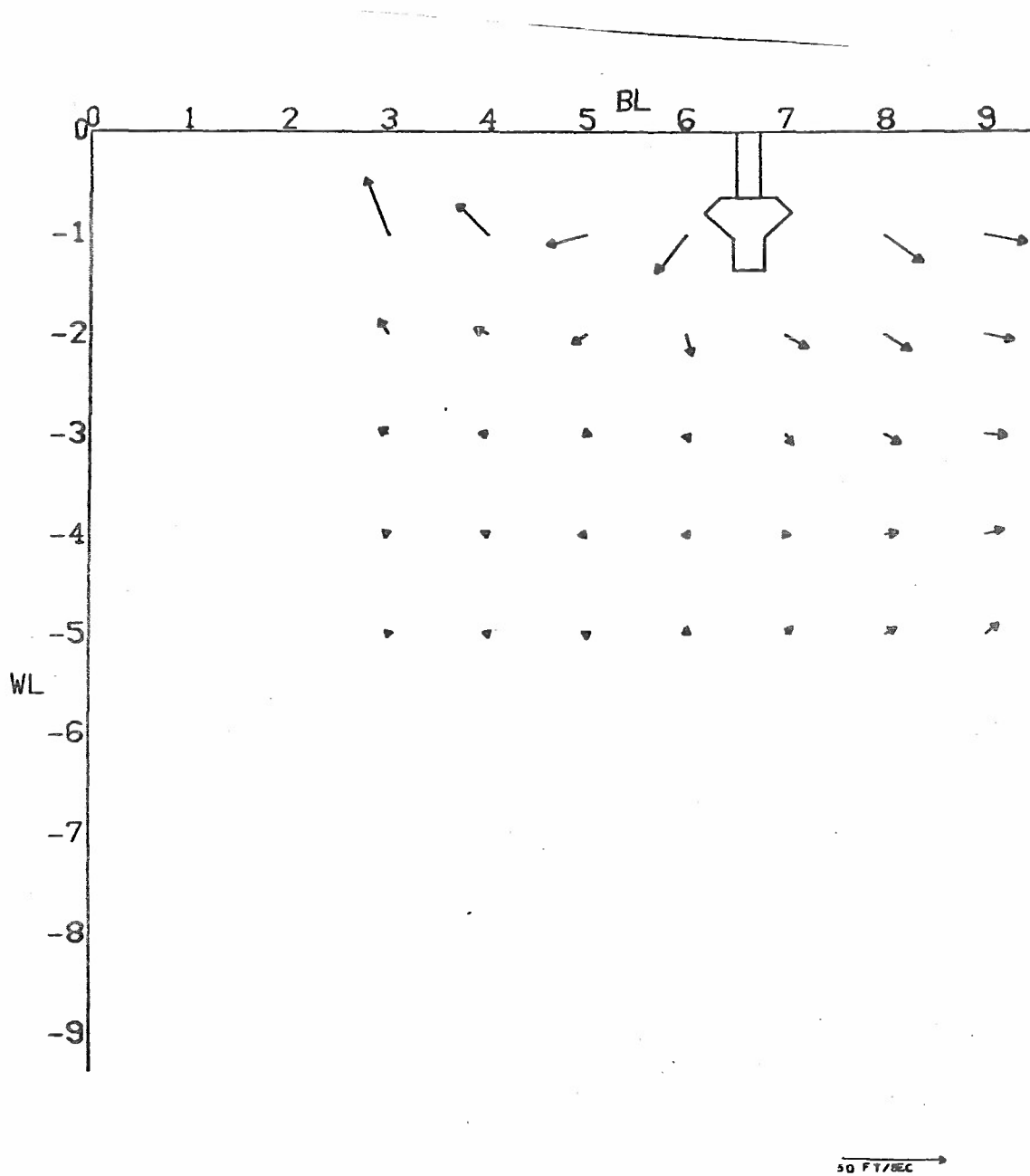
(a) MFS = 13

50 FT/SEC

Figure 17. Effect of an Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

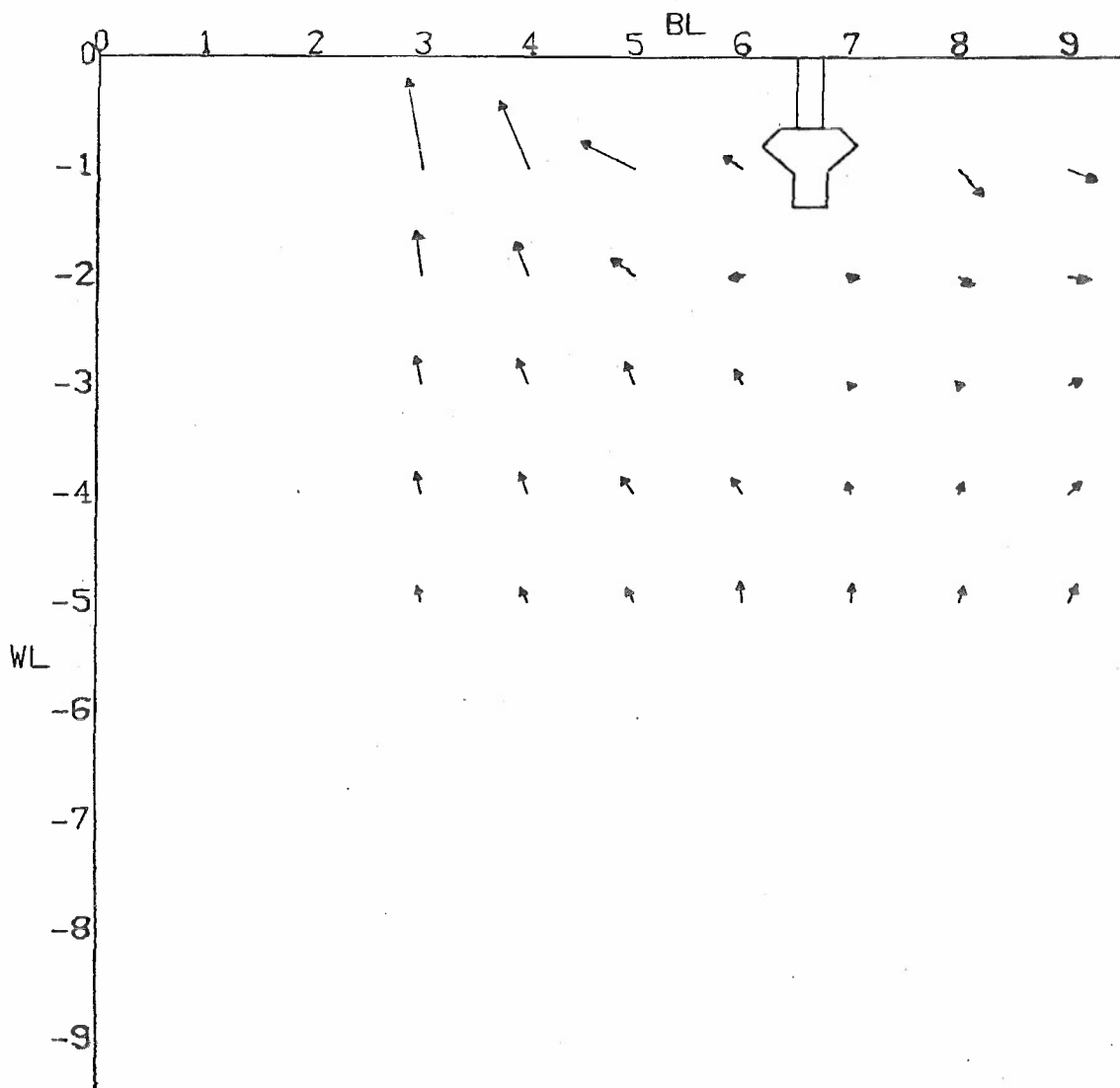


(b) MFS = 16
 Figure 17. Continued



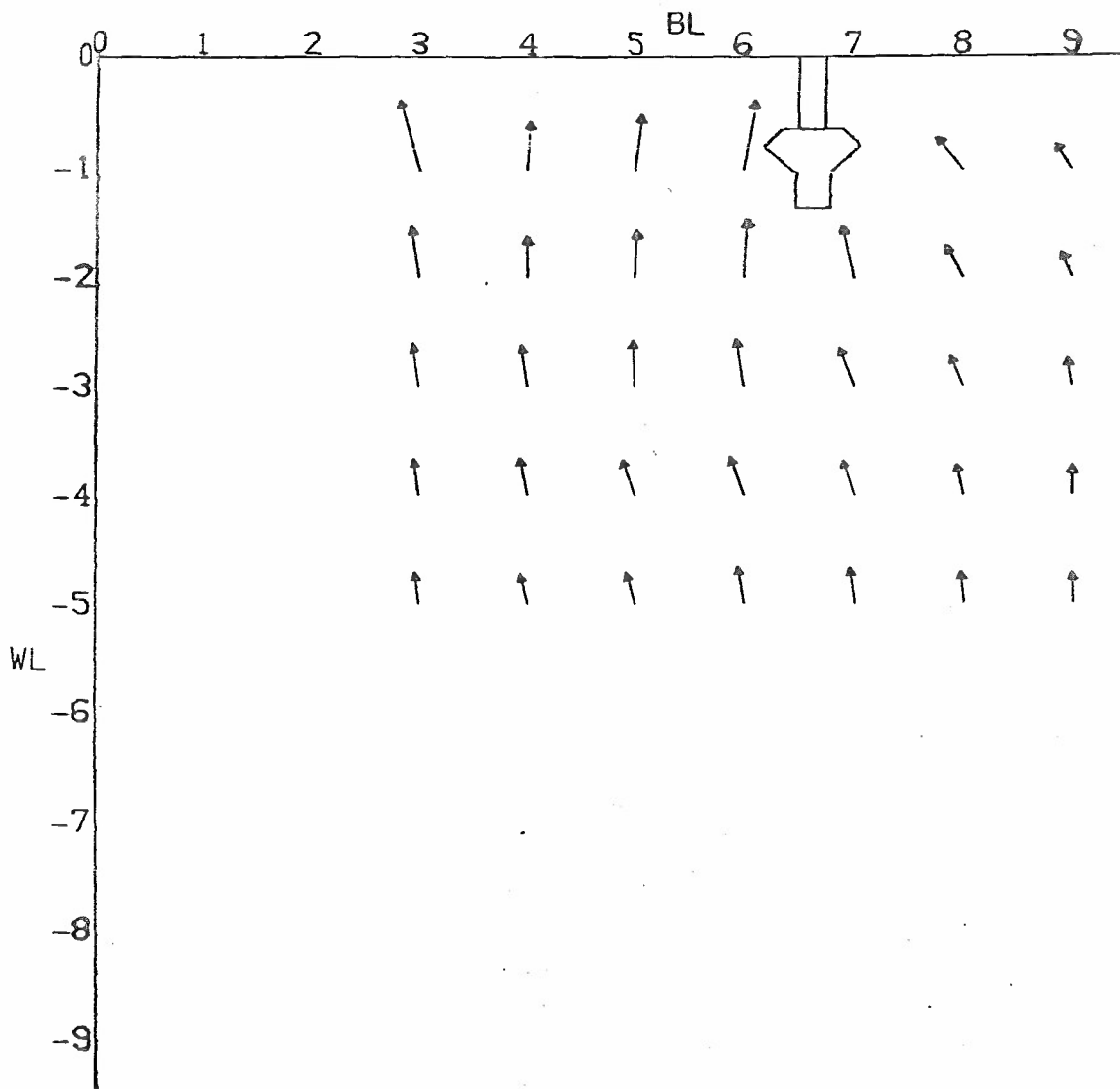
(c) MFS = 18

Figure 17. Continued



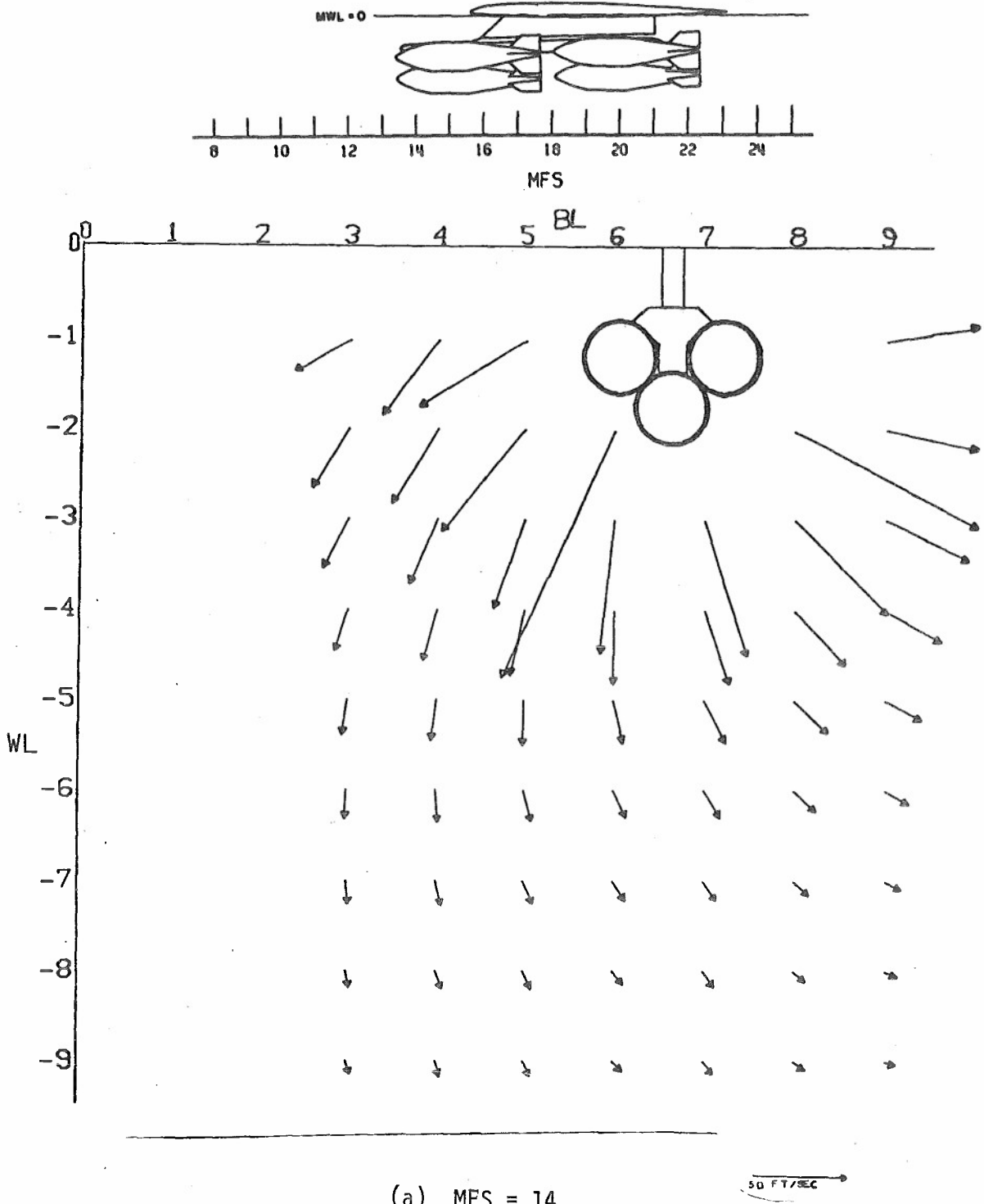
(d) MFS = 19

Figure 17. Continued



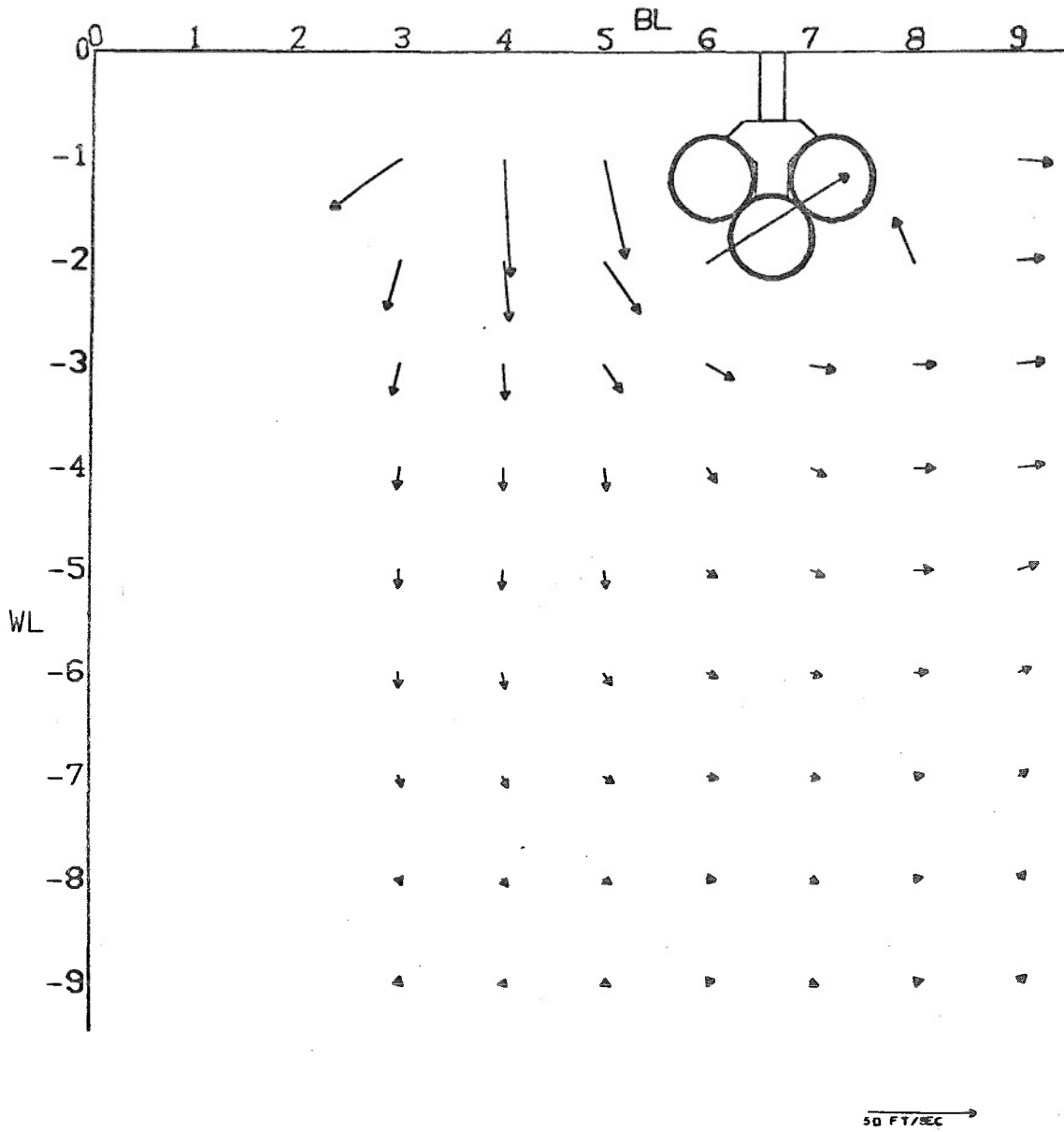
(e) MFS = 22

Figure 17. Concluded



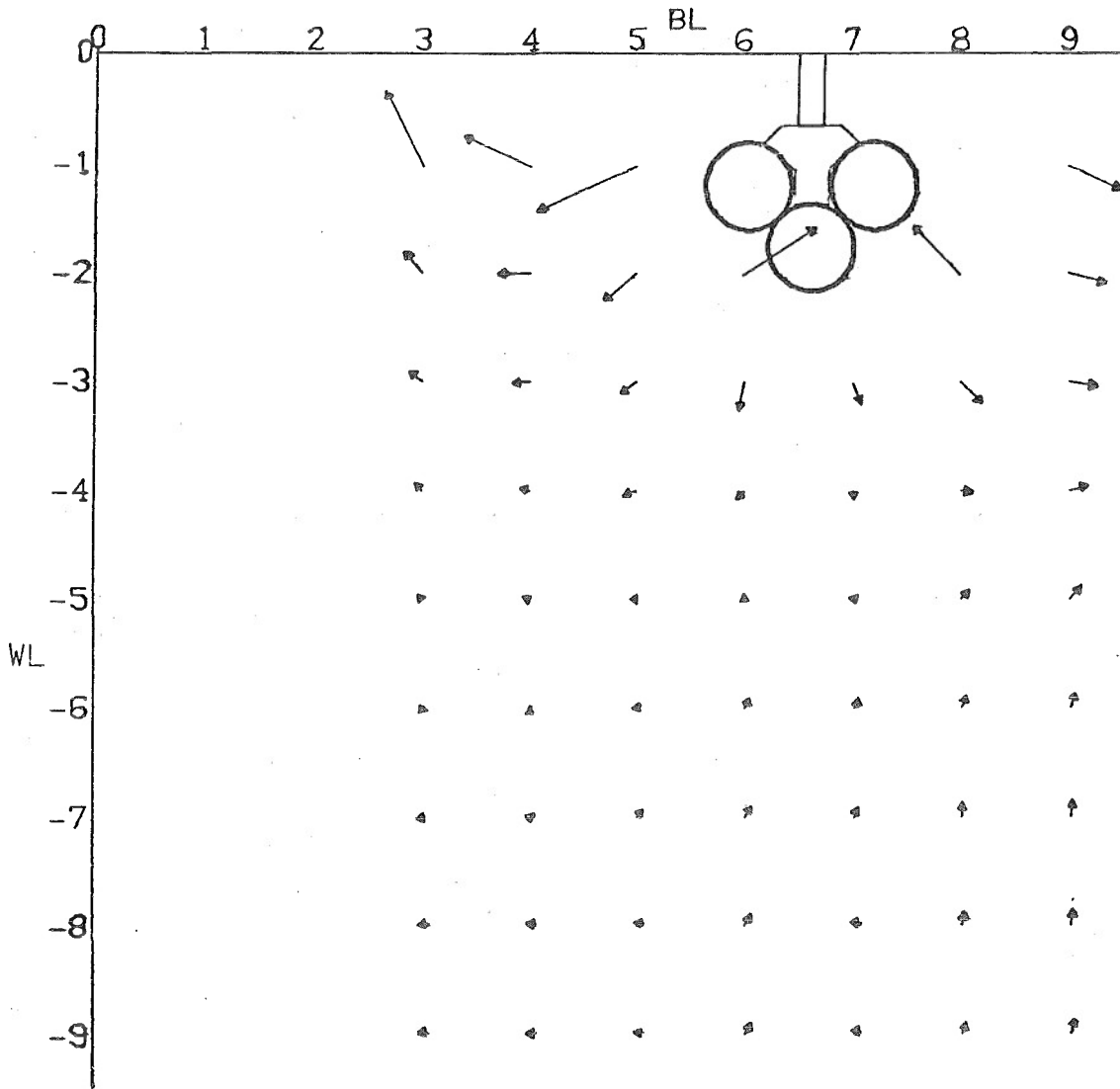
(a) MFS = 14

Figure 18. Effect of Six M-117 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



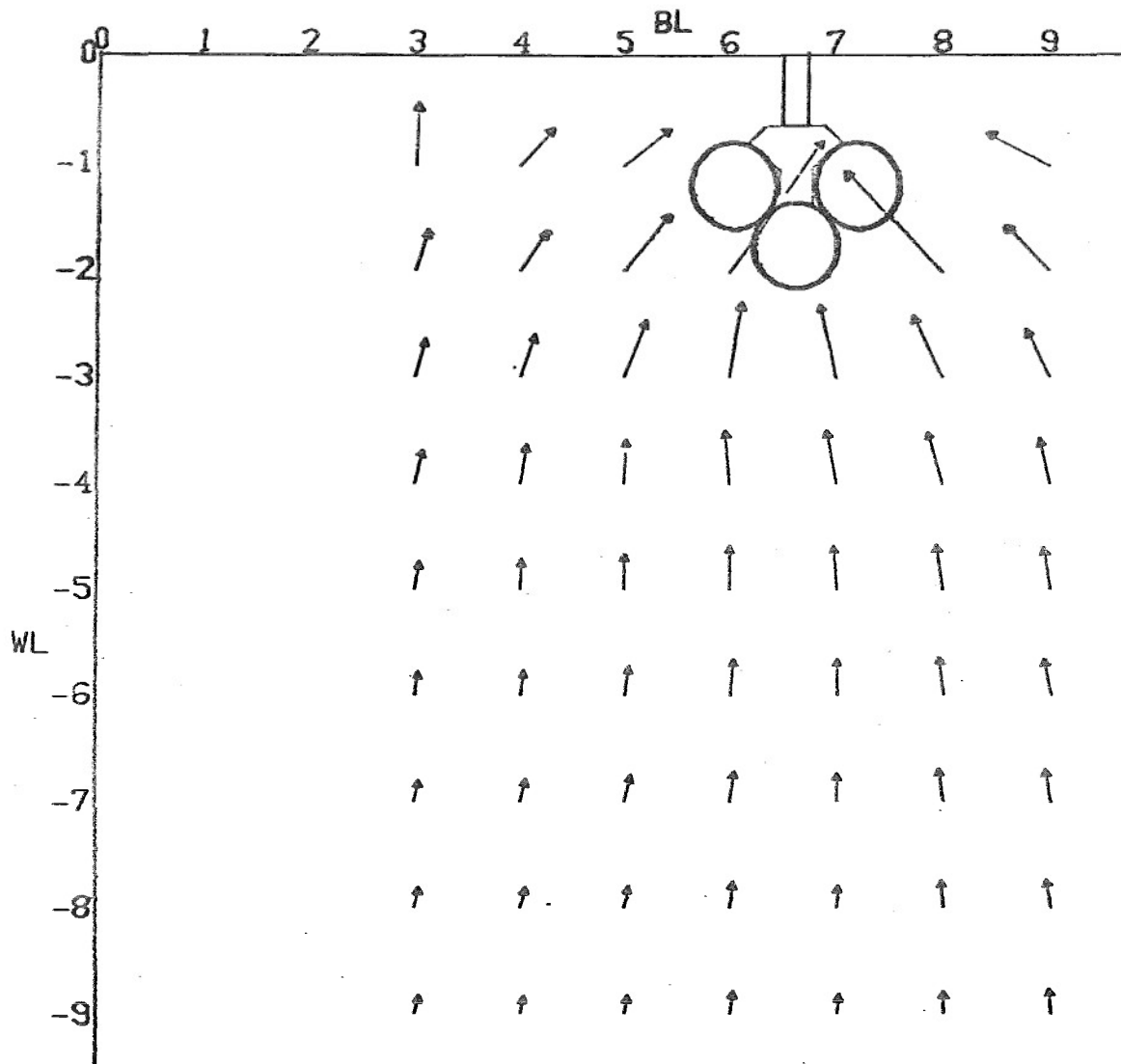
(b) MFS = 17

Figure 18. Continued



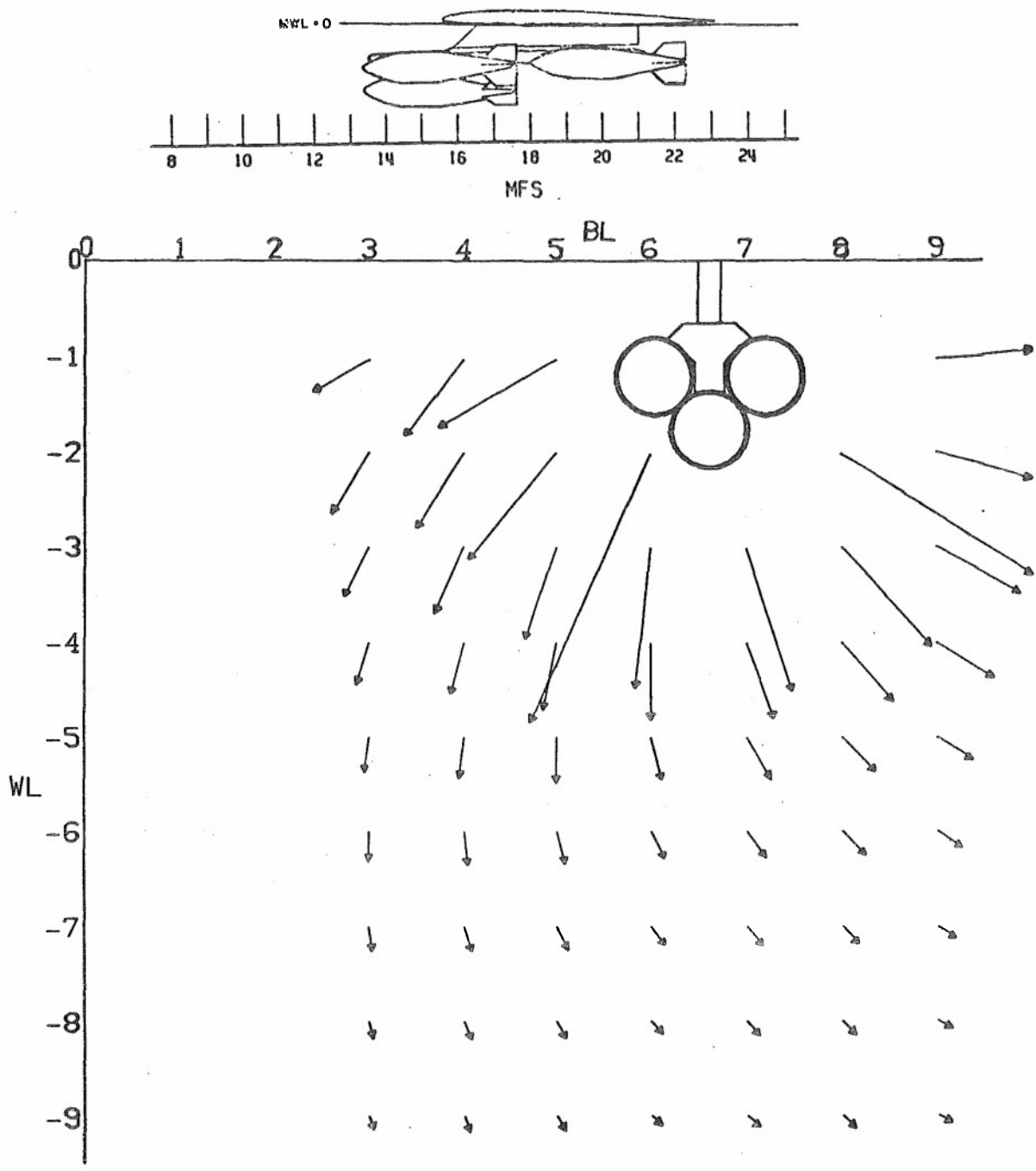
(c) MFS = 19

Figure 18. Continued



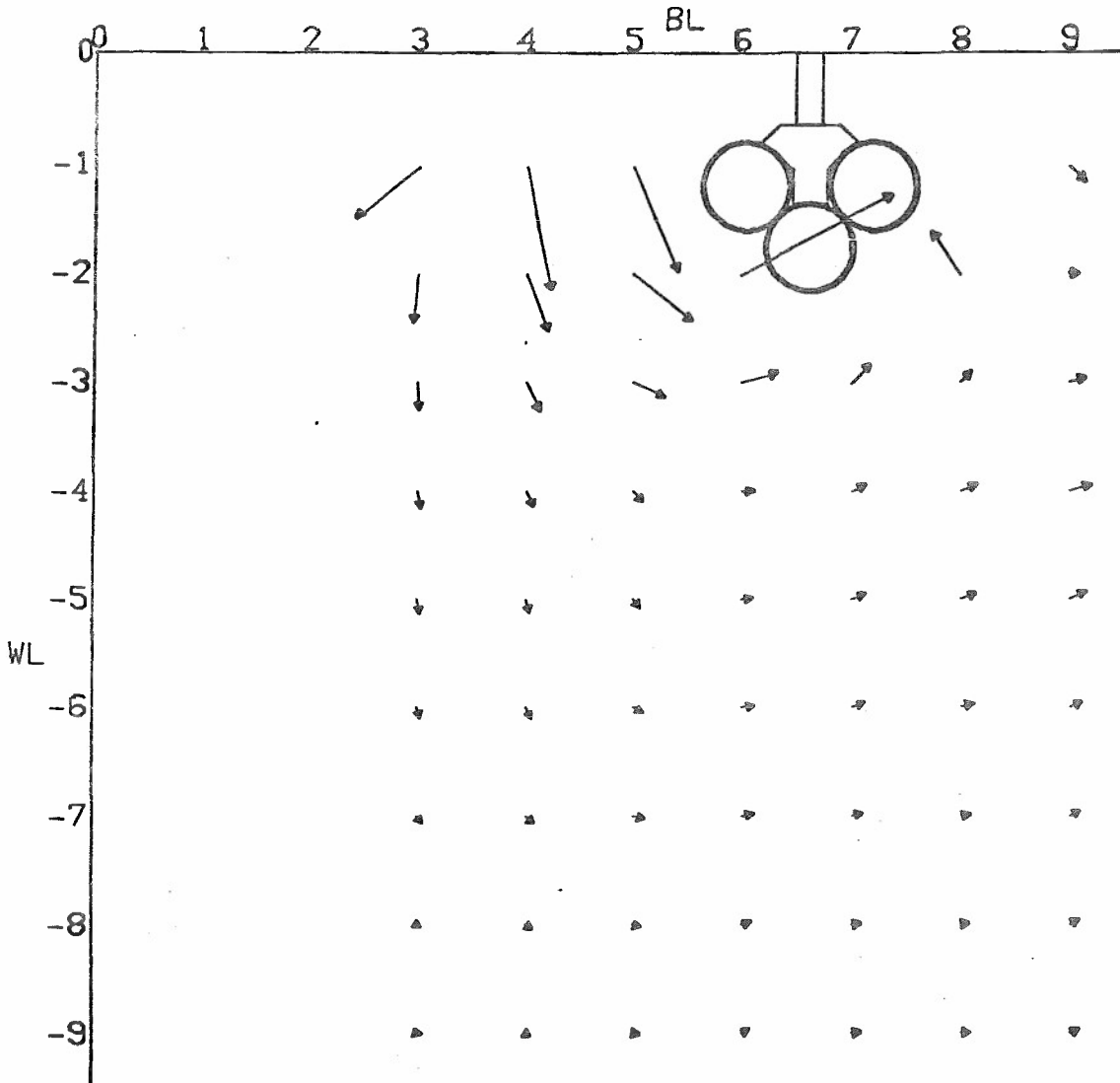
(d) $MFS = 22$

Figure 18. Concluded



(a) MFS = 14

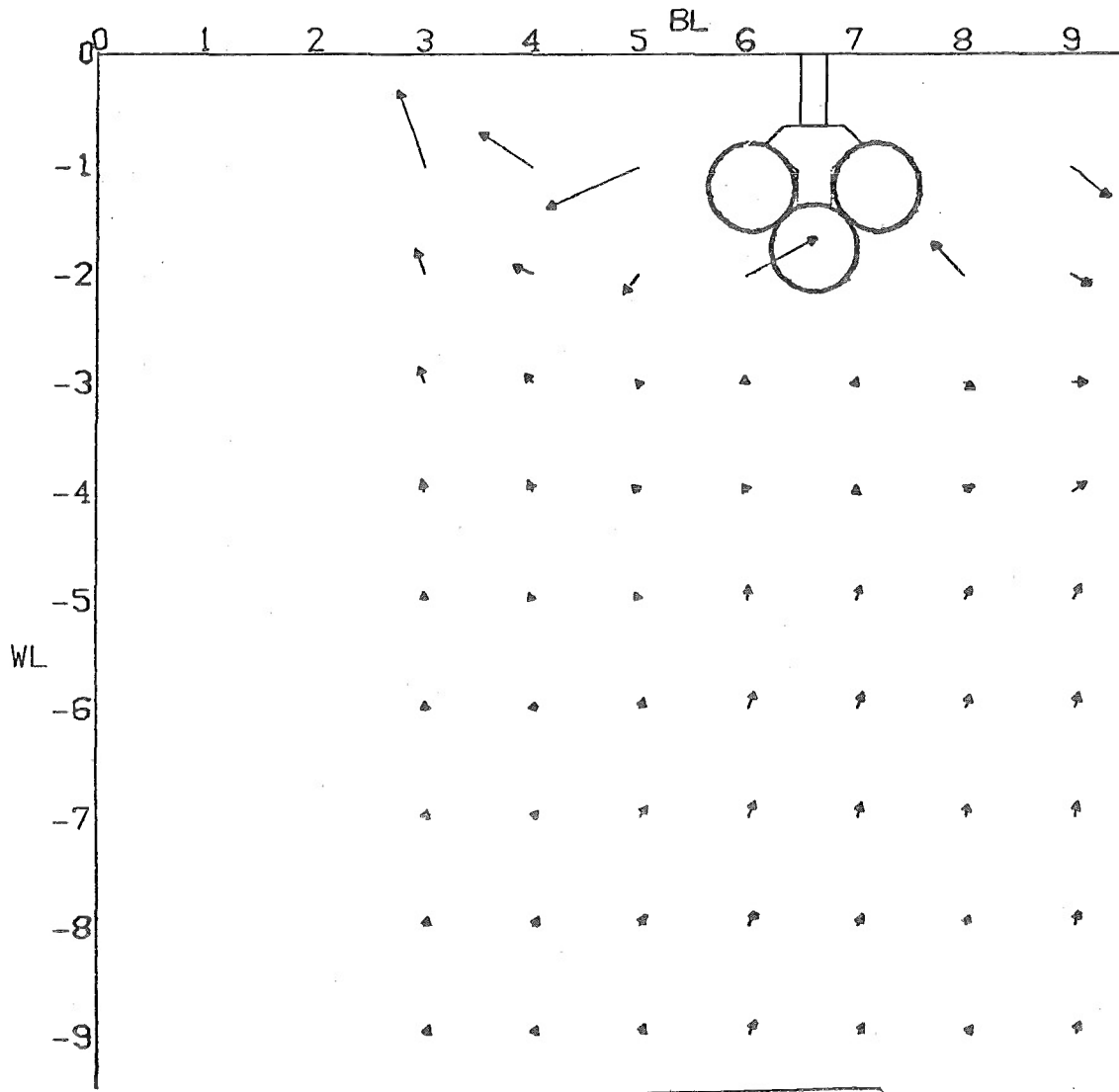
Figure 19. Effect of Five M-117 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



50 FT/SEC

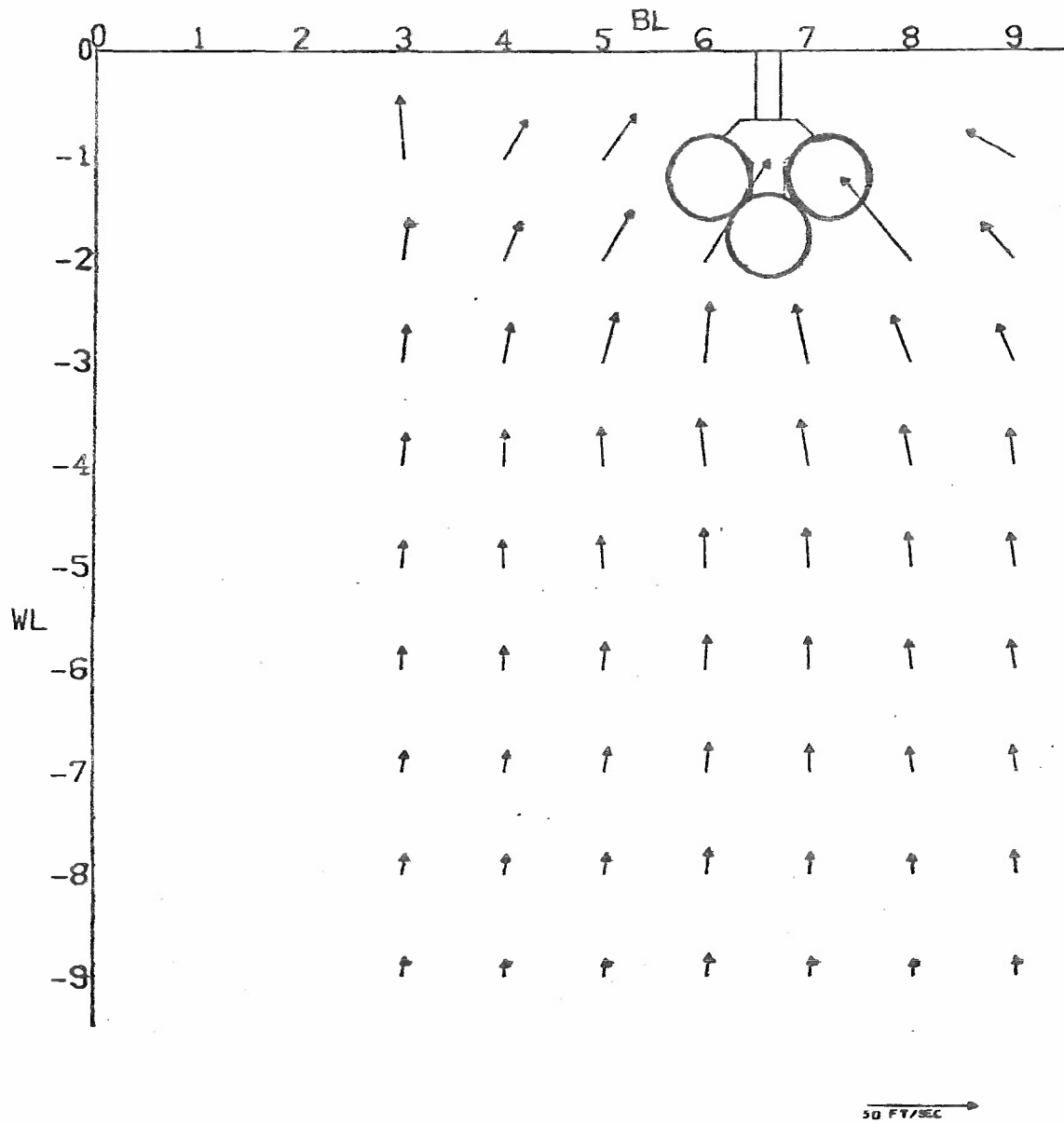
(b) MFS = 17

Figure 19. Continued



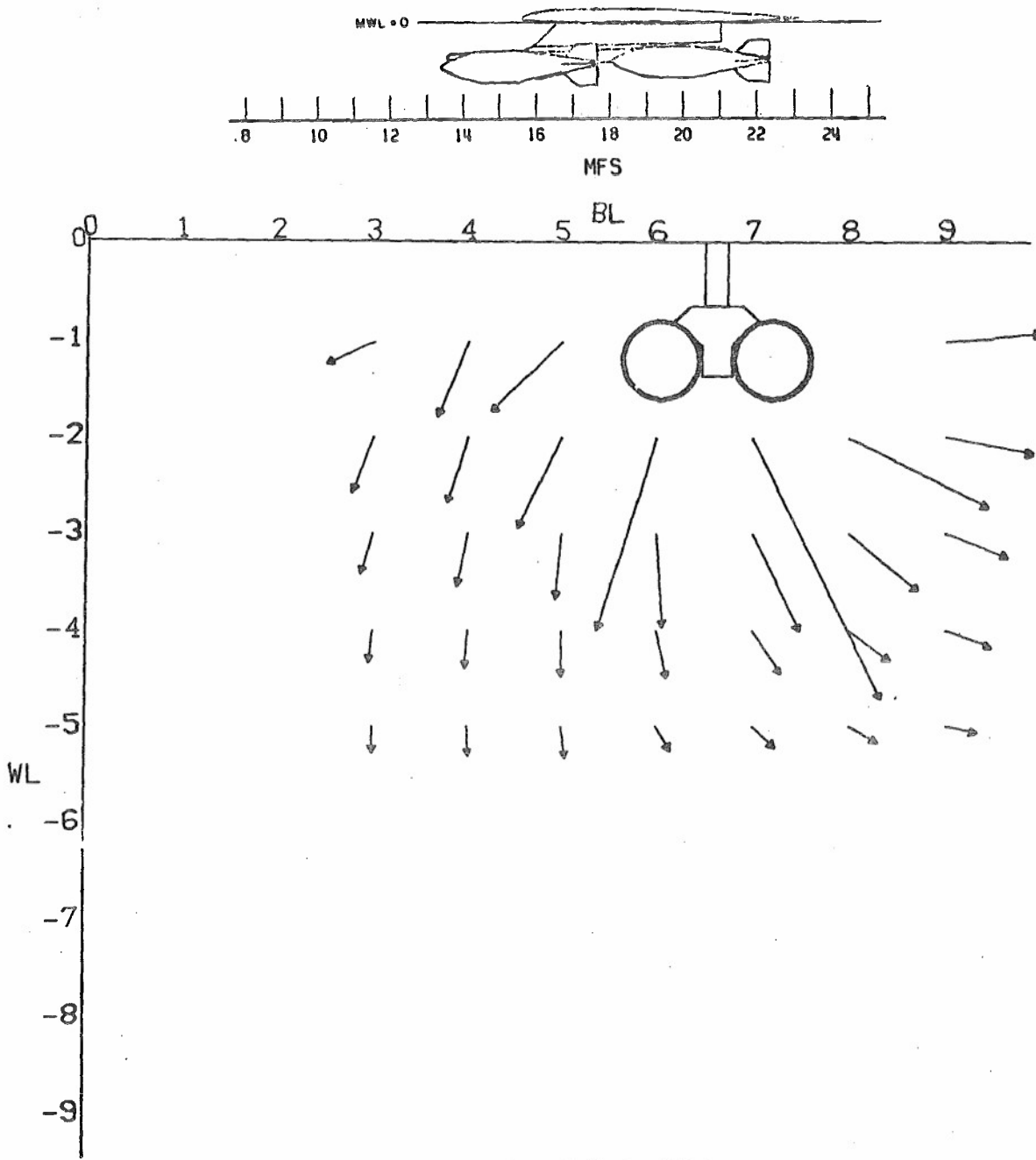
(c) MFS = 19

Figure 19. Continued



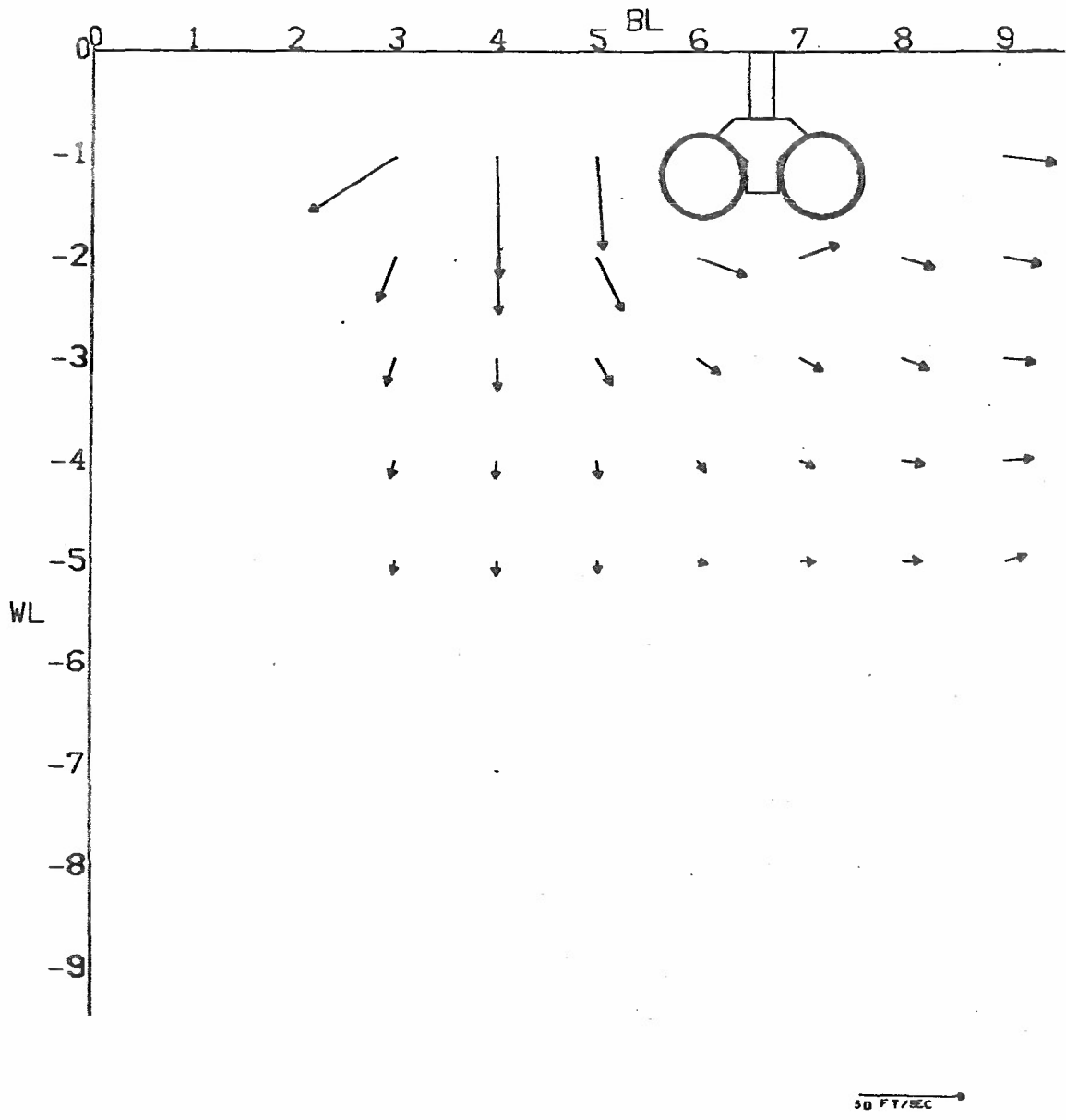
(d) MFS = 22

Figure 19. Concluded



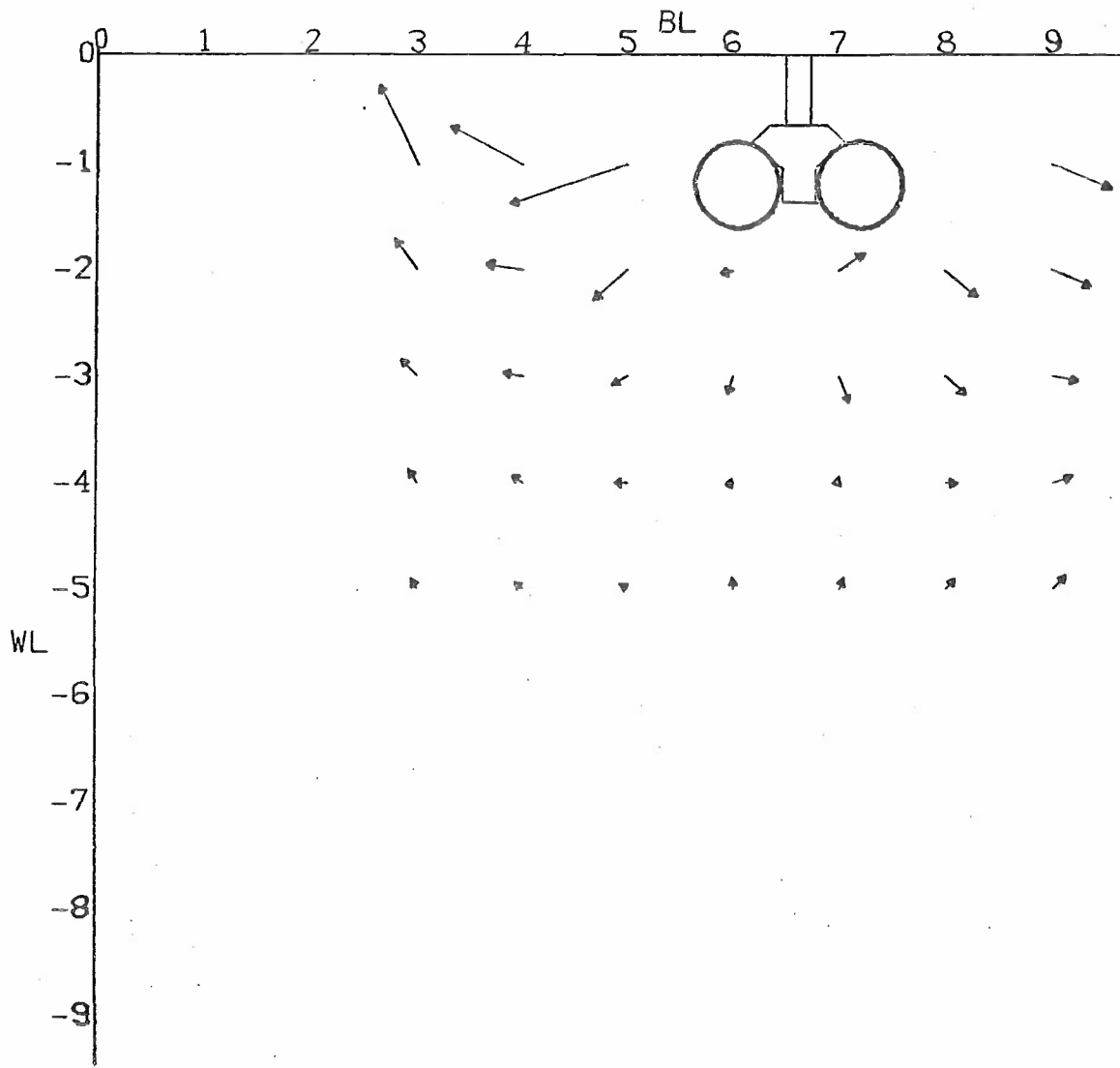
(a) MFS = 14

Figure 20. Effect of Four M-117 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



