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AFFDL ltr dtd 25 Oct 1972

AFFDL-TR-69-124
PART I
VOL. II

WING ROLL CONTROL DEVICES FOR TRANSONIC HIGH LIFT CONDITIONS

PART I — FIXED WING CONFIGURATION

VOL. II — APPENDICES

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GENERAL DYNAMICS, FORT WORTH DIVISION

TECHNICAL REPORT AFFDL-TR-69-124, PART I, VOL. II

JANUARY 1970

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AIR FORCE FLIGHT DYNAMICS LABORATORY
AIR FORCE SYSTEMS COMMAND
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

NOTICE

300 - September 1970 - CO305 - 5-71-80

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LIST OF SYMBOLS AND ABBREVIATIONS

Symbols

b	wing span
c	chord
$\bar{c}$	wing mean geometric chord
C_D	drag coefficient, Drag/q S_{ref}
C_{Dmin}	minimum value of drag coefficient at particular Mach number
C_l	rolling moment coefficient, rolling moment/$qS_{ref}b$
C_{l_p}	damping due to roll rate coefficient, $\frac{\partial C_l}{\partial \frac{\dot{\phi} b}{2V}}$
$C_{l_{\delta_a}}$	aileron effectiveness coefficient, $\frac{\partial C_l}{\partial \delta_a}$
C_L	lift coefficient, lift/qS_{ref}
C_{L_α}	lift curve slope, $\frac{\partial C_L}{\partial \alpha}$
C_{L_C}	lift coefficient at which drag polar becomes non-parabolic, see Figure 39,pg 105
$C_{L_{C_{Dmin}}}$	lift coefficient for minimum drag coefficient
C_m	pitching moment coefficient, pitching moment/$qS_{ref}\bar{c}$
C_n	yawing moment coefficient, yawing moment/$qS_{ref}b$
g	acceleration due to gravity
GW	gross weight
I_x	moment of inertia about longitudinal stability axis

LIST OF SYMBOLS AND ABBREVIATIONS (CONT'D)

I_z	moment of inertia about z stability axis
I_{xz}	cross product of inertia
K	drag due to lift factor defined by equation (1) pg 103
L	fuselage length
L_{δ_a}	roll acceleration per unit lateral control input
L/D	lift to drag ratio
M	Mach number
P_{ss}	steady state roll rate
q	dynamic pressure
Rn	Reynolds number
R_I	inertia ratio, Ix/Iz
R_β	stability ratio, directional stability/effective dihedral, C_{n_β}/C_{l_β}
R_δ	control moment ratio, $\left[\Delta C_n/\Delta C_l\right]$ roll control or $C_{n_{\delta_a}}/C_{l_{\delta_a}}$
S_f	planform area of flap segment
S_{ref}	reference area, area of wing planform excluding the highly swept inboard glove
S_w	reference wing area
s	Laplace operator
t	local thickness of wing section

t	time
V	velocity
$\bar{y}$	lateral distance to centroid of flap segment planform
α	wing angle of attack
α_{LO}	angle of attack for zero lift
β	aircraft point angle, see Figure 94, page 213
δ	deflection, positive leading edge down (leading edge devices), or trailing edge down (trailing edge devices)
δ_a	average aileron deflection, $1/2\ (\delta_{right} - \delta_{left})$
ζ_ϕ	damping ratio of numerator quadratic in ϕ/δ_a transfer function
ζ_d	damping ratio of dutch roll mode
ϕ	roll angle
Λ	sweep angle
T_R	time constant of the rolling convergence mode
T_s	time constant of the spiral mode
T_1	time to obtain maximum control input, see Appendix I
ω_ϕ	natural frequency of numerator quadratic in ϕ/δ_a transfer function
ω_d	natural frequency of the dutch roll mode

LIST OF SYMBOLS AND ABBREVIATIONS (CONT'D)

Subscripts

aero	aerodynamic contribution
eff	effective value of coefficient including approximation of control system effects
FCS gain	control system feedback gain
o	initial condition
pa	principal axis value

Abbreviations

AEDC	Arnold Engineering Development Center
CAL	Cornell Aeronautical Laboratory
FDCC	Control Criteria Branch of USAF Flight Dynamics Laboratory
F.S.	Fuselage Station
H.T.	Horizontal Tail
L.E.	Leading Edge
LEDE	Leading Edge Device Effectiveness
L/R	Left/Right Surface Deflection in Degrees
M.S.	Model Scale
NACA	National Advisory Committee for Aeronautics
NASA	National Aeronautics and Space Administration
PWT	Propulsion Wind Tunnel
RMS	root-mean-square
VG	Vortex Generators

APPENDIX I ROLL RATE EFFECTS ON AIR-TO-AIR COMBAT

A brief study of the effect of roll response on battle dominance during air-to-air combat was accomplished using a digital air combat program, ATAC. The objective of this effort was to select a roll control sizing criteria compatible with the transonic maneuvering requirements of advanced fighter aircraft. An additional objective was to evaluate the sensitivity of battle dominance in air-to-air combat to roll capability.

1. SIMULATION

The specific features of General Dynamics, Fort Worth Division digital air combat program ATAC utilized in this study are reviewed in this section. A more general discussion of ATAC may be found in Reference 24. The air combat situation is simulated in three spatial dimensions with identical situations-dependent guidance laws for both the attacker and target aircraft. For the case utilized, the guidance laws minimize the pointing angle (defined in Figure 94) by selecting the best values of angle of attack and roll angle attainable within the small time increment of integration. This is accomplished by a two-dimensional Fibonaccian search.

The parameters directly influencing basic aircraft performance i.e. drag polar, thrust, fuel flow, weight, the various structural and aerodynamic limits are simulated in detail. Roll response is specified by a maximum roll rate limit and sideslip is considered to be zero for all calculations.

Experience with this program has demonstrated that the simple simulation of lateral-directional response yields valid data for tactical effects of roll capability when the metric chosen is time to change bank angle. The following observations illustrate the underlying reasons that the simulation is adequate. For the major portion of an air combat encounter, the demands on roll are quite small. During this time the objective is to maintain the lift vector (turn force) in the plane defined by the aircraft velocity vector

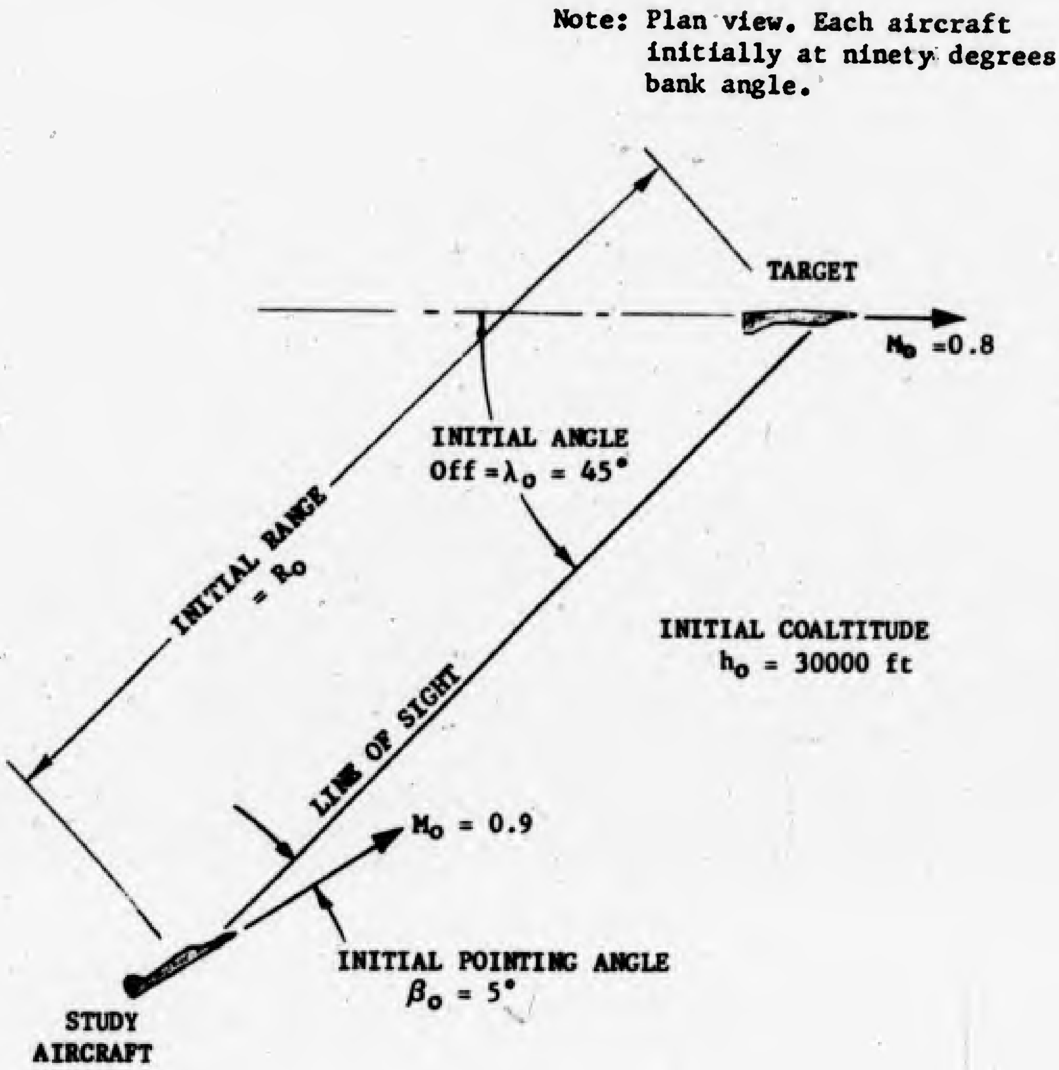


Figure 94 BATTLE CONDITIONS

and the range vector. However when a sudden large change in the direction of the relative range vector occurs a major reorientation of the attacker's lift vector through change in bank angle is dictated. The foremost example of such a situation is the classical scissors maneuver. In such cases a relatively small time increment when the lift vector is not properly orientated can result in a major degradation in battle dominance.

A plan view of the initial conditions is given in Figure 94 . The battle was begun with the aircraft at a co-altitude of 30,000 feet with each rolled ninety degrees toward the other. The study aircraft had an initial angle off the target, β_o , of fourty-five degrees and a pointing angle, λ_o , of five degrees. Six values of maximum roll rate for the study aircraft were evaluated at each of four initial ranges, 2,000, 3,000, 4,000, and 6,000 feet. The target aircraft had a fixed roll capability corresponding to the ability to roll through two hundred degrees and stop roll rate in 1.90 seconds.

The two parameters found to be most indicative of the tactical situation are the pointing angle from the study aircraft to the target aircraft and a corresponding AIM score. The AIM score is a numerical rating of the pointing angle with a maximum value of 25 for angles less than 2.5 degrees, 24 angles between 2.5 and 5.0 degrees, etc.

Analysis of simulated engagements must be done at several discrete times in a battle and conclusions drawn from the individual results when viewed as a whole. This is so because although battles have the same general trends, the critical portions occur at different times. Thus instantaneous or even averaged values at any given time for parameters such as pointing angle, and battle score may yield scattered results. It was found useful to average the pointing angle from the start of battle up to specific elapsed times of five, ten, fifteen, and twenty seconds. For the AIM score, integrations with time as the independent variable where accomplished for the same elapsed time increments.

2. RESULTS

It is important to first note that depending upon the initial range, two basic types of battles occured over the long term, as shown in Figure 95. For the shorter initial ranges (2000 and 3000 feet) the target reversed after the initial study aircraft overshoot leading to the classical scissors maneuver. For longer initial ranges (4000 and 6000 feet) with small overshoots, a circular tail chase developed. In both battle types, the study aircraft initially performed a rapid turn reversal by changing bank angle between 190 and 210 degrees. Thus the time to roll through 200 degrees and stop was chosen as the roll performance metric with minor adjustments being made whenever bank angle changes were slightly different from 200 degrees.

As mentioned above, average pointing angle and accumulated AIM score were evaluated for the first five, ten, fifteen and twenty seconds of battle. Results for the first fifteen sesonds were found to be the most representative and are shown in Figures 96 and 97. Note that the accumulated AIM score indicates the improvement in battle dominance with reduced time to roll more clearly that the average pointing angle. It was found that the somewhat irregular trends in accumulated AIM score could be removed by averaging the values accumulated over the four time intervals, five, ten, fifteen, and twenty seconds. This averaging results in a heavier weighting for the first portion of the battle when the initial reversal occurs. Such averaged AIM scores are given in Figure 98. For the longer ranges, 4,000 and 6,000 feet (resulting in a tail chase maneuver) reduction in time to roll below a specific value does not yield any tactical advantage. For the case of scissors maneuvers (developing when the initial range is 2,000 or 3,000 feet) the highest possible roll capability comparable with pilot technique and general flying qualities appears to be desirable.

One other aspect of the combat simulation is of interest in selecting a roll performance criteria. That is the time to reacquire the target after initiating the first rapid reversal. Reacquisitions was defined as reduction of the pointing angle to less than fifteen degrees. This data, given in Figure 99, demonstrates that the time to roll 200 degrees and stop should be 1.9 seconds or less. For the case of 2,000 feet initial range it was not found possible to establish a small steady state pointing angle after the initial roll reversal for any roll capability investigated.

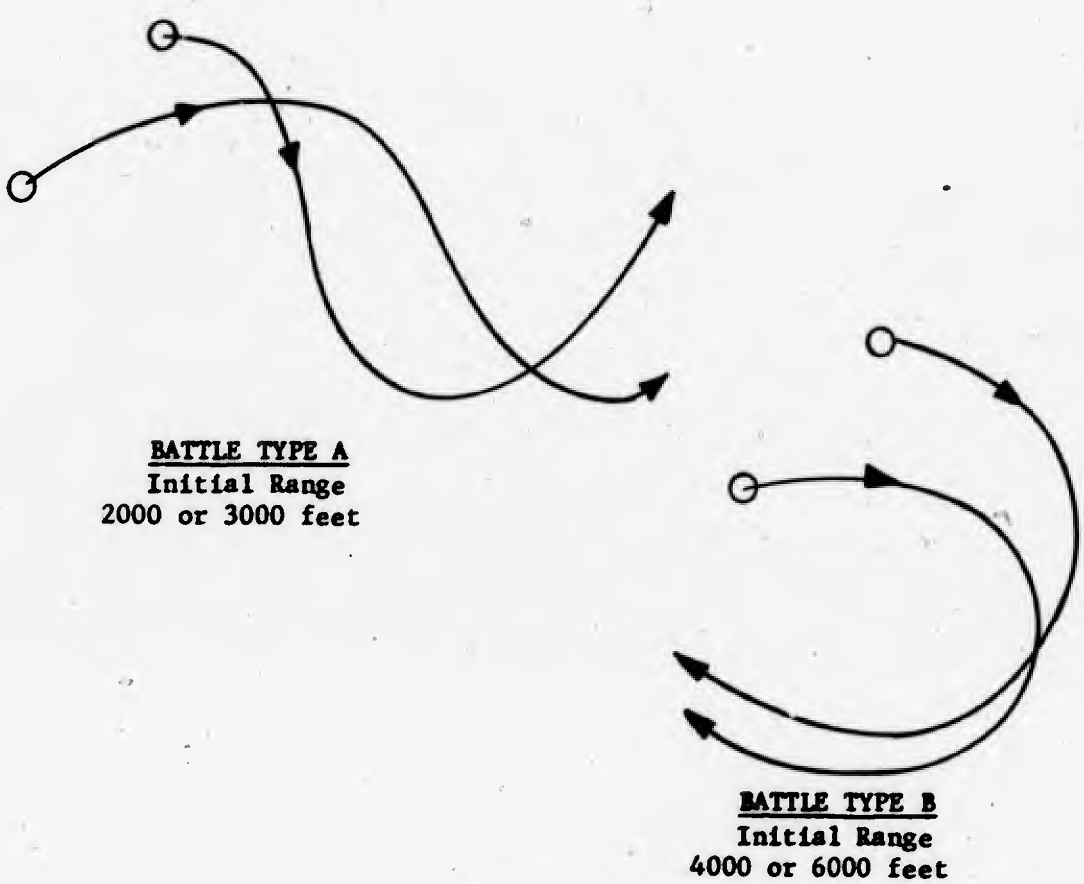


Figure 95 PLAN VIEWS OF BATTLE TYPES

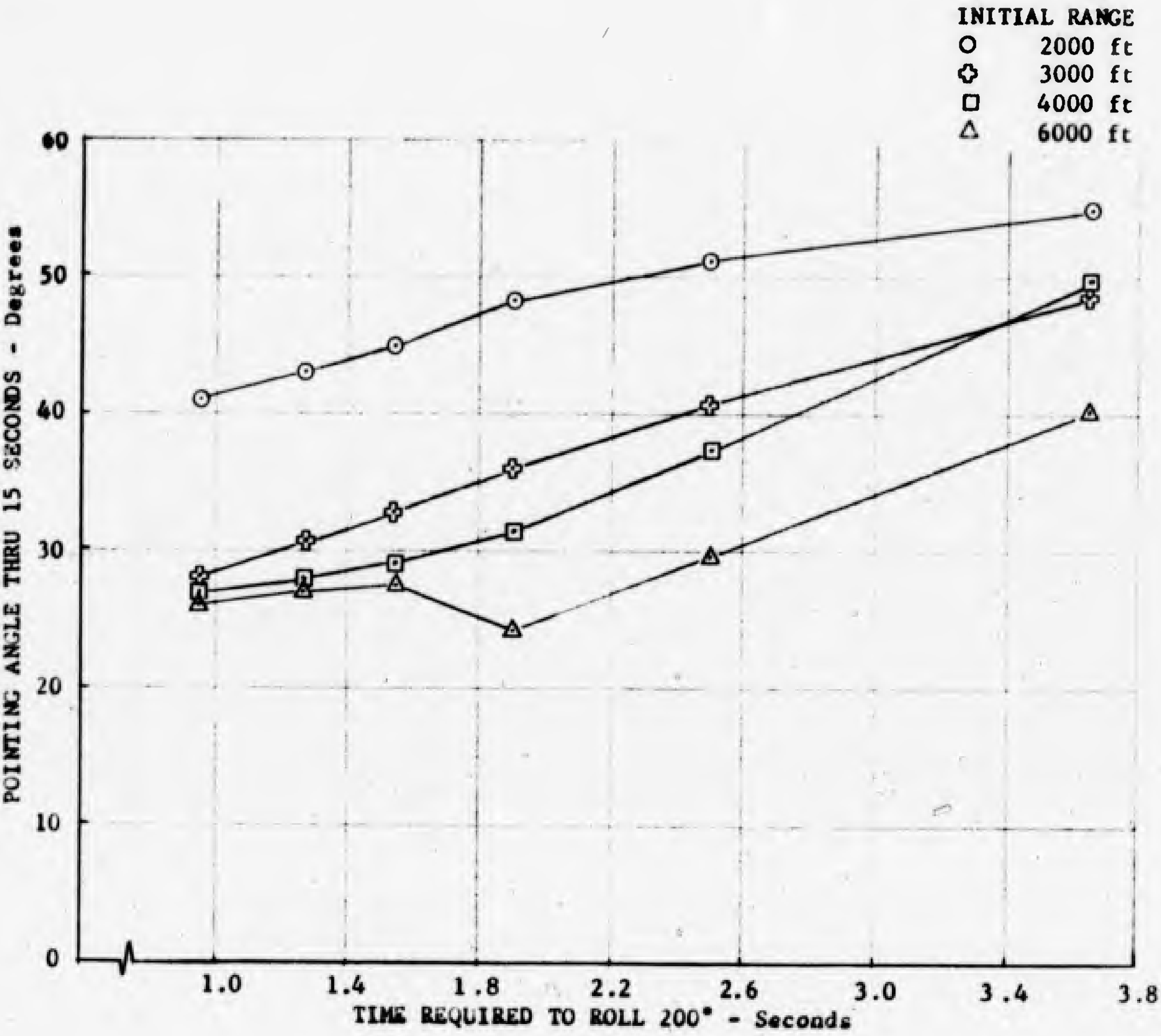


Figure 96 AVERAGE POINTING ANGLE

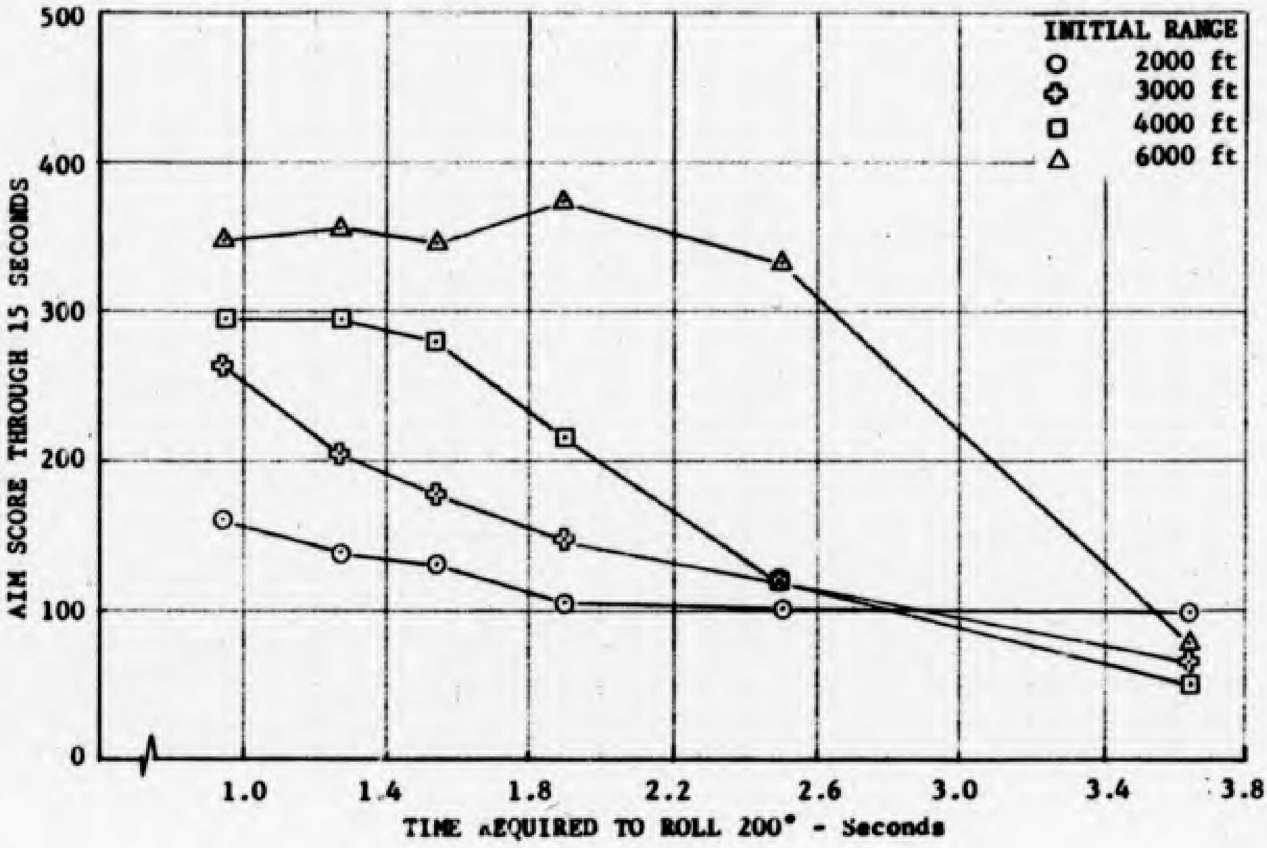


Figure 97 AIM SCORE

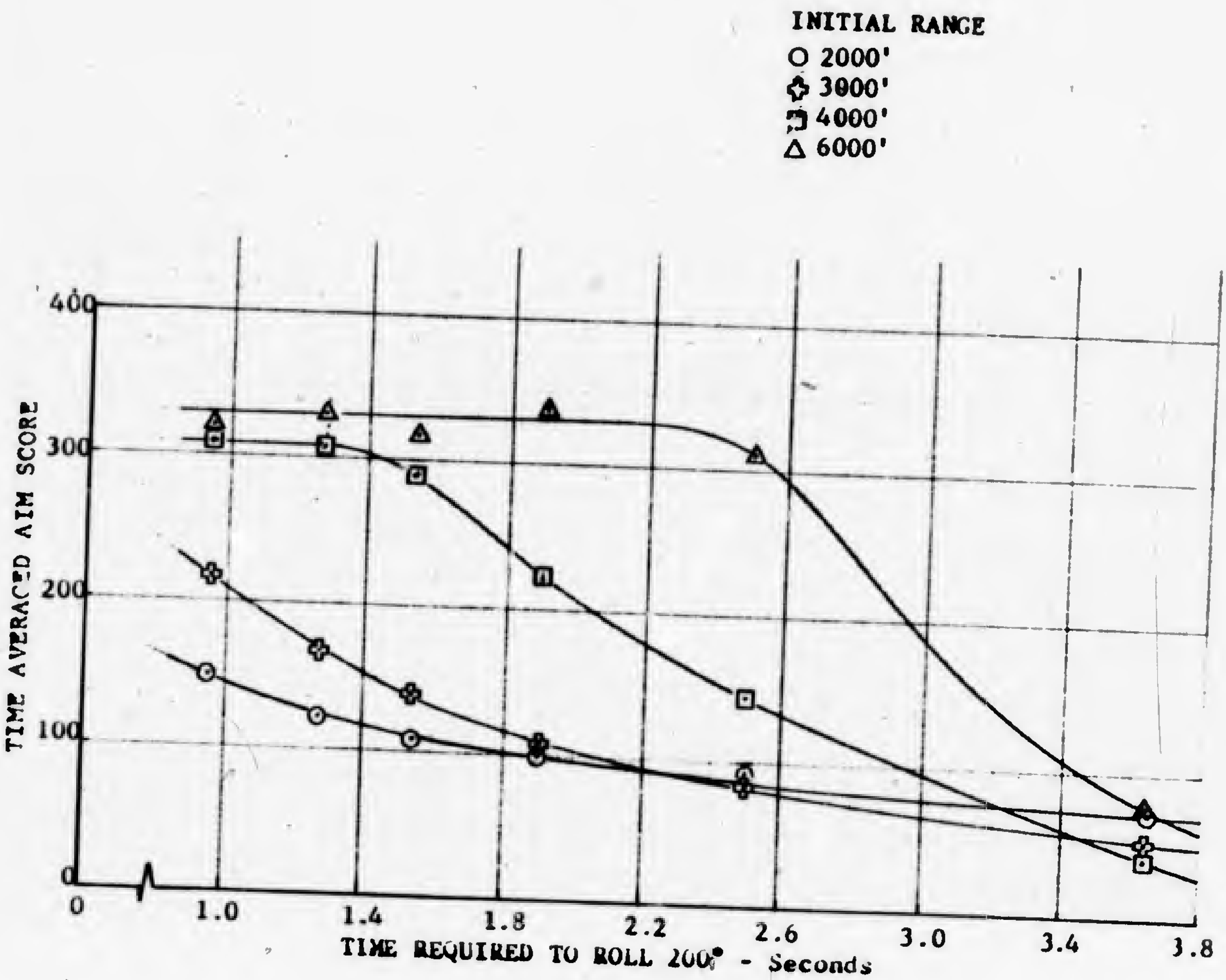


Figure 98 AVERAGED BATTLE SCORE

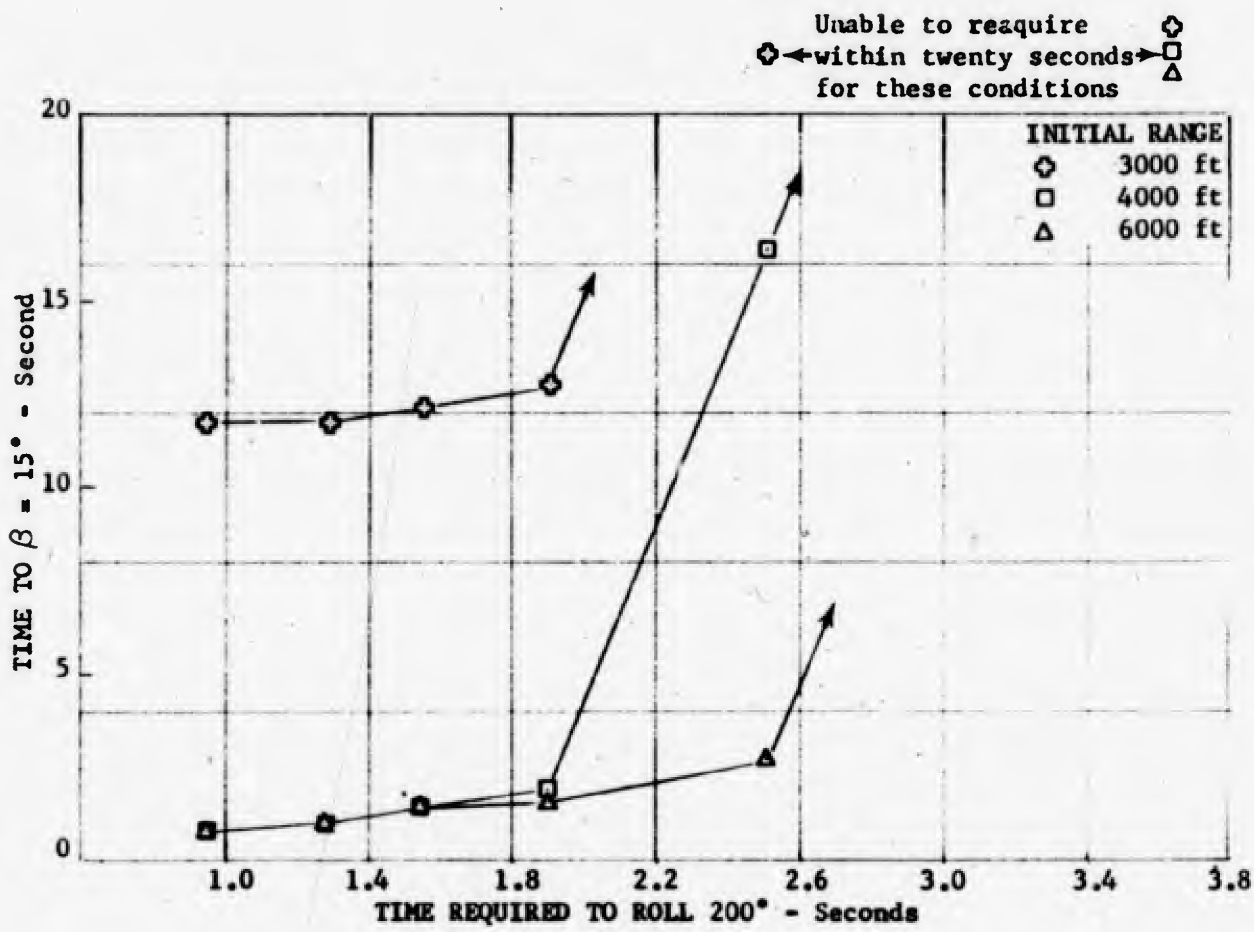


Figure 99 REACQUISITION TIME ANALYSIS

A nominal air-to-air performance criteria of 1.8 seconds for a 200 degree bank change and stop maneuver was selected based on the consideration of AIM score and reacquisition discussed above. This criteria is compared with handling qualities data and military specifications in Appendix II.

APPENDIX II ROLL CONTROL POWER CRITERIA

Selection of a roll control criteria may be divided into three tasks. First. convenient relationships between control power, steady state roll rate, and time to accomplish a specified bank angle change are required to interrelate the several measures of roll performance. Second, the capabilities and preferences of the human pilot for execution of rolling maneuvers are necessary to match the performance characteristics of the controller to those of the vehicle. Third, the tactical advantages of various levels of roll performance must be related to the vehicle capabilities and pilot perferences.

1. GENERAL RESPONSE ANALYSIS

The simple single degree of freedom rolling moment equation was used for roll performance analysis to focus attention upon the rolling convergence mode and allow concise presentation of results. However, the information is presented in terms of two key response parameters, the steady state roll rate and the roll time constant, so the effects of additional degrees of freedom and the flight control system may be approximated. The general development proceeds as follows.

First consider the rolling moment equation:

$$I_x \ddot{\phi} + qSbC_{l_p} \frac{\dot{\phi} b}{2V} + qSbC_{l_{\delta_a}} \delta_a = 0 \qquad (2)$$

The Steady State response is:

$$P_{ss} = \lim_{t \to \infty} \dot{\phi} = -\frac{2V}{b} \frac{C_{l_{\delta_a}}}{C_{l_p}} \delta_{a_{max}}$$

and solution of the homogeneous case:

$$I_x \ddot{\phi} + \frac{qSb^2}{2V} C_{l_p} \dot{\phi} = 0 \qquad (3)$$

gives

$$\dot{\phi} = C_1 + C_2 e^{-t/\tau_R}$$

where the roll time constant is given by

$$\tau_R = \frac{2V I_x}{qSb^2 C_{l_p}} \tag{4}$$

The rolling moment equation may now be expressed in terms of more general parameters, steady state roll rate and roll time constant.

$$\ddot{\phi} + \frac{\dot{\phi}}{\tau_R} = \frac{P_{ss}}{\tau_R} \frac{\delta_a}{\delta_{a_{max}}} \tag{5}$$

Before proceeding to the solution of this equation for the desired control inputs, several simple methods for approximating the effects of other degrees of freedom and flight control system augmentation will be mentioned briefly. Effects of yaw response on roll performance may be approximated by use of the system of primed coefficients as set forth in reference 26 where:

$$C'_{l_i} = \frac{C_{l_i} + C_{n_i} \frac{I_{xz}}{I_x}}{1 - \frac{I_{xz}^2}{I_x I_z}} \tag{6}$$

together with a steady state roll rate as derived below from the basic roll angle to lateral control transfer function.

In general

$$\frac{\varphi}{\delta_a} = - \frac{L'_{\delta_a} (s^2 + 2 \zeta_\varphi \omega_\varphi + \omega_\varphi^2)}{(s + \frac{1}{T_s})(s + \frac{1}{T_R})(s^2 + 2 \zeta_d \omega_d + \omega_d^2)} \tag{7}$$

where

$$L'_{\delta_a} = \frac{qSb}{I_x} C'_{l_{\delta_a}} \tag{8}$$

Now neglect the spiral mode $\frac{1}{T_s} \ll s$

employ a step aileron input $\delta_a(s) = \frac{\delta_{a_{max}}}{s}$

and use the final value theorem $P_{ss} = \lim_{s \to 0} s P(s)$

then $$P_{ss} = \lim_{s \to 0} s[s\varphi] = -\tau_R L'_{\delta_a} \delta_{a_{max}} \left(\frac{\omega_\varphi}{\omega_d}\right)^2 \quad (9)$$

Similarity at time zero:

$$\ddot{\varphi}(0) = \lim_{s \to \infty} s[s^2\varphi] = -L'_{\delta_a} \delta_{a_{max}}$$

Thus L'_{δ_a} is the initial roll acceleration per unit step control input. Note that from the single degree of freedom development, equations (3) and (4) yield

$$P_{ss} = -\tau_R L_{\delta_a} \delta_{a_{max}} \quad \text{where} \quad L_{\delta_a} = \frac{\bar{q}Sb}{I_x} C_{l_{\delta_a}}$$

while the general transfer function yields

$$P_{ss} = -\tau_R L'_{\delta_a} \delta_{a_{max}} \left(\frac{\omega_\varphi}{\omega_d}\right)^2 \quad \text{with} \quad L'_{\delta_a} = \frac{\bar{q}Sb}{I_x} C'_{l_{\delta_a}}$$

Hence the effects of additional degrees of freedom on roll response may be accounted for by use of the parameter $(\omega_\varphi/\omega_d)$ together with a primed system of stability and control coefficients.

Two methods may be employed to approximate the flight control system effects on roll performance. In cases where a detailed description of the stability augmentation and the corresponding effects on vehicle dynamics are not available, values of parameters such as P_{ss}, τ_R, and $(\omega_\varphi/\omega_d)$, augmentation ON, may be selected based on design objectives and previous experience with similar systems. These parameters may then be used in the simplified single degree of freedom analysis. In cases where rate and/or acceleration feedback is employed for stability augmentation, effective values may be estimated for key derivatives. As an example, the effects of roll rate feedback may be approximated by:

$$C'_{l_{p_{eff}}} \simeq C'_{l_{p_{aero}}} + C'_{l_{\delta_a}} \frac{\delta_a}{\left(\frac{Pb}{2V}\right)_{FCS\ gain}}$$

The basic rolling moment equation (5) (repeated below) was solved for two control inputs of particular interest using Laplace transform techniques.

$$\ddot{\phi} + \frac{\dot{\phi}}{\tau_R} = \frac{P_{ss}}{\tau_R}\left(\frac{\delta_a}{\delta_{a_{max}}}\right) \qquad (5)$$

The first control input shown below is a ramp to maximum control input, corresponding to a rapid roll through a specific bank angle change with no attempt to zero roll rate at the end of the maneuver.

Current flying qualities requirements on roll performance, MIL-F-8785A(USAF), are stated in terms of the time to accomplish specific bank angle changes using this type control input. For zero initial values of bank angle and roll rate, the response is given in terms of the simple analytical expressions below.

Step Input, $T_1 = 0$

$$\frac{\phi}{\tau_R P_{ss}} = \frac{t}{\tau_R} - 1 + e^{-t/\tau_R} \qquad (10)$$

Ramp to Maximum Command

1) For $t/\tau_R \leq T_1/\tau_R$

$$\frac{\phi}{\tau_R P_{ss}} = \frac{\tau_R}{T_1} - \frac{t}{\tau_R} + \frac{t^2}{2T_1\tau_R} - \frac{\tau_R}{T_1}e^{-t/\tau_R} \qquad (11)$$

2) For $t/\tau_R \geq T_1/\tau_R$

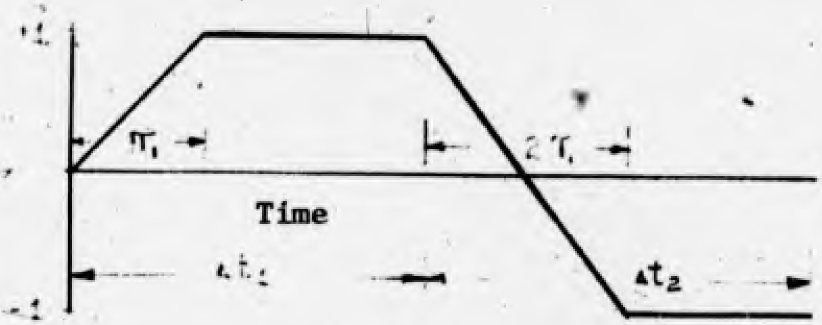
$$\frac{\phi}{\tau_R P_{ss}} = \frac{t}{\tau_R} - 1 - \frac{1}{2}\frac{T_1}{\tau_R} + \frac{\tau_R}{T_1}\left(e^{-\frac{t-T_1}{\tau_R}} - e^{-t/\tau_R}\right) \qquad (12)$$

Note that for $t/\tau_R > 4$

$$\frac{\phi}{\tau_R P_{ss}} \cong \frac{t}{\tau_R} - 1 - \frac{1}{2}\frac{\tau_1}{\tau_R} \qquad \text{(Error less than 1\%)}$$

These results are presented in graphical form on Figure 100 for a wide range of the key parameters.

Response for a second typical control input (indicated schematically below) was obtained to provide rolling performance data for the roll and stop maneuver indicative of air-to-air combat usage.



The conditions used with equation (5) were zero initial bank angle and roll rate and zero final roll rate. The analytical solution by Laplace transforms is rather lengthy. After considerable simplification, the results may be expressed in the form given below.

$$\frac{\Delta\varphi}{\tau_R P_{ss}} = \frac{3}{2}\frac{\tau_1}{\tau_R} + \frac{\Delta t_1 - \Delta t_2}{\tau_R} \qquad (13)$$

$$\frac{\Delta t_2}{\tau_R} = \ln\left\{ \frac{\tau_R}{\tau_1}\left(e^{\frac{\tau_1}{\tau_R}} - 1\right)\left(1 + e^{\frac{\tau_1}{\tau_R}} - e^{-\frac{\Delta t_1}{\tau_R}}\right) \right\} \qquad (14)$$

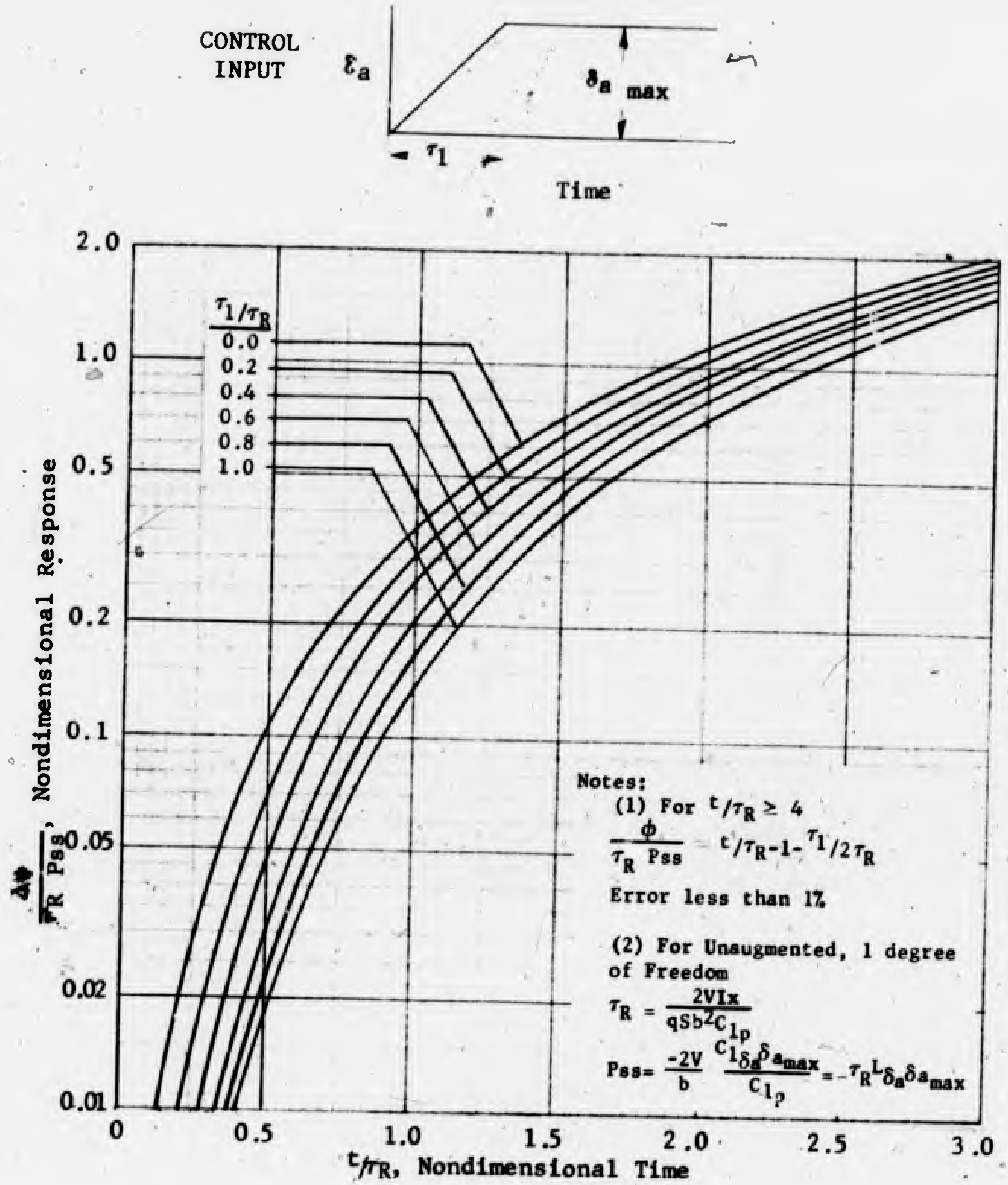


Figure 100 GENERALIZED ROLL PERFORMANCE

Substitution of specific values of $\Delta t_1/\tau_R$ in these expressions yields generalized characteristics for the roll and stop maneuver with τ_1/τ_R as a parameter (noting that the total maneuver time, t_{total}, is the sum of Δt_1 and Δt_2). This information is given in graphical form in Figure 101.

2. HANDLING QUALITIES CONSIDERATIONS

For purposes of roll control surface sizing, it is most convenient to consider handling qualities in terms of the maximum roll acceleration, $L_{\delta_a} \delta_{a_{max}}$. Normal operation boundaries from the work of Creer et al, Reference 27, are given in Figure 102 in terms of the maximum roll acceleration and roll time constant. A desirable region for precision tracking tasks taken from Reference 28 is also indicated in this Figure. Results for the two rolling maneuvers, discussed in subsection 1, are given for a typical control input time, τ_1 of 0.2 seconds and the single degree of freedom approximation, ω_φ/ω_d of 1.0. It is significant to note that the control power for the MIL-F-8785A (USAF) requirement to roll through 90 degrees bank angle in one second is almost identical to that for a 200 degree bank and stop within 1.8 seconds (selected from ATAC simulations of air-to-air combat). The control power requirement for othermaneuvers is also good agreement with the boundary of Creer.

Based upon the considerations reviewed above, the control power criteria for this study was selected to be a maximum roll acceleration, $L_{\delta_a} \delta_a$, of seven radians per second squared. Selection of the corresponding control rolling moment coefficient is given in subsection 3.

A brief study of general lateral coordination effects was accomplished to provide guide lines on acceptable values for the ratio of yawing moment to rolling moment produced by lateral control deflection and to compare the effects of this parameter to the effects resulting from lateral-directional stability and cross product of inertia variations. A convenient metric for studying these effects is the ratio of roll numerator frequency to dutch roll frequency, ω_φ/ω_d (this parameter also gives an indication of the correction to single degree of freedom steady roll rate). Since the corresponding damping factors ζ_φ and ζ_d are normally about equal, when ω_φ/ω_d is near unity the dutch roll roots are essentially cancelled by complex

For Single Degree of Freedom

$$\tau_R = \frac{2VI_x}{qSb^2\, C_{l_p}}$$

$$P_{ss} = -\frac{2V}{b}\,\frac{C_{l\delta_a}\ \delta_{a_{max}}}{C_{l_p}} = -\tau_R\, L_{\delta_a}\delta_{a_{max}}$$

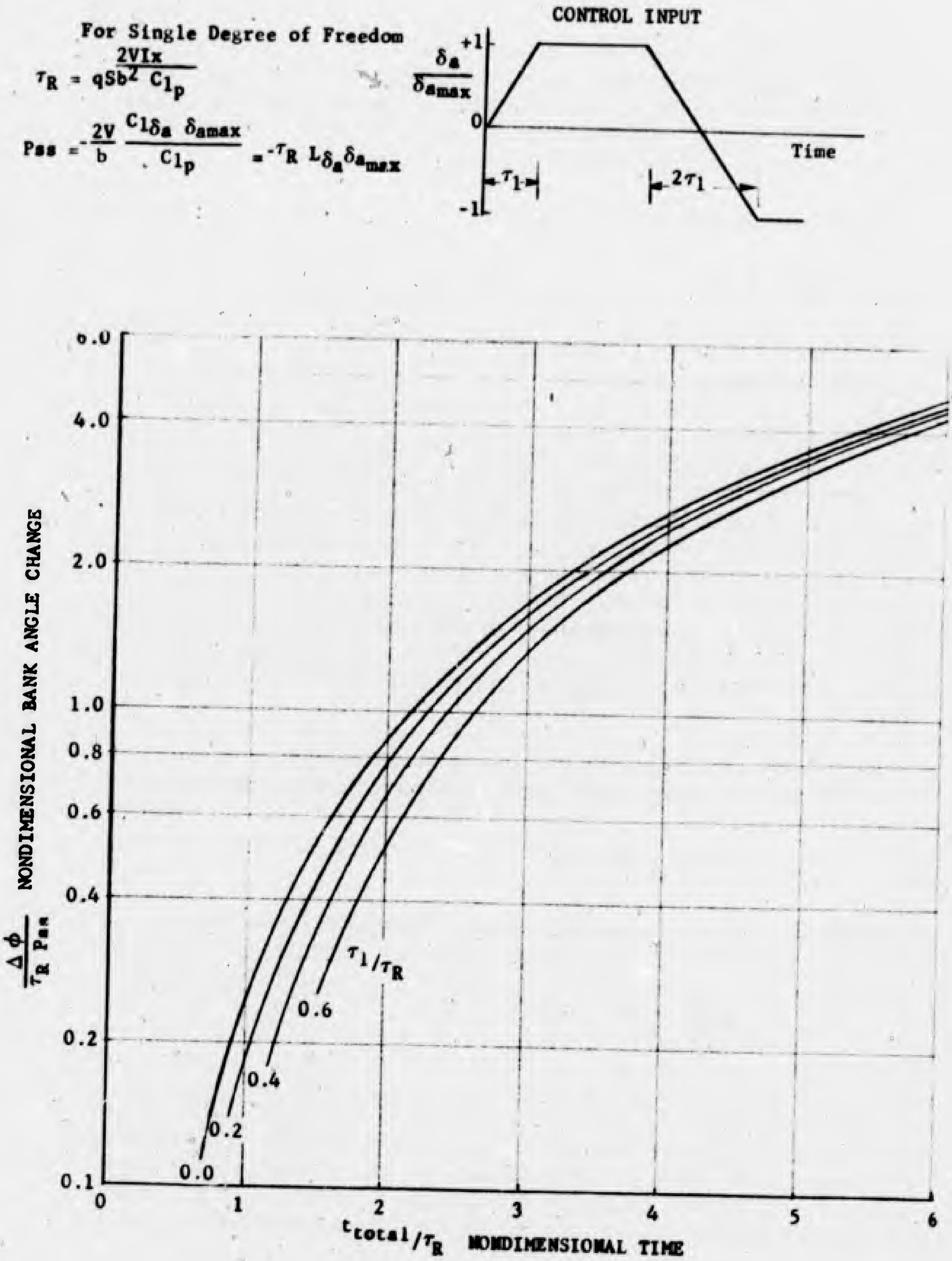


Figure 101 GENERALIZED PERFORMANCE FOR ROLL AND STOP MANEUVER

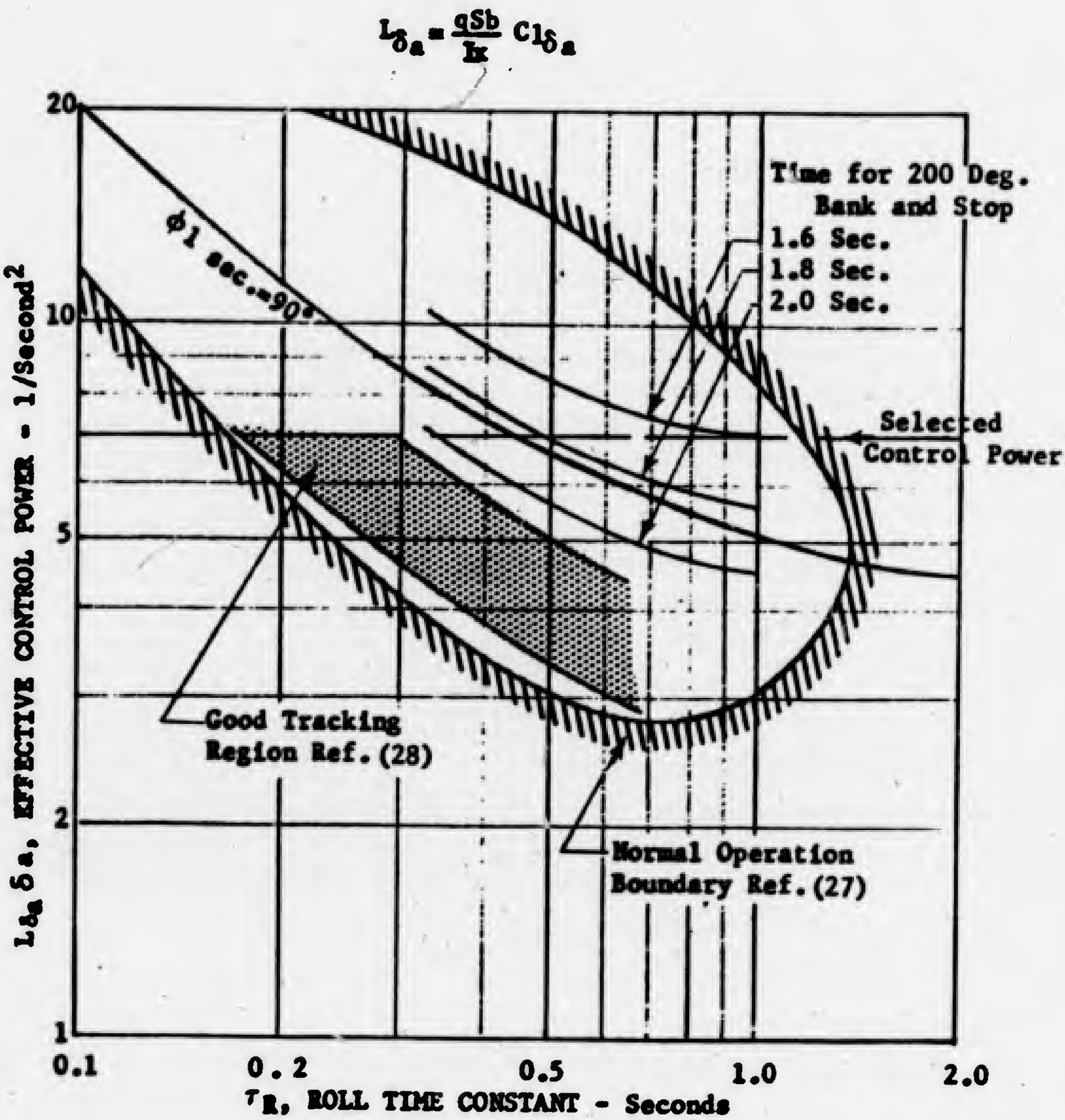


Figure 102 SUMMARY OF ROLL HANDLING QUALITIES CRITERIA

zeroes in the transfer function numerator thus suppressing the objectionable dutch roll mode. For adverse yaw, $\omega_\varphi/\omega_d < 1$, the primary effect is reduction of roll response. As shown previously, neglecting the spiral mode, the steady state response is

$$P_{ss} = -T_R \, L'_{\delta_a} \delta_a \left(\frac{\omega_\varphi}{\omega_d}\right)^2 \qquad (9)$$

It should be noted that so called "favorable" yaw $\omega_\varphi/\omega_d > 1$ does not yield desirable handling qualities. Although the steady state response is improved in such cases, aileron inputs to stop or modify roll response then induce objectionable dutch roll oscillations with notable tendencies for pilot coupling. A typical desired range might be $0.8 < \omega_\varphi/\omega_d < 1.1$ with a value of 1.0 being optimum.

A convenient analytical expression for ω_φ/ω_d is given in Reference 26, repeated below.

$$\left(\frac{\omega_\varphi}{\omega_d}\right)^2 = 1 - \frac{C_{n_{\delta_a}} + \frac{I_{xz}}{I_x} C_{l_{\delta_a}}}{C_{l_{\delta_a}} + \frac{I_{xz}}{I_z} C_{n_{\delta_a}}} \cdot \frac{C_{l_\beta} + \frac{I_{xz}}{I_z} C_{n_\beta}}{C_{n_\beta} + \frac{I_{xz}}{I_x} C_{l_\beta}} \qquad (15)$$

Note that the lateral control characteristics and the stability characteristics have similar effects on ω_φ/ω_d and that in both cases the inertial characteristics modify aerodynamic characteristics about the stability axes. General inertia characteristics were established from the data of Reference 29.

$$R_I = \frac{I_x}{I_z} \simeq \frac{1.44}{(1+L/b)^2}$$ with a typical length/wing span, L/b, for a fighter being 1.5 to yield

$$R_I = 0.23$$

Neglecting differences between stability and principal axes for yawing and rolling inertias

$$I_{xz} \simeq \frac{I_x - I_z}{2} \sin 2\alpha_{pa}$$

where $\alpha_{pa} = \alpha_{wing} + i_{pa}$

Then using the short hand notation

$$R_\delta \equiv \frac{C_{n_{\delta a}}}{C_{\ell_{\delta a}}}$$

$$R_\beta \equiv \frac{C_{n_\beta}}{C_{\ell_\beta}}$$

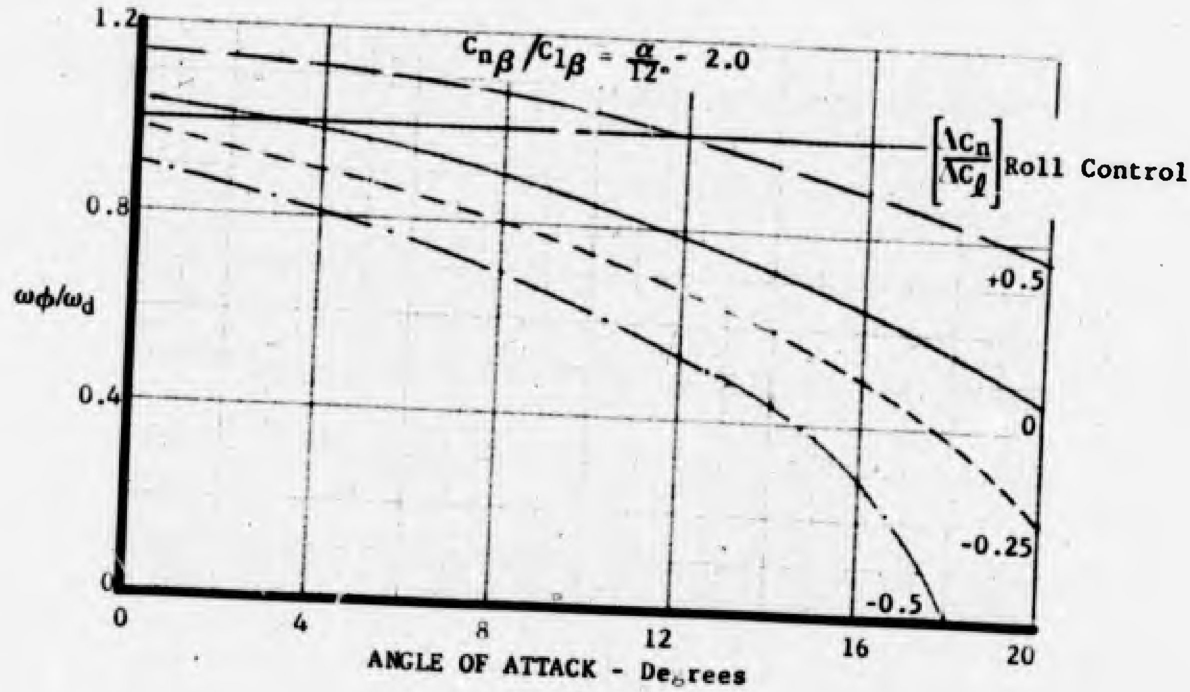
together with the numerical estimate for R_I, we obtain

$$\left(\frac{\omega_\varphi}{\omega_d}\right)^2 = 1 - \frac{R_\delta - 1.67 \sin 2\alpha_{pa}}{1 - 0.385 R_\delta \sin 2\alpha_{pa}} \; \frac{1 - 0.385 R_\beta \sin 2\alpha_{pa}}{R_\beta - 1.67 \sin 2\alpha_{pa}}$$

Trends for R_β with angle of attack were obtained from lateral-directional characteristics of several fighter type aircraft at transonic speeds. At low angles of attack a good rule of thumb is to have directional stability twice the magnitude of the effective dihedral. The configurations surveyed generally substantiated this criteria. Due to increases in effective dihedral and decreases in directional stability, R_β exhibits an approximately linear variation with angle of attack up to the angle for zero stability. An adequate approximation (tending to favor the data with higher static stability) is

$$R_\beta \simeq \frac{\alpha}{12^\circ} - 2.0$$

Variations of ω_φ/ω_d with angle of attack using the above discussed data and a principal axis three degrees below the wing chord plane are shown in Figure 103. Note that the combined adverse trends of cross product of inertia and decreased stability ratio ($-R_\beta$) with angle of attack are such that excessive adverse yaw occurs beyond twelve degrees even in the absence of aileron yaw. The addition of a small amount of adverse aileron yaw further deteriorates the overall control coordination at high angles of attack. A second plot was prepared with R_β constant at -2.0 to show the effects of aileron yaw and cross product of inertia in the presence of desirable stability characteristics. In this case, the inertia effects alone are strong enough to yield excessive adverse yaw for angles of attack greater than sixteen degrees. Also, the effects of aileron yaw are not as severe as those due to representative loss of stability with angle of attack.



$i_{PA} = -3°$

$$\frac{\omega\phi}{\omega d} = \left[1 - \frac{N'\delta_a}{L'\delta_a}\,\frac{L'\beta}{N'\beta}\right]^{1/2}$$

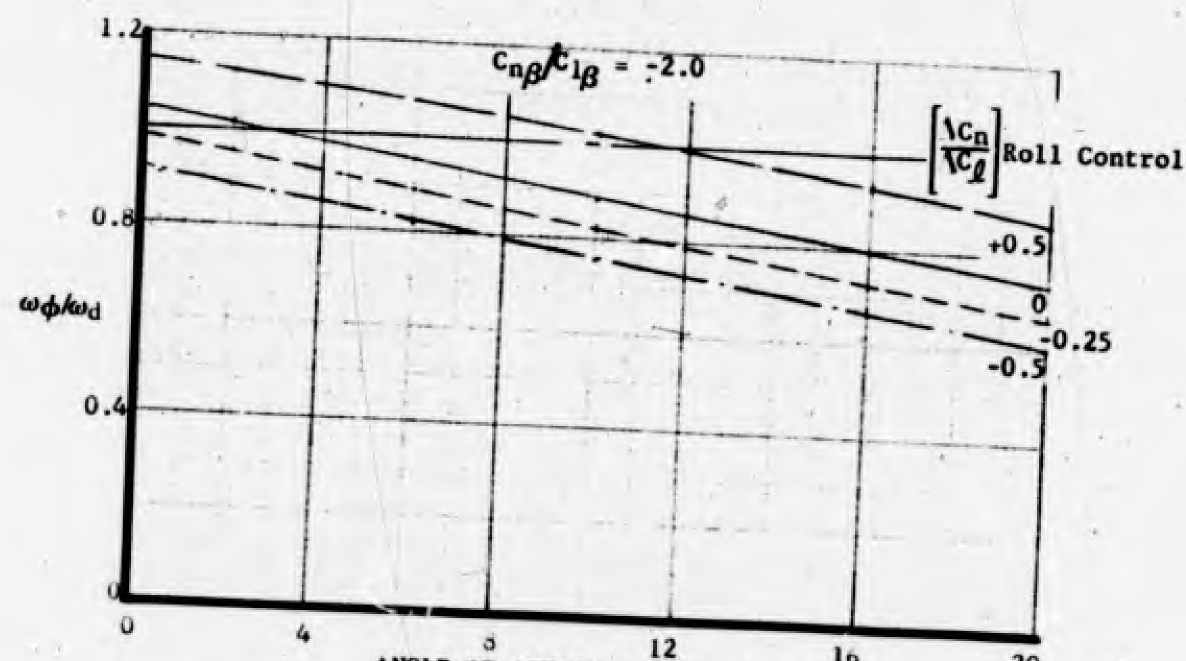


Figure 103 GENERALIZED LATERAL COORDINATION EFFECTS

The specific effects of aileron yaw variations with angle of attack on ω_φ/ω_d and the attendant implications for coordination via the flight control system are more evident when the data of Figure 103 is presented as lines of constant ω_φ/ω_d in the plane of the yawing moment to rolling moment ratio versus angle of attack. The data is given in this form in Figure 104 to show the extent that specific bounds on ω_φ/ω_d limit the allowable combinations of $\Delta C_n/\Delta C_l$ and angle of attack or conversely indicate conditions where specific compensation should be provided by the flight control system.

The results of this brief study must be considered only qualitative due to simplifications used and the neglection of damping effects. However, some general effects are evident for roll coordination at high angles of attack. The inertia effects alone are strong enough to yield poor characteristics even with optimum aerodynamics. For representative configurations, the loss in directional stability and increase in effective dihedral with angle of attack can easily overshadow effects due to aileron yaw. Major compensation through the flight control system would be required to obtain suitable lateral control coordination at high angles of attack. This would be in the form of autmented directional stability and/or effective "favorable" yaw ac high angles of attack. In the case of effective "favorable" yaw, such as by interconnecting the lateral and directional controls, the gain would require scheduling as a function of α to preclude pilot induced oscillation at low angles of attack.

3. ROLLING MOMENT REQUIREMENT

The design value of rolling moment coefficient to be produced by the lateral control was obtained from the roll acceleration requirement in the following manner.

$$L'_{\delta_a}\delta_a = \frac{qSb}{I_x}\,\Delta C_{\ell_{req.}}$$

$$I_x = \left(R_x \frac{b}{2}\right)^2 \frac{GW}{g}$$

giving

$$\Delta C_{\ell_{req.}} = \left(\frac{GW}{qS}\right)\left(\frac{b}{g}\right)\left(\frac{R_x}{2}\right)^2 L'_{\delta_a}\delta_a \qquad (16)$$

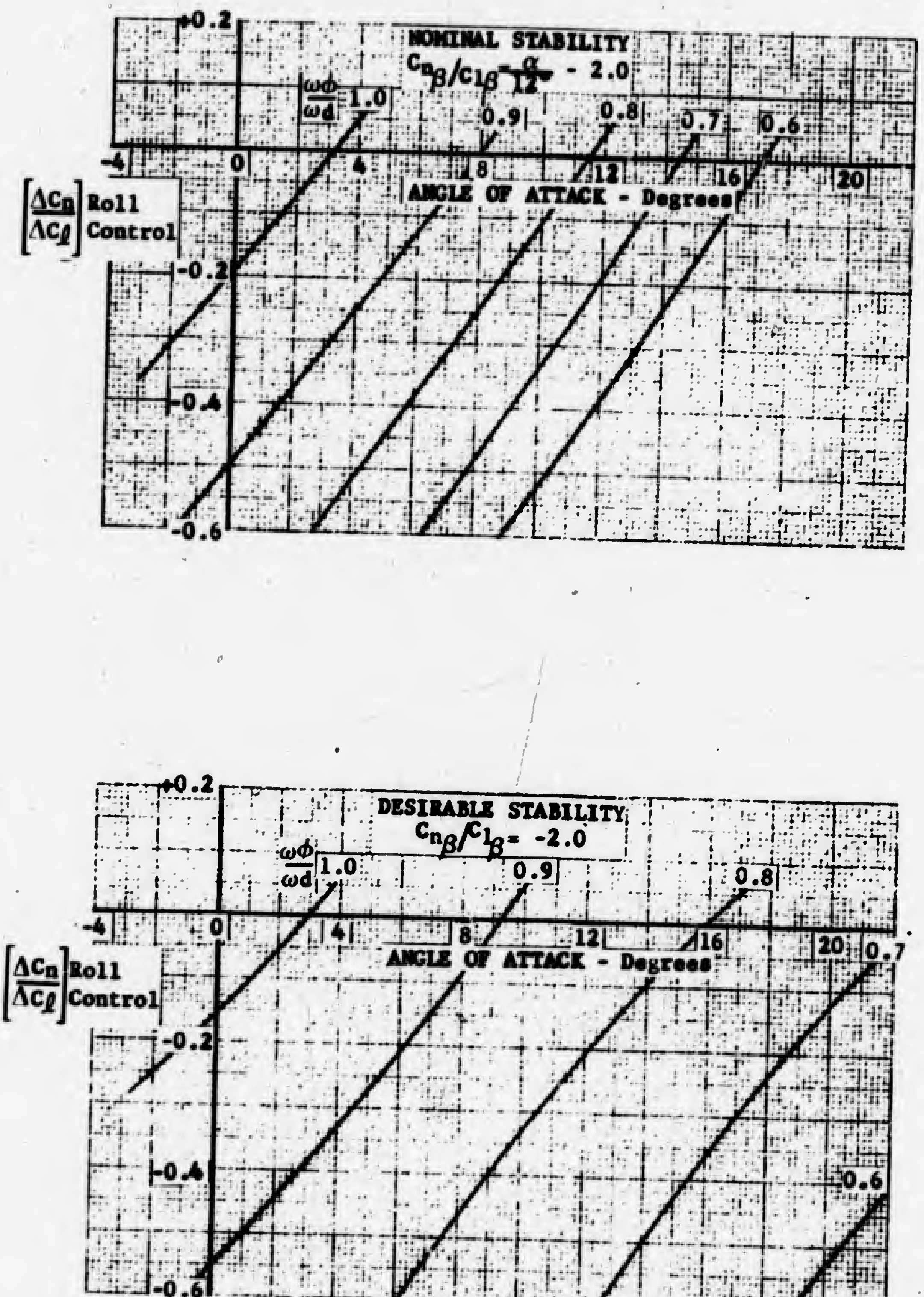


Figure 104 EFFECTS OF CONTROL MOMENT RATIO ON COORDINATION

The following representative values were used to obtain a numerical value:

One "g" Lift Coefficient at 0.9 Mach — $\frac{GW}{qS} \leq 0.3$

Wing Span — $b = 45 \text{ ft.}$

Roll radius of gyration based on general data of Reference 28

$$\bar{R}_x = 0.22$$

Effective Control Power — $L_{\delta_a}\delta_a = 7 \text{ sec.}^{-2}$

Giving — $\Delta C_{\ell_{req._{0.9M}}} = 0.0356$

For 1.2 Mach number, the one "g" Lift Coefficient was reduced by the dynamic pressure ratio to yield the value given below.

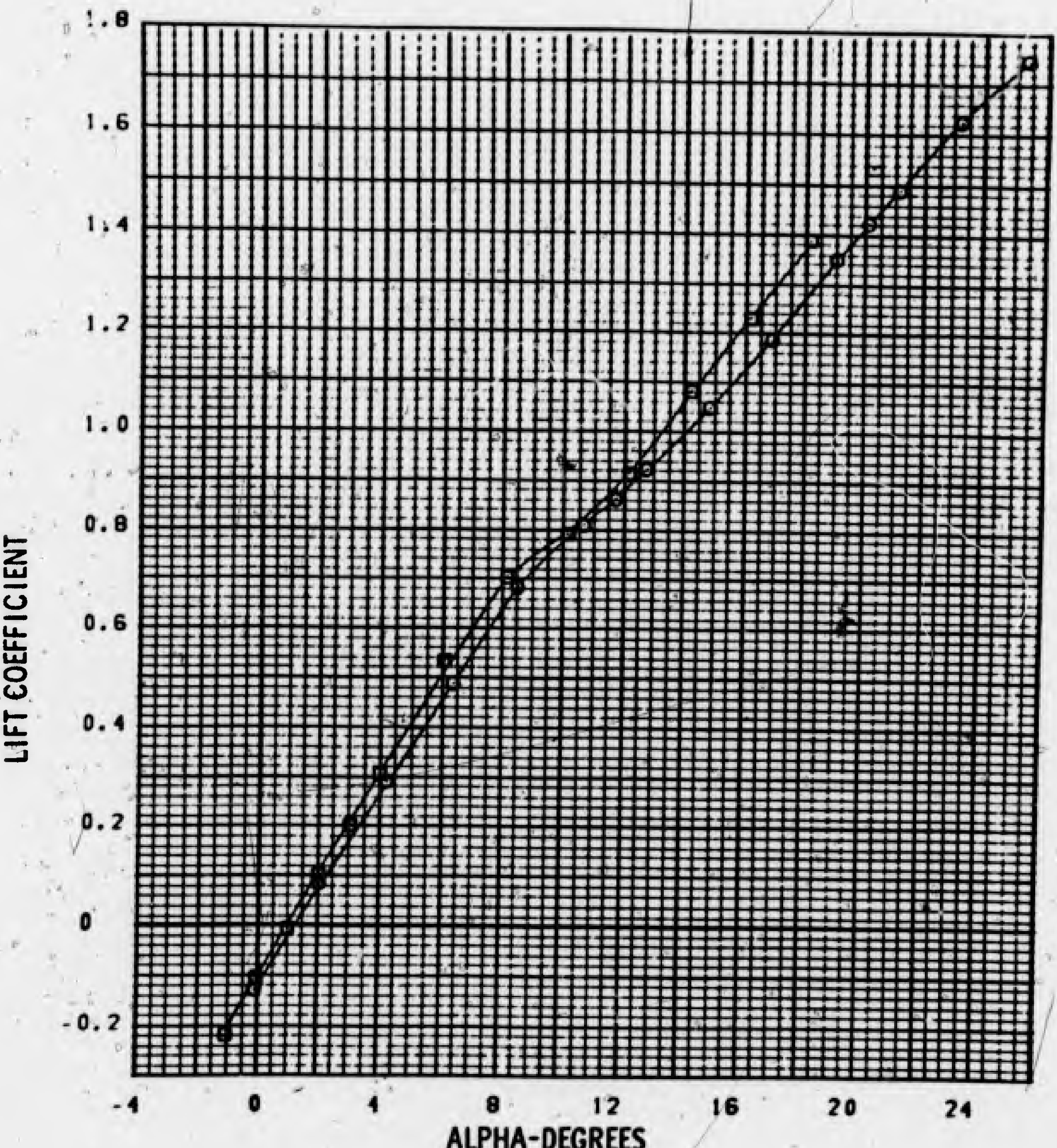
$$\Delta C_{\ell_{req._{1.2M}}} = 0.0356\left(\frac{0.9}{1.2}\right)^2 = 0.0200$$

APPENDIX III FORCE AND MOMENT COMPARISONS VARIOUS WIND TUNNELS USED

This appendix presents comparison plots which show the relative standing of the aerodynamic data obtained during the tests of the LEDE configuration in the 4T and 16T facilities. Plots are also presented for the tie-in configuration data obtained during the 4T tests to provide a continuity of all the data with other test results.

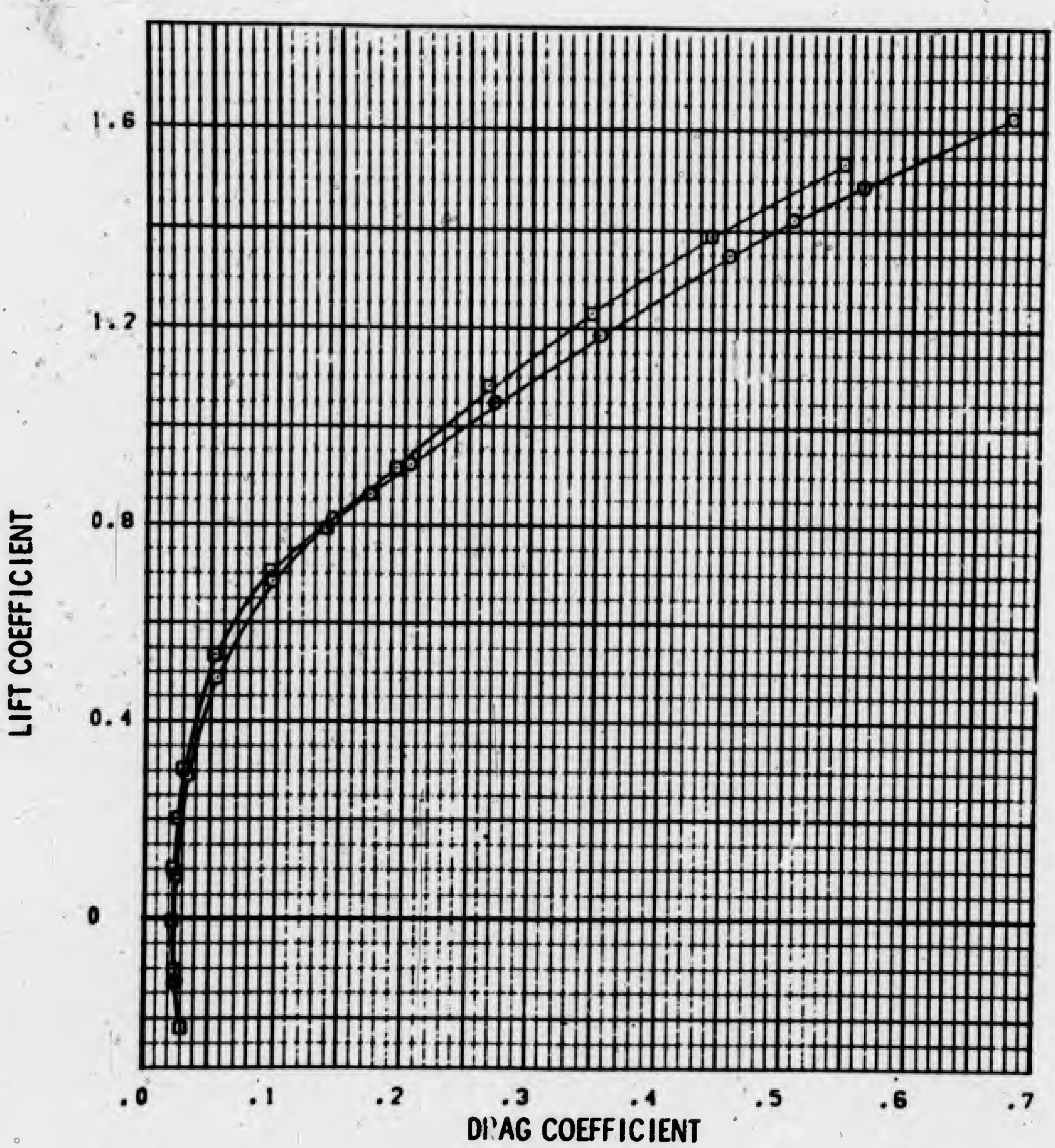
1. TIE-IN RUNS

The basic longitudinal aerodynamic data obtained for the F-111 configuration tested during the 4T tests are compared with similar data obtained in the Cornell Aeronautical Laboratory 8-foot transonic tunnel. These data are presented in this subsection in Figure 105.



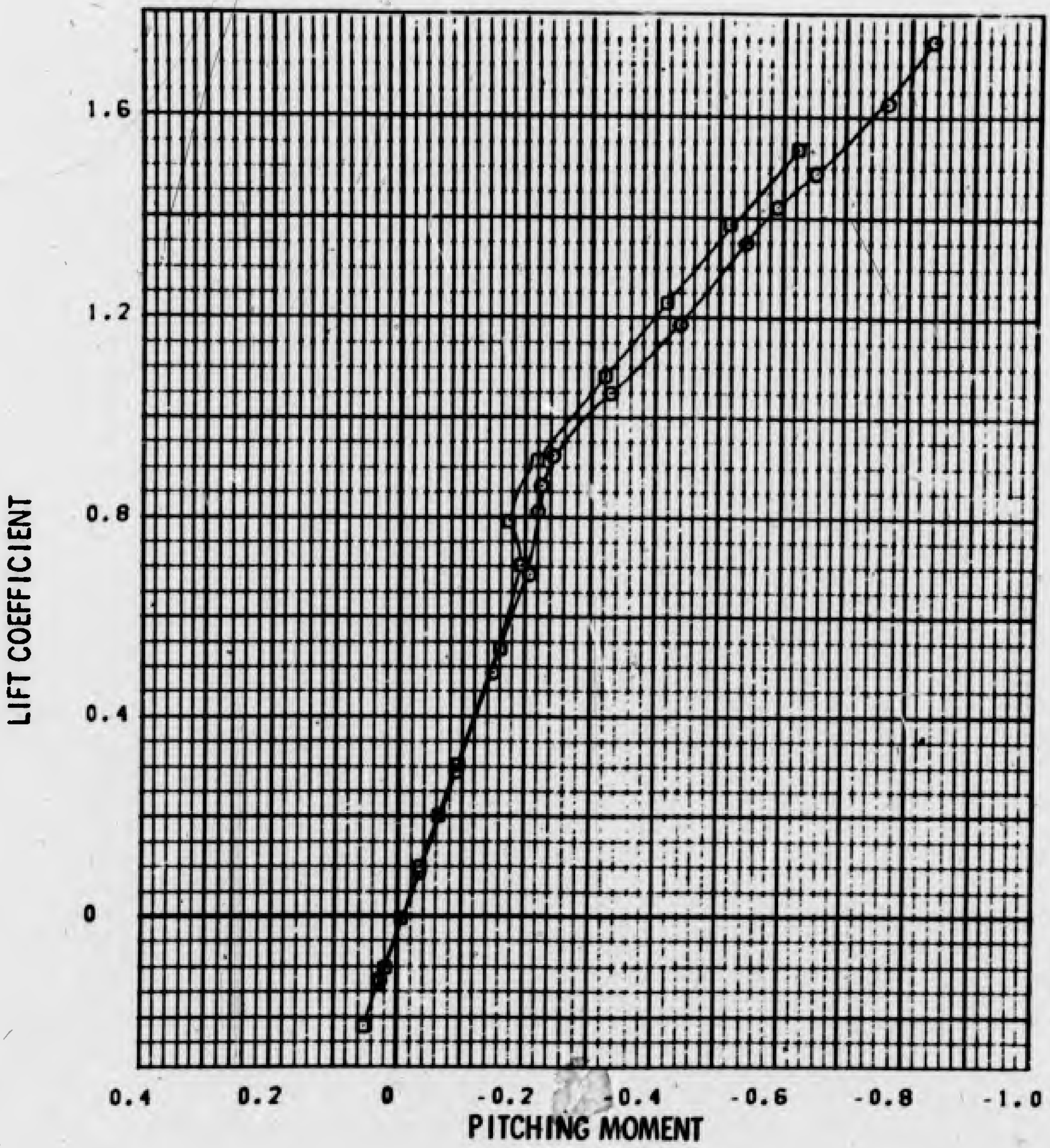
SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC 043	13	3.0 MILLION
⊡	CAL G52-253	269	3.0 MILLION

FIGURE 105a TIE-IN COMPARISON BETWEEN CAL AND PWT 4T AT L.E. SWEEP = 45 DEG., M = 0.9



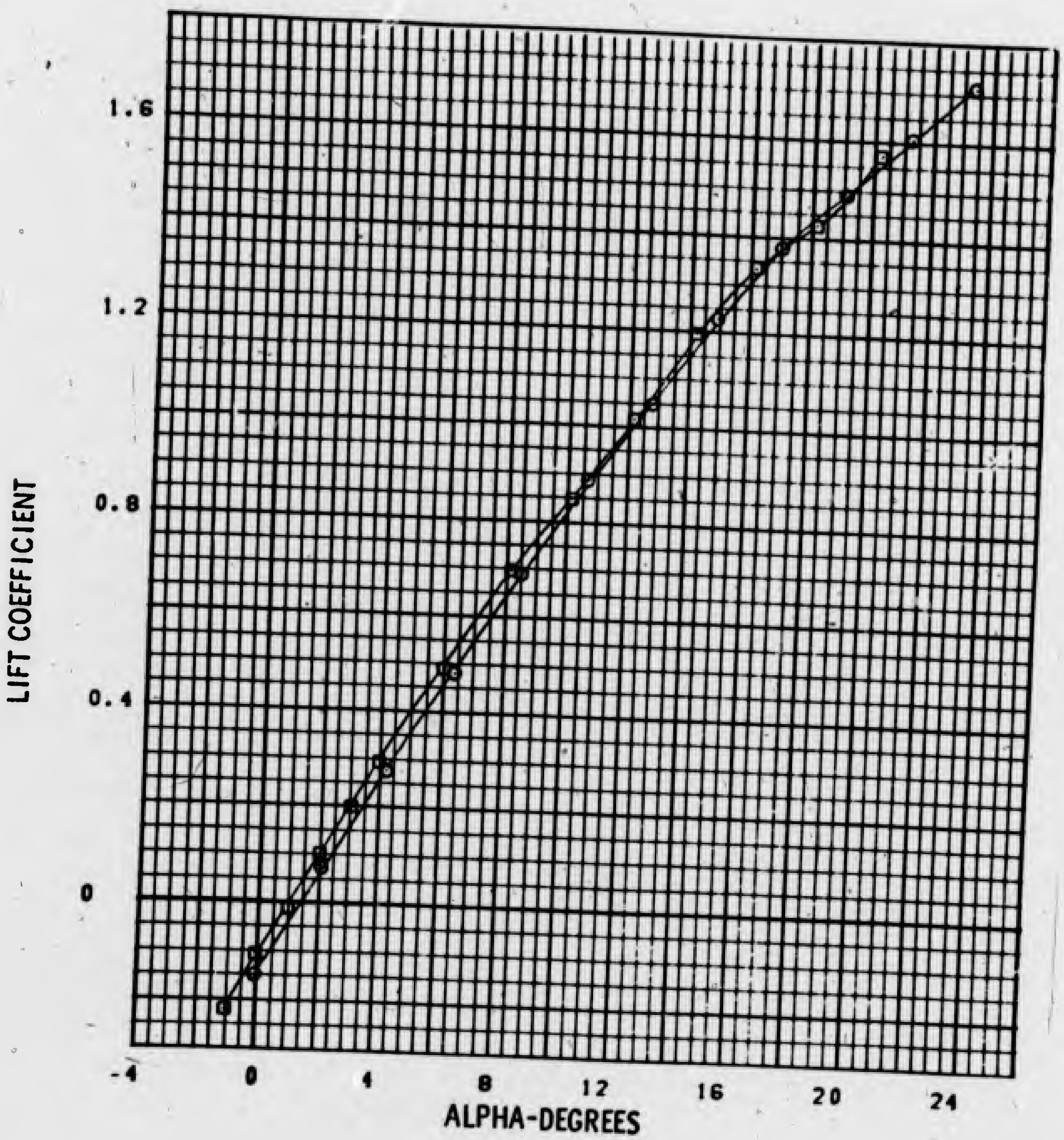
SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC 043	13	3.0 MILLION
⊡	CAL G52-253	269	3.0 MILLION

FIGURE 105a TIE-IN COMPARISON BETWEEN CAL AND PWT 4T
AT L.E. SWEEP = 45 DEG., M = 0.9



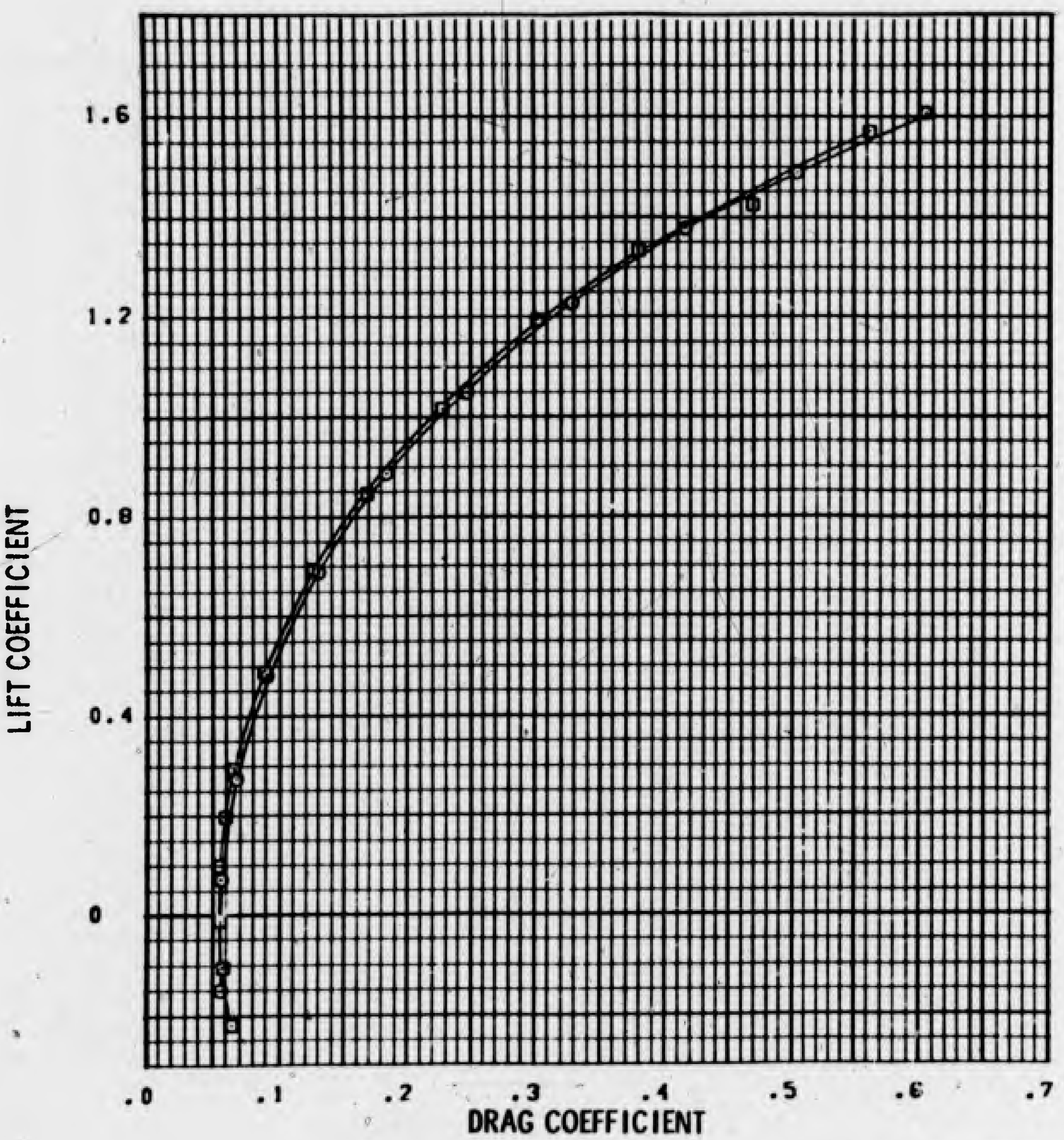
SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC 043	13	3.0 MILLION
⊡	CAL G52-253	269	3.0 MILLION

FIGURE 105a TIE-IN COMPARISON BETWEEN CAL AND PWT 4T AT L.E. SWEEP = 45 DEG., M = 0.9



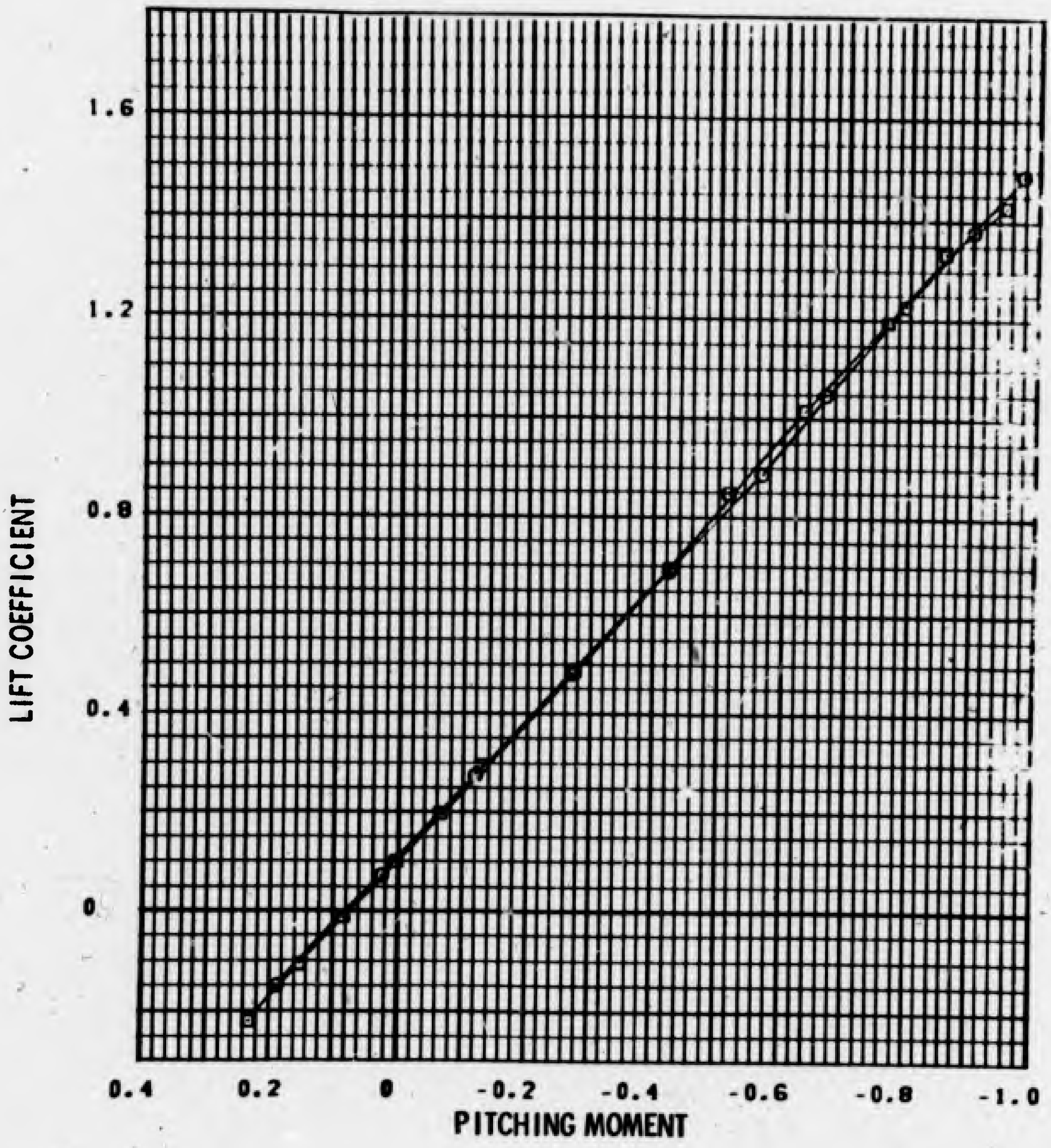
SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC-043	14	3.0 MILLION
⊡	CAL G52-253	266	3.0 MILLION

FIGURE 105b TIE-IN COMPARISON BETWEEN CAL AND PWT 4T AT L.E. SWEEP = 45 DEG.. M = 1.2



SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC-043	14	3.0 MILLION
⊡	CAL G52-253	266	3.0 MILLION

FIGURE 105b TIE-IN COMPARISON BETWEEN CAL AND PWT 4T AT L.E. SWEEP = 45 DEG., M = 1.2

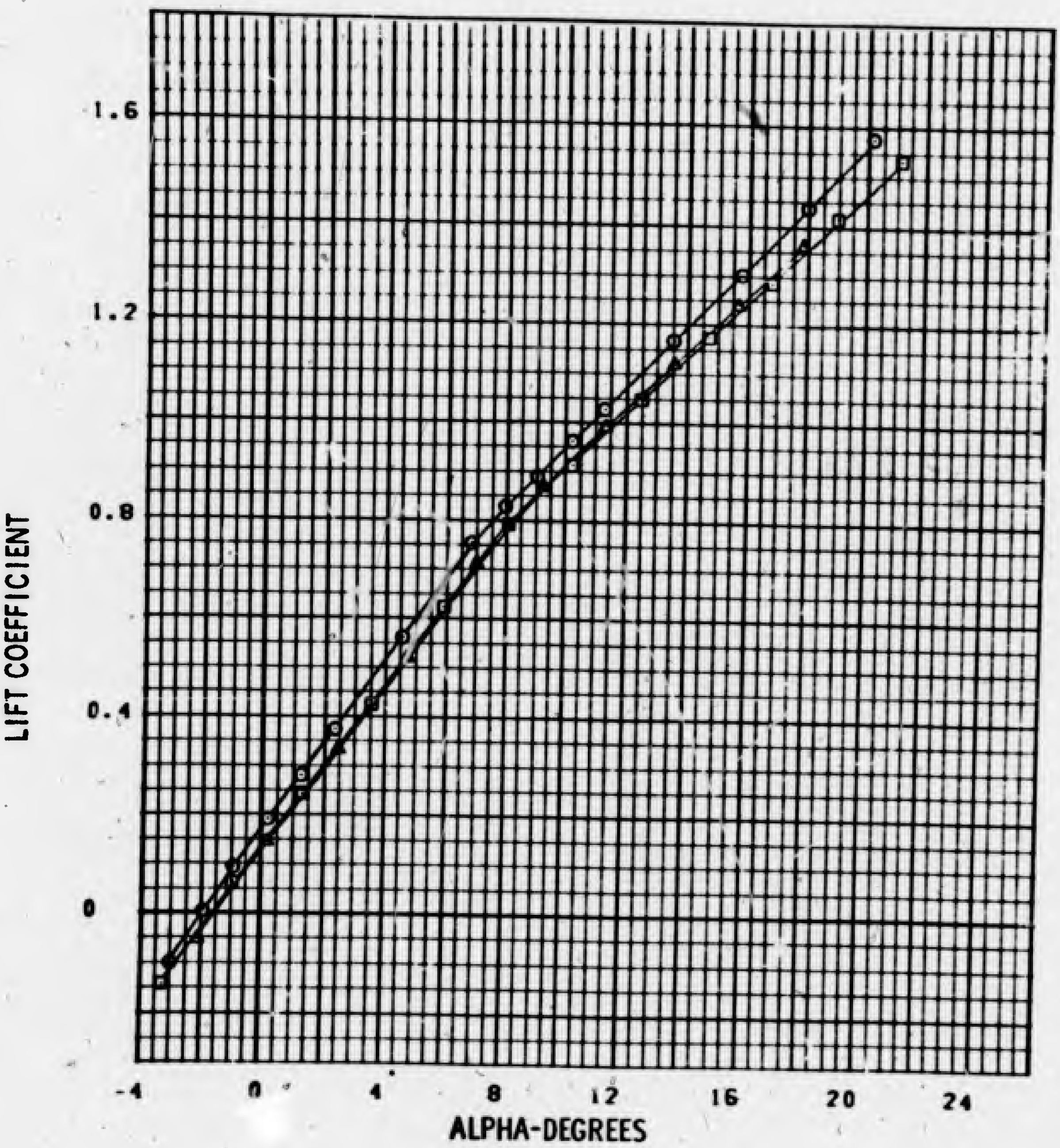


SYM	TEST	PART	RN/FT
⊙	AEDC PWT TC-043	14	3.0 MILLION
⊡	CAL G52-253	266	3.0 MILLION

FIGURE 105b TIE-IN COMPARISON BETWEEN CAL AND PWT 4T AT L.E. SWEEP = 45 DEG., M = 1.2

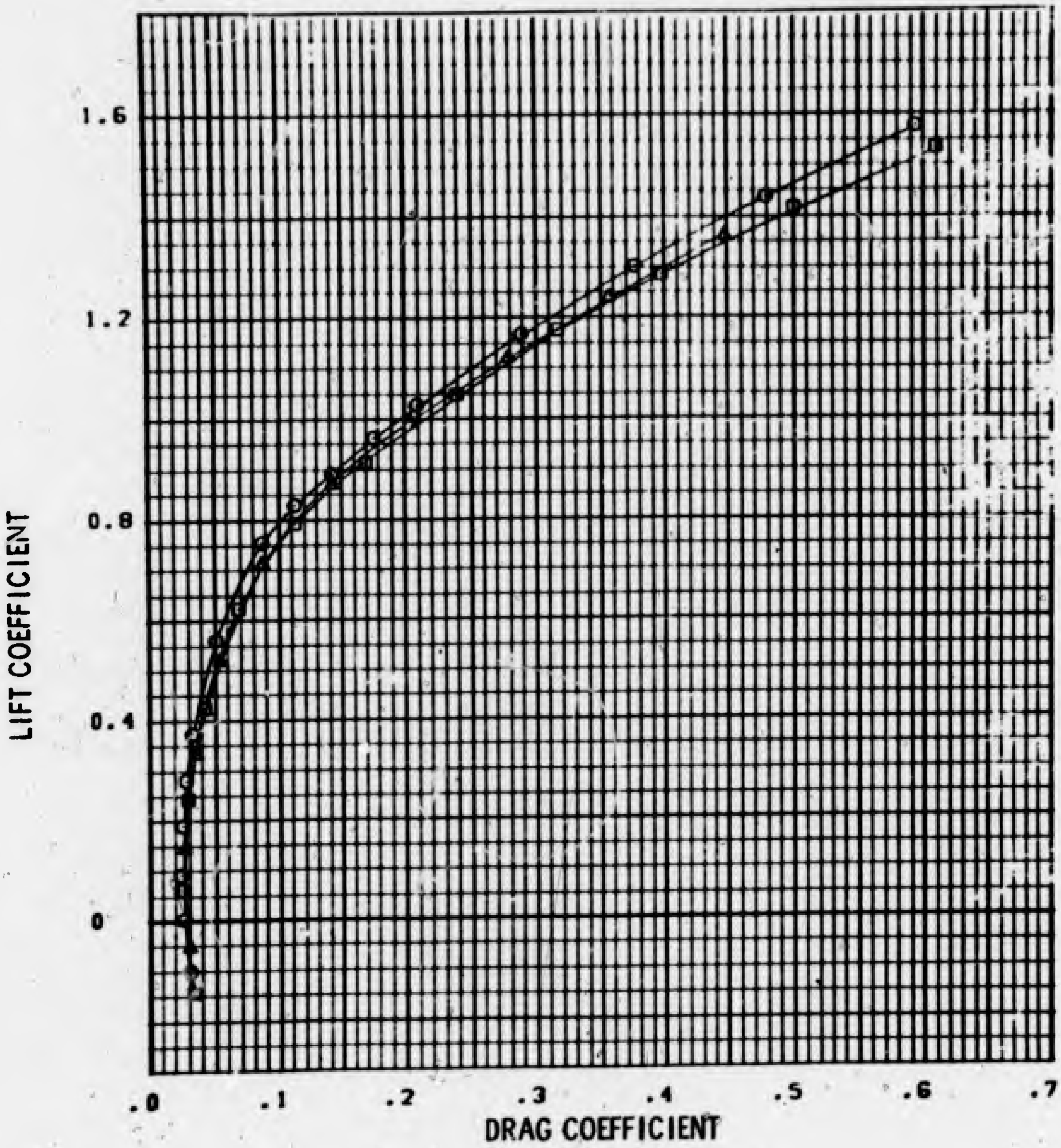
2. LEDE CONFIGURATION LONGITUDINAL DATA

A complete set of the longitudinal aerodynamic data for the LEDE configuration obtained during both entires into the 4-foot tunnel, and the 16-foot tunnel are compared in this subsection in Figure 106.



