

UNCLASSIFIED

AD NUMBER
AD905000
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution authorized to U.S. Gov't. agencies only; Test and evaluation; 11 Apr 1972. Other requests shall be referred to Air Force Avionics Lab., Attn: RSA, Wright-Patterson AFB, 45433.
AUTHORITY
WRDC/IST Notice, 25 Sep 1990

THIS PAGE IS UNCLASSIFIED

7000
506
AD-905000
AFAL-TR-72-226
Volume II

191101

**TARGET SIGNATURE ANALYSIS CENTER: DATA COMPILATION
ELEVENTH SUPPLEMENT**

Volume II

Bidirectional Reflectance: Graphic Data

Prepared by

Target Signature Analysis Center
Infrared and Optics Division
Willow Run Laboratories
The University of Michigan
Ann Arbor, Michigan

October 1972

Distribution limited to U. S. Government agencies only;
Test and Evaluation: 11 April 1972. Other requests for
this document must be submitted to AFAL RSA, Wright-
Patterson Air Force Base, Ohio 45433

Air Force Avionics Laboratory
Air Force Systems Command
Wright-Patterson Air Force Base, Ohio

TARGET SIGNATURE ANALYSIS CENTER: DATA COMPILATION
ELEVENTH SUPPLEMENT
Volume II
Bidirectional Reflectance: Graphic Data

Prepared by
Target Signature Analysis Center
Infrared and Optics Division
Willow Run Laboratories
The University of Michigan
Ann Arbor, Michigan

Distribution limited to U. S. Government agencies only;
Test and Evaluation: 11 Apr 1972. Other requests for
this document must be submitted to AFAL/BSA, Wright-
Patterson Air Force Base, Ohio 45433

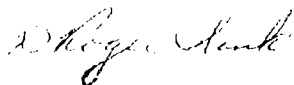
FOREWORD

The work reported herein, covering the period from 1 November 1969 to 30 July 1972, was carried out by the Infrared and Optics Division of the Willow Run Laboratories, a unit of The University of Michigan's Institute of Science and Technology, Ann Arbor, Michigan. The work was performed under Contract F33615-70-C-1123, Project 6239, Task 10, for the Air Force Avionics Laboratory (AFAL), Air Force Systems Command, Wright-Patterson Air Force Base, Ohio. Volume I contains a definition of the parameters pertinent to the bidirectional reflectance, a discussion of the data, some equations for application of the data, and an index and cross reference of the data contained in Volume II. Bidirectional reflectance data in graphical form are presented in Volume II. The data were reduced and this supplement was prepared by (Mrs.) Sharon Ladd, Dwayne Carner, Daniel Rice, Dennis Ladd, and John Ulrich under the direction of J. Robert Maxwell. The data reported in this supplement were obtained almost entirely from the laboratory measurements phase of the Target Signature Measurement Program conducted at The University of Michigan, sponsored by the Avionics Laboratory under U. S. Air Force Contracts AF33(615)-3924, F33(615)-68-C-1281 and F33(615)-70-C-1698, under the direction of Max Bair.

The Target Signature program is part of a comprehensive multispectral program at The University of Michigan devoted to the improvement of remote sensing capabilities; this comprehensive program is under the supervision of R. R. Legault, Associate Director of the Willow Run Laboratories. The Principal Investigator for this contract is J. R. Maxwell. The Willow Run Laboratories' number for this report is 32210-41-B (I and II).

This report was submitted by the authors on 10 August 1972.

This technical report has been reviewed and is approved.



D. ROGER SINK, ACTING CHIEF
Reconnaissance Applications Branch
Reconnaissance Division
Air Force Avionics Laboratory

ABSTRACT

This report is the eleventh supplement to the Target Signature Analysis Center: Data Compilation and contains 2200 curves of bidirectional reflectance versus angle. The significance of this report to the Air Force is that these data provide the Air Force with essential optical properties-of-materials data to analyze the angular dependence of the reflected radiance from various targets. Volume I contains a definition of the parameters pertinent to the bidirectional reflectance, a discussion of the data, some equations for application of the data, and an index and cross reference of the data contained in Volume II. Bidirectional reflectance data are presented graphically in Volume II.

This supplement to the Target Signature Analysis Center: Data Compilation augments an ordered, indexed compilation of reflectance, radar cross sections, and apparent temperatures of target and background materials. The Data Compilation includes spectral reflectances and transmittances in the optical region from 0.3 to 15 μm , normalized radar cross sections, and apparent temperatures at mm wavelengths. When available, the experimental parameters associated with each curve are listed to provide the user with a description of the important experimental conditions.

CONTENTS

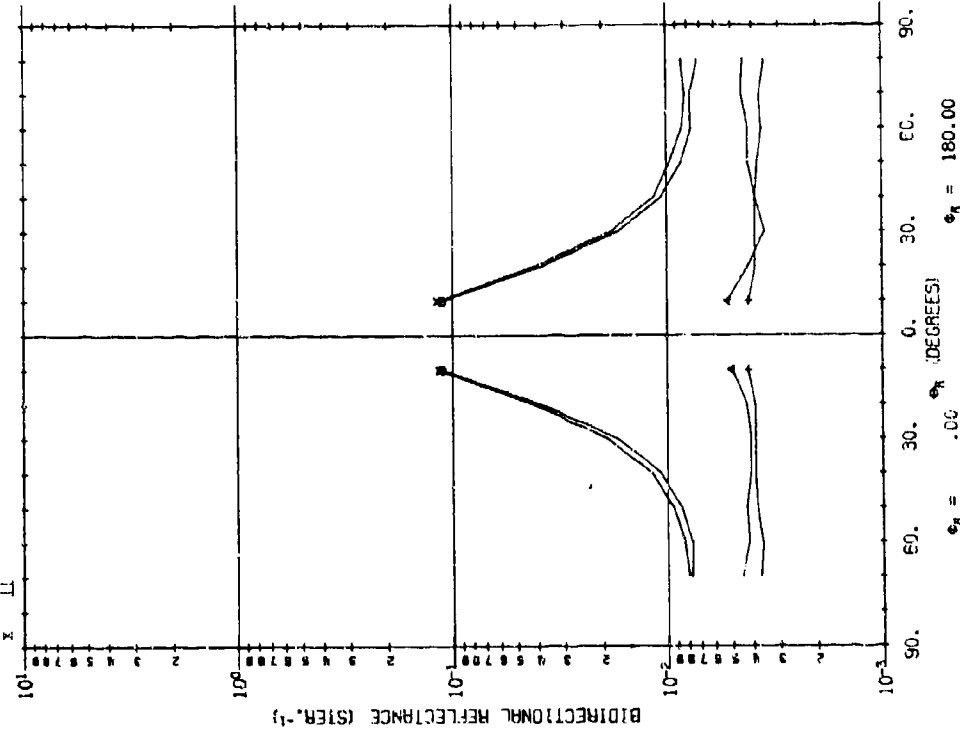
Paint	1
Cloth and Canvas	193
Wood	297
Soil	329
Vegetation	341
Asphalt and Concrete	351
Reflectance Standards Material	367
Metal	423
Miscellaneous	439
Distribution List	447

PAINT

R01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (WET BECKED) ON ANODIZED
ALUMINUM

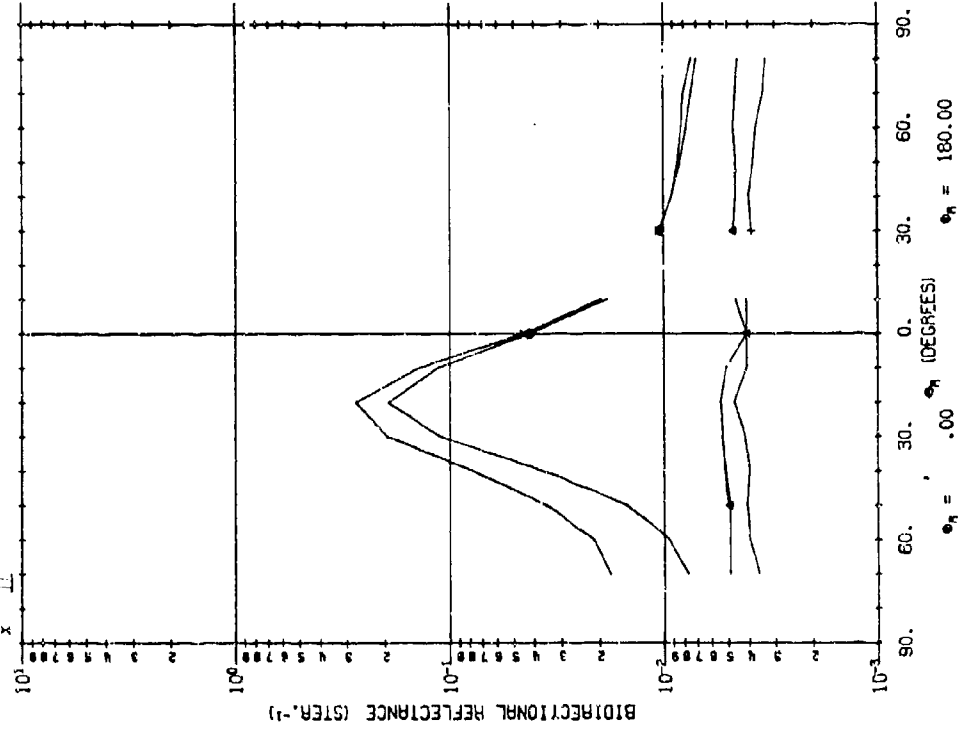
0 | | $\epsilon_1 = 0.0$
+ | | $\epsilon_2 = 180.0$
x | | $\lambda = 0.63$



R01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (WET BECKED) ON ANODIZED
ALUMINUM

0 | | $\epsilon_1 = 20.0$
+ | | $\epsilon_2 = 180.0$
x | | $\lambda = 0.63$

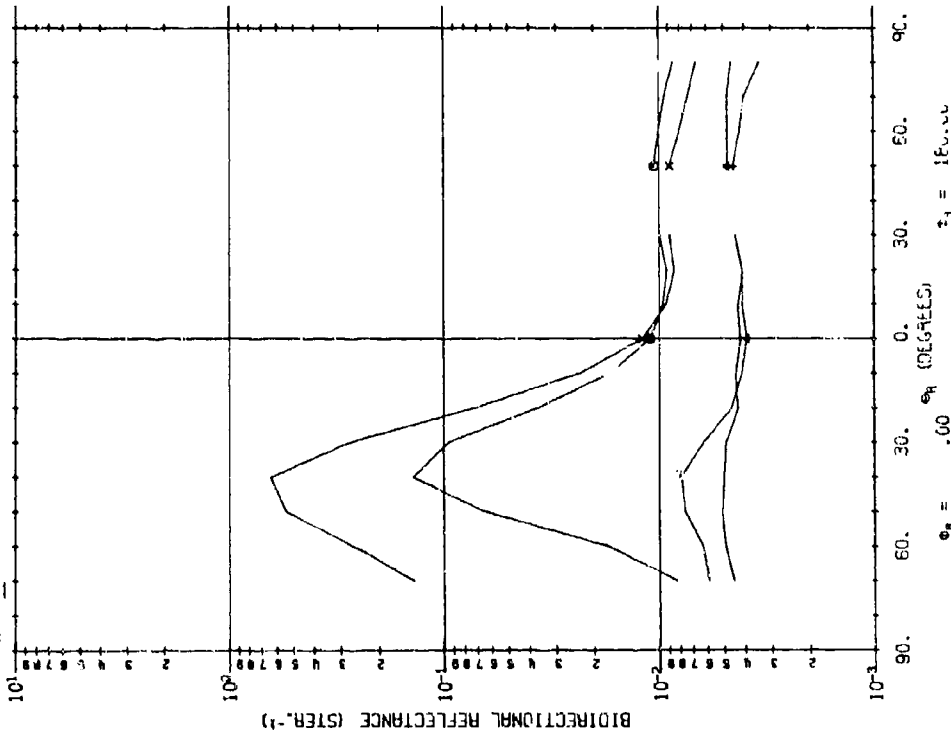


PAINT

A01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (NET DECKED) ON ANODIZED
ALUMINUM

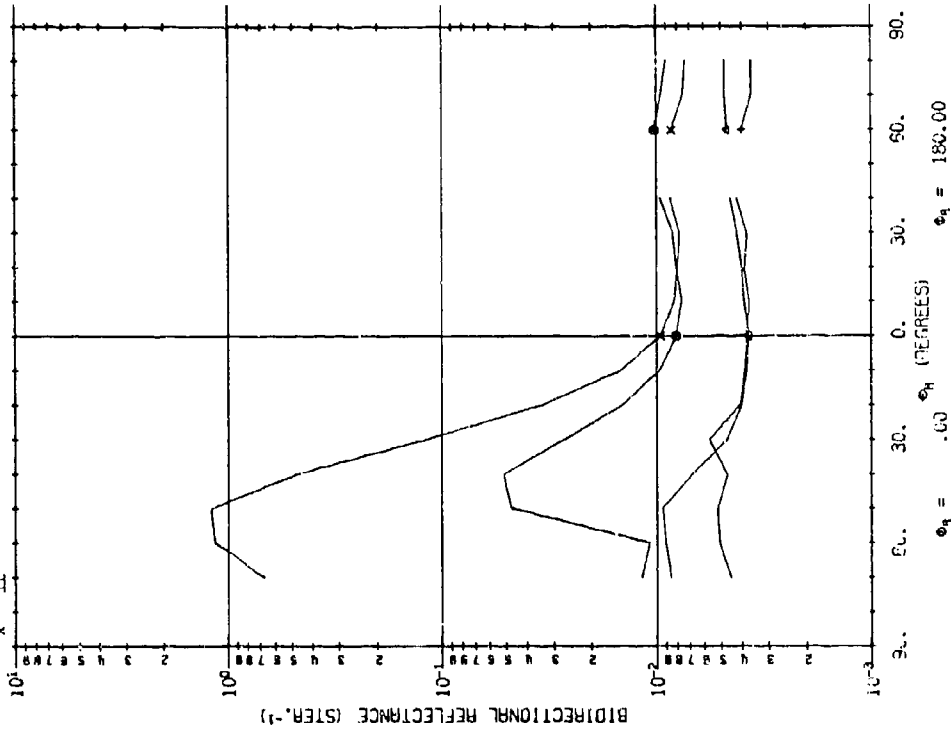
$\theta_1 = 40.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (NET DECKED) ON ANODIZED
ALUMINUM

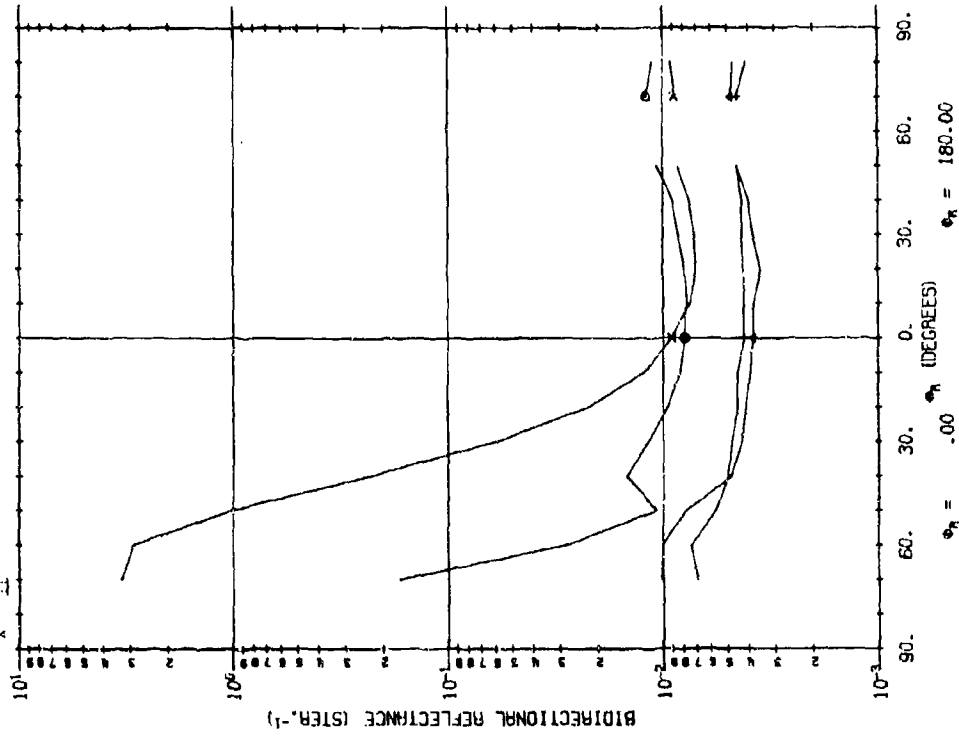
$\theta_1 = 50.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (WET DECKED) ON ANODIZED
ALUMINUM

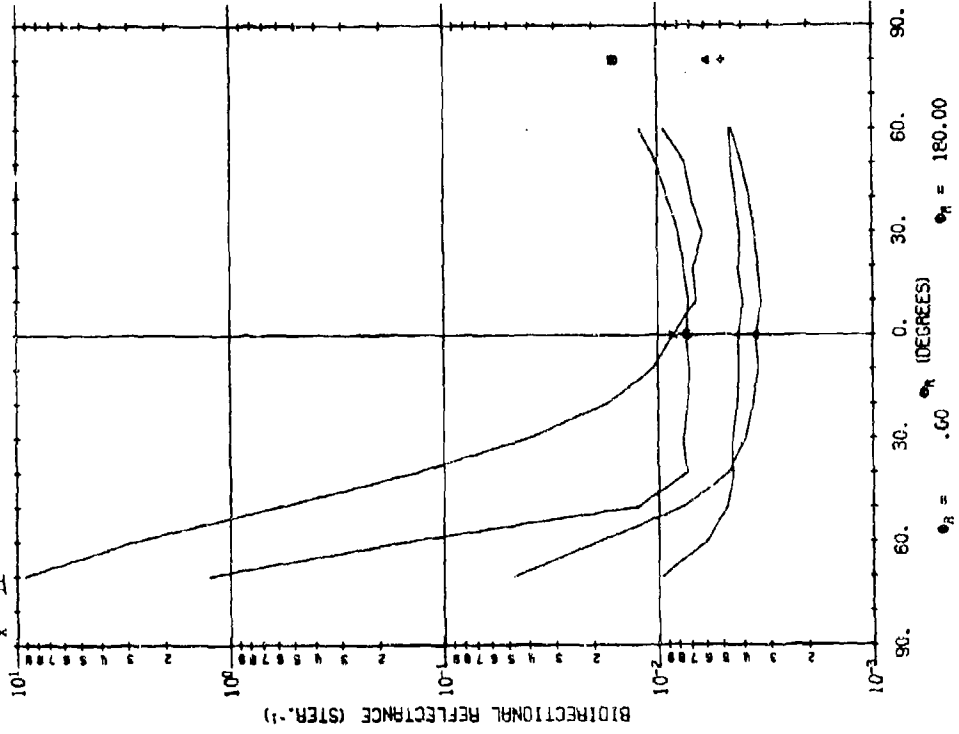
0 || $\theta_i = 60.0$
+ || $\theta_r = 180.0$
- || $\lambda = 0.63$
x ||



A01027 003

ONE COAT OLIVE DRAB PAINT ON TWO COATS
ZINC CHROMATE (WET DECKED) ON ANODIZED
ALUMINUM

0 || $\theta_i = 70.0$
+ || $\theta_r = 180.0$
- || $\lambda = 0.63$
x ||

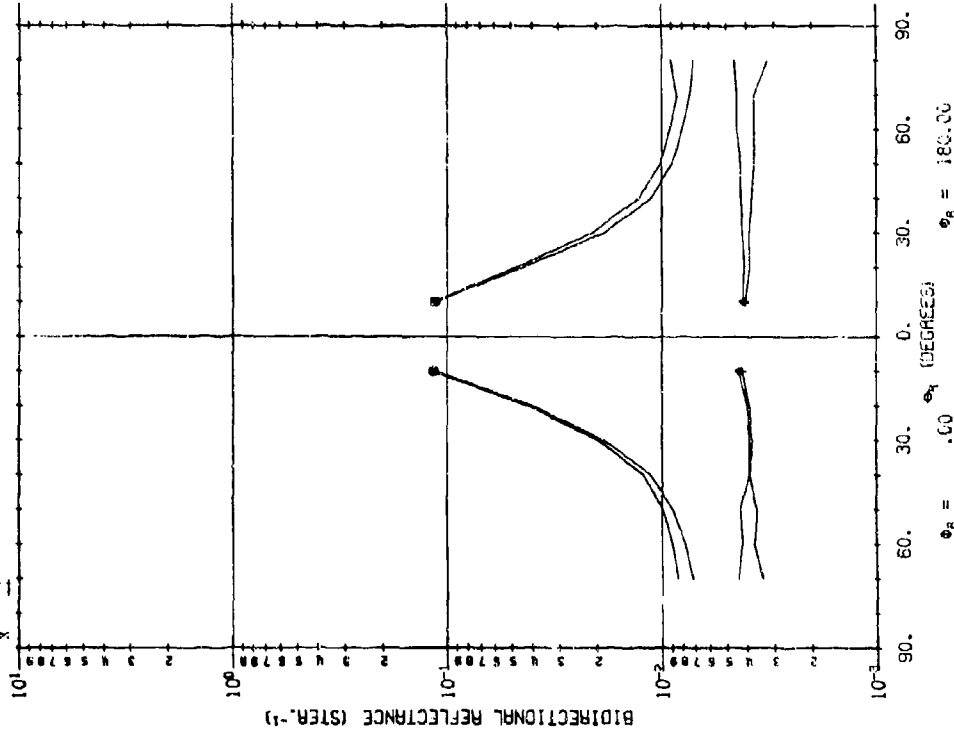


PAINT

AO1044 003

TWO COATS DEEP ROSS GREEN PAINT ON TPO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

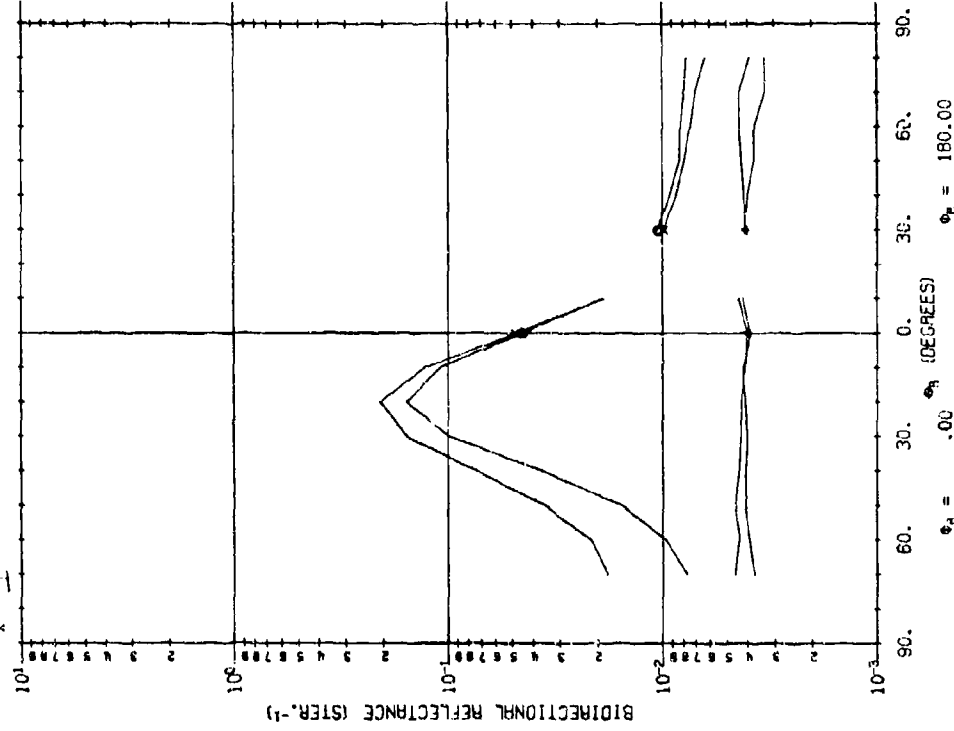
$\epsilon_1 = 0.0$
 $\epsilon_2 = 180.0$
 $\epsilon_3 = 0.63$



AO1044 003

TWO COATS DEEP ROSS GREEN PAINT ON TPO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

$\epsilon_1 = 20.0$
 $\epsilon_2 = 180.0$
 $\epsilon_3 = 0.63$

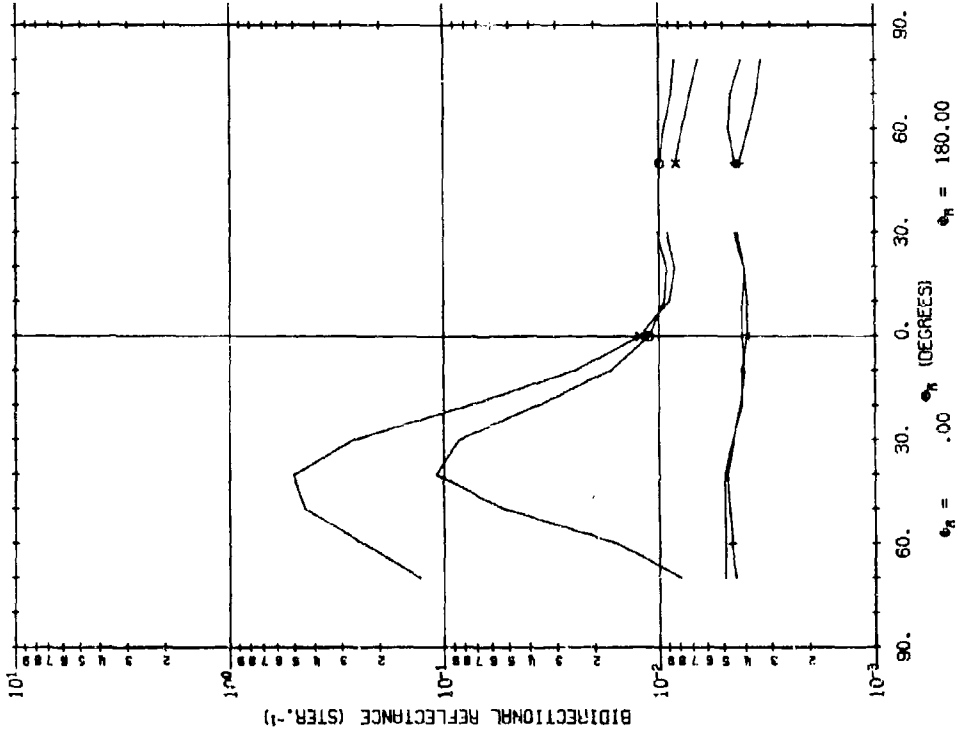


R01044 003

TWO COATS DEEP MOSS GREEN PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

$\theta_i = 40.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$

0
+
Δ
x

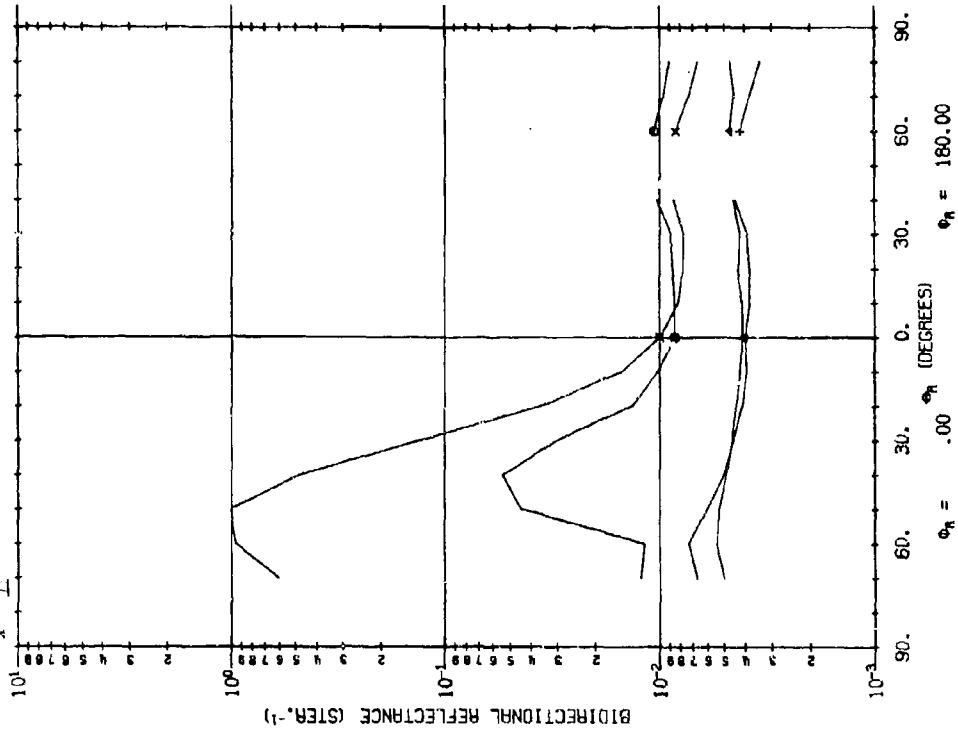


R01044 003

TWO COATS DEEP MOSS GREEN PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

$\theta_i = 50.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$

0
+
Δ
x



PAINT

R01044 003

TWO COATS DEEP MOSS GREEN PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

$\theta_i = 60.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$

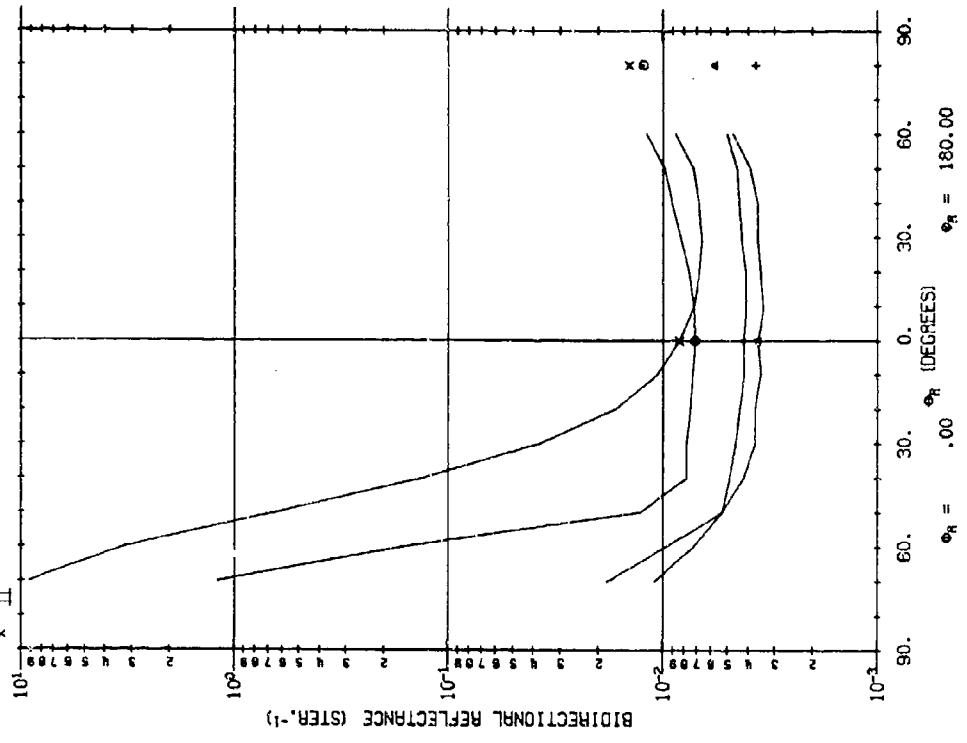
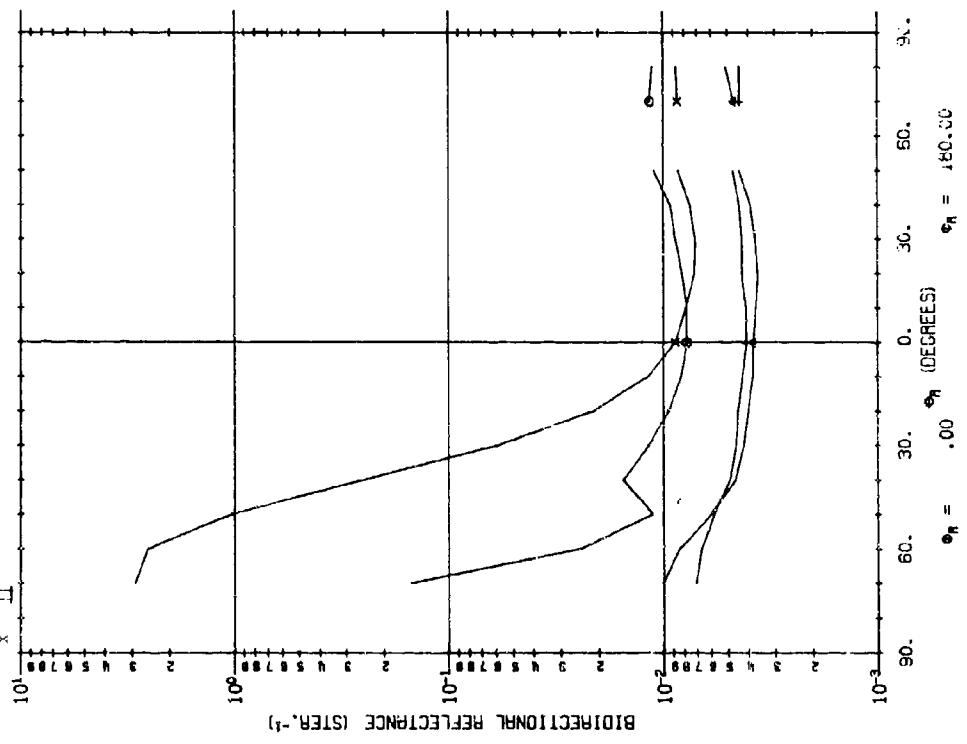
0 ||
+ ||
x ||

$\theta_i = 70.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$

TWO COATS DEEP MOSS GREEN PAINT ON
TWO COATS ZINC CHROMATE (WET DECKED)
ON ANODIZED ALUMINUM

0 ||
+ ||
x ||

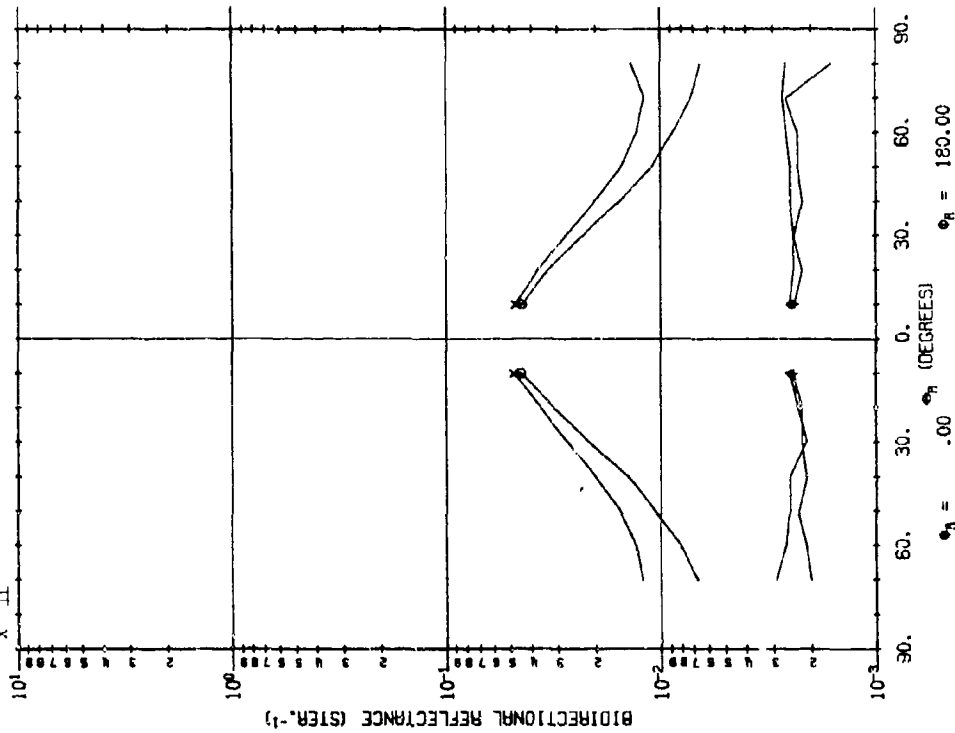
$\theta_i = 70.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$



A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

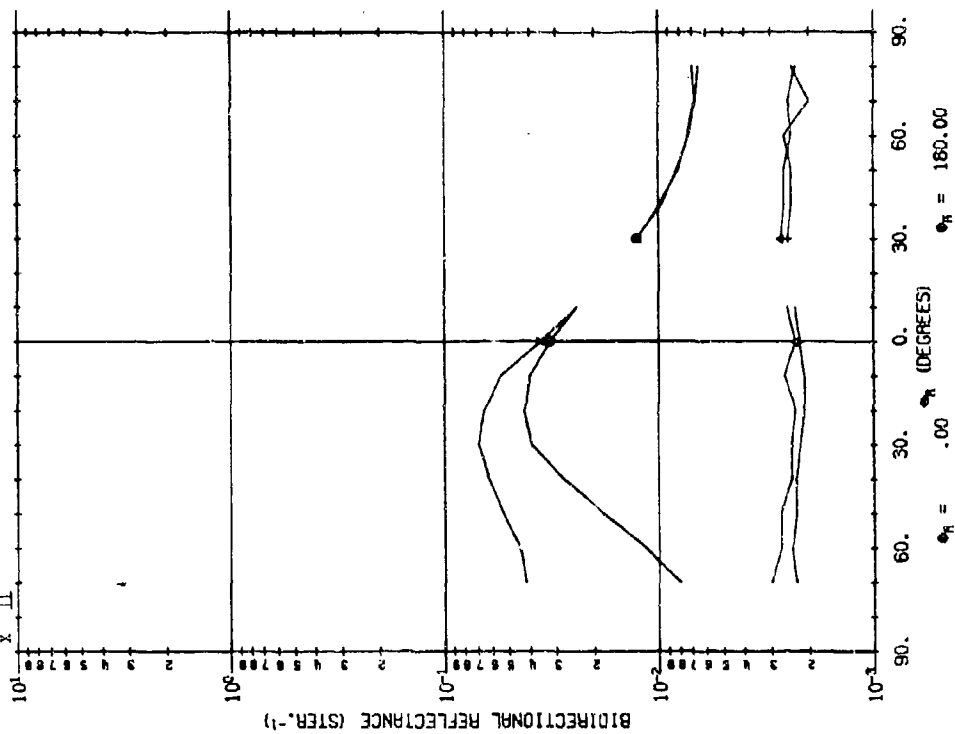
0 // $\phi_1 = 6.0$
+ // $\phi_1 = 180.0$
Δ // $\phi_1 = 180.0$
X // $\lambda = 0.63$



A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

0 // $\phi_1 = 20.3$
+ // $\phi_1 = 180.0$
Δ // $\phi_1 = 180.0$
X // $\lambda = 0.63$

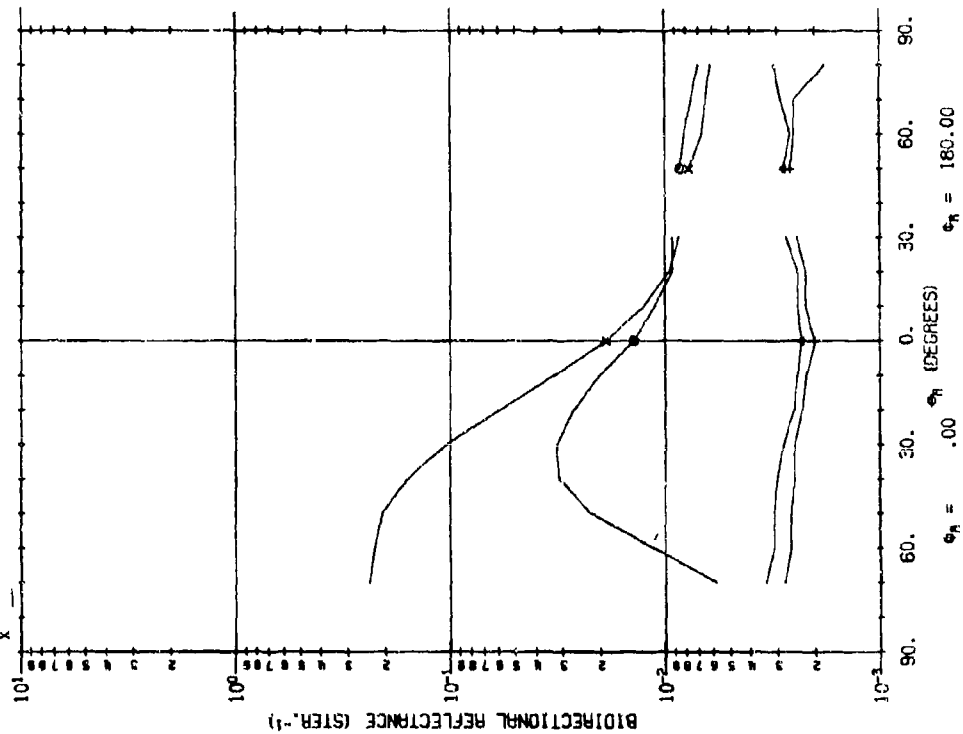


PAINT

A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

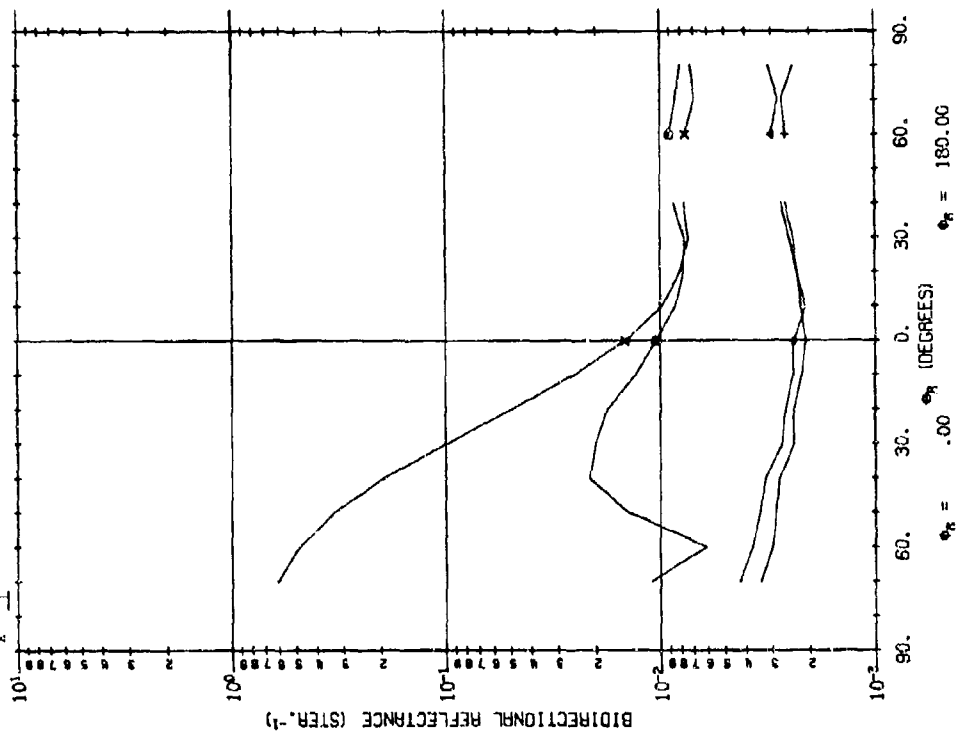
$\theta_1 = 40.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

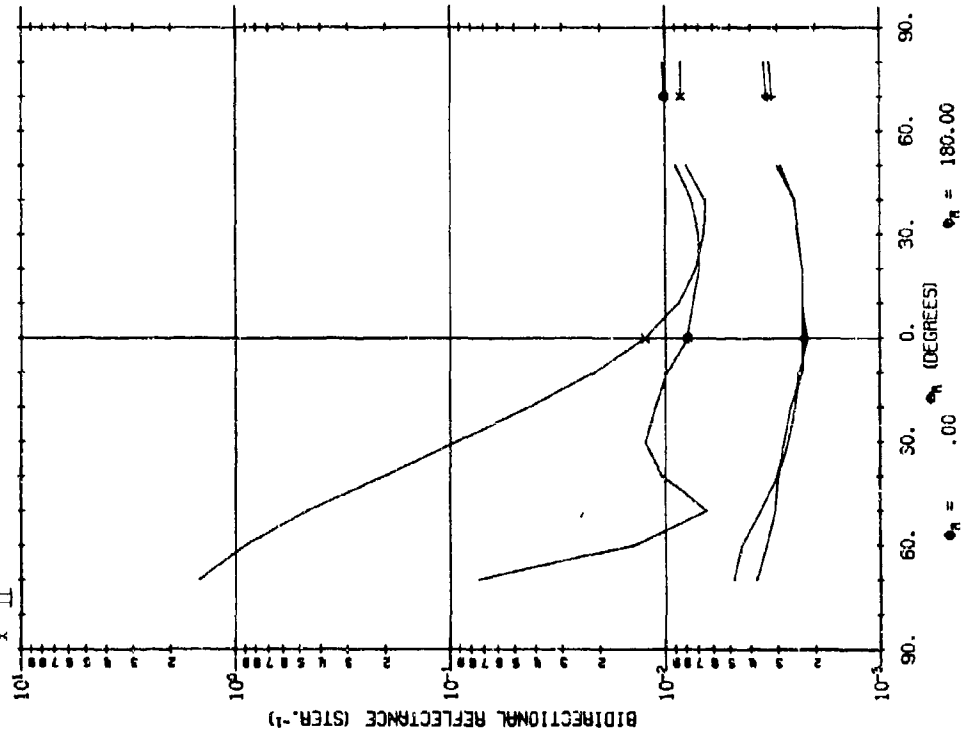
$\theta_1 = 50.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

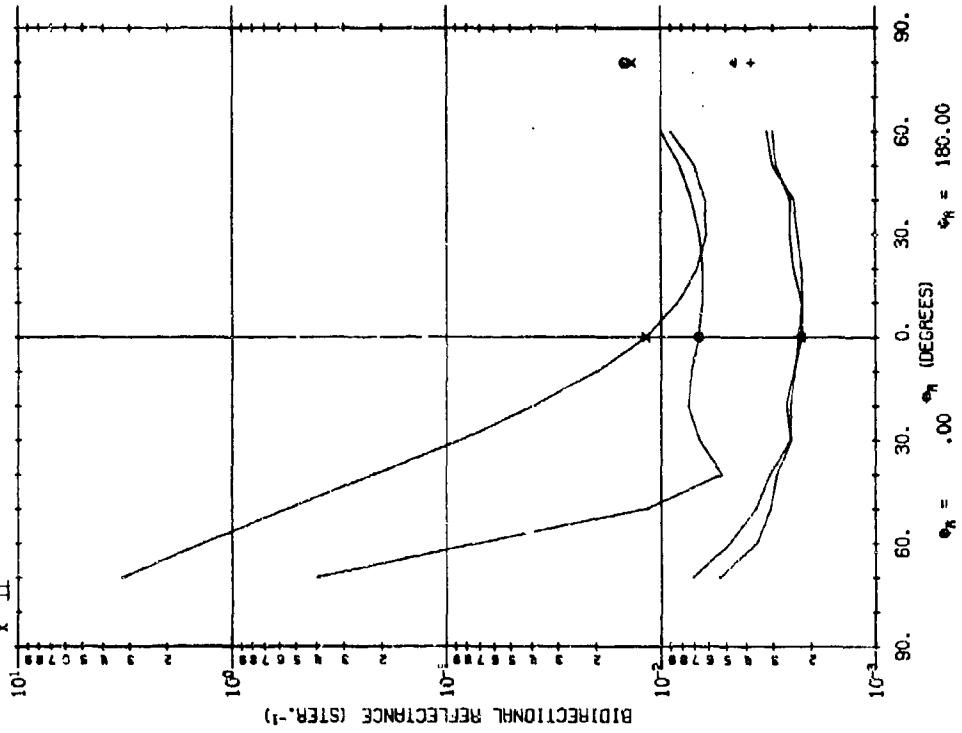
$\theta_i = 60.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$



A01047 003

TWO COATS OLIVE DRAB PAINT ON TWO
COATS ZINC CHROMATE (WET DECKED) ON
ANODIZED ALUMINUM

$\theta_i = 70.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$

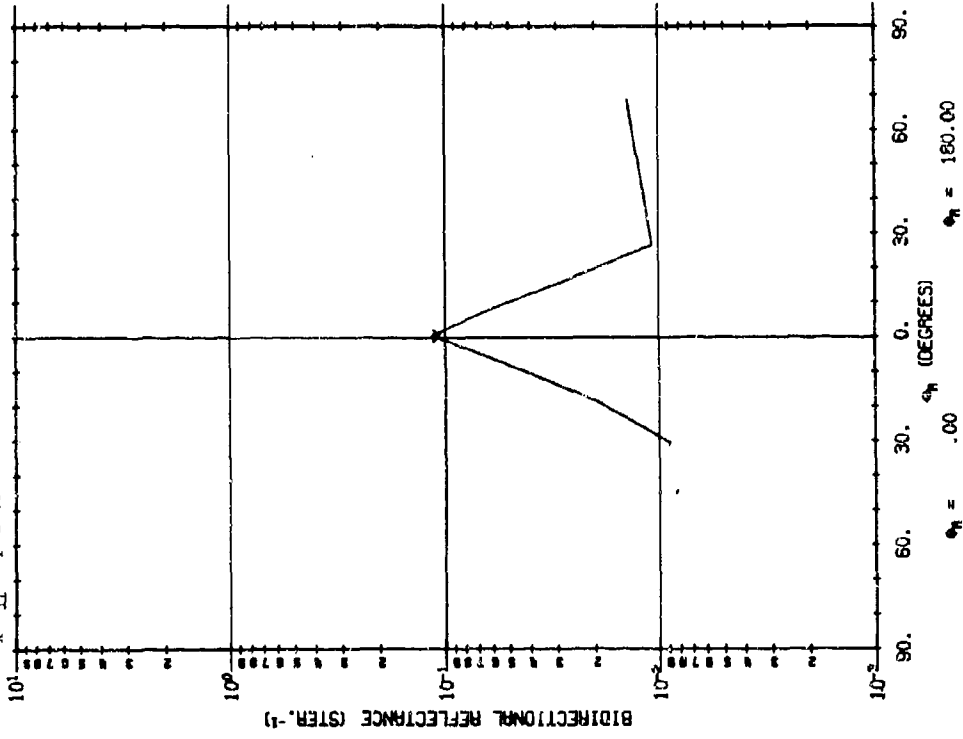


PAINT

R01049 001

Olive Drab Paint on Aluminium

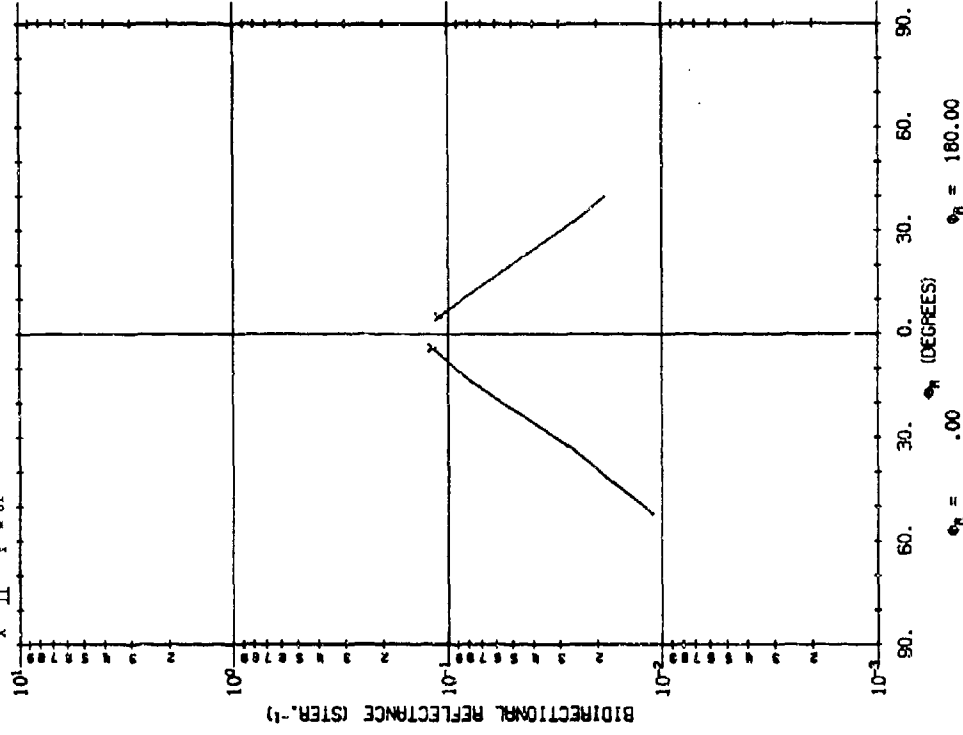
0 || $\epsilon_1 = 1.10$
+ || $\phi_1 = \phi_r$
 Δ || $\lambda = 10.6$
X || $\gamma = \text{UT}$



R01049 001

Olive Drab Paint on Aluminium

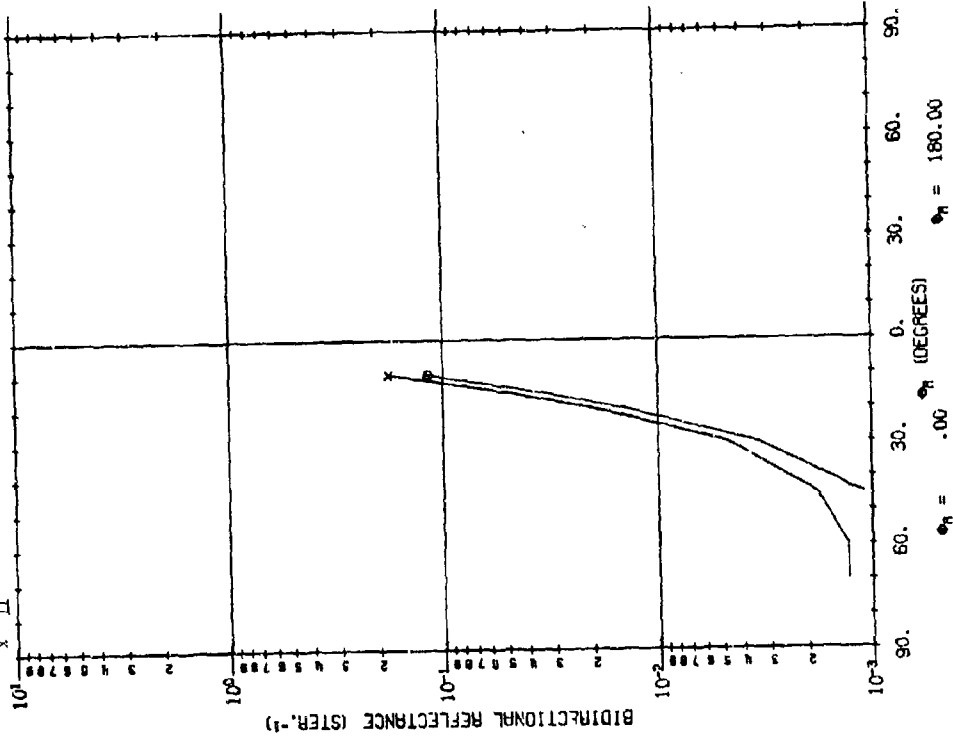
0 || $\epsilon_1 = 0.0$
+ || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
X || $\gamma = \text{UT}$



R01187 001

BLACK PAINT ON STEEL

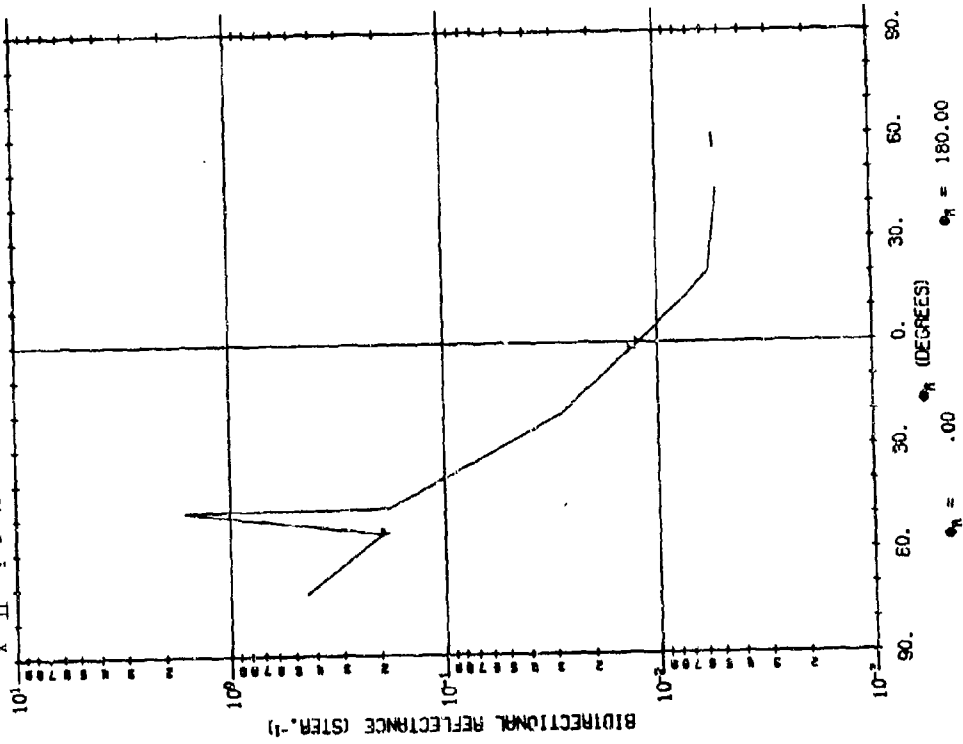
0 || $\epsilon_1 = 0.0$
 + || $\phi_1 = 180.0$
 2 || $\lambda = 0.63$
 x ||



R01049 001

Olive Drab Paint on Aluminum

0 || $\epsilon_1 = 50.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
 x || $\gamma = VT$

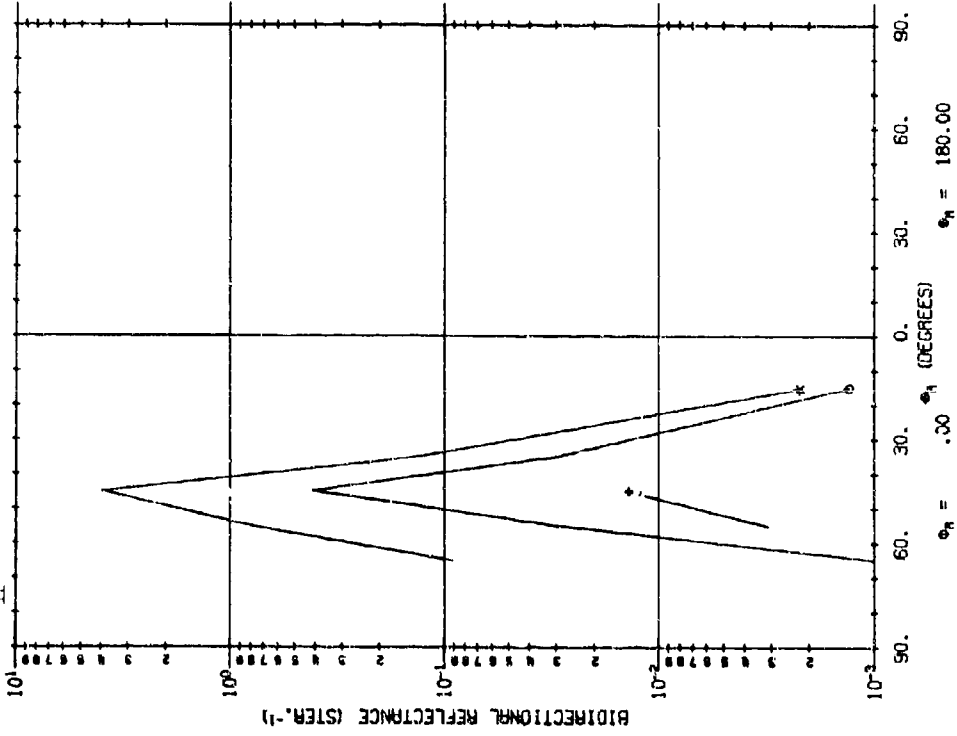


PAINT

A01187 001

BLACK PAINT ON STEEL

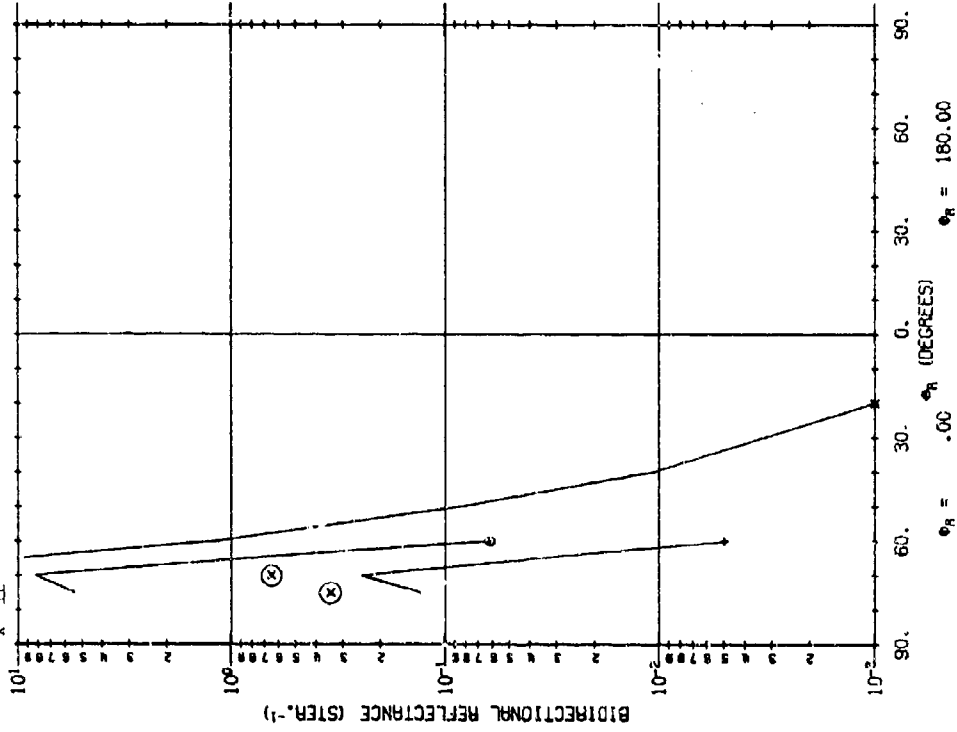
$\theta_1 = 45.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01187 001

BLACK PAINT ON STEEL

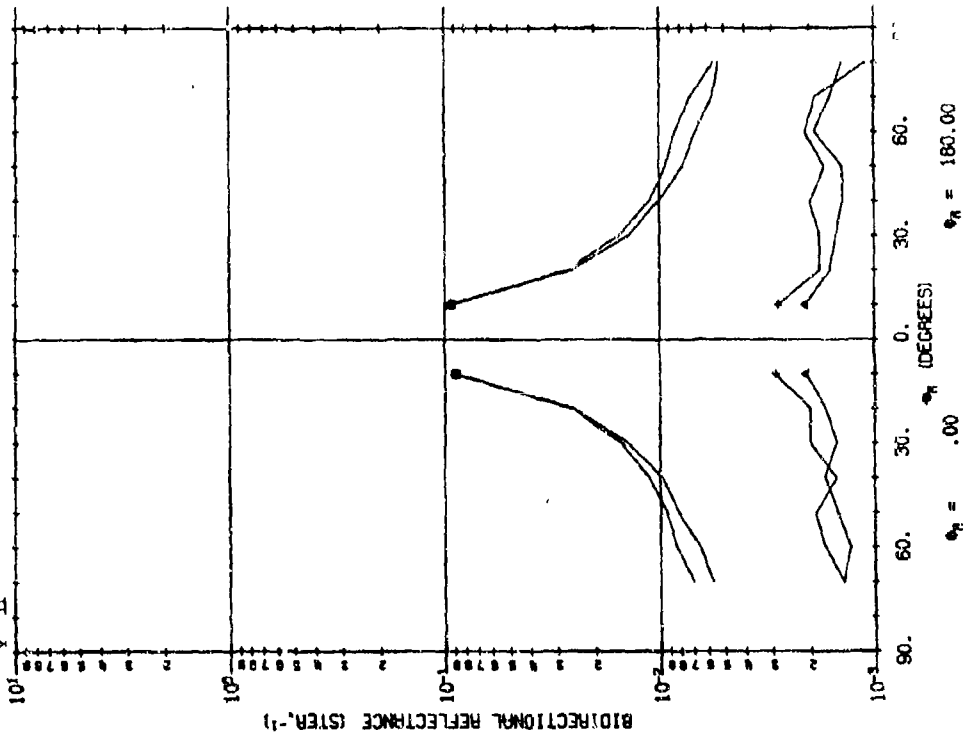
$\theta_1 = 70.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



A01224 004

Olive Drab Paint on Metal

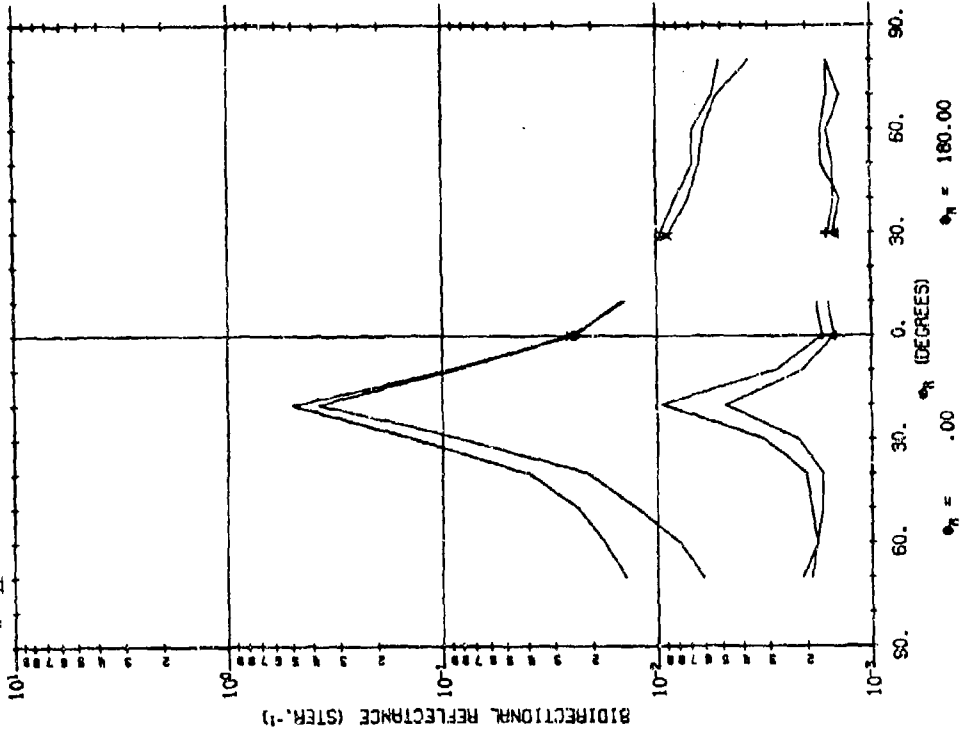
G || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
A || $\lambda = 0.63$
X ||



A01224 004

Olive Drab Paint on Metal

0 || $\theta_1 = 20.00$
+ || $\theta_2 = 180.00$
A || $\lambda = 0.63$
X ||



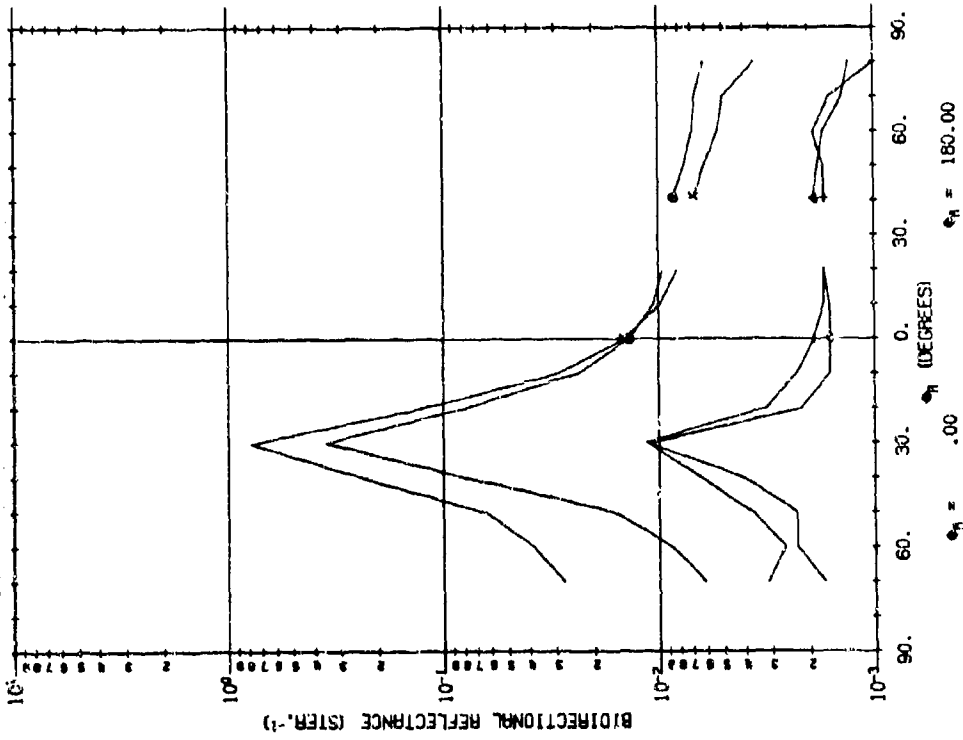
PAINT

AC1224 004

Olive Drab Paint on Metal

$\theta_i = 30.00$
 $\theta_r = 180.00$
 $\lambda = 0.63$

C II
+ II
x II

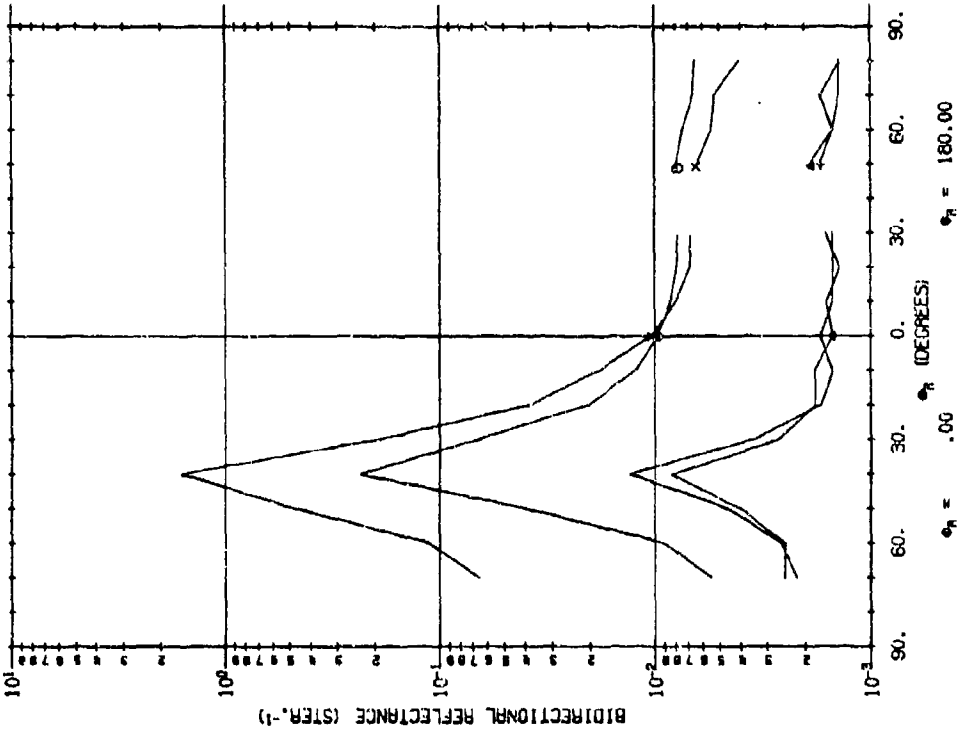


AC1224 004

Olive Drab Paint on Metal

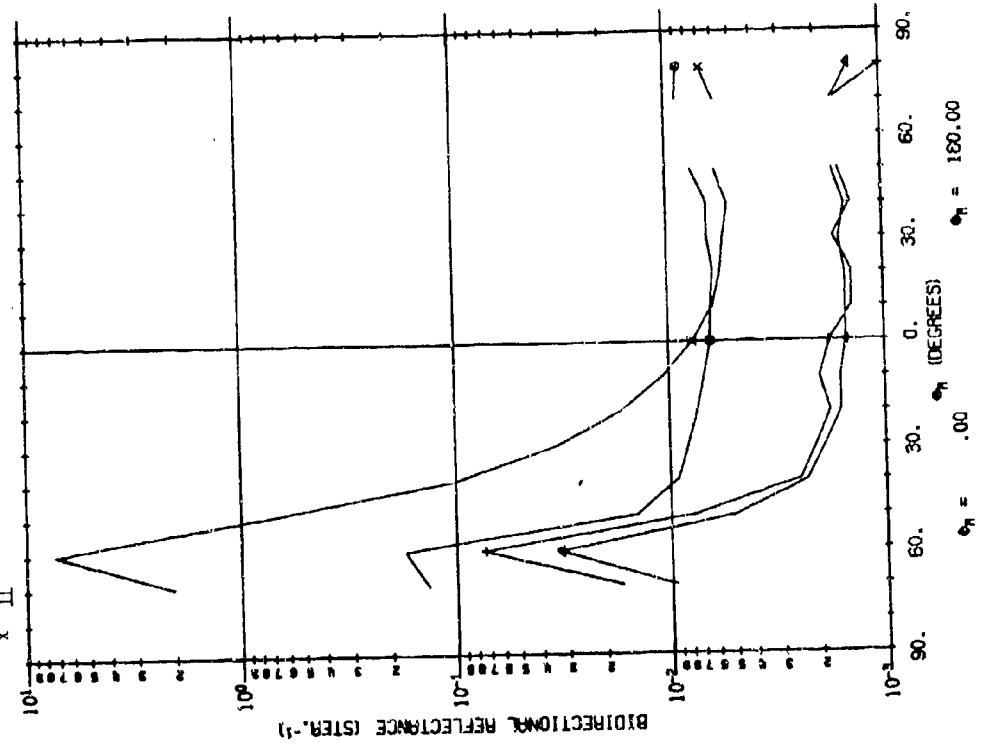
$\theta_i = 40.00$
 $\theta_r = 180.00$
 $\lambda = 0.63$

C II
+ II
x II



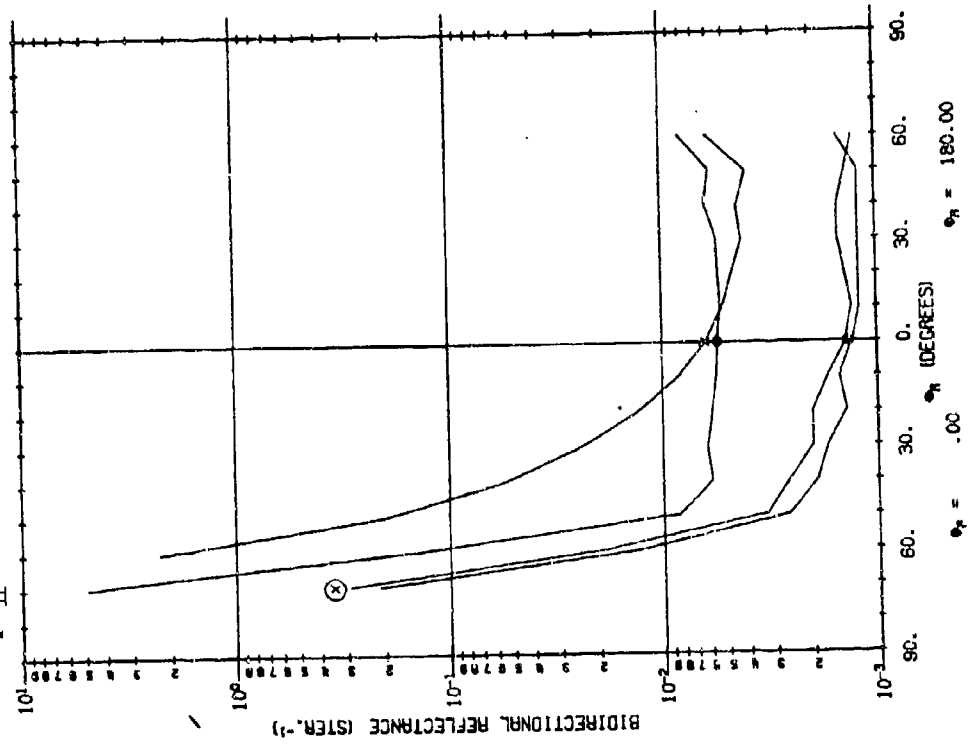
AO1224 004
 $\epsilon_1 = 60.00$
 $\epsilon_2 = 180.00$
 $\lambda = 0.53$

Olive Drab Paint on Metal



AO1224 004
 $\epsilon_1 = 60.00$
 $\epsilon_2 = 180.00$
 $\lambda = 0.63$

Olive Drab Paint on Metal



PAINT

AO1295 004

lt. Green Paint on Metal

$2\theta = 7.0$

$\phi_1 = \phi_r$

$\lambda = 0.63$

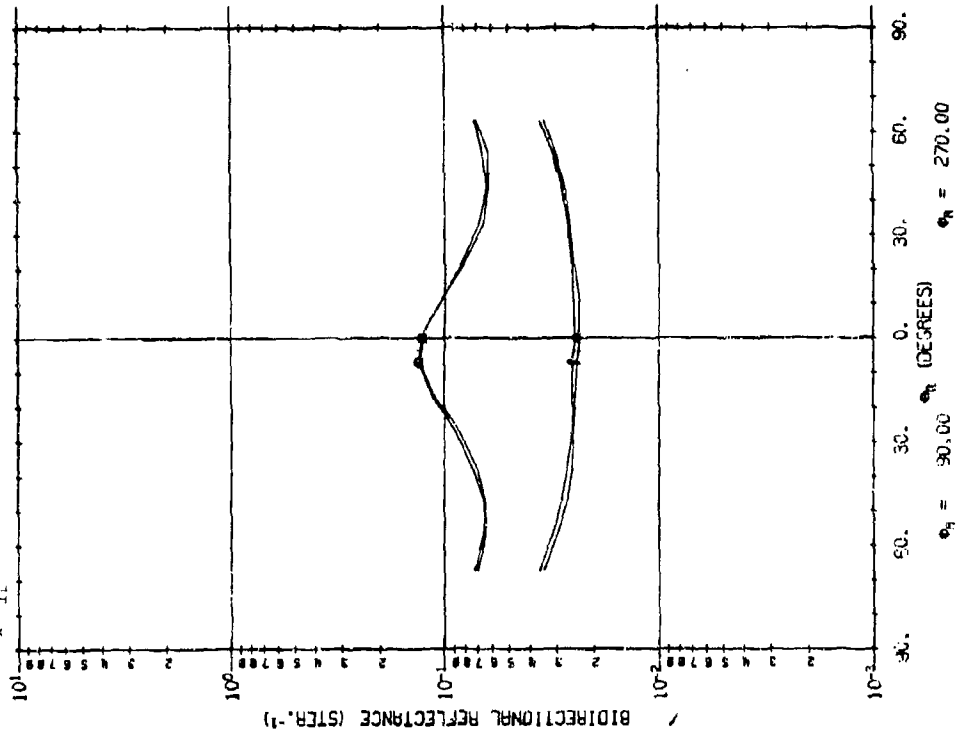
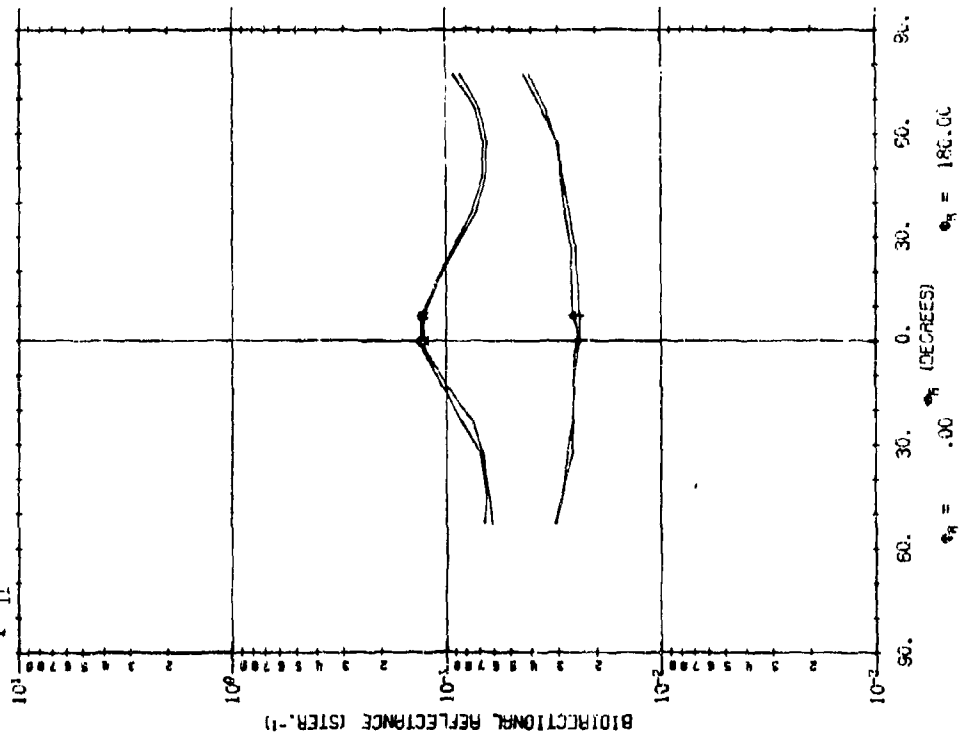
AO1295 004

lt. Green Paint on Metal

$2\theta = 7.0$

$\phi_1 = \phi_r$

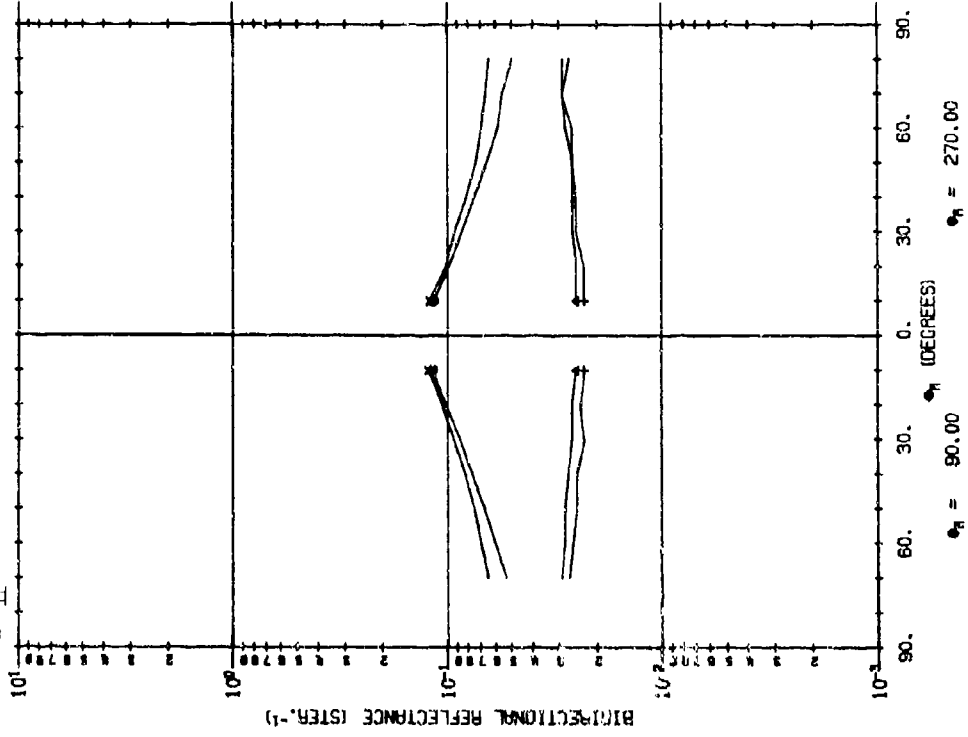
$\lambda = 0.63$



A01295 004
 0 || 1/2
 + || 1/4
 Δ || 1/8
 x ||

lt. Green Paint on Metal

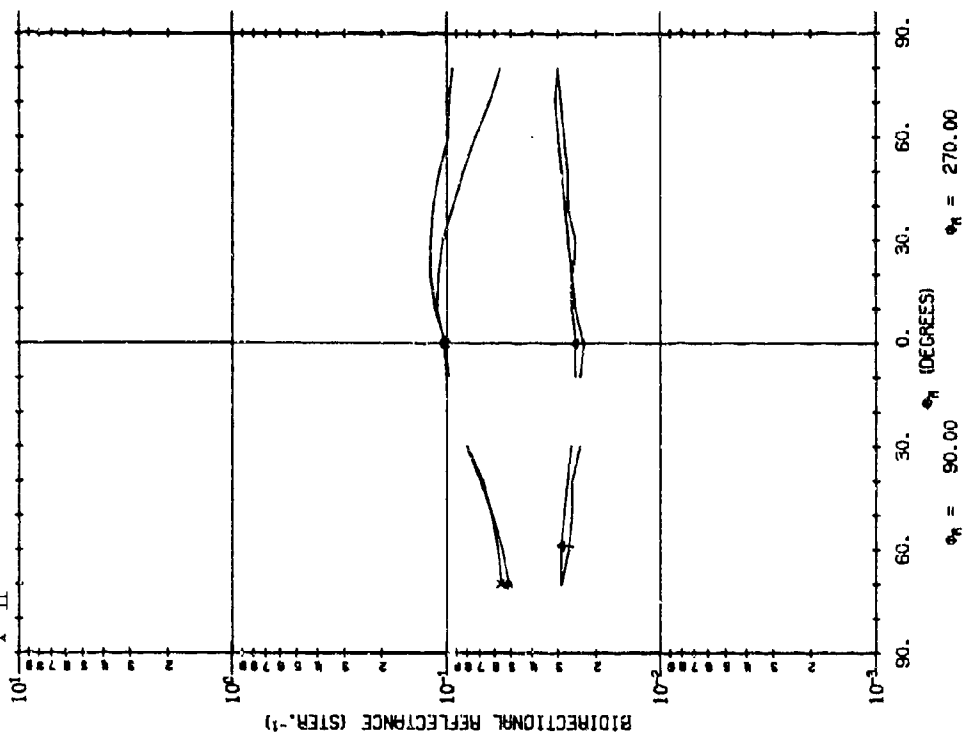
0.0
 90.00
 0.63



A01295 004
 0 || 1/2
 + || 1/4
 Δ || 1/8
 x ||

lt. Green Paint on Metal

20.00
 90.00
 0.63

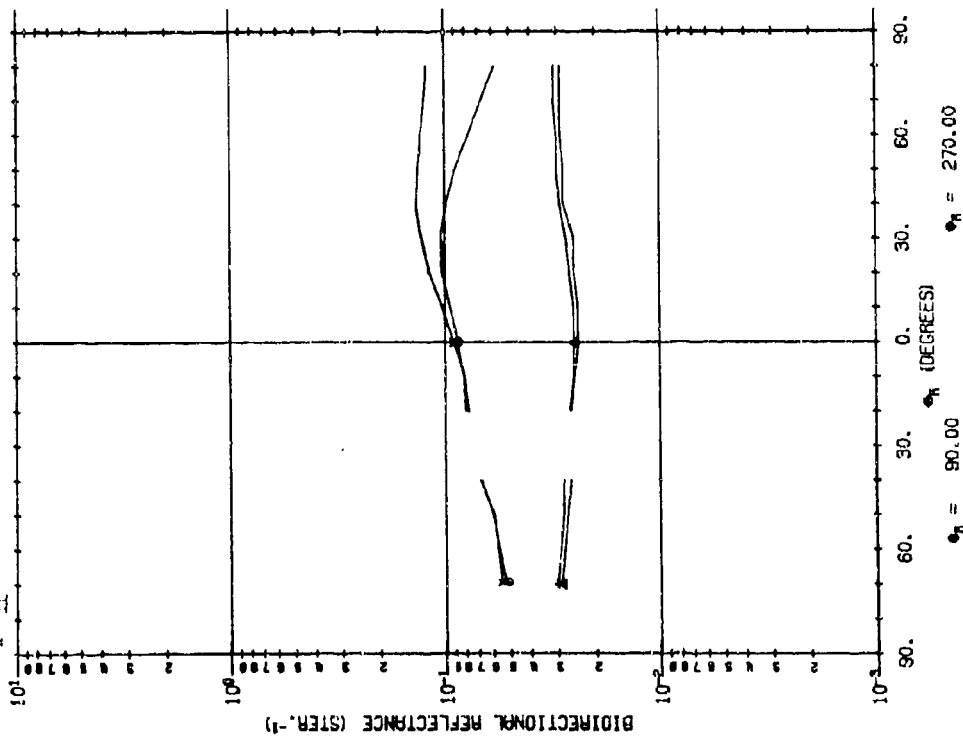


PAINT

A01295 004

Ir. Green Paint on Metal

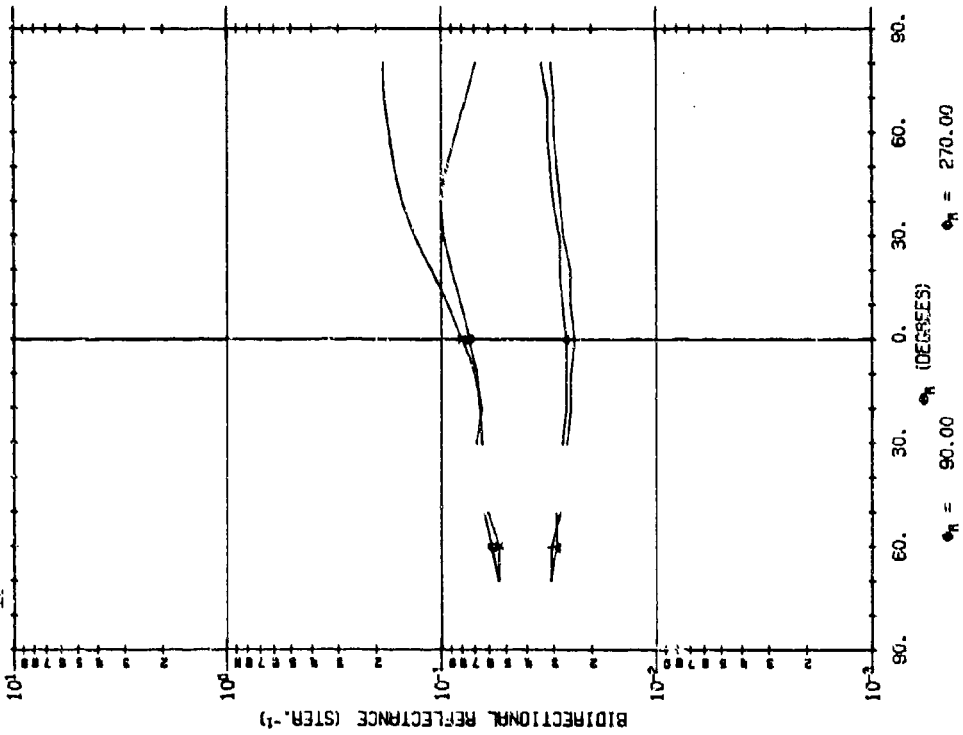
$\theta_1 = 30.00$
 $\theta_2 = 90.00$
 $\lambda = 0.63$



A01295 004

Ir. Green Paint on Metal

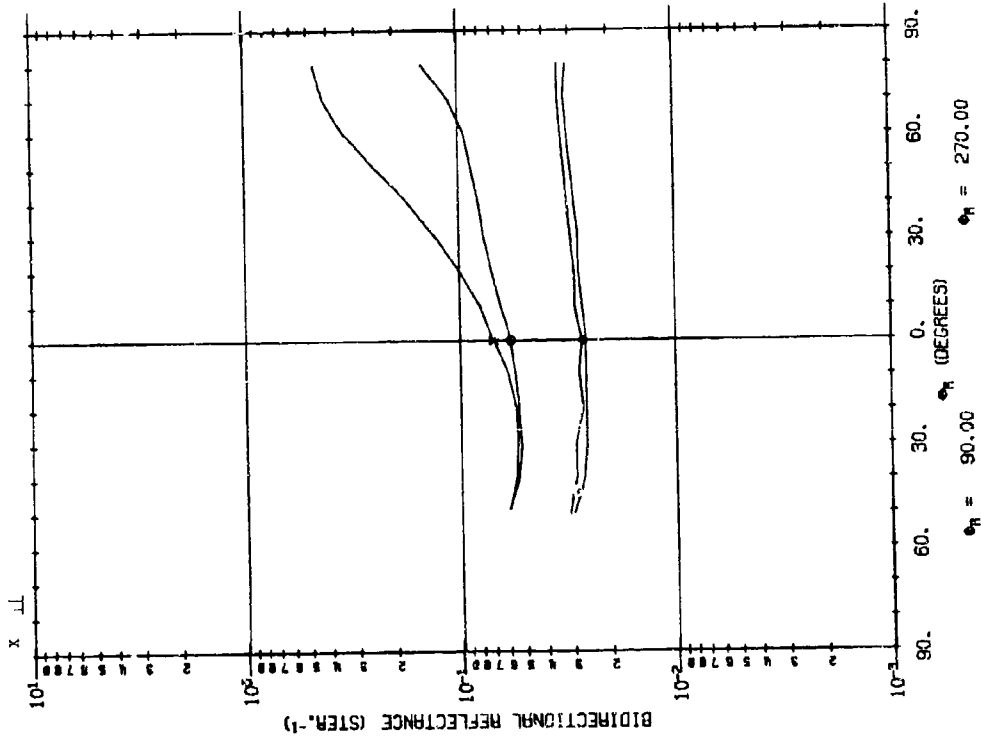
$\theta_1 = 40.00$
 $\theta_2 = 90.00$
 $\lambda = 0.63$



R01295 004

Lt. Green Paint on Metal

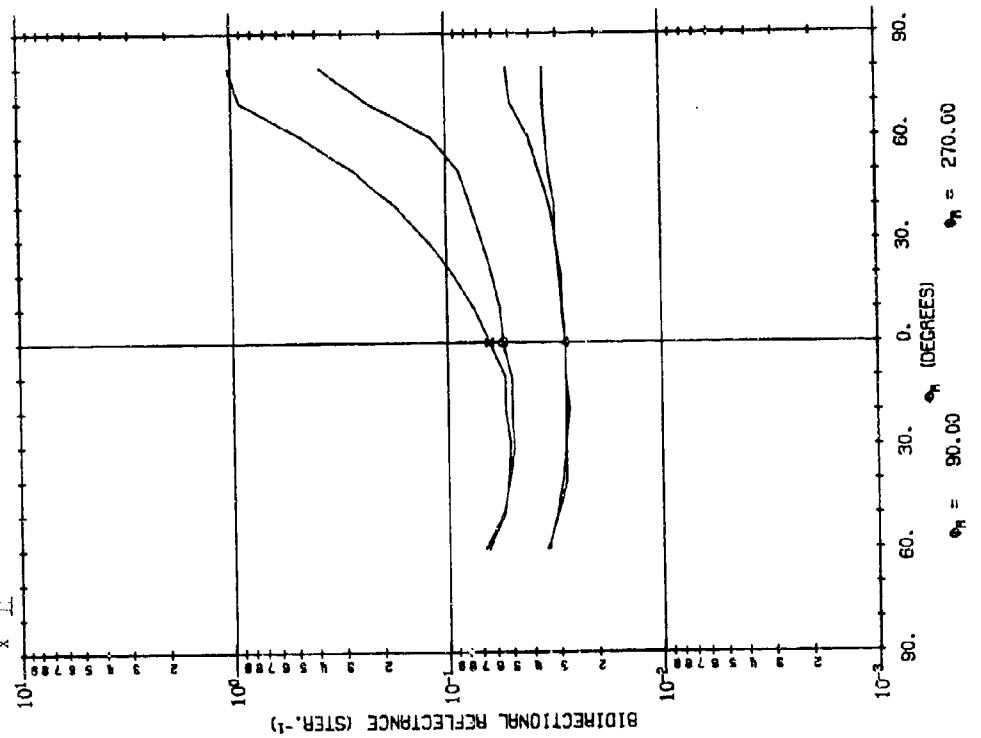
$\theta_1 = 60.00$
 $\theta_2 = 90.00$
 $\lambda = 0.63$



R01295 004

Lt. Green Paint on Metal

$\theta_1 = 70.00$
 $\theta_2 = 90.00$
 $\lambda = 0.63$

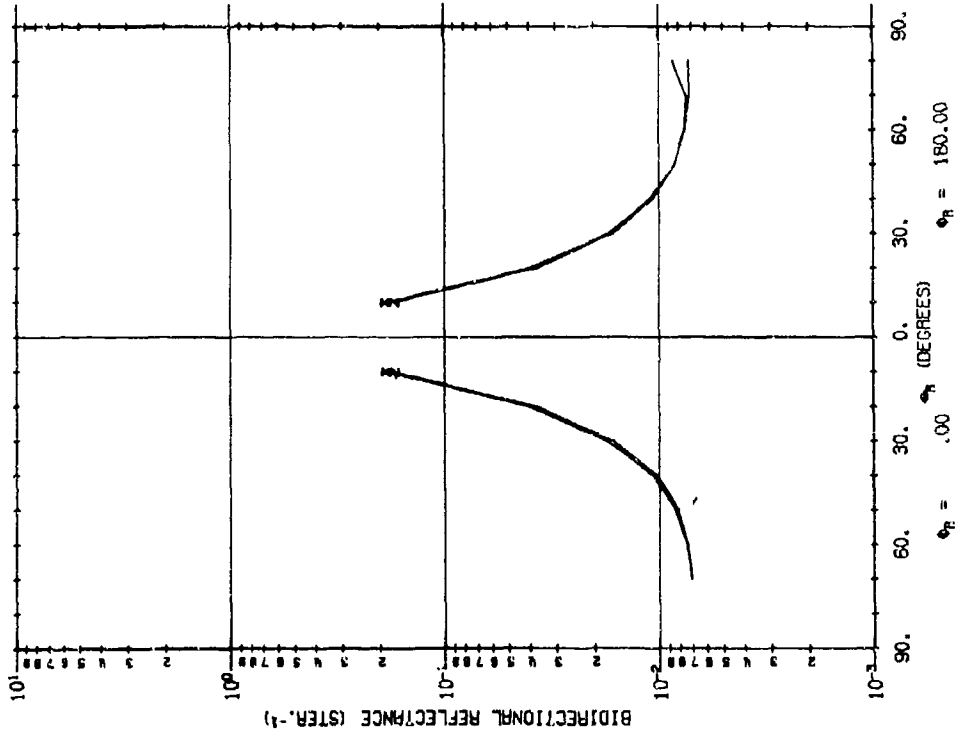


PAINT

A01337 001

X | T $\theta_1 = 0.0$
Z | T $\phi_1 = 180.0$
 $\lambda = 1.06$

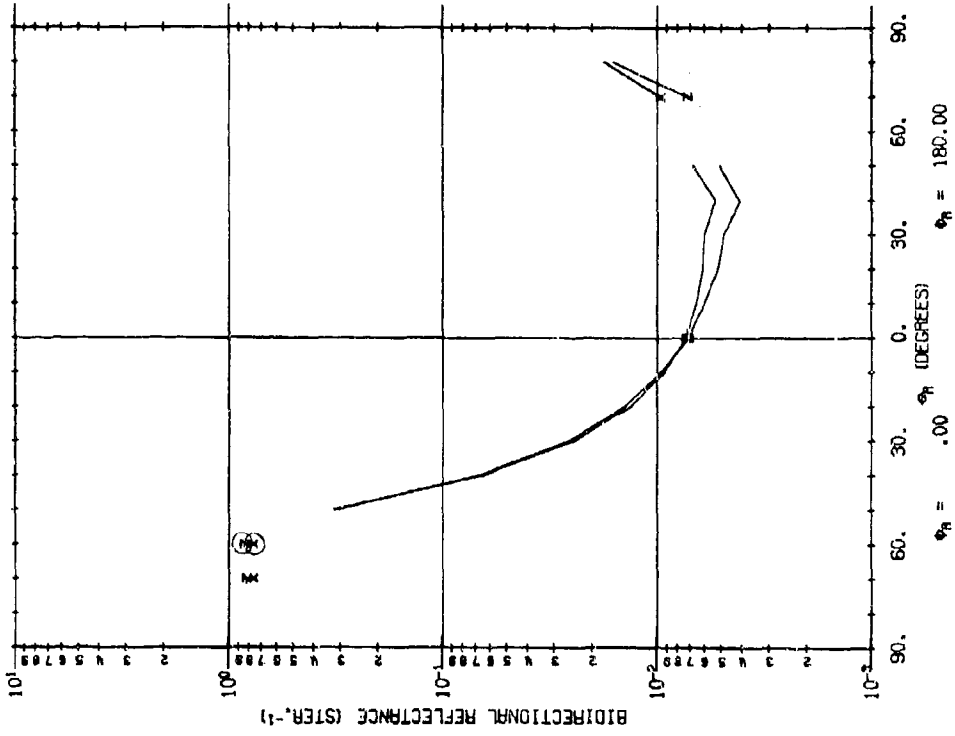
THREE COATS 3K BLACK VELVET PAINT
COVERING 30% OF ALCLAD ALUMINUM
PANEL



A01337 001

X | T $\theta_1 = 60.0$
Z | T $\phi_1 = 180.0$
 $\lambda = 1.06$

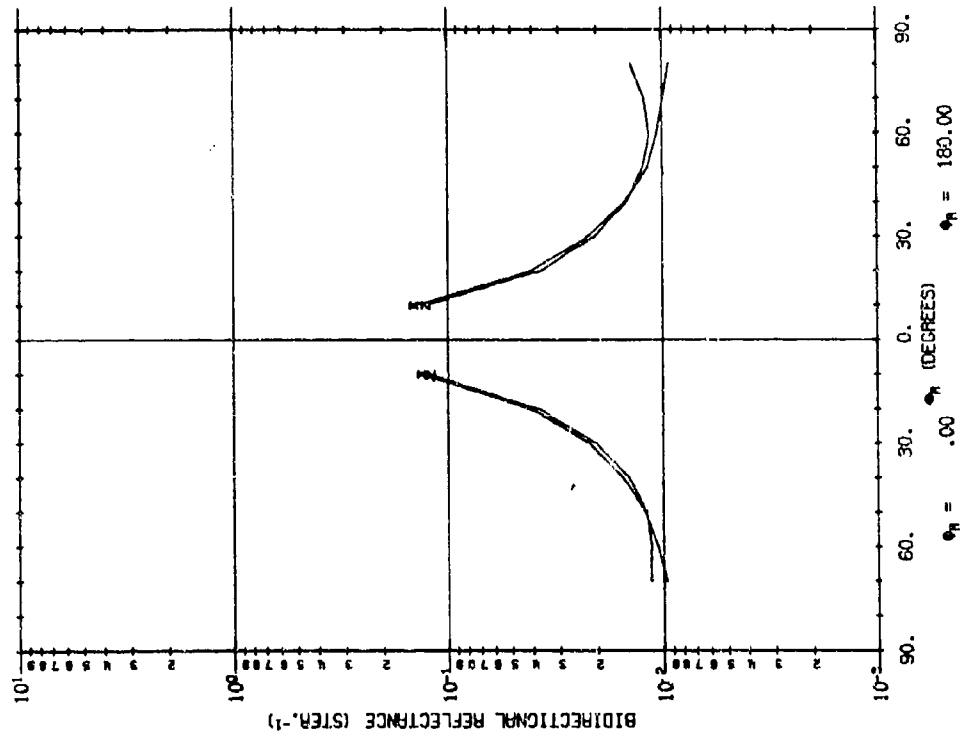
THREE COATS 3K BLACK VELVET PAINT
COVERING 30% OF ALCLAD ALUMINUM
PANEL



A01338 001

X | I $\phi_1 = 0.0$
 Z | I $\phi_1 = 180.0$
 $\lambda = 1.06$

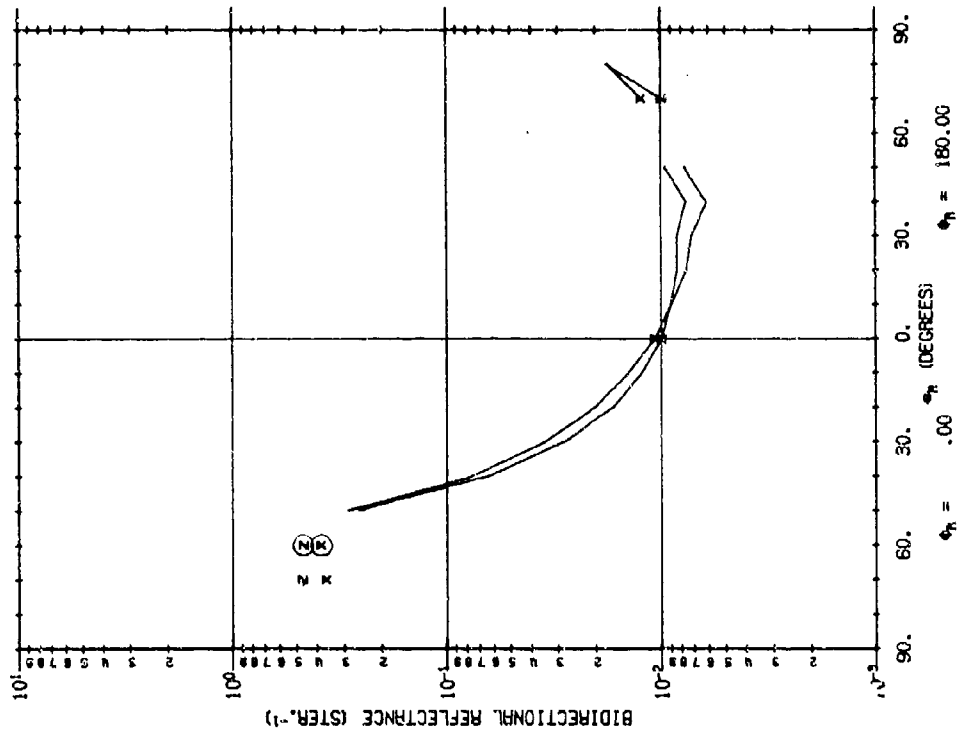
THREE COATS 3M BLACK VELVET PAINT
 COVERING 64.4% OF ALCLAD ALUMINUM
 PANEL



A01338 001

X | I $\phi_1 = 60.0$
 Z | I $\phi_1 = 180.0$
 $\lambda = 1.06$

THREE COATS 3M BLACK VELVET PAINT
 COVERING 64.4% OF ALCLAD ALUMINUM
 PANEL

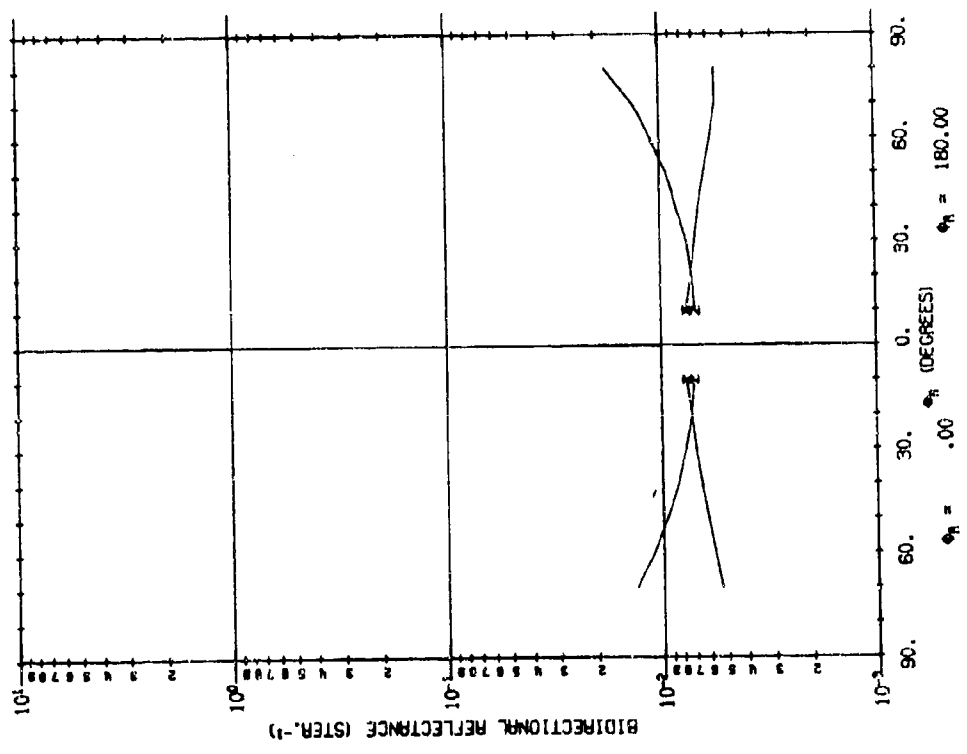


PAINT

R01339 001

THREE COATS 3M BLACK VELVET PAINT
ON ANCLAD ALUMINUM PANEL

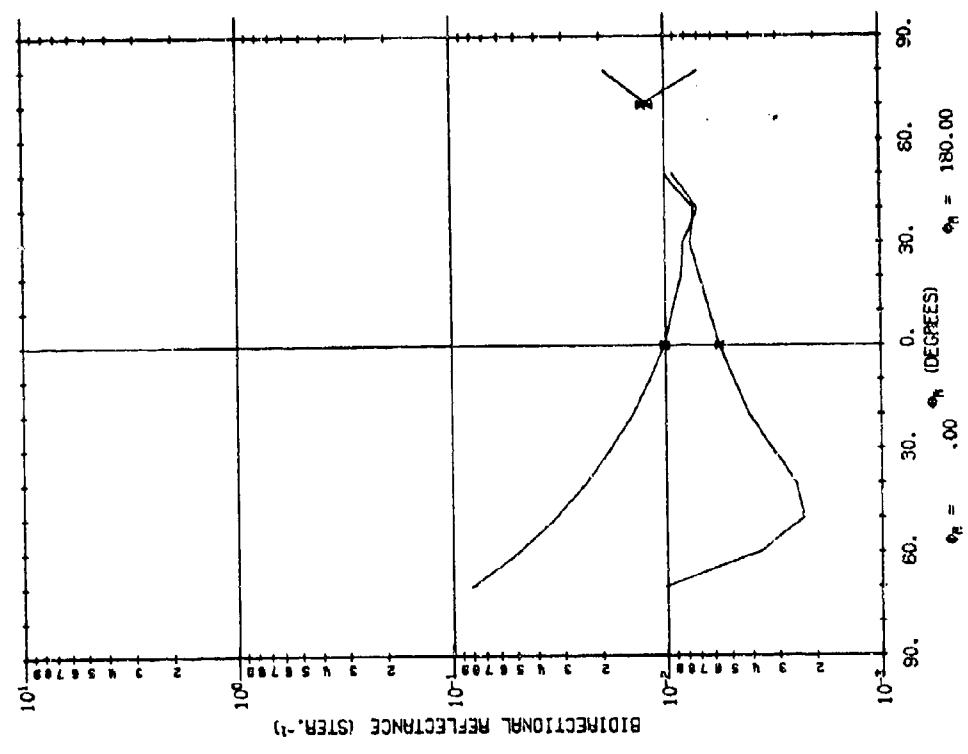
X |T $\theta_1 = 0.0$
Z |T $\phi_1 = 180.0$
 $\lambda = 1.06$



R01339 001

THREE COATS 3M BLACK VELVET PAINT
ON ANCLAD ALUMINUM PANEL

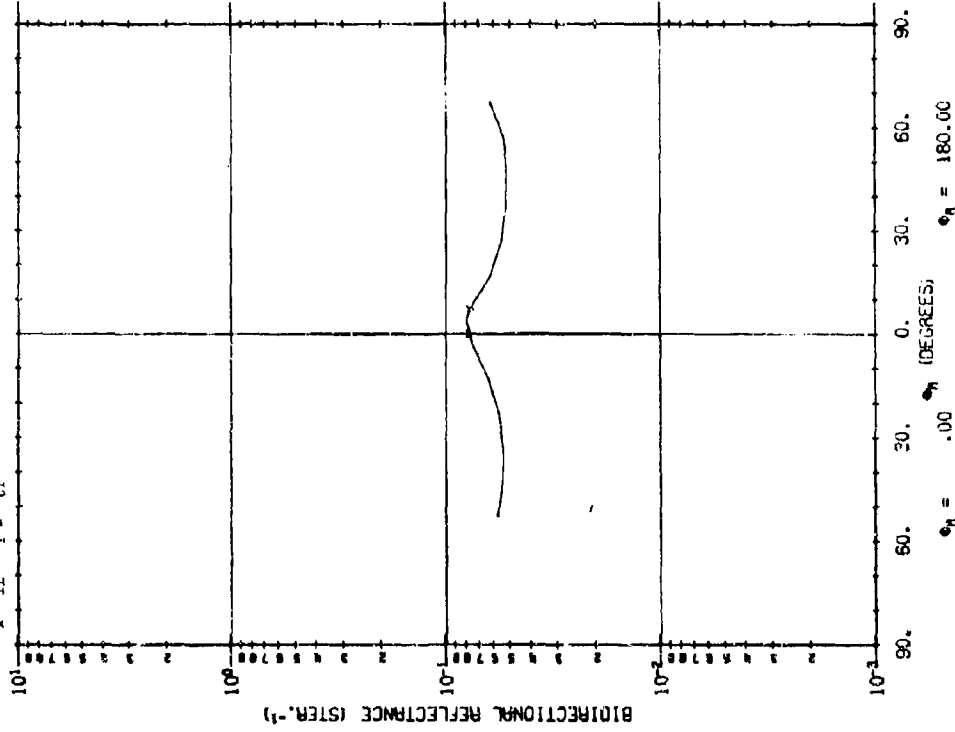
X |T $\theta_1 = 60.0$
Z |T $\phi_1 = 180.0$
 $\lambda = 1.06$



R01341 006

OLIVE DRAB PAINT ON METAL

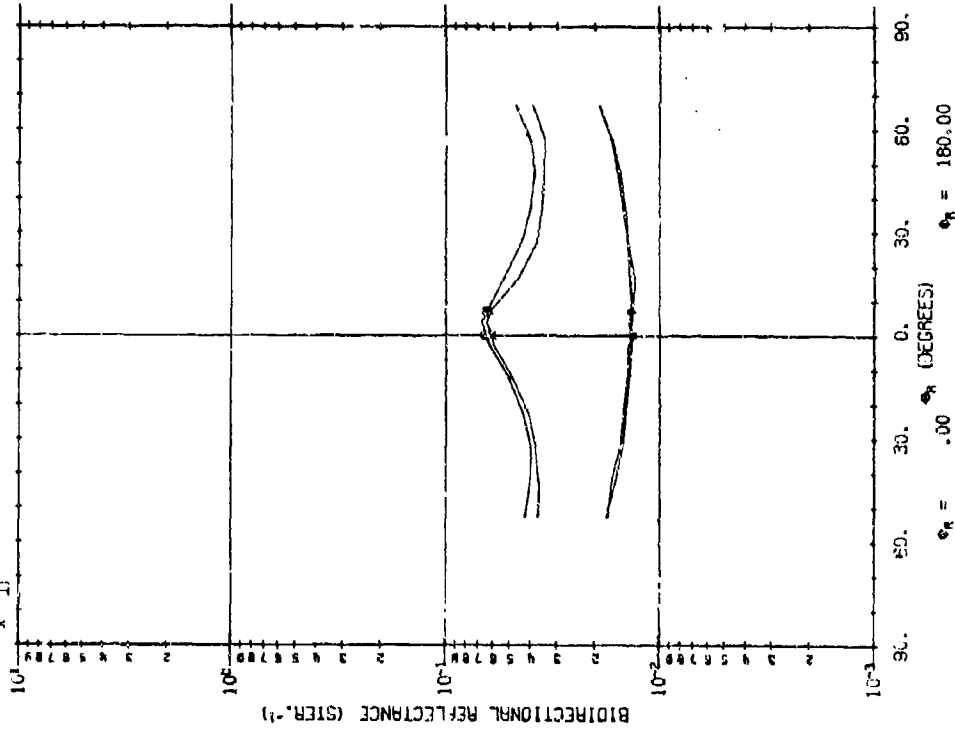
0 || 28 = 7.0
+ || $\theta_1 = 42$
 Δ || $\lambda = 0.63$
x || $\gamma = 0.63$
|| $\psi = 0.63$



R01341 006

OLIVE DRAB PAINT ON METAL

0 || 28 = 7.0
+ || $\theta_1 = 42$
 Δ || $\lambda = 0.63$
x || $\gamma = 0.63$
|| $\psi = 0.63$

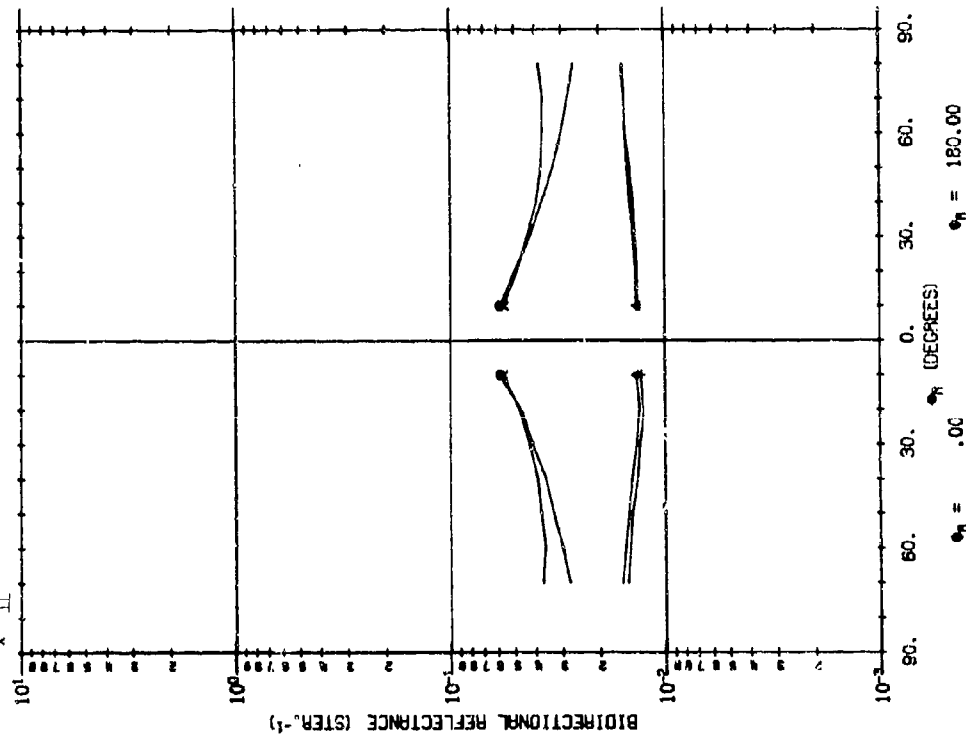


PAINT

A01341 006

Olive Drab Paint on Metal

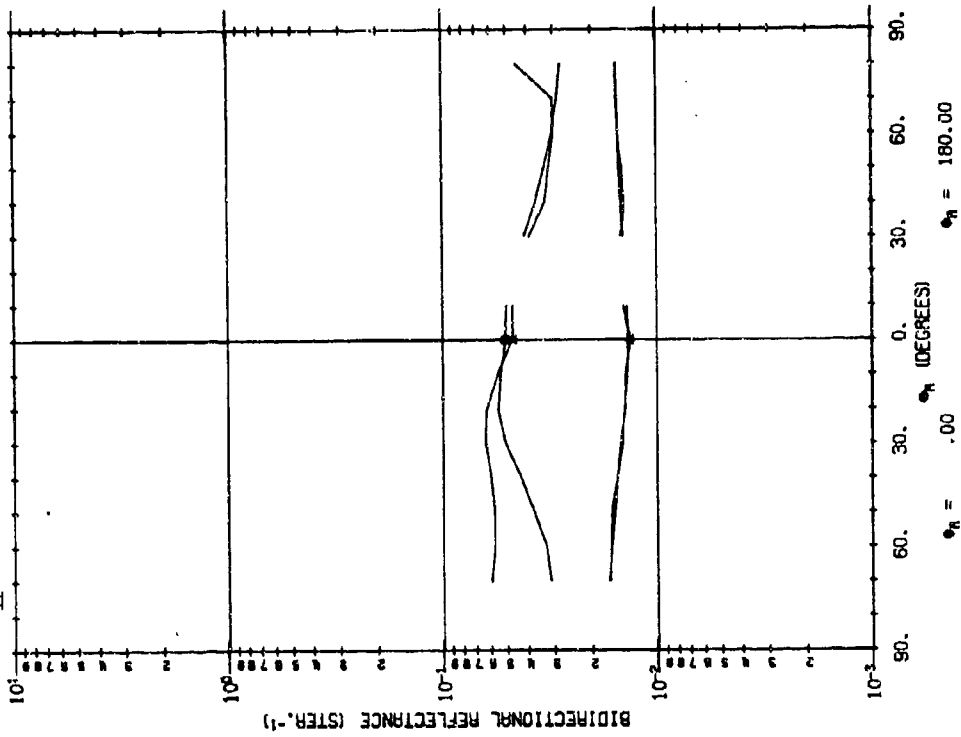
$\theta_1 = 0.0$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



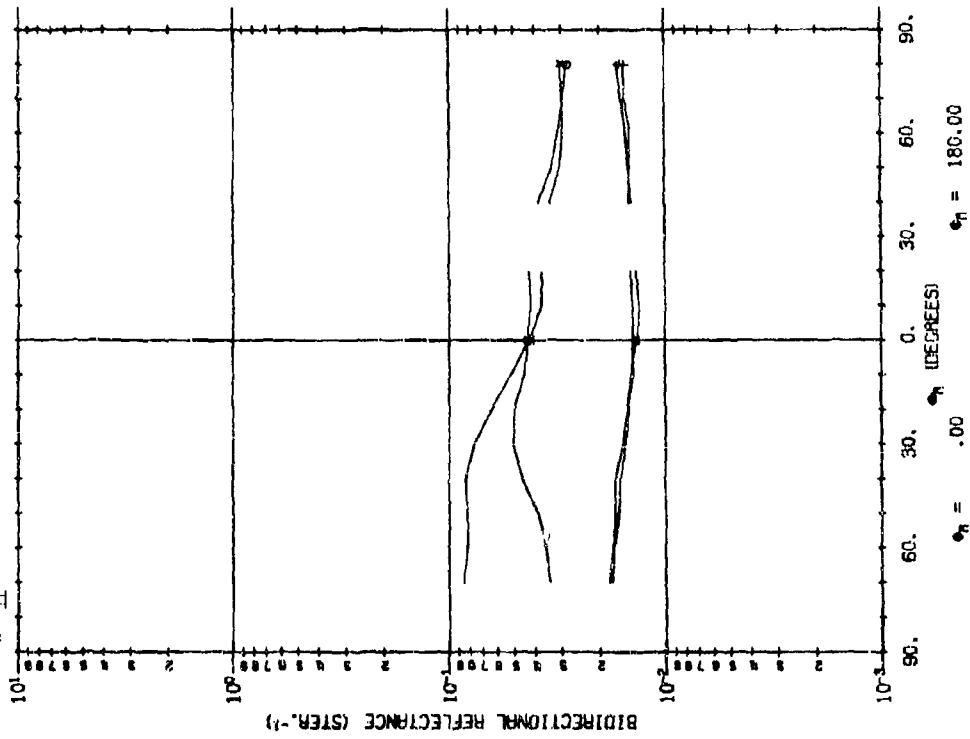
A01341 006

Olive Drab Paint on Metal

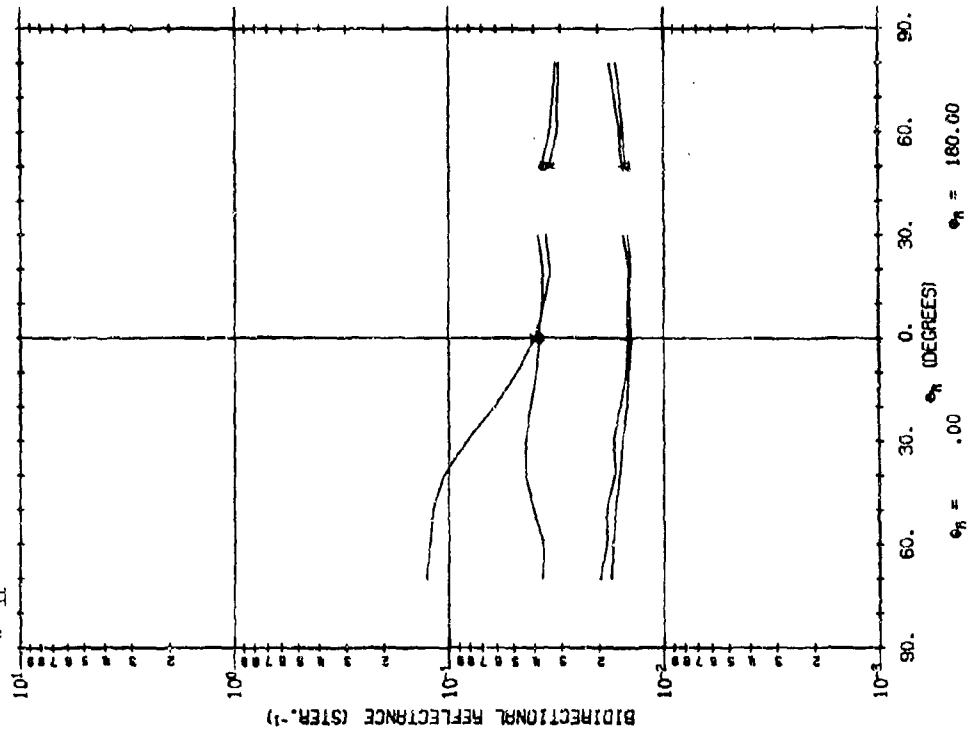
$\theta_1 = 20.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



A01341 006
 Olive Drab Paint on Metal
 $\epsilon_1 = 30.00$
 $\mu_1 = 180.00$
 $\lambda = 0.63$
 + ||
 A ||
 X ||



A01341 006
 Olive Drab Paint on Metal
 $\epsilon_1 = 40.00$
 $\mu_1 = 180.00$
 $\lambda = 0.63$
 + ||
 A ||
 X ||

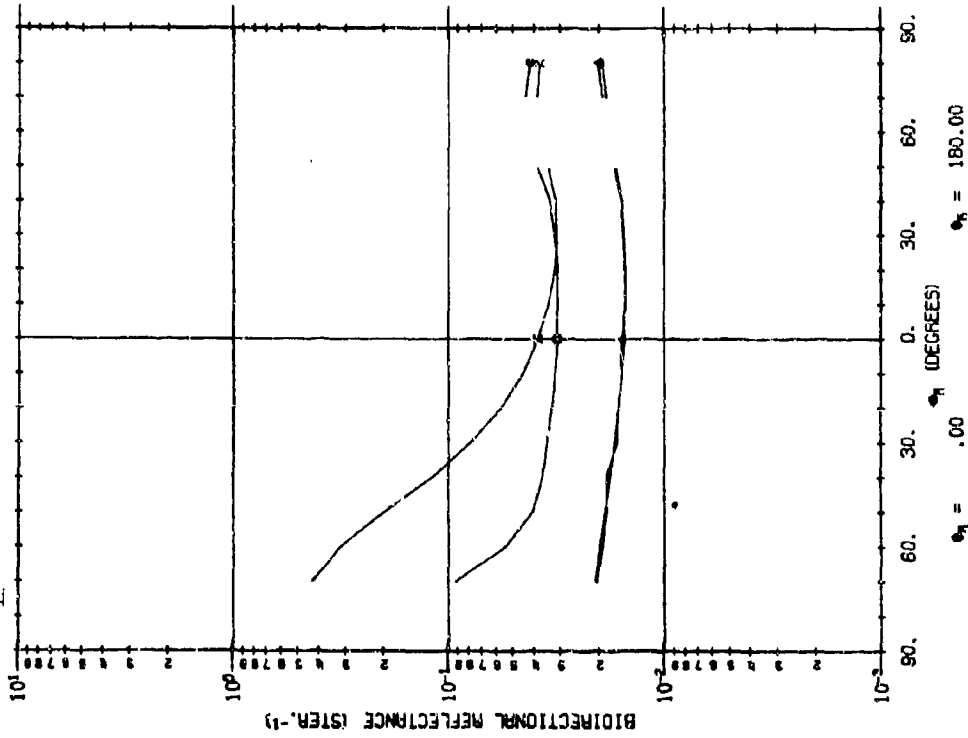


PAINT

A01341 006

Olive Drab Paint on Metal

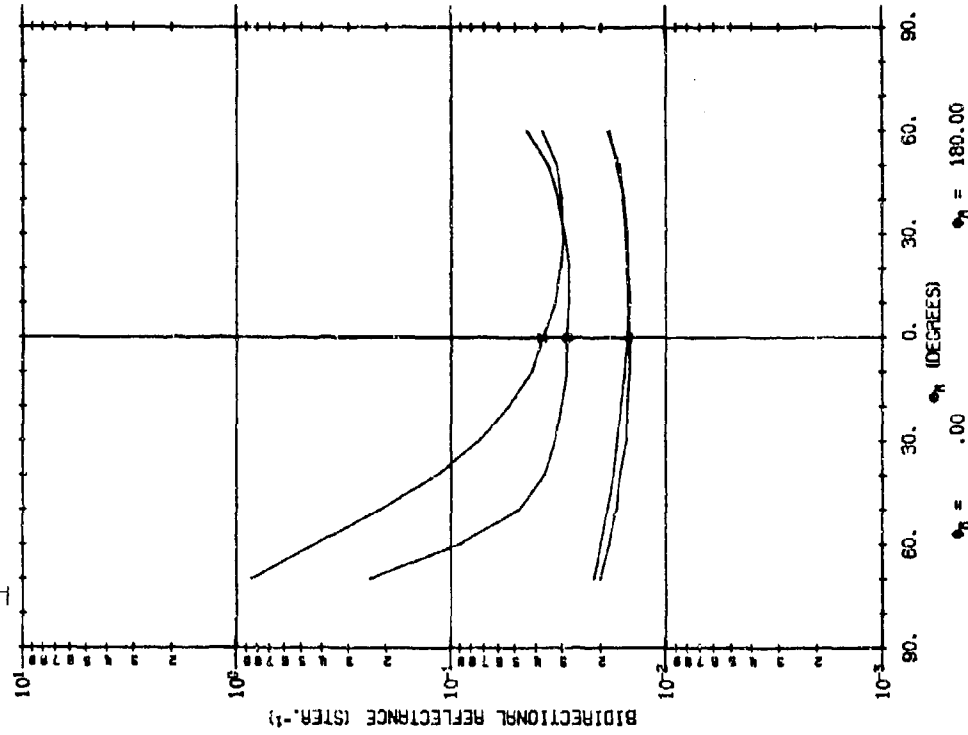
$\theta_1 = 60.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



A01341 006

Olive Drab Paint on Metal

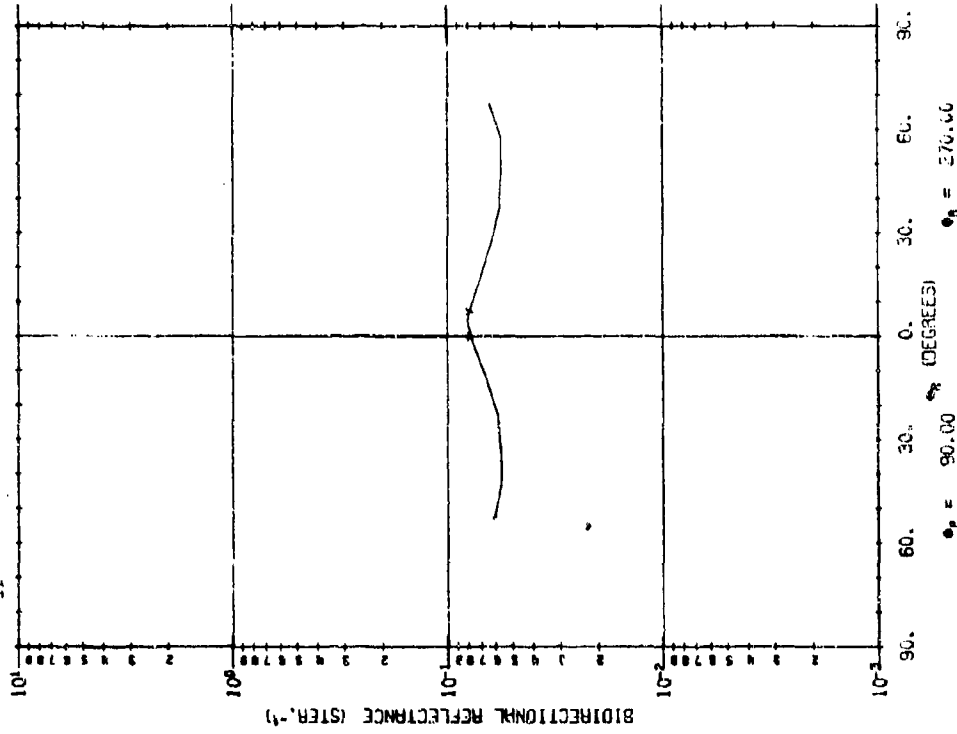
$\theta_1 = 70.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



HC1341 006

OLIVE DRAB PAINT ON METAL

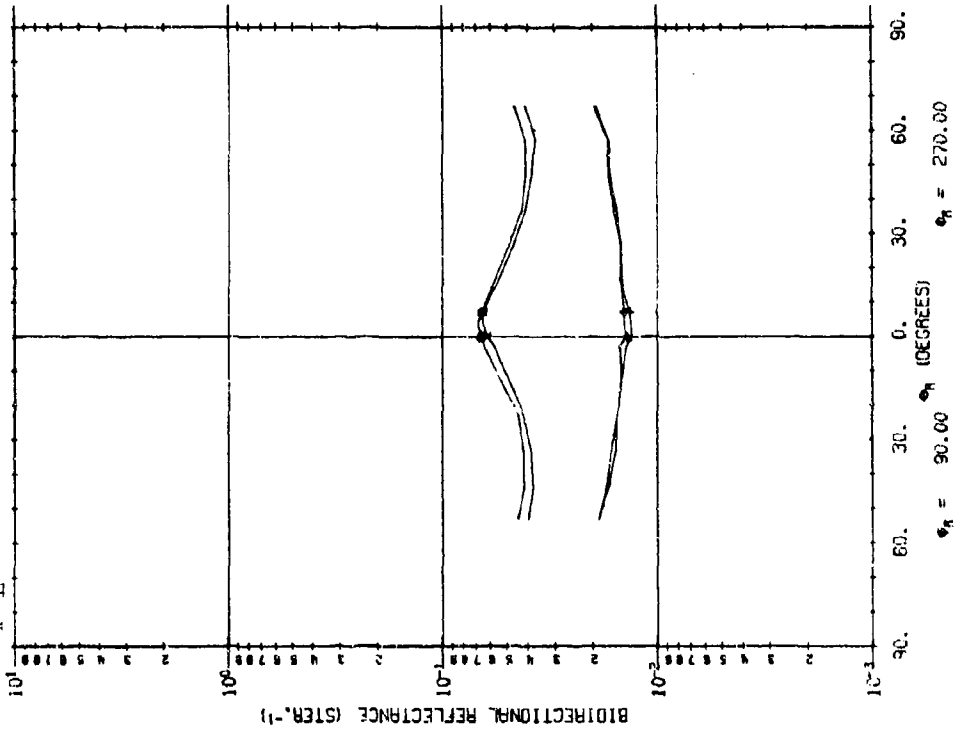
2θ = 7.0
+ || ϕ_L = ϕ_r
Δ || λ = 0.63
x || γ = 0°



HC1341 006

OLIVE DRAB PAINT ON METAL

2θ = 7.0
+ || ϕ_L = ϕ_r
Δ || λ = 0.63
x || γ = 0°

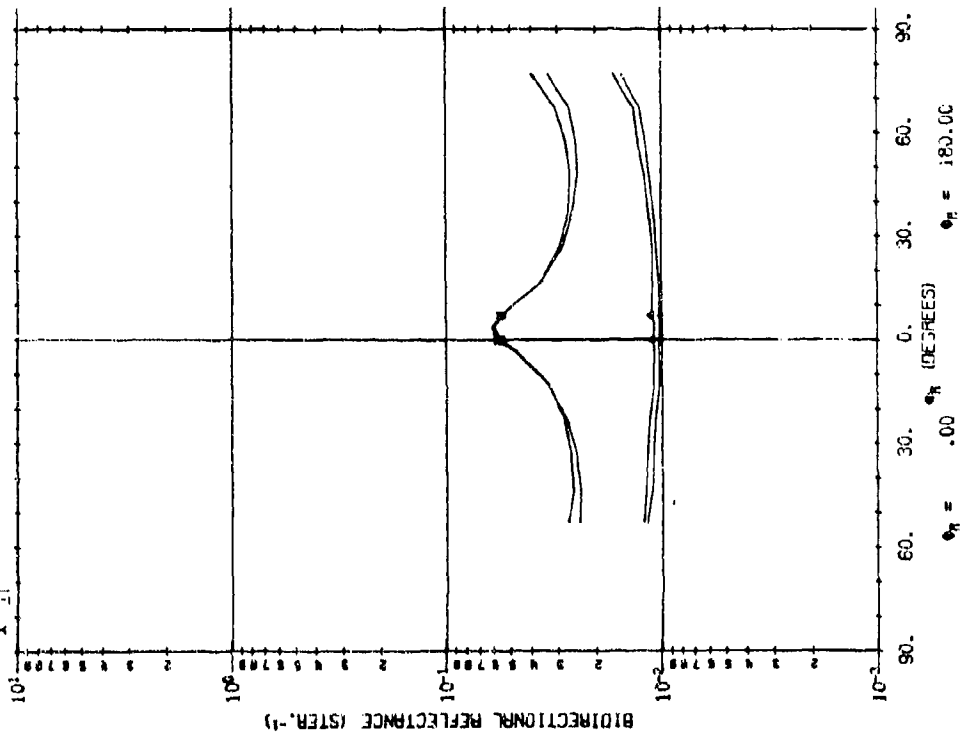


PAINT

R01342 005

OLIVE DRAB PAINT ON METAL

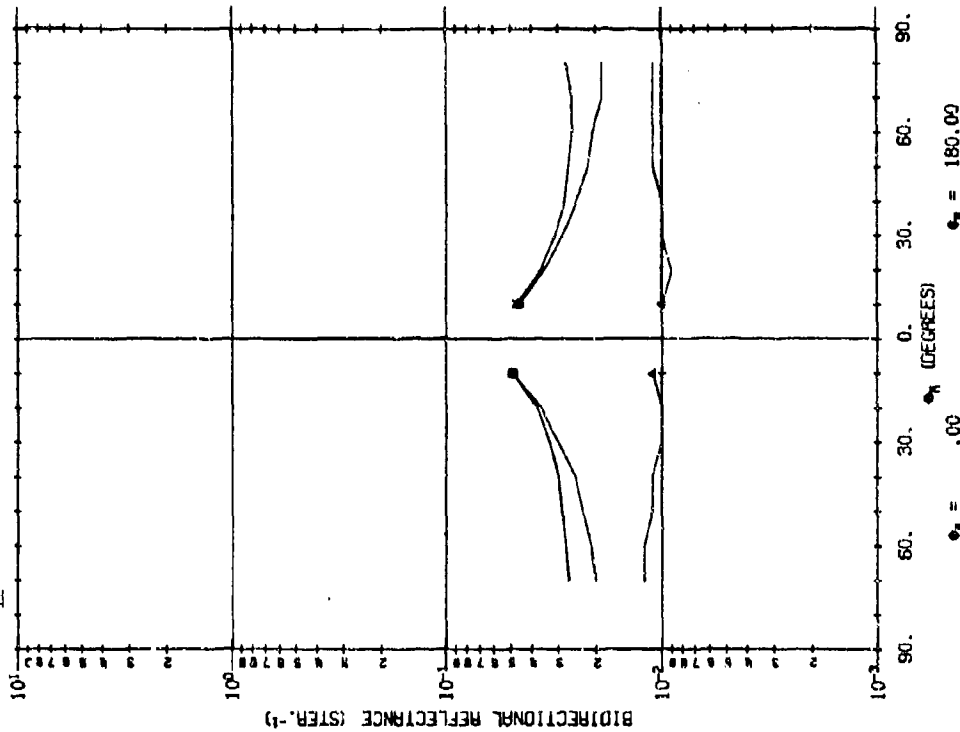
0 || 23 = 7.0
+ || 41 = 4x
Δ || 3 = 0.63
X ||



R01342 005

OLIVE DRAB PAINT ON METAL

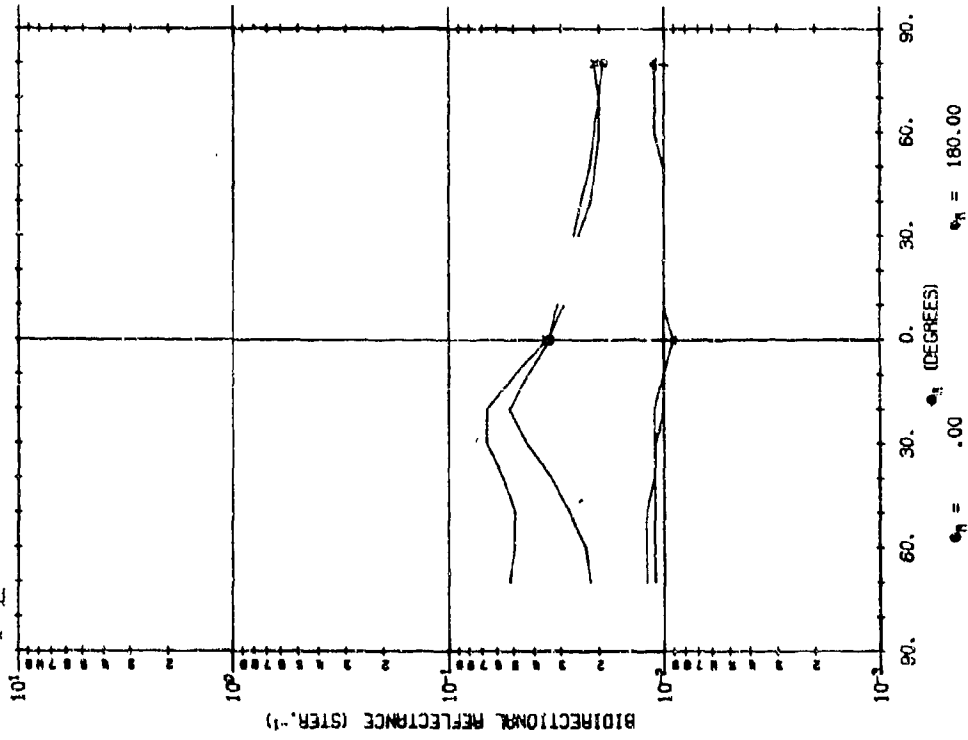
0 || 23 = 0.0
+ || 41 = 180.00
Δ || 3 = 0.63
X ||



A01342 C05

Olive Drab Paint on Metal

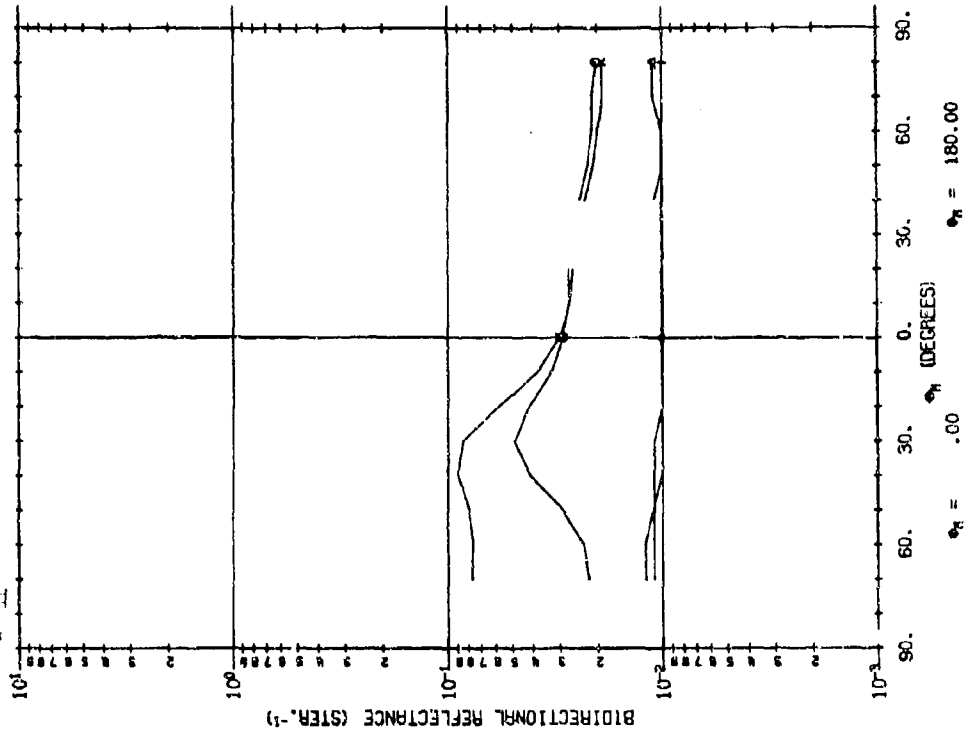
0 | | $\theta_1 = 20.00$
+ | | $\theta_2 = 180.00$
Δ | | $\lambda = 0.63$
x | |



A01342 C05

Olive Drab Paint on Metal

0 | | $\theta_1 = 30.00$
+ | | $\theta_2 = 180.00$
Δ | | $\lambda = 0.63$
x | |

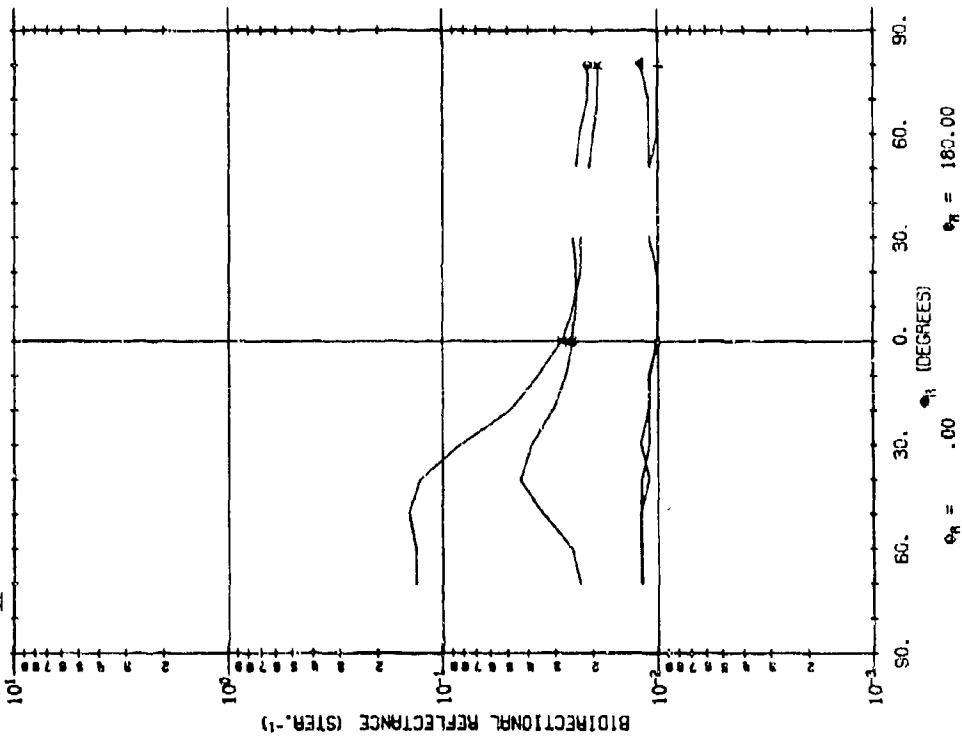


PAINT

A01342 005

Olive Drab Paint on Metal

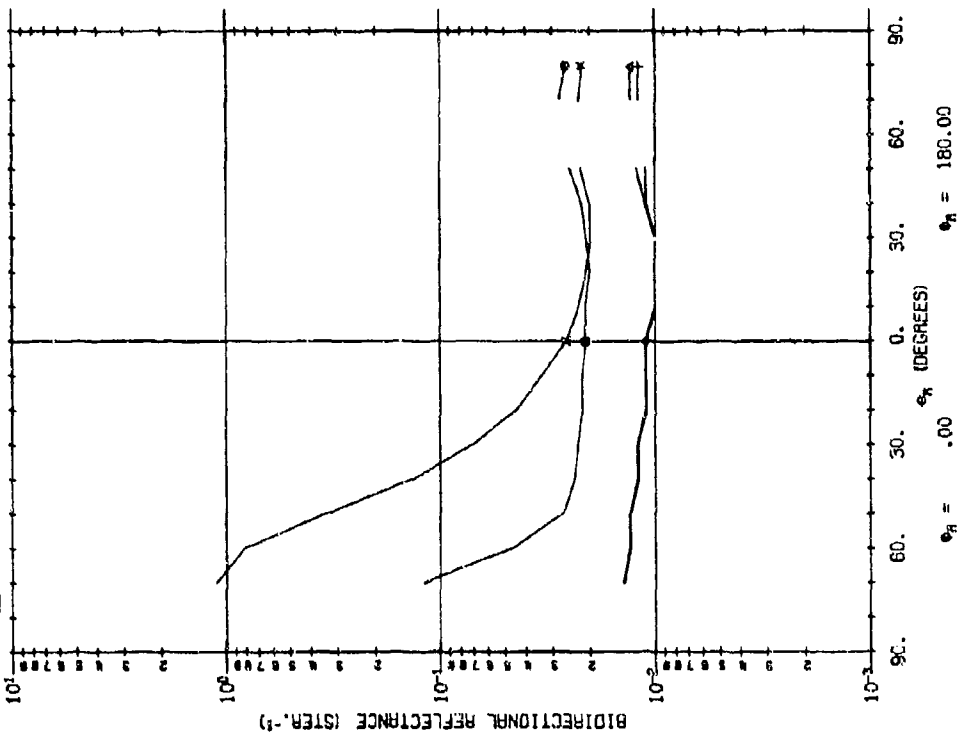
0 40.00
+ 1 180.00
Δ 1 0.63
x 1



A01342 005

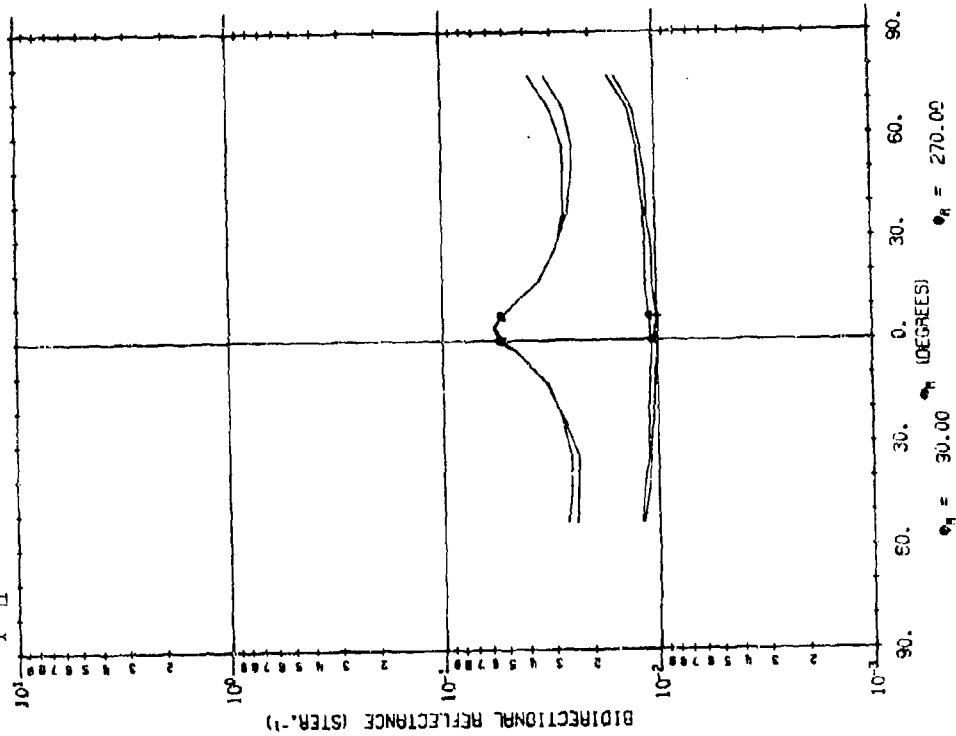
Olive Drab Paint on Metal

0 60.00
+ 1 180.00
Δ 1 0.63
x 1



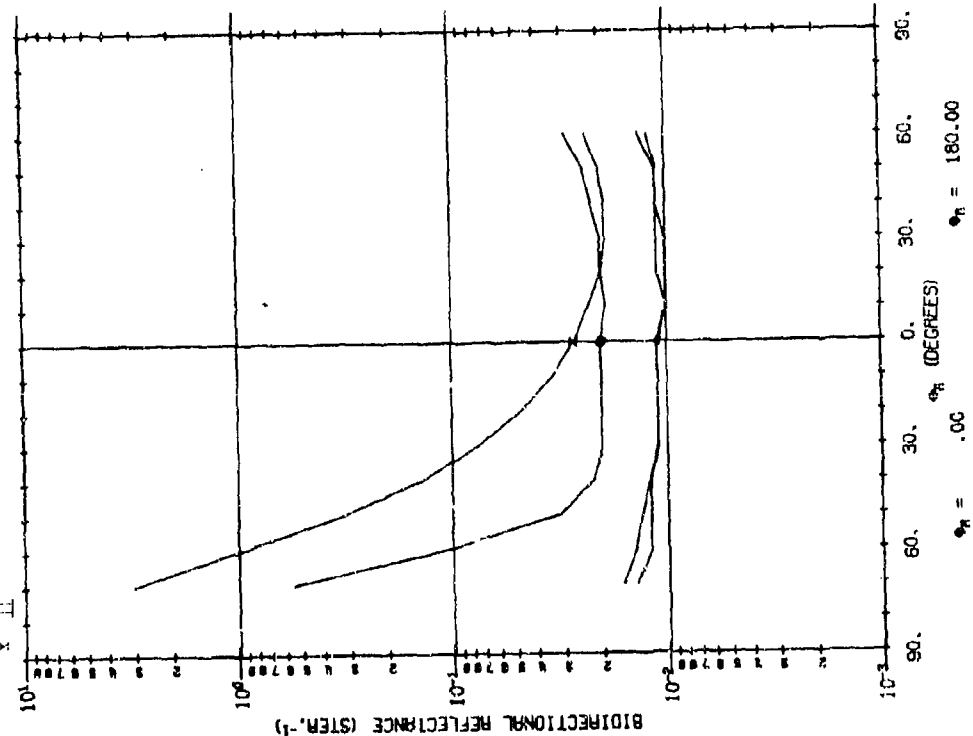
AO1342 005
 OLIVE DRAB PAINT ON METAL

$\phi_1 = 7.0$
 $\phi_2 =$
 $\lambda = 0.63$



AO1342 005
 OLIVE DRAB PAINT ON METAL

$\phi_1 = 70.00$
 $\phi_2 = 180.00$
 $\lambda = 0.63$



PAINT

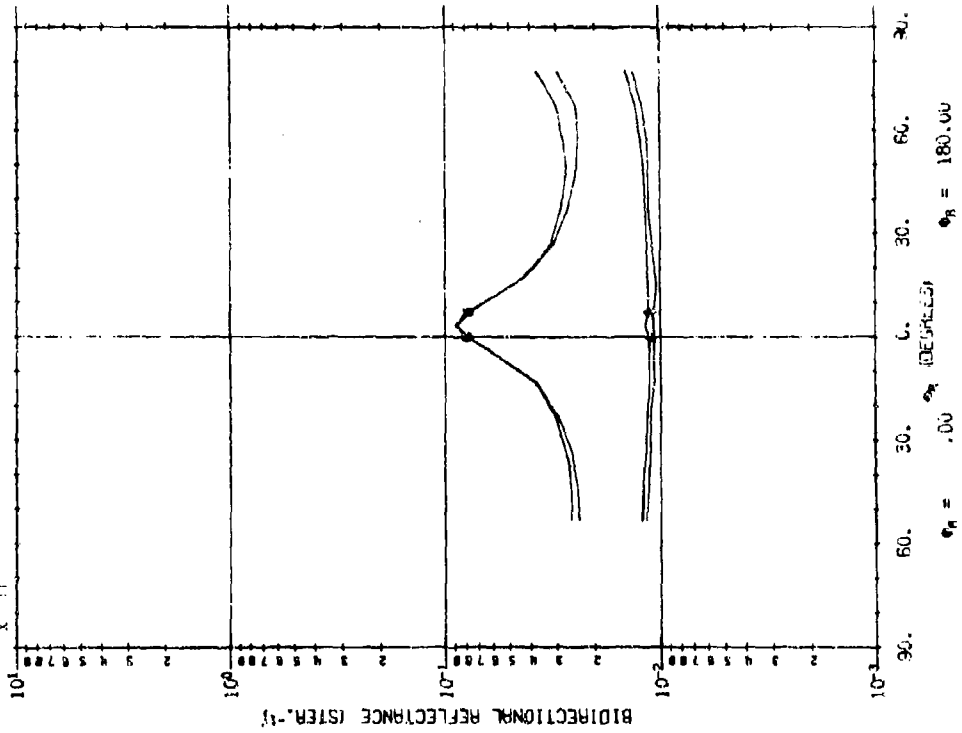
A01313 004

OLIVE DRAB PAINT ON METAL

$2\theta = 7.0$

$\lambda_1 = 0.63$
 $\lambda_2 = 0.63$

0 ||
+ ||
x ||



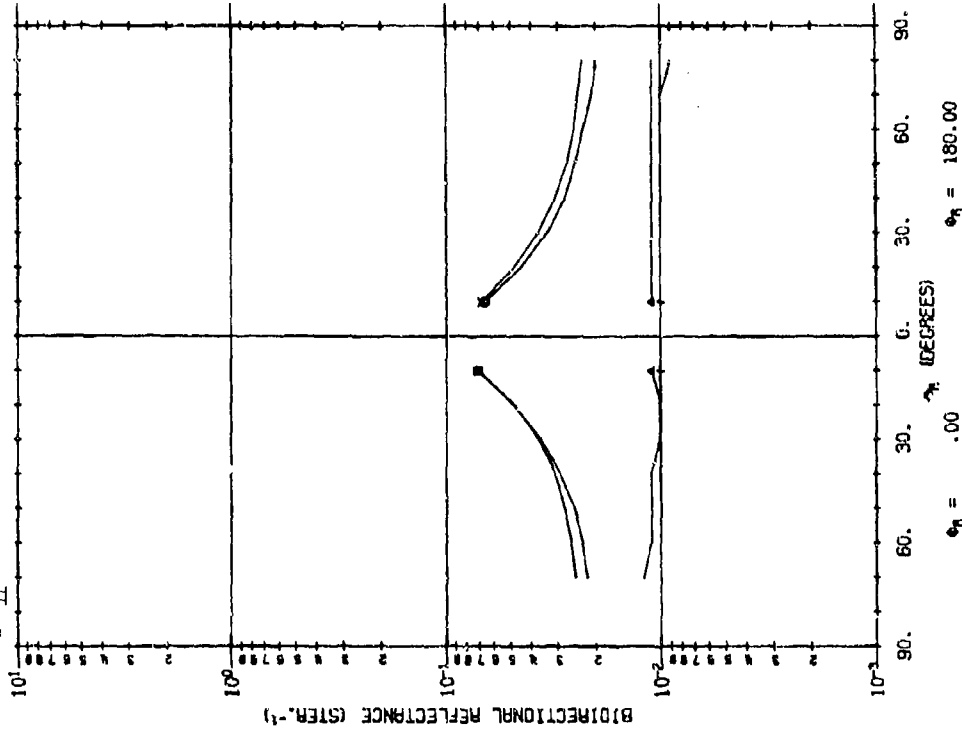
A01343 004

OLIVE DRAB PAINT ON METAL

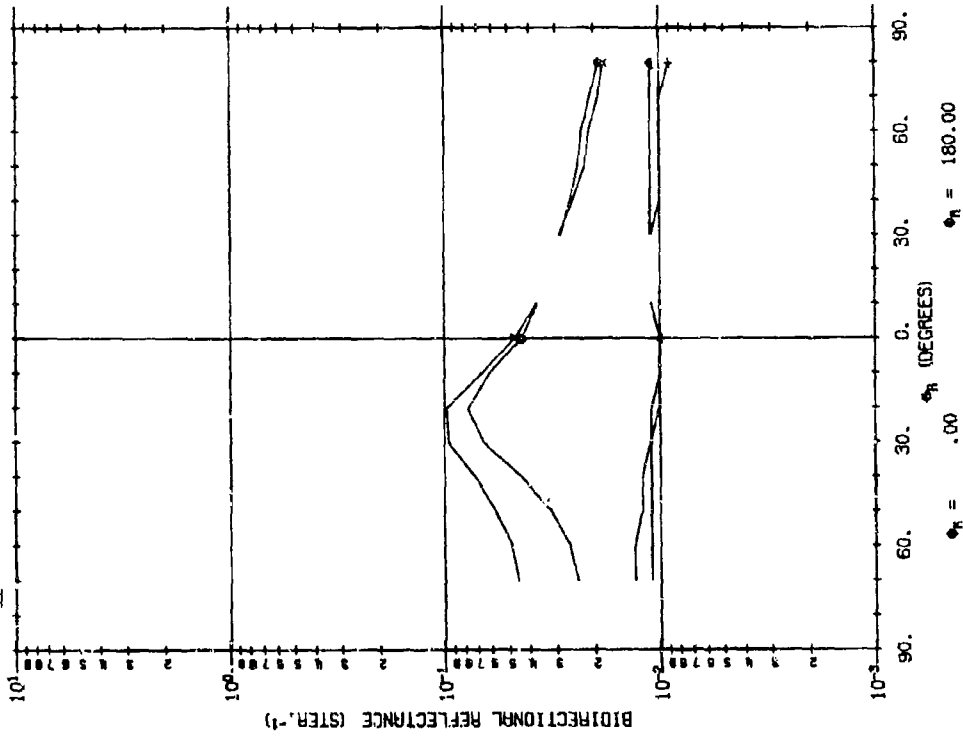
$2\theta = 0.0$

$\lambda_1 = 0.63$
 $\lambda_2 = 0.63$

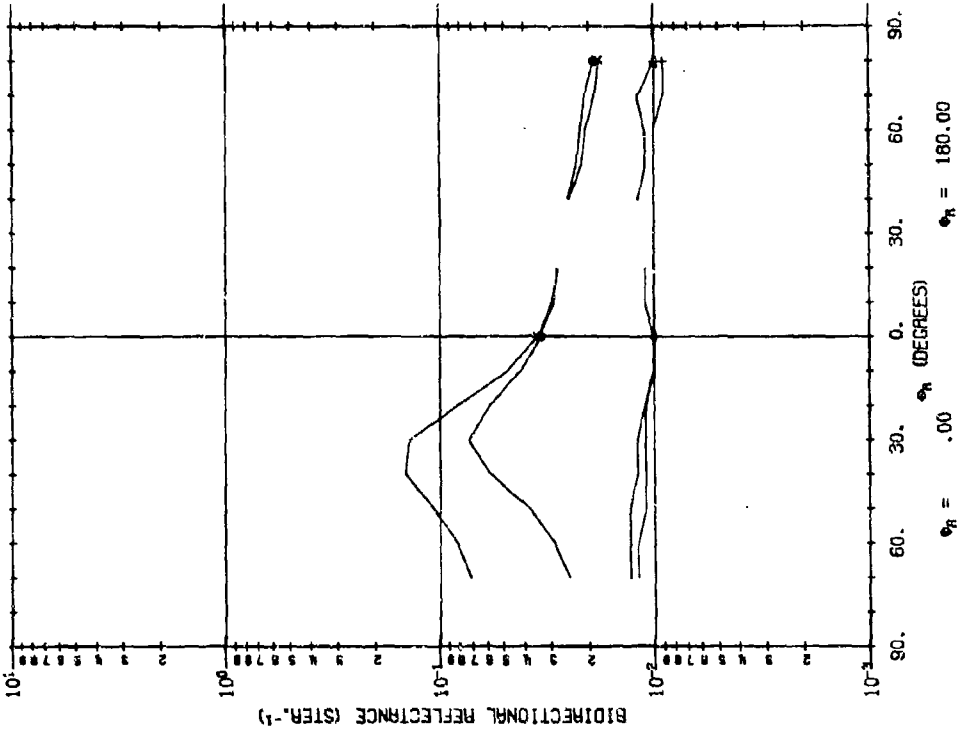
0 ||
+ ||
x ||



A01343 004
 Olive Drab Paint on Metal
 $\rho_1 = 20.00$
 $\rho_2 = 180.00$
 $\lambda = 0.63$



A01343 004
 Olive Drab Paint on Metal
 $\rho_1 = 30.00$
 $\rho_2 = 180.00$
 $\lambda = 0.63$

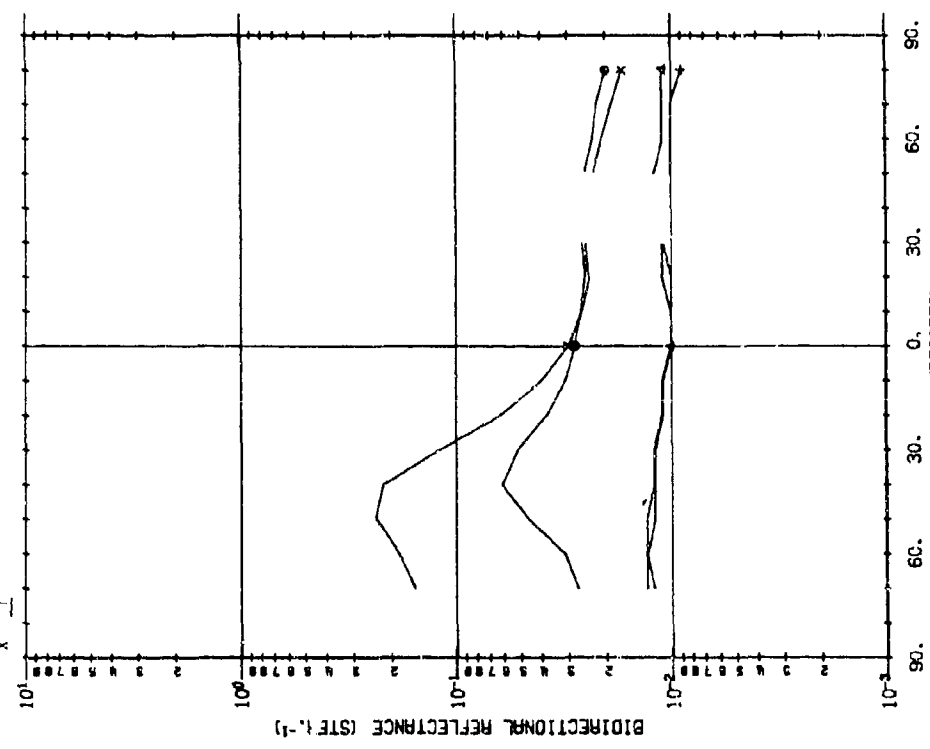


PAINT

A01343 004
 0 1 2 3 4 5 6 7 8 9
 + 1 2 3 4 5 6 7 8 9
 Δ 1 2 3 4 5 6 7 8 9
 X 1 2 3 4 5 6 7 8 9

Olive Drab Paint on Metal

40.00
 180.00
 0.63

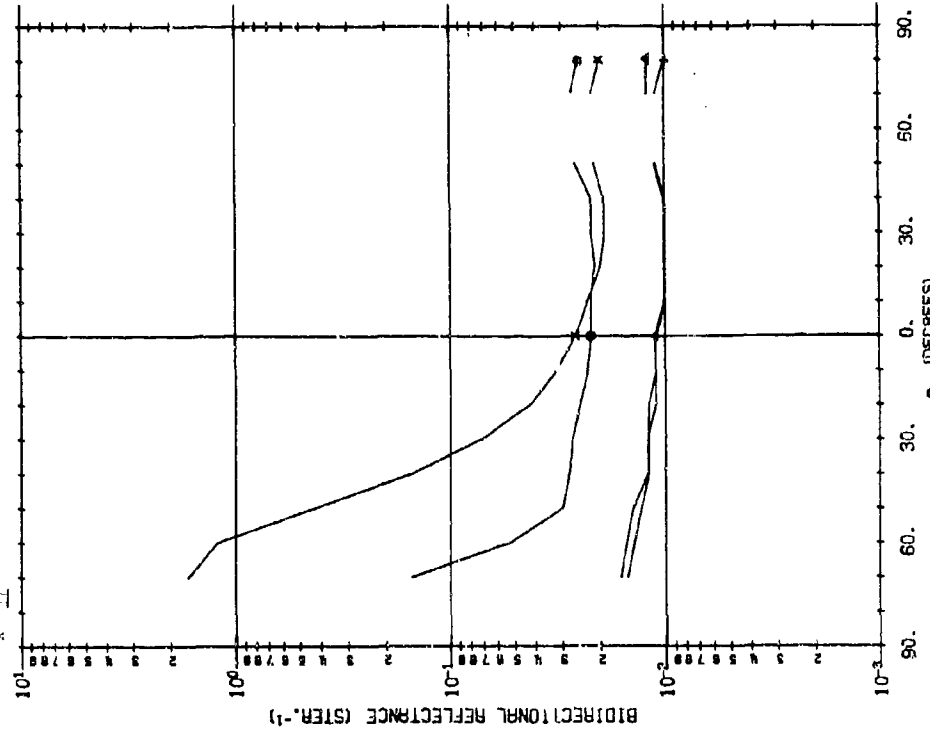


$\phi_n = 0.00$ $\phi_n = 180.00$

A01343 004
 0 1 2 3 4 5 6 7 8 9
 + 1 2 3 4 5 6 7 8 9
 Δ 1 2 3 4 5 6 7 8 9
 X 1 2 3 4 5 6 7 8 9

Olive Drab Paint on Metal

60.00
 180.00
 0.63

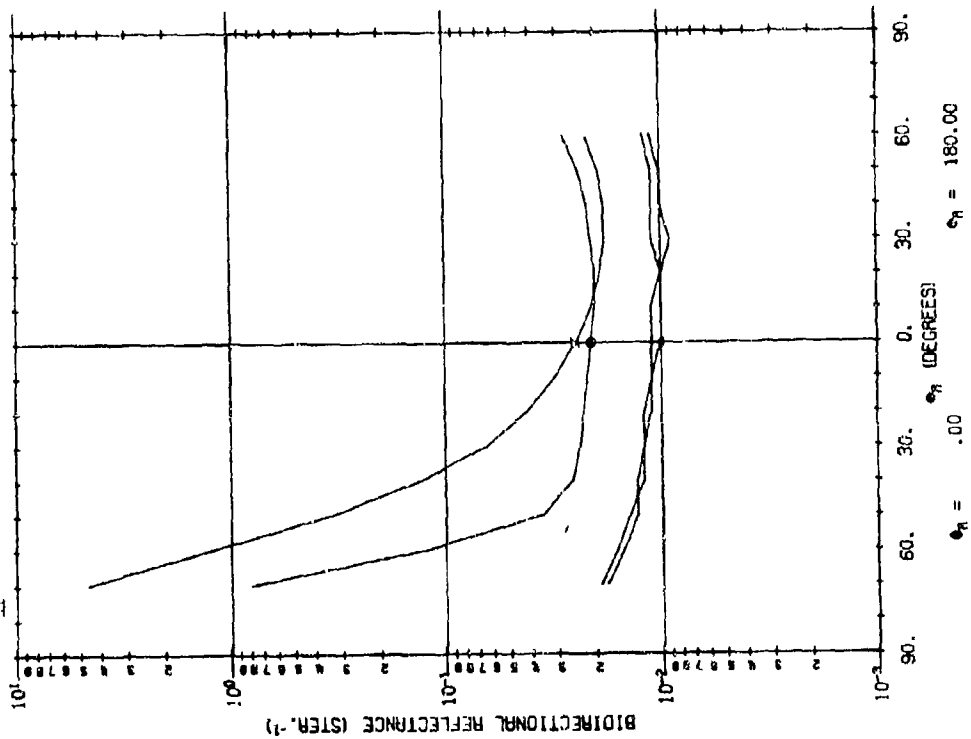


$\phi_n = 0.00$ $\phi_n = 180.00$

R01343 004

Olive Drab Paint on Metal

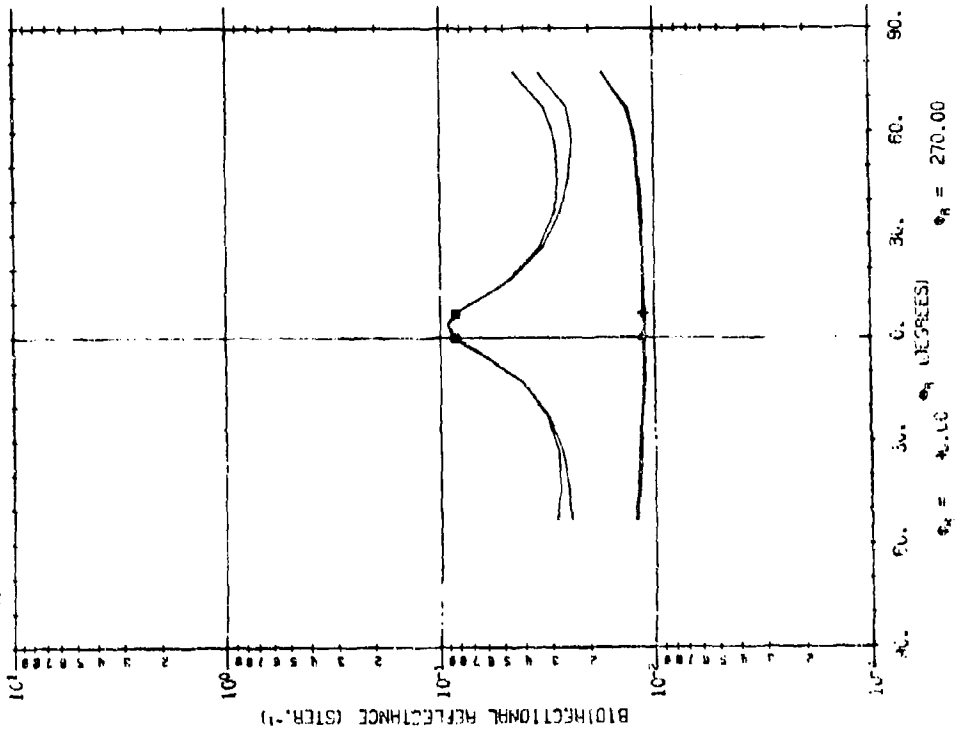
$\epsilon_1 = 70.00$
 $\epsilon_2 = 180.00$
 $\lambda = 0.63$



R01343 004

OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 7.0$
 $\epsilon_2 = 0.63$

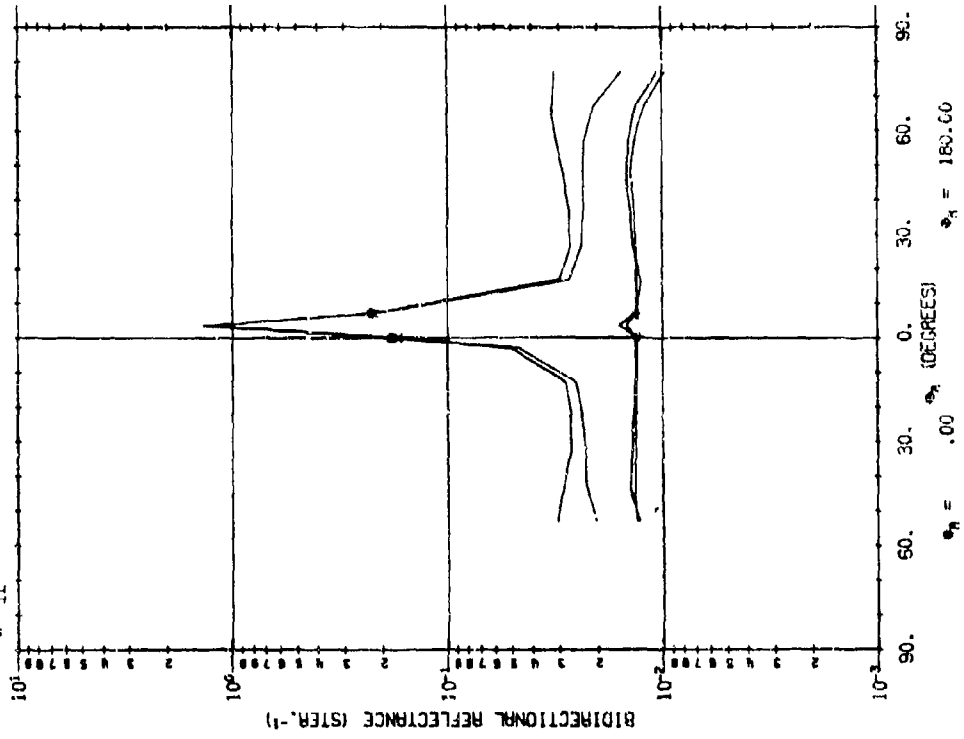


PAIN

001444 004

BLUE PAINT ON METAL

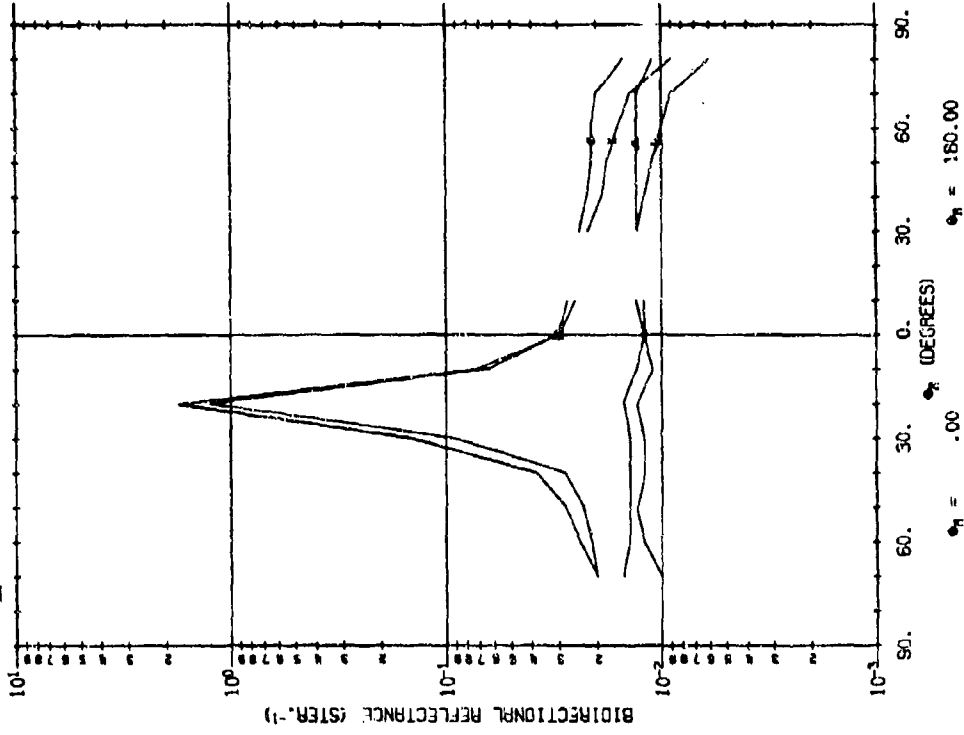
0 11 2E - 7.0
+ 11 41 - 4x
x 11 1 - 0.63



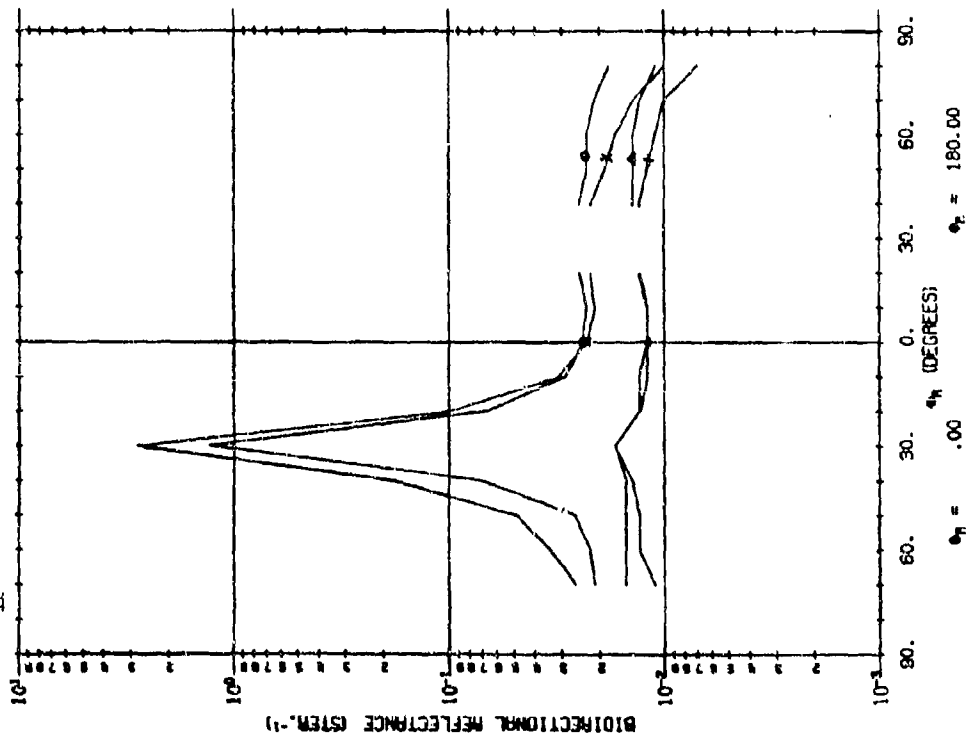
001444 004

Blue Paint on Metal

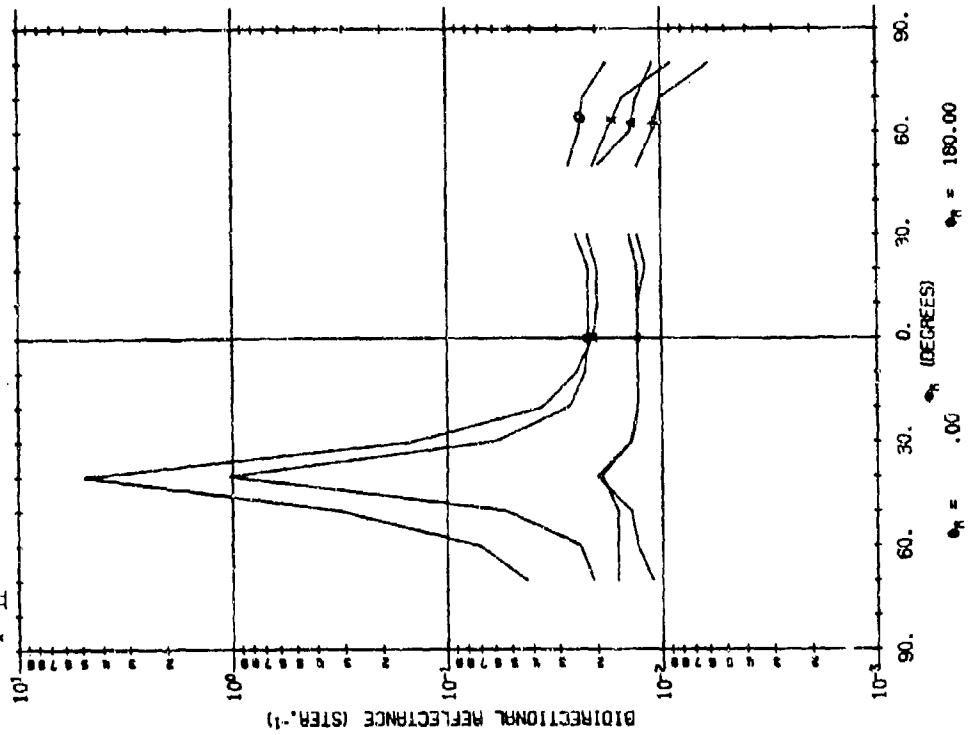
0 11 2E - 25.00
+ 11 41 - 180.0
x 11 1 - .63



R01444 004
 Blue Paint on Metal
 $\epsilon_1 = 30.0$
 $\epsilon_2 = 180.0$
 $\lambda = .63$



R01444 004
 Blue Paint on Metal
 $\epsilon_1 = 40.0$
 $\epsilon_2 = 180.0$
 $\lambda = .63$

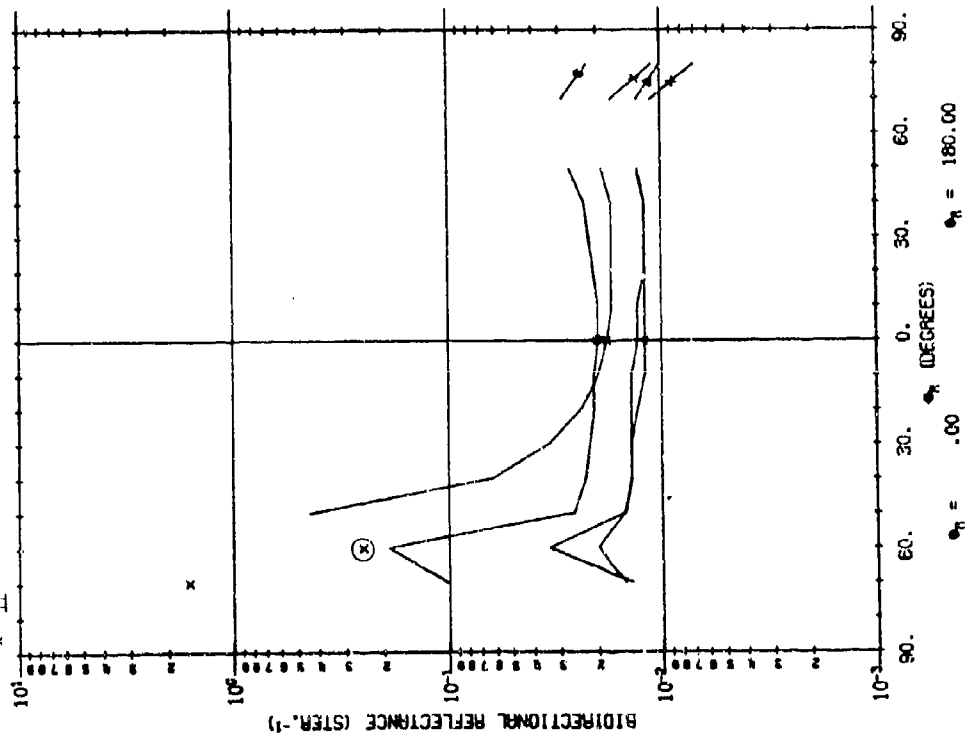


PAINT

AO1444 004

Blue Paint on Metal

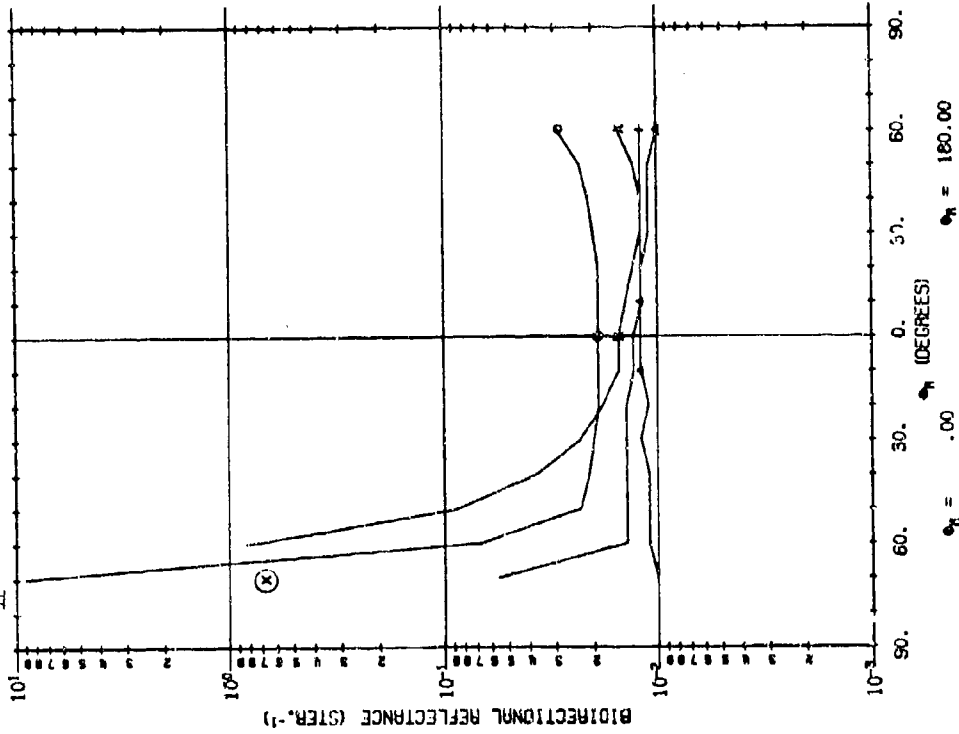
0 $\theta_1 = 60.0$
 + $\theta_2 = 180.0$
 x $\lambda = .63$



AO1444 004

Blue Paint on Metal

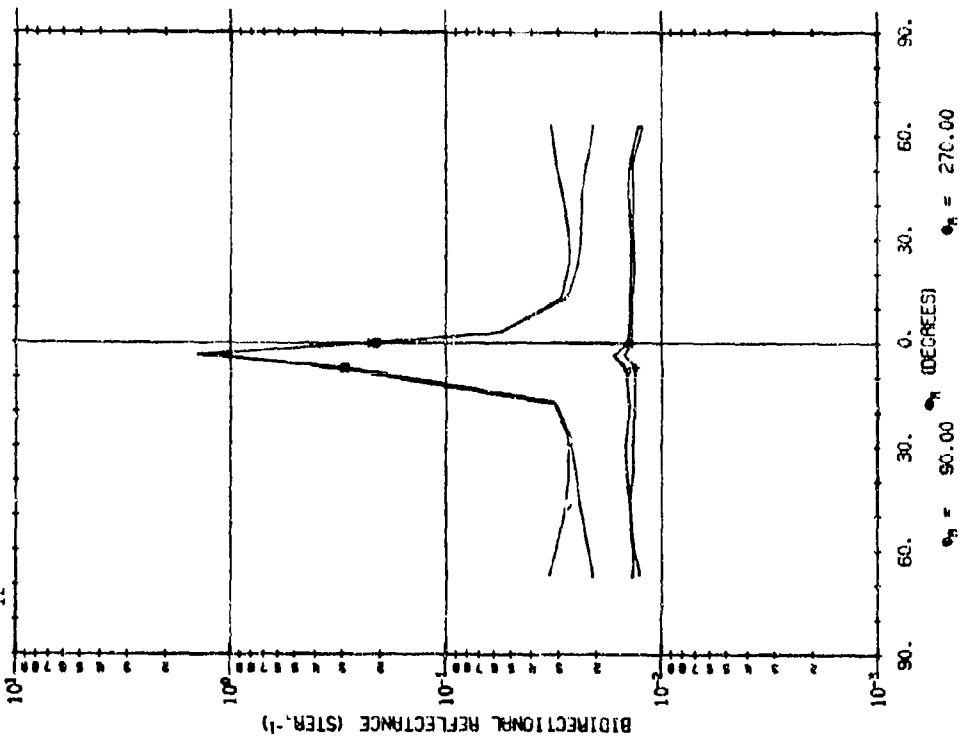
0 $\theta_1 = 70.0$
 + $\theta_2 = 180.0$
 x $\lambda = .63$



004

BLUE PAINT ON METAL

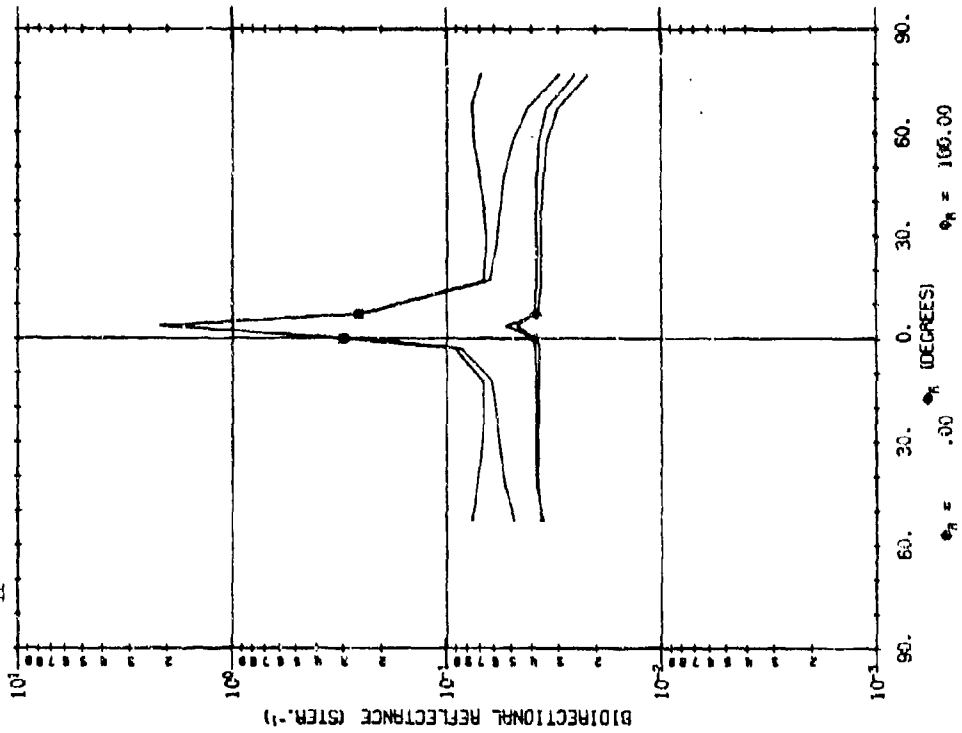
0 || 2θ = 7.0
+ || φ_i = φ_r
Δ || λ = 0.63
X ||



005

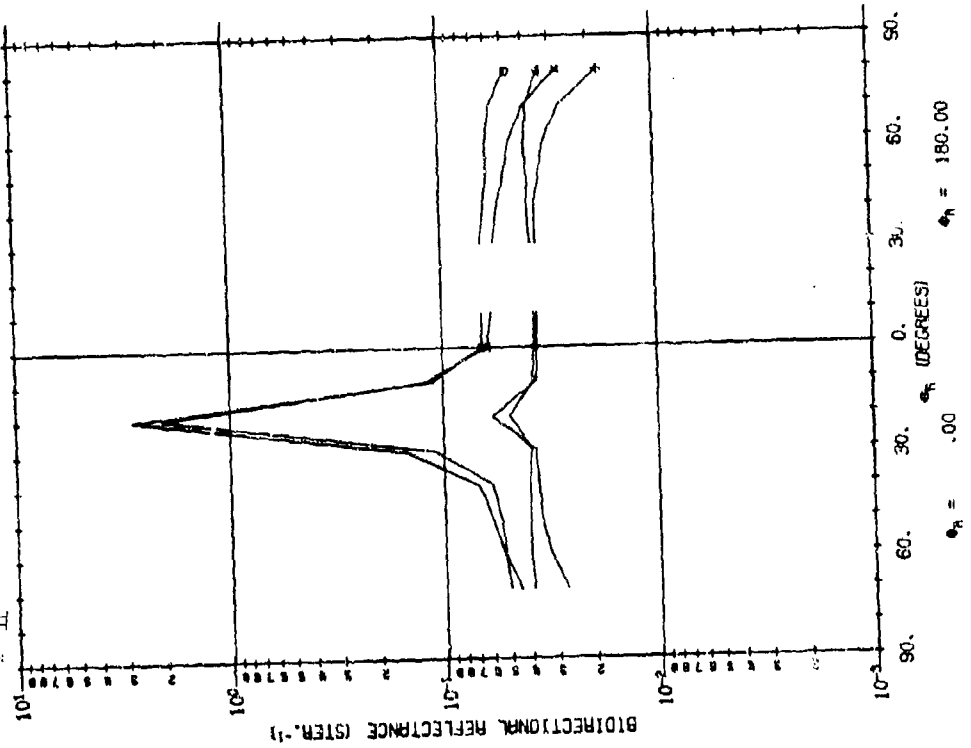
BLUE PAINT ON METAL

0 || 2θ = 7.0
+ || φ_i = φ_r
Δ || λ = 1.06
X ||

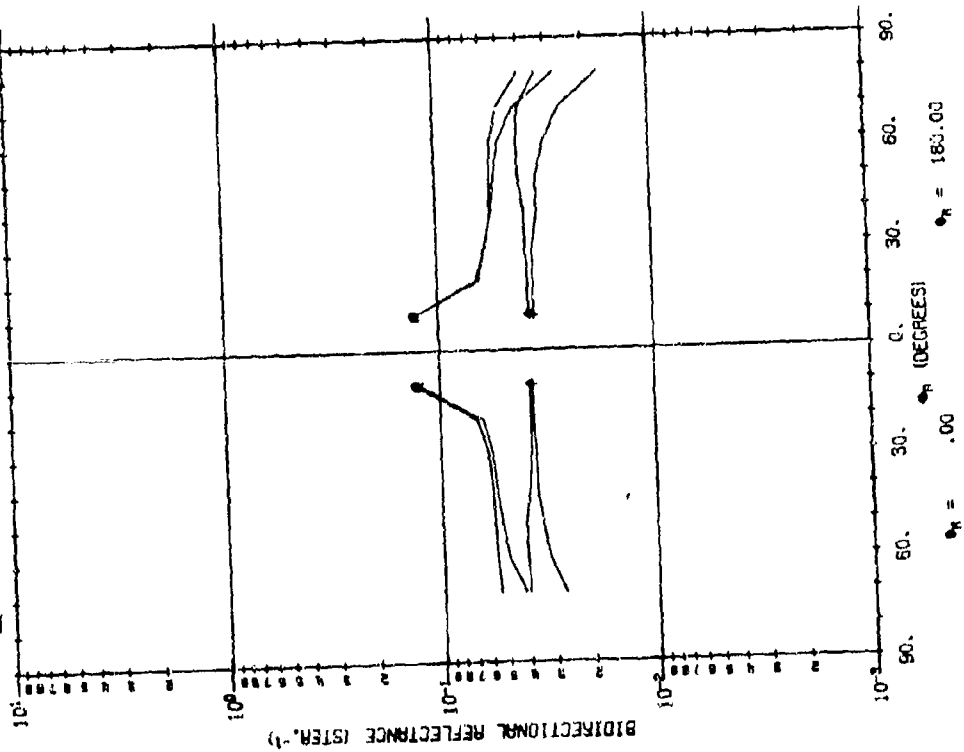


PAINT

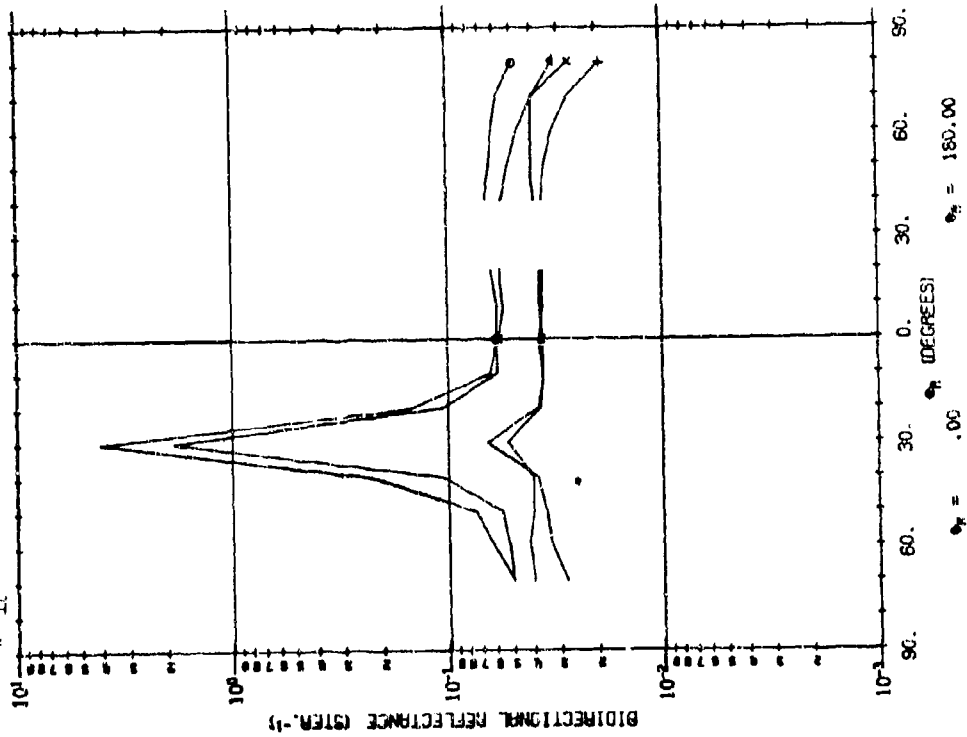
005
 Blue Paint on Metal
 $\epsilon_1 = 20.00$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$



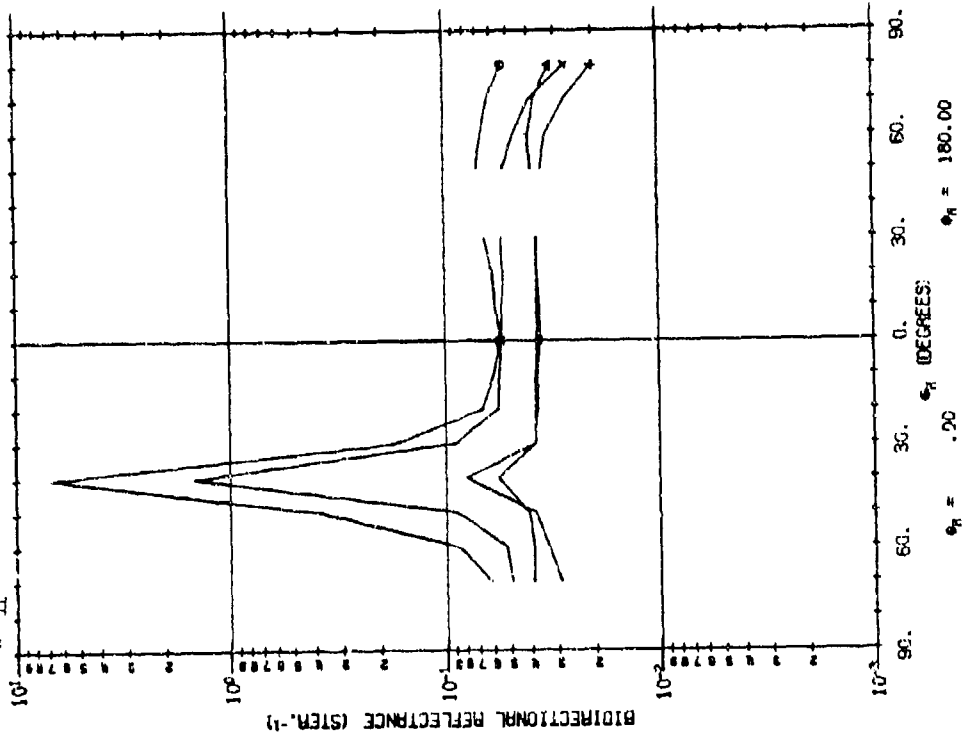
005
 Blue Paint on Metal
 $\epsilon_1 = 0.0$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$



RG1444 005
 Blue Paint on Metal
 $r_1 = 30.00$
 $\theta_1 = 180.00$
 $\lambda = 1.06$



RG1444 005
 Blue Paint on Metal
 $r_1 = 40.00$
 $\theta_1 = 180.00$
 $\lambda = 1.06$

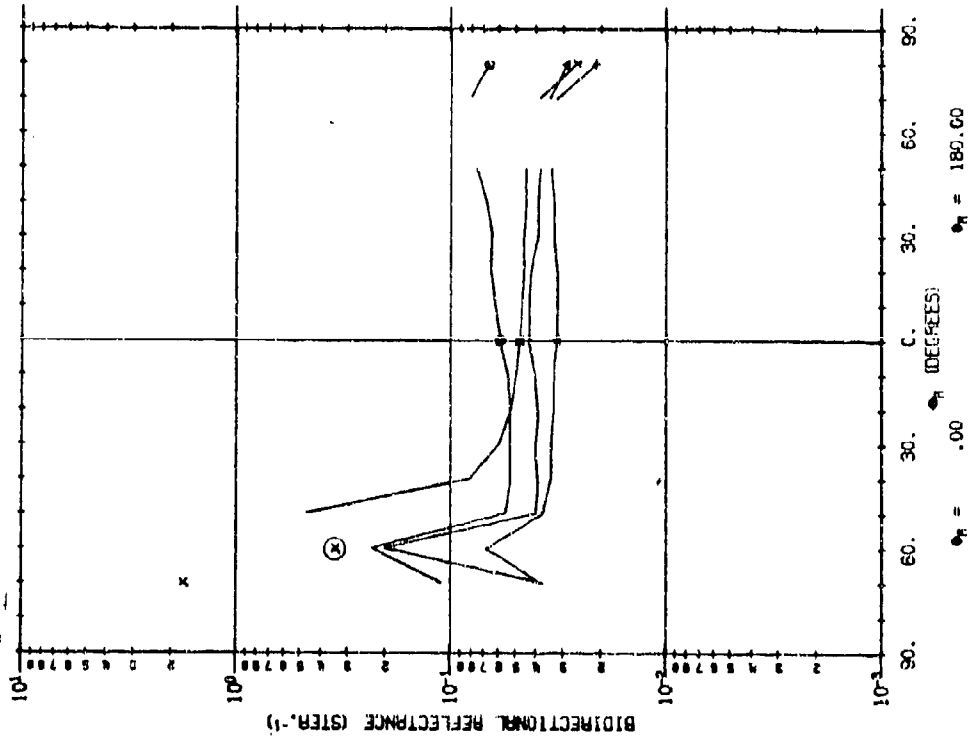


PAINT

AO1444 005

Blue Paint on Metal

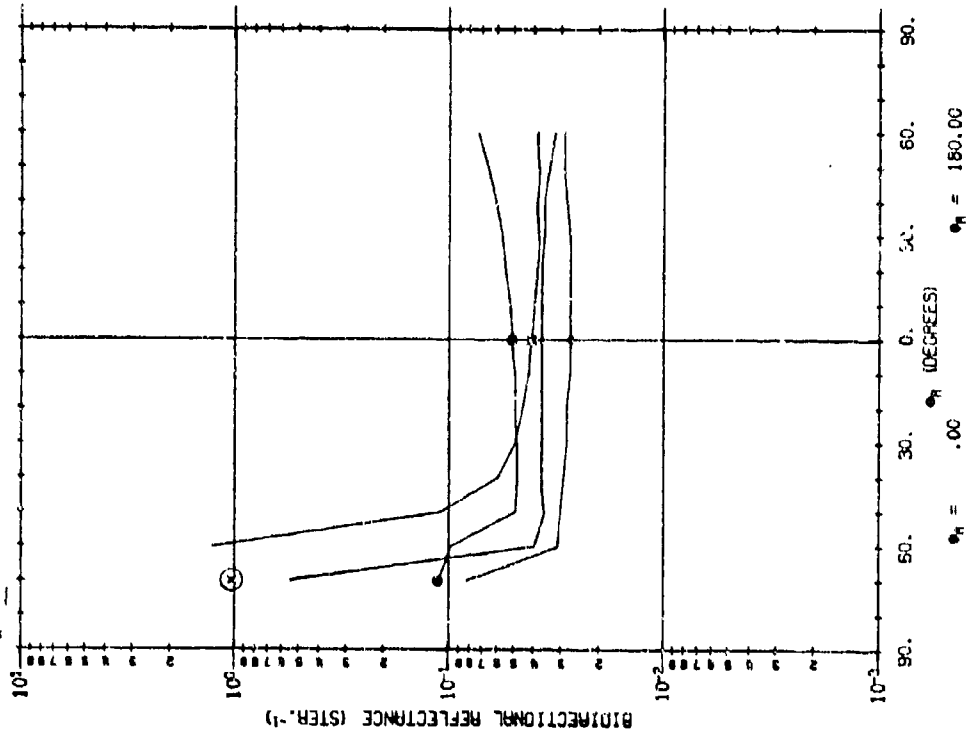
$\theta_i = 50.00$
 $\theta_r = 180.00$
 $\theta_n = 1.06$



AO1444 005

Blue Paint on Metal

$\theta_i = 70.00$
 $\theta_r = 180.00$
 $\theta_n = 1.06$



AO1453 005

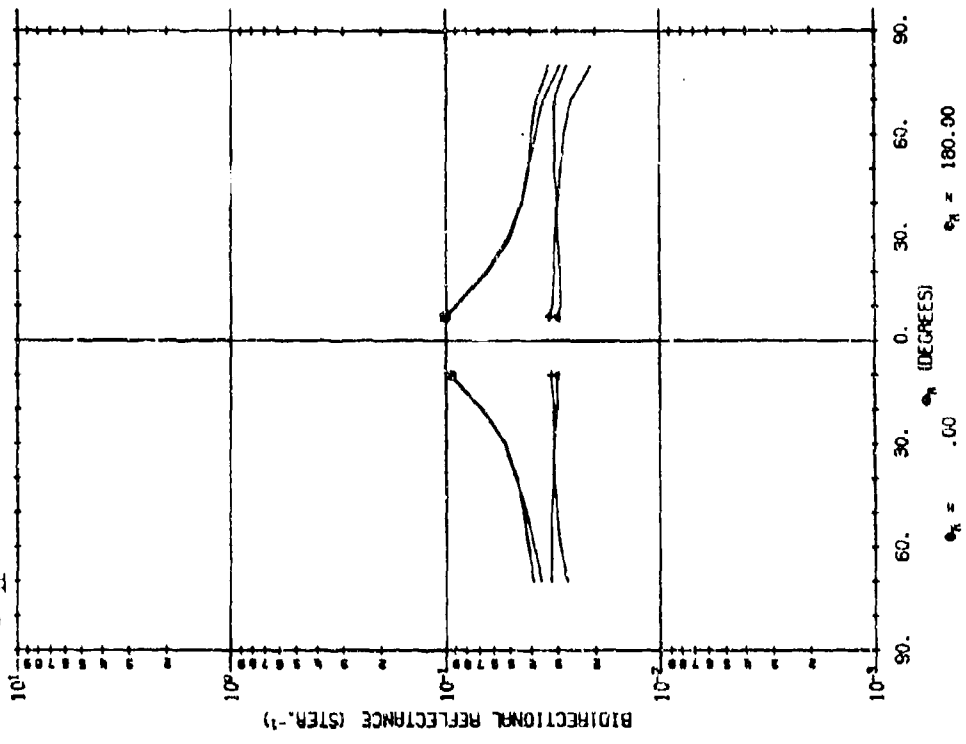
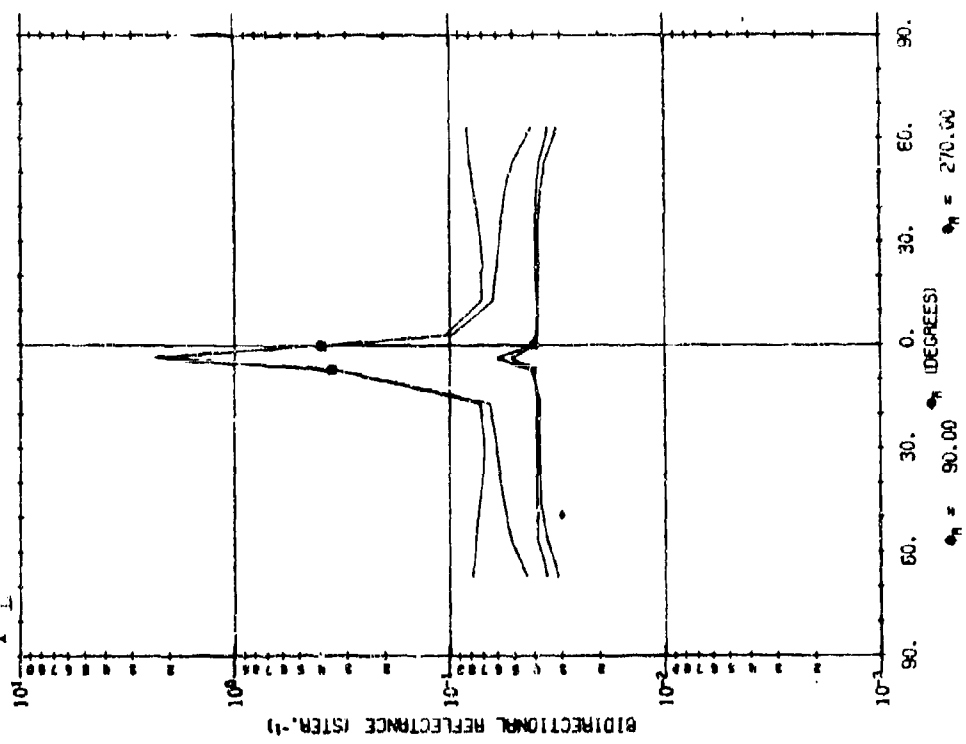
BLUE PAINT ON METAL

$\theta_1 = 7.0$
 $\theta_2 = \theta_1$
 $\theta_3 = 1.06$

AO1453 005

Light Brown Paint on Metal

$\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\theta_3 = 0.63$



PAINT

R01453 005

Light Brown Paint on Metal

$\theta_1 = 20.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

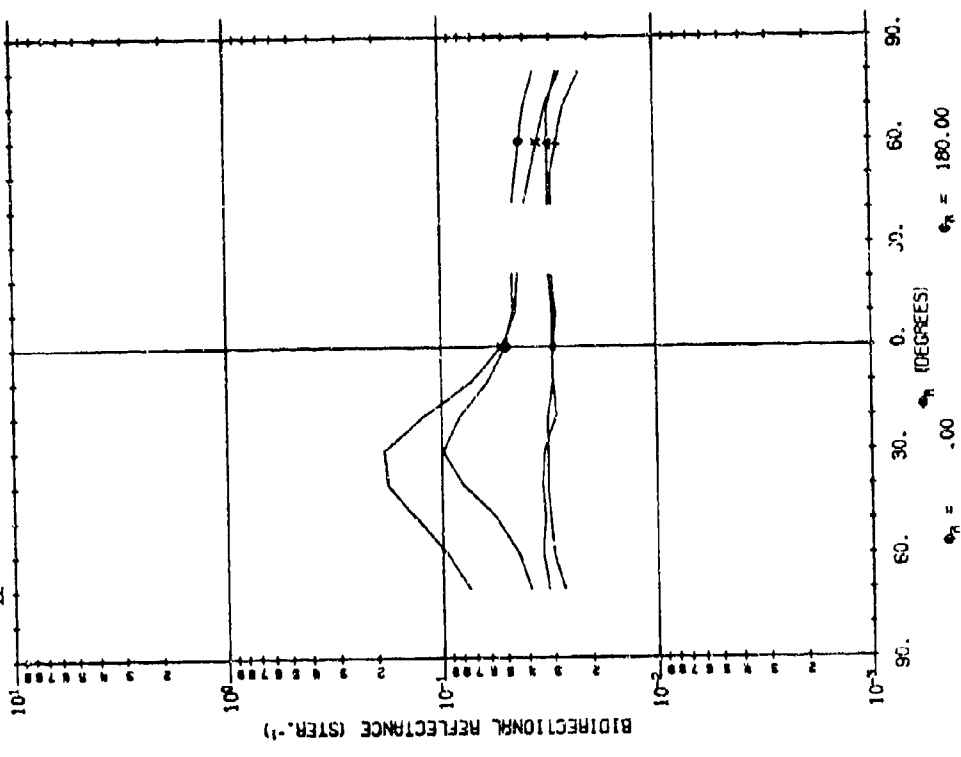
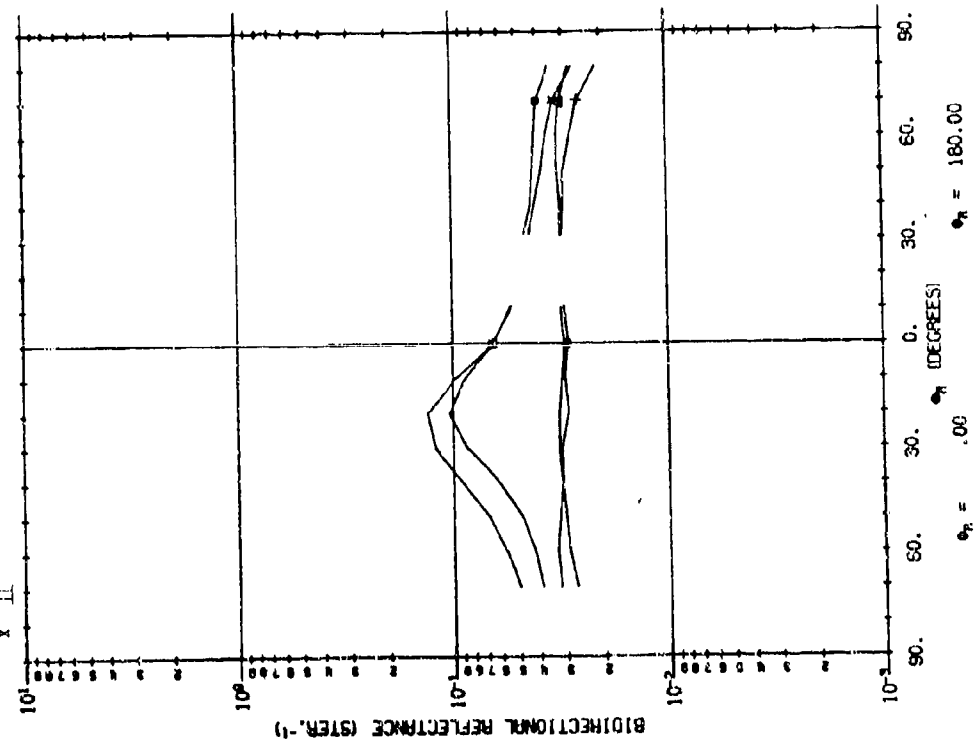
$\theta_1 = 30.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

Light Brown Paint on Metal

R01453 005

Light Brown Paint on Metal

$\theta_1 = 30.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

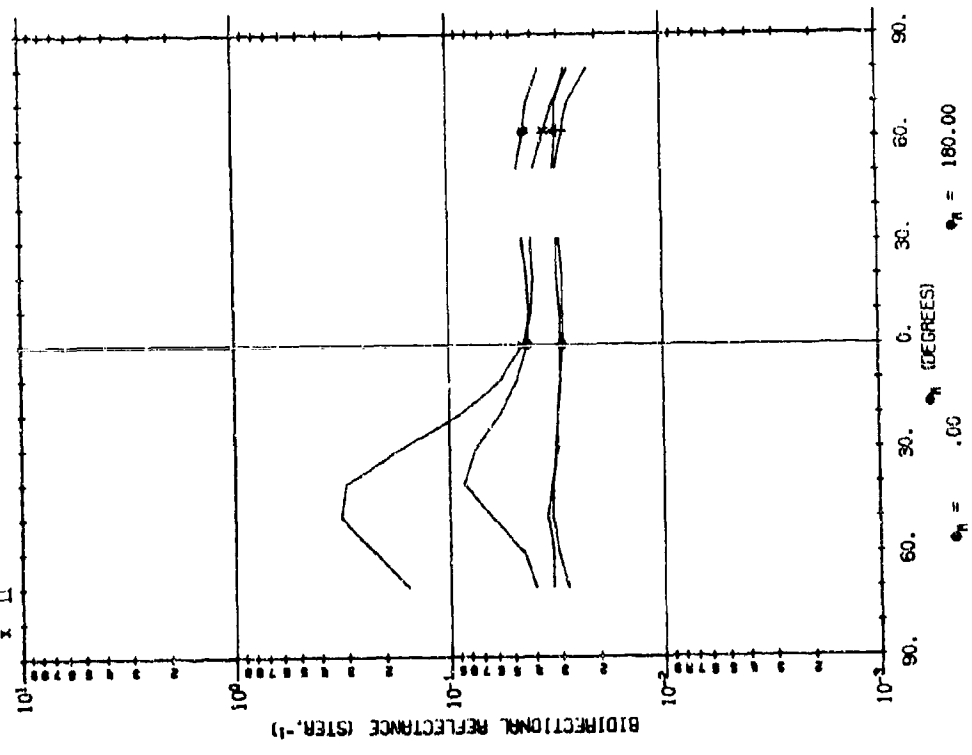


A01453 005

Light Brown Paint on Metal

$\theta_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 II
+ II
- II
x II

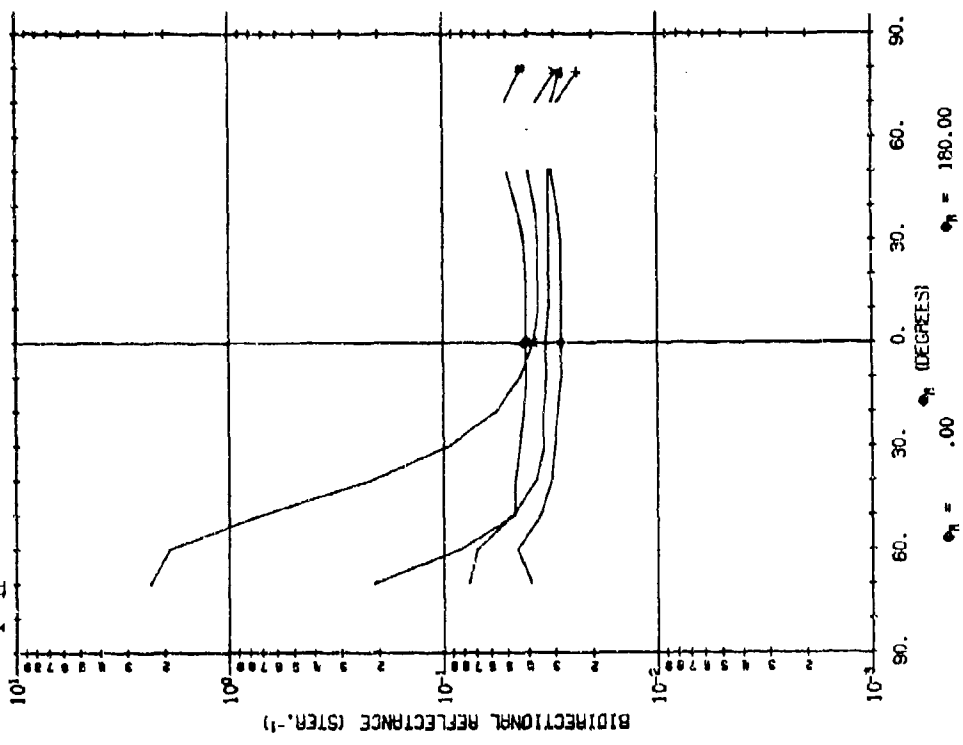


A01453 005

Light Brown Paint on Metal

$\theta_1 = 60.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 II
+ II
- II
x II

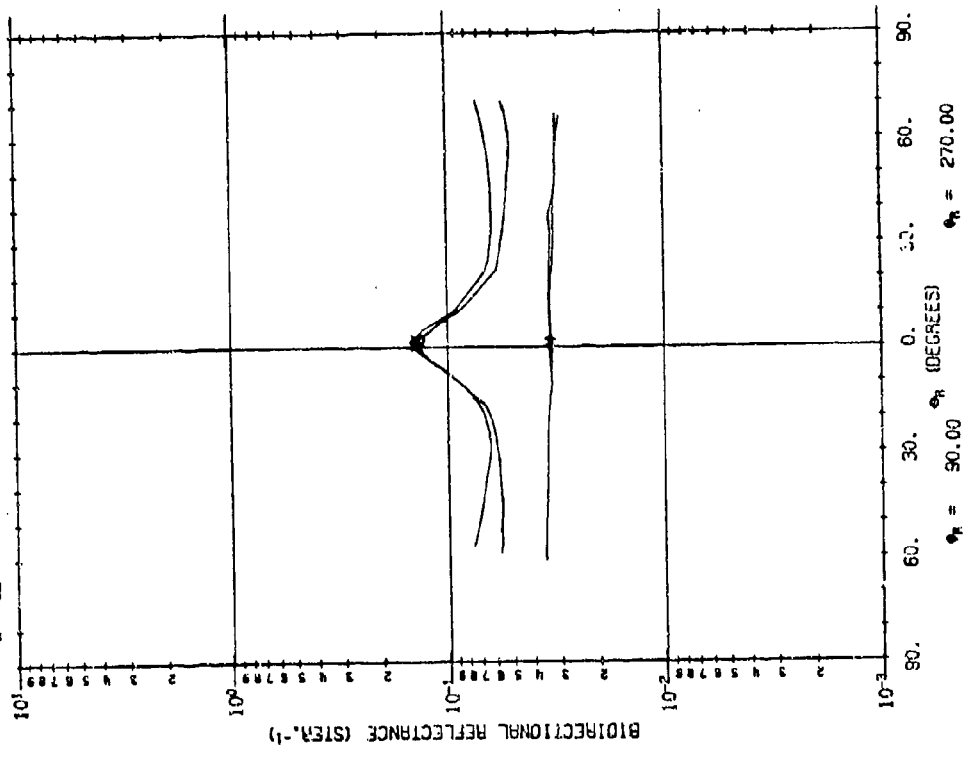


PAINT

A01453 005

LIGHT BROWN PAINT ON METAL

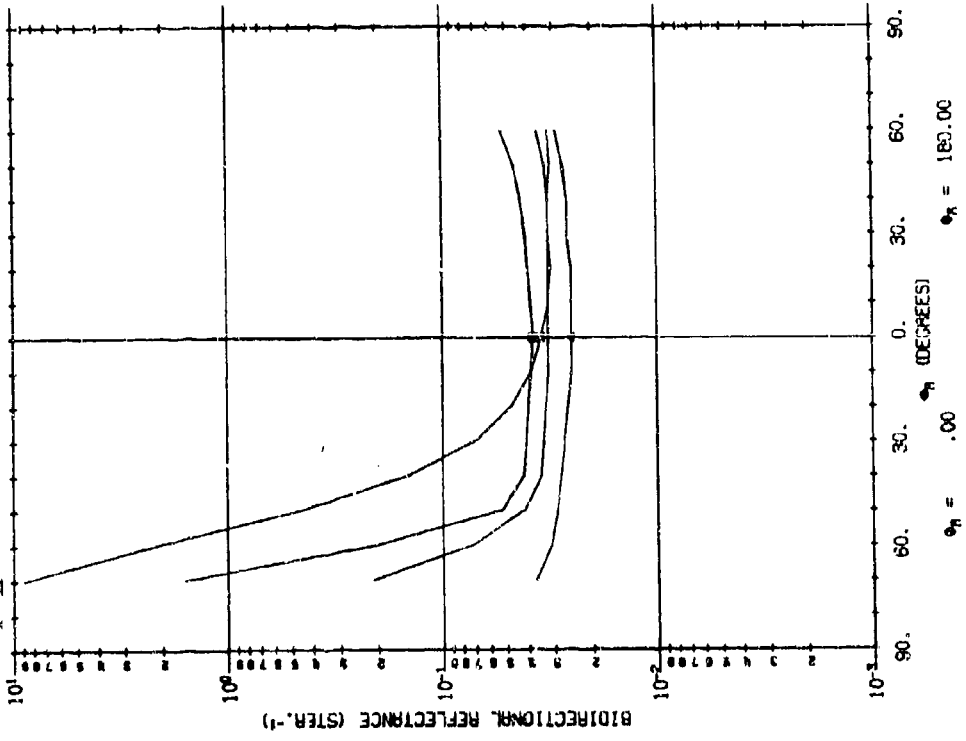
0 || 23 - 2.0
 + || $\phi_1 = \phi_2$
 6 || $\lambda = 0.63$
 X ||



A01453 005

Light Brown Paint on Metal

$\theta_1 = 70.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

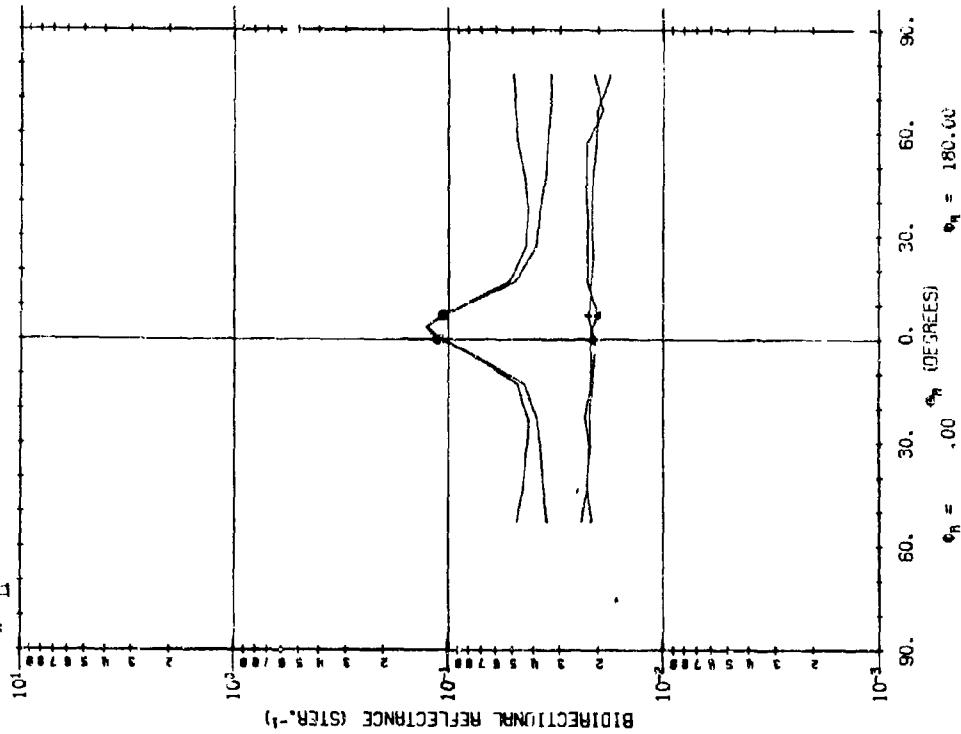


A01453 006

LIGHT BROWN PAINT ON METAL

$\theta_i = 7.0$
 $\theta_s = \theta_r$
 $\lambda = 1.06$

0 ||
+ ||
Δ ||
X ||

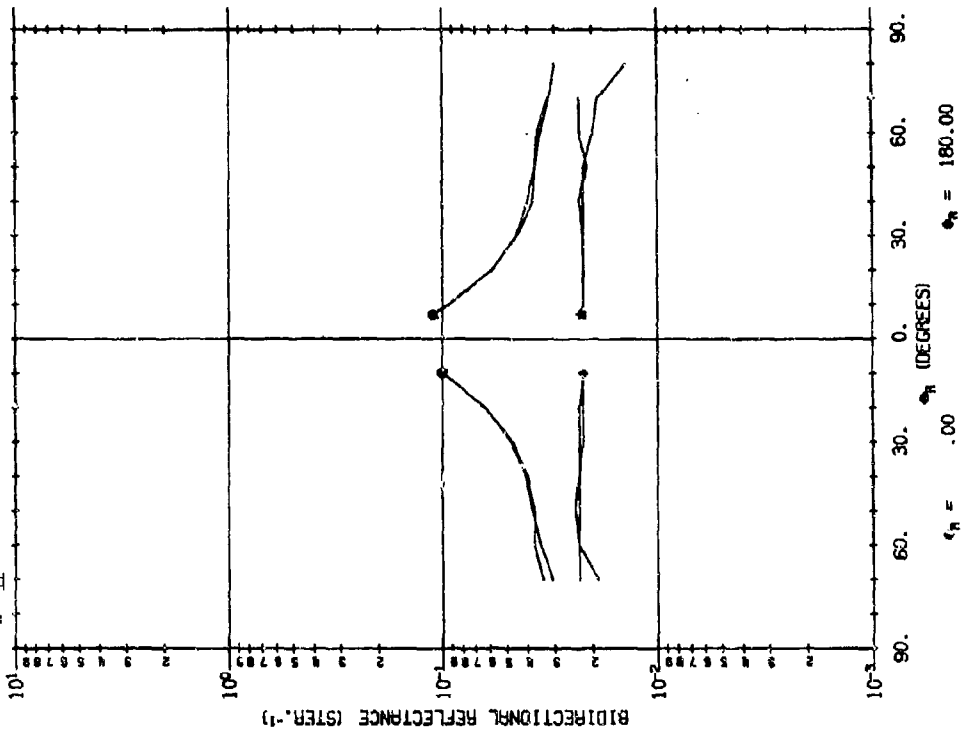


A01453 006

Light Brown Paint on Metal

$\theta_i = 0.0$
 $\theta_s = 180.00$
 $\lambda = 1.06$

0 ||
+ ||
Δ ||
X ||



PAINT

A01453

006

Light Brown Paint on Metal

$\rho_1 = 20.00$

$\phi_1 = 180.00$

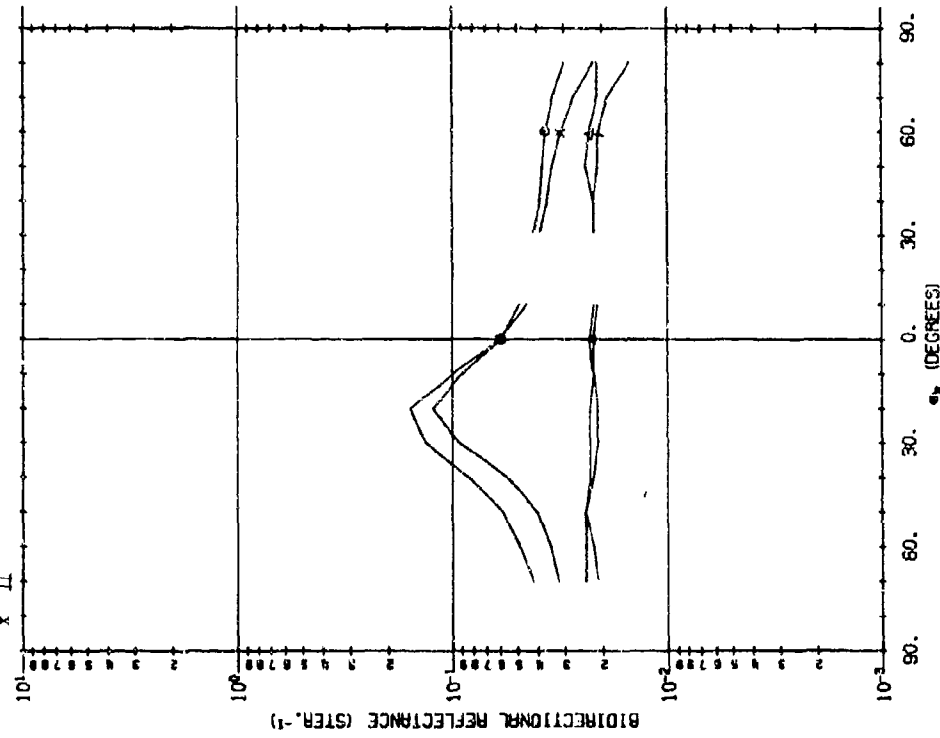
$\lambda = 1.06$

0 ||

+ ||

Δ ||

x ||



A01453

006

Light Brown Paint on Metal

$\rho_1 = 30.00$

$\phi_1 = 180.00$

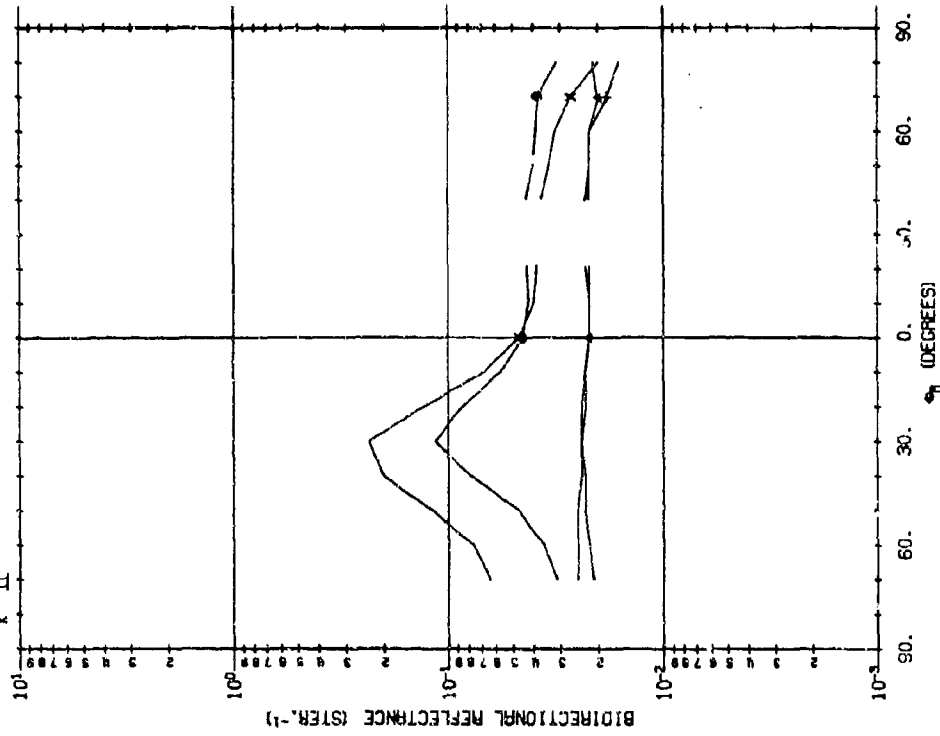
$\lambda = 1.06$

0 ||

+ ||

Δ ||

x ||

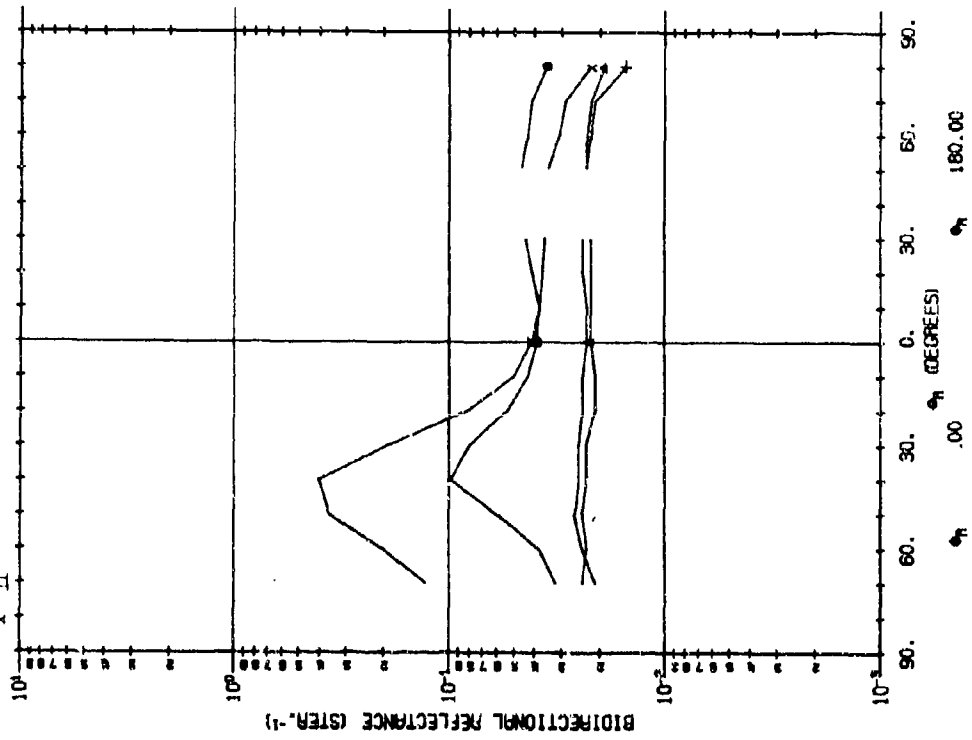


R01453 006

Light Brown Paint on Metal

$\theta_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$

0 ||
+ ||
Δ ||
x ||

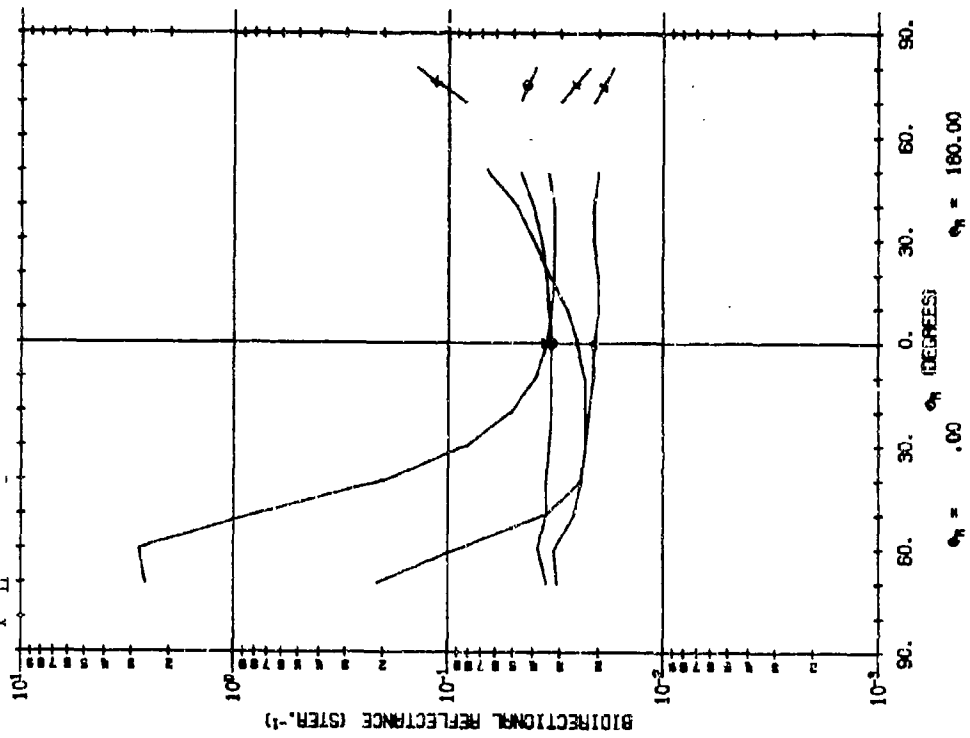


R01453 006

Light Brown Paint on Metal

$\theta_1 = 60.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$

0 ||
+ ||
Δ ||
x ||



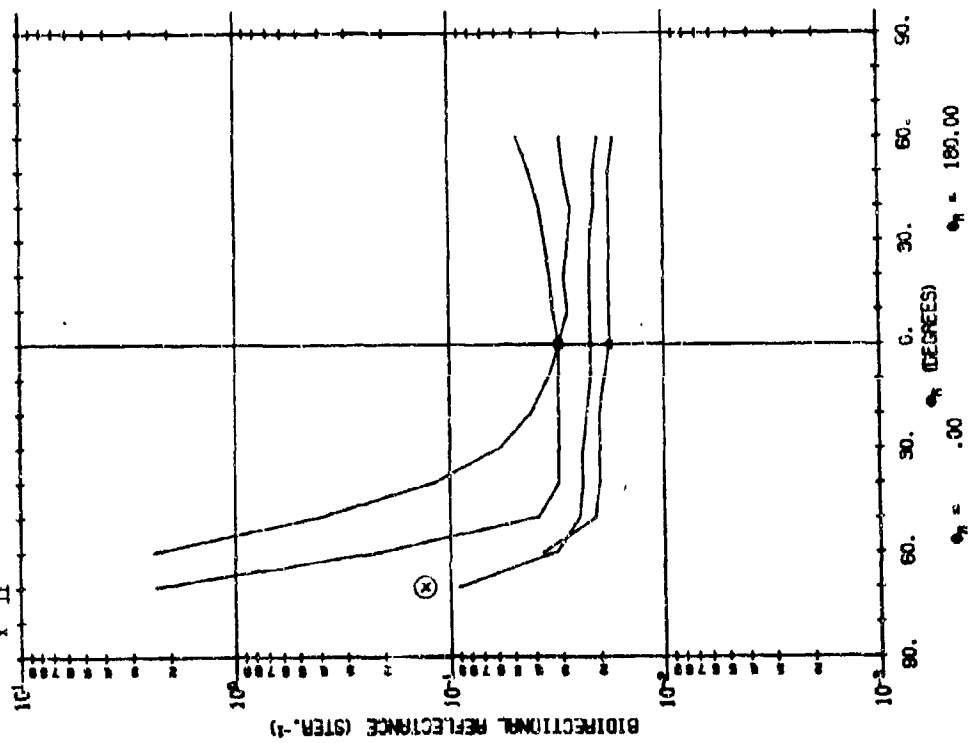
PAINT

A01453 006

Light Brown Paint on Metal

$\theta_1 = 70.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$

0 ||
+ ||
A ||
x ||

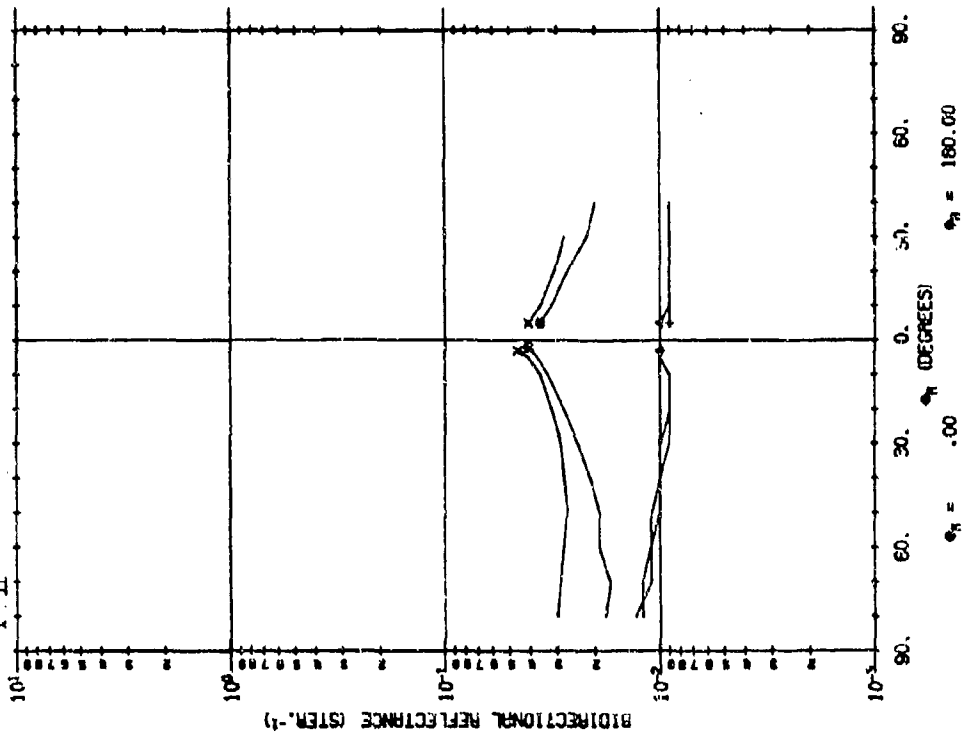


A01454 005

Field Drab Paint on Metal

$\theta_1 = 0.0$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

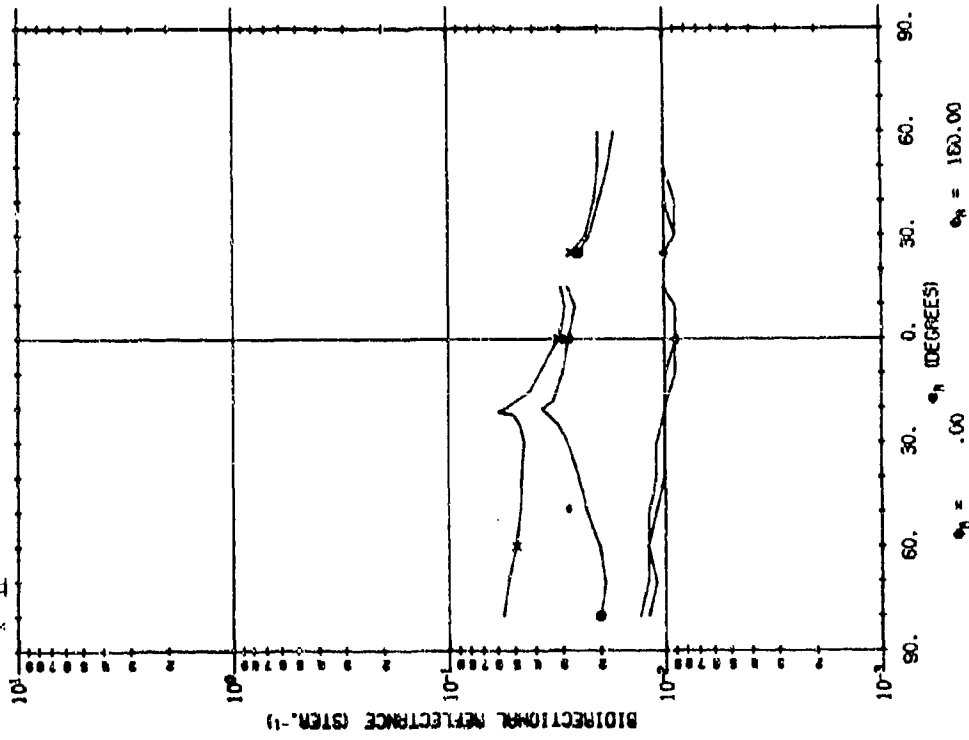
0 ||
+ ||
A ||
x ||



R01454 005

Field Drab Paint on Metal

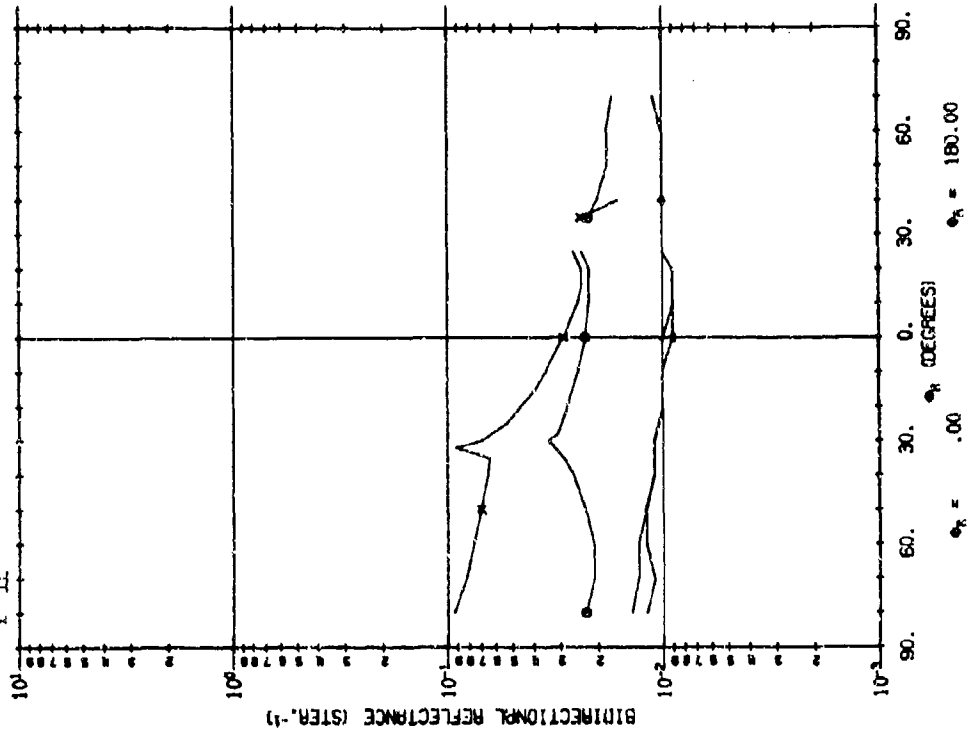
$\theta_i = 20.00$
 $\phi_i = 180.00$
 $\lambda = 0.63$



R01454 005

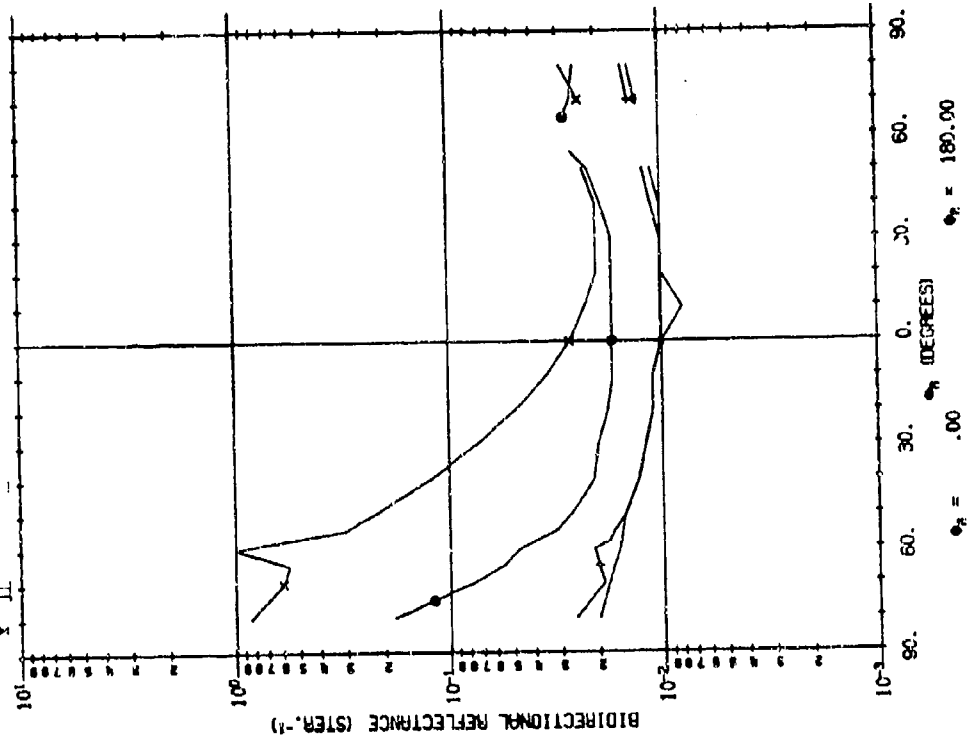
Field Drab Paint on Metal

$\theta_i = 30.00$
 $\phi_i = 180.00$
 $\lambda = 0.63$

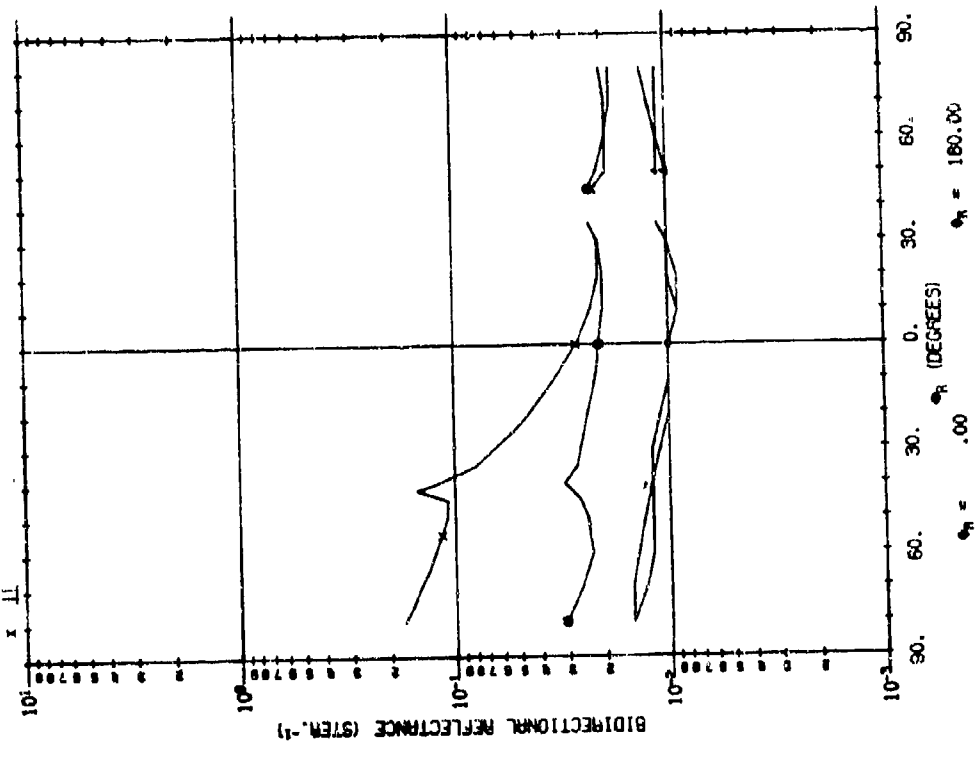


PAINT

R01454 005
 Field Drab Paint on Metal
 $\theta_1 = 60.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$



R01454 005
 Field Drab Paint on Metal
 $\theta_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

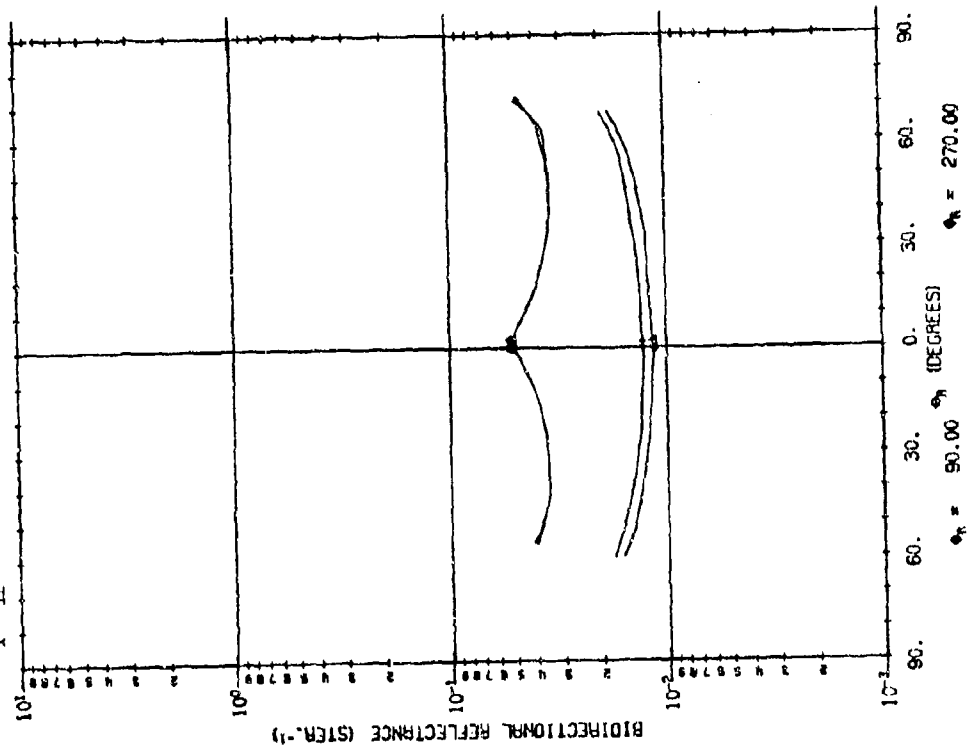


A01454 005

LIGHT BROWN PAINT ON METAL

$\theta_1 = 25 = 2.0$
 $\theta_2 = 91 = 0.9$
 $\lambda = 1 = 0.63$

0 II
+ II
Δ II
x II

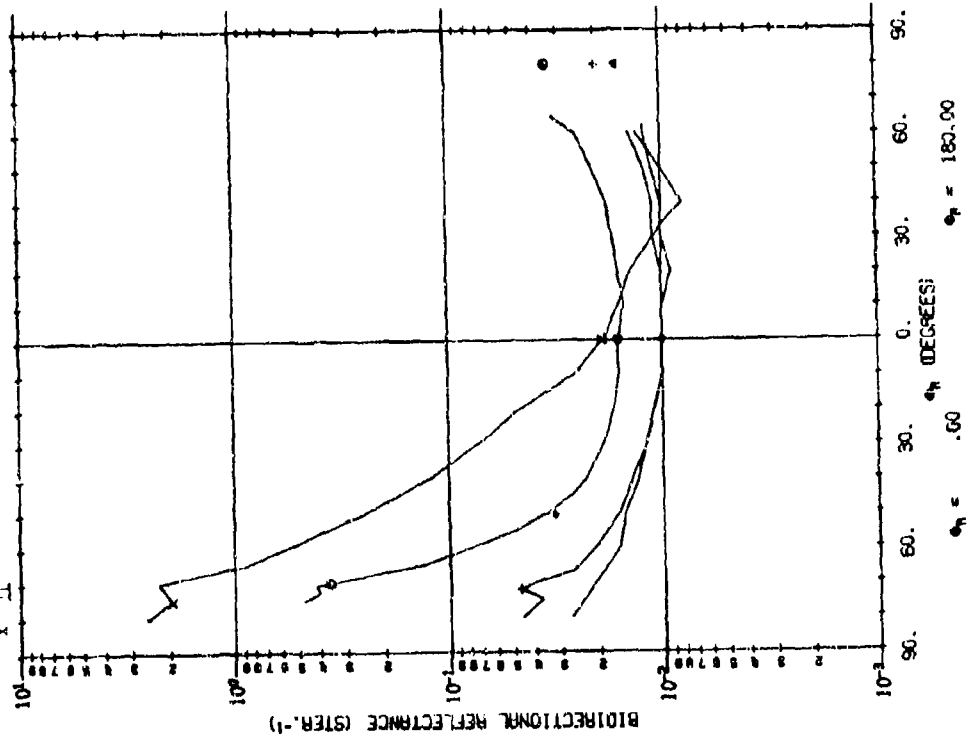


A01454 005

Field Drab Paint on Metal

$\theta_1 = 30.00$
 $\theta_2 = 180.00$
 $\lambda = 1 = 0.63$

0 II
+ II
Δ II
x II

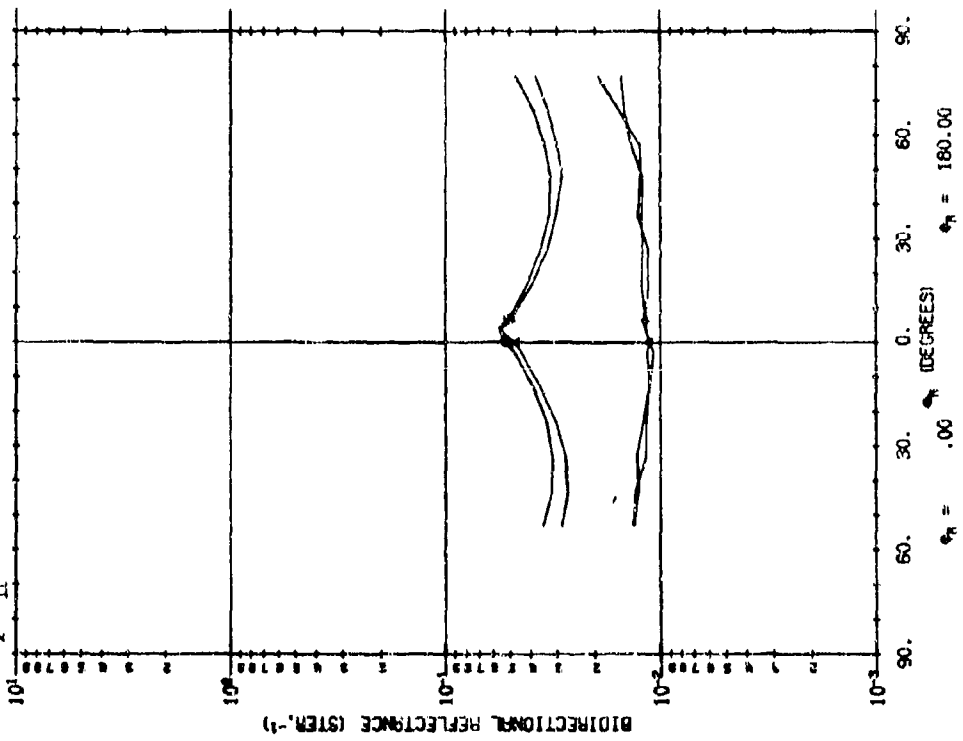


PAINT

AO1454 004

FIELD DRAB PAINT ON METAL

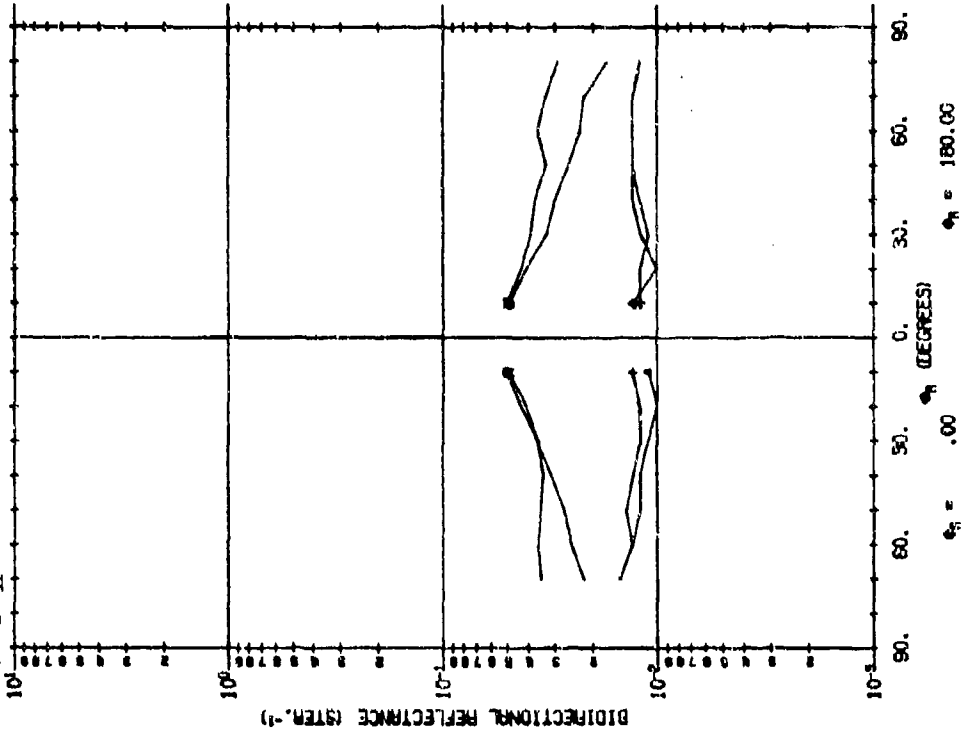
0 || 25 = 7.0
 + || 1 = 42
 Δ || 1 = 1.06
 X ||