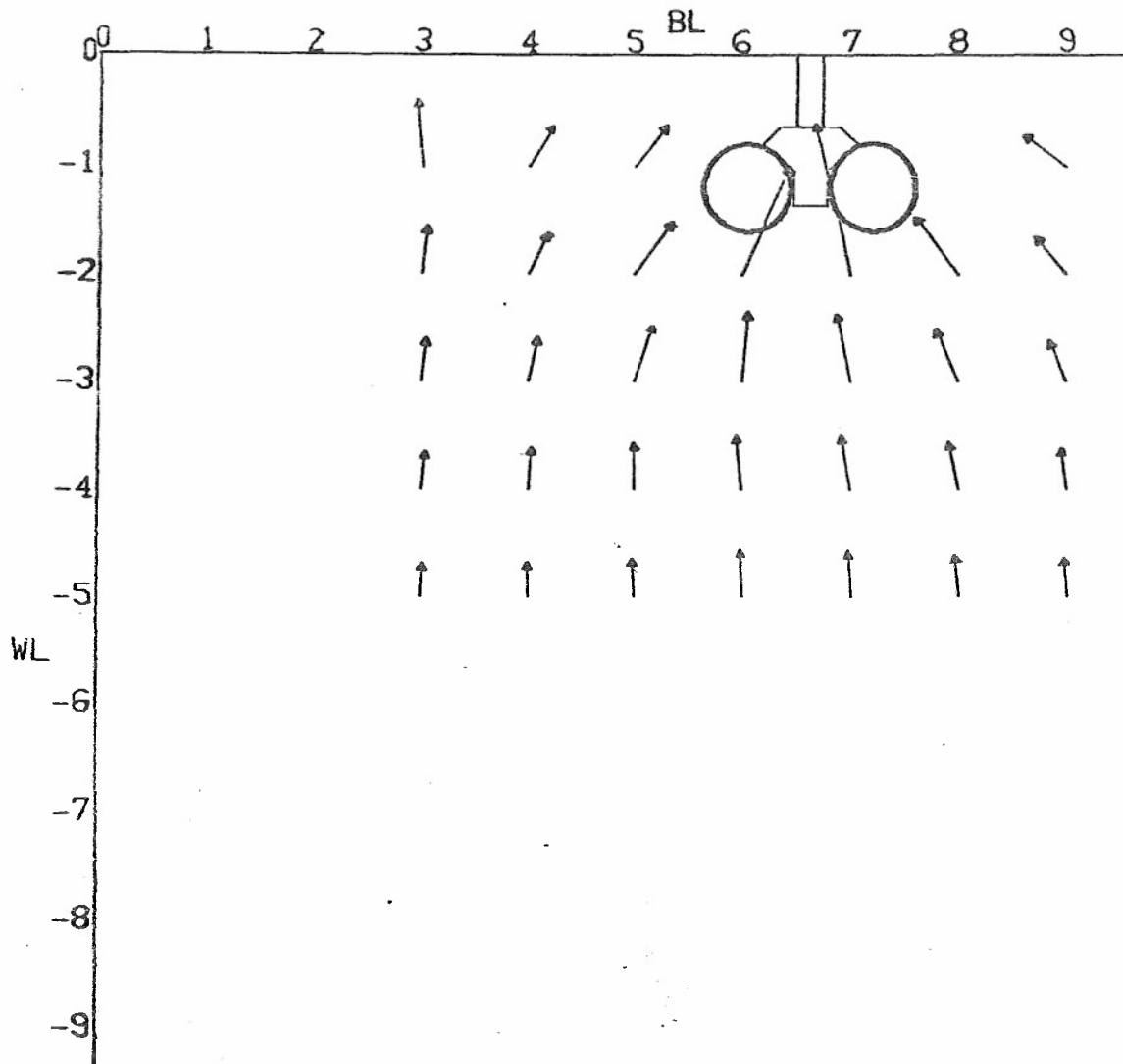
(a) MFS = 17

Figure 20. Continued



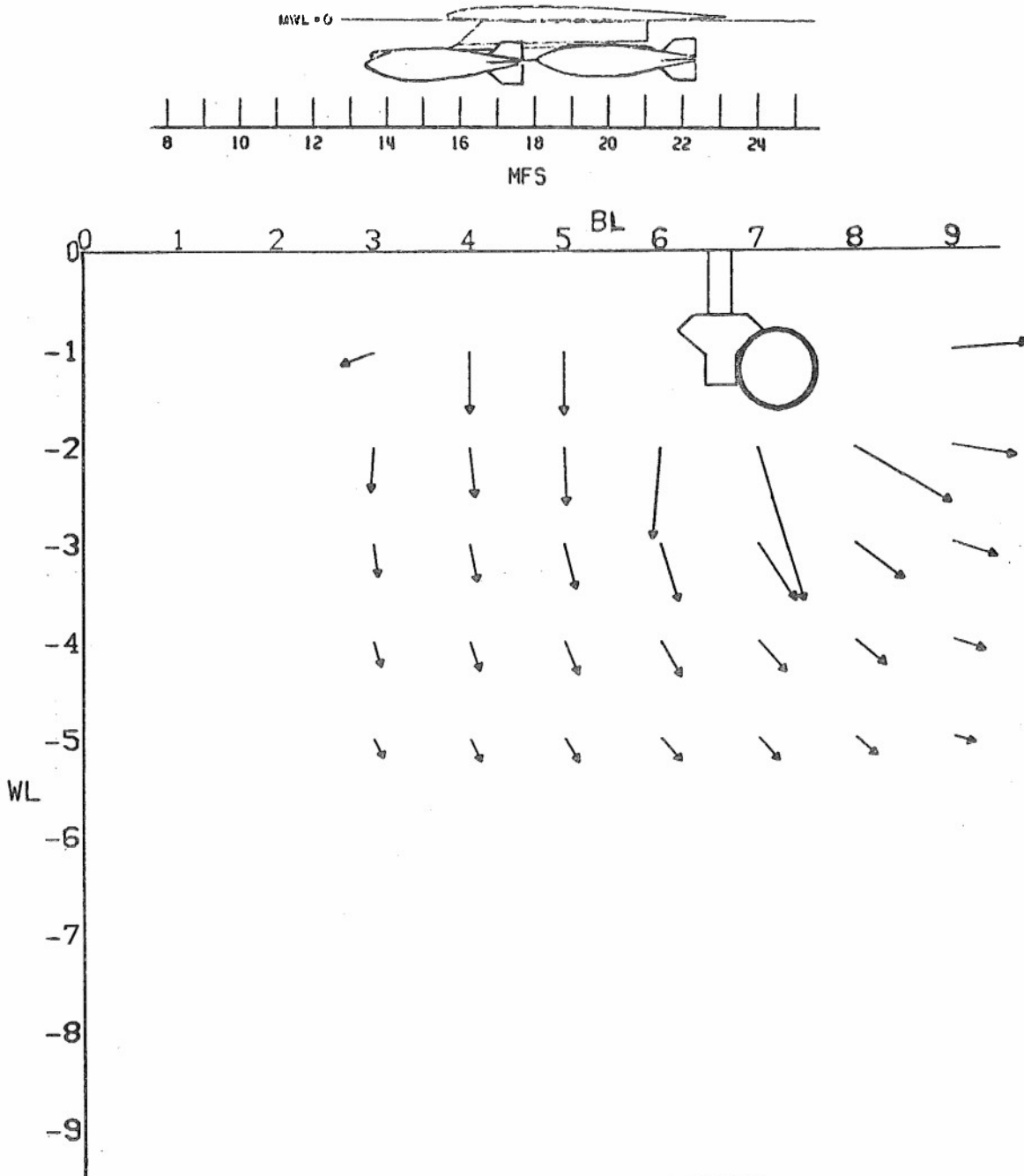
(c) MFS = 19

Figure 20. Continued



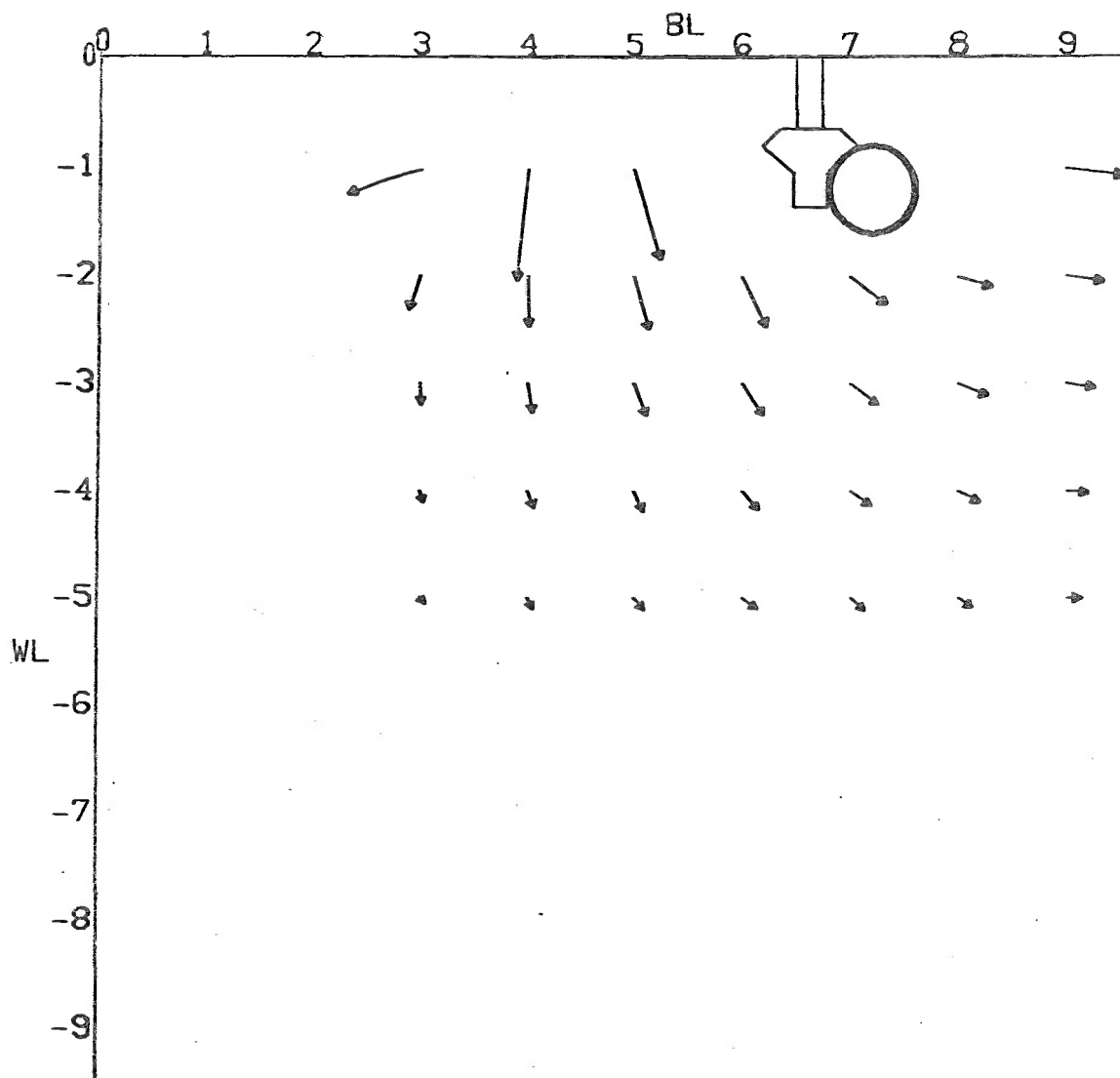
(d) MFS = 22

Figure 20. Concluded



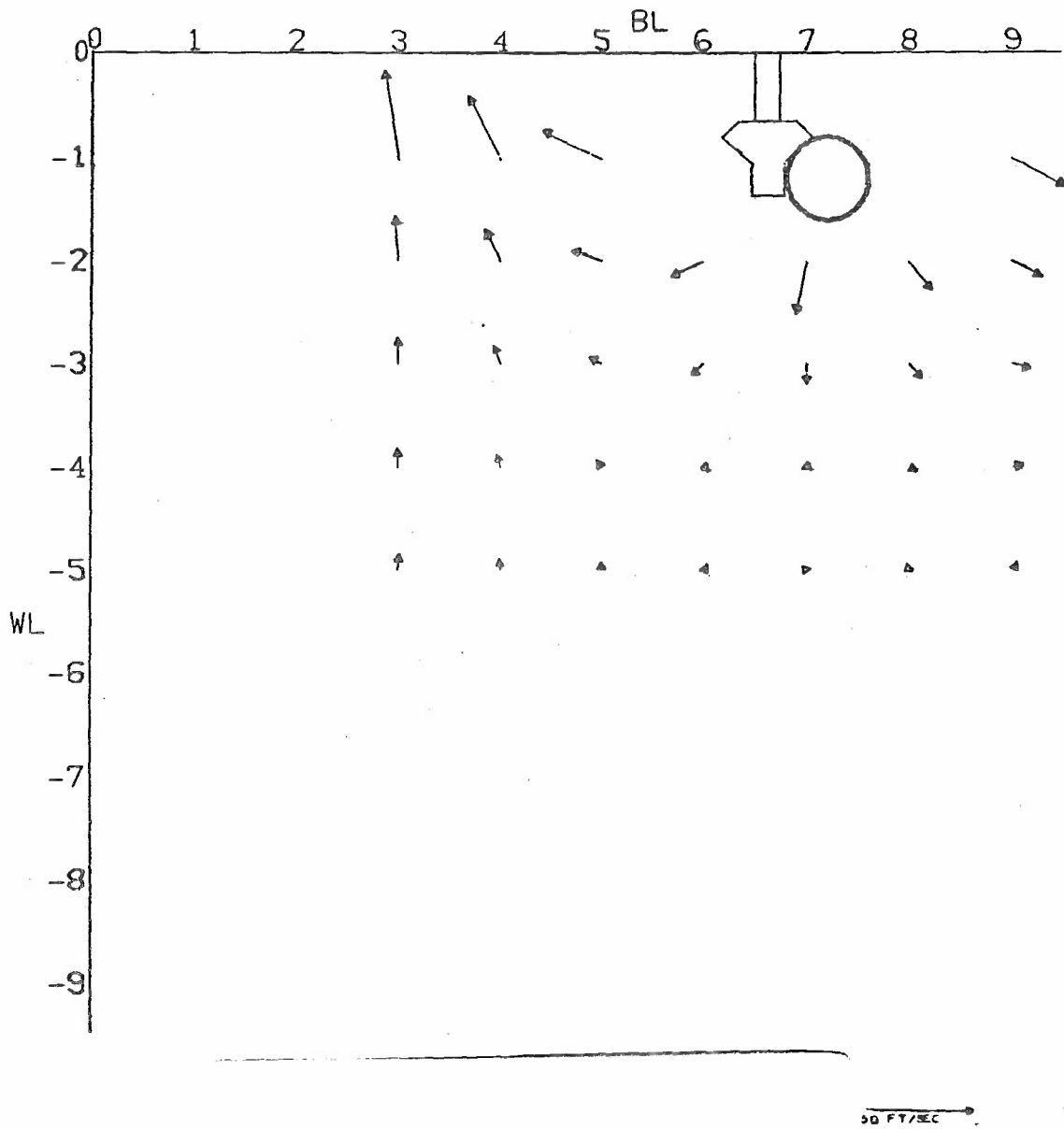
(a) MFS = 14

Figure 21. Effect of Two M-117 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



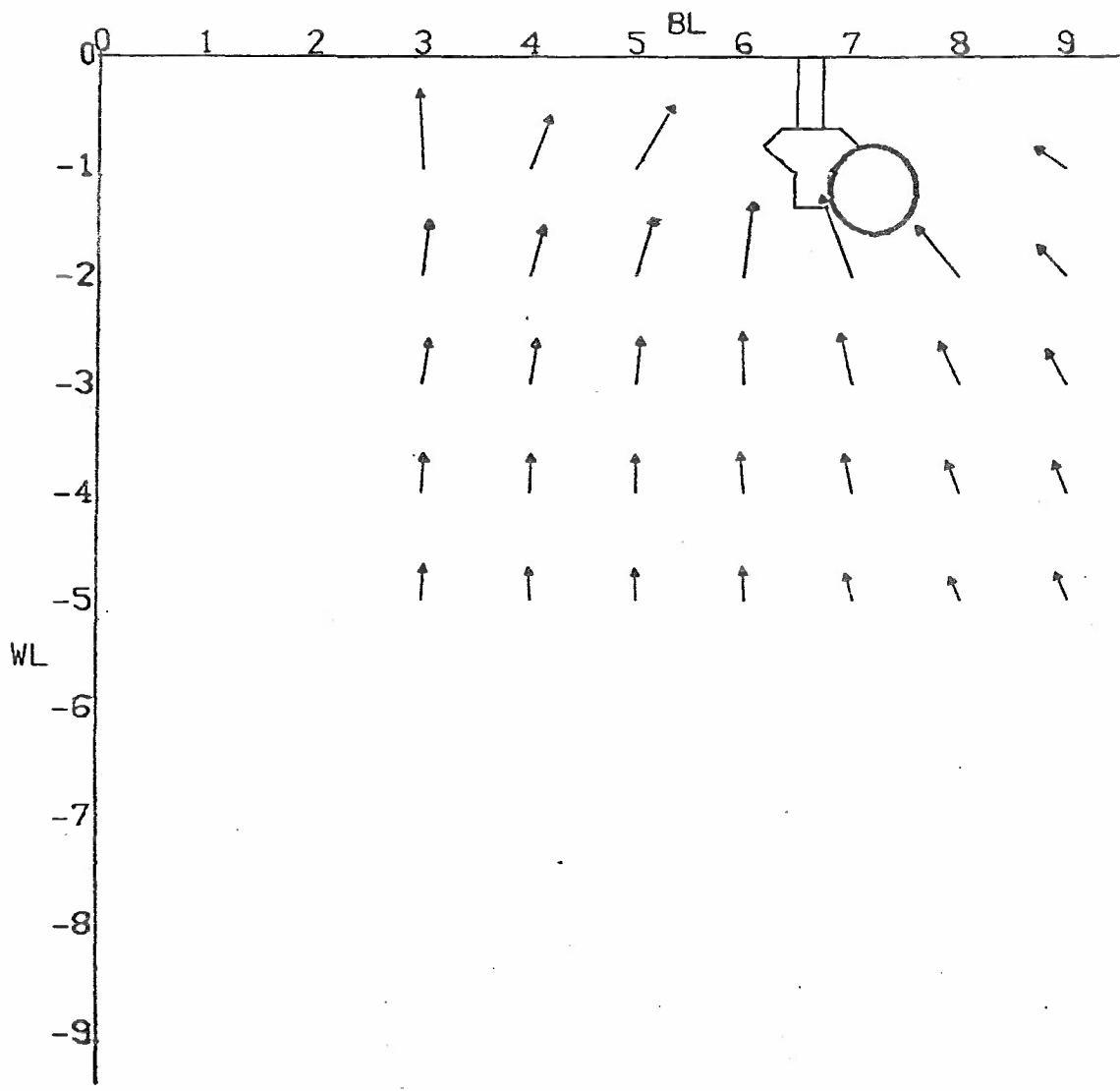
(b) MFS = 17

Figure 21. Continued



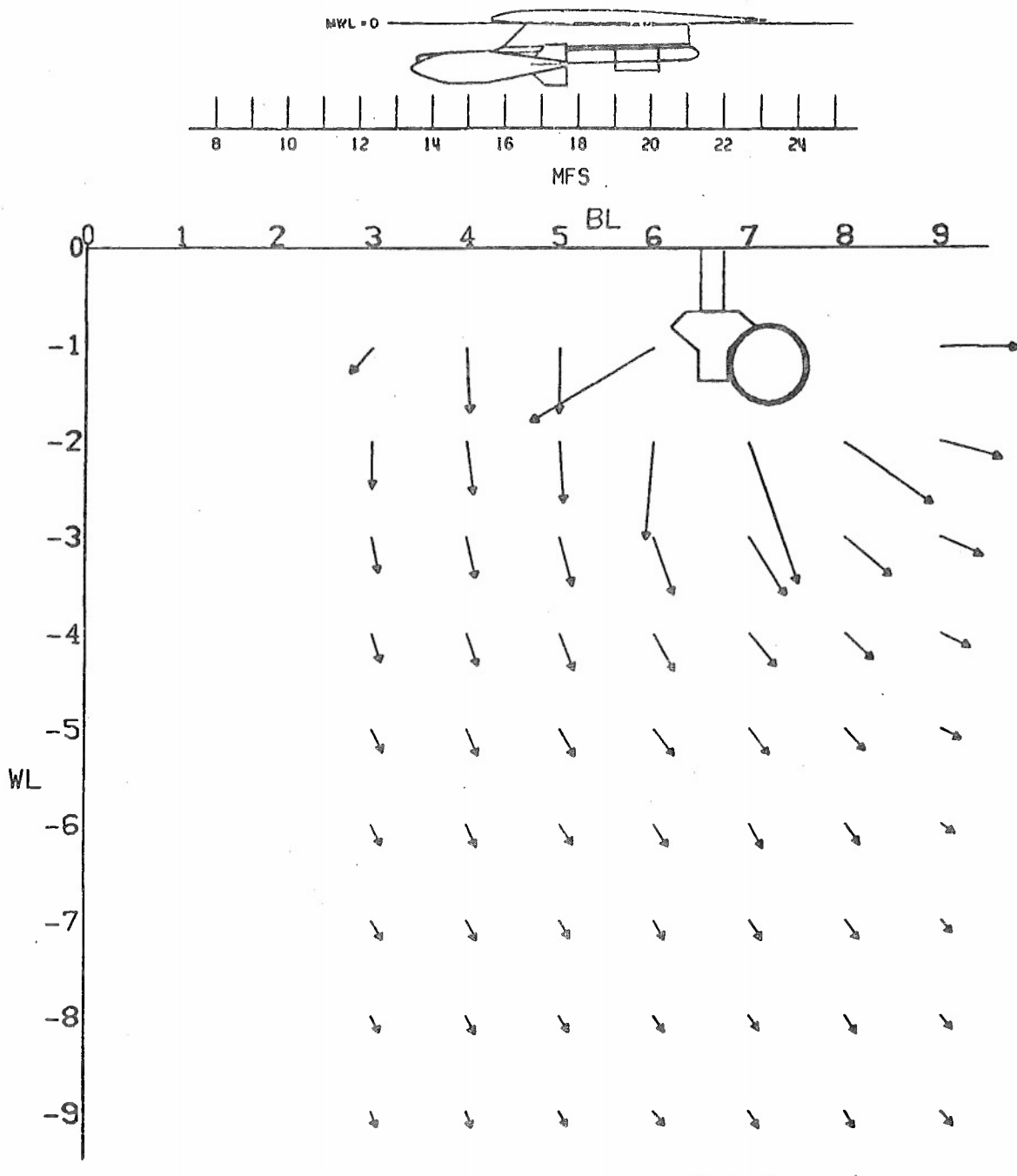
(c) MFS = 19

Figure 21. Continued



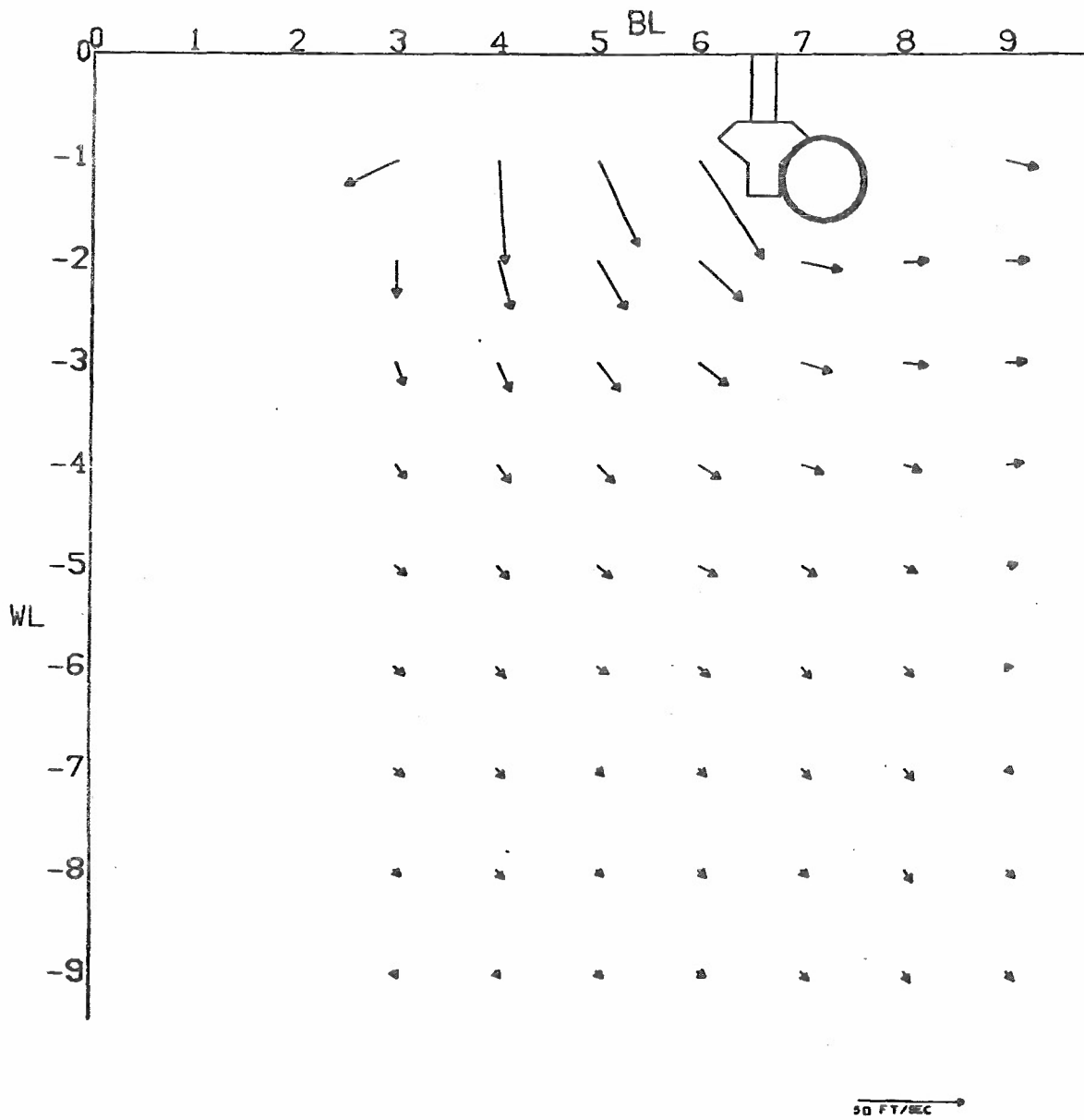
(d) MFS = 22

Figure 21. Concluded

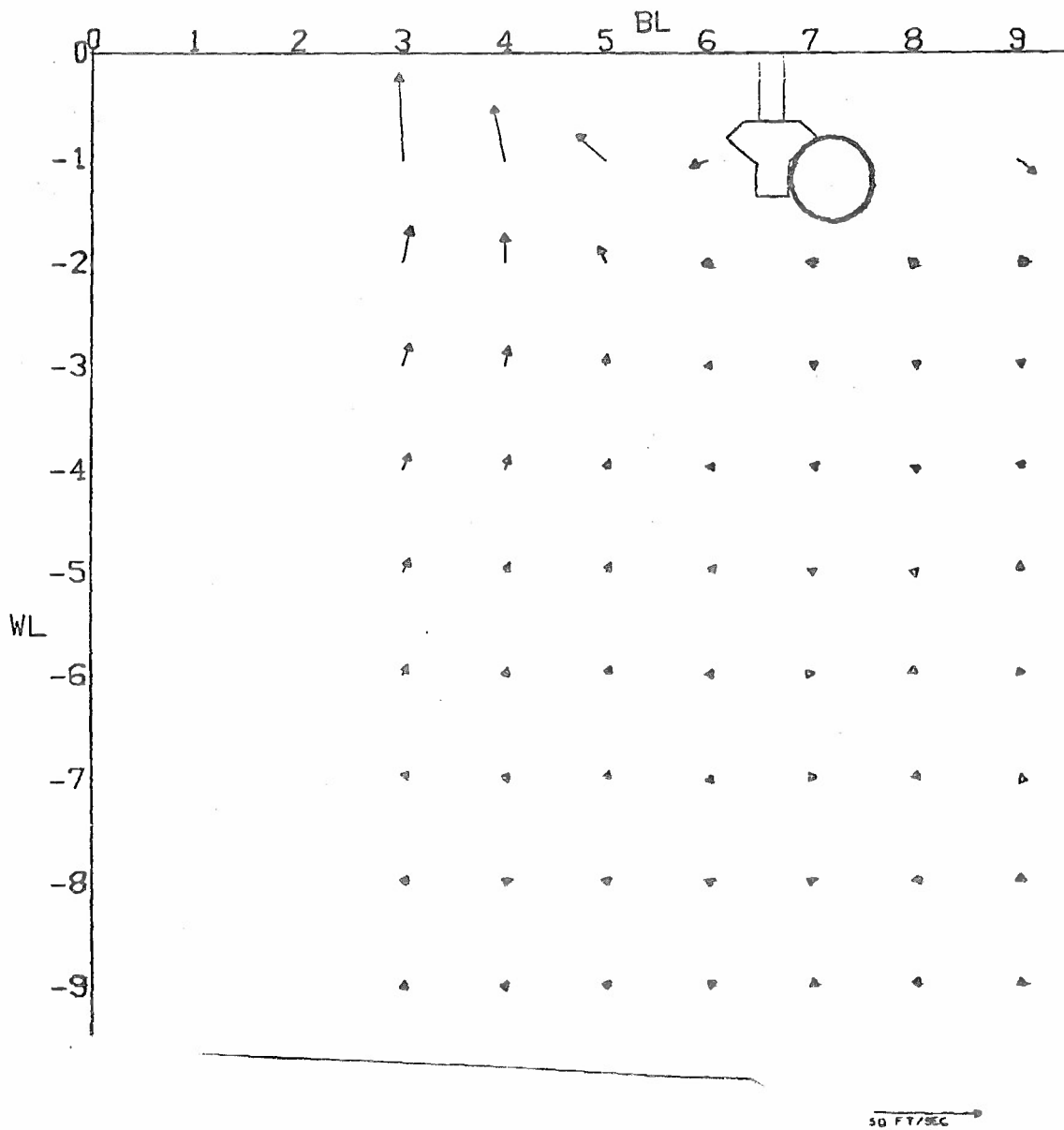


(a) MFS = 14

Figure 22. Effect of One M-117 Bomb and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

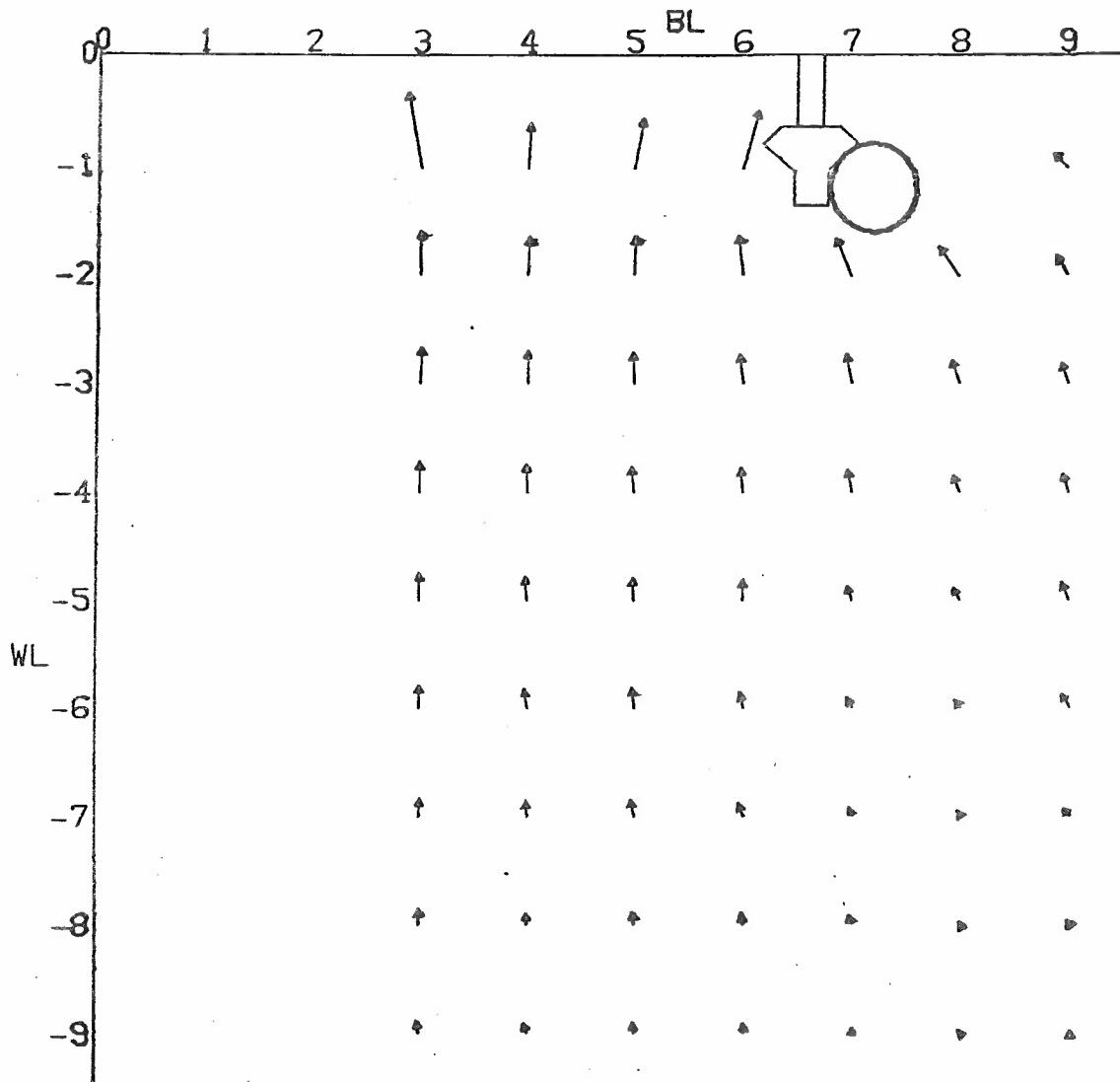


(b) MFS = 17
 Figure 22. Continued



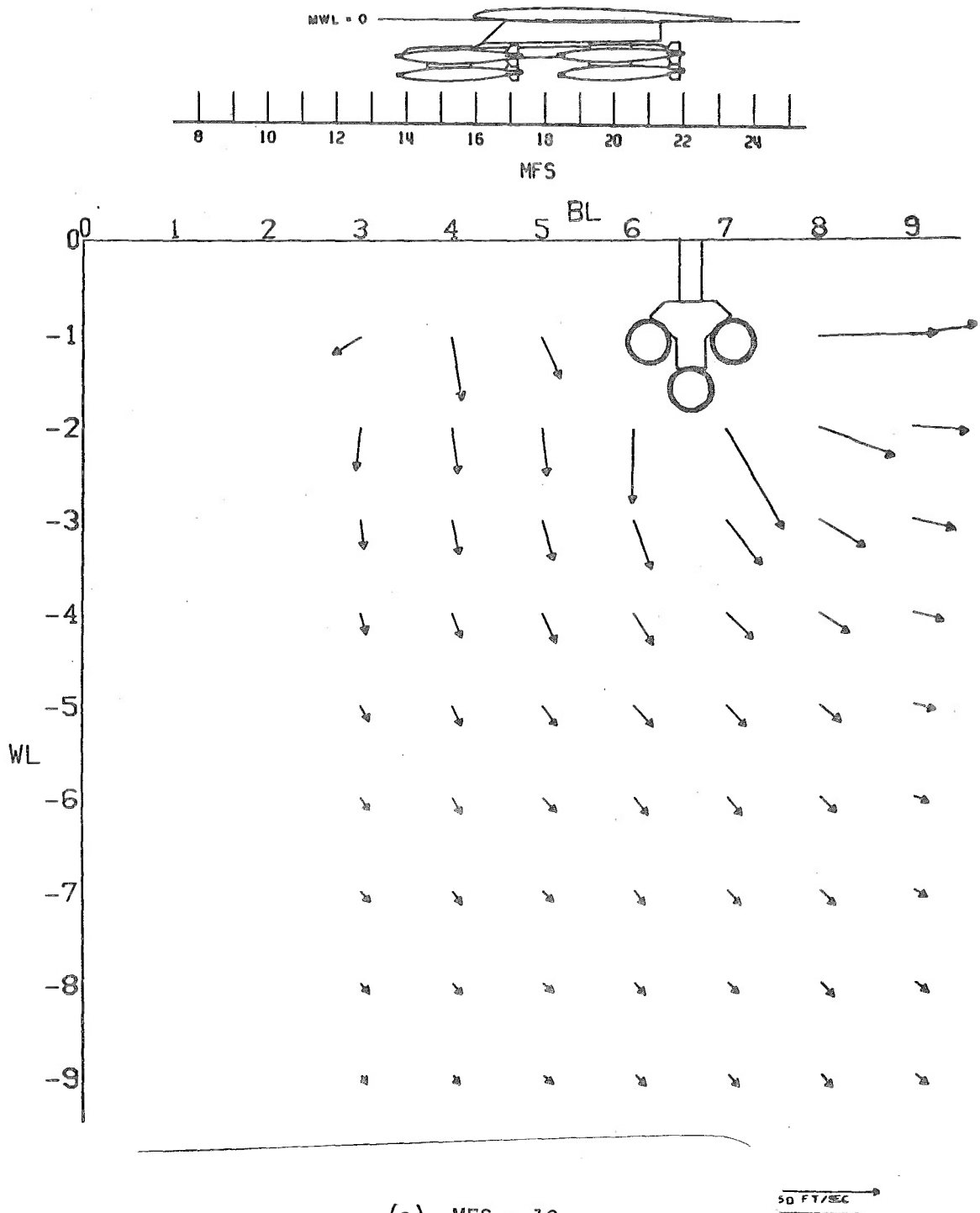
(c) MFS = 19

Figure 22. Continued



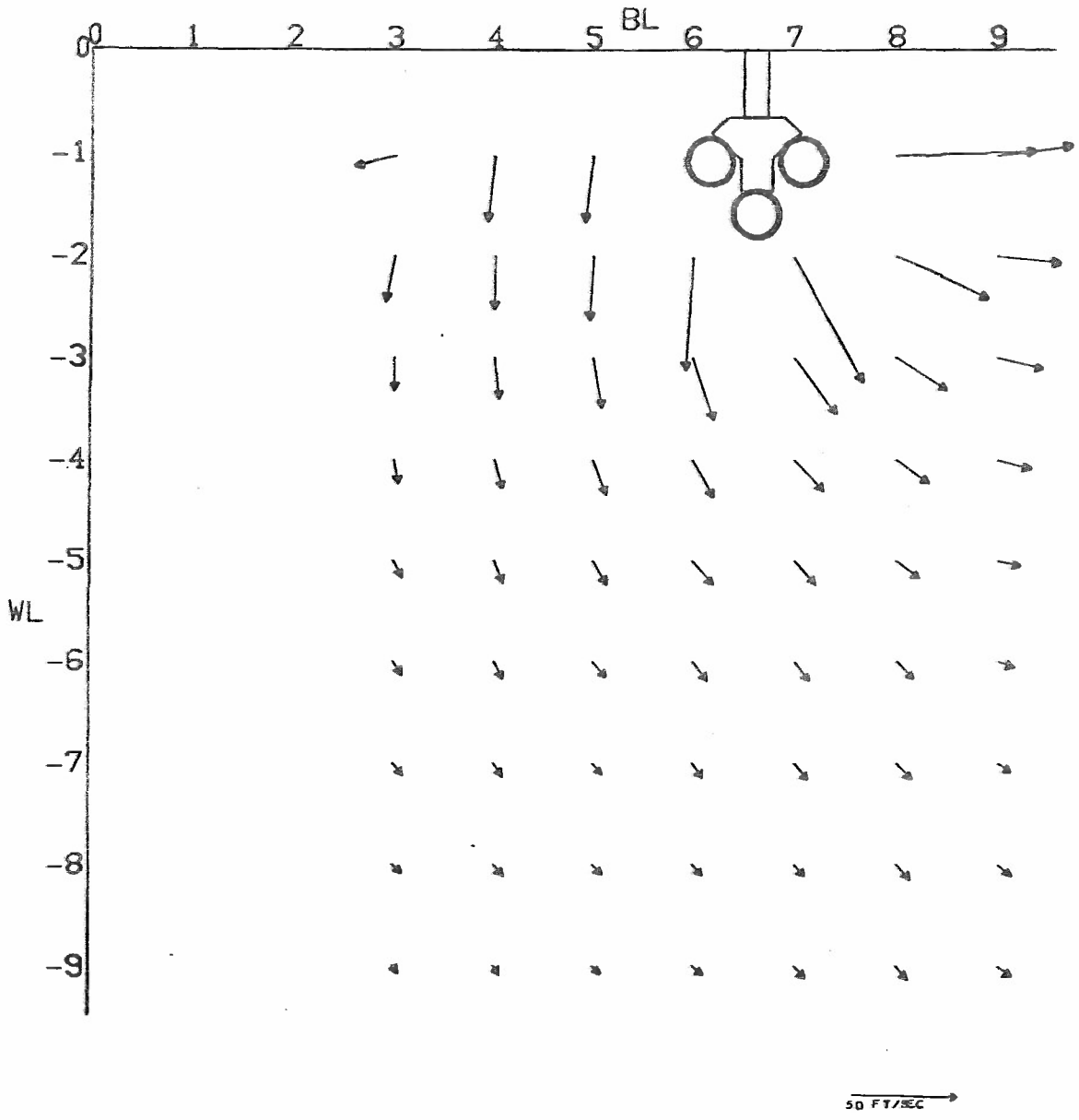
(d) MFS = 22

Figure 22. Concluded



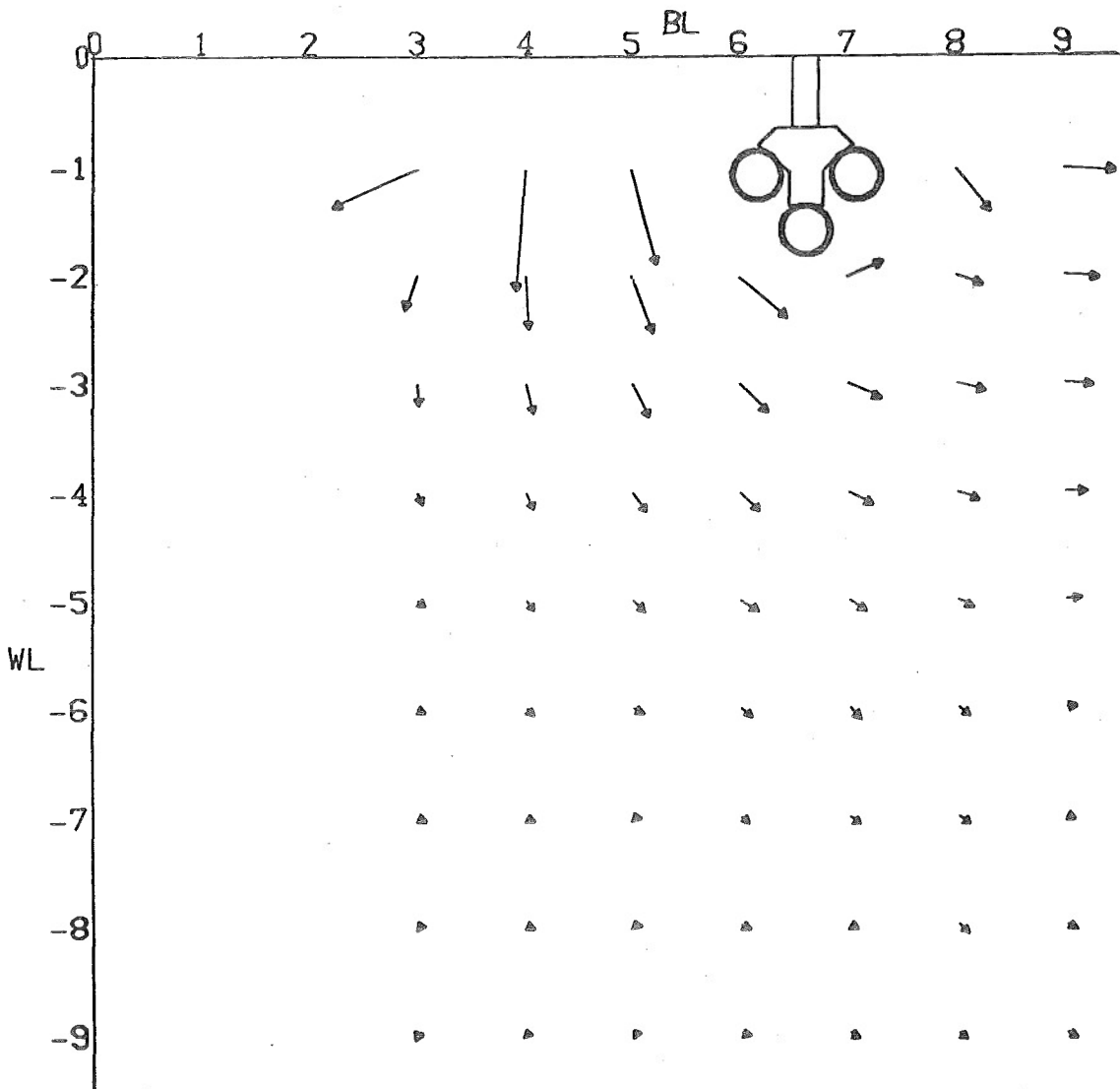
(a) MFS = 13

Figure 23. Effect of Six MK-81 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$