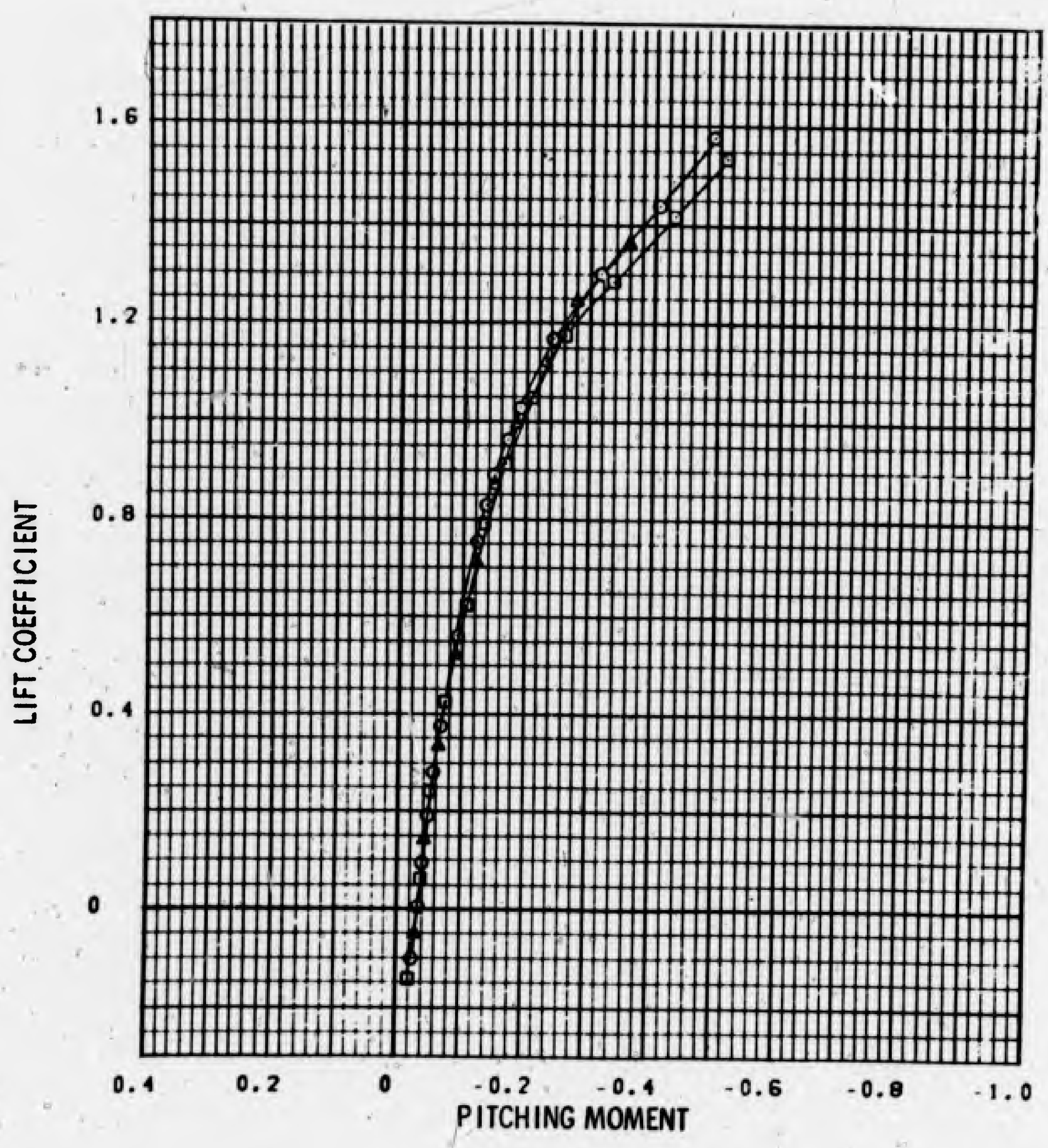
SYM	TEST	PART
⊙	PWT 16T TF-216	49
⊡	PWT 4T TC-043	268
▲	PWT 4T TC-043	438

FIGURE 106a LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.7



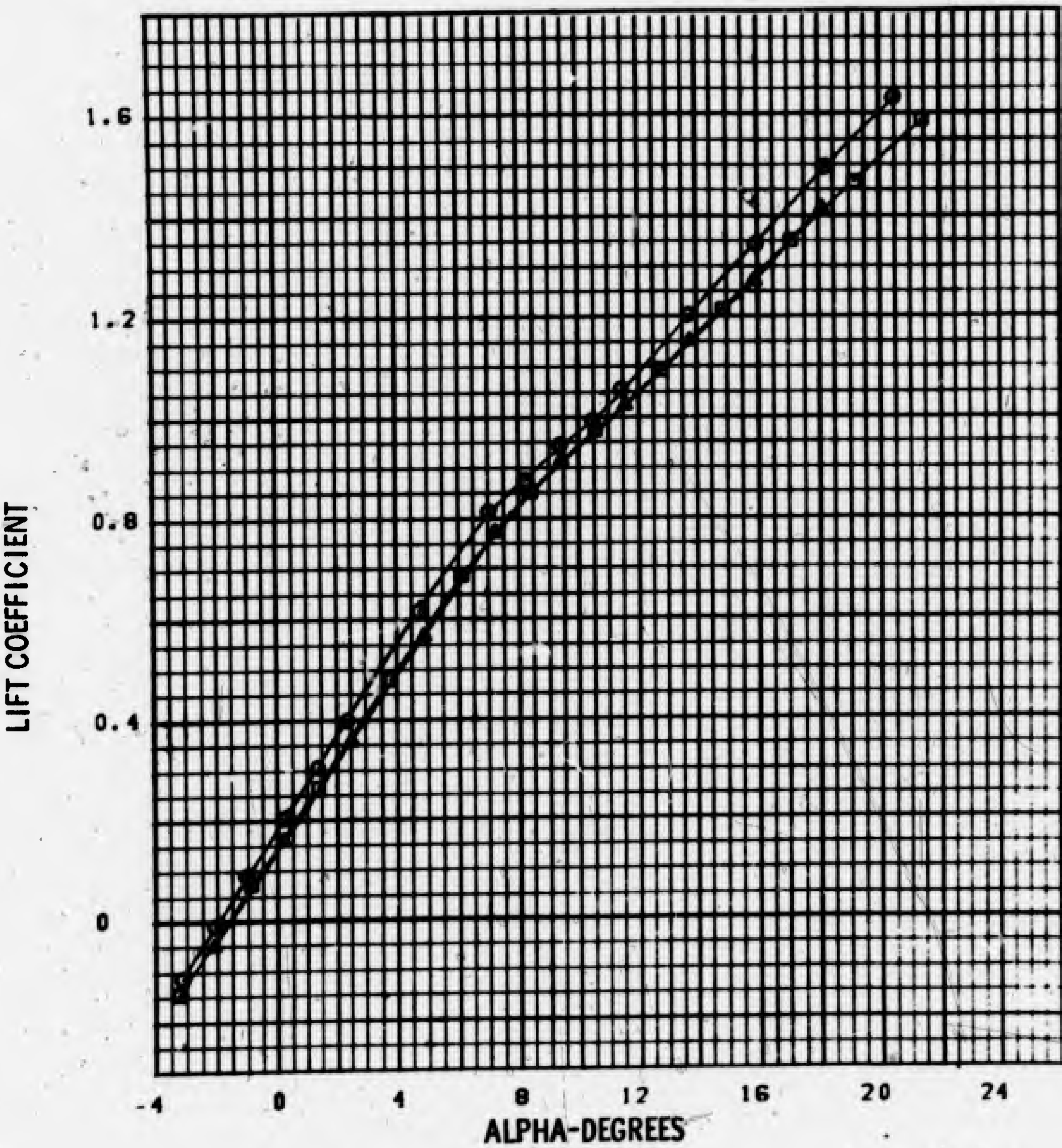
SYM	TEST	PART
⊙	PWT 16T TF-216	49
⊡	PWT 4T TC-043	268
▲	PWT 4T TC-043	438

FIGURE 106a LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.7



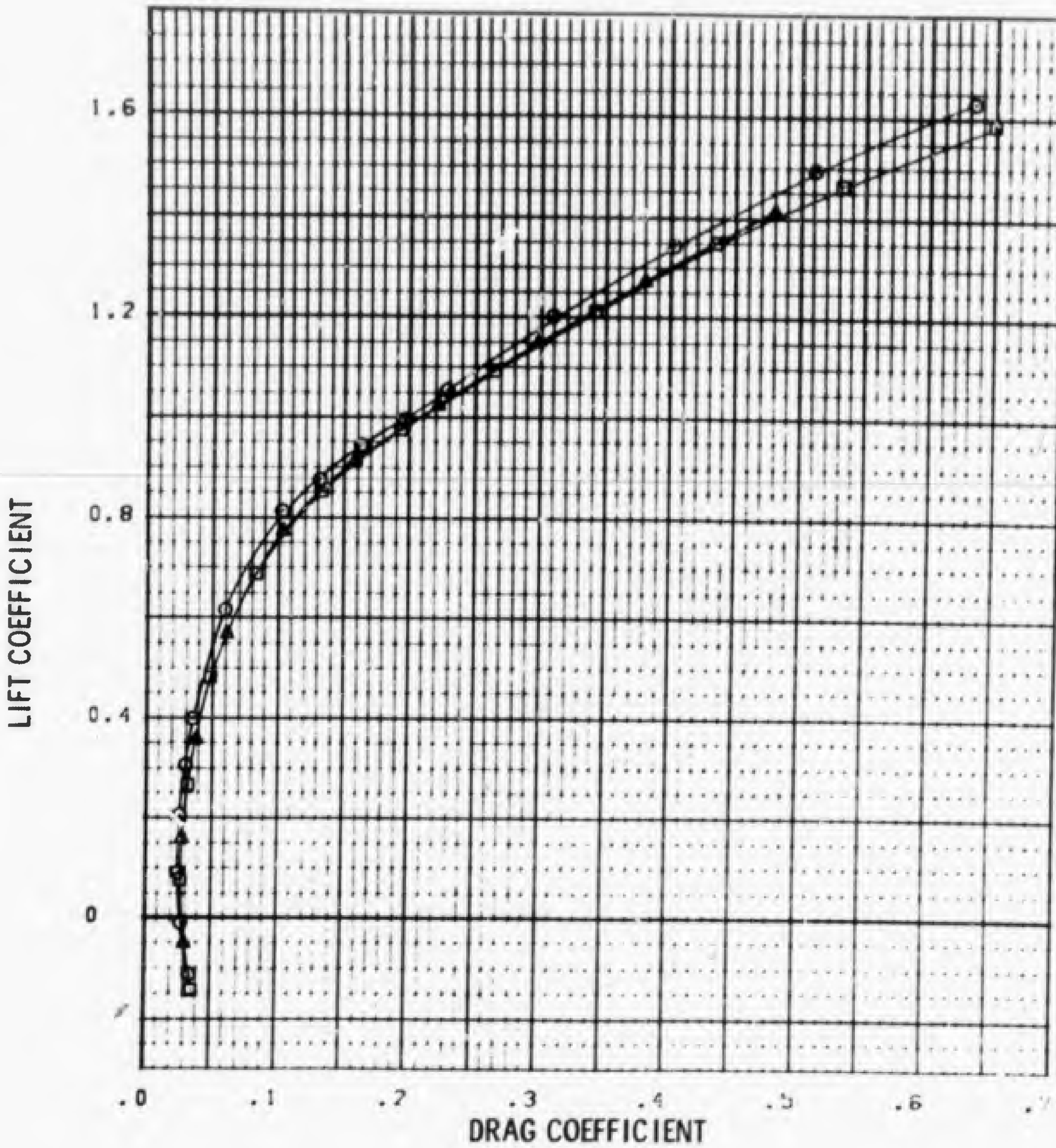
SYM	TEST	PART
⊙	PWT 16T TF 216	49
⊡	PWT 4T TC-043	268
▲	PWT 4T TC-043	438

FIGURE 106a LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.7



SYM	TEST	PART
⊙	PWT 16T TF-216	50
⊡	PWT 4T TC-043	267
▲	PWT 4T TC-043	440

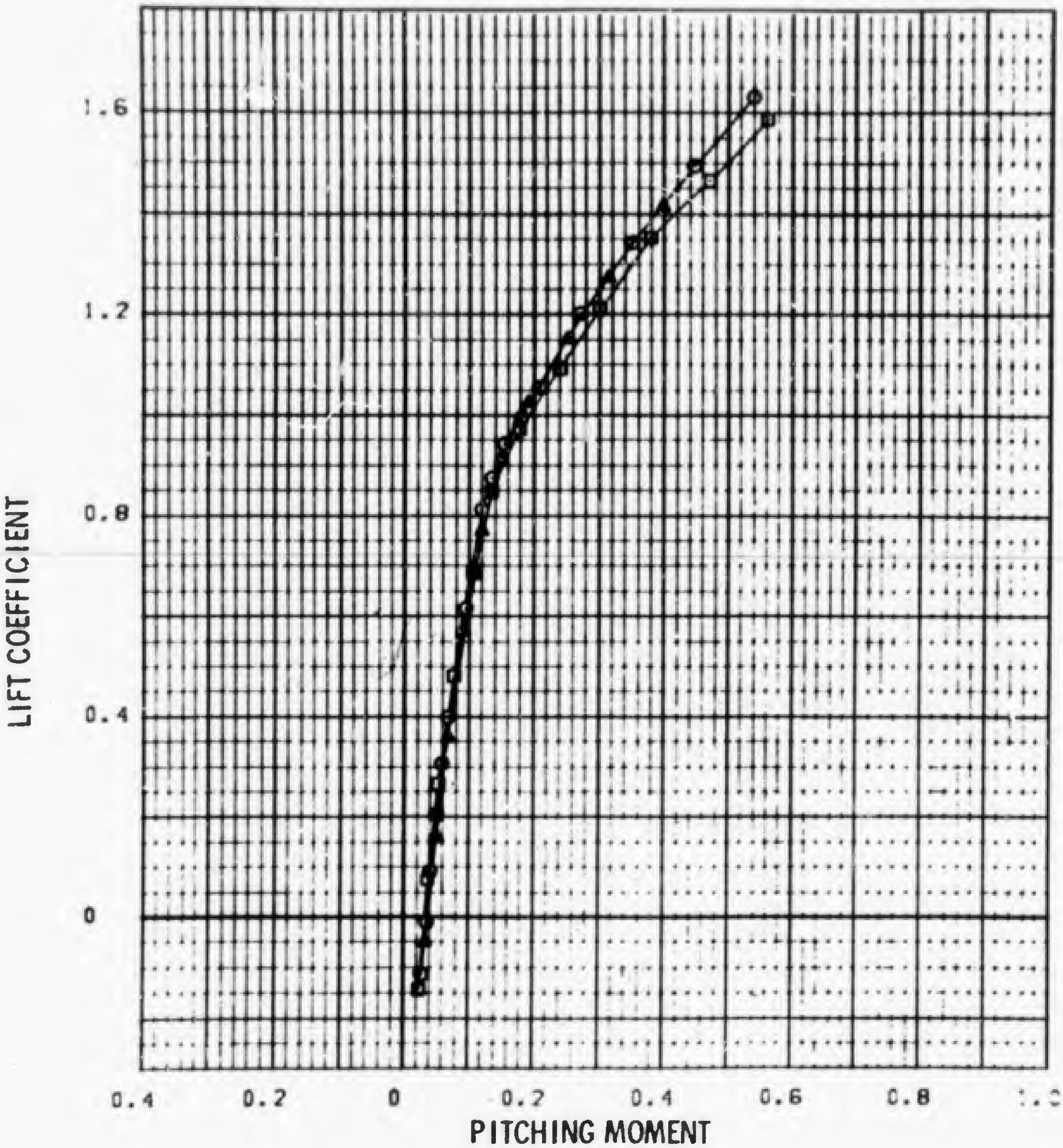
FIGURE 106b LEDE, CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.8



○	[illegible]	[illegible]6	[illegible]	[illegible]
□	[illegible]	4[illegible]	[illegible] 043	76[illegible]
▲	[illegible]	4[illegible]	[illegible] 043	440

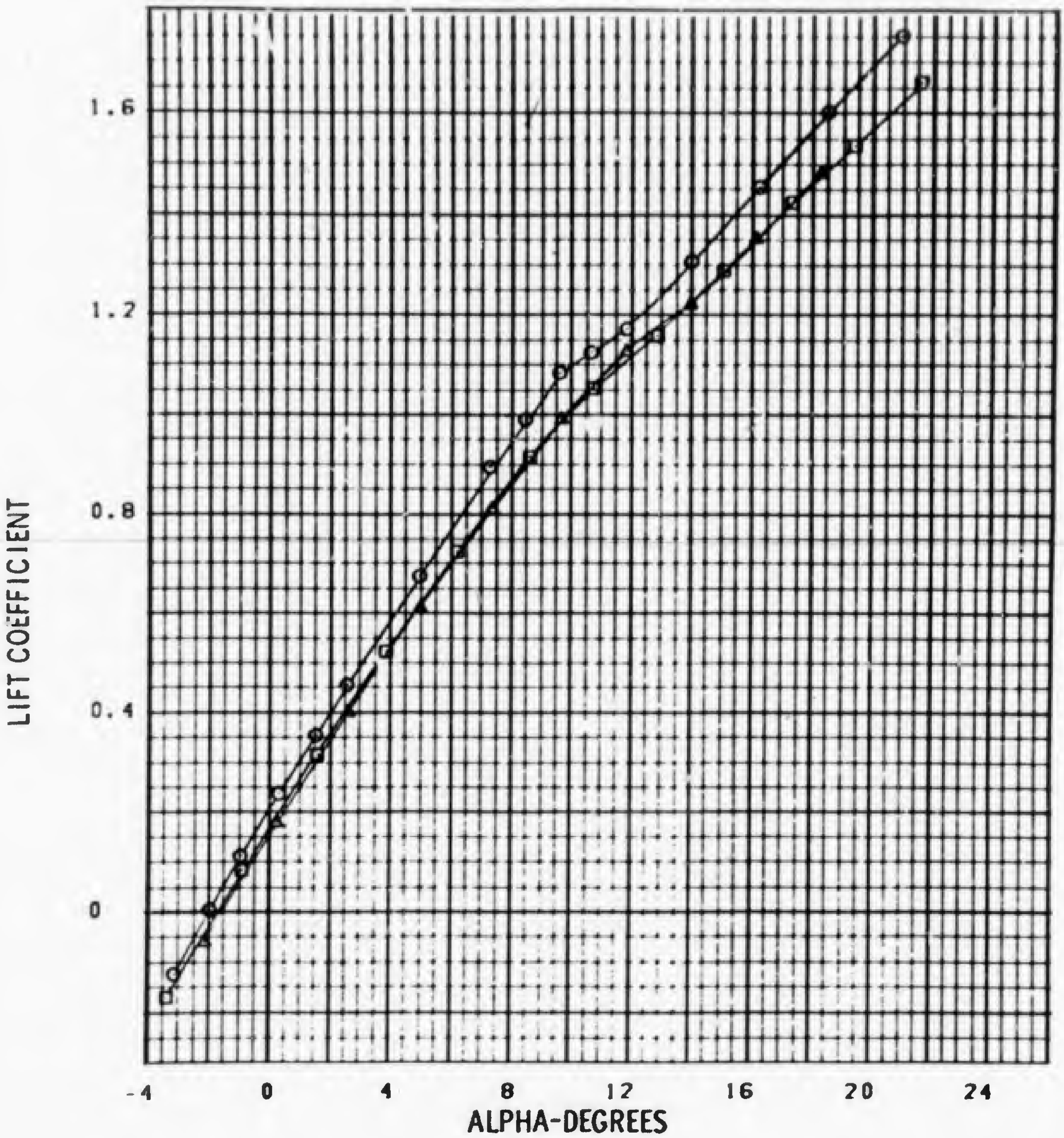
[illegible] 106b [illegible] C[illegible]EAN WING COMPARISON [illegible]

M [illegible].8



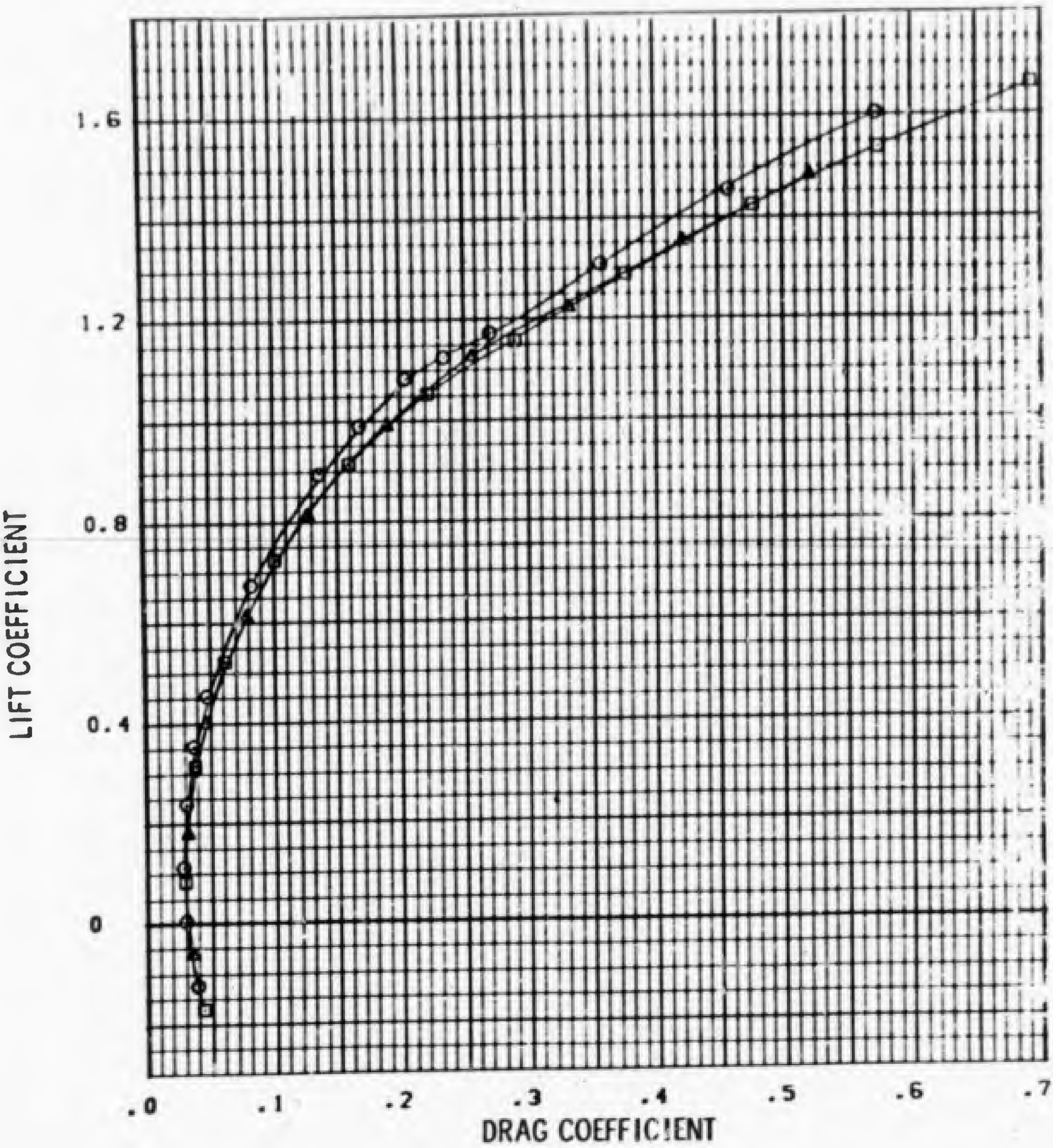
SYM	TEST	PART
⊙	PWT 16T TF 216	50
⊡	PWT 4T TC 043	267
▲	PWT 4T TC 043	440

FIGURE 106b . CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M 0.8



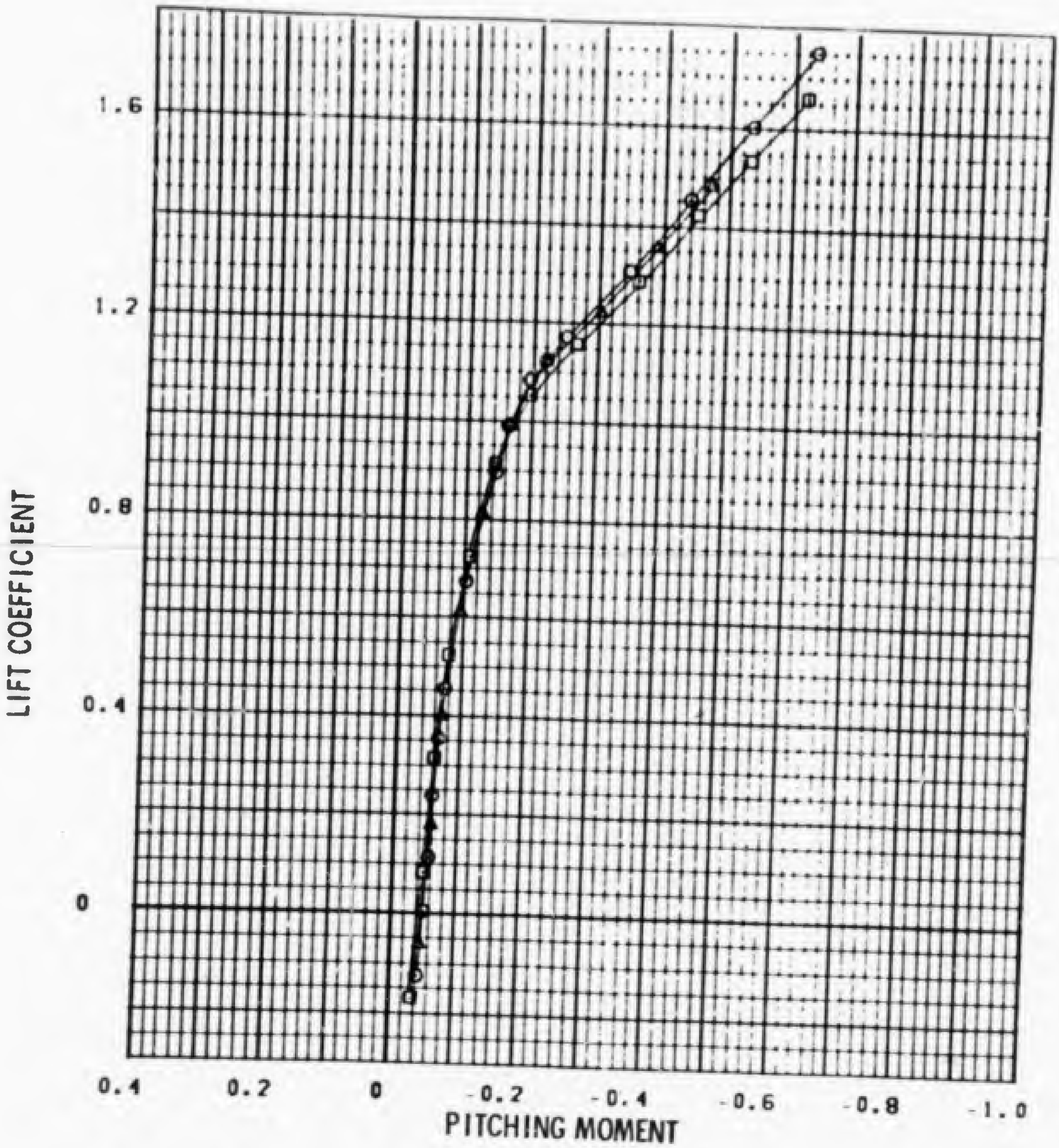
SYM	TEST	PART
⊙	PWT 16T TF 236	52
⊡	PWT 4T TC 043	264
▲	PWT 4T TC 043	441

FIGURE 106c LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.9



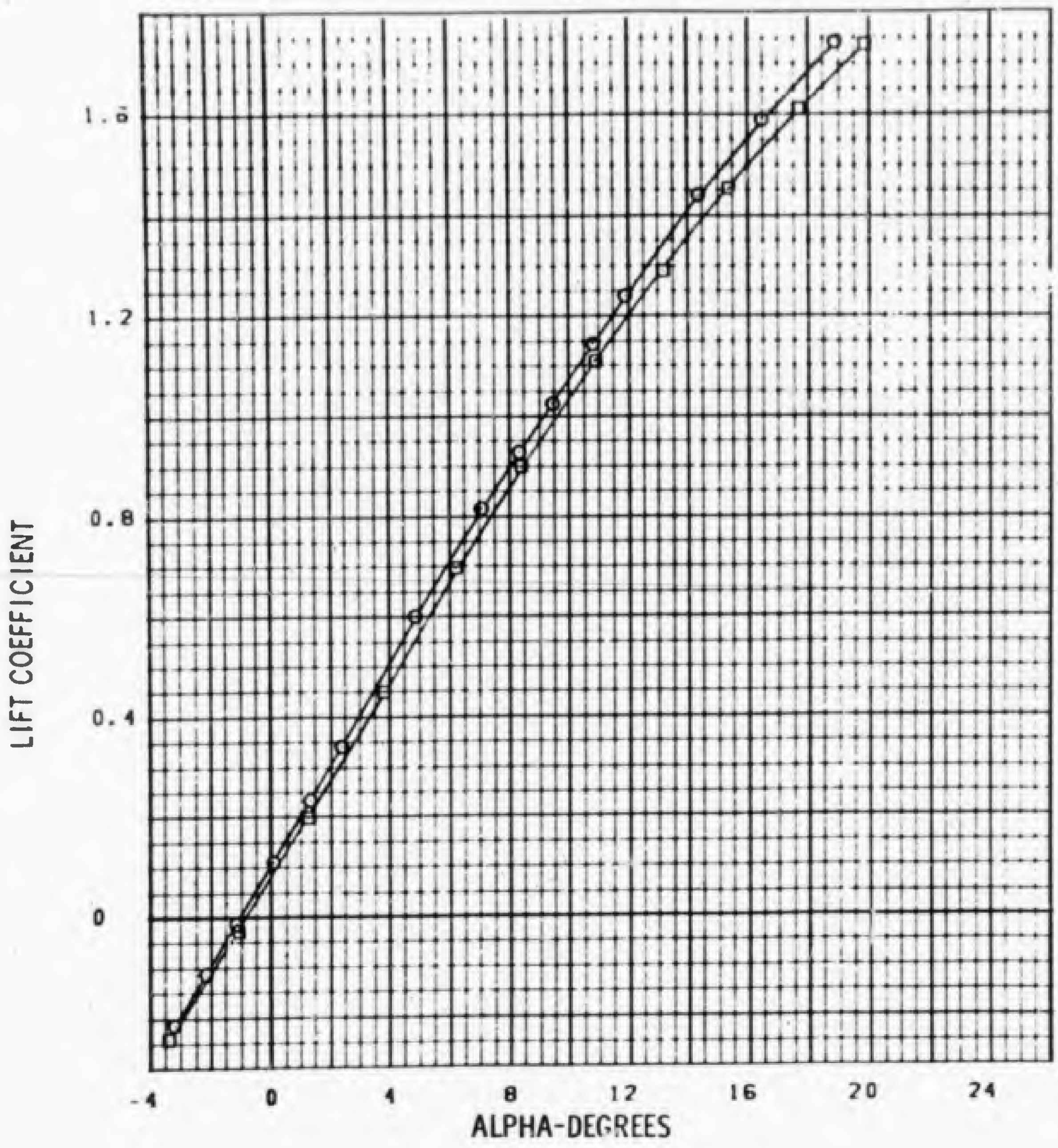
SYM	TEST	PART
⊙	PWT 16T TF-216	52
⊡	PWT 4T TC-043	264
▲	PWT 4T TC-043	441

FIGURE 106c LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.9



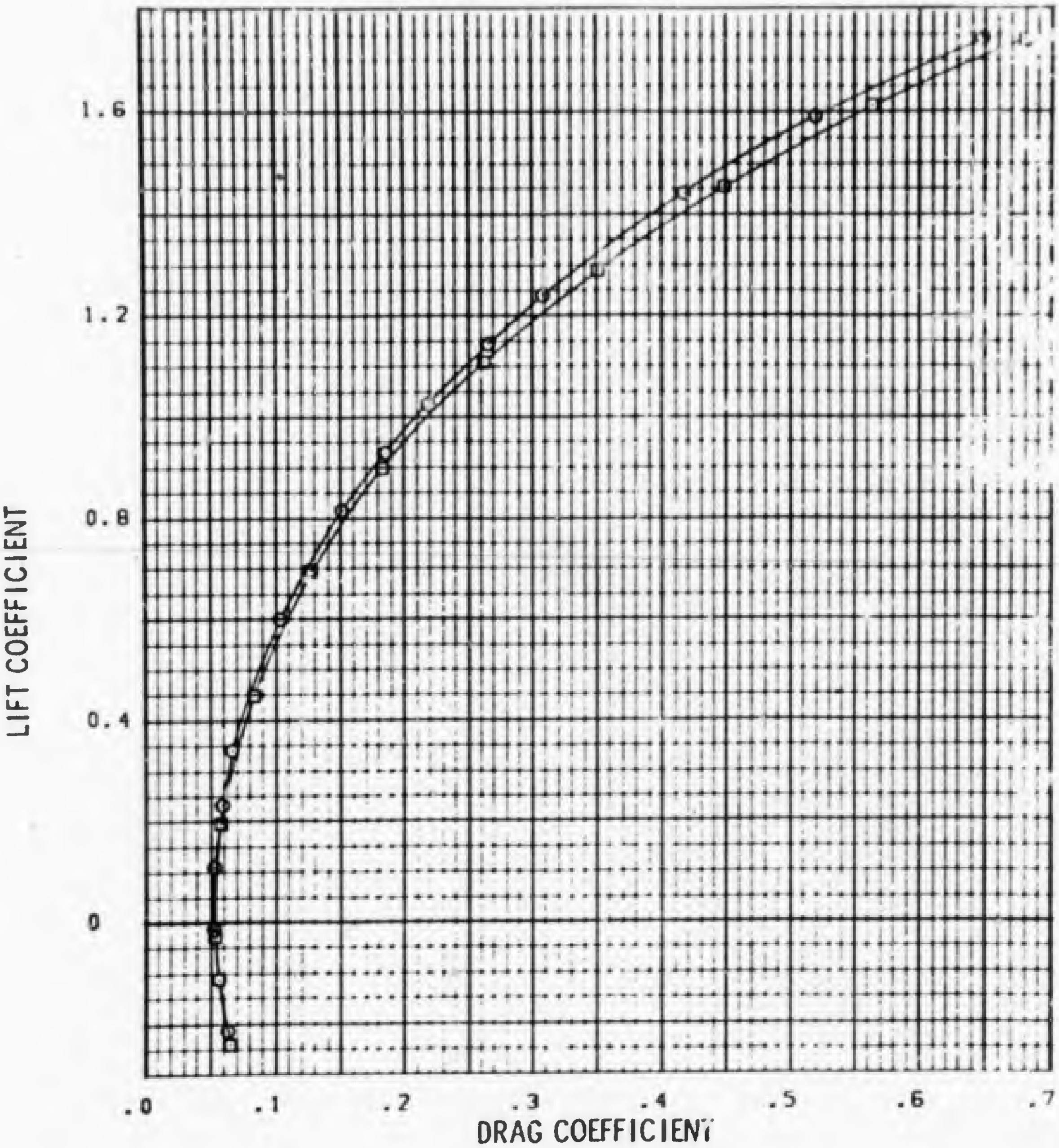
SYM	TEST	PART
⊙	PWT 16T TF-216	52
⊡	PWT 4T TC-043	264
▲	PWT 4T TC-043	441

FIGURE 106c LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 0.9



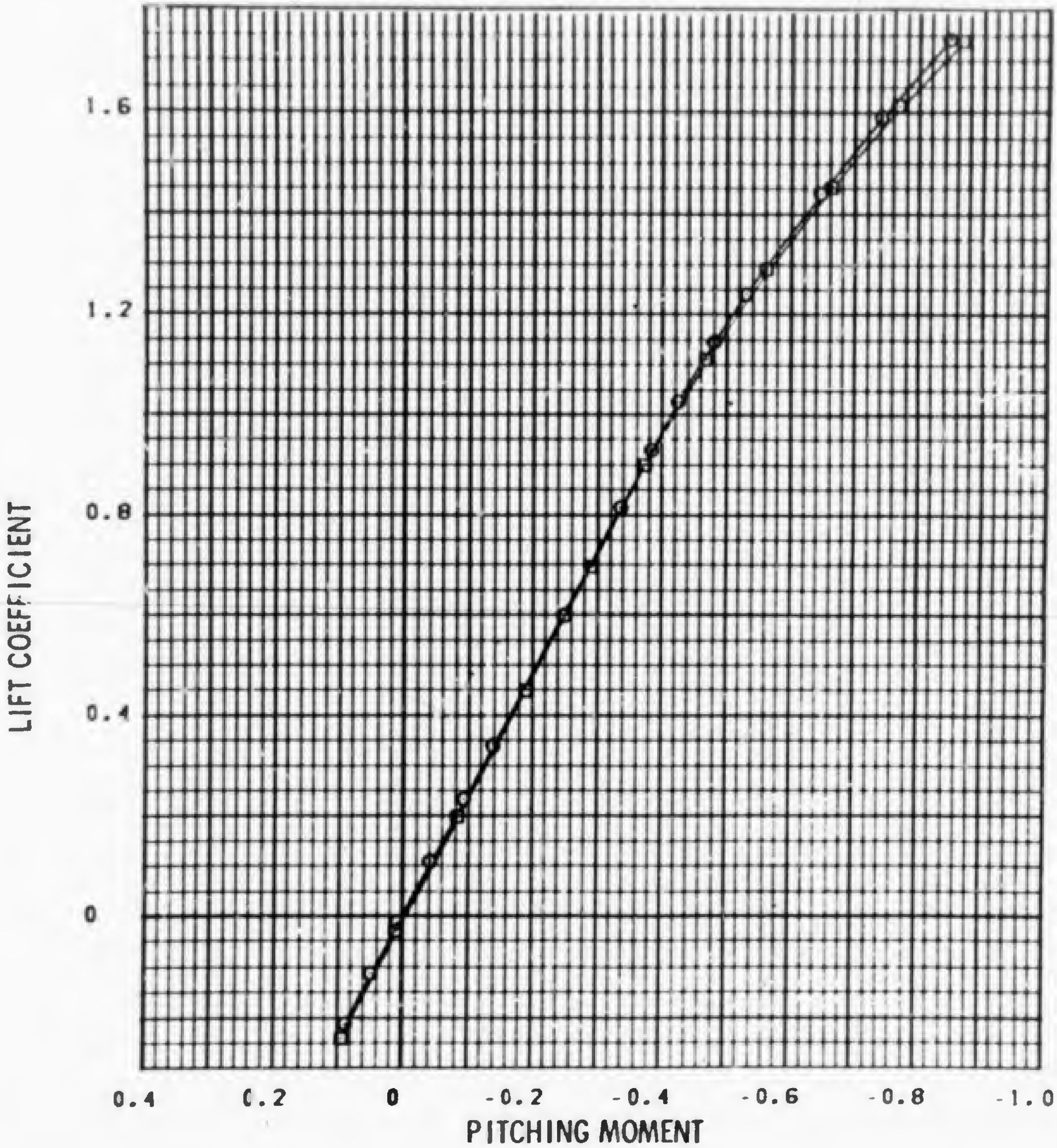
SYM	TEST	PART
⊙	PWT 16T TF 216	54
⊡	PWT 4T TC 043	269

FIGURE 106d LEDE, CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 1.2



SYM	TEST	PART
○	PWT 16T TF 216	54
⊡	PWT 4T TC 043	269

FIGURE 106d MODEL C FAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 1.2

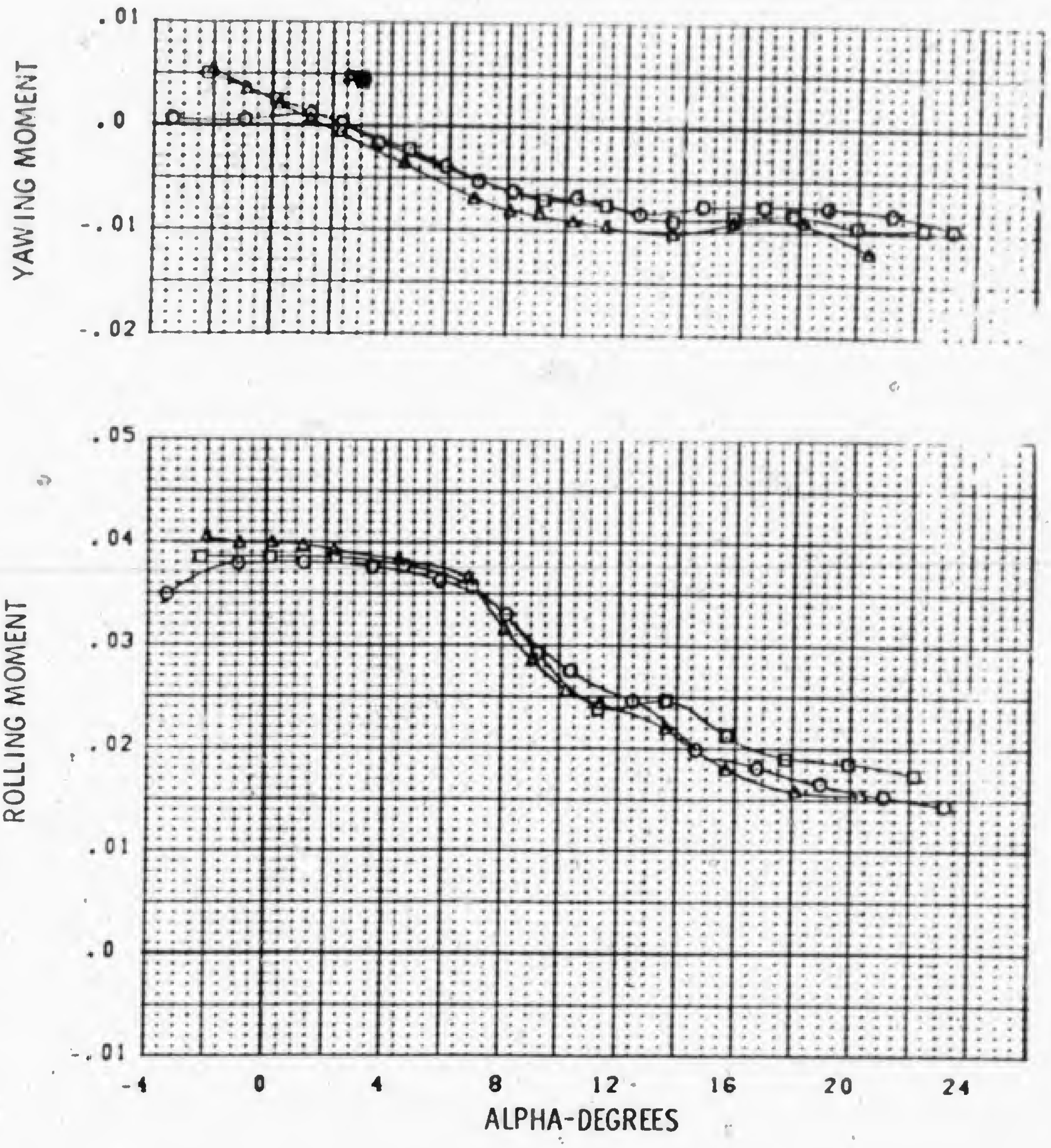


SYM	TEST	PART
⊙	PWT 16T TF 216	54
⊡	PWT 4T TC 043	269

FIGURE 106d LEDE. CLEAN WING COMPARISON BETWEEN PWT 4T AND 16T
M = 1.2

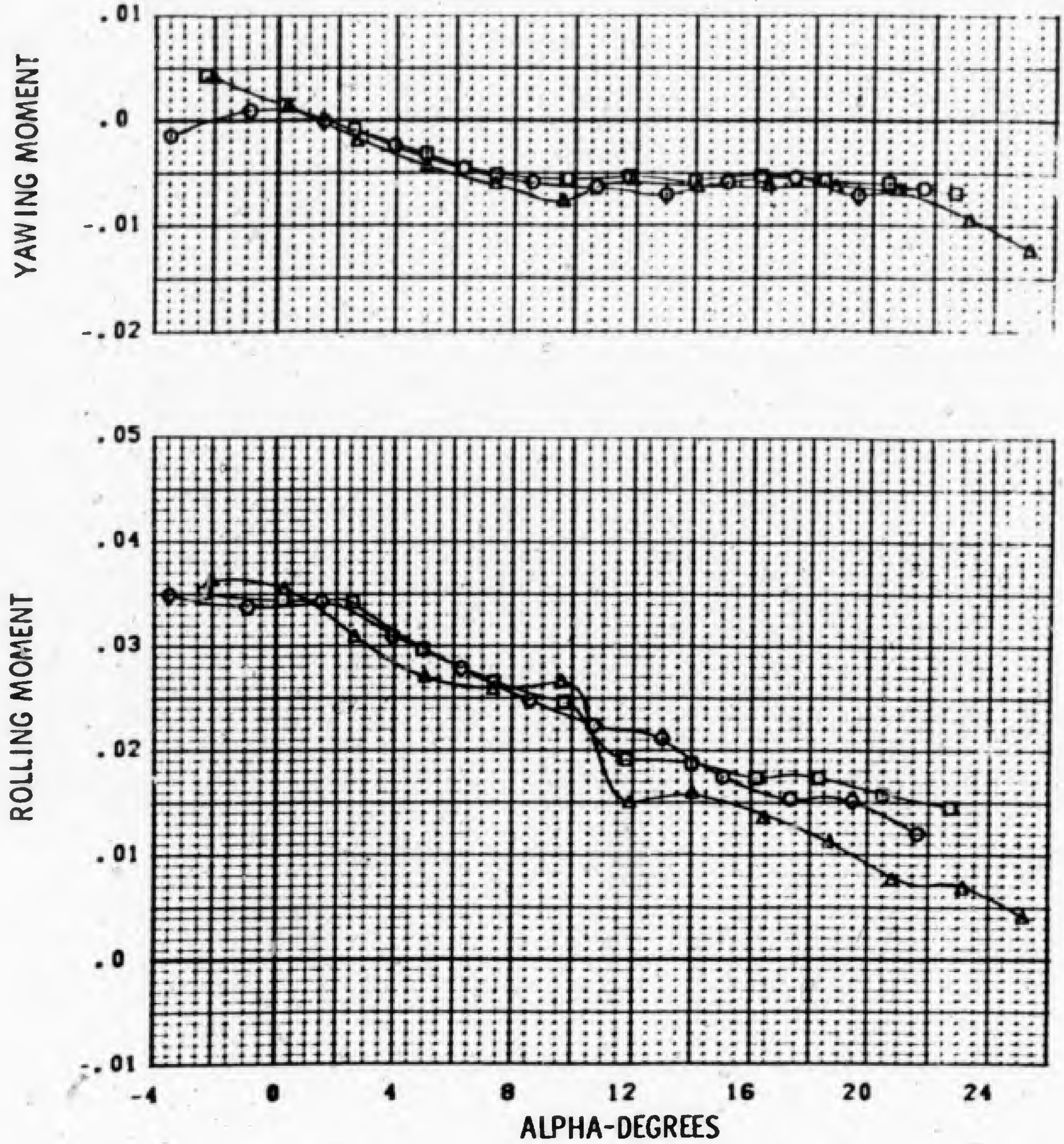
3. LEDE CONFIGURATION LATERAL-DIRECTIONAL DATA

Rolling and yawing moment data for the LEDE configuration obtained during the two entries into the 4-foot tunnel, and the 16-foot tunnel data are compared in this subsection in Figures 107 through 109.



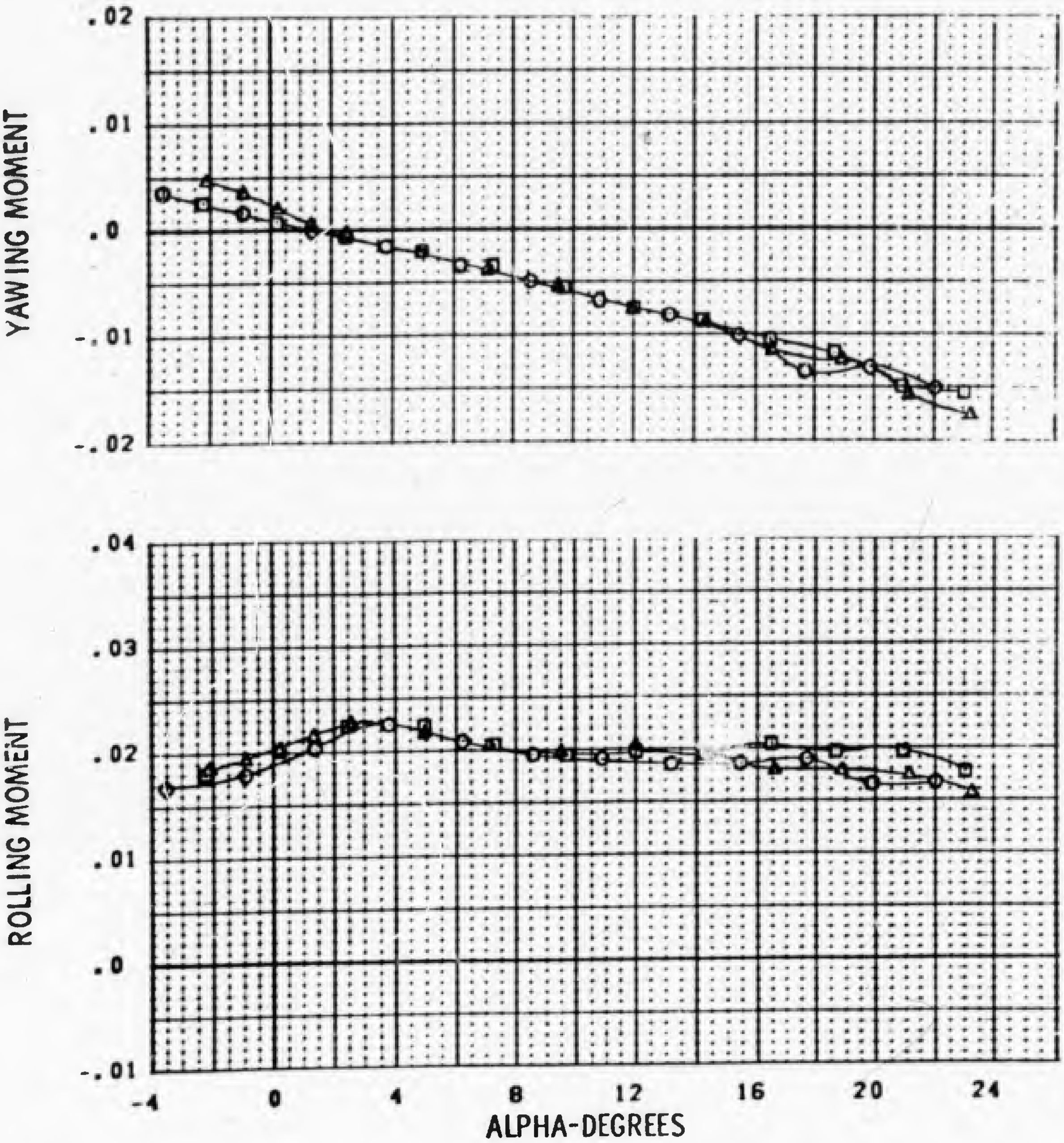
SYM	TEST	PART	L.E. (L/R)		AILERON (L/R)	
O	PWT 4T TC-043	215	K1	0/0	MID	20/-20
□	PWT 4T TC-043	410	K1	0/0	MID	20/-20
Δ	PWT 16T TF-216	13	K1	0/0	MID	20/-20

FIGURE 107a LEDE. MID AILERONS. COMPARISONS BETWEEN PWT 4T AND 16T. M = 0.7



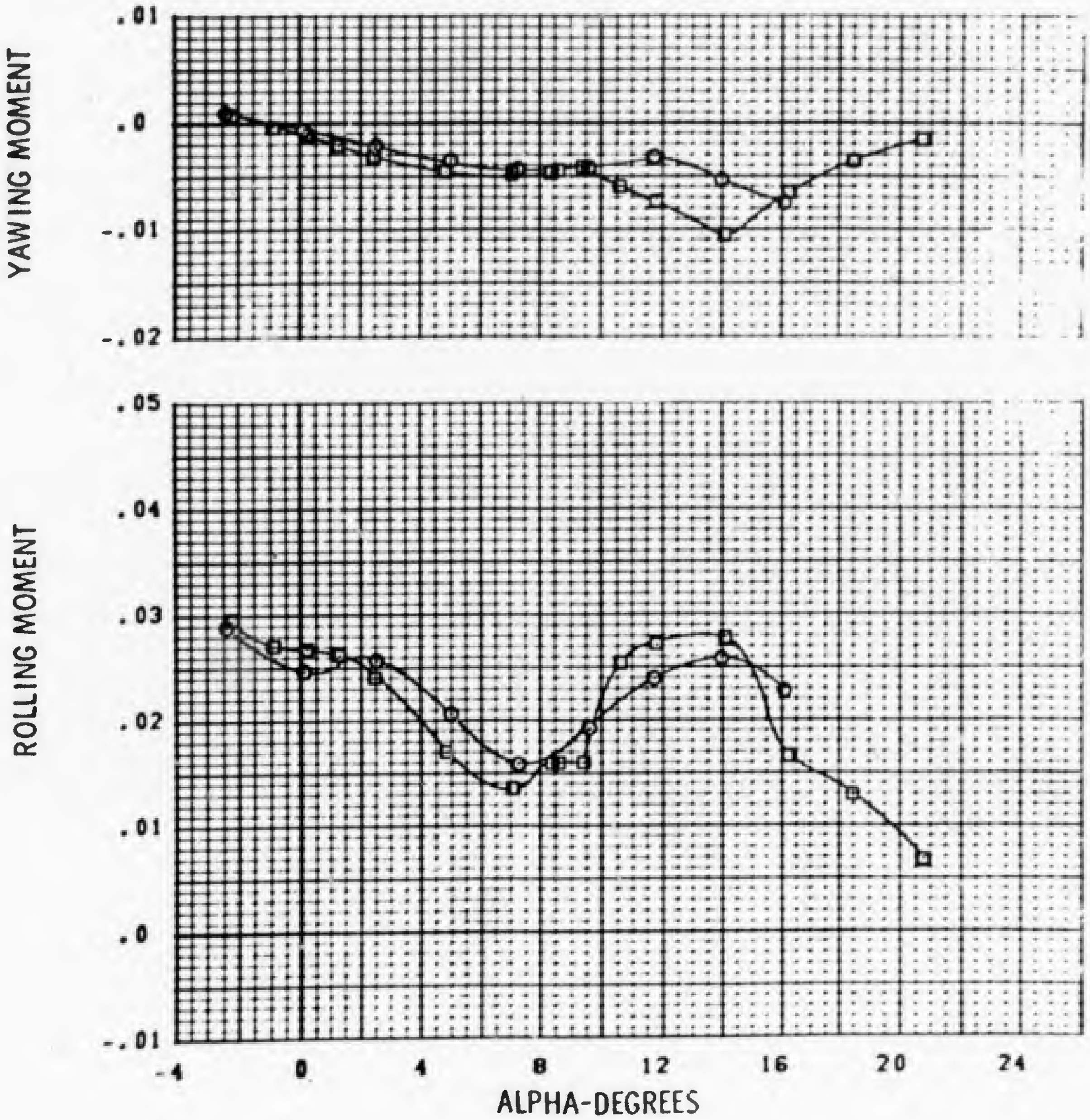
SYM	TEST	PART	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	213	K1	0/0	MID	20/-20
□	PWT 4T TC-043	412	K1	0/0	MID	20/-20
▲	PWT 16T TF-216	8	K1	0/0	MID	20/-20

FIGURE 107b LEDE, MID AILERONS, COMPARISONS BETWEEN PWT 4T AND 16T, M = 0.9



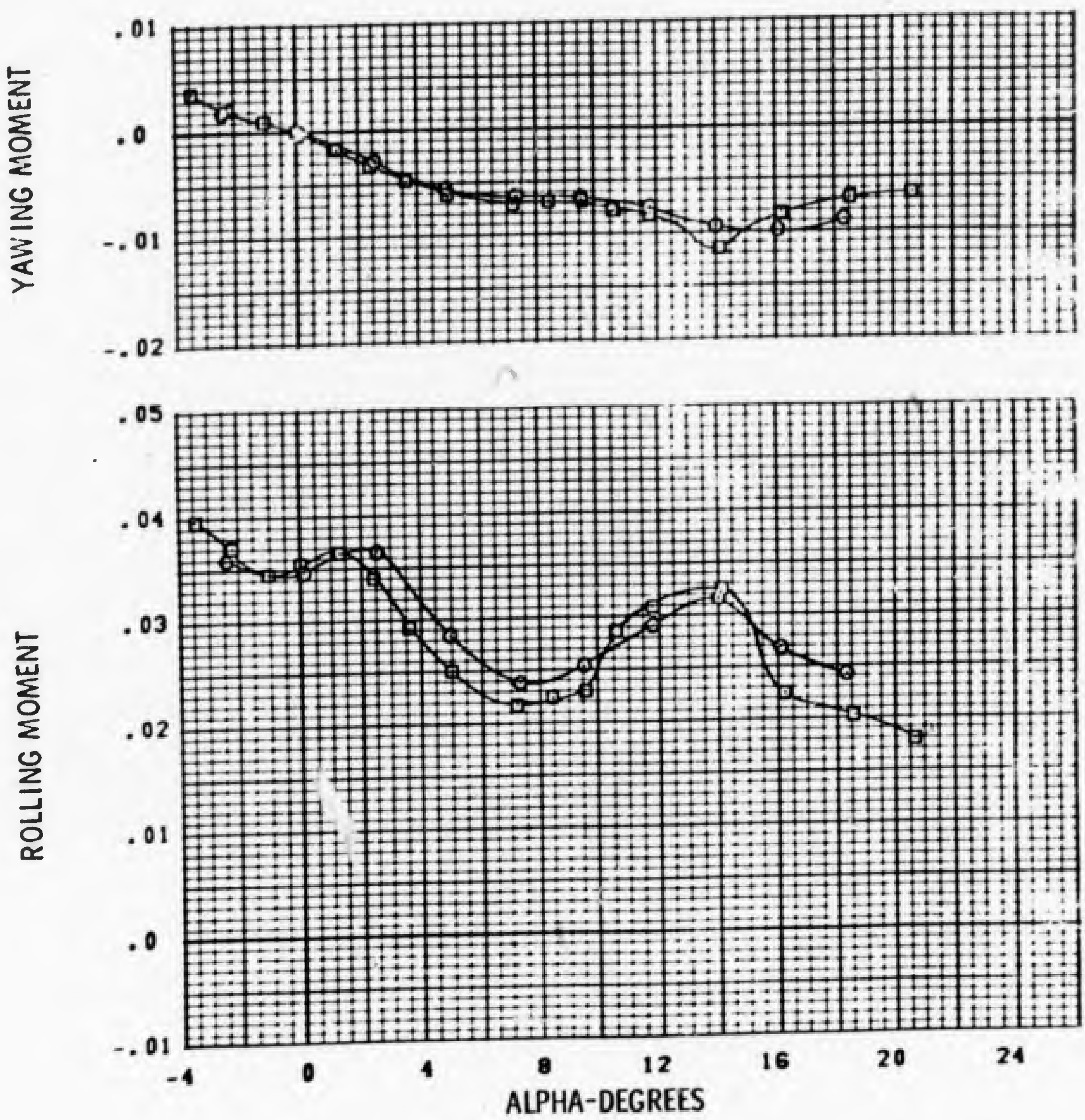
SYM	TEST	PART	L.E.	(L/R)	AILERON	(L/R)
○	PWT 4T TC-043	216	K1	0/0	MID	20/-20
□	PWT 4T TC-043	414	K1	0/0	MID	20/-20
▲	PWT 16T TF-216	10	K1	0/0	MID	20/-20

FIGURE 107c LEDE, MID AILERONS, COMPARISONS BETWEEN PWT 4T AND 16T, M = 1.2



SYM	TEST	PART	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	425	K1 10/0	MID 20/-20
⊡	PWT 16T TF-216	31	K1 10/0	MID 20/-20

FIGURE 108 LEDE, DIFFERENTIAL L.E.FLAP AND MID AILERONS
COMPARISON BETWEEN PWT 4T AND 16T M = 0.9



SYM	TEST	PART	L.E. (L/R)		AILERON (L/R)
O	PWT 4T TC-043	513	K1	10/0	3 SEGM. 20/-20
□	PWT 16T TF-216	68	K1	10/0	3 SEGM. 20/-20

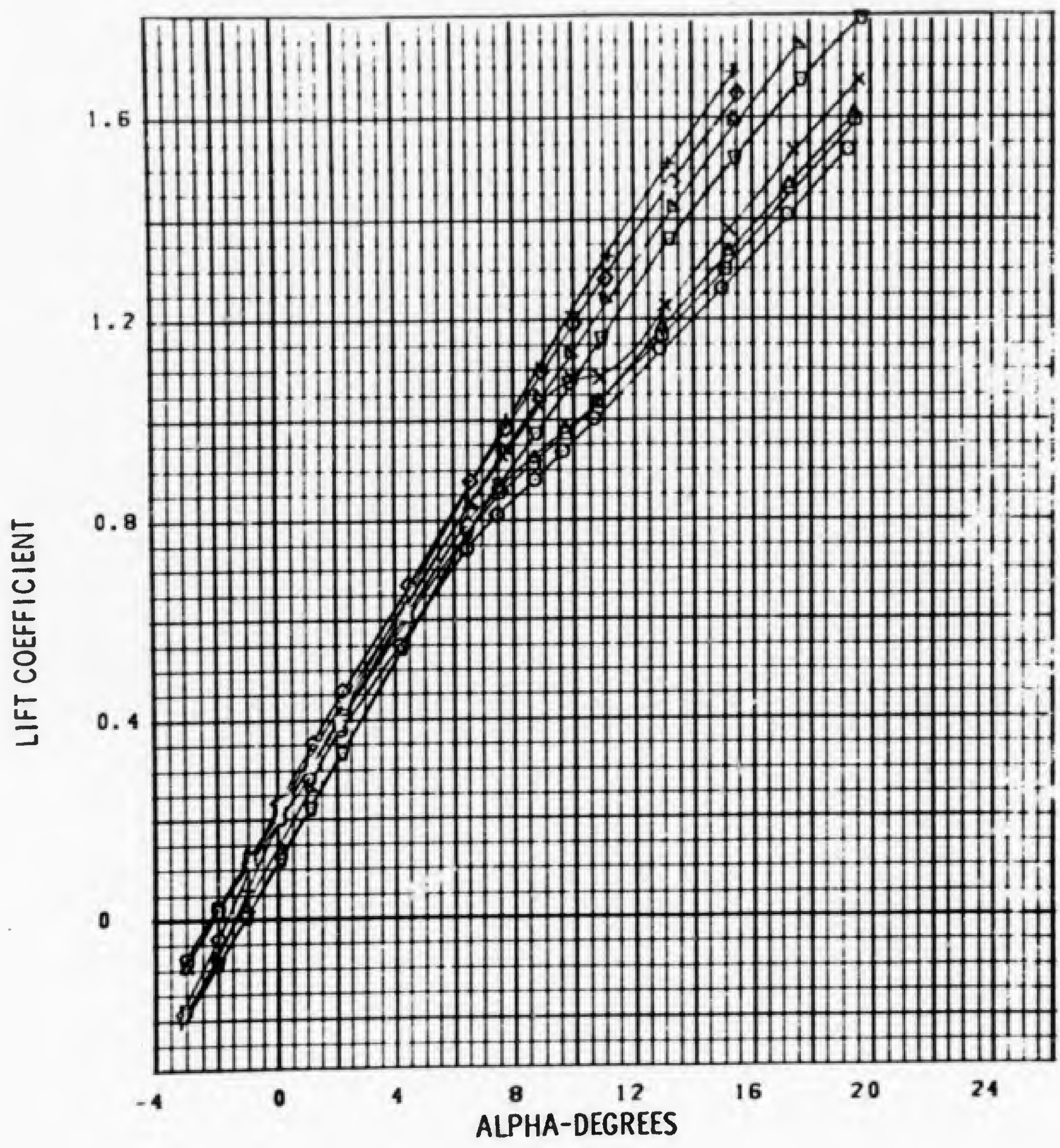
FIGURE 109 LEDE. DIFFERENTIAL L.E. FLAP AND EXTENDED AILERONS
COMPARISON BETWEEN PWT 4T AND 16T M = 0.9

APPENDIX IV - FORCE AND MOMENT COMPARISONS SYMMETRICAL CONFIGURATIONS

A complete set of comparison plots are presented in this appendix which show the effect of symmetrical configuration test variables on the longitudinal aerodynamic characteristics of the LEDE test configuration. These plots are presented in the same order as the discussion of symmetrical configuration effects (Section VI) and cover the complete range of conditions tested. Both the basic force data and incremental plots are shown for each configuration.

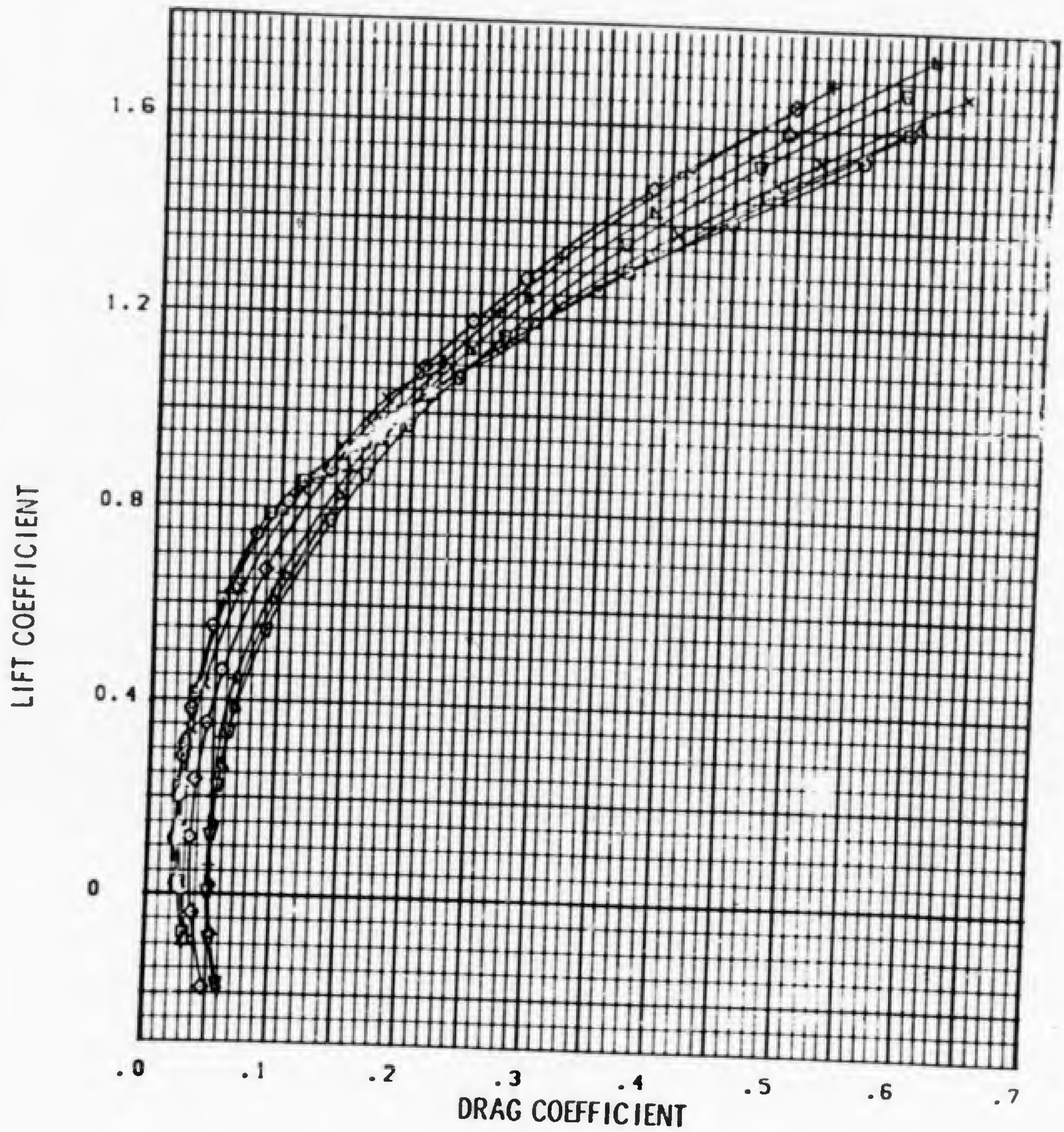
1. LEDE CONFIGURATION LONGITUDINAL CHARACTERISTICS

The lift, drag, and pitching moment characteristics of the basic configuration (tail-on) are presented in the following subsection. These data are from the 16T facility and were chosen as the baseline for evaluation the general characteristics of the configuration.



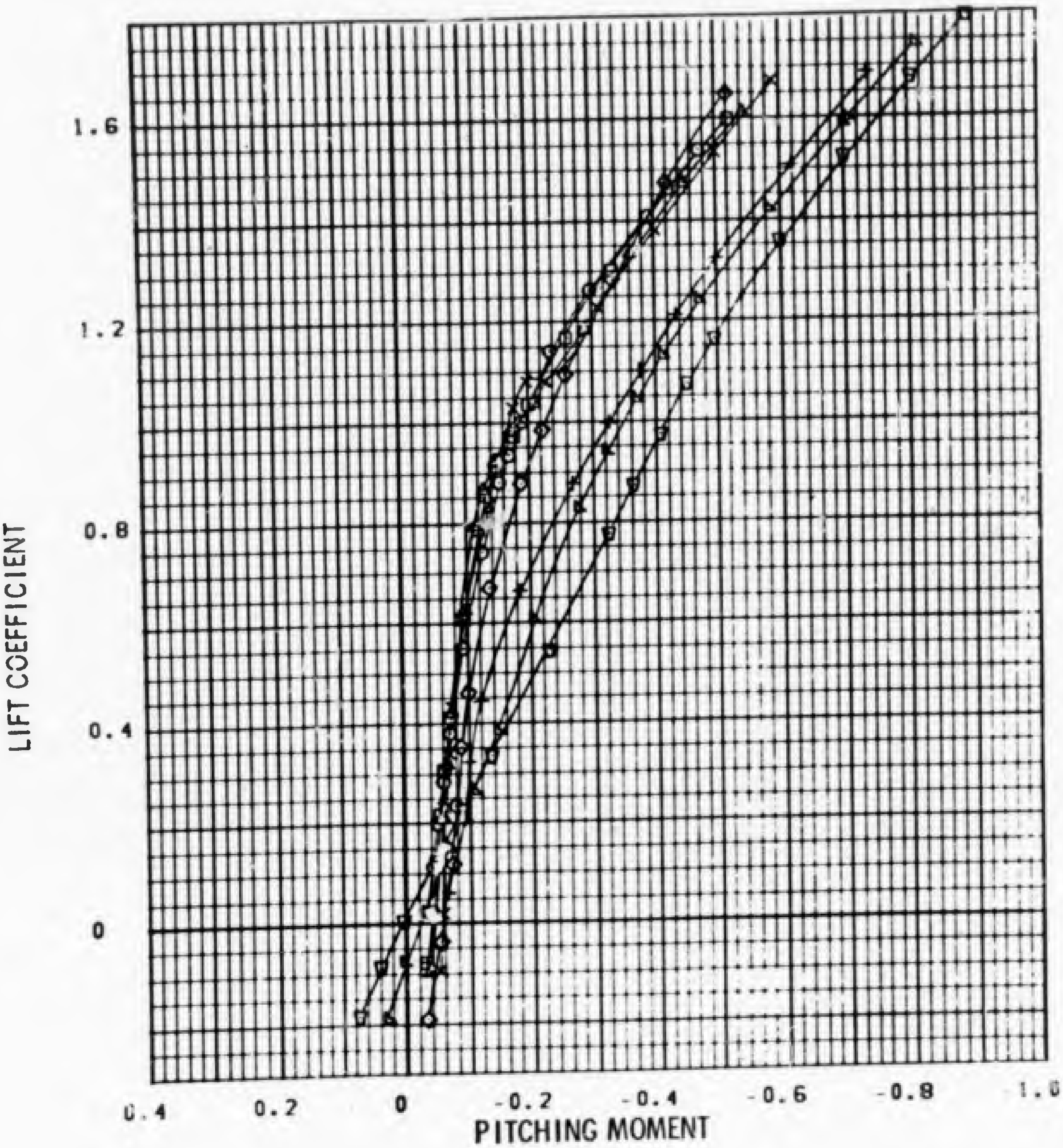
SYM	TEST	PART	MACH NO.
⊙	PWT 16T TF-216	39	0.70
⊡	PWT 16T TF-216	40	0.80
▲	PWT 16T TF-216	46	0.85
×	PWT 16T TF-216	47	0.90
◈	PWT 16T TF-216	42	0.95
+	PWT 16T TF-216	43	1.00
◣	PWT 16T TF-216	44	1.10
▽	PWT 16T TF-216	45	1.20

FIGURE 110 MACH NUMBER EFFECTS ON LEDE CLEAN WING
RN/FT = 3.0 MILLION



SYM	TEST	PART	MACH NO.
⊙	PWT 16T TF 216	39	0.70
⊡	PWT 16T TF-216	40	0.80
▲	PWT 16T TF-216	46	0.85
×	PWT 16T TF-216	47	0.90
◇	PWT 16T TF-216	42	0.95
+	PWT 16T TF-216	43	1.00
◣	PWT 16T TF-216	44	1.10
▽	PWT 16T TF-216	45	1.20

FIGURE 110 MACH NUMBER EFFECTS ON LEDE CLEAN WING
RN/FT = 3.0 MILLION

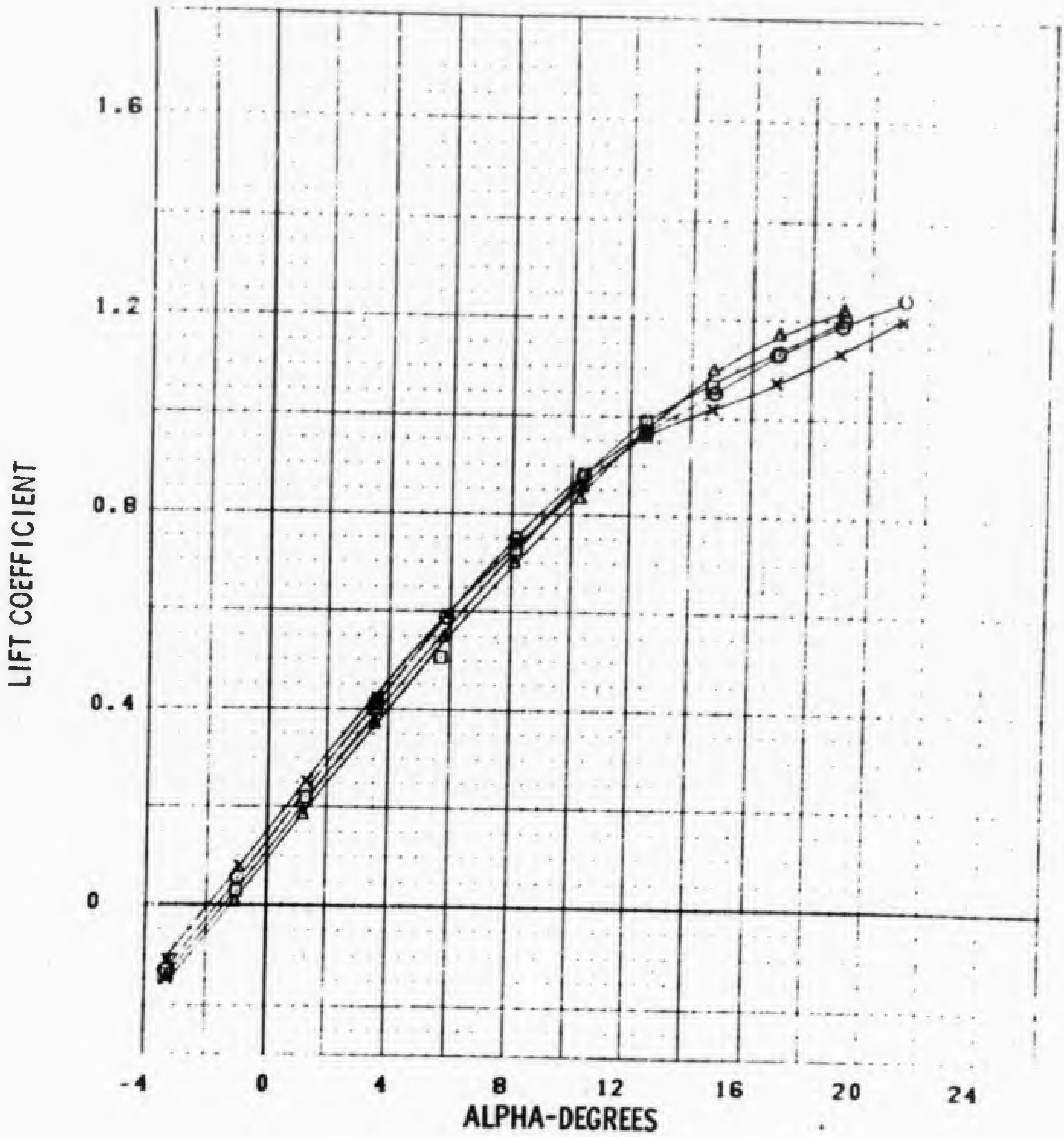


SYM	TEST	PART	MACH NO.
⊙	PWT 16T TF-216	39	0.70
⊡	PWT 16T TF-216	40	0.80
▲	PWT 16T TF-216	46	0.85
×	PWT 16T TF-216	47	0.90
◇	PWT 16T TF-216	42	0.95
+	PWT 16T TF-216	43	1.00
◣	PWT 16T TF-216	44	1.10
▽	PWT 16T TF-216	45	1.20

FIGURE 110 MACH NUMBER EFFECTS ON LEDF CLEAN WING
RN/FT = 3.0 MILLION

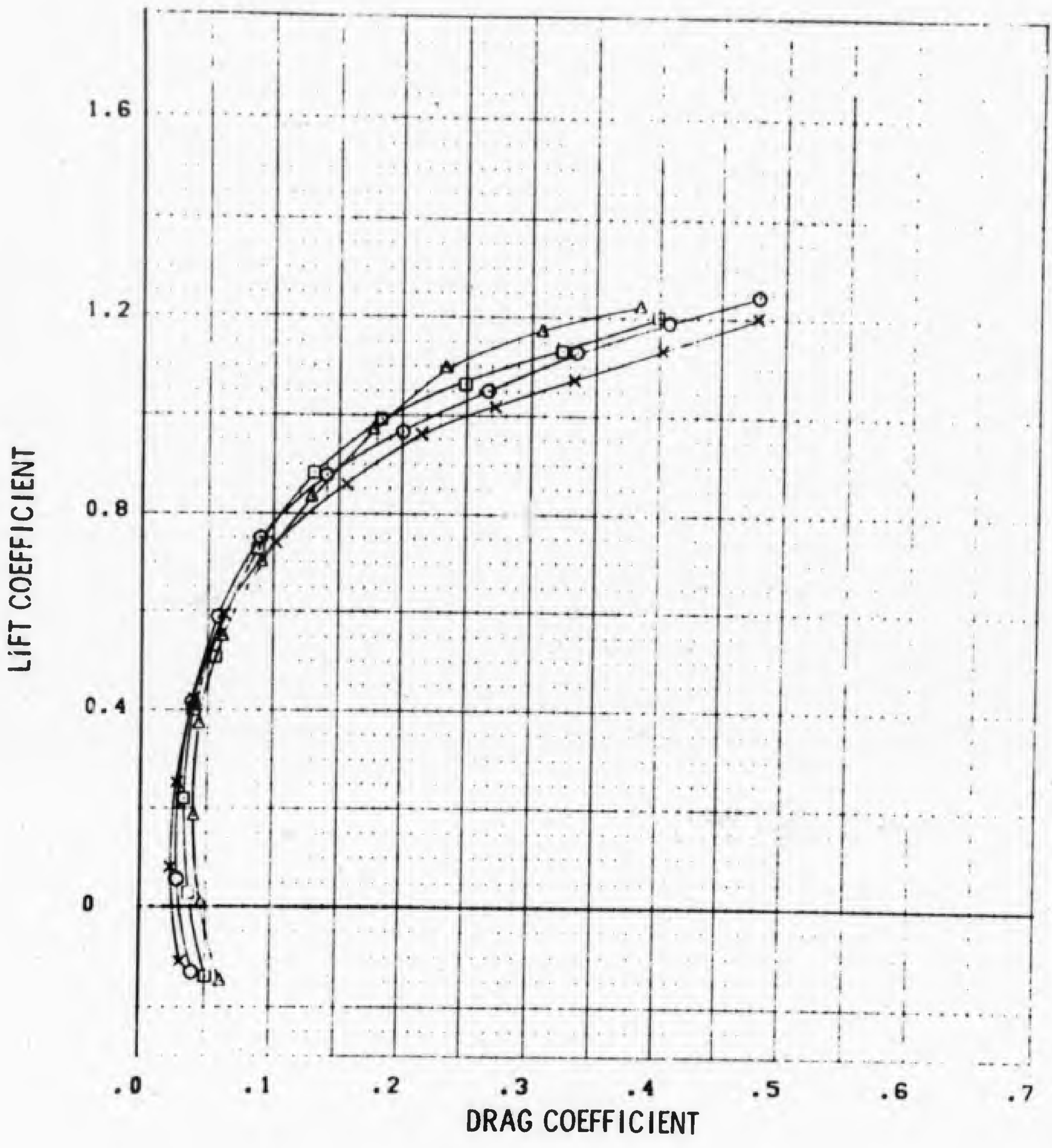
2. LEADING EDGE FLAP EFFECTS

The effects of symmetrical leading edge flap deflection on the aerodynamic characteristics of the LEDE configuration are presented in this subsection. Comparison plots for the configuration with the tail off are presented first, followed by the tail-on plots.



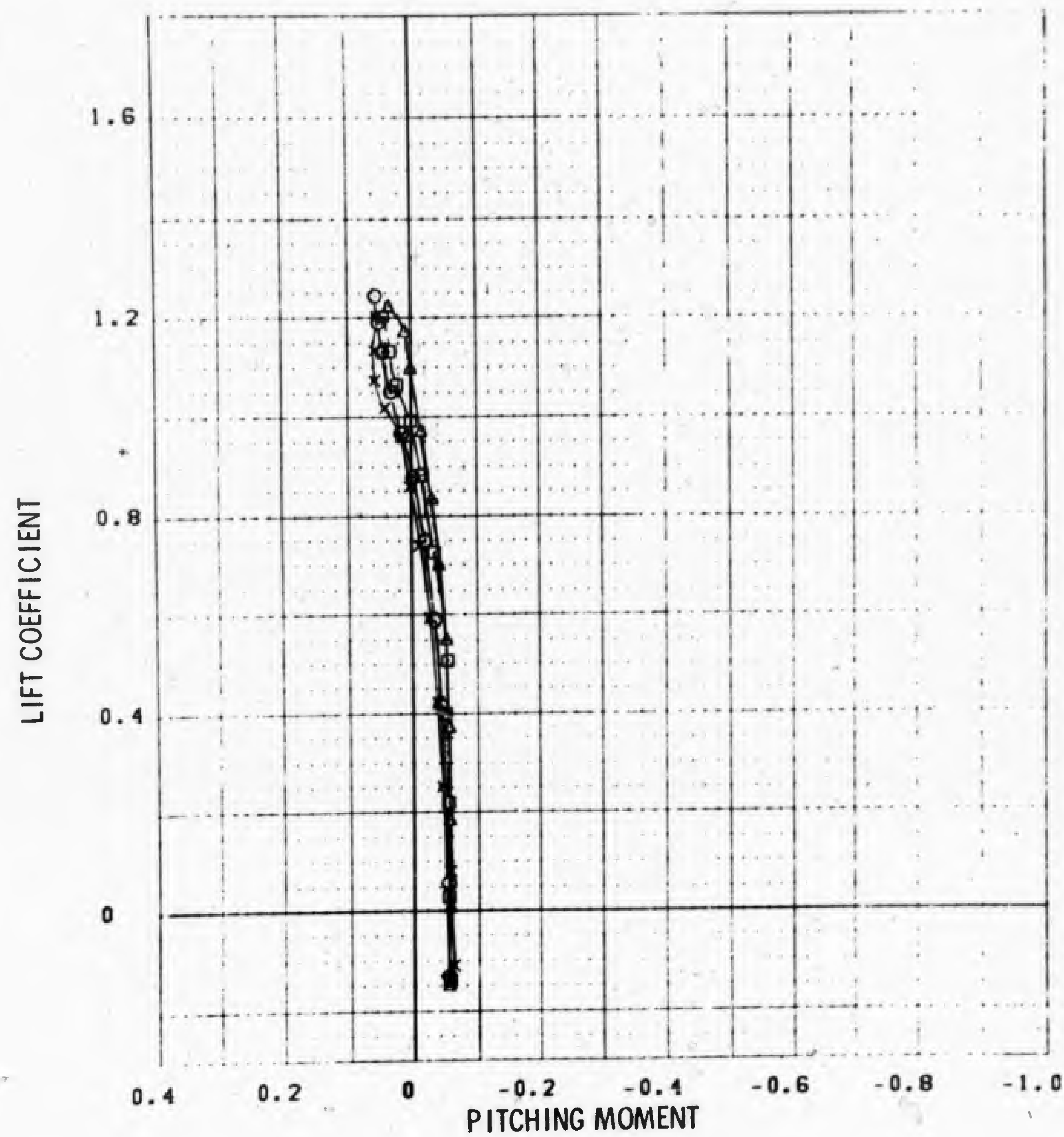
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	42	K1 5/5
⊡	PWT 4T TC-043	49	K1 10/10
△	PWT 4T TC-043	56	K1 15/15
×	PWT 4T TC-043	32	K1 0/0

FIGURE 111a SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 0.7



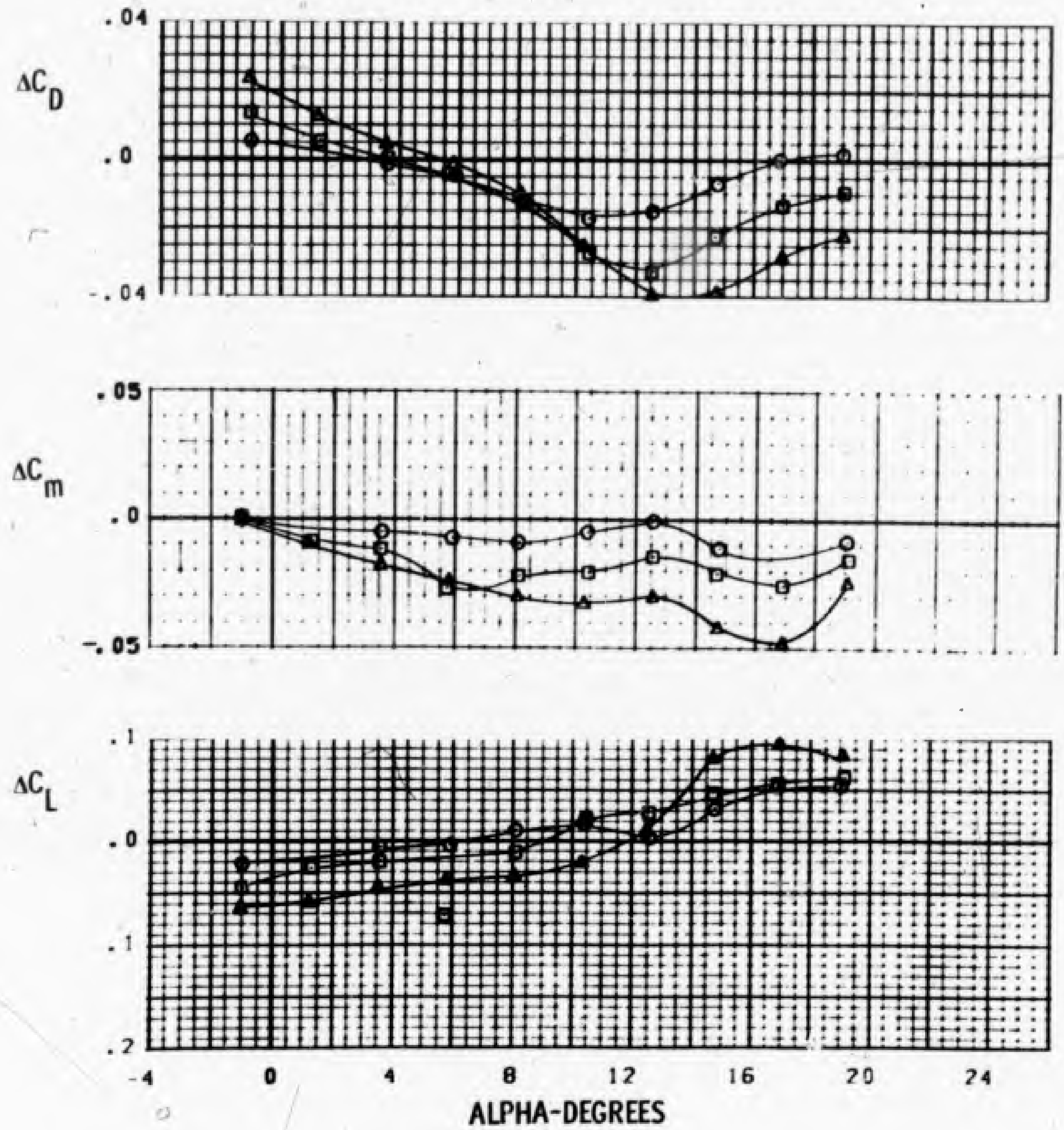
SYM	TEST	PART	L.E. (L/R)
○	PWT 4T TC-043	42	K1 5/5
□	PWT 4T TC-043	49	K1 10/10
Δ	PWT 4T TC-043	56	K1 15/15
×	PWT 4T TC-043	32	K1 0/0

FIGURE 111a SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 0.7



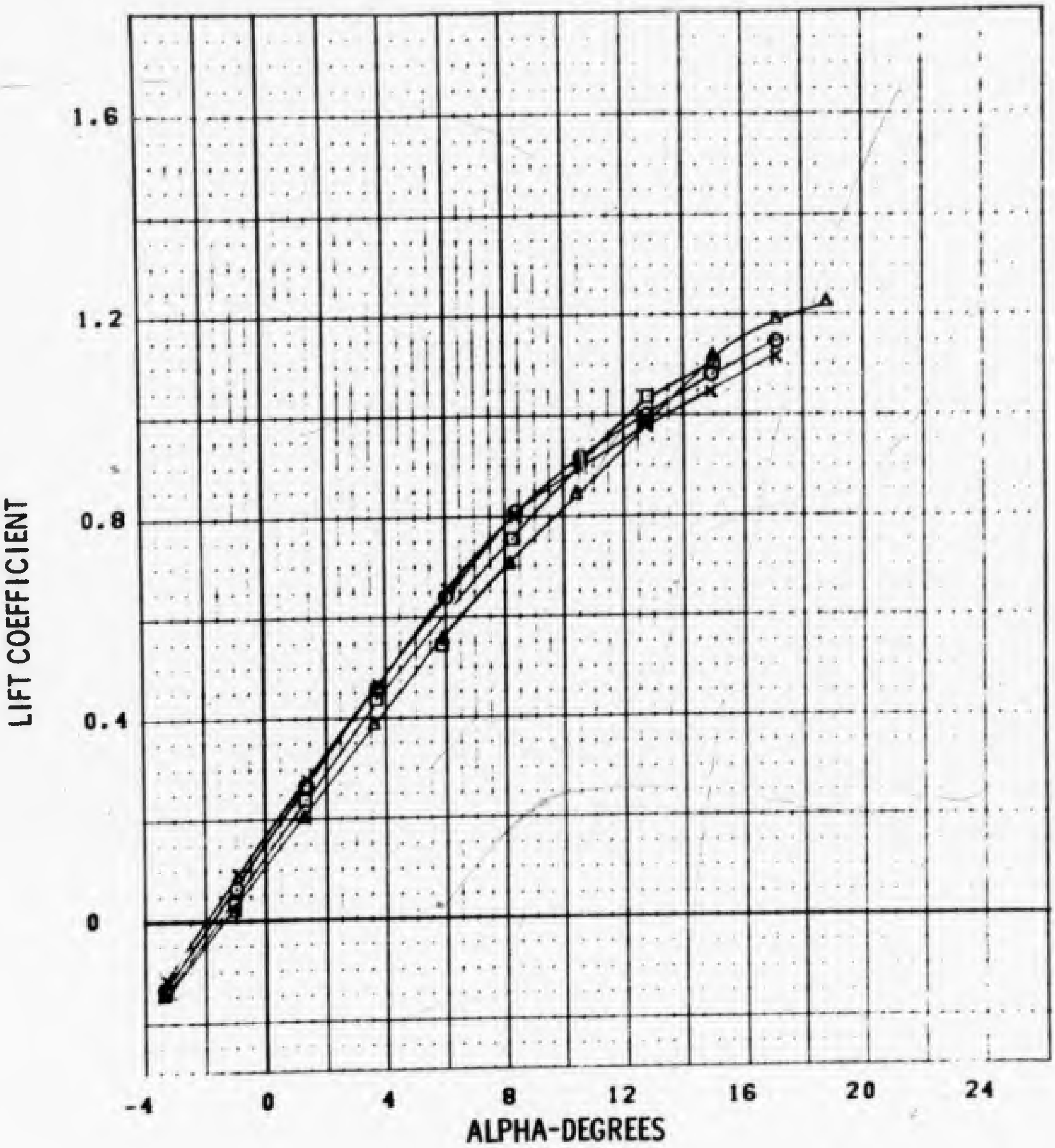
SYM	TEST	PART	L.E. (L/R)
○	PWT 4T TC-043	42	K1 5/5
□	PWT 4T TC-043	49	K1 10/10
△	PWT 4T TC-043	56	K1 15/15
×	PWT 4T TC-043	32	K1 0/0

FIGURE 111a SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 0.7



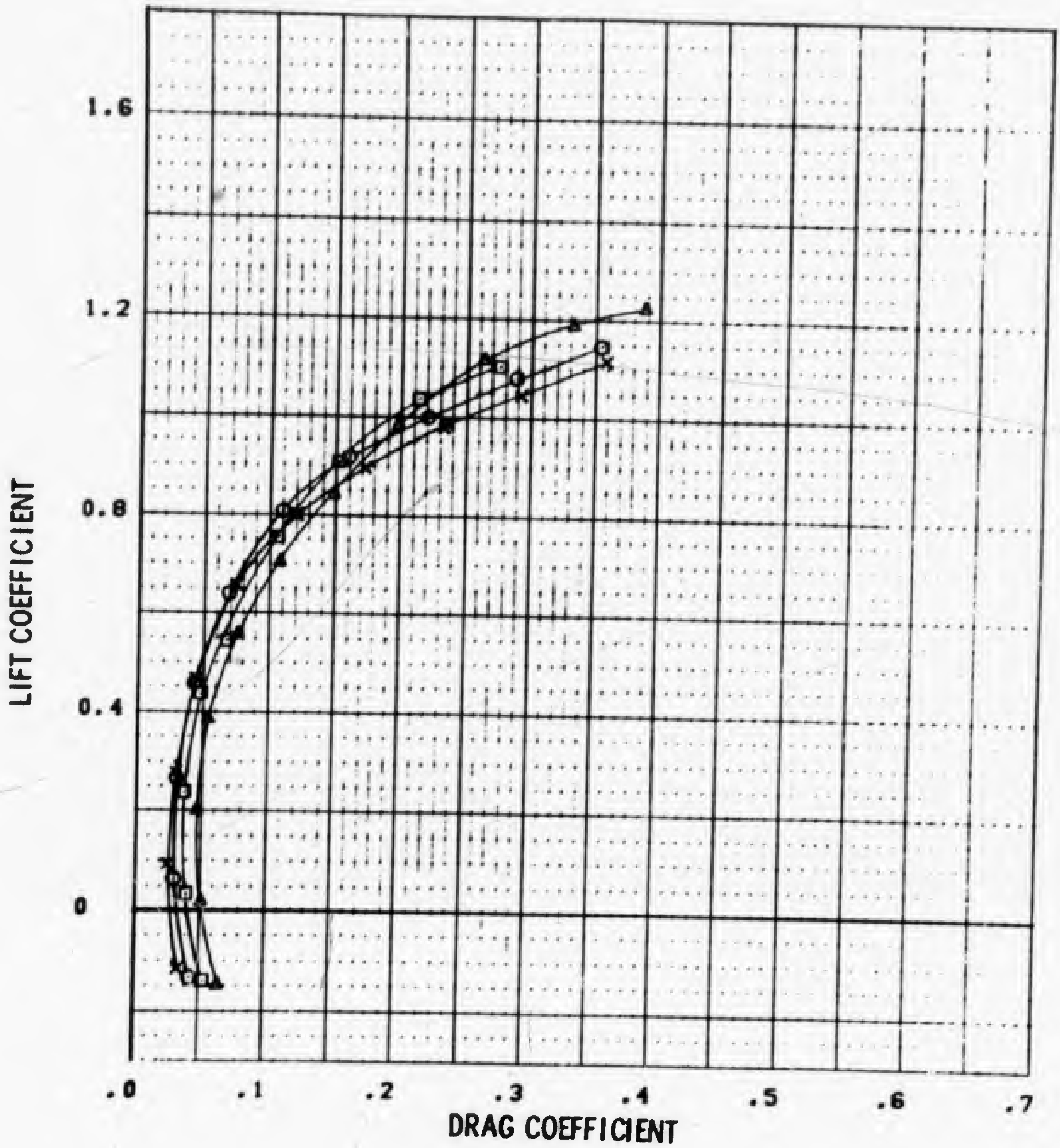
SYM	TEST	INCREMENT	[illegible]
⊙	PWT 4T TC 043	PN 42 - PN 32	[illegible] 5/5
⊡	PWT 4T TC 043	PN 49 - PN 32	[illegible] 10/10
▲	PWT 4T TC 043	PN 56 - PN 32	[illegible] 15/15

FIGURE 111a SYMMETRIC LEADING EDGE FLAP EFFECTS. [illegible]
M = 0.7



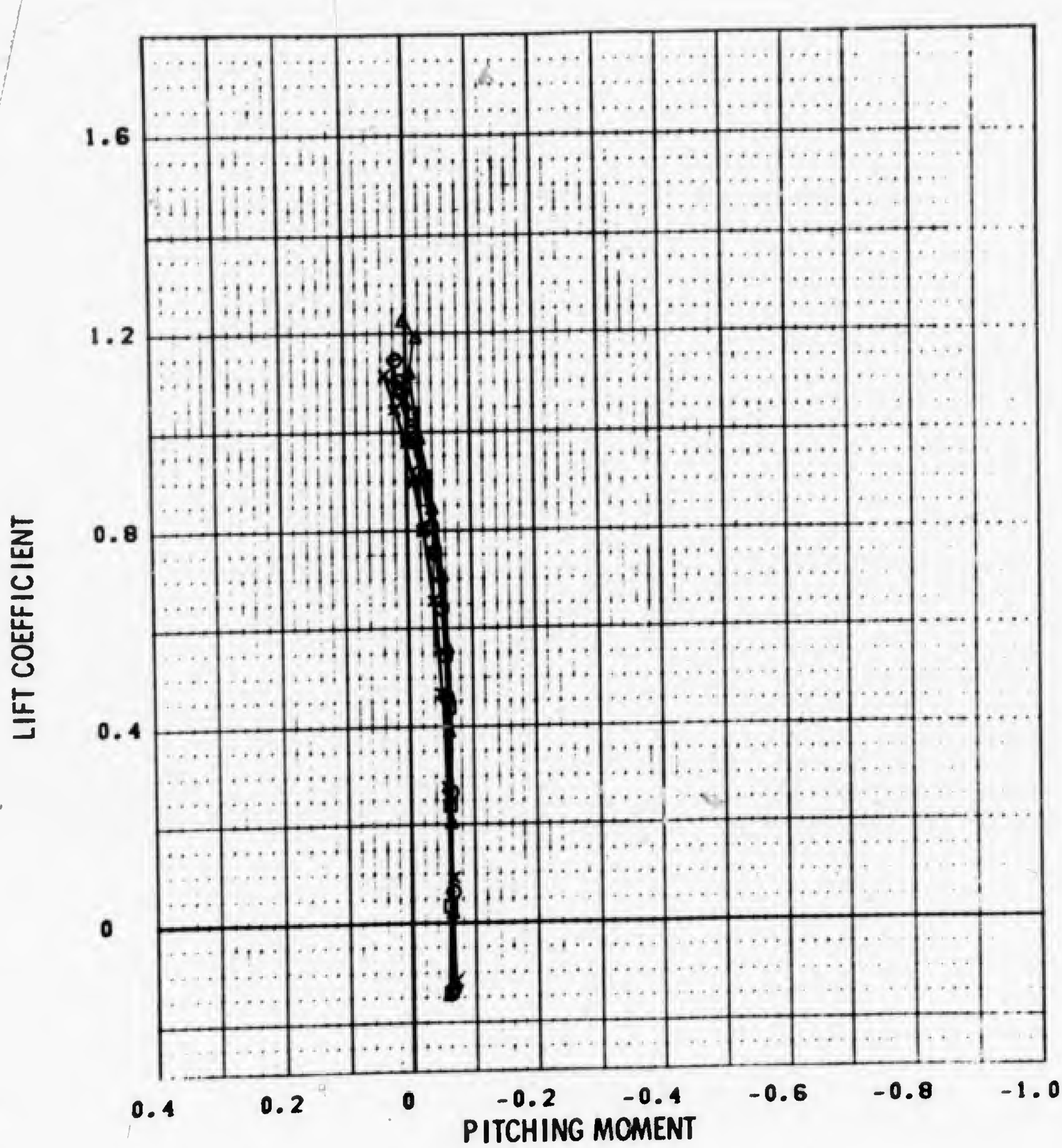
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	38	K1 5/5
⊡	PWT 4T TC-043	48	K1 10/10
▲	PWT 4T TC-043	55	K1 15/15
×	PWT 4T TC-043	31	K1 0/0

FIGURE 111b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 0.8



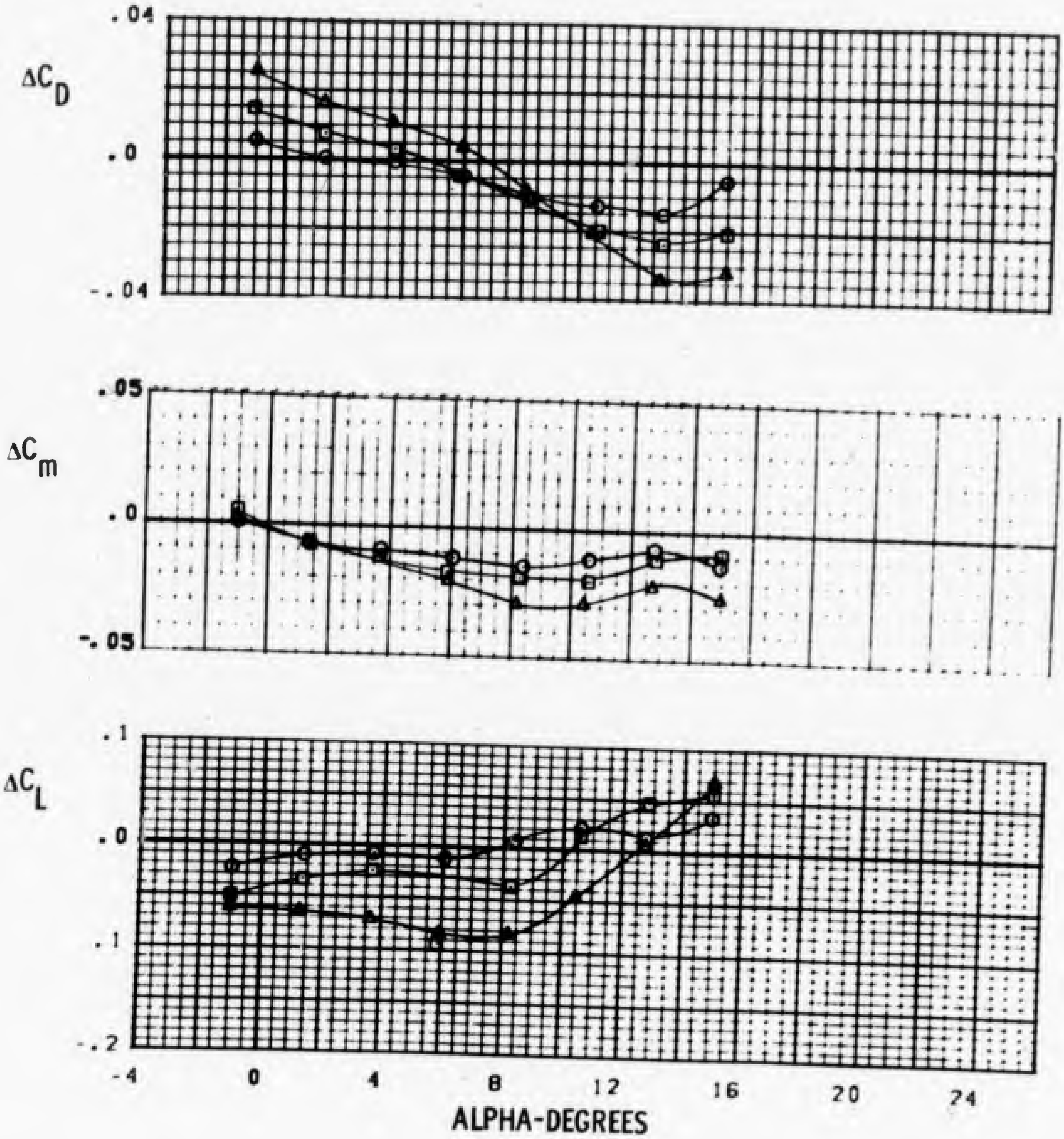
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	38	K1 5/5
⊡	PWT 4T TC-043	48	K1 10/10
▲	PWT 4T TC-043	55	K1 15/15
×	PWT 4T TC-043	31	K1 0/0

FIGURE 111b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 0.8



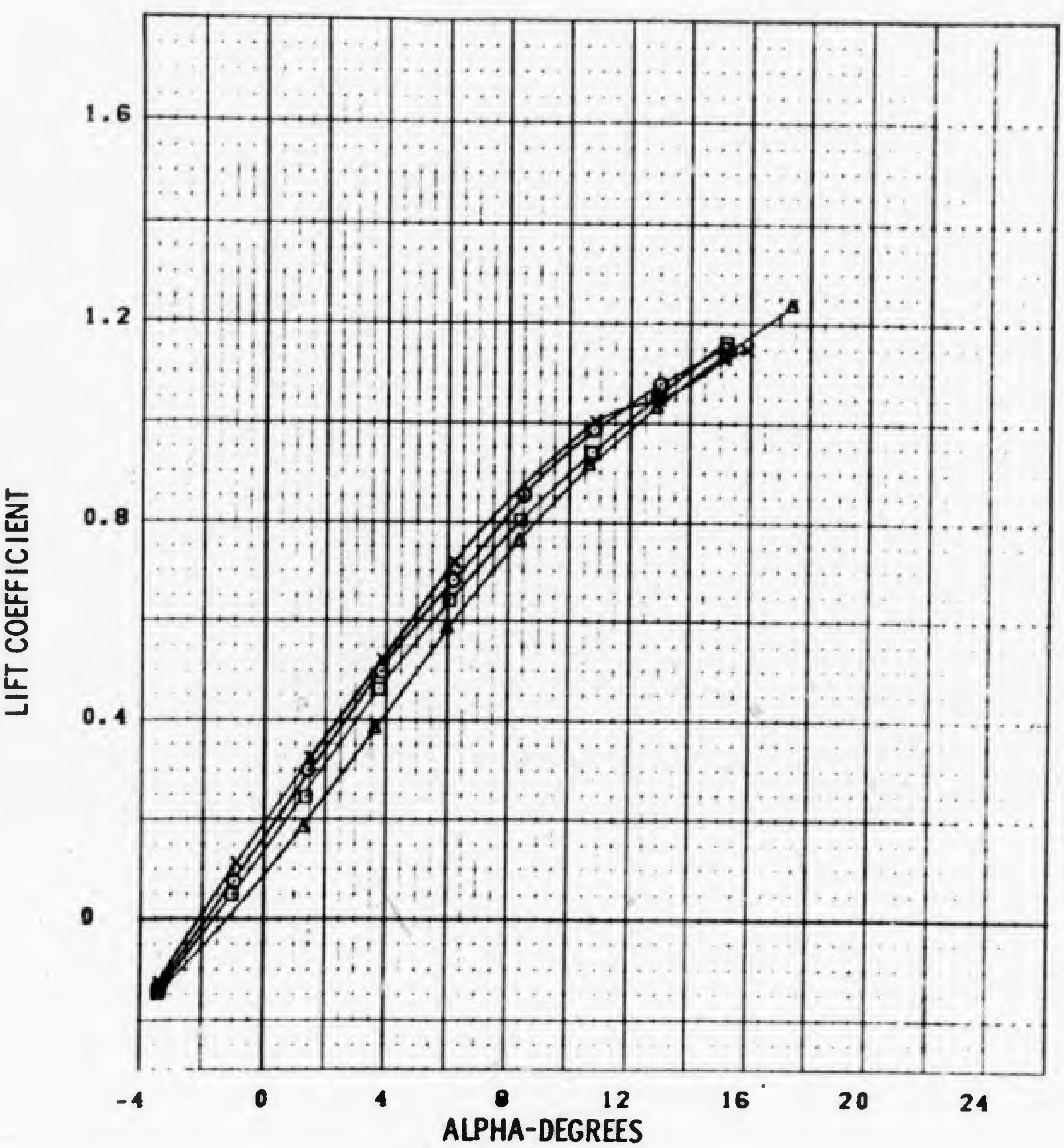
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	38	K1 5/5
⊡	PWT 4T TC-043	48	K1 10/10
▲	PWT 4T TC-043	55	K1 15/15
×	PWT 4T TC-043	31	K1 0/0

FIGURE 111b SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 0.8



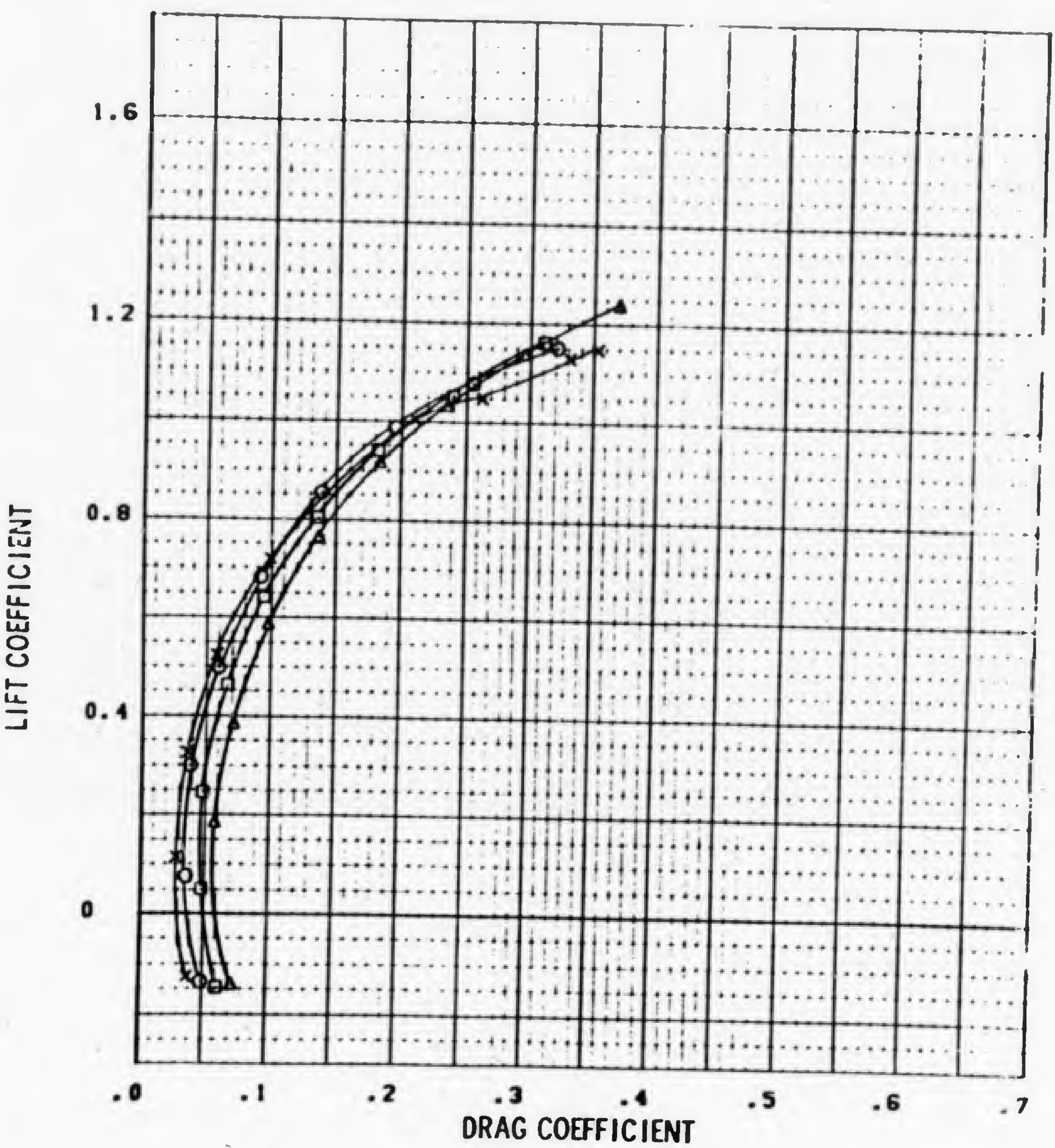
SYM	TEST	INCREMENT		[illegible]
⊙	PWT 4T TC 043	PN 38	PN 31	K: 5/5
⊡	PWT 4T TC-043	PN 48	PN 31	K: 10/10
▲	PWT 4T TC-043	PN 55	PN 31	K: 15/15

FIGURE 111b SYMMETRIC LEADING EDGE FLAP EFFECTS. [illegible] OFF
M = 0.8



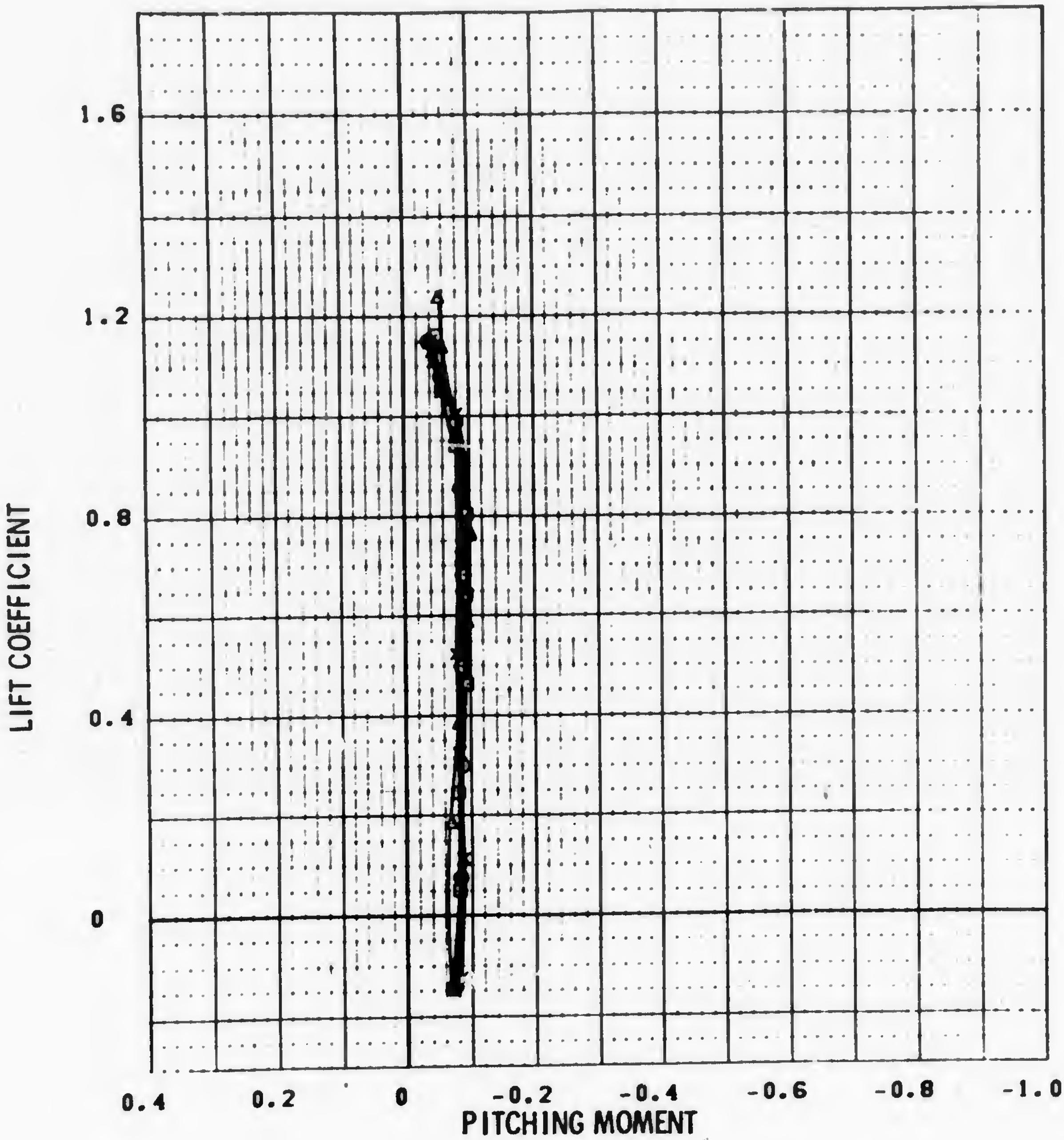
SYM	TEST	PART	L.E. (L/R)
O	PWT 4T TC-043	37	K1 5/5
□	PWT 4T TC-043	47	K1 10/10
Δ	PWT 4T TC-043	54	K1 15/15
×	PWT 4T TC-043	30	K1 0/0

FIGURE 111c SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 0.9



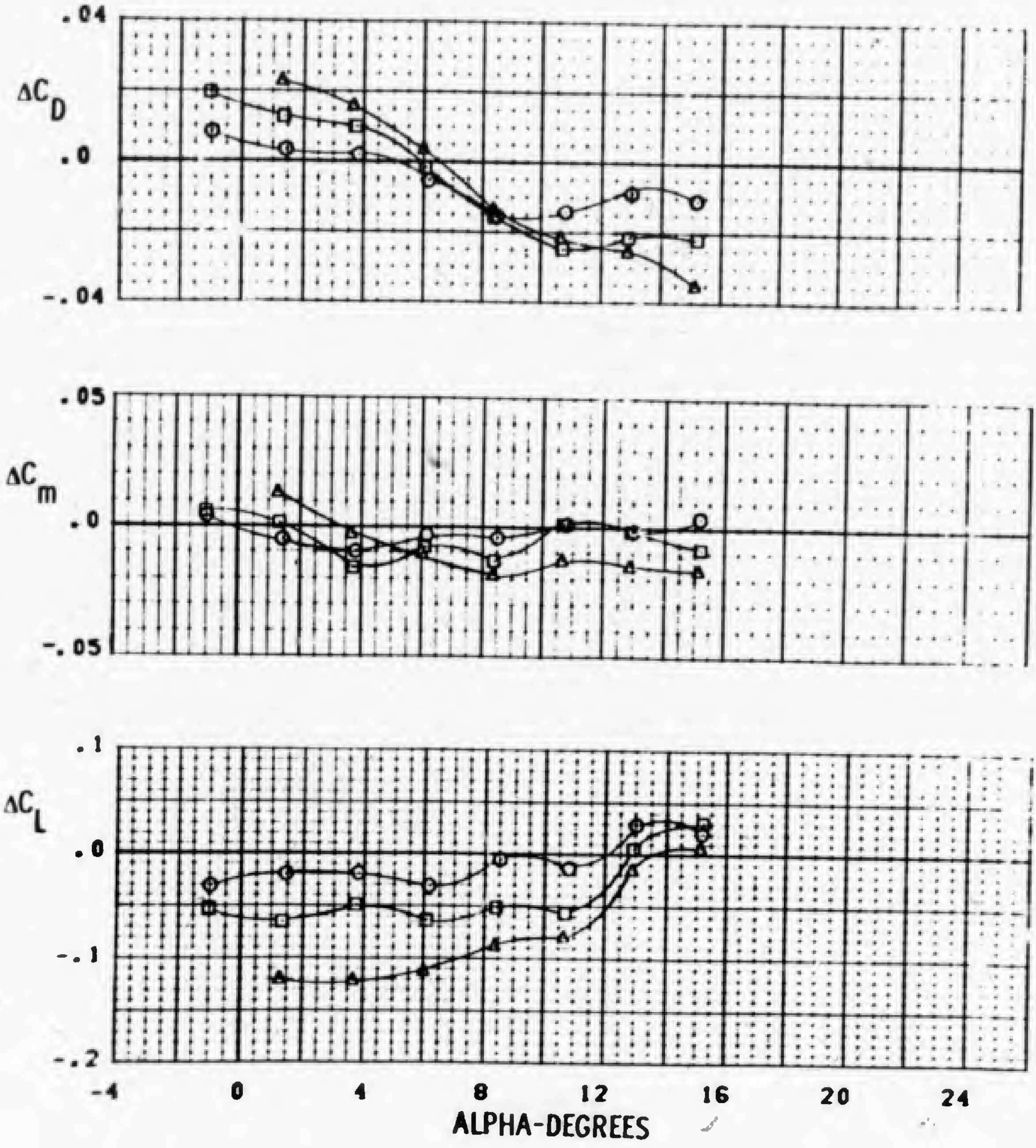
SYM	TEST	PART	L.E. (L/R)
○	PWT 4T TC-043	37	K1 5/5
□	PWT 4T TC-043	47	K1 10/10
△	PWT 4T TC-043	54	K1 15/15
×	PWT 4T TC-043	30	K1 0/0

FIGURE 111c SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 0.9



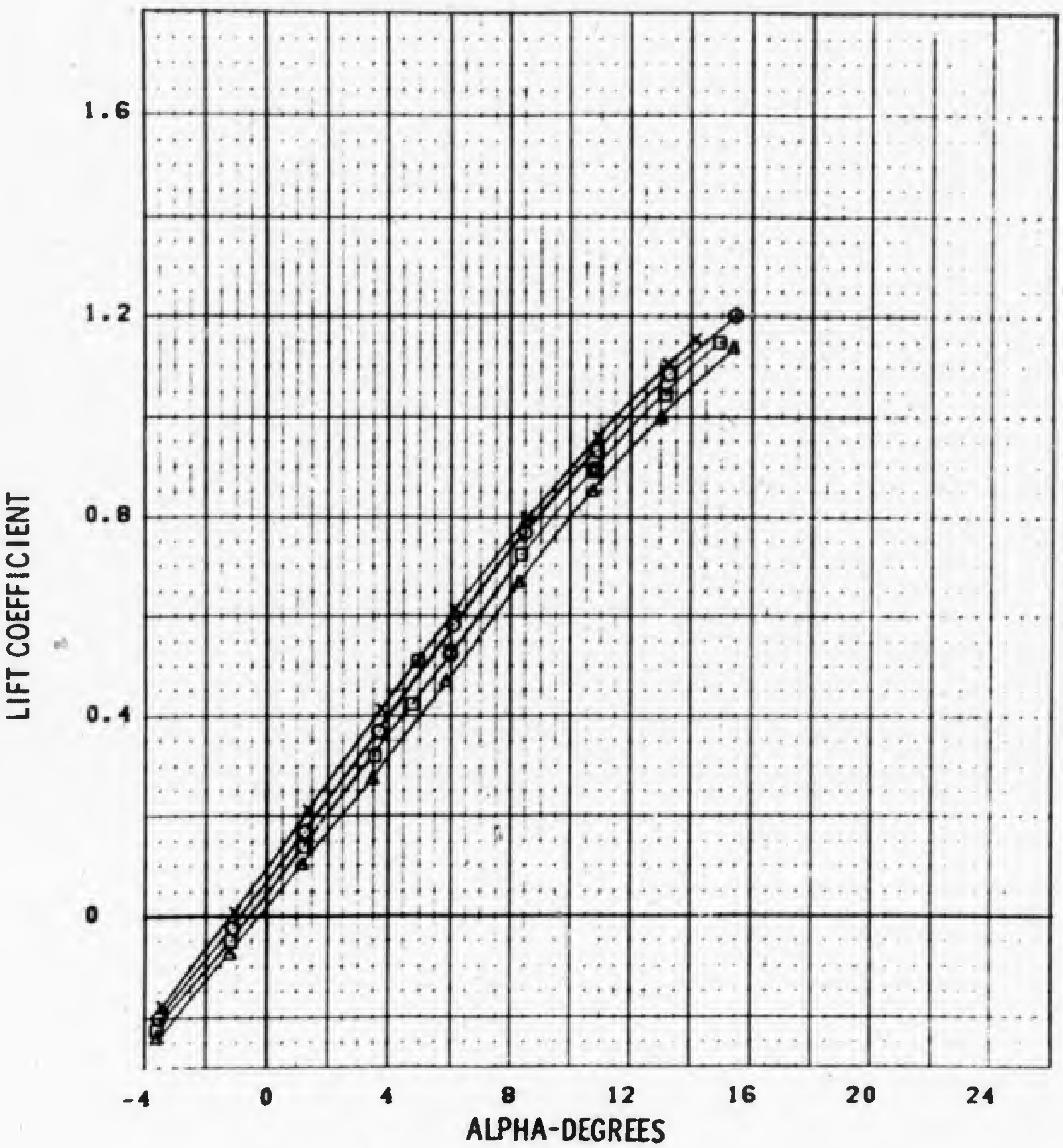
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	37	K1 5/5
⊡	PWT 4T TC-043	47	K1 10/10
△	PWT 4T TC-043	54	K1 15/15
×	PWT 4T TC-043	30	K1 0/0

FIGURE 111c SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 0.9



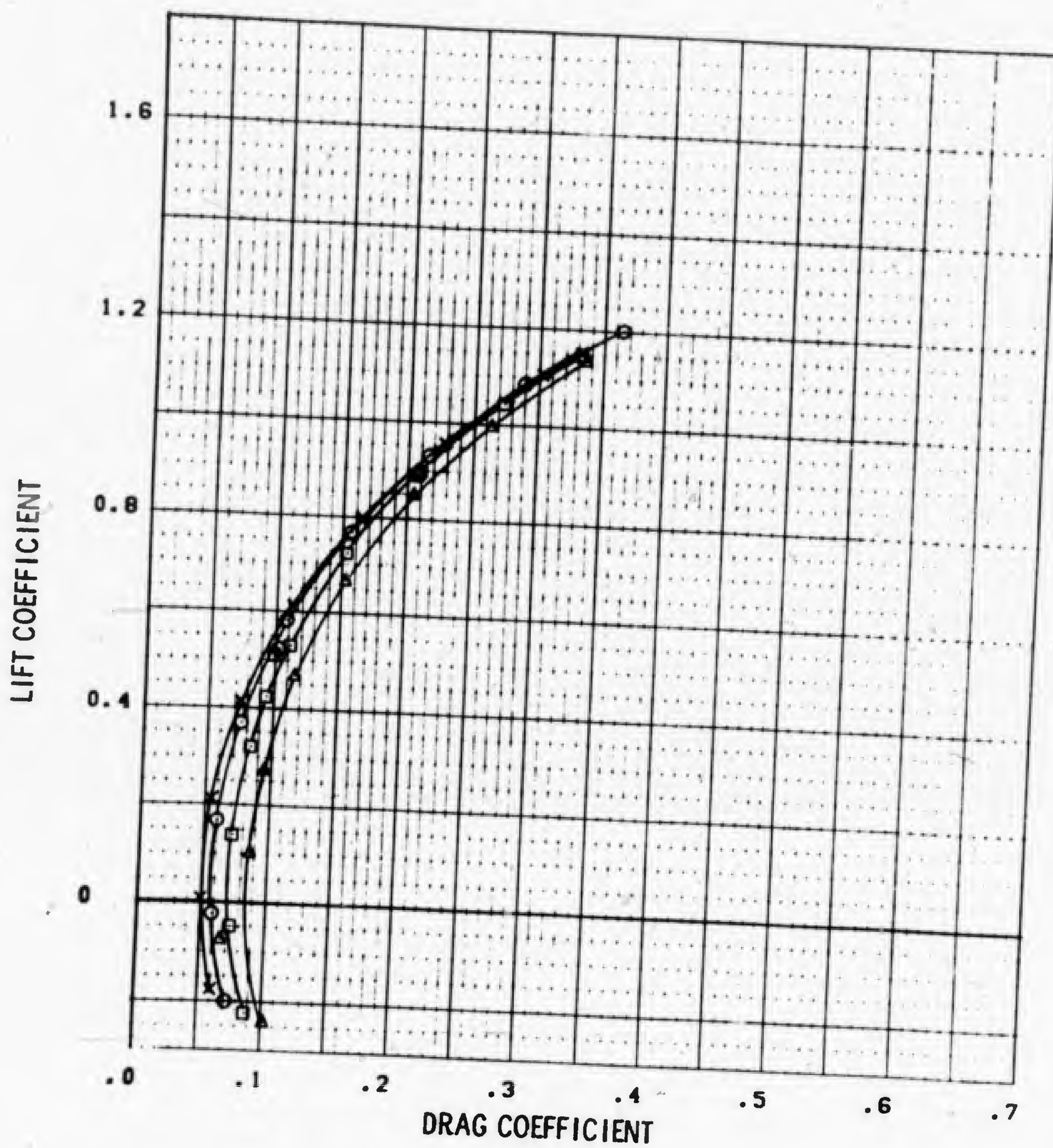
SYM	TEST	INCREMENT	L.E. (L/R)
○	PWT 4T TC-043	PN 37 - PN 30	K1 5/5
□	PWT 4T TC-043	PN 47 - PN 30	K1 10/10
△	PWT 4T TC-043	PN 54 - PN 30	K1 15/15

FIGURE 111c SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 0.9



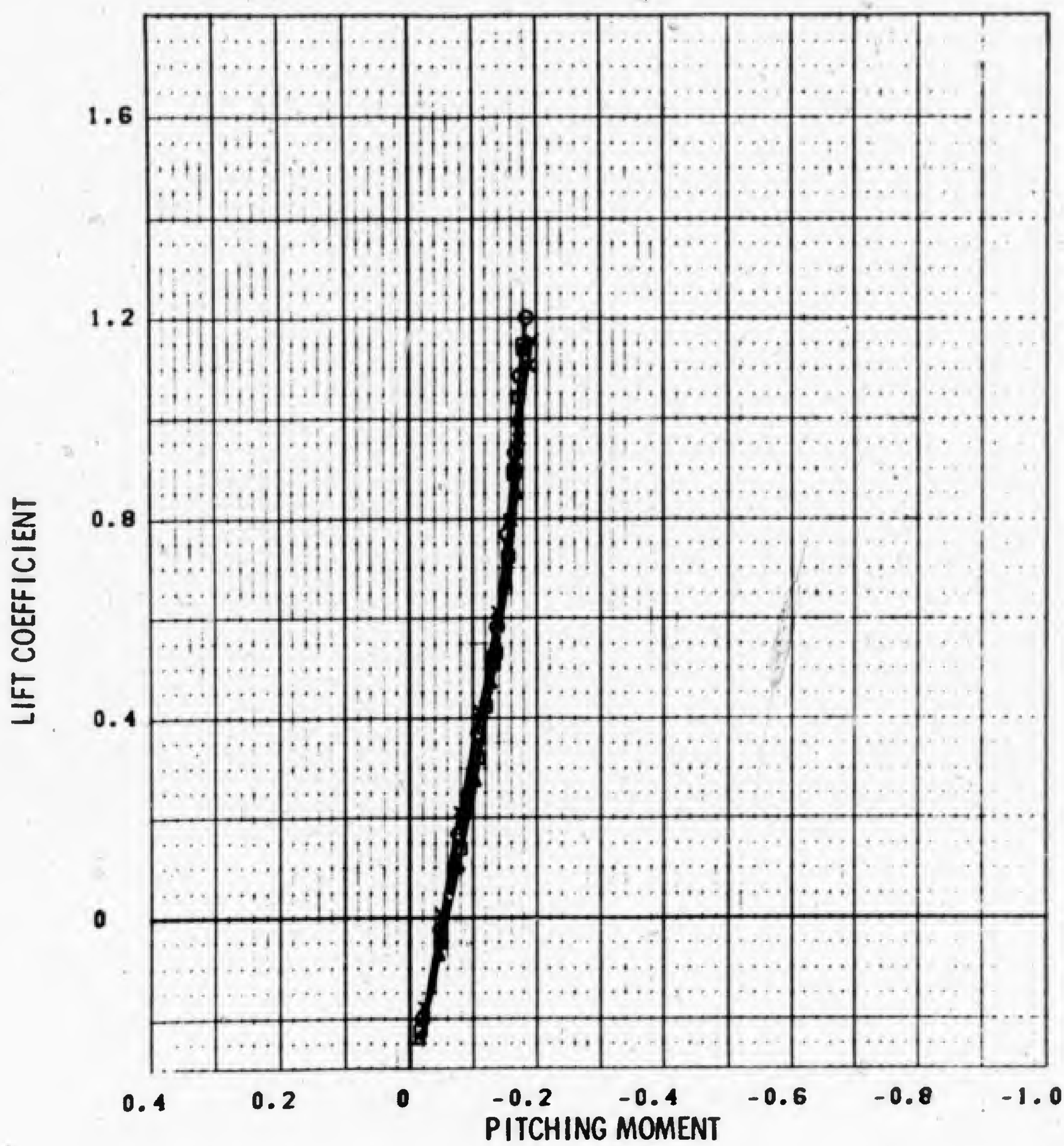
SYM	TEST	PART	L.E. (L/R)
○	PWT 4T TC-043	43	K1 5/5
□	PWT 4T TC-043	50	K1 10/10
△	PWT 4T TC-043	57	K1 15/15
×	PWT 4T TC-043	33	K1 0/0