AO1454 004

FIELD DRAB PAINT ON METAL

0 || 0 = 0.0
 + || 1 = 180.0
 Δ || 1 = 1.06
 X ||

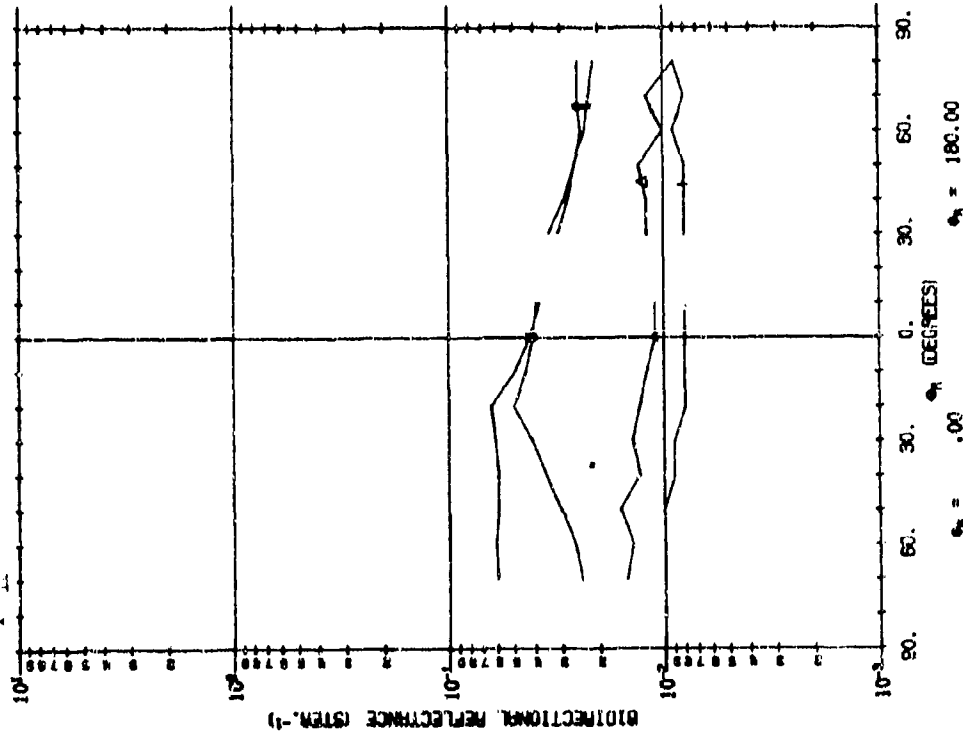


R01454 004

Field Drab Paint on Metal

$\epsilon_1 = 20.00$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$

0
+
A
X

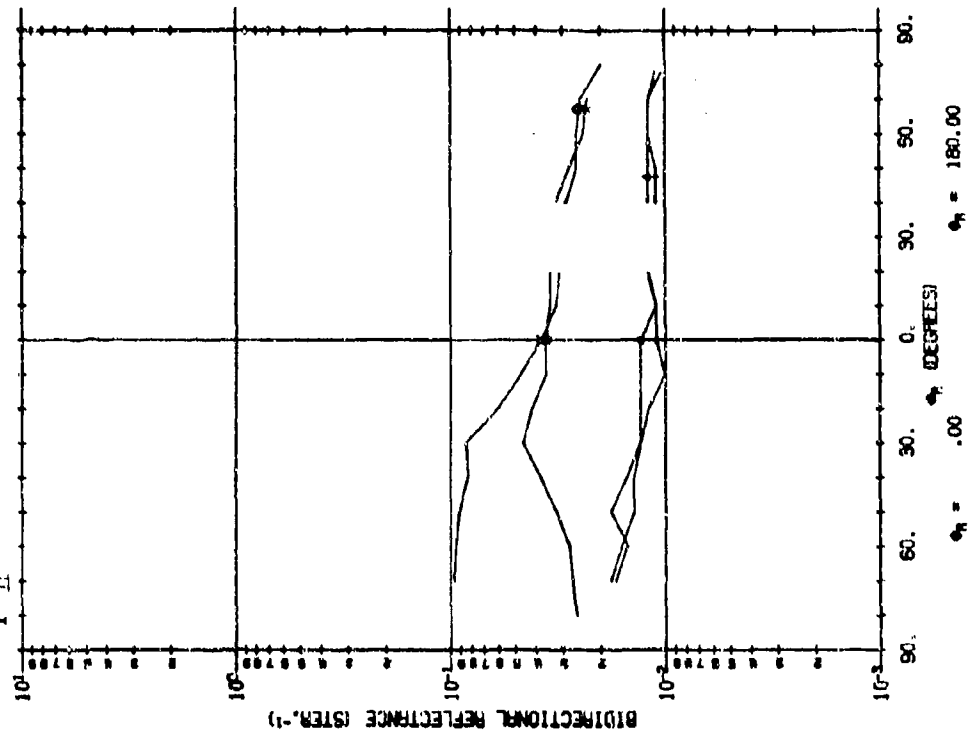


R01454 004

Field Drab Paint on Metal

$\epsilon_1 = 30.00$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$

0
+
A
X



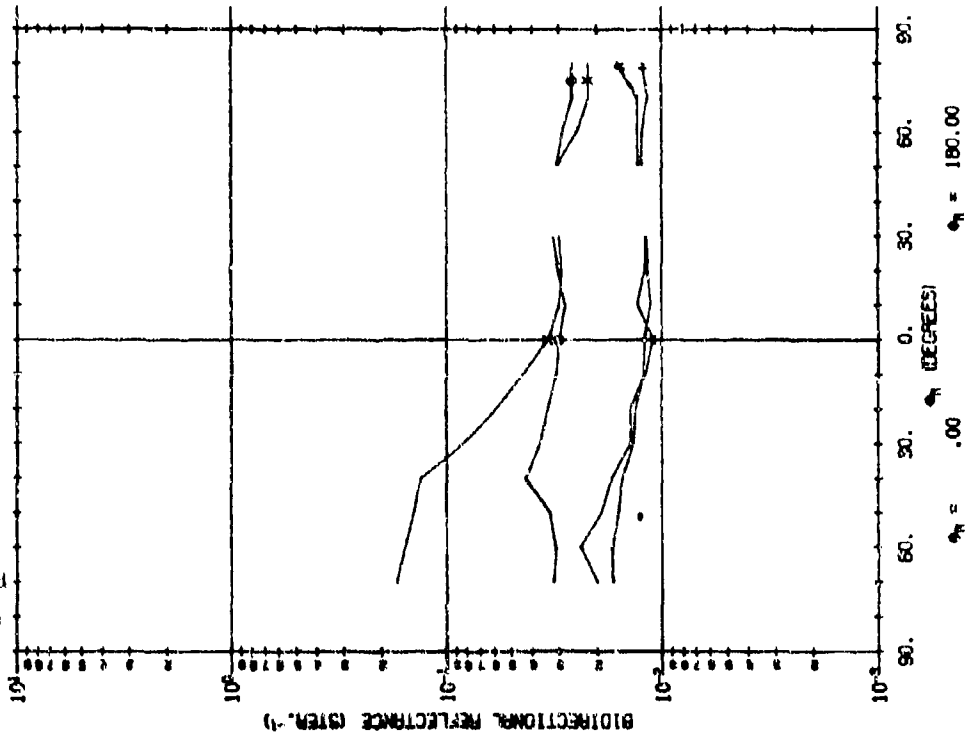
PAINT

R01454j 004

Field Drab Paint on Metal

$\theta_1 = 40.00$
 $\theta_2 = 180.00$
 $\lambda = 1.06$

0 II
+ II
A II
X II

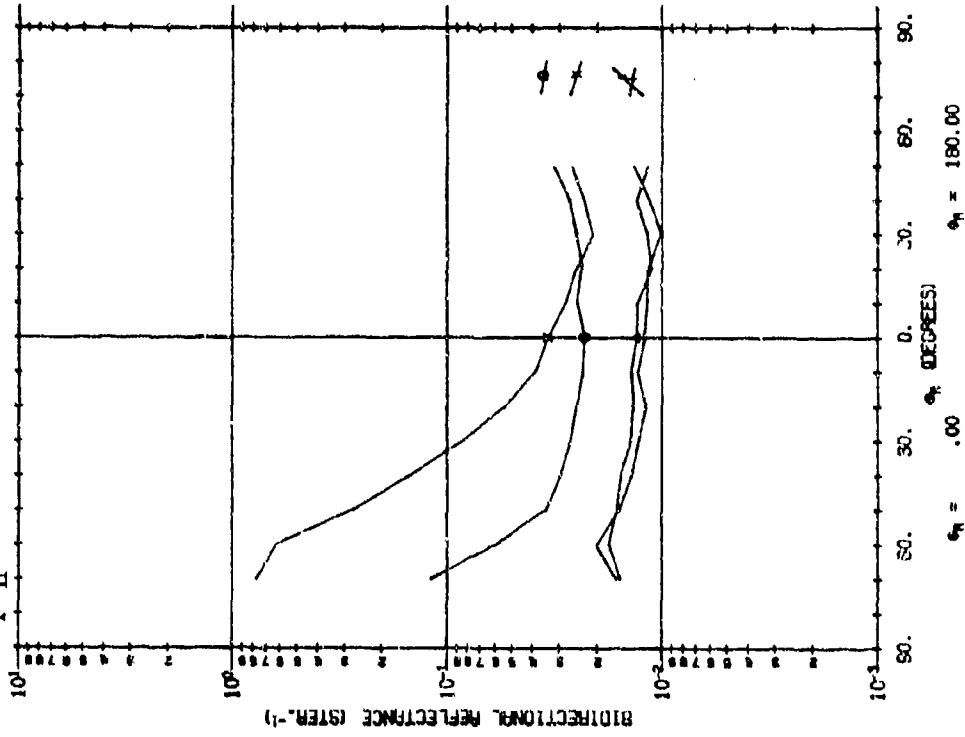


R01454 004

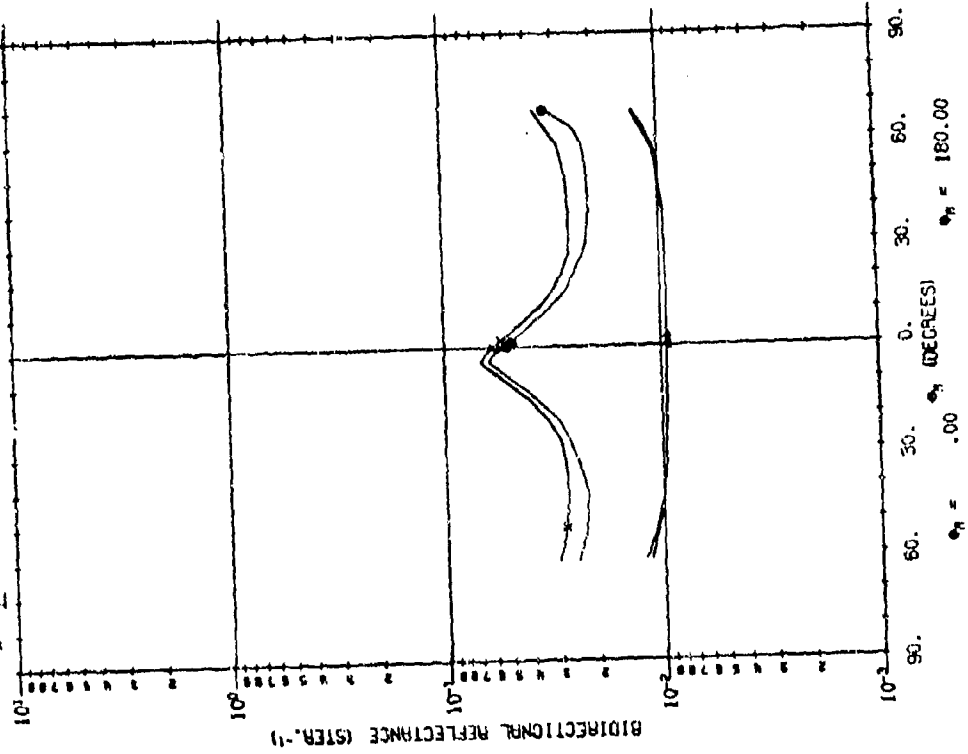
Field Drab Paint on Metal

$\theta_1 = 50.00$
 $\theta_2 = 180.00$
 $\lambda = 1.06$

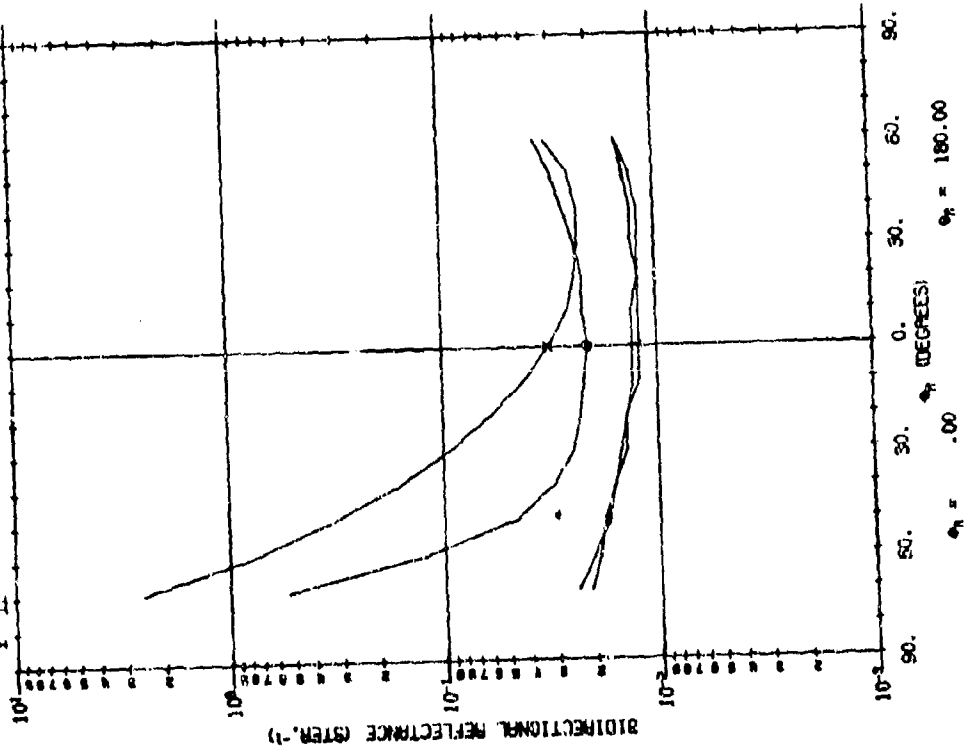
0 II
+ II
A II
X II



R01455 005
 OLIVE DRAB PAINT ON METAL
 $2\theta = 2.0$
 $\theta_1 = 0.1^\circ$
 $\theta_2 = 0.53^\circ$



R01454 004
 Field Drab Paint on Metal
 $\theta_1 = 70.00$
 $\theta_2 = 180.00$
 $\lambda = 3.06$



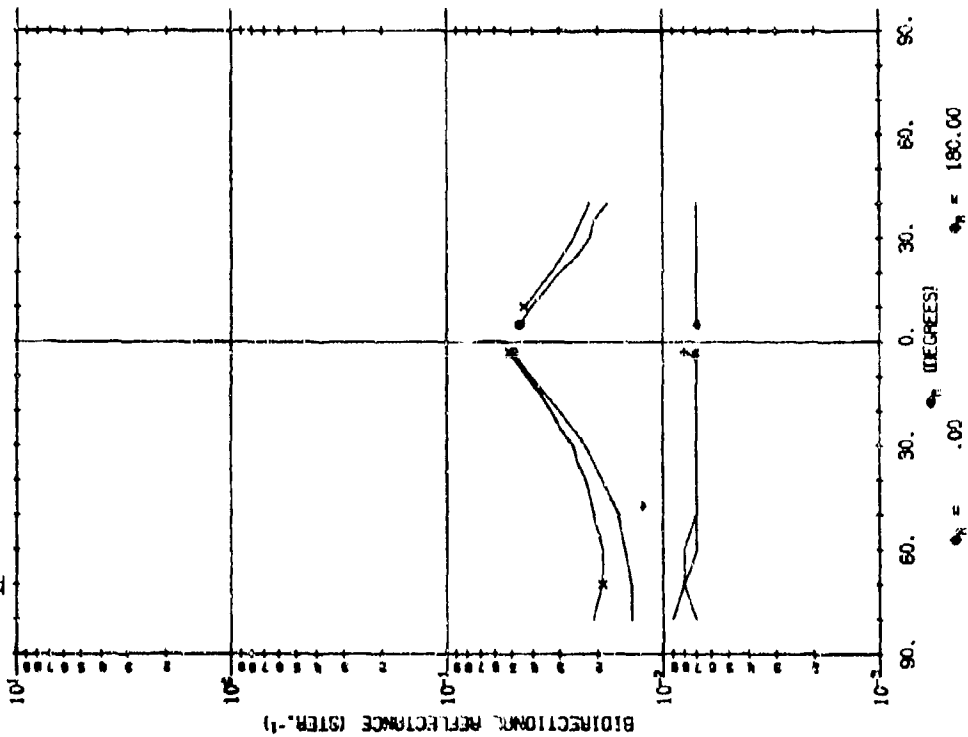
PAINT

R01455 005

Olive Drab Paint on Metal

$\theta_1 = 0.0$
 $\theta_2 = 180.00$
 $\lambda = 0.63$

0 | |
+ | |
Δ | |
x | |

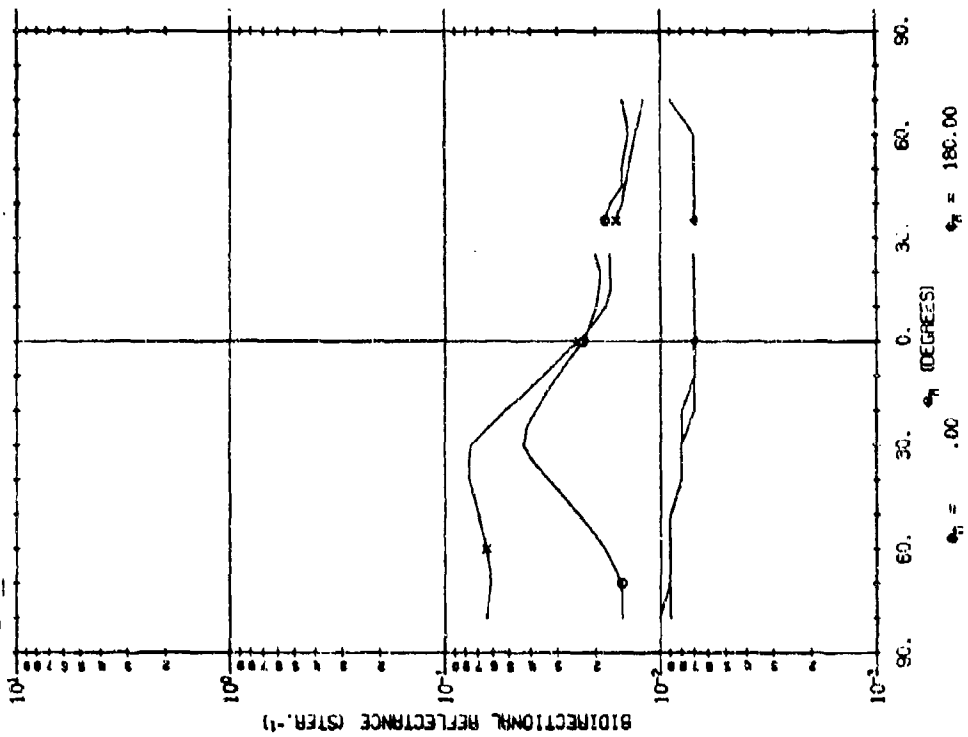


R01455 005

Olive Drab Paint on Metal

$\theta_1 = 30.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$

0 | |
+ | |
Δ | |
x | |



A01456 005

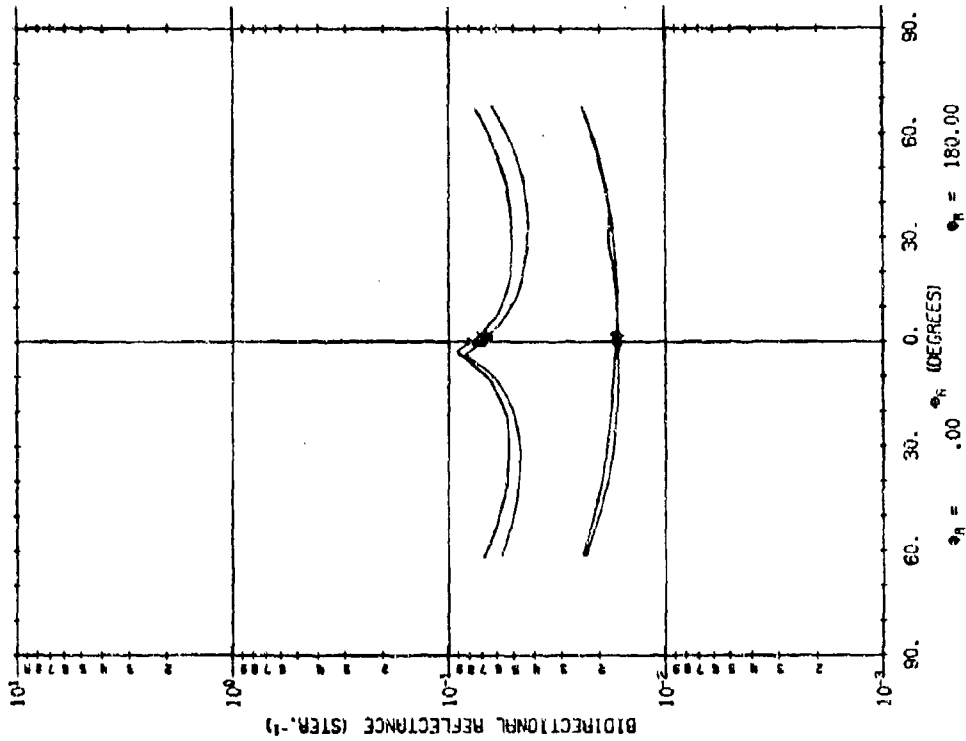
OLIVE DRAB PAINT ON METAL

$2E = 2.0$

$\lambda_1 = \lambda_2$

$\lambda = 0.63$

0
+
-
x



A01455 005

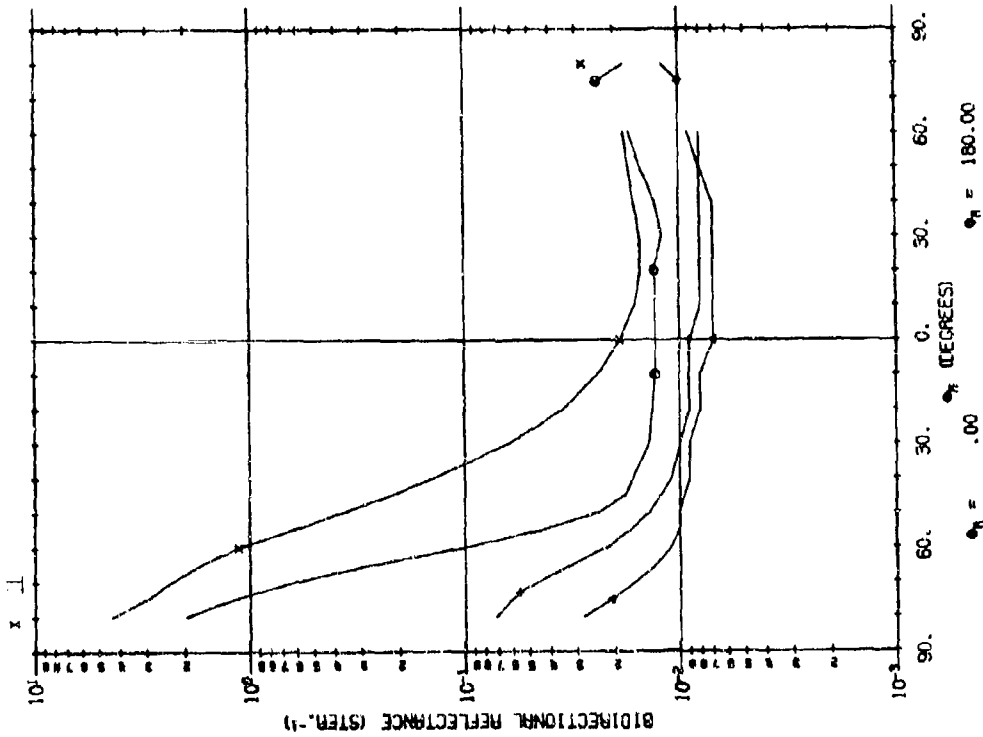
OLIVE DRAB PAINT ON METAL

$\theta_1 = 70.00$

$\theta_2 = 180.00$

$\lambda = 0.63$

0
+
-
x



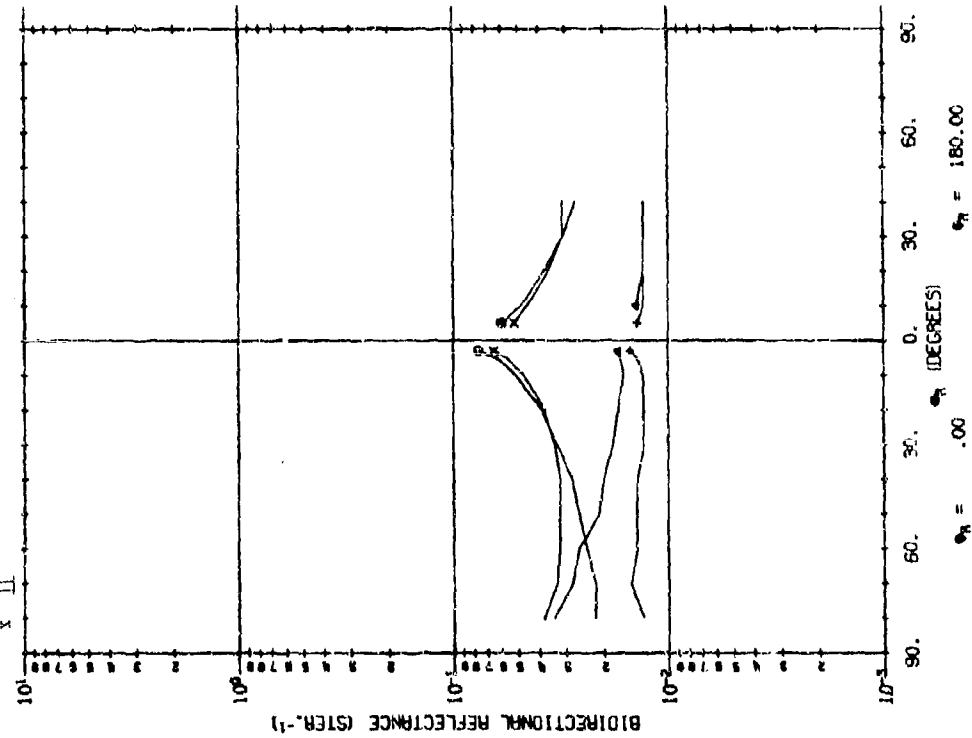
PAINT

R01456 005

Olive Drab Paint on Metal

$\theta_1 = 0.0$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 ||
+ ||
Δ ||
x ||

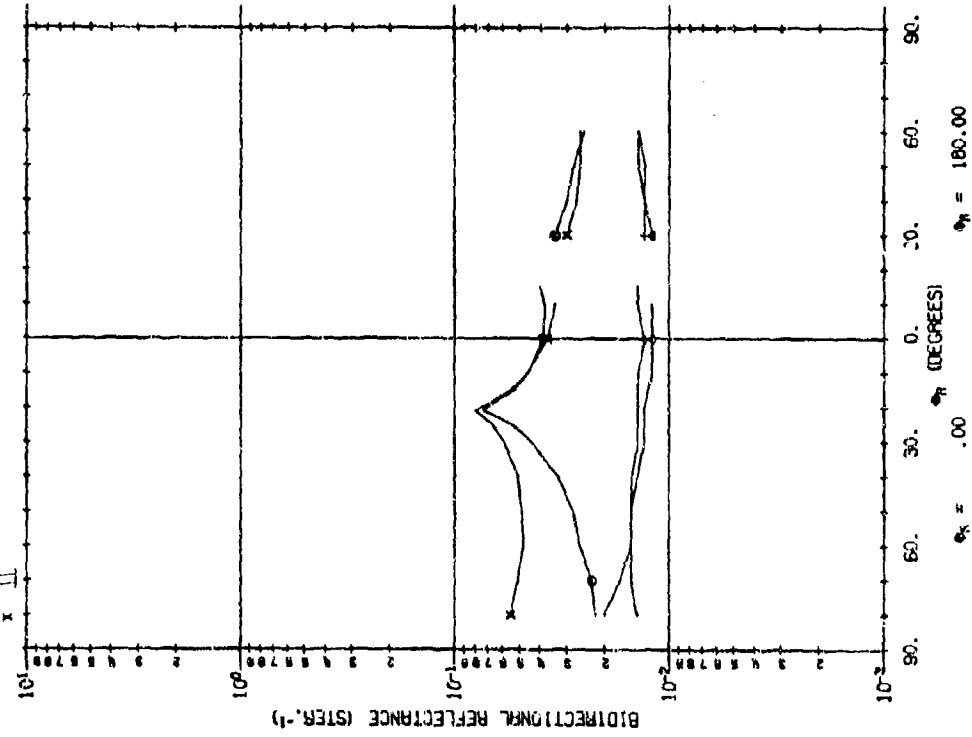


R01456 005

Olive Drab Paint on Metal

$\theta_1 = 20.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 ||
+ ||
Δ ||
x ||

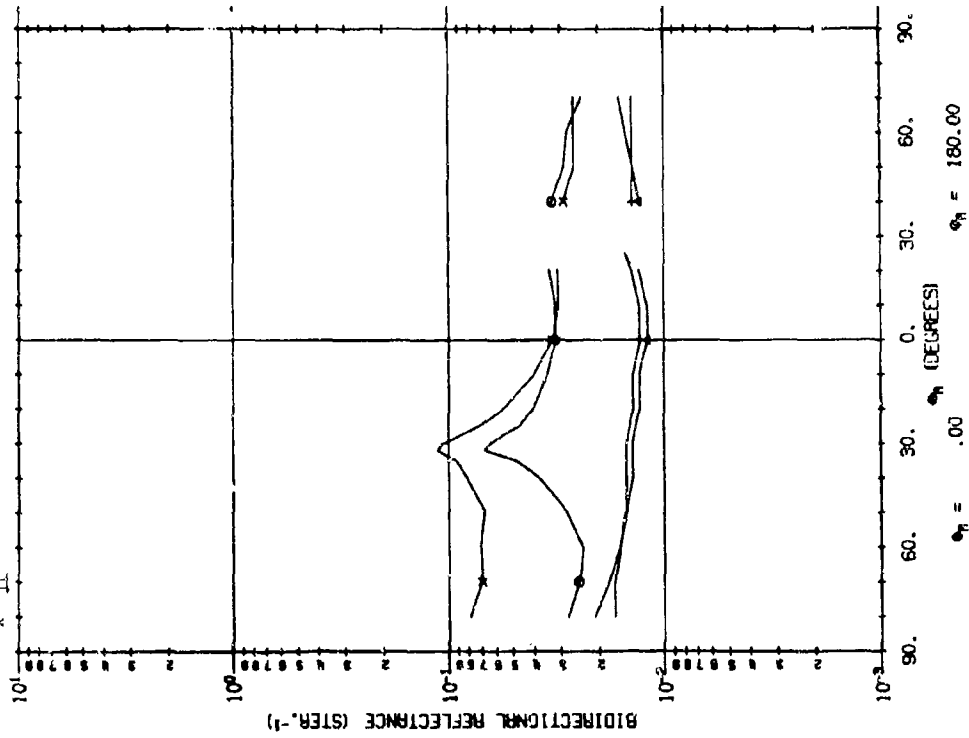


A01456 005

Olive Drab Paint on Metal

$\epsilon_1 = 30.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 ||
 + ||
 Δ ||
 X ||



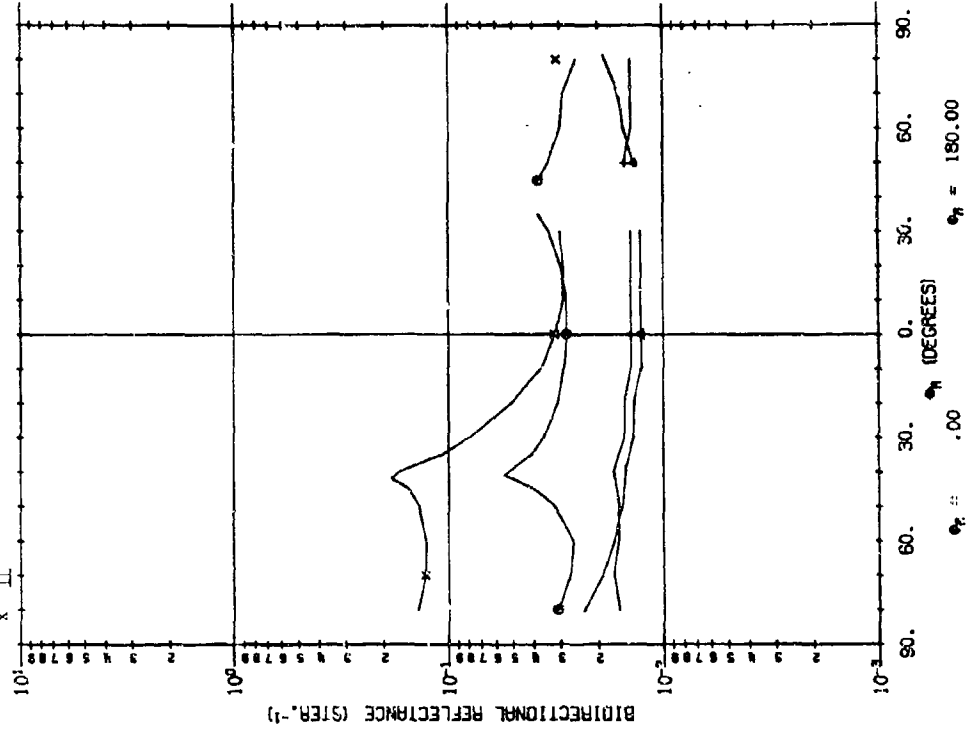
$\theta_i = .00$ $\theta_r = 180.00$

A01456 005

Olive Drab Paint on Metal

$\epsilon_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 ||
 + ||
 Δ ||
 X ||



$\theta_i = .00$ $\theta_r = 180.00$

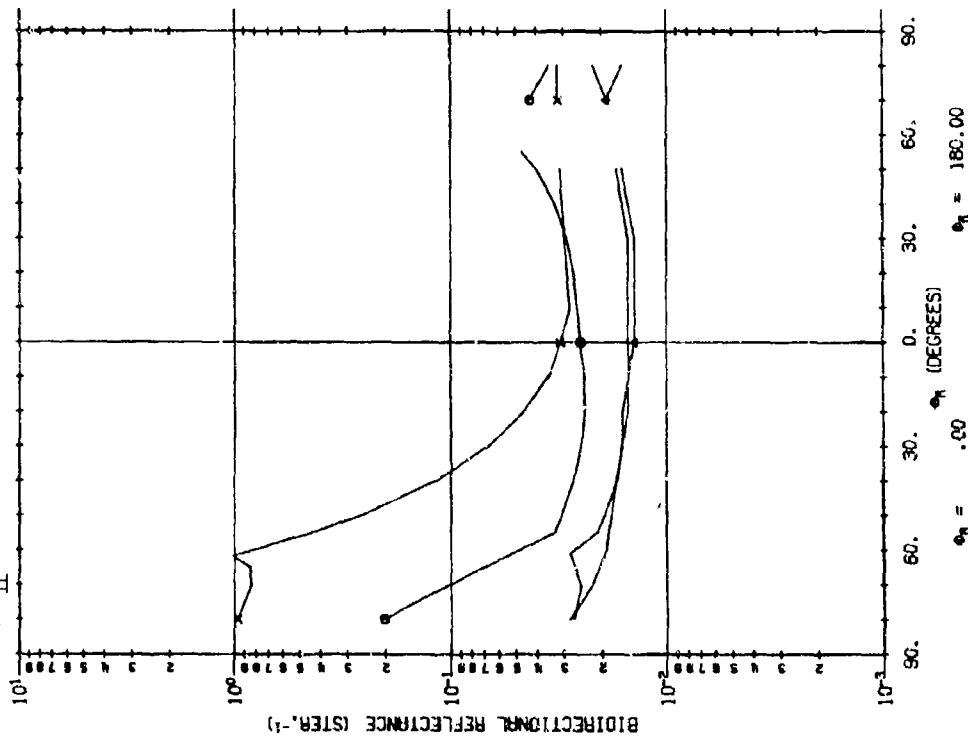
PAINT

R01456 005

Olive Drab Paint on Metal

$\theta_1 = 60.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

0 II
+ II
△ II
x II

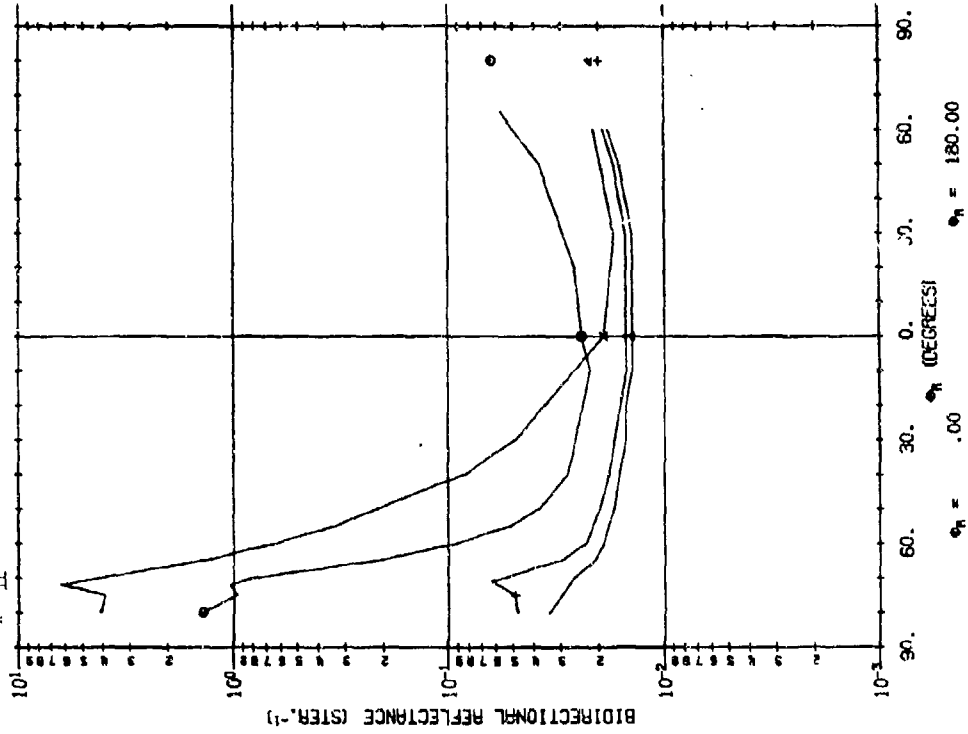


R01456 005

Olive Drab Paint on Metal

$\theta_1 = 70.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

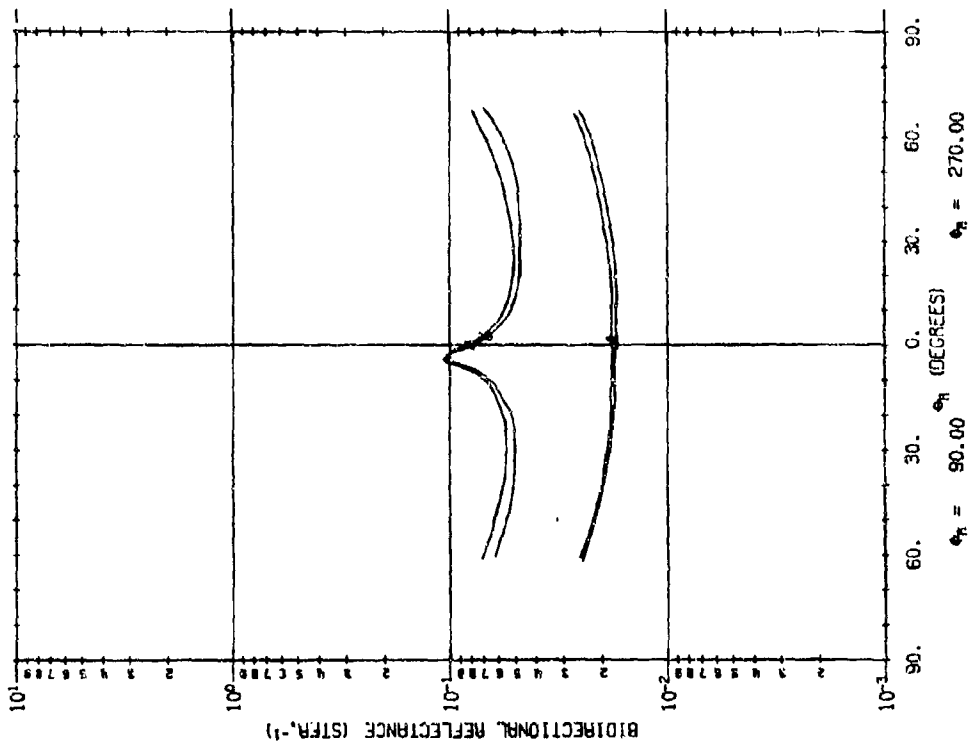
0 II
+ II
△ II
x II



A01456 005

OLIVE DRAB PAINT ON METAL

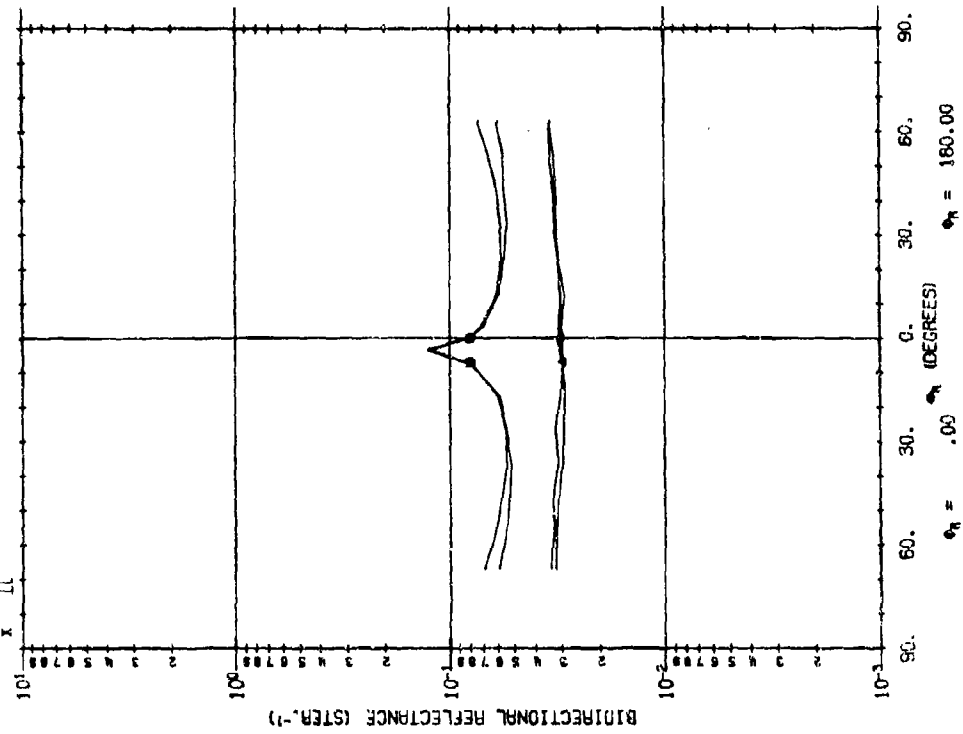
0 || 28 = 2.0
 + || $\rho_1 = \frac{1}{2} \rho_2$
 Δ || $\lambda = 0.63$
 X ||



A01456 004

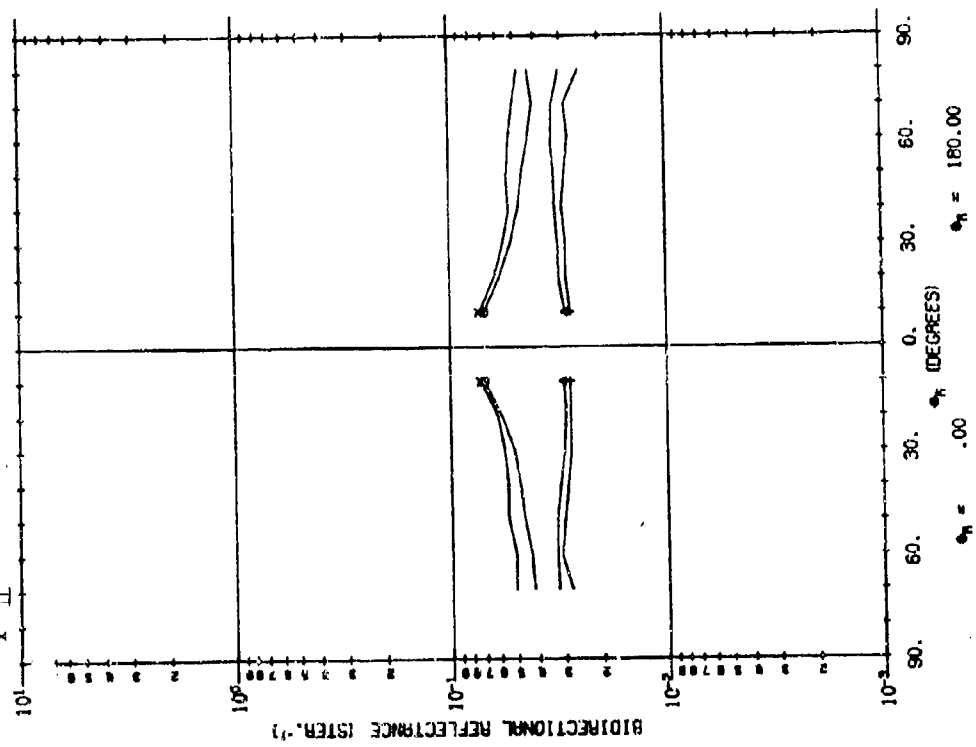
OLIVE DRAB PAINT ON METAL

0 || 28 = 2.0
 + || $\rho_1 = \frac{1}{2} \rho_2$
 Δ || $\lambda = 1.06$
 X ||

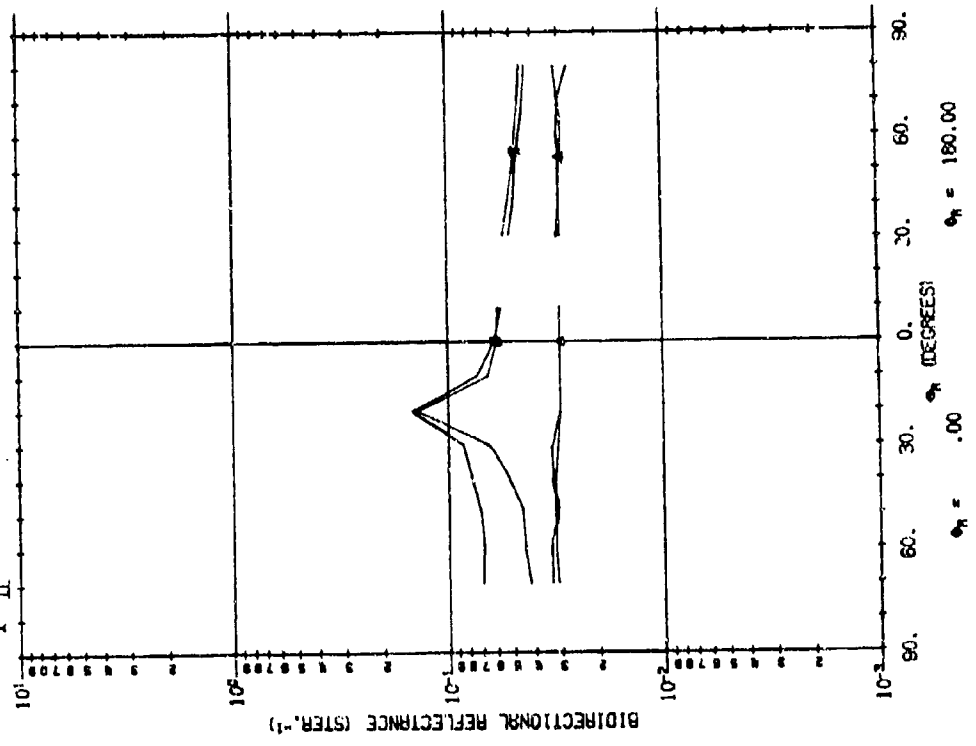


PAINT

A01456 004
 Olive Drab Paint on Metal
 $\epsilon_1 = 0.6$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$



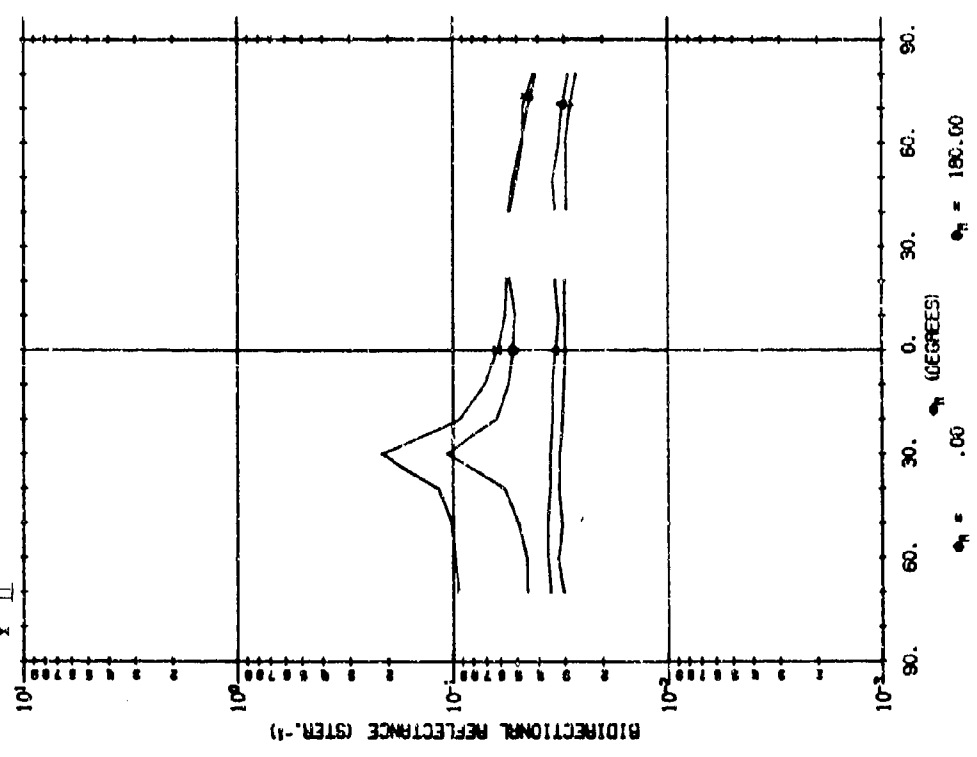
A01456 004
 Olive Drab Paint on Metal
 $\epsilon_1 = 20.00$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$



A01456 004
 0 ||
 + ||
 Δ ||
 X ||

Olive Drab Paint on Metal

$\theta_1 = 30.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$

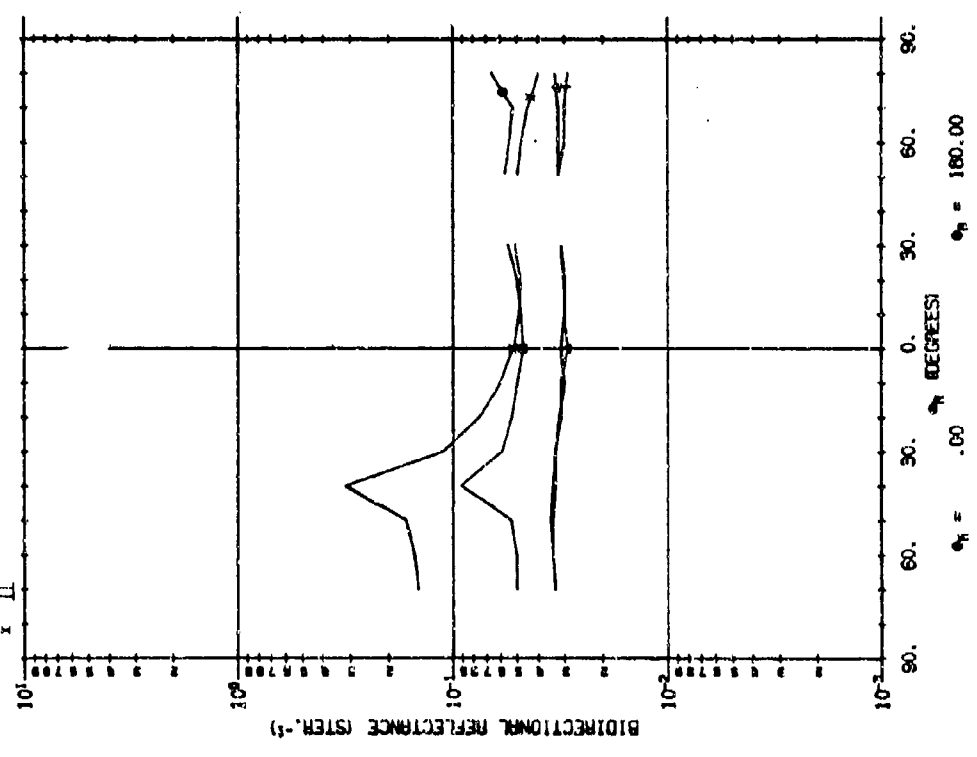


$\theta_1 = 30.00$ $\phi_1 = 180.00$

A01456 004
 0 ||
 + ||
 Δ ||
 X ||

Olive Drab Paint on Metal

$\theta_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$



$\theta_1 = 40.00$ $\phi_1 = 180.00$

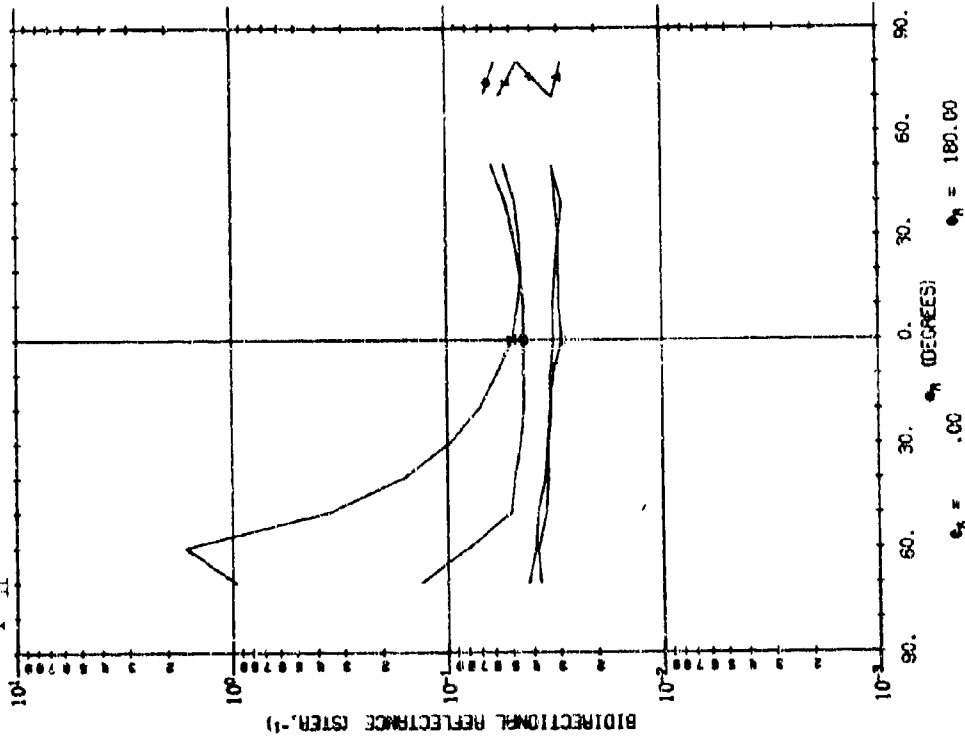
PAINT

A01456 004

Olive Drab Paint on Metal

$\phi_i = 60.00$
 $\phi_r = 180.00$
 $\lambda = 1.06$

0 ||
 + ||
 Δ ||
 X ||



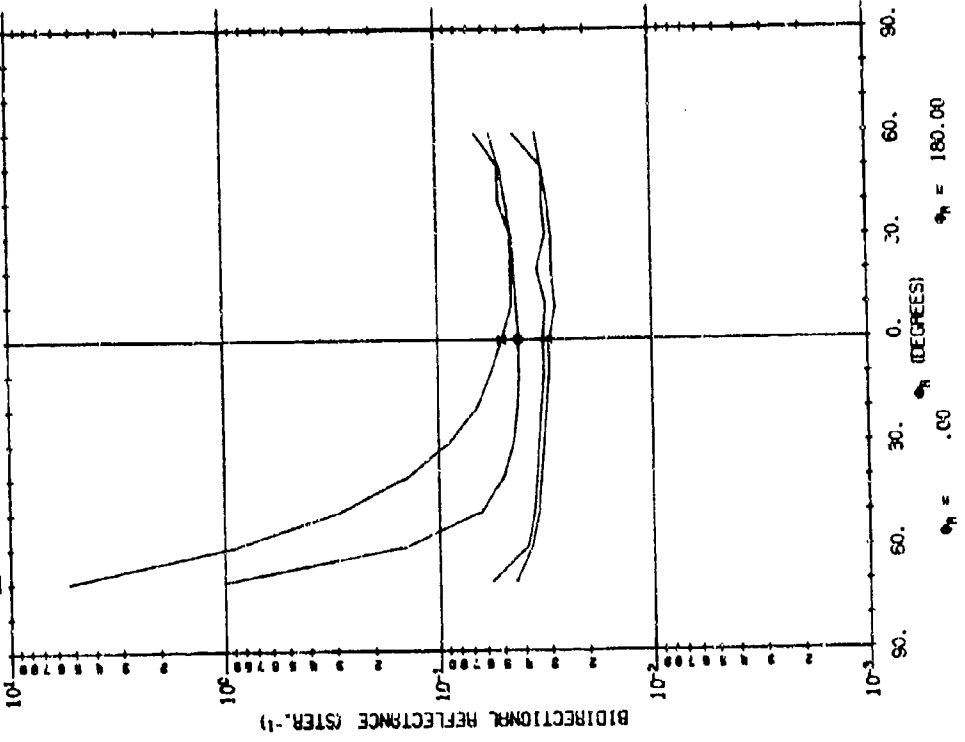
$\phi_i = 60.00$ $\phi_r = 180.00$

A01456 004

Olive Drab Paint on Metal

$\phi_i = 70.00$
 $\phi_r = 180.00$
 $\lambda = 1.06$

0 ||
 + ||
 Δ ||
 X ||

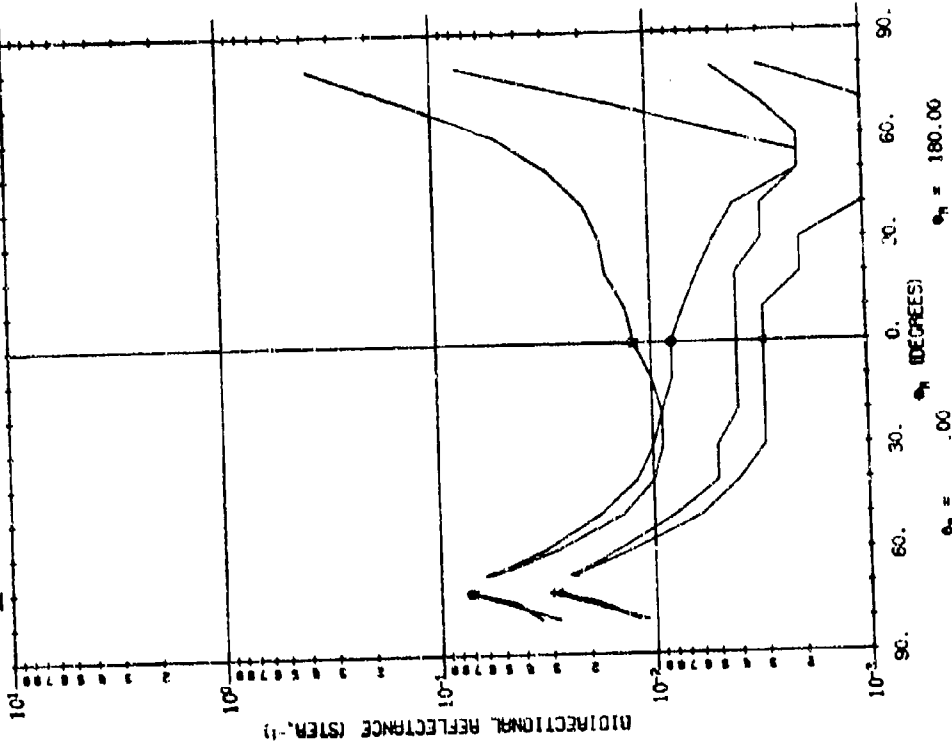


$\phi_i = 70.00$ $\phi_r = 180.00$

R01457 006
 OLIVE DRAB PAINT ON LOUVERED
 METAL PANEL

$\theta_1 = 70.00$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

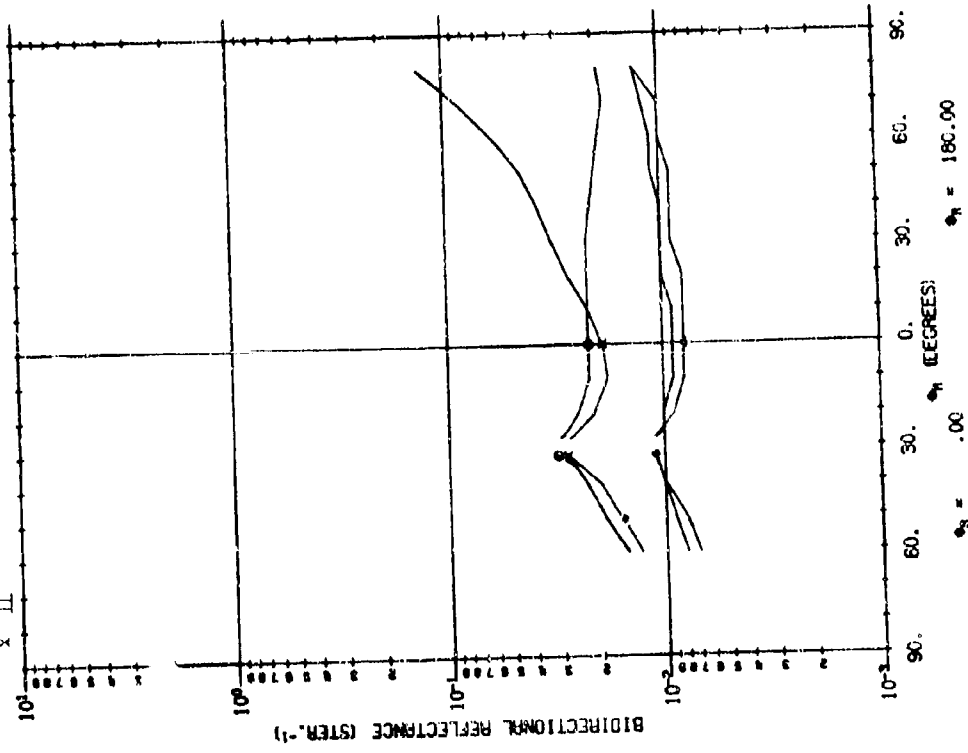
0 II
 + II
 A II
 X II



R01457 008
 OLIVE DRAB PAINT ON LOUVERED
 METAL PANEL

$\theta_1 = 50.00$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

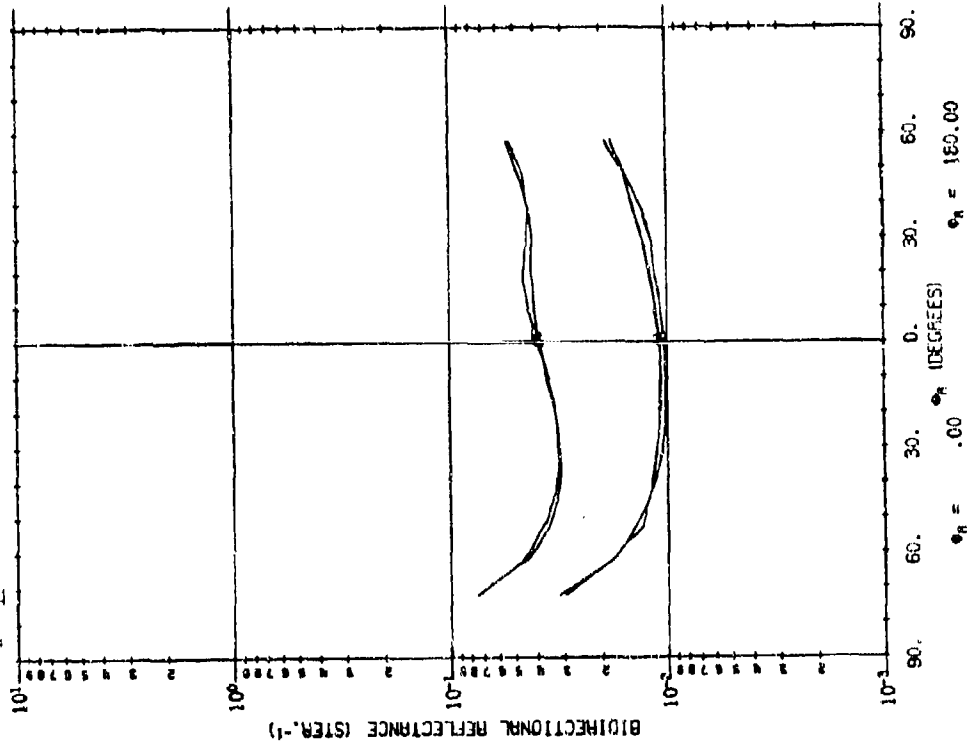
0 II
 + II
 A II
 X II



R01457 006

OLIVE DRAB PAINT ON L/SPOURED
METAL PANEL
 $\theta_1 = 2.0$
 $\theta_2 = 4$
 $\theta_3 = 4$
 $\theta_4 = 0.63$

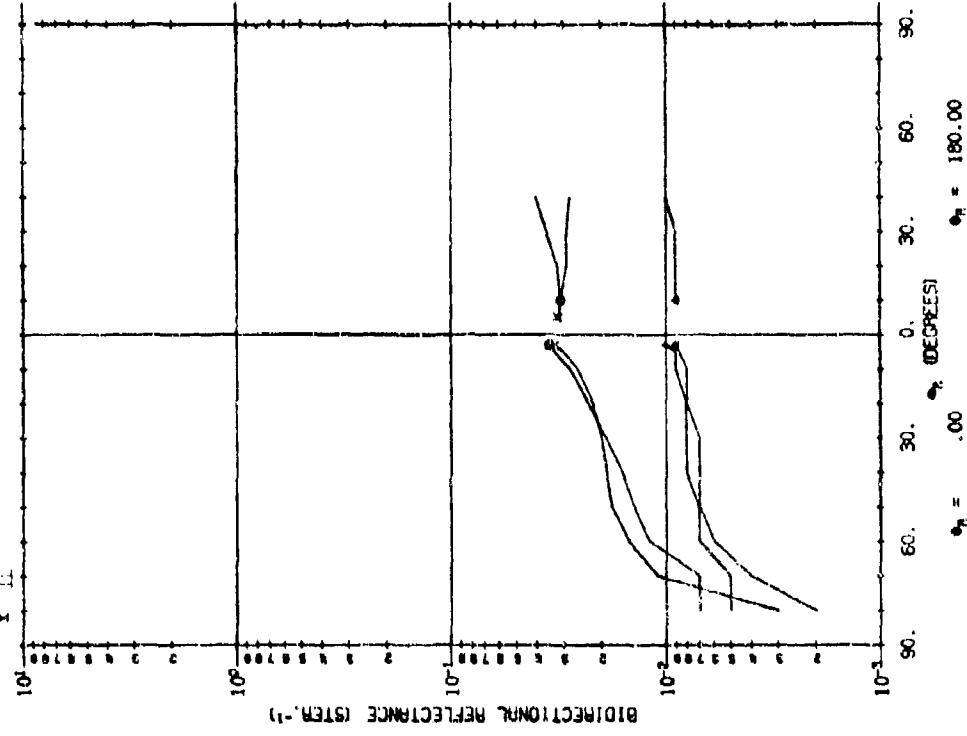
0	1	2	3	4	5	6	7	8	9	10
+	+	+	+	+	+	+	+	+	+	+
x	x	x	x	x	x	x	x	x	x	x



R01457 006

OLIVE DRAB PAINT ON L/SPOURED
METAL PANEL
 $\theta_1 = 0.0$
 $\theta_2 = 4$
 $\theta_3 = 4$
 $\theta_4 = 0.63$

0	1	2	3	4	5	6	7	8	9	10
+	+	+	+	+	+	+	+	+	+	+
x	x	x	x	x	x	x	x	x	x	x



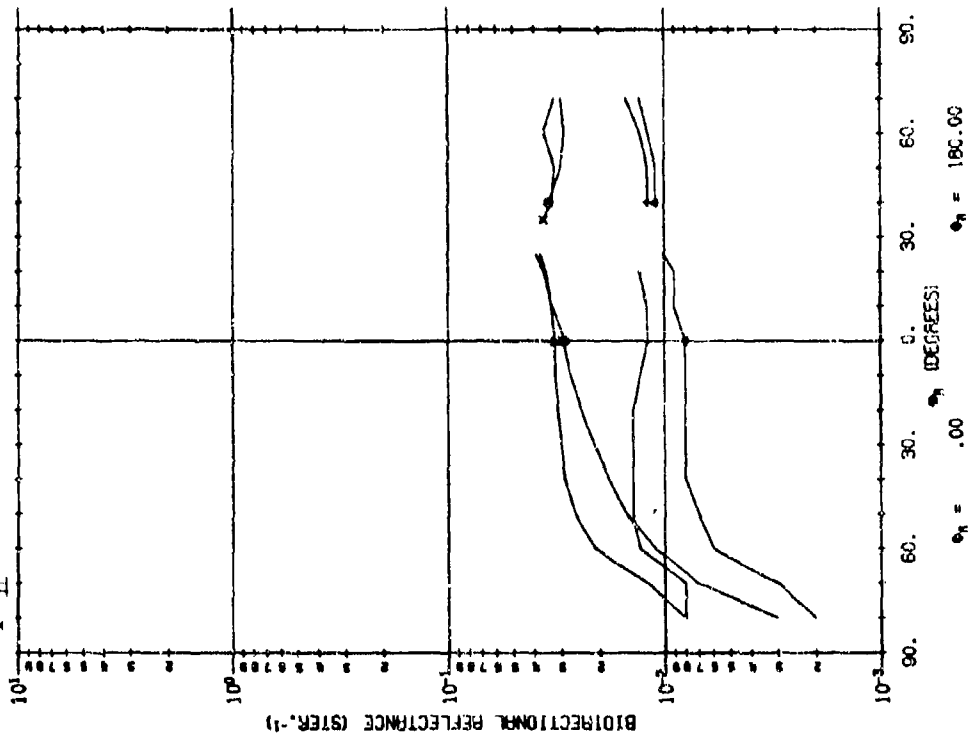
PAINT

AO1457 006

OLIVE DRAB PAINT ON LOUVERED
METAL PANEL

$\theta_1 = 30.00$
 $\theta_2 = 150.00$
 $\lambda = 0.63$

0 II
+ II
Δ II
X II

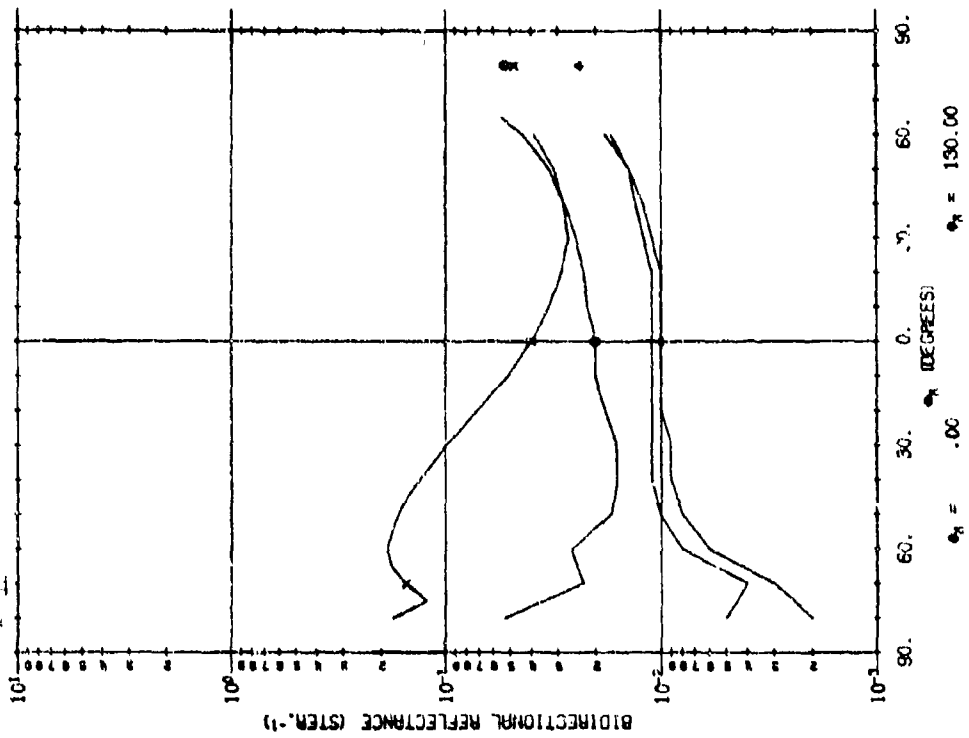


AO1457 006

OLIVE DRAB PAINT ON LOUVERED
METAL PANEL

$\theta_1 = 70.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$

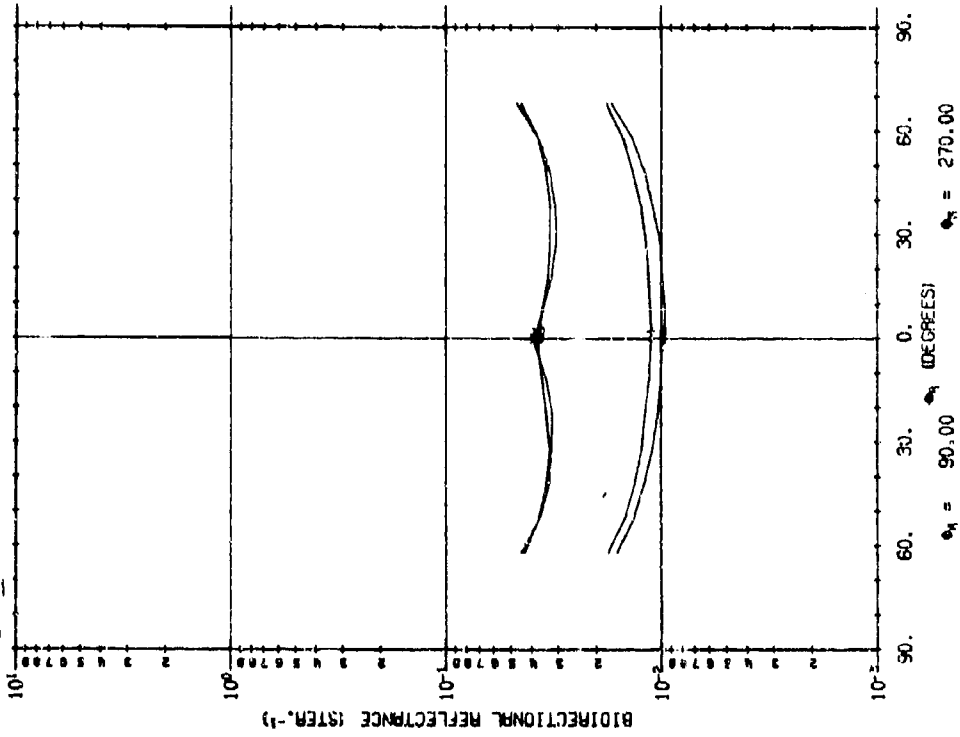
0 II
+ II
Δ II
X II



A01457 006

OLIVE DRAB PAINT ON LAMINATED
METAL PANEL

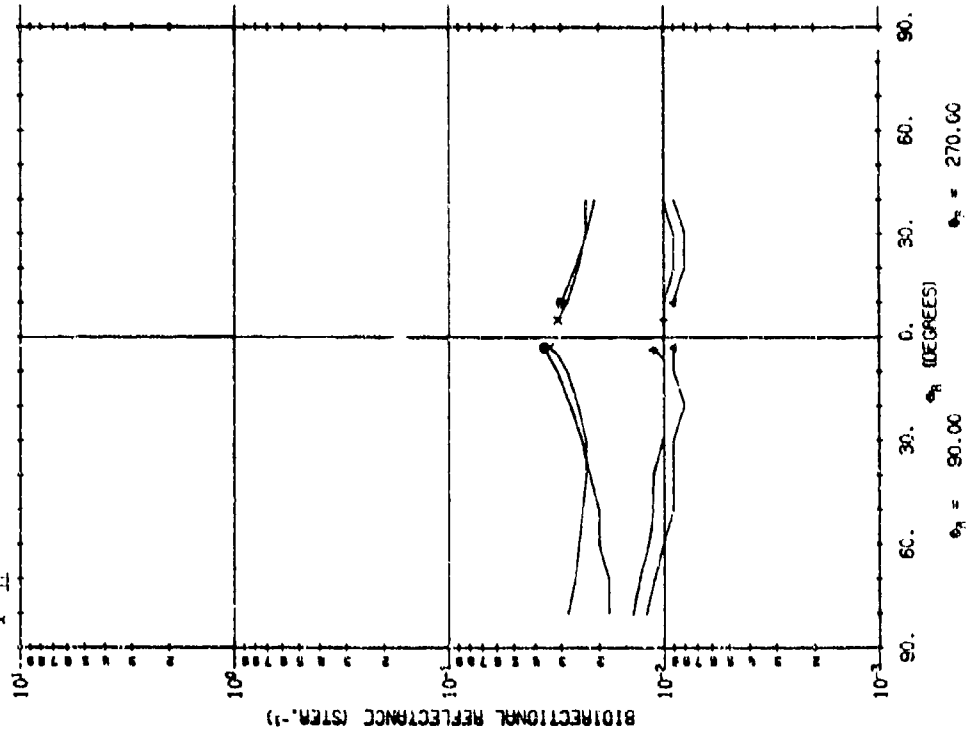
0 II 2.0
+ II $\theta_1 = 45^\circ$
- II $\lambda = 0.63$
X II



A01457 006

OLIVE DRAB PAINT ON LAMINATED
METAL PANEL

0 II 0.3
+ II $\theta_1 = 270.00$
- II $\lambda = 0.63$
X II

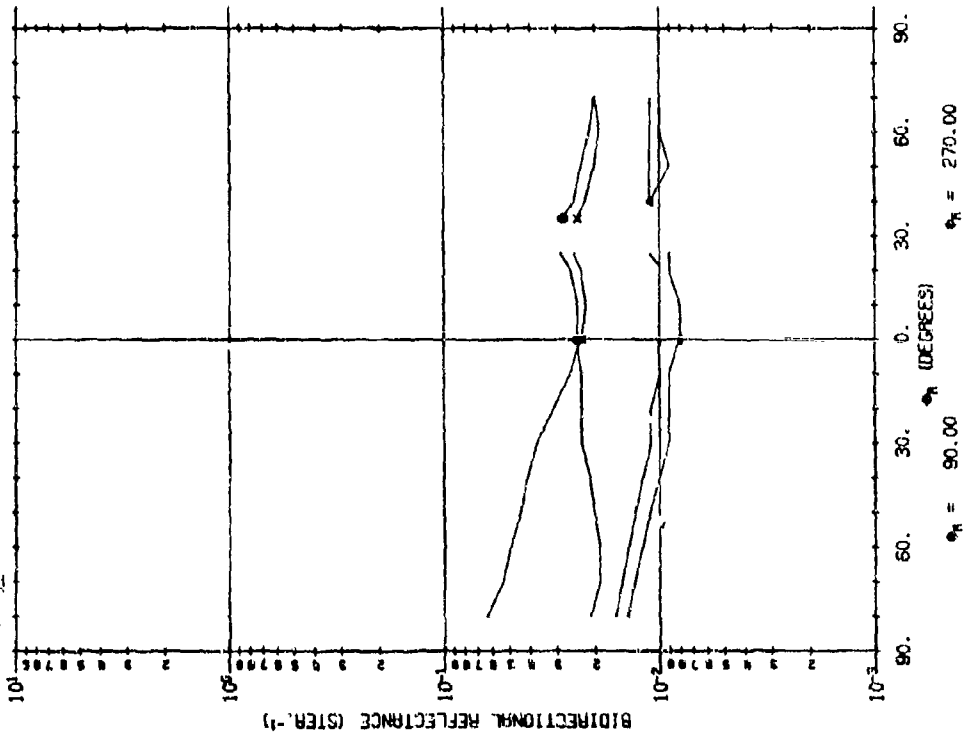


PAINT

A01457 006
 0 1 1 1 1
 + 1 1
 x 1 1
 x 1 1

OLIVE DRAB PAINT ON METAL PANEL

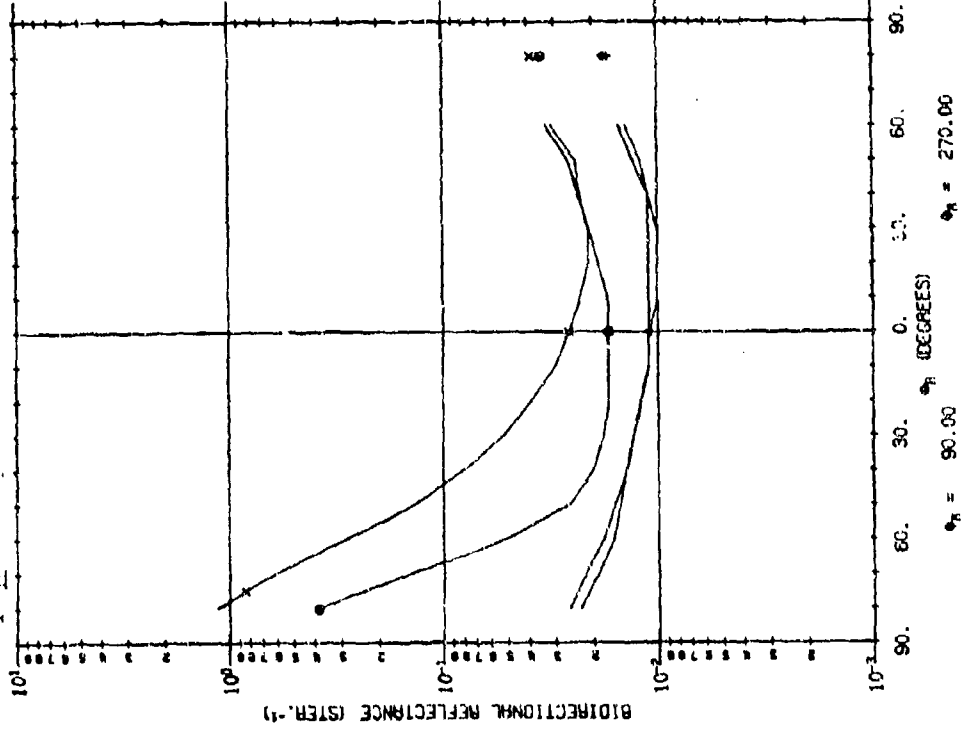
$\theta_1 = 30.00$
 $\theta_2 = 270.00$
 $\lambda = 0.63$



A01457 006
 0 1 1 1 1
 + 1 1
 x 1 1
 x 1 1

OLIVE DRAB PAINT ON LOUVERED METAL PANEL

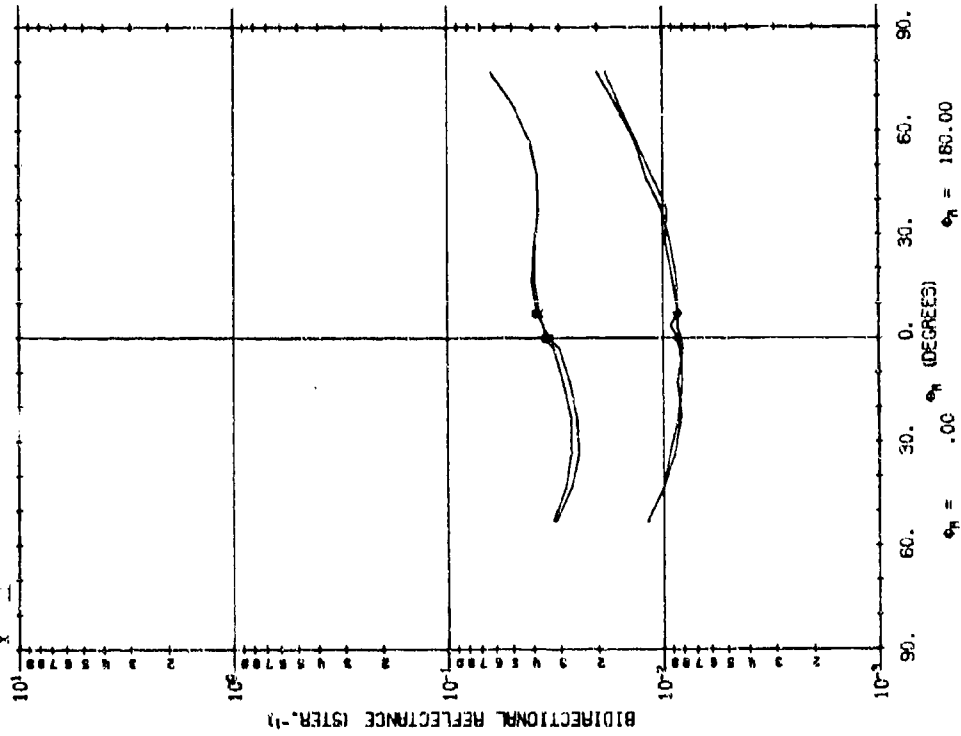
$\theta_1 = 70.00$
 $\theta_2 = 270.00$
 $\lambda = 0.63$



R01457 005

OLIVE DRAB PAINT ON METAL

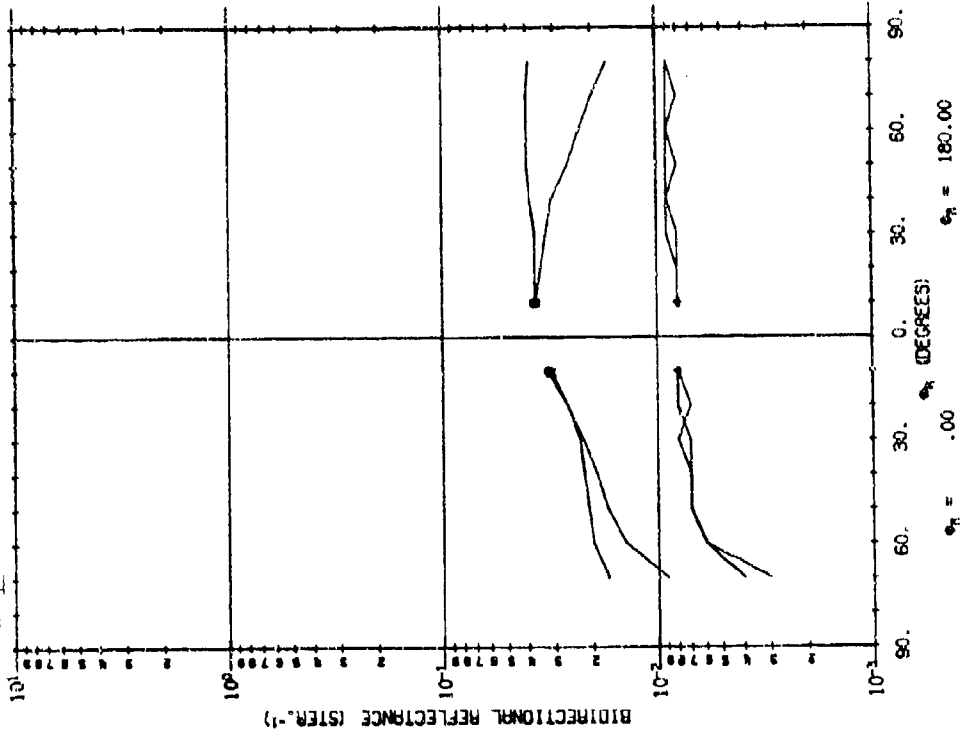
$\theta_i = 7.0$
 $\phi_i = 0.0$
 $\lambda = 1.06$



R01457 005

OLIVE DRAB PAINT ON LOWERED METAL PANEL

$\theta_i = 0.0$
 $\phi_i = 0.0$
 $\lambda = 1.06$



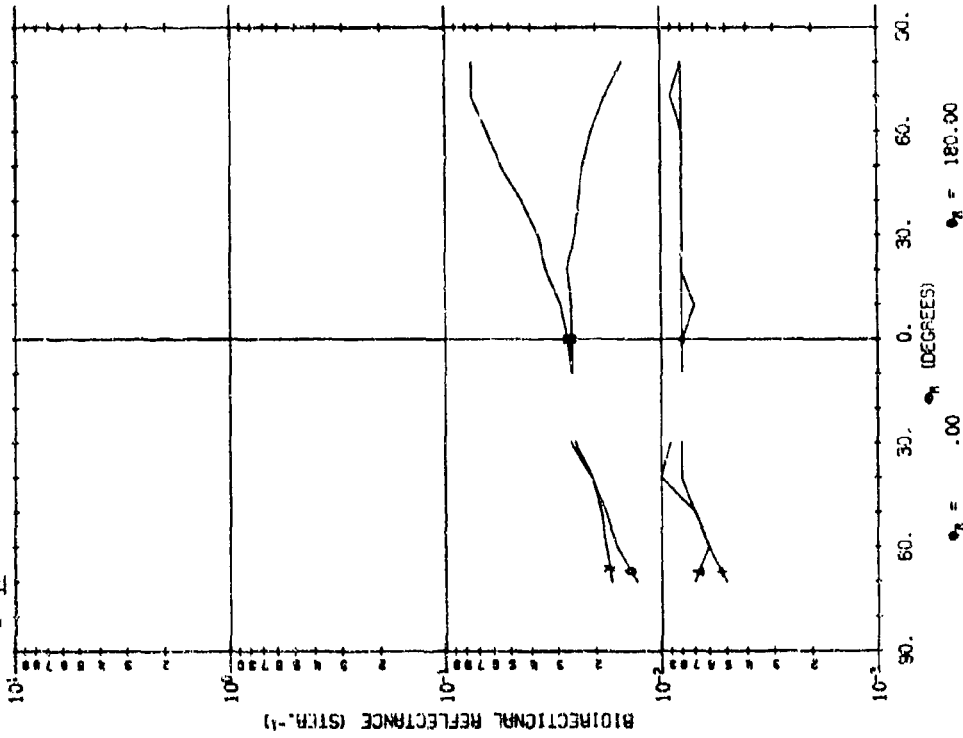
PAINT

R01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_1 = 20.00$
 $\theta_2 = 0.0$
 $\lambda = 1.06$

0 | |
+ | |
△ | |
x | |

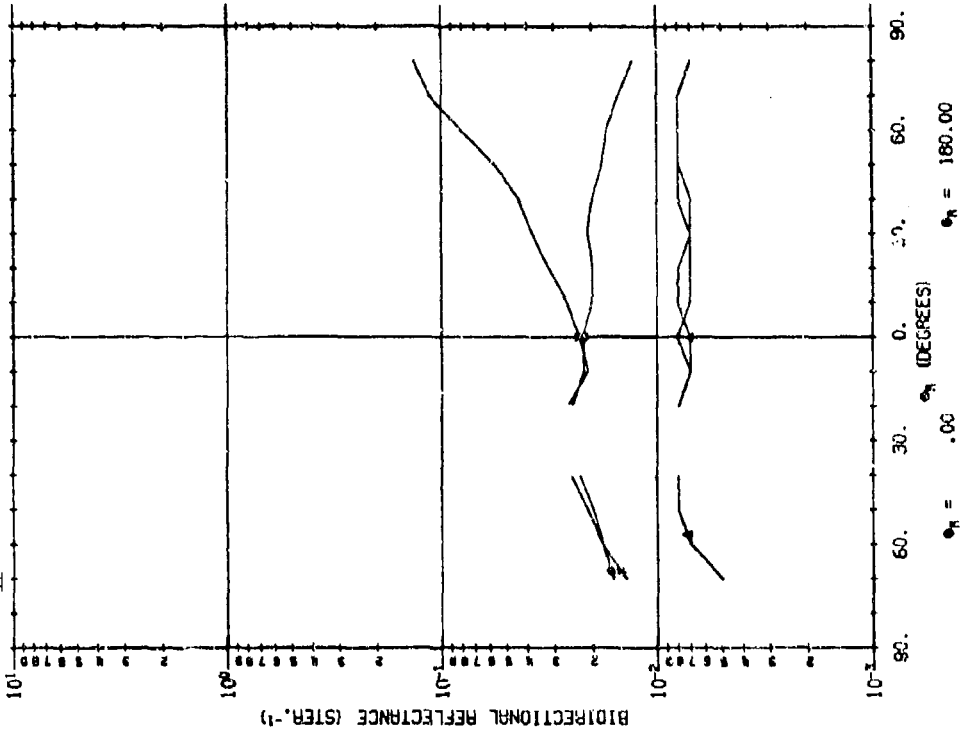


R01457 005

Olive Drab Paint on Louvered Metal Panel

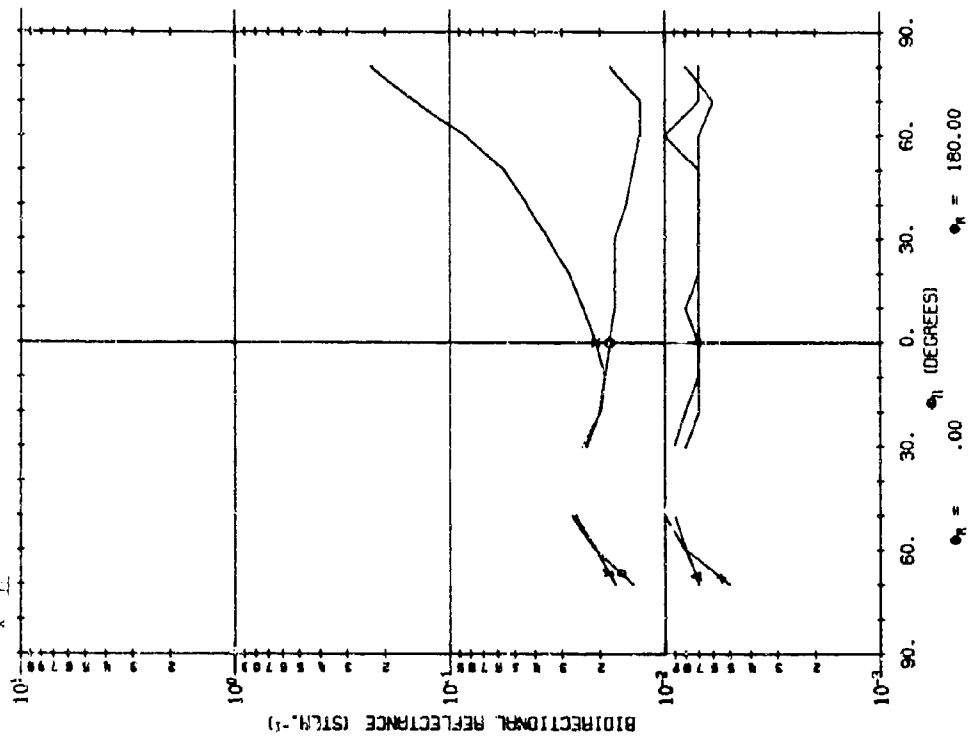
$\theta_1 = 30.00$
 $\theta_2 = 0.0$
 $\lambda = 1.06$

0 | |
+ | |
△ | |
x | |



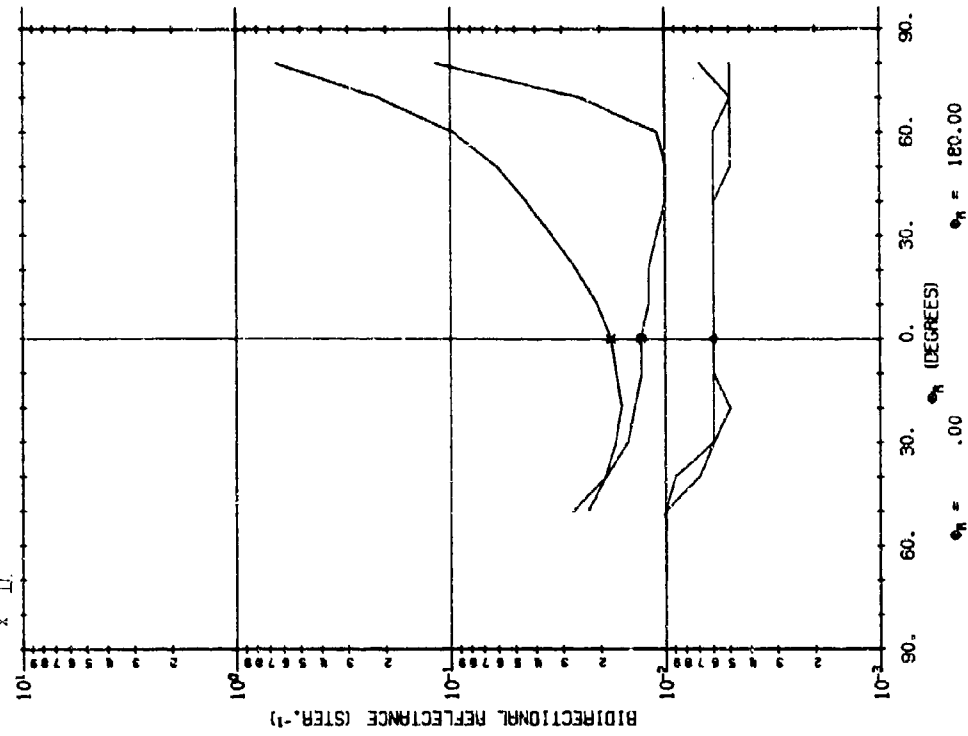
A01457 005
 + $\theta_i = 40.00$
 Δ $\theta_i = 0.0$
 x $\lambda = 1.06$

Olive Drab Paint on Louvered Metal Panel



A01457 005
 + $\theta_i = 60.00$
 Δ $\theta_i = 0.0$
 x $\lambda = 1.06$

Olive Drab Paint on Louvered Metal Panel

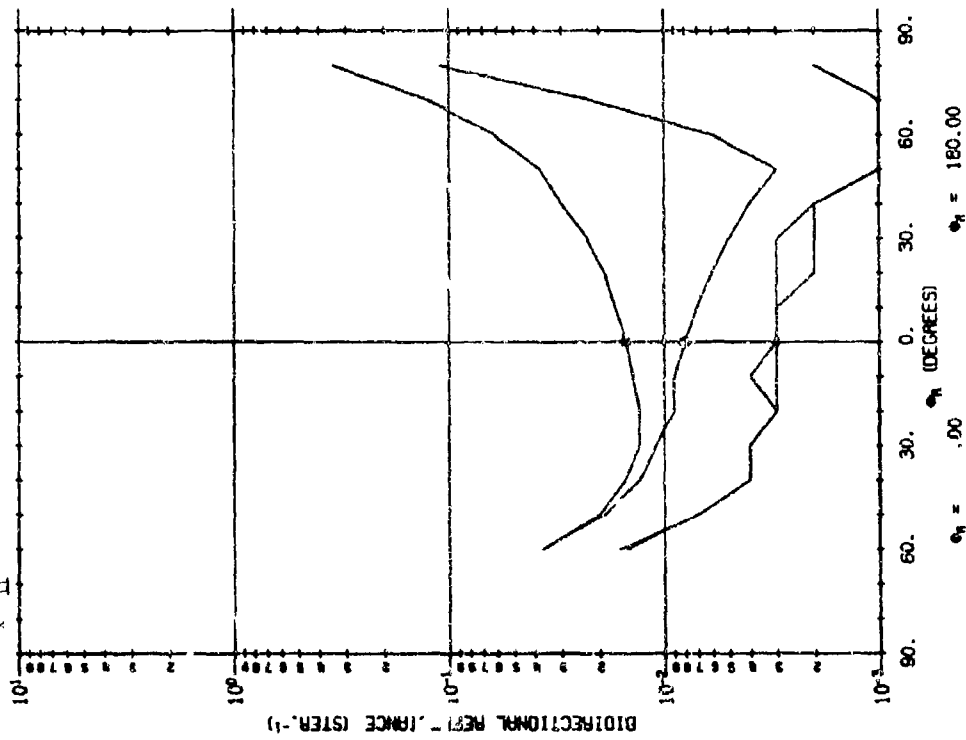


PAIN

A01457 005
 0 II
 + II
 Δ II
 X II

Olive Drab Paint on Louvered Metal Panel

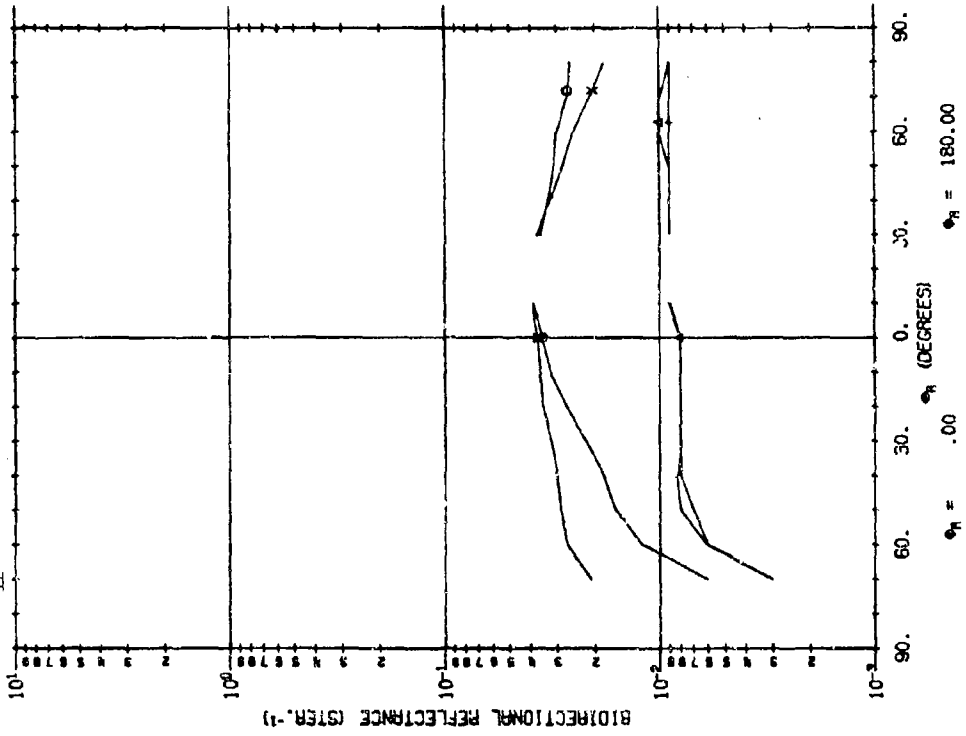
$\epsilon_1 = 70.00$
 $\phi_1 = 0.0$
 $\lambda = 1.06$



A01457 005
 0 II
 + II
 Δ II
 X II

Olive Drab Paint on Louvered Metal Panel

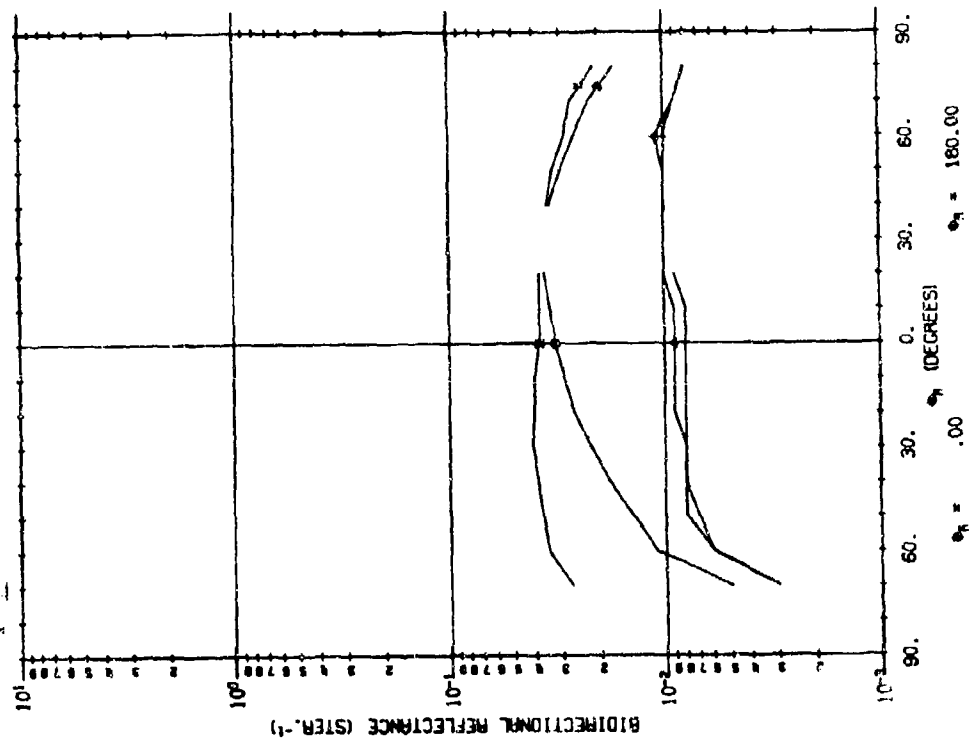
$\epsilon_1 = 20.00$
 $\phi_1 = 180.00$
 $\lambda = 1.06$



A01457 005

Olive Drab Paint on Louvered Metal Panel

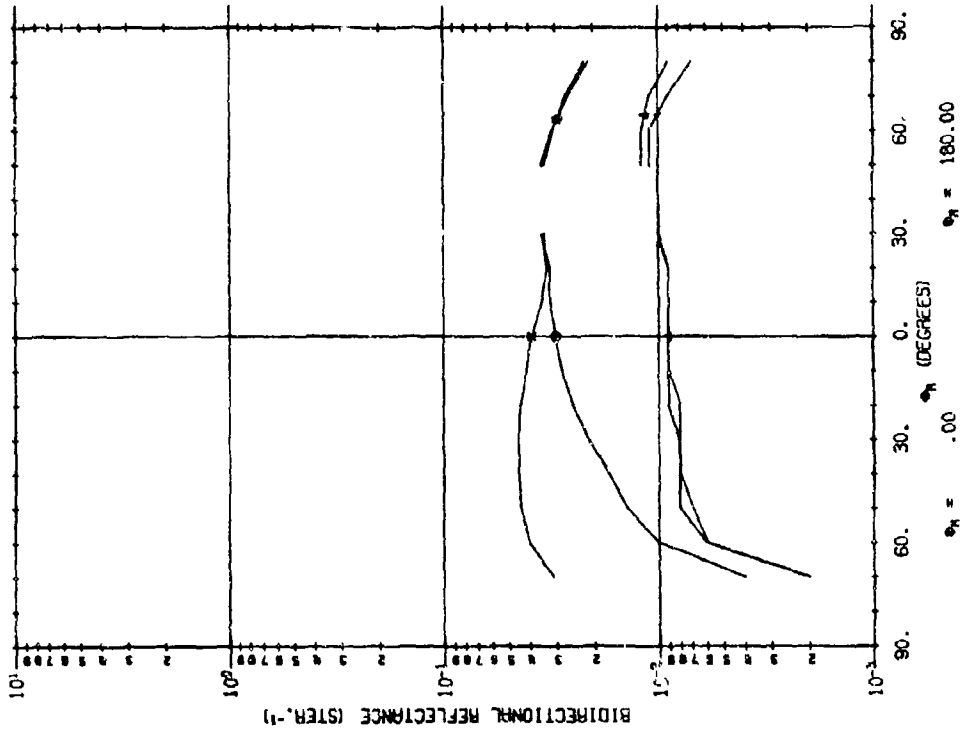
$\theta_i = 30.00$
 $\theta_r = 180.00$
 $\theta_t = 1.06$



A01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_i = 40.00$
 $\theta_r = 180.00$
 $\theta_t = 1.06$

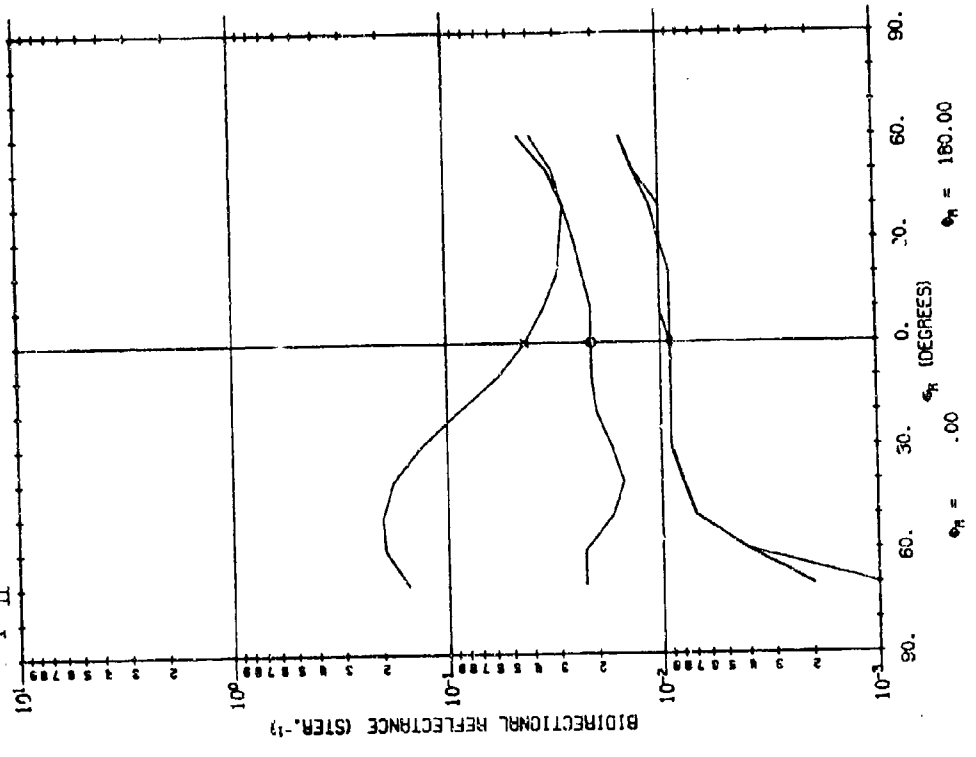


PAINT

A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 70.00$
 $\theta_r = 180.00$
 $\lambda = 1.06$

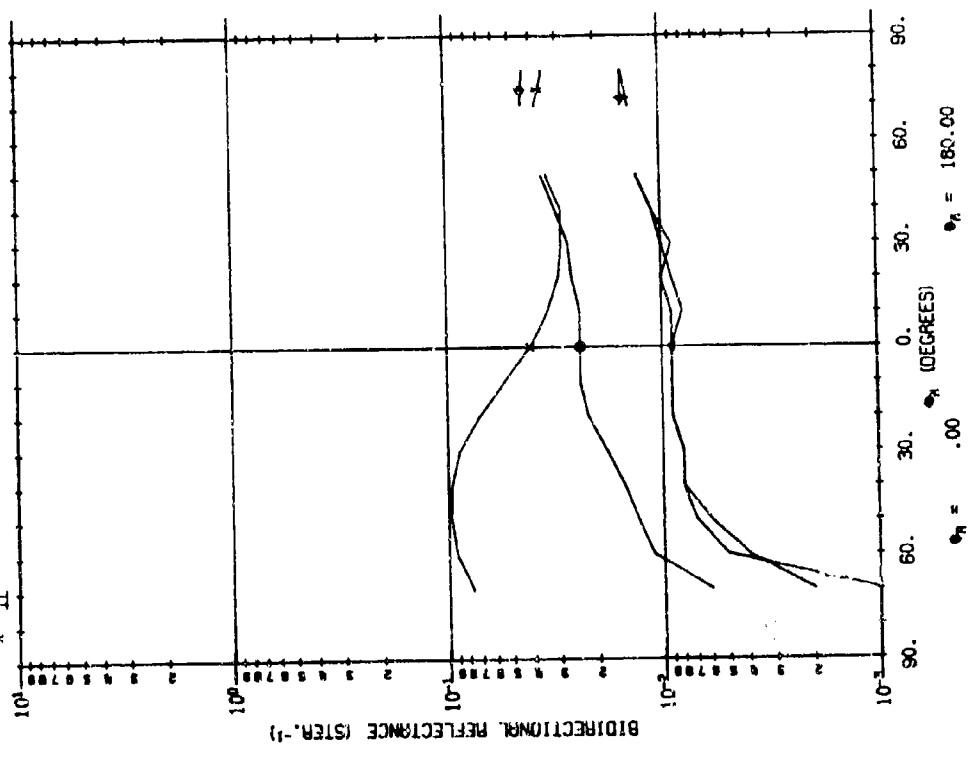
0 ||
 + ||
 Δ ||
 X ||



A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_i = 60.00$
 $\theta_r = 180.00$
 $\lambda = 1.06$

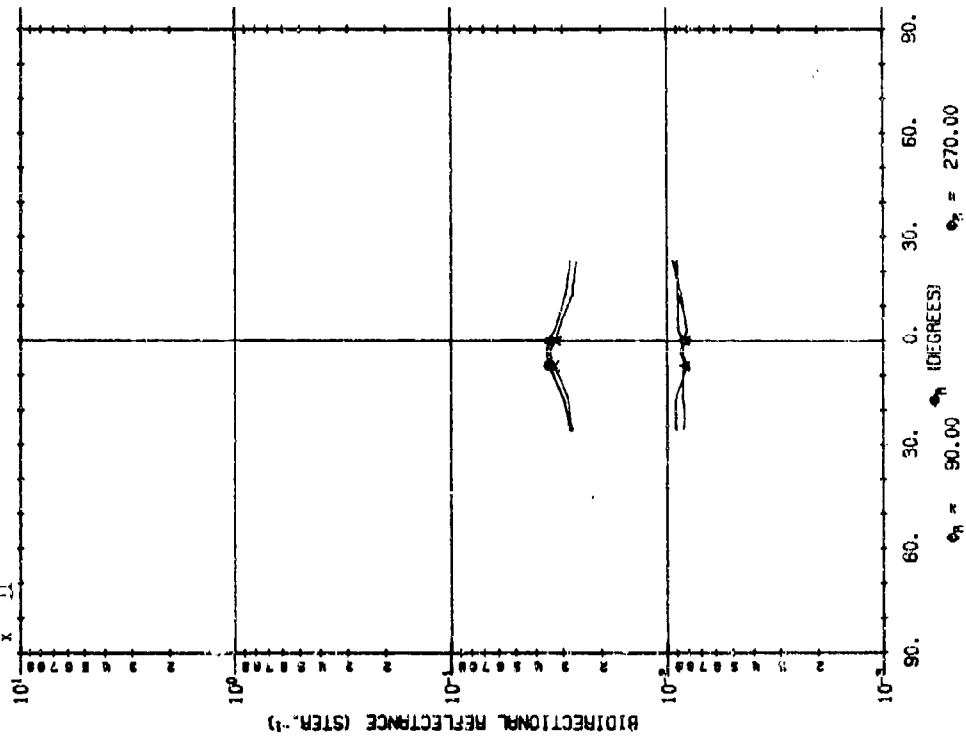
0 ||
 + ||
 Δ ||
 X ||



A01457 005

OLIVE DRAB PAINT ON METAL

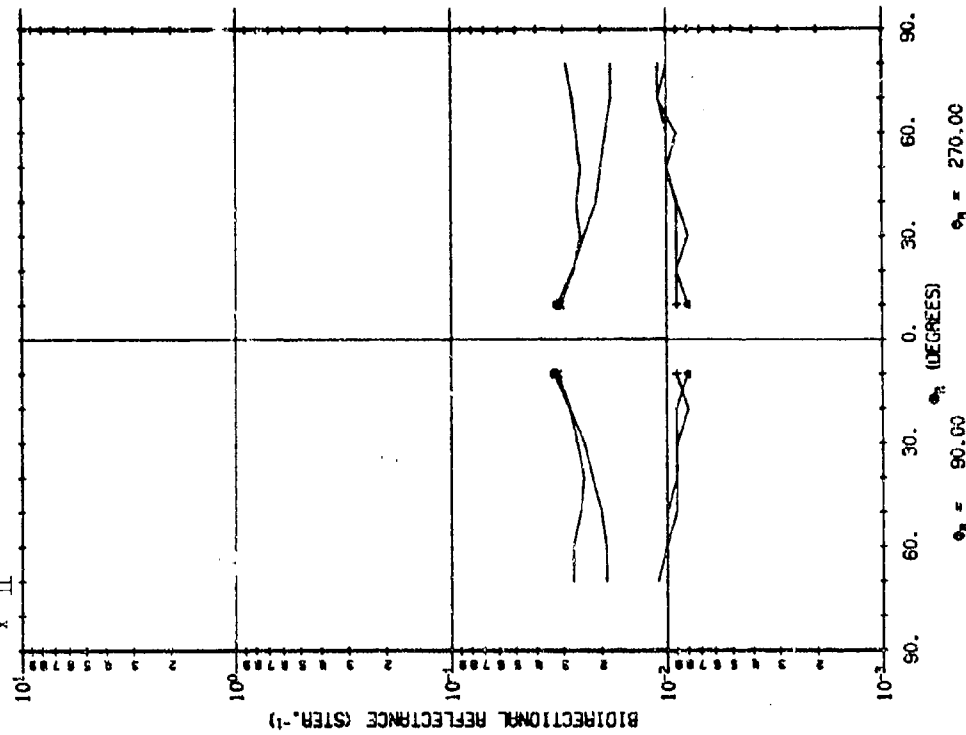
0 || 2E = 7.0
 + || $\phi_1 = \phi_2$
 - || $\phi_1 = 1.06$
 X ||



A01457 005

OLIVE DRAB PAINT ON LEVERED METAL PANEL

0 || $\phi_1 = 0.0$
 + || $\phi_1 = 270.00$
 - || $\lambda = 1.06$
 X ||

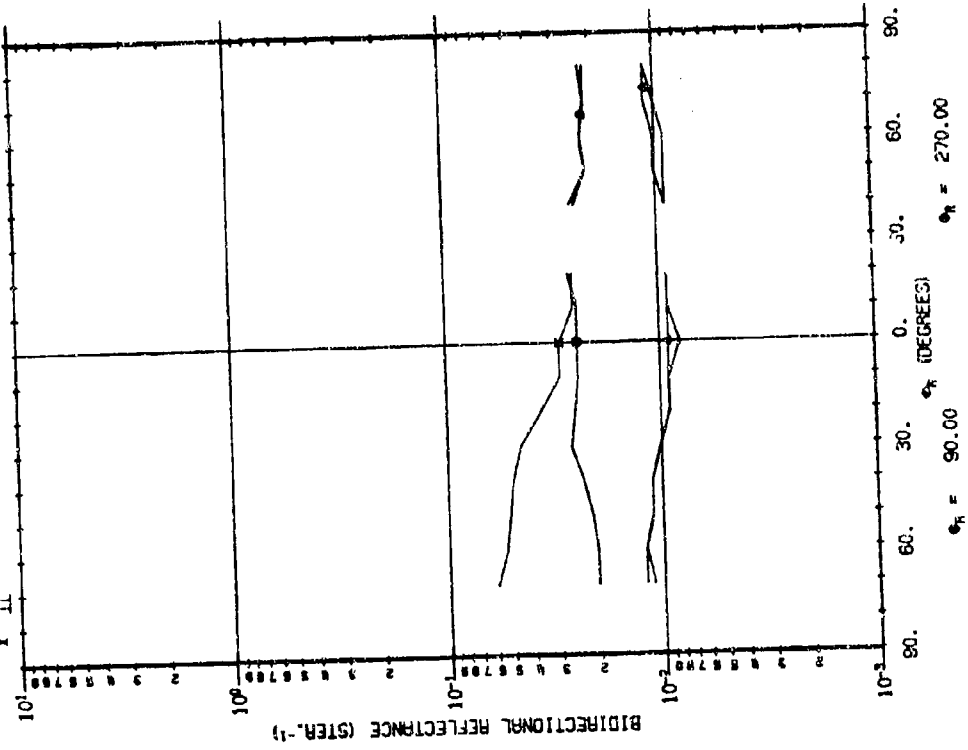


PAINT

A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_1 = 30.00$
 $\phi_1 = 270.00$
 $\lambda = 1.06$

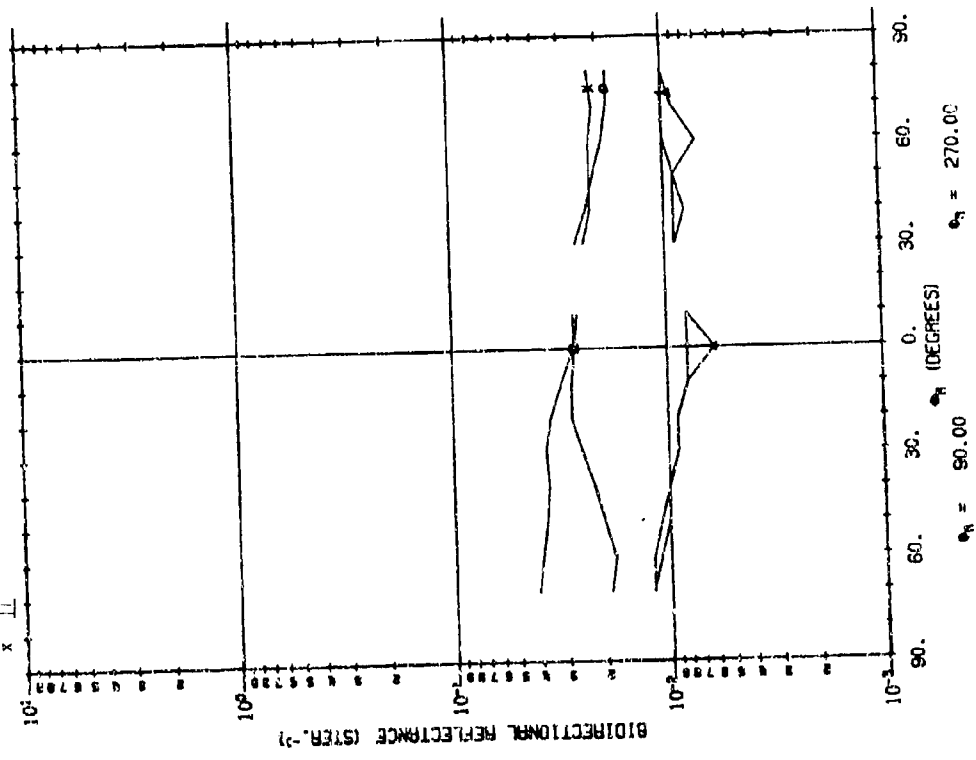
0 || ||
 + || ||
 Δ || ||
 X || ||



A01457 005 Olive Drab Paint on Louvered Metal Panel

$\theta_1 = 20.00$
 $\phi_1 = 270.00$
 $\lambda = 1.06$

0 || ||
 + || ||
 Δ || ||
 X || ||

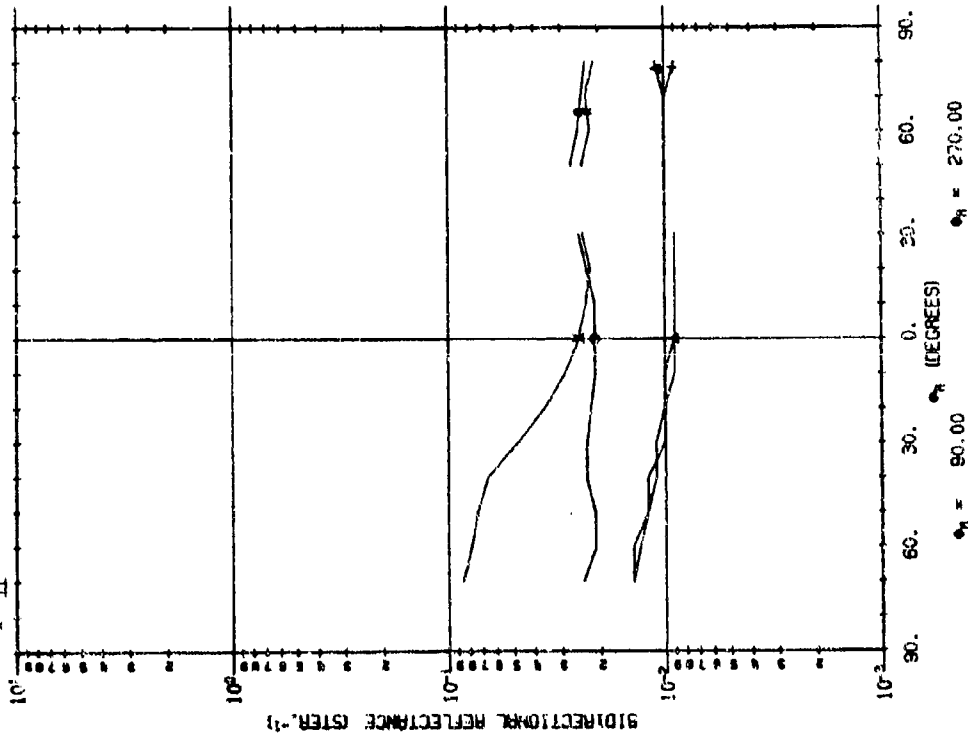


R01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_i = 40.00$
 $\phi_i = 270.00$
 $\lambda = 1.06$

0 || ||
+ || ||
Δ || ||
x || ||

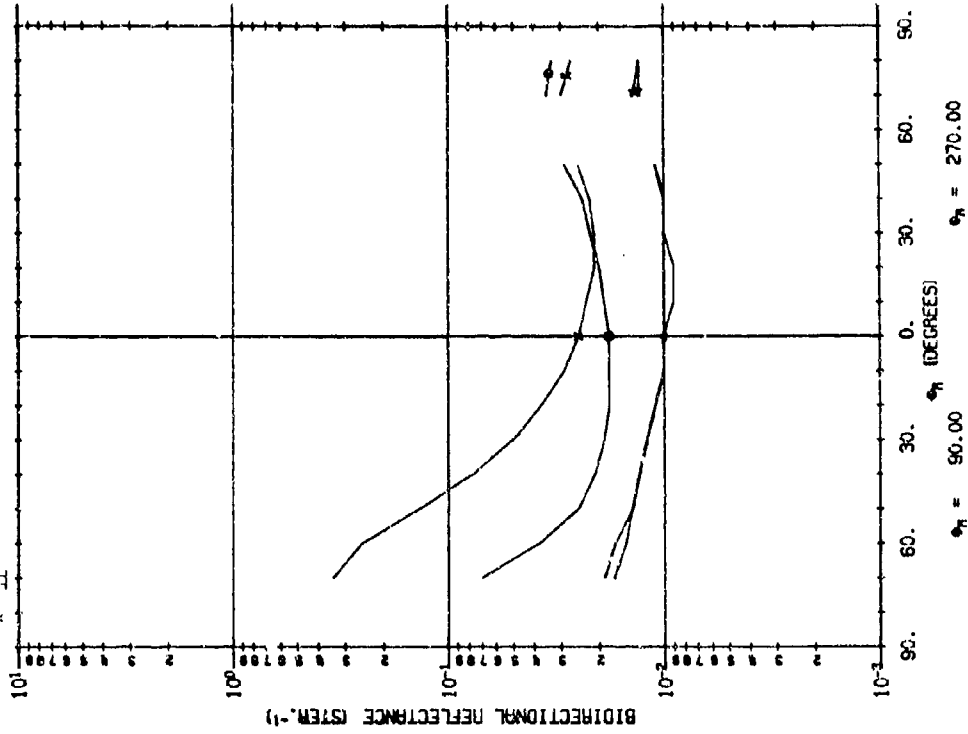


R01457 005

Olive Drab Paint on Louvered Metal Panel

$\theta_i = 60.00$
 $\phi_i = 270.00$
 $\lambda = 1.06$

0 || ||
+ || ||
Δ || ||
x || ||



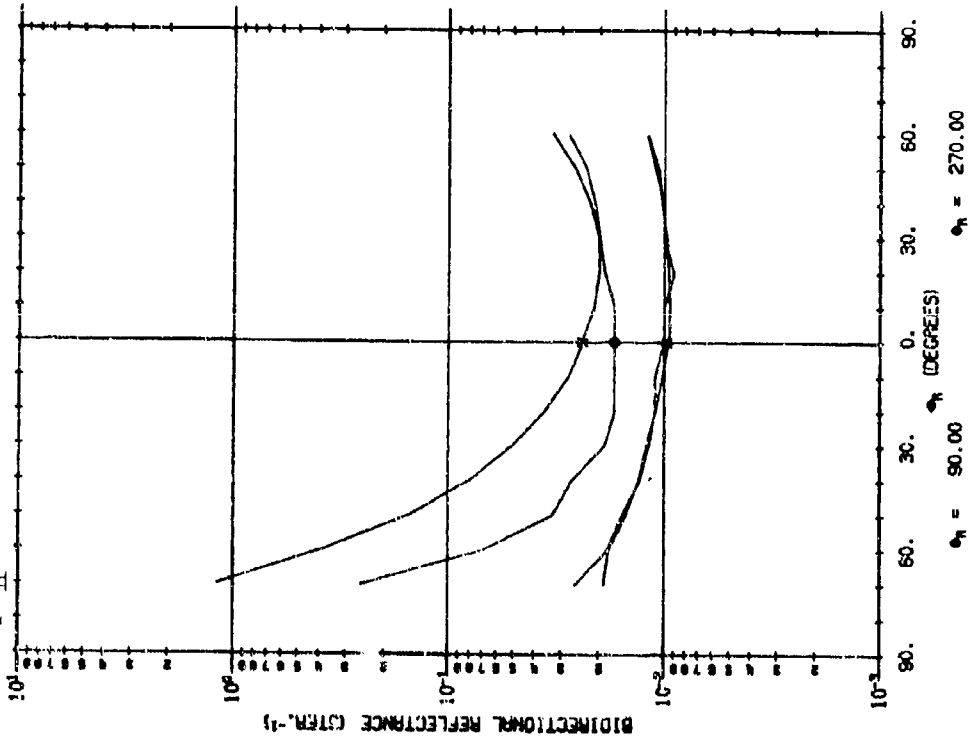
PAINT

R01457 005

Olive Drab Paint on Lowered Metal Panel

$\theta_1 = 70.00$
 $\phi_1 = 270.00$
 $\lambda = 1.06$

0 || ||
 + || ||
 7 || ||
 X || ||

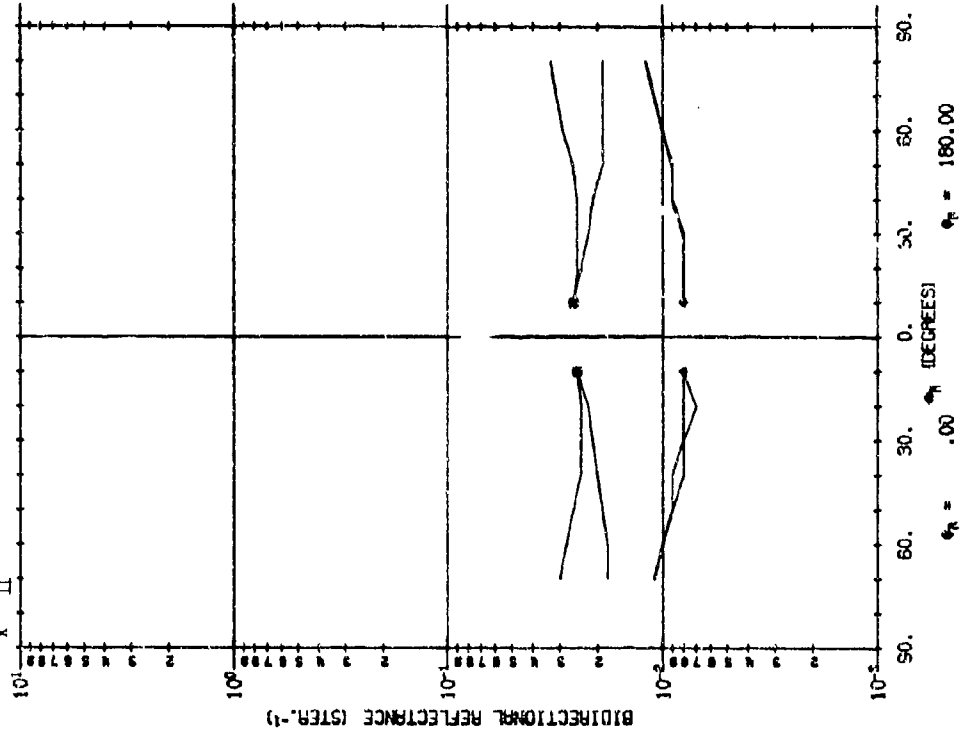


R01509 001

Olive Drab Paint on Steel

$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 0.63$

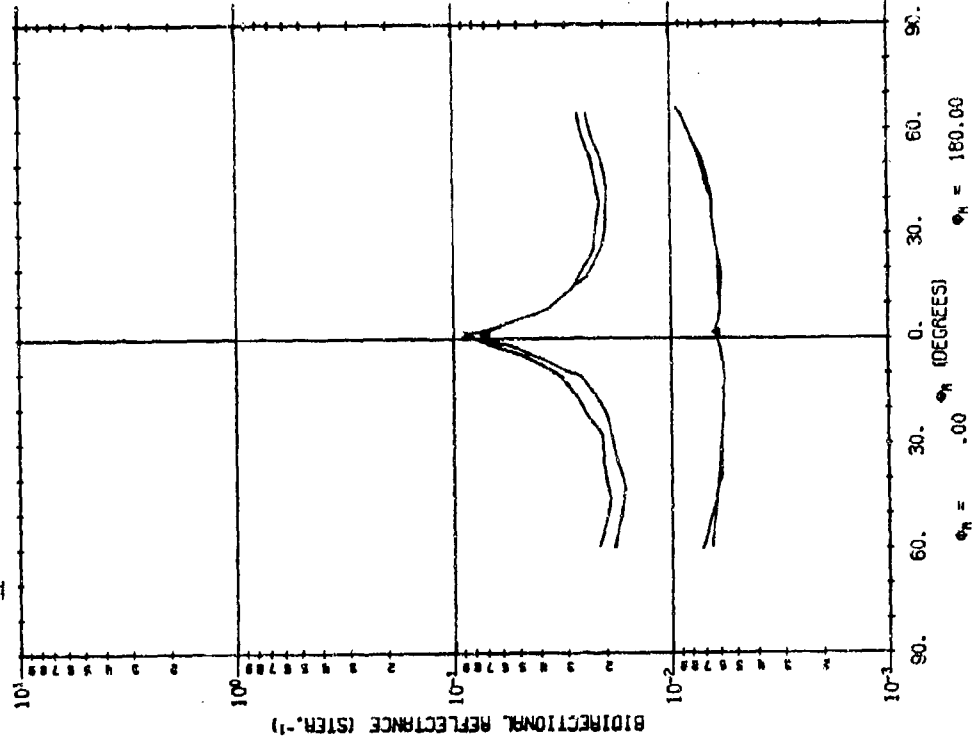
0 || ||
 + || ||
 7 || ||
 X || ||



A01569 003

GREEN PAINT ON STEEL

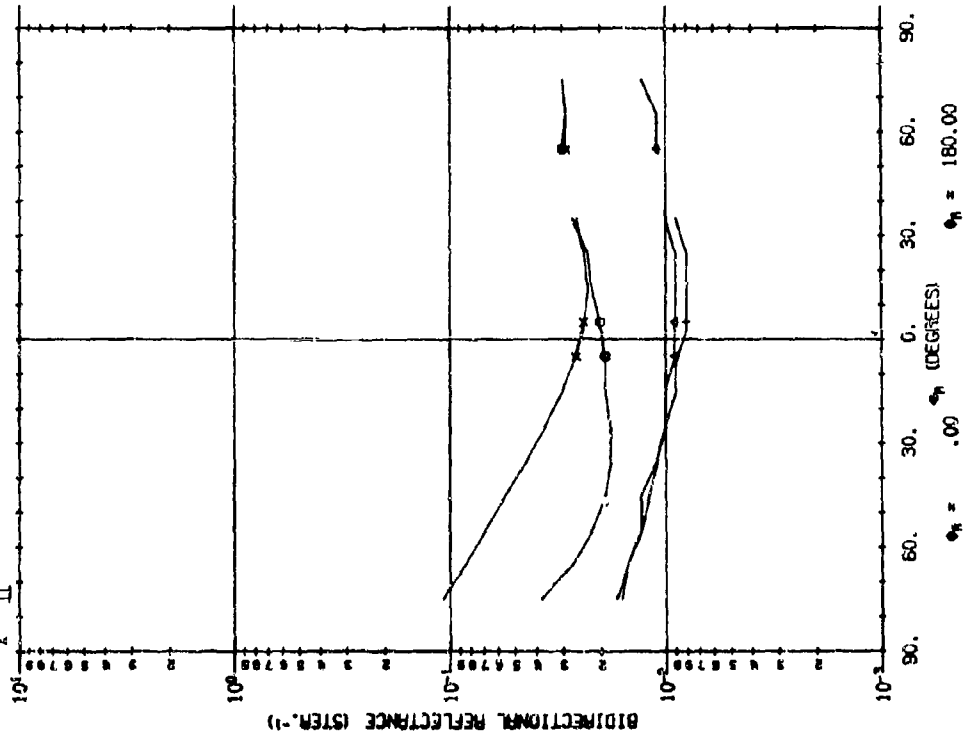
0 || $\theta_i = 2.0$
+ || $\phi_i = \phi_r$
Δ || $\lambda = 0.63$
X ||



A01509 001

OLIVE DRAB PAINT ON STEEL

0 || $\theta_i = 45.0$
+ || $\phi_i = 180.0$
Δ || $\lambda = 0.63$
X ||



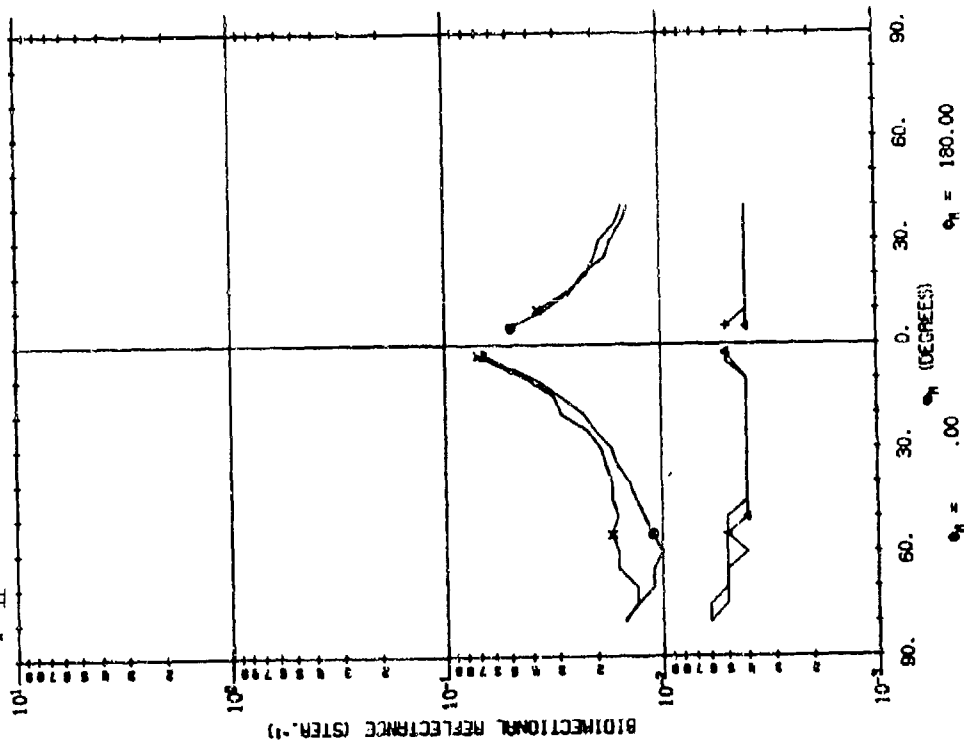
PAINT

A01569 003

Green Paint on Steel

$\theta_1 = 0.0$
 $\theta_2 = 180.00$
 $\lambda = 0.63$

0 || ||
 + || ||
 Δ || ||
 X || ||

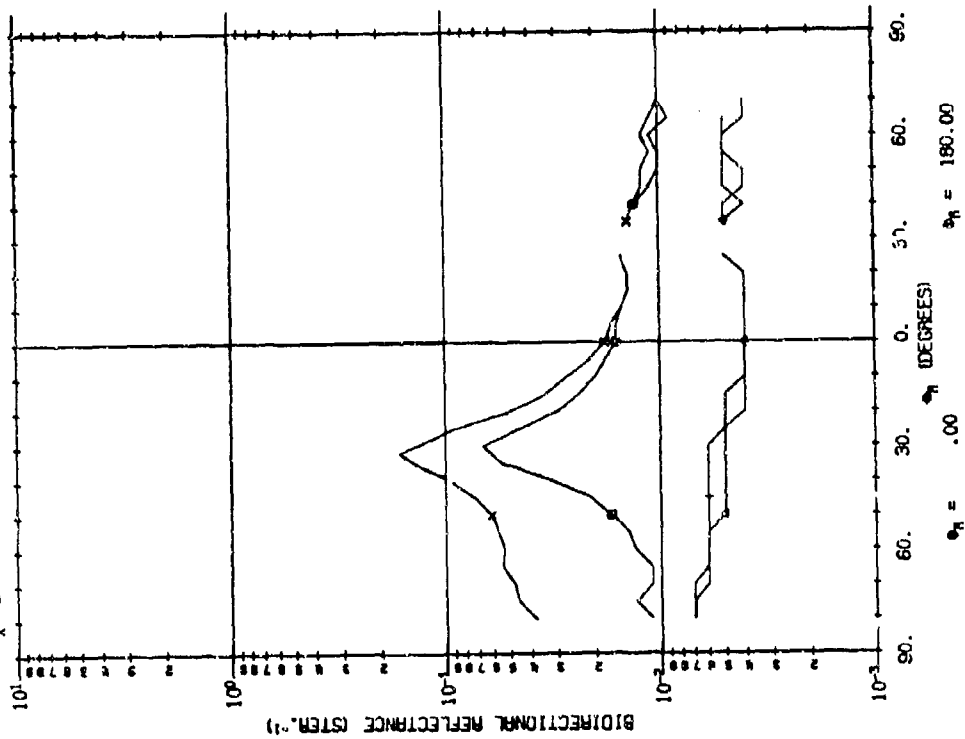


A01569 003

Green Paint on Steel

$\theta_1 = 30.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$

0 || ||
 + || ||
 Δ || ||
 X || ||

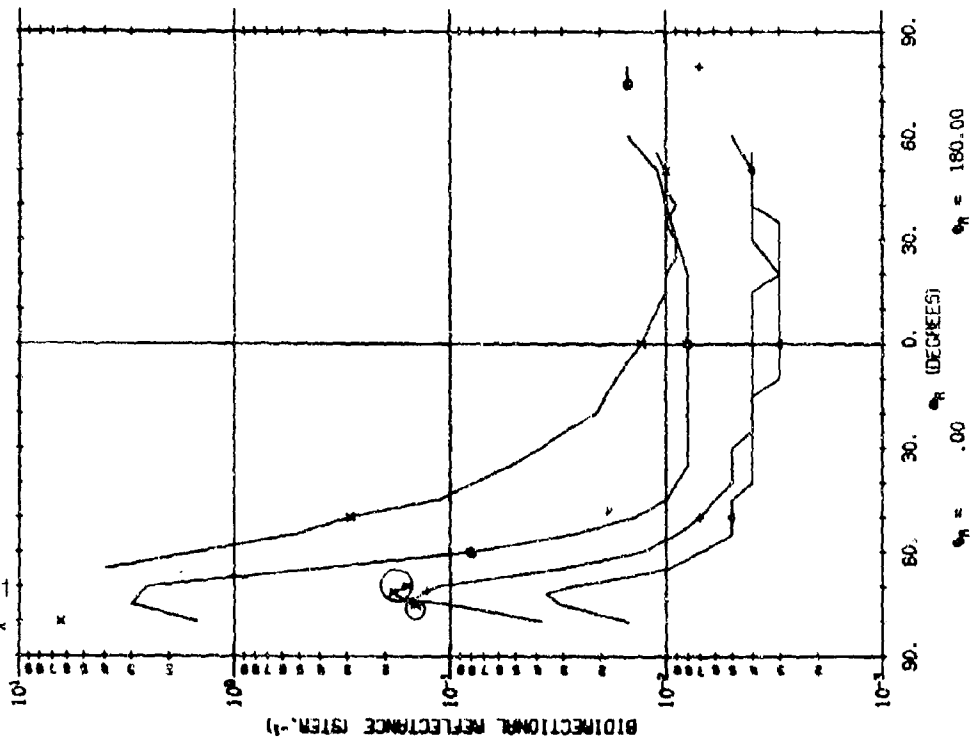


A01569 003

Green Paint on Steel

$\theta_2 = 70.00$
 $\theta_1 = 180.00$
 $\lambda = 0.63$

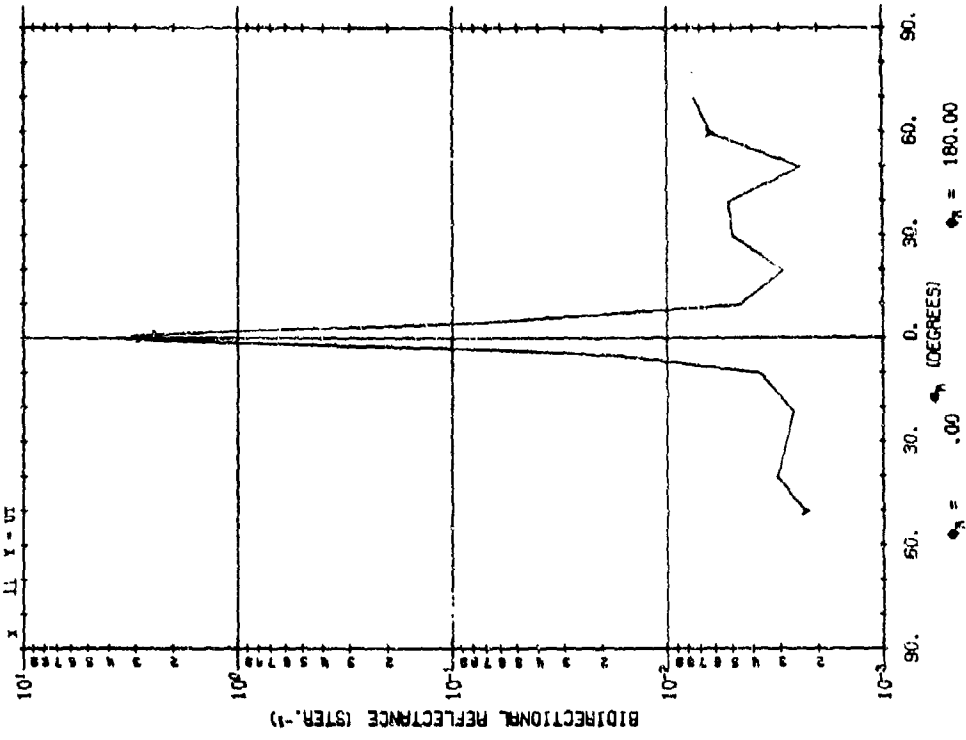
0 ||
 + ||
 Δ ||
 X ||



A01569 004

GREEN PAINT ON STEEL

0 || $\theta_2 = 1.0$
 + || $\theta_1 = 90$
 Δ || $\lambda = 10.6$
 X || Y-VT

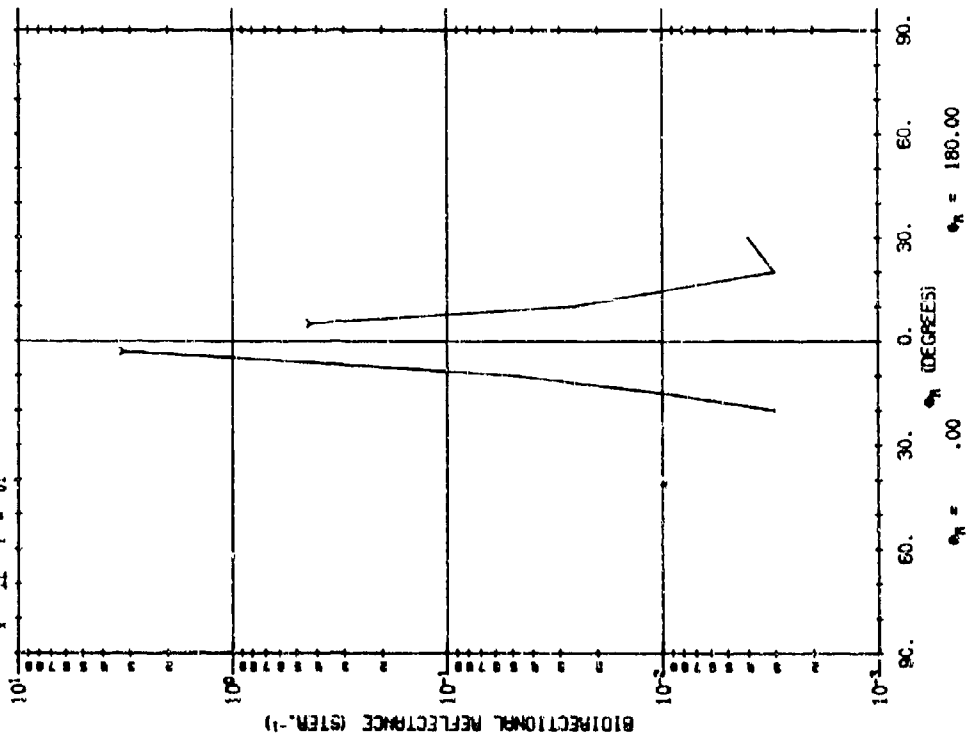


PAINT

A01569 004

Green Paint on Steel

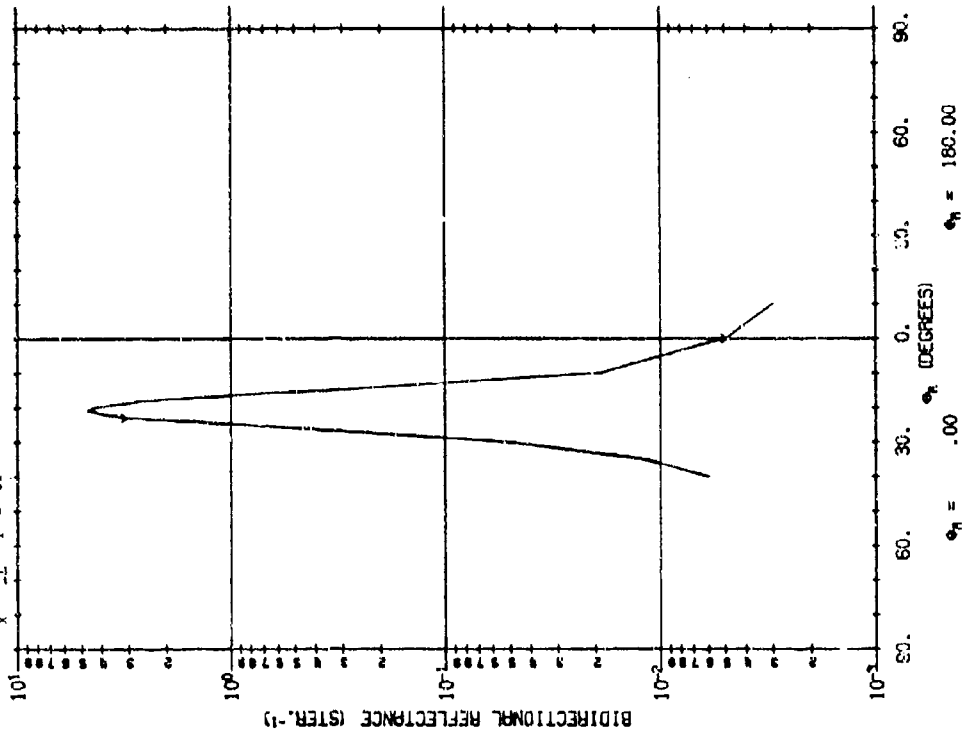
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.00$
x || $\lambda = 10.6$
|| $\gamma = \nu$



A01569 004

Green Paint on Steel

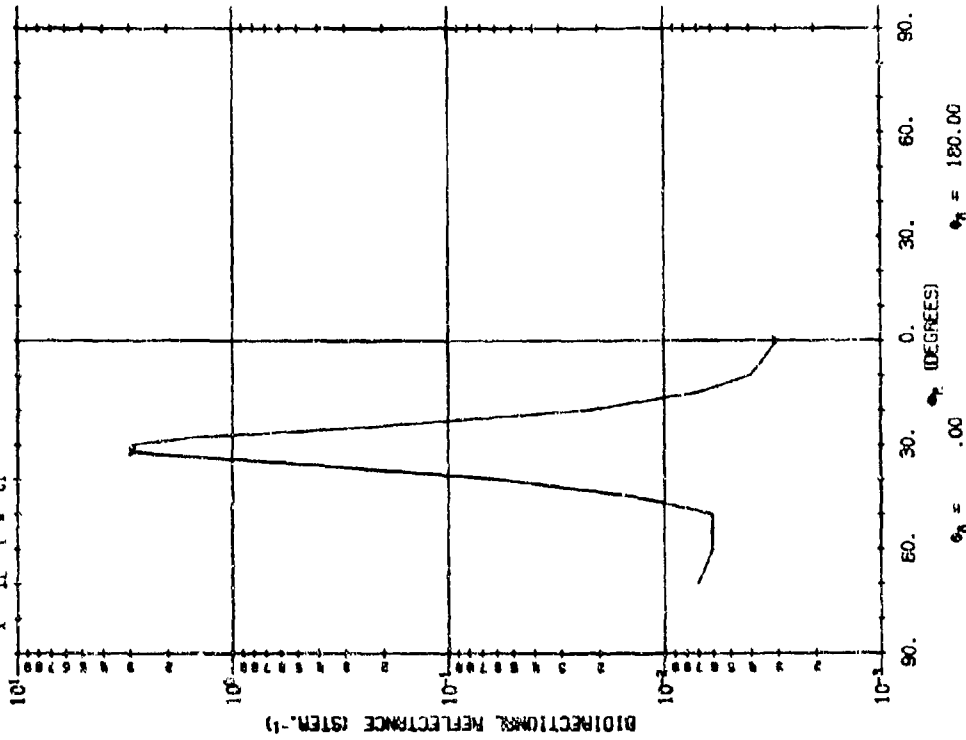
0 || $\phi_1 = 20.00$
+ || $\phi_2 = 180.00$
x || $\lambda = 10.6$
|| $\gamma = \nu$



A01569 004

Green Paint on Steel

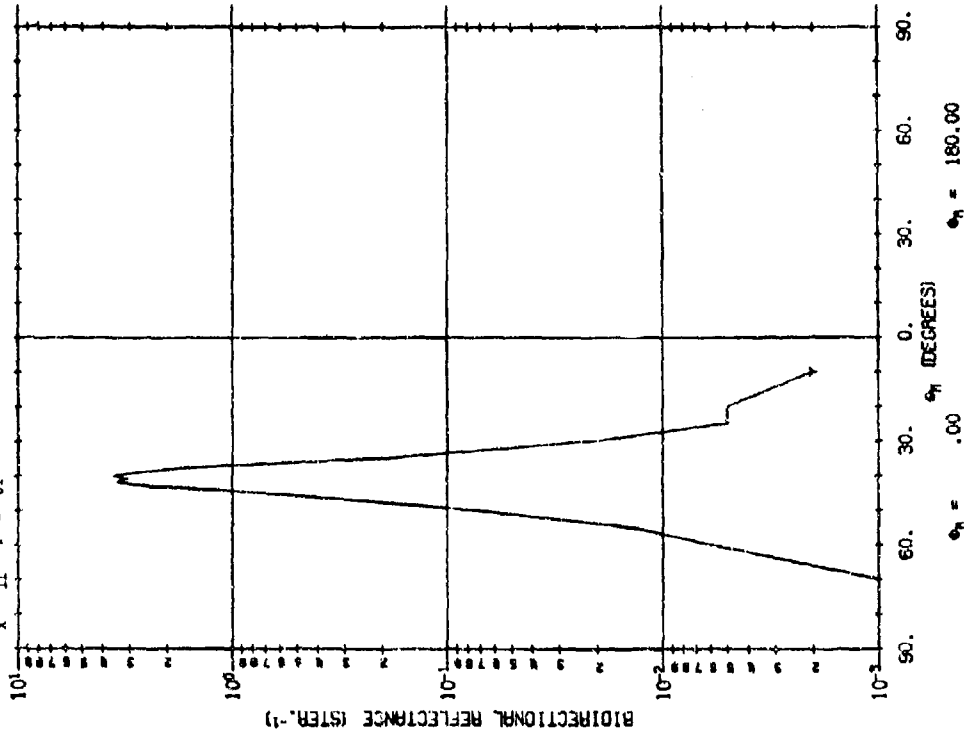
G || $\rho_1 = 30.00$
 + || $\rho_2 = 180.00$
 A || $\lambda = 10.6$
 X || Y = UT



A01569 004

Green Paint on Steel

G || $\rho_1 = 40.00$
 + || $\rho_2 = 180.00$
 A || $\lambda = 10.5$
 X || Y = UT

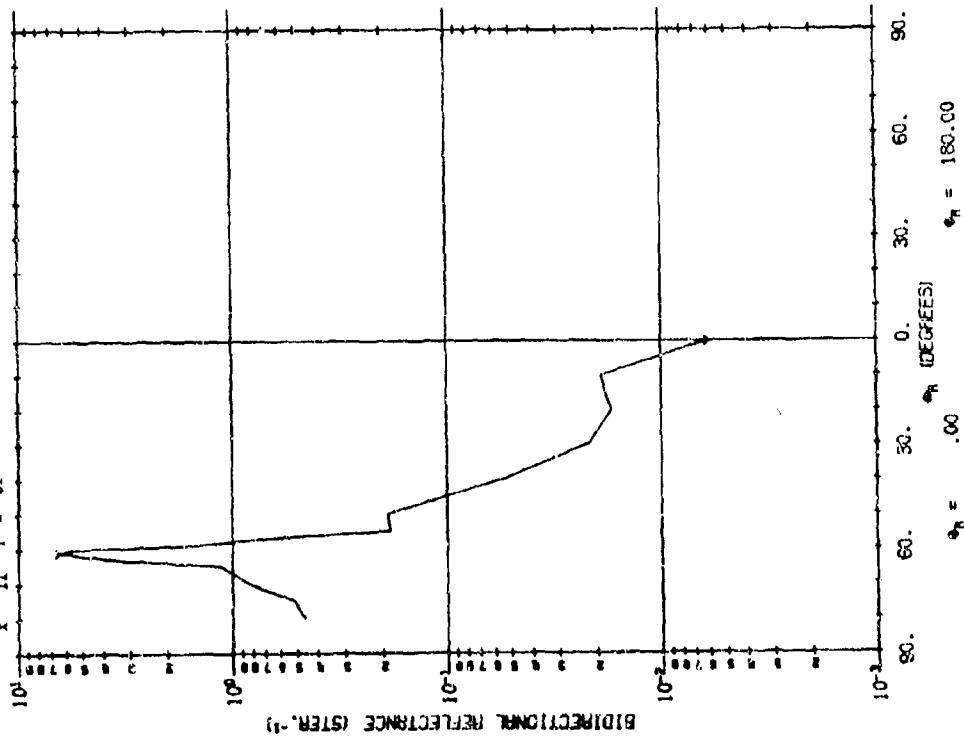


PAINT

R01569 004

Green Paint on Steel

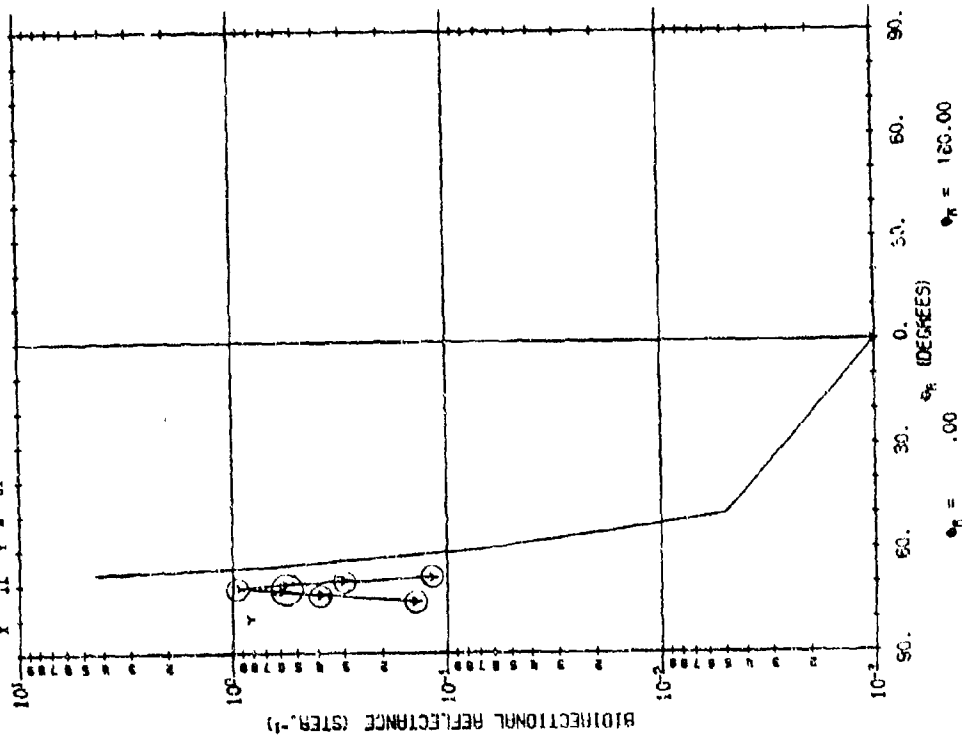
0 // $\theta_1 = 60.00$
+ // $\theta_2 = 180.00$
Δ // $\lambda = 10.6$
X // Y = VI



R01569 004

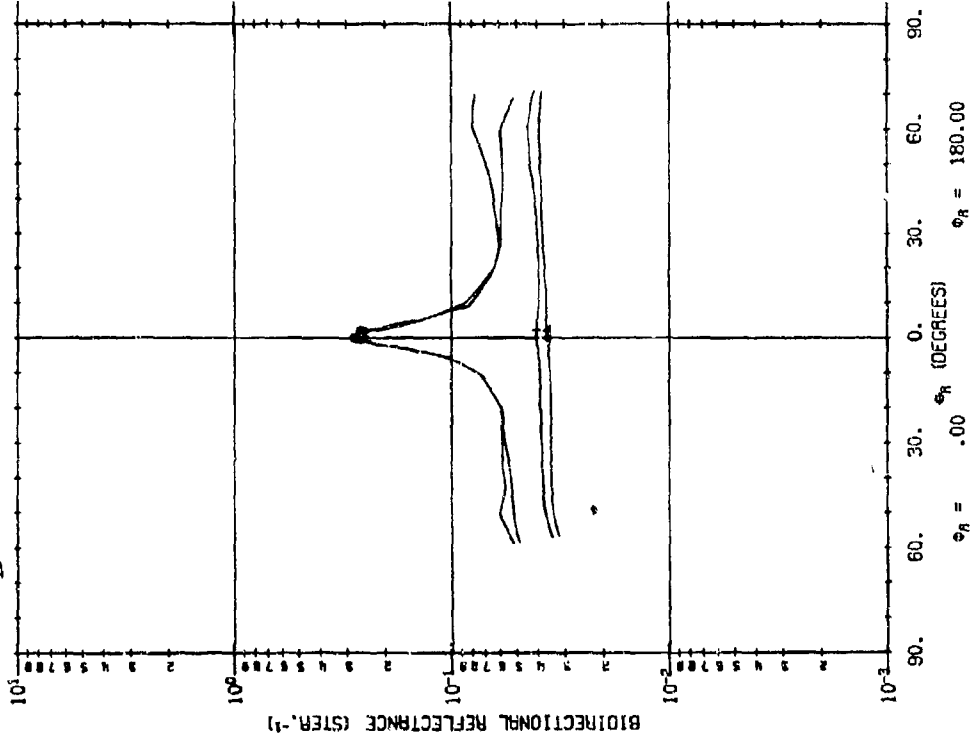
Green Paint on Steel

0 // $\theta_1 = 70.00$
+ // $\theta_2 = 180.00$
Δ // $\lambda = 10.6$
X // Y = VI



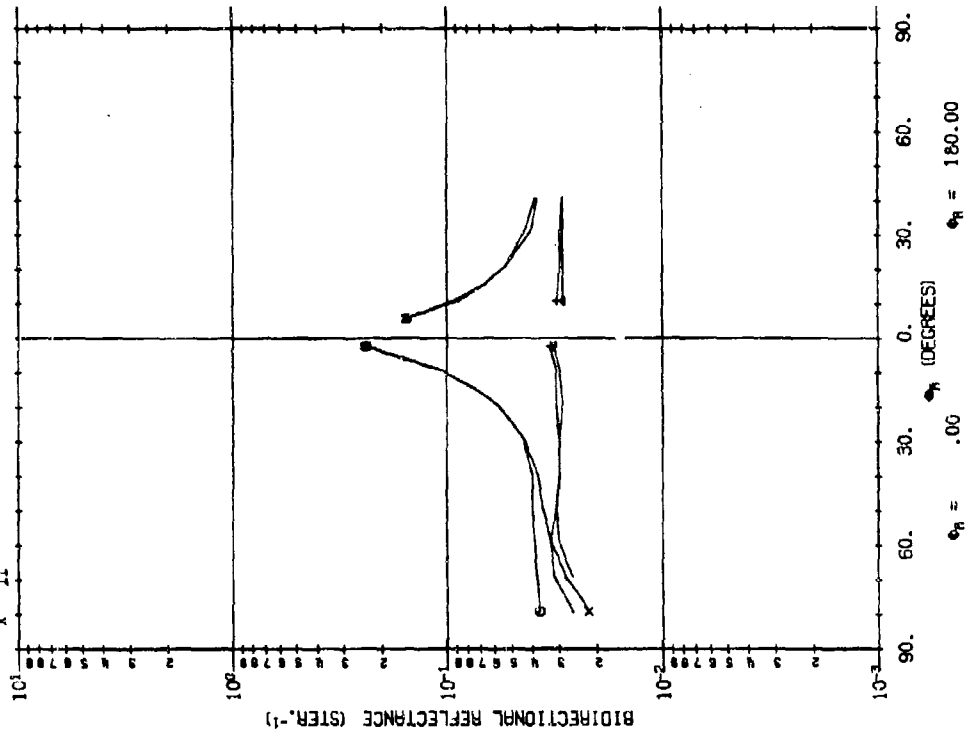
R01570 004
 LIGHT BROWN PAINT ON METAL

0 || 2₁ = 2.0
 + || $\phi_1 = \phi_2$
 Δ || $\phi_1 = 180.00$
 x || $\lambda = 0.63$



R01570 004
 Light Brown Paint on Metal

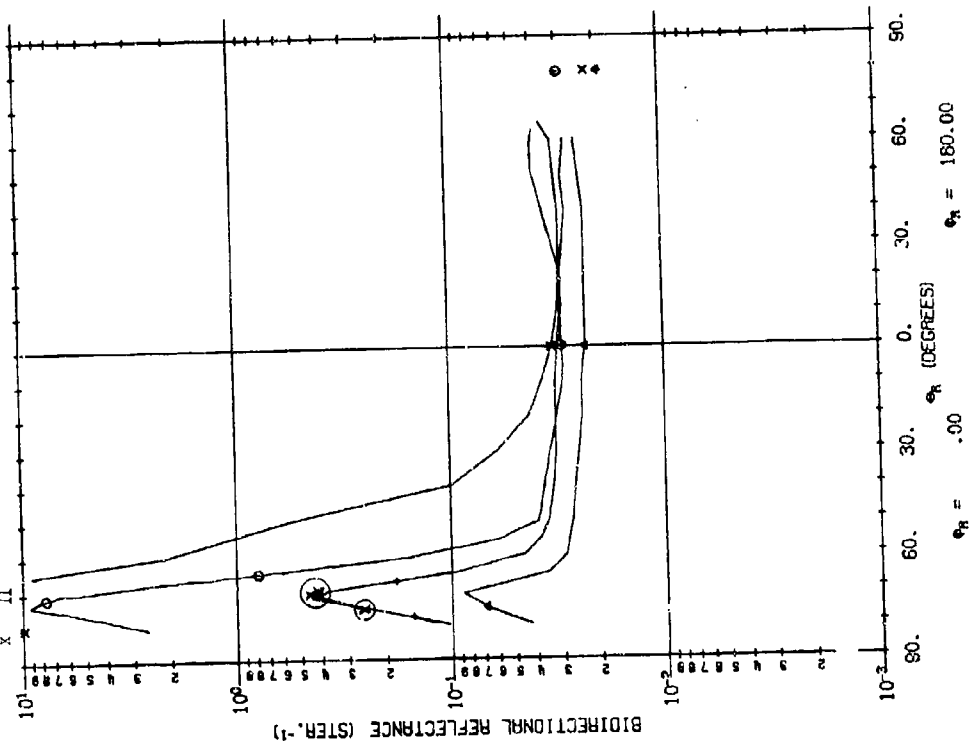
0 || $\phi_1 = 0.0$
 + || $\phi_1 = 180.00$
 Δ || $\lambda = 0.63$
 x ||



PAINT

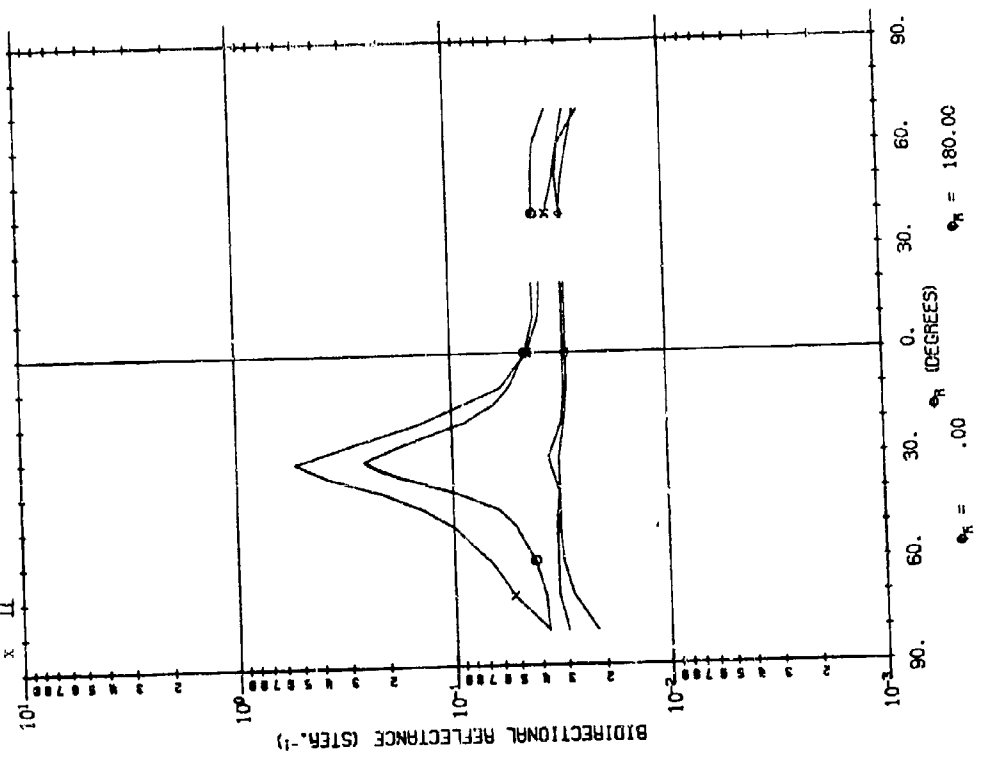
A01570 004
Light Brown Paint on Metal

0 || $\epsilon_1 = 70.00$
+ || $\epsilon_2 = 180.00$
A || $\lambda = 0.63$
X ||



A01570 004
Light Brown Paint on Metal

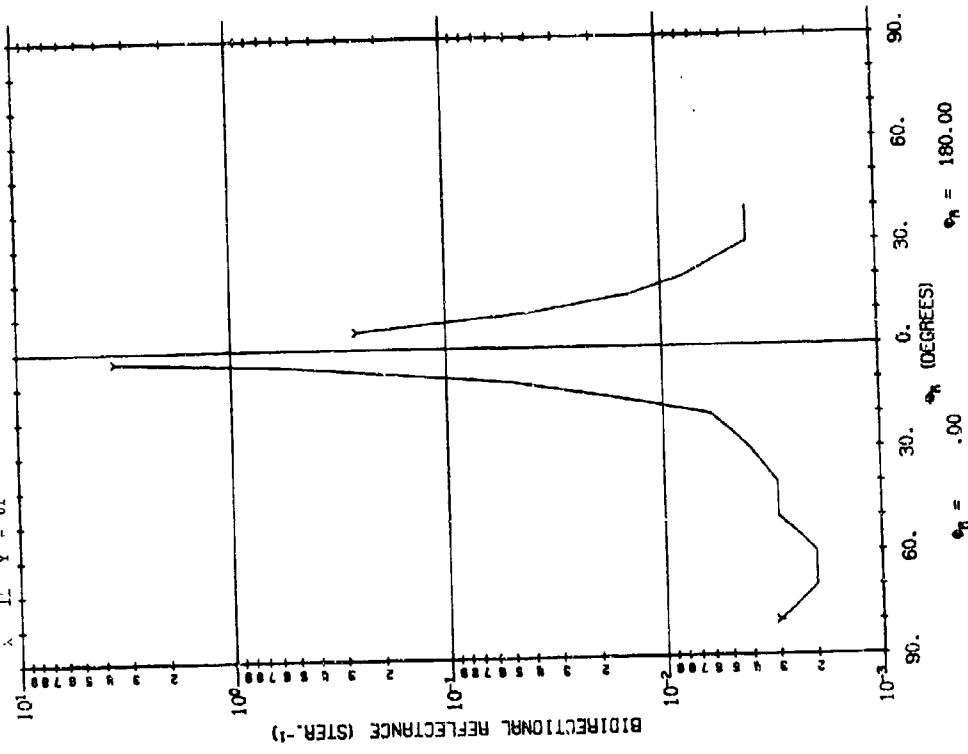
0 || $\epsilon_1 = 30.00$
+ || $\epsilon_2 = 180.00$
A || $\lambda = 0.63$
X ||



R01570 003

Light Brown Paint on Metal

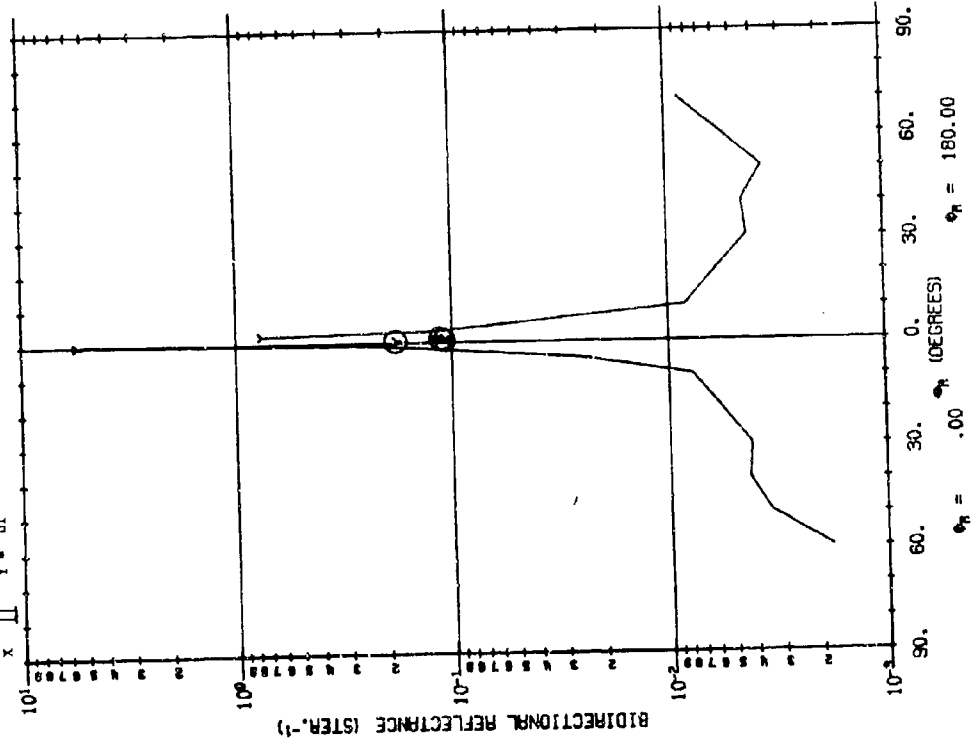
0 || $\theta_1 = 0.0$
+ || $\phi_1 = 180.00$
 Δ || $\lambda = 10.6$
X || Y - UT



R01570 003

LIGHT BROWN PAINT ON METAL

0 || $2\theta = 1.1$
+ || $\phi_1 = \phi_2$
 Δ || $\lambda = 10.6$
X || Y - UT

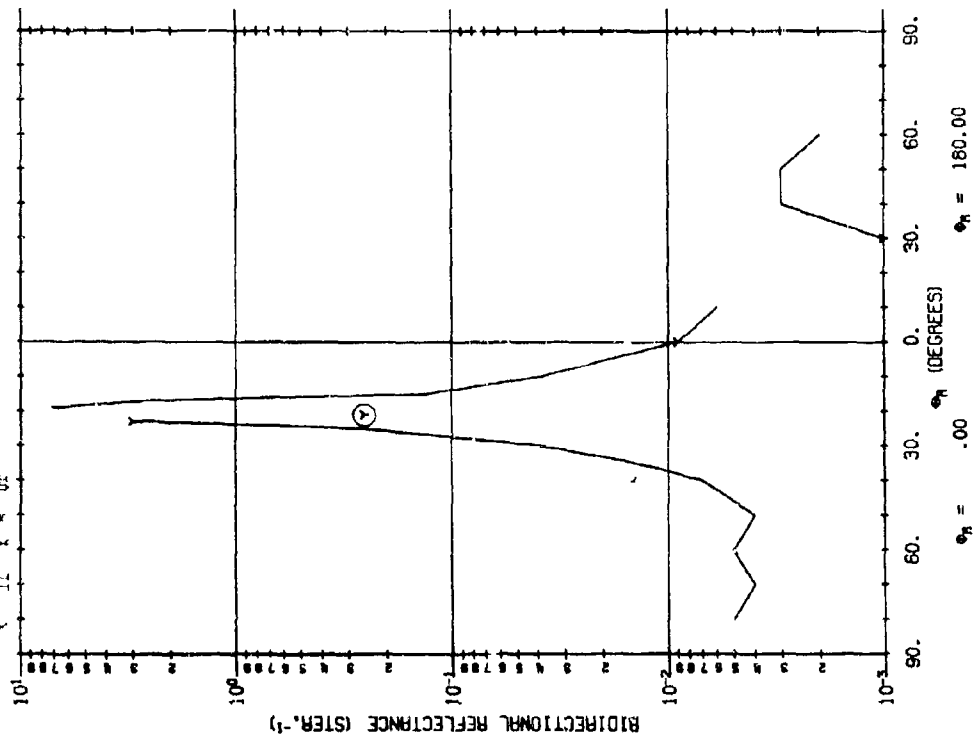


PAINT

R01570 003

Light Brown Paint on Metal

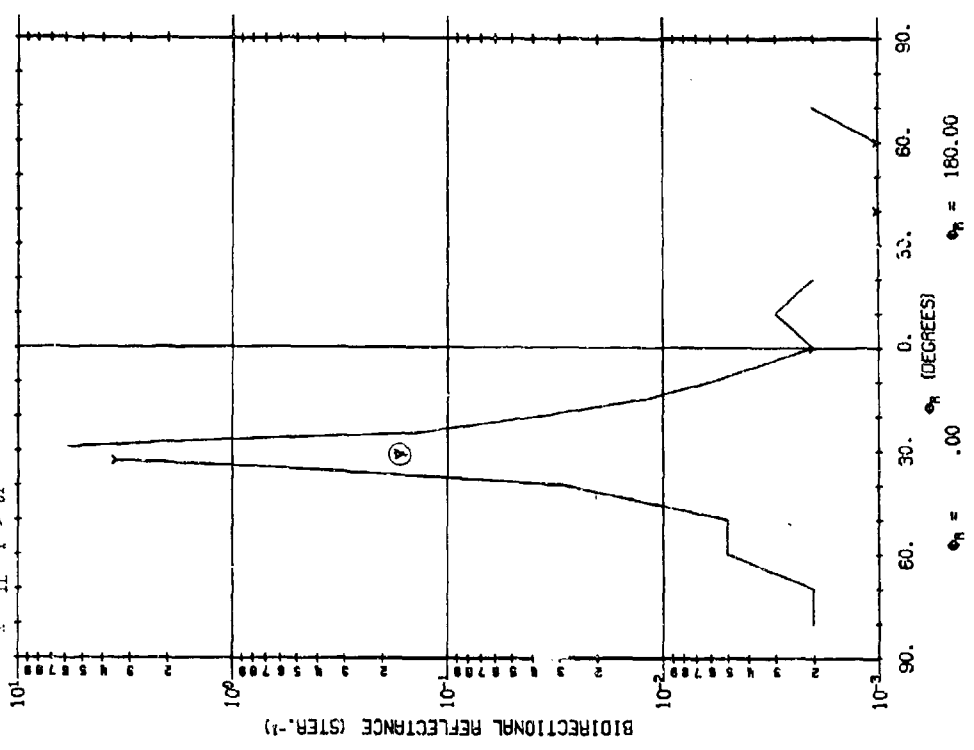
0 // $\theta_1 = 20.00$
+ // $\theta_2 = 180.00$
△ // $\lambda = 10.6$
▽ // X = VT



R01570 003

Light Brown Paint on Metal

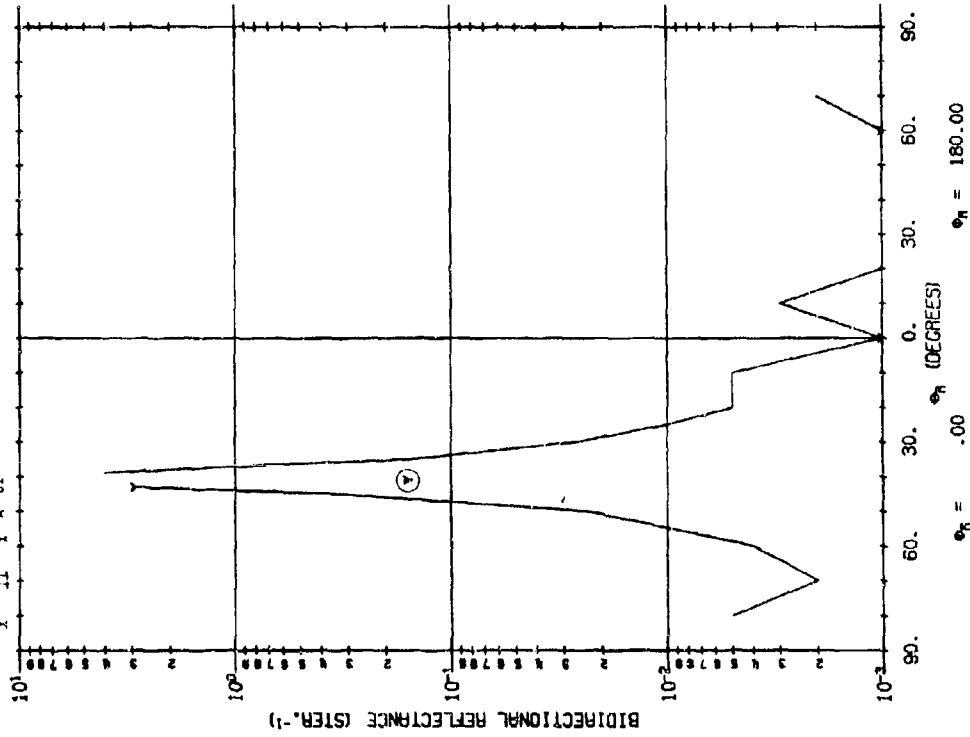
0 // $\theta_1 = 30.00$
+ // $\theta_2 = 180.00$
△ // $\lambda = 10.6$
▽ // X = VT



A01570 003

Light Brown Paint on Metal

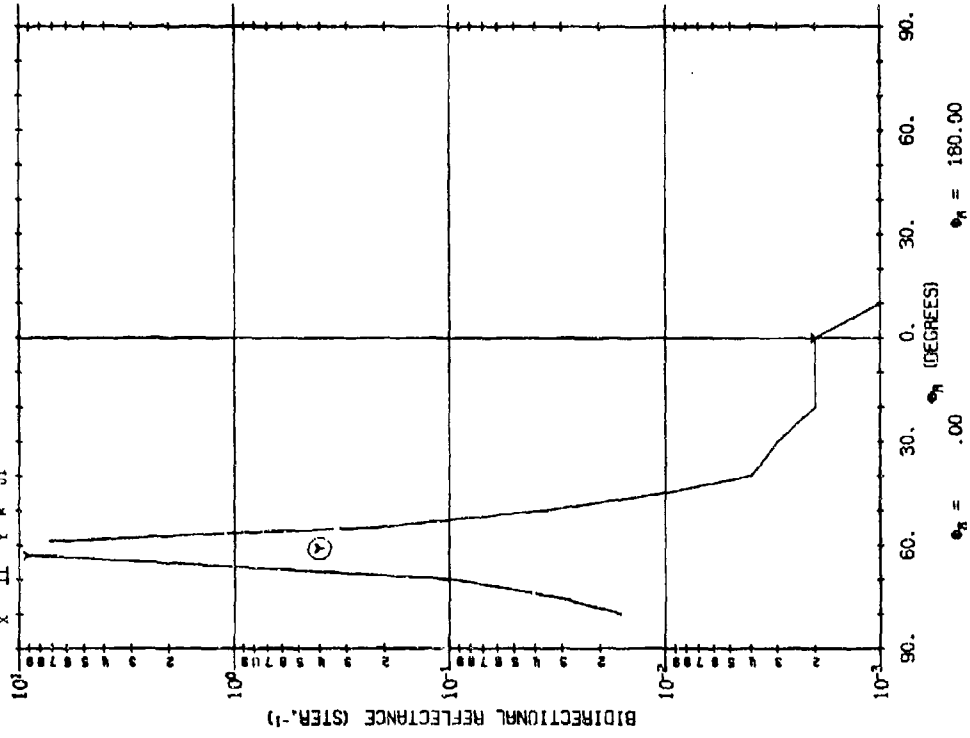
0 || $\theta_1 = 40.00$
+ || $\theta_2 = 180.00$
Δ || $\lambda = 10.6$
X || Y M UT



A01570 003

Light Brown Paint on Metal

0 || $\theta_1 = 60.00$
+ || $\theta_2 = 180.00$
Δ || $\lambda = 10.6$
X || Y M UT



PAINT

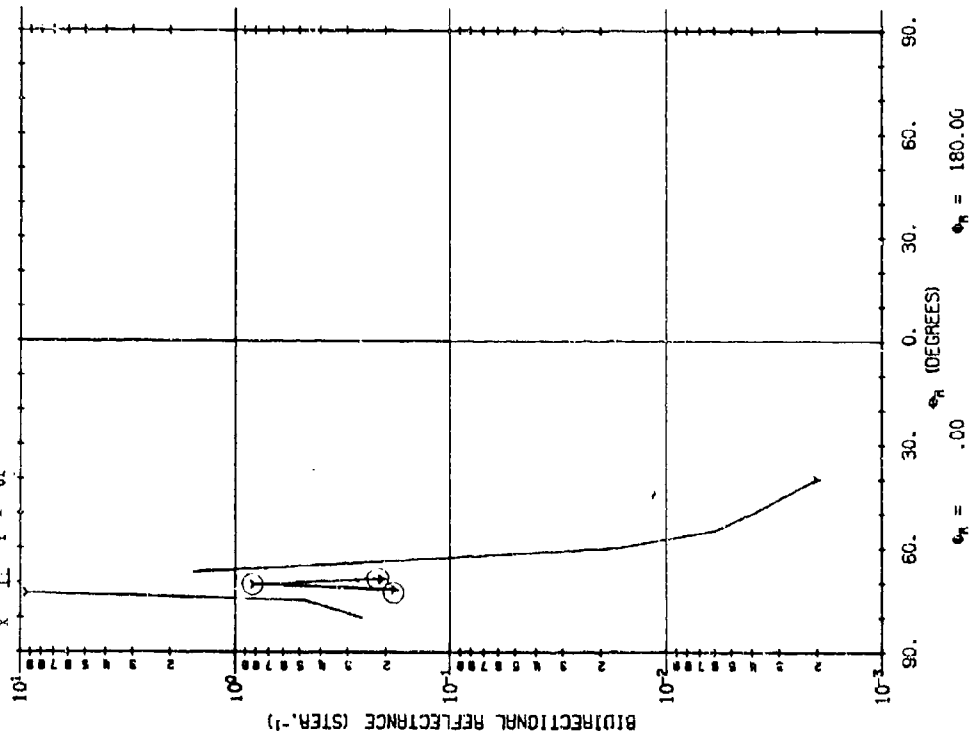
A01570 003

Light Brown Paint on Metal

$\theta_1 = 70.00$
 $\theta_2 = 180.00$
 $\lambda = 10.6$
Y = VI

0 ||
+ ||
Δ ||
X ||

ZZ = 1.10
r = r
λ = 10.6
Y = VI

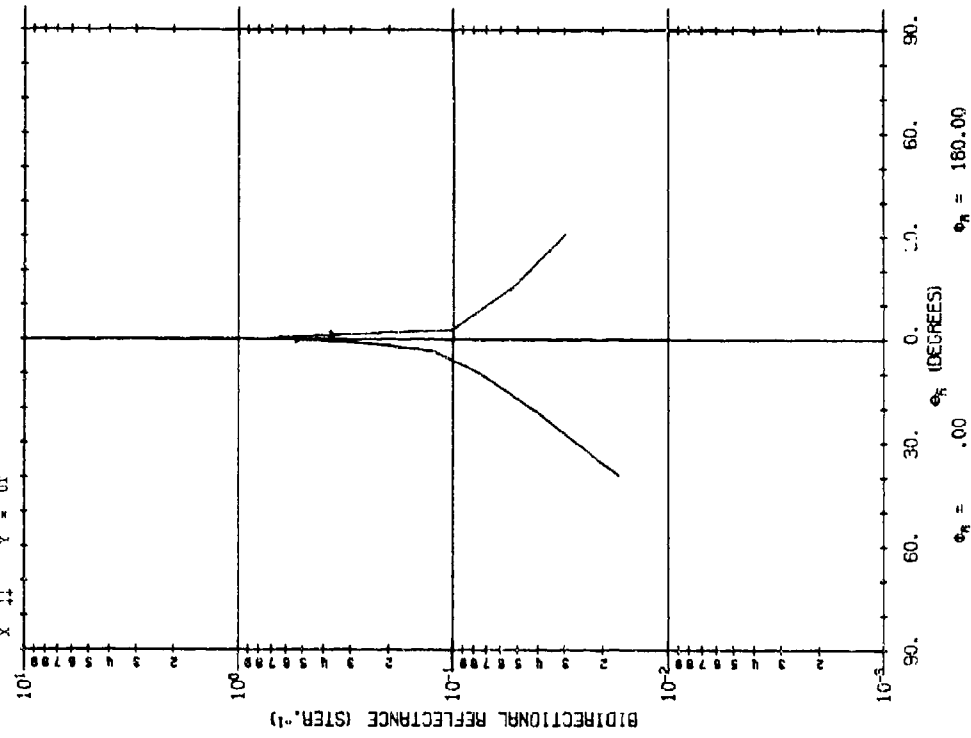


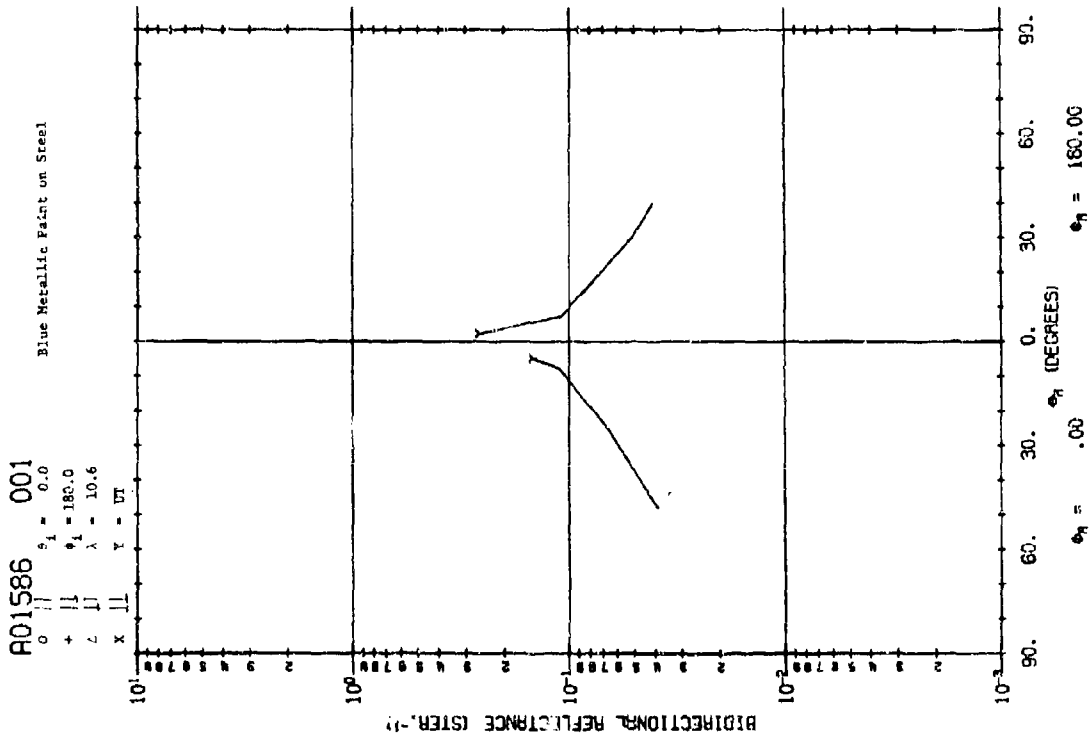
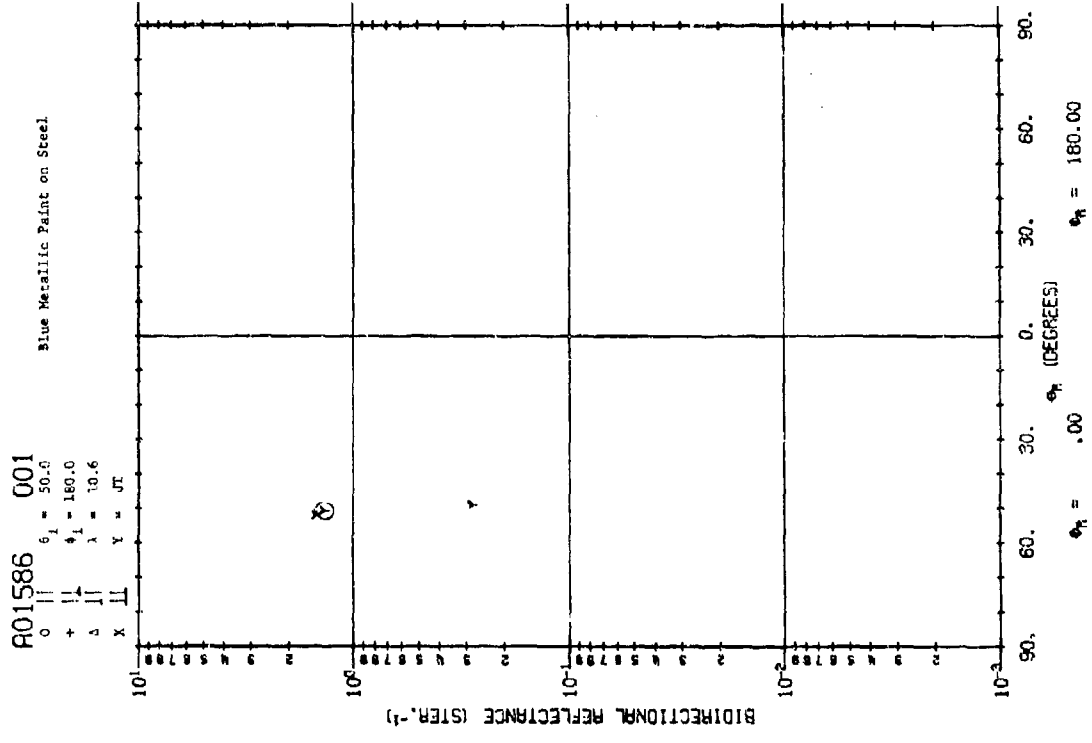
A01586 001

Blue Metallic Paint on Steel

0 ||
+ ||
Δ ||
X ||

ZZ = 1.10
r = r
λ = 10.6
Y = VI



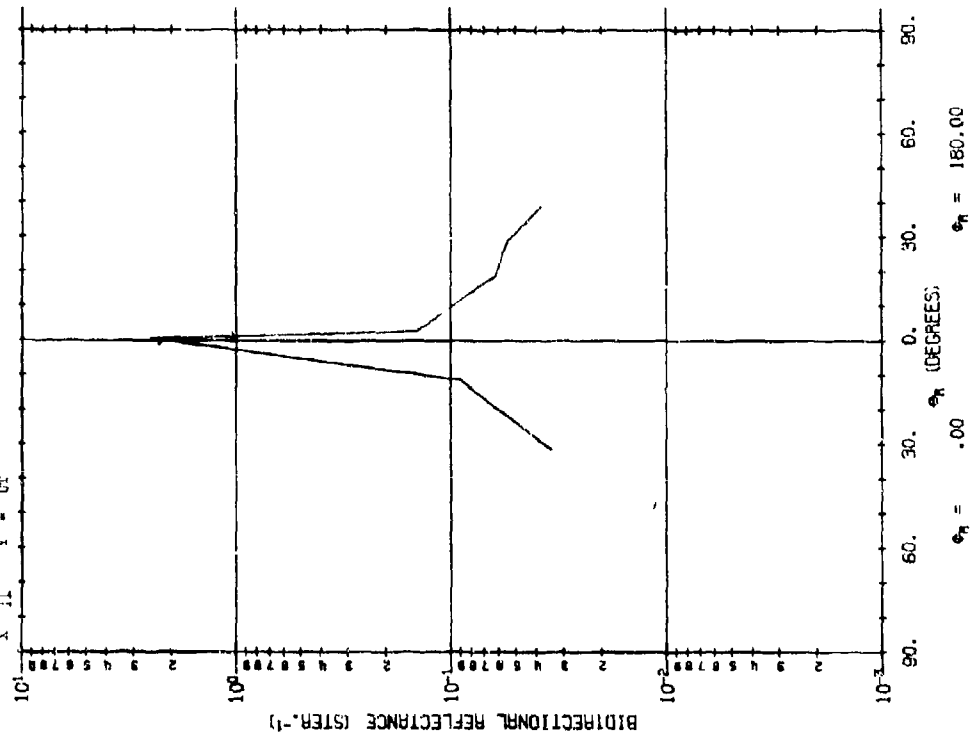


PAINT

A01587 001

Green Metallic Paint on Steel

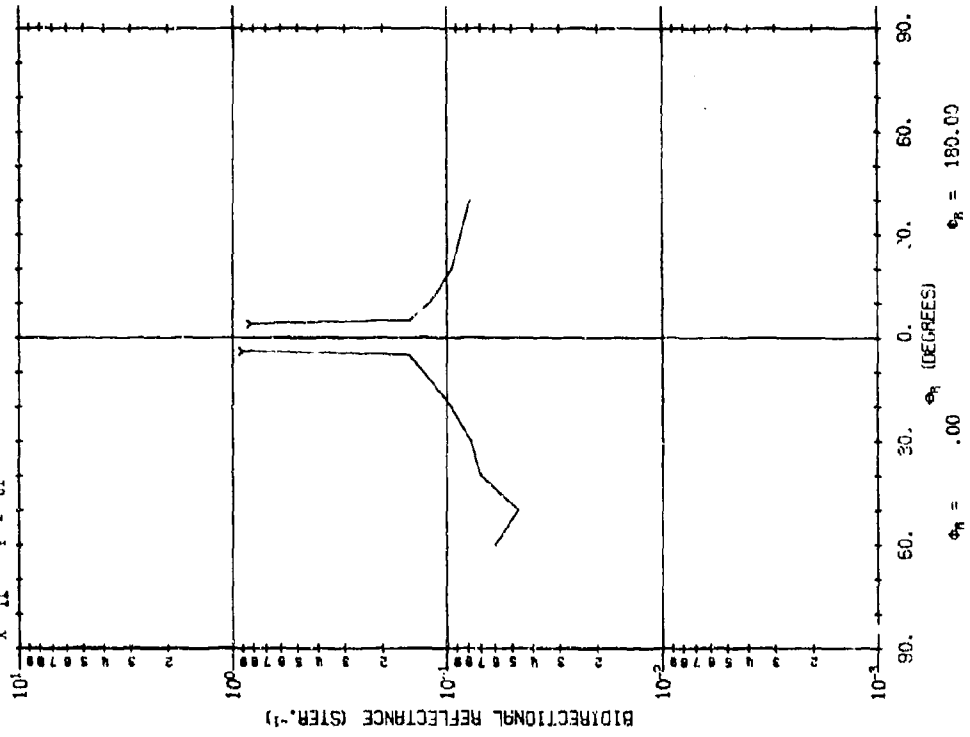
0 || 23 = 1.10
+ || θ_1 = *
- || θ_2 = 10.6
x || λ = 10.6
y = UT



A01587 001

Green Metallic Paint on Steel

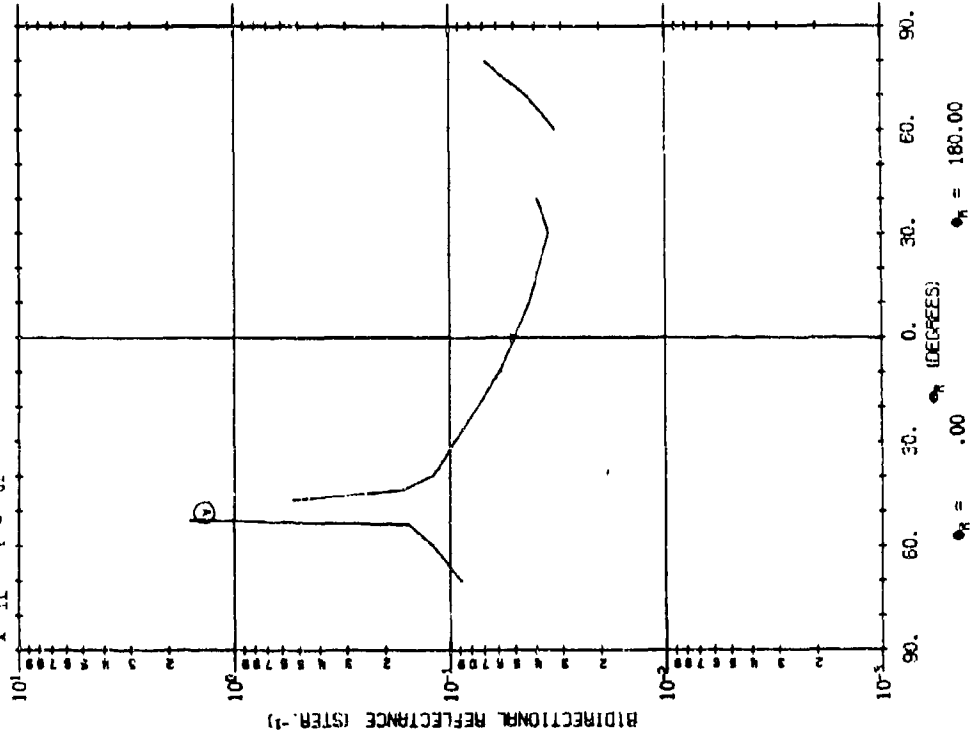
0 || θ_1 = 0.0
+ || θ_2 = 10.6
- || λ = 10.6
x || λ = 10.6
y = UT



A01587 001

Green Metallic Paint on Steel

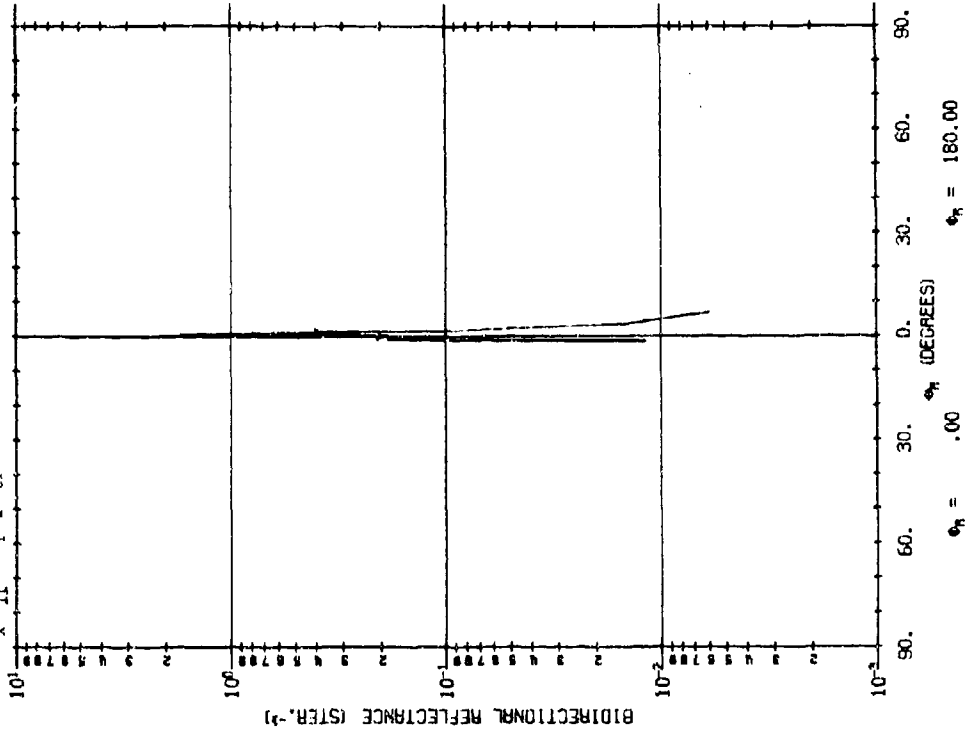
$\theta_i = 50.0$
 $\theta_r = 186.0$
 $\lambda = 10.6$
X II Y = UT



A01588 001

Red Paint on Steel

$\theta_i = 1.10$
 $\theta_r = \theta_r$
 $\lambda = 10.6$
X II Y = UT

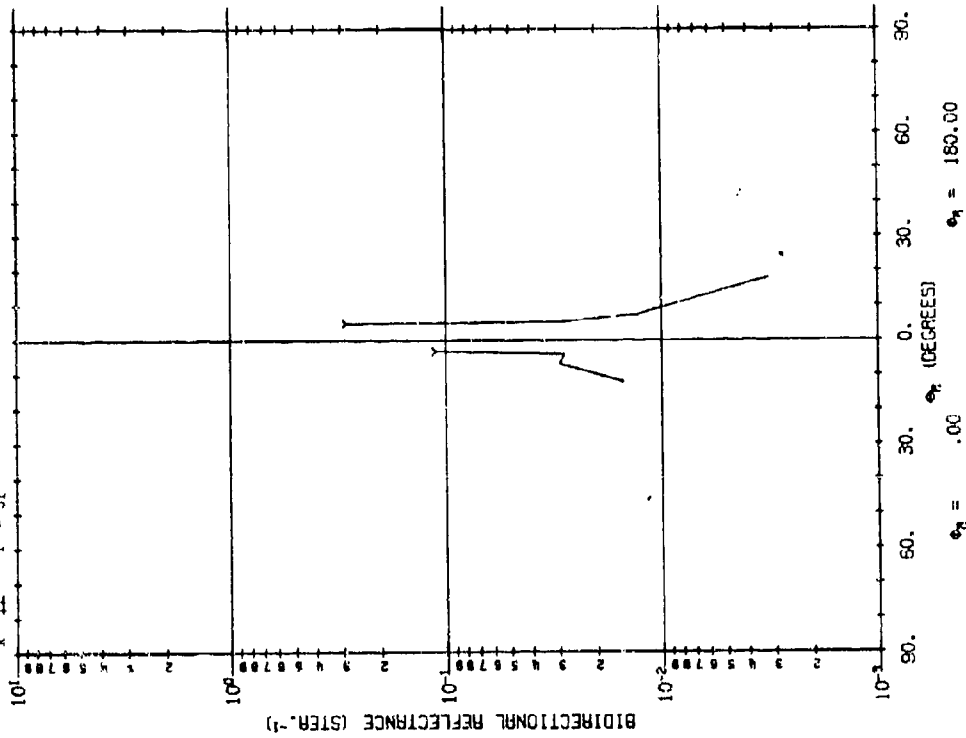


PAINT

A01588 001

Red Paint on Steel

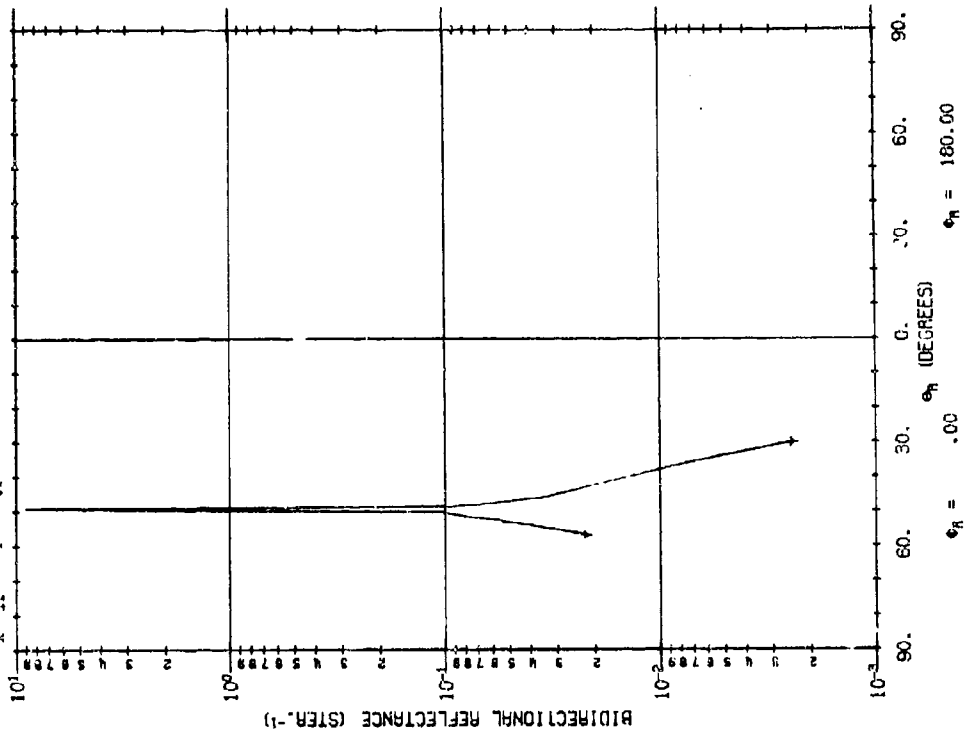
$\phi_1 = 0.0$
 $\phi_2 = 180.0$
 $\lambda = 10.6$
Y = JT



A01588 001

Red Paint on Steel

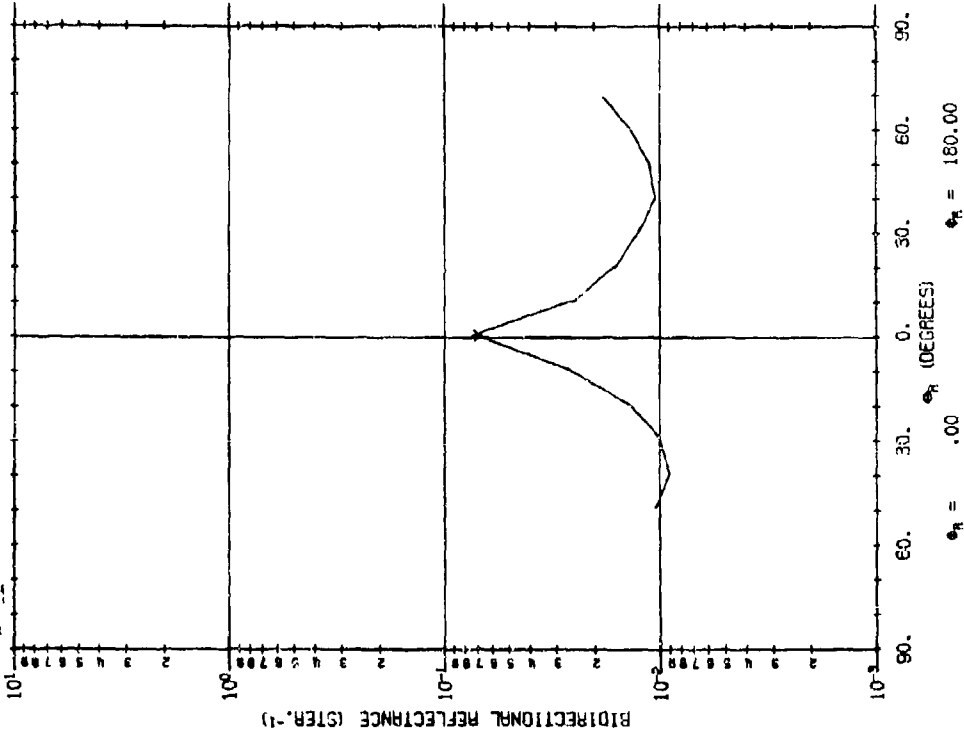
$\phi_1 = 50.0$
 $\phi_2 = 180.0$
 $\lambda = 10.6$
Y = VT



R01589 001

White Paint on Plywood

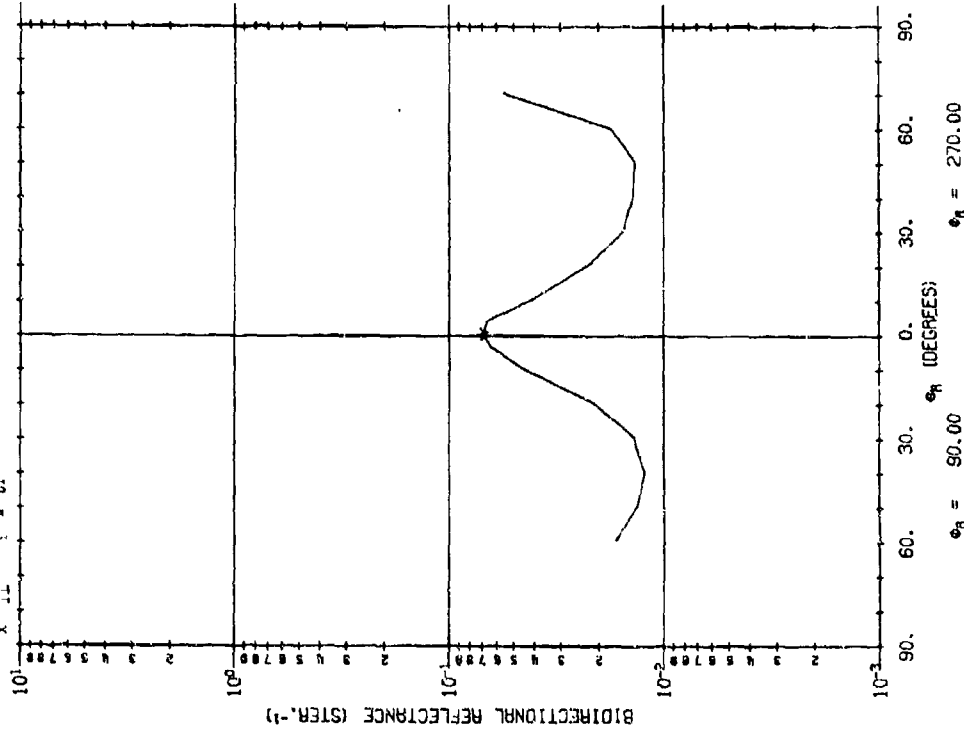
0 // 2 θ = 1.10
+ // ϕ_1 = ϕ_2
- // λ = 10.6
X // Y = UT



R01589 001

White Paint on Plywood

0 // 2 θ = 1.10
+ // ϕ_1 = ϕ_2
- // λ = 10.6
X // Y = UT

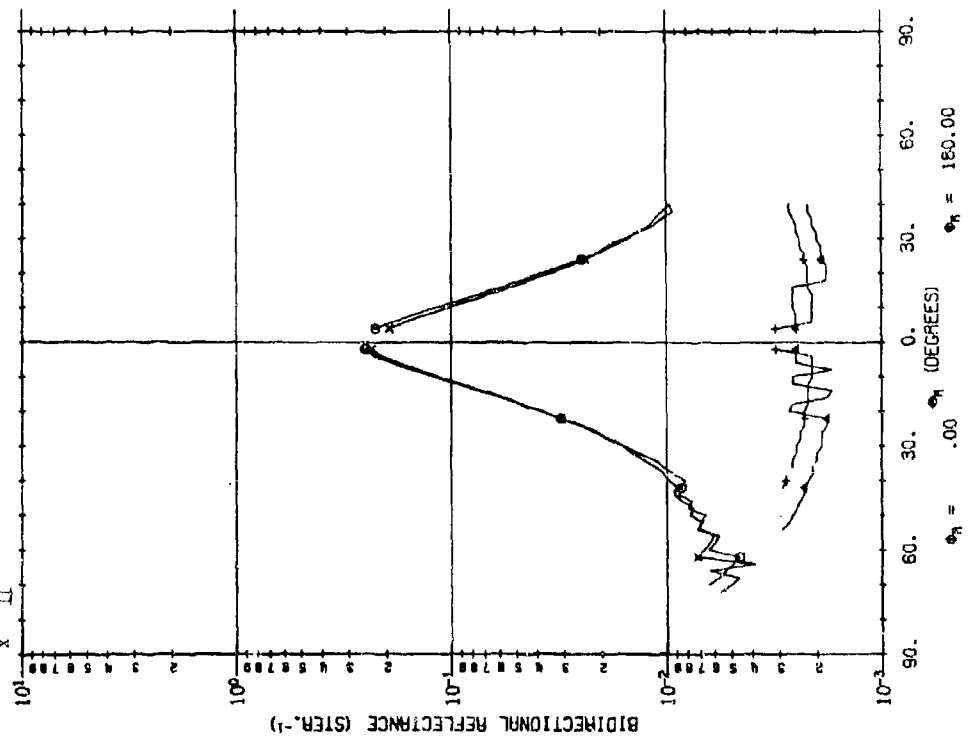


PAINT

A01608 201

OLIVE DRAB PAINT ON STEEL

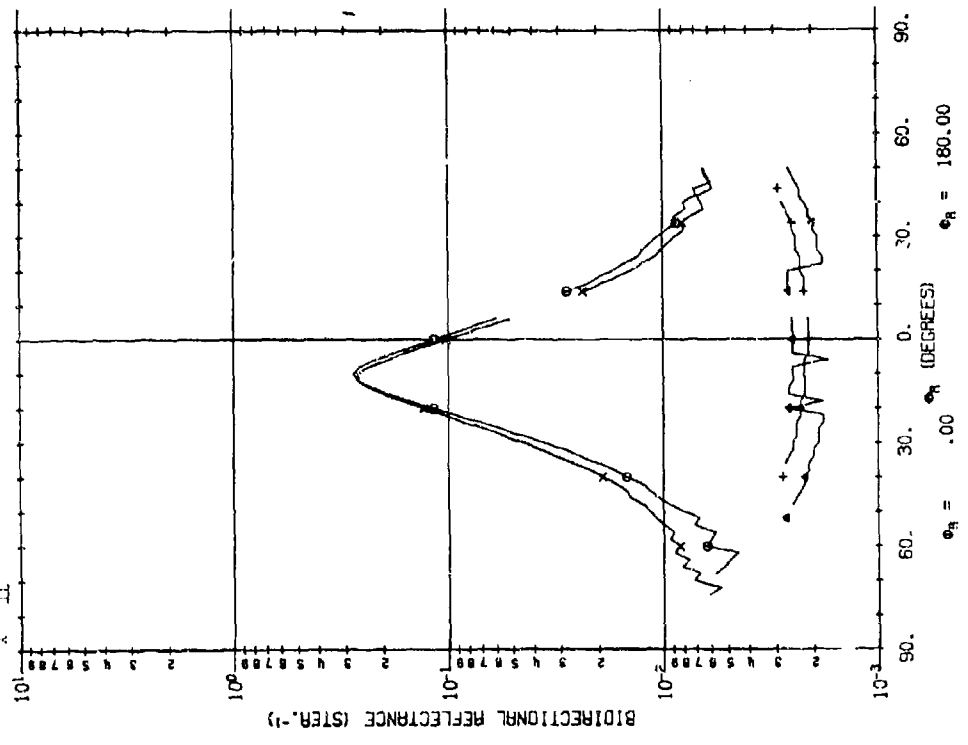
0 $\theta_1 = 0.0$
+ $\theta_1 = 180.0$
x $\theta_1 = 0.63$



A01608 201

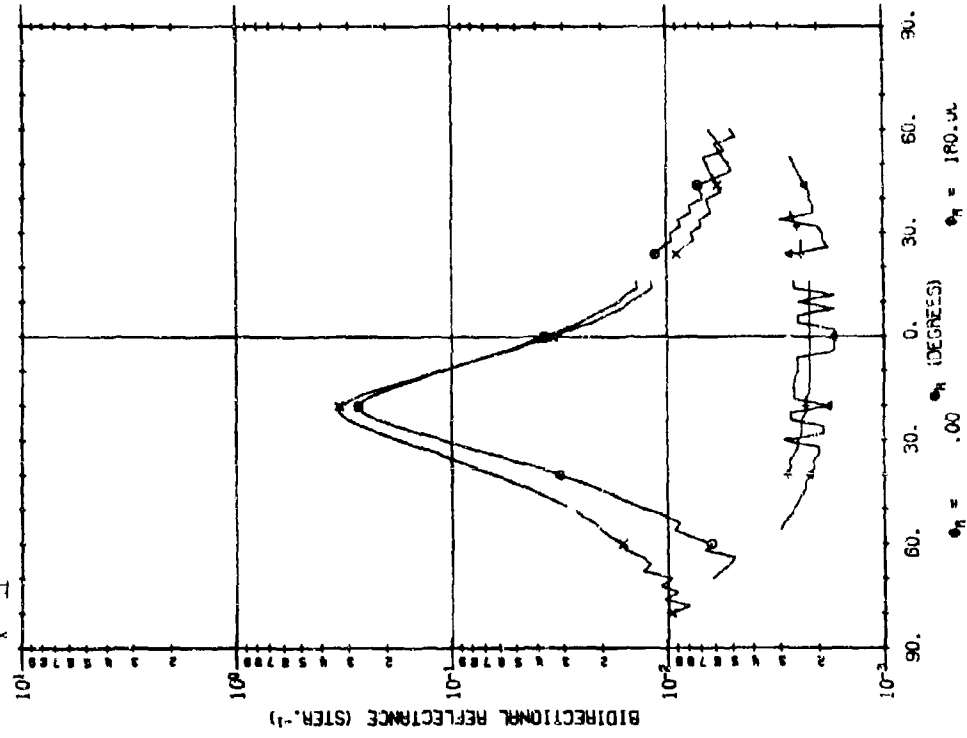
OLIVE DRAB PAINT ON STEEL

0 $\theta_1 = 10.0$
+ $\theta_1 = 180.0$
x $\theta_1 = 0.63$



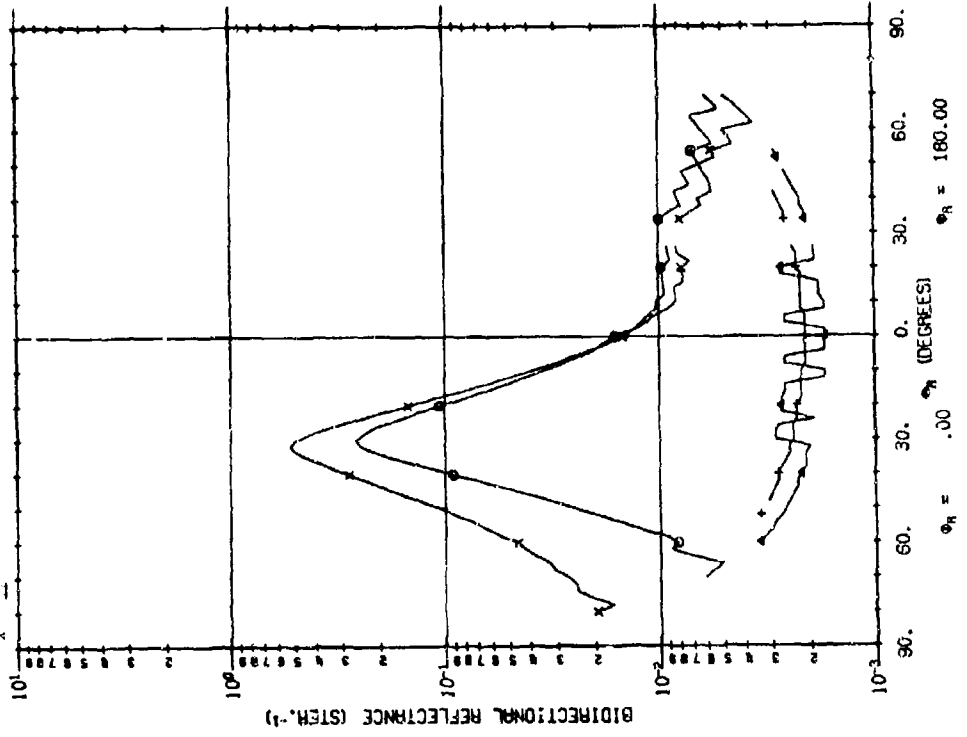
R01608 201
OLIVE DRAB PAINT ON STEEL

0 | | $\theta_1 = 20.0$
+ | | $\theta_2 = 180.0$
x | | $\lambda = 0.63$

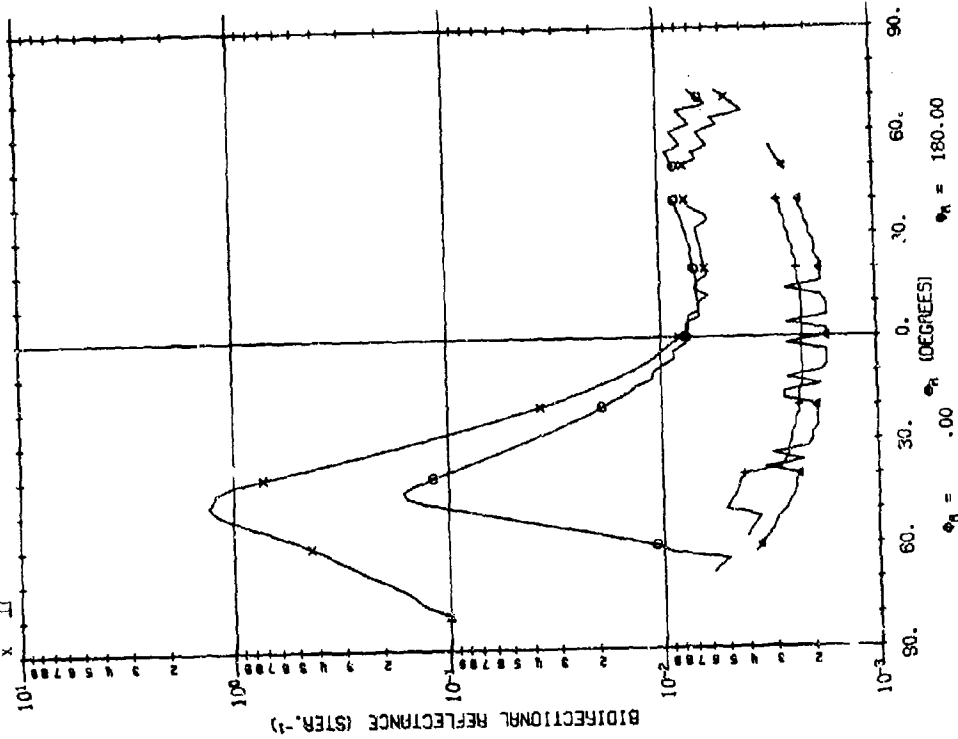


R01608 201
OLIVE DRAB PAINT ON STEEL

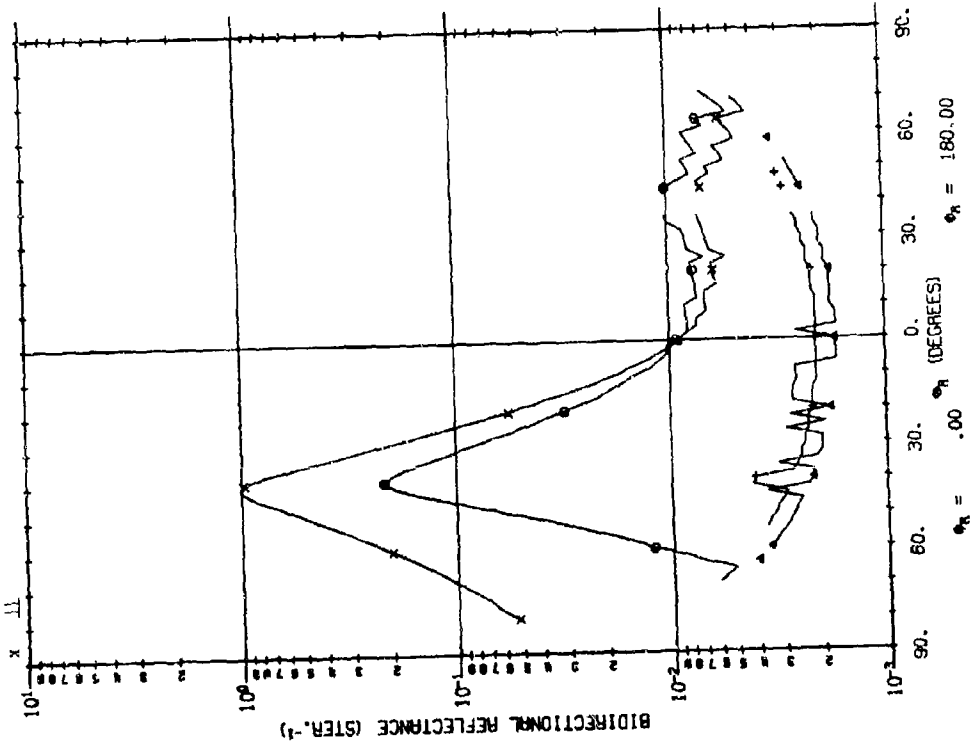
0 | | $\theta_1 = 30.0$
+ | | $\theta_2 = 180.0$
x | | $\lambda = 0.63$



R01608 201
 OLIVE DRAB PAINT ON STEEL
 $\theta_i = 45.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$



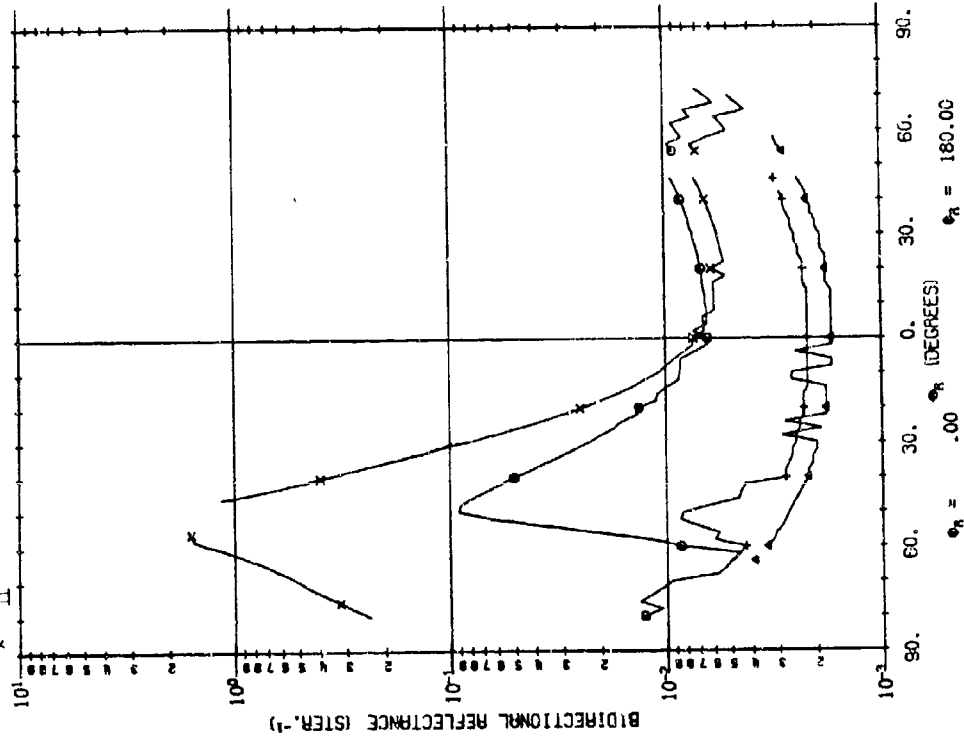
R01608 201
 OLIVE DRAB PAINT ON STEEL
 $\theta_i = 45.0$
 $\phi_i = 180.0$
 $\lambda = 0.63$



A01608 201

OLIVE DRAB PAINT ON STEEL

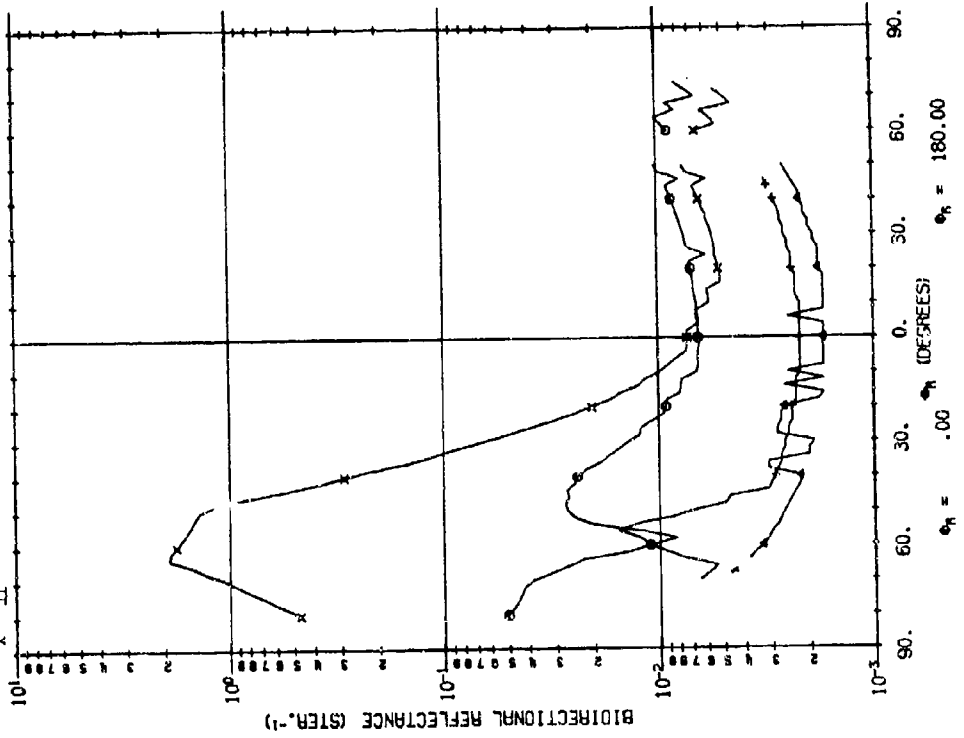
0 || $\theta_1 = 50.0$
+ || $\theta_1 = 180.0$
Δ || $\lambda = 0.63$
X ||



A01608 201

OLIVE DRAB PAINT ON STEEL

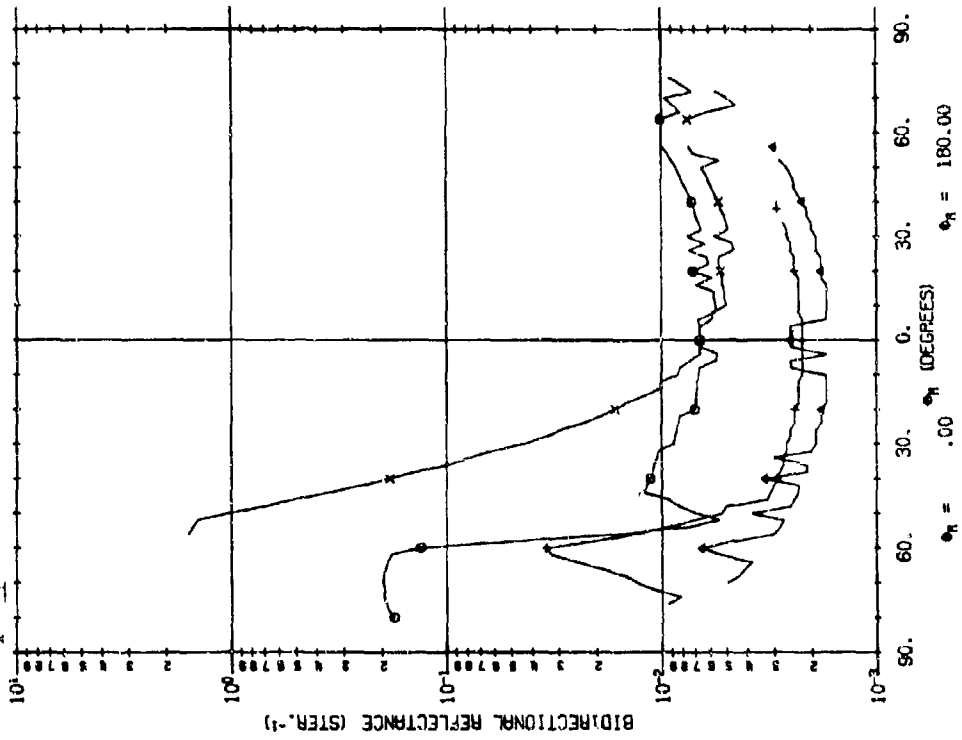
0 || $\theta_1 = 55.0$
+ || $\theta_1 = 180.0$
Δ || $\lambda = 0.63$
X ||



R01608 201

OLIVE DRAB PAINT ON STEEL

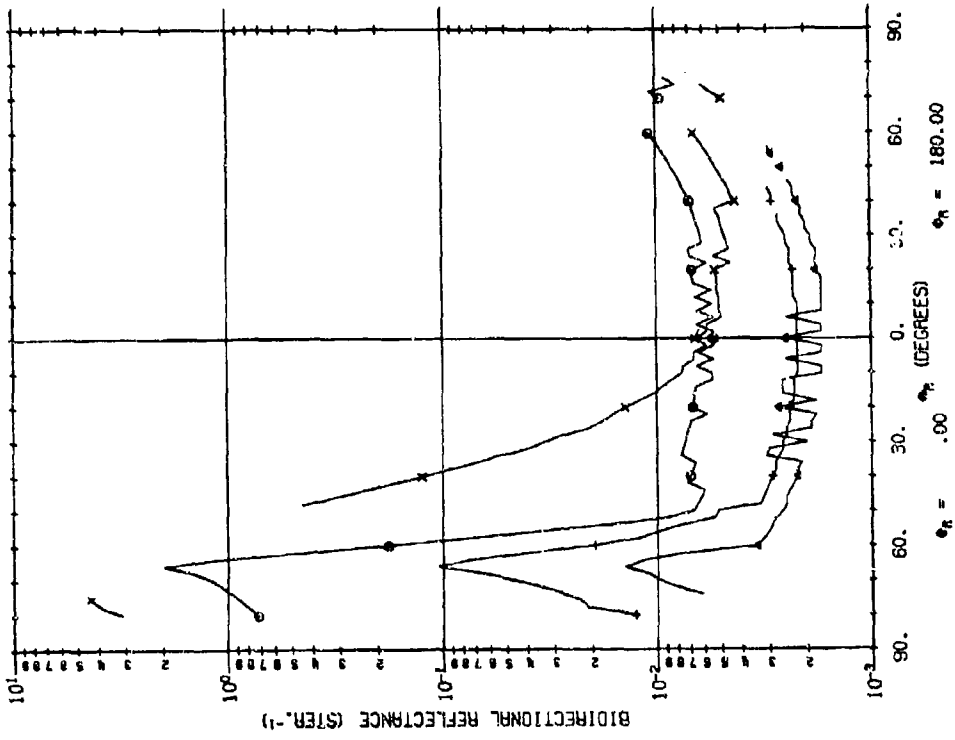
0 || $\phi_1 = 65.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 0.63$
x ||



R01608 201

OLIVE DRAB PAINT ON STEEL

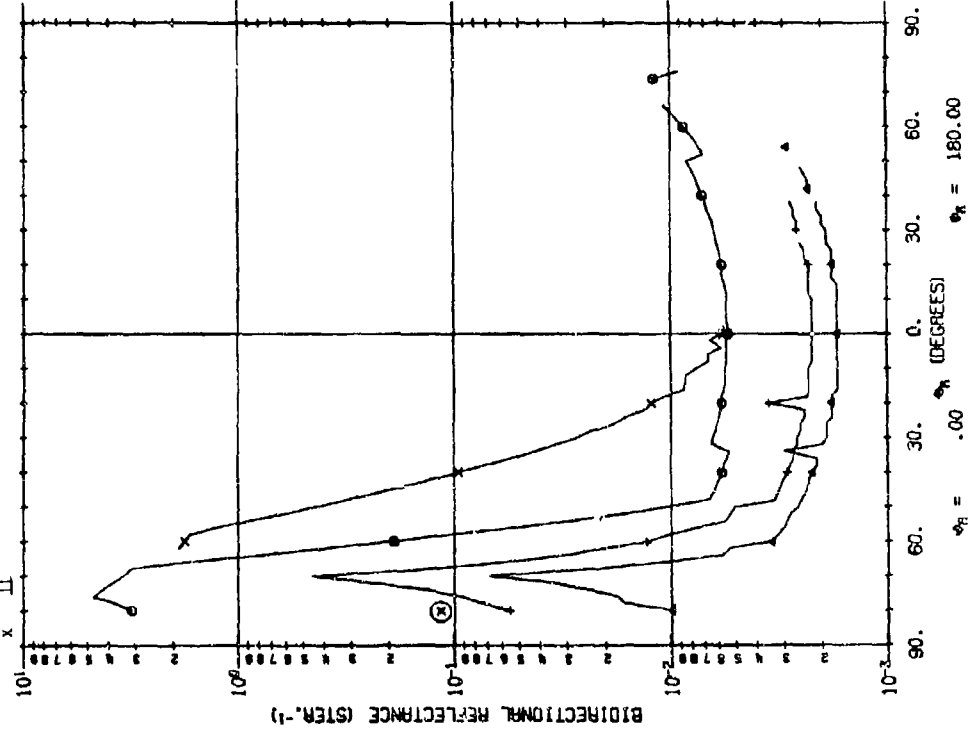
0 || $\phi_1 = 65.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 0.63$
x ||



R01608 201

OLIVE DRAB PAINT ON STEEL

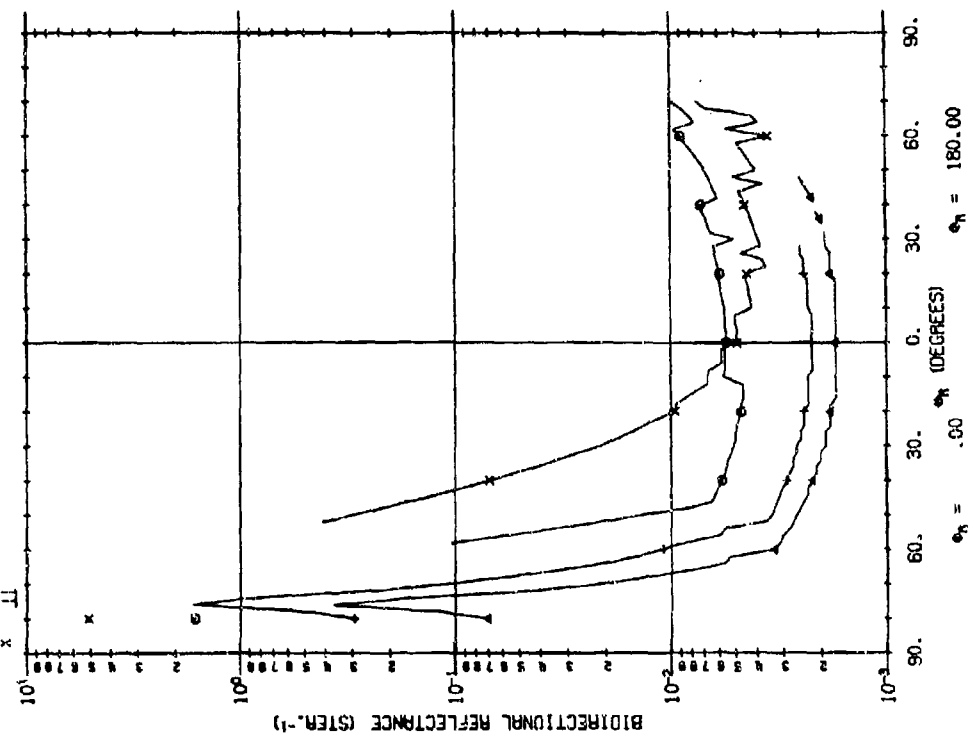
0 || $\phi_1 = 70.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 0.63$
x ||



R01608 201

OLIVE DRAB PAINT ON STEEL

0 || $\phi_1 = 75.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 0.63$
x ||

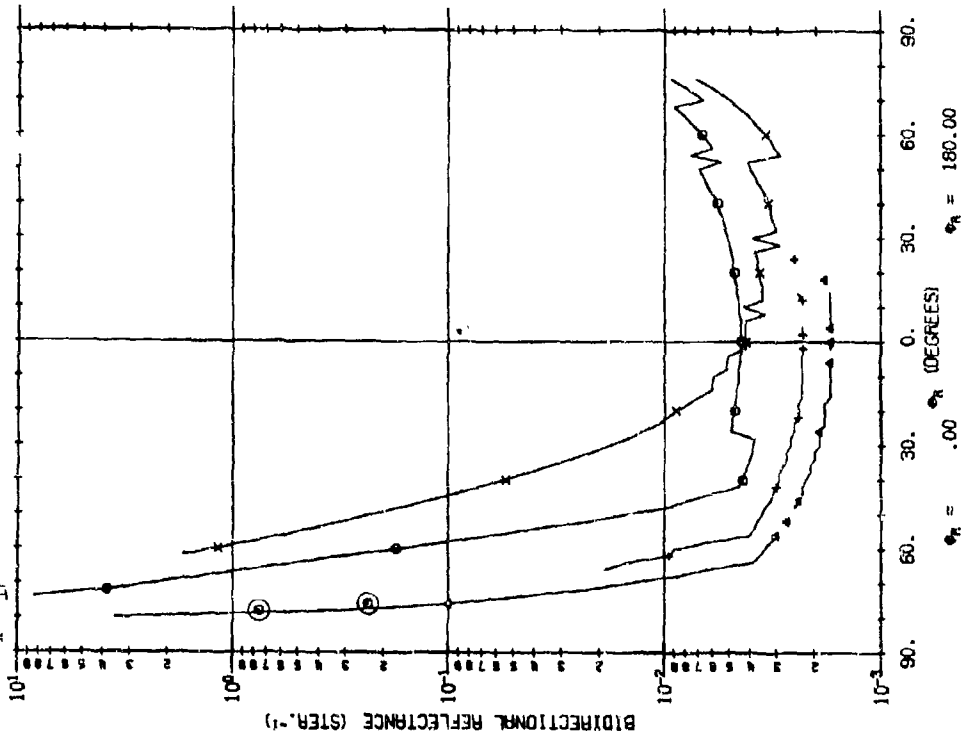


PAINT

A01608 201

OLIVE DRAB PAINT ON STEEL

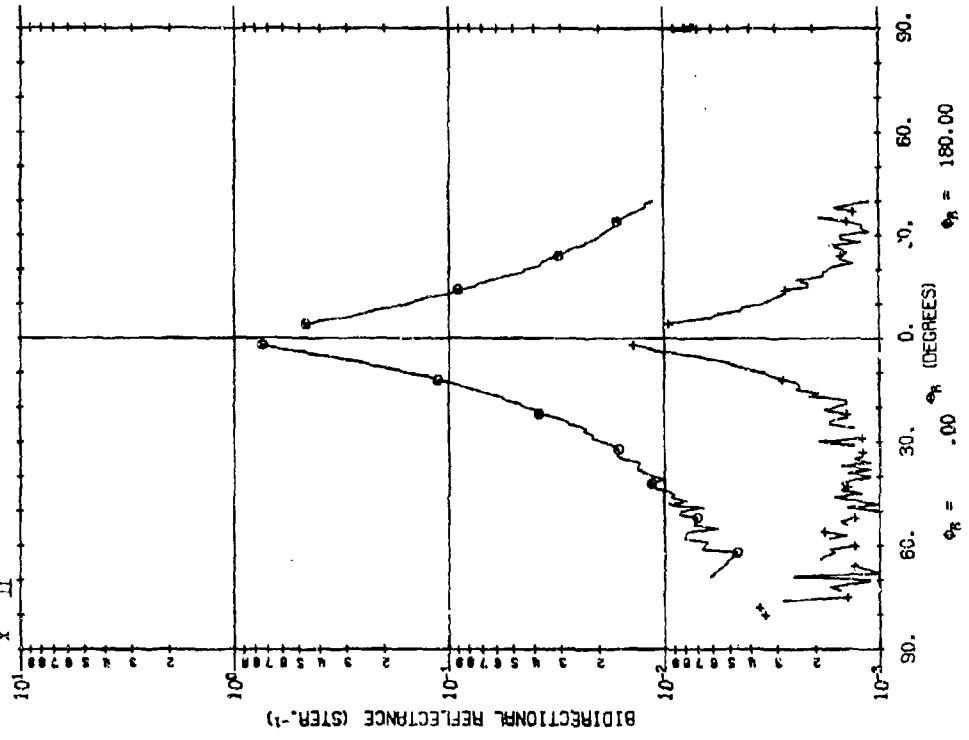
0 || $\phi_1 = 80.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 0.63$
 x ||



A01610 101

OLIVE DRAB PAINT ON STEEL

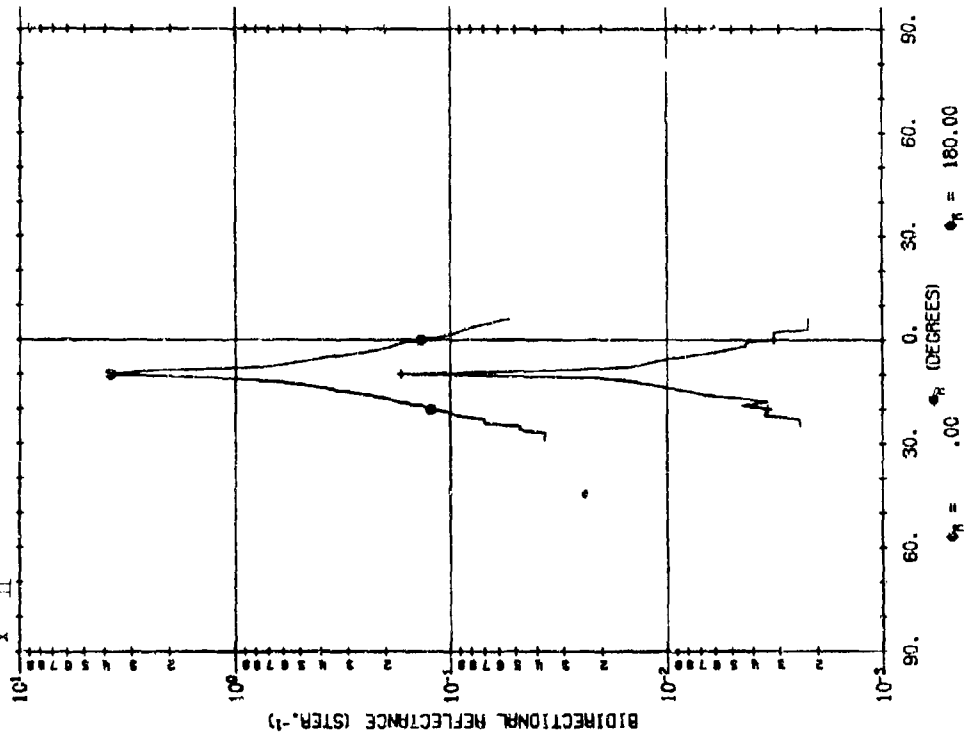
0 || $\phi_1 = 0.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
 x ||



R01610 101

OLIVE DRAB PAINT ON STEEL

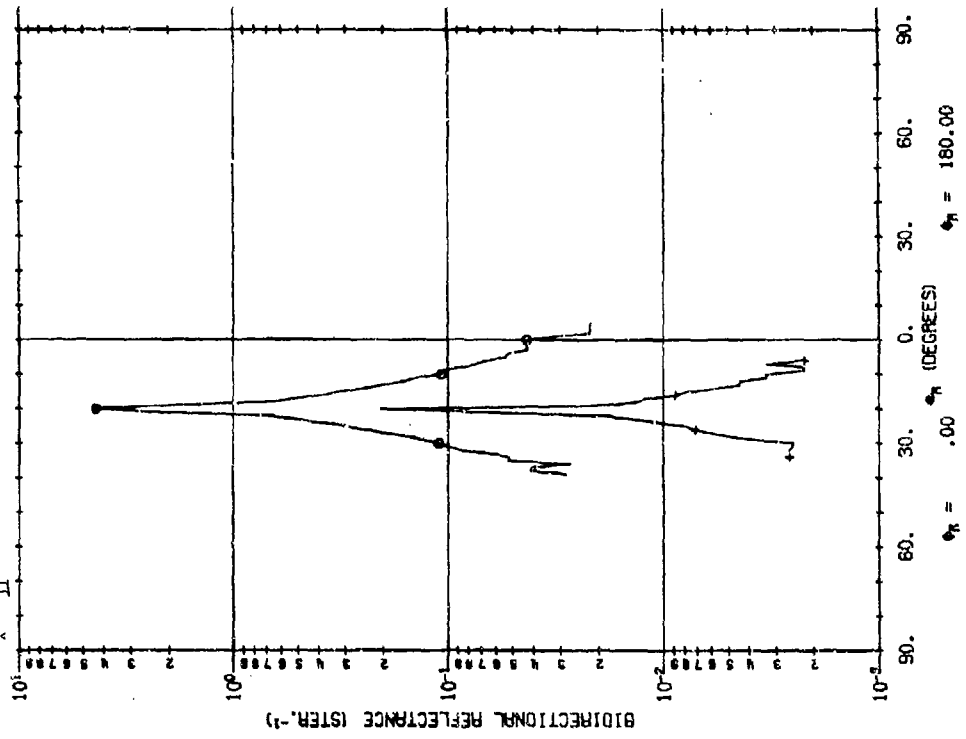
0 || $\phi_1 = 10.0$
+ || $\phi_2 = 180.0$
 Δ || $\lambda = 10.6$
x ||



R01610 101

OLIVE DRAB PAINT ON STEEL

0 || $\phi_1 = 20.0$
+ || $\phi_2 = 180.0$
 Δ || $\lambda = 10.6$
x ||

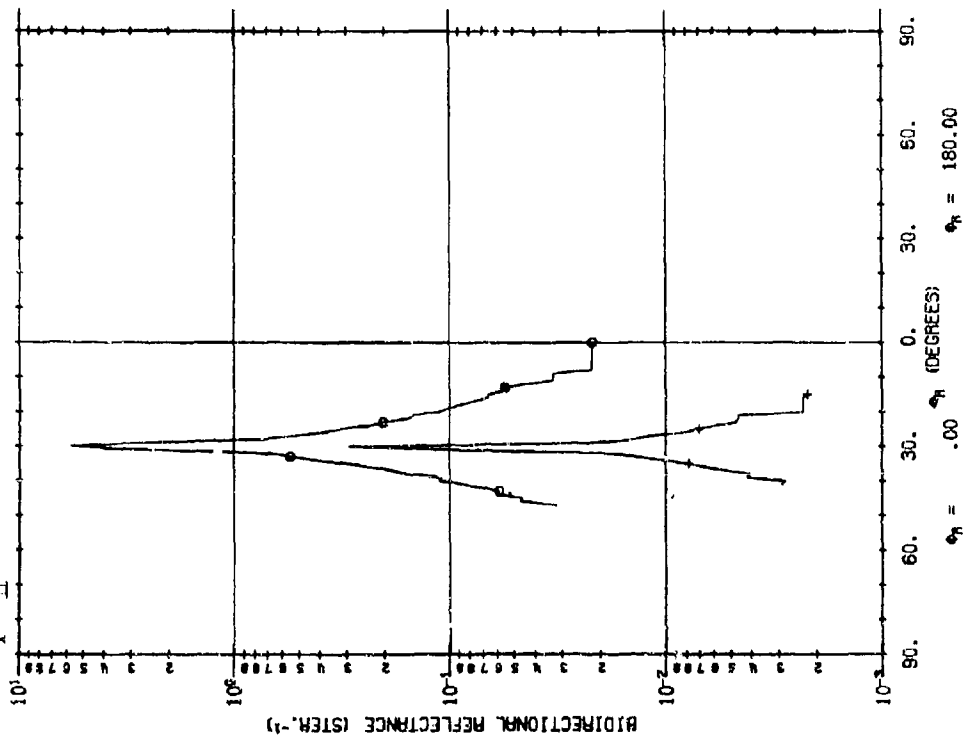


PAINT

R01610 101

OLIVE DRAB PAINT ON STEEL

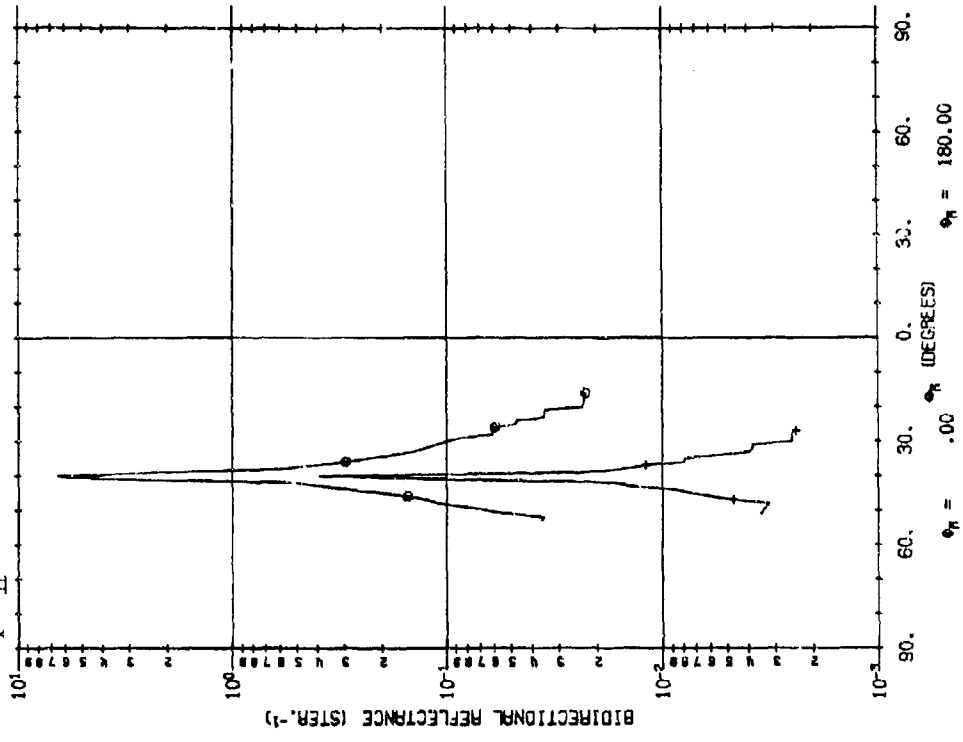
$\theta_i = 30.3$
 $\theta_r = 180.3$
 $\lambda = 10.6$



R01610 101

OLIVE DRAB PAINT ON STEEL

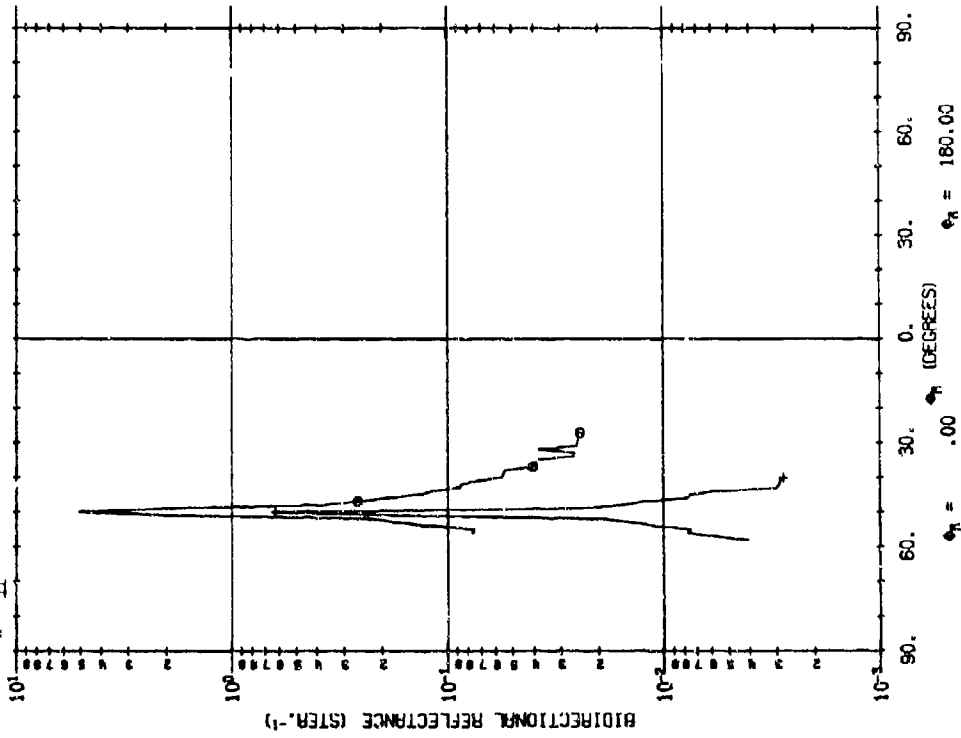
$\theta_i = 40.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$



R01610 101

OLIVE DRAB PAINT ON STEEL

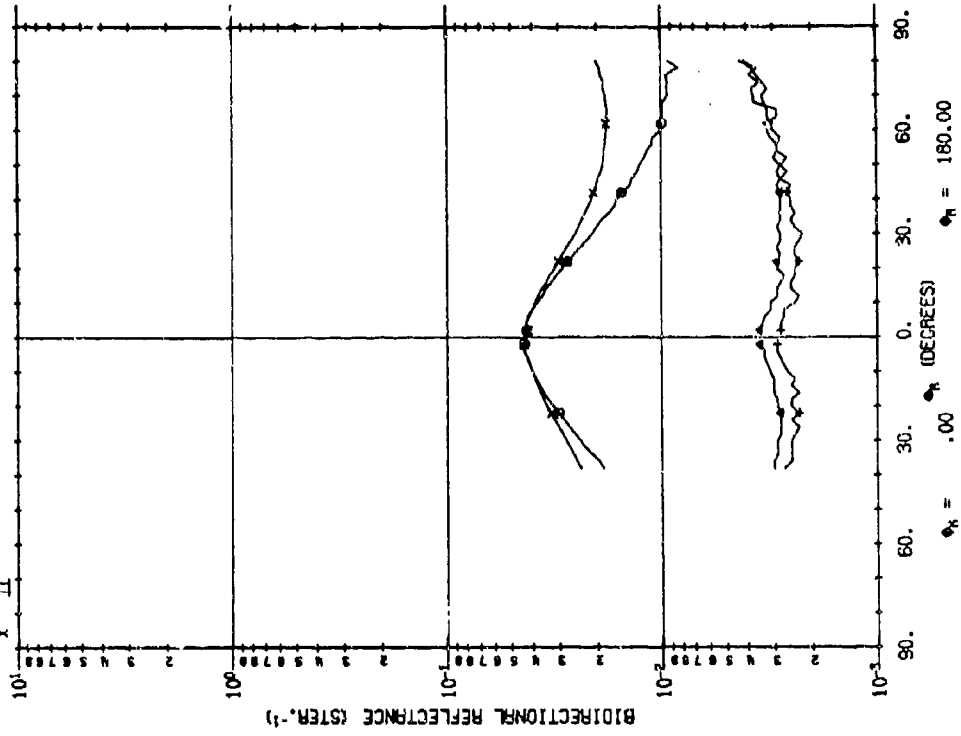
0 || $\phi_1 = 50.0$
 + || $\phi_2 = 180.0$
 Δ || $\lambda = 10.6$
 X ||