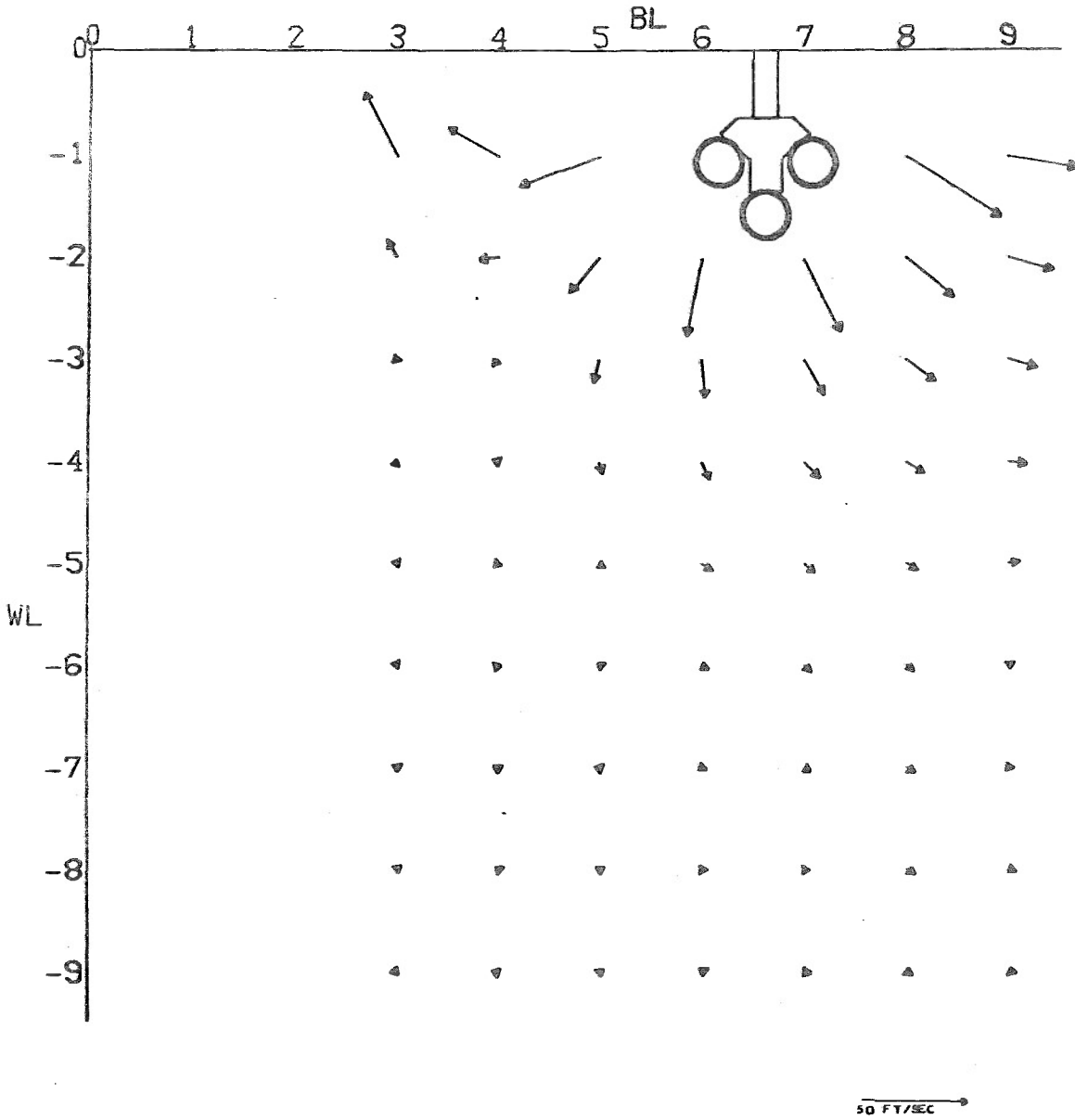
(b) MFS = 14

Figure 23. Continued



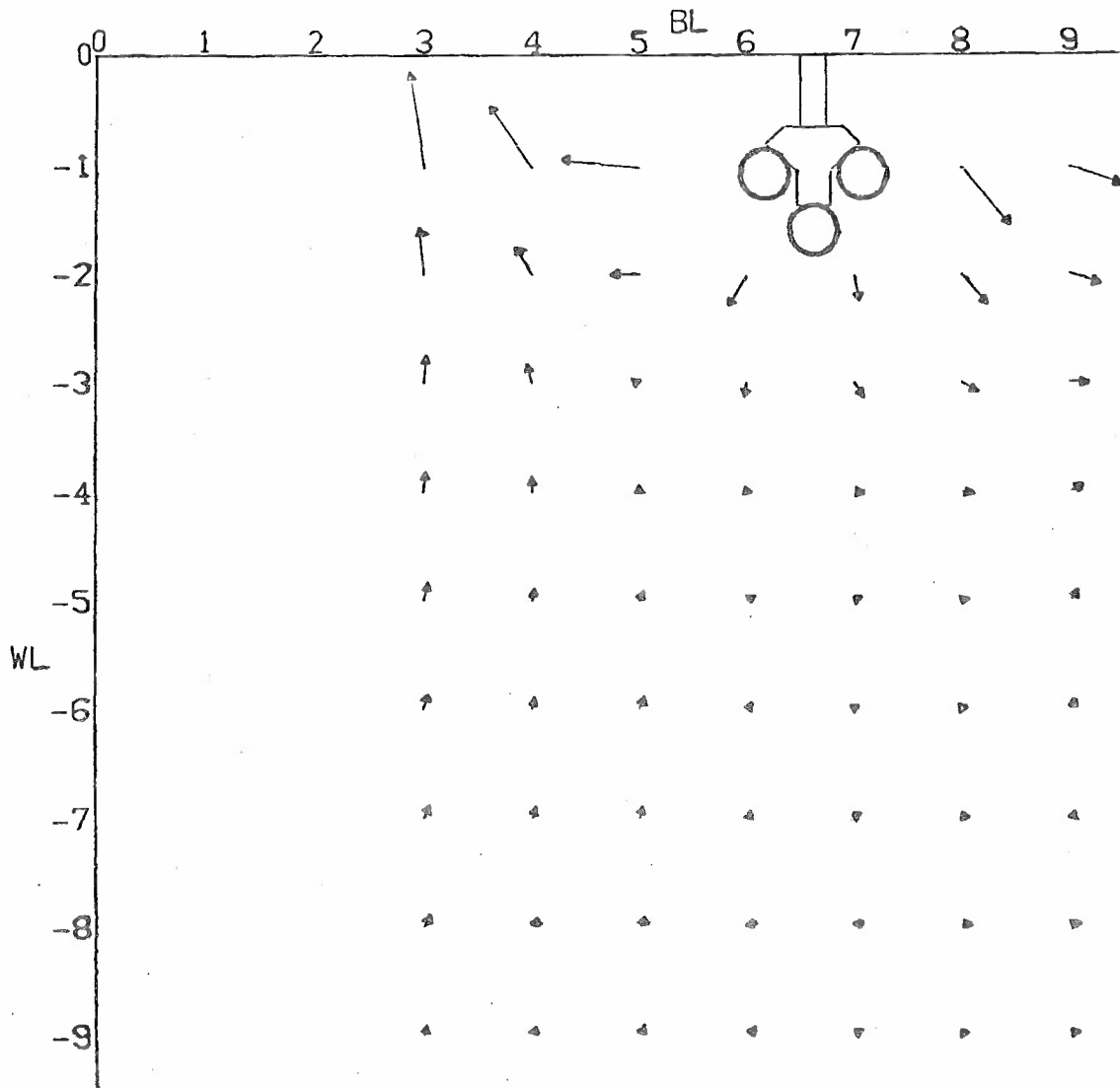
(c) MFS = 17

Figure 23. Continued



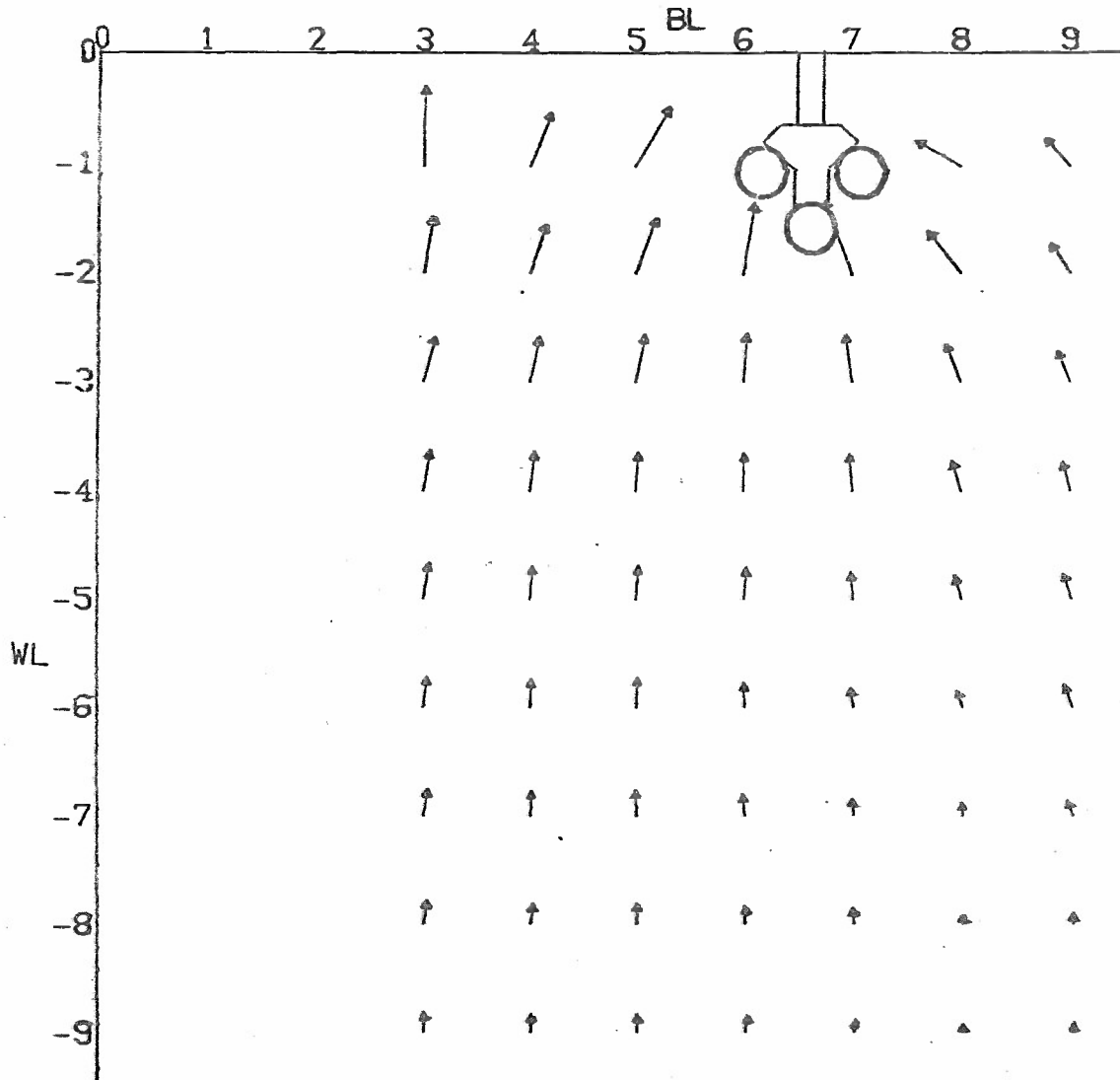
(d) MFS = 18

Figure 23. Continued

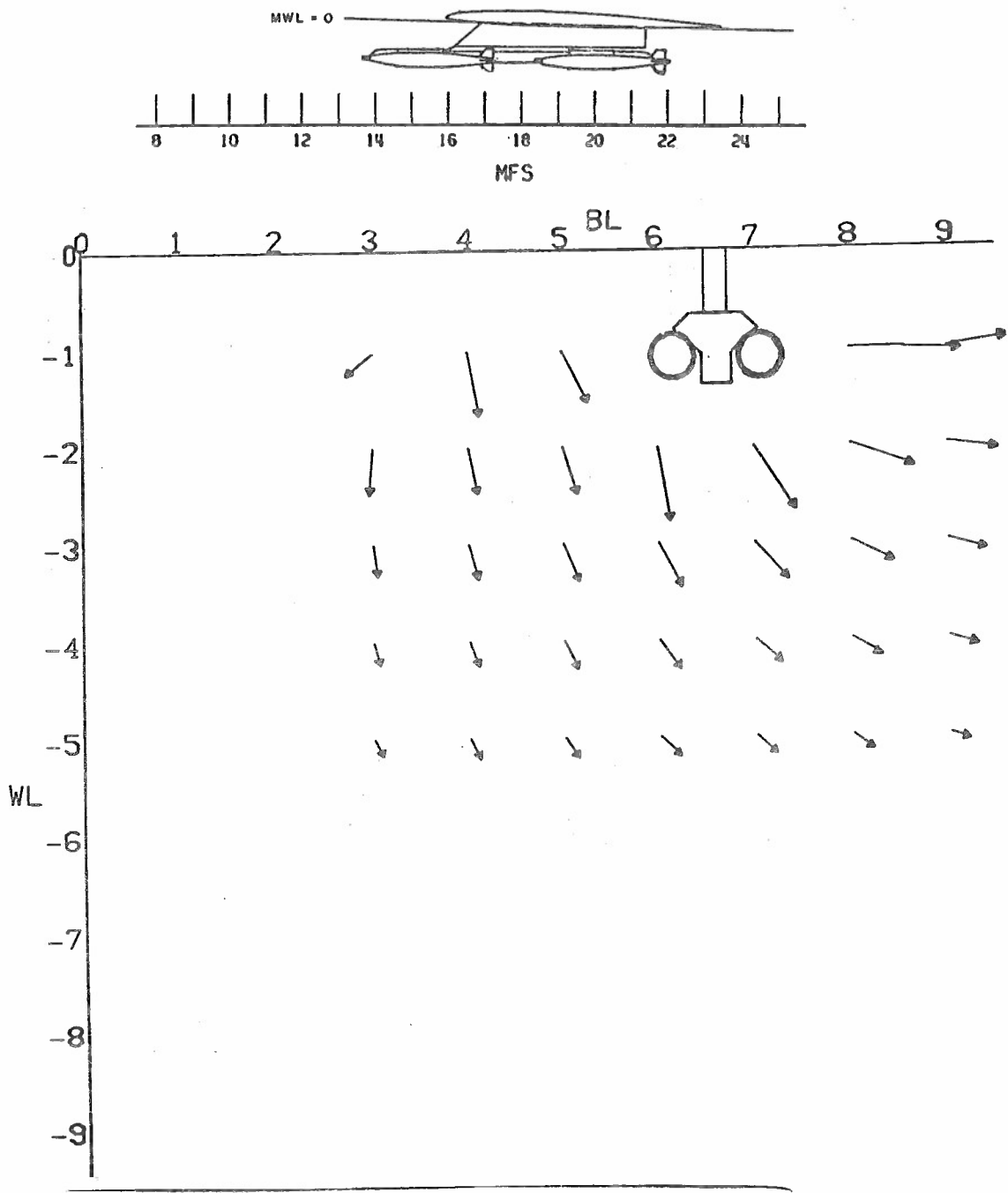


(e) MFS = 19

Figure 23. Continued



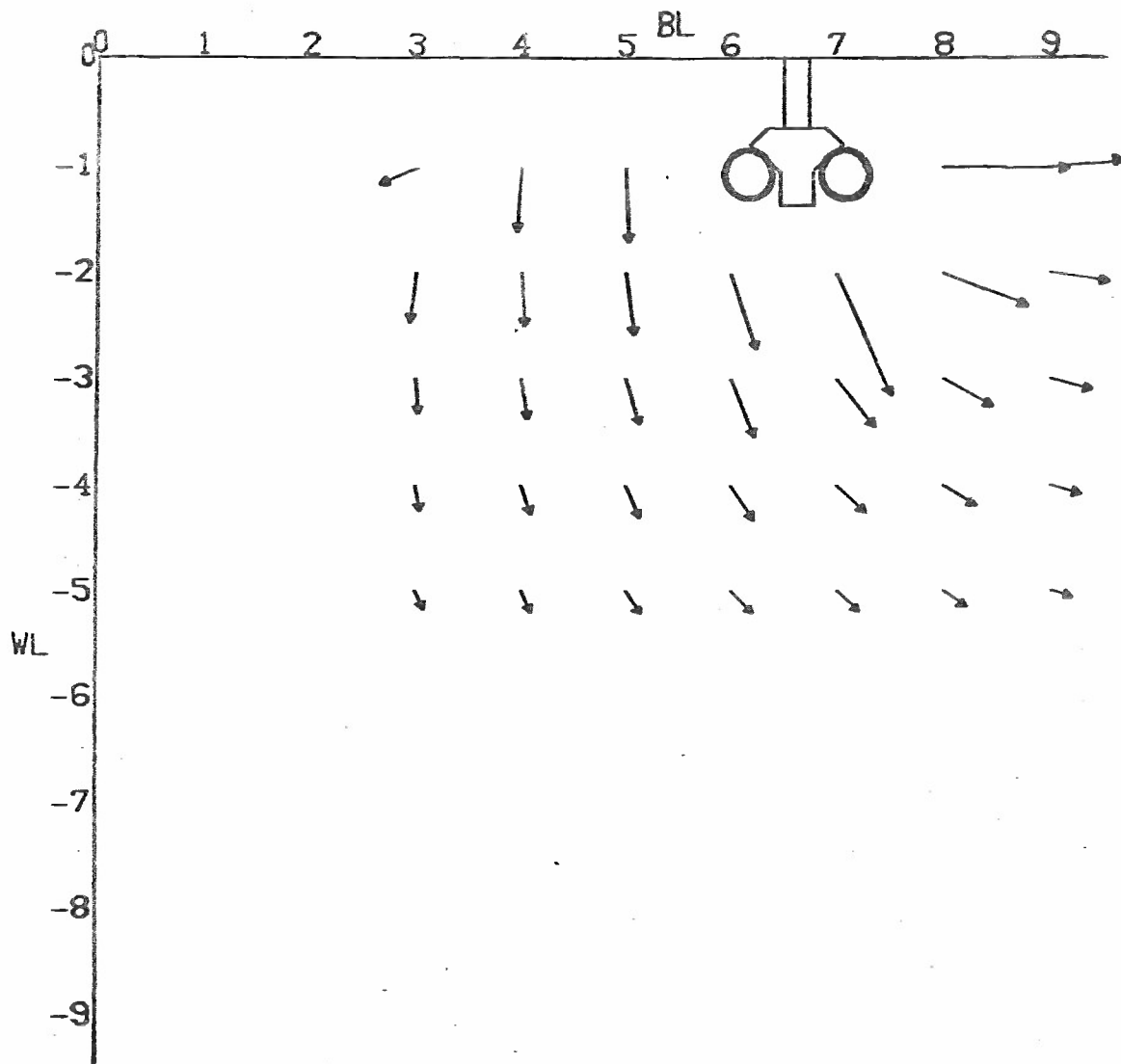
(f) MFS = 22
 Figure 23. Concluded



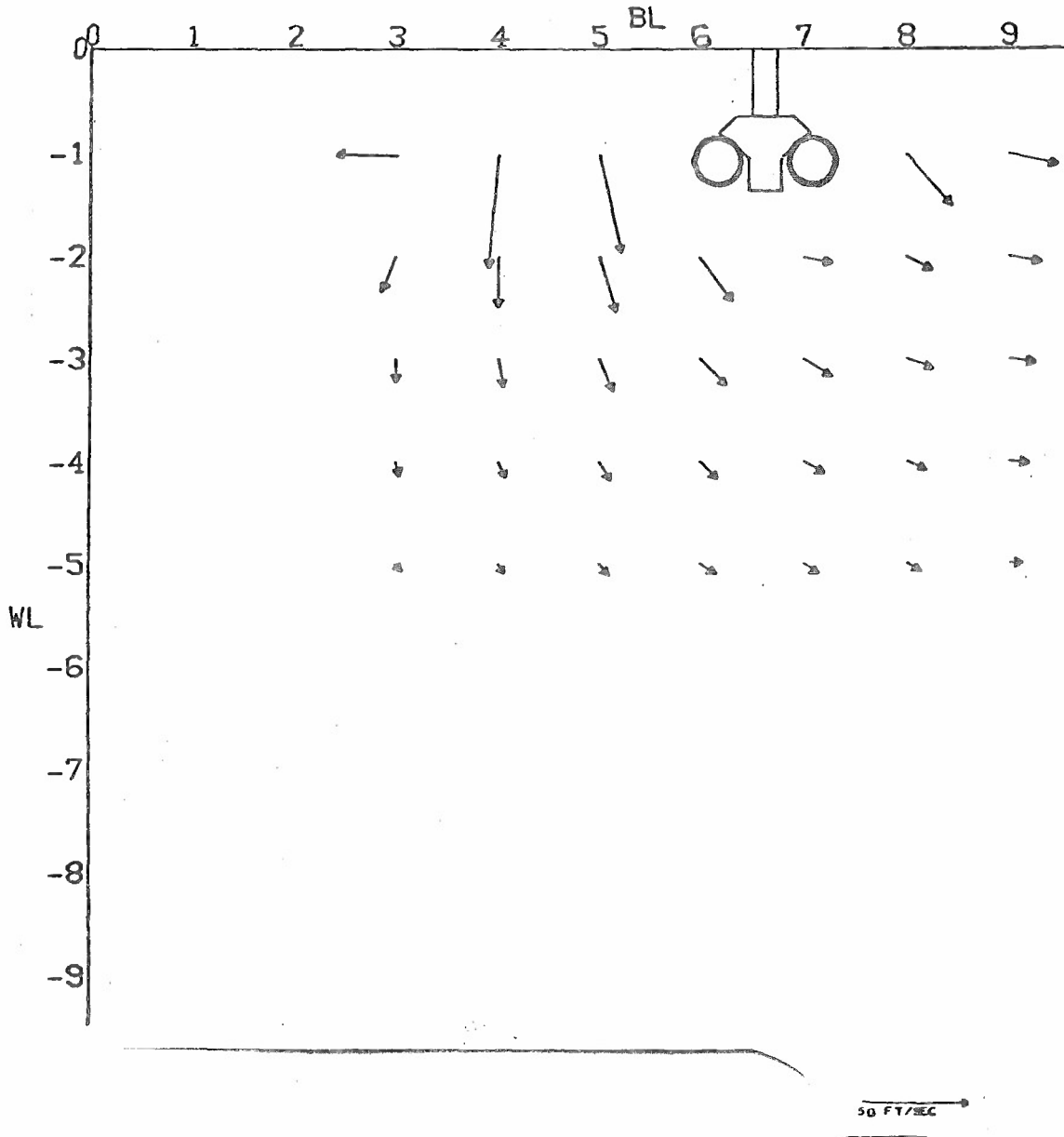
(a) MFS = 13

50 FT/SEC

Figure 24. Effect of Four MK-81 Bombs and Outboard MER on the Transverse Velocity Components of the Flow Field at $M_\infty = 0.85$, $V_\infty = 935$, $\alpha_p = 0.3$

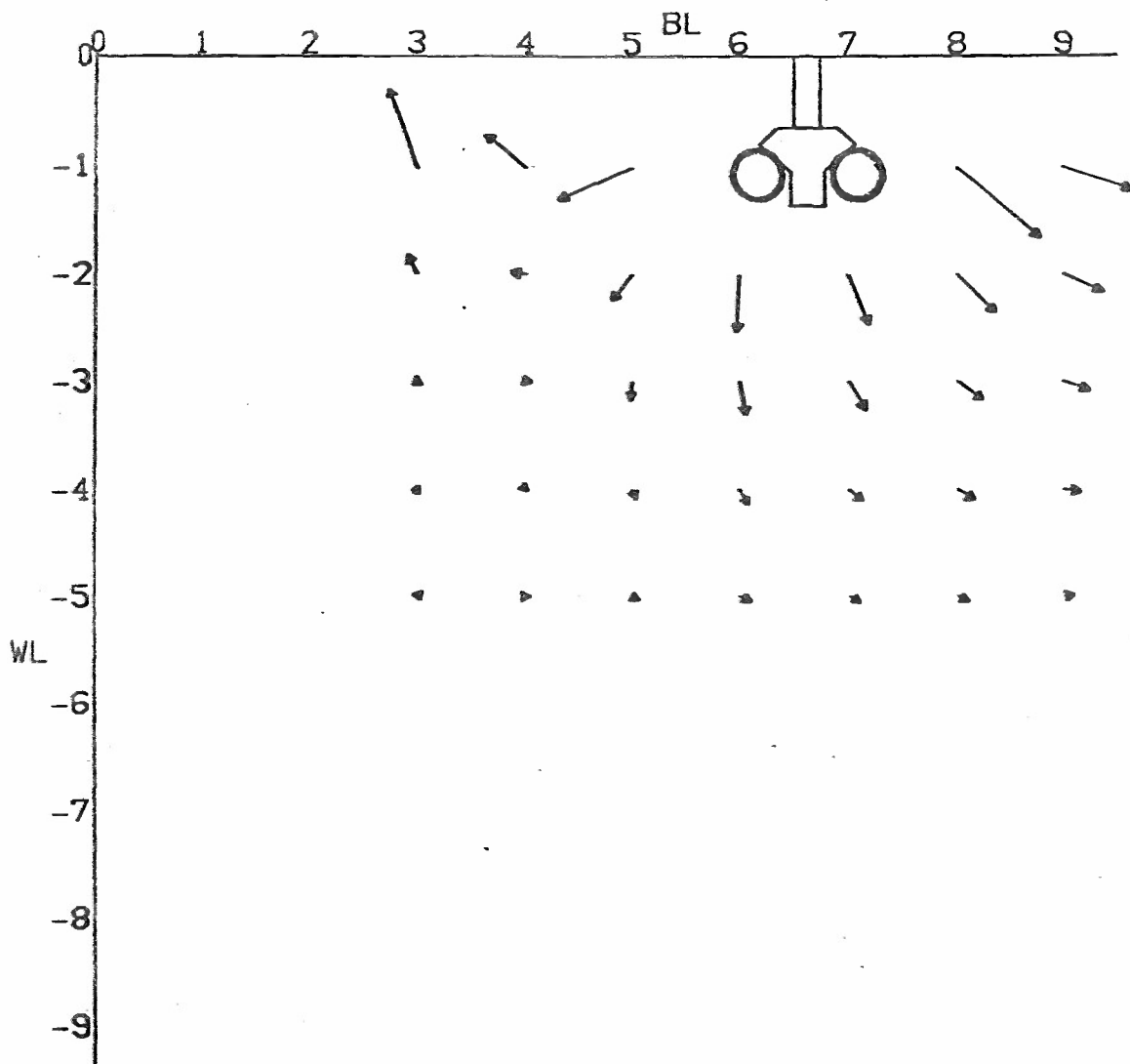


(b) MFS = 14
 Figure 24. Continued



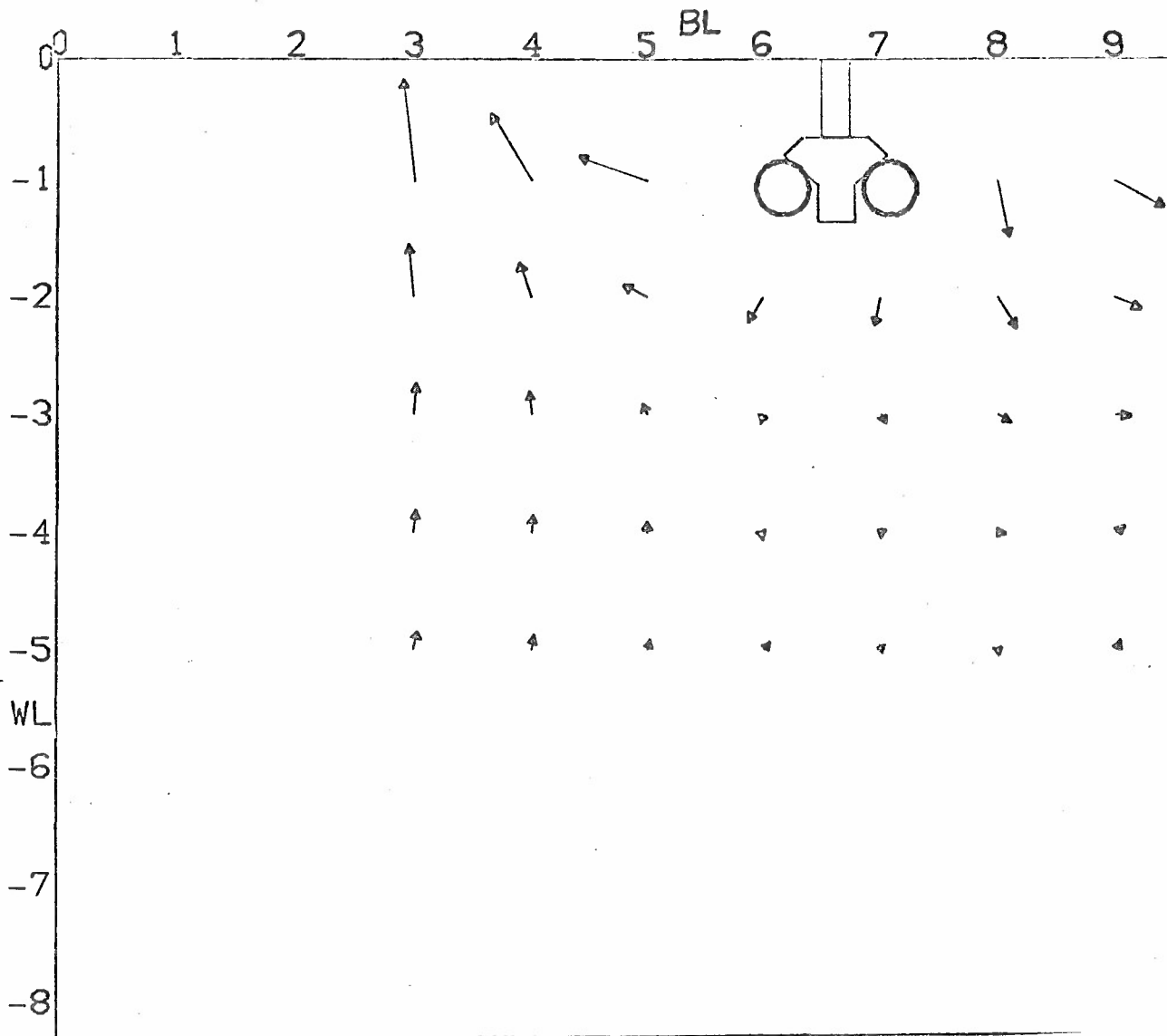
(c) MFS = 17

Figure 24. Continued



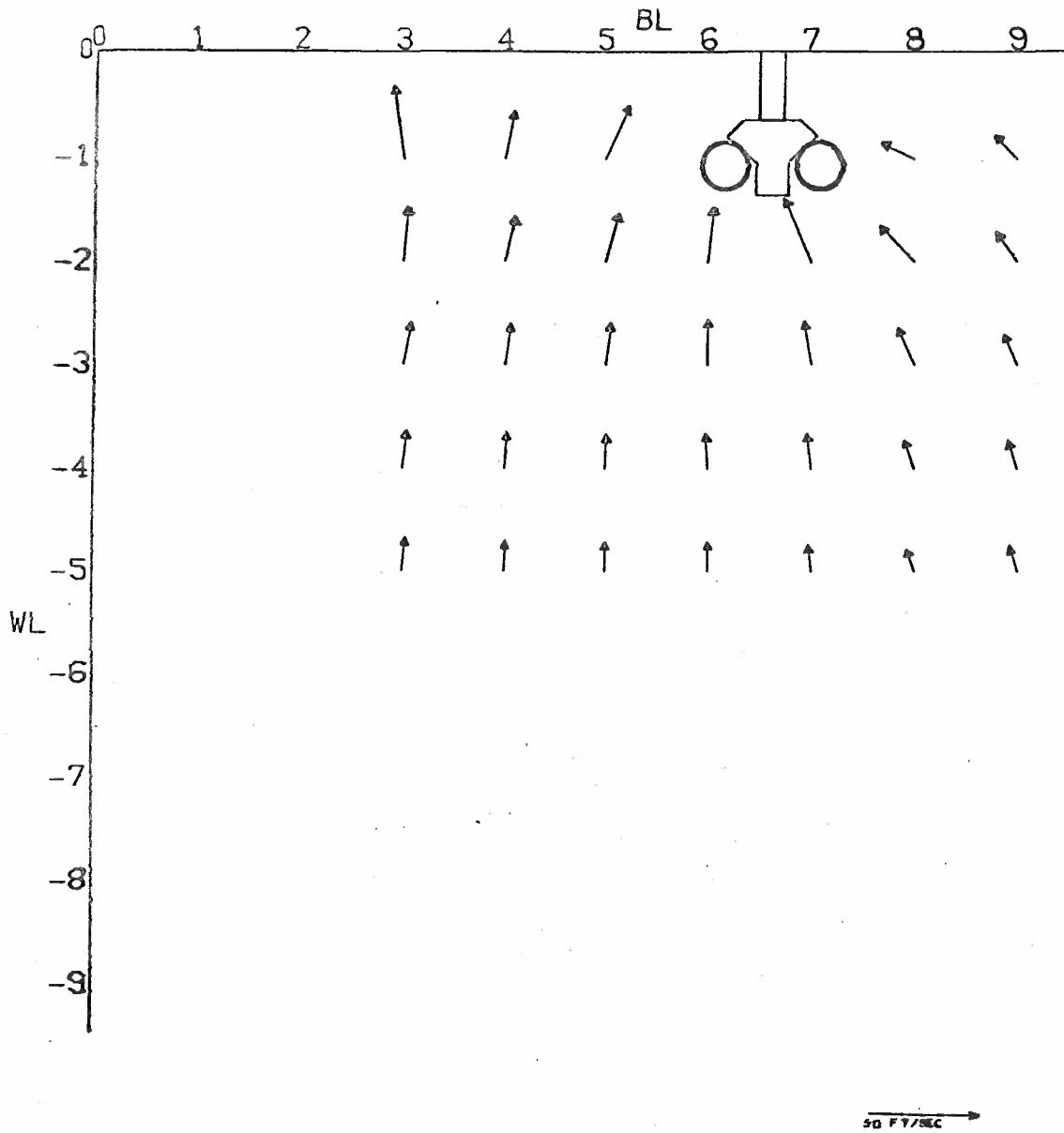
(d) MPS = 18

Figure 24. Continued



(e) MFS = 19

Figure 24. Continued



(f) MFS = 22

Figure 24. Concluded

configurations with the MK-81 T2 and T1 flow fields, respectively, were simulated. Then they were compared to trajectories of the MK-81 in the T2 and T1 configurations, but this time calculated using the T3 MK-81 flow field with a scale factor of 1/3 and 1/5 placed on all the flow angularities for the T2 and T1 configurations, respectively. The comparison plot for the T2 configuration (Figure 25) shows that the curves appear nearly on top of each other. As shown on the comparison plot for the T1 configuration (Figure 26) the yaw prediction is somewhat different. Since the scale factor of 1/5 for the T1 configuration in the T3 flow field produces good results in all parameters except yaw, it can be concluded that the flow field cannot be scaled by a single parameter. However, the results are adequate for showing trends if that is all that is desired. If good accuracy is desired, a T1 flow field should be used with a T1 configuration. The same results were found with the M-117 bomb in Reference 1. The T2 configuration can be used with the T3 flow field with good results.

The second major approximation was that the flow angularities could be scaled in a direct relation to the diameter of the bomb being launched to the diameter of the bomb that was used in collecting the flow field data. In order to investigate this approximation, the M-117 and MK-81 bombs were tested in both the TER and the MER configurations, and their flow patterns are displayed in Figures 7(a), 7(b), 10(a), 10(b), 11(a), 11(b), 12(a), 12(b), 13(a), 13(b), 14(a), 14(b), 18(a) to 18(d), 19(a) to 19(d), 20(a) to 20(d), 21(a) to 21(d), 23(a) to 23(f), and 24(a) to 24(f).

Similar flow pictures exist for both the M-117 and MK-81 bombs in the same configurations. In order to find the effect of the differences that do exist, the MK-81 was launched from the T3, T2, and T1 configuration using the MK-81 T3, T2, and T1 flow fields, respectively. These trajectories were then compared to the MK-81 bomb launched in the T3, T2, and T1 configuration using the M-117 T3, T2, and T1 flow fields, respectively, and a flow field scale factor based on the ratio of the weapon diameters,

$$\frac{\text{MK-81 DIA}}{\text{M-117 DIA}} = \frac{9}{16}$$

The resulting comparisons are displayed in Figures 27, 28, and 29. For the bottom station launch shown in Figure 27, the M-117 flow field produces more pitch than the MK-81 flow field; however, the comparison is still very good considering the large difference in bomb diameter. The shoulder station comparisons (Figures 28 and 29) show nearly identical trajectories. The diameter ratio scaling is a simple, accurate means of adjusting the flow fields for various diameter bombs.

A third approximation was that the angle of attack of the aircraft could be added to the flow angularities in the flow field. To investigate

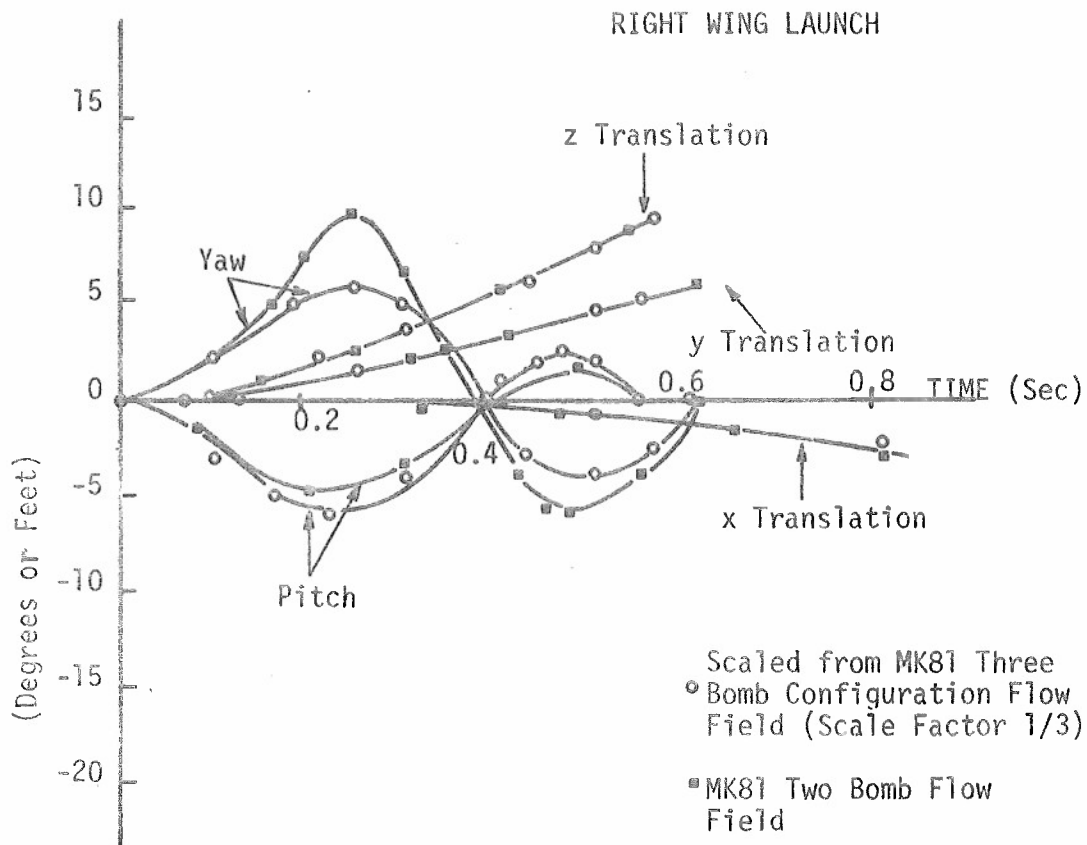


Figure 25. Pitch, Yaw, x, y, and z Time Histories of a MK-81 Launched from the Outboard Shoulder Station of the TER at $M = 0.85$ Using Scaled and Unscaled MK-81 Flow Field Data

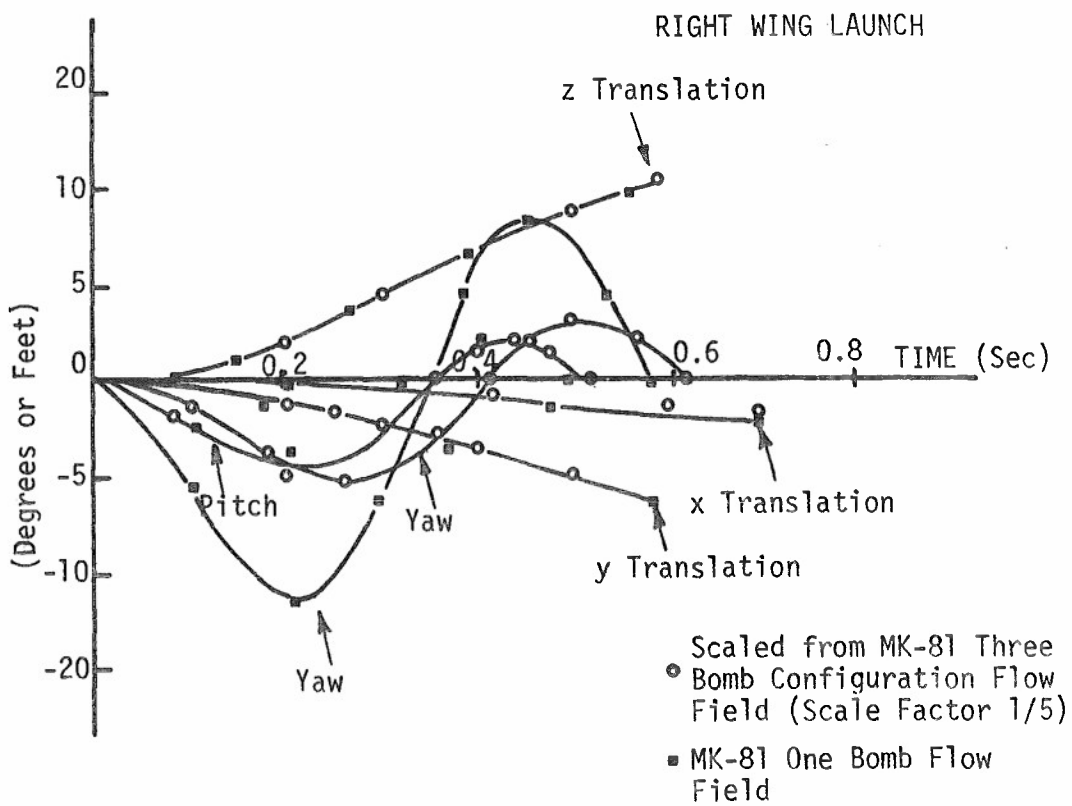


Figure 26. Pitch, Yaw, x, y, and z Time Histories of a MK-81 Launched from the Inboard Shoulder Station of the TER at M = 0.85 Using Scaled and Unscaled MK-81 Flow Field Data

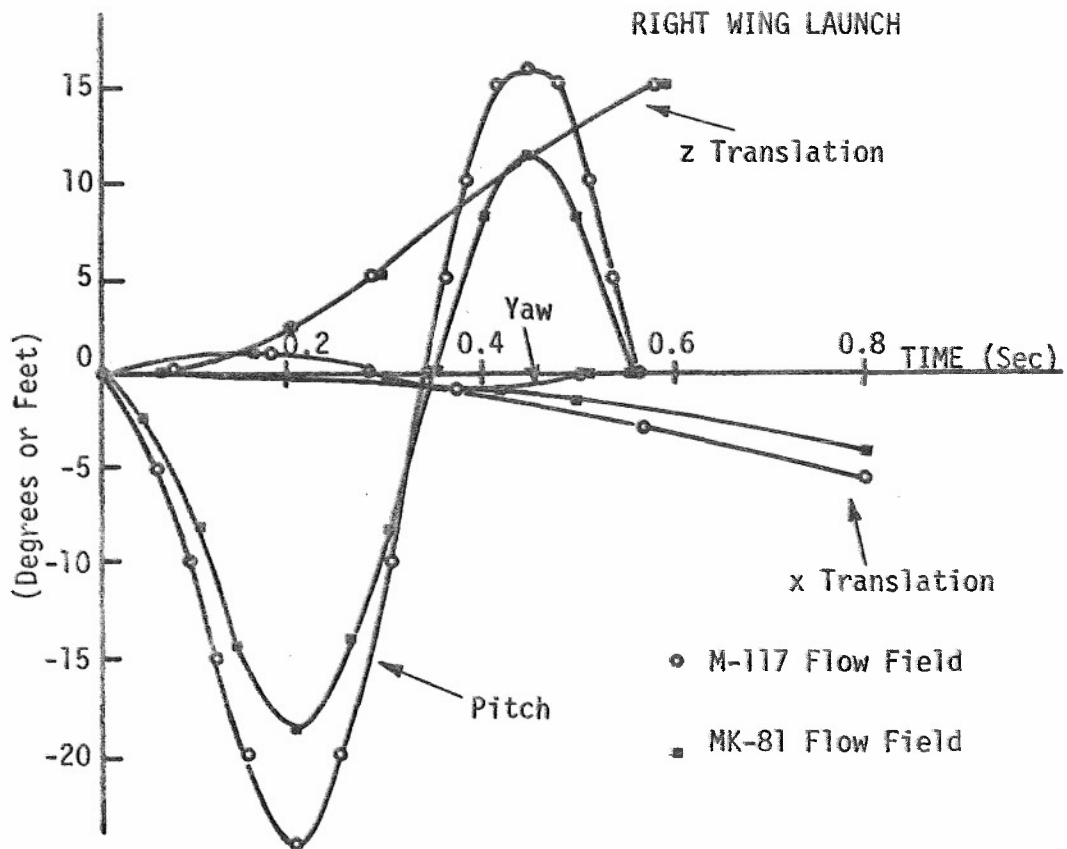


Figure 27. Pitch, Yaw, x, and z Time Histories of a MK-81 Launched from the Bottom TER Station at $M = 0.85$ Using M-117 and MK-81 Flow Field Data

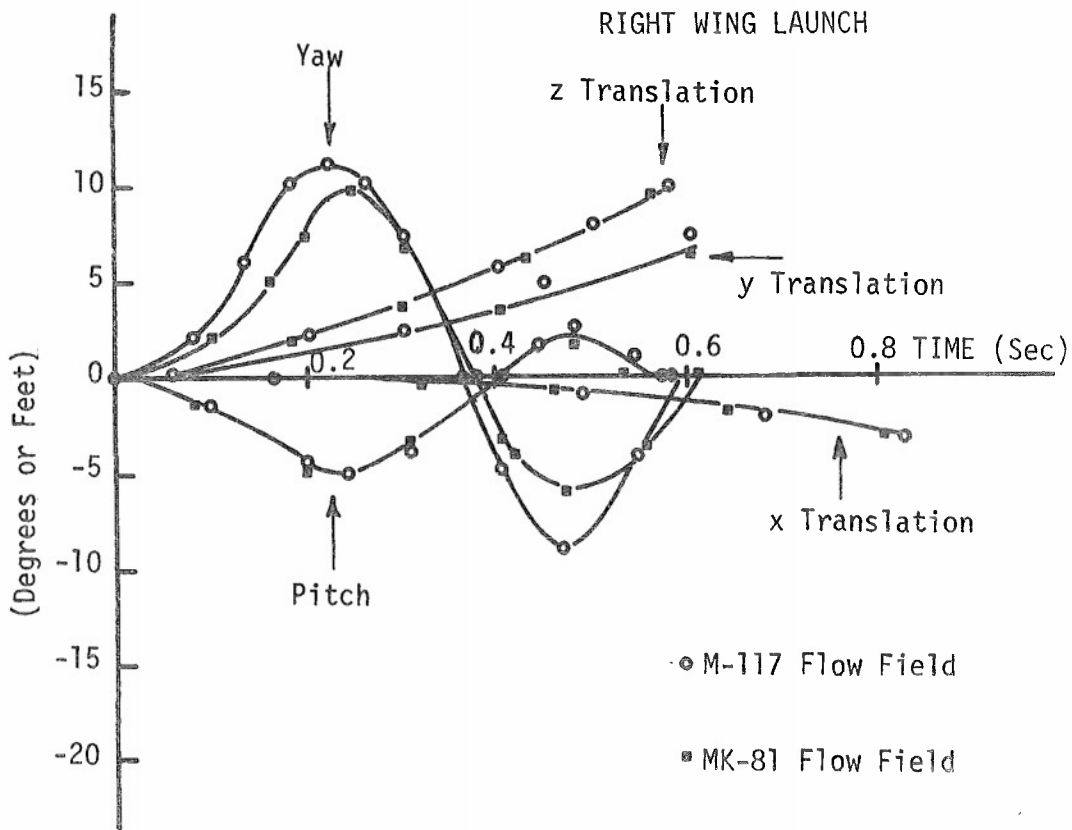


Figure 28. Pitch, Yaw, x, y, and z Time Histories of a MK-81 Launched from the Outboard Shoulder Station of the TER at M = 0.85 Using M-117 and MK-81 Flow Field Data

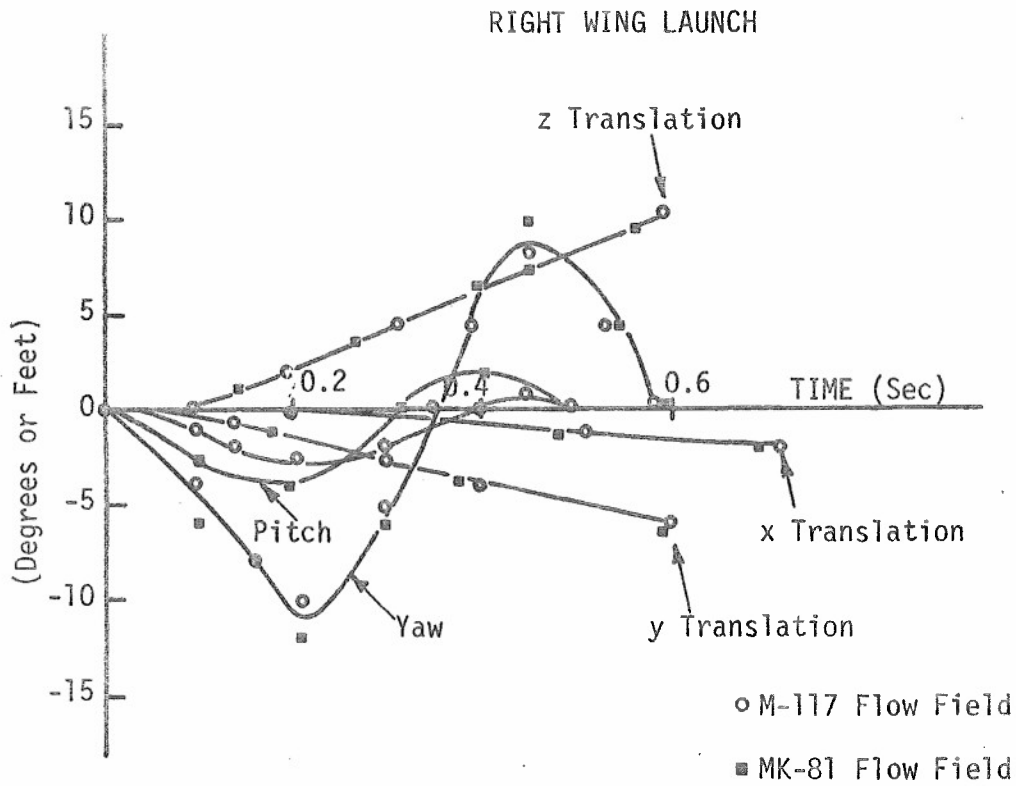


Figure 29. Pitch, Yaw, x, y, and z Time Histories of a MK-81 Launched from the Inboard Shoulder Station of a TER at $M = 0.85$ Using M-117 and MK-81 Flow Field Data

the validity of this approximation, the M-117 and MK-81 bombs were tested in the T3 configuration at aircraft angles of attack (α_p) of 0.3 and 3.3 degrees. The flow pictures for the 3.3 degree conditions are displayed in Figures 7(c), 7(d), 12(c), and 12(d). The actual upwash angles are presented for the M-117 bomb at $\alpha_p = 0.3$ in Figures 8(a) and 8(b) and for $\alpha_p = 3.3$ in Figures 9(a) and 9(b). These figures tend to show that the angle of attack can be added to the flow field angles and is the only practical way to handle the angle of attack variations.

The effect of Mach number on flow angularity was discussed in Reference (1), and an attempt was made to collect data at a Mach number of 1.3 during the test described in Reference (3). The method for collecting data gave very poor and inconsistent results at this Mach number and could not be analyzed. In Reference (1), it was assumed that Mach number had an insignificant effect on the flow angularity in the subsonic region; however, this assumption produced trajectories with larger pitch and yaw excursions at low Mach numbers (0.5 and 0.6) than experimental data obtained by the captive trajectory system. To investigate this problem, a theoretical solution developed by Auburn University (Reference 1) was used to calculate the flow angularities beneath two unfinned M-117 shaped bodies installed on the TER. The resultant flow angle (upwash angle \bar{u}) was calculated at a position that would correspond to the centerline location of the bottom bomb if it were attached. These angles were displayed in Figure 30 for various Mach numbers. The analysis shows there is a Mach number effect at the nose and tail in a region of the flow field that would be used in the flow angularity program to calculate the trajectory. To account for this Mach number effect, a second order correction factor is used to fit the flow angularities at $M = .85$ to values at higher or lower Mach numbers.

An objective of the test was to collect flow field data on single carriage of large diameter bombs and multiple ejector rack configurations. Figures 15(a) to 15(c) and 16(a) to 16(c) show the flow patterns around the MK-84 bomb on the inboard and outboard wing stations (configurations IP1 and OP1). As in the TER configurations, a downwash exists on the nose and an upwash exists at the tail of the bomb. Figures 31 and 32 display example trajectories of the MK-84 calculated with the flow field program. Trajectories of MER Configurations M6, M5, M4, M2, and M1 are presented in Figures 33, 34, 35, 36, and 37, respectively.

Some additional build-up configurations have their flow fields displayed: clean wing in Figures 4(a) and 4(b), wing/pylon in Figures 5(a) and 5(b), wing/pylon/TER in Figures 6(a) and 6(b), and wing/pylon/MER in Figures 17(a) to 17(e).

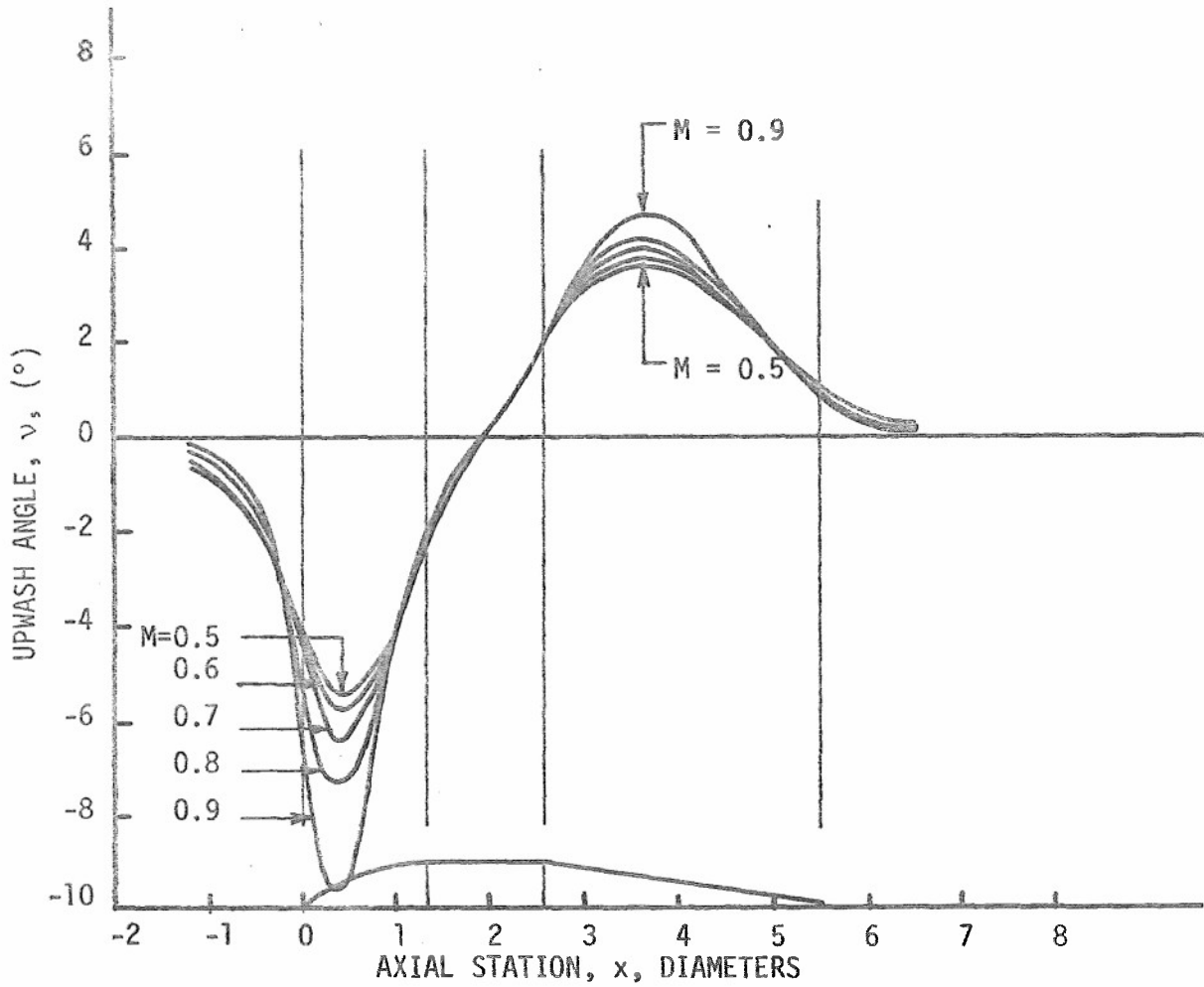


Figure 30. Mach Number Effect on Upwash Angle for Triple Ejector Rack and M-117 Bombs

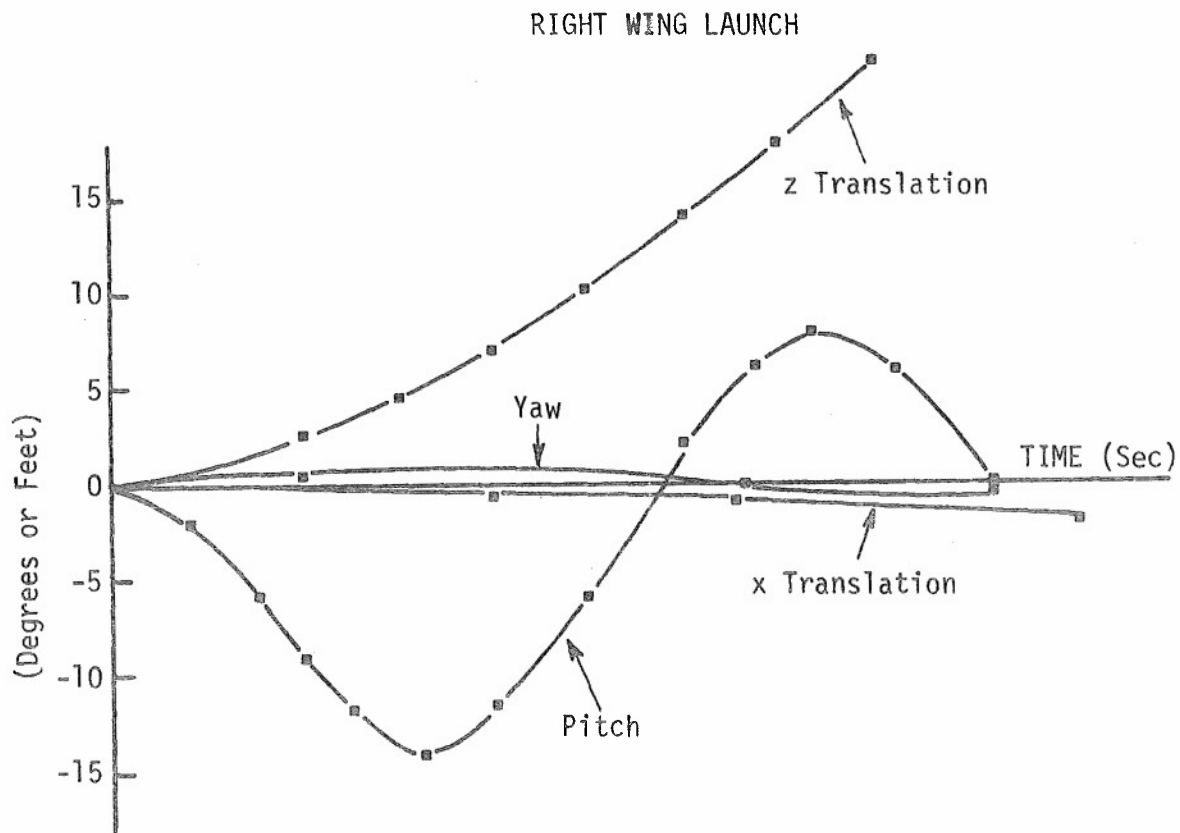


Figure 31. Pitch, Yaw, x, and z Time Histories of a MK-84 Bomb Launch from the Inboard Pylon at $M = 0.85$ Using the MK-84 Flow Field at that Station

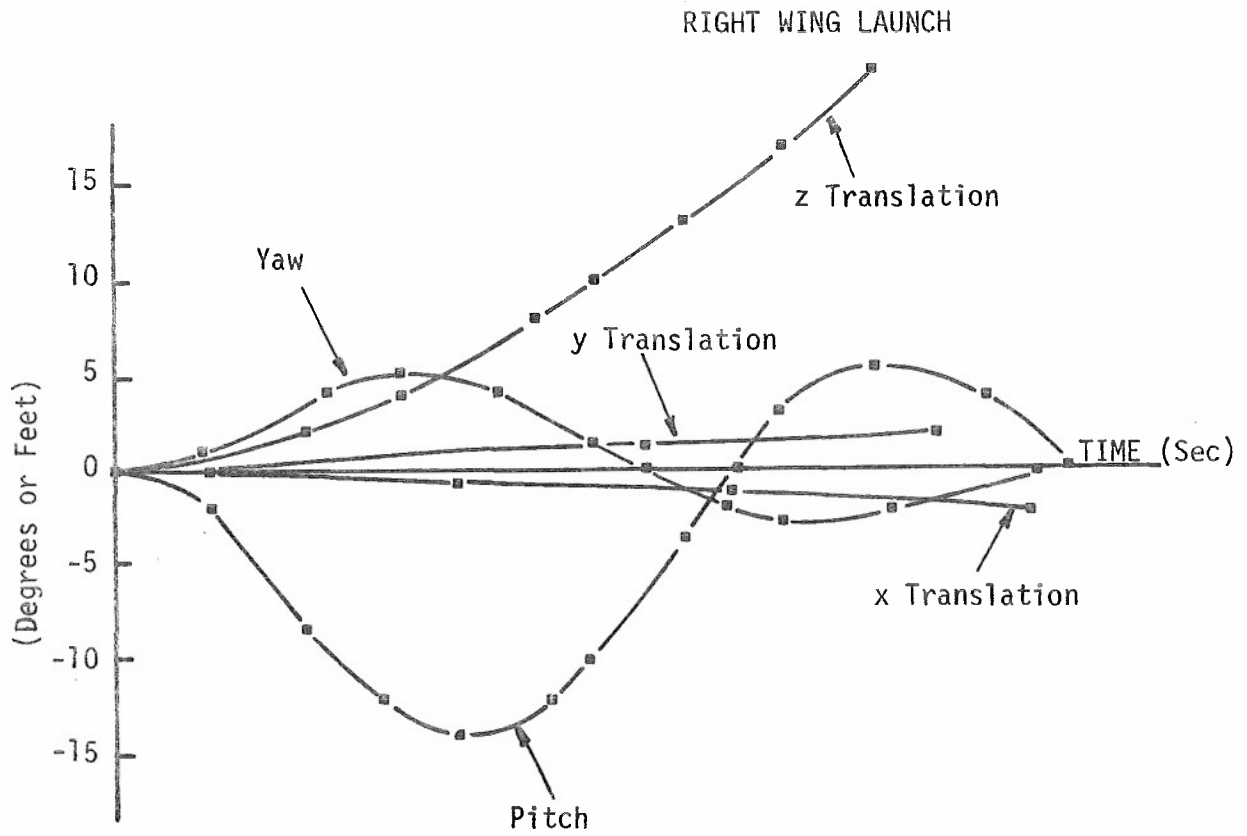


Figure 32. Pitch, Yaw, x, y, z Time Histories of a MK-84 Bomb Launch from the Outboard Pylon at $M = 0.85$ using the MK-84 Flow Field at that Station