FIGURE 111d SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 1.2



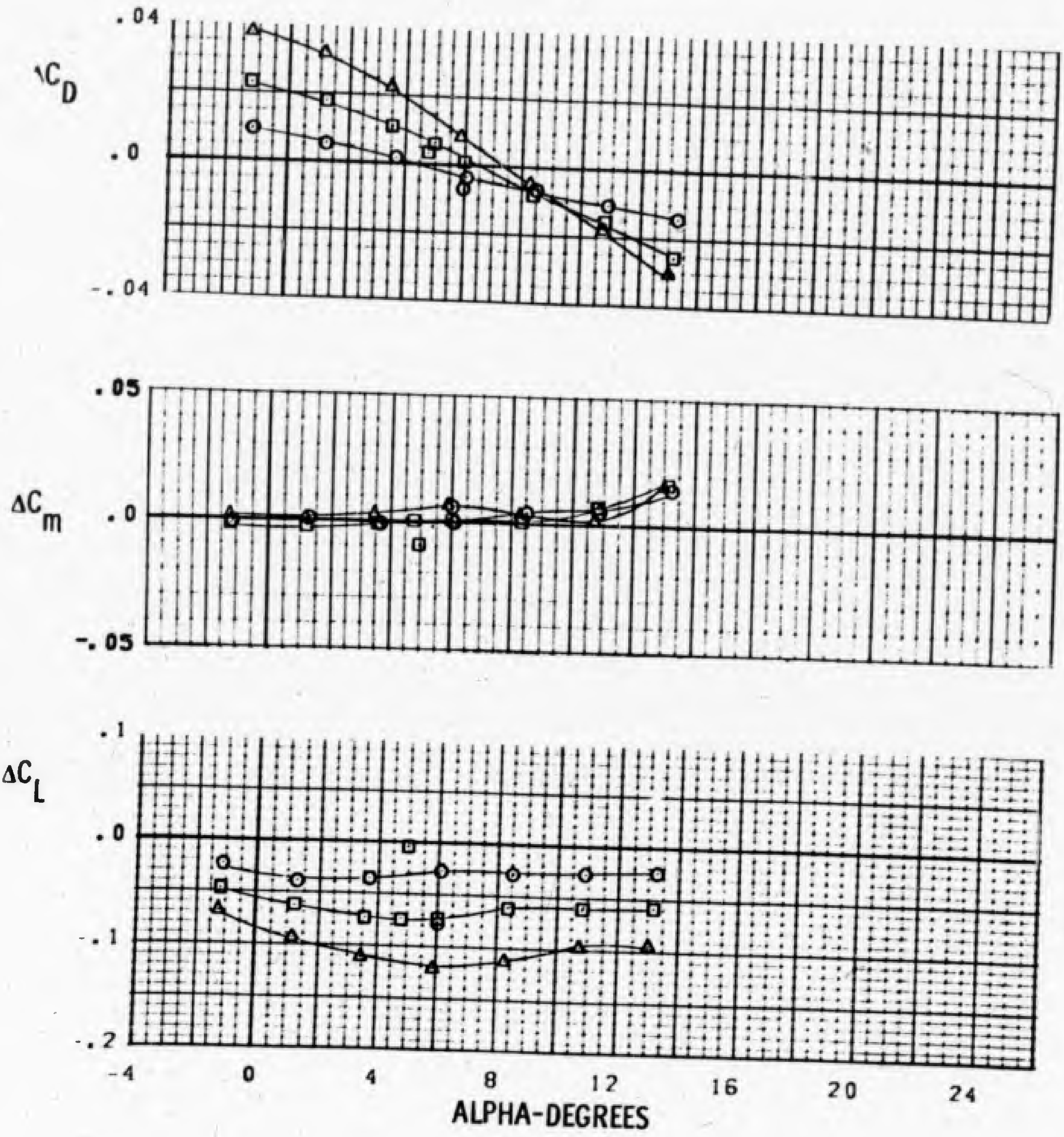
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	43	K1 5/5
⊡	PWT 4T TC-043	50	K1 10/10
△	PWT 4T TC-043	57	K1 15/15
×	PWT 4T TC-043	33	K1 0/0

FIGURE 111d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M = 1.2



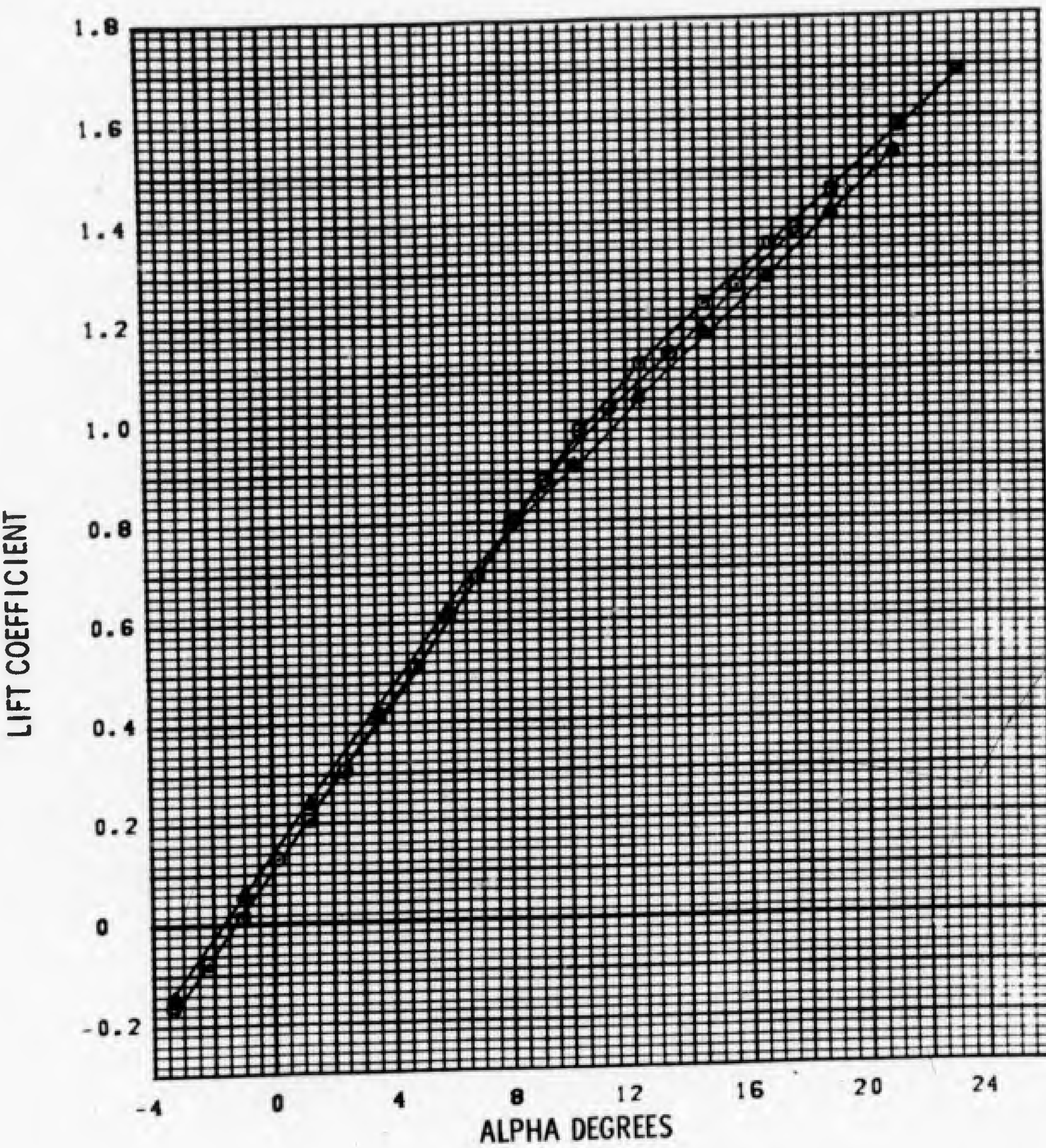
SYM	TEST		PART	L.E. (L/R)
O	PWT 4T	TC-043	43	K1 5/5
◻	PWT 4T	TC-043	50	K1 10/10
Δ	PWT 4T	TC-043	57	K1 15/15
×	PWT 4T	TC-043	33	K1 0/0

FIGURE 111d SYMMETRIC LEADING EDGE FLAP EFFECTS. H.T. OFF
M = 1.2



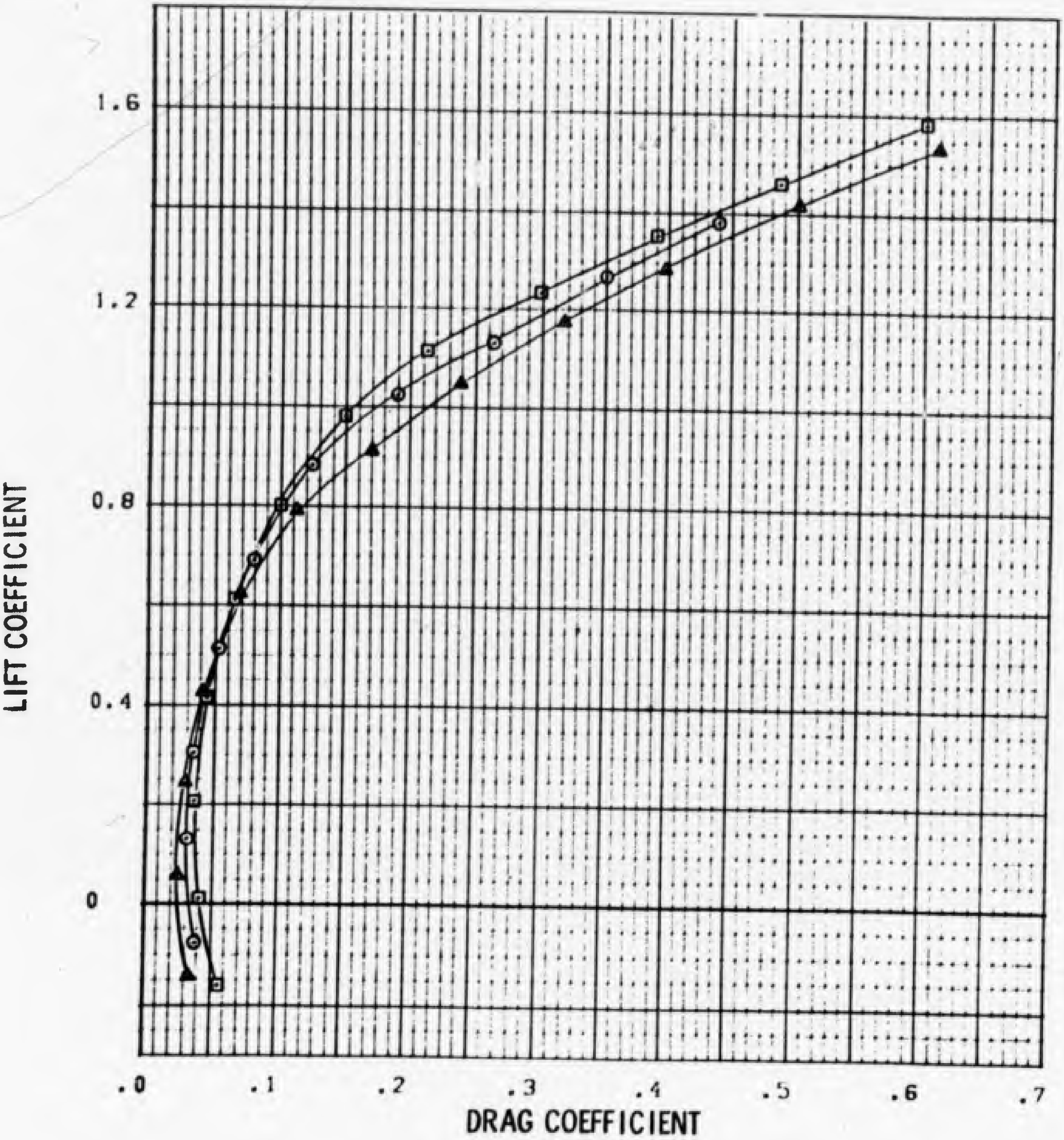
SYM	TEST		INCREMENT		L.E. (/R)
⊙	PWT 41	TC 043	PN 43	PN 33	KI 5/5
⊡	PWT 41	TC 043	PN 50	PN 33	KI 10/10
▲	PWT 41	TC 043	PN 57	PN 33	KI 15/15

FIGURE 111d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. OFF
M 1.2



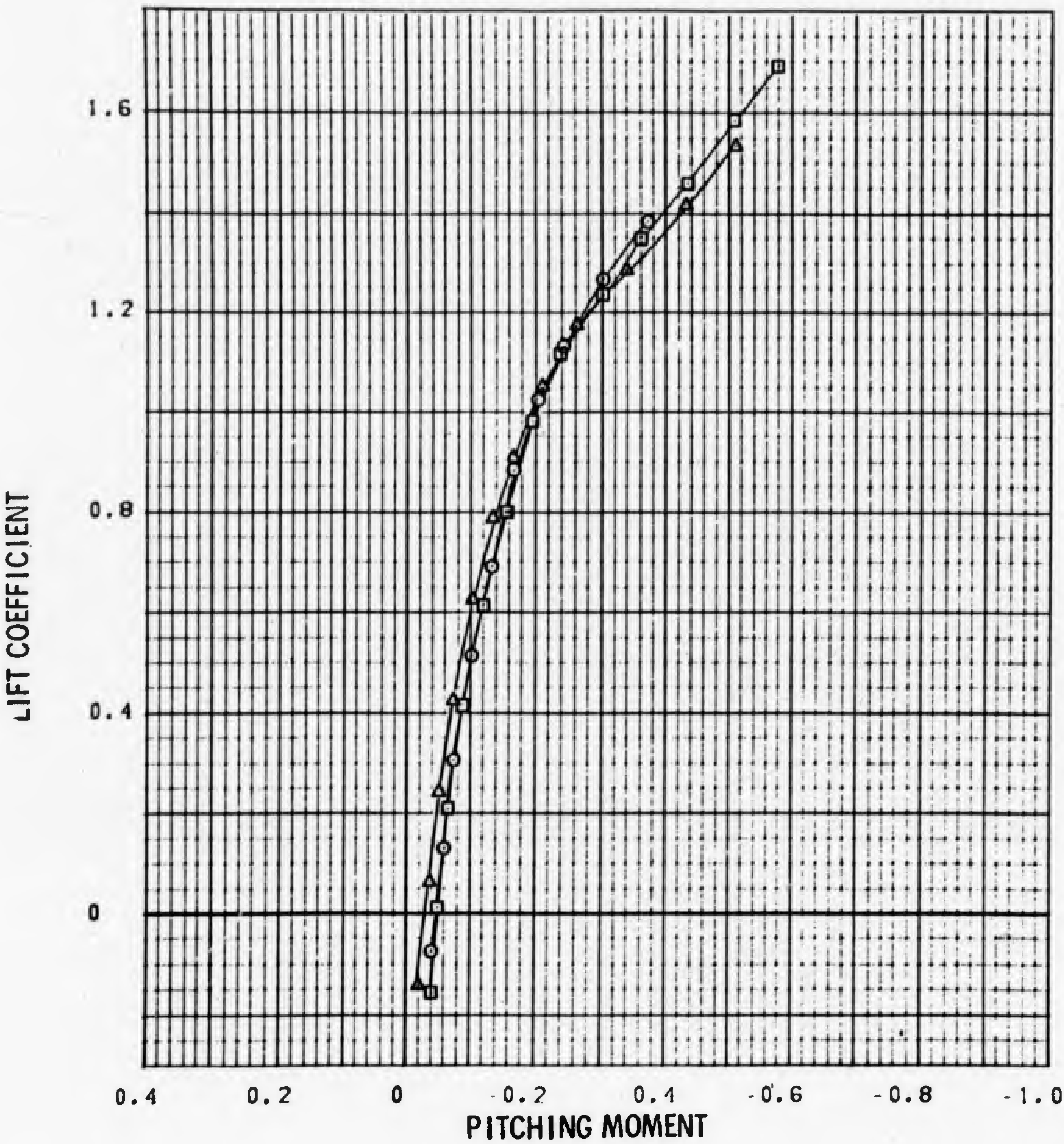
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	448	K1 5/5
⊡	PWT 4T TC-043	128	K1 10/10
▲	PWT 4T TC-043	268	K1 0/0

FIGURE 112a SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. CN
M = 0.7



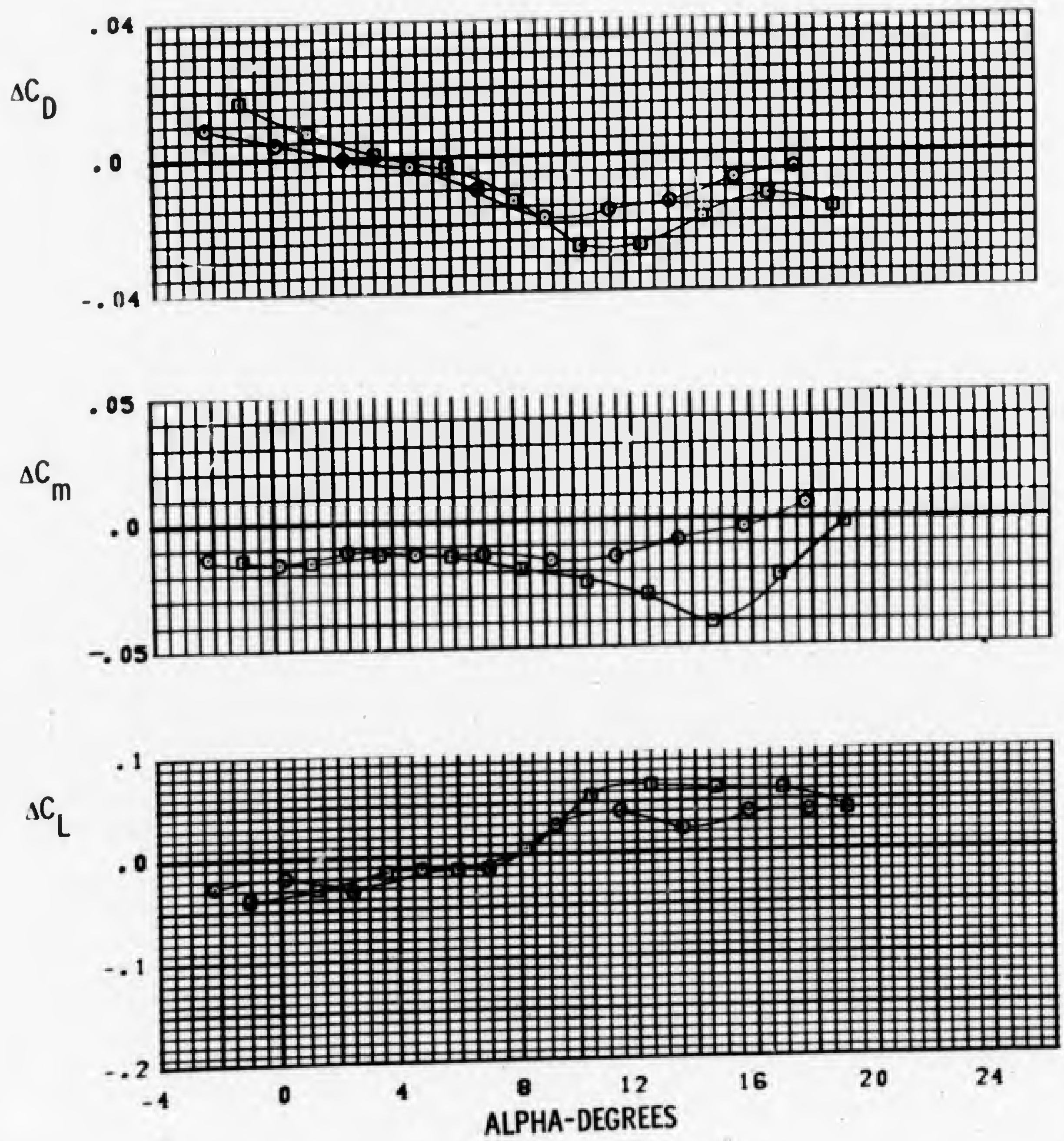
SYM	TEST	[illegible]	[illegible]
⊙	PWT 41 TC 043	448	[illegible] 5/5
⊡	PWT 41 TC 043	128	[illegible] 10/10
▲	PWT 41 TC 043	268	[illegible] 0/0

FIGURE 112a SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.7



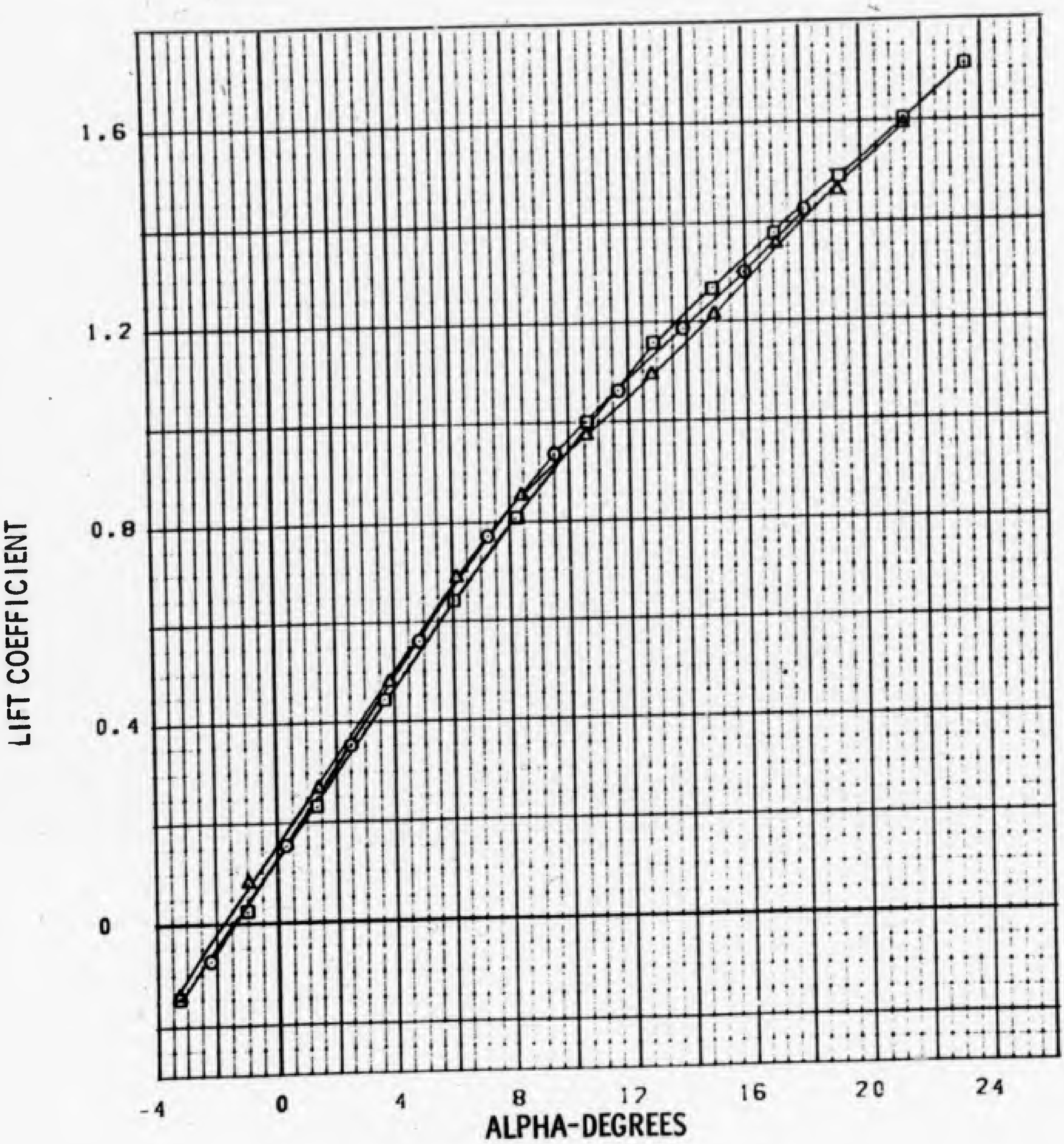
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 41 TC 043	448	KI 5/5
⊡	PWT 41 TC 043	128	KI 10/10
▲	PWT 41 TC 043	268	KI 0/0

FIGURE 112a SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.7



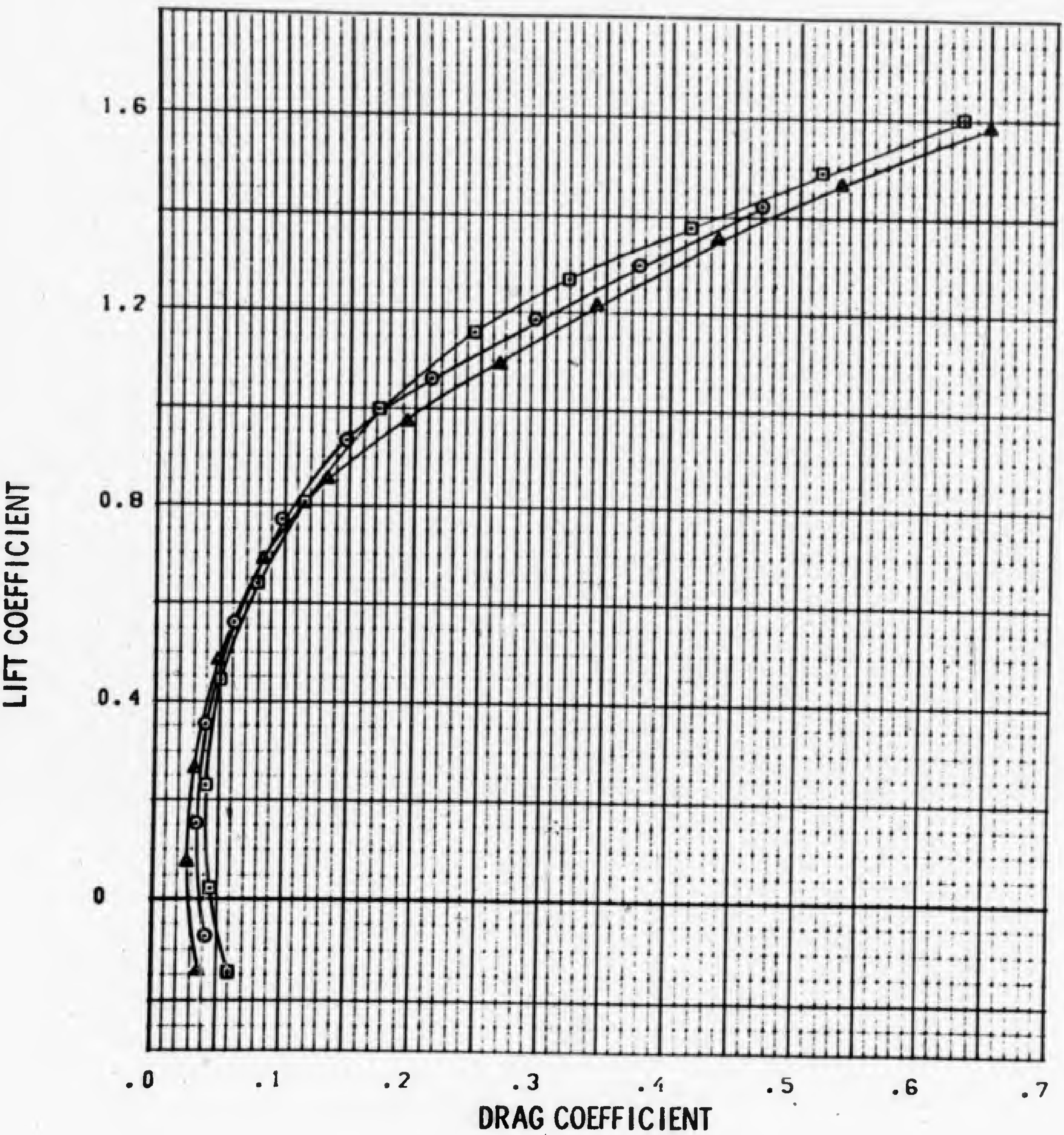
SYM	TEST	INCREMENT	L.E. (L/R)
⊙	PWT 4T TC-043	PN 448 - PN 268	K1 5/5
⊡	PWT 4T TC-043	PN 128 - PN 268	K1 10/10

FIGURE 112a SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 0.7



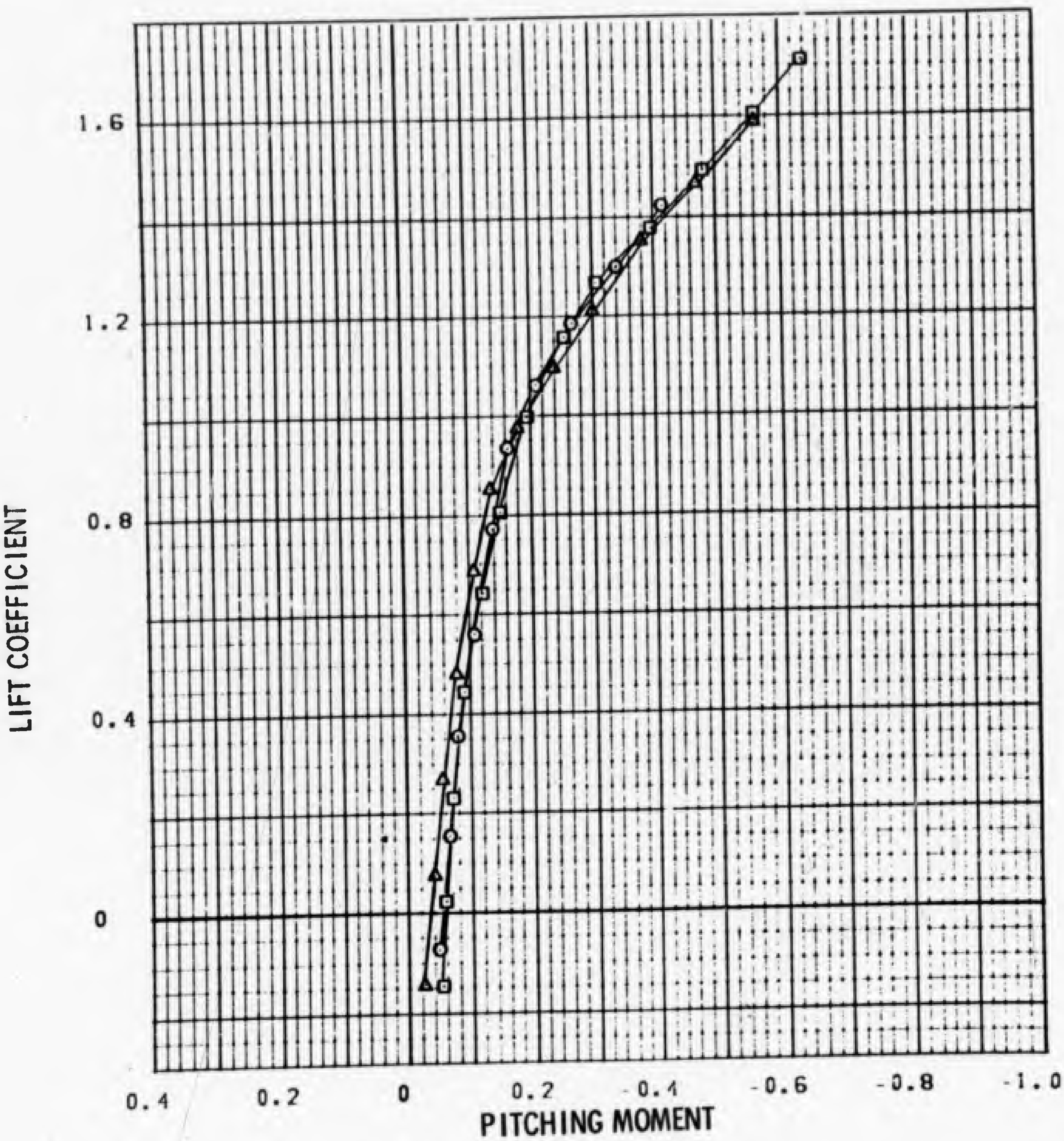
SYM	[illegible]	[illegible]	L.E. (L/R)
⊙	PWT 41 TC 043	447	K1 5/5
⊡	PWT 41 TC 043	127	K1 10/10
▲	PWT 41 TC 043	767	K1 0/0

FIGURE 112b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.8



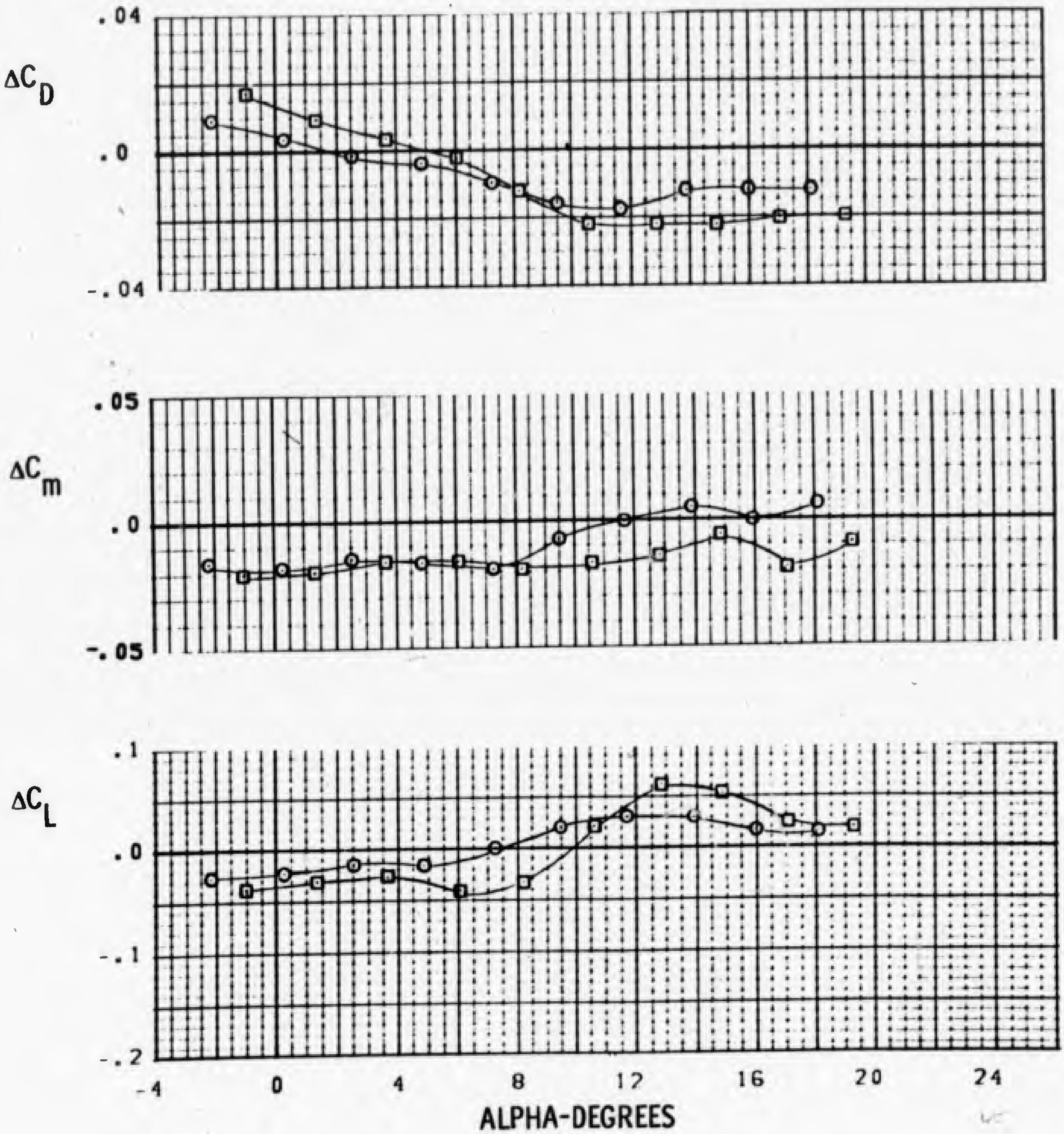
SYM	?S?	PAR?	L.E. (L/R)
⊙	PWT 41 TC 043	447	K1 5/5
⊡	PWT 41 TC 043	127	K1 10/10
▲	PWT 41 TC 043	267	K1 0/0

FIGURE 112b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.8



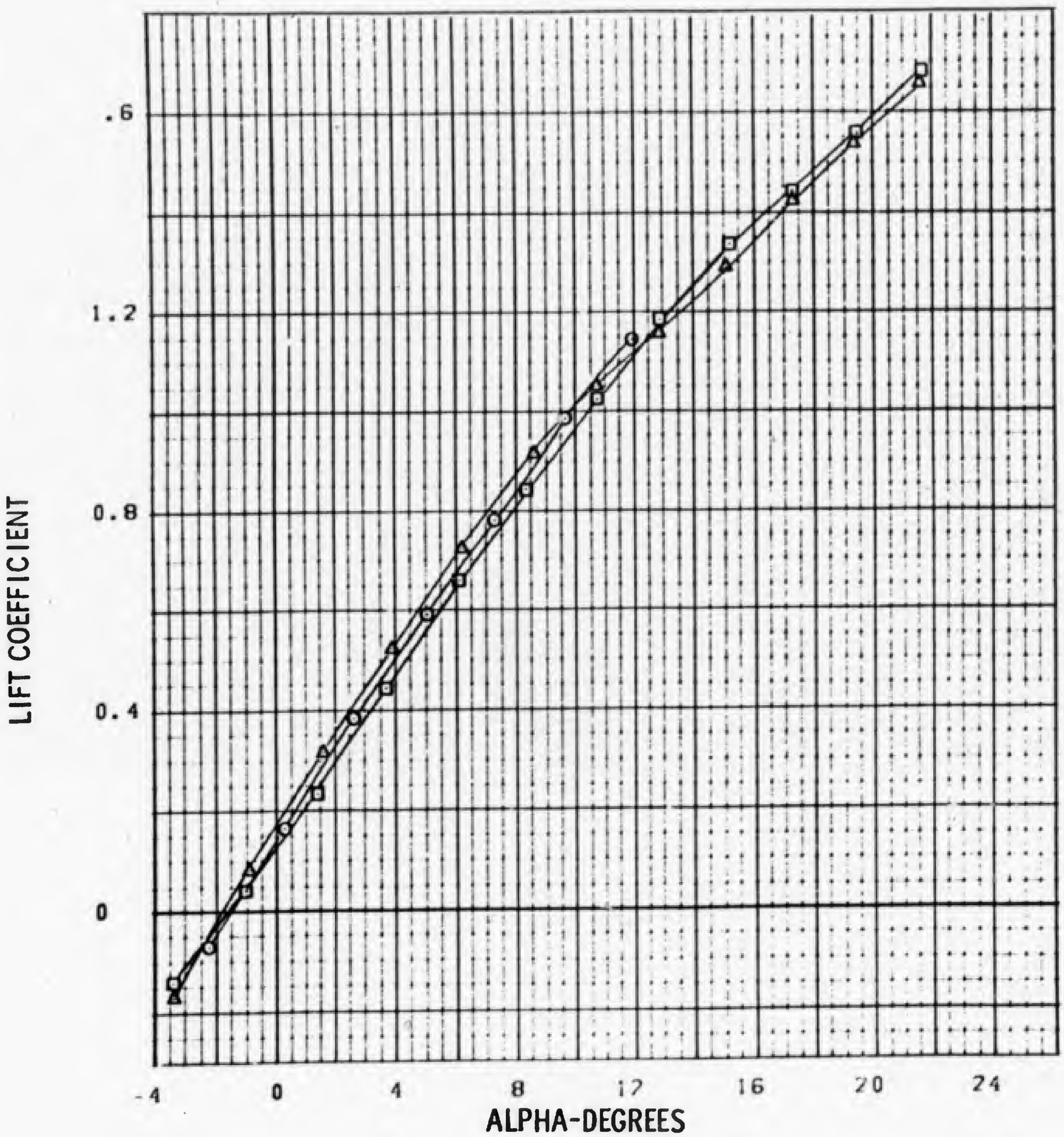
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC 043	447	KI 5/5
⊡	PWT 4T TC 043	127	KI 10/10
▲	PWT 4T TC 043	267	KI 0/0

FIGURE 112b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.8



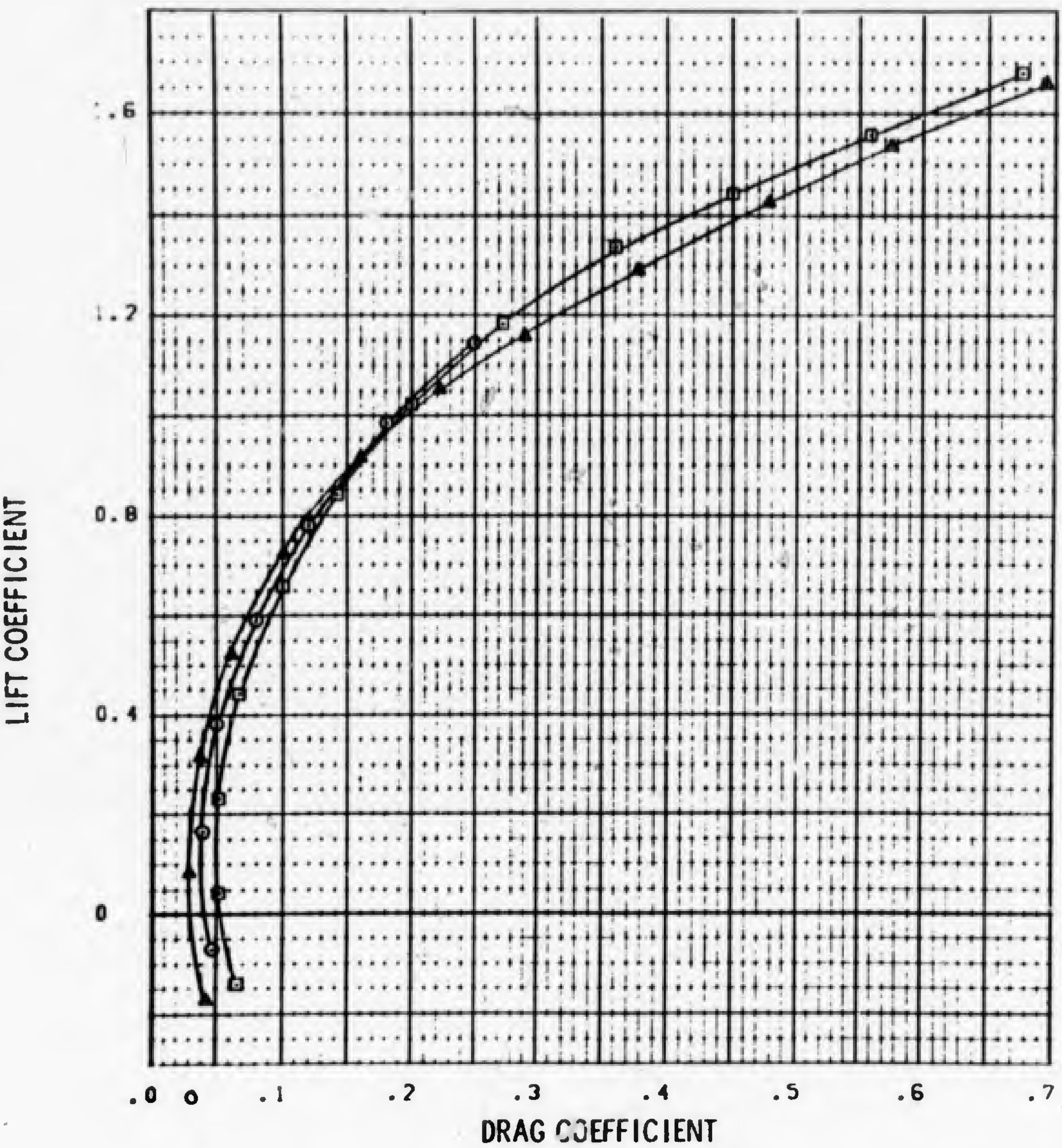
SYM	TEST	INCREMENT	[illegible]
⊙	PWT 41 TC 043	PN 447 - PN 267	KI 5/5
⊡	PWT 41 TC 043	PN 127 - PN 267	KI 10/10

FIGURE 112b SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 0.8



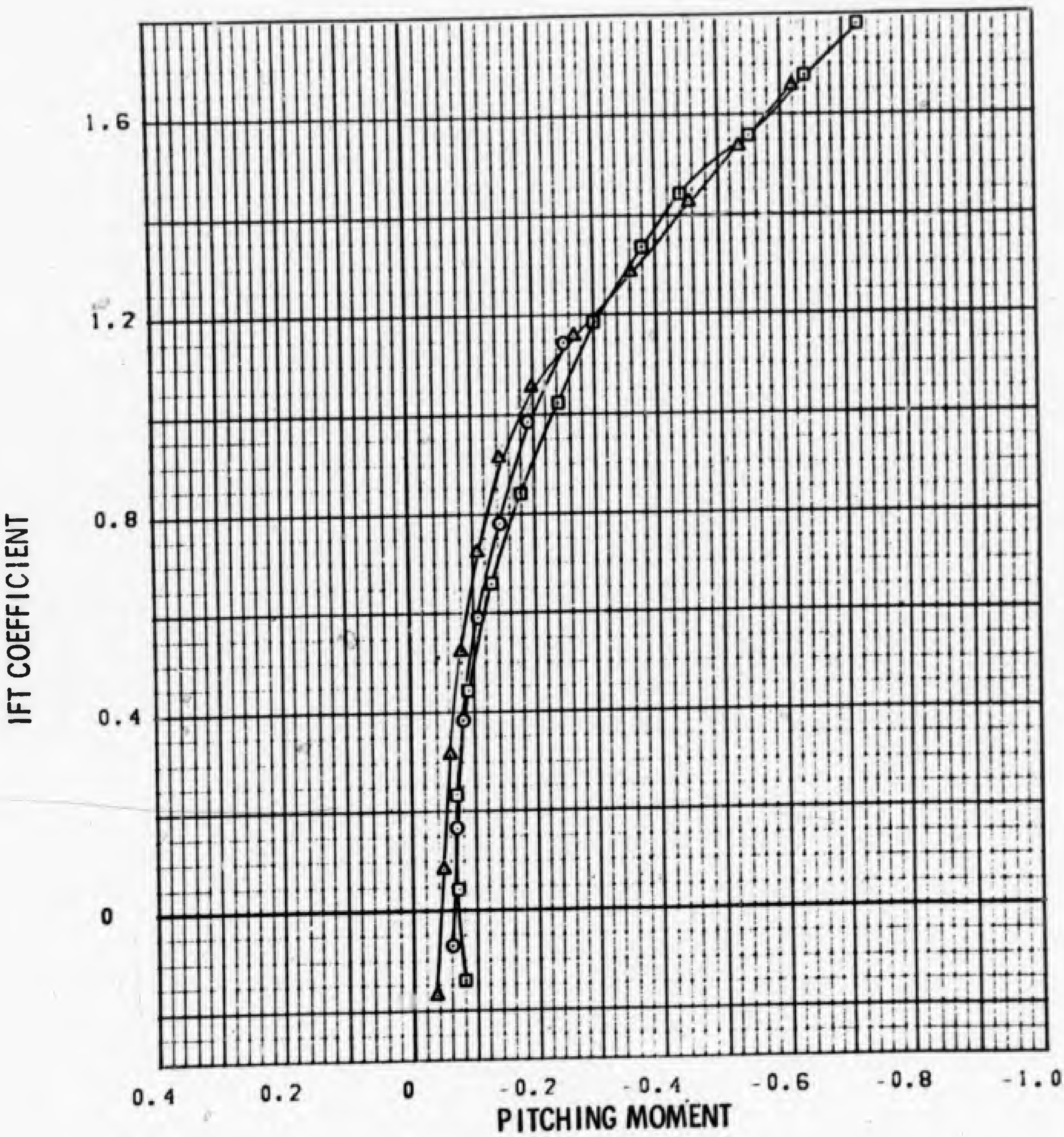
SYM	TEST	PART	LE. (L/R)
⊙	PWT 41 TC 043	445	KI 5/5
⊡	PWT 41 TC 043	176	KI 10/10
△	PWT 41 TC 043	264	KI 0/0

FIGURE 112c SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.9



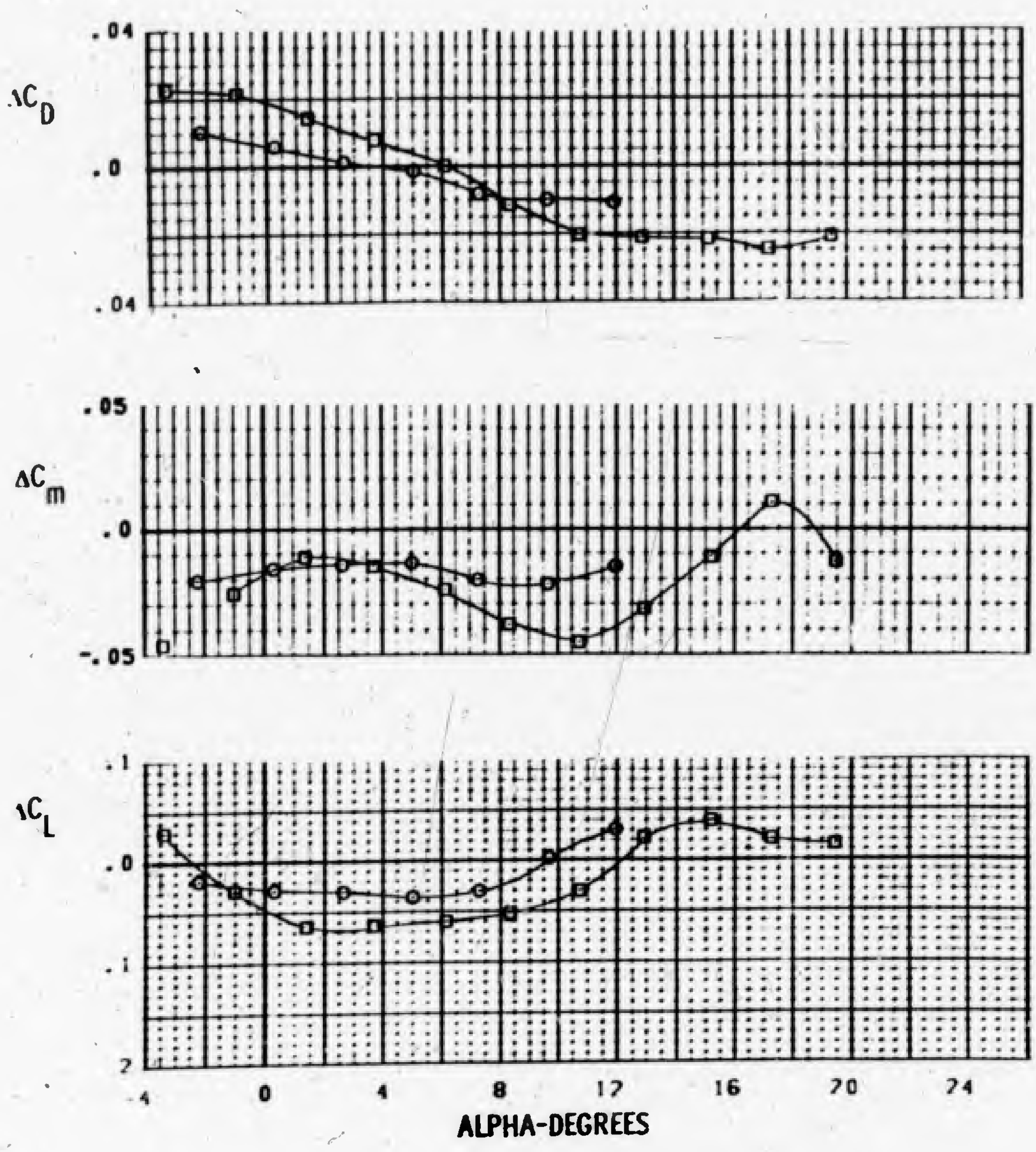
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC 043	445	KI 5/5
⊡	PWT 4T TC 043	176	KI 10/10
▲	PWT 4T TC 043	264	KI 0/0

FIGURE 112c SYMMETRIC LEADING EDGE FLAP EFFECTS H.T. ON
M - 0.9



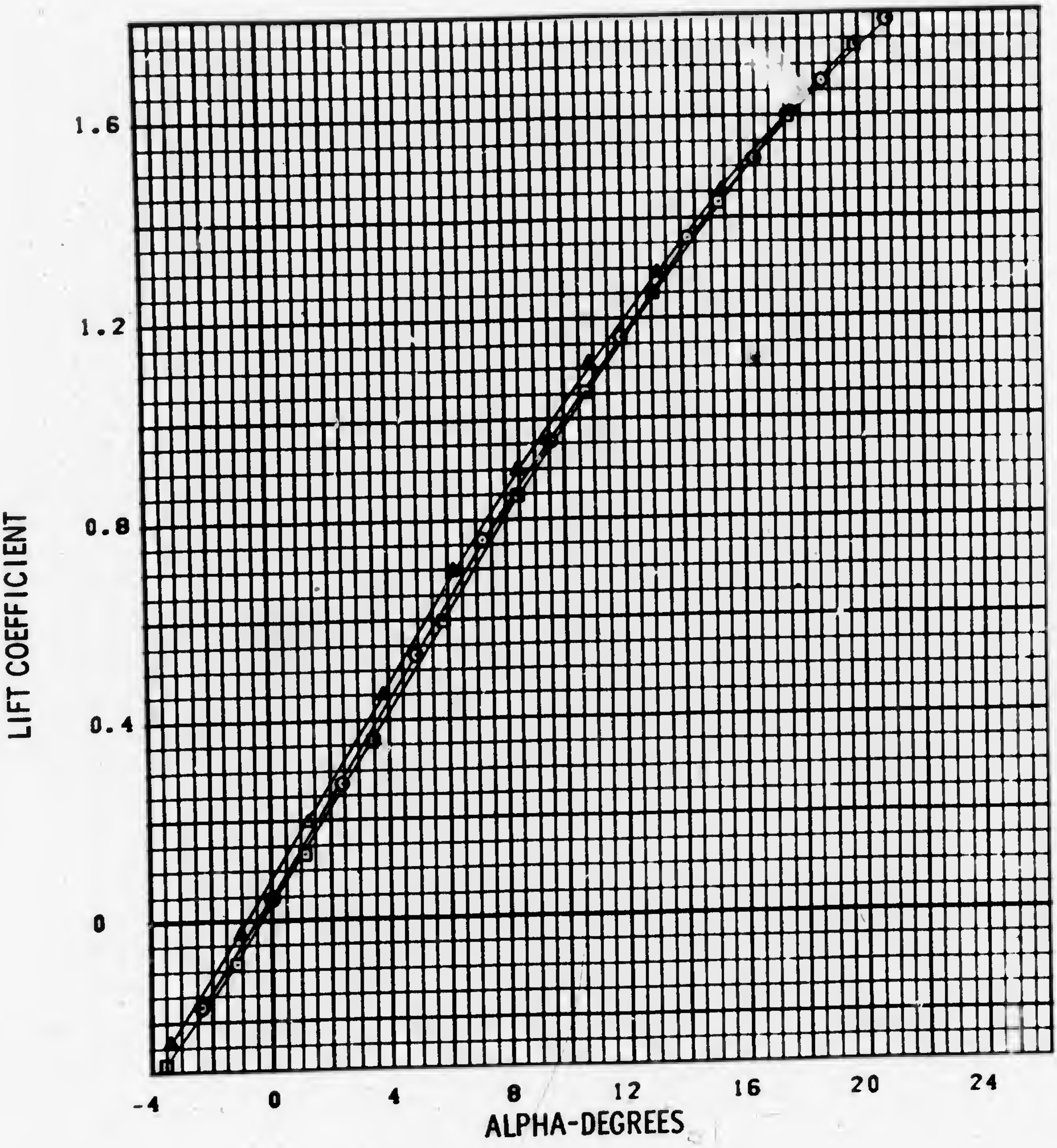
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 41 TC-043	445	KT 5/5
⊡	PWT 41 TC-043	126	KT 10/10
▲	PWT 41 TC-043	264	KT 0/0

FIGURE 112c SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M 0.9



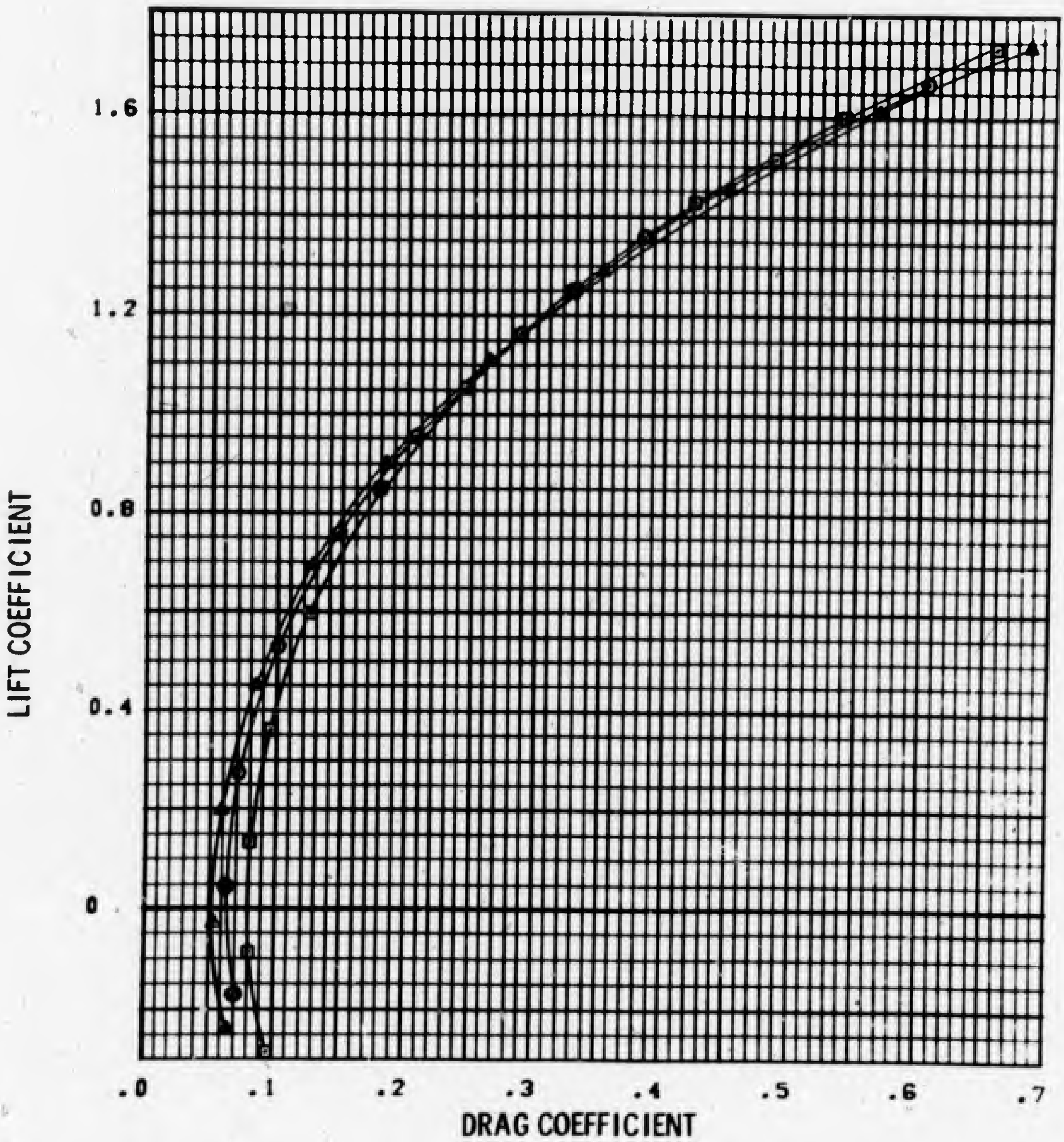
SYM	TEST		INCREMENT	L.E. (L/R)	
○	PWT 4T	TC-043	PN 445 - PN 264	K1	5/5
□	PWT 4T	TC-043	PN 126 - PN 264	K1	10/10

Figure 112c SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 0.9



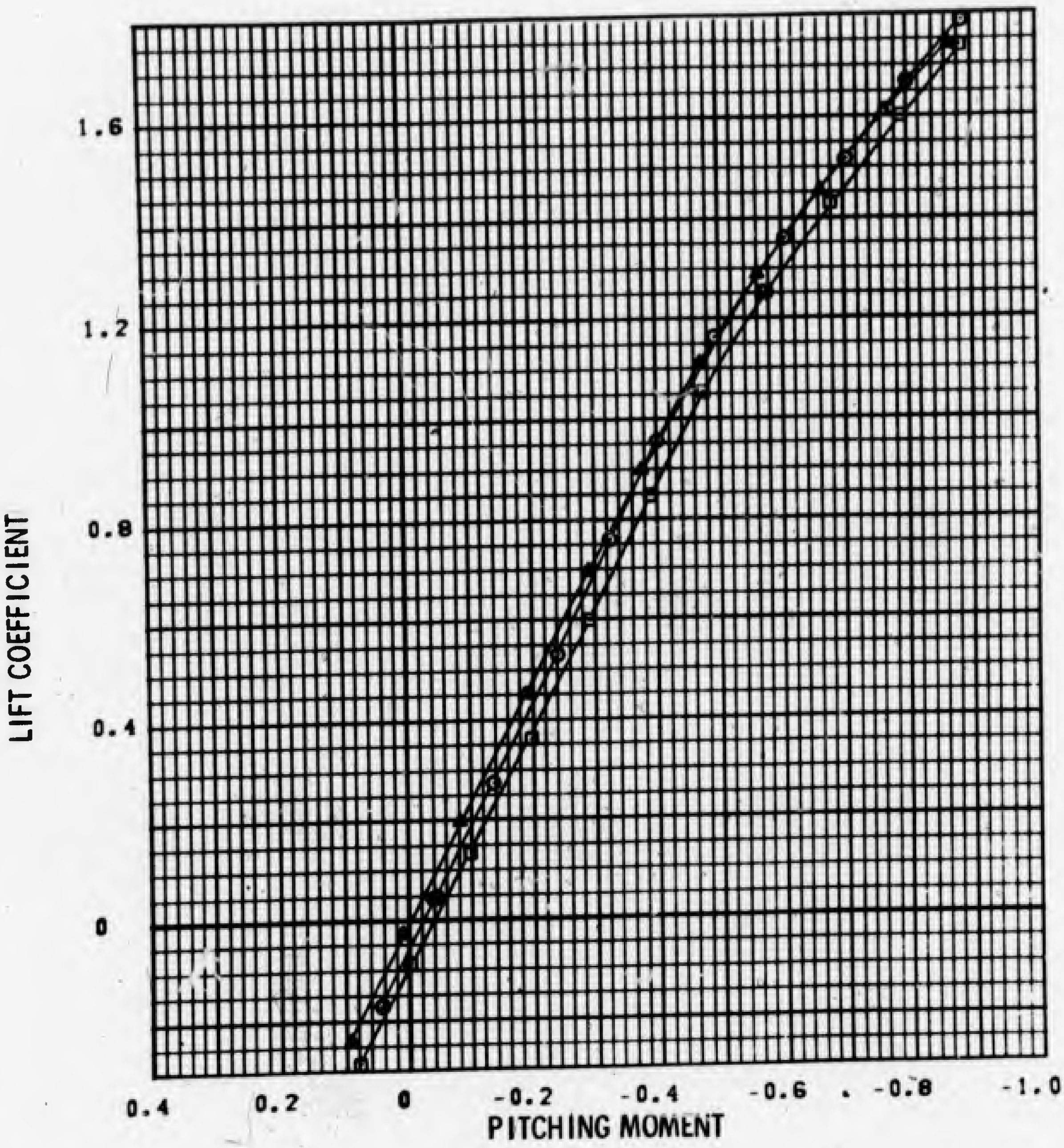
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	449	K1 5/5
⊡	PWT 4T TC-043	129	K1 10/10
▲	PWT 4T TC-043	269	K1 0/0

FIGURE 112d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 1.2



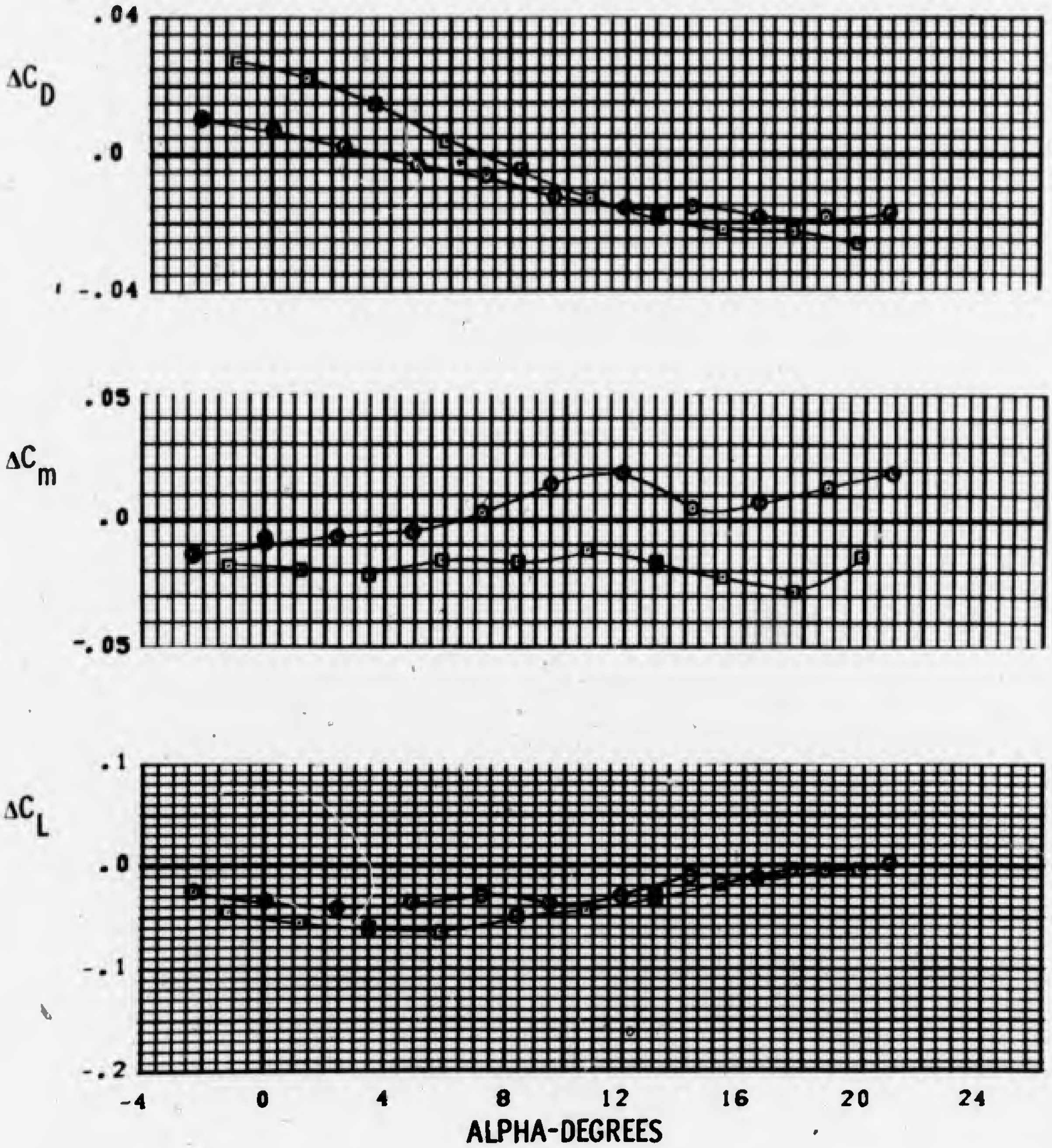
SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	449	K1 5/5
⊡	PWT 4T TC-043	129	K1 10/10
▲	PWT 4T TC-043	269	K1 0/0

FIGURE 112d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 1.2



SYM	TEST	PART	L.E. (L/R)
⊙	PWT 4T TC-043	449	K1 5/5
⊡	PWT 4T TC-043	129	K1 10/10
▲	PWT 4T TC-043	269	K1 0/0

FIGURE 112d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 1.2

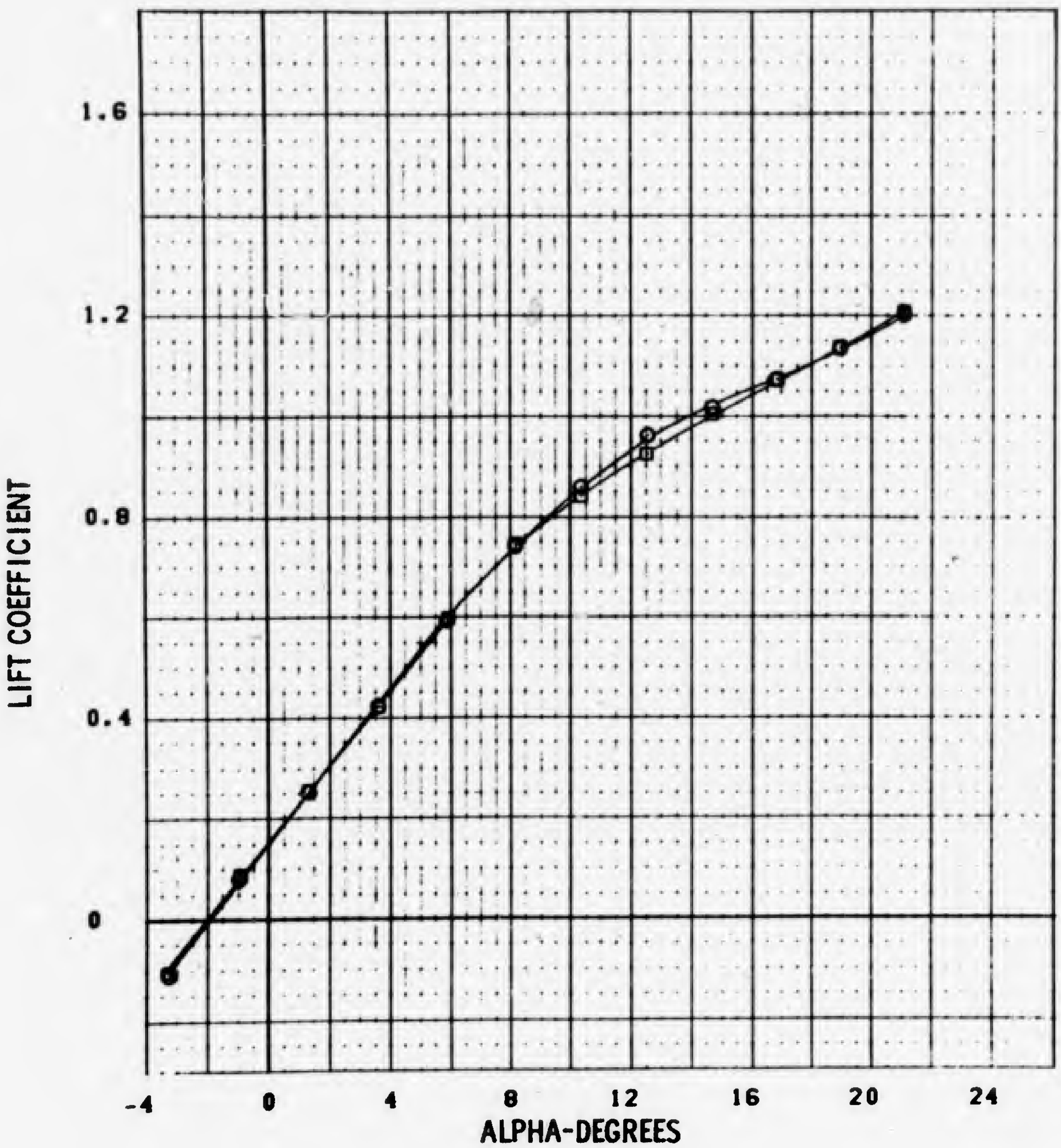


SYM	TEST	INCREMENT	L.E. (L/R)
⊙	PWT 4T TC-043	PN 449 - PN 269	K1 5/5
⊡	PWT 4T TC-043	PN 129 - PN 269	K1 10/10

FIGURE 112d SYMMETRIC LEADING EDGE FLAP EFFECTS, H.T. ON
M = 1.2

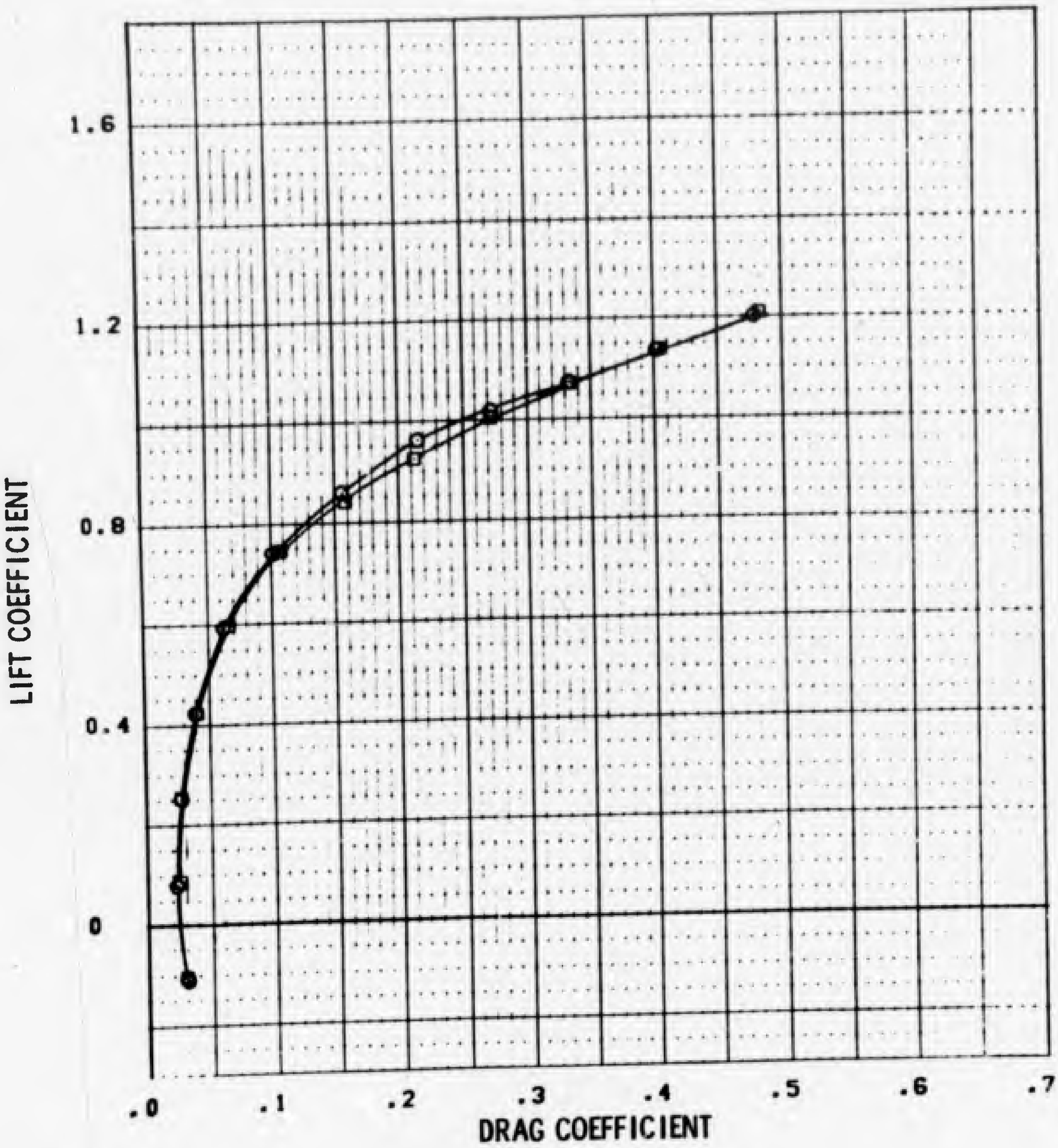
3. ALTERNATE LEADING EDGE

Comparison plots showing the effect of the alternate leading edge airfoil geometry in comparison to the basic leading edge are presented in this subsection.



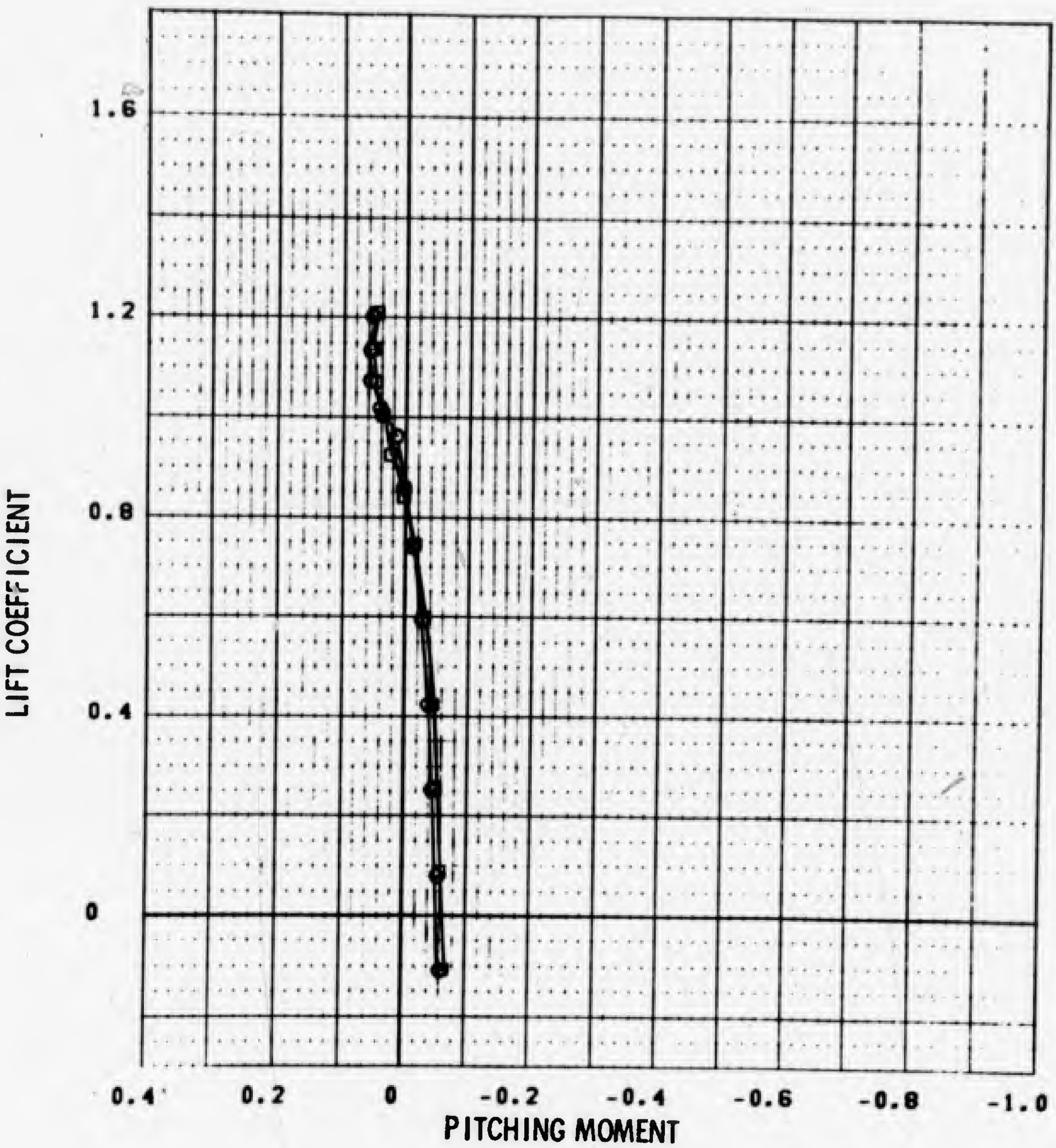
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	32	K1 0/0	OFF
⊡	PWT 4T TC-043	63	K2 0/0	OFF

FIGURE 113a EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



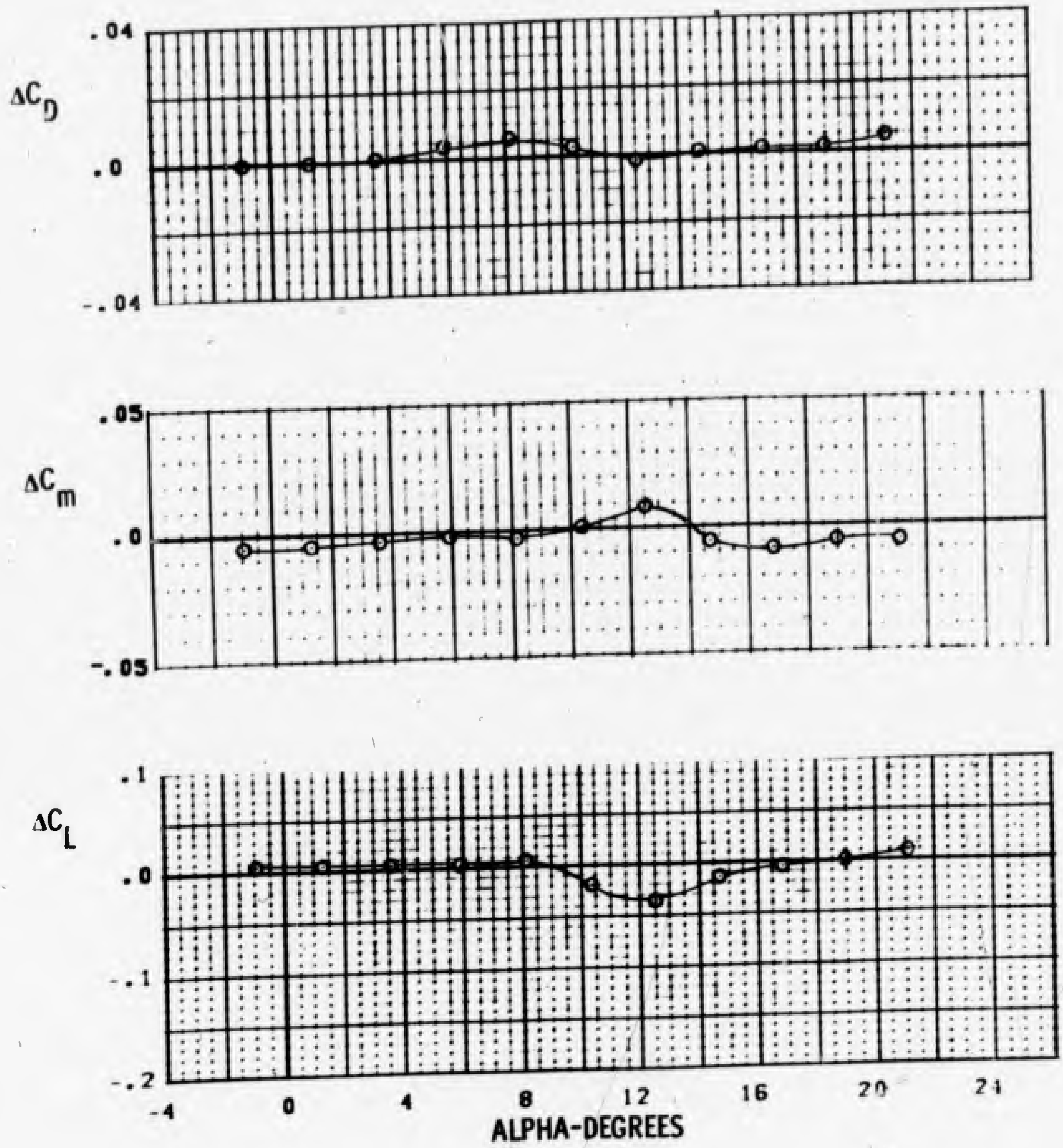
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	32	K1 0/0	OFF
⊡	PWT 4T TC-043	63	K2 0/0	OFF

FIGURE 113a EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



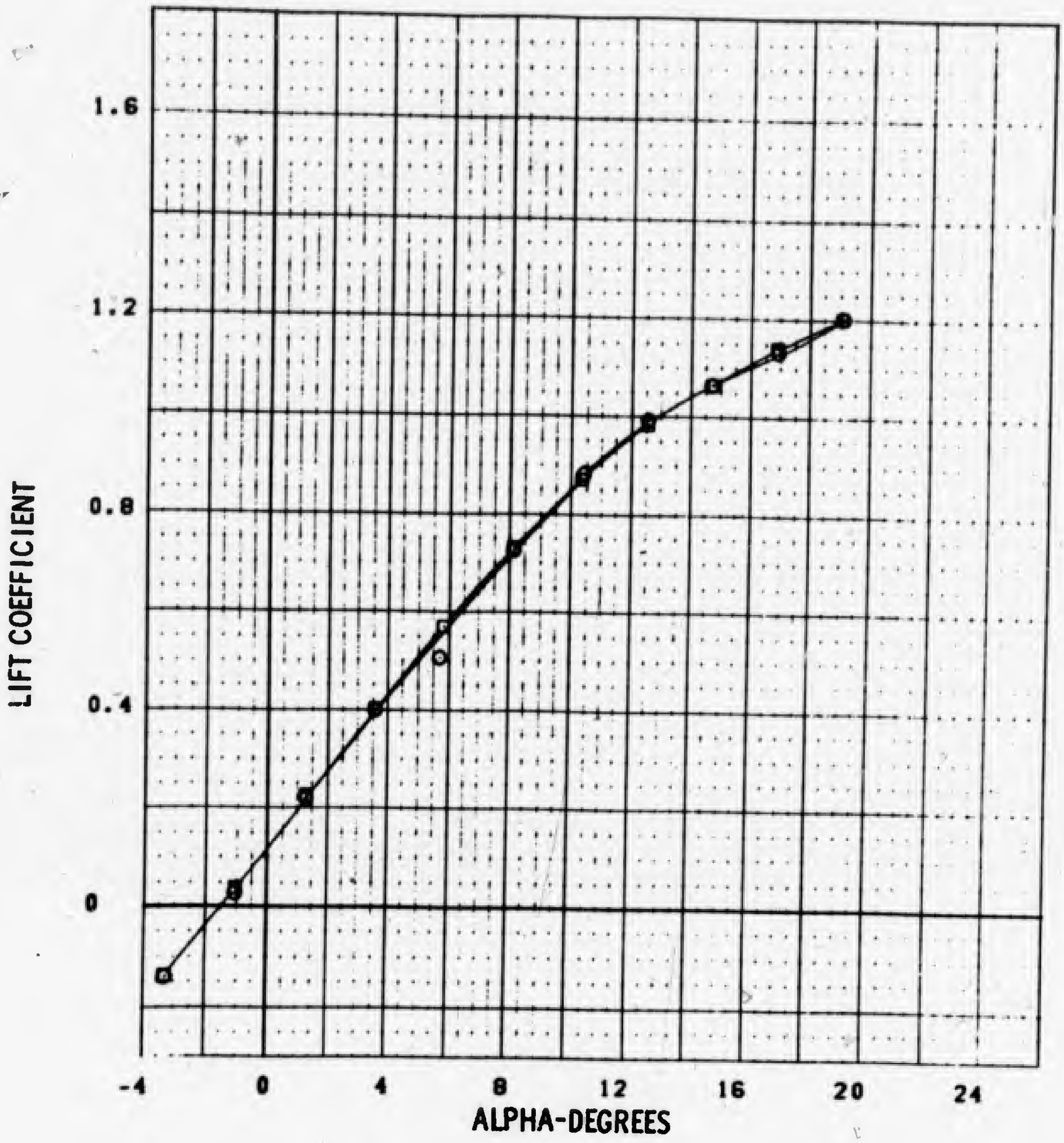
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	32	K1 0/0	OFF
⊡	PWT 4T TC-043	63	K2 0/0	OFF

FIGURE 113a EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



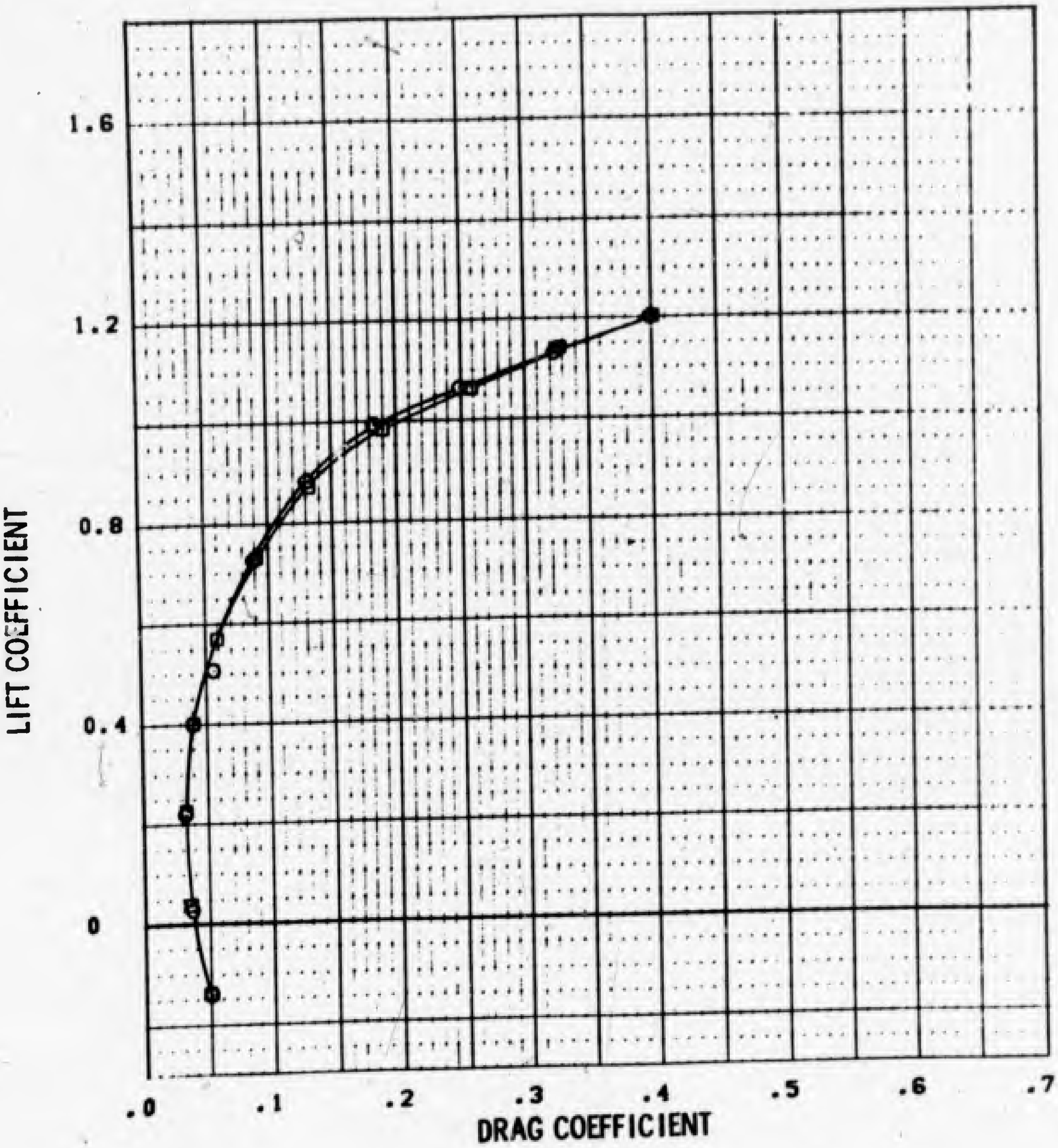
SYM	TEST	INCREMENT (K2 - K1)	L.E. (/R)	M.'.
⊙	PWT 4T TC-043	PN 63 - PN 32	0/0	OFF

FIGURE 113a EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



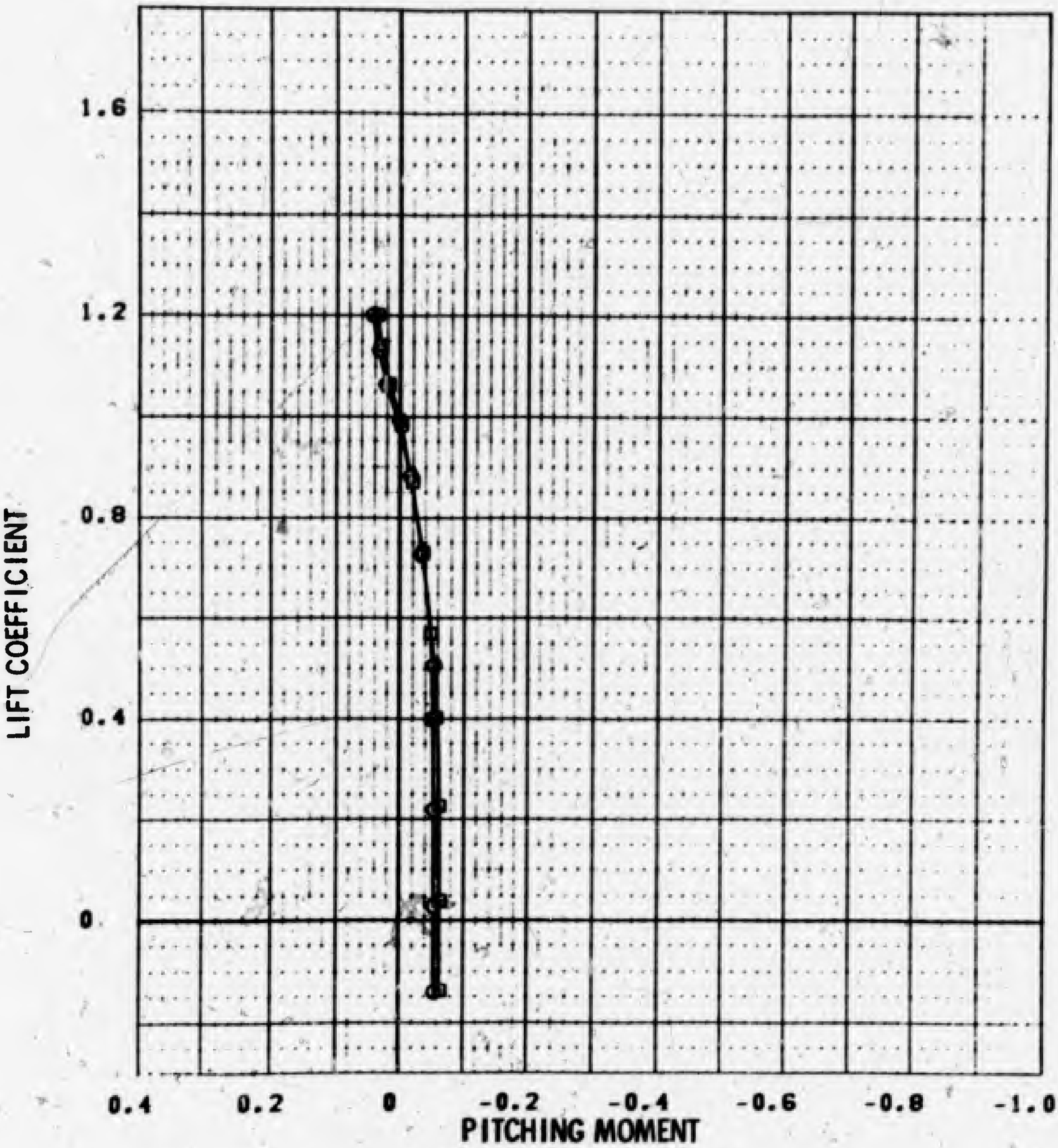
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	49	K1 10/10	OFF
⊡	PWT 4T TC-043	74	K2 10/10	OFF

FIGURE 113b EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



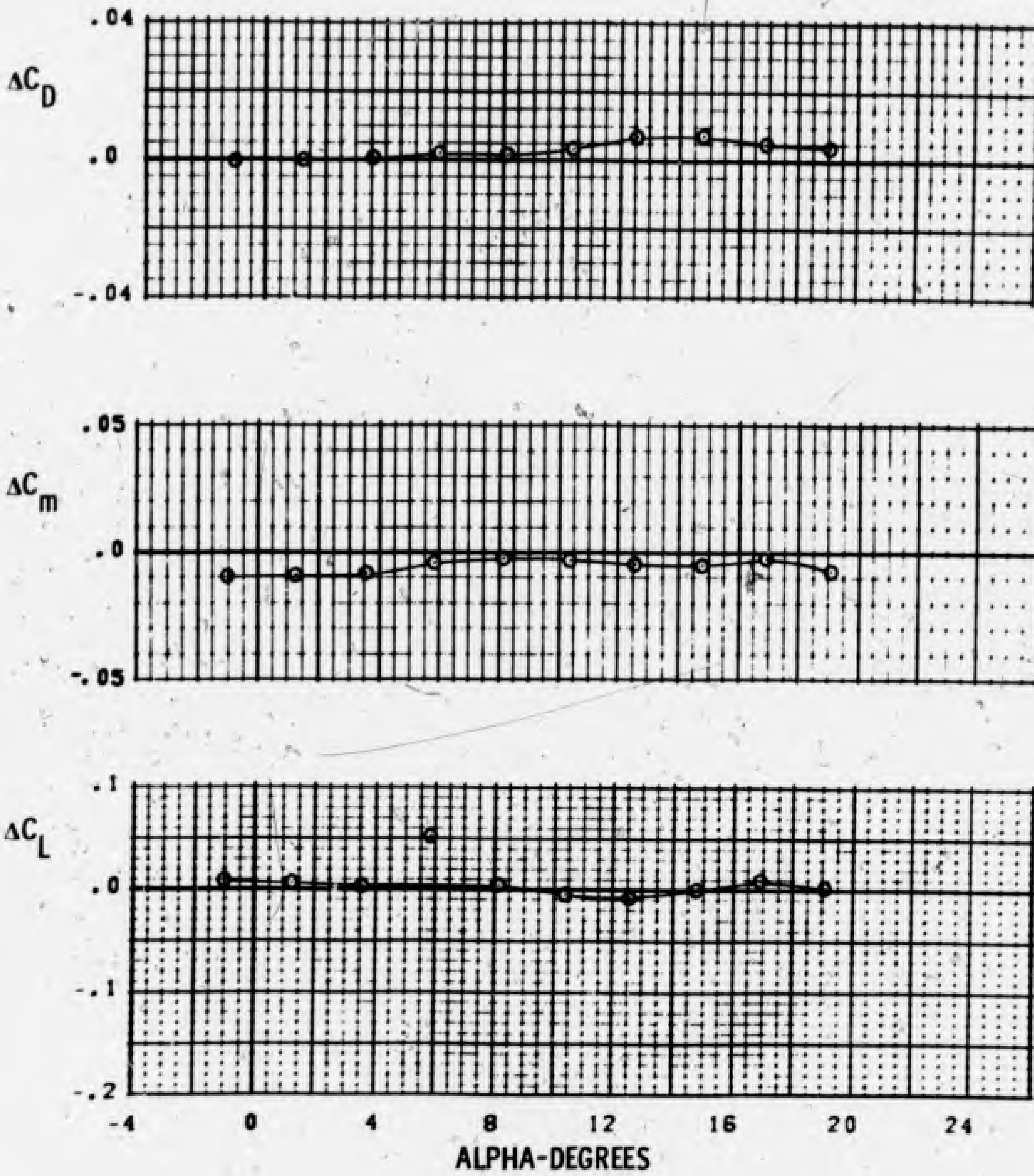
SYM	TEST	PART	L.E. (L/R)	H.T.
○	PWT 4T TC-043	49	K1 10/10	OFF
▫	PWT 4T TC-043	74	K2 10/10	OFF

FIGURE 113b EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



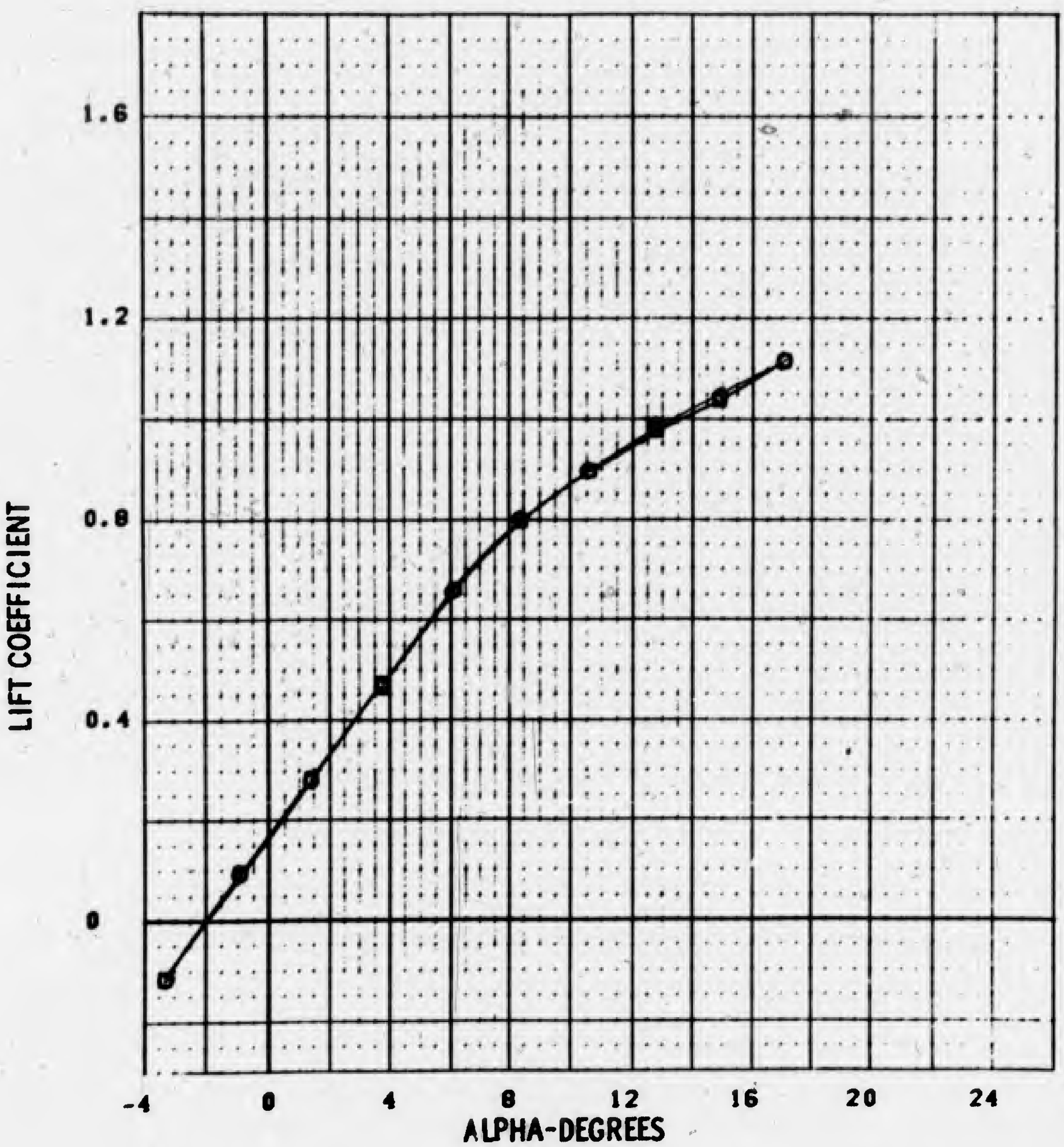
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	49	K1 10/10	OFF
⊡	PWT 4T TC-043	74	K2 10/10	OFF

FIGURE 113b EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



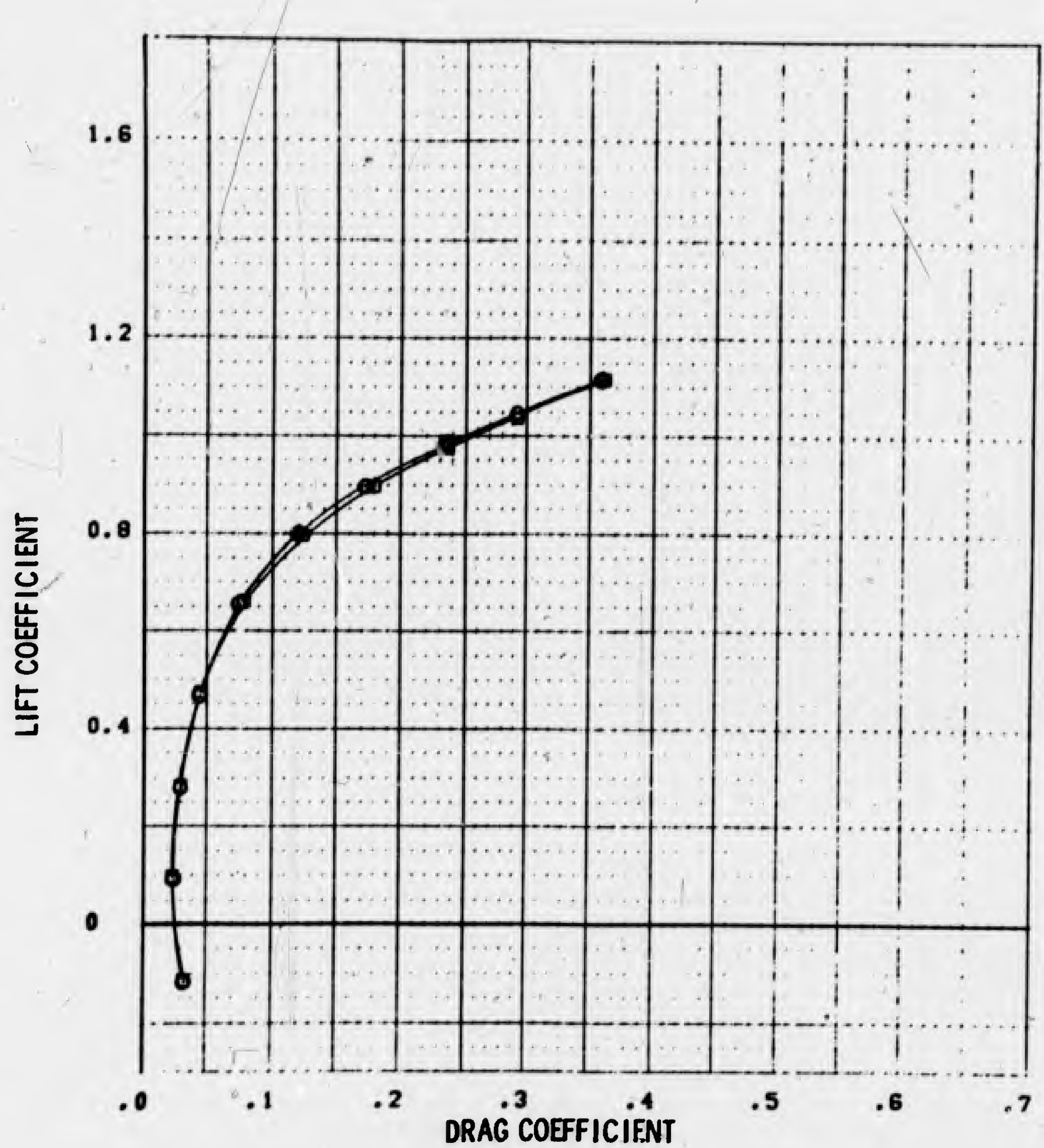
SYM	TEST	INCREMENT (K2 - K1)	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	PN 74 - PN 49	10/10	OFF

FIGURE 113b EFFECT OF ALTERNATE LEADING EDGE
M = 0.7



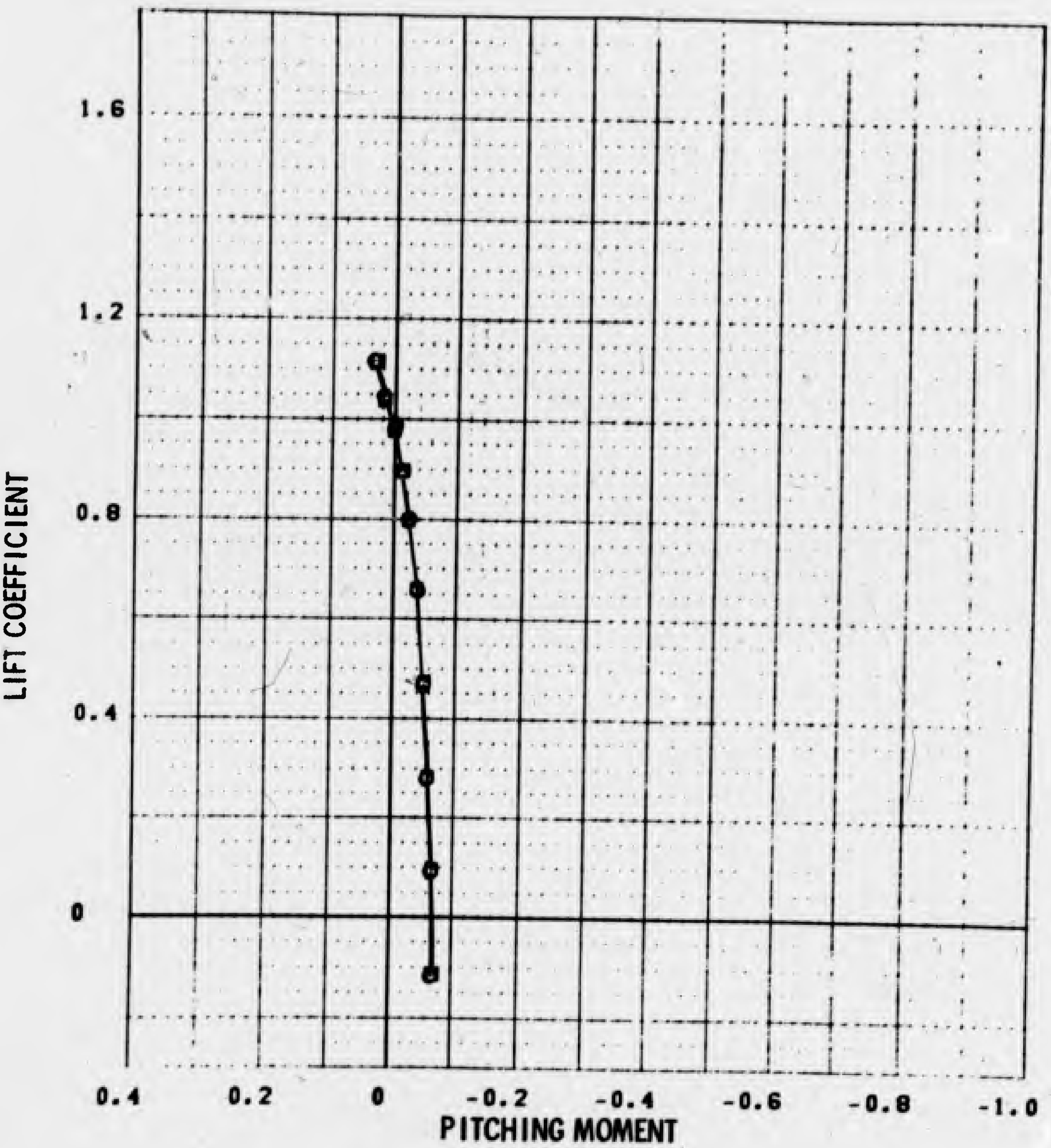
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	31	K1 0/0	OFF
⊡	PWT 4T TC-043	62	K2 0/0	OFF

FIGURE 113c EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



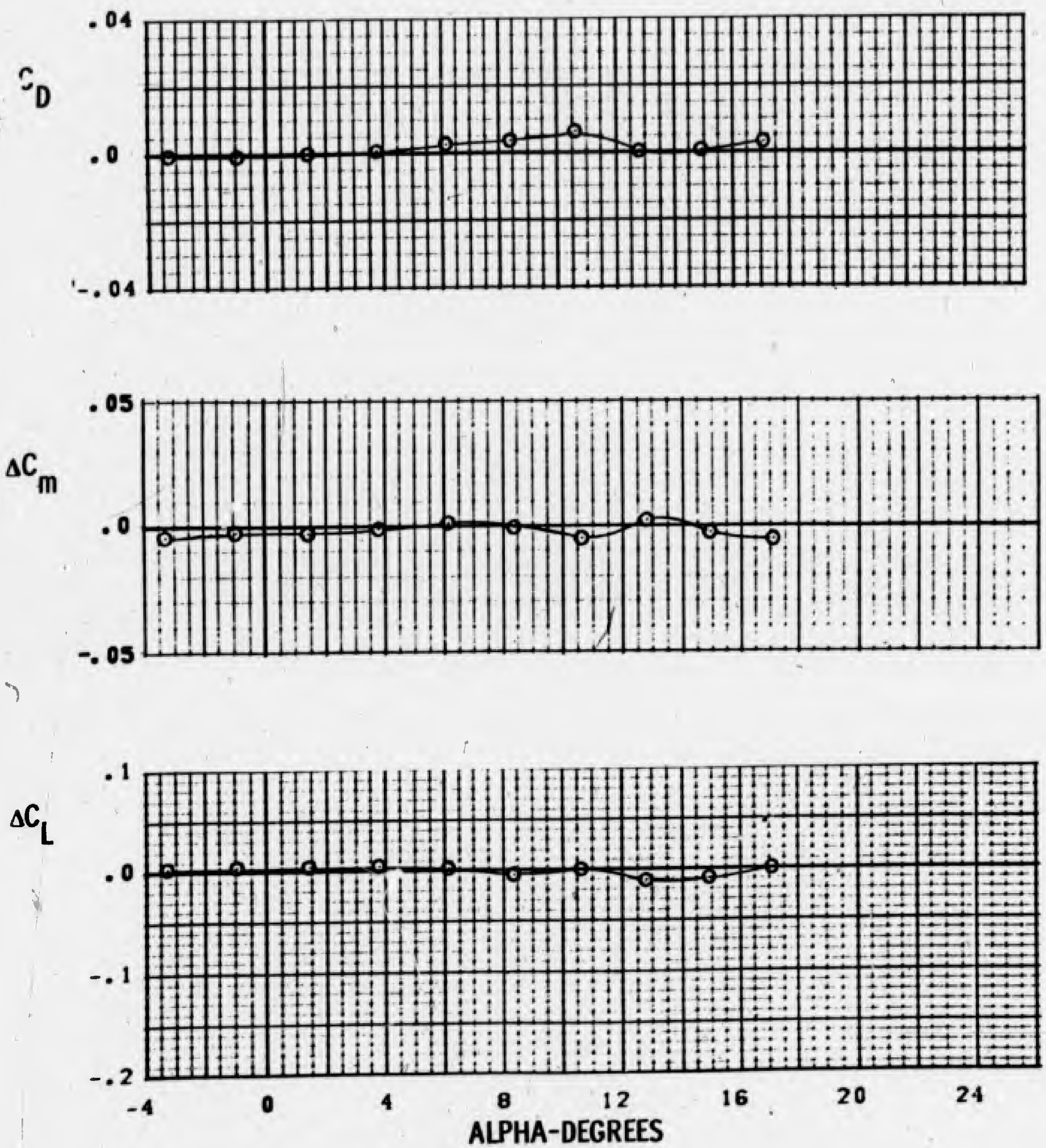
SYM	TEST	PART	L.E.	(L/R)	H.T.
⊙	PWT 4T TC-043	31	K1	0/0	OFF
⊡	PWT 4T TC-043	62	K2	0/0	OFF

FIGURE 113c EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



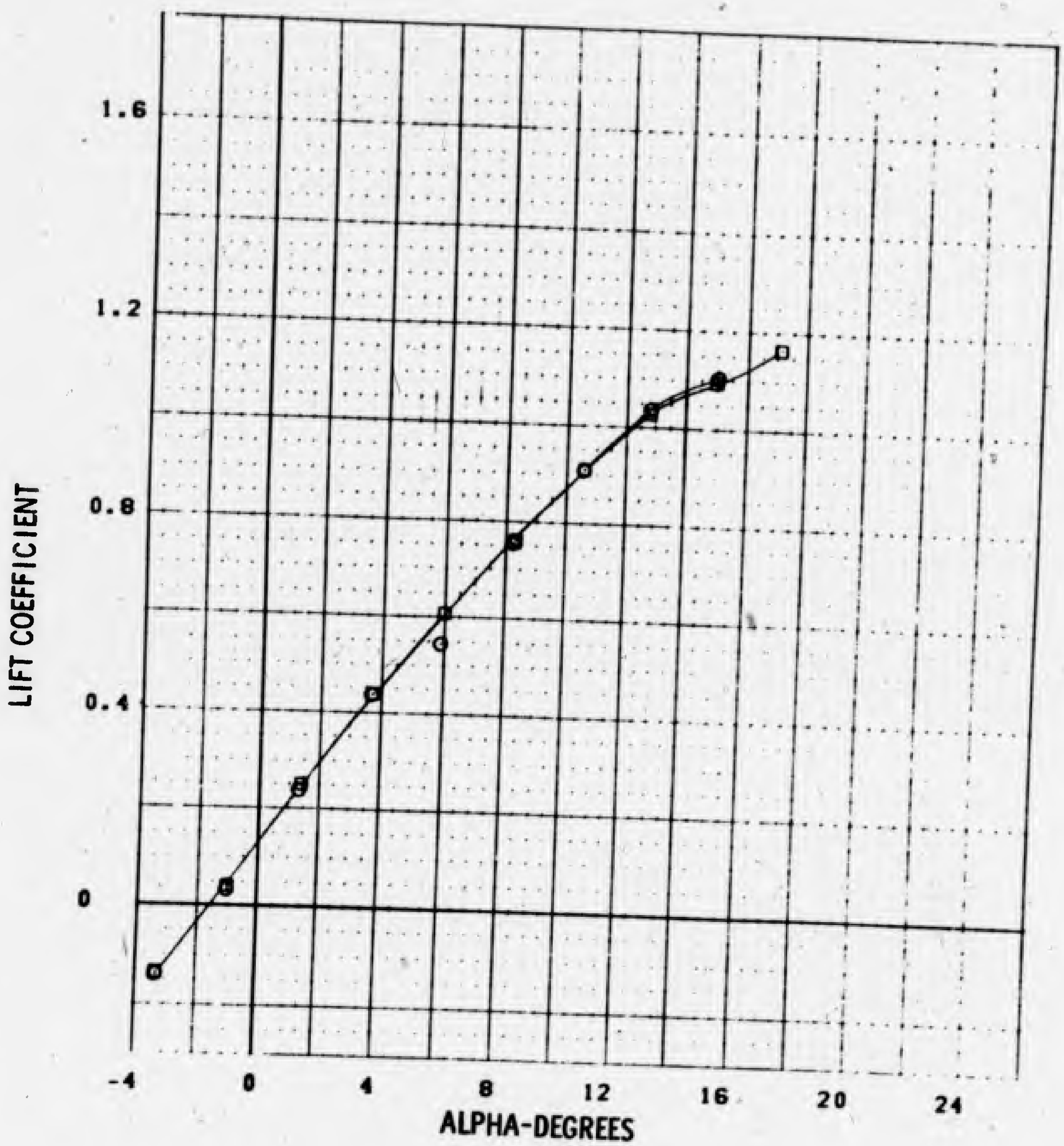
SYM	TEST	PART	L.E. (L/R)	H.T.
O	PWT 4T TC-043	31	K1 0/0	OFF
□	PWT 4T TC-043	62	K2 0/0	OFF