R01629 101

OLIVE DRAB PAINT ON STEEL

0 || $\phi_1 = 0.0$
 + || $\phi_2 = 0.0$
 Δ || $\lambda = 0.63$
 X ||



R01629 101

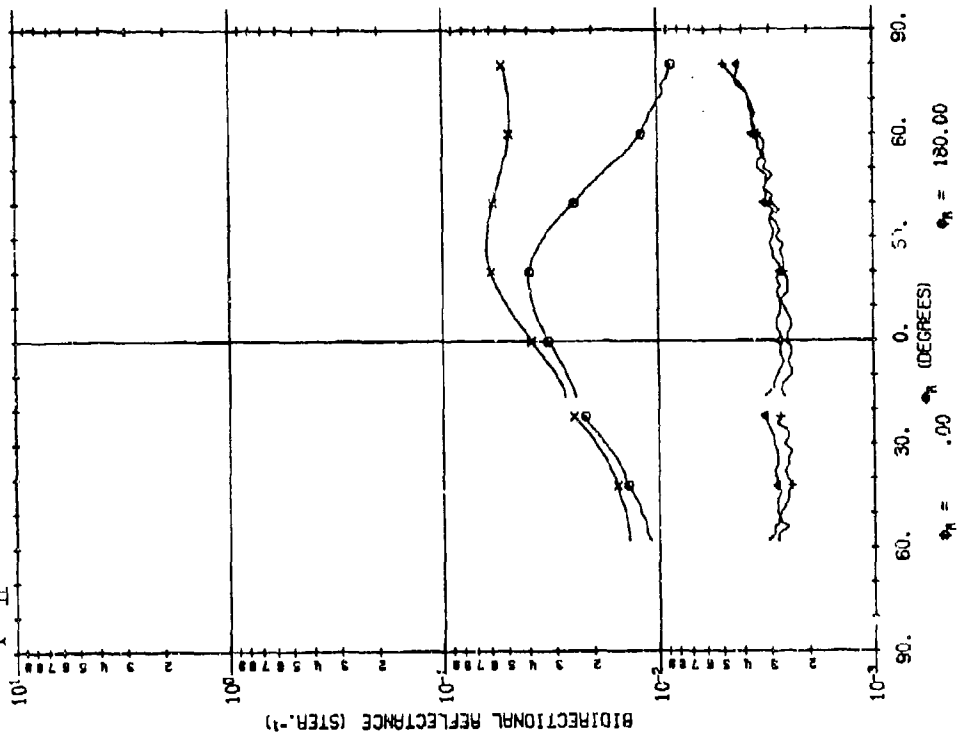
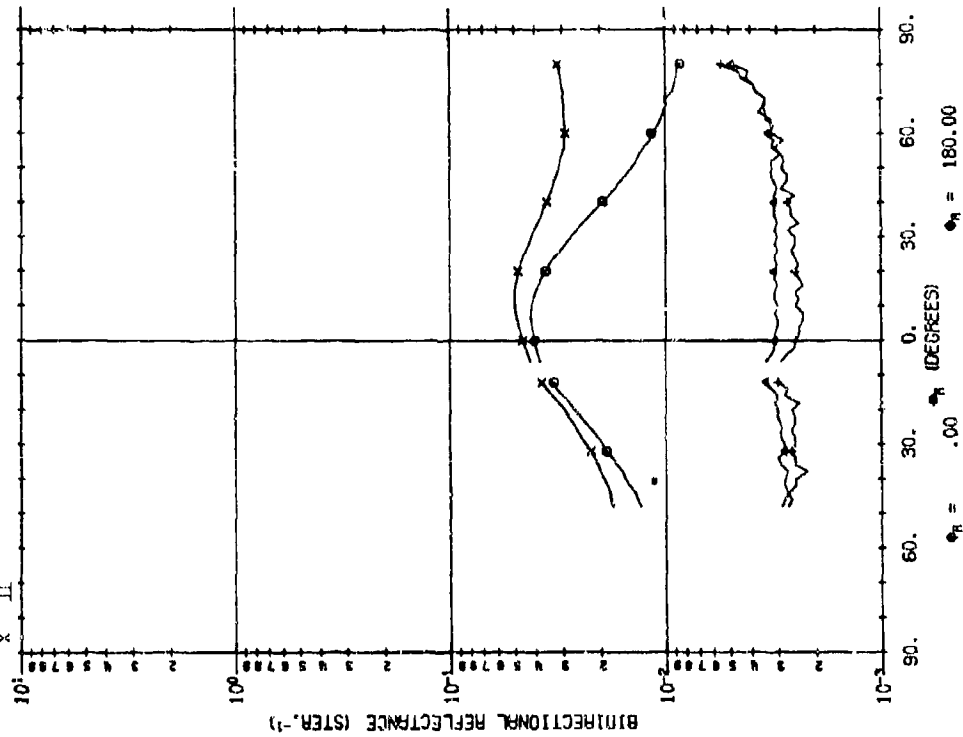
OLIVE DRAB PAINT ON STEEL

$\theta_1 = 10.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

R01629 101

OLIVE DRAB PAINT ON STEEL

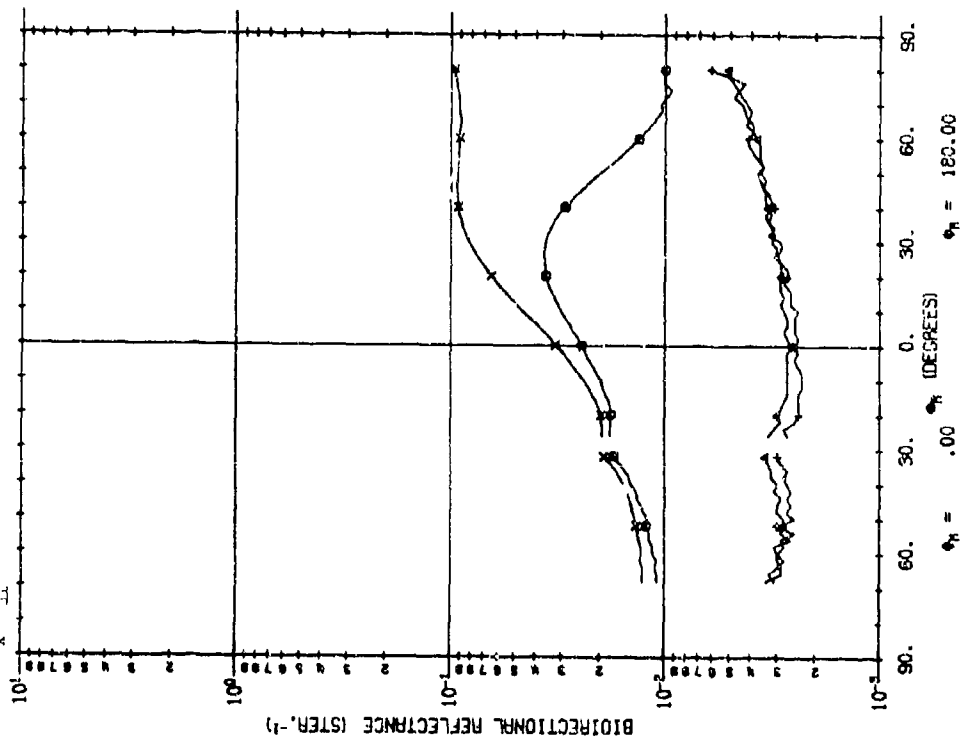
$\theta_1 = 20.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$



A01629 101

OLIVE DRAB PAINT ON STEEL

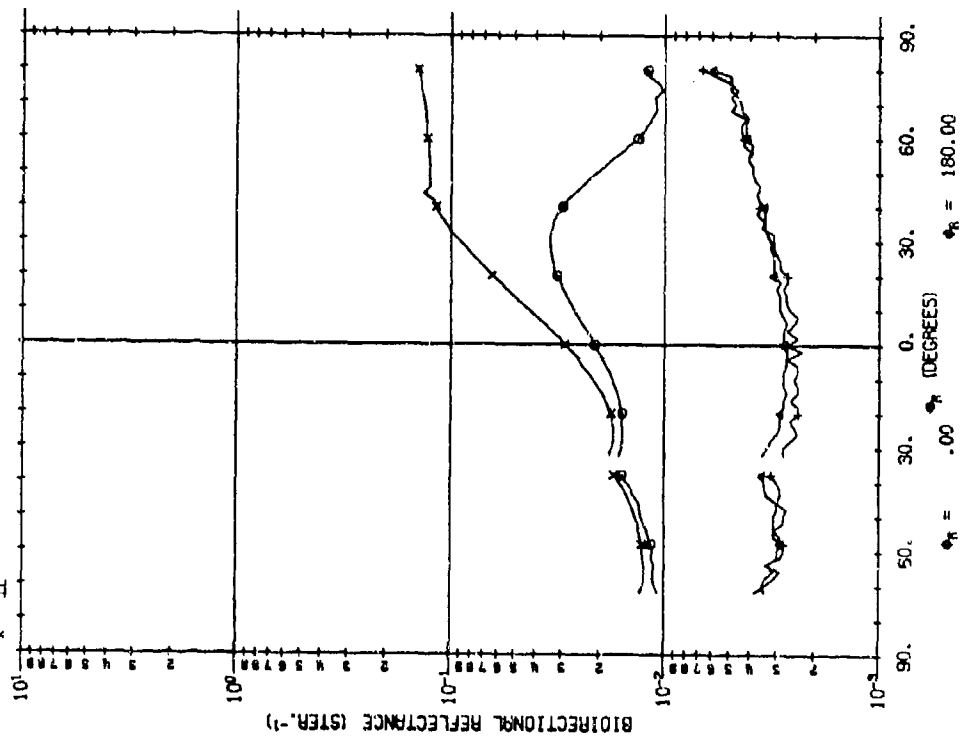
$\epsilon_1 = 30.0$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 0.63$



A01629 101

OLIVE DRAB PAINT ON STEEL

$\epsilon_1 = 35.0$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 0.63$

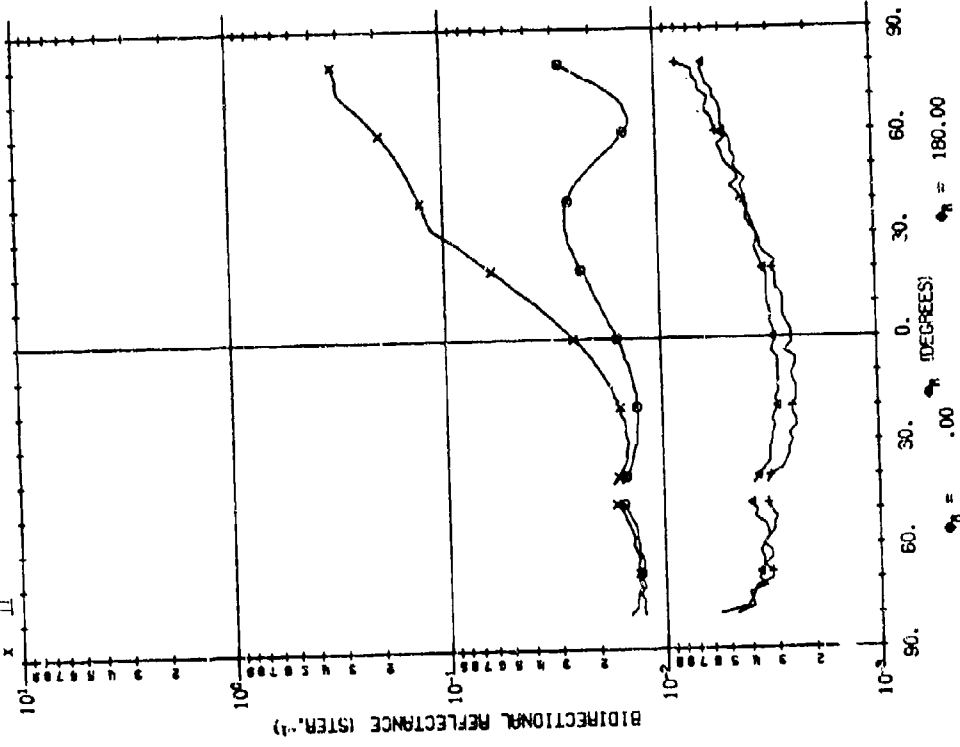


PAINT

R01629 101

OLIVE DRAB PAINT ON STEEL

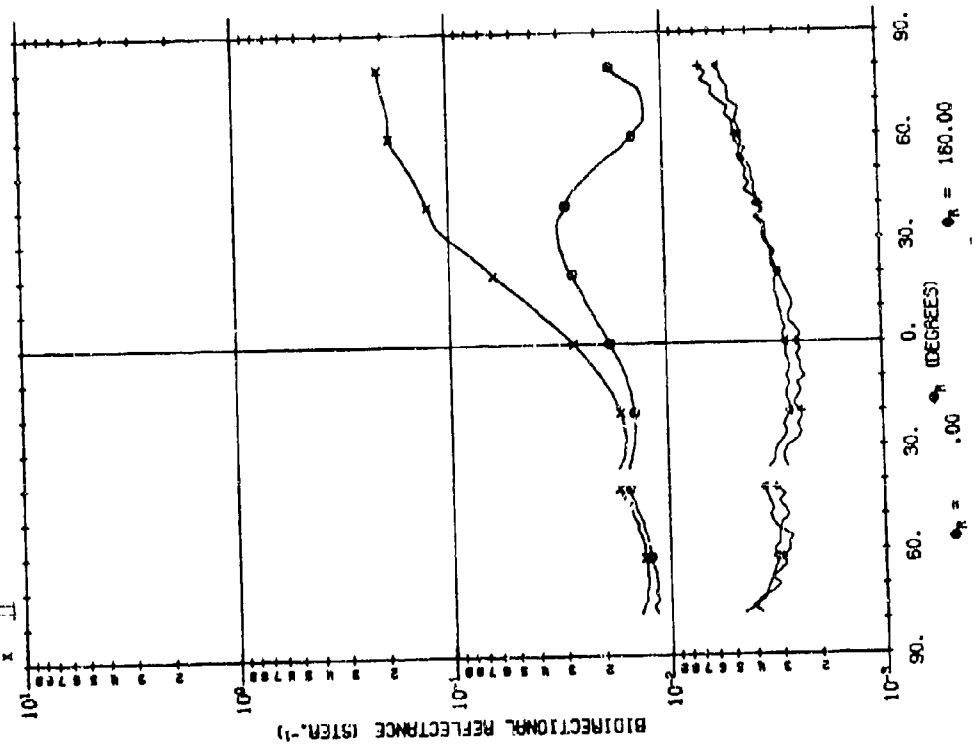
0 $\rho_1 = 45.0$
 + $\rho_2 = 0.0$
 x $\rho_3 = 0.63$

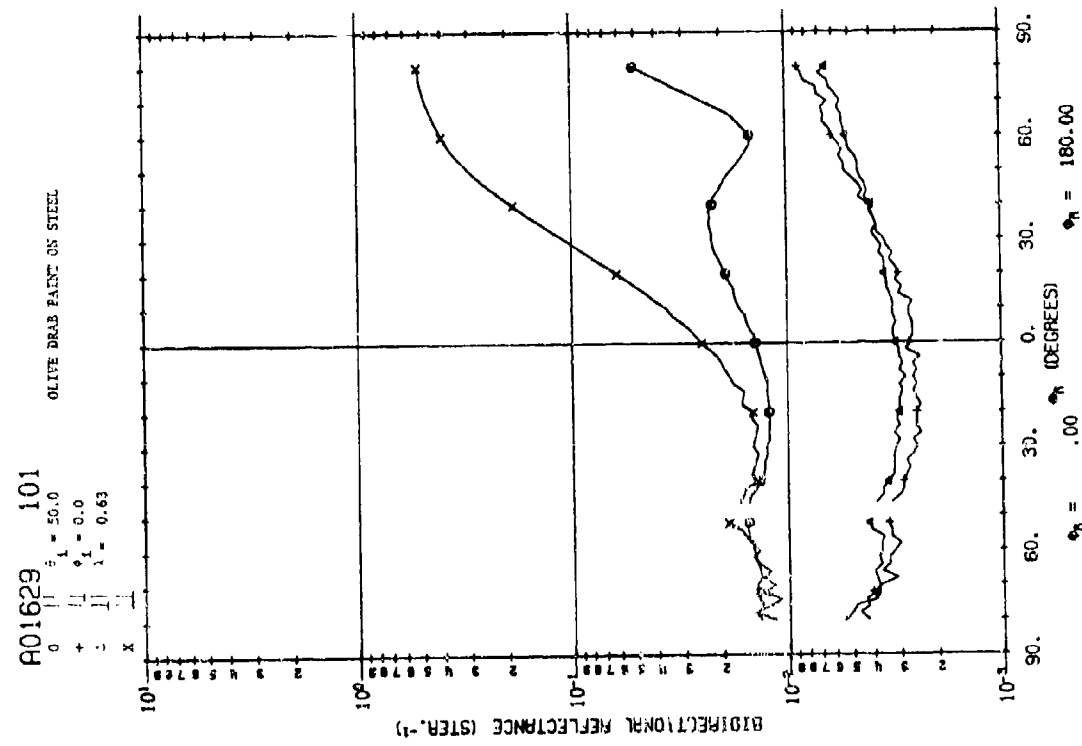
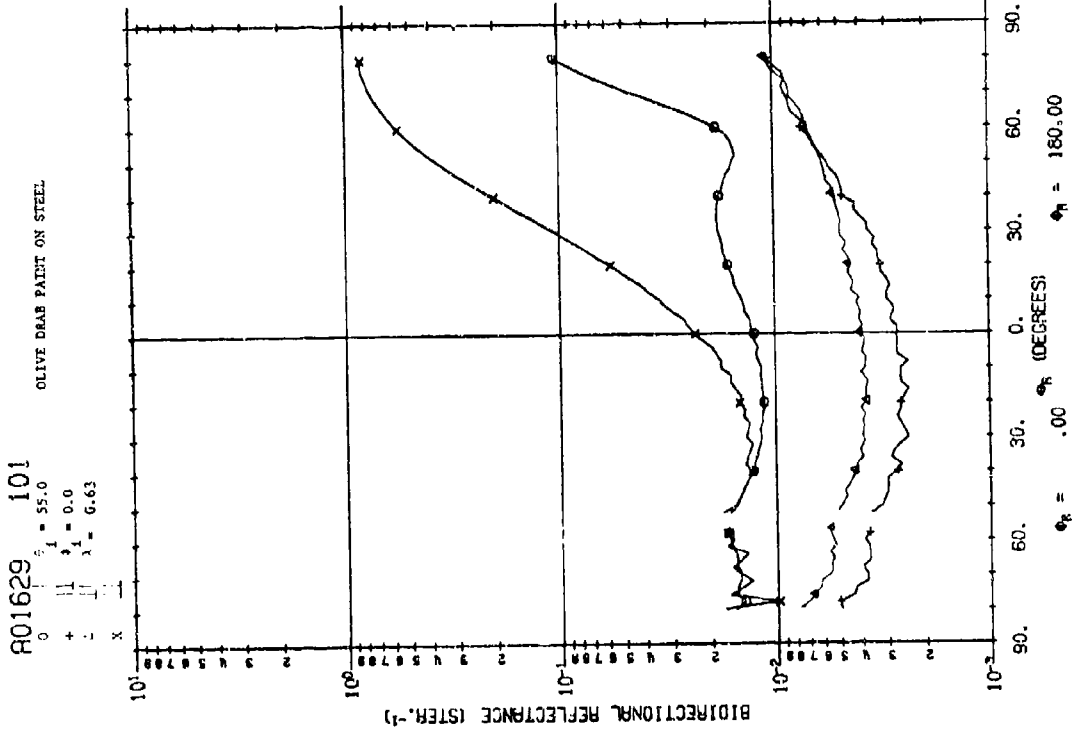


R01629 101

OLIVE DRAB PAINT ON STEEL

0 $\rho_1 = 40.0$
 + $\rho_2 = 0.0$
 x $\rho_3 = 0.63$



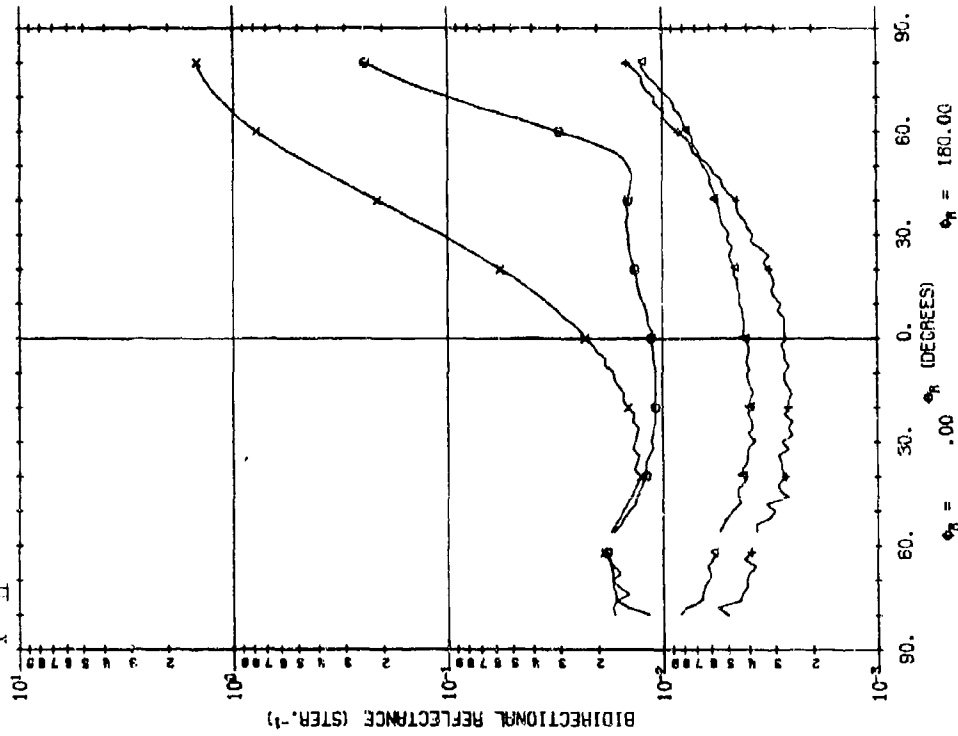


PAINT

A01629 101

OLIVE DRAB PAINT ON STEEL

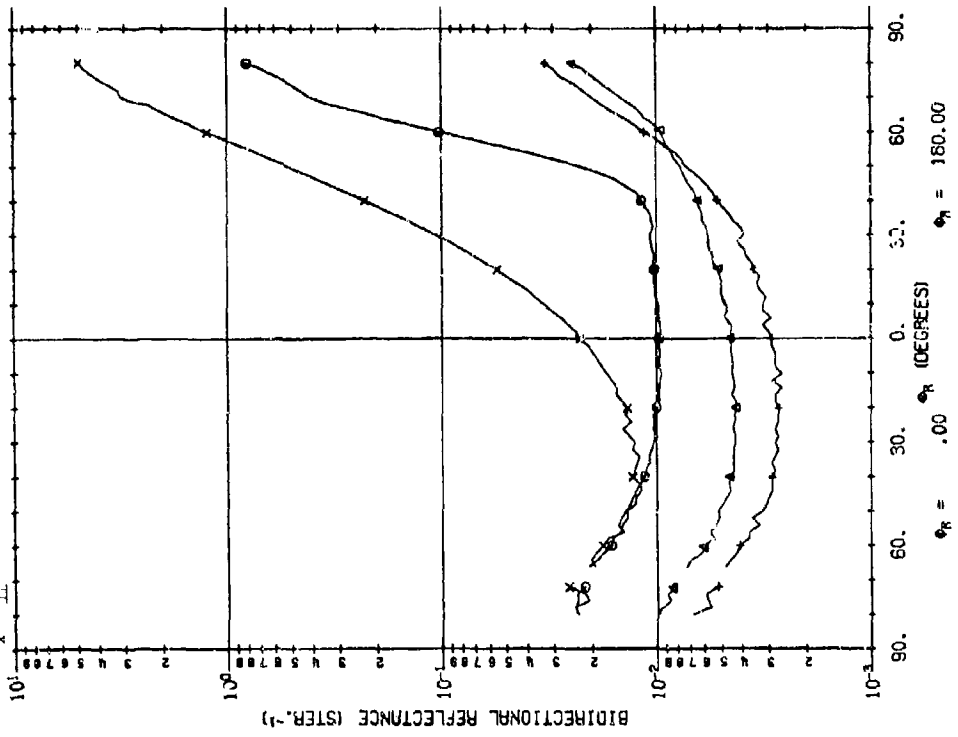
0 || $\phi_1 = 60.0$
+ || $\phi_1 = 0.0$
x || $\phi_1 = 0.63$



A01629 101

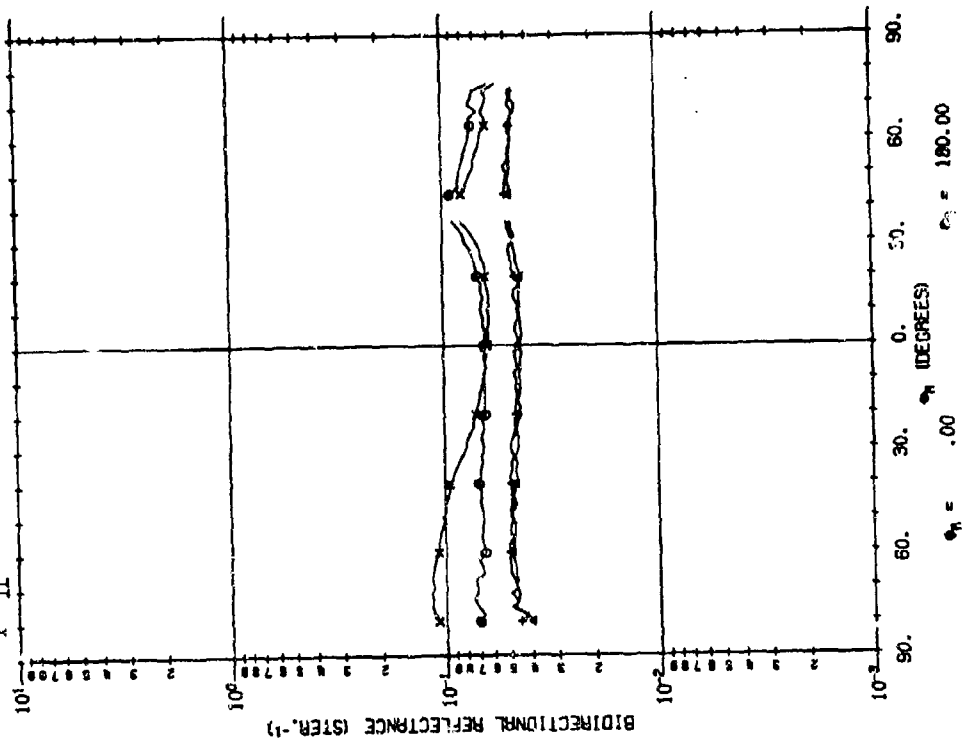
OLIVE DRAB PAINT ON STEEL

0 || $\phi_1 = 70.0$
+ || $\phi_1 = 0.0$
x || $\phi_1 = 0.63$



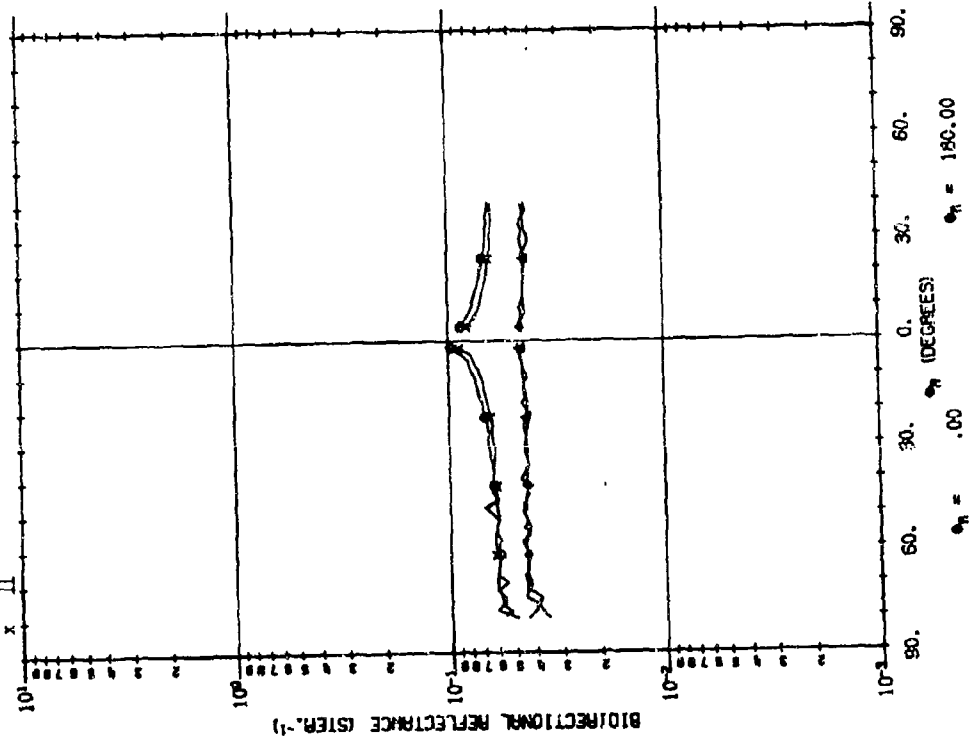
R01638 101
 Light Tan Paint on Steel

0 || $\theta_1 = 40.00$
 + || $\phi_1 = 180.00$
 A || $\lambda = 0.63$
 X ||



R01638 101
 Light Tan Paint on Steel

0 || $\theta_1 = 0.0$
 + || $\phi_1 = 180.00$
 A || $\lambda = 0.63$
 X ||



PAINT

R01638 101

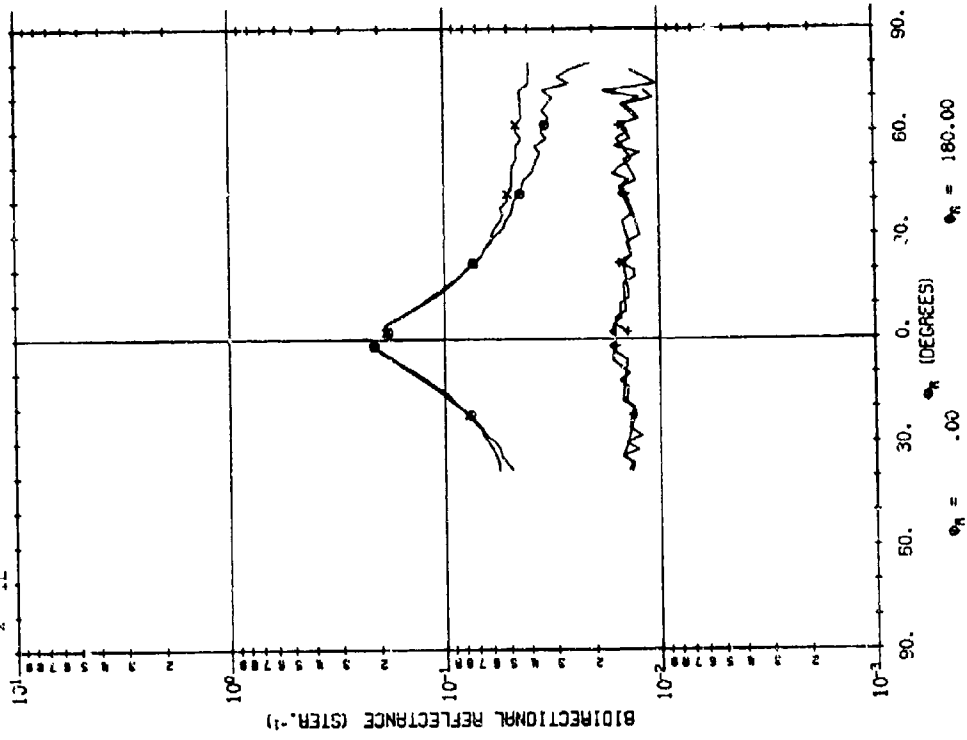
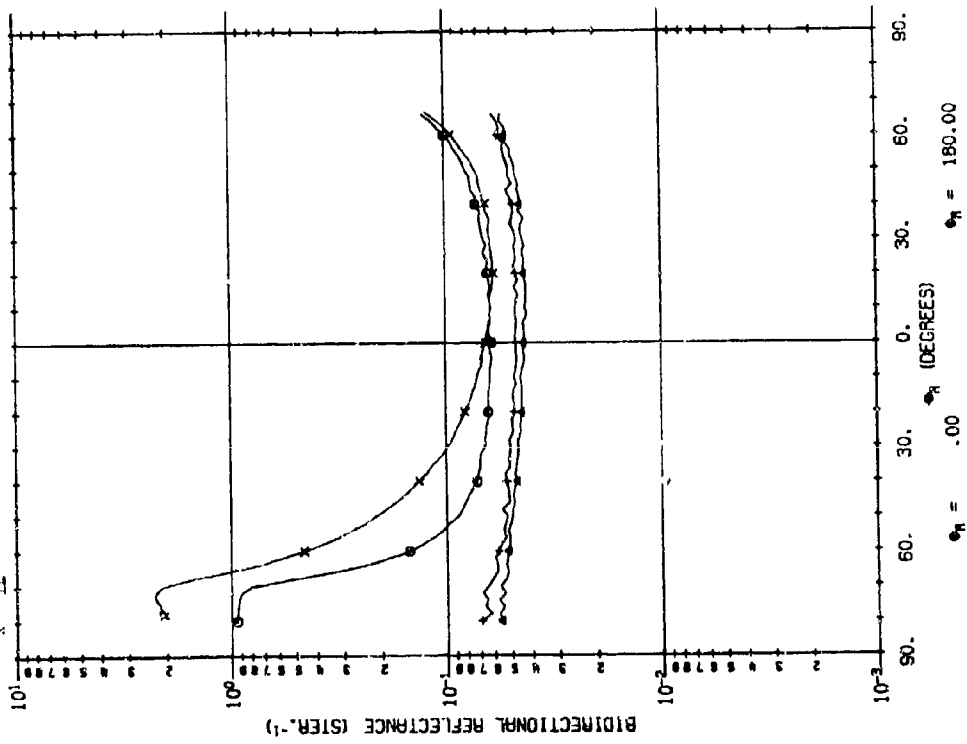
Light Tan Paint on Steel

$\theta_i = 70.00$
 $\phi_i = 180.00$
 $\theta_r = 0.63$

R01640 101

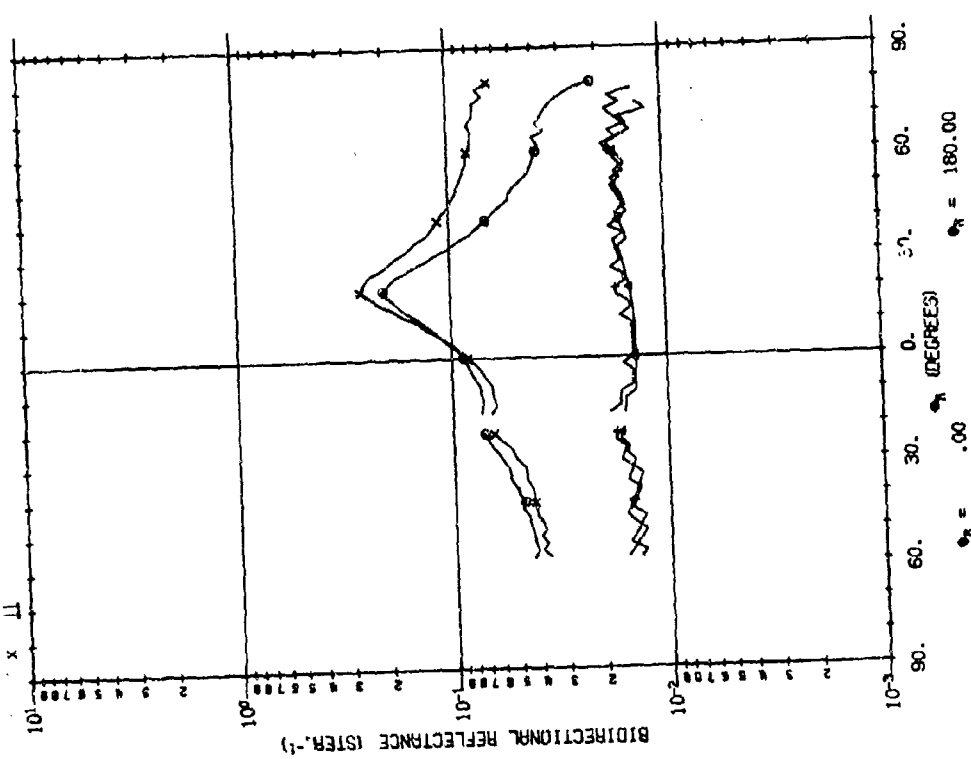
Olive Drab Paint on Steel

$\theta_i = 0.0$
 $\phi_i = 0.0$
 $\theta_r = 0.63$



AD1640 101 Olive Drab Paint on Steel

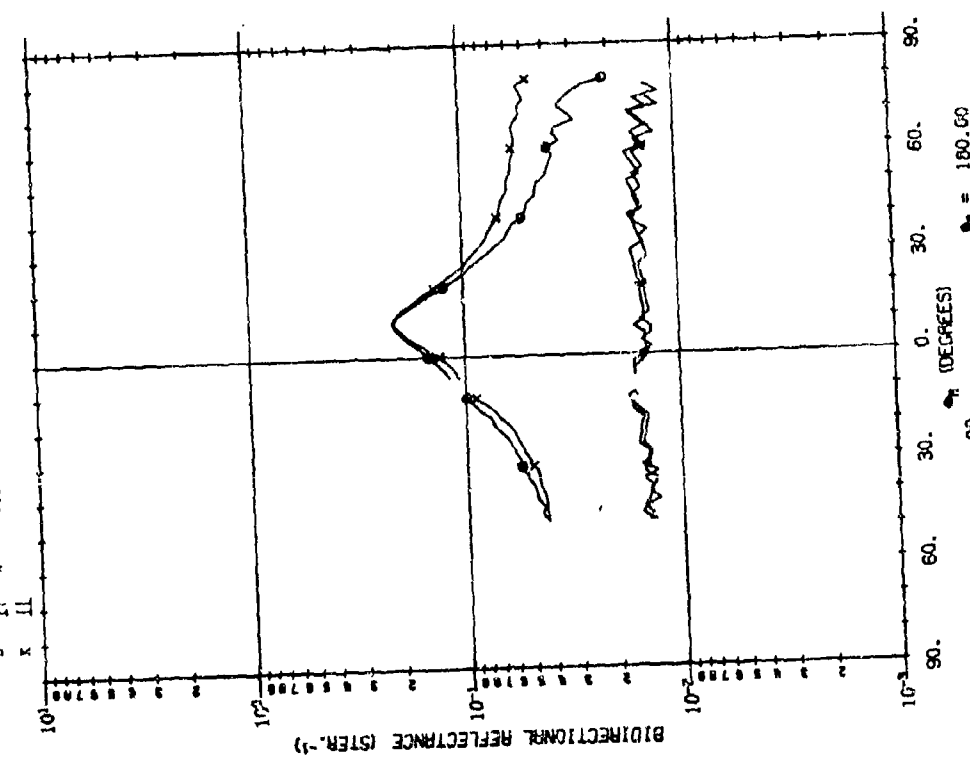
0 || $\theta_i = 20.00$
 + || $\phi_1 = 0.0$
 x || $\lambda = 0.63$



$\theta_i = .00$ $\theta_r = 180.00$

AD1640 101 Olive Drab Paint on Steel

0 || $\theta_i = 10.00$
 + || $\phi_1 = 0.0$
 x || $\lambda = 0.63$



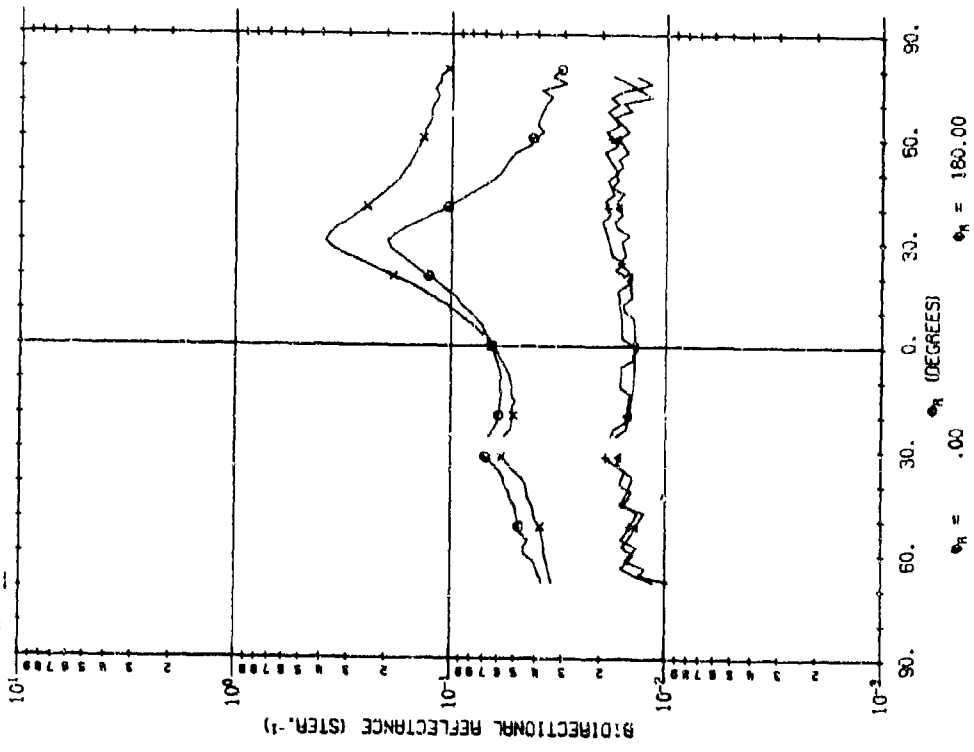
$\theta_i = .00$ $\theta_r = 180.00$

PAINT

AO1640 101

Olive Drab Paint on Steel

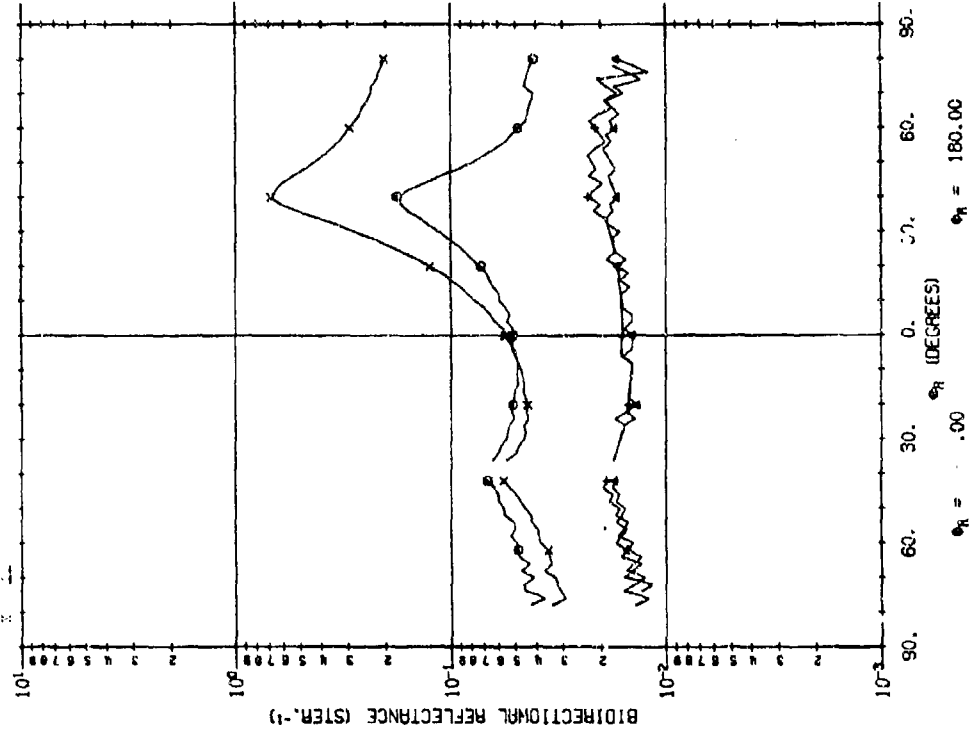
$\epsilon_1 = 30.00$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 0.63$



AO1640 101

Olive Drab Paint on Steel

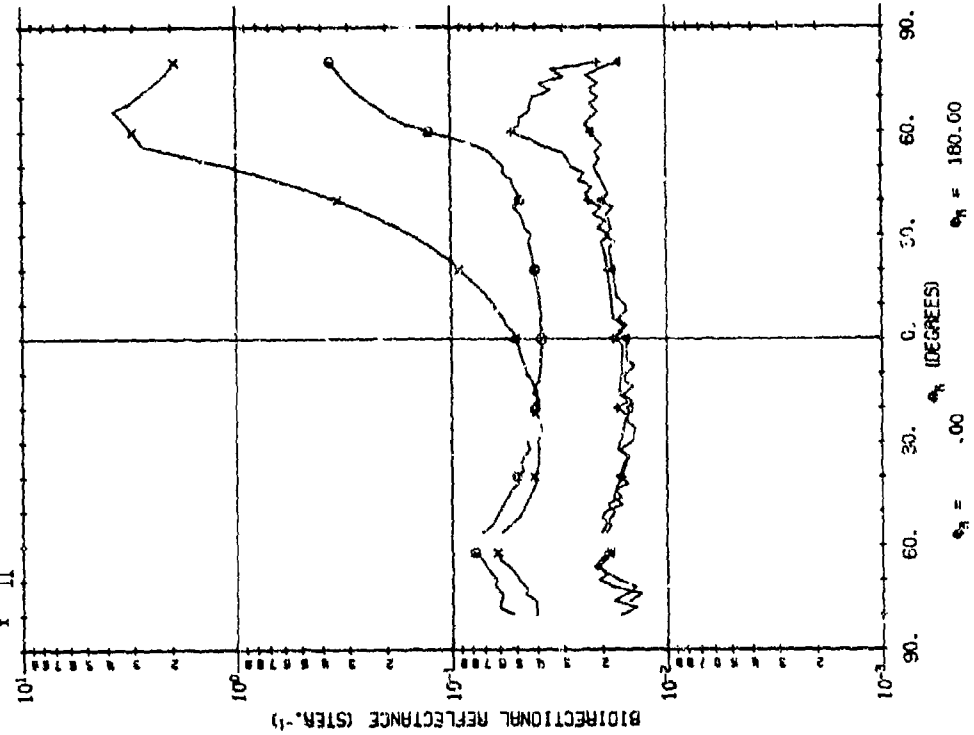
$\epsilon_1 = 40.68$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 0.63$



R01640 101 Olive Drab Paint on Steel

$\theta_1 = 60.00$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

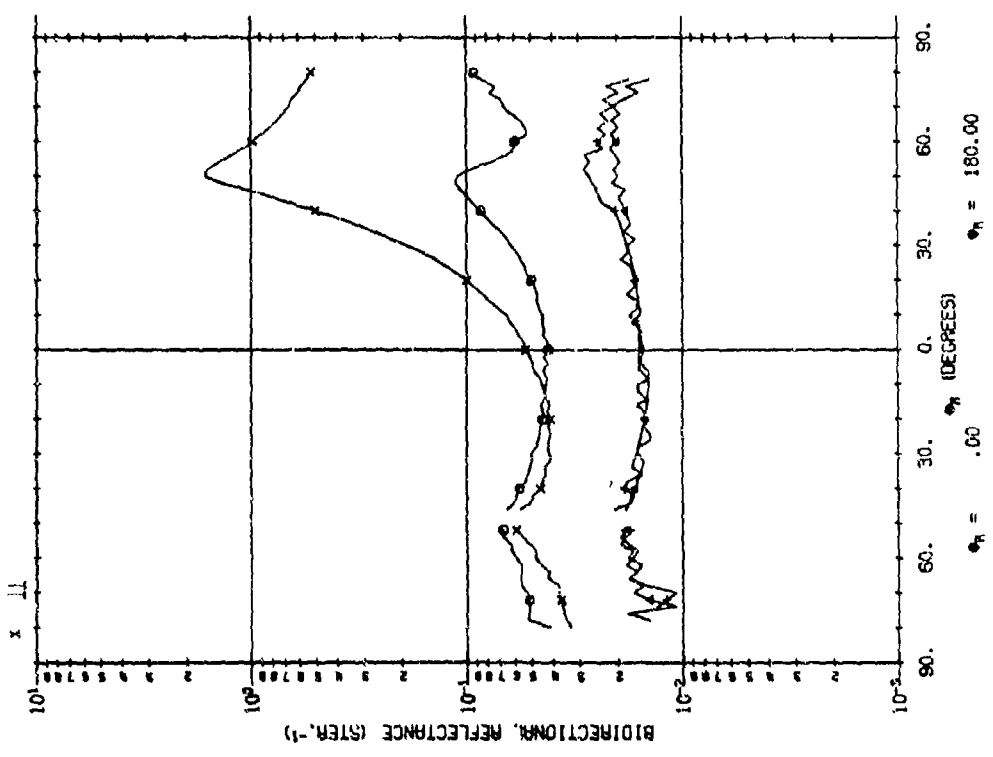
0 II
 + II
 x II



R01640 101 Olive Drab Paint on Steel

$\theta_1 = 50.00$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

0 II
 + II
 x II

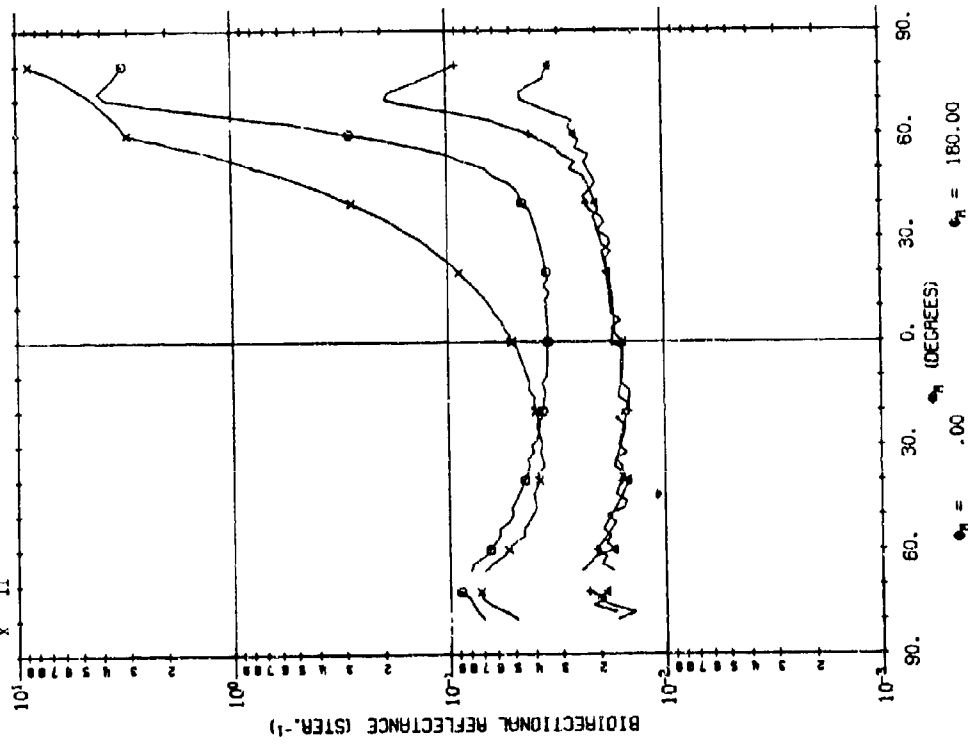


PAINT

A01640 101

Olive Drab Paint on Steel

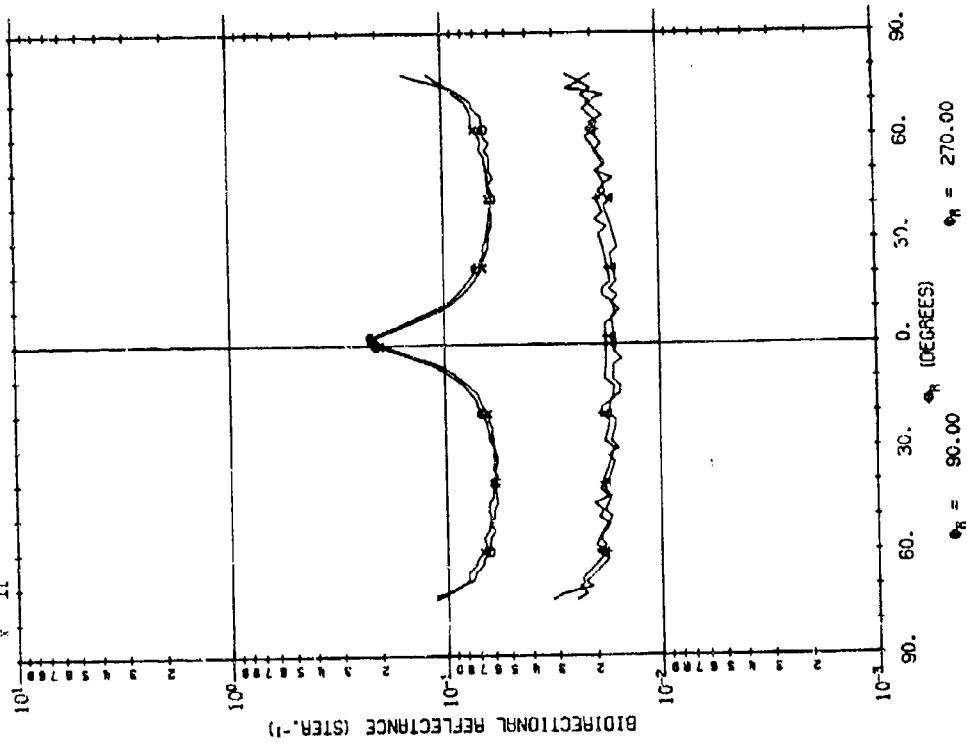
0 $\lambda_1 = 70.00$
 + $\lambda_2 = 0.0$
 - $\lambda_3 = 0.63$
 x $\lambda_4 = 0.63$

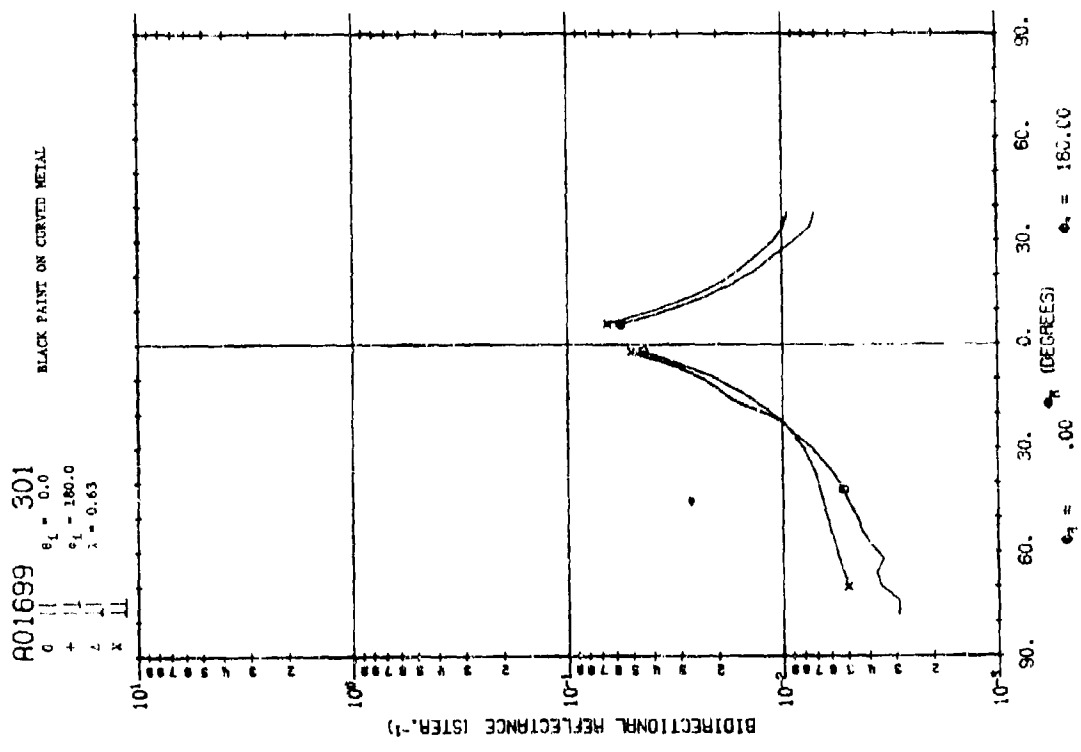
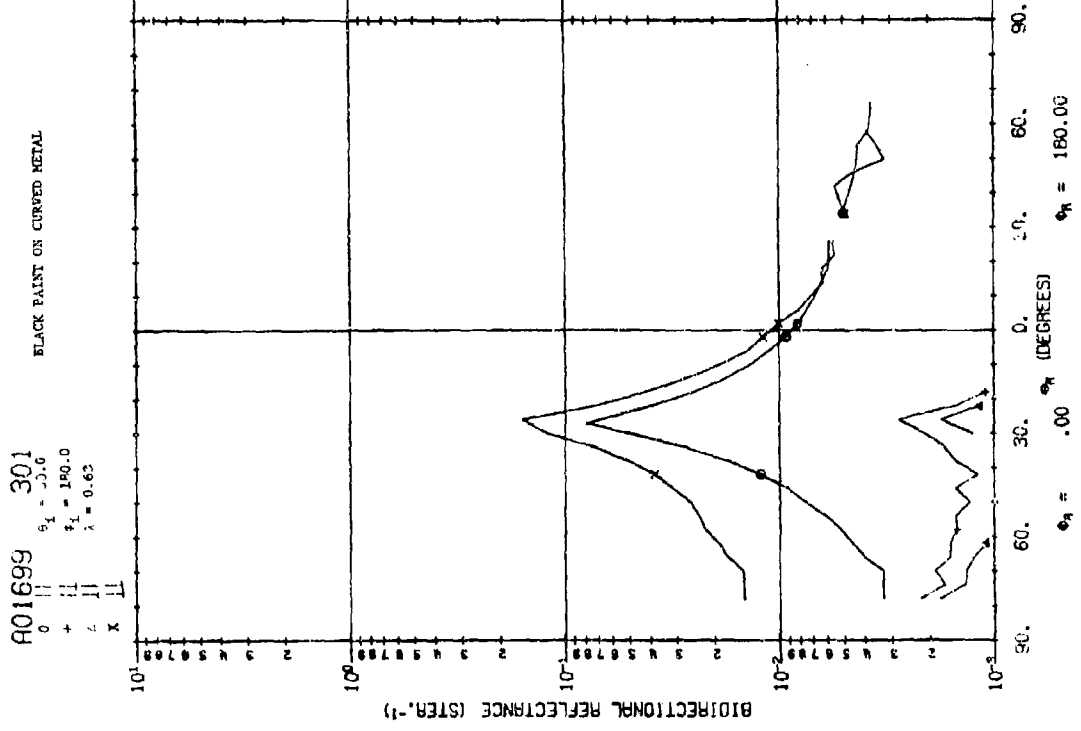


A01640 101

Olive Drab Paint on Steel

0 $\lambda_1 = 2.0$
 + $\lambda_2 = 0.63$
 - $\lambda_3 = 0.63$
 x $\lambda_4 = 0.63$





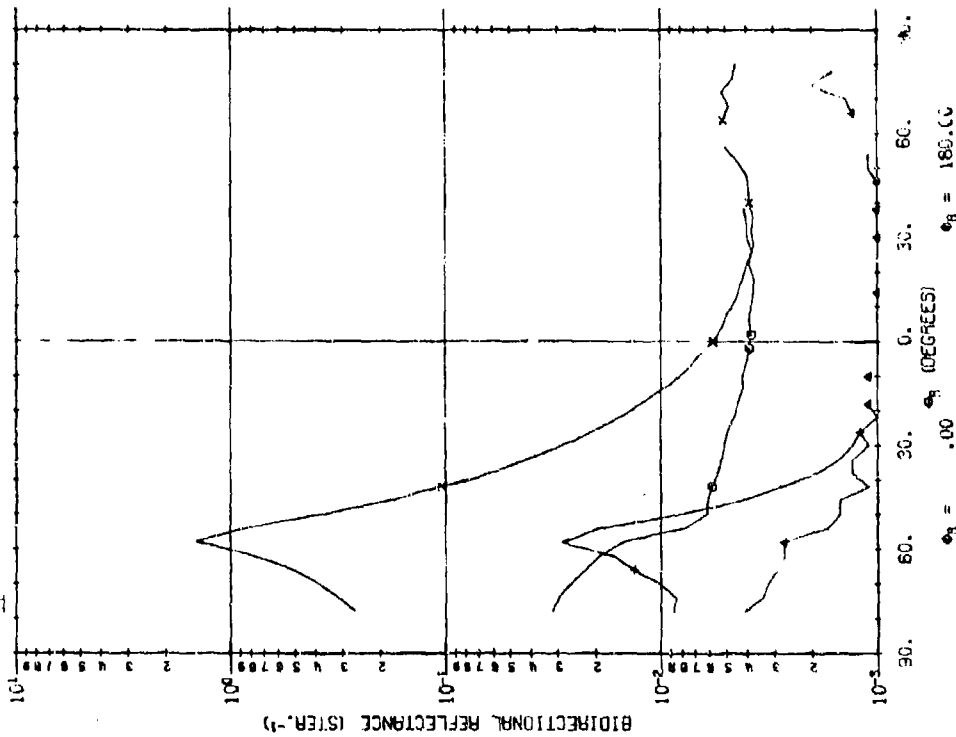
PAINT

A01699 301

BLACK PAINT ON CURVED METAL

$\phi_1 = 60.0$
 $\phi_2 = 180.0$
 $\lambda = 0.63$

0 \square
+ \square
- \square
x \square

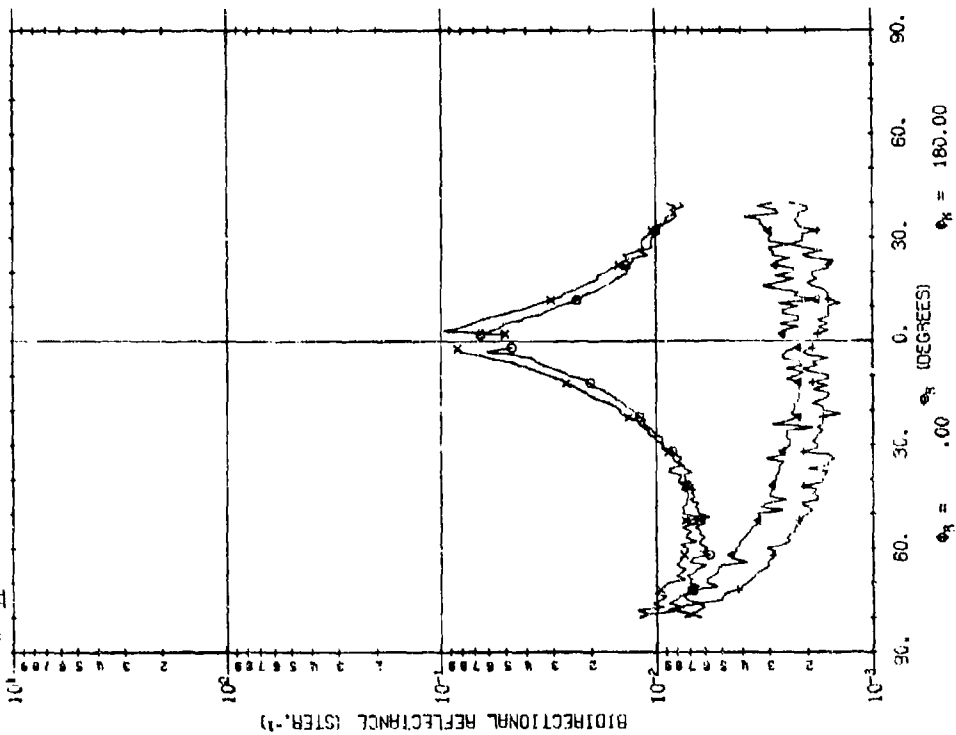


A01693 302

BLACK PAINT ON CURVED METAL

$\phi_1 = 0.0$
 $\phi_2 = 0.0$
 $\lambda = 1.06$

0 \square
+ \square
- \square
x \square

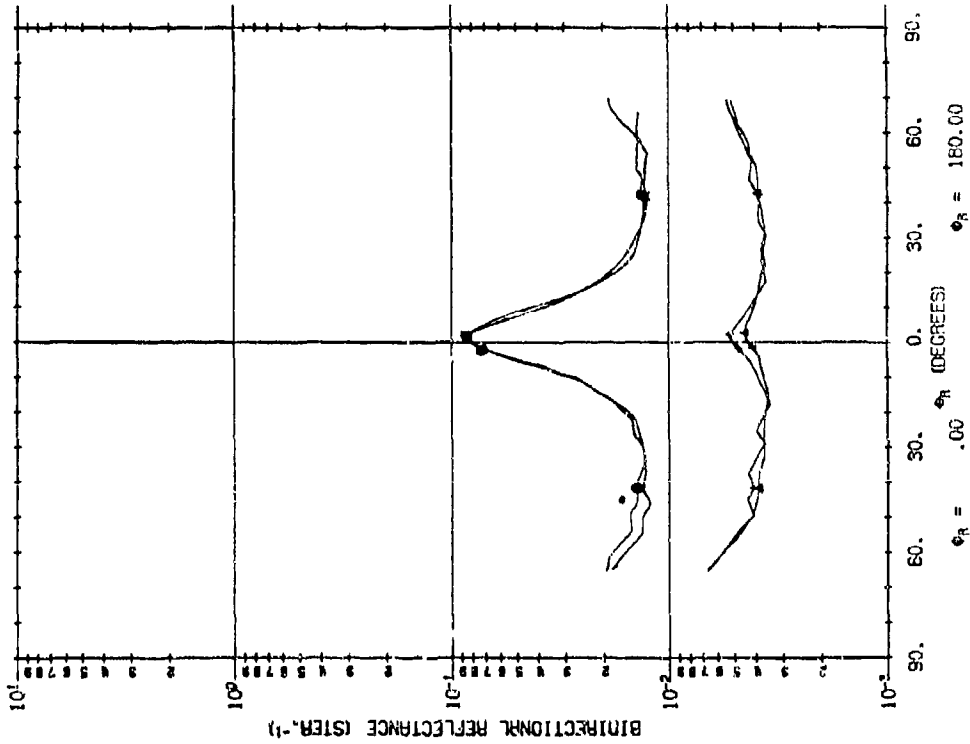


R01701 102

DARK OLIVE DRAB PAINT ON METAL

$2\epsilon = 2.0$
 $\phi_1 = \phi_r$
 $\lambda = 0.63$

0 ||
+ ||
x ||
x ||

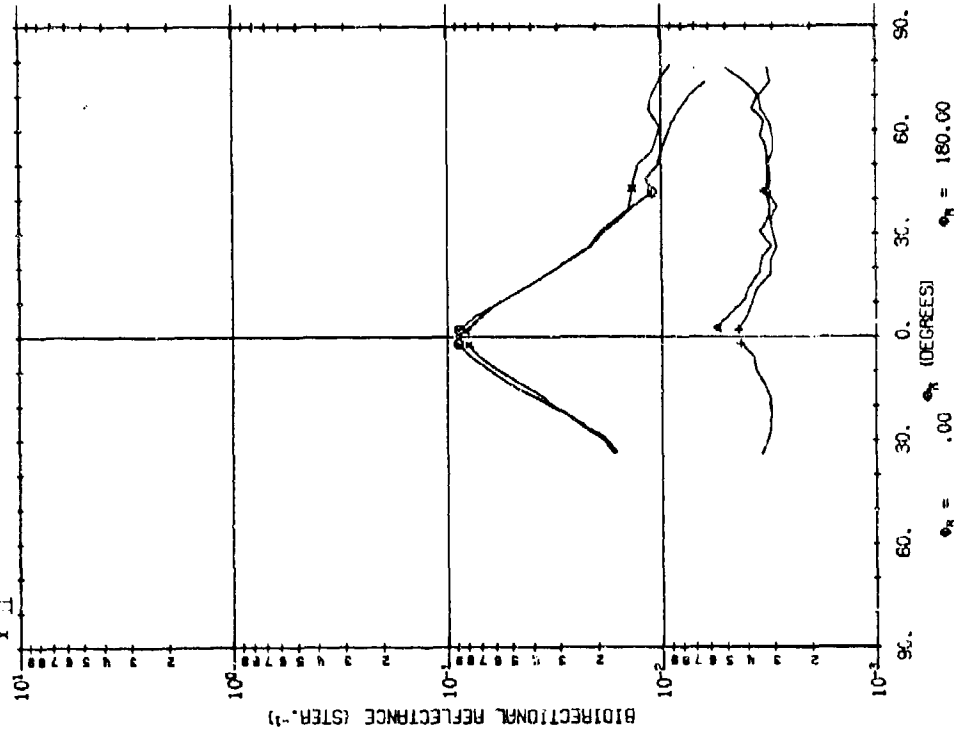


R01701 102

DARK OLIVE DRAB PAINT ON METAL

$2\epsilon = 0.0$
 $\phi_1 = \phi_r$
 $\lambda = 0.63$

0 ||
+ ||
x ||
x ||



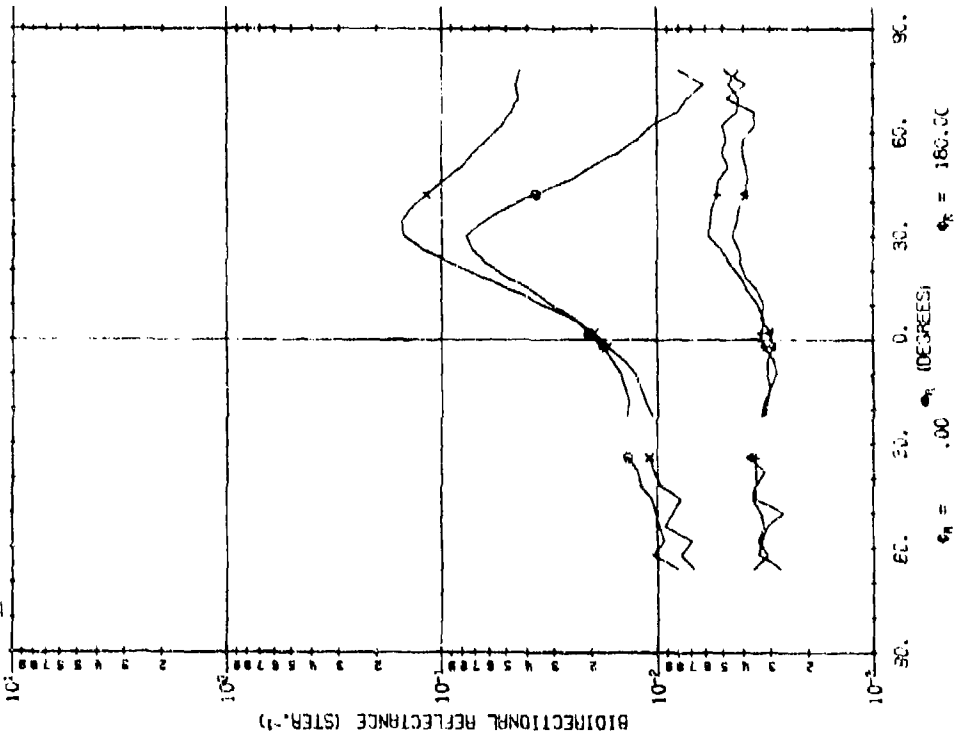
PAINT

AO1701 102

DARK OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 30.0$
 $\epsilon_2 = 0.0$
 $\nu = 0.63$

0
 +
 -
 x

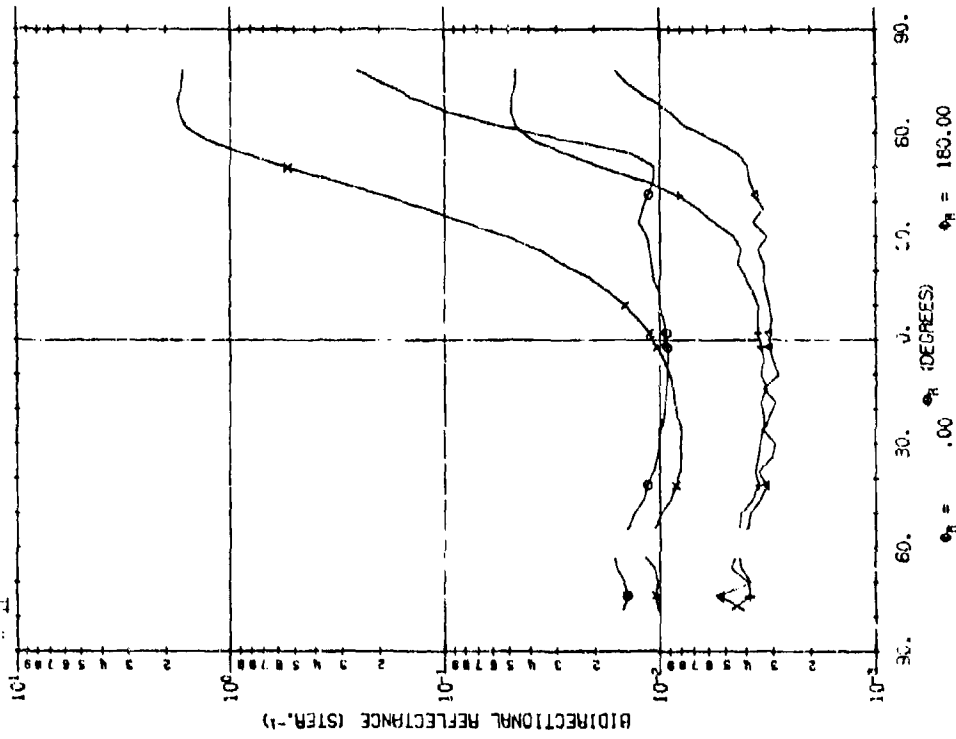


AO1701 102

DARK OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 60.0$
 $\epsilon_2 = 0.0$
 $\nu = 0.63$

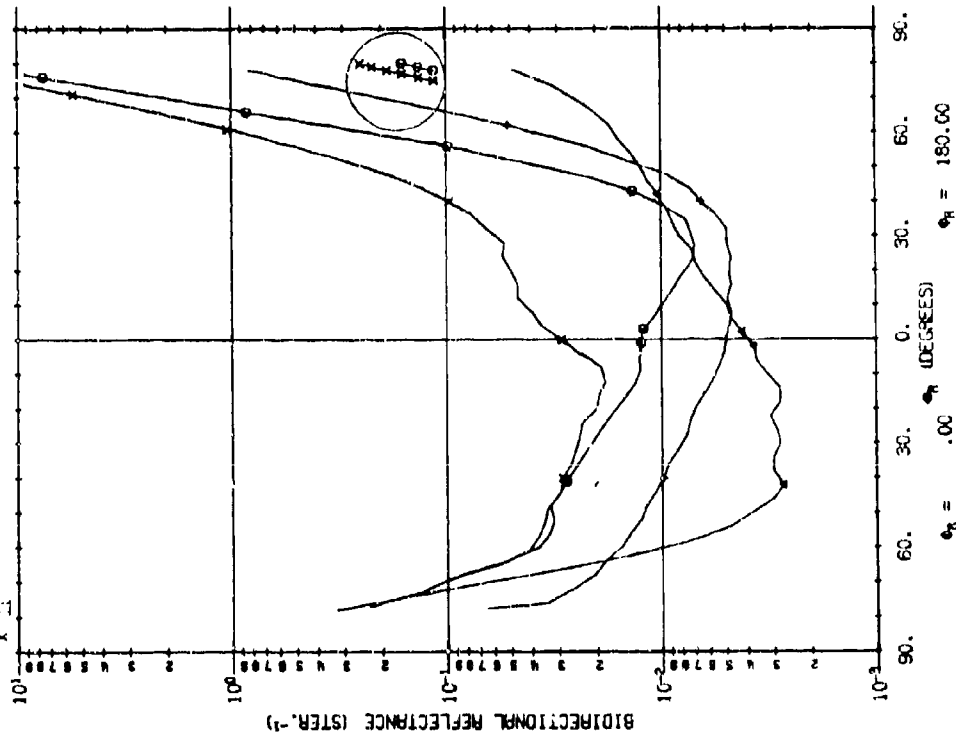
0
 +
 -
 x



A01701 102

DARK OLIVE DRAB PAINT ON METAL

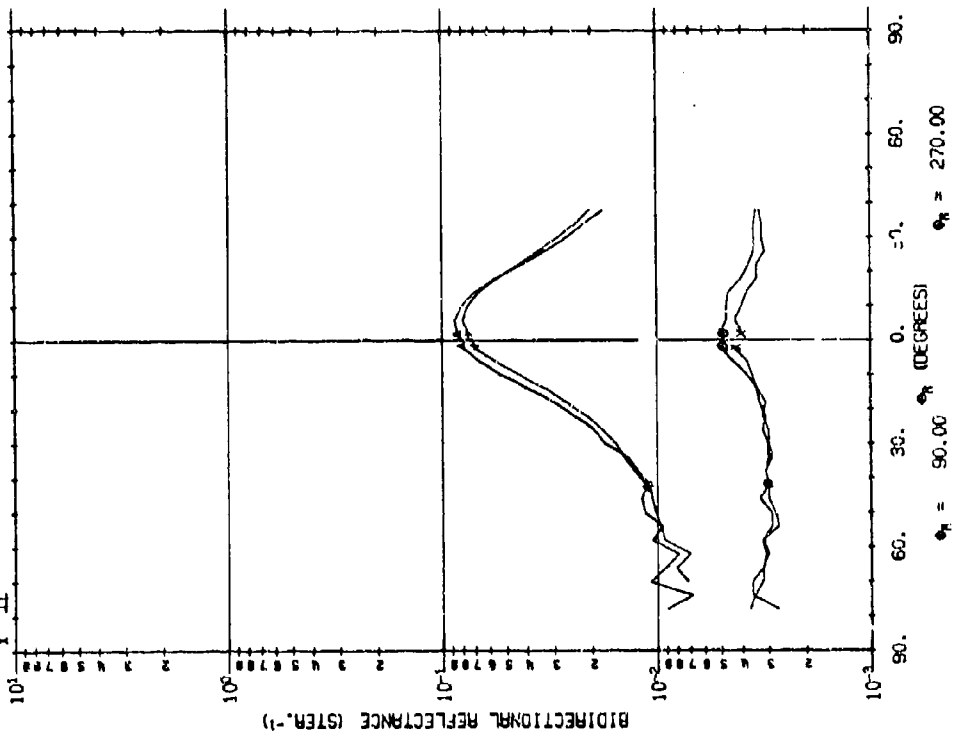
0 || $\phi_L = 80.0$
+ || $\phi_L = 0.0$
x || $\lambda = 0.63$
K ||



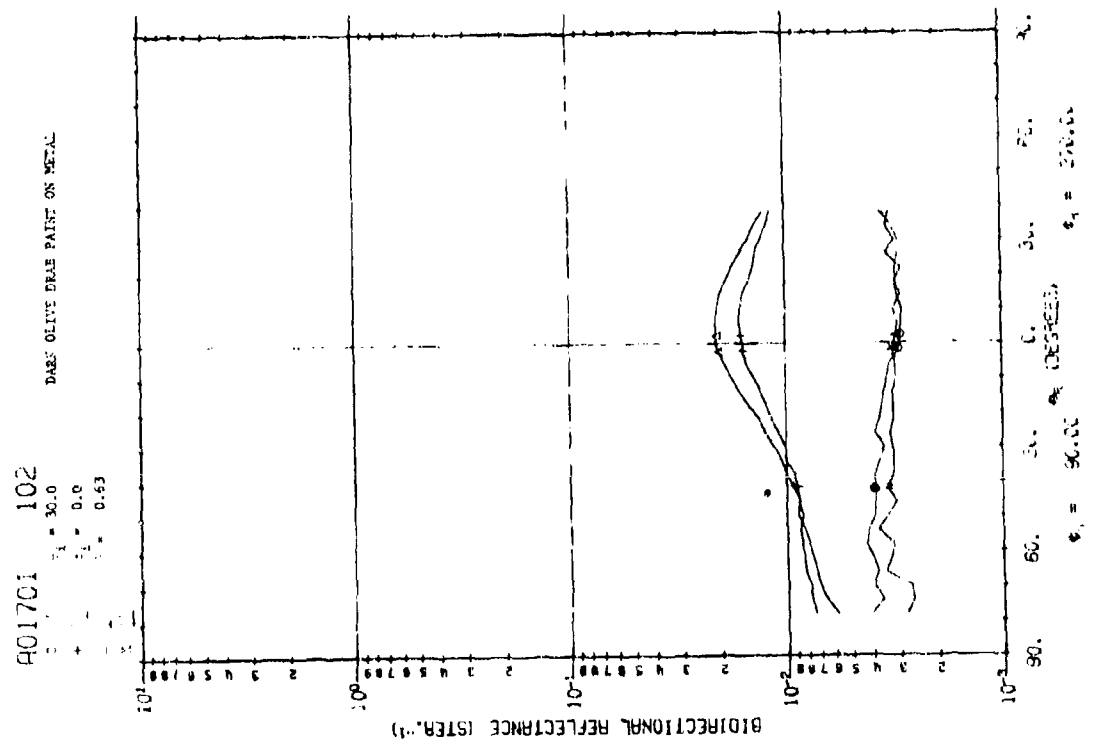
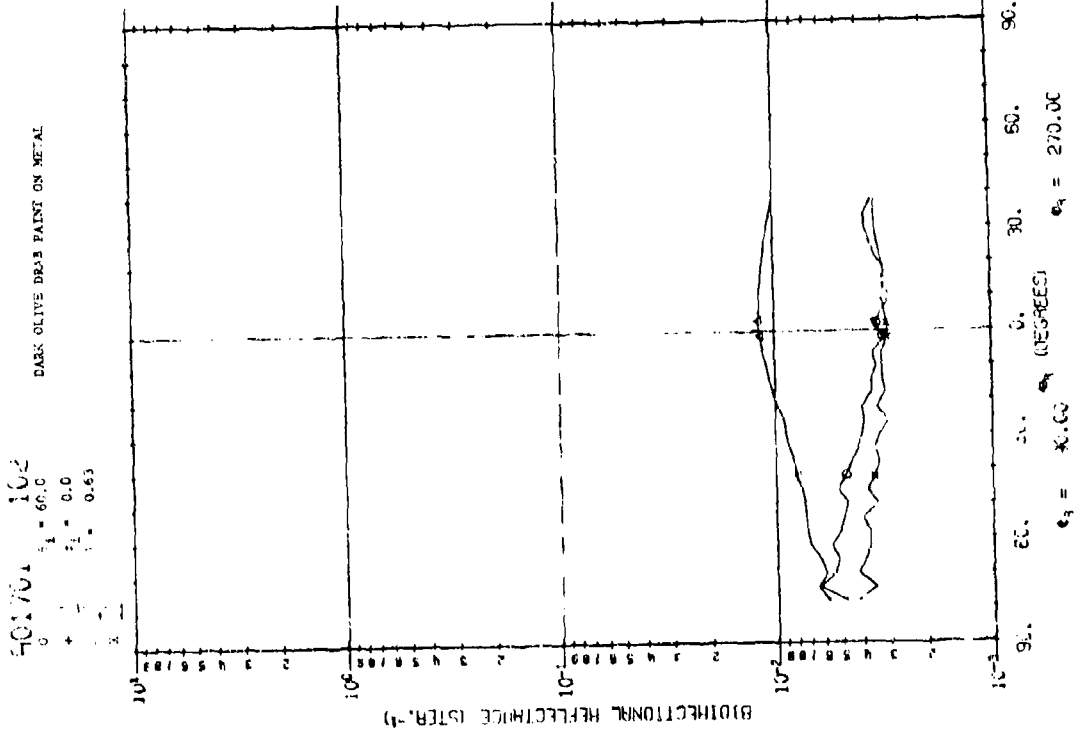
A01701 102

DARK OLIVE DRAB PAINT ON METAL

0 || $\phi_L = 0.0$
+ || $\phi_L = 0.0$
x || $\lambda = 0.63$
K ||



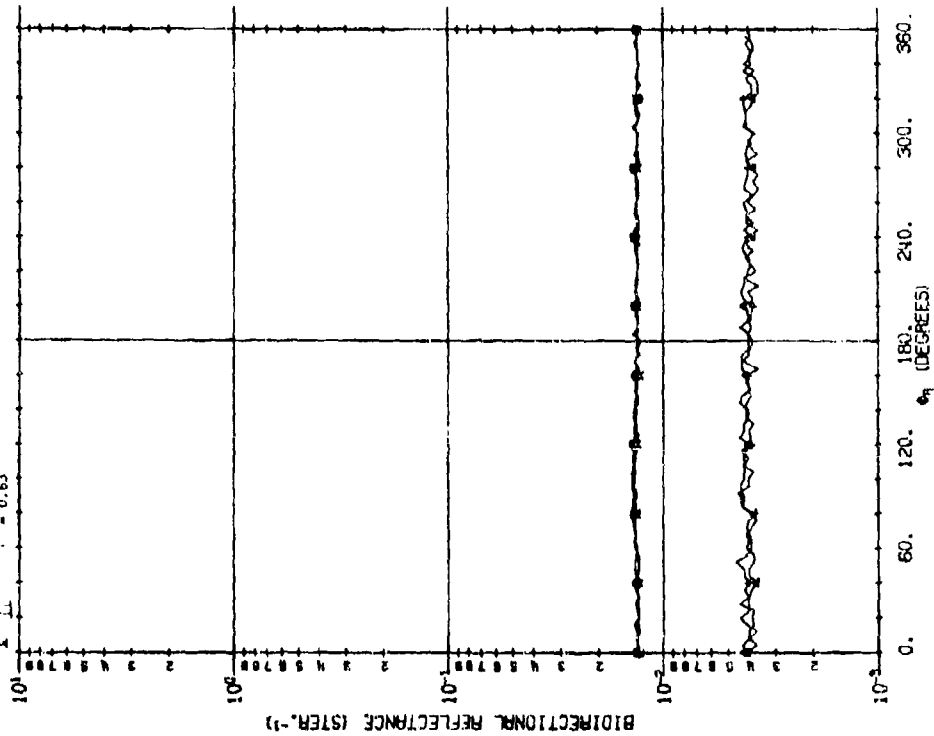
PAINT



A01701 102

DARK OLIVE DRAB PAINT ON METAL

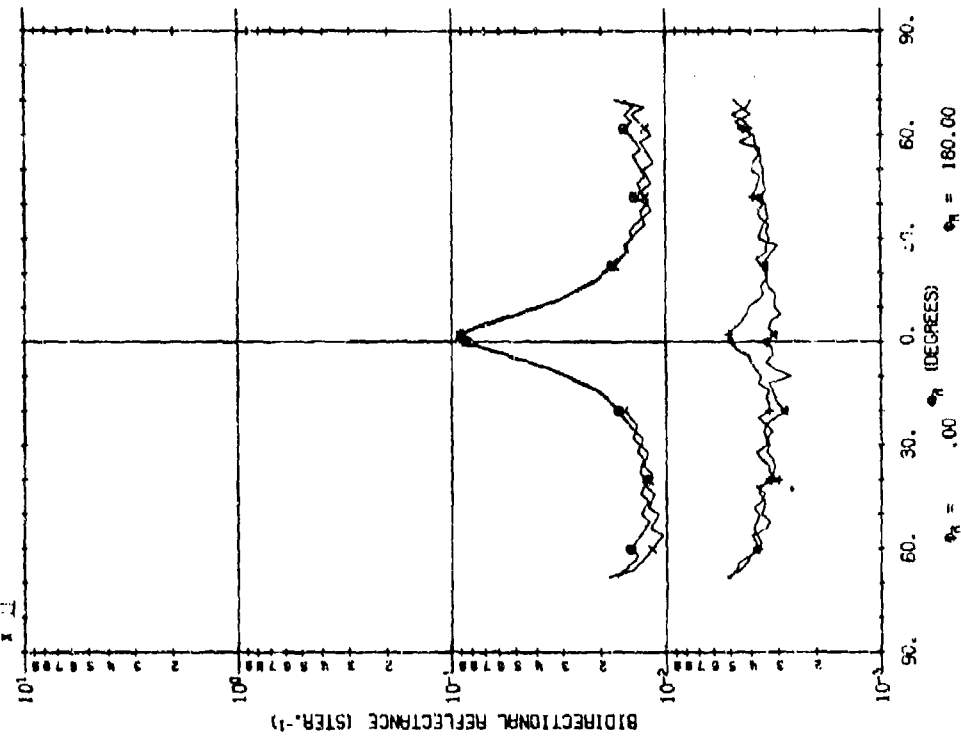
$\theta_i = 45.0$
 $\theta_r = 47.0$
 $\phi_i = 45$
 $\phi_r = 0.63$



A01701 201

DARK OLIVE DRAB PAINT ON METAL

$\theta_i = 2.0$
 $\theta_r = 4$
 $\phi_i = 45$
 $\phi_r = 0.63$

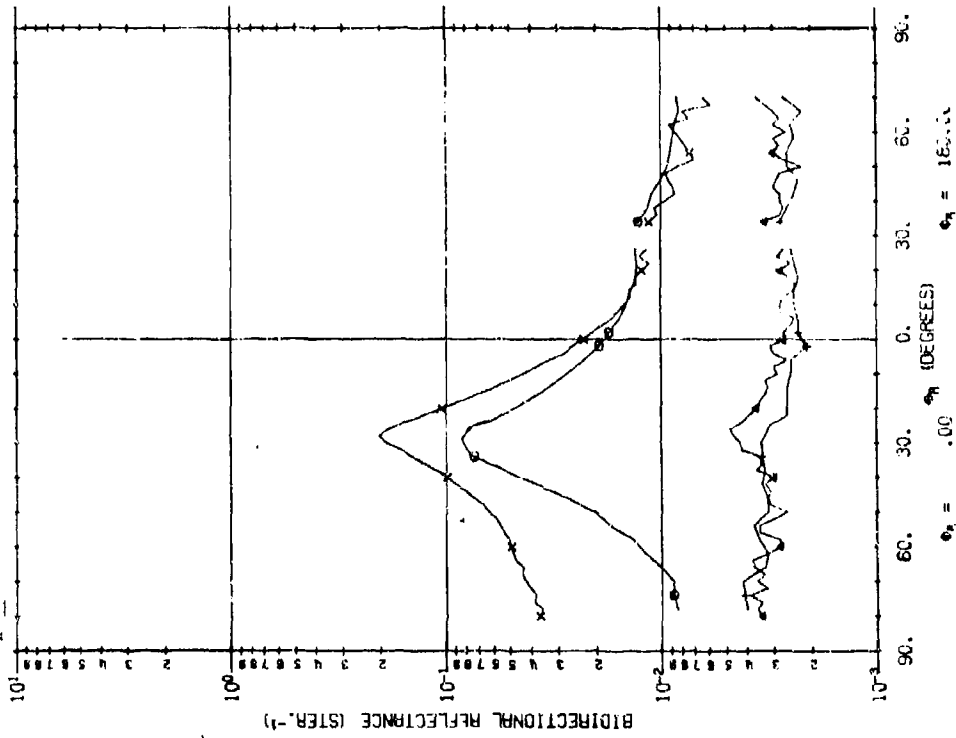


PAINT

A01701 201

DARK OLIVE DRAB PAINT ON METAL

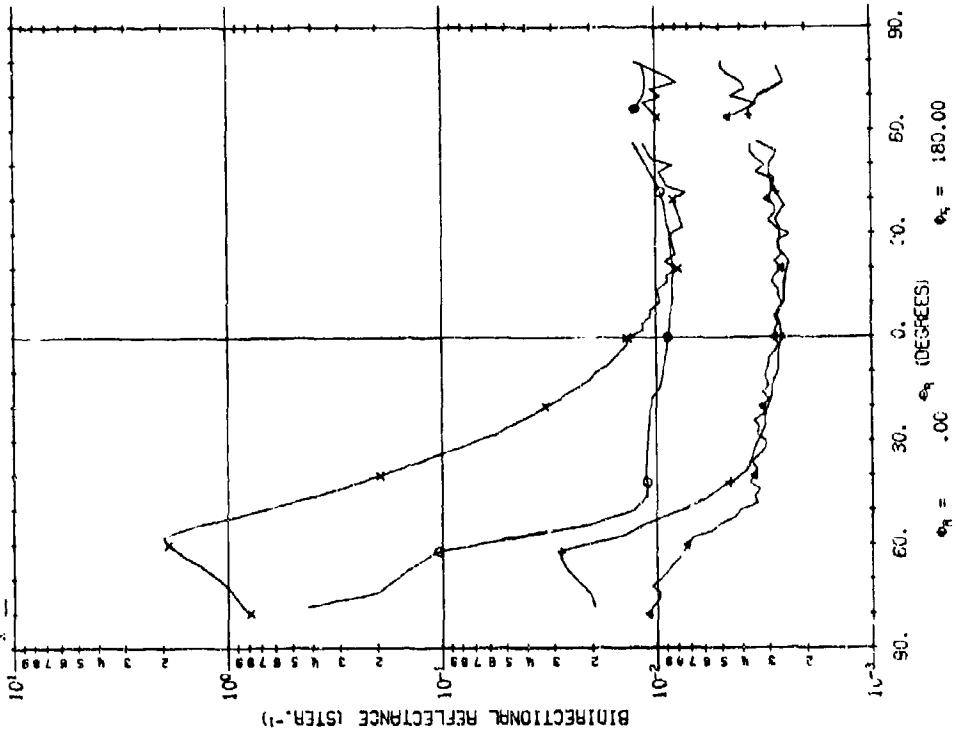
$\theta_i = 30.0$
 $\theta_r = 180.0$
 $\phi = 0.63$



A01701 201

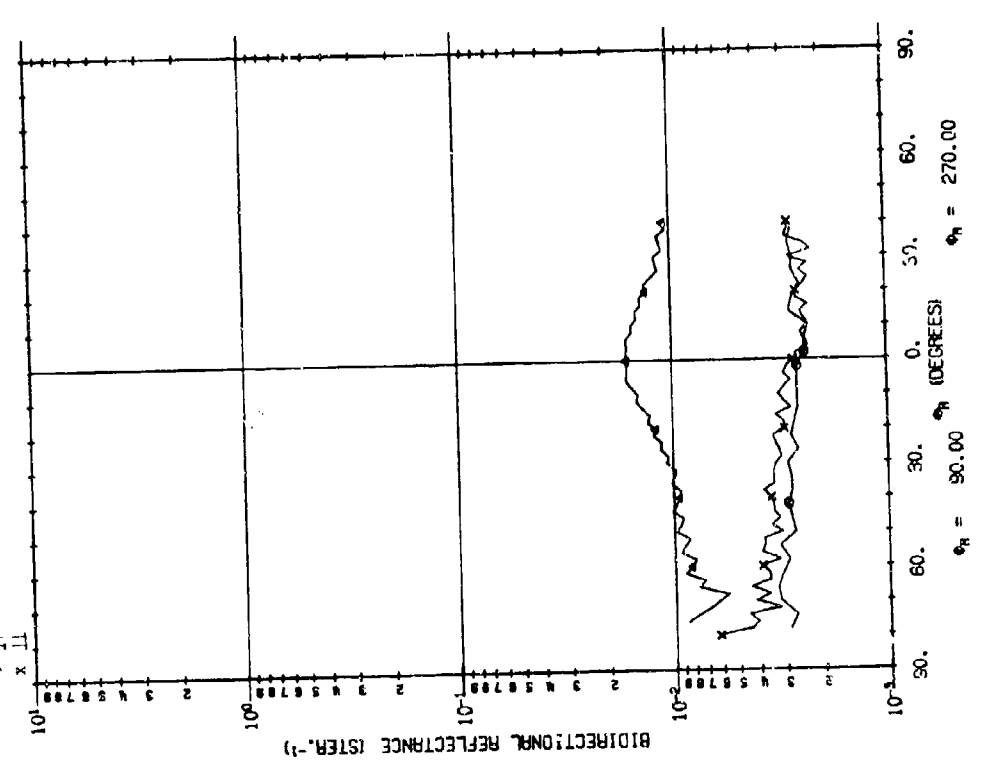
DARK OLIVE DRAB PAINT ON METAL

$\theta_i = 60.0$
 $\theta_r = 180.0$
 $\phi = 0.63$



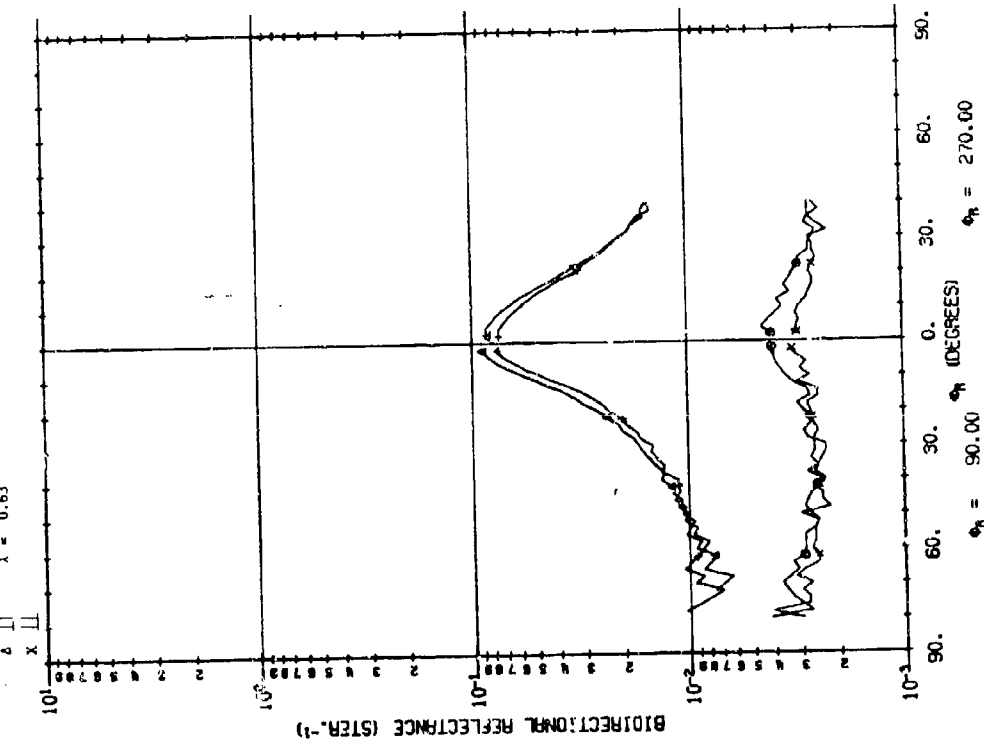
A01701 201
 0 || $\phi_1 = 30.0$
 + || $\phi_2 = 180.0$
 : || $\lambda = 0.63$
 X ||

DARK OLIVE DRAB PAINT ON METAL



A01701 201
 0 || $\phi_1 = 0.0$
 + || $\phi_2 = 180.0$
 : || $\lambda = 0.63$
 X ||

DARK OLIVE DRAB PAINT ON METAL

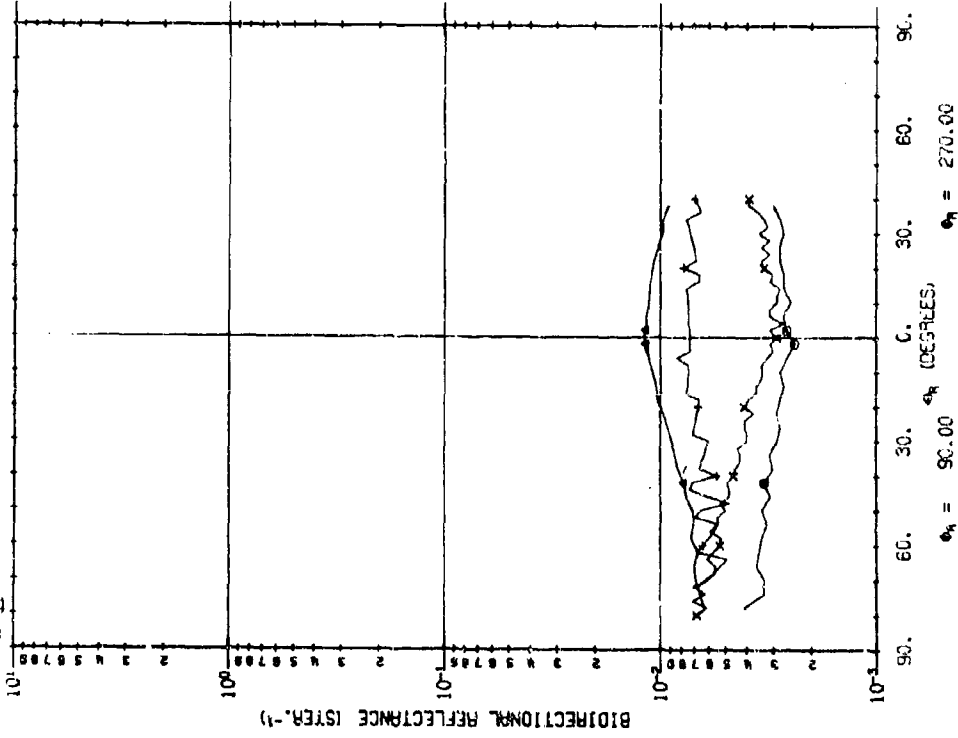


PAINT

R01701 201

DARK OLIVE DRAB PAINT ON METAL

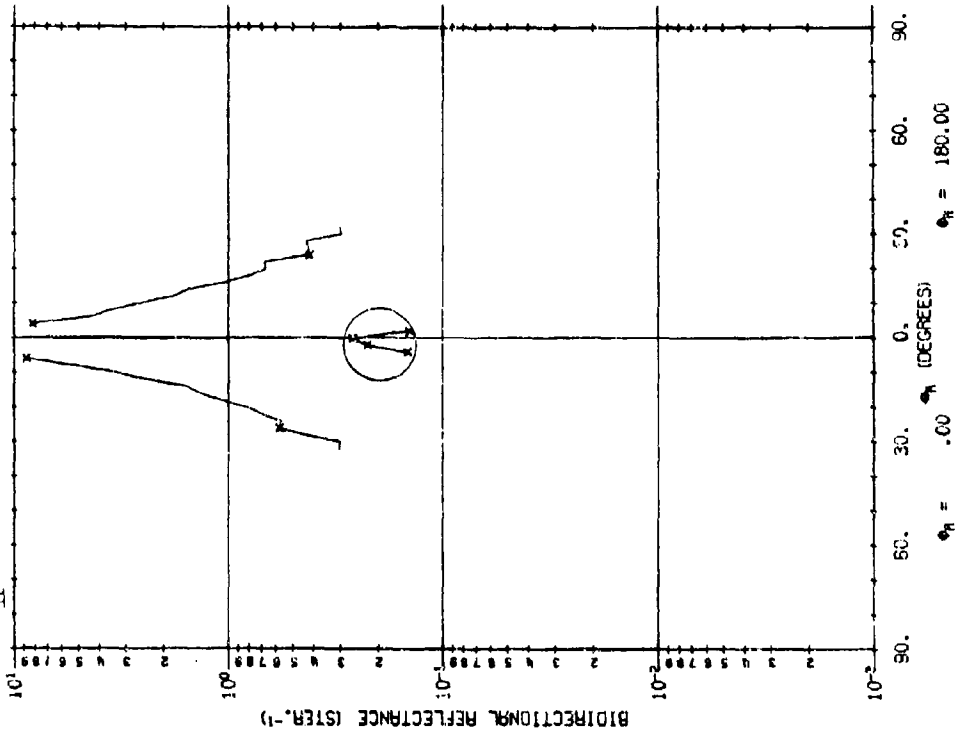
0 | | $\epsilon_1 = 60.0$
+ | | $\epsilon_2 = 180.0$
x | | $\lambda = 0.63$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

0 | | $\epsilon_1 = 3.0$
+ | | $\epsilon_2 = 6.0$
x | | $\lambda = 10.6$



A01701 101

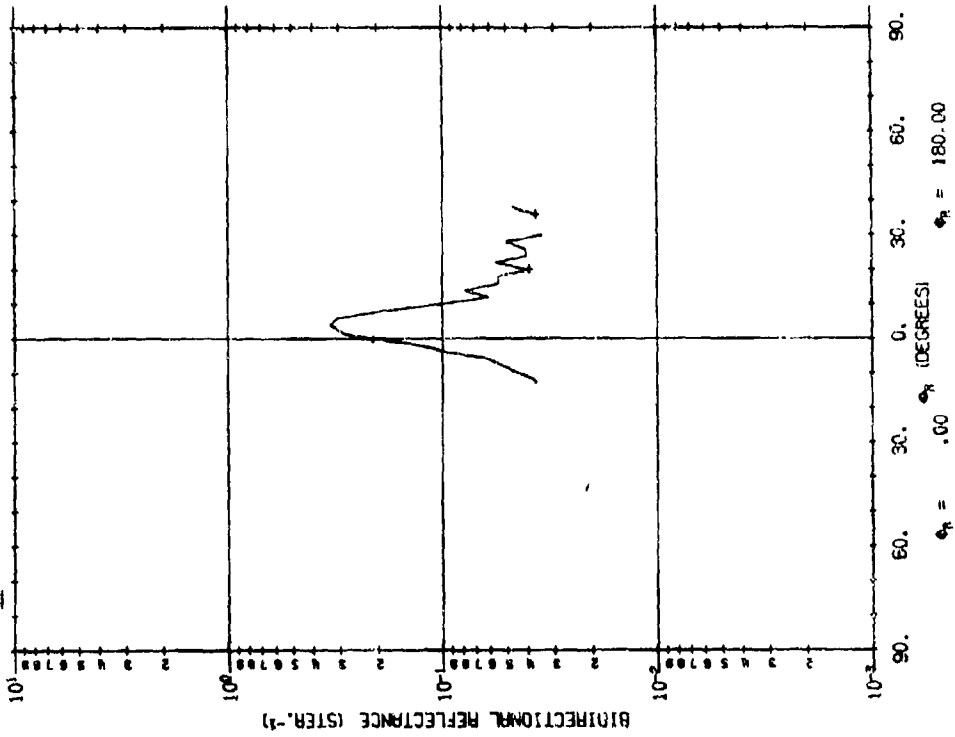
DARK OLIVE DRAB PAINT ON METAL

$2\theta = 1.0$

$\phi_1 = \phi_2$

$\lambda = 10.6$

0 ||
+ ||
Δ ||
x ||



A01701 101

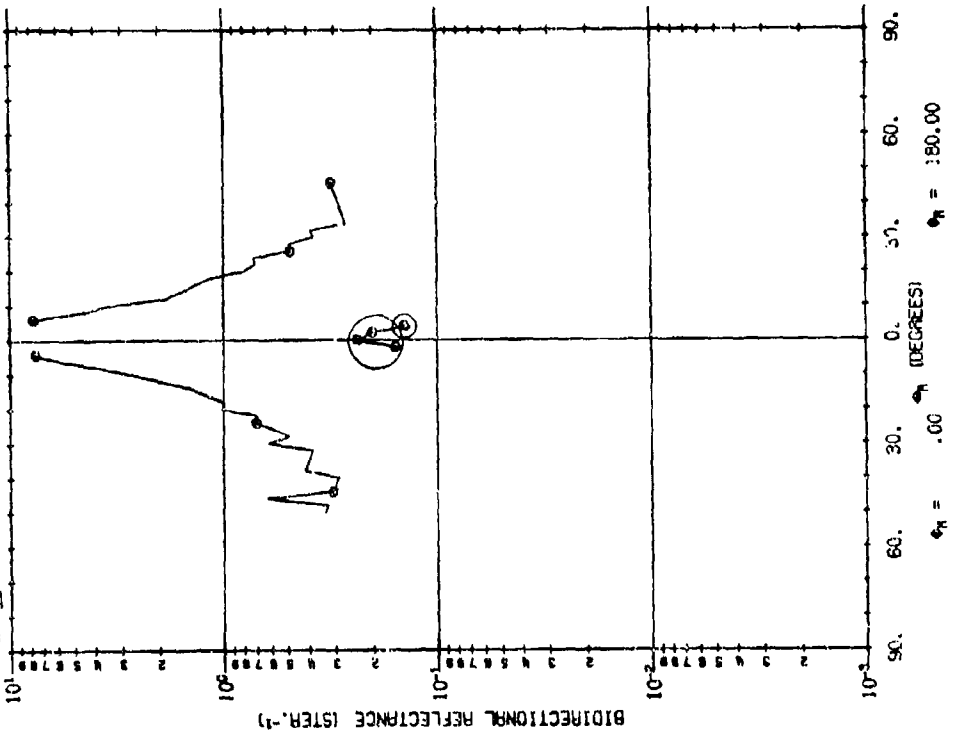
DARK OLIVE DRAB PAINT ON METAL

$2\theta = 1.0$

$\phi_1 = \phi_2$

$\lambda = 10.6$

0 ||
+ ||
Δ ||
x ||

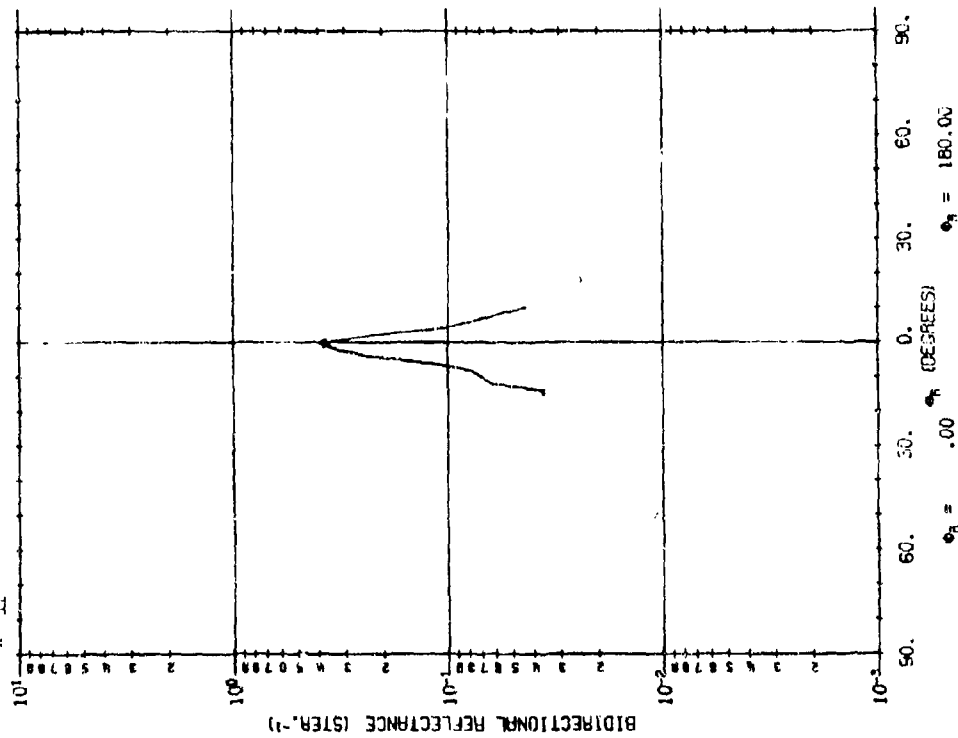


R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 1.0$
 $\theta_2 = 2.0$
 $\theta_3 = 10.6$

0 II
+ II
- II
x II

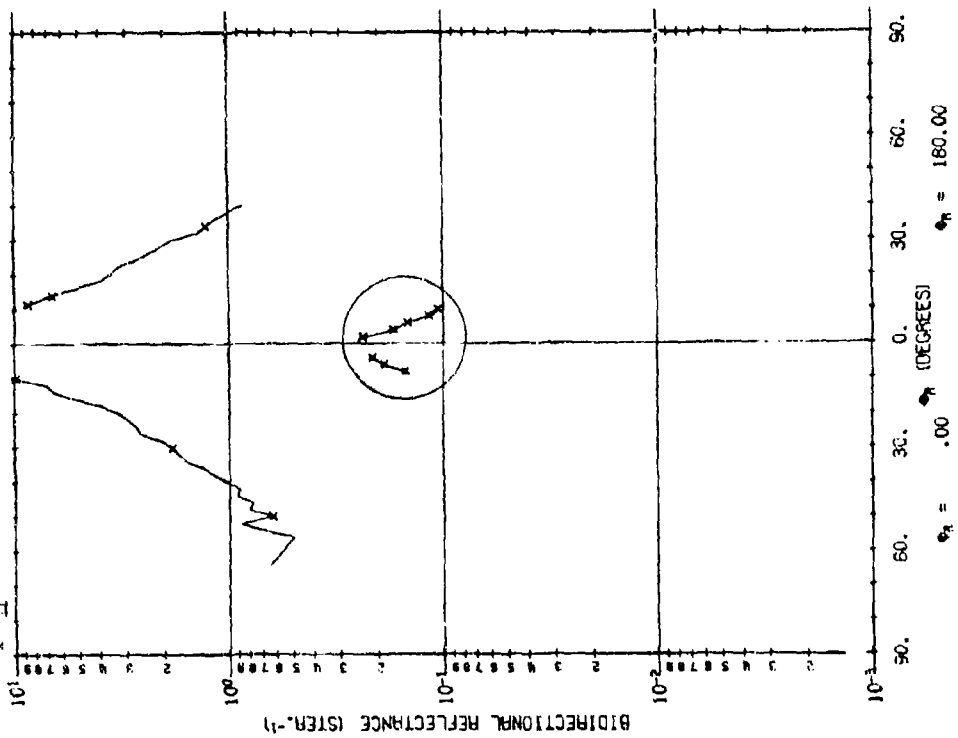


R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\theta_3 = 10.6$

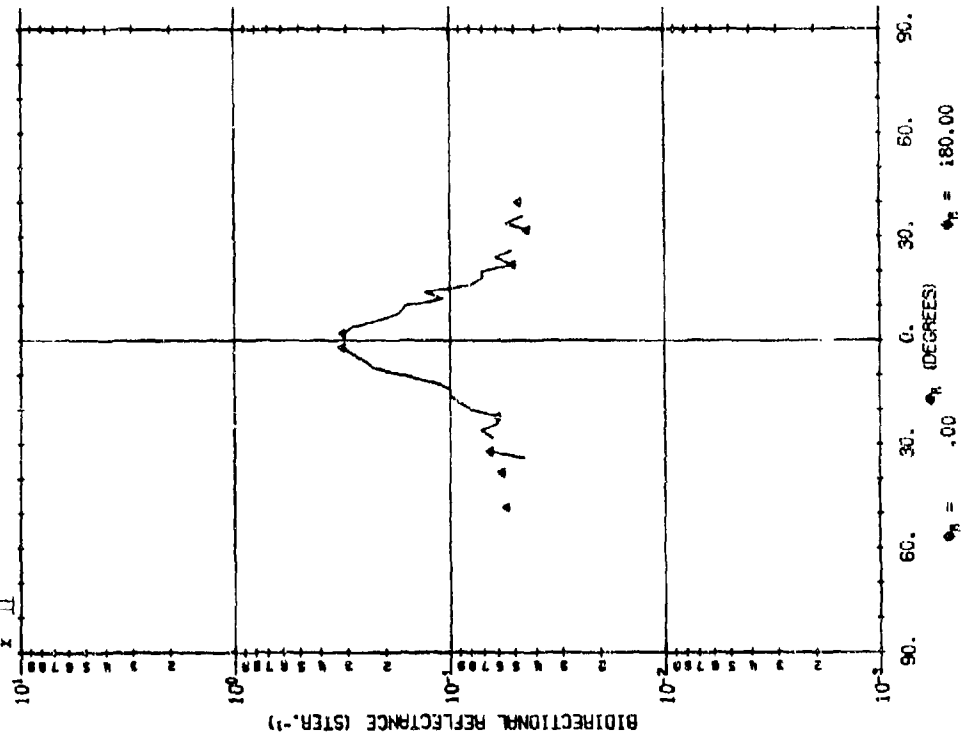
0 II
+ II
- II
x II



R01701 101

DARK OLIVE DRAB PAINT ON METAL

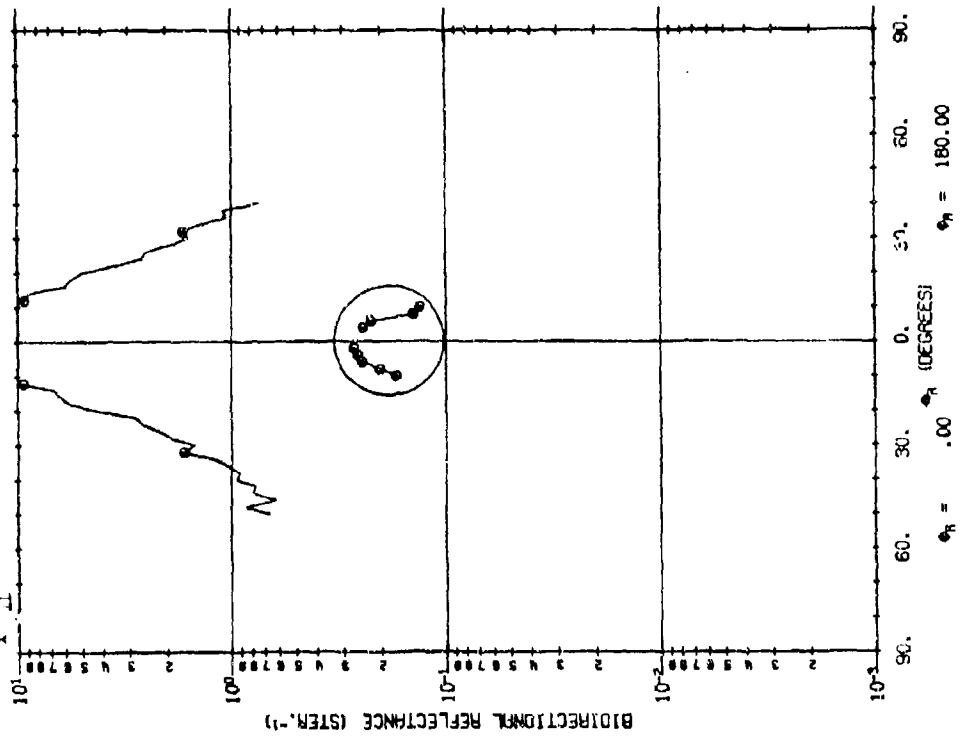
$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$

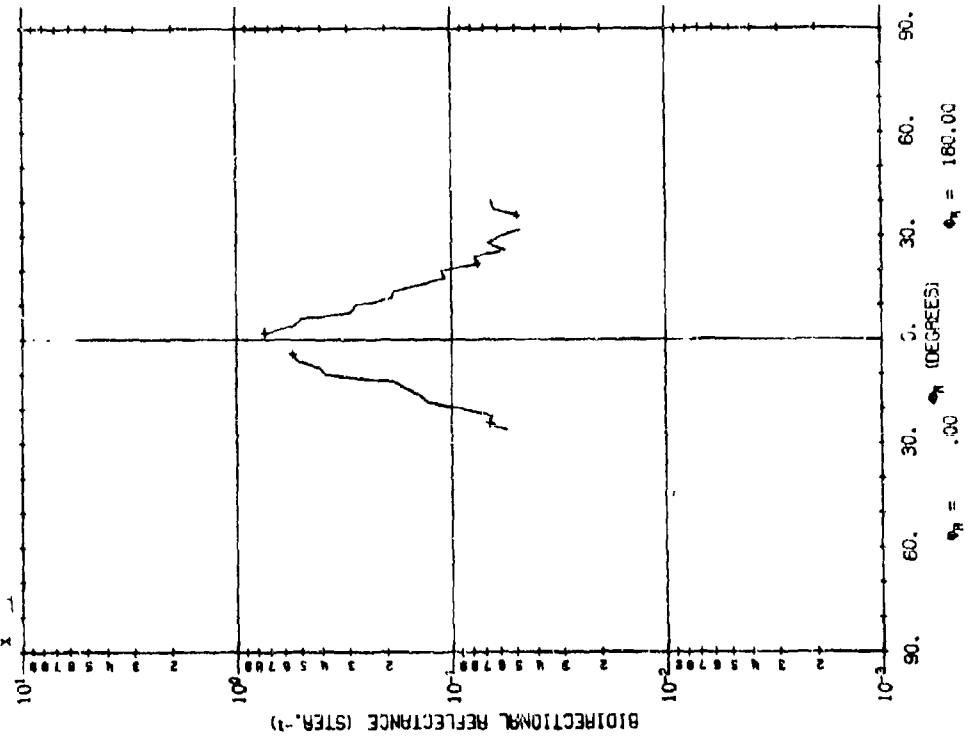


PAINT

R01701 101

DARK OLIVE DRAB PAINT ON METAL

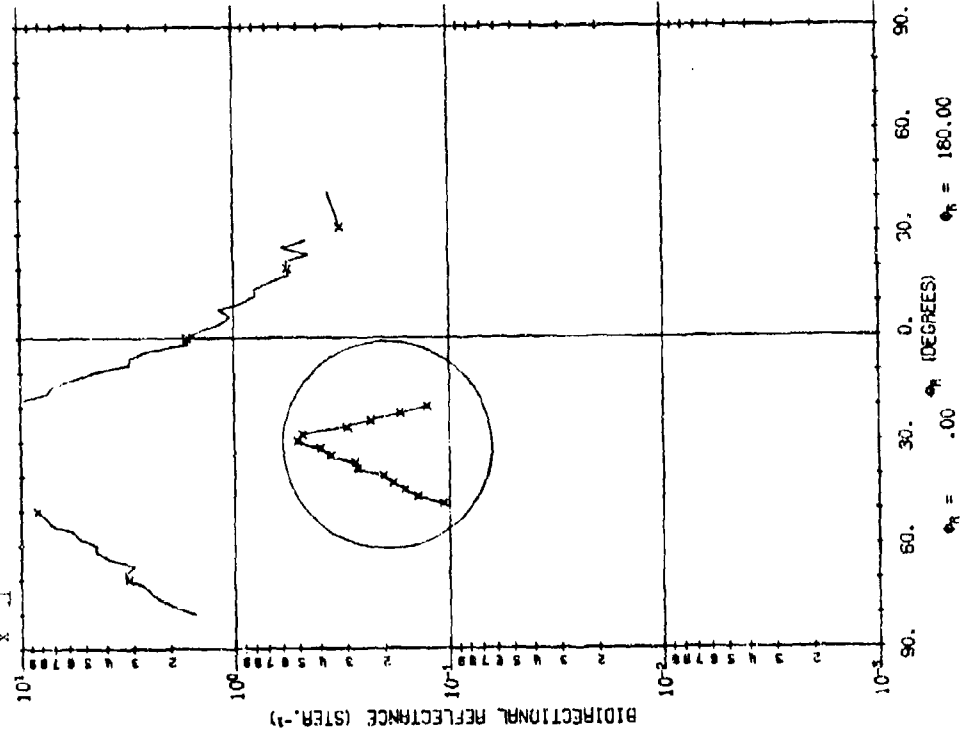
$\theta = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$



R01701 101

DARK CLIVE DRAB PAINT ON METAL

$\theta = 30.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$

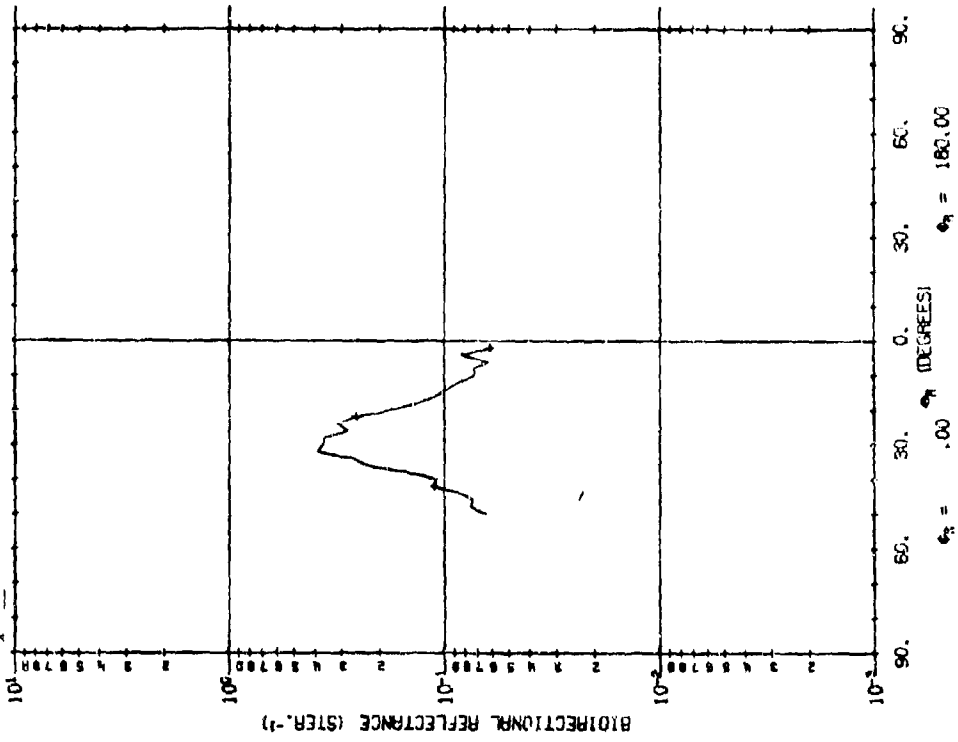


R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$

0 ||
+ ||
x ||

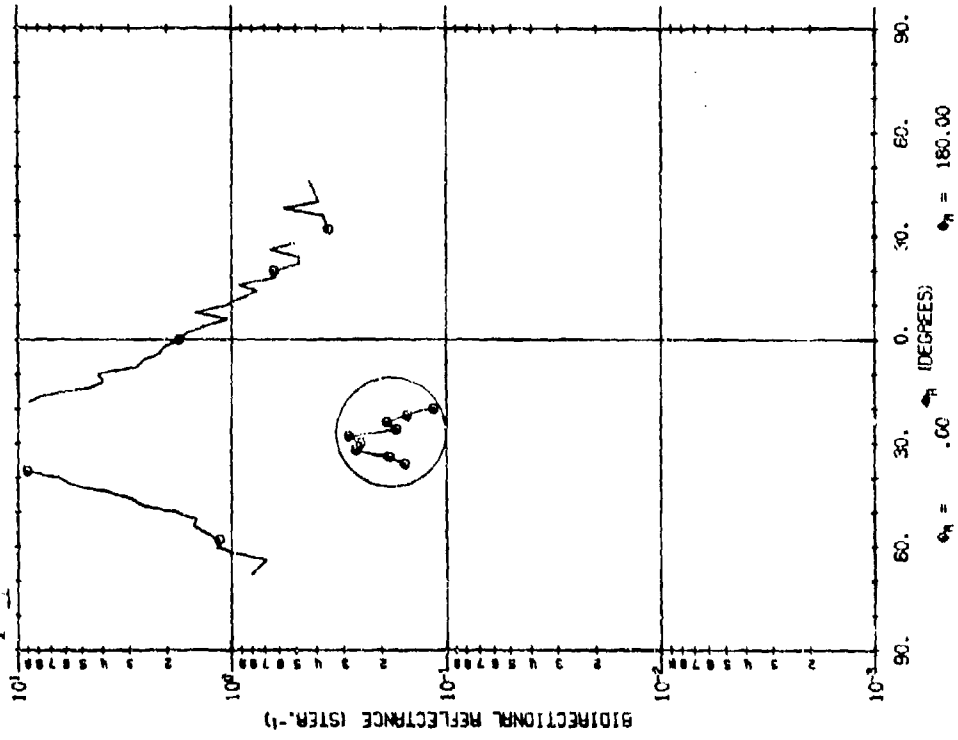


R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$

0 ||
+ ||
x ||

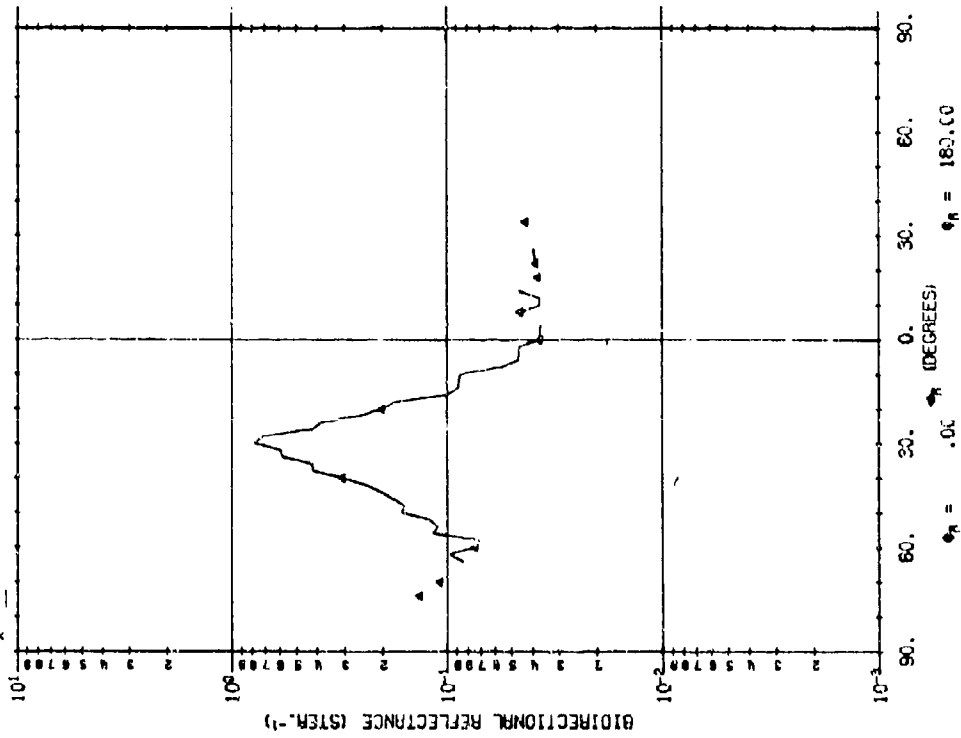


PAINT

R01/01 101

DARK OLIVE DRAB PAINT ON METAL

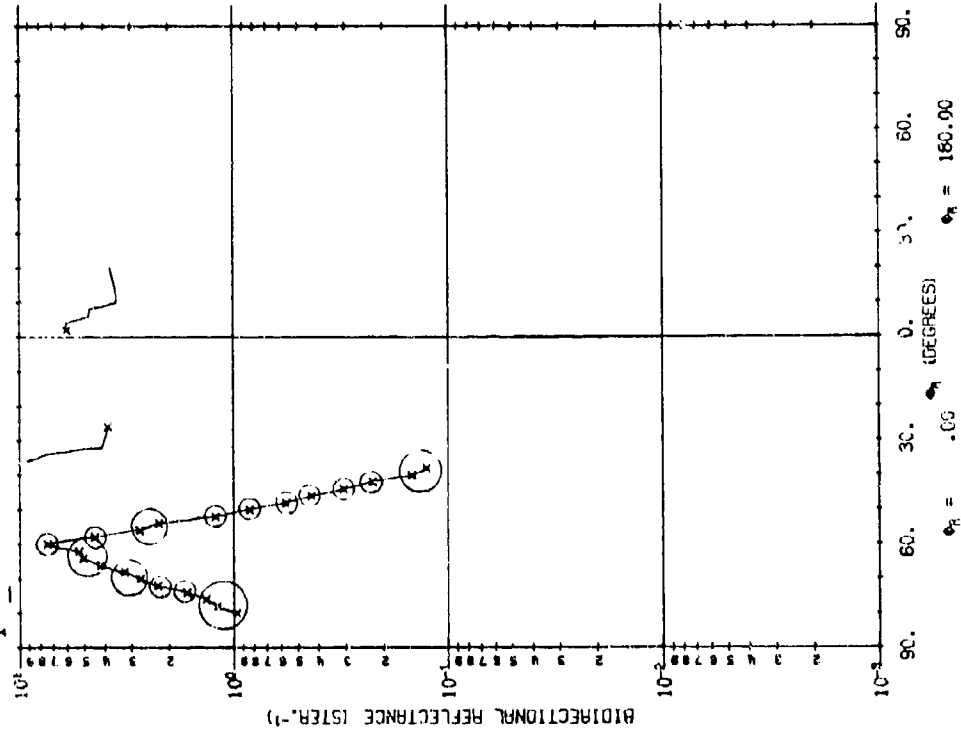
$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$



R01/01 101

DARK OLIVE DRAB PAINT ON METAL

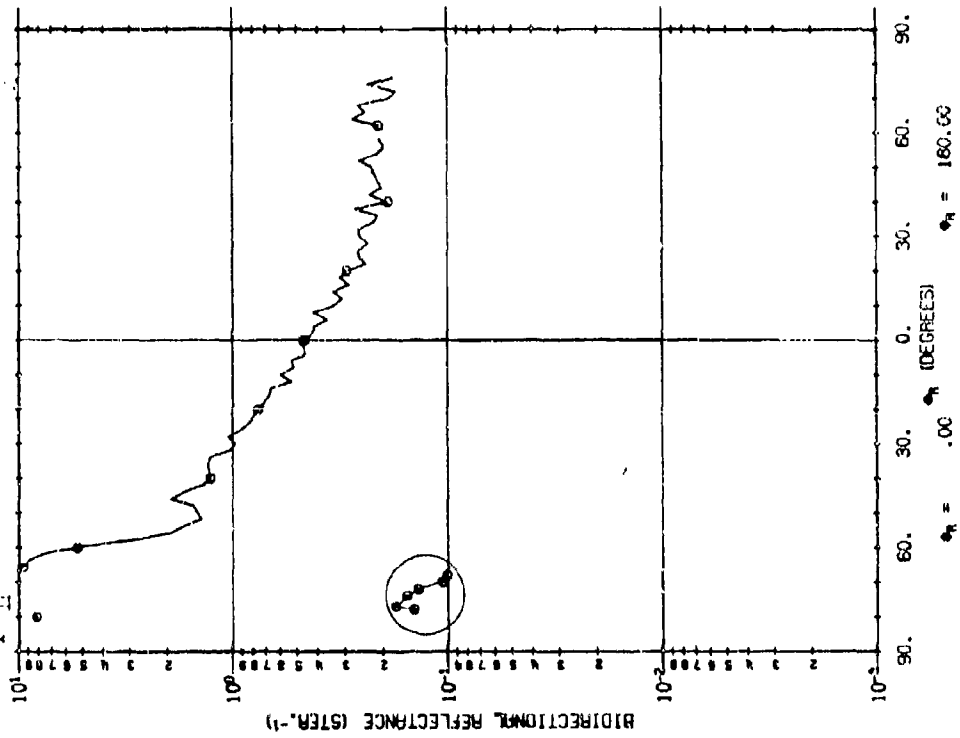
$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

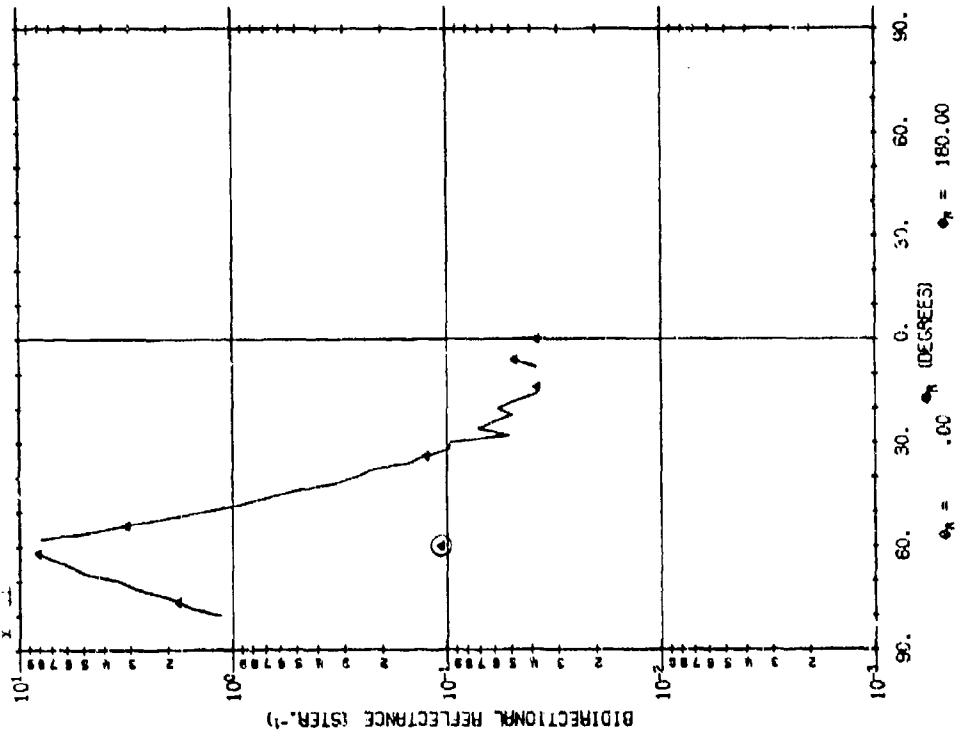
$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$

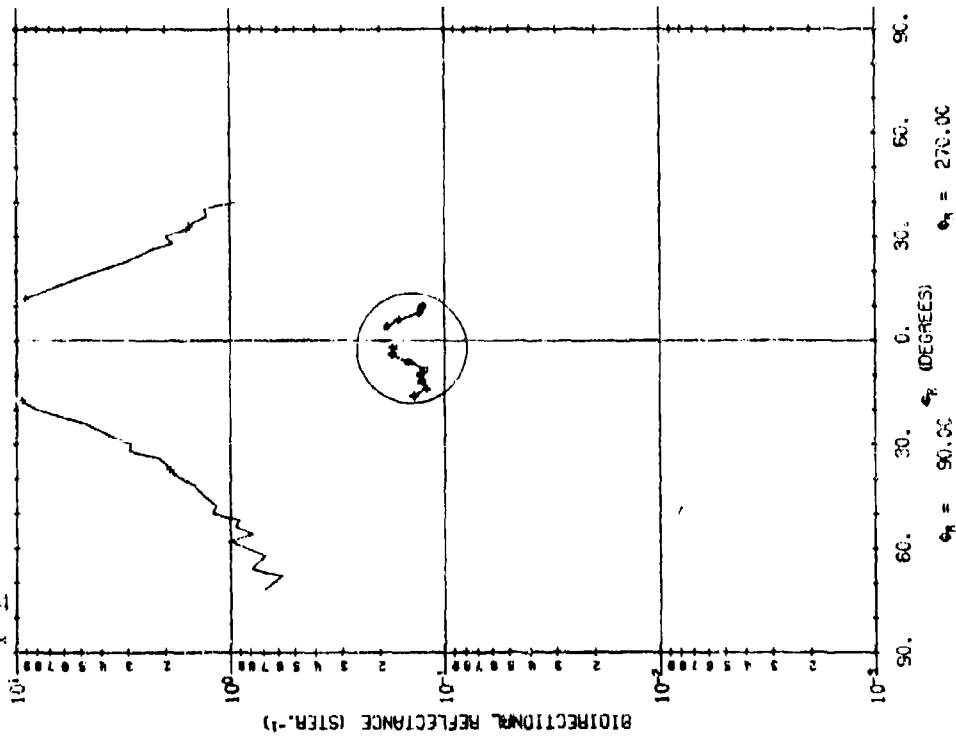


PAINT

AO1701 101

DARK OLIVE DRAB PAINT ON METAL

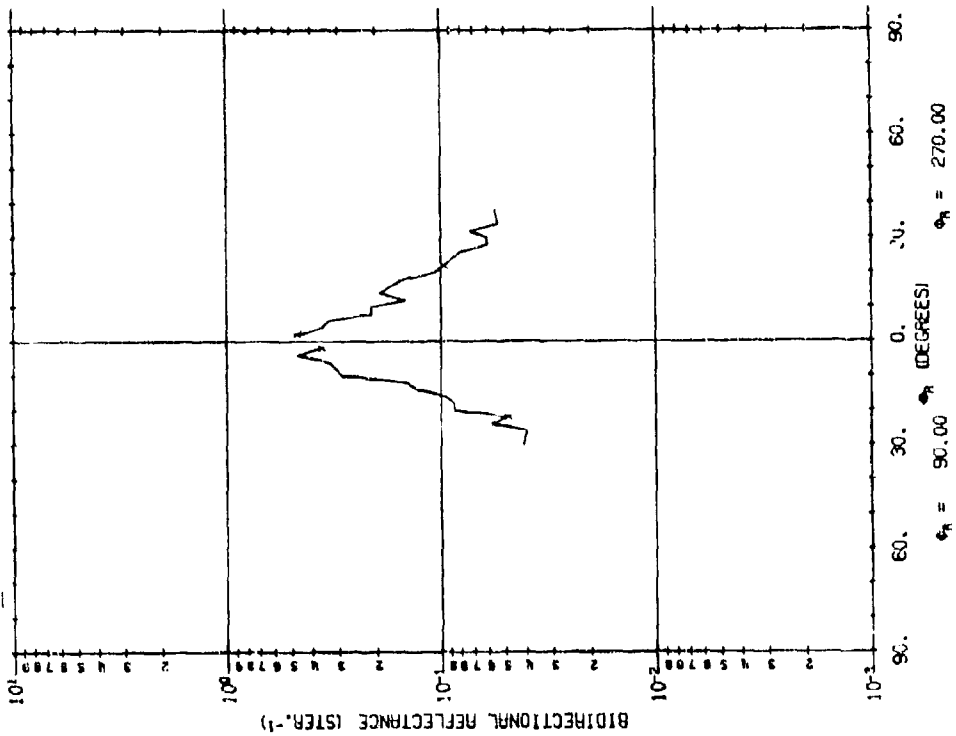
$\epsilon_1 = 0.0$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 30.6$



AO1701 101

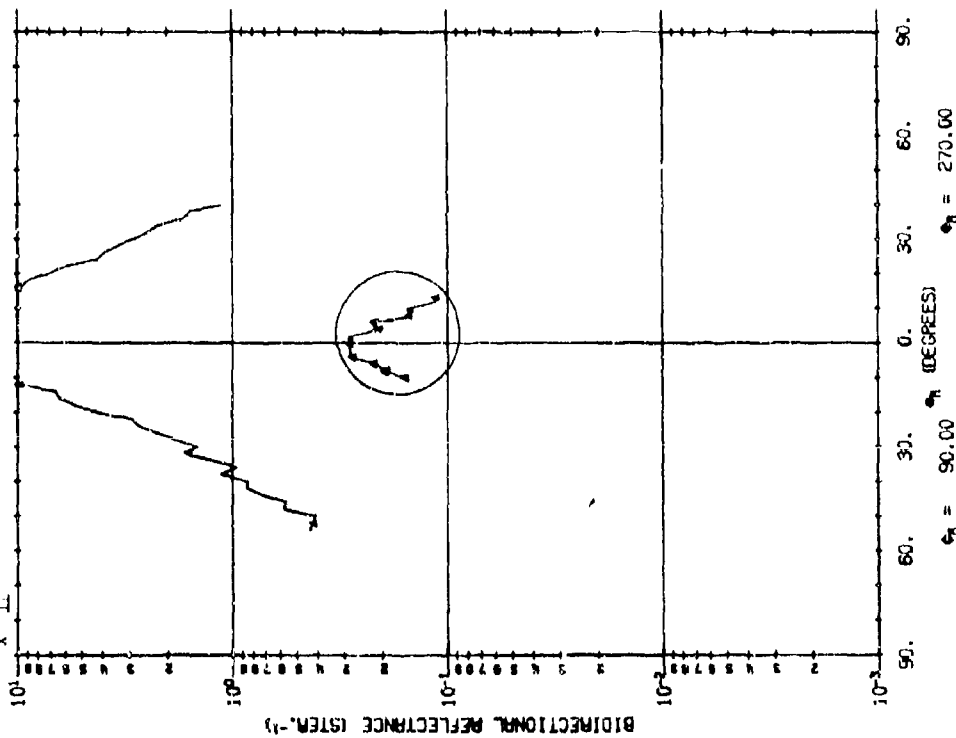
DARK OLIVE DRAB PAINT ON METAL

$\epsilon_1 = 0.0$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 10.4$



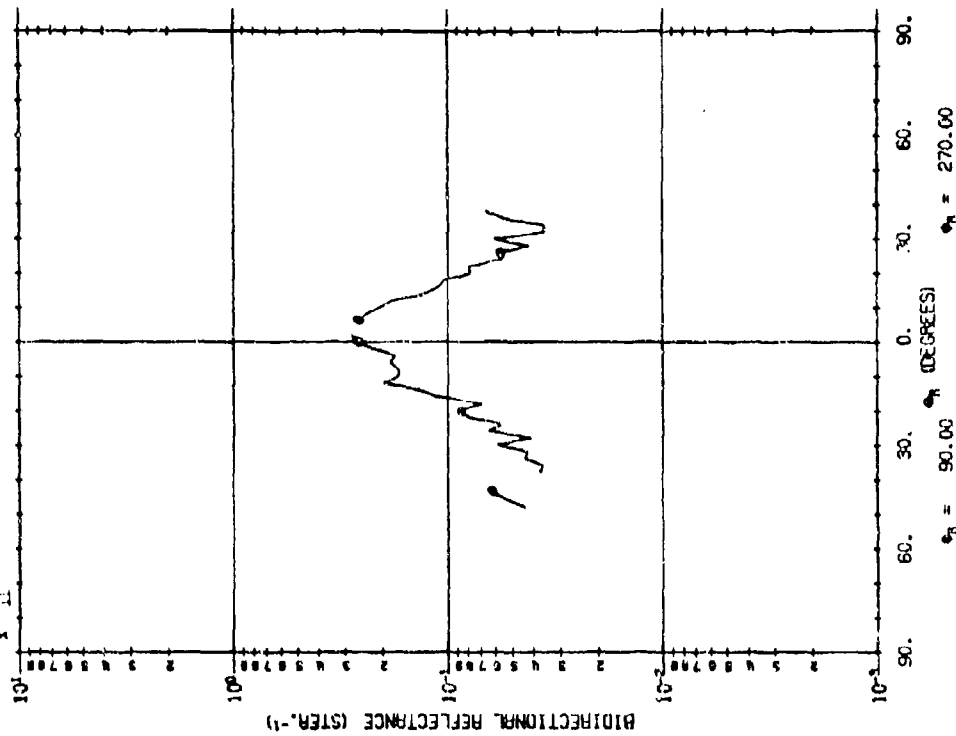
RC1701 101
 0 II 0.0
 + II 0.0
 - II 0.0
 X II 10.6

DARK OLIVE DRAB PAINT ON METAL



RC1701 101
 0 II 0.0
 + II 0.0
 - II 0.0
 X II 10.6

DARK OLIVE DRAB PAINT ON METAL

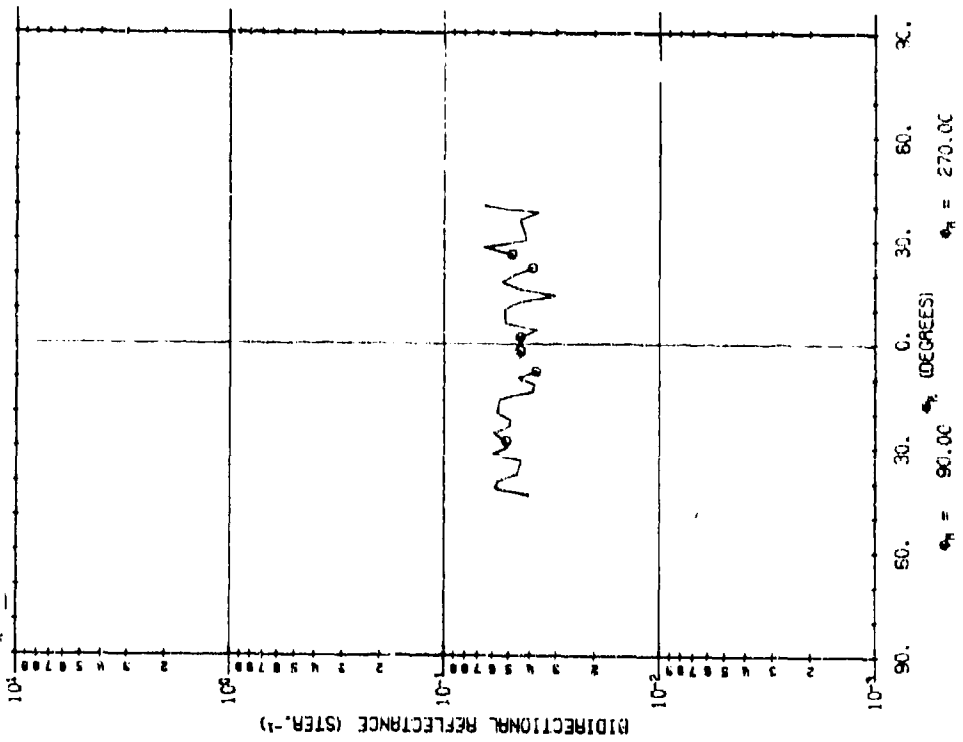


PAINT

RC1701 101

DARK OLIVE DRAB PAINT ON METAL

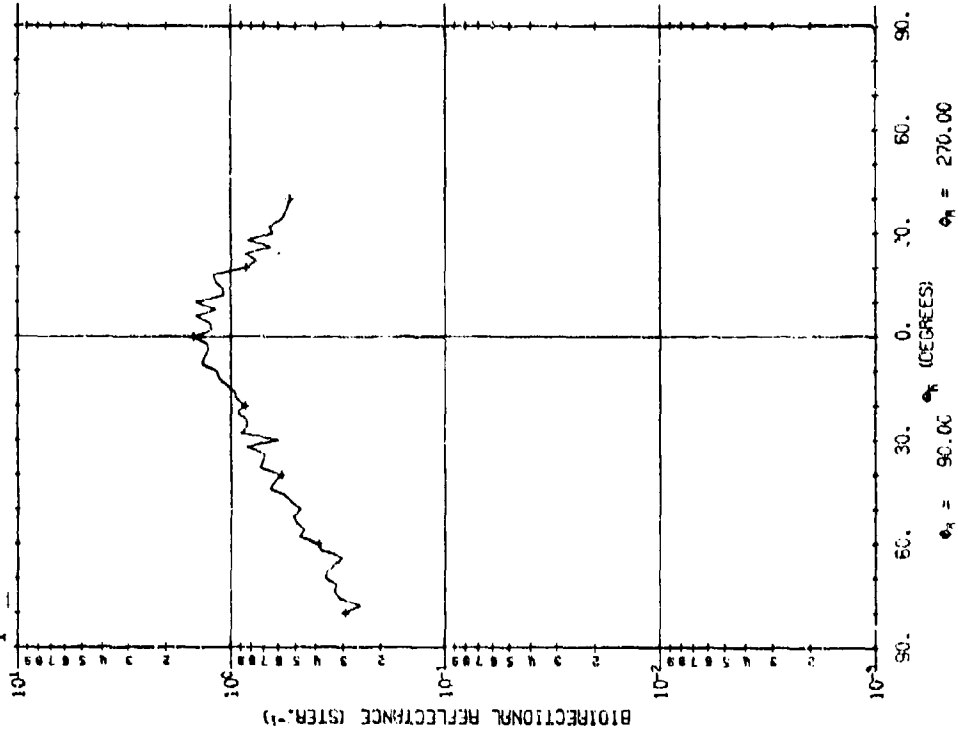
$\theta_1 = 59.0$
 $\theta_2 = 0.0$
 $\lambda = 10.6$



RC1701 101

DARK OLIVE DRAB PAINT ON METAL

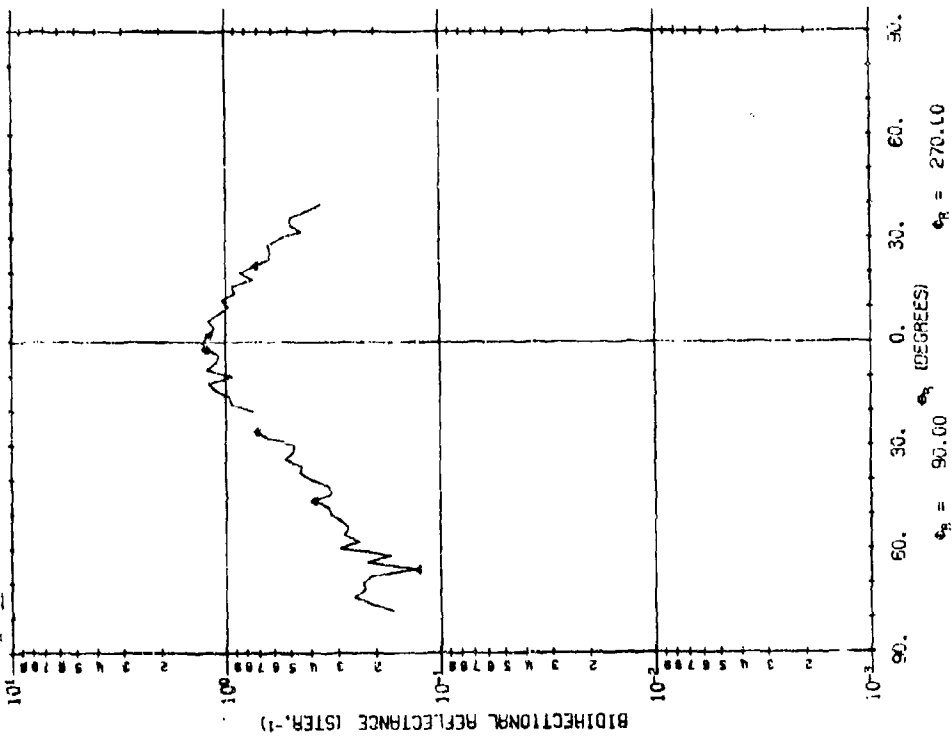
$\theta_1 = 30.0$
 $\theta_2 = 0.0$
 $\lambda = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

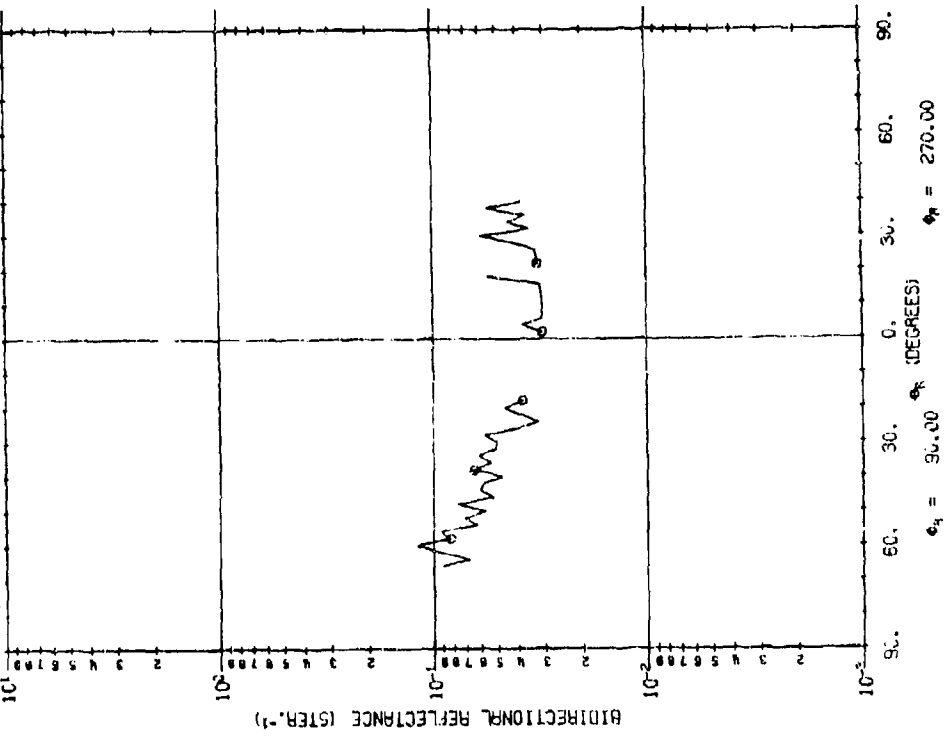
$\phi_1 = 30.0$
 $\phi_2 = 0.0$
 $\phi_3 = 10.6$



R01701 101

DARK OLIVE DRAB PAINT ON METAL

$\phi_1 = 60.0$
 $\phi_2 = 0.0$
 $\phi_3 = 10.6$



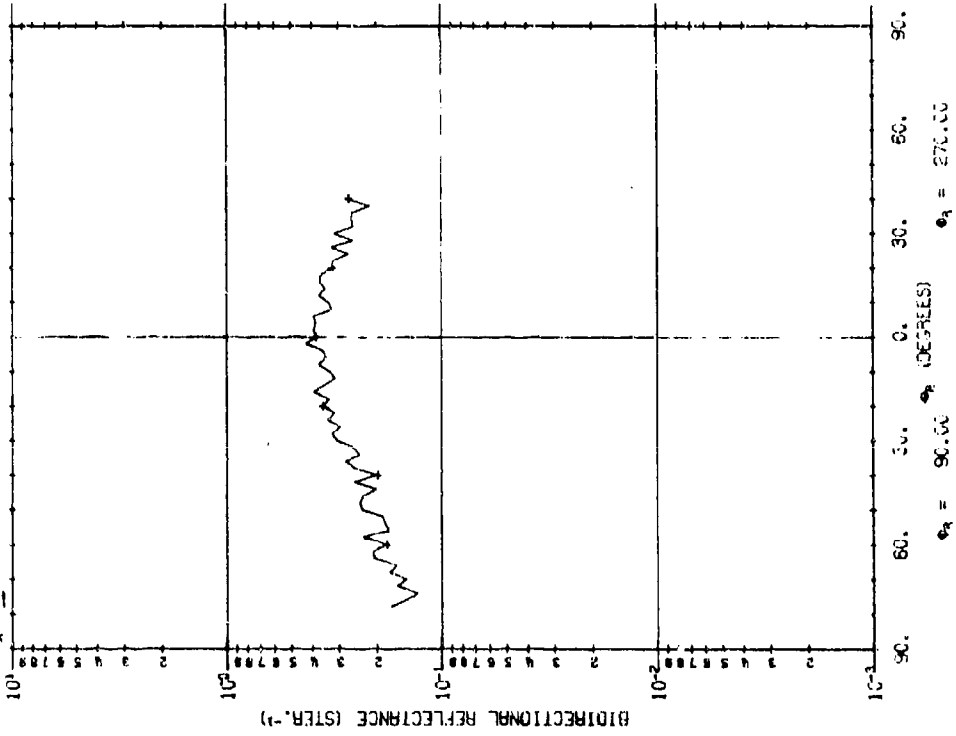
PAINT

RC1701 101

DARK OLIVE DRAB PAINT ON METAL

$\phi_1 = 60.0$
 $\phi_2 = 0.0$
 $\lambda = 10.6$

0
+
-
x

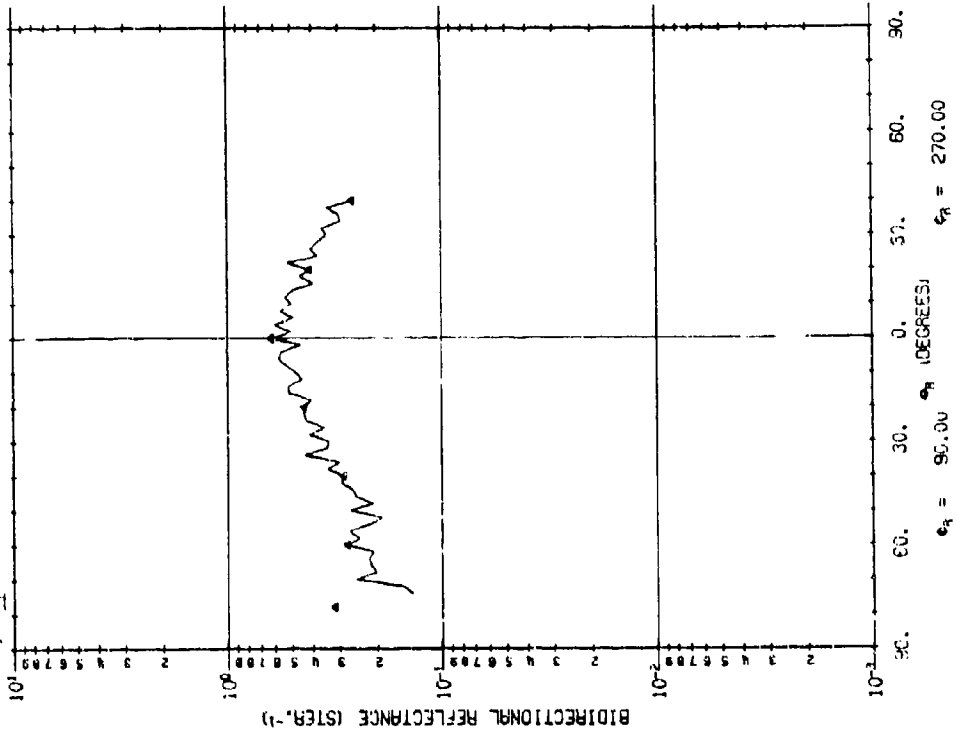


RC1701 101

DARK OLIVE DRAB PAINT ON METAL

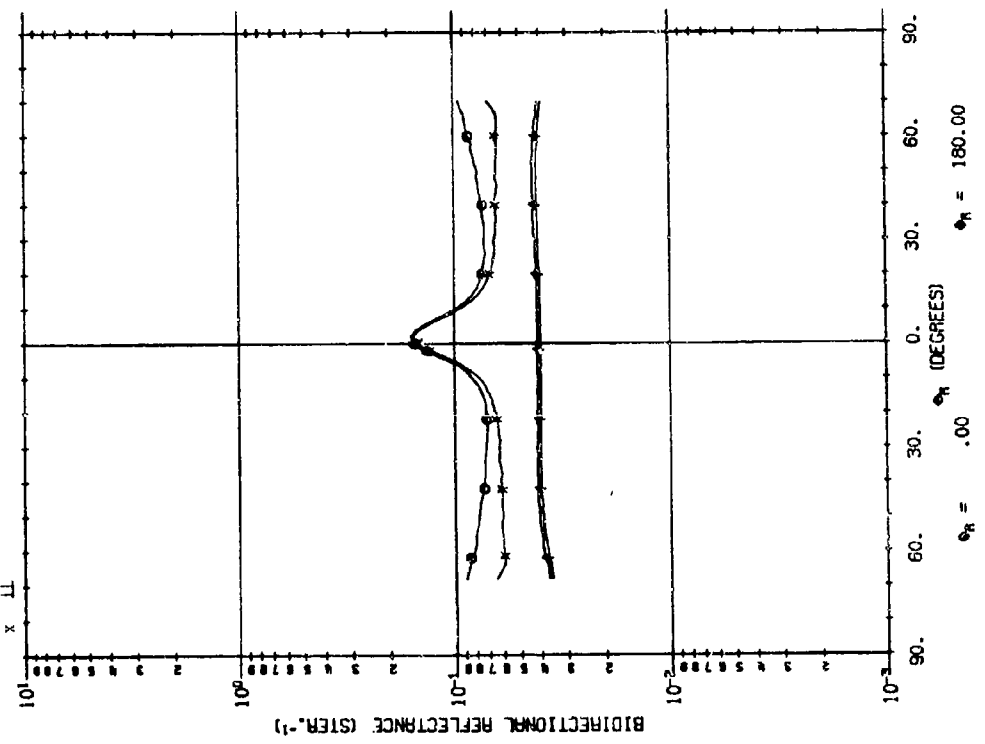
$\phi_1 = 60.0$
 $\phi_2 = 0.0$
 $\lambda = 10.6$

0
+
-
x



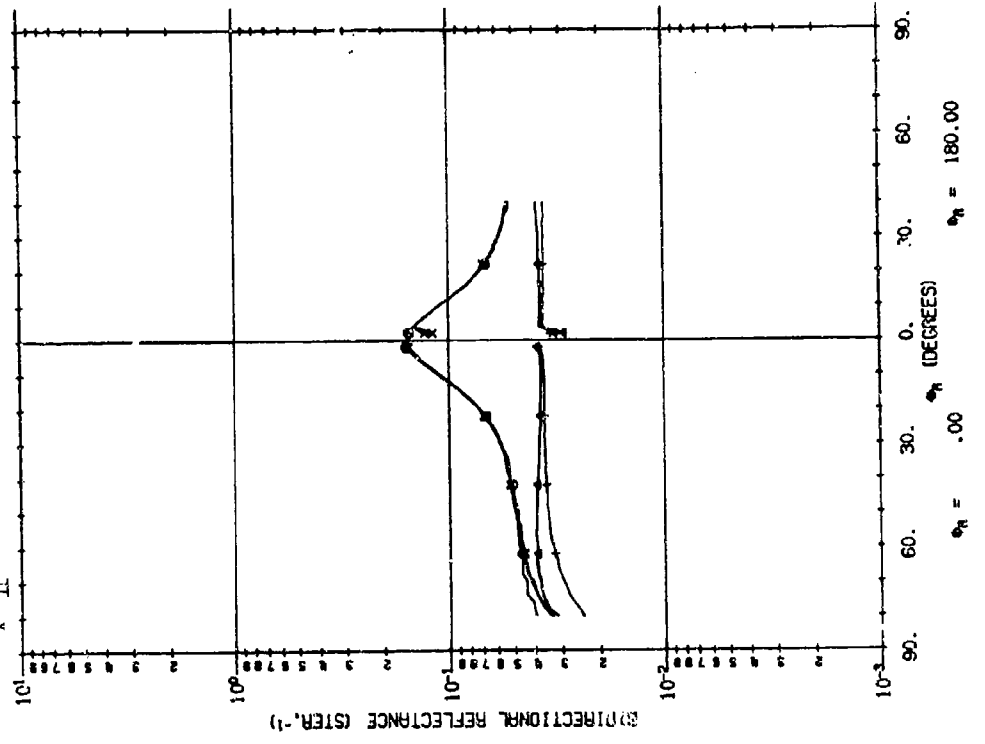
A01807 301
 0 ||| 23 = 2.0
 + ||| $\phi_1 = \phi_r$
 - ||| $\lambda = 0.63$
 x |||

Camouflage Paint on Metal



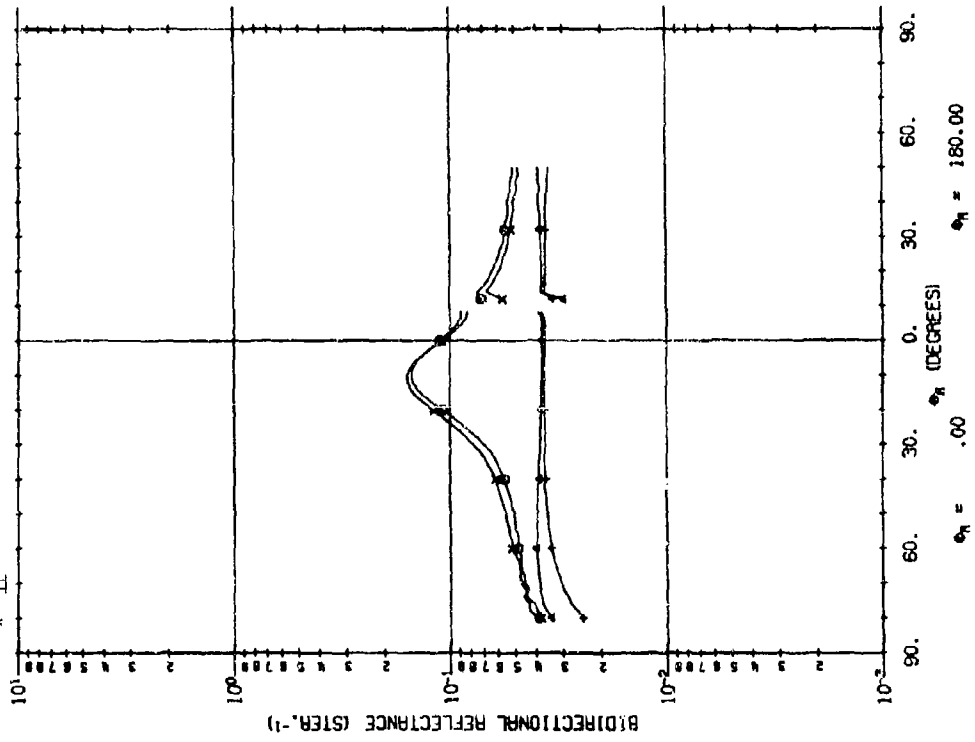
A01807 301
 0 ||| $\phi_1 = 0.0$
 + ||| $\phi_1 = 180.0$
 - ||| $\lambda = 0.63$
 x |||

Camouflage Paint on Metal



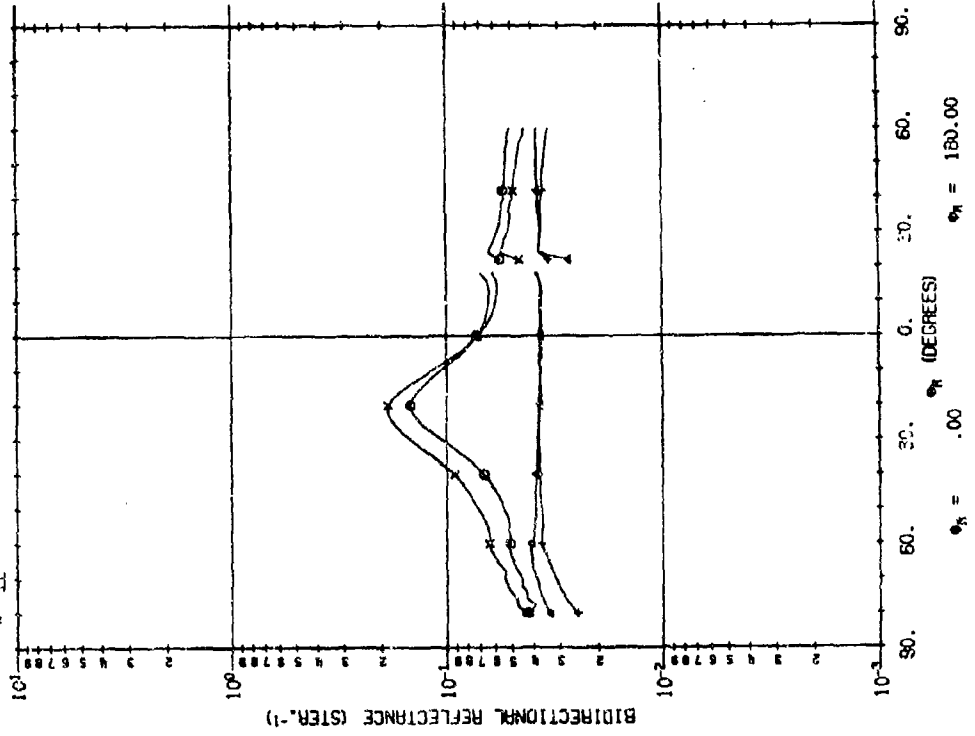
A01807 301
 $\epsilon_1 = 10.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

Camouflage Paint on Metal

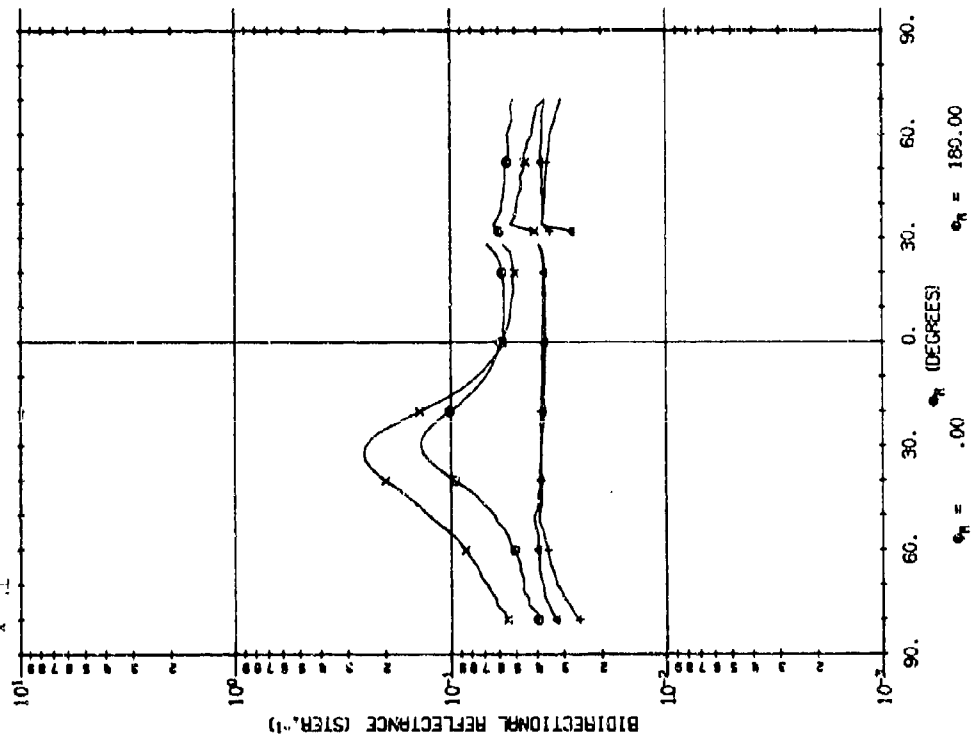


A01807 301
 $\epsilon_1 = 20.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

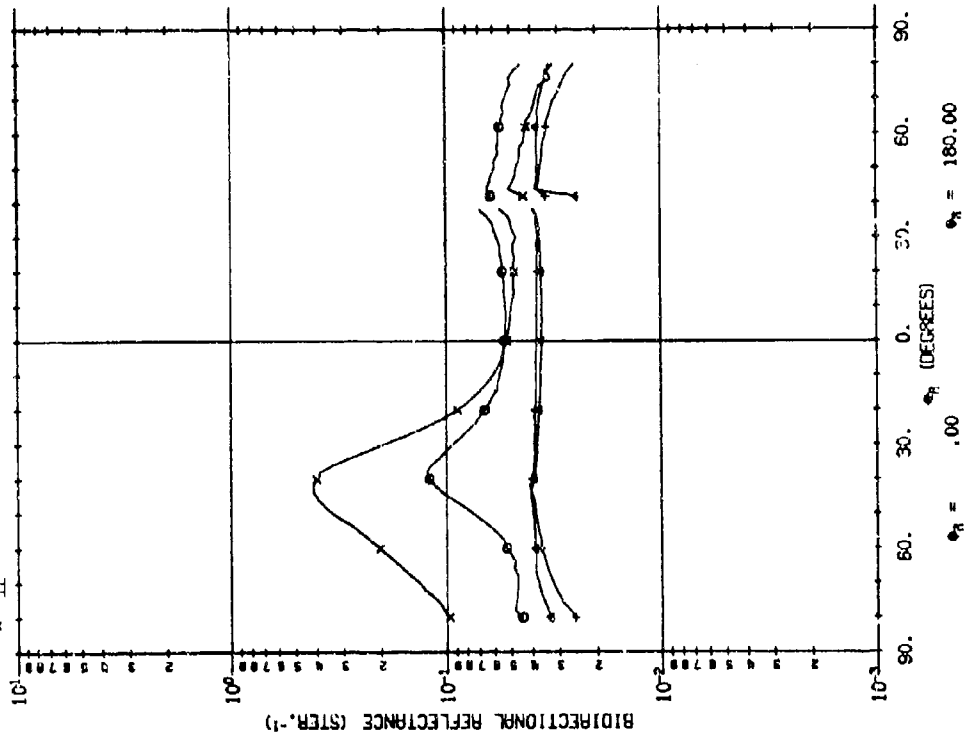
Camouflage Paint on Metal



A01807 301
 Camouflage Paint on Metal
 $\theta_i = 30.00$
 $\theta_r = 180.00$
 $\lambda = 0.63$



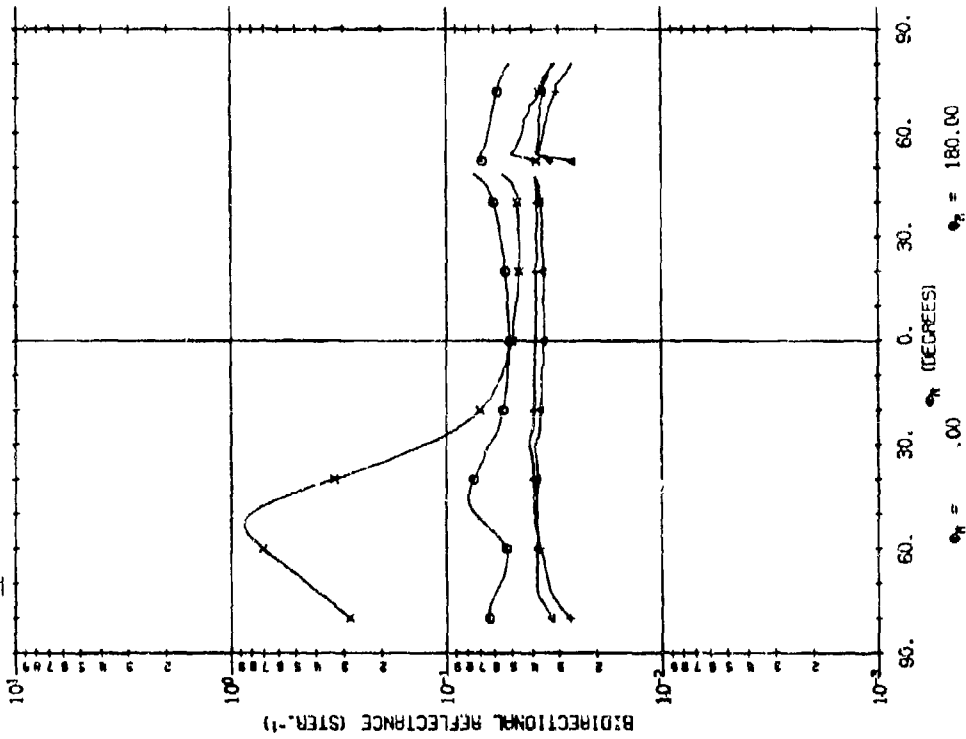
A01807 301
 Camouflage Paint on Metal
 $\theta_i = 40.00$
 $\theta_r = 180.00$
 $\lambda = 0.63$



A01807 301
 0 II II
 + II II
 - II II
 x II II

Camouflage Paint on Metal

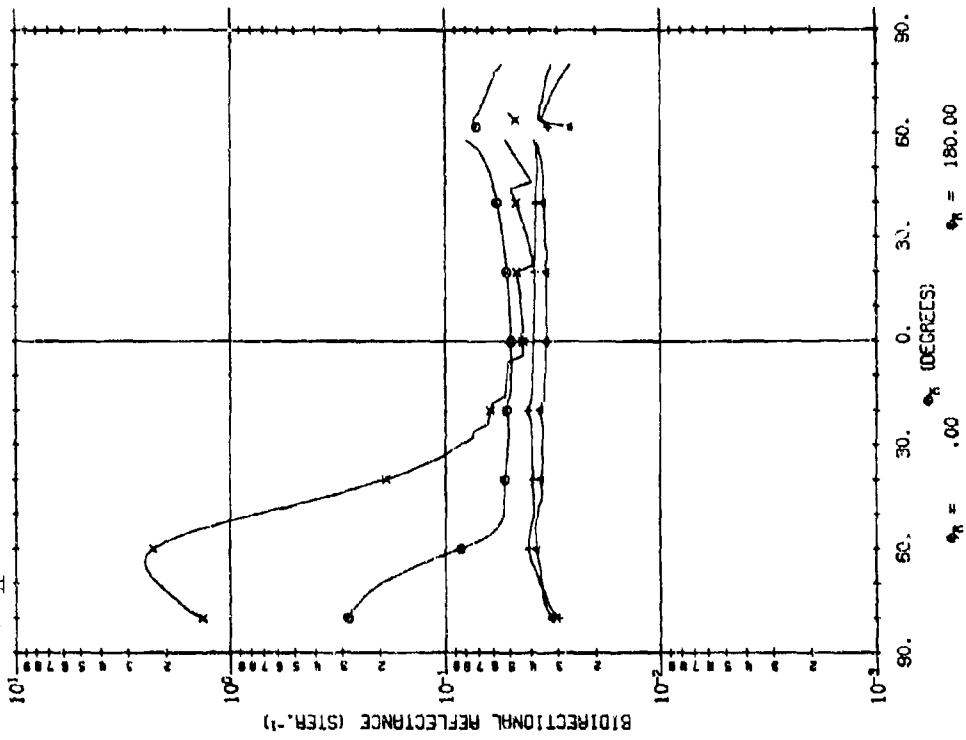
$\theta_1 = 50.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



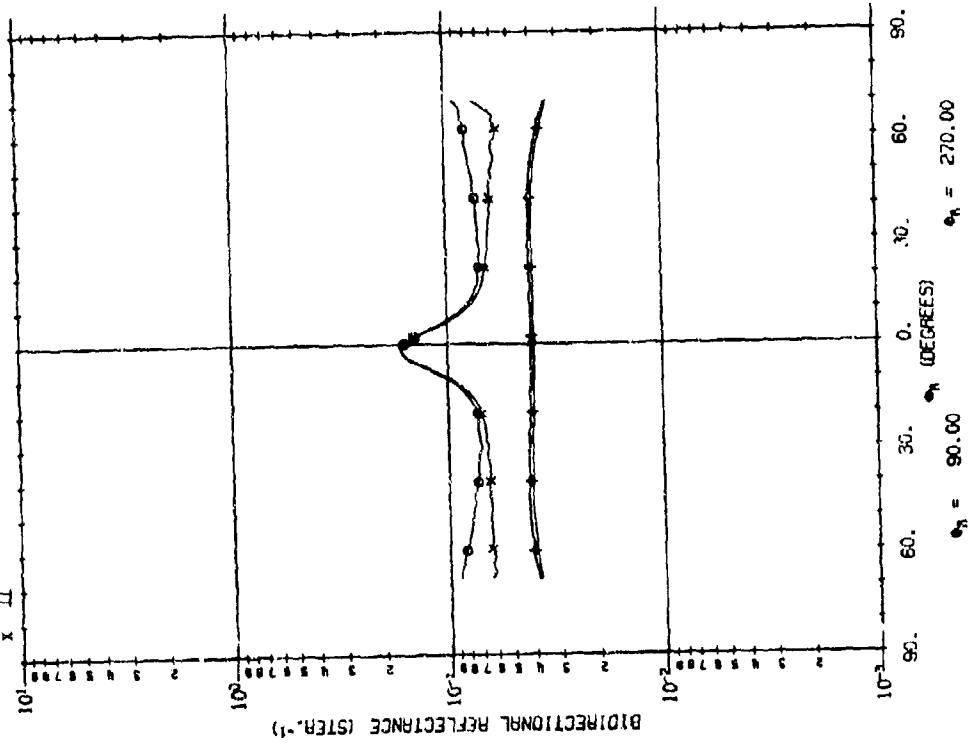
A01807 301
 0 II II
 + II II
 - II II
 x II II

Camouflage Paint on Metal

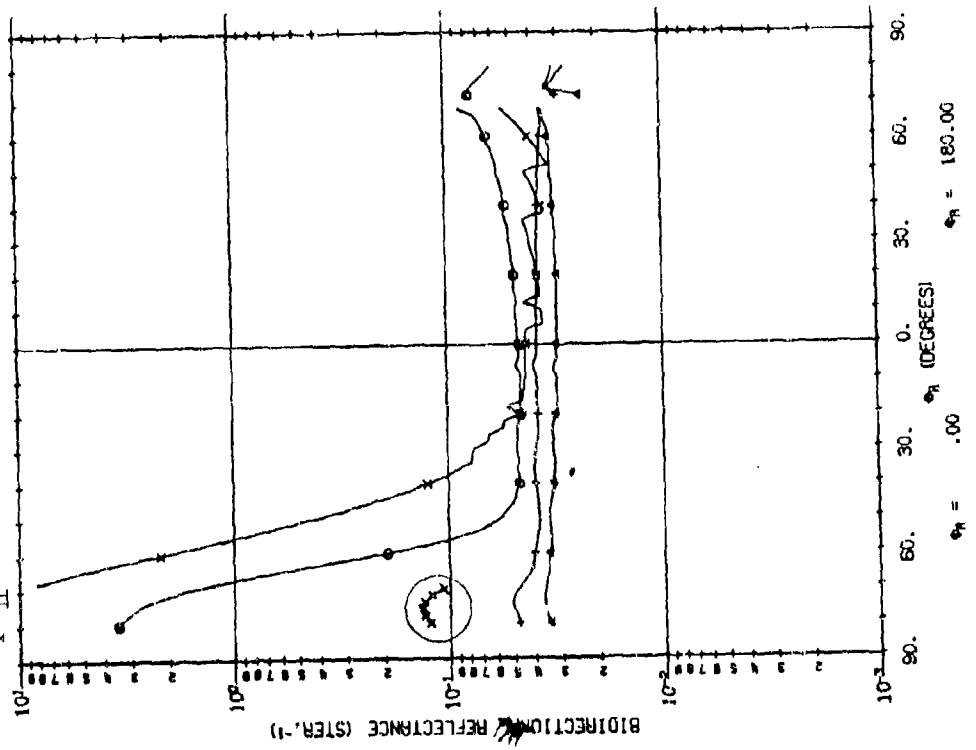
$\theta_1 = 50.00$
 $\theta_2 = 180.00$
 $\lambda = 0.63$



AO1807 301
 Camouflage Paint on Metal
 $z_1 = 2.0$
 $\phi_1 = 0.63$
 $\lambda = 0.63$



AO1807 301
 Camouflage Paint on Metal
 $z_1 = 70.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

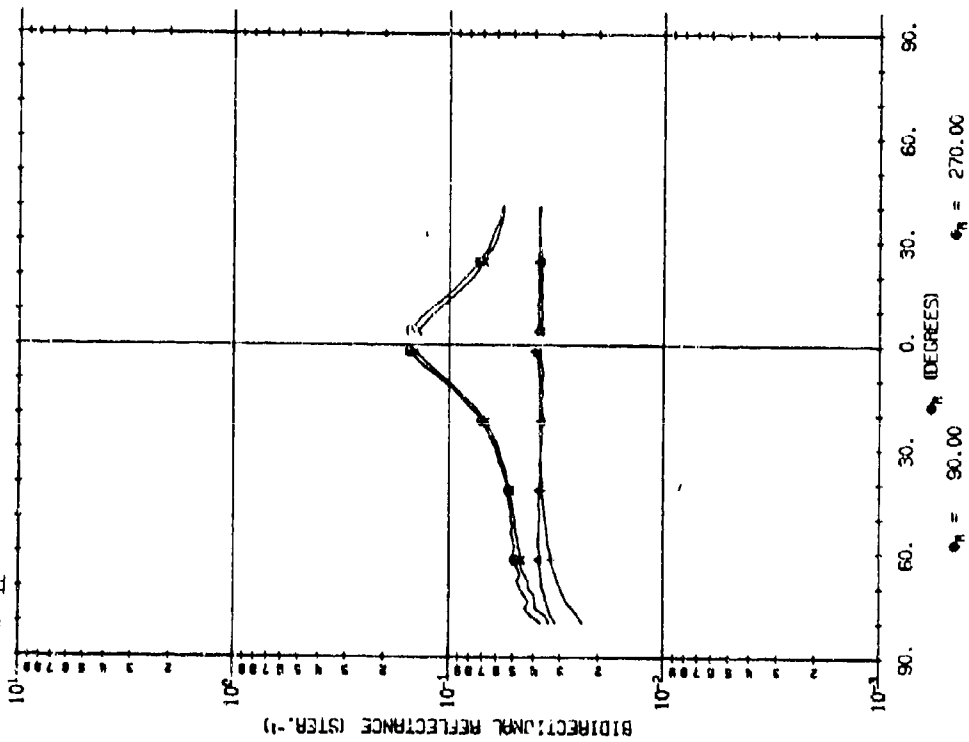


PAINT

R01807 301
 Camouflage Paint on Metal

$\epsilon_1 = 0.0$
 $\phi_1 = 270.00$
 $\lambda = 0.63$

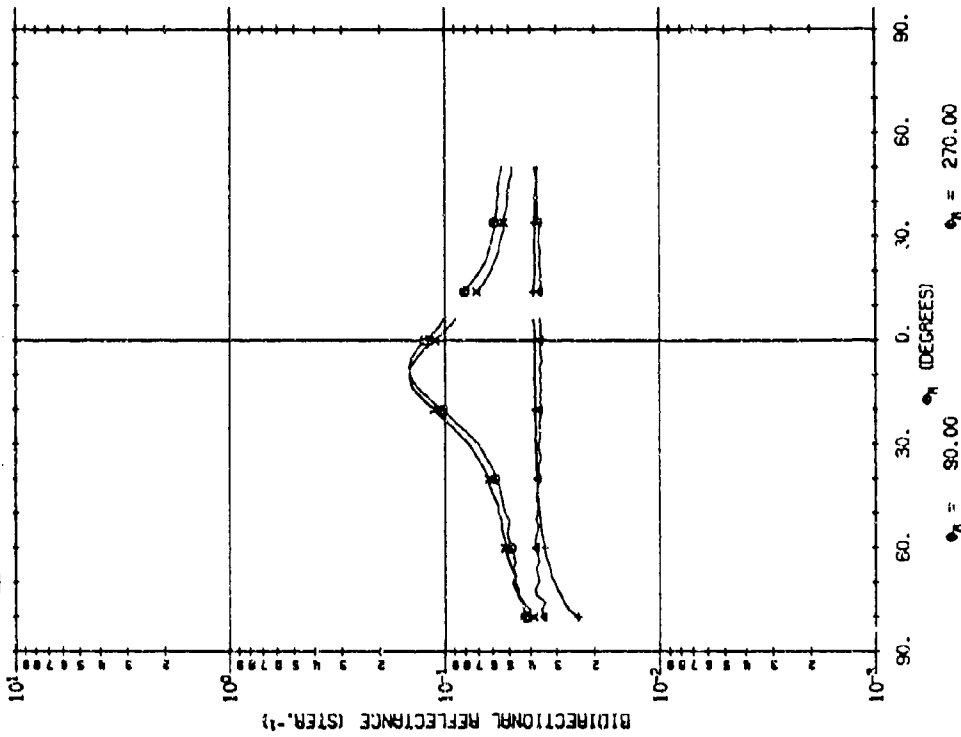
o II
 + II
 - II
 x II



R01807 301
 Camouflage Paint on Metal

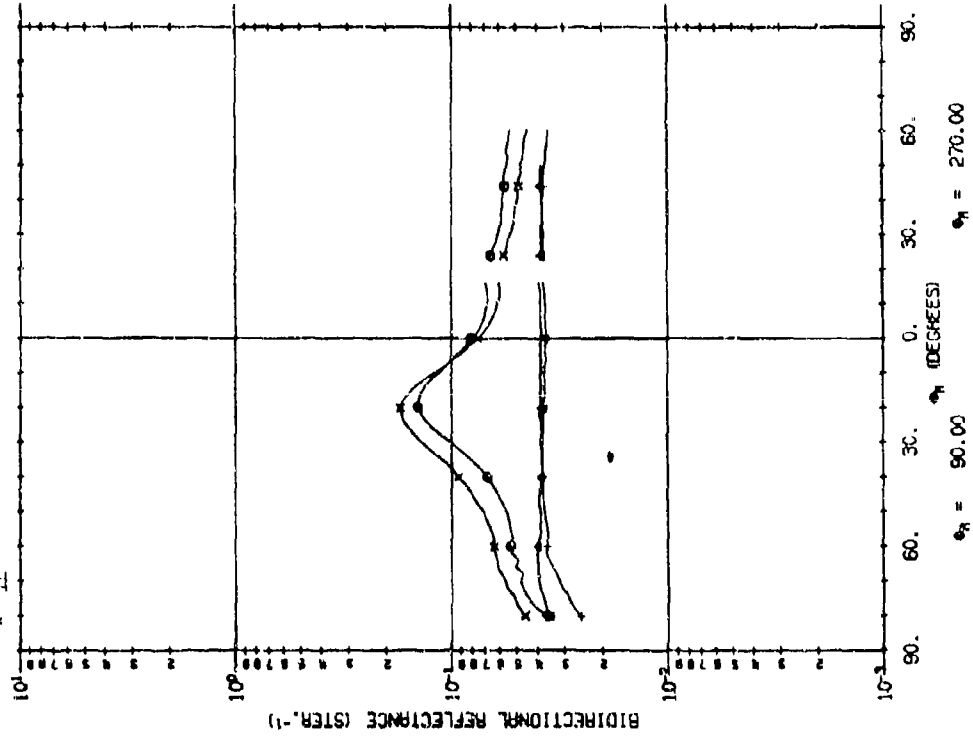
$\epsilon_1 = 10.00$
 $\phi_1 = 270.00$
 $\lambda = 0.63$

o II
 + II
 - II
 x II



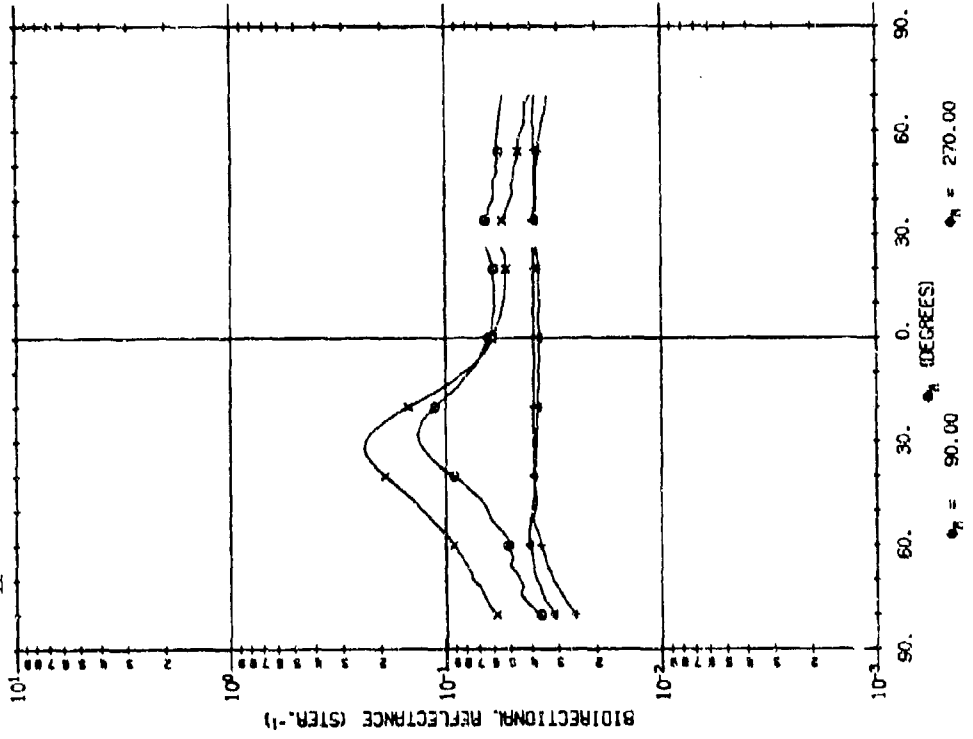
R01807 301
 $\epsilon_1 = 20.00$
 $\phi_1 = 270.00$
 $\lambda = 0.63$

CamoFlage Paint on Metal



R01807 301
 $\epsilon_1 = 30.00$
 $\phi_1 = 270.00$
 $\lambda = 0.63$

CamoFlage Paint on Metal

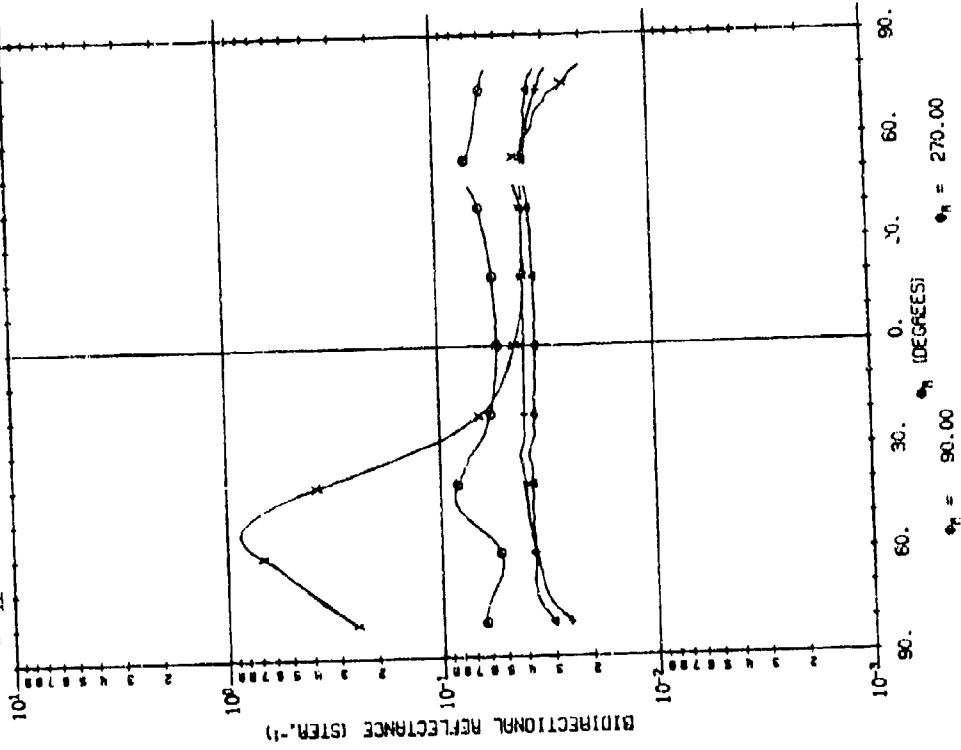


PAINT

R01807 301 Camouflage Paint on Metal

$\epsilon_1 = 50.00$
 $\epsilon_2 = 1.0$
 $\epsilon_3 = 270.00$
 $\lambda = 0.63$

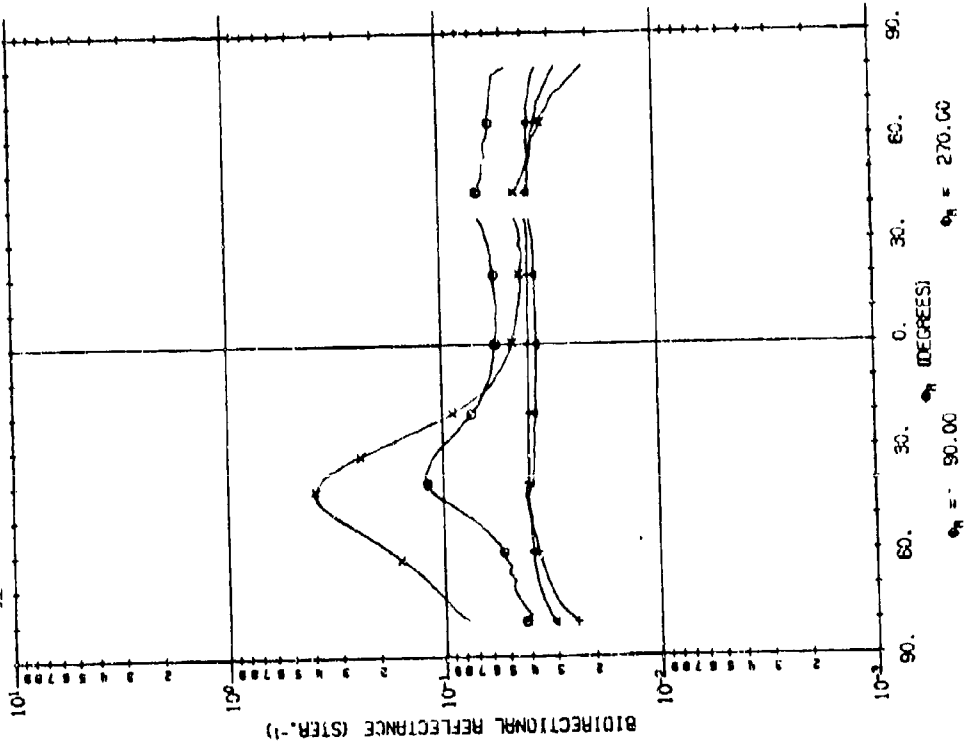
0
+
-
x



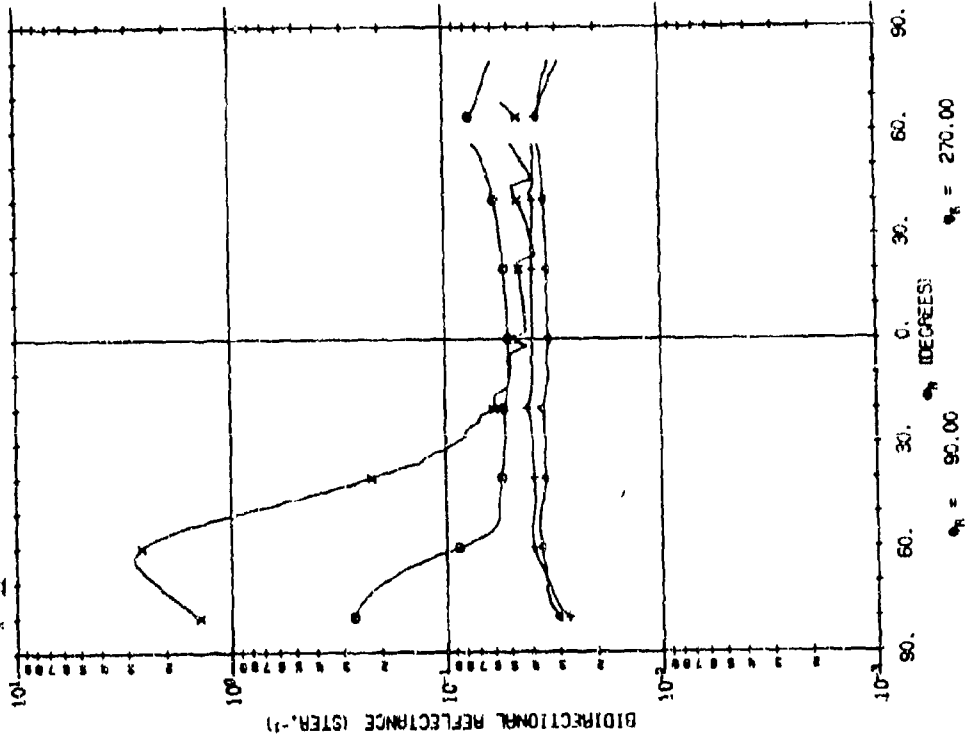
R01807 301 Camouflage Paint on Metal

$\epsilon_1 = 40.00$
 $\epsilon_2 = 1.0$
 $\epsilon_3 = 270.00$
 $\lambda = 0.63$

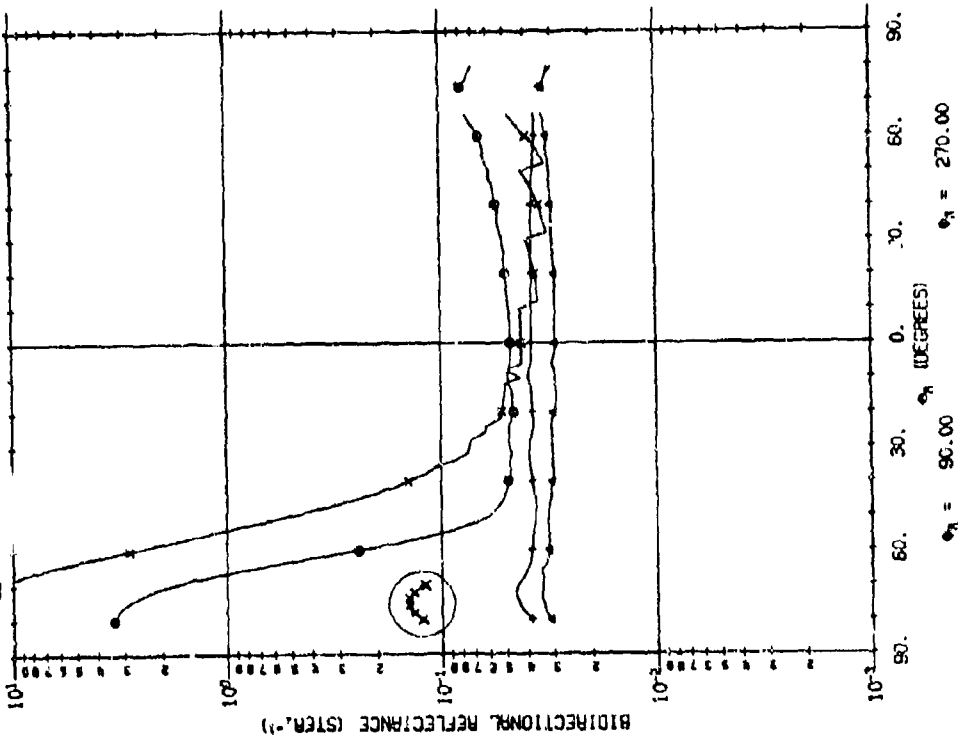
0
+
-
x



R01807 301
 Camouflage Paint on Metal
 $\theta_1 = 60.00$
 $\theta_2 = 270.00$
 $\lambda = 0.63$



R01807 301
 Camouflage Paint on Metal
 $\theta_1 = 70.00$
 $\theta_2 = 270.00$
 $\lambda = 0.63$

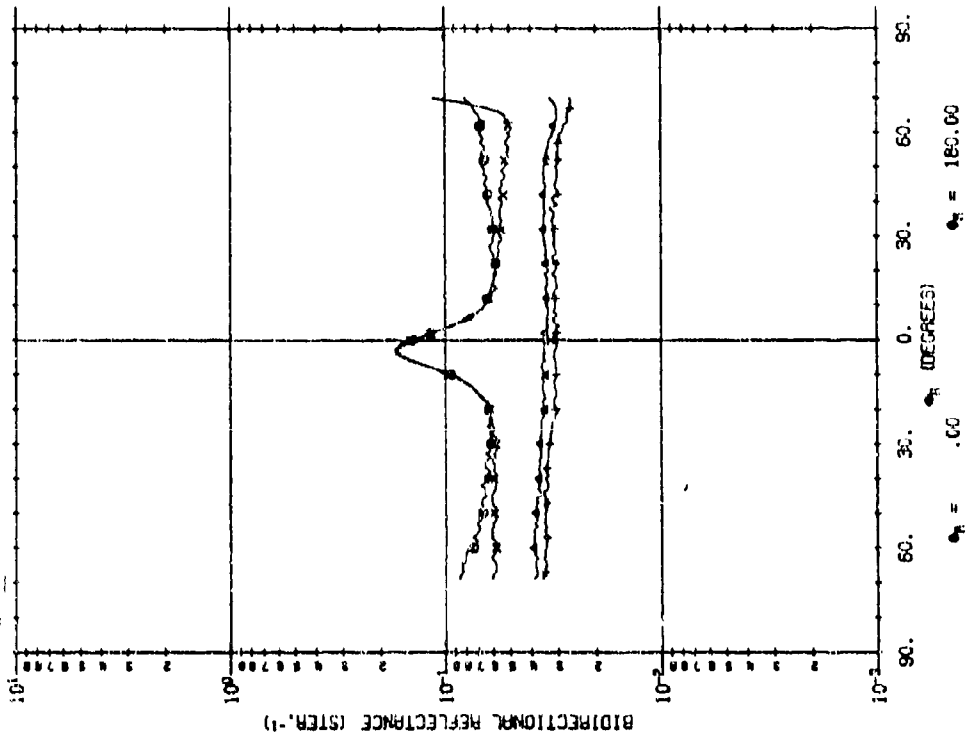


PAINT

R01807 101

Camouflage Paint on Metal

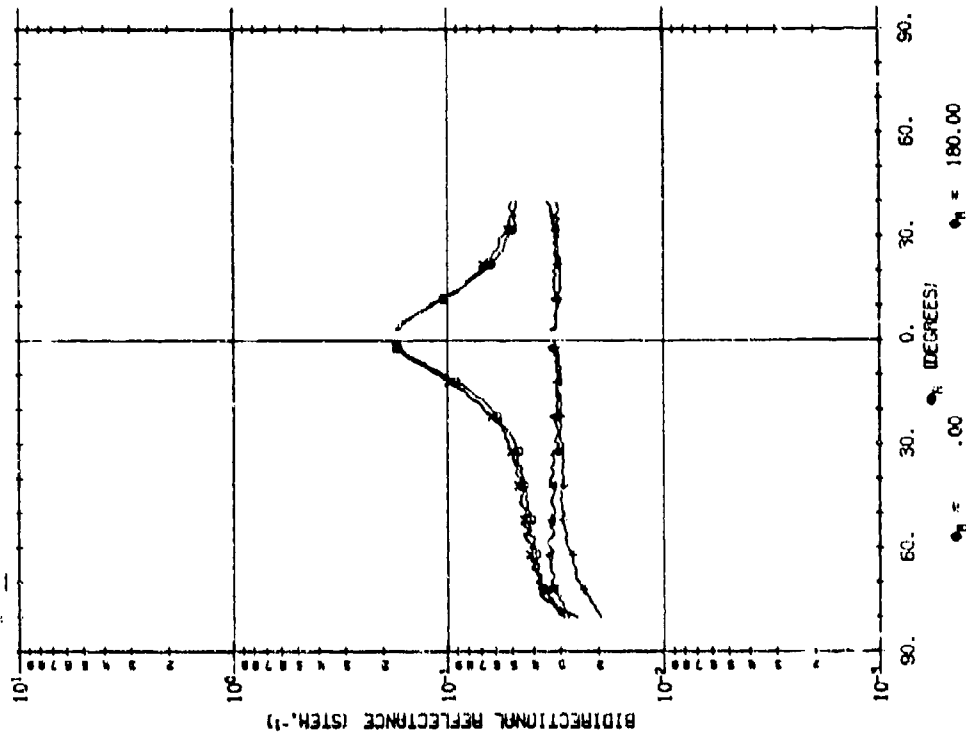
0 2.0
+ 1.0
x 1.0
- 1.0
X 1.06



R01807 101

Camouflage Paint on Metal

0 5.0
+ 1.0
x 1.0
- 1.0
X 1.06

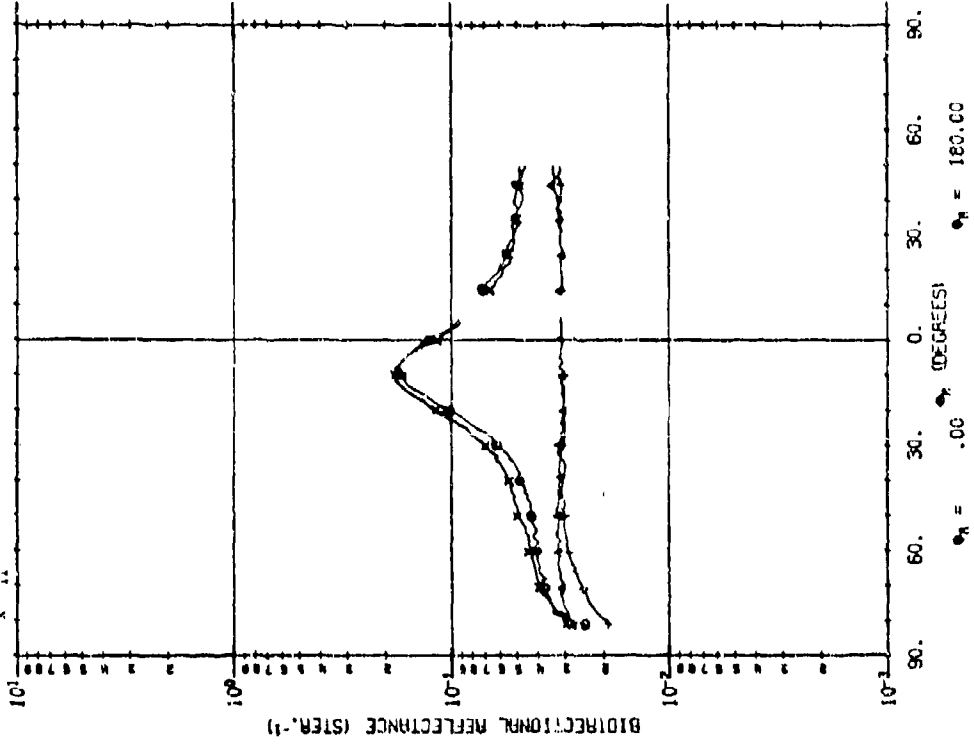


R01807 101

Camouflage Paint on Metal

$\theta_1 = 10.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$

0 | |
+ | |
x | |
o | |
x | |

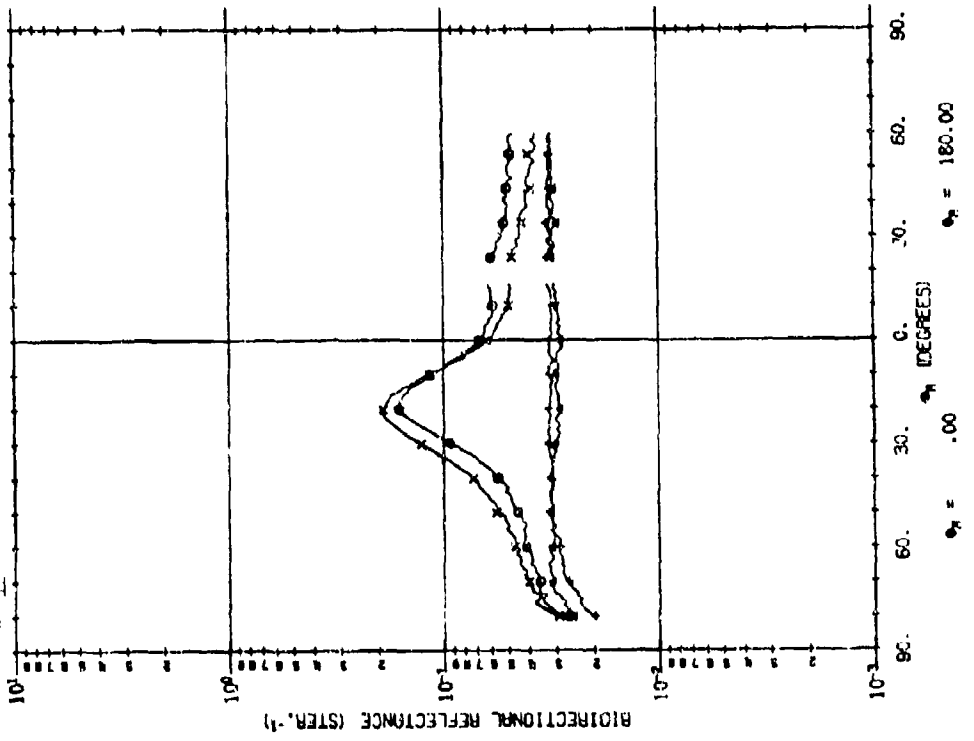


R01807 101

Camouflage Paint on Metal

$\theta_1 = 20.00$
 $\theta_2 = 180.00$
 $\lambda = 1.06$

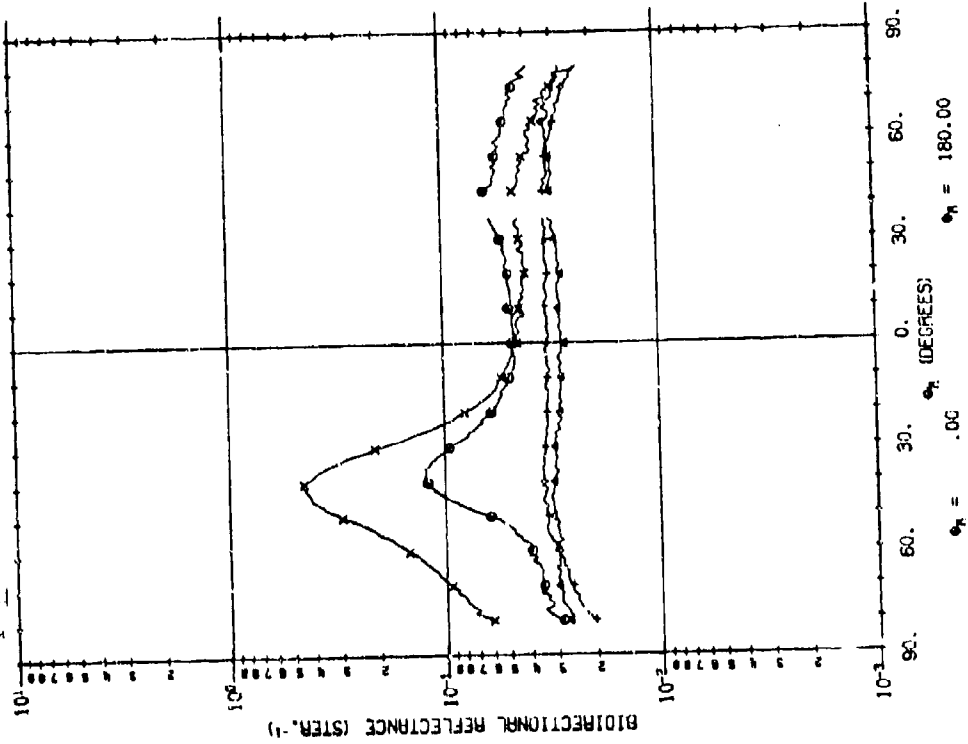
0 | |
+ | |
x | |
o | |
x | |



PAINT

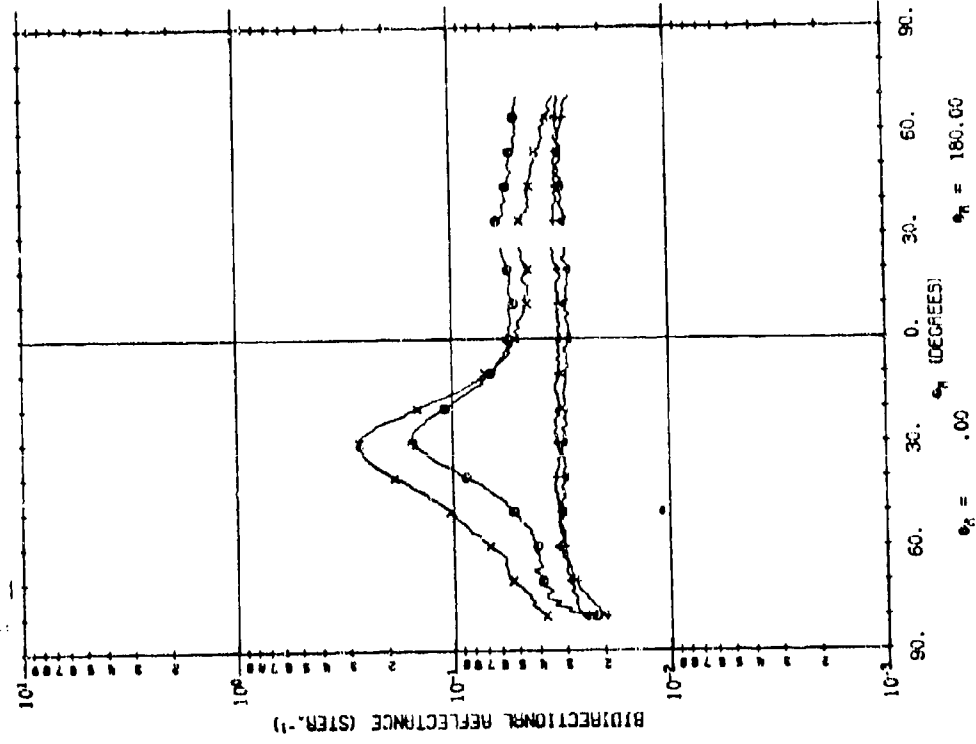
AC1807 101 Camouflage Paint on Metal

$\lambda_1 = 45.00$
 $\lambda_2 = 180.00$
 $\lambda_3 = 1.06$



AC1807 101 Camouflage Paint on Metal

$\lambda_1 = 30.00$
 $\lambda_2 = 180.00$
 $\lambda_3 = 1.06$

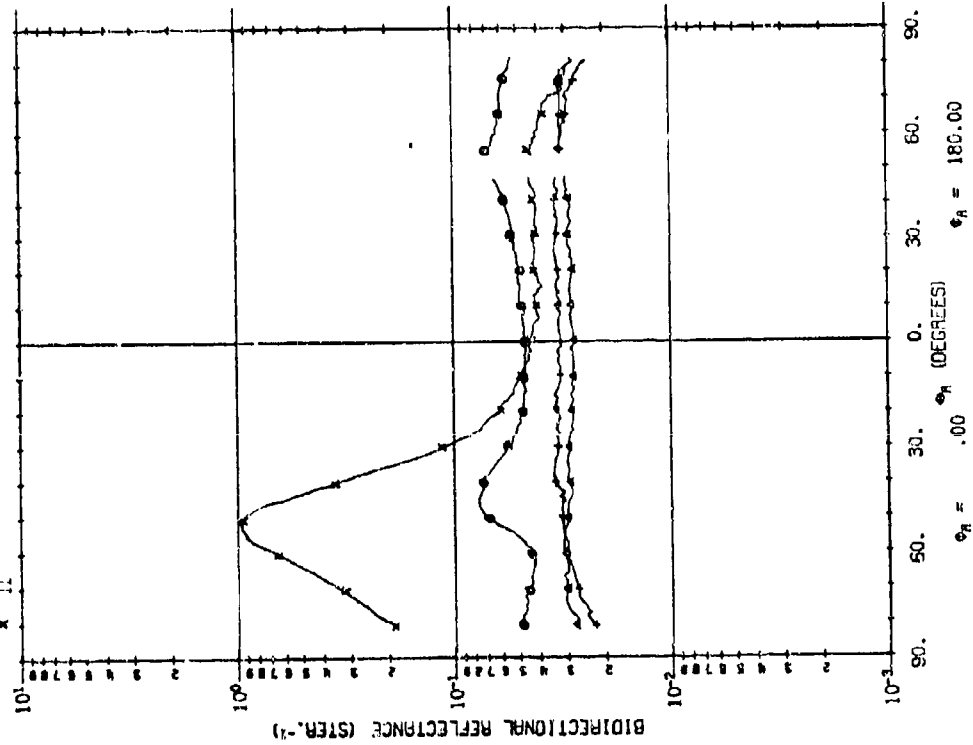


R01807 101

Camouflage Paint on Metal

$\epsilon_1 = 50.0$
 $\epsilon_2 = 180.0$
 $\lambda = 0.63$

o | | | | |
+ | | | | |
Δ | | | | |
x | | | | |

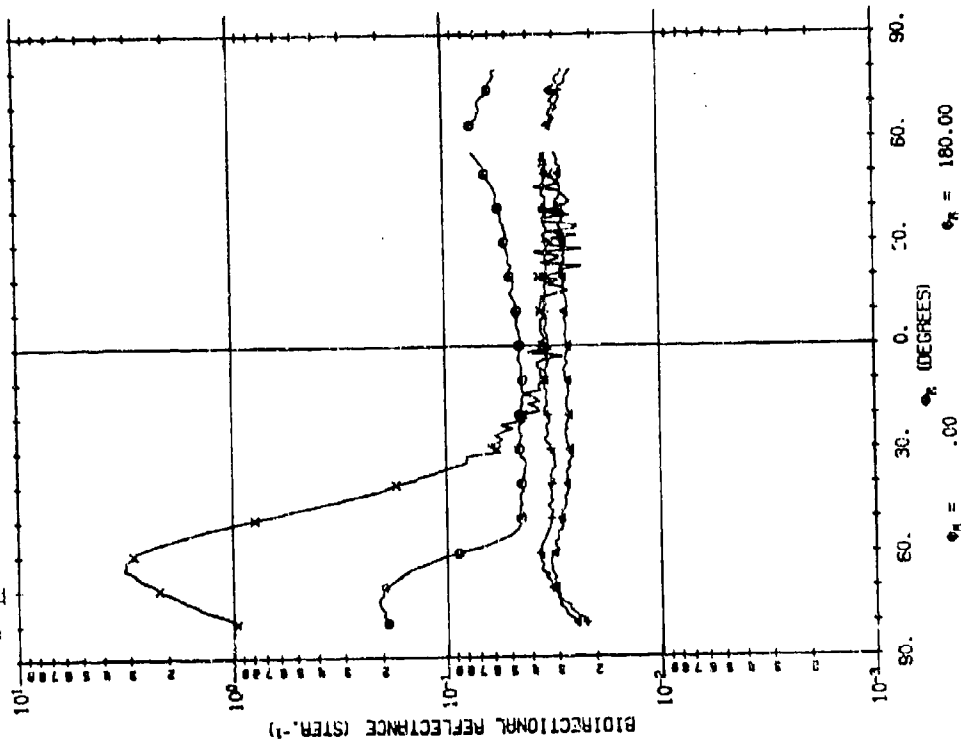


R01807 101

Camouflage Paint on Metal

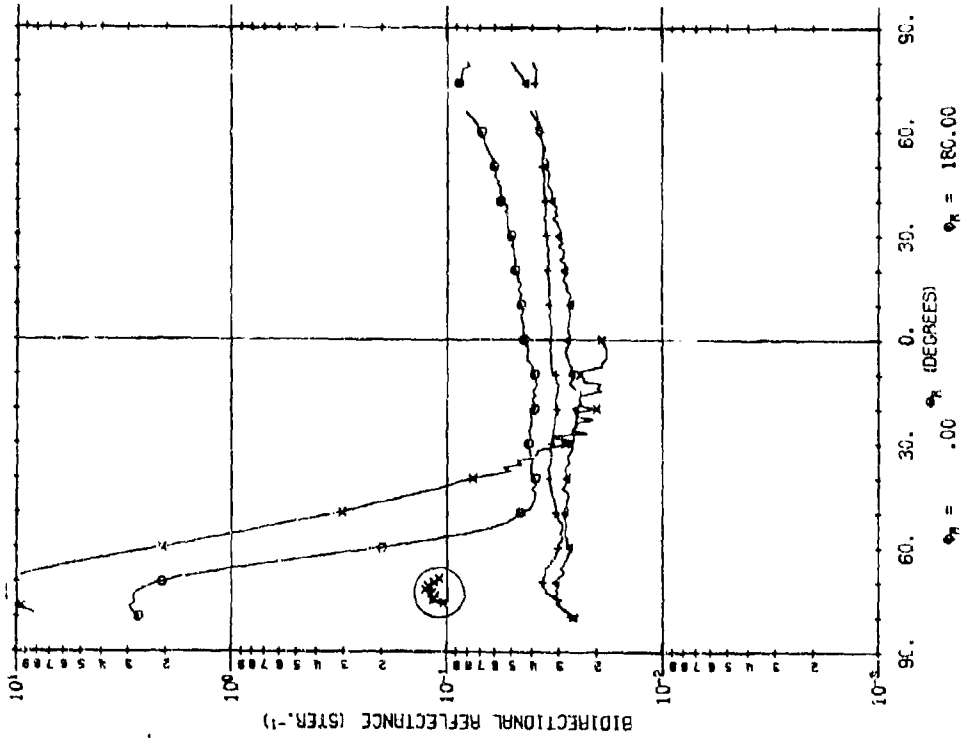
$\epsilon_1 = 60.00$
 $\epsilon_2 = 180.00$
 $\lambda = 1.06$

o | | | | |
+ | | | | |
Δ | | | | |
x | | | | |

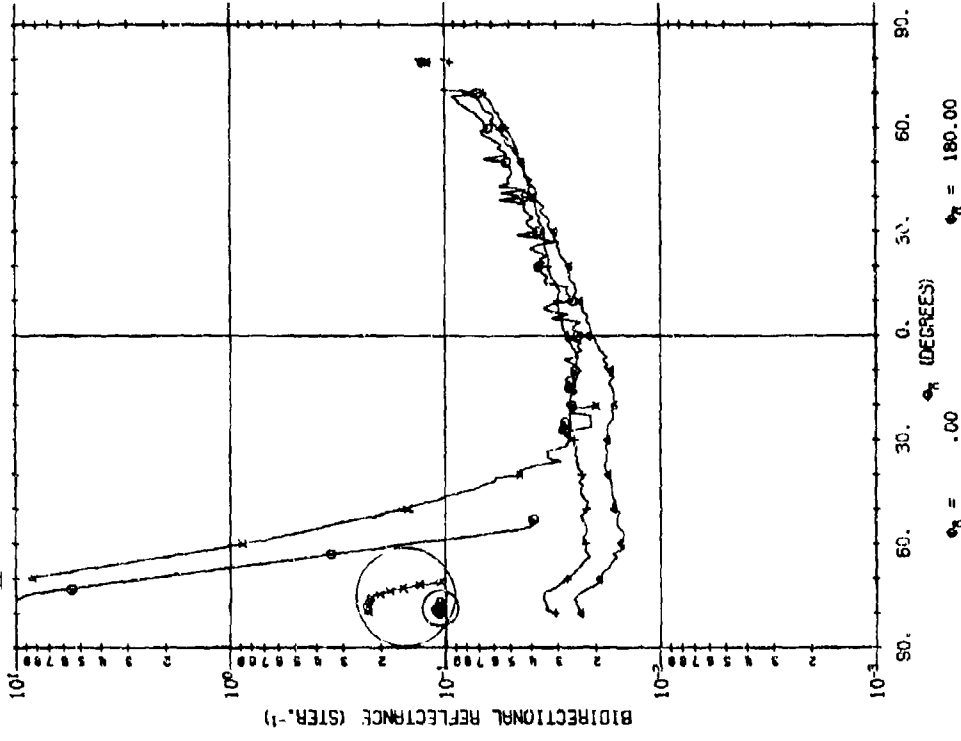


PAINT

AO1807 101
 CAMOUFLAGE PAINT ON METAL
 $\lambda_1 = 70.0$
 $\lambda_2 = 180.0$
 $\lambda_3 = 1.06$



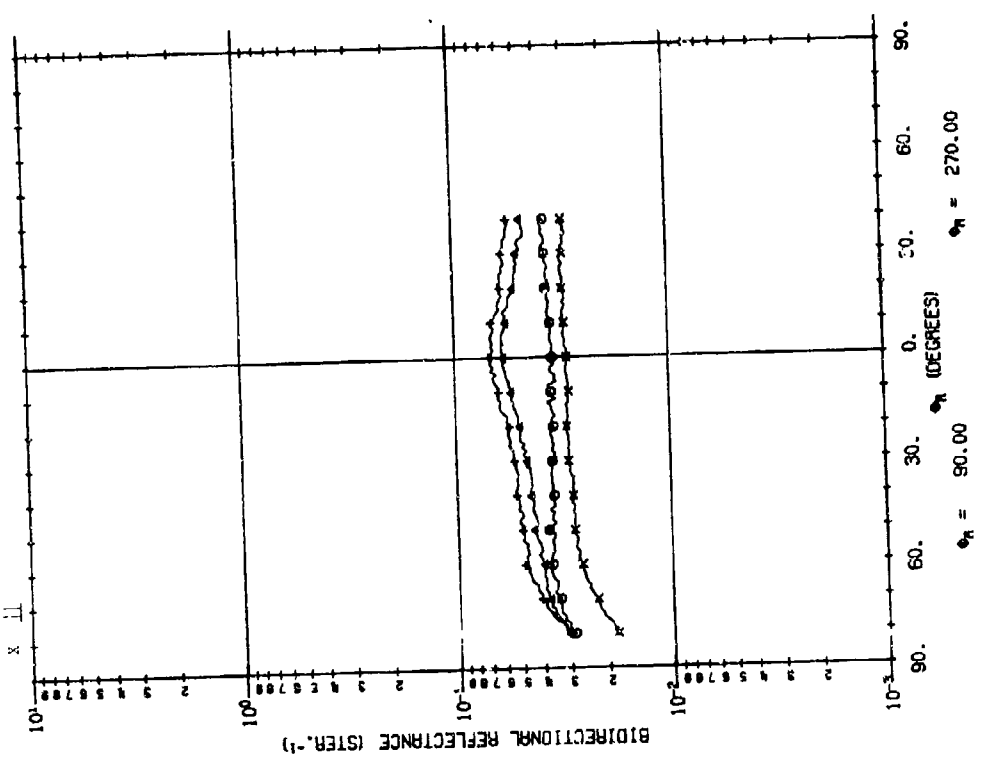
AO1807 101
 CAMOUFLAGE PAINT ON METAL
 $\lambda_1 = 75.00$
 $\lambda_2 = 180.00$
 $\lambda_3 = 1.06$



A01807 101 Camouflage Paint on Metal

$\lambda = 20.00$
 $\lambda = 180.00$
 $\lambda = 1.06$

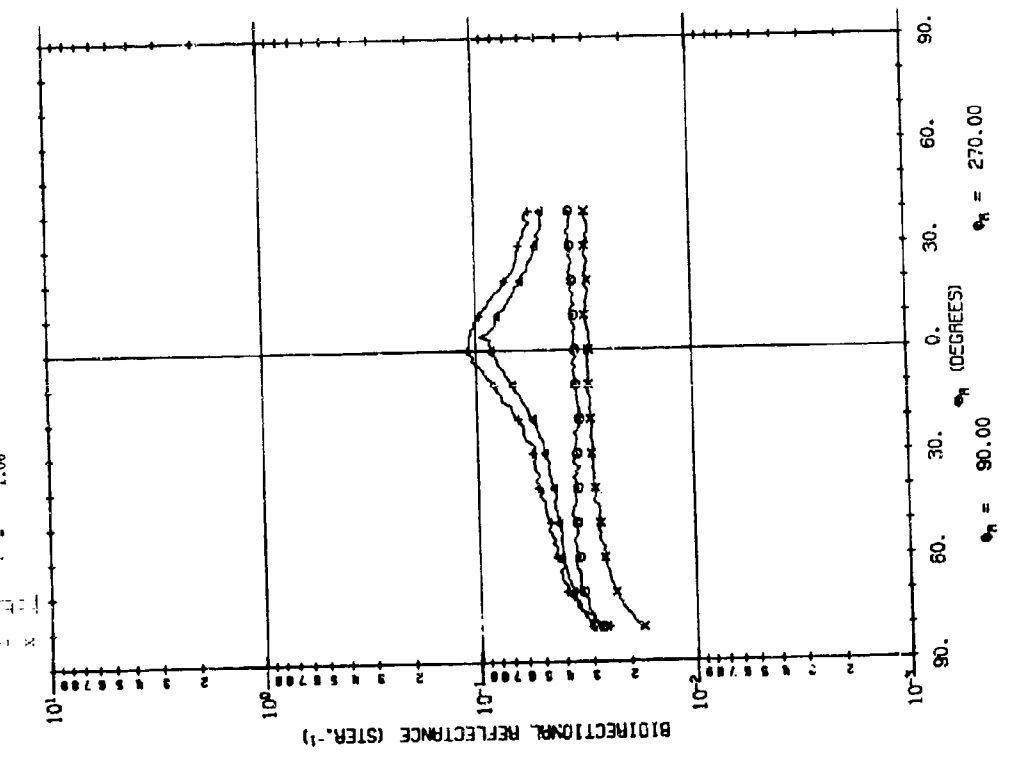
0
 +
 -
 x



A01807 101 Camouflage Paint on Metal

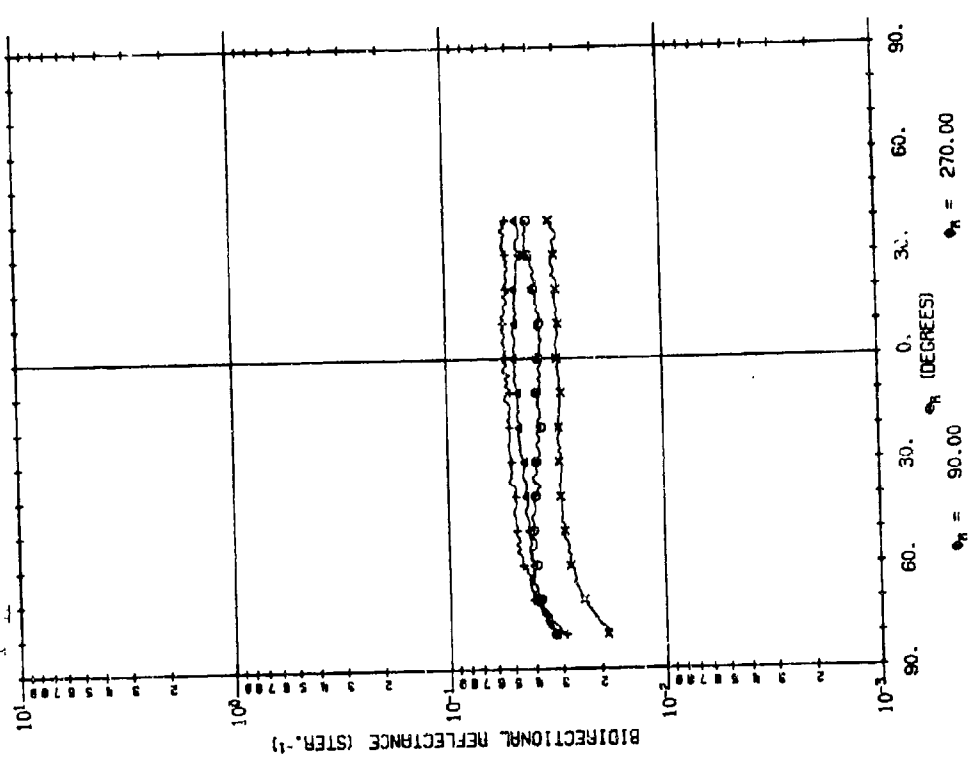
$\lambda = 10.00$
 $\lambda = 180.00$
 $\lambda = 1.06$

0
 +
 -
 x

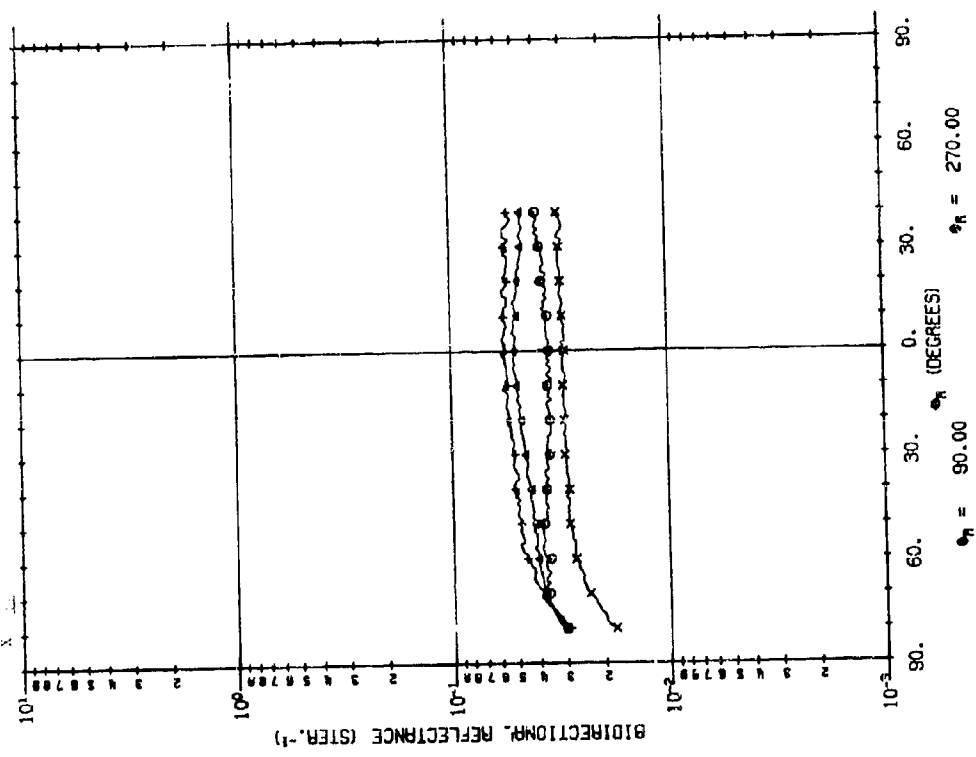


PAINT

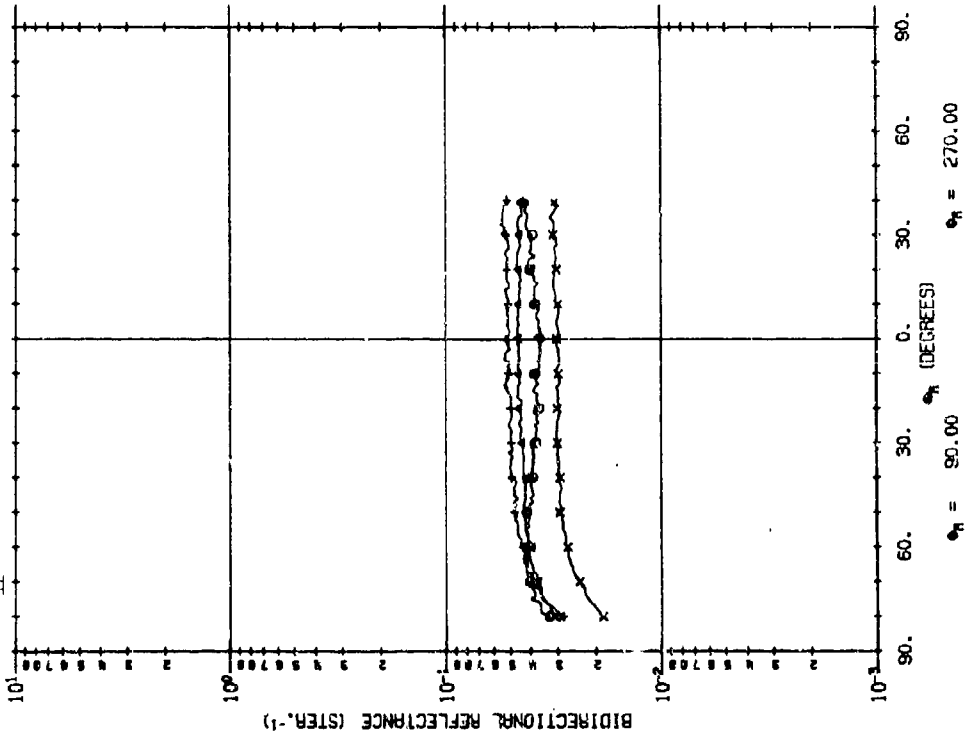
A01807 101 Camouflage Paint on Metal
 0 40.00
 + 11 180.00
 3 11 1.06
 X



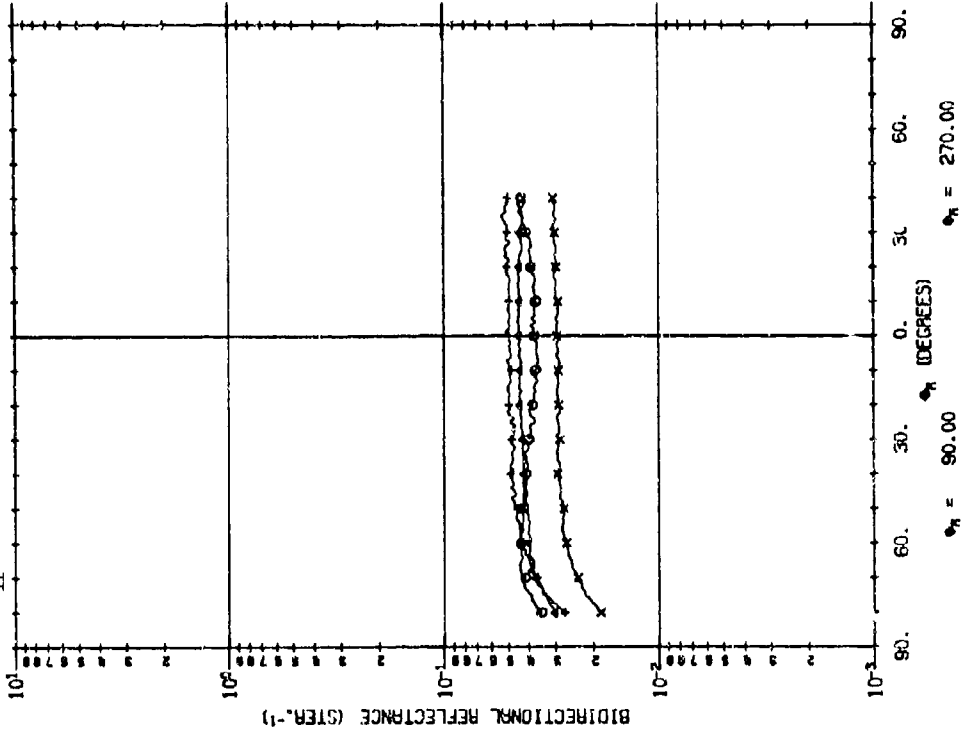
A01807 101 Camouflage Paint on Metal
 0 30.00
 + 11 100.00
 3 11 1.06
 X



AO1807 101
 Camouflage Paint on Metal
 $\theta_1 = 50.00$
 $\theta_2 = 180.00$
 $\lambda = 1.06$



AO1807 101
 Camouflage Paint on Metal
 $\theta_1 = 60.00$
 $\theta_2 = 180.00$
 $\lambda = 1.06$

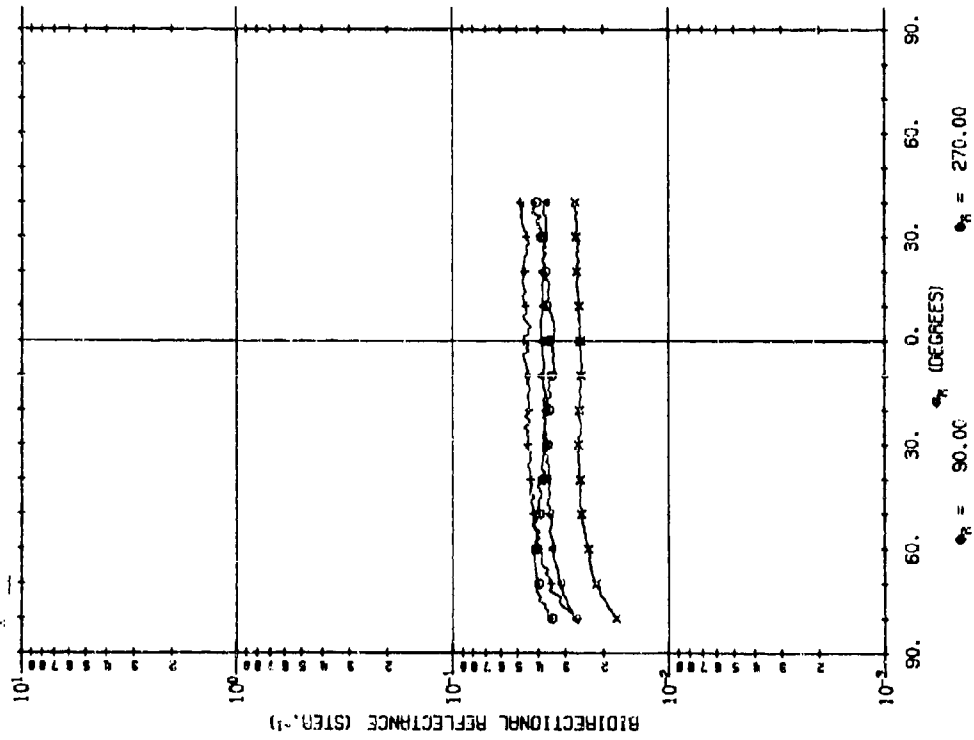


PAINT

R01807 101

Camouflage Paint on Metal

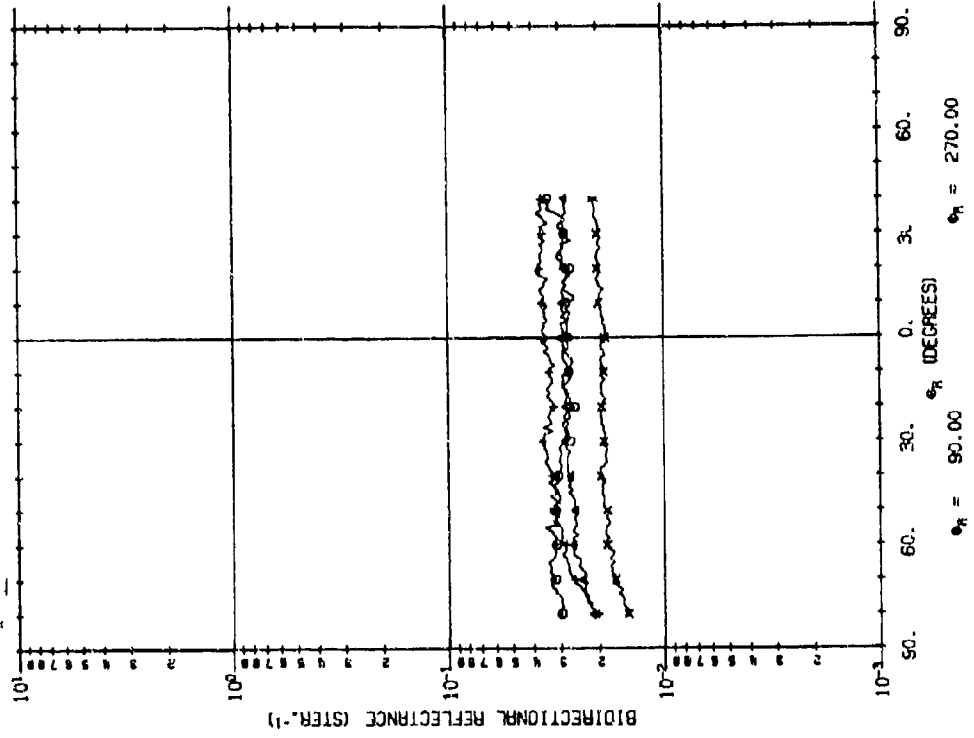
0 $\theta_i = 70.00$
+ $\theta_i = 180.00$
- $\theta_i = 1.06$
x



R01807 101

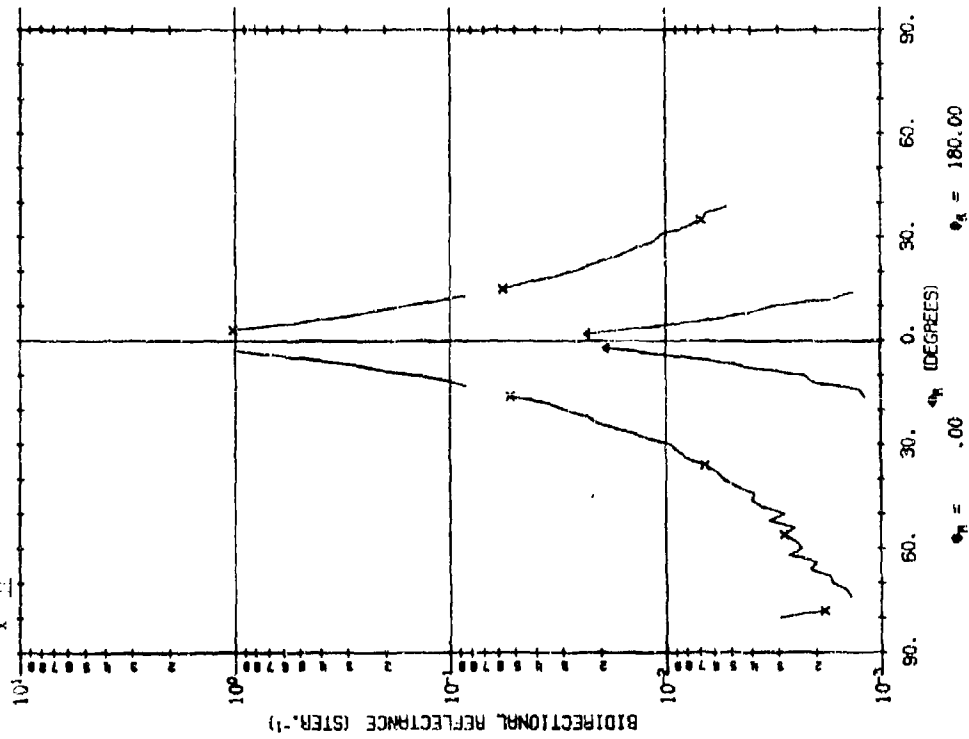
Camouflage Paint on Metal

0 $\theta_i = 75.00$
+ $\theta_i = 180.00$
- $\theta_i = 1.06$
x



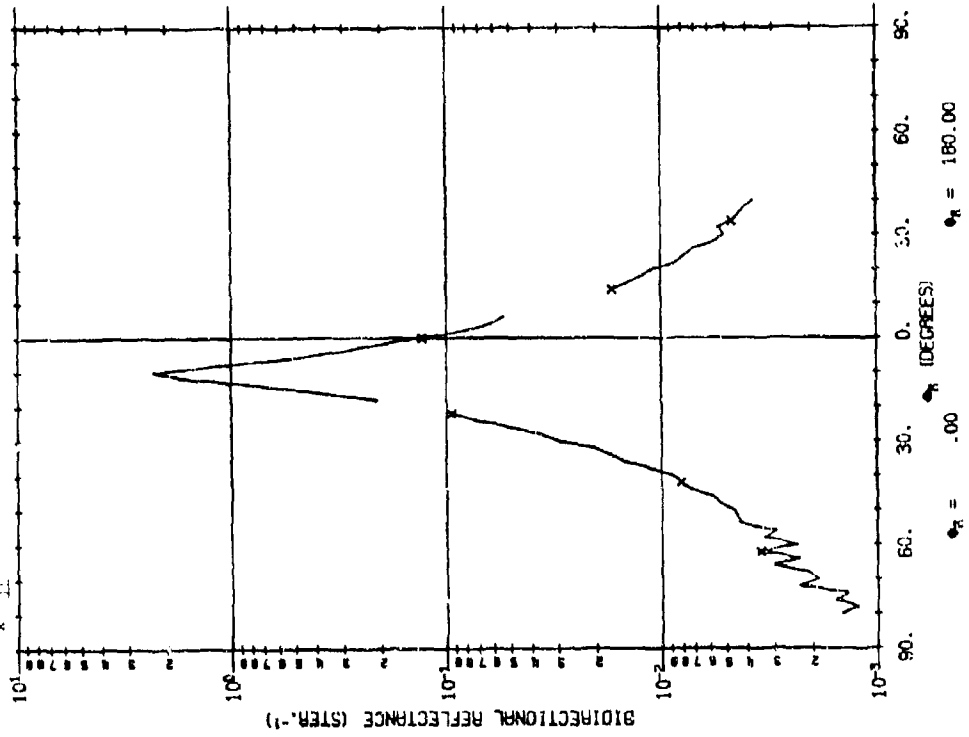
AD1807 302
 Camouflage Paint on Metal

0 | 0.0
 + | 180.00
 - | 10.60
 x |



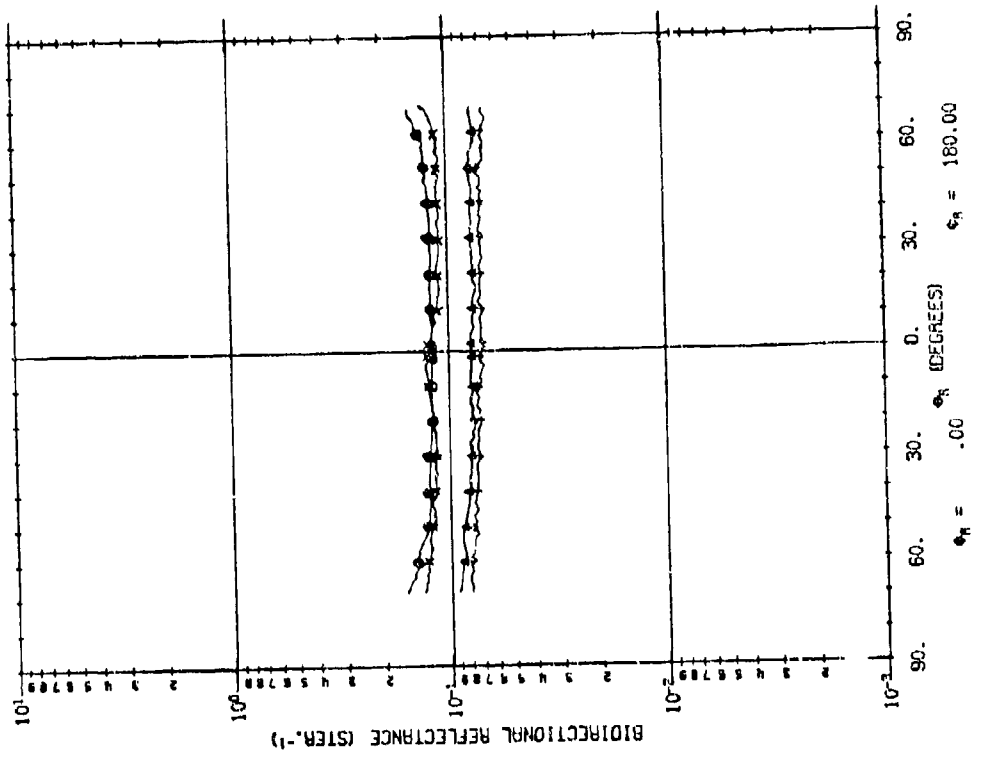
AD1807 302
 Camouflage Paint on Metal

0 | 10.00
 + | 180.00
 - | 10.60
 x |

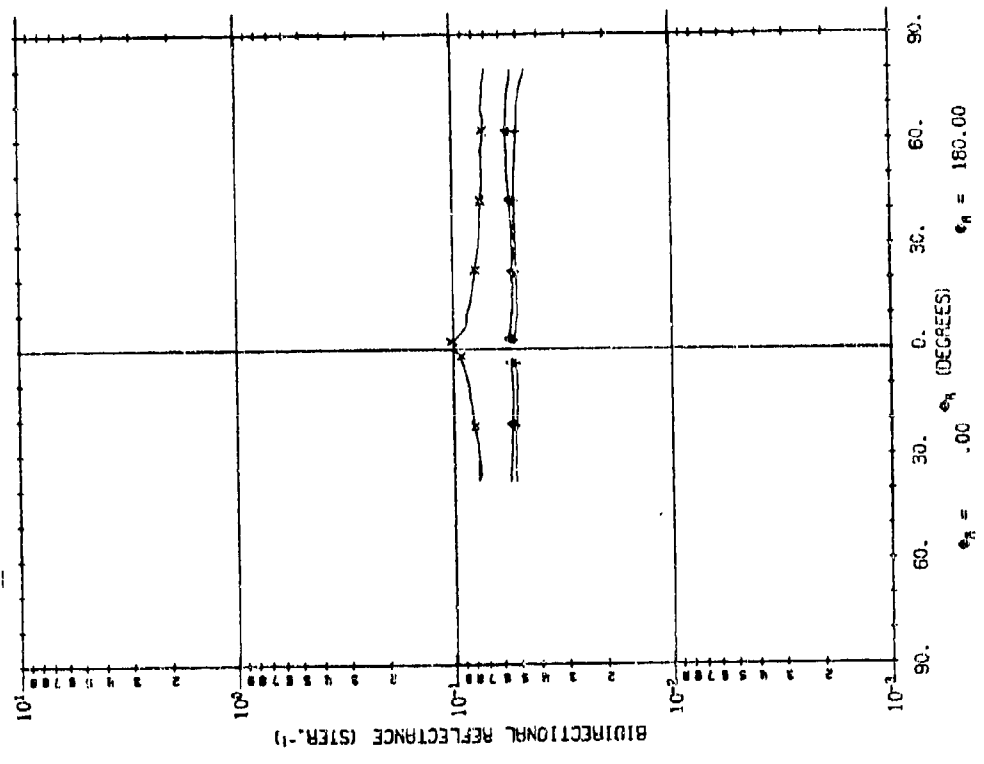


PAINT

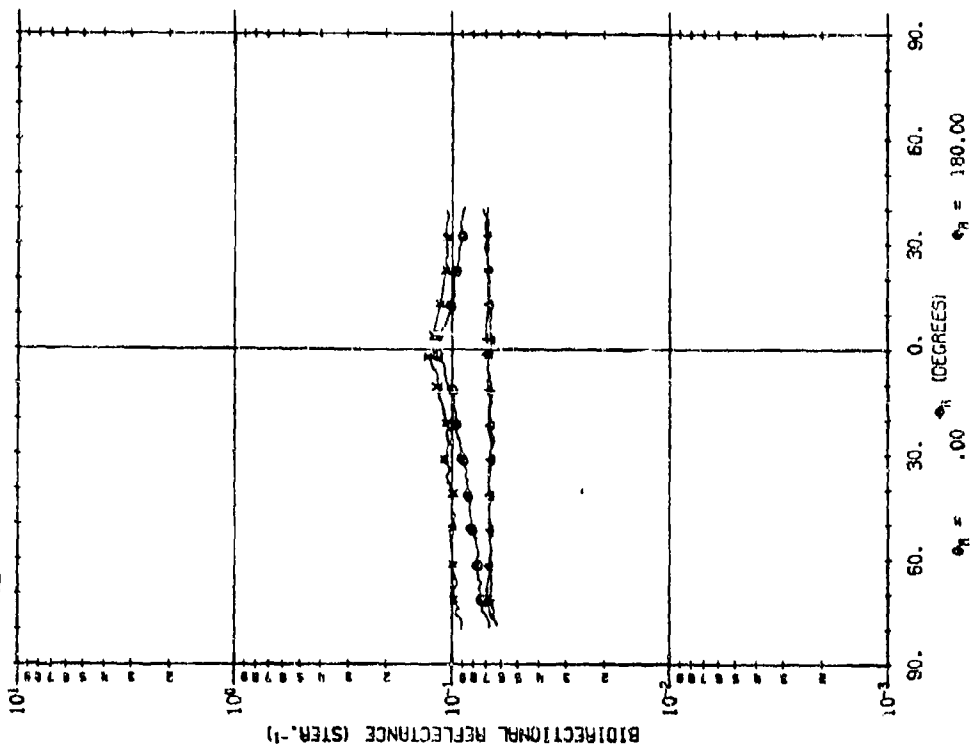
R01808 101
 Camouflage Paint on Metal
 $\epsilon_1 = 2.0$
 $\epsilon_2 = 1$
 $\epsilon_3 = 1.06$



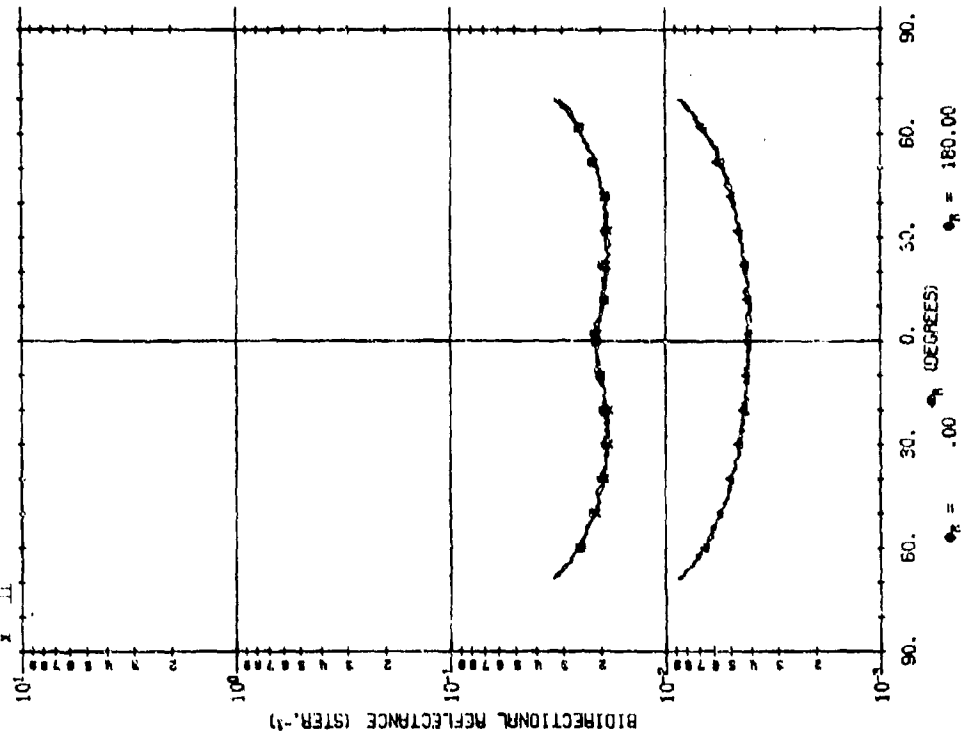
R01808 301
 Camouflage Paint on Metal
 $\epsilon_1 = 0.0$
 $\epsilon_2 = 0.0$
 $\epsilon_3 = 0.63$



R01808 101
 Camouflage Paint on Metal
 $\theta_1 = 0.0$
 $\theta_2 = 0.0$
 $\lambda = 1.06$



R01839 301
 OLIVE DRAB PAINT OF METAL
 $\theta_1 = 2.0$
 $\theta_2 = 0.0$
 $\lambda = 1.06$

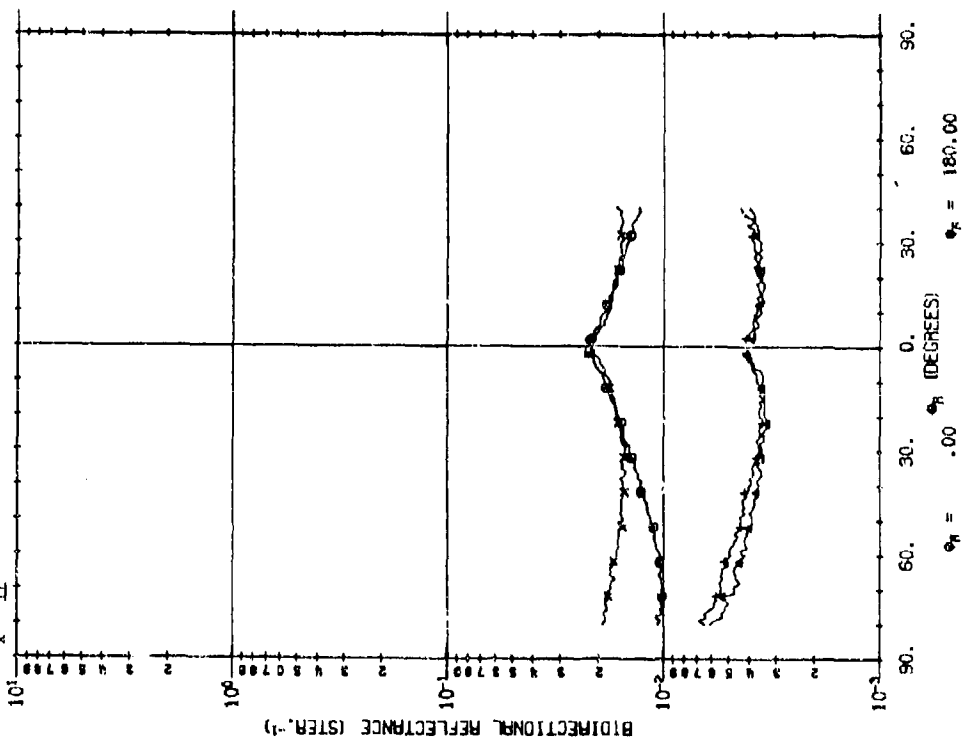


PAINT

A01839 301

OLIVE DRAB PAINT ON METAL

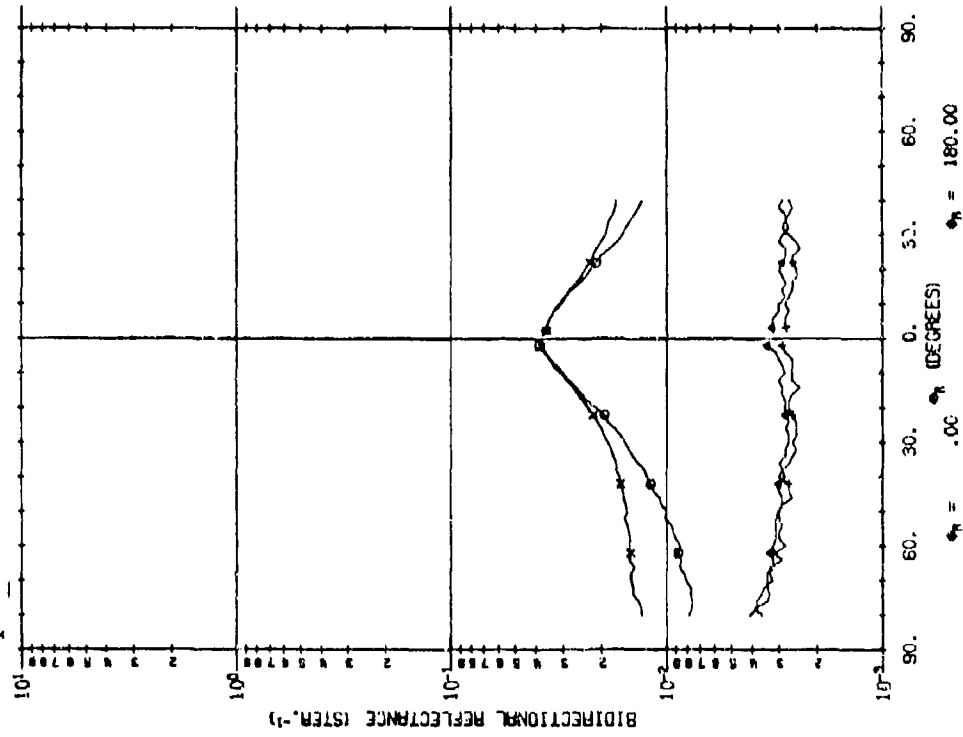
0 | | $\epsilon_1 = 0.0$
+ | | $\epsilon_2 = 0.0$
x | | $\lambda = 1.06$
| |