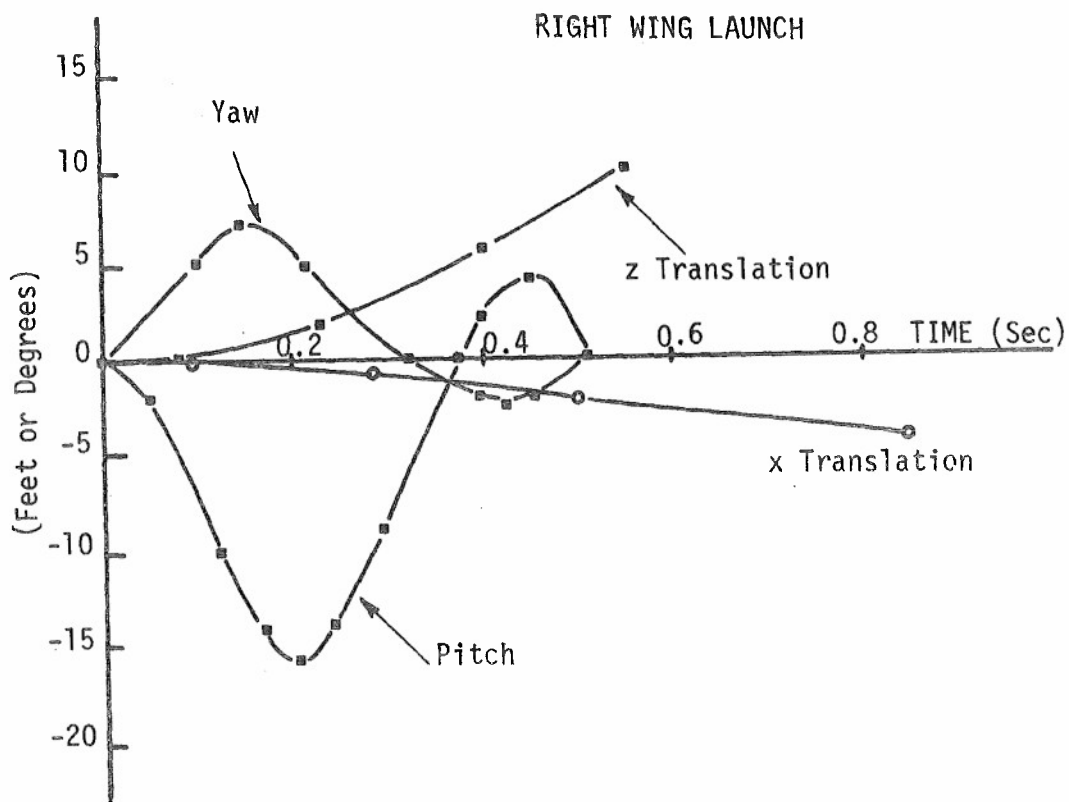


Figure 33. Pitch, Yaw, x, and z Time Histories of an M-117 Bomb Launched from the Bottom Back Station of the MER at $M = 0.85$ Using the Six Bomb Flow Field

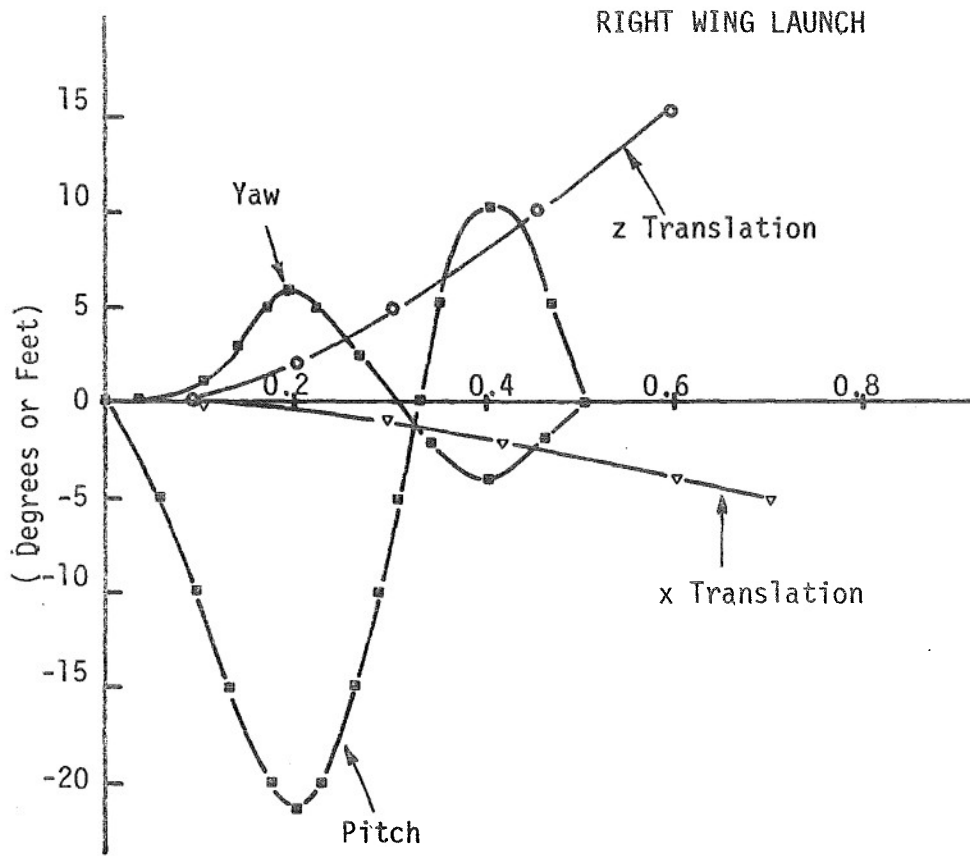


Figure 34. Pitch, Yaw, x, and z Time Histories of an M-117 Bomb Launched from the Bottom Forward MER Station at $M = 0.85$ Using the Five Bomb Flow Field

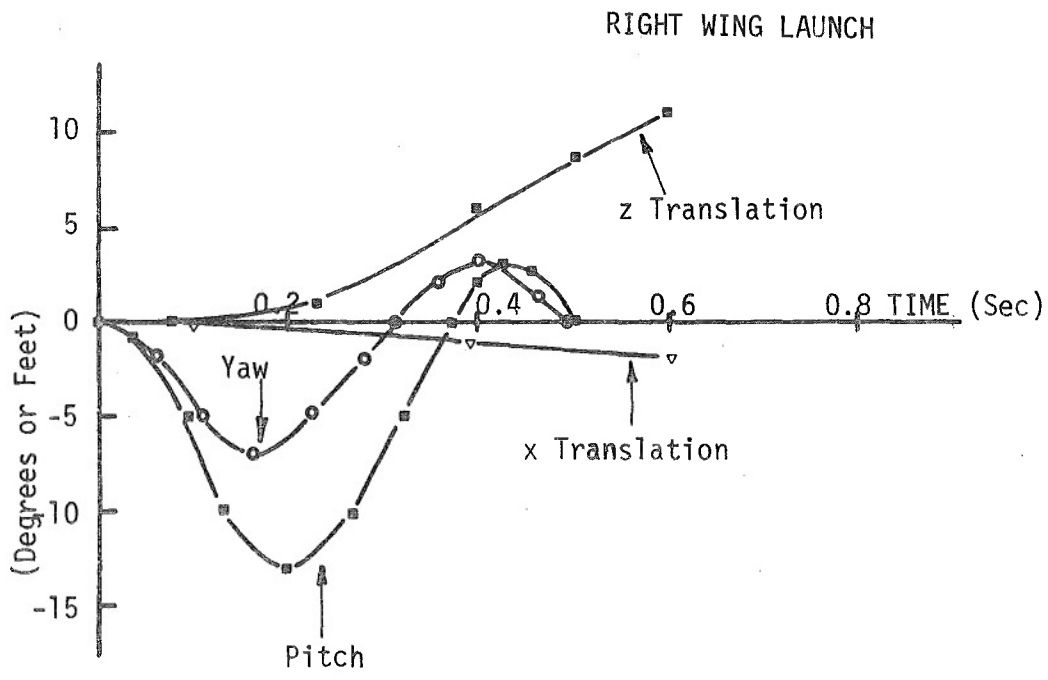


Figure 35. Pitch, Yaw, x, and z Translation of an M-117 Bomb from the Aft Inboard Shoulder Station of MER at M = 0.85 Using the Four Bomb Flow Field

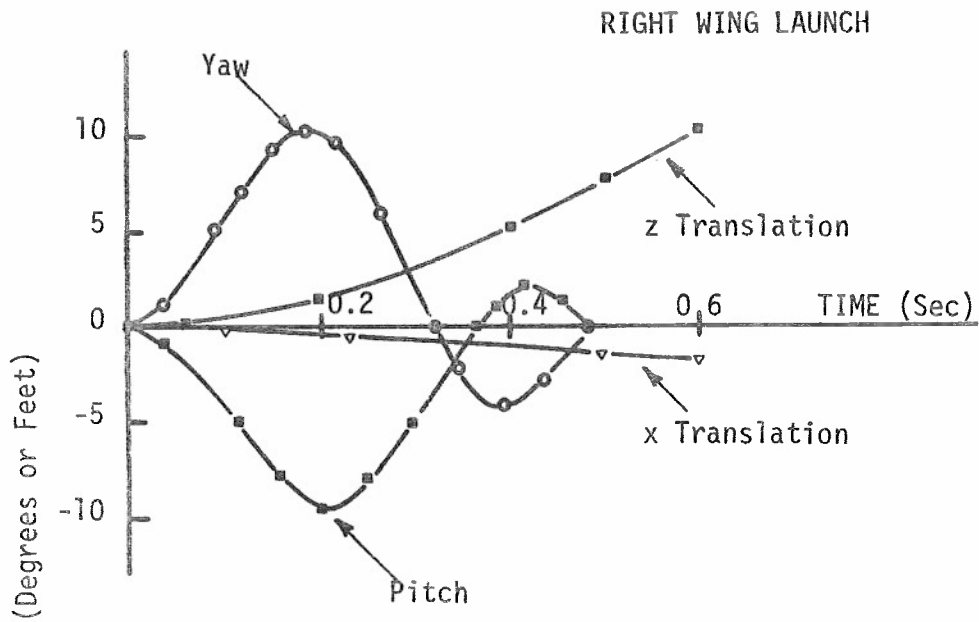


Figure 36. Pitch, Yaw, x, and z Time Histories of an M-117 Bomb Launched from the Aft Outboard Shoulder Station at $M = 0.85$ Using the Two Bomb Flow Field

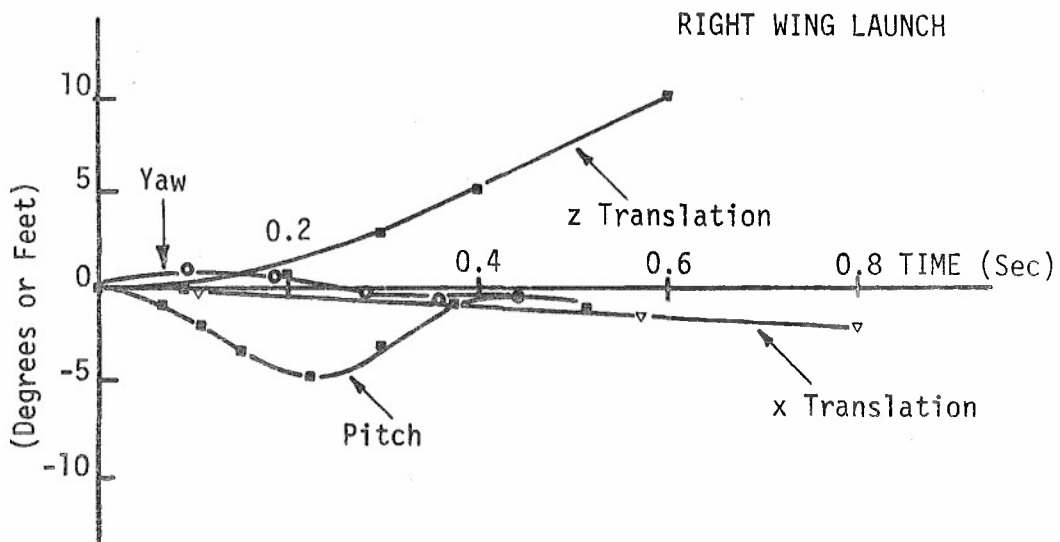


Figure 37. Pitch, Yaw, x, and z Time Histories of an M-117 Bomb Launched from the Forward Outboard Shoulder Station of a MER at $M = 0.85$ Using the One Bomb Flow Field

SECTION III

RESULTS

As a result of the second flow field test, the effects of the approximations made in the flow angularity technique (Reference 1) are more clearly defined. The use of the scaled flow field for T3 configuration on a TER for calculating trajectories from T2 and T1 configurations gives good results; however, more accurate results can be obtained by using the actual flow field. The diameter scaling parameter for the flow field produces good results, and the best results will be obtained by using a flow field that was produced by a store close to the diameter of the one being simulated. The new Mach number correction which comes from theoretical calculations will improve the programs accuracy at low Mach numbers.

With the additional flow field data, good trajectories can now be calculated for stores of large diameter launched from a pylon and all the MER configurations.

APPENDIXES

APPENDIX I

PROGRAM INTRODUCTION

The flow angularity technique for predicting store separation trajectories is based on a general six-degree-of-freedom digital computer program that has been modified to accept flow field data and build the interference aerodynamic coefficients as explained in Reference 1. Table I-1 presents a list of modules used in the simulation. Differential equations are formulated in state variable form, where derivatives of state variables are computed in the appropriate module. Integration is accomplished by executive routines after each pass through the modules. An Adams-Moulton (fourth-order) integration algorithm with Runga-Kutta start, is employed with a fixed integration step size as long as the bomb remains in the interference flow field. After the bomb is free of the interference flow field, the integration step size can be changed for the rest of the flight to the ground. Executive routines monitor input/output which permit many trajectories to be simulated with each run. A table look-up routine with linear interpolation between data points is used to extract flow field data or any other data that needs to be entered in the program but is a function of one, two, or three variables. A plot routine that is designed for the 4020 Stromberg/Carlson plotter will permit trajectory plots.

A module interconnection diagram is presented in Figure I-1 to show how the different modules fit together. Figures I-2 and I-3 explain the axis systems used in the program.

The program text, definitions, and input data are presented in Appendixes II, III, and IV, respectively. Two example runs are displayed in Appendixes V and VI. Example 1 consists of an M-117 launched from the bottom TER station at $M = .85$ and $M = .5$. Example 2 is a MK-84 bomb dropped from the outboard pylon at $M = .85$, and a MK-81 launched from the outboard pylon at $M = .5$.

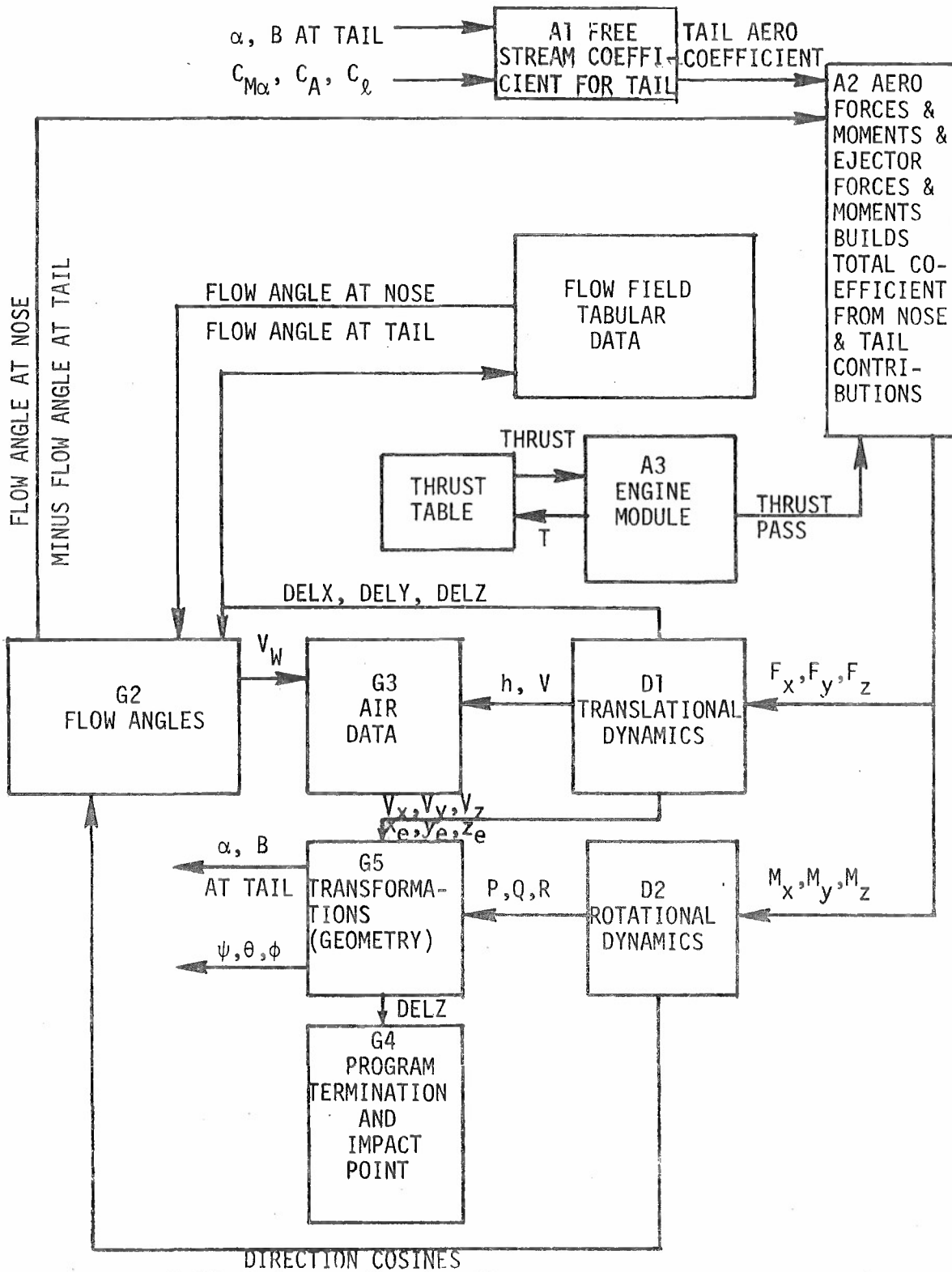


Figure I-1. Module Interconnection Diagram

x_e, y_e, z_e - Earth Axis System

x_B, y_B, z_B - Bomb Body Axis System

x_T, y_T, z_T - Aircraft Body Axis System

$RTXE, RTYE, RTZE$ - Origin Coordinates of the Aircraft Body Axis System with respect to the Earth Axis System

RXE, RYE, RZE - Origin Coordinates of the Bomb Body Axis System with respect to the Earth Axis System (Origin at bomb C_g)

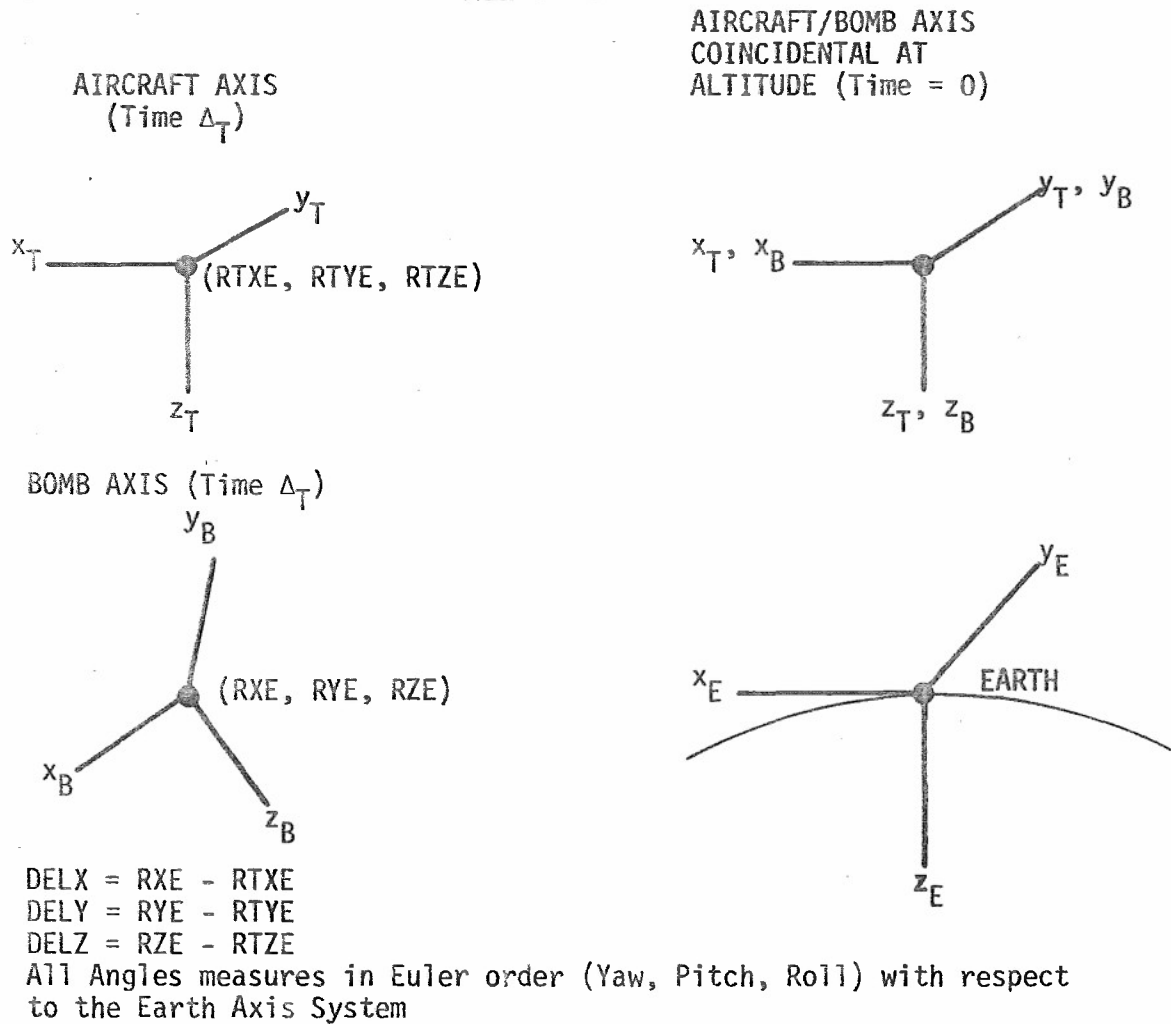


Figure I-2. Axes Systems Definition

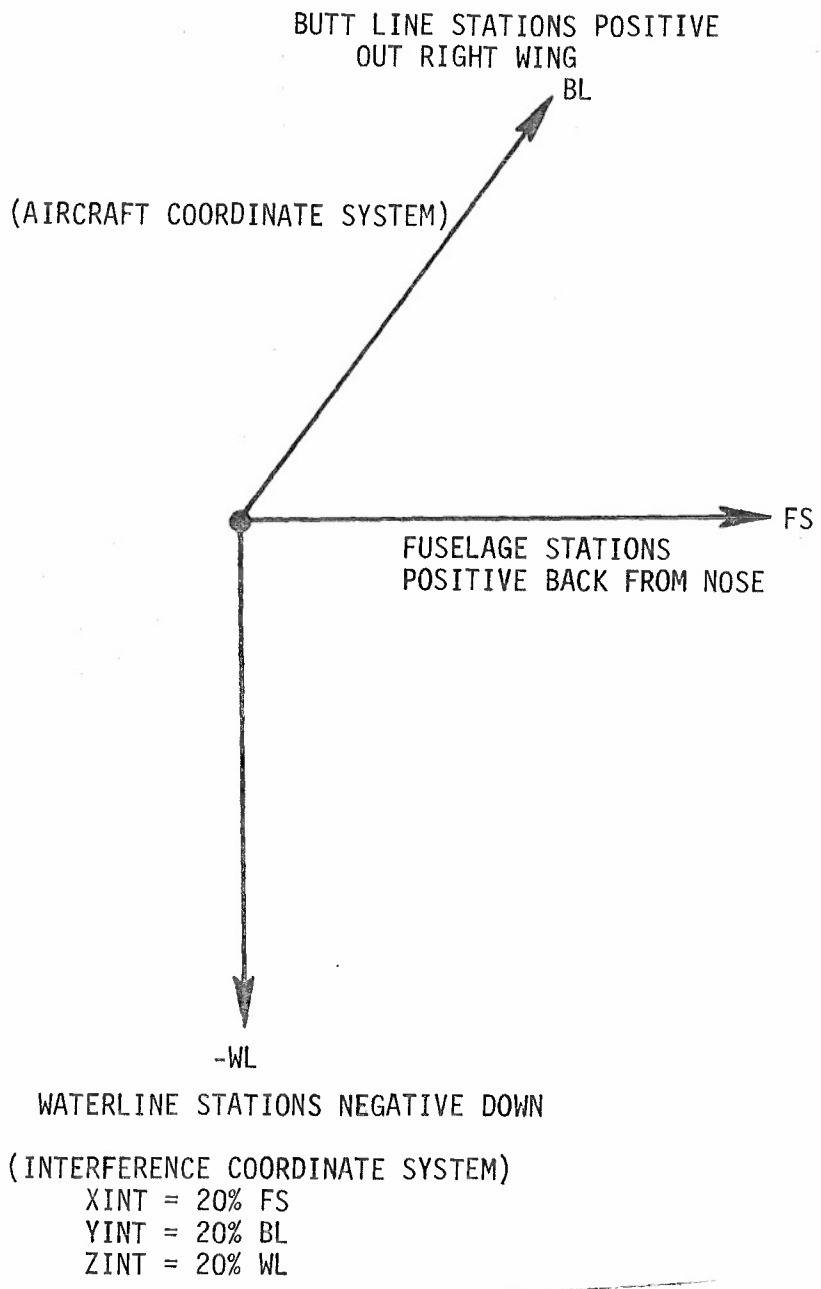


Figure I-3. Conversion from Aircraft Coordinate System to Interference Coordinate System

TABLE I-1. PROGRAM MODULES

I. GEOPHYSICAL AND EXTERNAL ENVIRONMENT

- G2 - Flow field table look-up to determine the flow angularities at the nose and tail of the bomb.
- G3 - Air data, including dynamic pressure, density, speed of sound.
- G4 - Terminal Geometry, computes impact point.
- G5 - Transformation of position and velocity between various coordinate systems.

II. AIRFRAME

- A1 - Free stream aerodynamic coefficients.
- A2 - Aerodynamic forces and movements, in bomb body axes.
- A3 - Engine, computes thrust as well as c.g. shifts and mass changes - including table look-up for thrust.

III. DYNAMICS

- D1 - Translational dynamics of bomb-accelerations in body axes are transformed into earth coordinates and integrated into velocities and positions.
- D2 - Rotational dynamics of bomb, computes rotational accelerations and velocities referred to bomb body axes.

APPENDIX II

PROGRAM TEXT

1. MAIN

MAIN is the central executive routine of the entire program. MAIN calls subroutine ZERO initially then sets the value of the integration parameter NPT. MAIN then decides by REPPLT whether it will use the old and/or new type 4 and 7 cards for multiple runs. OINPT1 is called, and all the input parameters are read into the C array. LSTEP is set equal to STEP, and this parameter will determine whether another set of data exists behind the present set. Next, AUXI is called, and from AUXI, all the initialization routines are called. SUBL2 is called to set the printing and graphing parameters. The VAR and DER arrays are filled from the C array according to the number of state variables found in the initialization routines. AUXSUB is called next to find the derivatives of all the state variables before entering the integration loop. AMRK is called and this routine integrates all the derivatives of the state variables, and then, MAIN places the new values of the state variables back into the C array. SUBL3 is called next and, in turn, calls STAG3 and OUP3. STAG3 sets KSTEP=2 if it is time to terminate the trajectory, and OUP3 prints the variable listed on the type 4 cards at certain time intervals. If it is not time to terminate, AMRK is called again; the program starts looping between AMRK, MAIN, and SUBL3. If KSTEP equals 2, the program leaves the integration loop, zeros the VAR array, and calls RESET. RESET zeros all C array elements that need zeroing. If LSTEP equals 2, the control is transferred back to where OINPT1 is called and the process starts over. If LSTEP equals 11, the program will exit. If OPTIN10 is greater than zero, DUMPO will be called before the exit.

2. SUBROUTINE ZERO

ZERO makes sure that the counters which count the numbers of the various types of input cards and the number of points to be plotted are set equal to zero.

3. OINPT1

OINPT1 reads all the input cards. When a type 6 input card is read, the subroutine returns. It also prints out the values of the input cards as it reads them.

4. AUXI

AUXI has the capability of calling the initialization routine of any regular subroutine. The type 2 cards determine which subroutines will be used in the program, and the DUMMY subroutine has entry statements for any subroutine that does not need an initialization routine.

5. A3I

A3I identifies the thrust as the derivative of the total impulse and stores the C storage location of thrust in the IPL array.

6. D1I

D1I identifies the derivative of the state variables that define the position of the bomb and aircraft and stores the value of their C storage location in the IPL array. The initial velocity of the store is set by the read-in Mach number (VMACH) and RZE displacement. The initial locations of store and aircraft are defined.

7. D2I

D2I is the rotational dynamics initialization module. The derivatives of the elements of the position matrix, the pitch, yaw, and roll accelerations are defined and stored in the IPL array. Also, the angular rate derivatives are reset to zero.

8. SUBL2

SUBL2 calls staging and output routines according to the values placed on the type 1 cards.

9. STAG2

STAG2 sets KCONV=0, LCONV=0, KSTEP=1.

10. OUPT2

OUPT2 updates DOC by 1, and if that value is less than 7, DUMPO is called. OUPT2 initializes the counters needed to space the printing on the page. It also stores the first values of the variables to be plotted in the graph array and initializes OPOINT equal to 1.

DTCNT decides how many lines of data will be printed each time OUPT3 is called.

11. AUXSUB

AUXSUB calls the regular subroutines according to the value on the type 2 cards in columns 20 through 25.

NOMOD = number of type 2 cards.

XMODNO or MODNO array stores the value on columns 20 to 25 read in E.15 format from the type 2 cards.

12. G2

G2 calculates the nose and tail positions of the bomb in the interference flow field after scaling the unit length of the flow field by the ratio of DIASC. The values of the flow angularity are found in the tabular data.

The angularity at the tail is then converted into a cross-flow velocity when the freestream velocity is multiplied by the angularity. These cross-flow velocities VWXE, VWYE, and VWZE are inputs in subroutine G3. The angularity at the nose minus the angularity at the tail is then passed on to A2 for calculations of the nose moment and force contribution.

13. G3

G3 calculates the store velocity at the tail with respect to the air mass in earth axis system. It also sets the speed of sound, Mach number, and density for the calculated altitude.

14. G5

G5 calculates pitch, yaw, and roll angles in degrees and their associated derivatives. It then calculates a total velocity of the store with respect to earth axis system (VTOTE) and the distance the store has moved from its initial position (RANGO). The velocity of the store with respect to the air mass in body axes are calculated, and from these velocities, the angles of attack and side slip are calculated.

15. A1

A1 calculates the moment and force coefficients CX, CY, CZ, CM, and CL from input parameters CAA, CNA, and CMA which are C_a , C_N^α , and C_M^α , respectively. The wind tunnel angle of attack and roll angle α are used to position the store with respect to the free stream velocity rather than the angle of attack and side slip angles. These coefficients, however, do not include the nose correction yet.

16. A2

A2 makes the corrections to the moment and force correction due to the flow field at the nose having a different angularity than the tail. These aerodynamic coefficients are then transferred to body forces and moments. Ejector forces and moments are then combined with the aerodynamic forces and moments to give the resultant values. The ejector forces and moments last over either an ejector force time (EFT) or an ejector stroke distance (EJD). When the time is greater than EFT or the distance traveled is greater than EJD, the ejector force and moment become zero.

This routine has an option for a rail launched missile. Until the missile leaves the rail, it is restricted to move only in the X direction. The lug loads are calculated during that time. If no rail launch is desired, make OPTN4 = 2 and RAIL = RLUG = 0. Any forces and moments found due to a thrusting motor are also added to the total forces and moments.

17. A3

A3 calculates the thrust and thrust misalignment effects. It also calculates any c.g. and IXX, IYY, and IZZ changes due to burning the propellant. If no thrust exists, the thrust values in the table look-up must be zero. If no thrust exists, the specific impulse (ISP) must be read in as 1.

18. D1

D1 is the translational dynamics module that transfers the forces calculated in A2 into body accelerations in body axis and then transfers then into earth axis. The gravity term is added to the verticle acceleration, and the velocity is defined as the integral of the acceleration and the derivative of the position. Also, the aircraft velocity is integrated to find its position.

19. D2

D2 is the rotational dynamics module that calculates the body angular rates and the derivatives of elements of the position matrix.

20. AMRK

AMRK is the integration subroutine. This routine under usual operation does three Runge-Kutta integrations and then uses the Adams-Moulton predictor corrector until completion. The variable NPT is set equal to 2 at

the beginning of the program unless RKUTTA is set equal to 1. On coming into AMRK with NPT equal to 2, KOUNT is set equal to 0, and NPT is set equal to ZERO. Each time through AMRK, COUNTS is updated by 1 until COUNTS equals 3, at which time AMRK switches from Runge-Kutta to Adams-Moulton.

The Runge-Kutta integration calls AUXSUB four times, and the Adams-Moulton predictor corrector calls AUXSUB twice.

If RKUTTA is set equal to 1, NPT is set equal to one and Runge-Kutta integration is used all the time.

21. STAG3

STAG3 calls G4 which determines whether ground impact has occurred. If impact has occurred, LCONV will be equal to 2. STAG3 also determines whether TF, which is the maximum trajectory time that is read as an input, has been exceeded by T. If either condition has been met, one more integration is performed with DER(1)=0. Then OUP3 is called to write the results of the last integration, and the KSTEP is equal to 2. KSTEP equal to 2 eventually terminates the integration in MAIN.

22. G4

G4 calculates the distance the impact point is from the origin of the earth axis system by determining when RZE becomes positive and then interpolating between that position and the position of the store at its previously calculated position. The miss distances X, Y, Z, and T are printed from this subroutine.

23. OUP3

OUP3 checks to see if the computer ITCNT is less than 7 and, if so, DUMPO is called. The main purpose of OUP3 is printing the value of the variables listed on the type 4 cards and their alphanumeric names. PCNT is updated by CPP which is the time interval between printing. OUP3 also stores the values of the variables to be plotted in the GRAPH array (these are variables input by type 7 cards). PPNT is updated by PPP which is the time interval between saving points to be plotted. If a DUMPO has occurred, PGCNT will equal 1, and the printing format is adjusted by printing the variable names at the top of the next page. PGCNT counts the number of lines that have been printed, and when PGCNT equals or is greater than 112, the new heading is printed and PGCNT is reinitialized by the number of lines that were used for the heading print out. OPOINT counts the number of times that data is stored in the graph array.

24. DUMPO

DUMPO prints all values stored in the C array 9 to a line with a counter in the first 5 columns.

25. DUMMY

This subroutine contains entry statements that are used if a subroutine is called and is not present in the program. If the subroutine is present in the program, the appropriate entry statement in DUMMY should be removed or preferably a C placed in Column 1 of that card turning that entry into a comment card.

APPENDIX III

NOMENCLATURE DEFINITION

1. EXECUTIVE ROUTINES

Variable Name	Reset To Zero	C Storage Location	Variable's Dimension	Input	Definition
RKUTTA	YES	1972	1	YES	If RUNGE-KUTTA integration desired exclusively, RKUTTA=1; otherwise, RKUTTA=0.
NJ	YES	1974	1	NO	NJ=N-1.
NPT	YES	1975	1	NO	Controls integration.
PLOTN4	NO	1982	1	YES	Number of variables plotted by type 4 graph routine.
PLOTN2	NO	1983	1	YES	Number of variables plotted by type 2 graph routine.
OUTPLOT	NO	1985	15	NO	Array containing C storage location of variables to be plotted.
T	NO	2000	1	YES	Time (initially zero)

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
TF	NO	2001	1	YES	Maximum allowable trajectory time before the program shuts itself off.
PCNT	YES	2003	1	NO	The value of time at which the next print out will occur.
PPNT	YES	2004	1	NO	The updated plotting time.
PPP	NO	2005	1	YES	Plotting time is updated by adding PPP to the last plotting time.
REPPLT	NO	2006	1	YES	0. Use new type 4 and 7 cards, and discard old. 1. Use old plus those added type 4 and 7 cards. -1. Use new type 7 cards and discard old.
PTLESS	YES	2007	1	YES	Number of last plotting points deleted.
PLOTNO	NO	2008	1	YES	Total number of variables to be plotted.
NOPLT	NO	2009	1	YES	Integer value of PLOTNO.

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
STEP	NO	2010	1	YES	STEP=2, another set of data behind this set. STEP=11, last set of data.
KSTEP	YES	2011	1	NO	Flag set to take the program out of the integration loop after G4 decides the bomb has contacted the ground. KSTEP=2 at this time.
LSTEP	NO	2012	1	NO	Integer value of STEP.
DOC	NO	2013	1	YES	Counter for DUMPO. $DOC \geq 6$, C array not printed. $DOC < 6$, C array printed.
ITCNT	YES	2014	1	NO	Counter that counts iteration so DUMPO can be called. (If ITCNT > 6, DUMPO will not be called)
CPP	NO	2015	1	YES	Value that updates PCNT after each print out.
PGCNT	YES	2016	1	NO	A counter that automatically counts the lines of data printed on an output page. When PGCNT is greater than or equal to

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
					112, a flag is set so that headings will be printed at the top of the next page.
DTCNT	YES	2017	1	NO	A counter that is automatically set during operation subroutine OUPT2 to the required number of lines of numerical data per print out. DTCNT is used in operational subroutine OUTP3 to determine when headings should be printed on each output page.
OPOINT	NO	2023	1	NO	Number of points to be plotted for each variable. It is a counter.
TIME	NO	2025	300	NO	Storage array containing the times during trajectory that variable values will be saved for plotting.
VLABLE	NO	2325	(2,15)	NO	Array containing alphanumeric names of variables to be plotted.
IR(I)	YES	2355	2	YES	Value on columns 1 and 2 of input cards. Determines card type.
VR(1) VR(2)	YES	2357	2	YES	Value on columns 31-45 on type 3 cards. Value on columns 46-61 on type 3 cards.

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
NOMOD	NO	2361	99	NO	The number of modules to be processed.
NOSUB	NO	2461	1	NO	Number of type 1 cards.
SUBNO	NO	2462	99	NO	Storage values on type 1 cards (columns 21-25)
N	NO	2561	1	NO	Number of state variables as counted in the initialization subroutines.
IPL	YES	2562	101	NO	Storage array for the C locations of all the derivatives of the state variables.
DER	YES	2664	101	NO	Storage array for the derivative of the state variables.
VAP	YES	2965	101	NO	Storage array for values of all state variables.
NOLIST	NO	3066	1	NO	Number of type 3 cards to be reset. If VR(2) equal 1 the variable is reset.
LISTNO	NO	3067	50	NO	Storage array of the C storage locations of variables on type 3 cards that need to be reset.

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
VALUE	NO	3117	50	NO	Storage array of the values of the variables that will be reset.
OUTNO	NO	3168	50	NO	Storage array for the locations of variables on type 4 cards.

2. G2

Variable Name	Reset to Zero	Cstorage Location	Variable's Dimension	Input	Definition
COUNTE	YES	42	1	YES	COUNTE=2. No flow angularity calculated. COUNTE=0. Flow angularity calculated.
ZLUN	YES	44	1	NO	ZINT coordinate of the store for table look up in the flow angularity table. (inch)
XLUN	YES	45	1	NO	XINT coordinate of the nose of the store for table look up in the flow angularity table. (inch)
PWY3	YES	46	1	NO	Flow angularity in the XINT, YINT plane at the store nose after all scaling. (rad)
OPTNW	NO	50	1	YES	0=No interference flow field. 1=Interference flow field.
XPOS	NO	54	1	YES	FS position of the C.g. for the store being launched (FT)

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
YPOS	NO	55	1	YES	BL position of the c.g. for the store being launched (FT)
ZPOS	NO	56	1	YES	WL position of the c.g. for the store being launched (FT)
XTAIL	NO	57	1	YES	Length from store c.g. to tail of store being launched (FT; usually negative)
TNOSOS	NO	58	1	YES	Scale factor used to adjust the flow field if the three store flow field is used for other configurations. 1. store on TER TNOSOS=5 2. Stores on TER TNOSOS=3 3. Stores on TER TNOSOS=1 All other configurations TNOSOS=1.
XNOSE	NO	59	1	YES	Length from store c.g. to nose of the store used to generate the flow field.
AAN	YES	60	1	NO	Flow angularity at the nose minus flow angularity at the tail after all scaling in the XINT, YINT plane (rad)
ASN	YES	61	1	NO	Flow angularity at nose minus flow angularity at the tail after all scaling in the XINT, YINT plane (rad)

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
PWZ1	YES	62	1	NO	Flow angularity at the nose in the XINT, ZINT plane before scaling.
PWY1	YES	63	1	NO	Flow angularity at the nose in the XINT, YINT plane before scaling.
XLUN	YES	67	1	NO	XINT coordinate of the nose of the store for table lookup in the flow angularity table.
DIASC	YES	69	1	YES	Ratio of the diameter of the store used to generate the flow field and the diameter of the store being launched.
DELX	YES	70	1	NO	Store RXE position minus aircraft RTXE position.
DELY	YES	71	1	NO	Store XYE position minus aircraft RTYE position.
DELZ	YES	72	1	NO	Store RZE position minus aircraft RTZE position.
XNOSE1	NO	73	1	YES	Distance from store c.g. to the estimated center of pressure of the nose body. (FT)

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
XNPOS	YES	90	1	NO	Positions of the nose of the store calculated during the trajectory.
YNPOS	YES	91	1	NO	
ZNPOS	YES	92	1	NO	
XTPOS	YES	93	1	NO	Positions of the tail of the store calculated during the trajectory.
YTPOS	YES	94	1	NO	
ZTPOS	YES	95	1	NO	
VWXE	YES	100	1	NO	Cross wind components at tail due to the interference flow field.
VWYE	YES	101	1	NO	
VWZE	YES	102	1	NO	
PPP1	NO	120	1	YES	Value of PPP desired after store leaves the interference flow field.
CPP1	NO	121	1	YES	Value of CPP desired after store leaves the interference flow field.
DER1	NO	122	1	YES	Integration step size desired after the store leaves the interference flow field.
XTL	NO	123	1	YES	The upper limits of the values of XINT, YINT and ZINT that define the interference flow field control volume(model inch).
YTL	NO	125	1	YES	
ZTL	NO	127	1	YES	

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
XLL	NO	124	1	YES	The lower limits of the values of XINT, YINT, and ZINT that defines the interference flow field control volume(model inch).
YLL	NO	126	1	YES	
ZLL	NO	128	1	YES	

3. G3

Variable Name	Reset to Zero	C Storage Location	Variable's Dimension	Input	Definition
VMWXE	YES	200	1	NO	Store velocity WRT the air mass in earth axis system with a tail interference velocity correction included.
VMWYE	YES	201	1	NO	
VMWZE	YES	202	1	NO	
PDYNMC	YES	203	1	NO	Dynamic pressure,
VMACH	YES	204	1	YES	Initial and updated Mach number.
DRHO	YES	205	1	NO	Standard atmosphere density at the calculated altitude.
VSOUND	YES	206	1	NO	Velocity of sound at the calculated altitude.
VAIRSP	YES	207	1	NO	Calculated airspeed of store WRT the air mass including the interference flow field velocity.
RW	YES	209	1	NO	Calculated altitude.

4. G4

Variable	Reset to Zero	C Storage Location	Variable's Dimension	Input	Definition
RMISS	YES	N/A	N/A	NO	Distance of impact point from the origin of the earth axis system.
TZERO	YES	N/A	N/A	NO	Time of impact.
RDZ	YES	N/A	N/A	NO	Xe, Ye, Ze components of distance that locate the impact point from the origin of the earth axis system.
RDY	YES	N/A	N/A	NO	
RDX	YES	N/A	N/A	NO	

5. G5

Variable	Reset to Zero	C Storage Location	Variable's Dimension	Input	Definition
BTHT BPSI BPHI	YES YES YES	350 351 352	1 1 1	NO NO NO	Euler pitch, yaw and roll angles of store WRT earth axis system.
BTHTD BPSID BPHID	YES YES YES	353 354 355	1 1 1	NO NO NO	Derivatives of Euler pitch, yaw, and roll angles.
VTOTE	YES	356	1	NO	Total velocity of store with respect to the earth axis system.
611 VMWU VMWV VMWW	YES YES YES	360 361 362	1 1 1	NO NO NO	Velocity components of store with respect to air in body axis system.
BALPHA	YES	367	1	NO	Angle of attack of store,
BALPAY	YES	368	1	NO	Angle of side slip of store,
BALPHP	YES	369	1	NO	Angle of attack of store in wind tunnel axis system.
BPHIP	YES	370	1	NO	Roll angle in wind tunnel axis system.

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
RANGO	YES	380	1	NO	Distance of the store from launch point in the earth axis system.
ALPHA0	YES	381	1	YES	Initial angle attack of aircraft.

6. A1

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
CMAA	YES	1272	1	YES	CM_{α}
CNA	YES	1273	1	YES	CN_{α}
CAA	YES	1274	1	YES	CA
CL2	YES	1240	1	NO	Cl
121 CX	YES	1203	1	NO	(body axis) axial force coefficient
CY	YES	1204	1	NO	(body axis) side force coefficient.
CZ	YES	1205	1	NO	(body axis) normal force coefficient.
CM	YES	1210	1	NO	(body axis) pitching moment coefficient
CN	YES	1211	1	NO	(body axis) yawing moment coefficient
CMQ	NO	1207	1	YES	Pitch damping coefficient.

Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
CNR	NO	1208	1	YES	Yaw damping coefficient.
CLP	NO	1206	1	YES	Roll damping coefficient,
CL	YES	1209	1	NO	Rolling moment coefficient in body axis

7. A2

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
RFAREA	NO	1306	1	YES	Cross sectional area of store (max)
RFLGTH	NO	1307	1	YES	Diameter at maximum cross section of store.
RLUG	NO	1316	1	YES	For rail launch only; distance between lugs
RAIL	NO	1317	1	YES	Rail length between front lug and end of rail
OPTN4	NO	3504	1	YES	If $OPTN4=0$, no rail launch. If $OPTN4>0$, can be rail launch, if $RAIL$ or $RLUG>0$.
FXBA FYBA FZBA	YES YES YES	1300 1301 1302	1 1 1	NO NO NO	Combination of aerodynamic and ejector forces on the store.
FMXBA FMYBA FMZBA	YES YES YES	1303 1304 1305	1 1 1	NO NO NO	Combination of aerodynamic and ejector moments on store.

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Variable Name	Reset to Zero	C storage Location	Variable's Dimension	Input	Definition
FMXTH	YES	1320	1	NO	Moments caused by thrust misalignments.
FMYTH	YES	1321	1	NO	
FMZTH	YES	1322	1	NO	
FMXLUG	YES	1323	1	NO	Moments for store transferred to the lugs.
FMYLUG	YES	1324	1	NO	
FMZLUG	YES	1325	1	NO	
EFT	NO	1332	1	YES	Ejector force action time.
EJD	YES	1333	1	YES	Ejector stroke length.
EFORCX	NO	1326	1	YES	Ejector forces in earth axis system.
EFORCY	NO	1327	1	YES	
EFORCZ	NO	1328	1	YES	
EMOMX	NO	1329	1	YES	Ejector moments in earth axis.
EMOMY	NO	1330	1	YES	
EMOMZ	NO	1331	1	YES	

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8. A3

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
BALPHT	NO	1401	1	YES	Angle between the thrust vector and X body axis.
BPHIT	NO	1402	1	YES	Angle between the thrust vector projected into the Y_B, Z_B plane and the Z_B axis
QNALGN	NO	1403	1	YES	QNALGN > 0 include thrust misalignment angles
PCFTH	NO	1404	1	YES	Fractional increase in total impulse
CISP	NO	1414	1	YES	Specific impulse (sec) must be greater than zero
DWT	NO	1415	1	YES	Total store and propellant weight.
DWP	NO	1416	1	YES	Total propellant weight.
RDCGO	NO	1417	1	YES	Launch value of c.g.

VARIABLE NAME	RESET TO ZERO	C storage Location	VARIABLE'S DIMENSION	INPUT	DEFINITION
RDCGF	NO	1418	1	YES	Final c.g. position.
FMIYO	NO	1419	1	YES	Initial moments of inertia,
FMIYO	NO	1420	1	YES	
			1		
RLCGO	NO	1421	1	YES	Launch value of c.g.
RDELCO	YES	1308	1	NO	C.g. shift at each time.
DWP	YES	1409	1	NO	Weight of propellant used,
FTHRST	YES	1410	1	NO	Thrust value read in table.
FTHX	YES	1411	1	NO	Thrust in body axis system because of thrust alignment.
FTHY	YES	1412	1	NO	
FTHZ	YES	1413	1	NO	
RLCG	YES	1422	1	NO	C.g. location at each time.
DMASS	YES	1628	1	NO	Mass of store and propellant.

9. D11

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
VTARG	YES	1643	1	NO	Aircraft total velocity.
RXO	YES	1668	1	NO	Initial position of store WRT earth axis system.
RYO	YES	1669	1	NO	
RZO	YES	1670	1	NO	

10. D1

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
AGRAV	NO	1627	1	YES	Gravity
VXED	YES	1600	1	NO	Three components of velocity and accelerations of the store with respect to the earth axis system.
VXE	YES	1603	1	NO	
VYED	YES	1604	1	NO	
VYE	YES	1607	1	NO	
VZED	YES	1608	1	NO	
VZE	YES	1611	1	NO	
RXED	YES	1612	1	NO	Three components of position and velocity of the store WRT the earth axis system.
RXE	NO	1615	1	YES	
RYED	YES	1616	1	NO	
RYE	NO	1619	1	YES	
RZED	YES	1620	1	NO	
RZE	NO	1623	1	YES	

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
RTXED	NO	1648	1	NO	Three components of position and velocity of the aircraft WRT earth axis system.
RTXE	NO	1651	1	YES	
RTYED	NO	1652	1	NO	
RTYE	NO	1655	1	YES	
RTZED	NO	1656	1	NO	
RTZE	NO	1659	1	YES	
VTXE	NO	1660	1	NO	Three components of velocity of aircraft WRT earth axis system.
VTYE	NO	1661	1	NO	
VTZE	NO	1662	1	NO	
AXBA	NO	1624	1	NO	Three components of acceleration of the store WRT the body axis system,
AYBA	NO	1625	1	NO	
AZBA	NO	1626	1	NO	
VDELX	NO	1632	1	NO	The separation velocity of the store from the aircraft WRT earth axis system
VDELY	NO	1633	1	NO	
VDELZ	NO	1634	1	NO	
RDELX	NO	1635	1	NO	The separation distance of the store from the aircraft WRT earth axis system.
RDELY	NO	1636	1	NO	
RDELZ	NO	1677	1	NO	
DELX	NO	70	1	NO	Separation distance of the aircraft from the store WRT earth axis system.
DELY	NO	71	1	NO	
DELZ	NO	72	1	NO	

11. D2I

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
BPHIO	NO	1752	1	YES	Euler angles that located the body axis at time T=0 from the earth axis system.
BTHTO	YES	1753	1	YES	
BPSIO	YES	1754	1	YES	

12. D2

VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
CRAD	NO	1751	1	YES	57.3
OPTN3	NO	3504	1	YES	OPTN3>0 roll acceleration is locked to zero.
CFA11D	YES	1700	1	NO	Elements and their derivative of the matrix that orients the body axis WRT the earth axis system,
CFA11	YES	1703	1	NO	
CFA12D	YES	1704	1	NO	
CFA12	YES	1707	1	NO	
CFA13D	YES	1708	1	NO	
CFA13	YES	1711	1	NO	
CFA21D	YES	1712	1	NO	
CFA21	YES	1715	1	NO	
CFA22D	YES	1716	1	NO	
CFA22	YES	1719	1	NO	
CFA23D	YES	1720	1	NO	
CFA23	YES	1723	1	NO	
CFA31D	YES	1724	1	NO	
CFA31	YES	1727	1	NO	

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VARIABLE NAME	RESET TO ZERO	C STORAGE LOCATION	VARIABLE'S DIMENSION	INPUT	DEFINITION
CFAS2D	YES	1728	1	NO	Elements and their derivatives of the e matrix that orients the body axis WRT the earth axis system
CFAS2	YES	1731	1	NO	
CFAS3D	YES	1732	1	NO	
CFAS3	YES	1735	1	NO	
WPD	YES	1736	1	NO	Roll, pitch and yaw Euler angle velocities and accelerations.
WP	NO	1739	1	YES	
WQD	YES	1740	1	NO	
WQ	NO	1743	1	YES	
WRD	YES	1744	1	NO	
WR	NO	1747	1	YES	

APPENDIX IV

INPUT DATA

1. TYPE 1 CARDS (See Figure IV-1)

Type 1 cards determine which output and staging subroutines will be called. The value located in columns 20 to 25 (I5 Format) is the determining factor. Under normal operation there should be the following type 1 cards:

<u>Column 2</u>	<u>Columns 9 to 15</u>	<u>Column 25</u>
1	OUPT 2,3	3
1	STAG 2,3	4

These two cards will allow SUBL2 to call STAG2 and OUPT2 and SUBL3 to call STAG3 and OUPT3.

2. TYPE 2 CARDS (See Figure IV-1)

Type 2 cards determine which regular or functional subroutines are called and the order of calling. The value located in columns 20 to 25 (I5 Format) is the determining factor. Under normal operation, there should be the following type 2 cards.

<u>Column 2</u>	<u>Columns 9 to 15</u>	<u>(Right-Hand Justified)</u> <u>Columns 20 to 25</u>
2	G2	23
2	G3	24
2	G5	26
2	A1	2
2	A3	4
2	A2	3
2	D1	17
2	D2	18

These type 2 cards will allow subroutines AUXI and AUXSUB to call subroutines G2, G3, G5, A1, A3, A2, D1, D2 in consecutive order.

3. TYPE 3 CARDS (See Figure IV-1)

Type 3 cards can initialize any variable found in the C array. To keep the input list short and simple, the core of the computer should be cleared to zero by a control card; or a loop that zeros the entire C array

DESCRIPTION TYPE COLUMN NO.	VARIABLE NAME			C LOCATION		VARIABLE'S VALUE	RESET FLAG	
	2 3	9	20	21	25	31 45	46 60	
FORMAT	I2	A6	A6	A6	I5	5X	E15.9	E15.9
	1	XX	XX	XX	XXXXX		BLANK	BLANK
	2	XX	XX	XX	XXXXX		BLANK	BLANK
	3	XX	XX	XX	XXXXX		XXXXX	OPTIONAL
	4	--	XX	XX	XXXX		BLANK	BLANK
	7	--	XX	XX	XXXX		BLANK	BLANK
	6	BLANK			BLANK		BLANK	BLANK

Figure IV-1. Format for Input Cards

should be inserted at the beginning of the program. This will initialize all variables to zero and only non-zero variables will have to be read in by type 3 cards. An exception to this occurs for multiple runs. Any input variable that is initially zero, but has its value calculated during the trajectory and is not set to zero in RESET SUBROUTINE, must be either read in initially as zero and have the reset parameter 1. punched in columns 46 through 61 or be read in as zero for each run after the first. The reset parameter allows the initial value of the variable to be stored in the VALUE array, and at the end of each run, the parameters are reinitialized to the initial value.