FIGURE 113c EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



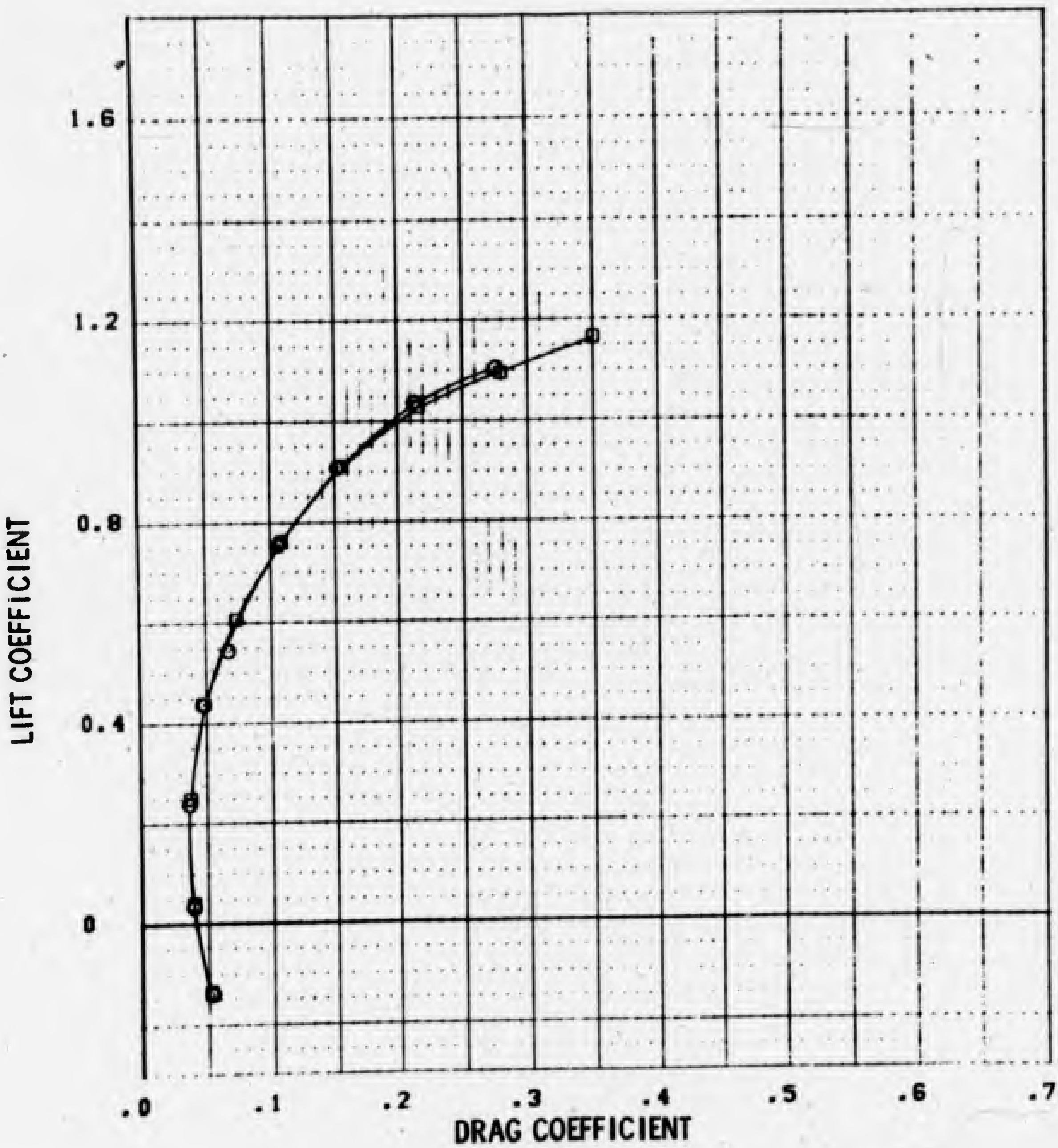
SYM	TEST	INCREMENT (K2 - K1)	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	PN 62 - PN 31	0/0	OFF

FIGURE 113c EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



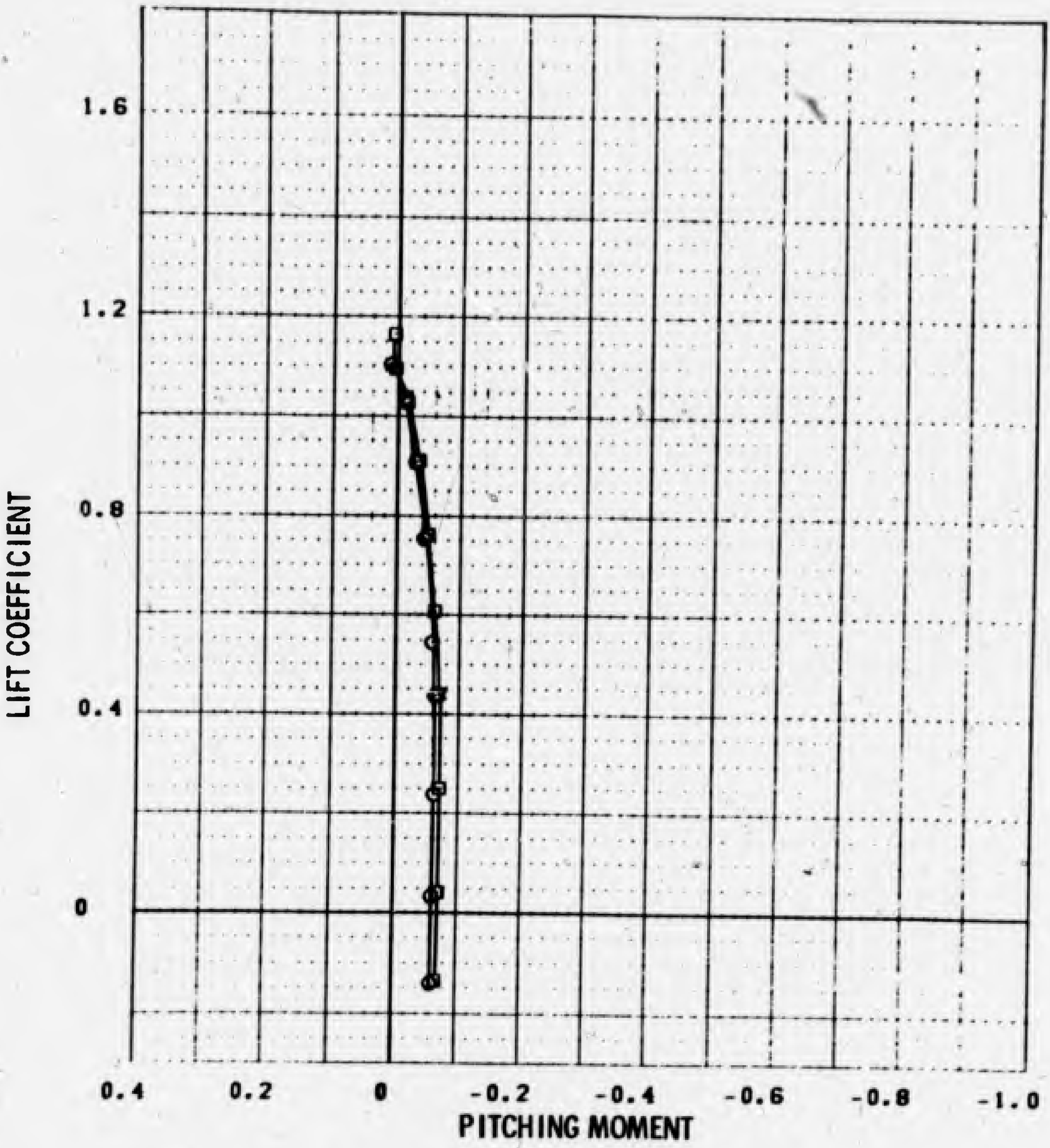
SYM	TEST	PART	L.E. (L/R)	H.T.
○	PWT 4T TC-043	48	K1 10/10	OFF
□	PWT 4T TC-043	73	K2 10/10	OFF

FIGURE 113d EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



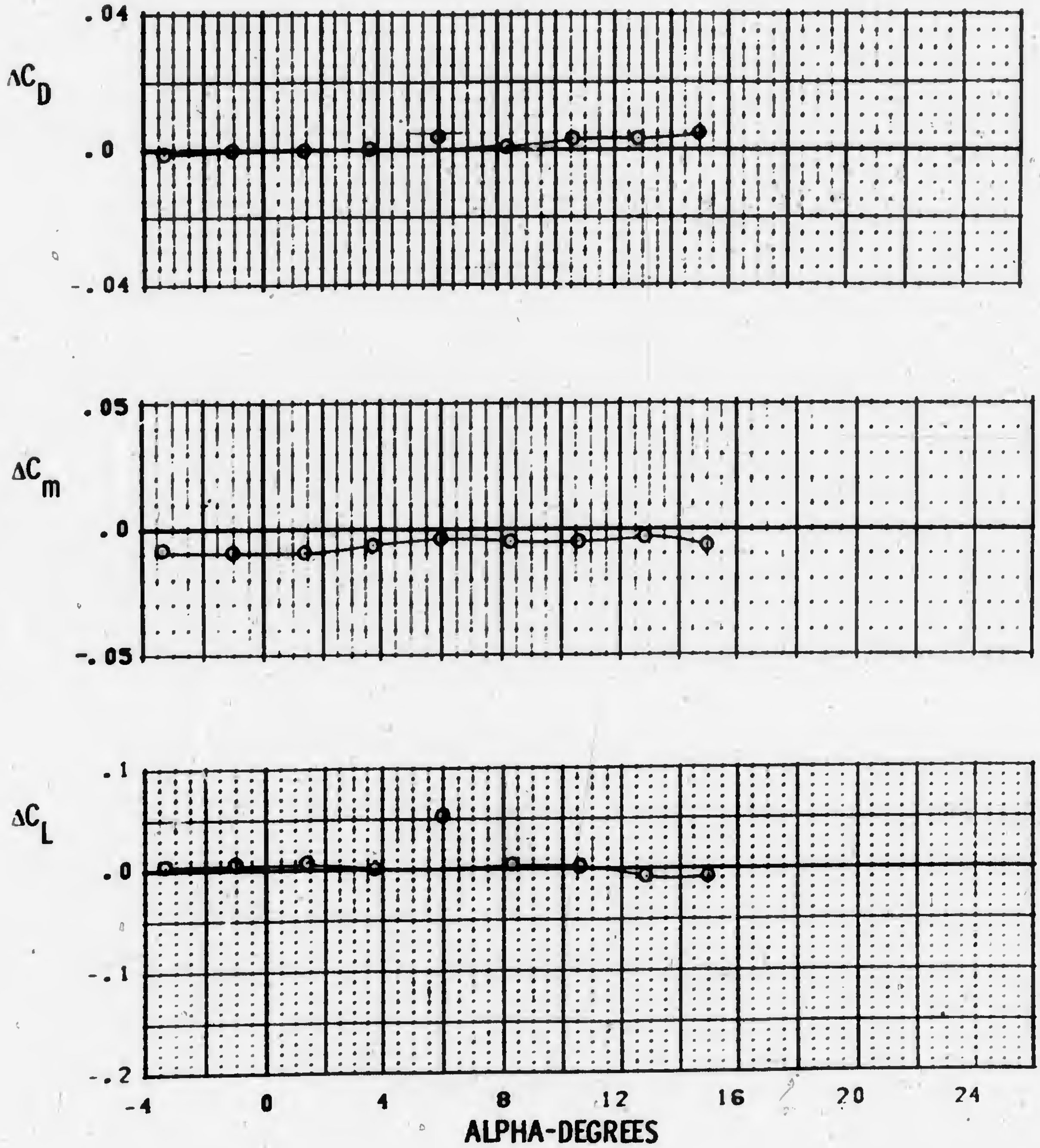
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	48	K1 10/10	OFF
⊡	PWT 4T TC-043	73	K2 10/10	OFF

FIGURE 113d EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



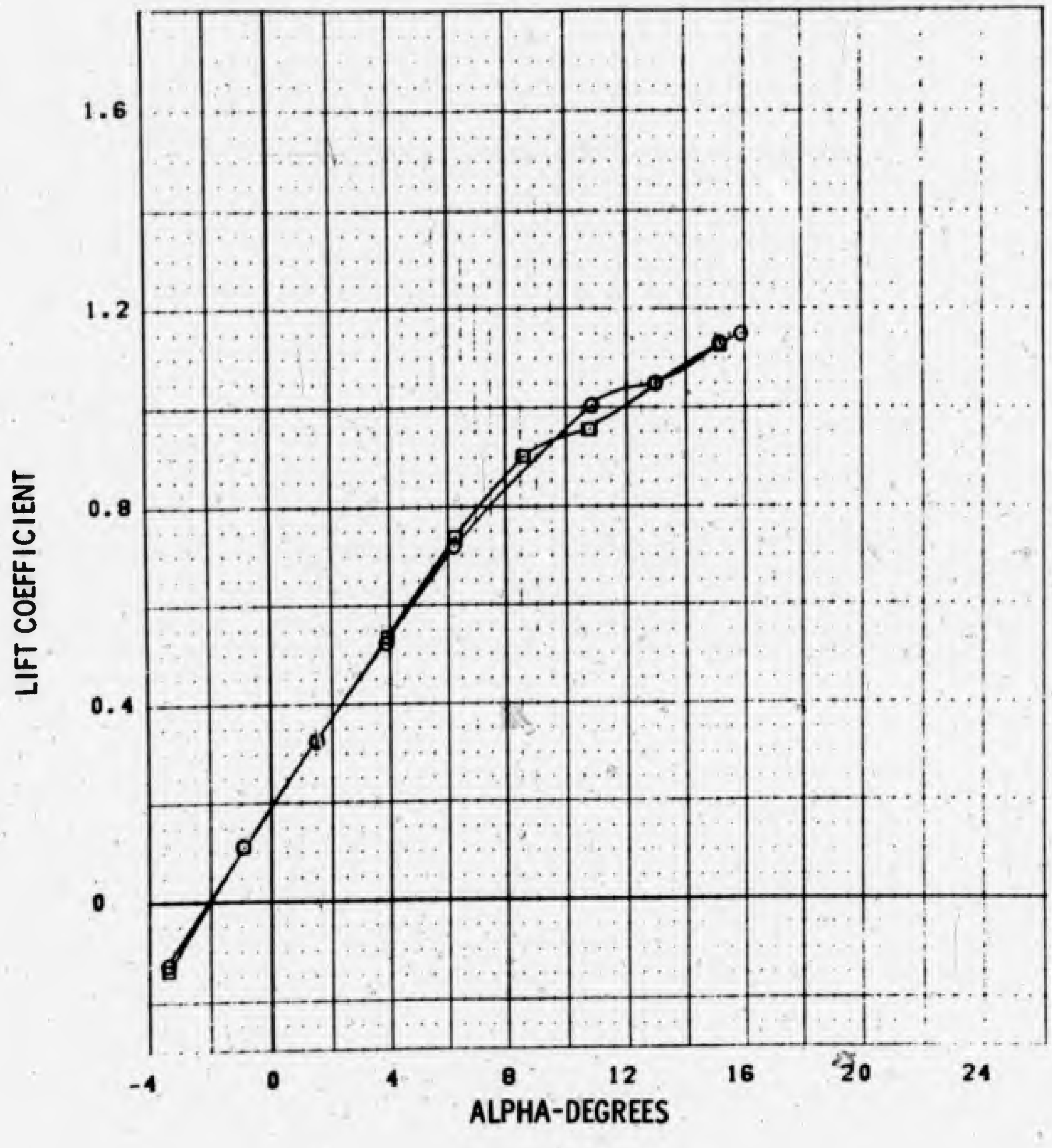
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	48	K1 10/10	OFF
⊡	PWT 4T TC-043	73	K2 10/10	OFF

FIGURE 113d EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



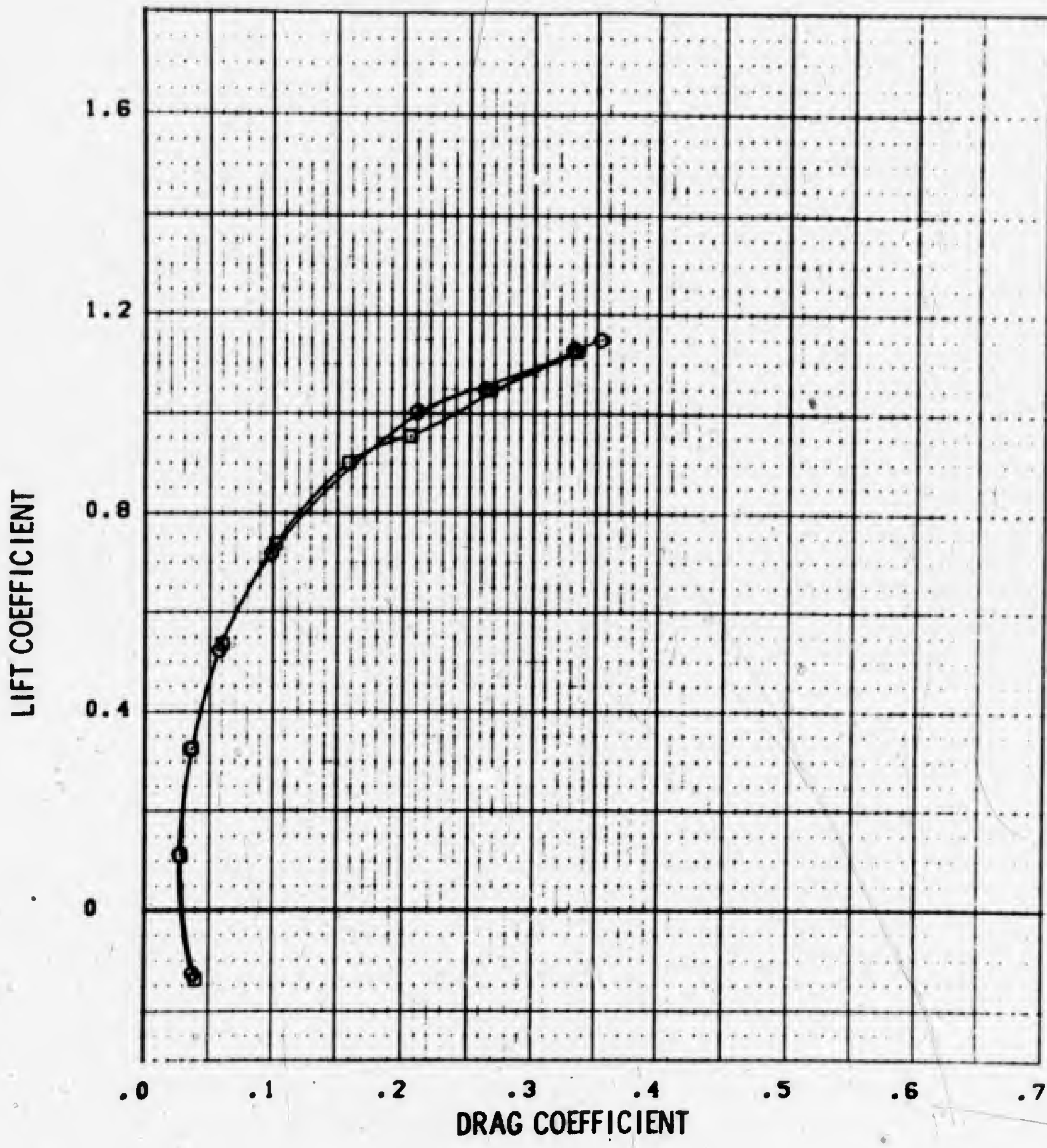
SYM	TEST	INCREMENT (K2 K1)	L.E. (L/R)	...
○	PWT 4T TC-043	PN 73 - PN 48	10/10	OFF

FIGURE 113d EFFECT OF ALTERNATE LEADING EDGE
M = 0.8



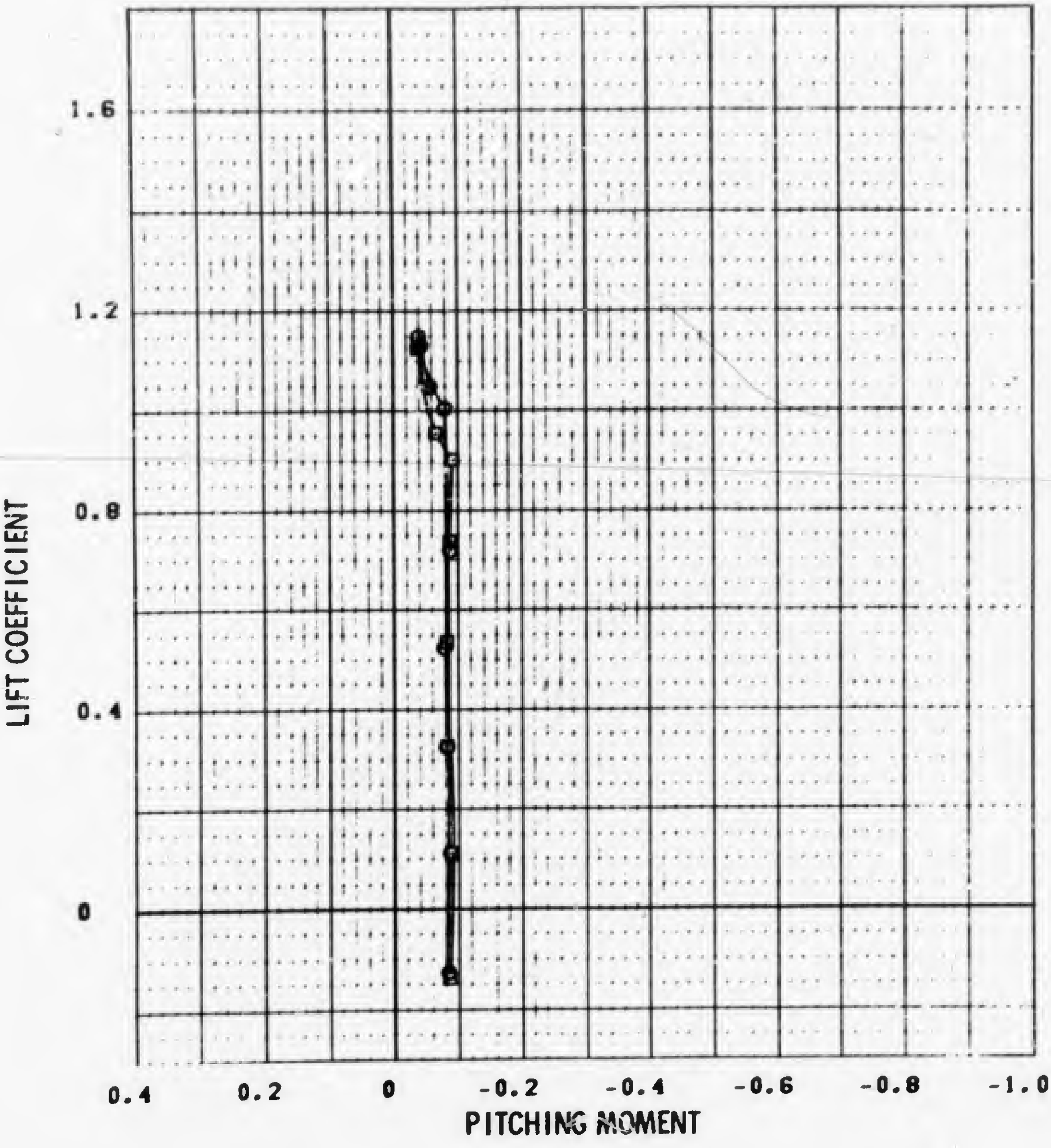
SYM	TEST	PART	L.E.	(L/R)	H.T.
⊙	PWT 4T TC-043	30	K1	0/0	OFF
⊡	PWT 4T TC-043	61	K2	0/0	OFF

FIGURE 113e EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



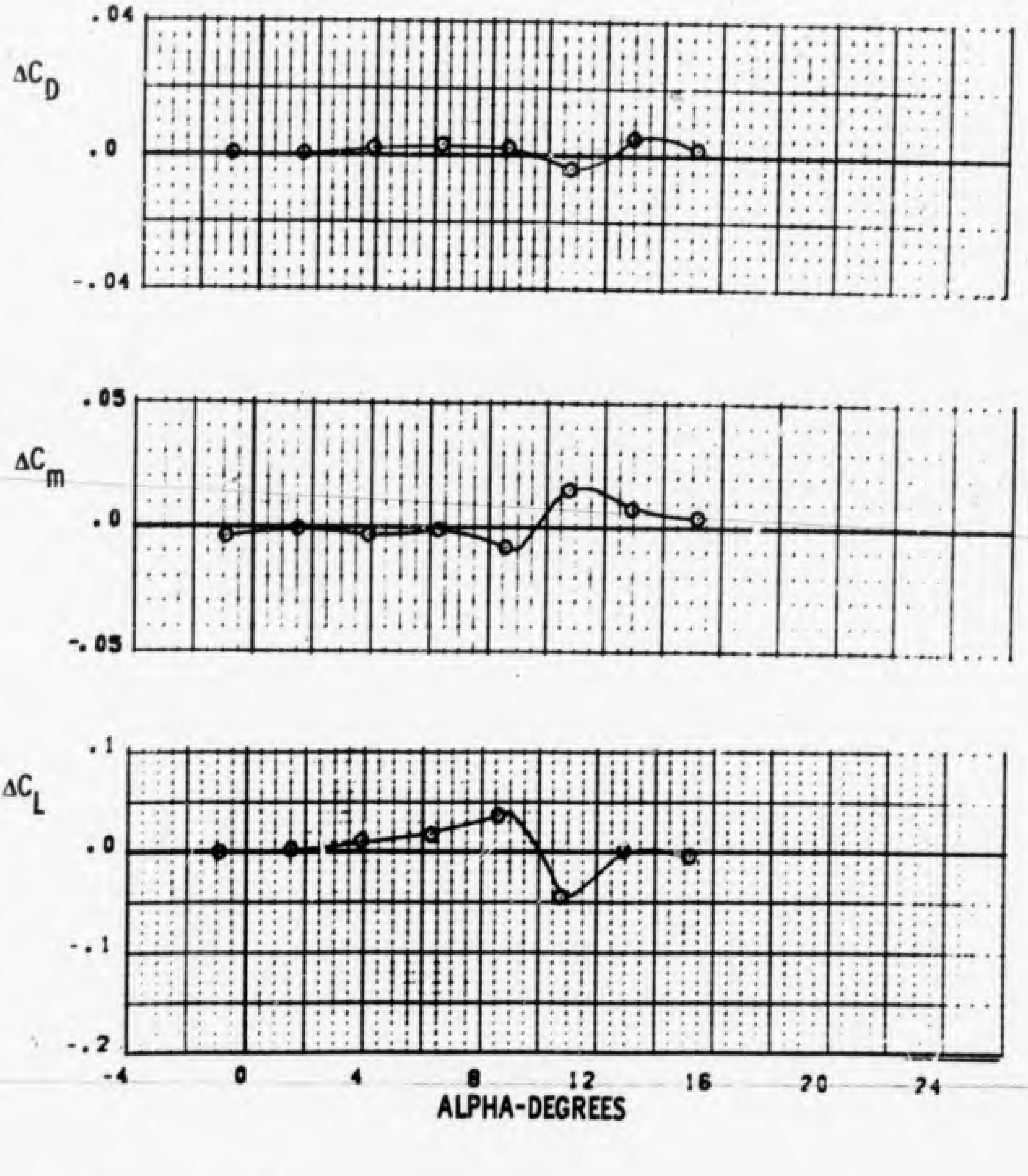
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	30	K1 0/0	OFF
⊡	PWT 4T TC-043	61	K2 0/0	OFF

FIGURE 113e EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



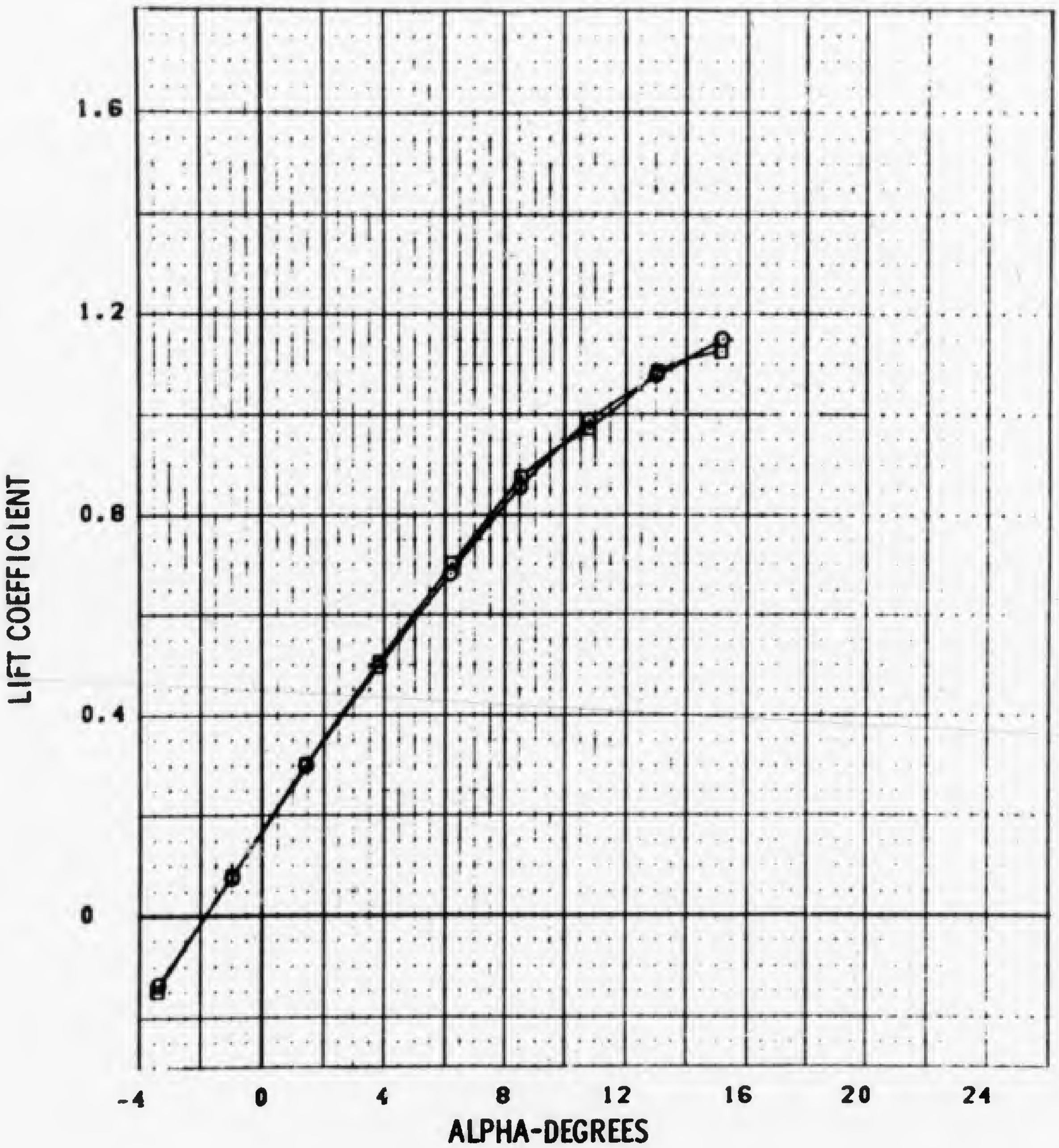
SYM	TEST	PART	L.E. (L/R)	H.T.
O	PWT 4T TC-043	30	K1 0/0	OFF
□	PWT 4T TC-043	61	K2 0/0	OFF

FIGURE 113e EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



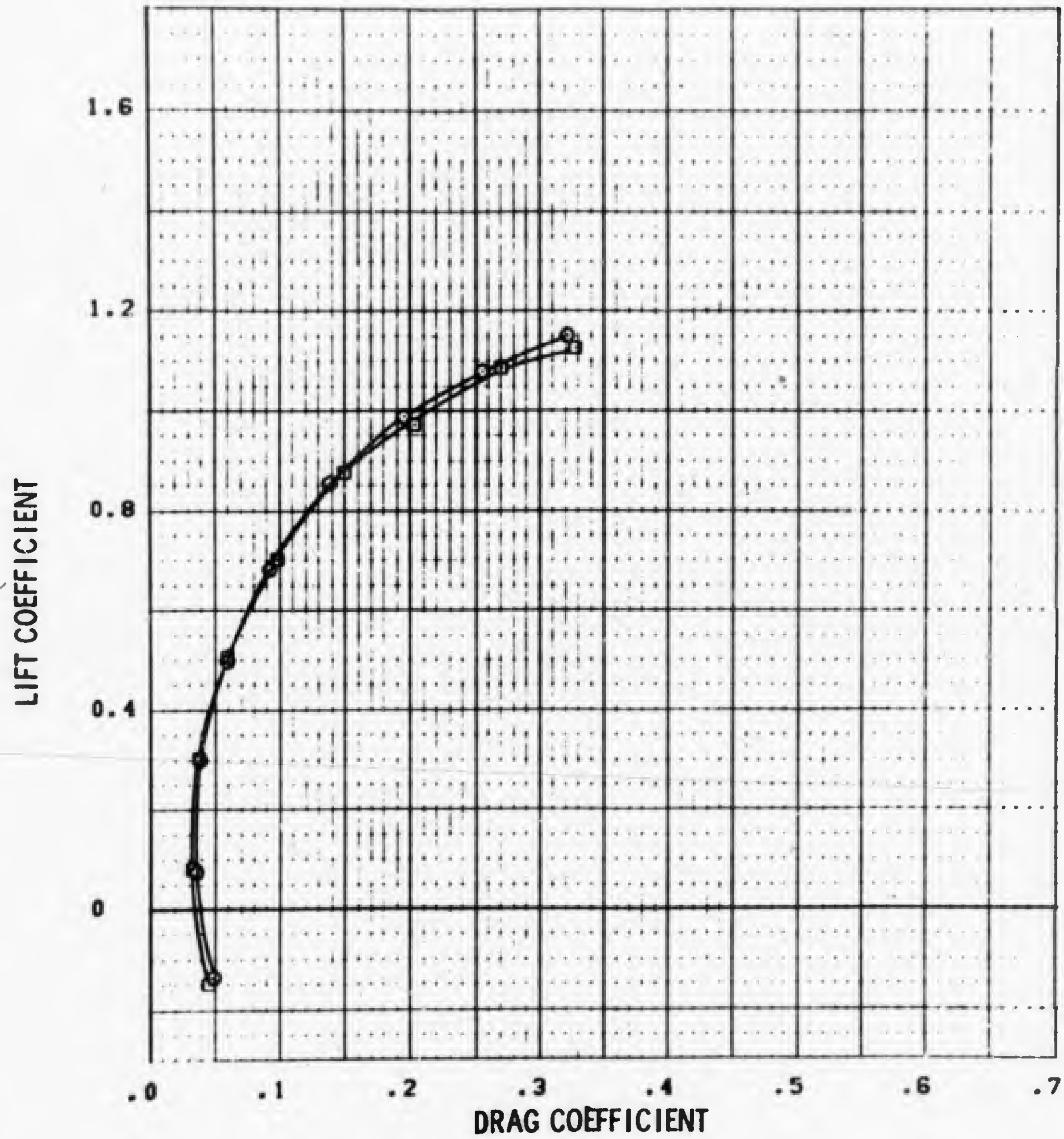
SYM	TEST	INCREMENT (K2 - K1)	L.E. (L/R)	
⊙	PWT 4T TC-043	PN 61 - PN 30	0/0	0

FIGURE 113e EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



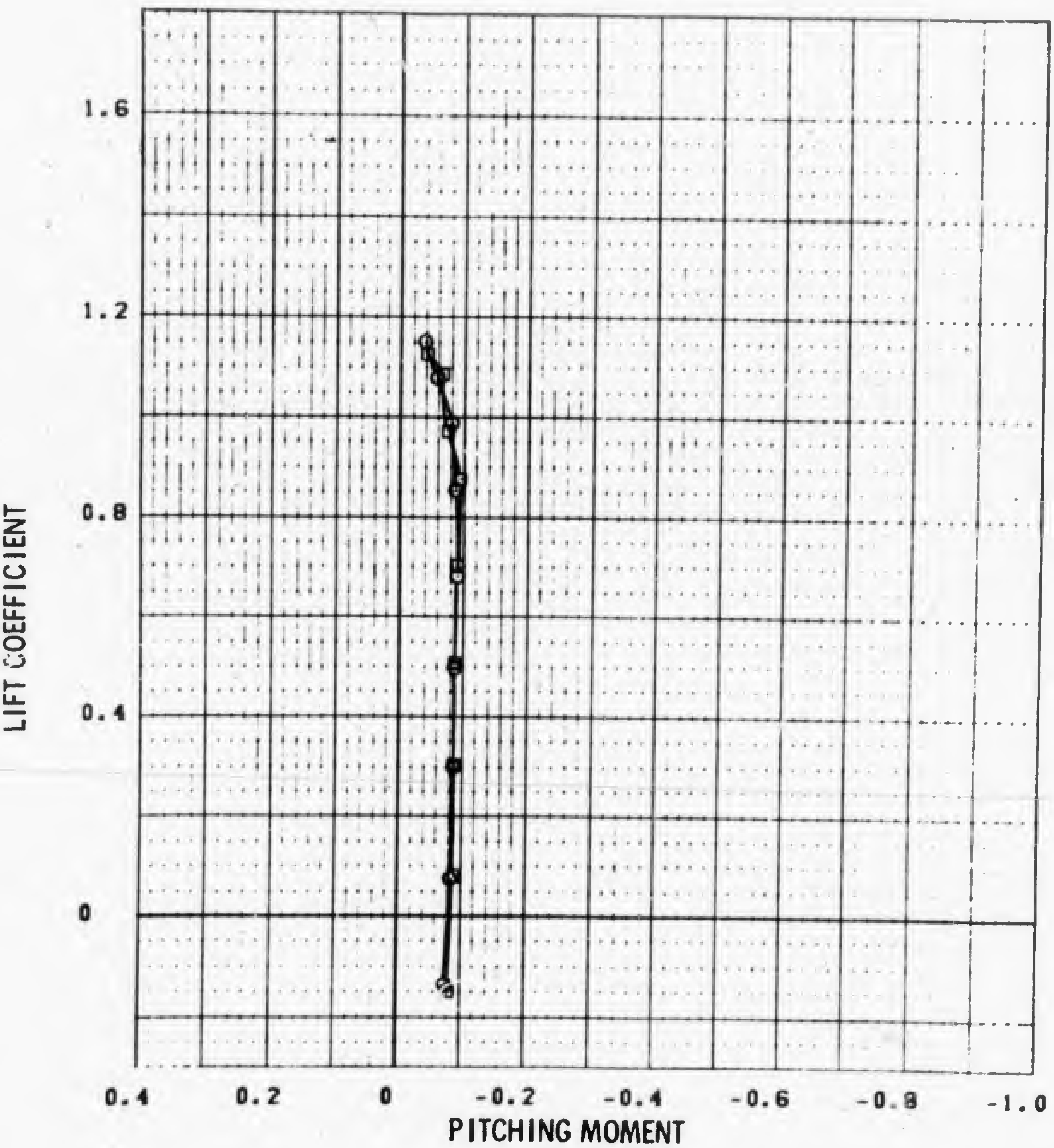
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	37	K1 5/5	OFF
⊡	PWT 4T TC-043	68	K2 5/5	OFF

FIGURE 113f EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



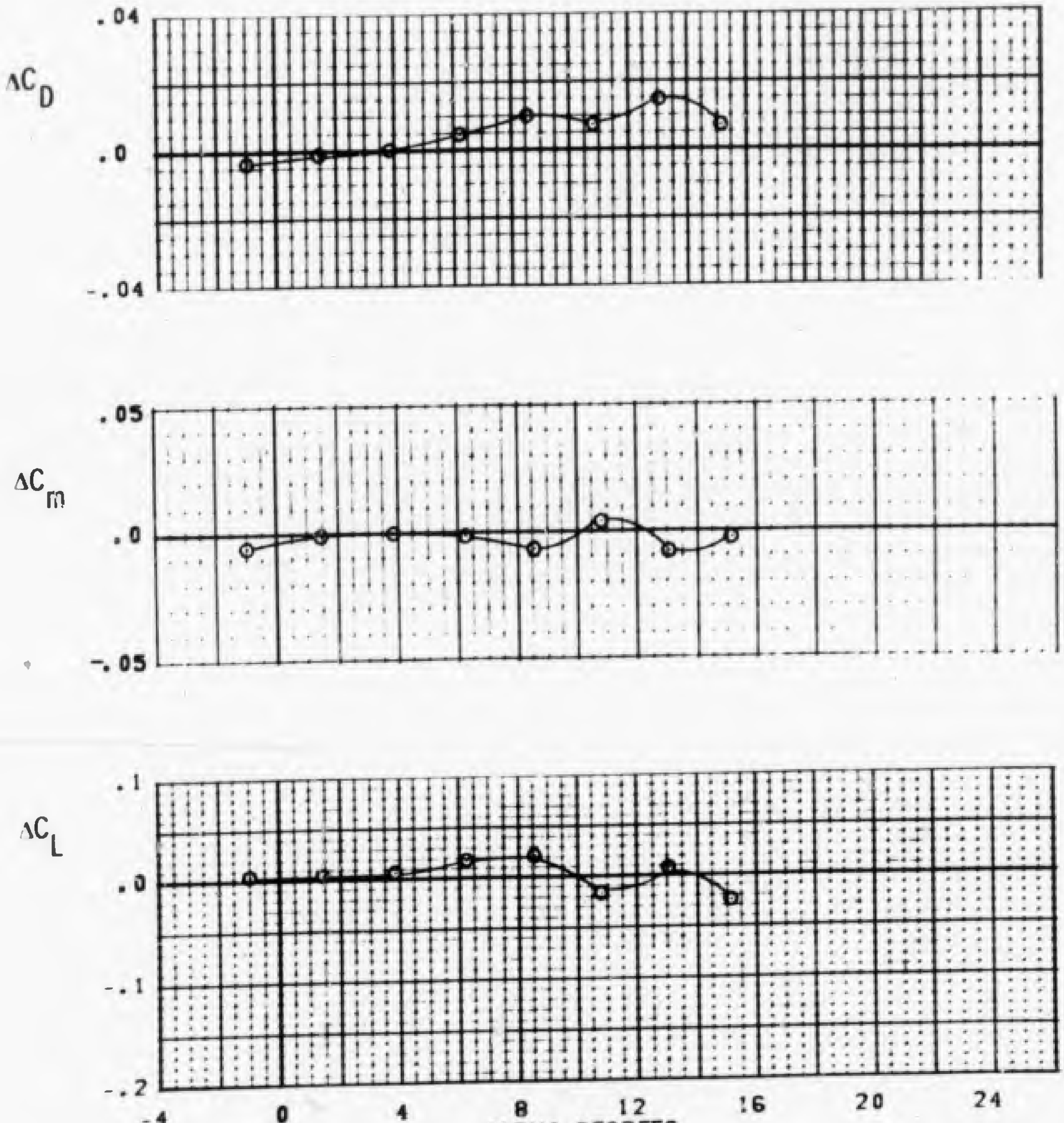
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	37	K1 5/5	OFF
⊡	PWT 4T TC-043	68	K2 5/5	OFF

FIGURE 113f EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



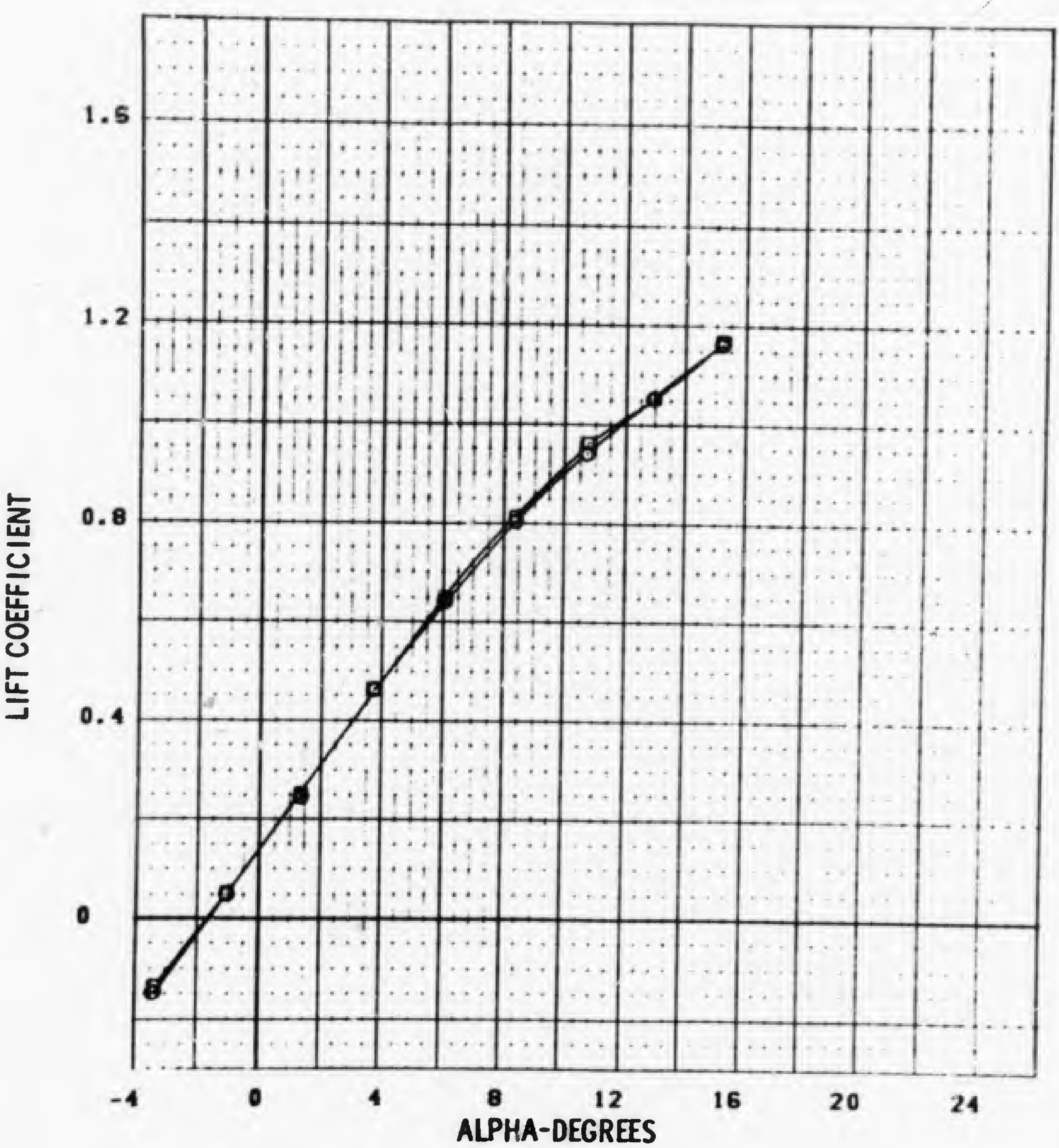
SYM	TEST	PART	L.E. (L/R)	H.T.
○	PWT 4T TC-043	37	K1 5/5	OFF
◻	PWT 4T TC-043	68	K2 5/5	OFF

FIGURE 113f EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



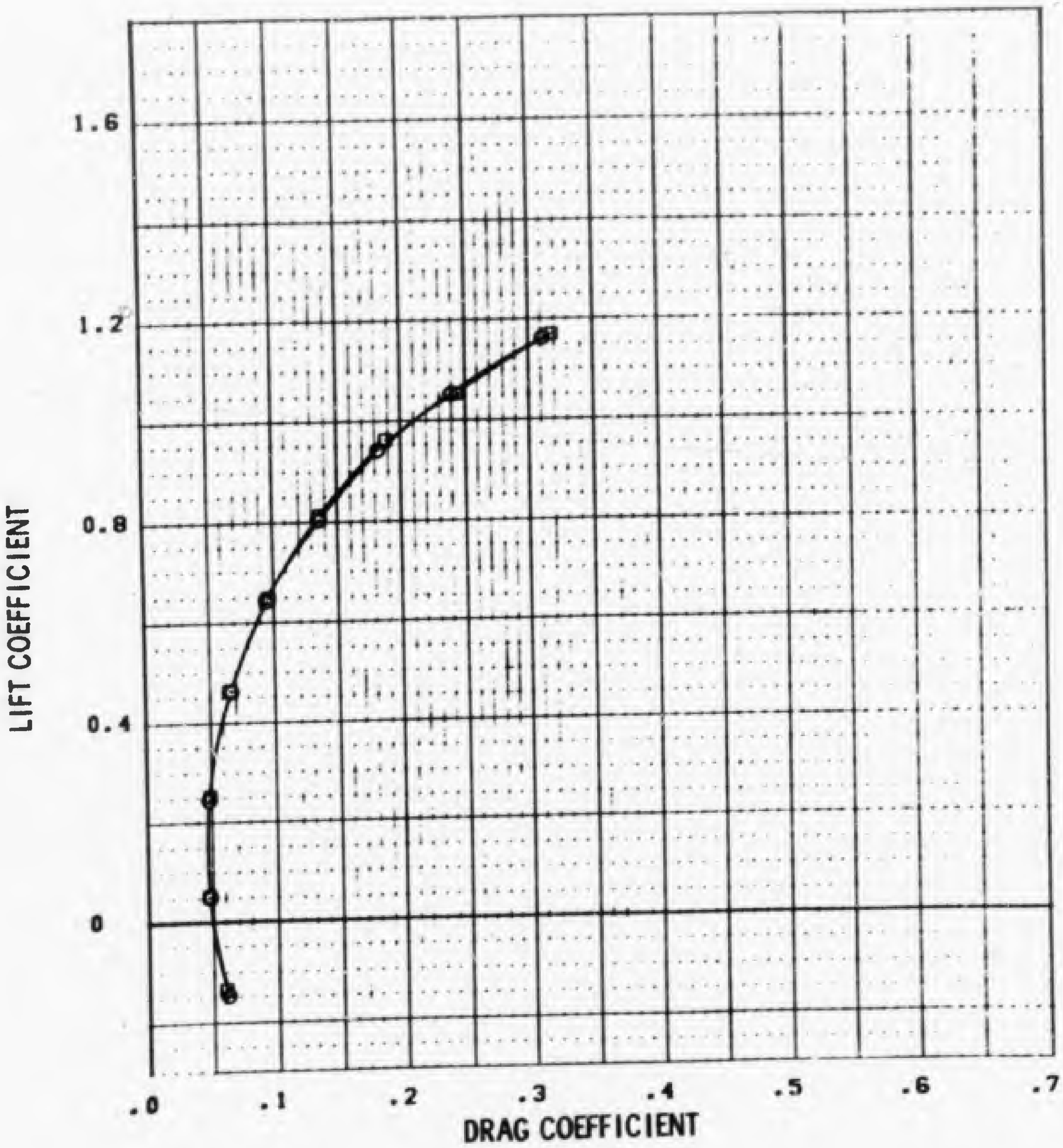
SYM	TEST	INCREMENT (K2 - K1)	L.E. (L/R)	...
⊙	PWT 4T TC-043	PN 68 - PN 37	5/5	OFF

FIGURE 113E EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



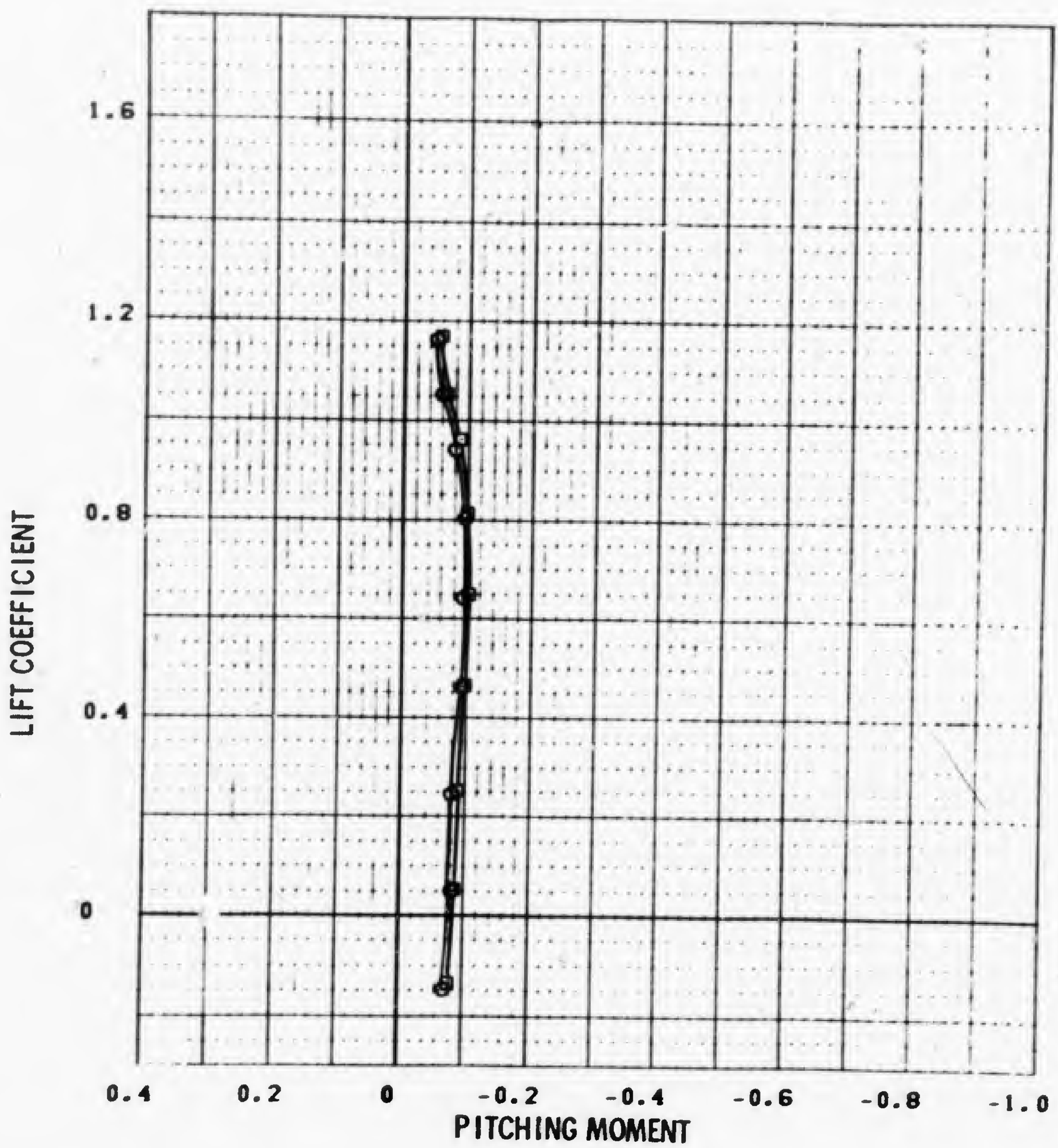
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	47	K1 10/10	OFF
⊡	PWT 4T TC-043	72	K2 10/10	OFF

FIGURE 113g EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



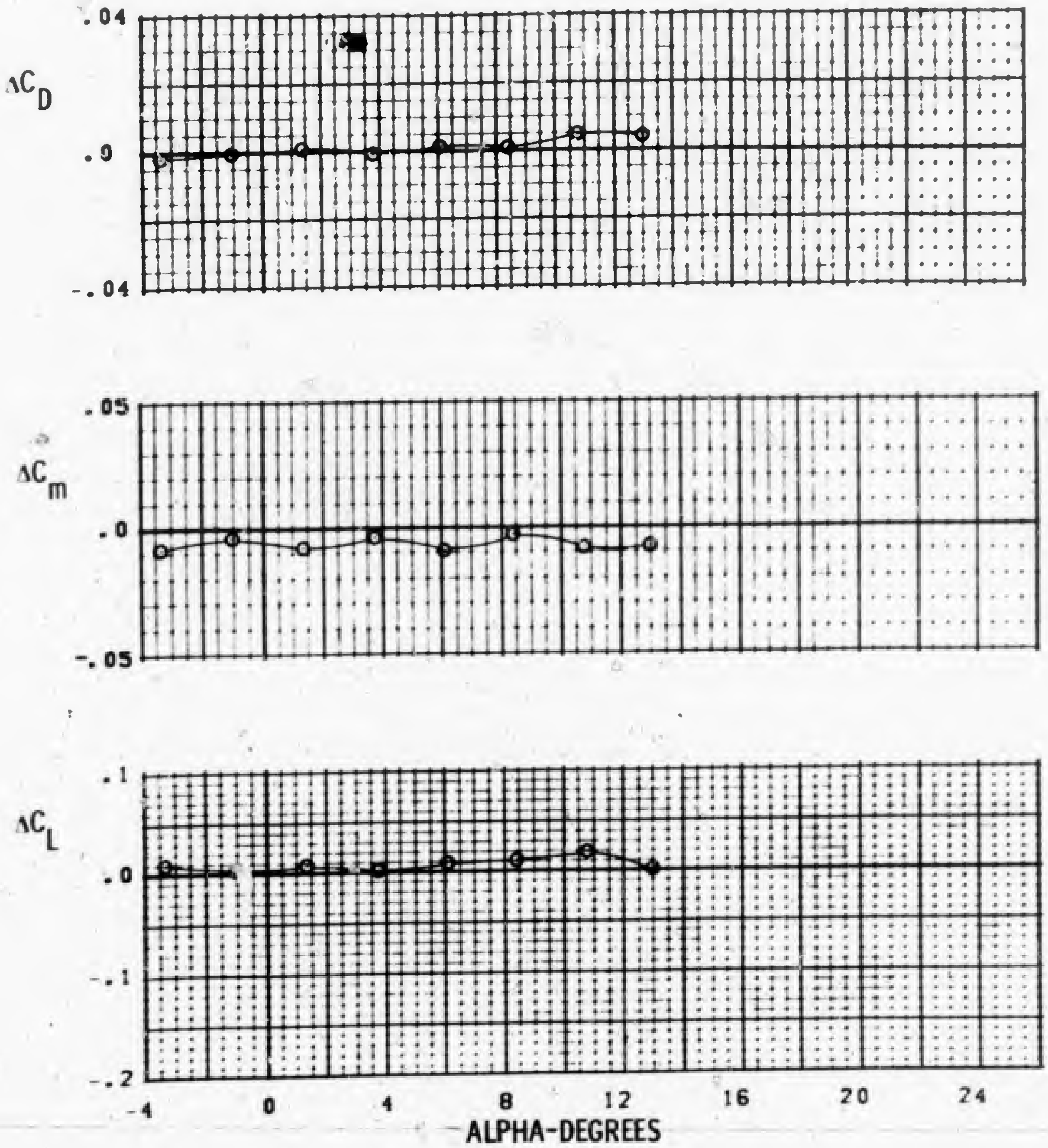
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	47	K1 10/10	OFF
⊡	PWT 4T TC-043	72	K2 10/10	OFF

FIGURE 113g EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



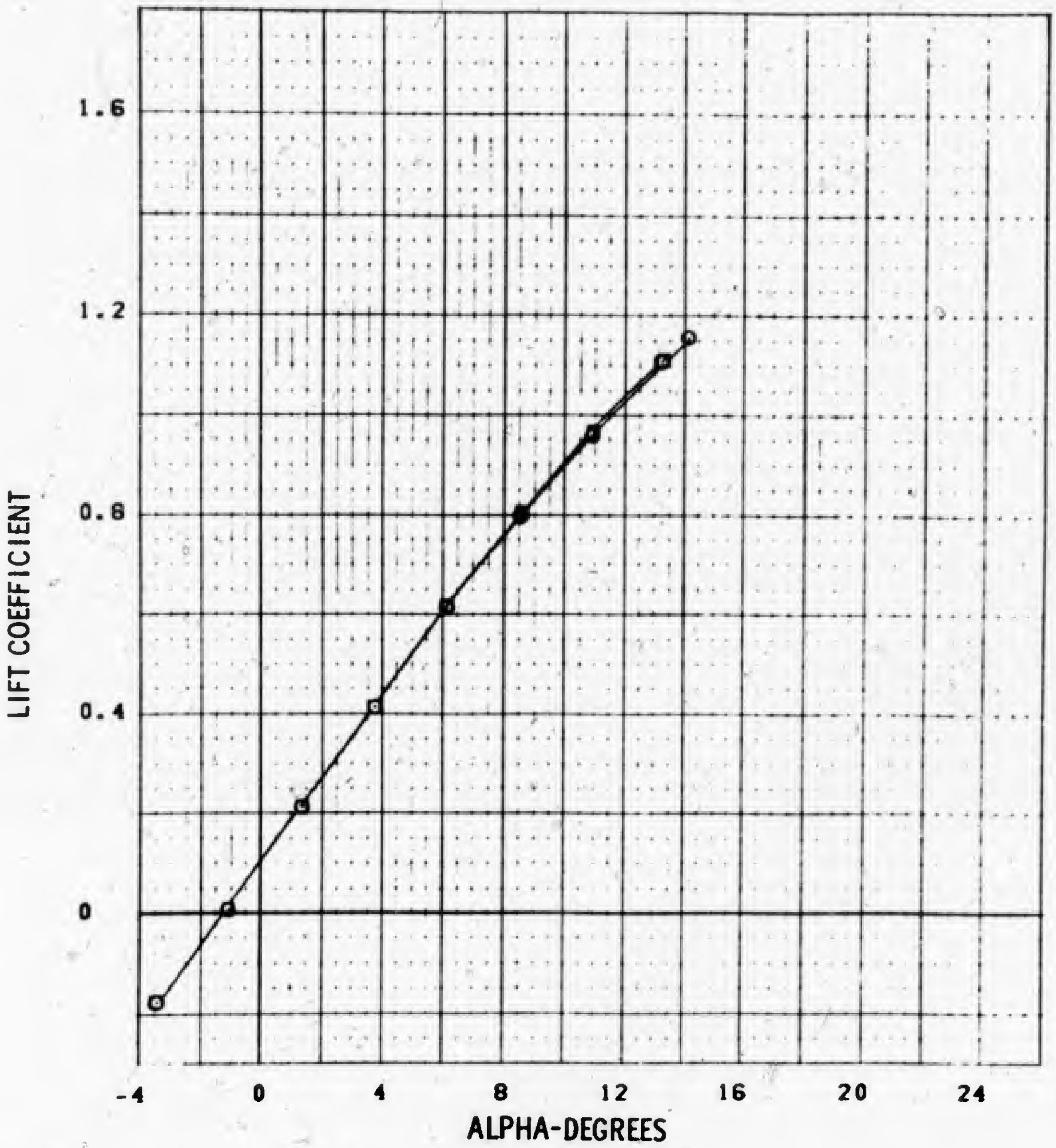
SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	47	K1 10/10	OFF
⊡	PWT 4T TC-043	72	K2 10/10	OFF

FIGURE 113g EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



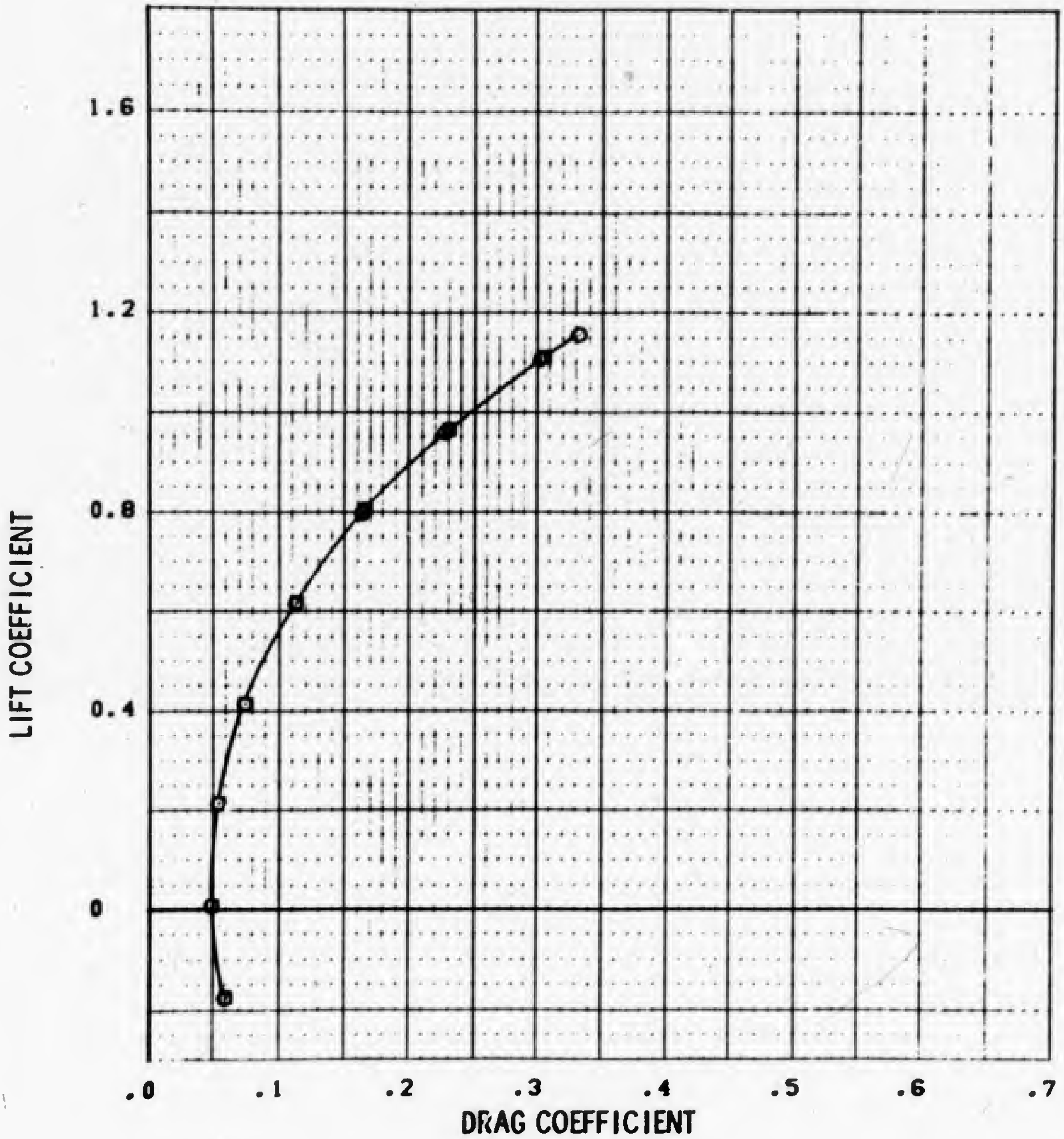
SYM	TEST	INCREMENT (K2 - K1)	L.E. (L/R)	H.T.
O	PWT 4T TC-043	PN 72 - PN 47	10/10	OFF

FIGURE 113g EFFECT OF ALTERNATE LEADING EDGE
M = 0.9



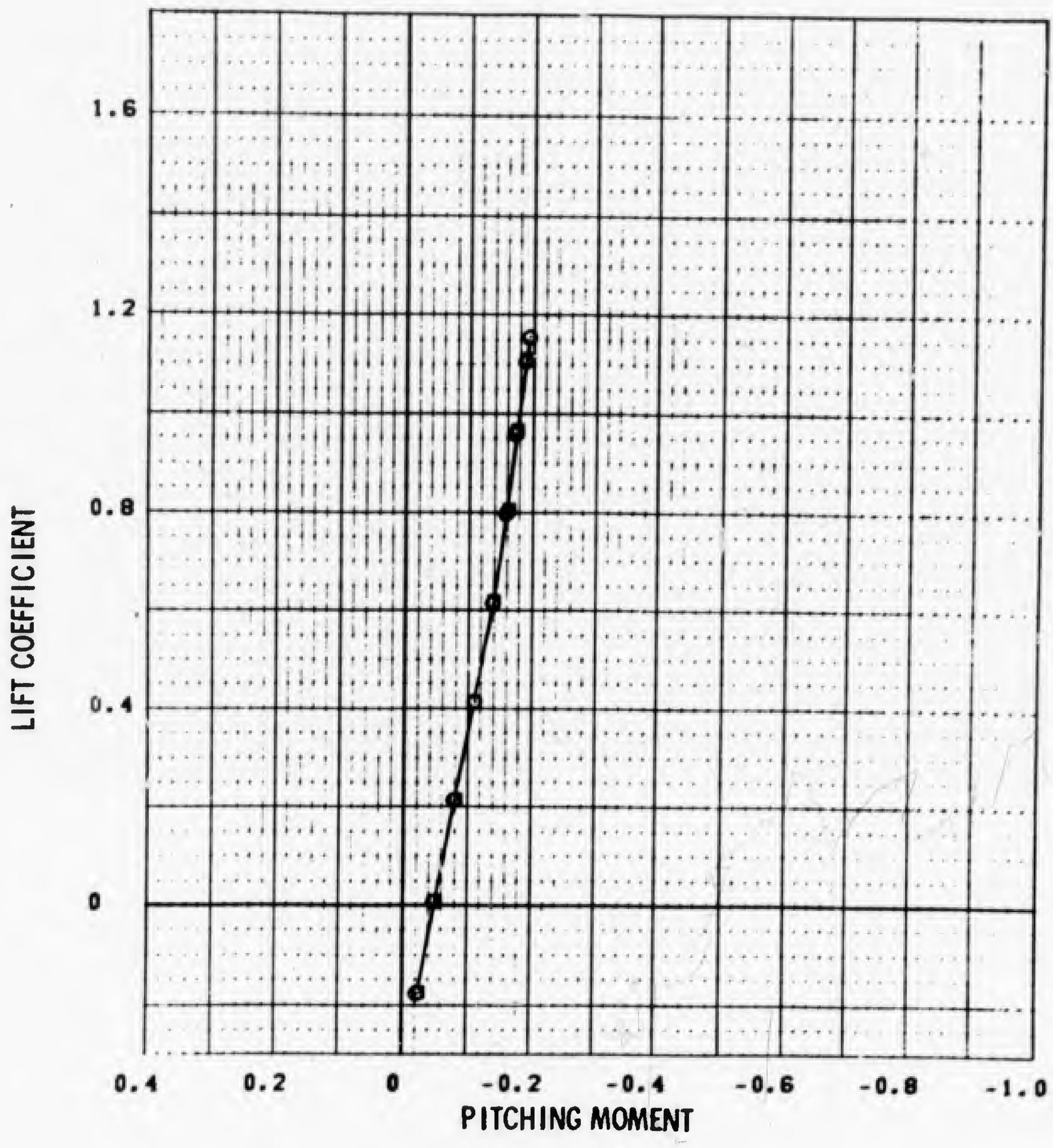
SYM	TEST	PART	L.E. (L/R)	H.T.
○	PWT 4T TC-043	33	K1 0/0	OFF
□	PWT 4T TC-043	64	K2 0/0	OFF

FIGURE 113h EFFECT OF ALTERNATE LEADING EDGE
M = 1.2



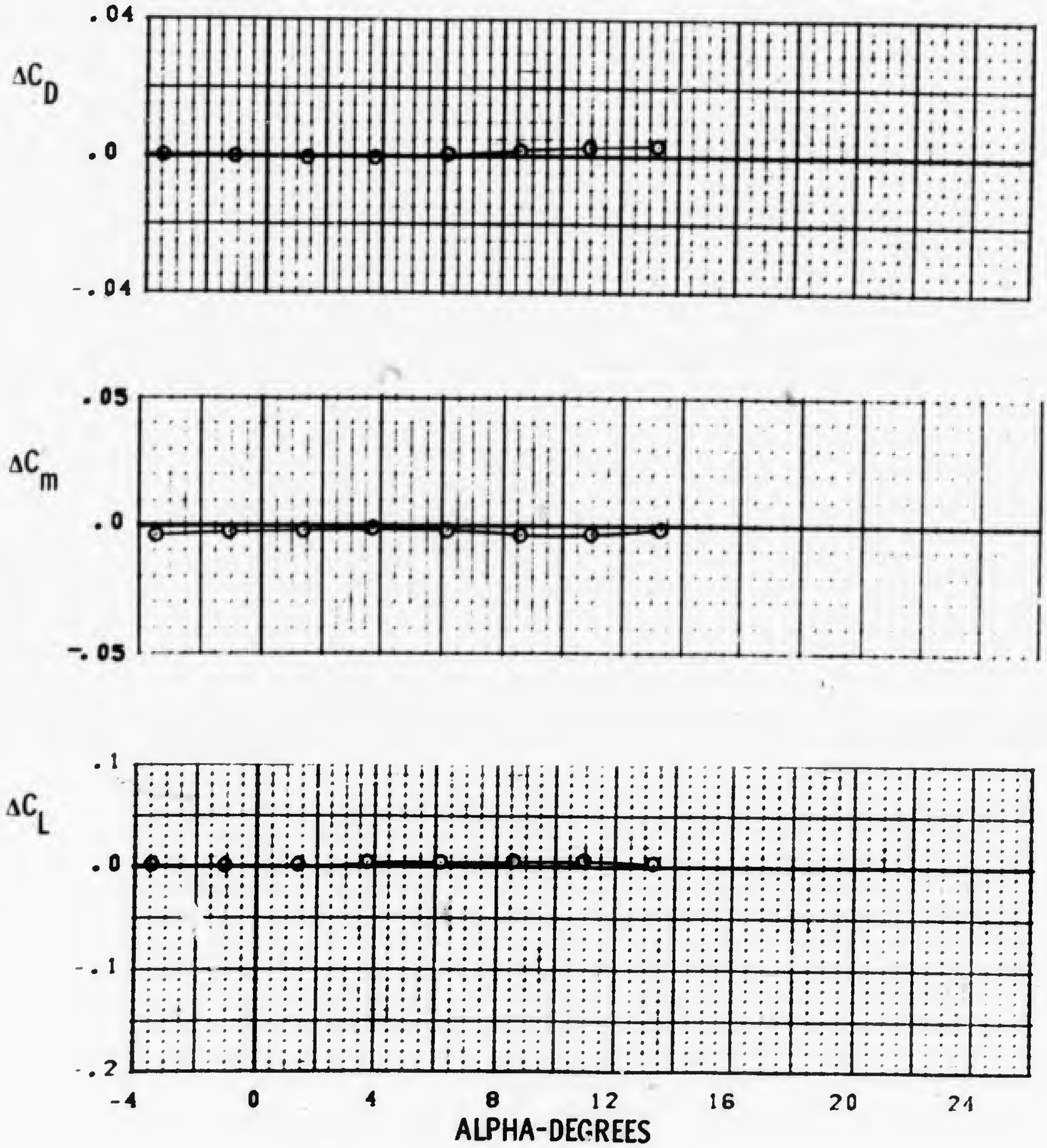
SYM	TEST	PART	L.E.	(L/R)	H.T.
⊙	PWT 4T TC-043	33	K1	0/0	OFF
⊡	PWT 4T TC-043	64	K2	0/0	OFF

FIGURE 113h EFFECT OF ALTERNATE LEADING EDGE
M = 1.2



SYM	TEST	PART	L.E. (L/R)	H.T.
⊙	PWT 4T TC-043	33	K1 0/0	OFF
⊡	PWT 4T TC-043	64	K2 0/0	OFF

FIGURE 113h EFFECT OF ALTERNATE LEADING EDGE
M = 1.2



SYM	TEST	INCREMENT (K2 - K1)	L.E. (/R)	..
⊙	PWT 4T TC-043	PN 64 - PN 33	0/0	0

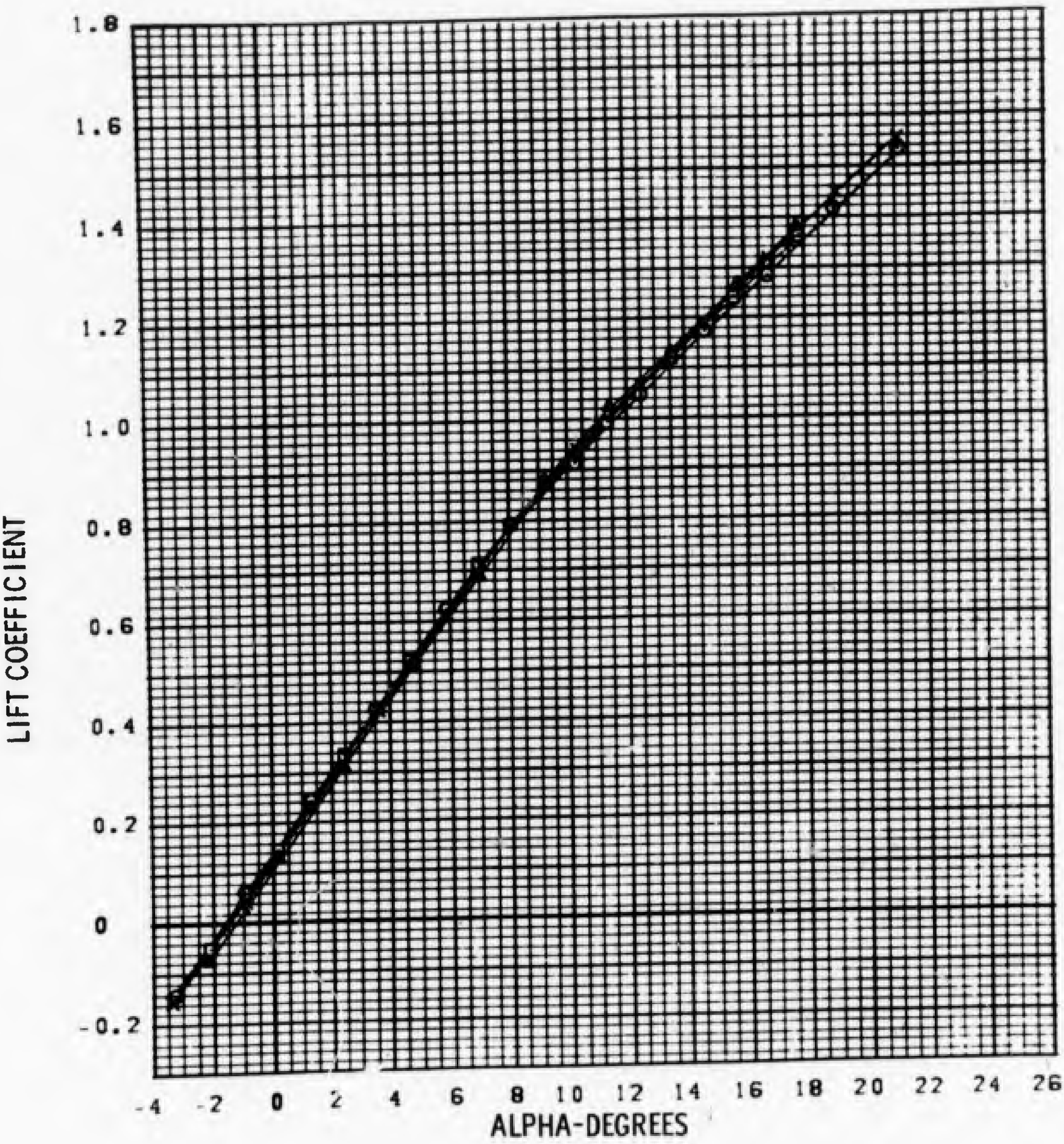
FIGURE 113h EFFECT OF ALTERNATE LEADING EDGE
M = 1.2

4. AUXILIARY DEVICES

The effect of the three types of auxiliary devices tested on the longitudinal aerodynamic characteristics of the test configuration are shown by the comparison plots presented in this subsection.

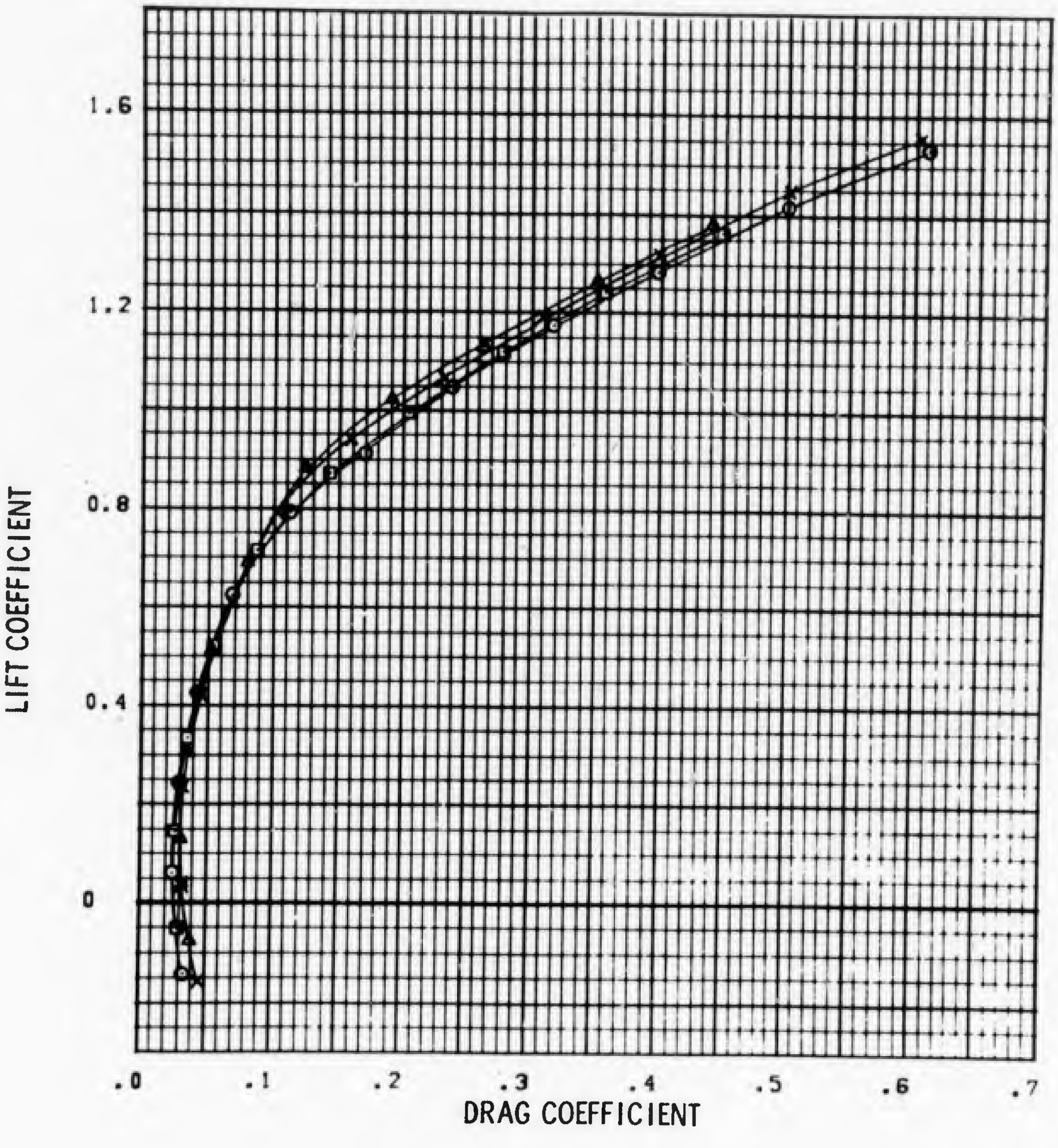
a. Vortex Generators

Comparison plots showing the longitudinal characteristics of the LEDE configuration with and without the vortex generator pattern are presented in the following subsection. A direct comparison between the configurations with and without the generators in the same tunnel entry is not possible. As a result, a comparison is also shown between the two entries into the four foot tunnel to establish a basis for comparison of the two sets of data. The first entry into the 4T are denoted by part numbers prior to part number 317. The second entry begins with part number 400.



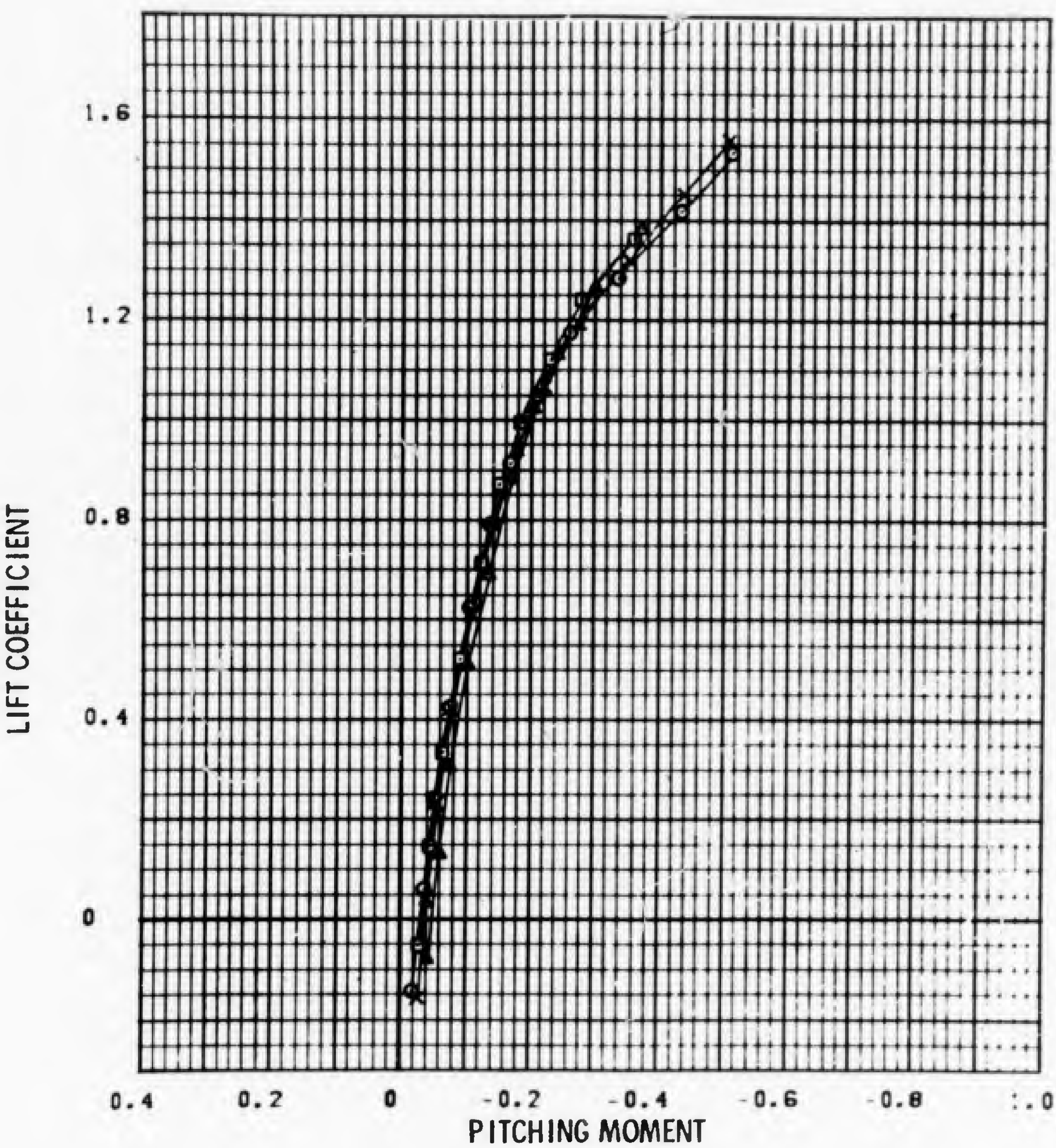
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	268	K1 0/0	OFF
⊡	PWT 4T TC-043	438	K1 0/0	OFF
▲	PWT 4T TC-043	448	K1 5/5	OFF
×	PWT 4T TC-043	243	K1 5/5	ON

FIGURE 114a EFFECT OF VORTEX GENERATORS
M = 0.7



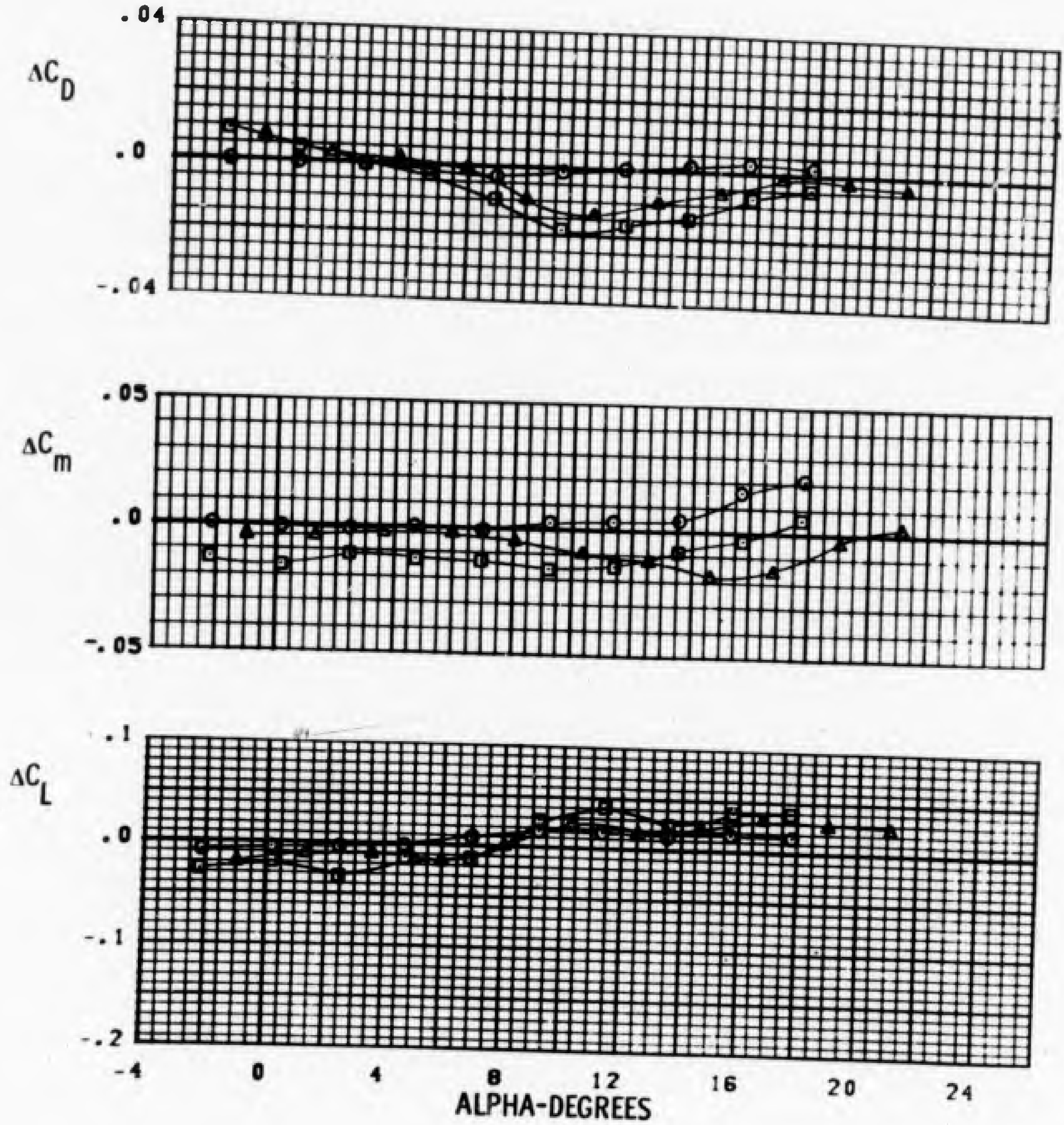
SYM	TEST	PART	L.E. (_ ?)	V.G.
⊙	PWT 4T TC-043	268	K1 0/0	OFF
⊡	PWT 4T TC-043	438	K1 0/0	OFF
▲	PWT 4T TC-043	448	K1 5/5	OFF
×	PWT 4T TC-043	243	K1 5/5	ON

FIGURE 114a EFFECT OF VORTEX GENERATORS
M = 0.7



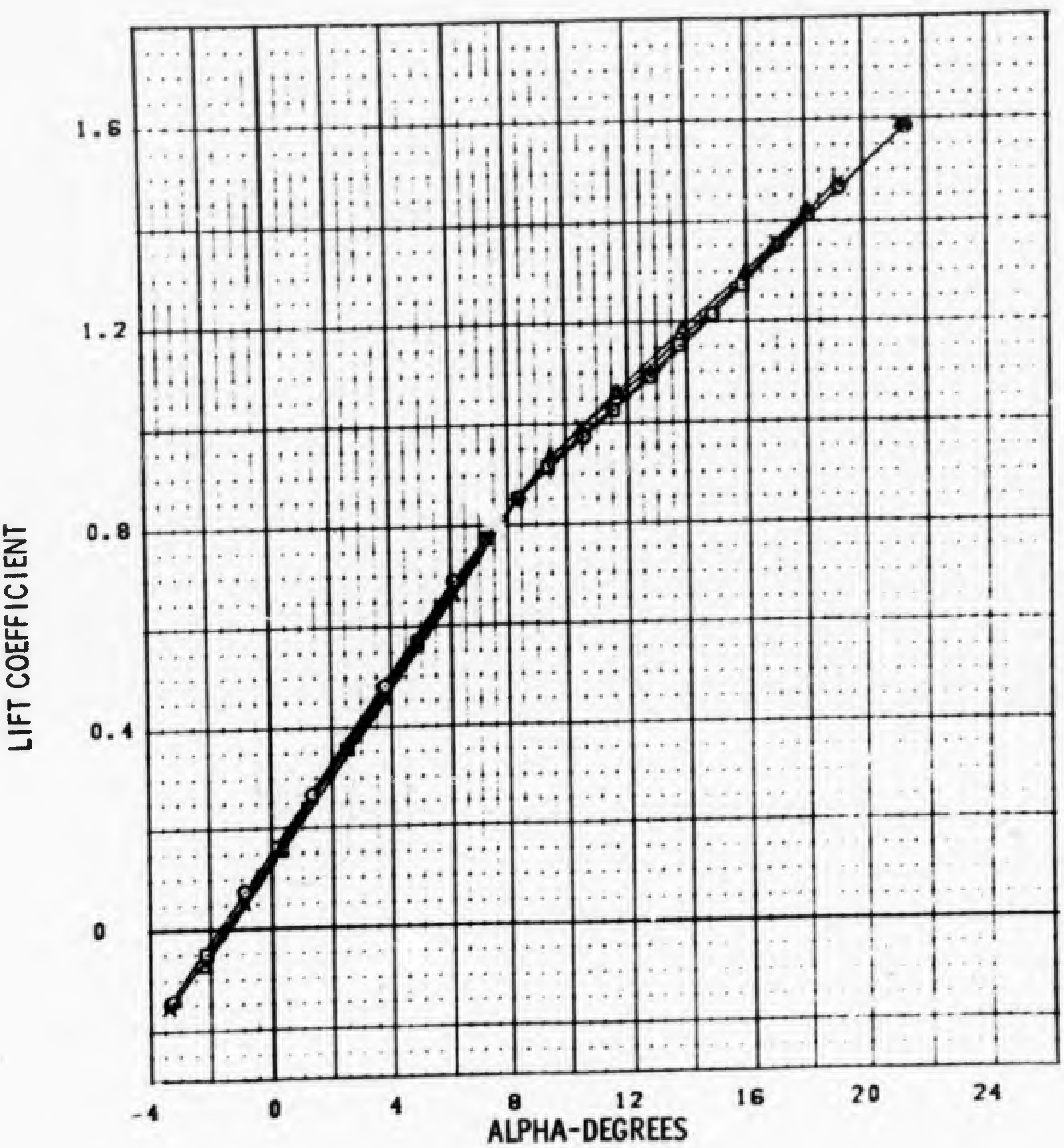
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	268	K1 0/0	OFF
⊡	PWT 4T TC-043	438	K1 0/0	OFF
▲	PWT 4T TC-043	448	K1 5/5	OFF
×	PWT 4T TC-043	243	K1 5/5	ON

FIGURE 114a EFFECT OF VORTEX GENERATORS
M = 0.7



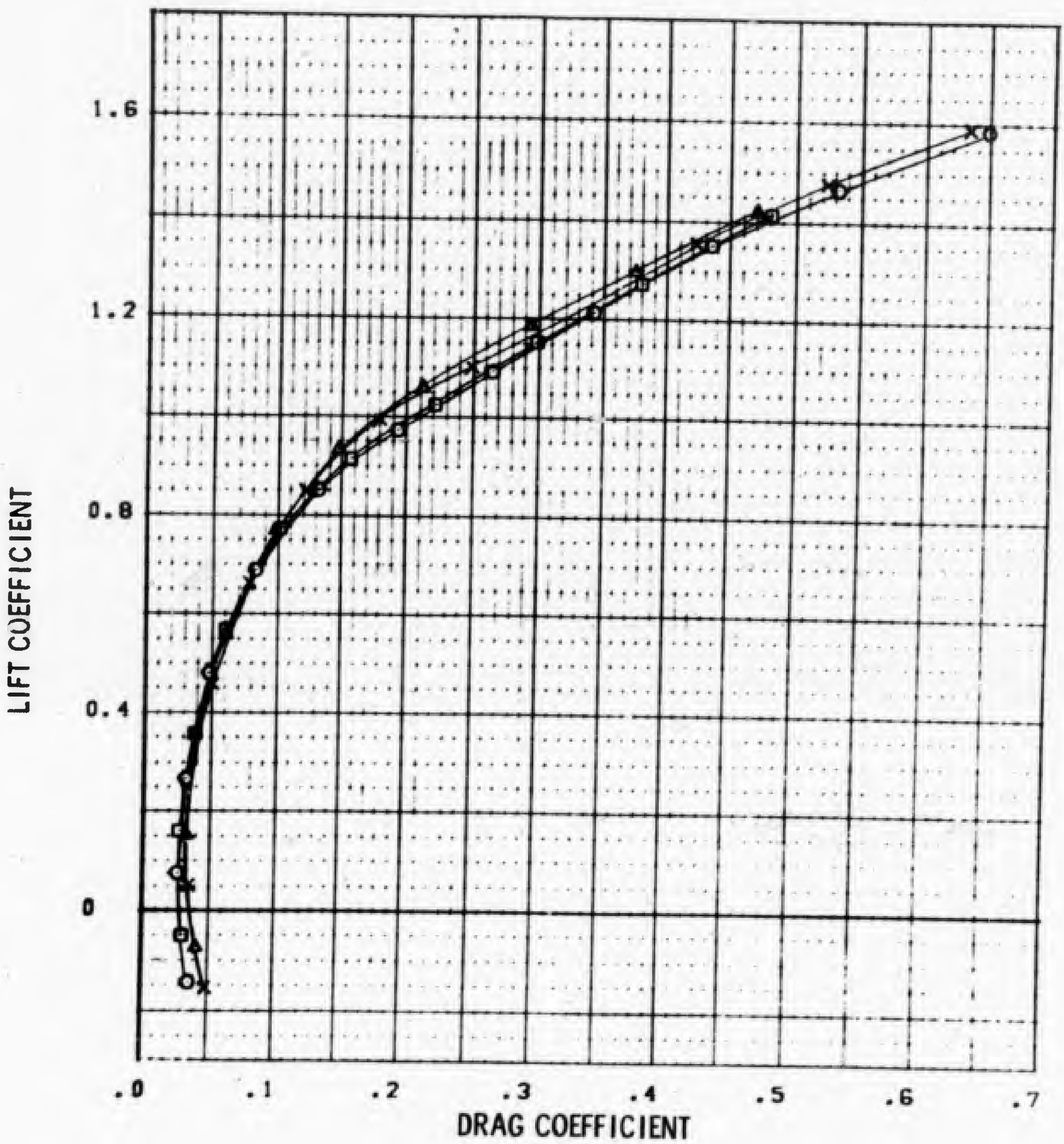
SYM	TEST	INCREMENT	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	PN 438 - PN 268	K1 0/0	OFF
⊡	PWT 4T TC-043	PN 448 - PN 268	K1 5/5	OFF
▲	PWT 4T TC-043	PN 243 - PN 268	K1 5/5	ON

FIGURE 114a EFFECT OF VORTEX GENERATORS
M = 0.7



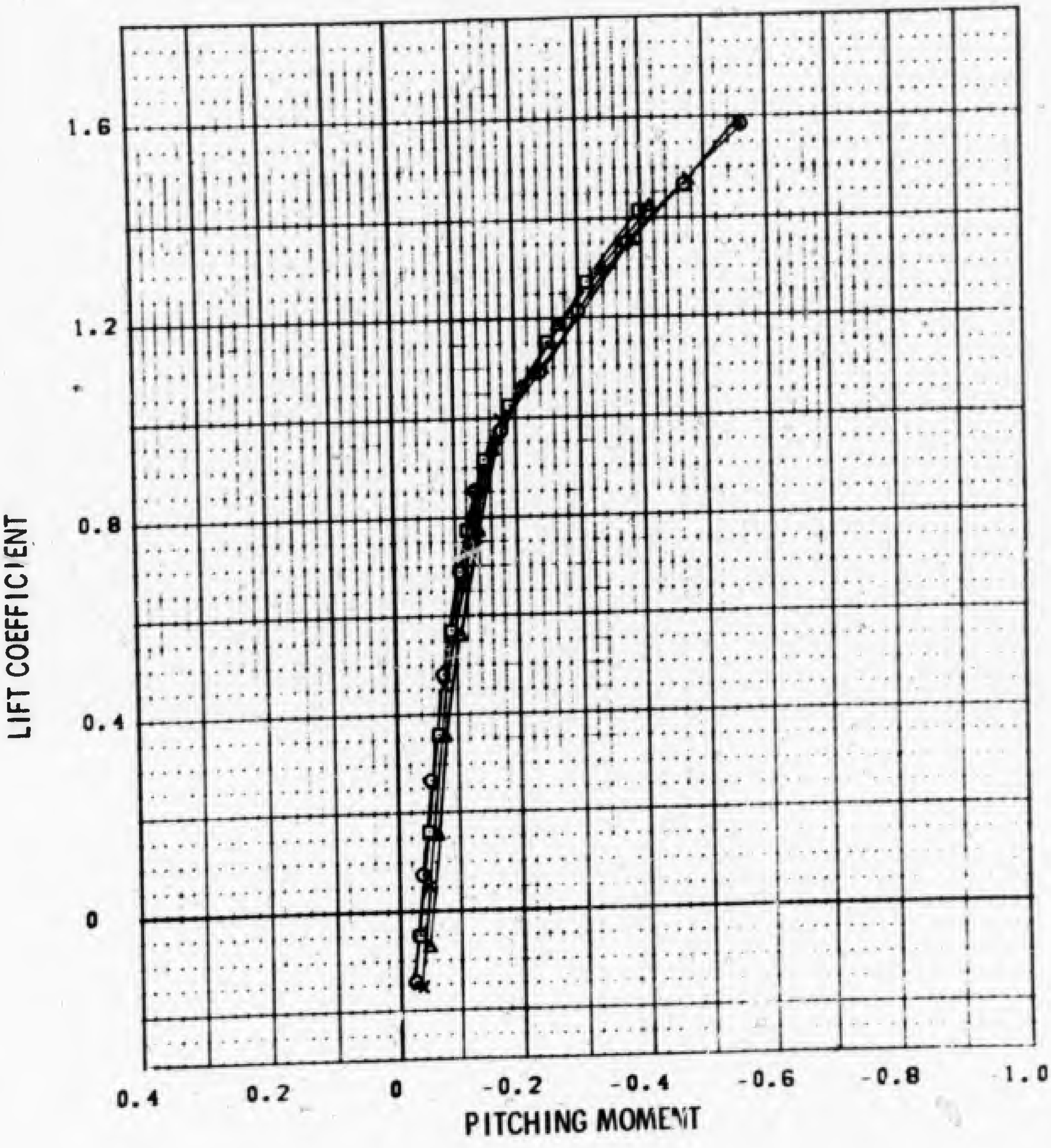
SYM	TEST	PART	L.E. (L/R)		V.G.
⊙	PWT 4T TC-043	267	K1	0/0	OFF
⊡	PWT 4T TC-043	440	K1	0/0	OFF
▲	PWT 4T TC-043	447	K1	5/5	OFF
×	PWT 4T TC-043	242	K1	5/5	ON

FIGURE 114b EFFECT OF VORTEX GENERATORS
M = 0.8



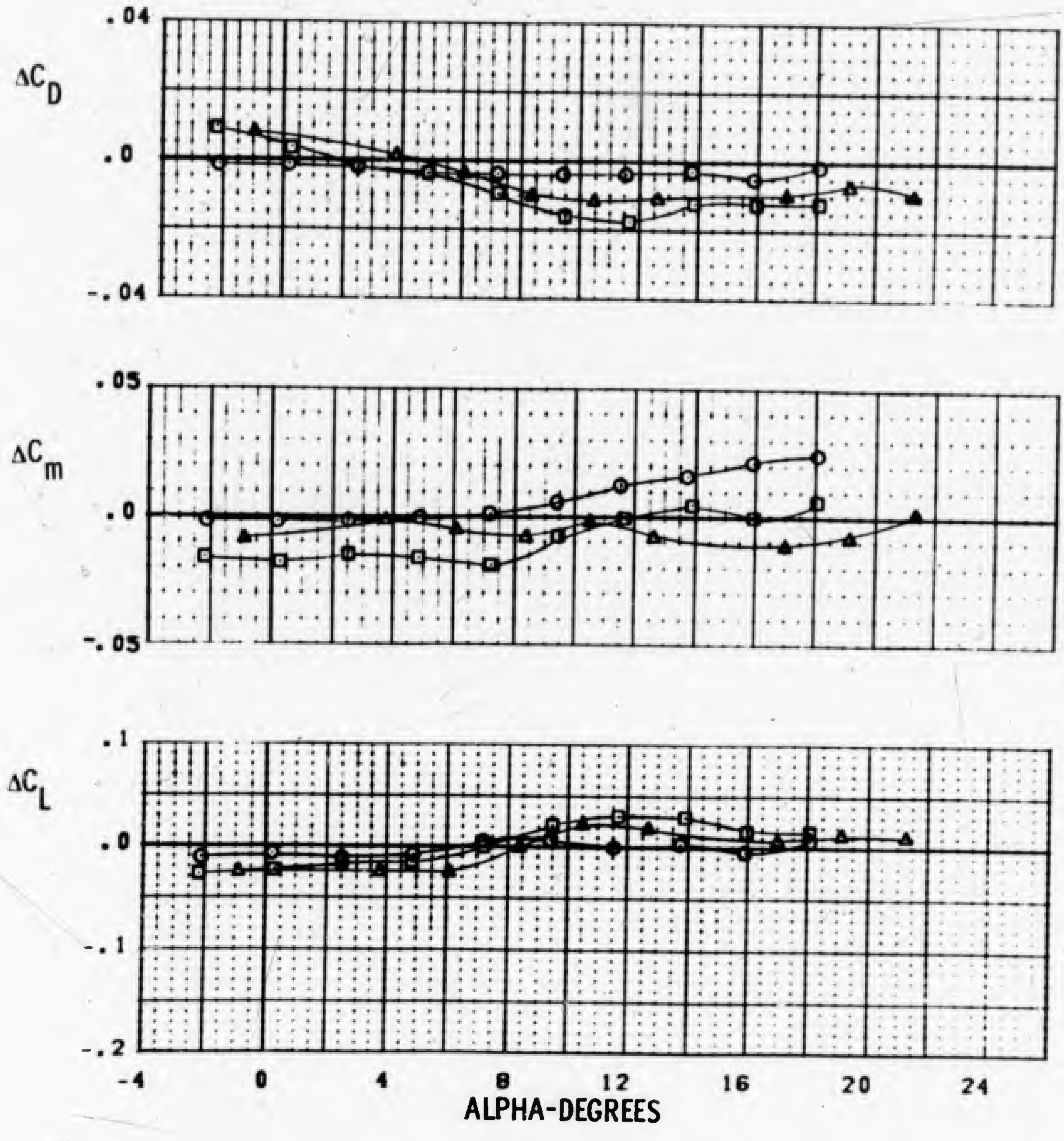
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	267	K1 0/0	OFF
⊡	PWT 4T TC-043	440	K1 0/0	OFF
▲	PWT 4T TC-043	447	K1 5/5	OFF
×	PWT 4T TC-043	242	K1 5/5	ON

FIGURE 114b EFFECT OF VORTEX GENERATORS
M = 0.8



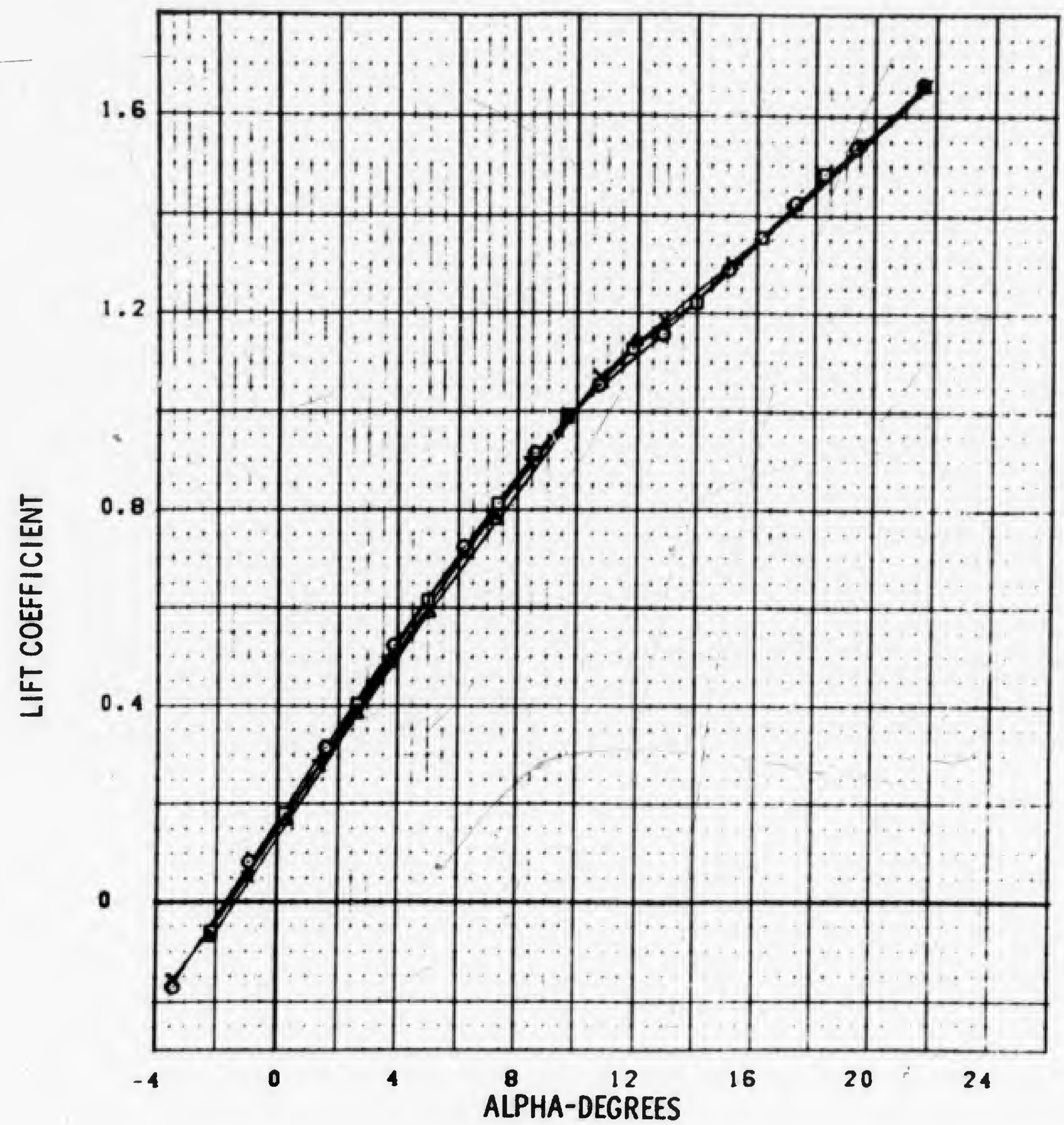
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	267	K1 0/0	OFF
⊡	PWT 4T TC-043	440	K1 0/0	OFF
△	PWT 4T TC-043	447	K1 5/5	OFF
x	PWT 4T TC-043	242	K1 5/5	ON

FIGURE 114b EFFECT OF VORTEX GENERATORS
M = 0.8



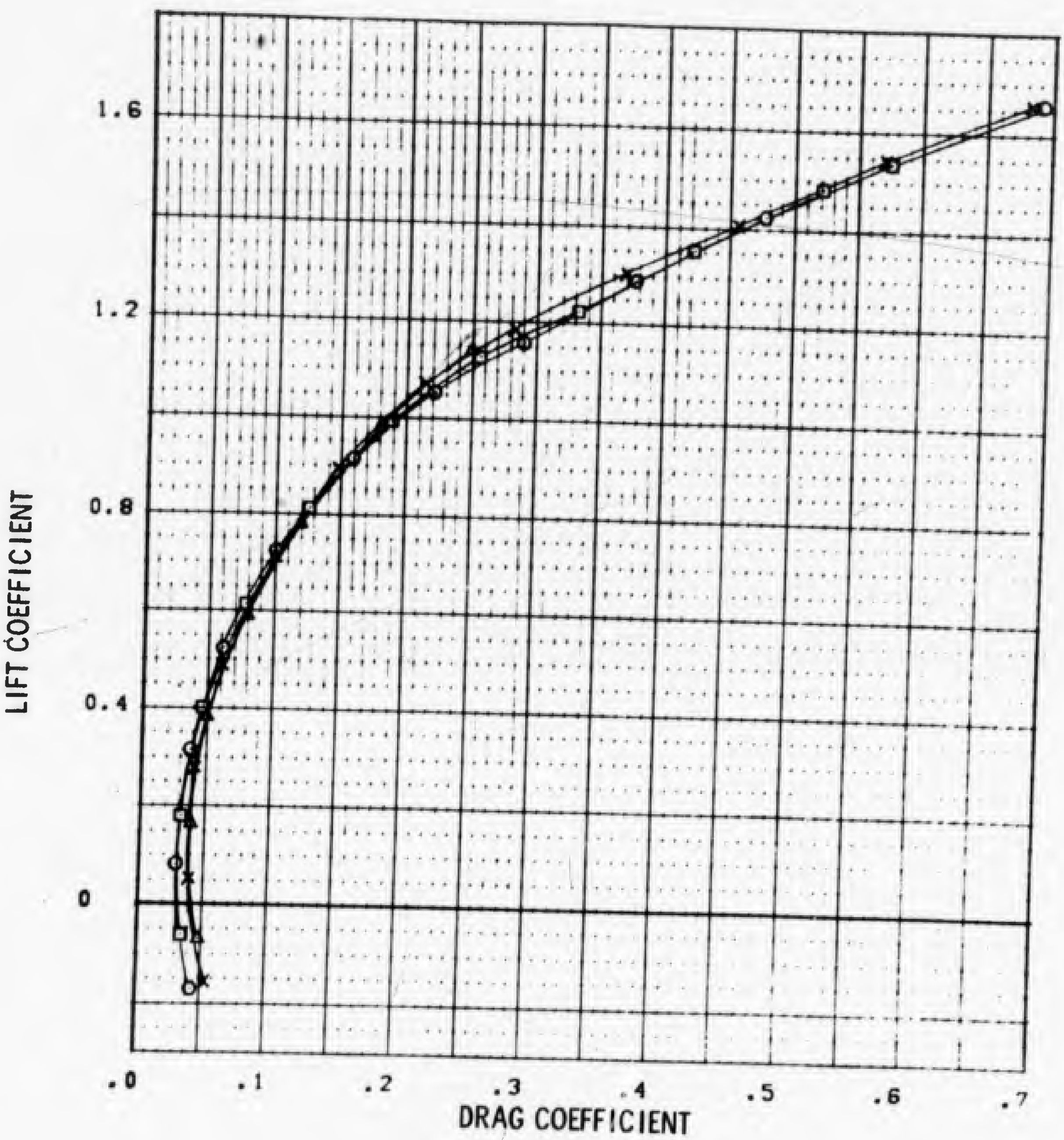
SYM	TEST	INCREMENT	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	PN 440 - PN 267	K1 0/0	OFF
⊡	PWT 4T TC-043	PN 447 - PN 267	K1 5/5	OFF
▲	PWT 4T TC-043	PN 242 - PN 267	K1 5/5	ON

FIGURE 114b EFFECT OF VORTEX GENERATORS
M = 0.8



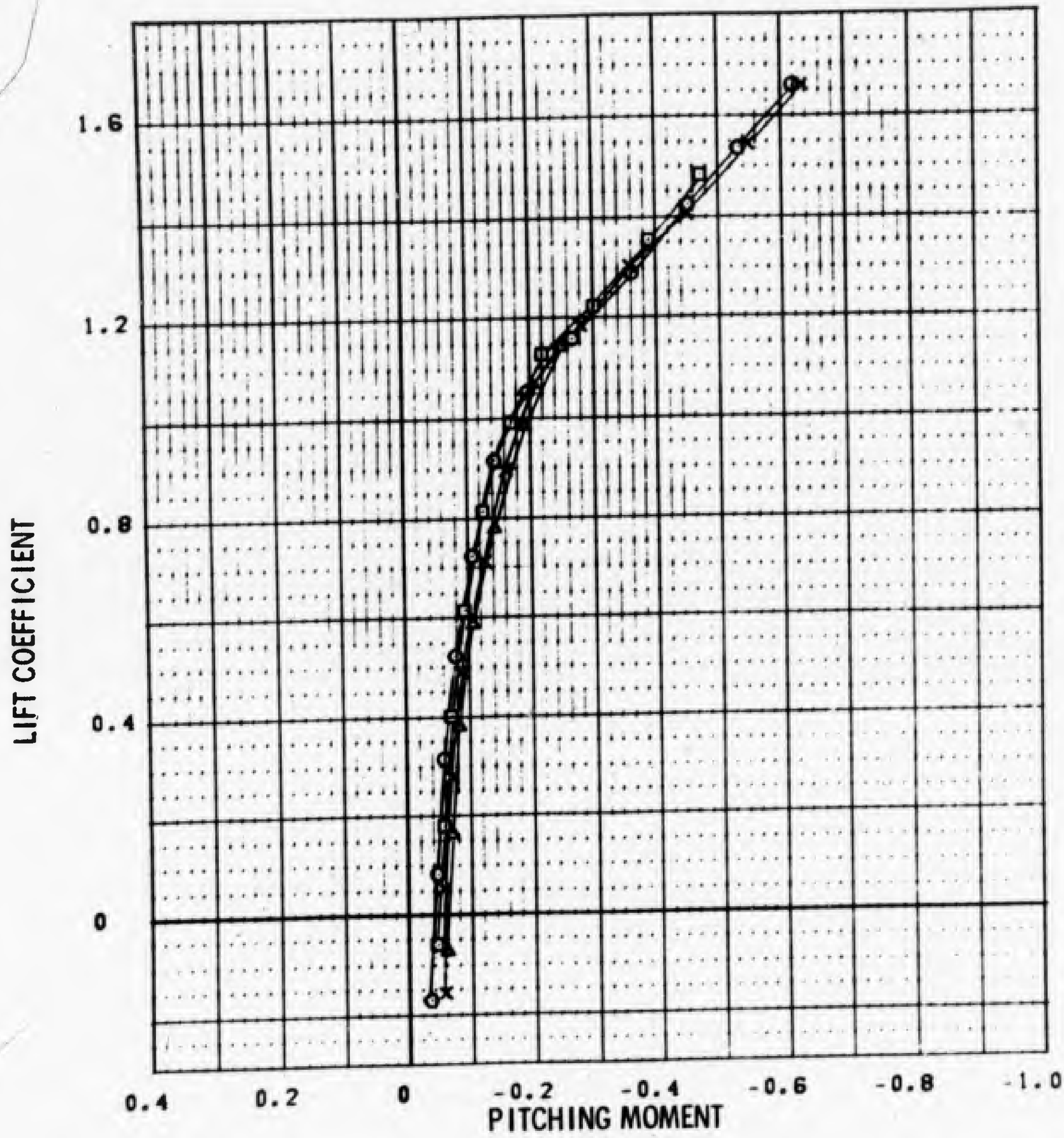
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	264	K1 0/0	OFF
⊡	PWT 4T TC-043	441	K1 0/0	OFF
▲	PWT 4T TC-043	445	K1 5/5	OFF
×	PWT 4T TC-043	241	K1 5/5	ON