A01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

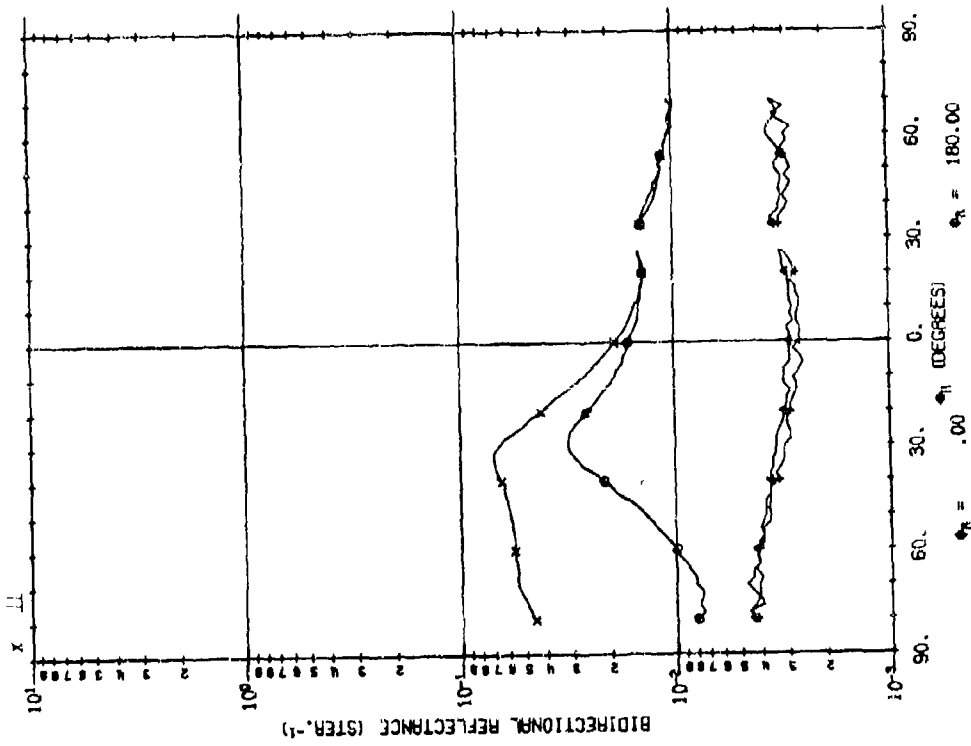
0 | | $\epsilon_1 = 0.0$
+ | | $\epsilon_2 = 180.9$
x | | $\lambda = 1.06$
| |



AO1848 301

OLIVE DRAB AND WHITE PAINT ON METAL

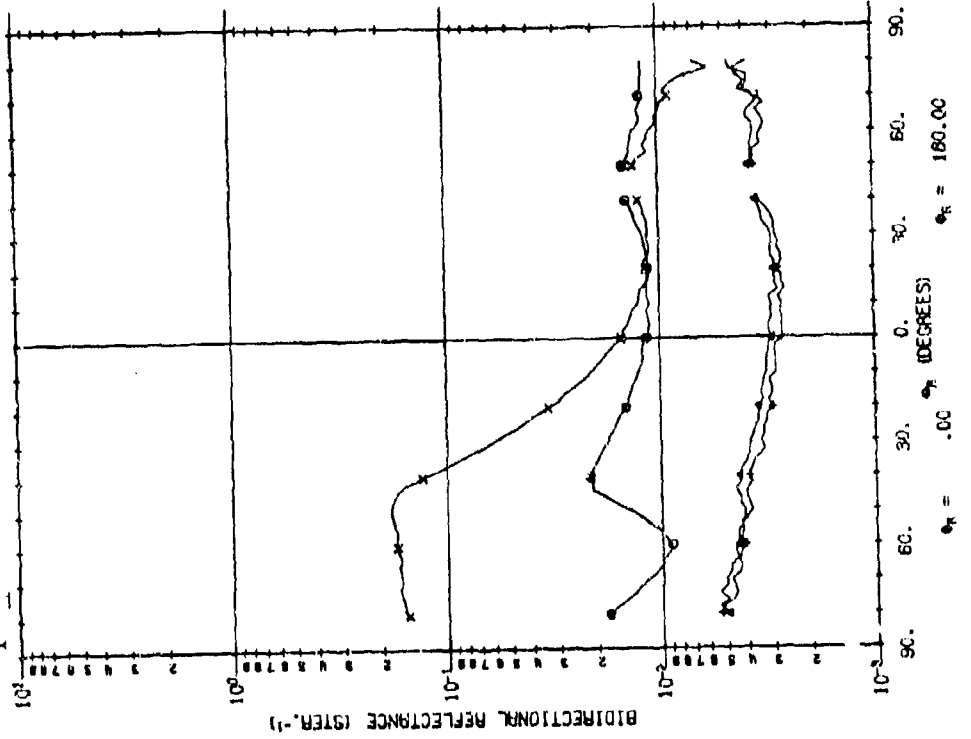
C || $\theta_1 = 30.0$
+ || $\theta_1 = 180.0$
x || $\theta_1 = 1.06$



AO1848 301

OLIVE DRAB AND WHITE PAINT ON METAL

C || $\theta_1 = 45.0$
+ || $\theta_1 = 180.0$
x || $\theta_1 = 1.06$

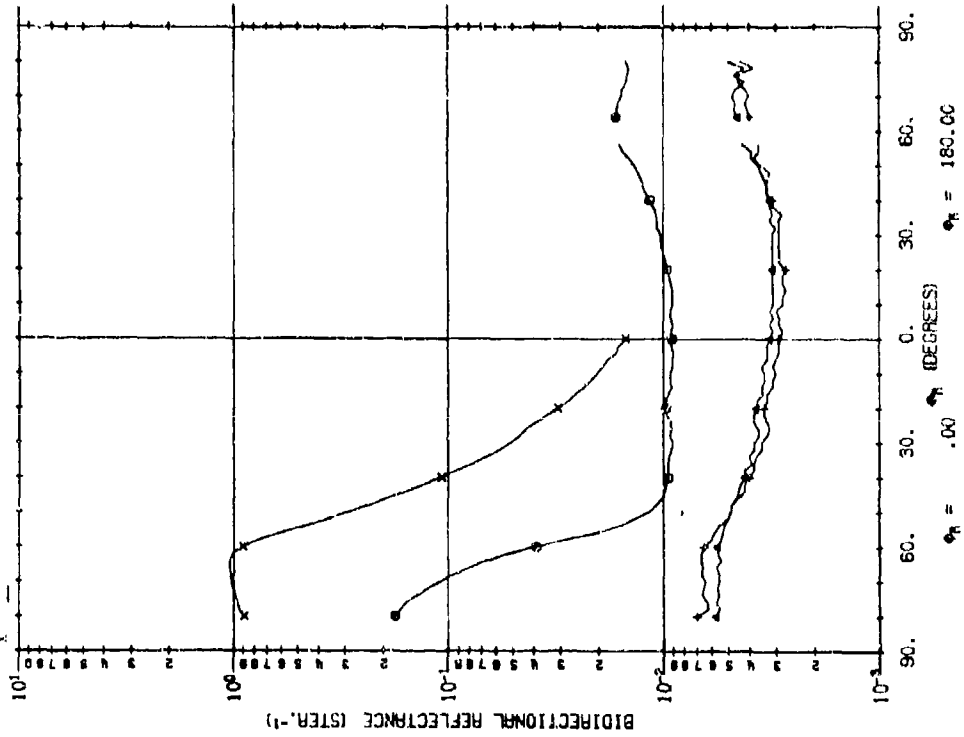


PAINT

R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

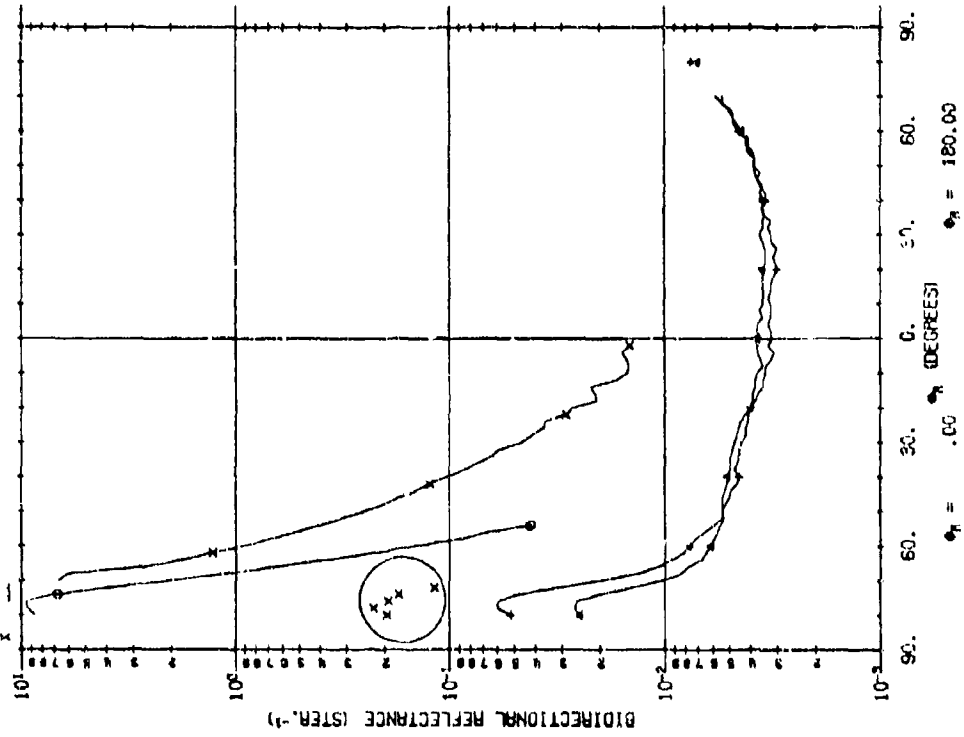
$\theta_i = 60.0$
 $\theta_r = 180.0$
 $\phi = 1.06$



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

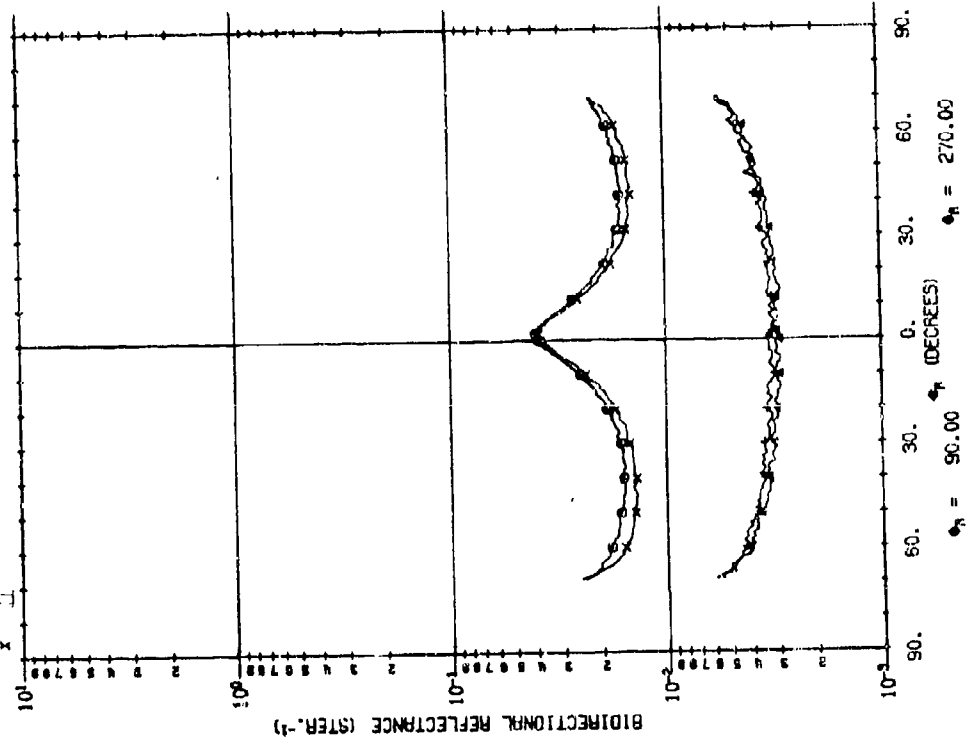
$\theta_i = 75.0$
 $\theta_r = 180.0$
 $\phi = 1.06$



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

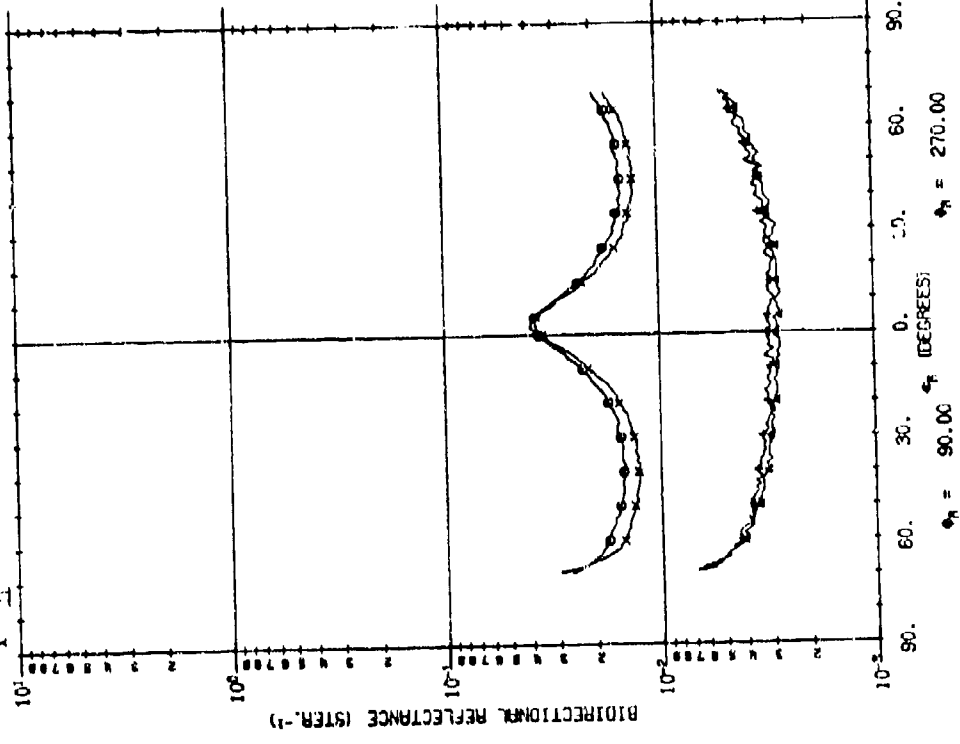
0 || $z_1 = 2.0$
+ || $\theta_1 = 4^\circ$
- || $\lambda = 1.06$
x ||



R01848 301

OLIVE DRAB AND WHITE PAINT ON METAL

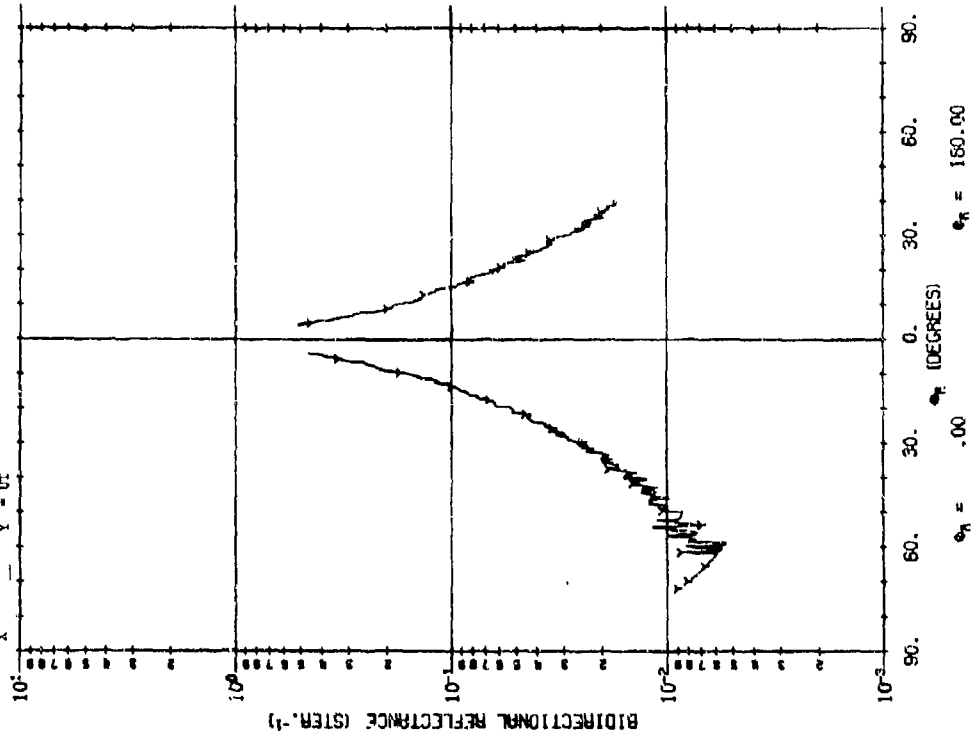
0 || $z_1 = 5.0$
+ || $\theta_1 = 4^\circ$
- || $\lambda = 1.06$
x ||



PAINT

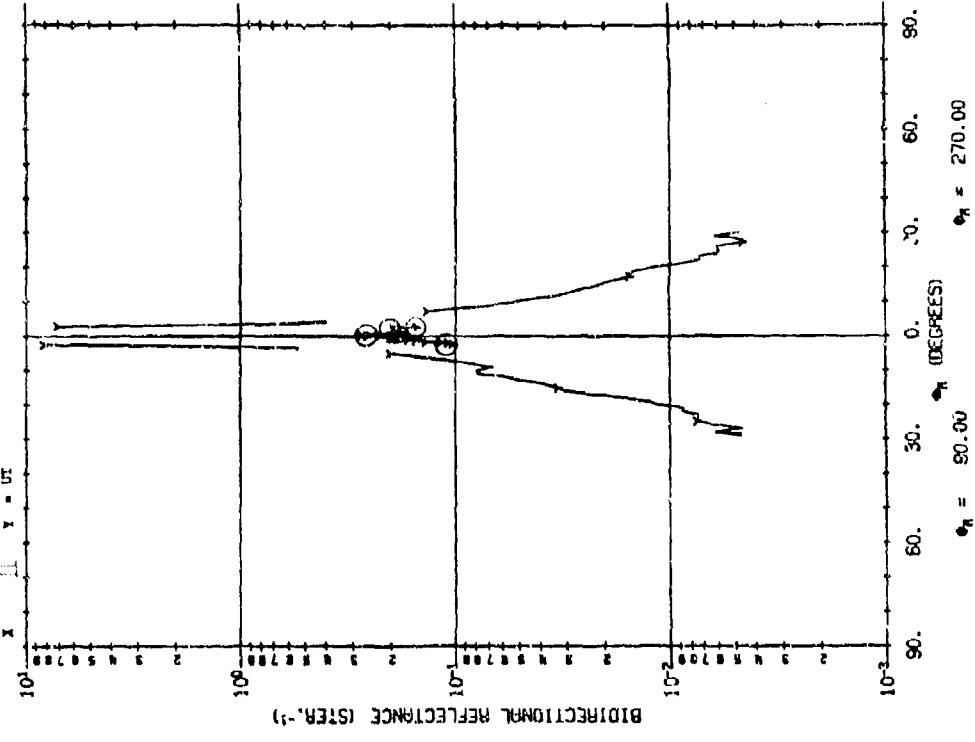
A01879 201
 0 0.0
 + 180.0
 2 10.6
 X Y = UT

Green Paint on Metal



A01879 201
 0 2.0
 + 10.6
 2 10.6
 X Y = UT

Green Paint on Metal

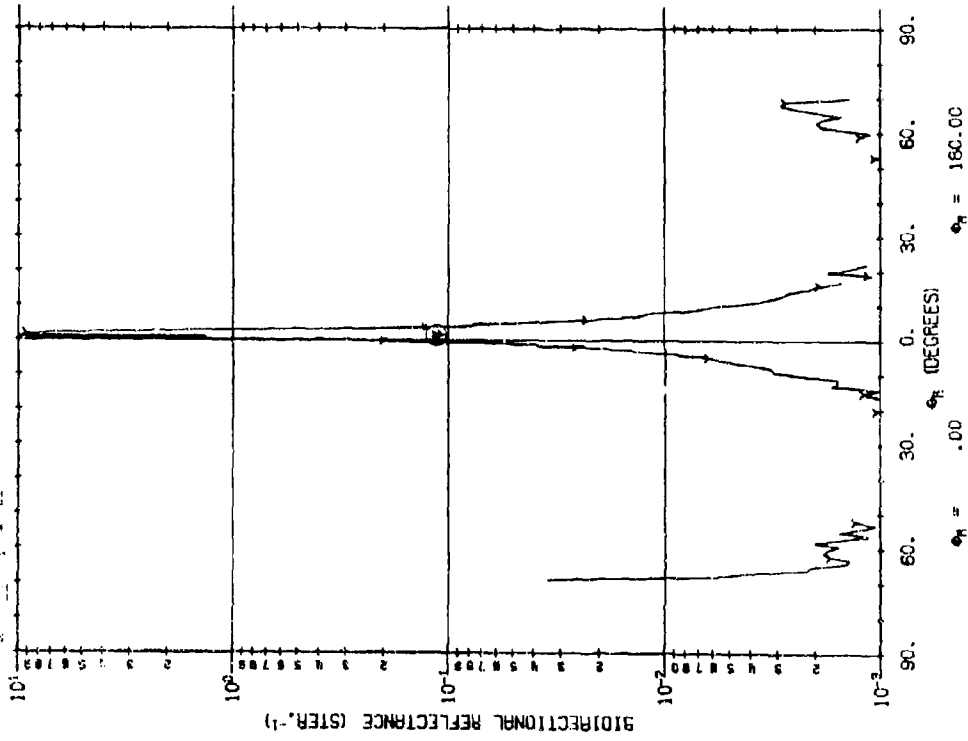


PAINT

A01880 201

Green Paint on Metal

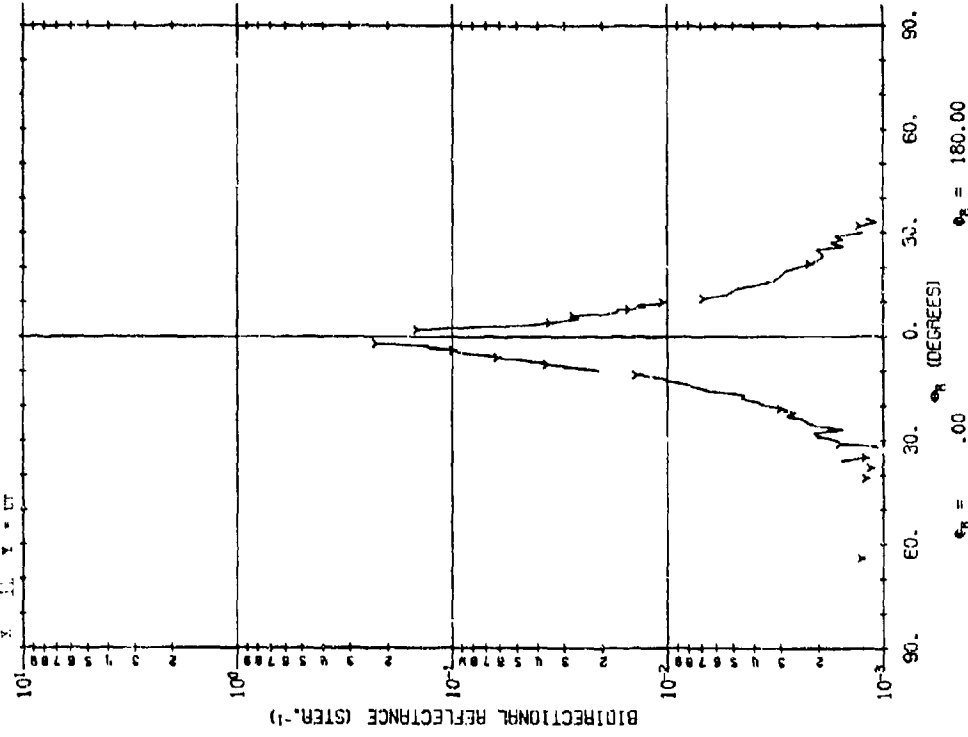
$\theta_i = 2.0$
 $\theta_r = 45$
 $\theta_t = 10.6$
 $\phi = 0$
 $\phi = 180$



A01880 201

Green Paint on Metal

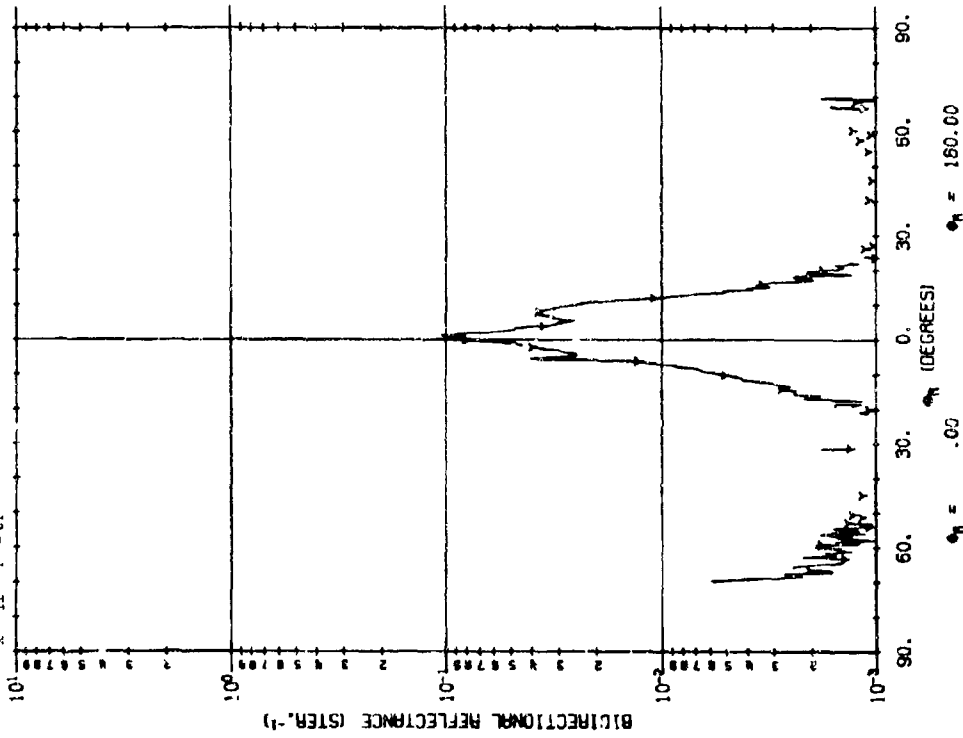
$\theta_i = 0.0$
 $\theta_r = 180.0$
 $\theta_t = 10.6$
 $\phi = 0$
 $\phi = 180$



A01881 301

Black Paint on Metal

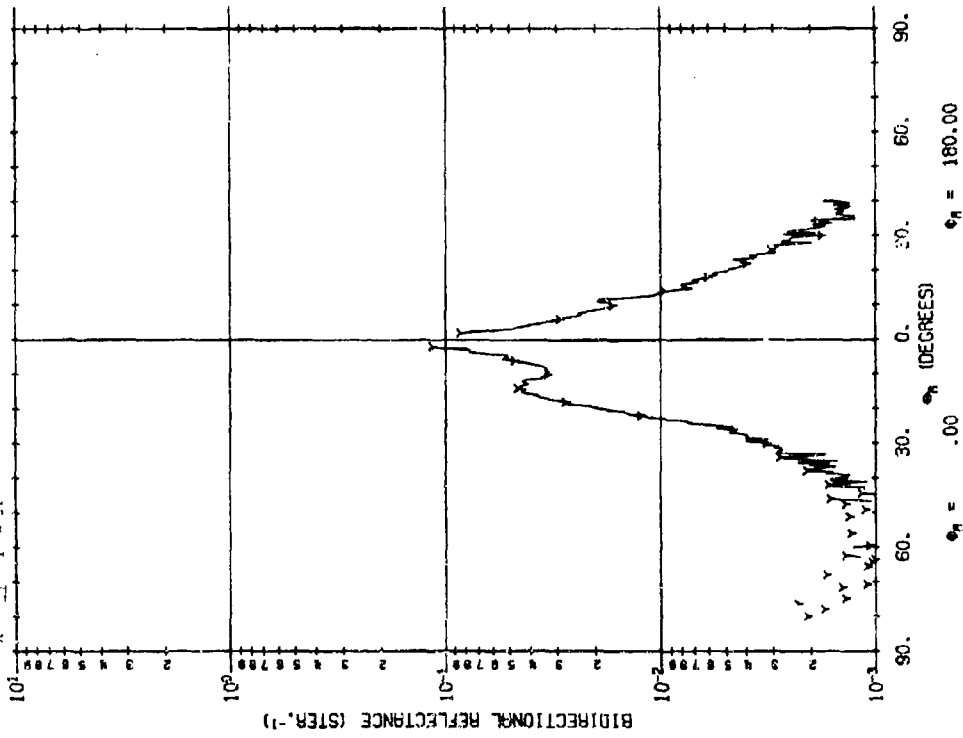
0 1 22 = 2.0
+ 1 1 = ϕ_1
- 1 1 = ϕ_2
X II Y = UT



A01881 301

Black Paint on Metal

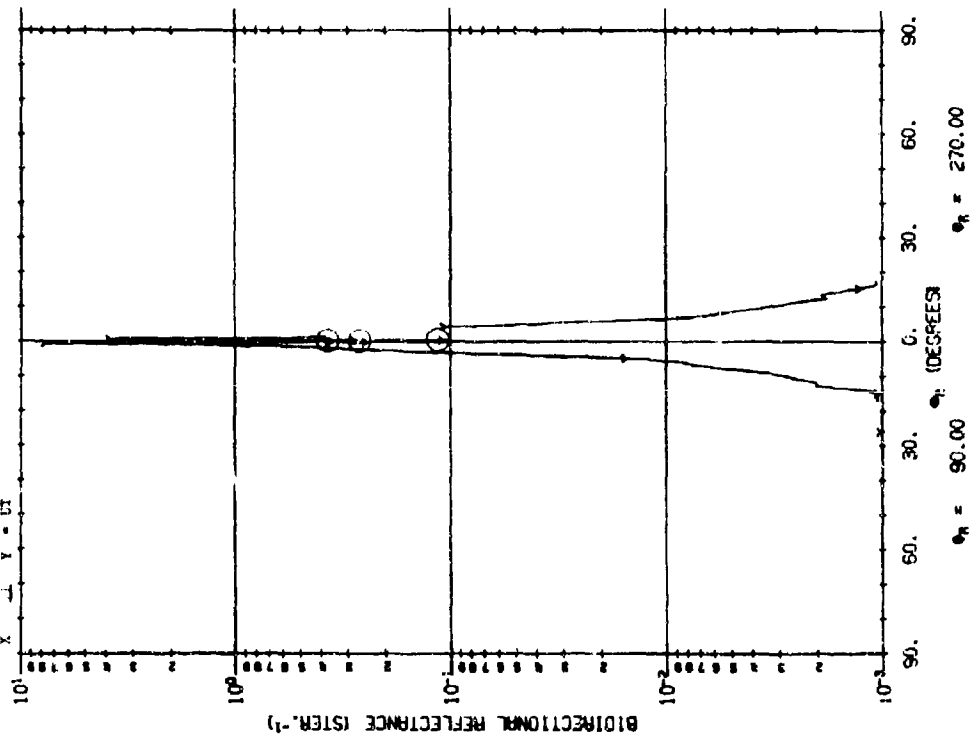
0 1 1 $\phi_1 = 0.0$
+ 1 1 = ϕ_2
- 1 1 = ϕ_3
X II Y = UT



A01881 301

Black Paint on Metal

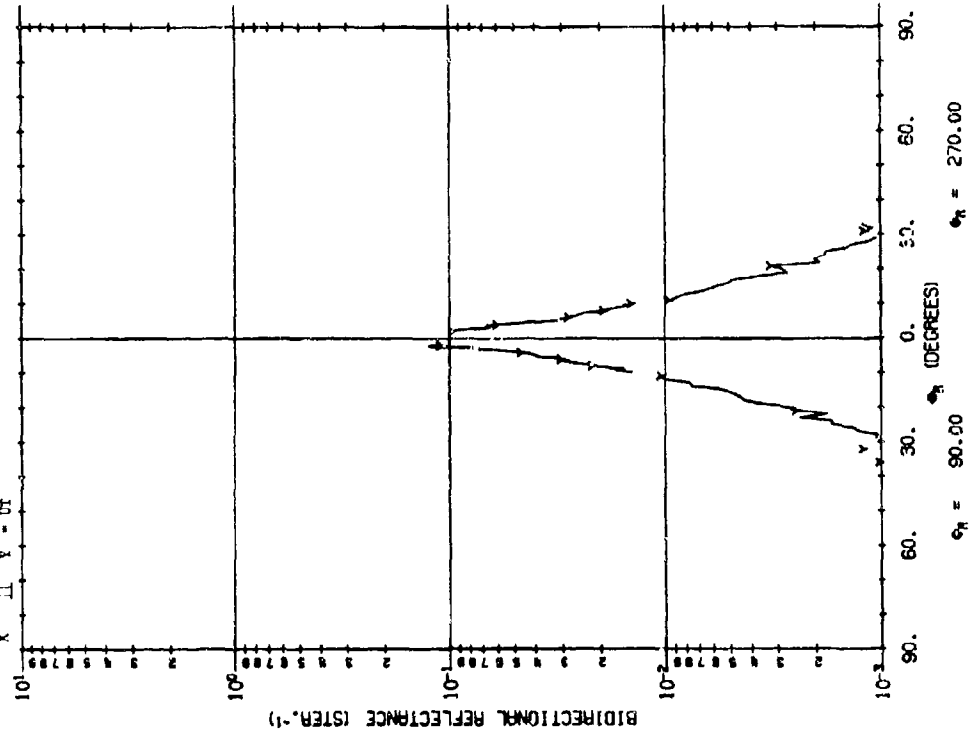
0 || 2θ = 2.0
+ || φ₁ = 4°
· || λ = 30.6
X || Y = DT



A01881 301

Black Paint on Metal

0 || φ₁ = 0.0
+ || φ₁ = 270.0
· || λ = 10.6
X || Y = DT

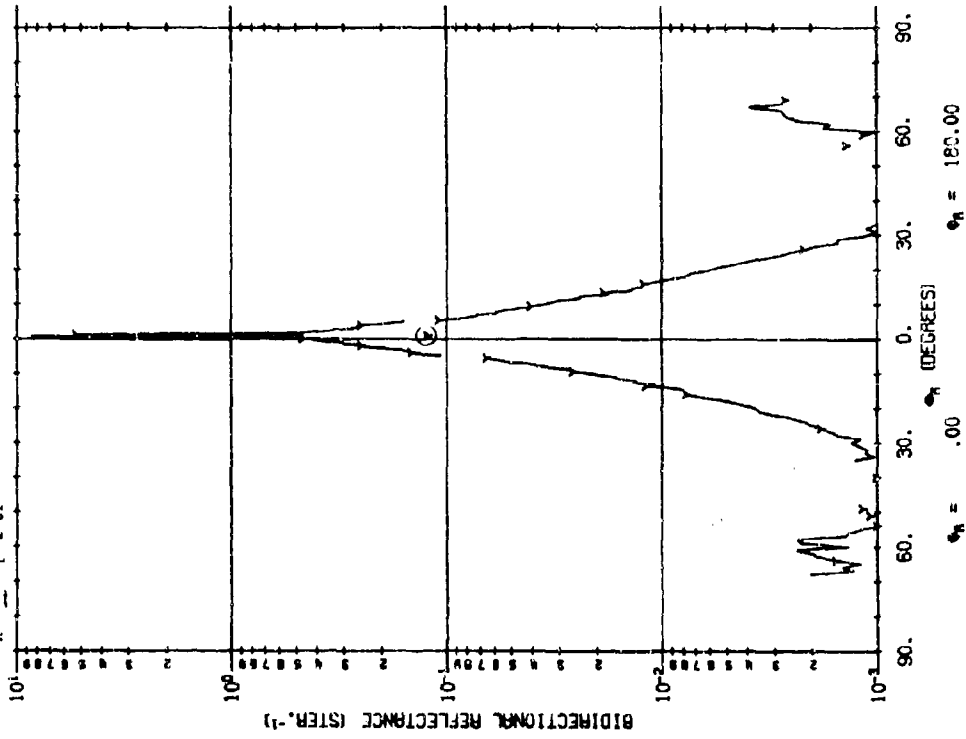


PAINT

R01882 201

Orange Paint on Metal

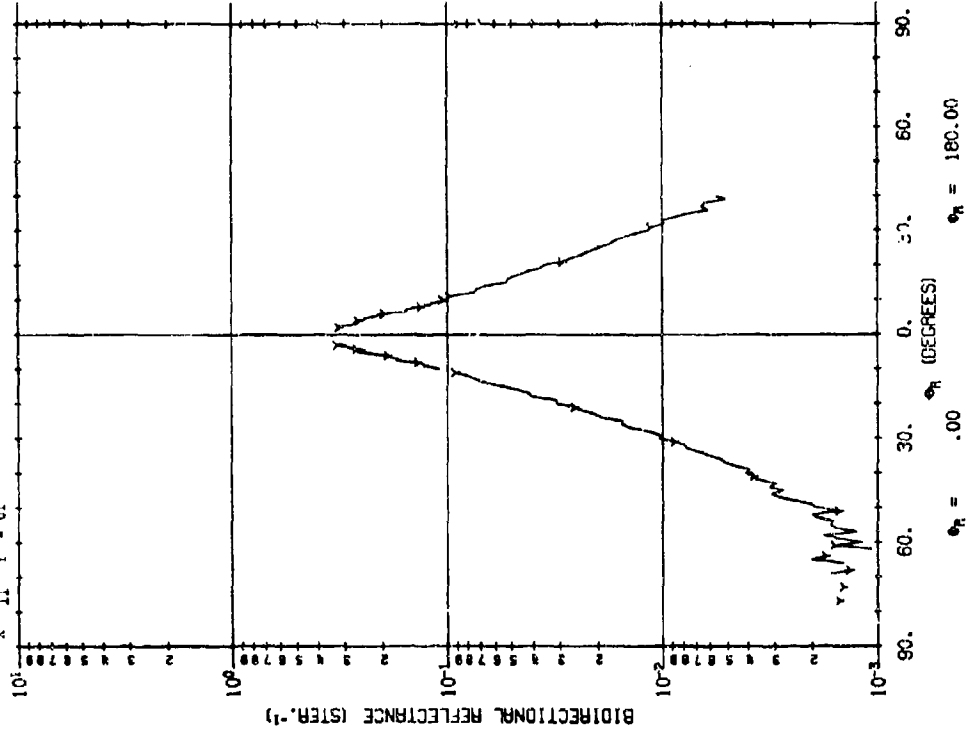
0 θ_1 = 2.0
+ θ_2 = 0.0
x θ_3 = 0.0
z θ_4 = 180.0
A θ_5 = 10.6
X θ_6 = 0.0
Y = 0.0



R01882 201

Orange Paint on Metal

0 θ_1 = 0.0
+ θ_2 = 0.0
x θ_3 = 180.0
z θ_4 = 10.6
A θ_5 = 0.0
X θ_6 = 0.0
Y = 0.0



R01882 201

Orange Paint on Metal

$2\theta = 2.0$

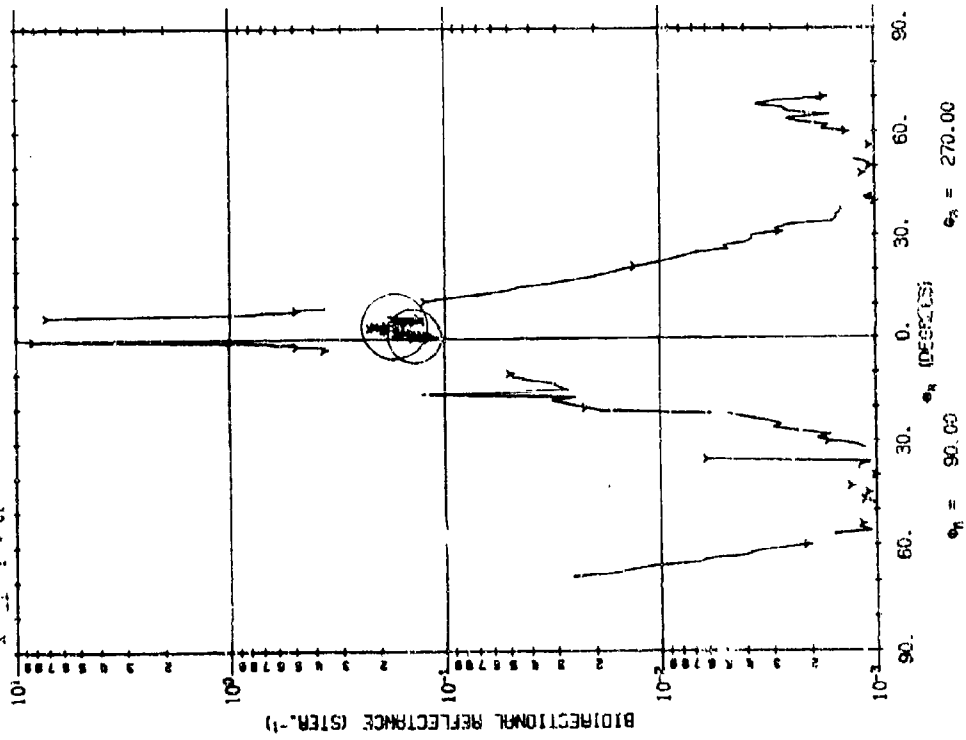
$\phi_1 = \phi_2$

$\lambda = 10.6$

$\psi = 0^\circ$

$\chi = 0^\circ$

$\gamma = 0^\circ$



R01883 101

Olive Drab Paint on Metal

$2\theta = 2.0$

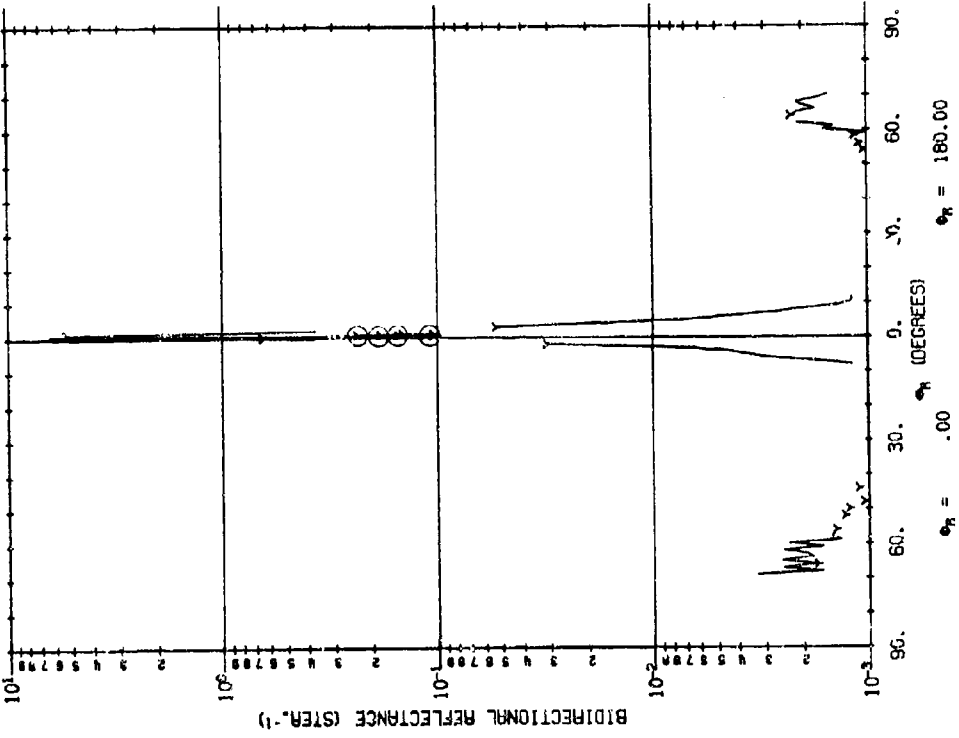
$\phi_1 = \phi_2$

$\lambda = 10.6$

$\psi = 0^\circ$

$\chi = 0^\circ$

$\gamma = 0^\circ$

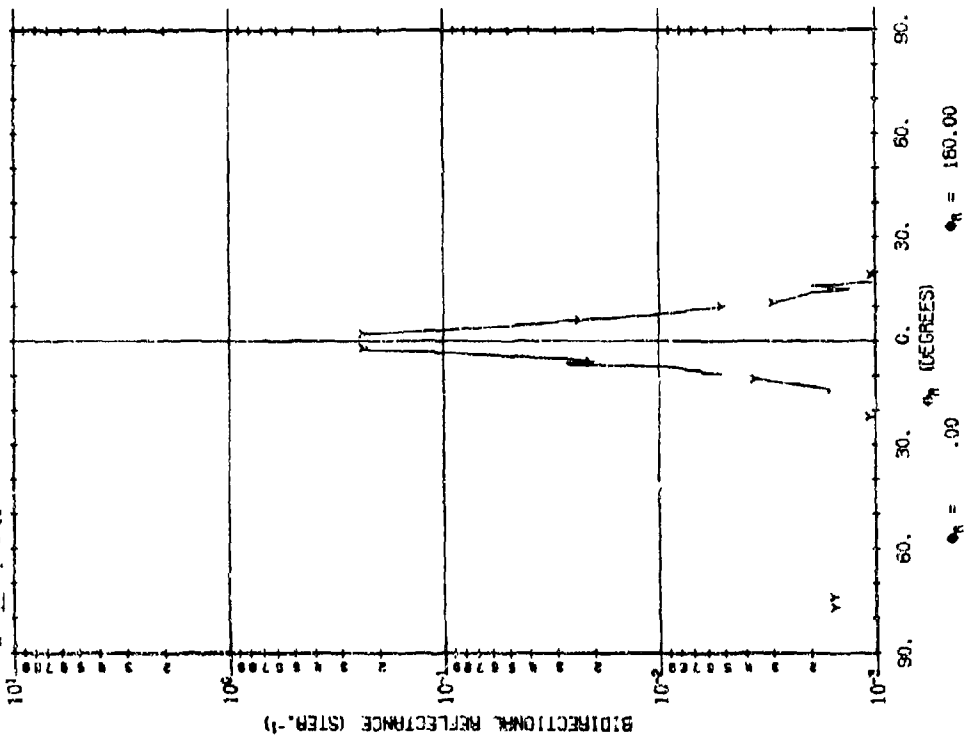


PAINT

R01883 101

Olive Drab Paint on Metal

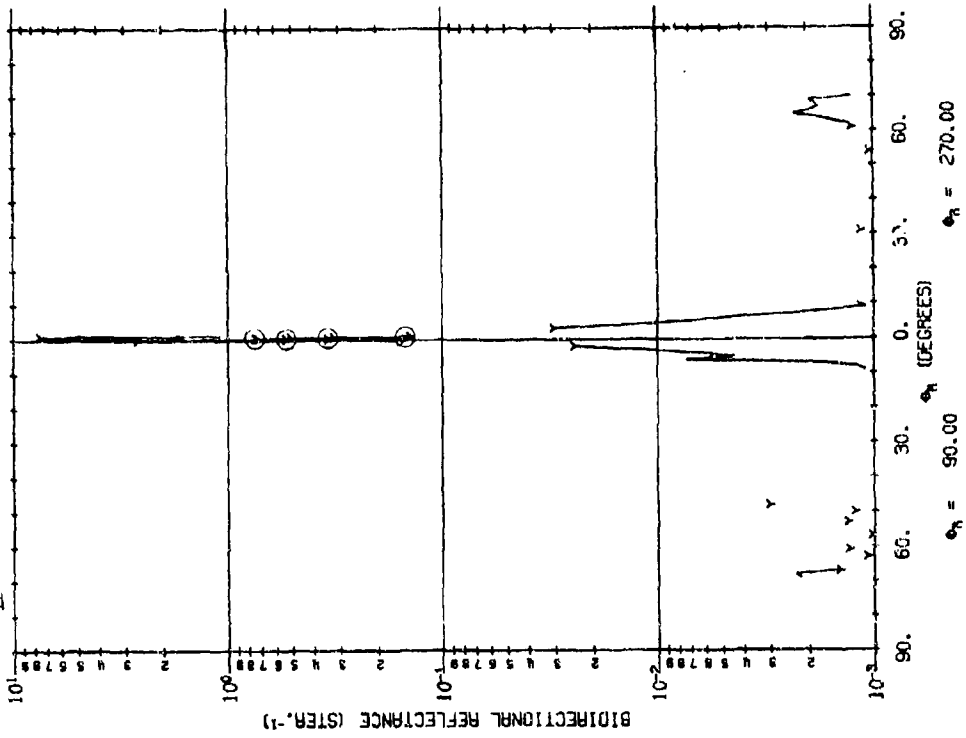
0 $\theta_i = 0.0$
+ $\theta_r = 180.0$
- $\lambda = 10.6$
X $\theta_n = 0.0$
Y $\theta_n = 0.0$



R01883 101

Olive Drab Paint on Metal

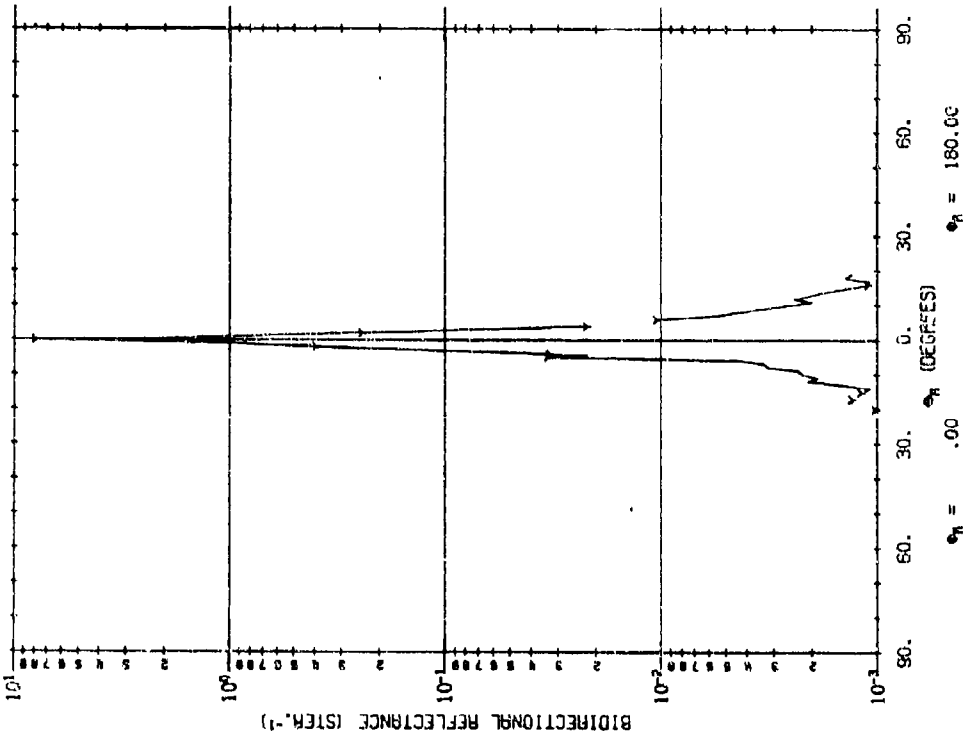
0 $\theta_i = 2.0$
+ $\theta_r = 0.0$
- $\lambda = 10.6$
X $\theta_n = 0.0$
Y $\theta_n = 0.0$



001887 201

Blue Paint on Metal

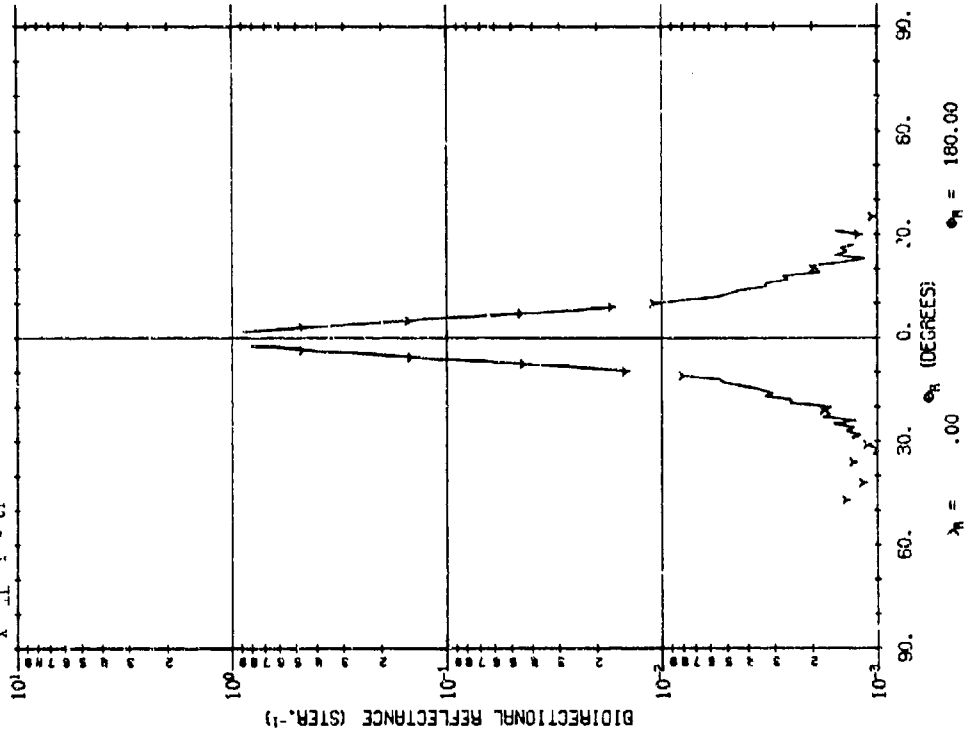
0 $\theta_1 = 2.0$
 1 $\theta_2 = 45$
 2 $\theta_3 = 10.6$
 X $\theta_4 = 180$



001887 201

Blue Paint on Metal

0 $\theta_1 = 0.0$
 1 $\theta_2 = 180.0$
 2 $\theta_3 = 10.6$
 X $\theta_4 = 180$

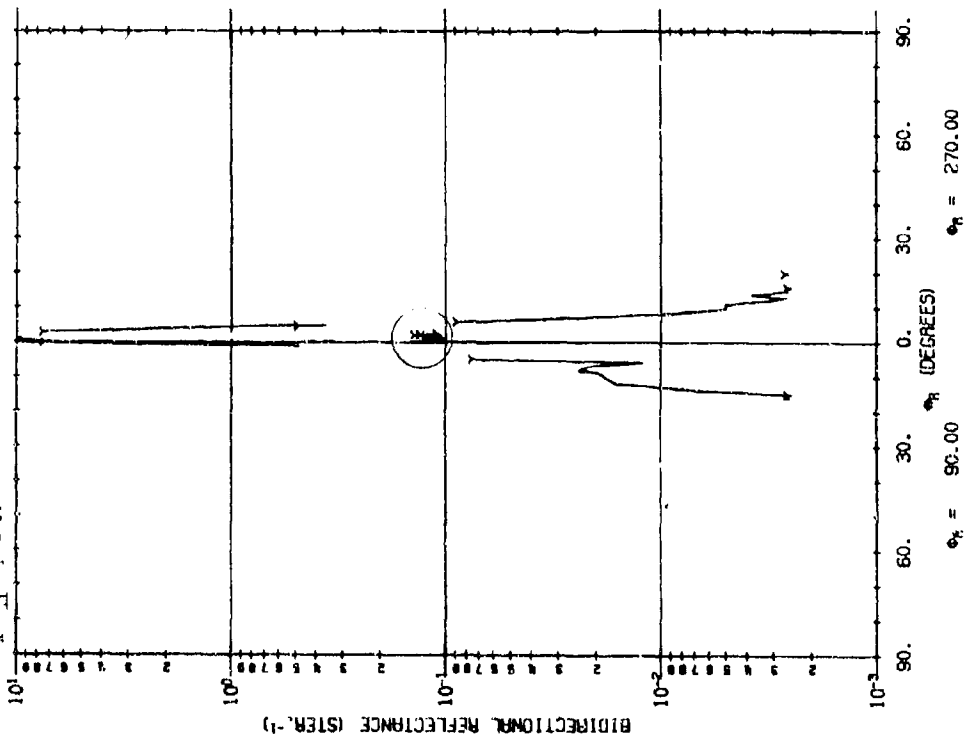


PAINT

R01887 201

Blue Paint on Metal

0 | 25 = 2.0
+ | | $\phi_1 = \phi_r$
- | | $\lambda = 10.6$
x | | $\gamma = \text{UT}$

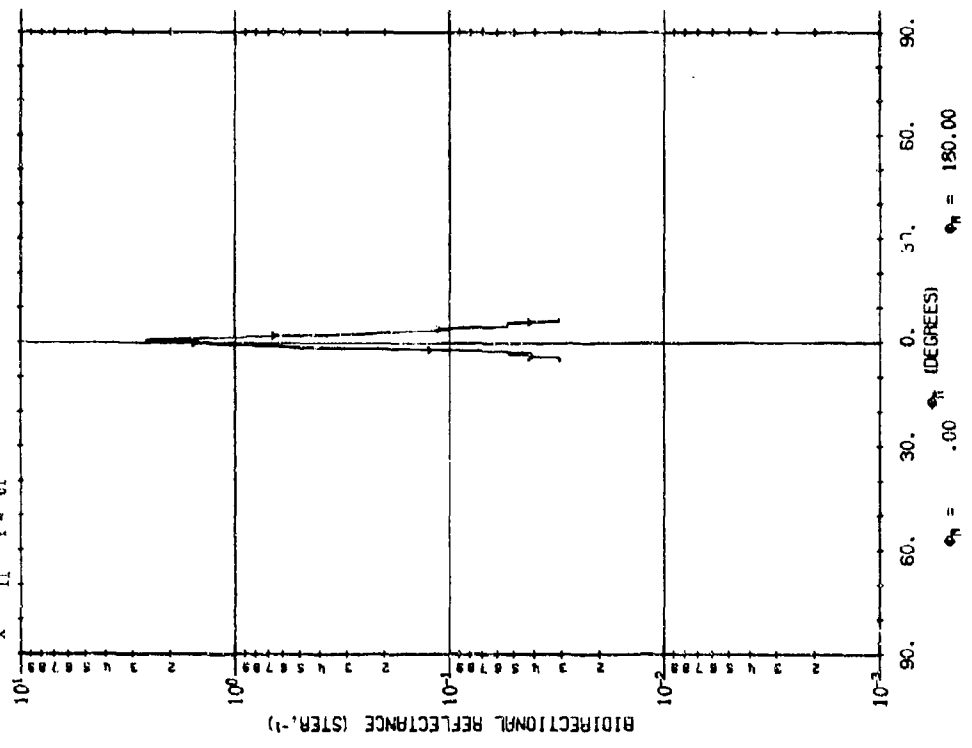


$\phi_r = 90.00$ $\phi_r = 270.00$

R01888 201

OLIVE DR.-9 PAINT ON BLUE PAINTED METAL

0 | 25 = 2.0
+ | | $\phi_1 = \phi_r$
- | | $\lambda = 10.6$
x | | $\gamma = \text{UT}$

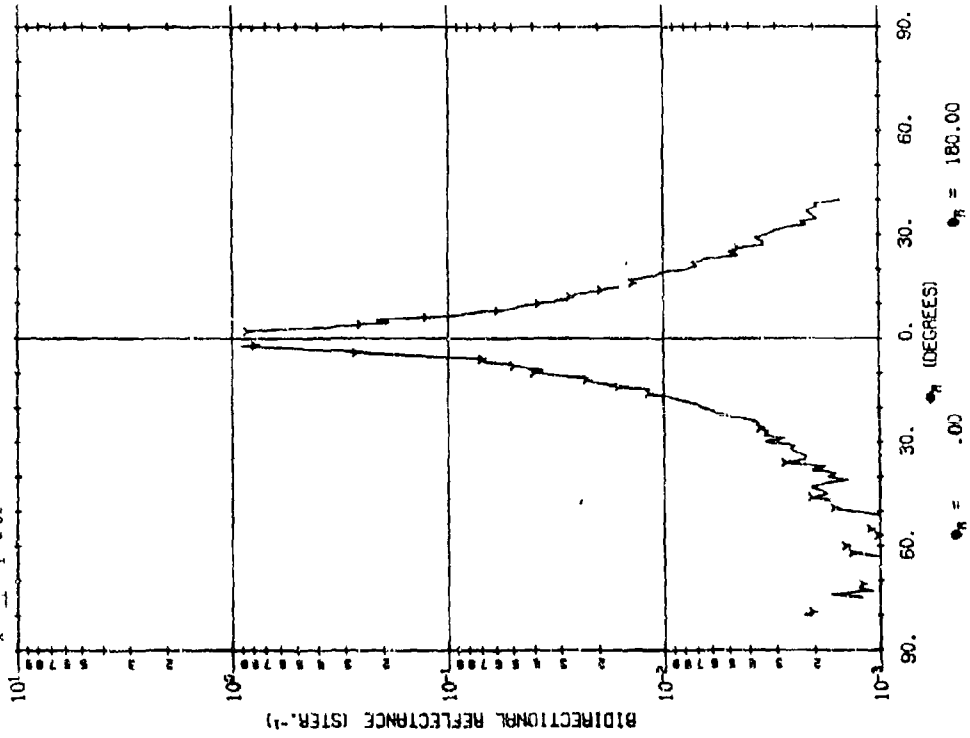


$\phi_r = 90.00$ $\phi_r = 180.00$

A01888 201

Olive Drab Paint on Blue Painted Metal

0 // $\theta_1 = 0.0$
+ // $\theta_2 = 180.0$
- // $\theta_3 = 18.6$
x // $\theta_4 = 18.6$



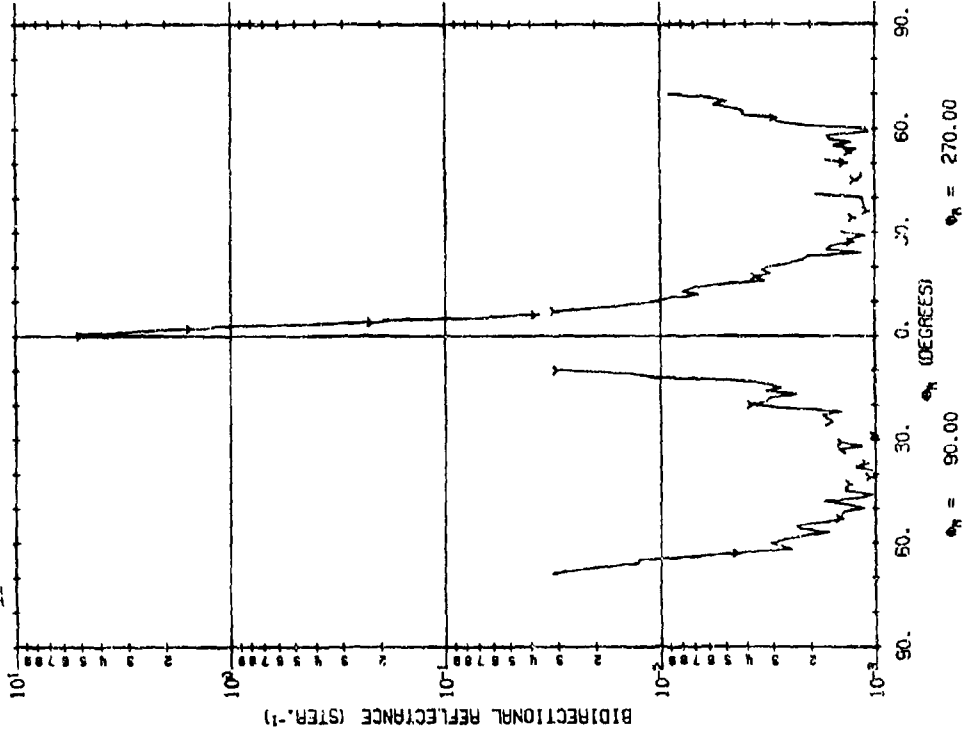
$\theta_1 = .00$

$\theta_2 = 180.00$

A01888 201

Olive Drab Paint on Blue Painted Metal

0 // $\theta_1 = 2.0$
+ // $\theta_2 = 6.0$
- // $\theta_3 = 10.6$
x // $\theta_4 = 18.6$



$\theta_1 = 90.00$

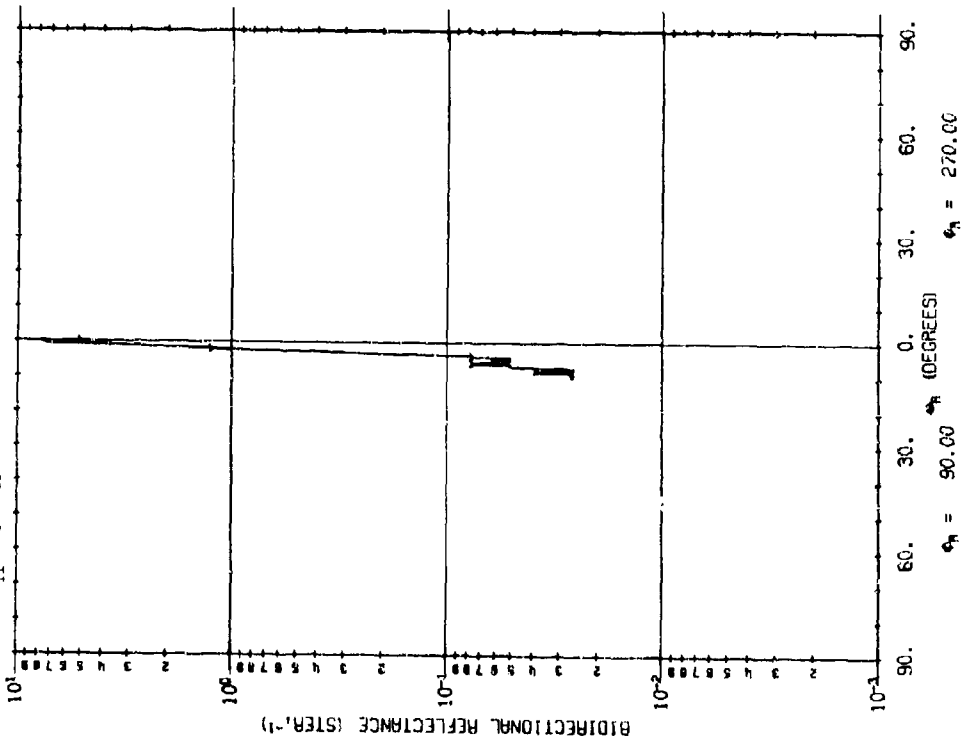
$\theta_2 = 270.00$

PAINT

R01888 201

OLIVE DRAB PAINT ON BLUE PAINTED METAL

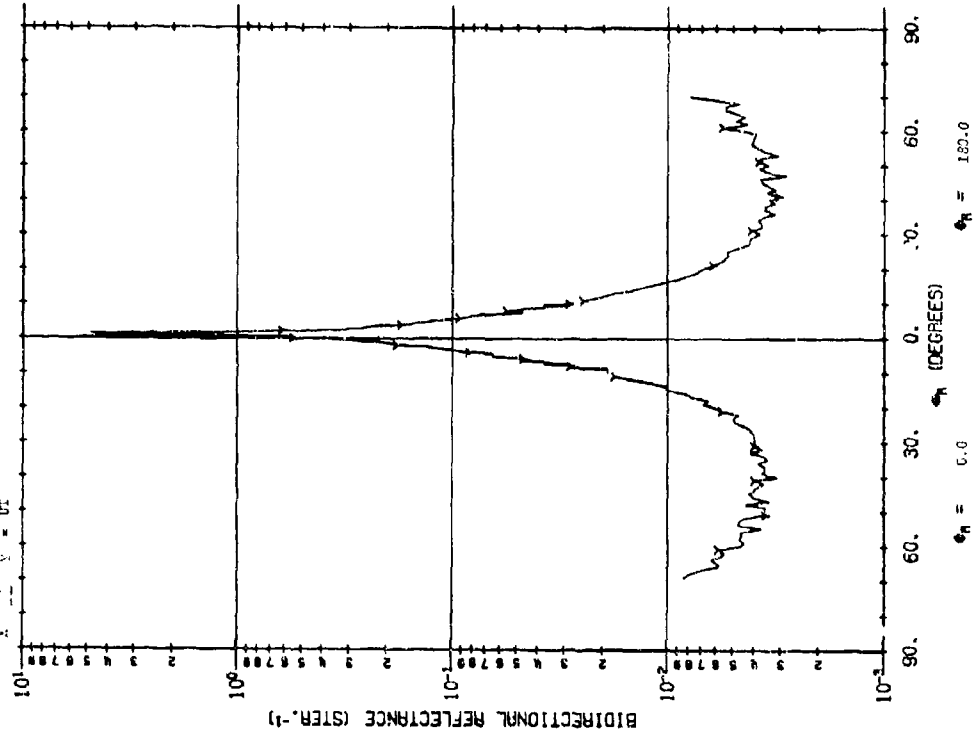
$\phi_1 = 0.0$
 $\phi_2 = 0.0$
 $\phi_3 = 10.6$
 $\phi_4 = 10.6$
 $Y = UT$



R01889 101

OLIVE DRAB PAINT ON GREEN PRIMER ON ALUMINUM

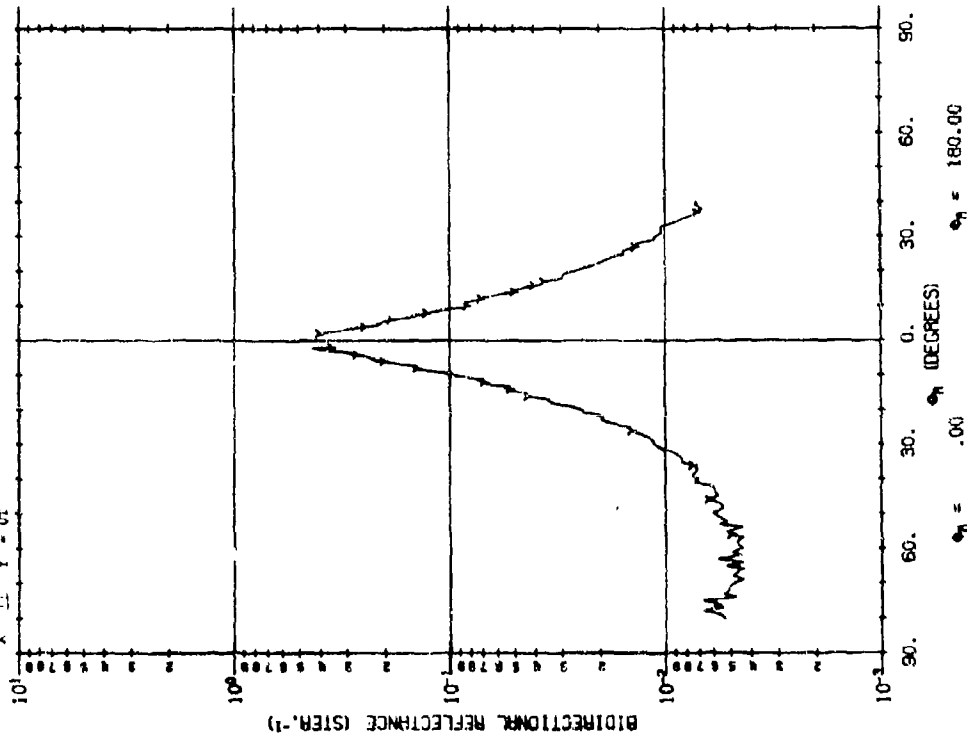
$\phi_1 = 2.0$
 $\phi_2 = 2.0$
 $\phi_3 = 10.6$
 $\phi_4 = 10.6$
 $Y = UT$



A01889 101

Olive Drab Paint on Green Primer on
Aluminum

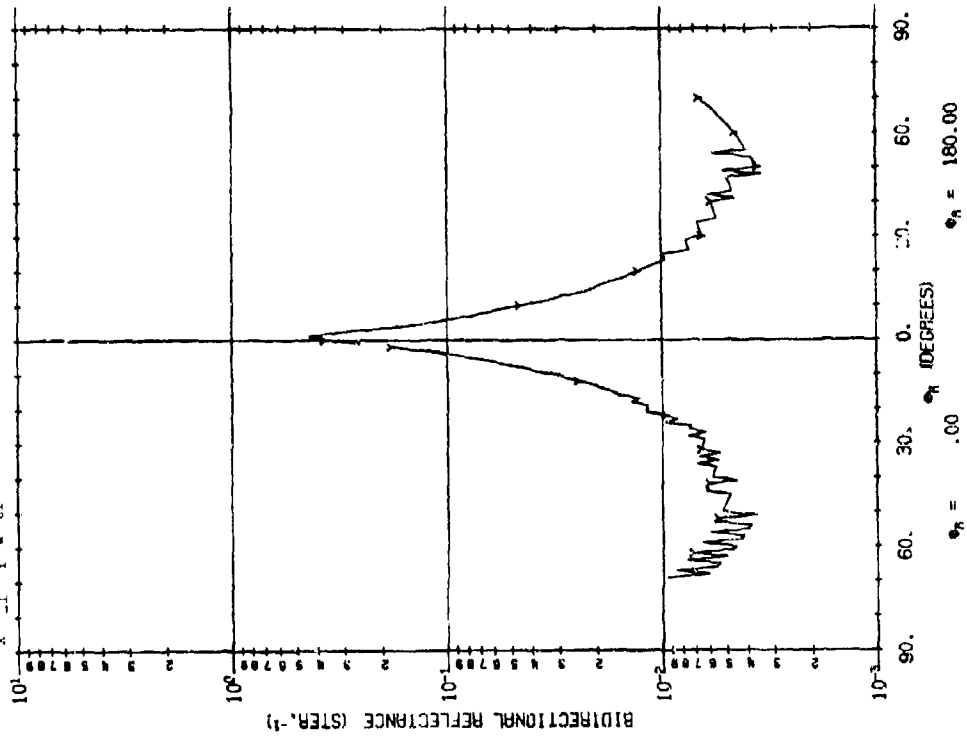
$\theta_i = 0.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y = UT



A01892 301

Olive Drab Paint on Aluminum

$\theta_i = 2.0$
 $\theta_r = 0$
 $\lambda = 10.6$
X Y = UT

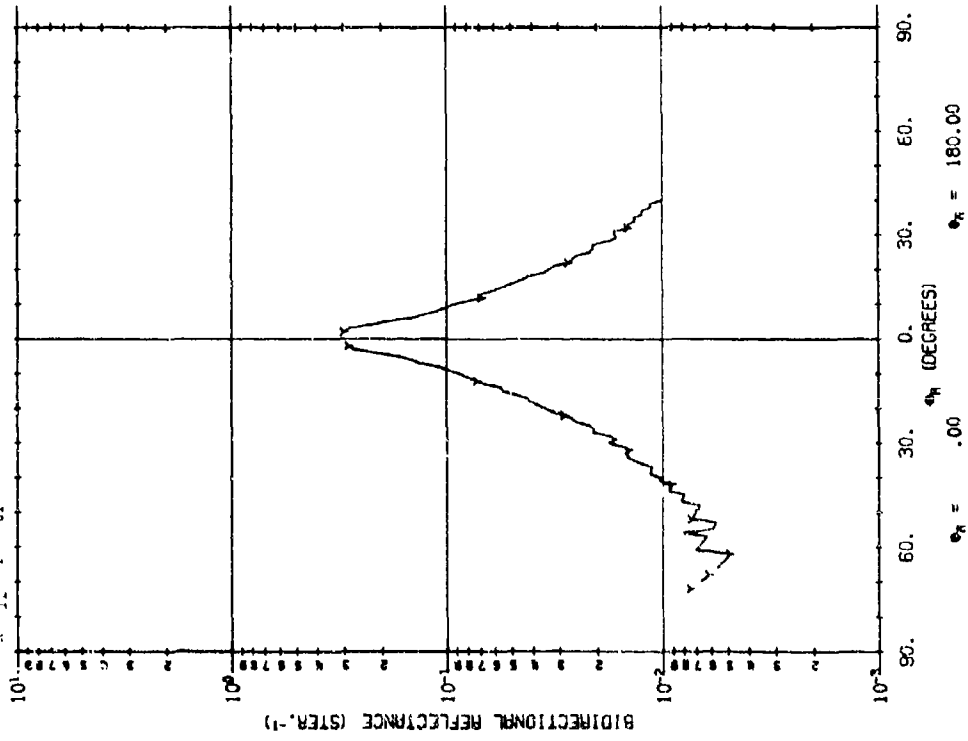


PAINT

R01892 301

Olive Drab Paint on Aluminum

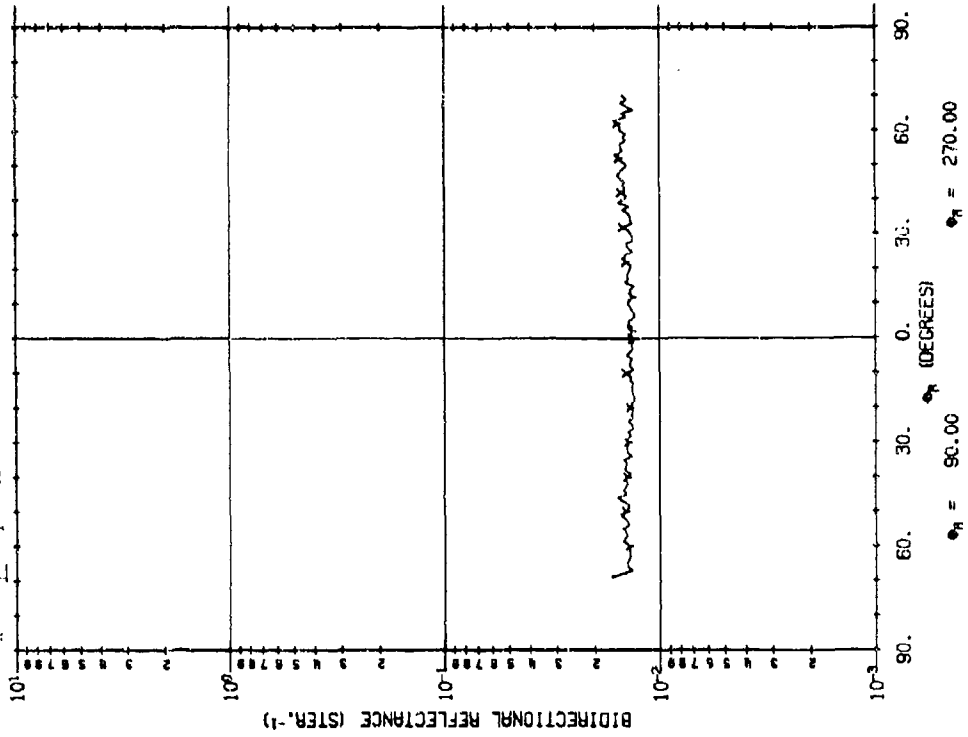
$\epsilon_1 = 0.0$
 $\epsilon_2 = 189.0$
 $\epsilon_3 = 10.6$
X Y = UT



R01897 101

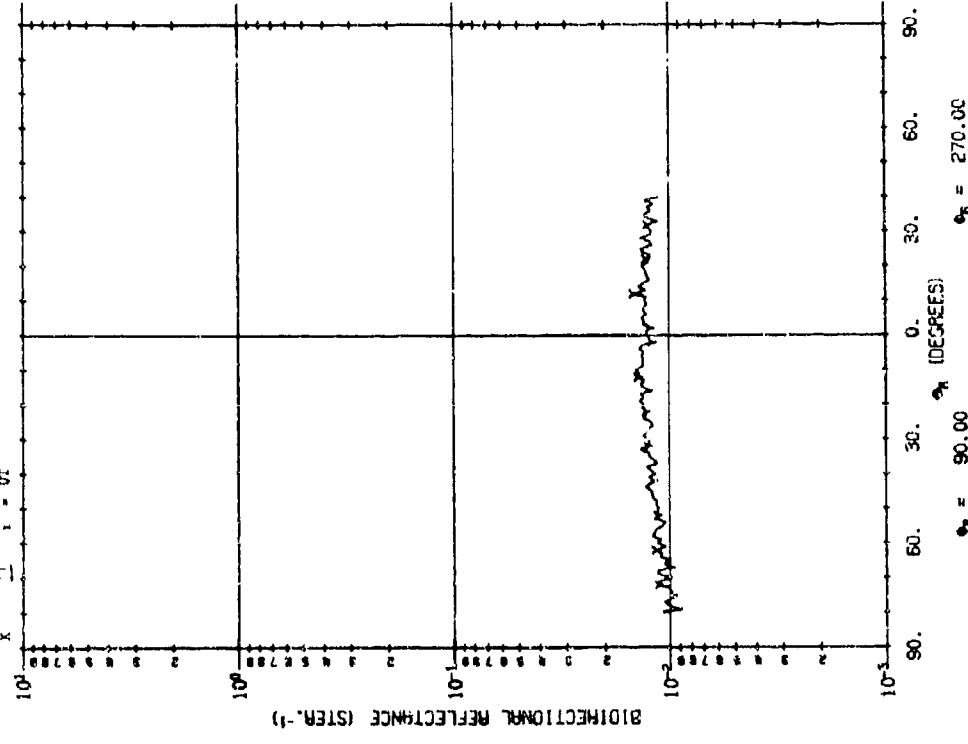
Two Coats 3M Black Paint on Plywood

$\epsilon_1 = 2.0$
 $\epsilon_2 = 1.0$
 $\epsilon_3 = 10.6$
X Y = UT



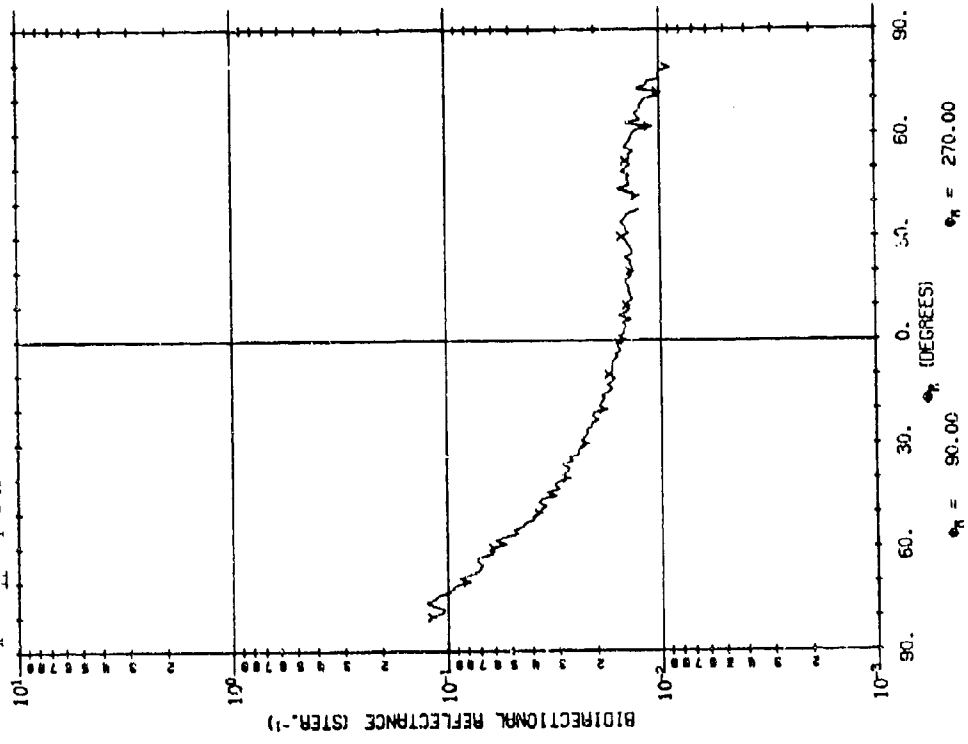
RC1897 101
Two Coats 3M Black Paint on Plywood

$\epsilon_1 = 0.0$
 $\epsilon_2 = 270.0$
 $\lambda = 10.6$
 $\chi = VT$



RC1897 101
Two Coats 2M Black Paint on Plywood

$\epsilon_1 = 40.0$
 $\epsilon_2 = 270.0$
 $\lambda = 10.6$
 $\chi = VT$

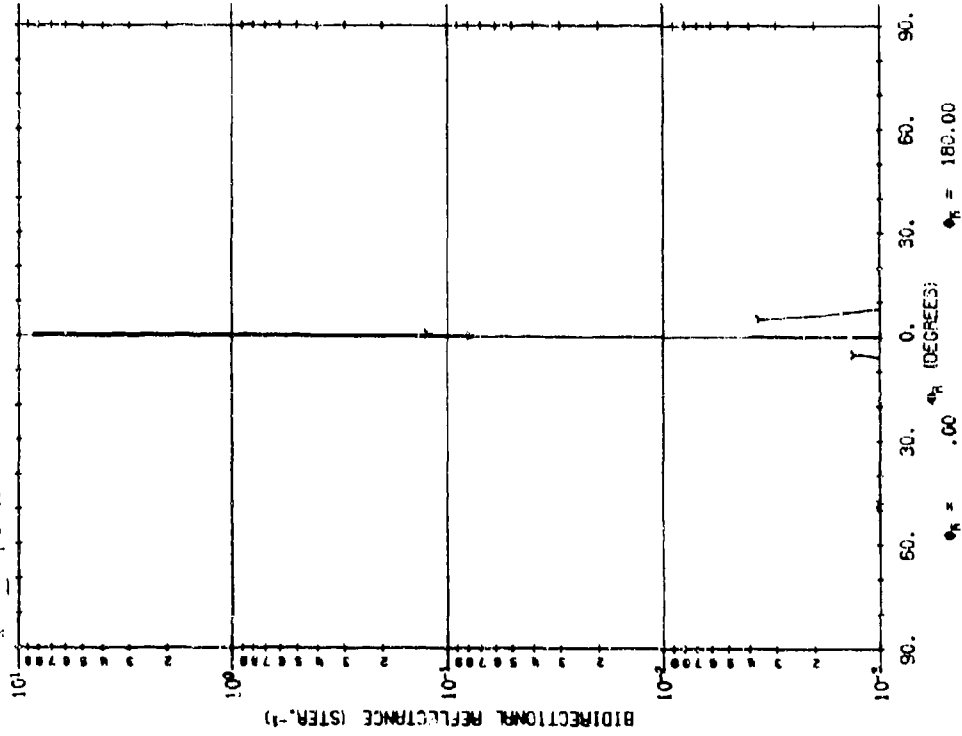


PAINT

R01917 101

OLIVE DRAB KEVLON PAINT ON ALUMINUM

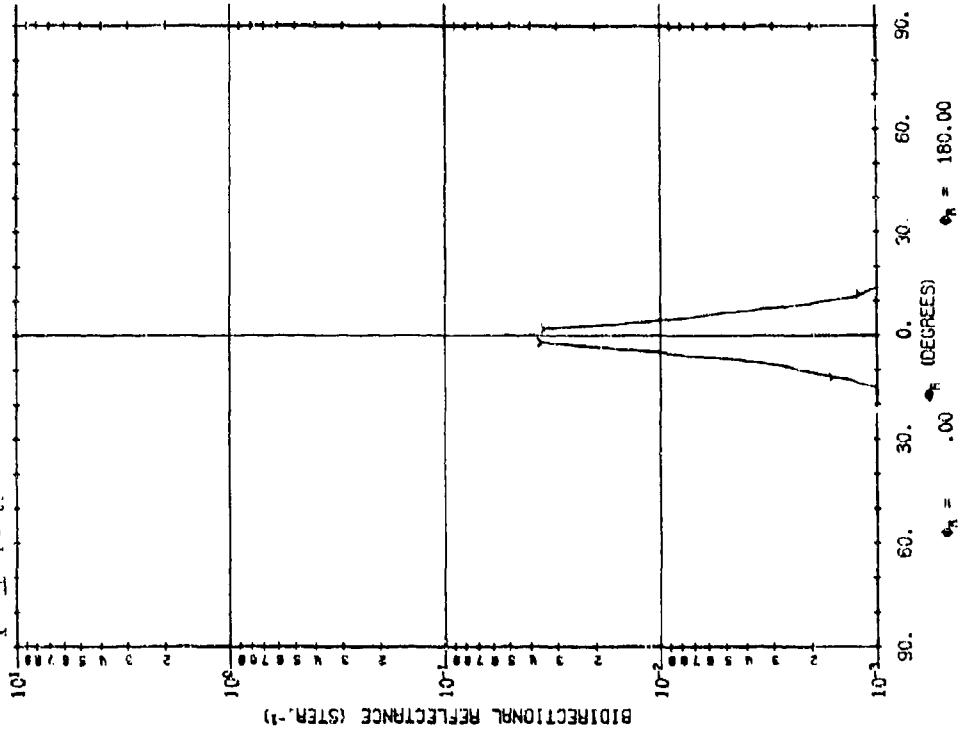
C 2F = 2.0
+ 1 = 1.0
- 2 = 1.0
X 1 = 10.6
Y = UT



R01917 101

OLIVE DRAB KEVLON PAINT ON ALUMINUM

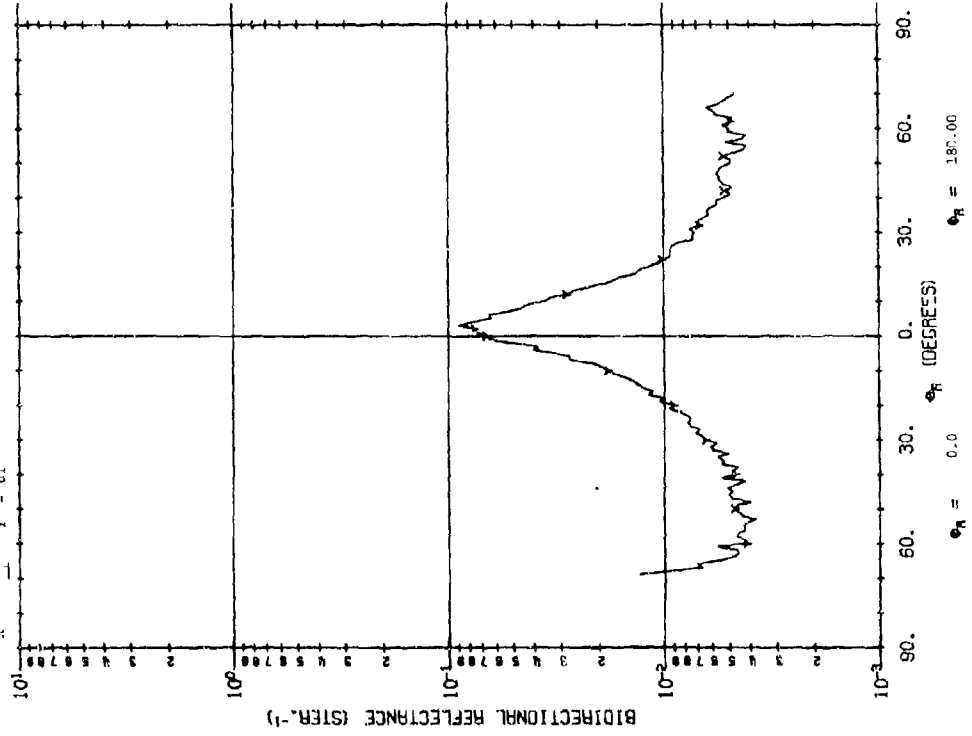
0 1 = 0.0
+ 1 = 183.0
- 1 = 10.6
X 1 = UT



A01920 101

Olive Drab Krylon Paint on Cork

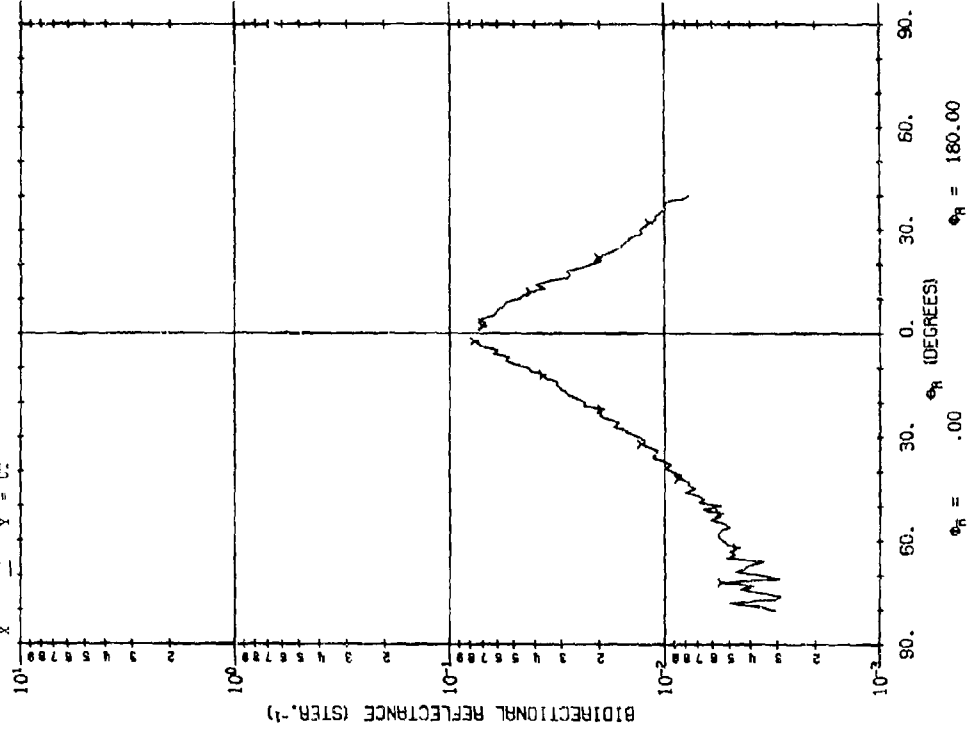
$2\theta = 2.0$
 $\phi_1 = \phi_2$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
 $Y = U^*$



A01920 101

Olive Drab Krylon Paint on Cork

$\phi_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
 $Y = U^*$

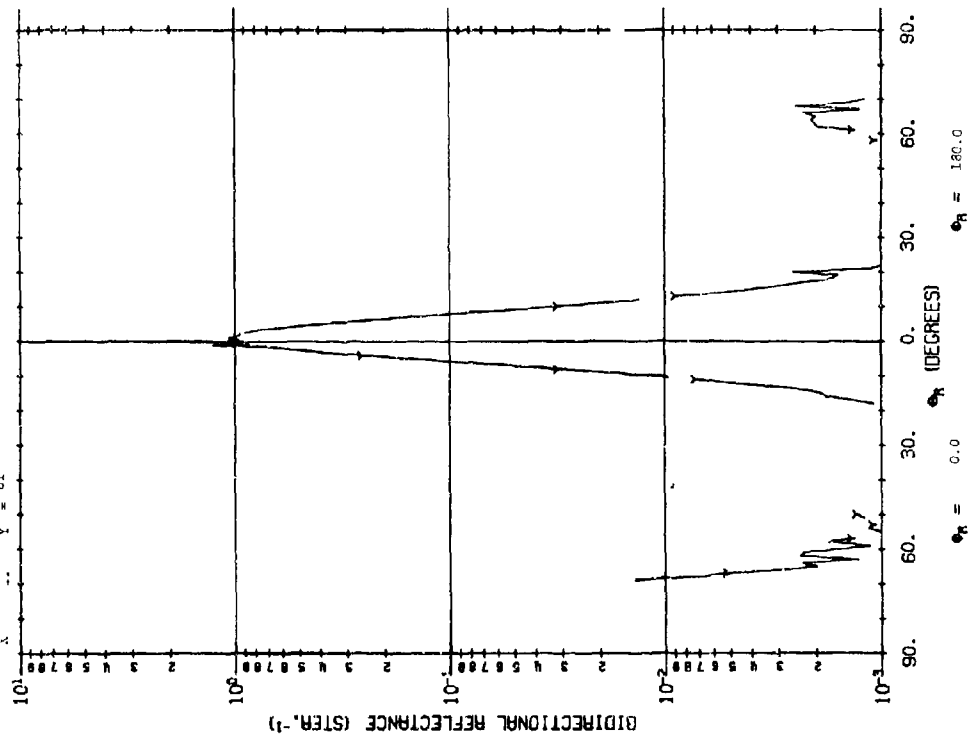


PAINT

R01922 101

Olive Drab Krylon Paint on
White Posterboard

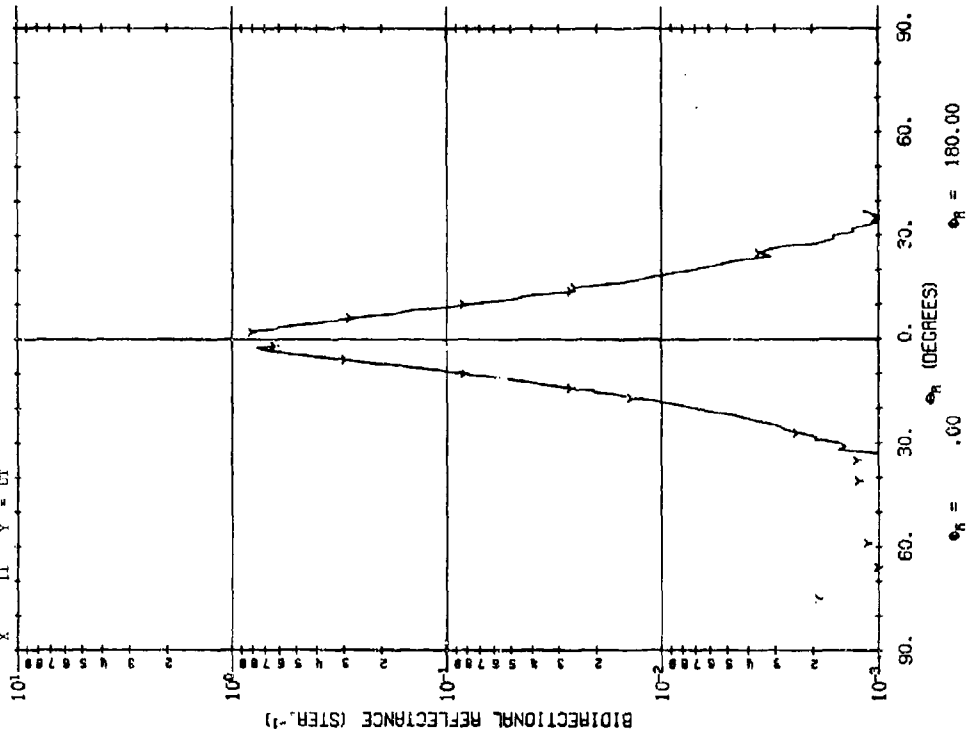
0 $\theta_i = 2.0$
+ $\theta_r = \theta_r$
- $\theta_i = 10.6$
X $\theta_r = \theta_r$



R01922 101

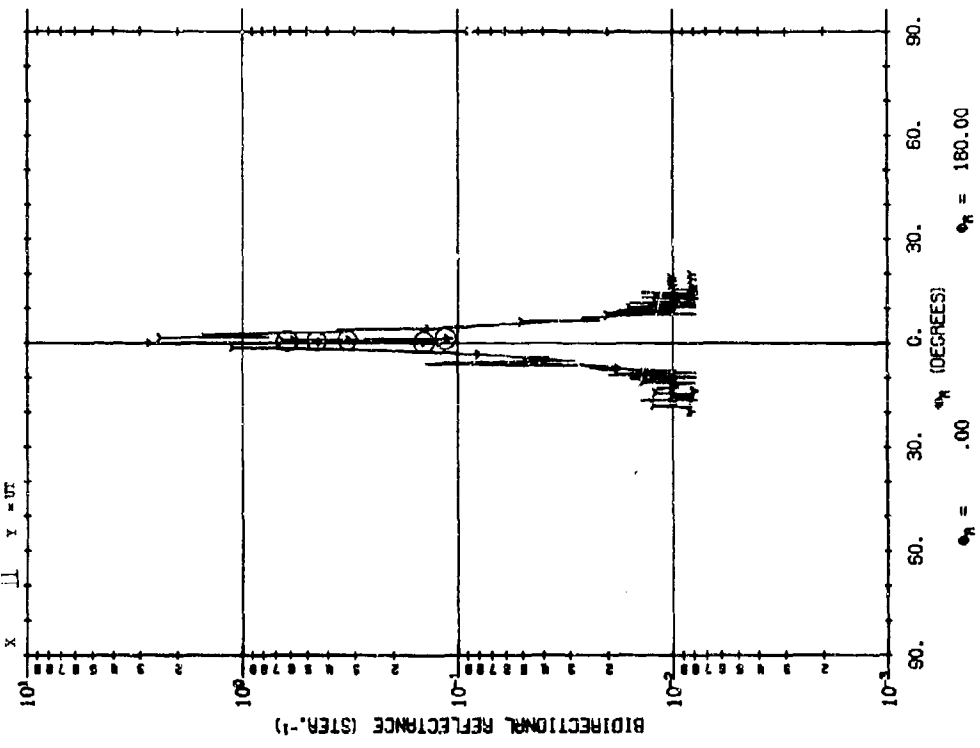
Olive Drab Krylon Paint on
White Posterboard

0 $\theta_i = 0.0$
+ $\theta_r = 180.0$
- $\theta_i = 10.6$
X $\theta_r = \theta_r$



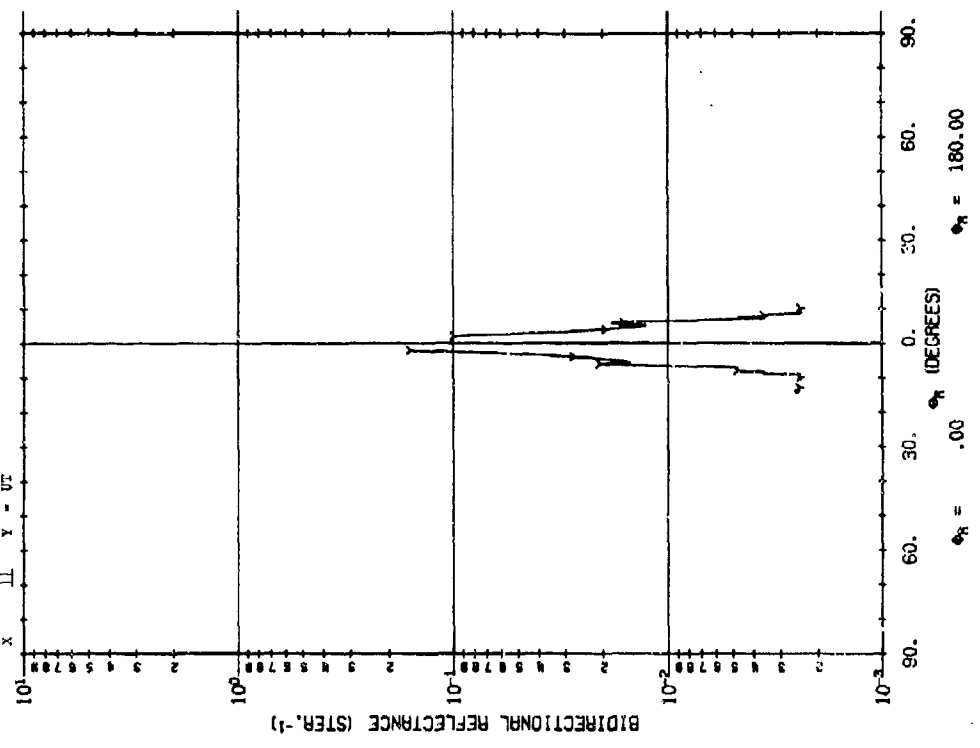
R01924 101
 0 28 = 2.0
 + 11 11 $\phi_1 = \phi_r$
 A 11 11 $\lambda = 10.6$
 X 11 11 Y = UT

Olive Drab Krylon Paint on
 Acrylic Plexiglass



R01924 101
 0 11 11 $\phi_1 = 0.0$
 + 11 11 $\phi_1 = 180.0$
 A 11 11 $\lambda = 10.6$
 X 11 11 Y = UT

Olive Drab Krylon Paint on
 Acrylic Plexiglass

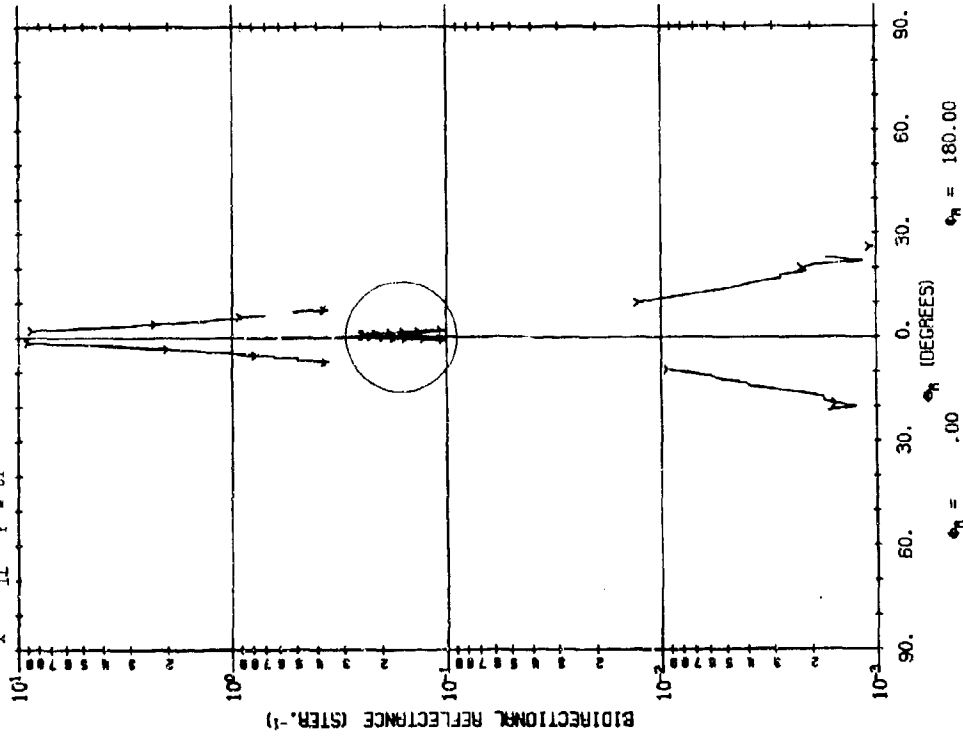


PAINT

A01926 101

Olive Drab Krylon Paint on Brown
Corrugated Cardboard

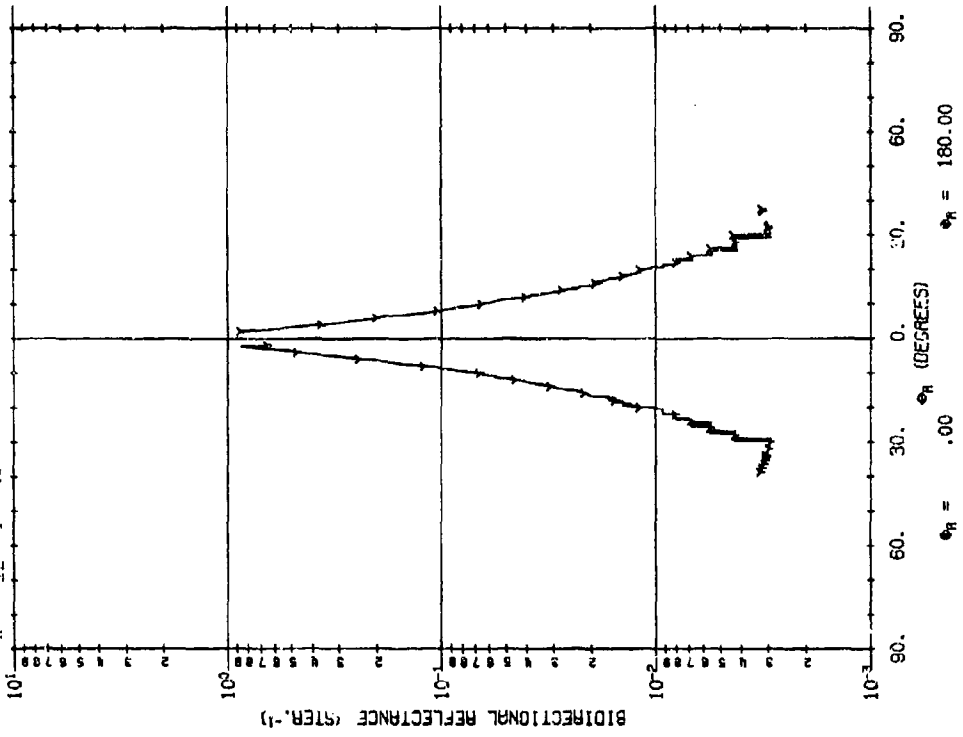
0 || 25 = 2.0
+ || 11 21 = 6
2 || 17 14 = 10.6
X || 11 Y = UT



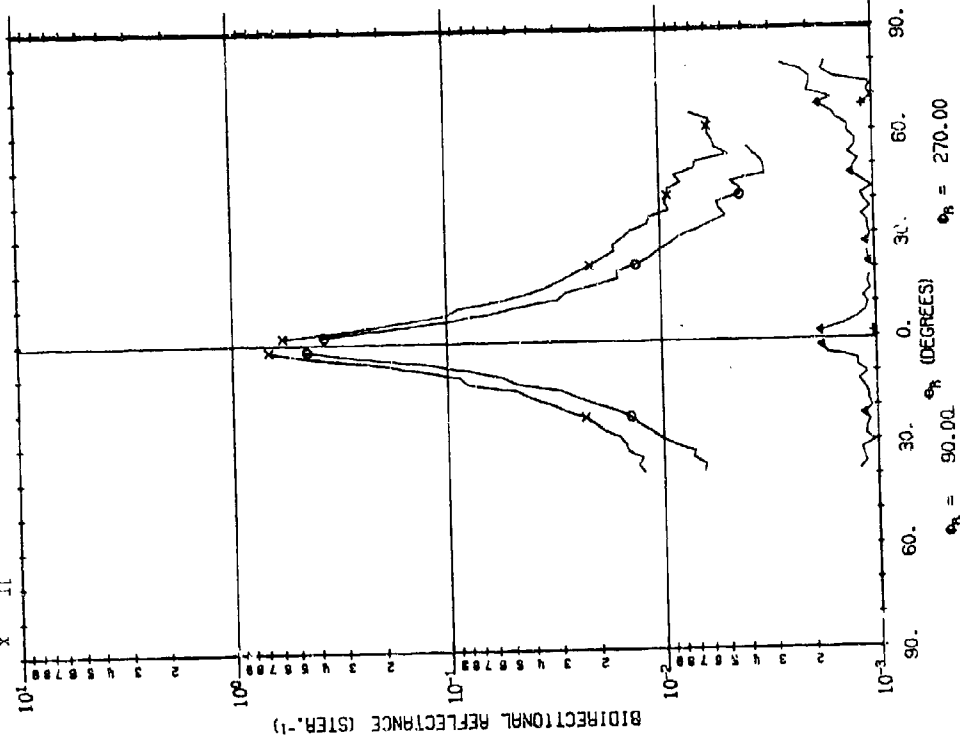
A01926 101

Olive Drab Krylon Paint on Brown
Corrugated Cardboard

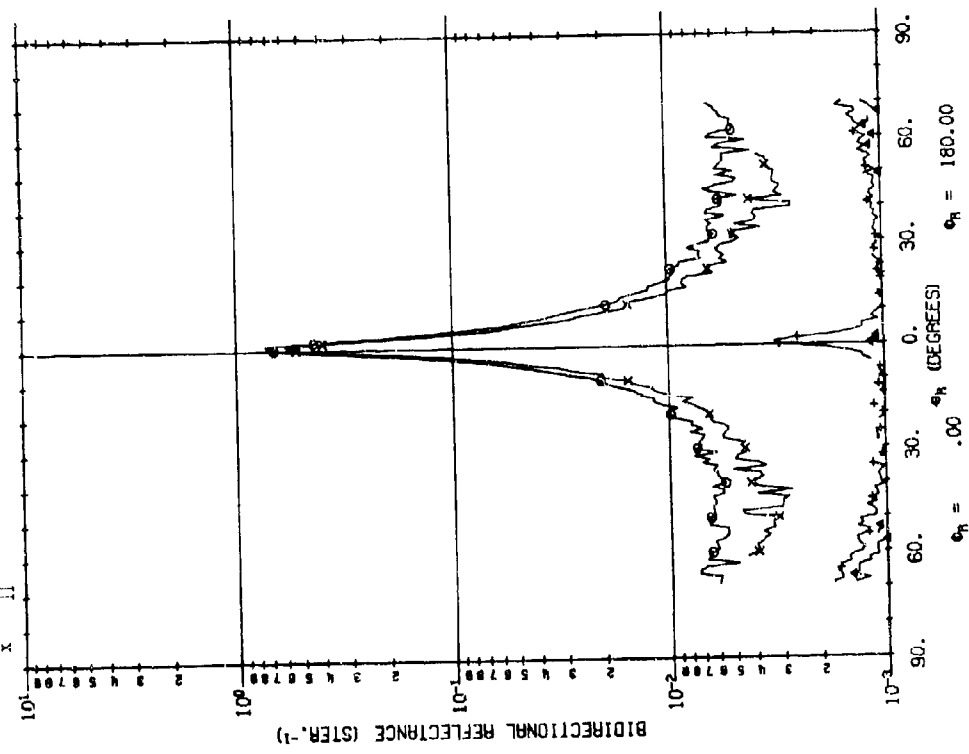
0 || 11 21 = 0.0
+ || 11 21 = 180.0
2 || 11 14 = 10.6
X || 11 Y = UT



R02001 101
 Olive Drab Paint on Steel
 $\theta_1 = 0.0$
 $\phi_1 = 90.0$
 $\lambda = 1.06$



R02001 101
 Olive Drab Paint on Steel
 $\theta_1 = 2.0$
 $\phi_1 = 90.0$
 $\lambda = 1.06$



PAINT

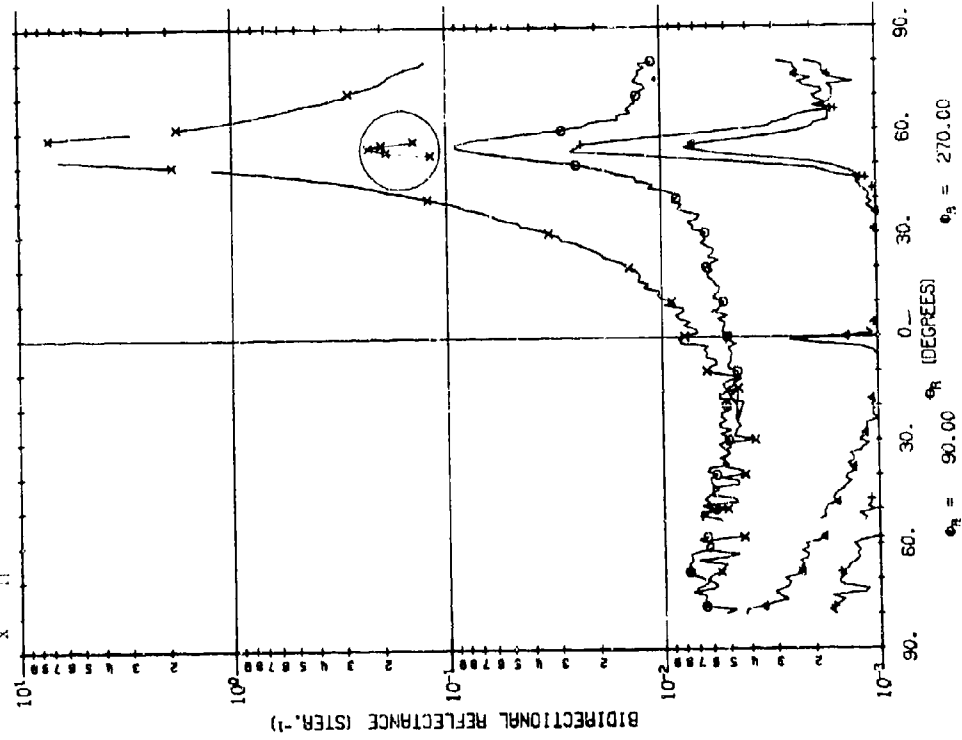
A02001

101

Olive Drab Paint on Steel

$\theta_i = 56.0$
 $\theta_r = 90.0$
 $\lambda = 1.06$

C || ||
+ || ||
- || ||
X || ||



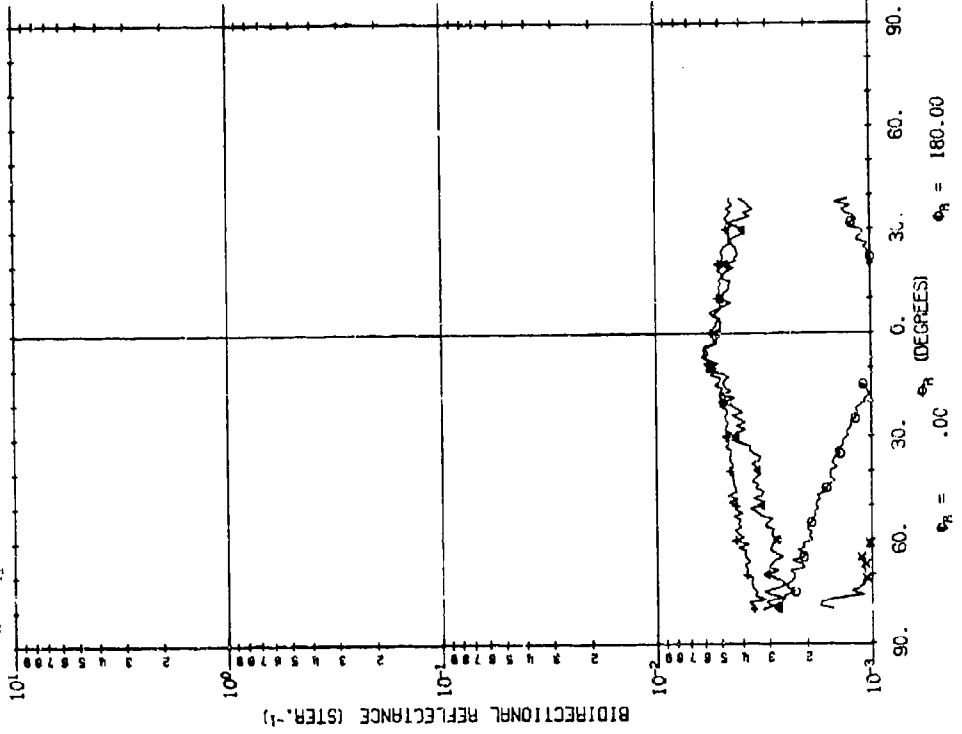
A02001

101

Olive Drab Paint on Steel

$\theta_i = 56.0$
 $\theta_r = 90.0$
 $\lambda = 1.06$

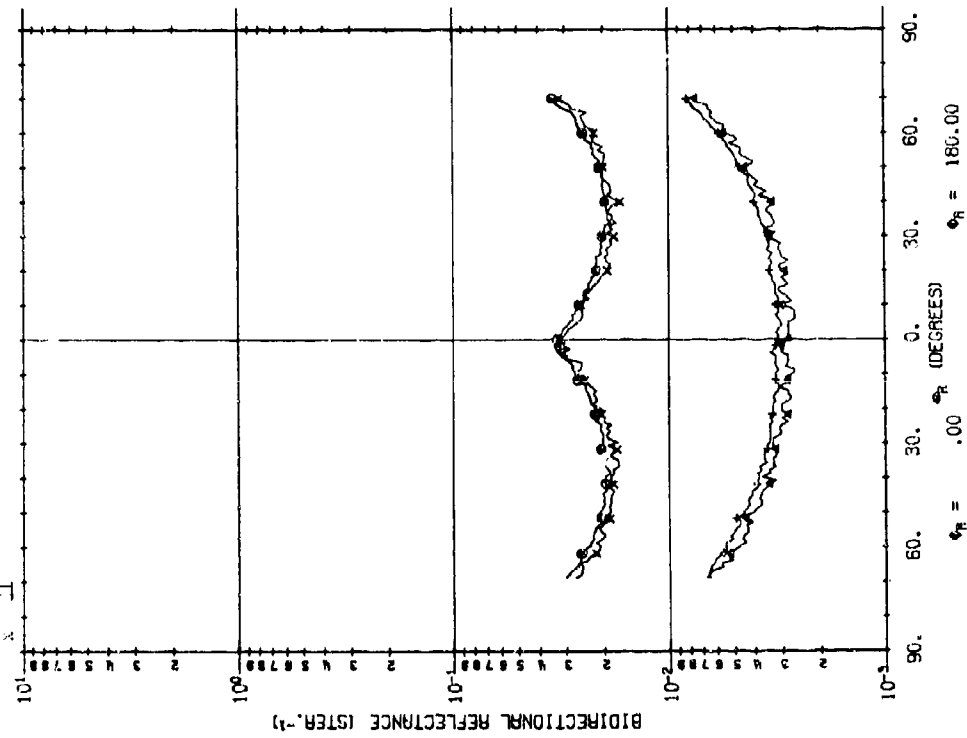
0 || ||
+ || ||
- || ||
X || ||



R02004 101

OLIVE DRAB PAINT ON STEEL

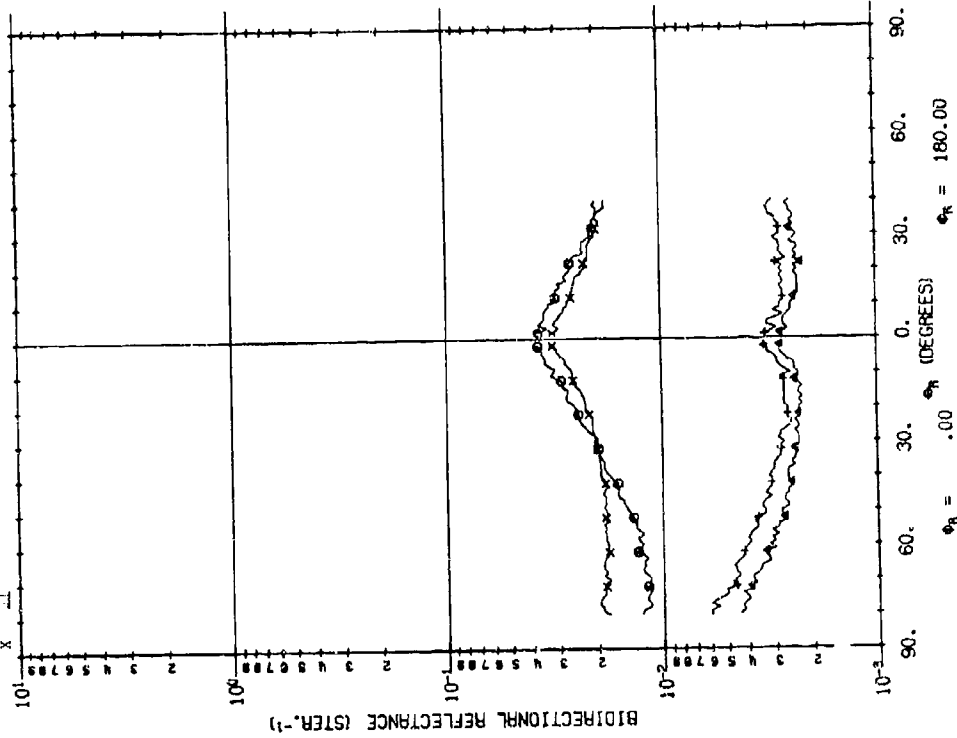
0 || $\theta_1 = 2.0$
+ || $\phi_1 = \phi_r$
Δ || $\lambda = 1.06$
X ||



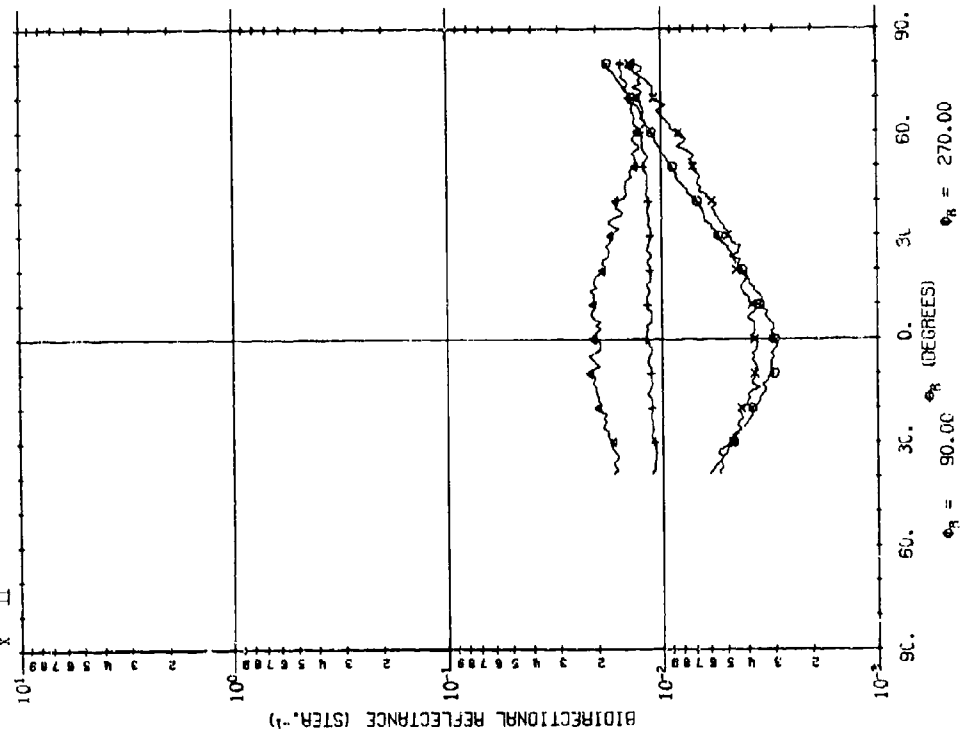
R02004 101

OLIVE DRAB PAINT ON STEEL

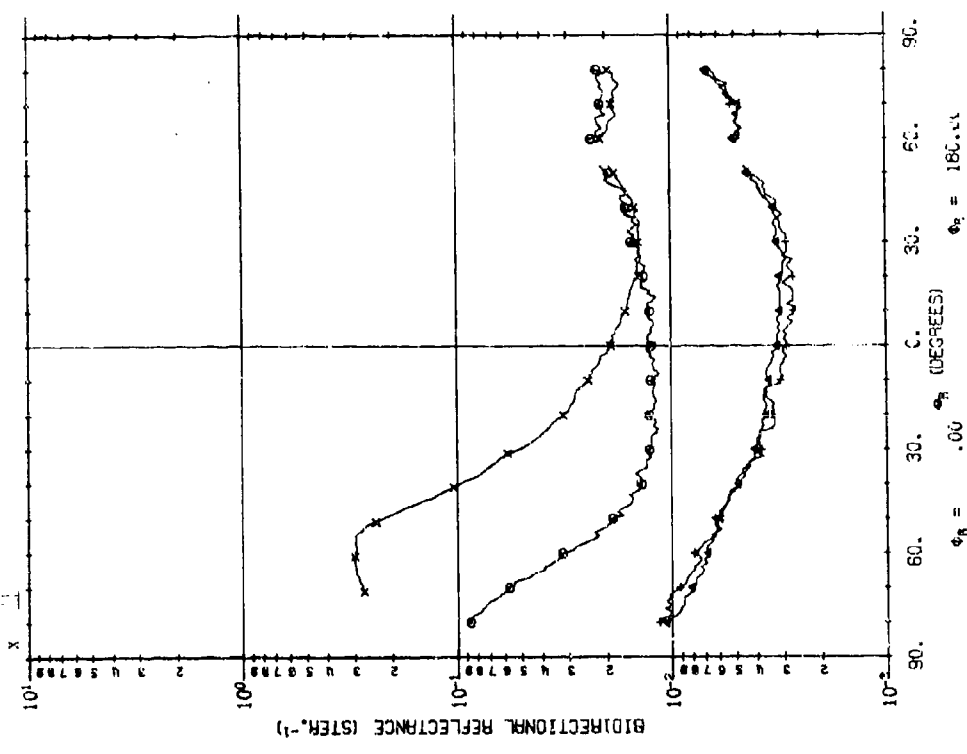
0 || $\theta_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 1.06$
X ||



R02004 101
 OLIVE DRAB PAINT ON STEEL
 $\epsilon_1 = 56.0$
 $\epsilon_2 = 180.0$
 $\lambda = 1.06$



R02004 101
 OLIVE DRAB PAINT ON STEEL
 $\epsilon_1 = 56.0$
 $\epsilon_2 = 180.0$
 $\lambda = 1.06$

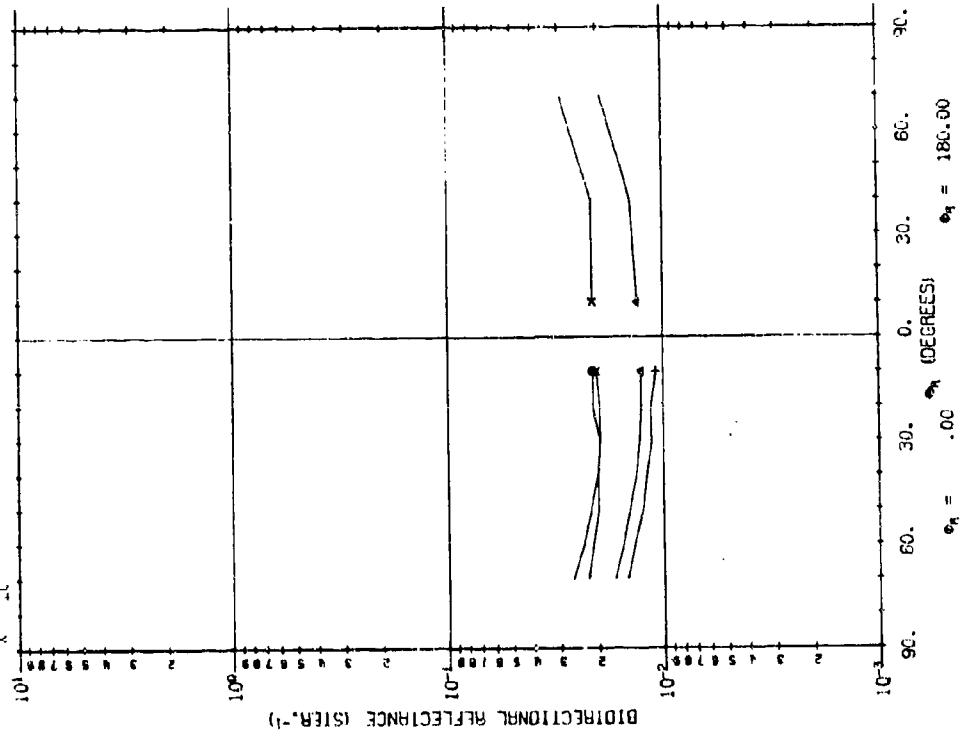


CLOTH AND CANVAS

R01013 007

BLUE GRAY COTTON

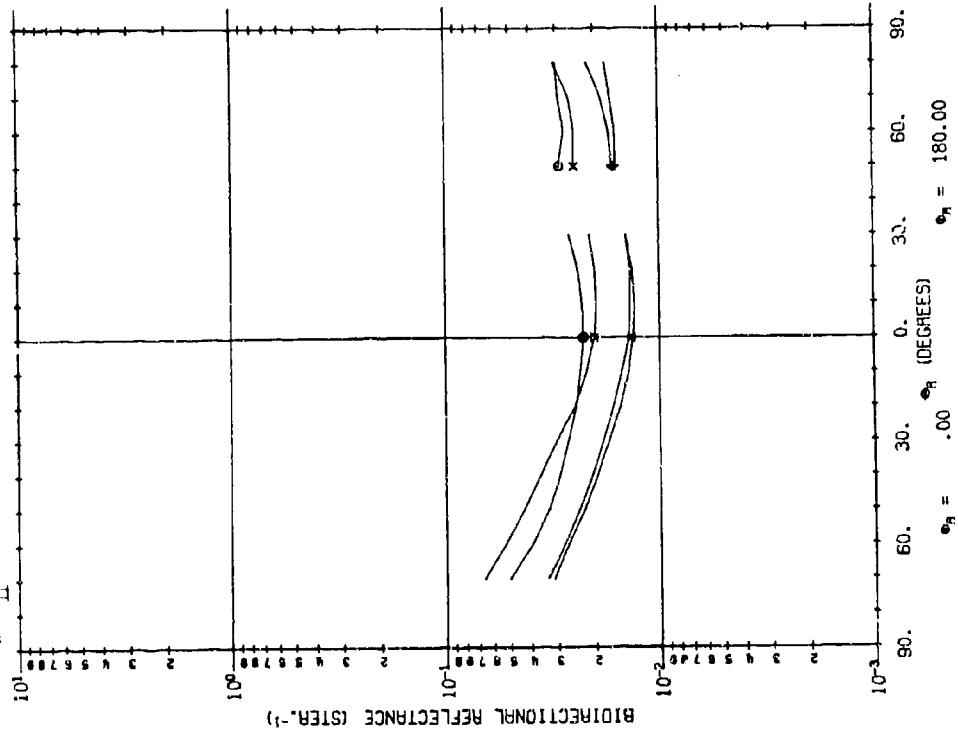
0 | | $\epsilon_1 = 0.0$
+ | | $\epsilon_2 = 180.0$
- | | $\lambda = 0.63$
x | |



R01013 007

BLUE GRAY COTTON

0 | | $\epsilon_1 = 40.0$
+ | | $\epsilon_2 = 180.0$
- | | $\lambda = 0.63$
x | |

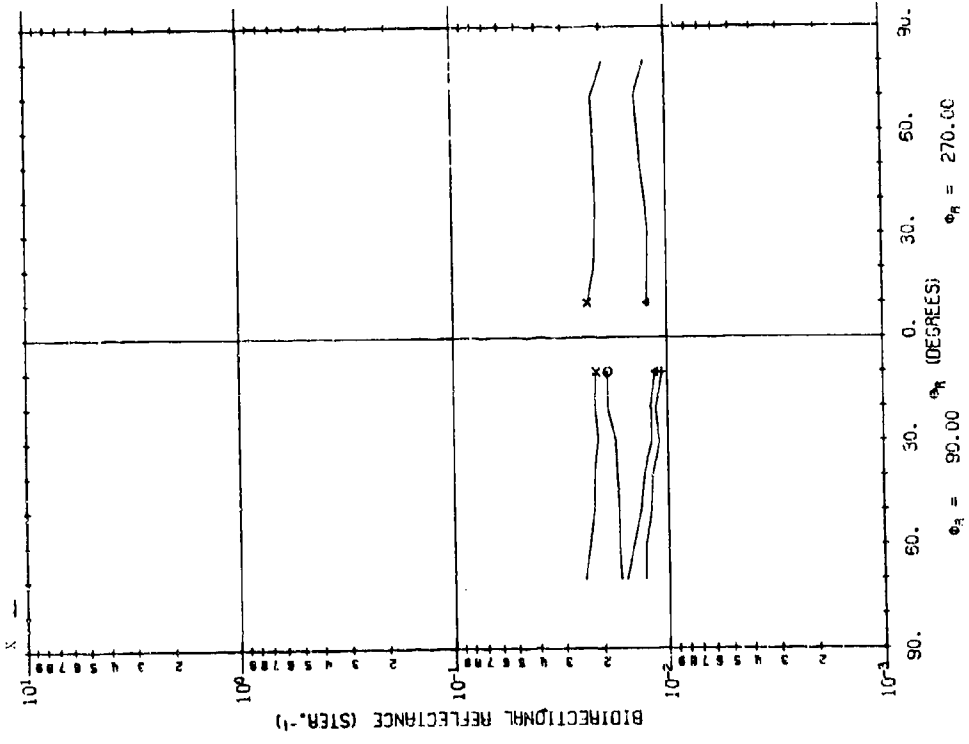


CLOTH AND CANVAS

AG1013 007

BLUE GRAY COTTON

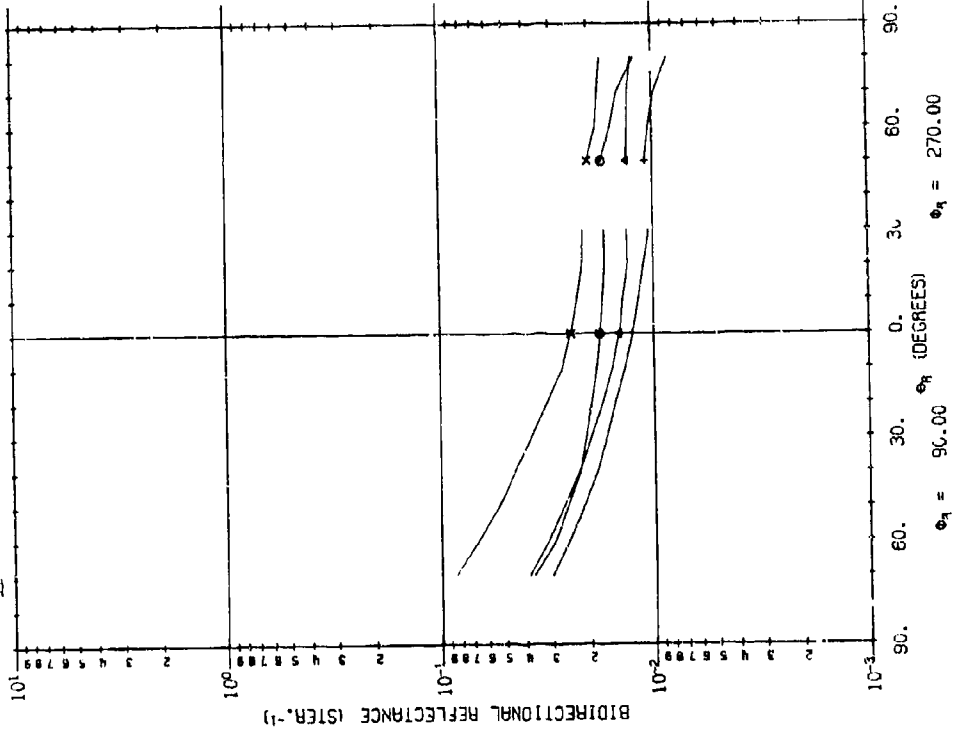
$\lambda_1 = 0.0$
 $\lambda_2 = 270.0$
 $\lambda_3 = 0.53$



AG1013 007

BLUE GRAY COTTON

$\lambda_1 = 40.0$
 $\lambda_2 = 270.0$
 $\lambda_3 = 0.53$



R01057 014

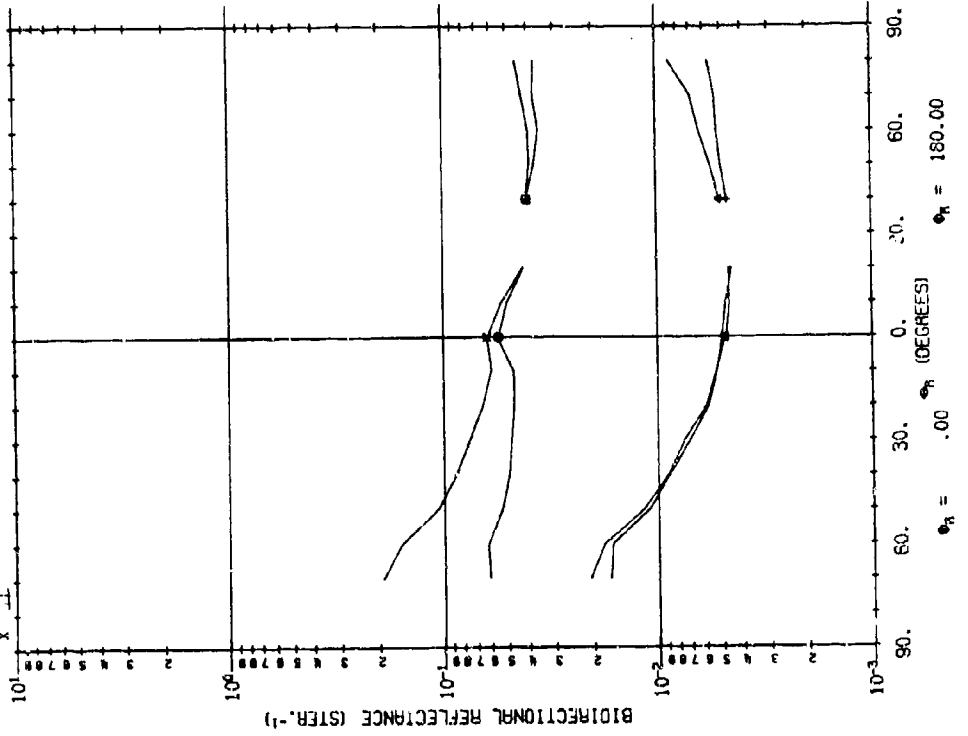
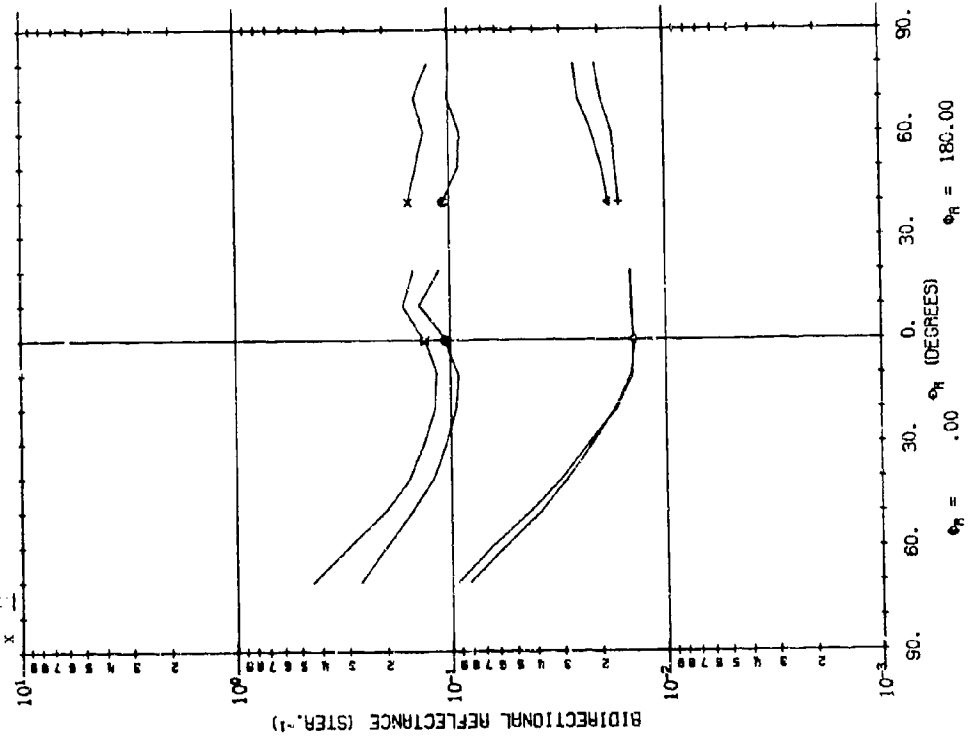
WHITE NYLON, PLAIN WEAVE, RIB STOP
PATTERN

$f_1 = 30.0$
 $f_2 = 180.0$
 $f_3 = 0.63$

R01058 014

OLIVE GREEN NYLON, PLAIN WEAVE, RIB
STOP PATTERN

$f_1 = 30.0$
 $f_2 = 180.0$
 $f_3 = 0.63$

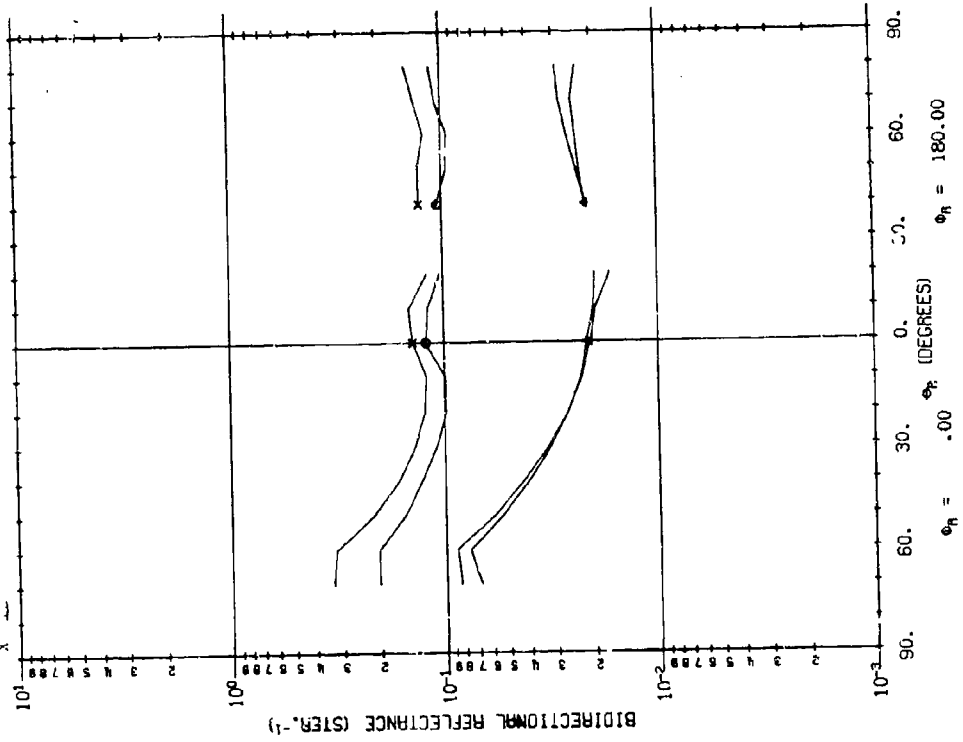


CLOTH AND CANVAS

A01059 015

ORANGE NYLON, PLAIN WEAVE, RIB STOP
PATTERN, FOUR LAYERS OVER SYCAMORE
LEAVES

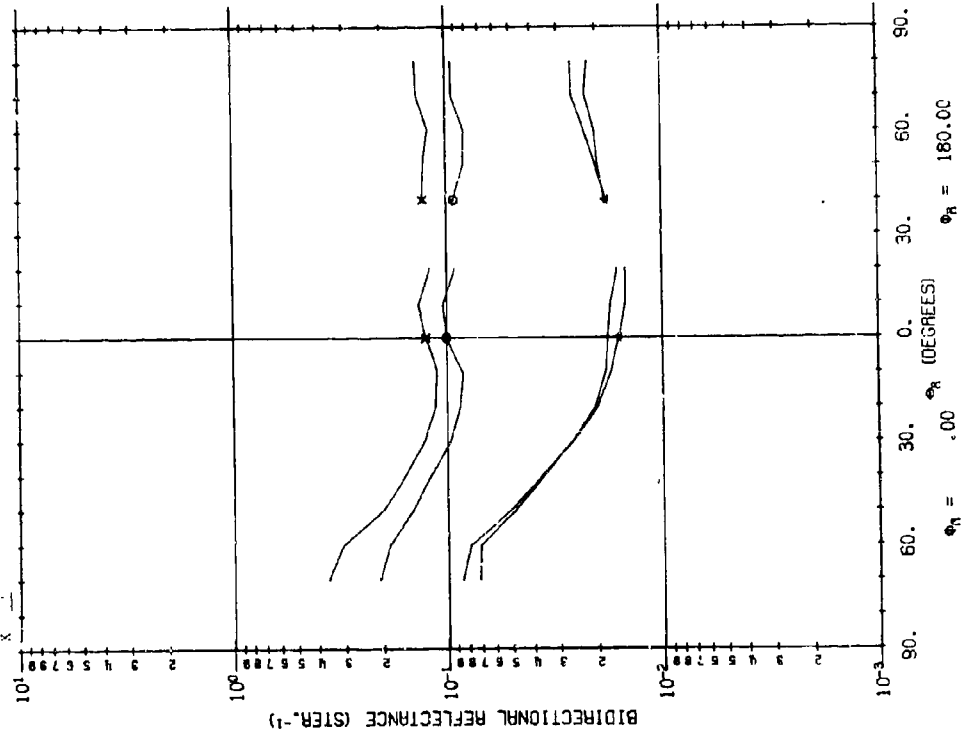
$\lambda_1 = 30.0$
 $\lambda_2 = 180.0$
 $\lambda = 0.63$



A01059 014

ORANGE NYLON, PLAIN WEAVE, RIB STOP
PATTERN

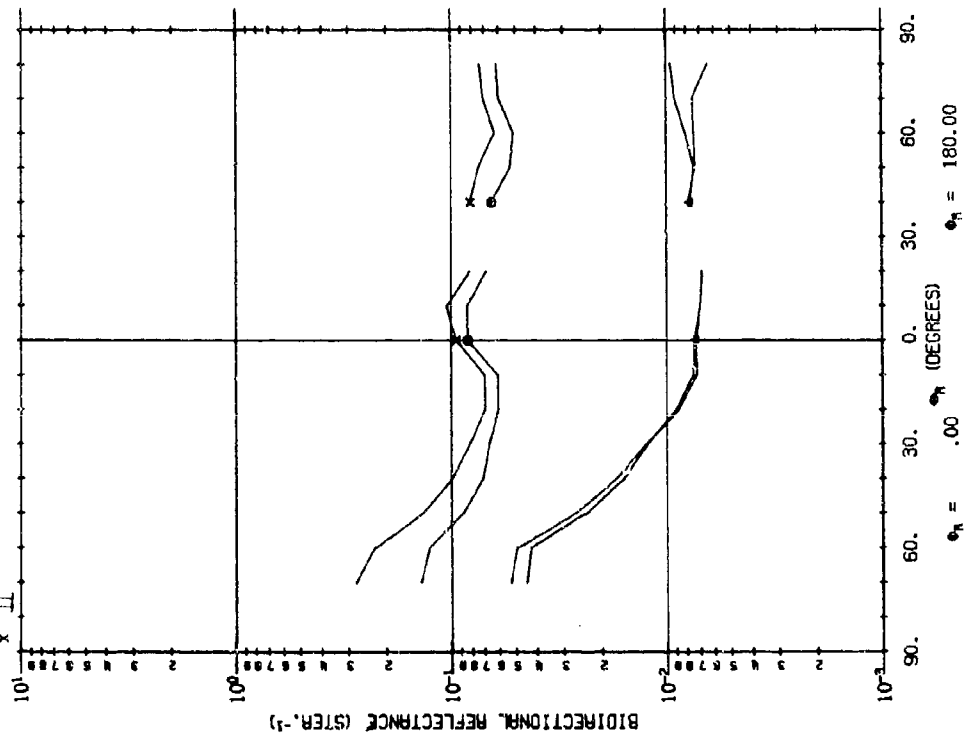
$\lambda_1 = 30.0$
 $\lambda_2 = 180.0$
 $\lambda = 0.63$



A01060 U14

SAND (BEIGE) NYLON, PLAIN WEAVE, RIB
STOP PATTERN

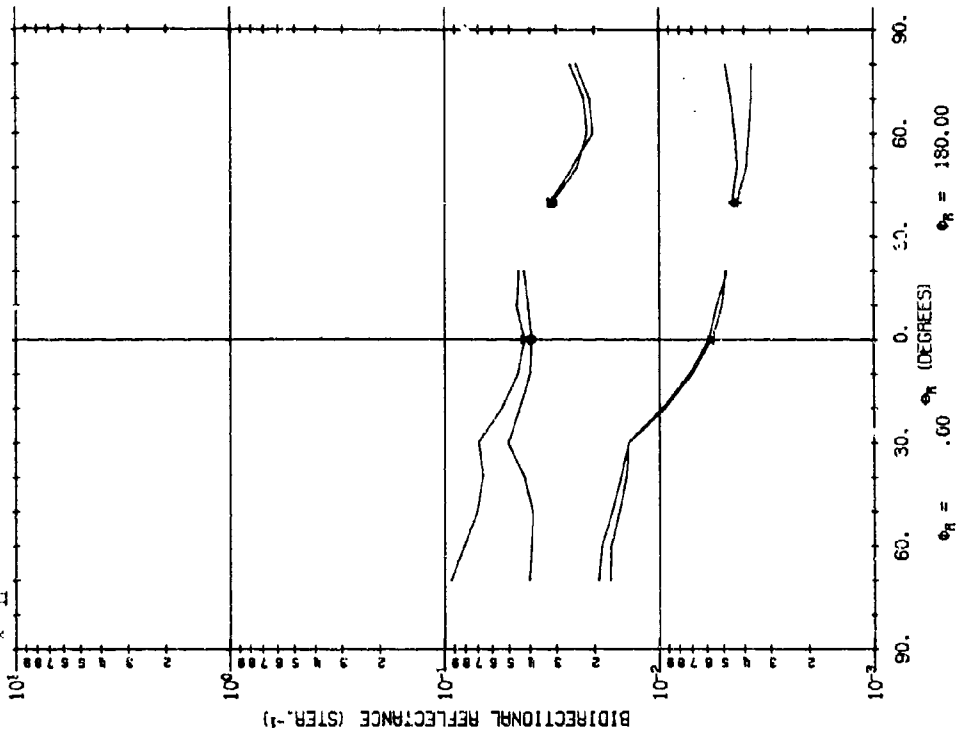
0 || $\theta_1 = 30.0$
+ || $\theta_1 = 180.0$
Δ || $\lambda = 0.63$
x ||



A01061 014

OLIVE GREEN NYLON, DOBBY WEAVE

0 || $\theta_1 = 30.0$
+ || $\theta_1 = 150.0$
Δ || $\lambda = 0.63$
x ||



CLOTH AND CANVAS

R01096 72

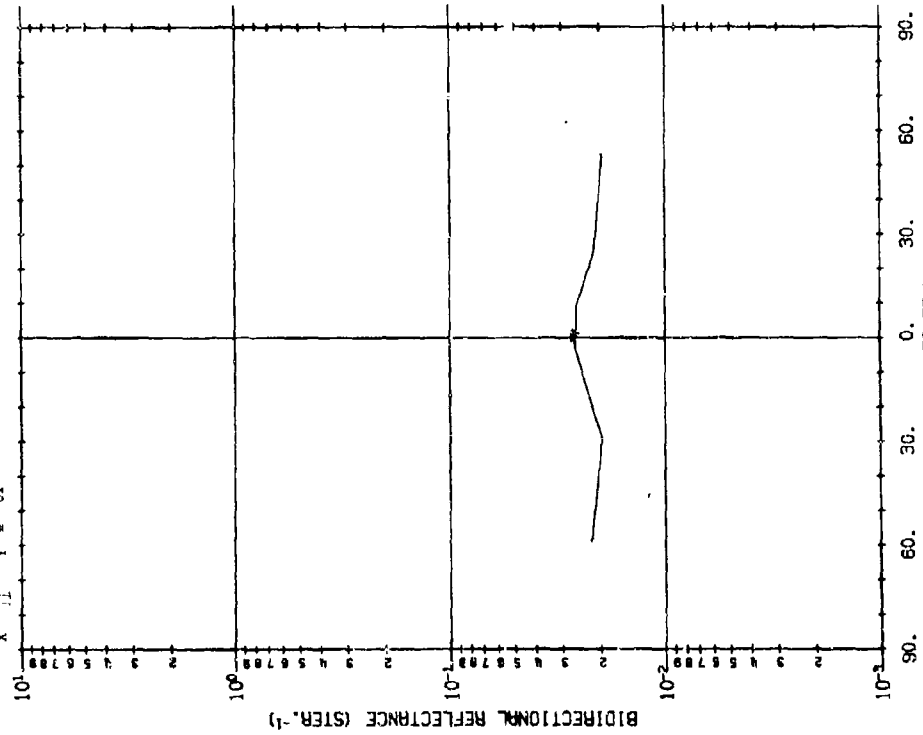
Green Canvas

0 || $\epsilon_1 = 1.10$

+ || $\epsilon_2 = \epsilon_1$

- || $\epsilon_3 = 10.6$

X || Y = 0T



$\phi_n = .00$ $\phi_n = 180.00$

R01096 002

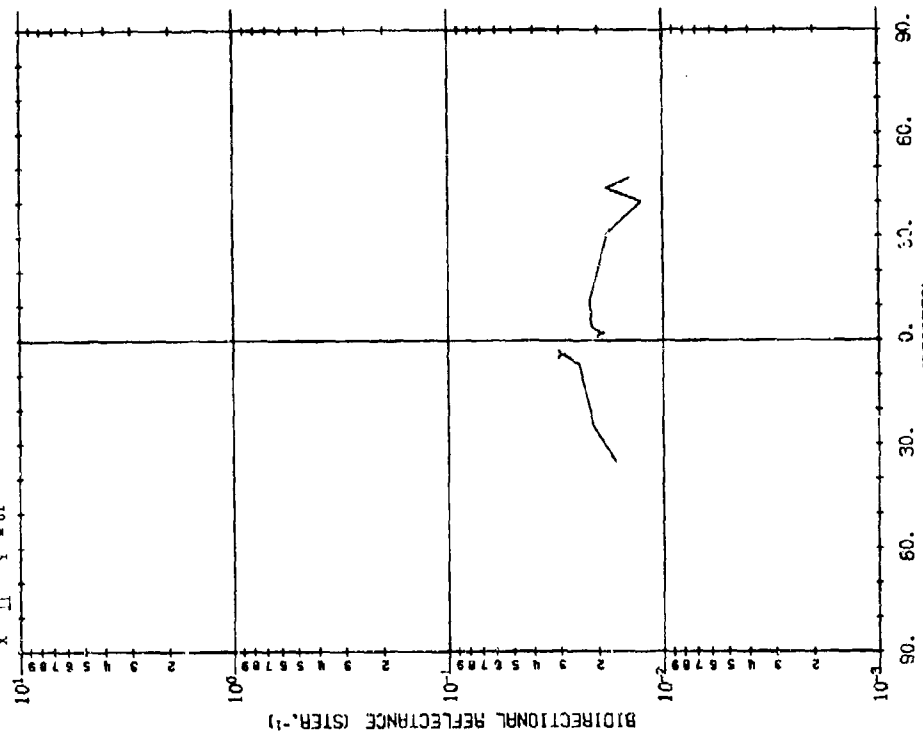
Green Canvas

0 || $\epsilon_1 = 0.0$

+ || $\epsilon_2 = 180.0$

- || $\epsilon_3 = 10.6$

X || Y = 0T

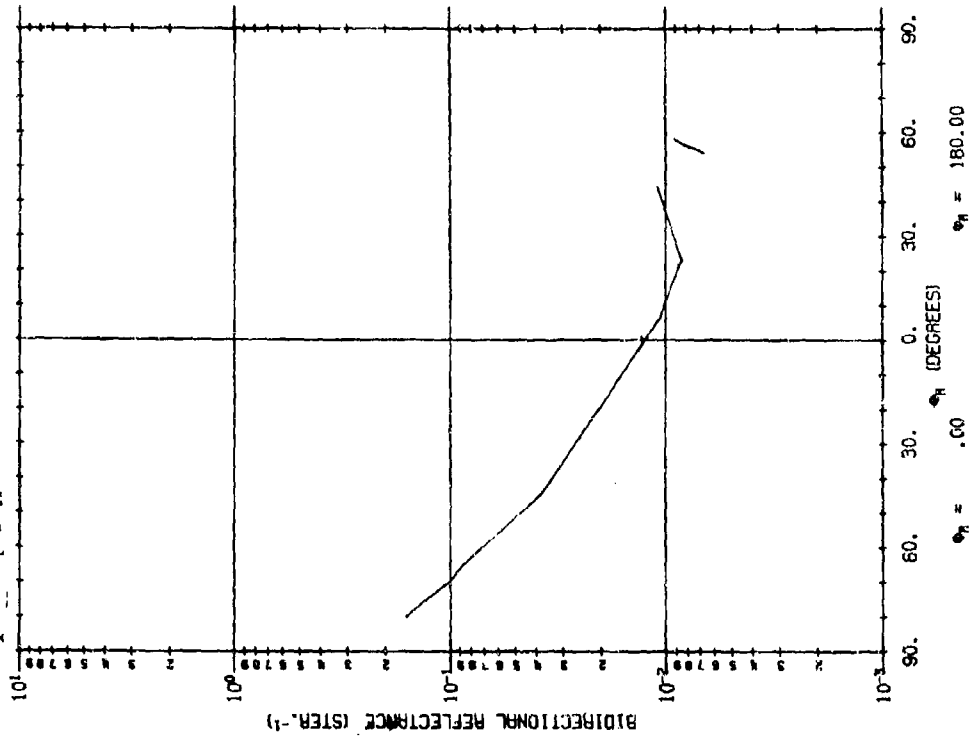


$\phi_n = .00$ $\phi_n = 180.00$

A01096 002

Green Canvas

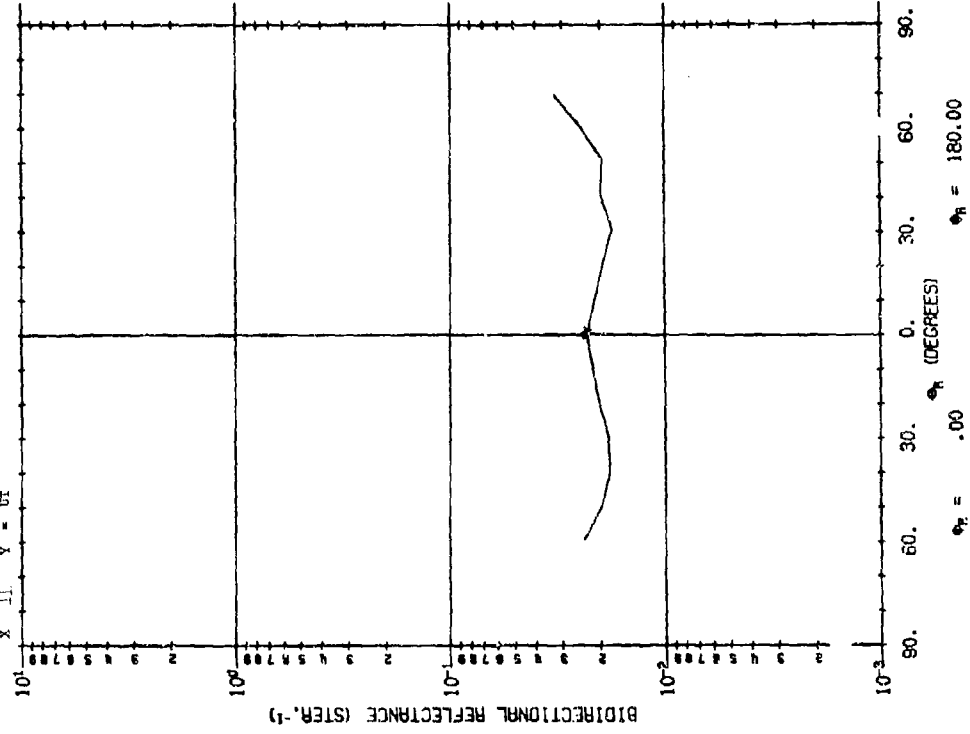
0 || $\rho_1 = 50.00$
+ || $\phi_1 = 180.0$
L || $\lambda = 10.6$
X || Y = 5T



A01099 002

White Canvas

0 || $\rho_1 = 1.10$
+ || $\phi_1 = 47$
L || $\lambda = 10.6$
X || Y = 5T

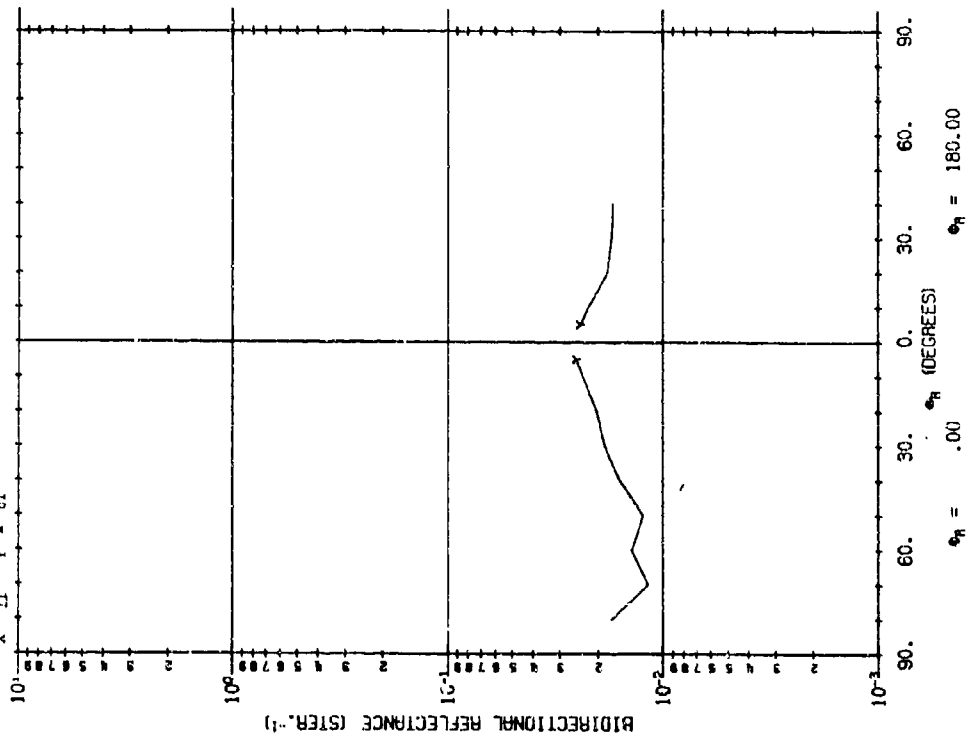


CLOTH AND CANVAS

R01099 002

White Canvas

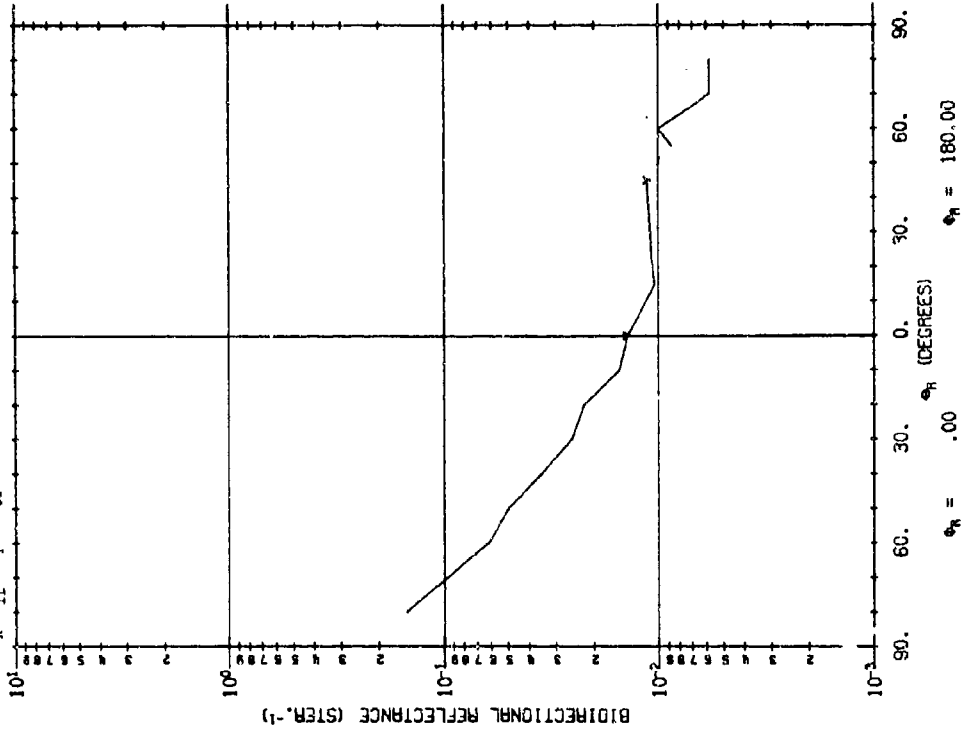
0 || $\phi_4 = 0.0$
+ || $\phi_1 = 180.0$
2 || $\lambda = 10.6$
X || Y = UT



R01099 002

White Canvas

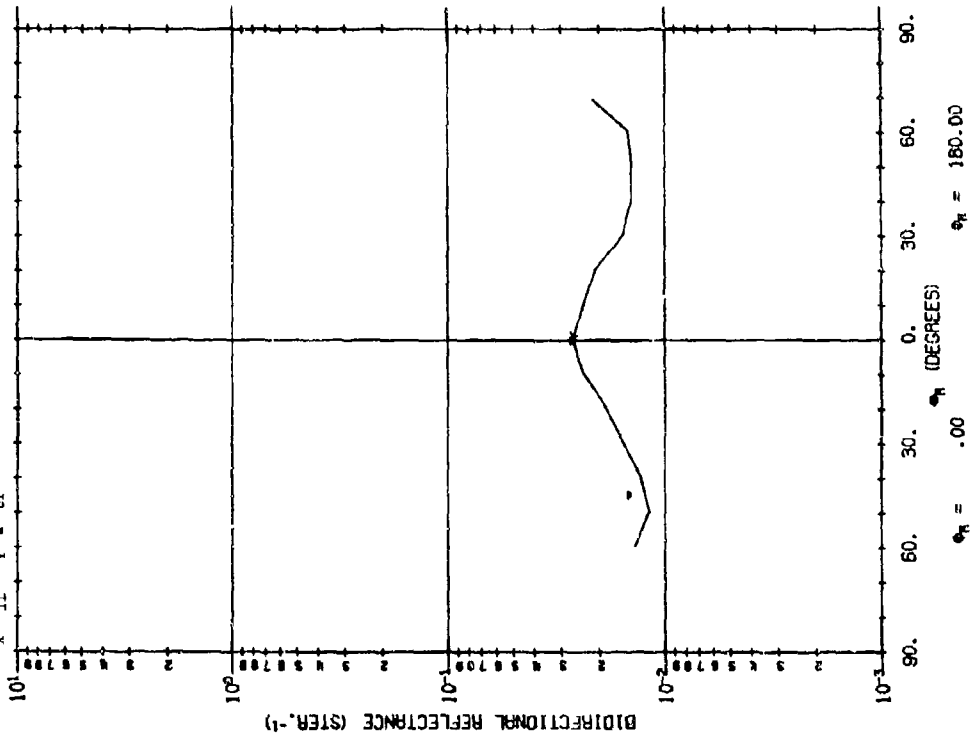
0 || $\phi_4 = 50.0$
+ || $\phi_1 = 180.0$
2 || $\lambda = 10.6$
X || Y = UT



R01103 002

Black Canvas

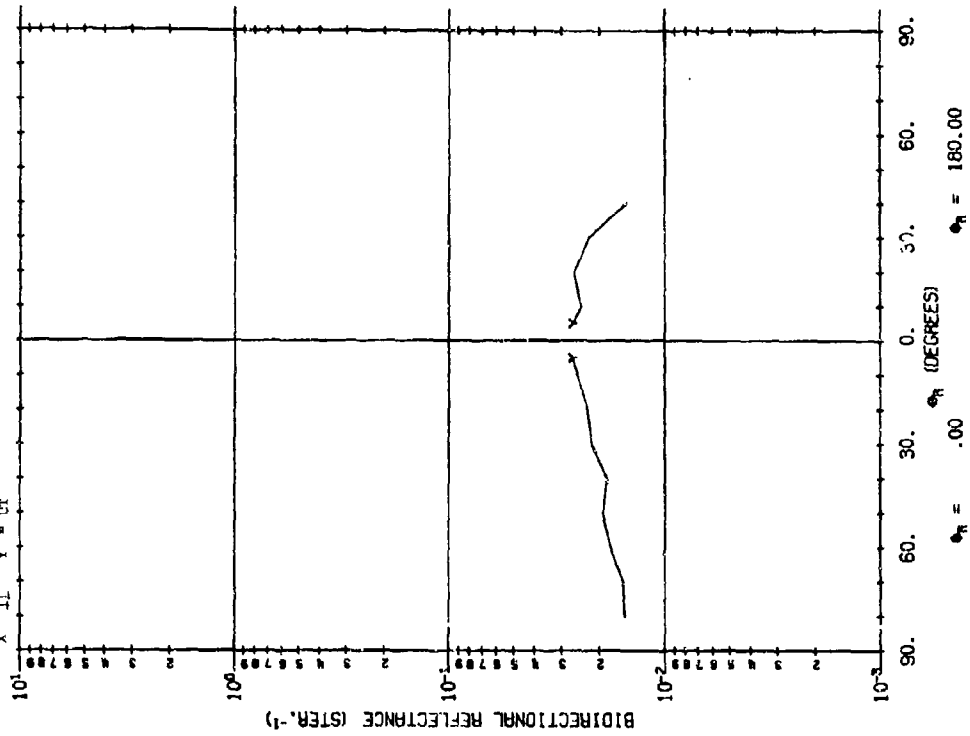
0 // 2₃ = 1.10
+ // ϕ_1 = ϕ_2
△ // λ = 10.6
x // Y = UT



R01103 002

Black Canvas

0 // ϕ_1 = 0.0
+ // ϕ_2 = 180.0
△ // λ = 10.6
x // Y = UT

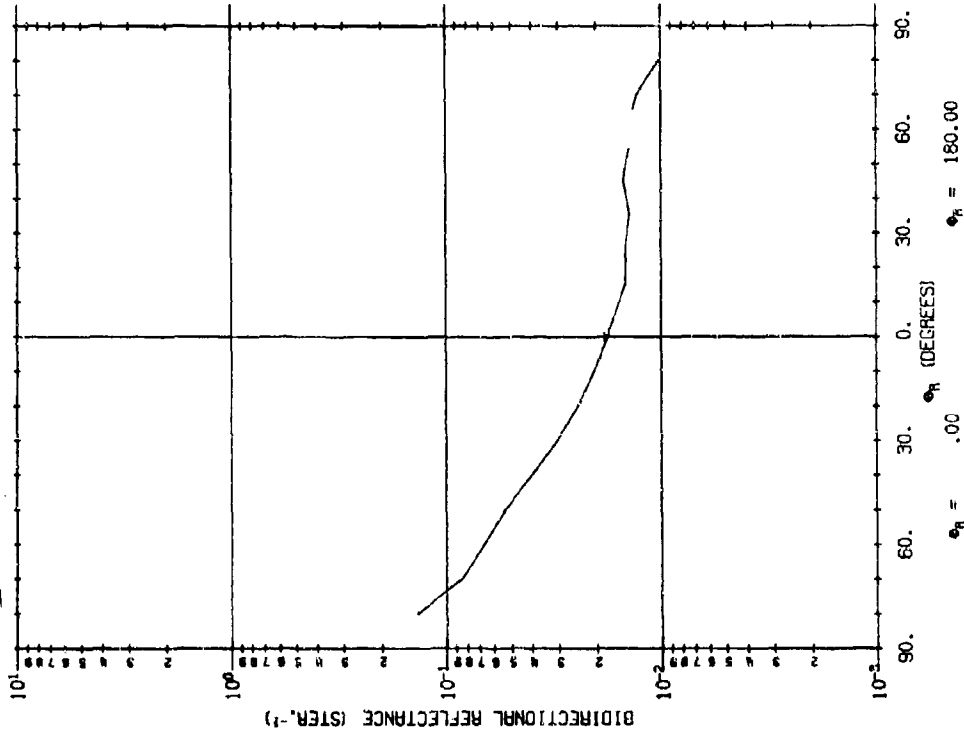


CLOTH AND CANVAS

A01103 002

Black Canvas

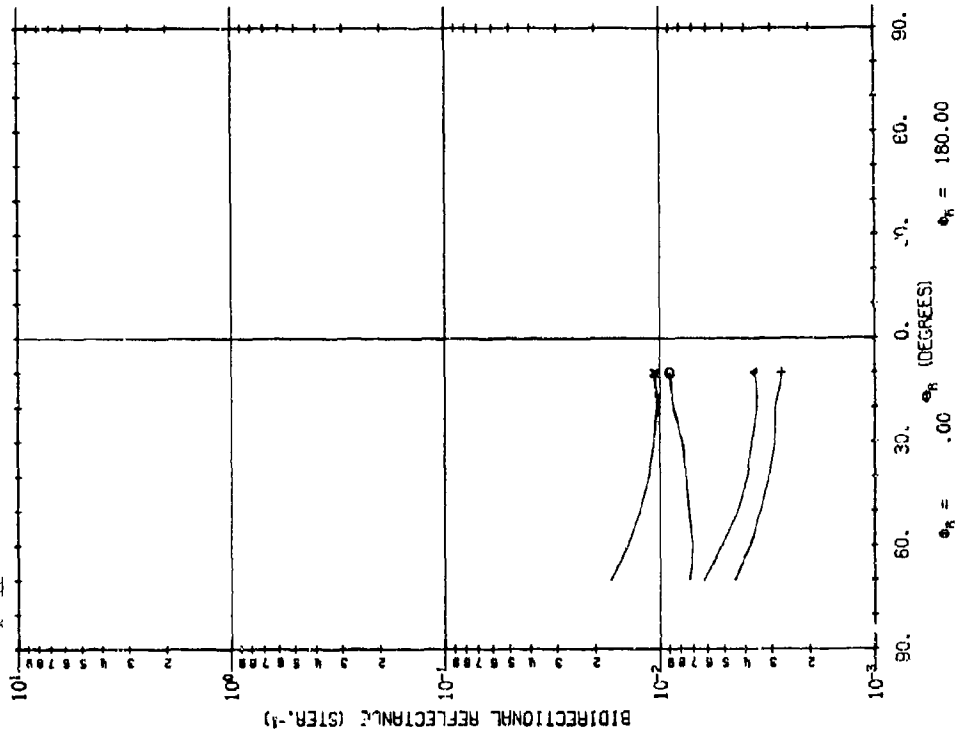
0 || $\theta_1 = 50.0$
+ || $\theta_1 = 180.0$
- || $\theta_1 = 10.6$
x || Y = UT



A01188 007

FADED BLACK COTTON

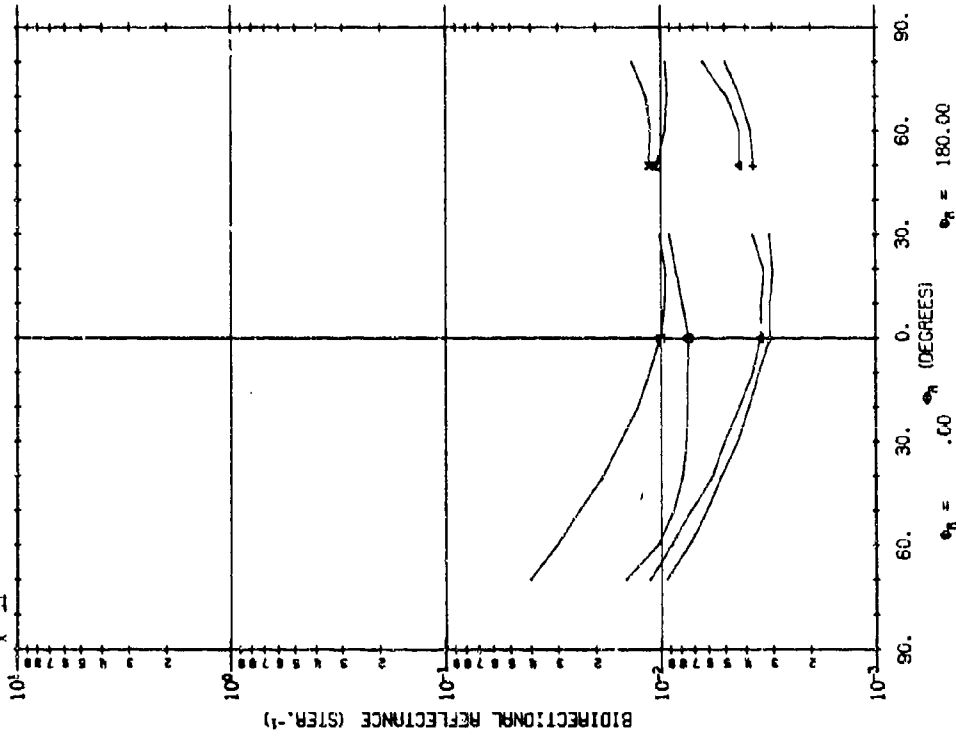
0 || $\theta_1 = 0.0$
+ || $\theta_1 = 180.0$
- || $\theta_1 = 180.0$
x || $\theta_1 = 0.63$



A01188 007

FADED BLACK COTTON

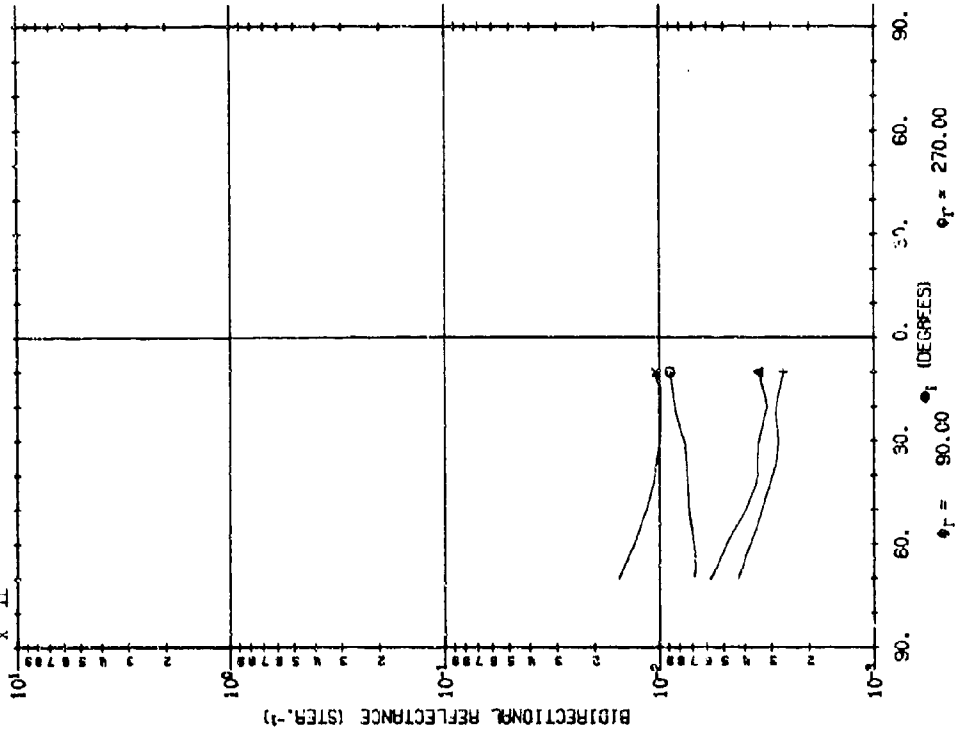
$\theta_1 = 40.0$
 $\phi_1 = 180.0$
 $\lambda = 0.63$



A01188 007

FADED BLACK COTTON

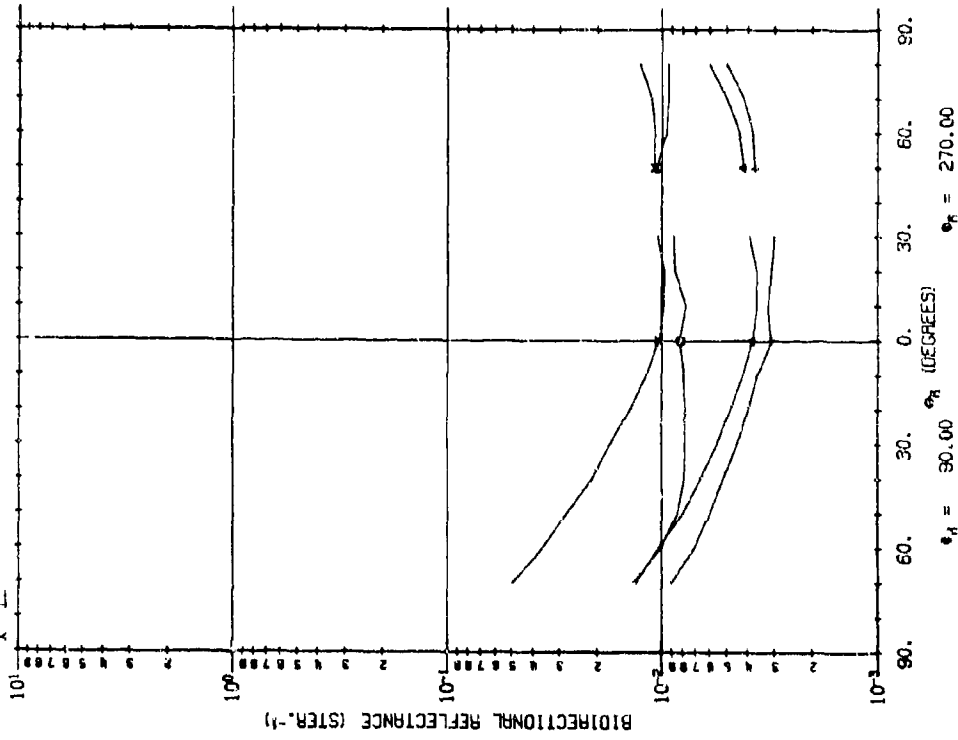
$\theta_1 = 0.0$
 $\phi_1 = 270.0$
 $\lambda = 0.63$



R01188 007

FADED BLACK COTTON

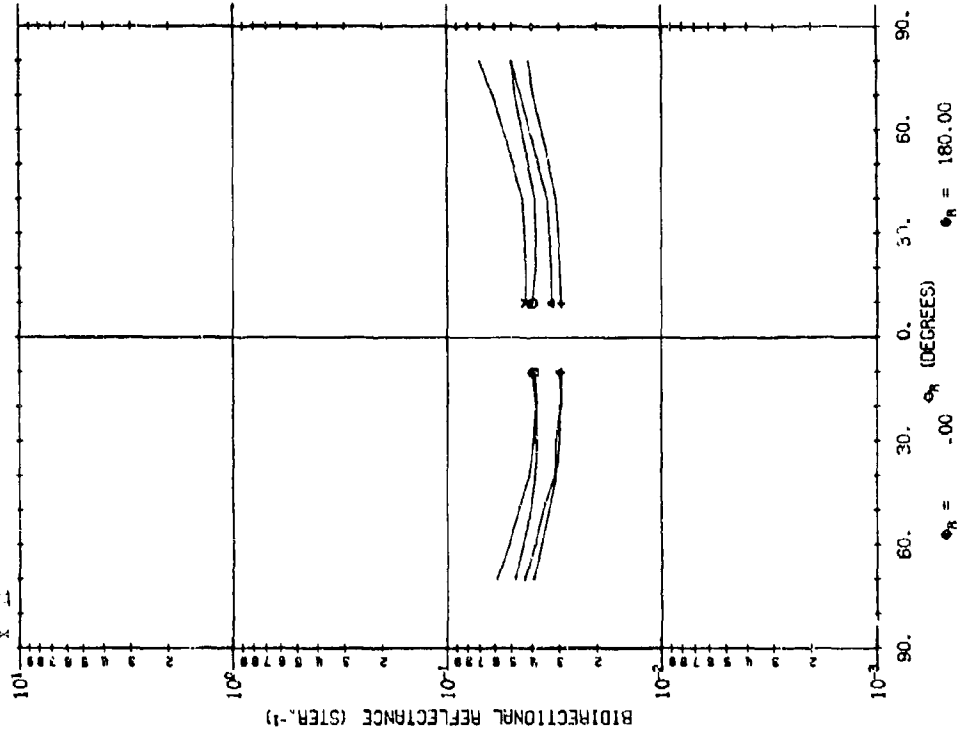
0 || $\theta_i = 40.0$
+ || $\theta_r = 270.0$
4 || $\lambda = 0.63$
X ||



R01189 008

GRAY-GREEN HEAVY COTTON DRILL

0 || $\theta_i = 0.0$
+ || $\theta_r = 180.0$
1 || $\lambda = 0.63$
X ||



A01189 008

GRAY-GREEN HEAVY COTTON DRILL

$\rho_1 = 40.0$
 $\rho_2 = 189.0$
 $\lambda = 0.63$

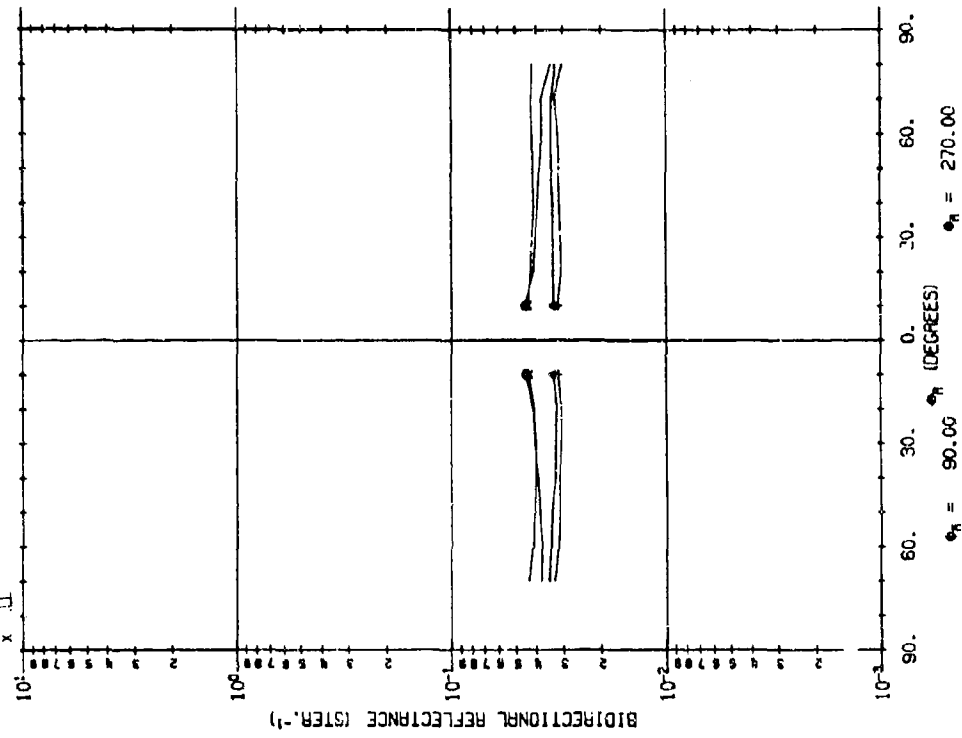
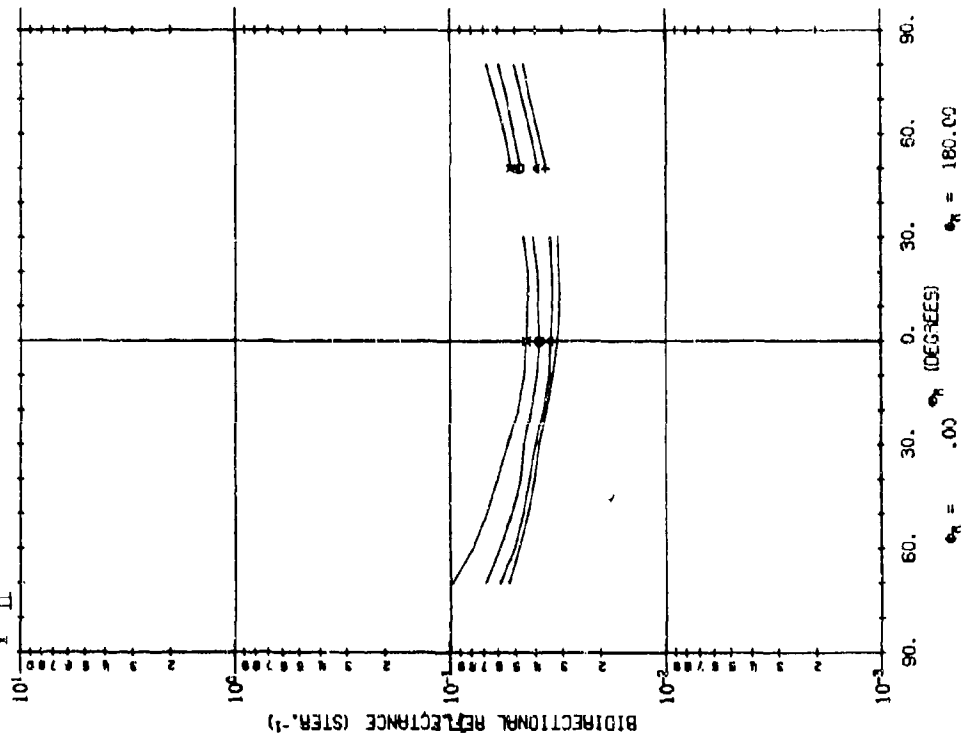
0 ||
+ ||
x ||

A01189 008

GRAY-GREEN HEAVY COTTON DRILL

$\rho_1 = 0.0$
 $\rho_2 = 270.0$
 $\lambda = 0.63$

0 ||
+ ||
x ||



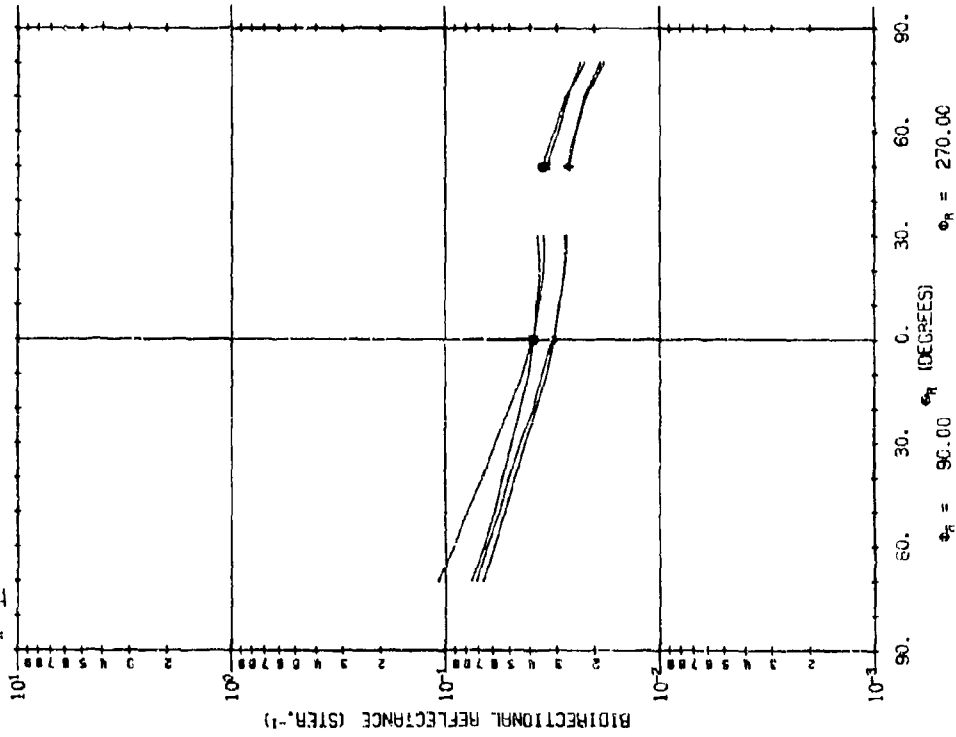
CLOTH AND CANVAS

R01189 008

GRAY-GREEN HEAVY COTTON DRILL

$\theta_1 = 40.0$
 $\theta_2 = 270.0$
 $\lambda = 0.63$

0 1 1
+ 1 1
- 1 1
X 1 1

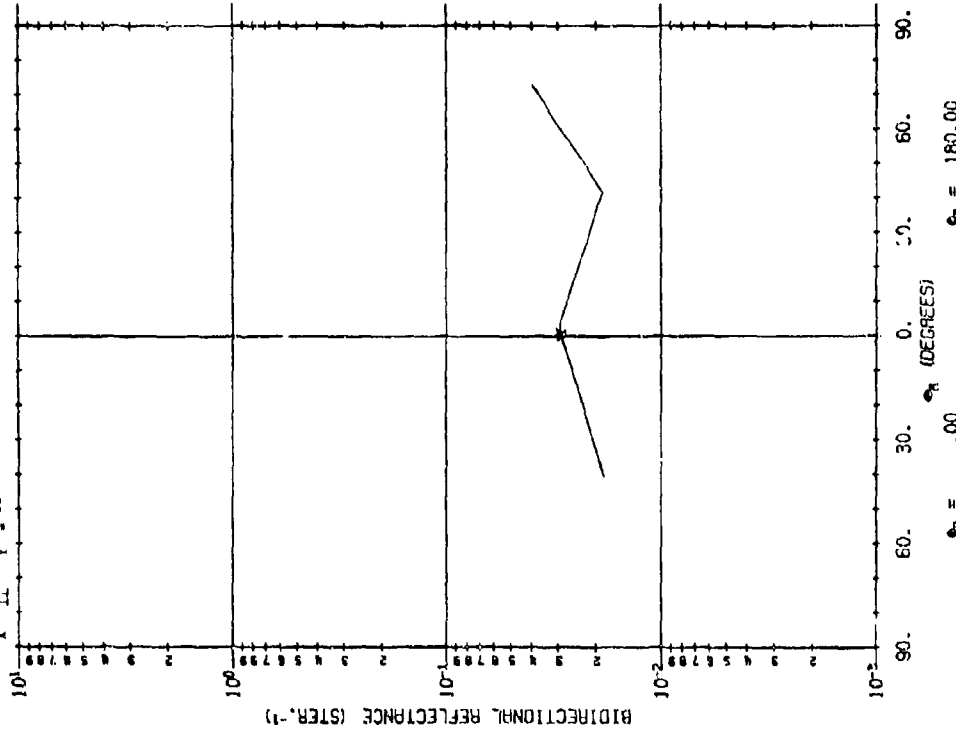


R01466 002

Black Paint on Canvas, 4% Reflectance

$\theta_1 = 1.10$
 $\theta_2 = 4r$
 $\lambda = 10.6$

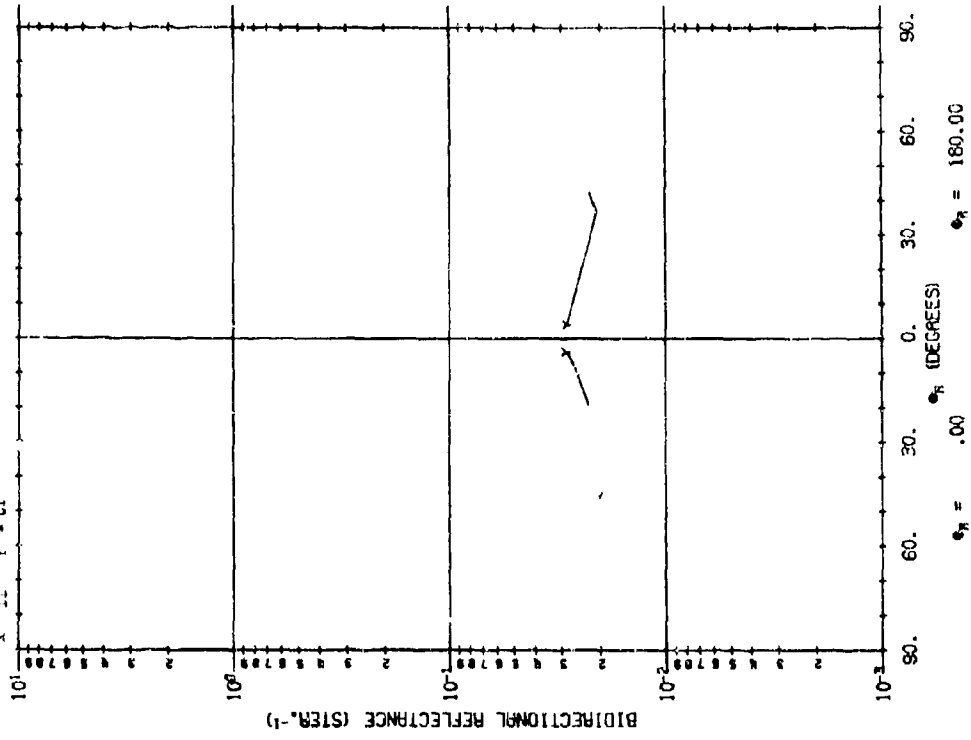
0 1 1
+ 1 1
- 1 1
X 1 1



R01466 002

Black Paint on Canvas, 4% Reflectance

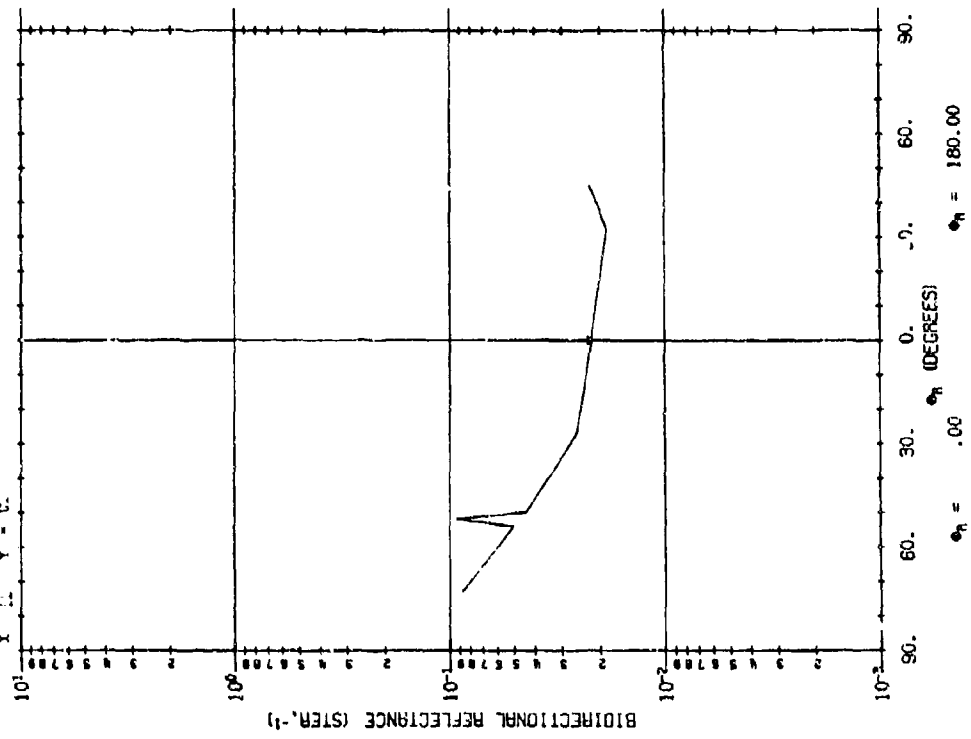
0 // $\phi_1 = 90.0$
+ // $\phi_2 = 180.0$
- // $\phi_3 = 10.6$
X // Y = U



R01466 002

Black Paint on Canvas, 4% Reflectance

0 // $\phi_1 = 90.0$
+ // $\phi_2 = 180.0$
- // $\phi_3 = 10.6$
X // Y = U



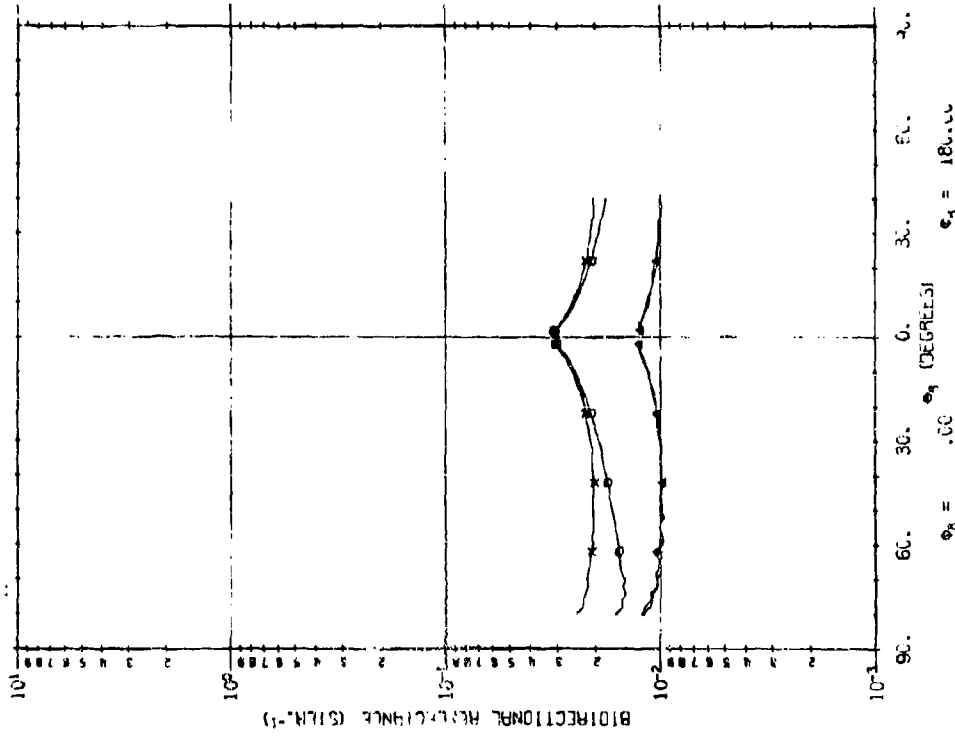
CLOTH AND CANVAS

901170 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

0 1 2 3 4 5 6 7 8 9 10
+ 1 2 3 4 5 6 7 8 9 10
x 1 2 3 4 5 6 7 8 9 10

$\epsilon_1 = 0.0$
 $\epsilon_2 = 180.0$
 $\epsilon_3 = 0.63$

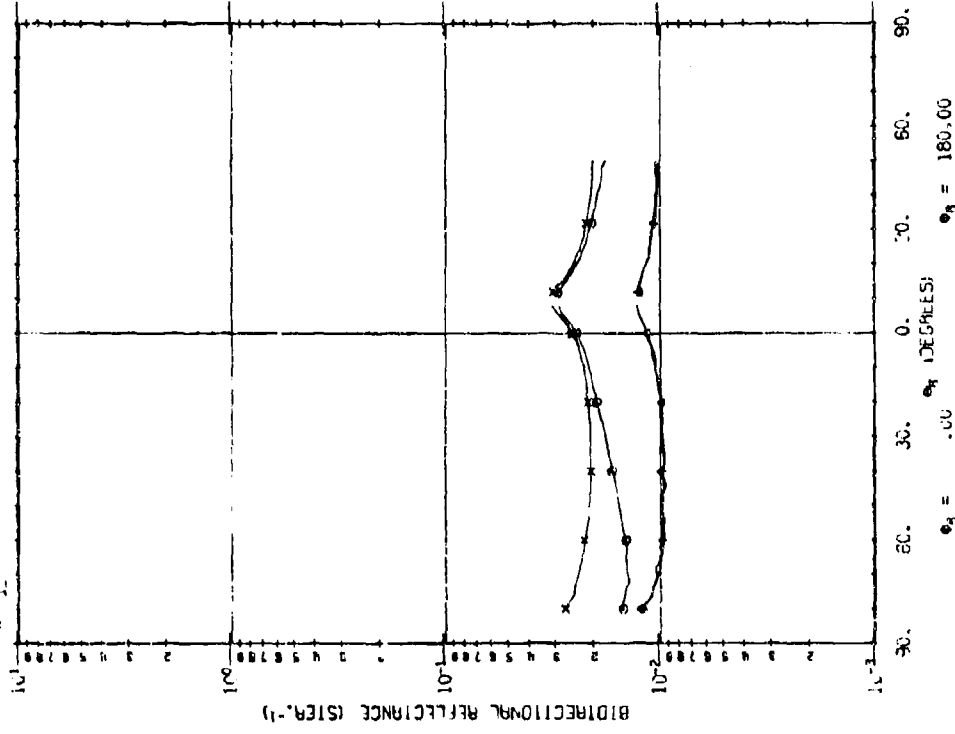


901470 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

0 1 2 3 4 5 6 7 8 9 10
+ 1 2 3 4 5 6 7 8 9 10
x 1 2 3 4 5 6 7 8 9 10

$\epsilon_1 = 10.0$
 $\epsilon_2 = 180.0$
 $\epsilon_3 = 0.63$



A01470 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

$\theta_1 = 20.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$

A01470 101

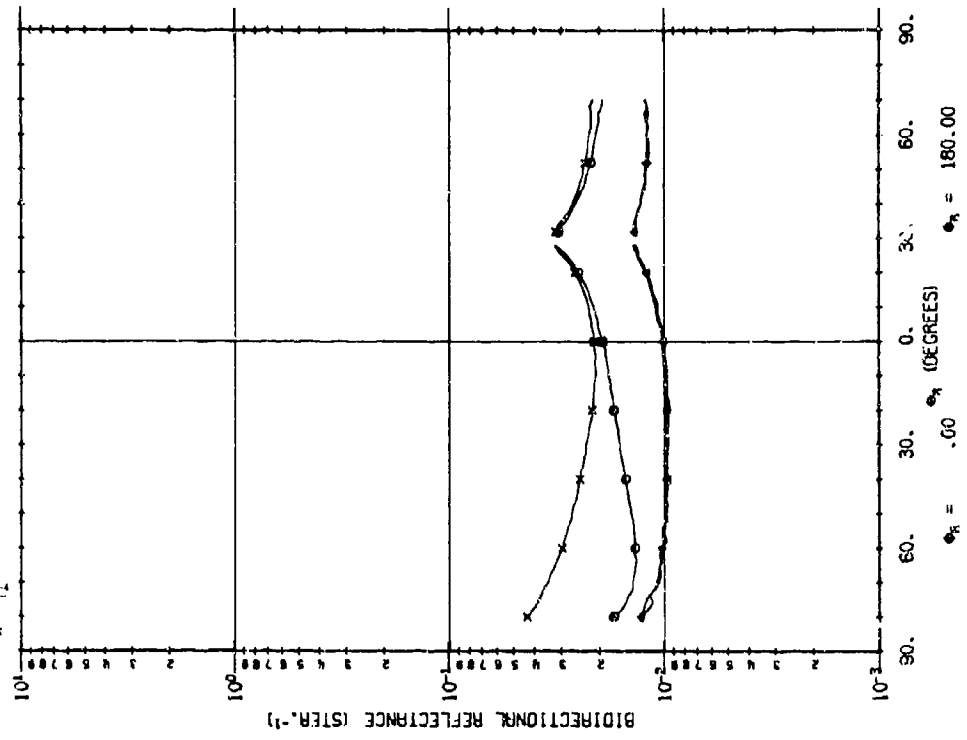
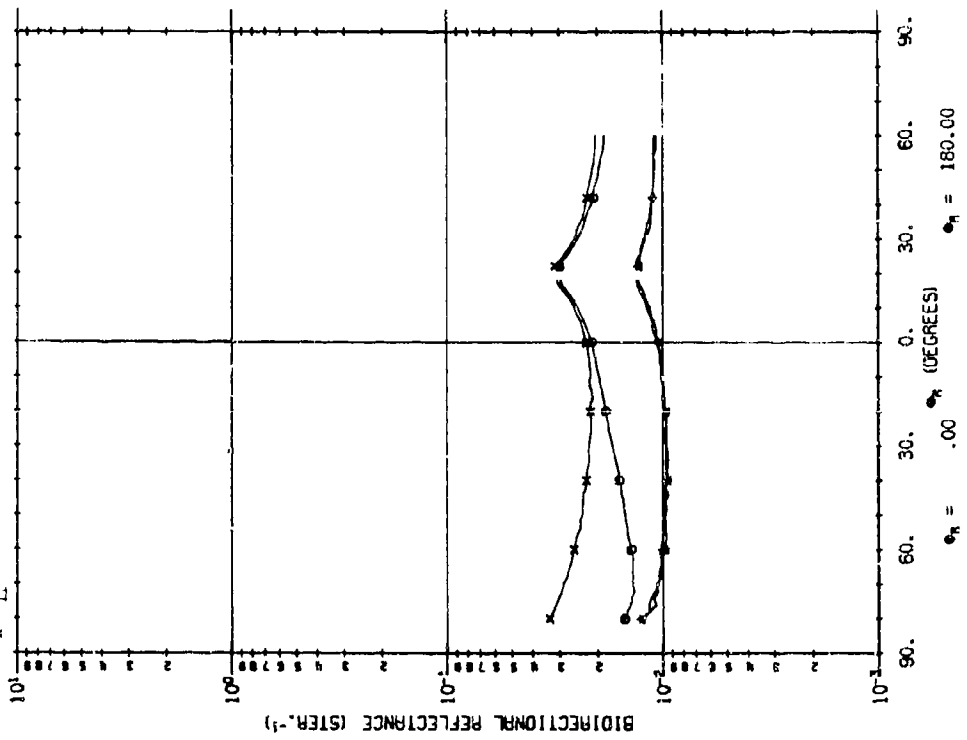
MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$

A01470 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 0.63$



CLOTH AND CANVAS

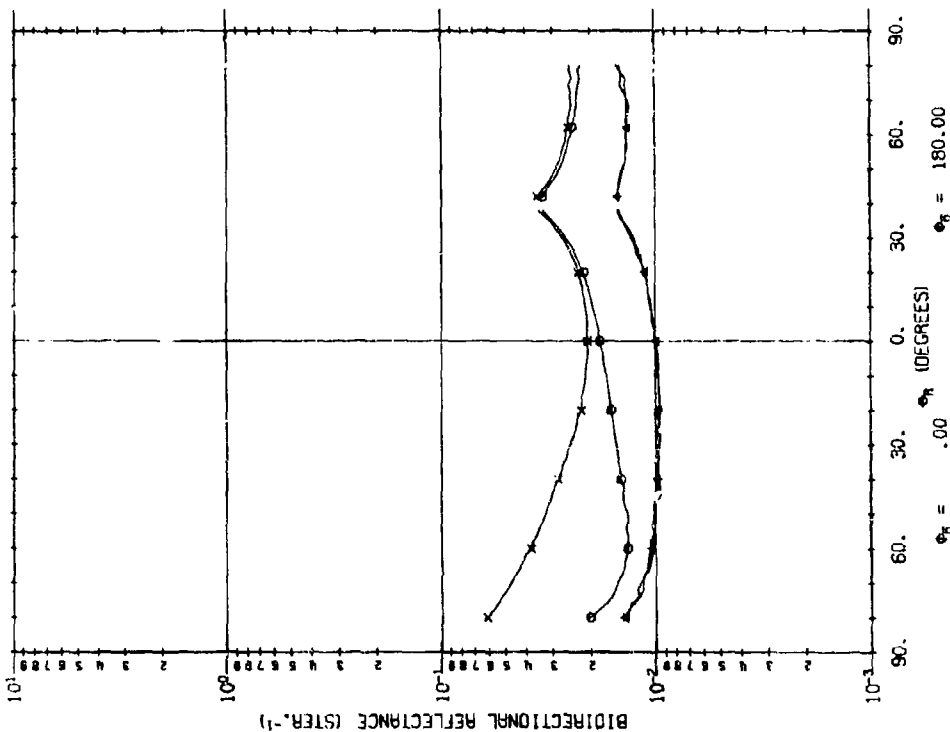
A01470 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

$\frac{1}{2} \lambda = 40.0$
 $\lambda = 80.0$
 $\lambda = 120.0$
 $\lambda = 160.0$
 $\lambda = 200.0$

$\lambda = 0.63$

0
+
x



$\phi_n = .00$ $\phi_n = 180.00$

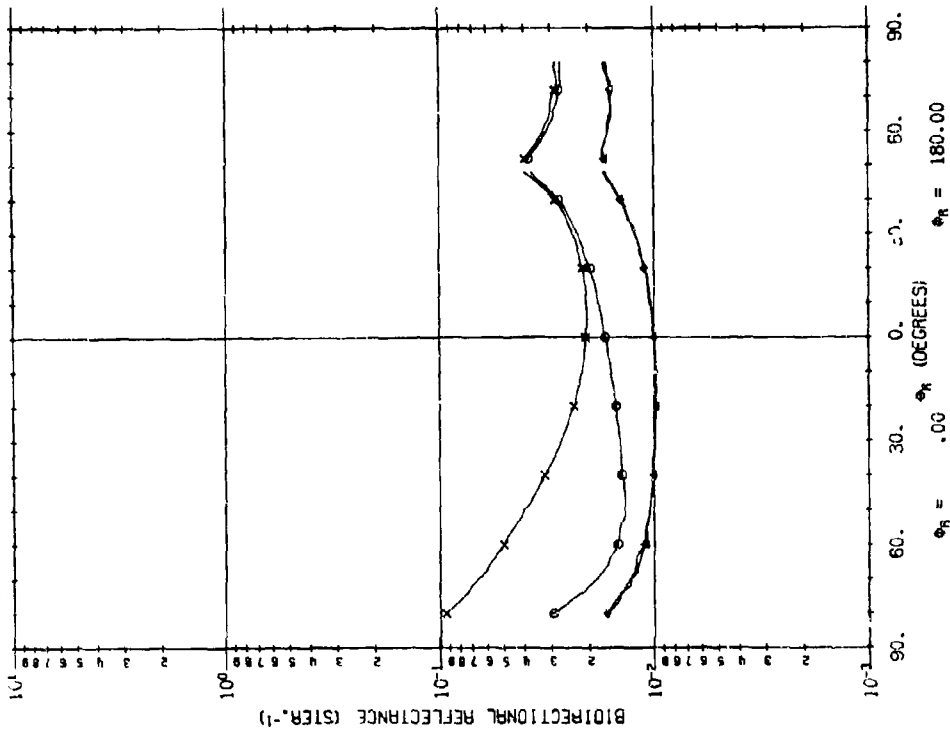
A01470 101

MEDIUM GRAY PAINT ON CANVAS,
16 PERCENT REFLECTANCE

$\frac{1}{2} \lambda = 50.0$
 $\lambda = 100.0$
 $\lambda = 150.0$
 $\lambda = 200.0$

$\lambda = 0.63$

0
+
x



$\phi_n = .00$ $\phi_n = 180.00$

AO1470 002

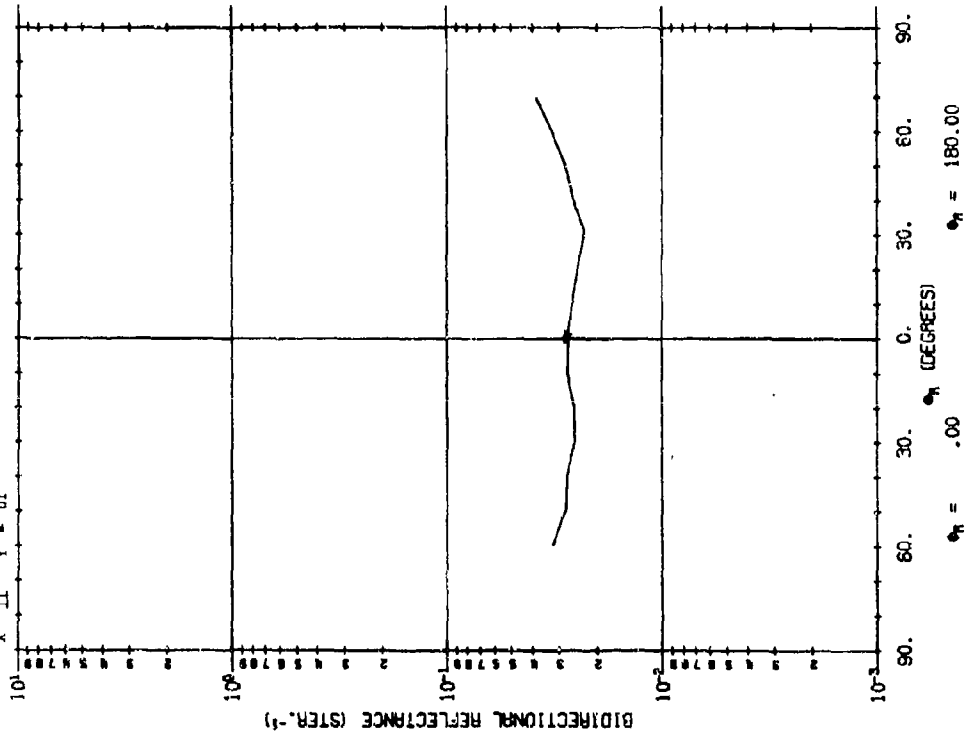
Medium Gray Paint on Canvas, 16% Reflectance

0 11 23 = 1.10

+ 11 $\phi_1 = \phi_r$

Δ 11 $\lambda = 56.6$

X 11 Y = UT



AO1470 002

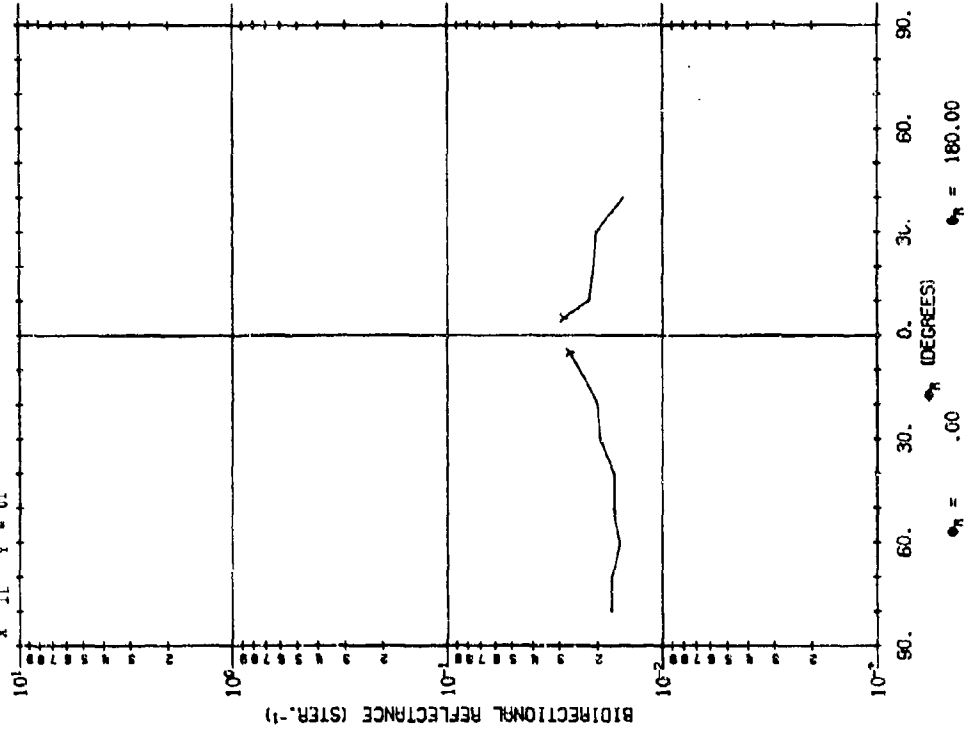
Medium Gray Paint on Canvas, 16% Reflectance

0 11 $\phi_1 = 0.0$

+ 11 $\phi_1 = 180.0$

Δ 11 $\lambda = 10.6$

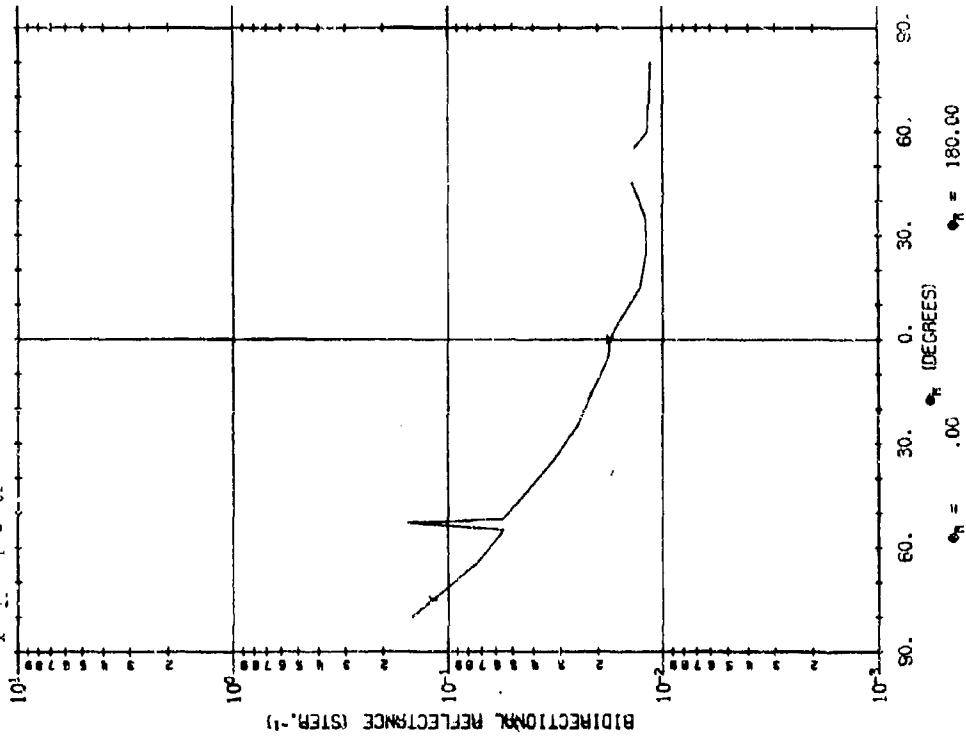
X 11 Y = UT



R01470 002

Medium Gray Paint on Canvas, 16% Reflectance

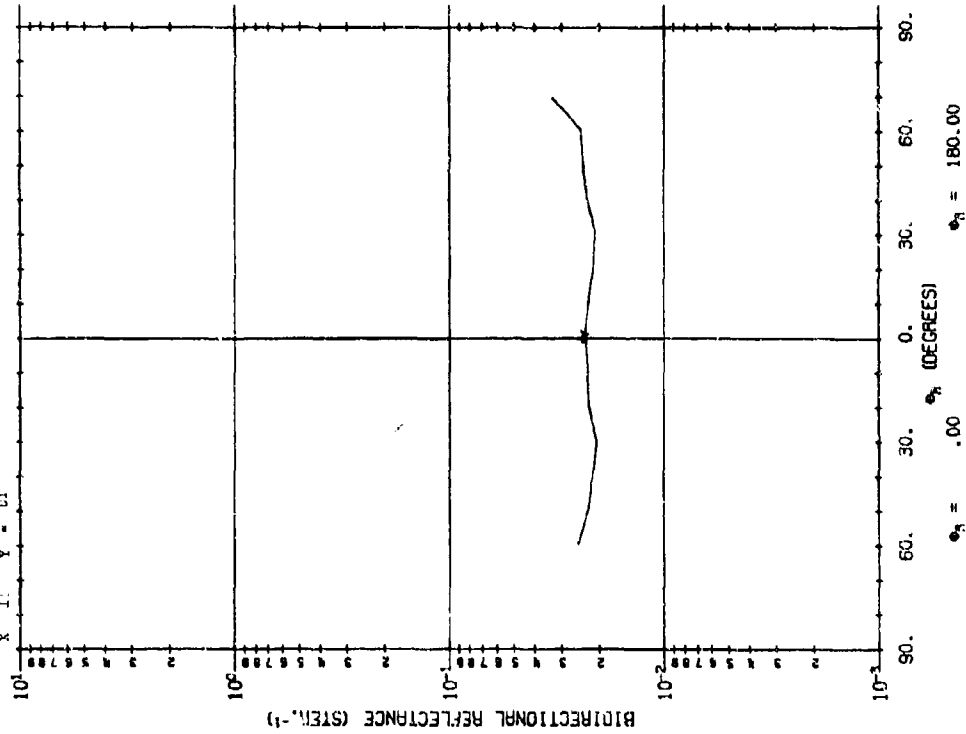
$\theta_i = 50.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y Z
UT



R01471 002

Medium Gray Paint on Canvas, 16% Reflectance

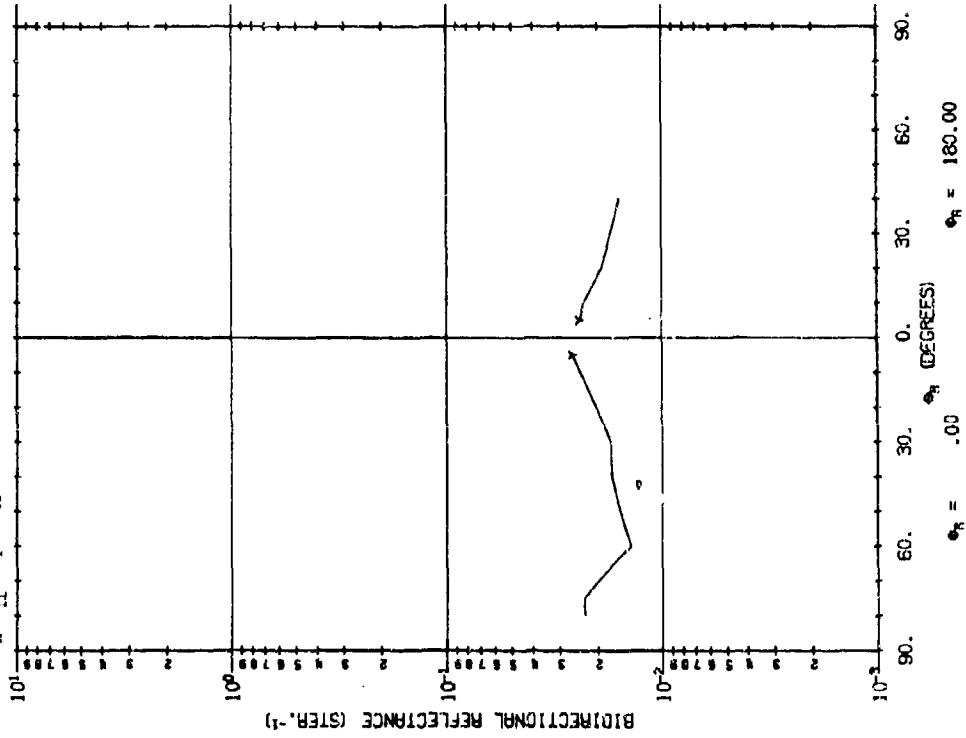
$\theta_i = 25 = 1.10$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y Z
UT



R01471 002

Medium Gray Paint on Canvas, 16% Reflectance

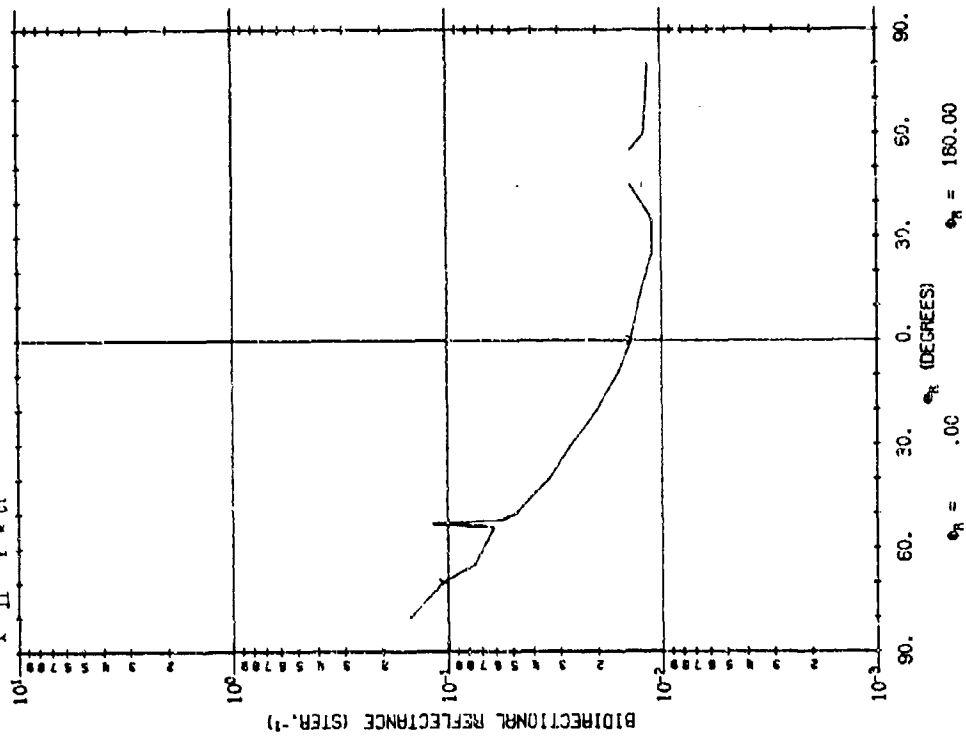
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 10.6$
x || $\gamma = \text{UT}$



R01471 002

Medium Gray Paint on Canvas, 16% Reflectance

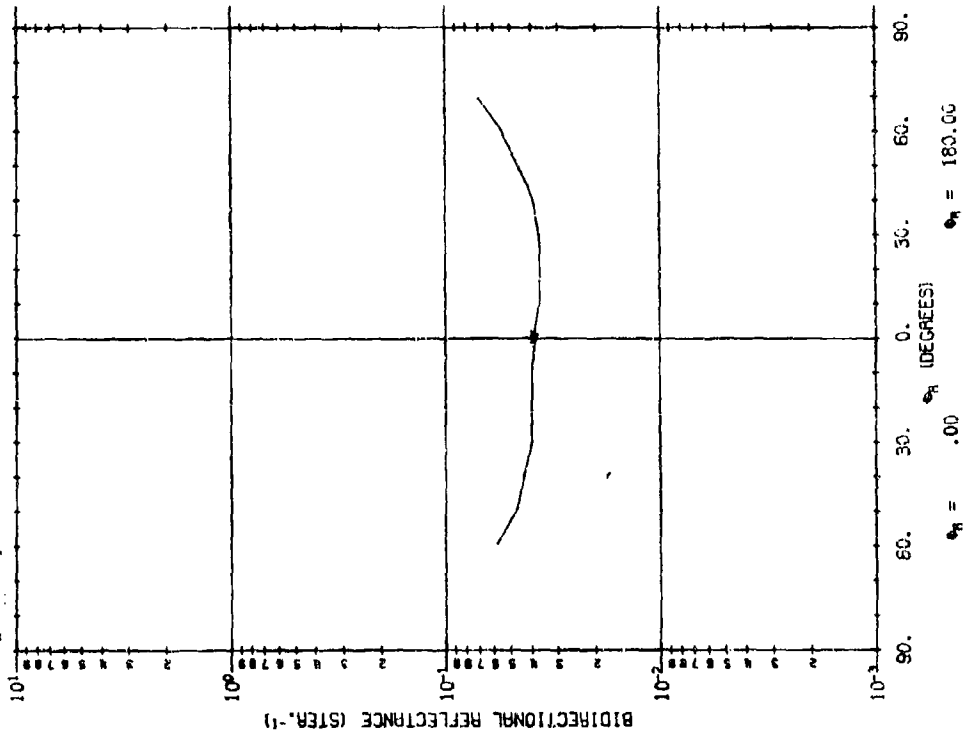
0 || $\theta_1 = 50.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 10.6$
x || $\gamma = \text{UT}$



AO1474 .002

Grayish-White Paint on Canvas, 647 Reflectance

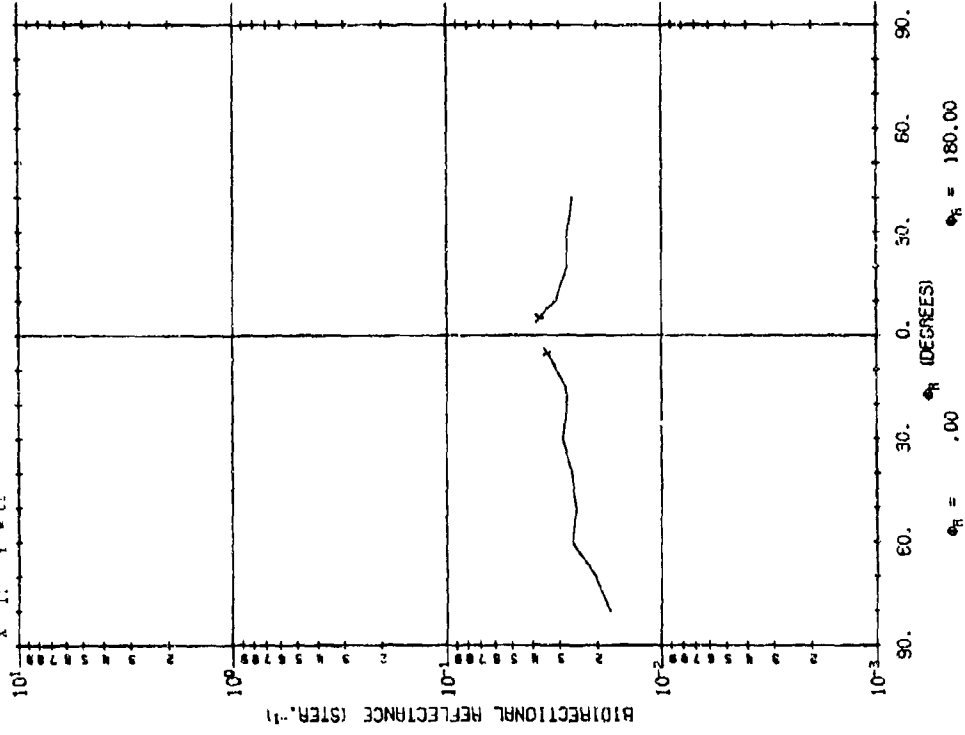
0 11 21 = 1.10
+ 11 21 = 10
- 11 21 = 10.6
X 11 Y = 10



AO1474 .002

Grayish-White Paint on Canvas, 641 Reflectance

0 11 21 = 0.0
+ 11 21 = 180.0
- 11 21 = 10.6
X 11 Y = 10

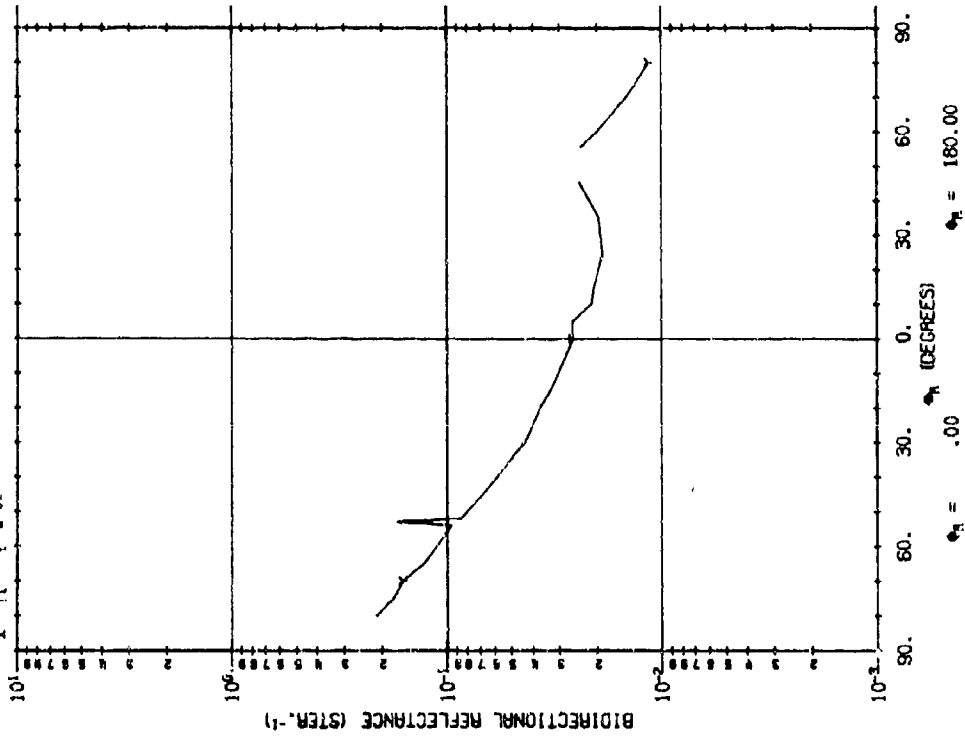


CLOTH AND CANVAS

A01474 002

Grayish-White Paint on Canvas, 64% Reflectance

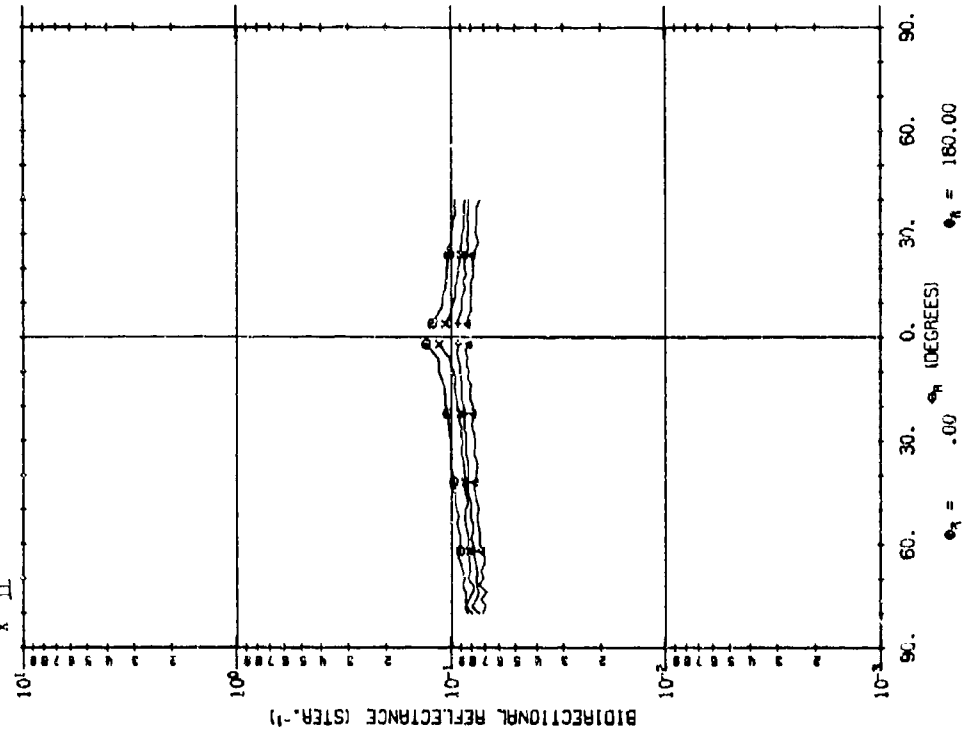
0 | | $\epsilon_1 = 50.0$
+ | | $\phi_1 = 180.0$
 λ | | $\lambda = 10.6$
X | | $\gamma = \text{VT}$



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,
66 PERCENT REFLECTANCE

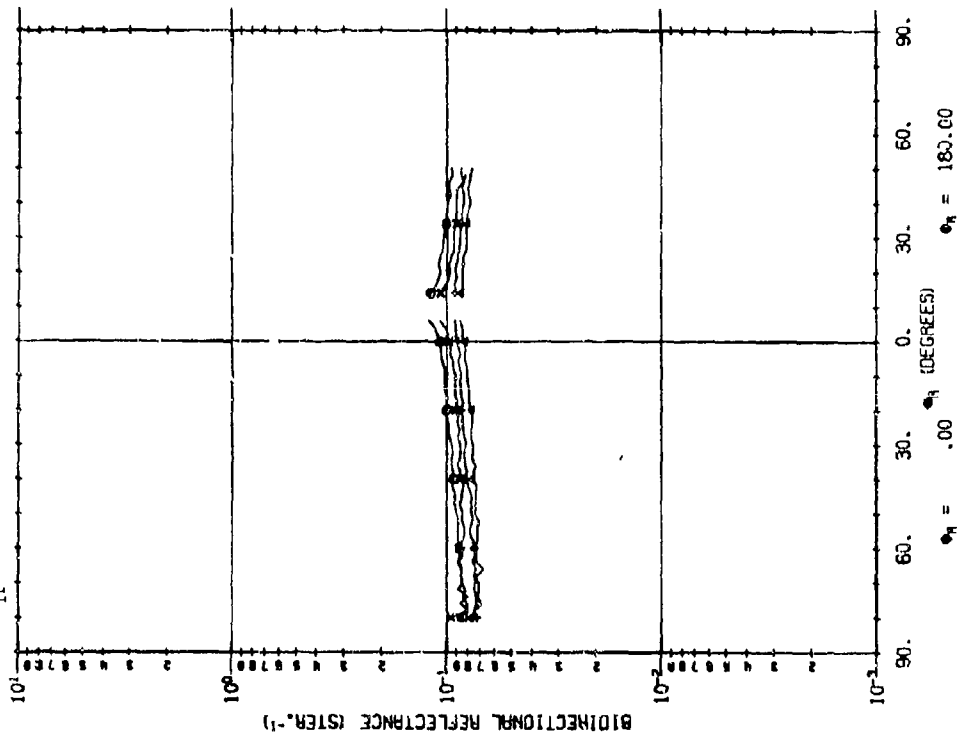
0 | | $\epsilon_1 = 0.0$
+ | | $\phi_1 = 180.0$
 Δ | | $\lambda = 0.63$
X | |



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

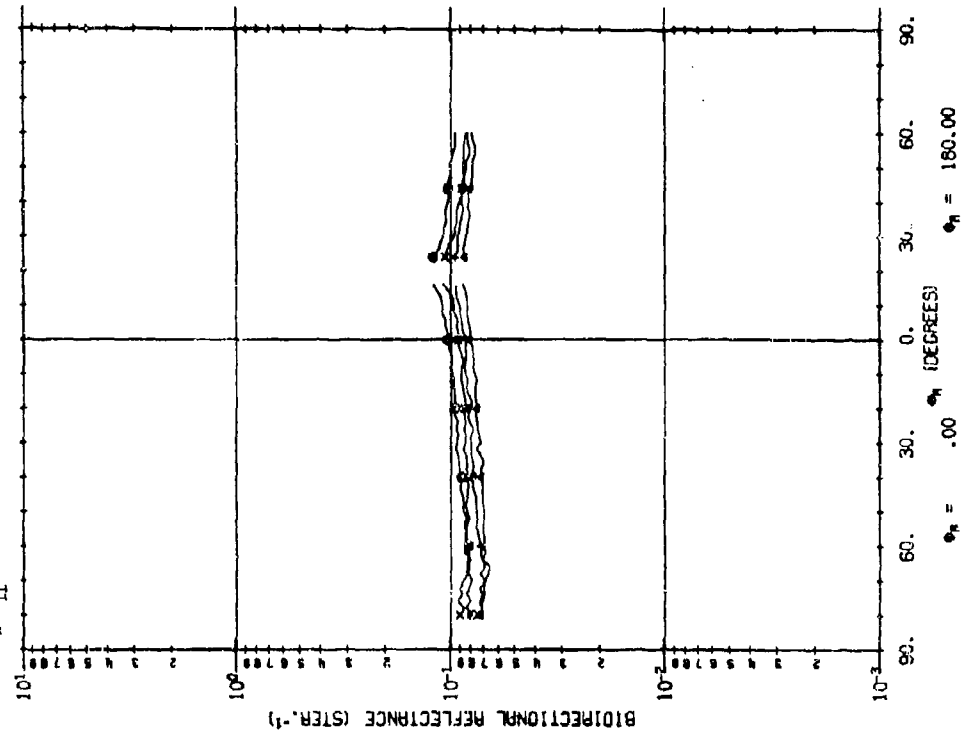
0 | | $\theta_i = 10.0$
+ | | $\phi_i = 180.0$
Δ | | $\lambda = 0.63$
x | |



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

0 | | $\theta_i = 20.0$
+ | | $\phi_i = 180.0$
Δ | | $\lambda = 0.63$
x | |

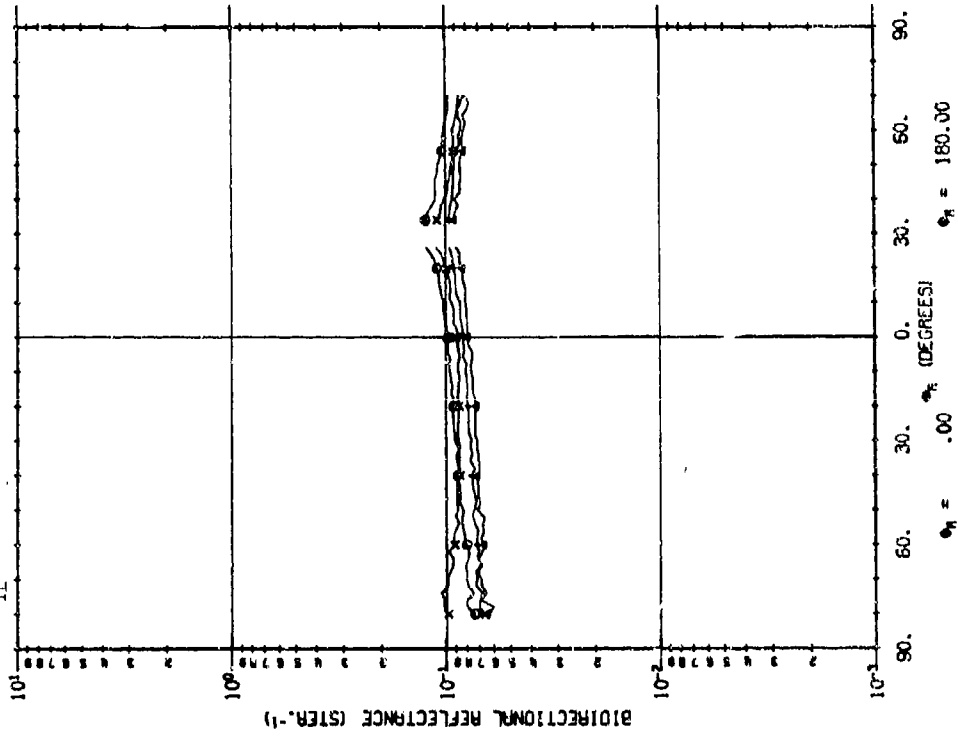


CLOTH AND CANVAS

A01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

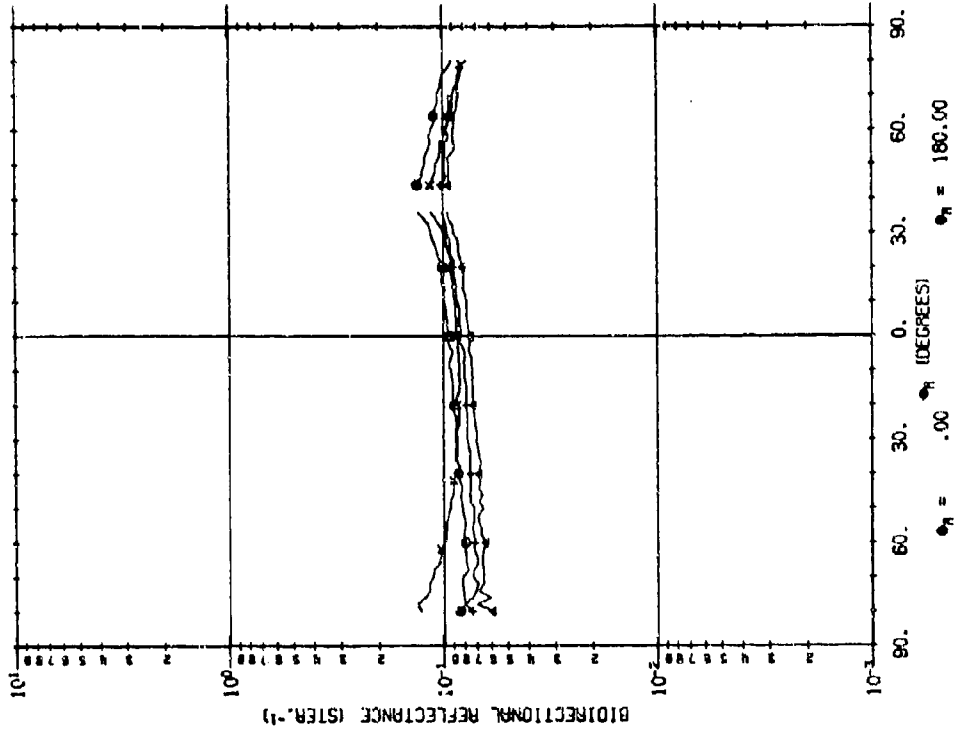
0 || $\phi_1 = 30.0$
+ || $\phi_1 = 180.0$
△ || $\lambda = 0.63$
X ||



A01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

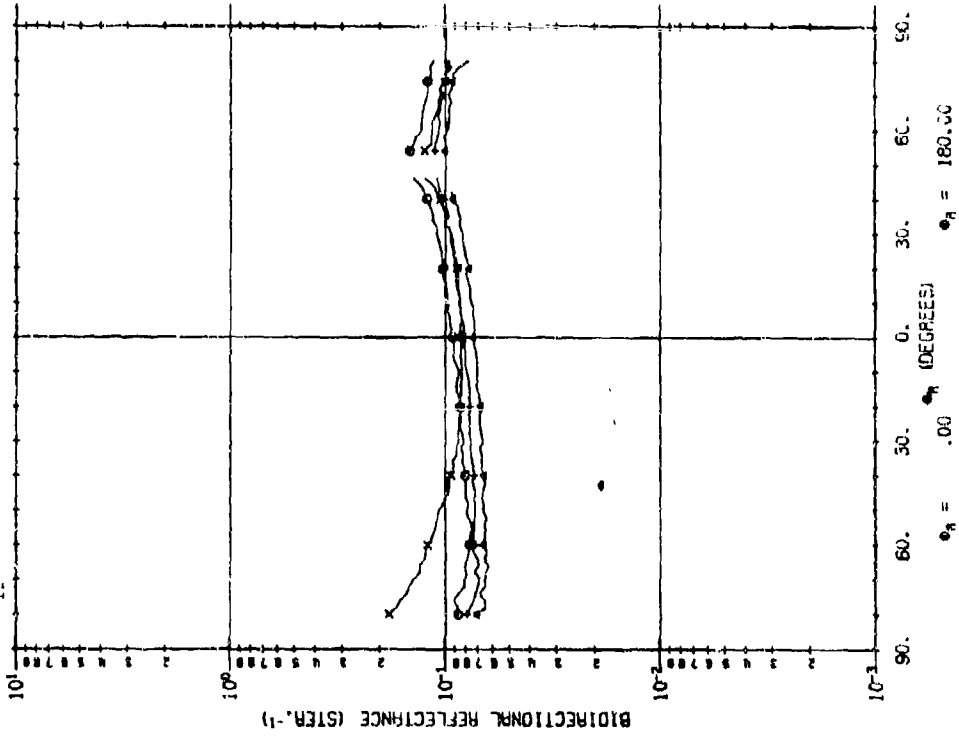
0 || $\phi_1 = 40.0$
+ || $\phi_1 = 180.0$
△ || $\lambda = 0.63$
X ||



R01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

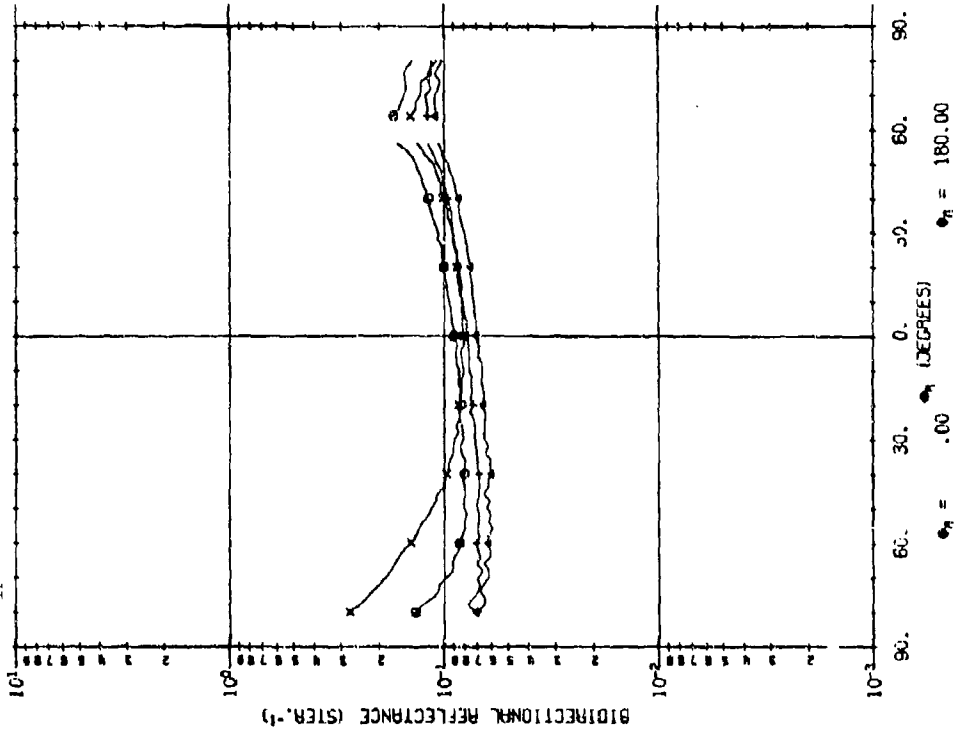
0 | | $\theta_1 = 50.0$
+ | | $\theta_1 = 180.0$
x | | $\theta_1 = 0.53$
x | |



R01475 101

GRAYISH-WHITE PAINT ON CANVAS,
64 PERCENT REFLECTANCE

0 | | $\theta_1 = 60.0$
+ | | $\theta_1 = 180.0$
x | | $\theta_1 = 0.63$
x | |

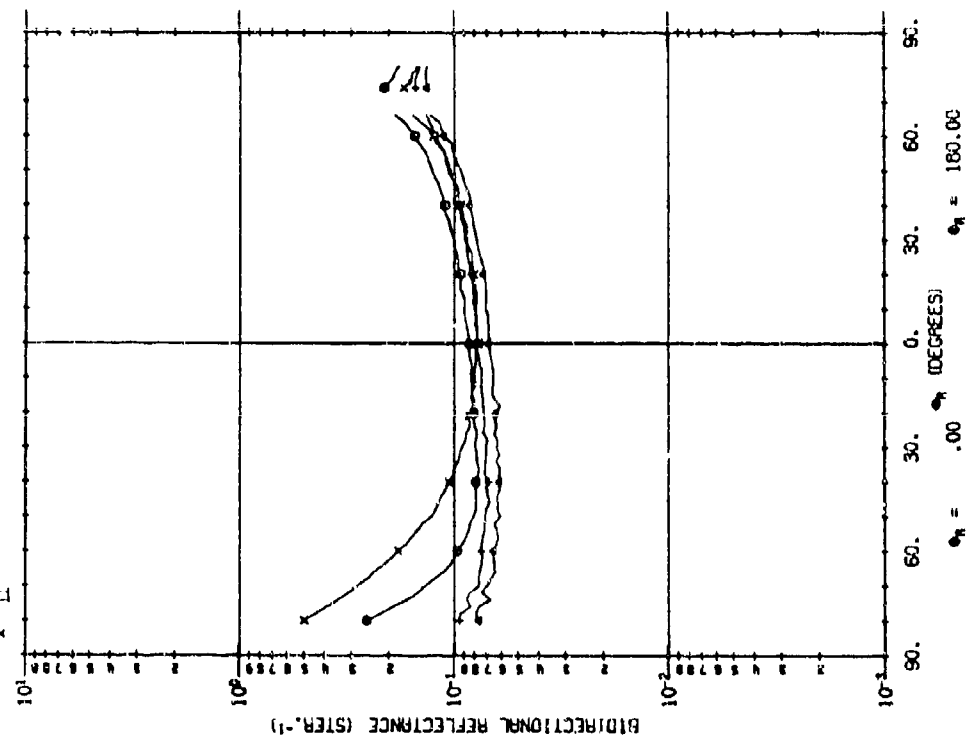


CLOTH AND CANVAS

A01475 101

GRAYISH-WHITE PAINT ON CANVAS.
64 PERCENT REFLECTANCE

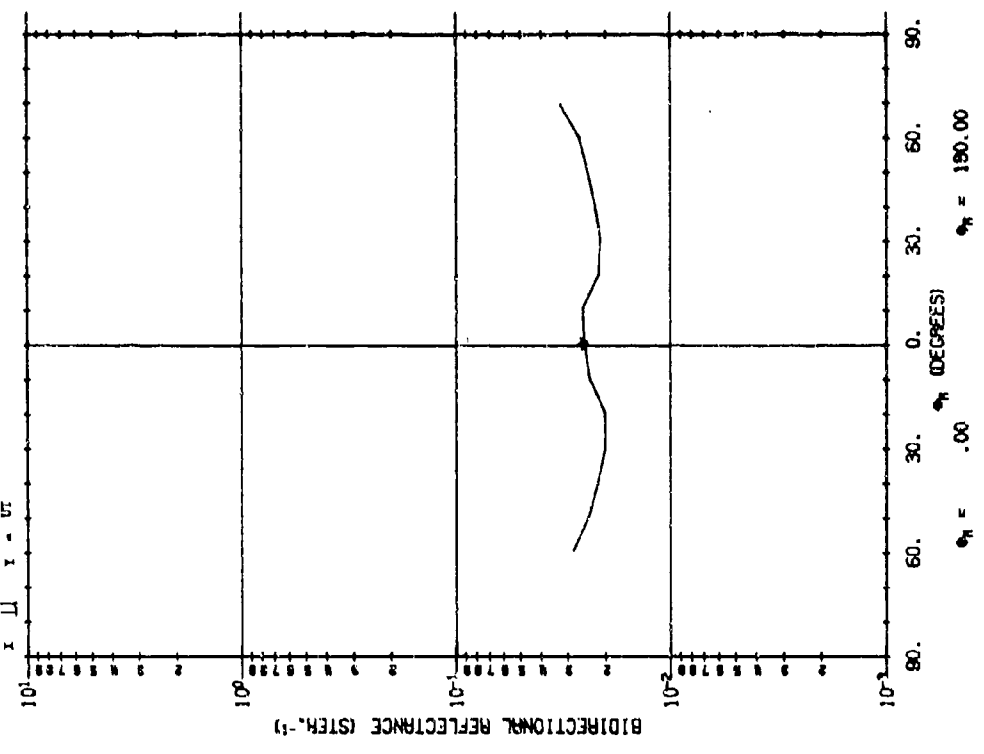
0 || 5.1 = 70.0
+ || 1.1 = 180.0
x || 1.1 = 0.63
x ||



A01478 002

Green Paint on Canvas

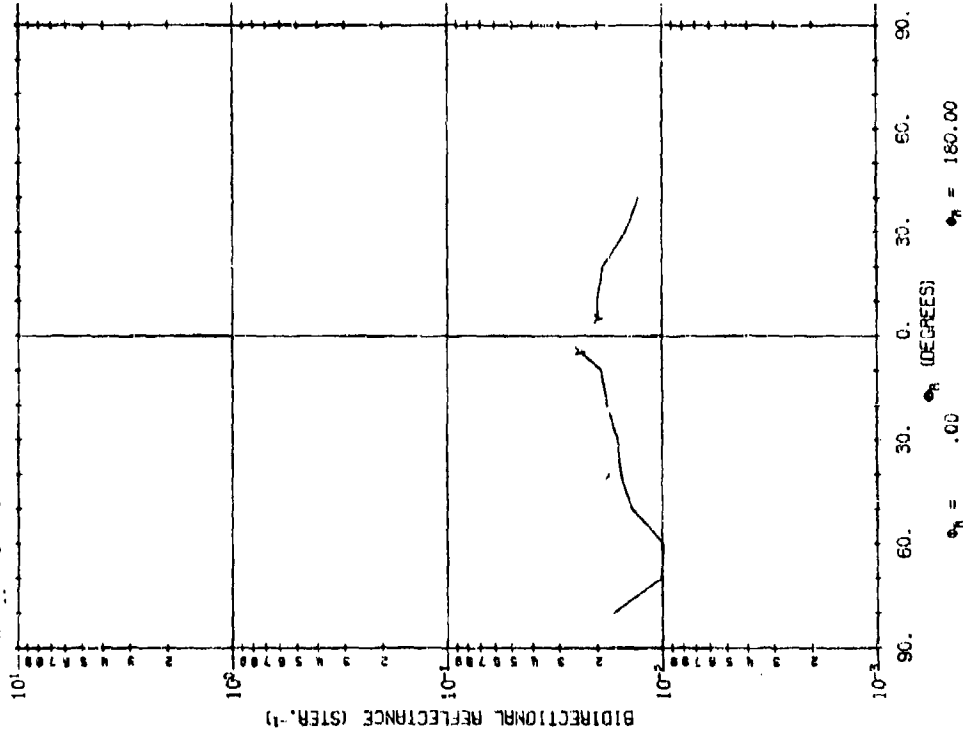
0 || 23 = 1.10
+ || 1.1 = 4r
x || 1.1 = 10.6
x || 1.1 = UT



A01478 002

Green Paint on Canvas

C $\theta_i = 0.0$
+ $\theta_r = 180.0$
- $\theta_i = 10.6$
X $\theta_r = 180.0$
Y = UT

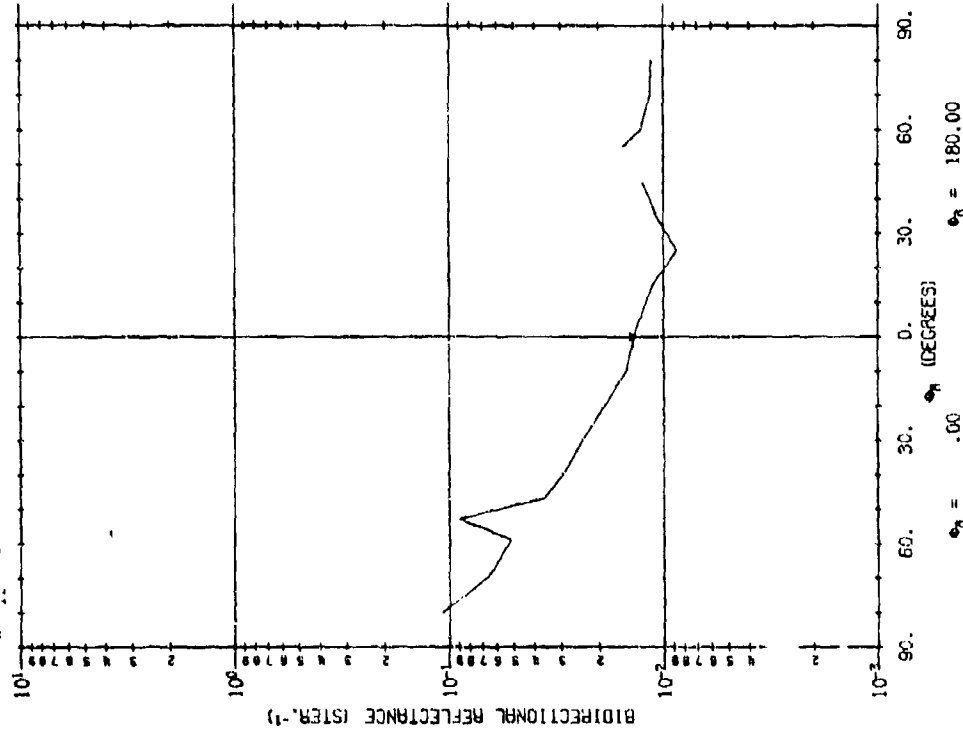


$\theta_i = .00$ $\theta_r = 180.00$

A01478 002

Green Paint on Canvas

C $\theta_i = 53.6$
+ $\theta_r = 180.0$
- $\theta_i = 10.6$
X $\theta_r = 180.0$
Y = UT