For normal operation, the following type 3 cards should be included:
(See Figure IV-1)

<u>Column 2</u>	<u>Columns 9 to 15</u>	<u>Columns 20 to 25</u>	<u>Columns 31 to 45</u>	<u>Columns 46 to 61</u>
3	TF	2001	--	--
3	T	2000	0.	1.
3	REPPLT	2006	1.	0.
3	PPP	2005	--	0.
3	CPP	2015	.1	--
3	DOC	2013	6.	1.
3	DER (1)	2664	.002	0.
3	OPTN4	3502	0.	0.
3	AGRAV	1627	32.174	0.
3	CRAD	1751	57.29577	0.
3	WP	1739	0.	1.
3	WQ	1743	0.	1.
3	WR	1747	0.	1.
3	RXE	1615	0.	1.
3	RYE	1619	0.	1.
3	RZE	1623	--	1.
3	RTXE	1651	0.	1.
3	RTYE	1655	0.	1.
3	RTZE	1659	--	--
3	EFORCX	1326	--	0.
3	EFORCY	1327	--	0.
3	EFORCZ	1328	--	0.
3	EMOMX	1329	--	0.
3	EMOMY	1330	--	0.
3	EMOMZ	1331	--	0.
3	EFT	1332	--	0.
3	EJD	1333	--	--
3	VMACH	204	--	--
3	CAA	1274	--	--
3	CNAA	1273	--	--
3	CMAA	1272	--	--

<u>Column 2</u>	<u>Columns 9 to 15</u>	<u>Columns 20 to 25</u>	<u>Columns 31 to 45</u>	<u>Columns 46 to 61</u>
3	CMQ	1207	--	0
3	CNR	1208	--	0
3	CLP	1206	--	0
3	ALPHA0	381	--	--
3	DIASC	69	--	--
3	TNOSOS	58	--	--
3	OPTNW	50	1.	1.
3	FMIYO	1419	--	0
3	FMIYO	1420	--	0
3	XTAIL	57	-4.	0.
3	XNOSE	59	2.17	0
3	XNOSE1	73	--	1.
3	RFLGTH	1307	--	0
3	RFAREA	1306	--	0.
3	DWT	1415	--	0
3	DWP	1416	1.	0
3	CISP	1414	1.	0
3	XINTER	1252	-1.0	1.
3	STEP	2010	--	--
3	XPOS	54	--	--
3	YPOS	55	--	--
3	ZPOS	56	--	--

OTHER POSSIBLE INPUTS

OPTN10	2022
PTLESS	2007
RKUTTA	1972
COUNTE	42
RLUG	1316
RAIL	1317
BALPHT	1401
BPHIT	1402
QNALGN	1403
PCFTH	1404
RDCGO	1417
RDCGF	1418
BPHIO	1752
BPHTO	1753
BPSIO	1754
OPTN3	3504
PLOTN2	1983
PLOTN4	1982
PLOTNO	2008

dimensional variables

length = ft

area = ft²

weight = lb

moment of inertia = slug - ft²

angles = degrees

4. TYPE 4 CARDS (See Figure IV-1)

Type 4 cards control the variables which have values that are printed out at regular periods of time (CPP). The variables are printed five per line in the order in which these cards appear in the deck. The label appearing in columns 9 to 20 is used as a header regardless of the "Program Name" of the variable. The C storage location of the variable appears in columns 21 to 25. A maximum of 50 such cards are allowed.

5. TYPE 7 CARDS (See Figure IV-1)

Type 7 cards control the variables to be plotted using the SC4020 microfilm plotter (hard copy). Labels and identification are the same as type 4 cards. If four variables are to be plotted such as (RXE, RZE, RTXE, RTZE), then they are set up on type 7 cards and PLOTN4 is set to 4. The variables on the first and third type 7 cards lie on the abscissa and the second and fourth on the ordinate. PLOTN4 can be set to 0; in which case, the program will expect the first type 7 card to be a PLOTN2 variety.

PLOTN2 is another full page plot option available for plotting one or more variables (ordinates) versus a single variable (abscissa). The program variable "PLOTN2" is set to the number of variables involved and the type 7 cards are placed directly after the seven cards that defined the PLOTN4 variables. The remaining variables are plotted three to a frame, versus time, where the variable PLOTNO must equal the total number of type 7 cards or plotted variables (15 maximum). The plotting interval in seconds is controlled by the input data parameter PPP. The total number of plotting points for each variable must be less than 300.

6. CARD ORDER FOR MULTIPLE RUNS

RUN 1 TYPE 1
 TYPE 2
 TYPE 3
 TYPE 4
 TYPE 7
 TYPE 6

RUN 2 TYPE 3
 TYPE 6

RUN 3 TYPE 3
 TYPE 6

ETC.

APPENDIX V

EXAMPLE 1

The first example is a multiple run that simulates the trajectory of an M-117 bomb from the bottom station of the triple ejector rack (T3). The flow field data used in simulating the trajectories were collected in the presence of M-117 bombs in configuration T3 at $M=.85$ and angle of attack = 0.3 . The first trajectory occurs at $M=.85$ and angle = 0.3 degree. All the scale factors are 1.. The second launch occurs at $M=.5$. The ejector force is 1200 pounds and acts until the bomb is 0.255 foot down from its initial position. The trajectory is allowed to run for only 1 second.

EXAMPLE I. PROGRAM TEXT

```

PROGRAM          SIXD                                CDC 6600 FTN V3.0-P304 OPT=1 30
      PROGRAM SIXD(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT,FILMPL)
C
C*****DIMODS TO BE USED WITH FORTRAN AMRK INTEGRATION ROUTINE
C
5      COMMON      C(3510)          ,GRAPH          ,TEMPS(1000)
      EQUIVALENCE (C(2662),HMIN ), (C(2663),HMAX ), (C(2664),DER ),
C          (C(2561),N ), (C(2562),IPL ), (C(2965),VAR ),
C          (C(2000),T ), (C(2011),KSTEP ), (C(2010),STEP ),
10     C          (C(2012),LSTEP ), (C(2008),PLOTNO), (C(2009),NOPLOT),
C          (C(2023),OPOINT), (C(2025),TIME ), (C(2325),VLABLE),
C          (C(3167),NOOUT ), (C(2022),OPTN10), (C(2006),REPPLT),
C          (C(2865),EU ), (C(2765),EL ), (C(2007),PTLESS)
      EQUIVALENCE (C(1971),RITE ), (C(1972),RKUTTA)
      EQUIVALENCE (C(1973),KASE ), (C(1974),NJ ), (C(1975),NPT )
15     DIMENSION GRAPH(300,15) , TIME(300)
      DIMENSION VLABLE(2,15) , IPL(100) , DER(101)
      DIMENSION VAR(101) , EL(100) , EU(100)
      EQUIVALENCE (C(1980),RN )
      EQUIVALENCE (C(1981),RNT )
20     EQUIVALENCE (C(1982),PLOTN4)
      EQUIVALENCE (C(1983),PLOTN2)
      EQUIVALENCE (C(1984),NPLOT )
      INTEGER OPOINT
      INTEGER OPT
25     EXTERNAL AUXSUB
      NPT=2
      CALL COUNTV
      1000 CALL ZERO
      1001 NPT=2
30     IF(PLOTNO.LE.0.) GO TO 7
      IF(REPPLT.GT.0.)GOTO7
C
C          REPPLT = 0. USE NEW NO.4,7 (DISCARD OLD)
C          1. USE OLD PLUS THOSE ADDED
35     C          -1. USE NEW NO. 7 (DISCARD OLD)
      IF (REPPLT.GT.-1.0) NOOUT = 0
      NPLOT=0
      7 CALL OINPT1
      KASE=0
40     IF(RKUTTA.GT.0.0) NPT=1
      LSTEP = STEP
      NPLOT4=PLOTN4
      NPLOT2=PLOTN2
      NOPLOT=PLOTNO
45     1002 CONTINUE
      1003 CALL AUXI
      1004 CALL SUBL2
      1005 DO 60 I = 2,N
          J = IPL(I-1)
50         EL(I-1)=C(J+1)
          EU(I-1)=C(J+2)
          VAR(I) = C(J+3)
          60 DER(I) = C(J)
          VAR(1) = T
55     1006 CALL AUXSUB

```

PROGRAM SIXD

CDC 6600 FTN V3.0-P304 OPT=1 30

```
1007 NJ=N-1
      CALL AMRK(AUXSUB)
1008 DO 50 I = 2, N
      J = IPL(I-1)
60      50 C(J+3) = VAR(I)
      T = VAR(1)
1009 CALL  SUBL3
      IF ( KSTEP .EQ. 1 ) GO TO 1007
      DO 155 JV=2,N
65      155 VAR(JV)=0.
      CALL RESET
      IF(LSTEP.EQ.5.OR.LSTEP.EQ.7.OR.NOPLT.EQ.0)GOTO5
      CALL TIMEV(DELT)
      WRITE(6,96)DELT
70      96 FORMAT(1H ,17HSTART PLOTTING ATF14.7)
      LESSPT=PTLESS
      OPOINT=OPOINT-LESSPT
      CALL PLOT4(GRAPH,OPOINT,VLABLE,TIME,NPLOT4,NPLOT2,NOPLT)
      CALL PLOT2(GRAPH,OPOINT,VLABLE,TIME,NPLOT4,NPLOT2,NOPLT)
75      CALL PLOTN(GRAPH,OPOINT,VLABLE,TIME,NPLOT4,NPLOT2,NOPLT)
      CALL TIMEV(DELT)
      WRITE(6,97)DELT
      97 FORMAT(1H ,18HPLOTTING ENDED AT F14.7)
      IF((RNT.GT.0.1 .AND. RN.EQ.RNT).AND. LSTEP.EQ.2)GO TO 70
80      5 GO TO (1000,1001,1002,1003,1004,1005,1006,1007,1008,1009,1010),
      1 LSTEP
1010 IF(OPTN10.GT.0.) CALL DUMPO
      70 CALL S8
      CALL EXIT
85      FND
```

BLOCK DATA CCL2

CDC 6600 FTN V3.0-P304 OPT=1 3

```

BLOCK DATA CCL2
COMMON/NCL2/NCL2(4)
*   /CL2ARG/ALP(7),AM(5)
*   /CL2FUN/CL2(35)
5   DATA NCL2/7,5,0,0/
    DATA ALP/0., 4., 8., 12., 16., 20.,50./
    DATA AM/0., .6, .9, 1.1, 1.4/
    DATA CL2/
10  * 0., .05, .05, .05, .05, .05, .05,
    * 0., .05, .05, .05, .05, .05, .05,
    * 0., .05, .05, .05, -.1, -.05, -.05,
    * 0., .05, .10, 0., -.15, -.4, -.6,
    * 0., .05, .1, -.05, -.2 , -.55, -.8/
    END
```

BLOCK DATA CX00

CDC 6600 FTN V3.0-P304 OPT=1 3

5

```
BLOCK DATA CX00
COMMON /NCX0/NCX0(2)
*      /CX0ARG/AM(8)
*      /CX0FUN/CX0(8)
DATA NCX0/8,0/
DATA AM/0., .75, .85, .95, 1., 1.1, 1.2, 1.4/
DATA CX0/
* .06, .074, .074, .14, .14, .14, .14, .14/
END
```


BLOCK DATA THST

COC 6600 FTN V3.0-P304 OPT=1 3

```

      BLOCK DATA THST
      COMMON/NTH/NTH(2)
      *      /THARG/THA(13)
      *      /THFUN/THF(13)
5     DATA NTH/13,0/
      DATA THA/
      *0.0, .08,.16, .4, .56, .72, .8, 1.6, 2.4, 4., 4.8, 5.6, 100./
      DATA THF/
10    *0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
      END
```

```

BLOCK DATA VZC
COMMON/NVZ/NVZ(3)
* /VZARG/YLOP(7),ZLOP(9),XLOP(10)
* /VZFUN/VZ1(63),VZ2(63),VZ3(63),VZ4(63),VZ5(63),VZ6(63),VZ7(63)
5 * ,VZ8(63),VZ9(63),VZ10(63)
DATA NVZ/7,9,10/
DATA YLOP/1.,2.,3.,4.,5.,6.,7./
DATA ZLOP/1.,2.,3.,4.,5.,6.,7.,8.,9./
DATA XLOP/9.,10.,11.,12.,13.,14.,15.,16.,17.,20./
10 DATA VZ1/
C -.010, -.085, -.159, .025, .001, .002, .003,
C -.028, -.045, -.039, -.025, -.012, -.003, -.001,
C -.025, -.029, -.028, -.022, -.012, -.007, -.005,
15 C -.020, -.022, -.023, -.018, -.014, -.008, -.004,
C -.017, -.019, -.019, -.017, -.012, -.005, -.002,
C -.014, -.017, -.016, -.015, -.009, -.003, -.001,
C -.011, -.012, -.012, -.011, -.006, -.002, -.001,
C -.009, -.008, -.008, -.007, -.005, -.001, -.002,
C -.005, -.006, -.005, -.005, -.004, .000, -.001/
20 DATA VZ2/
C .026, .035, .045, .026, .011, .009, .007,
C -.002, -.013, -.019, -.026, -.010, -.002, -.000,
C -.012, -.018, -.024, -.025, -.017, -.010, -.007,
25 C -.015, -.019, -.024, -.023, -.019, -.011, -.006,
C -.015, -.018, -.021, -.020, -.016, -.008, -.004,
C -.013, -.016, -.017, -.016, -.011, -.005, -.002,
C -.010, -.012, -.013, -.012, -.007, -.003, -.002,
C -.008, -.008, -.008, -.008, -.006, -.001, -.002,
C -.004, -.006, -.005, -.005, -.004, .000, -.001/
30 DATA VZ3/
C .024, .068, .111, -.130, .024, .017, .010,
C -.004, -.021, -.063, -.130, -.051, -.012, -.003,
C -.016, -.031, -.061, -.083, -.054, -.025, -.012,
35 C -.017, -.028, -.041, -.046, -.038, -.022, -.011,
C -.016, -.022, -.028, -.030, -.024, -.014, -.007,
C -.013, -.018, -.020, -.020, -.015, -.007, -.004,
C -.010, -.013, -.013, -.013, -.009, -.004, -.002,
C -.008, -.008, -.008, -.008, -.006, -.002, -.002,
C -.004, -.005, -.004, -.005, -.004, .000, -.001/
40 DATA VZ4/
C .006, .036, .066, -.254, .028, .019, .010,
C -.013, -.036, -.138, -.254, -.113, -.021, -.004,
C -.021, -.044, -.100, -.145, -.089, -.033, -.014,
45 C -.020, -.033, -.052, -.061, -.046, -.026, -.012,
C -.016, -.023, -.030, -.033, -.026, -.014, -.006,
C -.012, -.017, -.019, -.020, -.014, -.006, -.003,
C -.008, -.011, -.012, -.012, -.007, -.003, -.001,
C -.006, -.006, -.007, -.006, -.004, -.000, -.001,
C -.002, -.004, -.003, -.003, -.002, .002, .000/
50 DATA VZ5/
C -.002, -.011, -.021, -.022, -.022, -.010, .002,
C -.014, -.032, -.019, -.022, .012, -.011, -.003,
C -.015, -.024, -.031, -.020, -.017, -.009, -.005,
55 C -.013, -.017, -.021, -.018, -.015, -.007, -.003,
C -.010, -.013, -.015, -.013, -.010, -.003, .000,

```

	C	-.007,	-.010,	-.010,	-.009,	-.005,	.000,	.002,
	C	-.005,	-.006,	-.006,	-.006,	-.002,	.002,	.002,
	C	-.003,	-.003,	-.003,	-.002,	-.001,	.003,	.002,
	C	.000,	-.001,	-.000,	-.000,	.000,	.004,	.002/
60		DATA VZ6/						
	C	.001,	-.031,	-.063,	.089,	-.060,	-.034,	-.007,
	C	-.006,	-.018,	.016,	.089,	.045,	-.005,	-.002,
	C	-.004,	-.000,	.020,	.048,	.029,	.010,	.001,
	C	-.002,	.002,	.010,	.017,	.014,	.008,	.005,
65		C	-.002,	-.000,	.003,	.006,	.006,	.008,
	C	-.001,	-.002,	.000,	.001,	.004,	.008,	.007,
	C	-.000,	-.001,	.000,	.001,	.004,	.007,	.006,
	C	.000,	.001,	.002,	.002,	.003,	.006,	.005,
	C	.002,	.002,	.003,	.002,	.003,	.006,	.004/
70		DATA VZ7/						
	C	.005,	-.027,	-.059,	.075,	-.063,	-.039,	-.014,
	C	-.001,	-.012,	.000,	.075,	.029,	-.007,	-.004,
	C	.001,	.005,	.025,	.045,	.032,	.011,	.002,
	C	.003,	.008,	.016,	.022,	.018,	.012,	.008,
75		C	.003,	.006,	.009,	.011,	.011,	.012,
	C	.003,	.003,	.005,	.006,	.009,	.011,	.010,
	C	.003,	.003,	.005,	.005,	.008,	.010,	.008,
	C	.003,	.004,	.005,	.005,	.006,	.009,	.007,
	C	.005,	.004,	.006,	.005,	.006,	.009,	.006/
80		DATA VZ8/						
	C	.000,	-.028,	-.056,	.061,	-.046,	-.034,	-.021,
	C	-.001,	-.009,	.000,	.061,	.020,	-.006,	-.006,
	C	.002,	.005,	.020,	.038,	.027,	.009,	.001,
	C	.005,	.008,	.014,	.020,	.016,	.012,	.007,
85		C	.005,	.007,	.010,	.012,	.012,	.013,
	C	.005,	.005,	.007,	.008,	.010,	.013,	.011,
	C	.005,	.006,	.006,	.007,	.010,	.012,	.010,
	C	.005,	.006,	.007,	.007,	.008,	.011,	.008,
	C	.007,	.006,	.007,	.007,	.007,	.010,	.008/
90		DATA VZ9/						
	C	-.003,	-.020,	-.038,	.042,	-.030,	-.026,	-.022,
	C	.001,	-.004,	-.000,	.042,	.016,	-.005,	-.006,
	C	.004,	.006,	.015,	.028,	.021,	.008,	.001,
	C	.006,	.009,	.013,	.017,	.014,	.012,	.008,
95		C	.007,	.008,	.010,	.011,	.011,	.014,
	C	.007,	.007,	.008,	.009,	.011,	.014,	.012,
	C	.007,	.007,	.008,	.008,	.011,	.013,	.011,
	C	.007,	.008,	.008,	.009,	.009,	.012,	.010,
	C	.008,	.008,	.009,	.008,	.009,	.011,	.009/
100		DATA VZ10/						
	C	.004,	.003,	.002,	.039,	-.014,	-.014,	-.014,
	C	.007,	.006,	.009,	.039,	.019,	.000,	-.002,
	C	.008,	.010,	.016,	.027,	.021,	.011,	.004,
	C	.010,	.012,	.014,	.018,	.015,	.013,	.010,
105		C	.010,	.010,	.011,	.012,	.012,	.015,
	C	.009,	.009,	.010,	.010,	.012,	.015,	.014,
	C	.009,	.009,	.009,	.009,	.012,	.014,	.012,
	C	.008,	.009,	.010,	.010,	.010,	.013,	.011,
	C	.010,	.009,	.010,	.009,	.010,	.013,	.010/
110		END						

```

BLOCK DATA VYC
COMMON/NVY/NVY(3)
* /VYARG/YLOP(7),ZLOP(9),XLOP(10)
* /VYFUN/VY1(63),VY2(63),VY3(63),VY4(63),VY5(63),VY6(63),VY7(63)
5 * ,VY8(63),VY9(63),VY10(63)
DATA NVY/7,9,10/
DATA YLOP/1.,2.,3.,4.,5.,6.,7./
DATA ZLOP/1.,2.,3.,4.,5.,6.,7.,8.,9./
DATA XLOP/9.,10.,11.,12.,13.,14.,15.,16.,17.,20./
10 DATA VY1/
C -.043, -.023, .016, .027, .039, .035, .032,
C -.018, -.004, .024, .028, .032, .033, .030,
C -.007, -.000, .011, .019, .025, .023, .022,
15 C -.003, .002, .007, .012, .013, .015, .018,
C .000, .002, .005, .008, .011, .014, .017,
C -.003, .000, .004, .008, .011, .013, .014,
C -.004, .000, .004, .007, .010, .011, .011,
C -.003, -.001, .003, .006, .008, .008, .009,
C -.003, .000, .002, .004, .006, .006, .008/
20 DATA VY2/
C -.017, -.043, -.096, -.026, .044, .039, .037,
C -.022, -.019, .000, .017, .034, .039, .035,
C -.014, -.011, -.001, .013, .026, .028, .026,
25 C -.008, -.005, .001, .009, .014, .018, .020,
C -.003, -.002, .002, .006, .011, .015, .018,
C -.005, -.002, .002, .007, .011, .013, .014,
C -.005, -.001, .003, .007, .010, .011, .011,
C -.003, -.001, .002, .006, .007, .008, .009,
C -.003, -.000, .002, .003, .005, .006, .008/
30 DATA VY3/
C -.029, -.085, -.196, -.036, .125, .076, .051,
C -.038, -.058, -.072, .015, .103, .073, .050,
C -.026, -.032, -.026, .014, .051, .047, .036,
35 C -.015, -.014, -.007, .009, .022, .026, .025,
C -.006, -.005, -.001, .006, .013, .018, .020,
C -.007, -.003, .001, .006, .012, .014, .015,
C -.006, -.002, .002, .006, .010, .011, .011,
C -.004, -.002, .002, .005, .007, .008, .009,
C -.003, -.000, .001, .003, .005, .006, .007/
40 DATA VY4/
C -.040, -.102, -.227, -.014, .200, .105, .058,
C -.046, -.084, -.211, .008, .227, .099, .055,
C -.030, -.043, -.048, .014, .071, .057, .038,
45 C -.016, -.017, -.011, .009, .025, .027, .025,
C -.007, -.006, -.002, .005, .013, .017, .019,
C -.006, -.003, .001, .006, .011, .013, .013,
C -.005, -.002, .001, .005, .009, .010, .010,
C -.004, -.002, .001, .005, .006, .007, .008,
C -.003, -.000, .001, .003, .005, .005, .007/
50 DATA VY5/
C -.022, -.041, -.079, -.004, .071, .047, .035,
C -.024, -.027, .049, .011, -.027, .030, .029,
C -.013, -.011, -.000, .015, .021, .021, .019,
55 C -.006, -.004, .002, .007, .010, .011, .013,
C -.001, -.001, .002, .004, .007, .009, .012,

```

	C	-.003,	-.001,	.001,	.004,	.007,	.009,	.010,
	C	-.003,	-.001,	.002,	.004,	.007,	.008,	.008,
	C	-.003,	-.001,	.001,	.004,	.005,	.006,	.006,
	C	-.003,	.000,	.001,	.003,	.004,	.005,	.006/
60		DATA VY6/						
	C	.006,	.028,	.071,	.026,	-.019,	.004,	.016,
	C	.002,	.021,	.119,	.012,	-.096,	-.016,	.007,
	C	.006,	.016,	.031,	.011,	-.013,	-.008,	.001,
	C	.005,	.009,	.012,	.006,	-.003,	-.004,	.002,
65		C	.005,	.006,	.005,	.003,	.001,	.002,
	C	.001,	.002,	.003,	.004,	.005,	.005,	.005,
	C	-.001,	.001,	.003,	.005,	.006,	.006,	.005,
	C	-.001,	-.000,	.002,	.005,	.005,	.005,	.004,
	C	-.002,	.001,	.002,	.003,	.003,	.004,	.004/
70		DATA VY7/						
	C	.017,	.039,	.082,	.017,	-.047,	-.008,	.012,
	C	.010,	.023,	.103,	.007,	-.088,	-.021,	.001,
	C	.012,	.020,	.032,	.007,	-.016,	-.014,	-.005,
	C	.009,	.013,	.013,	.005,	-.007,	-.009,	-.003,
75		C	.008,	.008,	.007,	.002,	-.002,	-.002,
	C	.003,	.003,	.004,	.004,	.003,	.003,	.003,
	C	.001,	.002,	.004,	.005,	.005,	.004,	.003,
	C	.000,	.001,	.003,	.004,	.004,	.004,	.003,
	C	-.001,	.002,	.003,	.003,	.003,	.003,	.004/
80		DATA VY8/						
	C	.018,	.034,	.068,	.007,	-.054,	-.012,	.009,
	C	.009,	.018,	.078,	.005,	-.067,	-.019,	.000,
	C	.011,	.017,	.026,	.007,	-.014,	-.014,	-.006,
	C	.009,	.012,	.011,	.003,	-.007,	-.009,	-.004,
85		C	.008,	.007,	.005,	.001,	-.003,	-.003,
	C	.003,	.003,	.004,	.003,	.002,	.001,	.001,
	C	.001,	.002,	.003,	.004,	.004,	.003,	.002,
	C	.000,	.001,	.003,	.004,	.003,	.003,	.002,
	C	-.001,	.001,	.002,	.002,	.002,	.002,	.003/
90		DATA VY9/						
	C	.017,	.033,	.065,	.016,	-.032,	-.008,	.003,
	C	.006,	.012,	.057,	.004,	-.049,	-.015,	-.001,
	C	.008,	.012,	.018,	.005,	-.010,	-.012,	-.006,
	C	.007,	.009,	.008,	.002,	-.007,	-.009,	-.005,
95		C	.008,	.006,	.004,	.000,	-.003,	-.004,
	C	.003,	.002,	.003,	.002,	.001,	.001,	.001,
	C	.000,	.002,	.003,	.003,	.004,	.002,	.001,
	C	-.000,	.001,	.002,	.003,	.003,	.002,	.001,
	C	-.000,	.001,	.002,	.002,	.002,	.002,	.002/
100		DATA VY10/						
	C	.018,	.034,	.066,	.019,	-.028,	-.011,	-.002,
	C	.005,	.008,	.041,	.001,	-.040,	-.013,	-.002,
	C	.005,	.008,	.013,	.003,	-.010,	-.011,	-.007,
	C	.005,	.006,	.005,	.000,	-.008,	-.010,	-.005,
105		C	.006,	.004,	.002,	-.001,	-.004,	-.002,
	C	.002,	.002,	.002,	.001,	.001,	-.000,	-.000,
	C	-.000,	.001,	.002,	.003,	.003,	.001,	.000,
	C	.000,	.000,	.002,	.003,	.002,	.001,	.001,
	C	-.001,	.001,	.001,	.002,	.001,	.001,	.001/
110		END						

SUBROUTINE G2

COC 6600 FTN V3.0-P304 OPT=1 ↓

```
      SUBROUTINE G2
C**WIND AND GUSTS MOOULE
      COMMON C(3510)
      COMMON/NVZ/NVZ/VZARG/VZA/VZFUN/VZF
5     */NVY/NVY/VYARG/VYA/VYFUN/VYF
C**INPUT OATA
      EQUIVALENCE (C( 50),OPTNW )
      EQUIVALENCE (C(204),VMACH)
      EQUIVALENCE (C(120),PPP1)
10     EQUIVALENCE (C(121),CPP1)
      EQUIVALENCE (C(122),OER1)
      EQUIVALENCE (C(123),XTL)
      EQUIVALENCE (C(124),XLL)
      EQUIVALENCE (C(125),YTL)
15     EQUIVALENCE (C(126),YLL)
      EQUIVALENCE (C(127),ZTL)
      EQUIVALENCE (C(128),ZLL)
C**OUTPUT OATA
      EQUIVALENCE (C( 100),VWXE )
20     EQUIVALENCE (C( 101),VWYE )
      EQUIVALENCE (C( 102),VWZE )
C**INPUTS FROM OTHER MODULES
      EQUIVALENCE (C(1635),ROELX)
      EQUIVALENCE (C(1636),ROELY)
25     EQUIVALENCE (C(1637),ROELZ)
      EQUIVALENCE (C( 54),XPOS)
      EQUIVALENCE (C( 55),YPOS)
      EQUIVALENCE (C( 56),ZPOS)
      EQUIVALENCE (C( 57),XTAIL )
30     EQUIVALENCE (C(1648),RTXEO)
      EQUIVALENCE (C( 47),PHY2)
      EQUIVALENCE (C( 46),PHY3)
      EQUIVALENCE (C( 45),YLUN)
      EQUIVALENCE (C( 44),ZLUN)
35     EQUIVALENCE (C( 58),TNOSOS)
      EQUIVALENCE (C( 59),XNOSE)
      EQUIVALENCE (C( 60),AAN)
      EQUIVALENCE (C( 61),ASN)
      EQUIVALENCE (C( 62),PWZ1)
40     EQUIVALENCE (C( 63),PHY1)
      EQUIVALENCE (C( 43),CLMT)
      EQUIVALENCE (C( 48),CROFLO)
      EQUIVALENCE (C( 42),COUNT)
      EQUIVALENCE (C( 41),OBSTAL)
45     EQUIVALENCE (C( 67),XLUN)
      EQUIVALENCE (C( 69),DIASC)
      EQUIVALENCE (C( 90),XNPOS)
      EQUIVALENCE (C( 91),YNPOS)
      EQUIVALENCE (C( 92),ZNPOS)
50     EQUIVALENCE (C( 93),XTPOS)
      EQUIVALENCE (C( 94),YTPOS)
      EQUIVALENCE (C( 95),ZTPOS)
      EQUIVALENCE (C(1703),CFA11)
      EQUIVALENCE (C(1707),CFA12)
55     EQUIVALENCE (C(1711),CFA13)
```

```

        XT=CFA11*XTAIL
        YT=CFA12*XTAIL
        ZT=CFA13*XTAIL
        XN=CFA11*XNOSE
60      YN=CFA12*XNOSE
        ZN=CFA13*XNOSE
        XNPOS=RDELX -XN
        YNPOS=-RDELY +YN
        ZNPOS= -RDELZ + ZN
65      XTPDS=RDELX -XT
        YTPDS=-RDELY +YT
        ZTPDS= -RDELZ + ZT
        IF(CDUNTE .EQ.1.) RETURN
        IF(CDUNTE.EQ.2.) GO TO 10
70      IF(OPTNW.LE.0.) GO TO 10
        XLUN=(+RDELX-XN+XPOS) *.6
        YLUN=((-RDELY+YN)*DIASC +YPOS)*.6
        ZLUN=((-RDELZ+ZN)*DIASC-ZPOS)*.6
        XLUP=(+RDELX-XT+XPOS) *.6
75      YLUP=((-RDELY+YT)*DIASC +YPOS)*.6
        ZLUP=((-RDELZ+ZT)*DIASC-ZPOS)*.6
        PWZ1=0.0
        PWY1=0.0
        VWZE=0.
80      VWYE=0.
        AAN=0.
        ASN=0.
        IF(XLUP.GT.XTL.OR.XLUP.LT.XLL) GO TO 10
        IF(YLUP.GT.YTL. OR.YLUP.LT.YLL) GO TO 10
85      IF(ZLUP.GT.ZTL. OR.ZLUP.LT.ZLL) GO TO 10
        IF(XLUN.GT.XTL.OR.XLUN.LT.YLL) GO TO 112
        IF(YLUN.GT.YTL. OR.YLUN.LT.YLL) GO TO 112
        IF(ZLUN.GT.ZTL. OR.ZLUN.LT.ZLL) GO TO 112
        CALL TABL3 (YLUN,ZLUN,XLUN,VZA,VZF,NVZ,XINTER,4HPWZ1,PWZ1)
90      CALL TABL3(YLUN,ZLUN,XLUN,VYA,VYF,NVY,XINTER,4HPWY1,PWY1)
        FPMC=2.3832*VMACH**2 - 2.0232*VMACH + .9966
        PWZ1=PWZ1*FFMC
        PWY1=PWY1*FFMC
        PWZ1=-PWZ1
95      PWZ1=PWZ1/(TNOSOS*DIASC)
        PWY1=PWY1/(TNOSOS*DIASC)
        PWY2=PWY1
112     CALL TABL3 (YLUP,ZLUP,XLUP,VZA,VZF,NVZ,XINTER,4HPWZE,PWZE)
        CALL TABL3 (YLUP,ZLUP,XLUP,VYA,VYF,NVY,XINTER,4HPWYE,PWYE)
100     PWZE=-PWZE
        PWZE=PWZE*FFMC/(TNOSOS*DIASC)
        PWYE=PWYE*FFMC/(TNOSOS*DIASC)
        VWZE=(RTXED*PWZE)
        VWYE=(RTXED*PWYE)
105     PWY3=PWY2-PWYE
        PWZ1=PWZ1-PWZE
        AAN=ASIN(PWZ1)
        ASN=ASIN(PWY3)
110     RETURN
        10 VWXE = 0.

```

SUBROUTINE G2

CDC 6600 FTN V3.0-P304 OPT=1 3

```
115      VWYE = 0.  
        VWZE = 0.  
        AAN=0.  
        ASN=0.  
        COUNT=1.  
        C(2005)=PPP1  
        C(2015)=CPP1  
        G(2664)=DER1 /  
120      RETURN  
        END
```



```

C**AIR DATA MODULE G3
  SUBROUTINE G3
  COMMON C(3510)
5  C**INPUT DATA
    EQUIVALENCE (C(0208),RHZRO )
C**INPUTS FROM OTHER MODULES
    EQUIVALENCE (C(0100),VMXE )
    EQUIVALENCE (C(0101),VMYE )
    EQUIVALENCE (C(0102),VMZE )
10   EQUIVALENCE (C(1603),VXE )
    EQUIVALENCE (C(1607),VYE )
    EQUIVALENCE (C(1611),VZE )
    EQUIVALENCE (C(1623),RZE )
C**INPUTS FROM MAIN PROGRAM
15  C**STATE VARIABLE OUTPUTS
    C**NONE
    C**OTHER OUTPUTS
    EQUIVALENCE (C(0200),VMWXE )
    EQUIVALENCE (C(0201),VMWYE )
20   EQUIVALENCE (C(0202),VMWZE )
    EQUIVALENCE (C(0203),PDYNMC)
    EQUIVALENCE (C(0204),VMACH )
    EQUIVALENCE (C(0205),DRHO )
    EQUIVALENCE (C(0206),VSOUND)
25   EQUIVALENCE (C(0207),VAIRSP)
    EQUIVALENCE (C(0209),RH )
C**CALCULATE PRESENT ALTITUDE
    RH= -RZE+RHZRO
C**CALCULATE MISSILE VELOCITY WRT AIR MASS IN EARTH AXES
30   VMWXE = VXE-VMXE
    VMWYE = VYE-VMYE
    VMWZE = VZE-VMZE
    VAIRSP = SQRT (VMWXE*VMWXE+VMWYE*VMWYE+VMWZE*VMWZE)
C**AIR DENSITY, SPEED OF SOUND, DYNAMIC PRESSURE, AND MACH
35   DRHO=(.076475)/(1.+ .3325E-04*RH+RH*RH*RH*.02315E-12)
    VSOUND = -.00392*RH+1117.3
    PDYNMC = (DRHO*VAIRSP*VAIRSP)/64.344
    VMACH = VAIRSP/VSOUND
    RETURN
40   END

```

```

SUBROUTINE G4
C** ENO-OF-RUN CALCULATIONS SUBROUTINE G4
C** THIS IS A SUBROUTINE, NOT A MODULE.
C** IT IS CALLED BY STAGE 3 TO COMPUTE MISS OISTANCE ANO STOP THE
5 C** PROGRAM IF RANGE IS ZERO.
C*****
COMMON C(3510)
C**INPUT OATA
C**NONE
10 C**INPUTS FROM OTHER MODULES
EQUIVALENCE (C(1615),RXE )
EQUIVALENCE (C(1619),RYE )
EQUIVALENCE (C(1623),RZE )
EQUIVALENCE (C(2000),T )
15 C**STATE VARIABLE OUTPUTS
C**NONE
C**OTHER OUTPUTS
EQUIVALENCE (C(2020),LCONV )
C** MISS OISTANCE PARAMETERS ARE OUTPUT OIRECTLY ANO ARE NOT IN COMMON
C** TEST FOR INCREASING RANGE ANO SOLVE FOR TIME AT WHICH RANGE IS ZERO
5 FORMAT (1H0, 16H MISS DISTANCE= 1PE17.8/1H0,13H TIME FINAL=
C 1PE17.8)
6 FORMAT (1H0,10X,10HXM EARTH=1PE17.8,3X,10HYM EARTH=1PE17.8,3X,
C 10HZM EARTH=1PE17.8)
25 7 FORMAT (1H0,40X,10HY FLTPATH=1PE17.8,3X,10HZ FLTPATH=1PE17.8)
C** TEST FOR INCREASING RANGE ANO SOLVE FOR TIME AT WHICH RANGE IS ZERO
IF(RZE.LT.0.0) GO TO 10
UXYZ=RZE/(RZE-UZE)
RDY=RYE-(RYE-UYE)*UXYZ
30 ROX=RXE-(RXE-UXE)*UXYZ
RDZ=0.0
TZERO=T-(T-UT)*UXYZ
RMISS=SQRT(ROX**2 + ROY**2 + ROZ**2)
WRITE (6,5) RMISS,TZERO
35 WRITE (6,6) RDX, RDY, RDZ
LCONV=2
RETURN
10 UT = T
UXE = RXE
40 UYE = RYE
UZE = RZE
IF (RZE .GT. 100.) LCONV = 2
RETURN
END

```

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C**COORDINATE CONVERSION MODULE
  SUBROUTINE G5
  COMMON C(3510)

```

```

C

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5  C**INPUTS FROM OTHER MODULES
    EQUIVALENCE (C(0200),VMWXE )
    EQUIVALENCE (C(0201),VMWYE )
    EQUIVALENCE (C(0202),VMWZE )
    EQUIVALENCE (C(1603),VXE   )
10  EQUIVALENCE (C(1607),VYE   )
    EQUIVALENCE (C(1611),VZE   )
    EQUIVALENCE (C(1668),RXO   )
    EQUIVALENCE (C(1669),RYO   )
    EQUIVALENCE (C(1670),RZO   )
15  EQUIVALENCE (C(1703),CFA11 )
    EQUIVALENCE (C(1707),CFA12 )
    EQUIVALENCE (C(1711),CFA13 )
    EQUIVALENCE (C(1715),CFA21 )
    EQUIVALENCE (C(1719),CFA22 )
20  EQUIVALENCE (C(1723),CFA23 )
    EQUIVALENCE (C(1727),CFA31 )
    EQUIVALENCE (C(1731),CFA32 )
    EQUIVALENCE (C(1735),CFA33 )
    EQUIVALENCE (C(1739),WP    )
25  EQUIVALENCE (C(1743),WQ    )
    EQUIVALENCE (C(1747),WR    )
    EQUIVALENCE (C(1751),CRAD  )
    EQUIVALENCE (C(3504),OPTN4)

```

```

C

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30  C**OTHER OUTPUTS
    EQUIVALENCE (C(0350),BTHT  )
    EQUIVALENCE (C(0351),BPSI  )
    EQUIVALENCE (C(0352),BPHI  )
    EQUIVALENCE (C(0353),BTHTD )
35  EQUIVALENCE (C(0354),BPSID )
    EQUIVALENCE (C(0355),BPHID )
    EQUIVALENCE (C(0356),VTOTE )
    EQUIVALENCE (C(0360),VMWU  )
    EQUIVALENCE (C(0361),VMWV  )
40  EQUIVALENCE (C(0362),VMWW  )
    EQUIVALENCE (C(0367),BALPHA)
    EQUIVALENCE (C(0368),BALPHY)
    EQUIVALENCE (C(0369),BALPHP)
    EQUIVALENCE (C(0370),BPHIP )
45  EQUIVALENCE (C( 380),RANGO )
    EQUIVALENCE (C(381),ALPHA0)

```

```

C

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```

C**CALCULATION OF HEADING, PITCH, ROLL EULER ANGLES IN DEGREES
  BPHI = ATAND(CFA23,CFA33)
50  BTHT = ATAND(-CFA13,SQRT(CFA11*CFA11+CFA12*CFA12))
  BPSI = ATAND(CFA12,CFA11)

```

```

C

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```

  IF(COSD(BTHT).EQ.0.0) GO TO 5
  BPSID = (WQ*SIND(BPHI)+WR*COSD(BPHI))/COSD(BTHT)
55  5  CONTINUE

```

```
      BPHID = WP+BPSID*SIND(BTHT)
      BHTD = WQ*COSD(BPHI)-WR*SIND(BPHI)
C
C**CALCULATION OF TOTAL VELOCITY
60      VTOTE = SQRT(VXE*VXE+VYE*VYE+VZE*VZE)
C
      RANGD = SQRT( (RXE-RXD)**2 + (RYE-RYD)**2 + (RZE-RZD)**2)
C
      IF ((DPTN4 .GT. 0.) .AND. (T .LT. DER)) GO TO 30
65      C**VELOCITY WRT AIR IN BDDY AXES
      VMWU = CFA11*VMWXE+CFA12*VMWYE+CFA13*VMWZE
      VMWV = CFA21*VMWXE+CFA22*VMWYE+CFA23*VMWZE
      VMWW = CFA31*VMWXE+CFA32*VMWYE+CFA33*VMWZE
C
70      C**VERTICAL AND HORIZONTAL ANGLES OF ATTACK
      BALPHA = ATAND(VMWV,VMWU)
      BALPHA=BALPHA+ALPHA0
      BALPHY = ATAND(VMWV,VMWU)
C**ALPHA PRIME AND PHI PRIME (WIND TUNNEL AXES)
75      IF ((BALPHA-BALPHY).EQ.0.) GO TO 30
      BPHIP = ATAND(BALPHY,BALPHA)
      30 BALPHP=SQRT(BALPHA**2+BALPHY**2)
      RETURN
      END
```

```

      SUBROUTINE A1
C
      COMMON C(3510)
C
5     C**TABLE LOOKUP FOR BODY FORCE COEFFICIENTS
      COMMON /NCXO /NCXO /CXOARG/ CXOA /CXOFUN/ CXOF
      1          /NCXCP / NCX /CXARG /CXA /CXFUN /CXF
      2          /NCZ /NCN /CZARG /CNA /CZFUN /CNF
10     3          /NOCZ/NCDCN /DCZARG/COCNA /OCZFUN/COCNF
      5          /NCY2 /NCY2 /CY2ARG/ CY2A /CY2FUN/ CY2F
C
      C**TABLE LOOKUP FOR BODY MOMENT COEFFICIENTS
      1          /NCL2/NCL2 /CL2ARG/ CL2A /CL2FUN/ CL2F
15     2          /NCL3/ NCL3 /CL3ARG/ CL3A /CL3FUN/ CL3F
      5          /NCM/ NCM /CMARG / CMA /CMFUN / CMF
      6          /NOCM/ NOCM /OCMARG/ COCMA /OCMFUN/ COCMF
      8          /NCN2/ NCN2 /CN2ARG/ CN2A /CN2FUN/ CN2F
      */NCLP/ NCLP /CLPARG/ CLPA /CLPFUN/ CLPF
      */NCMQ/ NCMQ /CMQARG/ CMQA /CMQFUN/ CMQF
20     C
      C**TABLE LOOKUP FOR SURFACE COEFFICIENTS
      COMMON /NCZO/ NCZO /CZOARG/ CZDA /CZOFUN/ CZDF
      2          /NCLD/ NCLD /CLOARG/ CLOA /CLOFUN/ CLOF
25     3          /NCMD/ NCMO /CMOARG/ CMOA /CMDFUN/ CMOF
C
      C** INPUT DATA
      EQUIVALENCE (C(1252),XINTER)
C
30     C**INPUTS FROM OTHER MODULES
      EQUIVALENCE (C(0204),VMACH )
      EQUIVALENCE (C(0367),BALPHA)
      EQUIVALENCE (C(0368),BALPHY)
      EQUIVALENCE (C(0369),BALPHP)
      EQUIVALENCE (C(0370),BPHIP )
35     C
      C**INPUTS FROM MAIN PROGRAM
      EQUIVALENCE (C(2000),T )
      EQUIVALENCE (C(2664),OER )
C
40     C**OUTPUTS - COEFFICIENTS FOR BODY FORCES
      EQUIVALENCE (C(1203),CX )
      C**OUTPUTS - COEFFICIENTS FOR BODY MOMENTS
      EQUIVALENCE (C(1206),CLP )
45     EQUIVALENCE (C(1207),CMQ )
      EQUIVALENCE (C(1208),CNR )
      EQUIVALENCE (C(1209),CL )
      EQUIVALENCE (C(1210),CM )
      EQUIVALENCE (C(1211),CN )
      EQUIVALENCE (C(1240),CL2 )
50     EQUIVALENCE (C(1247),CMP )
      EQUIVALENCE (C(1248),CNP )
      EQUIVALENCE (C(1249),CLR )
C
55     C**OUTPUTS - COEFFICIENTS FOR SURFACE EFFECTS, AND TOTAL EFFECTS
      EQUIVALENCE (C(1204),CY )

```

SUBROUTINE A1

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```

        EQUIVALENCE (C(1205),CZ      )
        EQUIVALENCE (C(1209),CL      )
        EQUIVALENCE (C(1210),CM      )
        EQUIVALENCE (C(1211),CN      )
60      EQUIVALENCE(C(1272),CMAA)
        EQUIVALENCE(C(1273),CNAA)
        EQUIVALENCE(C(1274),CAA)
        EQUIVALENCE(C(1250),P)
C
65      C INPUT VARIABLE XINTER IS THE INTERPOLATION CONTROL
C        LESS THAN ZERO - STRAIGHT LINE INTERPOLATION
C        POSITIVE - PARABOLIC INTERPOLATION , WITH END INTERVAL
C          INTERPOLATION (0. TO 1.)
C          0.0 - STRAIGHT LINE
70      C          1.0 - FULL PARABOLIC
C
C
C        IF(P.EQ.0..AND.T.LE.DER) UTIME=-1.
C        IF (T-UTIME .LE. 0.) RETURN
75      P=1.
        UTIME= T
C
C MULTIPLE ANGLE FORMULAE AND ABSOLUTE VALUES OF ANGLE OF ATTACK
80      USPHI = SIN0(BPHIP)
        UCPHI = COS0(BPHIP)
        CX=CAA
        CNP=CNAА*BALPHP
        CMP=CMAA*BALPHP
        CL2=.05
85      US4PHI=SINO(4.*BPHIP)
        CLR=CL2*US4PHI
        CY=-CNP*USPHI
        CZ=-CNP*UCPHI
        CM=CMP*UCPHI
90      CN=-CMP*USPHI
        CL=CLR
        RETURN
        ENO
```

```

C**AERO FORCE AND MOMENT MODULE   BODY AXES
      SUBROUTINE A2
      COMMON C(3510)

```

```

C

```

```

5  C**INPUT DATA
      EQUIVALENCE (C(1306),RFAREA)
      EQUIVALENCE (C(1307),RFLGTH)
      EQUIVALENCE (C(1308),RDELGC)
      EQUIVALENCE (C(1313),RFXCG )
10  EQUIVALENCE (C(1314),RFYCG )
      EQUIVALENCE (C(1315),RFZCG )
      EQUIVALENCE (C(1316),RLUG  )
      EQUIVALENCE (C(1317),RAIL  )
      EQUIVALENCE (C(1627),AGRAV )
15  EQUIVALENCE (C(3504),OPTN4 )
      EQUIVALENCE (C(1360),EMA )
      EQUIVALENCE (C(1361),SFORCZ)
      EQUIVALENCE (C(1362),SFORCY)

```

```

C

```

```

20  C**INPUTS FROM OTHER MODULES
      EQUIVALENCE (C(0203),PDYNMC)
      EQUIVALENCE (C(0207),VAIRSP)
      EQUIVALENCE (C( 350),BTHT  )
      EQUIVALENCE (C( 380),RANG0 )
25  EQUIVALENCE (C(1203),CX   )
      EQUIVALENCE (C(1204),CY   )
      EQUIVALENCE (C(1205),CZ   )
      EQUIVALENCE (C(1206),CLP  )
      EQUIVALENCE (C(1207),CMQ  )
30  EQUIVALENCE (C(1208),CNR  )
      EQUIVALENCE (C(1209),CL   )
      EQUIVALENCE (C(1210),CM   )
      EQUIVALENCE (C(1211),CN   )
      EQUIVALENCE (C(1236),CH1  )
35  EQUIVALENCE (C(1237),CH2  )
      EQUIVALENCE (C(1238),CH3  )
      EQUIVALENCE (C(1239),CH4  )
      EQUIVALENCE (C(1411),FTHX )
      EQUIVALENCE (C(1412),FTHY )
40  EQUIVALENCE (C(1413),FTHZ )
      EQUIVALENCE (C(1422),RLCG )
      EQUIVALENCE (C(1628),DMASS )
      EQUIVALENCE (C(1723),CFA23 )
      EQUIVALENCE (C(1735),CFA33 )
45  EQUIVALENCE (C(1739),WP   )
      EQUIVALENCE (C(1743),WQ   )
      EQUIVALENCE (C(1747),WR   )
      EQUIVALENCE (C(1749),FMIY )
      EQUIVALENCE (C(1750),FMIZ )
50  EQUIVALENCE (C(1703),CFA11)
      EQUIVALENCE (C(1707),CFA12)
      EQUIVALENCE (C(1711),CFA13)
      EQUIVALENCE (C(1715),CFA21)
      EQUIVALENCE (C(1719),CFA22)
55  EQUIVALENCE (C(1723),CFA23)

```

```

      EQUIVALENCE(C(1727),CFA31)
      EQUIVALENCE(C(1731),CFA32)
      EQUIVALENCE(C(1735),CFA33)
C
60   C**OTHER OUTPUTS
      EQUIVALENCE (C(1300),FXBA )
      EQUIVALENCE (C(1301),FYBA )
      EQUIVALENCE (C(1302),FZBA )
      EQUIVALENCE (C(1303),FMXBA )
65   EQUIVALENCE (C(1304),FMYBA )
      EQUIVALENCE (C(1305),FMZBA )
      EQUIVALENCE (C(1309),FMH1 )
      EQUIVALENCE (C(1310),FMH2 )
      EQUIVALENCE (C(1311),FMH3 )
70   EQUIVALENCE (C(1312),FMH4 )
      EQUIVALENCE (C(1320),FMXTH )
      EQUIVALENCE (C(1321),FMYTH )
      EQUIVALENCE (C(1322),FMZTH )
      EQUIVALENCE (C(1323),FMXLUG)
75   EQUIVALENCE (C(1324),FMYLUG)
      EQUIVALENCE (C(1325),FMZLUG)
      EQUIVALENCE(C(2000),T)
      EQUIVALENCE(C(1332),EFT)
      EQUIVALENCE(C(1333),EJD)
80   EQUIVALENCE(C(1326),EFORCX)
      EQUIVALENCE(C(1327),EFORCY)
      EQUIVALENCE(C(1328),EFORCZ)
      EQUIVALENCE(C(1329),EMOMX)
      EQUIVALENCE(C(1330),EMOMY)
85   EQUIVALENCE(C(1331),EMOMZ)
      EQUIVALENCE(C(61),ASN)
      EQUIVALENCE(C(60),AAN)
      EQUIVALENCE (C(73),XNOSE1)
      EQUIVALENCE (C(72),DELZ)
90   C
      C**FORCE VECTOR COMPONENTS
      UQS = PDYNMC*RFAREA
      UQSL = UQS*RFLGTH
      CY=CY+.04*ASN*57.3
95   CN=CN+.04*ASN*57.3*XNOSE1/RFLGTH
      CM=CM-.04*AAN*57.3*XNOSE1/RFLGTH
      CZ=CZ+.04*AAN*57.3
C
      FXBA=UQS*(-CX)+FTHX
100  FYBA=UQS*CY+FTHY
      FZBA=UQS*CZ+FTHZ
      IF(VAIRSP,LE.0.0) GO TO 72
C
      C**AERO MOMENTS
105  VAIRSP=VAIRSP*2.
      FMXBA = (CL+(CLP/VAIRSP)*RFLGTH*WP)*UQSL
      FMYBA = (CM+(CMQ/VAIRSP)*RFLGTH*WQ)*UQSL+FZBA*RDELCG
      FMZBA = (CN+(CNR/VAIRSP)*RFLGTH*WR)*UQSL-FYBA*RDELCG
      EFBAX=0.
110  EFBAY=0.