FIGURE 114c EFFECT OF VORTEX GENERATORS
M = 0.9



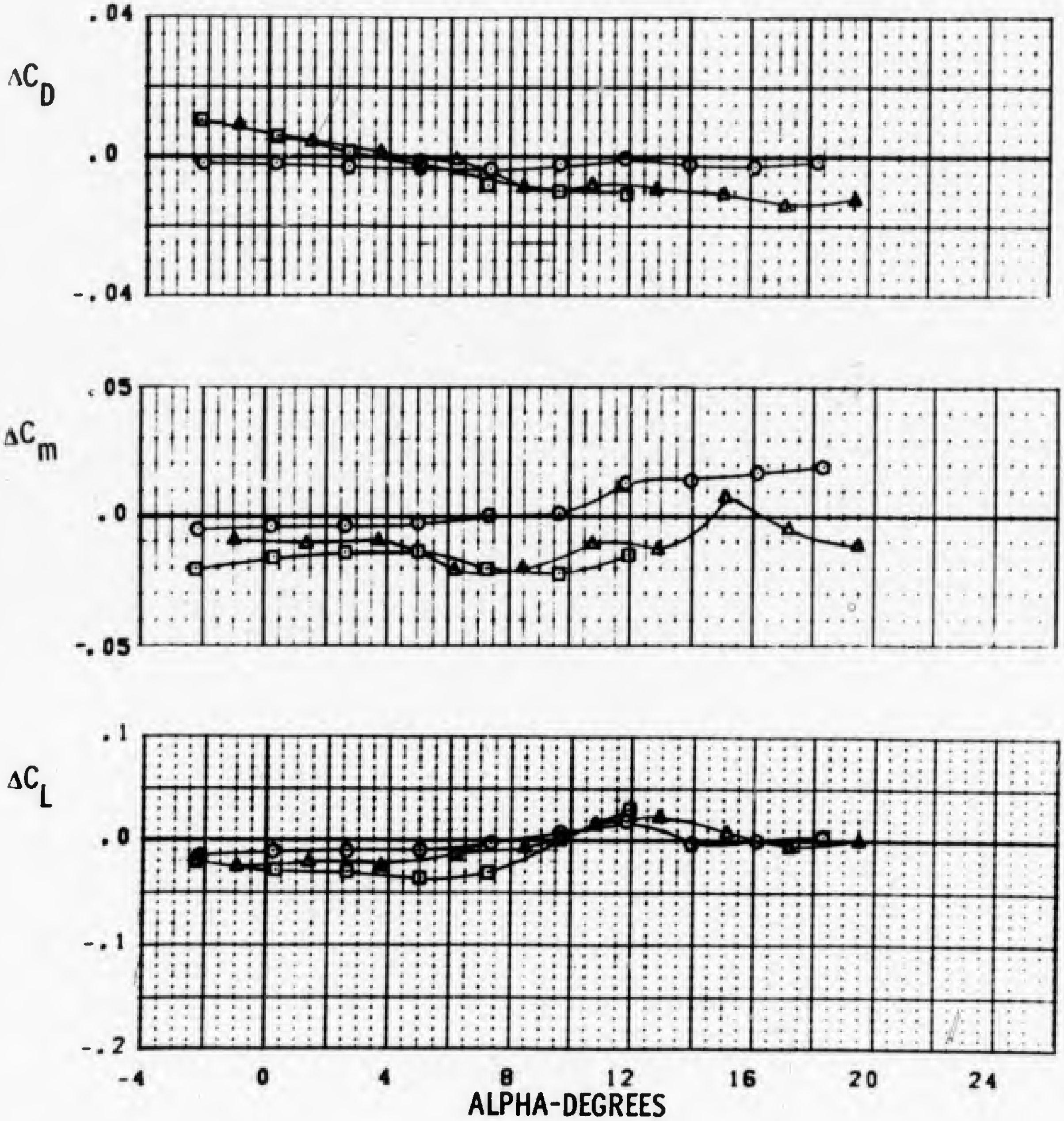
SYM	TEST	PART	L.E. (L/R)	V.G.
○	PWT 4T TC-043	264	K1 0/0	OFF
□	PWT 4T TC-043	441	K1 0/0	OFF
△	PWT 4T TC-043	445	K1 5/5	OFF
×	PWT 4T TC-043	241	K1 5/5	ON

FIGURE 114c EFFECT OF VORTEX GENERATORS
M = 0.9



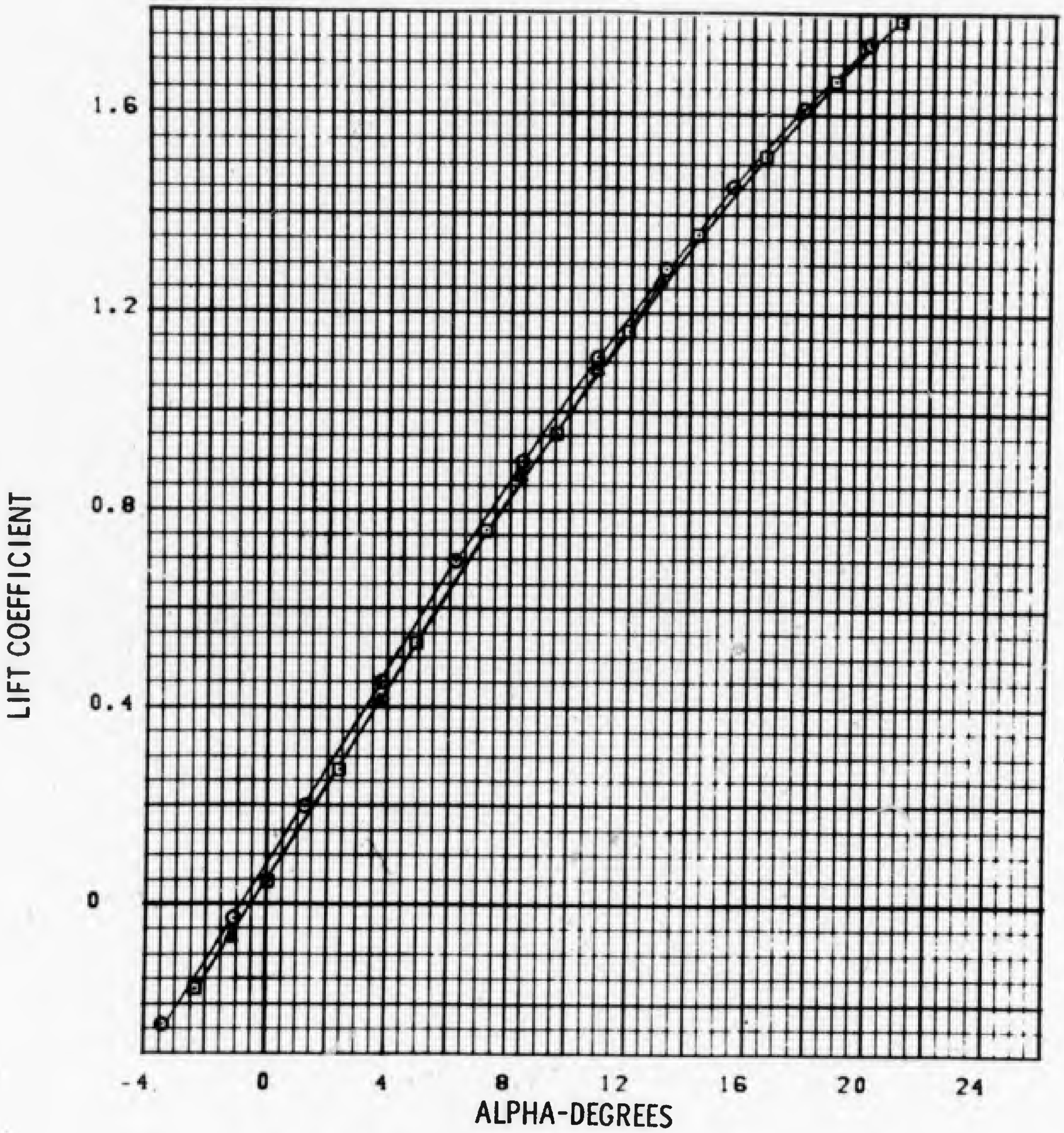
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	264	K1 0/0	OFF
⊡	PWT 4T TC-043	441	K1 0/0	OFF
▲	PWT 4T TC-043	445	K1 5/5	OFF
×	PWT 4T TC-043	241	K1 5/5	ON

FIGURE 114c EFFECT OF VORTEX GENERATORS
M = 0.9



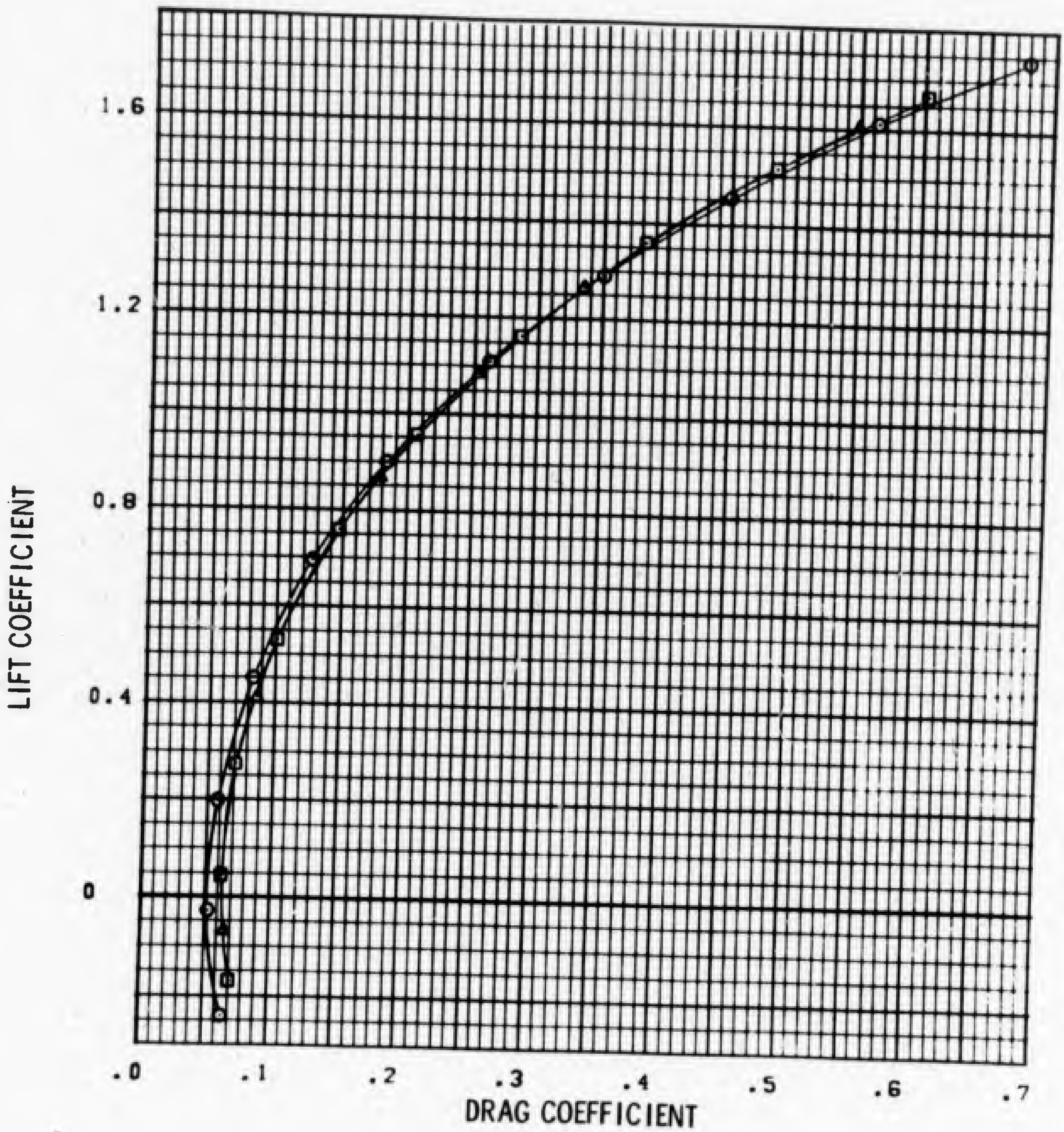
SYM	TEST	INCREMENT	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	PN 441 - PN 264	K1 0/0	OFF
⊡	PWT 4T TC-043	PN 445 - PN 264	K1 5/5	OFF
▲	PWT 4T TC-043	PN 241 - PN 264	K1 5/5	ON

FIGURE 114c EFFECT OF VORTEX GENERATORS
M = 0.9



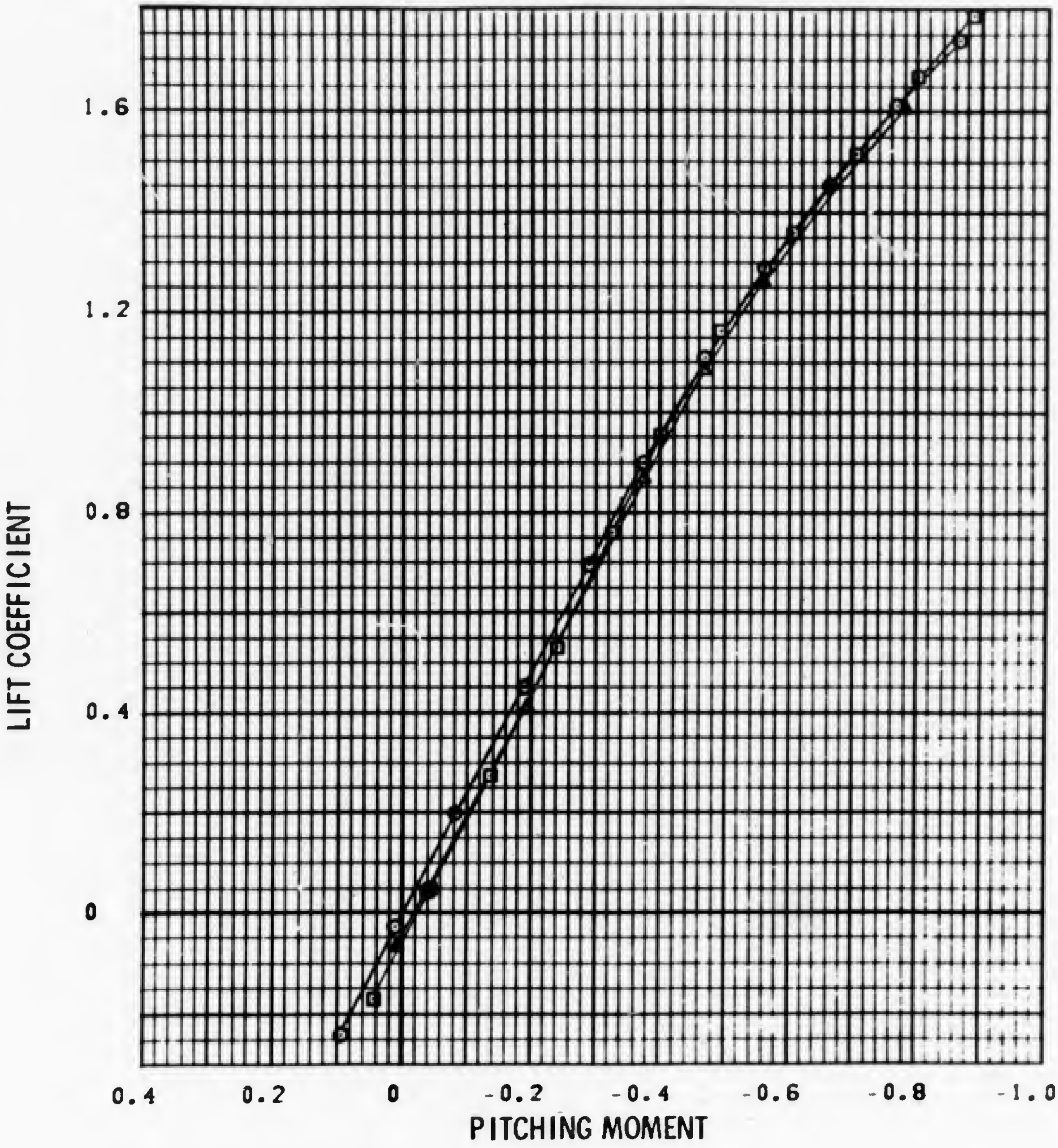
SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	269	K1 0/0	OFF
⊡	PWT 4T TC-043	449	K1 5/5	OFF
▲	PWT 4T TC-043	246	K1 5/5	ON

FIGURE 114d EFFECT OF VORTEX GENERATORS
M = 1.2



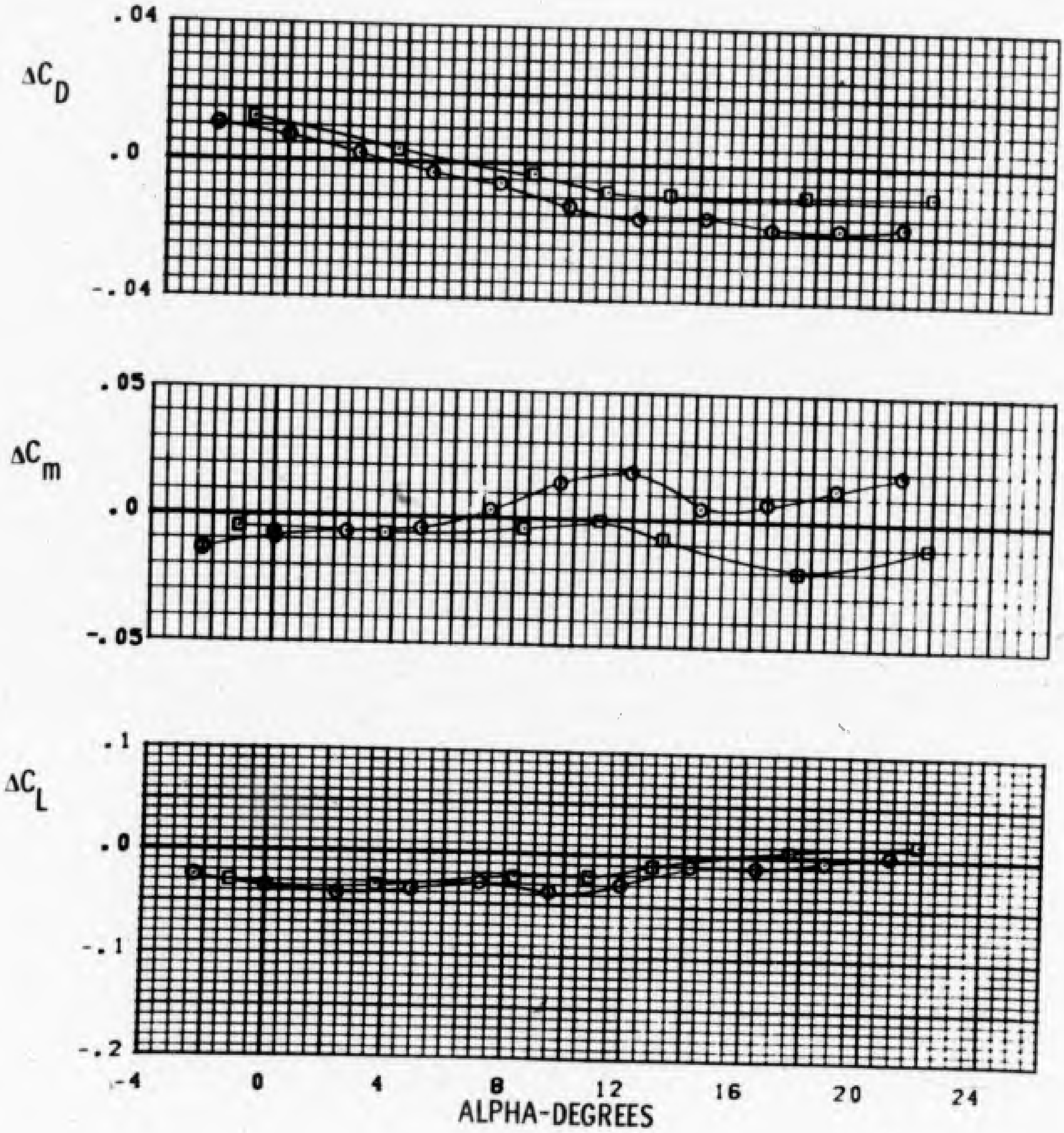
SYM	TEST		PART	L.E. (L/R)		V.G.
⊙	PWT 4T	TC-043	269	K1	0/0	OFF
⊡	PWT 4T	TC-043	449	K1	5/5	OFF
▲	PWT 4T	TC-043	246	K1	5/5	ON

FIGURE 114d EFFECT OF VORTEX GENERATORS
M = 1.2



SYM	TEST	PART	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	269	K1 0/0	OFF
⊡	PWT 4T TC-043	149	K1 5/5	OFF
▲	PWT 4T TC-043	246	K1 5/5	ON

FIGURE 114d EFFECT OF VORTEX GENERATORS
M = 1.2

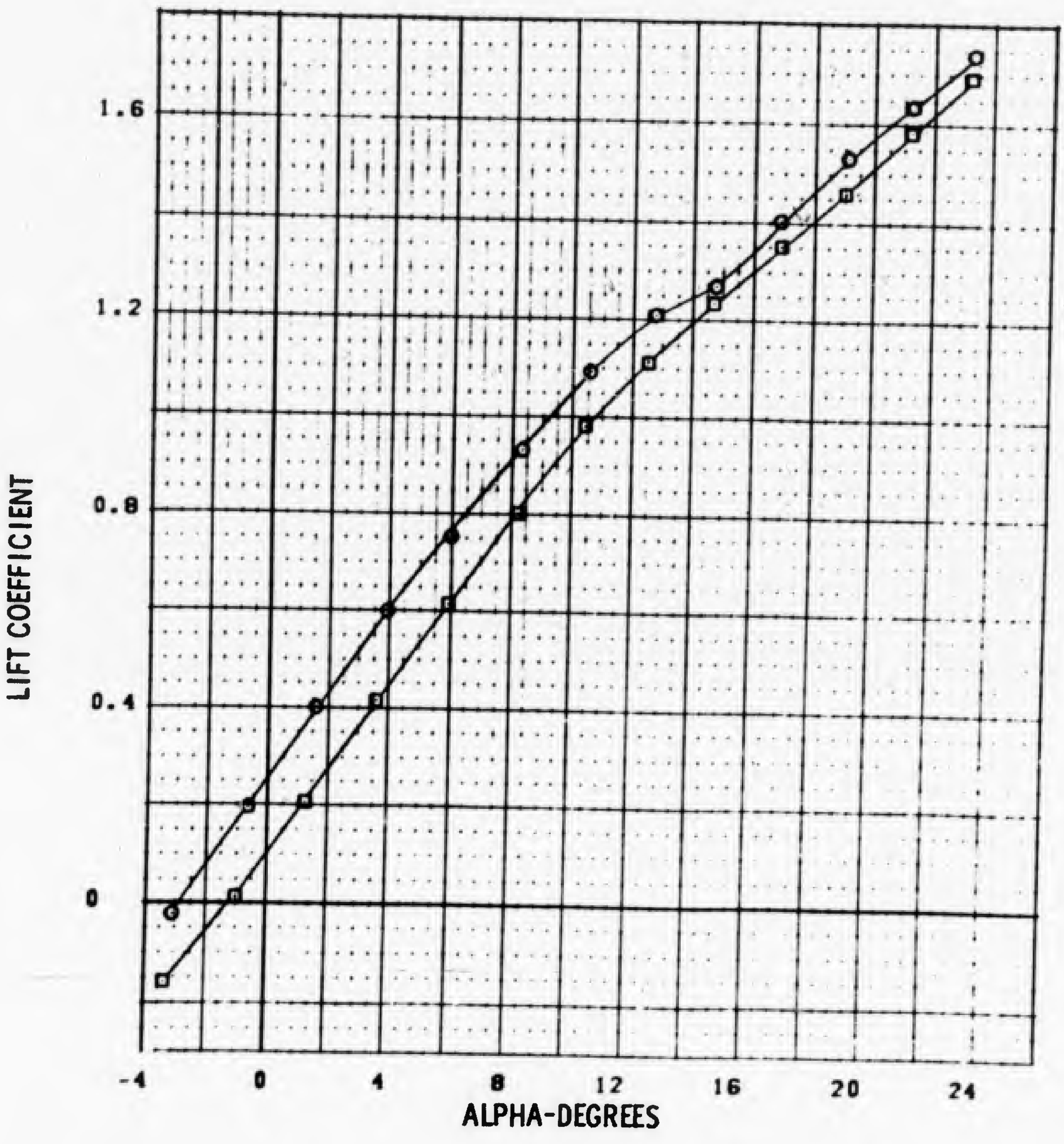


SYM	TEST	INCREMENT	L.E. (L/R)	V.G.
⊙	PWT 4T TC-043	PN 449 - PN 269	KI 5/5	OFF
⊡	PWT 4T TC-043	PN 246 - PN 269	KI 5/5	ON

FIGURE 114d EFFECT OF VORTEX GENERATORS
M = 1.2

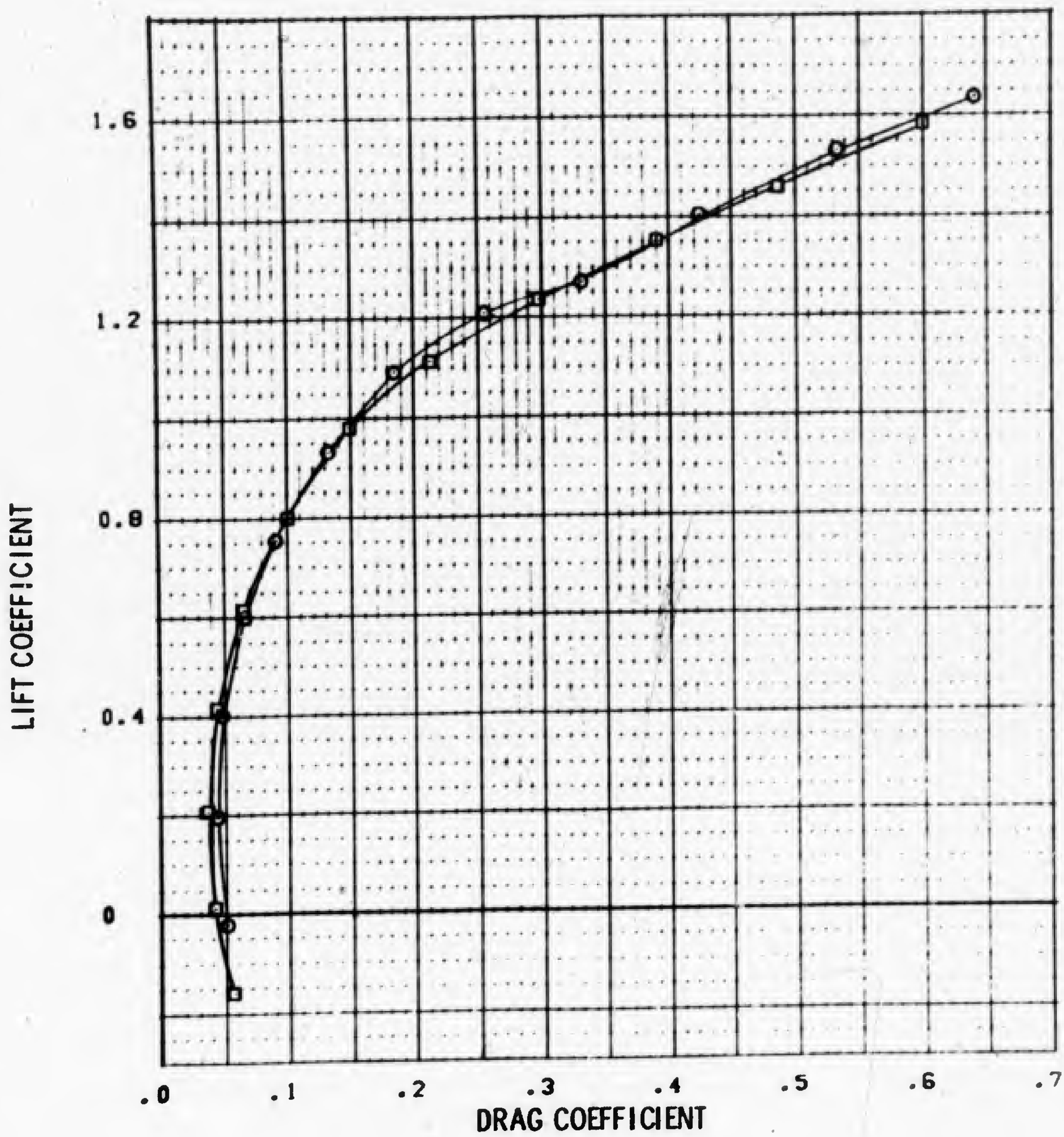
b. Drooped Trailing Edge

The effects of the drooped trailing edge (F1 deflected 10 degrees full span) on the longitudinal aerodynamic characteristics of the LEDE test configuration are presented in this subsection.



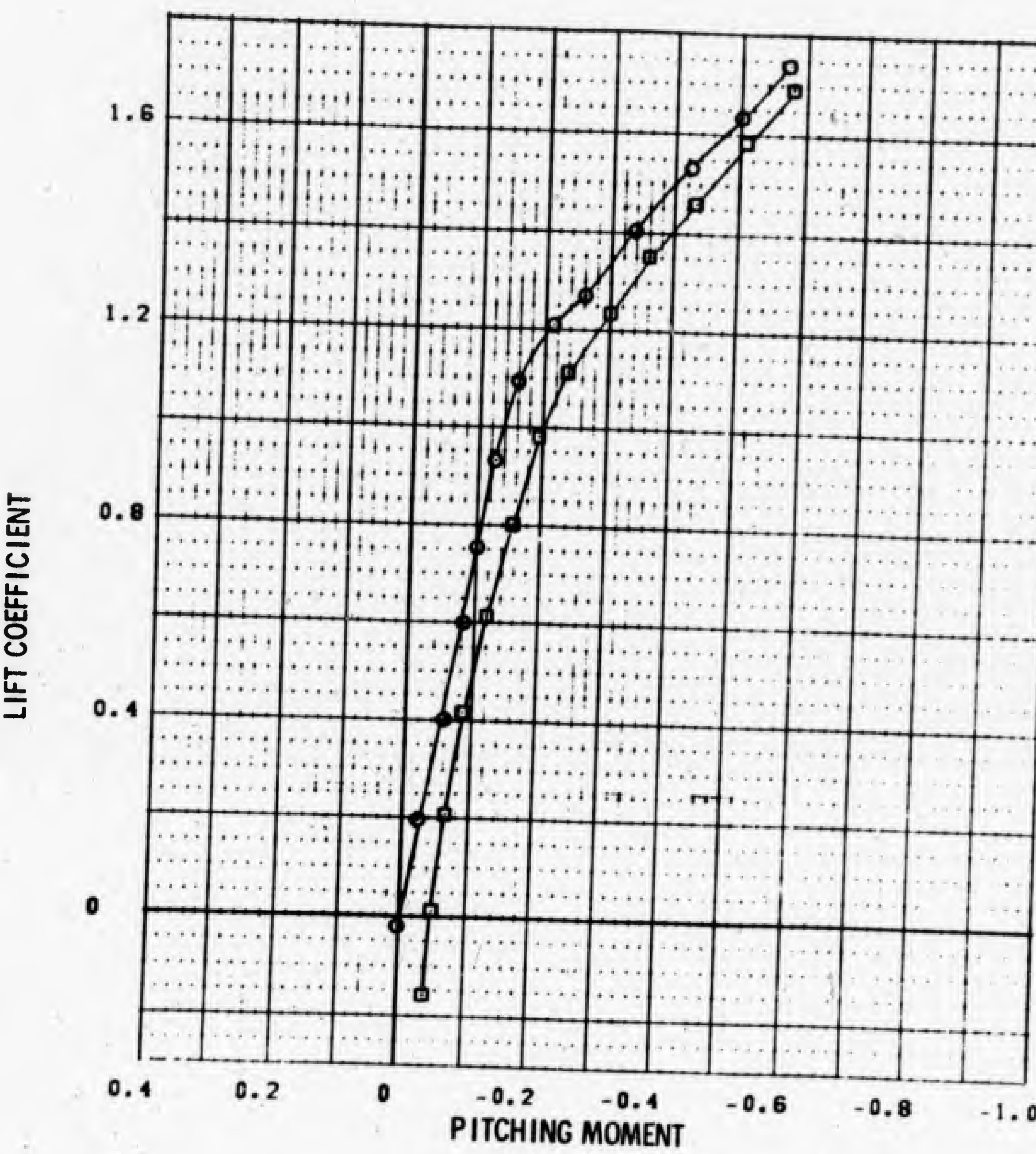
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	194	10	K1 10/10
⊡	PWT 4T TC-043	128	0	K1 10/10

FIGURE 115a EFFECT OF DROOPED TRAILING EDGE
M = 0.7



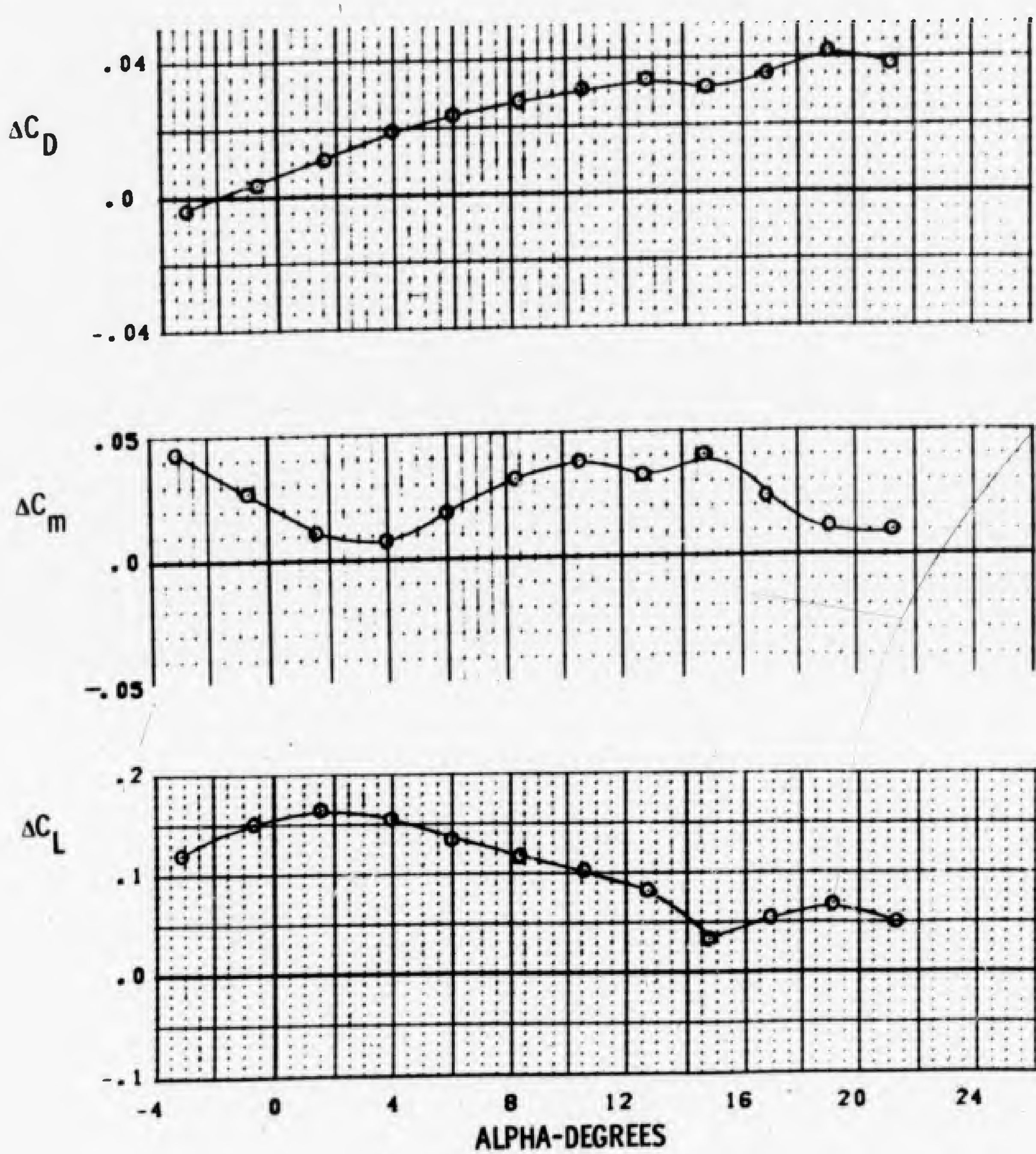
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	194	10	KI 10/10
⊡	PWT 4T TC-043	128	0	KI 10/10

FIGURE 115a EFFECT OF DROOPED TRAILING EDGE
M = 0.7



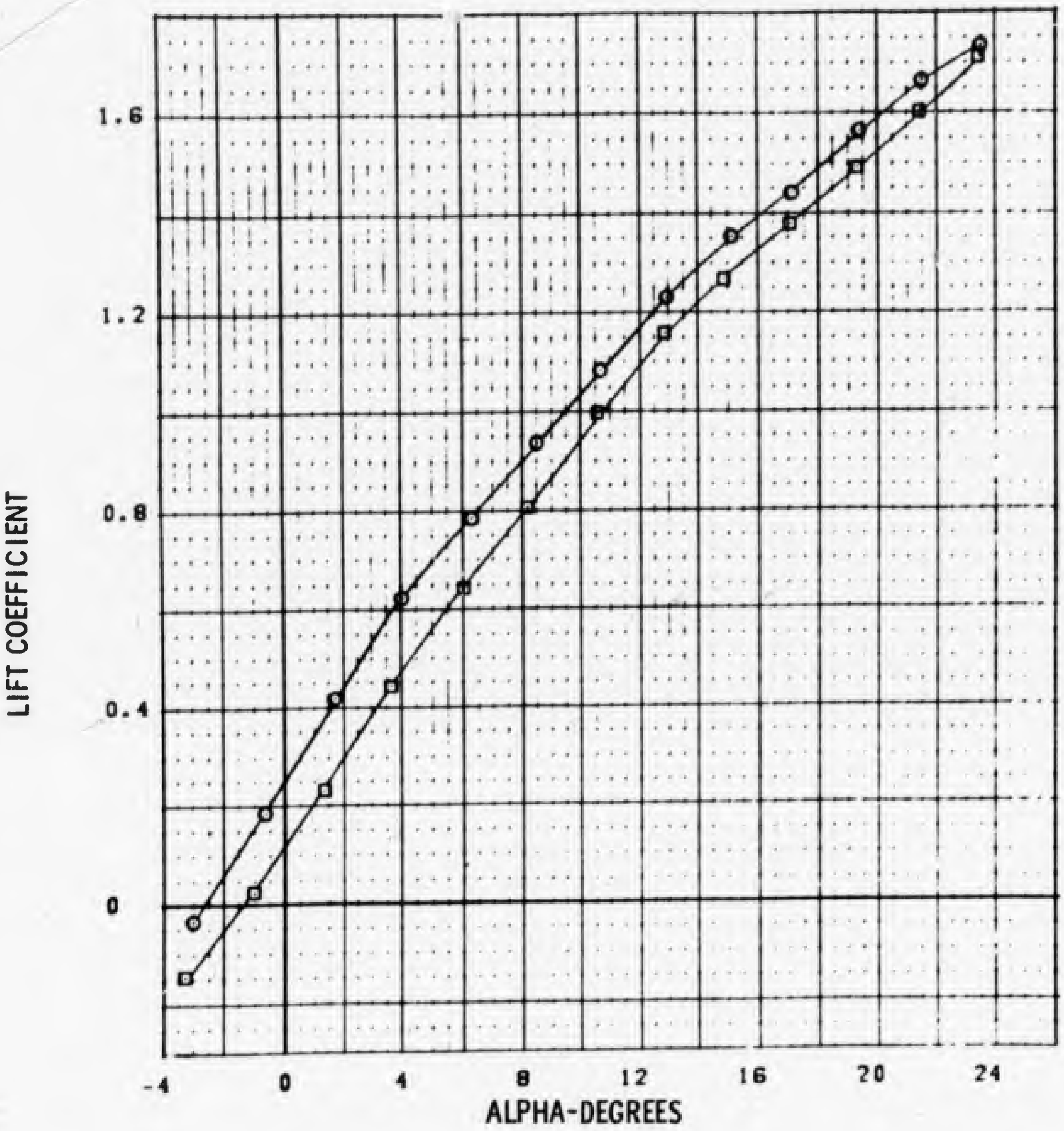
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
○	PWT 4T TC-043	194	10	K1 10/10
□	PWT 4T TC-043	128	0	K1 10/10

FIGURE 115a EFFECT OF DROOPED TRAILING EDGE
M = 0.7



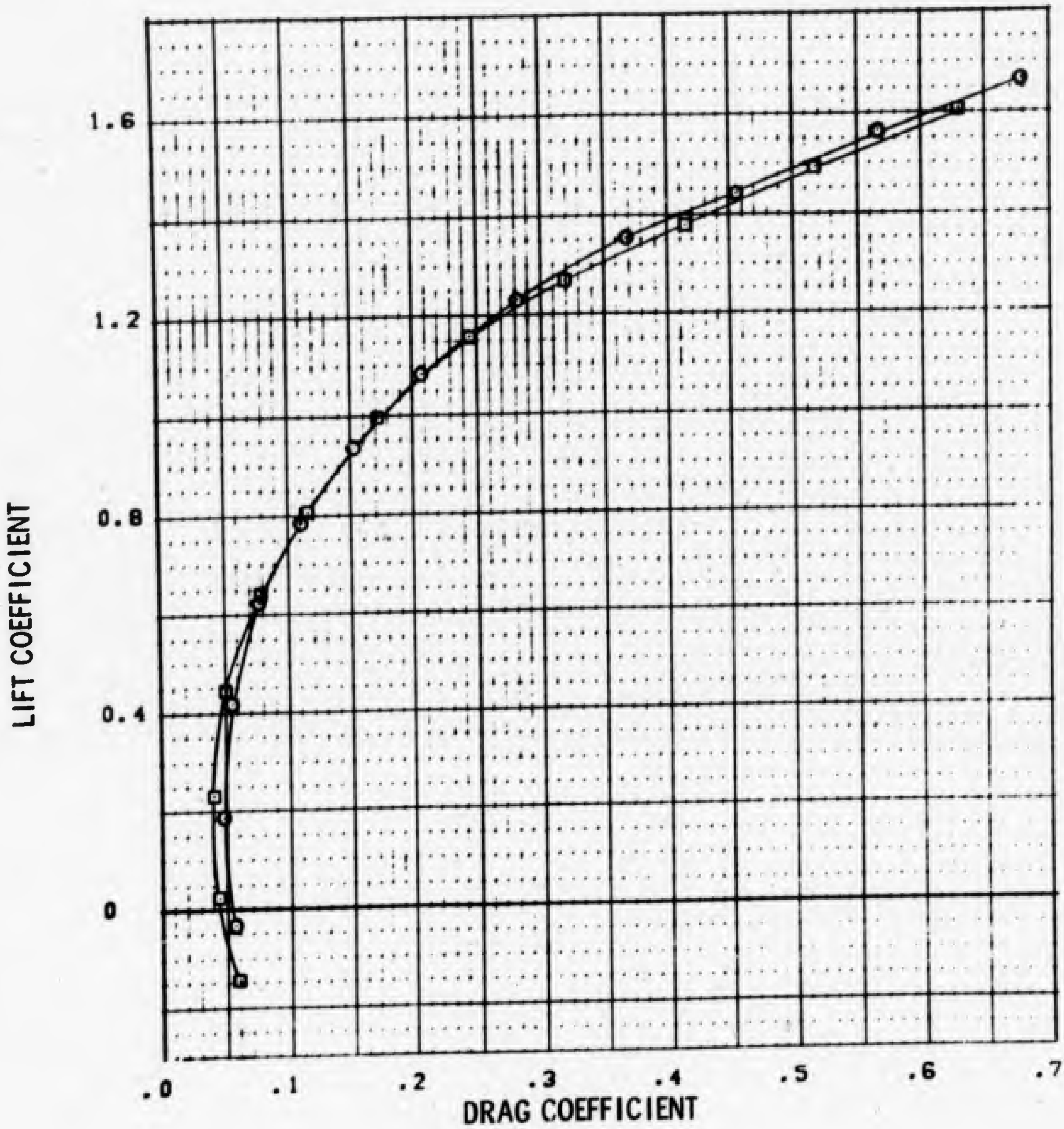
SYM	TEST	INCREMENT	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 194 - PN 128	10	K1 10/10

FIGURE 115a EFFECT OF DROOPED TRAILING EDGE
M = 0.7



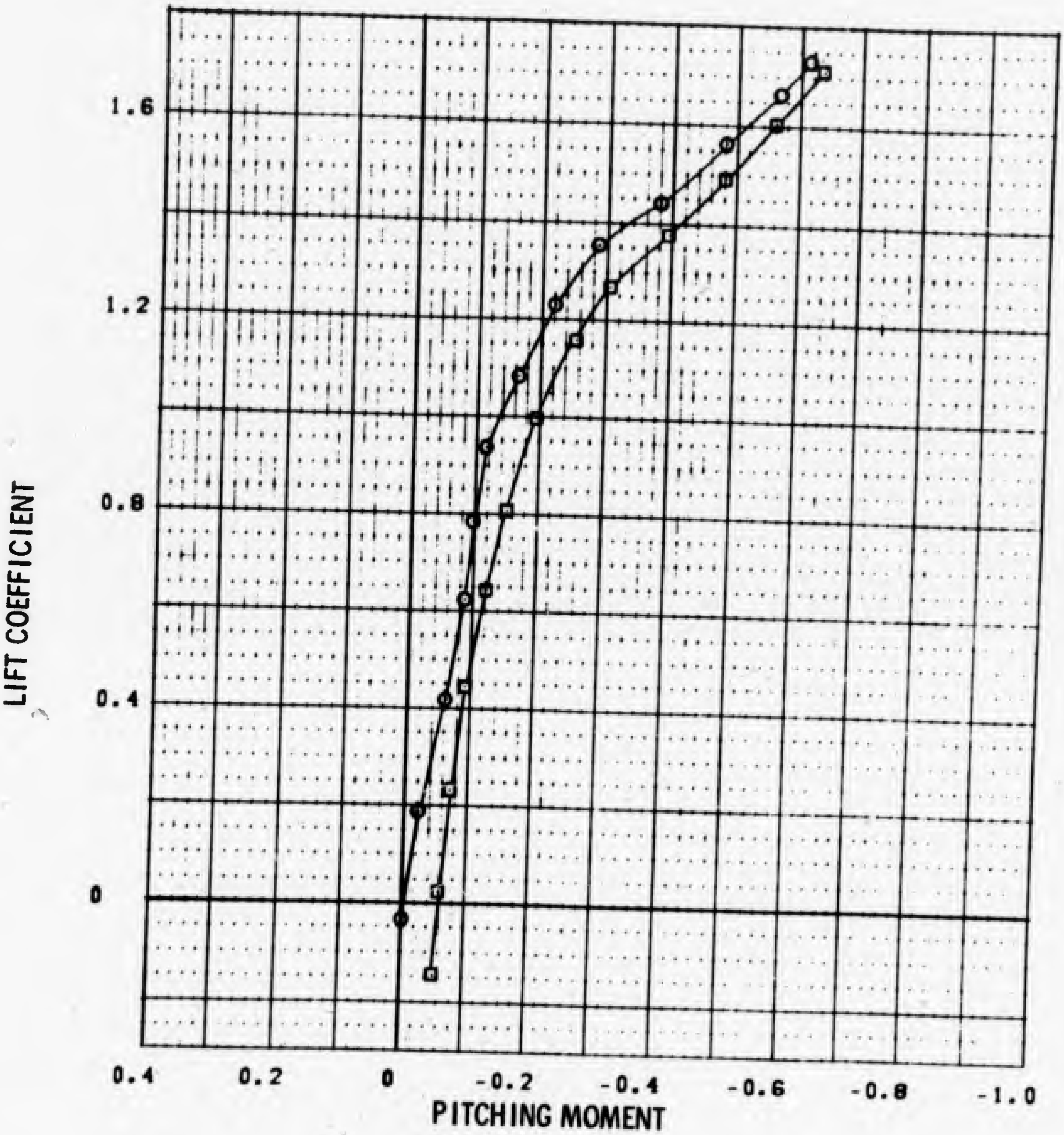
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	193	10	K1 10/10
⊡	PWT 4T TC-043	127	0	K1 10/10

FIGURE 115b EFFECT OF DROOPED TRAILING EDGE
M = 0.8



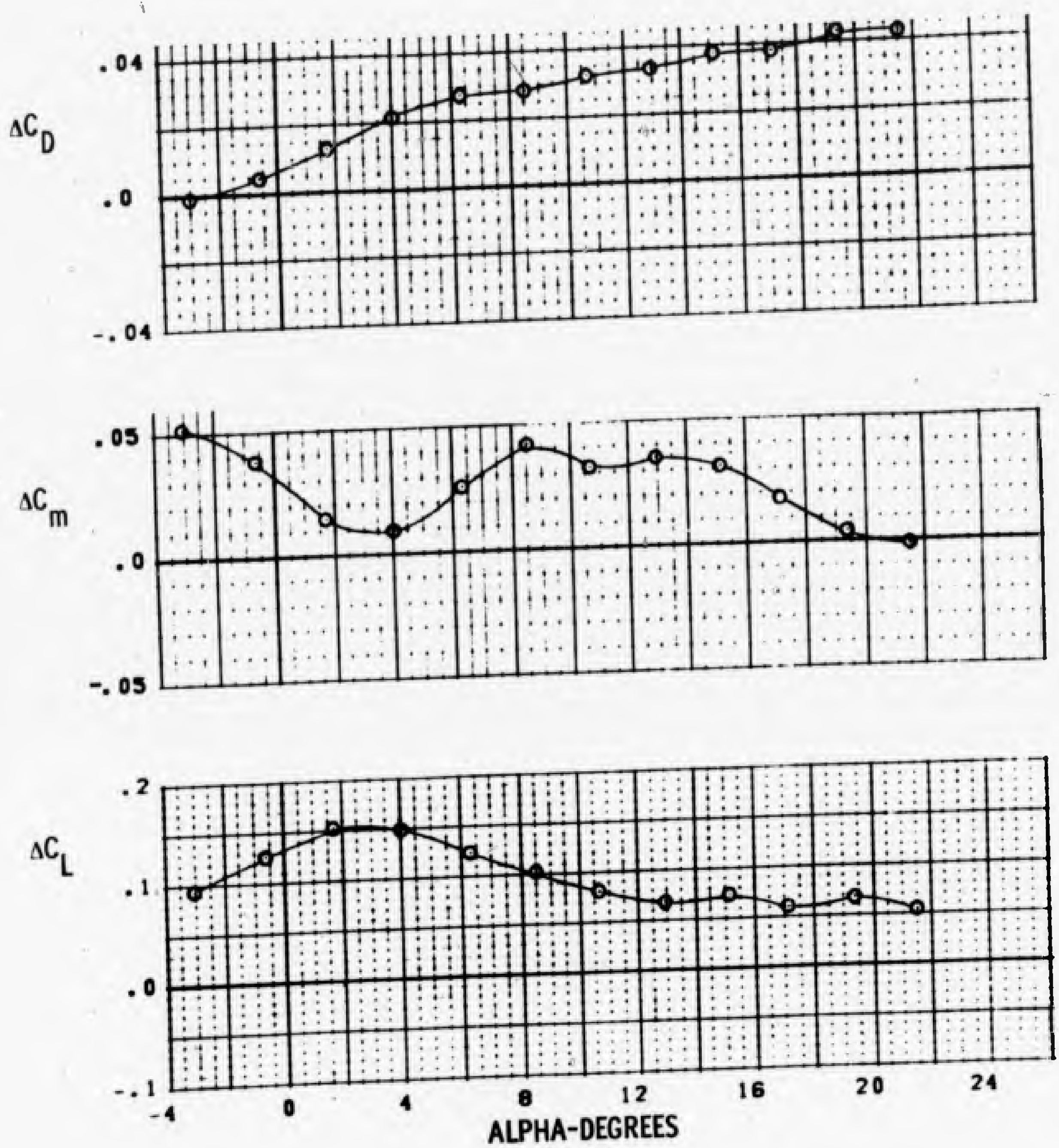
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	193	10	K1 10/10
⊡	PWT 4T TC-043	127	0	K1 10/10

FIGURE 115b EFFECT OF DROOPED TRAILING EDGE
M = 0.8



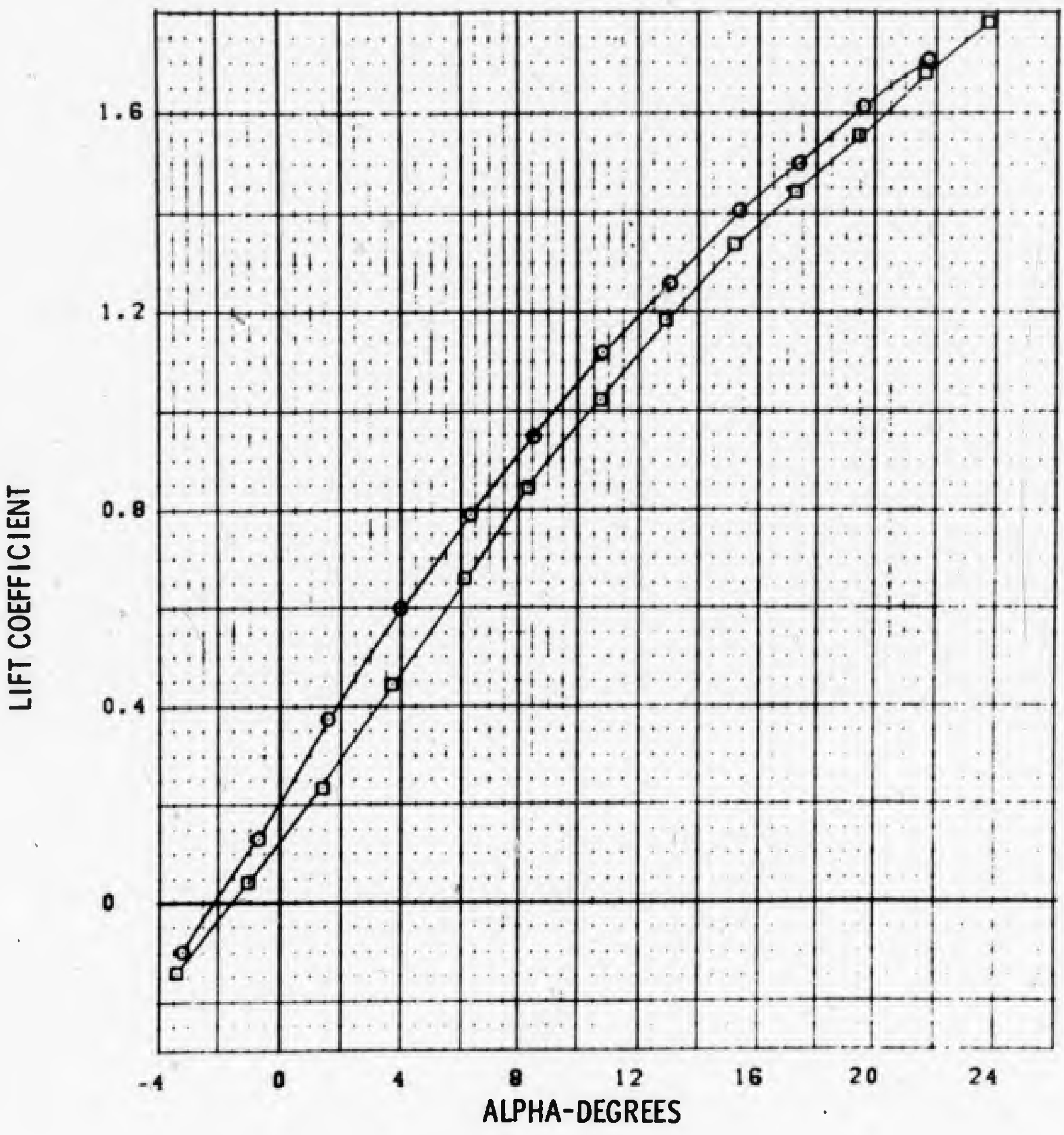
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	193	10	K1 10/10
⊡	PWT 4T TC-043	127	0	K1 10/10

FIGURE 115b EFFECT OF DROOPED TRAILING EDGE
M = 0.8



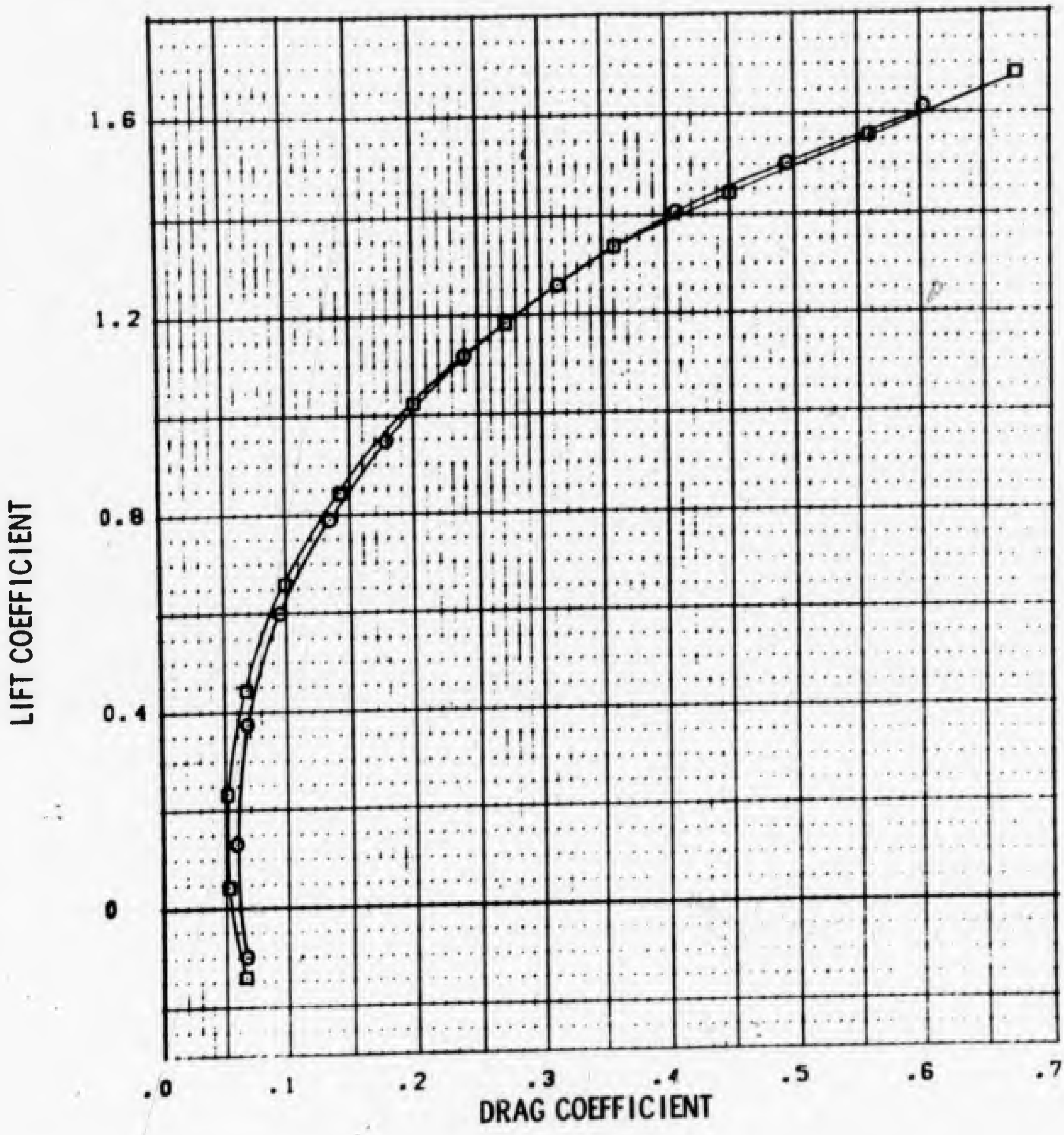
SYM	TEST	INCREMENT	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 193 - PN 127	10	K1 10/10

FIGURE 115b EFFECT OF DROOPED TRAILING EDGE
M = 0.8



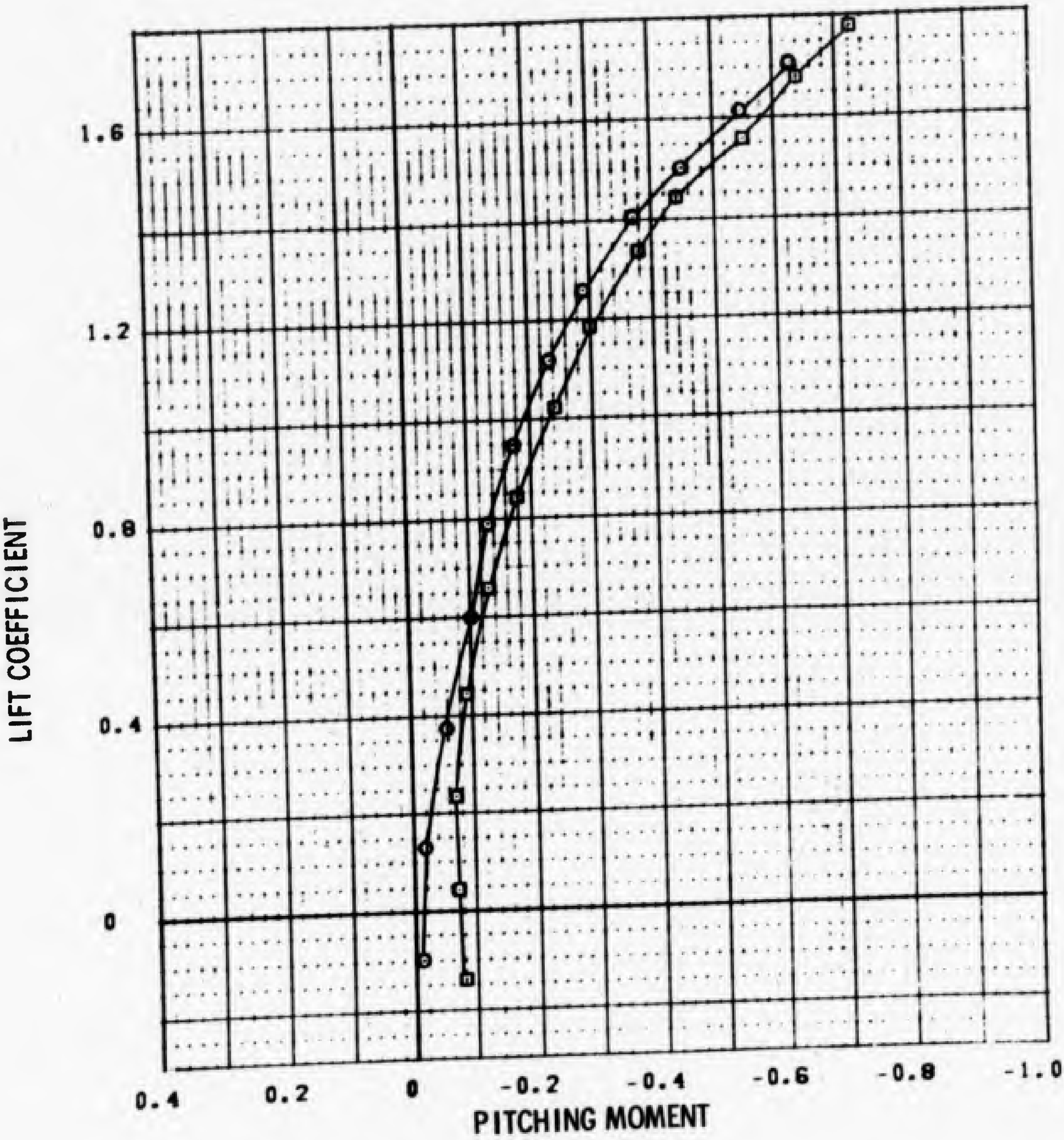
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	192	10	K1 10/10
⊡	PWT 4T TC-043	126	0	K1 10/10

FIGURE 115c EFFECT OF DROOPED TRAILING EDGE
M = 0.9



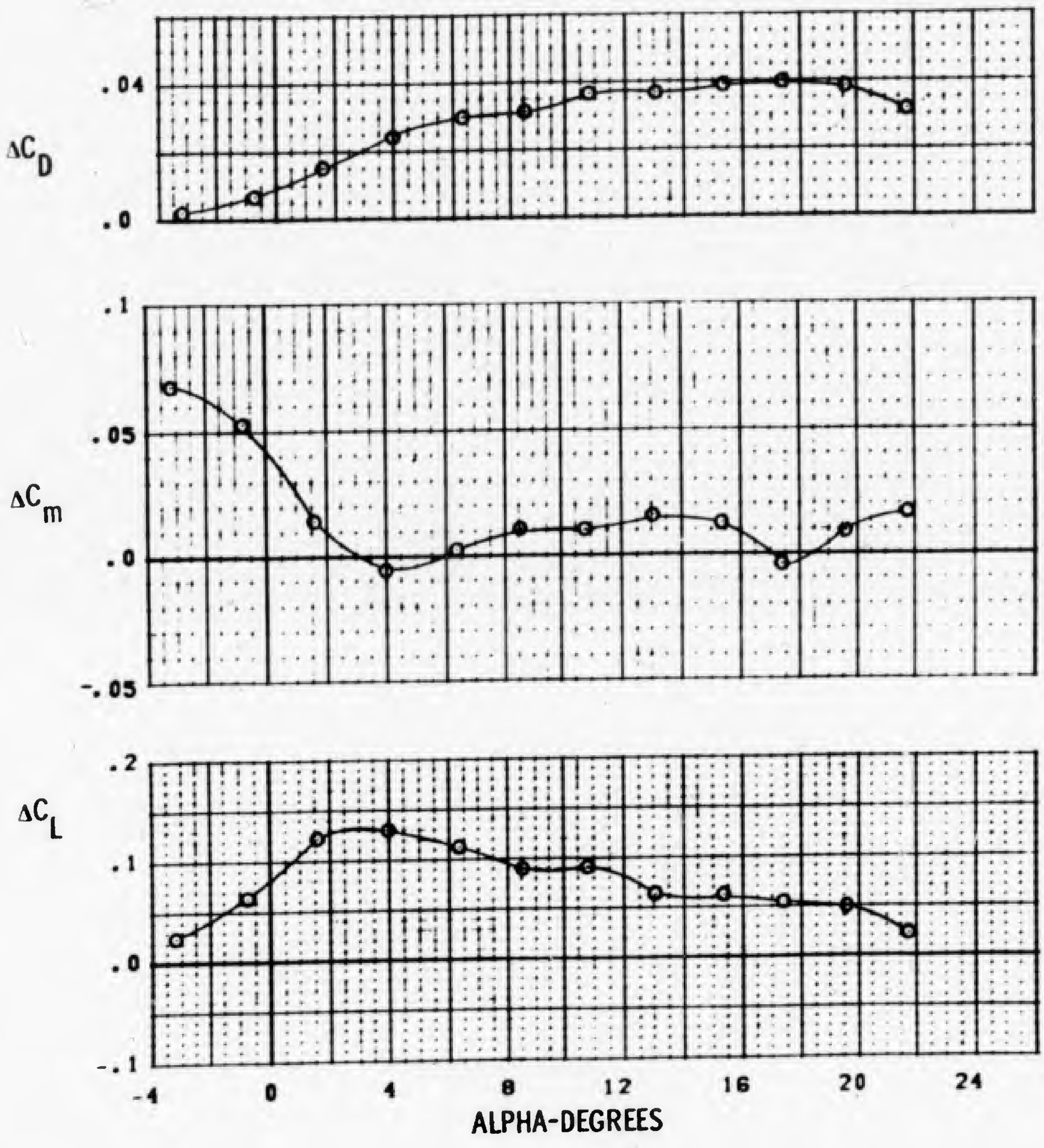
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	192	10	K1 10/10
⊡	PWT 4T TC-043	126	0	K1 10/10

FIGURE 115c EFFECT OF DROOPED TRAILING EDGE
M = 0.9



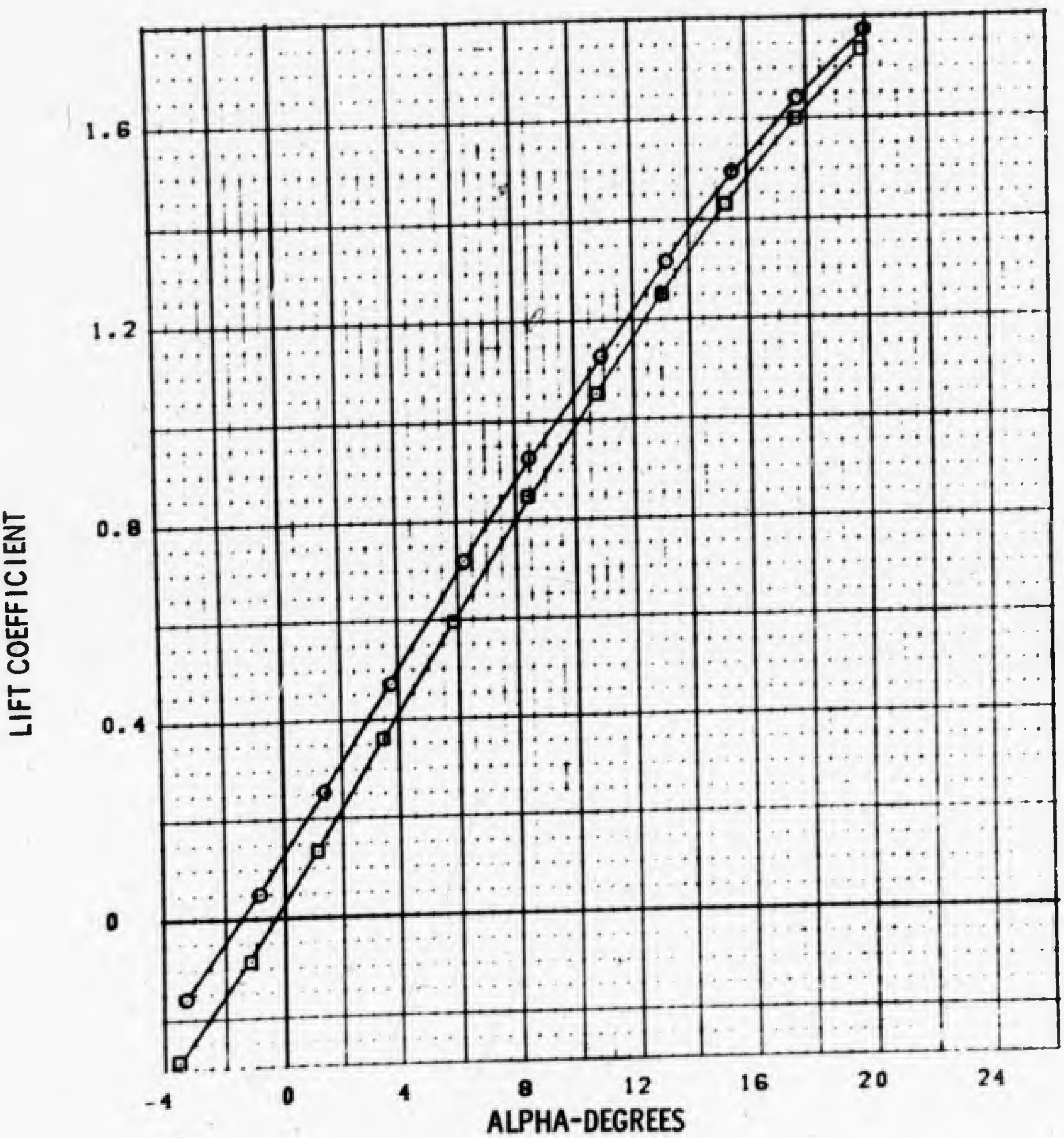
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
○	PWT 4T TC-043	192	10	K1 10/10
▫	PWT 4T TC-043	126	0	K1 10/10

FIGURE 115c EFFECT OF DROOPED TRAILING EDGE
M = 0.9



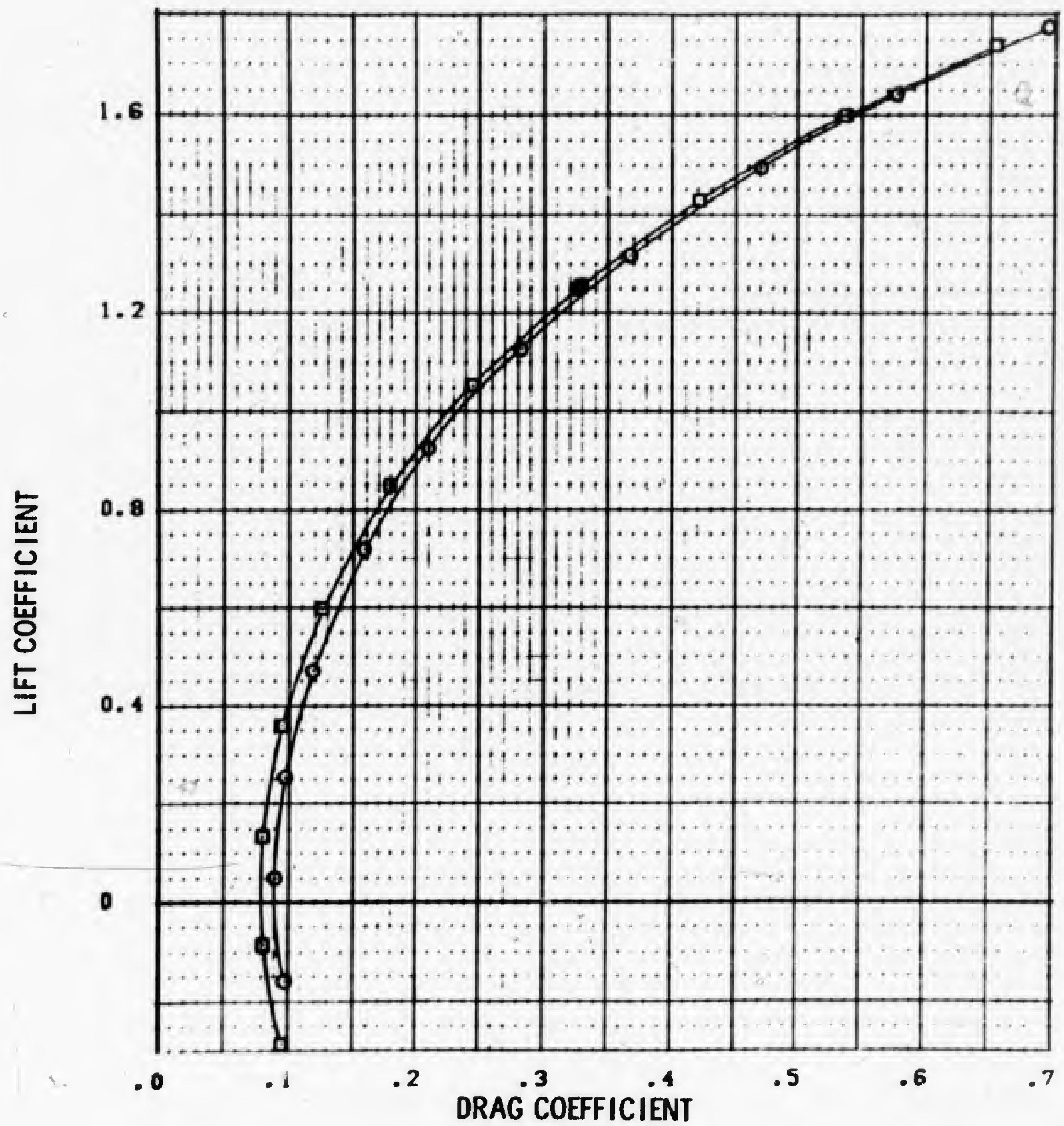
SYM	TEST	INCREMENT	T.E. DROOP	L.E. (L/R)
O	PWT 4T TC-043	PN 192 - PN 126	10	K1 10/10

FIGURE 115c EFFECT OF DROOPED TRAILING EDGE
M = 0.9



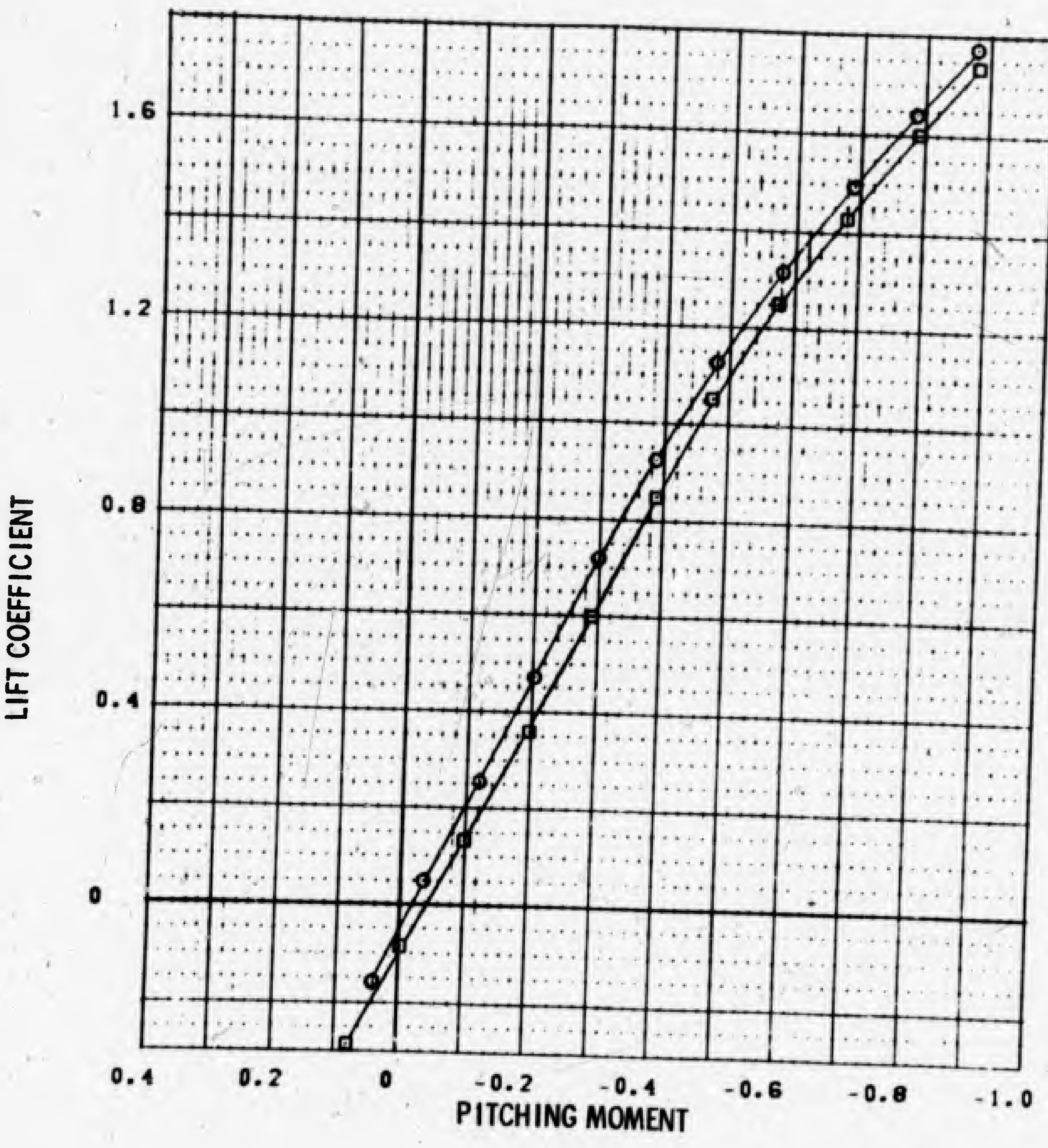
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
○	PWT 4T TC-043	195	10	K1 10/10
⊡	PWT 4T TC-043	129	0	K1 10/10

FIGURE 115d EFFECT OF DROOPED TRAILING EDGE
M = 1.2



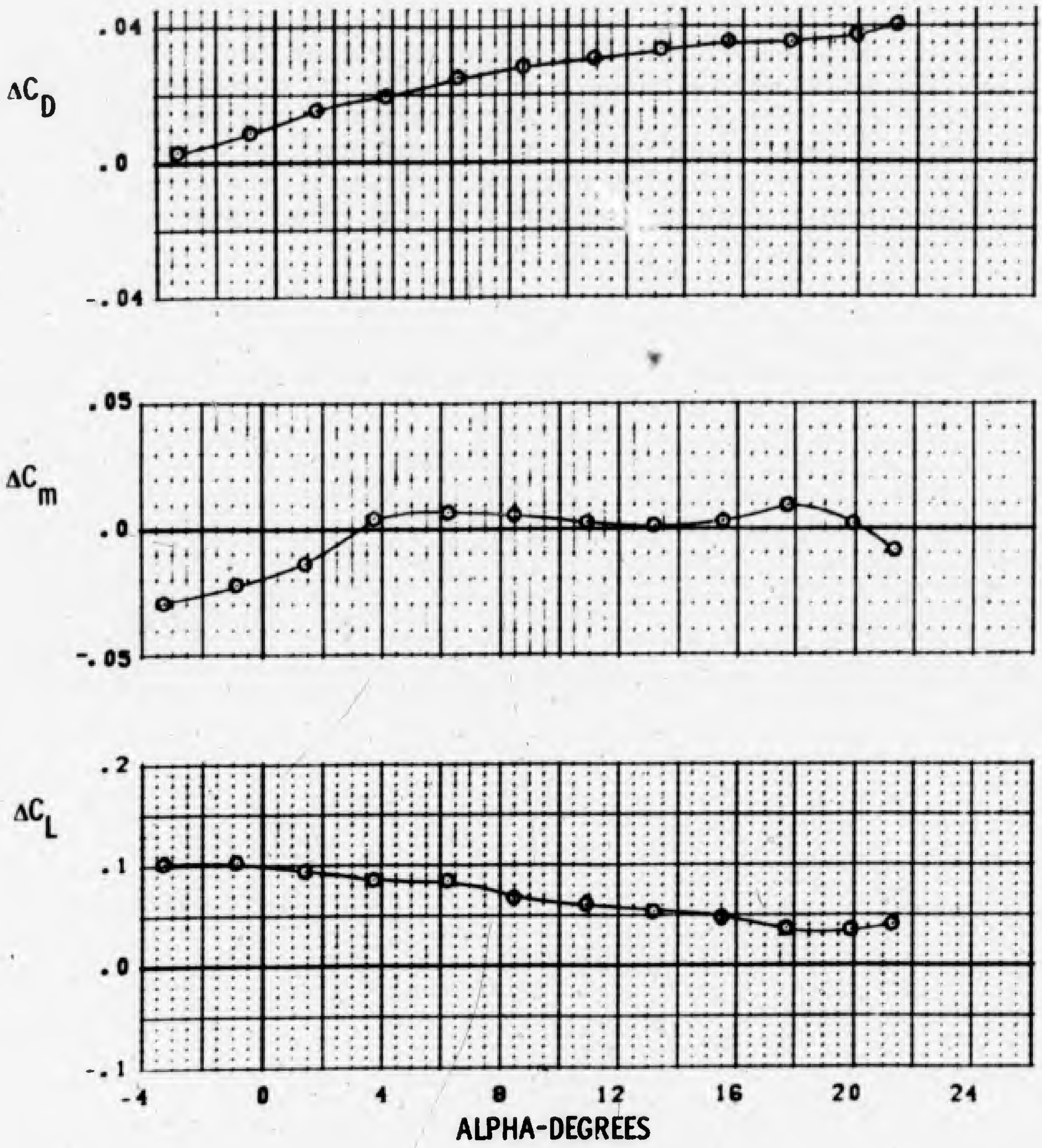
SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	195	10	K1 10/10
⊡	PWT 4T TC-043	129	0	K1 10/10

FIGURE 115d EFFECT OF DROOPED TRAILING EDGE
M = 1.2



SYM	TEST	PART	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	195	10	K1 10/10
⊡	PWT 4T TC-043	129	0	K1 10/10

FIGURE 115d EFFECT OF DROOPED TRAILING EDGE
M = 1.2

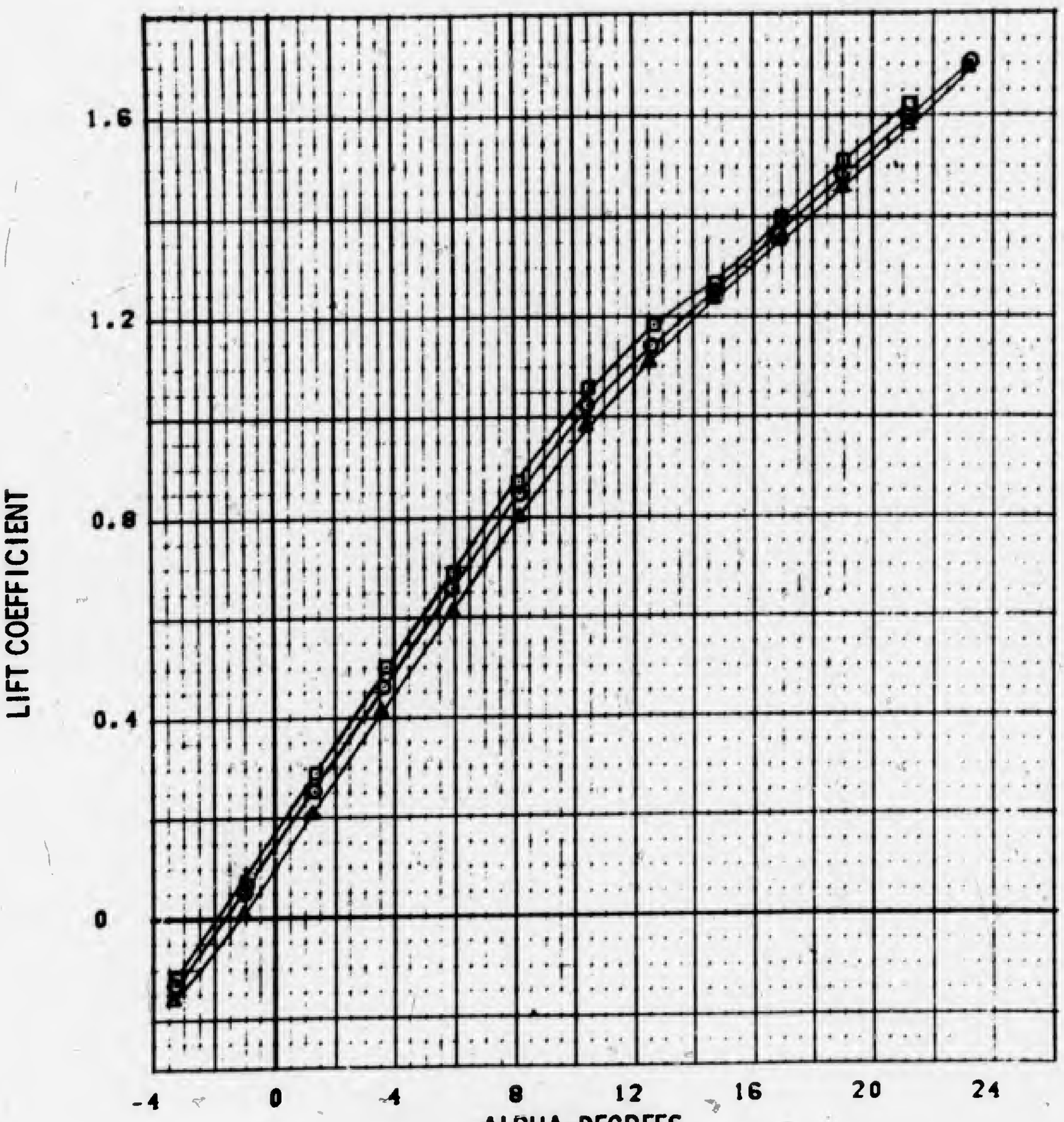


SYM	TEST	INCREMENT	T.E. DROOP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 195 - PN 129	10	K1 10/10

FIGURE 115d EFFECT OF DROOPED TRAILING EDGE
M = 1.2

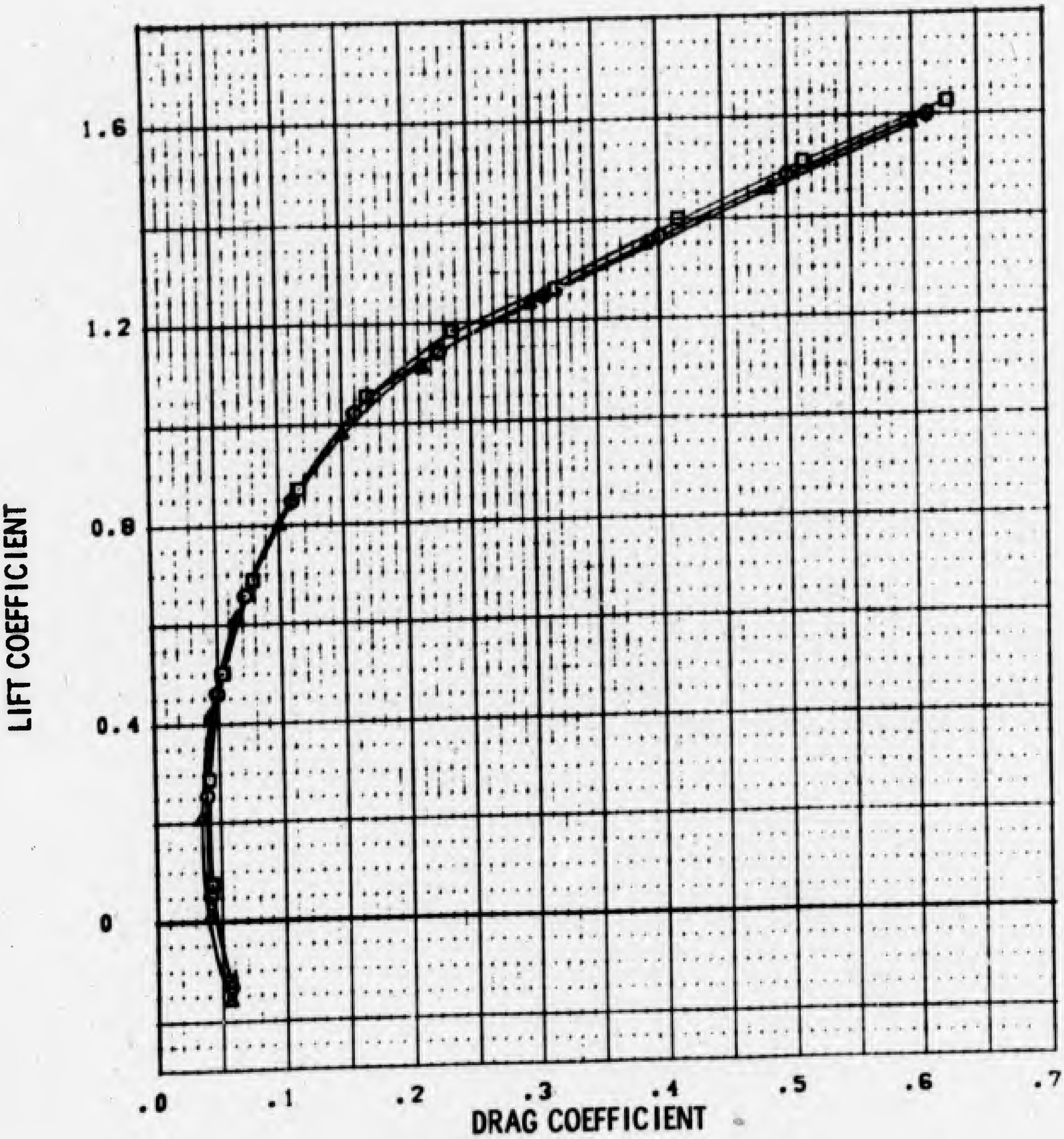
c. Split Trailing Edge Flaps

The effect of the two split trailing edge flaps (F2 and F3) on the longitudinal aerodynamic characteristics of the LEDE configuration with a clean trailing edge are compared in this subsection. These two flaps are attached to the two midspan aileron segments (segments 2 and 3) and are fabricated as a single piece so that the lower surfaces have equivalent deflection angles of 4.70 degrees (F2) and 9.46 degrees (F3), respectively.



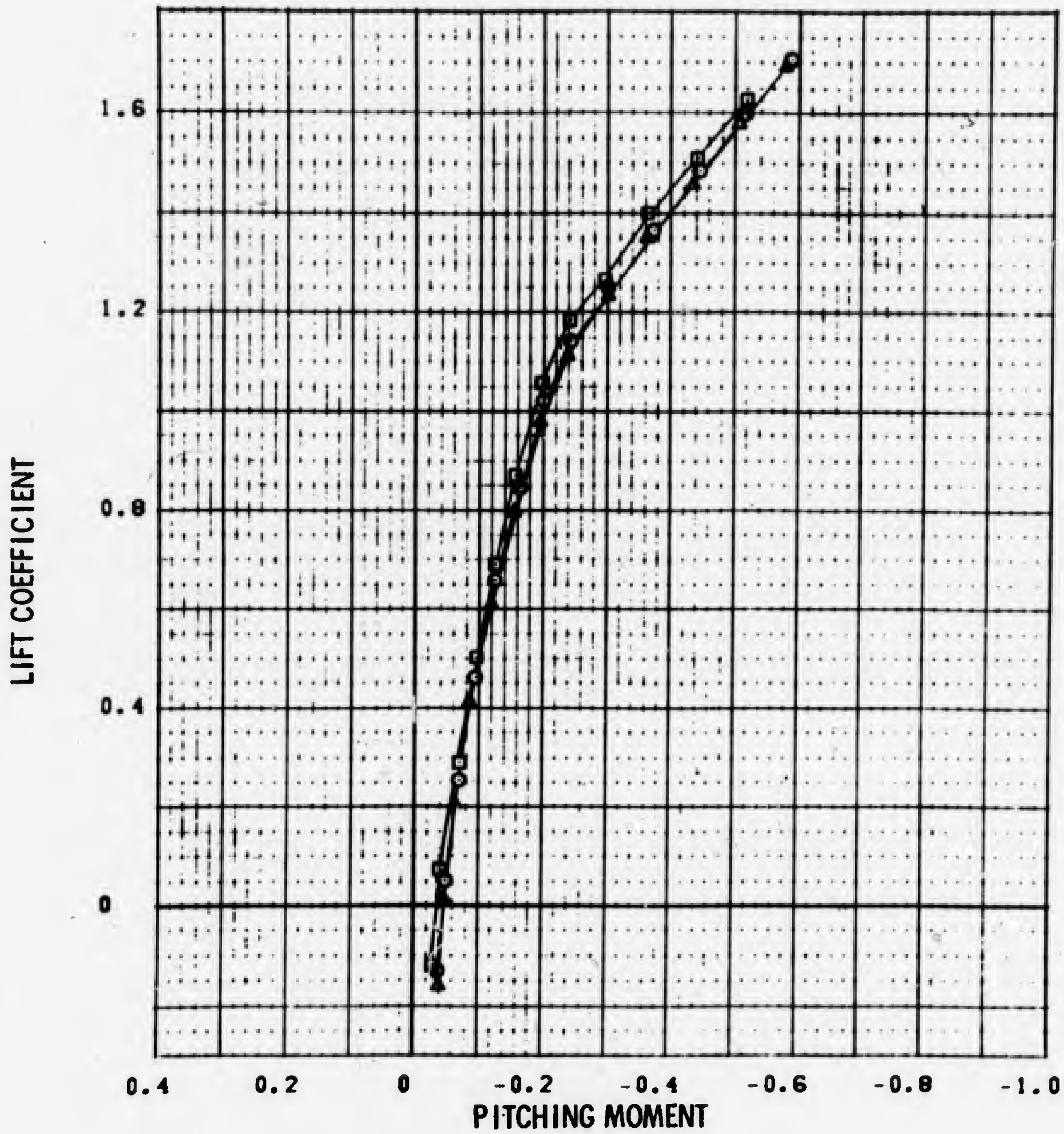
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	168	F2	K1 10/10
⊡	PWT 4T TC-043	149	F3	K1 10/10
▲	PWT 4T TC-043	128	F1	K1 10/10

FIGURE 116a EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.7



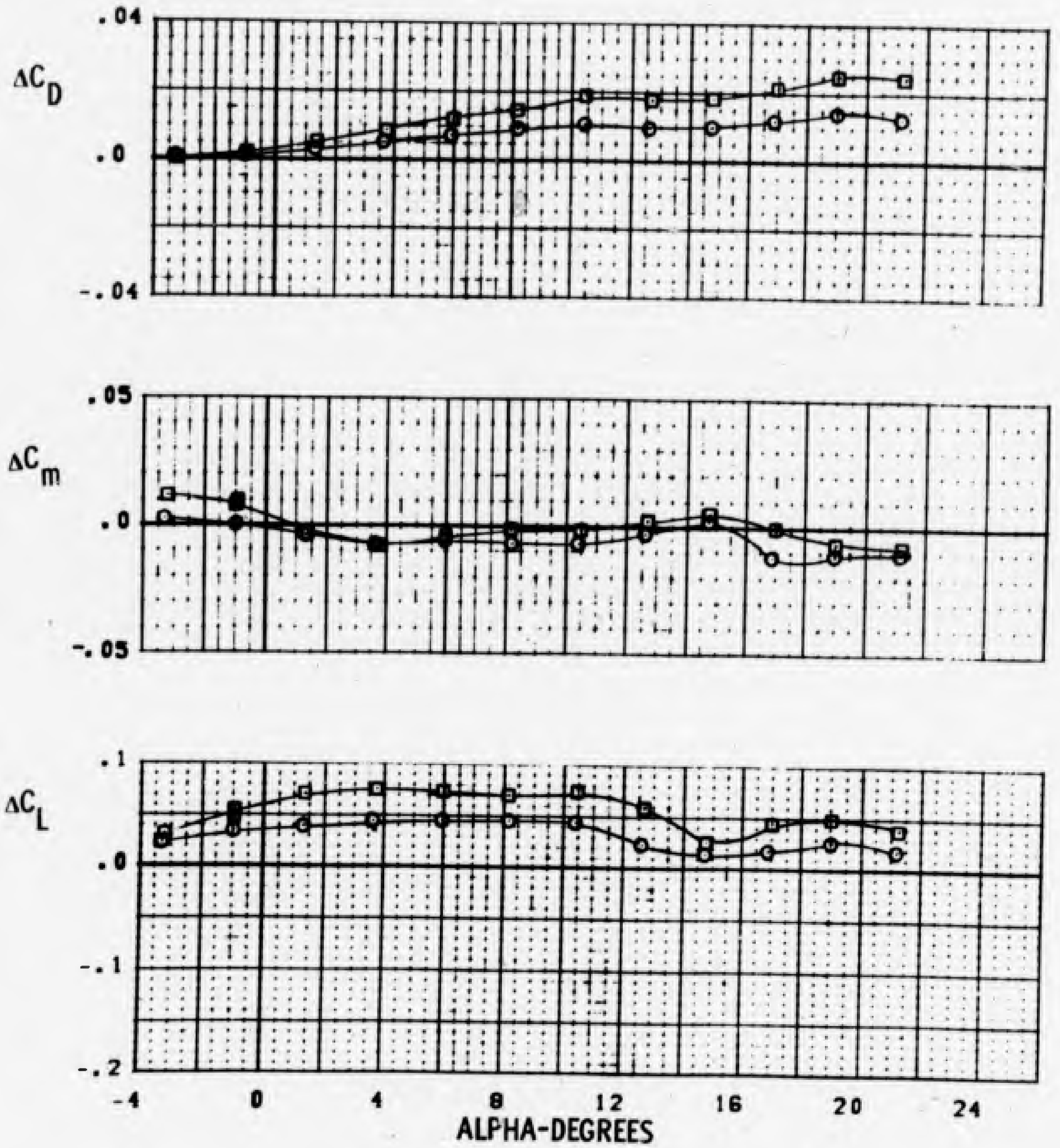
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	160	F2	K1 10/10
⊡	PWT 4T TC-043	149	F3	K1 10/10
▲	PWT 4T TC-043	128	F1	K1 10/10

FIGURE 116a EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.7



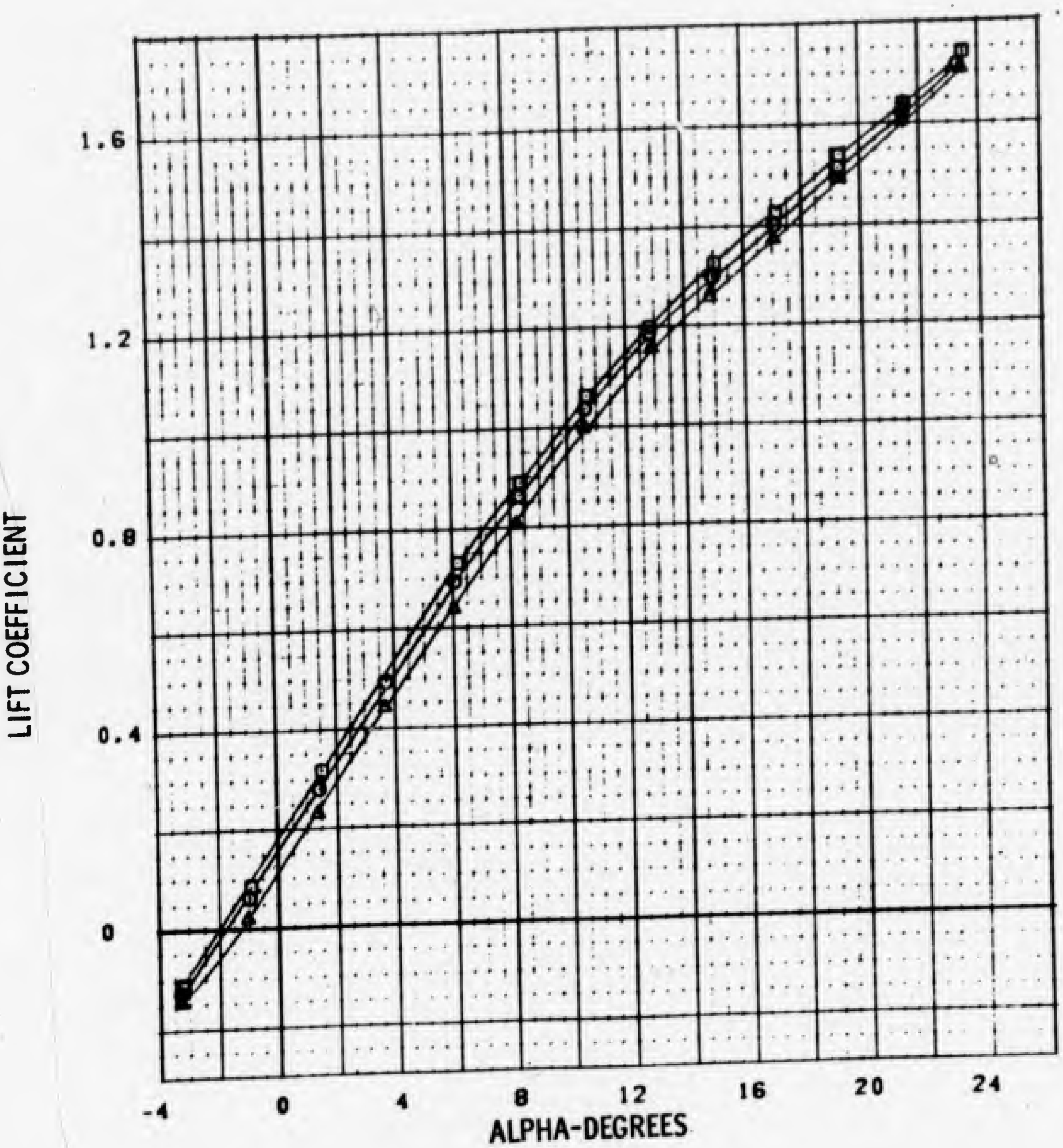
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	168	F2	K1 10/10
⊡	PWT 4T TC-043	149	F3	K1 10/10
▲	PWT 4T TC-043	128	F1	K1 10/10

FIGURE 116a EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.7



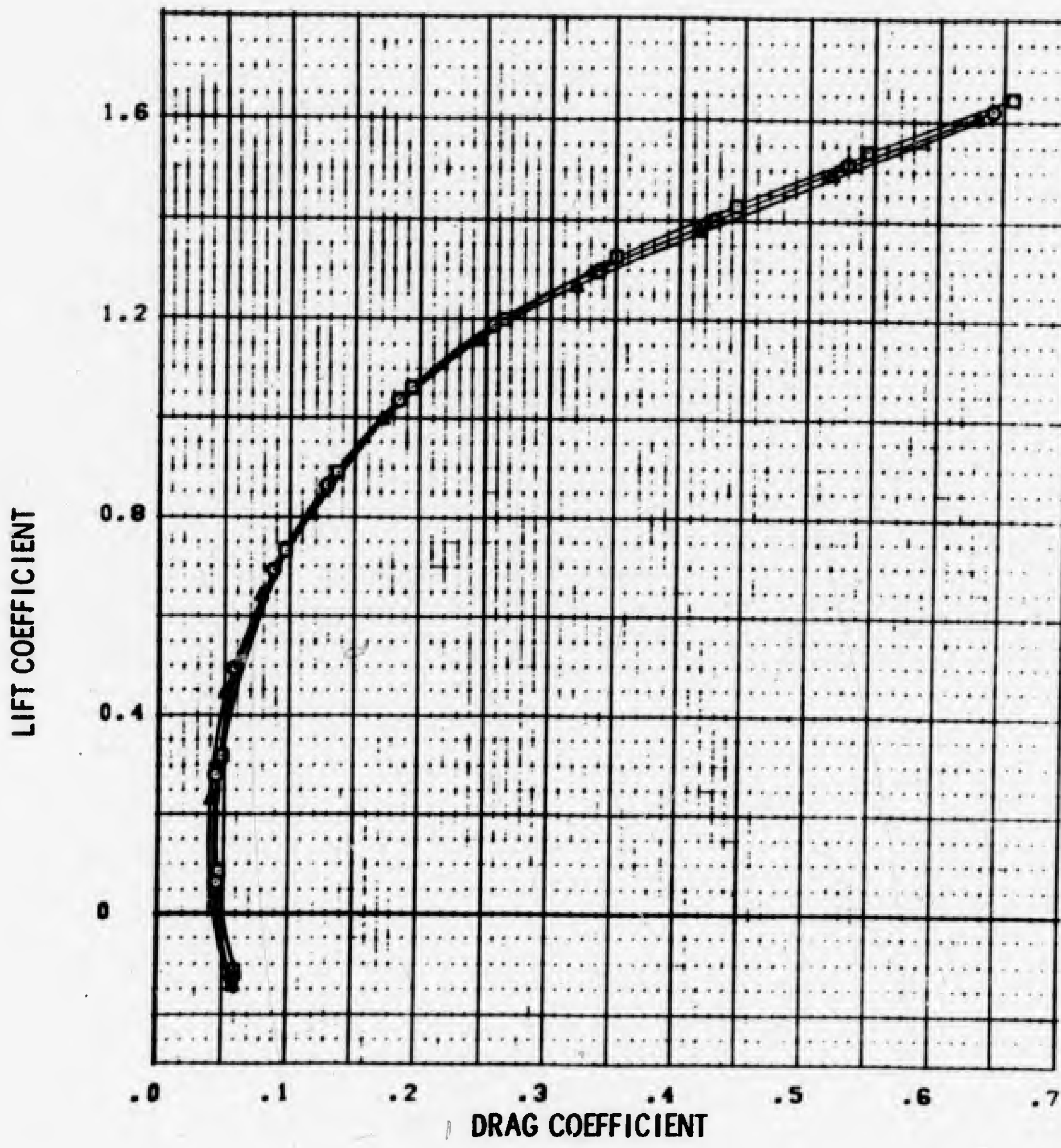
SYM	TEST	INCREMENT	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 168 - PN 128	F2	K1 10/10
⊡	PWT 4T TC-043	PN 149 - PN 128	F3	K1 10/10

FIGURE 116a EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.7



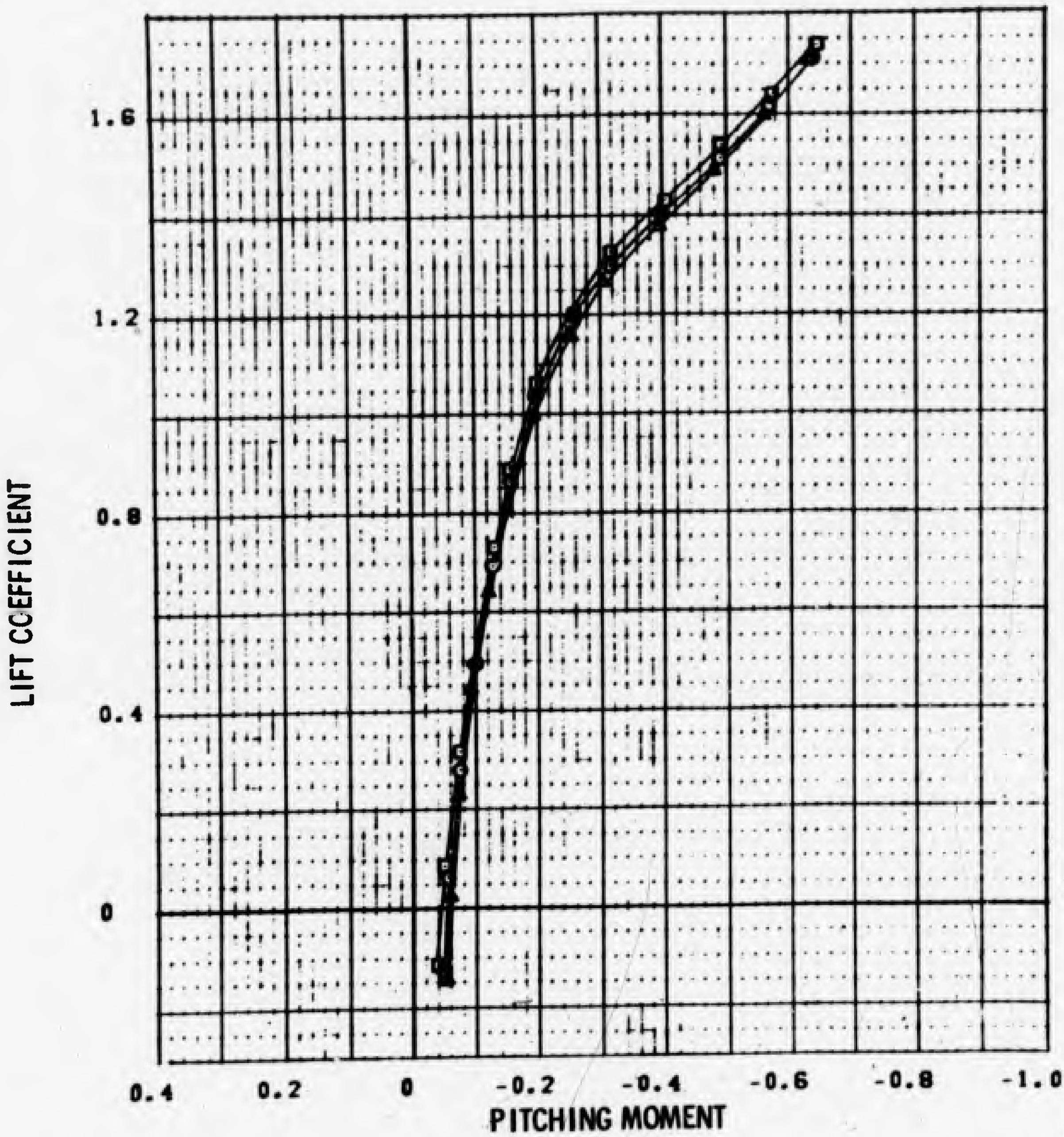
SYM	TEST	PART	FLAP	L.E. (L/R)
○	PWT 4T TC-043	167	F2	K1 10/10
□	PWT 4T TC-043	148	F3	K1 10/10
▲	PWT 4T TC-043	127	F1	K1 10/10

FIGURE 116b EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.8



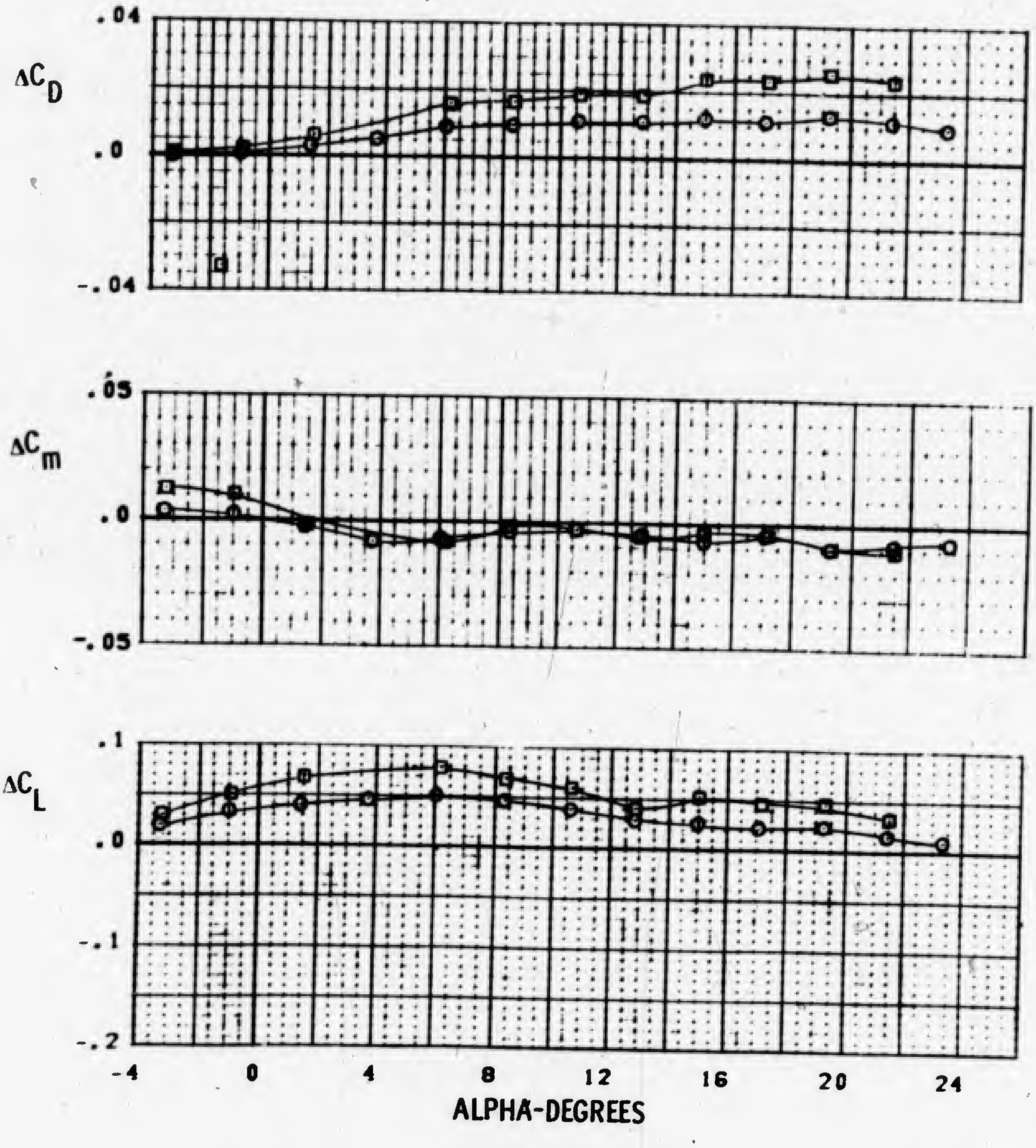
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	167	F2	K1 10/10
⊡	PWT 4T TC-043	148	F3	K1 10/10
▲	PWT 4T TC-043	127	F1	K1 10/10

FIGURE 116b EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.8



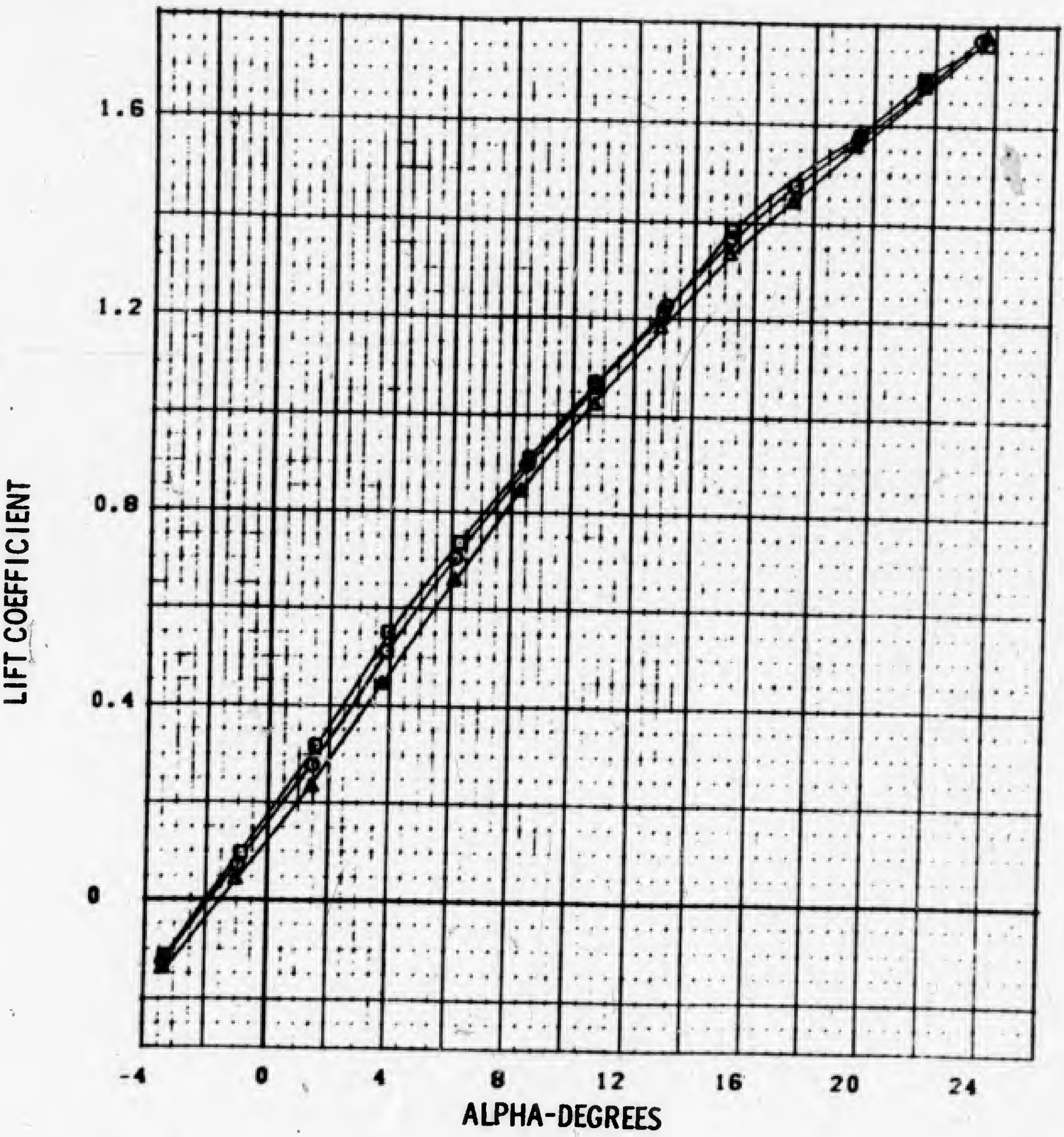
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	167	F2	K1 10/10
⊡	PWT 4T TC-043	148	F3	K1 10/10
▲	PWT 4T TC-043	127	F1	K1 10/10