$\theta_i = .00$ $\theta_r = 180.00$

CLOTH AND CANVAS

R01480 002

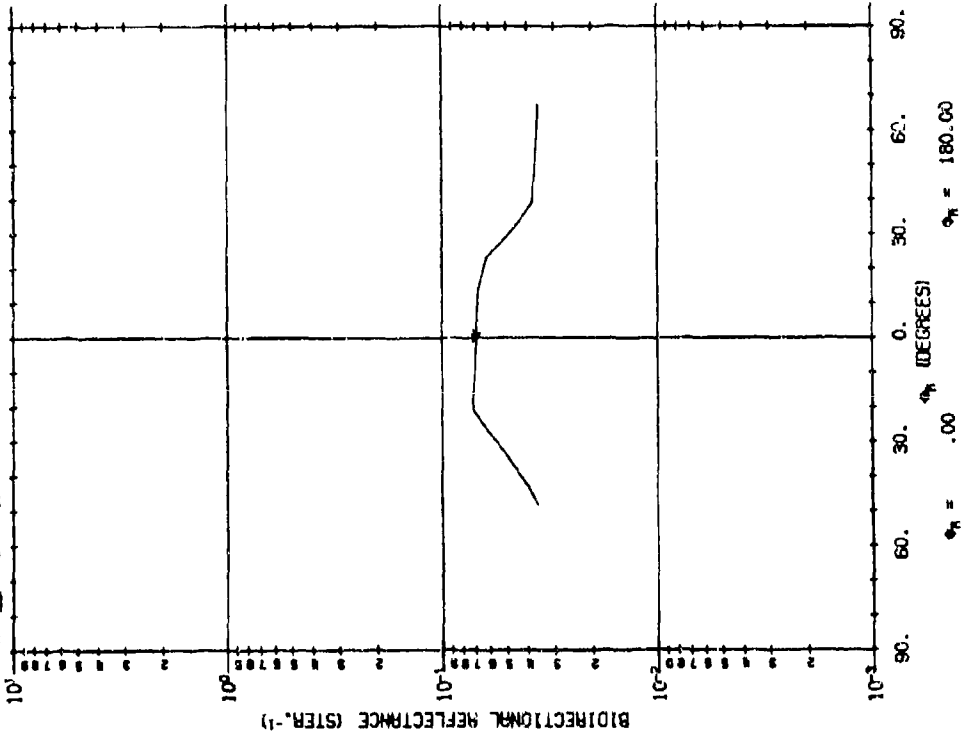
Undyed Cotton, Mercerized Medium

$2\beta = 1.10$

$\phi_1 = \phi_2$

$\lambda = 13.6$

$\gamma = \gamma'$



R01480 002

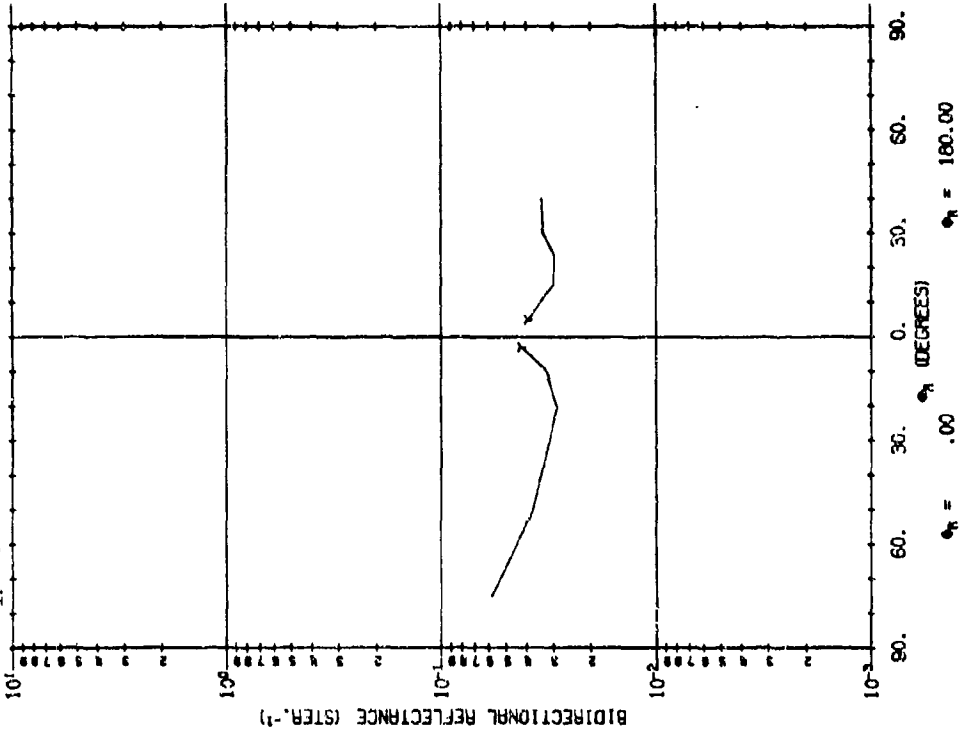
Undyed Cotton, Mercerized Medium

$\phi_1 = 0.0$

$\phi_2 = 180.0$

$\lambda = 13.6$

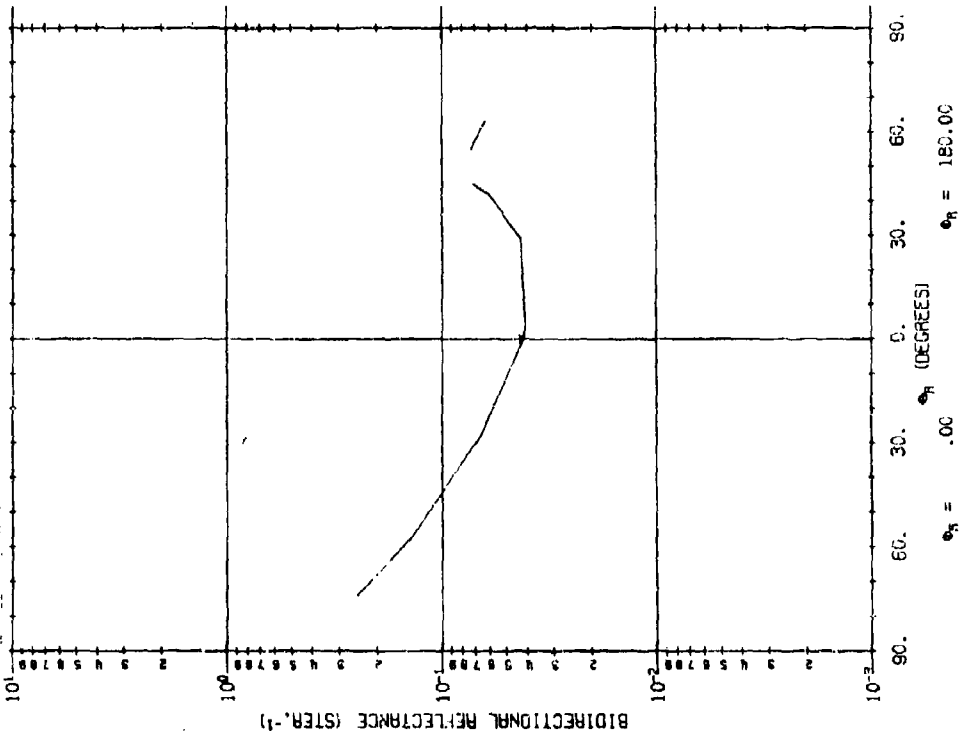
$\gamma = \gamma'$



A01480 002

Undyed Cotton, Mercerized Medium

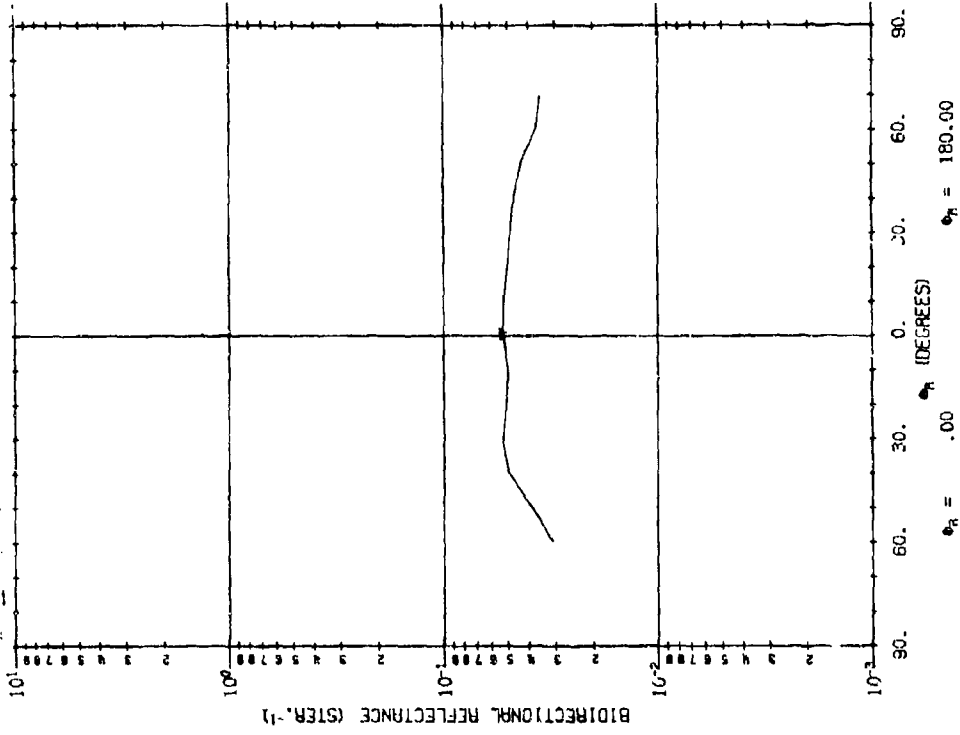
$\lambda_1 = 50.0$
 $\lambda_2 = 189.0$
 $\lambda_3 = 10.6$
 $\lambda_4 = \infty$



A01483 002

Vat Dyed Cotton, Mercerized Medium

$\lambda_1 = 1.10$
 $\lambda_2 = \infty$
 $\lambda_3 = 15.6$
 $\lambda_4 = \infty$

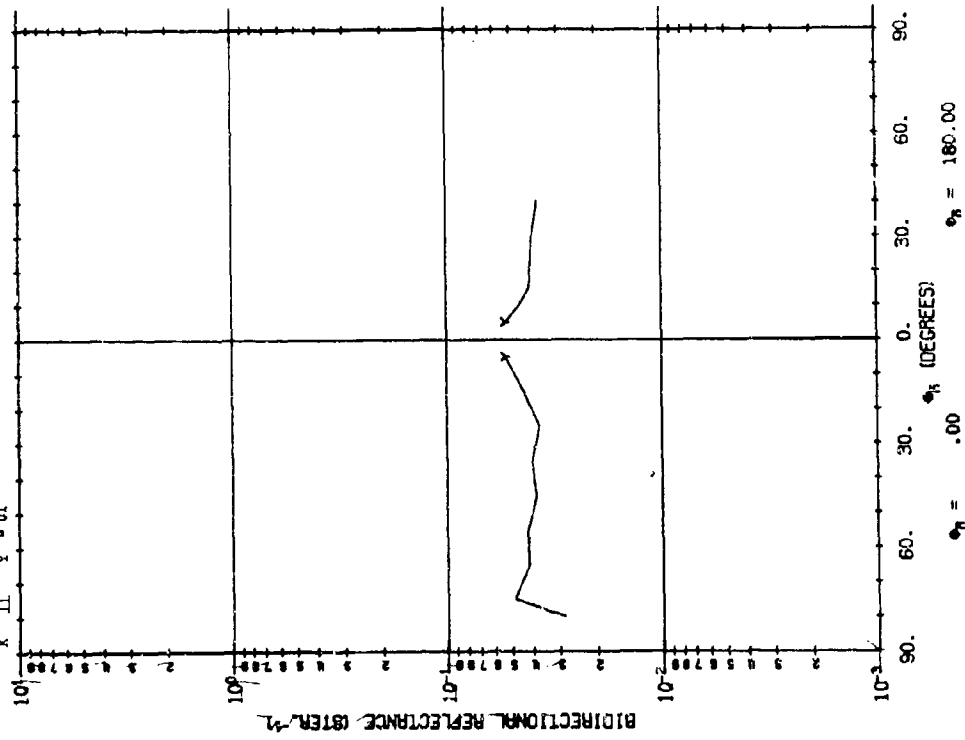


CLOTH AND CANVAS

AG1483 002

Vat Dyed Cotton, Mercerized Medium

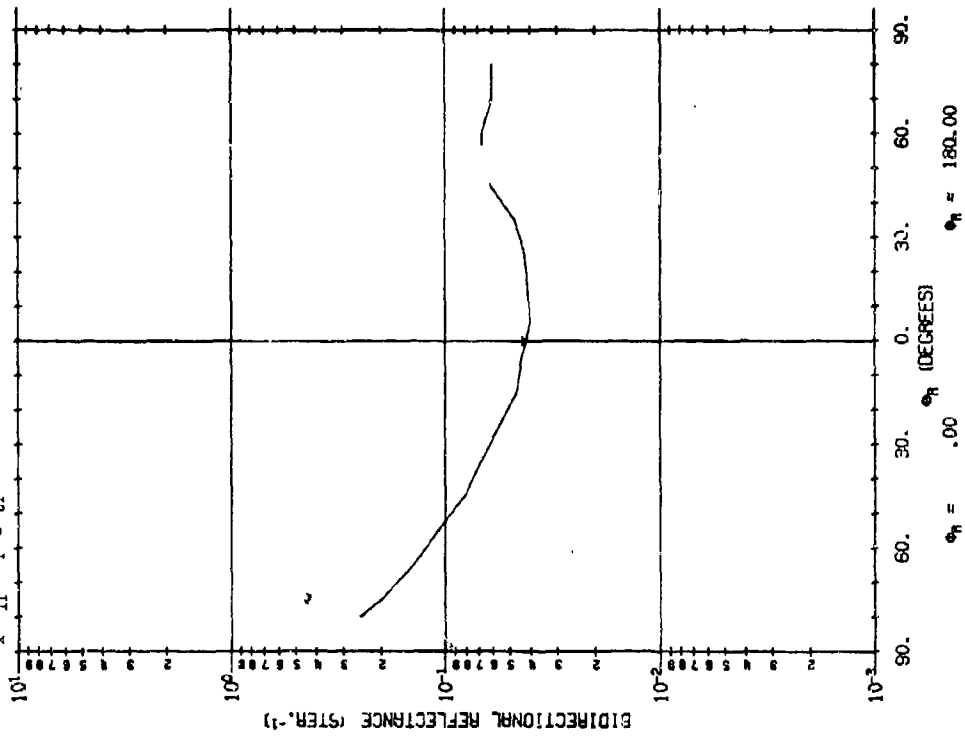
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = VT



A01483 002

Vat Dyed Cotton, Mercerized Medium

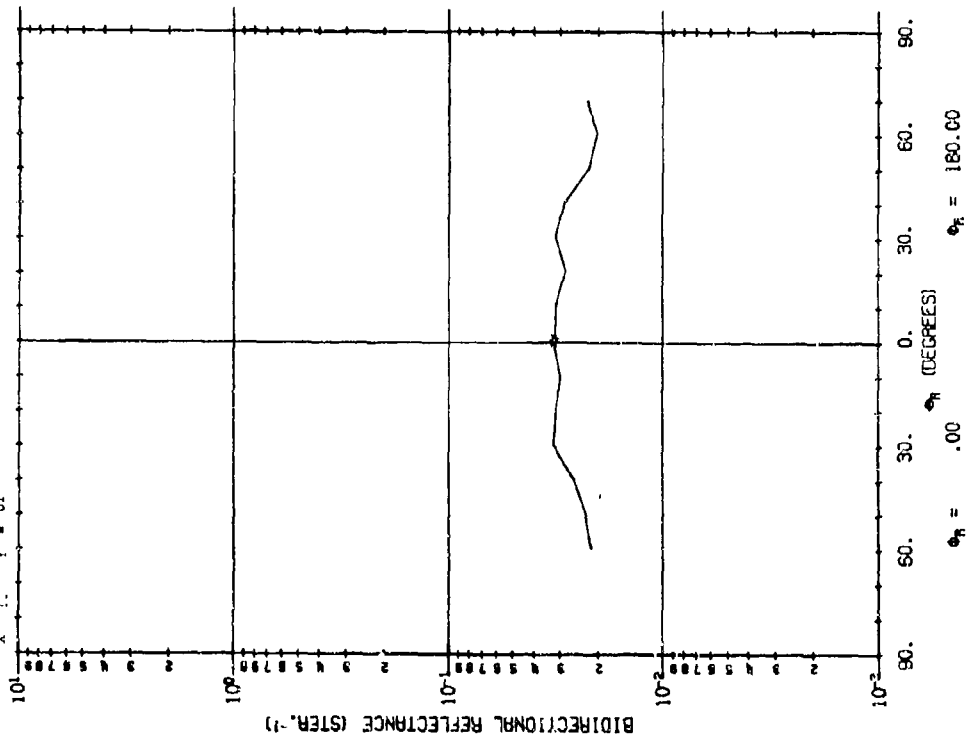
0 || $\theta_1 = 50.0$
+ || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = VT



R01486 002

Cotton, Sulfer Dye, Mercerized Medium

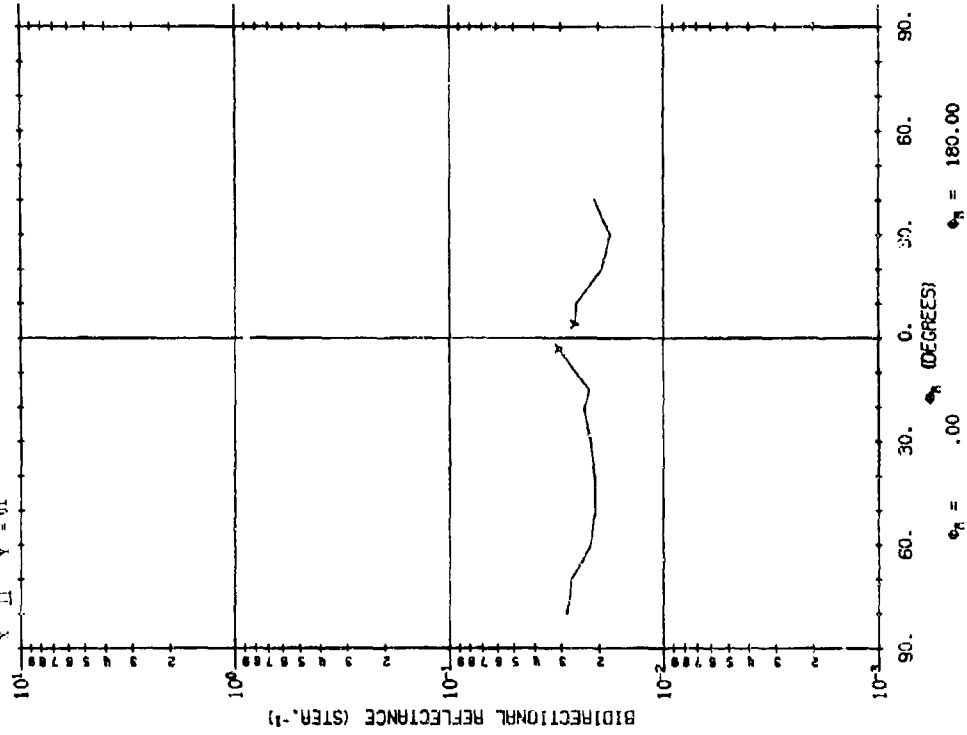
$Z_2 = 1.10$
 $\phi_1 = \phi_2$
 $\lambda = 10.6$
 $Y = UT$



R01486 002

Cotton, Sulfer Dye, Mercerized Medium

$\phi_1 = 0.0$
 $\phi_2 = \phi_3$
 $\lambda = 10.6$
 $Y = UT$

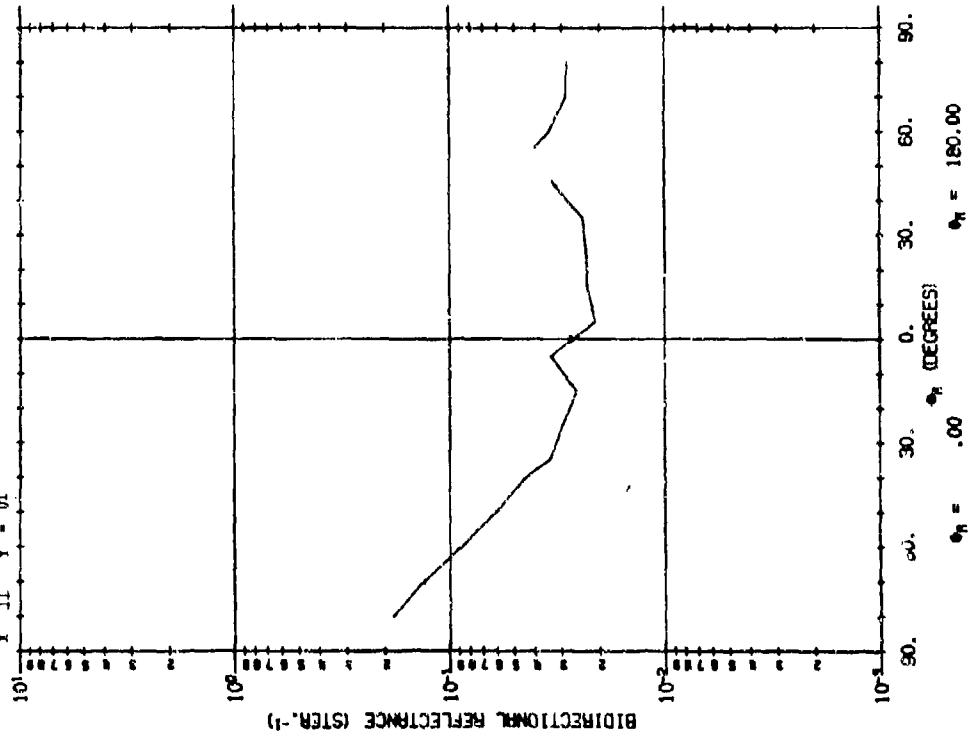


CLOTH AND CANVAS

A01486 002

Cotton, Sulfur Dye, Mercerized Medium

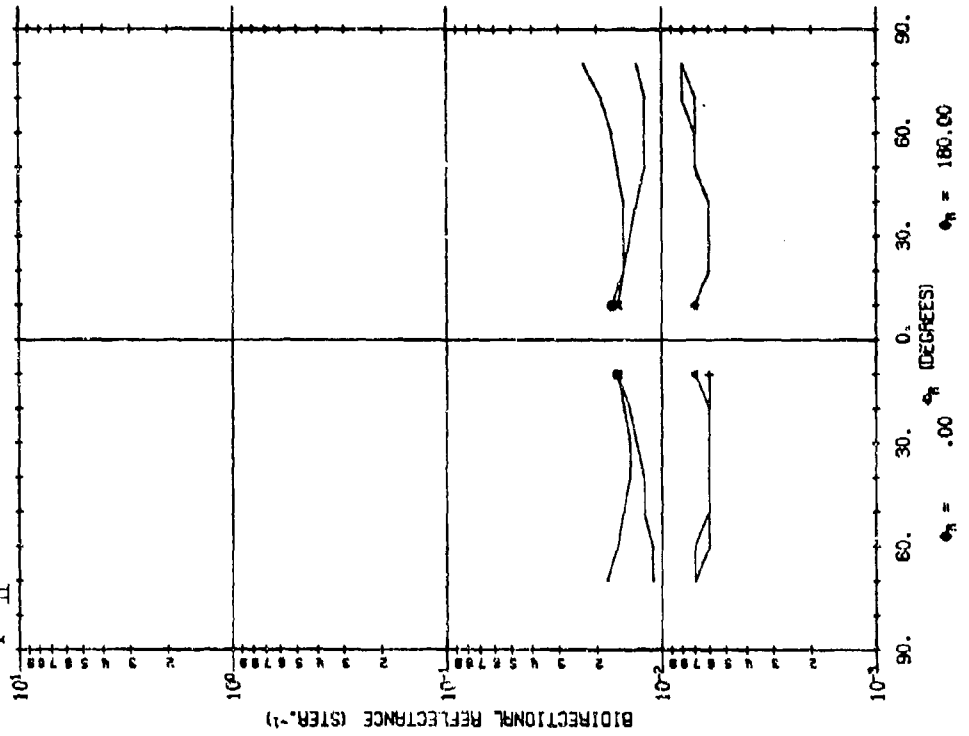
0 // $\epsilon_1 = 50.0$
+ // $\phi_1 = 180.0$
Δ // $\chi = 10.6$
X // $\gamma = VI$



A01510 001

OLIVE DRAB CANVAS TAMPALIN

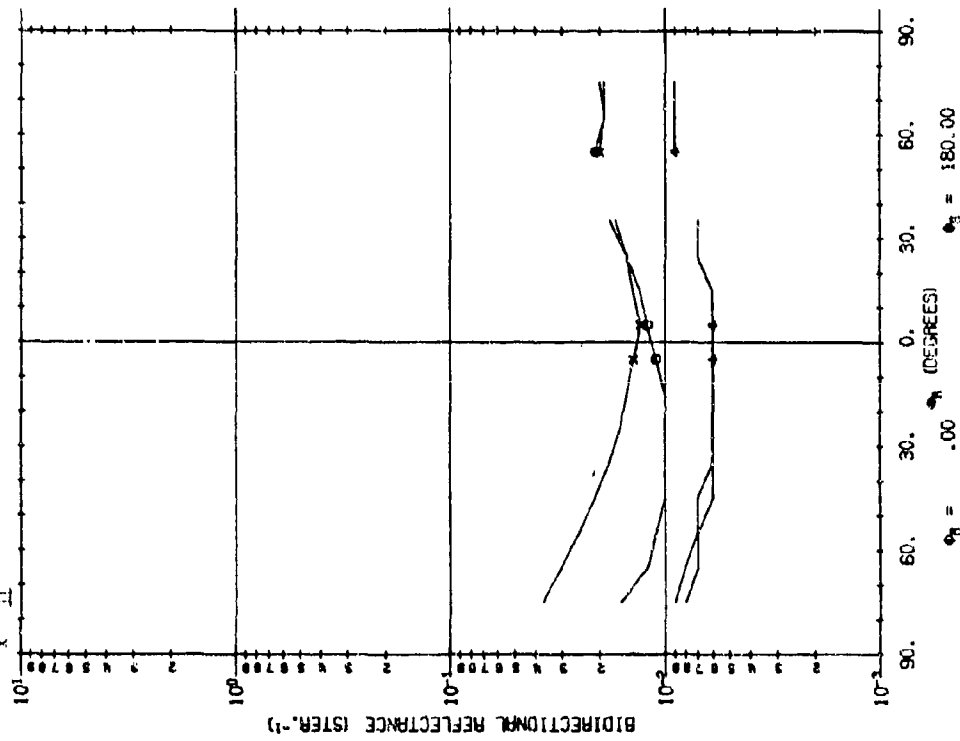
0 // $\epsilon_1 = 0.0$
+ // $\phi_1 = 180.0$
Δ // $\chi = 0.63$
X // $\gamma = II$



R01510 001

OLIVE DRAB CASVAS TARETTLES

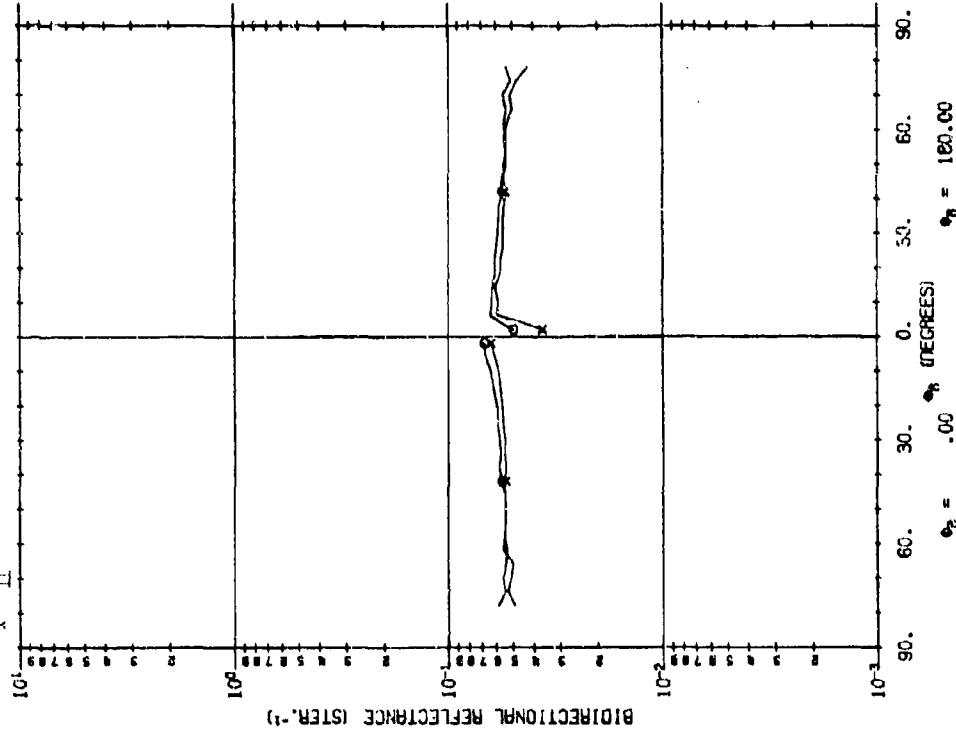
0 $\rho_1 = 45.0$
+ $\rho_2 = 180.0$
- $\rho_3 = 0.63$
X $\rho_4 = 0.63$



R01667 101

Red Canvas

0 $\rho_1 = 0.0$
+ $\rho_2 = 0.0$
- $\rho_3 = 0.63$
X $\rho_4 = 0.63$

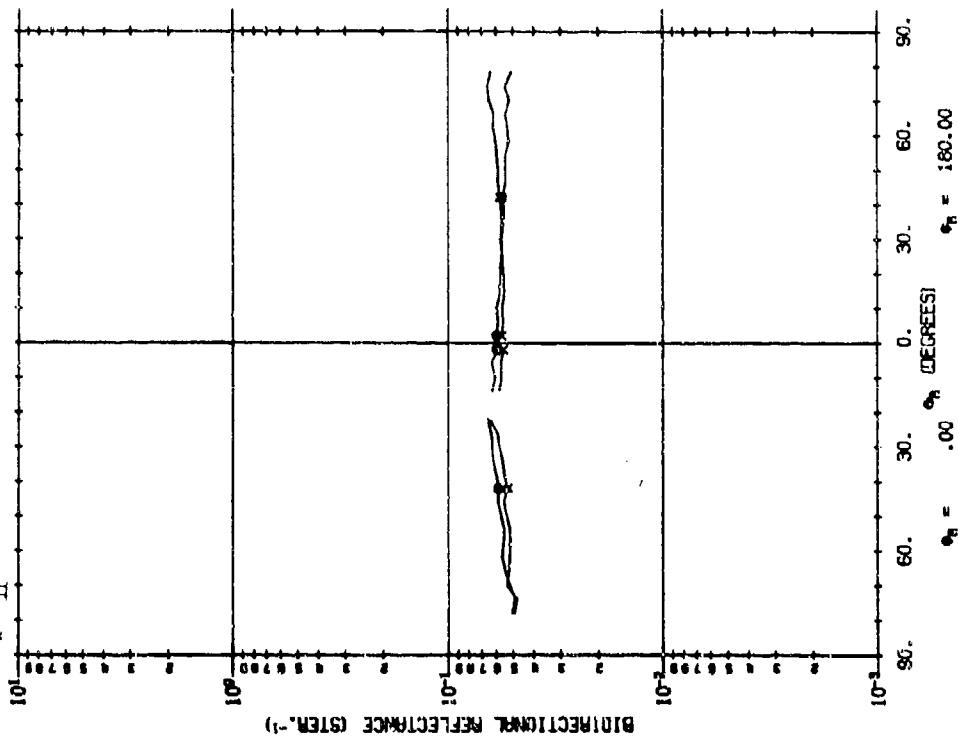


AO1667 101

Ref Curves

$\theta_1 = 20.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

0 || ||
+ || ||
A || ||
X || ||

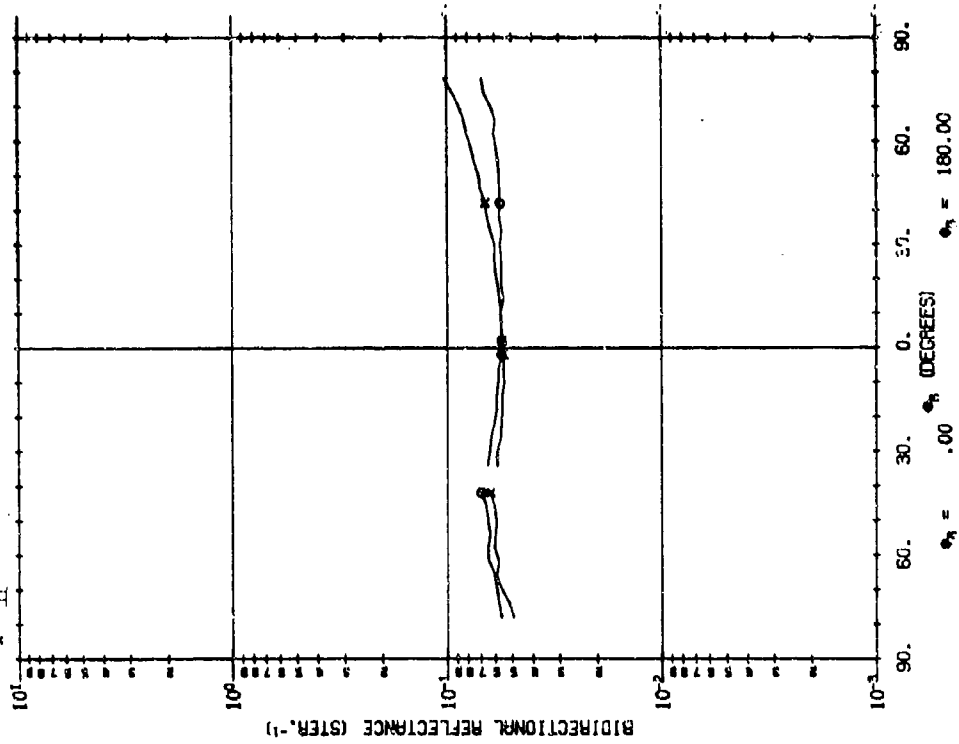


AO1667 101

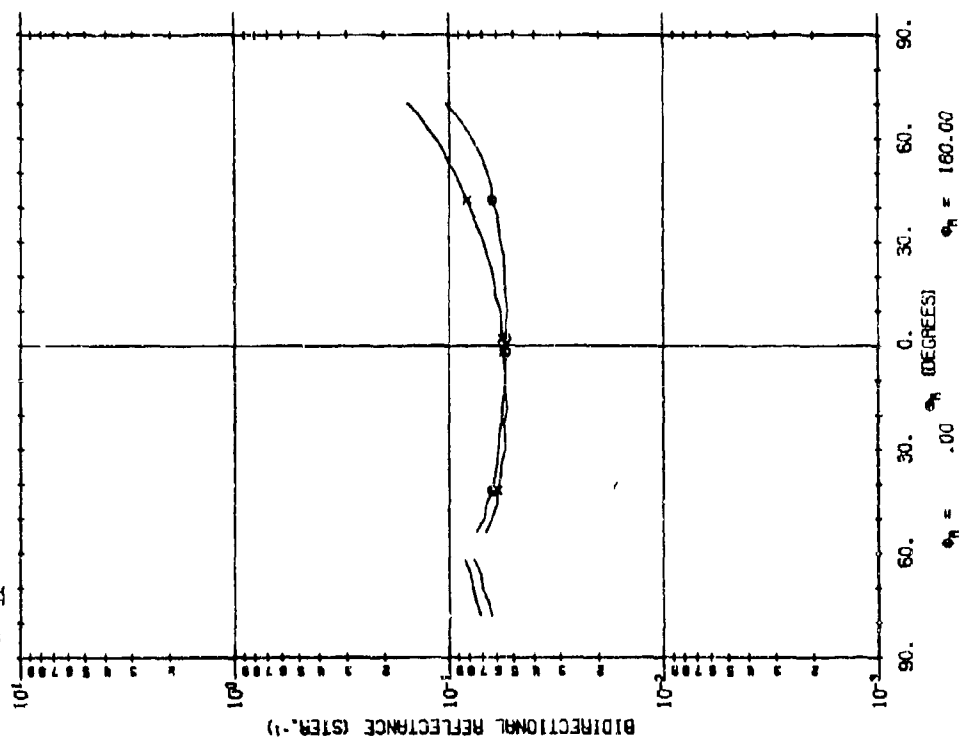
Ref Curves

$\theta_1 = 40.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

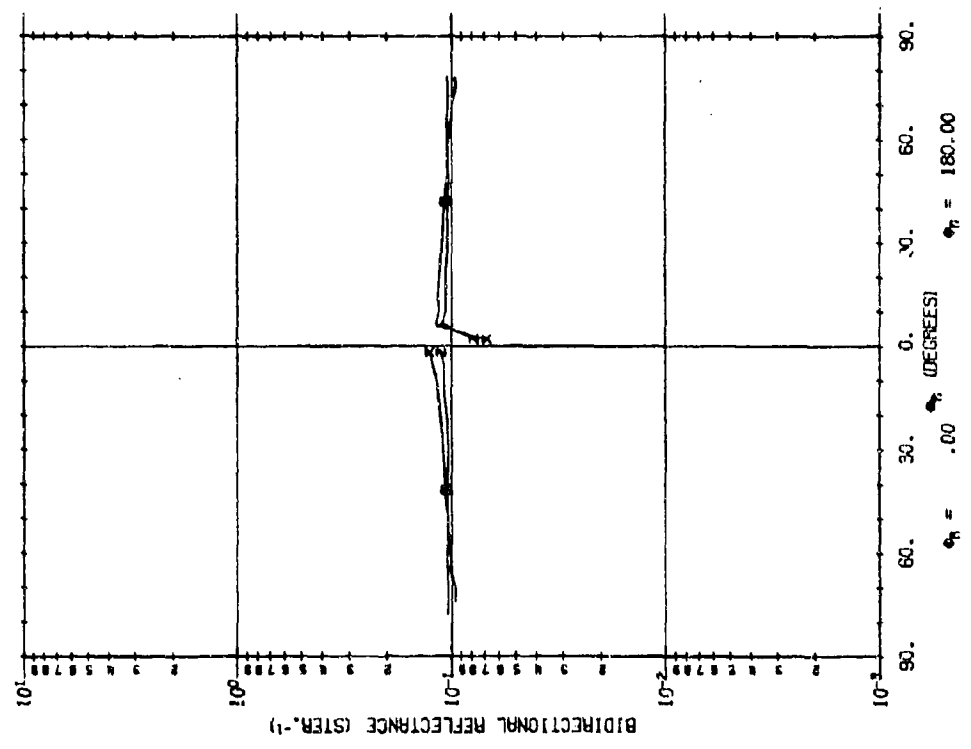
0 || ||
+ || ||
A || ||
X || ||



A01667 101
 Ref Canvas
 $\theta_1 = 60.0$
 $\psi_1 = 0.0$
 $\lambda = 0.63$



A01667 103
 Red Canvas
 $\theta_1 = 0.0$
 $\psi_1 = 0.0$
 $\lambda = 0.63$

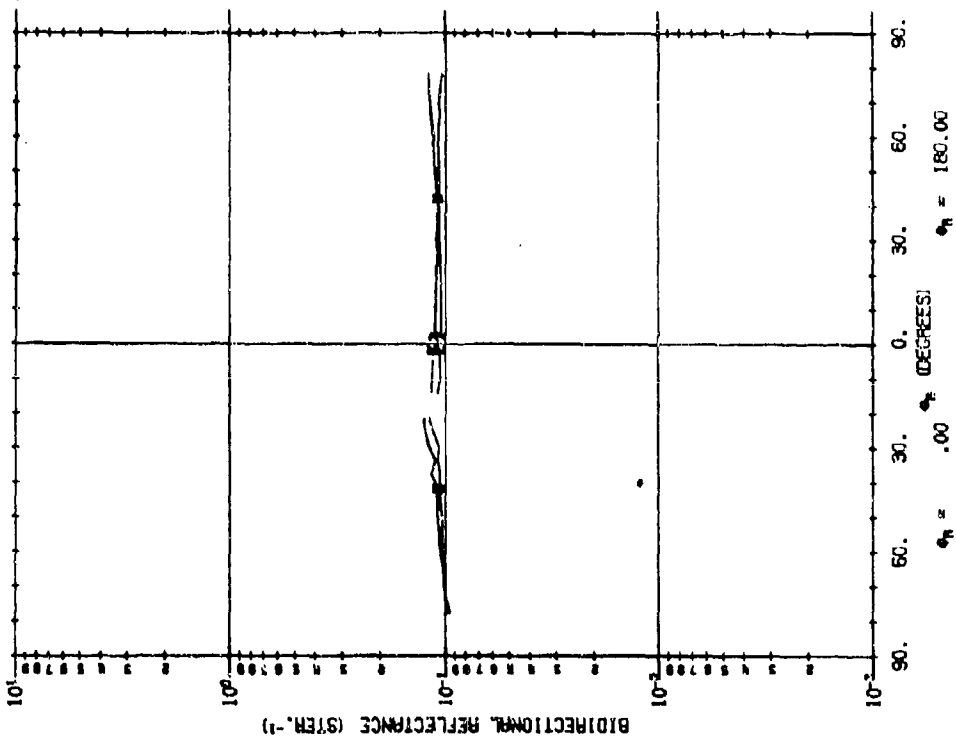


CLOTH AND CANVAS

A01667 103

Red Curves

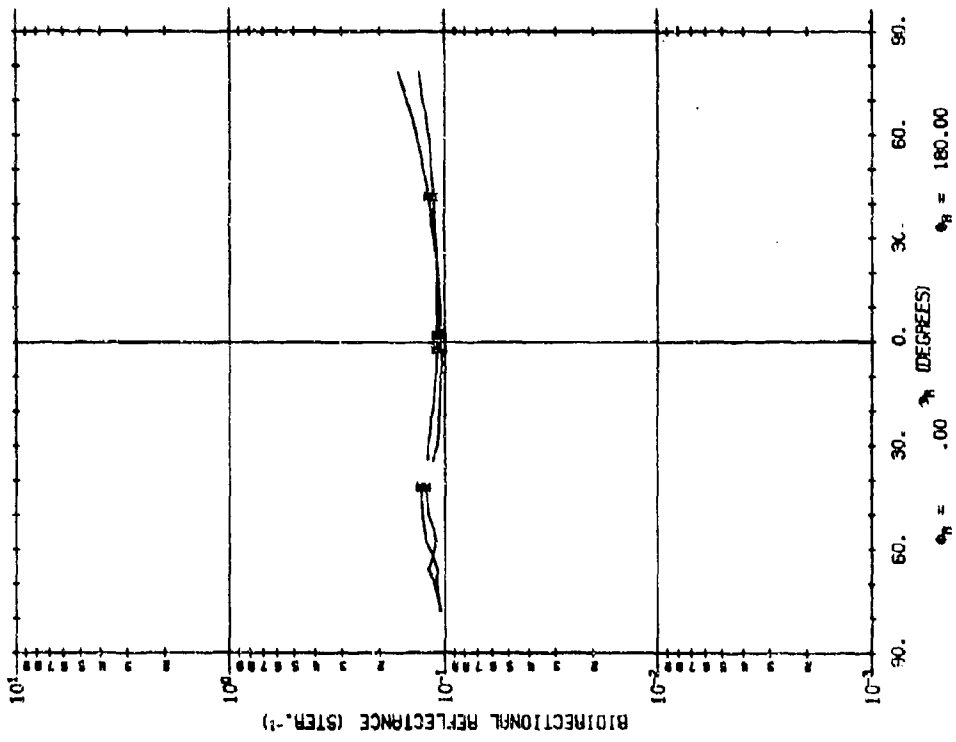
$\theta_1 = 20.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$



A01667 103

Red Curves

$\theta_1 = 40.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$



A01667 103

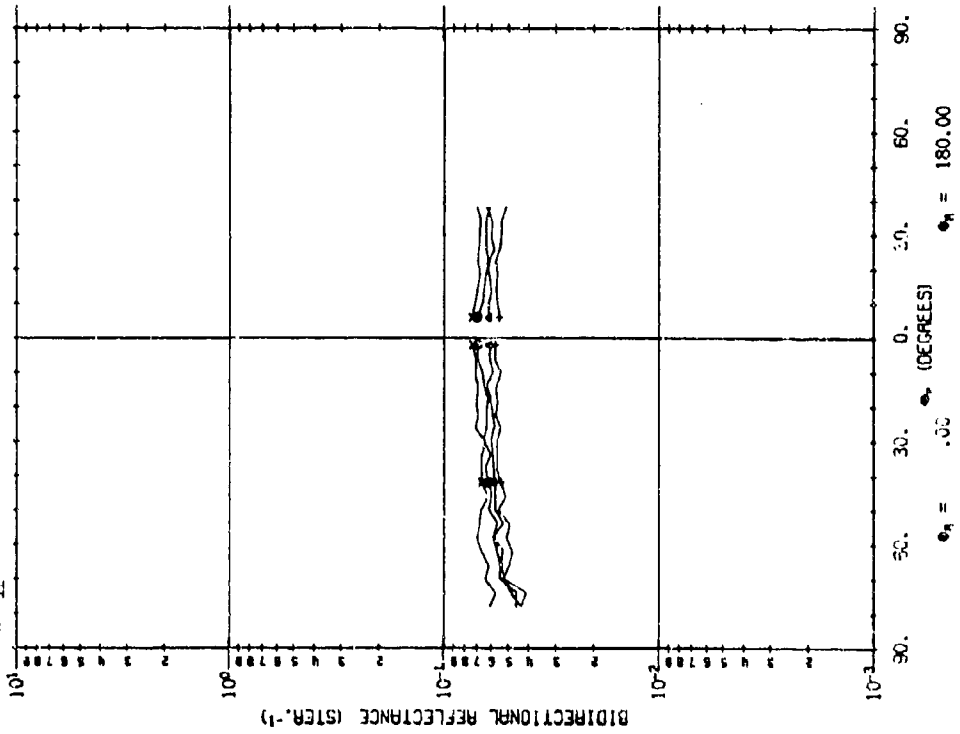
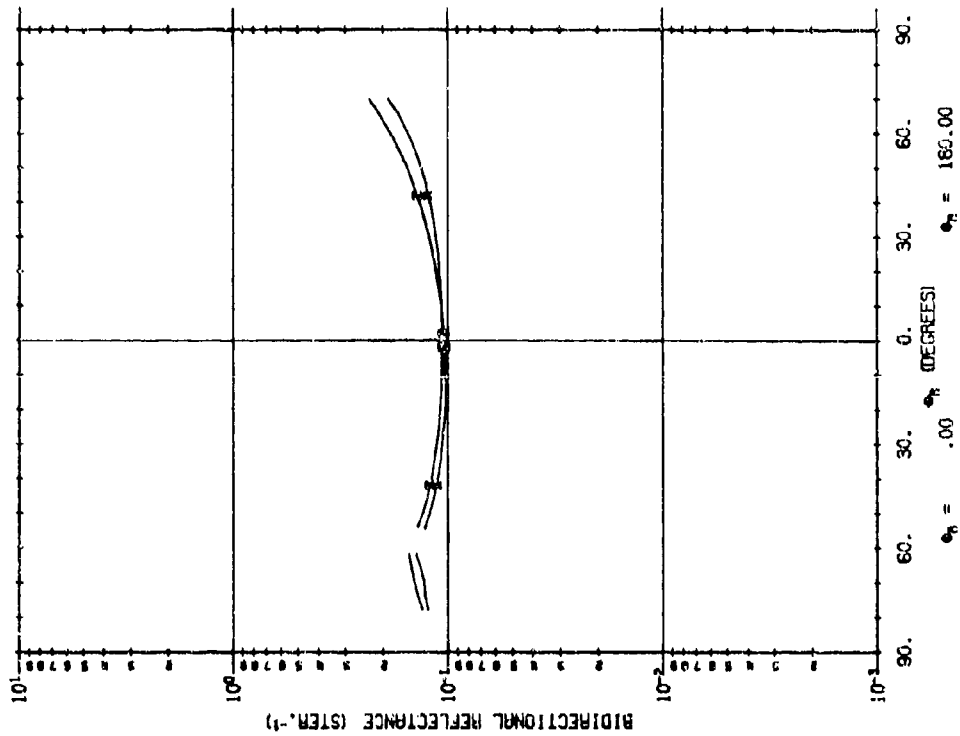
Red Canvas

X 11
Y 12
Z 13
A 0.65

A01667 102

RED CANVAS

X 11
Y 12
Z 13
A 1.15

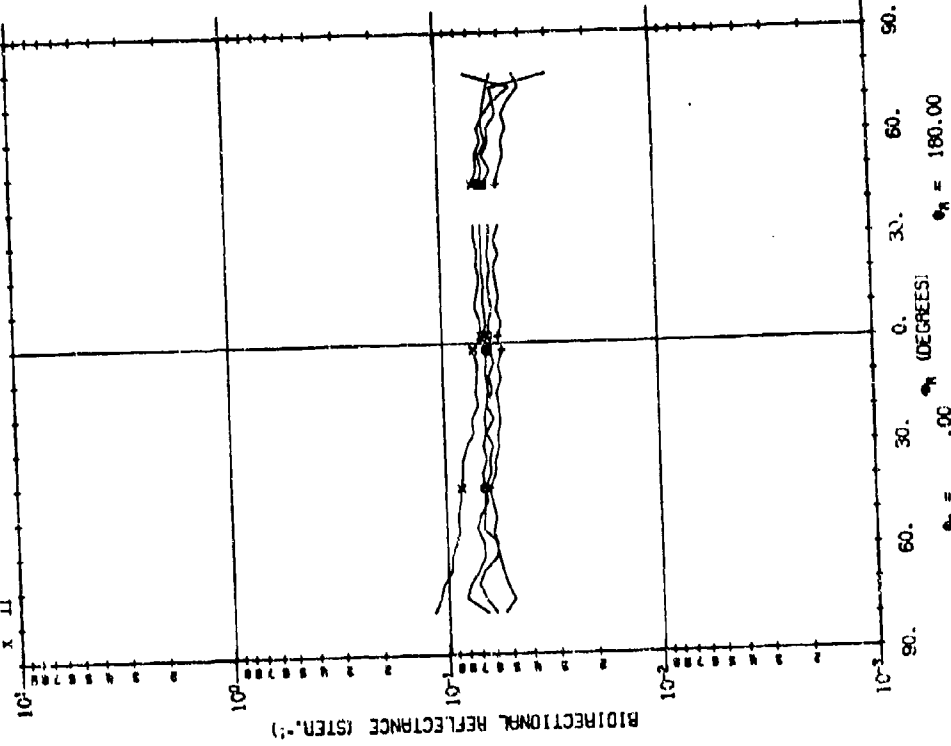


CLOTH AND CANVAS

R01667 102

KEE CARVAS

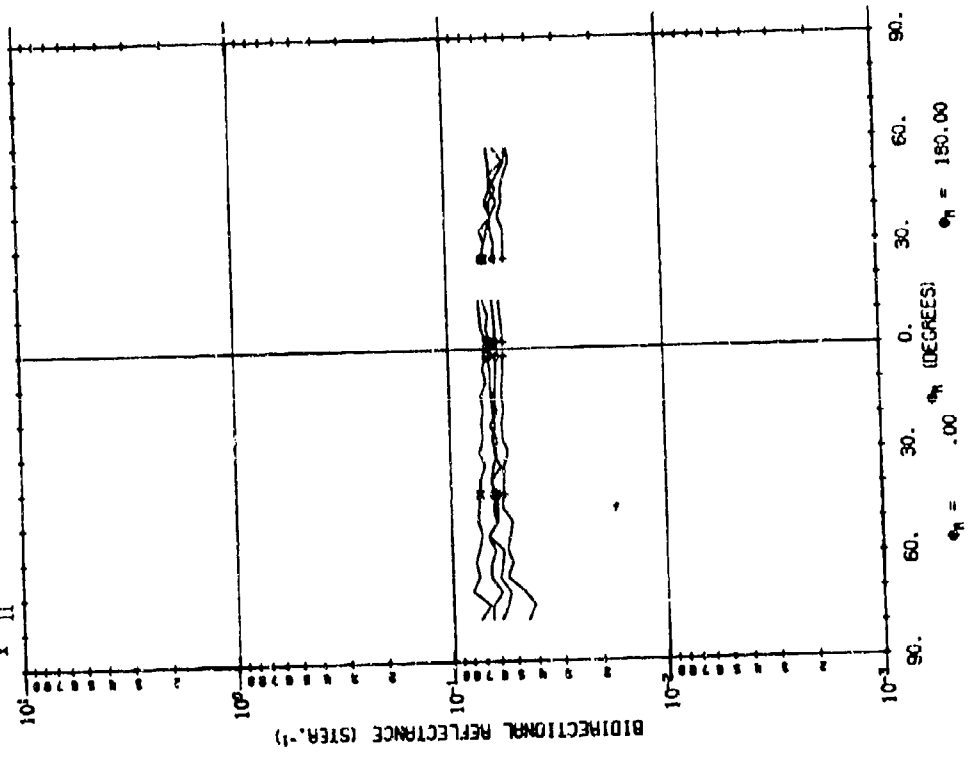
0		$\epsilon_1 = 40.0$
+		$\epsilon_2 = 180.0$
Δ		$\lambda = 1.15$
X		



R01667 102

KEE CARVAS

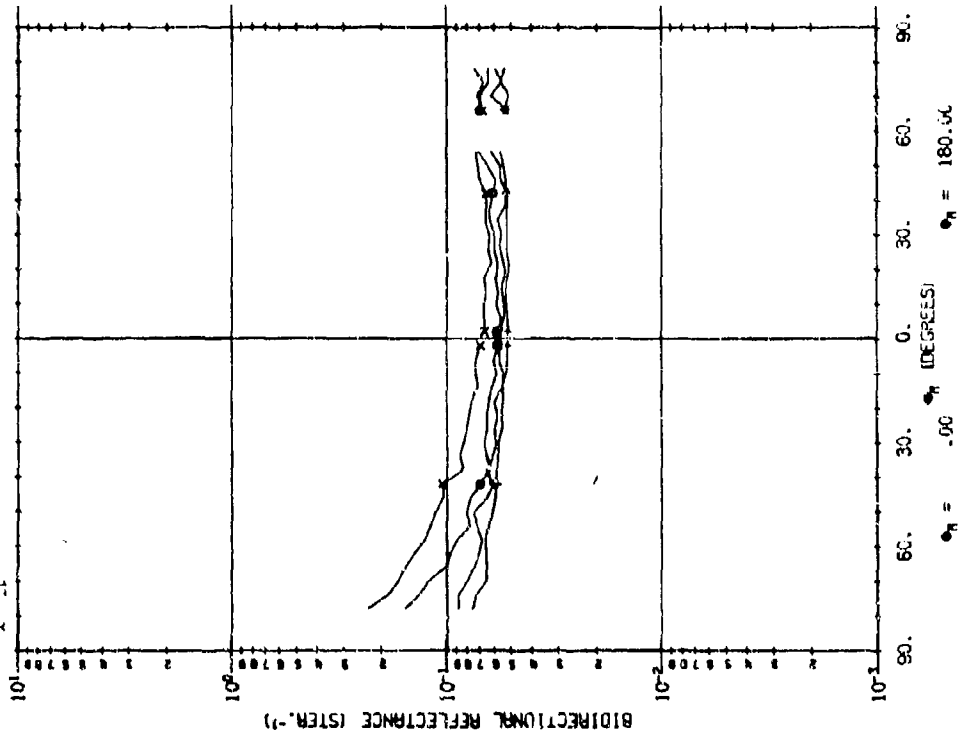
0		$\epsilon_1 = 20.0$
+		$\epsilon_2 = 180.0$
Δ		$\lambda = 1.15$
X		



AO1667 102

RED CANVAS

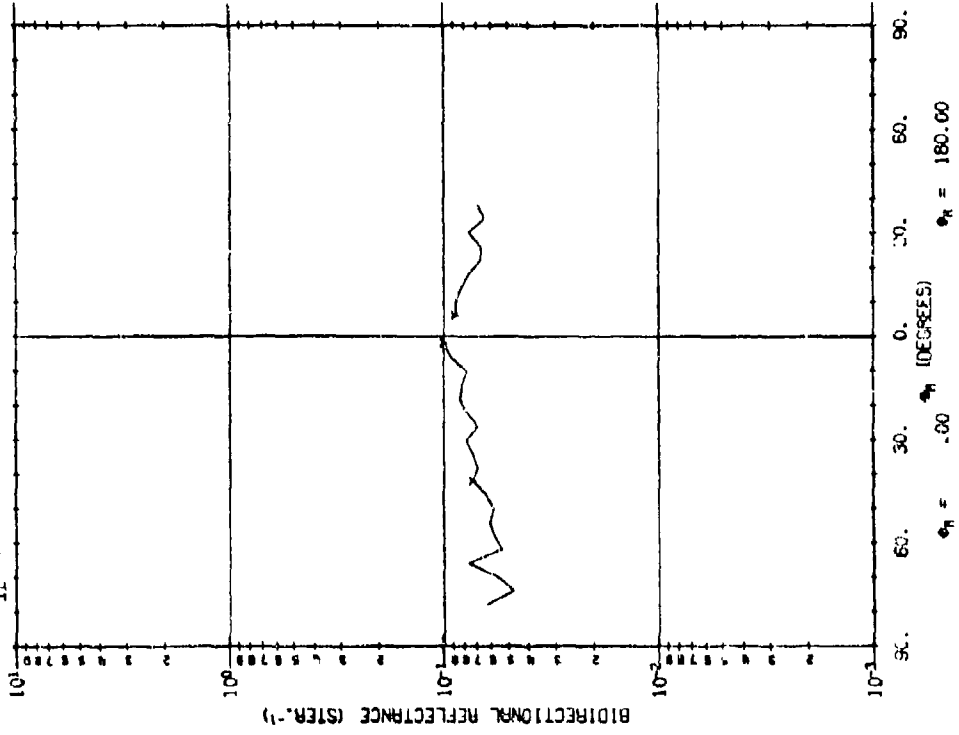
0 || $\epsilon_1 = 60.0$
+ || $\epsilon_2 = 180.0$
Δ || $\lambda = 1.15$
x || $\gamma = 51$



AO1668 102

BLUE CANVAS

0 || $\epsilon_1 = 0.0$
+ || $\epsilon_2 = 180.0$
Δ || $\lambda = 0.46$
x || $\gamma = 51$

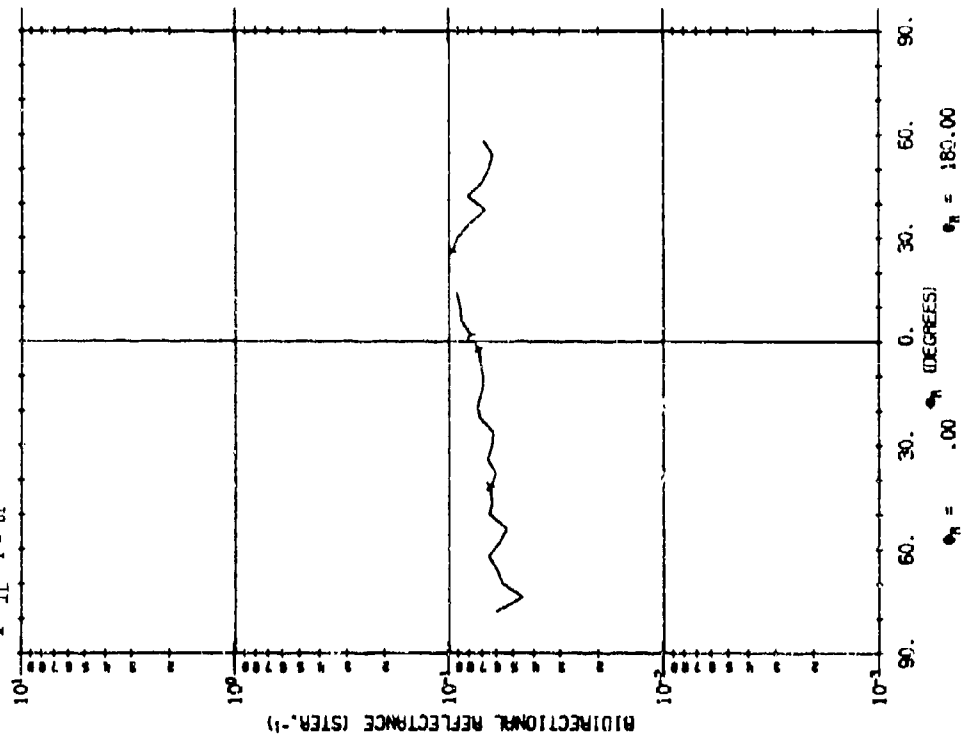


CLOTH AND CANVAS

AO1668 102

BLUE CANVAS

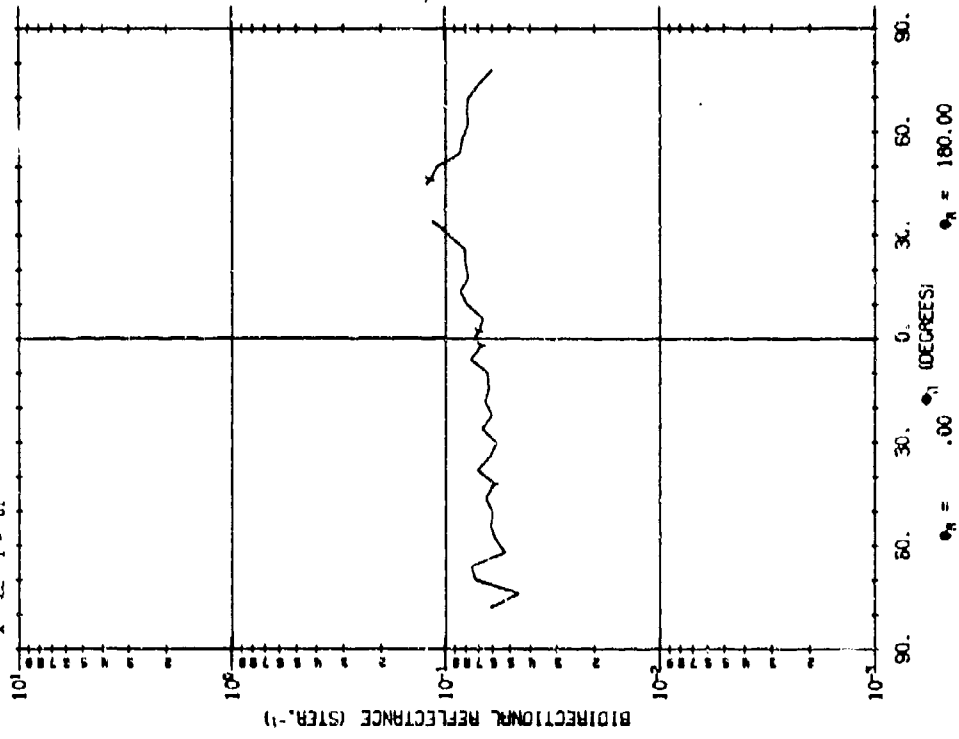
C || $\theta_1 = 20.0$
+ || $\theta_2 = 180.0$
A || $\lambda = 0.46$
X || Y = UT



AO1668 102

BLUE CANVAS

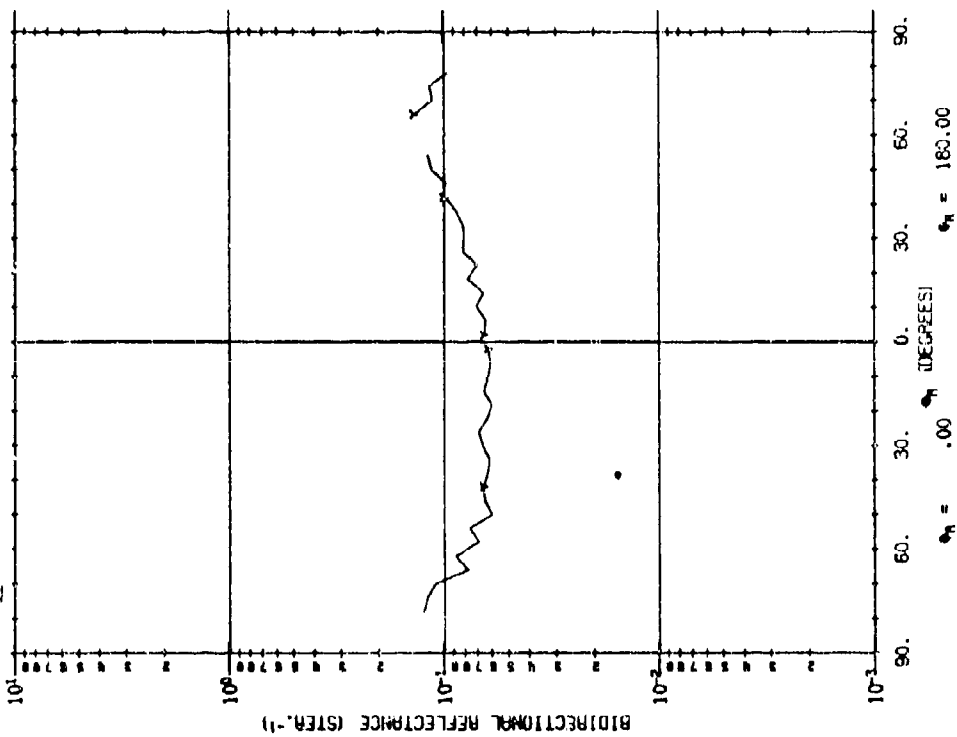
C || $\theta_1 = 40.0$
+ || $\theta_2 = 180.0$
A || $\lambda = 0.45$
X || Y = UT



A01668 102

BLUE CANVAS

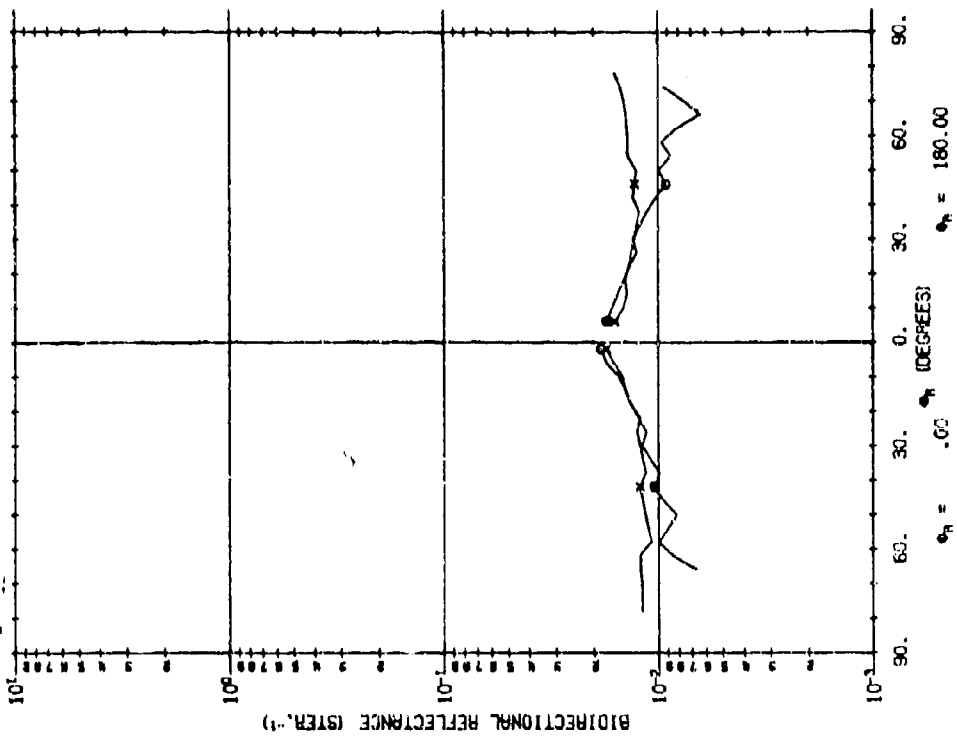
$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\theta_3 = 0.46$
 $\lambda = 0.0$
 $\mu = 0.0$



A01668 101

BLUE CANVAS

$\theta_1 = 60.0$
 $\theta_2 = 0.0$
 $\theta_3 = 0.0$
 $\lambda = 0.63$
 $\mu = 0.0$



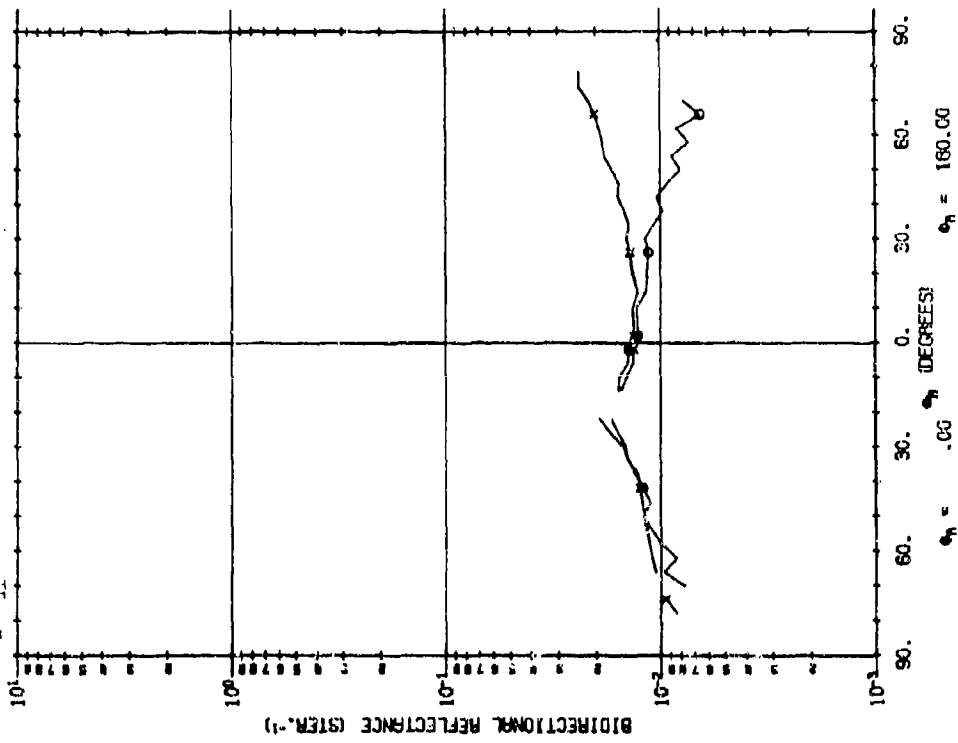
CLOTH AND CANVAS

R01658 101

Blue Canvas

$\theta_1 = 23.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

0 II
+ II
A II
X II

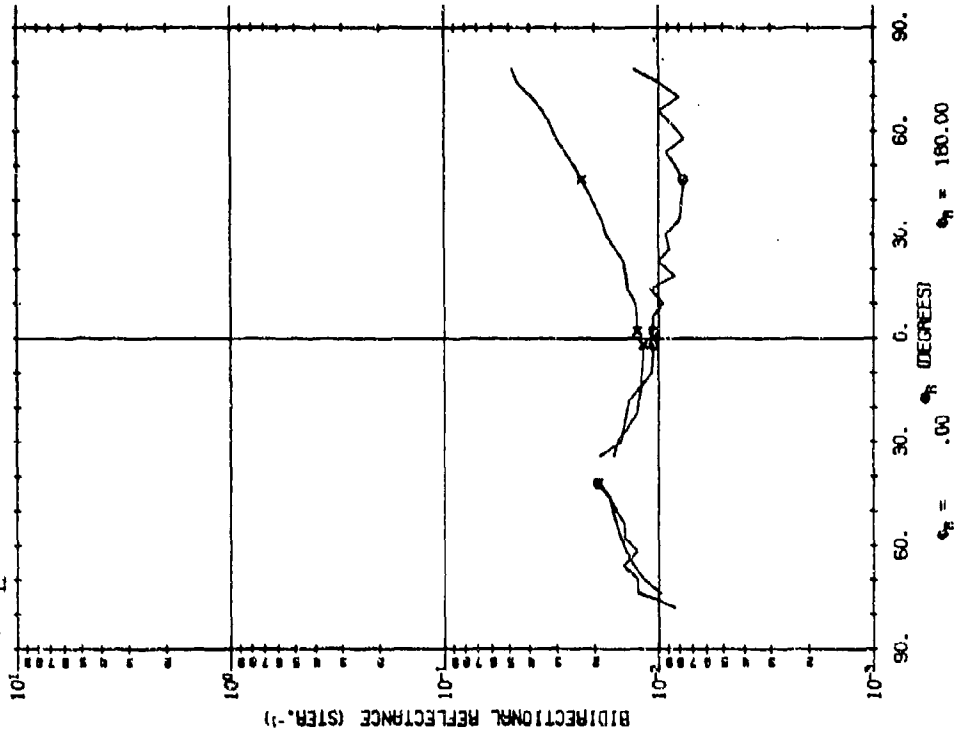


R01658 101

Blue Canvas

$\theta_1 = 40.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

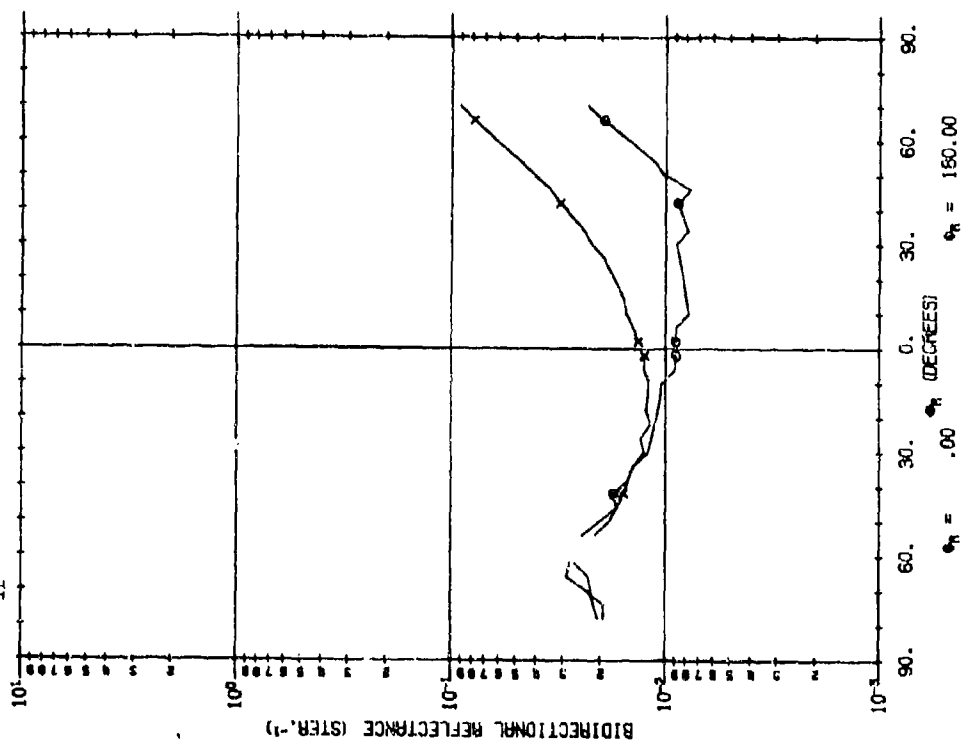
0 II
+ II
A II
X II



R01668 101
 C | |
 + | |
 / | |
 X | |

Blue Curves

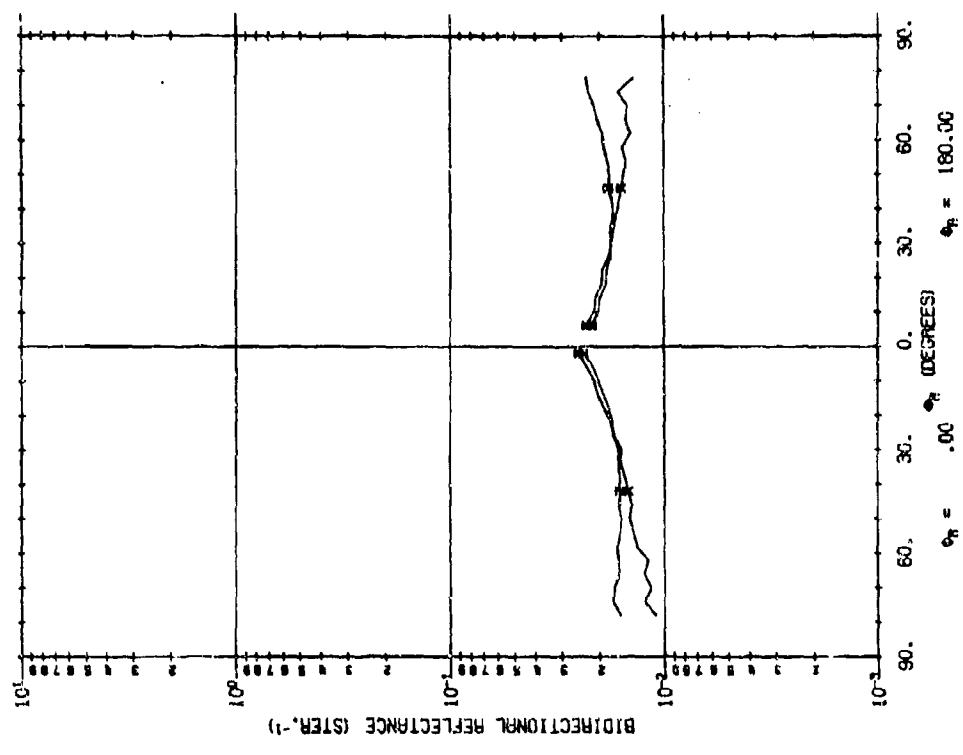
$\theta_1 = 60.0$
 $\theta_2 = 0.0$
 $\theta_3 = 0.0$
 $\lambda = 0.63$



R01668 104
 X | |
 / | |
 X | |

Blue Canvas

$\theta_1 = 0.0$
 $\theta_2 = 0.0$
 $\theta_3 = 0.0$
 $\lambda = 0.63$

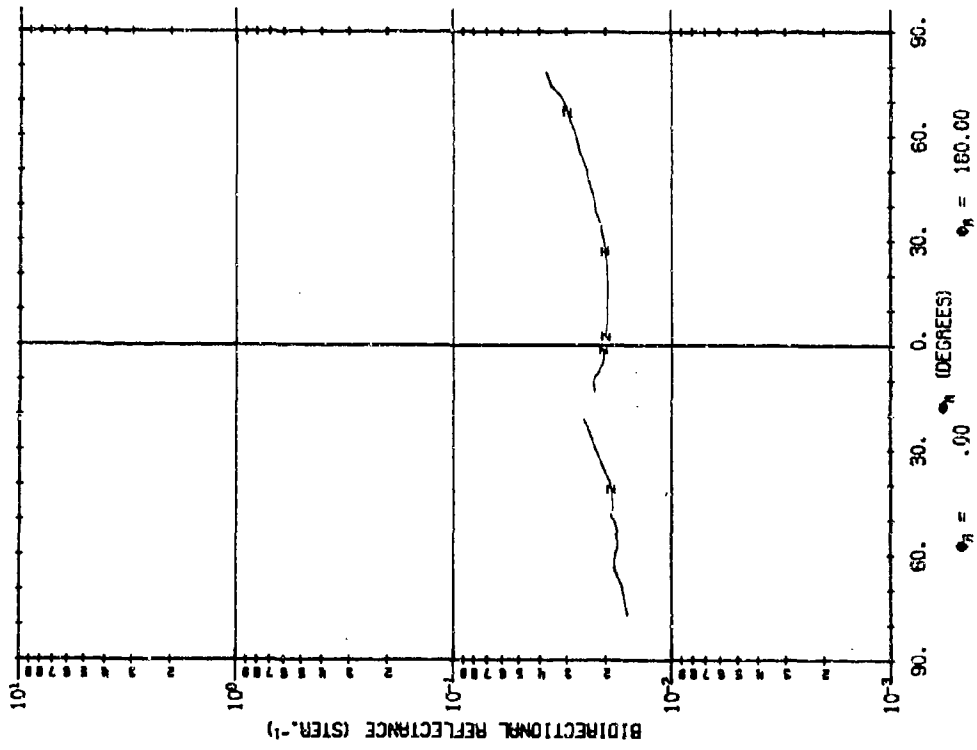


CLOTH AND CANVAS

R01668 104

Blue Canvas

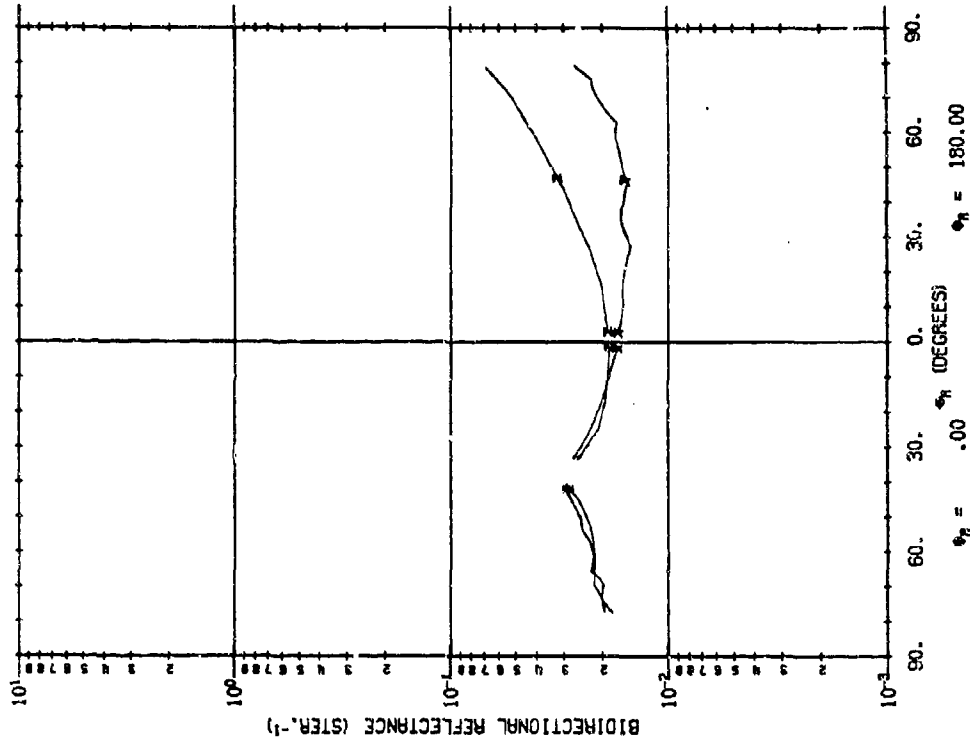
X |T| $\theta_1 = 20.0$
Z |T| $\phi_1 = 0.0$
 $\lambda = 0.63$



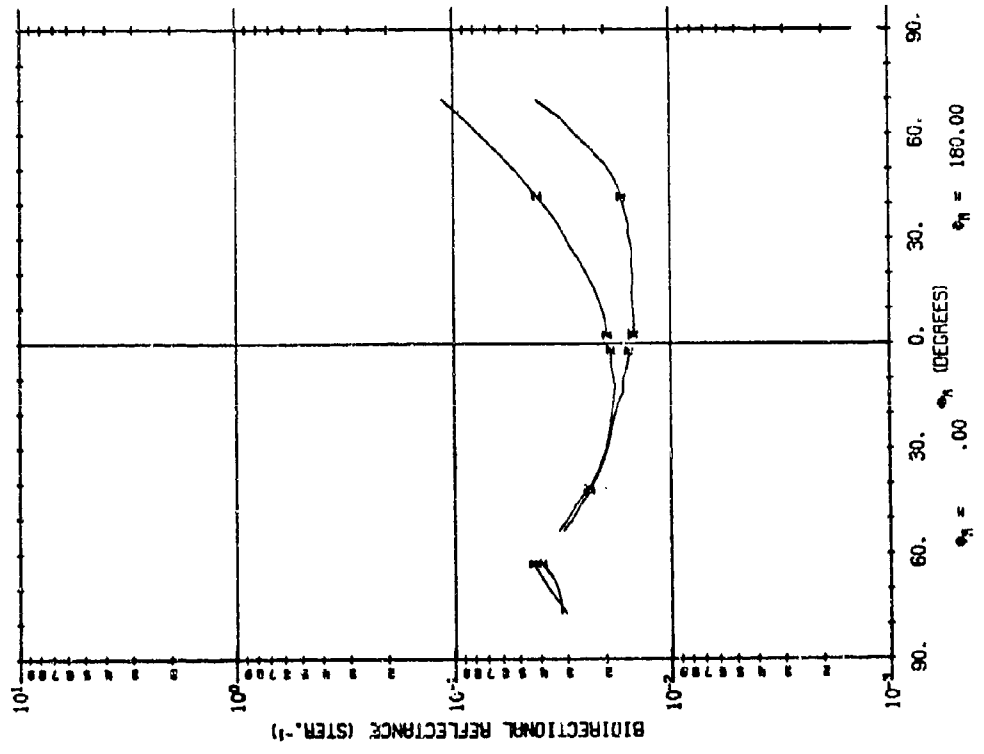
R01668 104

Blue Canvas

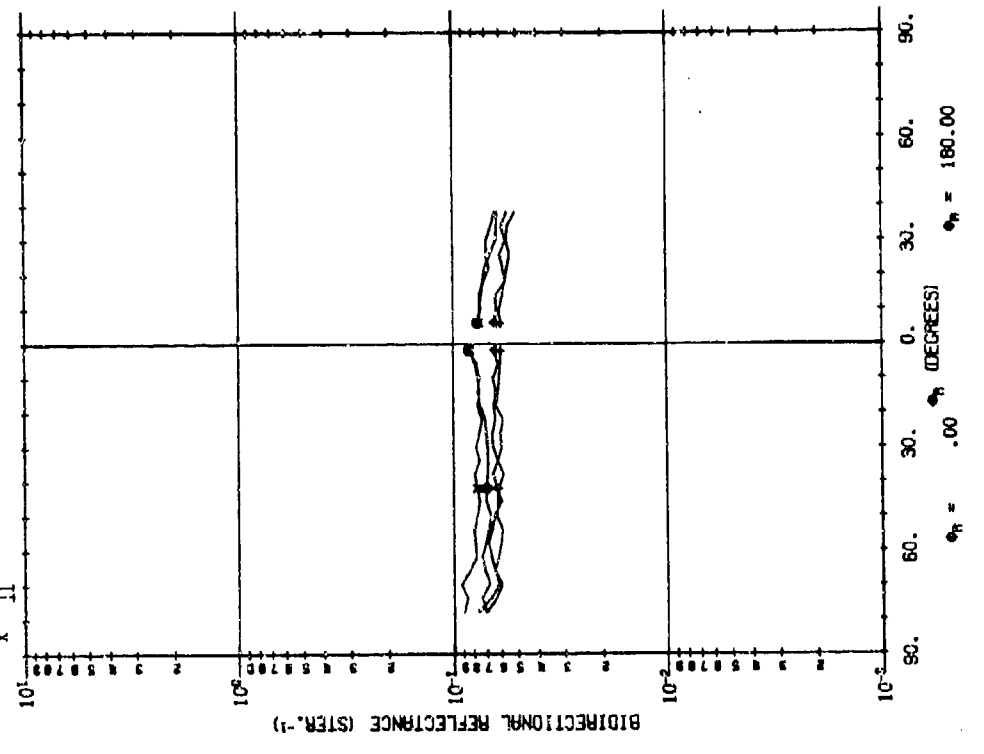
X |T| $\theta_1 = 40.0$
Z |T| $\phi_1 = 0.0$
 $\lambda = 0.63$



R01668 104
 Blue Canvas
 $\theta_1 = 60.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$



R01668 103
 Blue Canvas
 $\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 1.15$

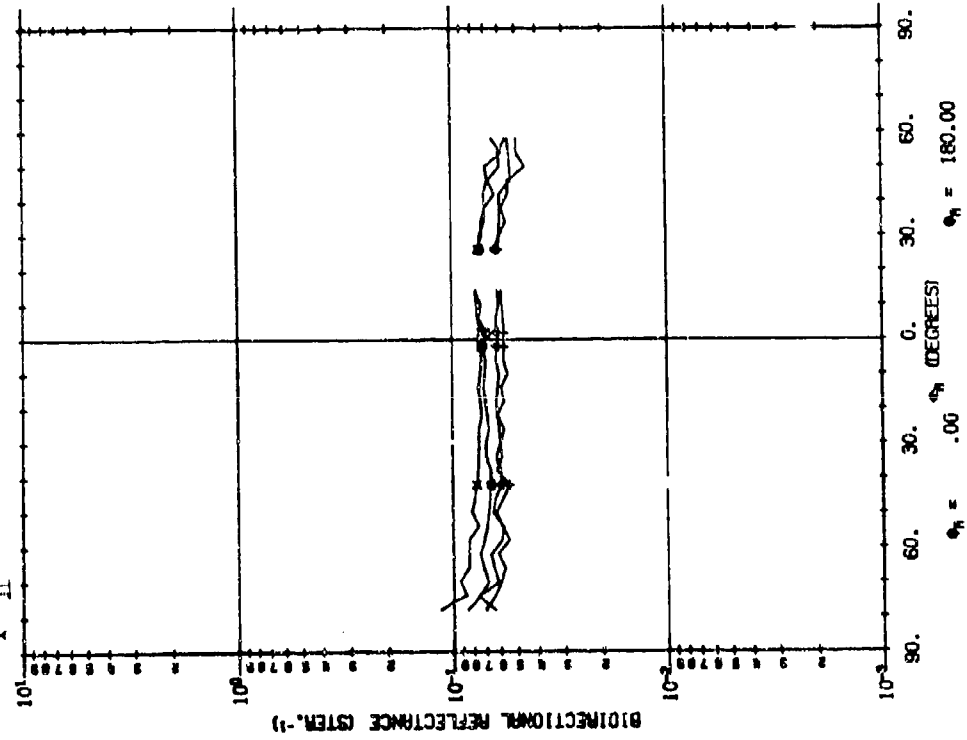


R01668 103

Blue Canvas

$\theta_i = 20.0$
 $\theta_r = 180.0$
 $\lambda = 1.15$

0 ||
+ ||
x ||

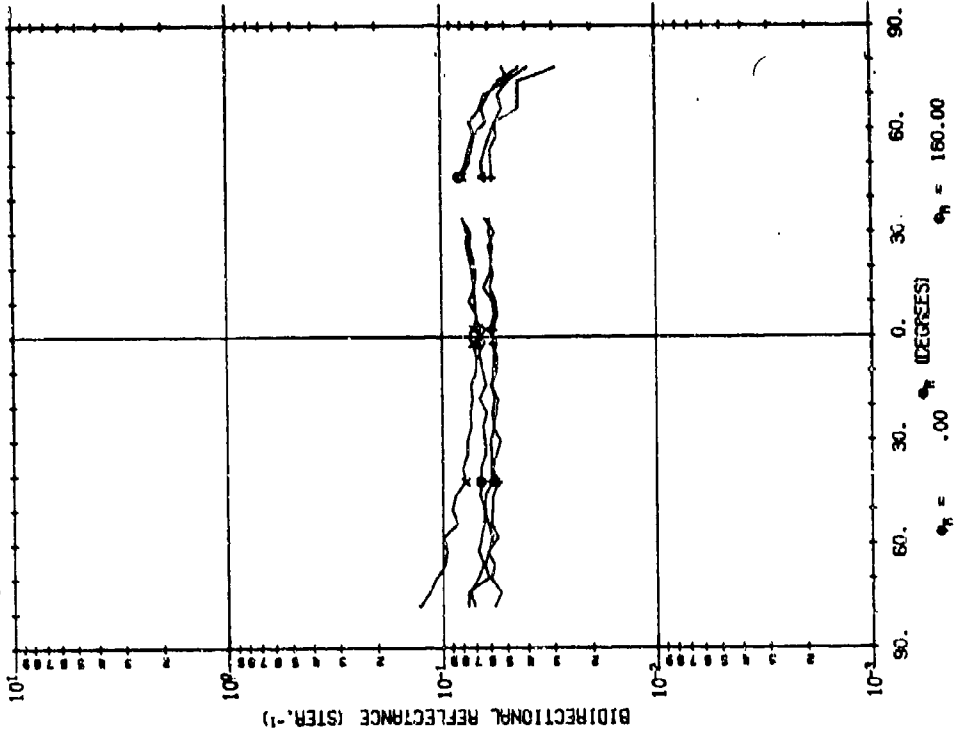


R01668 103

Blue Canvas

$\theta_i = 40.0$
 $\theta_r = 180.0$
 $\lambda = 1.15$

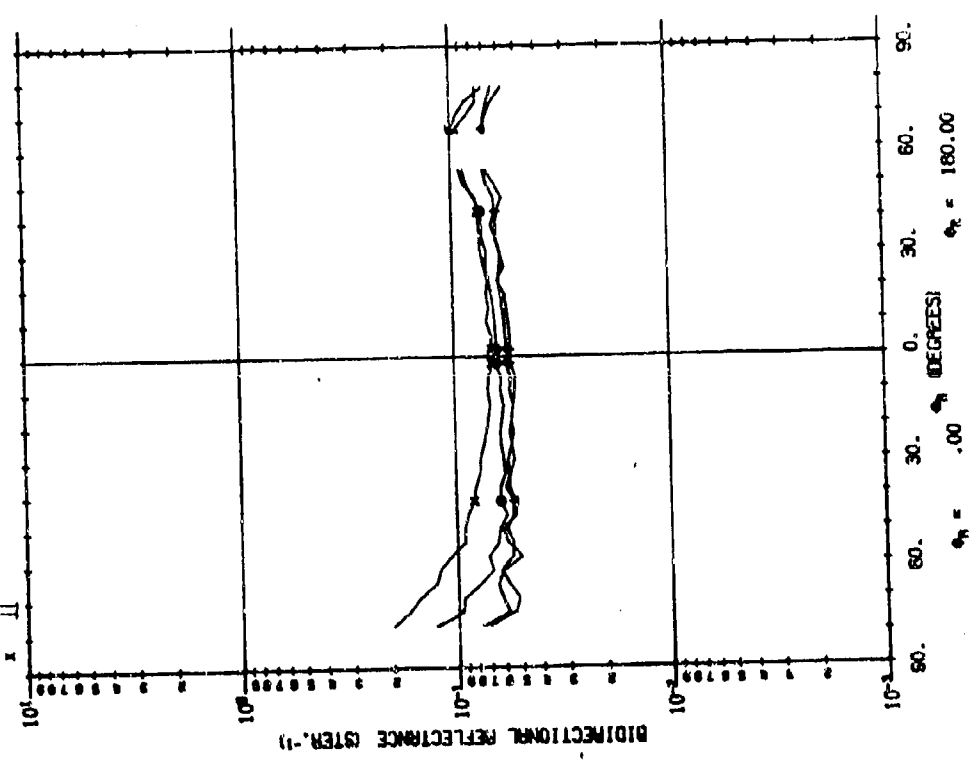
0 ||
+ ||
x ||



R01668 103

Blue Canvas

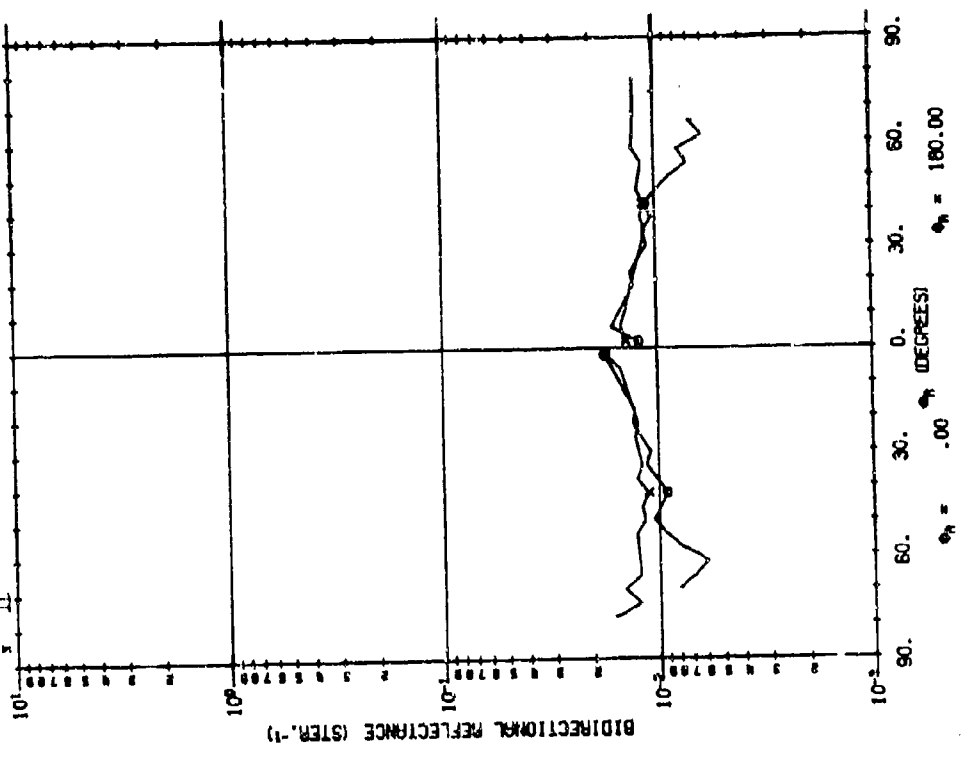
$\phi_1 = 60.0$
 $\phi_2 = 180.0$
 $\lambda = 1.15$



R01669 101

Green Canvas

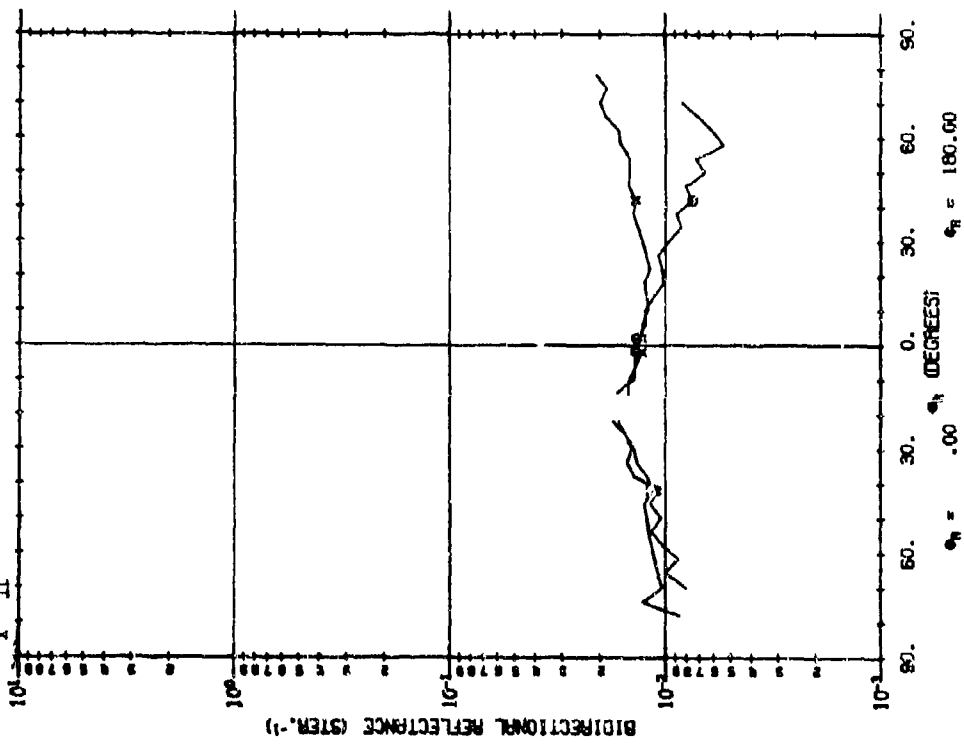
$\phi_1 = 0.0$
 $\phi_2 = 0.0$
 $\lambda = 0.83$



CLOTH AND CANVAS

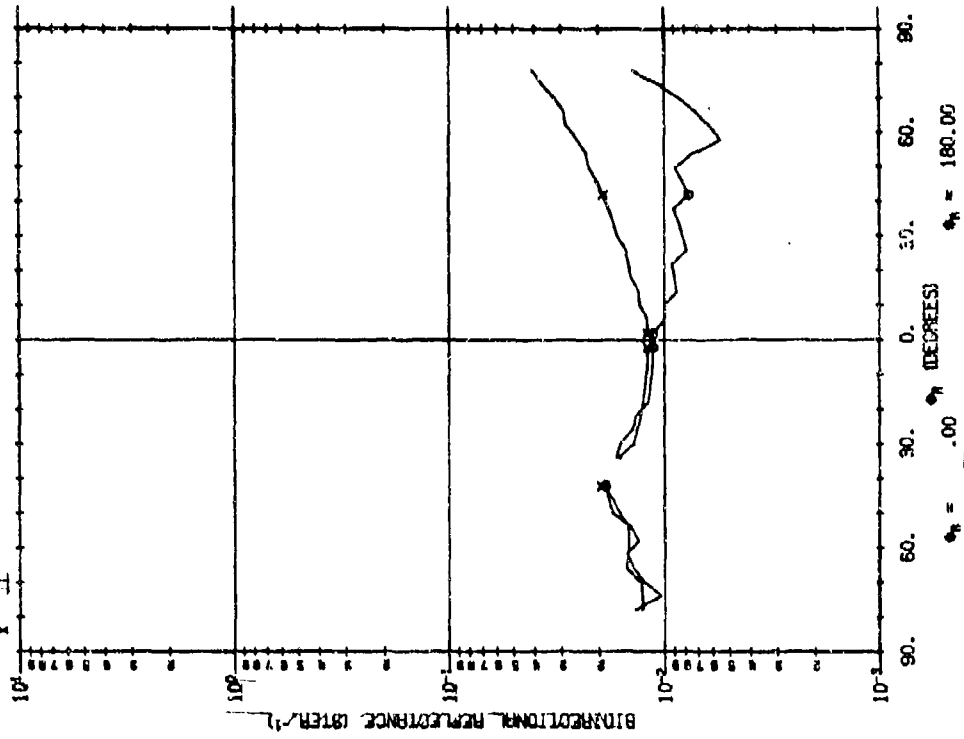
R01669 101
 0 || 20.0
 + || 0.0
 Δ || 0.63
 X ||

Green Canvas

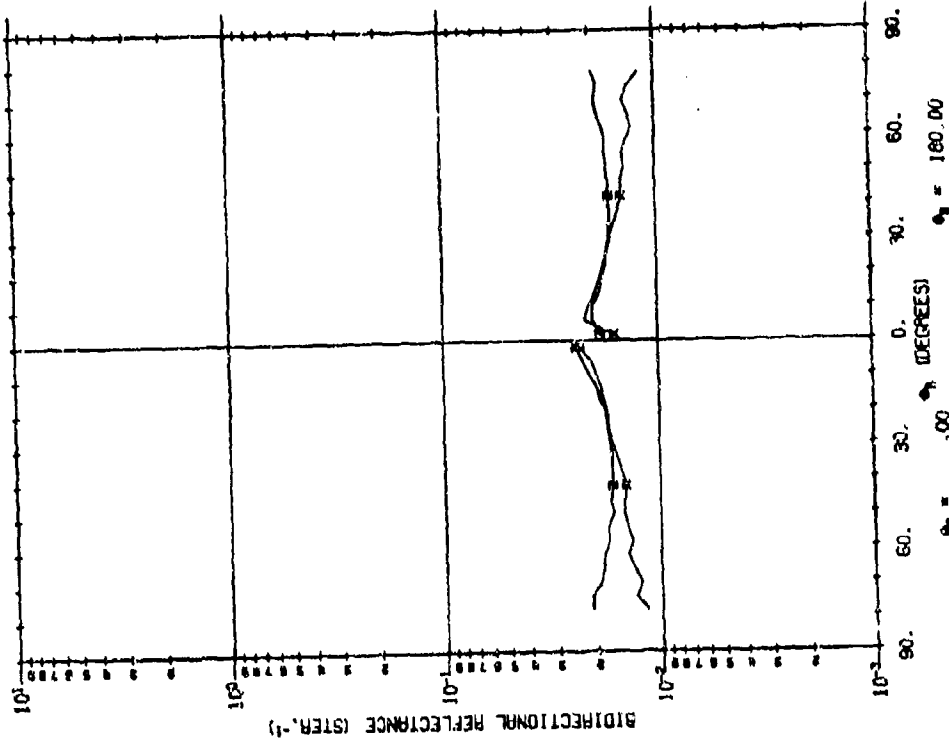


R01669 101
 0 || 40.0
 + || 0.0
 Δ || 0.63
 X ||

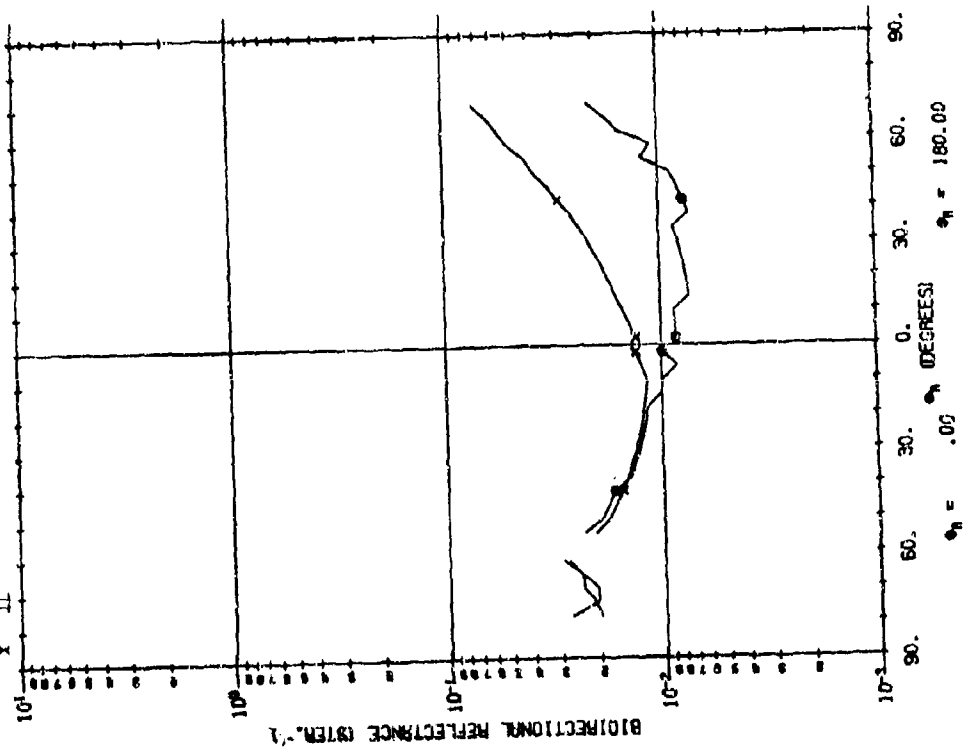
Green Canvas



AO1689 104
 Green Canvas
 $\alpha_1 = 0.0$
 $\alpha_2 = 0.0$
 $\lambda = 0.63$



AO1689 101
 Green Canvas
 $\alpha_1 = 60.0$
 $\alpha_2 = 0.0$
 $\lambda = 0.63$

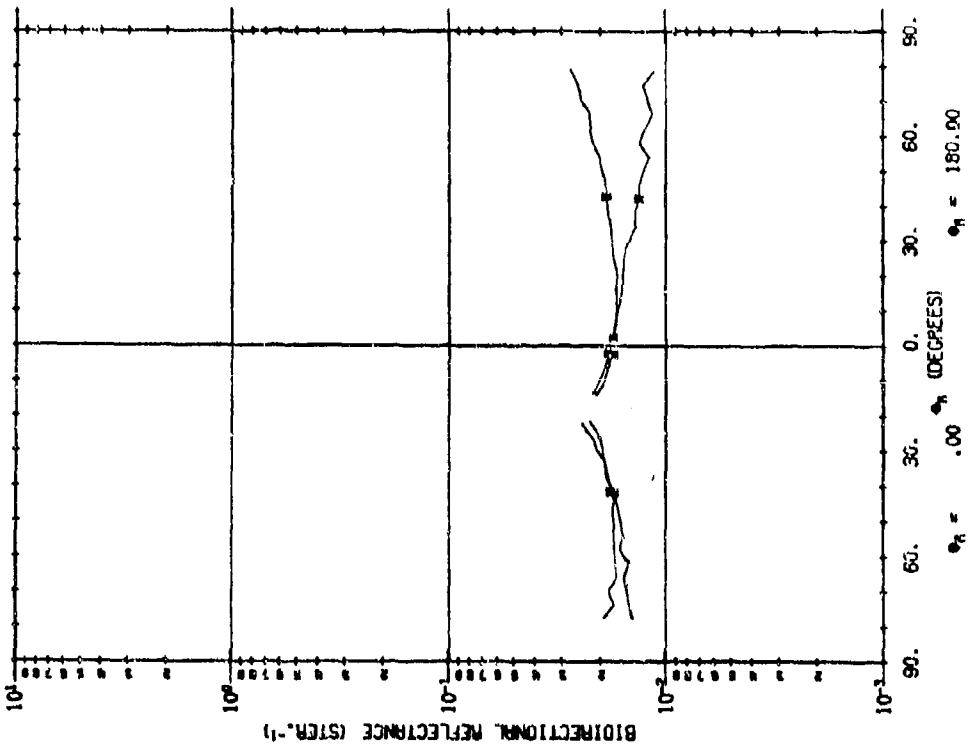


CLOTH AND CANVAS

R01669 104

Green Canvas

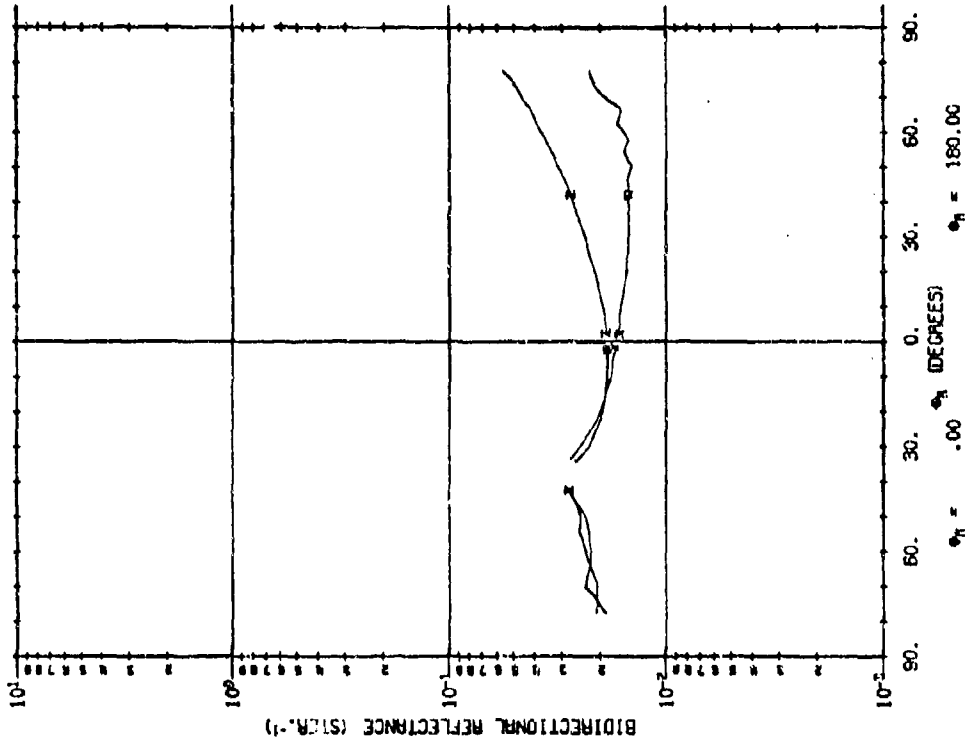
X Γ $\theta_1 = 20.0$
Z Γ $\theta_1 = 0.0$
 $\lambda = 0.63$



R01669 104

Green Canvas

X Γ $\theta_1 = 40.0$
Z Γ $\theta_1 = 0.0$
 $\lambda = 0.63$

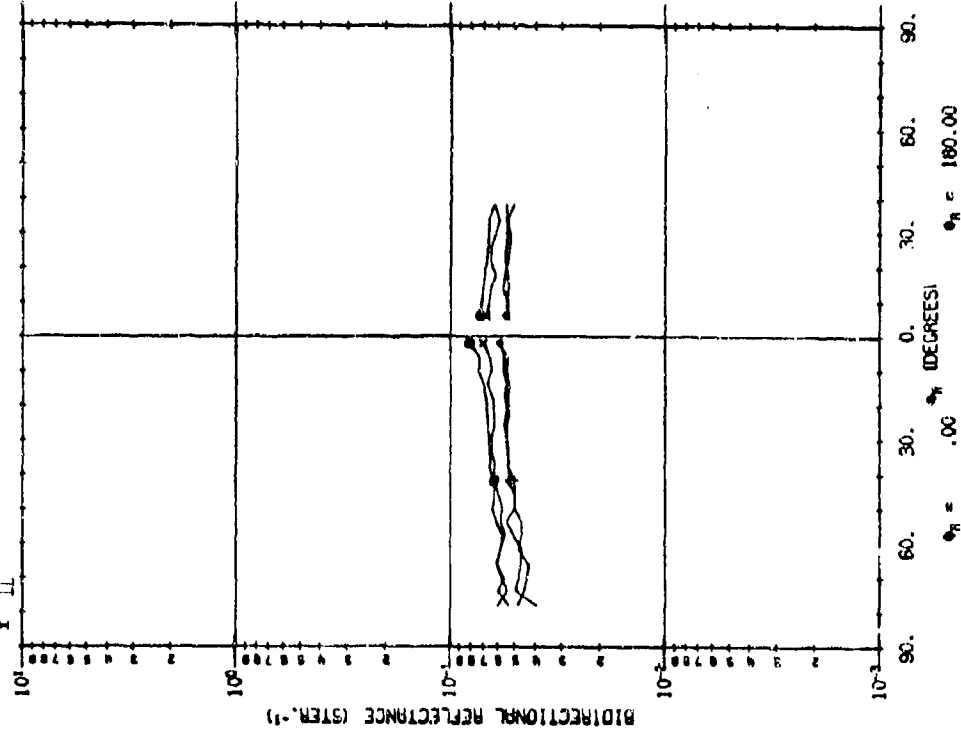
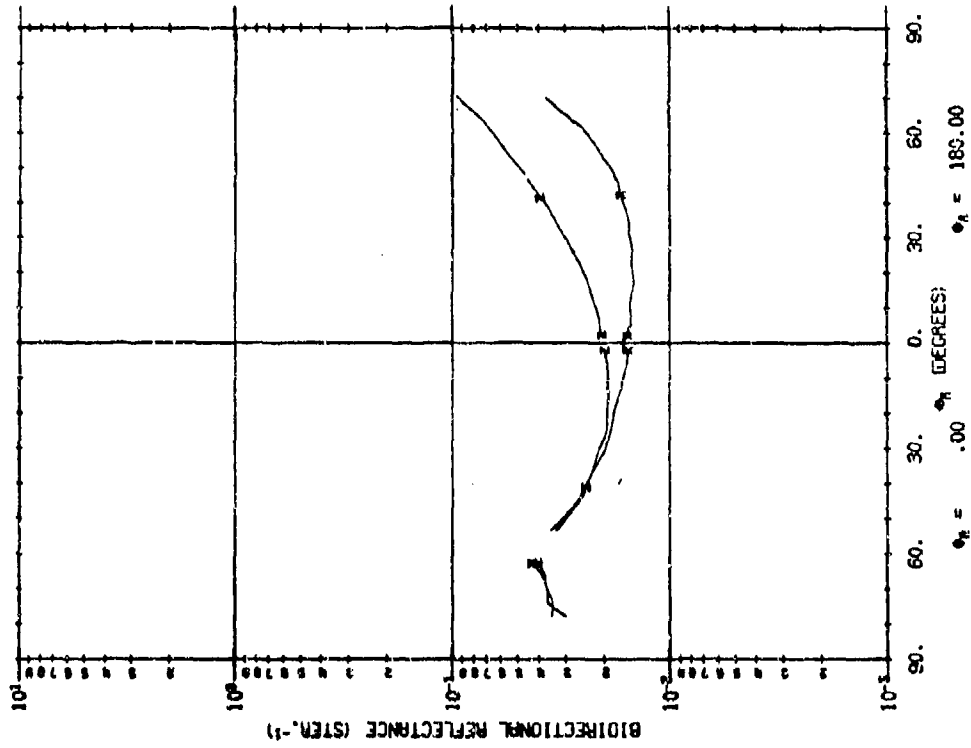


A01659 104

X II $\theta_1 = 60.0$
Z II $\theta_2 = 0.0$
Y = 0.63

A01669 103
CLOTH CANVAS

0 II $\theta_1 = 0.0$
+ II $\theta_2 = 180.0$
Z II $\lambda = 1.15$

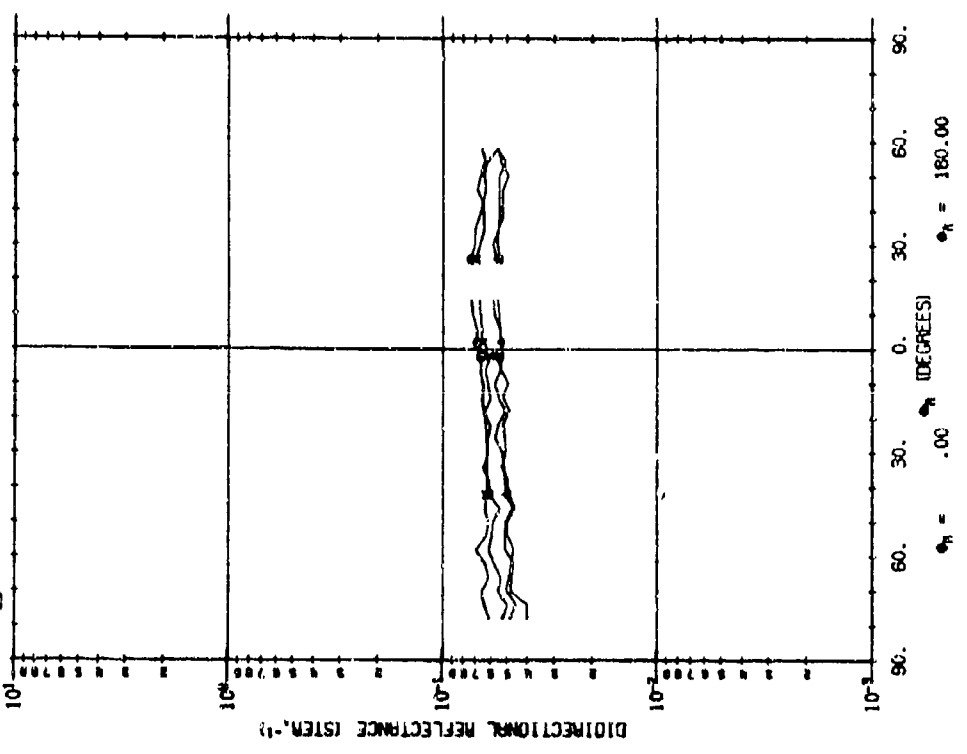


CLOTH AND CANVAS

R01669 103

GREEN CURVAS

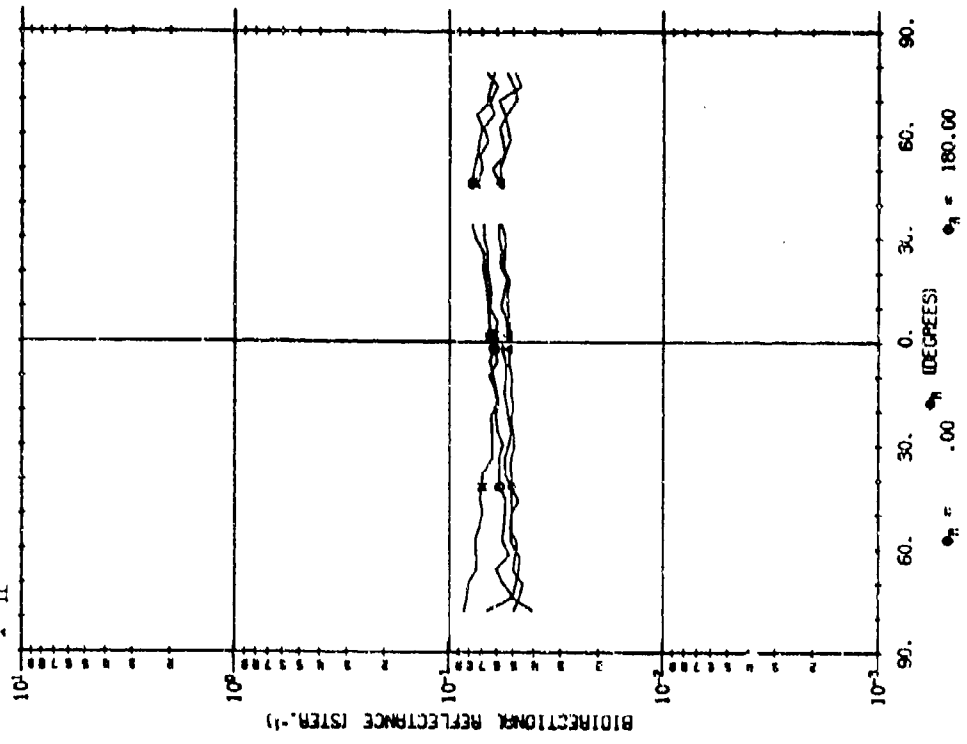
0 | | $\theta_1 = 20.0$
+ | | $\theta_2 = 180.0$
A | | $\lambda = 1.15$
X | |



R01669 103

GREEN CURVAS

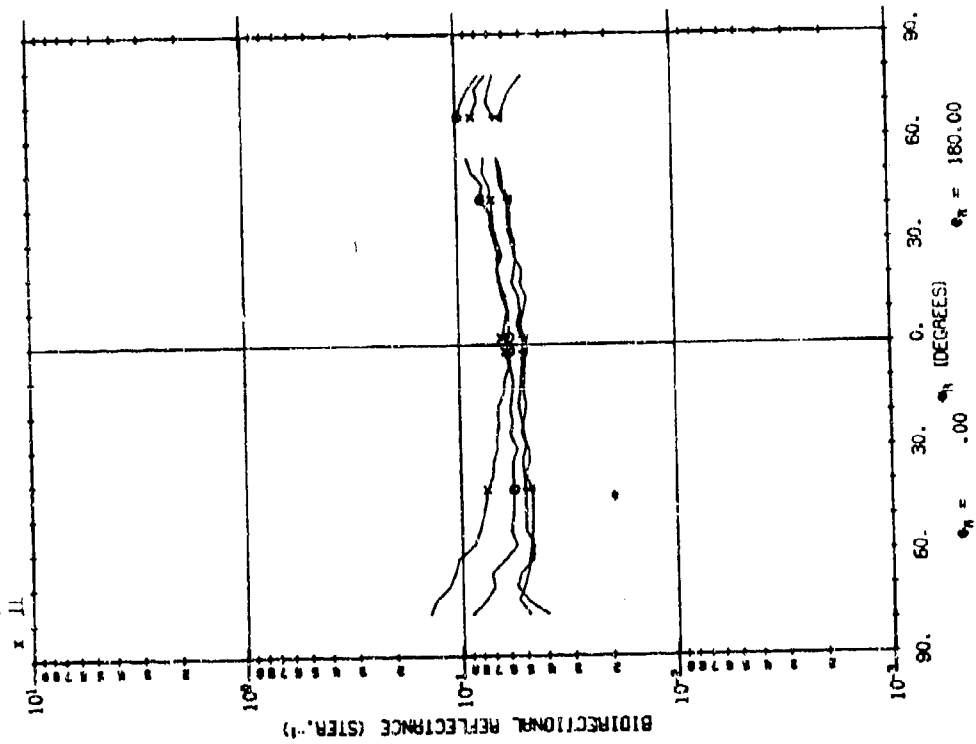
0 | | $\theta_1 = 40.0$
+ | | $\theta_2 = 180.0$
A | | $\lambda = 1.15$
X | |



R01689 103

GREEN CANVAS

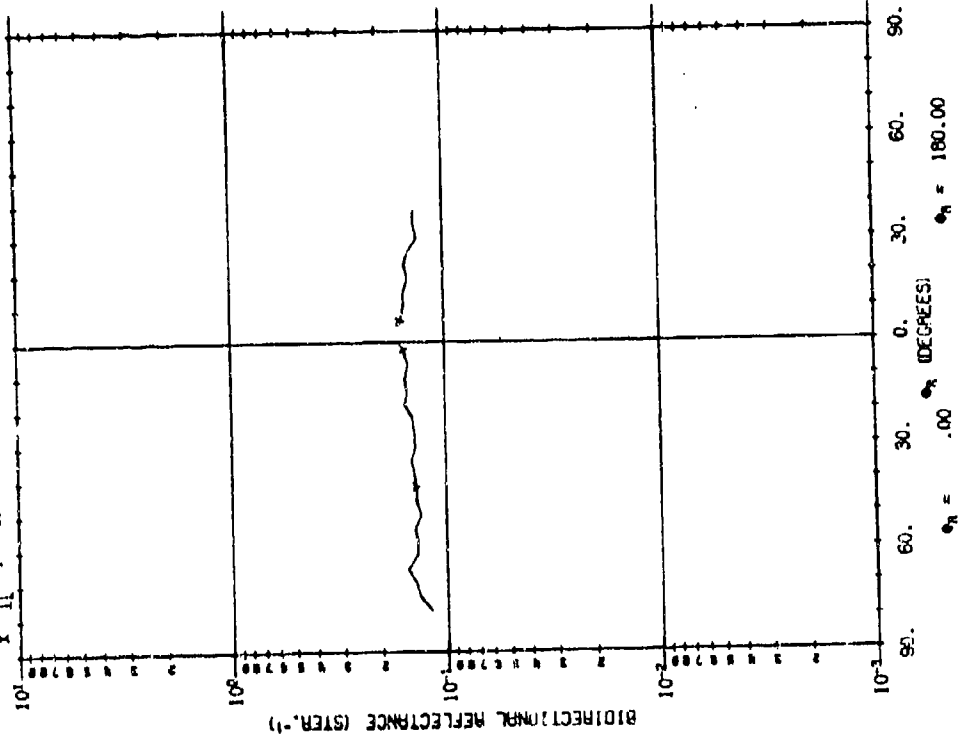
0 || $\phi_1 = 60.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 1.15$
x ||



R01670 102

GRAY TREATED CANVAS, 64
PERCENT REFLECTANCE

0 || $\phi_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 0.46$
x ||

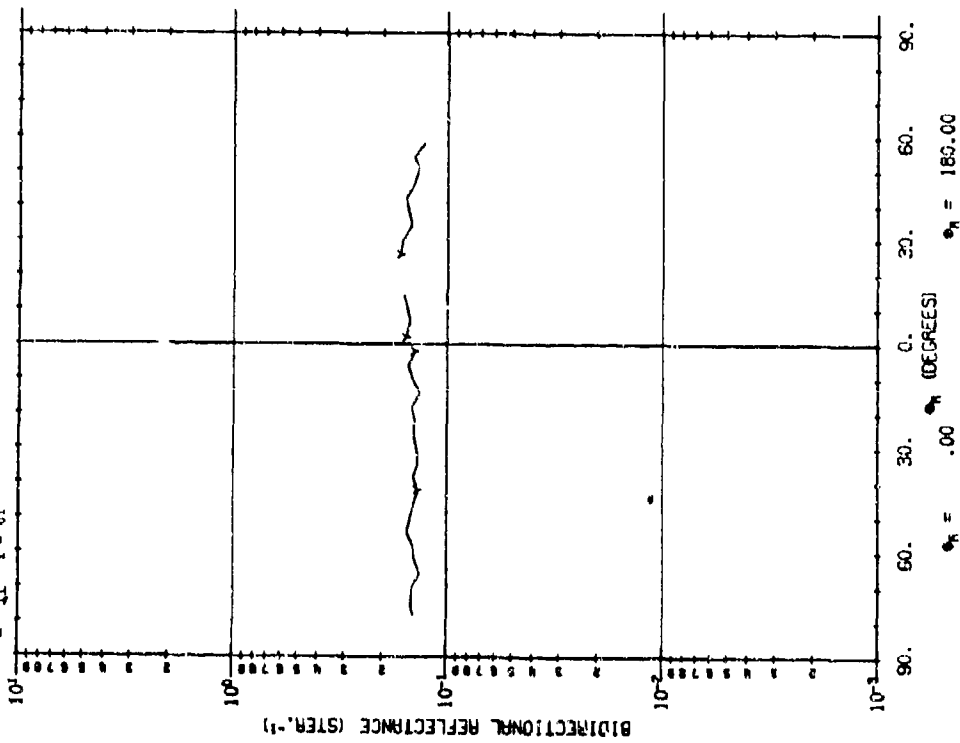


CLOTH AND CANVAS

R01670 102

GRAY TREATED CANVAS, 64
PERCENT REFLECTANCE

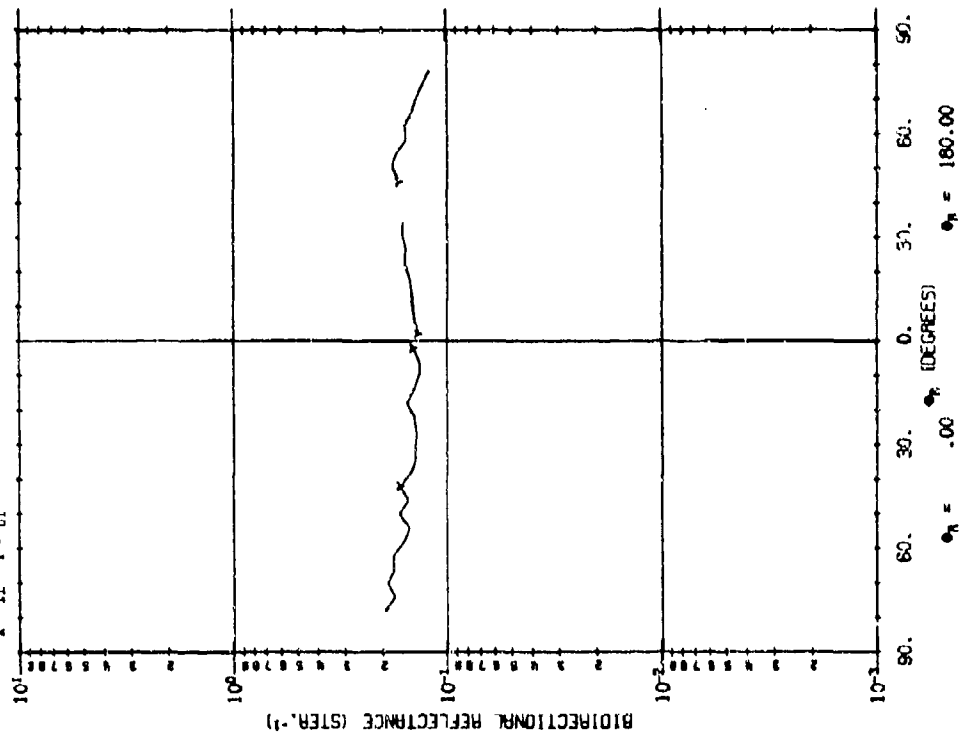
0 || $\theta_1 = 20.0$
+ || $\phi_1 = 180.0$
A || $\lambda = 0.45$
X || $Y = UT$



R01670 102

GRAY TREATED CANVAS, 64
PERCENT REFLECTANCE

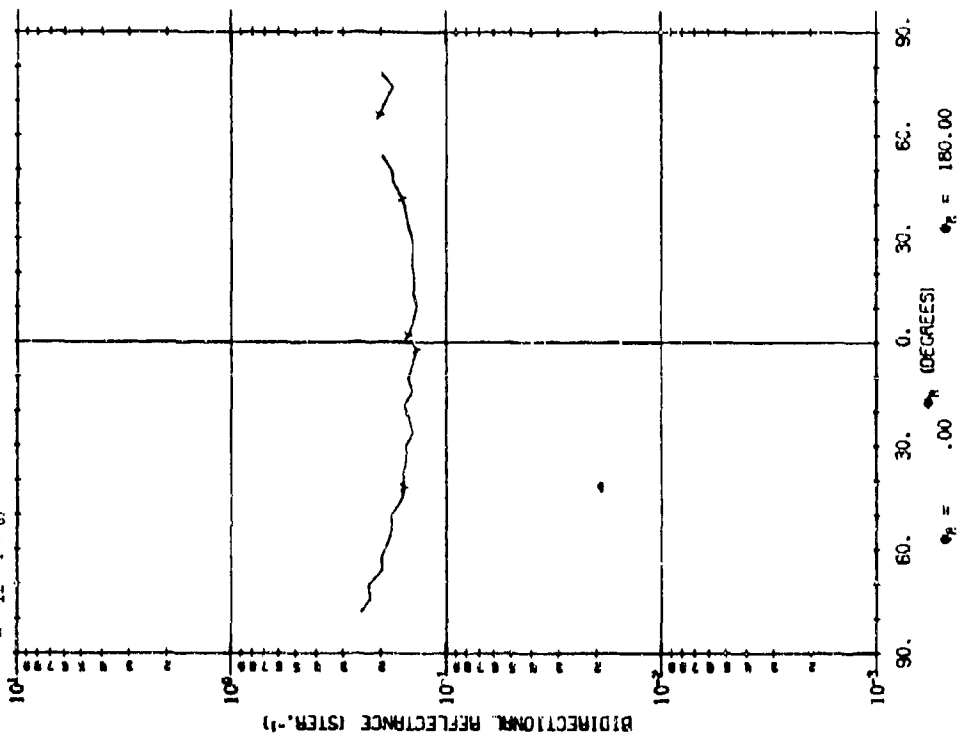
0 || $\theta_1 = 40.0$
+ || $\phi_1 = 180.0$
A || $\lambda = 0.45$
X || $Y = UT$



R01670 102

GRAY TREATED CANVAS, 64
PERCENT REFLECTANCE

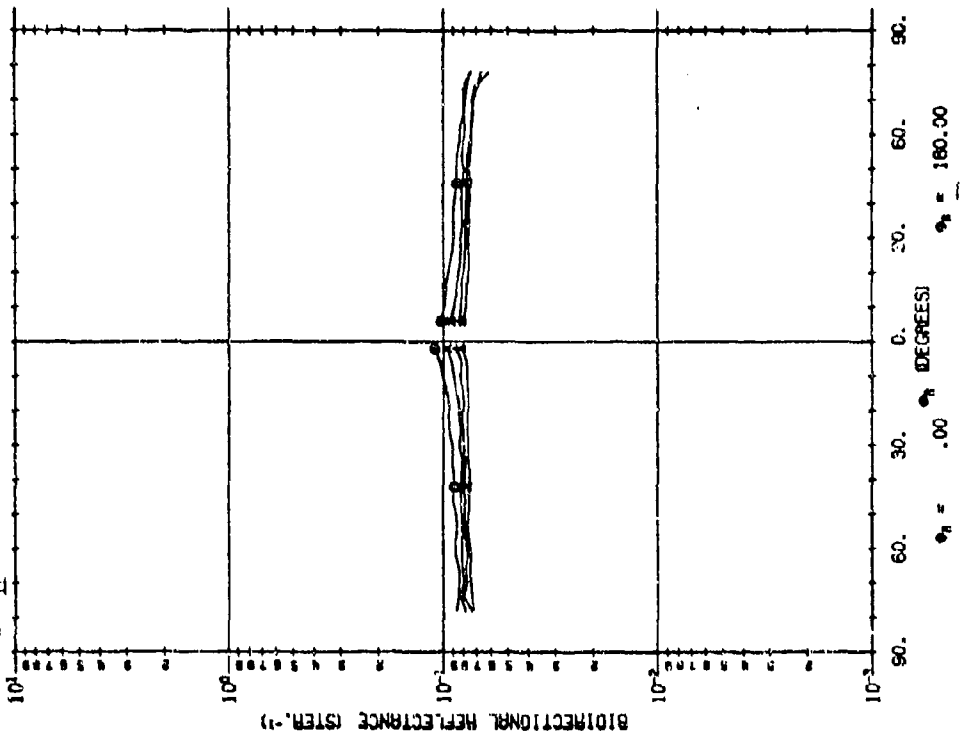
0 || $\theta_1 = 60.0$
+ || $\phi_1 = 180.0$
△ || $\lambda = 0.46$
X || $\gamma = 0.07$



R01670 101

GRAY TREATED CANVAS, 64 PERCENT REFLECTORS

0 || $\theta_1 = 0.0$
+ || $\phi_1 = 0.0$
△ || $\lambda = 0.63$
X || $\gamma = 0.07$



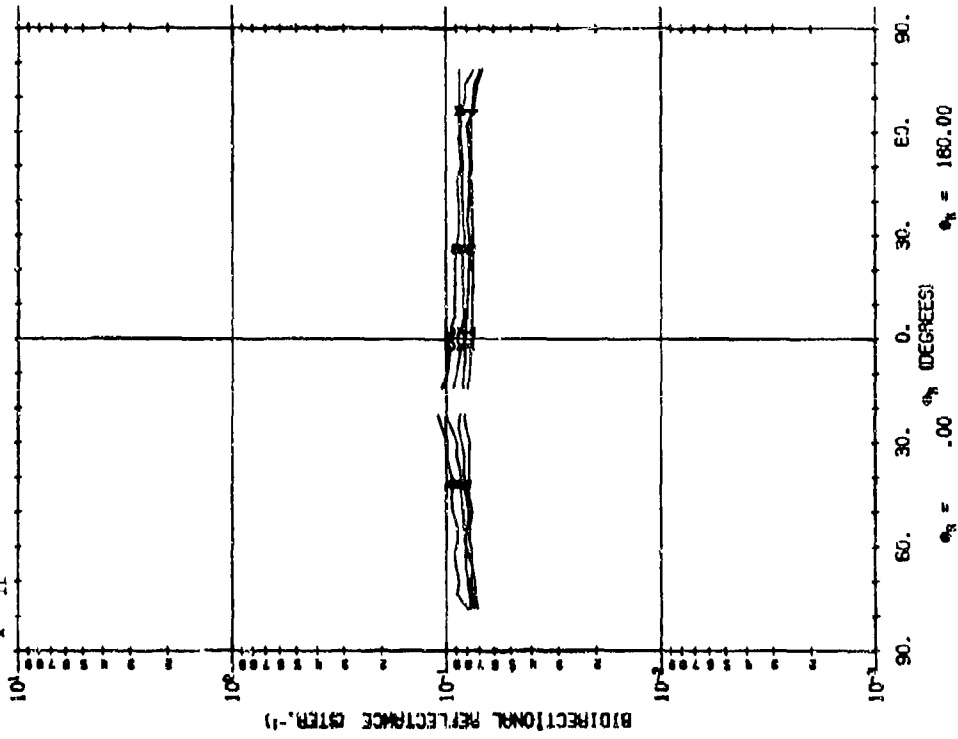
CLOTH AND CANVAS

R01670 101

Gray Treated Canvas, 64 Percent Reflectance

$\theta_1 = 20.0$
 $\phi_1 = 0.6$
 $\lambda = 0.63$

0 ||
+ ||
A ||
X ||

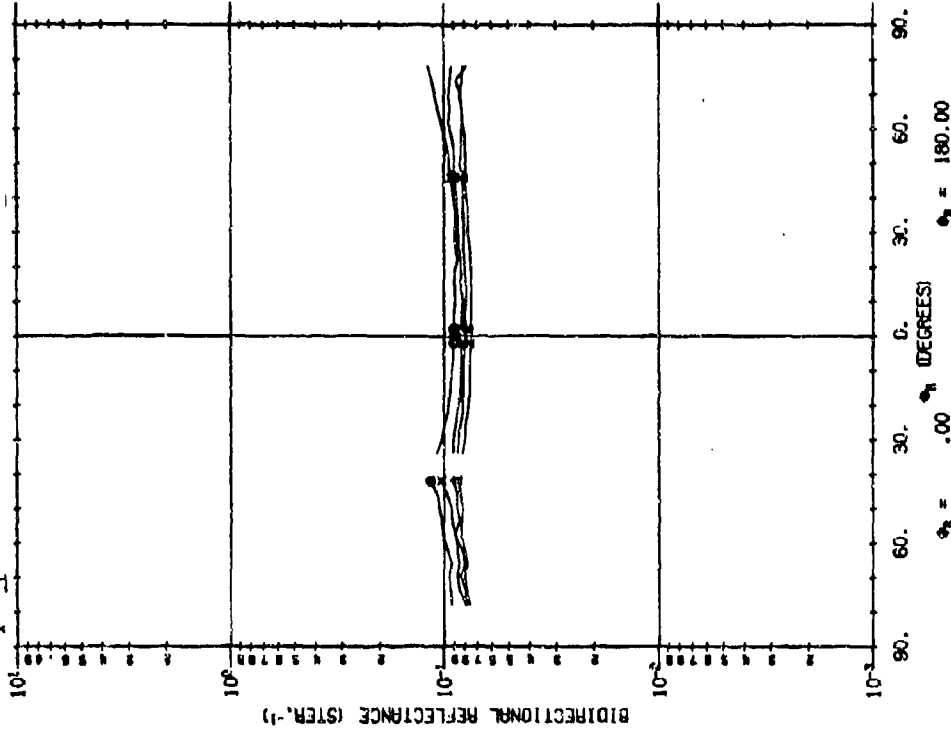


R01670 101

Gray Treated Canvas, 64 Percent Reflectance

$\theta_1 = 40.0$
 $\phi_1 = 0.6$
 $\lambda = 0.63$

0 ||
+ ||
A ||
X ||



AO1670 101

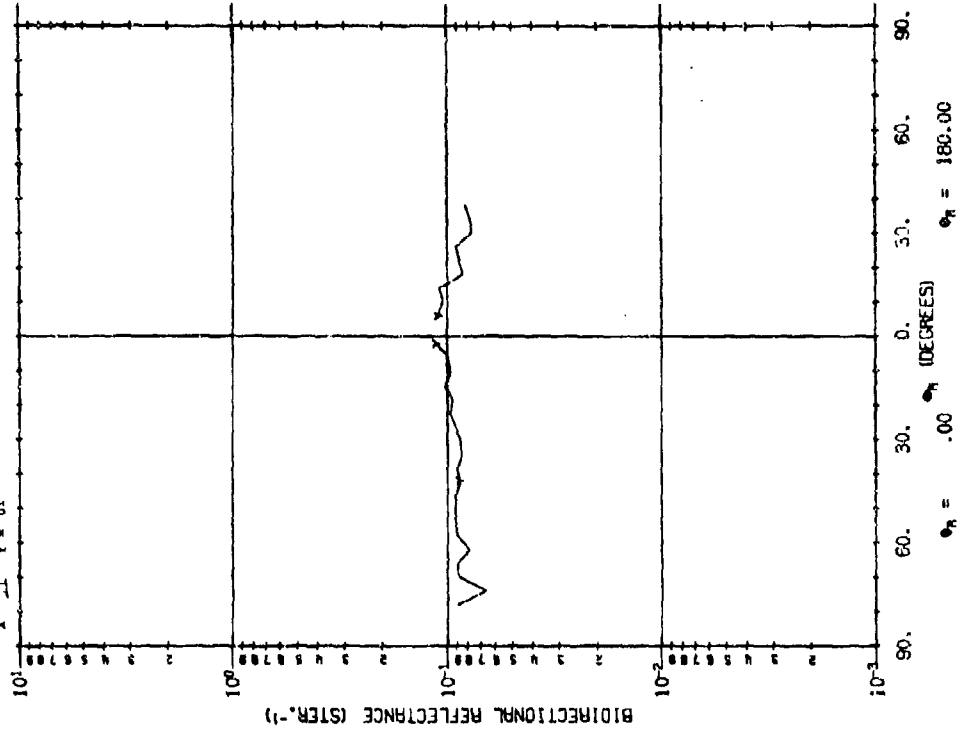
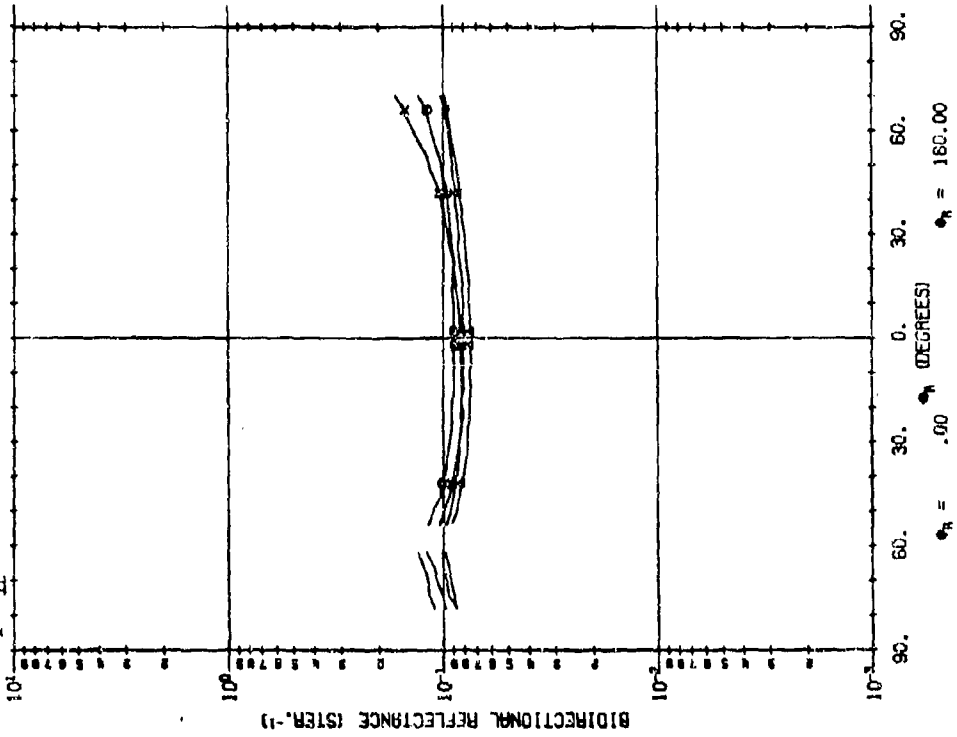
Gray treated Canvas, 64 Percent Reflectance

$\phi_1 = 60.0$
 $\phi_2 = 0.0$
 $\lambda = 0.63$

AO1671 102

GRAY TREATED CANVAS, 32
PERCENT REFLECTANCE

$\phi_1 = 0.0$
 $\phi_2 = 130.0$
 $\lambda = 0.46$

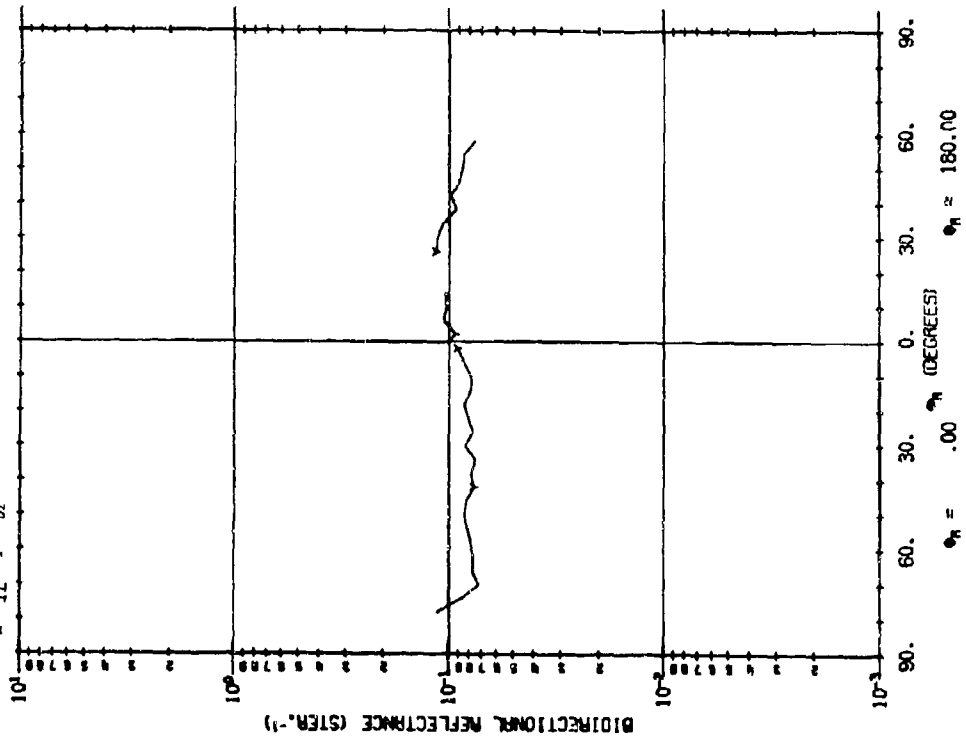


CLOTH AND CANVAS

A01671 102

GRAY TREATED CANVAS, 32
PERCENT REFLECTANCE

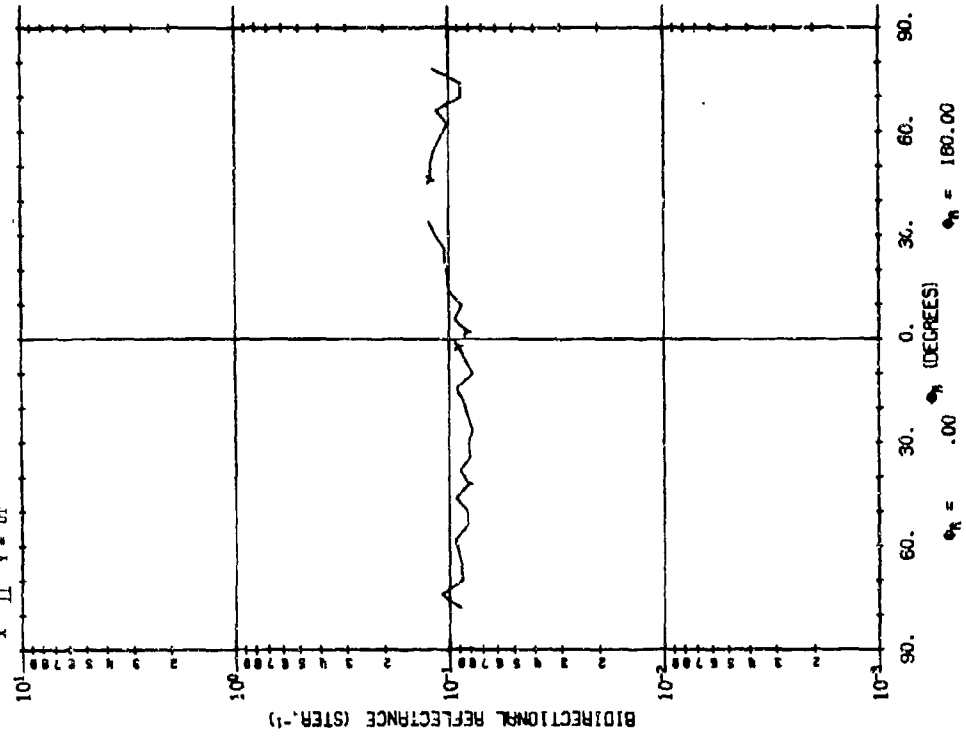
0 // $\theta_1 = 20.0$
+ // $\theta_2 = 180.0$
 Δ // $\lambda = 0.46$
X // Y = UT



A01671 102

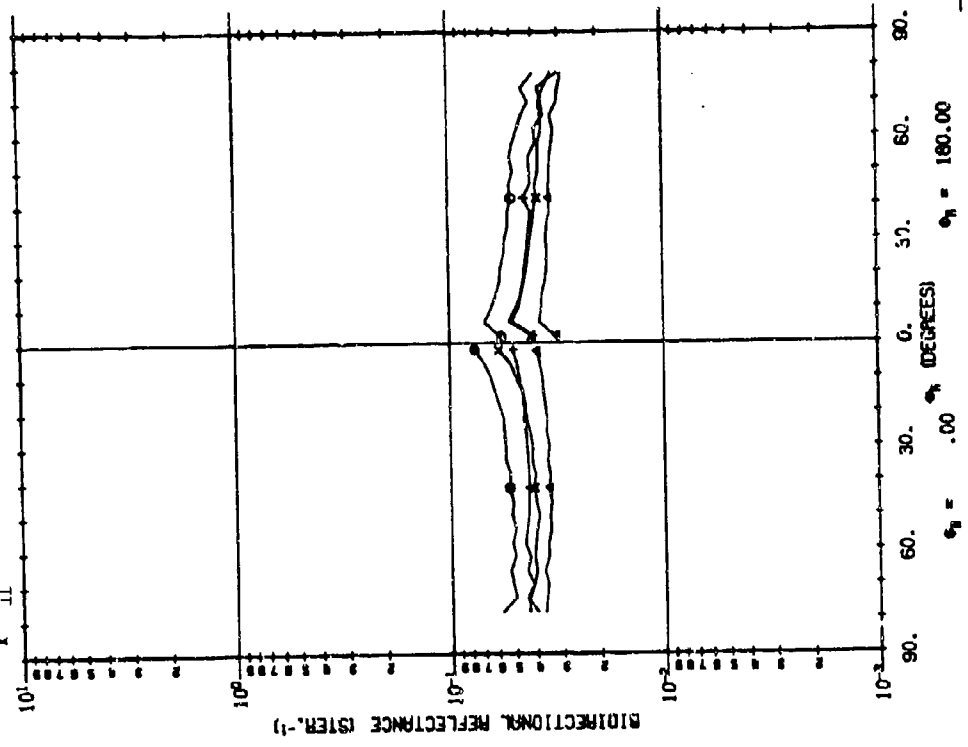
GRAY TREATED CANVAS, 32
PERCENT REFLECTANCE

0 // $\theta_1 = 40.0$
+ // $\theta_2 = 180.0$
 Δ // $\lambda = 0.46$
X // Y = UT



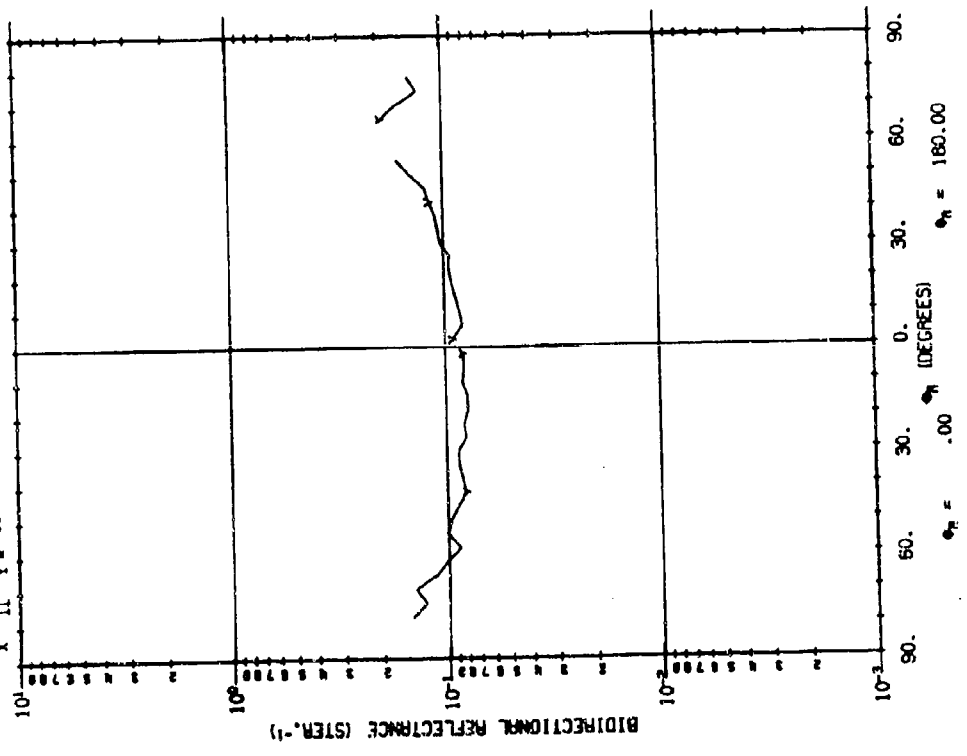
R01671 101
 0 || $\theta_1 = 0.0$
 + || $\phi_1 = 0.0$
 Δ || $\lambda = 0.63$
 X ||

Gray Treated Canvas, 32 Percent Reflectance



R01671 102
 0 || $\theta_1 = 60.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 0.46$
 X || $\gamma = \text{UT}$

GRAY TREATED CANVAS, 32
 PERCENT REFLECTANCE



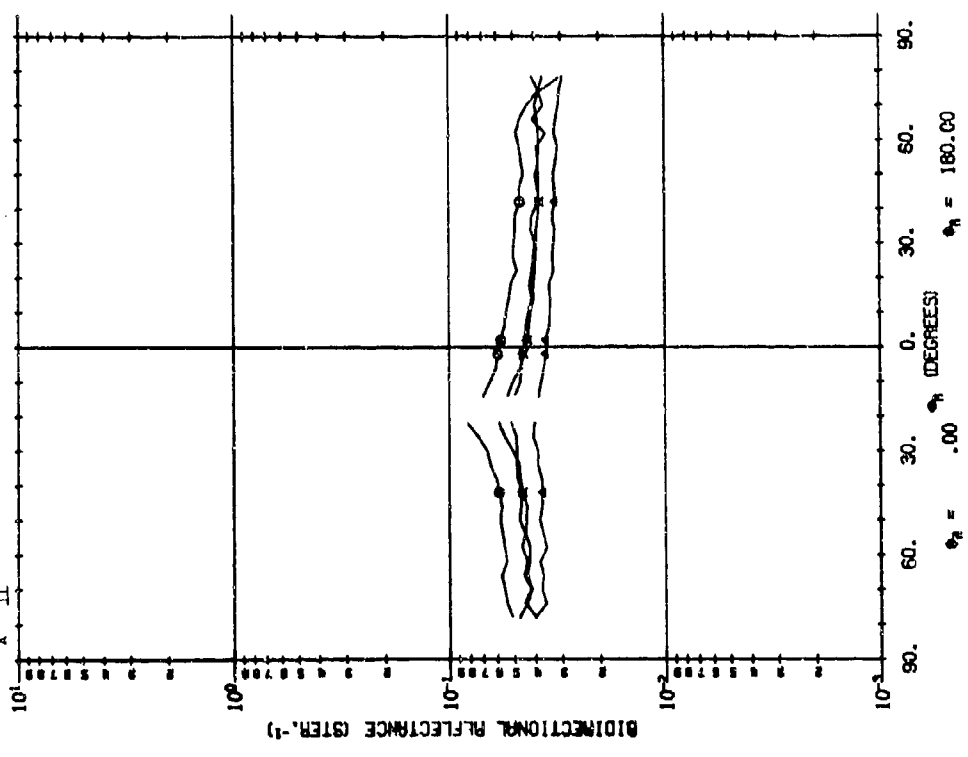
CLOTH AND CANVAS

A01671 101

Gray Treated Canvas, 32 Percent Reflectance

$\theta_1 = 20.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

0 || ||
+ || ||
A || ||
X || ||

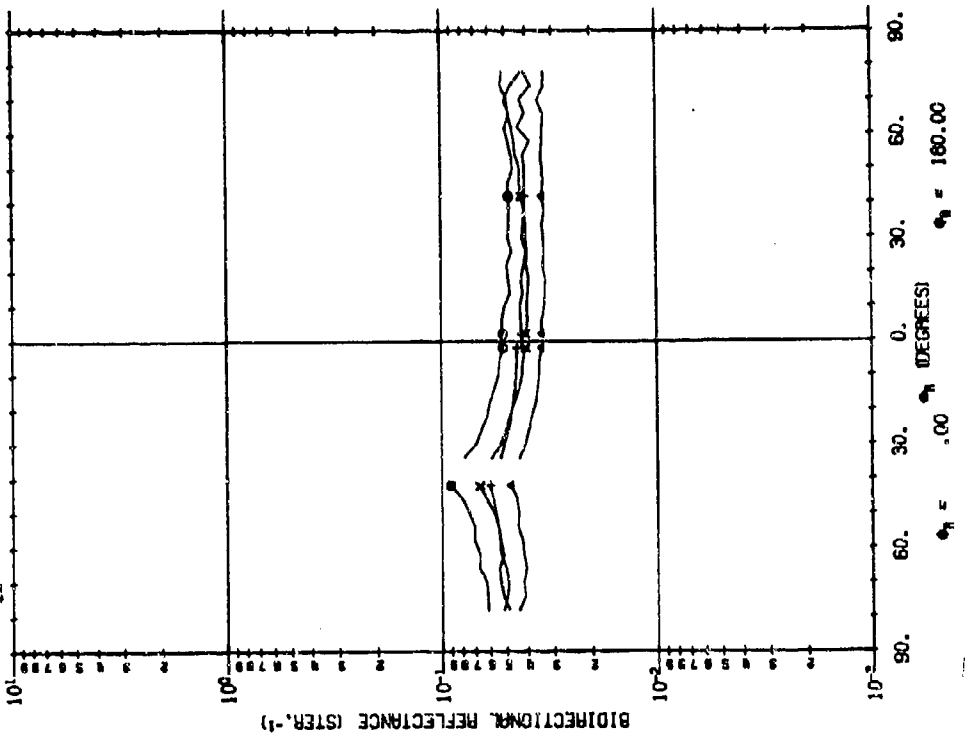


A01671 101

Gray Treated Canvas, 32 Percent Reflectance

$\theta_1 = 40.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

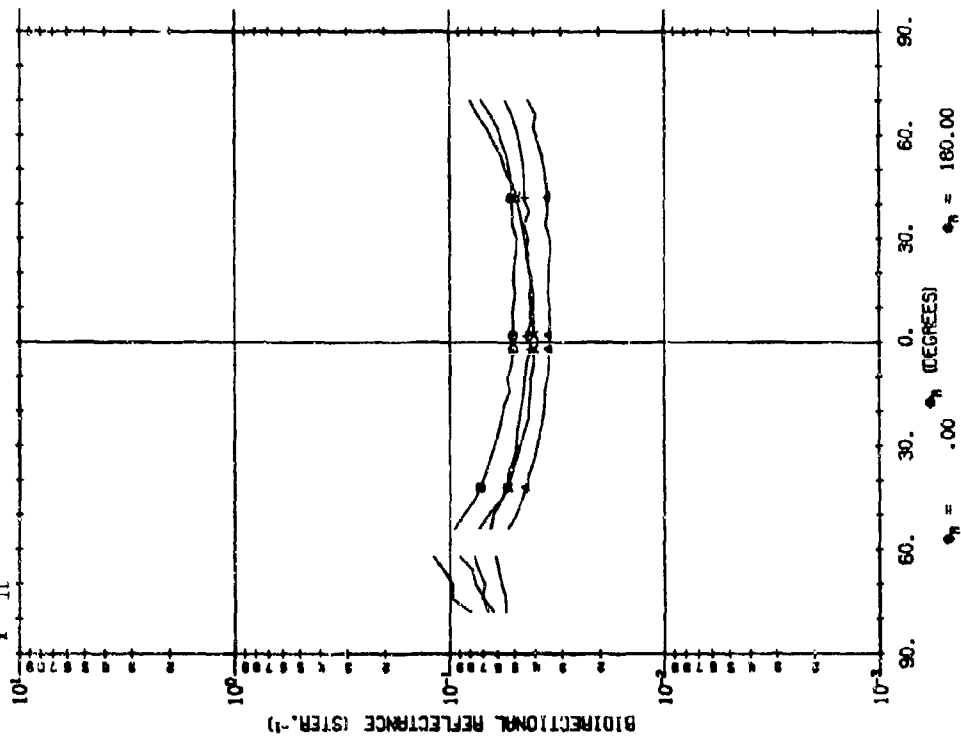
0 || ||
+ || ||
A || ||
X || ||



R01671 101

Gray Treated Canvas, 32 Percent Reflectance

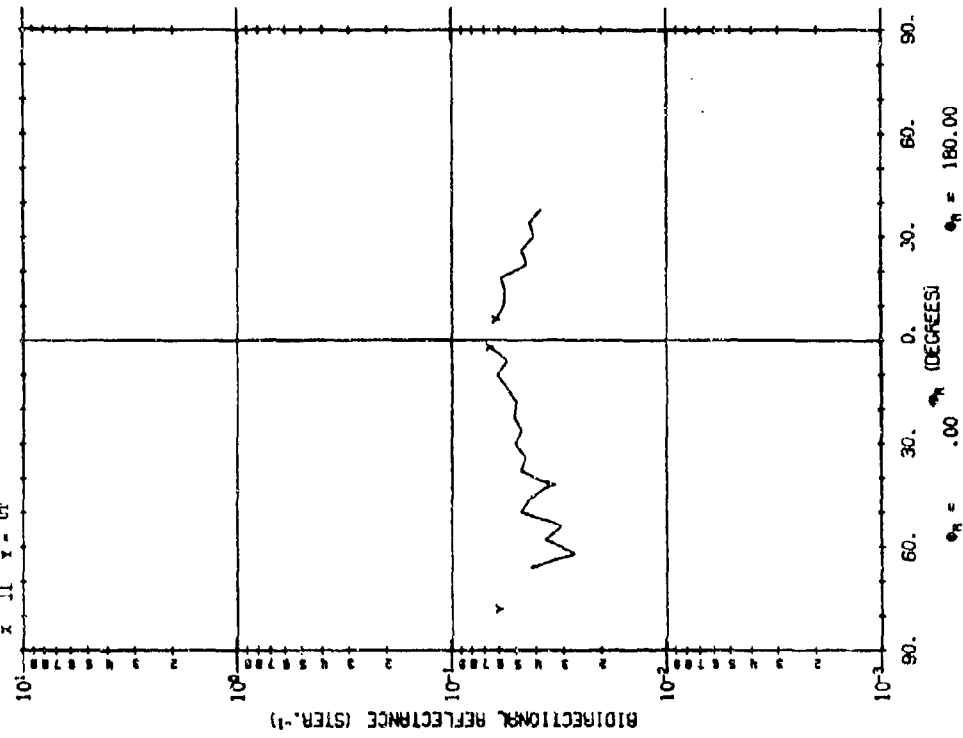
C || $\theta_1 = 60.0$
+ || $\phi_1 = 0.0$
A || $\lambda = 0.63$
X ||



R01672 102

GRAY TREATED CANVAS, 16
PERCENT REFLECTANCE

0 || $\theta_1 = 0.0$
+ || $\phi_1 = 180.0$
A || $\lambda = 0.46$
X || Y - UT

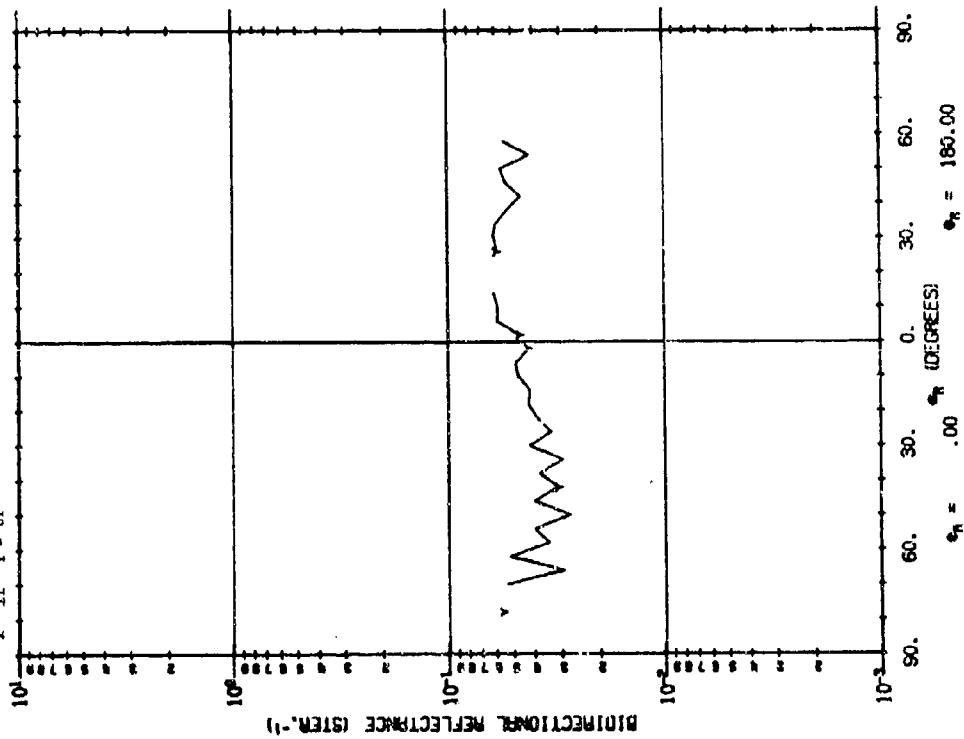


CLOTH AND CANVAS

R01672 102

GRAY TREATED CARVAS, 16
PERCENT REFLECTANCE

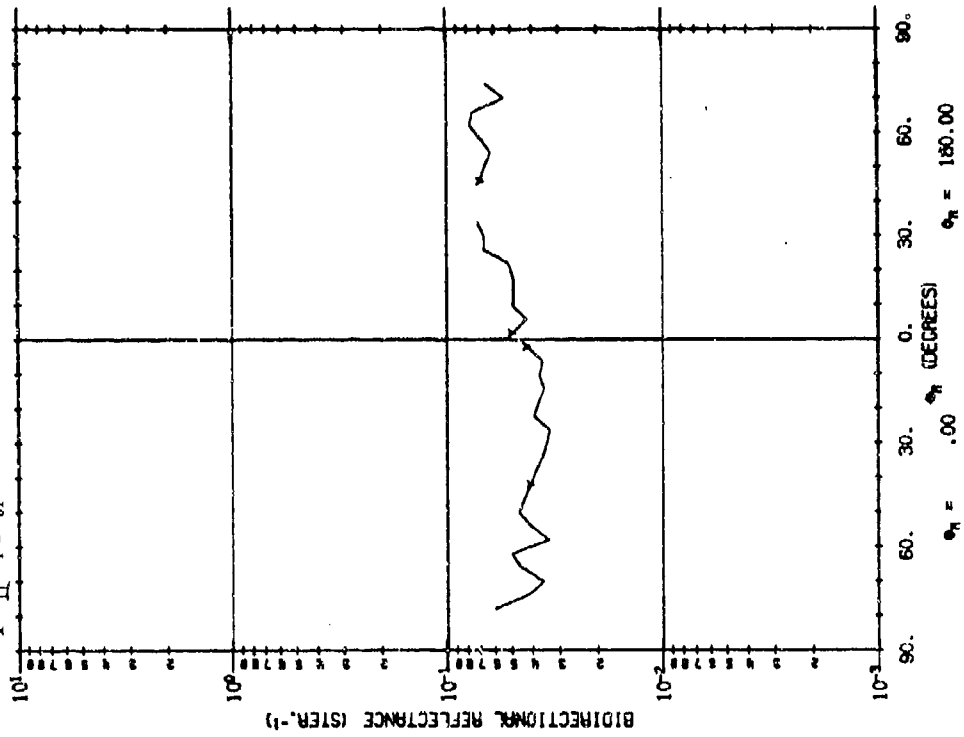
0 || $\theta_i = 20.0$
+ || $\theta_r = 180.0$
Δ || $\lambda = 0.45$
X || Y = UT



R01672 102

GRAY TREATED CARVAS, 16
PERCENT REFLECTANCE

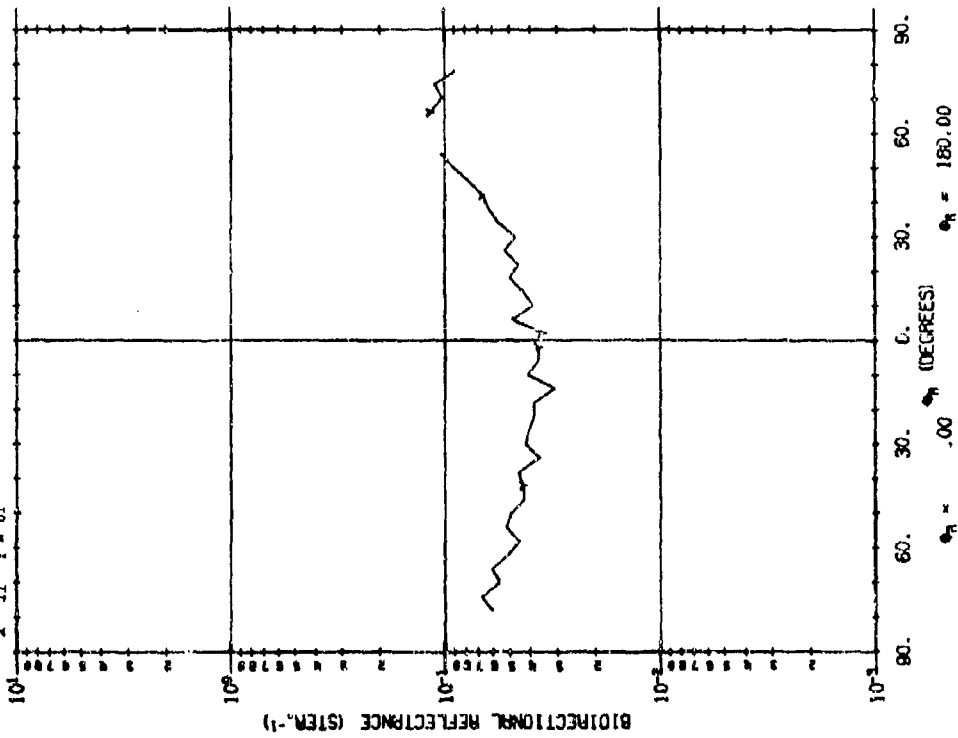
0 || $\theta_i = 40.0$
+ || $\theta_r = 180.0$
Δ || $\lambda = 0.46$
X || Y = UT



A01672 102

GRAY TREATED CANVAS, 16
PERCENT REFLECTANCE

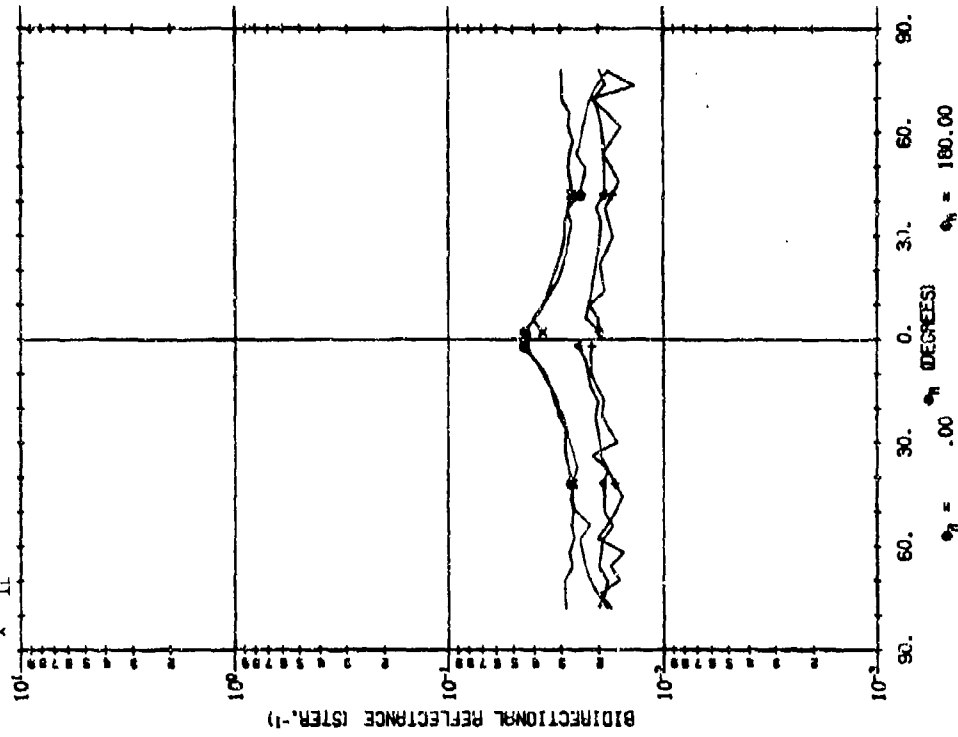
0 || $\theta_1 = 60.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 0.46$
x || $\gamma = 07$



A01672 101

GRAY TREATED CANVAS, 16 PERCENT REFLECTANCE

0 || $\theta_1 = 0.0$
+ || $\theta_2 = 0.0$
Δ || $\lambda = 0.63$
x ||

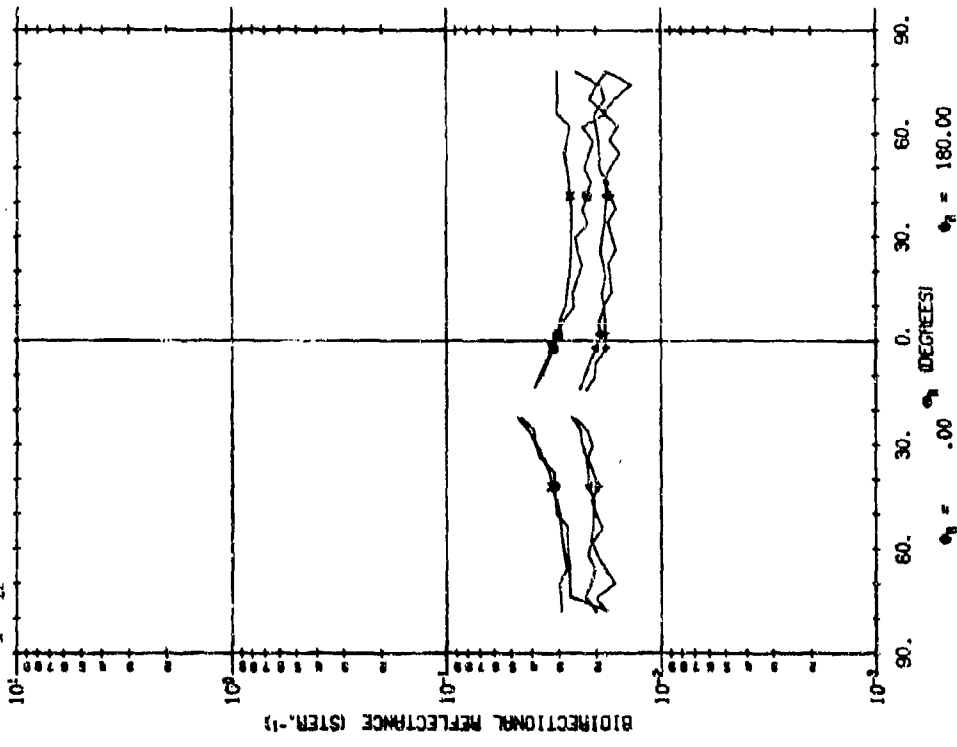


CLOTH AND CANVAS

R01672 101

Gray Treated Canvas, 16 Percent Reflectance

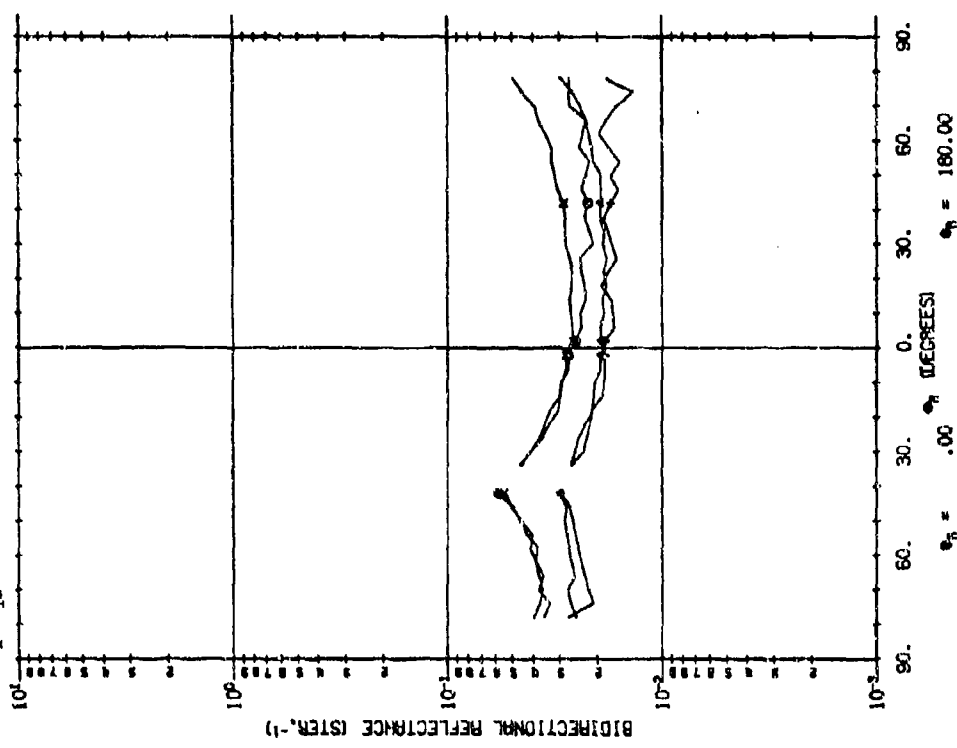
$\theta_i = 20.0$
 $\phi_i = 0.0$
 $\lambda_i = 0.63$



R01672 101

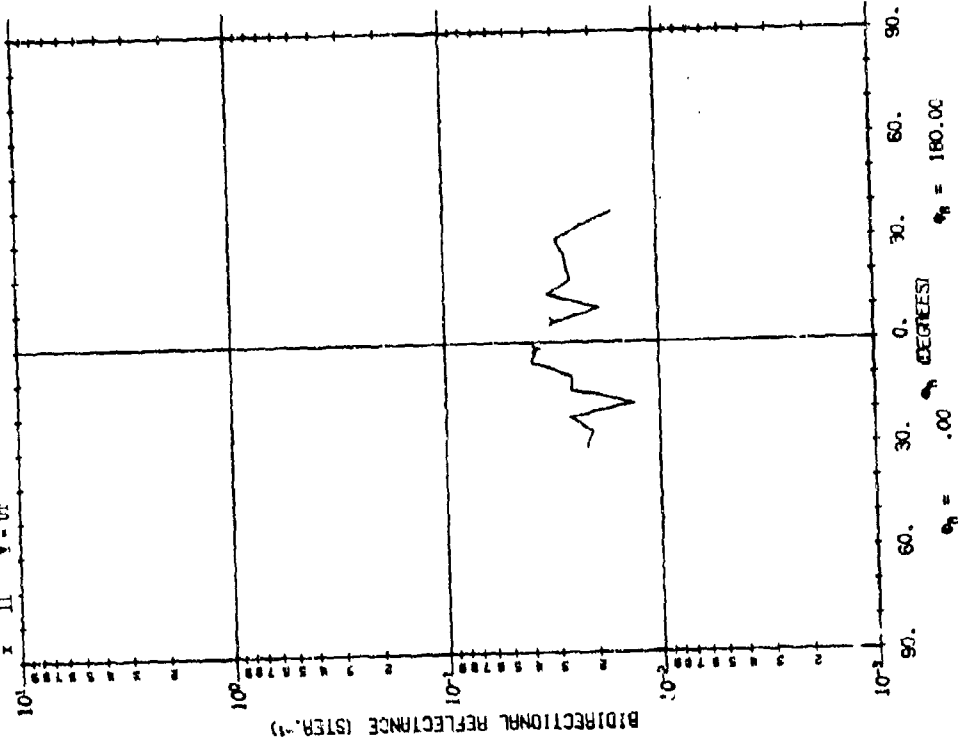
Gray Treated Canvas, 16 Percent Reflectance

$\theta_i = 40.0$
 $\phi_i = 0.0$
 $\lambda_i = 0.63$



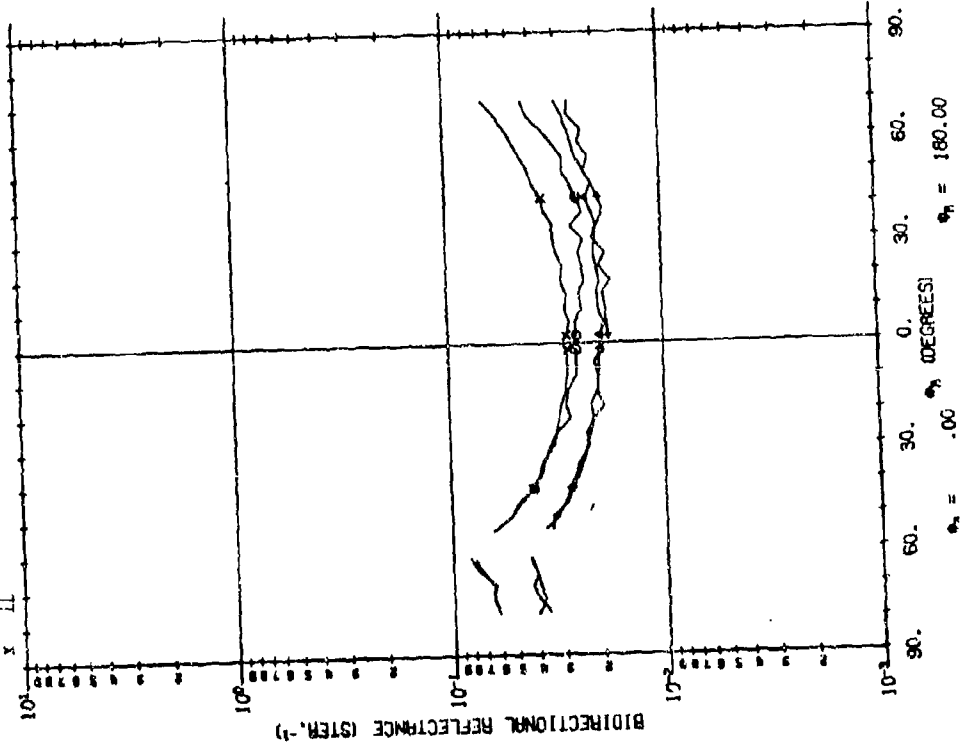
R01673 103
 0 ||
 + ||
 Δ ||
 X ||

Gray Treated Canvas, 8 Percent Reflectance
 $\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda = 0.46$
 $\gamma = 0.0$



R01672 101
 0 ||
 + ||
 Δ ||
 X ||

Gray Treated Canvas, 16 Percent Reflectance
 $\theta_1 = 60.0$
 $\theta_2 = 0.0$
 $\lambda = 0.65$



CLOTH AND CANVAS

A01673 103

Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 20.0$
 $\theta_2 = 180.0$
 $\lambda = 0.46$
 $Y = 07$

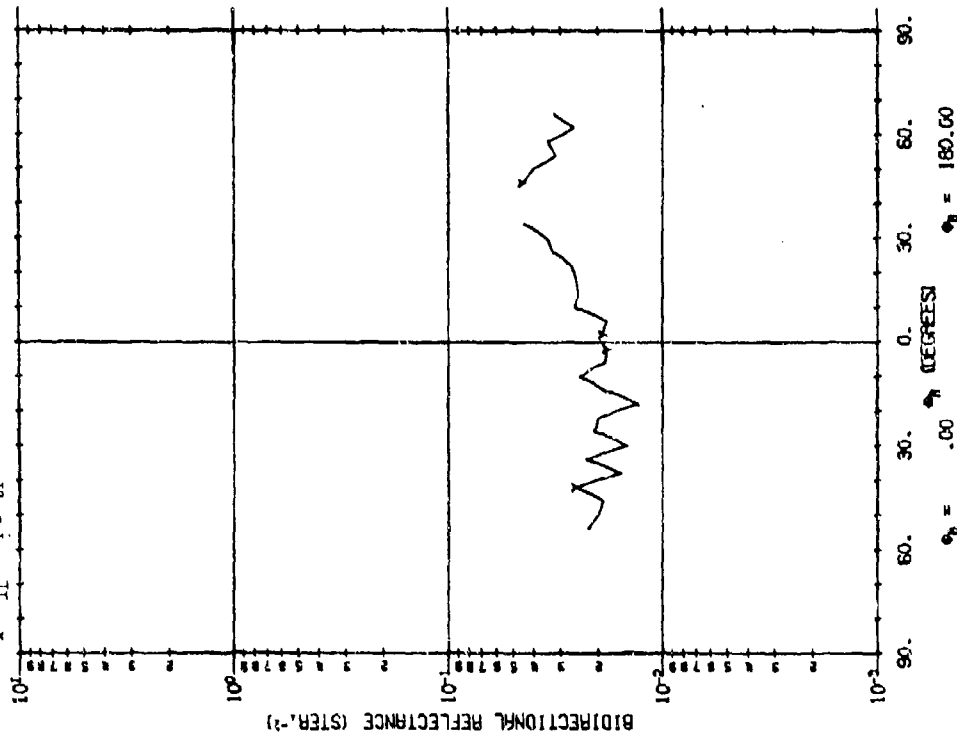
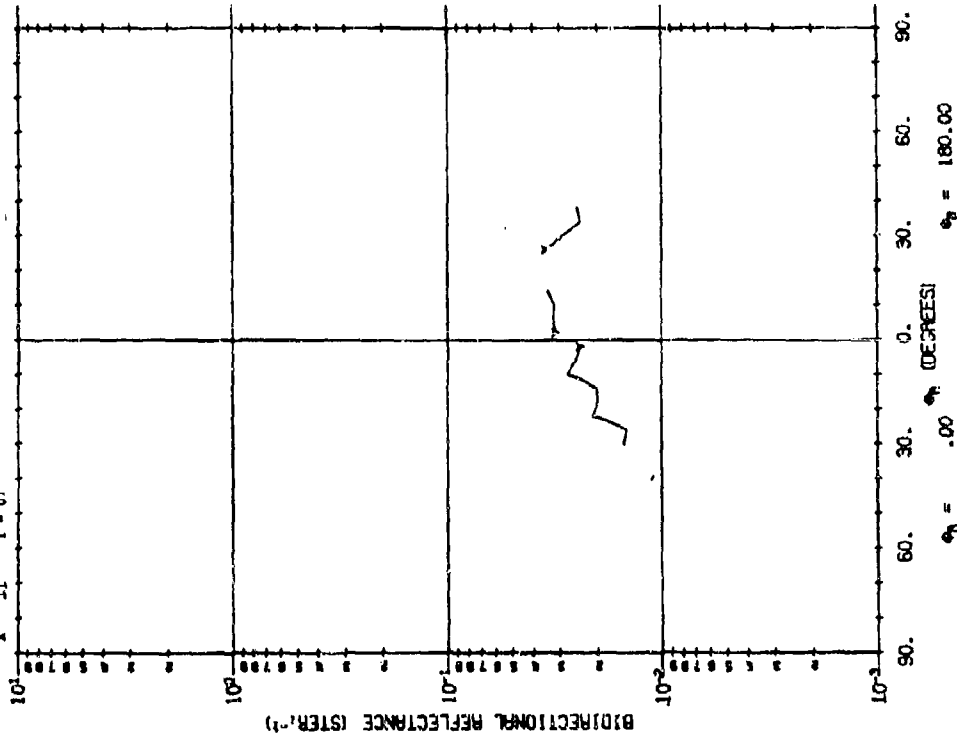
0 ||
+ ||
Δ ||
x ||

A01673 103

Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 40.0$
 $\theta_2 = 180.0$
 $\lambda = 0.46$
 $Y = 07$

0 ||
+ ||
Δ ||
x ||

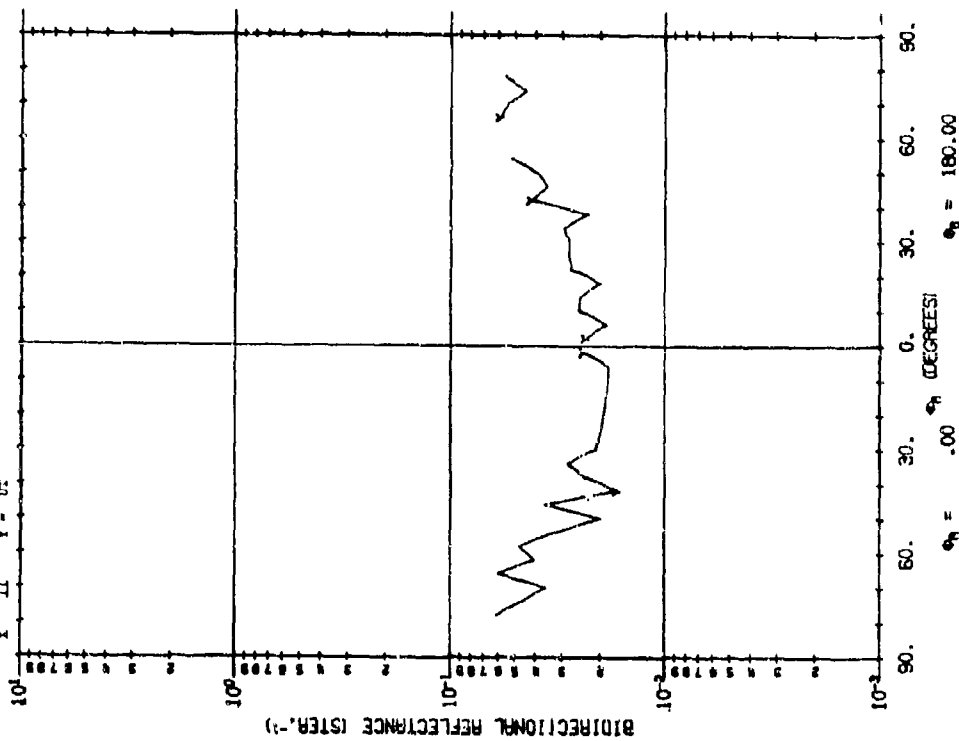


R01673 103

Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda_1 = 0.46$
 $\lambda_2 = 0.46$

Y - UZ

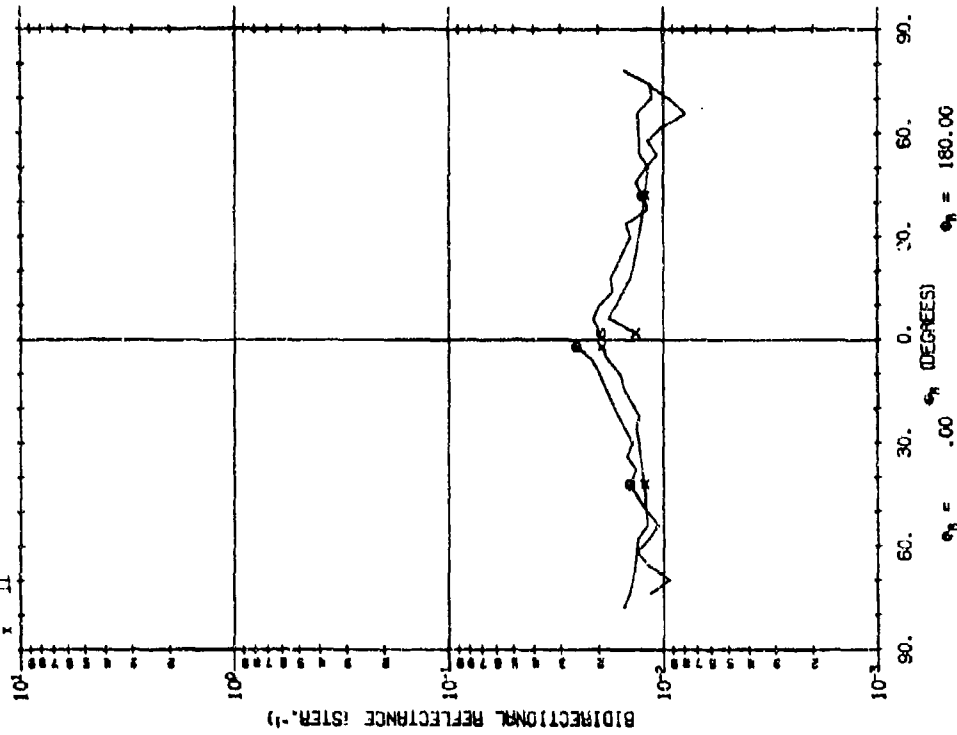


R01673 101

Gray treated Canvas, 8 Percent Reflectance

$\theta_1 = 0.0$
 $\theta_2 = 0.3$
 $\lambda_1 = 0.63$

X



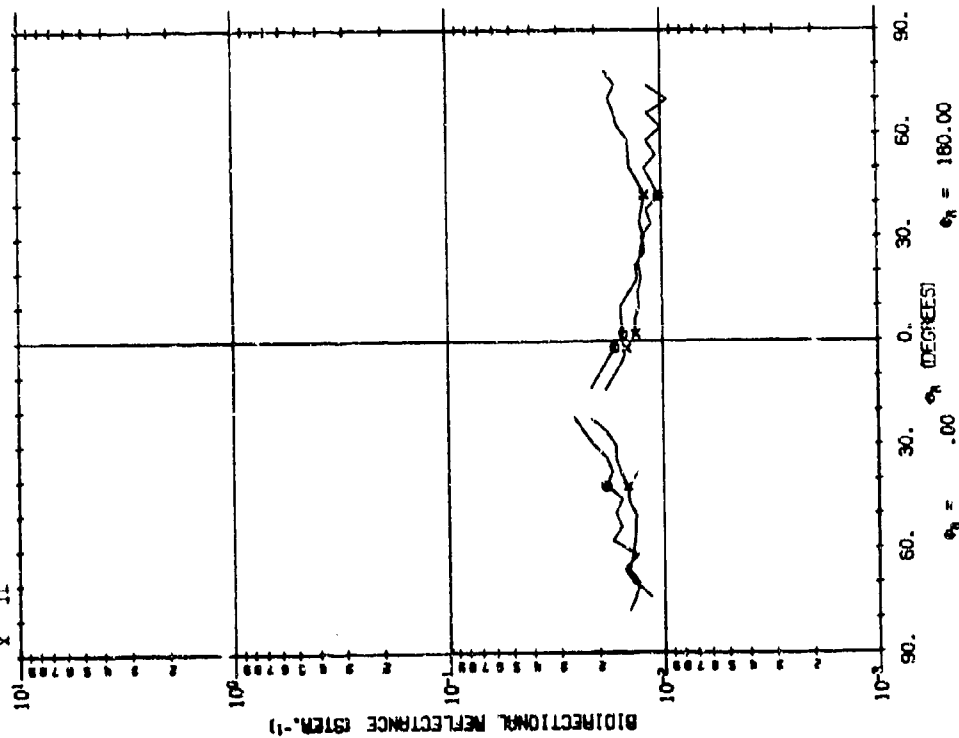
CLOTH AND CANVAS

A01673 101

Gray Treated Canvas, 6 Percent Reflectance

$\theta_i = 20.0$
 $\phi_i = 0.0$
 $\lambda = 0.63$

C || ||
+ || ||
A || ||
X || ||

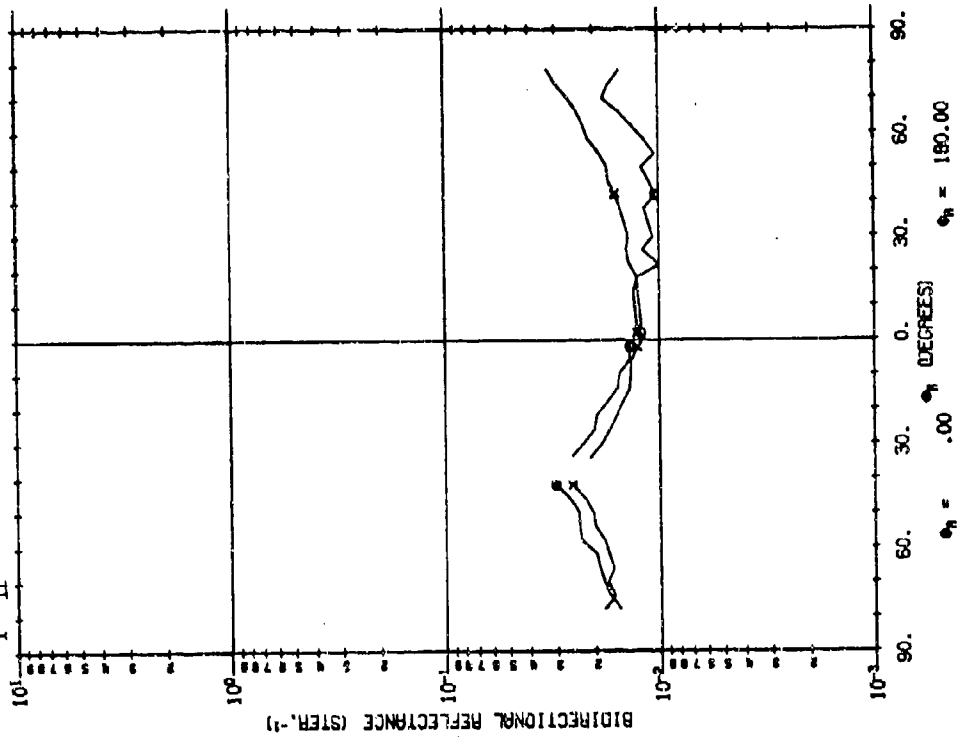


A01673 101

Gray Treated Canvas, 8 Percent Reflectance

$\theta_i = 40.0$
 $\phi_i = 0.0$
 $\lambda = 0.63$

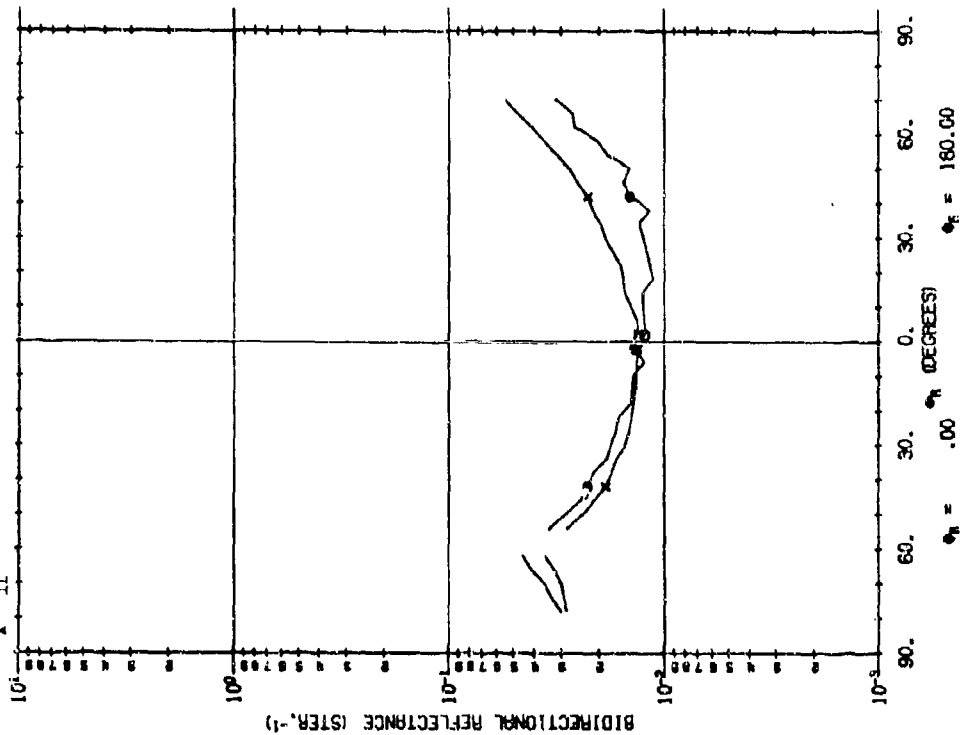
C || ||
+ || ||
A || ||
X || ||



R01673 101

Gray Treated Canvas, 8 Percent Reflectance

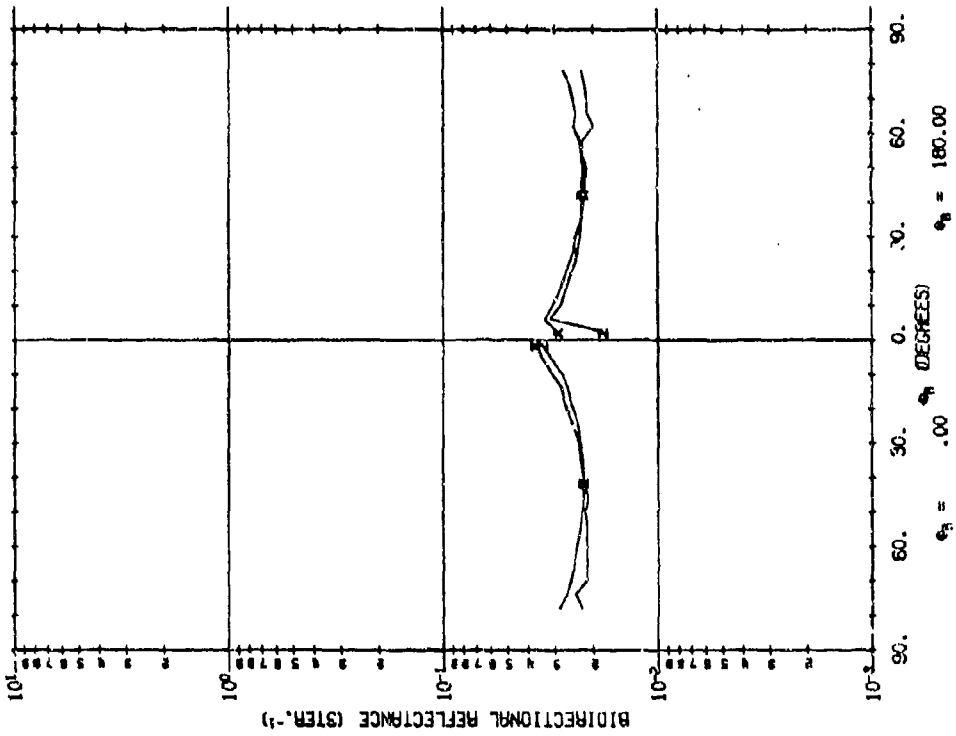
$\theta_1 = 60.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$



R01673 102

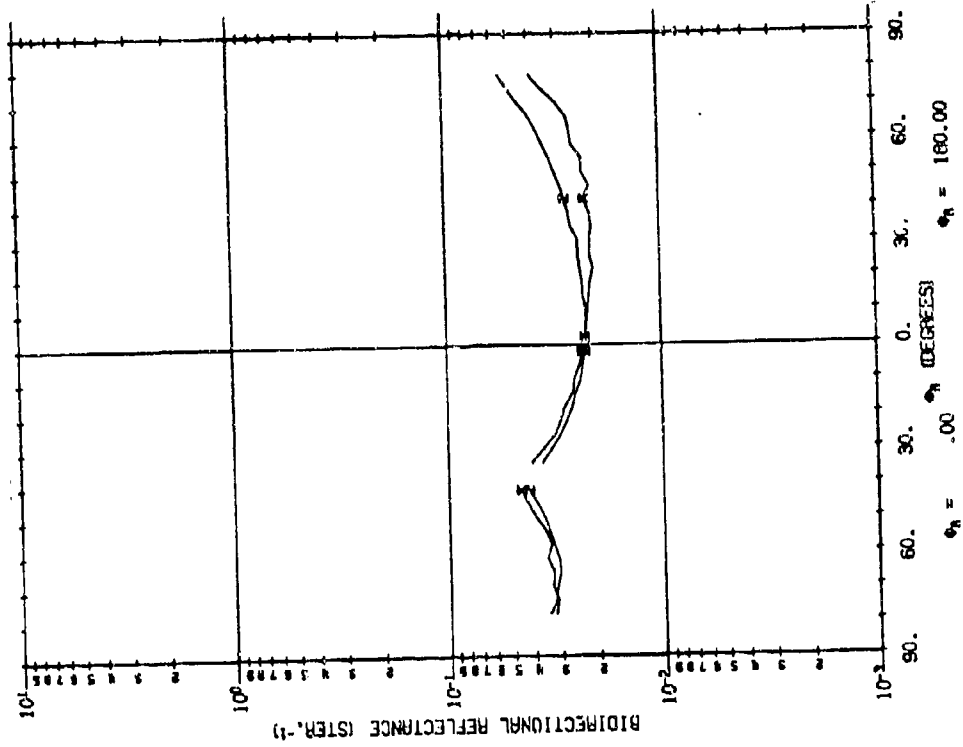
Gray Treated Canvas, 8 Percent Reflectance

$\theta_1 = 0.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

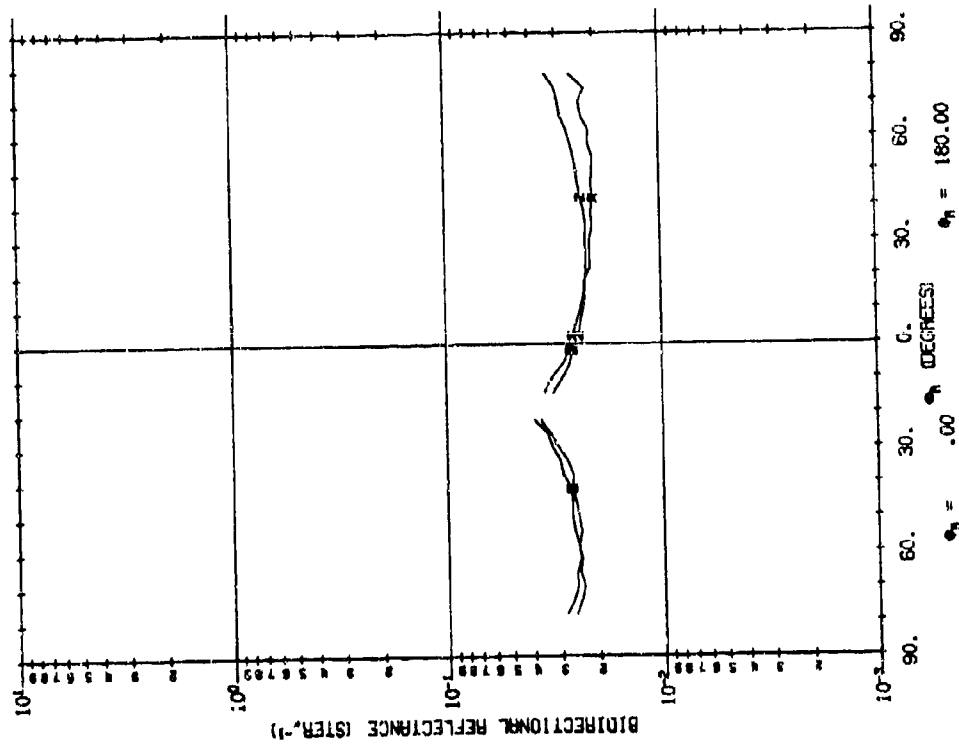


CLOTH AND CANVAS

A01673 102
 Gray Treated Canvas, 8 Percent Reflectance
 $\epsilon_1 = 40.0$
 $\epsilon_2 = 6.0$
 $\lambda = 0.63$

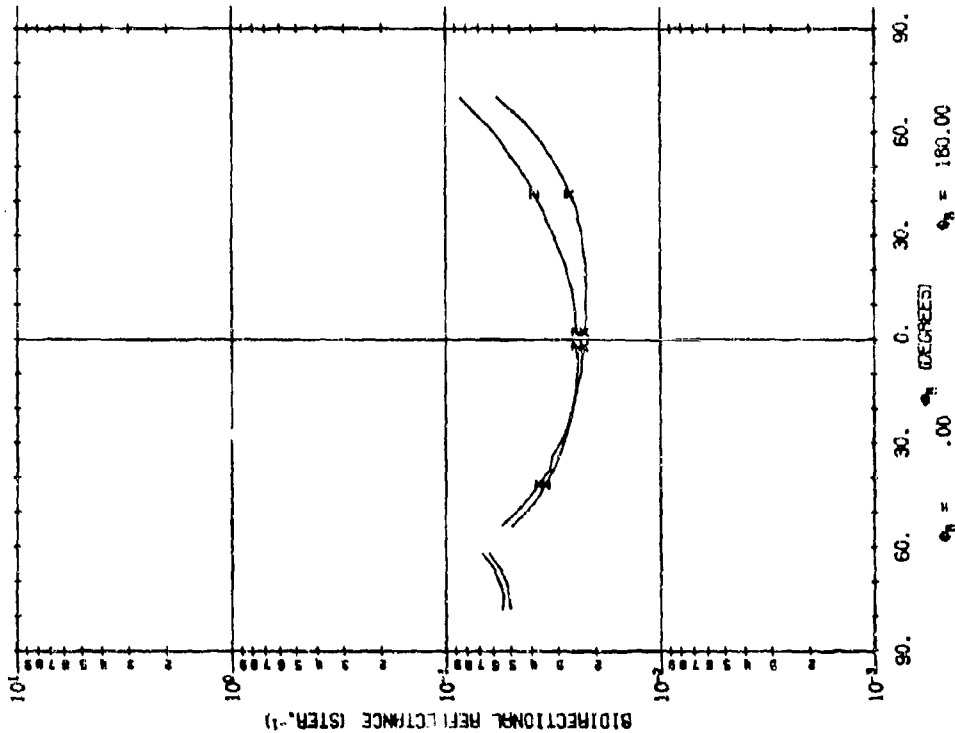


A01573 102
 Gray Treated Canvas, 8 Percent Reflectance
 $\epsilon_1 = 20.0$
 $\epsilon_2 = 0.0$
 $\lambda = 0.63$



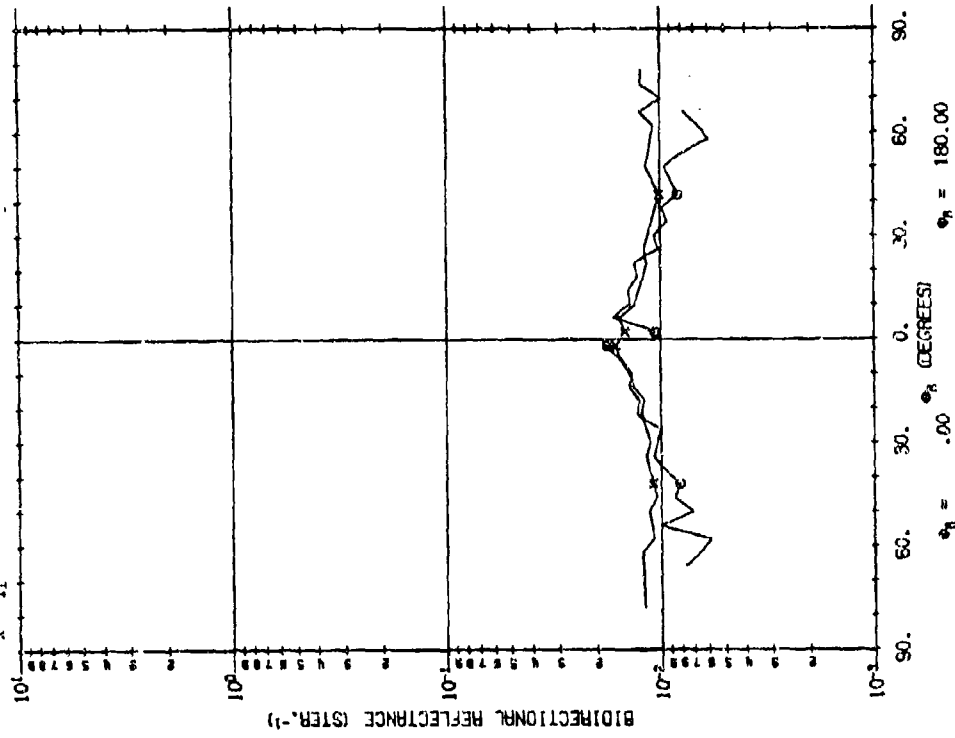
AO1673 102
 X II
 Z II
 $\rho_1 = 60.0$
 $\rho_2 = 0.0$
 $\lambda = 0.63$

Gray Treated Canvas, 8 Percent Reflectance



AO1674 101
 0 II
 + II
 4 II
 X II
 $\rho_1 = 0.0$
 $\rho_2 = 0.0$
 $\lambda = 0.63$

Black Treated Canvas, 8 Percent Reflectance



CLOTH AND CANVAS

AO1674 101

Black Treated Canvas, 4 Percent Reflectance

$\theta_1 = 20.0$

$\phi_1 = 0.0$

$\lambda = 0.63$

0

||

||

+

||

||

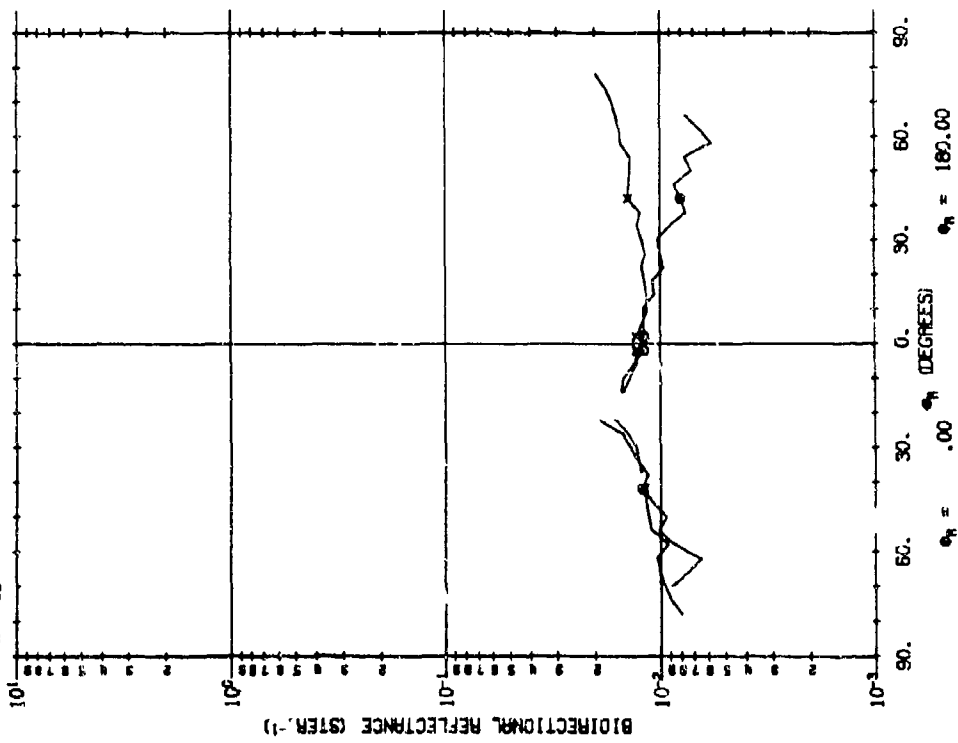
Δ

||

||

x

||



AO1674 101

Black Treated Canvas, 4 Percent Reflectance

$\theta_1 = 40.0$

$\phi_1 = 0.0$

$\lambda = 0.63$

0

||

||

+

||

||

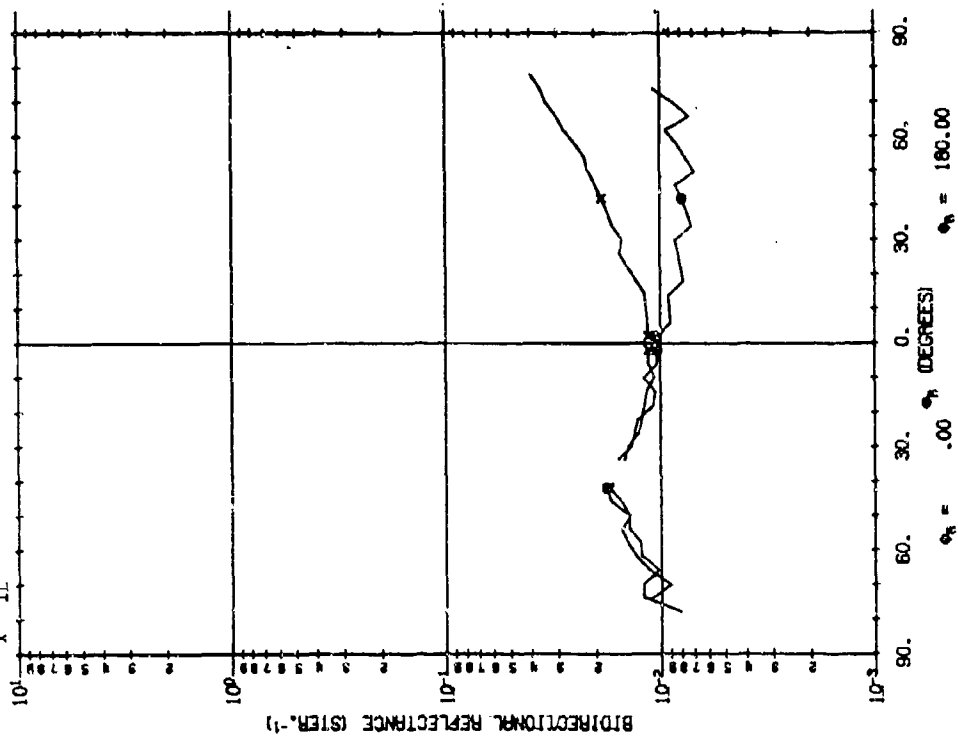
Δ

||

||

x

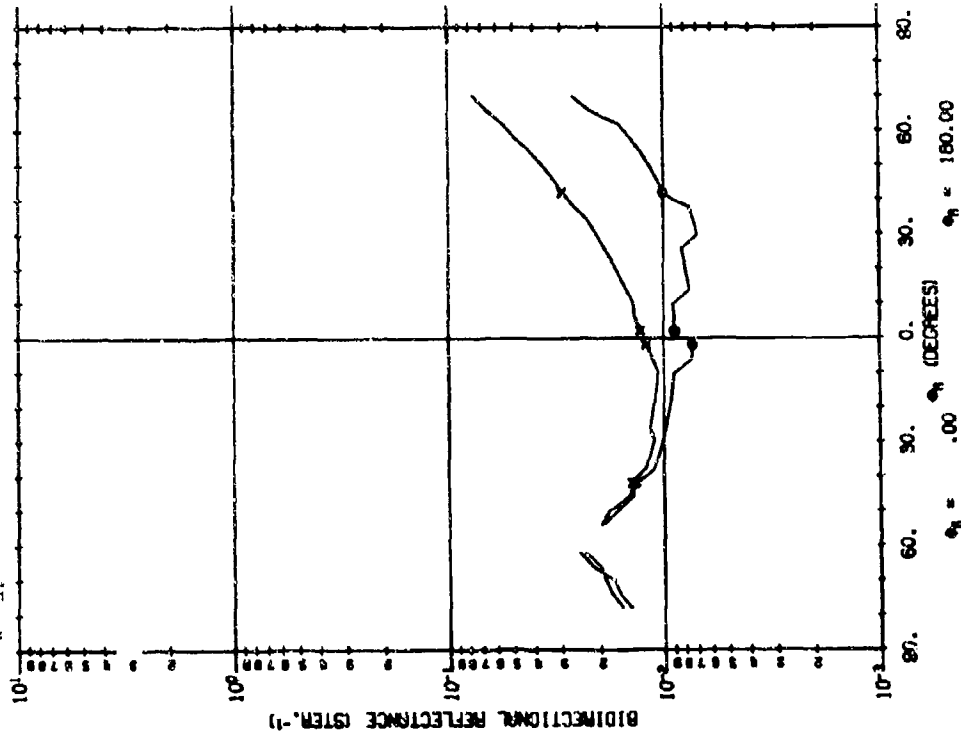
||



R01674 101

Black Treated Canvas, 4 Percent Reflectance

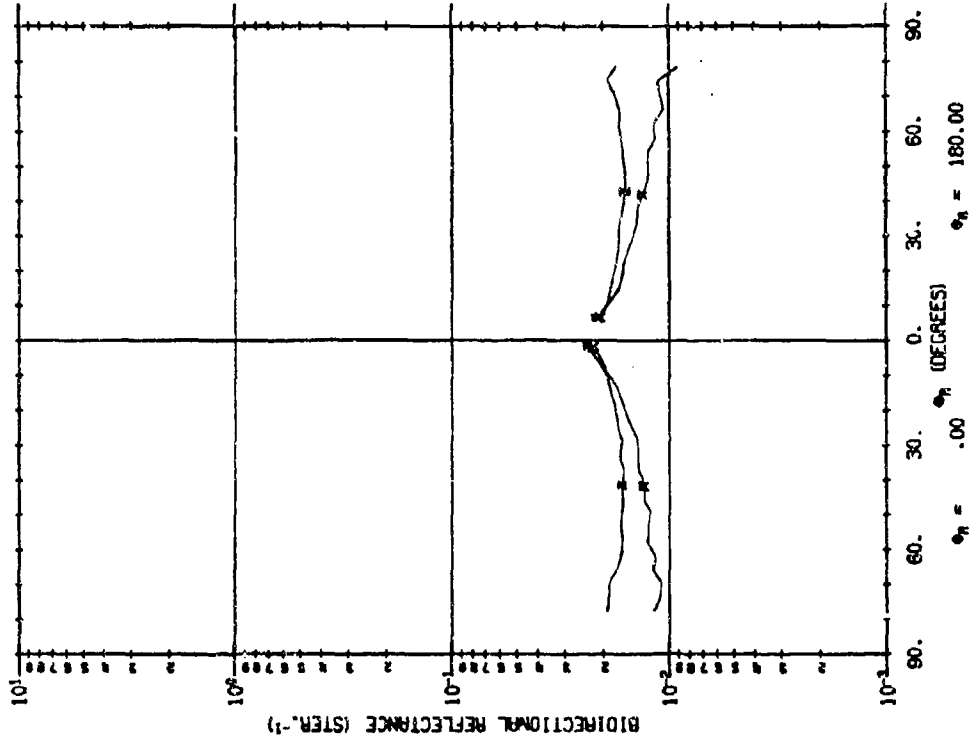
$\theta_1 = 60.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$



R01674 102

Black Treated Canvas, 4 Percent Reflectance

$\theta_1 = 0.0$
 $\phi_1 = 0.0$
 $\lambda = 0.63$

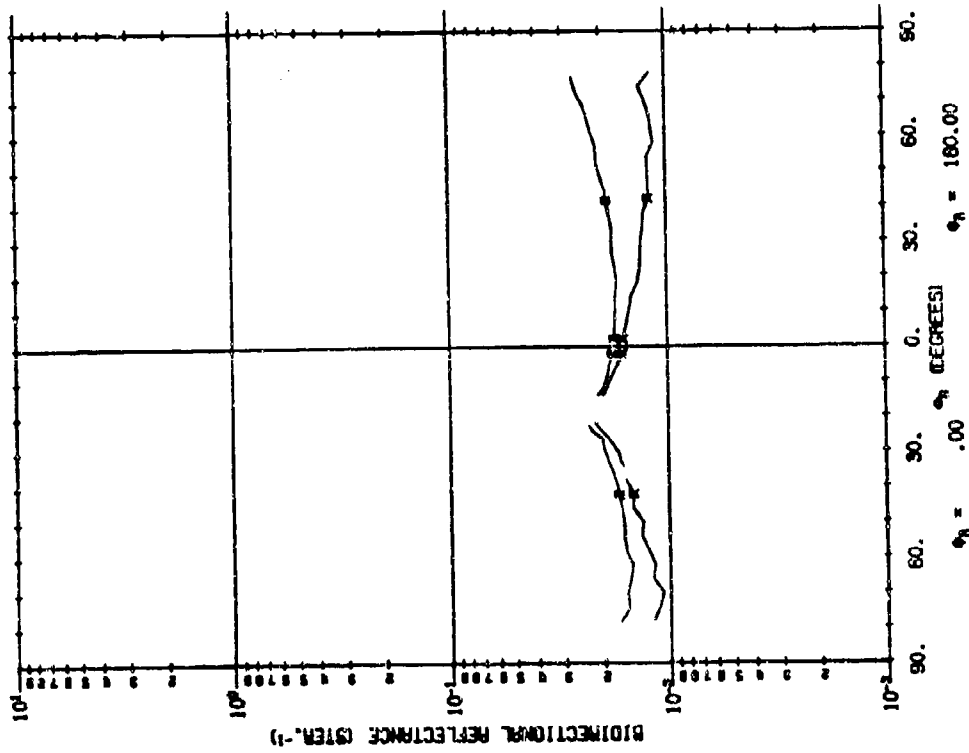


CLOTH AND CANVAS

A01674 102

Black Treated Canvas, 4 Percent Reflectance

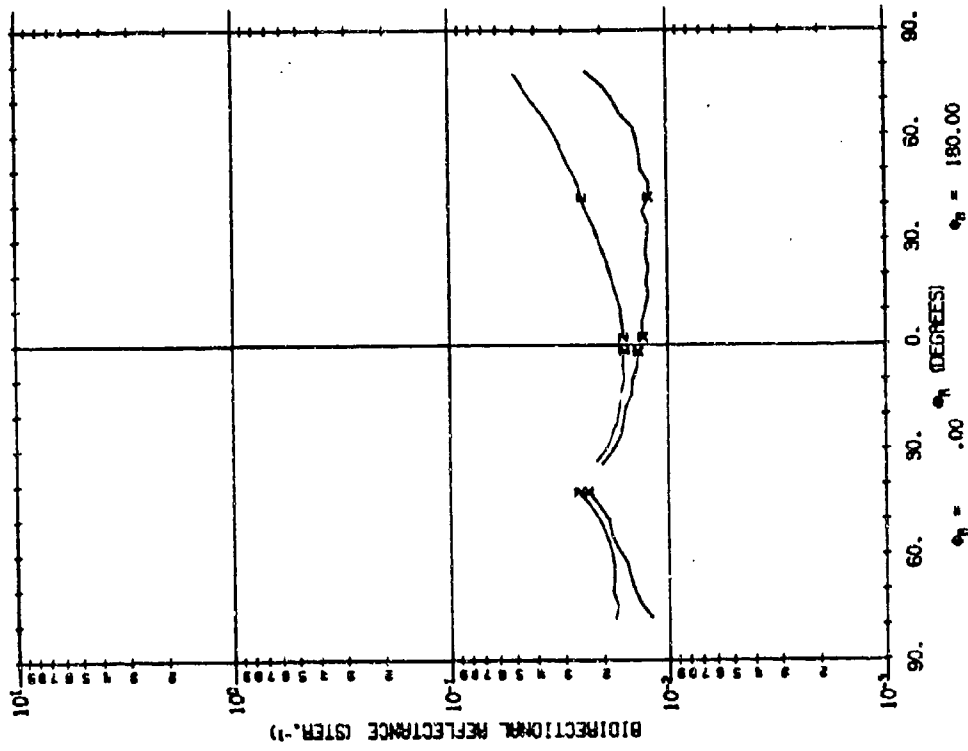
Σ |T| $\phi_1 = 20.0$
 Σ |R| $\phi_1 = 0.0$
 $\lambda = 0.63$

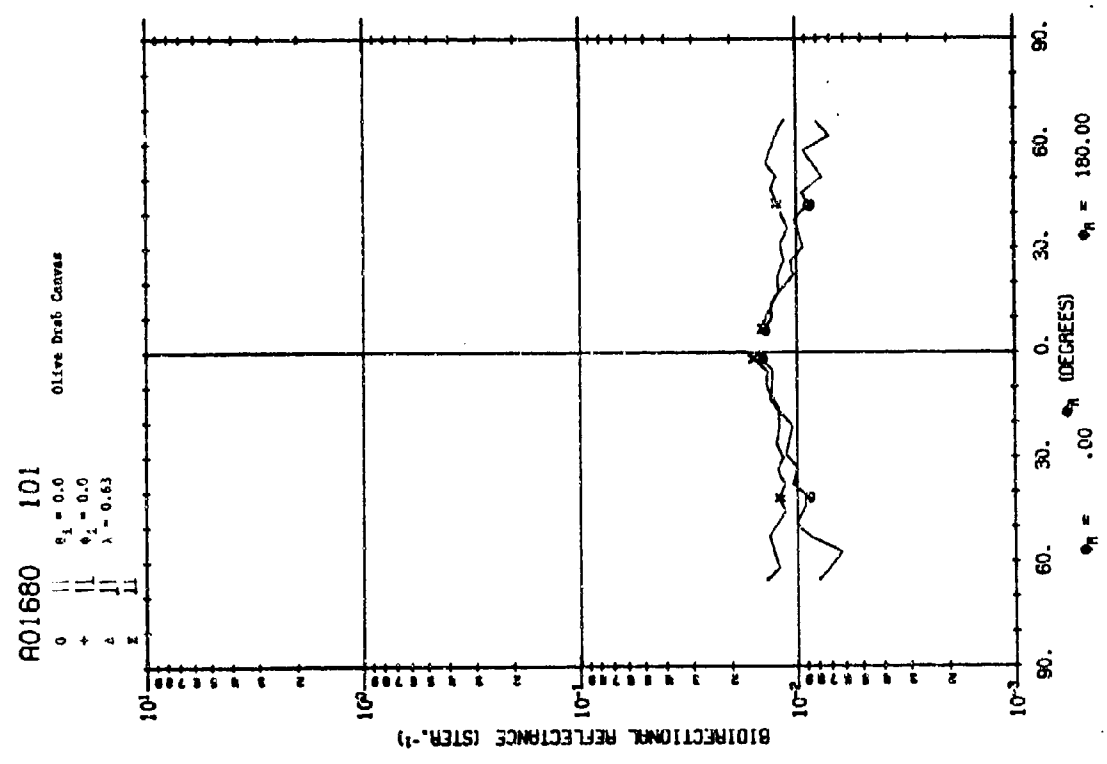
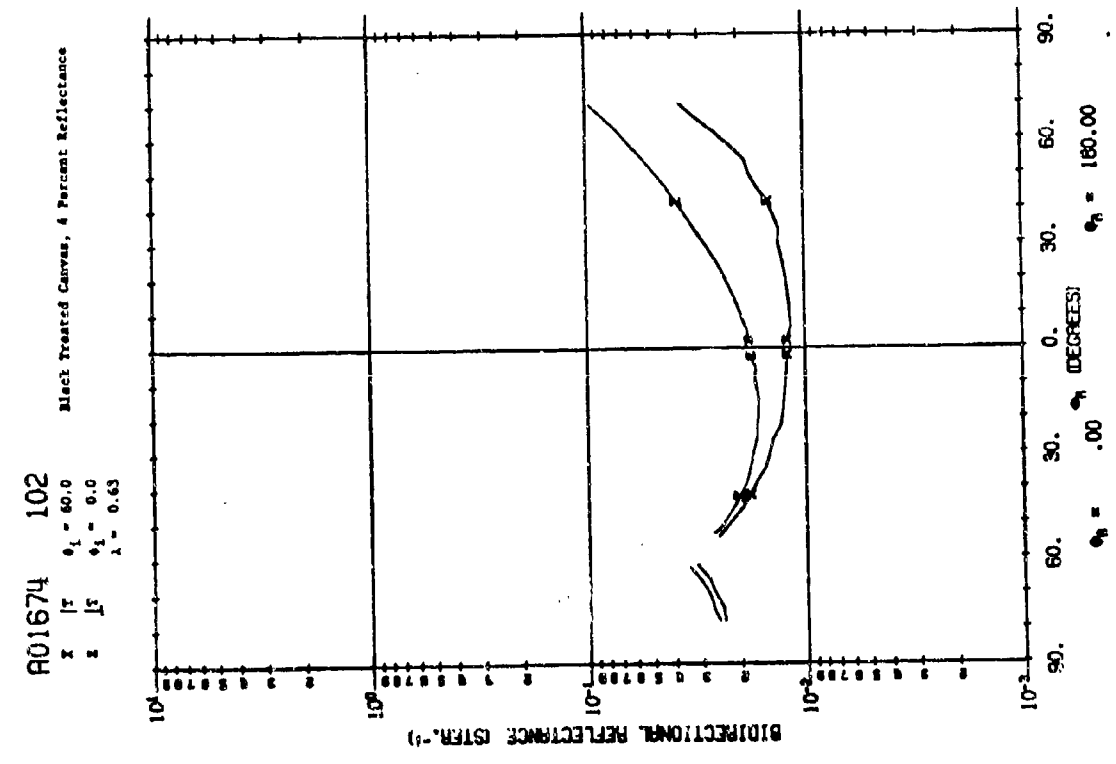


A01674 102

Black Treated Canvas, 4 Percent Reflectance

Σ |T| $\phi_1 = 40.0$
 Σ |R| $\phi_1 = 0.0$
 $\lambda = 0.63$



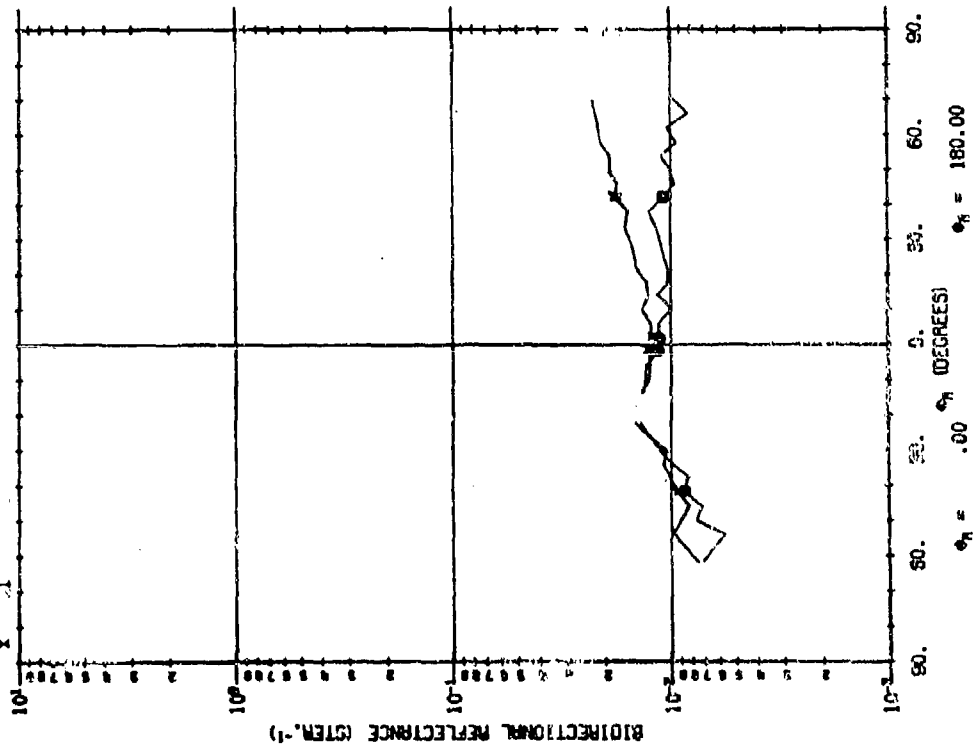


CLOTH AND CANVAS

R01680 101

Olive Drab Canvas

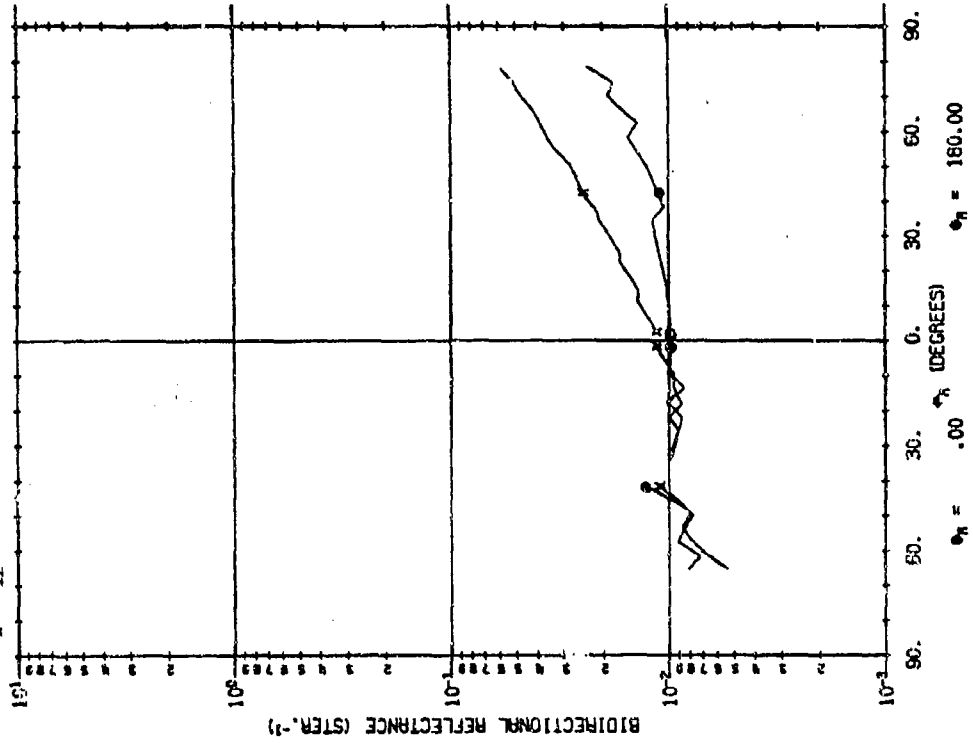
0 || $\theta_1 = 20.0$
+ || $\theta_2 = 0.0$
A || $\lambda = 0.63$
X ||



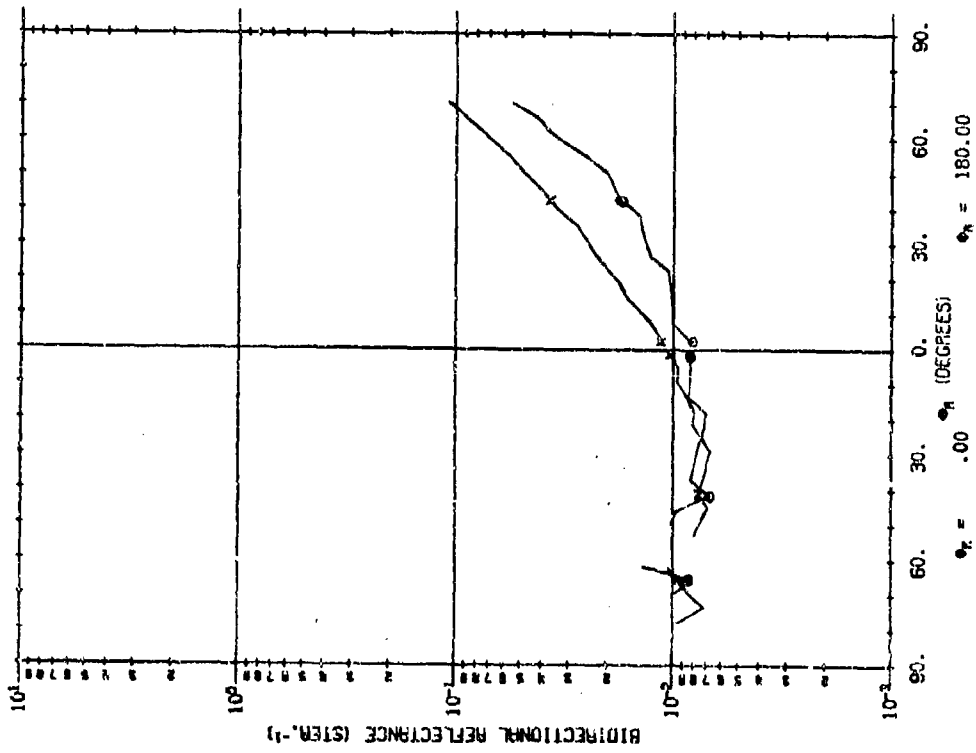
R01680 101

Olive Drab Canvas

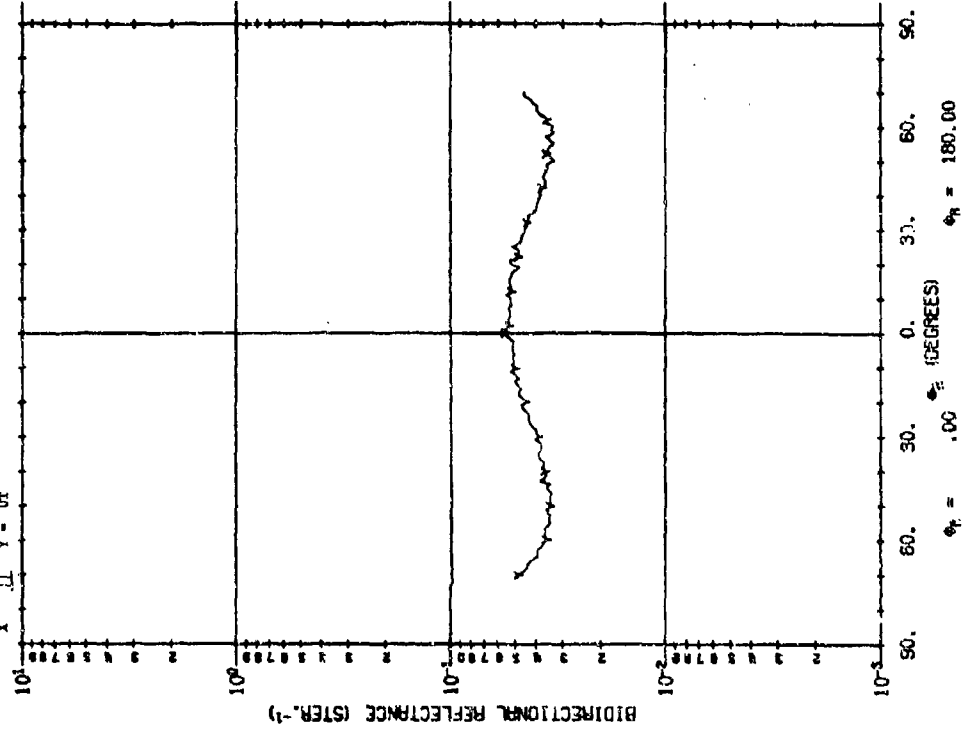
0 || $\theta_1 = 40.0$
+ || $\theta_2 = 0.0$
A || $\lambda = 0.63$
X ||



R01680 101
 OLIVE DRAB CANVAS
 0 || $\theta_1 = 60.0$
 + || $\theta_2 = 0.0$
 Δ || $\lambda = 0.63$
 X ||



R01680 301
 OLIVE DRAB CANVAS
 0 || $\theta_1 = 2.0$
 + || $\theta_2 = \theta_1$
 Δ || $\lambda = 10.6$
 X || Y - UT

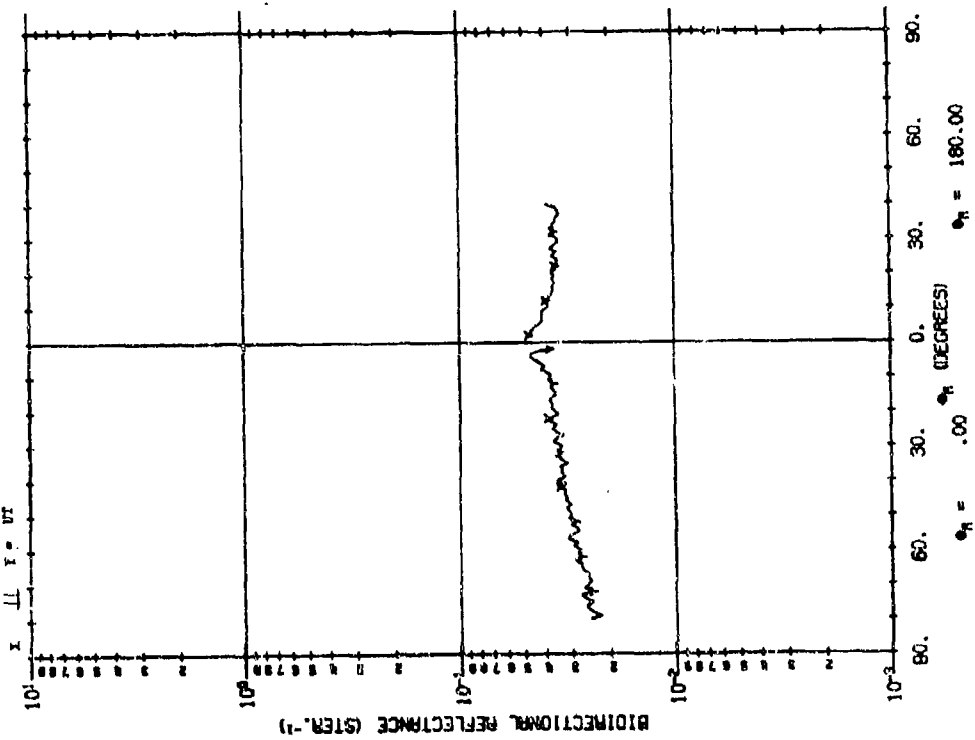


CLOTH AND CANVAS

A01680 301

OLIVE DRAB CURVAS

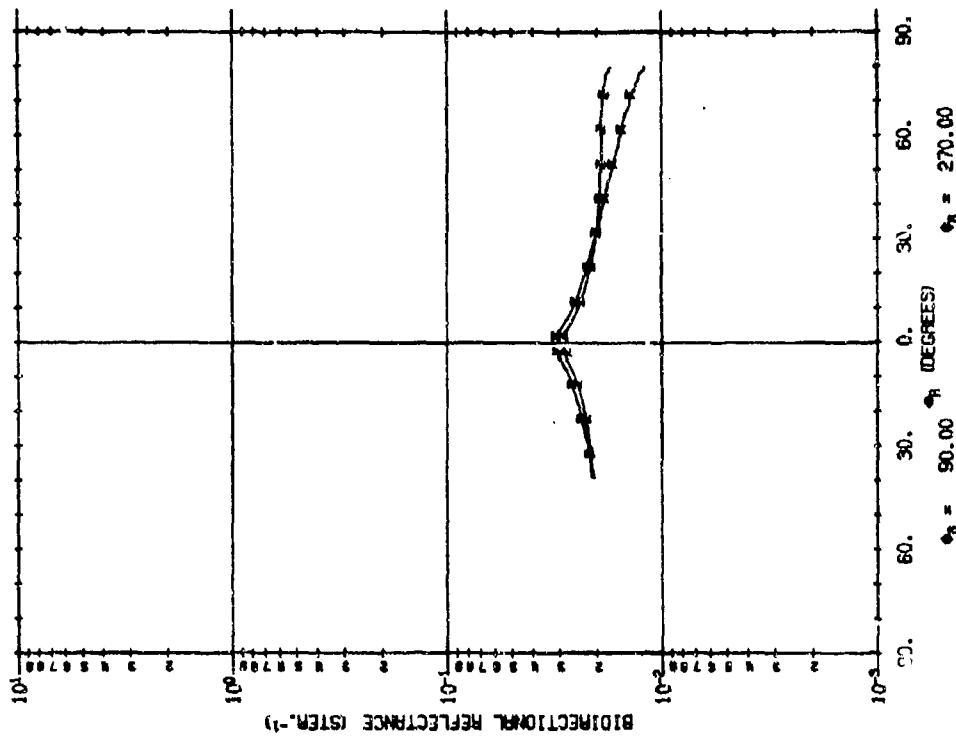
0 || $\theta_1 = 6.0$
 + || $\theta_2 = 180.0$
 A || $\lambda = 10.6$
 X || $\gamma = 0^\circ$



A01802 101

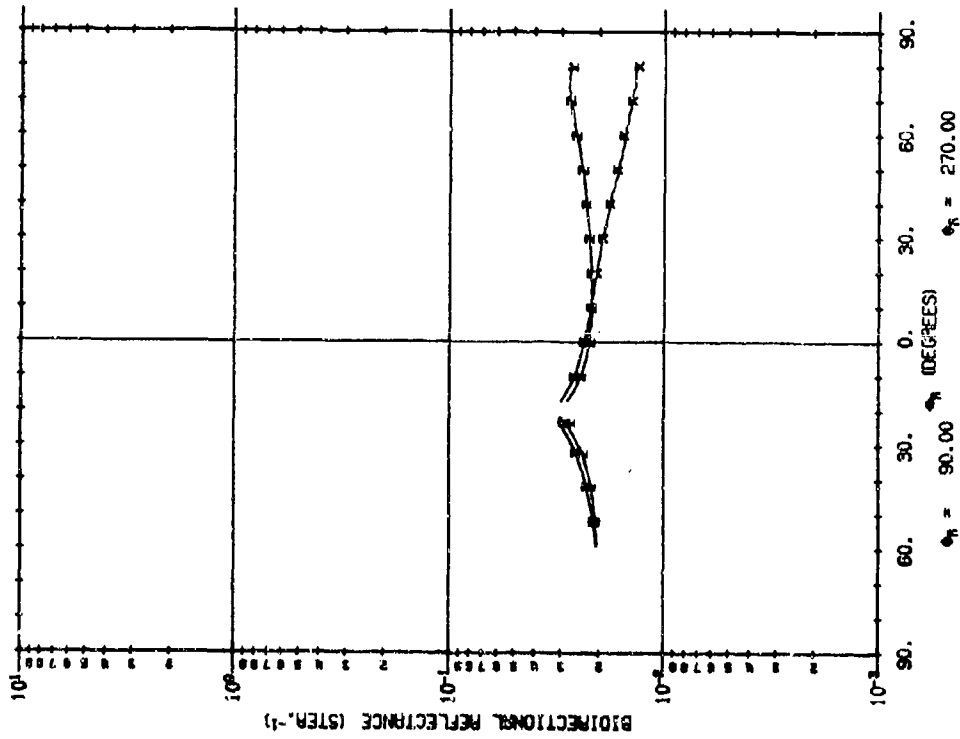
GRAY CURVAS, 8 PERCENT REFLECTANCE

X || $\theta_1 = 6.0$
 Z || $\theta_2 = 90.0$
 A || $\lambda = 0.63$



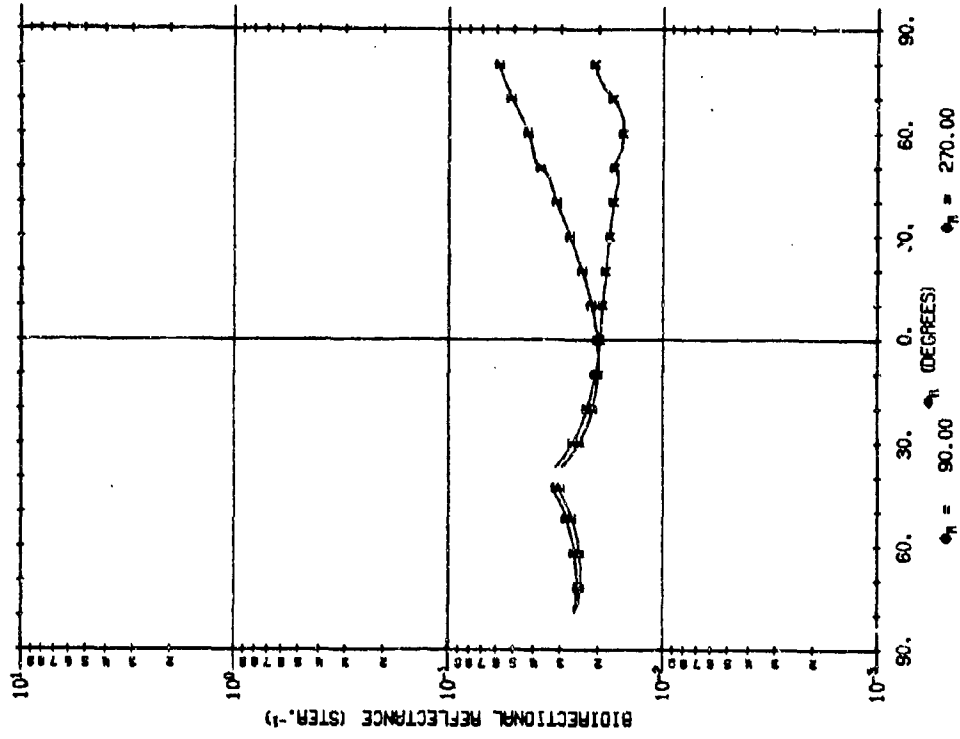
R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE
X $\epsilon_1 = 20.0$
Z $\epsilon_1 = 90.0$
A = 0.63



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE
X $\epsilon_1 = 40.0$
Z $\epsilon_1 = 90.0$
A = 0.63

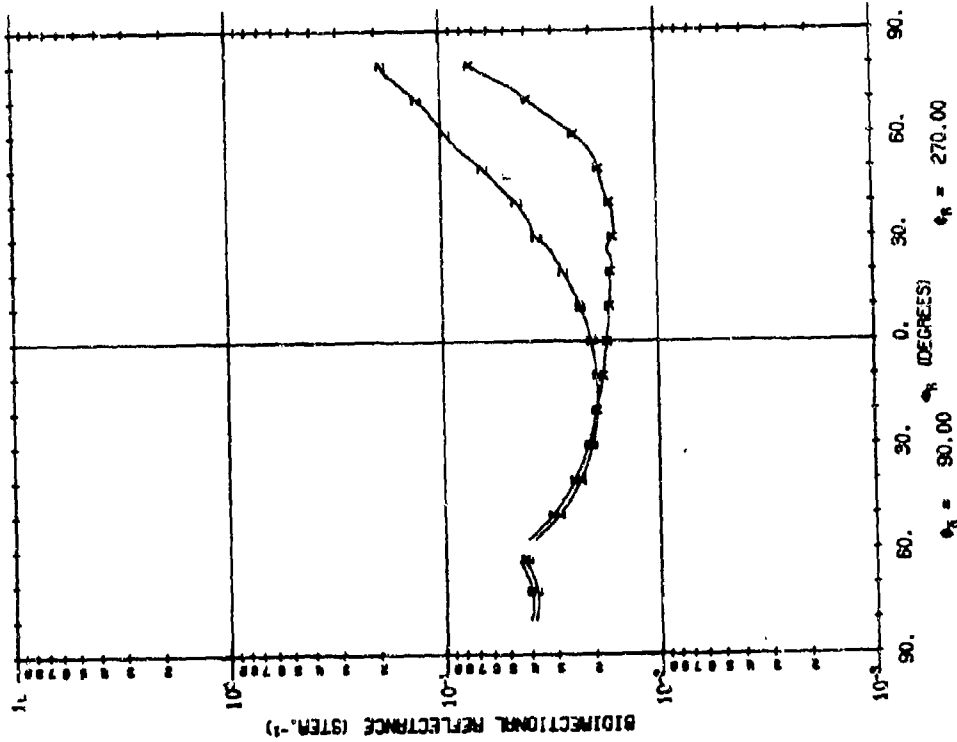


CLOTH AND CANVAS

R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

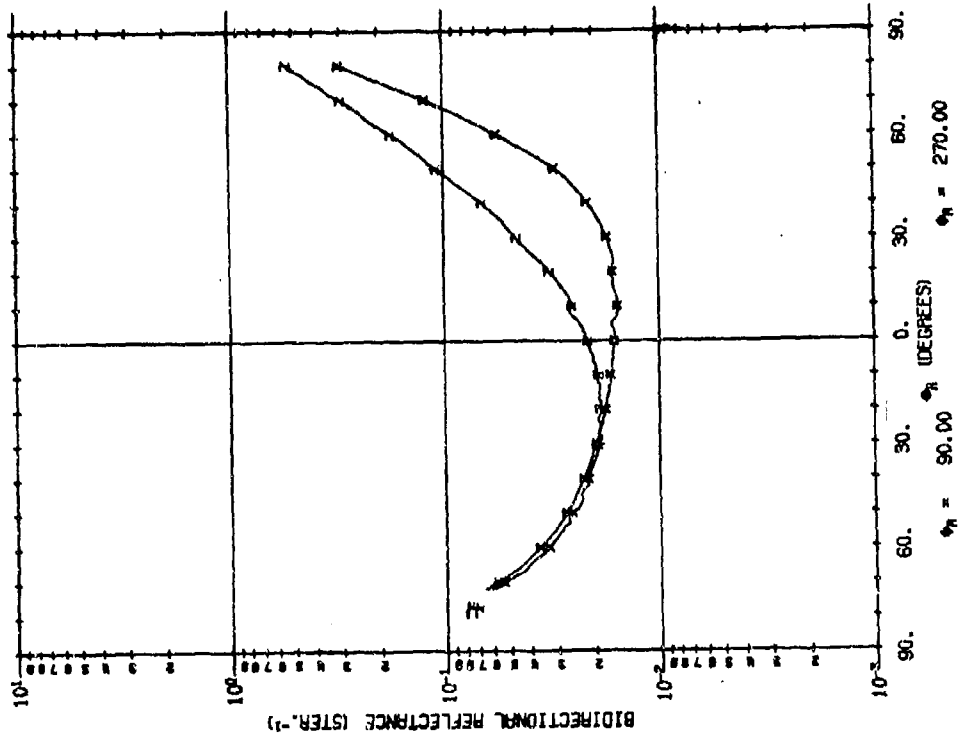
X $\theta_i = 60.0$
Z $\theta_r = 90.0$
 $\lambda = 0.63$



R01802 101

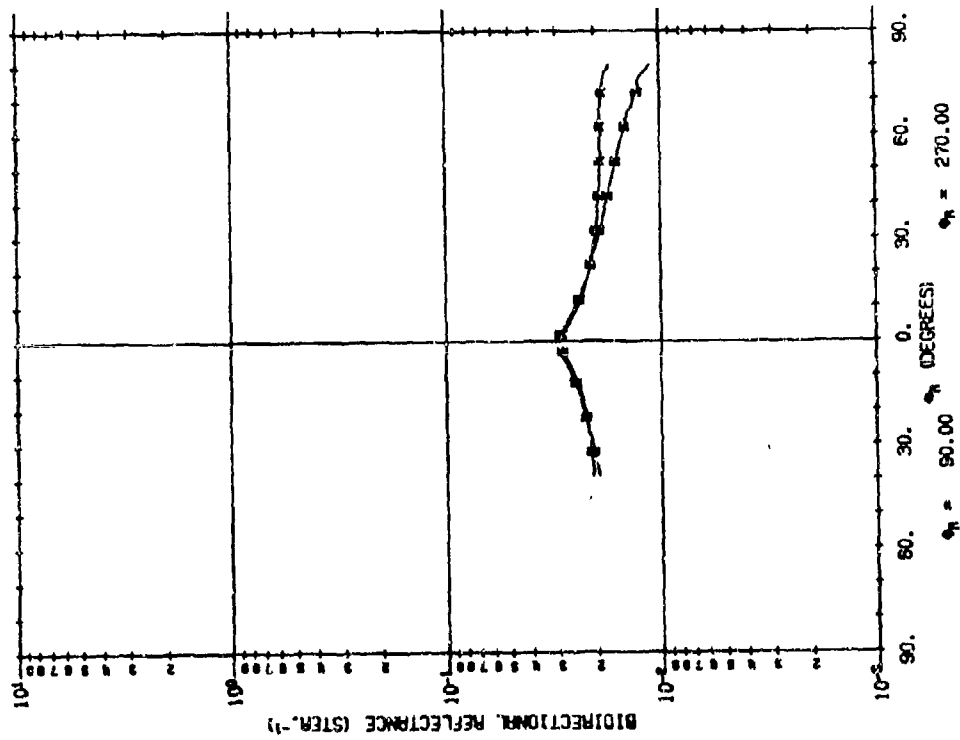
GRAY CANVAS, 8 PERCENT REFLECTANCE

X $\theta_i = 75.0$
Z $\theta_r = 90.0$
 $\lambda = 0.63$



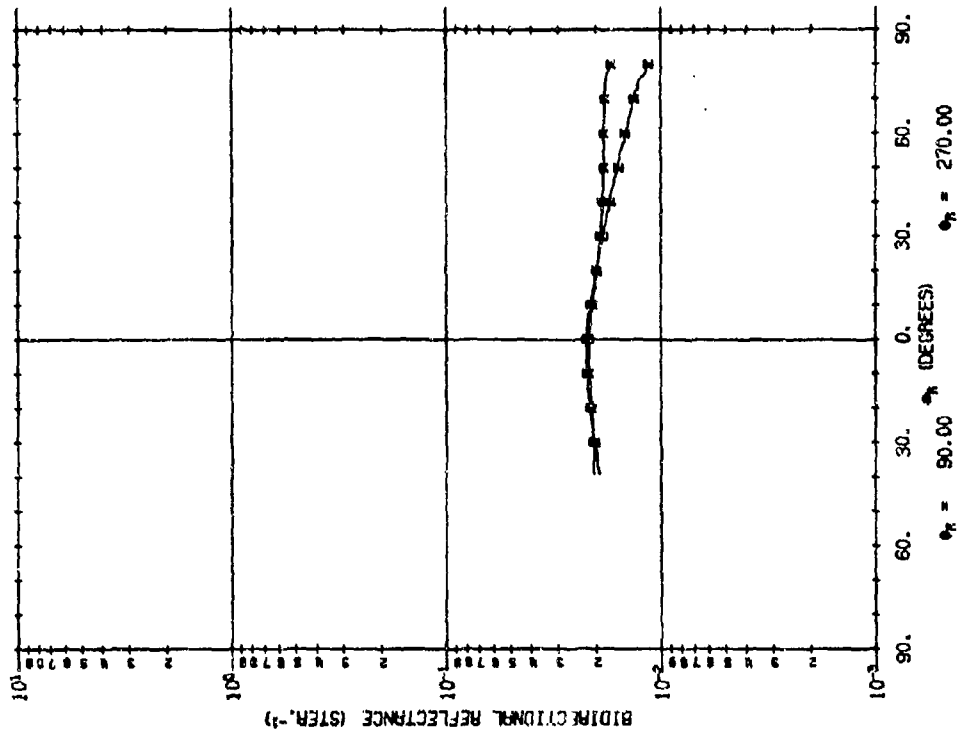
R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE
X $\int T \quad \phi_1 = 0.0$
Z $\int T \quad \phi_1 = 0.0$
 $\lambda = 0.63$



R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE
X $\int T \quad \phi_1 = 20.0$
Z $\int T \quad \phi_1 = 0.0$
 $\lambda = 0.63$