```



```

EFBAZ=0.
EMBAX=0.
EMBAY=0.
EMBAZ=0.
115 IF(T.GT.EFT) GO TO 37
IF(DE LZ.GT.EJD) GO TO 37
EFBAX=EFORCX*CFA11 +EFORCY*CFA12 +EFORCZ*CFA13
EFBAY=EFORCX*CFA21 +EFORCY*CFA22 +EFORCZ*CFA23
EFBAZ=EFORCX*CFA31 +EFORCY*CFA32 +EFORCZ*CFA33
120 EMBAX=EMOMX*CFA11 +EMOMY*CFA12 +EMOMZ*CFA13
EMBAY=EMOMX*CFA21 +EMOMY*CFA22 +EMOMZ*CFA23
EMBAZ=EMOMX*CFA31 +EMOMY*CFA32 +EMOMZ*CFA33
FXBA=FXBA+EFBAX
FYBA=FYBA+EFBAY
125 FZBA=FZBA+EFBAZ
FMXBA=FMXBA + EMBAX
FMYBA=FMYBA + EMBAY
FMZBA=FMZBA+EMBAZ
37 CONTINUE
130 VAIRSP=VAIRSP/2.
C
C**MOMENTS CAUSED BY THRUST MISALIGNMENTS
FMXTH = -FTHY*RFZCG + FTHZ*RFYCG
FMYTH = FTHX*RFZCG + FTHZ*RFXCG
135 FMZTH = -FTHX*RFYCG - FTHY*RFXCG
C
C**MOMENTS AND FORCES DUE TO LUGS
IF ( (OPTN4 .GT. 0.) .AND. (RANGO .LE. RAIL+RLUG) ) GO TO 70
140 FYLUG = 0.
FZLUG = 0.
FMXLUG = 0.
FMYLUG = 0.
FMZLUG = 0.
GO TO 74
145 70 IF (RANGO .LE. RAIL) GO TO 72
FYLUG = -(FYBA + DMASS*AGRAV*CFA23 + (FMZBA + FMZTH)*
* RLCG*DMASS/FMIZ)/(1. + DMASS*RLCG*RLCG/FMIZ)
FZLUG = -(FZBA + DMASS*AGRAV*CFA33 + (FMYBA + FMYTH)*
* RLCG*DMASS/FMIY)/(1. + DMASS*RLCG*RLCG/FMIY)
150 FMXLUG = -(FMXBA + FMXTH)
FMYLUG = FZLUG*RLCG
FMZLUG = FYLUG*RLCG
GO TO 74
72 CONTINUE
155 FYLUG = -(FYBA + DMASS*AGRAV*CFA23)
FZLUG = -(FZBA + DMASS*AGRAV*CFA33)
FMXLUG = -(FMXBA + FMXTH)
FMYLUG = -(FMYBA + FMYTH)
FMZLUG = -(FMZBA + FMZTH)
160 74 CONTINUE
C
C**TOTAL FORCE AND MOMENTS
FYBA = FYBA + FYLUG
FZBA = FZBA + FZLUG
165 FMXBA = FMXBA + FMXTH + FMXLUG

```

SUBROUTINE A2

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FMYBA = FMYBA + FMYTH + FMYLUG
FMZBA = FMZBA + FMZTH + FMZLUG

C

C** CALCULATE HINGE MOMENTS

170

FMH1 = CH1*UQSL
FMH2 = CH2*UQSL
FMH3 = CH3*UQSL
FMH4 = CH4*UQSL

175

RETURN
END

```
C**INITIALIZATION FOR ENGINE MODULE
SUBROUTINE A3I
COMMON C(3510)
DIMENSION IPL(101)
5  EQUIVALENCE (C(2561),N )
EQUIVALENCE (C(2562),IPL )
C(1499) = 0.
IPL(N ) = 1496
N = N+1
10 RETURN
END
```

```

C**ENGINE MODULE
      SUBROUTINE A3
      COMMON C(3510)
C
5     C**LOOK UP TABLE FOR THRUST
      COMMON /NTH/NTH /THARG/THA /THFUN/THF
C
C** INPUT DATA
10    EQUIVALENCE (C(1401),BALPHT)
      EQUIVALENCE (C(1402),BPHIT )
      EQUIVALENCE (C(1403),QNALGN)
      EQUIVALENCE (C(1404),PCFTH )
      EQUIVALENCE (C(1405),QBURN )
15    EQUIVALENCE (C(1414),CISP )
      EQUIVALENCE (C(1415),DWT )
      EQUIVALENCE (C(1416),DWP )
      EQUIVALENCE (C(1417),RDCGO )
      EQUIVALENCE (C(1418),RDCGF )
      EQUIVALENCE (C(1419),FMIXO )
20    EQUIVALENCE (C(1420),FMIYO )
      EQUIVALENCE (C(1421),RLCGO )
      EQUIVALENCE (C(1627),AGRAV )
C
25    C** INPUTS FROM OTHER MODULES
      EQUIVALENCE (C(1252),XINTER)
      EQUIVALENCE (C(2000),T )
C
C** OUTPUTS
30    EQUIVALENCE (C(1308),RDELCO)
      EQUIVALENCE (C(1409),UDWP )
      EQUIVALENCE (C(1410),FTHRST)
      EQUIVALENCE (C(1411),FTHX )
      EQUIVALENCE (C(1412),FTHY )
      EQUIVALENCE (C(1413),FTHZ )
35    EQUIVALENCE (C(1422),RLCG )
      EQUIVALENCE (C(1628),OMASS )
      EQUIVALENCE (C(1748),FMIX )
      EQUIVALENCE (C(1749),FMIY )
      EQUIVALENCE (C(1750),FMIZ )
40    C
C**STATE VARIABLES AND THEIR DERIVATIVES
      EQUIVALENCE (C(1496),UIMPD )
      EQUIVALENCE (C(1499),UIMP )
C
45    IF (QBURN.GT.0.) RETURN
      CALL TABLE (T,THA,THF,NTH,XINTER,6HFTHRST,FTHRST)
      FTHRST = FTHRST*(1. + PCFTH)
C
      IF (QNALGN) 20,20,10
50    10 USINA=SIND(BALPHT)
      FTHX=FTHRST*COSD(BALPHT)
      FTHY=-FTHRST*USINA*SIND(BPHIT)
      FTHZ=FTHRST*USINA*COSD(BPHIT)
      GO TO 30
55    20 FTHX=FTHRST

```

SUBROUTINE A3

CDC 6600 FTN V3.0-P304 OPT=1 30

```
      FTHY=0.  
      FTHZ=0.  
30  CONTINUE  
C  
60  UIMP0 = FTHRST  
      UDWP = UIMP/CISP  
C  
      DMASS = (DWT - UDWP)/AGRAV  
65  RDELCG = RDCGD - (RDCGD - RDCGF)*UDWP/DWP  
C  
      FMIX = FMIXD*(DWT - UDWP)/DWT  
      FMIY = FMIYD*(DWT - UDWP)/DWT  
      FMIZ = FMIY  
70  RLCG = RLCGO + RDELCG  
      IF (FTHRST .GT. 0.) RETURN  
C  
      WRITE (6,100) T  
100  FORMAT (//14H BURNDOUT TIME=,F8.4,5H SEC.)  
75  QBURN=1.0  
      FTHRST=0.  
      FTHX=0.  
      FTHY=0.  
      FTHZ=0.  
      RETURN  
80  END
```

```

C** TRANSLATIONAL DYNAMICS INITIALIZATION MODULE FOR 01
SUBROUTINE D1I
COMMON C(3510)
EQUIVALENCE (C(2561),N )
5 EQUIVALENCE (C(2562),IPL )
DIMENSION IPL (100)

C
C** INPUT DATA
10 EQUIVALENCE (C( 100),VWXE )
EQUIVALENCE (C( 101),VWYE )
EQUIVALENCE (C( 102),VWZE )
EQUIVALENCE (C( 204),VMACH )
EQUIVALENCE (C( 367),BALPHA)
EQUIVALENCE (C( 368),BALPHY)
15 EQUIVALENCE (C(1615),RXE )
EQUIVALENCE (C(1619),RYE )
EQUIVALENCE (C(1623),RZE )
EQUIVALENCE (C(1603),VXE )
EQUIVALENCE (C(1607),VYE )
20 EQUIVALENCE (C(1611),VZE )
EQUIVALENCE (C(1635),RDELX )
EQUIVALENCE (C(1636),RDELY )
EQUIVALENCE (C(1637),RDELZ )
EQUIVALENCE (C(1643),VTARG )
25 EQUIVALENCE (C(1651),RTXE )
EQUIVALENCE (C(1655),RTYE )
EQUIVALENCE (C(1659),RTZE )
EQUIVALENCE (C(1668),RXO )
EQUIVALENCE (C(1669),RYO )
30 EQUIVALENCE (C(1670),RZO )
EQUIVALENCE (C(1753),BTHTO )
EQUIVALENCE (C(1754),BPSIO )
EQUIVALENCE (C(0209), RH )
EQUIVALENCE (C(1660),VTXE)
35 EQUIVALENCE (C(1661),VTYE)
EQUIVALENCE (C(1662),VTZE)

C
IPL(N) = 1600
IPL(N+1) = 1604
40 IPL(N+2) = 1608
IPL(N+3) = 1612
IPL(N+4) = 1616
IPL(N+5) = 1620
IPL(N+6) = 1640
45 IPL(N+7) = 1644
IPL(N+8) = 1648
IPL(N+9) = 1652
IPL(N+10) = 1656
N = N+11

50 C
RH=-RZE
24 VSOUND = 1117.3 - .00392*RH
VMWTE = VMACH*VSOUND
VTARG=VMWTE
55 VMWXY = VMWTE*COSD(BALPHA - BTHTO)

```

SUBROUTINE D1I

CDC 6600 FTN V3.0-P304 OPT=1 30

```
      C
      VXE = VWXE + VMWXY*COSD(BALPHY + BPSIO)
      VYE = VWYE + VMWXY*SIND(BALPHY + BPSIO)
      VZE = VWZE + VMWTE*SIND(BALPHA - BTHTO)
60      C
      VTXE=VXE
      VTYE=VYE
      VTZE=VZE
      30 RDELX = RTXE-RXE
      RDELY = RTYE-RYE
65      RDELZ = RTZE-RZE
      RXO = RXE
      RYO = RYE
      RZO = RZE
70      RETURN
      END
```

```

C**TRANSLATIONAL DYNAMICS MODULE
  SUBROUTINE D1
  COMMON C(3510)
C
5  C**INPUT DATA
    EQUIVALENCE (C(1627),AGRAV )
    EQUIVALENCE (C(1628),DMASS )
C
10 C**INPUTS FROM OTHER MODULES
    EQUIVALENCE (C(1300),FXBA )
    EQUIVALENCE (C(1301),FYBA )
    EQUIVALENCE (C(1302),FZBA )
    EQUIVALENCE (C(1667),RZ )
15    EQUIVALENCE (C(1703),CFA11 )
    EQUIVALENCE (C(1707),CFA12 )
    EQUIVALENCE (C(1711),CFA13 )
    EQUIVALENCE (C(1715),CFA21 )
    EQUIVALENCE (C(1719),CFA22 )
    EQUIVALENCE (C(1723),CFA23 )
20    EQUIVALENCE (C(1727),CFA31 )
    EQUIVALENCE (C(1731),CFA32 )
    EQUIVALENCE (C(1735),CFA33 )
    EQUIVALENCE (C(2000),T )
C
25 C**STATE VARIABLE OUTPUTS
    EQUIVALENCE (C(1600),VXED )
    EQUIVALENCE (C(1603),VXE )
    EQUIVALENCE (C(1604),VYED )
    EQUIVALENCE (C(1607),VYE )
30    EQUIVALENCE (C(1608),VZED )
    EQUIVALENCE (C(1611),VZE )
    EQUIVALENCE (C(1612),RXED )
    EQUIVALENCE (C(1615),RXE )
    EQUIVALENCE (C(1616),RYED )
35    EQUIVALENCE (C(1619),RYE )
    EQUIVALENCE (C(1620),RZED )
    EQUIVALENCE (C(1623),RZE )
    EQUIVALENCE (C(1648),RTXED )
    EQUIVALENCE (C(1651),RTXE )
40    EQUIVALENCE (C(1652),RTYED )
    EQUIVALENCE (C(1655),RTYE )
    EQUIVALENCE (C(1656),RTZED )
    EQUIVALENCE (C(1659),RTZE )
C
45 C**OTHER OUTPUTS
    EQUIVALENCE (C(1624),AXBA )
    EQUIVALENCE (C(1625),AYBA )
    EQUIVALENCE (C(1626),AZBA )
    EQUIVALENCE (C(1632),VDELX )
50    EQUIVALENCE (C(1633),VDELY )
    EQUIVALENCE (C(1634),VDELZ )
    EQUIVALENCE (C(1635),RDELX )
    EQUIVALENCE (C(1636),RDELY )
    EQUIVALENCE (C(1637),RDELZ )
55    EQUIVALENCE (C(1660),VTXE )

```


SUBROUTINE D1

CDC 6600 FTN V3.0-P304 OPT=1 30

```

        EQUIVALENCE (C(1661),VTYE )
        EQUIVALENCE (C(1662),VTZE )
        EQUIVALENCE(C(72),DELZ)
        EQUIVALENCE(C(71),DELY)
60      EQUIVALENCE(C(70),DELX)
      C
      C**ADD AERO AND THRUST FDRCES TO GET TDTAL ACCELERATION IN BODY AXES
        AXBA = FXBA/DMASS
        AYBA = FYBA/DMASS
65      AZBA = FZBA/DMASS
      C
      C**RESOLVE FROM BDDY TD EARTH AXES
        AXE = CFA11*AXBA+CFA21*AYBA+CFA31*AZBA
        AYE = CFA12*AXBA+CFA22*AYBA+CFA32*AZBA
70      AZE = CFA13*AXBA+CFA23*AYBA+CFA33*AZBA
      C
      C**INTEGRATE ACCELERATIONS
        VXED = AXE
        VYED = AYE
75      VZED = AZE + AGRAV
      C
      C
      C**INTEGRATE VELOCITIES TO EARTH AXES PDSITION
        10 RXEC = VXE
80      RYED = VYE
        RZED = VZE
      C
      C
85      RTXED = VTXE
        RTYED = VTYE
        RTZED = VTZE
      C
        VDELX = VTXE-VXE
        VDELY = VTYE-VYE
90      VOELZ = VTZE-VZE
      C
        RDELX = RTXE-RXE
        RDELY = RTYE-RYE
        RDELZ = RTZE-RZE
95      DELX=-RDELX
        DELY=-RDELY
        DELZ=-RDELZ
        RETURN
      END
```

```

C**ROTATIONAL DYNAMICS INITIALIZATION MODULE D2IEUL
  SUBROUTINE D2I
  COMMON C(3510)
  DIMENSION IPL (100)
5  C**INPUT DATA
    EQUIVALENCE (C(1752),BPHIO )
    EQUIVALENCE (C(1753),BTHTO )
    EQUIVALENCE (C(1754),BPSIO )
10 C**INPUTS FROM OTHER MODULES
    C**NONE
    C**INPUTS FROM MAIN PROGRAM
      EQUIVALENCE (C(2561),N      )
      EQUIVALENCE (C(2562),IPL   )
15 C**STATE VARIABLE OUTPUTS
      EQUIVALENCE (C(1703),CFA11 )
      EQUIVALENCE (C(1707),CFA12 )
      EQUIVALENCE (C(1711),CFA13 )
      EQUIVALENCE (C(1715),CFA21 )
      EQUIVALENCE (C(1719),CFA22 )
20      EQUIVALENCE (C(1723),CFA23 )
      EQUIVALENCE (C(1727),CFA31 )
      EQUIVALENCE (C(1731),CFA32 )
      EQUIVALENCE (C(1735),CFA33 )
25 C**OTHER OUTPUTS
    C**NONE
    C**INITIAL CALCULATION OF EULER ANGLE MATRIX OF DIRECTION COSINES (CFA)
      USPHI = SIND(BPHIO)
      UCPHI = COSD(BPHIO)
      USTHT = SIND(BTHTO)
      UCTHT = COSD(BTHTO)
30      USPSI = SIND(BPSIO)
      UCPSI = COSD(BPSIO)
      CFA11 = UCPSI*UCTHT
      CFA12 = USPSI*UCTHT
35      CFA13 = -USTHT
      CFA21 = -USPSI*UCPHI+UCPSI*USTHT*USPHI
      CFA22 = UCPSI*UCPHI+USPSI*USTHT*USPHI
      CFA23 = UCTHT*USPHI
      CFA31 = UCPSI*USTHT*UCPHI+USPSI*USPHI
40      CFA32 = USPSI*USTHT*UCPHI-UCPSI*USPHI
      CFA33 = UCTHT*UCPHI
C
C**INTEGRATED PARAMATER LIST (IPL) FOR WPD,WQD,WRD,AND CFAD
45      IPL(N) = 1700
      IPL(N+1) = 1704
      IPL(N+2) = 1708
      IPL(N+3) = 1712
      IPL(N+4) = 1716
      IPL(N+5) = 1720
50      IPL(N+6) = 1724
      IPL(N+7) = 1728
      IPL(N+8) = 1732
      IPL(N+9) = 1736
      IPL(N+10) = 1740
55      IPL(N+11) = 1744

```

SUBROUTINE D2I

CDC 6600 FTN V3.0-P304 OPT=1 30

N = N+12

C** RESET ANGULAR RATE DERIVATIVES TO ZERO.

C(1700) = 0.

C(1704) = 0.

60

C(1708) = 0.

C(1712) = 0.

C(1716) = 0.

C(1720) = 0.

C(1724) = 0.

65

C(1728) = 0.

C(1732) = 0.

C(1736) = 0.

C(1740) = 0.

C(1744) = 0.

70

RETURN

END

```

C** ROTATIONAL DYNAMICS MODULE
SUBROUTINE D2
COMMON C(3510)
C
5 C**DATA INPUTS
EQUIVALENCE (C(1421),RAIL )
EQUIVALENCE (C(1748),FMIX )
EQUIVALENCE (C(1749),FMIY )
EQUIVALENCE (C(1750),FMIZ )
10 EQUIVALENCE (C(1751),CRAD )
EQUIVALENCE (C(3503),OPTN3)
EQUIVALENCE (C(3504),OPTN4 )
C
15 C**INPUTS FROM OTHER MODULES
EQUIVALENCE (C( 380),RANGO )
EQUIVALENCE (C(1303),FMXBA )
EQUIVALENCE (C(1304),FMYBA )
EQUIVALENCE (C(1305),FMZBA )
EQUIVALENCE (C(1308),RDELGG)
20 C
C**INPUTS FROM MAIN PROGRAM
C**STATE VARIABLE OUTPUTS
EQUIVALENCE (C(1700),CFA11D)
EQUIVALENCE (C(1703),CFA11 )
25 EQUIVALENCE (C(1704),CFA12D)
EQUIVALENCE (C(1707),CFA12 )
EQUIVALENCE (C(1708),CFA13D)
EQUIVALENCE (C(1711),CFA13 )
EQUIVALENCE (C(1712),CFA21D)
30 EQUIVALENCE (C(1715),CFA21 )
EQUIVALENCE (C(1716),CFA22D)
EQUIVALENCE (C(1719),CFA22 )
EQUIVALENCE (C(1720),CFA23D)
EQUIVALENCE (C(1723),CFA23 )
35 EQUIVALENCE (C(1724),CFA31D)
EQUIVALENCE (C(1727),CFA31 )
EQUIVALENCE (C(1728),CFA32D)
EQUIVALENCE (C(1731),CFA32 )
EQUIVALENCE (C(1732),CFA33D)
40 EQUIVALENCE (C(1735),CFA33 )
EQUIVALENCE (C(1736),WPD )
EQUIVALENCE (C(1739),WP )
EQUIVALENCE (C(1740),WQD )
EQUIVALENCE (C(1743),WQ )
45 EQUIVALENCE (C(1744),WRD )
EQUIVALENCE (C(1747),WR )
C
C**INTEGRATE BODY ANGULAR RATES
IF (OPTN3.GT.0.) GO TO 55
50 WPD = CRAD*FMXBA/FMIX
55 WQD = (CRAD*FMYBA+(FMIZ-FMIX)*WP*WR/CRAD)/FMIY
65 WRD = (CRAD*FMZBA+(FMIX-FMIY)*WP*WQ/CRAD)/FMIZ
C
55 C**INTEGRATE ATTITUDE DIRECTION COSINES
49 CFA11D=(CFA21*WR-CFA31*WQ)/CRAD

```

SUBROUTINE D2

CDC 6600 FTN V3.0-P304 OPT=1 30

```
60 CFA12D=(CFA22*WR-CFA32*WQ)/CRAD
    CFA13D=(CFA23*WR-CFA33*WQ)/CRAD
    CFA21D = (CFA31*WP-CFA11*WR)/CRAD
    CFA22D = (CFA32*WP-CFA12*WR)/CRAD
    CFA23D = (CFA33*WP-CFA13*WR)/CRAD
    CFA31D = (CFA11*WQ-CFA21*WP)/CRAD
    CFA32D = (CFA12*WQ-CFA22*WP)/CRAD
    CFA33D = (CFA13*WQ-CFA23*WP)/CRAD
65 RETURN
    END
```

```

C      BASIC INPUT SUBROUTINE OINPT1
      SUBROUTINE OINPT1
      COMMON C(3510)
      EQUIVALENCE (C(3218),ONAME1), (C(3268),ONAME2), (C(3318),ONAME3),
5      C      (C(3328),ONAME4), (C(2361),NOMOD ), (C(2362),MODNO ),
      C      (C(3440),NORNDM), (C(3441),RNDMNO), (C(3167),NOOUT ),
      C      (C(3168),OUTNO ), (C(2461),NOSUB ), (C(2462),SUBNO ),
      C      (C(2355),IR ), (C(2357),VR ), (C(3339),NOSTAT),
      C      (C(3338),LOSTAT), (C(3340),STATNO), (C(3066),NOLIST),
10     C      (C(3067),LISTNO), (C(3117),VALUE ), (C(2008),PLOTNO),
      * (C(2009),NOPLOT), (C(2325),VLABLE)
      EQUIVALENCE (C(1984),NPLOT )
      EQUIVALENCE (C(1985),OUTPLT)
      DIMENSION ONAME3(10),ONAME4(10)
15     DIMENSION LISTNO(50), VALUE(50)
      DIMENSION SUBNO(99), IR(2), VR(2)
      DIMENSION RNDMNO(50)
      DIMENSION ALPHA(3),ONAME1(50),ONAME2(50),OUTNO(50) ,MODNO(99)
      DIMENSION STATNO (100)
20     DIMENSION VLABLE(2,15)
      DIMENSION OUTPLT(15)
      REAL MODNO
      INTEGER OUTNO
      INTEGER RNDMNO
25     INTEGER STATNO
      INTEGER OUTPLT
      JAR = 0
      WRITE(6,31)
31     FORMAT(11H1INPUT DATA/)
17     1 READ(5,2) IR(1),ALPHA(1),ALPHA(2),ALPHA(3),IR(2),VR(1),VR(2)
      WRITE(6,30)IR(1),ALPHA(1),ALPHA(2),ALPHA(3),IR(2),VR(1),VR(2)
30     FORMAT(I2,3A6,I5,5X,1P2E15.7)
18     2 FORMAT(I2,3A6,I5,5X,2E15.9)
      7 IF( IR(1) .NE. 1 ) GO TO 3
35     NOSUB = NOSUB + 1
      SUBNO(NOSUB) = IR(2)
      GO TO 1
32     3. IF( IR(1) .NE. 2 ) GO TO 4
      NOMOD = NOMOD + 1
40     MODNO(NOMOD) = IR(2)
      GO TO 1
33     4 IF(IR(1) .NE. 3) GO TO 5
      L = IR(2)
45     C(L) = VR(1)
      IF (VR(2) .EQ. 0.) GO TO 1
      NOLIST = NOLIST + 1
      LISTNO(NOLIST) = L
      VALUE(NOLIST) = VR(1)
      GO TO 1
50     5 IF(IR(1) .NE. 4)GO TO 6
      NOOUT = NOOUT + 1
      IF (NOOUT.GT.50) GO TO 1
      ONAME1(NOOUT)=ALPHA(2)
      ONAME2(NOOUT) = ALPHA(3)
55     OUTNO(NOOUT) = IR(2)

```

SUBROUTINE OINPT1

CDC 6600 FTN V3.0-P304 OPT=1 30

```
      GO TO 1
      6 IF (IR(1) .NE. 5) GO TO 16
      IF (VR(1) .EQ. 0.) GO TO 17
      LOSTAT = LOSTAT + 1
60      17 NOSTAT = NOSTAT + 1
      STATNO(NOSTAT) = IR(2)
      ONAME3(NOSTAT)=ALPHA(2)
      ONAME4(NOSTAT)=ALPHA(3)
      GO TO 1
65      16 IF (IR(1).NE.7) GO TO 19
      NPLOT=NPLOT+1
      IF (NPLOT.GT.15) GO TO 1
      DO 20 I=1,2
70      20 VLABLE (I,NPLOT)=ALPHA(I+1)
      OUTPLT(NPLOT)=IR(2)
      GO TO 1
      19 IF (IR(2) .EQ. 0) RETURN
      RETURN
      END
```

```

C      OUTPUT INITIALIZATION SUBROUTINE OOPT2
      SUBROUTINE OOPT2
      COMMON      C(3510)      , GRAPH
5      EQUIVALENCE (C(2017),DTCNT ), (C(3167),NOOUT ), (C(2016),PGCNT ),
C      (C(2014),ITCNT ), (C(2003),PCNT ), (C(2015),GPP ),
C      (C(2018),TAPE ), (C(2019),TAPEND), (C(2013),DOC ),
C      (C(2000),T ), (C(2021),KCONV ), (C(2025),TIME ),
C      (C(2008),PLOTNO), (C(2009),NOPLT), (C(3168),OUTNO ),
C      (C(2004),PPNT ), (C(2023),OPOINT)
10     DIMENSION GRAPH(300,15) , TIME(300) , OUTNO(50)
      INTEGER      PGCNT , DTCNT , OUTNO , OPOINT
      EQUIVALENCE (C(1985),OUTPLT)
      INTEGER OUTPLT
15     DIMENSION OUTPLT(15)
      KCONV=0
      ITCNT = DOC + 1.0
      PCNT = Y-0.000001
      PPNT=PCNT
      PGCNT = 1
20     DTCNT = (NOOUT + 4)/5
      IF ( ITCNT .GE. 7) GO TO 2
      CALL DUMPO
C
25     2 TIME(1)=T
      OPOINT =1
      DO 10 J=1,NOPLT
      K=OUTPLT(J)
30     10 GRAPH(1,J)=C(K)
      RETURN
      END

```



```

C      OUTPUT SUBROUTINE OOPT3
      SUBROUTINE OOPT3
      COMMON      C(3510)          , GRAPH
      EQUIVALENCE (C(3168),OUTNO ), (C(3218),ONAME1), (C(3268),ONAME2),
5      C      (C(2017),DTCNT ), (C(3167),NOOUT ), (C(2016),PGCNT ),
      C      (C(2014),ITCNT ), (C(2003),PCNT ), (C(2015),CPP ),
      C      (C(2000),T ), (C(2664),DER ), (C(2018),TAPE ),
      C      (C(2019),TAPEND), (C(2008),PLOTNO), (C(2009),NOPLOT),
      C      (C(2005),PPP ), (C(2004),PPNT ), (C(2025),TIME ),
10     C      (C(2023),OPOINT)
      EQUIVALENCE (C(1985),OUTPLT)
      DIMENSION B(50),OUTNO(50),ONAME1(50),ONAME2(50)
      DIMENSION TIME(300),GRAPH(300,15)
      DIMENSION OUTPLT(15)
15     INTEGER DTCNT,PGCNT,OUTNO
      INTEGER OPOINT
      INTEGER OUTPLT
      IF (ITCNT. GT. 6) GO TO 7
      ITCNT = ITCNT + 1
20     C
      CALL DUMPO
      PGCNT = 1
      7 IF (DER. EQ. DER1) GO TO 8
      DER1 = DER
25     WRITE(6,20)T,DER
20     FORMAT(1H ,5HTIME=F14.7,2X,10HSTEP SIZE=1PE19.7)
      8 IF (T .LT. PCNT)GOTO15
      9 PCNT = PCNT + CPP
      IF (PGCNT. NE. 1) GO TO 3
30     1 WRITE(6,2) (ONAME1(I),ONAME2(I), I=1,NOOUT)
      2 FORMAT (1H1,3X,4HTIME,5X,5(7X,2A6)//(20X,2A6,7X,2A6,7X,2A6,7X,
      12A6,7X,2A6)//
      PGCNT = 2*DTCNT + 4
35     3 IF(PGCNT.GE.112) GO TO 1
      DO 4 I = 1,NOOUT
      J = OUTNO(I)
      4 B(I) = C(J)
      WRITE (6,5) T,(B(I), I = 1,NOOUT)
40     5 FORMAT (///,F14.7,1P5E19.7/(14X,1P5E19.7))
      PGCNT = PGCNT + DTCNT + 4
15     IF(T.LT.PPNT.OR.NOPLOT.EQ.0)RETURN
      PPNT=PPNT+PPP
      KPOINT =OPOINT +1
      IF (KPOINT-300) 16,13,18
45     13 WRITE (6,14)
      14 FORMAT (//71H **** WARNING=PLOTTING ARRAY FILLED-ONLY FIRST 300 P
      COINTS PLOTTED ****,/)
      16 OPOINT=KPOINT
      TIME (OPOINT)=T
50     DO 10 J=1,NOPLOT
      K=OUTPLT(J)
      10 GRAPH(OPOINT ,J)=C(K)
      18 RETURN
      END

```

SUBROUTINE OUMPO

CDC 6600 FTN V3.0-P304 OPT=1 3

```
      SUBROUTINE OUMPO
C     PRINT OUT A DUMP OF COMMON
      COMMON NN(3510)
      DIMENSION A(9),MM(9)
5     EQUIVALENCE (A(1),MM(1))
      WRITE (6,100)
      DO 30 I=1,3510,9
      N=I-1
      DO 20 J=1,9
10     K=J+N
      IF(AND(IABS(NN(K)),37770000000000000000)) 5,5,10
      5     A(J)=NN(K)
      GO TO 20
      10     MM(J)=NN(K)
15     20     CONTINUE
      WRITE(6,200)I,A
      30     CONTINUE
      RETURN
      100     FORMAT(1H1)
20     200     FORMAT(I5,1P9E14.7)
      END
```

SUBROUTINE ZERO

CDC 6600 FTN V3.0-P304 OPT=1 3

```

SUBROUTINE ZERO
COMMON C(3510)
EQUIVALENCE (C(1984),NPLOT )
EQUIVALENCE (C(2023),OPOINT)
5  EQUIVALENCE (C(2361),NOMOD )
EQUIVALENCE (C(2461),NOSUB )
EQUIVALENCE (C(3066),NOLIST)
EQUIVALENCE (C(3167),NOOUT )
10 EQUIVALENCE (C(3338),LOSTAT)
EQUIVALENCE (C(3339),NOSTAT)
EQUIVALENCE (C(3440),NORNDM)
EQUIVALENCE (C(2008),PLOTNO)
INTEGER OPOINT
15 LOSTAT = 0
NOSTAT = 0
NOSUB = 0
NOMOD = 0
NOOUT = 0
20 NORNDM = 0
NOLIST = 0
OPOINT=0
NPLOT=0
RETURN
END
```

SUBROUTINE SUBL1

CDC 6600 FTN V3.0-P304 OPT=1 30

```

      SUBROUTINE SUBL1
      COMMON C(3510)
      EQUIVALENCE (C(2461),NOSUB ), (C(2462),SUBNO )
      DIMENSION SUBNO(99)
5      DO 1 I = 1, NOSUB
      J = SUBNO(I)
      GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9 ), J
      2 CALL INPT1
      GO TO 1
10     3 CALL OUPT1
      GO TO 1
      4 CALL STGE1
      GO TO 1
      5 CALL CNTR1
      GO TO 1
15     6 CALL RNDM1
      GO TO 1
      7 CALL AUXA1
      GO TO 1
      8 CALL AUXB1
      GO TO 1
20     9 CALL AUXC1
      1 CONTINUE
      RETURN
25     END
```

SUBROUTINE SUBL2

CDC 6600 FTN V3.0-P304 OPT=1 30

```

SUBROUTINE SUBL2
COMMON C(3510)
EQUIVALENCE (C(2461),NOSUB ), (C(2462),SUBNO )
DIMENSION SUBNO(99)
5   00 1 I = 1, NOSUB
   J = SUBNO(I)
   GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9 ), J
2  CALL INPT2
   GO TO 1
10 3  CALL OOPT2
   GO TO 1
   4  CALL STGE2
   GO TO 1
15 5  CALL CNTR2
   GO TO 1
   6  CALL RNDM2
   GO TO 1
   7  CALL AUXA2
   GO TO 1
20 8  CALL AUXB2
   GO TO 1
   9  CALL AUXC2
1  CONTINUE
RETURN
25  END
```

SUBROUTINE SUBL3

CDC 6600 FTN V3.0-P304 OPT=1 3

```

SUBROUTINE SUBL3
COMMON C(3510)
EQUIVALENCE (C(2461),NOSUB ), (C(2462),SUBNO )
DIMENSION SUBNO(99)
5 DO 1 I = 1, NOSUB
  J = SUBNO(I)
  GO TO ( 1, 2, 3, 4, 5, 6, 7, 8, 9 ), J
2 CALL INPT3
  GO TO 1
10 3 CALL OOPT3
  GO TO 1
4 CALL STGE3
  GO TO 1
15 5 CALL CNTR3
  GO TO 1
6 CALL RNDM3
  GO TO 1
7 CALL AUXA3
  GO TO 1
20 8 CALL AUXB3
  GO TO 1
9 CALL AUXC3
1 CONTINUE
RETURN
25 END
```

SUBROUTINE STGE2

CDC 6600 FTN V3.0-P304 OPT=1 31

```
SUBROUTINE STGE2
COMMON      C(3510)
EQUIVALENCE (C(2011),KSTEP ), (C(2020),LCONV ), (C(2021),KCONV )
KCONV = 0
LCONV = 0
KSTEP = 1
RETURN
END
```

5
-

SUBROUTINE STGE3

COC 6600 FTN V3.0-P304 OPT=1

```

SUBROUTINE STGE3
COMMON C(3510),GRAPH,TEMPS(1000)
EQUIVALENCE (C(2000),T      ), (C(2001),TF      ), (C(2003),PCNT  )
EQUIVALENCE (C(2010),STEP  ), (C(2011),KSTEP  ), (C(2020),LCONV )
5 EQUIVALENCE (C(2021),KCONV ), (C(2561),N      ), (C(2662),HMIN  )
EQUIVALENCE (C(2663),HMAX  ), (C(2664),DER    ), (C(2765),EL    )
EQUIVALENCE (C(2865),EU    ), (C(2965),VAR    )
EQUIVALENCE (C(1973),KASE  ), (C(1974),NJ    ), (C(1975),NPT   )
10 DIMENSION  DER(101)      , VAR(101)      , EL(100)
DIMENSION  EU(100)        , GRAPH(300,15)
EXTERNAL AUXSUB
CALL G4
IF (ABS( T-TF) .LE. 0.01 ) GO TO 20
IF ( (TF-T) .LT. 0.) GO TO 10
15 IF (LCONV .EQ. 2) GO TO 20
IF (LCONV .EQ. 1) GO TO 10
IF ( DER. LT. 0.) DER = -DER*0.5
RETURN
20 IF (DER. GT. 0.) DER = -DER*0.5
KCONV = KCONV + 1
IF(KCONV .GE. 10) GO TO 20
RETURN
20 PCNT = 1.0
C DUMM = RECRM(LOC(X3),LOC(X4))
C WRITE (6,30) X3, X4
C 30 FORMAT (38H0 RESTART INITIALIZERS, X3 AND X4, ARE 2F11.0)
IF(STEP .EQ.11.)GOTO 40
PREDER = DER(1)
30 DER(1) = 0.
NJ=N-1
NPT=0
CALL AMRK(AUXSUB)
DER(1) = PREDER
35 40 CALL OOPT3
KSTEP = 2
RETURN
END
```


SUBROUTINE STGE3

CDC 6600 FTN V3.0-P304 OPT=1 30/01

ARO NO.	SEVERITY		DIAGNOSTIC
17	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED
17	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED
17	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED
19	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED
19	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED
19	I	DER	ARRAY NAME OPERAND NOT SUBSCRIPTED, FIRST ELEMENT WILL BE USED

```

      SUBROUTINE AMRK(AUXSUB)
      C*SINGLE PRECISION VERSION* INDEPENDENT VARIABLE IN DOUBLE PRECISION
      COMMON      C(3510)      , GRAPH      , T(1000)
      C      DOUBLE PRECISION DELT,TME
5      C      DOUBLE PRECISION NEWC(200),NEWP(200),OLO(200)
      DIMENSION OLD(200)
      REAL NEWC(200), NEWP(200)
      DIMENSION O(101)      ,EL(100)      ,EU(100)
      DIMENSION V(101)      , GRAPH(300,15)
10     EQUIVALENCE (C(2662),HMIN  ), (C(2663),HMAX  ), (C(2664),O    )
      EQUIVALENCE (C(2765),EL    ), (C(2865),EU    ), (C(2965),V    )
      EQUIVALENCE (C(1971),RITE  ), (J1,N1)
      EQUIVALENCE (C(1973),KASE  ), (C(1974),NJ    ), (C(1975),NPT  )
      DATA KOUNT/0/
15     DATA P1,P2,P3,P4/2.29166667,2.45833333,1.54166667,0.375/
      DATA C2,C3,C4/0.7916667,0.2083333,0.0416667/
      IF(KASE.GT.0)GO TO 20
      N1=NJ
      J2=J1+N1
20     J3=J2+N1
      J4=J3+N1
      J5=J4+N1
      J6=J5+N1
      J7=J6+N1
25     J8=J7+N1
      J9=J8+N1
      KASE=KASE+1
      C*NPT.EQ.0 AOAMS-MOULTON INTEGRATION MOOE
      C*NPT.EQ.1 RUNGE-KUTTA INTEGRATION MODE
30     C*NPT.EQ.2 BEGINNING AOAMS-MOULTON WITH RUNGE-KUTTA START
      20 IF(NPT.EQ.1)GO TO 40
      IF(NPT.EQ.2)GO TO 30
      IF(DELT.NE.(.5*O(1))) GO TO 30
      IF(KOUNT.LT.3)GO TO 40
35     GO TO 200
      30 KOUNT=0
      NPT=0
      C*START RUNGE-KUTTA INTEGRATION
      C*COMPUTE K1
40     40 DO 50 I=1,N1
      NEWP(I)=V(I+1)
      50 CONTINUE
      TME=V(1)
      KOUNT=KOUNT+1
45     DO 60 I=1,N1
      60 OLO(I)=O(1)*D(I+1)
      C COMPUTE K2
      OELT=0.5*O(1)
      TME=TME+DELT
50     V(1)=TME
      DO 70 I=1,N1
      IF(KOUNT.NE.2)GO TO 65
      K1=J9+I
      T(K1)=NEWP(I)
55     65 T(I)=D(I+1)

```

```

        NEWP(I)=NEWP(I)+0.5*OLD(I)
    70  V(I+1)=NEWP(I)
        CALL AUXSUB
        DO 80 I=1,N1
60      80  NEWC(I)=D(1)*D(I+1)
        .C COMPUTE K3
        DO 90 I=1,N1
            NEWP(I)=NEWP(I)+0.5*(NEWC(I)-OLD(I))
65      90  V(I+1)=NEWP(I)
            CALL AUXSUB
            DO 100 I=1,N1
                K2=J7+I
100     T(K2)=D(1)*D(I+1)
        C COMPUTE K4
70      TME=TME+DELT
            V(1)=TME
            DO 110 I=1,N1
                K2=J7+I
75      110  V(I+1)=NEWP(I)
                CALL AUXSUB
                DO 120 I=1,N1
                    K3=J8+I
80      120  T(K3)=D(1)*D(I+1)
        C COMPUTE VALUE OF FUNCTION
            DO 130 I=1,N1
                K2=J7+I
                K3=J8+I
85      NEWP(I)=NEWP(I)-T(K2)+0.16666667*
                X(OLD(I)+NEWC(I)+NEWC(I)+T(K2)+T(K2)+T(K3))
130     V(I+1)=NEWP(I)
140     CALL AUXSUB
            DO 150 I=1,N1
                K5=J1+I
90      K0=J2+I
                K1=J3+I
                K2=J4+I
                K3=J5+I
                K4=J6+I
95      T(K4)=T(K3)
                T(K3)=T(K2)
                T(K2)=T(K1)
                T(K1)=T(K0)
                T(K0)=T(K5)
100     T(K5)=T(I)
150     T(I)=D(I+1)
        RETURN
        C ADAMS-MOULTON INTEGRATION
105     200  KOUNT=KOUNT+1
            DELT=0.5*D(1)
            DO 210 I=1,N1
                K1=J2+I
                K2=J3+I
                K4=J1+I
110     C COMPUTE Y-PREDICTED

```

SUBROUTINE AMPK

CDC 6600 FTN V3.0-P304 OPT=1 30

```
      OLD(I)=NEWP(I)
      NEWP(I)=OLD(I)+D(1)*(P1*T(I)-P2*T(K4)+P3*T(K1)-P4*T(K2))
210  V(I+1)=NEWP(I)
      TME=TME+D(1)
115  V(1)=TME
      CALL AUXSUB
      K5=0
      DO 250 I=1,N1
      K2=J2+I
120  K4=J1+I
      C COMPUTE Y-CORRECTED
      NEWC(I)=OLD(I)+D(1)*(P4*D(I+1)+C2*T(I)-C3*T(K4)+C4*T(K2))
      250 CONTINUE
      C INTEGRATION IS FINISHED. SET UP DERIVATIVES AND EXIT.
125  290 DO 300 I=1,N1
      NEWP(I)=NEWC(I)
      300 V(I+1)=NEWC(I)
      GO TO 140
      END
```

SUBROUTINE AUXI

CDC 6600 FTN V3.0-P304 OPT=1 30

```

SUBROUTINE AUXI
COMMON      C(3510)
EQUIVALENCE (C(2361),NOMOD ), (C(2362),XMODNO), (C(2561),N      )
DIMENSION  XMODNO(99)
5          N = 1
          DO 1 I=1,NOMOD
          L =XMODNO(I)
          GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23
1          ,24,25,26,27,28,29,30,31,32,33,34,35,36,37),L
10         2 CALL A1I
          GO TO 1
          3 CALL A2I
          GO TO 1
          4 CALL A3I
15         GO TO 1
          5 CALL A4I
          GO TO 1
          6 CALL A5I
          GO TO 1
20         7 CALL C1I
          GO TO 1
          8 CALL C2I
          GO TO 1
          9 CALL C3I
25         GO TO 1
          10 CALL C4I
          GO TO 1
          11 CALL C5I
          GO TO 1
30         12 CALL C6I
          GO TO 1
          13 CALL C7I
          GO TO 1
          14 CALL C8I
35         GO TO 1
          15 CALL C9I
          GO TO 1
          16 CALL C10I
          GO TO 1
40         17 CALL D1I
          GO TO 1
          18 CALL D2I
          GO TO 1
          19 CALL D3I
45         GO TO 1
          20 CALL D4I
          GO TO 1
          21 CALL D5I
          GO TO 1
50         22 CALL G1I
          GO TO 1
          23 CALL G2I
          GO TO 1
          24 CALL G3I
55         GO TO 1
```

SUBROUTINE AUXI

CDC 6600 FTN V3.0-P304 OPT=1 30

```
25 CALL G4I
   GO TO 1
26 CALL G5I
   GO TO 1
60 27 CALL G6I
   GO TO 1
28 CALL S1I
   GO TO 1
65 29 CALL S2I
   GO TO 1
30 CALL S3I
   GO TO 1
31 CALL S4I
   GO TO 1
70 32 CALL S5I
   GO TO 1
33 CALL S6I
   GO TO 1
34 CALL S7I
   GO TO 1
75 35 CALL S8I
   GO TO 1
36 CALL S9I
   GO TO 1
80 37 CALL S10I
   1 CONTINUE
   RETURN
   END
```

```

SUBROUTINE AUXSUB
COMMON      C(3510)
EQUIVALENCE (C(2000),T      ), (C(2361),NOMOD ), (C(2362),XMODNO)
EQUIVALENCE (C(2561),N      ), (C(2562),IPL   ), (C(2664),DER   )
5  EQUIVALENCE (C(2965),VAR   )
EQUIVALENCE (C(2020),LCONV)
DIMENSION  DER(101)      , VAR(101)      , IPL(100)
DIMENSION  XMODNO(99)
DO 50 I = 2, N
10  J = IPL(I-1)
50  C(J+3) = VAR(I)
    T = VAR(1)
    DO 1 I=1,NOMOD
15  IF(LCONV.EQ.2)RETURN
    L =XMODNO(I)
    GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,
123,24,25,26,27,28,29,30,31,32,33,34,35,36,37),L
2  CALL A1
    GO TO 1
20 3  CALL A2
    GO TO 1
4  CALL A3
    GO TO 1
25 5  CALL A4
    GO TO 1
6  CALL A5
    GO TO 1
7  CALL C1
    GO TO 1
30 8  CALL C2
    GO TO 1
9  CALL C3
    GO TO 1
35 10 CALL C4
    GO TO 1
11 CALL C5
    GO TO 1
40 12 CALL C6
    GO TO 1
13 CALL C7
    GO TO 1
14 CALL C8
    GO TO 1
45 15 CALL C9
    GO TO 1
16 CALL C10
    GO TO 1
17 CALL D1
    GO TO 1
50 18 CALL D2
    GO TO 1
19 CALL D3
    GO TO 1
55 20 CALL D4
    GO TO 1
```

SUBROUTINE AUXSUB

CDC 6600 FTN V3.0-P304 OPT=1 30.

```
21 CALL D5
   GO TO 1
22 CALL G1
   GO TO 1
60 23 CALL G2
   GO TO 1
24 CALL G3
   GO TO 1
65 25 CALL G4
   GO TO 1
26 CALL G5
   GO TO 1
27 CALL G6
   GO TO 1
70 28 CALL S1
   GO TO 1
29 CALL S2
   GO TO 1
75 30 CALL S3
   GO TO 1
31 CALL S4
   GO TO 1
32 CALL S5
   GO TO 1
80 33 CALL S6
   GO TO 1
34 CALL S7
   GO TO 1
85 35 CALL S8
   GO TO 1
36 CALL S9
   GO TO 1
37 CALL S10
1 CONTINUE
90 DO 60 I = 2, N
   J = IPL(I-1)
60 DER(I) = C(J)
   RETURN
   END
```



```
SUBROUTINE RESET
COMMON      C(3510)
EQUIVALENCE (C(3066),NOLIST), (C(3067),LISTNO), (C(3117),VALUE )
DIMENSION  LISTNO(50)      , VALUE(50)
5          DO 10 I=1,3510
           IF(I.GE.1982.AND.I.LE.2000) GO TO 10
           IF(I.GE.2025.AND.I.LE.2354) GO TO 10
           IF(I.GE.3167.AND.I.LE.3338) GO TO 10
10          IF(I.GE.2361.AND.I.LE.2561) GO TO 10
           IF(I.GE.3066.AND.I.LE.3167) GO TO 10
           IF(I.EQ.3      ) GO TO 10
           IF(I.EQ.4      ) GO TO 10
           IF(I.EQ.23     ) GO TO 10
15          IF(I.EQ.24     ) GO TO 10
           IF(I.EQ.26     ) GO TO 10
           IF(I.EQ.28     ) GO TO 10
           IF(I.EQ.7      ) GO TO 10
           IF(I.EQ.10     ) GO TO 10
           IF(I.EQ.2      ) GO TO 10
20          IF(I.EQ.17     ) GO TO 10
           IF(I.EQ.18     ) GO TO 10
           IF(I.EQ.2000   ) GO TO 10
           IF(I.EQ.2001   ) GO TO 10
           IF(I.EQ.2015   ) GO TO 10
25          IF(I.EQ.2013   ) GO TO 10
           IF(I.EQ.2662   ) GO TO 10
           IF(I.EQ.2663   ) GO TO 10
           IF(I.EQ.2664   ) GO TO 10
           IF(I.GE.50.AND.I.LE.53) GO TO 10
30          IF(I.EQ.3502   ) GO TO 10
           IF(I.EQ.3504   ) GO TO 10
           IF(I.EQ.50     ) GO TO 10
           IF(I.GE.120. AND. I. LE. 128) GO TO 10
           IF(I.EQ.427    ) GO TO 10
35          IF(I.EQ.431    ) GO TO 10
           IF(I.EQ.441    ) GO TO 10
           IF(I.EQ.442    ) GO TO 10
           IF(I.EQ.443    ) GO TO 10
           IF(I.EQ.444    ) GO TO 10
40          IF(I.EQ.446    ) GO TO 10
           IF(I.EQ.447    ) GO TO 10
           IF(I.EQ.449    ) GO TO 10
           IF(I.EQ.448    ) GO TO 10
           IF(I.EQ.450    ) GO TO 10
45          IF(I.EQ.453    ) GO TO 10
           IF(I.EQ.456    ) GO TO 10
           IF(I.EQ.457    ) GO TO 10
           IF(I.EQ.458    ) GO TO 10
           IF(I.EQ.464    ) GO TO 10
50          IF(I.EQ.465    ) GO TO 10
           IF(I.EQ.850    ) GO TO 10
           IF(I.EQ.851    ) GO TO 10
           IF(I.EQ.852    ) GO TO 10
           IF(I.EQ.853    ) GO TO 10
55          IF(I.EQ.855    ) GO TO 10
```

SUBROUTINE RESET

CDC 6600 FTN V3.0-P304 OPT=1 3

```
IF(I.EQ.856 ) GO TO 10
IF(I.EQ.864 ) GO TO 10
IF(I.EQ.863 ) GO TO 10
IF(I.EQ.865 ) GO TO 10
60 IF(I.EQ.866 ) GO TO 10
IF(I.EQ.877 ) GO TO 10
IF(I.EQ.1103 ) GO TO 10
IF(I.EQ.1107 ) GO TO 10
IF(I.EQ.1111 ) GO TO 10
65 IF(I.EQ.1115 ) GO TO 10
IF(I.EQ.1140 ) GO TO 10
IF(I.EQ.1141 ) GO TO 10
IF(I.EQ.1142 ) GO TO 10
IF(I.EQ.1260 ) GO TO 10
70 IF(I.EQ.1261 ) GO TO 10
IF(I.EQ.1262 ) GO TO 10
IF(I.EQ.1263 ) GO TO 10
IF(I.EQ.1264 ) GO TO 10
IF(I.EQ.1265 ) GO TO 10
75 IF(I.EQ.1306 ) GO TO 10
IF(I.EQ.1307 ) GO TO 10
IF(I.EQ.1313 ) GO TO 10
IF(I.EQ.1314 ) GO TO 10
IF(I.EQ.1315 ) GO TO 10
80 IF(I.EQ.1316 ) GO TO 10
IF(I.EQ.1317 ) GO TO 10
IF(I.EQ.1403 ) GO TO 10
IF(I.EQ.1401 ) GO TO 10
IF(I.EQ.1402 ) GO TO 10
85 IF(I.EQ.1404 ) GO TO 10
IF(I.EQ.1414 ) GO TO 10
IF(I.EQ.1415 ) GO TO 10
IF(I.EQ.1416 ) GO TO 10
IF(I.EQ.1417 ) GO TO 10
90 IF(I.EQ.1418 ) GO TO 10
IF(I.EQ.1419 ) GO TO 10
IF(I.EQ.1420 ) GO TO 10
IF(I.EQ.1421 ) GO TO 10
IF(I.EQ.1627 ) GO TO 10
95 IF(I.EQ.1615 ) GO TO 10
IF(I.EQ.1619 ) GO TO 10
IF(I.EQ.1623 ) GO TO 10
IF(I.EQ.1739 ) GO TO 10
IF(I.EQ.1743 ) GO TO 10
100 IF(I.EQ.1747 ) GO TO 10
IF(I.EQ.1751 ) GO TO 10
IF(I.EQ.1752 ) GO TO 10
IF(I.EQ.2008 ) GO TO 10
IF(I.EQ.2009 ) GO TO 10
105 IF(I.EQ.2010 ) GO TO 10
IF(I.EQ.2012 ) GO TO 10
IF(I.EQ.2005) GO TO 10
IF(I.EQ.2006) GO TO 10
IF(I.EQ.2023) GO TO 10
110 IF(I.EQ.1326) GO TO 10
```

SUBROUTINE RESET

CDC 6600 FTN V3.0-P304 OPT=1 31

```
IF(I.EQ.1327) GO TO 10
IF(I.EQ.1328) GO TO 10
IF(I.EQ.1329) GO TO 10
IF(I.EQ.1330) GO TO 10
IF(I.EQ.1331) GO TO 10
IF(I.EQ.1332) GO TO 10
IF(I.EQ.54 ) GO TO 10
IF(I.EQ.55 ) GO TO 10
IF(I.EQ.56 ) GO TO 10
IF(I.EQ.58 ) GO TO 10
IF(I.EQ.57 ) GO TO 10
IF(I.EQ.73 ) GO TO 10
IF(I.EQ.59 ) GO TO 10
IF(I.EQ.1206) GO TO 10
IF(I.EQ.1207) GO TO 10
IF(I.EQ.1208) GO TO 10
IF(I.EQ.1252) GO TO 10
```

10

```
C(I)=0.0
CONTINUE
IF (NOLIST .EQ. 0) RETURN
DO 1 I = 1, NOLIST
  J = LISTNO(I)
  1 C(J) = VALUE(I)
RETURN
```

END

135
MORE MEMORY WOULD HAVE RESULTED IN BETTER OPTIMIZATION

```

C DUMMY SUBROUTINE
  SUBROUTINE DUMMY
C   ENTRY A1
5   C   ENTRY A1I
C   ENTRY A2
C   ENTRY A2I
C   ENTRY A3
C   ENTRY A3I
10  C   ENTRY A4
C   ENTRY A4I
C   ENTRY A5
C   ENTRY A5I
C   ENTRY C1
15  C   ENTRY C1I
C   ENTRY C2
C   ENTRY C2I
C   ENTRY C3
C   ENTRY C3I
C   ENTRY C4
20  C   ENTRY C4I
C   ENTRY C5
C   ENTRY C5I
C   ENTRY C6
C   ENTRY C6I
25  C   ENTRY C7
C   ENTRY C7I
C   ENTRY C8
C   ENTRY C8I
C   ENTRY C9
30  C   ENTRY C9I
C   ENTRY C10
C   ENTRY C10I
C   ENTRY D1
35  C   ENTRY D1I
C   ENTRY D2
C   ENTRY D2I
C   ENTRY D3
C   ENTRY D3I
40  C   ENTRY D4
C   ENTRY D4I
C   ENTRY D5
C   ENTRY D5I
C   ENTRY G1
45  C   ENTRY G1I
C   ENTRY G2
C   ENTRY G2I
C   ENTRY G3
C   ENTRY G3I
50  C   ENTRY G4
C   ENTRY G4I
C   ENTRY G5
C   ENTRY G5I
C   ENTRY G6
C   ENTRY G6I
55  C   ENTRY S1

```

```
        ENTRY S1I
        ENTRY S2
        ENTRY S2I
        ENTRY S3
60      ENTRY S3I
        ENTRY S4
        ENTRY S4I
        ENTRY S5
        ENTRY S5I
65      ENTRY S6
        ENTRY S6I
        ENTRY S7
        ENTRY S7I
        ENTRY S8
70      ENTRY S8I
        ENTRY S9
        ENTRY S9I
        ENTRY S10
        ENTRY S10I
75      ENTRY AUXA1
        ENTRY AUXA2
        ENTRY AUXA3
        ENTRY AUXB1
        ENTRY AUXB2
80      ENTRY AUXB3
        ENTRY AUXC1
        ENTRY AUXC2
        ENTRY AUXC3
        ENTRY CNTR1
85      ENTRY CNTR2
        ENTRY CNTR3
        ENTRY INPT1
        ENTRY INPT2
        ENTRY INPT3
90      ENTRY OOPT1
        C   ENTRY OOPT2
        C   ENTRY OOPT3
        ENTRY PROCES
        C
95      ENTRY RESET
        ENTRY RNDM1
        ENTRY RNDM2
        ENTRY RNDM3
        ENTRY STGE1
        C   ENTRY STGE2
100     C   ENTRY STGE3
        C   ENTRY SUBL1
        C   ENTRY SUBL2
        ENTRY KIKSET
        ENTRY COUNTV
105     RETURN
        END
```

```

C** FOR USE WITH CODIM2, FCN2, FCN3
C
      SUBROUTINE TERROR (XLABEL)
      COMMON C(3510)
5      EQUIVALENCE (C(2020),LCONV)
      WRITE (6,10) XLABEL
10     FORMAT ( 43H0          NO AERO POINTS SPECIFIED FOR ARG , 5X,
C       7HTABLE ,A6 )
      CALL EXIT
10
C
      ENTRY AERROR
      WRITE (6,20) XLABEL
20     FORMAT ( 43H0          OUT OF AERO TABLE ARGUMENT ARRAY , 5X,
C       7HTABLE ,A6 )
15     DO 40 I=1202,1251,7
40     WRITE(6,30) C(I),C(I+1),C(I+2),C(I+3),C(I+4),C(I+5),C(I+6)
30     FORMAT(1H ,7E15.7)
      WRITE (6,30) C(2000),C(367),C(368),C(204),C(369),C(370),C(1117),
20     C C(1118),C(1119),C(1120)
      LCONV=2
      RETURN
      END

```

FUNCTION SIND

CDC 6600 FTN V3.0-P304 OPT=1 30

```
FUNCTION SIND (X)
SIND= SIN (X/57.29578)
RETURN
END
```

FUNCTION COSD

CDC 6600 FTN V3.0-P304 OPT=1 30

```
FUNCTION COSD (X)
COSD= COS (X/57.29578)
RETURN
END
```


FUNCTION ATAND

CDC 6600 FTN V3.0-P304 OPT=1 30

```
5      1      FUNCTION ATAND (Y,X)
          IF(X.EQ.0.0.AND.Y.EQ.0.0) GO TO 1
          ATAND= 57.29578*ATAN2 (Y,X)
          CONTINUE
          RETURN
          END
```