FIGURE 116b EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.8



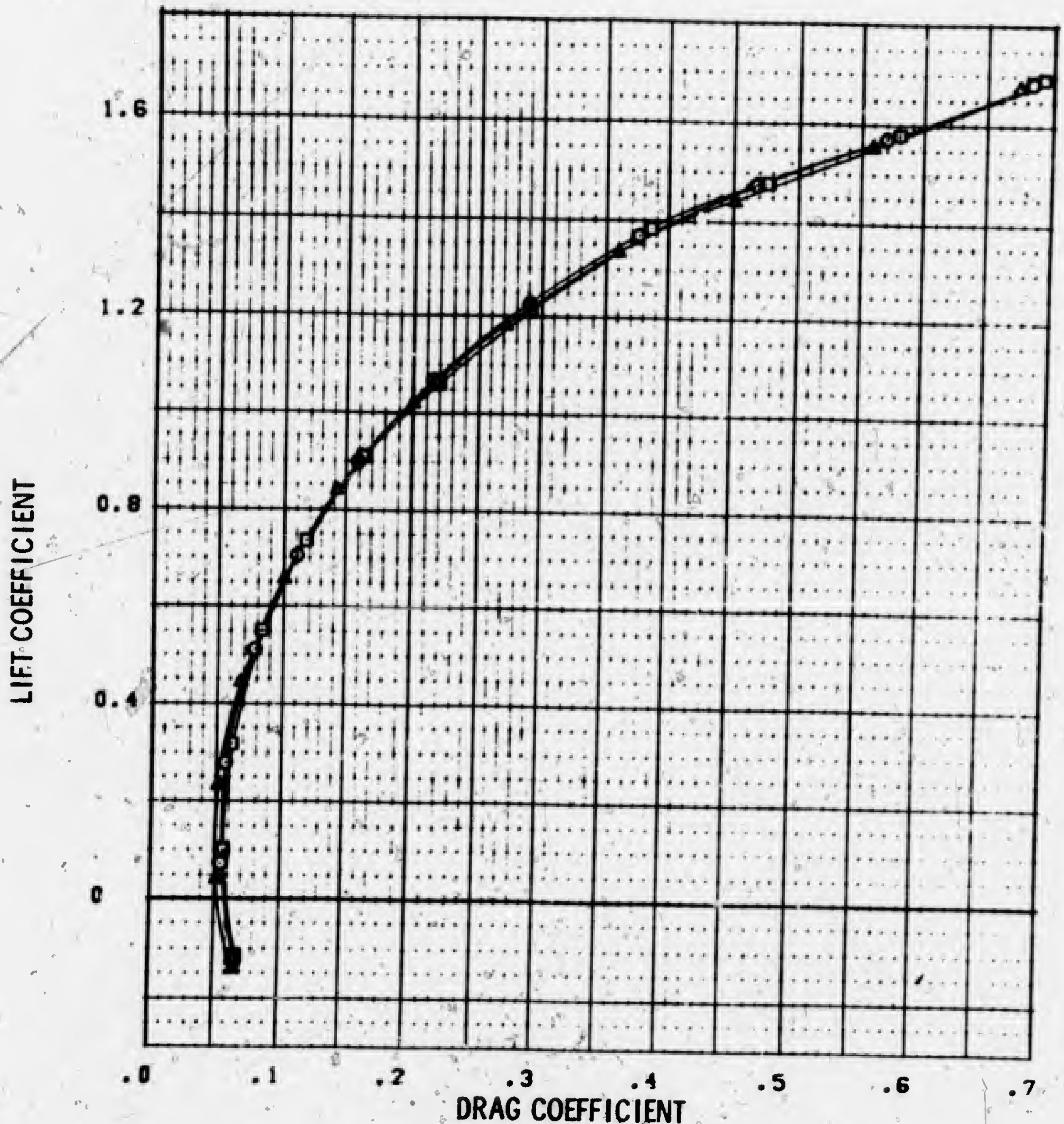
SYM	TEST	INCREMENT	FLAP	L.E. (L/R)
O	PWT 4T TC-043	PN 167 - PN 127	F2	K1 10/10
□	PWT 4T TC-043	PN 148 - PN 127	F3	K1 10/10

FIGURE 116b EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.8



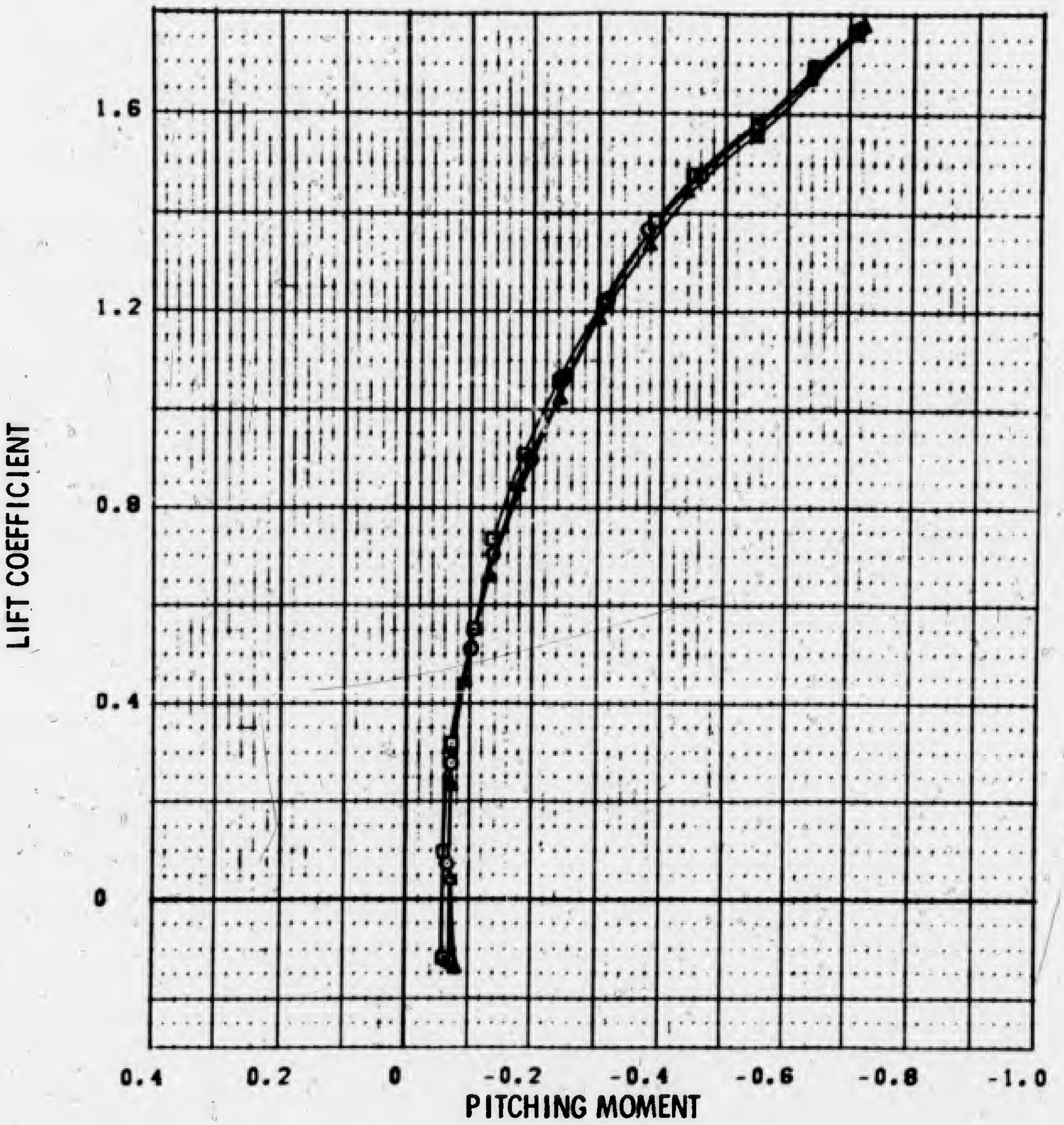
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	166	F2	K1 10/10
⊡	PWT 4T TC-043	147	F3	K1 10/10
▲	PWT 4T TC-043	126	F1	K1 10/10

FIGURE 116c EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.9



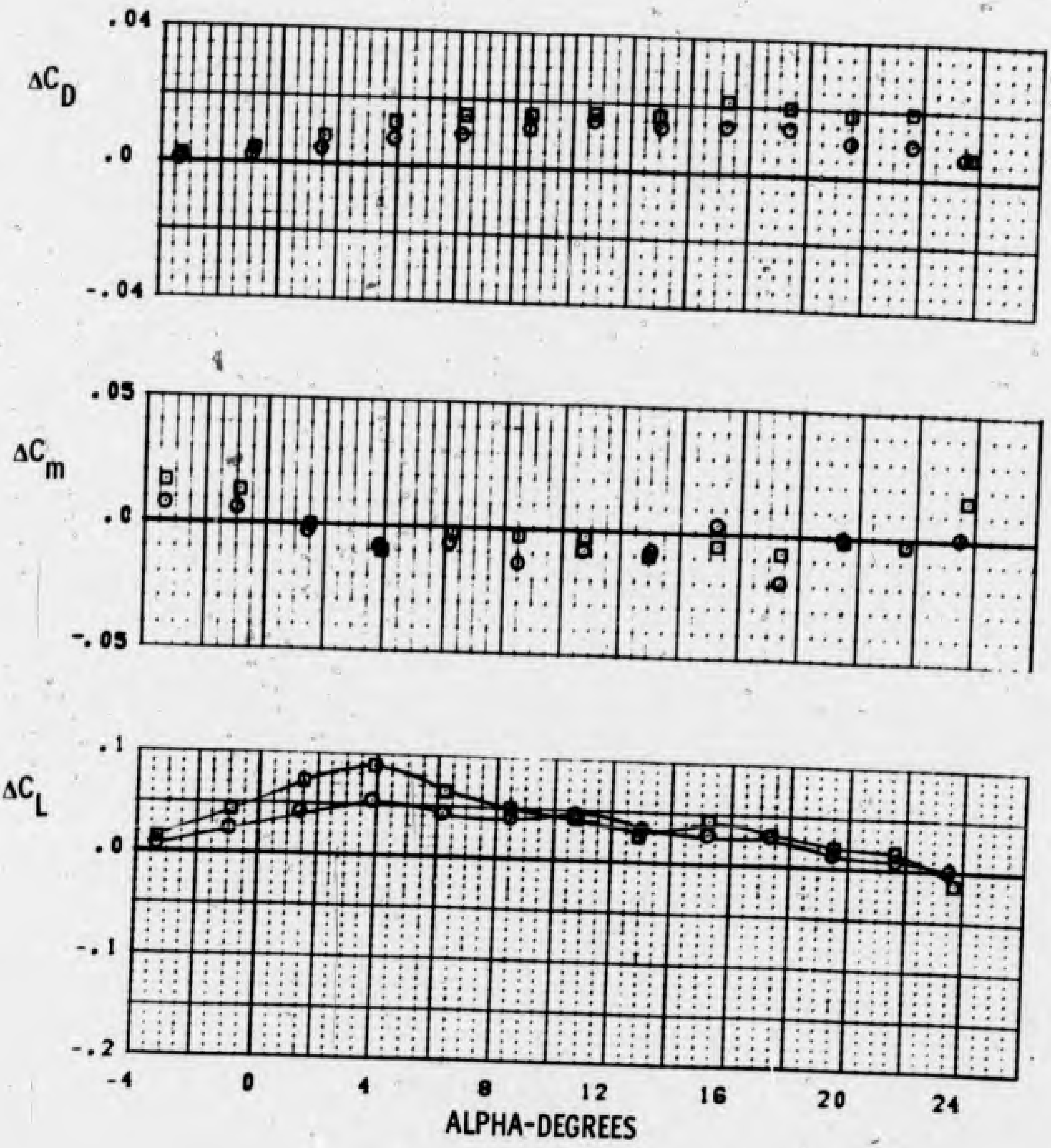
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	166	F2	K1 10/10
⊡	PWT 4T TC-043	147	F3	K1 10/10
▲	PWT 4T TC-043	126	F1	K1 10/10

FIGURE 116c EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.9



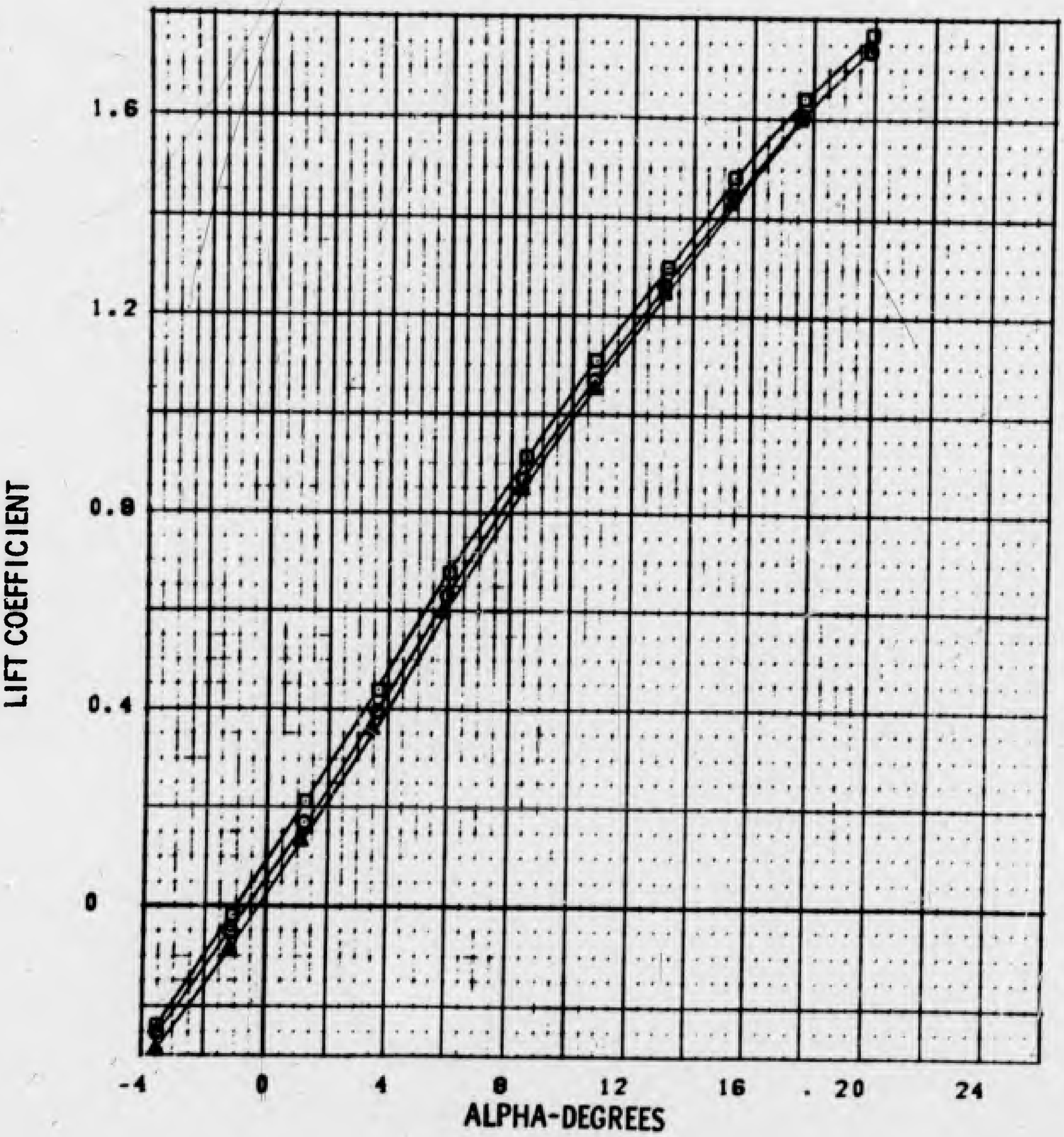
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	166	F2	K1 10/10
⊡	PWT 4T TC-043	147	F3	K1 10/10
▲	PWT 4T TC-043	126	F1	K1 10/10

FIGURE 116c EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.9



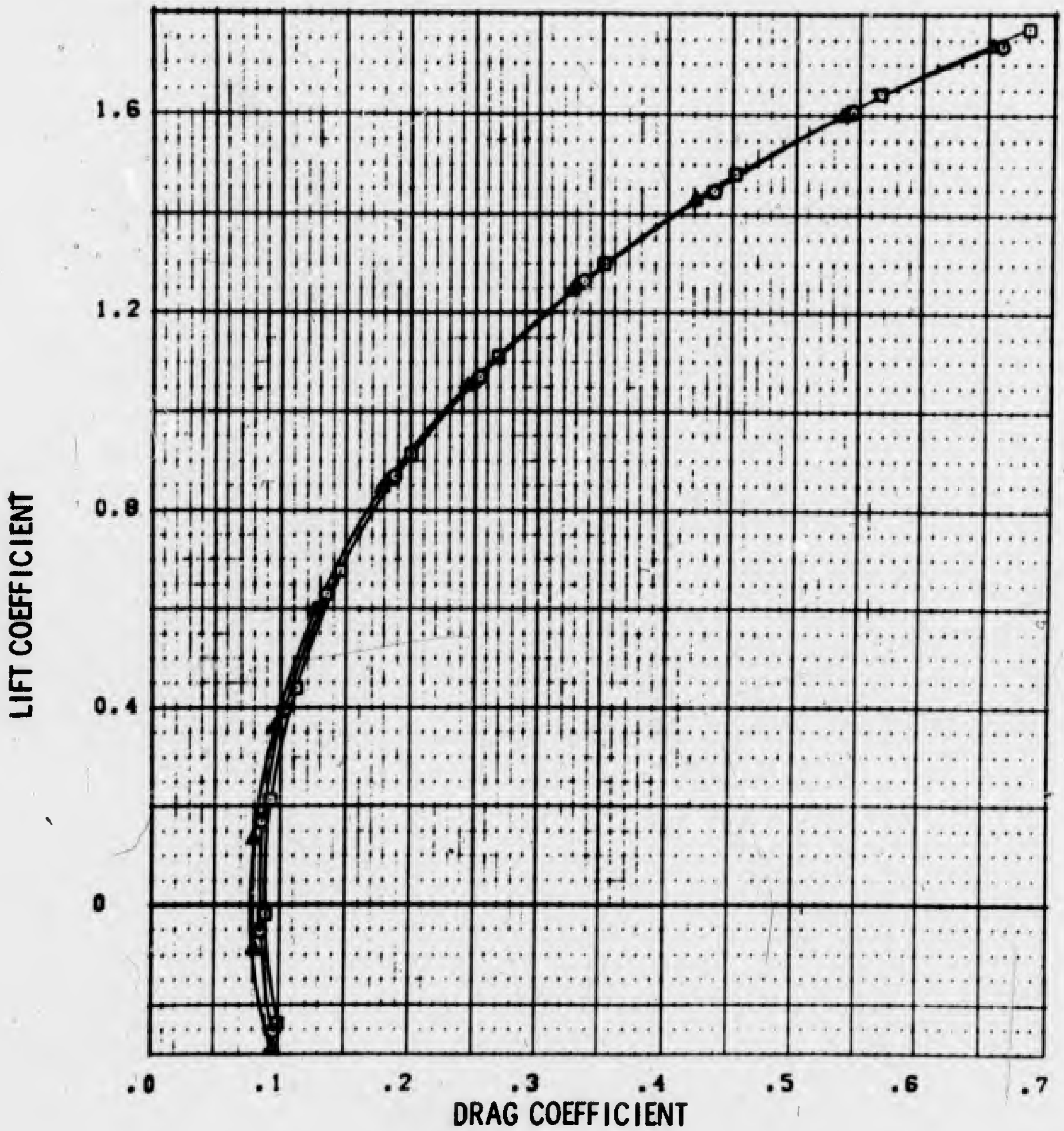
SYM	TEST	INCREMENT	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 166 - PN 126	F2	K1 10/10
⊡	PWT 4T TC-043	PN 147 - PN 126	F3	K1 10/10

FIGURE 116c EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 0.9



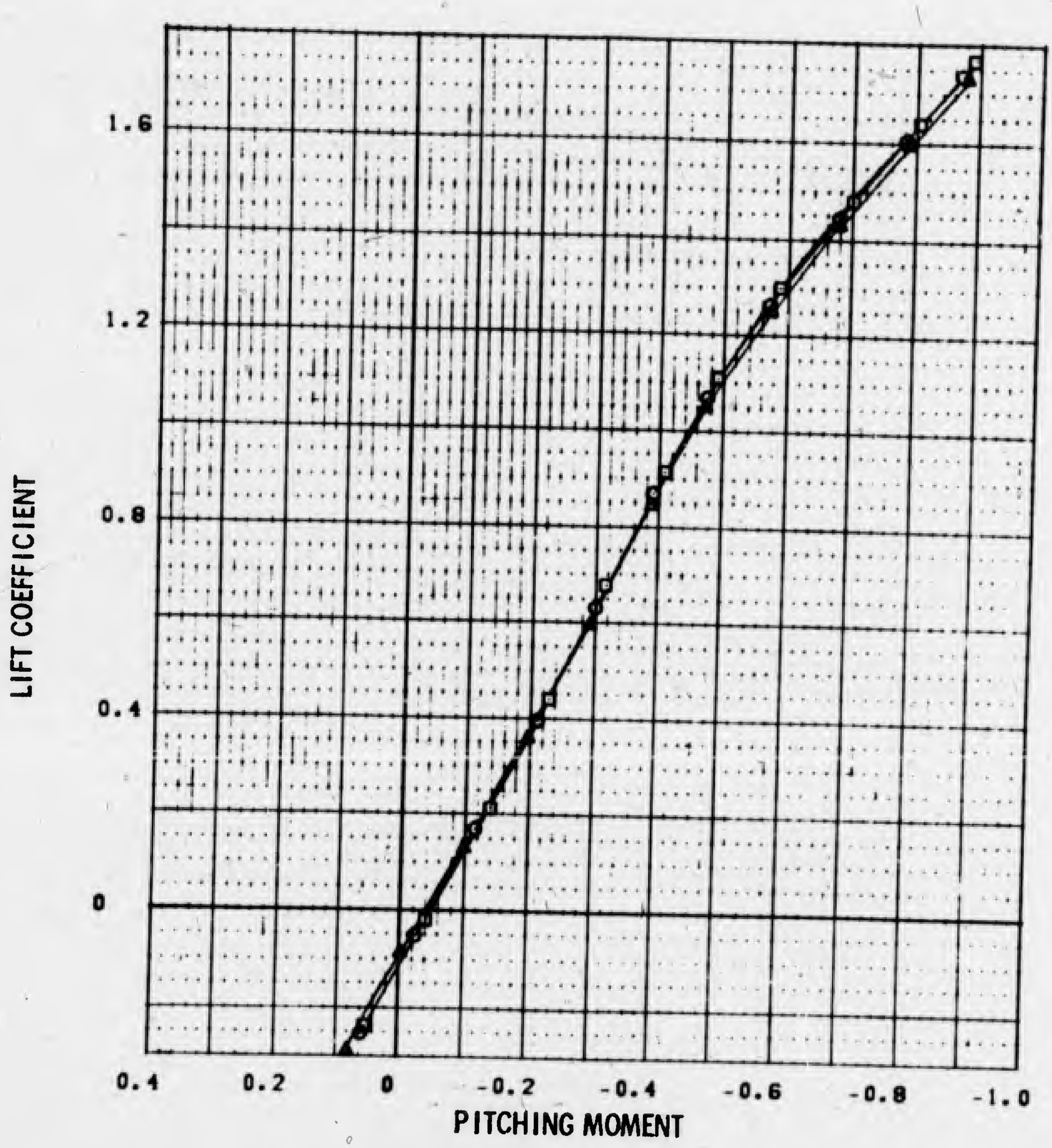
SYM	TEST	PART	FLAP	L.E. (L/R)
○	PWT 4T TC-043	169	F2	K1 10/10
□	PWT 4T TC-043	150	F3	K1 10/10
▲	PWT 4T TC-043	129	F1	K1 10/10

FIGURE 116d EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 1.2



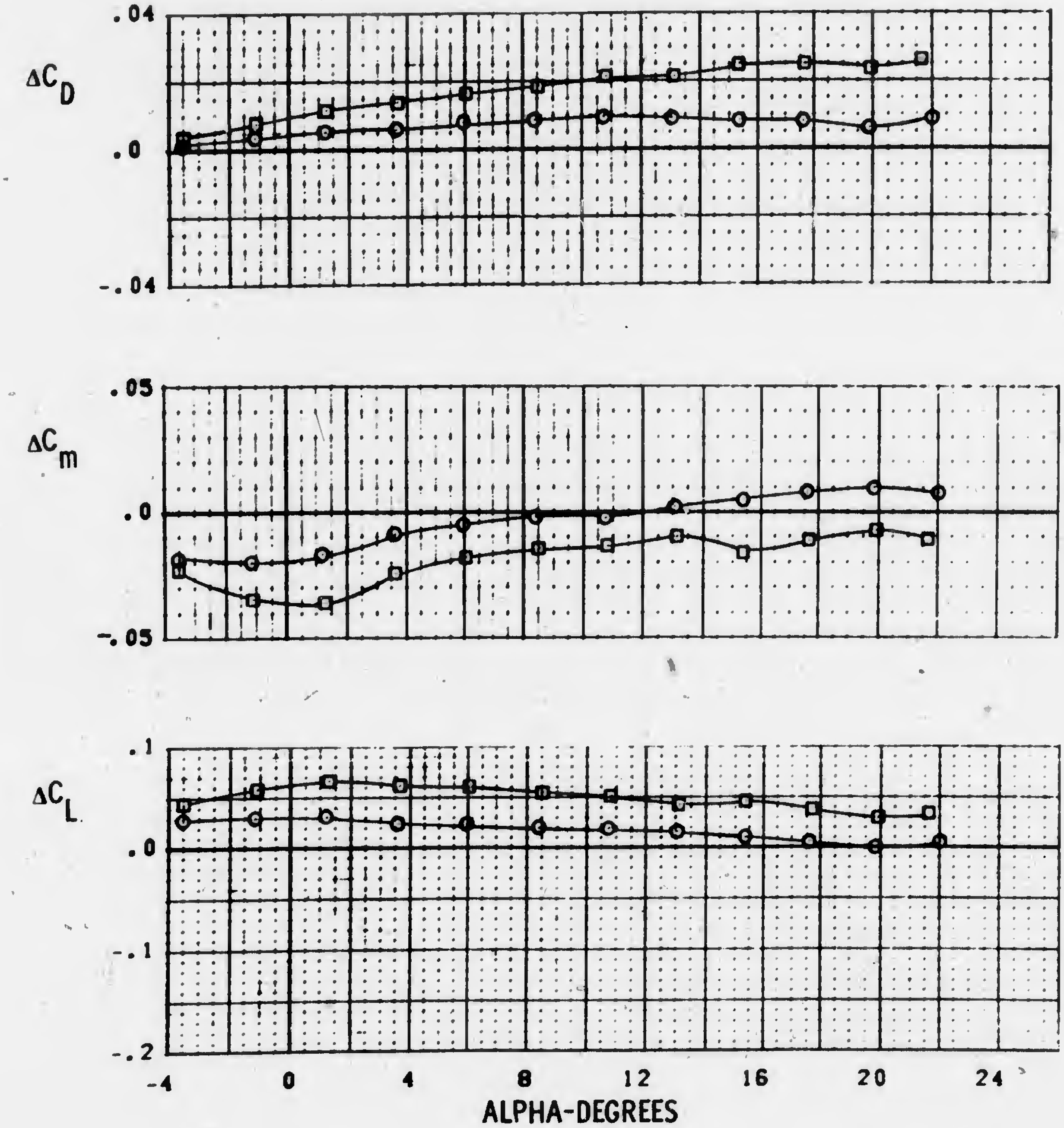
SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	169	F2	K1 10/10
⊡	PWT 4T TC-043	150	F3	K1 10/10
▲	PWT 4T TC-043	129	F1	K1 10/10

FIGURE 116d EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 1.2



SYM	TEST	PART	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	169	F2	K1 10/10
⊡	PWT 4T TC-043	150	F3	K1 10/10
▲	PWT 4T TC-043	129	F1	K1 10/10

FIGURE 116d EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 1.2



SYM	TEST	INCREMENT	FLAP	L.E. (L/R)
⊙	PWT 4T TC-043	PN 169 - PN 129	F2	K1 10/10
⊡	PWT 4T TC-043	PN 150 - PN 129	F3	K1 10/10

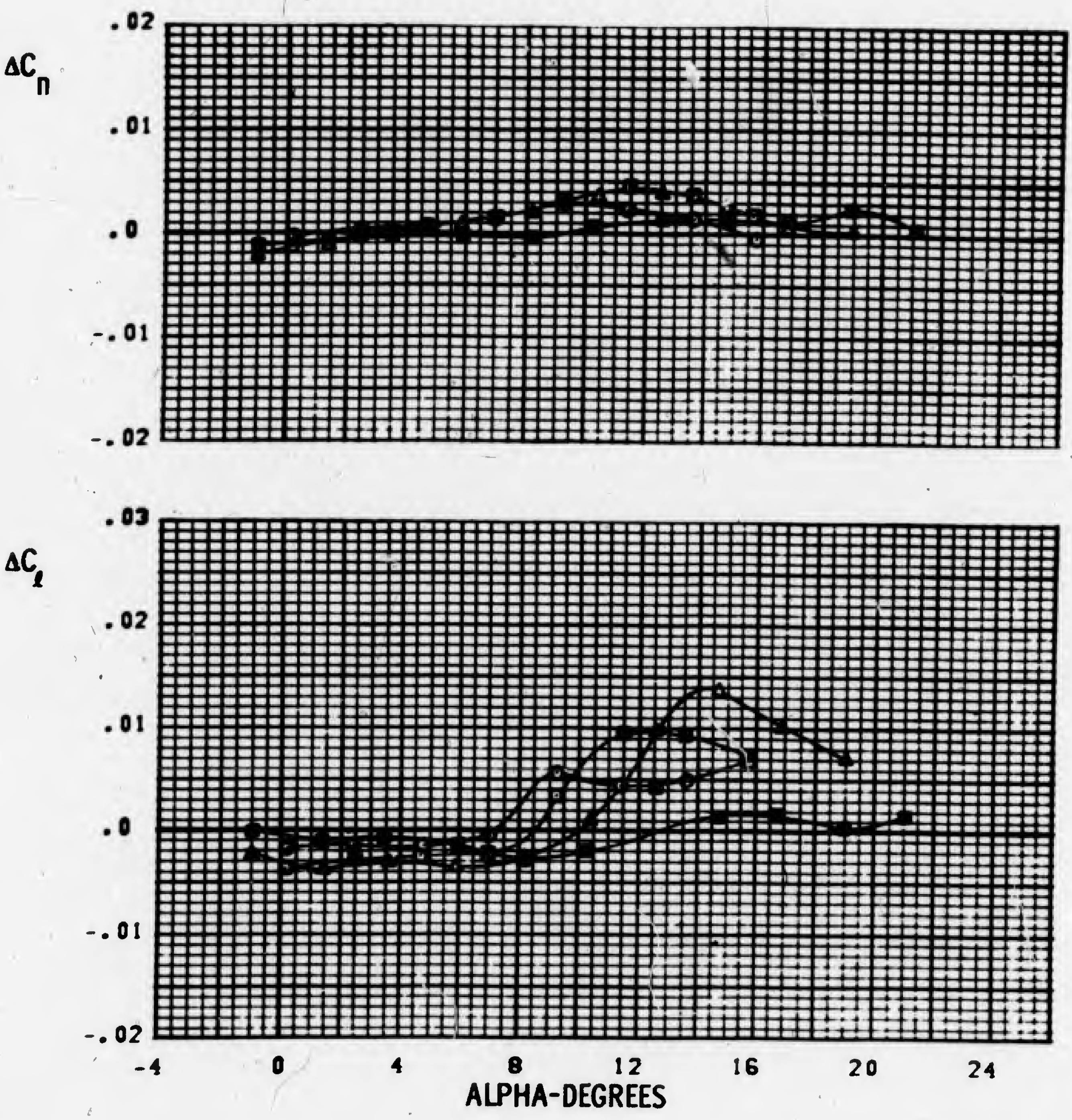
FIGURE 116d EFFECT OF SPLIT TRAILING EDGE FLAPS
M = 1.2

APPENDIX V

FORCE AND MOMENT COMPARISONS - ROLL CONTROL DEVICES

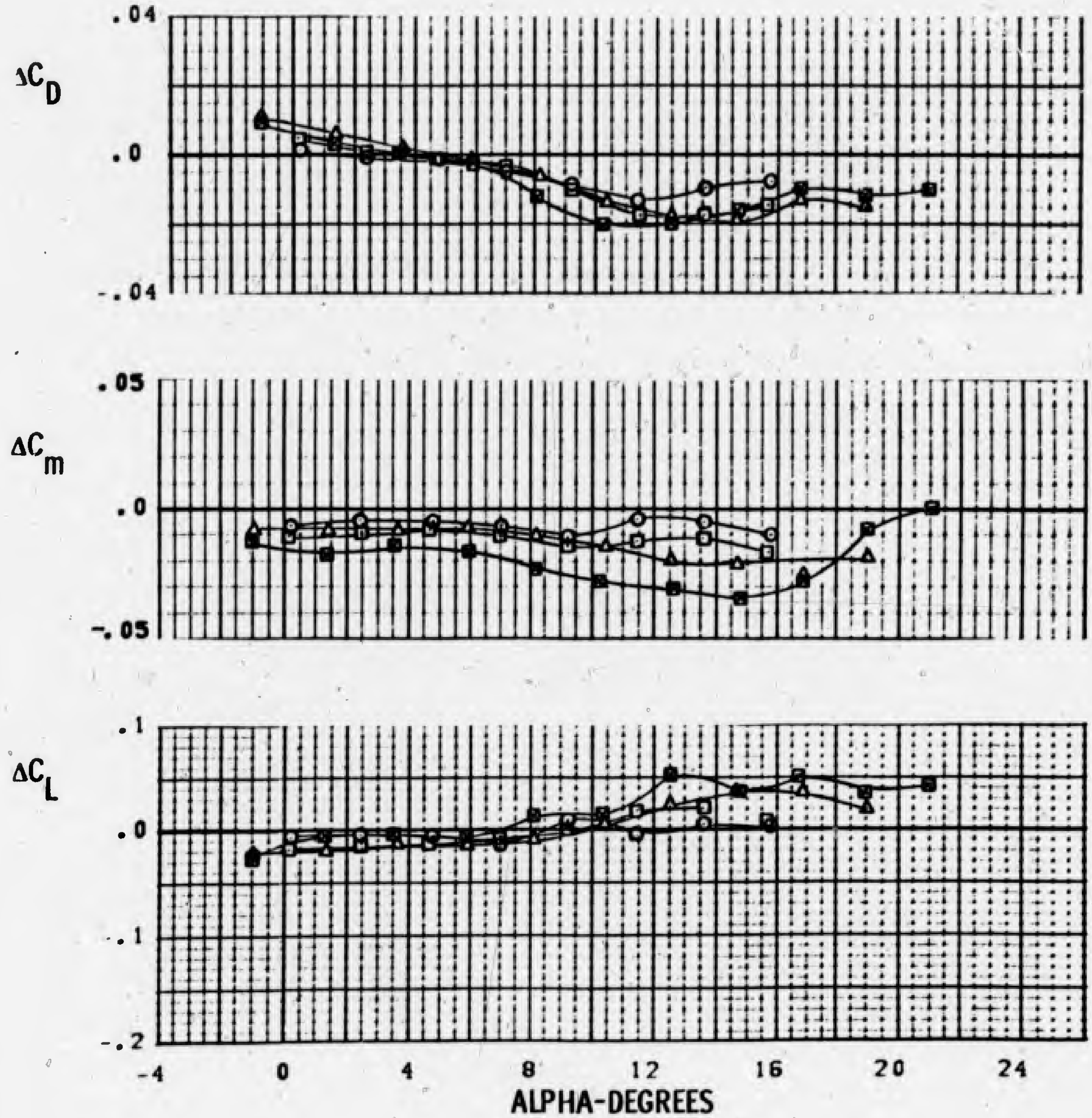
1. DIFFERENTIAL LEADING EDGE FLAPS

Incremental force and moment coefficients for various differential deflections of the leading edge flaps are presented in Figure 117. This data is also given in numerical form, Table V as an aid for estimating effects for other configurations.



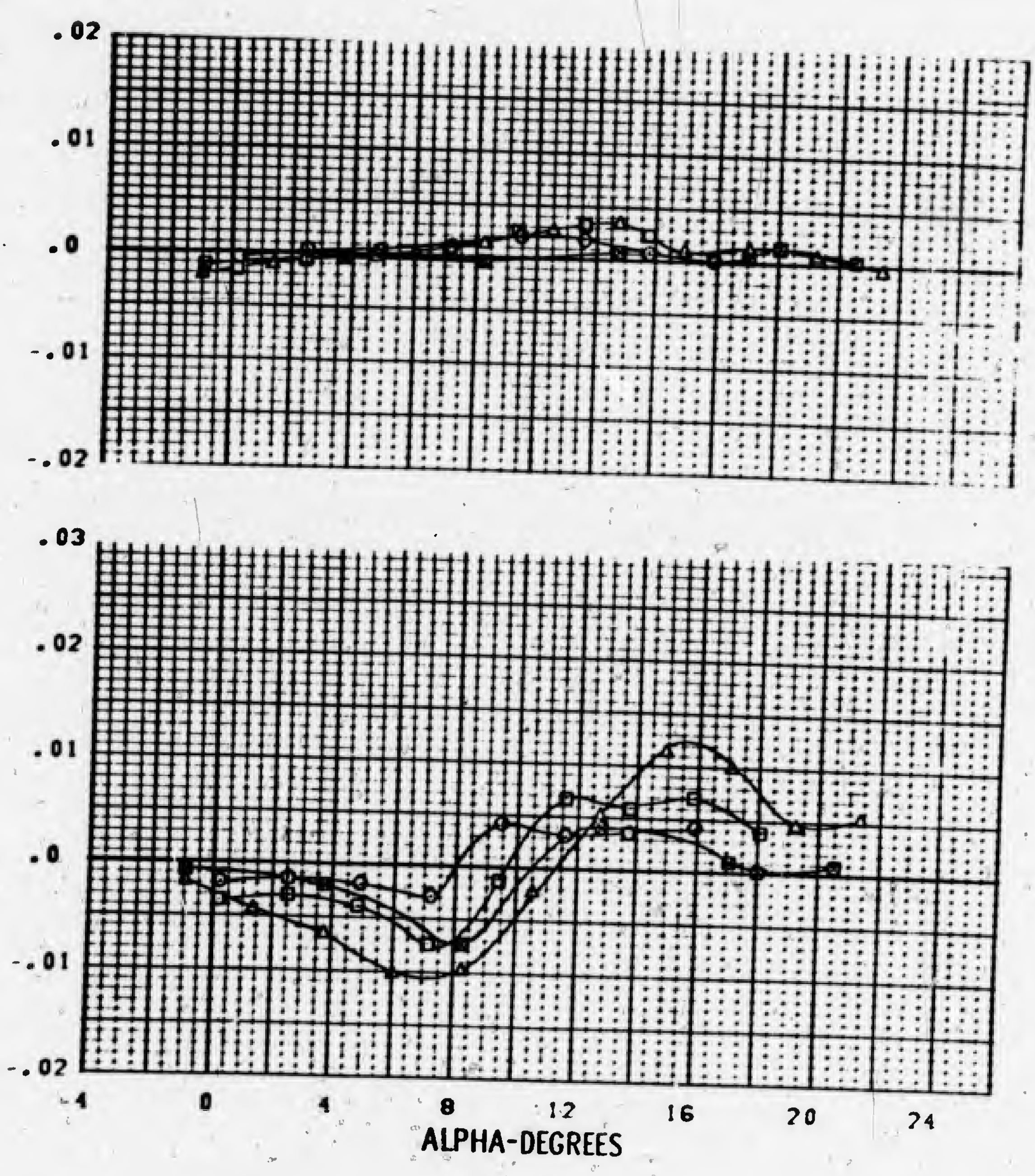
SYM	TEST	INCREMENT	L.E.	(L/R)
⊙	PWT 4T TC-043	PN 454 - PN 438	K1	5/0
⊡	PWT 4T TC-043	PN 433 - PN 438	K1	10/0
△	PWT 4T TC-043	PN 187 - PN 268	K1	15/0
■	PWT 4T TC-043	PN 257 - PN 268	K1	10/5

FIGURE 117a DIFFERENTIAL L.E. FLAP EFFECTS
M = 0.7



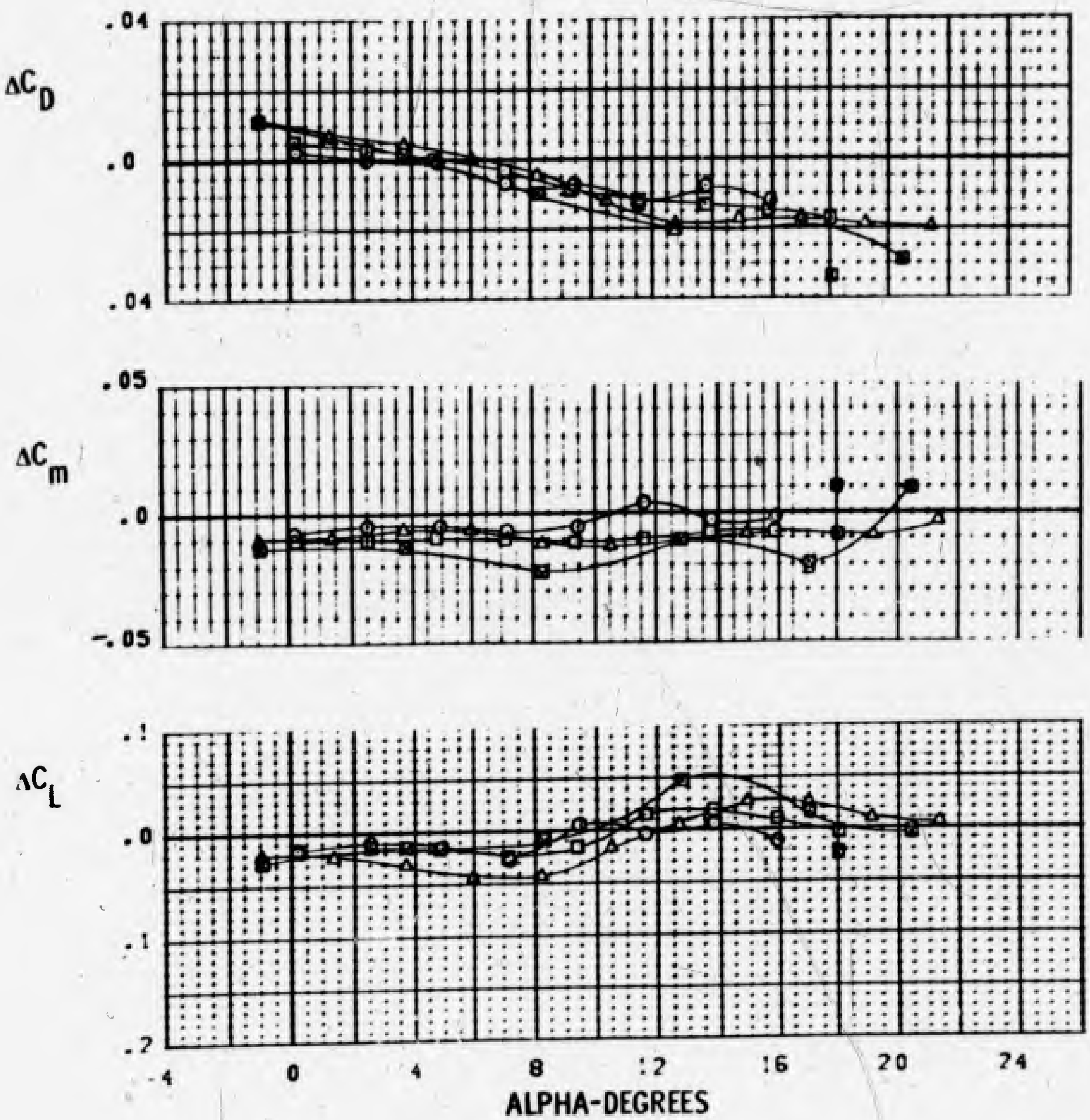
SYM	TEST	INCREMENT		L.E. (I/R)
○	PWT 4T TC 043	PN 454	PN 438	KI 5/0
□	PWT 4T TC 043	PN 433	PN 438	KI 10/0
△	PWT 4T TC 043	PN 187	PN 268	KI 15/0
■	PWT 4T TC 043	PN 257	PN 268	KI 10/5

FIGURE 117a DIFFERENTIAL L.E. FLAP EFFECTS
M 0.7



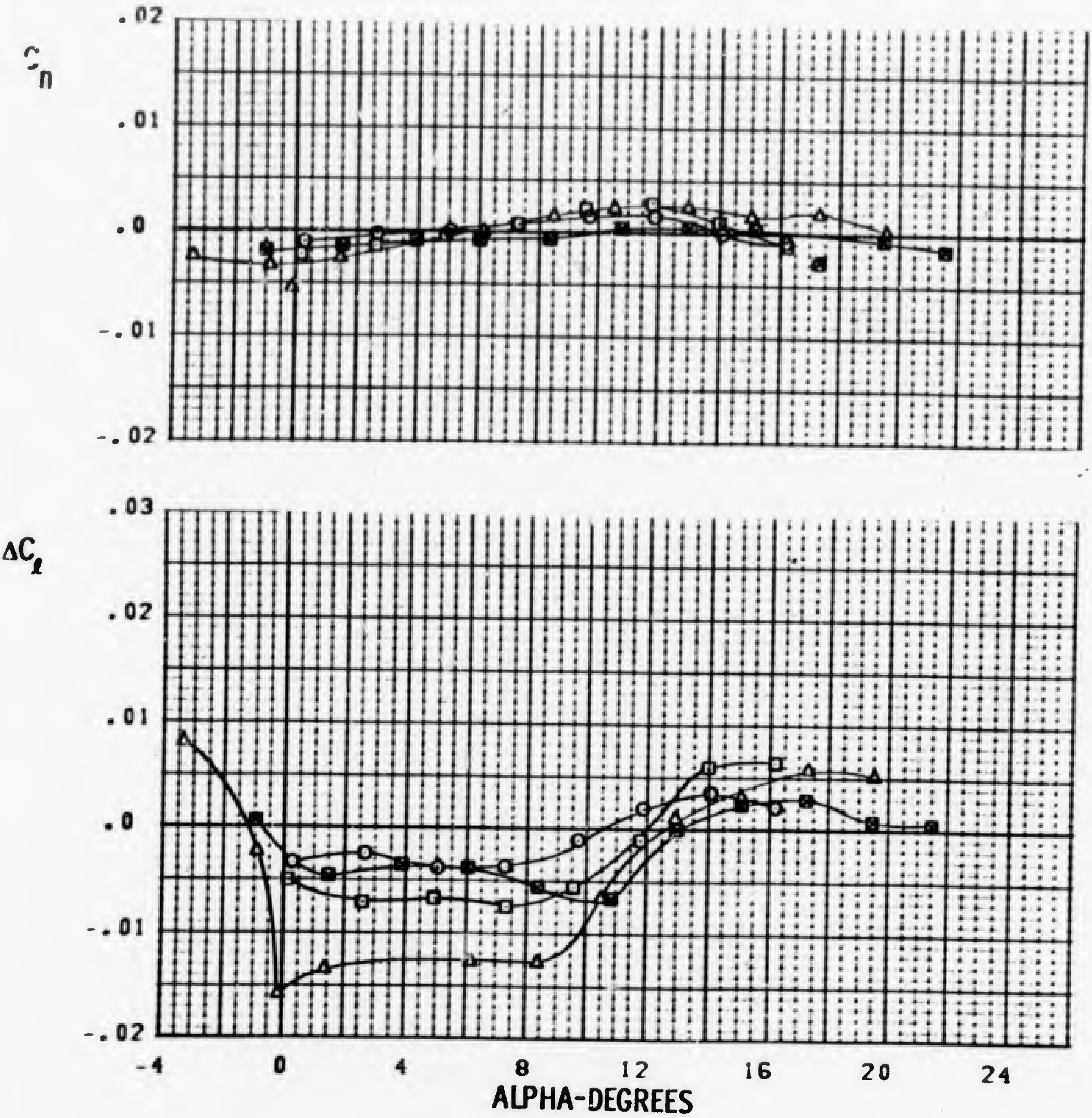
SYM	TEST		INCREMENT	L.E. (L/R)	
O	PWT 4T	TC-043	PN 455 - PN 440	K1	5/0
□	PWT 4T	TC-043	Pn 434 - PN 440	K1	10/0
Δ	PWT 4T	TC-043	PN 186 - PN 267	K1	15/0
⊠	PWT 4T	TC-043	PN 254 - ON 267	K1	10/5

Figure 117b DIFFERENTIAL L.E. FLAP EFFECTS
M = 0.8



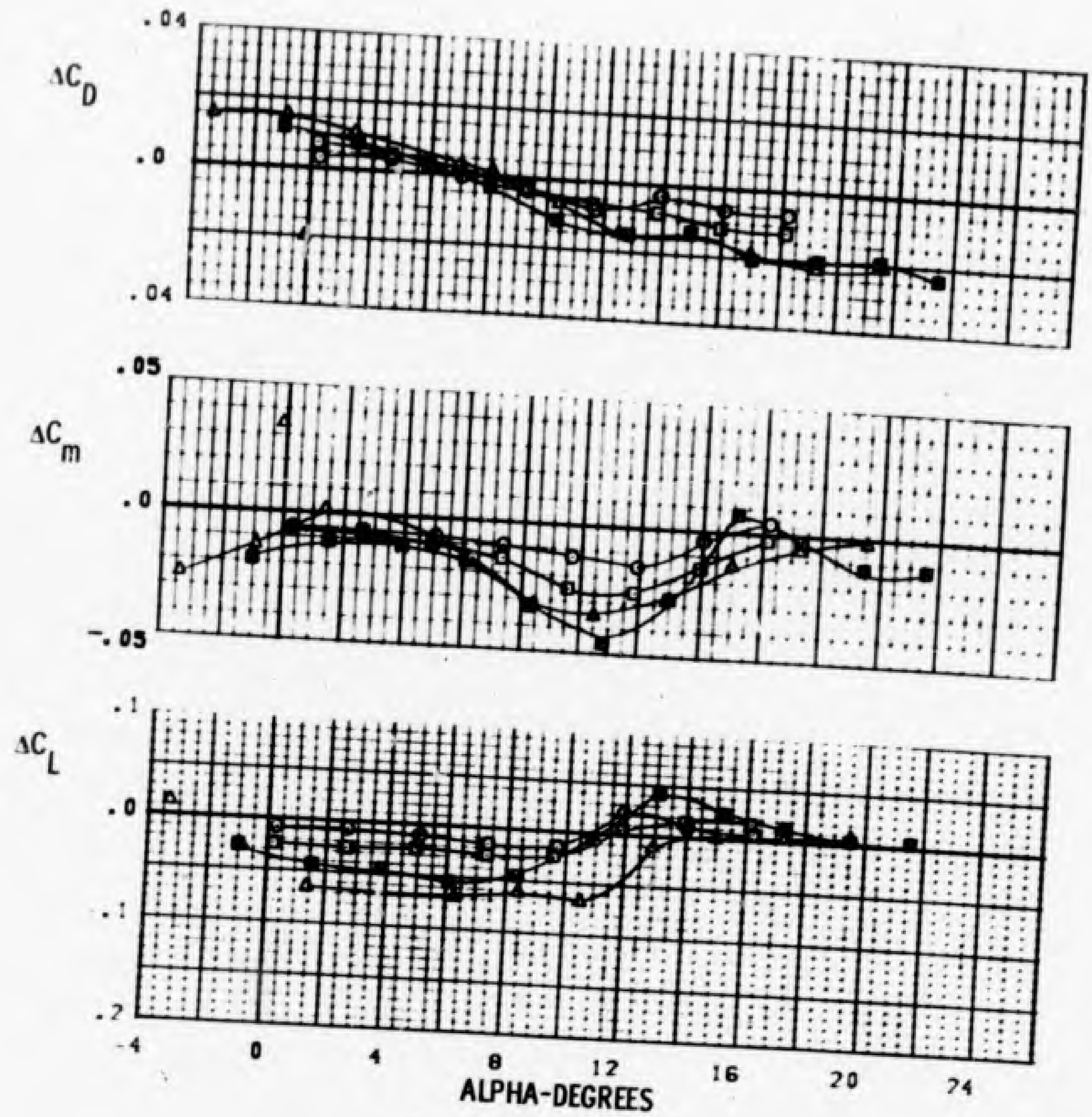
SYM	TEST		INCREMENT	L.E. (L/R)	
○	PWT 4T	TC-043	PN 455 - PN 440	K1	5/0
□	PWT 4T	TC-043	PN 434 - PN 440	K1	10/0
△	PWT 4T	TC-043	PN 186 - PN 267	K1	15/0
⊠	PWT 4T	TC-043	PN 254 - PN 267	K1	10/5

Figure 117b DIFFERENTIAL L.E. FLAP EFFECTS
$M = 0.8$



SYM	TEST	INCREMENT	L.E. (L/R)
⊙	PWT 4T TC-043	PN 453 - PN 441	KI 5/0
⊡	PWT 4T TC-043	PN 437 PN 441	KI 10/0
Δ	PWT 4T TC-043	PN 185 PN 264	KI 15/0
■	PWT 4T TC-043	PN 253 PN 264	KI 10/5

FIGURE 117c DIFFERENTIAL L.E. FLAP EFFECTS
M = 0.9



SYM	[illegible]S[illegible]		INCREMENT		[illegible]
⊙	PW[illegible] 4[illegible]	[illegible]C 043	PN 453	P[illegible] 44[illegible]	[illegible] 5/C
⊡	PW[illegible] 4[illegible]	[illegible]C 043	PN 432	P[illegible] 44[illegible]	[illegible] 10/C
Δ	PW[illegible] 4[illegible]	[illegible]C 043	PN [illegible]85	P[illegible] 264	[illegible] 15/C
■	PW[illegible] 4[illegible]	[illegible]C 043	PN 253	P[illegible] 264	[illegible] 10-5

FIGURE 117c DIFFERENTIAL [illegible] FLAP EFFECTS [illegible] 0.9

Table V DIFFERENTIAL LEADING EDGE FLAP ROLL CONTROL INCREMENTAL DATA SUMMARY

Horizontal Tail Cn — Ailerons Neutral

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.7	K1	5/0	0.20300	-0.00704	-0.00614	0.00168	-0.00170	-0.00040	PWT 4T	444	438
			2.42700	-0.00485	-0.00390	-0.00041	-0.00150	0.00020			
			4.79200	-0.00550	-0.00457	-0.00139	-0.00149	0.00060			
			7.02200	-0.01400	-0.00611	-0.00491	-0.00046	0.00139			
			9.23200	0.00805	-0.01056	-0.00878	0.00560	0.00300			
			11.42400	-0.00624	-0.00396	-0.01324	0.00441	0.00230			
			13.62000	0.00556	-0.00502	-0.00936	0.00502	0.00139			
			15.78600	0.00619	-0.00970	-0.00778	0.00686	-0.00049			
0.7	K1	10/0	0.14000	-0.01767	-0.01013	0.00496	-0.00370	-0.00140	PWT 4T	433	438
			2.45300	-0.01269	-0.00388	0.00109	-0.00280	-0.00010			
			4.68100	-0.01055	-0.00408	-0.00087	-0.00250	0.00150			
			6.97800	-0.01174	-0.01027	-0.00345	-0.00210	0.00150			
			9.22100	0.00271	-0.01421	-0.00991	0.00339	0.00330			
			11.43600	0.01758	-0.01231	-0.01744	0.00941	0.00449			
			13.58700	0.02053	-0.01130	-0.01723	0.00941	0.00380			
			15.70000	0.00974	-0.01636	-0.01434	0.00740	0.00100			
0.7	K1	15/0	-0.58100	-0.02281	-0.00797	0.01075	-0.00261	-0.00229	PWT 4T	197	268
			1.39400	-0.02110	-0.00788	0.00576	-0.00390	-0.00110			
			3.62800	-0.01653	-0.00692	0.00168	-0.00331	0.00010			
			5.86600	-0.01563	-0.00680	-0.00125	-0.00340	0.00090			
			8.17800	-0.00880	-0.00941	-0.00670	-0.00246	0.00198			
			10.38100	0.01303	-0.01628	-0.01306	0.00099	0.00368			
			10.40700	0.00677	-0.01320	-0.01446	0.00221	0.00327			
			10.41100	0.00843	-0.01403	-0.01409	0.00231	0.00327			
			12.53400	0.02419	-0.01865	-0.01791	0.00961	0.00390			
			12.53600	0.02267	-0.01870	-0.01338	0.00961	0.00490			
			12.53700	0.02361	-0.01859	-0.01212	0.00961	0.00390			
			14.66900	0.03544	-0.02113	-0.01308	0.01349	0.00260			
			16.85799	0.03632	-0.02367	-0.01373	0.01163	0.00053			
			19.00999	0.01936	-0.01775	-0.01490	0.00700	0.00150			

Table V CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.7	K1	10/5	-1.00500	-0.02742	-0.01184	0.01006	-0.00051	-0.00129	PWT 4T	257	269
			1.34200	-0.00677	-0.01570	0.00377	-0.00100	-0.00090			
			3.47500	-0.00846	-0.01320	0.00033	-0.00070	-0.00050			
			5.92800	-0.00835	-0.01584	-0.00309	-0.00150	-0.00060			
			8.13200	0.00968	-0.02208	-0.01237	-0.00283	-0.00051			
			10.24500	0.04936	-0.02665	-0.02063	-0.00199	0.00070			
			12.58000	0.05146	-0.02955	-0.01973	0.00423	0.00150			
			14.74100	0.03617	-0.03388	-0.01571	0.00140	0.00119			
			16.78795	0.04862	-0.02608	-0.01014	0.00170	0.00131			
			19.03295	0.03487	-0.00688	-0.01246	0.00041	0.00248			
			21.03658	0.04254	-0.00052	-0.01038	0.00177	0.00063			
0.9	K1	5/0	0.20000	-0.01545	-0.00698	0.00247	-0.00180	-0.00050	PWT 4T	455	440
			2.53000	-0.00892	-0.00432	0.00042	-0.00140	0.00030			
			4.90800	-0.01487	-0.00509	-0.00082	-0.00181	0.00040			
			7.21600	-0.02853	-0.00677	-0.00675	-0.00280	0.00130			
			9.44600	0.00533	-0.00542	-0.00717	0.00421	0.00230			
			11.61500	-0.00323	0.00389	-0.01289	0.00318	0.00180			
			13.78300	0.00478	-0.00258	-0.00765	0.00360	0.00080			
			15.94700	-0.01104	-0.00179	-0.01207	0.00419	0.00020			
0.8	K1	10/0	0.18500	-0.02000	-0.00967	0.00566	-0.00360	-0.00159	PWT 4T	434	440
			2.51900	-0.01304	-0.00982	0.00271	-0.00300	-0.00040			
			4.82300	-0.01669	-0.00840	0.00035	-0.00300	0.00000			
			7.12700	-0.02452	-0.00463	-0.00295	-0.00736	0.00081			
			9.37100	-0.01446	-0.01129	-0.00861	-0.00114	0.00271			
			11.58500	0.01420	-0.00992	-0.01215	0.00679	0.00330			
			13.78300	0.01927	-0.00778	-0.01295	0.00600	0.00230			
			15.91400	0.00966	-0.00763	-0.01446	0.00710	0.00050			
			18.07199	-0.00241	-0.00899	-0.01701	0.00381	0.00130			

NOT REPRODUCIBLE

Table V CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	DATA RUN	BASE RUN
0.8	K1	15/0	-0.96800	-0.02346	-0.01044	0.01084	-0.00200	-0.00249	PWT 4T	196	267
			-0.89600	-0.02201	-0.01209	0.01124	-0.00200	-0.00220			
			1.38400	-0.02495	-0.00887	0.00681	-0.00450	-0.00110			
			3.70400	-0.03179	-0.00513	0.00386	-0.00660	-0.00059			
			6.02000	-0.04379	-0.00562	-0.00011	-0.01027	0.00021			
			8.28300	-0.03952	-0.01200	-0.00465	-0.00980	0.00132			
			10.54400	-0.01526	-0.01279	-0.01201	-0.00251	0.00271			
			12.71200	0.00650	-0.01133	-0.01850	0.00500	0.00330			
			14.93800	0.02622	-0.00848	-0.01742	0.01111	0.00120			
			17.07799	0.02527	-0.02179	-0.01748	0.01000	0.00120			
			19.24799	0.00855	-0.00853	-0.01881	0.00421	0.00101			
			21.38499	0.00513	-0.00377	-0.02009	0.00529	-0.00050			
0.8	K1	10/5	-0.89000	-0.02936	-0.01365	0.01027	-0.00070	-0.00110	PWT 4T	254	267
			3.78700	-0.01522	-0.01320	0.00187	-0.00220	-0.00060			
			8.26300	-0.01088	-0.02356	-0.01081	-0.00750	-0.00058			
			12.83400	0.04523	-0.00987	-0.01955	0.00391	0.00100			
			17.09599	0.01815	-0.01916	-0.01845	0.00110	0.00020			
			18.08299	-0.02052	0.00941	-0.03380	0.00019	0.00125			
			20.51399	-0.00105	0.00816	-0.02850	0.00092	0.00038			
0.9	K1	5/0	0.30000	-0.00864	-0.00568	0.00350	-0.00340	-0.00100	PWT 4T	453	441
			2.65400	-0.00702	-0.00611	0.00371	-0.00250	-0.00030			
			5.03300	-0.01040	-0.00651	-0.00034	-0.00380	-0.00010			
			7.32100	-0.01596	-0.00892	-0.00362	-0.00368	0.00080			
			9.68000	-0.01500	-0.01245	-0.00785	-0.00110	0.00150			
			11.50800	0.02137	-0.01499	-0.00313	0.00120	0.00140			
			14.07000	0.01704	-0.00348	-0.00635	0.00317	[illegible]			
			16.22099	0.00672	0.00427	-0.00717	0.00216	-0.00078			

Table V CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.9	K1	10/0	0.16800	-0.02338	-0.00725	0.00780	-0.00501	-0.00220	PWT 4T	432	441
			2.59400	-0.02557	-0.00700	0.00547	-0.00710	-0.00140			
			4.91900	-0.02261	-0.01012	0.00234	-0.00670	-0.00060			
			7.32100	-0.02746	-0.01412	-0.00283	-0.00748	0.00060			
			9.58000	-0.02503	-0.02479	-0.00664	-0.00557	0.00211			
			11.94000	0.00511	-0.02522	-0.00794	-0.00110	0.00290			
			13.94400	0.01527	-0.01414	-0.01136	0.00581	0.00111			
			16.17099	0.01679	-0.00264	-0.01195	0.00639	-0.00140			
0.9	K1	15/0	-3.37100	0.01538	-0.02456	0.01444	0.00799	-0.00241	PWT 4T	185	264
			-0.98800	-0.02757	-0.01238	0.01449	-0.00260	-0.00330			
			-0.12200	-1.80998	0.03575	-0.02036	-0.01590	-0.00557			
			1.40500	-0.06363	0.00199	0.01045	-0.01330	-0.00271			
			6.16500	-0.06527	-0.01512	0.00151	-0.01269	-0.00030			
			8.42900	-0.05989	-0.03099	-0.00691	-0.01285	0.00163			
			10.52100	-0.06463	-0.03443	-0.01467	-0.00654	0.00220			
			12.92000	-0.01021	-0.02722	-0.01391	0.00100	0.00250			
			14.99000	0.00062	-0.01303	-0.01852	0.00310	0.00170			
			17.28899	0.00532	-0.00516	-0.02205	0.00581	0.00178			
			19.52299	0.00823	-0.00161	-0.02114	0.00500	0.00007			
0.9	K1	10/5	-1.00300	-0.02641	-0.01709	0.01291	0.00085	-0.00177	PWT 4T	253	264
			1.53300	-0.04109	-0.01049	0.00761	-0.00450	-0.00130			
			3.89200	-0.04558	-0.01119	0.00315	-0.00330	-0.00100			
			6.06300	-0.05197	-0.01597	-0.00276	-0.00348	-0.00099			
			8.38000	-0.04538	-0.03234	-0.01210	-0.00543	-0.00046			
			10.84400	-0.00596	-0.04480	-0.01499	-0.00678	0.00068			
			12.97600	0.03967	-0.02576	-0.01291	0.0	0.00061			
			15.12300	0.02634	0.00762	-0.02060	0.00230	0.00042			
			17.27499	0.01735	-0.00340	-0.01954	0.00301	-0.00262			
			19.42499	0.00738	-0.01302	-0.02028	0.00082	-0.00052			
			21.57399	0.00647	-0.01264	-0.02287	0.00093	-0.00108			

Table V CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
1.2	K1	5/0	-2.26700	-0.01810	-0.00296	0.00428	-0.00285	-0.00210	PWT 4T	456	269
			-2.25500	-0.01779	-0.00359	0.00479	-0.00275	-0.00220			
			0.13800	-0.02210	-0.00070	0.00253	-0.00404	-0.00180			
			2.39900	-0.02570	0.00179	-0.00054	-0.00438	-0.00113			
			4.91400	-0.02093	0.00261	-0.00296	-0.00365	-0.00011			
			7.27400	-0.02801	0.01299	-0.00545	-0.00285	0.00070			
			9.63500	-0.02154	0.01777	-0.00811	-0.00245	0.00165			
			12.04100	-0.01718	0.02220	-0.01024	-0.00130	0.00265			
			14.34100	-0.00863	0.01570	-0.01015	-0.00015	0.00315			
			16.40700	-0.00600	0.01612	-0.01138	0.00108	0.00290			
			18.62700	-0.00284	0.01958	-0.01084	0.00221	0.00339			
			20.58000	-0.00667	0.03245	-0.01357	0.00496	0.00315			
1.2	K1	10/0	-2.27300	-0.02405	-0.00447	0.01125	-0.00345	-0.00370	PWT 4T	435	269
			0.05400	-0.03042	-0.00360	0.00860	-0.00546	-0.00380			
			2.42900	-0.03718	-0.00085	0.00456	-0.00687	-0.00264			
			4.82500	-0.03960	0.00336	0.00018	-0.00726	-0.00121			
			7.18100	-0.03822	0.00921	-0.00431	-0.00586	0.00050			
			9.58900	-0.03463	0.01752	-0.00974	-0.00495	0.00205			
			11.88700	-0.03180	0.02148	-0.01386	-0.00433	0.00372			
			14.19000	-0.02015	0.01307	-0.01572	-0.00285	0.00485			
			16.41495	-0.01493	0.01497	-0.01758	-0.00082	0.00490			
			18.68100	-0.01068	0.01998	-0.01863	0.00029	0.00631			

Table V CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
1.2	K1	15/0	-1.11200	-0.02862	-0.00872	0.01759	-0.00490	-0.00400	PWT 4T	188	269
			1.25900	-0.04290	-0.00436	0.01529	-0.00830	-0.00360			
			3.61300	-0.05646	0.00106	0.00950	-0.01074	-0.00248			
			5.95700	-0.06974	0.00667	0.00160	-0.01181	-0.00052			
			8.43800	-0.05907	0.00234	-0.00429	-0.00990	0.00120			
			10.68000	-0.05639	0.00272	-0.01176	-0.00841	0.00269			
			13.03600	-0.05270	0.00676	-0.01864	-0.00732	0.00477			
			15.33900	-0.05036	0.00811	-0.02434	-0.00520	0.00600			
			17.56699	-0.03932	0.00175	-0.02717	-0.00343	0.00670			
			19.81799	-0.04257	0.01782	-0.03318	-0.00208	0.00708			
			22.02499	-0.02993	0.01803	-0.03306	0.00119	0.00640			
1.2	K1	10/5	-1.19300	-0.03440	-0.01063	0.01677	-0.00159	-0.00170	PWT 4T	258	269
			1.18500	-0.04270	-0.01265	0.01295	-0.00212	-0.00161			
			3.54400	-0.04639	-0.01366	0.00678	-0.00295	-0.00127			
			6.02800	-0.04785	-0.00993	-0.00021	-0.00371	-0.00071			
			8.40200	-0.04213	-0.00851	-0.00622	-0.00300	-0.00020			
			10.78200	-0.03826	-0.00661	-0.01303	-0.00331	0.00049			
			13.10300	-0.02504	-0.01275	-0.01724	-0.00291	0.00129			
			15.28000	-0.01395	-0.01930	-0.01941	-0.00240	0.00120			
			17.63199	-0.00253	-0.02517	-0.01977	-0.00182	0.00170			
			21.56399	0.00743	-0.01215	-0.02266	-0.00103	0.00210			

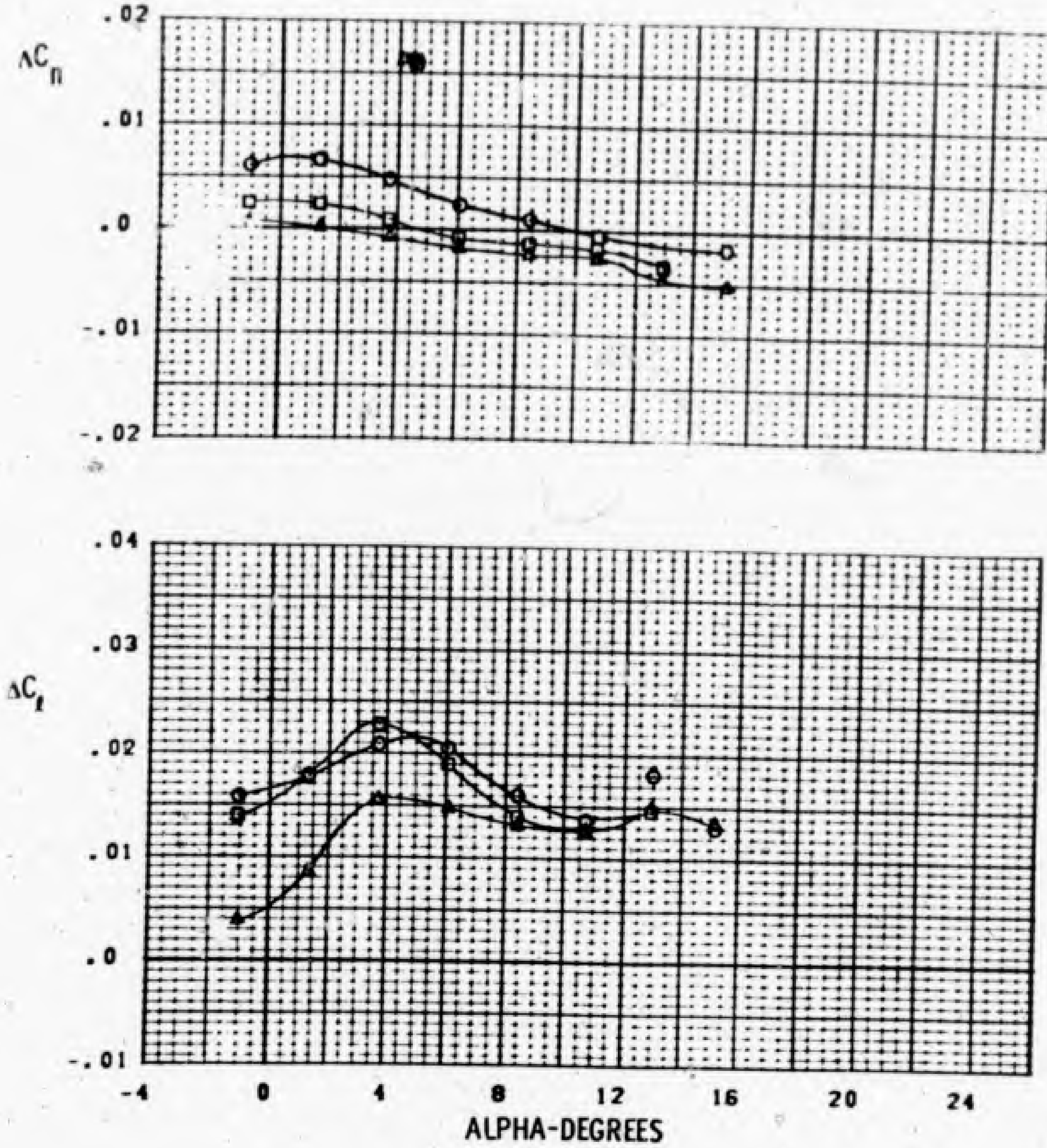
2. AILERONS

Characteristics for several specific effects associated with aileron type controls are given in this subsection. Data for the three basic span-wise locations, without horizontal tail, are presented in Figure 118. Similar characteristics for the mid-span and outboard ailerons, horizontal tail on, are given in Figure 119. Incremental differences due to the horizontal tail are given in Figures 120 and 121. The horizontal tail contributions to longitudinal characteristics illustrate the angle of attack ranges when the wing wake is near the horizontal tail.

The effects of Reynolds number variations over the attainable test range are illustrated in Figure 122. In this case, comparisons are shown for the basic lateral-directional moment measurements (not the incremental moment differences from the corresponding symmetrical configurations).

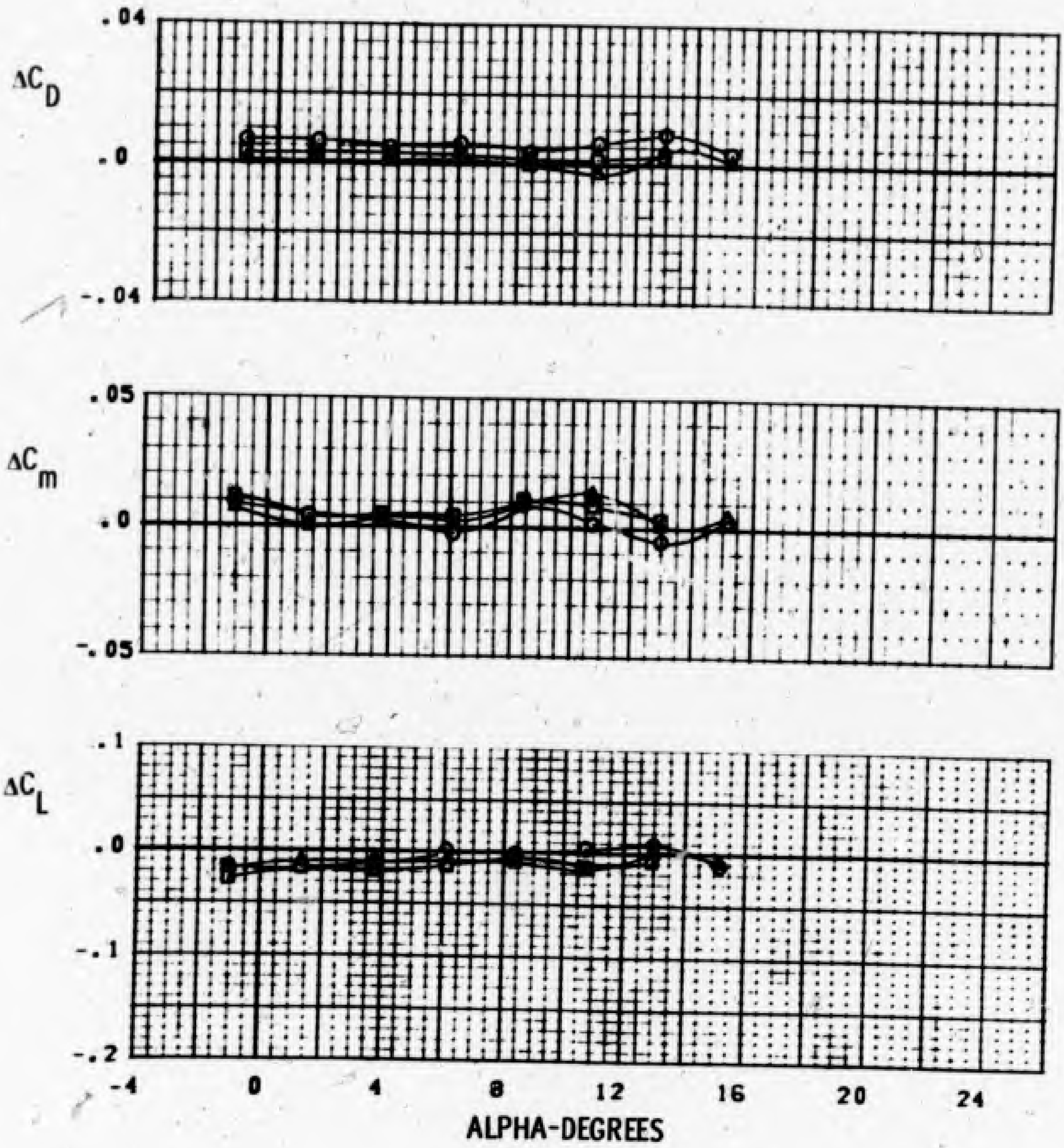
Comparisons of the effects on lateral-directional moments of various symmetrical leading edge flap deflections are presented in Figure 123. Comparable data with the K1 and K2 leading edge geometries are given in Figure 124. Characteristics obtained with both small and large deflections are shown in Figures 125 and 126 to illustrate the extent of linearity with deflection.

Numerical force and moment increments for key aileron effects are also given in Tables VI through X. This data is presented at the end of this subsection.



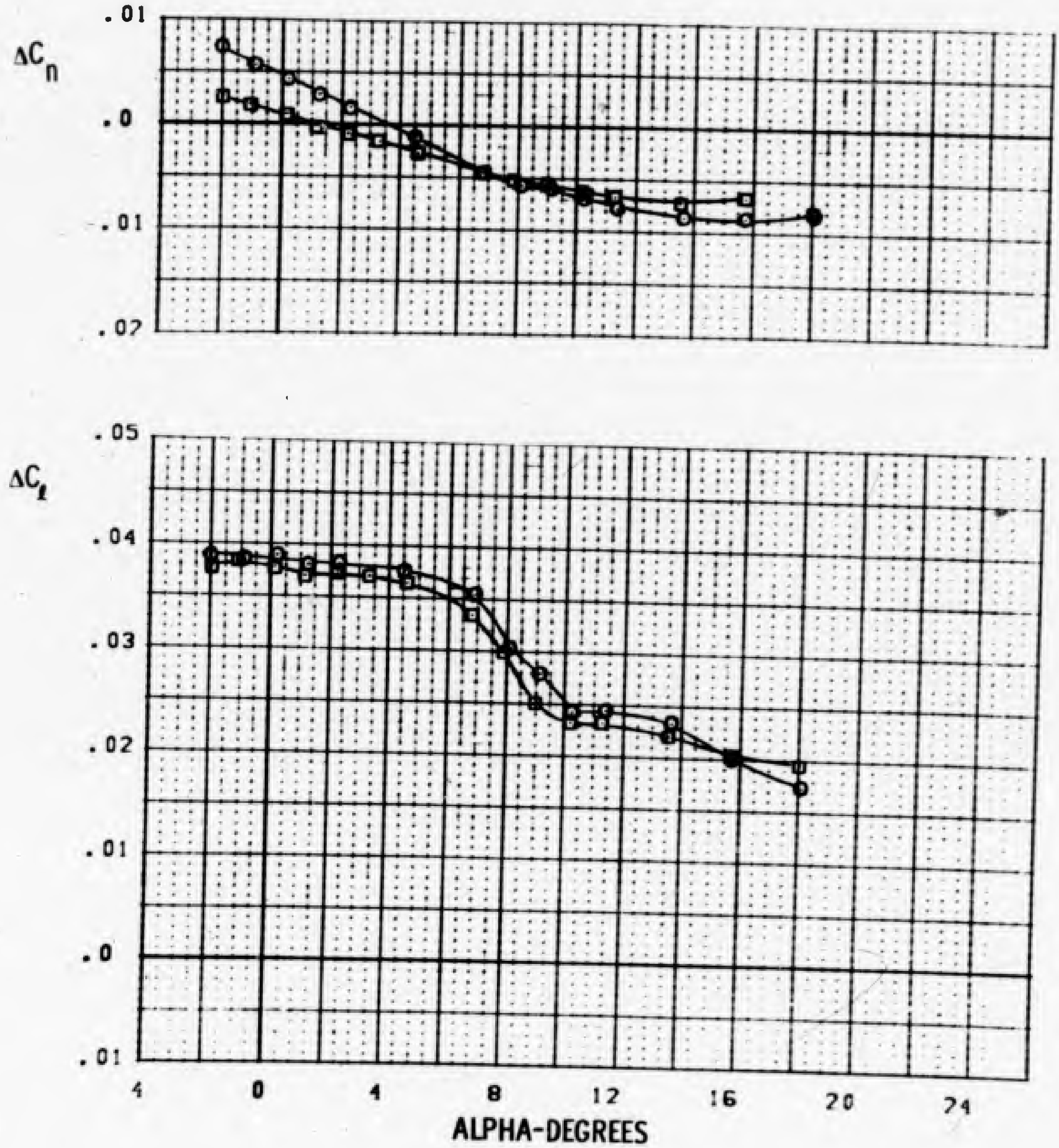
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 112 -PN 47	K1	10/10	INBD	10/-10
□	PWT 4T TC-043	PN 108 -PN 47	K1	10/10	MID	10/-10
▲	PWT 4T TC-043	PN 104 -PN 47	K1	10/10	OUTBD	10/-10

FIGURE 118 AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL OFF M = 0.9



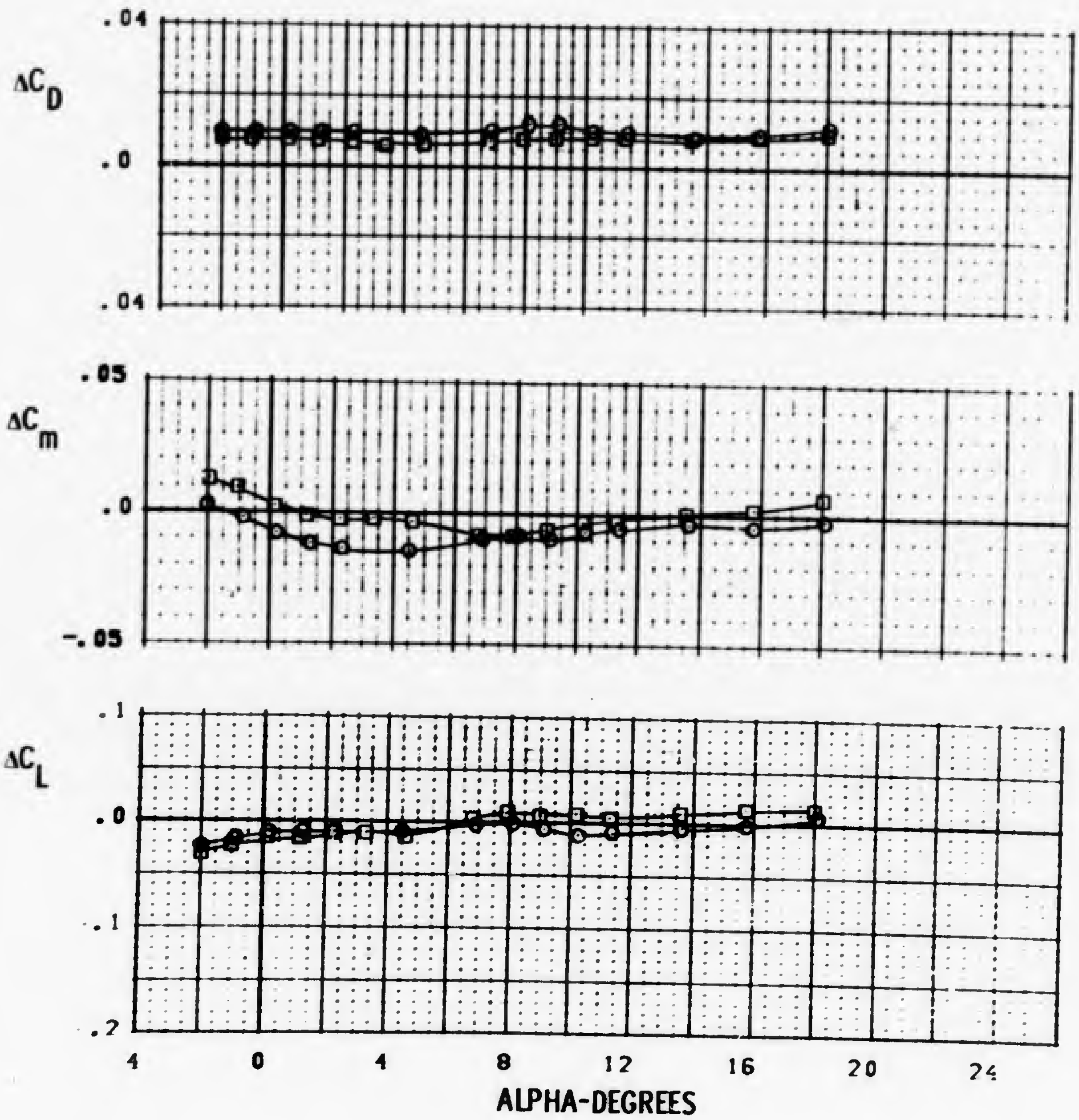
SYM	TEST	INCREMENT	L.E (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 112 -PN 47	K1	10/10	INBD	10/-10
⊡	PWT 4T TC-043	PN 108 -PN 47	K1	10/10	MID	10/-10
▲	PWT 4T TC-043	PN 104 -PN 47	K1	10/10	OUTBD	10/-10

FIGURE 118 AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL OFF M = 0.9



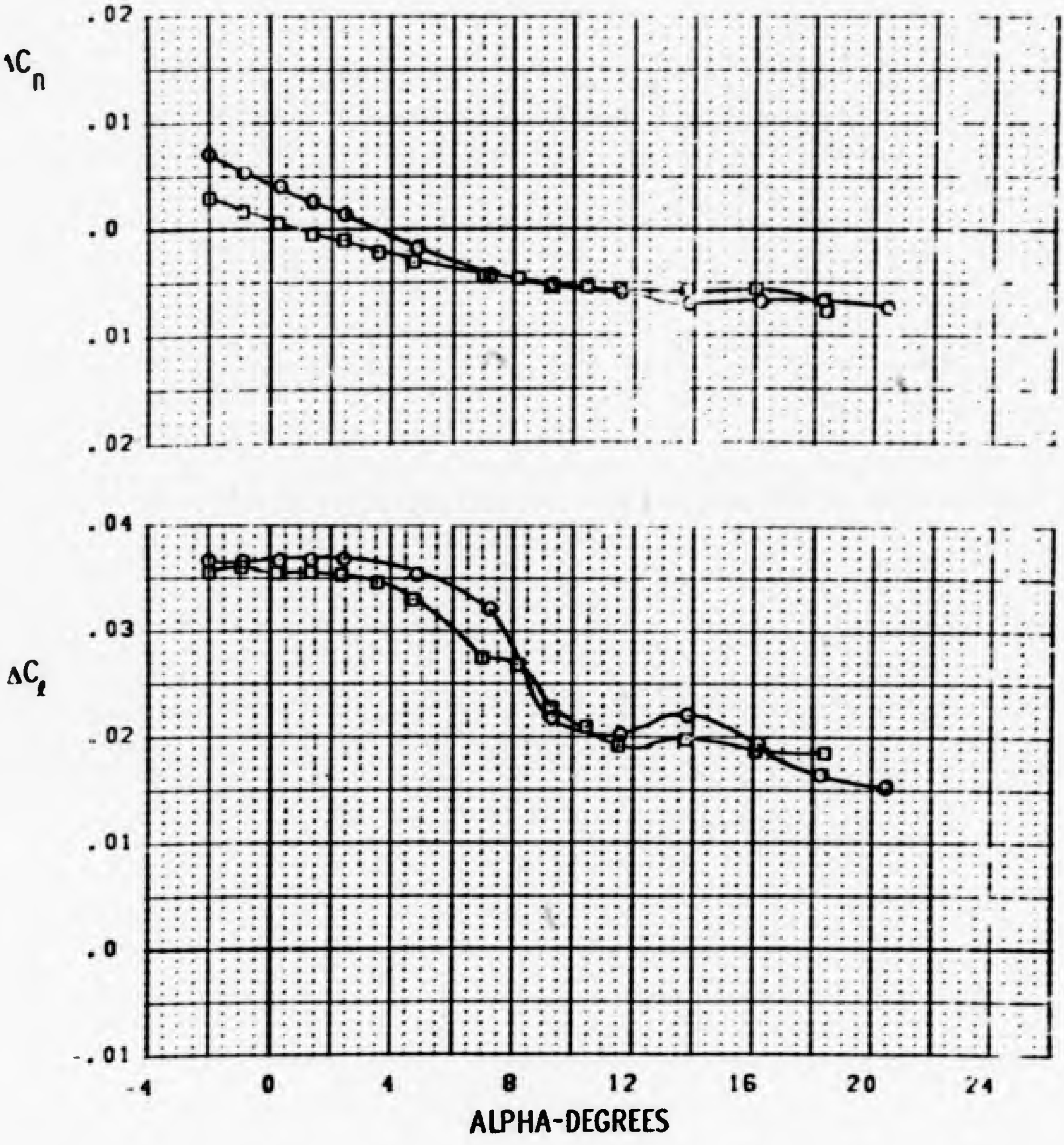
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)		
⊙	PWT 16T TF-216	PN 13 - PN 49	KI	0/0	MID	[illegible]	[illegible]
⊡	PWT 16T TF-216	PN 85 - PN 49	KI	0/0	OUTBD	[illegible]	[illegible]

FIGURE 119a AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.7



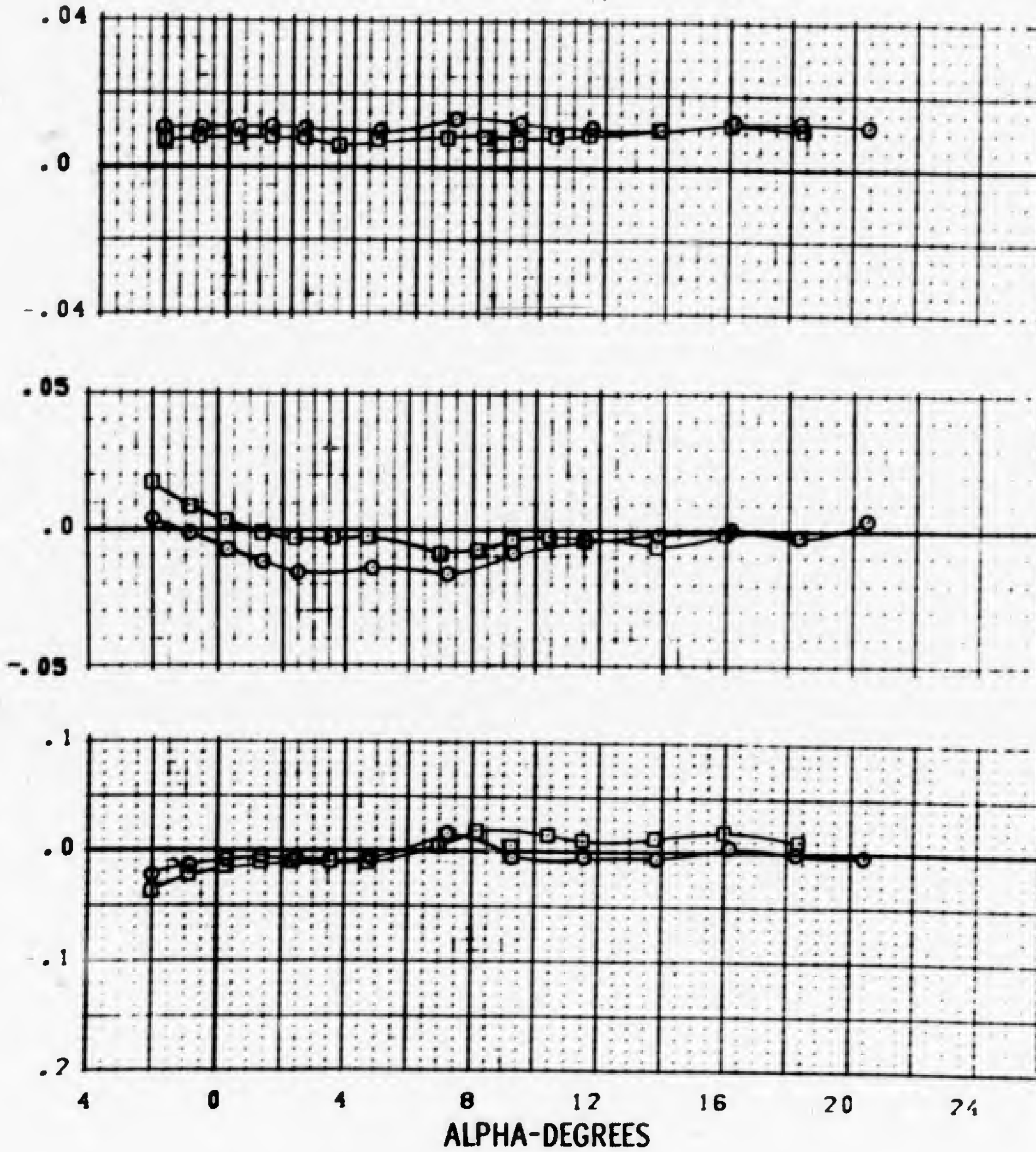
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 16T TF-216	PN 13 - PN 49	[illegible] 0/0	[illegible]
⊡	PWT 16T TF 216	PN 85 - PN 49	[illegible] 0/0	[illegible]

FIGURE 119a AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.7



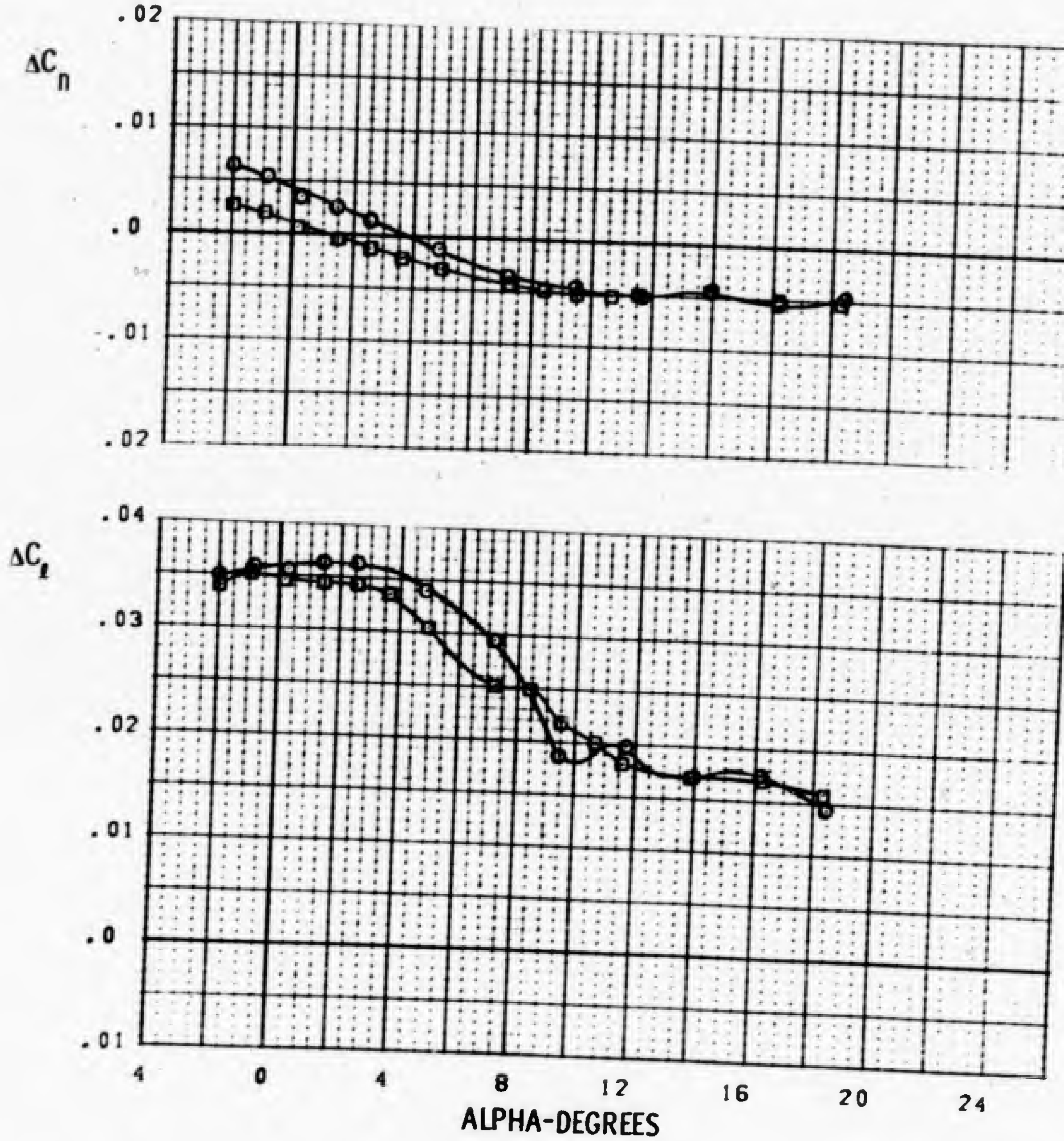
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 16T TF-216	PN 12 -PN 50	K1	0/0	MID	20/-20
□	PWT 16T TF-216	PN 84 -PN 50	K1	0/0	OUTBD	20/-20

FIGURE 119b AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.8



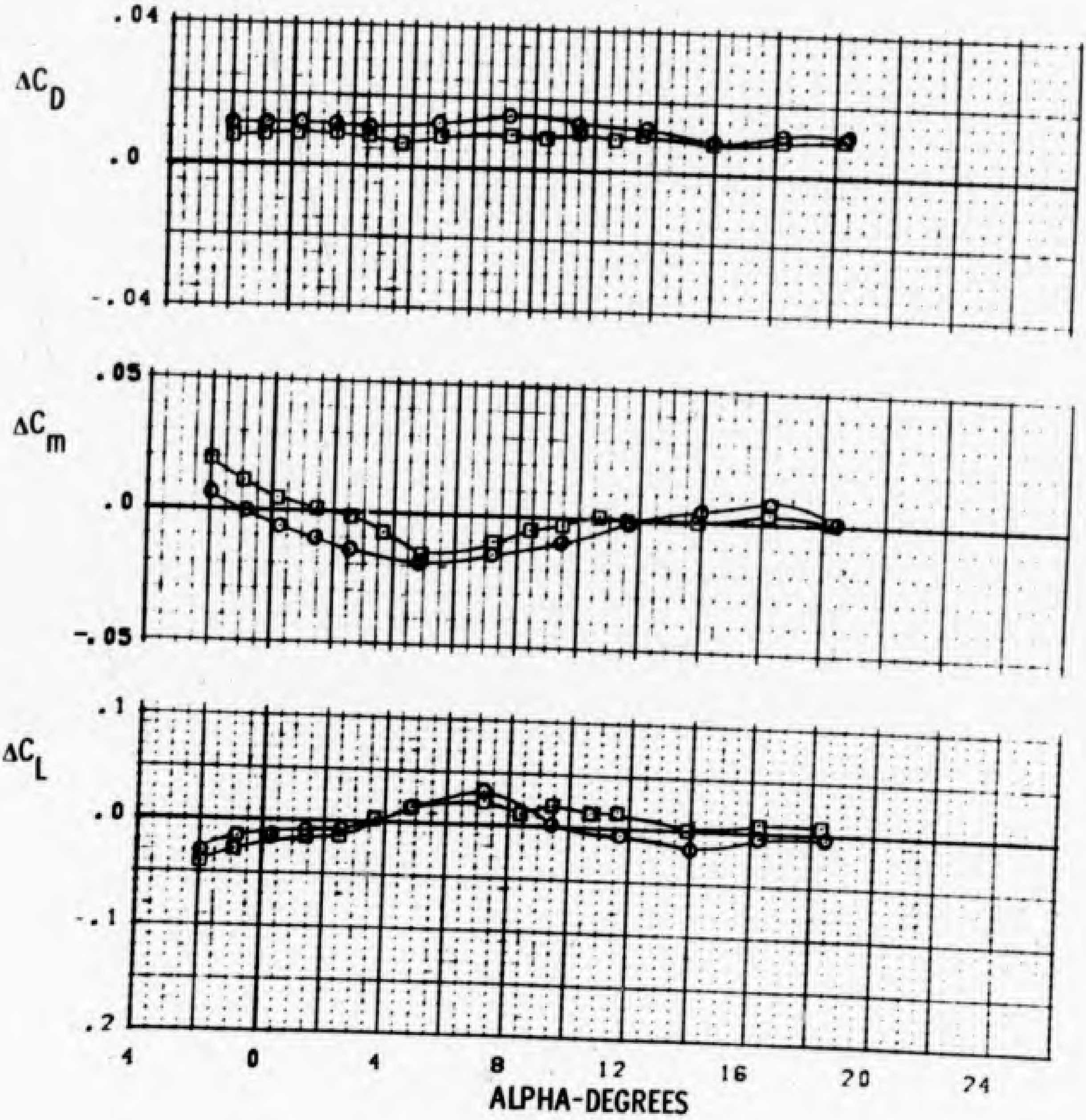
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 12 -PN 50	K1	0/0	MID	20/-20
⊡	PWT 16T TF-216	PN 84 -PN 50	K1	0/0	OUTBD	20/-20

FIGURE 119b AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.8



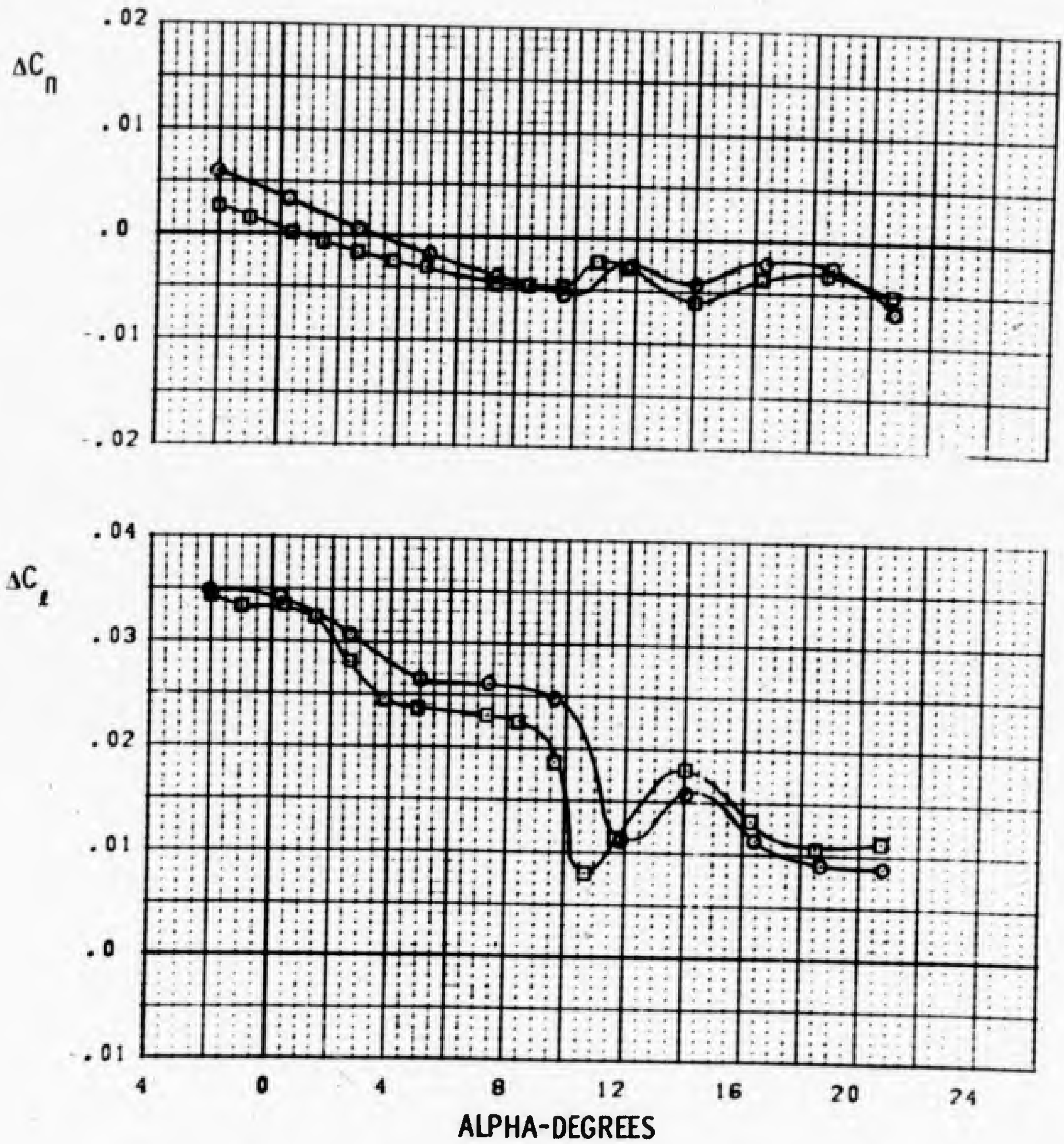
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 11 -PN 51	K1	0/0	MID	20/20
⊡	PWT 16T TF-216	PN 83 -PN 51	K1	0/0	OUTBD	20/20

FIGURE 119c AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.85



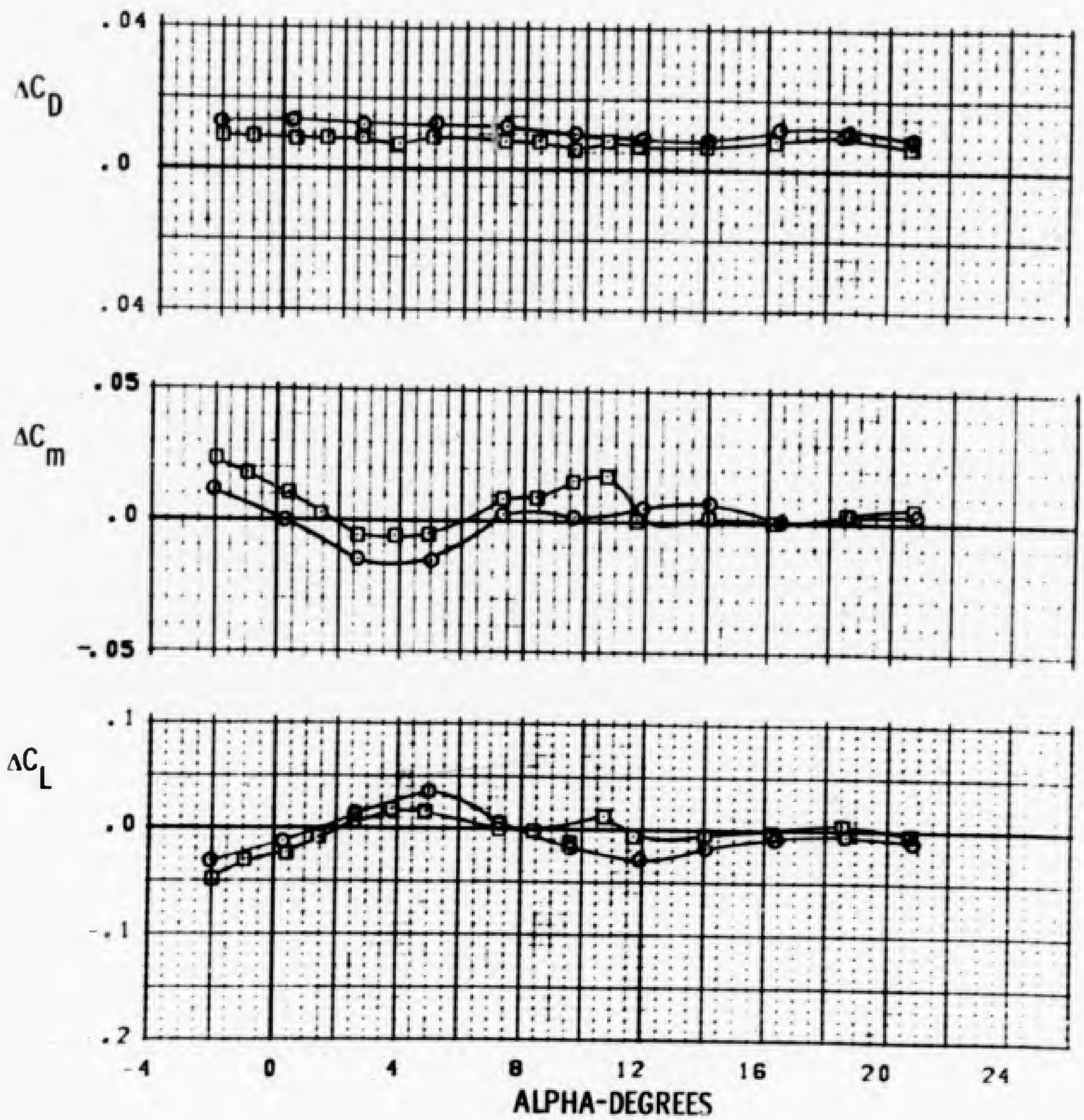
SYM.	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 11 -PN 51	KI	0/0	MID	20/20
⊡	PWT 16T FF 216	PN 83 -PN 51	KI	0/0	OUTBD	20/20

FIGURE 119c AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.85



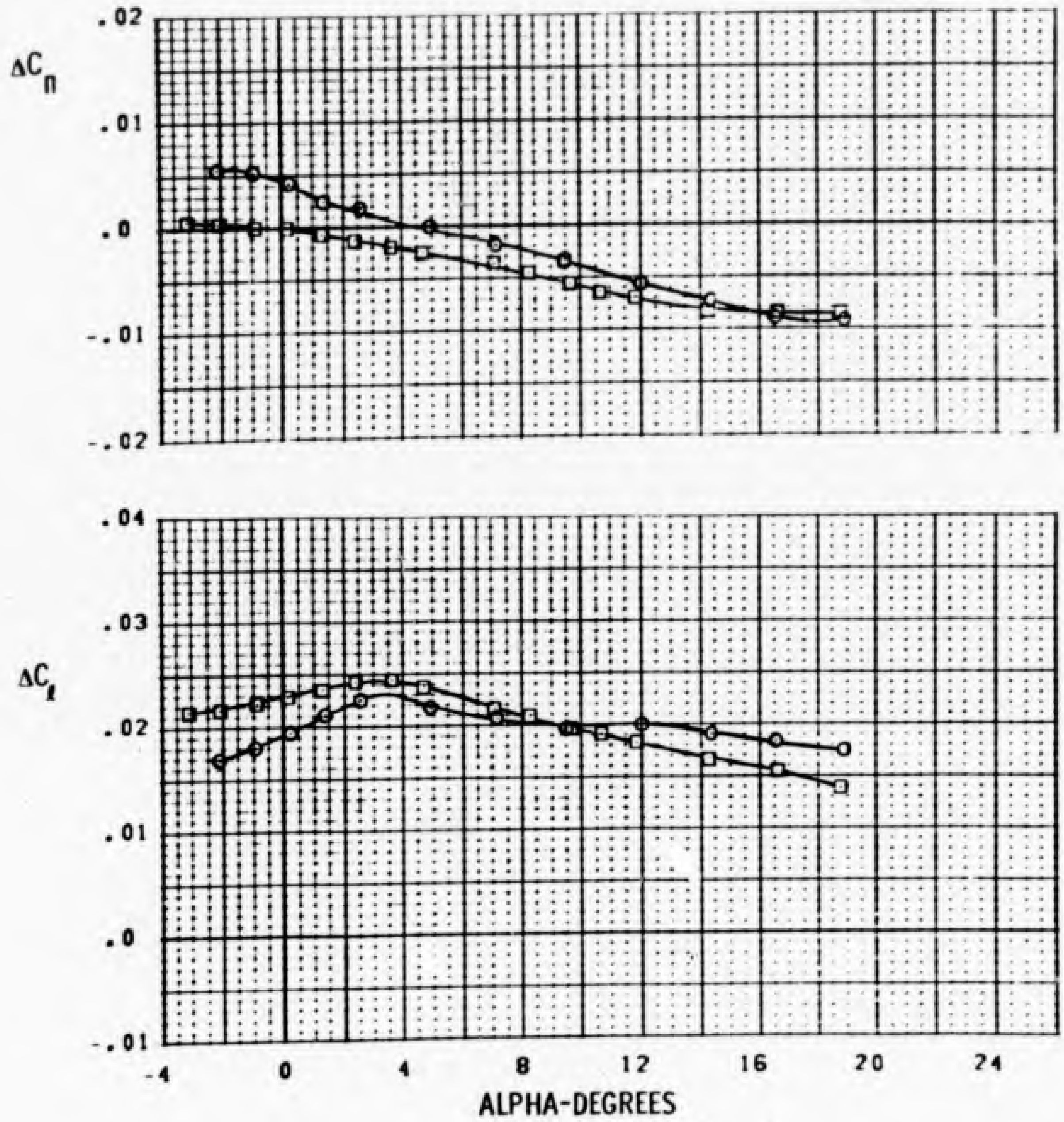
SYM	TEST	INCREMENT	L.E. (_/R)		AILERON (_/R)	
⊙	PWT 16T TF-216	PN 8 -PN 52	K1	0/0	MID	20/20
⊡	PWT 16T TF-216	PN 81 -PN 52	K1	0/0	OUTBD	20/20

FIGURE 119d AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.9



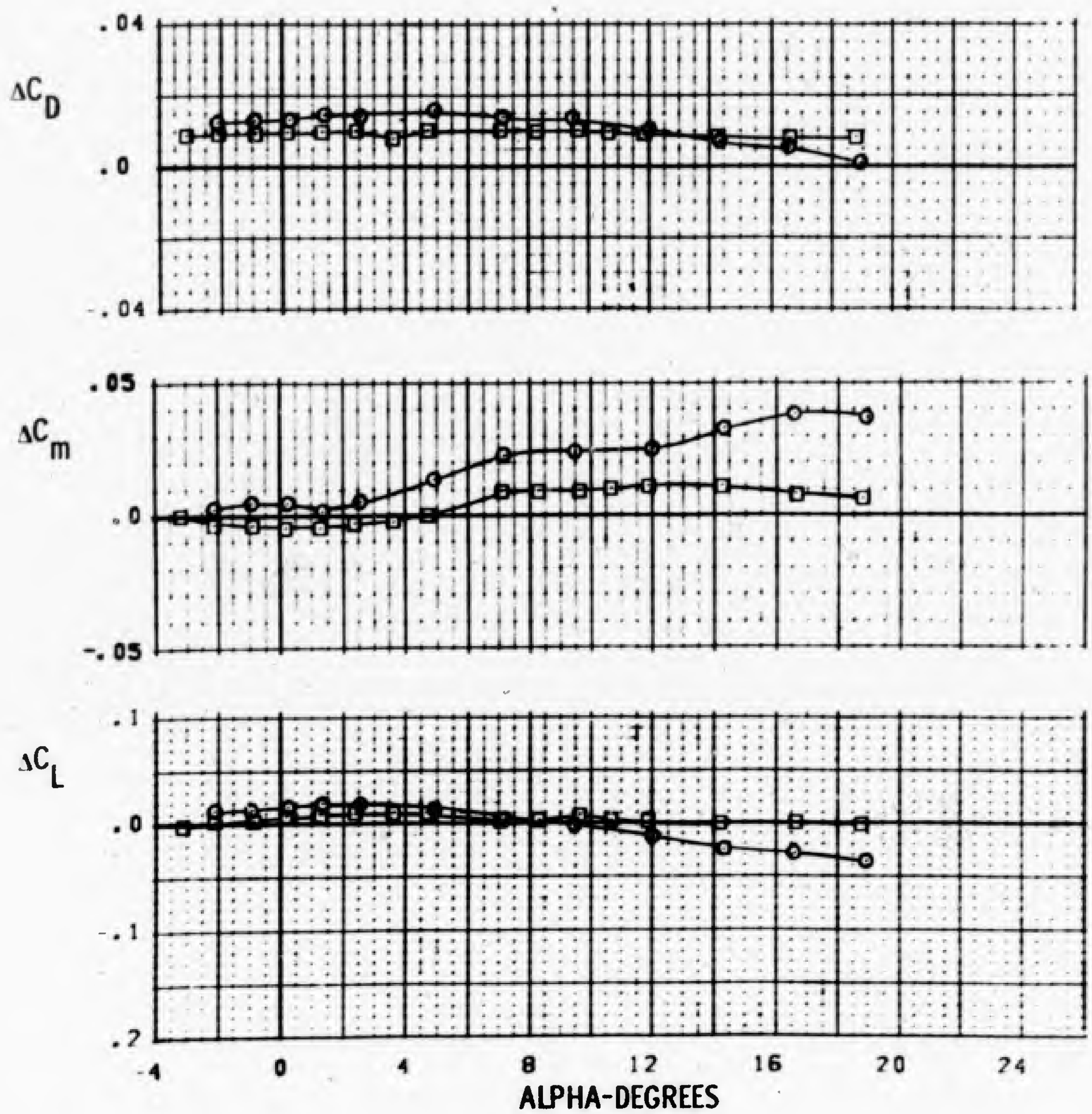
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 8 -PN 52	K1	0/0	MID	20/-20
⊡	PWT 16T TF-216	PN 81 -PN 52	K1	0/0	OUTBD	20/-20