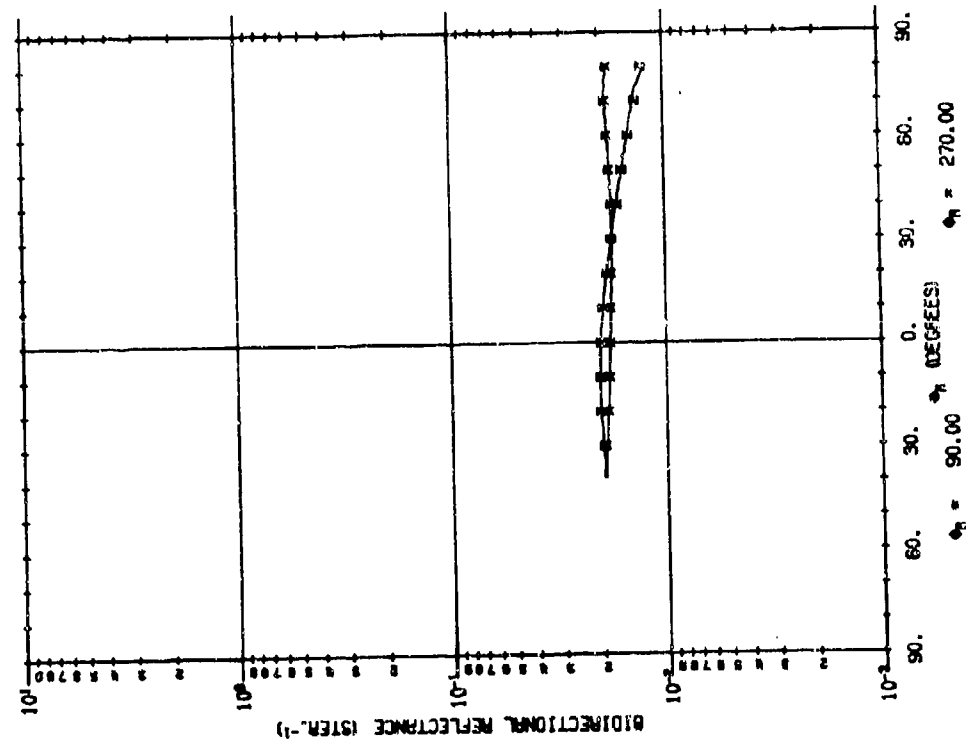


CLOTH AND CANVAS

R01802 101

GRAY CANVAS, 8 PERCENT REFLECTANCE

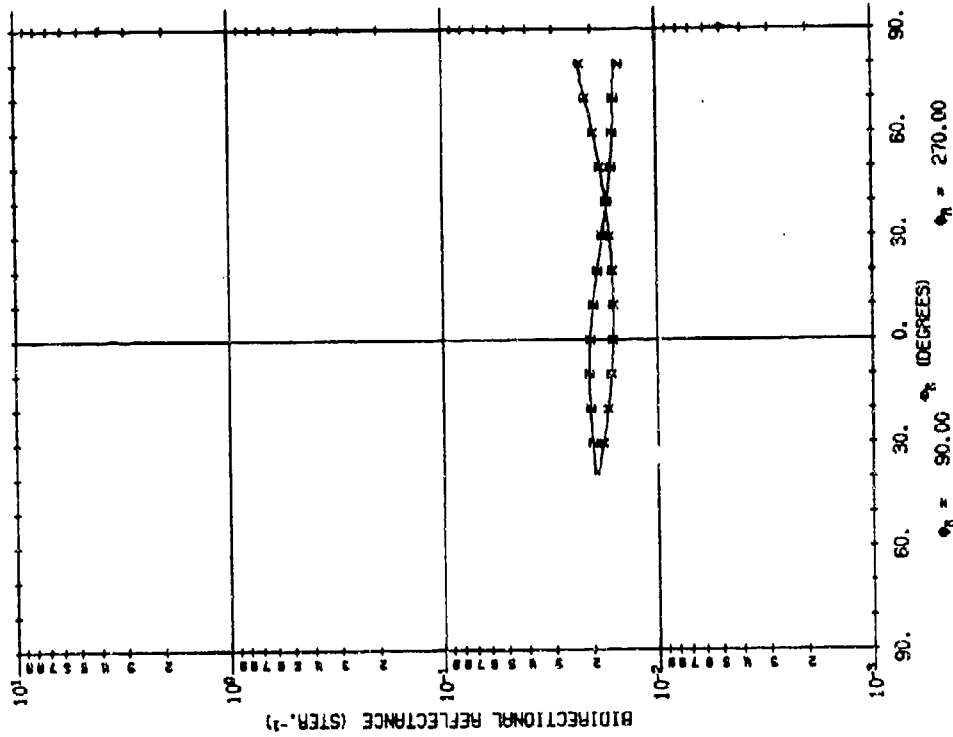
X $\beta_1 = 40.0$
Z $\beta_2 = 0.0$
 $\lambda = 0.63$



R01802 101

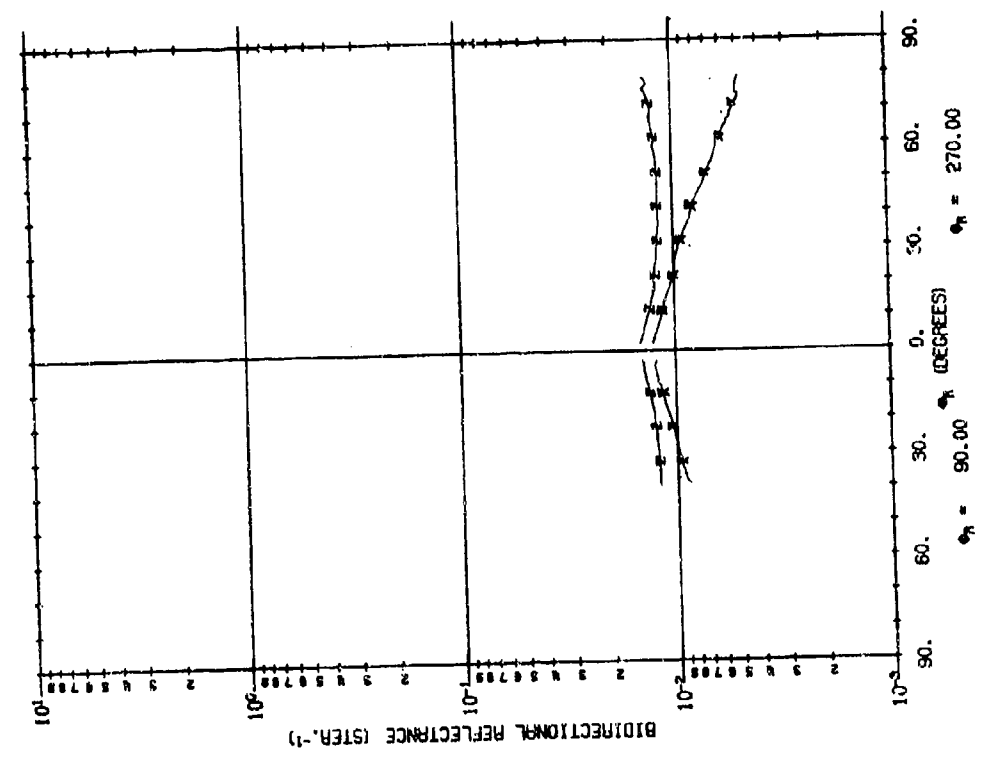
GRAY CANVAS, 8 PERCENT REFLECTANCE

X $\beta_1 = 60.0$
Z $\beta_2 = 0.0$
 $\lambda = 0.63$



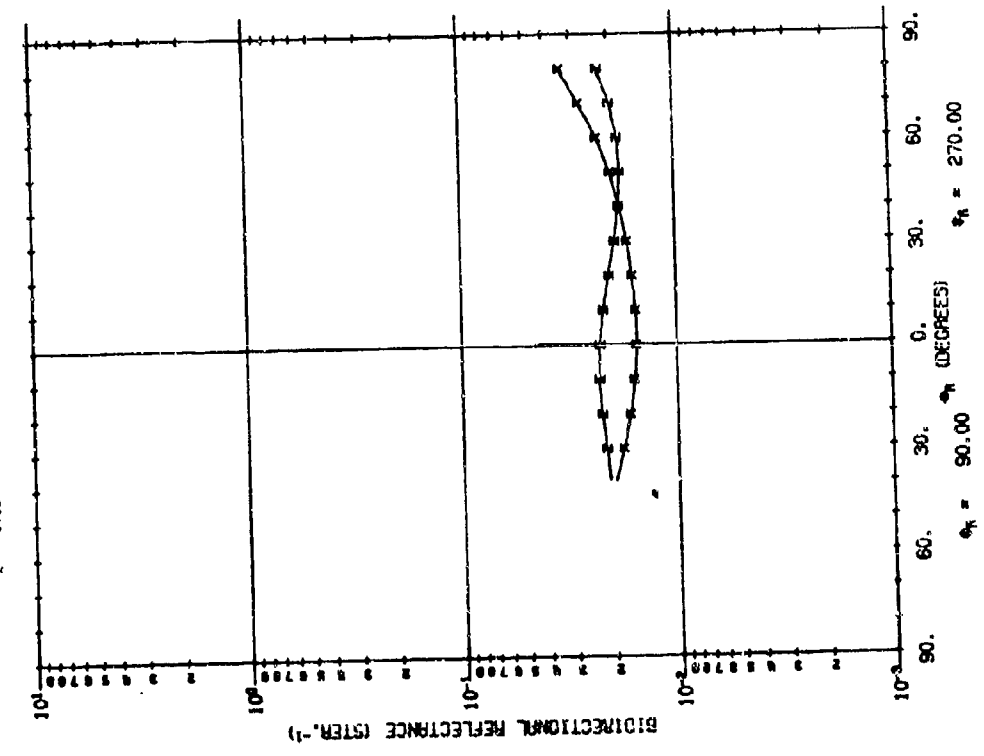
A01803 101
 X IT $\theta_1 = 0.0$
 Z IT $\theta_2 = 90.0$
 $\lambda = 0.63$

BLACK CANVAS, 4 PERCENT REFLECTANCE



A01802 101
 X IT $\theta_1 = 75.0$
 Z IT $\theta_2 = 0.0$
 $\lambda = 0.63$

GRAY CANVAS, 8 PERCENT REFLECTANCE

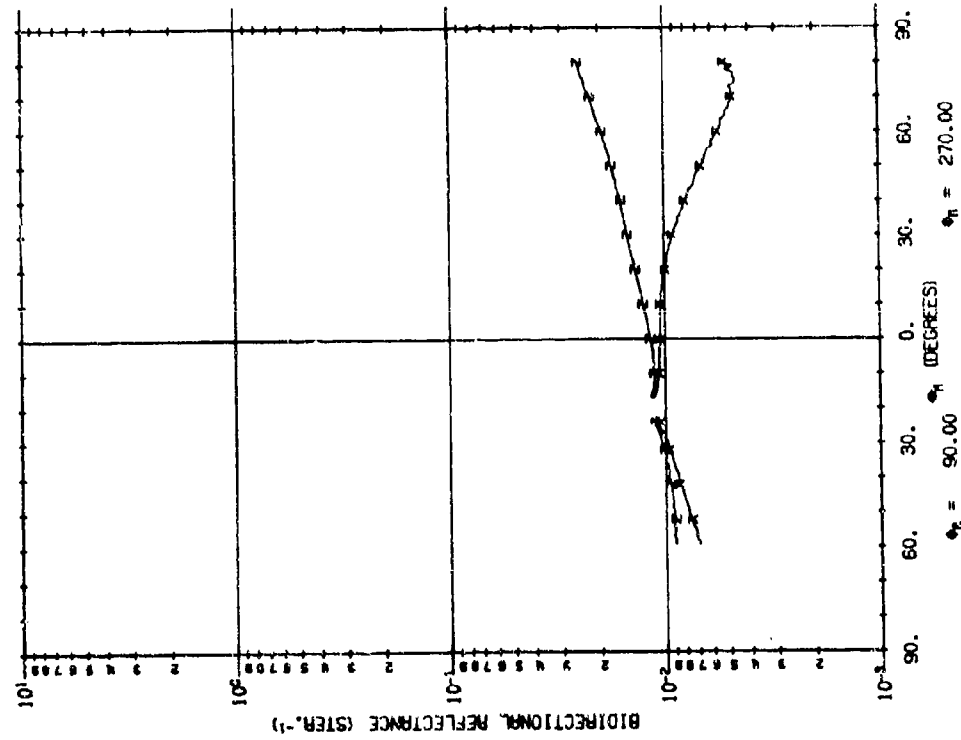


CLOTH AND CANVAS

R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

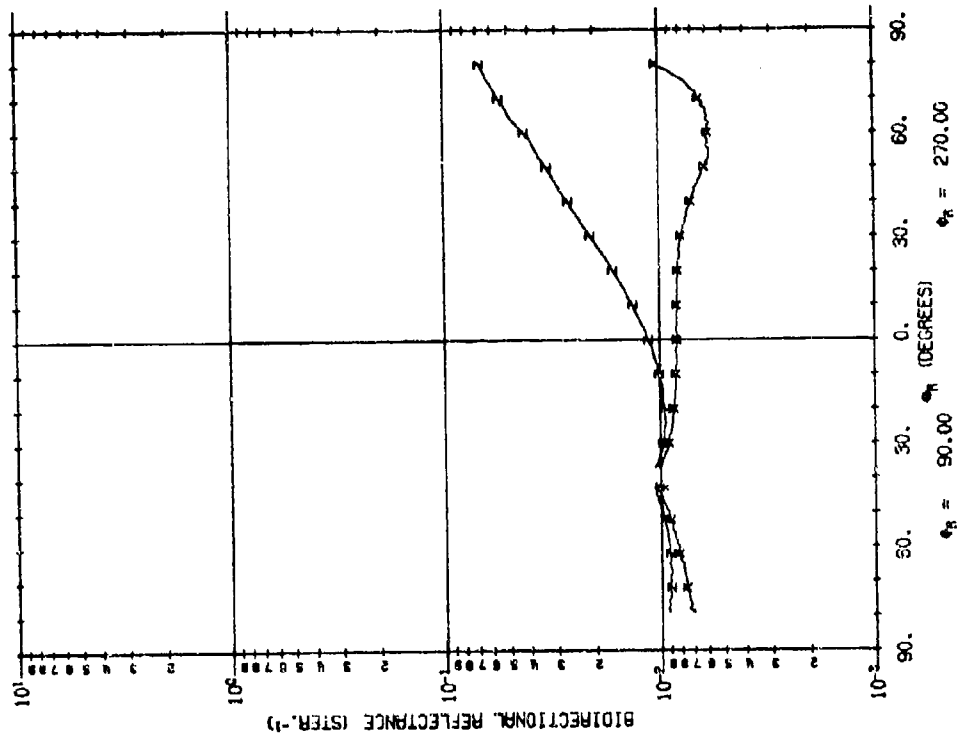
X $\theta_1 = 70.0$
Z $\theta_2 = 90.0$
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

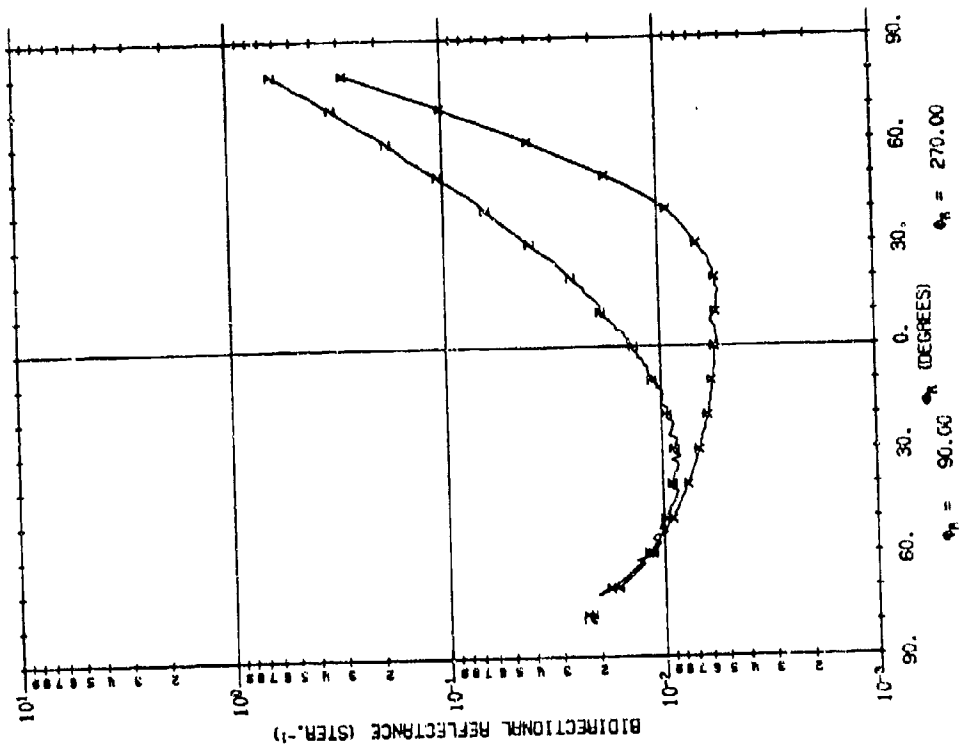
X $\theta_1 = 40.0$
Z $\theta_2 = 90.0$
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

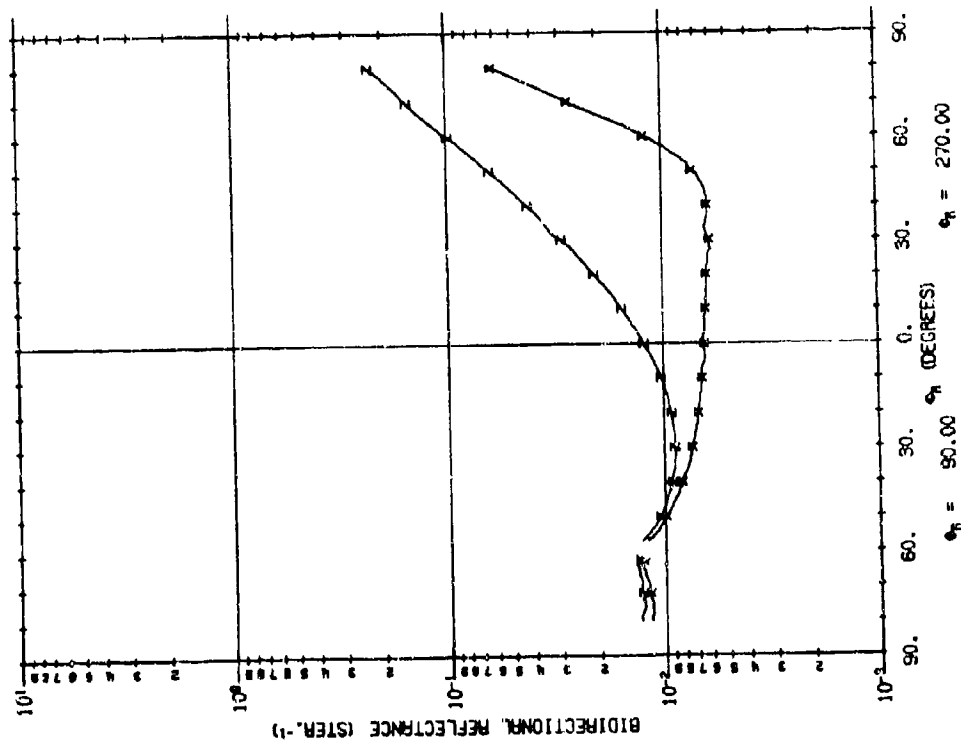
X $\theta_1 = 75.0$
Z $\theta_1 = 90.0$
 $\lambda = 0.63$



R01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

X $\theta_1 = 60.0$
Z $\theta_1 = 90.0$
 $\lambda = 0.63$

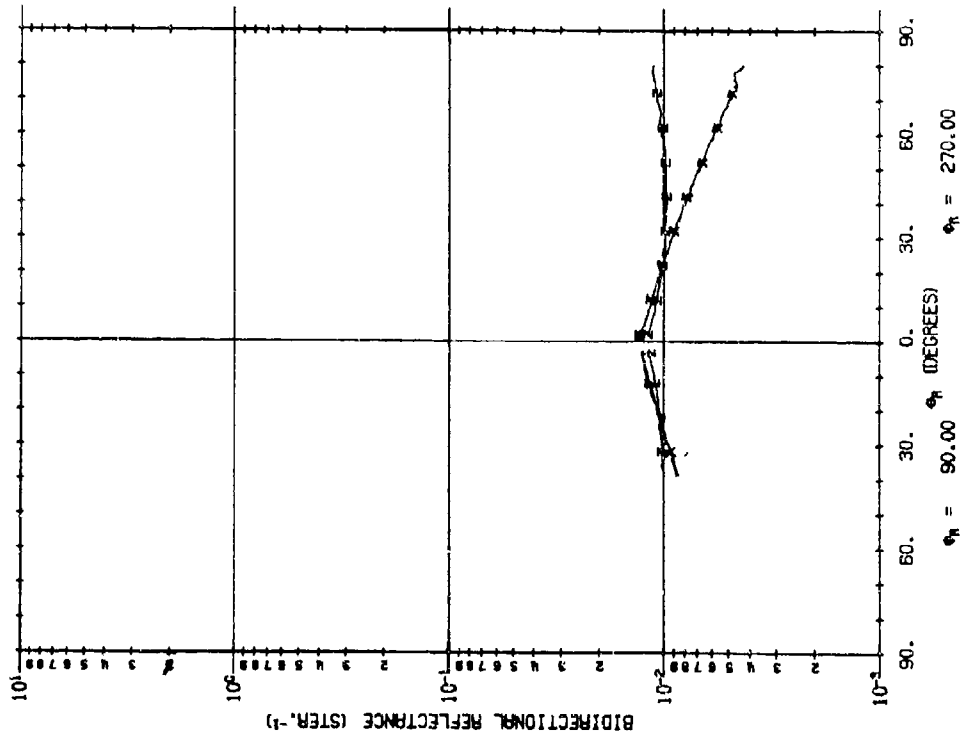


CLOTH AND CANVAS

A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

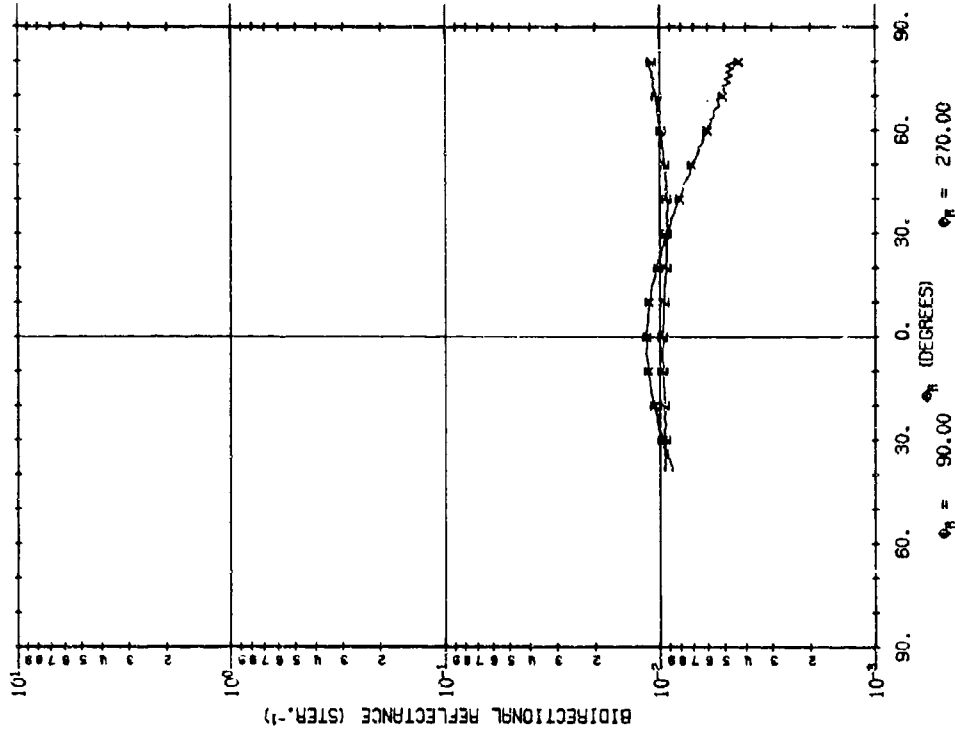
X $\int T$ $\rho_i = 0.0$
Z $\int T$ $\rho_i = 0.0$
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

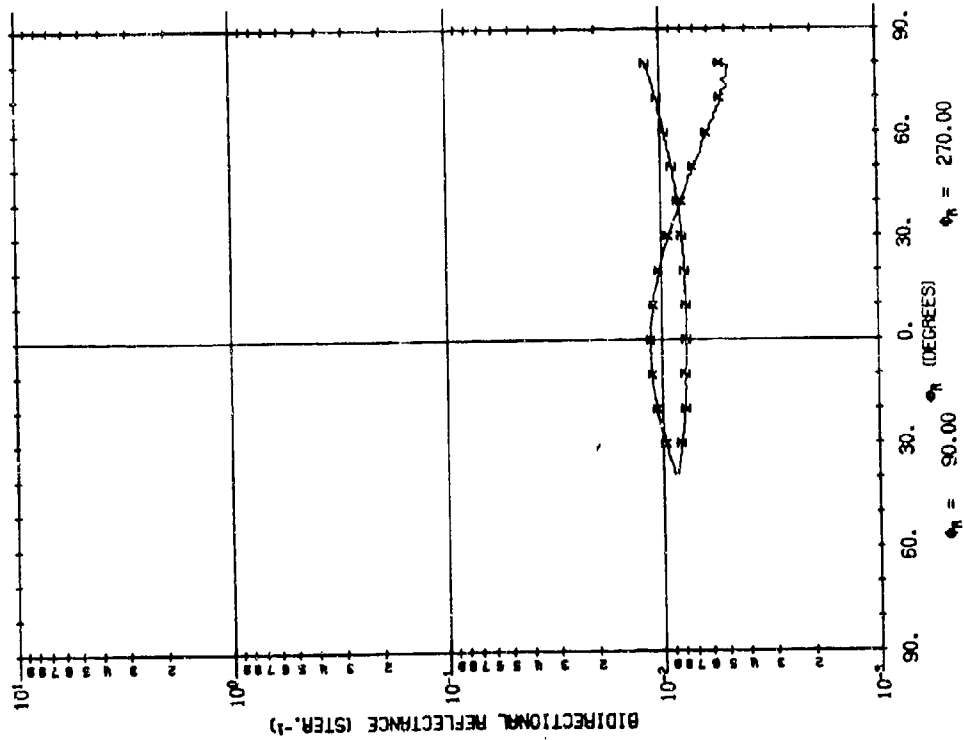
X $\int T$ $\rho_i = 20.0$
Z $\int T$ $\rho_i = 0.0$
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

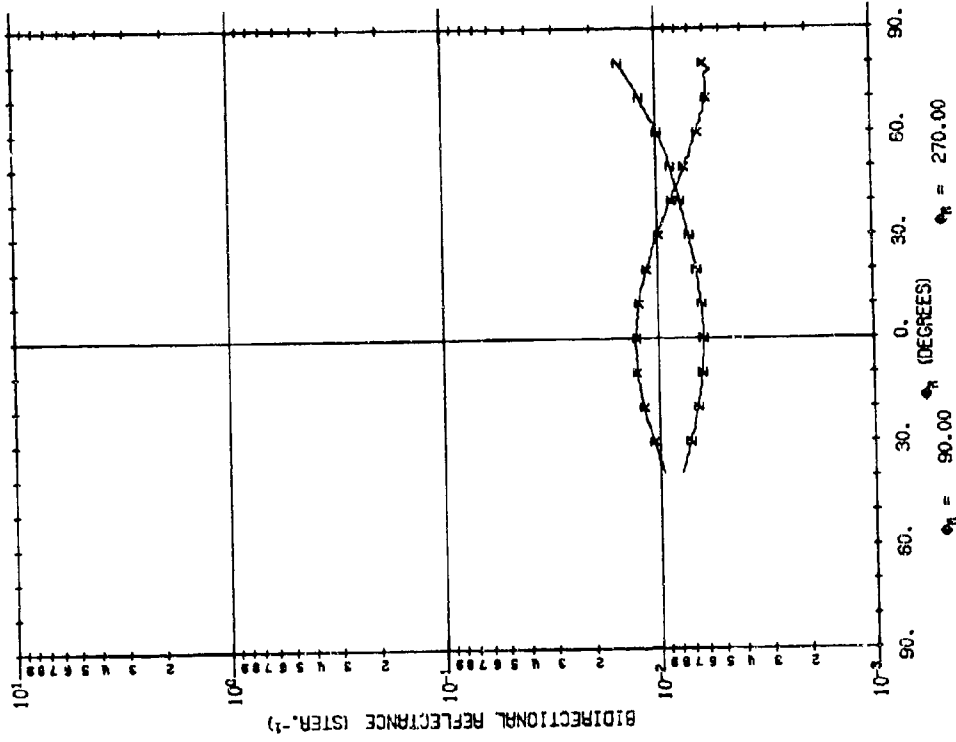
X $\theta_1 = 40.0$
Z $\theta_2 = 0.0$
 $\lambda = 0.63$



A01803 101

BLACK CANVAS, 4 PERCENT REFLECTANCE

X $\theta_1 = 60.0$
Z $\theta_2 = 0.0$
 $\lambda = 0.63$

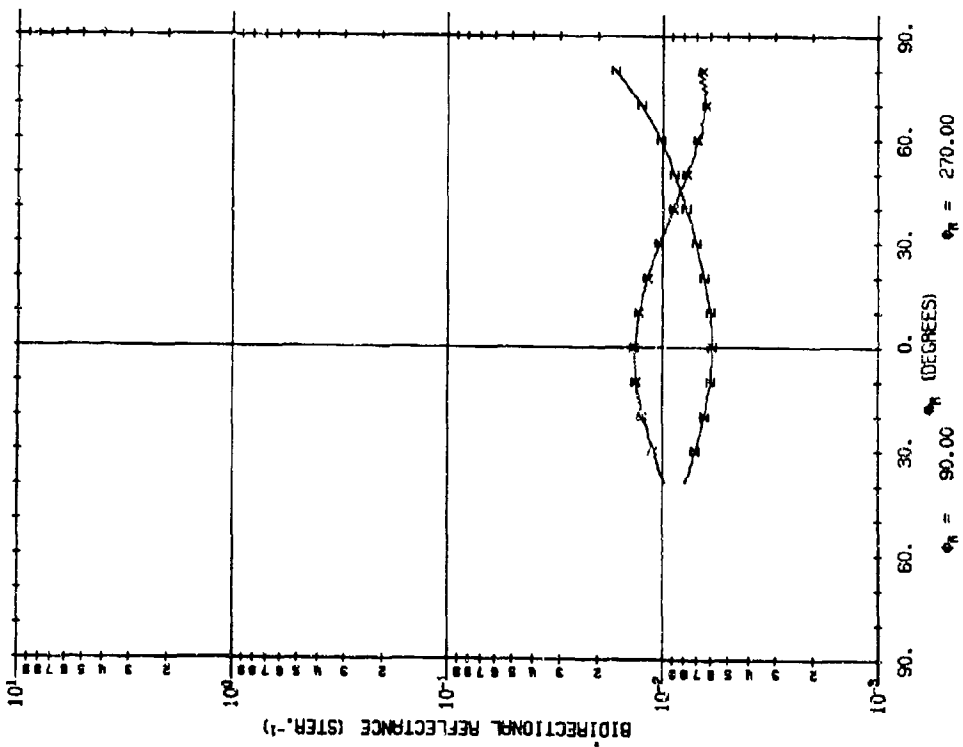


CLOTH AND CANVAS

A01803 101

BLACK CANYAS, 4 PERCENT REFLECTANCE

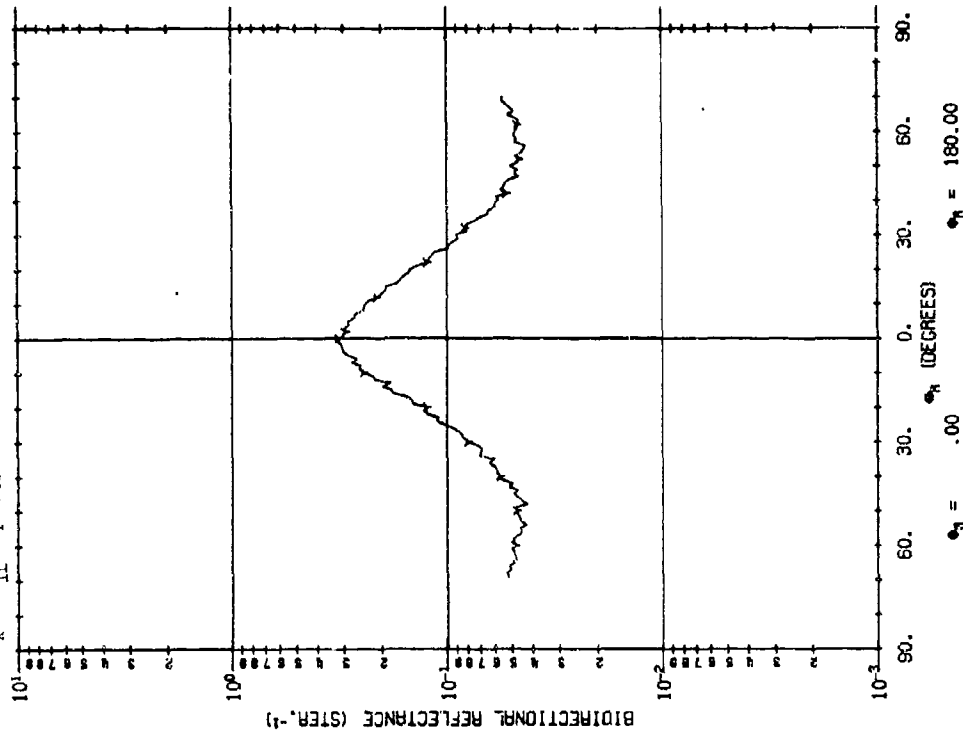
X $\Gamma_1 = 65.0$
 Z $\Gamma_2 = 0.0$
 $\lambda = 0.63$



A01820 101

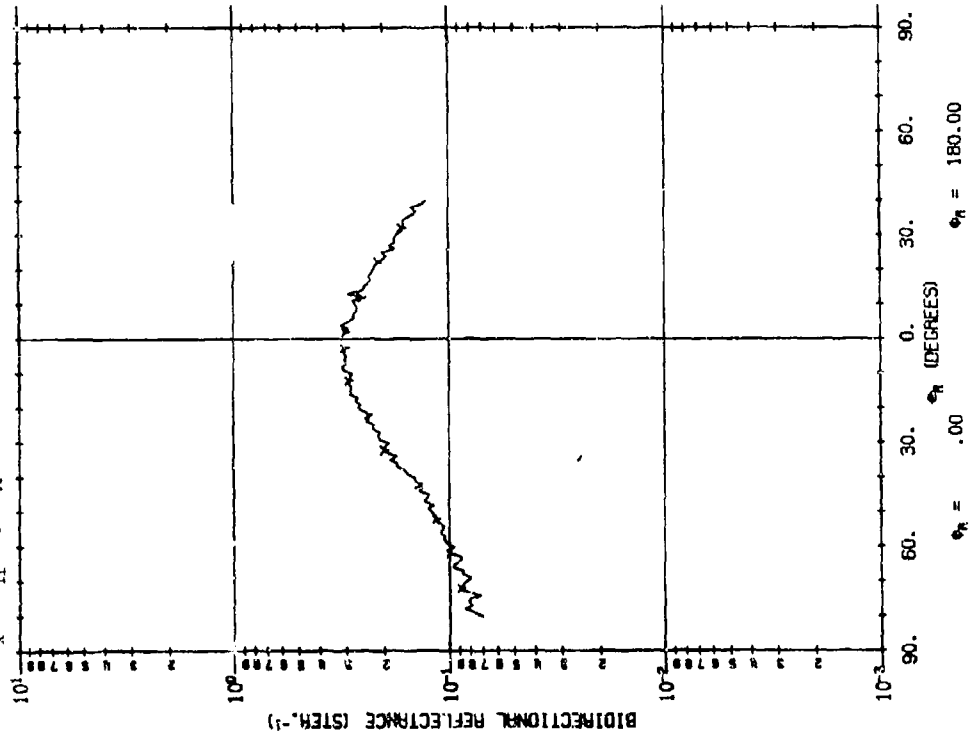
Gray Canvas Treated With
 A Metallic Coating

0 $Z_1 = 2.0$
 + $\Gamma_1 = \Gamma_2$
 - $\lambda = 10.6$
 X Y = VT



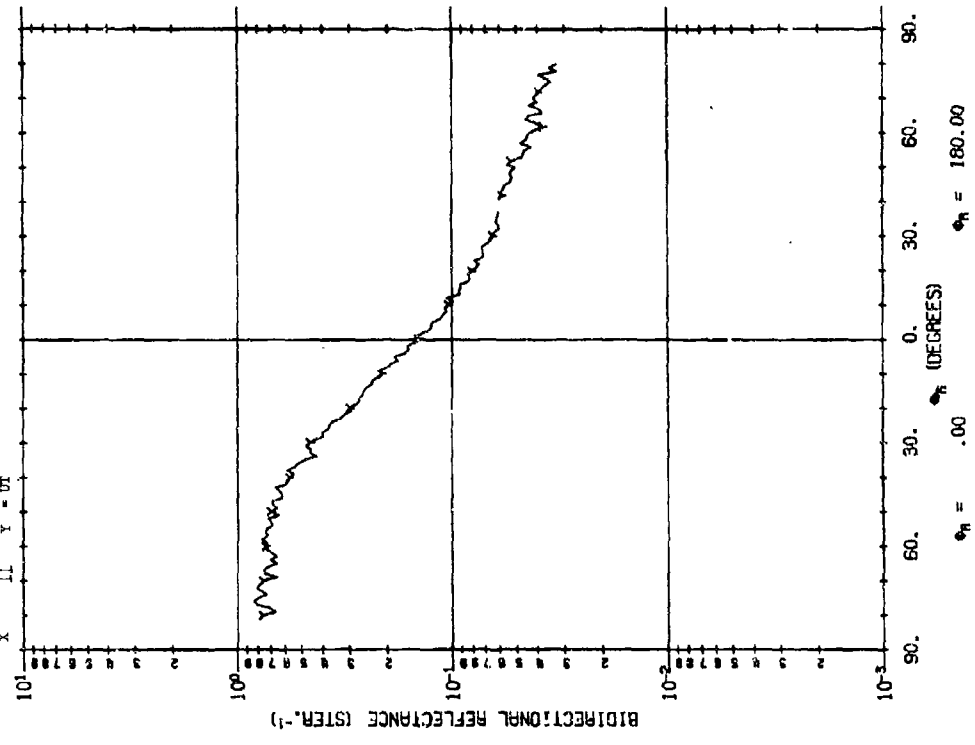
AO1820 101
 0 || $\theta_1 = 0.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
 X || $Y = VT$

Gray Canvas Treated With
 A Metallic Coating



AO1820 101
 0 || $\theta_1 = 40.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
 X || $Y = VT$

Gray Canvas Treated With
 A Metallic Coating

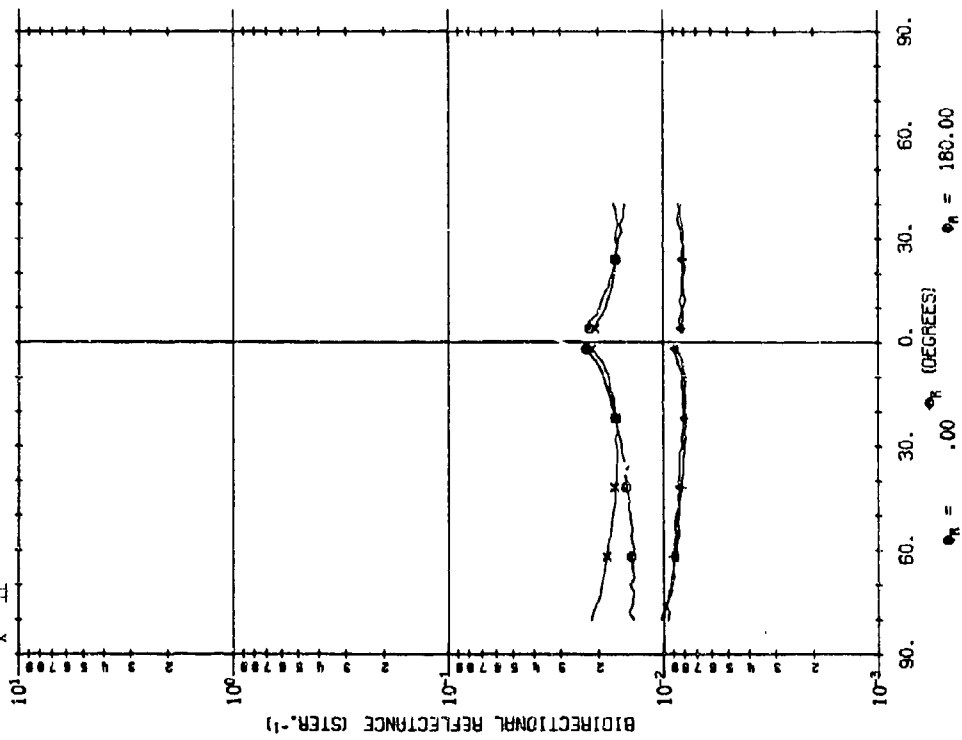


CLOTH AND CANVAS

R01853 301

OLIVE DRAB CANVAS

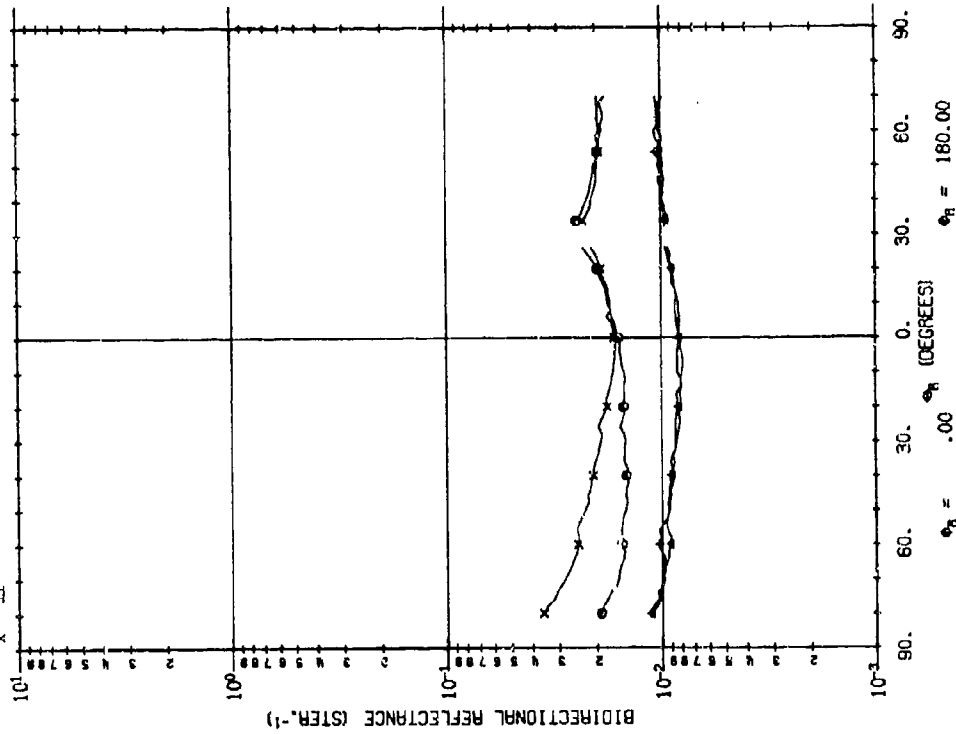
$\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



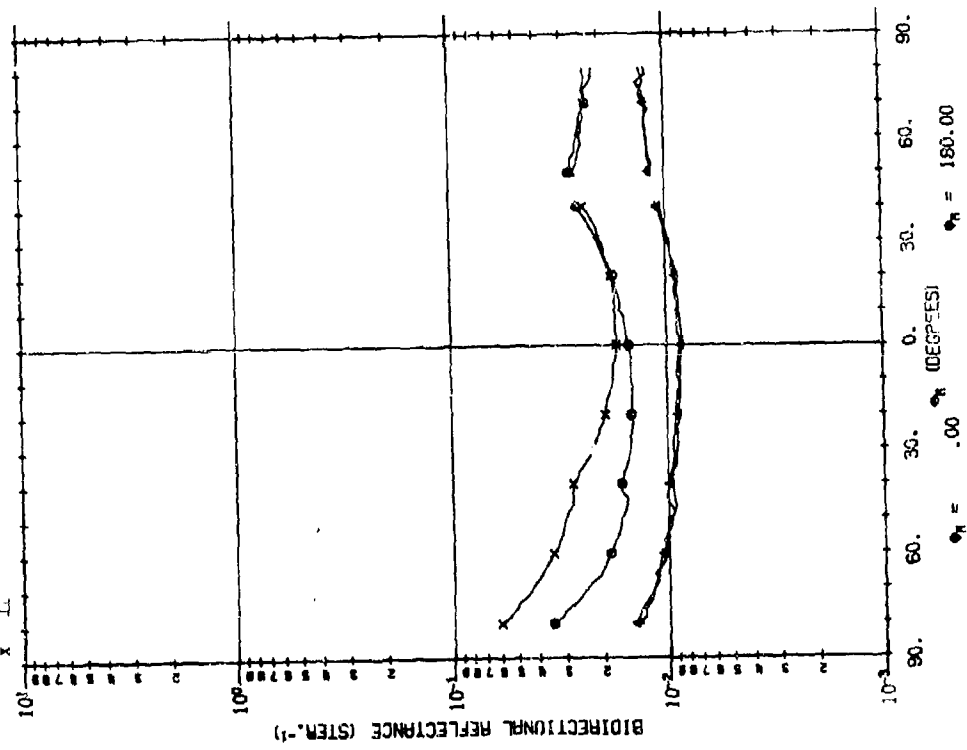
R01853 301

OLIVE DRAB CANVAS

$\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



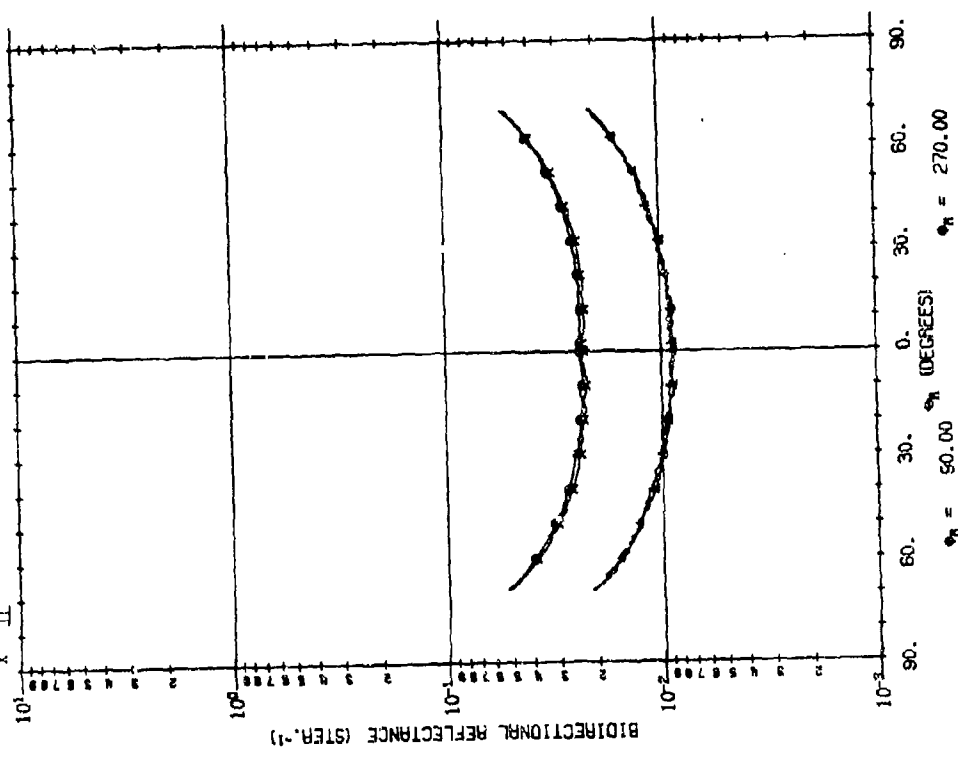
A01853 301
 OLIVE DRAB CANVAS
 $\theta_1 = 45.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



$\theta_1 = .00$ $\theta_2 = 180.00$

A01853 301
 OLIVE DRAB CANVAS

$\theta_1 = 2.0$
 $\theta_2 = \theta_1$
 $\lambda = 1.06$



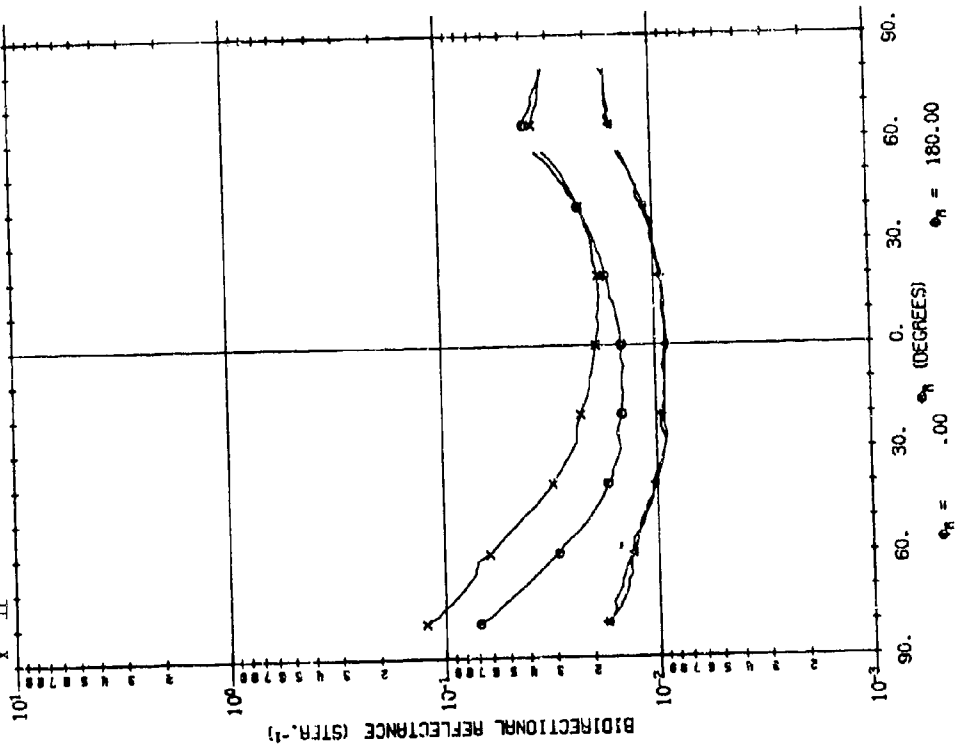
$\theta_1 = 50.00$ $\theta_2 = 270.00$

CLOTH AND CANVAS

R01853 301

OLIVE DRAB CANVAS

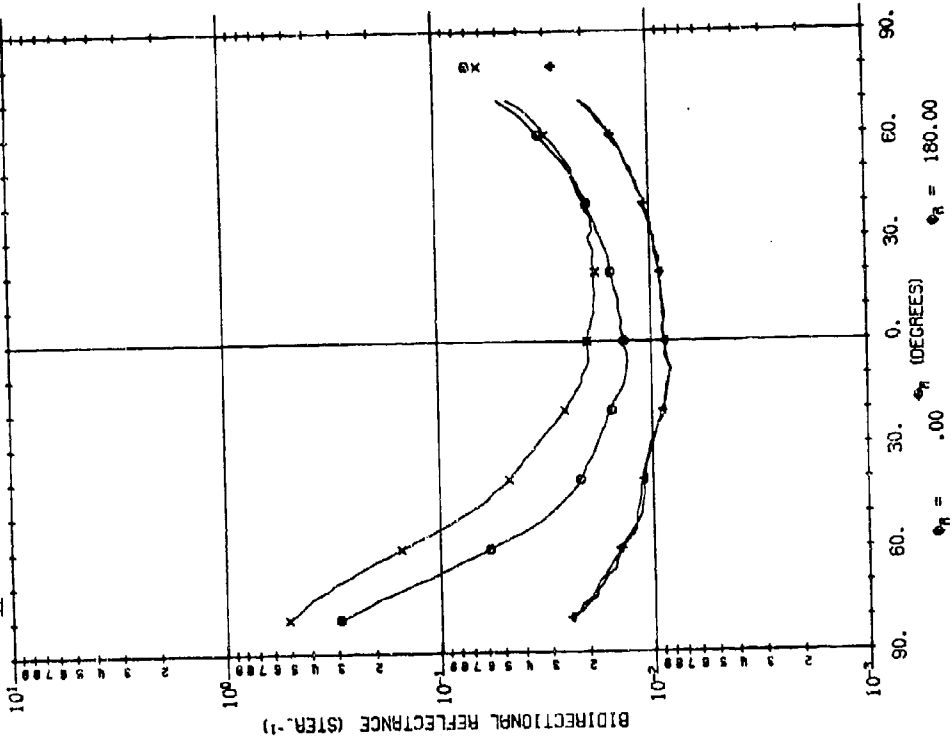
0 || $\theta_1 = 60.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 1.06$
X ||



R01853 301

OLIVE DRAB CANVAS

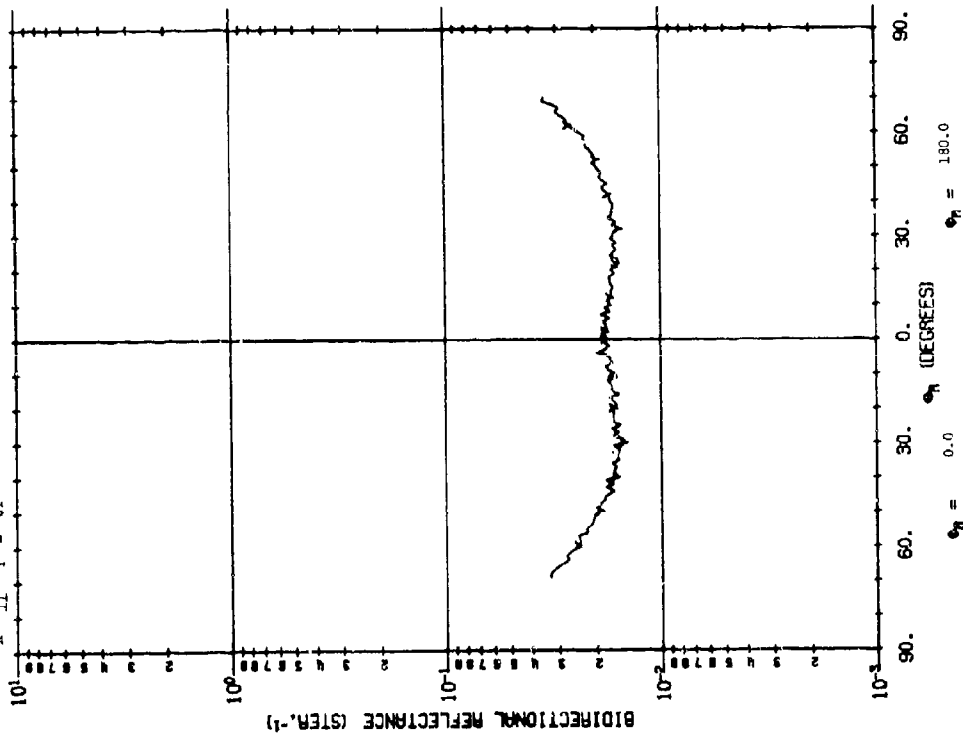
0 || $\theta_1 = 75.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 1.06$
X ||



AO1890 101

Olive Drab Canvas

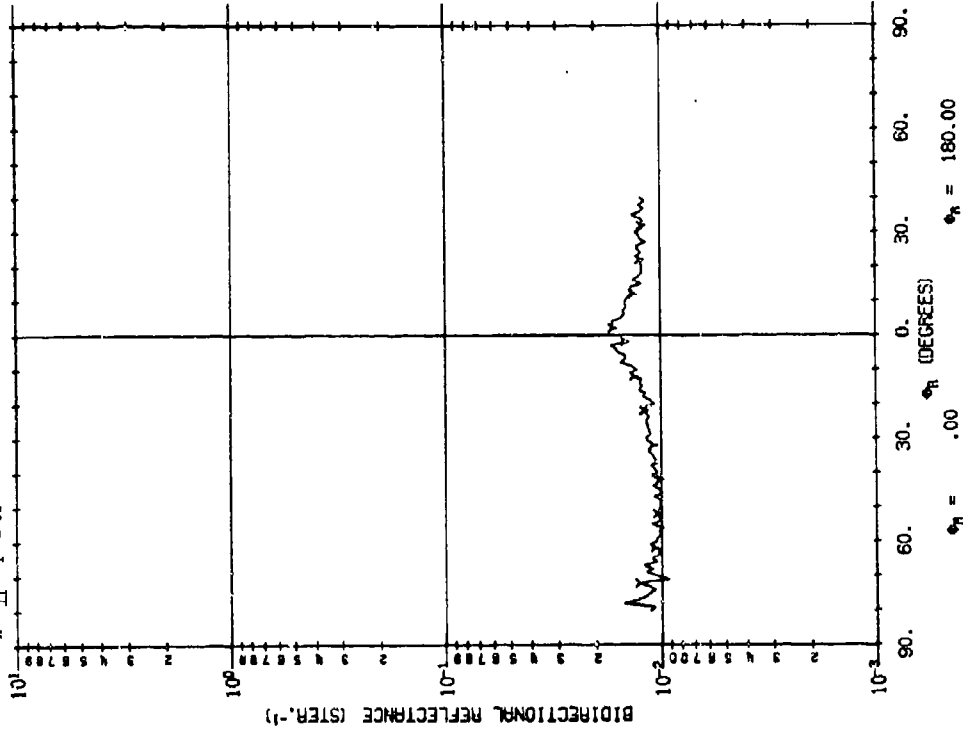
0 || $z_1 = 2.0$
+ || $\phi_1 = \phi_r$
 Δ || $\lambda = 10.6$
X || Y = VT



AO1890 101

Olive Drab Canvas

0 || $z_1 = 0.0$
+ || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = VT



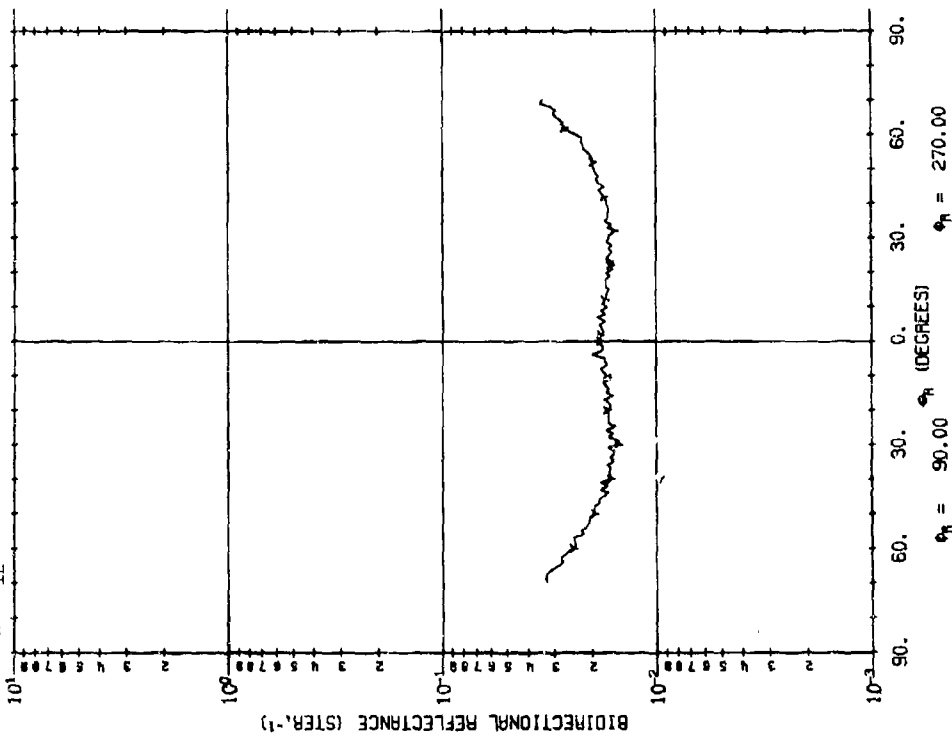
CLOTH AND CANVAS

R01890 101

OLIVE DRAB CANVAS

$2\theta = 2.0$

+ || $\phi_1 = \phi_2$
Δ || $\lambda = 10.6$
X || Y = VT

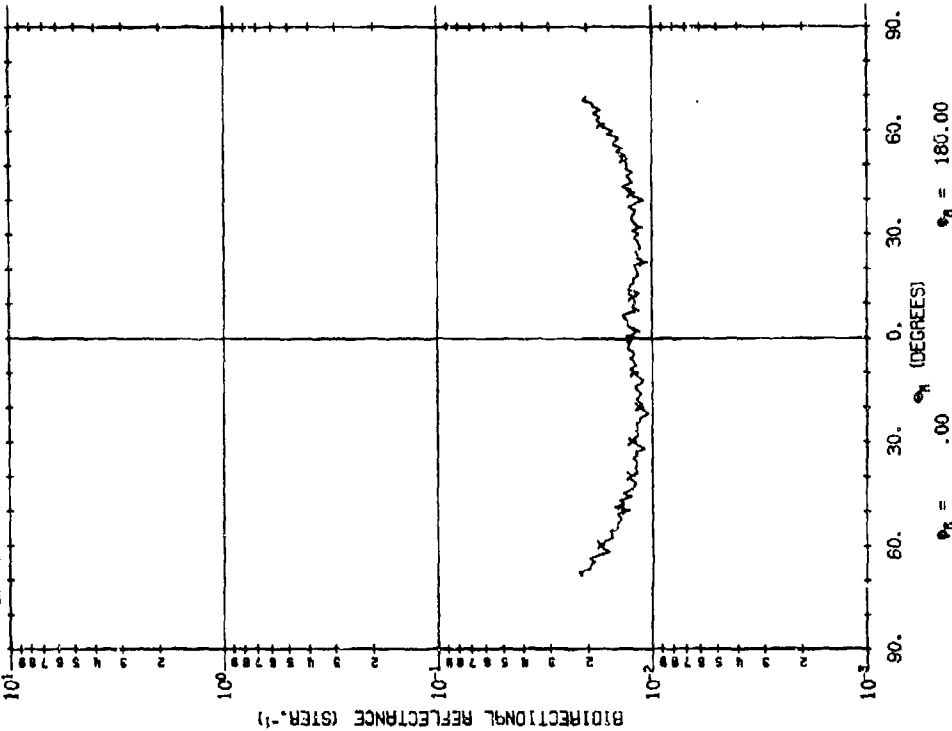


R01891 101

Viny² Coated Olive Drab Canvas

$2\theta = 2.0$

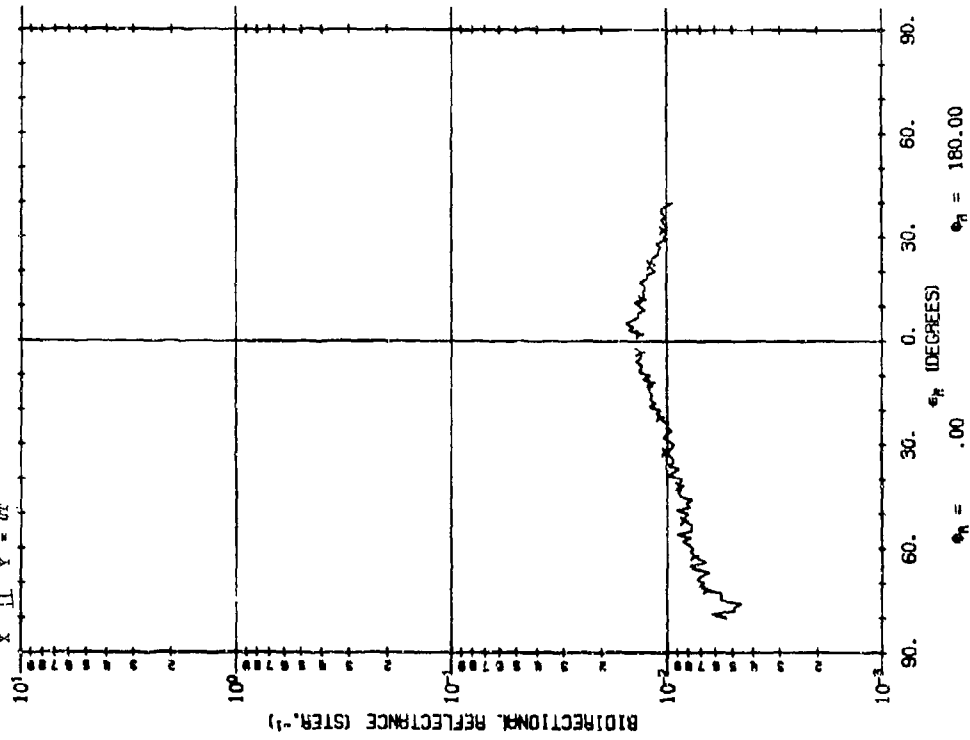
+ || $\phi_1 = \phi_2$
Δ || $\lambda = 10.6$
X || Y = VT



RC1891 101

Vinyl Coated Olive Drab Canvas

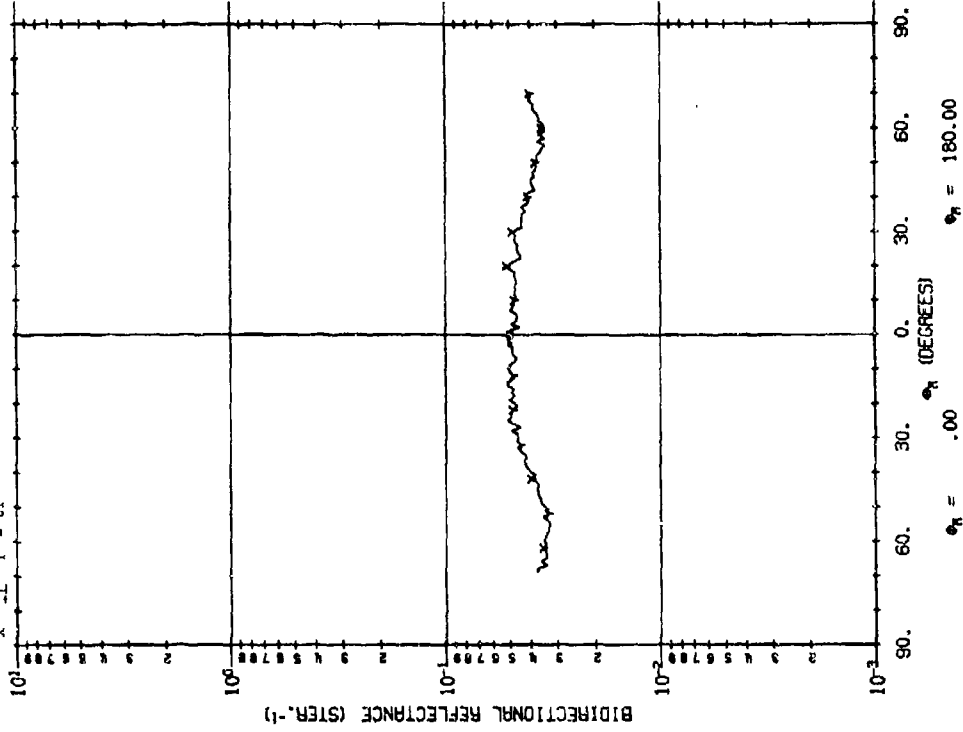
0 // $\epsilon_1 = 0.0$
+ // $\epsilon_2 = 180.0$
△ // $\lambda = 10.6$
X // $Y = UT$



RC1893 101

Olive Drab Canvas

0 // $2\theta = 2.0$
+ // $\phi_1 = \phi_2$
△ // $\lambda = 10.6$
X // $Y = UT$

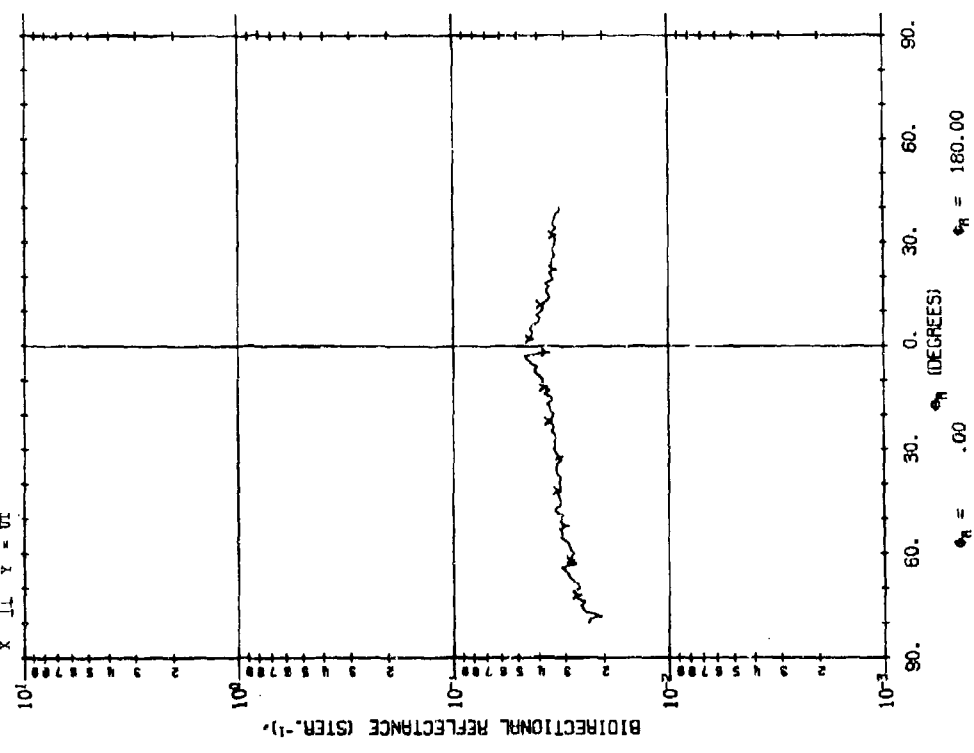


CLOTH AND CANVAS

R01893 101

Olive Drab Paint of Aluminum

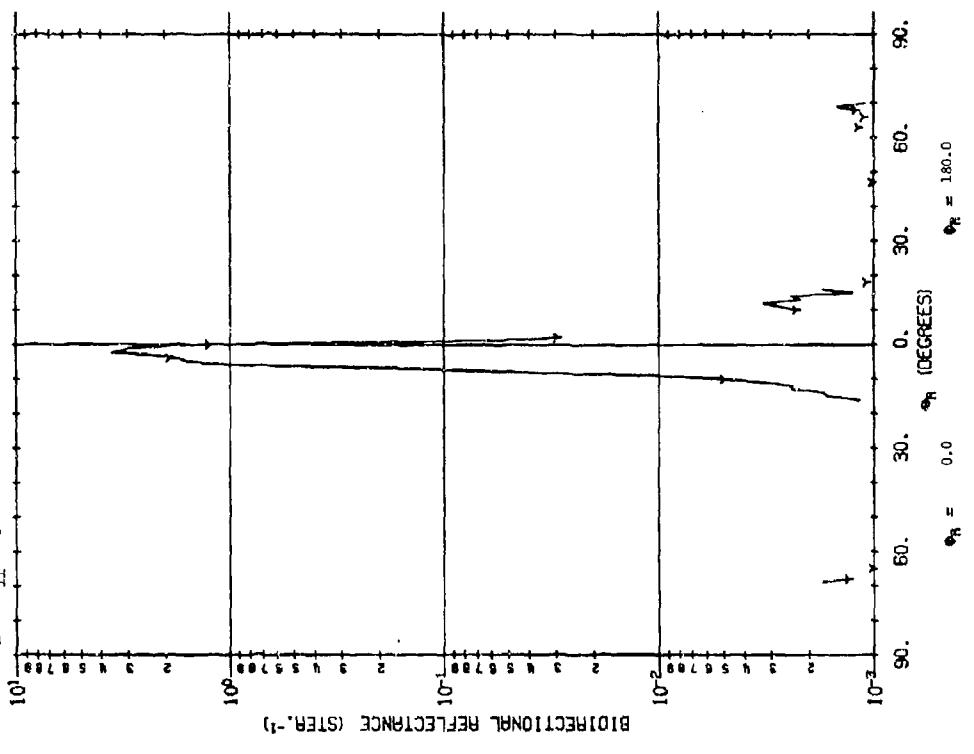
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = VI



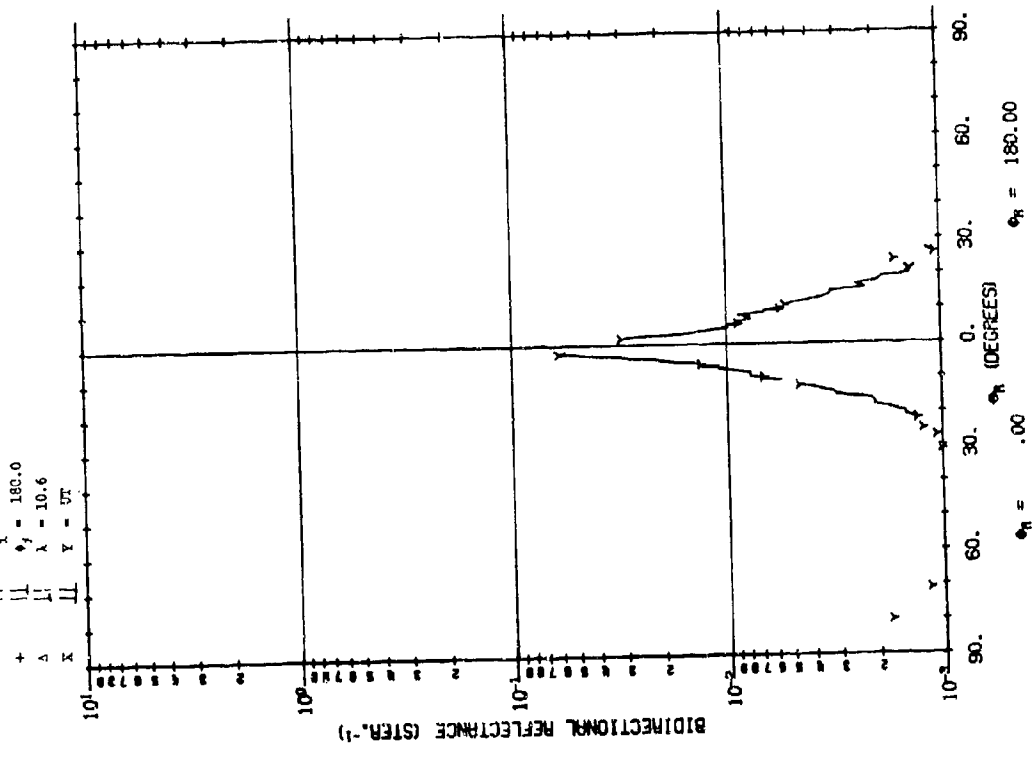
R01900 101

Vinyl Coated Olive Drab Canvas

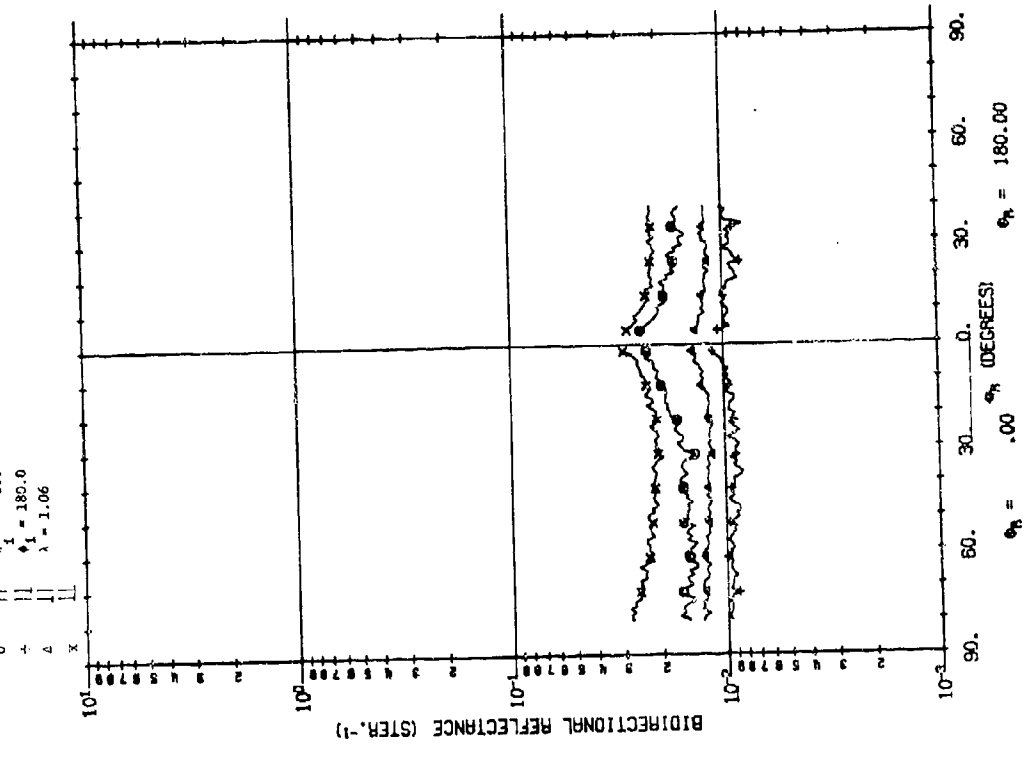
0 || $Z_1 = 2.0$
+ || $\theta_1 = 0.0$
 Δ || $\lambda = 10.6$
X || Y = VI



R01900 101
 Viry. Coated Olive Drab Canvas
 $\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$
 $\gamma = 57$



R01918 101
 Black Canvas
 $\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



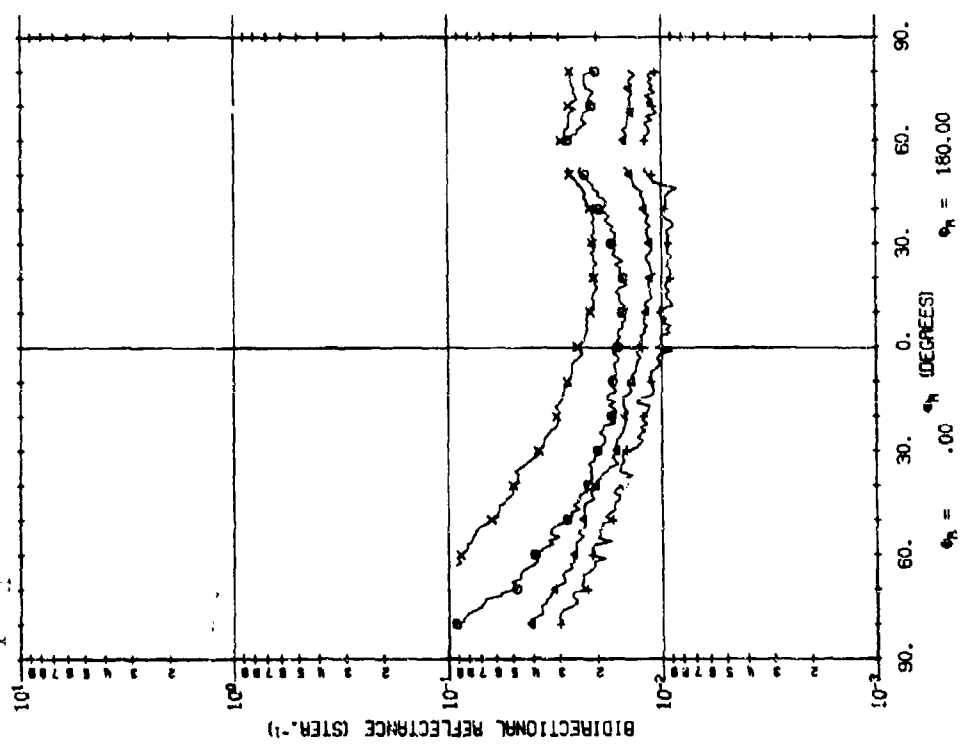
CLOTH AND CANVAS

R01918 101

Black Canvas

$\theta_1 = 56.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

0
+
x

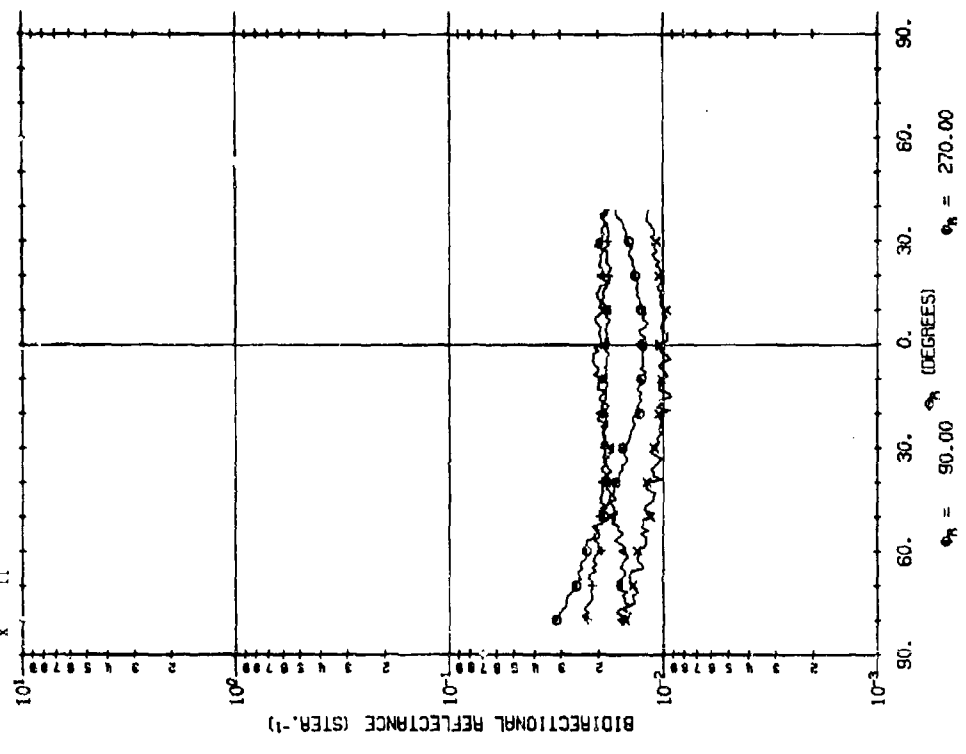


R01918 101

Black Canvas

$\theta_1 = 56.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

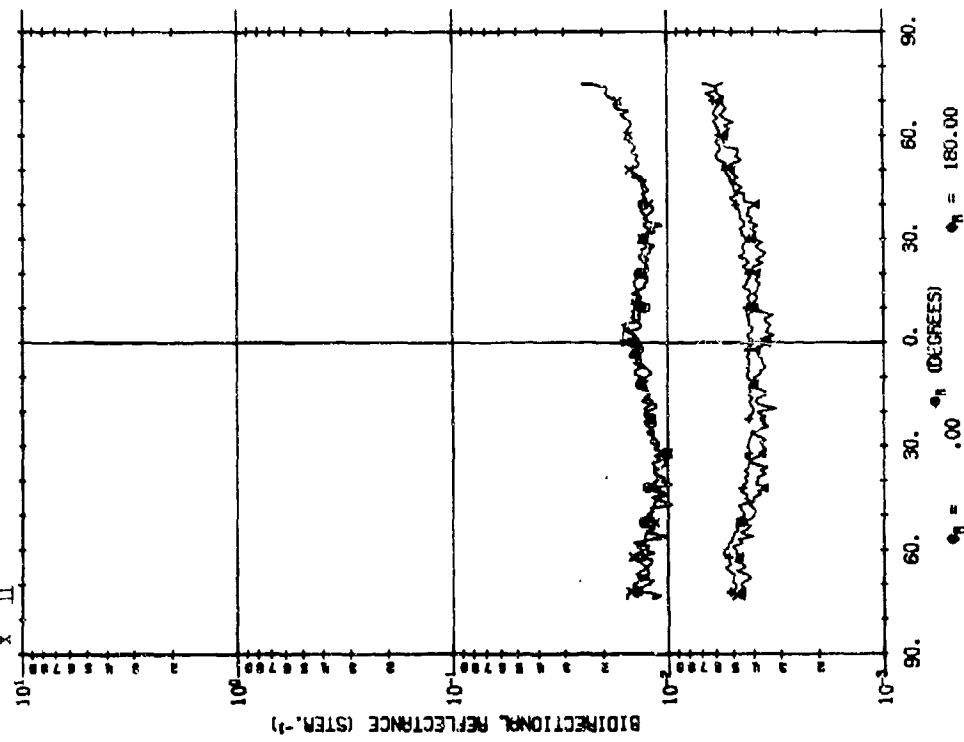
0
+
x



A01919 201

BLACK CANYAS

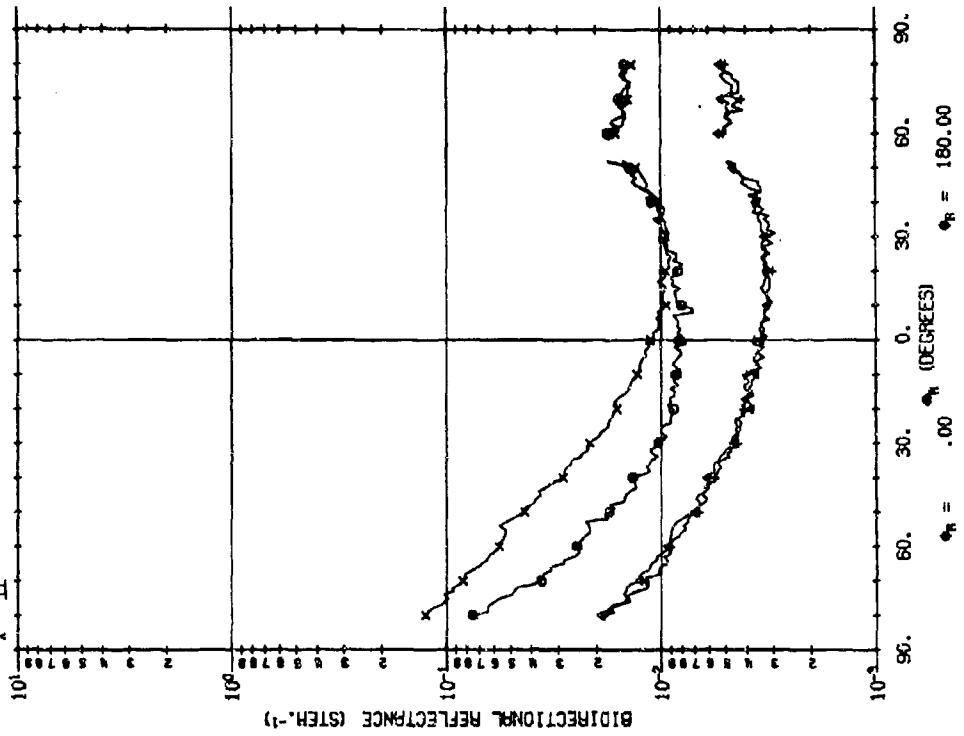
0 || 28 = 2.0
+ || $\phi_1 = \phi_r$
Δ || λ = 1.06
X ||



A01919 201

BLACK CANYAS

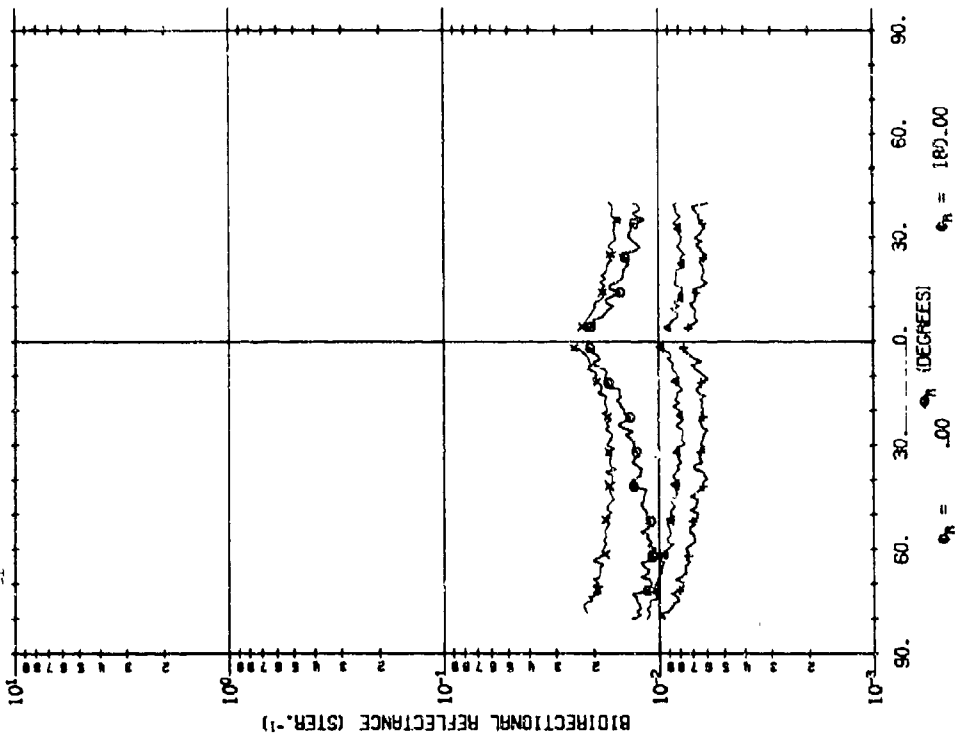
0 || $\phi_1 = 56.0$
+ || $\phi_1 = 180.0$
Δ || λ = 1.06
X ||



CLOTH AND CANYAS

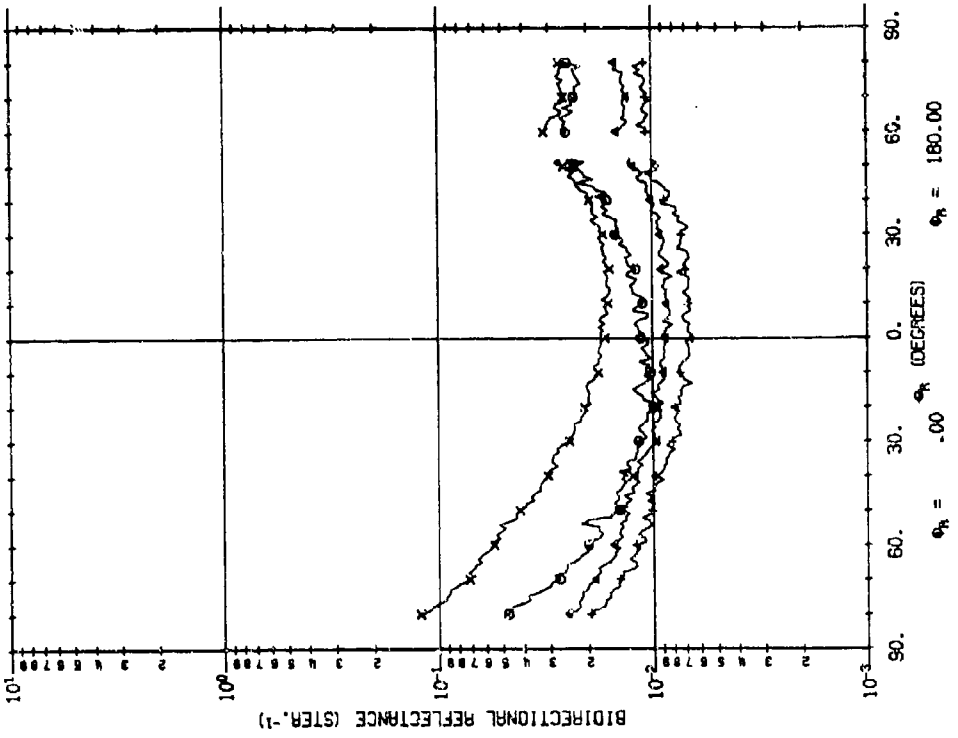
A02002 101
 0 || $\phi_1 = 0.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 1.06$
 X ||

Olive Drab Canvas



A02002 101
 0 || $\phi_1 = 56.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 1.06$
 X ||

Olive Drab Canvas

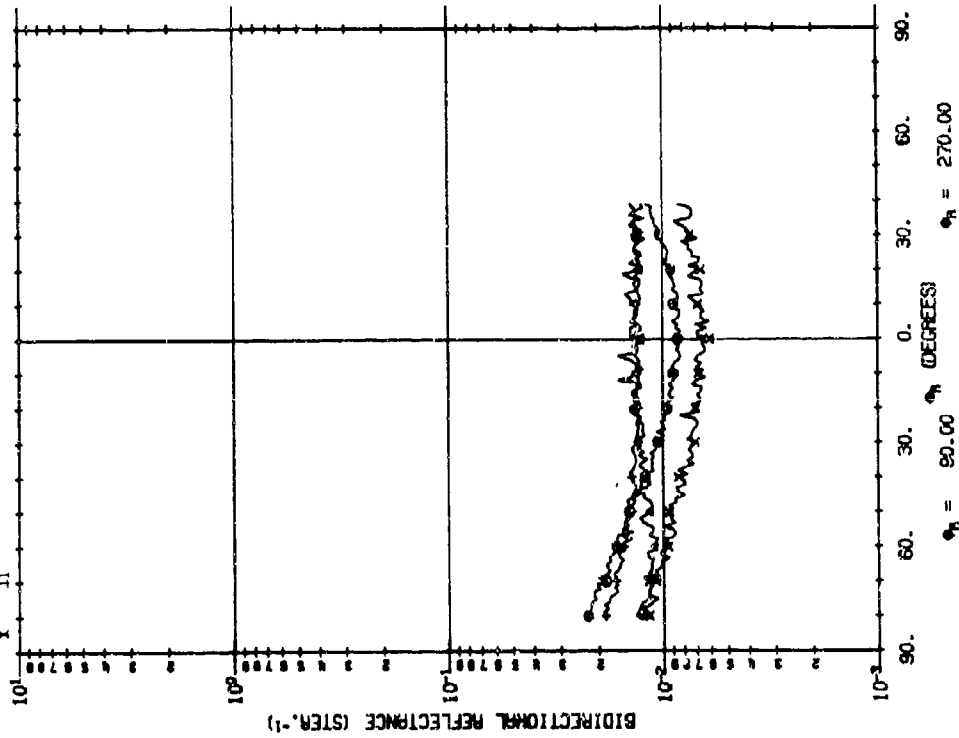


R02002 101

Olive Drab Canvas

0 || ||
+ || ||
Δ || ||
X || ||

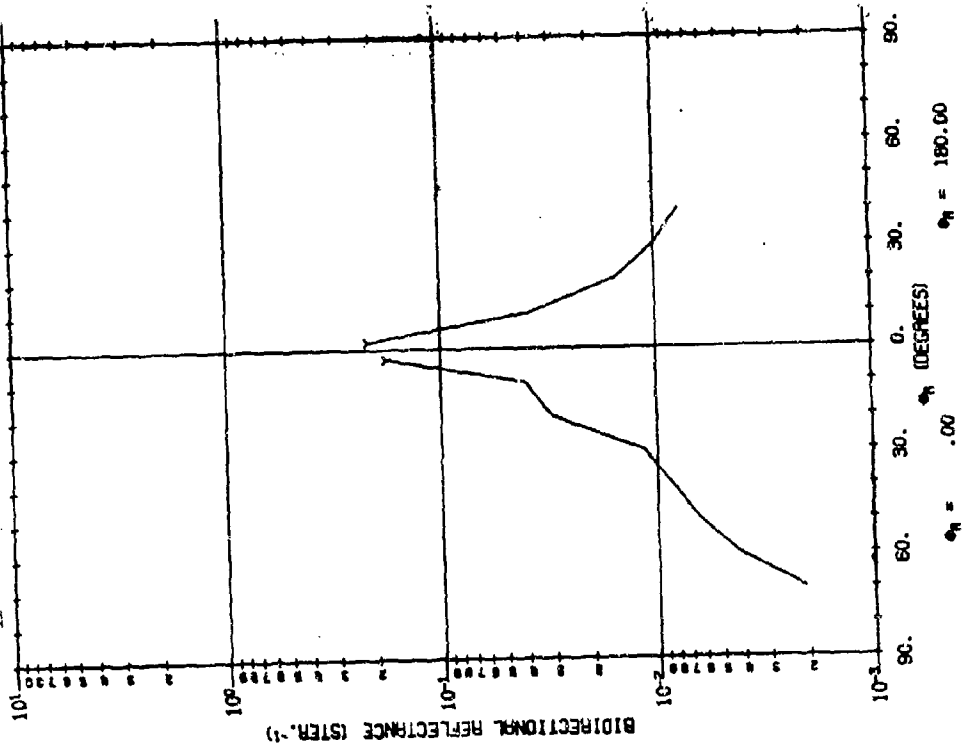
$\theta = 56.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$



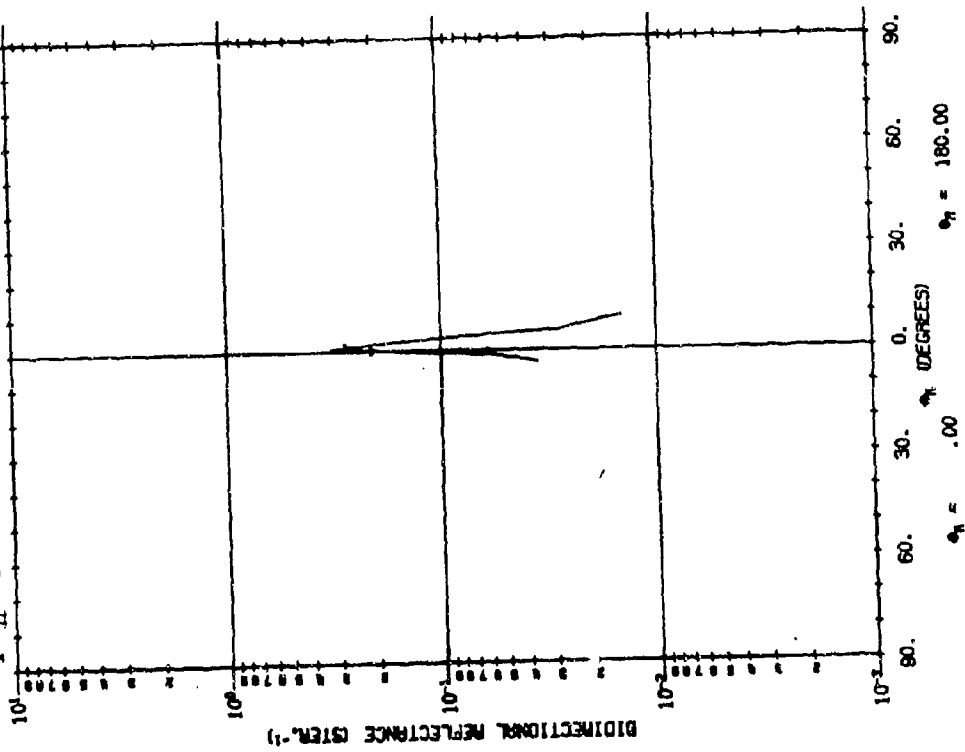
CLOTH AND CANVAS

WOOD

A00096 004 Redwood Block
 0 || $\theta_1 = 0.0$
 + || $\theta_2 = 180.0$
 A || $\lambda = 10.6$
 X || $\gamma = \pi$



A00096 004 Redwood Block
 0 || $2\theta = 1.10$
 + || $\theta_1 = \pi$
 A || $\lambda = 10.6$
 X || $\gamma = \pi$

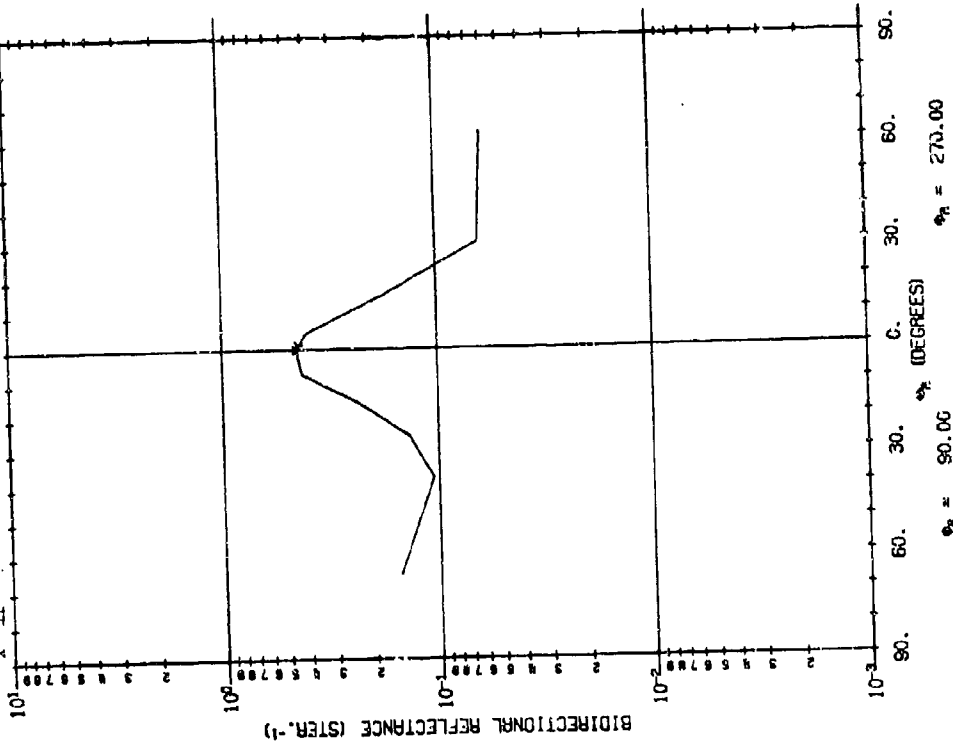


WOOD

A00096 004

Redwood Block

0 || 2 θ = 1.10
+ || $\phi_1 = \phi_2$
 Δ || $\lambda = 10.6$
X || Y = UT

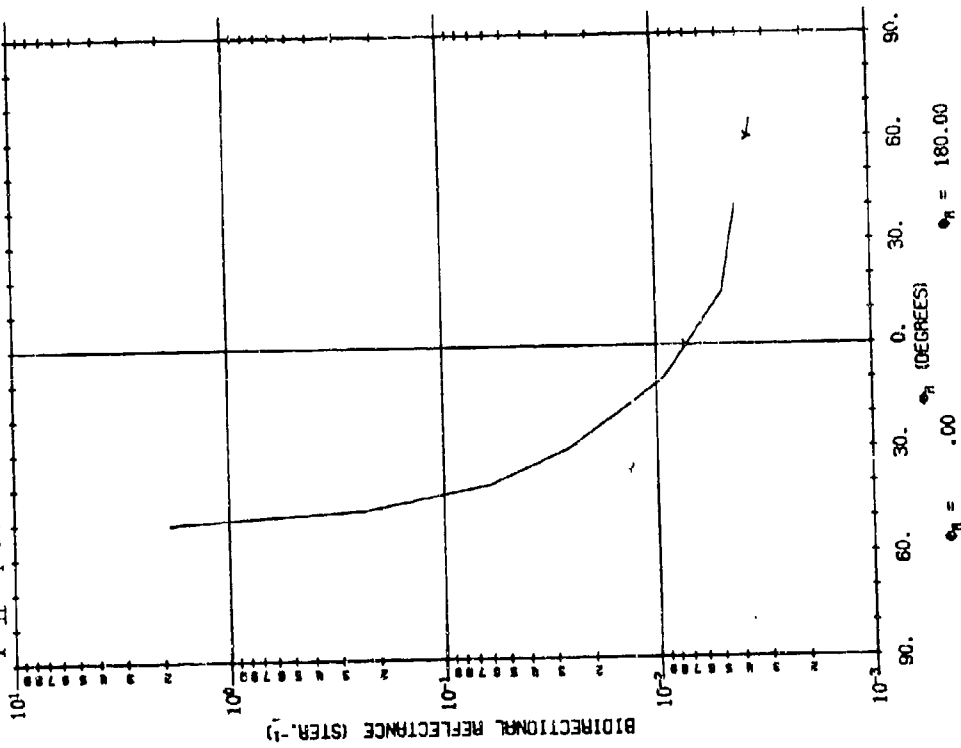


φ_h = 90.00 φ_h = 270.00

A00096 004

Redwood Block

0 || $\theta_1 = 50.0$
+ || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = UT

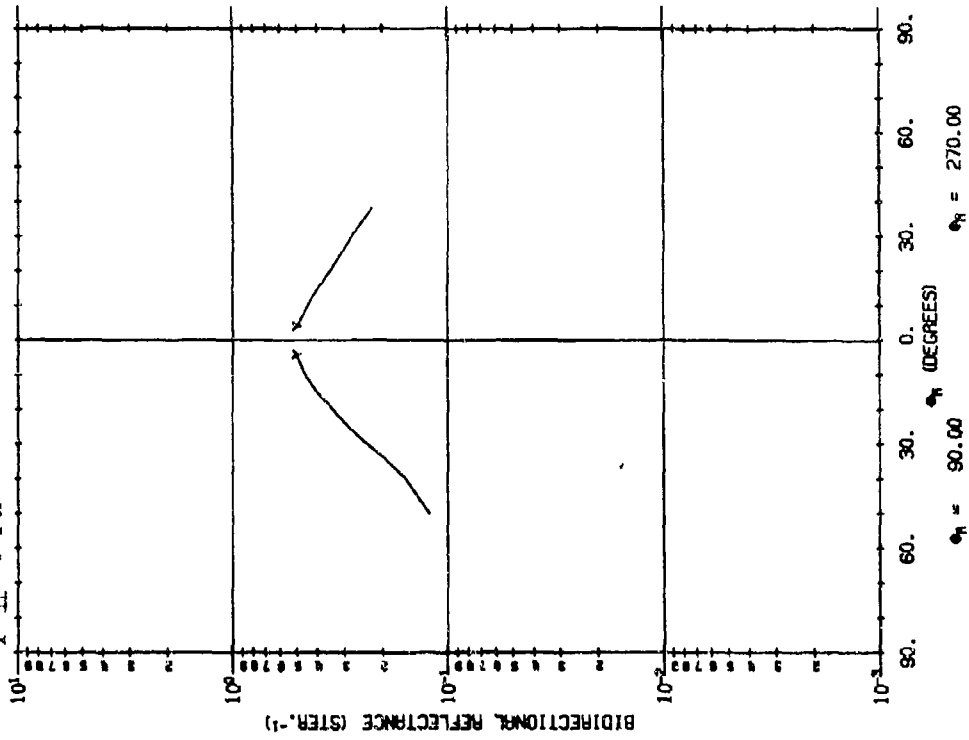


φ_h = .00 φ_h = 180.00

R00096 004

Redwood Block

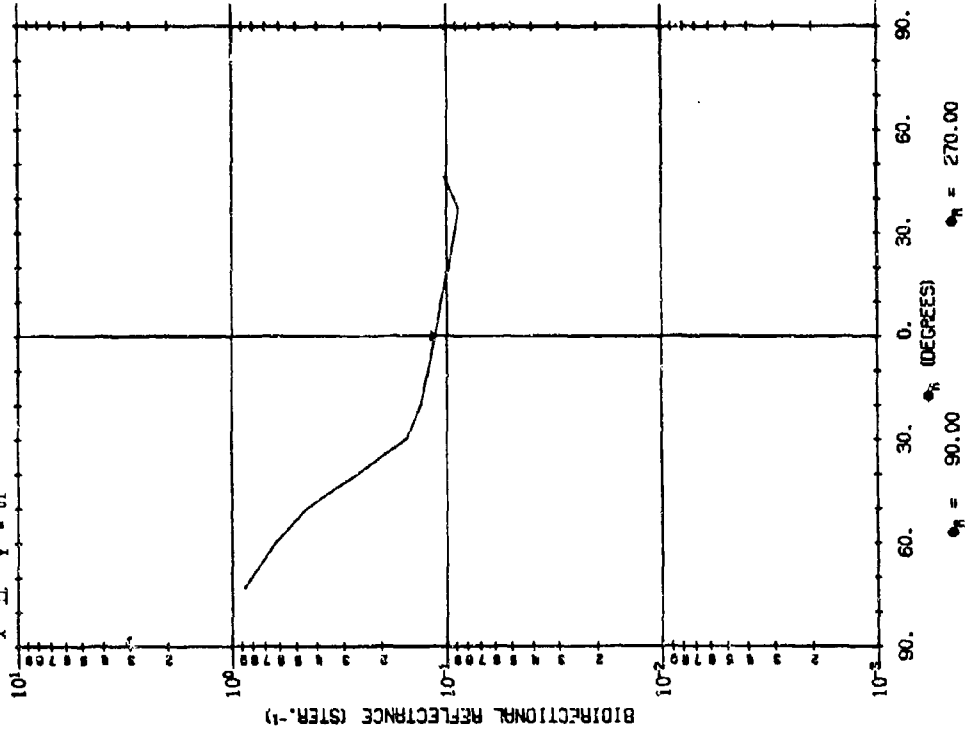
0 || $\phi_i = 0.0$
+ || $\phi_i = 270.0$
Δ || $\lambda = 10.6$
x || $\gamma = 01$



R00096 004

Redwood Block

0 || $\phi_i = 50.0$
+ || $\phi_i = 270.0$
Δ || $\lambda = 10.6$
x || $\gamma = 01$

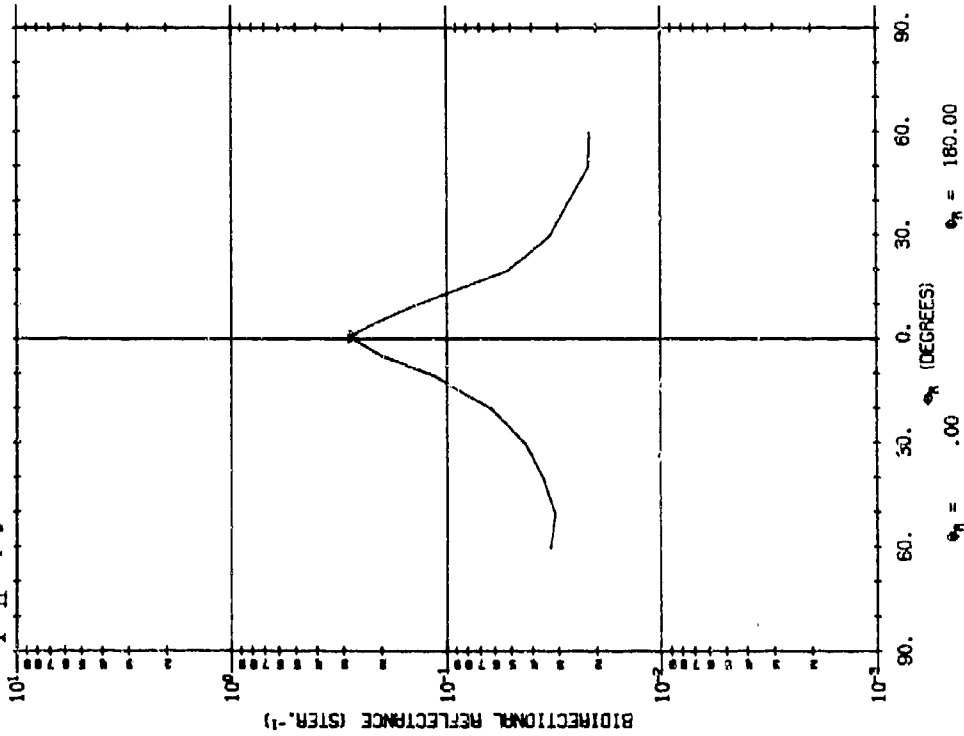


WOOD

R00106 002

White Oak Block

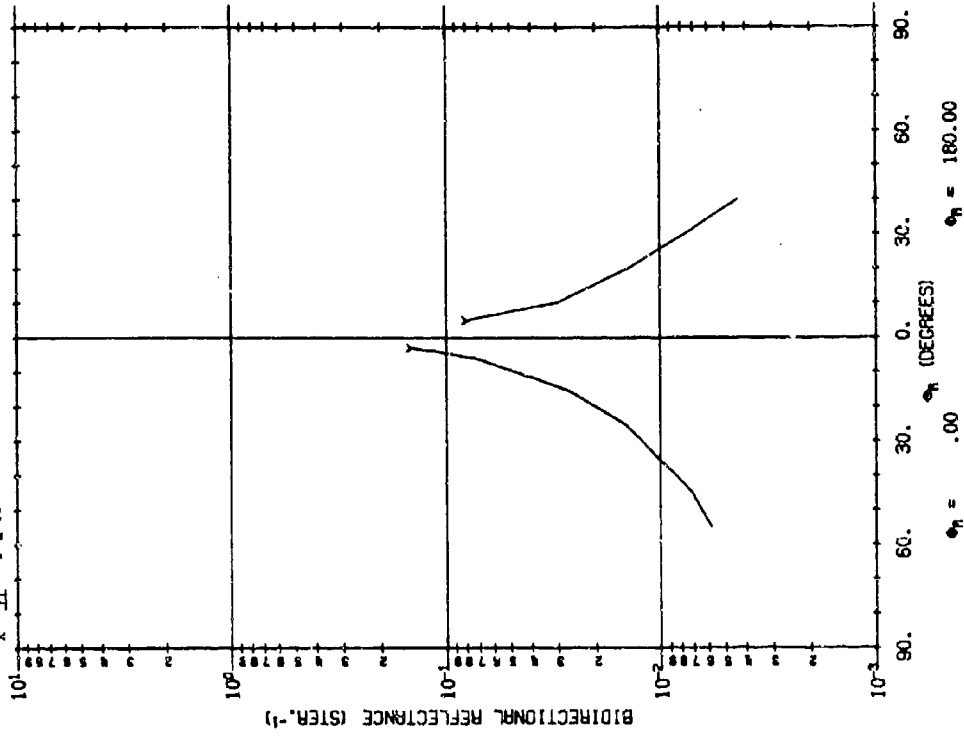
0 || $z_1 = 1.10$
+ || $\phi_1 = \phi_r$
Δ || $\lambda = 10.6$
X || $Y = \sqrt{t}$



R00106 002

White Oak Block

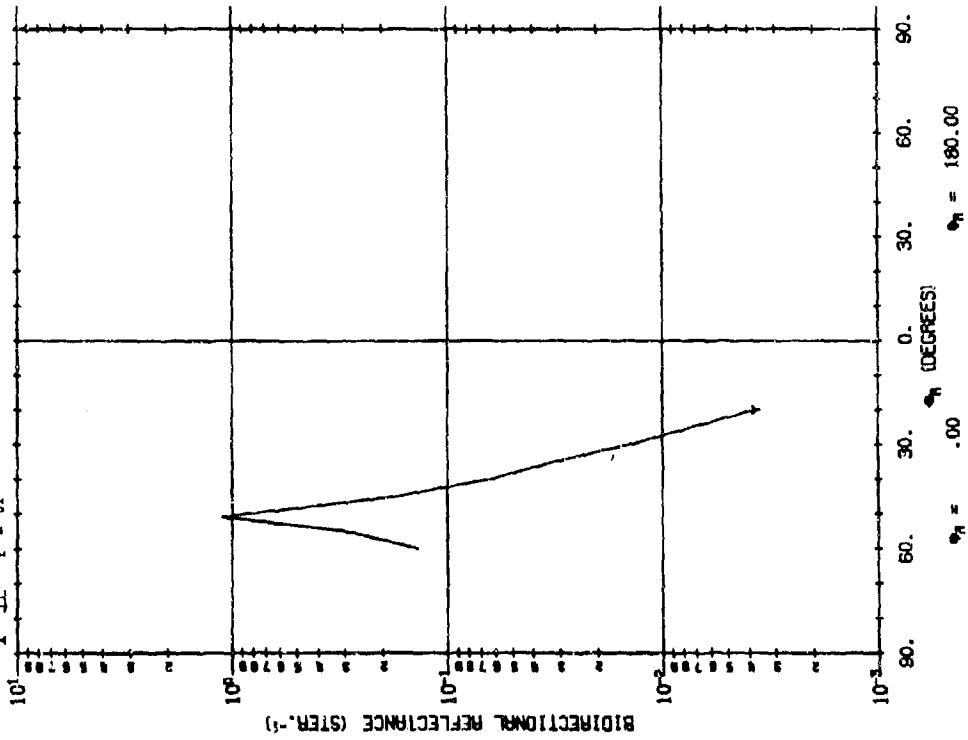
0 || $z_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || $Y = \sqrt{t}$



A00106 002

White Oak Block

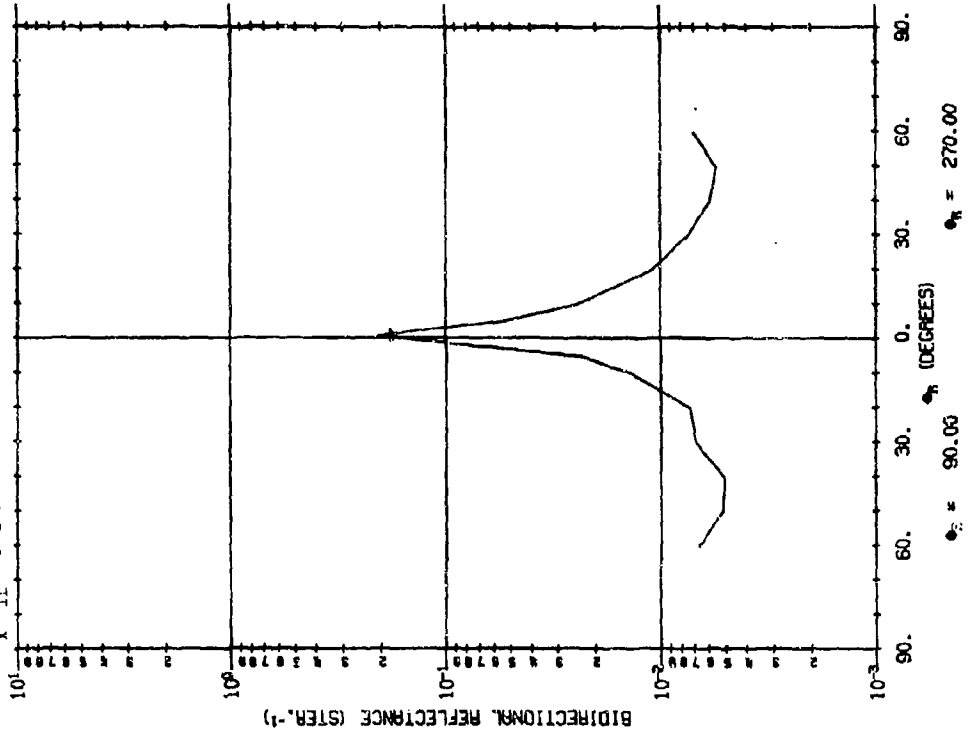
0 || $\theta_1 = 50.0$
+ || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = UT



A00106 002

White Oak Block

0 || $\theta_1 = 1.10$
+ || $\phi_1 = 0$
 Δ || $\lambda = 10.6$
X || Y = UT

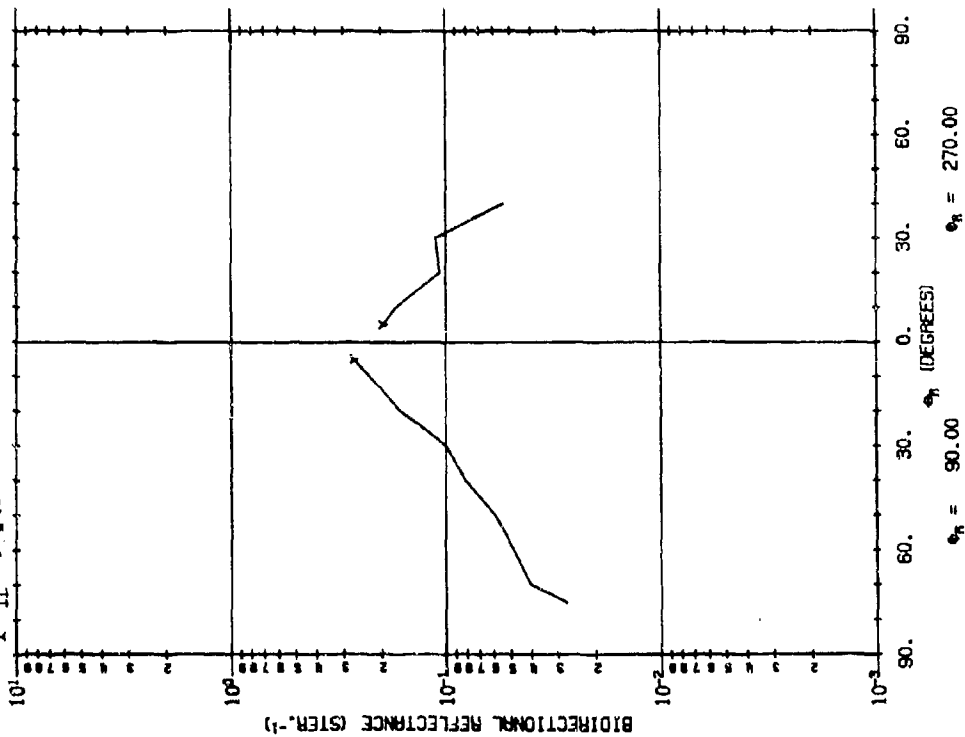


WOOD

A00106 002

White Oak Block

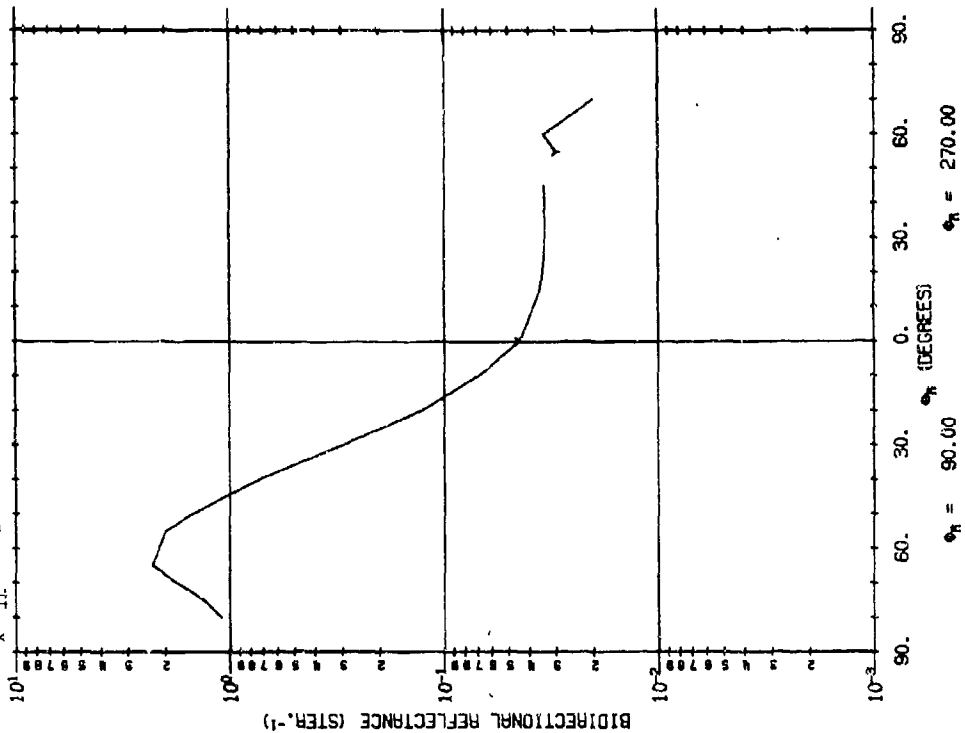
0 | | $\theta_1 = 0.0$
+ | | $\phi_1 = 270.0$
Δ | | $\lambda = 10.6$
X | | $Y = UT$



A00106 002

White Oak Block

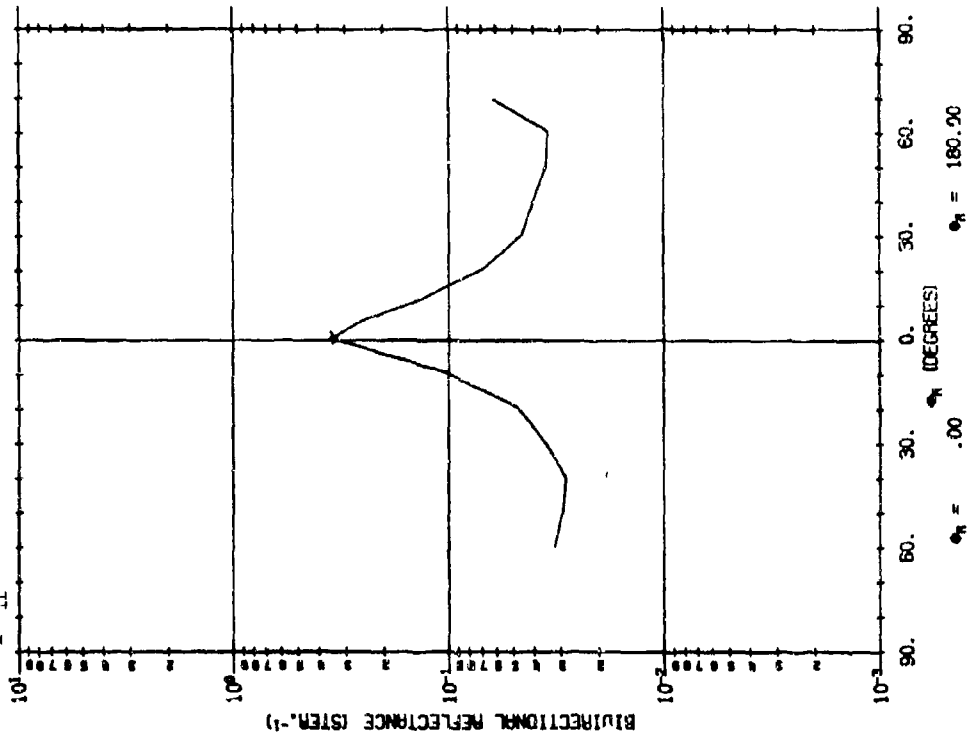
0 | | $\theta_1 = 50.0$
+ | | $\phi_1 = 270.0$
Δ | | $\lambda = 10.6$
X | | $Y = UT$



A00118 002

Red Oak Block

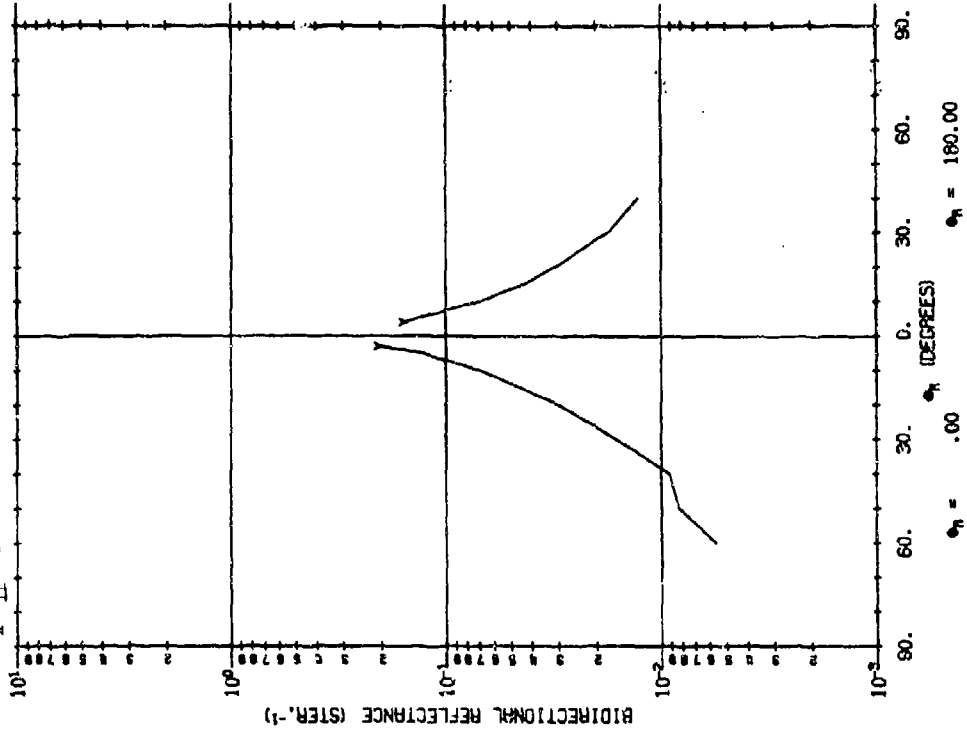
0 || 2B = 1.10
+ || $\psi_i = \psi_r$
A || $\lambda = 10.6$
X || Y = UT



A00118 002

Red Oak Block

0 || $\psi_i = 0.0$
+ || $\psi_r = 180.0$
A || $\lambda = 10.6$
X || Y = UT

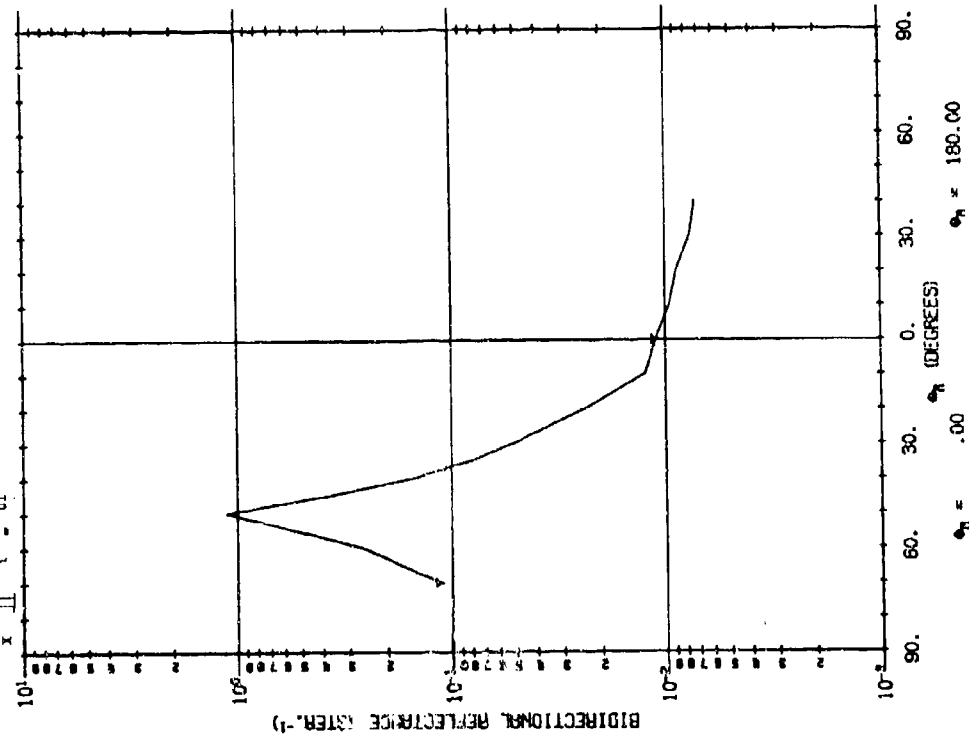


WOOD

R00118 002

Ref Oak Block

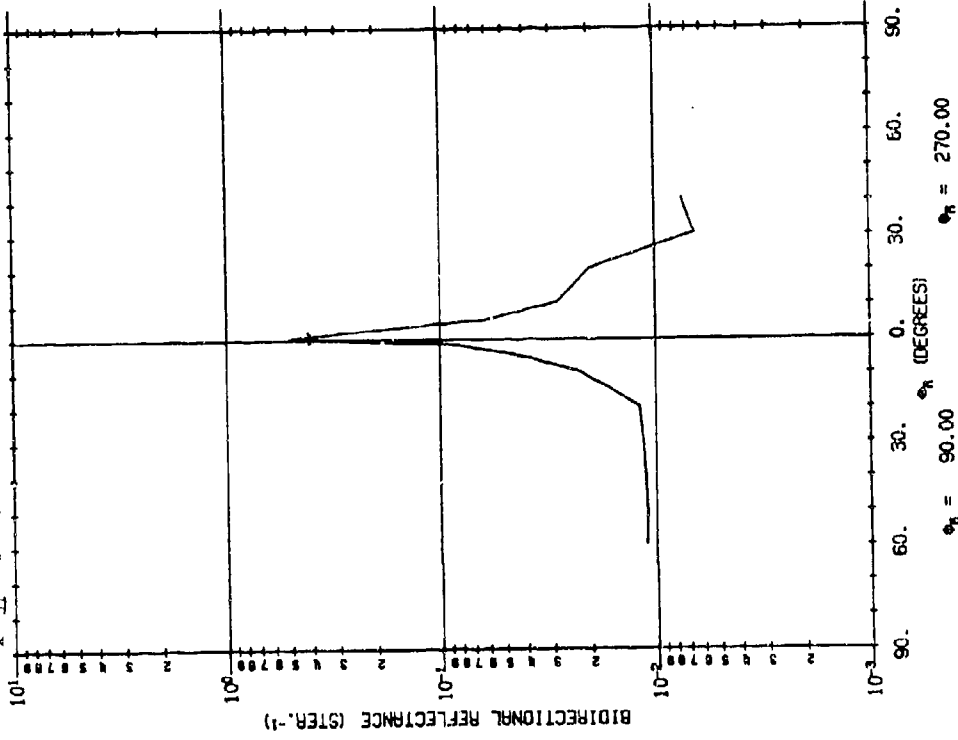
0 || $\theta_1 = 50.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || Y = UT



R00118 002

Ref Oak Block

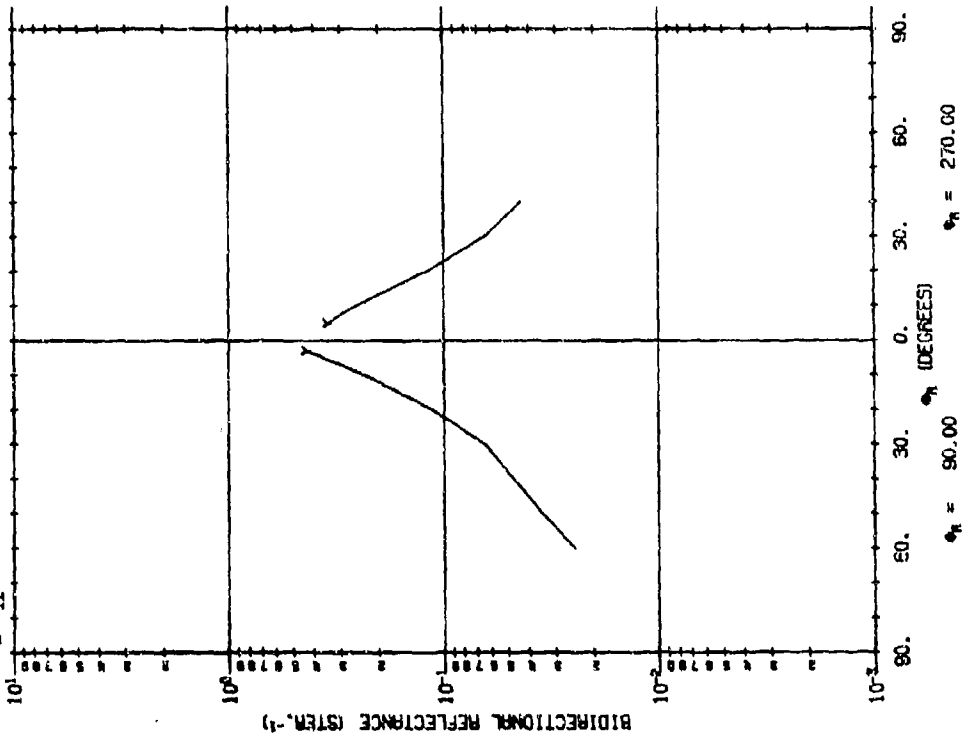
0 || $\theta_1 = 1.10$
+ || $\phi_1 = \phi_2$
Δ || $\lambda = 10.6$
X || Y = UT



A00118 002

Red Oak Block

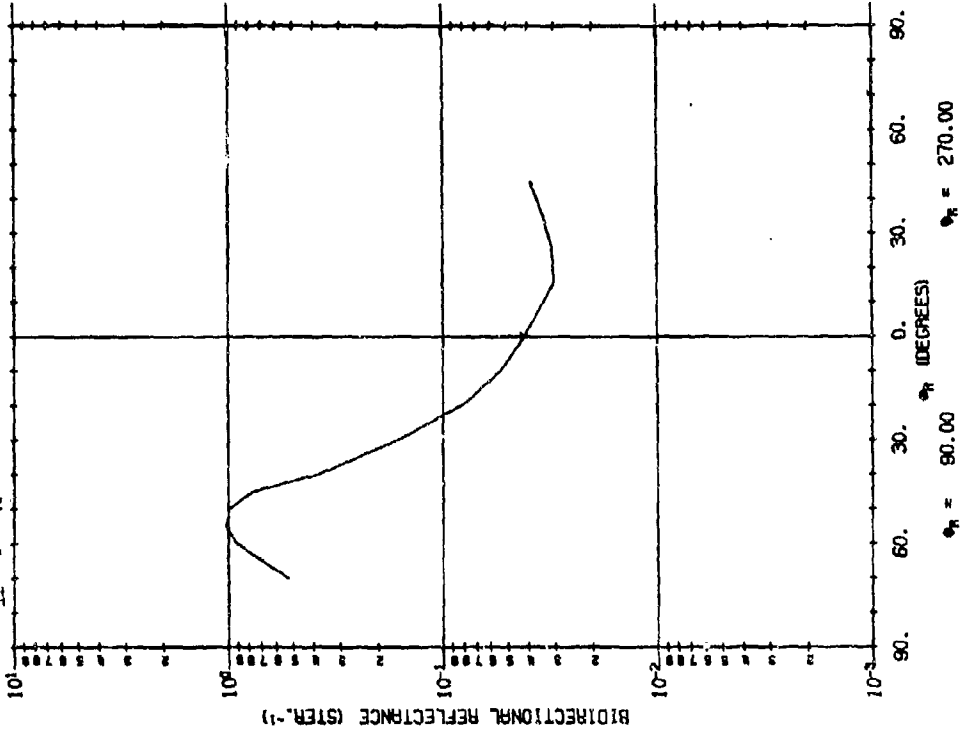
$\theta_1 = 0.0$
 $\phi_1 = 270.0$
 $\lambda = 10.6$
 $\chi = \text{UT}$



A00118 002

Red Oak Block

$\theta_1 = 50.0$
 $\phi_1 = 270.0$
 $\lambda = 10.6$
 $\chi = \text{UT}$

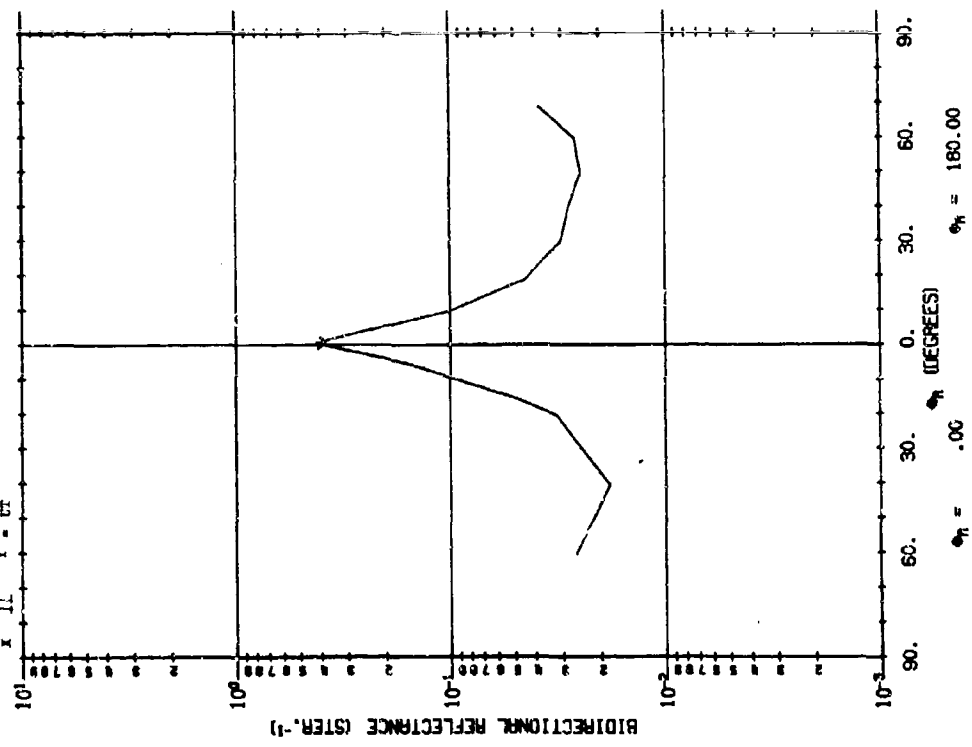


WOOD

R00137 002

California White Oak Block

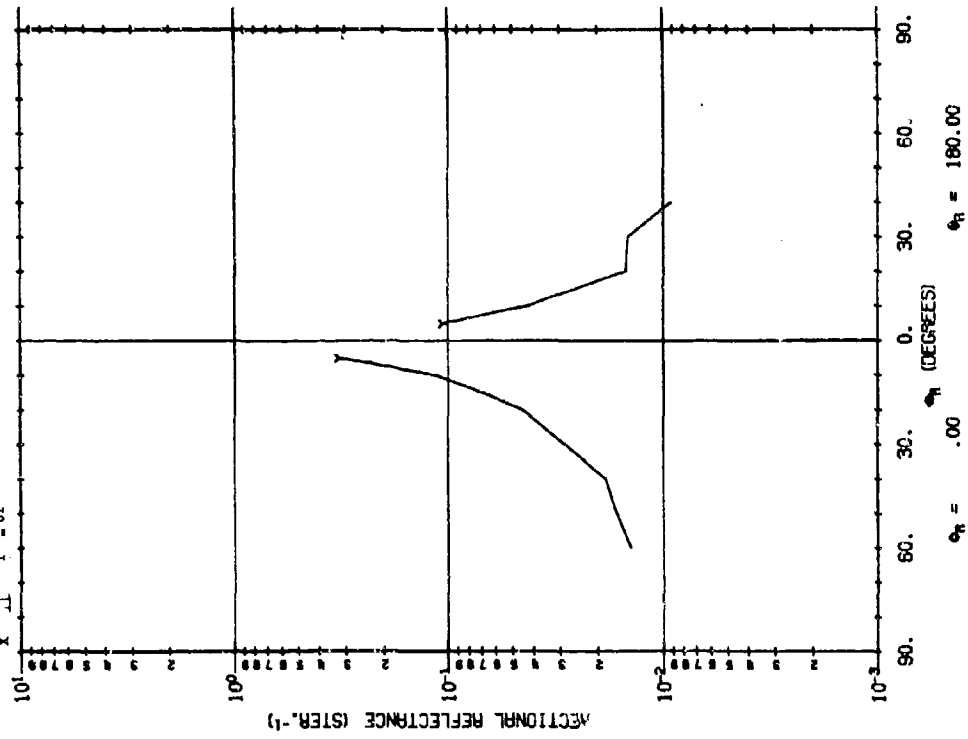
0 || $2\theta = 1.10$
+ || $\theta_1 = \theta_2$
 Δ || $\lambda = 10.6$
X || Y = UT



R00137 002

California White Oak Block

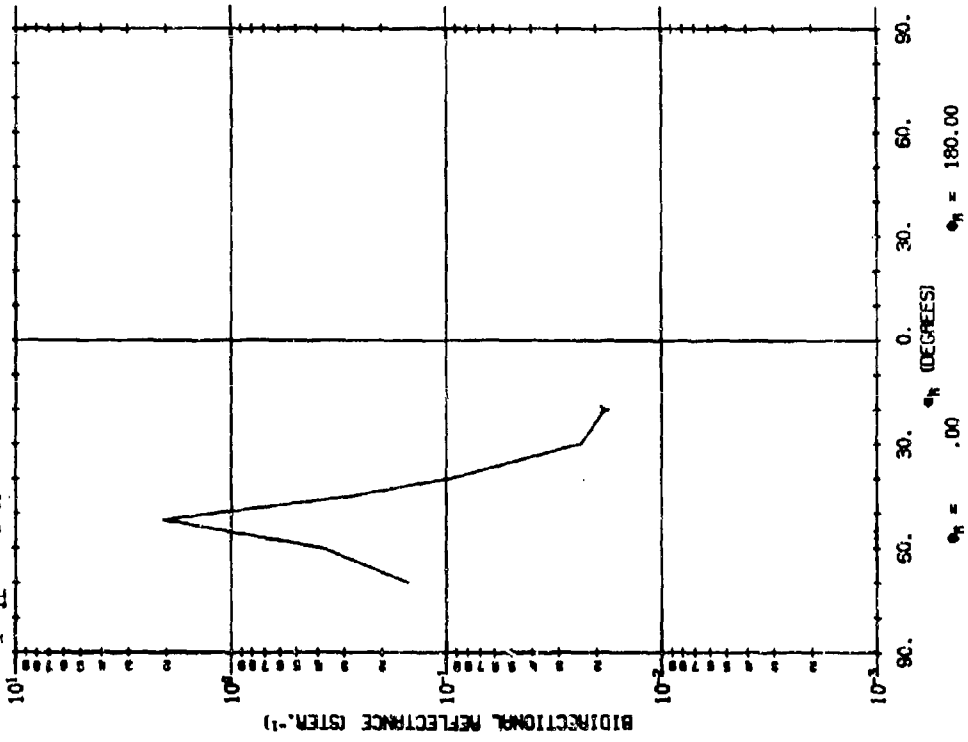
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = UT



R00137 002

California White Oak Block

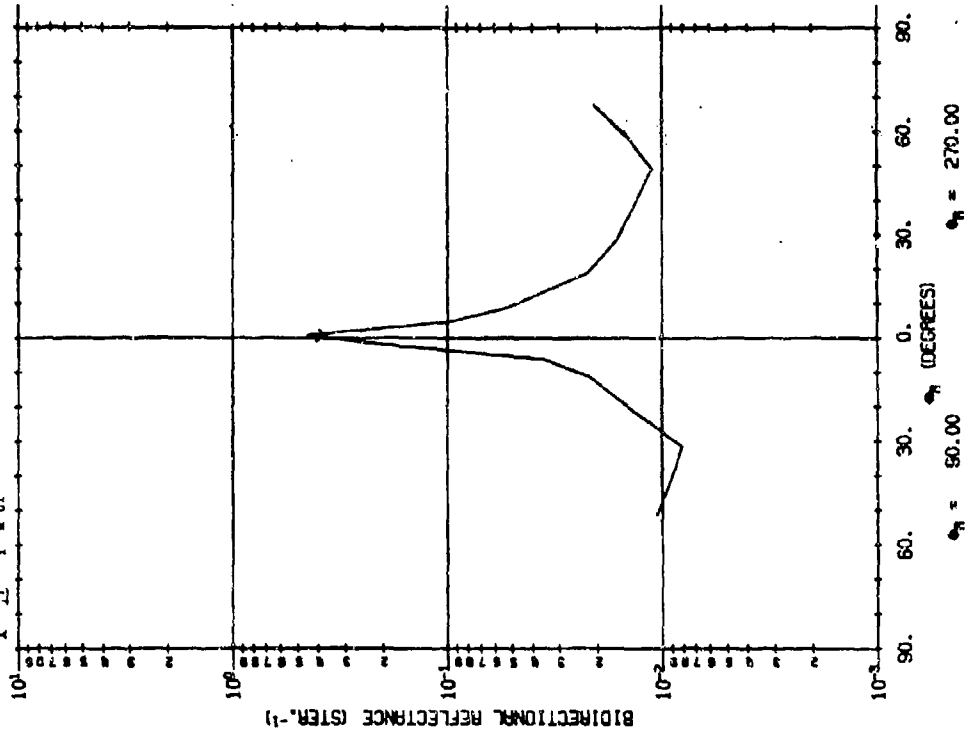
0 || $\phi_1 = 50.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 10.6$
X || Y = UT



R00137 002

California White Oak Block

0 || $\phi_1 = 1.10$
+ || $\phi_2 = \phi_1$
Δ || $\lambda = 10.6$
X || Y = UT

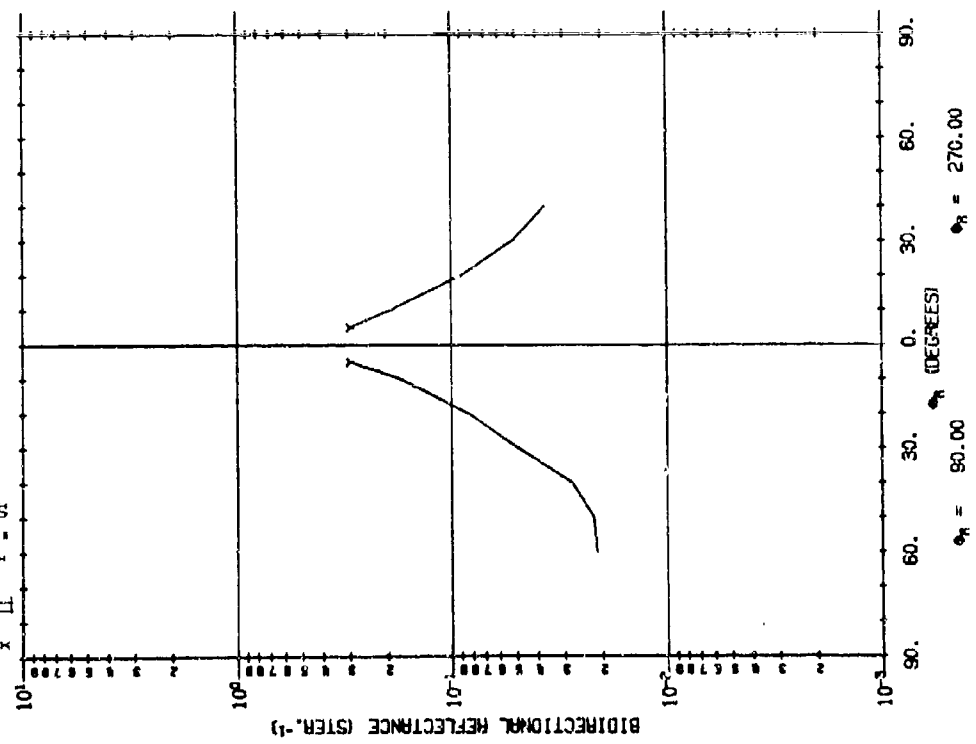


WOOD

A00137 002

California White Oak Block

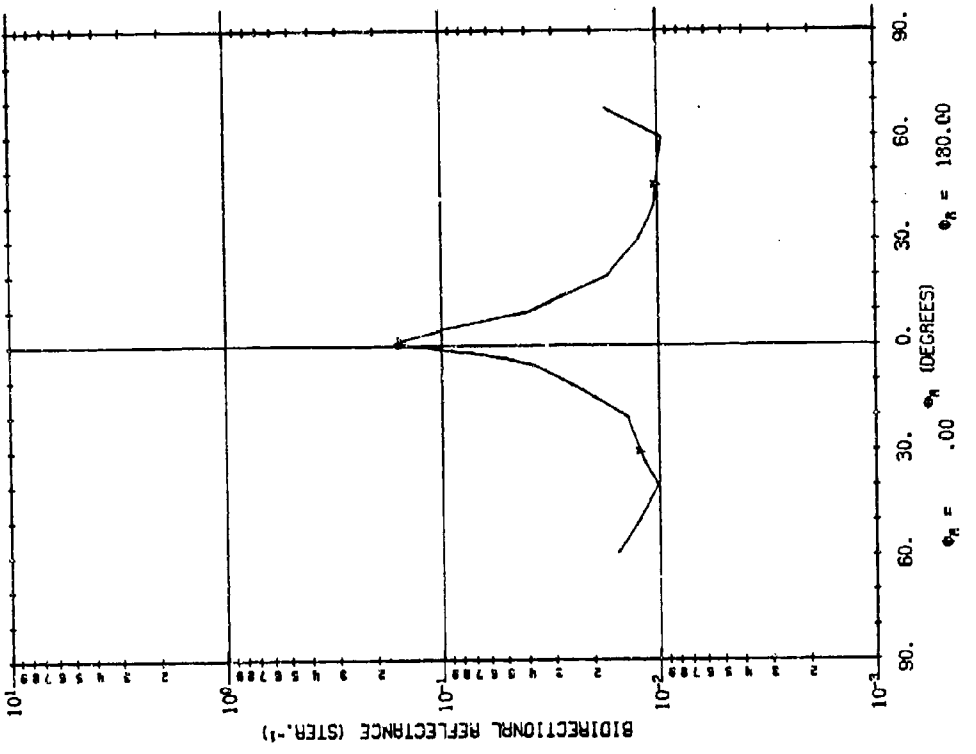
0 || $\theta_1 = 0.0$
 + || $\theta_1 = 270.0$
 Δ || $\lambda = 10.6$
 X || Y = VT



A00153 002

White Pine Block

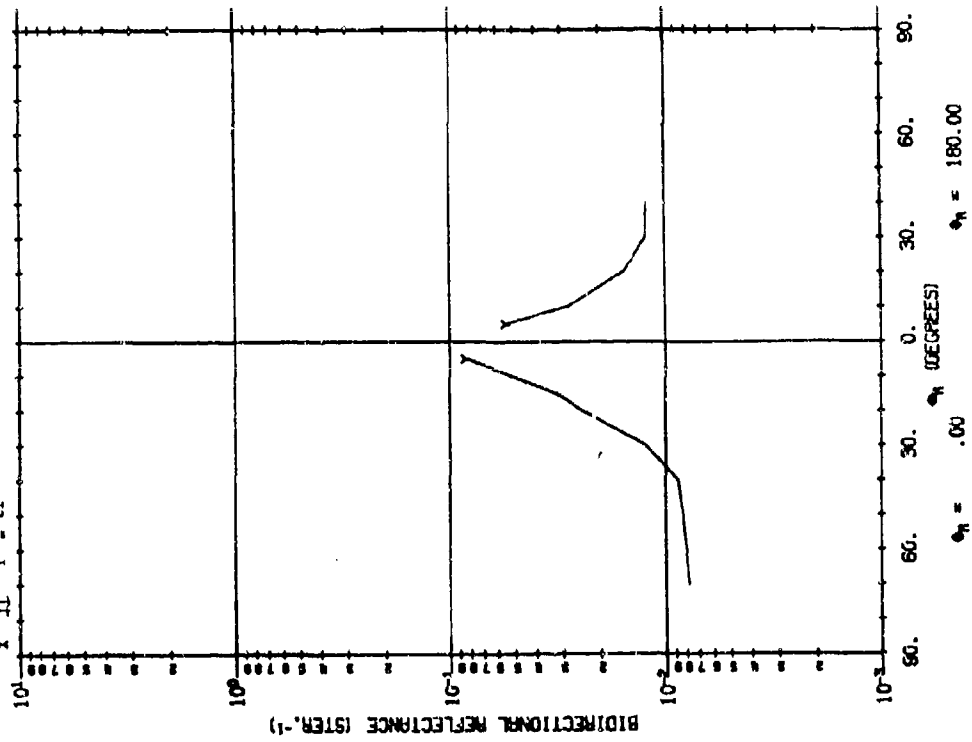
0 || $\theta_1 = 1.10$
 + || $\theta_1 = 90$
 Δ || $\lambda = 10.6$
 X || Y = VT



A00153 002

White Pine Block

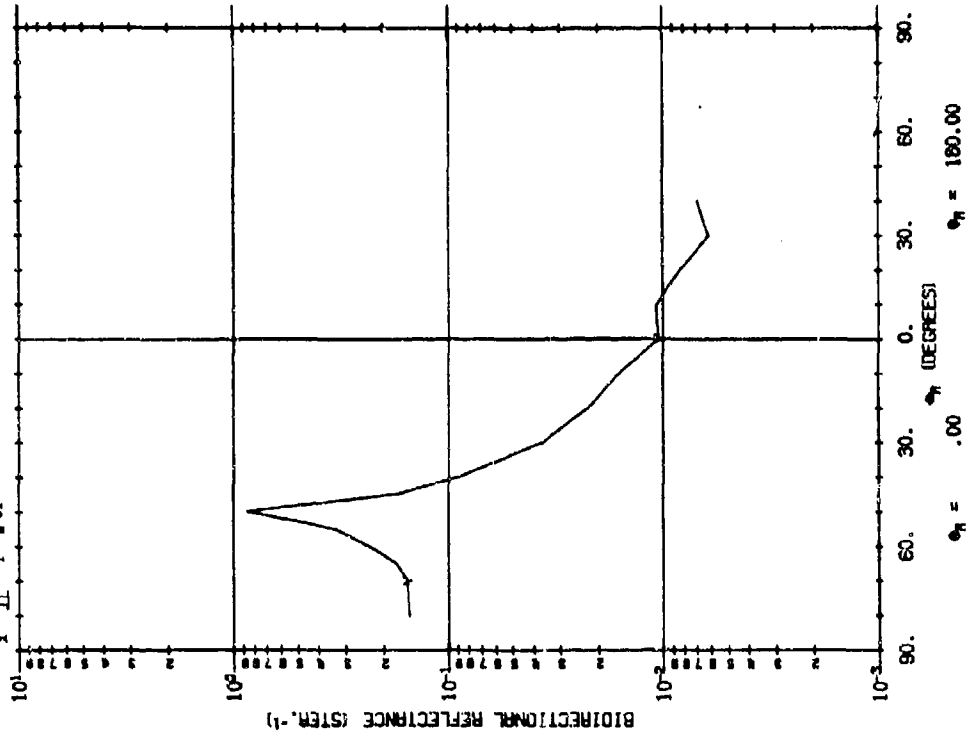
0 || $\phi_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || Y = UT



A00153 002

White Pine Block

0 || $\phi_1 = 50.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || Y = UT

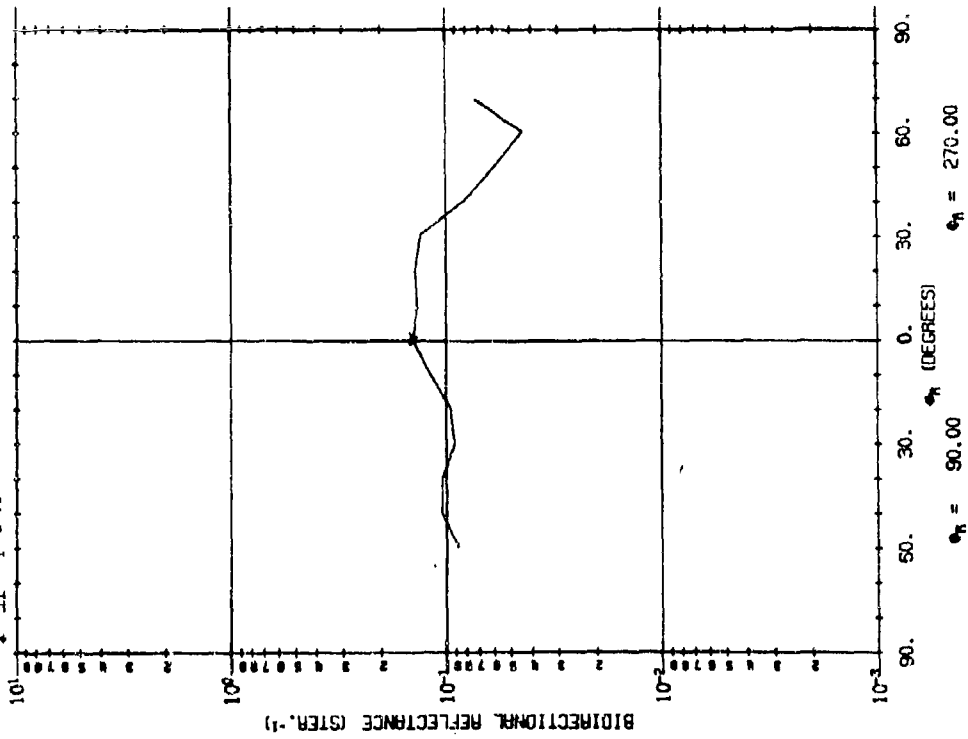


WOOD

R00153 002

White Pine Block

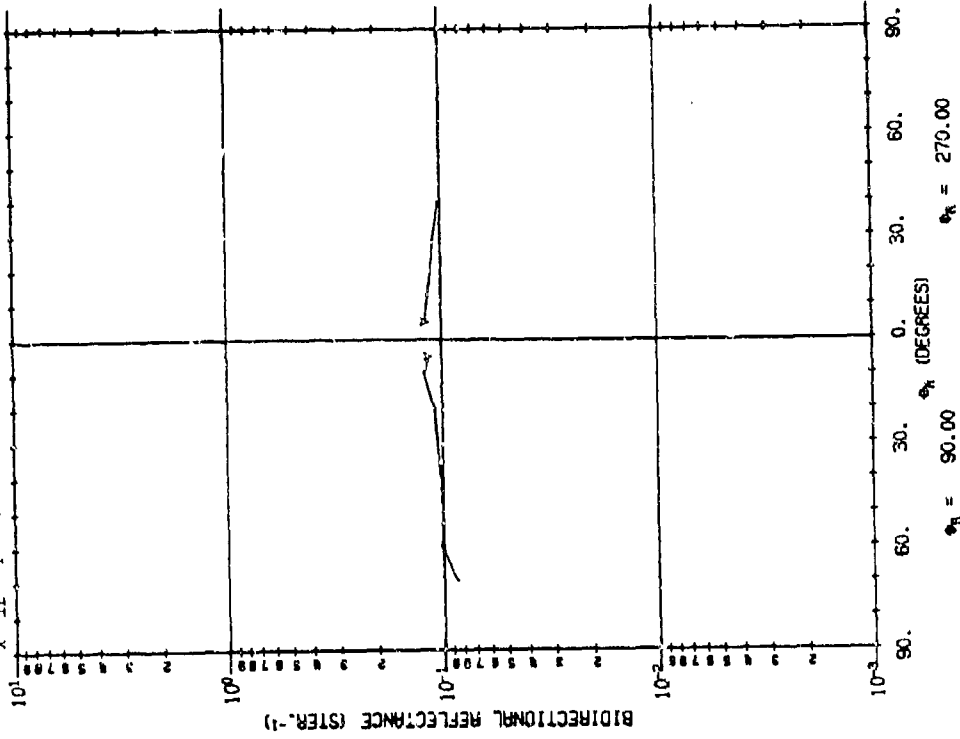
0 // 2a = 1.10
+ // $\epsilon_1 = 1$
Δ // $\lambda = 10.6$
X // Y = UT



R00153 002

White Pine Block

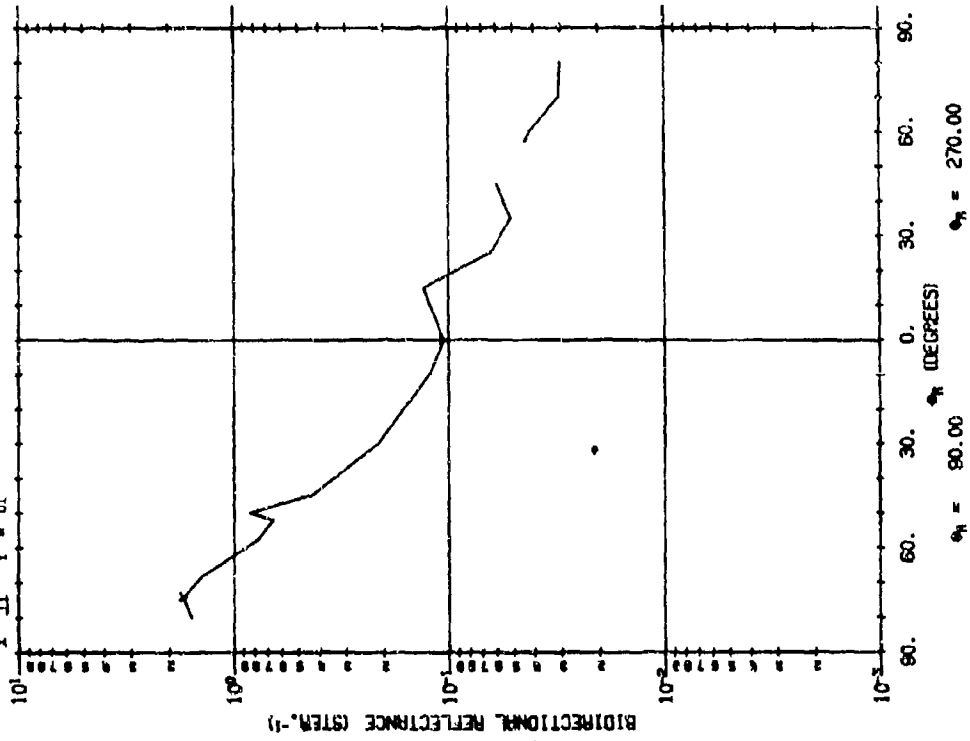
0 // $\epsilon_1 = 0.0$
+ // $\epsilon_1 = 270.0$
Δ // $\lambda = 10.6$
X // Y = UT



A00153 .002

White Pine Block

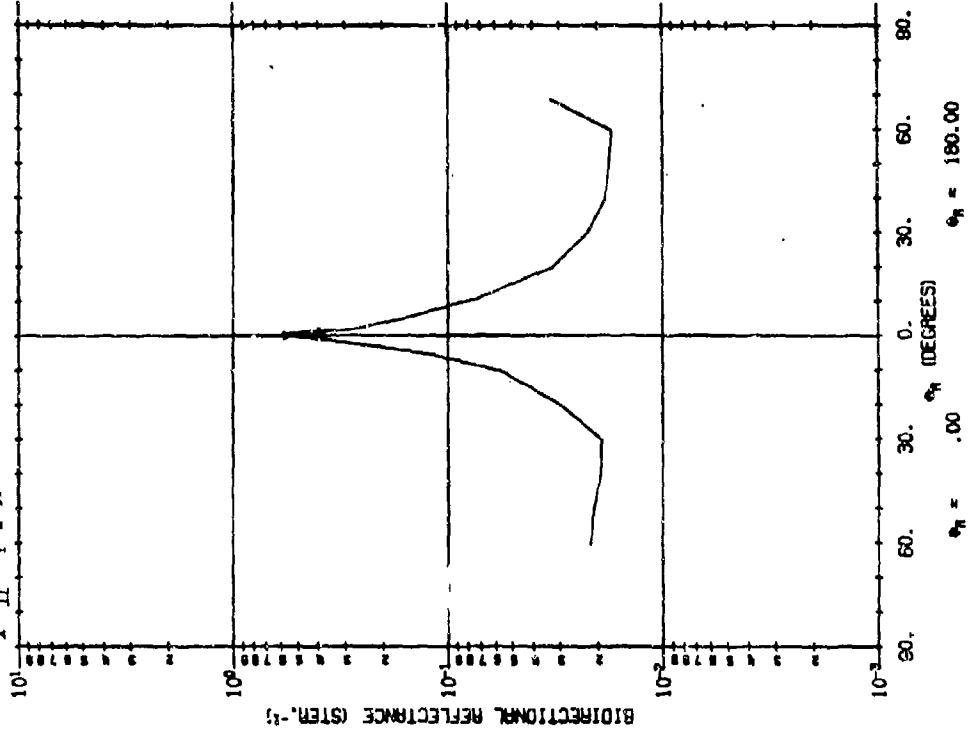
C || $\theta_i = 50.0$
+ || $\theta_r = 270.0$
A || $\lambda = 10.6$
X || Y = FT



A00167 .002

Oregon White Oak Block

C || $\theta_i = 1.10$
+ || $\theta_r = 0$
A || $\lambda = 10.6$
X || Y = FT

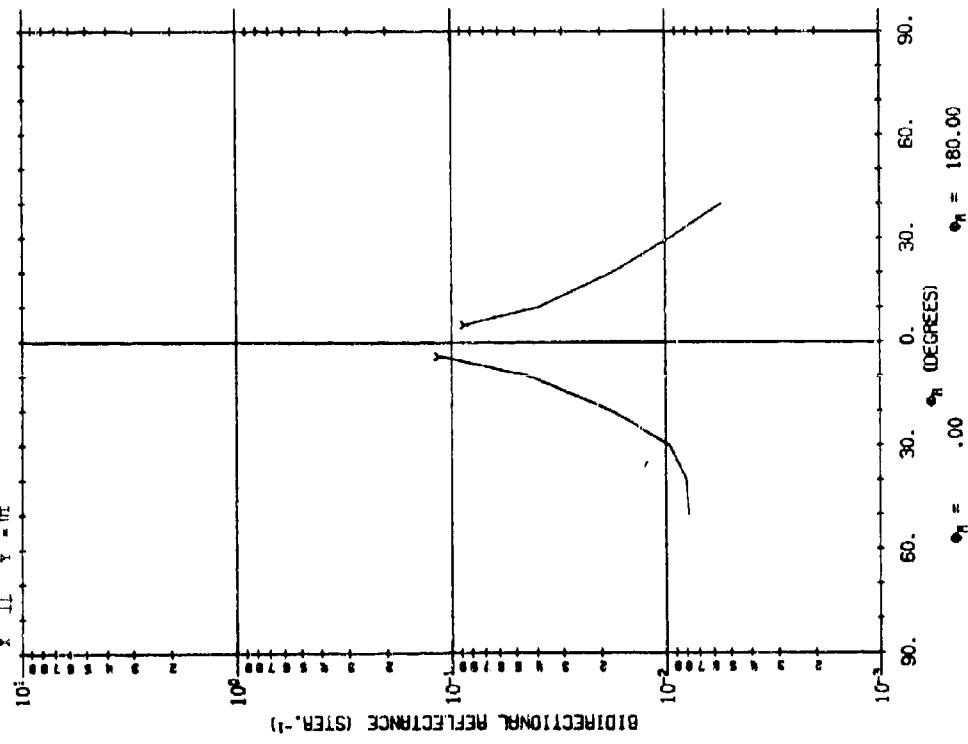


WOOD

A00167 002

Oregon White Oak Block

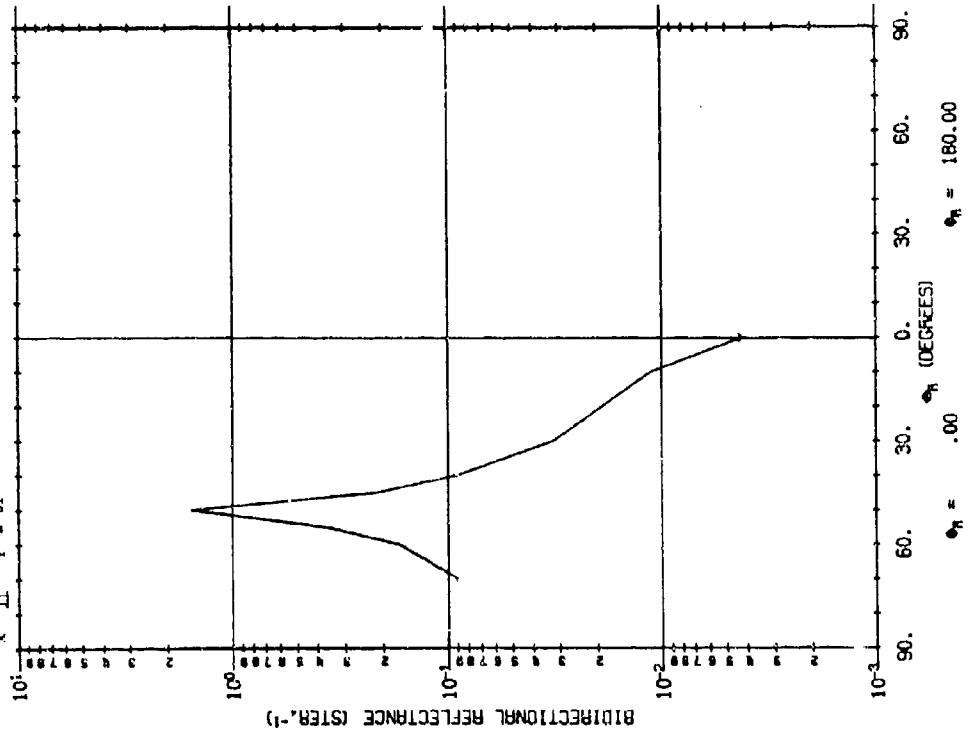
$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
 $Y = 17$



A00167 002

Oregon White Oak Block

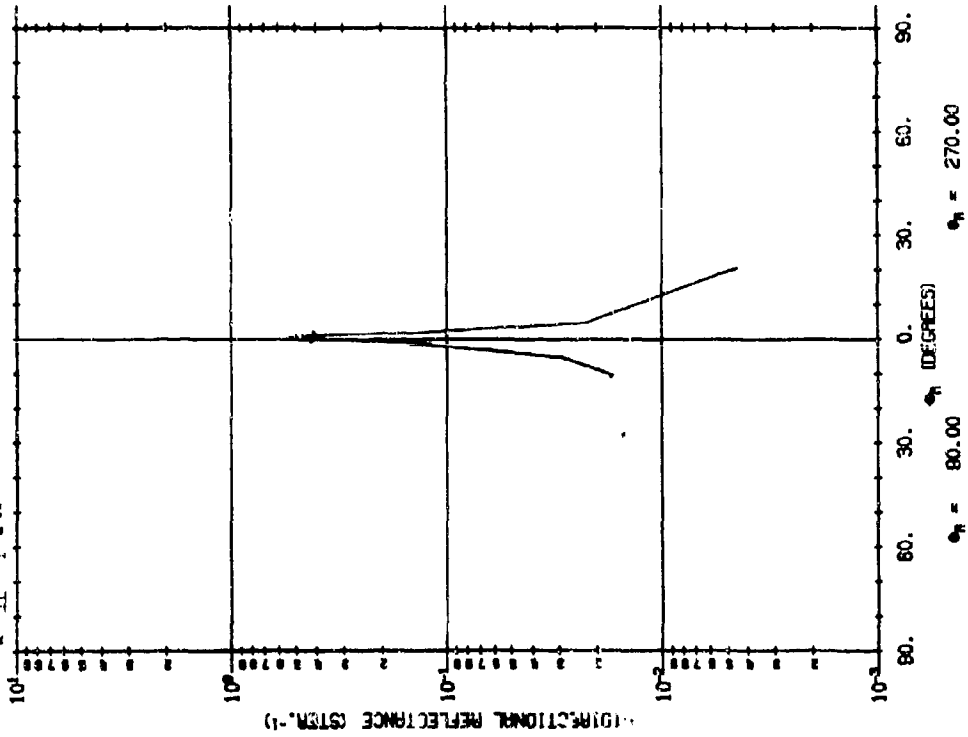
$\theta_1 = 50.00$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
 $Y = DT$



A00167 002

Oregon White Oak Block

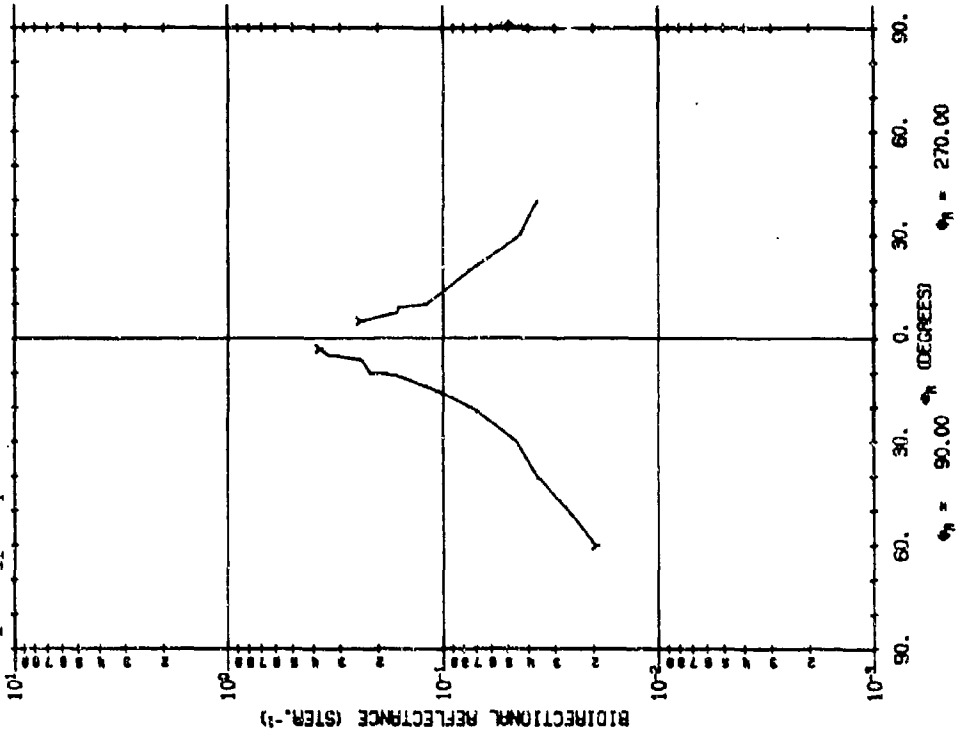
0 || 28 = 1.10
+ || $\phi_1 = \phi_r$
Δ || λ = 10.6
X || γ = 0°



A00167 002

Oregon White Oak Block

0 || $\phi_1 = 0.0$
+ || $\phi_2 = 270.0$
Δ || λ = 10.6
X || γ = 0°

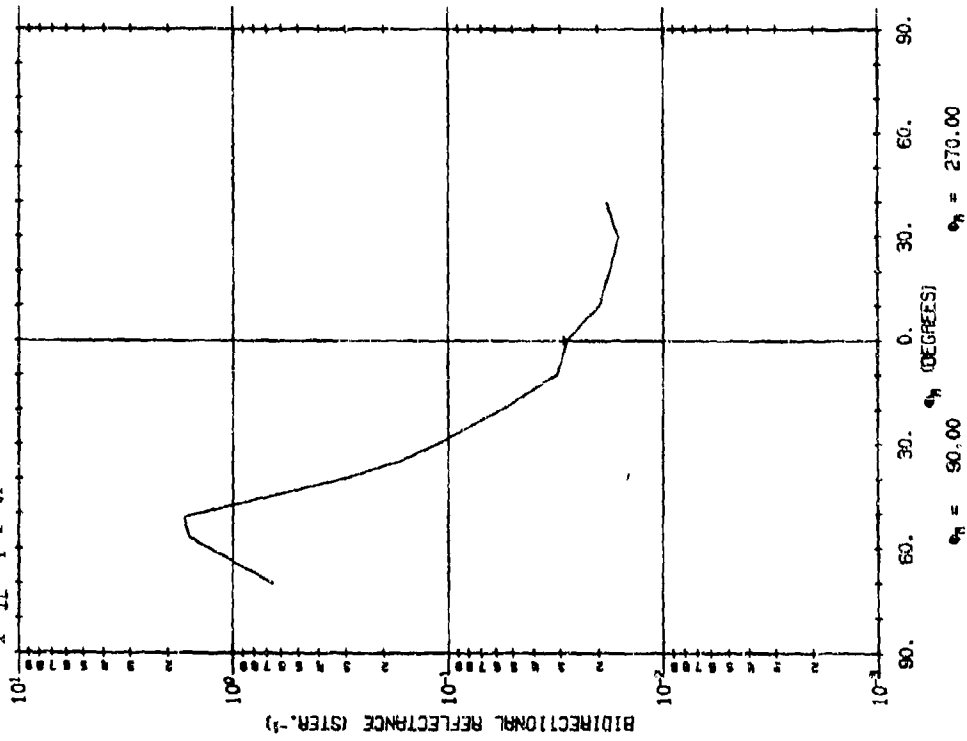


WOOD

R00167 002

Oregon White Oak Block

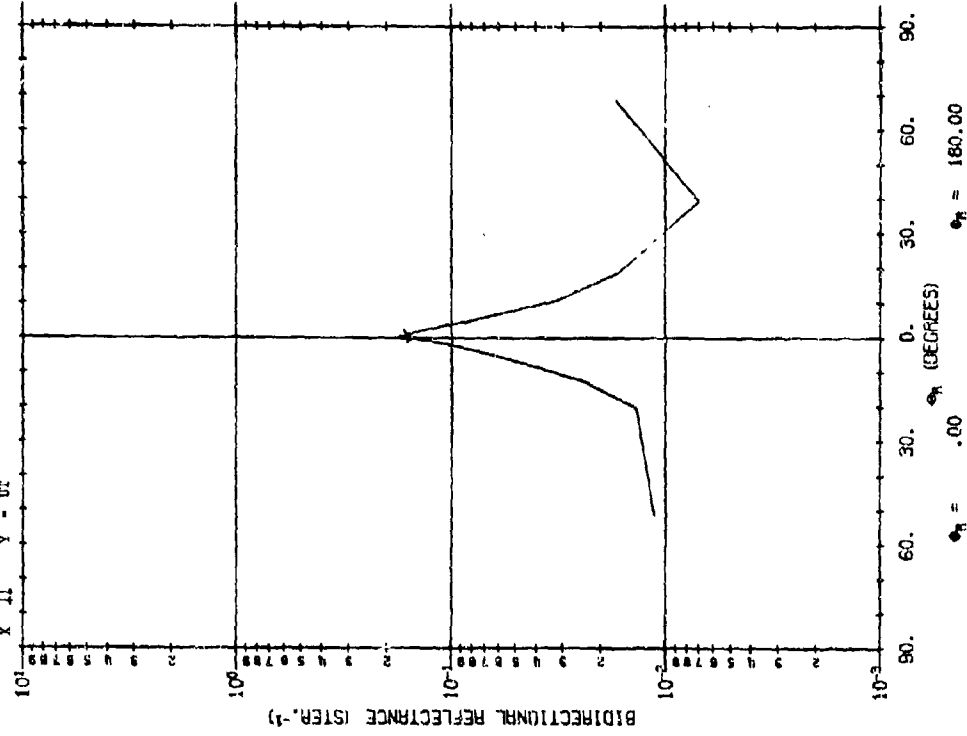
0 || $\phi_1 = 50.0$
+ || $\phi_2 = 270.0$
Δ || $\lambda = 10.6$
X || Y = UT



R01585 001

Untreated Wood

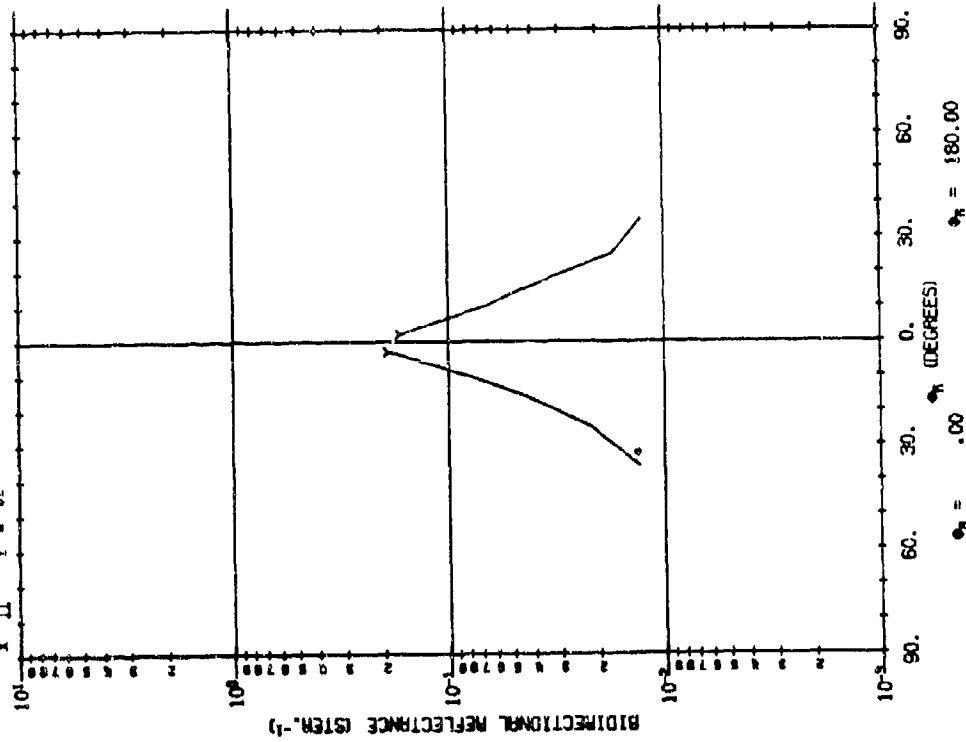
0 || $2Z = 1.10$
+ || $\phi_1 = 2$
Δ || $\lambda = 10.6$
X || Y = UT



R01585 001

Untreated Wood

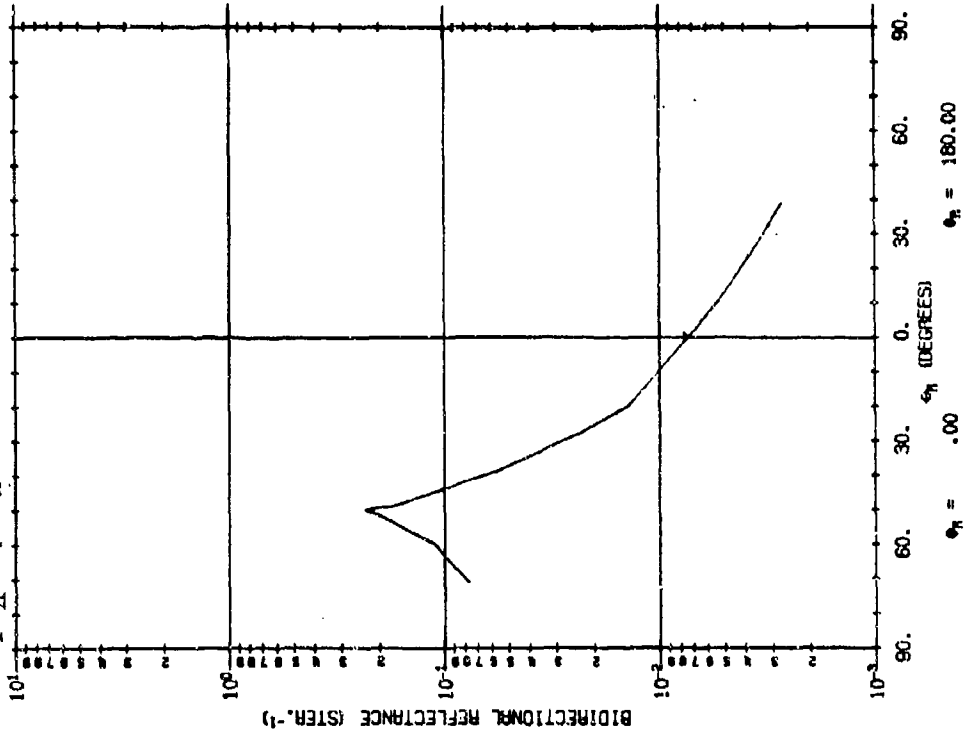
$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
Y = VT



R01585 001

Untreated Wood

$\theta_1 = 50.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
Y = VT

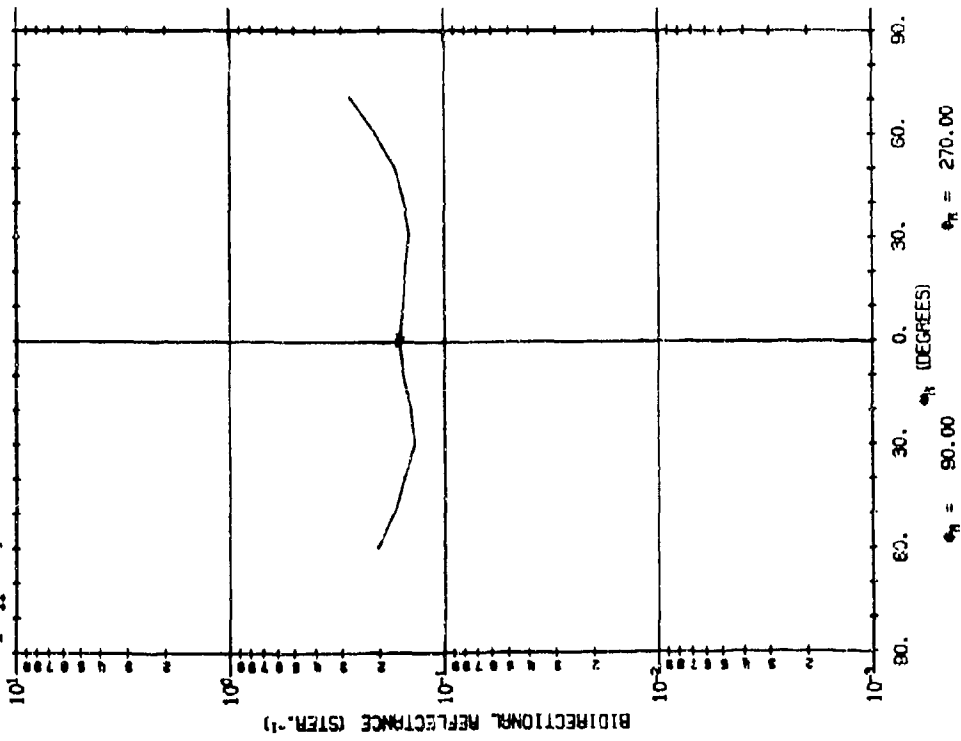


WOOD

R01585 001

Dtreated Wood

0 // 2P = 1.10
+ // $\phi_1 = \phi_r$
Δ // $\lambda = 10.6$
X // Y = 0T

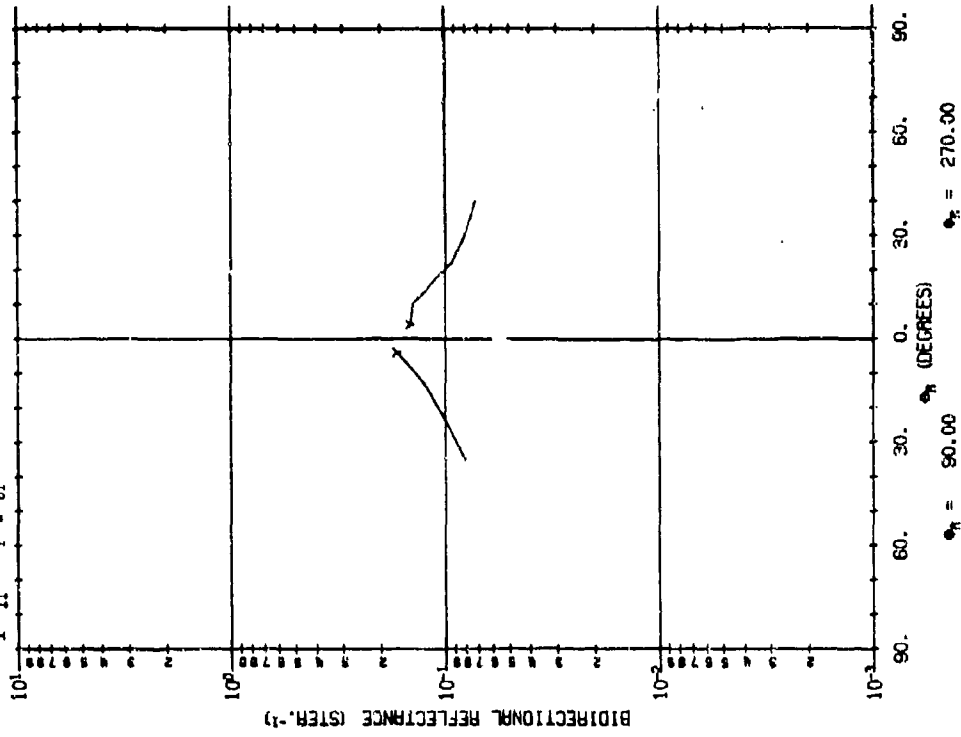


$\phi_t = 90.00$ $\phi_r = 270.00$

R01585 001

Untreated Wood

0 // $\phi_1 = 0.0$
+ // $\phi_1 = 270.0$
Δ // $\lambda = 10.6$
X // Y = 0T

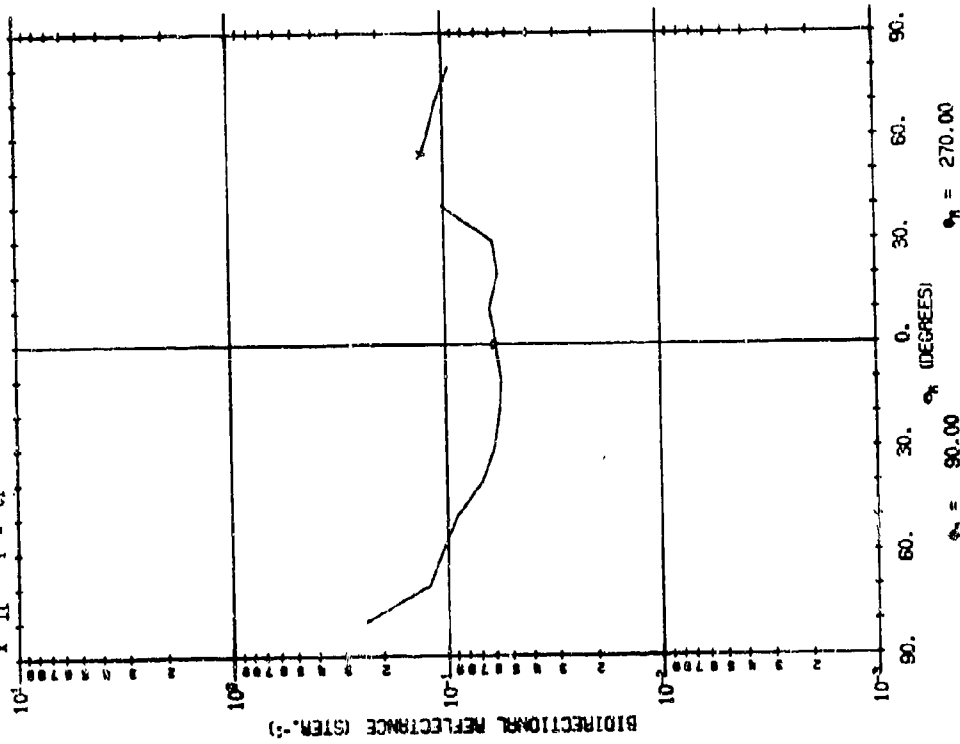


$\phi_t = 90.00$ $\phi_r = 270.00$

R01585 001

Untreated Wood

$\theta_i = 50.0$
 $\phi_1 = 270.0$
 $\lambda = 10.6$
 $\gamma = 0^\circ$

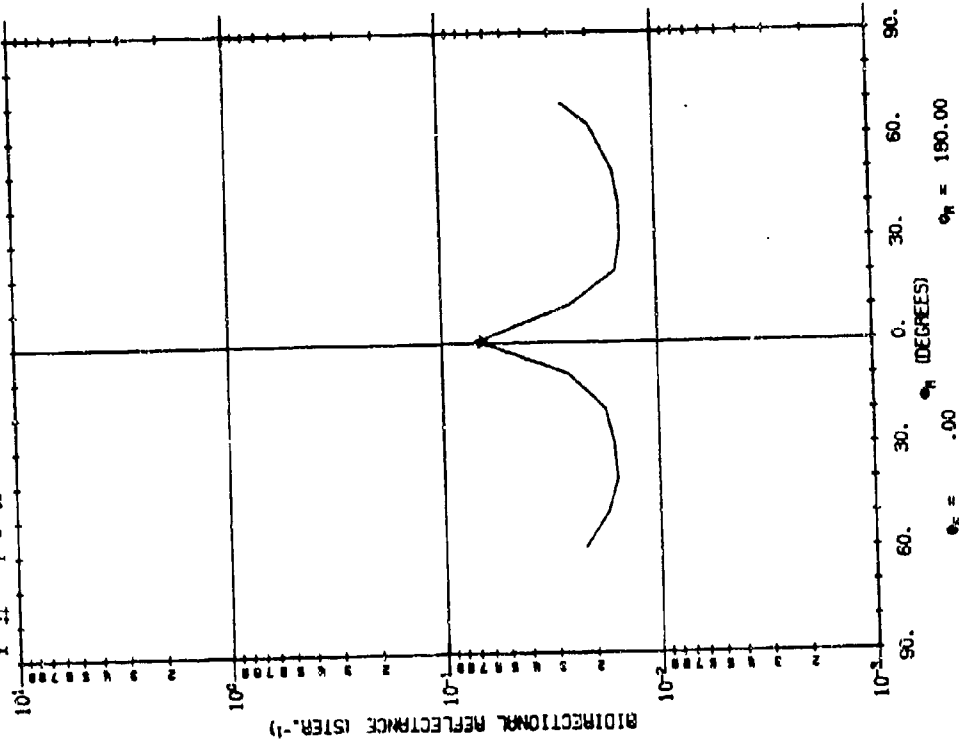


$\theta_r = 90.00$ $\phi_r = 270.00$

R01590 001

Unpainted Plywood

$\theta_i = 1.10$
 $\phi_1 = 0^\circ$
 $\lambda = 10.6$
 $\gamma = 0^\circ$



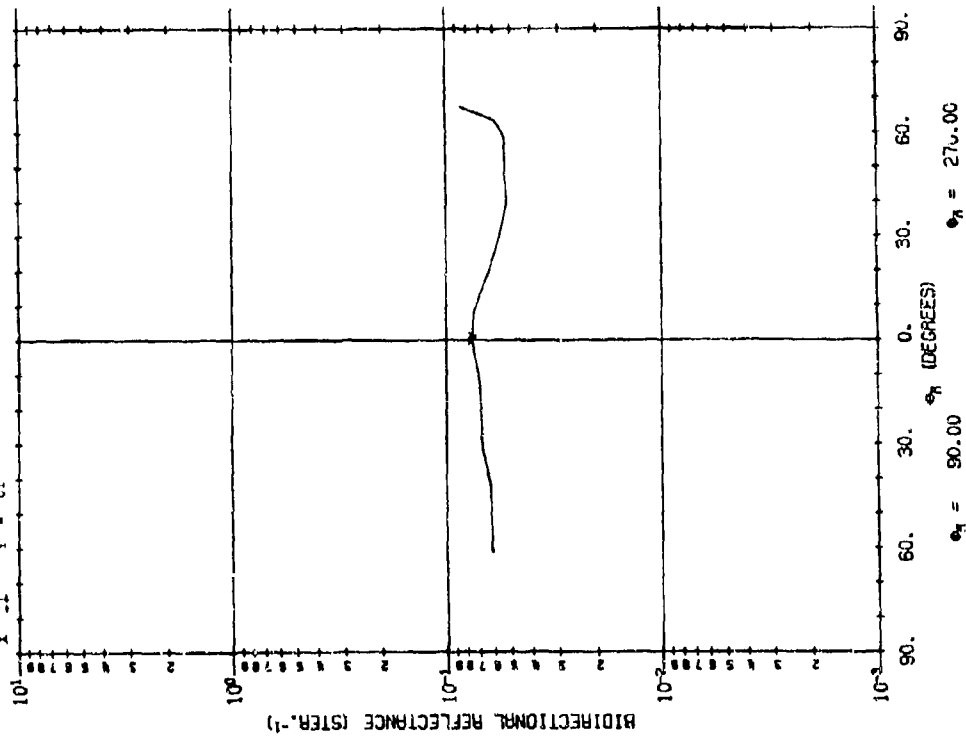
$\theta_r = .00$ $\phi_r = 180.00$

WOOD

AG1590 001

Unpainted Plywood

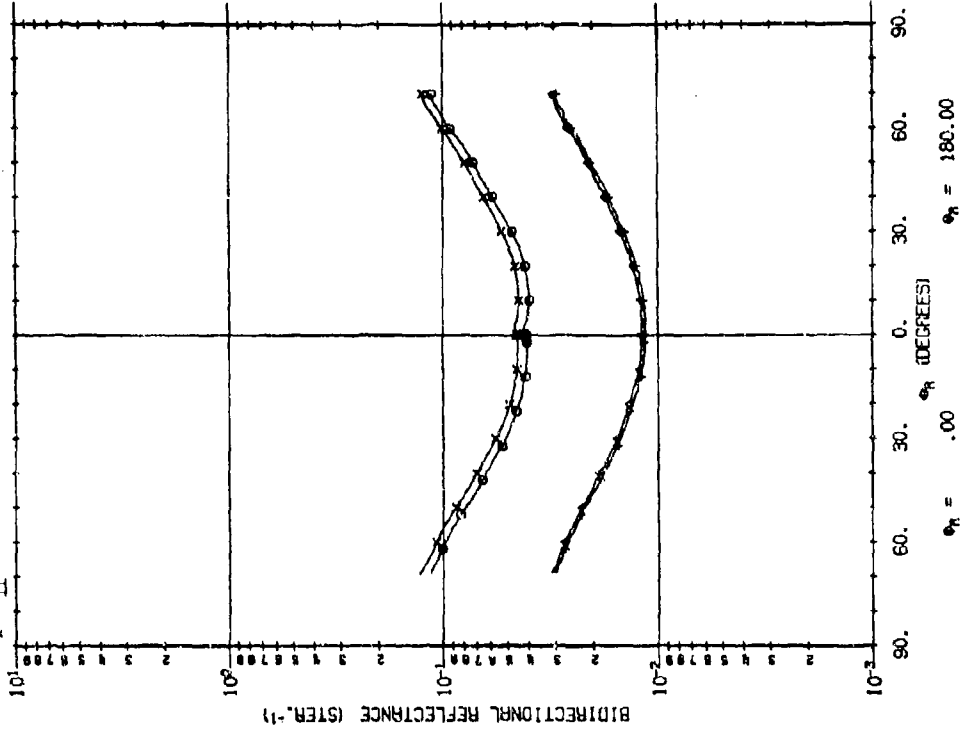
$z_f = 1.50$
 $\phi_1 = \phi_r$
 $\lambda = 10.6$
 $Y = UT$



AG1699 101

WOOD

$z_f = 2.0$
 $\phi_1 = \phi_r$
 $\lambda = 0.65$

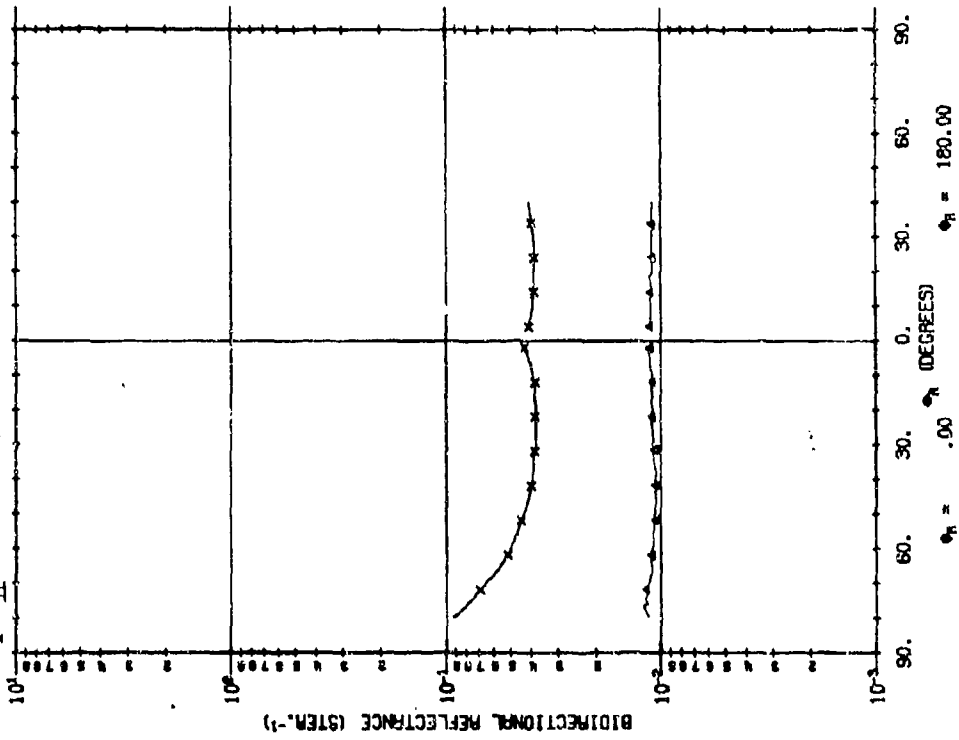


A01699 101

WOOD

$\epsilon_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 0.63$

C || ||
+ || ||
Δ || ||
x || ||

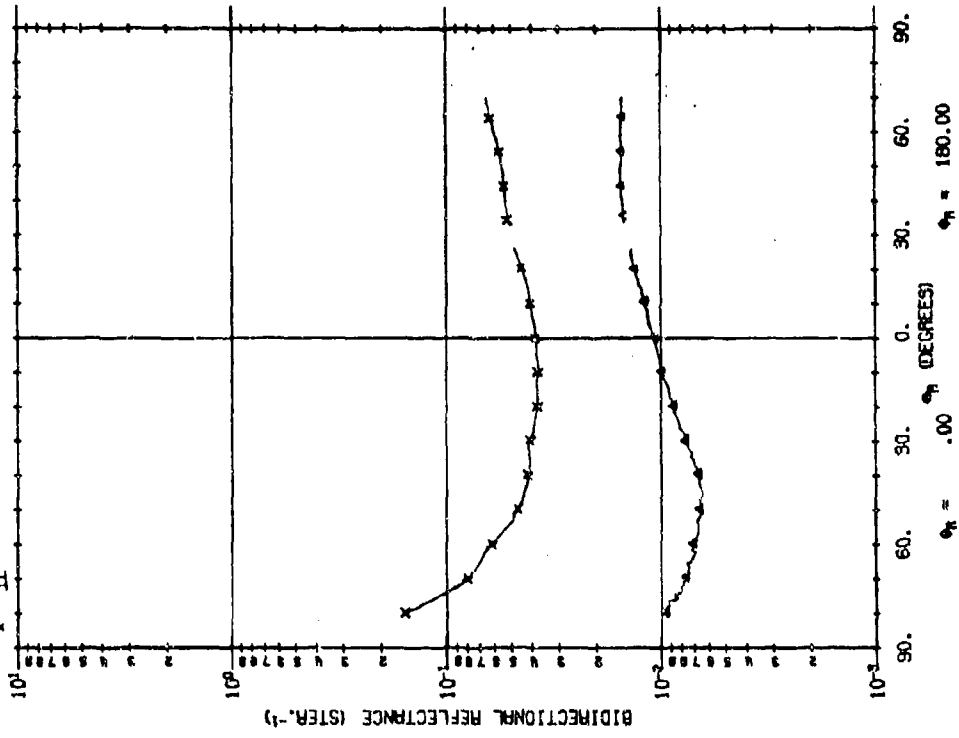


A01699 101

WOOD

$\epsilon_1 = 30.0$
 $\phi_1 = 180.0$
 $\lambda = 0.63$

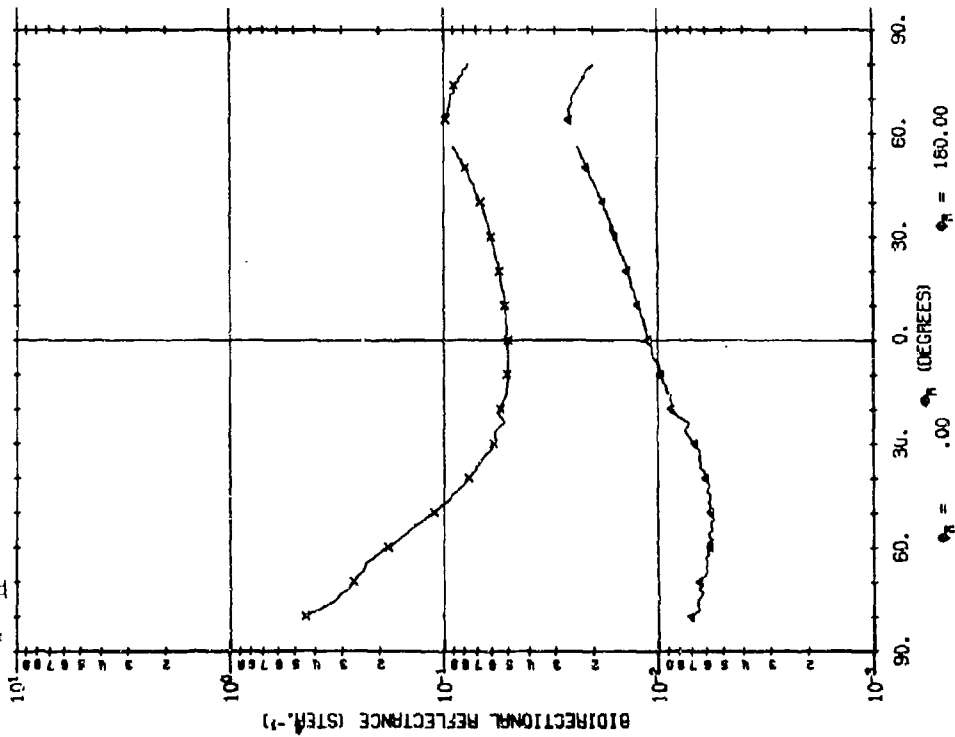
C || ||
+ || ||
Δ || ||
x || ||



WOOD

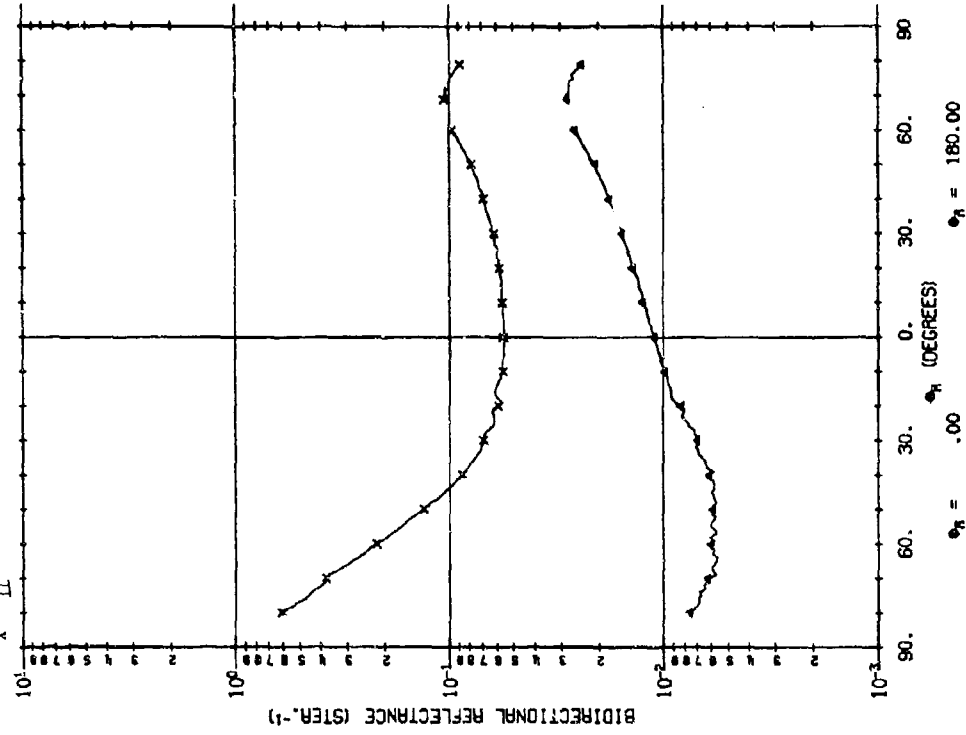
A01699 101

WOOD
0 || $\theta_1 = 60.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 0.63$
X ||



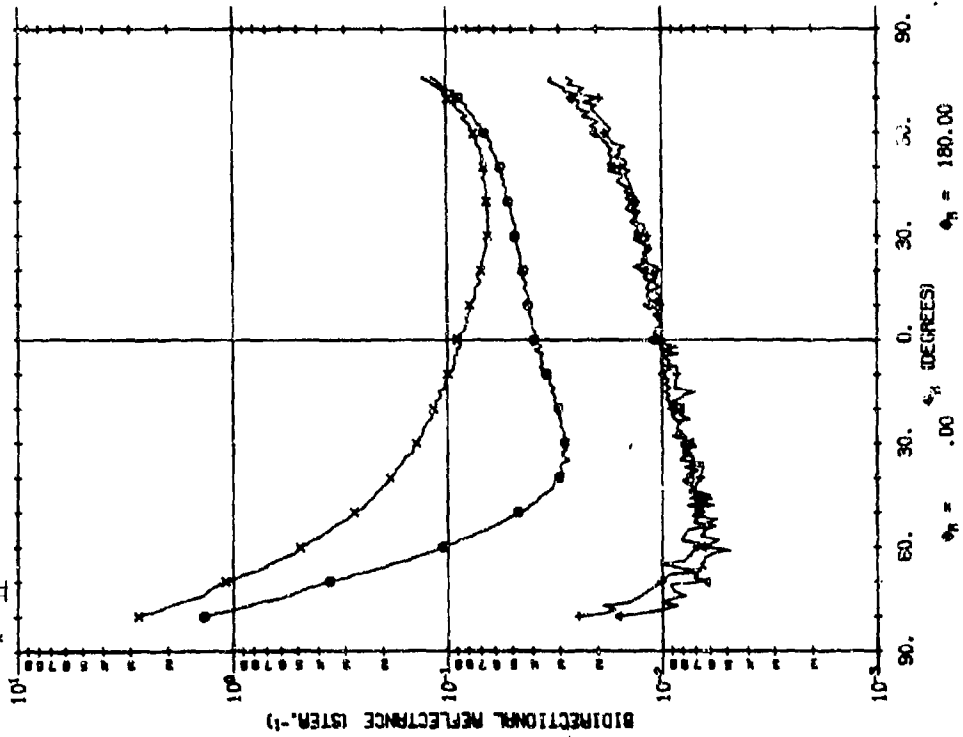
A01699 101

WOOD
0 || $\theta_1 = 65.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 0.63$
X ||



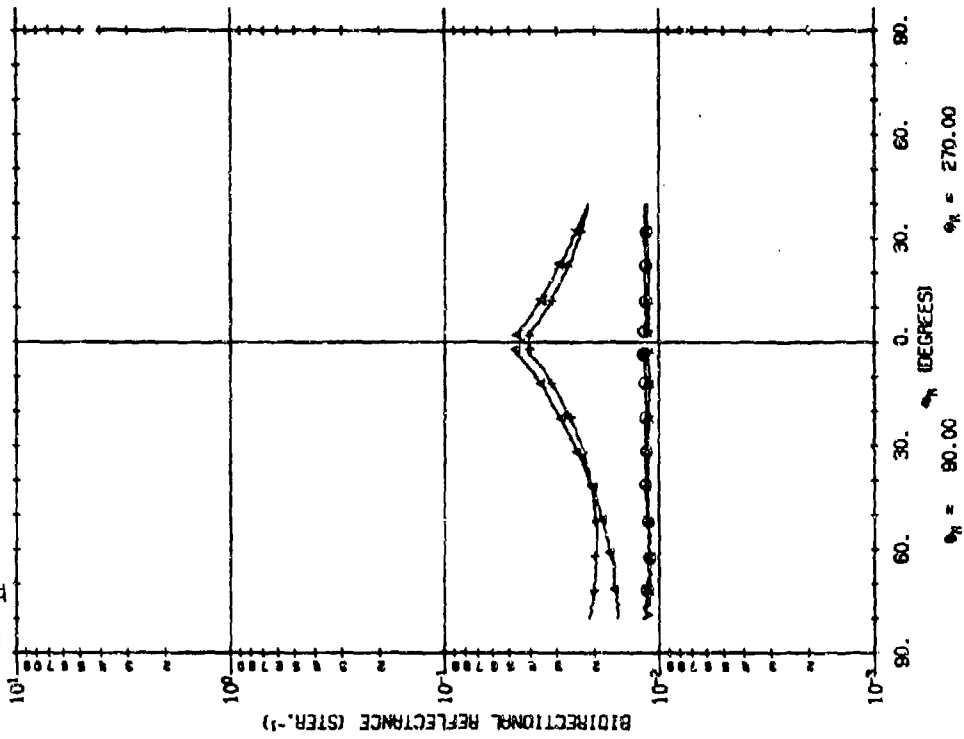
F01699 101
 0 || $\theta_1 = 80.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 0.63$
 X ||

WOOD



R01699 101
 0 || $\theta_1 = 0.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 0.63$
 X ||

WOOD

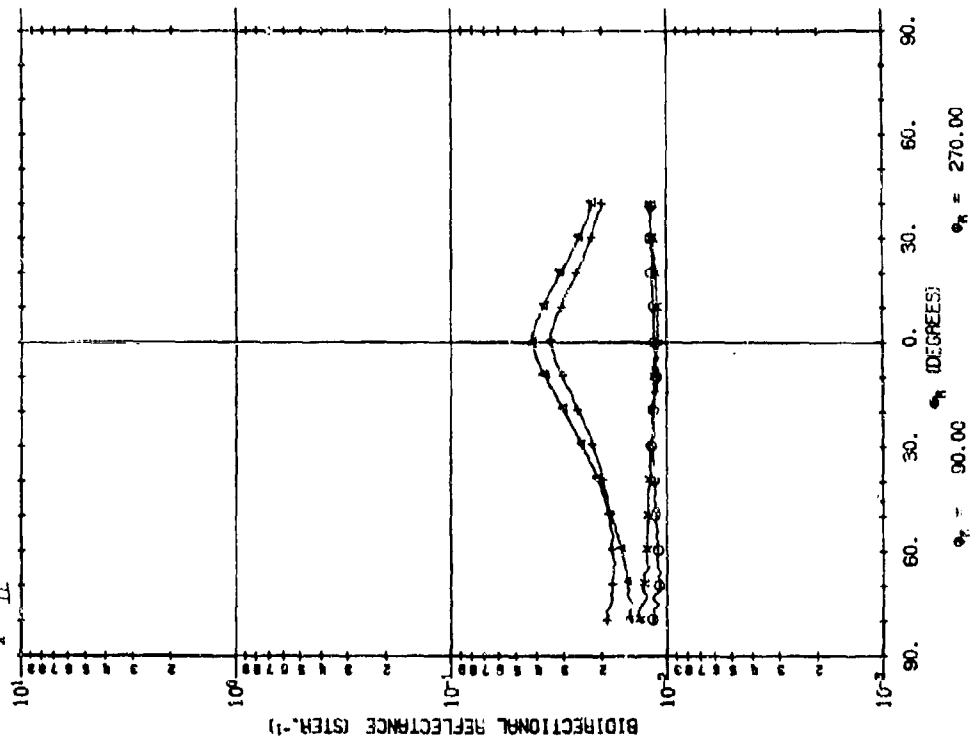


WOOD

R01699 101

WOOD

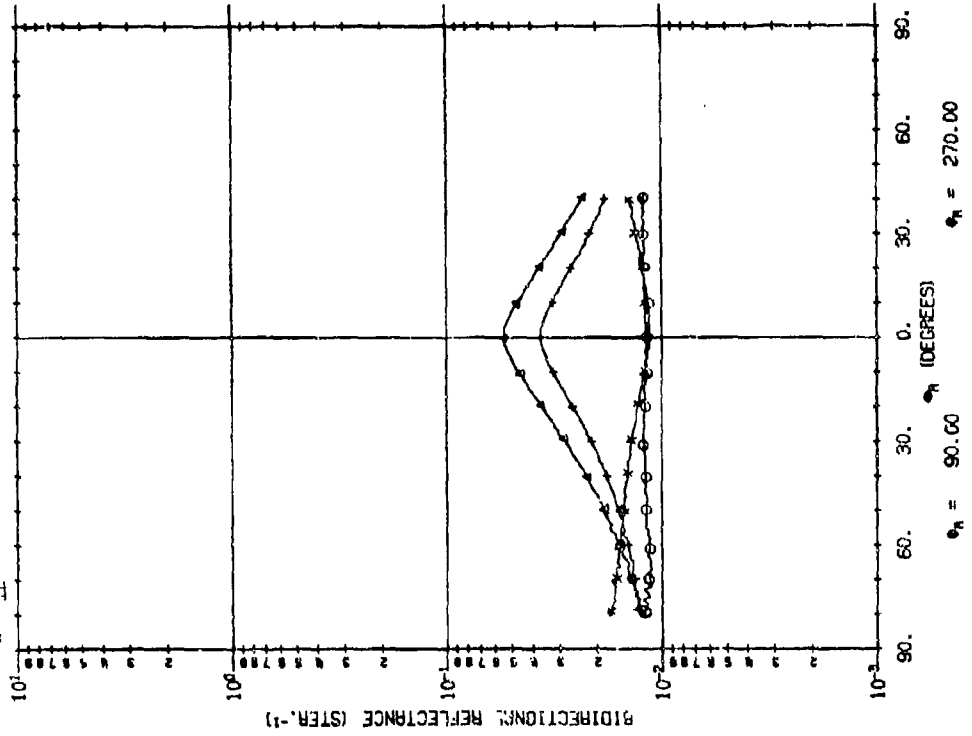
0 || $\epsilon_1 = 39.0$
+ || $\epsilon_2 = 180.0$
x || $\lambda = 0.63$



R01699 101

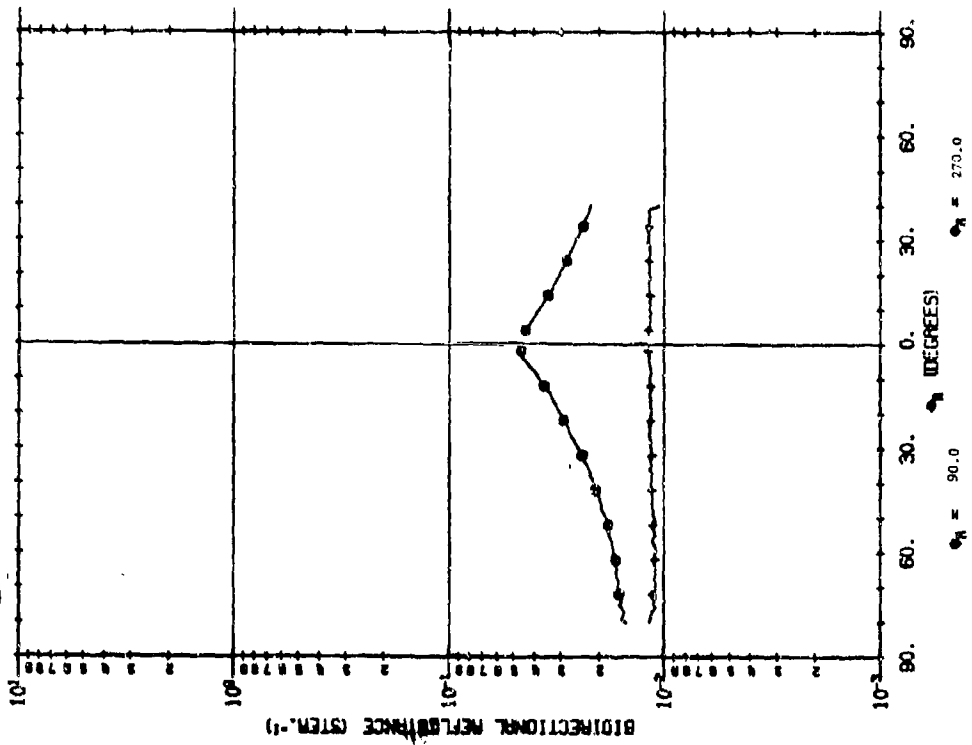
WOOD

0 || $\epsilon_1 = 60.0$
+ || $\epsilon_2 = 180.0$
x || $\lambda = 0.63$



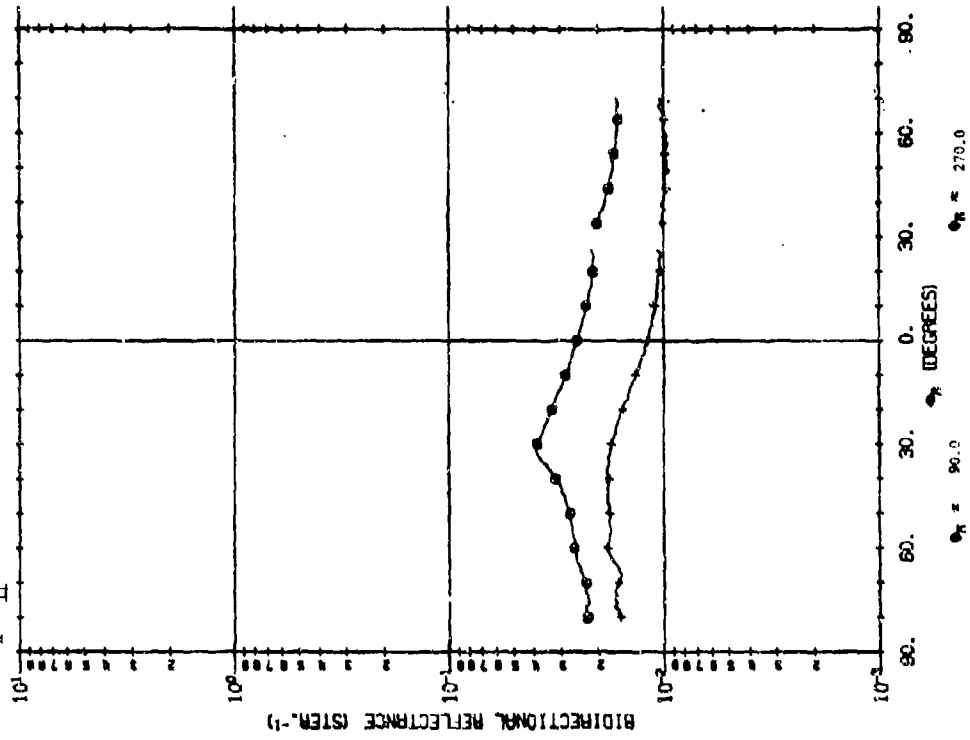
R01699 101

WOOD
 $\theta_1 = 0.0$
 $\theta_2 = 270.0$
 $\lambda = 0.63$



R01699 101

WOOD
 $\theta_1 = 30.0$
 $\theta_2 = 270.0$
 $\lambda = 0.63$

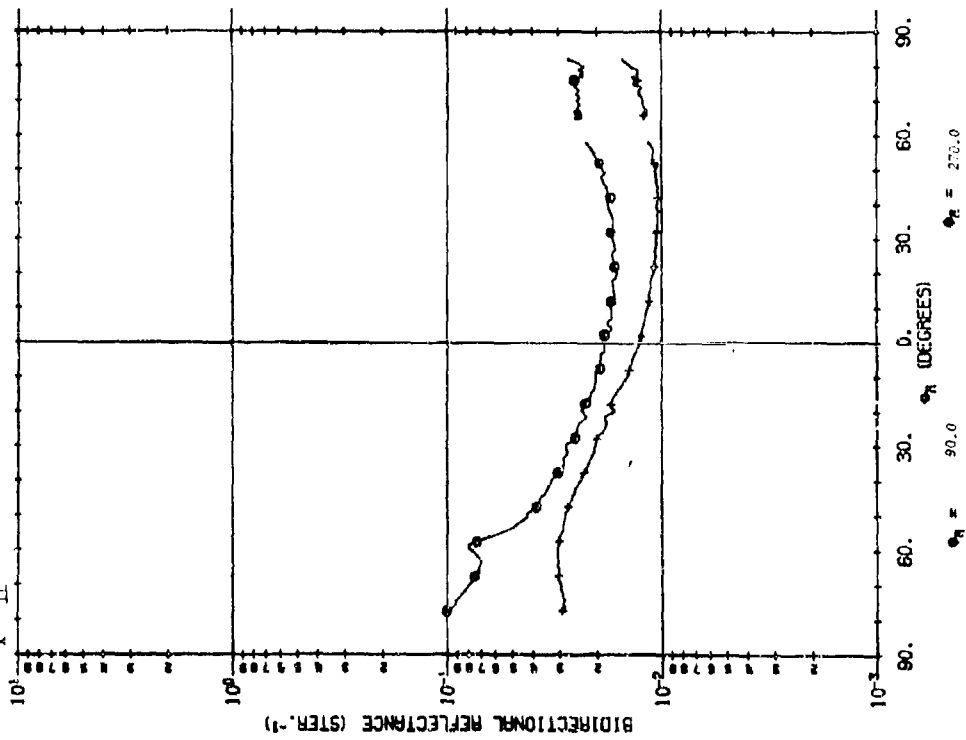


WOOD

AC1699 101

WOOD

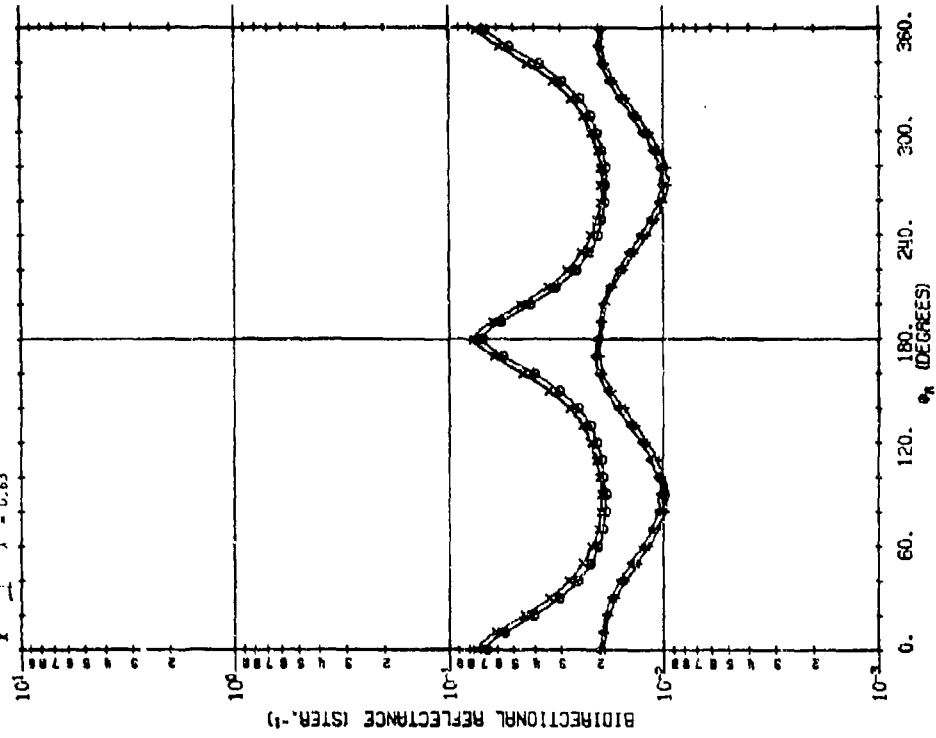
0 || $\theta_i = 60.0$
 + || $\phi_i = 270.0$
 Δ || $\lambda = 0.63$
 X ||

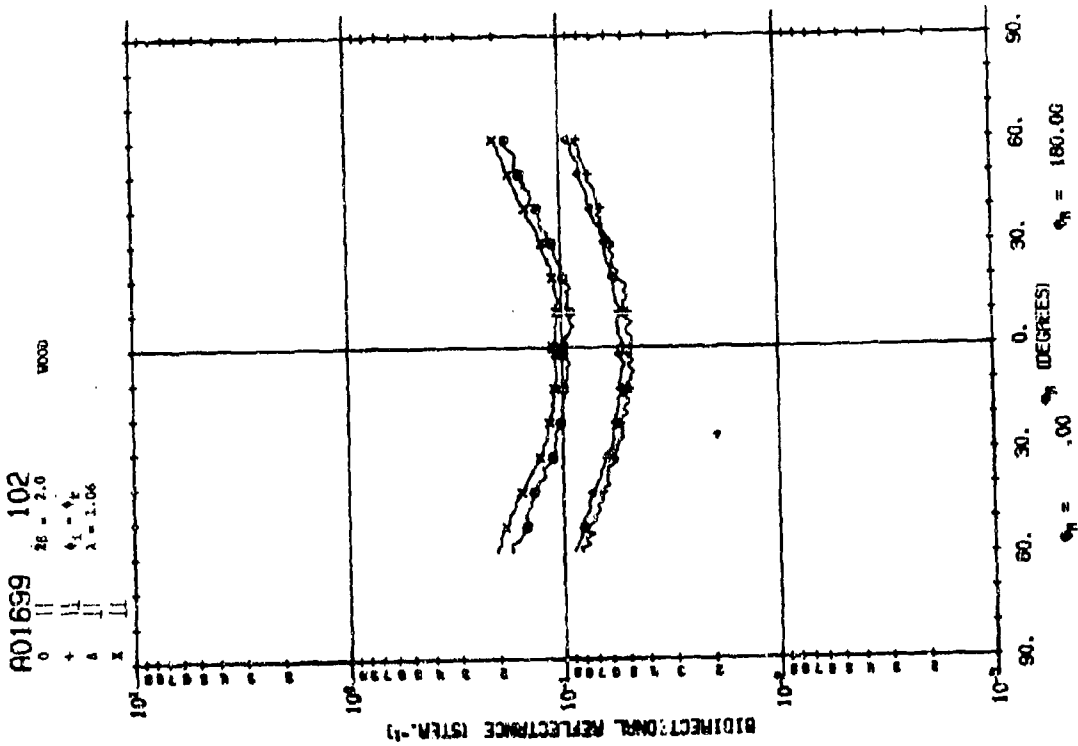
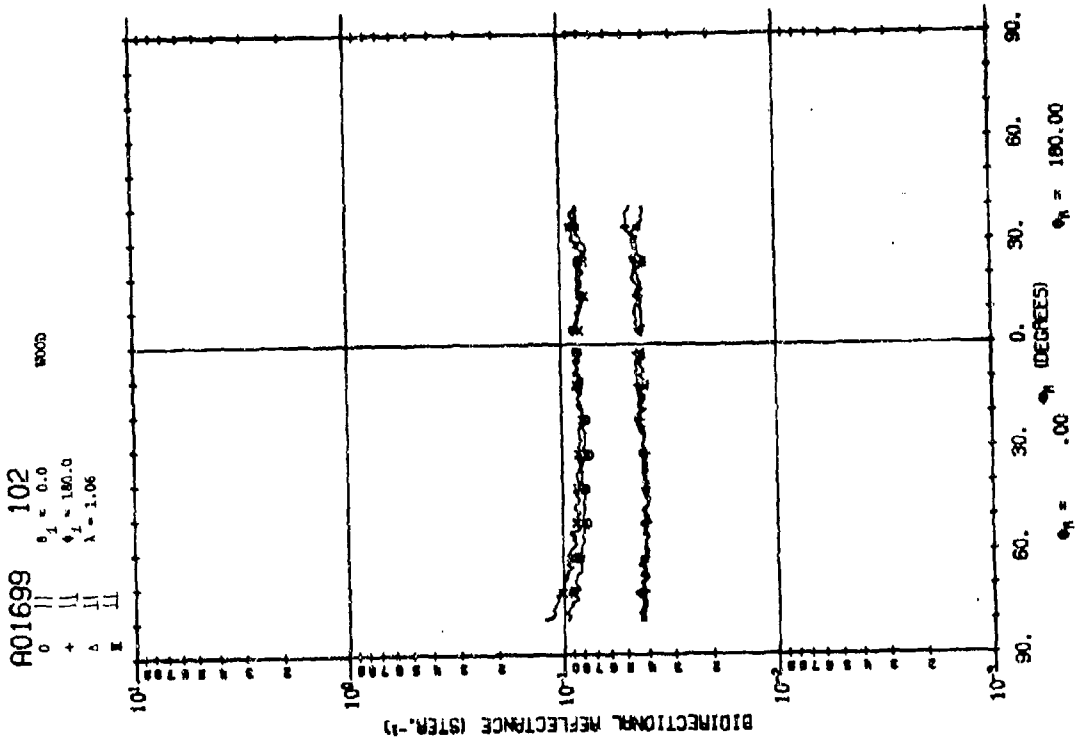


AC1699 101

WOOD

0 || $\theta_i = 45.0$
 + || $\phi_i = 47.0$, $2\beta = 2.0$
 Δ || $\theta_i = \phi_i$
 X || $\lambda = 0.63$





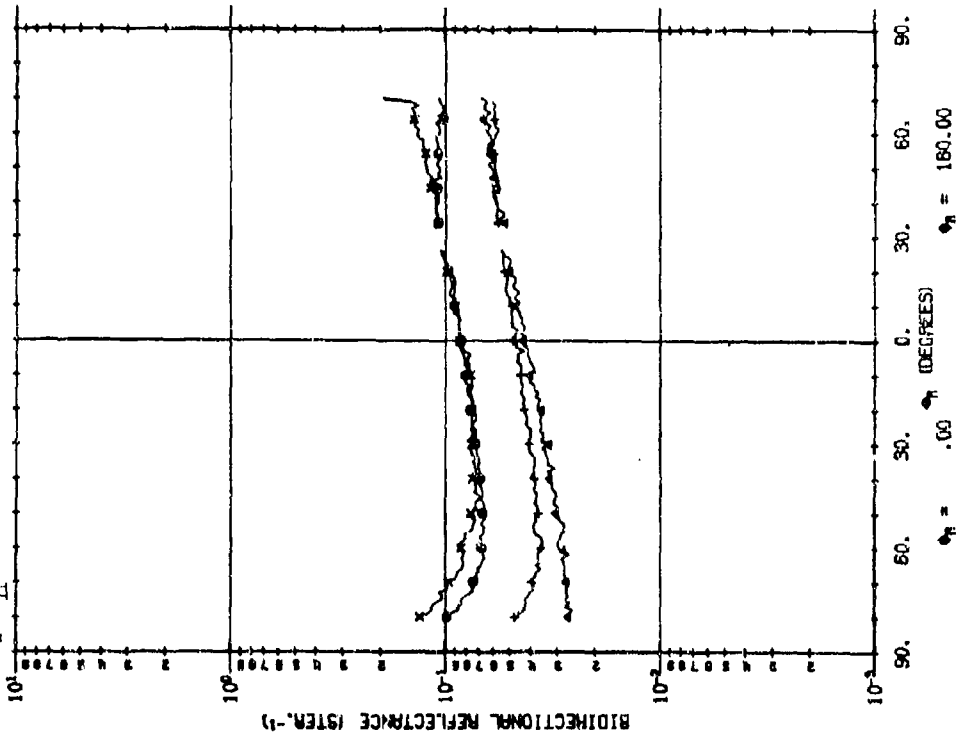
WOOD

R01699 102

WOOD

$\theta_1 = 30.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

0 ||
+ ||
A ||
X ||

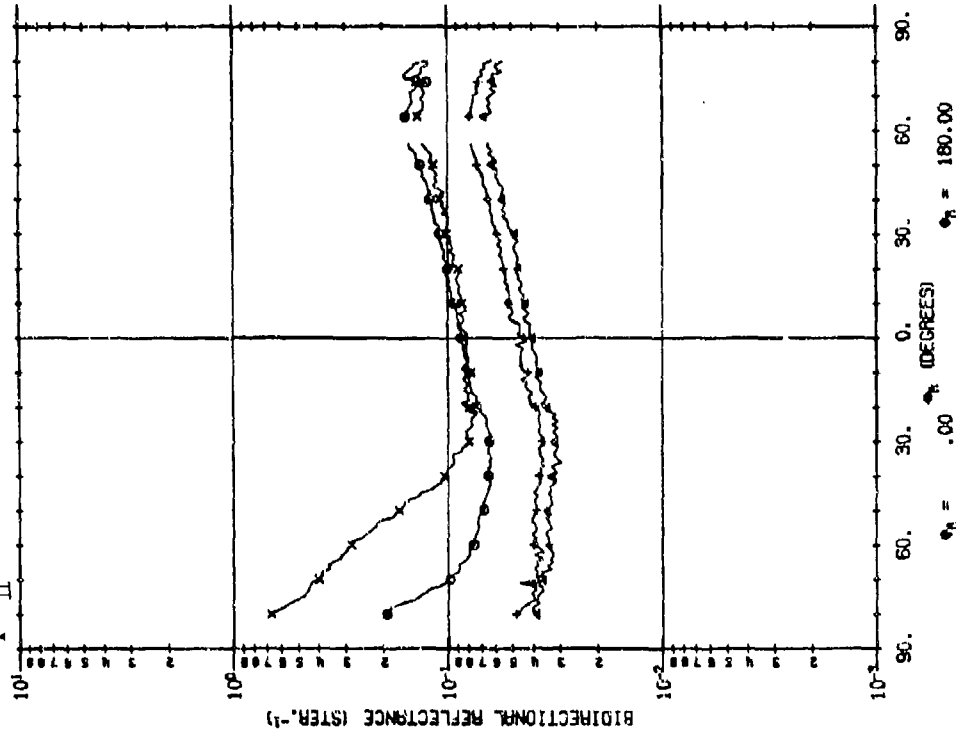


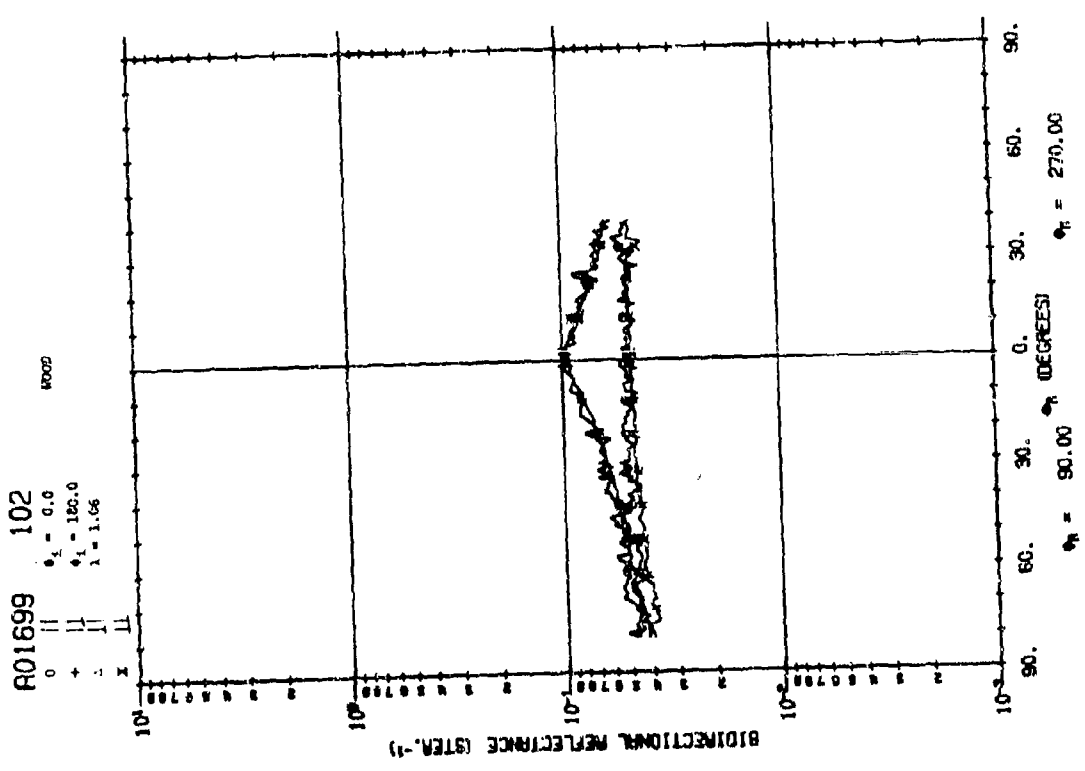
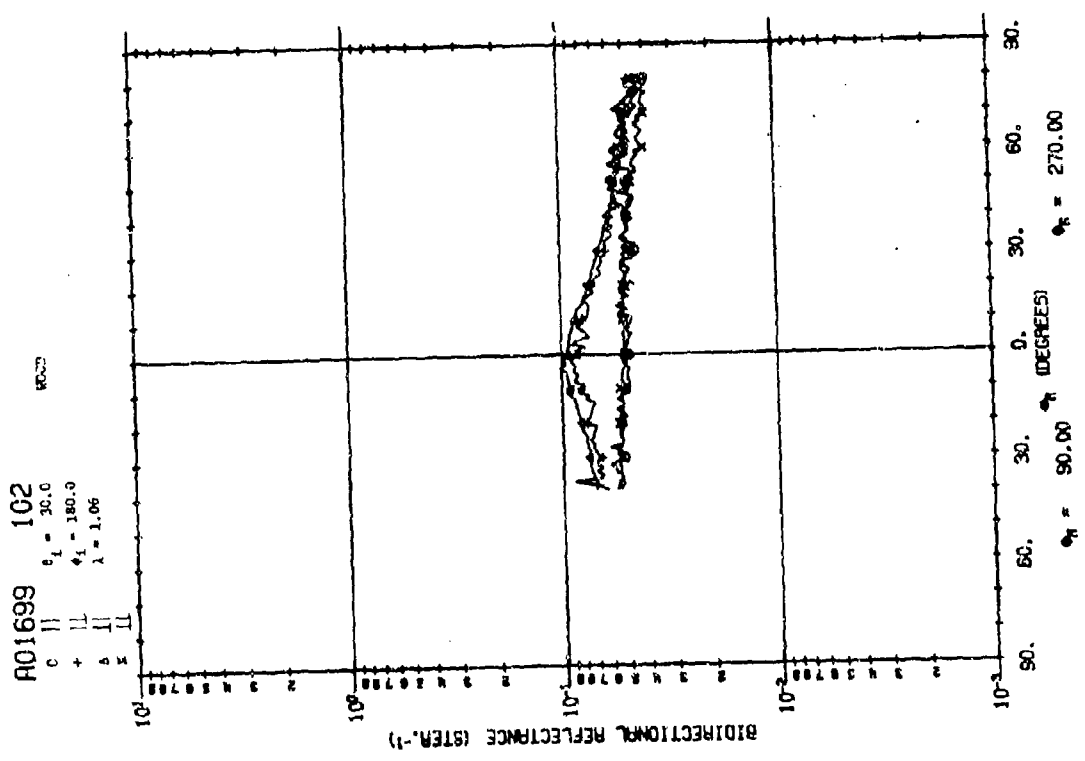
R01699 102

WOOD

$\theta_1 = 60.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

0 ||
+ ||
A ||
X ||



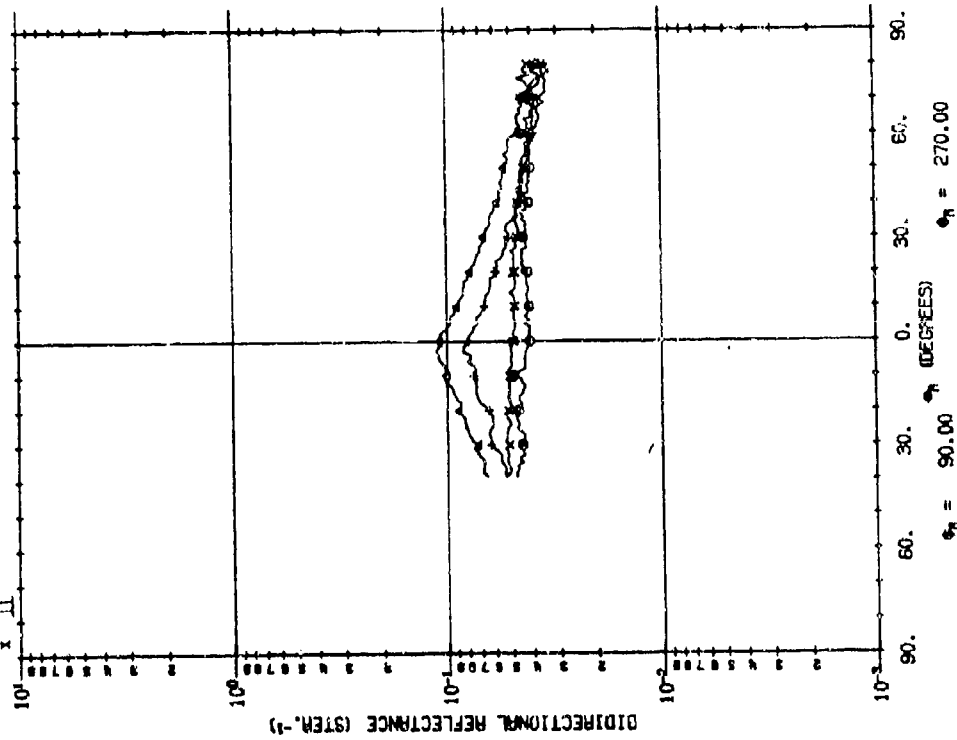


WOOD

A01699 102

WOOD

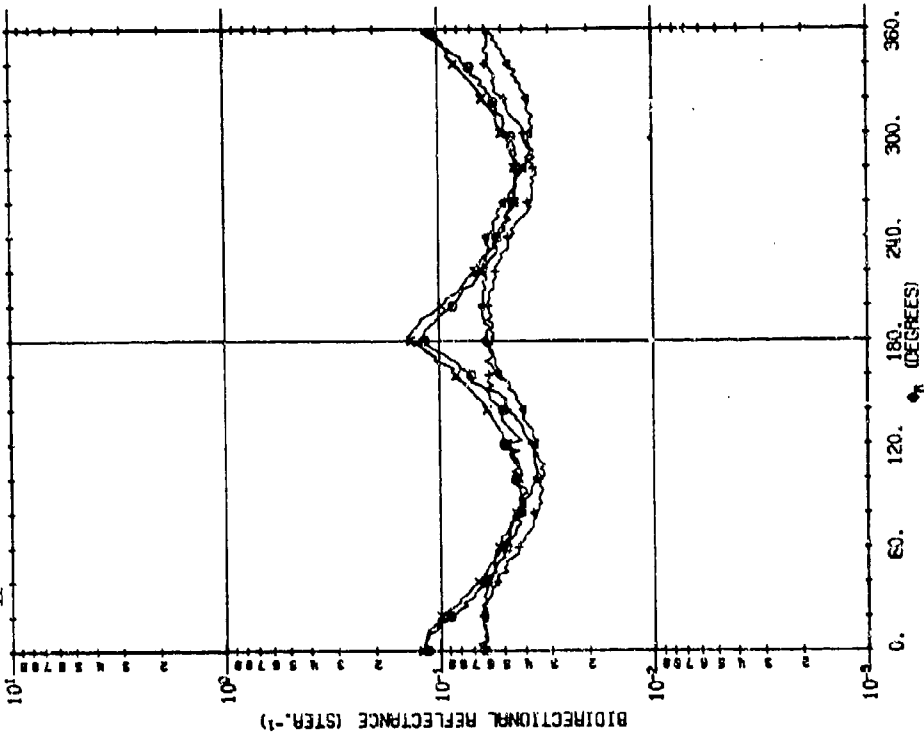
0 || $\theta_1 = 63.0$
+ || $\phi_1 = 180.0$
x || $\lambda = 1.06$



A01699 102

WOOD

0 || $\theta_1 = 45.0$
+ || $\phi_1 = 47.0$
x || $\lambda = 1.06$

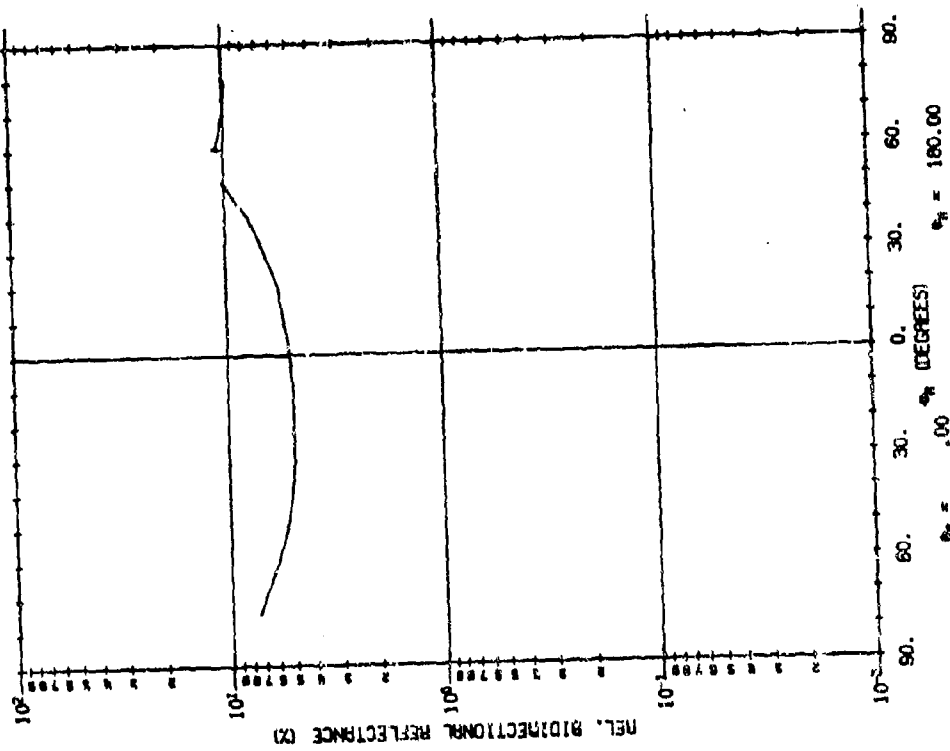


SOIL

B09010 014

RED CLAY, BKX

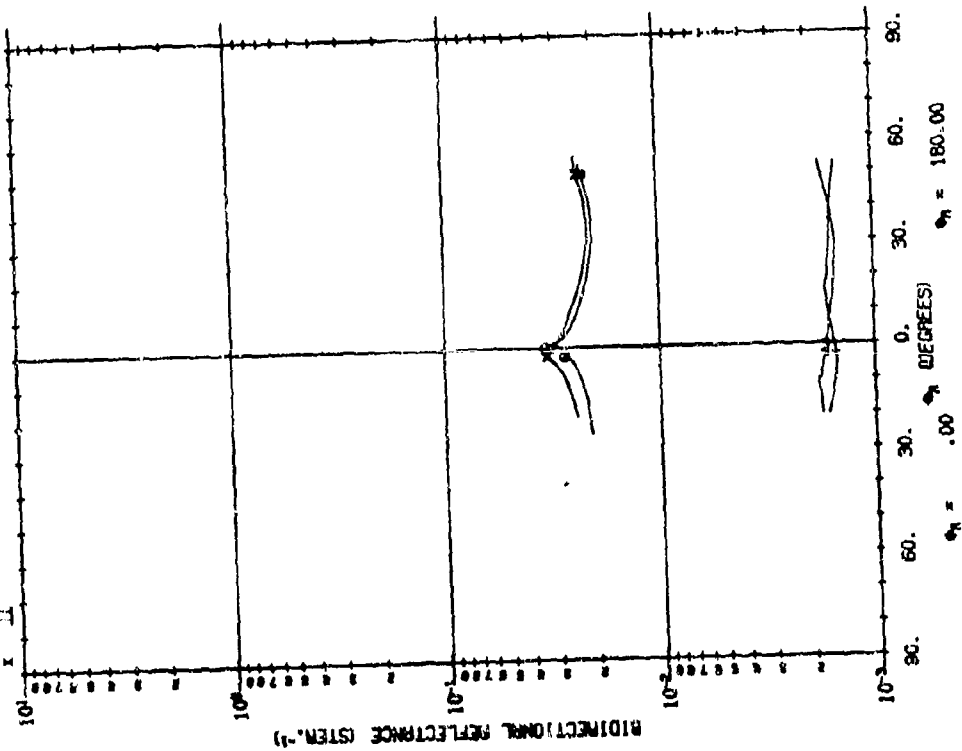
$\lambda = .4920$
 $\phi_1 = 53.0$
 $\psi_1 = 180.0$



R01959 101

SAND WITH OTHER PARTICLES IN IT
FROM CALIFORNIA

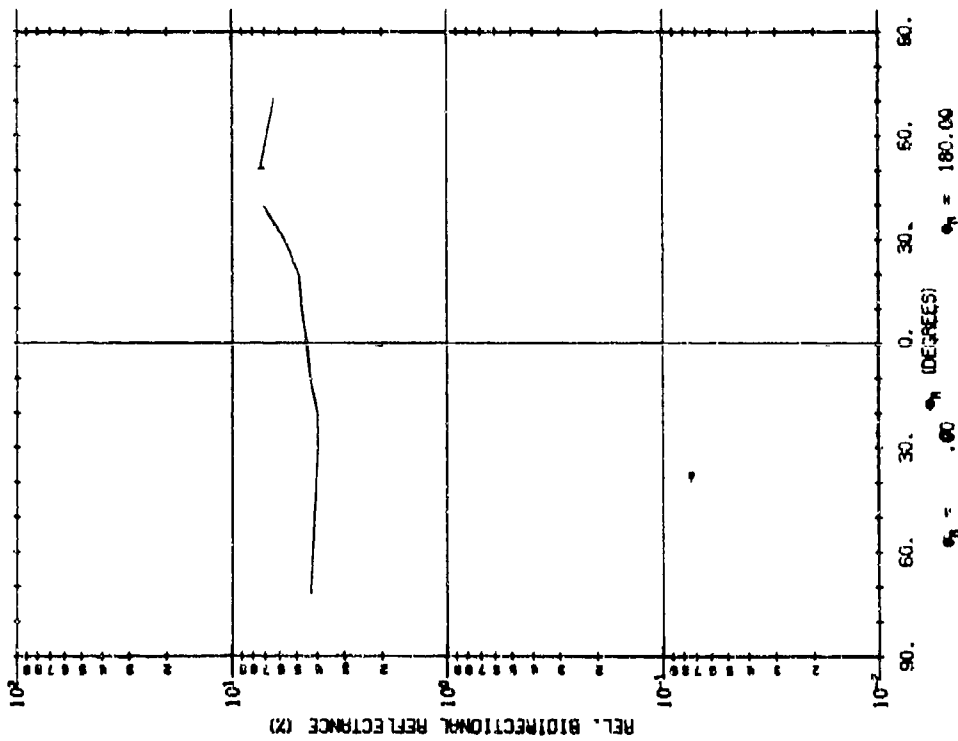
$2\theta = 2.5$
 $\lambda = 10.6$
 $\phi_1 = 0$
 $\psi_1 = 0$



SOIL

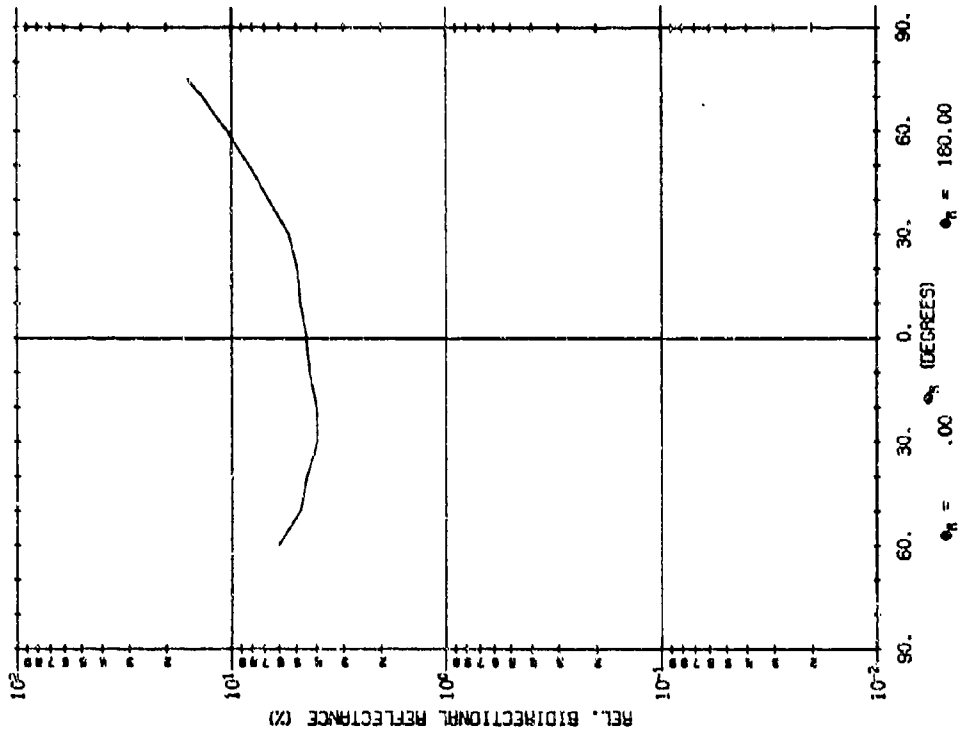
809010 019

UT
 $\lambda = .5200$ RED CLAY, DRY
 $\theta_1 = 45.0$
 $\theta_2 = 180.0$



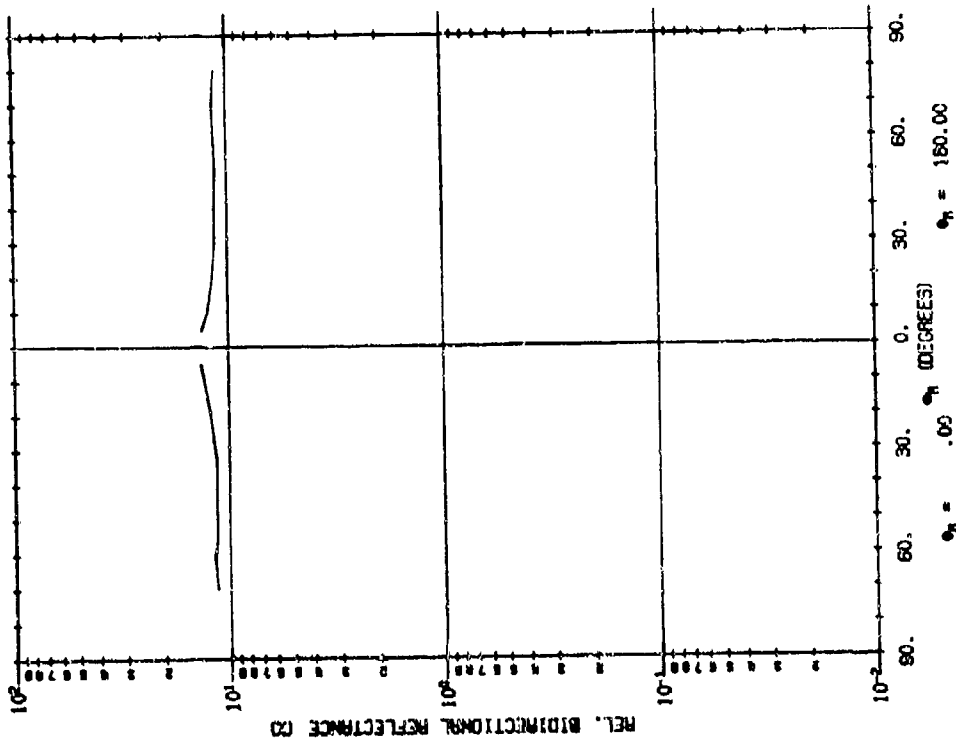
809010 017

UT
 $\lambda = .5200$ RED CLAY, DRY
 $\theta_1 = 80.0$
 $\theta_2 = 180.0$



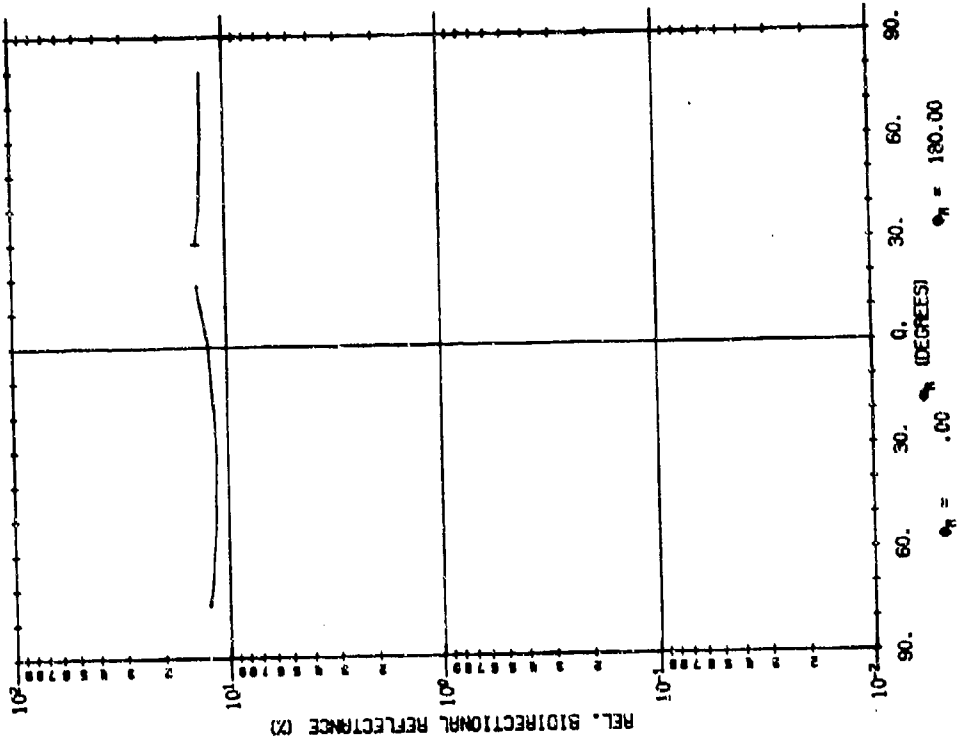
609010 006

|- UT MED CLAY, DEZ
 $\lambda = .6430$
 $\phi_1 = 0.0$
 $\phi_2 = 180.0$



609010 005

|- UT MED CLAY, INY
 $\lambda = .6430$
 $\phi_1 = 23.0$
 $\phi_2 = 180.0$



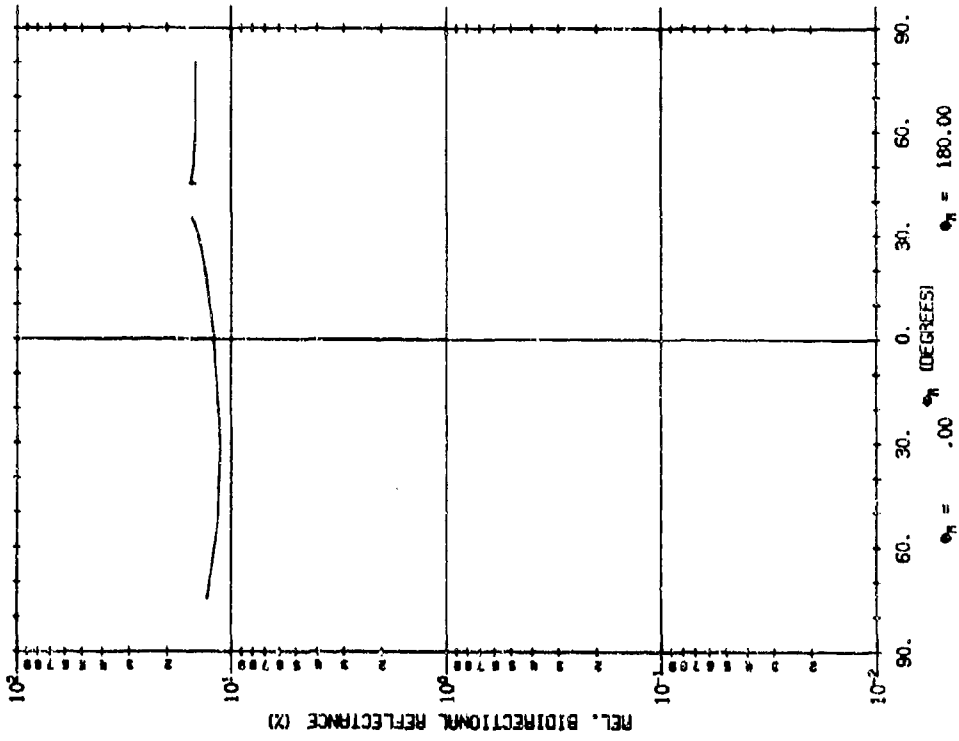
SOIL

809010 004

RED CLAY, DRY

$\lambda = .6430$
 $\phi_1 = 37.0$
 $\phi_2 = 180.0$

$\psi = 0^\circ$

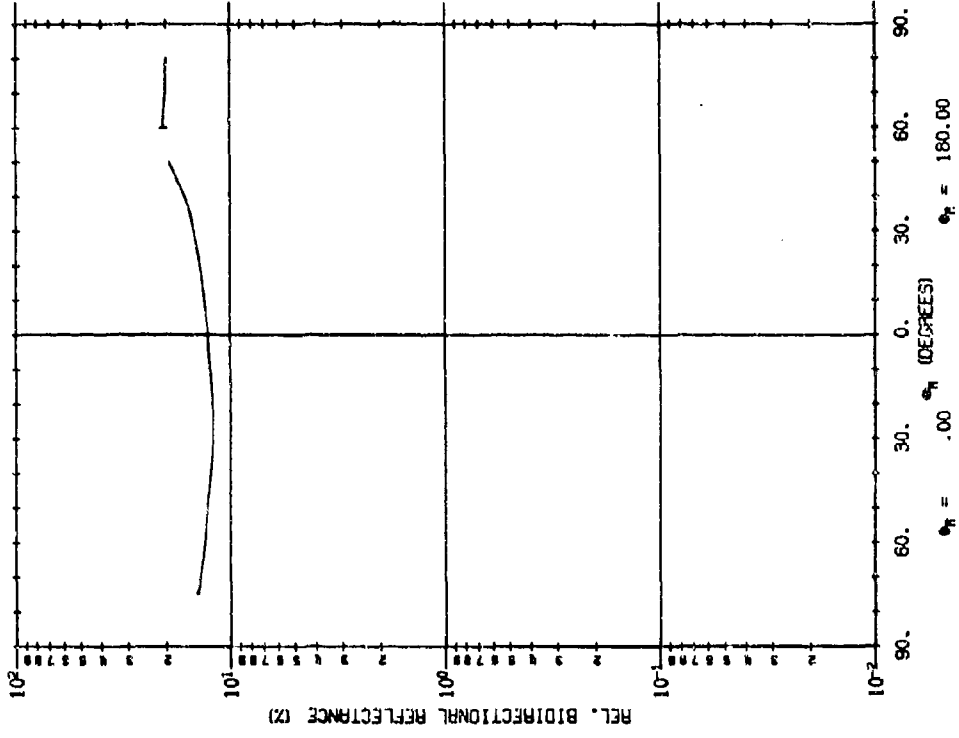


809010 003

RED CLAY, DRY

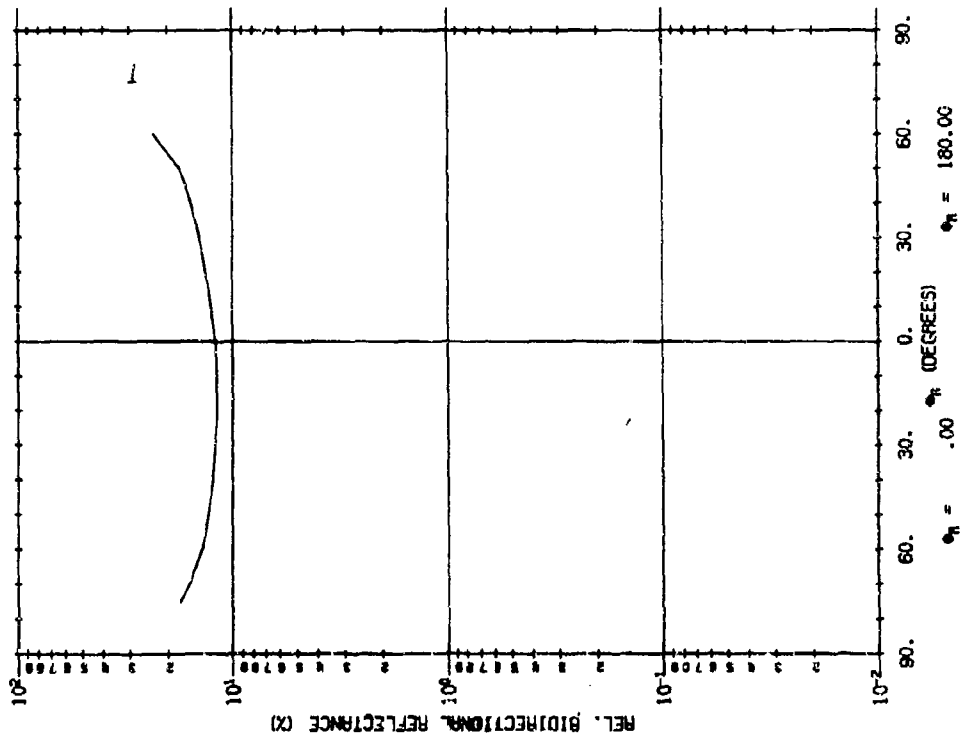
$\lambda = .6430$
 $\phi_1 = 53.0$
 $\phi_2 = 180.0$