SUBROUTINE TABLE

CDC 6600 FTN V3.0-P304 OPT=1 30

```
SUBROUTINE TABLE (X,XI,YI,NX,XK,XLABEL,Y)
DIMENSION XLABEL (2)
Y = CODIM2 (X,XI,YI,NX,XK,XLABEL)
RETURN
END
```

5

SUBROUTINE TABL2

CDC 6600 FTN V3.0-P304 OPT=1 30

```
SUBROUTINE TABL2(X,Y,XYI,ZI,NXY,XINTER,XLABEL,Z)
DIMENSION XYI(2),NXY(2)
Z = FCODN2 (X,Y,XYI,XYI(NXY+1),ZI,NXY,NXY(2),NXY,XINTER,XLABEL)
RETURN
END
```

5

SUBROUTINE TABL3

CDC 6600 FTN V3.0-P304 OPT=1 30

```
SUBROUTINE TABL3(X,Y,Z,XYZI,WI,NXYZ,XINTER,XLABEL,W)
DIMENSION XYZI(1),NXYZ(1)
NZI= NXYZ(1) + NXYZ(2) + 1
W = FCODN3 (X,Y,Z,XYZI,XYZI(NXYZ+1),XYZI(NZI), WI,NXYZ(3),
C NXYZ(2),NXYZ,XINTER,XLABEL)
RETURN
END
```

5

SUBROUTINE TIMEV

CDC 6600 FTN V3.0-P304 OPT=1 30

 SUBROUTINE TIMEV(DELT)
 RETURN
 END

SUBROUTINE WRITE

CDC 6600 FTN V3.0-P304 OPT=1 30

 SUBROUTINE WRITE(IA,F,N)
 RETURN
 END

```

SUBROUTINE PLOT4 (GRAPH, NP, YL, T, NPLLOT4, NPLLOT2, NOPLOTT)
C**PLOT SUBROUTINE
DIMENSION GRAPH(300,15), YL(2,15), T(300)
IF (NPLLOT4.EQ.0) RETURN
5   KK = 1
      XM1 = GRAPH(1,1)
      YM1 = GRAPH(1,2)
      XT1 = GRAPH(1,3)
      YT1 = GRAPH(1,4)
10  XM2 = XM1
      YM2 = YM1
      XT2 = XT1
      YT2 = YT1
15  DO 1 I=1, NP
      XM1 = AMIN1(GRAPH(I,1), XM1)
      YM1 = AMIN1(GRAPH(I,2), YM1)
      XT1 = AMIN1(GRAPH(I,3), XT1)
      YT1 = AMIN1(GRAPH(I,4), YT1)
      XM2 = AMAX1(GRAPH(I,1), XM2)
20  YM2 = AMAX1(GRAPH(I,2), YM2)
      XT2 = AMAX1(GRAPH(I,3), XT2)
1   YT2 = AMAX1(GRAPH(I,4), YT2)
      XMIN = AMIN1(XM1, XT1)
      YMIN = AMIN1(YM1, YT1)
25  XMAX = AMAX1(XM2, XT2)
      YMAX = AMAX1(YM2, YT2)
      DELX = ABS(XMAX-XMIN)
      DELY = ABS(YMAX-YMIN)
30  DEL = AMAX1(DELX, DELY)
      X1 = XMIN
      Y1 = YMIN-(DEL-DELY)/2.
      X2 = X1+DEL
      Y2 = Y1+DEL
      CALL CAMRAV (9)
35  CALL SETMIV (24,0,24,24)
      CALL DXDYV(1, X1, X2, DX, N, I, NX, 25., IERR)
      CALL DXDYV(2, Y2, Y1, DY, M, J, NY, 25., IERR)
      CALL GRID1V(KK, X1, X2, Y2, Y1, DX, DY, N, M, I, J, NX, NY)
40  DO 2 J=1,3,2
      K = J+1
      UTIME = 0.
      IX1 = NXV(GRAPH(1,J) )
      IY1 = NYV(GRAPH(1,K) )
45  DO 2 IJ=2, NP
      IX2 = NXV(GRAPH(IJ,J))
      IY2 = NYV(GRAPH(IJ,K))
      IF(T(IJ)-(0.5+UTIME)) 7,3,3
3   UTIME = T(IJ)
      CALL POINTV(IX2, IY2, -17, 2)
50  7 IF(J-2) 4,5,5
      5 CALL POINTV(IX2, IY2, 0, 2)
      GO TO 6
      4 CALL LINEV(IX1, IY1, IX2, IY2)
      6 IX1 = IX2
55  2 IY1 = IY2

```

SUBROUTINE PLOT4

CDC 6600 FTN V3.0-P304 OPT=1 30

LAB1=(YL(1,1).AND.77777777777700000000B).OR.(SHIFT(YL(2,1),-36)
*.AND.77777777B)

LAB2=(YL(1,2).AND.77777777777700000000B).OR.(SHIFT(YL(2,2),-36)
*.AND.77777777B)

60

CALL PRINTV(10,LAB1 ,524,12)
CALL APRNTV(0,-14,10,LAB2 ,12,524)
RETURN
END


```

C
C
SUBROUTINE PLOT2 (GRAPH, NP, YL, T, NPLOT4, NPLOT2, NOPLOT)
DIMENSION GRAPH(300,15), YL(2,15), T(300)
5   DIMENSION IXP(4), IYP(4), MRKPT(4)
DATA (MRKPT(I), I=1,4)/42,16,38,63/
DATA(IXP(I), I=1,4)/4,28,4,28/
DATA(IYP(I), I=1,4)/776,776,411,411/
10  IF (NPLOT2.EQ.0) RETURN
JX= NPLOT4+1
JY1= JX+1
JYN= NPLOT4+NPLOT2
X1= GRAPH(1,JX)
X2= X1
15  DO 110 I=2, NP
X1= AMIN1 (GRAPH(I,JX), X1)
110 X2= AMAX1 (GRAPH(I,JX), X2)
Y1= GRAPH(1,JY1)
Y2= Y1
20  DO 120 JY=JY1, JYN
DO 120 I=1, NP
Y1= AMIN1 (GRAPH(I,JY), Y1)
120 Y2= AMAX1 (GRAPH(I,JY), Y2)
CALL CAMRAV (9)
25  CALL SETMIV (36,24,24,24)
CALL DXDYV (1, X1, X2, DX, N, I, NX, 14.0, IERR)
CALL DXDYV (2, Y1, Y2, DY, M, J, NY, 14.0, IERR)
CALL GRID1V (1, X1, X2, Y1, Y2, DX, DY, N, M, I, J, -3, -3)
IMARK= 1
30  DO 140 JY=JY1, JYN
IX1= NXV (GRAPH(1,JX))
IY1= NYV (GRAPH(1,JY))
C
DO 130 IJ=2, NP
35  IX2= NXV (GRAPH(IJ,JX))
IY2= NYV (GRAPH(IJ,JY))
CALL LINEV (IX1, IY1, IX2, IY2)
CALL LINEV (IX1, IY1, IX2, IY2)
IX1= IX2
40  130 IY1= IY2
IF (IMARK.GT.4) GO TO 140
CALL APLOTV (NP, GRAPH(1,JX), GRAPH(1,JY), 20, 20, 1, MRKPT(IMARK), IRR)
140 IMARK= IMARK + 1
LAB1=(YL(1,JX).AND.777777777777700000000B).OR.(SHIFT(YL(2,JX), -36)
45  *.AND.77777777B)
CALL PRINTV (10, LAB1, ,468,8)
I=1
DO 150 JY=JY1, JYN
IF (I.GT.4) GO TO 150
IYQ= IYP(I) + 28
50  CALL PLOTV (IXP(I), IYQ, MRKPT(I))
LAB2=(YL(1,JY).AND.777777777777700000000B).OR.(SHIFT(YL(2,JY), -36)
*.AND.77777777B)
CALL APRNTV (0, -14, 10, LAB2, , IXP(I), IYP(I))
55  150 I= I+1

```

SUBROUTINE PLOT2

CDC 6600 FTN V3.0-P304 OPT=1 30,

RETURN
END

5
5

C
C

```

SUBROUTINE PLOTN (GRAPH, NP, YL, T, NPLCT4, NPLCT2, NOPLCT)
DIMENSION GRAPH(300,15), YL(2,15), T(300)
5  NPLCT3=NOPLCT-NPLCT2-NPLCT4
  IF (NPLCT3.LE.0) RETURN
  DO 100 NM=1, NPLCT3
  JY=NPLCT4+NPLCT2+NM
  IX=MOD(NM,3)
  IF (IX .EQ. 0) IX=3
  II=712-344*(IX-1)
  JJ=28+344*(IX-1)
  KK=1
  IF (IX .GT. 1) KK=2
  X1=T(1)
  X2=T(NP)
  Y1=GPAPH(1, JY)
  Y2=Y1
  DO 50 I=1, NP
  Y1=AMIN1 (GRAPH(I, JY), Y1)
50  Y2=AMAX1 (GRAPH(I, JY), Y2)
  CALL CAMRAV (9)
  CALL SETMIV (24, 0, II, JJ)
  CALL OXDYV (1, X1, X2, DX, N, I, NX, 14., IERR)
25  CALL OXDYV (2, Y1, Y2, DY, M, J, NY, 10., IERR)
  CALL GRID1V (KK, X1, X2, Y1, Y2, DX, DY, N, M, I, J, NX, -3)
  IX1=NXV (X1)
  IY1=NYV (GRAPH(1, JY))
  DO 55 IJ=2, NP
  IX2=NXV (T(IJ))
  IY2=NYV (GRAPH(IJ, JY))
  CALL LTNEV (IX1, IY1, IX2, IY2)
  IY1=IY2
30  IJ=2, NP
  IX2=NXV (T(IJ))
  IY2=NYV (GRAPH(IJ, JY))
  CALL LTNEV (IX1, IY1, IX2, IY2)
  IY1=IY2
55  IX1=IX2
  CALL PRINTV (-11, 10HTIME (SEC), 468, 696-344*(IX-1))
  LAB2=(YL(1, JY).AND.77777777777700000000).OR.(SHIFT (YL(2, JY), ~36)
35  *.AND.77777777B)
  CALL APRNTV (0, -14, 10, LAB2          , 4, 890-344*(IX-1))
  RETURN
40  END

```

```

C .....
C
C     SUBROUTINE CODIM2
C
5     C     PURPOSE
C         TO FIT A SET OF POINTS WITH A CONTINUOUS FUNCTION THAT
C         SIMULATES A FRENCH CURVE TYPE CURVE FIT.
C
C     USAGE
10    C     Y = CODIM2 ( X , XI , YI , N , F , XLABEL )
C         OR
C         Y = CODIM1 ( X , XI , YI , N , F , XLABEL )
C
C     DESCRIPTION OF PARAMETERS
15    C     X     ARGUMENT - INDEPENDENT VARIABLE
C         XI    ARRAY OF INDEPENDENT VARIABLE , X
C         YI    ARRAY OF DEPENDENT VARIABLE , Y
C         N     NUMBER OF POINTS REPRESENTED BY XI AND YI ARRAYS
C         F     INTERPOLATION CONTROL
20    C         LESS THAN ZERO - STRAIGHT LINE INTERPOLATION
C         POSITIVE - END INTERVAL INTERPOLATION
C         0.0   STRAIGHT LINE
C         1.0   FULL PARABOLIC
C         XLABEL HOLLERITH FIELD OF UP TO 6 CHARACTERS
25    C
C     REMARKS
C         EXTRAPOLATION IS DONE BY PASSING A STRAIGHT LINE THRU THE
C         TWO POINTS AT THE END INTERVAL.
C         THE ARRAY OF THE INDEPENDENT VARIABLE , XI , MAY BE IN
30    C         EITHER INCREASING OR DECREASING ORDER.
C
C .....
35    FUNCTION CODIM2 ( X , XI , YI , N , F , XLABEL )
C
C     DIMENSION XI(N) , YI(N) , P(2) , E(2) , IS(4,2) , XLABEL(2)
C     LOGICAL OUT
C     ENTRY CODIM1
40    DATA IS / -1, 0, -2, -1, 0, 1, -1, 0 /
C
100   OUT = .FALSE.
C     N1 = N
C     XX = X
45   J = 1
C     IF ( N1 - 2 ) 150 , 1200 , 300
150  CALL TERROR (XLABEL)
200  CODIM2 = YI(J)
C     RETURN
50
300  KPL = 1
C     KPU = 2
C     IF ( XI(1) - XI(2) ) 400 , 150 , 600
400  DO 500 J = 1 , N1
55   IF ( XX - XI(J) ) 900 , 200 , 500
C
C     209

```

FUNCTION CODIM2

CDC 6600 FTN V3.0-P304 OPT=1 30.

```
500 CONTINUE
    GO TO 800
600 DO 700 J = 1 , N1
    IF ( XI(J) - XX ) 900 , 200 , 700
60 700 CONTINUE

800 J = N1
    CALL AERROR (XLABEL)
    GO TO 1300
65

900 OUT = F .LT. 0.0
    IF ( J - 2 ) 1200 , 1000 , 1100
1000 KPL = 2
    GO TO 1500
70 1100 IF ( J - N1 ) 1500 , 1400 , 1300
1200 J = 2
1300 OUT = .TRUE.
1400 KPU = 1
75 1500 AL = ( XX - XI(J-1) ) / ( XI(J) - XI(J-1) )
    CODIM2 = AL * YI(J) + ( 1.0 - AL ) * YI(J-1 )
    IF ( OUT ) RETURN

    DO 1800 KP = KPL , KPU
    P(KP) = 0.0
80 DO 1600 K = 1 , 3
    J0 = J + KP + K - 4
    X0 = XI(J0)
    Y0 = YI(J0)
    J1 = J + IS(K,KP)
85 J2 = J + IS(K+1,KP)
1600 P(KP) = P(KP) + Y0 * ( XX - XI(J1) ) / ( X0 - XI(J1) )
    * ( XX - XI(J2) ) / ( X0 - XI(J2) )
    IF ( KPL .NE. KPU ) GO TO 1700
    J1 = 3 - KPL
90 P(J1) = CODIM2 + F * ( P(KP) - CODIM2 )
    E(J1) = ABS ( P(J1) - CODIM2 )
1700 E(KP) = ABS ( P(KP) - CODIM2 )
1800 CONTINUE

95 IF ( E(1) + E(2) .EQ. 0.0 ) RETURN
    CODIM2 = ( ( E(1) * AL ) * P(2) + ( E(2) * ( 1.0 - AL ) )
    * P(1) ) / ( ( E(1) * AL ) + ( E(2) * ( 1.0 - AL ) ) )

100 RETURN
    END
```

```

C      2-DIMENSIONAL INTERPOLATION SUBPROGRAM....FCODN2
C
C      CALLING SEQUENCE -
C      Z = FCODN2(X,Y,XI,YI,ZI,NXD,NY,NX,XK,XLABEL)
5
C
C      X = ARGUMENT - 1ST VARIABLE
C      Y = ARGUMENT - 2ND VARIABLE
C      XI = ARRAY OF 1ST VARIABLE
C      YI = ARRAY OF 2ND VARIABLE
10
C      ZI = ARRAY OF DEPENDENT VARIABLE
C      NXD = DIMENSIONED SIZE OF XI ARRAY
C      NY = NUMBER OF VALUES IN ARRAY YI
C      NX = NUMBER OF VALUES IN ARRAY XI
C      XK = END INTERVAL INTERPOLATION CONTROL CONSTANT
15
C      XLABEL = HOLLERITH FIELD OF UP TO 6 CHARACTERS
C
C      THIS ROUTINE DIFFERS FROM FCOOM2 IN THAT THE ZI ARRAY DOES NOT
C      HAVE TO BE PACKED - I.E., IT DOES NOT HAVE TO OCCUPY CON-
C      SECUTIVE LOCATIONS IN CORE, AND IN THAT EITHER OR BOTH THE
20
C      XI AND YI ARRAYS MAY BE IN ASCENDING OR DESCENDING ORDER.
C
C      FUNCTION FCODN2(X,Y,XI,YI,ZI,NXD,NY,NX,XK,XLABEL)
C
C      DIMENSION XI(1), YI(1), ZI(NXD,1), T(4), XLABEL(2)
25
C      IF (NY.GT.4) GO TO 120
C      N3=1
C      N3 IS THE INDEX NUMBER OF THE FIRST Y CURVE TO BE USED
C      N4=NY
30
C      N4 IS THE COUNT OF THE NUMBER OF Y CURVES TO BE USED
C      GO TO 200
C
C      120 N4=4
35
C      IF (YI(1)-YI(2)) 130,150,133
C      130 DO 132 K=1,NY
C      IF (Y-YI(K)) 150,150,132
C      132 CONTINUE
C      GO TO 140
C
C      133 DO 134 K=1,NY
C      IF (YI(K)-Y) 150,150,134
C      134 CONTINUE
40
C      140 N3=NY-3
C      GO TO 200
45
C
C      150 IF (K-3) 155,155,160
C      155 N3=1
C      GO TO 200
50
C
C      160 IF (K-NY) 165,140,140
C      165 N3=K-2
C
C      200 L=N3
55
C      DO 300 I=1,N4

```

FUNCTION FCODN2

CDC 6600 FTN V3.0-P304 OPT=1 30

T(I)=CODIM2(X,XI,ZI(1,L),NX,XK,XLABEL)

300 L=L+1

C

FCODN2=CODIM2(Y,YI(N3),T,N4,XK,XLABEL)

RETURN

END

60

```

C      3-DIMENSIONAL INTERPOLATION SUBPROGRAM....FCODN3
C
C      CALLING SEQUENCE -
5      C      W = FCOON3(X,Y,Z,XI,YI,ZI,WI,NZ,NY,NX,XK,XLABEL)
C          X = ARGUMENT - 1ST VARIABLE
C          Y = ARGUMENT - 2ND VARIABLE
C          Z = ARGUMENT - 3RD VARIABLE
C          XI = ARRAY OF 1ST VARIABLE
10     C          YI = ARRAY OF 2ND VARIABLE
C          ZI = ARRAY OF 3RD VARIABLE
C          WI = ARRAY OF DEPENDENT VARIABLE
C          NZ = NUMBER OF POINTS IN ZI ARRAY
C          NY = NUMBER OF POINTS IN YI ARRAY
15     C          NX = NUMBER OF POINTS IN XI ARRAY
C          XK = END INTERVAL INTERPOLATION CONTROL CONSTANT (0.0 TO 1.0)
C      XLABEL = HOLLERITH FIELD OF UP TO 6 CHARACTERS
C
C      FCOON3 DIFFERS FROM FCOOM3 IN THAT THE WI ARRAY DOES NOT NEED
20     C      TO BE PACKED, I.E., WI NEED NOT OCCUPY CONSECUTIVE LOCATIONS
C      IN CORE, AND ANY OR ALL ARRAYS MAY BE IN EITHER ASCENDING OR
C      DESCENDING ORDER.
C
C      FUNCTION FCOON3(X,Y,Z,XI,YI,ZI,WI,NZ,NY,NX,XK,XLABEL)
25     C
C      DIMENSION XI(1),YI(1),ZI(1), WI(NX,NY,1),T(4),XLABEL(2)
C
C      IF (NZ.GT.4) GO TO 120
C      N4=1
30     C      N5=NZ
C      GO TO 200
C
120    C      N5=4
C      IF (ZI(1)-ZI(2)) 130,150,133
35     C      130      DO 132 K=1,NZ
C          IF (Z-ZI(K)) 150,150,132
C      132      CONTINUE
C      GO TO 140
C
40     C      133      DO 134 K=1,NZ
C          IF (ZI(K)-Z) 150,150,134
C      134      CONTINUE
C      140      N4=NZ-3
C      GO TO 200
45     C
C      150      IF (K.GT.3) GO TO 160
C          N4=1
C          GO TO 200
C
50     C      160      IF (K.GE.NZ) GO TO 140
C          N4=K-2
C
200    C      L=N4
C          DO 300 I=1,N5
55     C          T(I)= FCOON2 (X,Y,XI,YI,WI(1,1,L),NX,NY,NX,XK,XLABEL)

```


FUNCTION FCODN3

CDC 6600 FTN V3.0-P304 OPT=1 30

300 L=L+1

C

FCODN3=CODIM2(Z,ZI(N4),T,NZ,XK,XLABEL)

RETURN

END

EO

EXAMPLE I. PROGRAM

INPUT DATA

1	OUPT 2,3	3	-0.	-0.
1	STAG2,3	4	-0.	-0.
2	G2-T	23	-0.	-0.
2	G3	24	-0.	-0.
2	G5	26	-0.	-0.
2	A1	2	-0.	-0.
2	A3-T	4	-0.	-0.
2	A2	3	-0.	-0.
2	D1	17	-0.	-0.
2	D2	18	-0.	-0.
3	TF	2001	1.00000000E+00	-0.
3	T	2000	-0.	1.00000000E+00
3	PPP	2005	1.00000000E-02	1.00000000E+00
3	REPPLT	2006	1.00000000E+00	-0.
3	CPP	2015	5.00000000E-02	1.00000000E+00
3	DOC	2013	6.00000000E+00	1.00000000E+00
3	DERX1<	2664	2.00000000E-03	1.00000000E+00
3	PPP1	120	6.00000000E-03	-0.
3	CPP1	121	1.00000000E-01	-0.
3	DER1	122	2.00000000E-03	-0.
3	XTL	123	2.00000000E+01	-0.
3	XLL	124	9.00000000E+00	-0.
3	YLT	125	7.00000000E+00	-0.
3	YLL	126	1.00000000E+00	-0.
3	ZTL	127	9.00000000E+00	-0.
3	ZLL	128	1.00000000E+00	-0.
3	OPTN4	3502	-0.	-0.
3	AGRAV	1627	3.21740000E+01	-0.
3	CRAD	1751	5.7295770E+01	-0.
3	WP	1739	-0.	1.00000000E+00
3	WQ	1743	-0.	1.00000000E+00
3	WR	1747	-0.	1.00000000E+00
3	RXE	1615	0.	1.00000000E+00
3	RYE	1619	-0.	1.00000000E+00
3	RZE	1623	-5.00000000E+03	1.00000000E+00
3	RTXE	1651	0.	1.00000000E+00
3	RTYE	1655	-0.	1.00000000E+00
3	RTZE	1659	-5.00000000E+03	1.00000000E+00
3	EFORCX	1326	-0.	-0.
3	EFT	1332	1.00000000E+01	-0.
3	EJD	1333	2.55400000E-01	1.00000000E+00
3	DIASC	69	1.00000000E+00	1.00000000E+00
3	FMIXO	1419	4.00000000E+00	-0.
3	FMIYO	1420	5.00000000E+01	-0.

3	OPTNW	50	1.0000000E+00	1.0000000E+00
3	XTAIL	57	-3.0000000E+00	-0.
3	XNOSE	59	2.5600000E+00	-0.
3	XNOSE1	73	2.0000000E+00	-0.
3	RFLGTH	1307	1.3333300E+00	-0.
3	RFAREA	1306	1.3960000E+00	-0.
3	DWT	1415	8.2300000E+02	-0.
3	DWP	1416	1.0000000E+00	-0.
3	CISP	1414	1.0000000E+00	-0.
3	XINTER	1252	-1.0000000E+00	1.0000000E+00
3	PLOTN0	2008	1.2000000E+01	-0.
3	PLOTN2	1983	-0.	-0.
3	PLOTN4	1982	-0.	-0.
3	CMQ	1207	-1.2200000E+00	-0.
3	CNR	1208	-1.2200000E+00	-0.
3	CLP	1206	-3.3000000E-01	-0.
3	TNOSOS	58	1.0000000E+00	-0.
3	YPOS	55	6.8000000E+00	-0.
3	XPOS	54	2.1966000E+01	-0.
3	ZPOS	56	-3.0000000E+00	-0.
3	EFORCZ	1328	1.2000000E+03	-0.
3	EFORCY	1327	-0.	-0.
3	EMOMZ	1331	-0.	-0.
3	CNA A	1273	9.6000000E-02	1.0000000E+00
3	CAA	1274	1.2000000E-01	1.0000000E+00
3	CMAA	1272	-1.3330000E-01	1.0000000E+00
3	VMACH	204	8.5000000E-01	1.0000000E+00
3	ALPHAD	381	-0.	-0.
3	STEP	2010	2.0000000E+00	-0.
4	P	1739	-0.	-0.
4	PHI MSL	352	-0.	-0.
4	CX	1203	-0.	-0.
4	CL	1209	-0.	-0.
4	XNOSE1	73	-0.	-0.
4	Q	1743	-0.	-0.
4	THETA MSL	350	-0.	-0.
4	CY	1204	-0.	-0.
4	CM	1210	-0.	-0.
4	AAN	60	-0.	-0.
4	R	1747	-0.	-0.
4	PSI	351	-0.	-0.
4	CZ	1205	-0.	-0.
4	CN	1211	-0.	-0.
4	ASN	61	-0.	-0.
4	FMXBA	1303	-0.	-0.
4	FXBA	1300	-0.	-0.
4	XNPOS	90	-0.	-0.
4	VXED	1600	-0.	-0.
4	XTPOS	93	-0.	-0.

4	FMYBA	1304	-0.	-0.
4	FYBA	1301	-0.	-0.
4	YNPOS	91	-0.	-0.
4	VYED	1604	-0.	-0.
4	YTPOS	94	-0.	-0.
4	FMZBA	1305	-0.	-0.
4	FZBA	1302	-0.	-0.
4	ZNPOS	92	-0.	-0.
4	VZED	1608	-0.	-0.
4	ZTPOS	95	-0.	-0.
4	RXED	1612	-0.	-0.
4	RXE	1615	-0.	-0.
4	RTXED	1648	-0.	-0.
4	RTXE	1651	-0.	-0.
4	DELX	70	-0.	-0.
4	RYED	1616	-0.	-0.
4	RYE	1619	-0.	-0.
4	RTYED	1652	-0.	-0.
4	RTYE	1655	-0.	-0.
4	DELY	71	-0.	-0.
4	RZED	1620	-0.	-0.
4	RZE	1623	-0.	-0.
4	RTZED	1656	-0.	-0.
4	RTZE	1659	-0.	-0.
4	DELZ	72	-0.	-0.
4	XLUN	67	-0.	-0.
4	YLUN	45	-0.	-0.
4	ZLUN	44	-0.	-0.
4	DIASC	69	-0.	-0.
4	TNOSOS	58	-0.	-0.
7	PITCH	350	-0.	-0.
7	YAW	351	-0.	-0.
7	ROLL	352	-0.	-0.
7	X FT	70	-0.	-0.
7	Y FT	71	-0.	-0.
7	Z FT	72	-0.	-0.
7	XNPOS	90	-0.	-0.
7	YNPOS	91	-0.	-0.
7	ZNPOS	92	-0.	-0.
7	XTPOS	93	-0.	-0.
7	YTPOS	94	-0.	-0.
7	ZTPOS	95	-0.	-0.
6		-0	-0.	-0.

BURNOUT TIME= -0.0000 SEC.

TIME= .0020000 STEP SIZE= 2.0000000E-03

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.0020000	-2.0695088E-01	-1.6590527E-04	1.2000000E-01	-5.2506054E-03	2.0000000E+00
	-6.6894790E+00	-6.3328780E-03	8.6983434E-02	-2.5173116E+00	2.8436694E-01
	2.4153754E-01	2.5074949E-04	8.9878075E-01	9.9718304E-02	1.6654031E-02
	-8.6156060E+00	-1.4892836E+02	-2.5599883E+00	-5.8321674E+00	3.0000116E+00
	-4.1596130E+03	1.0804517E+02	1.5921883E-05	4.2241069E+00	-8.4109238E-06
	1.6480858E+02	2.3164429E+03	4.6501905E-04	1.2273134E+02	-1.4952537E-04
	9.3303335E+02	1.8660784E+00	9.3304500E+02	1.8660900E+00	-1.1634401E-05
	5.7822214E-03	5.6034417E-06	0.	0.	5.6034417E-06
	2.0964013E-01	-4.9999998E+03	0.	-5.0000000E+03	2.1608488E-04
	1.1643607E+01	4.0800096E+00	1.8002790E+00	1.0000000E+00	1.0000000E+00

.0500000	-1.5307826E+01	-2.7851998E-01	1.2000000E-01	-4.4526276E-02	2.0000000E+00
	-1.7634668E+02	-4.6675290E+00	1.3721488E-01	-1.9510910E+00	2.8547267E-01
	6.5107912E+00	1.8112928E-01	1.3185769E+00	1.1077417E-01	2.2843481E-02
	-6.7799353E+01	-5.1445180E+01	-2.5435254E+00	-1.1040183E+01	2.9980072E+00
	-2.9782226E+03	1.6466820E+02	1.2873953E-02	6.9411358E+00	-4.6445650E-03
	1.7413204E+02	2.8342673E+03	3.4992475E-01	1.4241198E+02	-1.0251282E-01
	9.3269389E+02	4.6644281E+01	9.3304500E+02	4.6652254E+01	-7.9730889E-03
	2.1317294E-01	4.8094006E-03	0.	0.	4.8094006E-03
	5.8394288E+00	-4.9998584E+03	0.	-5.0000000E+03	1.4162601E-01
	1.1653485E+01	4.0877244E+00	2.0099548E+00	1.0000000E+00	1.0000000E+00

.1000000

1.2481862E+01	-3.3489561E-01	1.2000000E-01	1.6262692E-02	2.0000000E+00
-2.3443091E+02	-1.5648242E+01	1.7834545E-01	-2.2747261E-01	2.3939556E-01
1.0145149E+01	7.0416169E-01	2.1257385E+00	2.1714599E-02	2.0427898E-02
2.2058515E+01	-1.4896990E+02	-2.4201874E+00	-3.3531790E+01	2.9333284E+00
-3.9076237E+01	2.2140086E+02	5.4236256E-02	8.8467670E+00	-1.1561444E-02
2.1339426E+01	2.6389254E+03	1.2784501E+00	1.2989395E+02	-2.2125170E-01
9.3175417E+02	9.3259764E+01	9.3304500E+02	9.3304509E+01	-4.4744764E-02
5.6744150E-01	2.3942227E-02	0.	0.	2.3942227E-02
1.1770231E+01	-4.9994120E+03	0.	-5.0000000E+03	5.8795434E-01
1.1727488E+01	4.1125418E+00	2.5670701E+00	1.0000000E+00	1.0000000E+00

.1500000

2.5087339E+01	4.4964340E-01	1.2000000E-01	1.4734960E-02	2.0000000E+00
-1.3169227E+02	-2.5400050E+01	2.2460230E-01	1.3933599E+00	1.8404975E-01
6.9161447E+00	1.2069791E+00	2.7663162E+00	-7.8392862E-02	1.7729043E-02
1.4552031E+01	-1.4843709E+02	-2.1513902E+00	-6.2849506E+01	2.8700333E+00
2.4872850E+03	2.7782759E+02	1.1128396E-01	8.4891201E+00	5.4882125E-03
-1.3923050E+02	3.4218660E+03	2.4375570E+00	1.5059985E+02	5.2675324E-02
9.2945912E+02	1.3979613E+02	9.3304500E+02	1.3995676E+02	-1.6063705E-01
9.7604790E-01	6.2573161E-02	0.	0.	6.2573161E-02
1.8476279E+01	-4.9986605E+03	0.	-5.0000000E+03	1.3394924E+00
1.1888766E+01	4.1467704E+00	3.2625342E+00	1.0000000E+00	1.0000000E+00

.2000000

3.4828569E+01	1.9034253E+00	1.2000000E-01	1.7852128E-02	2.0000000E+00
6.2402220E+01	-2.7336164E+01	2.5569580E-01	2.1411766E+00	1.1810473E-01
-4.9055058E+00	1.3003987E+00	2.6825679E+00	-1.8073689E-01	1.2901211E-02
1.5723295E+01	-1.4723394E+02	-1.8538687E+00	-6.4519466E+01	3.0839560E+00
3.4135125E+03	3.1372583E+02	1.7205432E-01	6.5215112E+00	5.9965026E-02
-2.8865271E+02	3.2913753E+03	3.6201006E+00	1.4413205E+02	1.0668934E+00
9.2625060E+02	1.8618935E+02	9.3304500E+02	1.8660902E+02	-4.1966547E-01
1.3234410E+00	1.2044534E-01	0.	0.	1.2044534E-01
2.5683007E+01	-4.9975555E+03	0.	-5.0000000E+03	2.4445297E+00
1.2067279E+01	4.1832326E+00	3.9720603E+00	1.0000000E+00	1.0000000E+00

.2500000

4.9267442E+01	4.1791138E+00	1.2000000E-01	2.5434184E-02	2.0000000E+00
2.4512975E+02	-1.9303937E+01	2.1963031E-01	1.6131181E+00	6.3715292E-02
-3.3010444E+01	8.0567268E-01	1.7783999E+00	-2.4507415E-01	4.4769438E-03
2.2260265E+01	-1.4596019E+02	-1.5885771E+00	-3.3574277E+01	3.6583069E+00
2.2668410E+03	2.6714402E+02	2.2772116E-01	3.7815060E+00	1.5393650E-01
-3.5042015E+02	2.1631299E+03	4.7399806E+00	1.1060379E+02	2.9019615E+00
9.2378996E+02	2.3243402E+02	9.3304500E+02	2.3326127E+02	-8.2725569E-01
1.5889025E+00	1.9374835E-01	0.	0.	1.9374835E-01
3.2017062E+01	-4.9961063E+03	0.	-5.0000000E+03	3.8937021E+00
1.2226454E+01	4.2166327E+00	4.6439883E+00	1.0000000E+00	1.0000000E+00

.3000000

6.1887828E+01	7.1942630E+00	1.2000000E-01	8.6293250E-03	2.0000000E+00
3.0665284E+02	-4.6854461E+00	3.2908013E-02	1.5062857E-02	3.1605503E-02
-5.4864818E+01	-5.3665278E-02	3.1641187E-01	2.8114386E-02	5.5684871E-03
-9.8652366E+00	-1.4545494E+02	-1.2340190E+00	-6.8987157E+00	4.3073940E+00
-4.1184692E+02	3.9888609E+01	2.7377114E-01	-3.2413346E-01	2.7896143E-01
1.2347854E+02	3.8353057E+02	5.8153886E+00	4.6729958E+01	5.3612184E+00
9.2291556E+02	2.7859610E+02	9.3304500E+02	2.7991353E+02	-1.3174231E+00
1.6719512E+00	2.7616101E-01	0.	0.	2.7616101E-01
3.5954780E+01	-4.9943937E+03	0.	-5.0000000E+03	5.6062762E+00
1.2439189E+01	4.2442627E+00	5.2892331E+00	1.0000000E+00	1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.3500000	8.0993364E+01	1.0597466E+01	1.2000000E-01	4.0751693E-02	2.0000000E+00
	2.0464844E+02	8.9719353E+00	-2.5801017E-01	-1.6488411E+00	1.8380887E-02
	-4.7382734E+01	-6.9063947E-01	-1.0104128E+00	3.8133609E-01	1.7017328E-03
	3.4643107E+01	-1.4529636E+02	-6.9627620E-01	-1.3330133E+01	4.7952937E+00
	-2.9528354E+03	-3.1239949E+02	3.2761147E-01	-3.0481878E+00	3.9380969E-01
	6.8299249E+02	-1.2234108E+03	7.0334205E+00	-1.5595216E+01	7.9005055E+00
	9.2252195E+02	3.2473357E+02	9.3304500E+02	3.2656578E+02	-1.8322162E+00
	1.5839770E+00	3.5809112E-01	0.	0.	3.5809112E-01
	3.6578322E+01	-4.9925673E+03	0.	-5.0000000E+03	7.4326550E+00
	1.2761834E+01	4.2765669E+00	6.0200523E+00	1.0000000E+00	1.0000000E+00

.4000000	1.0655872E+02	1.5237661E+01	1.2000000E-01	4.7872897E-02	2.0000000E+00
	4.1677145E+00	1.4517597E+01	-5.1480148E-01	-2.2657894E+00	1.1866880E-02
	-2.8979652E-01	-9.0668394E-01	-1.5175955E+00	7.3058492E-01	1.2129331E-03
	3.6174295E+01	-1.4495632E+02	-9.6466952E-02	-2.4491278E+01	5.2853286E+00
	-3.6552481E+03	-6.2186442E+02	3.9362533E-01	-4.2335111E+00	4.7879731E-01
	1.1771075E+03	-1.8332089E+03	8.5848860E+00	-3.9530189E+01	9.9786511E+00
	9.2149982E+02	3.7083655E+02	9.3304500E+02	3.7321804E+02	-2.3814819E+00
	1.3960351E+00	4.3284108E-01	0.	0.	4.3284108E-01
	3.4982099E+01	-4.9907734E+03	0.	-5.0000000E+03	9.2266202E+00
	1.3121720E+01	4.3161752E+00	6.9509316E+00	1.0000000E+00	1.0000000E+00

.4500000	1.3077747E+02	2.1248241E+01	1.2000000E-01	4.9666165E-02	2.0000000E+00
	-1.5844746E+02	9.6834713E+00	-4.7337060E-01	-1.5481799E+00	7.7975361E-03
	7.4966108E+01	-6.3494706E-01	-1.0401487E+00	6.8405756E-01	2.0259851E-03
	2.9627901E+01	-1.4461126E+02	4.6385190E-01	-1.4647096E+01	5.9442930E+00
	-2.2486693E+03	-5.7045597E+02	4.6981581E-01	-2.8638524E+00	5.3055208E-01
	9.9280279E+02	-1.2534767E+03	1.0499156E+01	-1.9862914E+01	1.1434375E+01
	9.2044719E+02	4.1688307E+02	9.3304500E+02	4.1987029E+02	-2.9872204E+00
	1.2130895E+00	4.9778065E-01	0.	0.	4.9778065E-01
	3.3309425E+01	-4.9890702E+03	0.	-5.0000000E+03	1.0929761E+01
	1.3457911E+01	4.3618895E+00	8.0994935E+00	1.0000000E+00	1.0000000E+00

.5000000	1.3909359E+02	2.8223725E+01	1.2000000E-01	-4.8168293E-02	2.0000000E+00
	-2.1353033E+02	-1.7961888E+00	-3.0530927E-02	-2.1034299E-02	0.
	1.2635232E+02	-1.3609085E-01	-1.5148483E-02	4.2393464E-02	0.
	-1.3060443E+02	-1.4439060E+02	1.0711924E+00	-5.6031864E+00	6.6284411E+00
	2.6890332E+02	-3.6736490E+01	5.4961975E-01	-9.1511639E-01	5.6281954E-01
	-1.1107340E+02	-1.8227487E+01	1.2669512E+01	3.0690673E+01	1.2495238E+01
	9.2001402E+02	4.6289262E+02	9.3304500E+02	4.6652255E+02	-3.6299256E+00
	1.1184306E+00	5.5569735E-01	0.	0.	5.5569735E-01
	3.3504076E+01	-4.9874107E+03	0.	-5.0000000E+03	1.2589271E+01
	1.3638901E+01	4.3868444E+00	8.7648465E+00	1.0000000E+00	1.0000000E+00

.6000000	1.2173766E+02	4.1653545E+01	1.2000000E-01	4.9338204E-03	2.0000000E+00
	3.1322580E+00	-1.6787231E+01	9.5354182E-01	1.3911362E+00	0.
	-1.3070199E+00	5.4406267E-01	1.0018685E+00	-1.3240325E+00	0.
	-3.8719074E+01	-1.4401379E+02	2.5406833E+00	-2.4140777E+01	7.8634941E+00
	2.2215915E+03	1.1443598E+03	6.9297212E-01	1.9570865E+00	6.4242687E-01
	-2.1167995E+03	1.2023574E+03	1.6983856E+01	9.2638112E+01	1.5378027E+01
	9.1847171E+02	5.5483558E+02	9.3304500E+02	5.5982706E+02	-4.9914739E+00
	1.2114720E+00	6.6969949E-01	0.	0.	6.6969949E-01
	4.0664299E+01	-4.9837555E+03	0.	-5.0000000E+03	1.6244482E+01
	1.3638901E+01	4.3868444E+00	8.7648465E+00	1.0000000E+00	1.0000000E+00

.7000000

4.0727795E+01
1.2441459E+02
-1.5827821E+02
-8.3507348E+01
-1.5864381E+02
1.5740078E+02
9.1695953E+02
1.3601571E+00
4.7697954E+01
1.3638901E+01

5.0246788E+01
-3.2695294E+00
2.2230605E-01
-1.4366608E+02
3.5865132E+01
9.3308004E+00
6.4658911E+02
7.9943996E-01
-4.9792857E+03
4.3868444E+00

1.2000000E-01
2.9957077E-02
7.7937397E-03
3.9866379E+00
8.0935649E-01
2.0860308E+01
9.3304500E+02
0.
0.
8.7648465E+00

-4.2555211E-02
1.0821932E-02
-4.1596649E-02
-5.6844030E+00
5.9412358E-01
3.3162750E+01
6.5313156E+02
0.
-5.0000000E+03
1.0000000E+00

2.0000000E+00
0.
0.
9.5375424E+00
7.8781902E-01
2.0543205E+01
-6.5424501E+00
7.9943996E-01
2.0714304E+01
1.0000000E+00

.8000000

-1.5813697E+01
-4.0995794E+00
2.1344493E+00
-3.6038754E+01
-1.5183546E+03
2.0175359E+03
9.1601836E+02
1.3131468E+00
4.7561104E+01
1.3638901E+01

5.1598589E+01
8.8630268E+00
-2.2261391E-01
-1.4339050E+02
-1.0913732E+03
-8.2324680E+02
7.3824679E+02
9.3465127E-01
-4.9744771E+03
4.3868444E+00

1.2000000E-01
-9.1334354E-01
-6.8895509E-01
5.6598699E+00
9.2482359E-01
2.5128524E+01
9.3304500E+02
0.
0.
8.7648465E+00

-2.6412870E-02
-9.5664285E-01
1.2682156E+00
-1.3775310E+01
-1.2273654E+00
-1.9751911E+01
7.4643607E+02
0.
-5.0000000E+03
1.0000000E+00

2.0000000E+00
0.
0.
1.1153436E+01
9.4616809E-01
2.5985168E+01
-8.1892814E+00
9.3465127E-01
2.5522950E+01
1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.9000000	-5.4264678E+01	4.7970782E+01	1.2000000E-01	-4.7271993E-02	2.0000000E+00
	-1.1025387E+02	-2.5231301E+00	-3.9301187E-02	-2.8110257E-02	0.
	1.2953526E+02	-4.2528660E-02	-2.0244446E-02	5.4571335E-02	0.
	-5.4454761E+01	-1.4311985E+02	7.3892829E+00	-5.5022838E+00	1.2943887E+01
	1.1091997E+02	-4.6873167E+01	1.0577761E+00	-5.2161274E-01	1.0618991E+00
	-9.6056467E+01	-2.4144851E+01	3.0342922E+01	2.9936526E+01	3.0098156E+01
	9.1509230E+02	8.2979378E+02	9.3304500E+02	8.3974058E+02	-9.9467986E+00
	1.1991863E+00	1.0596744E+00	0.	0.	1.0596744E+00
	4.7451945E+01	-4.9697698E+03	0.	-5.0000000E+03	3.0230224E+01
	1.3638901E+01	4.3868444E+00	8.7648465E+00	1.0000000E+00	1.0000000E+00

START PLOTTING AT 0.0000000
 PLOTTING ENDED AT 0.0000000

INPUT DATA

3	ALPHAD	381	3.0000000E+00	-0.
3	VMACH	204	5.0000000E-01	-0.
3	STEP	2010	1.1000000E+01	-0.
6		-0	-0.	-0.

BURNOUT TIME= -0.0000 SEC.

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.0020000	-3.2073293E-02	-2.5698578E-05	1.2000000E-01	-2.3537737E-03	2.0000000E+00
	-1.8557438E+00	-1.7847485E-03	5.0351855E-02	-1.8489119E+00	1.6315556E-01
	4.8398780E-02	5.0274907E-05	2.2429544E-01	5.7720532E-02	9.6399894E-03
	-1.3367621E+00	-5.1356266E+01	-2.5599960E+00	-2.0092783E+00	3.0000040E+00
	-1.0542320E+03	2.1564173E+01	3.1924396E-06	8.4304127E-01	-1.6862528E-06
	3.2919761E+01	1.2960613E+03	2.3292630E-04	8.2841589E+01	5.9733766E-05
	5.4884598E+02	1.0976960E+00	5.4885000E+02	1.0977000E+00	-4.0158936E-06
	1.1580278E-03	1.1233423E-06	0.	0.	1.1233423E-06
	1.5866311E-01	-4.9999998E+03	0.	-5.0000000E+03	1.5997665E-04
	1.1643602E+01	4.0800019E+00	1.8001398E+00	1.0000000E+00	1.0000000E+00

.0500000	-1.0762983E+00	-2.5105408E-02	1.2000000E-01	-4.0748188E-03	2.0000000E+00
	-5.0882399E+01	-1.2923616E+00	6.1485124E-02	-1.7330752E+00	1.6347184E-01
	1.4767432E+00	3.6660078E-02	3.1064166E-01	6.6379419E-02	1.1521688E-02
	-2.0814224E+00	-2.4344532E+01	-2.5568281E+00	-2.1272559E+00	3.0017564E+00
	-9.4693217E+02	2.5815268E+01	2.5334741E-03	1.0306798E+00	-1.0231259E-03
	3.6668163E+01	1.3327771E+03	1.5835362E-01	8.4241836E+01	3.2953094E-02
	5.4874876E+02	2.7439982E+01	5.4885000E+02	2.7442502E+01	-2.5202649E-03
	3.7344829E-02	8.9615316E-04	0.	0.	8.9615316E-04
	4.0377621E+00	-4.9998994E+03	0.	-5.0000000E+03	1.0061878E-01
	1.1645503E+01	4.0815201E+00	1.8950122E+00	1.0000000E+00	1.0000000E+00

.1000000	-4.8056322E+00	-1.4988066E-01	1.2000000E-01	-2.6561198E-02	2.0000000E+00
	-9.0716405E+01	-4.9089776E+00	8.0992584E-02	-1.2553673E+00	1.5718757E-01
	3.0454235E+00	1.5636738E-01	5.9692865E-01	7.0757141E-02	1.3859340E-02
	-1.4076343E+01	-5.1421223E+01	-2.5402682E+00	-2.8620300E+00	2.9993163E+00
	-6.4053198E+02	3.4706148E+01	1.0963140E-02	1.3751349E+00	-4.1551194E-03
	3.7851339E+01	2.5579001E+02	6.1612973E-01	4.1961469E+01	1.4034366E-01
	5.4863412E+02	5.4874673E+01	5.4885000E+02	5.4885005E+01	-1.0332178E-02
	8.9280559E-02	4.0025224E-03	0.	0.	4.0025224E-03
	7.2914013E+00	-4.9996029E+03	0.	-5.0000000E+03	3.9706615E-01
	1.1655439E+01	4.0865779E+00	2.1696778E+00	1.0000000E+00	1.0000000E+00
.1500000	2.1806744E-01	-3.9755051E-01	1.2000000E-01	1.7281687E-02	2.0000000E+00
	-1.0822235E+02	-9.9939447E+00	9.0855537E-02	-4.6850893E-01	1.3668971E-01
	3.9354416E+00	3.6106142E-01	9.6904741E-01	4.9146536E-02	1.3263701E-02
	9.8225863E+00	-5.1414202E+01	-2.4960363E+00	-4.8046072E+00	2.9794877E+00
	-1.7612881E+02	3.8927208E+01	2.5918383E-02	1.6041419E+00	-8.5872412E-03
	2.4747926E+01	4.1518999E+02	1.2581131E+00	4.7799361E+01	2.9320799E-01
	5.4846189E+02	8.2302439E+01	5.4885000E+02	8.2327508E+01	-2.5068789E-02
	1.5350916E-01	1.0031205E-02	0.	0.	1.0031205E-02
	9.4280626E+00	-4.9991862E+03	0.	-5.0000000E+03	8.1384315E-01
	1.1681978E+01	4.0955510E+00	2.5548679E+00	1.0000000E+00	1.0000000E+00
.2000000	5.3409906E+00	-3.0400347E-01	1.2000000E-01	1.2479968E-02	2.0000000E+00
	-9.9269798E+01	-1.5293540E+01	1.0539161E-01	3.7694904E-01	1.1281758E-01
	4.4555859E+00	6.1581413E-01	1.3515377E+00	6.2578591E-03	1.1483599E-02
	5.9031811E+00	-5.1378351E+01	-2.4179723E+00	-7.9215670E+00	2.9448220E+00
	2.9910460E+02	4.5123728E+01	4.6101929E-02	1.7990157E+00	-1.1539518E-02
	-1.9403498E-01	5.7866483E+02	2.0204863E+00	5.3455832E+01	5.5395695E-01
	5.4816689E+02	1.0971878E+02	5.4885000E+02	1.0977001E+02	-5.1228624E-02
	2.2936937E-01	1.9562236E-02	0.	0.	1.9562236E-02
	1.1876152E+01	-4.9986547E+03	0.	-5.0000000E+03	1.3452521E+00
	1.1728817E+01	4.1076612E+00	3.0122918E+00	1.0000000E+00	1.0000000E+00

.2500000	9.4313397E+00	-3.1937586E-03	1.2000000E-01	1.3849486E-02	2.0000000E+00
	-6.6091914E+01	-1.9519109E+01	1.2368865E-01	1.1112222E+00	8.7565854E-02
	3.4302772E+00	8.4589252E-01	1.6400671E+00	-6.5460726E-02	7.9485990E-03
	5.7385853E+00	-5.1294758E+01	-2.3164641E+00	-1.1076542E+01	2.9234315E+00
	6.8915508E+02	5.2871495E+01	6.8776521E-02	1.9051460E+00	-8.5888730E-03
	-4.0206103E+01	7.0105702E+02	2.8613575E+00	5.7335625E+01	1.0036437E+00
	5.4771027E+02	1.3711636E+02	5.4885000E+02	1.3721251E+02	-9.6150352E-02
	3.1554818E-01	3.3155207E-02	0.	0.	3.3155207E-02
	1.4587689E+01	-4.9979940E+03	0.	-5.0000000E+03	2.0060090E+00
	1.1789722E+01	4.1212659E+00	3.5168145E+00	1.0000000E+00	1.0000000E+00

.3000000	1.3715628E+01	5.4026916E-01	1.2000000E-01	1.6494928E-02	2.0000000E+00
	-1.6083294E+01	-2.1625265E+01	1.4031092E-01	1.5812363E+00	6.2420531E-02
	3.5718491E-02	9.4224448E-01	1.7381921E+00	-1.4240638E-01	3.8895649E-03
	6.2488071E+00	-5.1172660E+01	-2.2121191E+00	-1.2578819E+01	2.9558356E+00
	9.1263395E+02	5.9834025E+01	9.0346566E-02	1.8591813E+00	5.3505025E-03
	-8.1000082E+01	7.4123263E+02	3.7499817E+00	5.8393861E+01	1.7009302E+00
	5.4712805E+02	1.6448764E+02	5.4885000E+02	1.6465502E+02	-1.6737135E-01
	4.0678426E-01	5.1211751E-02	0.	0.	5.1211751E-02
	1.7443554E+01	-4.9971935E+03	0.	-5.0000000E+03	2.8065348E+00
	1.1852329E+01	4.1342079E+00	4.0499890E+00	1.0000000E+00	1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.3500000	1.8294174E+01	1.3859450E+00	1.2000000E-01	1.8655258E-02	2.0000000E+00
	3.9214588E+01	-2.1040663E+01	1.4353487E-01	1.6537619E+00	4.4294656E-02
	-5.4687477E+00	8.1688457E-01	1.6165973E+00	-1.7576194E-01	1.7535446E-03
	6.4102130E+00	-5.1040329E+01	-2.1203846E+00	-1.1554747E+01	3.0683791E+00
	9.0482914E+02	6.1050559E+01	1.0781869E-01	1.5712504E+00	3.3835782E-02
	-9.5069096E+01	6.8759716E+02	4.6694965E+00	5.6592523E+01	2.6732876E+00
	5.4652745E+02	1.9182883E+02	5.4885000E+02	1.9209752E+02	-2.6868681E-01
	4.9277845E-01	7.3754625E-02	0.	0.	7.3754625E-02
	2.0296269E+01	-4.9962496E+03	0.	-5.0000000E+03	3.7503796E+00
	1.1907369E+01	4.1446912E+00	4.6016979E+00	1.0000000E+00	1.0000000E+00

.4000000	2.2813502E+01	2.5259850E+00	1.2000000E-01	2.0090588E-02	2.0000000E+00
	8.7386036E+01	-1.7811107E+01	1.2418194E-01	1.3613921E+00	2.8609463E-02
	-1.1646966E+01	4.8226561E-01	1.2555604E+00	-1.5034537E-01	1.6904024E-03
	6.1746249E+00	-5.0927415E+01	-2.0393732E+00	-8.2982241E+00	3.2539484E+00
	6.9680640E+02	5.2702210E+01	1.2067215E-01	1.0704259E+00	7.6116556E-02
	-7.5271468E+01	5.3285372E+02	5.6165732E+00	5.1464906E+01	3.9158814E+00
	5.4603323E+02	2.1914218E+02	5.4885000E+02	2.1954002E+02	-3.9783982E-01
	5.5911605E-01	1.0015735E-01	0.	0.	1.0015735E-01
	2.2987590E+01	-4.9951665E+03	0.	-5.0000000E+03	4.8335215E+00
	1.1955976E+01	4.1524033E+00	5.1699439E+00	1.0000000E+00	1.0000000E+00

.4500000	2.6923349E+01	3.8883952E+00	1.2000000E-01	1.9910353E-02	2.0000000E+00
	1.1759872E+02	-1.2561064E+01	7.9089082E-02	7.3124760E-01	1.9328533E-02
	-1.6750131E+01	4.2997335E-02	7.1254398E-01	-6.6322297E-02	3.2846084E-03
	5.1274651E+00	-5.0868724E+01	-1.9514169E+00	-4.5229013E+00	3.4755011E+00
	3.1438322E+02	3.3526339E+01	1.3107970E-01	5.0349540E-01	1.2700710E-01
	-2.3395773E+01	3.0205169E+02	6.6004478E+00	4.3327373E+01	5.3912592E+00
	5.4571939E+02	2.4643522E+02	5.4885000E+02	2.4698252E+02	-5.4730805E-01
	5.9778142E-01	1.2920459E-01	0.	0.	1.2920459E-01
	2.5352024E+01	-4.9939563E+03	0.	-5.0000000E+03	6.0436995E+00
	1.2008750E+01	4.1586478E+00	5.7602687E+00	1.0000000E+00	1.0000000E+00