FIGURE 119d AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 0.9



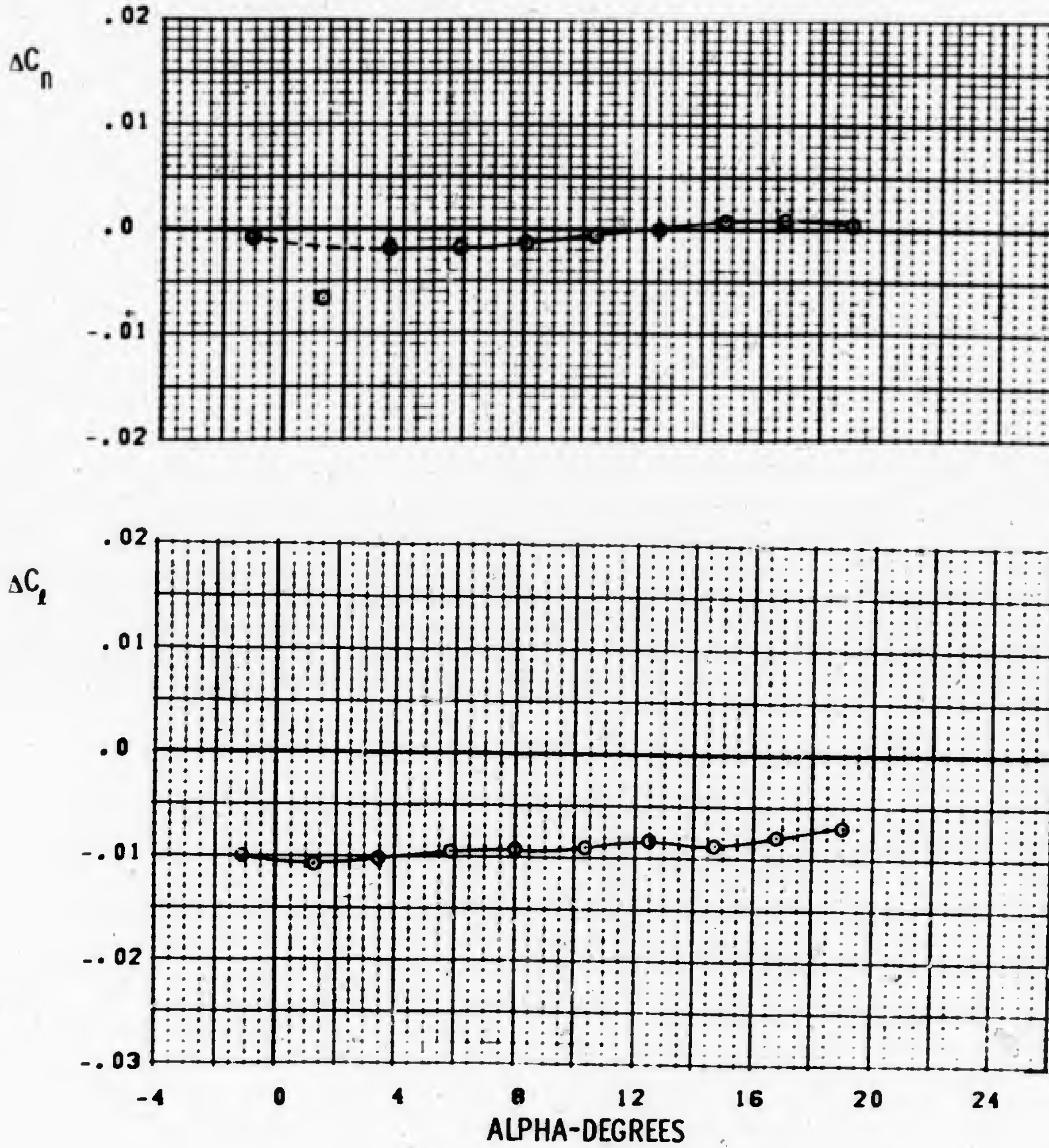
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 10 -PN 54	KI	0/0	MID	20/20
⊡	PWT 16T TF-216	PN 82 -PN 54	KI	0/0	OUTBD	20/20

FIGURE 119e AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON M = 1.2



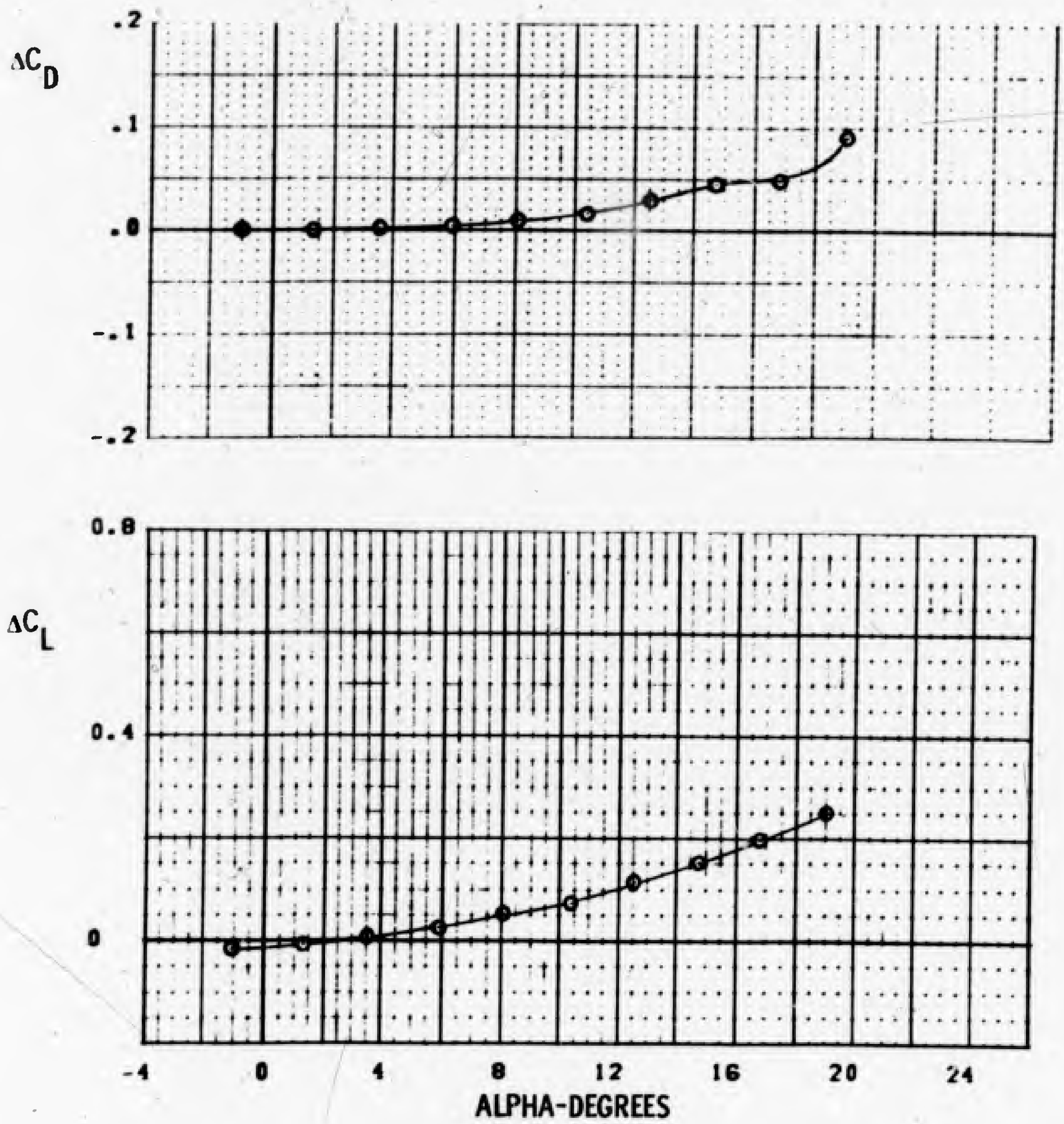
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON	(L/R)
⊙	PWT 16T TF-216	PN 10 -PN 54	K1	0/0	MID	20/-20
⊡	PWT 16T TF-216	PN 82 -PN 54	K1	0/0	OUTBD	20/-20

FIGURE 119e AILERON SPANWISE POSITION EFFECTS
HORIZONTAL TAIL ON $M = 1.2$



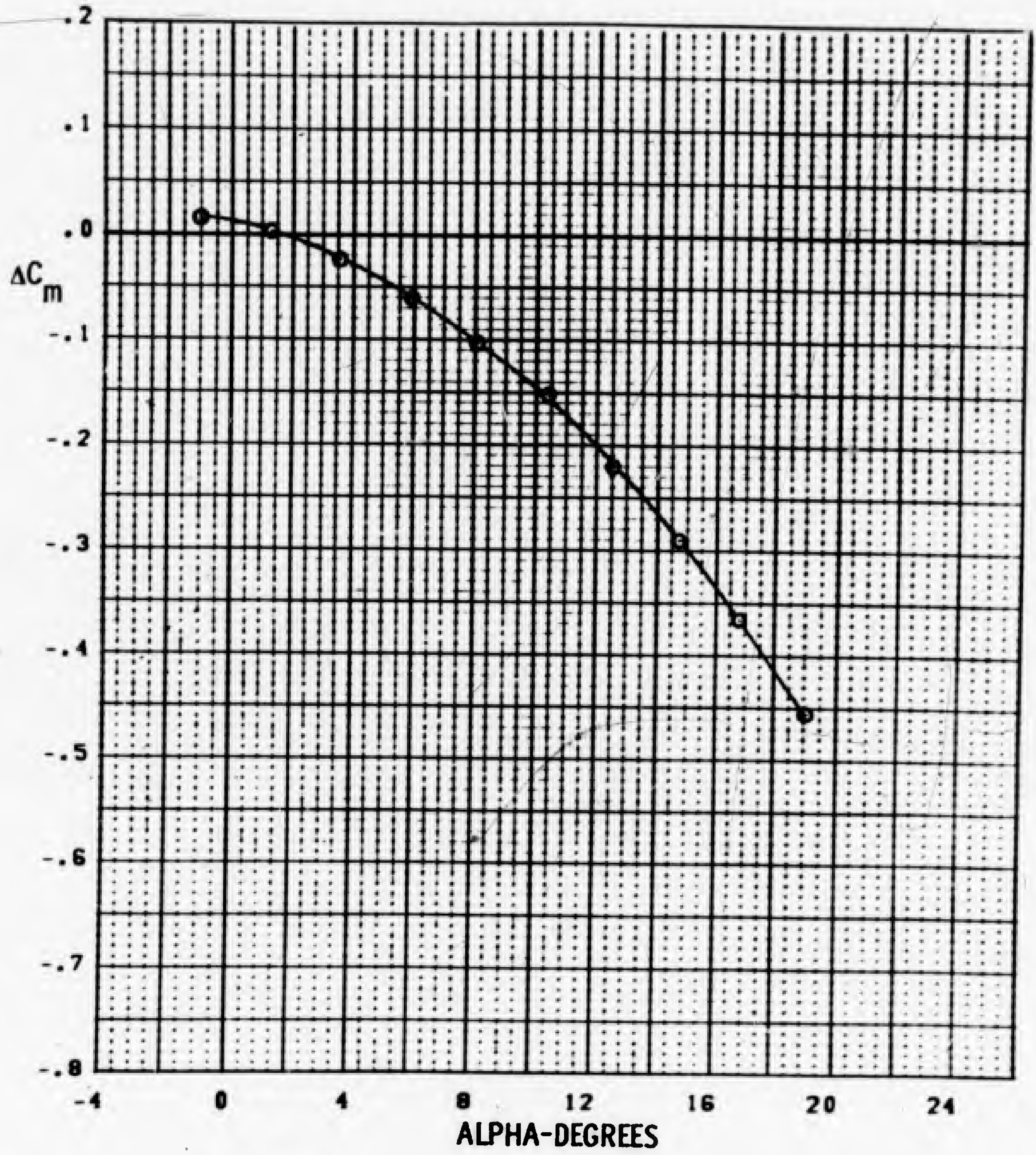
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 121 -PN 114	K1 10/10	INBD 10/-10

FIGURE 120a HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.7



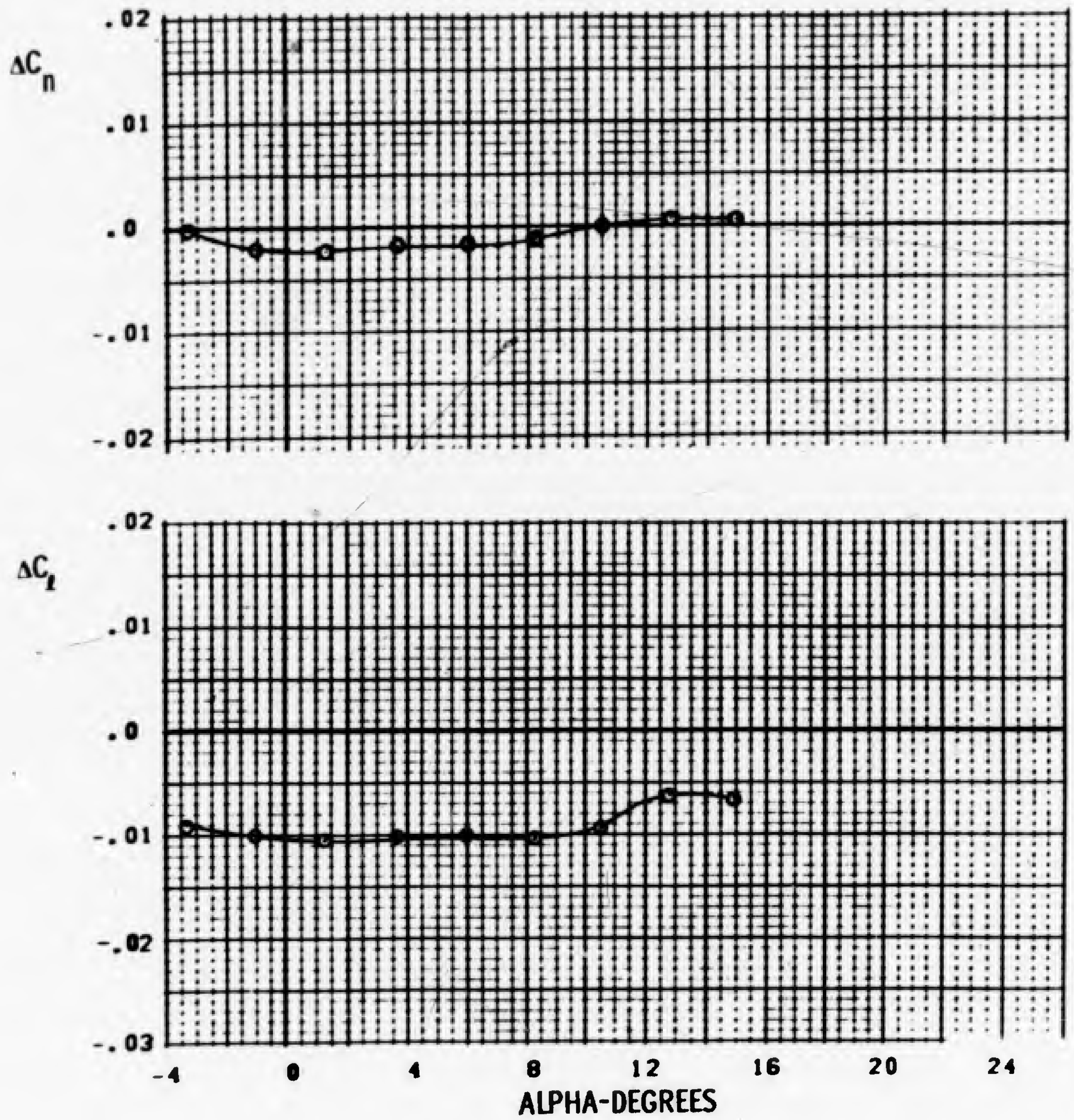
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
O	PWT 4T TC-043	PN 121 -PN 114	K1 10/10	INBD 10/-10

FIGURE 120a HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.7



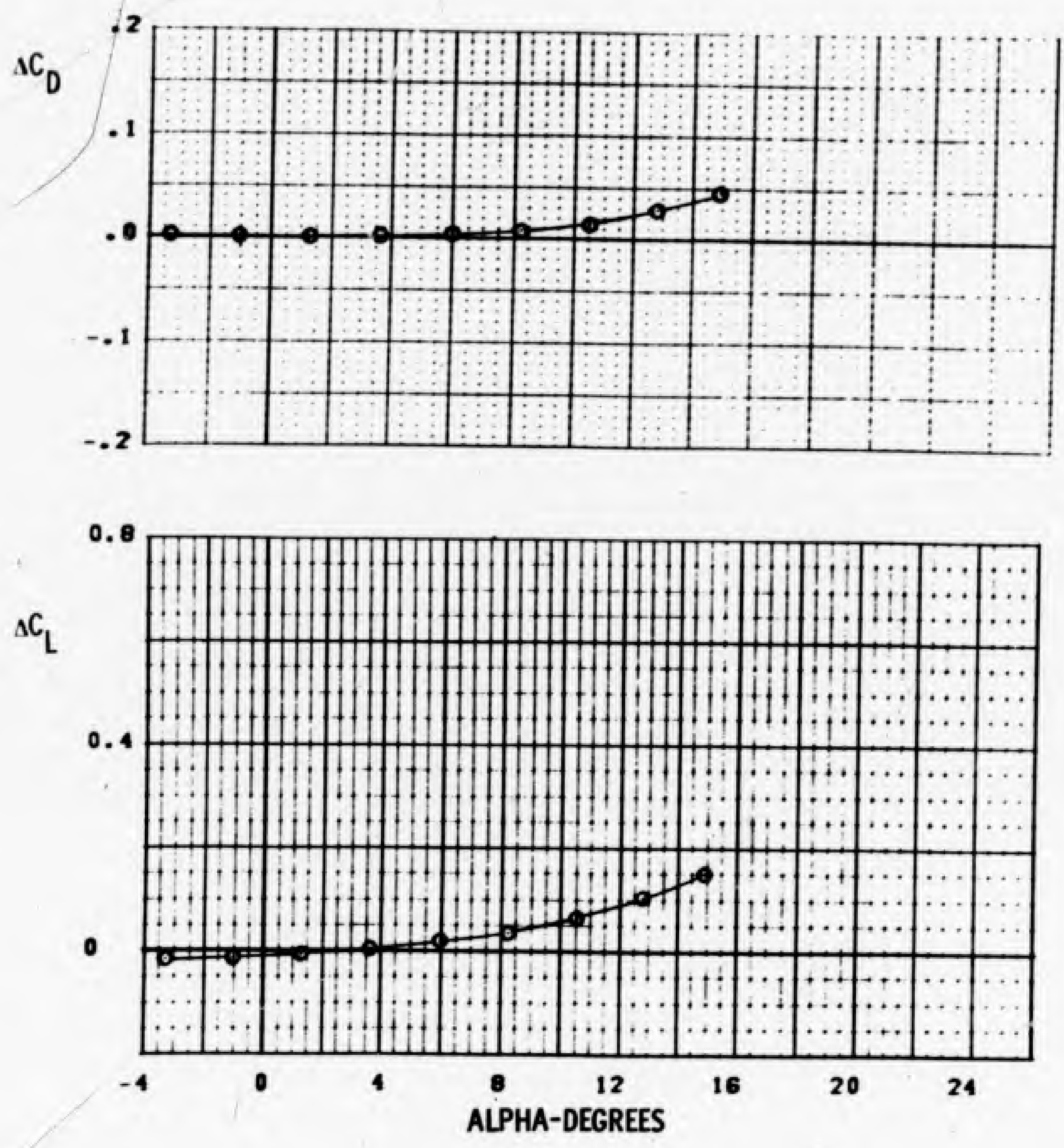
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 121 -PN 114	K1 10/10	INBD 10/-10

FIGURE 120a HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.7



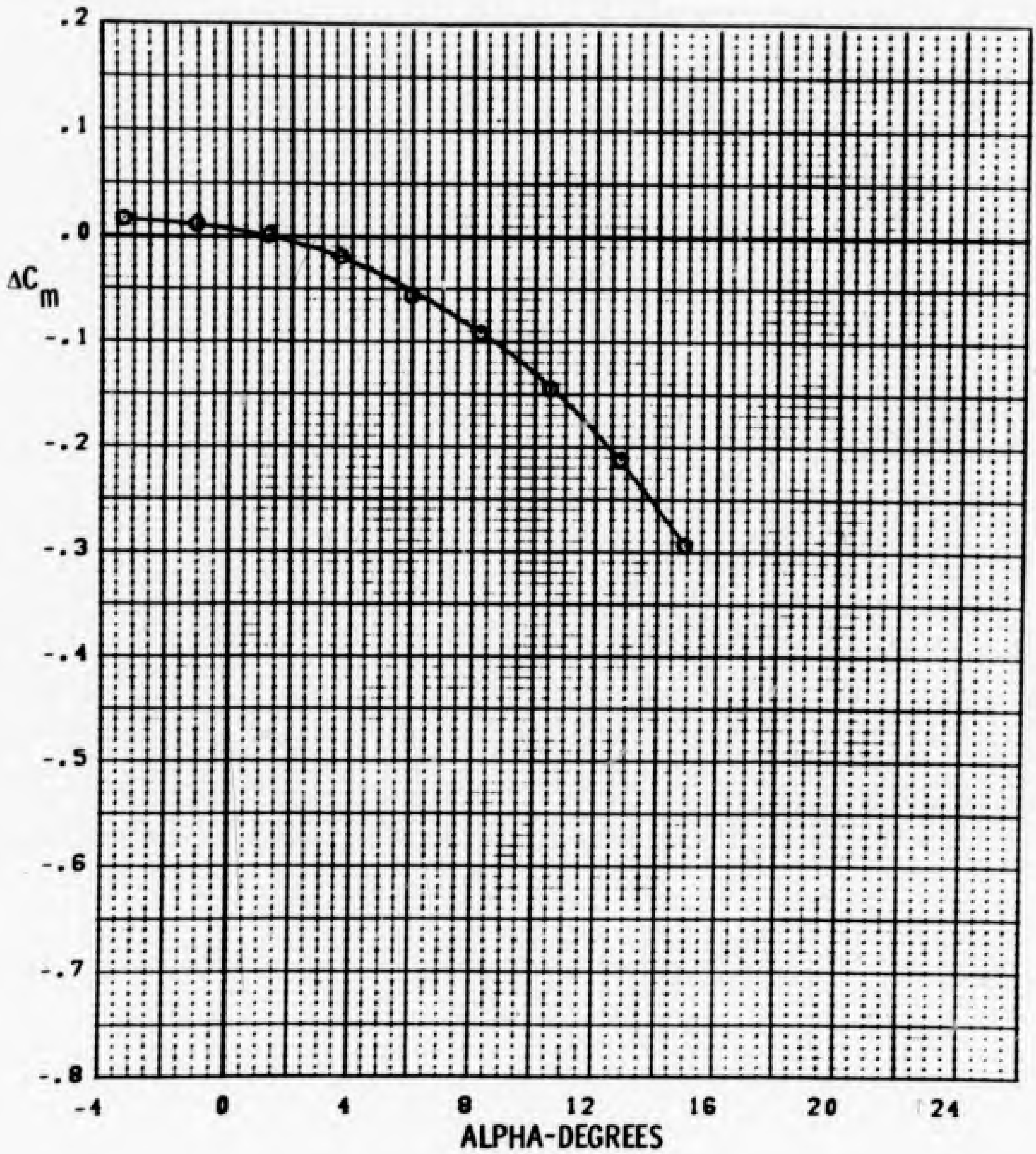
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 120 -PN 113	K1 10/10	INBD 10/-10

FIGURE 120b HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.8



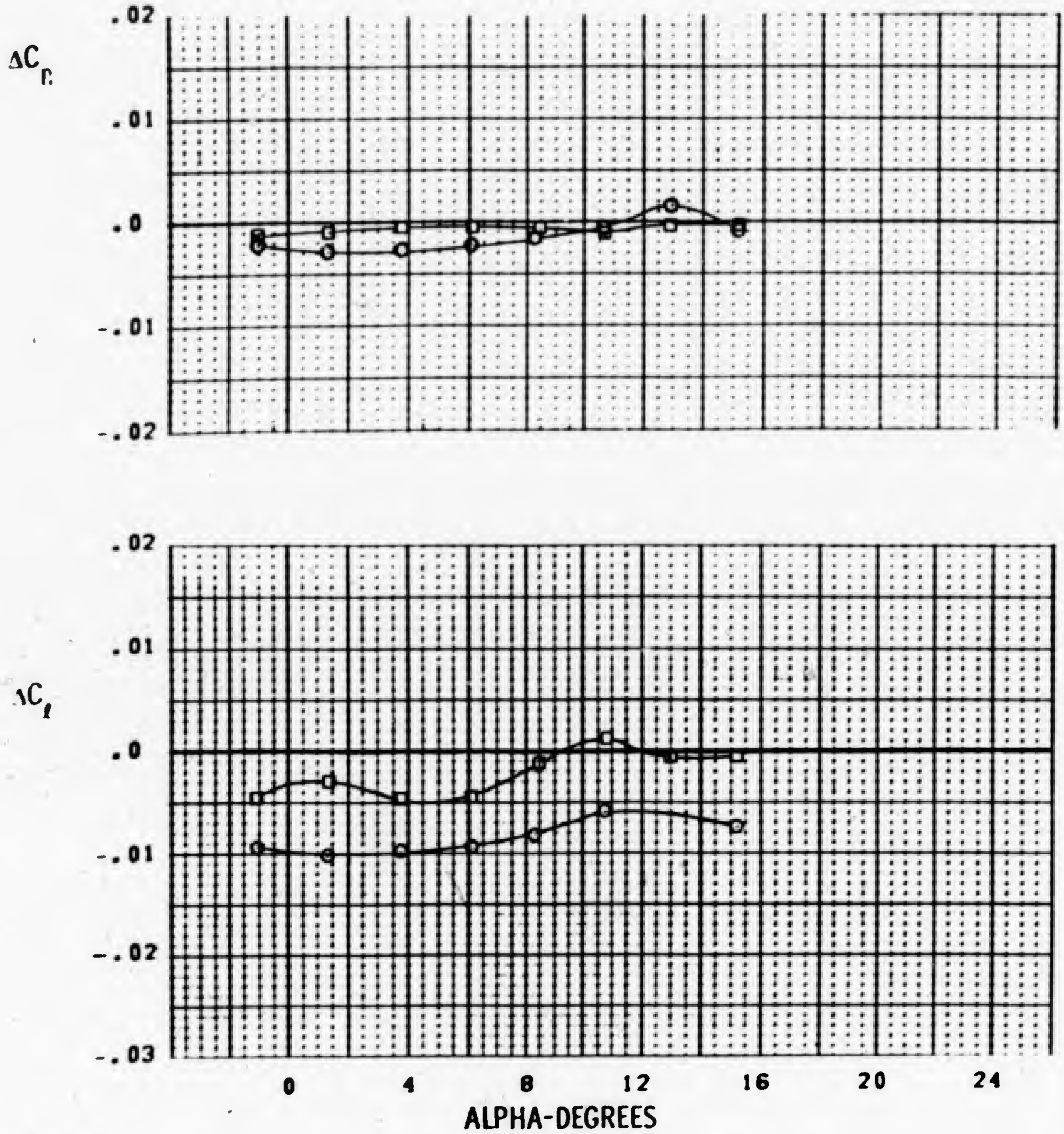
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 120 -PN 113	K1 10/10	INBD 10/-10

FIGURE 120b HORIZONTAL TAIL INTERFERENCE, RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.8



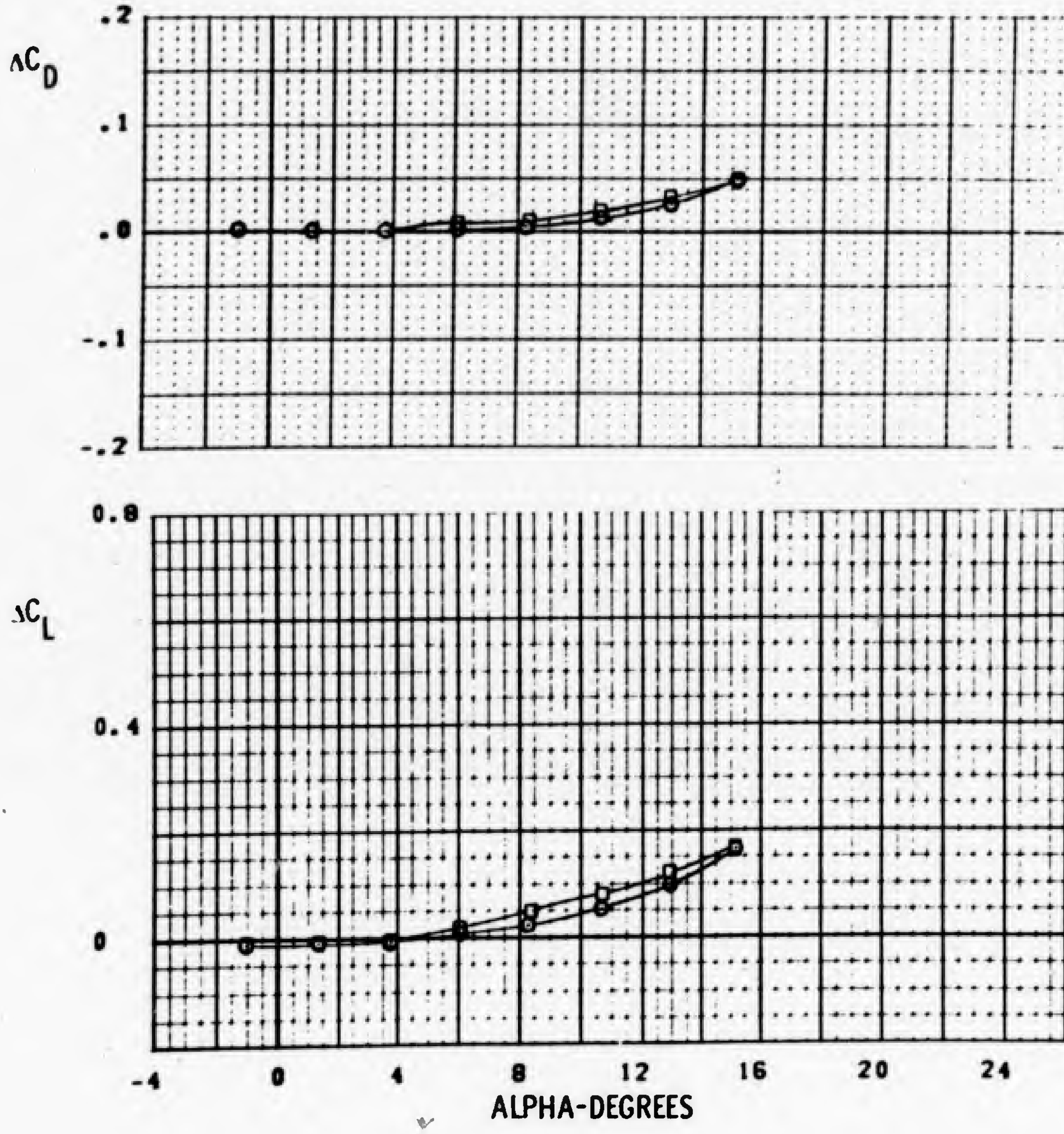
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 120 -PN 113	K1 10/10	INBD 10/-10

FIGURE 120b HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.8



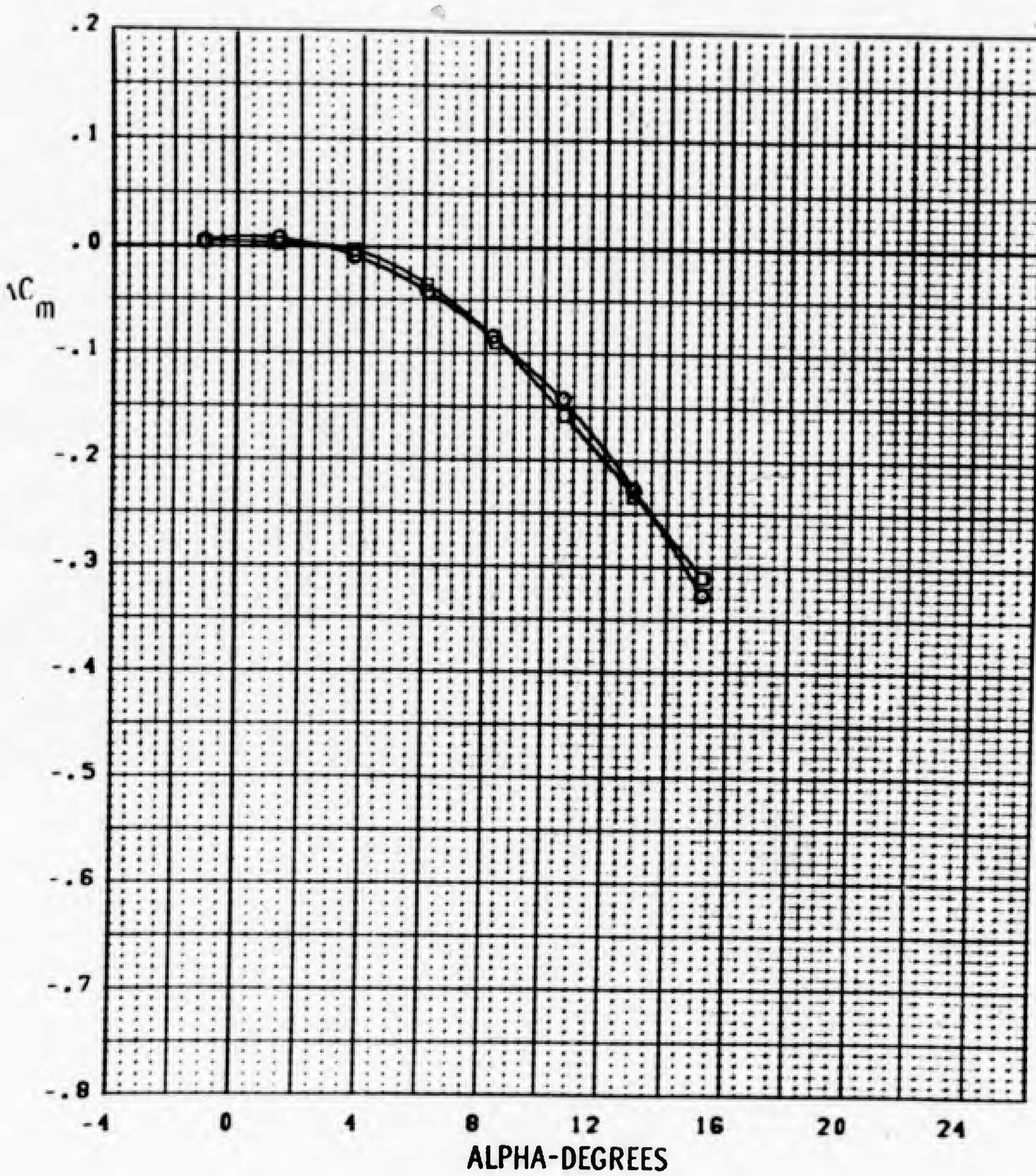
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 119 -PN 112	K1 10/10	INBO 10/-10
⊡	PWT 4T TC-043	PN 133 -PN 108	K1 10/10	MID 10/-10

FIGURE 120c HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION .
SMALL AILERON DEFLECTION M = 0.9



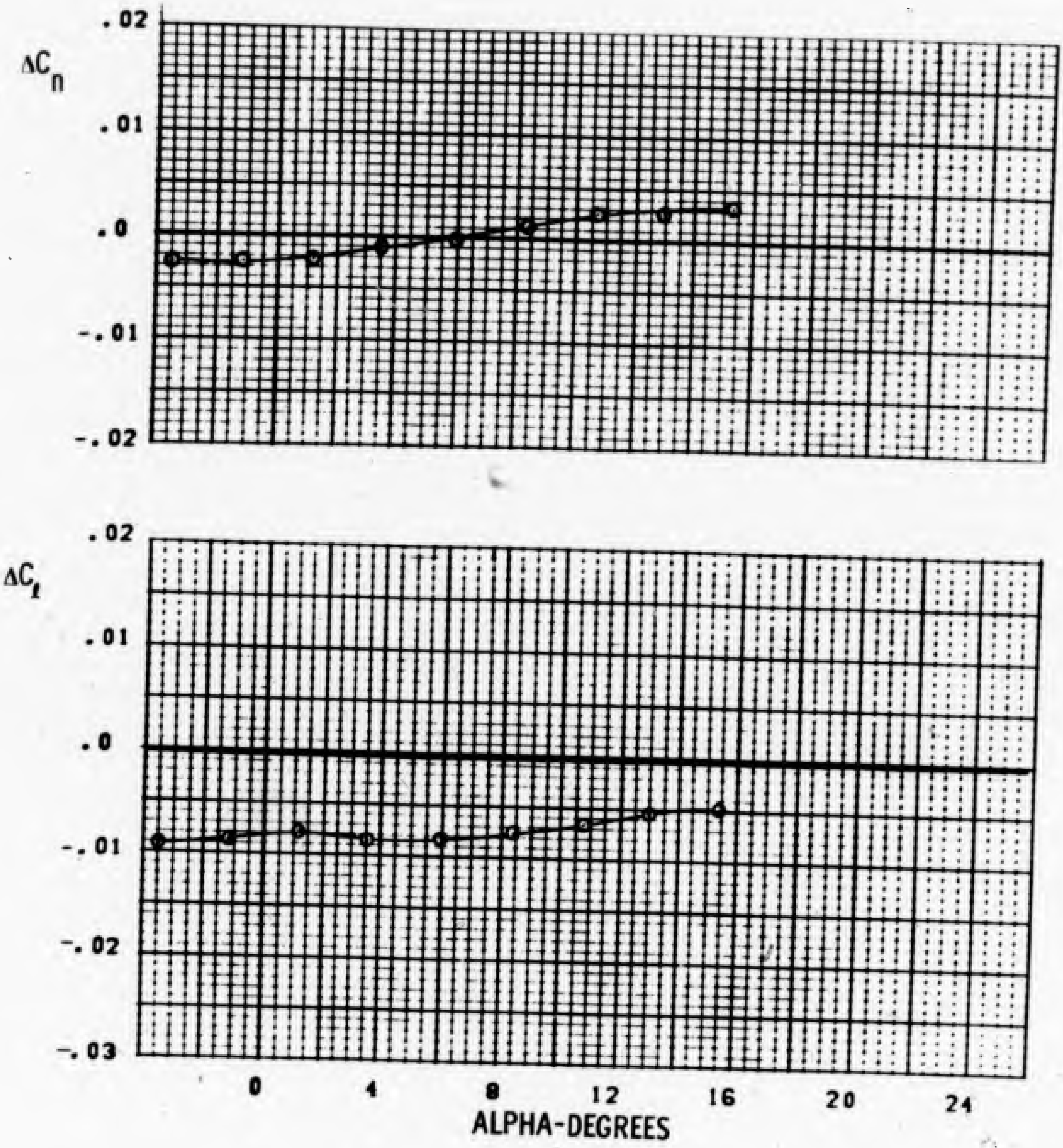
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 119 -PN 112	K1 10/10	INBO 10/-10
□	PWT 4T TC-043	PN 133 -PN 108	K1 10/10	MID 10/-10

FIGURE 120c HORIZONTAL TAIL INTERFERENCE, RN = 5.2 MILLION
SMALL AILERON DEFECTION; M = 0.9



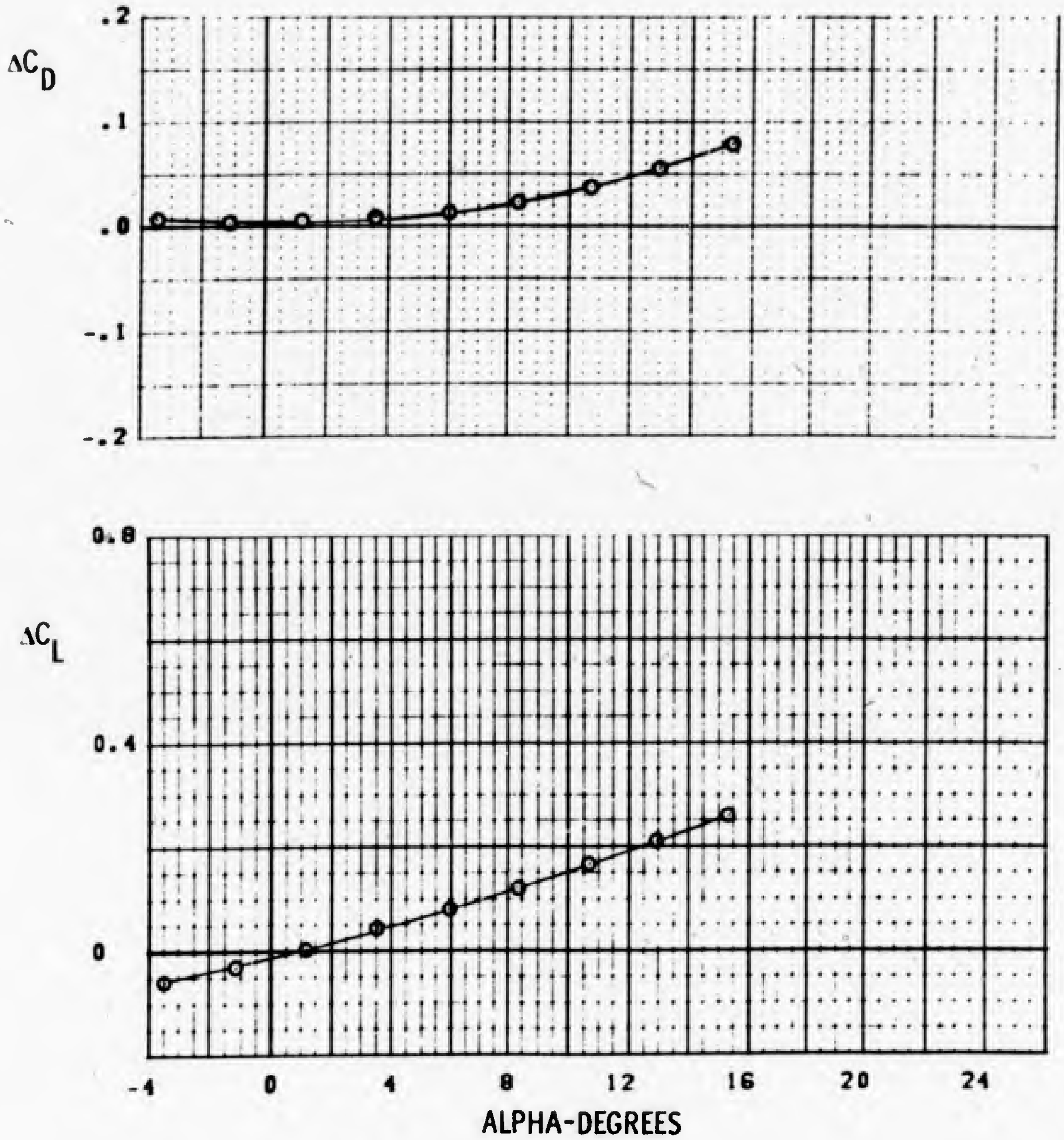
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 119 -PN 112	K1 10/10	INBD 10/-10
☐	PWT 4T TC-043	PN 133 -PN 108	K1 10/10	MID 10/-10

FIGURE 120c HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 0.9



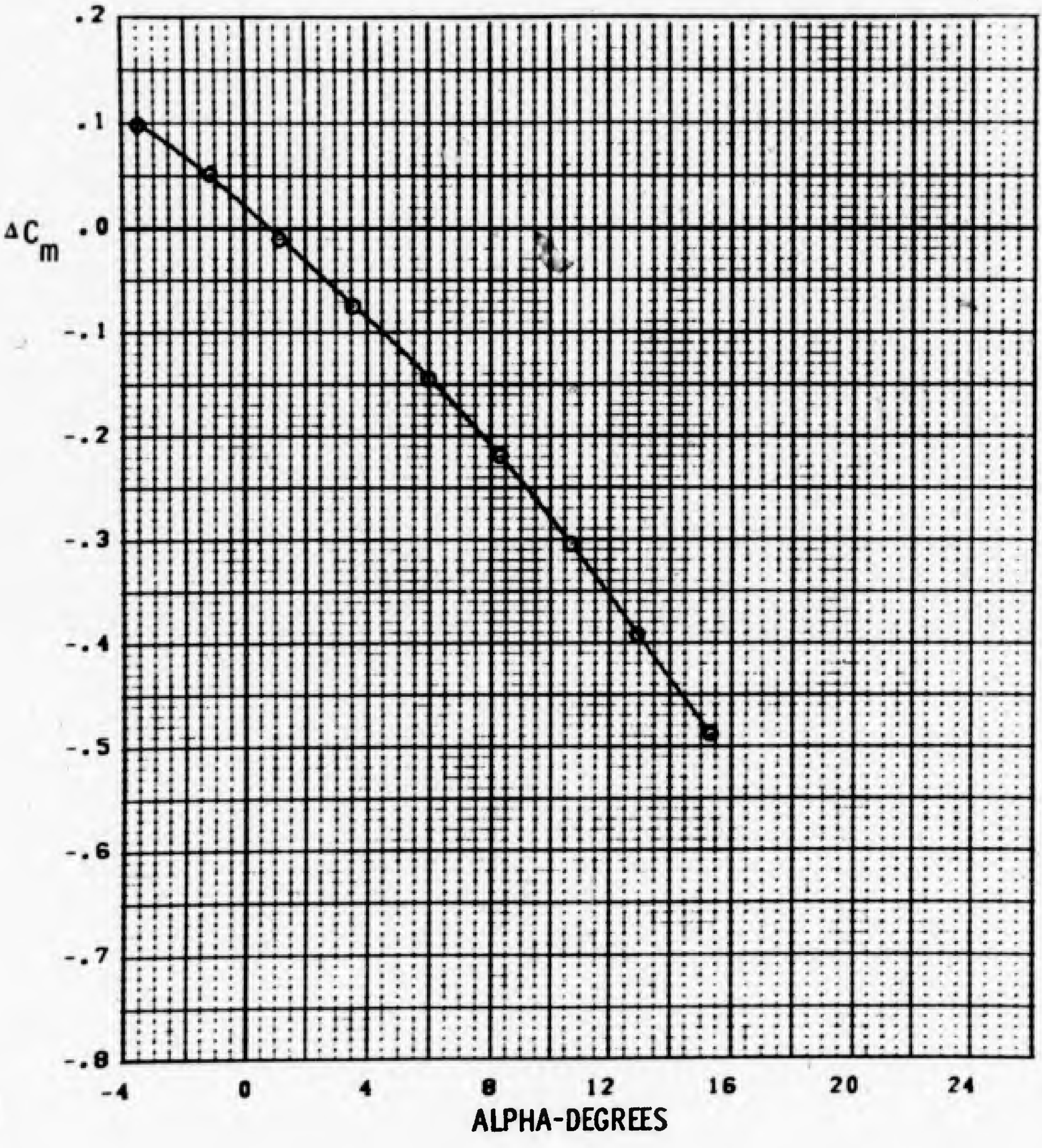
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 122 -PN 115	K1 10/10	INBD 10/-10

FIGURE 120d HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 1.2



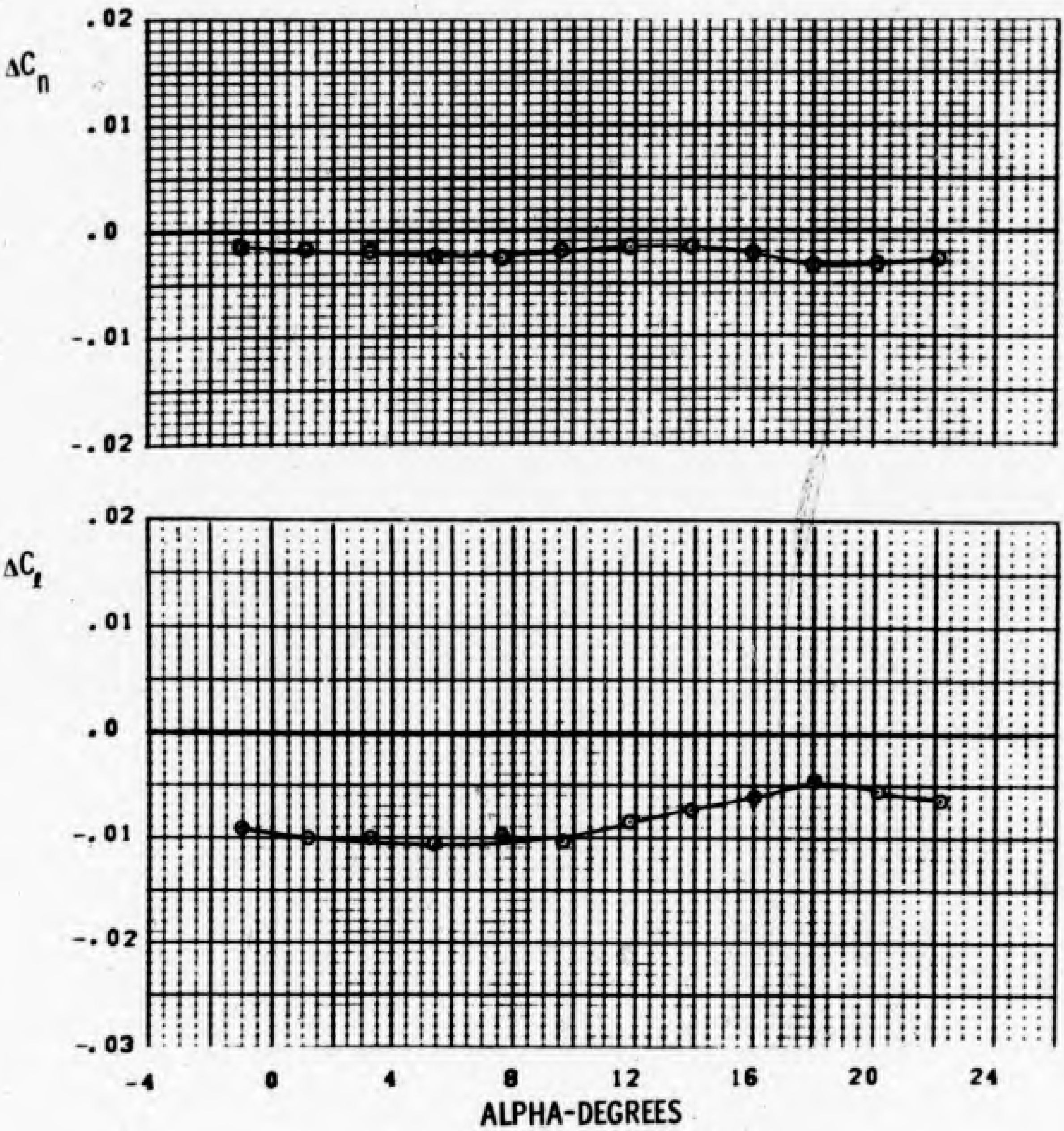
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 122 -PN 115	K1 10/10	INBD 10/-10

FIGURE 120d HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 1.2



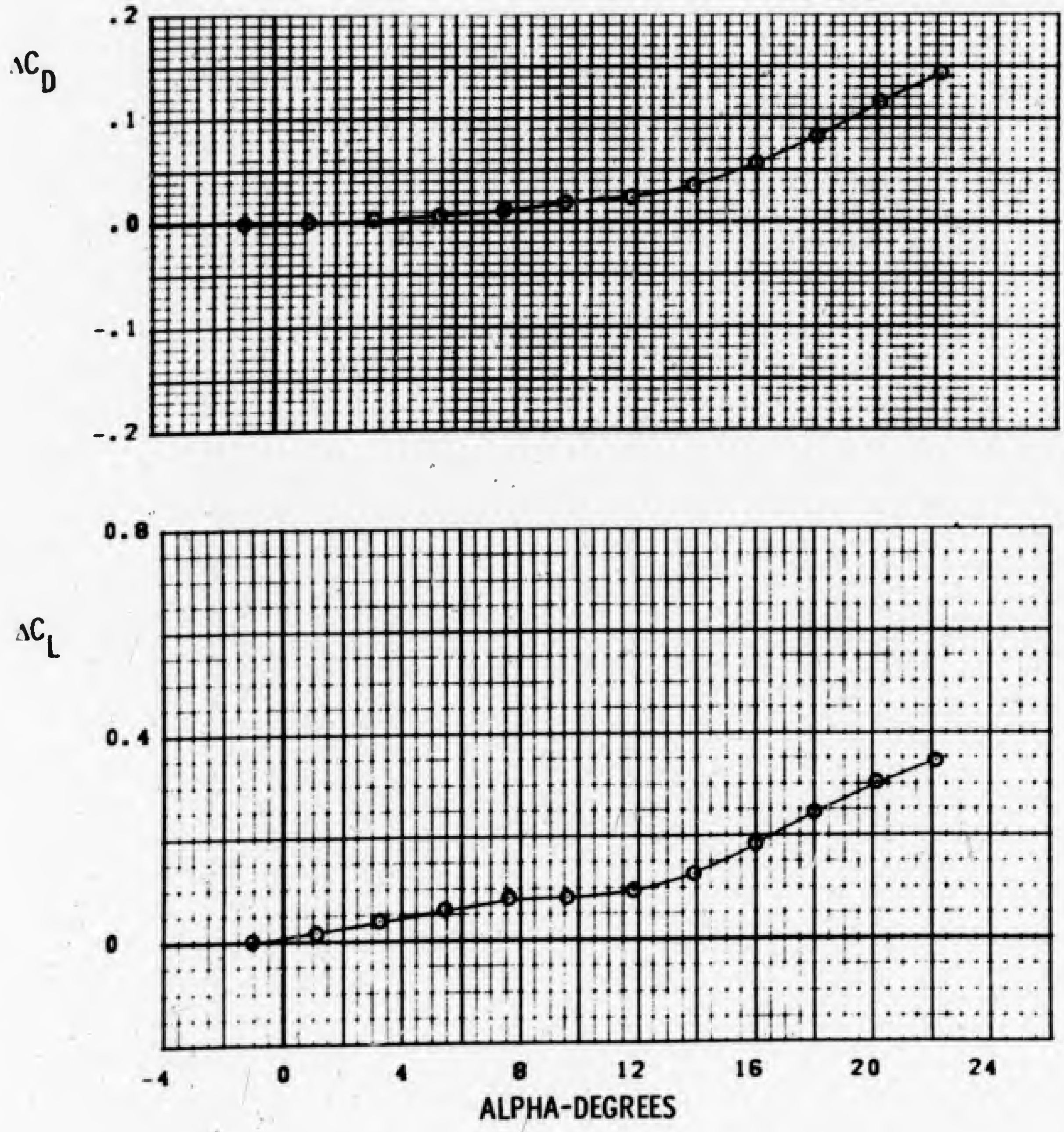
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 122 -PN 115	K1 10/10	INBD 10/-10

FIGURE 120d HORIZONTAL TAIL INTERFERENCE. RN = 5.2 MILLION
SMALL AILERON DEFLECTION M = 1.2



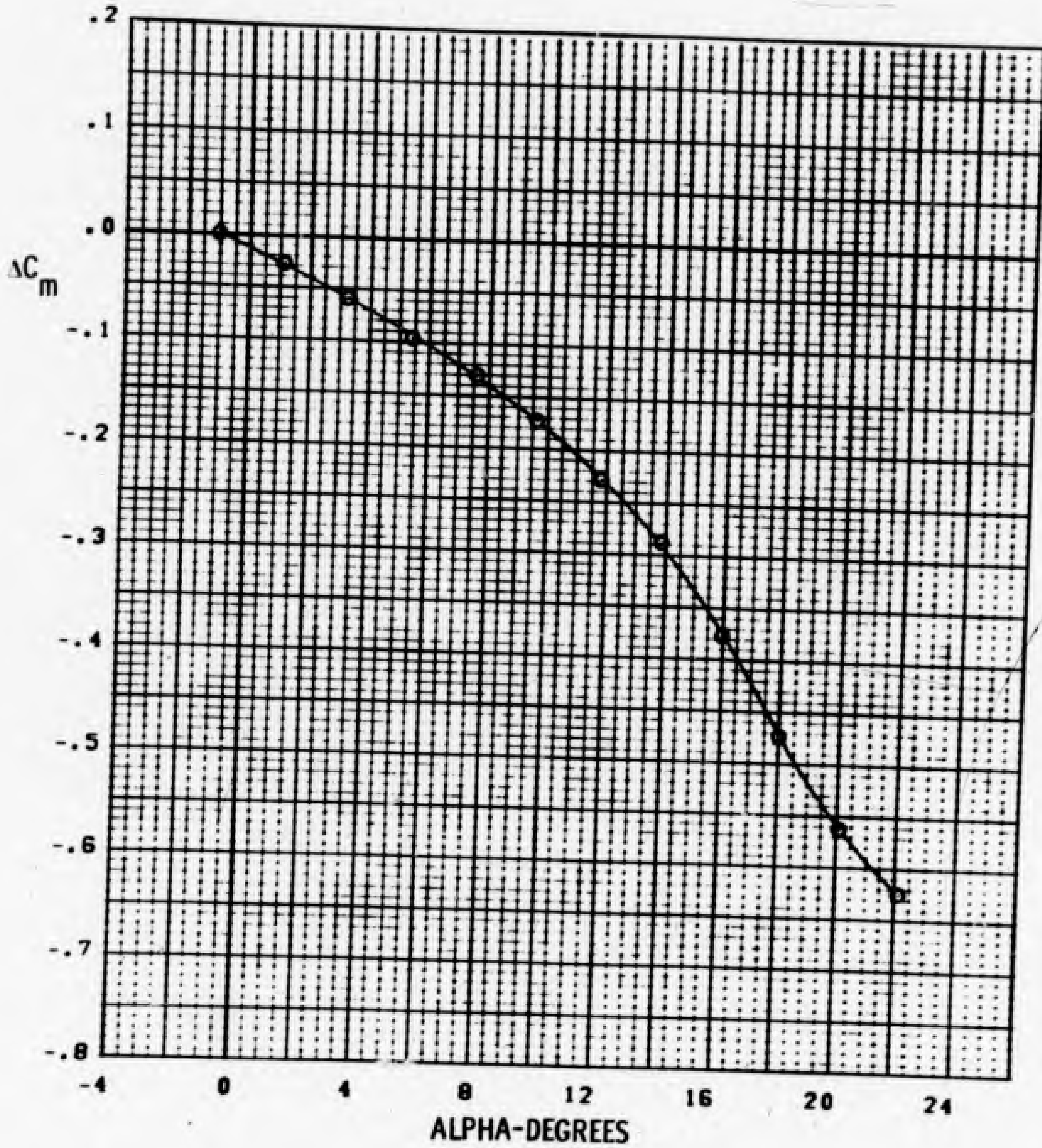
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 285 -PN 499 K1	0/0	MID 20/-20

FIGURE 121a HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.7



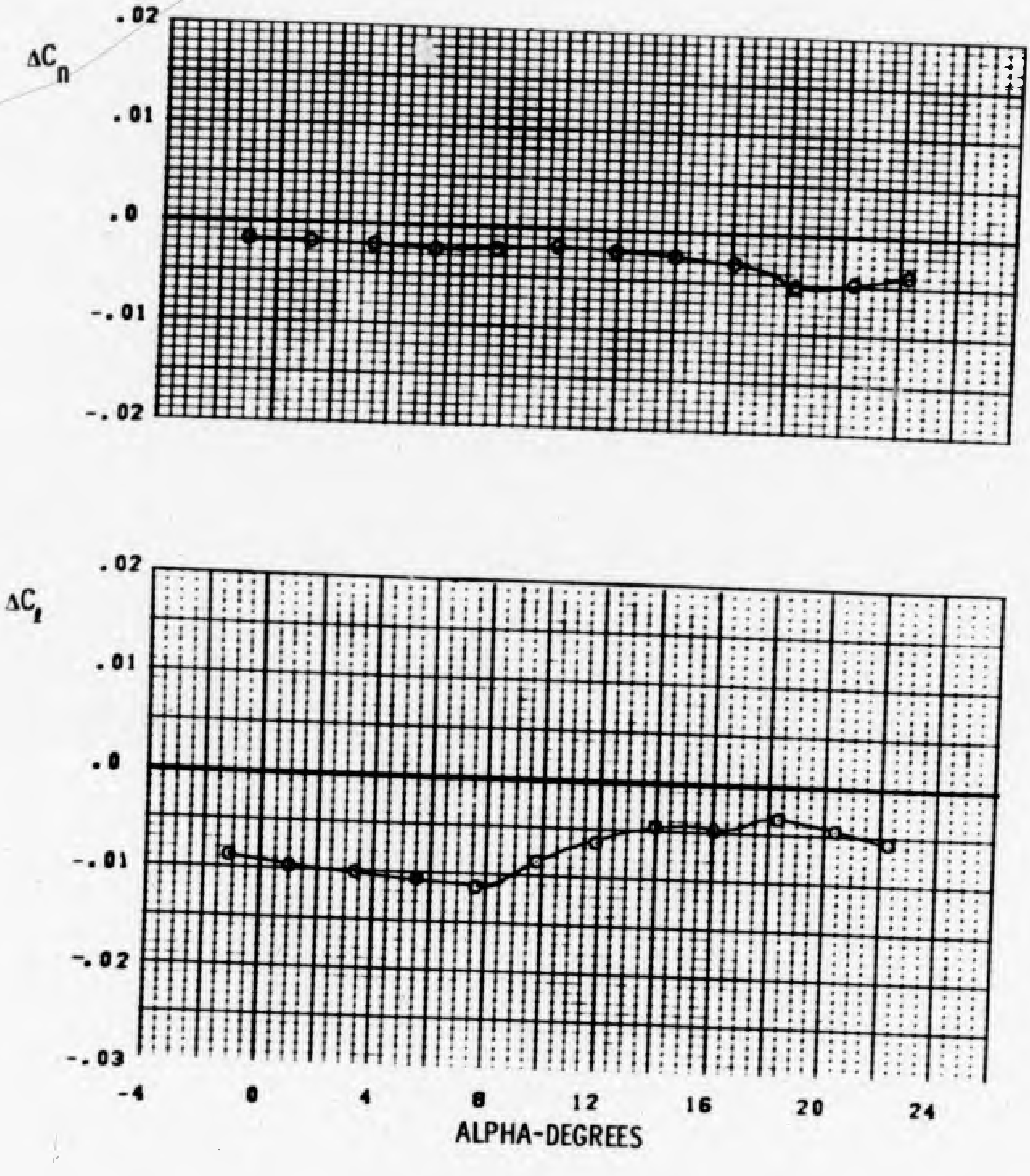
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
○	PWT 4T TC-043	PN 205 -PN 499	K1 0/0	MID 20/-20

FIGURE 121a HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.7



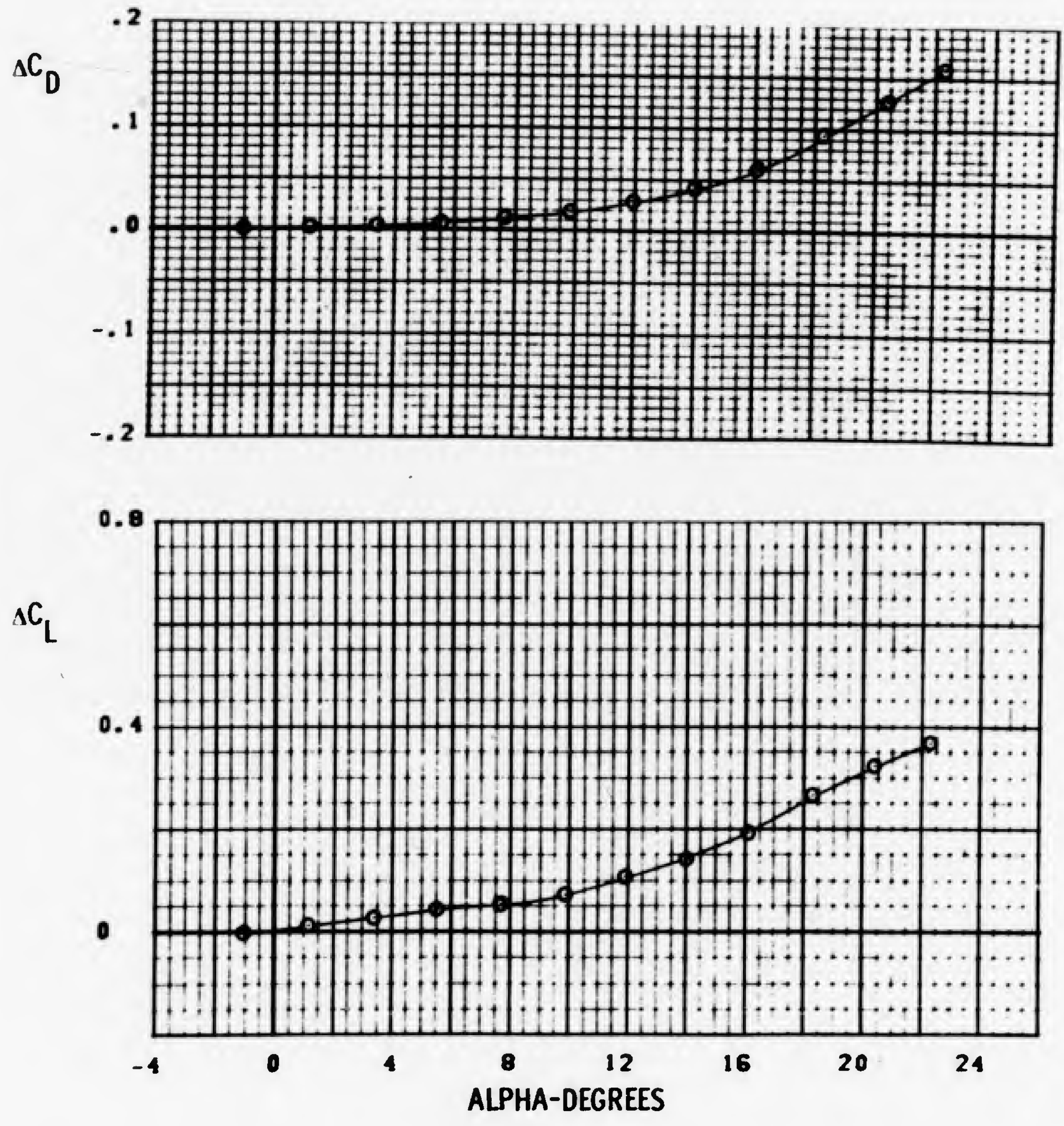
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 285 -PN 499	K1 0/0	MID 20/-20

FIGURE 121a HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION LARGE AILERON DEFLECTION M = 0.7



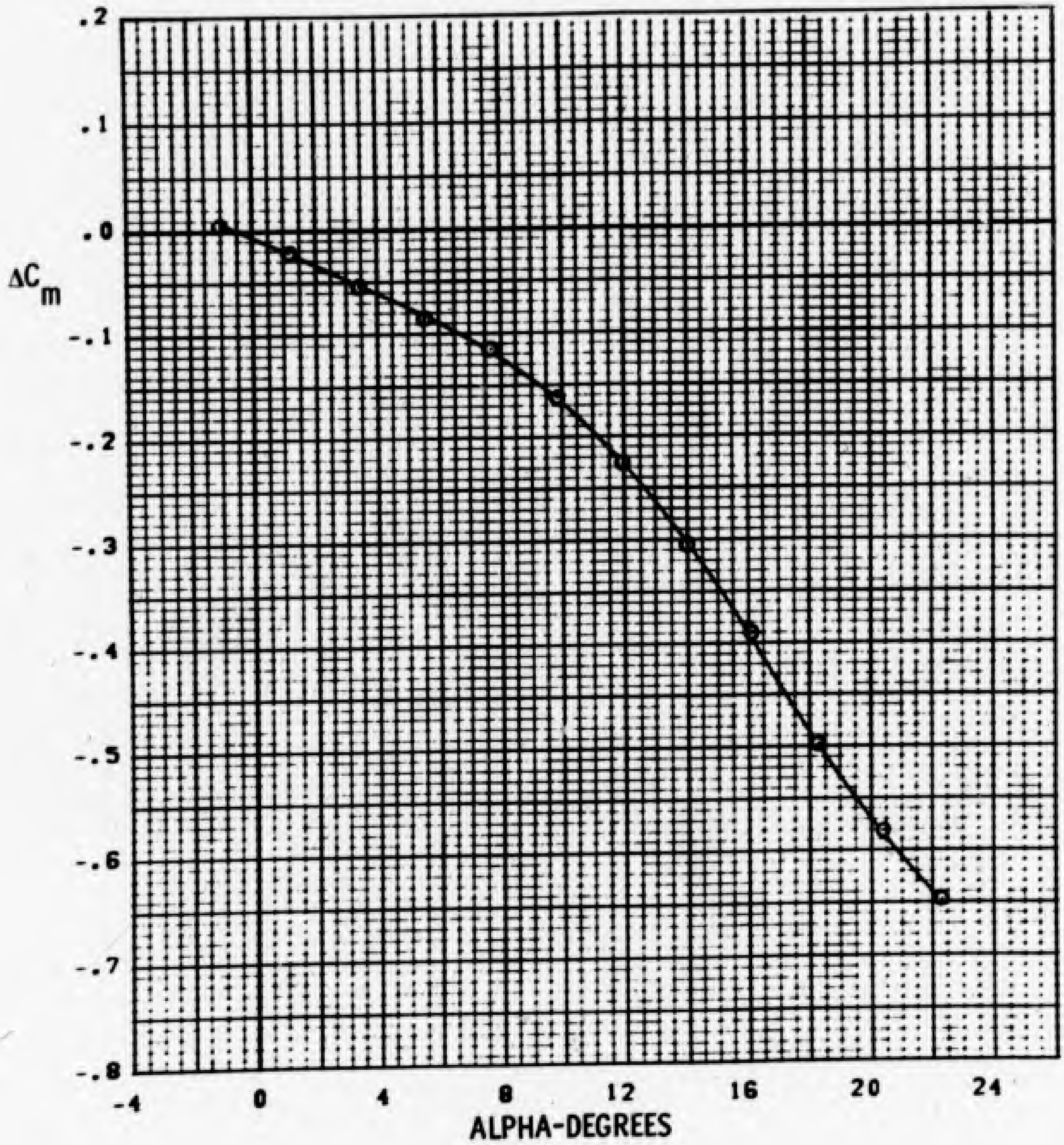
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 284 -PN 500 K1	0/0	MID 20/-20

FIGURE 121b HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.8



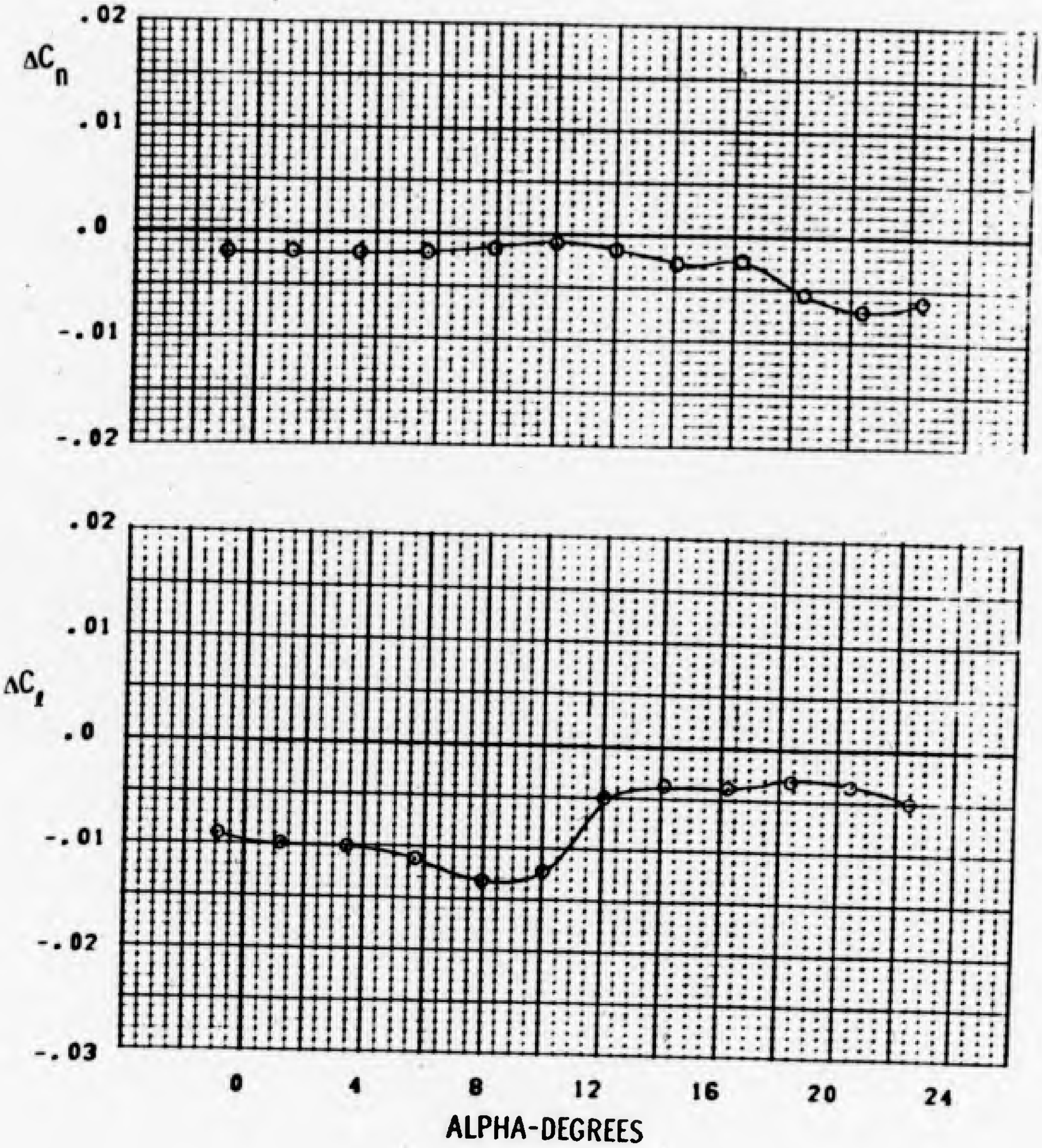
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 284 -PN 500	K1 0/0	MID 20/-20

FIGURE 121b HORIZONTAL TAIL INTERFERENCE, RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.8



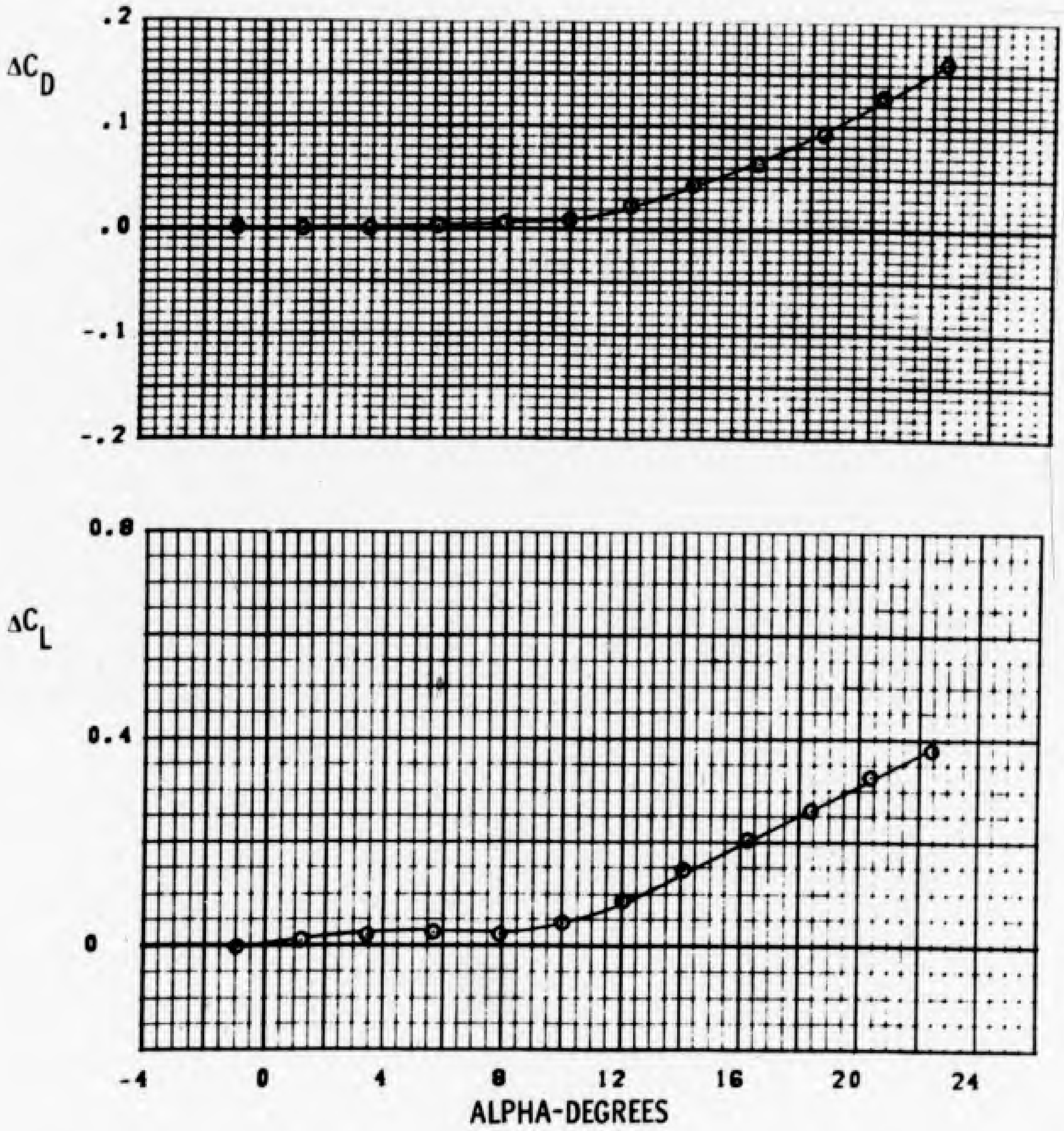
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 284 -PN 500	K1	0/0	MID	20/-20

FIGURE 121b HORIZONTAL TAIL INTERFERENCE, RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.8



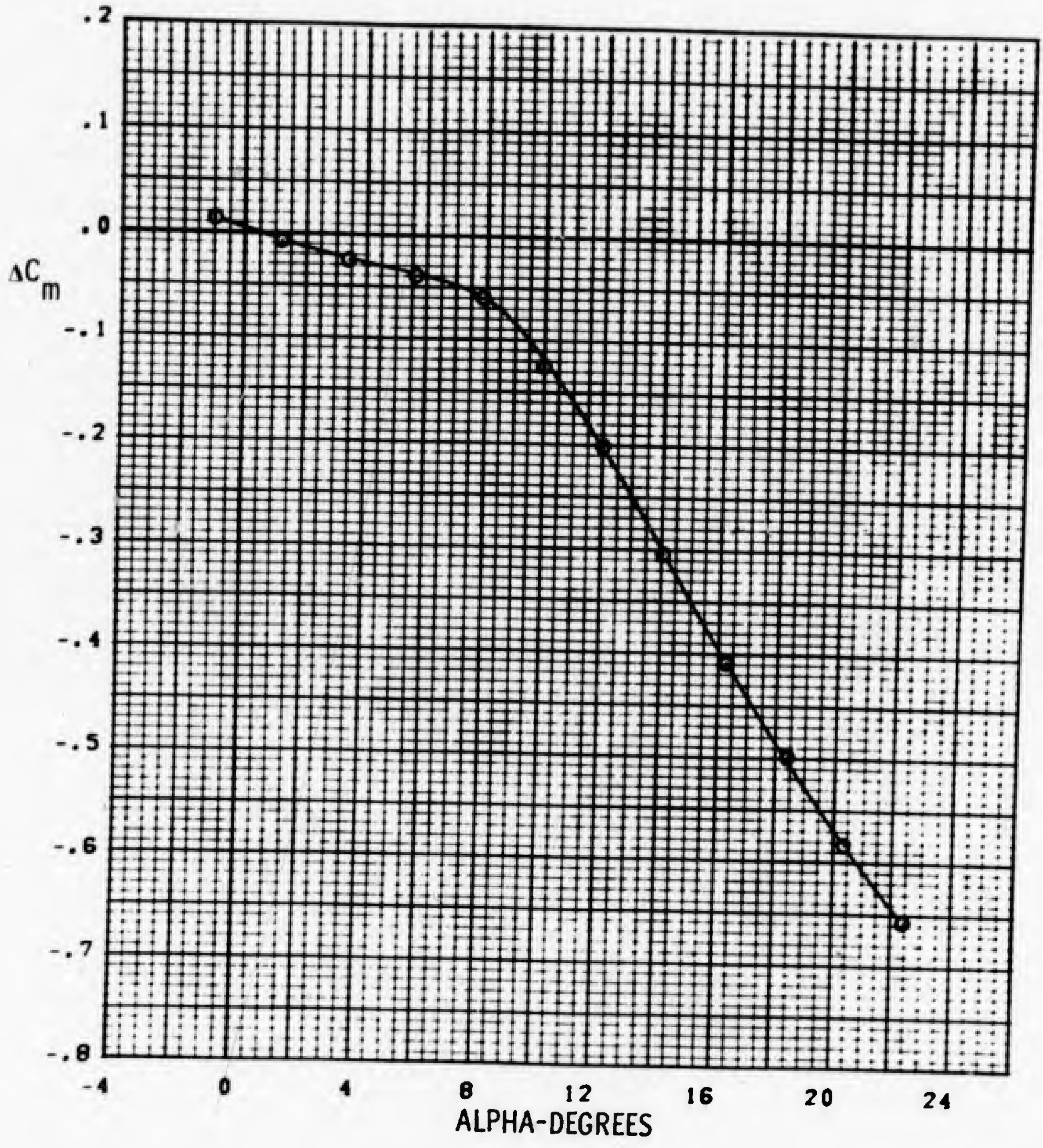
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 283 -PN501	K1 0/0	MID 20/-20

FIGURE 121c HORIZONTAL TAIL INTERFERENCE, RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.9



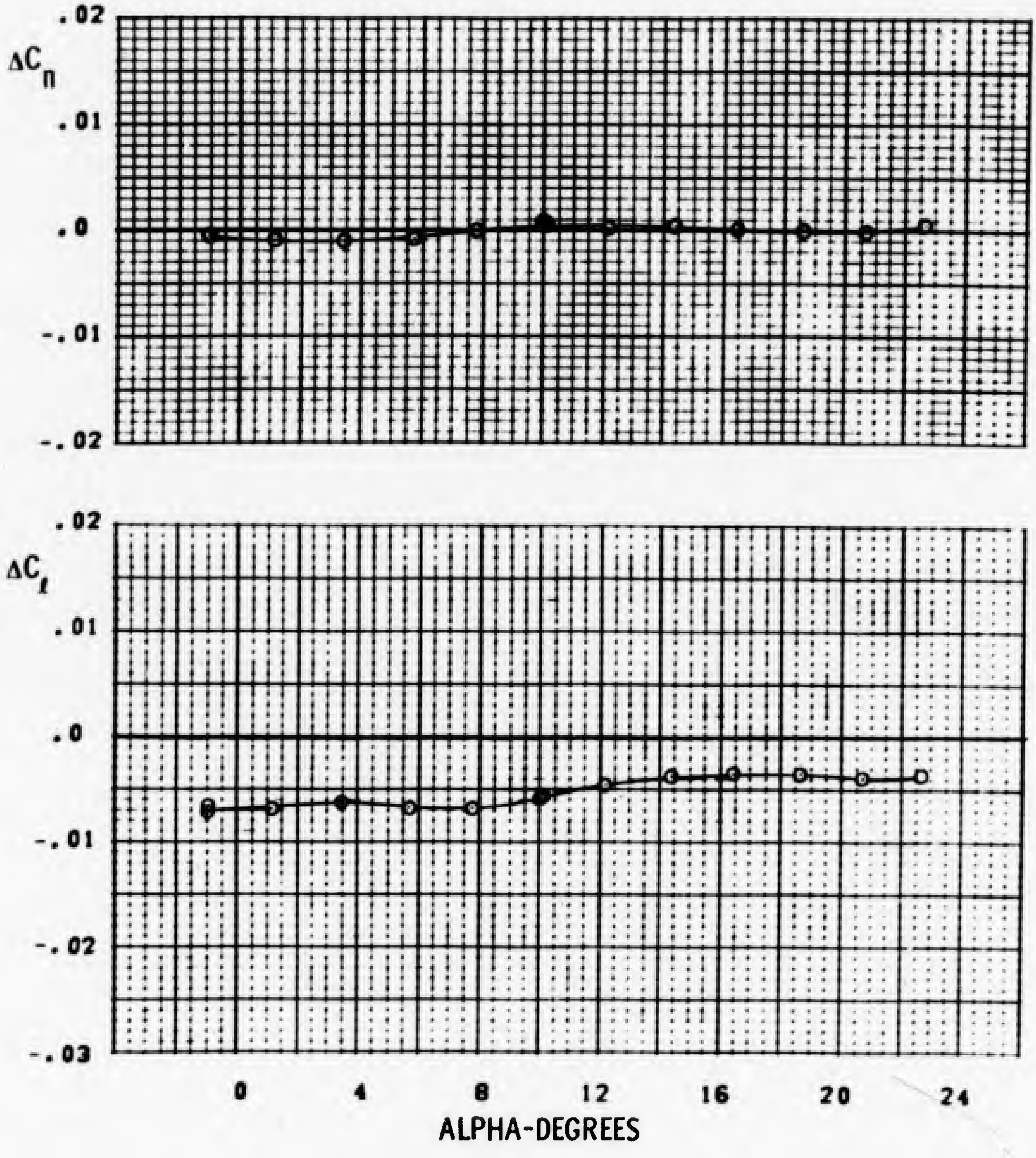
SYM	TEST,	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 283 -PN501	K1 0/0	MID 20/-20

FIGURE 121c HORIZONTAL TAIL INTERFERENCE, RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.9



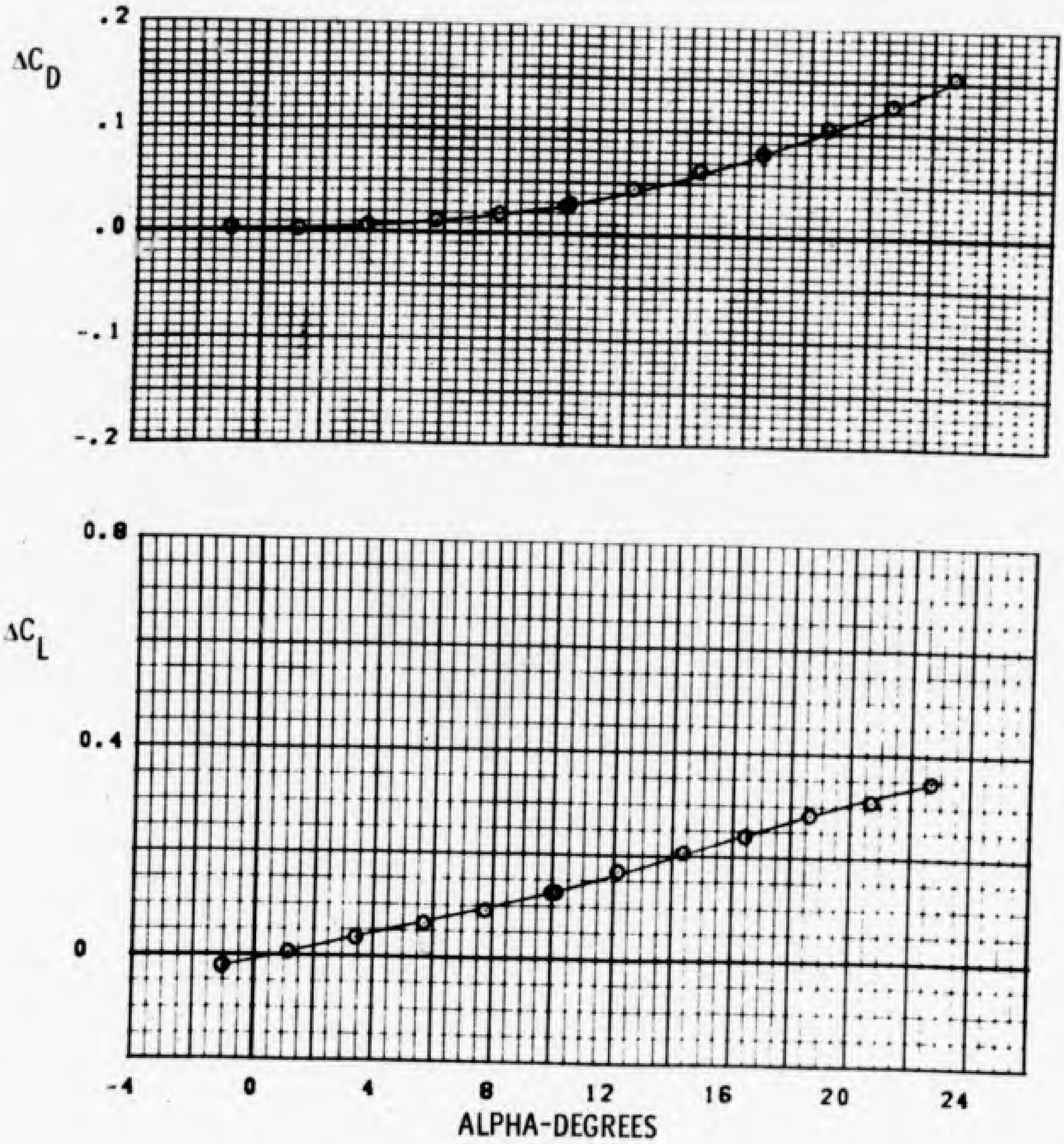
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 283 -PN501	K1	0/0	MID	20/-20

FIGURE 121c HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 0.9



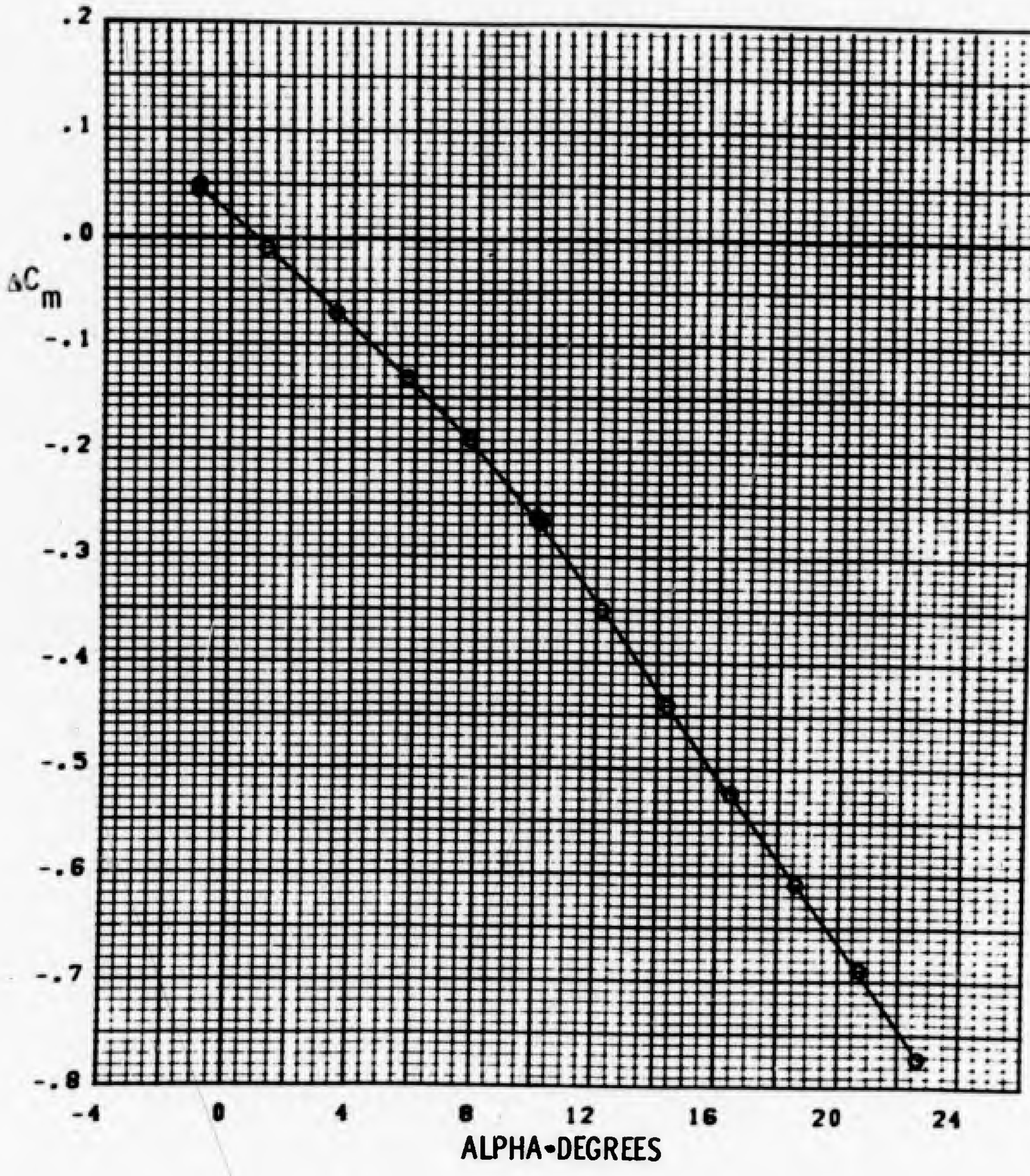
SYM	TEST	INCREMENT	L.E (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 286 -PN 502	K1 0/0	MID 20/-20

FIGURE 121d HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 1.2



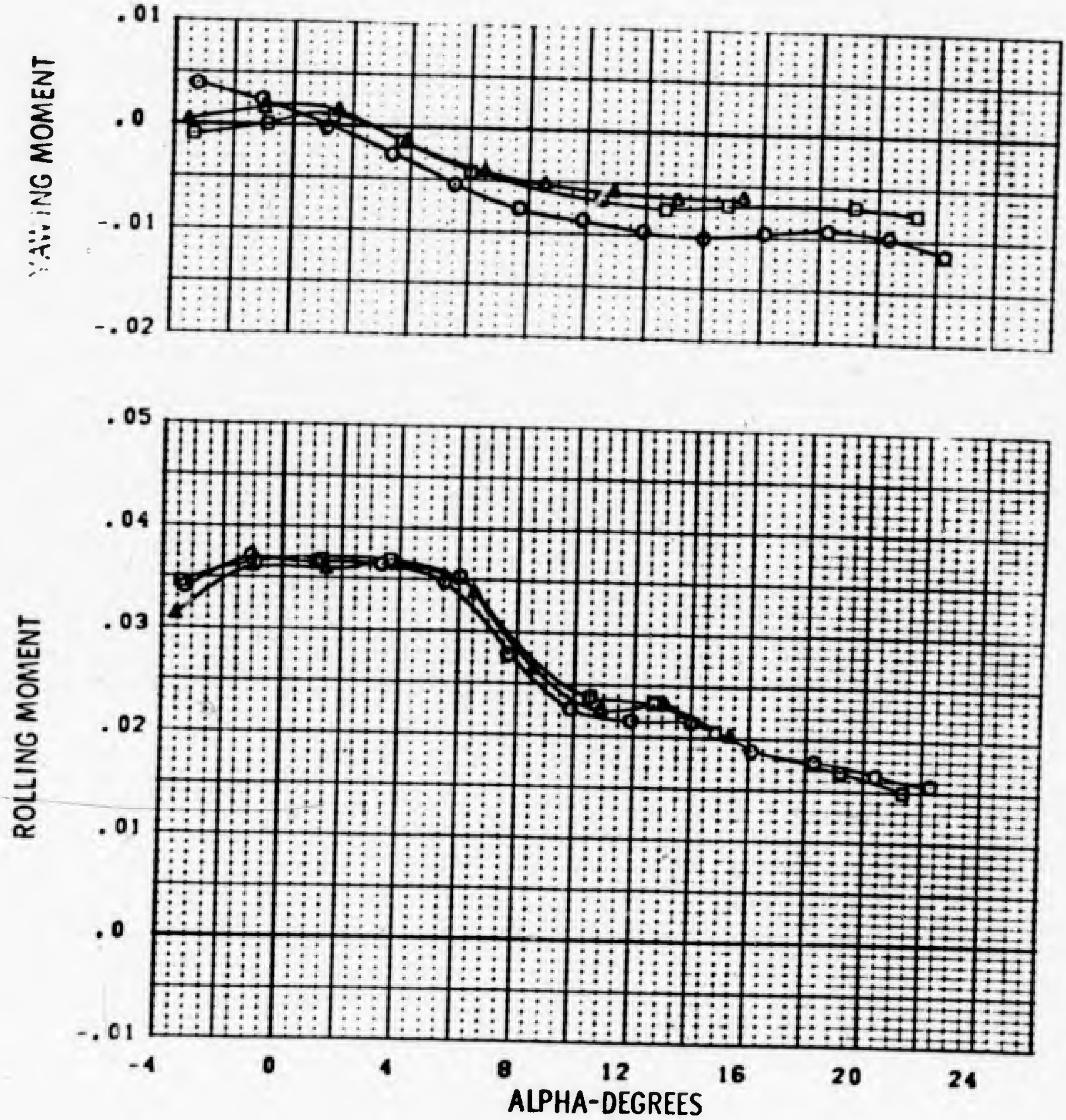
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 286 -PN 502 K1	0/0	MID 20/-20

FIGURE 121d HORIZONTAL TAIL INTERFERENCE, RN = 3.0 MILLION LARGE AILERON DEFLECTION M = 1.2



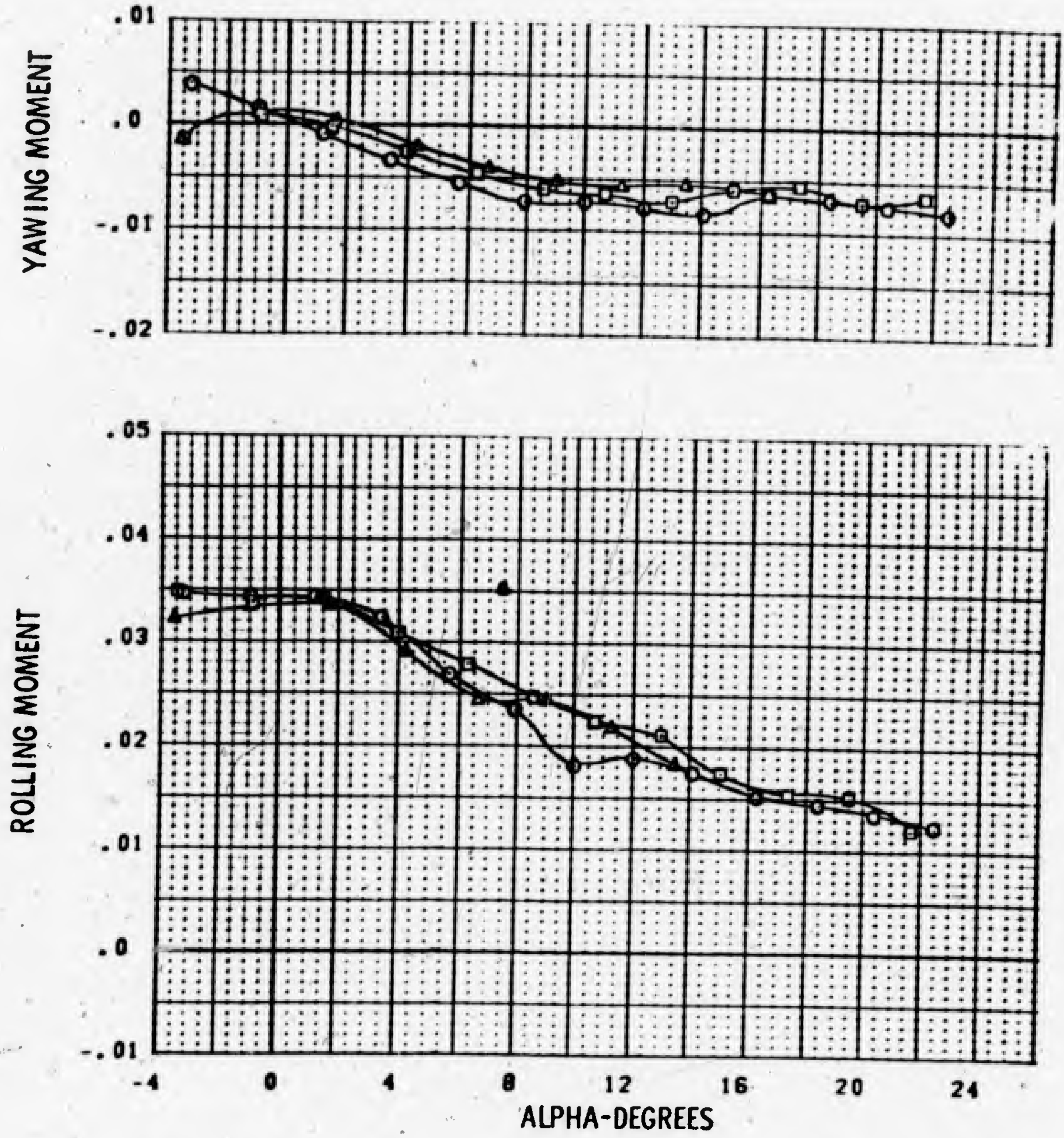
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 286 -PN 502	K1 0/0	MID 20/-20

FIGURE 121d HORIZONTAL TAIL INTERFERENCE. RN = 3.0 MILLION
LARGE AILERON DEFLECTION M = 1.2



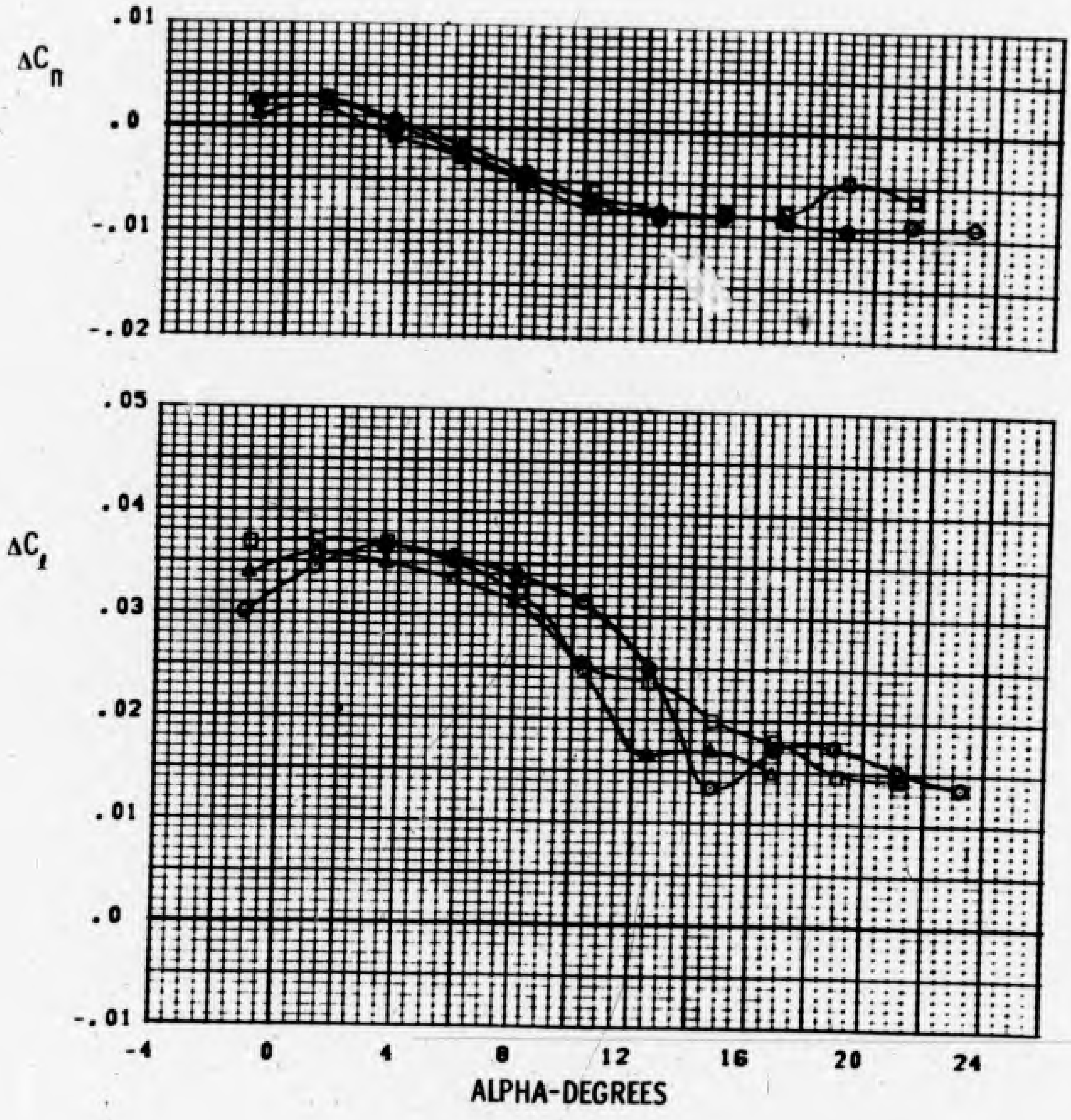
SYM		TEST	PART	L.E. (L/R)		AILERON (L/R)		RN/FT.
○	PWT	4T TC-043	284	K1	0/0	MID	20/-20	3.0 MILLION
□	PWT	4T TC-043	214	K1	0/0	MID	20/-20	5.2 MILLION
▲	PWT	4T TC-043	279	K1	0/0	MID	20/-20	6.2 MILLION

FIGURE 122a REYNOLDS NUMBER EFFECT ON MID AILERONS
M = 0.8



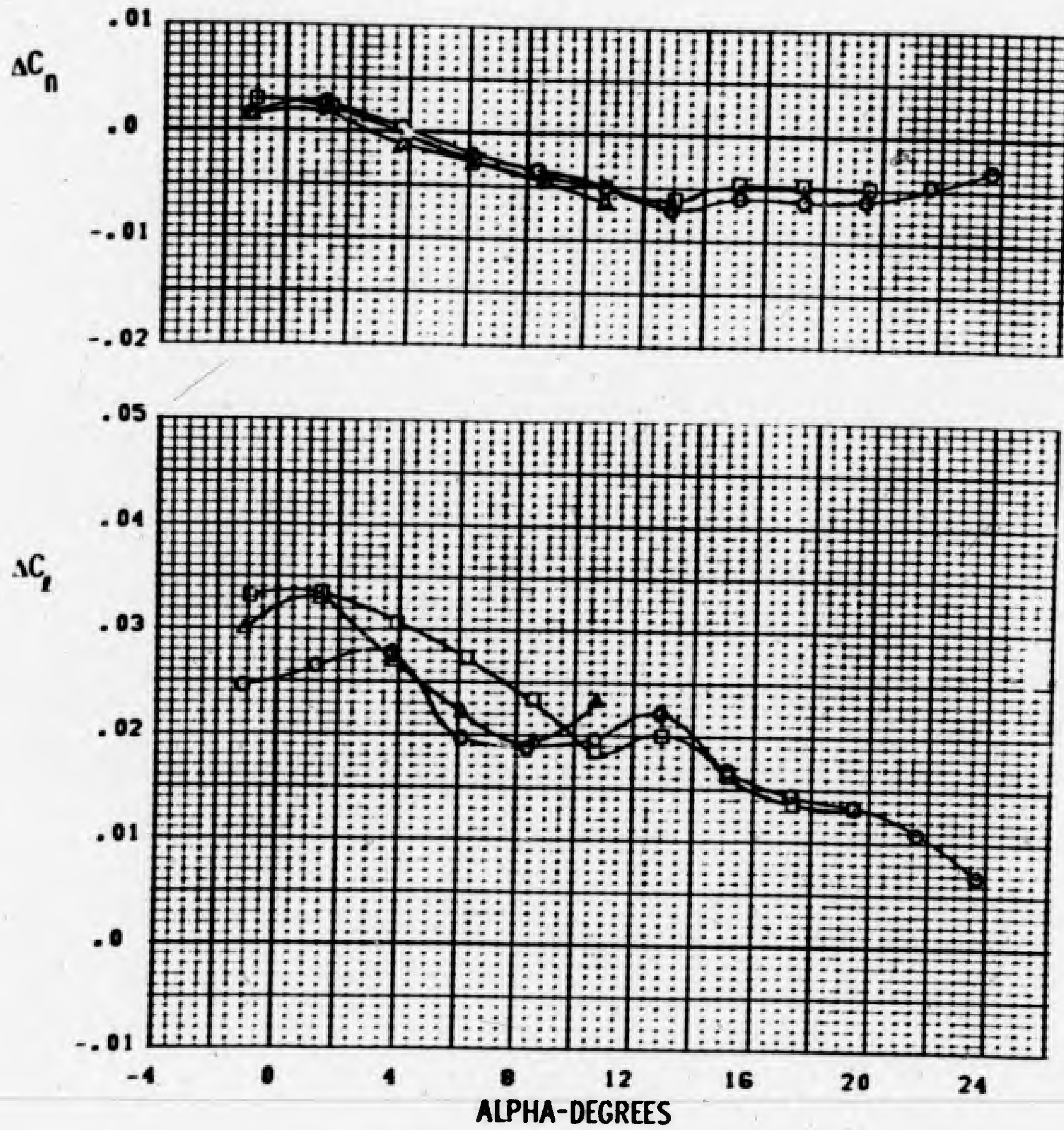
SYM	TEST	PART	L.E. (L/R)		AILERON (L/R)		RN/FT.
O	PWT 4T TC-043	283	K1	0/0	MID	20/-20	3.0 MILLION
□	PWT 4T TC-043	213	K1	0/0	MID	20/-20	5.2 MILLION
▲	PWT 4T TC-043	278	K1	0/0	MID	20/-20	6.4 MILLION

FIGURE 122b REYNOLDS NUMBER EFFECT ON MID AILERONS
M = 0.9



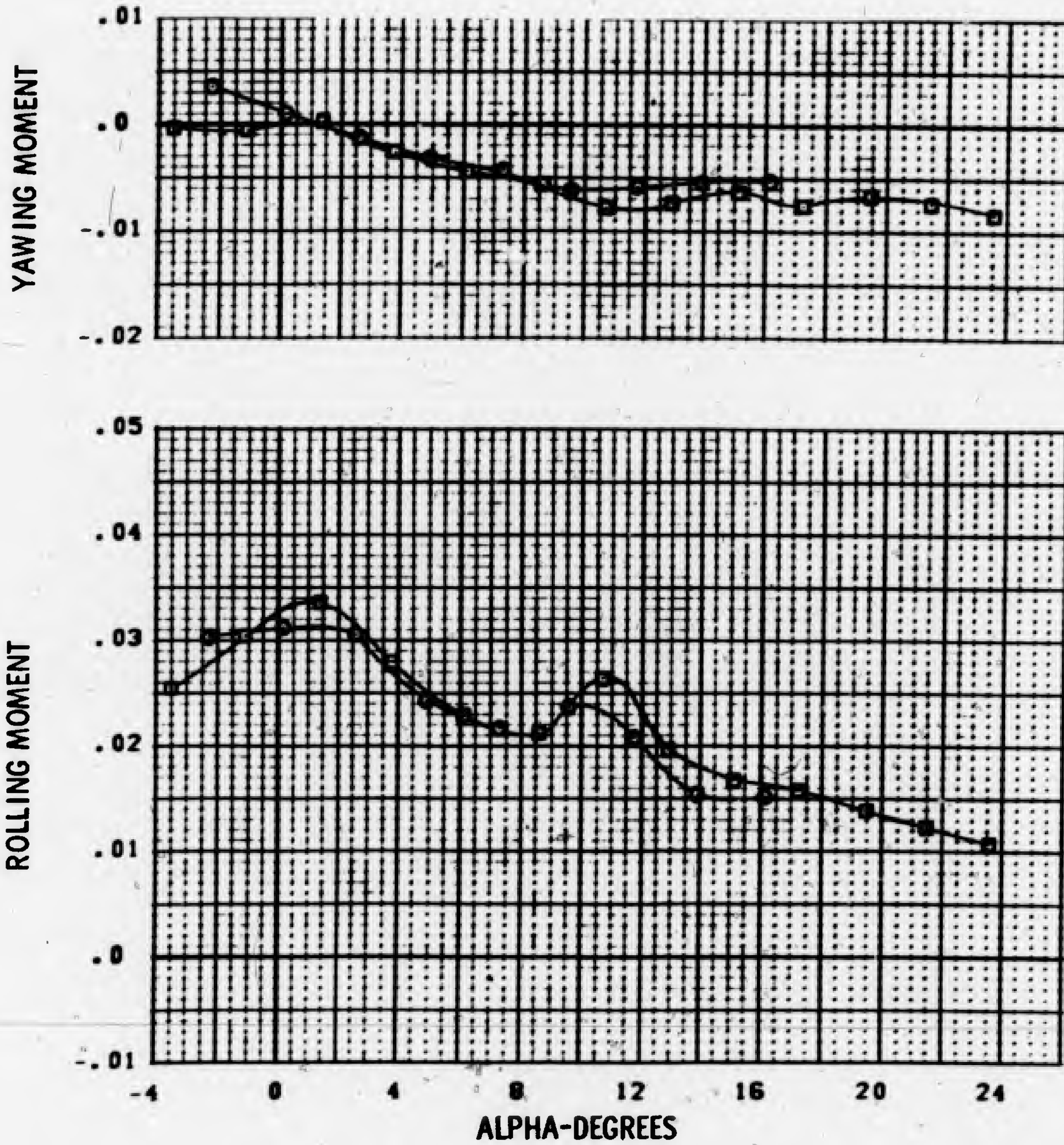
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
□	PWT 4T TC-043	PN 215 - PN 268	K1	0/0	MID	20/-20
△	PWT 4T TC-043	PN 293 - PN 448	K1	5/5	MID	20/-20
⊙	PWT 4T TC-043	PN 142 - PN 128	K1	10/10	MID	20/-20

FIGURE 123a SYMMETRICAL L.E. EFFECTS ON MID AILERONS
M = 0.7



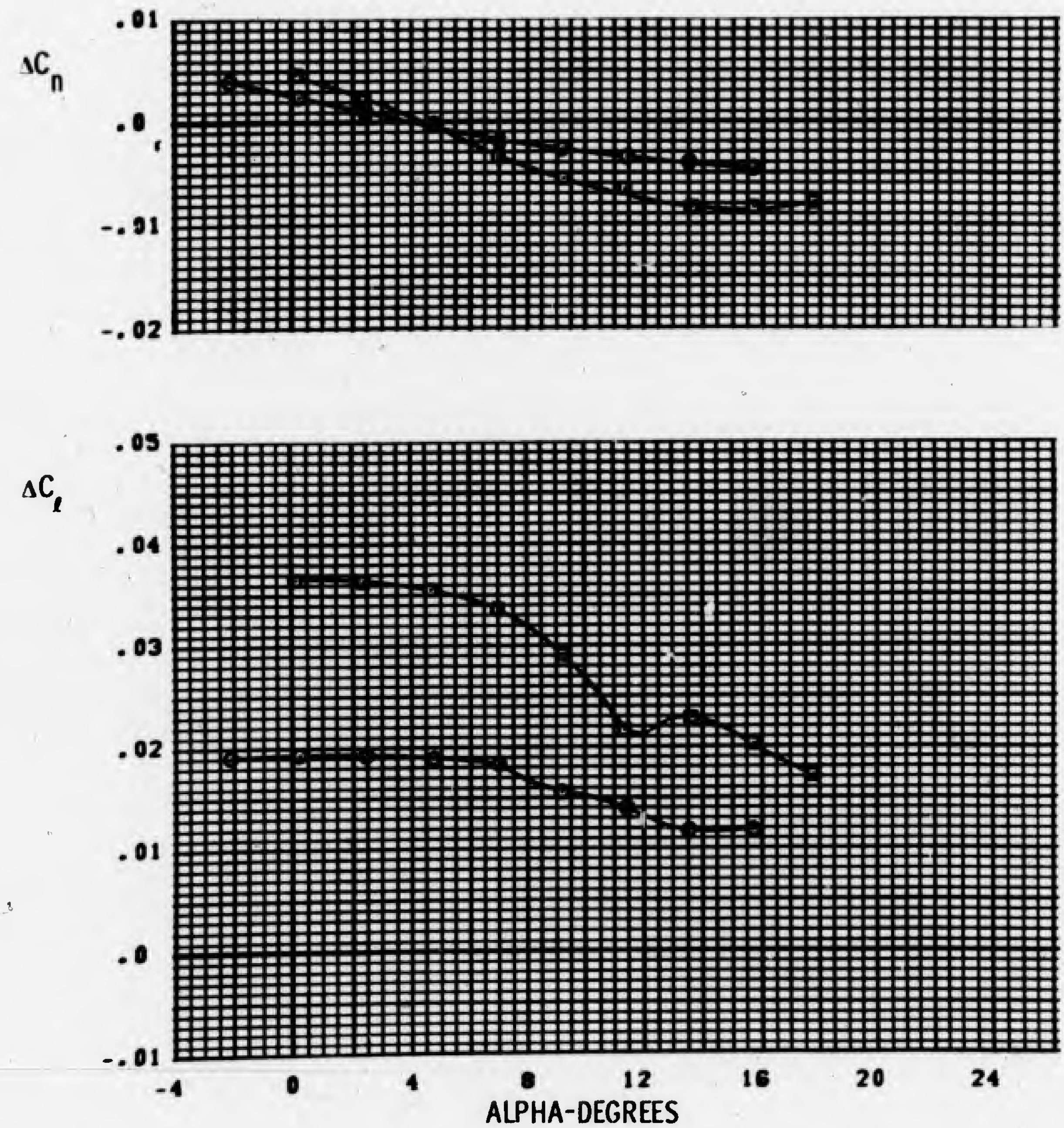
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
□	PWT 4T TC-043	PN 213 - PN 264	K1	0/0	MID.	20/-20
Δ	PWT 4T TC-043	PN 291 - PN 445	K1	5/5	MID	20/-20
⊖	PWT 4T TC-043	PN 140 - PN 126	K1	10/10	MID	20/-20