$\psi = 0^\circ$



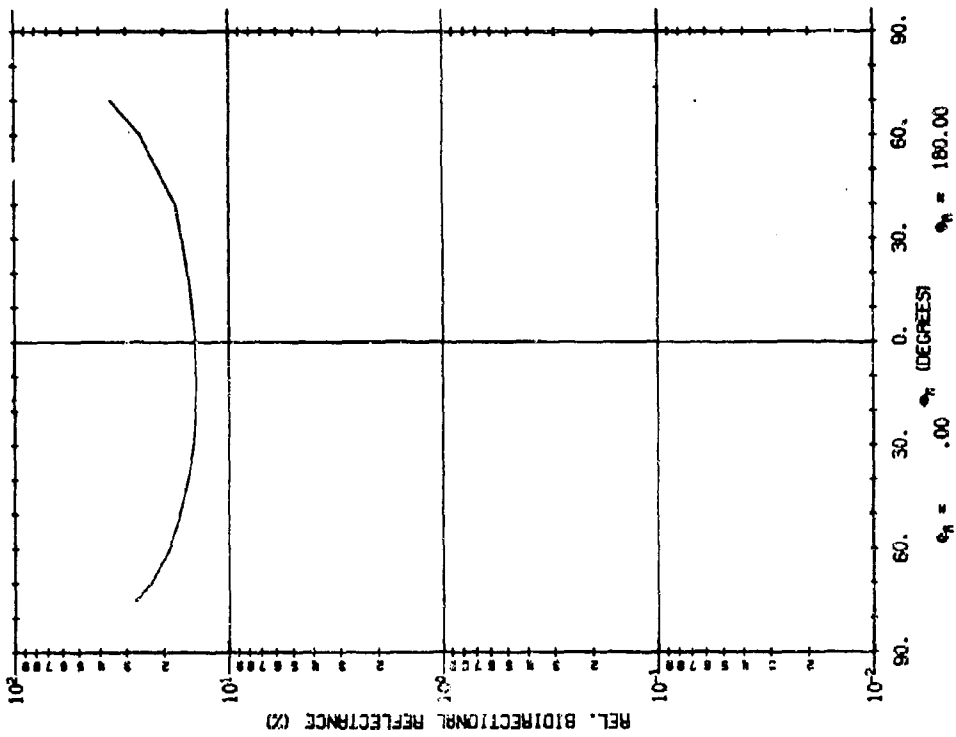
B09010 002

UT
RED CLAY, DRY
 $\lambda = 6430$
 $\phi_1 = 65.0$
 $\phi_2 = 180.0$



B09010 001

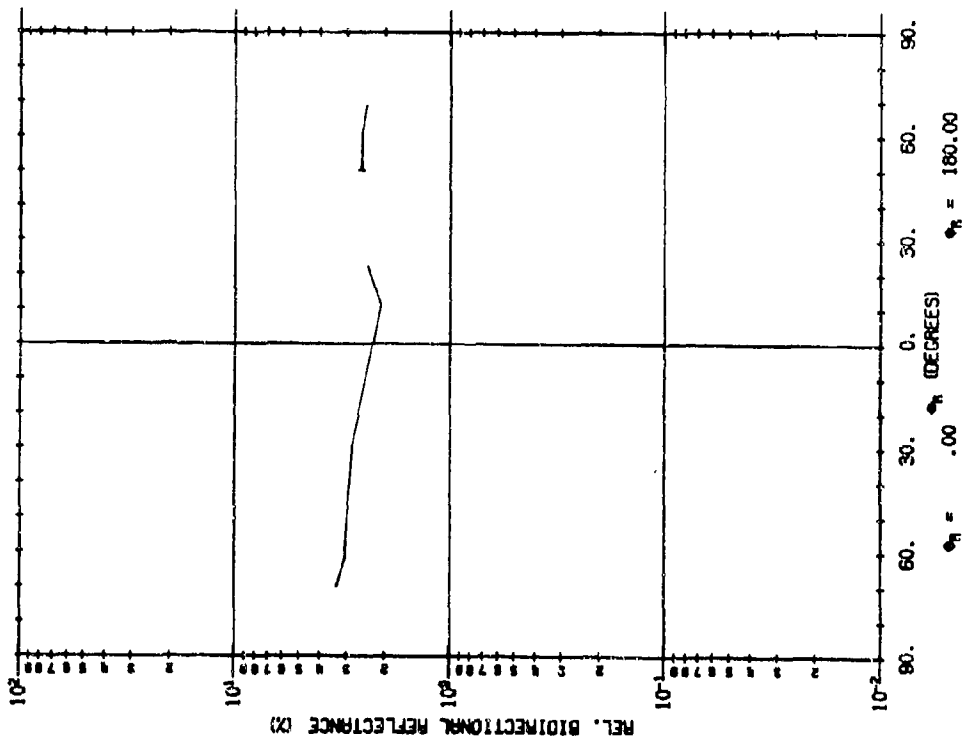
UT
RED CLAY, DRY
 $\lambda = 6430$
 $\phi_1 = 78.0$
 $\phi_2 = 180.0$



SOIL

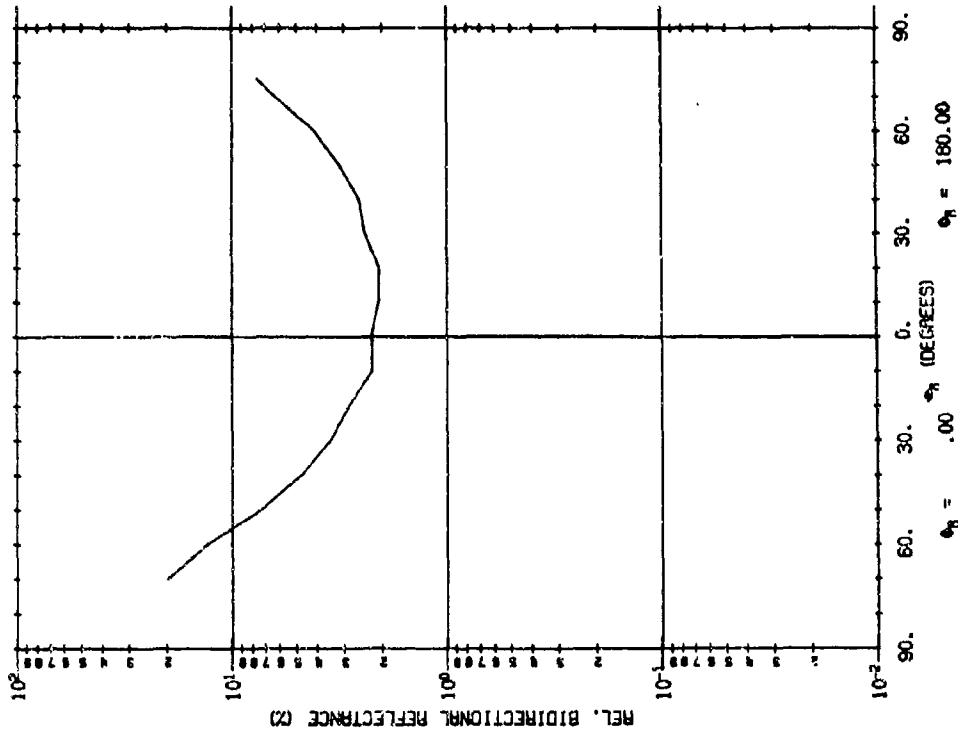
B09010 020

| = UT
RED CLAY, WET
 $\lambda = -5200$
 $\phi_1 = 45.0$
 $\phi_2 = 180.0$



B09010 018

| = UT
RED CLAY, WET
 $\lambda = -5200$
 $\phi_1 = 80.0$
 $\phi_2 = 180.0$



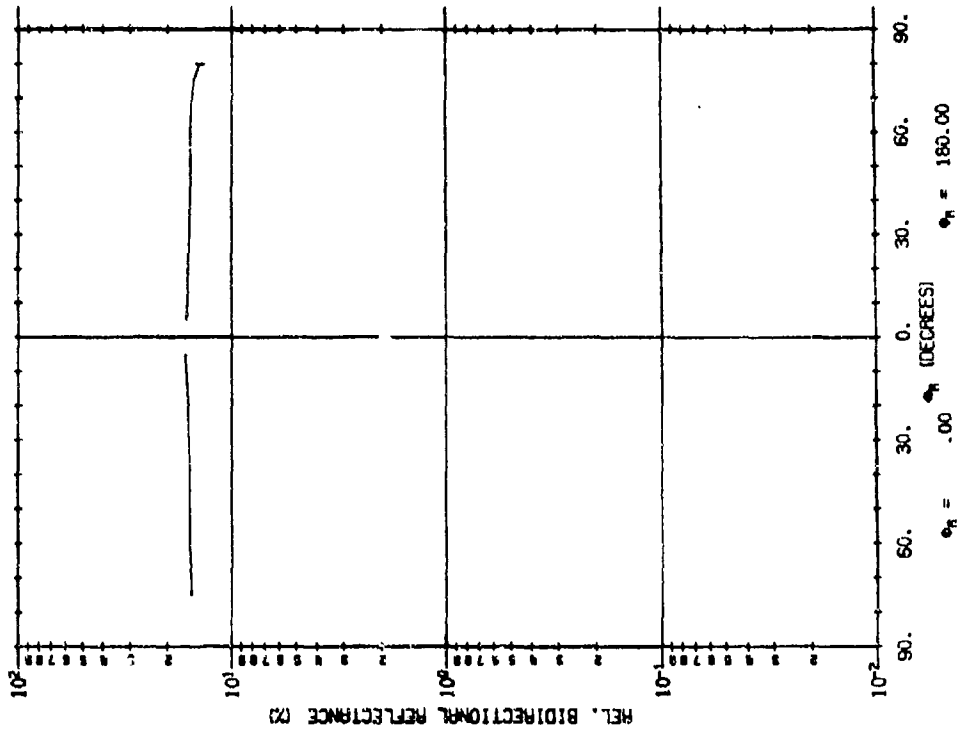
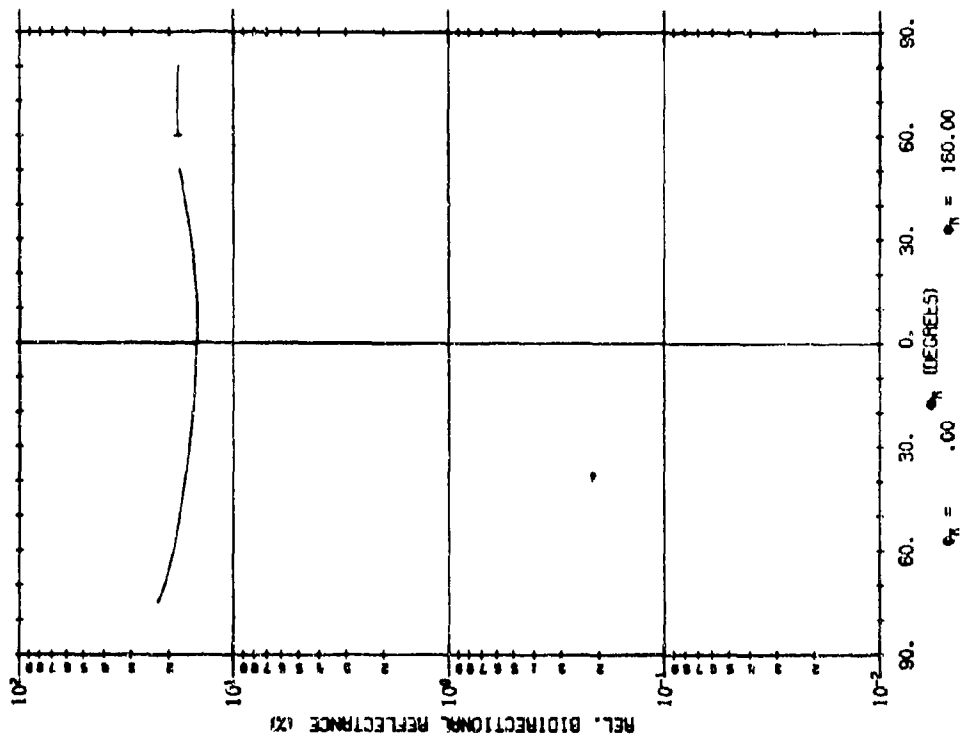
B09010 041

WHITE QUARTZ SAND
λ = .4920
φ₁ = 53.6
φ₂ = 180.0

λ = 0°

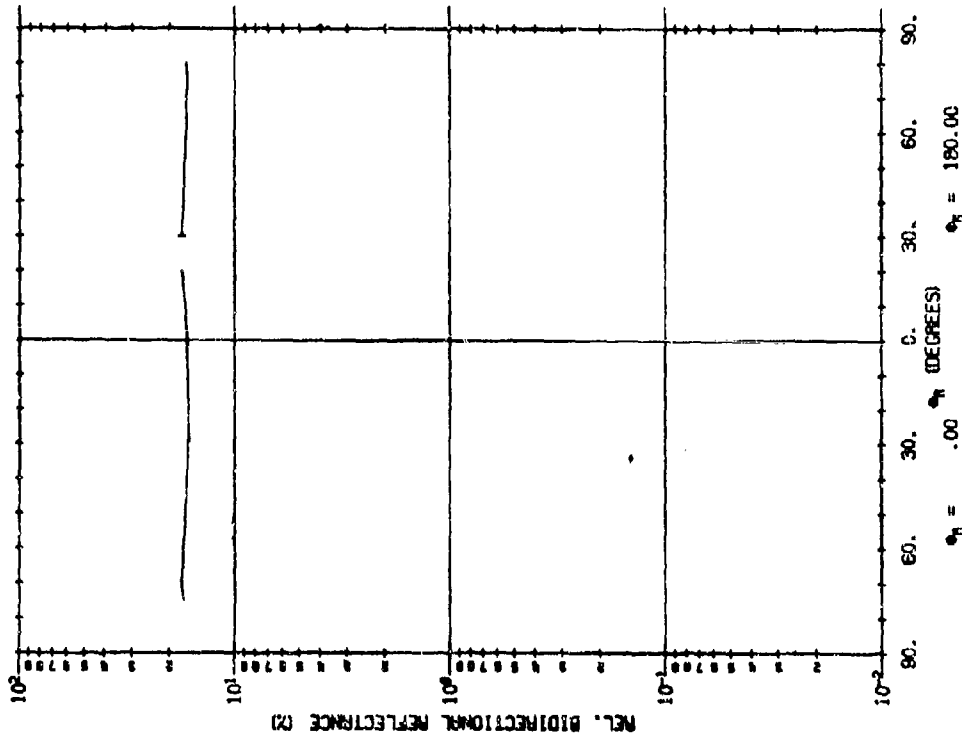
B09010 030

WHITE QUARTZ SAND
λ = .6130
φ₁ = 0.0
φ₂ = 180.0



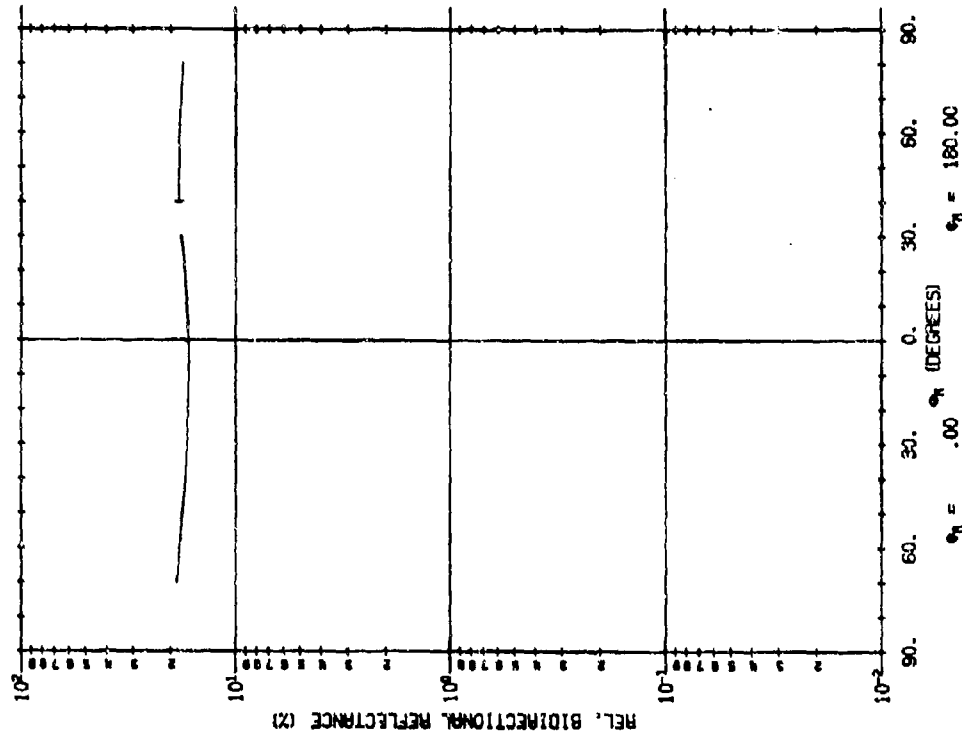
B09010 029

| - UT
 $\lambda = 6430$ WHITE QUARTZ SAND
 $\phi_1 = 23.0$
 $\phi_2 = 180.0$



B09010 028

| - UT
 $\lambda = 6430$ WHITE QUARTZ SAND
 $\phi_1 = 27.0$
 $\phi_2 = 180.0$



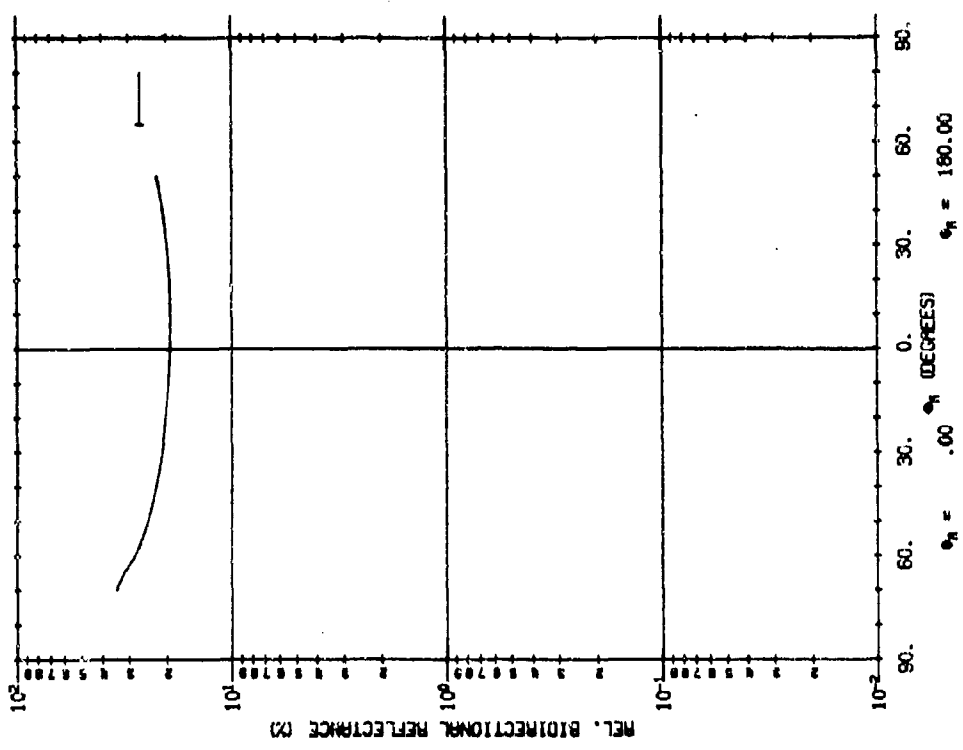
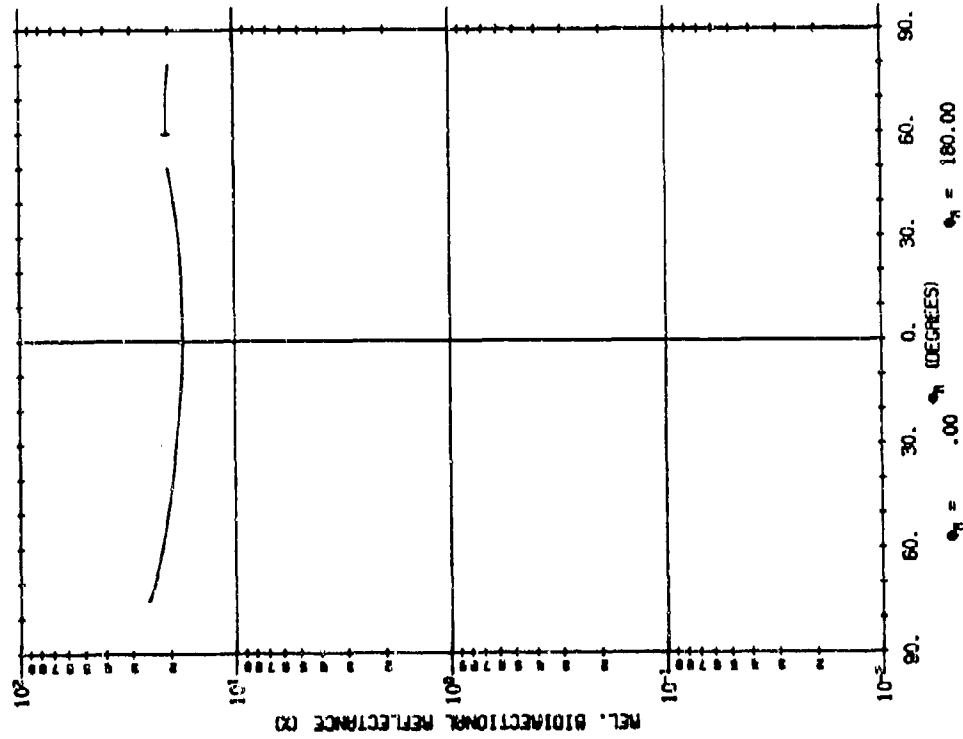
B09010 027

| - UT
λ = .6430
φ₁ = 53.0
φ₂ = 180.0

WHITE QUARTZ SAND

B09010 026
| - UT
λ = .6430
φ₁ = 66.0
φ₂ = 180.0

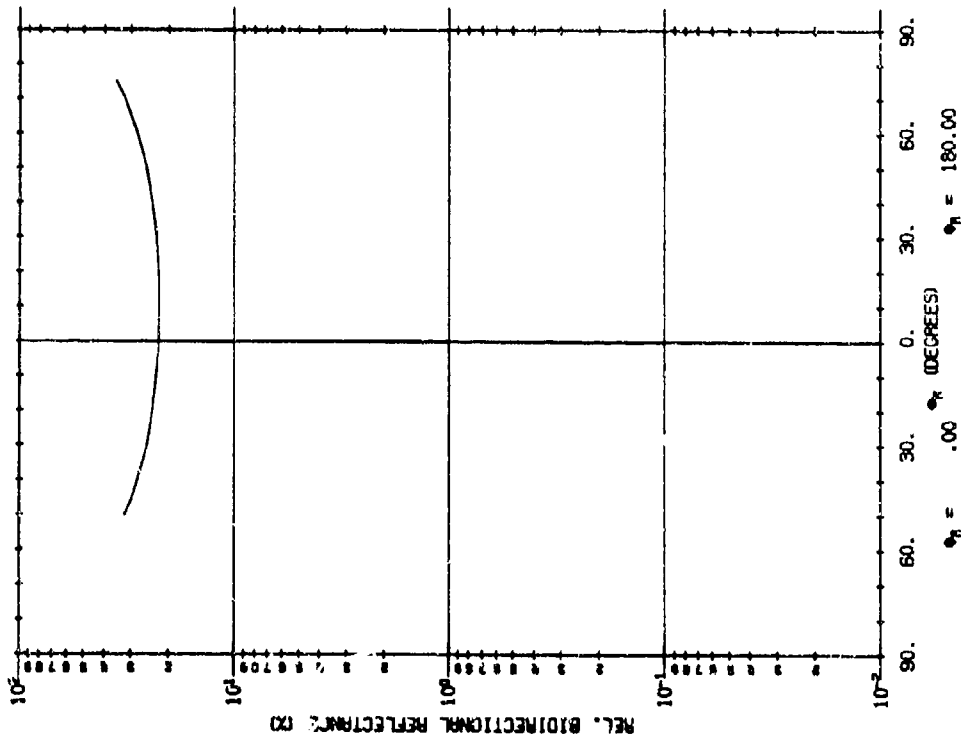
WHITE QUARTZ SAND



SOIL

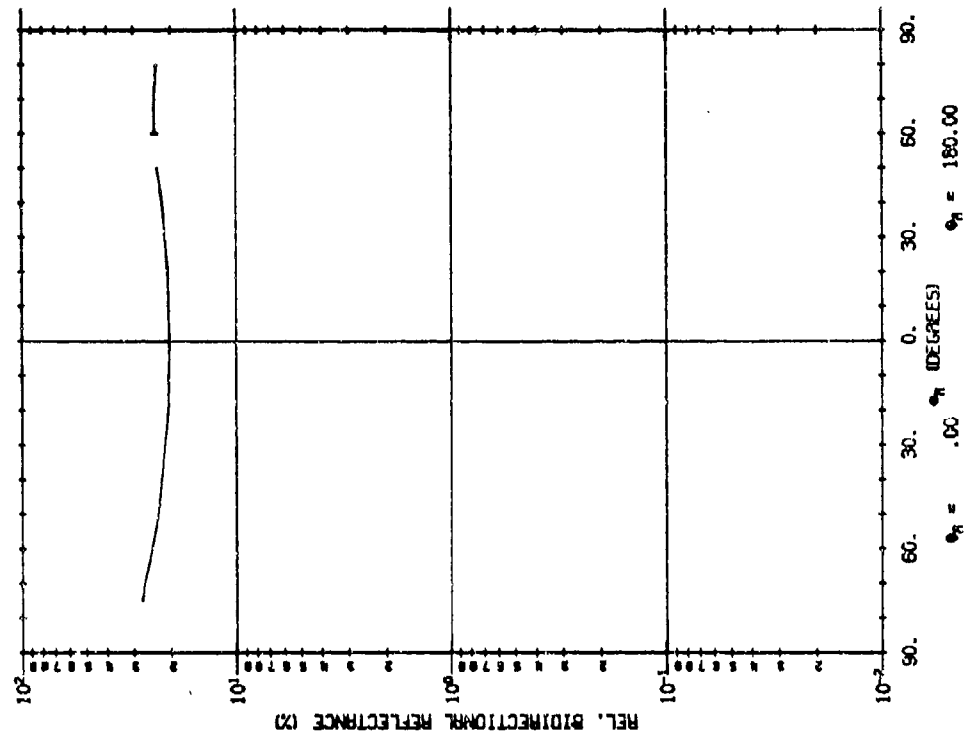
B09010 025

λ = 0.7
λ = 0.6430
φ₁ = 78.0
φ₂ = 180.0
WHITE QUARTZ SAND



B09010 039

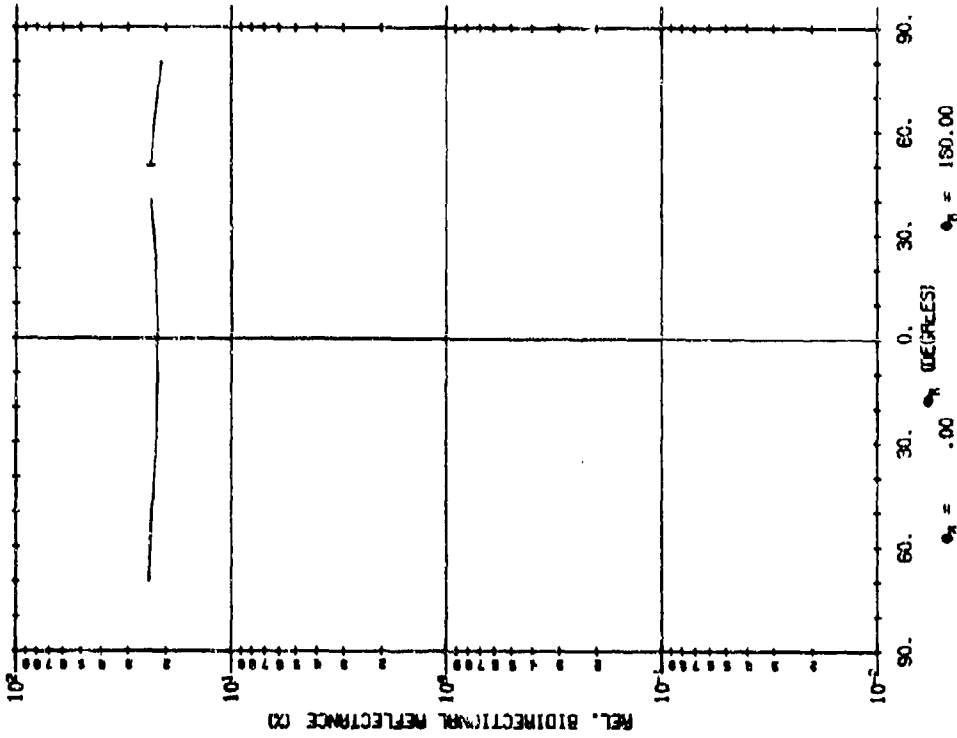
λ = 0.7
λ = 0.7940
φ₁ = 53.0
φ₂ = 180.0
WHITE QUARTZ SAND



B09010 045

λ = 0.5200
φ₁ = 50.0
φ₂ = 180.0

WHITE STY-RO SAND

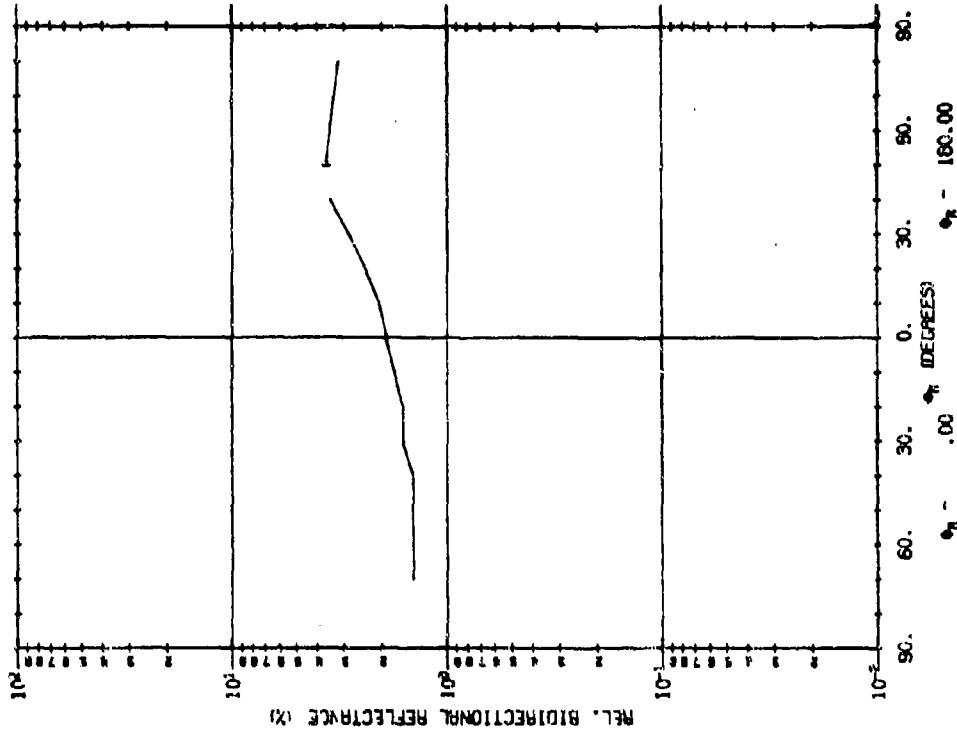


φ₁ = .00 φ₂ = 180.00

B09010 046

λ = 0.5200
φ₁ = 50.0
φ₂ = 180.0

BLACK LOAN SOIL



φ₁ = .00 φ₂ = 180.00

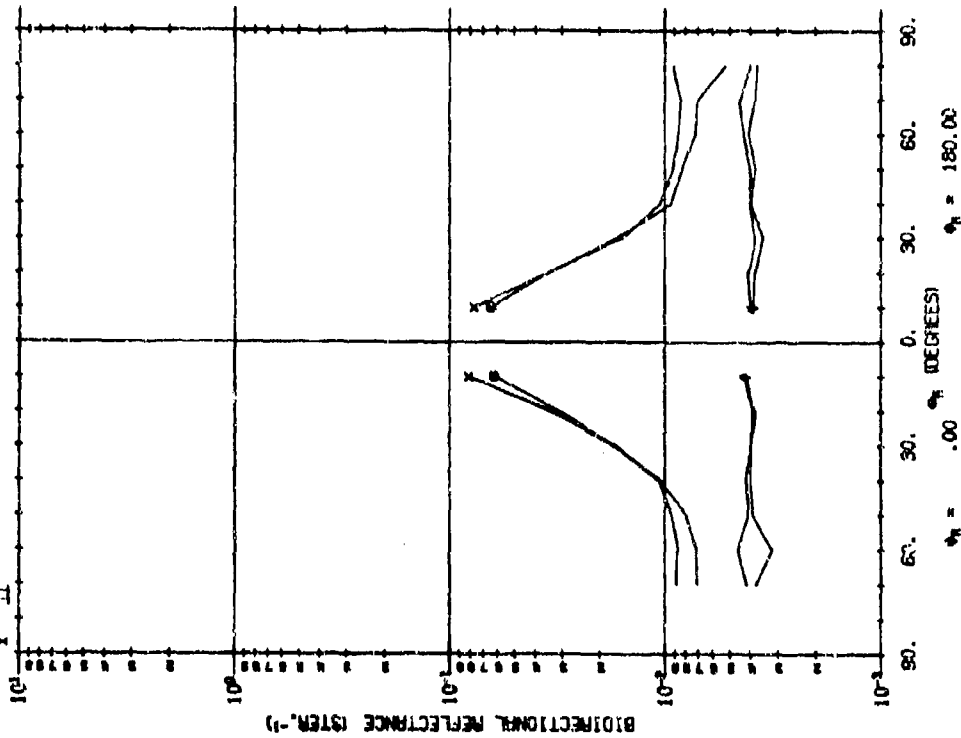
SOIL

VEGETATION

R01324 001

MATURE MULBERRY LEAF, 2 HOURS OLD

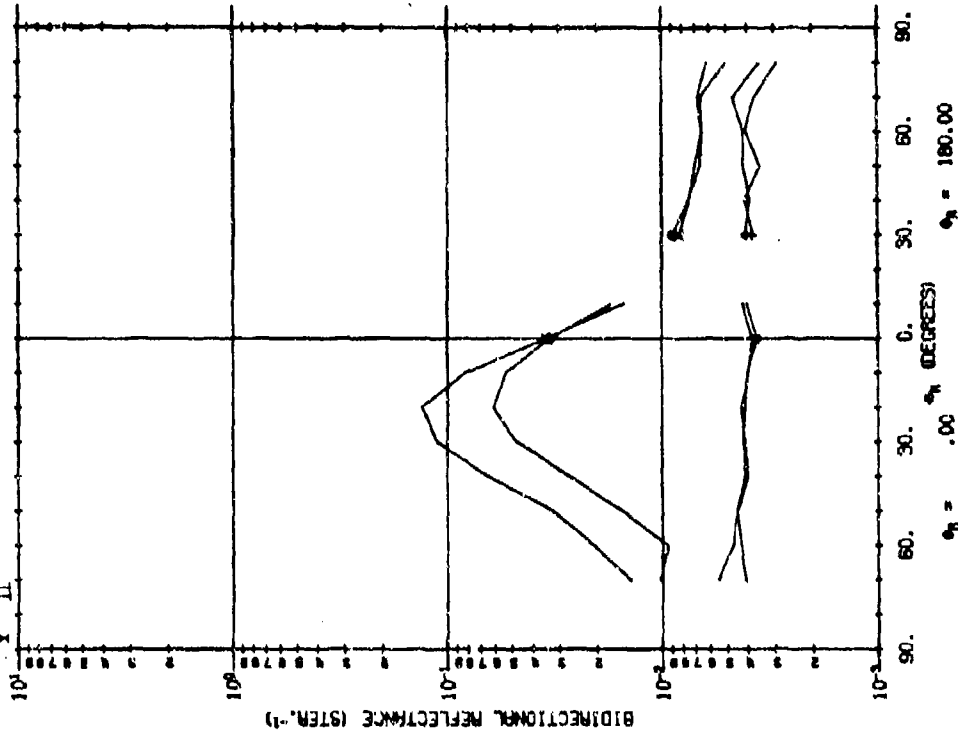
0 || $\theta_1 = 0.0$
 + || $\theta_2 = 180.0$
 x || $\lambda = 0.63$



R01324 001

MATURE MULBERRY LEAF, 2 HOURS OLD

0 || $\theta_1 = 20.0$
 + || $\theta_2 = 180.0$
 x || $\lambda = 0.63$

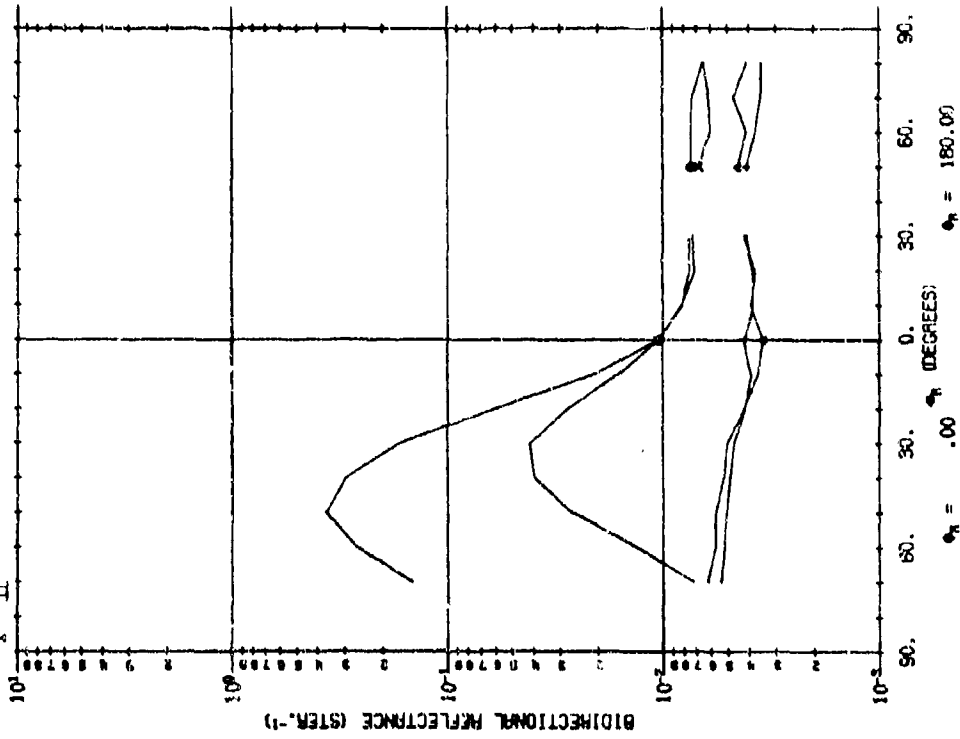


VEGETATION

R01324 001

MATURE MILBERRY LEAF, 2 MONTHS OLD

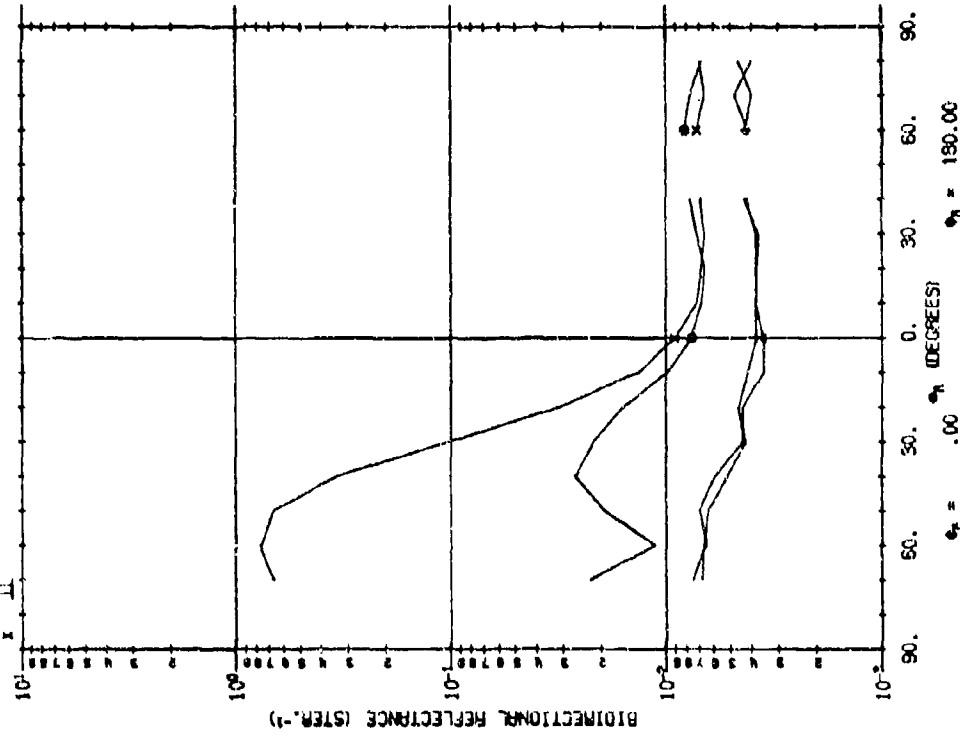
0 || $\theta_1 = 40.0$
+ || $\theta_1 = 180.0$
A || $\lambda = 0.63$
X ||



R01324 001

MATURE MILBERRY LEAF, 2 MONTHS OLD

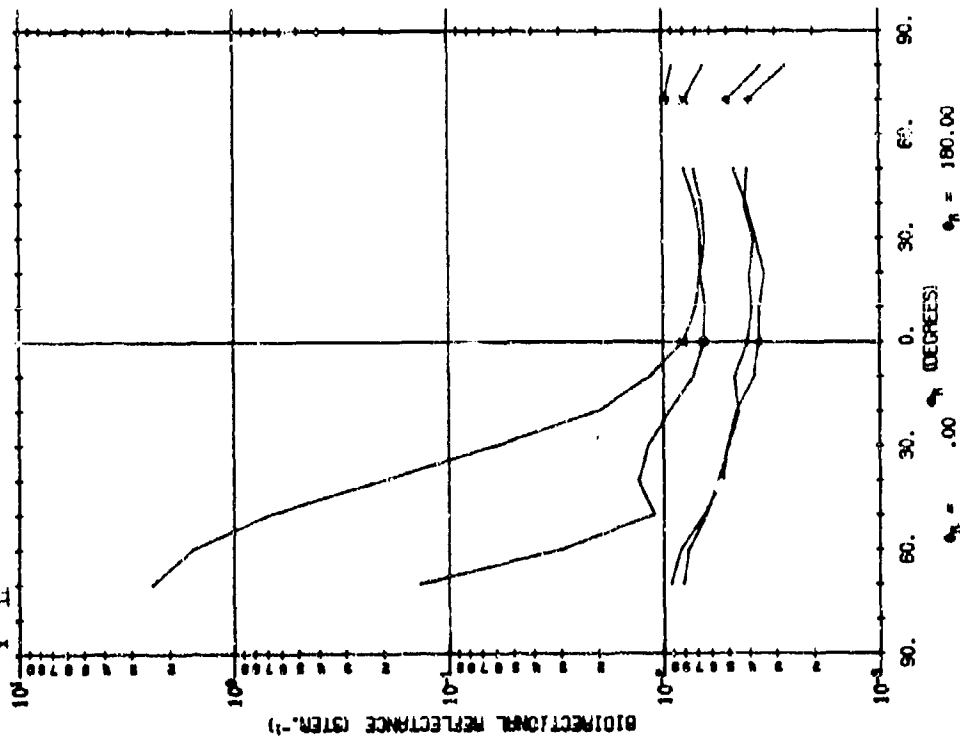
0 || $\theta_1 = 50.0$
+ || $\theta_1 = 180.0$
A || $\lambda = 0.63$
X ||



R01324 001

MATURE WETLAND: LEAF, 2 BOOTS OLD

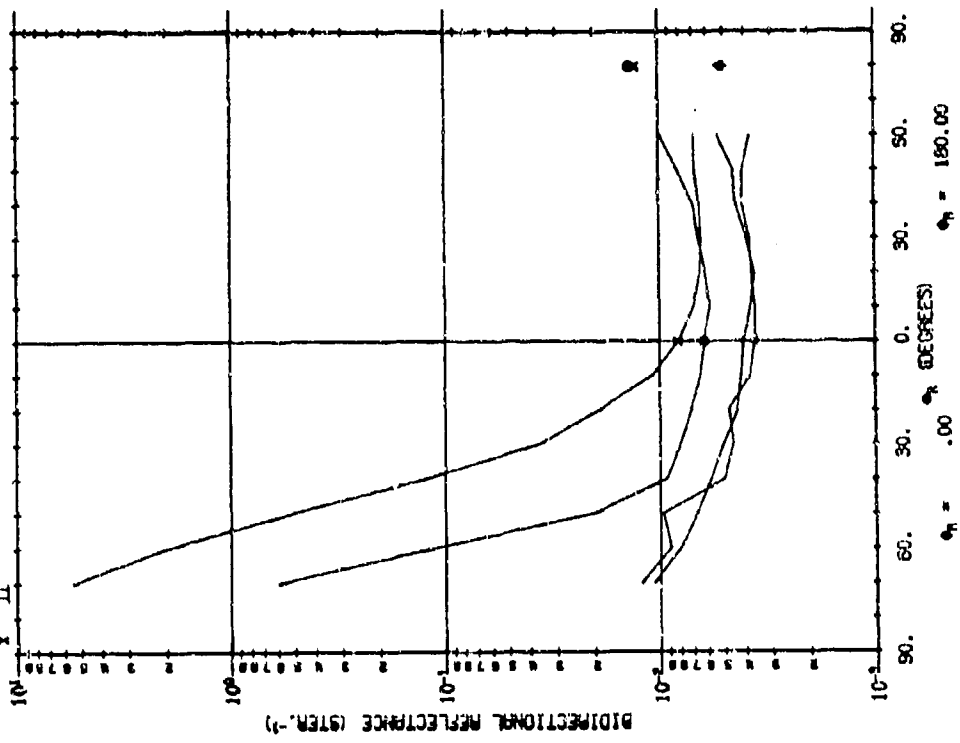
0 II $\phi_1 = 50.0$
 + II $\phi_1 = 100.0$
 A II $\phi_1 = 180.0$
 X II $\lambda = 0.63$



R01324 001

MATURE WETLAND: LEAF, 2 BOOTS OLD

0 II $\phi_1 = 70.0$
 + II $\phi_1 = 100.0$
 A II $\phi_1 = 180.0$
 X II $\lambda = 0.63$

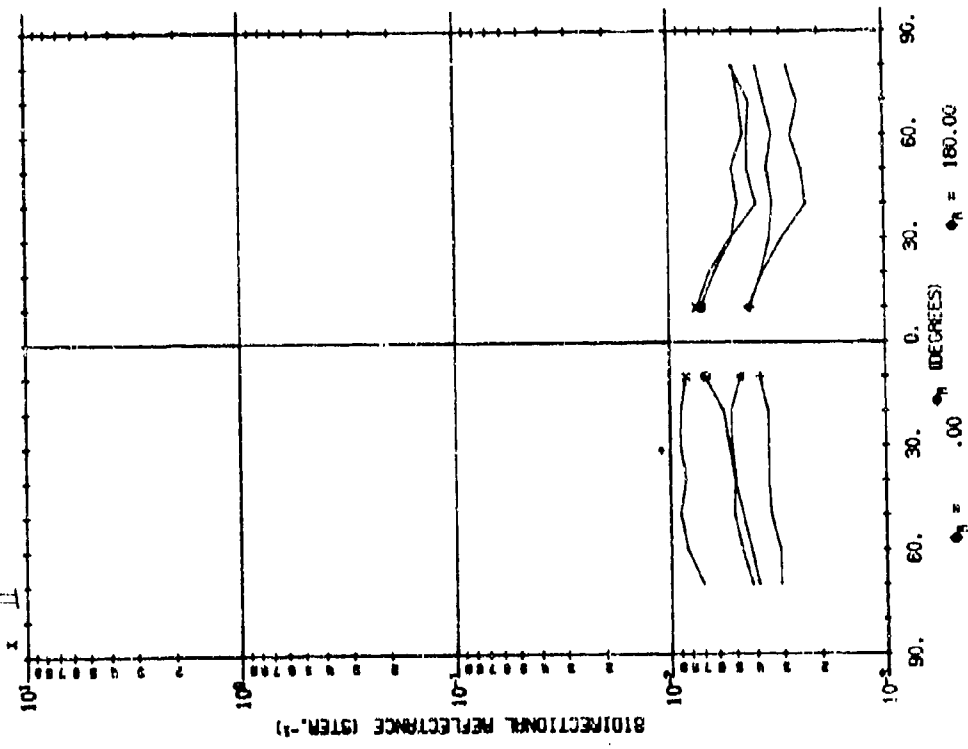


VEGETATION

R01327 001

MEADOW BLITE GRASS GROWING IN SANDY SOIL

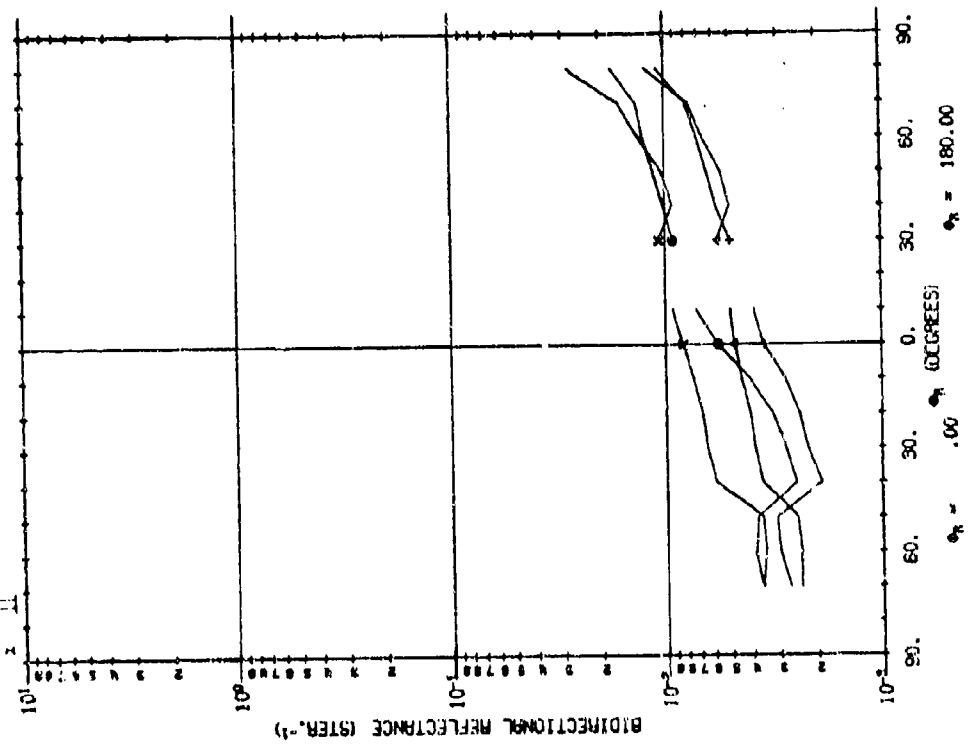
0 | | $\phi_1 = 0.0$
 + | | $\phi_2 = 180.0$
 x | | $\lambda = 0.63$



R01327 001

MEADOW BLITE GRASS GROWING IN SANDY SOIL

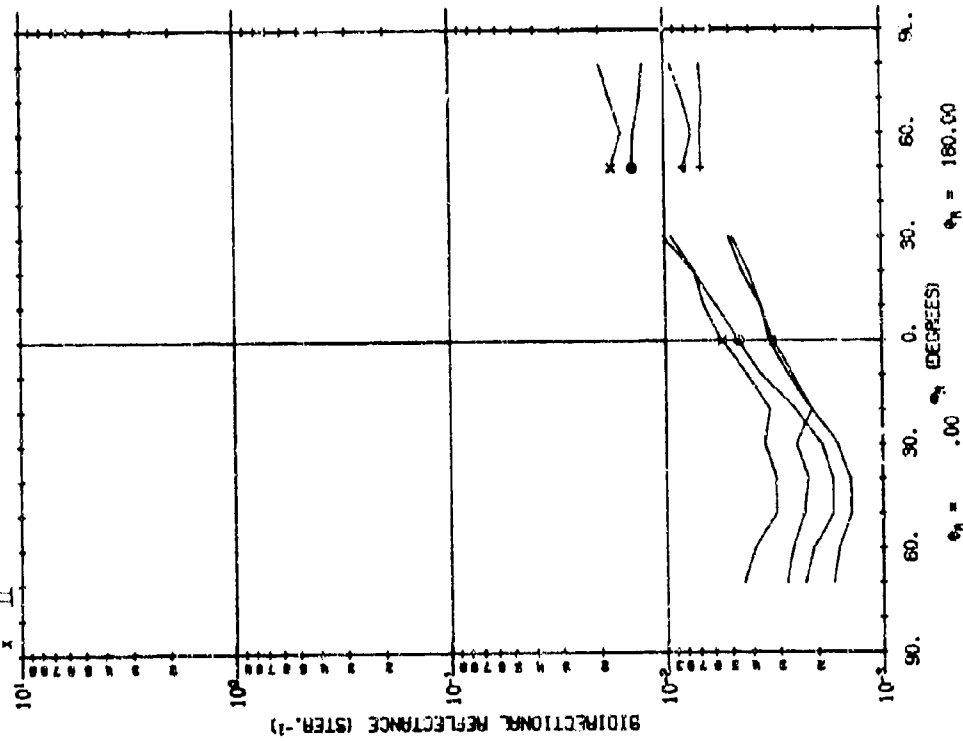
0 | | $\phi_1 = 20.0$
 + | | $\phi_2 = 180.0$
 x | | $\lambda = 0.63$



A01327 001

MEXICAN BLUZE GRASS GROWING IN SANDY SOIL

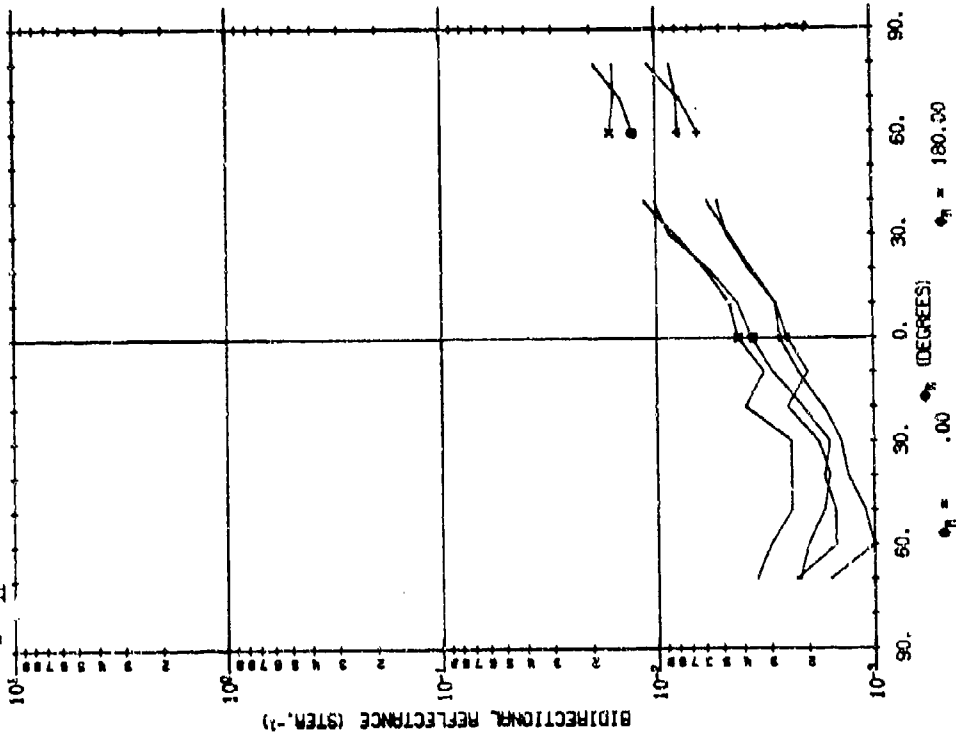
0 | | $\theta_1 = 40.0$
+ | | $\theta_1 = 180.0$
△ | | $\lambda = 0.63$
x | |



A01327 001

MEXICAN BLUZE GRASS GROWING IN SANDY SOIL

0 | | $\theta_1 = 50.0$
+ | | $\theta_1 = 180.0$
△ | | $\lambda = 0.63$
x | |

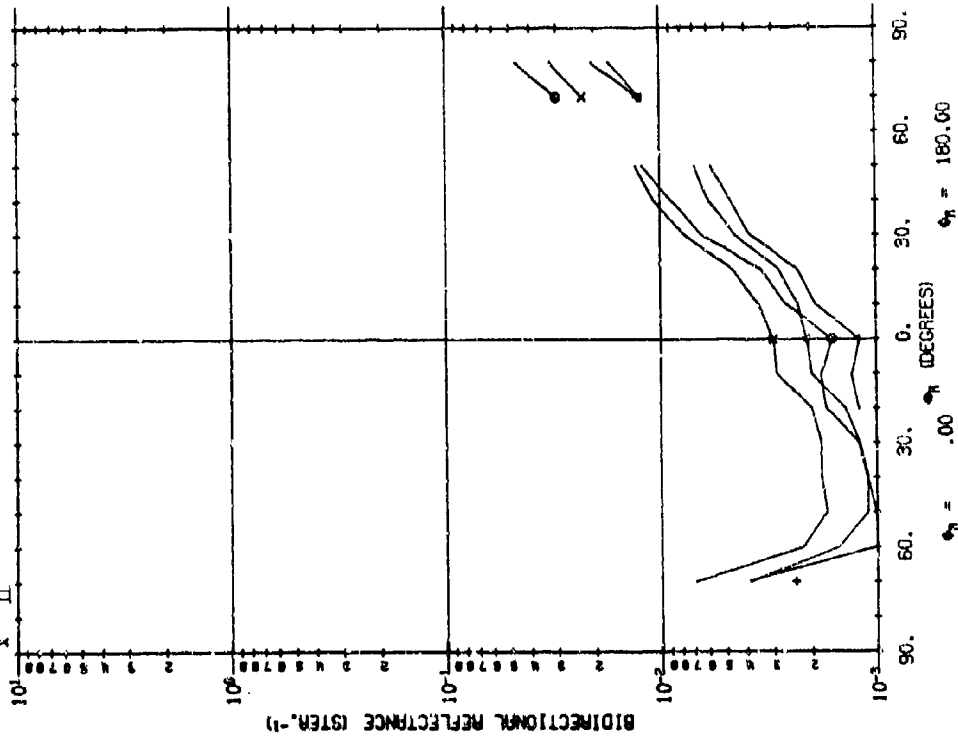


VEGETATION

R01327 001

MERION BLVD. GRASS GROWING IN SANDY SOIL

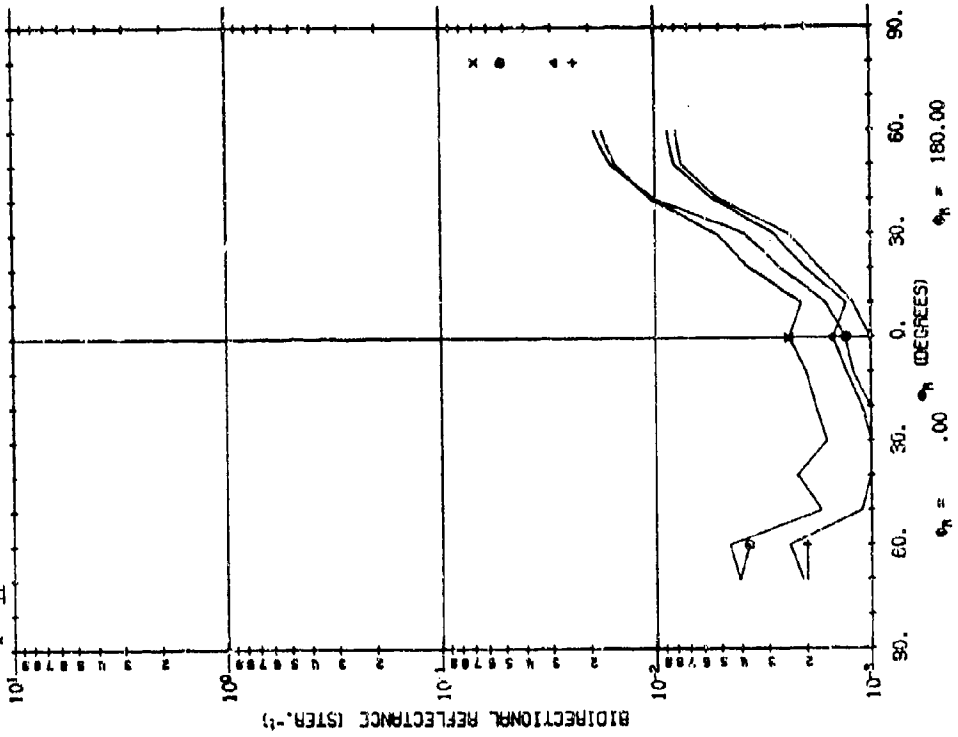
0 || $\phi_1 = 60.0$
 + || $\phi_2 = 180.0$
 Δ || $\lambda_1 = 0.53$
 x ||



R01327 001

MERION BLVD. GRASS GROWING IN SANDY SOIL

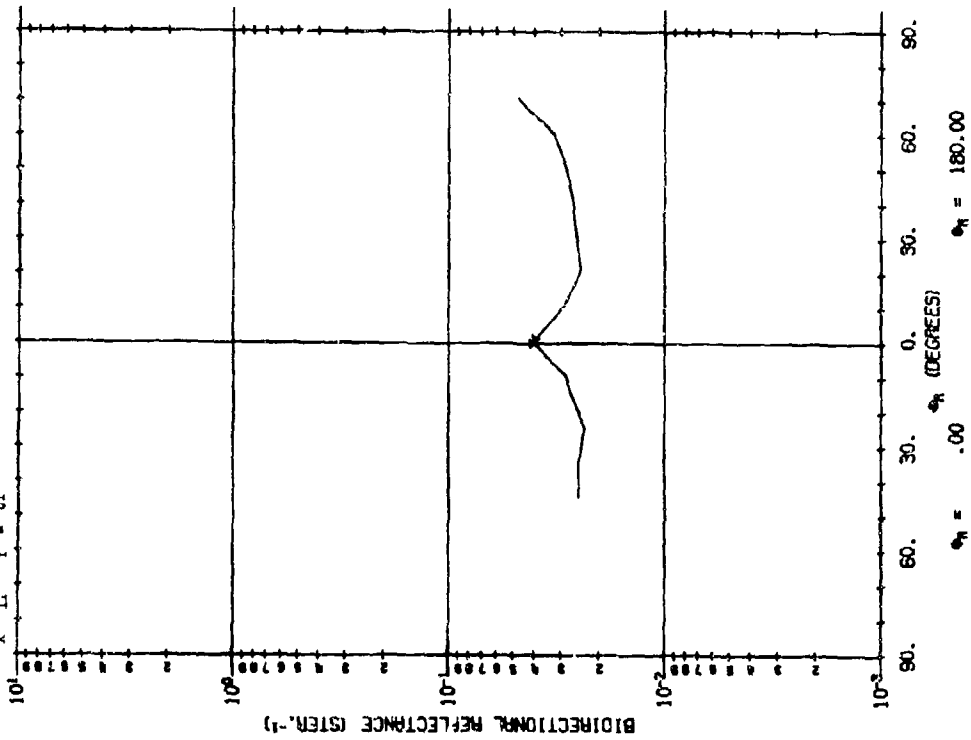
0 || $\phi_1 = 70.0$
 + || $\phi_2 = 180.0$
 Δ || $\lambda_1 = 0.63$
 x ||



R01516 003

Tree Bark

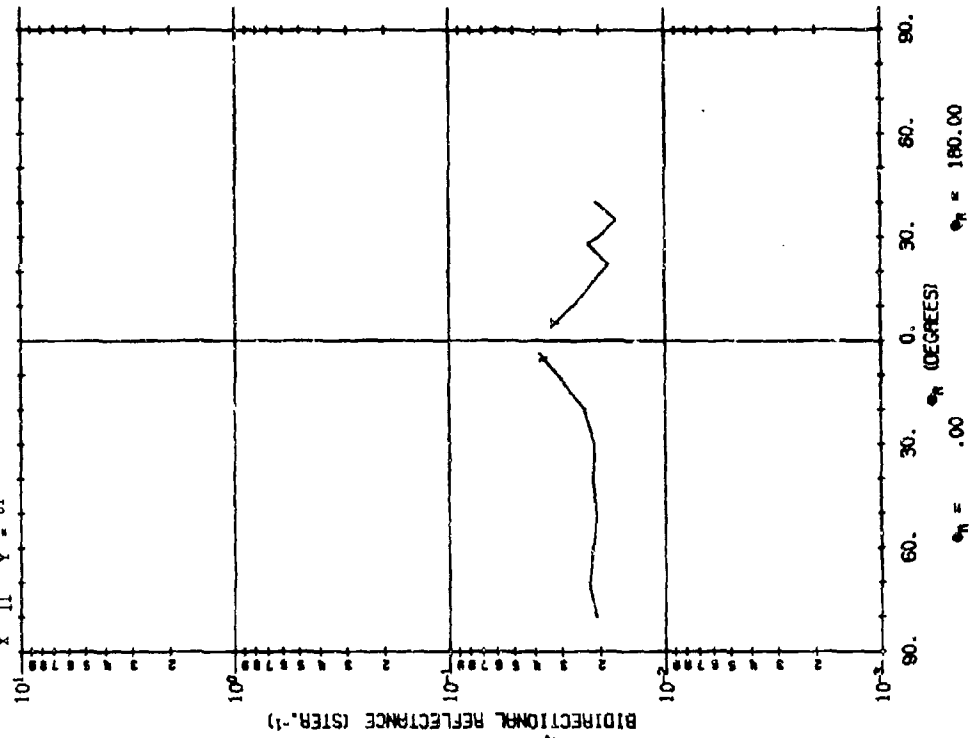
0 || 28 = 1.10
+ || $\phi_1 = \phi_r$
△ || $\lambda = 10.6$
X || Y = UT



R01516 003

Tree Bark

0 || $\phi_1 = 0.0$
+ || $\phi_1 = -180.0$
△ || $\lambda = 10.6$
X || Y = UT

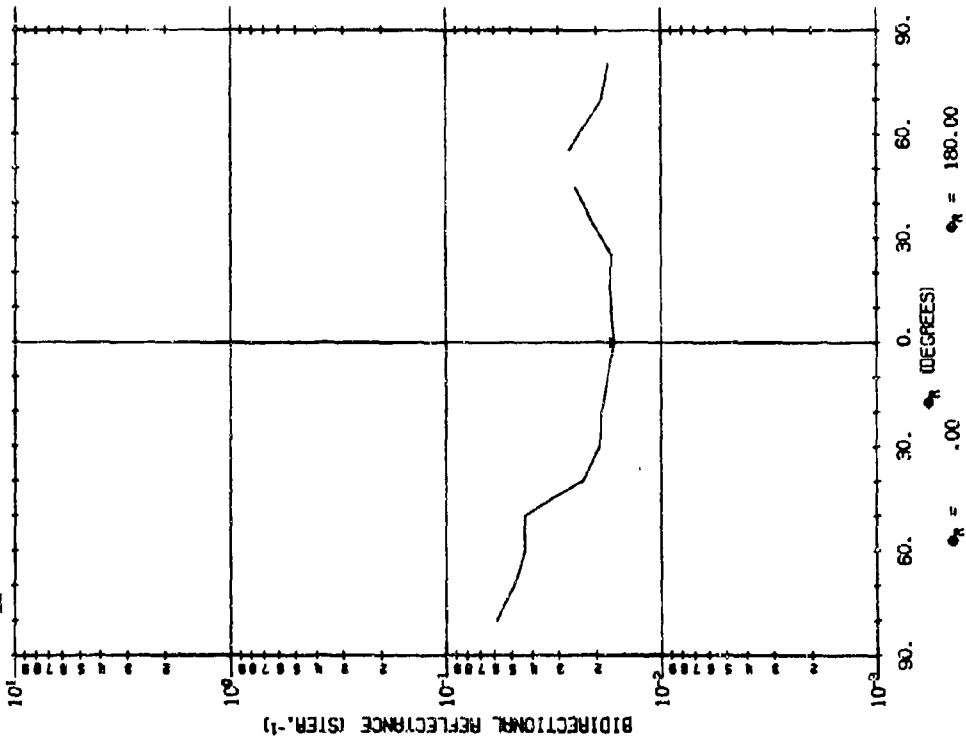


VEGETATION

A01516 003

Tree Bark

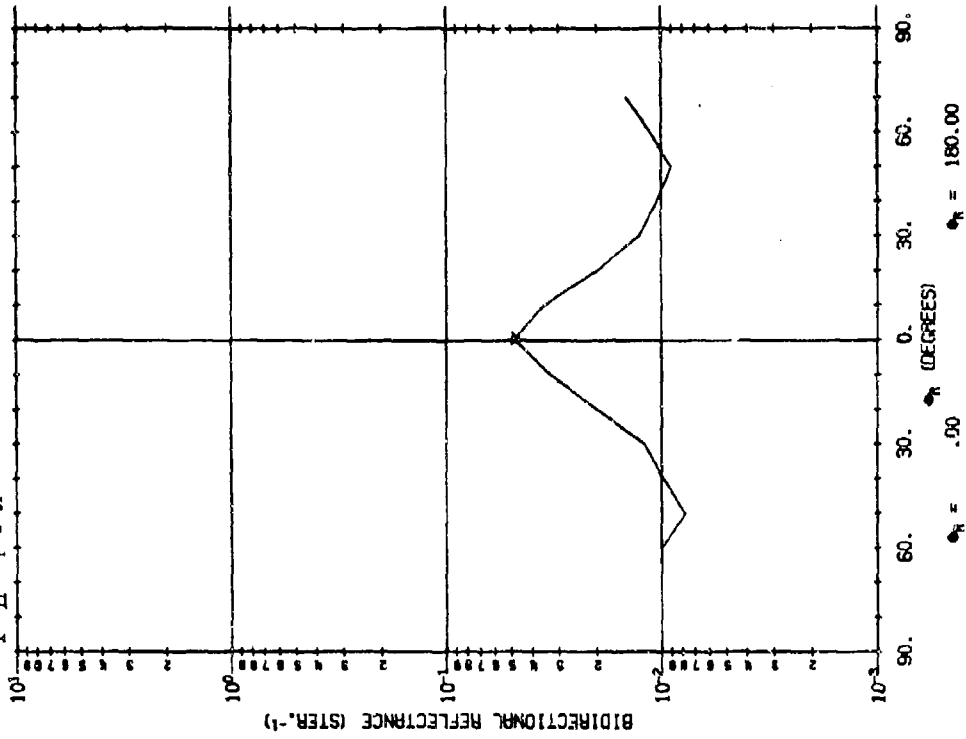
0 || $\theta_1 = 50.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 16.6$
 X || $\gamma = UT$



A01517 002

Plus Tree Bark

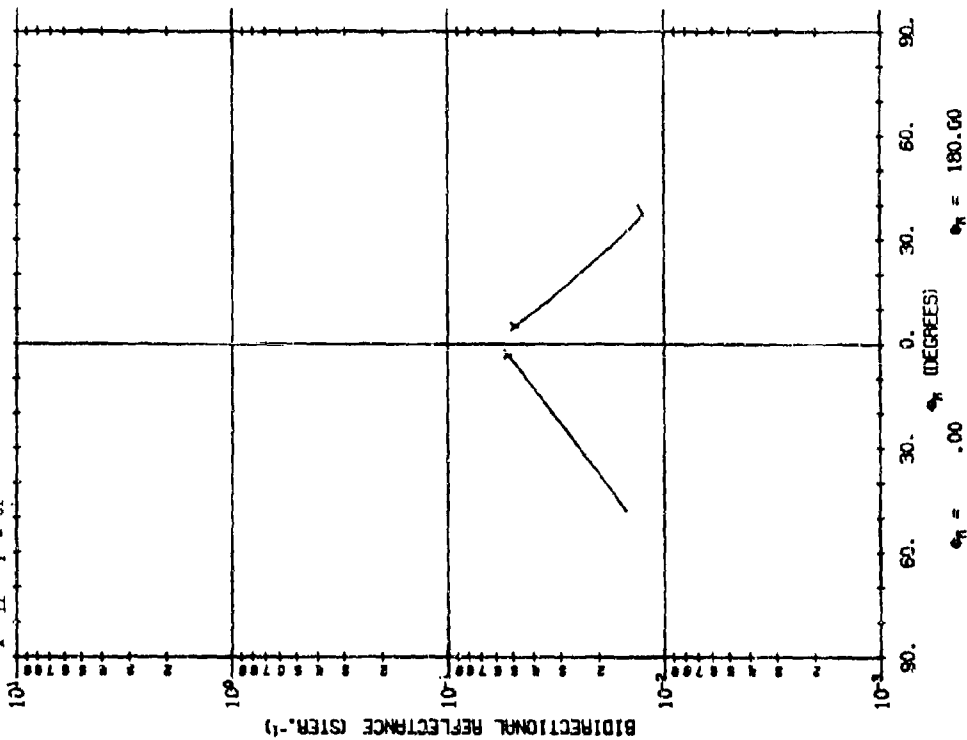
0 || $\theta_1 = 1.10$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 16.6$
 X || $\gamma = UT$



A01517 002

Pine Tree Bark

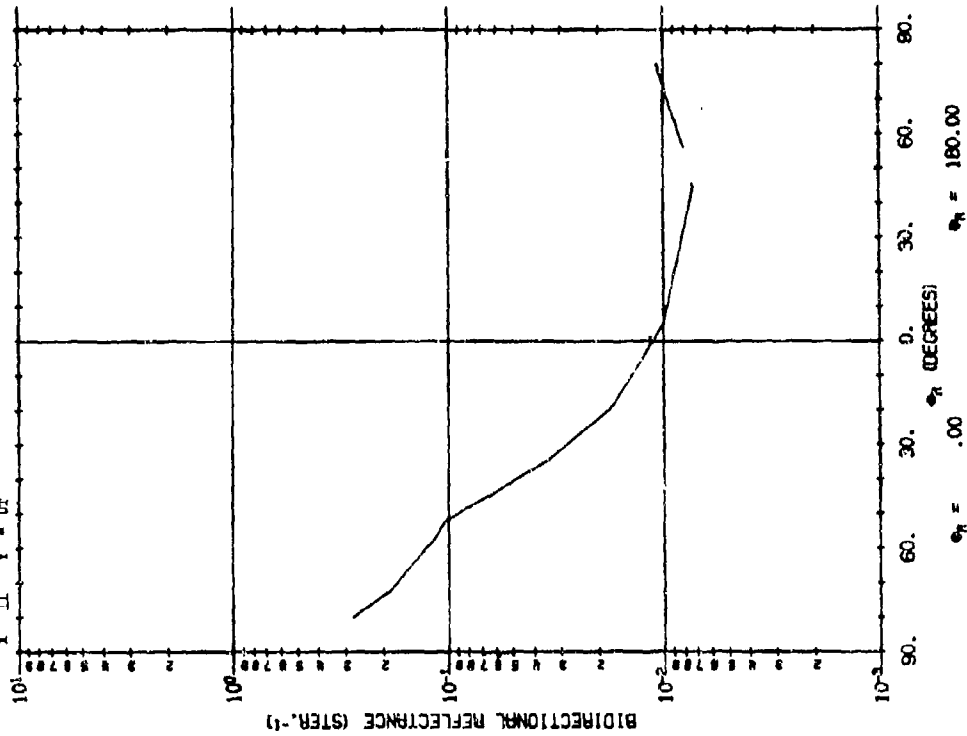
0 // $\theta_1 = 0.0$
+ // $\theta_2 = 180.0$
A // $\lambda = 10.6$
X // $Y = VC$



A01517 002

Pine Tree Bark

0 // $\theta_1 = 50.0$
+ // $\theta_2 = 180.0$
A // $\lambda = 10.6$
X // $Y = DT$



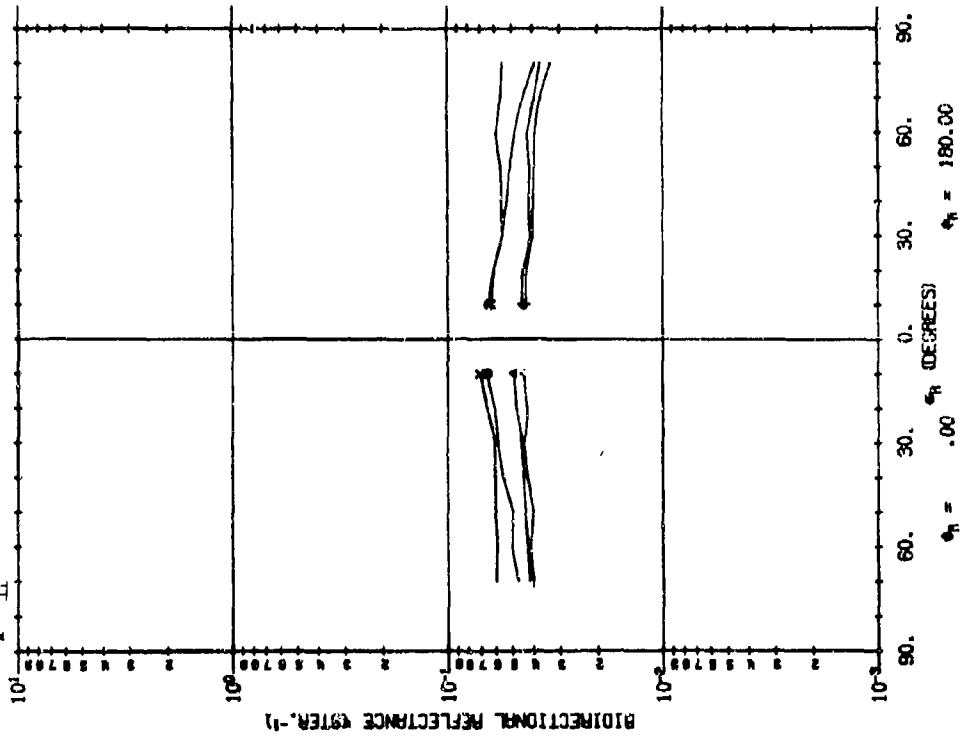
VEGETATION

**ASPHALT AND
CONCRETE**

A01329 001

CONCRETE

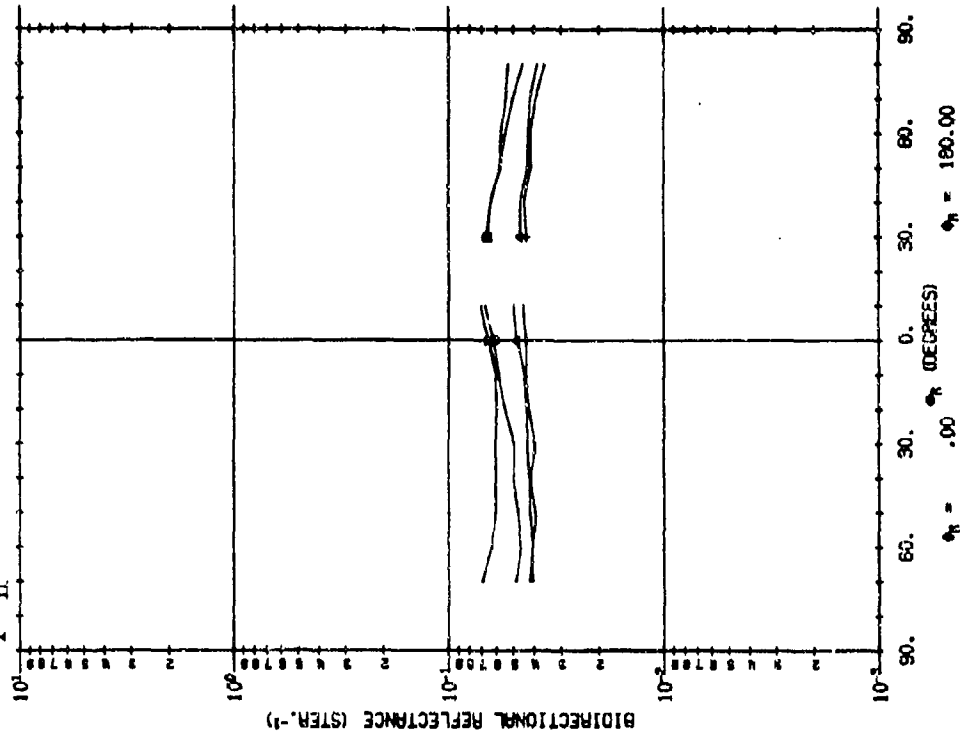
0 || $\theta_1 = 0.0$
+ || $\theta_1 = 180.0$
△ || $\lambda = 0.63$
X ||



A01329 001

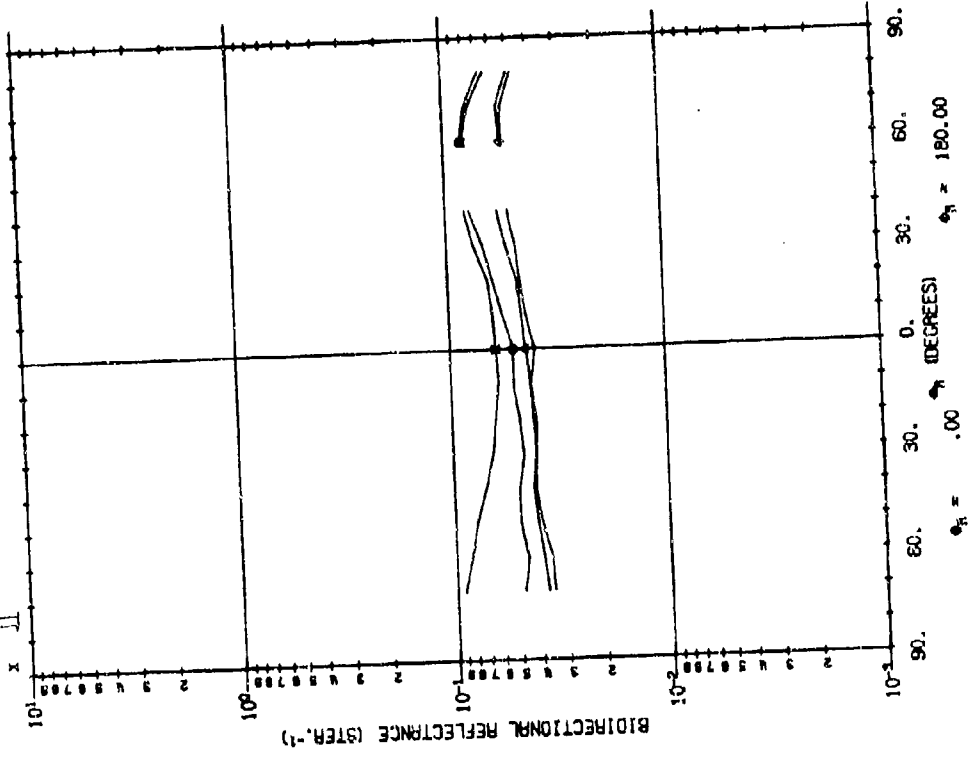
CONCRETE

0 || $\theta_1 = 20.0$
+ || $\theta_1 = 180.0$
△ || $\lambda = 0.63$
X ||



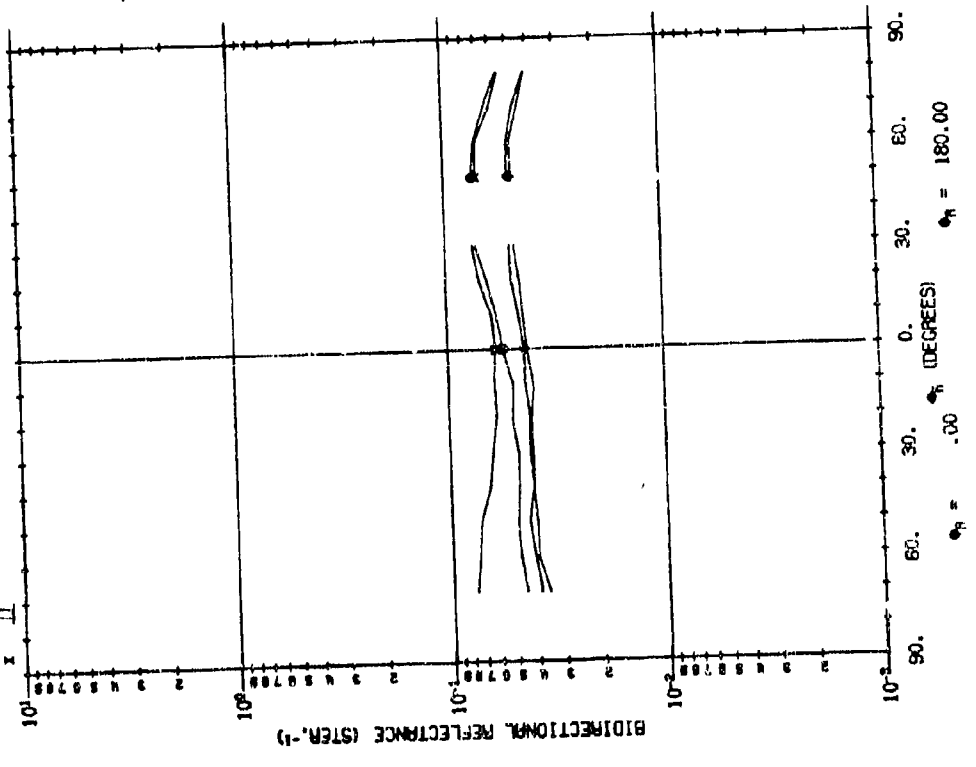
A01329 001
 CONCRETE

$\epsilon_1 = 50.0$
 $\epsilon_2 = 190.0$
 $\lambda = 0.63$



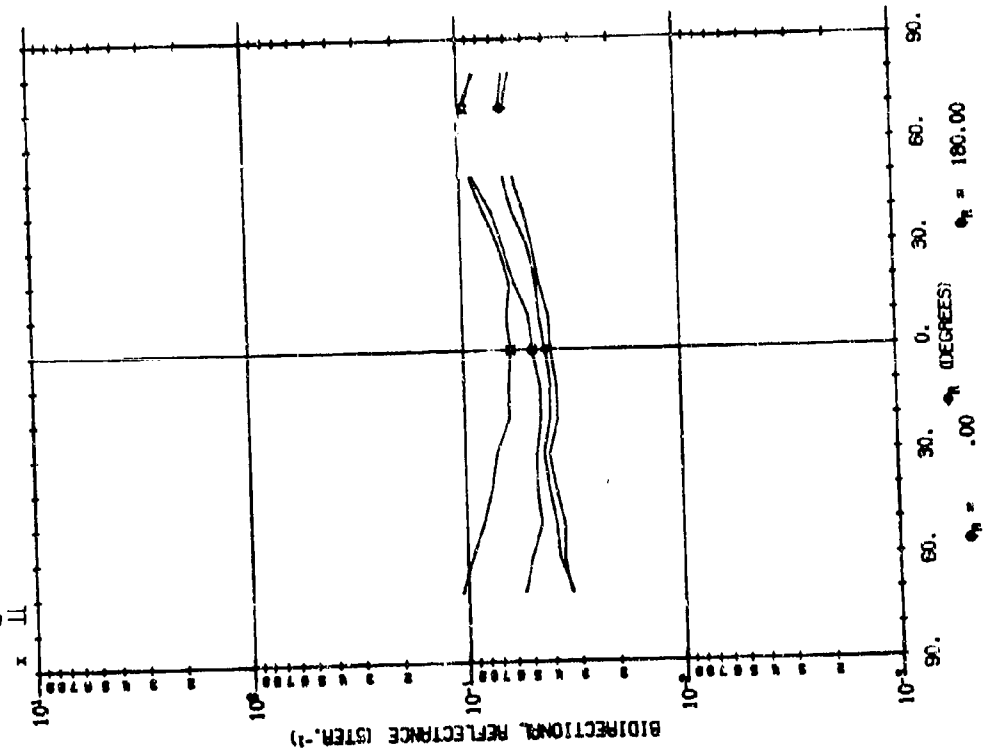
A01329 001
 CONCRETE

$\epsilon_1 = 40.0$
 $\epsilon_2 = 180.0$
 $\lambda = 0.63$



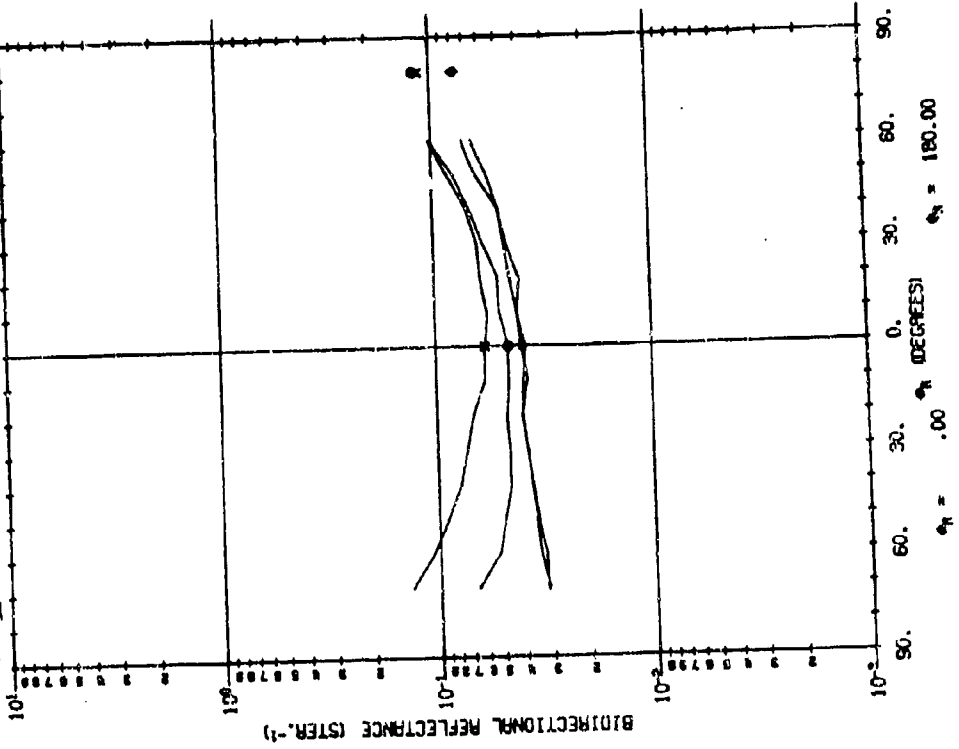
A01329 001
 0 II I - 60.0
 + II II - 180.0
 Δ II II - 0.63
 x II

CONCRETE



A01329 001
 0 II I - 70.0
 + II II - 180.0
 Δ II II - 0.63
 x II

CONCRETE

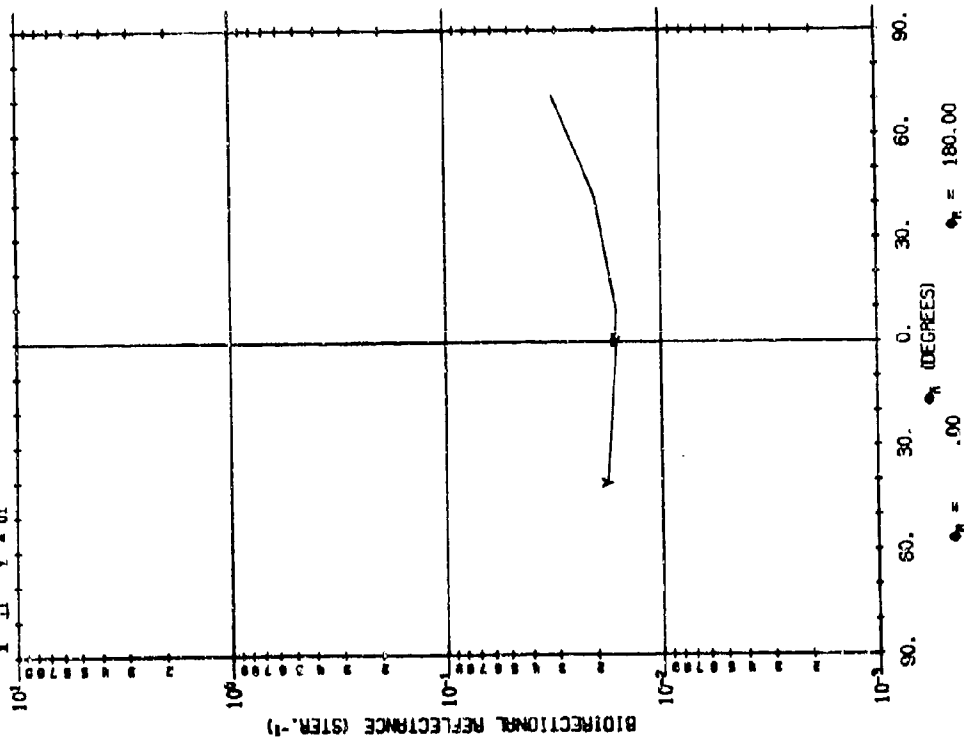


ASPHALT AND CONCRETE

R01530 002

Fine Textured Concrete

0 || 28 = 1.30
+ || 1 = 0.4
A || 1 = 10.6
X || Y = 0%

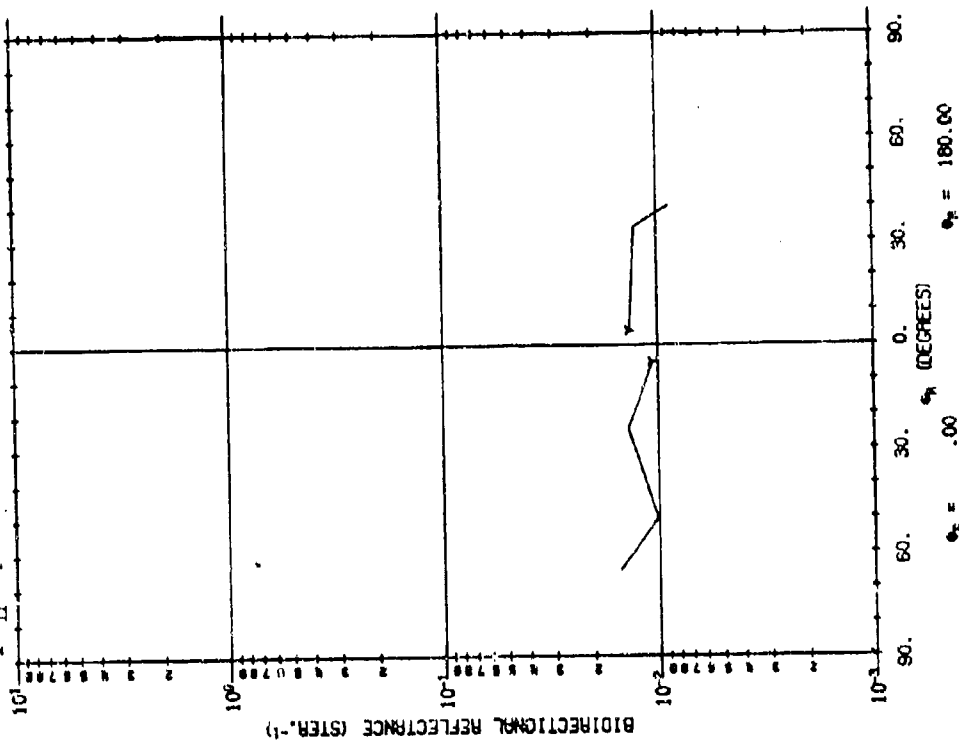


$\phi_r = .00$ $\phi_t = 180.00$

R01530 002

Fine Textured Concrete

0 || 31 = 0.0
+ || 1 = 180.0
A || 1 = 10.6
X || Y = 0%

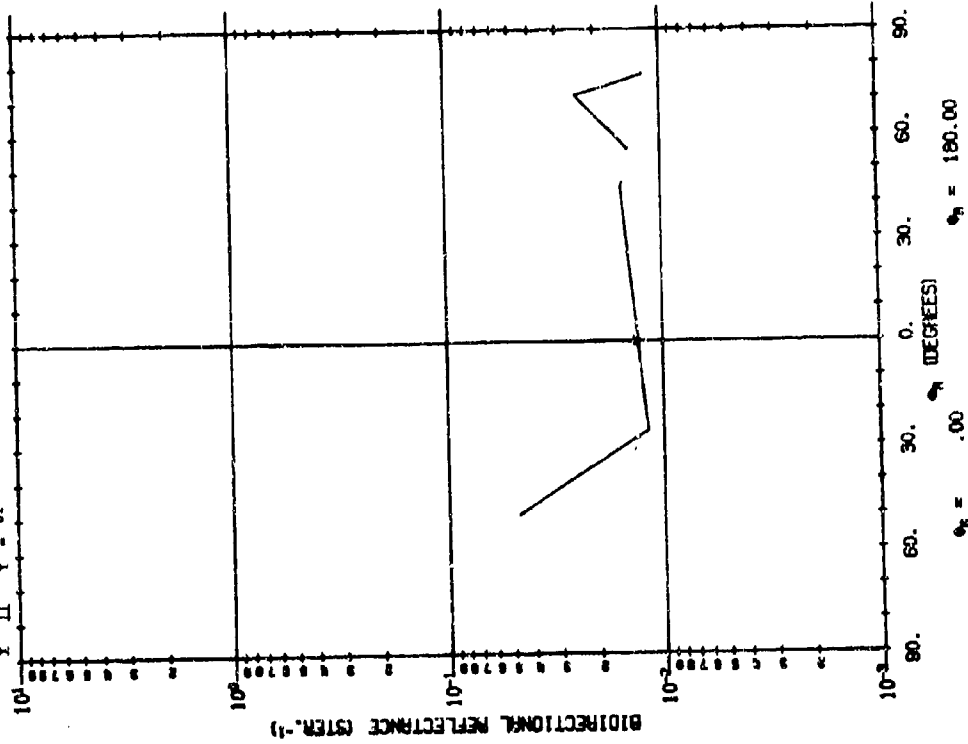


$\phi_r = .00$ $\phi_t = 180.00$

R01530 002

Fine Textured Concrete

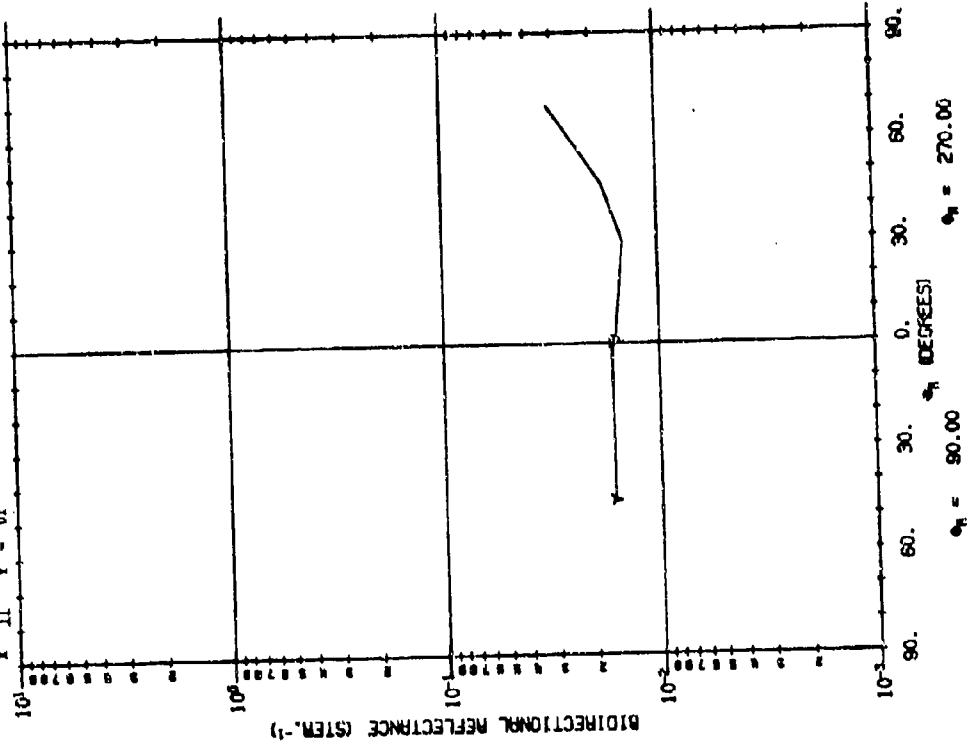
0 || $\phi_1 = 50.0$
+ || $\phi_2 = 100.0$
A || $\lambda = 10.6$
X || Y - VT



R01530 002

Fine Textured Concrete

0 || $\phi_1 = 1.10$
+ || $\phi_2 = 1.10$
A || $\lambda = 10.6$
X || Y - VT

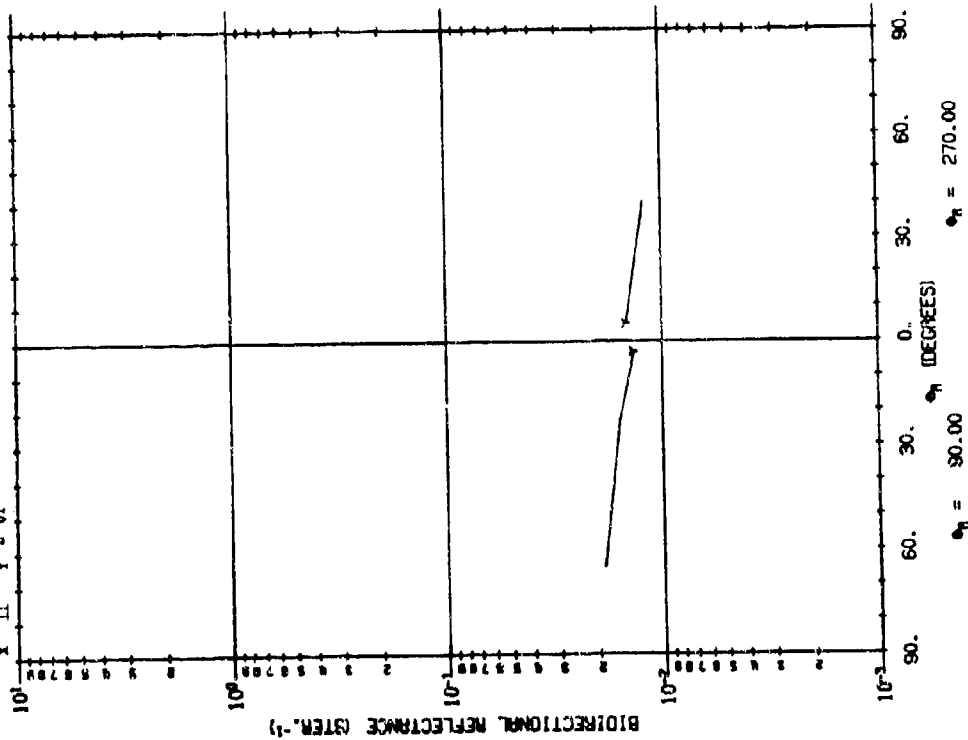


ASPHALT AND CONCRETE

A01530 002

Fine Textured Concrete

0 II $\phi_1 = 0.0$
+ II $\phi_1 = 270.0$
A II $\lambda = 10.6$
X II Y = VI

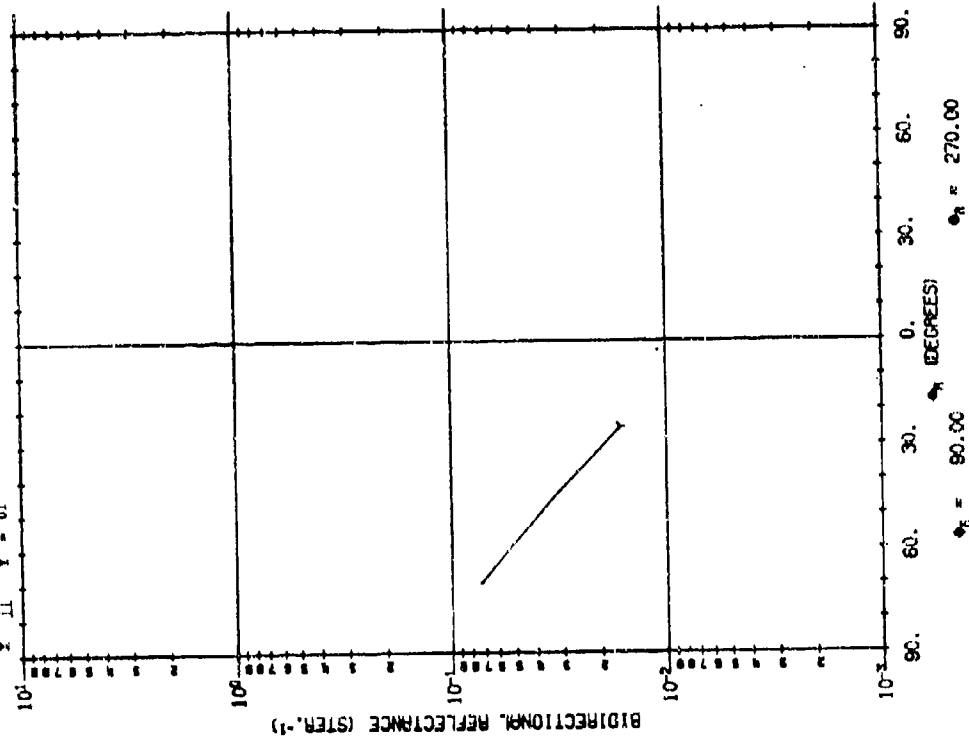


$\phi_1 = 80.00$ $\phi_2 = 270.00$

A01530 002

Fine Textured Concrete

0 II $\phi_1 = 50.0$
+ II $\phi_1 = 270.0$
A II $\lambda = 10.6$
X II Y = VI

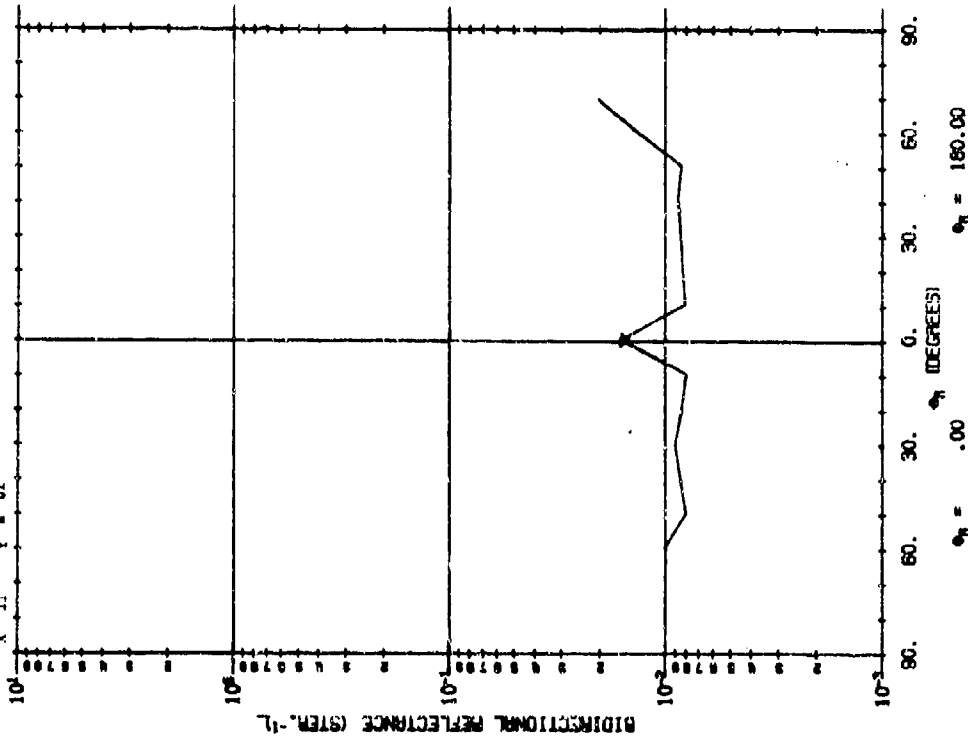


$\phi_1 = 80.00$ $\phi_2 = 270.00$

A01537 002

Very Fine Concrete

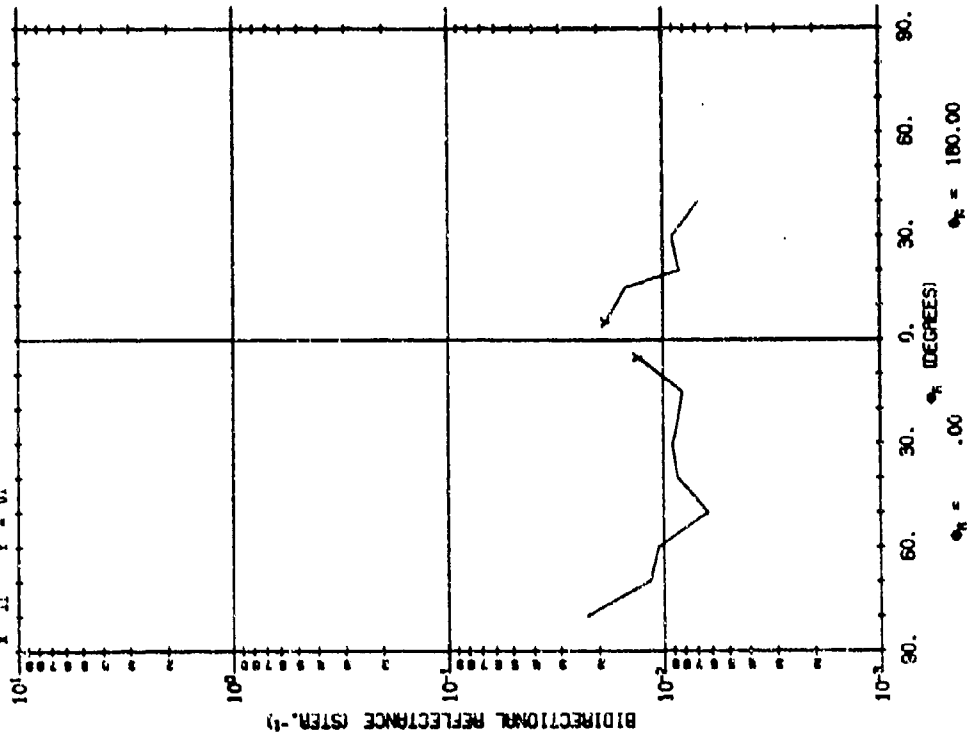
0 || 28 = 1.10
+ || ϕ_1 = ϕ_r
A || λ = 10.6
X || Y = ϕ_r



A01537 002

Very Fine Concrete

0 || ϕ_1 = 0.6
+ || ϕ_1 = 180.0
A || λ = 10.6
X || Y = ϕ_r

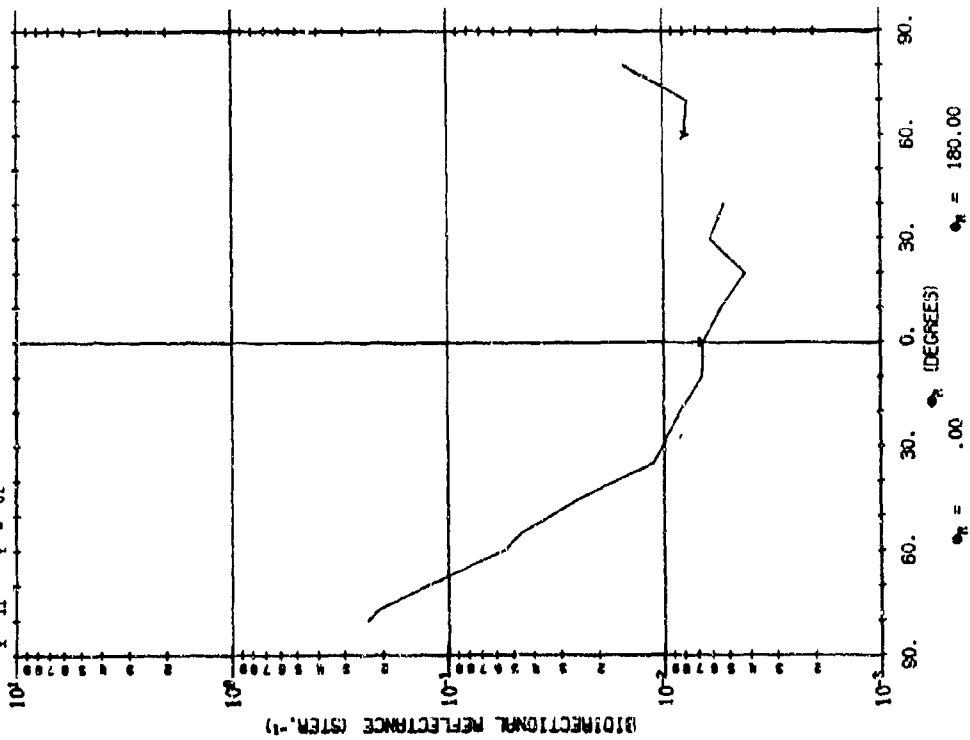


ASPHALT AND CONCRETE

R01537 002

Very Fine Concrete

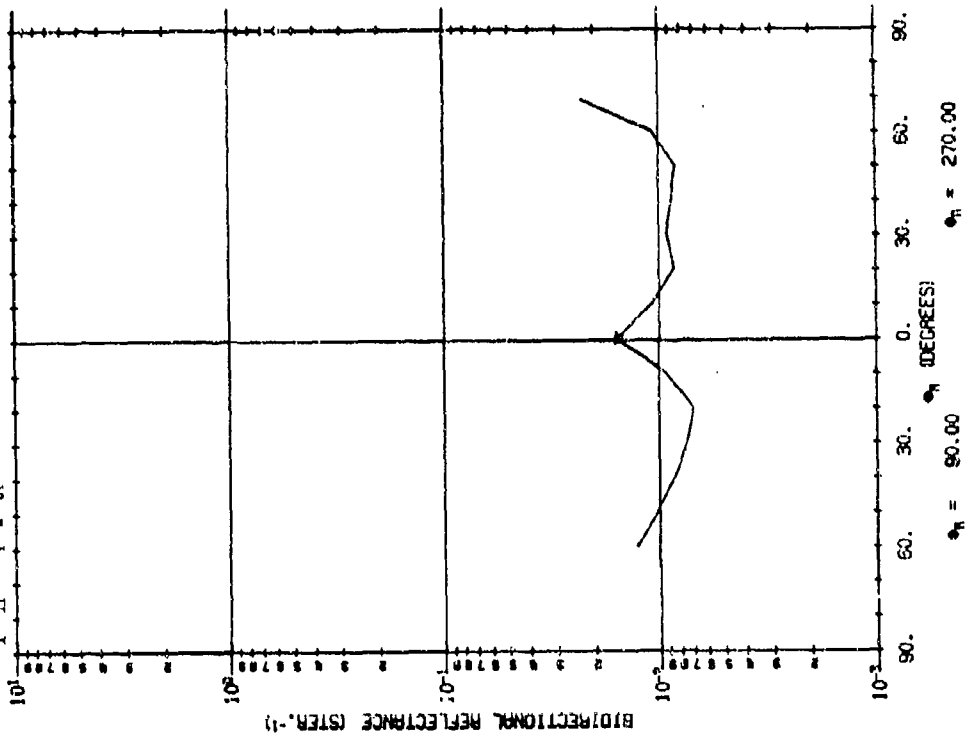
0 || $\theta_1 = 50.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
x || Y = UT



R01537 002

Very Fine Concrete

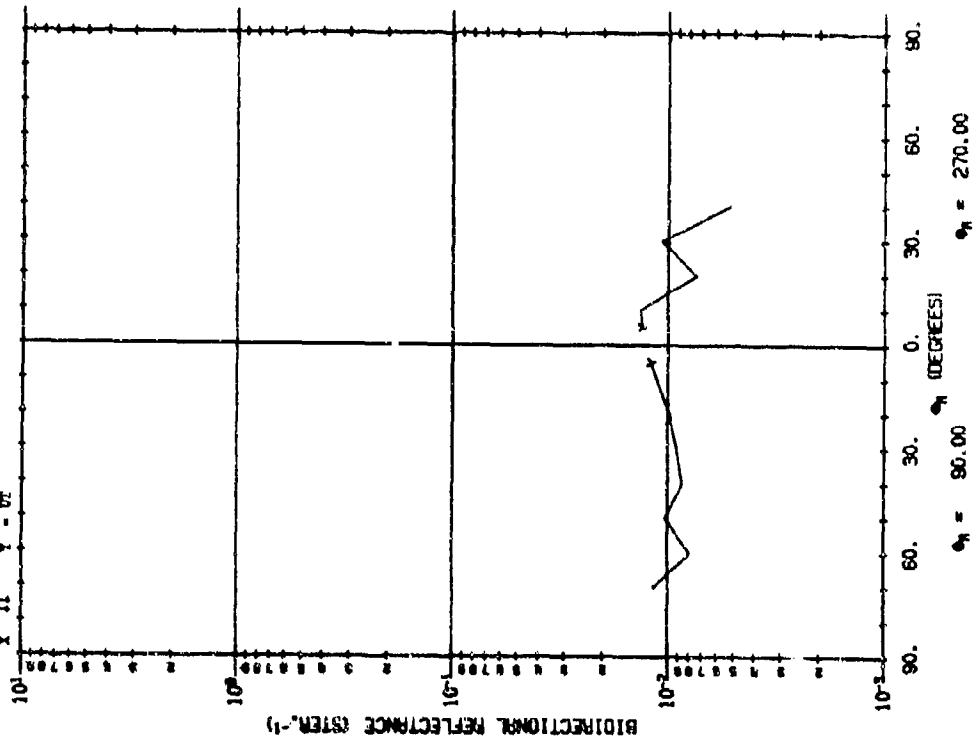
0 || $\theta_1 = 1.10$
+ || $\phi_1 = 0$
Δ || $\lambda = 10.6$
x || Y = UT



R01537 002

Very Fine Concrete

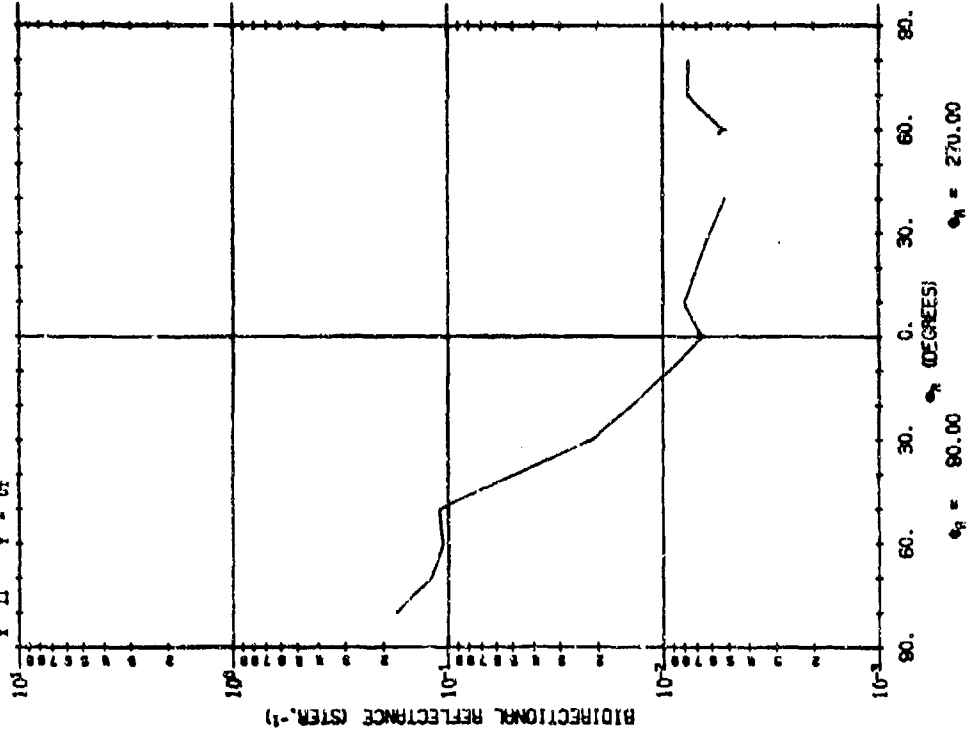
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 270.0$
Δ || $\lambda = 10.6$
X || $\gamma = 07$



R01537 002

Very Fine Concrete

0 || $\phi_1 = 56.0$
+ || $\phi_2 = 270.0$
Δ || $\lambda = 10.6$
X || $\gamma = 07$

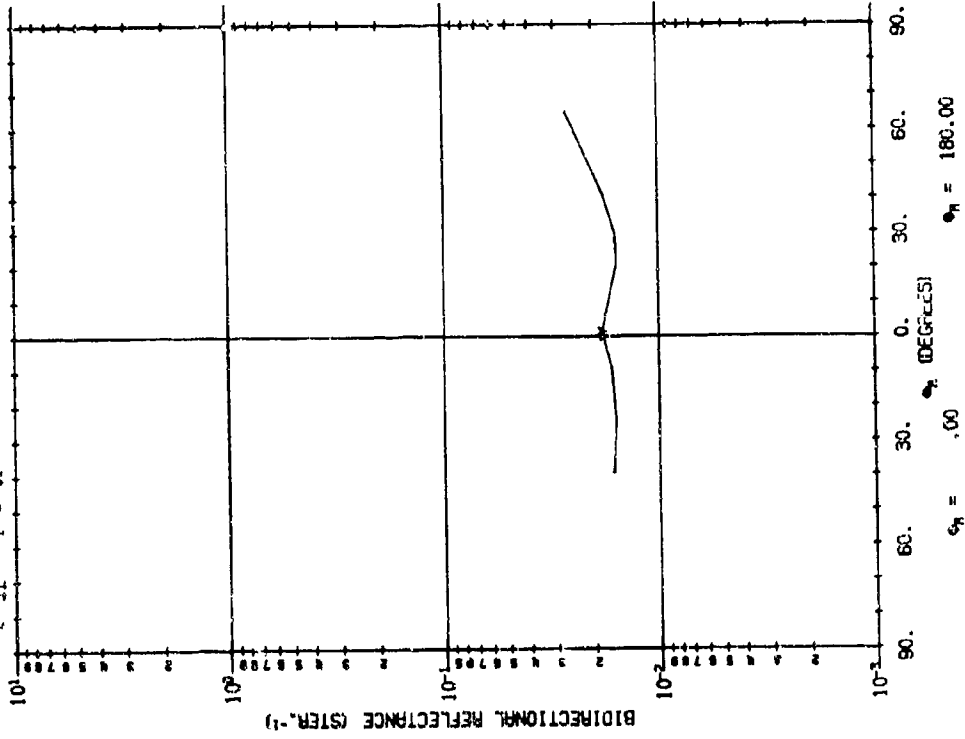


ASPHALT AND CONCRETE

R01543 002

Medium Fine Asphalt

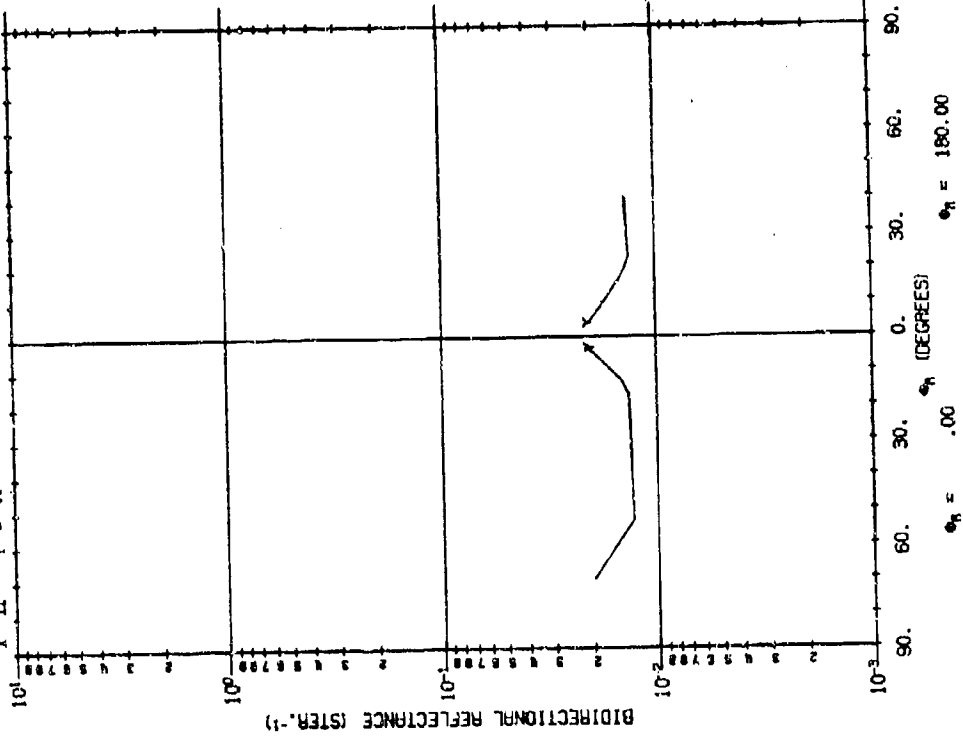
0 || 25 = 1.10
+ || $\phi_1 = 4$
Δ || $\phi_2 = 10.6$
X || Y = DT



R01543 002

Medium Fine Asphalt

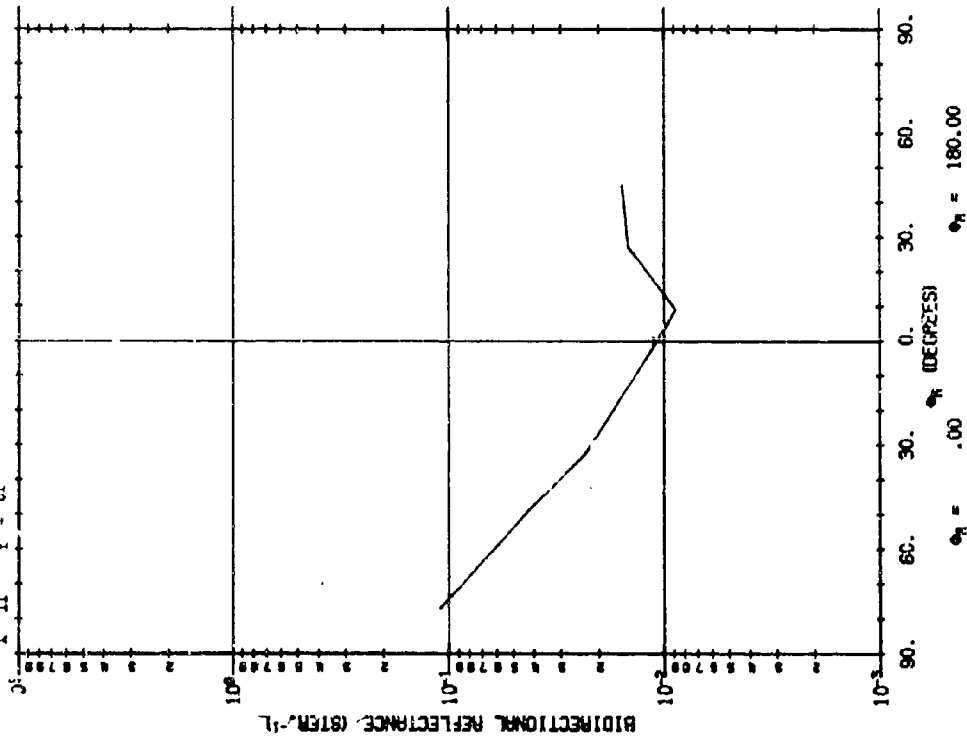
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 10.6$
X || Y = DT



R01543 002

Medium Fine Asphalt

0 // $\theta_1 = 50.0$
 + // $\phi_1 = 167.0$
 Δ // $\lambda = 10.6$
 X // Y = VT

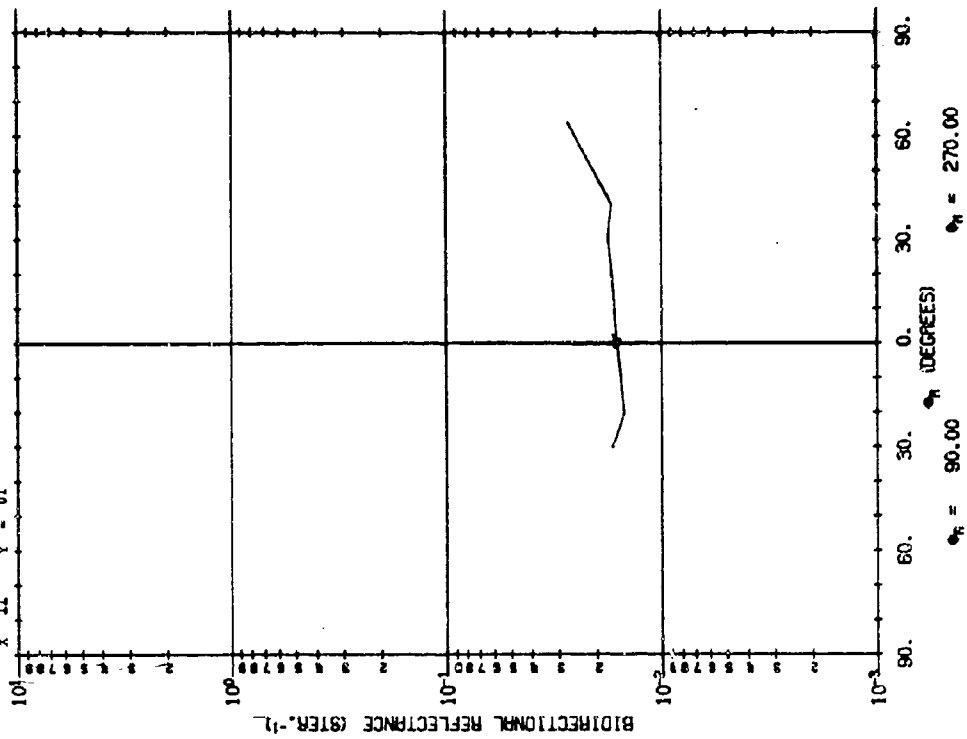


$\theta_1 = 50.00$ $\phi_1 = 180.00$

R01543 002

Medium Fine Asphalt

0 // $\theta_1 = 1.10$
 + // $\phi_1 = 9$
 Δ // $\lambda = 10.6$
 X // Y = VT



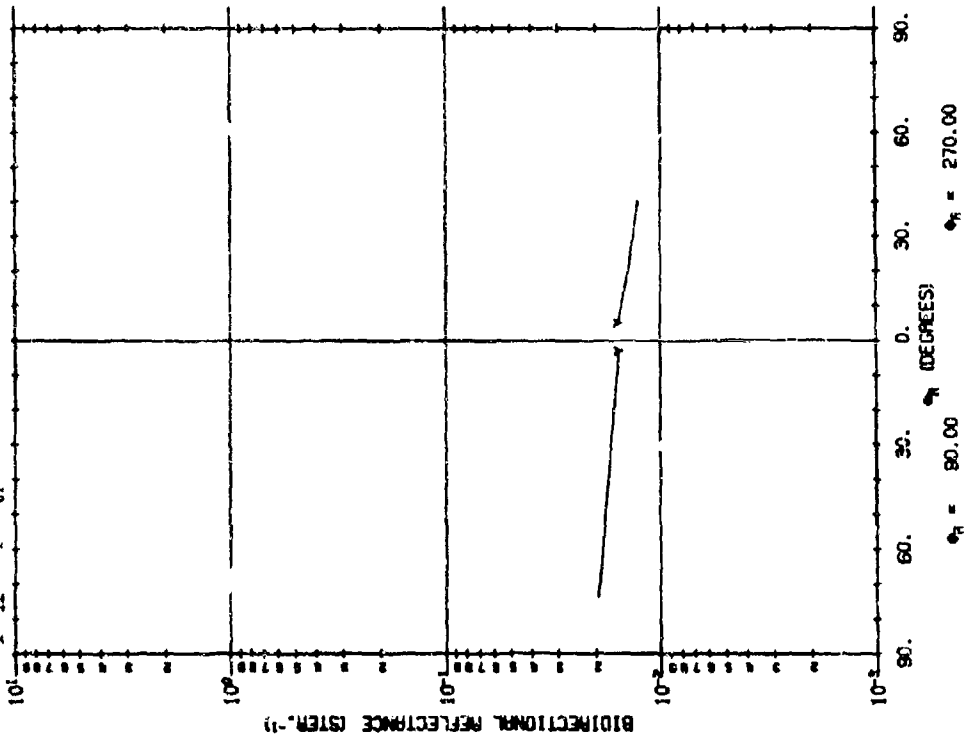
$\theta_1 = 90.00$ $\phi_1 = 270.00$

ASPHALT AND CONCRETE

R01543 002

Medium Fine Asphalt

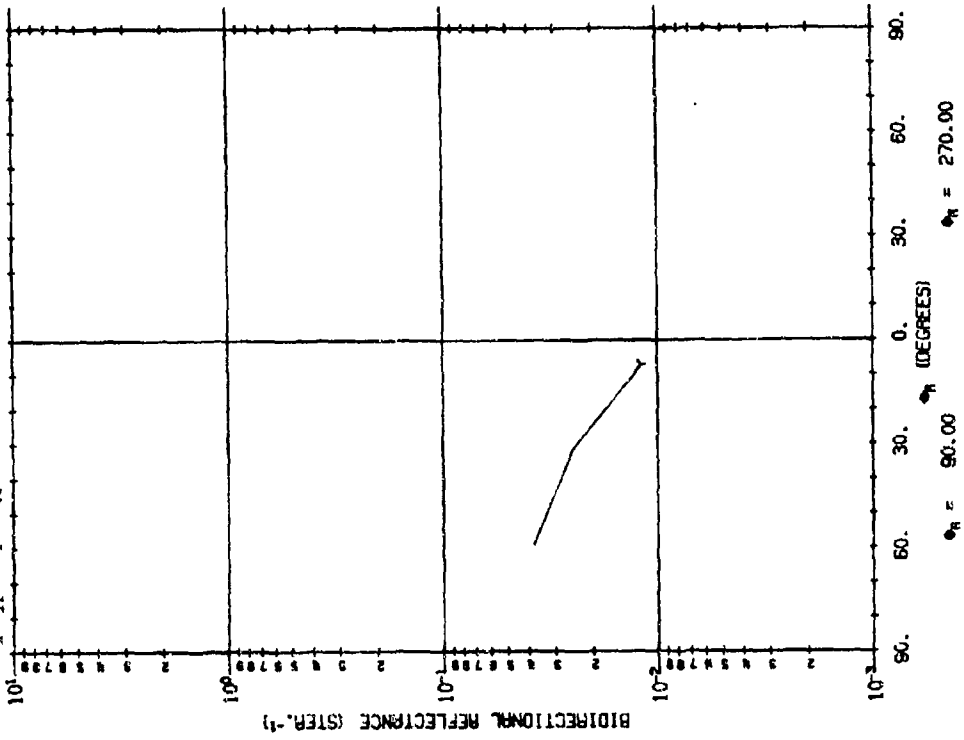
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 270.0$
4 || $\lambda = 10.6$
x || $\gamma = \text{VT}$



R01543 002

Medium Fine Asphalt

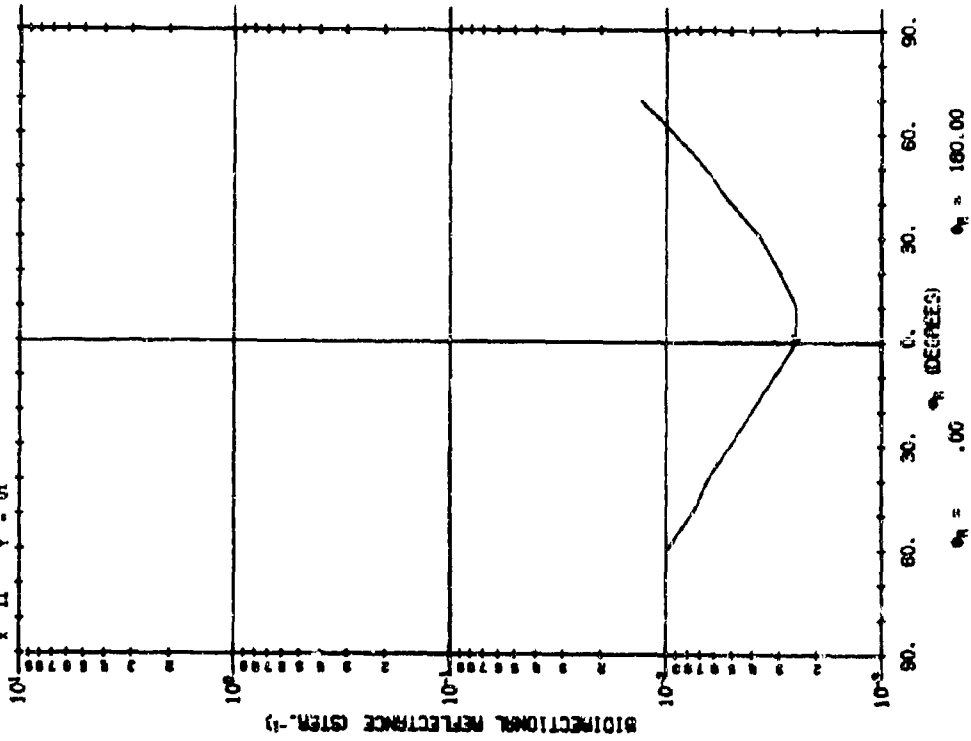
0 || $\theta_1 = 50.0$
+ || $\theta_2 = 270.0$
4 || $\lambda = 10.6$
x || $\gamma = \text{VT}$



A01546 002

Medium Fine Asphalt

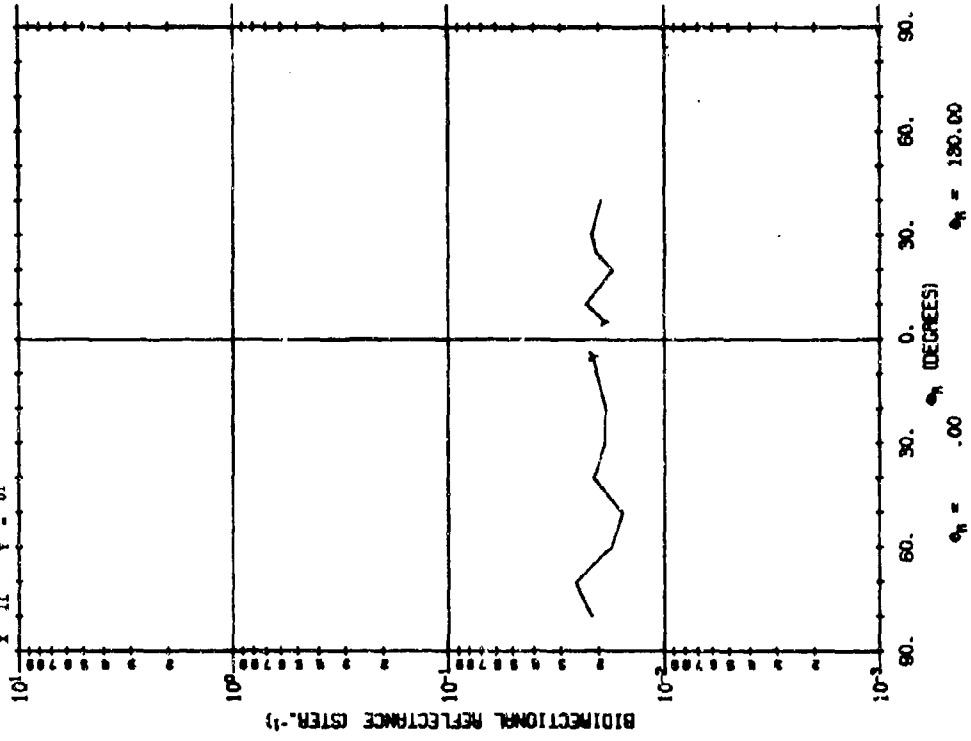
0 || $\theta_1 = 1.10$
+ || $\theta_2 = \theta_c$
A || $\lambda = 10.6$
X || $\gamma = \text{BT}$



A01546 002

Medium Fine Asphalt

0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
A || $\lambda = 10.6$
X || $\gamma = \text{BT}$

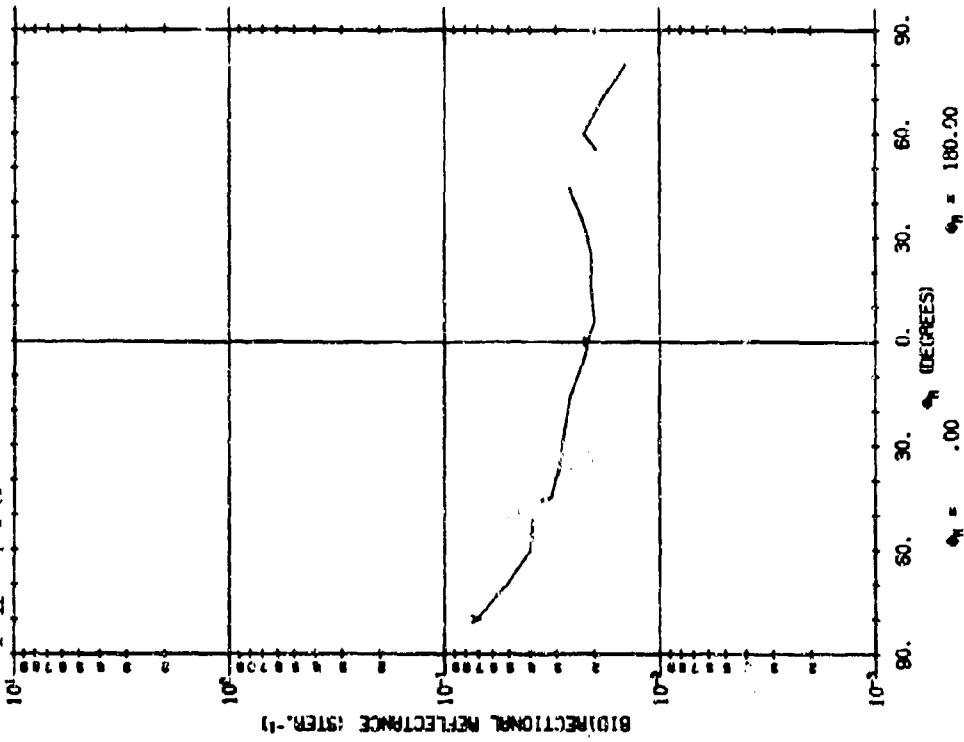


ASPHALT AND CONCRETE

R01546 002

Medium Fine Asphalt

0 // $\phi_1 = 35.0$
+ // $\phi_2 = 180.0$
A // $\lambda = 10.6$
X // $\gamma = \text{UT}$

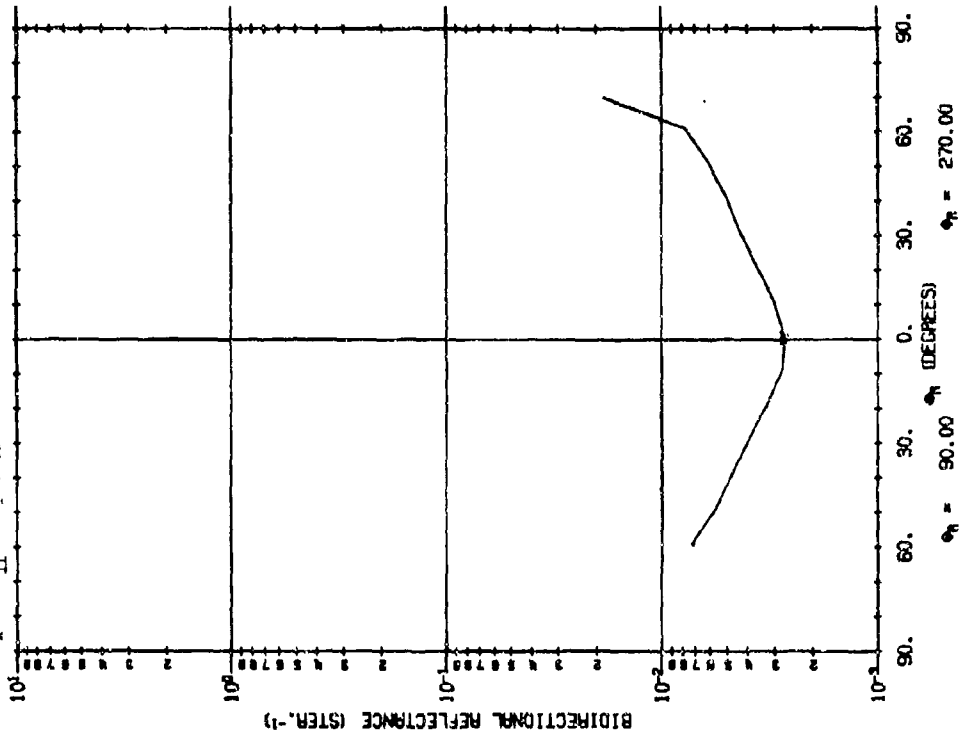


$\phi_1 = 35.0$
 $\phi_2 = 180.0$
 $\lambda = 10.6$
 $\gamma = \text{UT}$

R01546 002

Medium Fine Textured Asphalt

0 // $\phi_1 = 1.10$
+ // $\phi_2 = \phi_1$
A // $\lambda = 10.6$
X // $\gamma = \text{UT}$



$\phi_1 = 1.10$
 $\phi_2 = \phi_1$
 $\lambda = 10.6$
 $\gamma = \text{UT}$

R01546 002

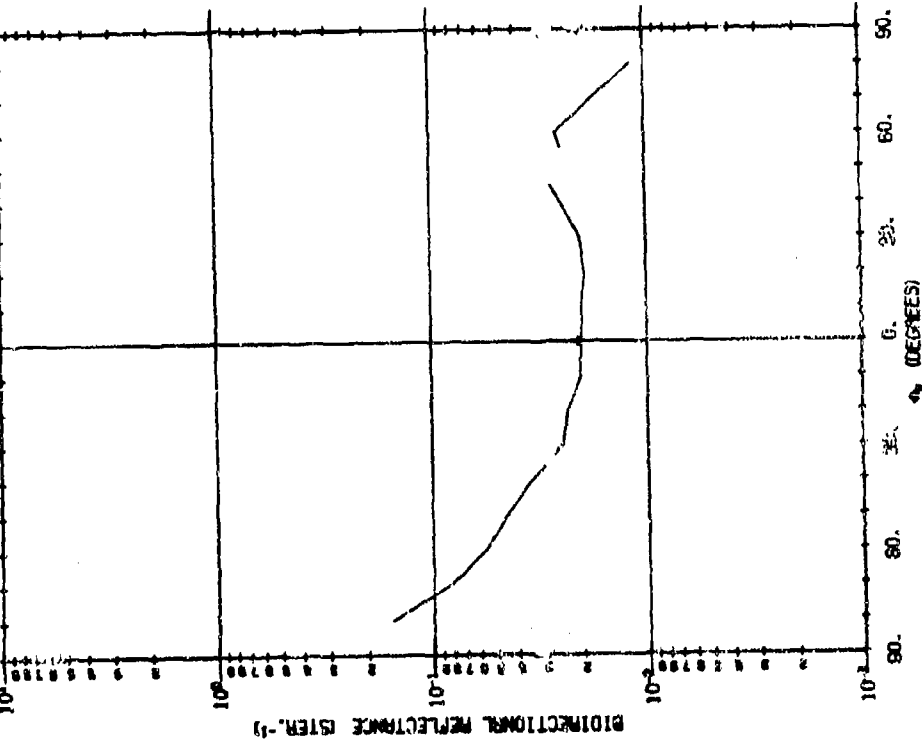
Medium Fine Asphalt

$\theta_1 = 90.0$

$\theta_2 = 270.0$

$\theta_3 = 10.6$

$\theta_4 = 197$



$\theta_1 = 90.00$

$\theta_2 = 270.00$

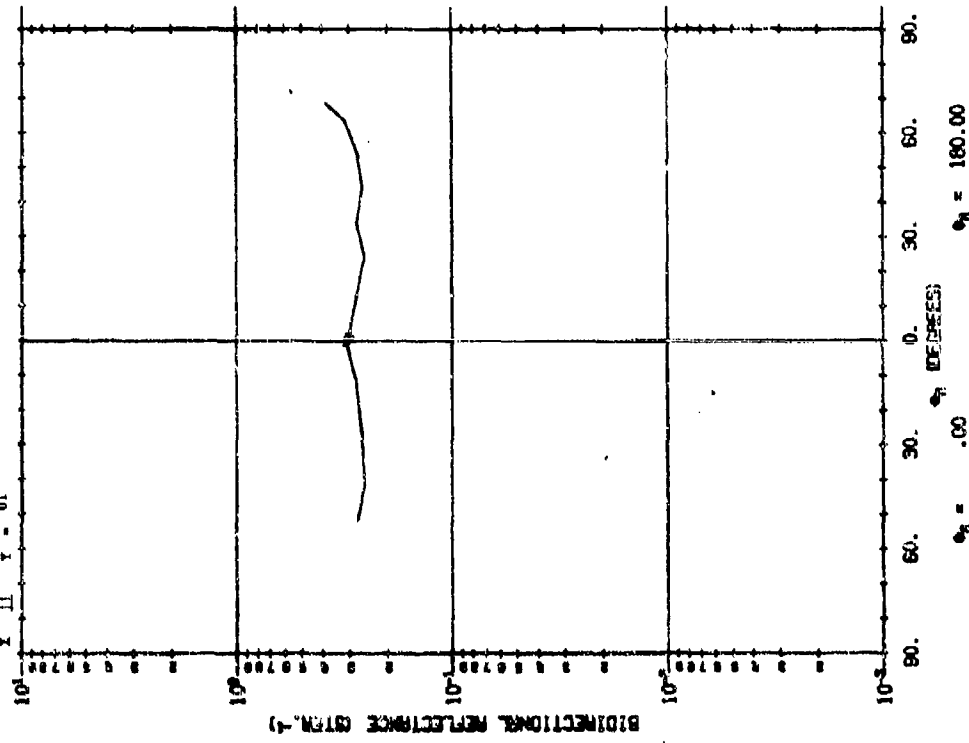
ASPHALT AND CONCRETE

REFLECTANCE
STANDARDS
MATERIAL

P01094 001

Flame Sprayed Aluminum Panel

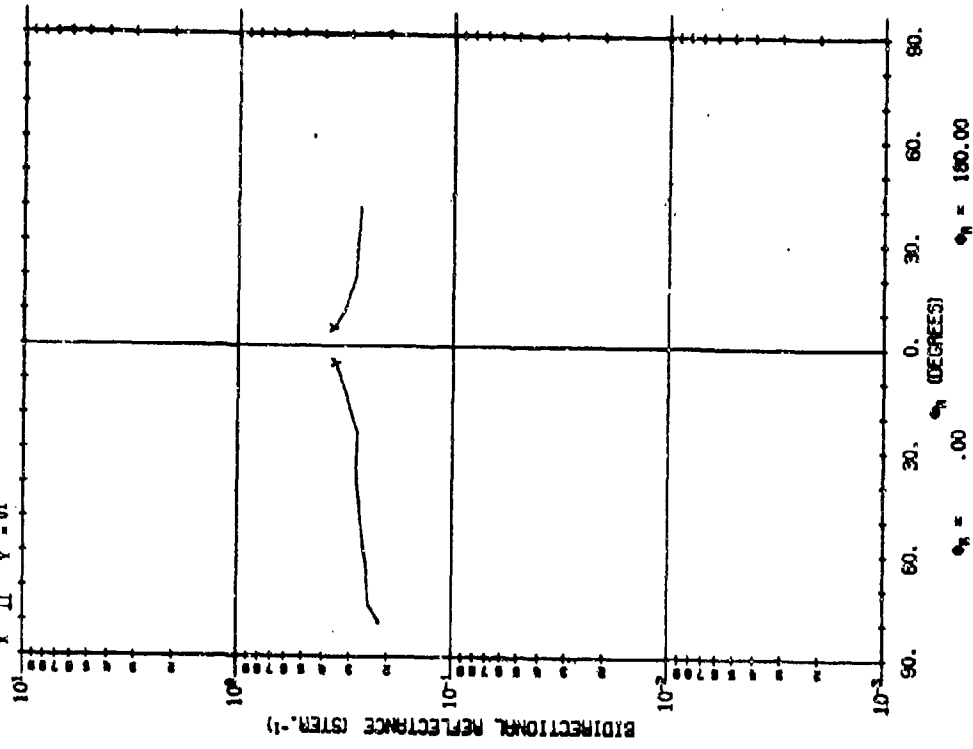
0 || ZI = 1.10
+ || θ_1 = 4°
A || λ = 10.6
X || Y = BT



P01094 001

Flame Sprayed Aluminum Panel

0 || θ_1 = 0.0
+ || ϕ_1 = 180.0
A || λ = 10.6
X || Y = BT

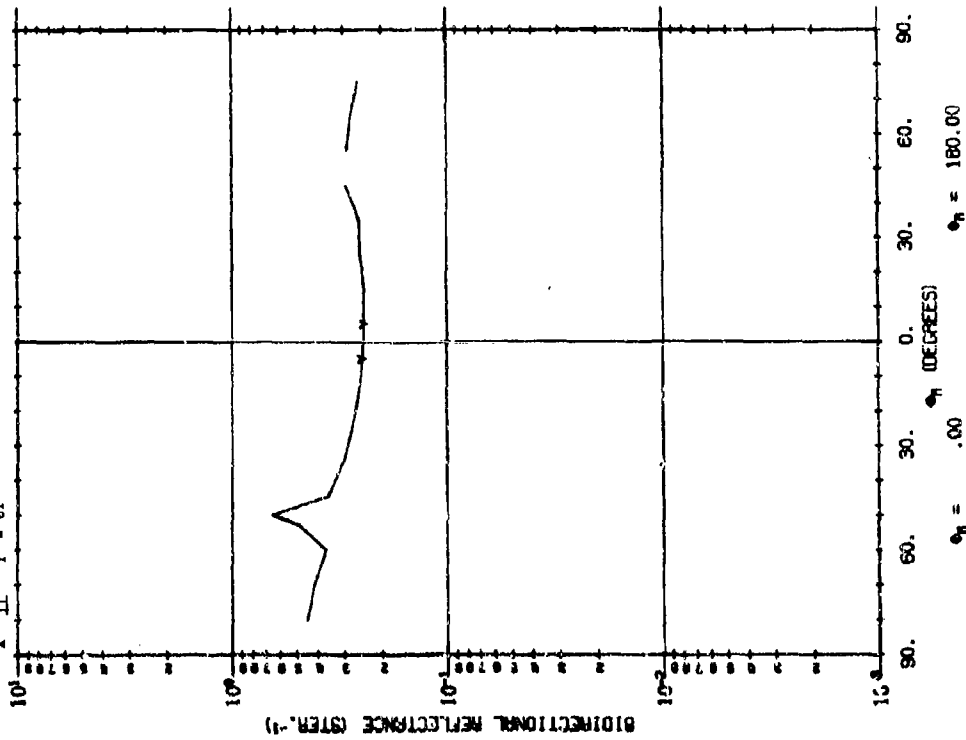


REFLECTANCE STANDARDS MATERIAL

AO1094

Flame Sprayed Aluminum Panel

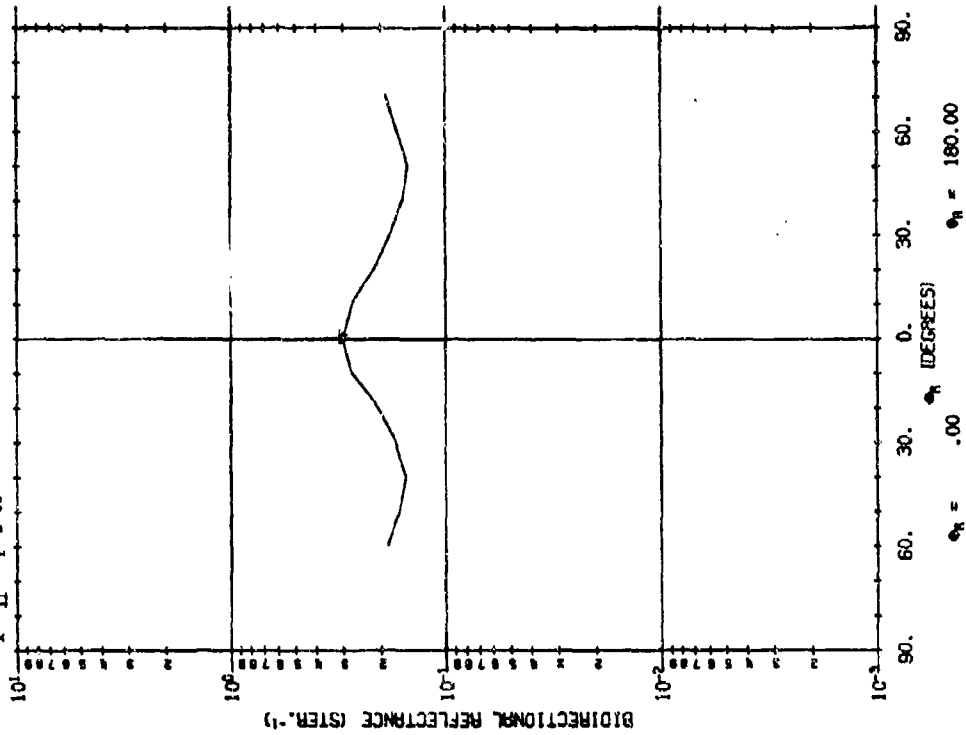
$\theta_1 = 50.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
Y = UT



AO1095

Flame Sprayed Copper Panel

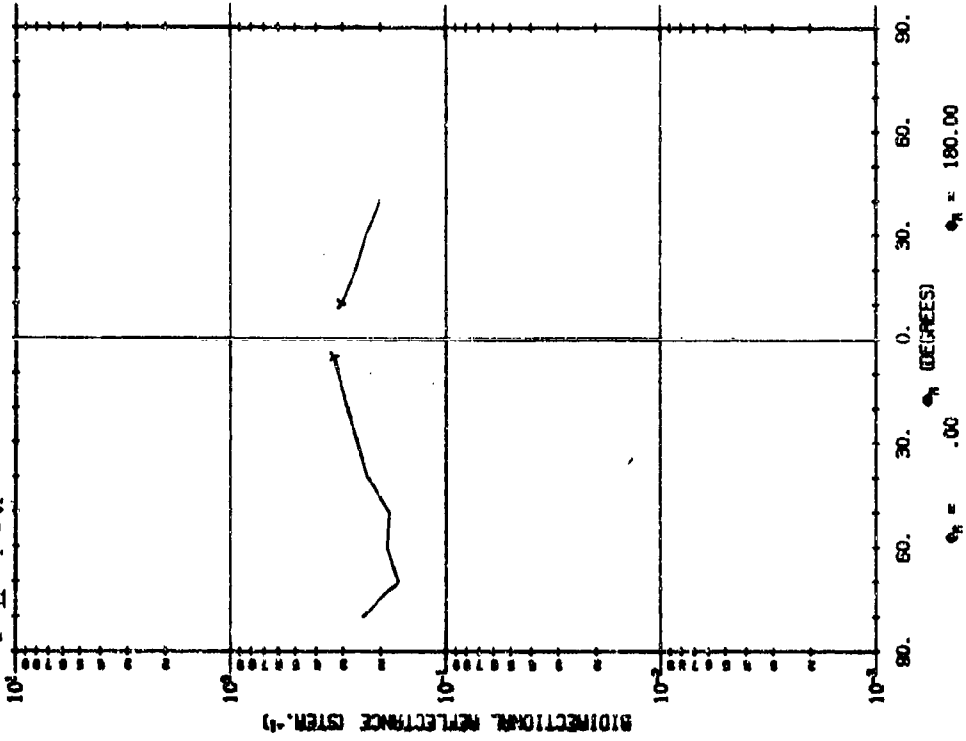
$\theta_1 = 1.10$
 $\phi_1 = 4r$
 $\lambda = 10.6$
Y = UT



R01095 001

Film Sprayed Copper Panel

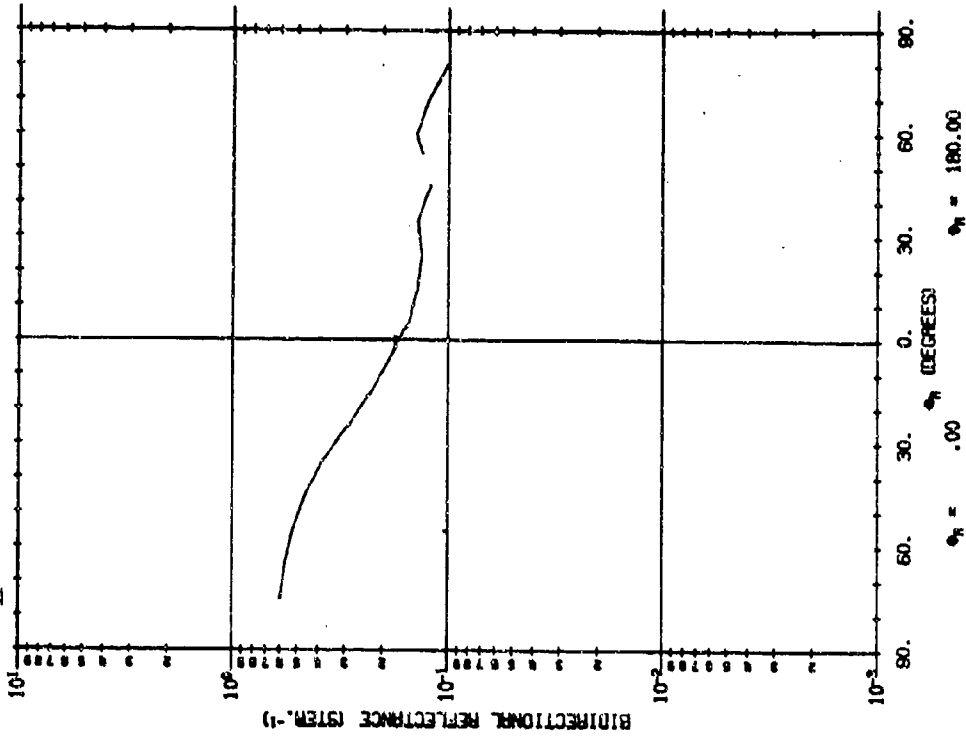
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
A || $\lambda = 10.6$
X || Y = UT



R01095 001

Film Sprayed Copper Panel

0 || $\phi_1 = 50.0$
+ || $\phi_2 = 180.0$
A || $\lambda = 10.6$
X || Y = UT

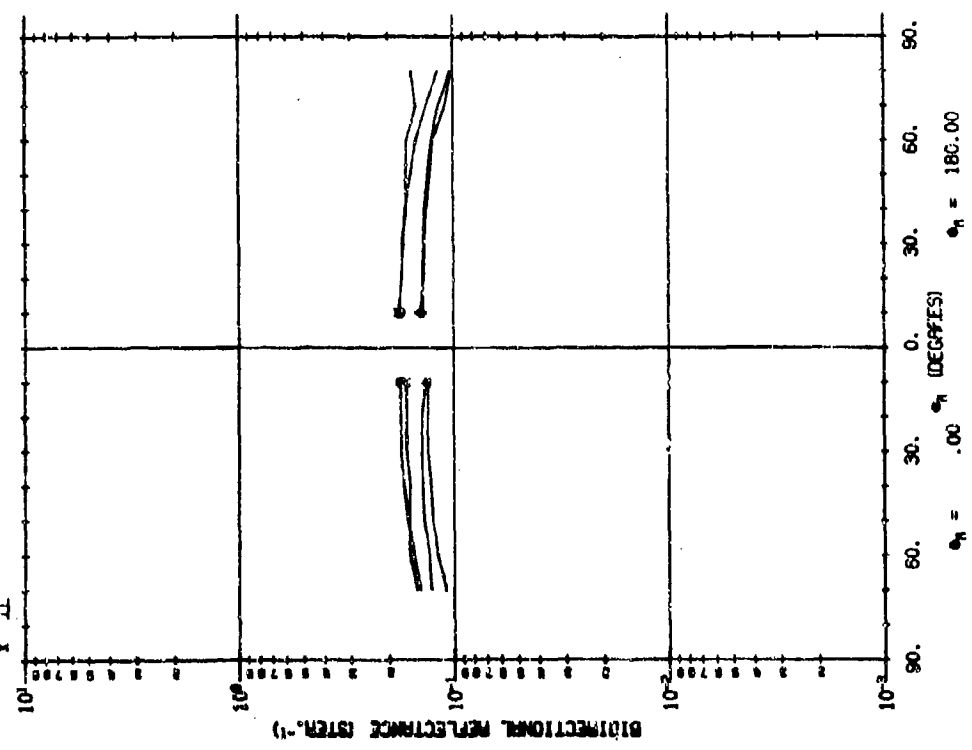


REFLECTANCE STANDARDS MATERIAL

A01190 001

SMOOTH MAGNESIUM OXIDE
ON ALUMINUM PLATE

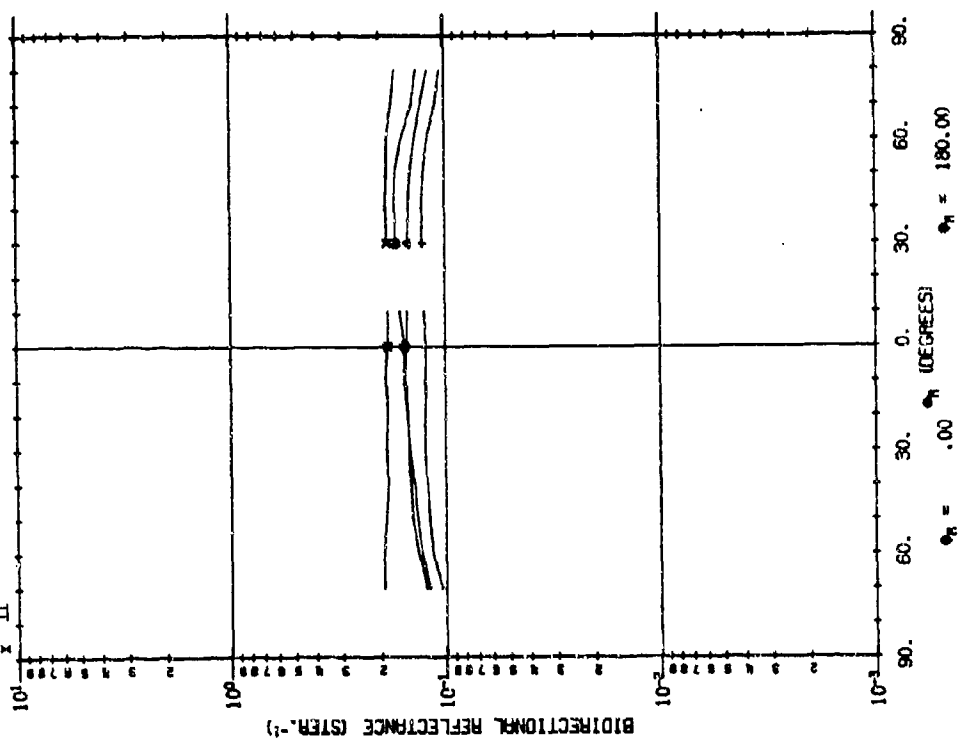
0 || $\theta_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 0.63$
X ||

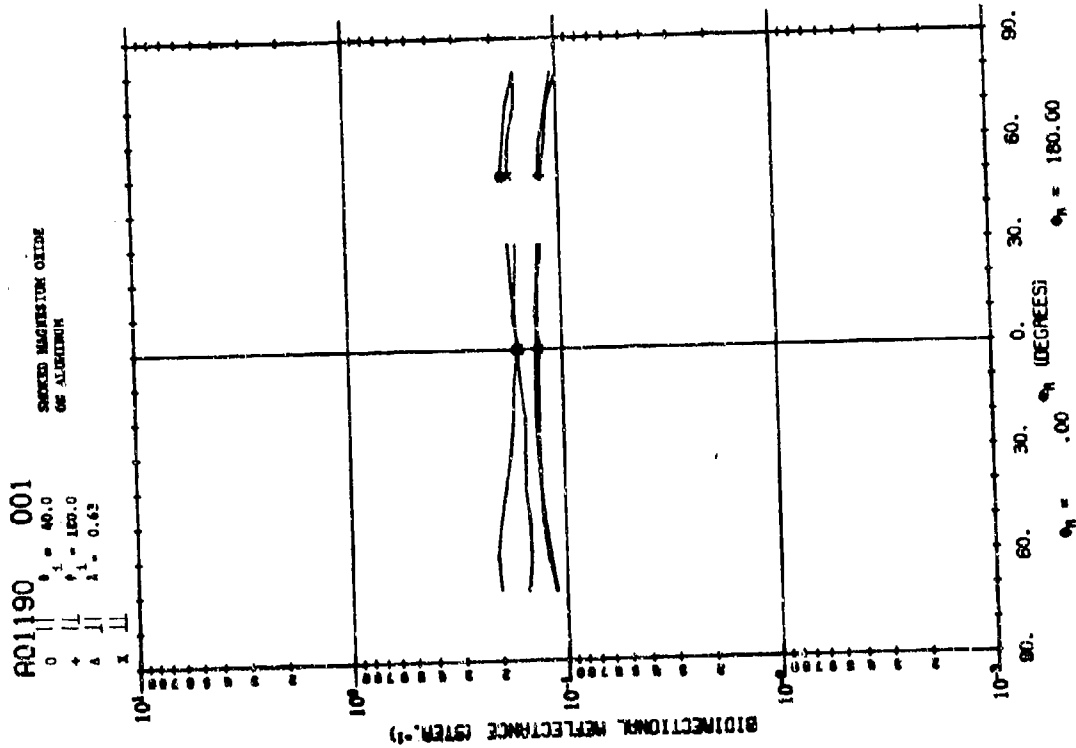
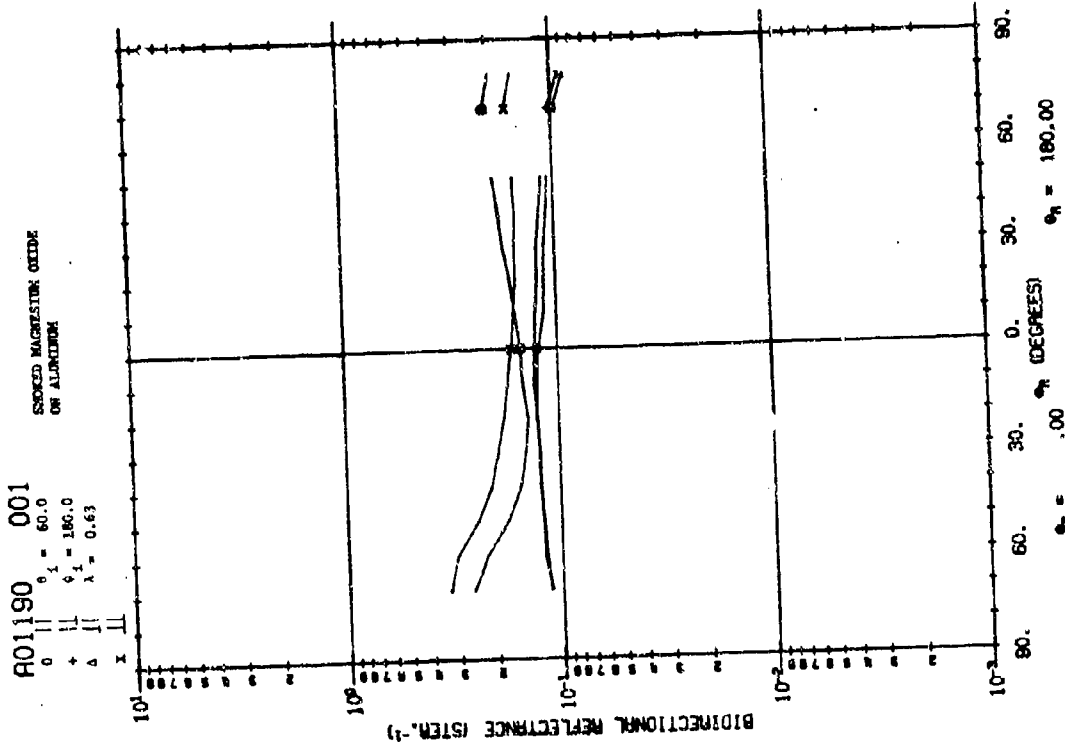


A01190 001

SMOOTH MAGNESIUM OXIDE
ON ALUMINUM PLATE

0 || $\theta_1 = 20.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 0.63$
X ||





REFLECTANCE STANDARDS MATERIAL

R01191 001

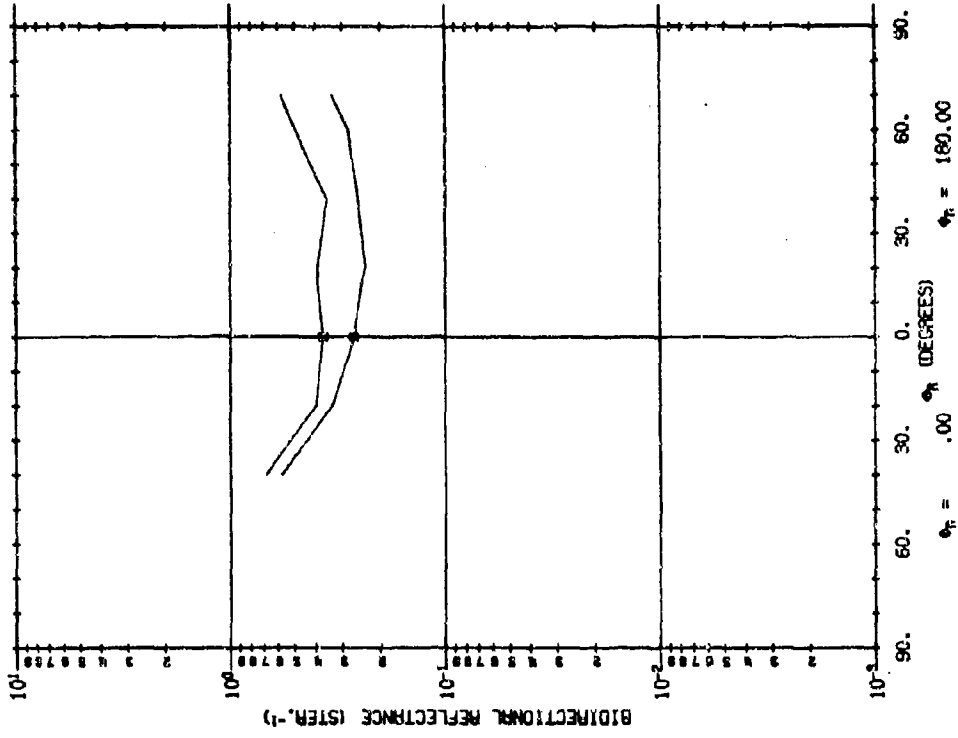
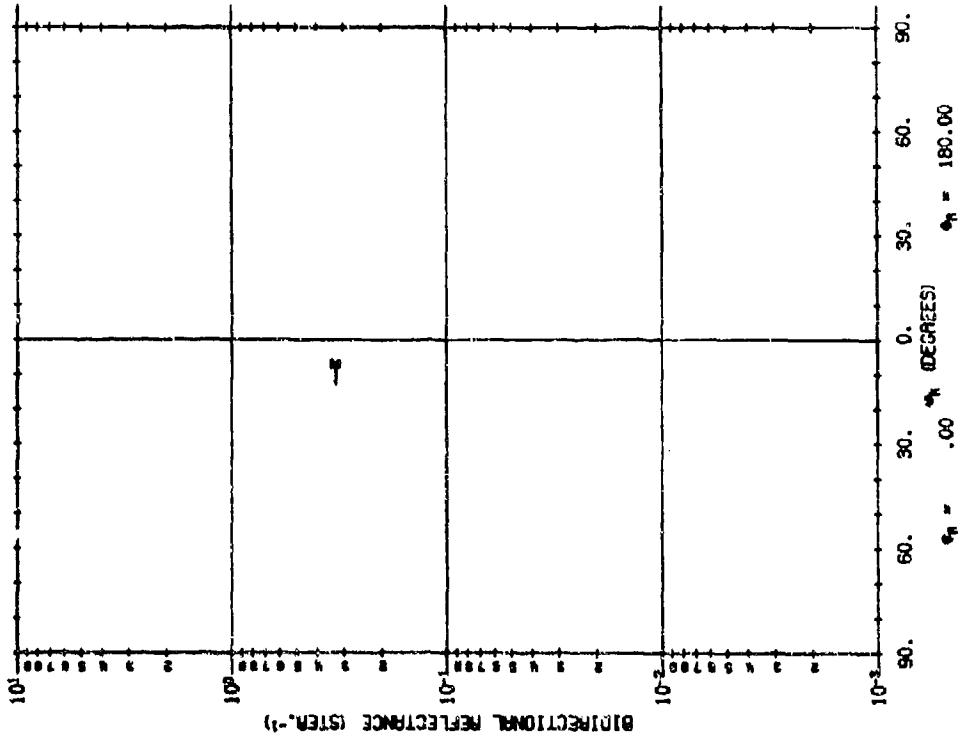
FIBERFAX TYPE 970 JH ON 1/4" PLYWOOD

R01191 001

FIBERFAX TYPE 970 JH ON 1/4" PLYWOOD

X | Y | $\theta_i = 0.0$
Z | $\phi_i = 180.0$
 $\lambda_i = 0.43$

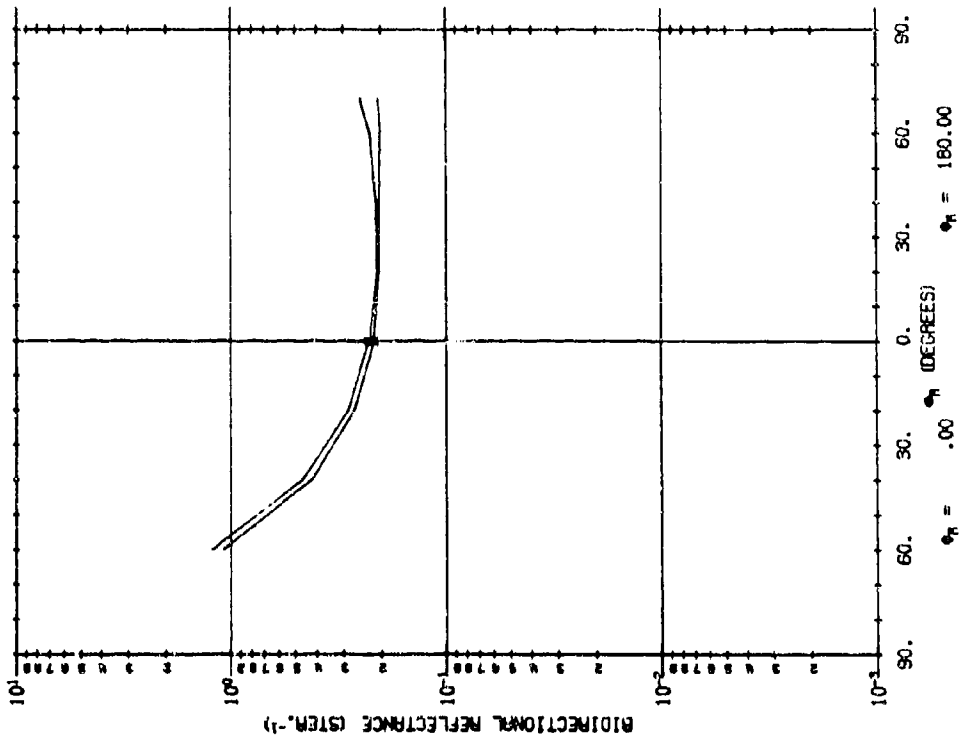
X | Y | $\theta_i = 80.0$
Z | $\phi_i = 180.0$
 $\lambda_i = 0.43$



A01191 001

FIBERGLASS TYPE 970 JE ON 1/4" PLYWOOD

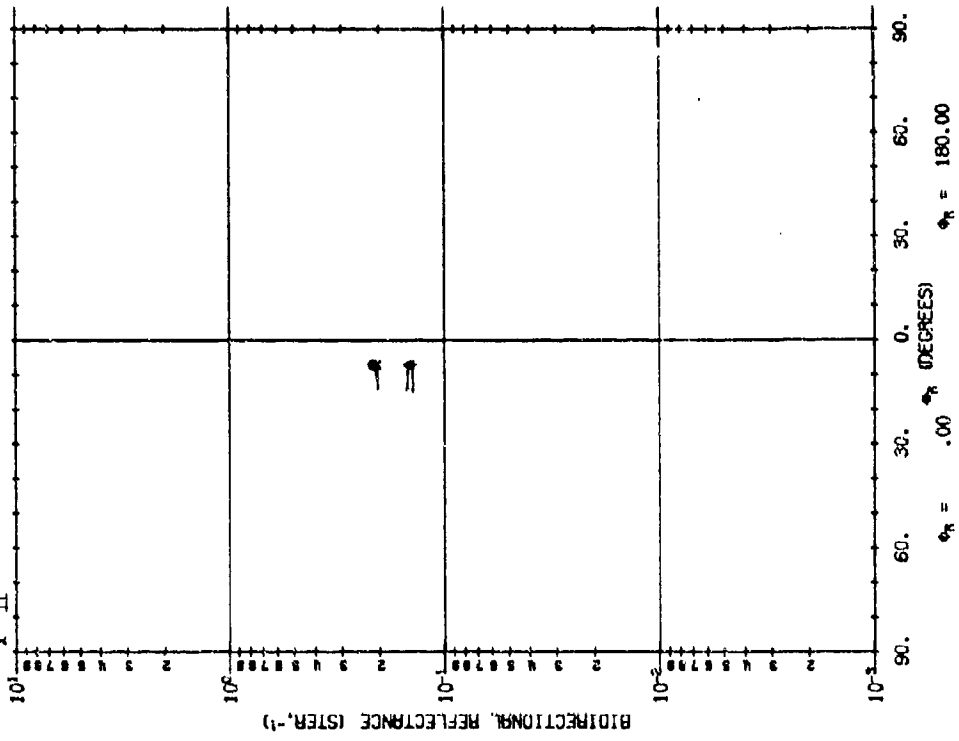
X | T $\phi_1 = 90.0$
Z | T $\phi_2 = 180.0$
 | $\lambda = 1.10$



A01191 002

FIBERGLASS TYPE 970 JE ON 1/4" PLYWOOD

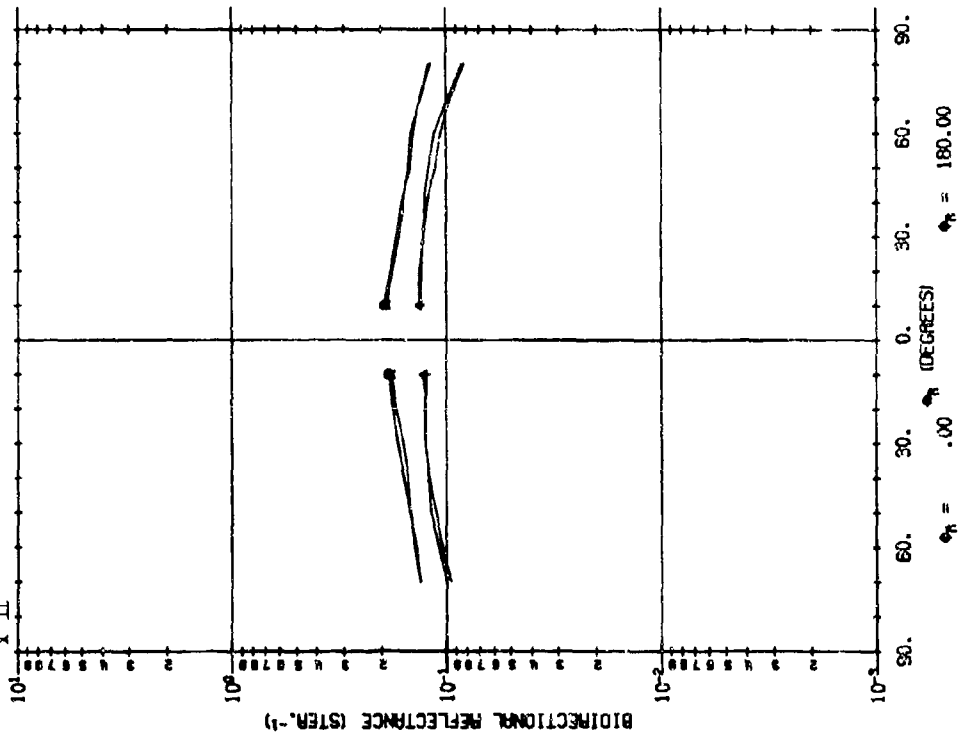
0 | T $\phi_1 = 0.0$
T | T $\phi_2 = 180.0$
Z | T $\lambda = 0.55$



A01191 002

FIBERFLAX TYPE 970 JH ON 1/4" PLYWOOD

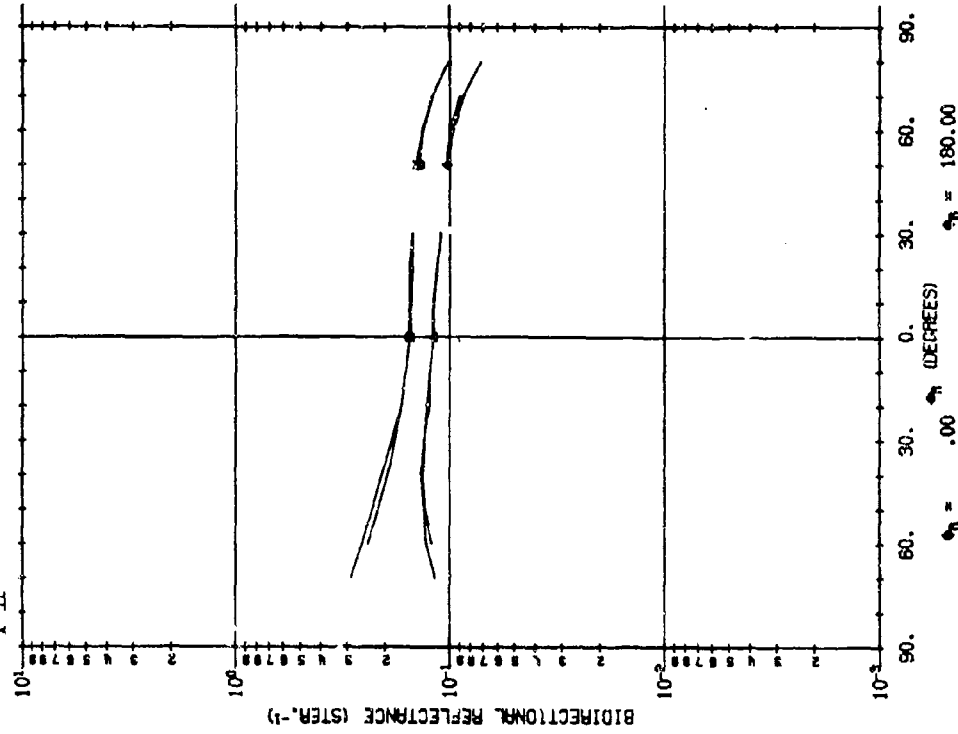
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 0.63$
x ||



A01191 002

FIBERFLAX TYPE 970 JH ON 1/4" PLYWOOD

0 || $\theta_1 = 40.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 0.63$
x ||

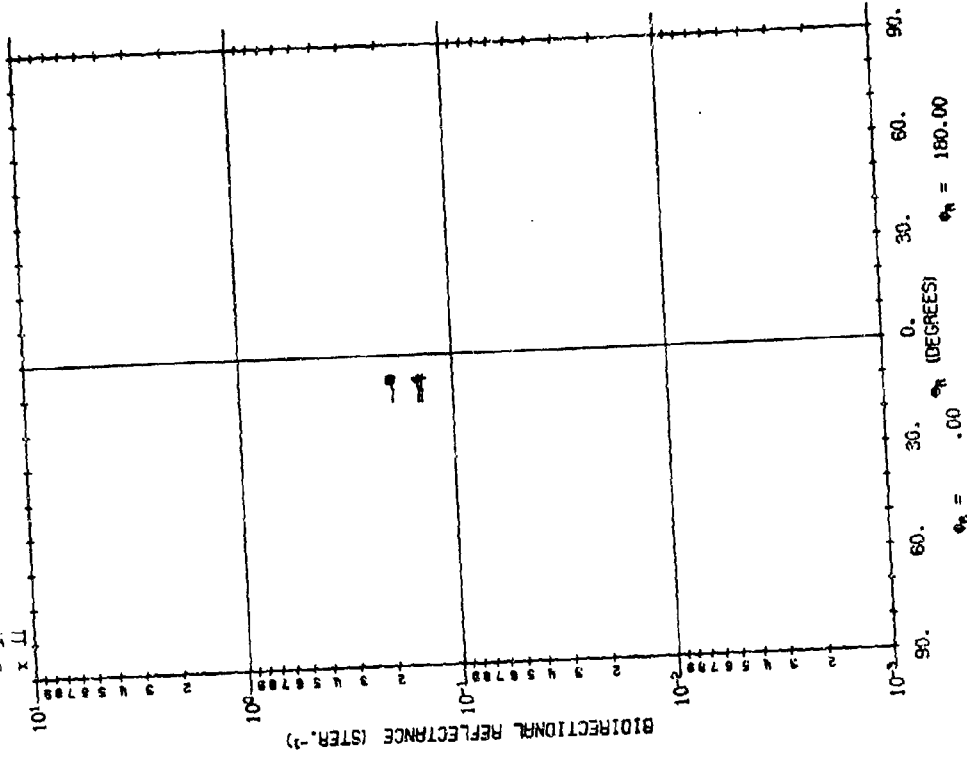


REFLECTANCE STANDARDS MATERIAL

R01191 002

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

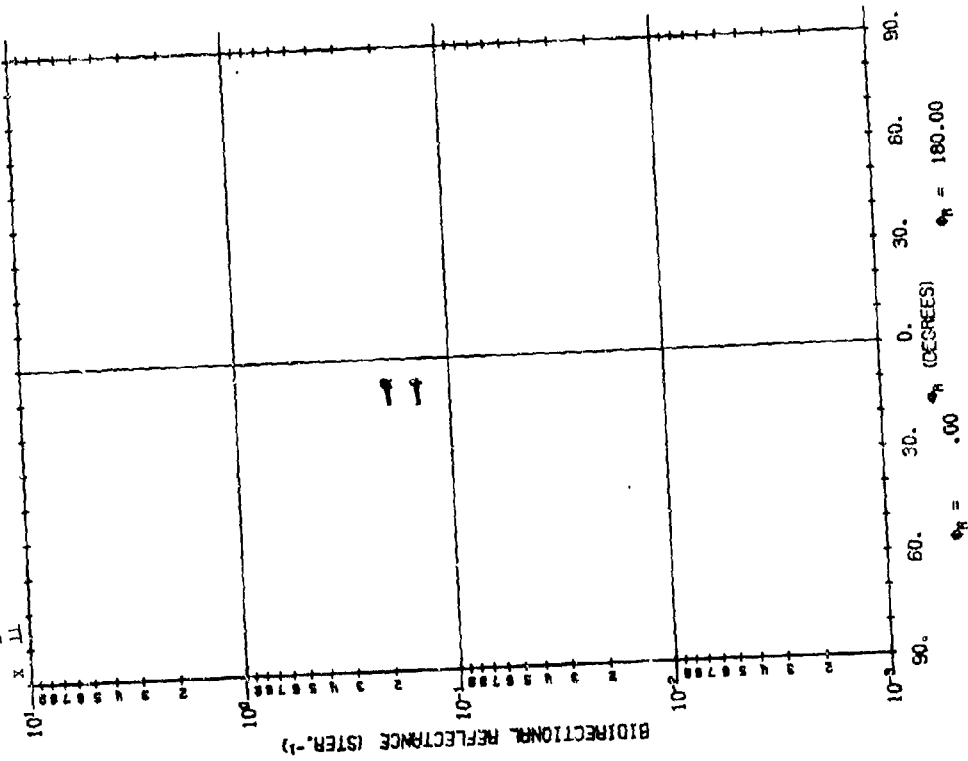
$\theta_i = 0.0$
 $\phi_i = 180.0$
 $\lambda = 1.10$



R01191 002

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

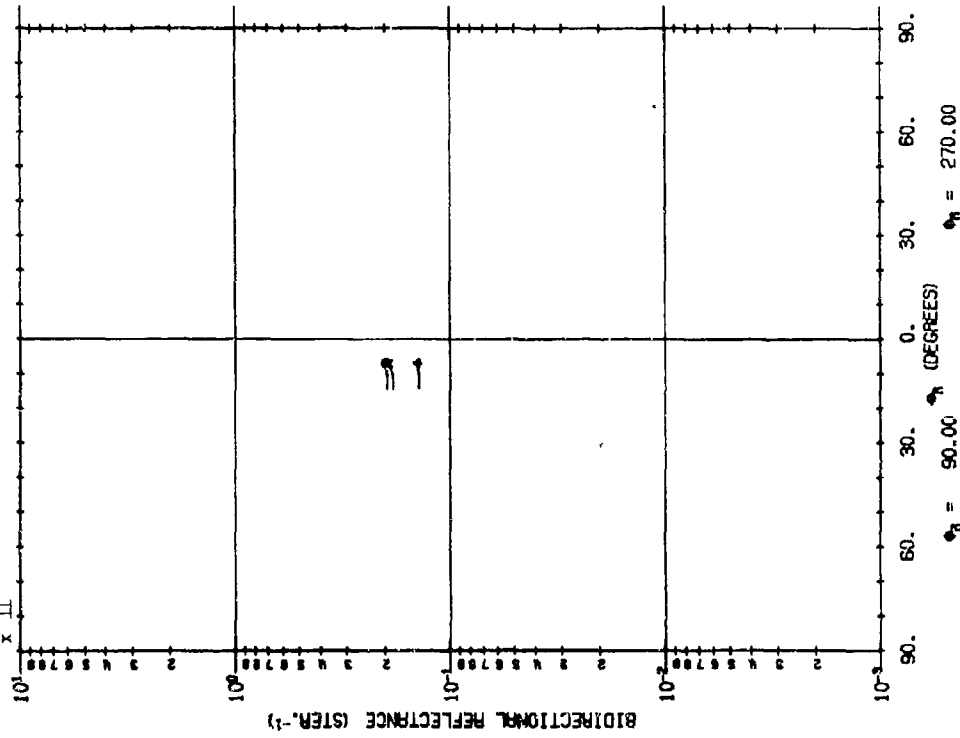
$\theta_i = 0.0$
 $\phi_i = 180.0$
 $\lambda = 0.75$



A01191 002

FIBERFRAX TYPE 970 JF ON 1/4" PLYWOOD

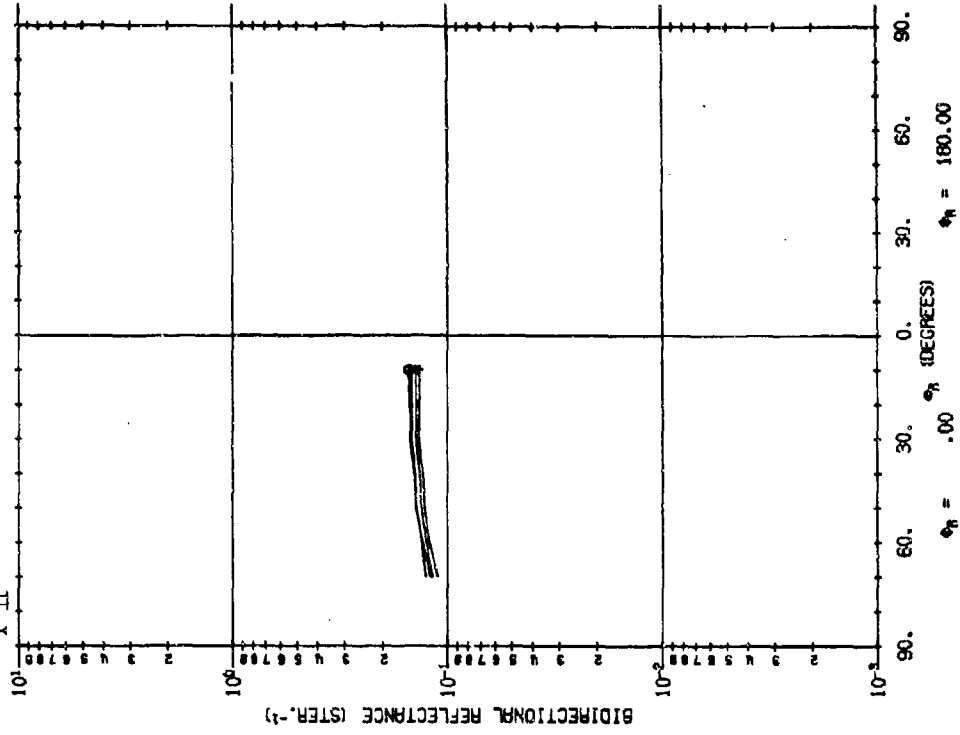
0 || $\phi_1 = 0.0$
+ || $\phi_1 = 270.0$
Δ || $\lambda = 1.10$
x ||



A01192 001

FLOWERS OF SULFUR

0 || $\phi_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 0.63$
x ||

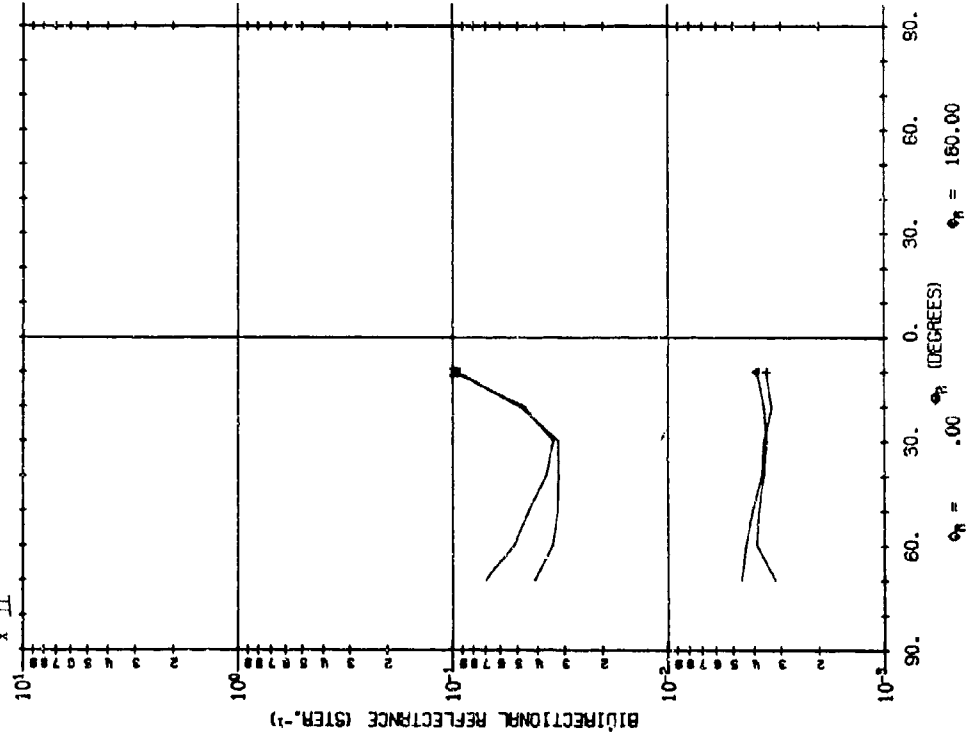


REFLECTANCE STANDARDS MATERIAL

A01194 001

CHROME PLATED GLASS BEADS

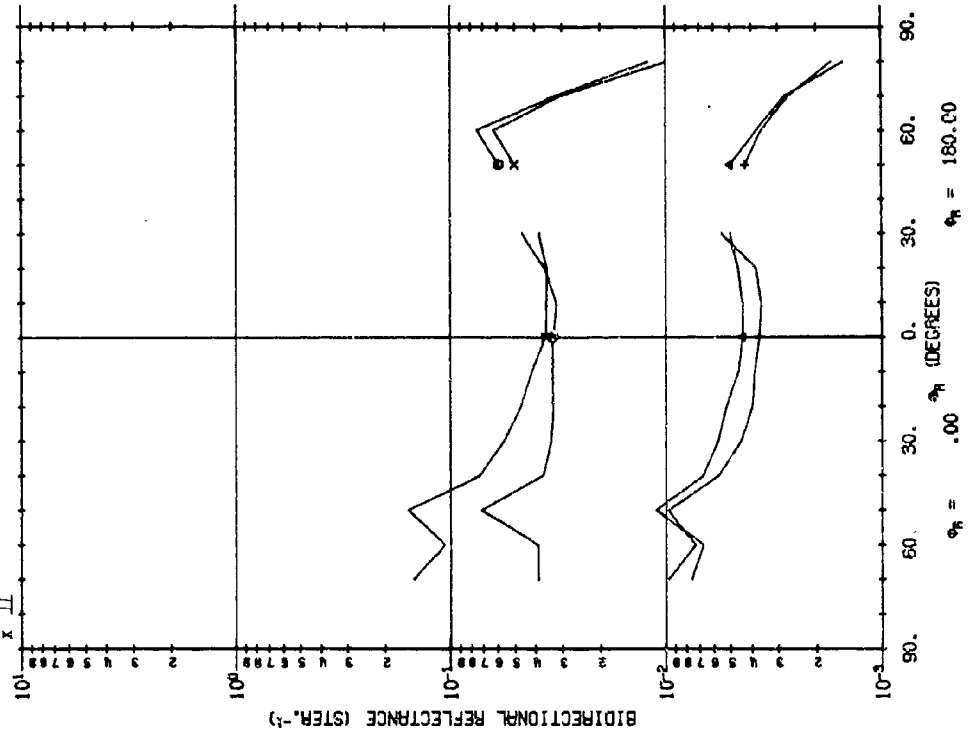
$\phi_1 = 0.0$
 $\phi_2 = 180.0$
 $\lambda = 0.63$



A01194 001

CHROME PLATED GLASS BEADS

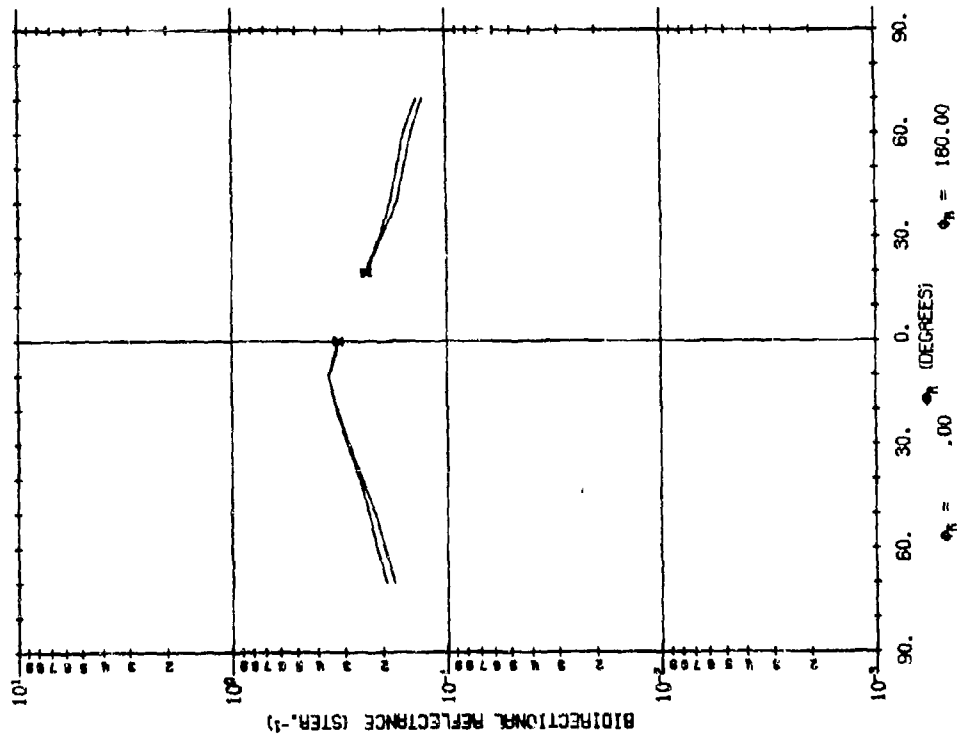
$\phi_1 = 60.0$
 $\phi_2 = 180.0$
 $\lambda = 0.63$



R01197 001

SANDBLASTED ALUMINUM

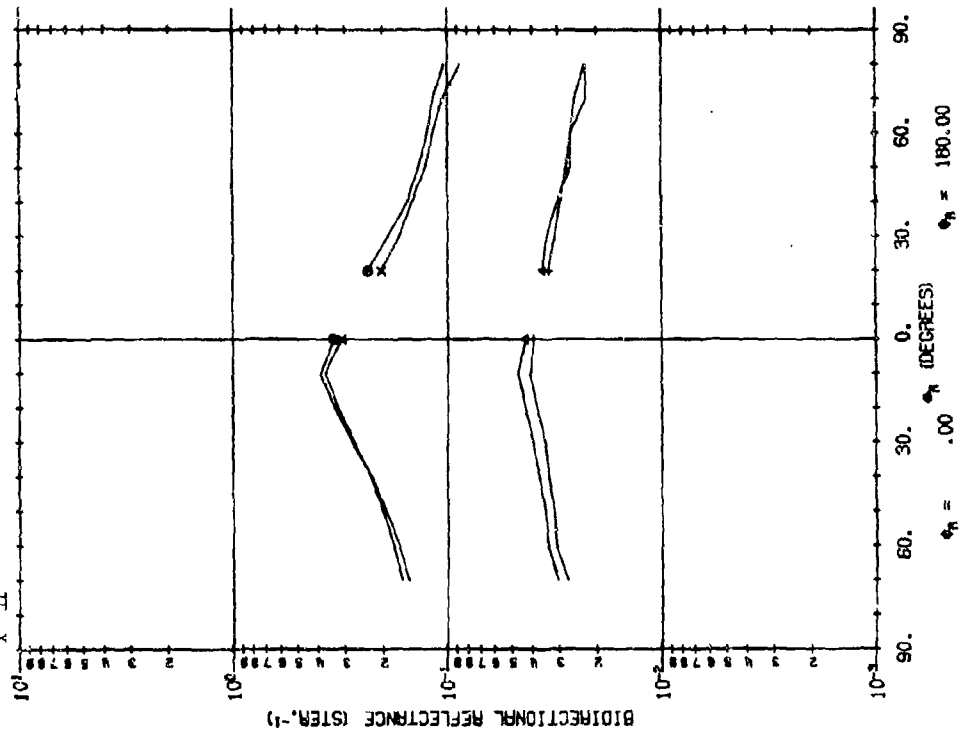
$\theta_1 = 10.0$
 $\theta_2 = 180.0$
 $\lambda = 0.54$



R01197 002

SANDBLASTED ALUMINUM

$\theta_1 = 10.0$
 $\theta_2 = 180.0$
 $\lambda = 1.08$

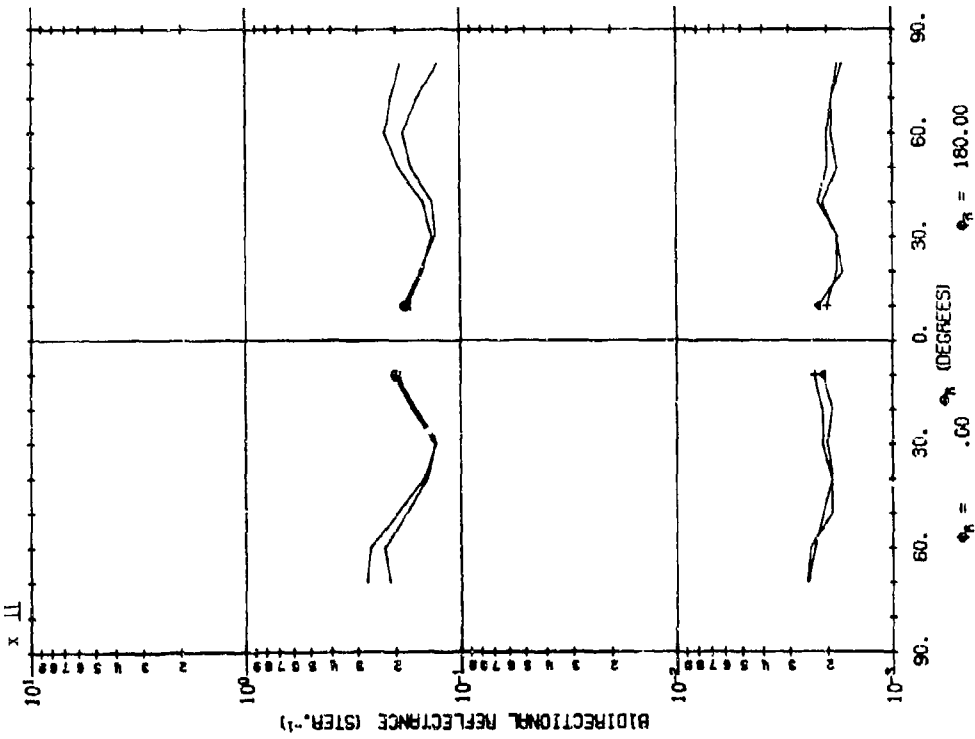


REFLECTANCE STANDARDS MATERIAL

R01272 001

CHROME PLATED GLASS BEADS

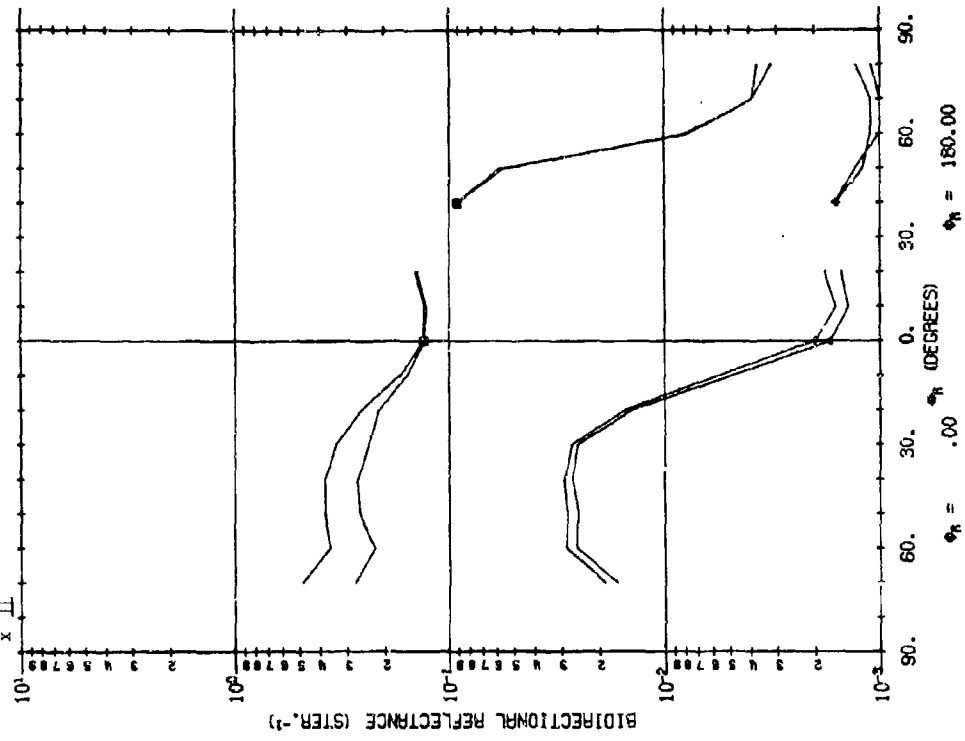
$\epsilon_1 = 0.0$
 $\epsilon_2 = 1.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$



R01272 001

CHROME PLATED GLASS BEADS

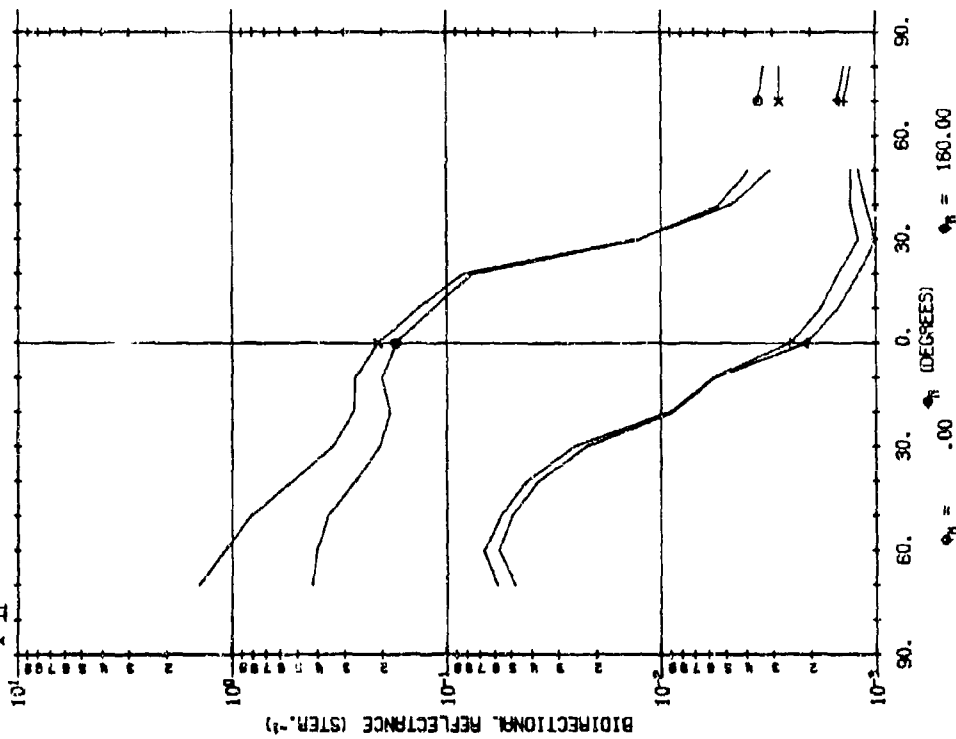
$\epsilon_1 = 30.0$
 $\epsilon_2 = 1.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$



R01272 001

CHROME PLATED GLASS BEADS

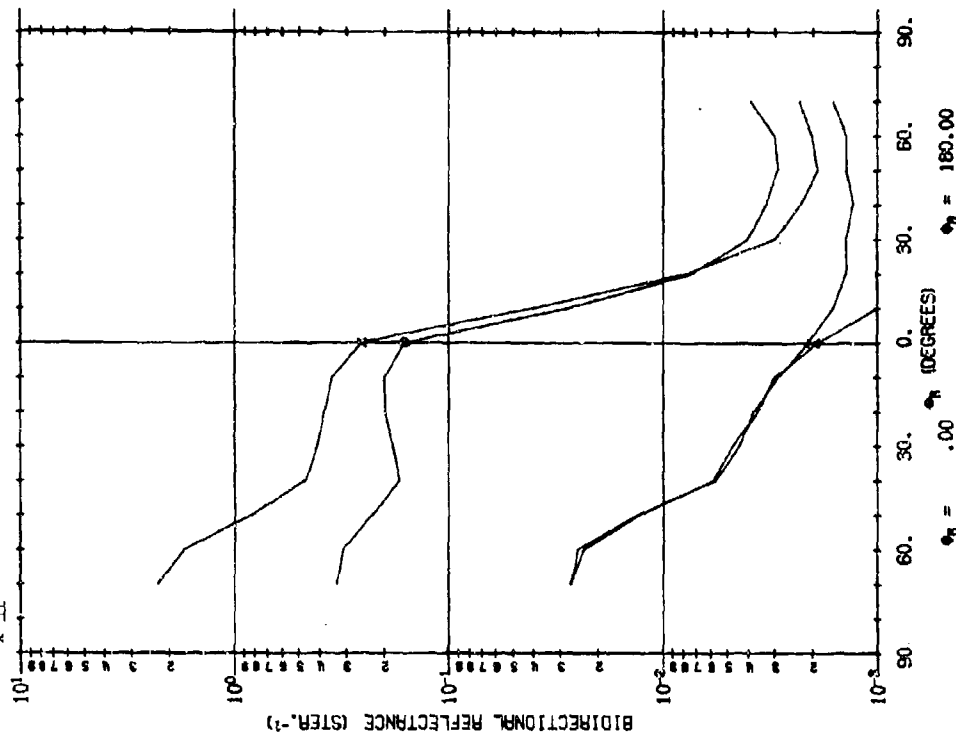
0 || $\phi_1 = 60.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 1.06$
x ||



R01272 001

CHROME PLATED GLASS BEADS

0 || $\phi_1 = 80.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 1.06$
x ||

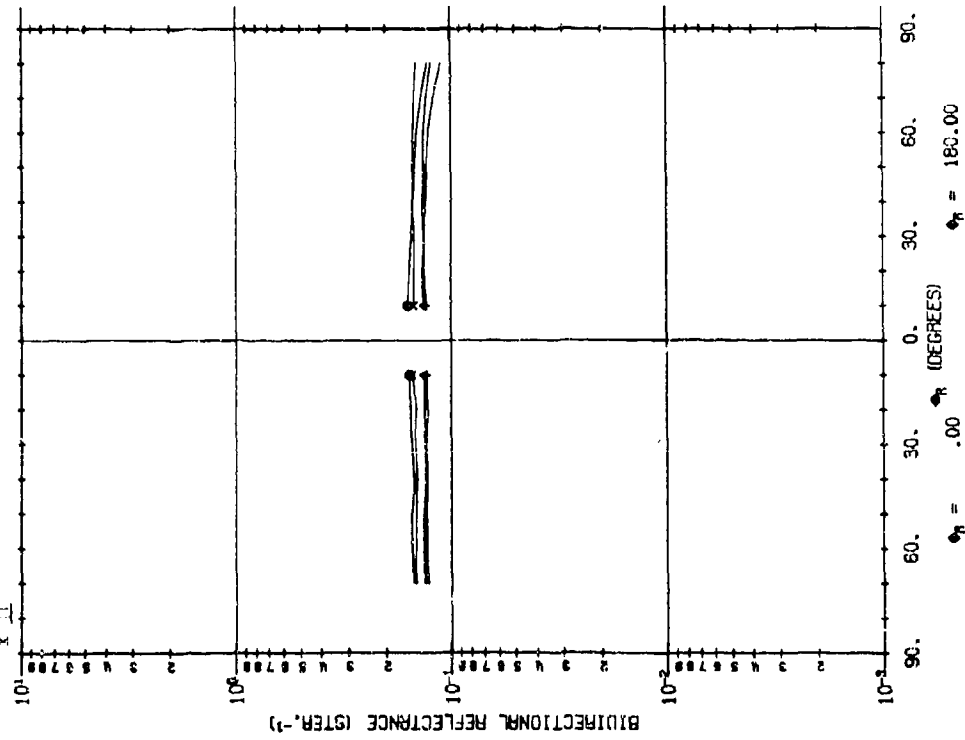


REFLECTANCE STANDARDS MATERIAL

A01290 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

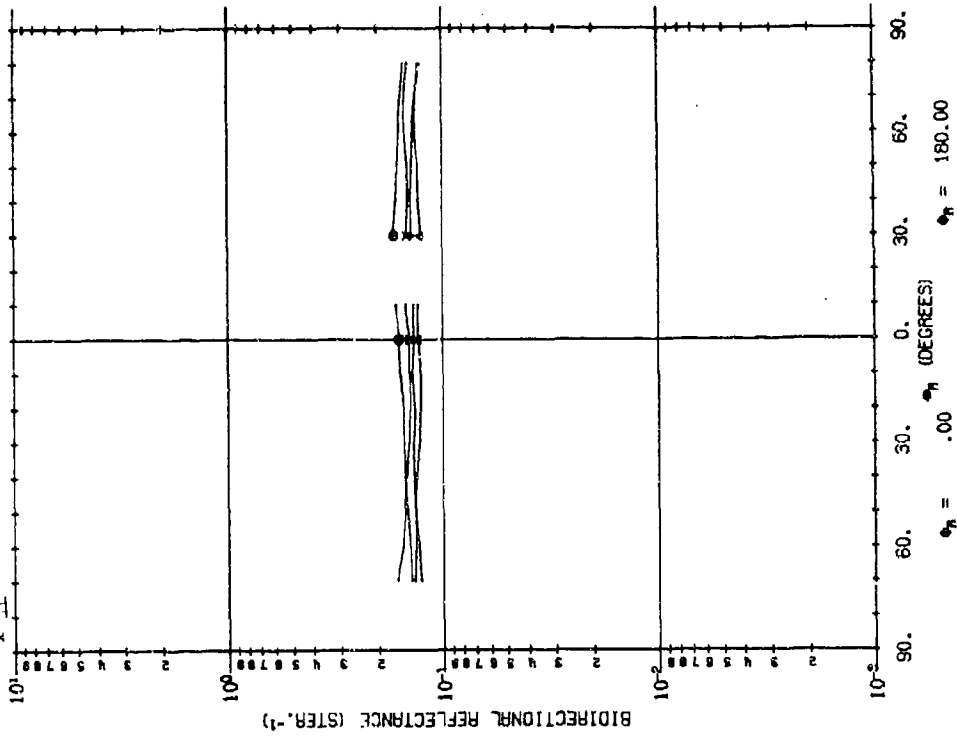
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
x || $\lambda = 1.06$



A01290 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

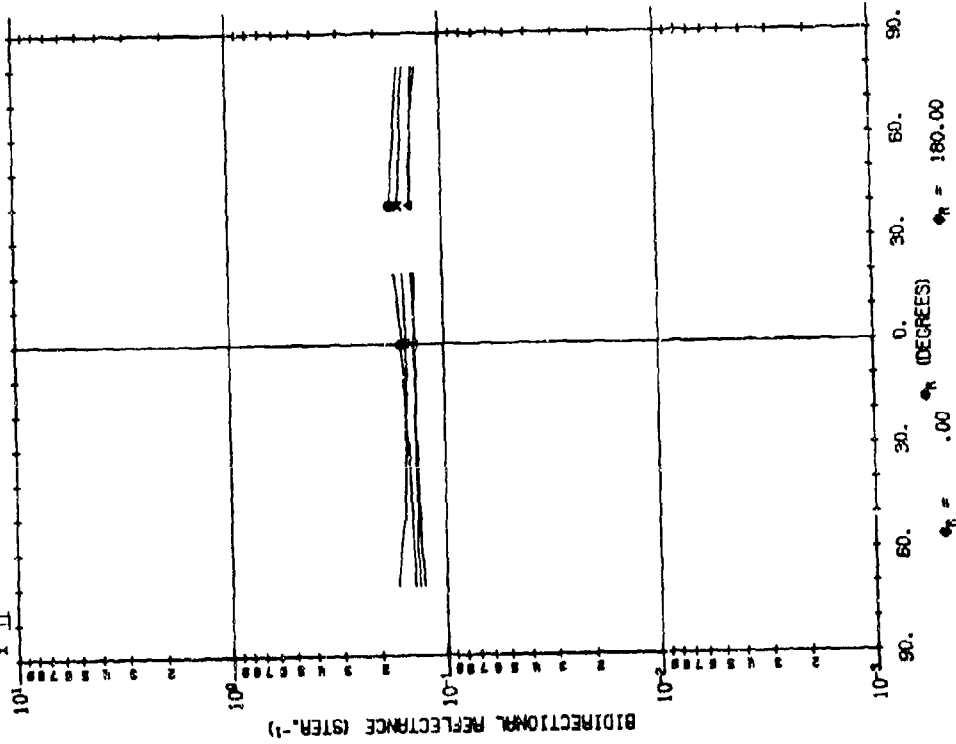
0 || $\phi_1 = 20.0$
+ || $\phi_2 = 180.0$
x || $\lambda = 1.06$



A01290 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

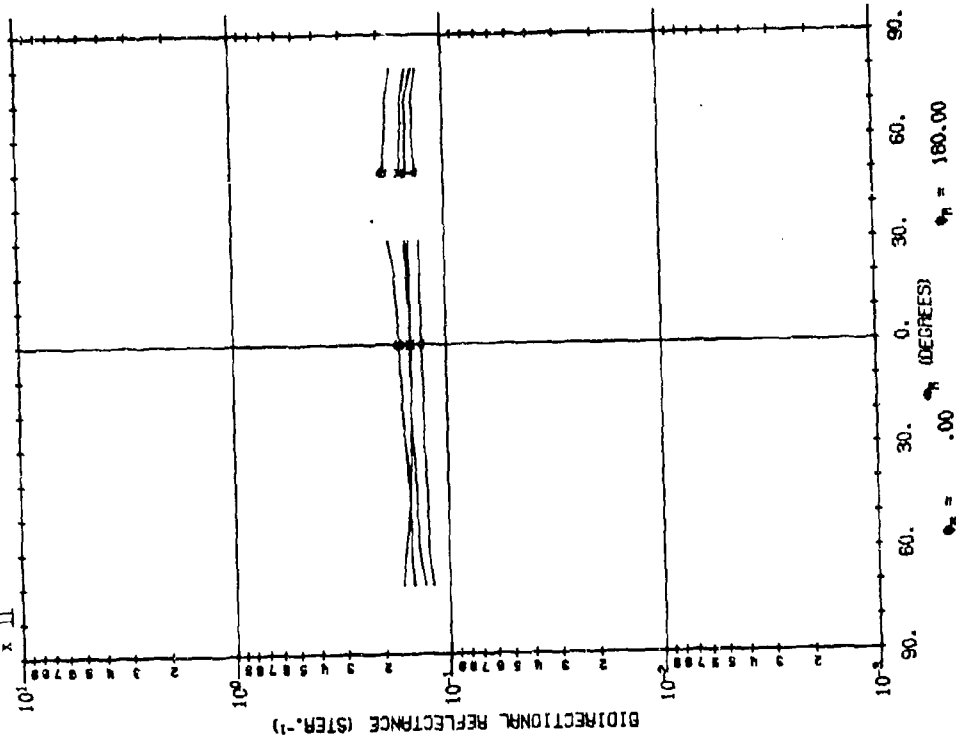
$\theta_1 = 30.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$



A01290 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

$\theta_1 = 40.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

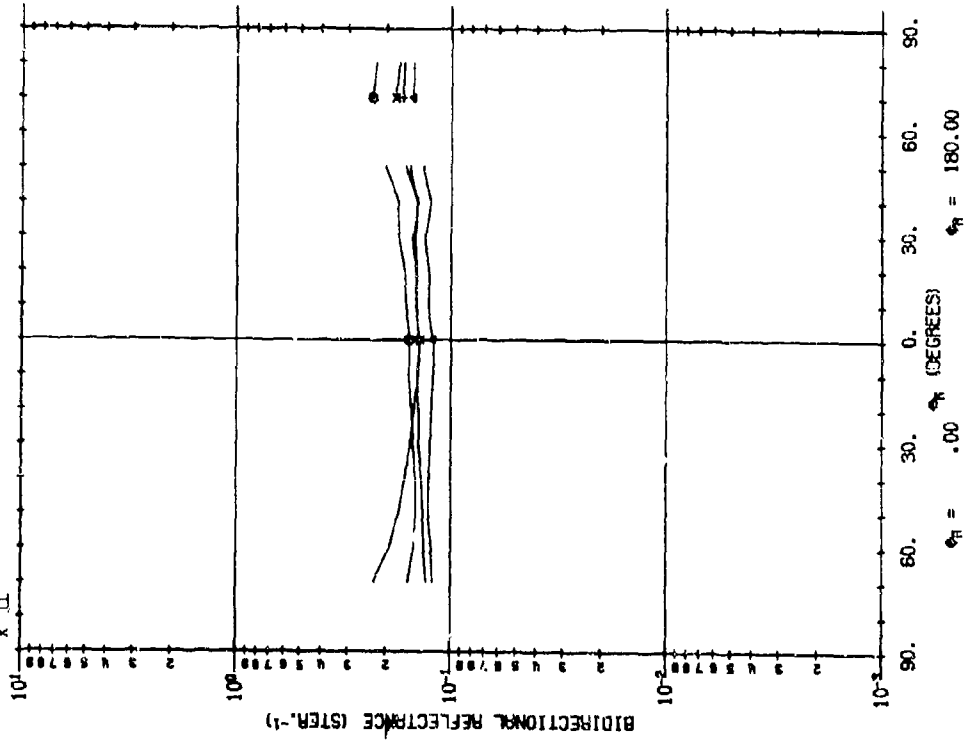


REFLECTANCE STANDARDS MATERIAL

R01230 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

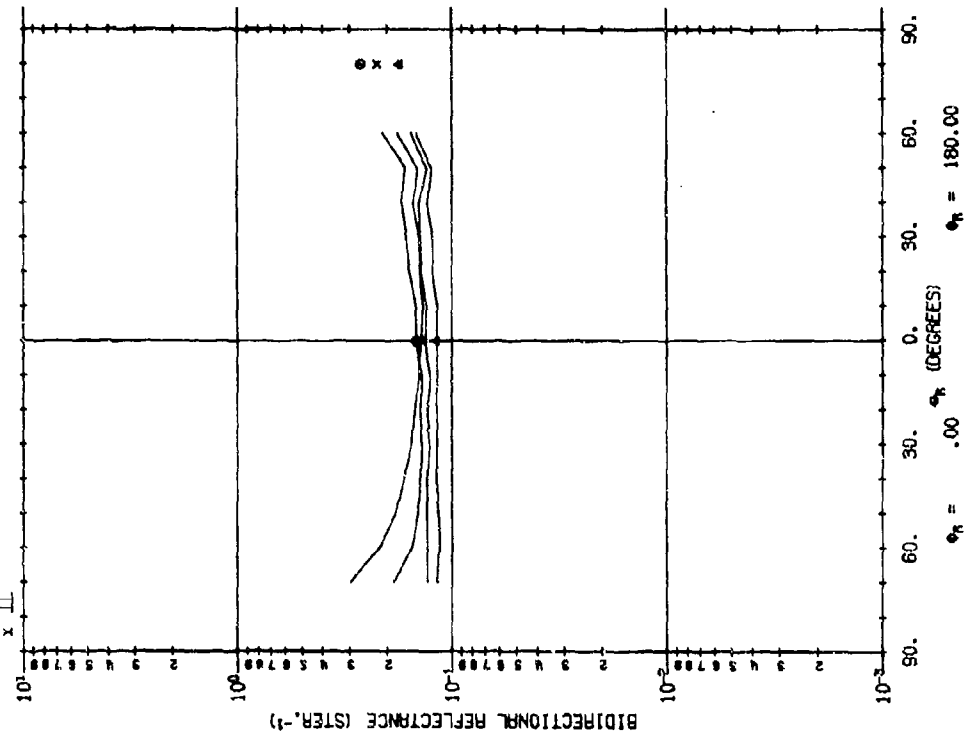
$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



R01290 001

TWO COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

$\theta_1 = 70.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

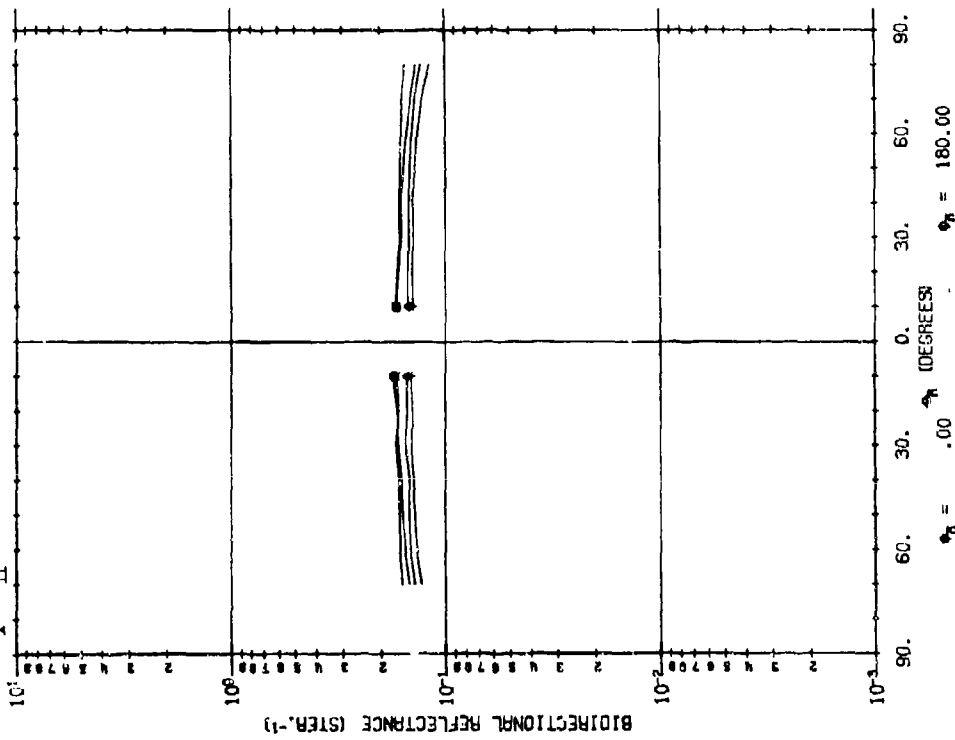


A01292 001

3M WHITE VELVET PAINT ON ALUMINUM

$\epsilon_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

0 ||
+ ||
△ ||
x ||

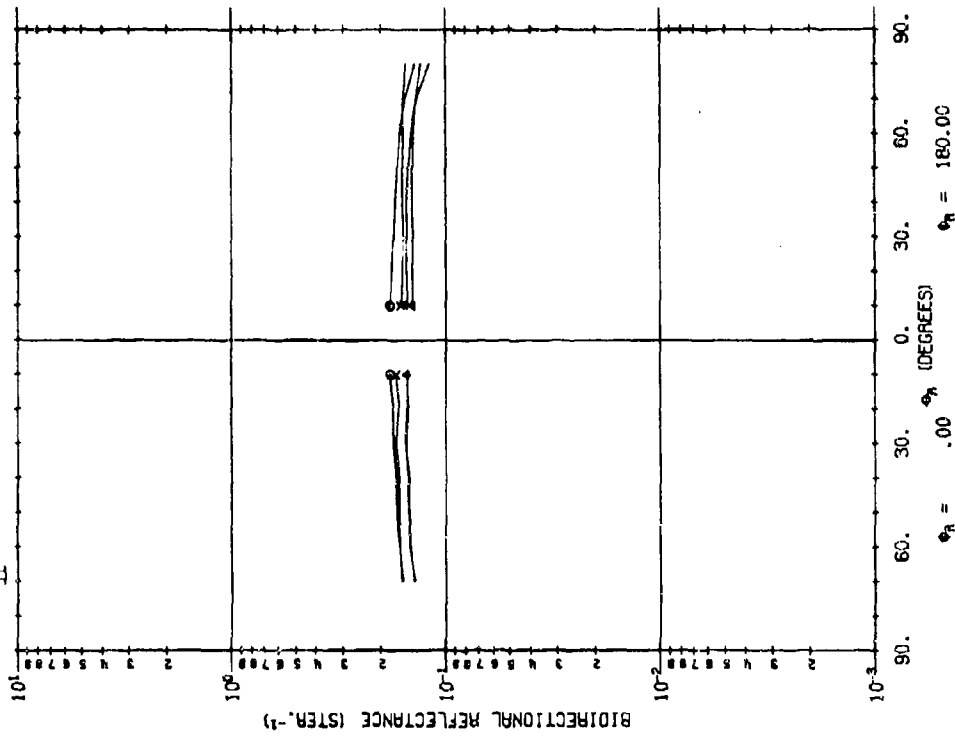


A01292 002

3M WHITE VELVET PAINT ON ALUMINUM

$\epsilon_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

0 ||
+ ||
△ ||
x ||



REFLECTANCE STANDARDS MATERIAL

R01292 003

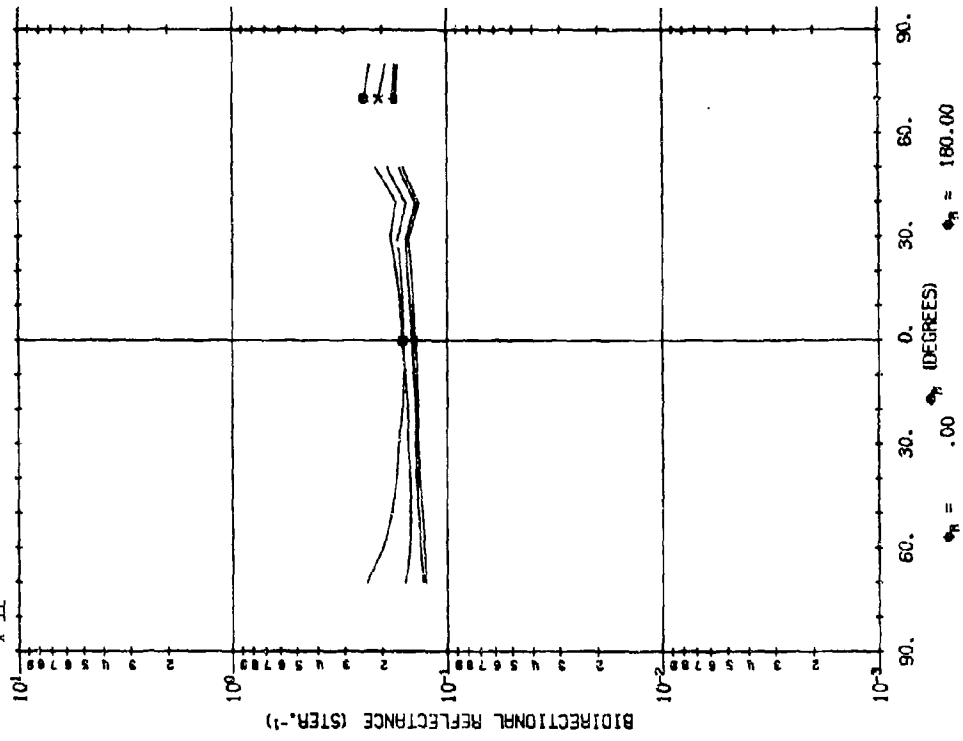
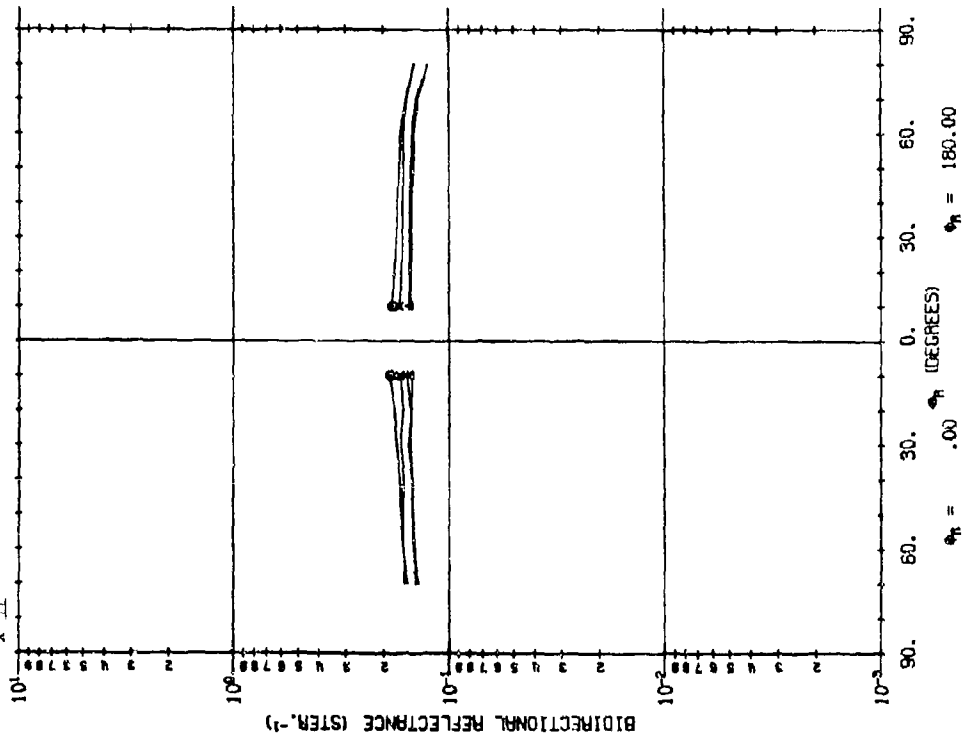
100 COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

$\theta_i = 0.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$

R01292 003

100 COATS 3M WHITE PAINT ON ZINC
CHROMATE PRIMER ON ANODIZED ALUMINUM

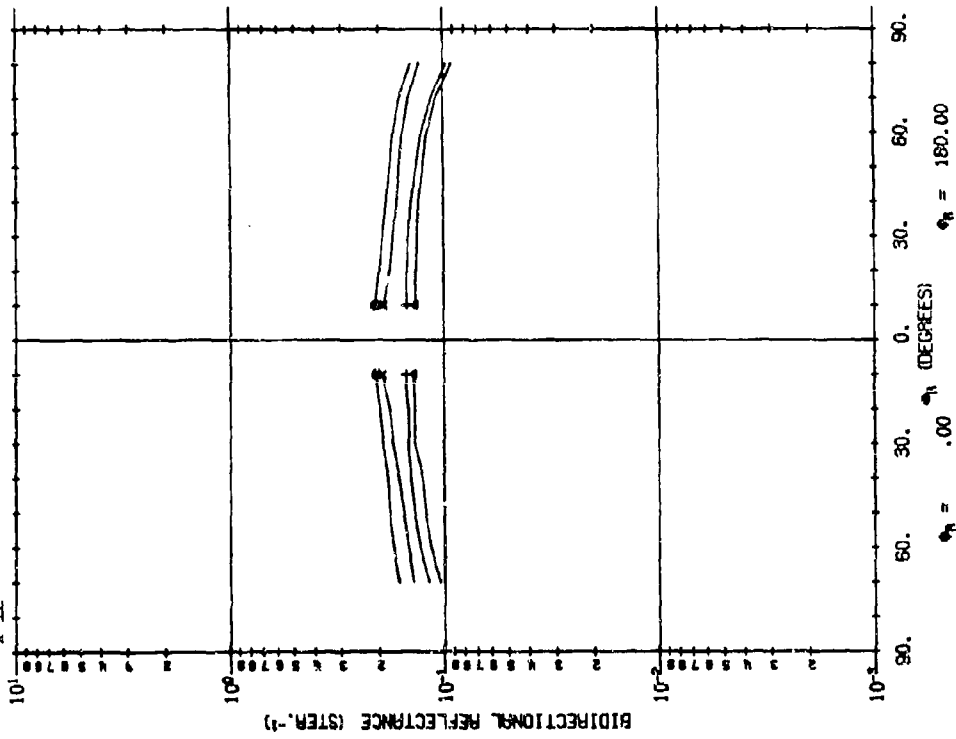
$\theta_i = 60.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$



A01293 001

FIBERFRAX TYPE 970 JR ON 1/4" PLYWOOD

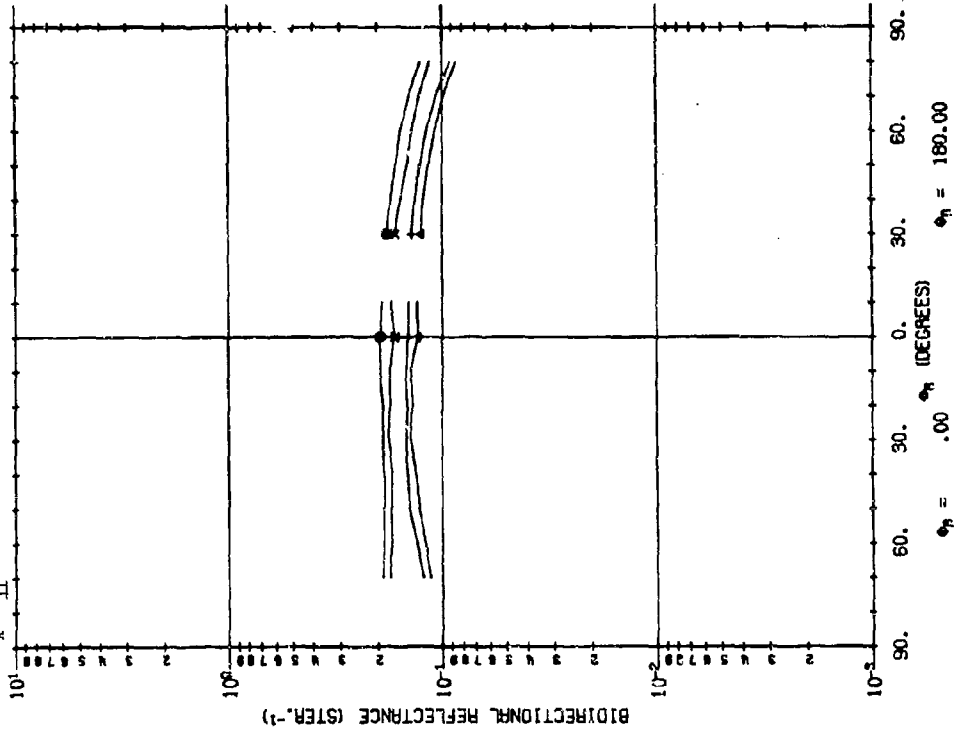
$\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



A01293 001

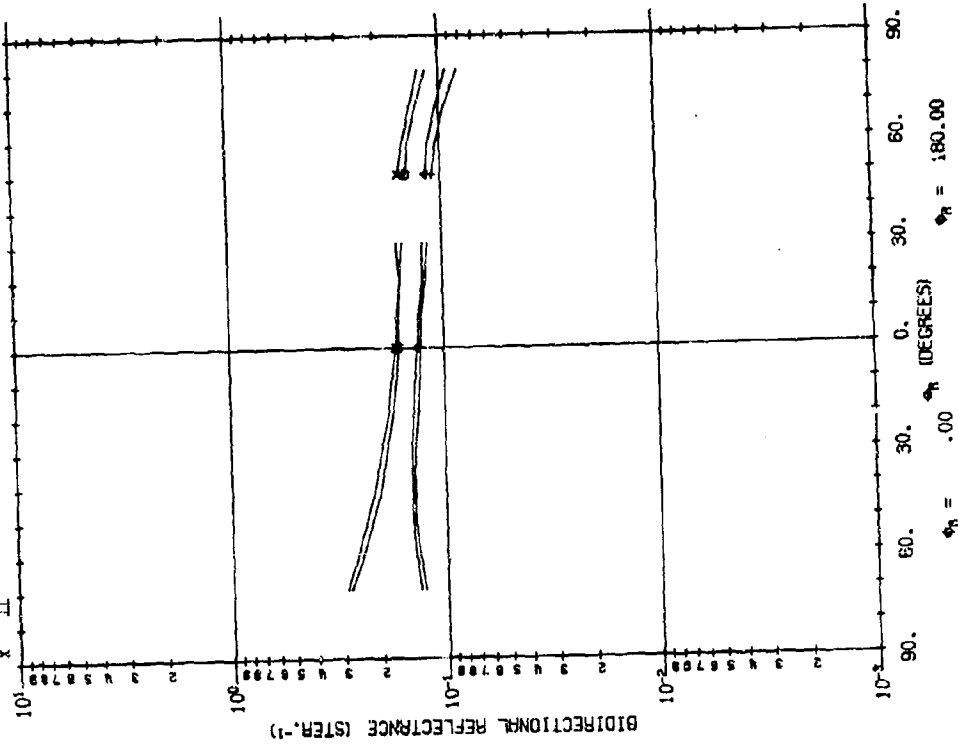
FIBERFRAX TYPE 970 JS ON 1/4" PLYWOOD

$\theta_1 = 20.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

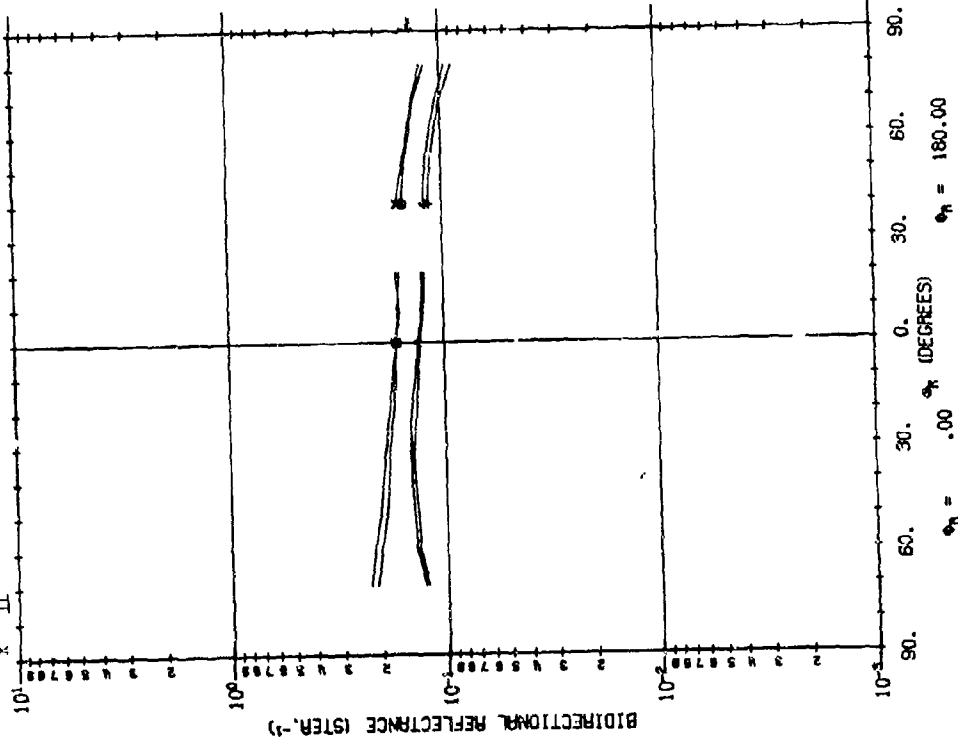


REFLECTANCE STANDARDS MATERIAL

R01293 001
 FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD
 $\theta_1 = 40.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$



R01293 001
 FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD
 $\theta_1 = 30.0$
 $\phi_1 = 180.0$
 $\lambda = 1.06$

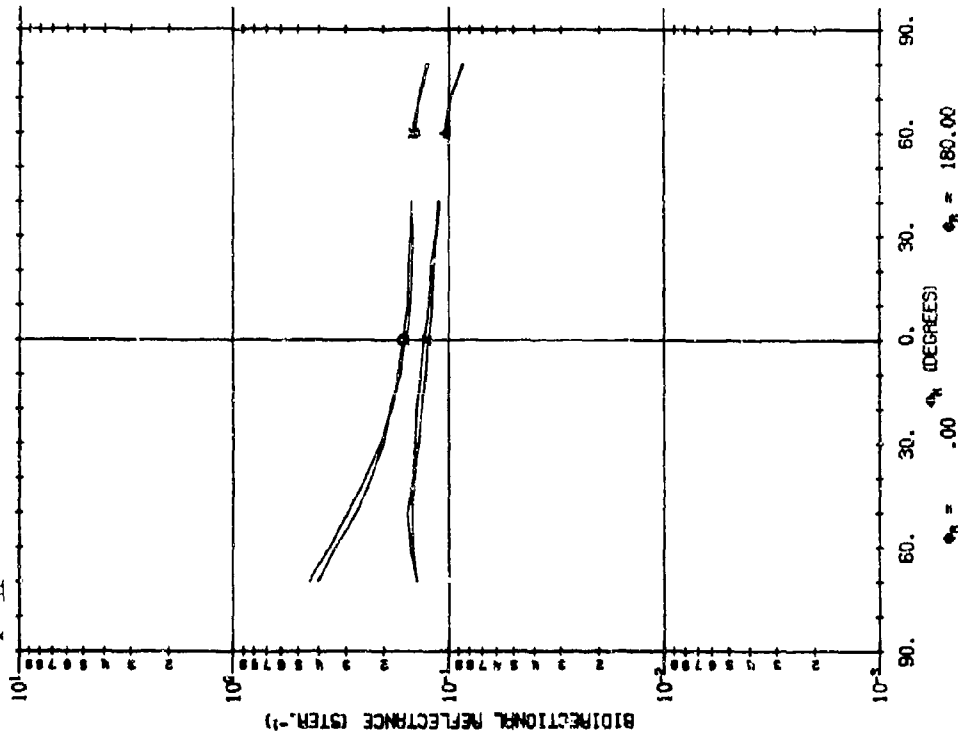


R01293 001

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

0 ||
+ ||
Δ ||
x ||

$\theta_1 = 50.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



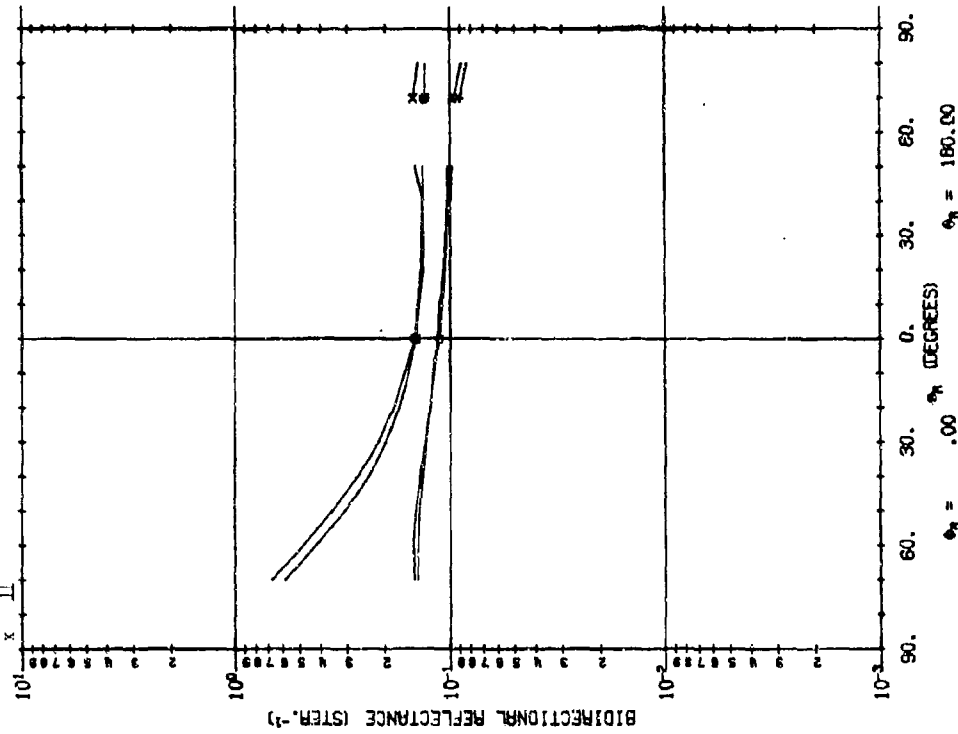
$\theta_1 = .00$ $\theta_2 = 180.00$

R01293 001

FIBERFRAX TYPE 970 JH ON 1/4" PLYWOOD

0 ||
+ ||
Δ ||
x ||

$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$



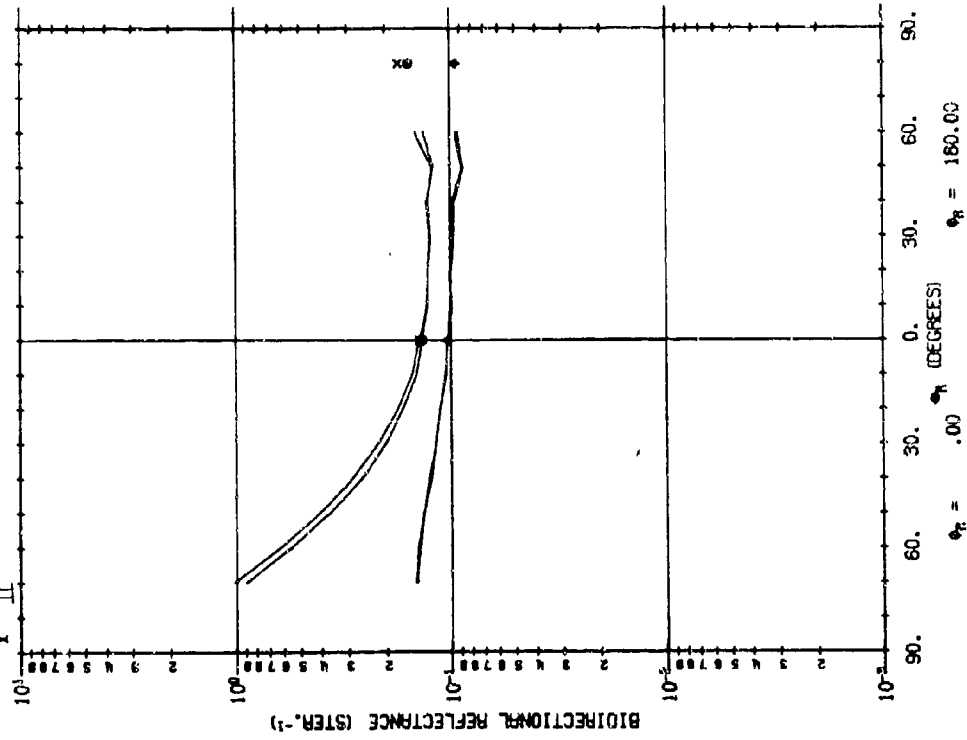
$\theta_1 = .00$ $\theta_2 = 180.00$

REFLECTANCE STANDARDS MATERIAL

B01293 001

FIBREFRAX TYPE 97C JH ON 1/4" PLYWOOD

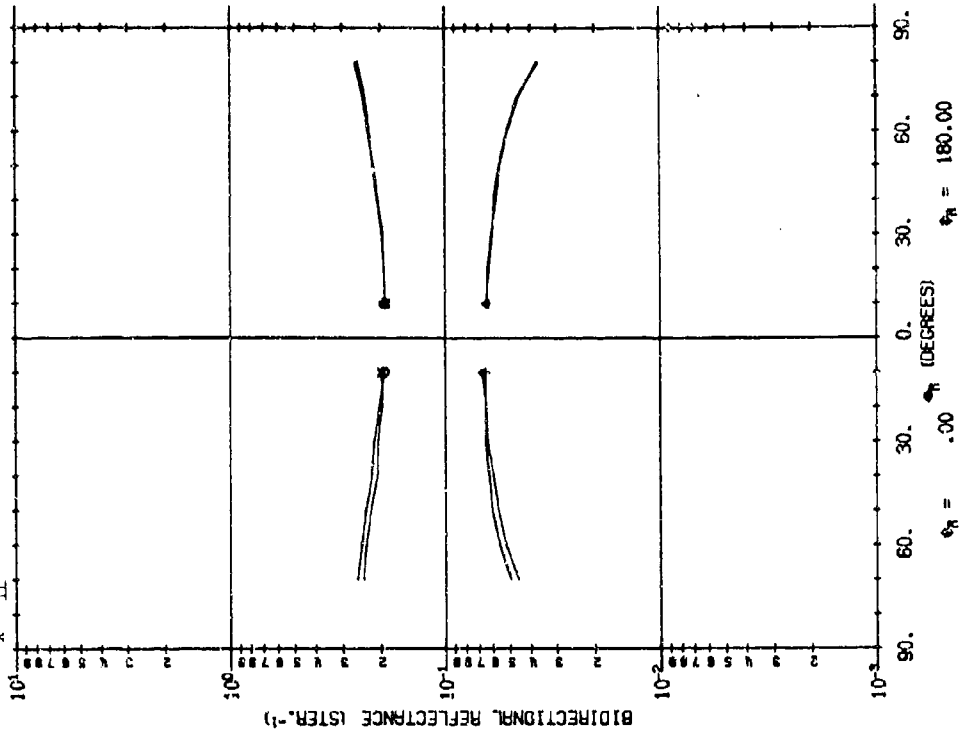
0 || $\phi_1 = 70.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 1.06$
X ||



B01296 001

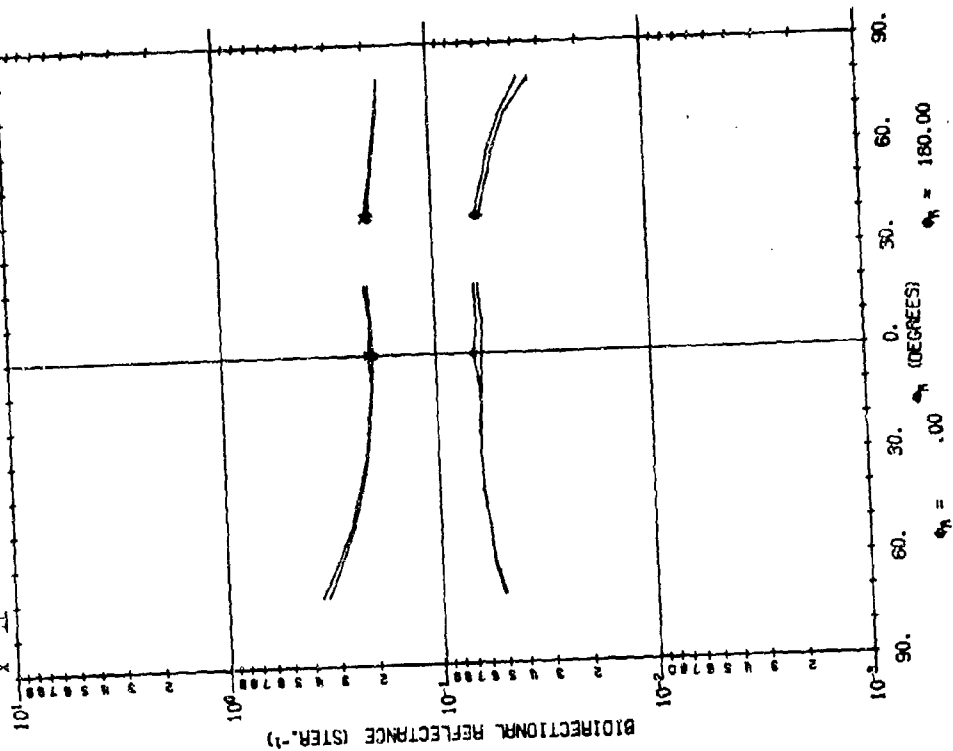
SANDBLASTED COPPER PLATED STAINLESS STEEL

0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
Δ || $\lambda = 1.06$
X ||



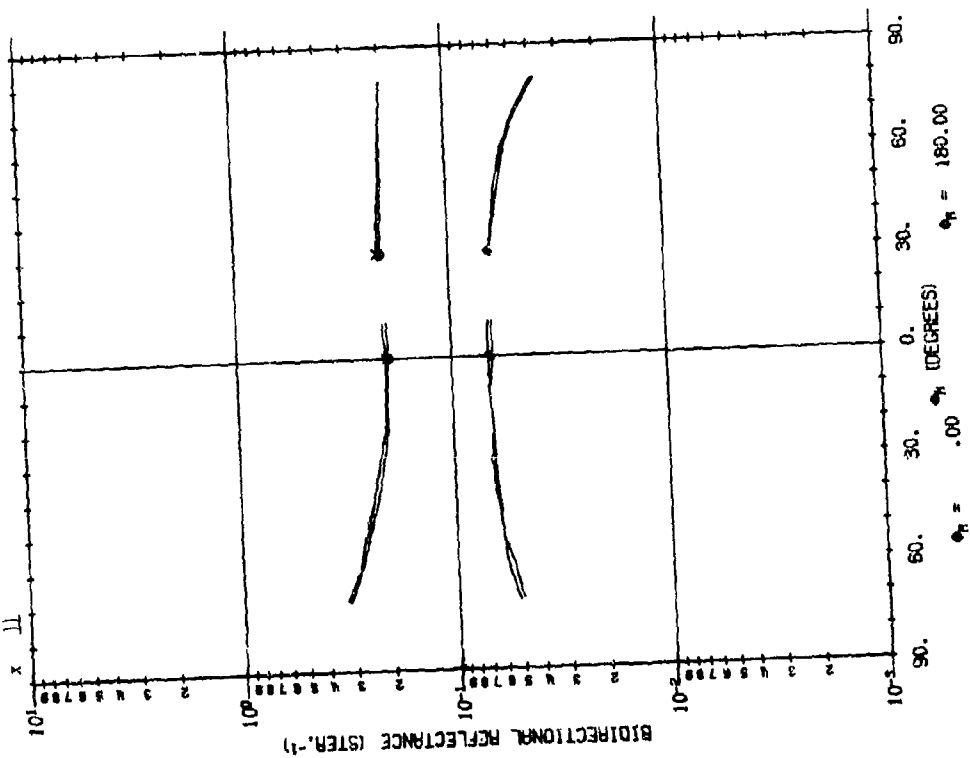
A01296 001
SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_i = 30.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$