.5000000	2.9358355E+01	5.3893609E+00	1.2000000E-01	-1.7478629E-02	2.0000000E+00
	1.2310593E+02	-6.3807331E+00	5.1434990E-03	-5.1806182E-02	1.3035952E-02
	-1.9686977E+01	-3.8565827E-01	8.8098263E-02	1.4907176E-02	1.6343244E-03
	-1.6553804E+01	-5.0847900E+01	-1.8358535E+00	-2.1381732E+00	3.6895784E+00
	-1.3280543E+02	2.1794677E+00	1.4234336E-01	-3.7851155E-02	1.7953564E-01
	2.4979594E+01	3.7330097E+01	7.6456319E+00	3.3404951E+01	7.0277228E+00
	5.4556344E+02	2.7371680E+02	5.4885000E+02	2.7442503E+02	-7.0823031E-01
	6.0842134E-01	1.5946787E-01	0.	0.	1.5946787E-01
	2.7262430E+01	-4.9926389E+03	0.	-5.0000000E+03	7.3611273E+00
	1.2078088E+01	4.1654060E+00	6.3873792E+00	1.0000000E+00	1.0000000E+00

.5500000	3.7217824E+01	7.0869795E+00	1.2000000E-01	3.2329594E-02	2.0000000E+00
	1.0316145E+02	-5.5045723E-01	-9.2831264E-02	-8.1118311E-01	9.6969700E-03
	-1.9517686E+01	-7.5632890E-01	-4.9103004E-01	1.3564520E-01	5.0379382E-04
	9.7977879E+00	-5.0845462E+01	-1.6847467E+00	-1.9150018E+00	3.8745117E+00
	-5.4503839E+02	-3.9333738E+01	1.5584412E-01	-4.9721888E-01	2.2923298E-01
	9.3047488E+01	-2.0805541E+02	8.7862797E+00	2.3894085E+01	8.7328640E+00
	5.4547088E+02	3.0099262E+02	5.4885000E+02	3.0186753E+02	-8.7491184E-01
	5.9454731E-01	1.8963466E-01	0.	0.	1.8963466E-01
	2.8680476E+01	-4.9912383E+03	0.	-5.0000000E+03	8.7616856E+00
	1.2168752E+01	4.1735065E+00	7.0717678E+00	1.0000000E+00	1.0000000E+00

.6000000

4.4579392E+01	9.1207597E+00	1.2000000E-01	3.7110198E-02	2.0000000E+00
6.3007386E+01	3.7509521E+00	-1.9715839E-01	-1.3586429E+00	6.8211476E-03
-1.4669625E+01	-1.0381174E+00	-9.1293131E-01	2.8312373E-01	7.1706238E-04
1.0820272E+01	-5.0834620E+01	-1.5074392E+00	-3.0079764E+00	4.0397391E+00
-8.2038584E+02	-8.3520600E+01	1.7233423E-01	-7.7287130E-01	2.7285214E-01
1.7225269E+02	-3.8673763E+02	1.0054694E+01	1.6891731E+01	1.0418427E+01
5.4534989E+02	3.2826338E+02	5.4885000E+02	3.2931003E+02	-1.0466572E+00
5.6237709E-01	2.1861585E-01	0.	0.	2.1861585E-01
2.9680458E+01	-4.9897778E+03	0.	-5.0000000E+03	1.0222168E+01
1.2275136E+01	4.1834005E+00	7.8328161E+00	1.0000000E+00	1.0000000E+00

.6500000

5.2716835E+01	1.1536775E+01	1.2000000E-01	4.2179051E-02	2.0000000E+00
1.2288804E+01	5.7120989E+00	-2.8615592E-01	-1.5793508E+00	0.
-4.3801377E+00	-1.1977354E+00	-1.1120213E+00	4.0334748E-01	0.
1.1816552E+01	-5.0790612E+01	-1.3208512E+00	-3.8835456E+00	4.2103316E+00
-9.0161897E+02	-1.2111695E+02	1.9246110E-01	-8.7828067E-01	3.0810415E-01
2.3130661E+02	-4.7066870E+02	1.1470638E+01	1.3490515E+01	1.2024024E+01
5.4517389E+02	3.5552665E+02	5.4885000E+02	3.5675254E+02	-1.2258804E+00
5.2027146E-01	2.4570682E-01	0.	0.	2.4570682E-01
3.0423508E+01	-4.9882746E+03	0.	-5.0000000E+03	1.1725434E+01
1.2387089E+01	4.1954767E+00	8.6823826E+00	1.0000000E+00	1.0000000E+00

TIME

P	PHI MSL	CX	CL	XNOSE1
Q	THETA MSL	CY	CM	AAN
R	PSI	CZ	CN	ASN
FMXBA	FXBA	XNPOS	VXED	XTPOS
FMYBA	FYBA	YNPOS	VYED	YTPOS
FMZBA	FZBA	ZNPOS	VZED	ZTPOS
RXED	RXE	RTXED	RTXE	DELX
RYED	RYE	RTYED	RTYE	DELY
RZED	RZE	RTZED	RTZE	DELZ
XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.7500000

7.0141513E+01	1.7688915E+01	1.2000000E-01	4.8966159E-02	2.0000000E+00
-7.3101475E+01	2.1551086E+00	-2.6956795E-01	-1.0522145E+00	0.
2.5687449E+01	-1.1364409E+00	-7.5778390E-01	3.7430633E-01	0.
1.1667332E+01	-5.0747479E+01	-9.4573514E-01	-2.4904845E+00	4.6092387E+00
-5.3187419E+02	-1.1399911E+02	2.4271755E-01	-3.8996963E-01	3.5291288E-01
1.8947109E+02	-3.2046352E+02	1.4742590E+01	1.8968127E+01	1.4951673E+01
5.4482969E+02	4.1002559E+02	5.4885000E+02	4.1163754E+02	-1.6119507E+00
4.4485747E-01	2.9345497E-01	0.	0.	2.9345497E-01
3.1935646E+01	-4.9851611E+03	0.	-5.0000000E+03	1.4838858E+01
1.2387089E+01	4.1954767E+00	8.6823826E+00	1.0000000E+00	1.0000000E+00

.8500000	7.5550727E+01	2.5370167E+01	1.2000000E-01	1.6367944E-02	2.0000000E+00
	-9.0885265E+01	-7.4784122E+00	7.3031551E-02	1.1990231E-01	0.
	4.4008955E+01	-9.3801506E-01	8.6351254E-02	-1.0140735E-01	0.
	-7.9438280E+00	-5.0746057E+01	-5.1391544E-01	-2.1940396E+00	4.9980517E+00
	1.4397946E+02	3.0883861E+01	2.9599837E-01	5.1524760E-01	3.8624533E-01
	-9.4159787E+01	3.6516547E+01	1.8483384E+01	3.3707622E+01	1.7759736E+01
	5.4463598E+02	4.6449858E+02	5.4885000E+02	4.6652255E+02	-2.0239687E+00
	4.5241112E-01	3.3755092E-01	0.	0.	3.3755092E-01
	3.4540776E+01	-4.9818498E+03	0.	-5.0000000E+03	1.8150193E+01
	1.2387089E+01	4.1954767E+00	8.6823826E+00	1.0000000E+00	1.0000000E+00

.9500000	7.6937310E+01	3.3041585E+01	1.2000000E-01	2.8185662E-02	2.0000000E+00
	-4.0974863E+01	-1.5363595E+01	5.0512412E-01	9.5058084E-01	0.
	2.2098390E+01	-1.0833852E+00	6.8458935E-01	-7.0138588E-01	0.
	-1.5988350E+00	-5.0730249E+01	-6.4421056E-03	-5.6144573E+00	5.3539064E+00
	5.7024080E+02	2.1354227E+02	3.3968278E-01	9.3534808E-01	4.4105175E-01
	-4.1391678E+02	2.8941157E+02	2.2473846E+01	4.5183107E+01	2.1000760E+01
	5.4425100E+02	5.1894592E+02	5.4885000E+02	5.2140755E+02	-2.4616320E+00
	5.3084559E-01	3.8635626E-01	0.	0.	3.8635626E-01
	3.8560707E+01	-4.9782044E+03	0.	-5.0000000E+03	2.1795591E+01
	1.2387089E+01	4.1954767E+00	8.6823826E+00	1.0000000E+00	1.0000000E+00

START PLOTTING AT
PLOTTING ENDED AT

0.0000000
0.0000000

APPENDIX VI

EXAMPLE 2

The second example is also a multiple run that simulates the trajectory of a MK-84 and a MK-81 bomb for the outboard pylon. The flow field data used in simulating the trajectories was collected in the presence of a MK-84 on the outboard pylon at $M=.85$ and angle of attack = $.3$. The first trajectory is that of the MK-84 at $M=.85$ with all the scale factors being 1. The second trajectory simulates the MK-81 and has the scale factor (DIASC) equal to 2 since the MK-81 diameter is $1/2$ that of the MK-84. This launch occurs at $M=.5$ and an angle of attack = 3.3 degrees. The ejector force for both runs was 10,000 pounds and acted until the bomb was 0.333 foot down from the aircraft. The trajectory was calculated until ground impact.

EXAMPLE II PROGRAM

INPUT DATA

1	OUPT 2,3	3	-0.	-0.
1	STAG2,3	4	-0.	-0.
2	G2-T	23	-0.	-0.
2	G3	24	-0.	-0.
2	G5	26	-0.	-0.
2	A1	2	-0.	-0.
2	A3-T	4	-0.	-0.
2	A2	3	-0.	-0.
2	D1	17	-0.	-0.
2	D2	18	-0.	-0.
3	TF	2001	1.0000000E+02	1.0000000E+00
3	T	2000	-0.	1.0000000E+00
3	PPP	2005	1.0000000E-02	1.0000000E+00
3	REPPLT	2006	1.0000000E+00	-0.
3	CPP	2015	5.0000000E-02	1.0000000E+00
3	DOC	2013	6.0000000E+00	1.0000000E+00
3	DER(1)	2664	2.0000000E-03	1.0000000E+00
3	PPP1	120	1.0000000E-01	-0.
3	CPP1	121	1.0000000E+00	-0.
3	DER1	122	1.0000000E-02	-0.
3	XTL	123	2.4000000E+01	-0.
3	XLL	124	1.2000000E+01	-0.
3	YLT	125	9.0000000E+00	-0.
3	YLL	126	3.0000000E+00	-0.
3	ZTL	127	9.0000000E+00	-0.
3	ZLL	128	1.0000000E+00	-0.
3	OPTN4	3502	-0.	-0.
3	AGRAV	1627	3.2174000E+01	-0.
3	CRAD	1751	5.7295770E+01	-0.
3	WP	1739	-0.	1.0000000E+00
3	WQ	1743	-0.	1.0000000E+00
3	WR	1747	-0.	1.0000000E+00
3	RXE	1615	0.	1.0000000E+00
3	RYE	1619	-0.	1.0000000E+00
3	RZE	1623	-1.0000000E+03	1.0000000E+00
3	RTXE	1651	0.	1.0000000E+00
3	RTYE	1655	-0.	1.0000000E+00
3	RTZE	1659	-1.0000000E+03	1.0000000E+00
3	EFORCX	1326	-0.	-0.
3	EFT	1332	1.0000000E+01	-0.
3	EJD	1333	3.3300000E-01	1.0000000E+00
3	DIASC	69	1.0000000E+00	1.0000000E+00
3	FMIYO	1420	3.6000000E+02	-0.
3	FMI XO	1419	1.8300000E+01	-0.
3	OPTNW	50	1.0000000E+00	1.0000000E+00
3	XTAIL	57	-6.8260000E+00	-0.

3	XNOSE	59	5.1660000E+00	-0.
3	XNOSE1	73	3.3330000E+00	-0.
3	RFLGTH	1307	1.5000000E+00	-0.
3	RFAREA	1306	1.7670000E+00	-0.
3	DWT	1415	2.0540000E+03	-0.
3	DWP	1416	1.0000000E+00	-0.
3	CISP	1414	1.0000000E+00	-0.
3	XINTER	1252	-1.0000000E+00	1.0000000E+00
3	PLOTN0	2008	1.2000000E+01	-0.
3	PLOTN2	1983	-0.	-0.
3	PLOTN4	1982	-0.	-0.
3	CMQ	1207	-1.3000000E+00	-0.
3	CNR	1208	-1.3000000E+00	-0.
3	CLP	1206	-3.3000000E-01	-0.
3	TNOSOS	58	1.0000000E+00	-0.
3	XPOS	54	2.9590000E+01	-0.
3	YPOS	55	1.1040000E+01	-0.
3	ZPOS	56	-1.8500000E+00	-0.
3	EFORCZ	1328	1.0000000E+04	-0.
3	EFORCY	1327	-0.	-0.
3	EMOMZ	1331	-0.	-0.
3	CNA A	1273	8.0000000E-02	1.0000000E+00
3	CMA A	1272	-1.5000000E-01	1.0000000E+00
3	CAA	1274	1.0000000E-01	1.0000000E+00
3	VMACH	204	8.5000000E-01	1.0000000E+00
3	ALPHAD	381	-0.	-0.
3	STEP	2010	2.0000000E+00	-0.
4	P	1739	-0.	-0.
4	PHI MSL	352	-0.	-0.
4	CX	1203	-0.	-0.
4	CL	1209	-0.	-0.
4	XNOSE1	73	-0.	-0.
4	Q	1743	-0.	-0.
4	THETA MSL	350	-0.	-0.
4	CY	1204	-0.	-0.
4	CM	1210	-0.	-0.
4	AAN	60	-0.	-0.
4	R	1747	-0.	-0.
4	PSI	351	-0.	-0.
4	CZ	1205	-0.	-0.
4	CN	1211	-0.	-0.
4	ASN	61	-0.	-0.
4	FMXBA	1303	-0.	-0.
4	FXBA	1300	-0.	-0.
4	XNPOS	90	-0.	-0.
4	VXED	1600	-0.	-0.
4	XTPOS	93	-0.	-0.
4	FMYBA	1304	-0.	-0.

4	FYBA	1301	-0.	-0.
4	YNPOS	91	-0.	-0.
4	VYED	1604	-0.	-0.
4	YTPOS	94	-0.	-0.
4	FMZBA	1305	-0.	-0.
4	FZBA	1302	-0.	-0.
4	ZNPOS	92	-0.	-0.
4	VZED	1608	-0.	-0.
4	ZTPOS	95	-0.	-0.
4	RXED	1612	-0.	-0.
4	RXE	1615	-0.	-0.
4	RTXED	1648	-0.	-0.
4	RTXE	1651	-0.	-0.
4	DELX	70	-0.	-0.
4	RYED	1616	-0.	-0.
4	RYE	1619	-0.	-0.
4	RTYED	1652	-0.	-0.
4	RTYE	1655	-0.	-0.
4	DELY	71	-0.	-0.
4	RZED	1620	-0.	-0.
4	RZE	1623	-0.	-0.
4	RTZED	1656	-0.	-0.
4	RTZE	1659	-0.	-0.
4	DELZ	72	-0.	-0.
4	XLUN	67	-0.	-0.
4	YLUN	45	-0.	-0.
4	ZLUN	44	-0.	-0.
4	DIASC	69	-0.	-0.
4	TNOSOS	58	-0.	-0.
7	PITCH	350	-0.	-0.
7	YAW	351	-0.	-0.
7	ROLL	352	-0.	-0.
7	X FT	70	-0.	-0.
7	Y FT	71	-0.	-0.
7	Z FT	72	-0.	-0.
7	XNPOS	90	-0.	-0.
7	YNPOS	91	-0.	-0.
7	ZNPOS	92	-0.	-0.
7	XTPOS	93	-0.	-0.
7	YTPOS	94	-0.	-0.
7	ZTPOS	95	-0.	-0.
6		-0	-0.	-0.

BURNOUT TIME= -0.0000 SEC.

TIME= .0020000 STEP SIZE= 2.0000000E-03

237

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS
.0020000	6.5593515E-01 -8.7759535E-01 4.9842943E-01 1.2529240E+02 -3.8358720E+03 2.2596736E+03 9.4636728E+02 8.3425806E-03 3.8230466E-01 1.4654403E+01	5.2526909E-04 -8.1119923E-04 4.7842150E-04 -1.8245079E+02 4.3351598E+02 1.0333607E+04 1.8927403E+00 9.0279773E-06 -9.9999962E+02 6.6240287E+00	1.0000000E-01 2.3737263E-01 1.8270567E-01 -5.1659943E+00 4.7832537E-05 4.4910011E-04 9.4637300E+02 0. 0. 1.1102695E+00	4.5917042E-02 -1.4014257E+00 8.2554670E-01 -2.8602703E+00 6.7891170E+00 1.9404036E+02 1.8927460E+00 0. -1.0000000E+03 1.0000000E+00	3.3330000E+00 9.2861488E-02 6.7654397E-02 6.8260057E+00 -5.2301027E-05 2.7931621E-04 -5.7144067E-06 9.0279773E-06 3.8460963E-04 1.0000000E+00
.0500000	1.6238170E+01 -2.6082335E+01 1.4225971E+01 6.6360363E+01 -3.6786653E+03 1.9121305E+03 9.4622884E+02 2.6266123E-01 9.5796755E+00 1.4656818E+01	4.3769054E-01 -6.5541730E-01 3.6017447E-01 -6.8311646E+01 5.4436334E+02 1.0352751E+04 4.7315065E+01 6.4018314E-03 -9.9976058E+02 6.6473231E+00	1.0000000E-01 2.5614395E-01 1.9359349E-01 -5.1619706E+00 3.8871849E-02 2.9850846E-01 9.4637300E+02 0. 0. 1.2891051E+00	2.8453518E-02 -1.3691484E+00 7.1235616E-01 -2.9714242E+00 7.2693624E+00 1.9437777E+02 4.7318654E+01 0. -1.0000000E+03 1.0000000E+00	3.3330000E+00 9.2173492E-02 6.3317395E-02 6.8290079E+00 -3.6507197E-02 1.6133269E-01 -3.5894179E-03 6.4018314E-03 2.3941831E-01 1.0000000E+00

.1000000	9.2886794E+00	1.2027597E+00	1.0000000E-01	-2.0913859E-02	3.3330000E+00
	-4.8240171E+01	-2.5611275E+00	2.9165066E-01	-1.0704549E+00	9.0032375E-02
	2.4123518E+01	1.3200784E+00	3.3202758E-01	3.8038122E-01	4.9085603E-02
	-6.3938761E+01	-1.8263694E+02	-5.1448851E+00	-3.4768769E+00	6.8319566E+00
	-2.7966372E+03	5.3266184E+02	1.4612201E-01	8.0644705E+00	-1.2986984E-01
	9.7409934E+02	6.0640501E+02	1.0638780E+00	4.1708318E+01	5.2801282E-01
	9.4607405E+02	9.4622724E+01	9.4637300E+02	9.4637309E+01	-1.4585067E-02
	5.7840160E-01	2.7229992E-02	0.	0.	2.7229992E-02
	1.2967385E+01	-9.9916696E+02	0.	-1.0000000E+03	8.3303750E-01
	1.4667069E+01	6.7116732E+00	1.7483268E+00	1.0000000E+00	1.0000000E+00

.1500000	2.8076346E+00	1.5776642E+00	1.0000000E-01	-2.4903792E-02	3.3330000E+00
	-6.1547241E+01	-5.3839492E+00	3.2980058E-01	-5.7489103E-01	8.2351442E-02
	2.6004390E+01	2.5429266E+00	5.2130198E-01	-2.6666196E-02	3.1351855E-02
	-7.0200650E+01	-1.8255005E+02	-5.1040434E+00	-4.6652050E+00	6.8232941E+00
	-1.4008064E+03	6.0205112E+02	2.9343842E-01	8.8182888E+00	-2.3627380E-01
	-1.4627768E+02	9.5163702E+02	2.0178573E+00	4.6999313E+01	8.9265500E-01
	9.4588247E+02	1.4192186E+02	9.4637300E+02	1.4195596E+02	-3.4101151E-02
	9.5046192E-01	6.5246241E-02	0.	0.	6.5246241E-02
	1.5079686E+01	-9.9846686E+02	0.	-1.0000000E+03	1.5331376E+00
	1.4691574E+01	6.8000631E+00	2.3207144E+00	1.0000000E+00	1.0000000E+00

.2000000	6.0729816E+00	1.5721438E+00	1.0000000E-01	2.9872421E-02	3.3330000E+00
	-6.2599219E+01	-8.5768945E+00	3.8549496E-01	6.1631395E-02	6.6697289E-02
	2.0589421E+01	3.6535622E+00	7.0406397E-01	-3.1739796E-01	2.1487105E-02
	7.7407402E+01	-1.8244057E+02	-5.0329720E+00	-6.5250869E+00	6.8008162E+00
	3.4496345E+02	7.0329922E+02	4.4912252E-01	1.0065018E+01	-3.0650342E-01
	-9.2658139E+02	1.2844984E+03	3.1160513E+00	5.1934636E+01	1.3276053E+00
	9.4561796E+02	1.8920975E+02	9.4637300E+02	1.8927462E+02	-6.4872775E-02
	1.3956708E+00	1.2360925E-01	0.	0.	1.2360925E-01
	1.7461078E+01	-9.9765439E+02	0.	-1.0000000E+03	2.3456141E+00
	1.4734217E+01	6.8934735E+00	2.9796308E+00	1.0000000E+00	1.0000000E+00

.2500000

2.1215018E+01	2.1108270E+00	1.0000000E-01	4.4734485E-02	3.3330000E+00
-5.0837325E+01	-1.1487513E+01	4.3302522E-01	6.4211870E-01	5.3523921E-02
1.1067058E+01	4.3783488E+00	8.8150172E-01	-4.8736703E-01	1.7274719E-02
1.0713841E+02	-1.8225787E+02	-4.9363835E+00	-8.7462362E+00	6.7810982E+00
1.8985749E+03	7.8922252E+02	5.9230733E-01	1.0790904E+01	-3.0484980E-01
-1.3635509E+03	1.6066062E+03	4.3126628E+00	5.6696788E+01	1.9244039E+00
9.4525053E+02	2.3648192E+02	9.4637300E+02	2.3659327E+02	-1.1135794E-01
1.8994277E+00	2.0582406E-01	0.	0.	2.0582406E-01
2.0108248E+01	-9.9671617E+02	0.	-1.0000000E+03	3.2838334E+00
1.4792170E+01	6.9793844E+00	3.6975977E+00	1.0000000E+00	1.0000000E+00

239

.3000000

3.8079037E+01	3.5554624E+00	1.0000000E-01	4.8776137E-02	3.3330000E+00
-2.8750401E+01	-1.3523736E+01	4.6797161E-01	1.0904270E+00	4.0577078E-02
-1.9768148E-01	4.5632961E+00	9.9087520E-01	-5.4285827E-01	1.7855957E-02
1.0598010E+02	-1.8201958E+02	-4.8279671E+00	-1.0449266E+01	6.7945716E+00
3.0580670E+03	8.5179997E+02	7.1354305E-01	1.0767748E+01	-2.1409094E-01
-1.4816064E+03	1.8035869E+03	5.5682184E+00	5.9727073E+01	2.7639114E+00
9.4478072E+02	2.8373305E+02	9.4637300E+02	2.8391193E+02	-1.7887412E-01
2.4240965E+00	3.1393074E-01	0.	0.	3.1393074E-01
2.2971043E+01	-9.9563984E+02	0.	-1.0000000E+03	4.3601604E+00
1.4857220E+01	7.0521258E+00	4.4509311E+00	1.0000000E+00	1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

240	.3500000	5.3984227E+01	5.9536715E+00	1.0000000E-01	4.9560421E-02	3.3330000E+00
		-5.7780997E-01	-1.4241631E+01	4.7282741E-01	1.3063735E+00	3.0049460E-02
		-1.2167731E+01	4.1918874E+00	9.9912264E-01	-5.4909154E-01	1.7939722E-02
		9.6609645E+01	-1.8177993E+02	-4.7222742E+00	-1.0800725E+01	6.8700787E+00
		3.5637116E+03	8.5950533E+02	8.1385138E-01	9.6762477E+00	-3.5787580E-02
		-1.4629988E+03	1.8162044E+03	6.8536885E+00	6.0253145E+01	3.9035161E+00
		9.4425469E+02	3.3095902E+02	9.4637300E+02	3.3123058E+02	-2.7156327E-01
		2.9226349E+00	4.4783832E-01	0.	0.	4.4783832E-01
		2.5939366E+01	-9.9441721E+02	0.	-1.0000000E+03	5.5827931E+00
		1.4920635E+01	7.1123108E+00	5.2222131E+00	1.0000000E+00	1.0000000E+00

	.4000000	6.8248488E+01	9.2203196E+00	1.0000000E-01	4.9215849E-02	3.3330000E+00
		2.7097720E+01	-1.3446653E+01	4.3232168E-01	1.2118350E+00	2.4969960E-02
		-2.4949092E+01	3.3468623E+00	8.9703186E-01	-5.3665188E-01	1.4487053E-02
		8.5381797E+01	-1.8160233E+02	-4.6254457E+00	-9.5364832E+00	7.0179224E+00
		3.2249334E+03	7.8510624E+02	8.9819460E-01	7.5064588E+00	2.1728699E-01
		-1.3917490E+03	1.6290307E+03	8.1548595E+00	5.7926094E+01	5.3662411E+00
		9.4374959E+02	3.7815887E+02	9.4637300E+02	3.7854924E+02	-3.9036836E-01
		3.3408848E+00	6.0485869E-01	0.	0.	6.0485869E-01
		2.8871797E+01	-9.9304644E+02	0.	-1.0000000E+03	6.9535594E+00
		1.4978733E+01	7.1629168E+00	6.0029157E+00	1.0000000E+00	1.0000000E+00

.4500000	8.0682333E+01	1.3208562E+01	1.0000000E-01	4.8290354E-02	3.3330000E+00
	4.8308566E+01	-1.1254859E+01	3.3904900E-01	8.9564157E-01	2.2188412E-02
	-3.8106072E+01	2.1491705E+00	7.0056502E-01	-4.5632161E-01	9.4648154E-03
	7.3912341E+01	-1.8146537E+02	-4.5307228E+00	-7.1776688E+00	7.2223821E+00
	2.3022150E+03	6.1525652E+02	9.6991125E-01	4.5663461E+00	5.2884421E-01
	-1.1350545E+03	1.2712829E+03	9.4752151E+00	5.2792807E+01	7.1346948E+00
	9.4333616E+02	4.2533553E+02	9.4637300E+02	4.2586789E+02	-5.3236443E-01
	3.6369913E+00	7.7990536E-01	0.	0.	7.7990536E-01
	3.1620663E+01	-9.9153305E+02	0.	-1.0000000E+03	8.4669498E+00
	1.5035566E+01	7.2059467E+00	6.7951291E+00	1.0000000E+00	1.0000000E+00

.5000000	9.1797873E+01	1.7758550E+01	1.0000000E-01	4.9833584E-02	3.3330000E+00
	5.9852367E+01	-8.0204442E+00	1.9231269E-01	4.8819189E-01	1.8527665E-02
	-4.9085581E+01	7.4820986E-01	4.4655014E-01	-2.2158744E-01	7.3943148E-03
	7.0122306E+01	-1.8135488E+02	-4.4230343E+00	-4.7480829E+00	7.4506511E+00
	1.1599547E+03	3.4876846E+02	1.0328249E+00	1.2717950E+00	8.7776093E-01
	-4.6494109E+02	8.0984048E+02	1.0831212E+01	4.5390402E+01	9.1580109E+00
	9.4304464E+02	4.7249455E+02	9.4637300E+02	4.7318655E+02	-6.9199741E-01
	3.7807671E+00	9.6602540E-01	0.	0.	9.6602540E-01
	3.4056198E+01	-9.8988958E+02	0.	-1.0000000E+03	1.0110419E+01
	1.5100179E+01	7.2436950E+00	7.6087271E+00	1.0000000E+00	1.0000000E+00

.5500000	9.5148889E+01	2.2709194E+01	1.0000000E-01	-3.8343341E-02	3.3330000E+00
	6.0987967E+01	-4.2436309E+00	3.0911554E-03	7.1185474E-02	1.4172481E-02
	-5.4307647E+01	-6.5315152E-01	1.8067033E-01	1.1180793E-01	6.2360659E-03
	-1.7206768E+02	-1.8126232E+02	-4.2879831E+00	-3.2056381E+00	7.6703623E+00
	2.2313355E+01	5.6031001E+00	1.0965359E+00	-1.8629892E+00	1.2328627E+00
	4.5647750E+02	3.2748724E+02	1.2248164E+01	3.6716817E+01	1.1360784E+01
	9.4285315E+02	5.1964168E+02	9.4637300E+02	5.2050520E+02	-8.6351897E-01
	3.7628364E+00	1.1552638E+00	0.	0.	1.1552638E+00
	3.6090469E+01	-9.8813411E+02	0.	-1.0000000E+03	1.1865892E+01
	1.5181210E+01	7.2819215E+00	8.4588981E+00	1.0000000E+00	1.0000000E+00

TIME= .5900000 STEP SIZE=

.6000000

7.8789043E+01	2.7162553E+01	1.0000000E-01	-4.1184108E-02	3.3330000E+00
5.4302577E+01	-4.8705654E-01	-2.1353361E-01	-9.8814344E-02	0.
-5.1429262E+01	-1.8569783E+00	-5.2700983E-02	4.0037552E-01	0.
-1.6792991E+02	-1.8099923E+02	-4.1198414E+00	-2.9512577E+00	7.8654272E+00
-4.2063846E+02	-3.8649419E+02	1.1725109E+00	-4.6110718E+00	1.5610941E+00
1.2313118E+03	-9.5388374E+01	1.3756133E+01	2.8056878E+01	1.3654194E+01
9.4270515E+02	5.6678060E+02	9.4637300E+02	5.6782386E+02	-1.0432582E+00
3.6003692E+00	1.3399138E+00	0.	0.	1.3399138E+00
3.7692448E+01	-9.8628778E+02	0.	-1.0000000E+03	1.3712221E+01
1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

1.6000000

-1.9816087E+01	2.4210702E+01	1.0000000E-01	2.3662054E-02	3.3330000E+00
-1.5944406E+01	2.4637372E+00	-3.3037497E-01	-7.9461242E-01	0.
2.4098990E+01	-1.44445120E+00	-4.2379329E-01	6.1945307E-01	0.
7.8086532E+01	-1.8028631E+02	1.7222315E+00	-3.5447796E+00	1.3699338E+01
-2.1041816E+03	-5.9562085E+02	4.0612123E+00	-3.5129885E+00	4.3632370E+00
1.6076456E+03	-7.6404131E+02	6.4813999E+01	1.7567569E+01	6.5329500E+01
9.3847526E+02	1.5073151E+03	9.4637300E+02	1.5141969E+03	-6.8818156E+00
2.3435560E+00	4.1913206E+00	0.	0.	4.1913206E+00
6.6419842E+01	-9.3496393E+02	0.	-1.0000000E+03	6.5036070E+01
1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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2.6000000	2.4606693E+00	3.0327874E+01	1.0000000E-01	-4.2203827E-02	3.3330000E+00
	-2.8502125E+01	-8.8203590E+00	2.2487604E-01	2.4942546E-01	0.
	2.4569330E+01	1.7527682E+00	1.3302691E-01	-4.2164258E-01	0.
	-1.1601265E+02	-1.8048724E+02	1.1517466E+01	-3.8917383E+00	2.3362103E+01
	7.5530106E+02	4.0587257E+02	7.0762731E+00	3.4711214E+00	6.7138139E+00
	-1.2105033E+03	2.4009660E+02	1.4852082E+02	3.8120629E+01	1.4668201E+02
	9.3499949E+02	2.4439501E+03	9.4637300E+02	2.4605700E+03	-1.6619984E+01
	2.5812359E+00	6.9201304E+00	0.	0.	6.9201304E+00
	9.7682031E+01	-8.5227132E+02	0.	-1.0000000E+03	1.4772868E+02
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

3.6000000	1.7156682E+00	2.6614068E+01	1.0000000E-01	3.3087425E-02	3.3330000E+00
	1.3846890E+01	-1.0836011E+01	1.2898760E-01	3.5003927E-01	0.
	-1.8451074E+01	5.9409150E-01	1.8668761E-01	-2.4185174E-01	0.
	8.8795157E+01	-1.8138479E+02	2.4730643E+01	-3.9998619E+00	3.6508183E+01
	9.1332800E+02	2.3396388E+02	9.8353278E+00	8.5891957E-01	9.7132038E+00
	-6.0599036E+02	3.3862293E+02	2.6347367E+02	3.7910016E+01	2.6121919E+02
	9.3144953E+02	3.3771389E+03	9.4637300E+02	3.4069431E+03	-2.9804256E+01
	3.1657700E+00	9.7827184E+00	0.	0.	9.7827184E+00
	1.3137286E+02	-7.3749753E+02	0.	-1.0000000E+03	2.6250247E+02
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

4.6000000	-1.2948997E+01	2.9586904E+01	1.0000000E-01	-1.9570632E-02	3.3330000E+00
	9.0632219E+00	-7.4666318E+00	-1.6476749E-01	-2.5231844E-01	0.
	-5.5815500E+00	-7.9928390E-01	-1.3456983E-01	3.0893905E-01	0.
	-4.4388934E+01	-1.8300248E+02	4.1053711E+01	-2.1338121E+00	5.2942869E+01
	-7.1835738E+02	-3.0152860E+02	1.2578378E+01	-2.1731316E+00	1.2744244E+01
	8.6389729E+02	-2.4626613E+02	4.0984662E+02	2.6163107E+01	4.0828827E+02
	9.2843983E+02	4.3071408E+03	9.4637300E+02	4.3533162E+03	-4.6175408E+01
	2.8421326E+00	1.2649831E+01	0.	0.	1.2649831E+01
	1.6277788E+02	-5.9082470E+02	0.	-1.0000000E+03	4.0917530E+02
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

5.6000000	2.1611782E+01	2.8279001E+01	1.0000000E-01	4.6115495E-02	3.3330000E+00
	-1.3987031E+01	-1.1113815E+01	-1.6137200E-02	-1.0011242E-01	0.
	1.3951818E+01	3.0306179E-01	-5.3393290E-02	3.0257251E-02	0.
	1.1242938E+02	-1.8525622E+02	6.0452213E+01	-2.5433301E+00	7.2219153E+01
	-2.3812191E+02	-2.9895168E+01	1.5449360E+01	3.0821617E-01	1.5387120E+01
	4.4106237E+01	-9.8914392E+01	5.8823053E+02	3.0058040E+01	5.8591897E+02
	9.2565584E+02	5.2341681E+03	9.4637300E+02	5.2996893E+03	-6.5521260E+01
	2.6090811E+00	1.5422548E+01	0.	0.	1.5422548E+01
	1.9333044E+02	-4.1276526E+02	0.	-1.0000000E+03	5.8723474E+02
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

6.6000000	-1.5373756E+01	2.8861416E+01	1.0000000E-01	1.4171967E-03	3.3330000E+00
	-2.3838574E+00	-1.5328980E+01	9.3501710E-02	1.7781839E-01	0.
	-1.1843001E+00	6.4229040E-01	9.4836472E-02	-1.7531571E-01	0.
	1.5307812E+01	-1.8816548E+02	8.2816087E+01	-3.8531063E+00	9.4380733E+01
	5.0879652E+02	1.7593794E+02	1.8264587E+01	1.0212307E+00	1.8134941E+01
	-4.9139391E+02	1.7844950E+02	7.9815879E+02	3.5038738E+01	7.9498858E+02
	9.2261897E+02	6.1582644E+03	9.4637300E+02	6.2460624E+03	-8.7797988E+01
	2.8621790E+00	1.8208737E+01	0.	0.	1.8208737E+01
	2.2535936E+02	-2.0320689E+02	0.	-1.0000000E+03	7.9679311E+02
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00

MISS DISTANCE= 6.94246672E+03

TIME FINAL= 7.45109003E+00

XM EARTH= 6.94243618E+03 YM EARTH= 2.05946911E+01 ZM EARTH= 0.

7.4600000	7.7301141E-01	2.8305247E+01	1.0000000E-01	3.2929430E-02	3.3330000E+00
	3.5354392E+00	-1.6197034E+01	3.8699510E-02	1.0478473E-01	0.
	-5.5114328E+00	2.7835293E-01	5.5885190E-02	-7.2561582E-02	0.
	9.3861532E+01	-1.9118988E+02	1.0434848E+02	-3.4413303E+00	1.1586436E+02
	2.9014546E+02	7.3989548E+01	2.0644562E+01	2.1009417E-01	2.0588615E+01
	-1.9194335E+02	1.0684683E+02	1.0036902E+03	3.3281443E+01	1.0003451E+03
	9.2004515E+02	6.9506339E+03	9.4637300E+02	7.0599433E+03	-1.0930937E+02
	2.8933681E+00	2.0620460E+01	0.	0.	2.0620460E+01
	2.5260314E+02	2.2492019E+00	0.	-1.0000000E+03	1.0022492E+03
	1.5260398E+01	7.3175216E+00	9.1775738E+00	1.0000000E+00	1.0000000E+00
START PLOTTING AT	0.0000000				
PLOTTING ENDED AT	0.0000000				

INPUT DATA

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N	ALPHAD	381	3.0000000E+00	-0.
N	VMACH	204	5.0000000E-01	-0.
3	DIASC	69	2.0000000E+00	1.0000000E+00
3	DWT	1415	2.6000000E+02	-0.
3	RFAREA	1306	4.4170000E-01	-0.
3	RFLGTH	1307	7.5000000E-01	-0.
3	FMIY0	1419	7.0000000E-01	-0.
3	FMIY0	1420	1.4600000E+01	-0.
3	XNOSE1	73	2.1000000E+00	-0.
3	STEP	2010	1.1000000E+01	-0.
6		-0	-0.	-0.

BURNOUT TIME= -0.0000 SEC.
 TIME= .0020000 STEP SIZE= 2.0000000E-03

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

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.0020000	2.0786934E-01	1.6744957E-04	1.0000000E-01	1.2595407E-02	2.1000000E+00
	-8.7096109E-01	-8.4476829E-04	8.9756698E-02	-1.1613504E+00	4.2156125E-02
	2.2254234E-01	2.1648418E-04	-1.3750026E-01	3.4989712E-01	2.4169675E-02
	1.4825236E+00	-1.5604137E+01	-5.1659961E+00	-1.9491642E+00	6.8260039E+00
	-1.3710816E+02	1.4167321E+01	2.0859498E-05	1.7495354E+00	-2.4450616E-05
	4.1312717E+01	9.9783415E+03	2.6067162E-03	1.2669554E+03	2.4299063E-03
	5.5668610E+02	1.1133761E+00	5.5669000E+02	1.1133800E+00	-3.8976657E-06
	2.1984114E-03	2.3355734E-06	0.	0.	2.3355734E-06
	2.5322603E+00	-9.9999747E+02	0.	-1.0000000E+03	2.5328506E-03
	1.4654402E+01	6.6240250E+00	1.1131281E+00	2.0000000E+00	1.0000000E+00
.0500000	2.1111077E+00	8.3356835E-02	1.0000000E-01	-1.5451526E-03	2.1000000E+00
	-2.9354653E+01	-7.1723779E-01	4.5990067E-02	-1.2797987E+00	2.8839360E-02
	4.5631309E+00	1.3633878E-01	-3.4728262E-01	1.1136919E-01	9.1385582E-03
	-2.3871114E-01	-1.5807113E+01	-5.1631565E+00	-1.8730568E+00	6.8278699E+00
	-1.4868277E+02	7.2697020E+00	1.3746825E-02	9.0502516E-01	-1.4786604E-02
	1.2730371E+01	-5.4895357E+01	1.2179583E+00	2.5358273E+01	1.0678444E+00
	5.5659373E+02	2.7832078E+01	5.5669000E+02	2.7834503E+01	-2.4240940E-03
	5.2551161E-02	1.4552178E-03	0.	0.	1.4552178E-03
	3.0673706E+01	-9.9884671E+02	0.	-1.0000000E+03	1.1532919E+00
	1.4656106E+01	6.6404962E+00	2.5715499E+00	2.0000000E+00	1.0000000E+00

.1000000	-1.1677982E+00	1.2353651E-01	1.0000000E-01	-1.4604479E-02	2.1000000E+00	
	-5.1305294E+01	-2.7802270E+00	5.2507236E-02	-7.9939905E-01	1.6422489E-02	
	5.7502587E+00	3.9729497E-01	-2.3708498E-01	3.8391476E-02	6.3434309E-03	
	-1.7000965E+00	-1.5801621E+01	-5.1502966E+00	-1.7354768E+00	6.8273000E+00	
	-8.9423183E+01	8.2969945E+00	4.0816654E-02	1.0247051E+00	-4.2238594E-02	
	3.9541191E+00	-3.7463270E+01	2.9693588E+00	2.7450897E+01	2.3876859E+00	
	5.5650457E+02	5.5659507E+01	5.5669000E+02	5.5669005E+01	-9.4986237E-03	
	9.1967936E-02	5.0376761E-03	0.	0.	5.0376761E-03	
	3.1964900E+01	-9.9728122E+02	0.	-1.0000000E+03	2.7187820E+00	
	1.4663822E+01	6.6729800E+00	4.6732305E+00	2.0000000E+00	1.0000000E+00	
	.1500000	-1.6580038E+01	-2.6539878E-01	1.0000000E-01	-4.4112924E-02	2.1000000E+00
		-6.2629236E+01	-5.6737675E+00	6.3835156E-02	-3.3688967E-01	1.3029697E-02
		4.7542040E+00	6.7377900E-01	-3.0094724E-02	-5.9743321E-02	2.7250500E-03
-4.7918062E+00		-1.5801423E+01	-5.1193951E+00	-1.9019526E+00	6.8130302E+00	
-3.3436386E+01		1.0086863E+01	7.1361212E-02	1.2231948E+00	-6.8966544E-02	
-7.5727754E+00		-4.7553947E+00	4.8632812E+00	3.1389358E+01	3.6777022E+00	
5.5641649E+02		8.3482567E+01	5.5669000E+02	8.3503508E+01	-2.0940894E-02	
1.4492907E-01		1.0909882E-02	0.	0.	1.0909882E-02	
3.3418900E+01		-9.9564745E+02	0.	-1.0000000E+03	4.3525492E+00	
1.4682363E+01		6.7096335E+00	6.9459374E+00	2.0000000E+00	1.0000000E+00	
.2000000		-9.9385633E+00	-1.0826778E+00	1.0000000E-01	4.9940801E-02	2.1000000E+00
		-6.2794967E+01	-8.8555991E+00	6.8806130E-02	1.5621938E-01	1.0609292E-02
		1.7533341E+00	8.7880115E-01	2.0532785E-01	-9.9819894E-02	1.3501390E-03
	6.1794779E+00	-1.5800310E+01	-5.0666297E+00	-2.5674211E+00	6.7810253E+00	
	2.5018117E+01	1.0871582E+01	9.7995394E-02	1.3817183E+00	-8.3737875E-02	
	-1.2010540E+01	3.2442437E+01	6.8596043E+00	3.5813948E+01	5.0134992E+00	
	5.5630815E+02	1.1130082E+02	5.5669000E+02	1.1133801E+02	-3.7188381E-02	
	2.0842372E-01	1.9707066E-02	0.	0.	1.9707066E-02	
	3.5089082E+01	-9.9393567E+02	0.	-1.0000000E+03	6.0643261E+00	
	1.4714022E+01	6.7415945E+00	9.3415252E+00	2.0000000E+00	1.0000000E+00	

.2500000	9.5847114E+00	-1.0576083E+00	1.0000000E-01	3.1855950E-02	2.1000000E+00
	-5.2047752E+01	-1.1767964E+01	7.0002679E-02	6.0210478E-01	8.4165965E-03
	-7.6865190E-01	9.6039021E-01	4.1777670E-01	-1.1305434E-01	8.3576556E-04
	3.5223120E+00	-1.5797651E+01	-4.9968456E+00	-3.5990041E+00	6.7414521E+00
	7.6730825E+01	1.1058779E+01	1.1664372E-01	1.4588757E+00	-8.0131718E-02
	-1.3315317E+01	6.5998905E+01	8.9186751E+00	3.9744662E+01	6.4729222E+00
	5.5615627E+02	1.3911265E+02	5.5669000E+02	1.3917251E+02	-5.9862746E-02
	2.7901006E-01	3.1875405E-02	0.	0.	3.1875405E-02
	3.6973858E+01	-9.9213492E+02	0.	-1.0000000E+03	7.8650763E+00
	1.4755893E+01	6.7639725E+00	1.1812410E+01	2.0000000E+00	1.0000000E+00
TIME=	.2540000	STEP SIZE=	1.0000000E-02		

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.3040000	2.1135408E+01	-1.8492974E-01	1.0000000E-01	2.2654320E-02	2.1000000E+00
	-2.8599797E+01	-1.3984017E+01	6.5703413E-02	1.0431264E+00	0.
	-3.1933975E+00	8.7905642E-01	5.5633406E-01	-1.2319390E-01	0.
	2.1264945E+00	-1.5785769E+01	-4.9179337E+00	-4.5403819E+00	6.7172915E+00
	1.2646099E+02	1.0371789E+01	1.2579724E-01	1.2490280E+00	-5.2729382E-02
	-1.4254613E+01	8.7821608E+01	1.1169124E+01	4.2243382E+01	8.2712429E+00
	5.5593651E+02	1.6913940E+02	5.5669000E+02	1.6923378E+02	-9.4372249E-02
	3.4999294E-01	4.8890281E-02	0.	0.	4.8890281E-02
	3.9187366E+01	-9.9007925E+02	0.	-1.0000000E+03	9.9207544E+00
	1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

TIME	P	PHI MSL	CX	CL	XNOSE1
	Q	THETA MSL	CY	CM	AAN
	R	PSI	CZ	CN	ASN
	FMXBA	FXBA	XNPOS	VXED	XTPOS
	FMYBA	FYBA	YNPOS	VYED	YTPOS
	FMZBA	FZBA	ZNPOS	VZED	ZTPOS
	RXED	RXE	RTXED	RTXE	DELX
	RYED	RYE	RTYED	RTYE	DELY
	RZED	RZE	RTZED	RTZE	DELZ
	XLUN	YLUN	ZLUN	DIASC	TNOSOS

219 1.3040000	2.1785685E+01	5.9064598E+01	1.0000000E-01	2.4179205E-02	2.1000000E+00
	2.4150817E+01	-7.9750741E+00	-1.0693661E-01	2.5436261E-02	0.
	-3.6868219E+01	-3.4003130E+00	1.3566006E-02	2.0050615E-01	0.
	2.2995929E+00	-1.5848107E+01	-2.8398480E+00	-1.7860410E+00	9.0152651E+00
	5.1507482E-01	-1.6947429E+01	1.5444858E-01	-1.2024884E+00	8.5883705E-01
	2.7661449E+01	2.1499552E+00	6.6514553E+01	3.0255896E+01	6.4850755E+01
	5.5316604E+02	7.2365665E+02	5.5669000E+02	7.2592383E+02	-2.2671829E+00
	3.3434889E-01	4.5789028E-01	0.	0.	4.5789028E-01
	7.2615526E+01	-9.3420219E+02	0.	-1.0000000E+03	6.5797810E+01
	1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

2.3040000	3.0161247E+01	4.3322908E+01	1.0000000E-01	2.6177788E-02	2.1000000E+00
	-1.7407736E+01	-9.3118179E+00	-1.6725857E-01	-4.1455774E-01	0.
	1.7893194E+01	-1.6683965E+00	-2.2109746E-01	3.1360983E-01	0.
	2.3495128E+00	-1.6048409E+01	1.7158061E+00	-1.0563103E+00	1.3544764E+01
	-4.8075511E+01	-2.6842341E+01	6.7824231E-01	6.2713593E-01	1.0227873E+00
	3.5874302E+01	-3.5482625E+01	1.5412313E+02	2.6451396E+01	1.5218273E+02
	5.5111912E+02	1.2758023E+03	5.5669000E+02	1.2826139E+03	-6.8115697E+00
	4.1883712E-01	8.2666786E-01	0.	0.	8.2666786E-01
	1.0284271E+02	-8.4671277E+02	0.	-1.0000000E+03	1.5328723E+02
	1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

3.3040000

-2.5971374E+01	4.6203784E+01	1.0000000E-01	-2.2808408E-03	2.1000000E+00
-9.8724288E+00	-1.8965623E+01	1.7716070E-01	3.2468244E-01	0.
5.8454639E+00	-2.1972940E+00	1.7316397E-01	-3.3217632E-01	0.
4.1823321E-01	-1.6376858E+01	8.6212686E+00	-3.5473934E+00	1.9953933E+01
4.0925391E+01	2.9013356E+01	1.1378046E+00	8.7867825E-02	1.5726256E+00
-4.1419253E+01	2.8358817E+01	2.7392206E+02	3.6263171E+01	2.7002465E+02
5.4896537E+02	1.8258007E+03	5.5669000E+02	1.8393039E+03	-1.3503235E+01
5.9679866E-01	1.3251199E+00	0.	0.	1.3251199E+00
1.3469581E+02	-7.2775689E+02	0.	-1.0000000E+03	2.7224311E+02
1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

4.3040000

1.0428571E+01	5.2906360E+01	1.0000000E-01	-4.1927267E-02	2.1000000E+00
1.1176274E+01	-1.7918157E+01	-6.0308699E-02	-6.7283622E-02	0.
-1.0392022E+01	-2.5441237E+00	-3.5884598E-02	1.1307881E-01	0.
-5.5769830E+00	-1.6829174E+01	1.7433088E+01	-1.5402988E+00	2.8832196E+01
-9.6955703E+00	-1.0149456E+01	1.6880957E+00	-9.3120149E-02	2.1945870E+00
1.5391361E+01	-6.0390815E+00	4.2456518E+02	3.0151173E+01	4.2087574E+02
5.4672413E+02	2.3736503E+03	5.5669000E+02	2.3959940E+03	-2.2343677E+01
5.6354841E-01	1.9062850E+00	0.	0.	1.9062850E+00
1.6677868E+02	-5.7702418E+02	0.	-1.0000000E+03	4.2297582E+02
1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

5.3040000

1.7504527E+01	5.4915584E+01	1.0000000E-01	1.3872574E-02	2.1000000E+00
-1.0797343E+01	-2.1025969E+01	-3.4702304E-02	-7.4922197E-02	0.
1.1347567E+01	-2.3628496E+00	-3.9958505E-02	6.5066820E-02	0.
1.3233212E+00	-1.7408658E+01	2.8379206E+01	-1.6011070E+00	3.9563243E+01
-8.5965201E+00	-6.0412053E+00	2.3605311E+00	3.4101859E-01	2.8220169E+00
7.2493315E+00	-6.9562393E+00	6.0693117E+02	3.0368192E+01	6.0262854E+02
5.4492381E+02	2.9194869E+03	5.5669000E+02	2.9526841E+03	-3.3197146E+01
7.4669604E-01	2.5593333E+00	0.	0.	2.5593333E+00
1.9753856E+02	-3.9492235E+02	0.	-1.0000000E+03	6.0507765E+02
1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

6.3040000	-2.1253299E+00	5.5407000E+01	1.0000000E-01	-2.3701851E-03	2.1000000E+00
	2.2848330E+00	-2.5610868E+01	5.7474747E-02	1.0523978E-01	0.
	-1.2508873E+00	-2.7827688E+00	5.6127883E-02	-1.0776515E-01	0.
	-2.6131968E-01	-1.8111781E+01	4.1410807E+01	-2.7996478E+00	5.2211861E+01
	1.4038776E+01	1.0409700E+01	3.0897243E+00	-1.6851493E-01	3.6147279E+00
	-1.4498037E+01	1.0165759E+01	8.2071435E+02	3.2805529E+01	8.1553072E+02
	5.4274295E+02	3.4633103E+03	5.5669000E+02	3.5093741E+03	-4.6063763E+01
	7.7343307E-01	3.3158892E+00	0.	0.	3.3158892E+00
	2.2916013E+02	-1.8151869E+02	0.	-1.0000000E+03	8.1848131E+02
	1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

MISS DISTANCE= 3.87184325E+03

TIME FINAL= 7.05773162E+00

XM EARTH= 3.87184124E+03 YM EARTH= 3.93932850E+00 ZM EARTH= 0.

7.0640000	9.3486511E+00	5.4119488E+01	1.0000000E-01	2.9273585E-03	2.1000000E+00
	3.7971207E+00	-2.7223304E+01	2.2108618E-02	4.2685987E-02	0.
	-3.0986879E+00	-2.6692897E+00	2.2765859E-02	-4.1453659E-02	0.
	1.3916510E-01	-1.8732027E+01	5.2636291E+01	-2.3960274E+00	6.3288388E+01
	5.5615878E+00	4.1413923E+00	3.7306685E+00	-1.5650043E-02	4.2272866E+00
	-5.4685397E+00	4.2645069E+00	1.0039474E+03	3.1757898E+01	9.9846156E+02
	5.4115314E+02	3.8752335E+03	5.5669000E+02	3.9324586E+03	-5.7225078E+01
	8.4167886E-01	3.9446052E+00	0.	0.	3.9446052E+00
	2.5288557E+02	1.5841874E+00	0.	-1.0000000E+03	1.0015842E+03
	1.4759480E+01	6.7652809E+00	1.2012049E+01	2.0000000E+00	1.0000000E+00

START PLOTTING AT 0.0000000
 PLOTTING ENDED AT 0.0000000

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UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) Product Assurance Division Air Force Armament Laboratory Eglin Air Force Base, Florida 32542		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE VALIDATION AND EXPANSION OF THE FLOW ANGULARITY TECHNIQUE FOR PREDICTING STORE SEPARATION TRAJECTORIES			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Final Report (April - August 1972)			
5. AUTHOR(S) (First name, middle initial, last name) Capt. Stephen C. Korn			
<i>This document has been approved for public release distribution is unlimited Per TAB 748 Dtd 12 April 74</i>			
6. REPORT DATE September 1972	7a. TOTAL NO. OF PAGES 261	7b. NO. OF REFS 4	
8a. CONTRACT OR GRANT NO.		9a. ORIGINATOR'S REPORT NUMBER(S) AFATL-TR-72-184	
b. PROJECT NO. 2567			
c.		9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)	
d.			
10. DISTRIBUTION STATEMENT Distribution limited to U.S. Government agencies only; this report documents test and evaluation; distribution limitation applied September 1972. Other requests for this document must be referred to the Air Force Armament Laboratory (DLGC), Eglin Air Force Base, Florida 32542.			
11. SUPPLEMENTARY NOTES Available in DDC		12. SPONSORING MILITARY ACTIVITY Air Force Armament Laboratory Air Force Systems Command Eglin Air Force Base, Florida 32542	
13. ABSTRACT This report documents the external flow fields caused by various weapon configurations on the wing of an F-4 aircraft, verifies assumptions made in the flow angularity technique, and presents the documentation for the "Flow Angularity Computer Program" with example trajectories. The flow angularity program is presently capable of calculating the trajectories of stores off the inboard and outboard wing stations in either single, triple ejector rack, or multiple ejector rack configurations. The assumptions made in the flow angularity technique have been analyzed and generally validated as good approximations.			

14.	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	External Flow Fields						
	Flow Angularity (Computer Programs) --						
	2 Stores Trajectory						
	F-4 Aircraft						
	Wind Tunnel Test						
	3 Stores -- Separation						
	4 " -- Flow Angularity						