A01296 001
SANDBLASTED COPPER PLATED STAINLESS STEEL

$\theta_i = 20.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$

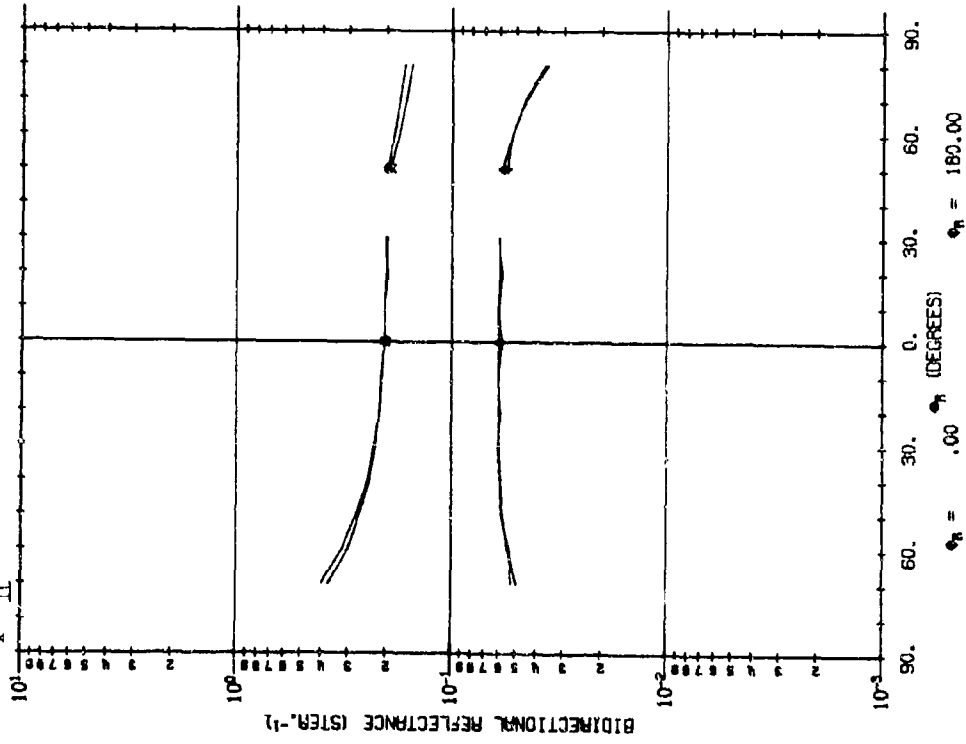


REFLECTANCE STANDARDS MATERIAL

A01296 001

SANDBLASTED COPPER PLATED STAINLESS STEEL

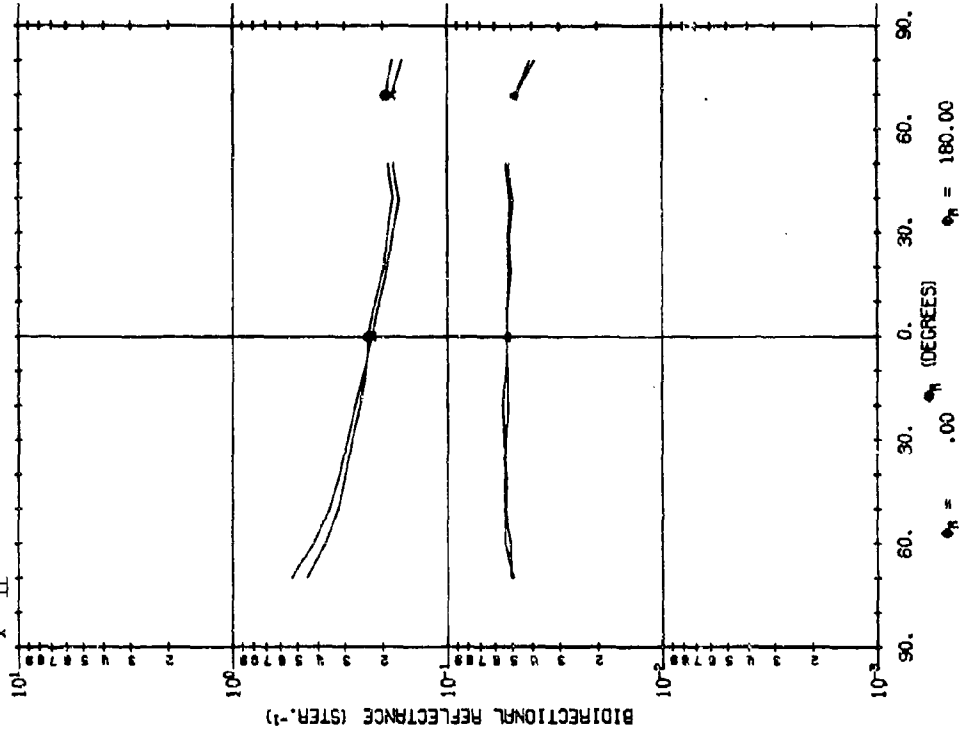
0 || $\theta_2 = 40.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 1.06$
 X ||



A01295 001

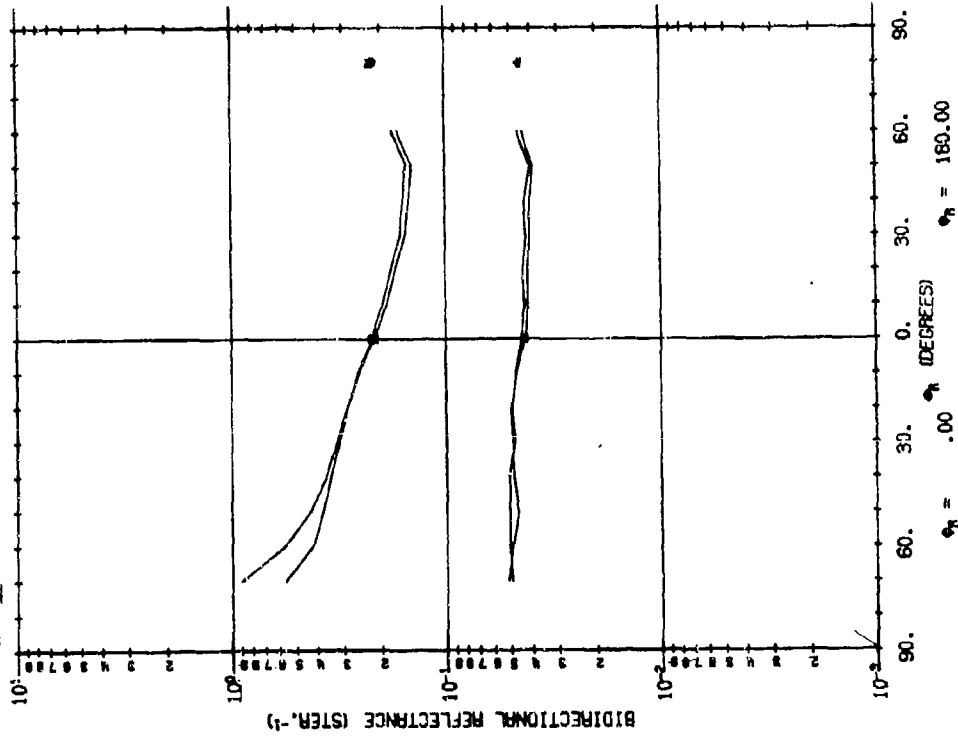
SANDBLASTED COPPER PLATED STAINLESS STEEL

0 || $\theta_1 = 60.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 1.06$
 X ||



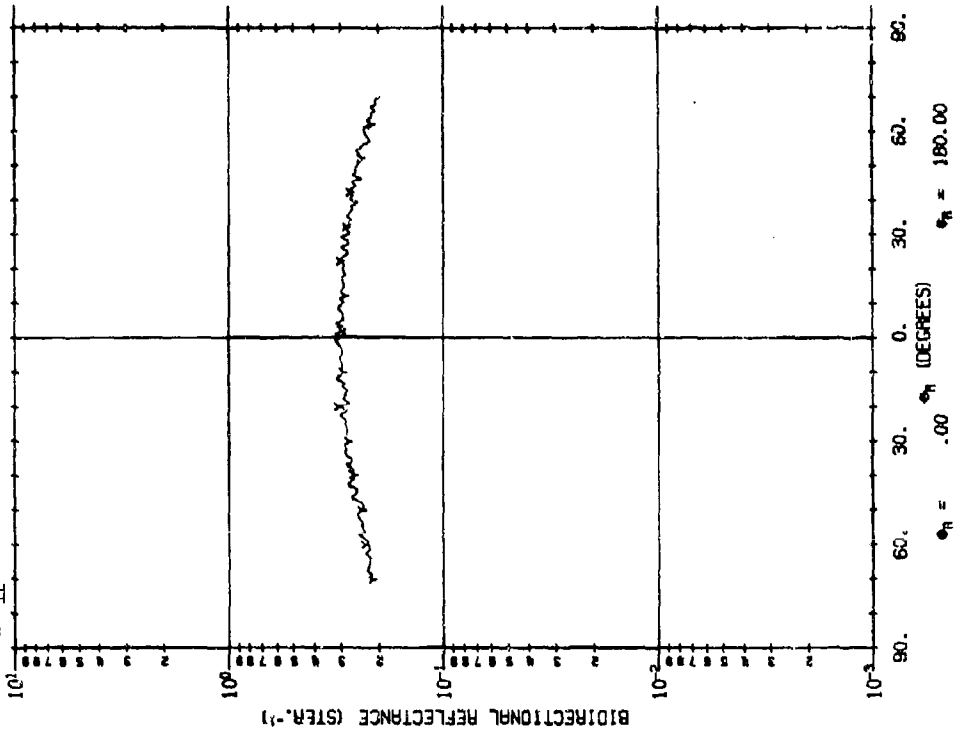
R01296 001
 0 || $\theta_1 = 70.0$
 + || $\phi_1 = 180.0$
 Δ || $\lambda = 1.06$
 X ||

SANDBLASTED COPPER PLATED STAINLESS STEEL



R01296 101
 0 || 25 = 2.0
 + || $\phi_1 = \phi_r$
 Δ || $\lambda = 10.6$
 X || $\gamma = 0^\circ$

SANDBLASTED COPPER PLATED STAINLESS STEEL

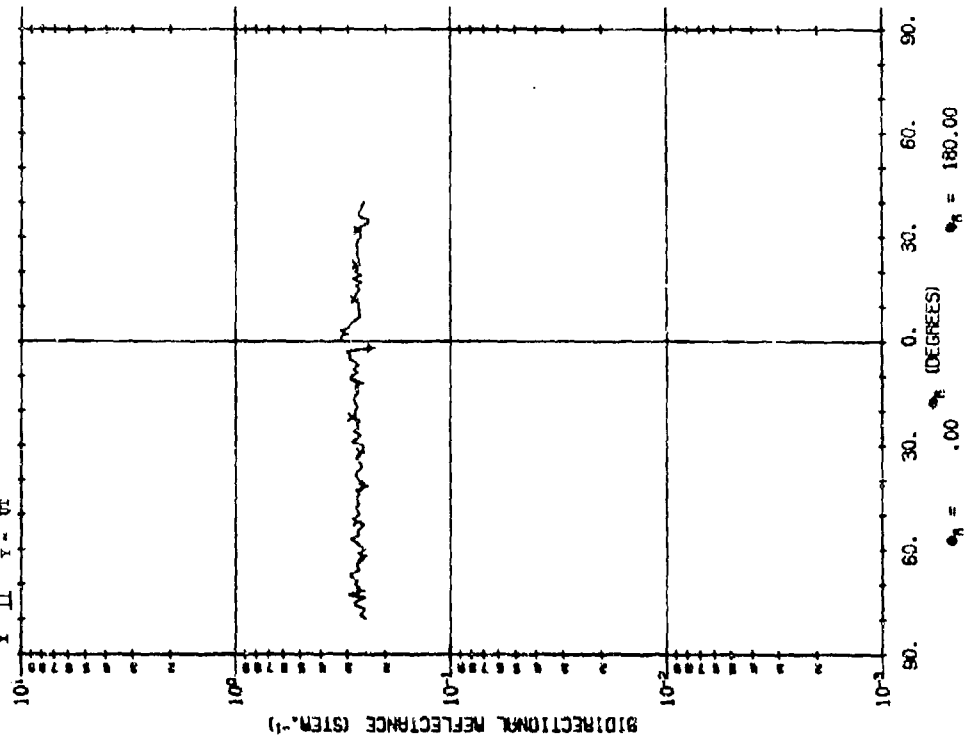


REFLECTANCE STANDARDS MATERIAL

R01296 101

SANDBLASTED COPPER PLATED STAINLESS STEEL

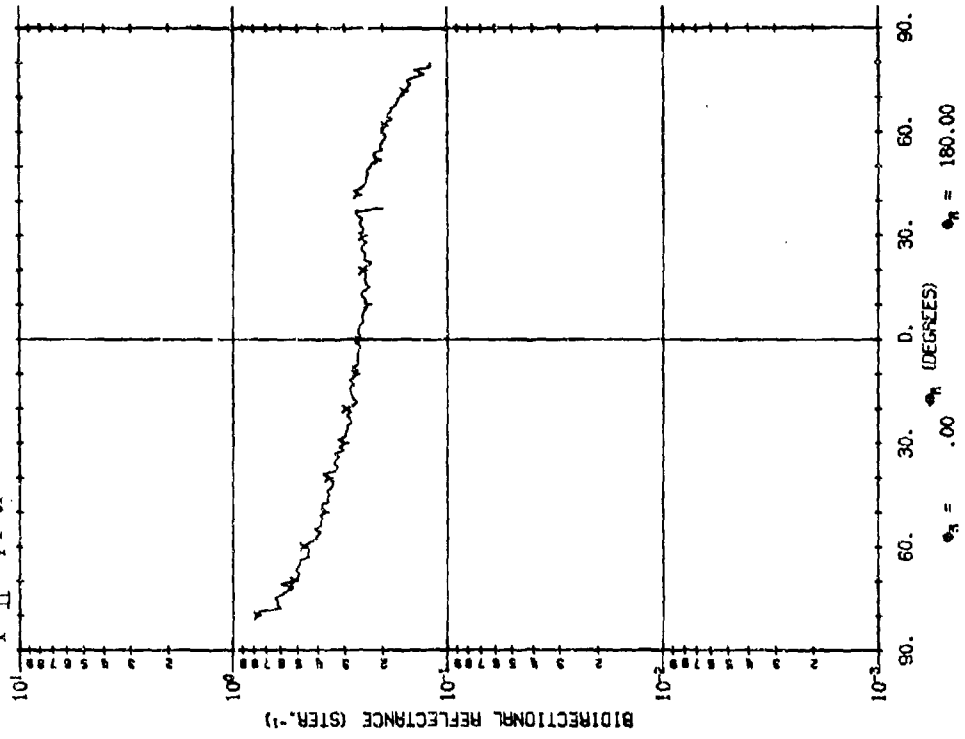
0 || $\epsilon_1 = 0.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || $\psi = \psi$



R01296 101

SANDBLASTED COPPER PLATED STAINLESS STEEL

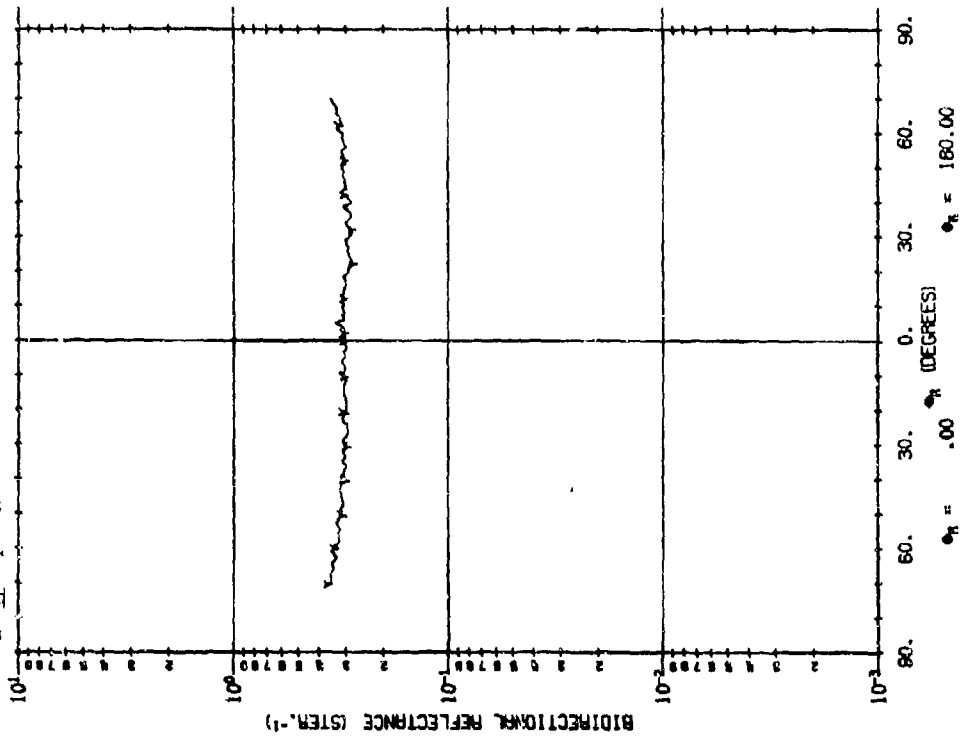
0 || $\epsilon_1 = 40.0$
+ || $\phi_1 = 180.0$
Δ || $\lambda = 10.6$
X || $\psi = \psi$



R01297 101

WHITE SALT STANDARD

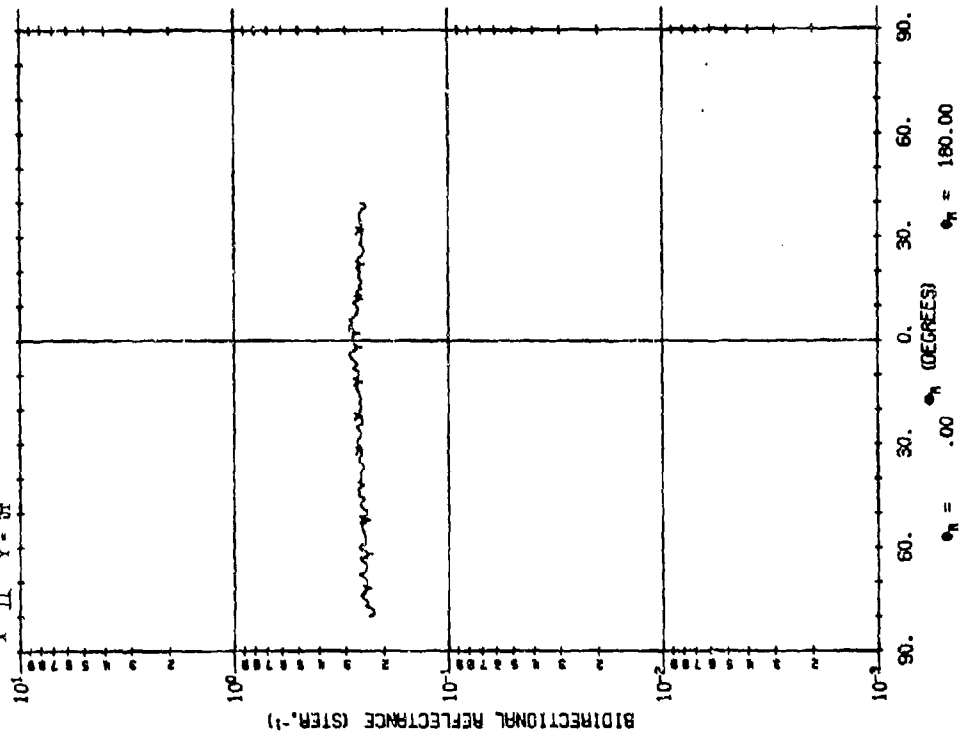
0 || $2\theta = 2.0$
+ || $\phi_1 = \phi_2$
 Δ || $\lambda = 10.6$
X || $\gamma = \gamma'$



R01297 101

WHITE SALT STANDARD

0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
 Δ || $\lambda = 10.6$
X || $\gamma = \gamma'$



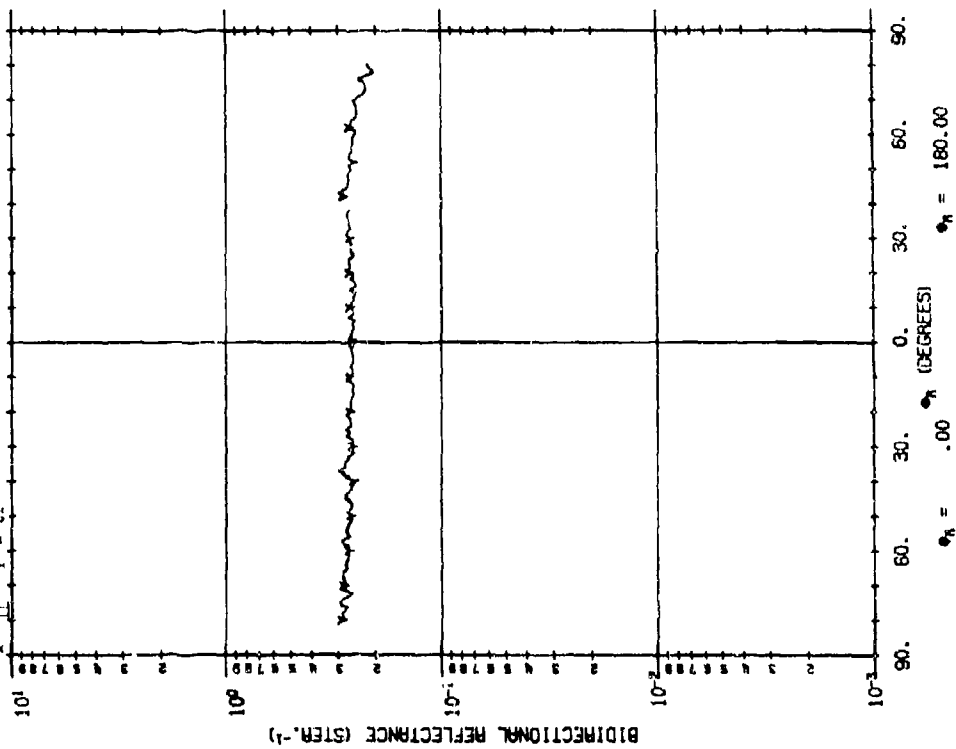
REFLECTANCE STANDARDS MATERIAL

R01297 101

WHITE SALT STANDARD

$\theta_1 = 40.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$

X Y Z VT

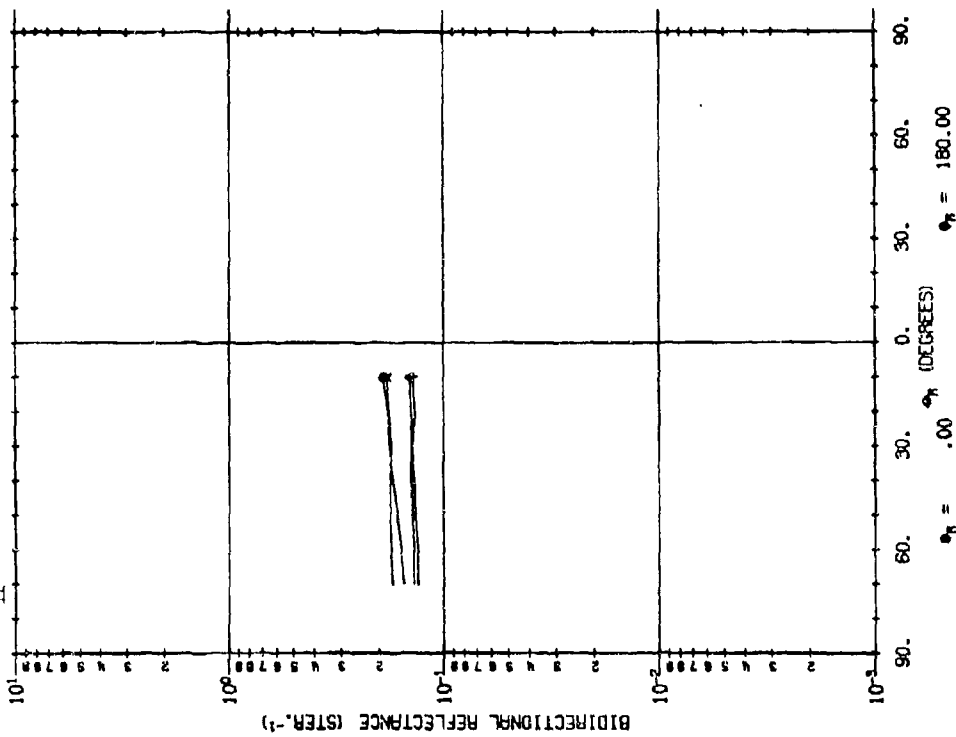


R01317 001

PRESSED MAGNESTON OXIDE

$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 0.63$

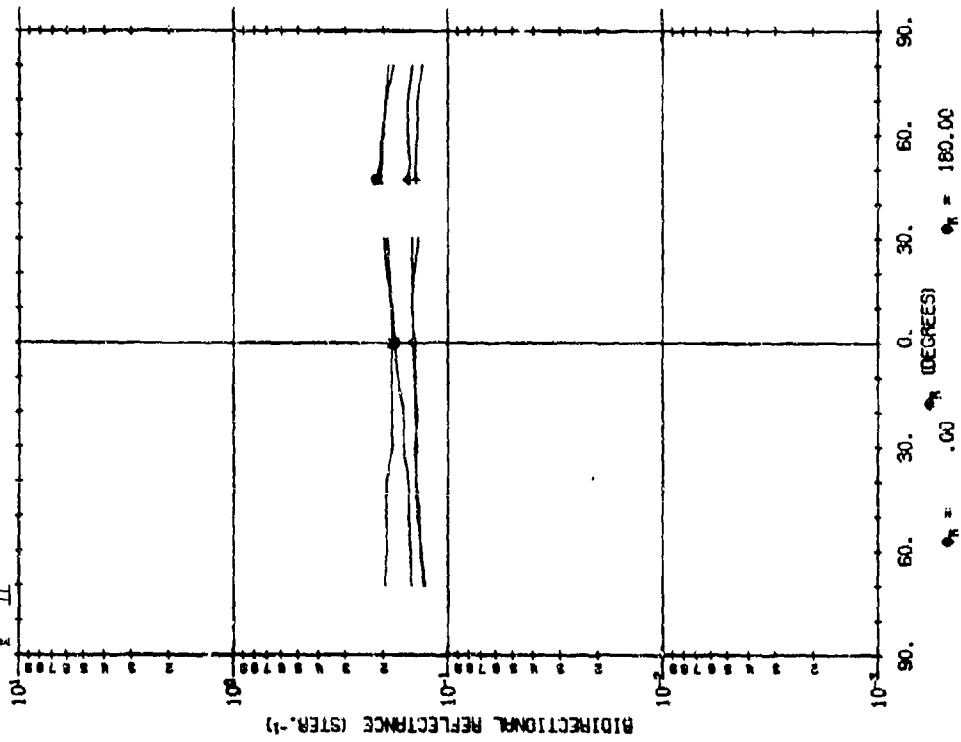
X



A01317 001

PRESSED MAGNESIUM OXIDE

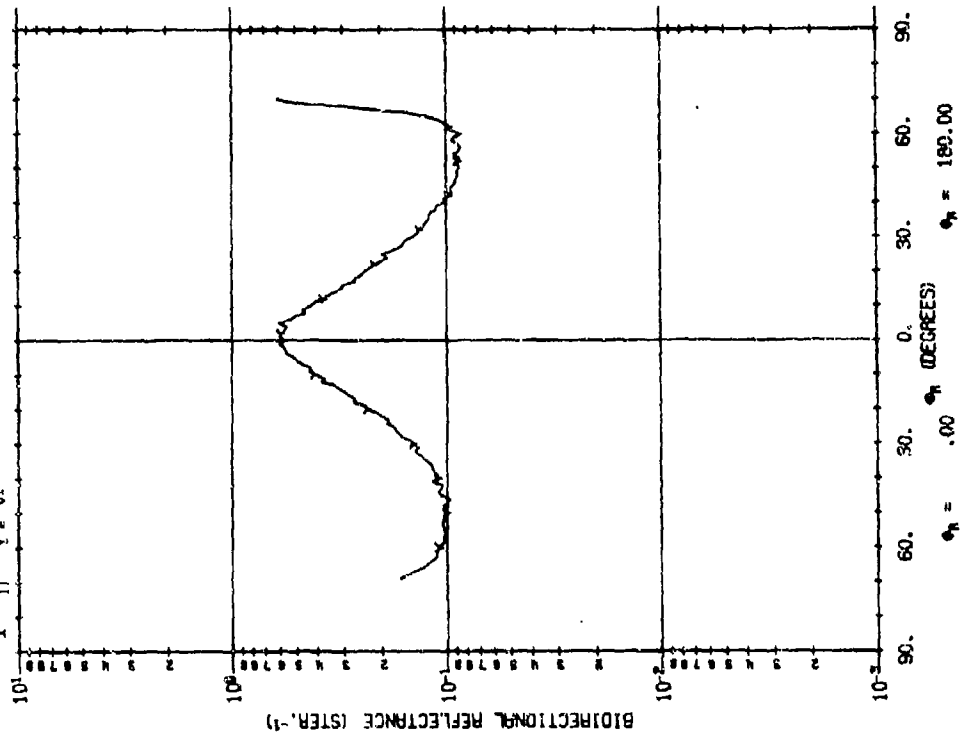
0 || $\theta_1 = 40.0$
 + || $\theta_2 = 180.0$
 Δ || $\lambda = 0.63$
 X ||



A01331 101

GOLD PLATED SILICON CARBIDE PAPER

0 || $2\theta = 2.0$
 + || $\theta_1 = \theta_2$
 Δ || $\lambda = 10.6$
 X || $\gamma = \gamma'$

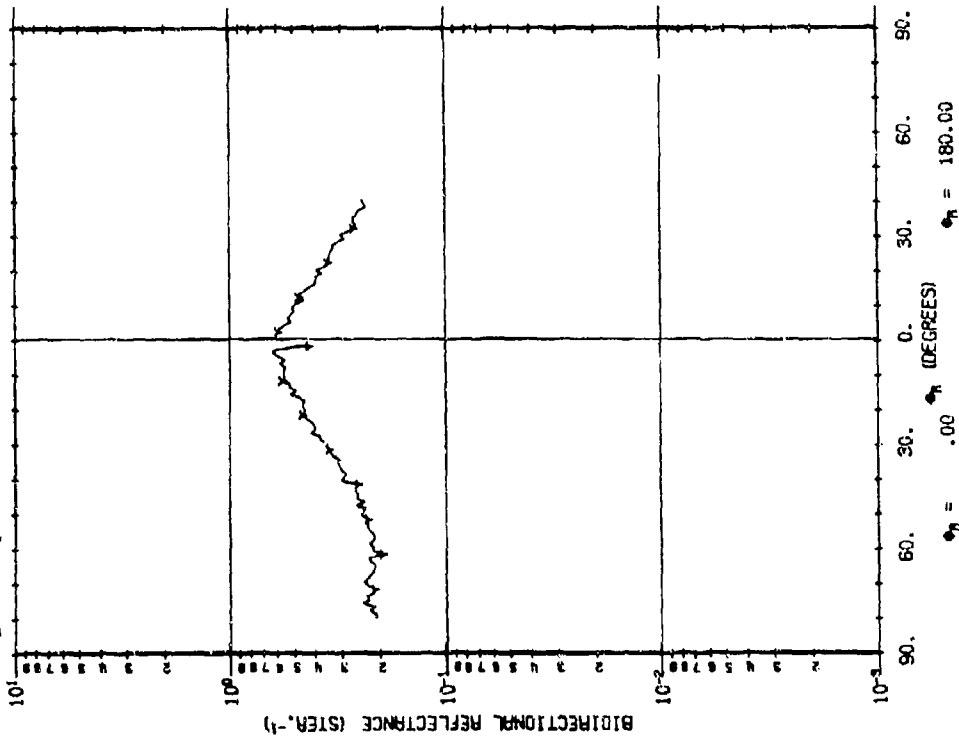


REFLECTANCE STANDARDS MATERIAL

R01331 101

GOLD PLATED SILICON CARBIDE PAPER

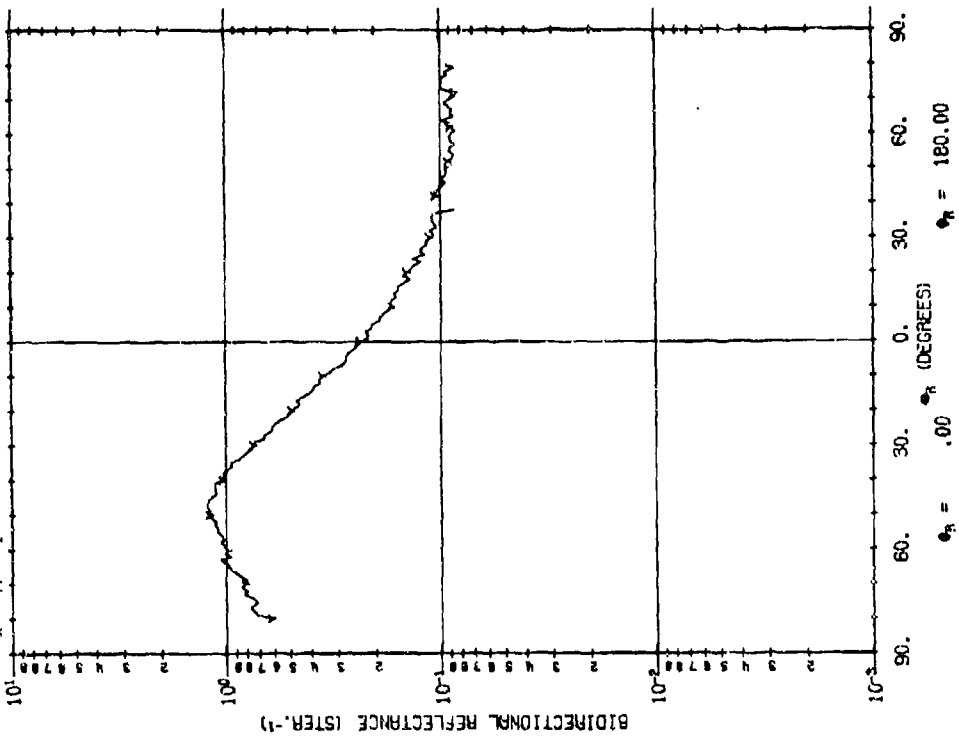
$\theta_1 = 0.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
Y = UT



R01331 101

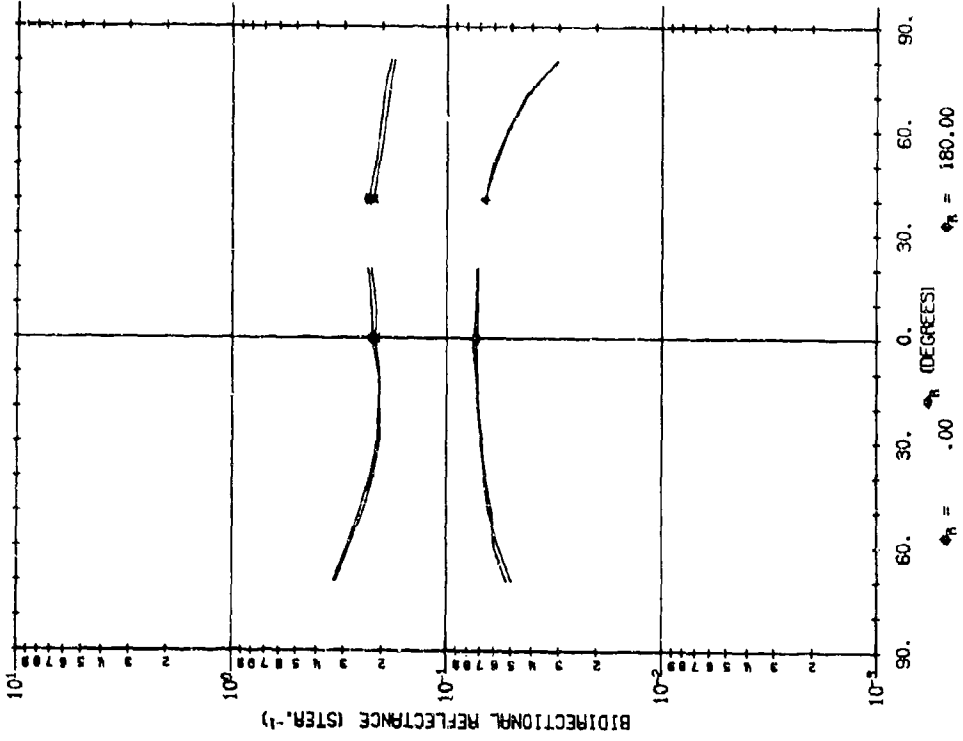
GOLD PLATED SILICON CARBIDE PAPER

$\theta_1 = 40.0$
 $\phi_1 = 180.0$
 $\lambda = 10.6$
Y = UT



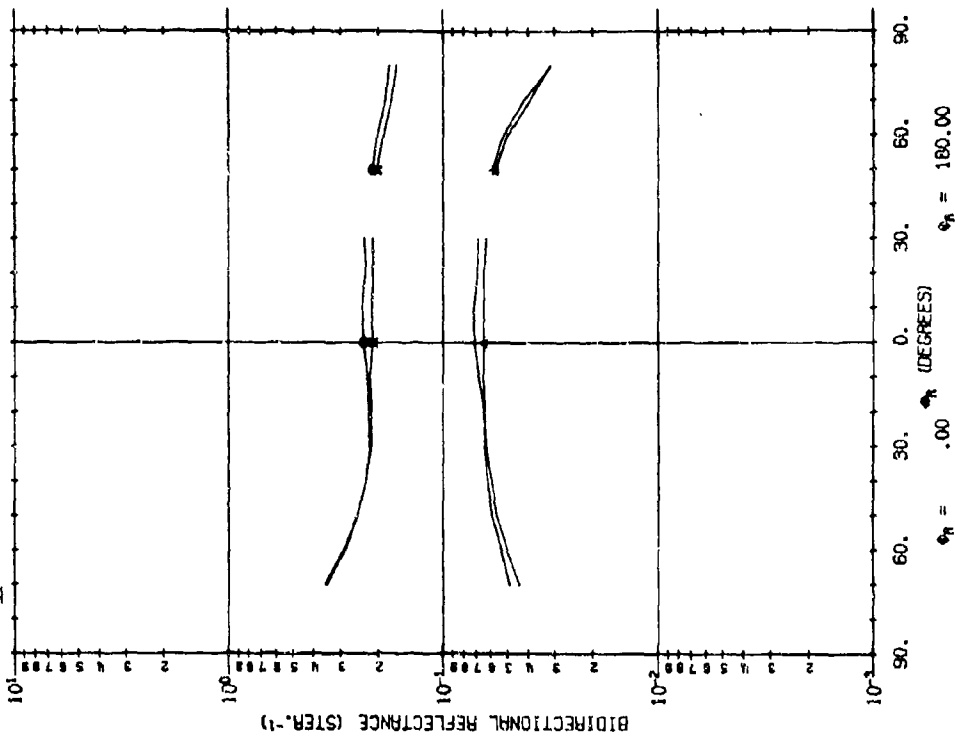
A01332 001
 $\theta_1 = 30.0$
 $\theta_2 = 180.0$
 $\lambda = 1.36$

COPPER PLATED STAINLESS STEEL



A01332 001
 $\theta_1 = 40.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

COPPER PLATED STAINLESS STEEL

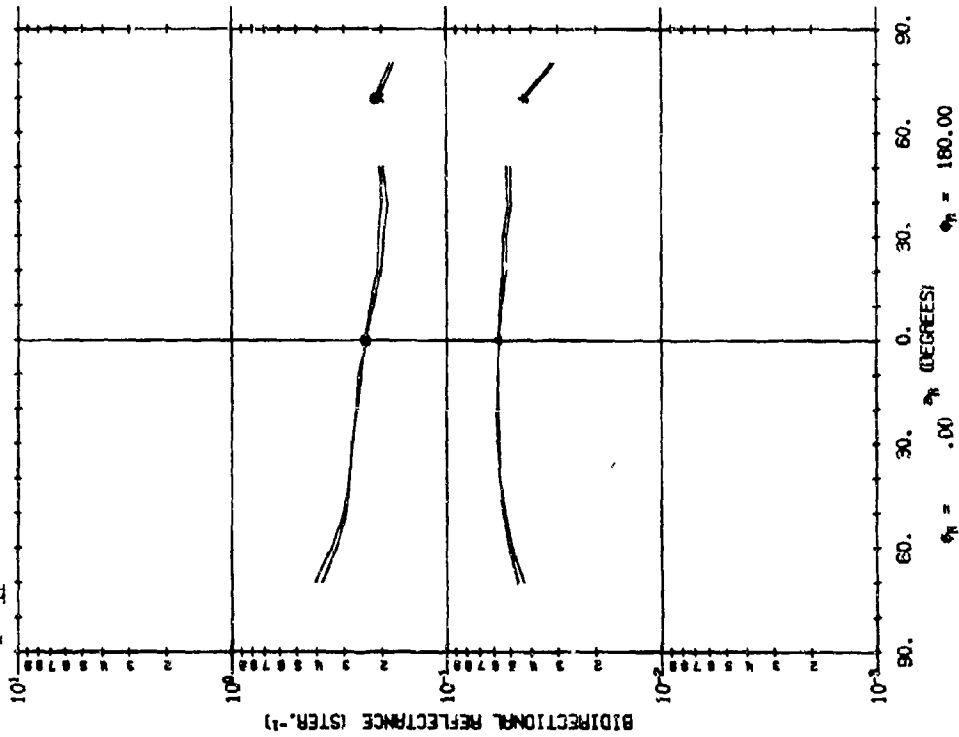


A01332 001

COPPER PLATED STAINLESS STEEL

$\theta_1 = 60.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

0 || ||
+ || ||
A || ||
X || ||

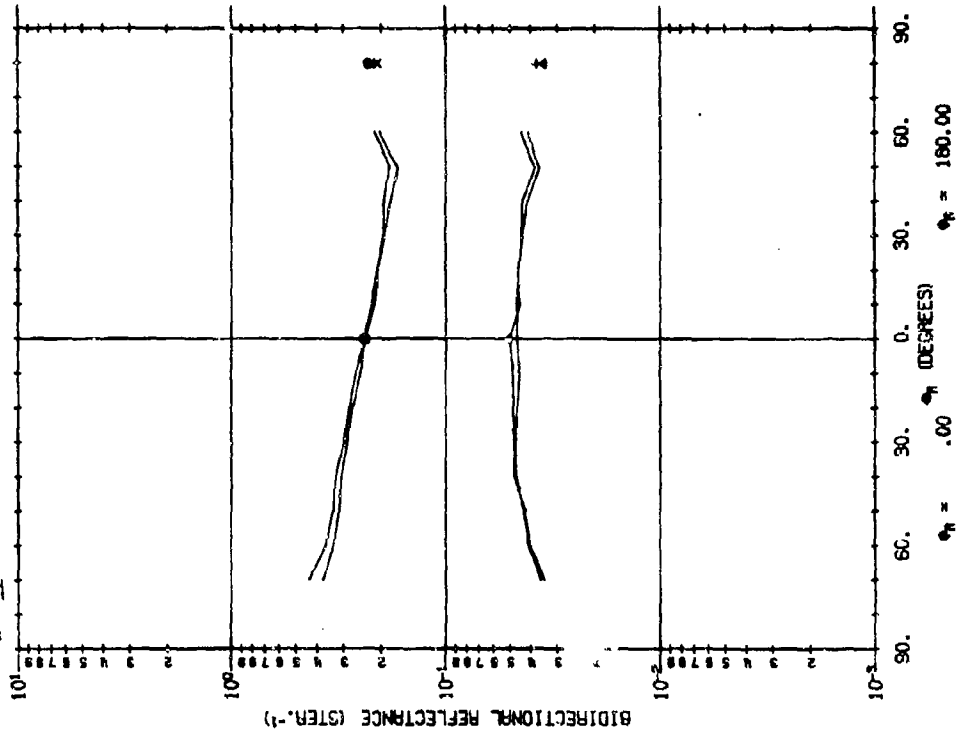


A01332 001

COPPER PLATED STAINLESS STEEL

$\theta_1 = 70.0$
 $\theta_2 = 180.0$
 $\lambda = 1.06$

0 || ||
+ || ||
A || ||
X || ||

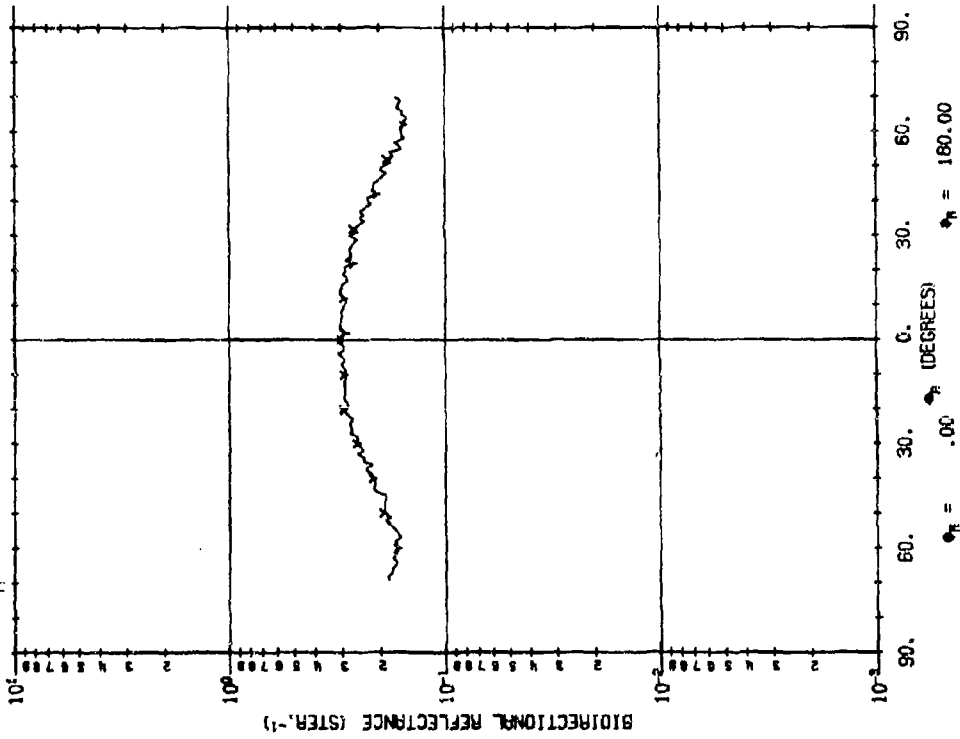


REFLECTANCE STANDARDS MATERIAL

R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED
STAINLESS STEEL

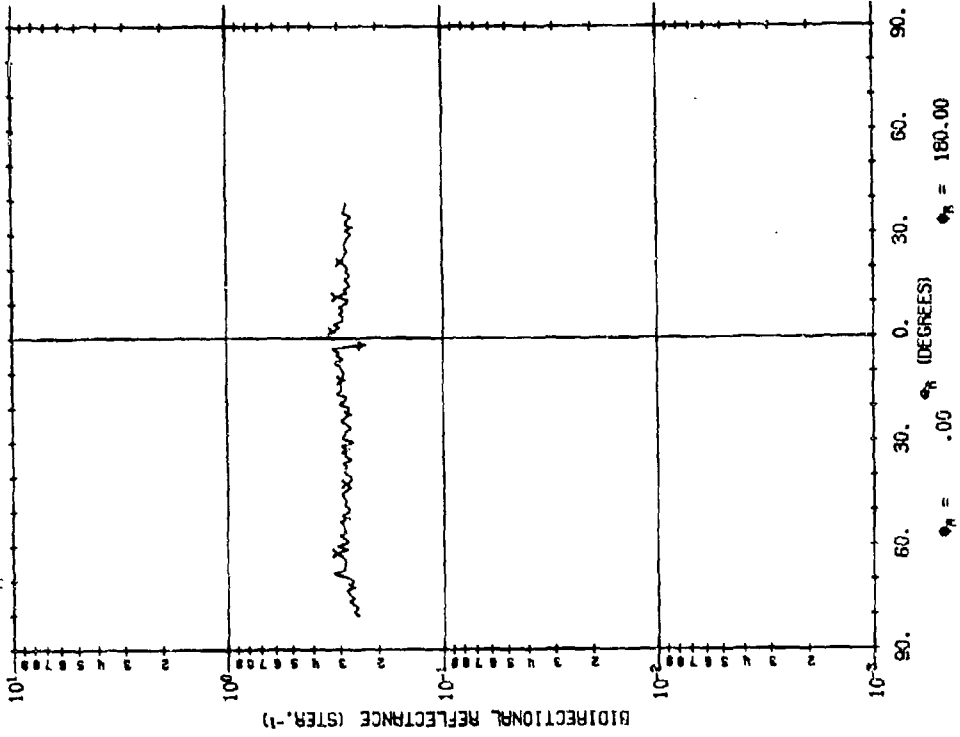
0 || 2 θ = 2.0
+ || ϕ_1 = ϕ_2
 Δ || ϕ_1 = 180.0
X || λ = 10.6
Y = UT



R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED
STAINLESS STEEL

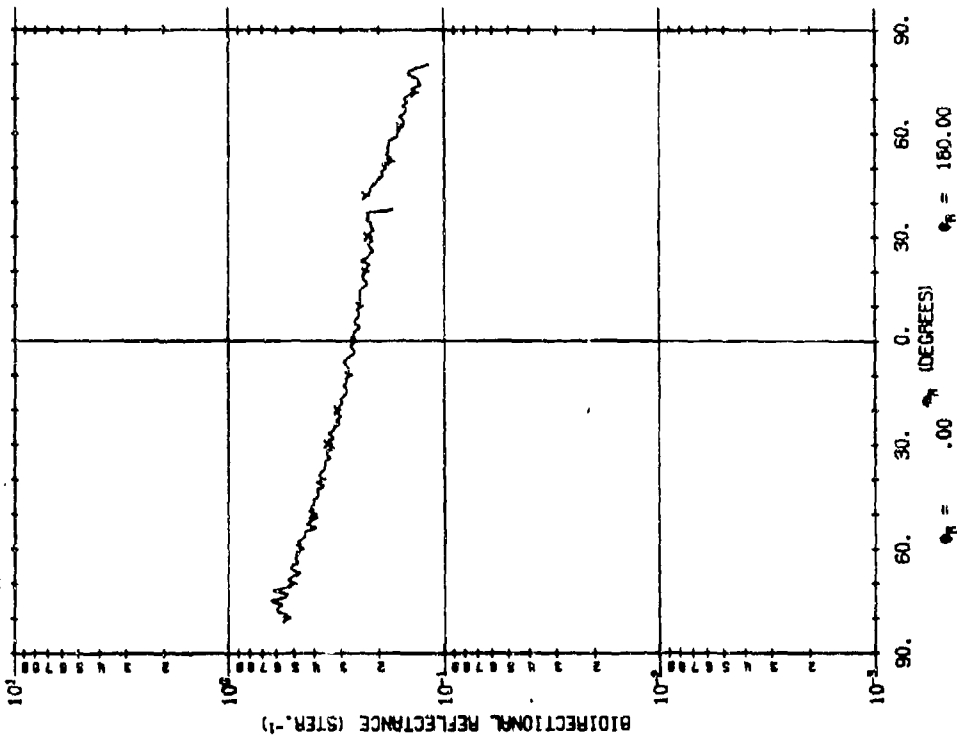
0 || ϕ_1 = 0.0
+ || ϕ_2 = 180.0
 Δ || λ = 10.6
X || Y = 73



R01435 101

ELECTRO-PLATED COPPER ON SANDBLASTED
STAINLESS STEEL

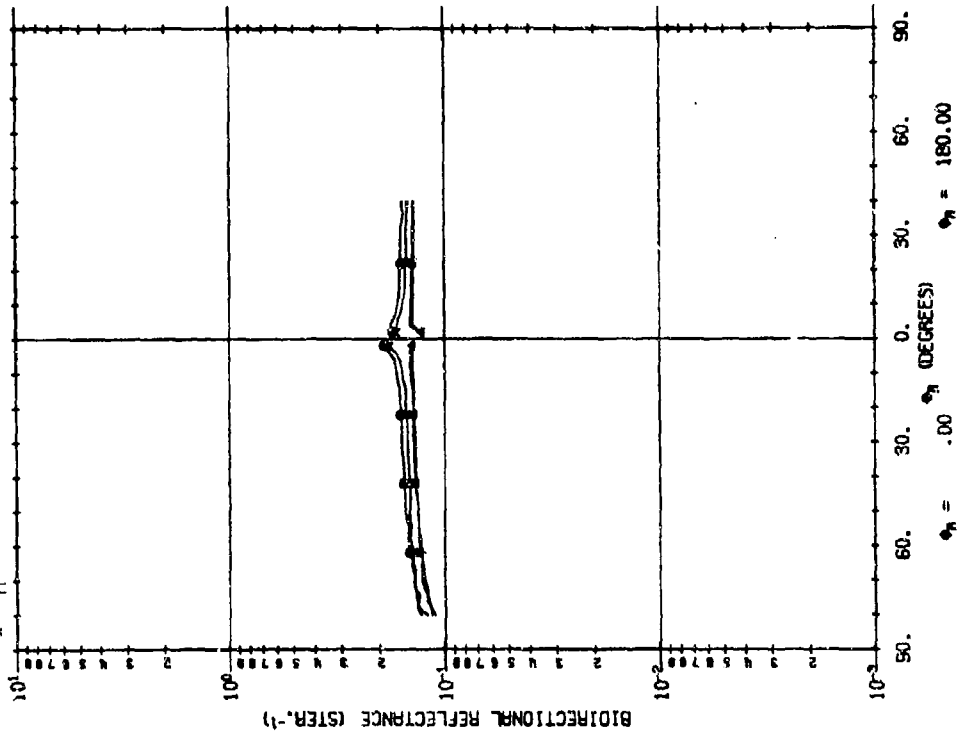
D // $\theta_1 = 40.0$
+ // $\phi_1 = 180.0$
 Δ // $\lambda = 10.6$
x // $\gamma = \text{UT}$



R01460 401

3M WHITE VELVET ON ANNOXIDIZED ALUMINUM

D // $\theta_1 = 0.0$
+ // $\phi_1 = 180.0$
 Δ // $\lambda = 0.63$
x //

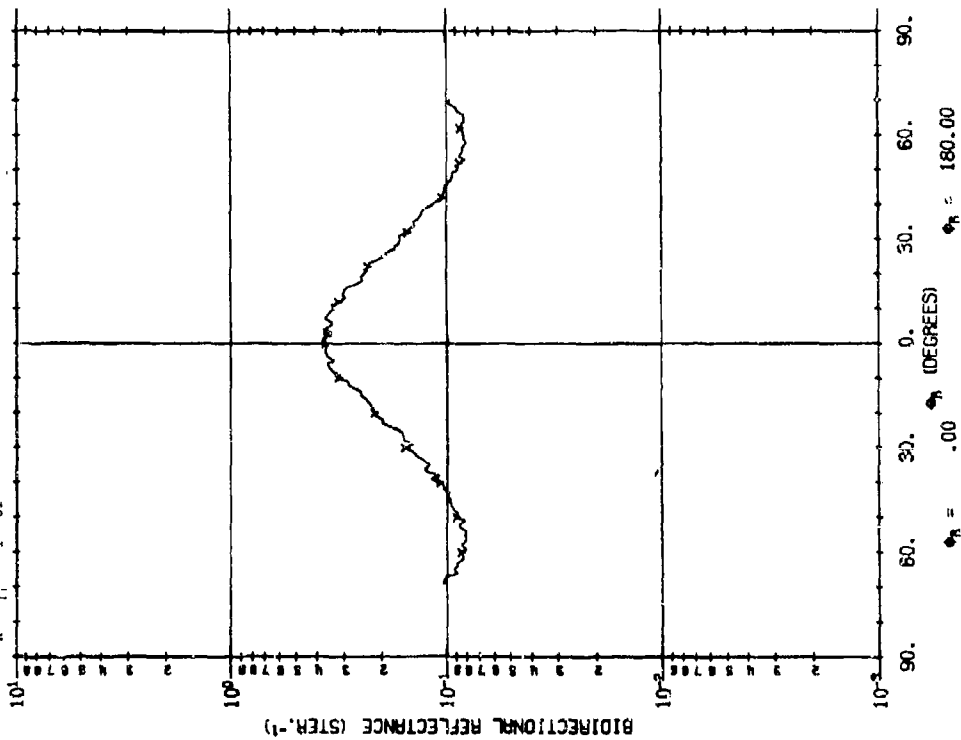


REFLECTANCE STANDARDS MATERIAL

AO1598 101

GOLD PLATED, SANDBLASTED STAINLESS STEEL

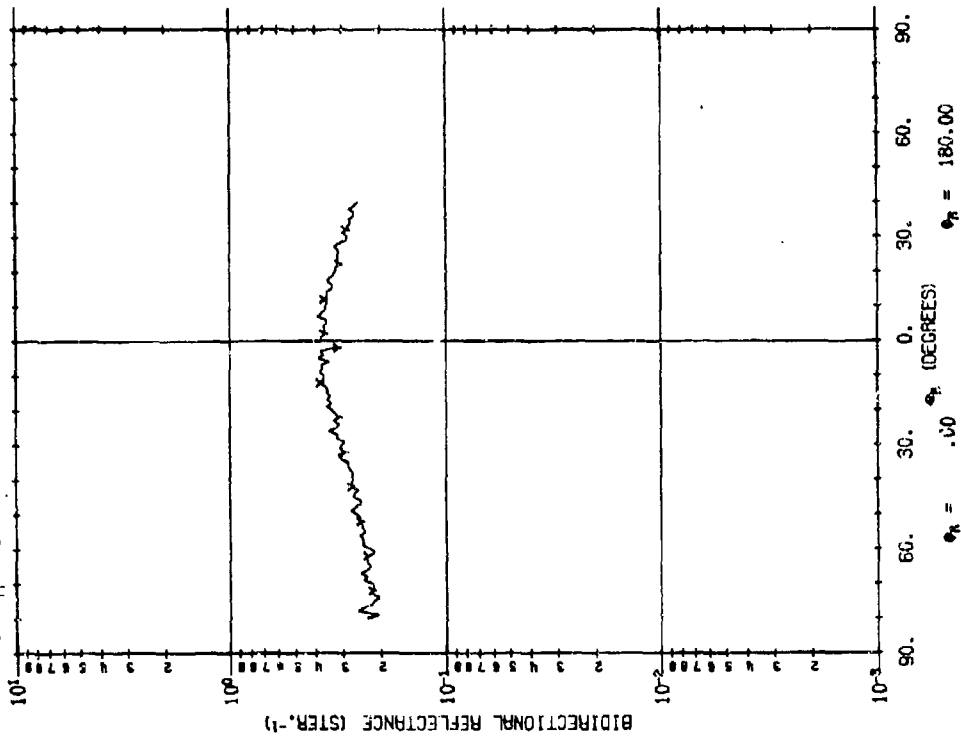
0 || 25 = 2.0
+ || || $\phi_1 = \phi_2$
Δ || || $\lambda = 10.6$
X || || Y = UT



AO1598 101

GOLD PLATED, SANDBLASTED STAINLESS STEEL

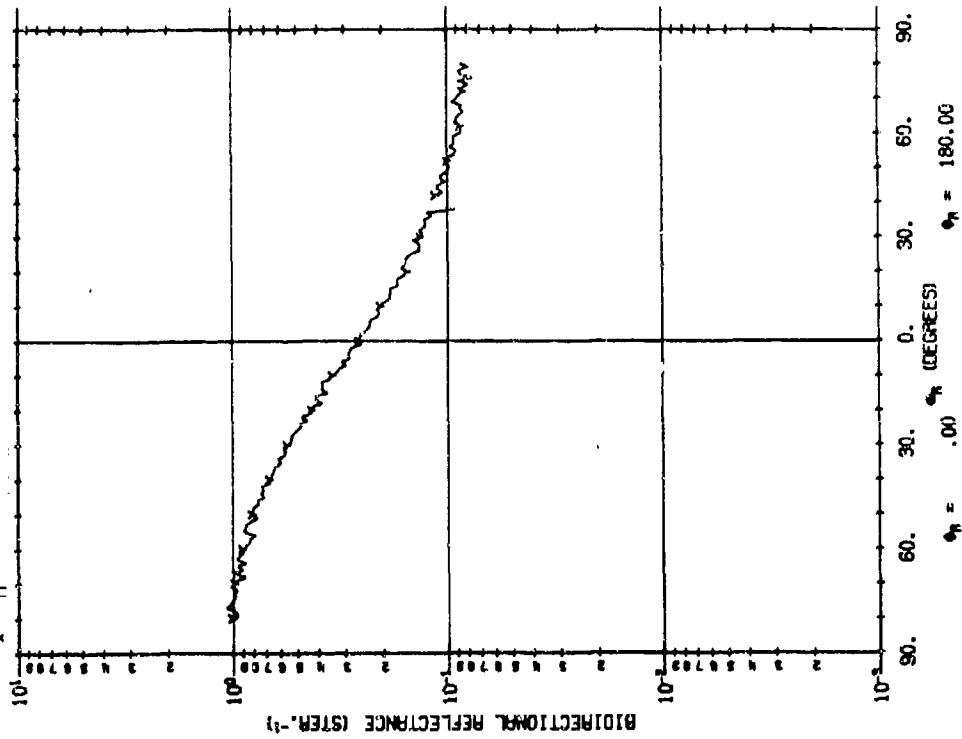
0 || $\phi_1 = 0.0$
+ || || $\phi_2 = 180.0$
Δ || || $\lambda = 10.6$
X || || Y = UT



R01598 101

GOLD PLATED, SANDEBLASTED STAINLESS STEEL

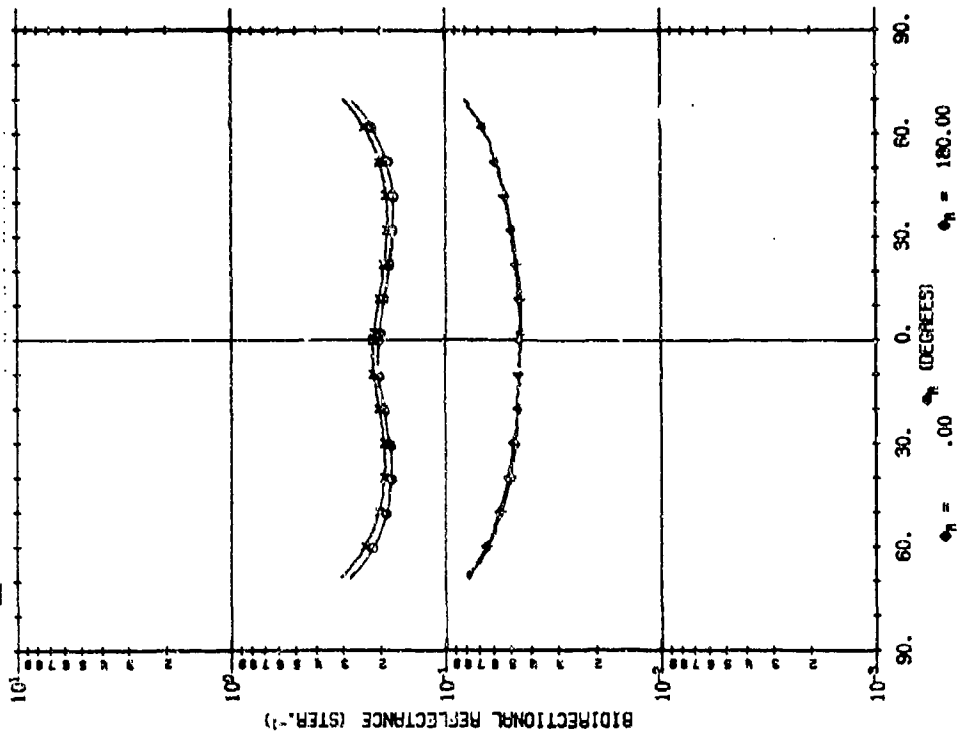
0 || $\phi_1 = 40.0$
 + || $\phi_2 = 180.0$
 A || $\lambda = 10.6$
 X || Y = UT



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
 ON .25" ALUMINUM SUBSTRATE

0 || $\phi_1 = 2.0$
 + || $\phi_2 = 4.0$
 A || $\lambda = 0.63$
 X || Y = UT

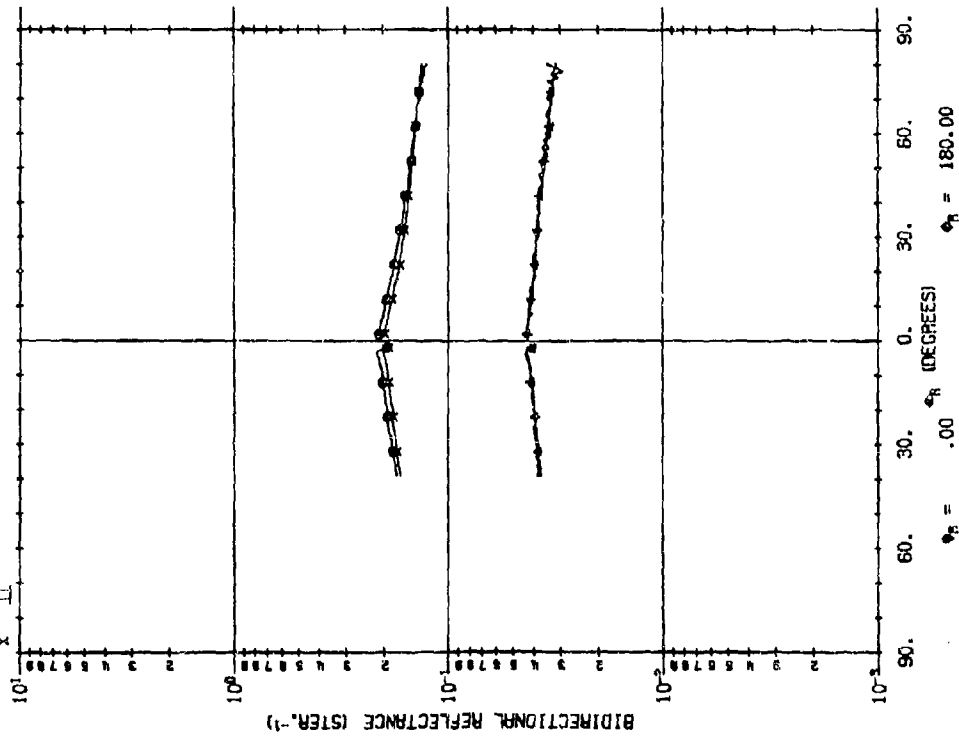


REFLECTANCE STANDARDS MATERIAL

R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

0 || $\theta_1 = 0.0$
+ || $\theta_2 = 0.0$
x || $\lambda = 0.63$

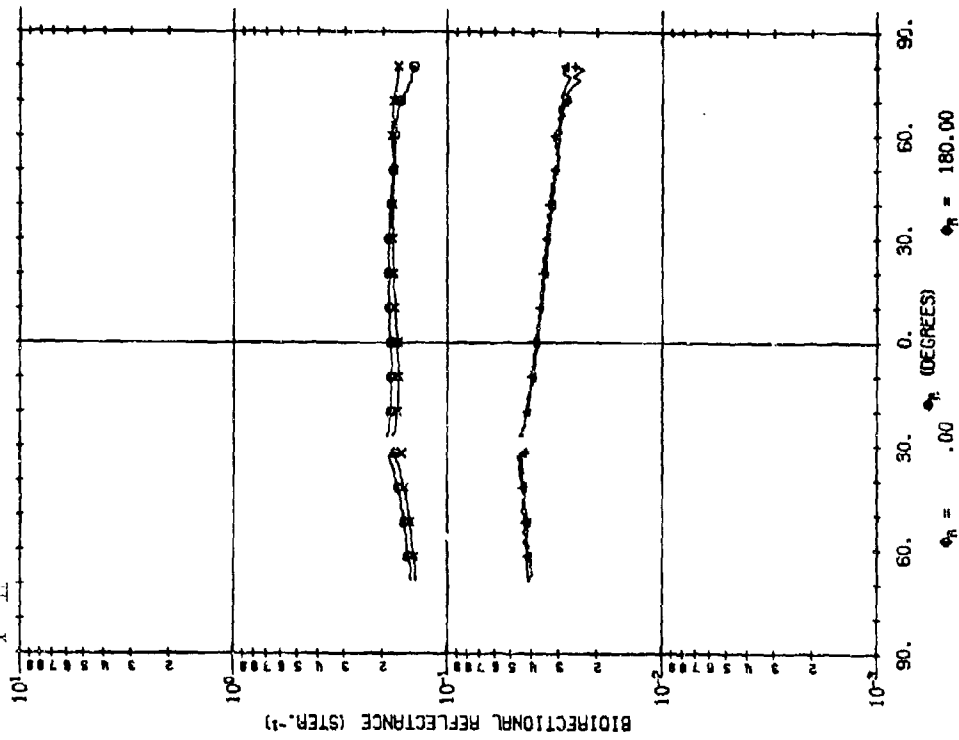


$\theta_H = .00$ $\theta_H = 180.00$

R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

0 || $\theta_1 = 30.0$
+ || $\theta_2 = 0.0$
x || $\lambda = 0.63$

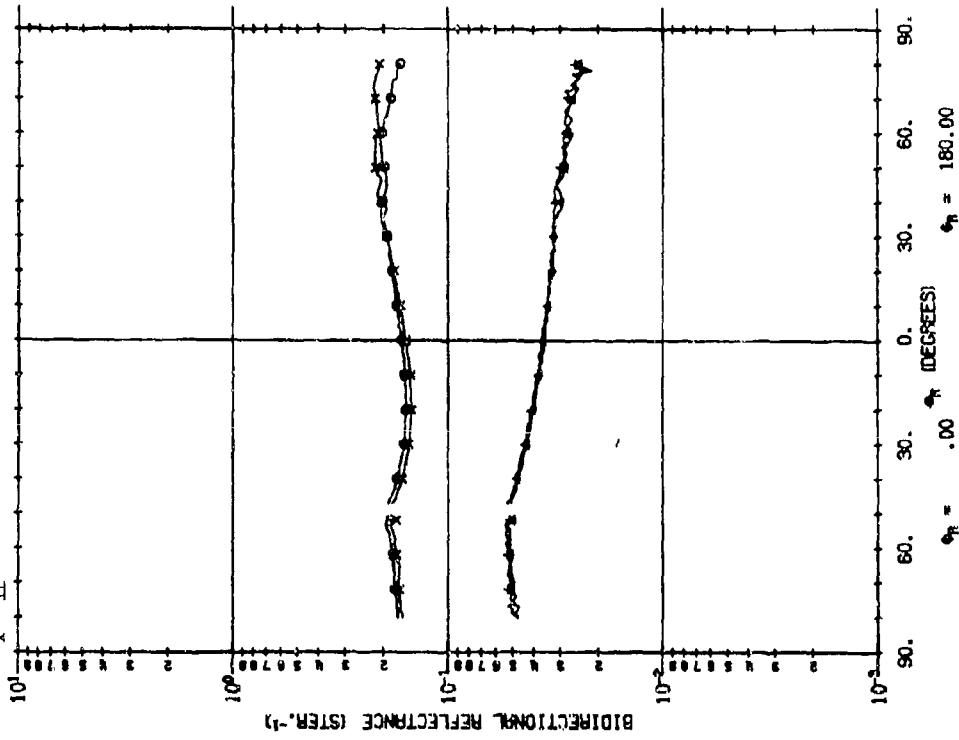


$\theta_H = .00$ $\theta_H = 180.00$

RD1683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

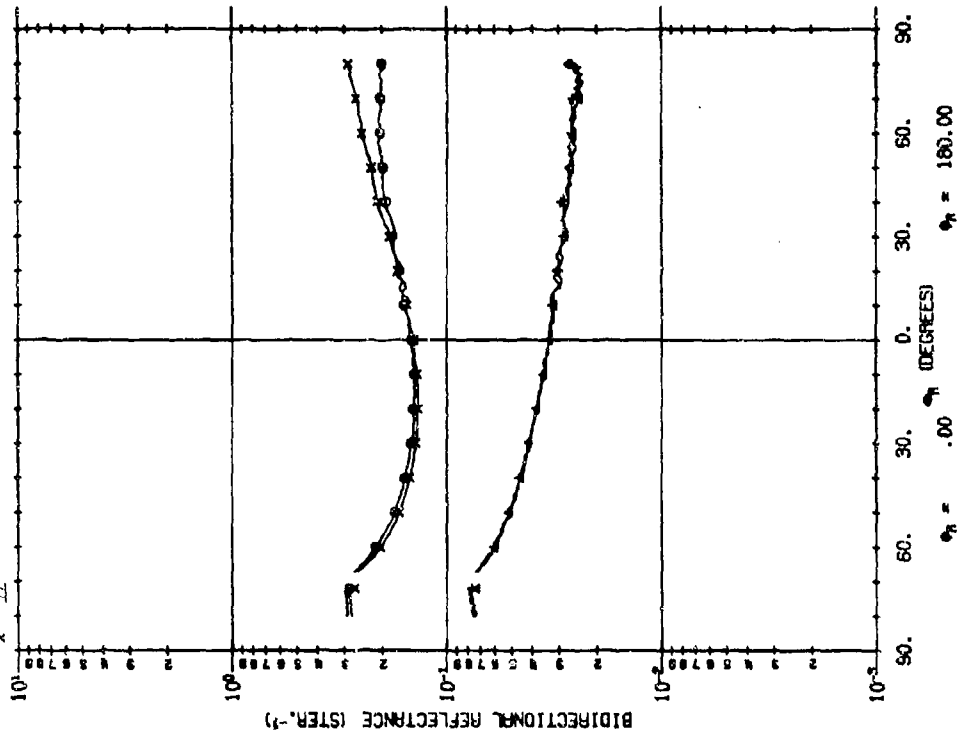
0 || $\theta_1 = 50.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
X ||



RD1683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

0 || $\theta_1 = 70.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
X ||



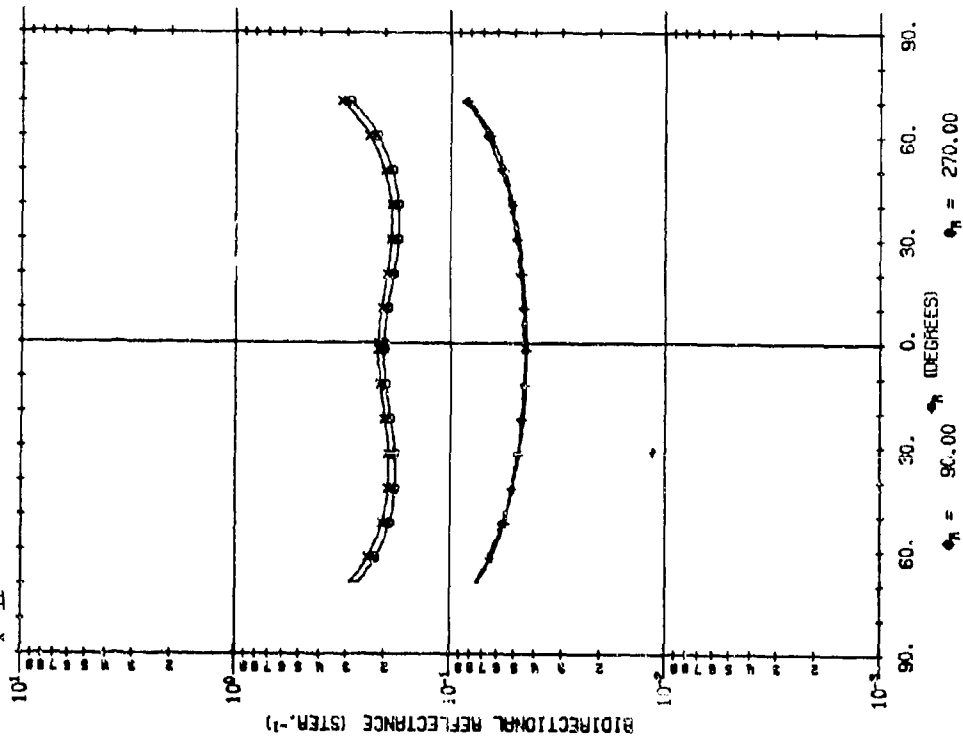
REFLECTANCE STANDARDS MATERIAL

R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

$\epsilon_1 = 2.0$
 $\epsilon_2 = 0.0$
 $\lambda = 0.63$

0 || ||
+ || ||
Δ || ||
x || ||

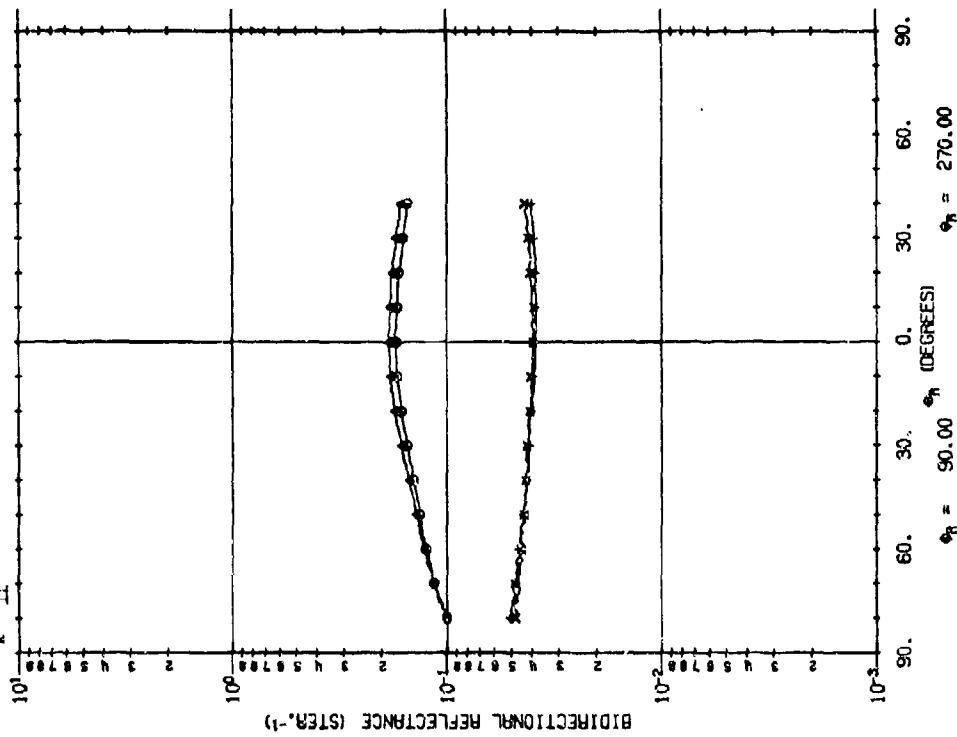


R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

$\epsilon_1 = 30.0$
 $\epsilon_2 = 0.0$
 $\lambda = 0.63$

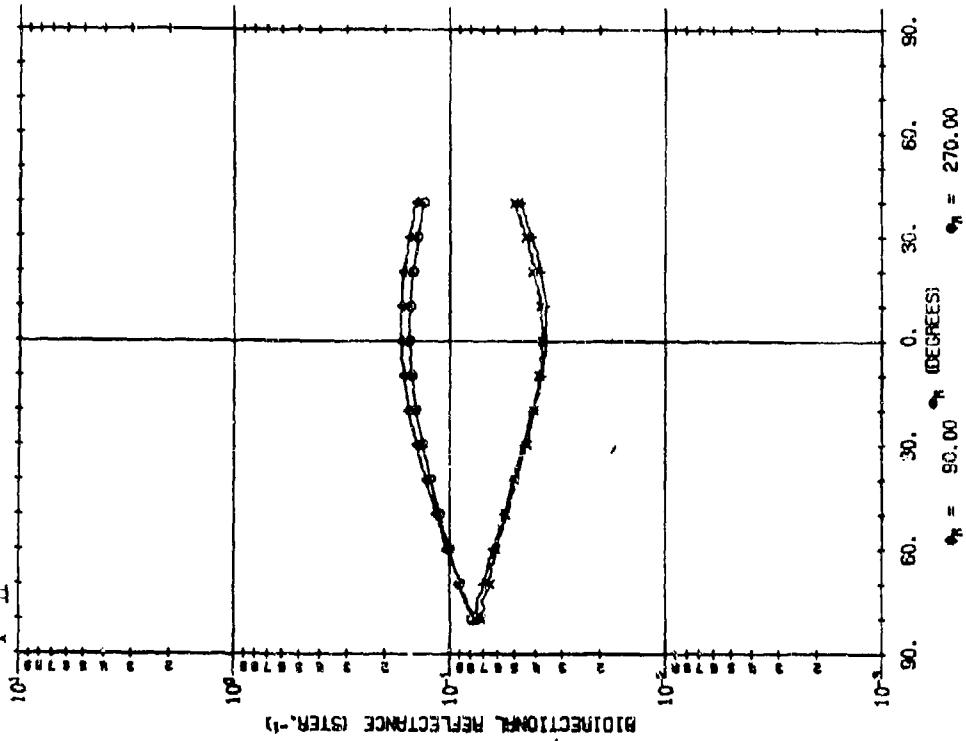
0 || ||
+ || ||
Δ || ||
x || ||



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

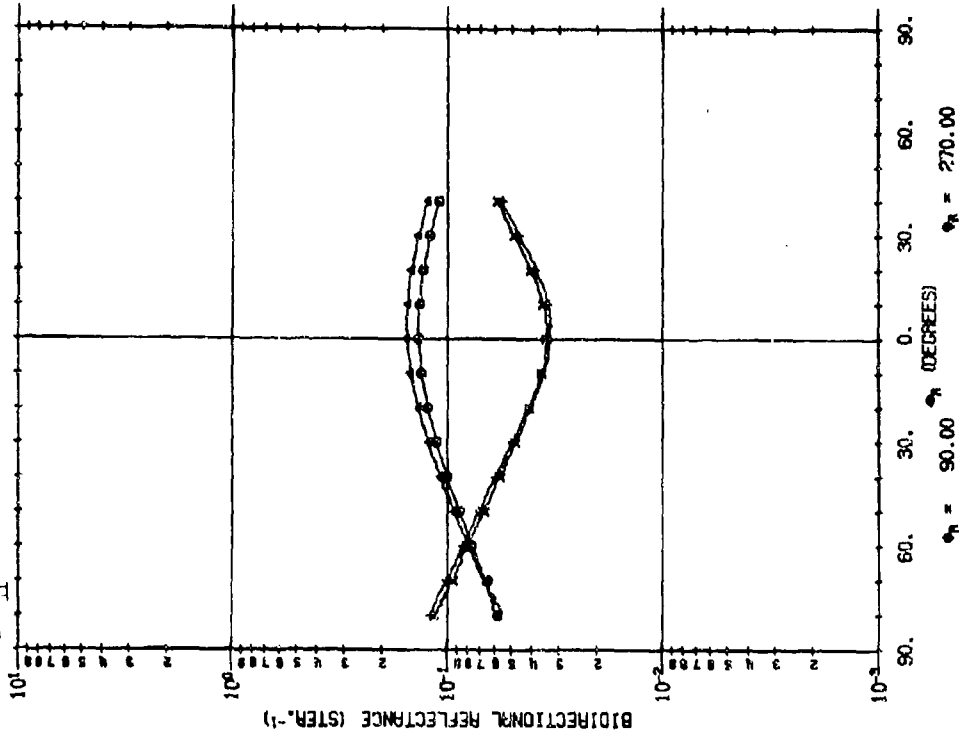
0 || $\epsilon_1 = 50.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
X ||



R01683 102

FLAME-SPRAYED ALUMINUM .03" THICK
ON .25" ALUMINUM SUBSTRATE

0 || $\epsilon_1 = 70.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
X ||

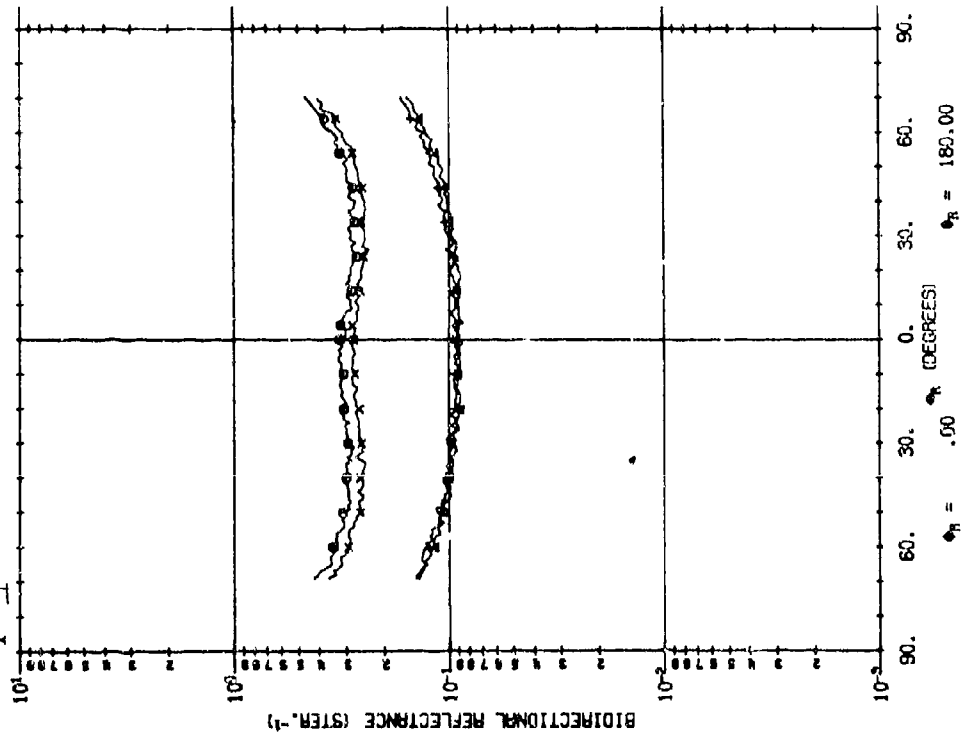


REFLECTANCE STANDARDS MATERIAL

R01683 101

FLAME-SPRAYED ALUMINUM .03" THICK
OF .75" ALUMINUM SUBSTRATE

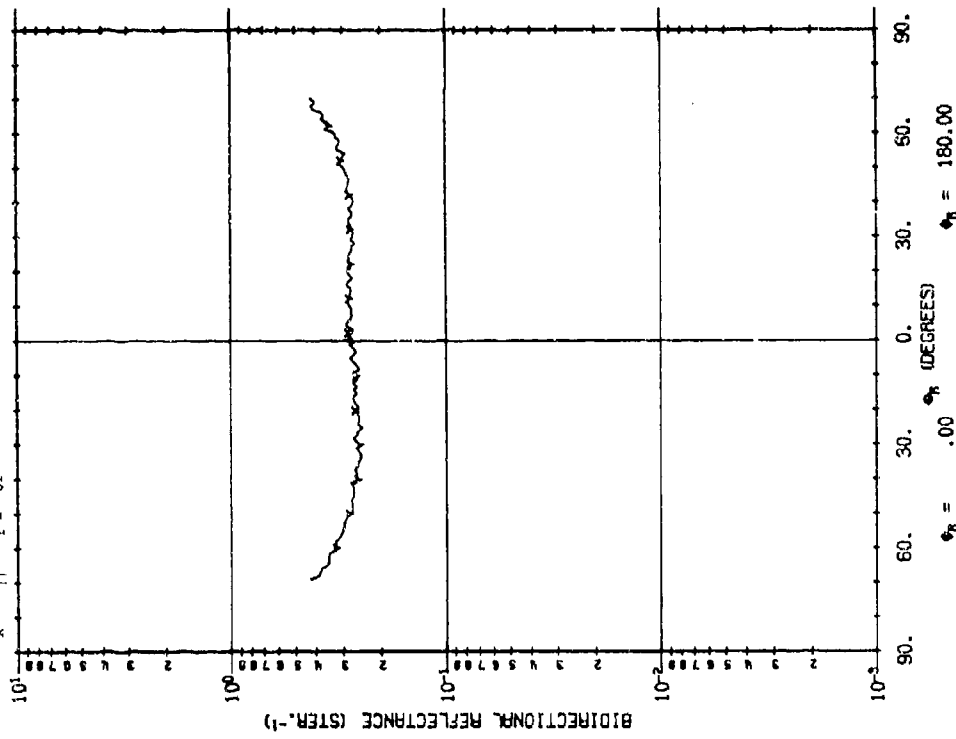
0 || 2 ϵ = 4.0
+ || ϕ_s = ϕ_r
 Δ || λ = 10.6
x ||



R01684 101

FLAME SPRAYED ALUMINUM ON
1/4" THICK ALUMINUM

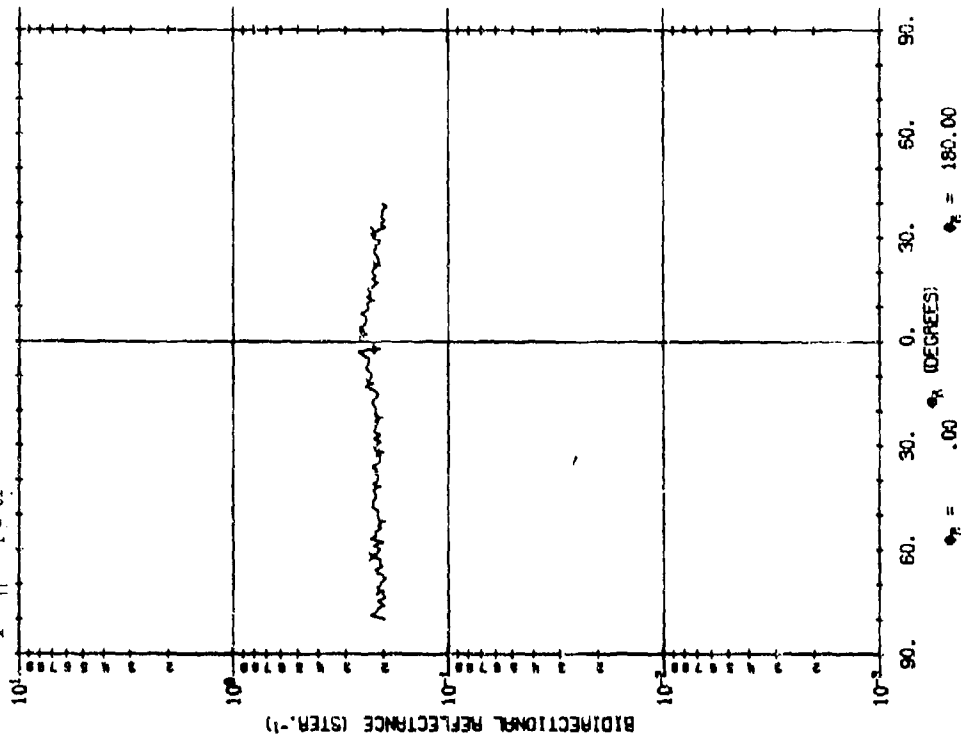
0 || 2 ϵ = 2.0
+ || ϕ_s = ϕ_r
 Δ || λ = 10.6
x || y = UT



A01684 101

FLAME SPRAYED ALUMINUM ON 1/4"
THICK ALUMINUM

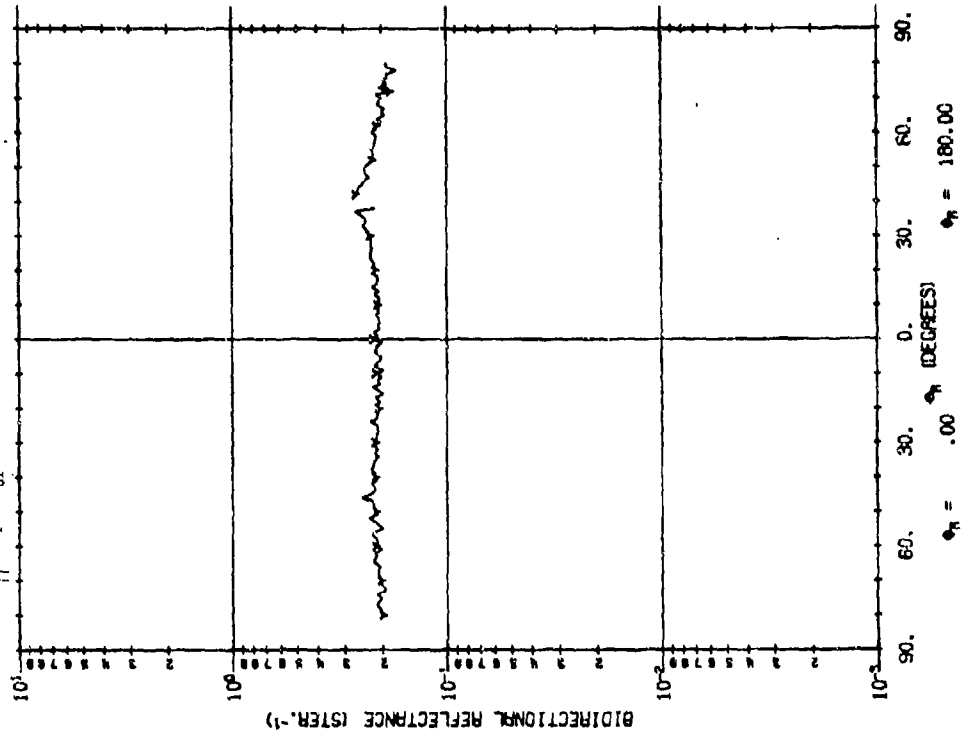
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 10.6$
X || Y = VT



A01684 101

FLAME SPRAYED ALUMINUM ON
1/4" THICK ALUMINUM

0 || $\theta_1 = 40.0$
+ || $\theta_2 = 180.0$
Δ || $\lambda = 10.6$
X || Y = VT

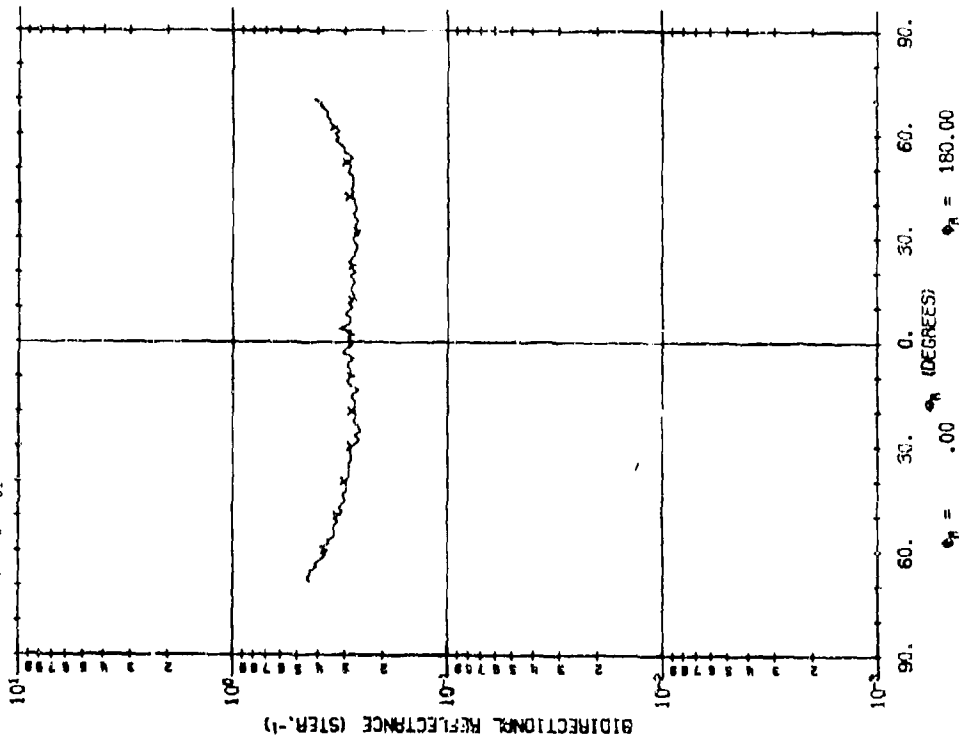


REFLECTANCE STANDARDS MATERIAL

RQ1688 101

FLAME SPRAYED ALUMINUM ON
1/4" THICK ALUMINUM

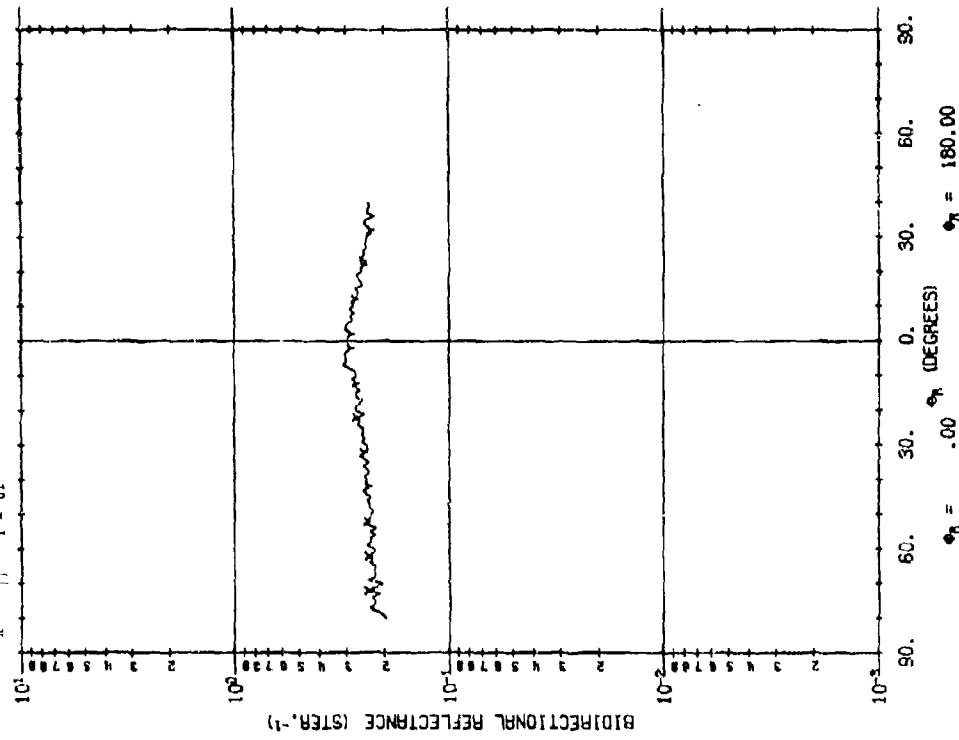
$\theta_1 = 2.0$
 $\theta_2 = \theta_r$
 $\lambda_1 = 10.6$
Y = UT



RQ1688 101

FLAME SPRAYED ALUMINUM ON
1/4" THICK ALUMINUM

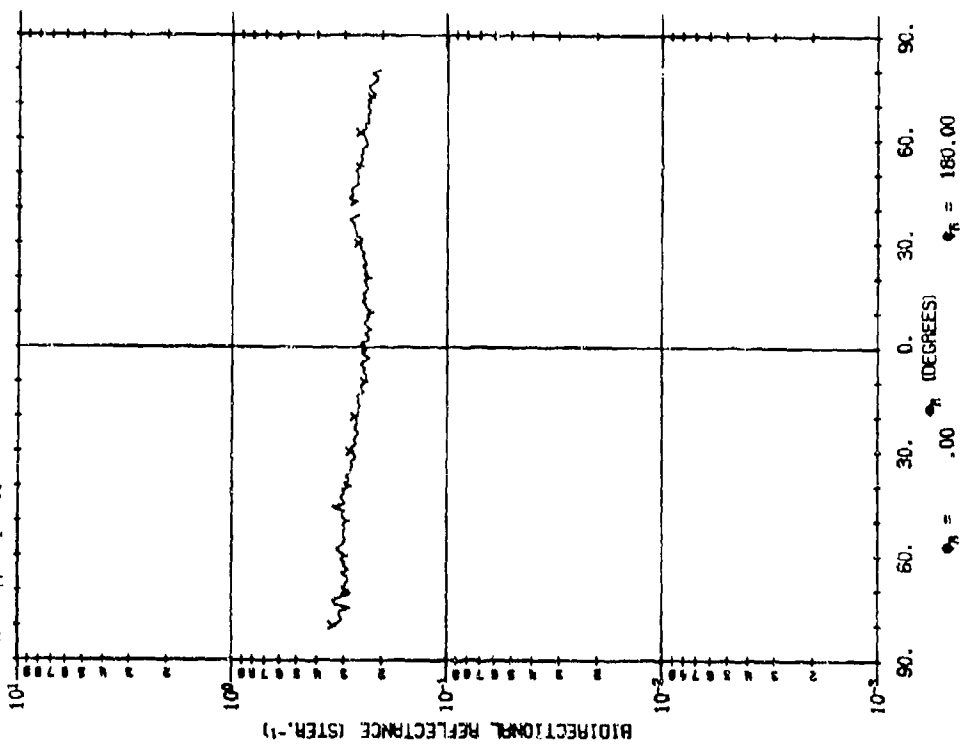
$\theta_1 = 0.0$
 $\theta_2 = 180.0$
 $\lambda_1 = 10.6$
Y = UT



R01688 101

FLAME SPRAYED ALUMINUM ON
1/4" THICK ALUMINUM

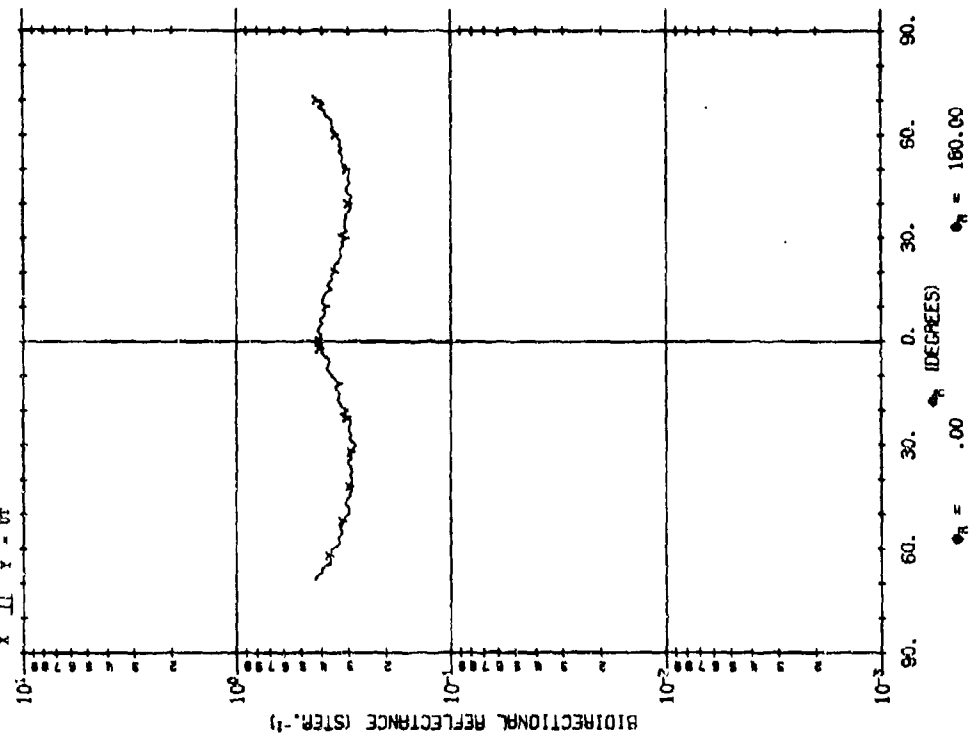
$\theta_1 = 40.0$
 $\theta_2 = 180.0$
 $\lambda = 10.6$
X Y = VT



R01894 101

FLAME SPRAYED ALUMINUM OVER
SANDBLASTED ALUMINUM PLATE

$\theta_1 = 22$
 $\theta_2 = 2.0$
 $\lambda = 10.6$
X Y = VT

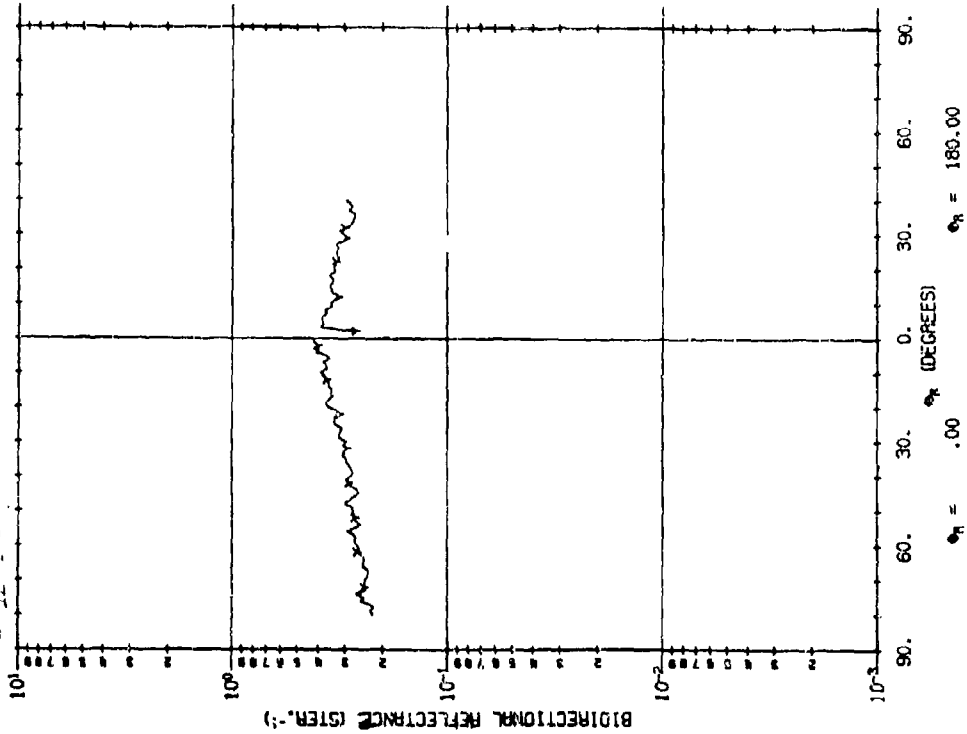


REFLECTANCE STANDARDS MATERIAL

R01894 101

Flame Sprayed Aluminum over Sandblasted
Aluminum Plate

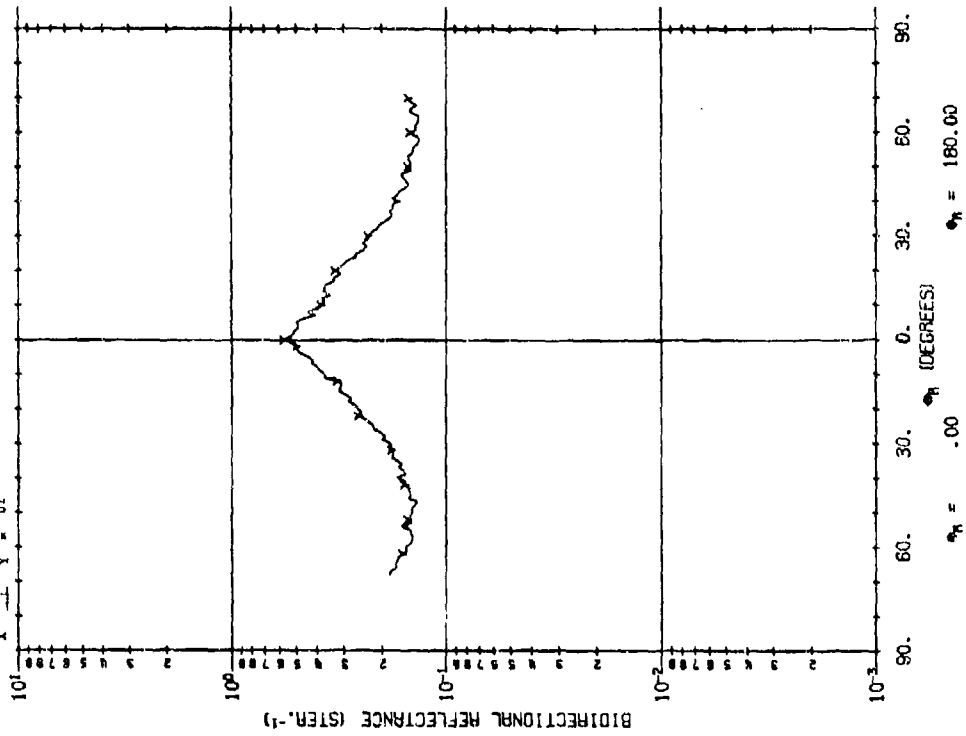
0 // $\epsilon_1 = 0.0$
+ // $\epsilon_2 = 180.0$
2 // $\lambda = 10.5$
X // Y = UT



R01895 101

Sandblasted Aluminum

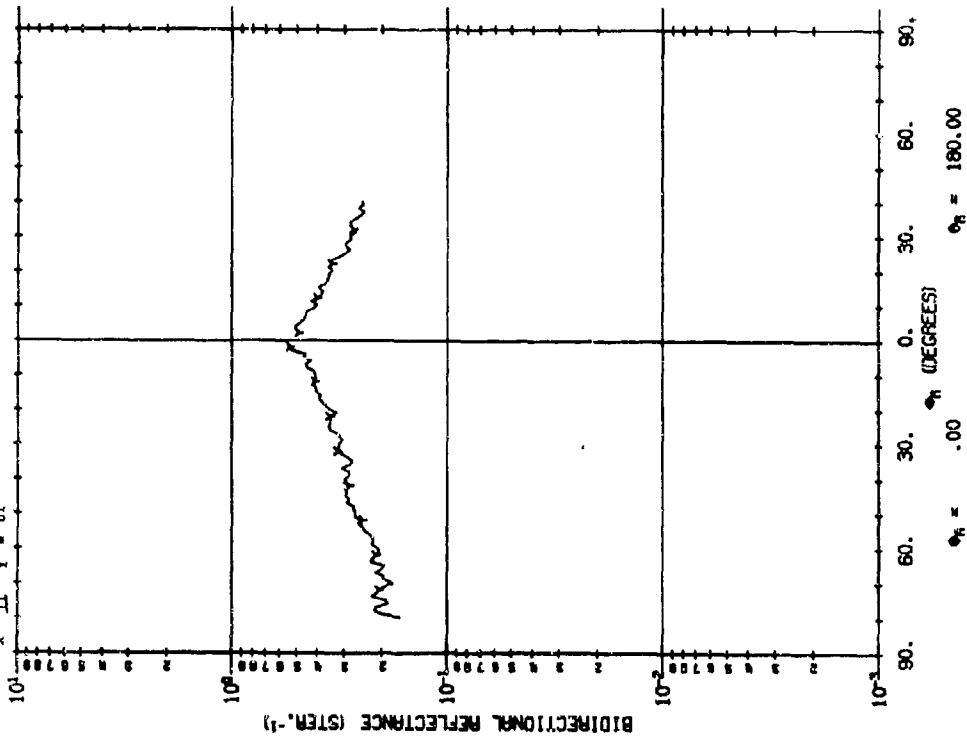
0 // $\epsilon_1 = 2.0$
+ // $\epsilon_2 = 180.0$
2 // $\lambda = 10.6$
X // Y = UT



R01895 101

Sandblasted Aluminum

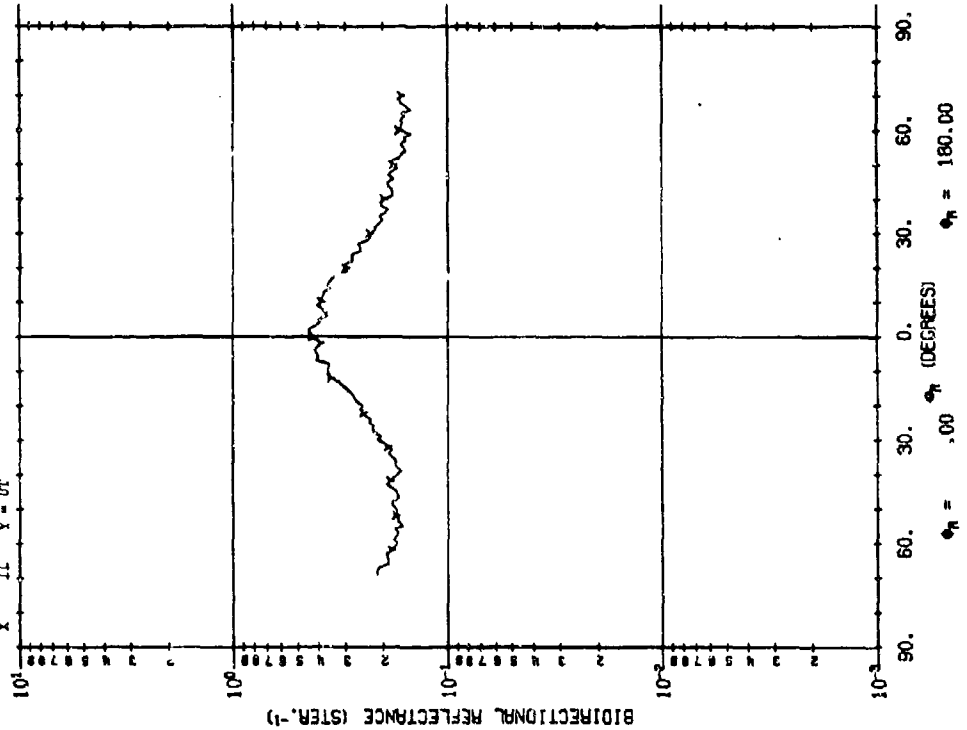
0 // $\theta_i = 0.0$
+ // $\phi_i = 180.0$
Δ // $\lambda = 10.6$
X // Y = UT



R01895 201

Sandblasted Aluminum

0 // $2\theta = 2.0$
+ // $\phi_i = \phi_r$
Δ // $\lambda = 10.6$
X // Y = UT

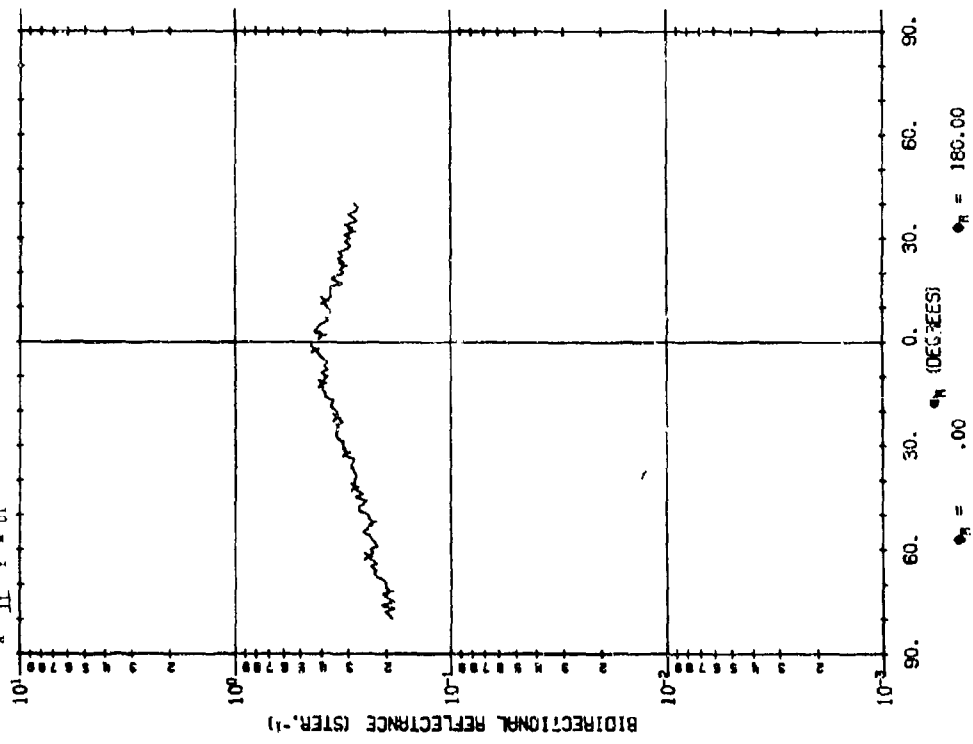


REFLECTANCE STANDARDS MATERIAL

R01895 201

Sandblasted Aluminum

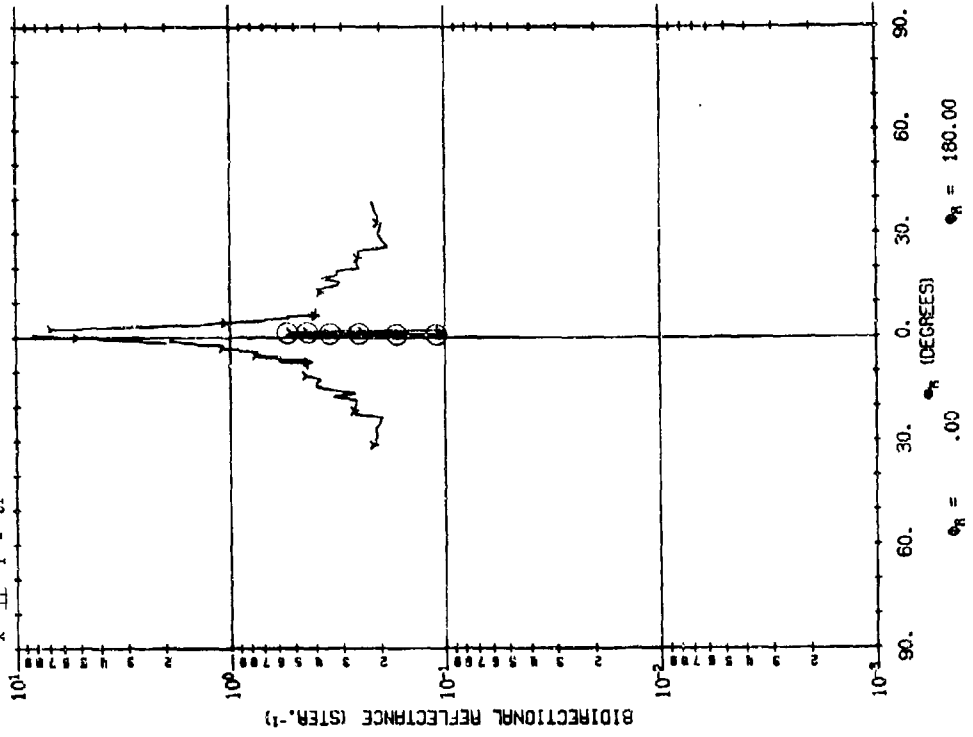
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
5 || $\lambda = 10.6$
X || Y = UT



R01895 301

Sandblasted Aluminum

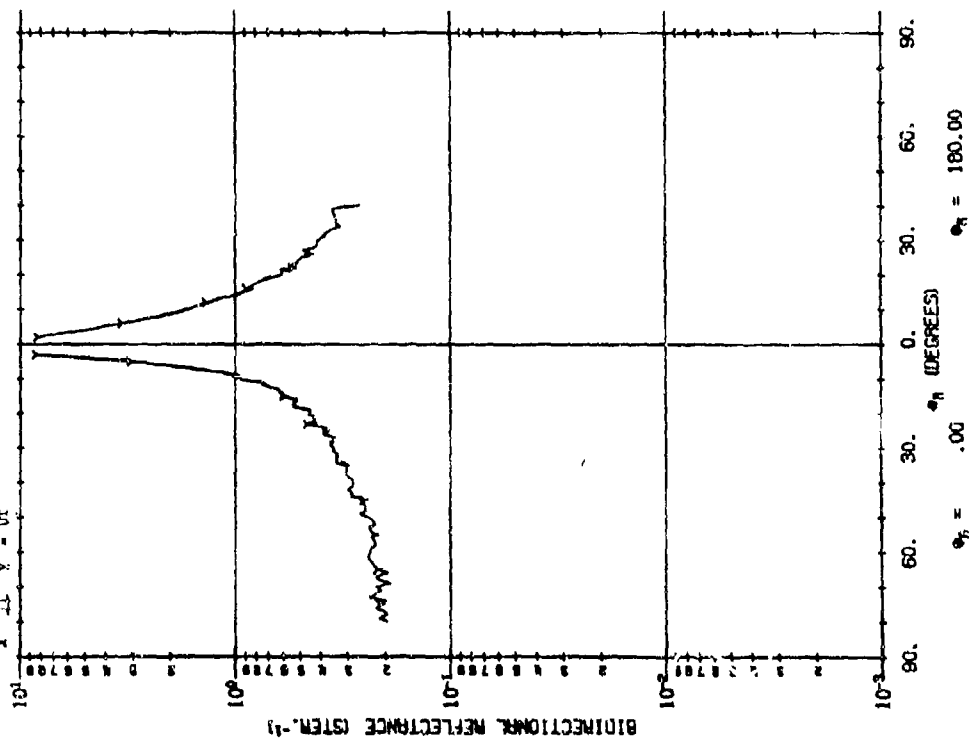
0 || $2\theta = 2.0$
+ || $\phi_1 = \phi_r$
4 || $\lambda = 10.6$
X || Y = UT



A01895 301

Sandblasted Aluminum

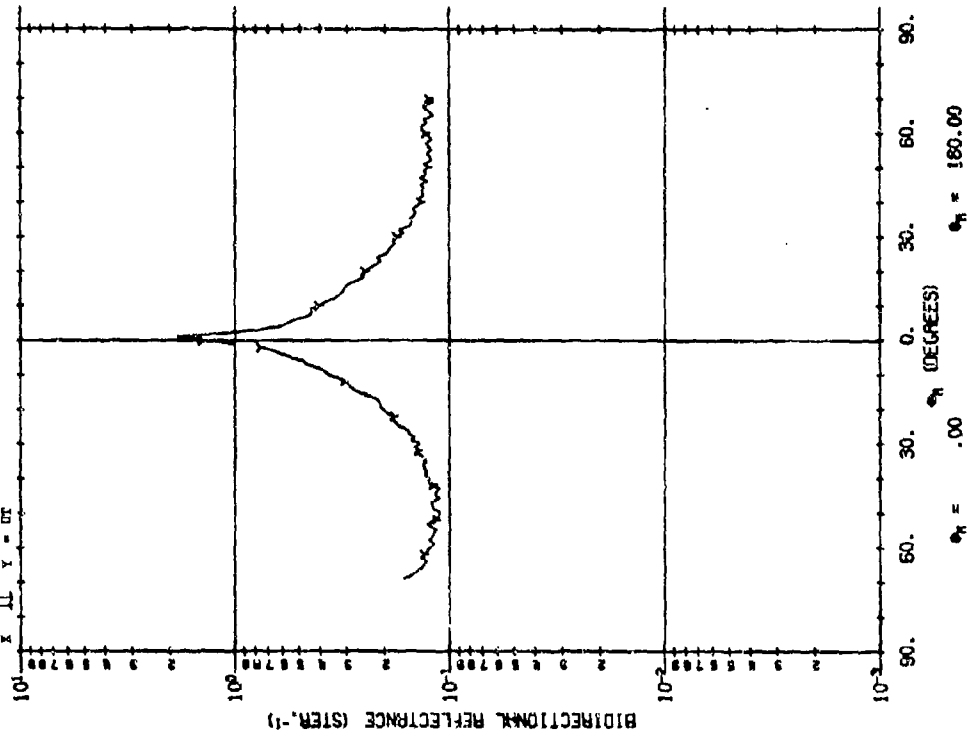
$\theta_i = 0.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y = DT



A01896 101

Sandblasted Galvanized Steel

$\theta_i = 2.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y = DT

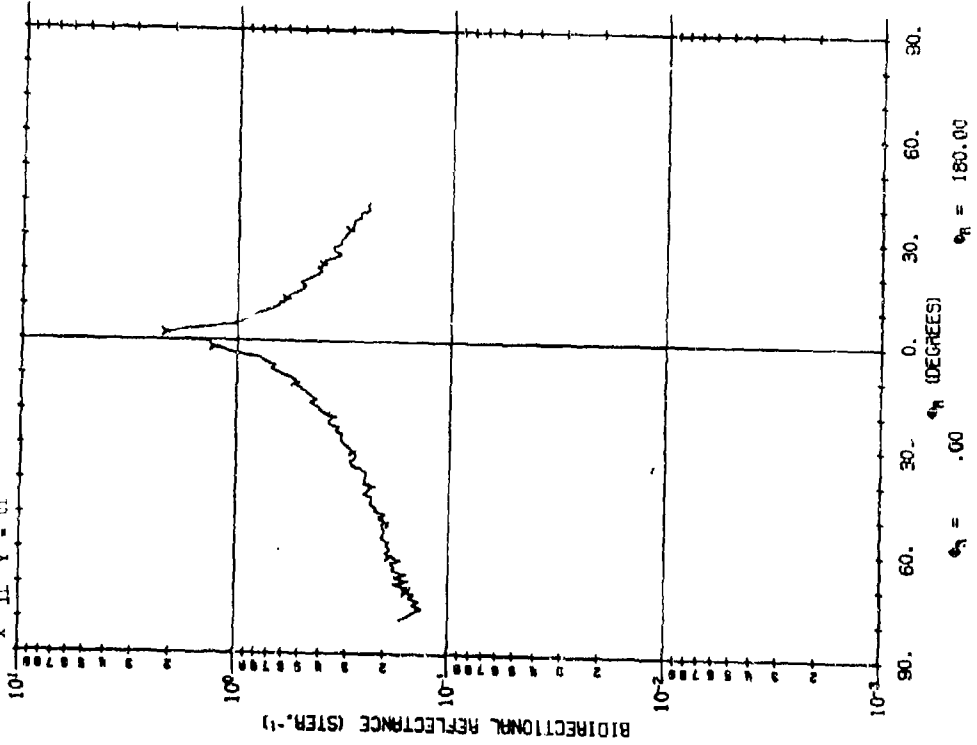


REFLECTANCE STANDARDS MATERIAL

A01896 101

Sandblasted Galvanized Steel

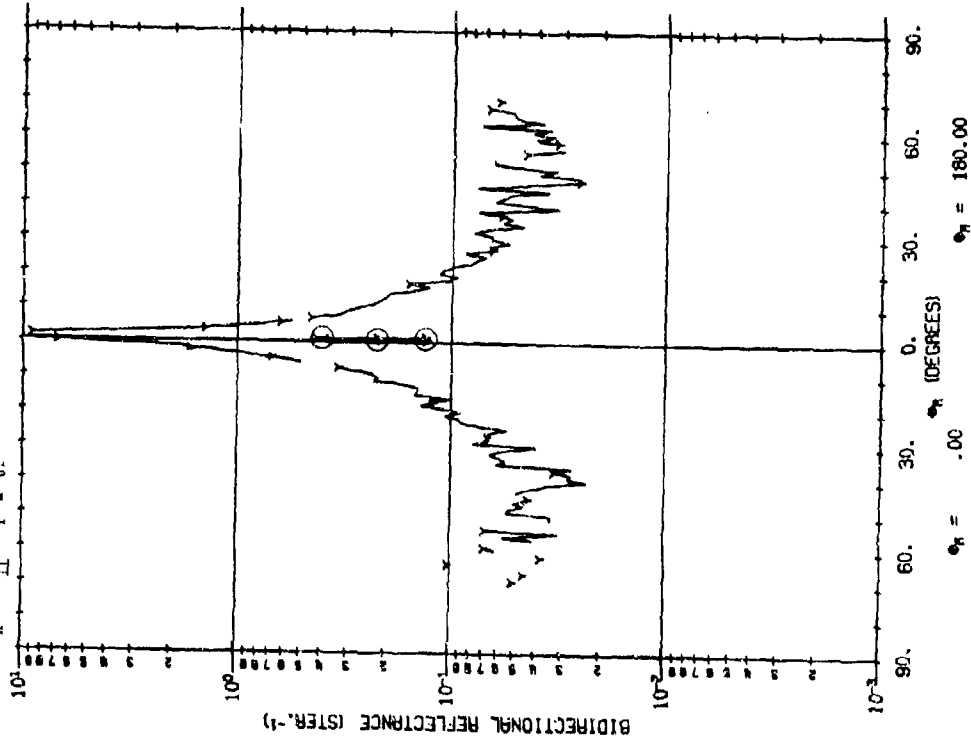
0 | | $\phi_1 = 0.0$
+ | | $\phi_2 = 180.0$
x | | $\lambda = 20.6$
Y - VT



A01896 201

Sandblasted Galvanized Steel

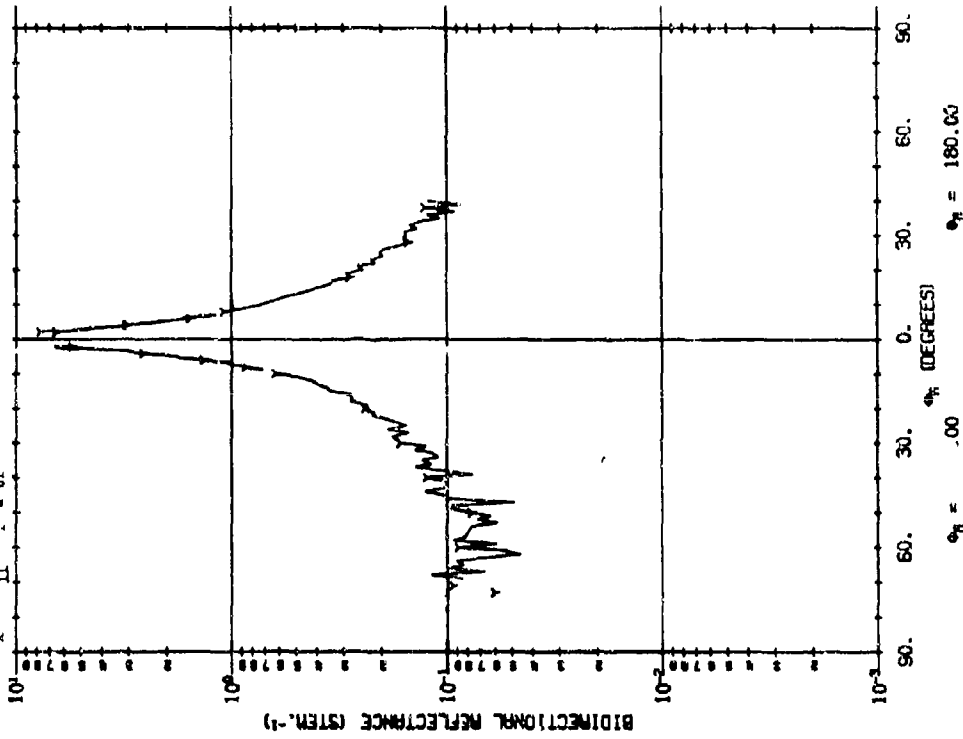
0 | | $2\theta = 2.0$
+ | | $\phi_1 = 0$
x | | $\lambda = 15.6$
Y - VT



R01896 201

Sandblasted Galvanized Steel

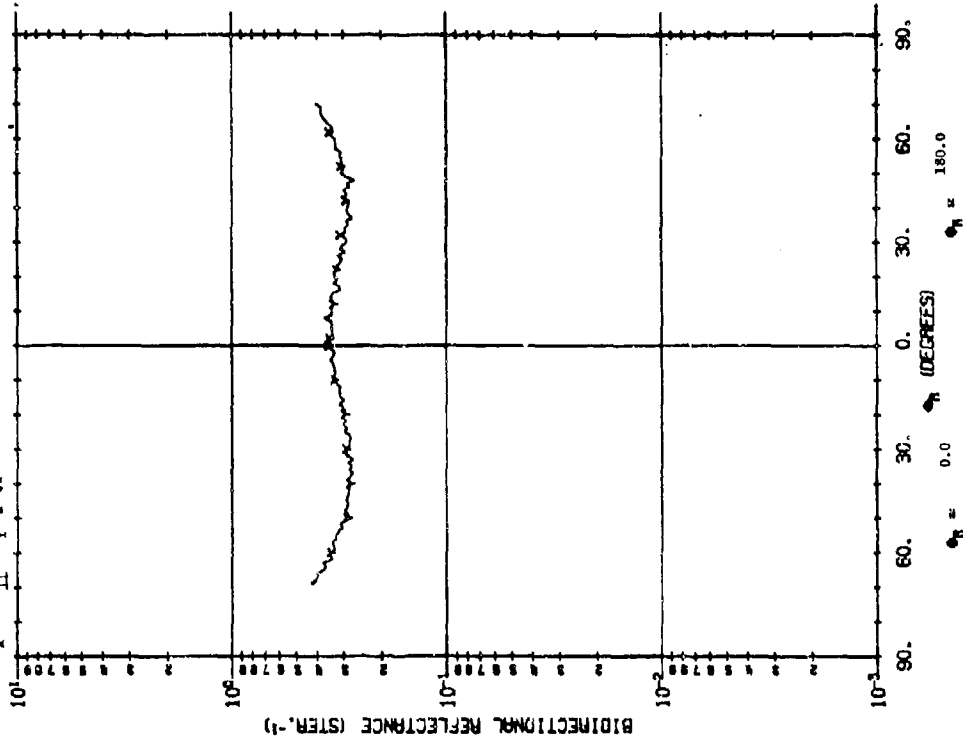
0 || $\theta_1 = 0.0$
+ || $\phi_1 = 180.0$
 Δ || $\lambda = 10.6$
X || Y = VT



R01915 101

Flame Sprayed Aluminum on Aluminum Substrate

0 || $2\theta = 2.0$
+ || $\phi_1 = \psi$
 Δ || $\lambda = 10.6$
X || Y = VT

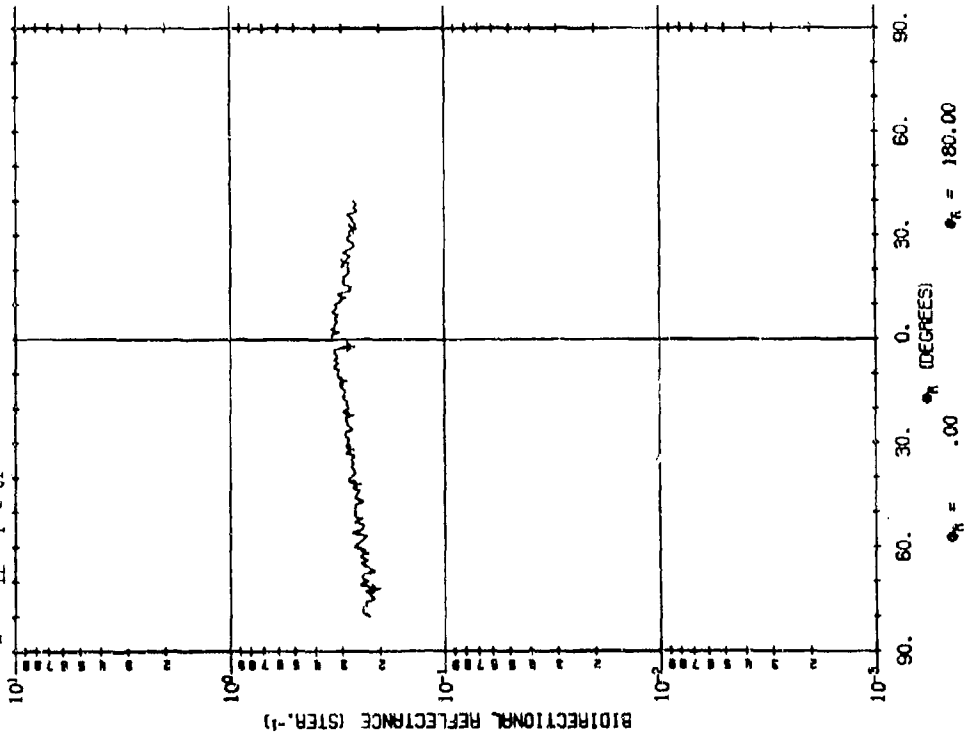


REFLECTANCE STANDARDS MATERIAL

R01915 101

Flame Sprayed Aluminum on Aluminum

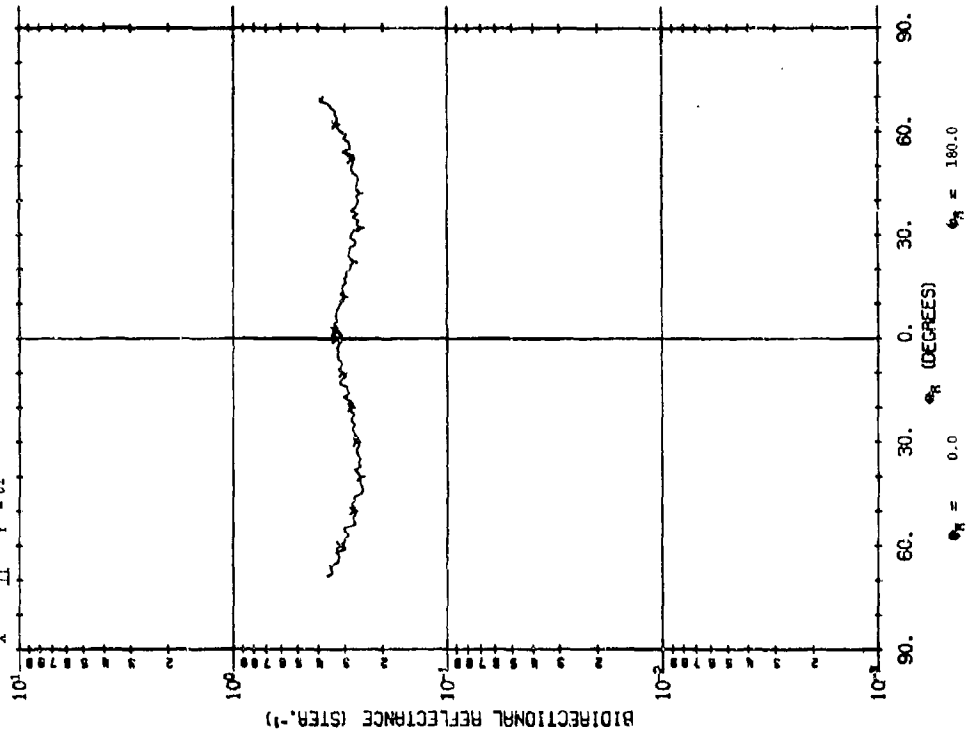
0 // $\theta_1 = 0.0$
+ // $\phi_1 = 180.0$
A // $\lambda = 10.6$
X // Y = UT



R01916 101

Flame Sprayed Aluminum on Aluminum

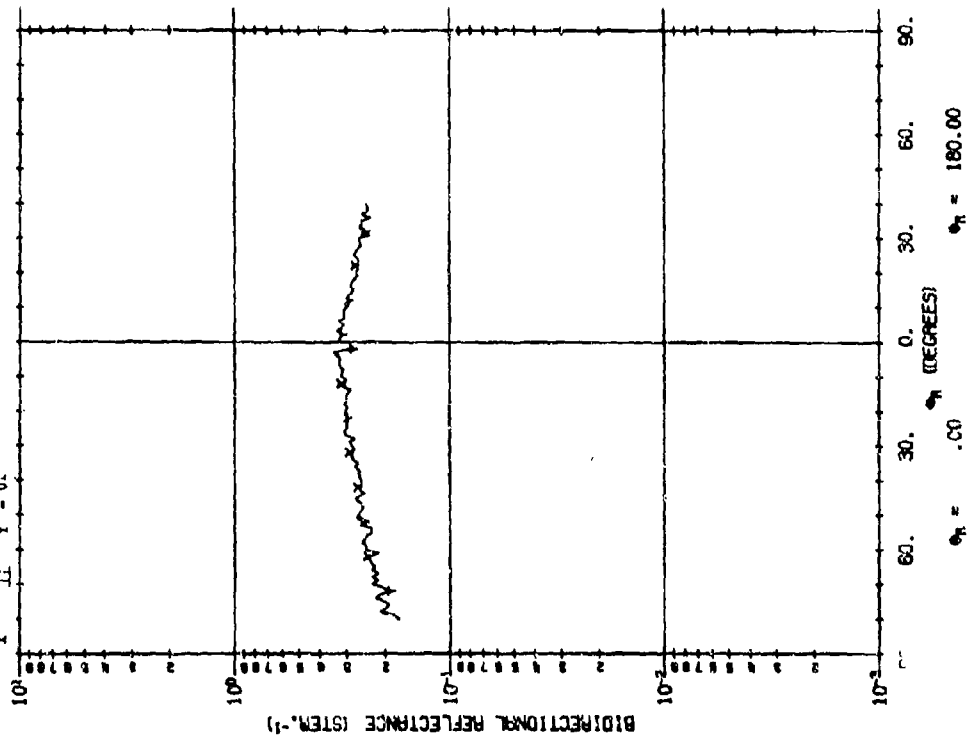
0 // $\theta_1 = 2.0$
+ // $\phi_1 = \phi_2$
A // $\lambda = 10.6$
X // Y = UT



R01916 101

Flame Sprayed Aluminum on Aluminum

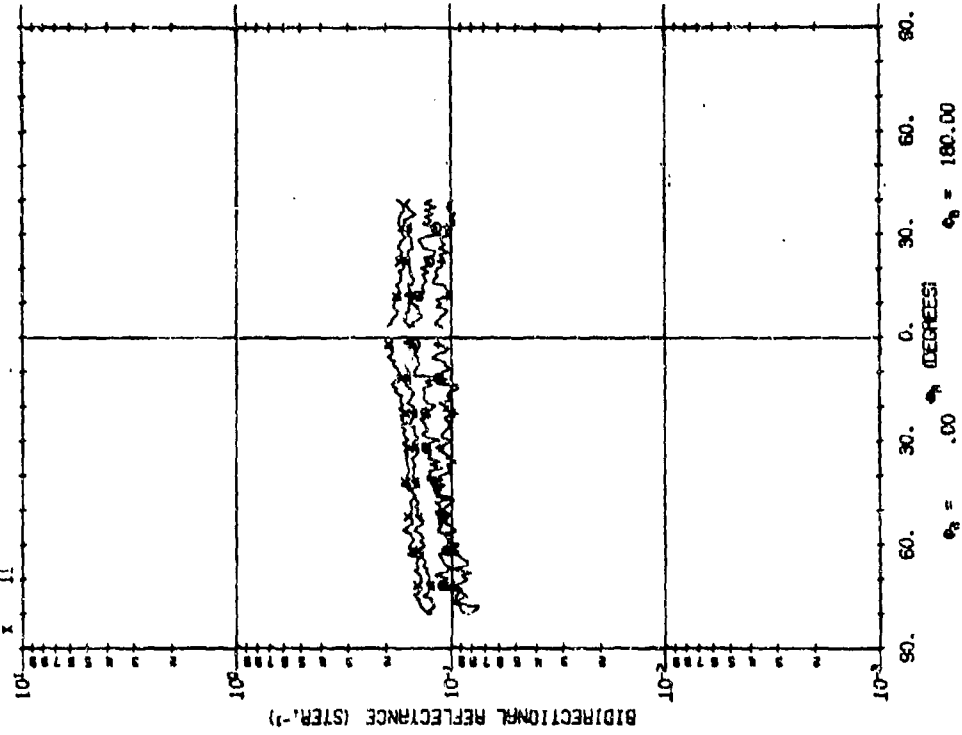
$\theta_i = 0.0$
 $\theta_r = 180.0$
 $\lambda = 10.6$
X Y - UT



R02003 101

3M White Paint on Fiberboard

$\theta_i = 0.0$
 $\theta_r = 180.0$
 $\lambda = 1.06$
X Y - UT

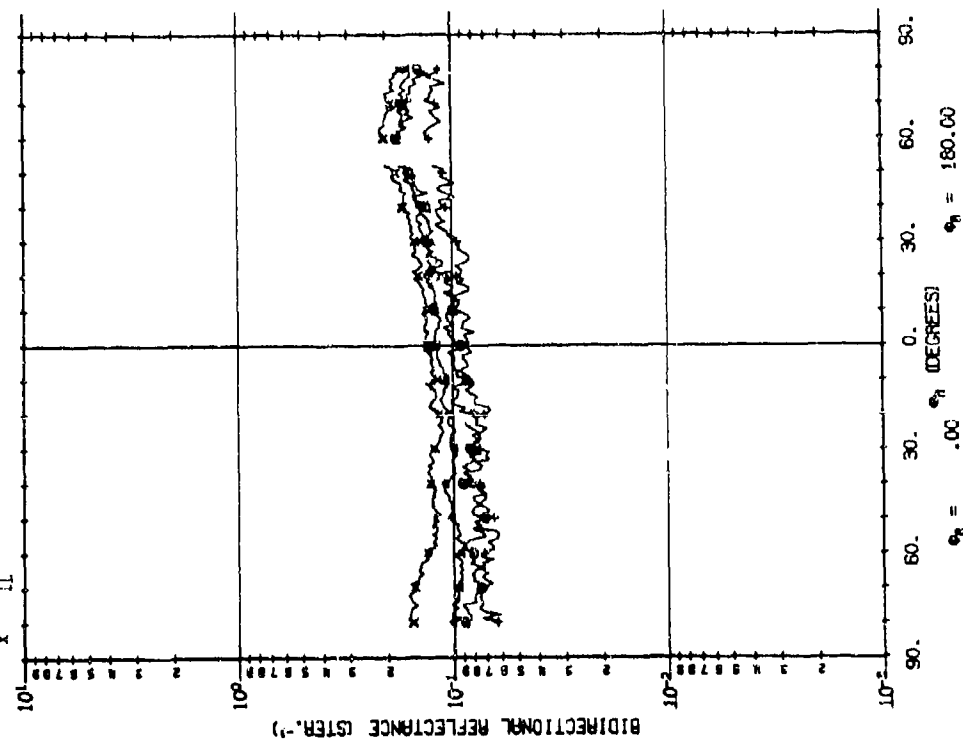


REFLECTANCE STANDARDS MATERIAL

R02003 101

3M White Paint on Fiberboard

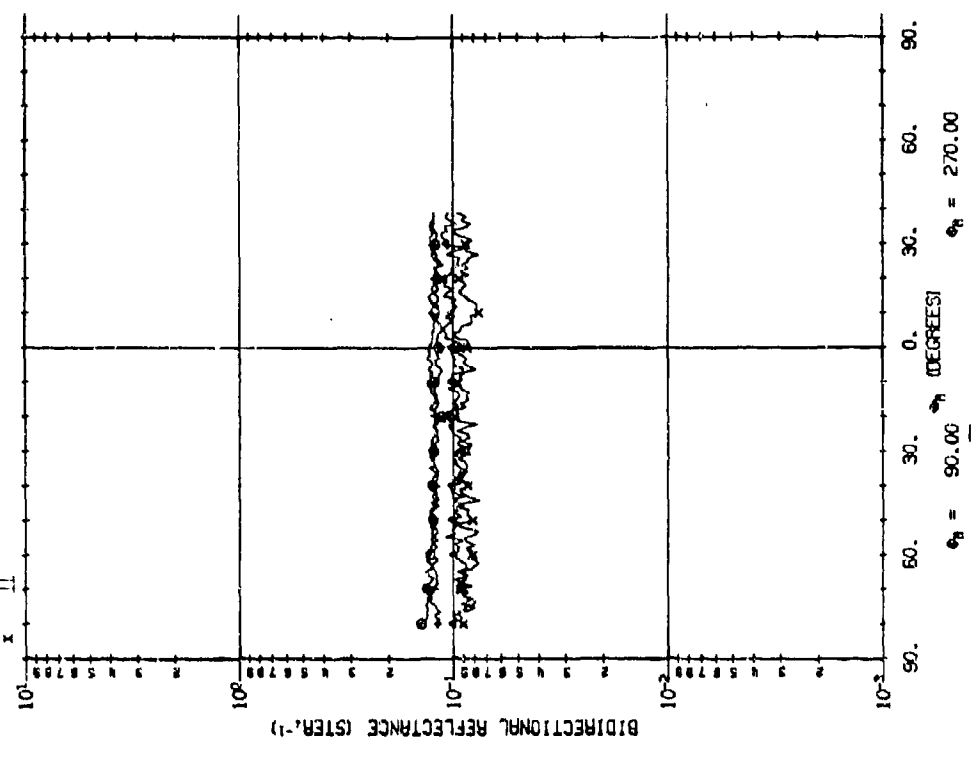
$\theta_i = 56.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$



R02003 101

3M White Paint on Fiberboard

$\theta_i = 56.0$
 $\phi_i = 180.0$
 $\lambda = 1.06$



METAL

R01294 004

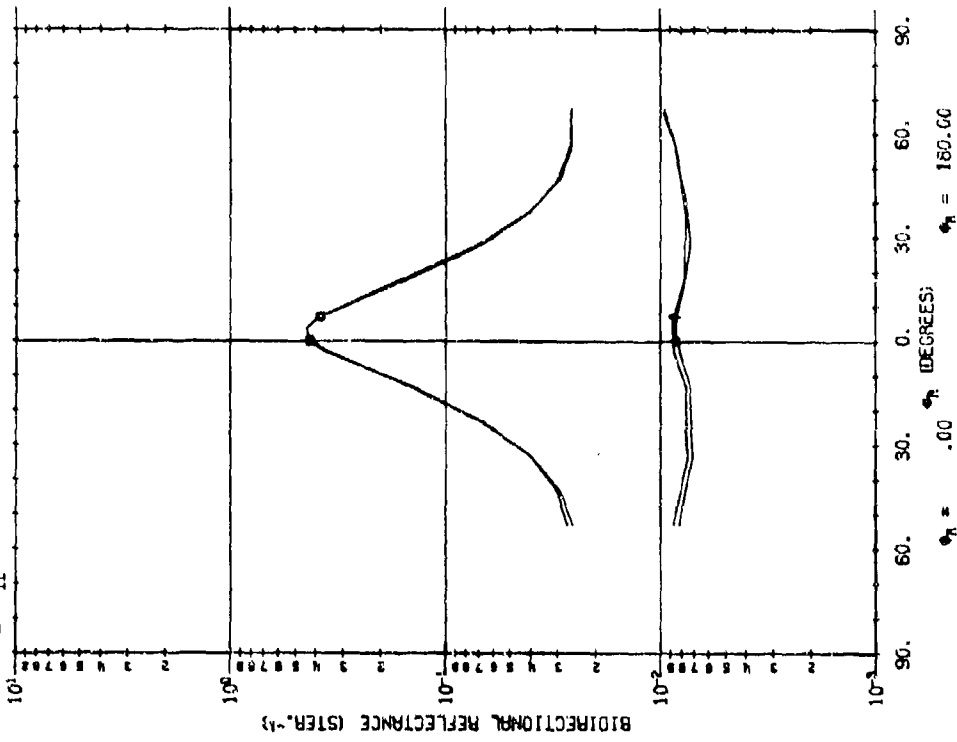
BASE METAL

$2E = 7.0$

$\phi_1 = \phi_2$

$\lambda = 0.63$

0 II
+ II
Δ II
Z II



R01294 004

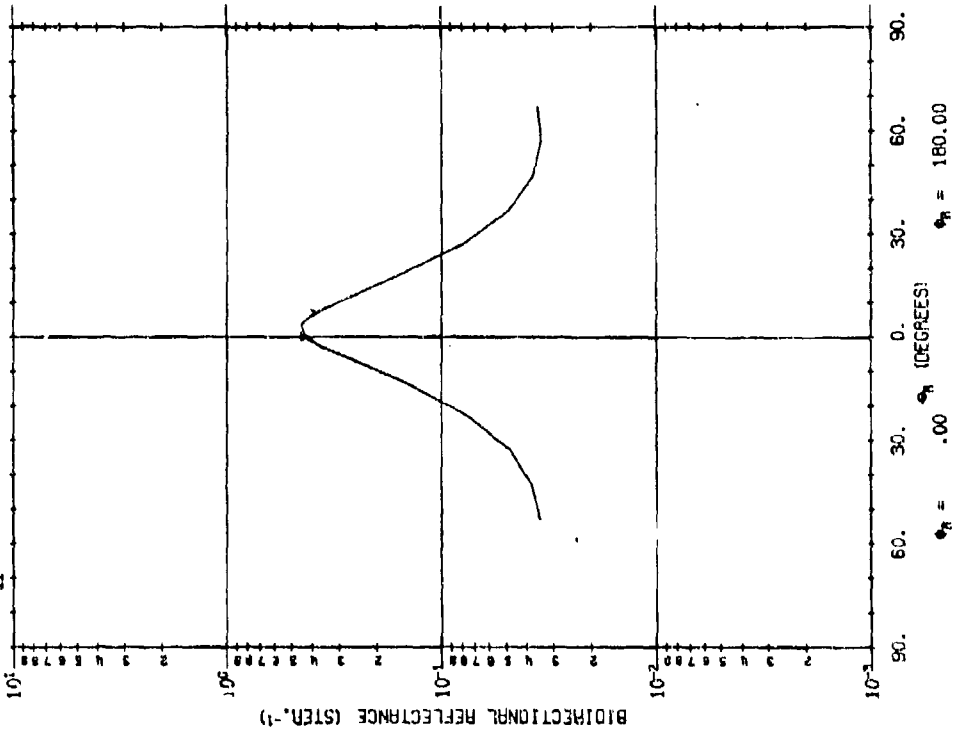
BASE METAL

$2E = 7.0$

$\phi_1 = \phi_2$

$\lambda = 0.63$

+ II
Δ II
X II

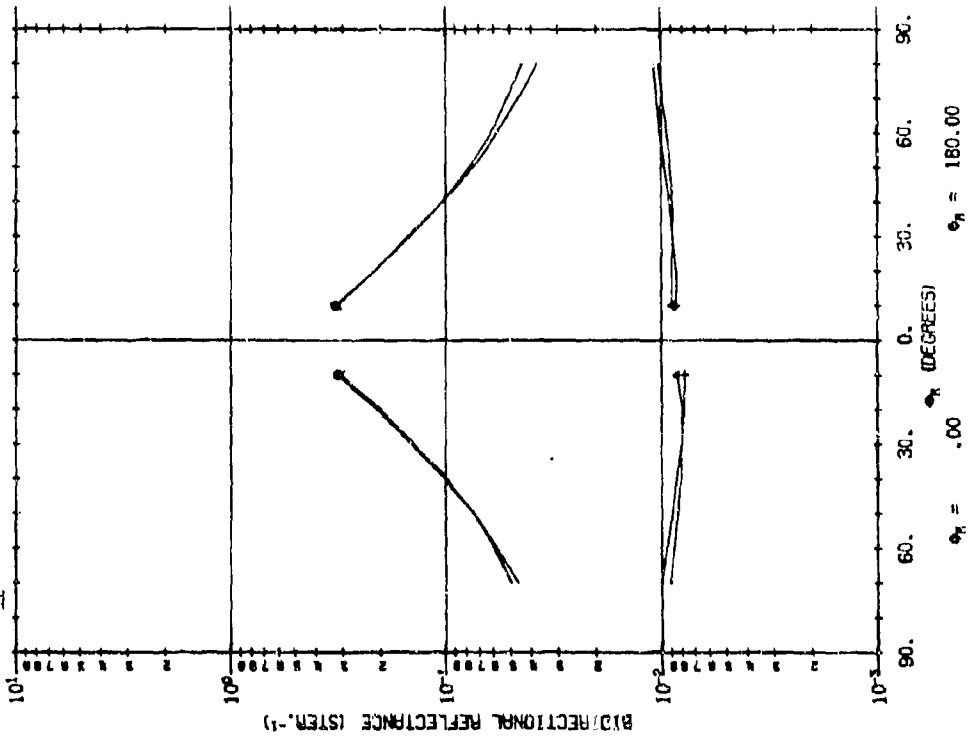


METAL

A01294 004

Bare Metal

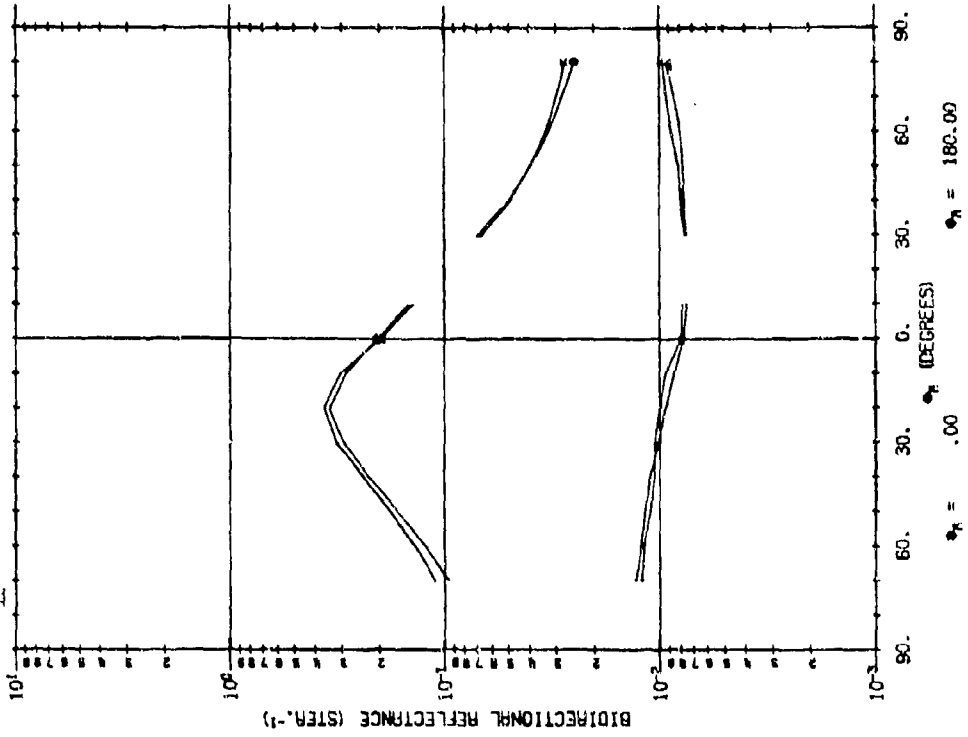
$\epsilon_1 = 0.0$
 $\mu_1 = 180.00$
 $\lambda = 0.63$



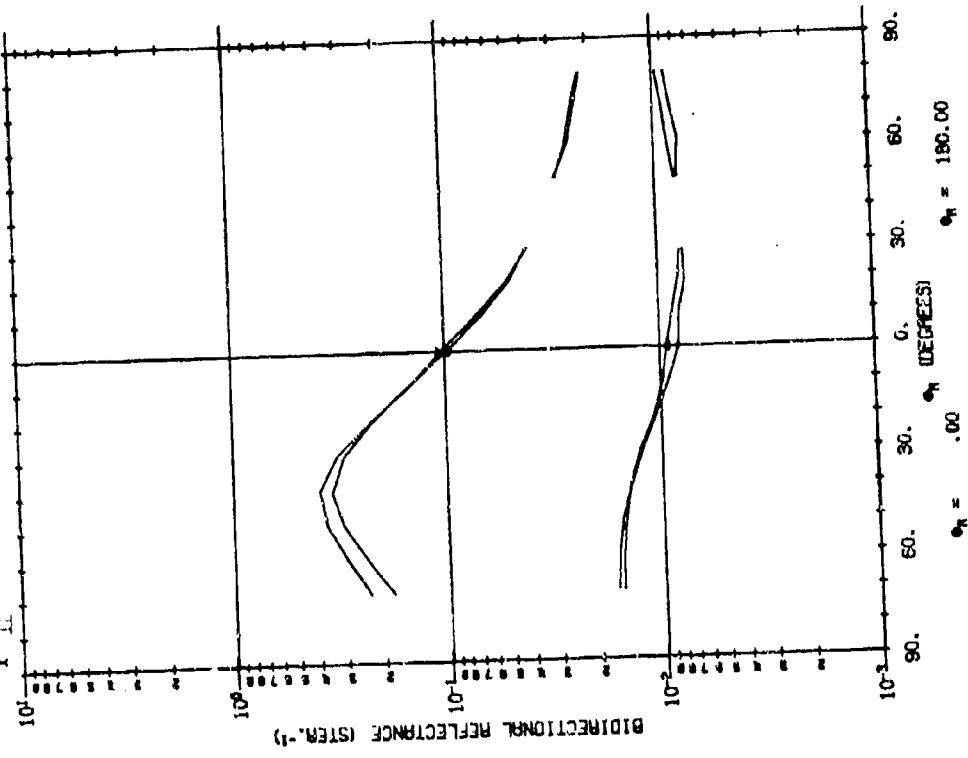
A01294 004

Bare Metal

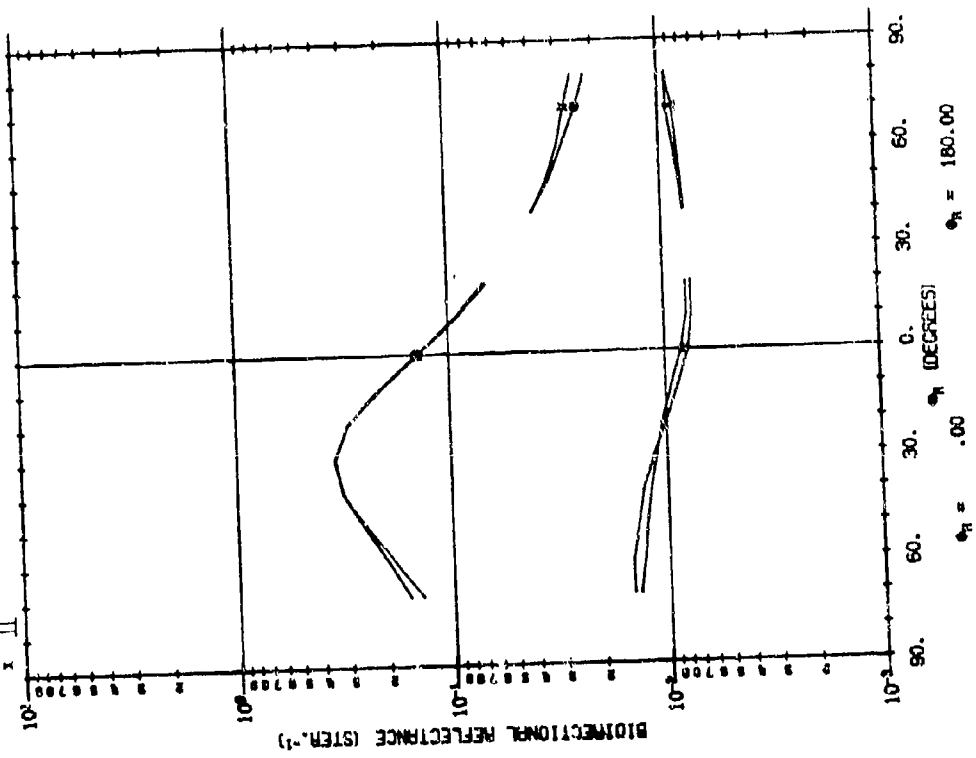
$\epsilon_1 = 20.00$
 $\mu_1 = 180.00$
 $\lambda = 0.63$



A01294 004
 Bare Metal
 $\epsilon_1 = 40.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$



A01294 004
 Bare Metal
 $\epsilon_1 = 30.00$
 $\phi_1 = 180.00$
 $\lambda = 0.63$

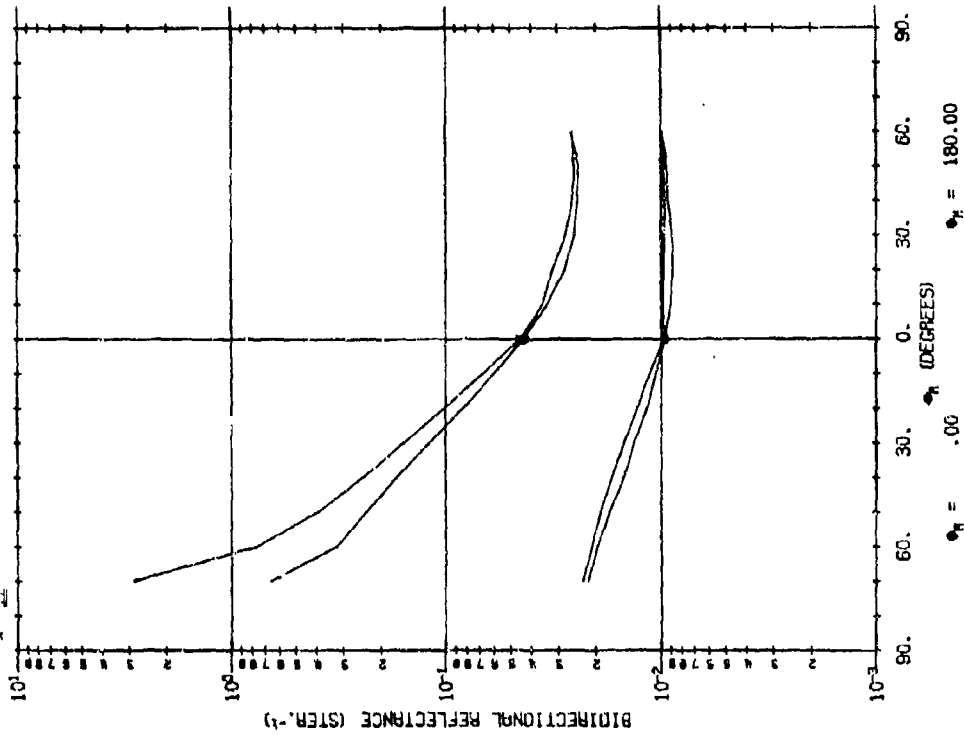


METAL

A01294 004 Bare Metal

$\epsilon_1 = 70.00$
 $\epsilon_2 = 180.00$
 $\epsilon_3 = 0.63$

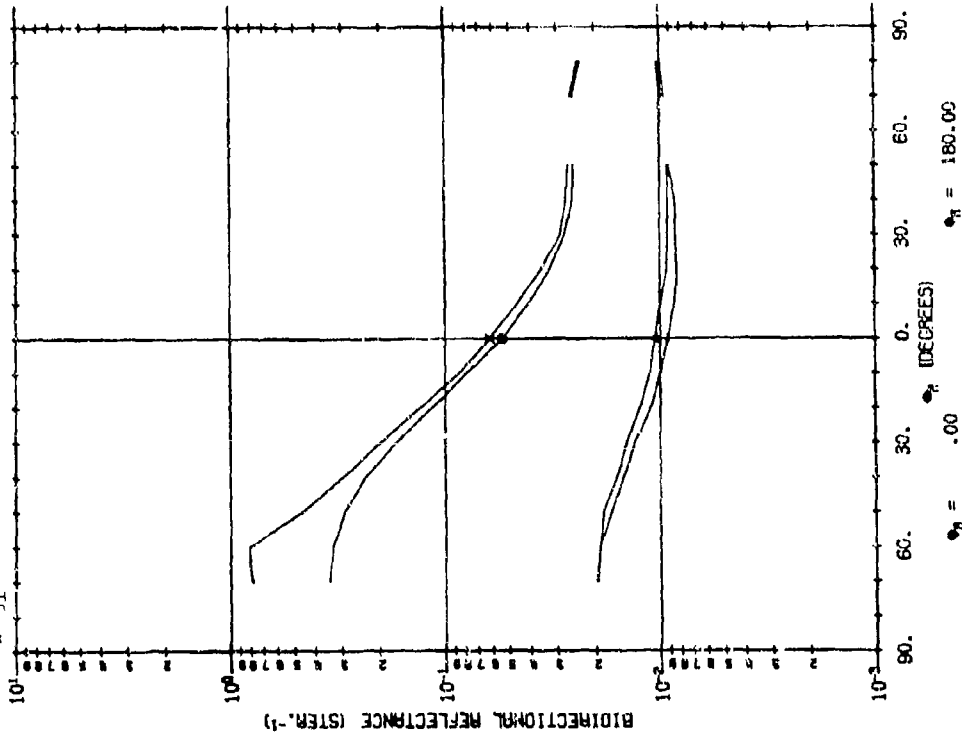
0
 +
 A
 X



A01294 004 Bare Metal

$\epsilon_1 = 50.00$
 $\epsilon_2 = 180.00$
 $\epsilon_3 = 0.63$

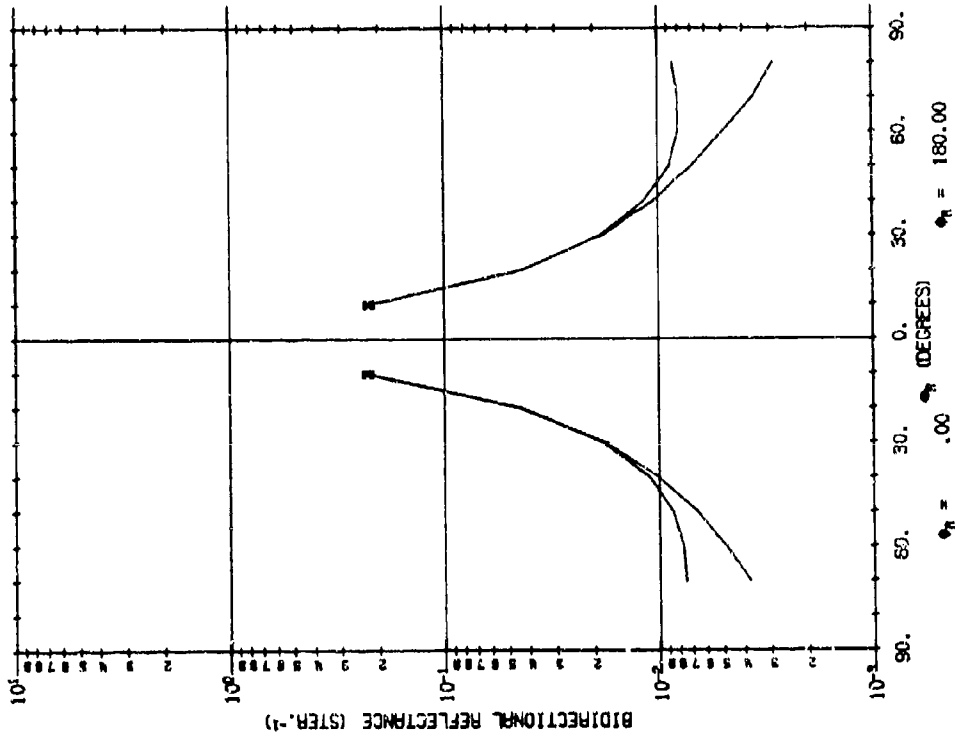
0
 +
 A
 X



R01336 001

ALCLAD ALUMINUM PANEL

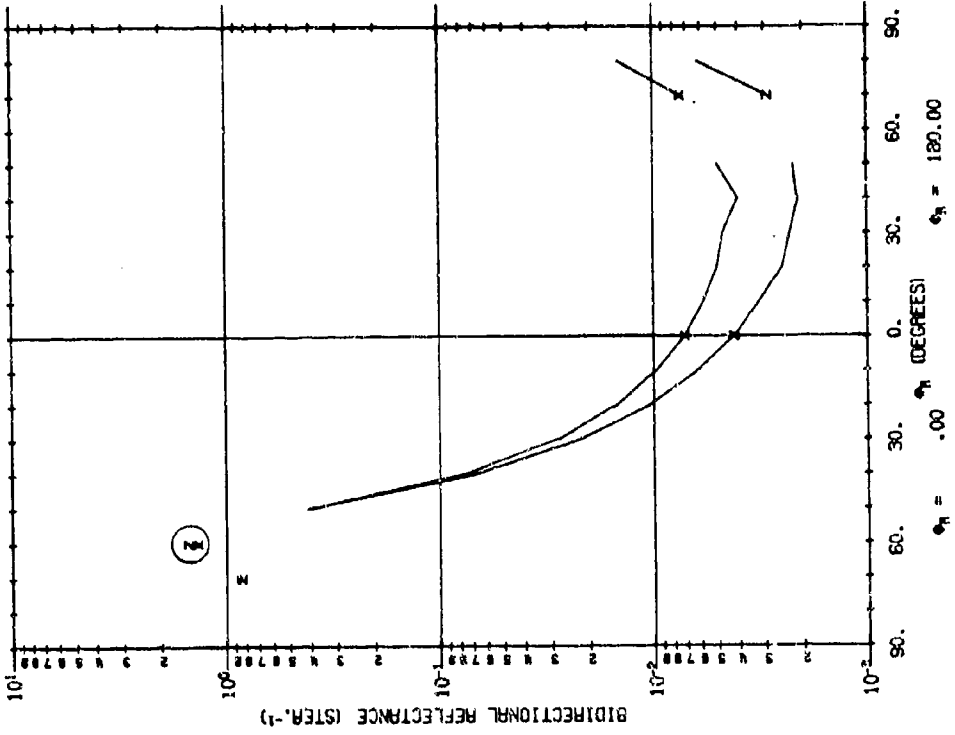
X IT $\phi_1 = 0.0$
Z IT $\phi_2 = 180.0$
 $\lambda = 1.06$



R01336 001

ALCLAD ALUMINUM PANEL

X IT $\phi_1 = 60.0$
Z IT $\phi_2 = 180.0$
 $\lambda = 1.06$

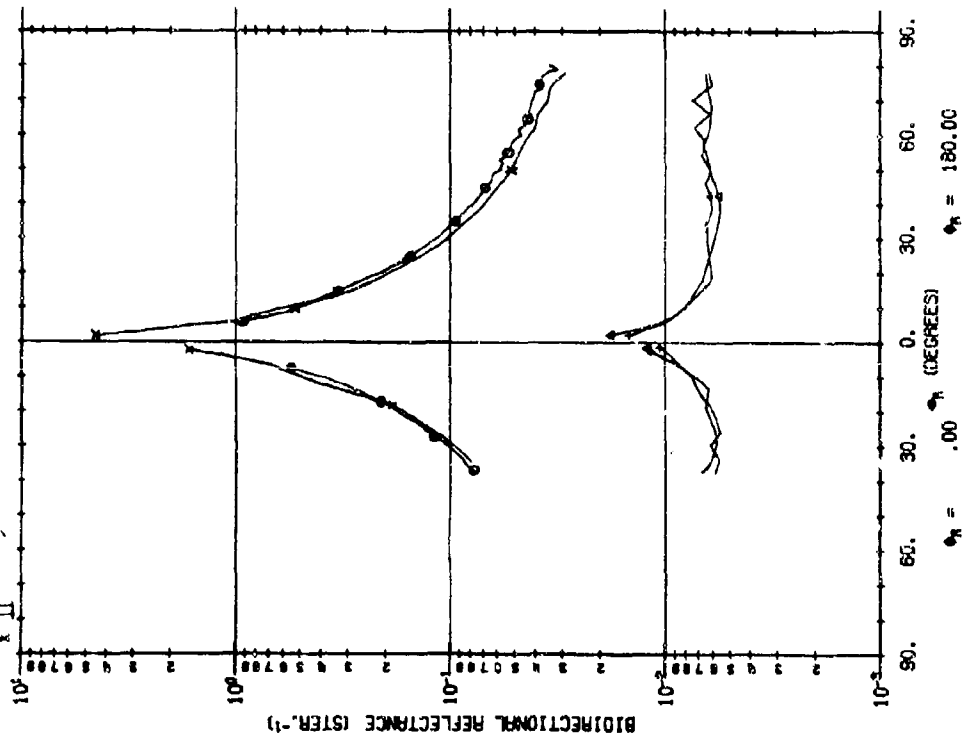


METAL

A01699 201

BARE METAL

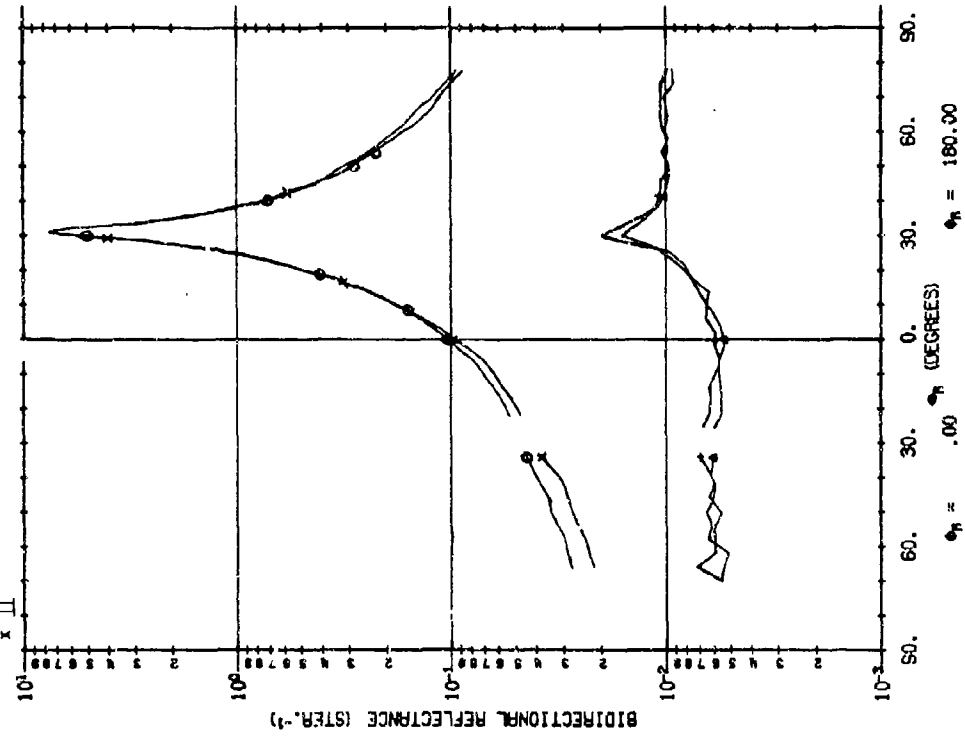
0 || $\theta_1 = 0.0$
+ || $\theta_2 = 0.0$
Δ || $\lambda = 0.63$
x ||



A01699 201

BARE METAL

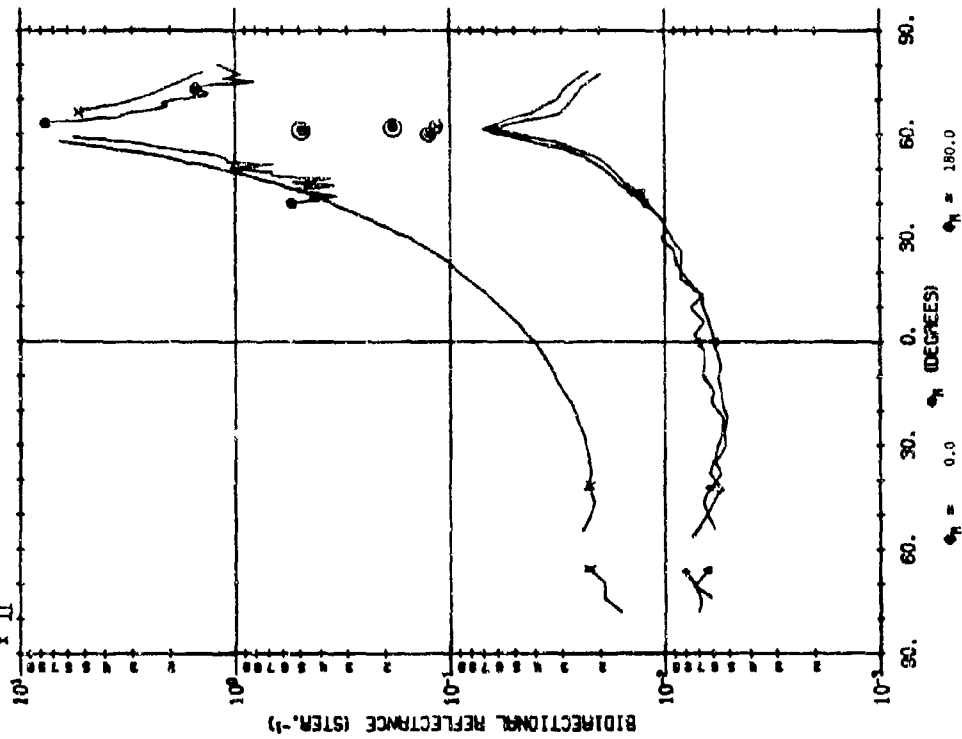
0 || $\theta_1 = 30.0$
+ || $\theta_2 = 0.0$
Δ || $\lambda = 0.63$
x ||



A01699 201

BARE METAL

$\theta_1 = 60.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$

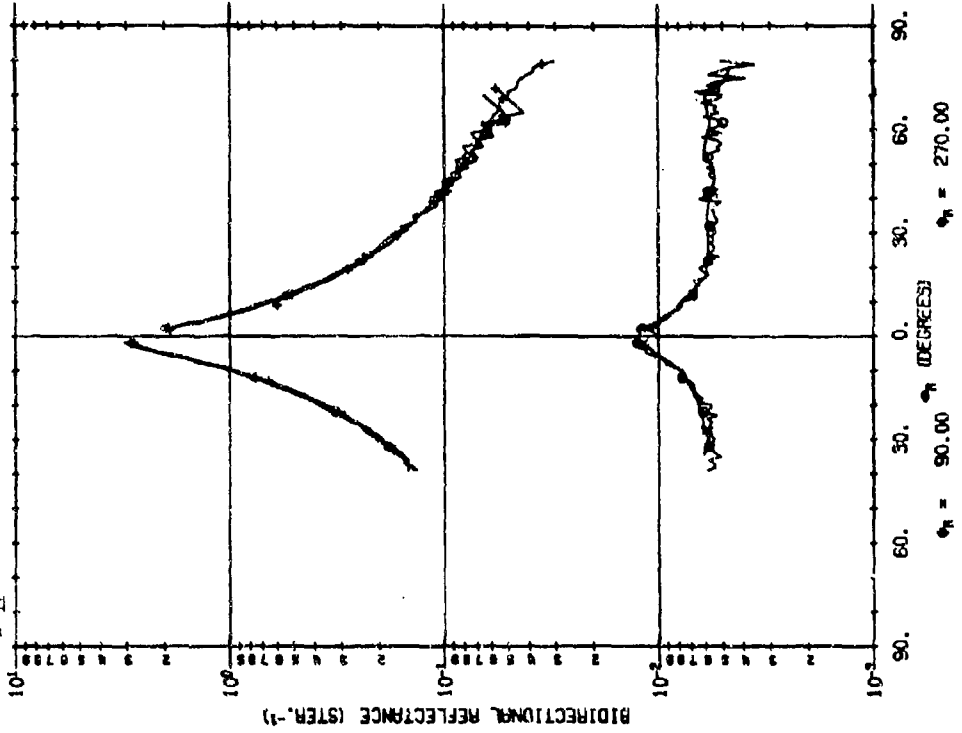


$\theta_1 = 0.0$ $\theta_2 = 180.0$

A01699 201

BARE METAL

$\theta_1 = 0.0$
 $\theta_2 = 0.0$
 $\lambda = 0.63$



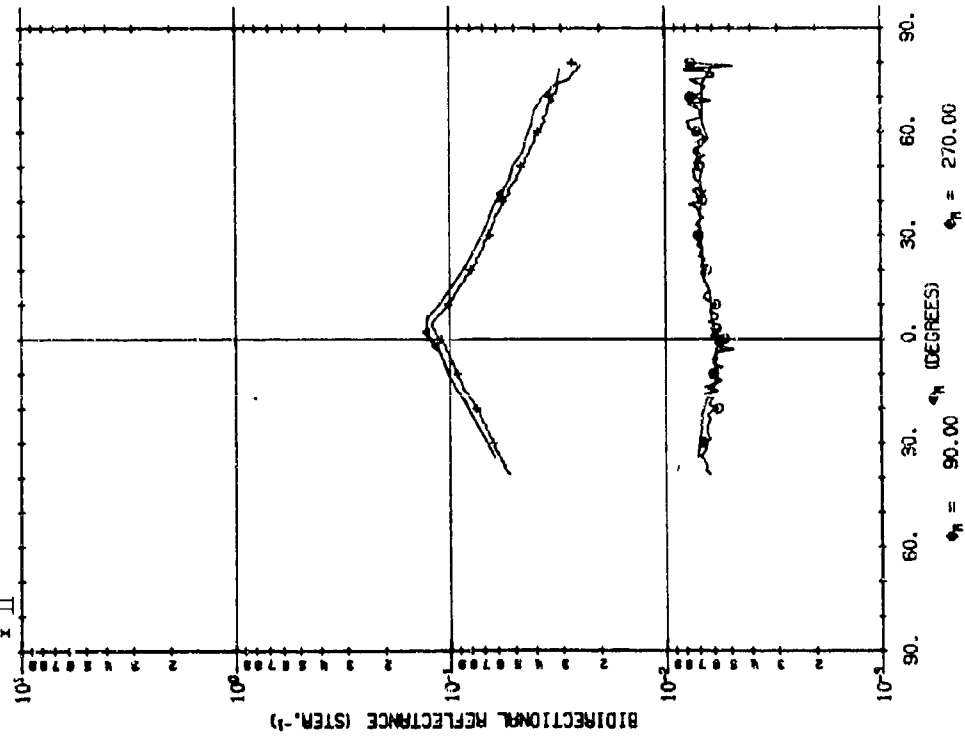
$\theta_1 = 90.00$ $\theta_2 = 270.00$

METAL

P01699 201

BARE METAL

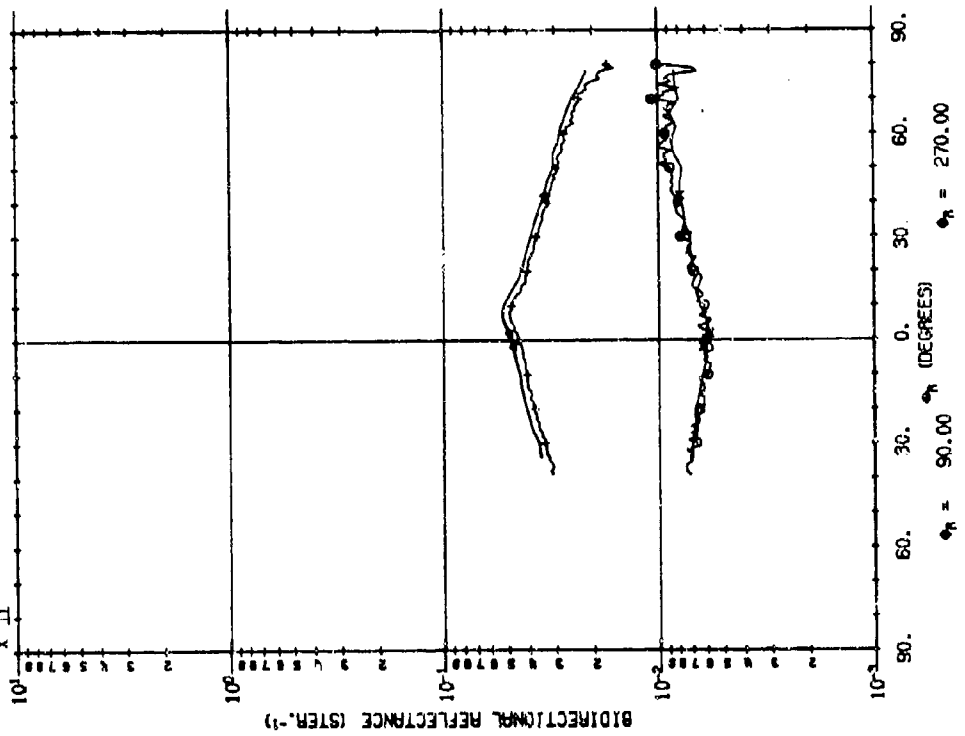
0 || $\theta_1 = 30.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
x ||



P01699 201

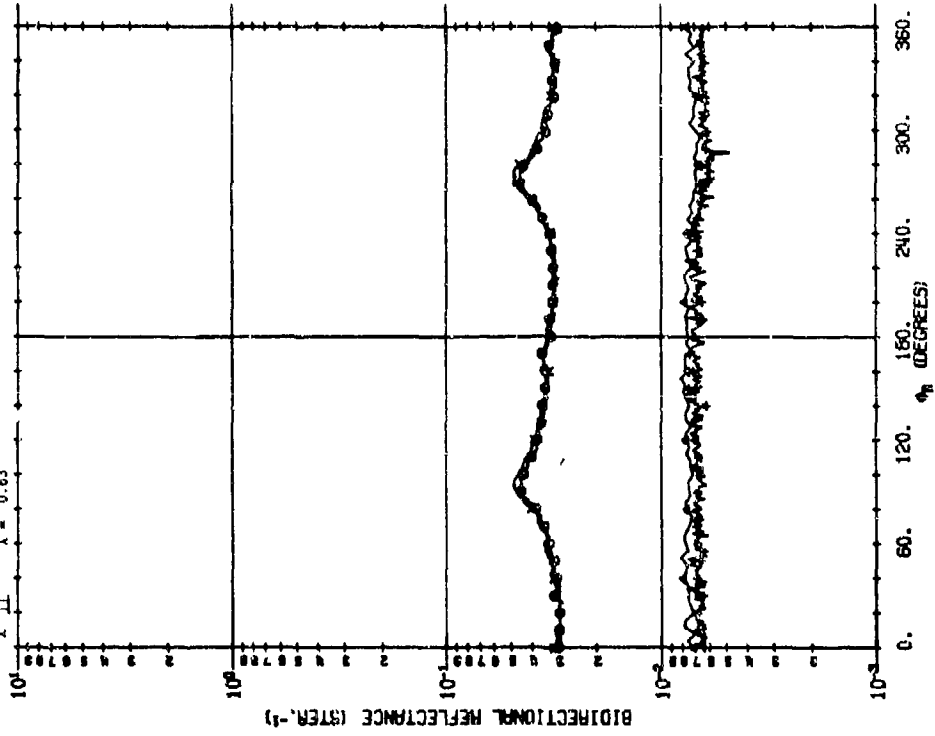
BARE METAL

0 || $\theta_1 = 60.0$
+ || $\phi_1 = 0.0$
Δ || $\lambda = 0.63$
x ||



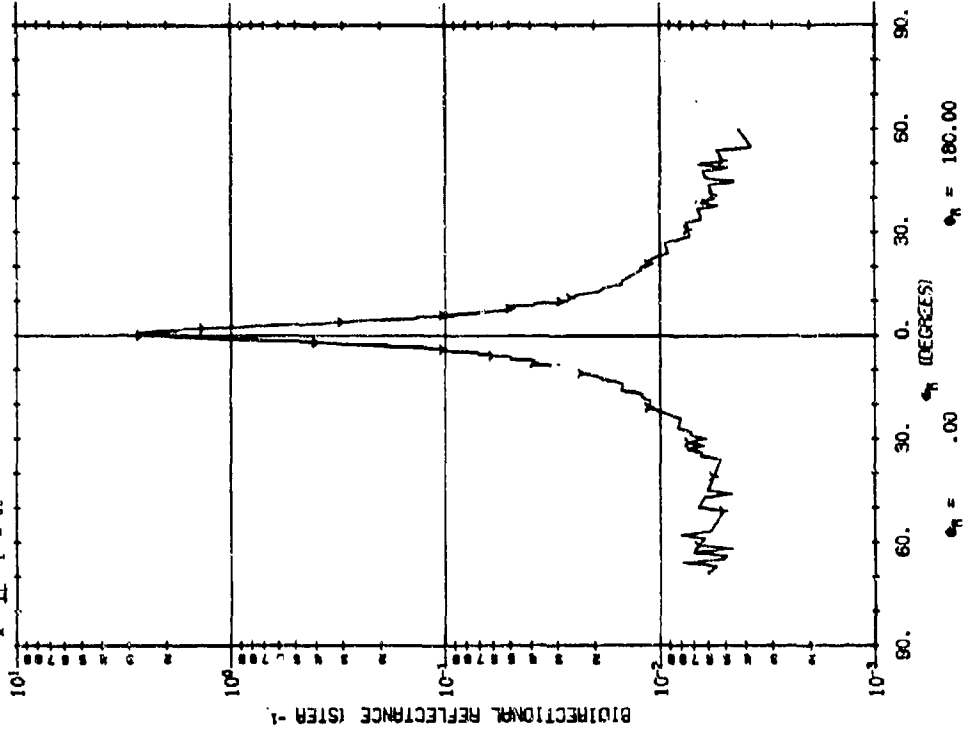
R01699 201

0 || $\theta_1 = 45.0$ BARE METAL
+ || $\theta_1 = 47.0, 28 = 2.0$
 Δ || $\theta_1 = \theta_r$
X || $\lambda = 0.63$



R01884 201

0 || $2\theta = 2.0$ Galvanized Pipe
+ || $\theta_1 = \theta_r$ One and Five-Eighths Inch Diameter
 Δ || $\lambda = 10.5$
X || $\gamma = \gamma_c$

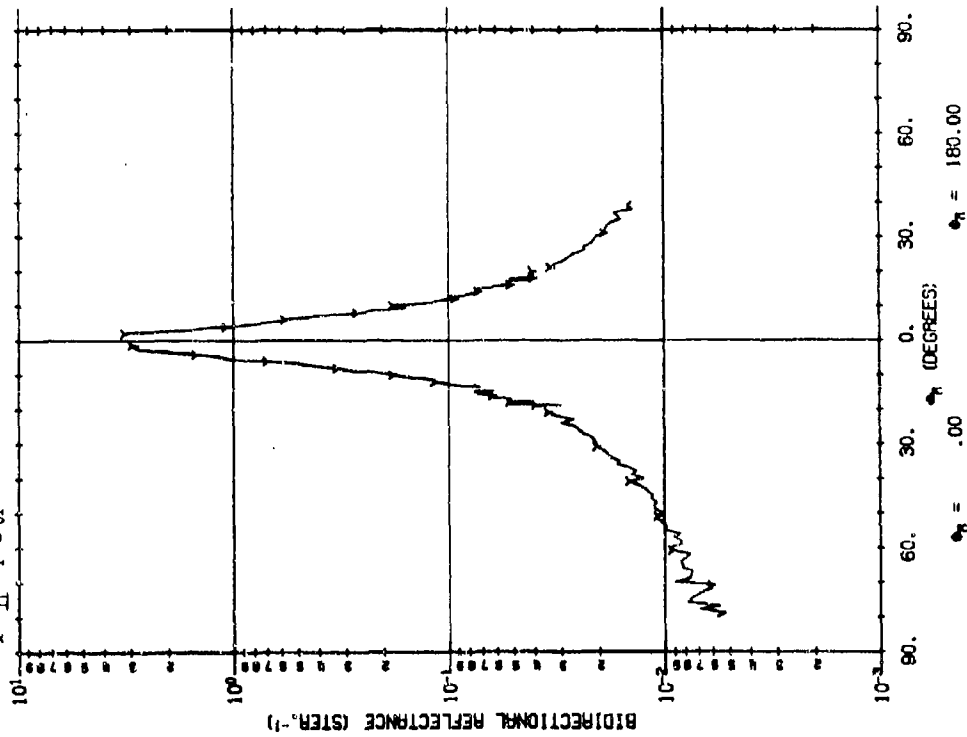


METAL

R01884 201

Galvanized Pipe
One and Five-Eighths Inch Diameter

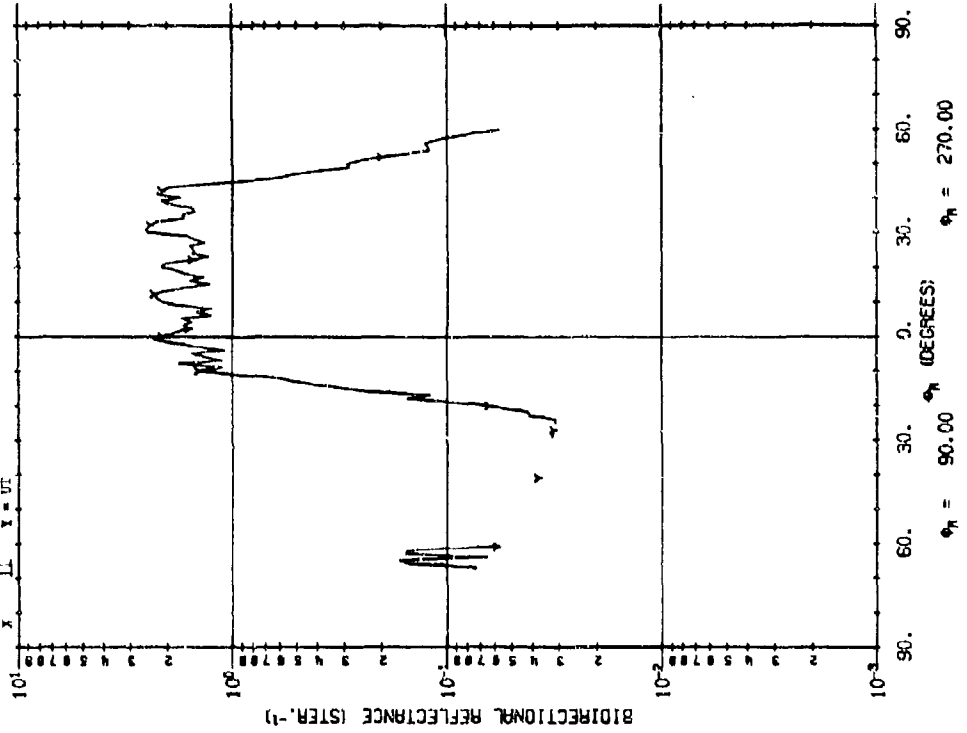
0 || $\phi_1 = 0.0$
+ || $\phi_1 = 180.0$
A || $\lambda = 10.6$
X || Y = UT



R01884 201

GALVANIZED PIPE
One and Five-Eighths Inch Diameter

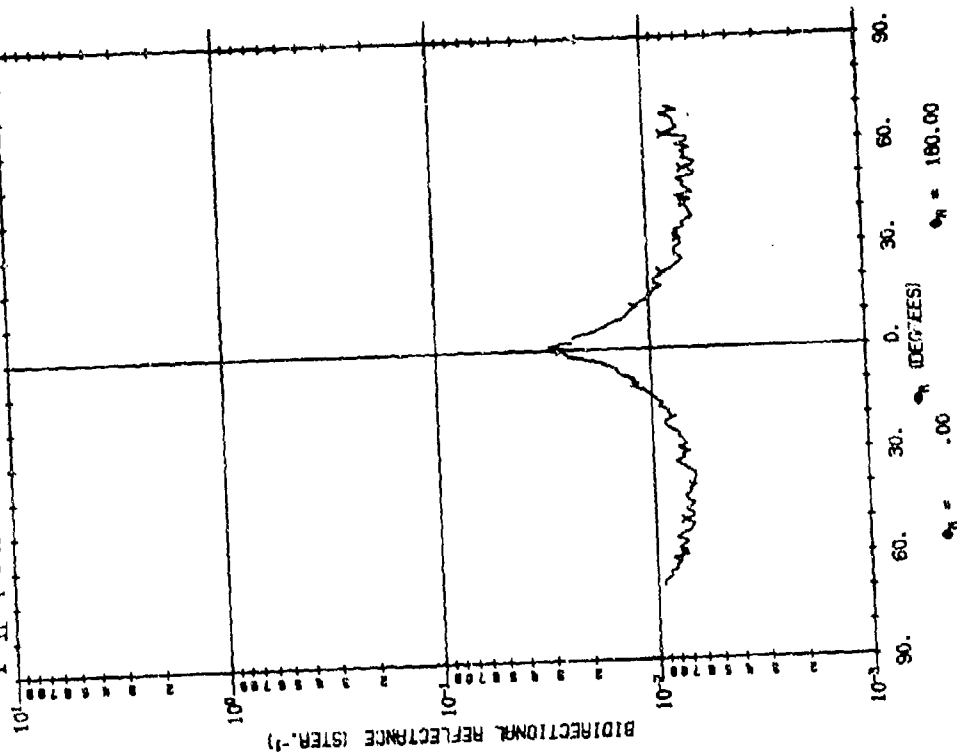
0 || $2\theta = 2.0$
+ || $\phi_1 = 0$
A || $\lambda = 10.6$
X || Y = UT



AO1885 201

Galvanized Pipe
Two and Seven-Eighths Inch Diameter

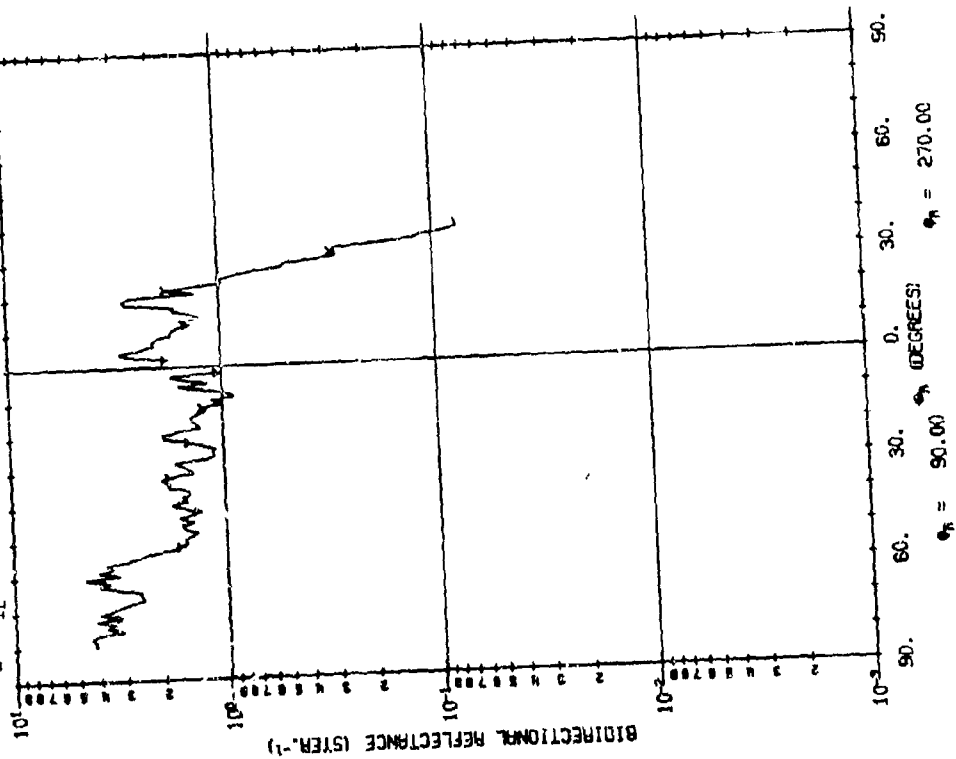
0 || 2 θ = 2.0
+ || ϕ_1 = ϕ_r
 Δ || λ = 10.6
X || Y = UT



AO1884 201

GALVANIZED PIPE
One and Five-Eighths Inch Diameter

0 || ϕ_1 = 0.0
+ || ϕ_r = 0.0
 Δ || λ = 10.6
X || Y = UT

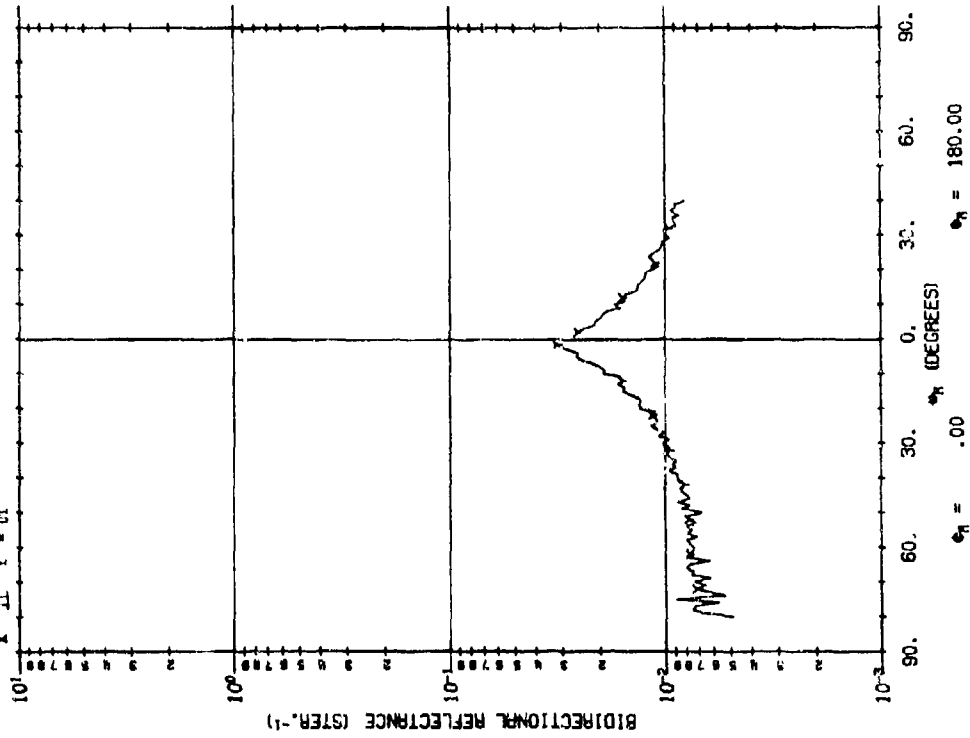


METAL

A01885 201

Galvanized Pipe
Two and Seven-Eighths Inch Diameter

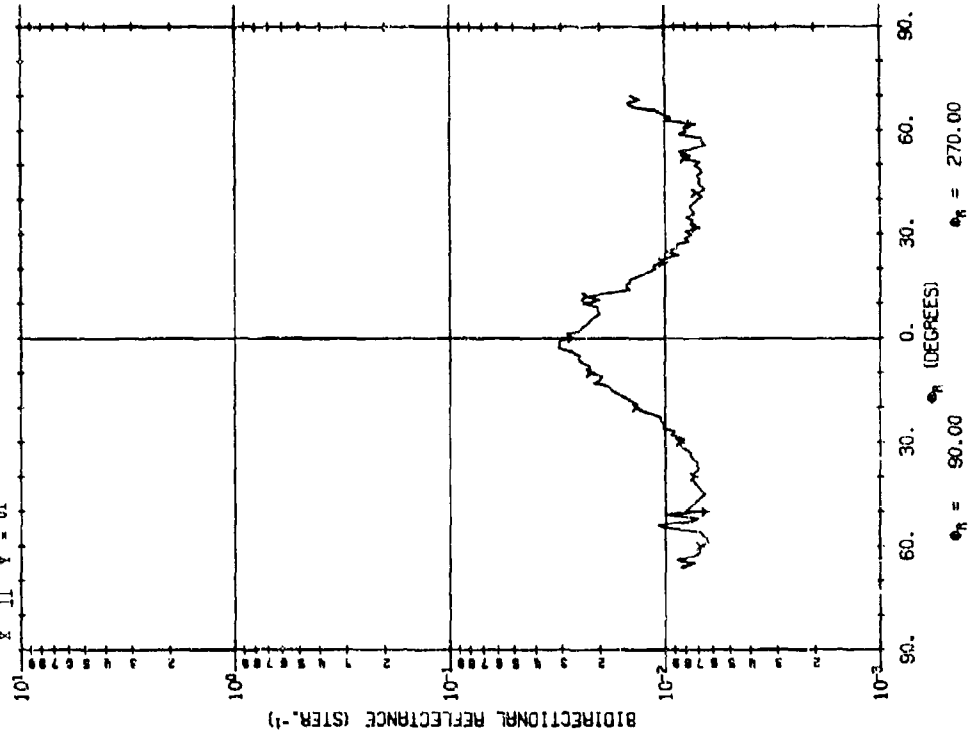
0 || $\phi_1 = 0.0$
+ || $\phi_2 = 180.0$
△ || $\lambda = 10.6$
X || Y = VT



A01885 201

Galvanized Pipe
Two and Seven-Eighths Inch Diameter

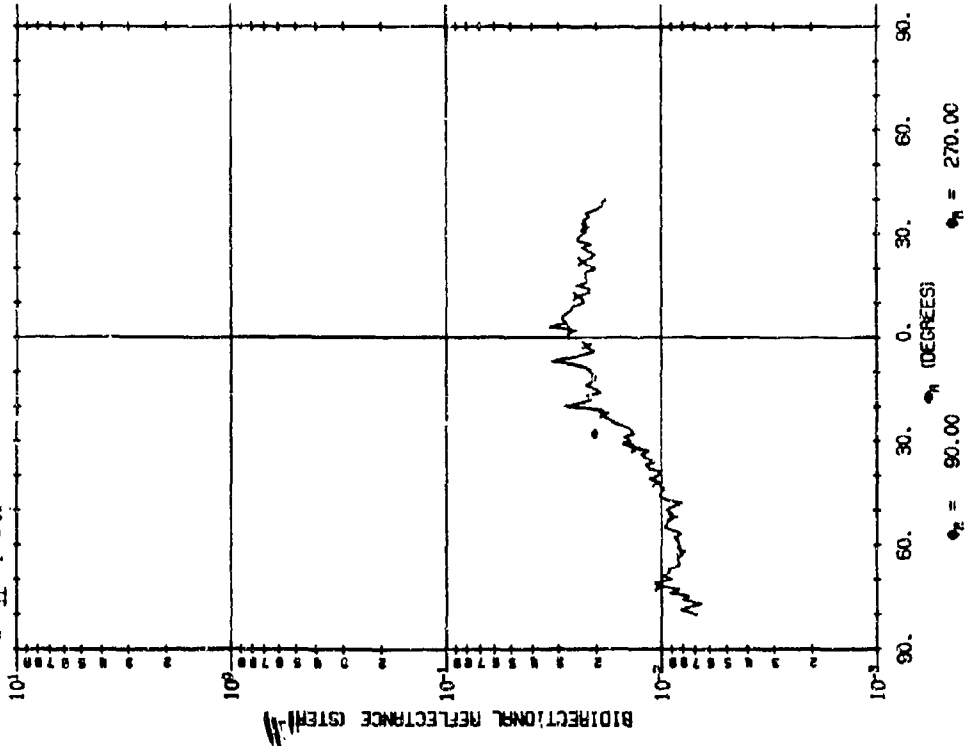
5 || $2\epsilon = 2.0$
+ || $\phi_1 = 0$
△ || $\lambda = 10.6$
X || Y = VT



R01885 201

Galvanized Pipe
Two and Seven-Eighths Inch Diameter

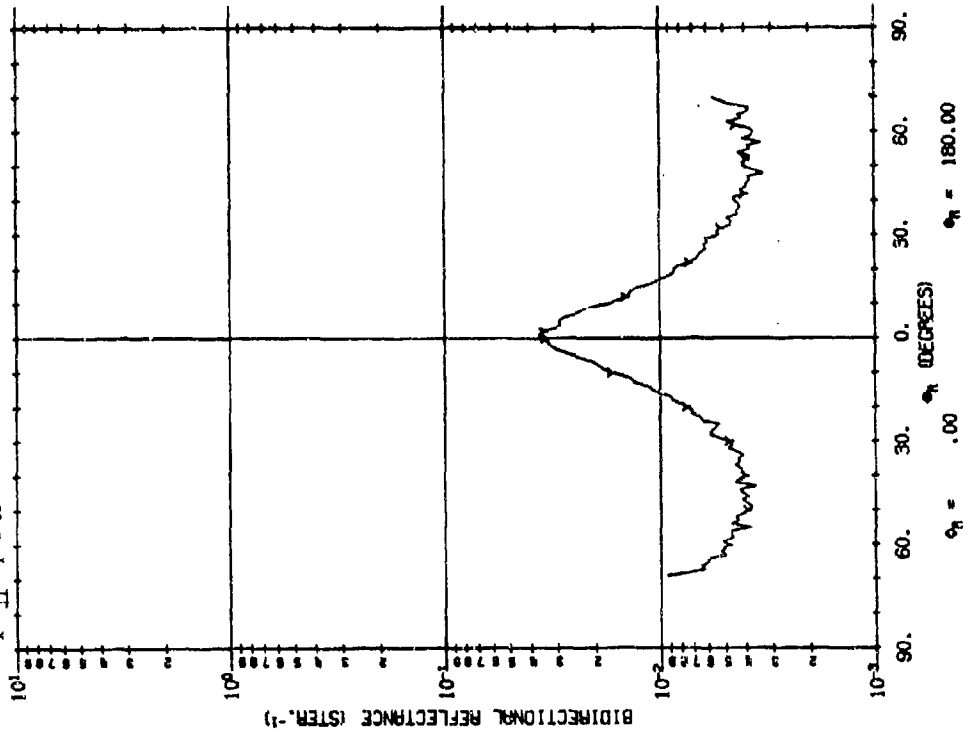
0 || $\theta_1 = 0.0$
+ || $\theta_1 = 270.0$
Δ || $\lambda = 10.6$
X || Y = UT



R01886 201

Galvanized Pipe
Three and One Half Inch Diameter

0 || $\theta_1 = 2.0$
+ || $\theta_1 = \uparrow$
Δ || $\lambda = 10.6$
X || Y = VT

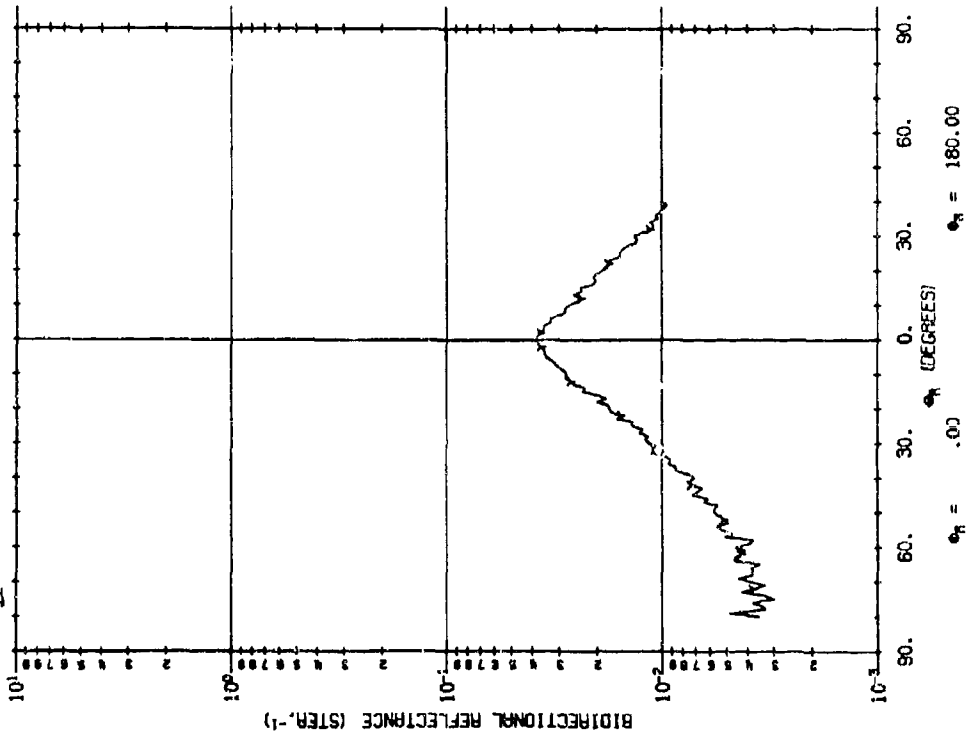


METAL

A01886 201

Galvanized Pipe
Three and One Half Inch Diameter

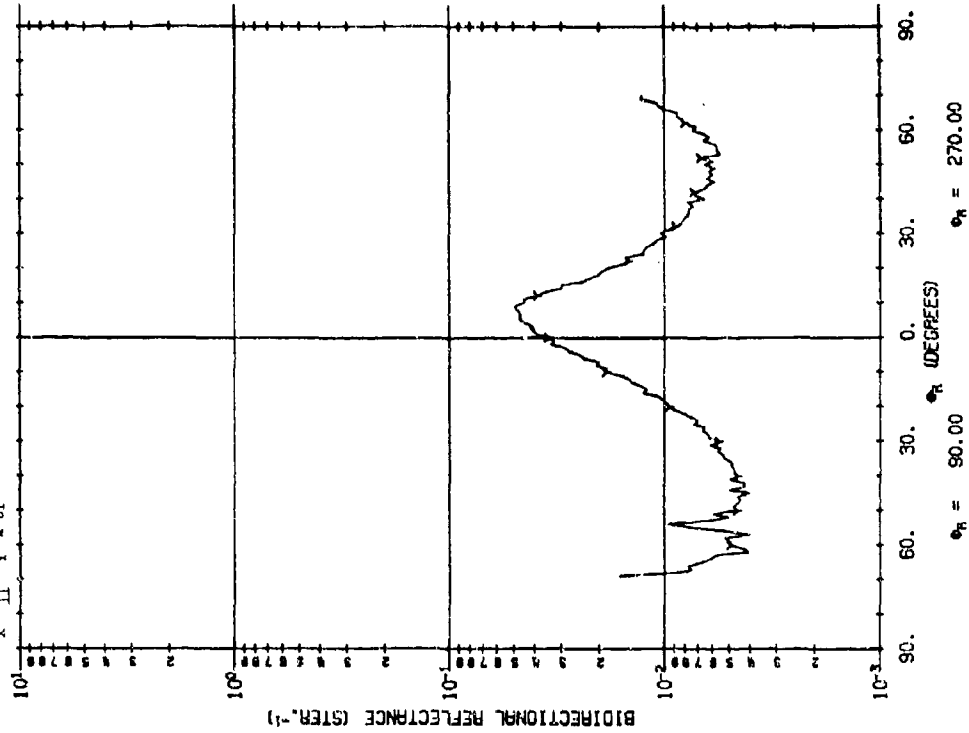
$\phi_1 = 0.0$
 $\phi_2 = 180.0$
 $\lambda = 10.6$
X Y = UT



A01886 201

Galvanized Pipe
Three and One Half Inch Diameter

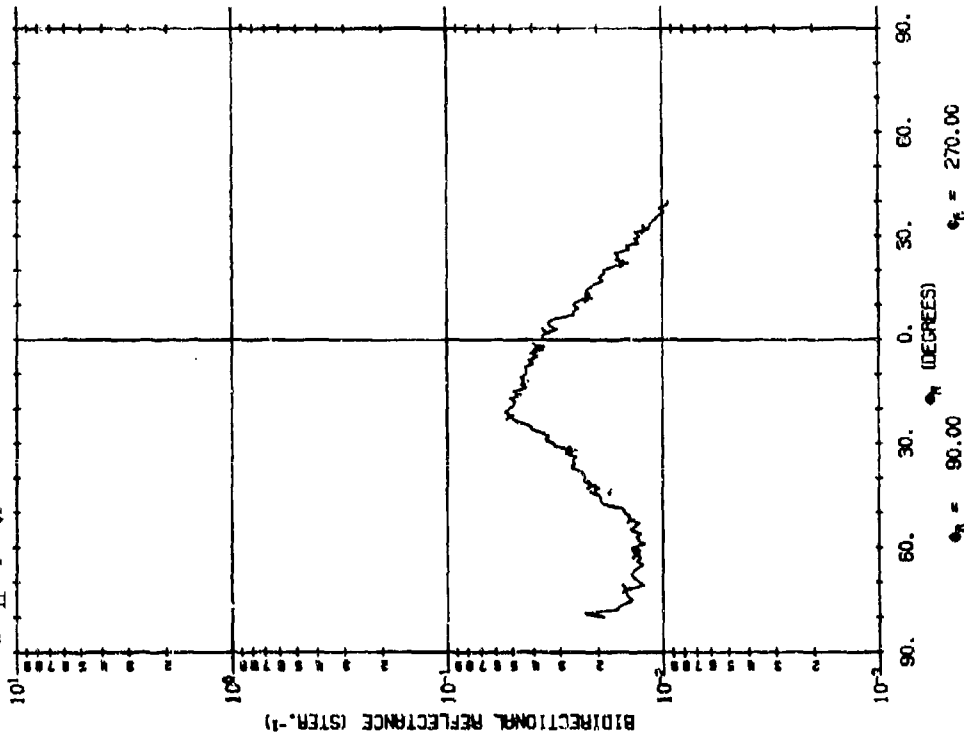
$\phi_1 = 270.0$
 $\phi_2 = 90.0$
 $\lambda = 10.6$
X Y = UT



R01866 201

0 || $\theta_1 = 0.0$
+ || $\phi_1 = 270.0$
2 || $\lambda = 10.6$
X || Y = VT

Galvanized Pipe
Three and One Half Inch Diameter

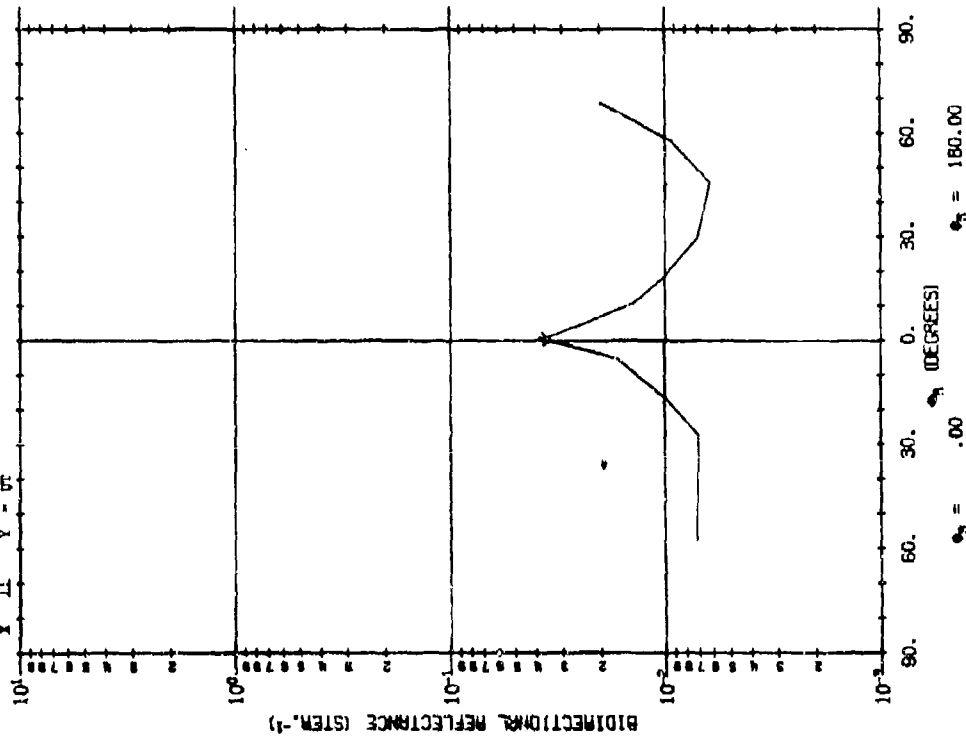


METAL

MISCELLANEOUS

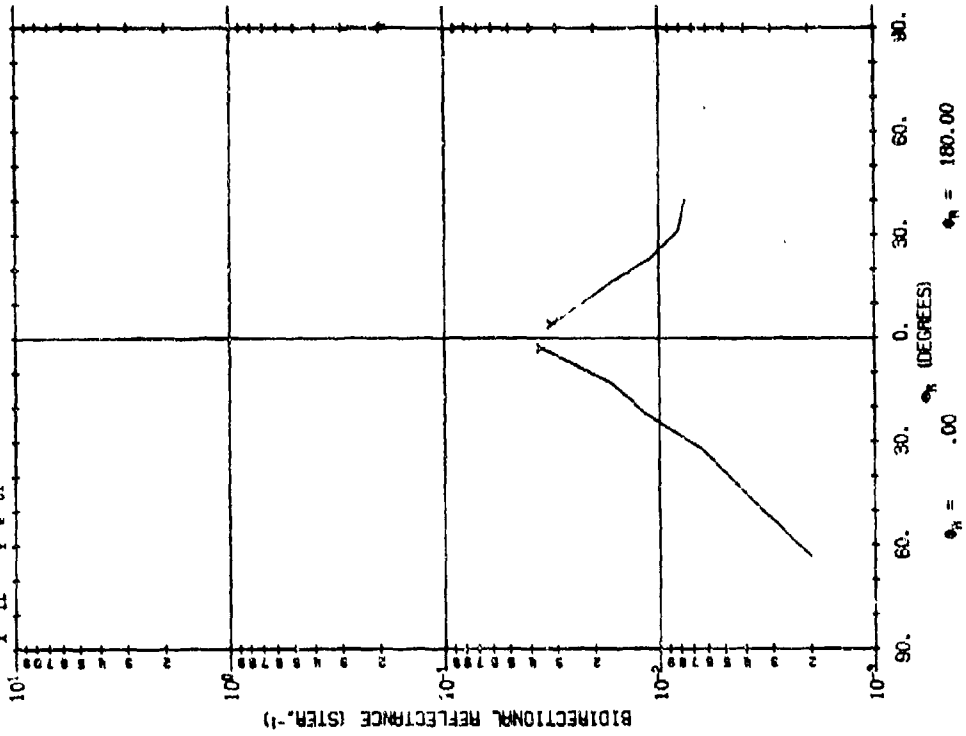
R01584 001
 0 || 2 θ = 1.10
 + || θ_1 = θ_r
 A || λ = 10.6
 X || Y = VT

Creosote Treated Wood



R01584 001
 0 || θ_1 = 0.0
 + || θ_r = 180.0
 L || λ = 10.6
 X || Y = VT

Creosote Treated Wood

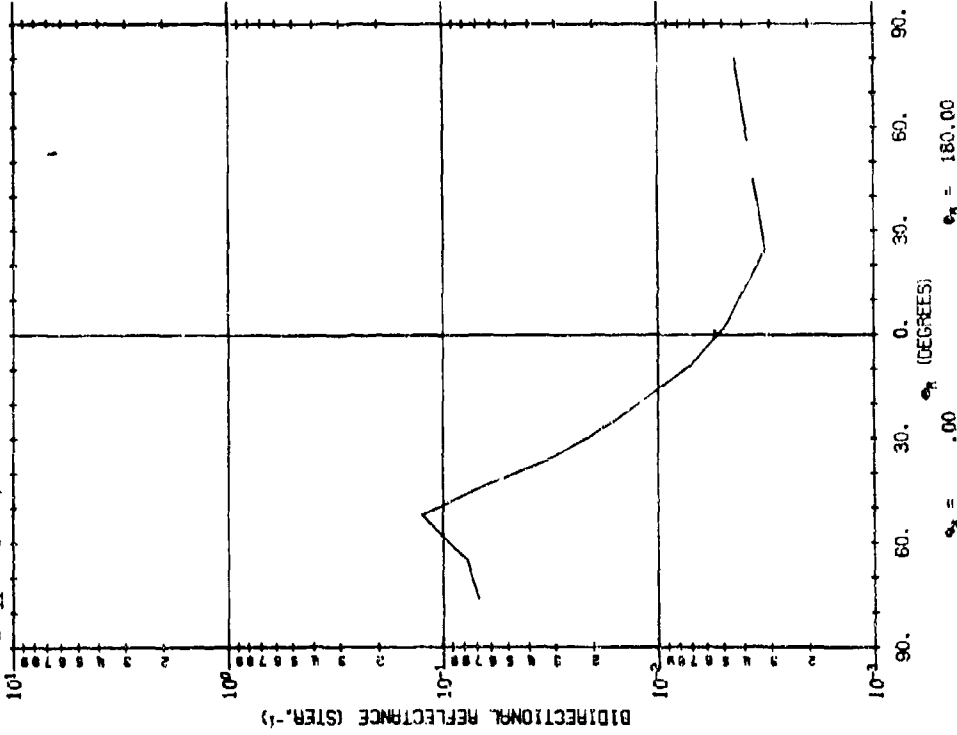


MISCELLANEOUS

R01584 001

Creosote Treated Wood

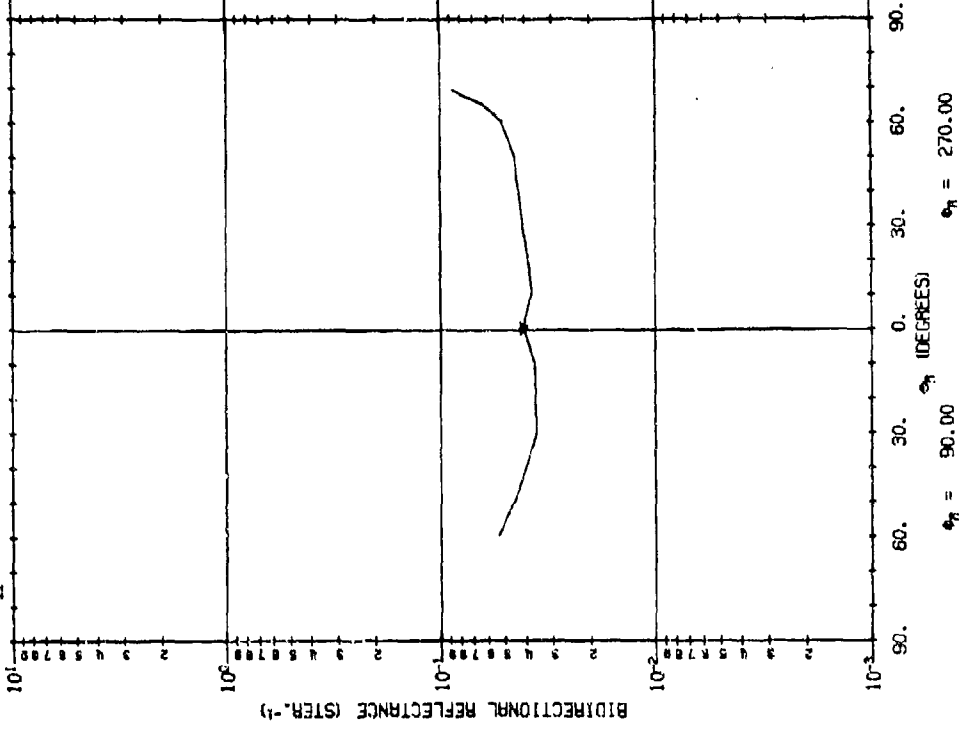
0 // $\theta_1 = 50.0$
+ // $\theta_2 = 180.0$
L // $\lambda = 10.6$
X // Y = UT



R01584 001

Creosote Treated Wood

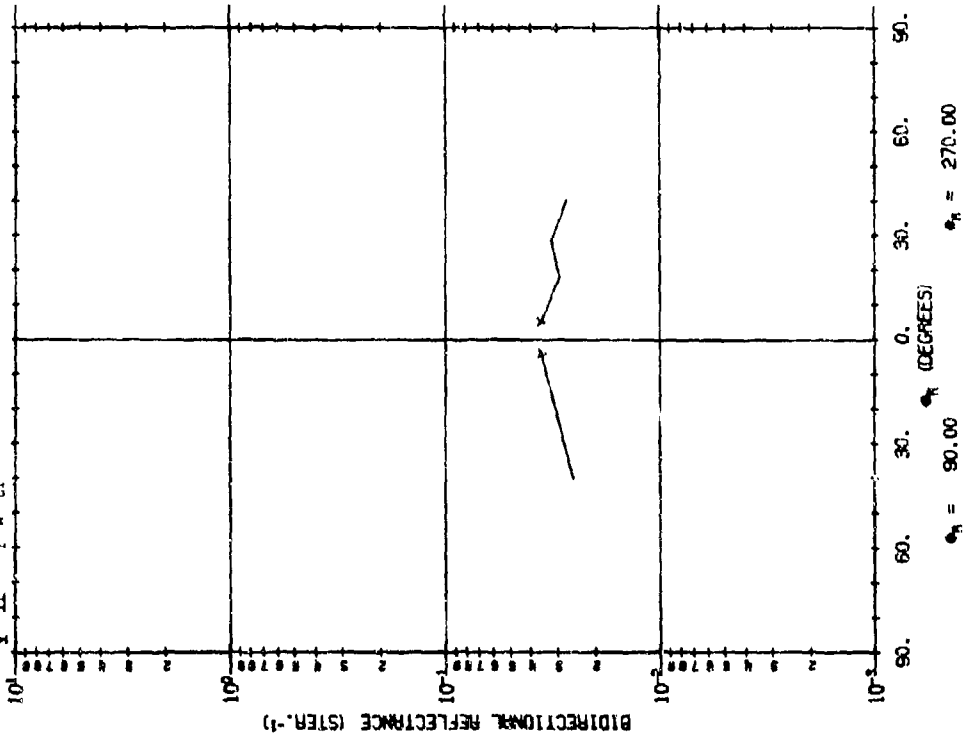
C // $\theta_1 = 1.10$
+ // $\theta_2 = \theta_1$
L // $\lambda = 10.6$
X // Y = UT



AD1584 001

Creosote Treated Wood

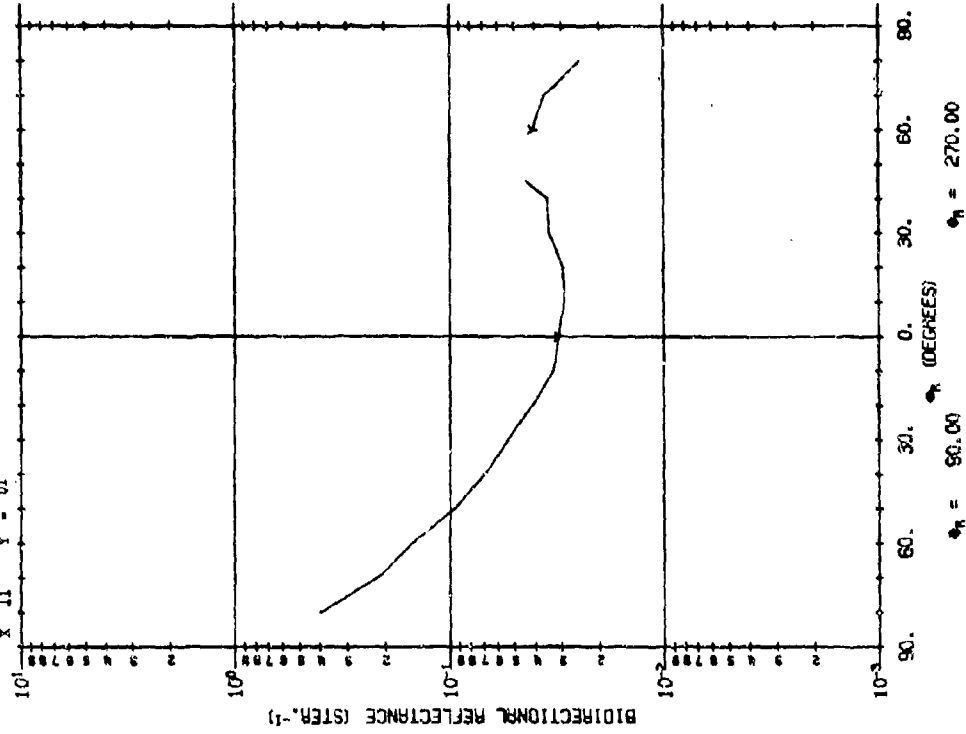
0 || $\theta_1 = 0.0$
+ || $\phi_1 = 270.0$
Δ || $\lambda = 10.6$
X || $\gamma = 0^\circ$



AD1584 001

Creosote Treated Wood

0 || $\theta_1 = 50.0$
+ || $\phi_1 = 270.0$
Δ || $\lambda = 10.6$
X || $\gamma = 0^\circ$

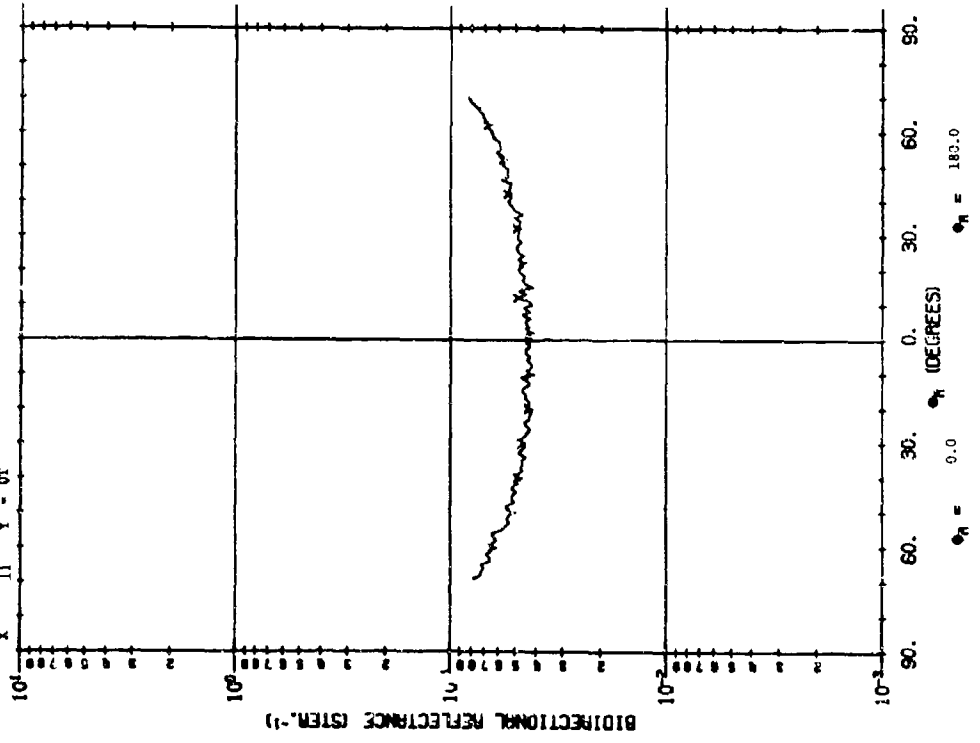


MISCELLANEOUS

A01921 101

Pressed Cork

0 || 2 θ = 2.0
 + || ϕ_1 = ϕ_2
 Δ || λ = 10.6
 X || Y = UT

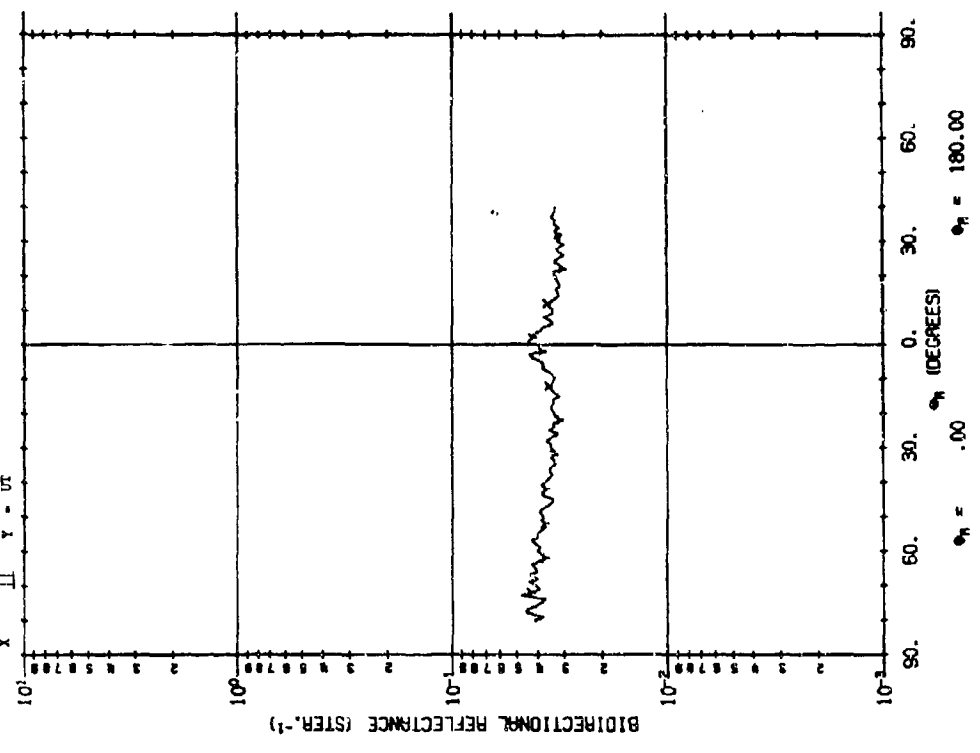


$\phi_n = 0.0$ $\phi_n = 180.0$

A01921 101

Pressed Cork

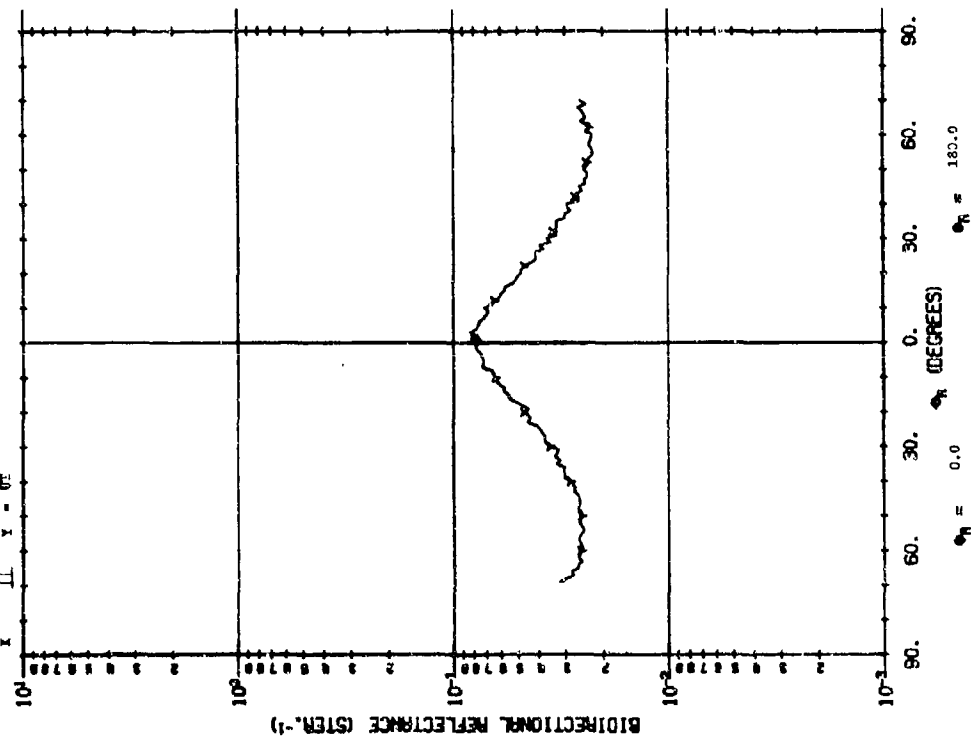
0 || ϕ_1 = 0.0
 + || ϕ_2 = 180.0
 Δ || λ = 10.6
 X || Y = UT



$\phi_n = .00$ $\phi_n = 180.00$

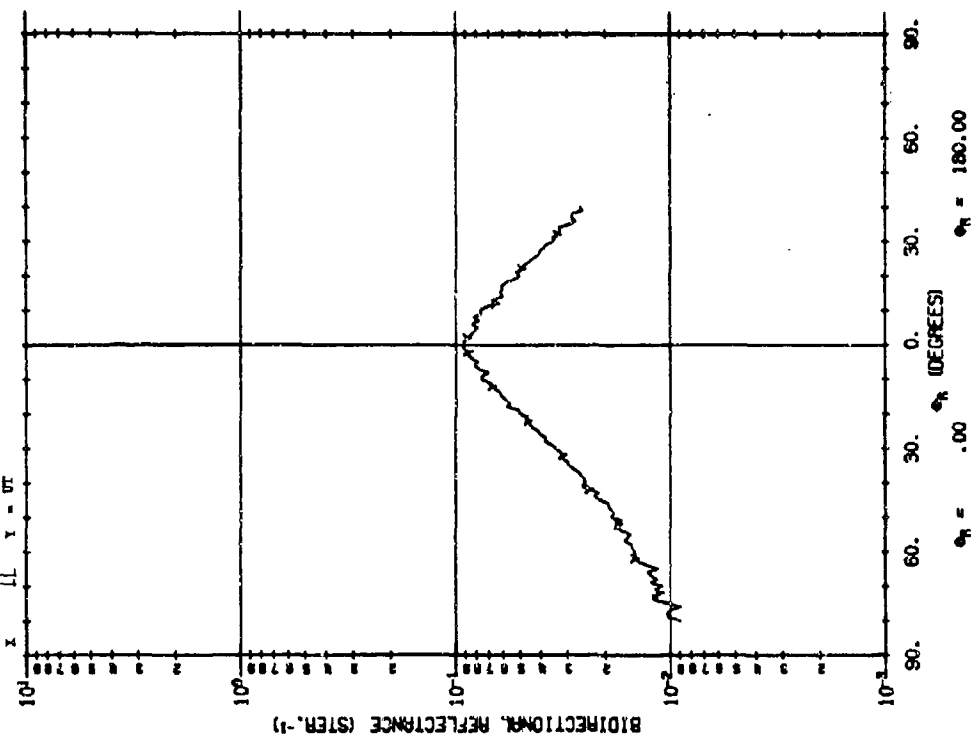
R01923 101

White Posterboard
0 || 22 = 2.0
+ || || $\theta_1 = \theta_2$
 Δ || || $\lambda = 10.6$
X || || $\gamma = 0^\circ$



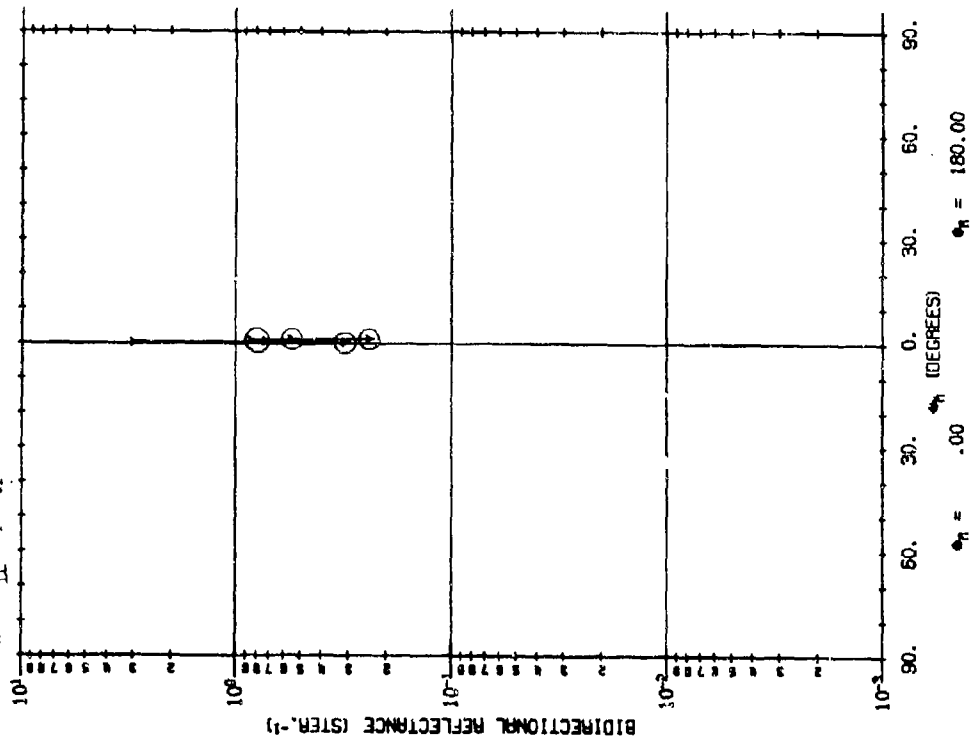
R01923 101

White Posterboard
0 || $\theta_1 = 0.0$
+ || || $\theta_2 = 180.0$
 Δ || || $\lambda = 10.6$
X || || $\gamma = 0^\circ$

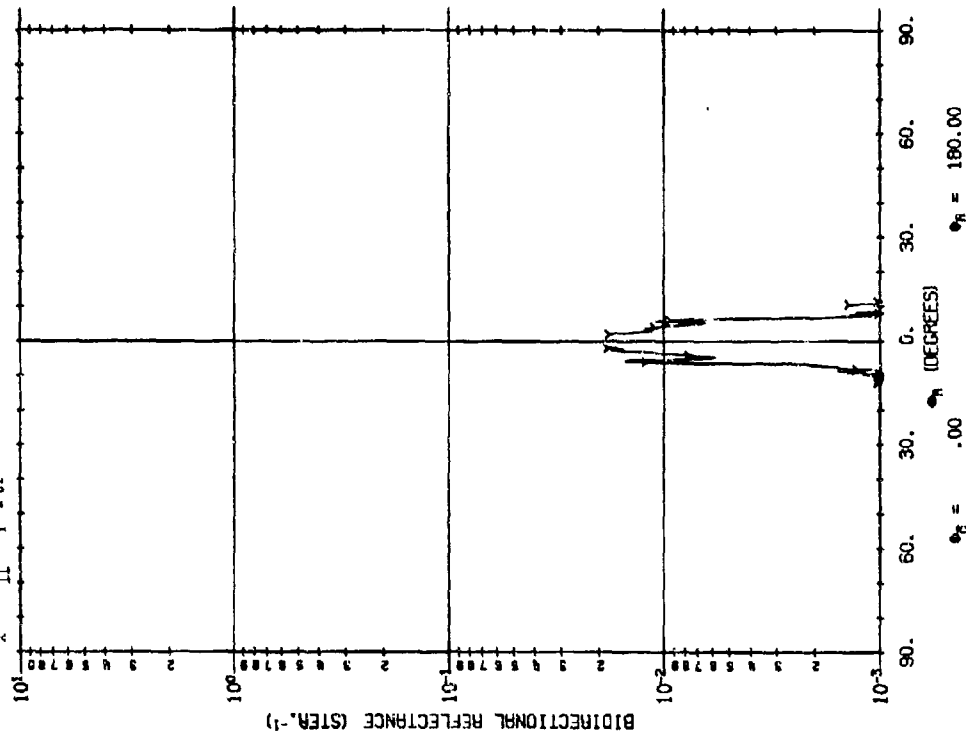


MISCELLANEOUS

A01925 101
 Acrylic Plexiglass
 2 θ = 2.0
 $\phi_1 = \phi_2$
 $\lambda = 10.6$
 Y = 0V



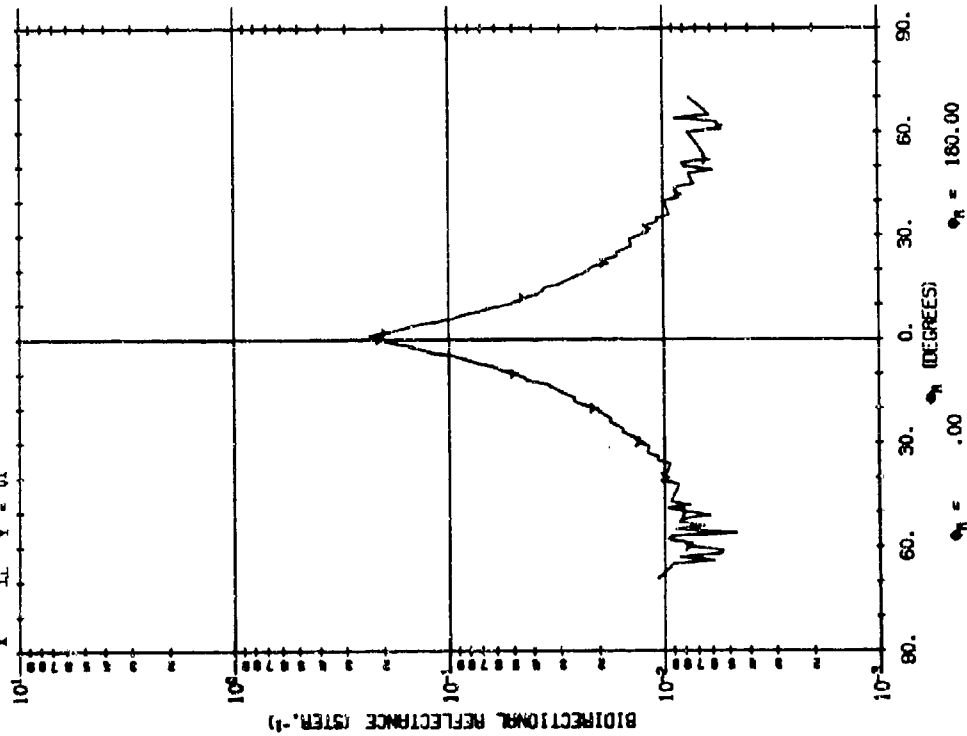
A01925 101
 Acrylic Plexiglass
 $\phi_1 = 0.0$
 $\phi_2 = 180.0$
 $\lambda = 10.6$
 Y = 0V



R01927 101

Brown Corrugated Cardboard

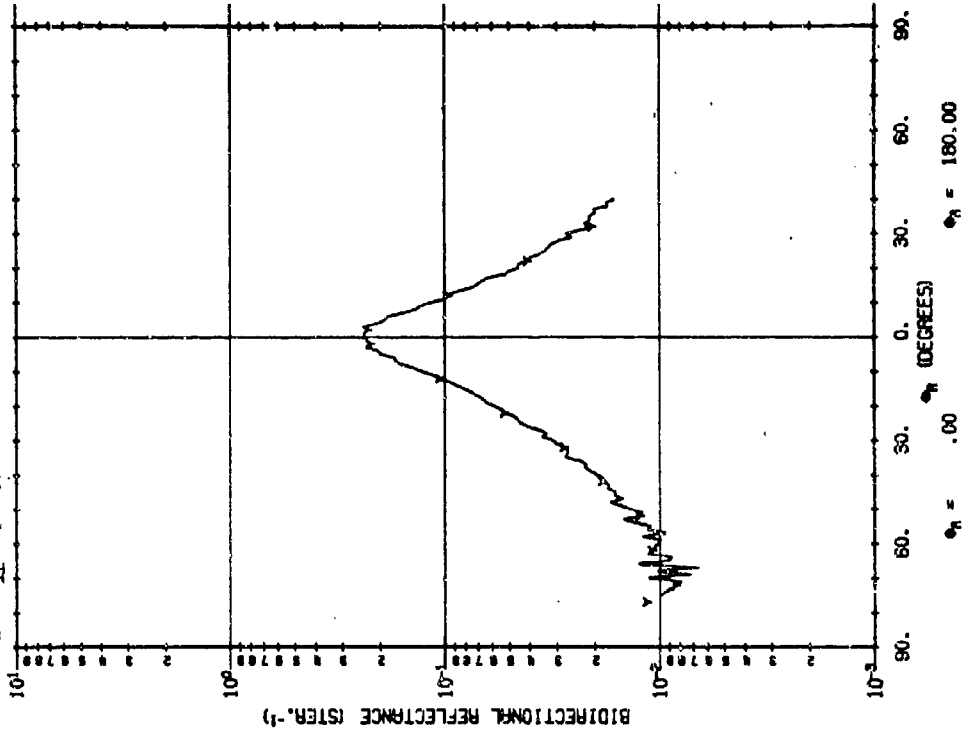
0 | | $\theta_i = 2.0$
+ | | $\theta_r = 0$
A | | $\lambda = 10.6$
K | | $\gamma = \text{VT}$



R01927 101

Brown Corrugated Cardboard

0 | | $\theta_i = 0.0$
+ | | $\theta_r = -180.0$
A | | $\lambda = 10.6$
K | | $\gamma = \text{VT}$



DISTRIBUTION LIST

Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL HSP Mr. Gumborg	(1)	Headquarters SAC (INEP) Offutt Air Force Base, Nebraska 68113	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base Ohio 45433 ATTN: AFAL ISA Avionics Central	(1)	Space and Missile Systems Organization Los Angeles Air Force Station, California 90014 ATTN: SYAS	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL HSP Mr. Richard Jemmwine	(1)	Air Force Materials Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFML LAM Mr. J. H. Charlesworth	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL HSP Mr. Bruno K. Wernicke	(1)	Air Force Materials Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFML LPT Mr. R. M. Van Vleet	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL AAM Capt. Fred Howard	(1)	Headquarters, ESD (NW) Shop-1a L. G. Hanscom Field Bedford, Massachusetts 01730	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL HSE Mr. W. C. Caulfield	(1)	The RAND Corporation 1700 Main Street Santa Monica, California 90406 ATTN: Library - D	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL NVN - Lt. Lester McEwan	(1)	Air Force Cambridge Research Laboratories L. G. Hanscom Field Bedford, Massachusetts 01730 ATTN: AFRL LWH Dr. John F. Cronin	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL NVT Mr. Robert L. Mawdsley	(1)	Air Force Cambridge Research Laboratories L. G. Hanscom Field Bedford, Massachusetts 01730 ATTN: OPA Dr. Robert Fenn	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL NVT (LAS) Mr. Donald Stevenson	(1)	Air Force Cambridge Research Laboratories L. G. Hanscom Field Bedford, Massachusetts 01730 ATTN: AFRL PHL Dr. Salisbury	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL HSE Mr. L. W. Crouch	(1)	Air Force Cambridge Research Laboratories L. G. Hanscom Field Bedford, Massachusetts 01730 ATTN: LZ/Mr. C. J. Stetten	(1)
Aeronautical Systems Division Wright-Patterson Air Force Base, Ohio 45433 ATTN: ASD ENVWA-40 Mr. H. L. Williams	(1)	Headquarters, USAF Washington, D.C. 20330 ATTN: RDVJ	(1)
Aeronautical Systems Division Wright-Patterson Air Force Base, Ohio 45433 ATTN: ASD ENRS Mr. Lee W. Cunningham	(1)	Headquarters, USAF Washington, D.C., 20330 ATTN: SAMID	(1)
Aeronautical Systems Division Wright-Patterson Air Force Base, Ohio 45433 ATTN: ASD INH	(1)	AFSC Liaison Office Langley Research Center (NASA) Langley Air Force Base, Virginia 23365	(1)
Rome Air Development Center Griffins Air Force Base, New York 13442 ATTN: INAP Mr. Ragazzo	(1)	Technical Library Building 305 Aberdeen Proving Ground, Maryland 21005 ATTN: LWL Mr. H. Forst	(1)
Rome Air Development Center Griffins Air Force Base, New York 13442 ATTN: RADC INR Data Base	(1)	Director, Human Engineering Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: Mr. John D. Weisz	(1)
Air Force Armament Laboratory Eglin Air Force Base, Florida 32542 ATTN: ATTY Mr. Long	(1)	Commanding Officer Coating and Chemical Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: RD-CS/Dr. James McLuskey	(1)
6585 Test Group Holloman Air Force Base, New Mexico 88330 ATTN: GD. Dr. Martin Jachtke	(1)	Commanding Officer U.S. Army Mobility Equipment Research and Development Center Fort Belvoir, Virginia 22060 ATTN: Technical Document Center, SMEFB-MW Mr. D. Gee	(1)
Air Force Weapons Laboratory Kirtland Air Force Base, New Mexico 87117 ATTN: WLIL	(1)	Commanding Officer U.S. Army Mobility Equipment Research and Development Center Fort Belvoir, Virginia 22060 ATTN: SMEFB-MW (Countersurveillance Branch)	(1)
Air University Library Maxwell Air Force Base, Alabama 36112	(1)		
ADIC (TRGPA) Eglin Air Force Base, Florida 32542 ATTN: Mr. Franklin Gay	(1)		
USAF/AWC (AYN) Eglin Air Force Base, Florida 32542 ATTN: Maj Robert L. Ingram	(1)		

<p>Commanding Officer U.S. Army Frankford Arsenal Philadelphia, Pennsylvania 19137 ATTN: SMUFA-N5160 Mr. Jacob H. Kabanoff</p>	(U)	<p>Commander, U.S. Naval Weapons Center China Lake, California 93555 ATTN: Code 408 Mr. Lawrence Nichols</p>	
<p>U.S. Army Behavior and System Research Laboratory 1300 Wilson Boulevard The Rosslyn Commonwealth Building Arlington, Virginia 22209 ATTN: CRDMRC BESRL D</p>	(U)	<p>Commander, U.S. Naval Weapons Center China Lake, California 93555 ATTN: Code 4096 Mr. E. E. Benton</p>	
<p>Commanding Officer U.S. Army Topographical Command 6400 Brooks Lane Washington, D.C. 20315 ATTN: PHRD (85000), Dr. J. S. Baker</p>	(U)	<p>Commander, U.S. Naval Weapons Center China Lake, California 93555 ATTN: Code 3633 Mr. Paul C. Driver</p>	
<p>Commanding General U.S. Army Missile Command Advanced Sensors Laboratory Redstone Arsenal, Alabama 35809 ATTN: AMSMI-REB Mr. L. W. Root</p>	(U)	<p>Commander, U.S. Naval Weapons Center China Lake, California 93555 ATTN: Code 1056 Mr. Fred E. Nicodemus</p>	
<p>Commanding General U.S. Army Missile Command Advanced Sensors Laboratory Redstone Arsenal, Alabama 35809 ATTN: Physical Sciences Directorate Dr. Herbert Holl</p>	(U)	<p>Commander, U.S. Naval Missile Center Point Muen, California 93042 ATTN: Code 5363 Mr. James Karney</p>	(U)
<p>Commanding Officer U.S. Army Natick Laboratories Natick, Massachusetts 01760 ATTN: AMXRE-CTR Mr. Frank Bizzo</p>	(U)	<p>Geography Programs Office of Naval Research Arlington, Virginia 22217 ATTN: Code 414</p>	(U)
<p>Director U.S. Army Engineer Waterways Experiment Station Vicksburg, Mississippi 39180 ATTN: WESFT</p>	(U)	<p>Commanding Officer, U.S. Naval Avionics Facility 21st Street and Arlington Indianapolis, Indiana 46218 ATTN: 021 Mr. P. Prink</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR-BSP Dr. D. Reysl</p>	(U)	<p>Commanding Officer, U.S. Naval Avionics Facility 21st Street and Arlington Indianapolis, Indiana 46218 ATTN: Division 811 Mr. W. Wuster</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR Mr. A. Downs</p>	(U)	<p>U.S. Department of Agriculture Agriculture Research Service Soil and Water Conservation Research Division Rio Grande Soil and Water Research Center P.O. Box 287 Weslaco, Texas 78596 ATTN: Dr. William Allen</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR-BSP Mr. D. Meune</p>	(U)	<p>NASA Scientific and Technical Information Facility P.O. Box 33 College Park, Maryland 20740 ATTN: Acquisitions and Input Branch</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR-BSP Mr. James Rupp</p>	(U)	<p>Spectrophotometry Group Radiation Thermometry Section Heat Division, JBS National Bureau of Standards Washington, D.C. 20234 ATTN: Mr. Victor R. Weidner</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR-BSP Mr. D. Meune</p>	(U)	<p>Institute of Defense Analyses 400 Army-Navy Drive Arlington, Virginia 22202 ATTN: Mr. Lueta Biberman</p>	(U)
<p>Commanding General U.S. Army Research and Development Center Ballistic Research Laboratory Aberdeen Proving Ground, Maryland 21005 ATTN: AMXIR-BSP Mr. James Rupp</p>	(U)	<p>Defense Documentation Center Cameron Station Alexandria, Virginia 22314 ATTN: TIPC R</p>	(U)
<p>U.S. Army Electronics Command Night Vision Laboratory Fort Belvoir, Virginia 22060 ATTN: AMSEL-NV-VI Dr. M. L. Yatsui</p>	(U)	<p>Vought Missiles and Space Company Michigan LTV Aerospace Corporation P.O. Box 909 Warren, Michigan 48090</p>	(U)
<p>Commanding General U.S. Army Electronics Command Fort Monmouth, New Jersey 07703 ATTN: AMSEL-CT-HBR</p>	(U)	<p>Water Resources Systems Section Water and Land Resources Department Water and Land Resources Department Bethell-Northwest P.O. Box 909 Richland, Washington 99362 ATTN: Mr. Jay R. Kilson</p>	(U)
<p>Commanding General U.S. Army Electronics Command Fort Monmouth, New Jersey 07703 ATTN: AMSEL-CT-L Mr. Blaford</p>	(U)	<p>Texas Instruments Incorporated 13536 North Central Expressway Dallas, Texas 75222 ATTN: Mail Station 381 Mr. Frank E. Kinsman</p>	(U)
<p>Commanding General U.S. Army Electronics Command Fort Monmouth, New Jersey 07703 ATTN: AMSEL-RI-CT-R</p>	(U)	<p>Texas Instruments Incorporated 13536 North Central Expressway Dallas, Texas 75222 ATTN: Mail Station 381 Dr. Dmitri Andrychuk</p>	(U)
<p>Commanding General U.S. Army Tank Automotive Command Warren, Michigan 48090 ATTN: AMSTA-PGD Mr. D. Wilbur</p>	(U)		

Texas Instruments Incorporated 13510 North Central Expressway Dallas, Texas 75222 ATTN: Mail Station 208 Dr. Guy S. Rumbie	(1)	Commander, Naval Weapons Center China Lake, California 93555 ATTN: Code 4082 Mr. H. P. Leet	(1)
Ohio State University Electroscience Laboratory 1320 Kinnear Road Columbus, Ohio 43212 ATTN: Mr. Robert A. Fouty	(1)	Technology Incorporated 7400 Colonel Glen Highway Dayton, Ohio 45431 ATTN: Mr. W. S. Arnold	(1)
Honeywell, Incorporated Radiation Center 2 Forbes Road Lexington, Massachusetts 02173 ATTN: Mail Station 42/Mr. G. J. Borrer	(1)	NASA Lewis Research Center Cleveland, Ohio 44135 ATTN: Mr. Ronald J. Schertler	(1)
Aerospace Corporation P.O. Box 95085 Los Angeles, California 90045 ATTN: Mr. David Pterason	(1)	4950 TZDE Wright-Patterson Air Force Base, Ohio 45433	(1)
Aerospace Corporation P.O. Box 95085 Los Angeles, California 90045 ATTN: Mr. D. A. Lacer	(1)	2750th ABW SSL Wright-Patterson Air Force Base, Ohio 45433	(1)
Thermophysical Properties Research Center Purdue University, Research Park 2595 Yeager Road West Lafayette, Indiana 47906	(1)	Electro-Optical Systems Xerox Corporation 300 N. Hampstead Street Pasadena, California 91107 ATTN: Mr. Lee W. Carrier	(1)
RACIC Battelle Memorial Institute 505 King Avenue Columbus, Ohio 43201	(1)	Hughes Research Laboratories Division of Hughes Aircraft Company 3011 Malibu Canyon Road Malibu, California 90265 ATTN: Mr. F. H. Tenney	(1)
The University of Texas at Austin Applied Research Laboratories Aerospace Technology Division P.O. Box 8029 10000 FM Road 1325 Austin, Texas 78712	(1)	Willow Run Laboratories, Building 2041 Institute of Science and Technology The University of Michigan P.O. Box 618 Ann Arbor, Michigan 48107 ATTN: Mr. Howard Courtney	(1)
Air Force Avionics Laboratory Wright-Patterson Air Force Base, Ohio 45433 ATTN: AFAL TEL Mr. Richard Piradon	(1)	Willow Run Laboratories, Building 2041 Institute of Science and Technology The University of Michigan P.O. Box 618 Ann Arbor, Michigan 48107 ATTN: Mr. Max E. Blair	(1)
GTE Sylvania, Incorporated Sylvania Electronic System - West P.O. Box 205 Mountain View, California 94024 ATTN: Mr. Steven Ross	(1)	Willow Run Laboratories, Building 2041 Institute of Science and Technology The University of Michigan P.O. Box 618 Ann Arbor, Michigan 48107 ATTN: Mr. Richard Legault	(1)
General Dynamics Electro-Dynamics Division P.O. Box 127 3090 Pacific Highway San Diego, California 92112 ATTN: Dr. J. V. Raventis	(1)	Willow Run Laboratories, Building 2041 Institute of Science and Technology The University of Michigan P.O. Box 618 Ann Arbor, Michigan 48107 ATTN: Infrared Information and Analysis Center	(1)
Commander, Naval Ordnance Laboratory White Oak Silver Spring, Maryland 20910 ATTN: Code 213/Mr. W. W. Talbert	(1)		