FIGURE 123b SYMMETRICAL L.E. EFFECTS ON MID AILERONS
M = 0.9



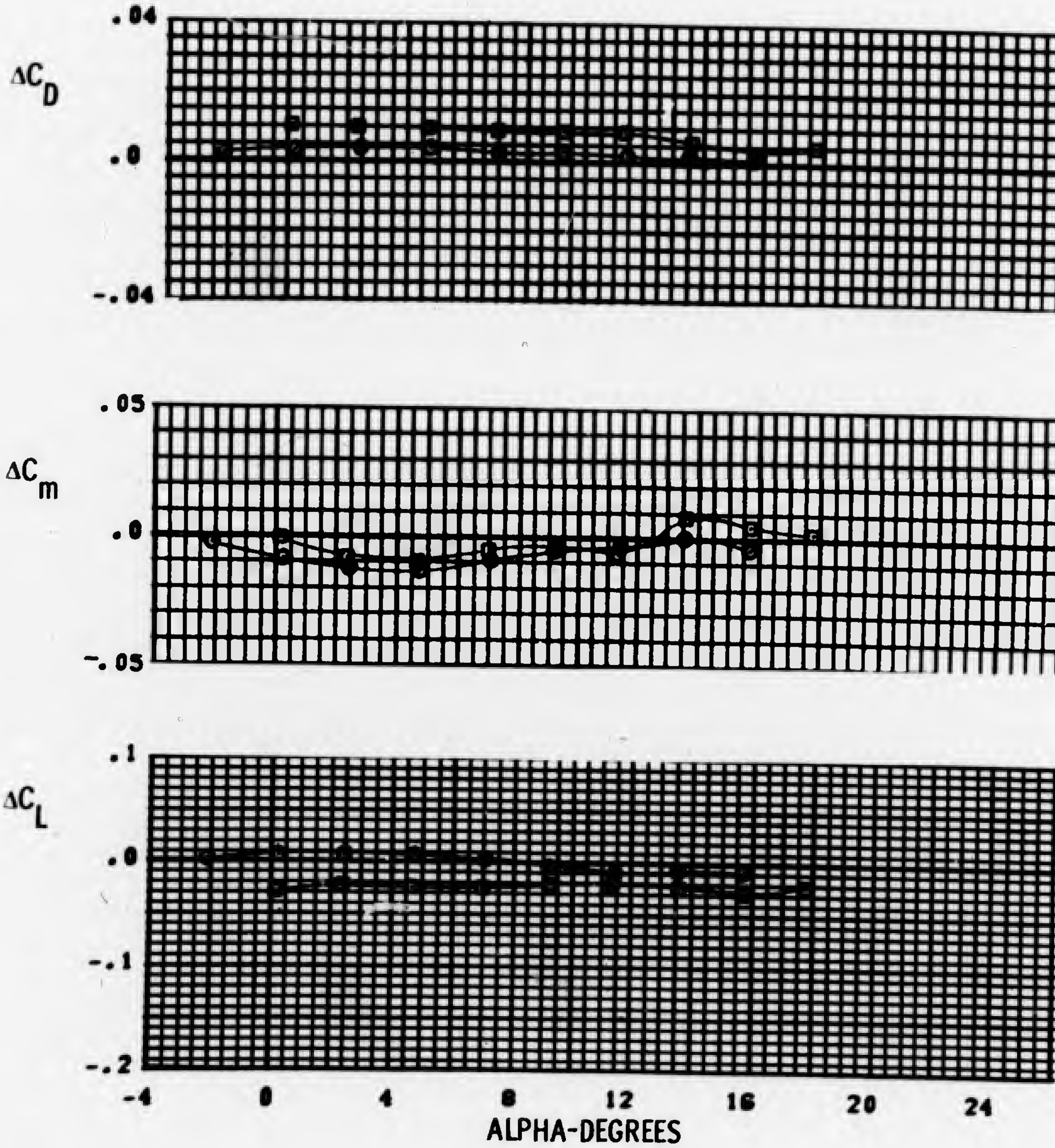
SYM	TEST		PART	L.E.	(L/R)	AILERON	(L/R)
⊙	PWT	4T TC-043	506	K2	5/5	MID	20/-20
⊡	PWT	4T TC-043	291	K1	5/5	MID	20/-20

FIGURE 124 EFFECTS OF LEADING EDGE SECTION GEOMETRY WITH MID AILERONS M = 0.9



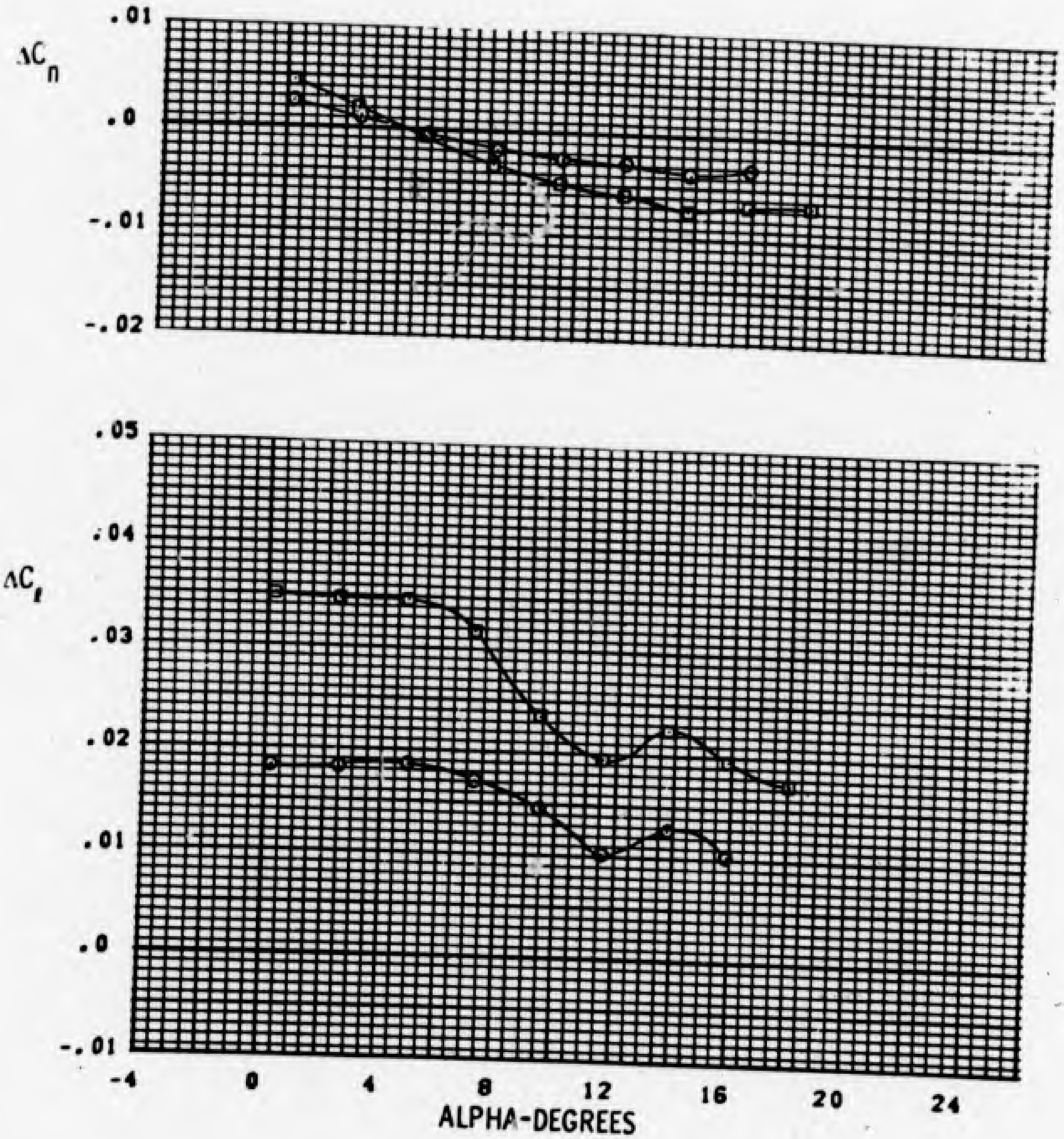
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 475 -PN 438	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 410 -PN 438	K1	0/0	MID	20/-20

FIGURE 125a LINEARITY OF AILERON WITH DEFLECTION
M = 0.7



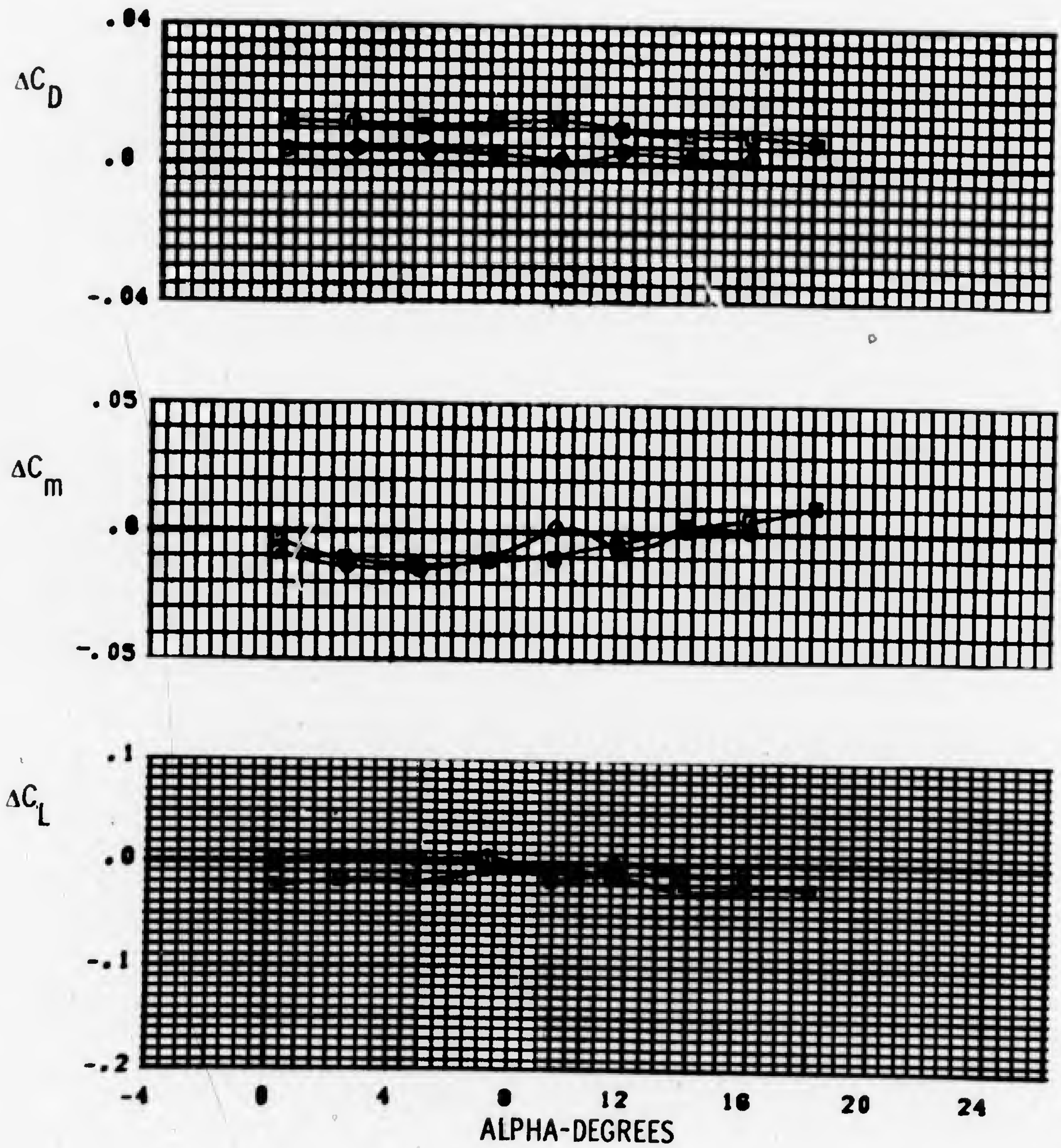
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 475 -PN 438	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 410 -PN 438	K1	0/0	MID	20/-20

FIGURE 125a LINEARITY OF AILERON WITH DEFLECTION
M = 0.7



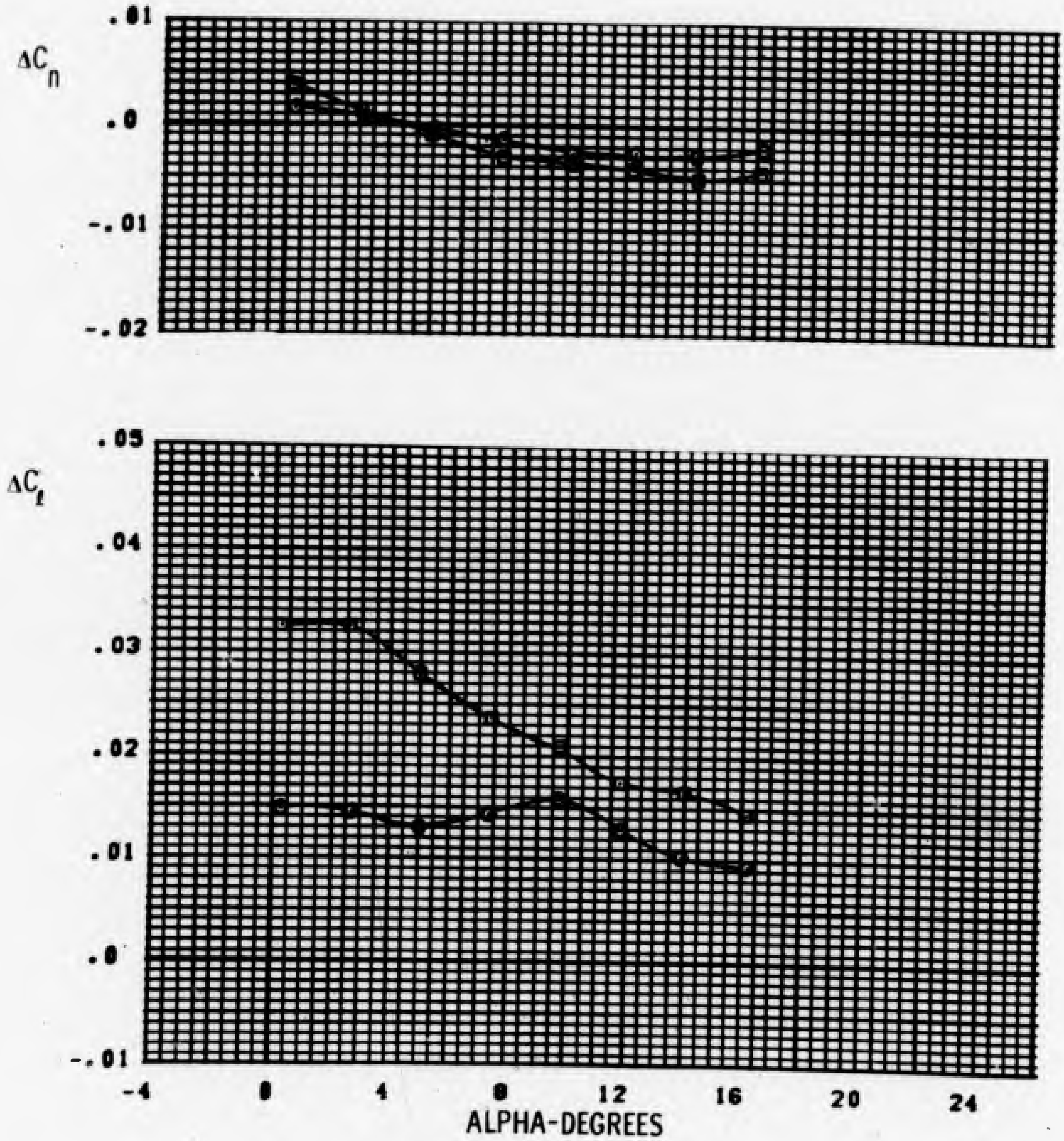
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 476 -PN 440	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 411 -PN 440	K1	0/0	MID	20/-20

FIGURE 125b LINEARITY OF AILERON WITH DEFLECTION
M = 0.8



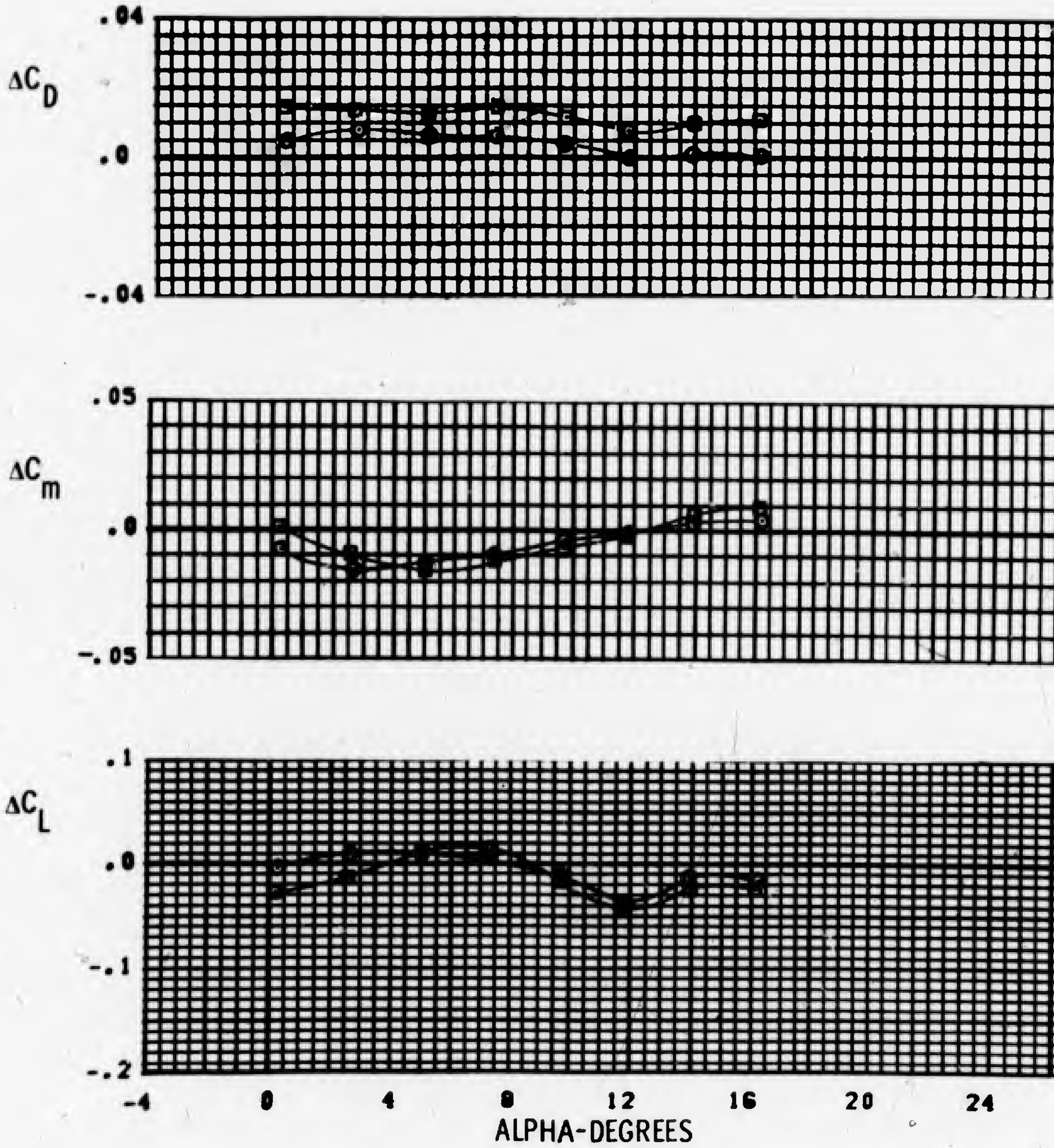
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 476 -PN 440	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 411 -PN 440	K1	0/0	MID	20/-20

FIGURE 125h LINEARITY OF AILERON WITH DEFLECTION
M = 0.8



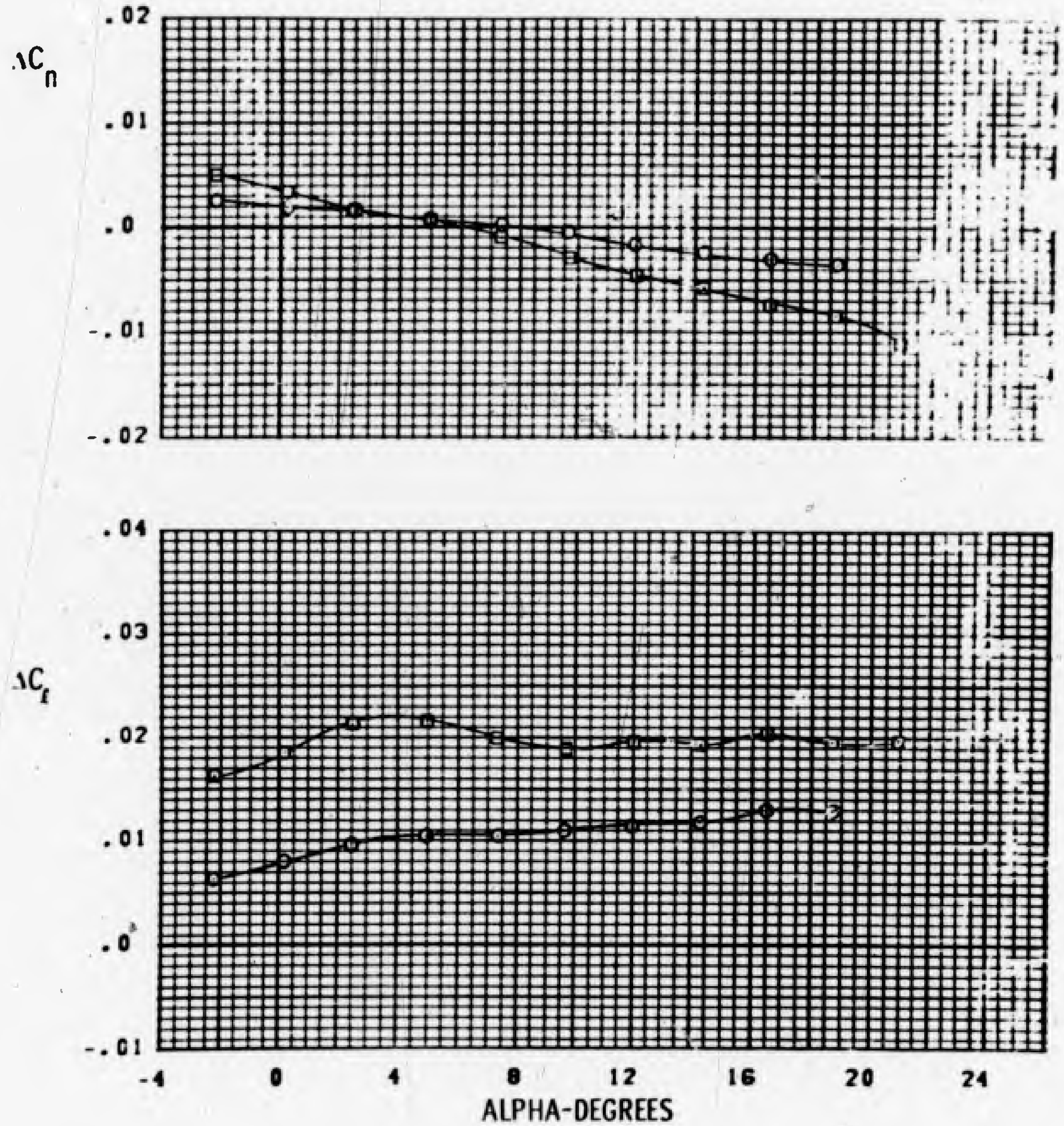
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 474 -PN 441	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 412 -PN 441	K1	0/0	MID	20/-20

FIGURE 125c LINEARITY OF AILERON WITH DEFLECTION
M = 0.9



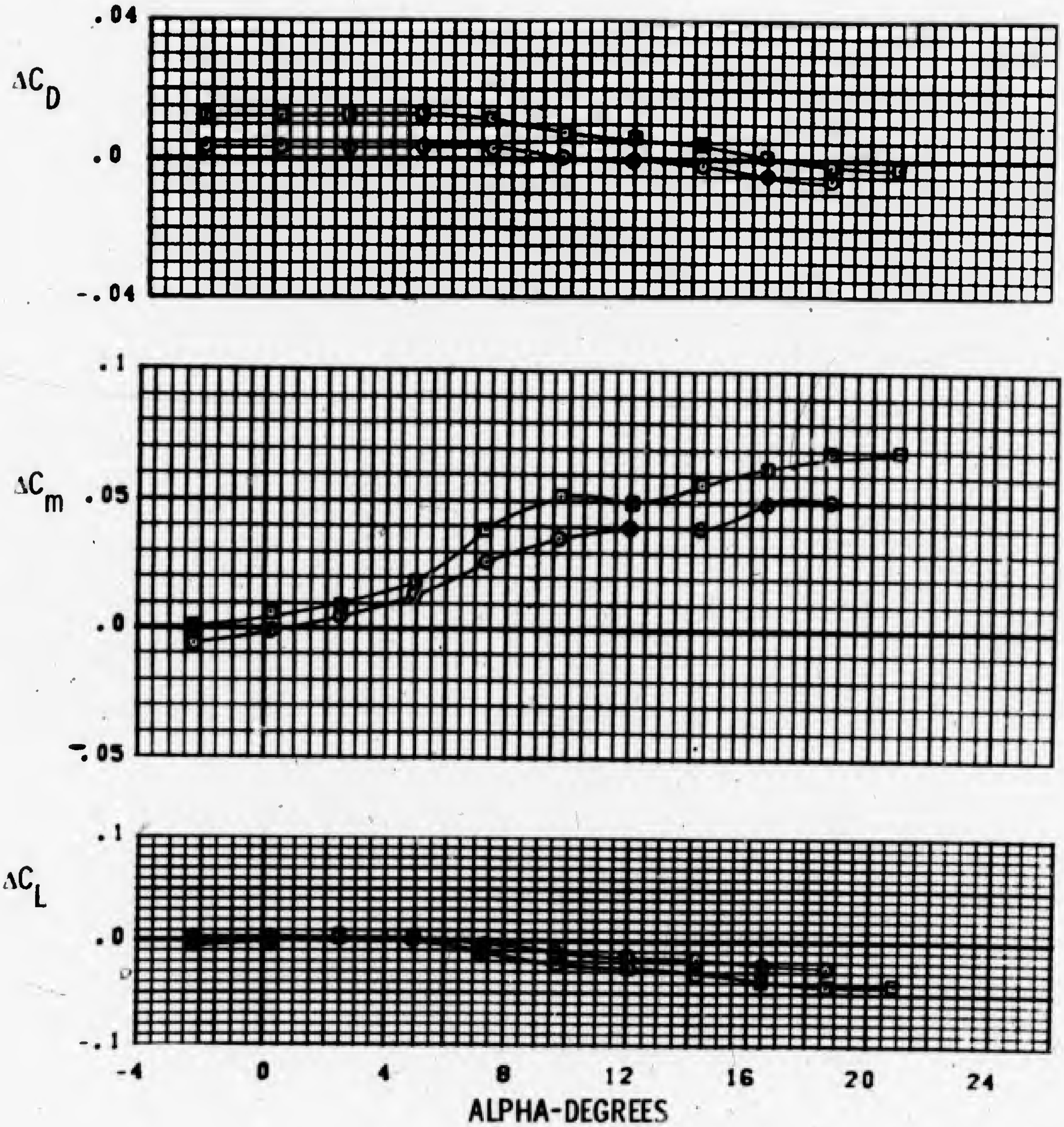
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 474 -PN 441	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 412 -PN 441	K1	0/0	MID	20/-20

FIGURE 125c LINEARITY OF AILERON WITH DEFLECTION
M = 0.9



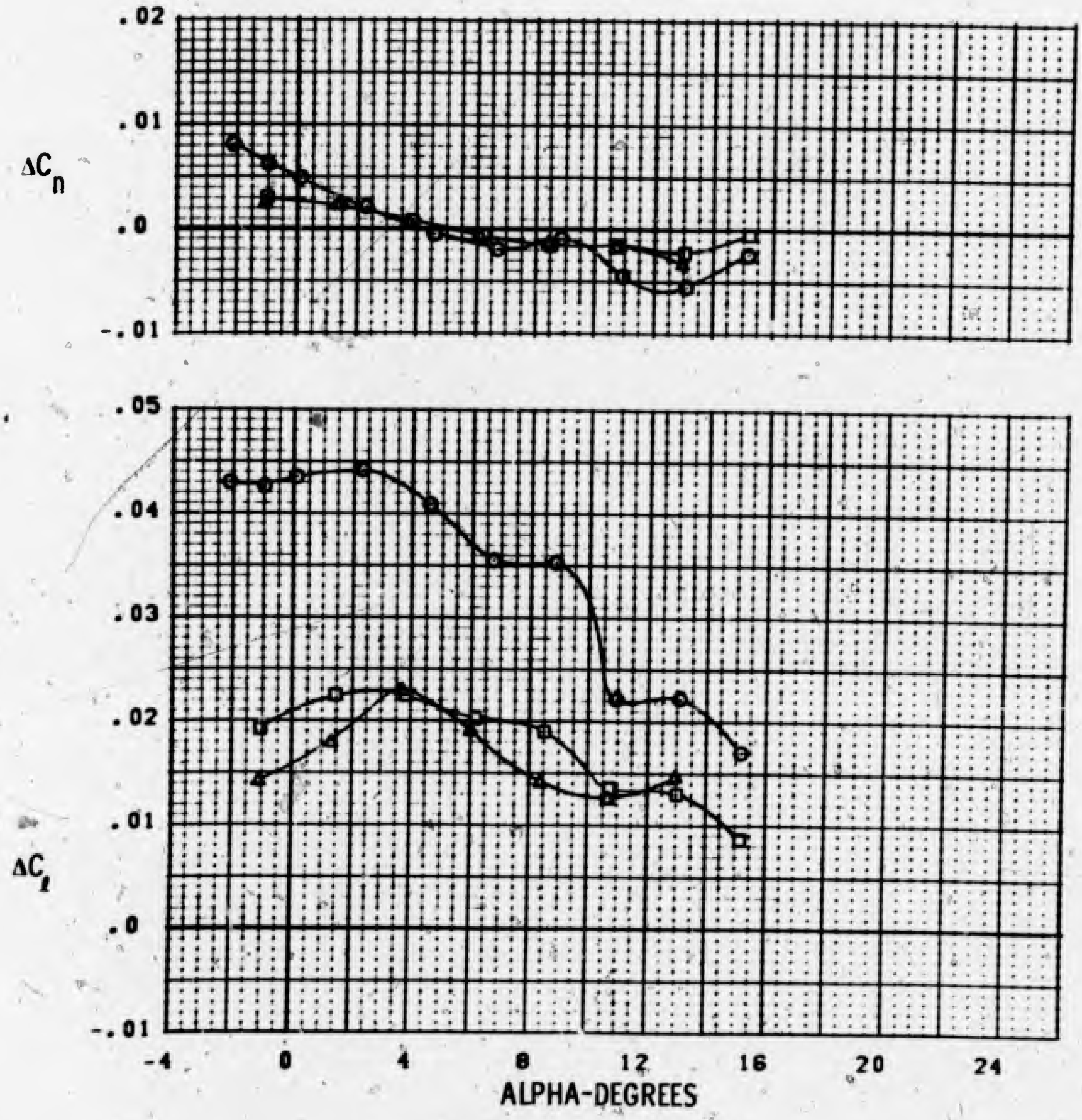
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON	(L/R)
⊙	PWT 4T TC-043	PN 477 -PN 269	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 414 -PN 269	K1	0/0	MID	20/-20

FIGURE 125d LINEARITY OF AILERON WITH DEFLECTION
$M = 1.2$



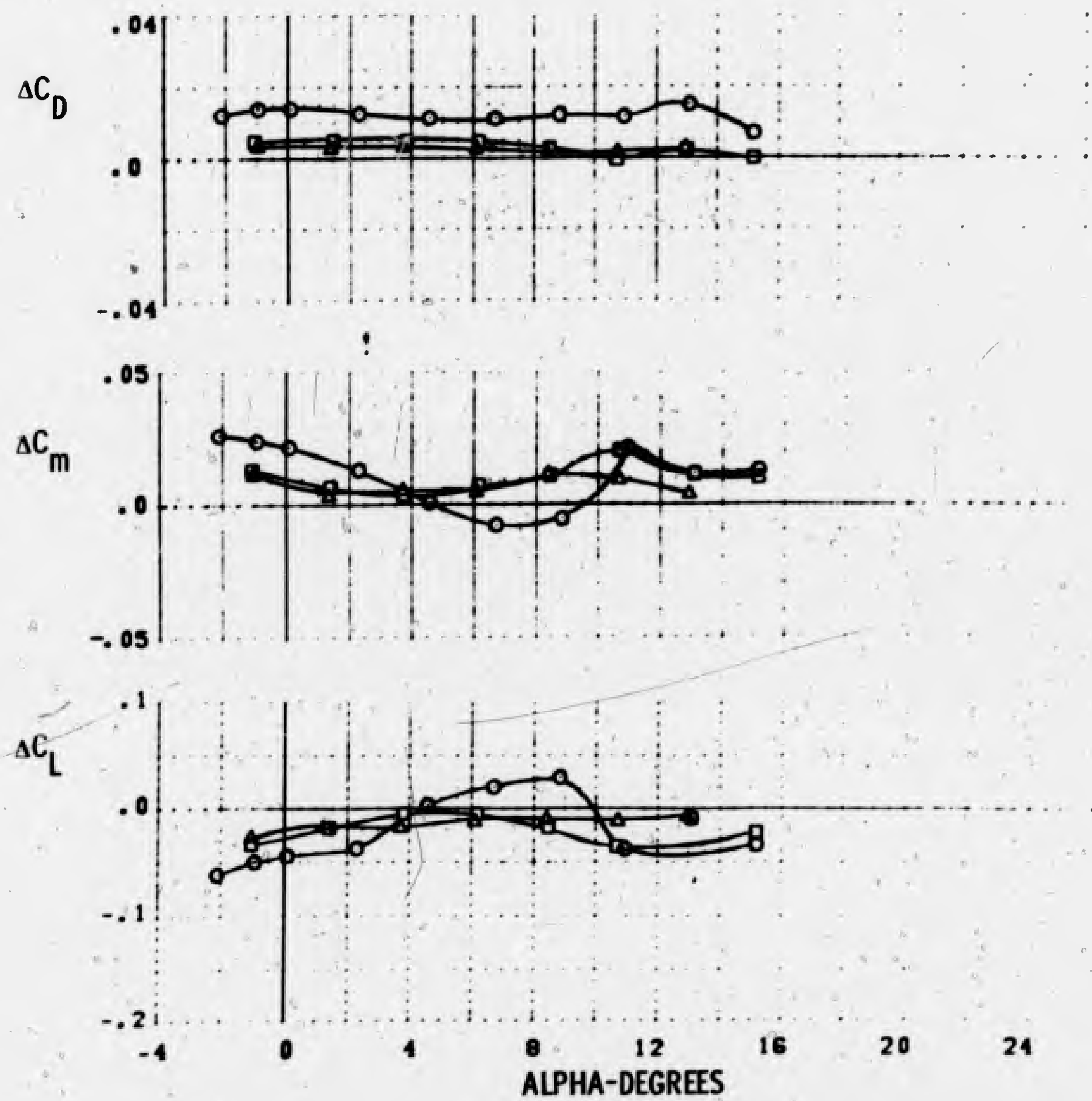
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 477 -PN 269	K1	0/0	MID	10/-10
⊡	PWT 4T TC-043	PN 414 -PN 269	K1	0/0	MID	20/-20

FIGURE 125d LINEARITY OF AILERON WITH DEFLECTION
M = 1.2



SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 501 - PN 30	K1	0/0	MID	20/-20
⊡	PWT 4T TC-043	PN 96 - PN 37	K1	5/5	MID	10/-10
⚠	PWT 4T TC-043	PN 108 - PN 47	K1	10/10	MID	10/-10

FIGURE 126 LINEARITY OF AILERON WITH DEFLECTION (H.T. OFF)
M = 0.9



SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 501 - PN 30	K1	0/0	MID	20/-20
⊡	PWT 4T TC-043	PN 96 - PN 37	K1	5/5	MID	10/-10
▲	PWT 4T TC-043	PN 108 - PN 47	K1	10/10	MID	10/-10

FIGURE 126 LINEARITY OF AILERON WITH DEFLECTION (H.T. OFF)
M = 0.3

Table VI AILERON SPANWISE LOCATION INCREMENTAL DATA SUMMARY

Horizontal Tail Off — L. E. Flap Deflected 10^0

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	DATA RUN	BASE RUN
0.9	OUTBD	10/-10	-1.03400	-0.01572	0.00709	0.00116	0.00380	0.00071	PWT 4T	104	47
			1.34800	-0.00737	0.00061	0.00210	0.00851	0.00010			
			3.74500	-0.00738	0.00398	0.00145	0.01560	-0.00080			
			6.09700	-0.00376	0.00199	0.00223	0.01470	-0.00170			
			8.40300	-0.00870	0.00974	-0.00009	0.01311	-0.00230			
			10.69000	-0.01629	0.01390	-0.00209	0.01262	-0.00270			
			12.96600	0.00242	0.00097	0.00373	0.01500	-0.00450			
			15.20400	-0.00733	0.00533	0.00064	0.01360	-0.00520			
0.9	MID	10/-10	-1.05300	-0.02735	0.01140	0.00285	0.01400	0.00241	PWT 4T	108	47
			1.33900	-0.01523	0.00381	0.00270	0.01761	0.00231			
			3.73200	-0.01760	0.00530	0.00305	0.02280	0.00090			
			6.09800	-0.01193	0.00509	0.00232	0.01900	-0.00080			
			8.40600	-0.00951	0.01115	0.00096	0.01401	-0.00130			
			10.69500	-0.01219	0.00876	0.00141	0.01252	-0.00180			
			12.95400	-0.00760	0.00340	0.00240	0.01460	-0.00330			
0.9	INBD	10/-10	-1.03000	-0.01575	0.00951	0.00554	0.01580	0.00611	PWT 4T	112	47
			1.35200	-0.01571	0.00451	0.00630	0.01791	0.00670			
			3.74100	-0.01092	0.00346	0.00433	0.02090	0.00480			
			6.10500	0.00083	-0.00240	0.00624	0.02050	0.00230			
			8.41200	-0.00142	0.00876	0.00345	0.01601	0.00100			
			10.73100	0.00365	0.00171	0.00612	0.01361	-0.00050			
			12.98700	0.00494	-0.00506	0.00462	0.01811	-0.00361			
			15.19900	-0.01143	0.00304	0.00330	0.01299	-0.00169			

Table VII AILERON SPANWISE LOCATION INCREMENTAL DATA SUMMARY

Horizontal Tail On — L.E. Flap Deflected 0^0

MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.7	MID	20/ -20	-2.00900	-0.02424	0.00320	0.01015	0.03891	0.00741	PWT 16T	13	49
			-0.85700	-0.01539	-0.00161	0.01006	0.03842	0.00561			
			0.20400	-0.01048	-0.00736	0.01002	0.03889	0.00430			
			1.27400	-0.01021	-0.01167	0.00989	0.03811	0.00290			
			2.29600	-0.00970	-0.01315	0.00977	0.03827	0.00160			
			4.53800	-0.00910	-0.01418	0.00916	0.03770	-0.00110			
			6.89700	-0.00233	-0.00926	0.01047	0.03539	-0.00450			
			8.11900	-0.00157	-0.00808	0.01242	0.03027	-0.00569			
			9.14600	-0.00592	-0.00937	0.01230	0.02786	-0.00592			
			10.26900	-0.01111	-0.00667	0.01051	0.02415	-0.00681			
			11.40900	-0.00905	-0.00546	0.01000	0.02437	-0.00781			
			13.65000	-0.00378	-0.00354	0.00882	0.02334	-0.00856			
			15.73900	-0.00148	-0.00434	0.00952	0.02008	-0.00866			
			18.12199	0.00765	-0.00196	0.01177	0.01734	-0.00830			
0.7	OUTBD	20/ -20	-1.95600	-0.02976	0.01276	0.00752	0.03780	0.00270	PWT 16T	85	49
			-1.05100	-0.02238	0.00918	0.00773	0.03836	0.00189			
			0.15000	-0.01578	0.00271	0.00777	0.03776	0.00099			
			1.16800	-0.01478	-0.00108	0.00756	0.03695	-0.00009			
			2.23000	-0.01051	-0.00232	0.00749	0.03722	-0.00081			
			3.33300	-0.01042	-0.00185	0.00615	0.03713	-0.00161			
			4.59500	-0.01283	-0.00327	0.00646	0.03639	-0.00270			
			6.80300	0.00261	-0.00806	0.00726	0.03341	-0.00450			
			7.89000	0.00876	-0.00818	0.00795	0.03002	-0.00510			
			9.02400	0.00778	-0.00587	0.00829	0.02509	-0.00540			
			10.20300	0.00811	-0.00310	0.00831	0.02321	-0.00610			
			11.29000	0.00544	-0.00258	0.00857	0.02320	-0.00670			
			13.56400	0.01018	0.00101	0.00806	0.02211	-0.00711			
			15.76100	0.01362	0.00236	0.00927	0.02028	-0.00667			
			18.03999	0.01388	0.00564	0.00956	0.01948	-0.00807			

Table VII CONT'D

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.8	MID	20/-20	-2.00100	-0.02242	0.00418	0.01086	0.03681	0.00709	PWT 16T	12	50
			-0.84200	-0.01317	-0.00131	0.01093	0.03665	0.00531			
			0.31200	-0.00787	-0.00714	0.01087	0.03680	0.00400			
			1.38600	-0.00478	-0.01167	0.01121	0.03690	0.00260			
			2.47900	-0.00845	-0.01541	0.01092	0.03691	0.00141			
			4.85500	-0.00537	-0.01388	0.01043	0.03531	-0.00170			
			7.24000	0.01686	-0.01587	0.01345	0.03207	-0.00422			
			9.32100	-0.00567	-0.00855	0.01186	0.02180	-0.00520			
			11.59100	-0.00499	-0.00371	0.01097	0.02017	-0.00596			
			13.85300	-0.00734	-0.00179	0.01074	0.02198	-0.00699			
			16.19499	0.00405	0.00051	0.01272	0.01933	-0.00666			
			18.30699	-0.00096	-0.00217	0.01256	0.01646	-0.00674			
			20.46399	-0.00348	0.00419	0.01175	0.01521	-0.00742			
0.8	OUTBD	20/-20	-1.98200	-0.03716	0.01730	0.00762	0.03551	0.00289	PWT 16T	84	50
			-0.89200	-0.02187	0.00379	0.00838	0.03624	0.00181			
			0.19900	-0.01524	0.00343	0.00835	0.03529	0.00060			
			1.35600	-0.01025	-0.00041	0.00875	0.03570	-0.00040			
			2.40100	-0.00928	-0.00331	0.00873	0.03530	-0.00100			
			3.56000	-0.01047	-0.00265	0.00611	0.03465	-0.00210			
			4.70900	-0.01123	-0.00232	0.00760	0.03300	-0.00310			
			6.98500	0.00405	-0.00842	0.00841	0.02760	-0.00420			
			8.14800	0.01813	-0.00709	0.00862	0.02678	-0.00469			
			9.26600	0.00488	-0.00343	0.00748	0.02281	-0.00520			
			10.42600	0.01551	-0.00213	0.00905	0.02081	-0.00530			
			11.53300	0.00921	-0.00384	0.00887	0.01919	-0.00563			
			13.78300	0.01167	-0.00574	0.01058	0.01979	-0.00569			
			16.04900	0.01731	-0.00076	0.01230	0.01881	-0.00562			
			18.40199	0.01035	-0.00175	0.01115	0.01852	-0.00767			

Table VII CONT'D

MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.85	MID	20/-20	-1.97500	-0.02990	0.00621	0.01187	0.03501	0.00632	PWT 16T	11	51
			-0.82900	-0.01569	0.00021	0.01203	0.03591	0.00529			
			0.27400	-0.01438	-0.00596	0.01228	0.03571	0.00351			
			1.43800	-0.00900	-0.01020	0.01204	0.03629	0.00251			
			2.58700	-0.00821	-0.01443	0.01149	0.03633	0.00130			
			4.85400	0.01539	-0.01855	0.01274	0.03401	-0.00110			
			7.19600	0.03137	-0.01471	0.01529	0.02939	-0.00360			
			9.47100	0.00143	-0.00920	0.01334	0.01868	-0.00434			
			11.71000	-0.00534	-0.00076	0.01229	0.01979	-0.00518			
			14.01200	-0.01729	0.00463	0.00941	0.01709	-0.00423			
			16.25099	-0.00519	0.00759	0.01124	0.01747	-0.00545			
			18.45999	-0.00461	0.00056	0.01168	0.01435	-0.00469			
0.85	OUTBD	20/-20	-1.96000	-0.04132	0.01942	0.00801	0.03391	0.00262	PWT 16T	83	51
			-0.92100	-0.02775	0.01096	0.00892	0.03510	0.00199			
			0.16900	-0.01667	0.00470	0.00899	0.03469	0.00061			
			1.47600	-0.01460	0.00111	0.00888	0.03449	-0.00048			
			2.55800	-0.01316	-0.00151	0.00866	0.03432	-0.00120			
			3.62200	0.00139	-0.00744	0.00661	0.03349	-0.00210			
			3.66200	0.00363	-0.00706	0.00660	0.03350	-0.00200			
			4.93900	0.01597	-0.01500	0.00909	0.03042	-0.00300			
			7.24200	0.02346	-0.00974	0.00983	0.02519	-0.00420			
			8.42000	0.01140	-0.00490	0.00916	0.02488	-0.00477			
			9.90400	0.02027	-0.00257	0.01058	0.02176	-0.00516			
			10.66800	0.01339	0.00112	0.00936	0.02010	-0.00517			
			11.59400	0.01624	-0.00007	0.01093	0.01810	-0.00490			
			13.91700	0.00122	-0.00010	0.00867	0.01704	-0.00441			
			16.26099	0.00807	0.00362	0.01014	0.01696	-0.00495			
			18.33099	0.00766	0.00126	0.01075	0.01590	-0.00510			

Table VII CONT'D

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.9	MID	20/-20	-2.01700	-0.03061	0.01165	0.01347	0.03491	0.00601	PWT 16T	8	52
			0.28100	-0.01266	0.00001	0.01372	0.03420	0.00330			
			2.66200	0.01385	-0.01489	0.01276	0.03068	0.00060			
			5.02800	0.03485	-0.01504	0.01306	0.02642	-0.00181			
			7.37200	0.00515	0.00281	0.01243	0.02611	-0.00390			
			9.62700	-0.01667	0.00159	0.01034	0.02482	-0.00538			
			11.90900	-0.02808	0.00513	0.00885	0.01107	-0.00262			
			14.08800	-0.01732	0.00738	0.00852	0.01572	-0.00423			
			16.43300	-0.00841	0.00099	0.01213	0.01127	-0.00218			
			18.70999	-0.00596	0.00290	0.01140	0.00904	-0.00249			
			20.83099	-0.01086	0.00333	0.00943	0.00876	-0.00673			
0.9	OUTBD	20/-20	-2.00800	-0.04861	0.02341	0.00943	0.03431	0.00271	PWT 16T	81	52
			-0.97400	-0.03087	0.01761	0.00956	0.03330	0.00150			
			0.38500	-0.02384	0.01084	0.00905	0.03343	0.00021			
			1.44200	-0.00820	0.00280	0.00912	0.03235	-0.00072			
			2.61400	0.00792	-0.00569	0.00887	0.02805	-0.00170			
			3.81100	0.01867	-0.00560	0.00724	0.02459	-0.00240			
			4.92200	0.01675	-0.00509	0.00947	0.02371	-0.00300			
			7.31500	-0.00065	0.00849	0.00818	0.02310	-0.00440			
			8.40700	-0.00115	0.00974	0.00850	0.02259	-0.00460			
			9.59900	-0.01192	0.01579	0.00599	0.01862	-0.00470			
			10.71400	0.01306	0.01769	0.00821	0.00797	-0.00224			
			11.71500	-0.00535	0.00134	0.00693	0.01137	-0.00301			
			14.04100	-0.00461	0.00200	0.00733	0.01797	-0.00597			
			16.27899	-0.00189	-0.00020	0.00884	0.01319	-0.00380			
			18.54099	0.00471	0.00347	0.01002	0.01069	-0.00319			
			20.75400	-0.00393	0.00577	0.00662	0.01124	-0.00499			

Table VII CONT'D

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
1.2	MID	20/-20	-2.09100	0.01268	0.00251	0.01264	0.01681	0.00556	PWT 16T	10	54
			-0.92000	0.01296	0.00469	0.01305	0.01799	0.00520			
			0.26600	0.01609	0.00476	0.01350	0.01937	0.00416			
			1.37200	0.02001	0.00157	0.01454	0.02111	0.00240			
			2.59800	0.01863	0.00553	0.01450	0.02254	0.00172			
			4.92100	0.01356	0.01385	0.01596	0.02180	0.0			
			7.16600	0.00287	0.02247	0.01417	0.02061	-0.00181			
			9.49100	-0.00267	0.02419	0.01357	0.01960	-0.00320			
			12.03400	-0.01231	0.02533	0.01065	0.02001	-0.00572			
			14.36500	-0.02470	0.03279	0.00748	0.01910	-0.00730			
			16.59800	-0.02844	0.03821	0.00542	0.01827	-0.00907			
			18.55659	-0.03617	0.03709	0.00095	0.01740	-0.00930			
1.2	OUTBD'	20/-20	-3.11800	-0.00116	0.00025	0.00902	0.02142	0.00064	PWT 16T	82	54
			-2.08600	0.00209	-0.00319	0.00926	0.02161	0.00046			
			-0.88300	0.00318	-0.00362	0.00924	0.02220	0.00012			
			0.19100	0.00709	-0.00436	0.00964	0.02284	-0.00002			
			1.29900	0.00910	-0.00446	0.00993	0.02359	-0.00069			
			2.39800	0.01010	-0.00276	0.01039	0.02420	-0.00130			
			3.64000	0.01055	-0.00223	0.00804	0.02445	-0.00190			
			4.71000	0.01080	0.00051	0.01022	0.02376	-0.00241			
			7.10800	0.00343	0.00954	0.01025	0.02160	-0.00360			
			8.30500	0.00277	0.00926	0.00995	0.02090	-0.00450			
			9.65400	0.00750	0.00914	0.01038	0.01978	-0.00562			
			10.67300	0.00309	0.01030	0.00966	0.01911	-0.00639			
			11.87600	0.00181	0.01092	0.00943	0.01820	-0.00690			
			14.29300	-0.00024	0.01132	0.00834	0.01659	-0.00829			
			16.63300	0.00006	0.00798	0.00786	0.01545	-0.00846			
			18.78859	-0.00018	0.00611	0.00824	0.01375	-0.00844			

Table VIII AILERON CONTROL LINEARITY INCREMENTAL DATA SUMMARY

L.E. Deflected 0^0 — Horzontal Tail On

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	DATA RUN	BASE RUN
0.7	MID	10/-10	-2.10200	0.00319	-0.00221	0.00261	0.01910	0.00400	PWT 4T	475	438
			0.24800	0.00678	-0.00825	0.00330	0.01929	0.00239			
			2.44900	0.00715	-0.01221	0.00410	0.01920	0.00100			
			4.73500	0.00626	-0.01277	0.00404	0.01890	-0.00030			
			7.04800	0.00330	-0.00907	0.00275	0.01826	-0.00191			
			9.21000	-0.00402	-0.00485	0.00305	0.01558	-0.00270			
			11.43400	-0.00871	-0.00295	0.00193	0.01401	-0.00351			
			13.56200	-0.00694	0.00053	0.00197	0.01170	-0.00400			
			15.71600	-0.00856	-0.00397	0.00138	0.01169	-0.00460			
0.7	MID	20/-20	0.15600	-0.02873	-0.00052	0.01048	0.03660	0.00460	PWT 4T	410	438
			2.39600	-0.02222	-0.00816	0.00991	0.03631	0.00211			
			4.67100	-0.02511	-0.00940	0.00971	0.03550	-0.00030			
			6.98000	-0.02488	-0.00475	0.00900	0.03370	-0.00340			
			9.25300	-0.02073	-0.00224	0.00893	0.02908	-0.00560			
			11.38400	-0.02026	-0.00609	0.00870	0.02160	-0.00660			
			13.61200	-0.02419	0.00849	0.00594	0.02282	-0.00831			
			15.72500	-0.02897	0.00496	0.00320	0.02019	-0.00840			
			17.78600	-0.02150	0.00217	0.00493	0.01712	-0.00781			
0.8	MID	10/-10	0.23200	0.00057	-0.00806	0.00388	0.01820	0.00250	PWT 4T	476	440
			2.54200	0.00401	-0.01279	0.00441	0.01820	0.00110			
			4.92800	0.00349	-0.01435	0.00392	0.01858	-0.00040			
			7.25300	0.00516	-0.01085	0.00293	0.01712	-0.00181			
			9.45100	-0.01683	0.00188	0.00098	0.01451	-0.00261			
			11.60800	-0.00102	-0.00710	0.00366	0.01018	-0.00281			
			13.80800	-0.00993	0.00126	0.00159	0.01260	-0.00370			
			15.90900	-0.00976	0.00142	0.00153	0.01030	-0.00310			

Table VIII CONT'D

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.8	MID	20/-20	0.21100	-0.02405	-0.00230	0.01188	0.03510	0.00450	PWT 4T	411	440
			2.43000	-0.01745	-0.01022	0.01180	0.03481	0.00201			
			4.81100	-0.01771	-0.01323	0.01086	0.03470	-0.00070			
			7.13300	-0.00615	-0.01096	0.01175	0.03174	-0.00329			
			9.42900	-0.00620	-0.01036	0.01294	0.02350	-0.00490			
			11.56300	-0.01243	-0.00431	0.01012	0.01940	-0.00590			
			13.76800	-0.02487	0.00331	0.00868	0.02240	-0.00720			
			15.91000	-0.02212	0.00585	0.00849	0.01950	-0.00670			
			18.09698	-0.02490	0.01076	0.00645	0.01731	-0.00660			
0.9	MID	10/-10	0.28000	-0.00329	-0.00701	0.00502	0.01470	0.00170	PWT 4T	474	441
			2.67300	0.00928	-0.01504	0.00787	0.01440	0.00060			
			5.05400	0.01199	-0.01254	0.00673	0.01299	-0.00030			
			7.37100	0.00490	-0.00937	0.00644	0.01429	-0.00140			
			9.70700	-0.01137	-0.00377	0.00396	0.01571	-0.00270			
			11.81500	-0.03793	-0.00081	0.00014	0.01287	-0.00259			
			13.94000	-0.01295	0.00321	0.00108	0.01021	-0.00279			
			16.24300	-0.01639	0.00440	0.00082	0.00935	-0.00207			
0.9	MID	20/-20	0.22500	-0.02734	0.00131	0.01476	0.03260	0.00390	PWT 4T	412	441
			2.58000	-0.01328	-0.00879	0.01356	0.03250	0.00140			
			5.02400	0.01078	-0.01532	0.01263	0.02800	-0.00090			
			7.39600	0.01478	-0.01149	0.01466	0.02369	-0.00300			
			9.72000	-0.01748	-0.00656	0.01175	0.02083	-0.00371			
			11.79500	-0.04499	-0.00208	0.00767	0.01745	-0.00408			
			13.99100	-0.02532	0.00638	0.01001	0.01650	-0.00500			
			16.17099	-0.02351	0.00936	0.01115	0.01439	-0.00420			

Table VIII CONT'D

MACH	AILERON SPANWISE LOCAT'N	AILERON DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
1.2	MID	10/-10	-2.20800	0.00260	-0.00571	0.00358	0.00635	0.00250	PWT 4T	477	269
			0.20400	0.00249	-0.00073	0.00380	0.00797	0.00191			
			2.51000	0.00284	0.00467	0.00326	0.00965	0.00155			
			4.96900	0.00109	0.01313	0.00353	0.01045	0.00080			
			7.35200	-0.00563	0.02642	0.00298	0.01045	0.00020			
			9.65700	-0.01201	0.03560	0.00059	0.01095	-0.00045			
			11.99100	-0.01489	0.03941	-0.00050	0.01139	-0.00166			
			14.29600	-0.01656	0.03943	-0.00154	0.01175	-0.00235			
			16.51399	-0.02299	0.04915	-0.00465	0.01299	-0.00300			
			18.70799	-0.02611	0.05034	-0.00597	0.01288	-0.00358			
1.2	MID	20/-20	-2.23100	-0.00280	0.00129	0.01236	0.01615	0.0[illegible]500	PWT 4T	414	269
			-2.22600	-0.00326	-0.00173	0.01259	0.01635	0.00500			
			0.21000	0.00060	0.00601	0.01239	0.01857	0.00331			
			2.48200	0.00483	0.00919	0.01274	0.02134	0.00176			
			4.96300	0.00390	0.01877	0.01364	0.02165	0.00040			
			7.32500	-0.01127	0.03881	0.01176	0.01985	-0.00100			
			9.70000	-0.02276	0.05163	0.00771	0.01895	-0.00295			
			12.05800	-0.02593	0.04980	0.00640	0.01960	-0.00465			
			14.30700	-0.03129	0.05634	0.00397	0.01935	-0.00565			
			16.51500	-0.03836	0.06329	0.00060	0.02040	-0.00750			
			18.67599	-0.04338	0.06915	-0.00186	0.01949	-0.00849			
			20.90999	-0.04144	0.06974	-0.00250	0.01963	-0.01115			

Table IX HORIZONTAL TAIL / AILERON CONTROL INTERFERENCE INCREMENTAL DATA SUMMARY

Intermediate Aileron Deflection — L.E. Flap Deflected 10^0

MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL L/R							TUNNEL	TAIL ON RUN	TAIL OFF RUN
0.7	INBD	10/ -10	-1.01500	-0.01614	0.01670	0.00034	-0.00980	-0.00079	PWT 4T	121	114
			-1.01100	-0.01413	0.01630	0.00127	-0.00970	-0.00060			
			1.31000	-0.00577	0.00340	0.00019	-0.01070	-0.00659			
			3.55400	0.00934	-0.02255	0.00179	-0.00992	-0.00179			
			5.90600	0.02771	-0.05967	0.00440	-0.00937	-0.00177			
			8.07600	0.05438	-0.10208	0.00967	-0.00905	-0.00135			
			10.40900	0.07723	-0.15098	0.01645	-0.00881	-0.00061			
			12.53100	0.12019	-0.21953	0.02962	-0.00813	-0.00003			
			14.76600	0.15809	-0.29009	0.04540	-0.00869	0.00080			
			16.82100	0.20202	-0.36608	0.04810	-0.00779	0.00088			
			19.04999	0.25606	-0.45540	0.09125	-0.00700	0.00040			
0.8	INBD	10/ -10	-3.30500	-0.01640	0.01661	0.00145	-0.00911	-0.00011	PWT 4T	120	113
			-1.01900	-0.01415	0.01299	0.00084	-0.00989	-0.00199			
			1.28000	-0.00603	0.00269	0.00051	-0.01045	-0.00220			
			3.63900	0.00455	-0.01910	0.00192	-0.01023	-0.00185			
			5.98600	0.02209	-0.05549	0.00413	-0.01002	-0.00173			
			8.23500	0.03692	-0.09074	0.00790	-0.01042	-0.00124			
			10.53700	0.16387	-0.14420	0.01436	-0.00931	-0.00004			
			12.79000	0.10975	-0.21223	0.02817	-0.00628	0.00067			
			14.94000	0.15431	-0.29387	0.04497	-0.00668	0.00051			
0.9	INBD	10/ -10	-1.04100	-0.00906	0.00573	0.00193	-0.00930	-0.00209	PWT 4T	119	112
			1.33400	-0.00761	0.00867	0.00090	-0.01018	-0.00279			
			3.75300	-0.00518	-0.00906	0.00065	-0.00979	-0.00269			
			6.10500	0.00910	-0.04190	0.00220	-0.00930	-0.00230			
			8.26600	0.02614	-0.08299	0.00450	-0.00822	-0.00159			
			10.67700	0.05638	-0.14182	0.01266	-0.00602	-0.00053			
			12.93800	0.10032	-0.22727	0.02619	-0.01106	0.00156			
			15.18300	0.16813	-0.32691	0.04897	-0.00744	-0.00088			

Table IX CONT'D

MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL L/R							TUNNEL	TAIL ON RUN	TAIL OFF RUN
0.9	MID	10/ -10	-1.06600	-0.00920	0.00522	0.00262	-0.00449	-0.00099	PWT 4T	133	108
			1.33000	-0.00611	0.00267	0.00240	-0.00308	-0.00080			
			3.73200	-0.00390	-0.00220	0.00159	-0.00480	-0.00050			
			6.09300	0.02180	-0.03500	0.00676	-0.00461	-0.00030			
			8.39800	0.04976	-0.08710	0.01014	-0.00151	-0.00070			
			10.68500	0.08559	-0.15555	0.01900	0.00080	-0.00090			
			12.90500	0.12537	-0.23231	0.03188	-0.00071	-0.00021			
			15.17400	0.17366	-0.31033	0.04942	-0.00104	-0.00011			
1.2	INBD	10/ -10	-3.46000	-0.05914	0.09920	0.00690	-0.00860	-0.00260	PWT 4T	122	115
			-1.14200	-0.02937	0.05260	0.00431	-0.00841	-0.00250			
			1.18400	0.00515	-0.00956	0.00540	-0.00769	-0.00220			
			3.54800	0.04479	-0.07459	0.00854	-0.00839	-0.00101			
			5.98100	0.08157	-0.14392	0.01353	-0.00819	-0.00013			
			8.36700	0.12151	-0.21891	0.02344	-0.00753	0.00126			
			10.71300	0.16941	-0.30487	0.03746	-0.00654	0.00255			
			12.94800	0.21431	-0.39254	0.05515	-0.00553	0.00267			
			15.35100	0.26235	-0.48780	0.07809	-0.00490	0.00331			

Table X HORIZONTAL TAIL / AILERON CONTROL INTERFERENCE INCREMENTAL DATA SUMMARY

High Aileron Deflection — L.E. Flap Deflected 10^0

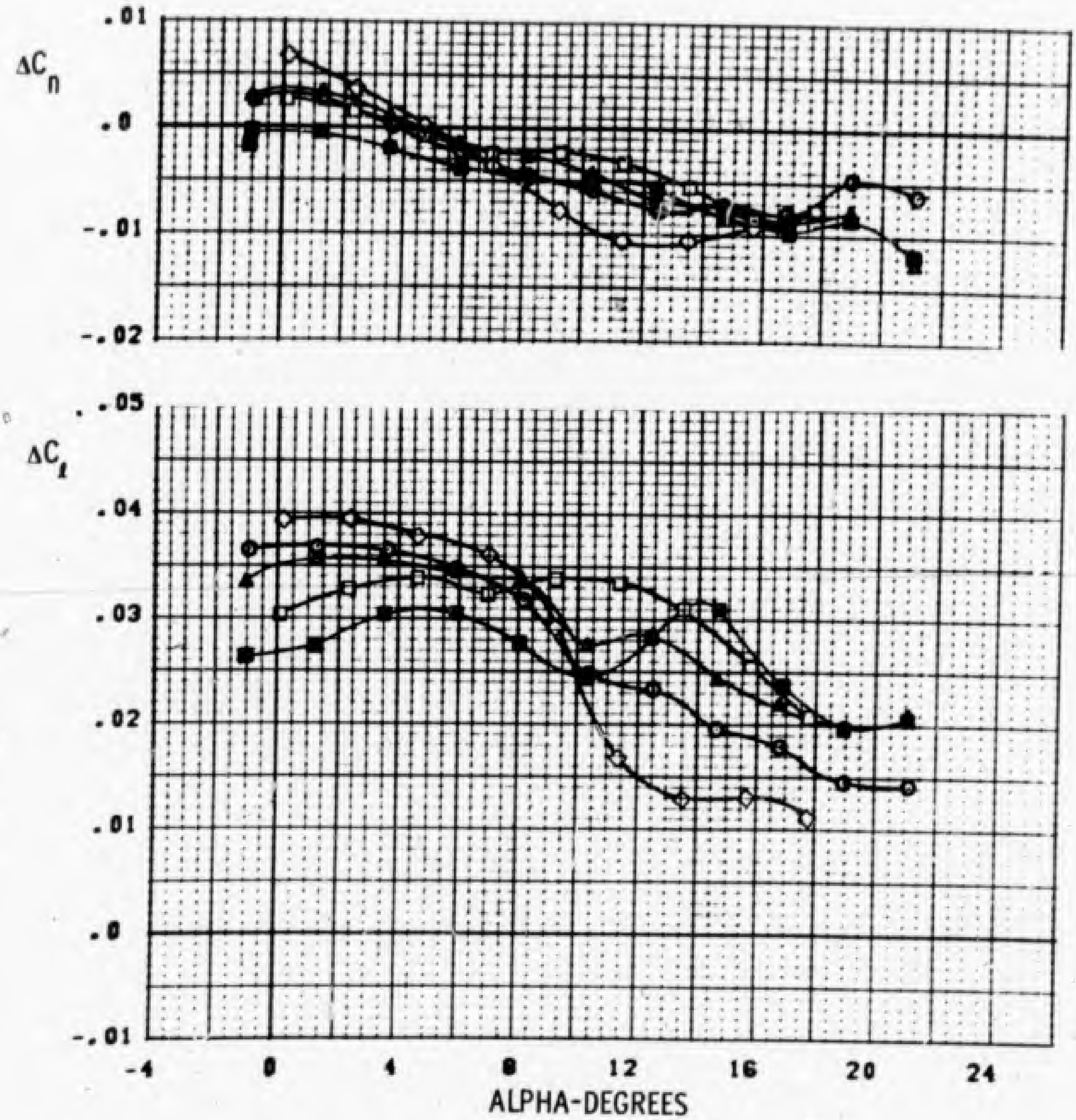
MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL L/R							TUNNEL	TAIL ON RUN	TAIL OFF RUN
C.7	MID	20/ -20	-1.00600	0.00066	0.00187	-0.00046	-0.00905	-0.00149	PWT 4T	285	499
			1.11900	0.01764	-0.02630	0.00107	-0.00980	-0.00168			
			3.26400	0.03829	-0.05871	0.00314	-0.00996	-0.00194			
			5.45000	0.05917	-0.09566	0.00688	-0.01071	-0.00232			
			7.61100	0.08038	-0.13015	0.01229	-0.00965	-0.00257			
			9.62300	0.08122	-0.17256	0.01812	-0.01048	-0.00192			
			11.85400	0.09388	-0.22802	0.02392	-0.00828	-0.00158			
			13.90600	0.12510	-0.28815	0.03497	-0.00726	-0.00161			
			16.01299	0.18435	-0.37687	0.05666	-0.00616	-0.00209			
			18.04900	0.24354	-0.47333	0.08206	-0.00455	-0.00327			
			20.14600	0.30439	-0.56225	0.11491	-0.00536	-0.00310			
			22.16299	0.34399	-0.62467	0.14303	-0.00625	-0.00272			
0.8	MID	20/ -20	-1.01000	-0.00112	0.00612	0.00023	-0.00859	-0.00169	PWT 4T	284	500
			1.15500	0.01312	-0.02056	0.00138	-0.00964	-0.00196			
			3.40700	0.02734	-0.05331	0.00404	-0.01020	-0.00208			
			5.54700	0.04372	-0.08447	0.00686	-0.01056	-0.00236			
			7.68600	0.05555	-0.11400	0.01196	-0.01139	-0.00224			
			9.87500	0.07320	-0.16163	0.01835	-0.00861	-0.00184			
			11.94100	0.10852	-0.22502	0.02874	-0.00637	-0.00209			
			14.03300	0.14205	-0.30485	0.04176	-0.00487	-0.00246			
			16.12299	0.19338	-0.39043	0.06049	-0.00509	-0.00305			
			18.28600	0.26643	-0.49658	0.09378	-0.00357	-0.00510			
			20.40700	0.32413	-0.58129	0.12711	-0.00460	-0.00484			
			22.30199	0.36793	-0.64678	0.15838	-0.00591	-0.00395			

Table X CONT'D

MACH	AILERON		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	SPANWISE LOCAT'N	DEFL L/R							TUNNEL	TAIL ON RUN	TAIL OFF RUN
C.9	MID	20/-20	-0.95600	-0.00359	0.01494	0.00216	-0.00900	-0.00192	PWT 4T	283	501
			1.22000	0.01072	-0.00587	0.00022	-0.00975	-0.00183			
			3.43200	0.01976	-0.02445	0.00125	-0.01006	-0.00191			
			5.67100	0.02538	-0.03841	0.00439	-0.01124	-0.00184			
			7.91800	0.02238	-0.05823	0.00637	-0.01323	-0.00140			
			10.00800	0.04277	-0.12473	0.00972	-0.01231	-0.00081			
			12.03300	0.08690	-0.20143	0.02271	-0.00468	-0.00140			
			14.10200	0.14614	-0.30430	0.04283	-0.00374	-0.00267			
			16.26900	0.20451	-0.40784	0.06422	-0.00381	-0.00239			
			18.42899	0.26067	-0.49961	0.09221	-0.00293	-0.00546			
			20.40399	0.32711	-0.58328	0.12710	-0.00339	-0.00698			
			22.44699	0.37867	-0.65804	0.16124	-0.00485	-0.00612			
1.2	MID	20/-20	-1.01200	-0.02330	0.05015	0.00246	-0.00672	-0.00044	PWT 4T	286	502
			-1.00300	-0.02148	0.04508	0.00336	-0.00593	-0.00044			
			1.15600	0.00637	-0.00829	0.00295	-0.00667	-0.00092			
			3.43600	0.03457	-0.07009	0.00624	-0.00615	-0.00104			
			5.72400	0.06444	-0.13141	0.01220	-0.00673	-0.00082			
			7.79500	0.08952	-0.18873	0.01854	-0.00677	0.00003			
			9.99600	0.12518	-0.26208	0.02666	-0.00576	0.00088			
			10.12300	0.12510	-0.26734	0.02882	-0.00565	0.00052			
			12.16500	0.16738	-0.34988	0.04451	-0.00451	0.00020			
			14.37300	0.20580	-0.44033	0.06195	-0.00369	0.00042			
			16.46300	0.23871	-0.52334	0.07970	-0.00335	0.00012			
			18.62399	0.28085	-0.60949	0.10395	-0.00360	0.0			
			20.70200	0.30781	-0.68924	0.12671	-0.00378	-0.00018			
			22.70399	0.34649	-0.77282	0.15456	-0.00377	0.00056			

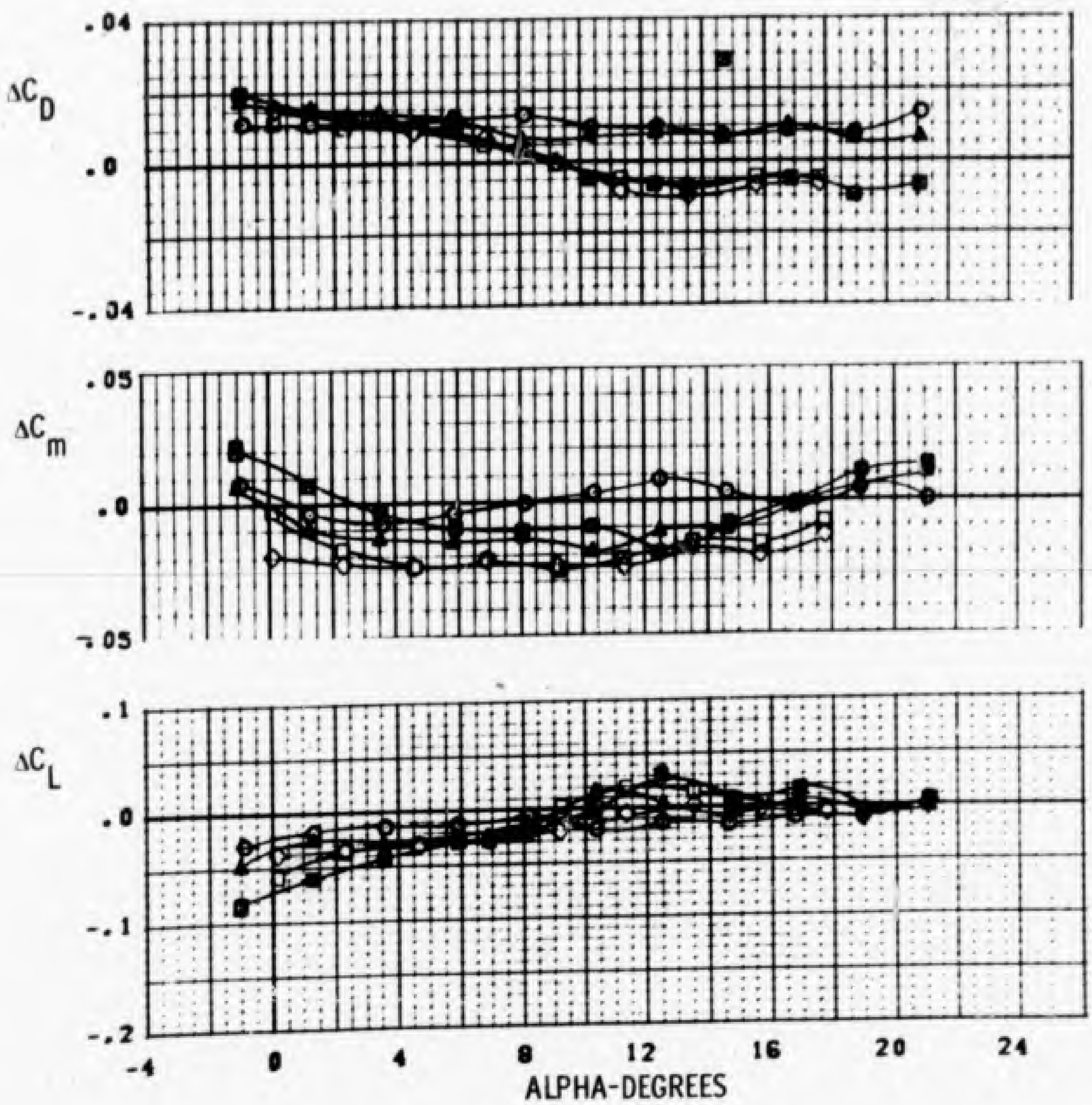
3. COMBINED LEADING AND TRAILING EDGE DEVICES

Incremental force and moment characteristics for aileron controls in combination with various differential leading edge deflections are given in this subsection. Data for ailerons with the undeflected leading edge is also included as a baseline for leading edge effects. Characteristics with the mid-span ailerons are illustrated in Figure 127 while Figure 128 is for the extended span ailerons (mid-span and tip trailing edge segments). Numerical values of the various force and moment increments are given in Tables XI and XII.



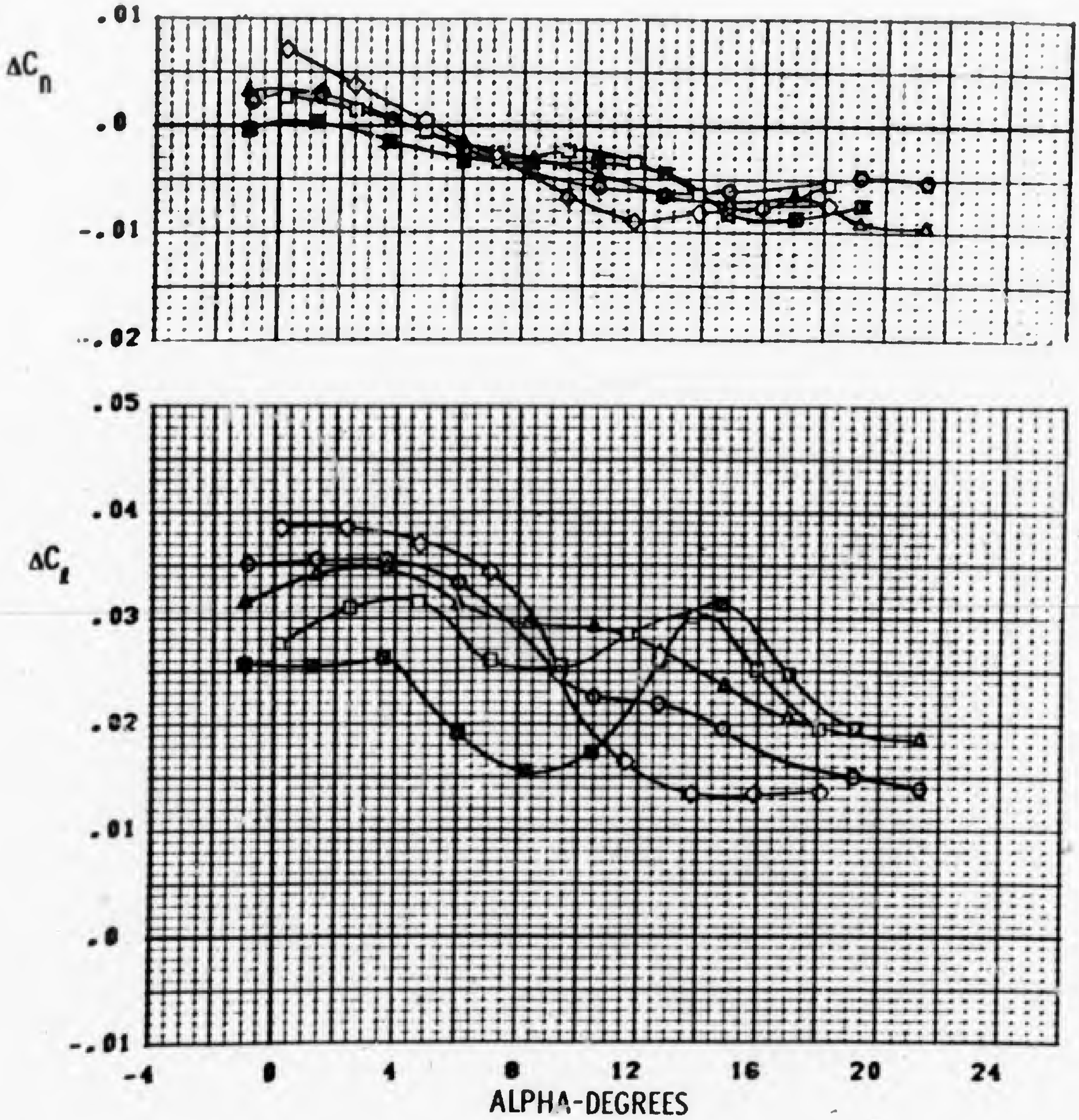
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 215 - PN 268	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 180 - PN 268	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 312 - PN 268	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 419 - PN 438	K1	0/10	MID	20/-20
⊡	PWT 4T TC-043	PN 426 - PN 438	K1	10/0	MID	20/-20

FIGURE 127a DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.7



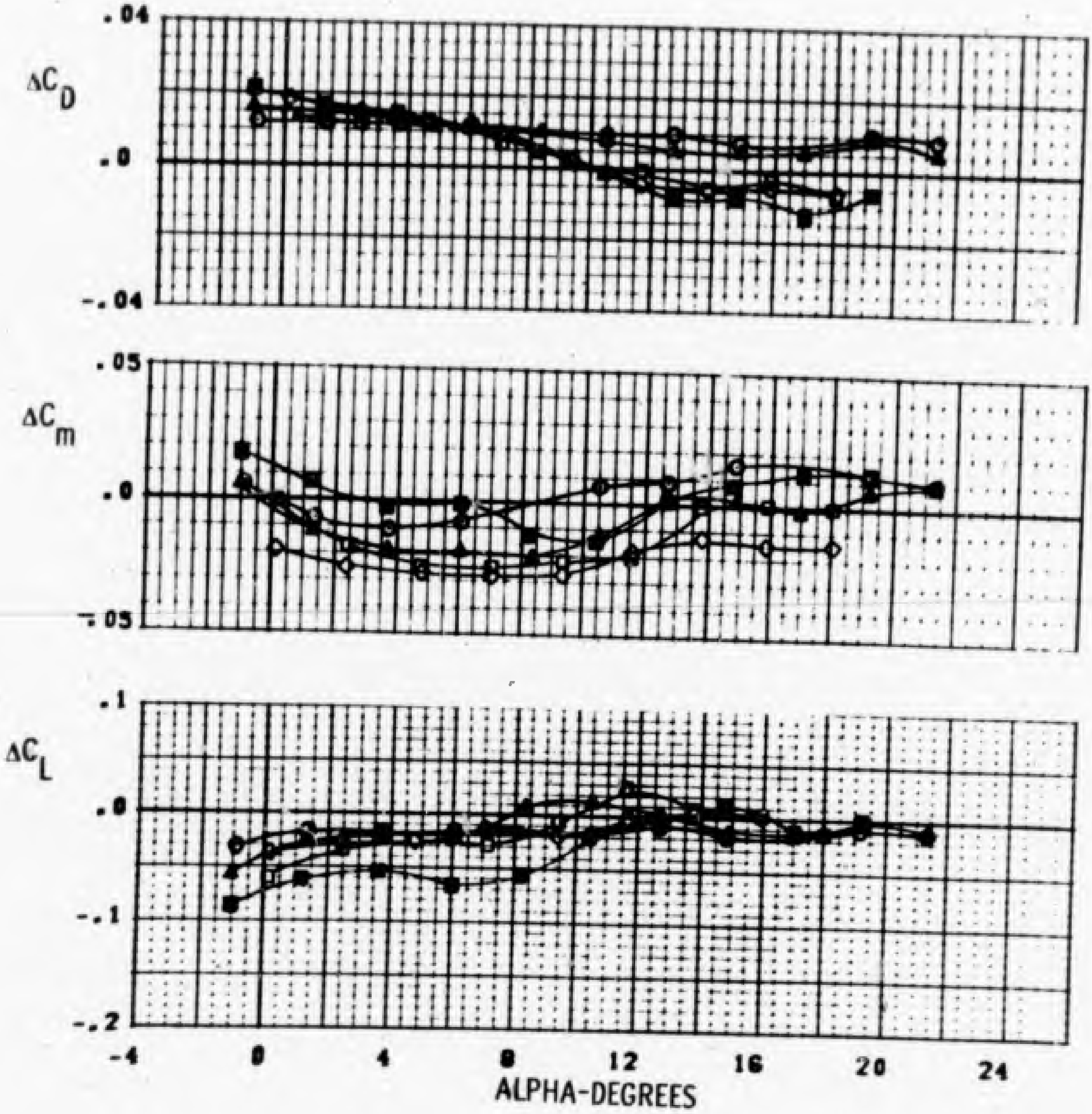
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 215 - PN 268	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 180 - PN 268	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 312 - PN 288	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 419 - PN 438	K1	0/10	MID	20/-20
◘	PWT 4T TC-043	PN 428 - PN 438	K1	10/0	MID	20/-20

FIGURE 127a DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.7



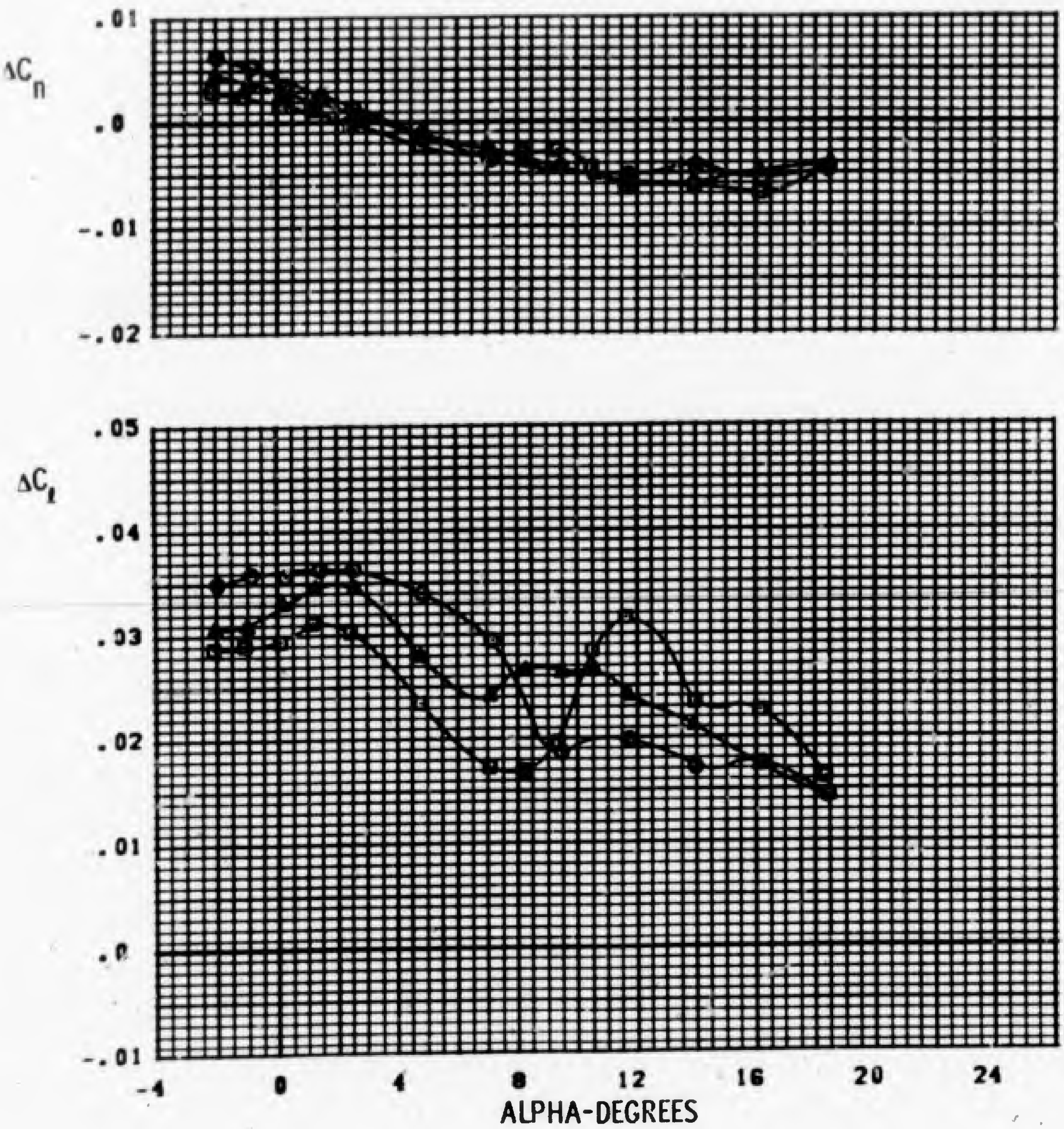
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 214 - PN 267	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 179 - PN 267	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 311 - PN 267	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 420 - PN 440	K1	0/10	MID	20/-20
⊡	PWT 4T TC-043	PN 427 - PN 440	K1	10/0	MID	20/-20

FIGURE 127b DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.8



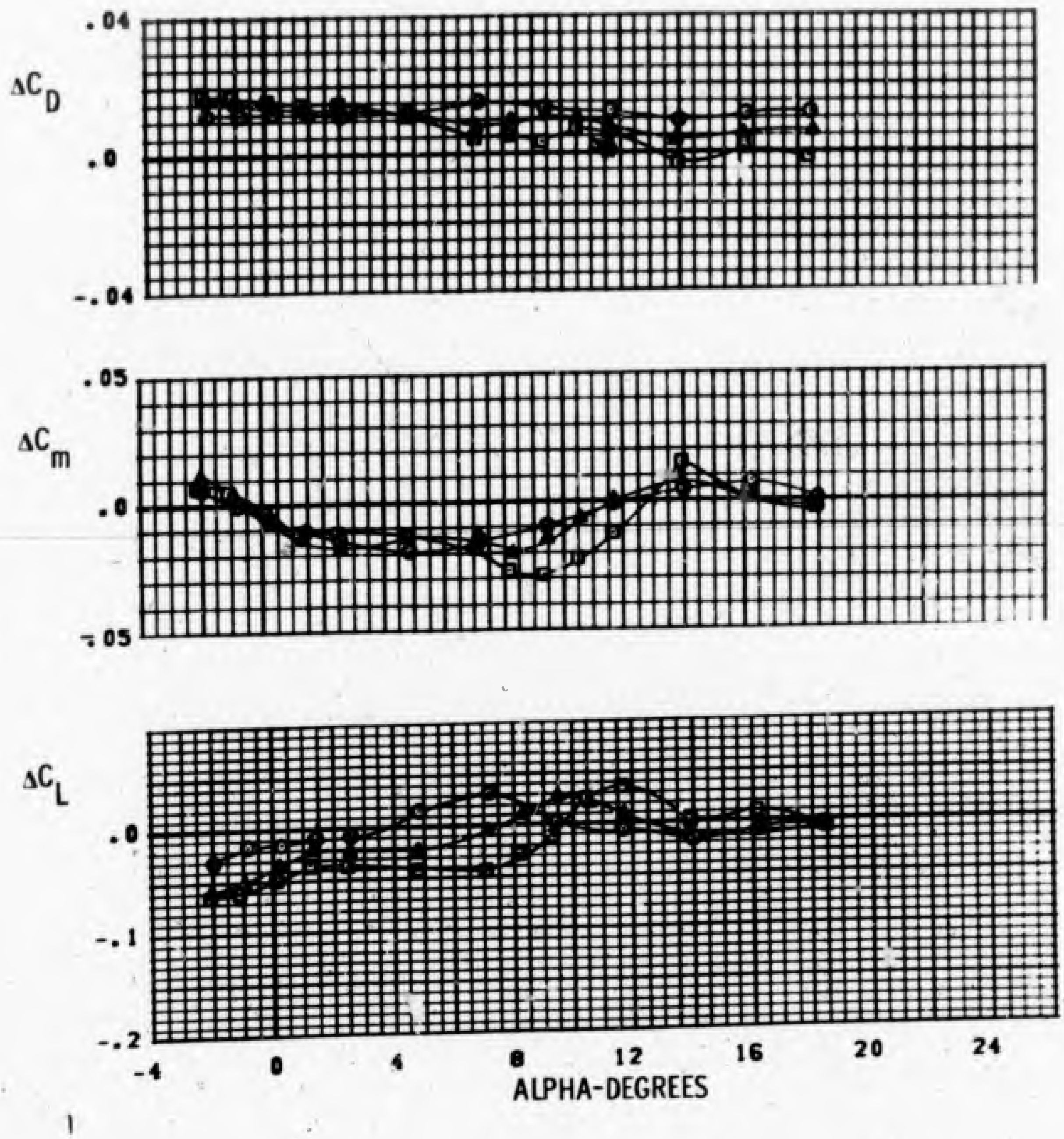
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON	(L/R)
○	PWT 4T TC-043	PN 214 - PN 267	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 179 - PN 267	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 311 - PN 267	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 420 - PN 440	K1	0/10	MID	20/-20
⊡	PWT 4T TC-043	PN 427 - PN 440	K1	10/0	MID	20/-20

FIGURE 127b DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.8



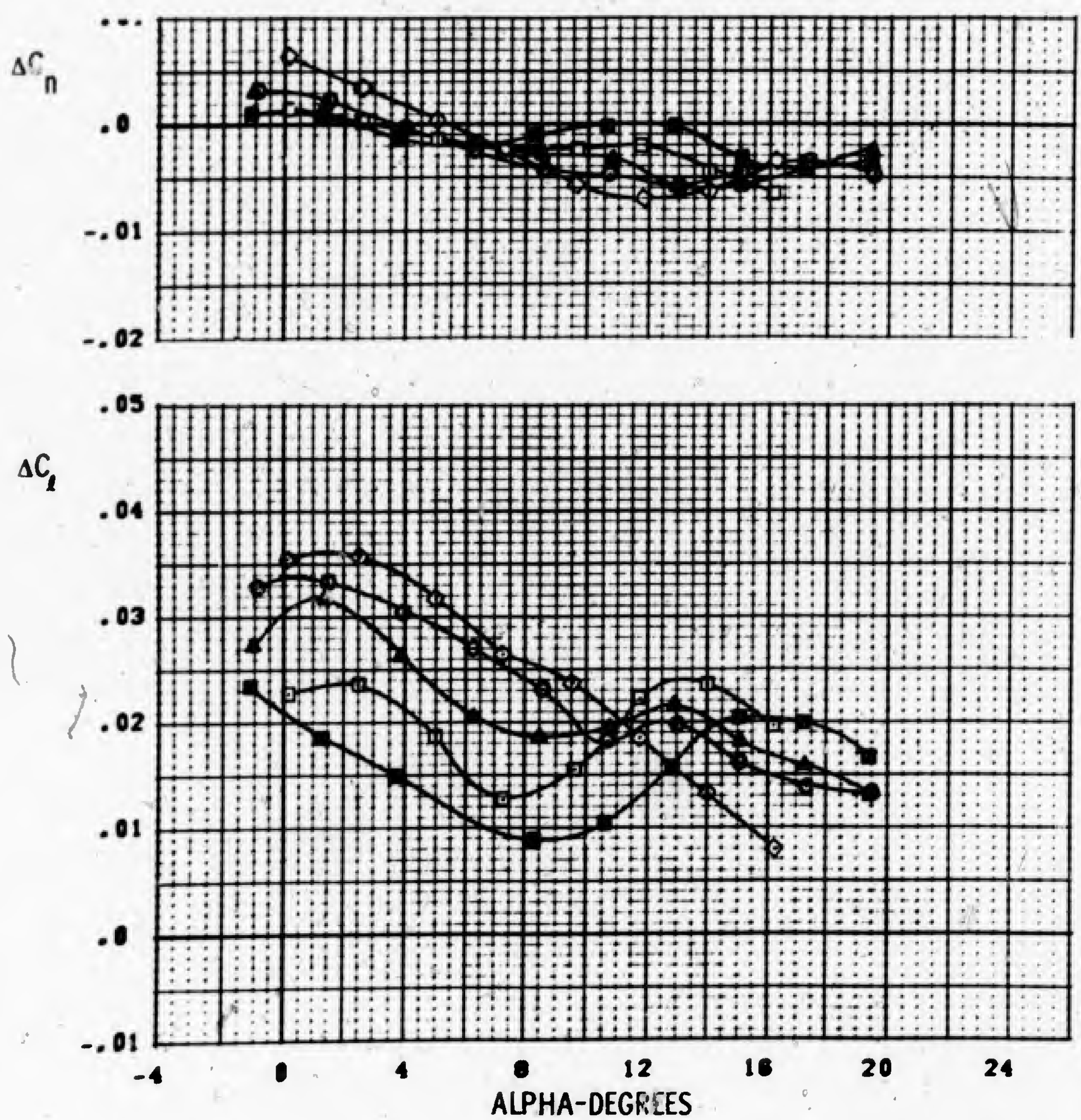
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 11 - PN 51	K1	0/0	MID	20/-20
⊡	PWT 16T TF-216	PN 32 - PN 51	K1	10/0	MID	20/-20
▲	PWT 16T TF-216	PN 26 - PN 51	K1	5/0	MID	20/-20

FIGURE 127c DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.85



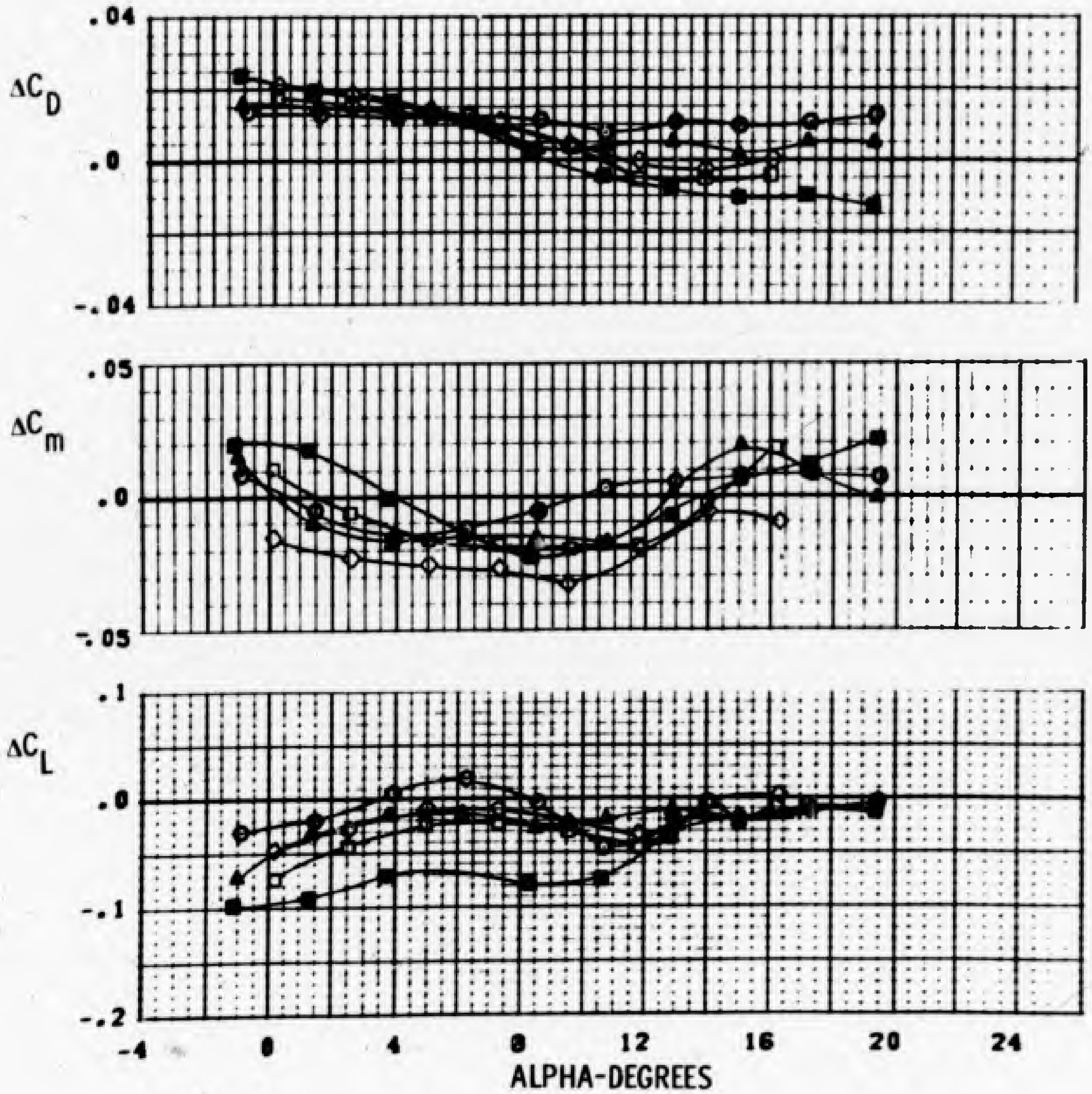
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 16T TF-216	PN 11 - PN 51	K1	0/0	MID	20/-20
⊡	PWT 16T TF-216	PN 32 - PN 51	K1	10/0	MID	20/-20
▲	PWT 16T TF-216	PN 26 - PN 51	K1	5/0	MID	20/-20

FIGURE 127c DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.85



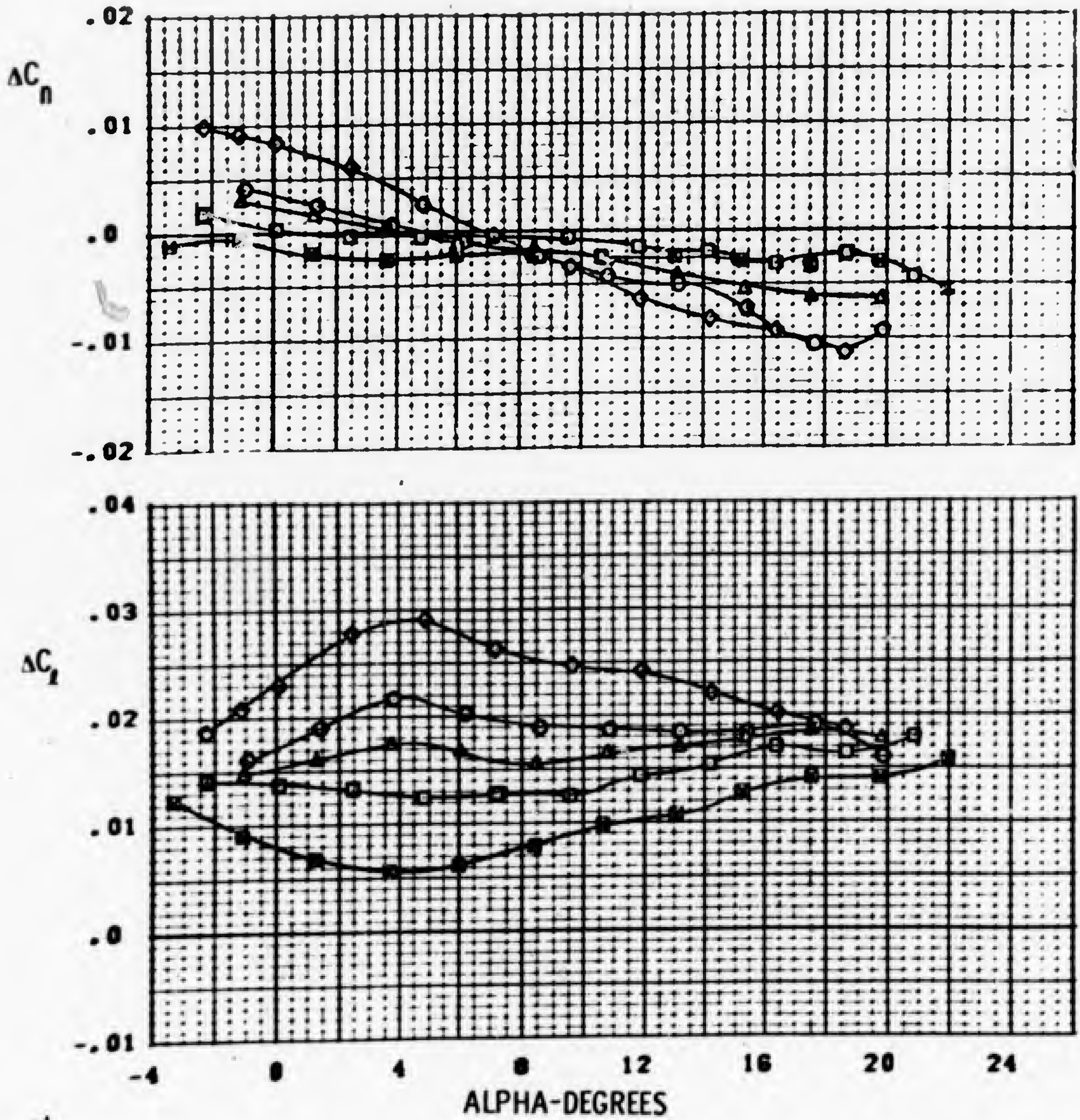
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 213 - PN 264	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 178 - PN 264	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 310 - PN 264	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 418 - PN 441	K1	0/10	MID	20/-20
⊡	PWT 4T TC-043	PN 425 - PN 441	K1	10/0	MID	20/-20

FIGURE 127d DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.9



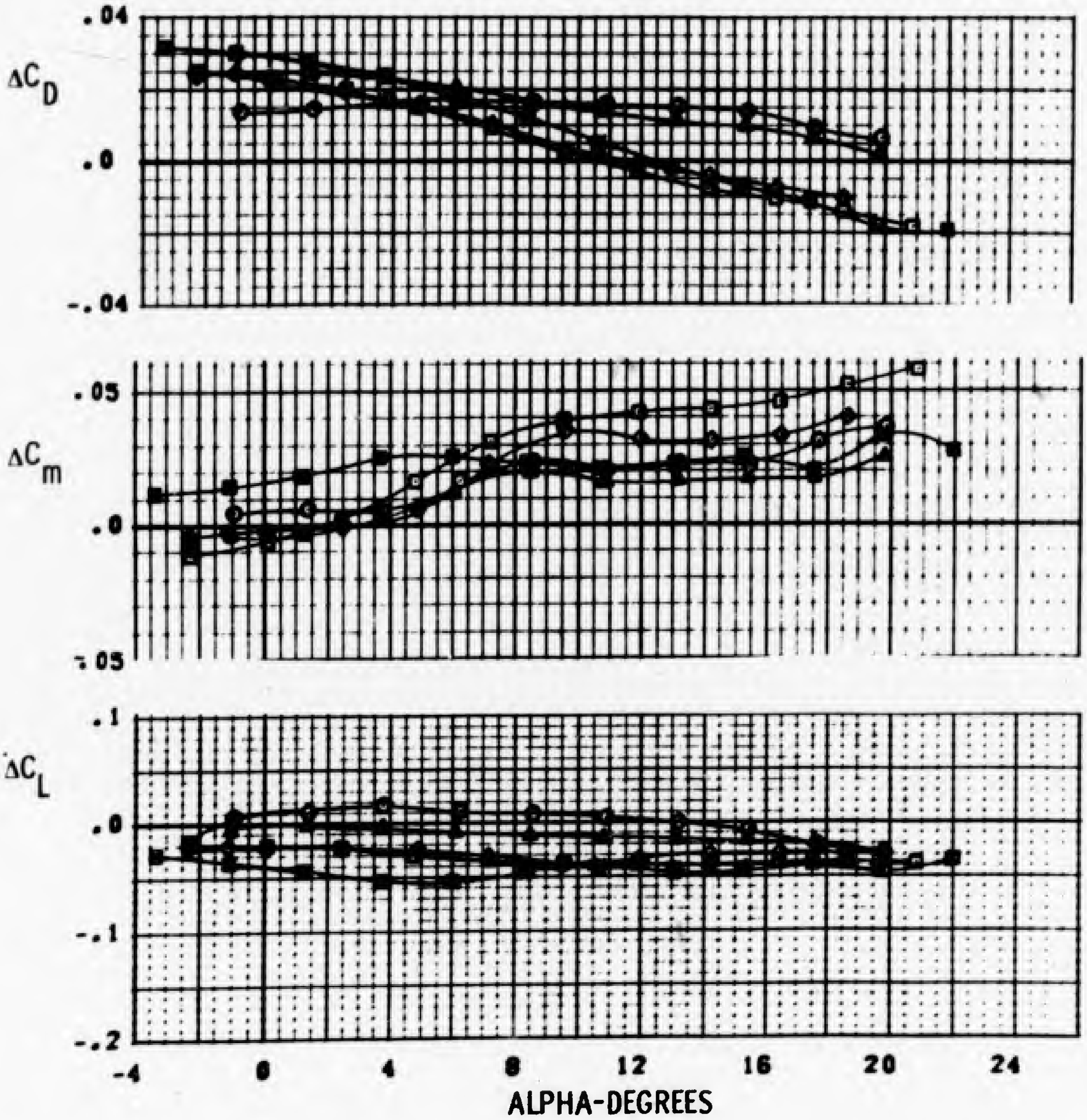
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 213 - PN 264	K1	0/0	MID	20/-20
■	PWT 4T TC-043	PN 178 - PN 264	K1	15/0	MID	20/-20
▲	PWT 4T TC-043	PN 310 - PN 264	K1	5/0	MID	20/-20
◇	PWT 4T TC-043	PN 418 - PN 441	K1	0/10	MID	20/-20
⊡	PWT 4T TC-043	PN 425 - PN 441	K1	10/0	MID	20/-20

FIGURE 127d DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 0.9



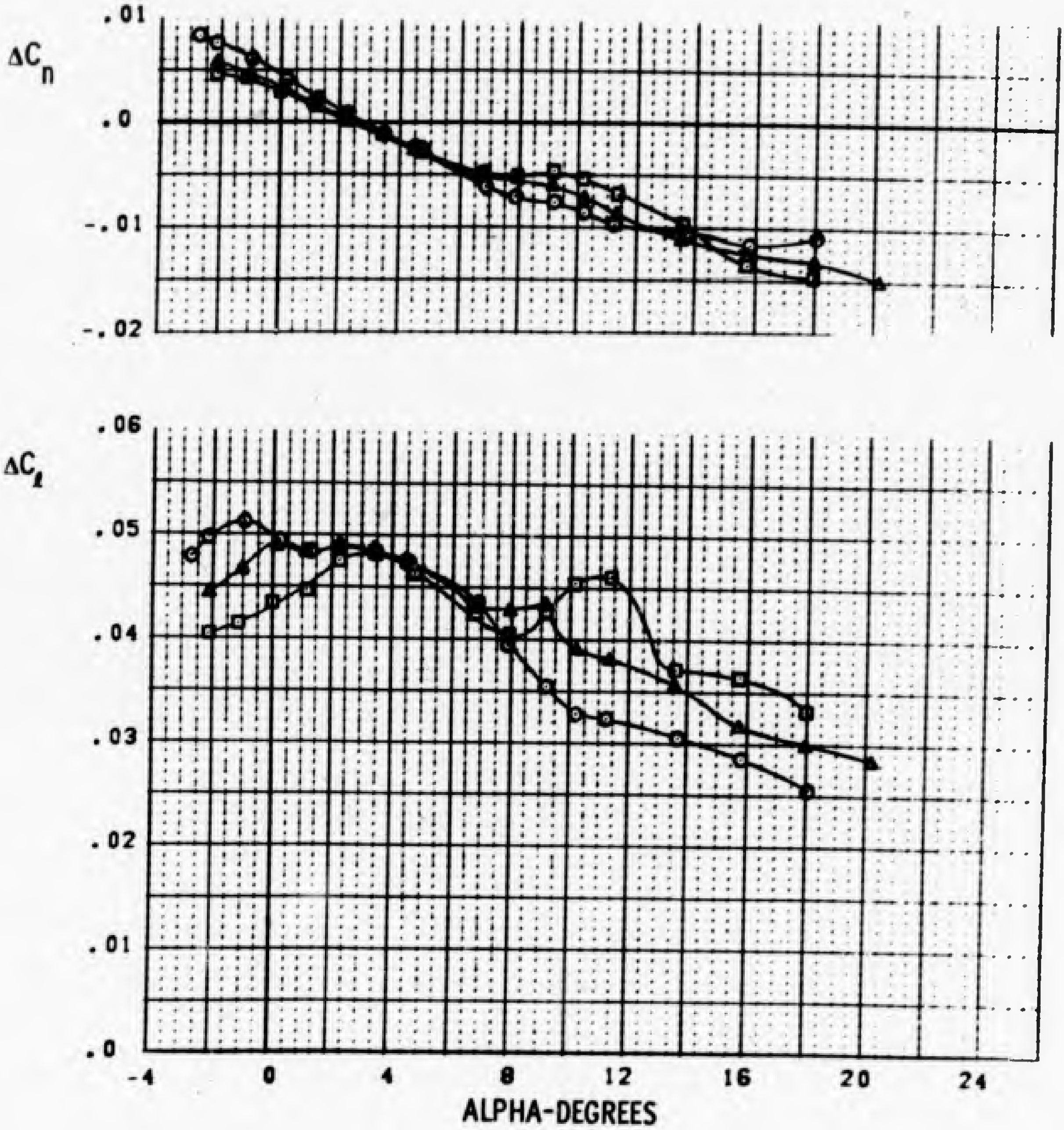
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 216 - PN 269	K1	0/0	MID	20/-20
□	PWT 4T TC-043	PN 428 - PN 269	K1	10/0	MID	20/-20
▲	PWT 4T TC-043	PN 313 - PN 269	K1	5/0	MID	20/-20
■	PWT 4T TC-043	PN 181 - PN 269	K1	15/0	MID	20/-20
◇	PWT 4T TC-043	PN 421 - PN 269	K1	0/10	MID	20/-20

FIGURE 127e DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 1.2



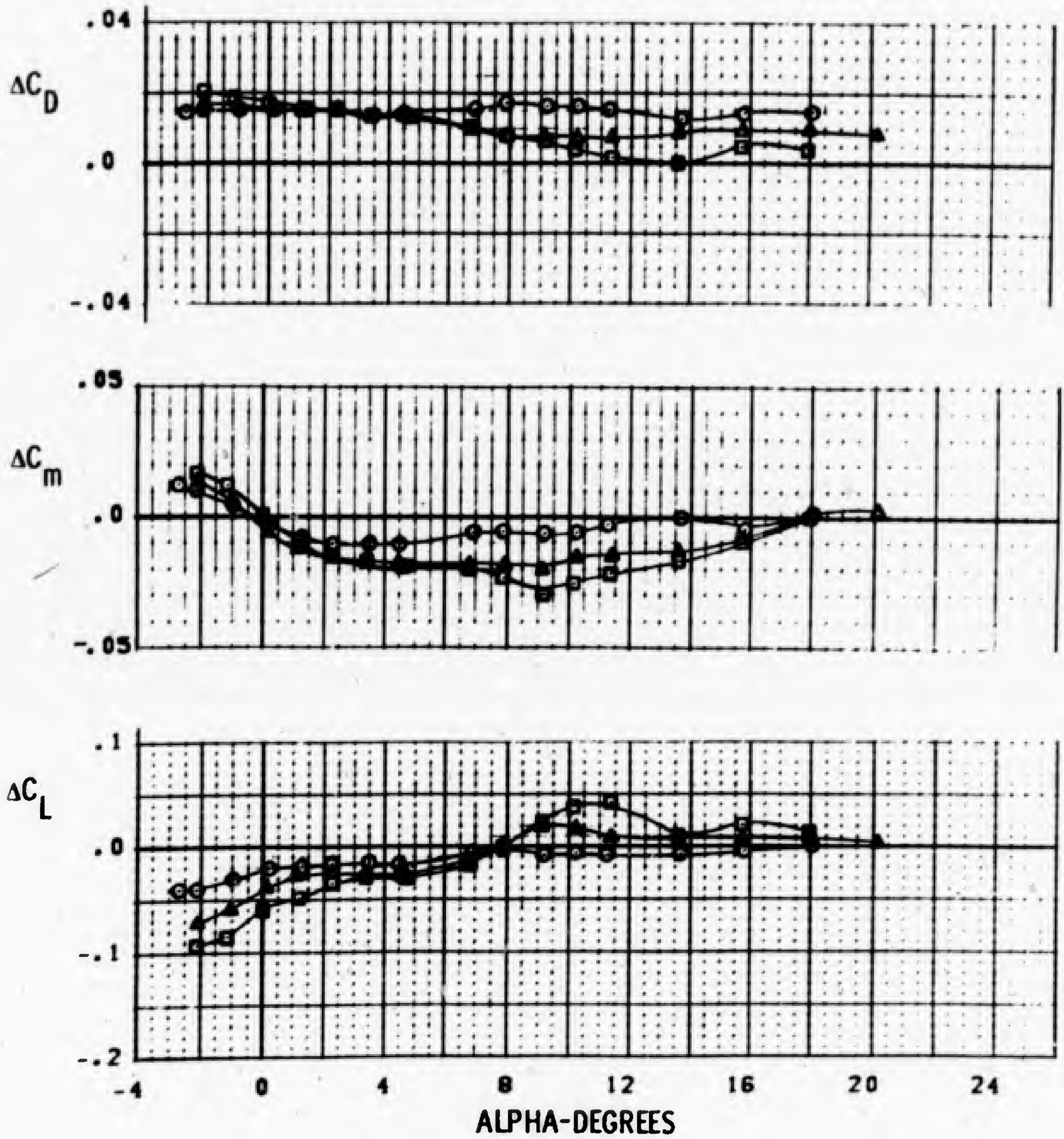
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 216 - PN 269	K1	0/0	MID	20/-20
⊡	PWT 4T TC-043	PN 428 - PN 288	K1	10/0	MID	20/-20
▲	PWT 4T TC-043	PN 313 - PN 288	K1	5/0	MID	20/-20
■	PWT 4T TC-043	PN 181 - PN 288	K1	15/0	MID	20/-20
◇	PWT 4T TC-043	PN 421 - PN 288	K1	0/10	MID	20/-20

FIGURE 127e DIFFERENTIAL L.E. FLAP WITH MID SPAN AILERONS
M = 1.2



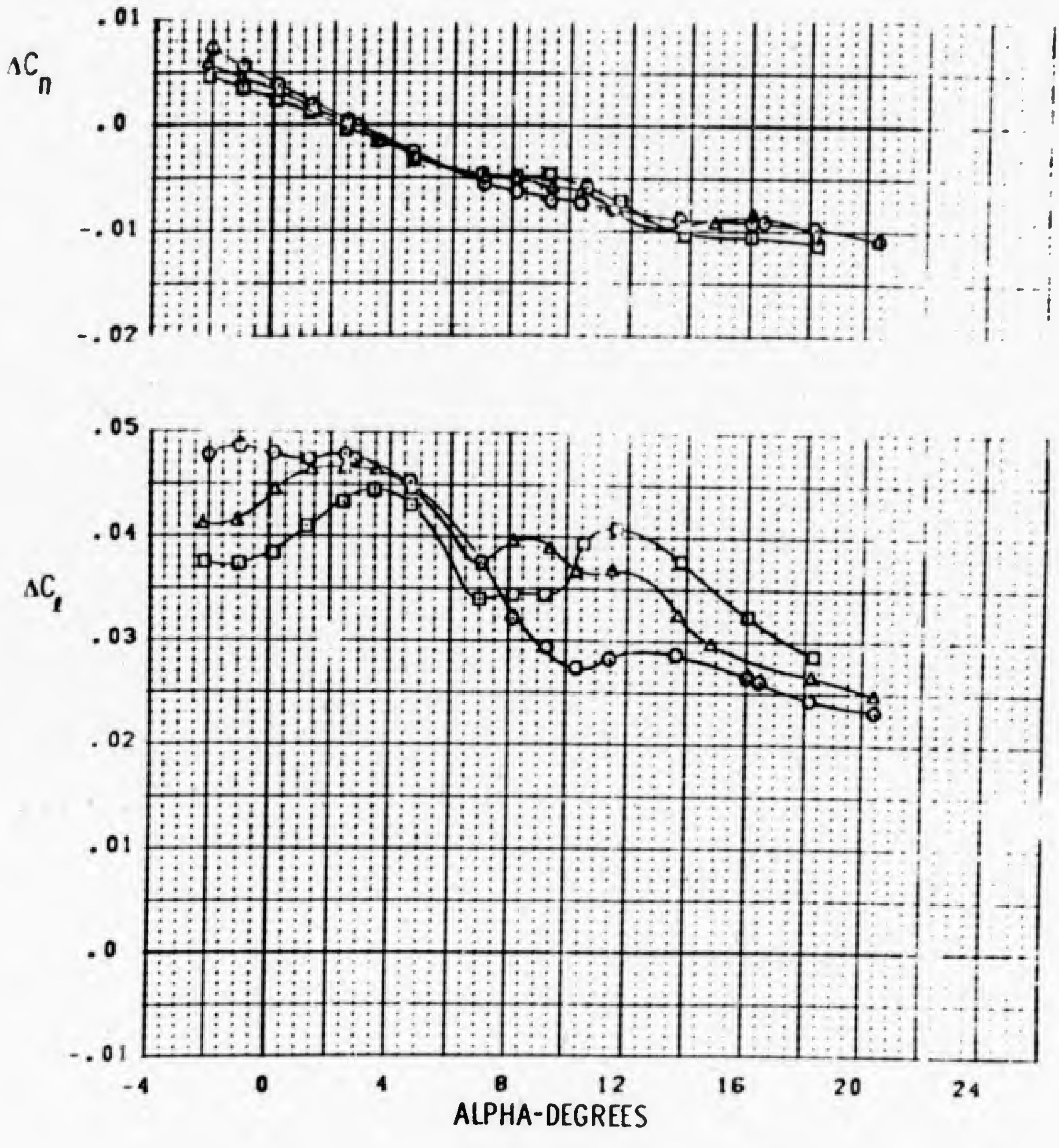
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 16T TF-216	PN 63 - PN 49	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 72 - PN 49	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 78 - PN 49	K1	5/0	3 SEGM. 20/-20

FIGURE 128a DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.7



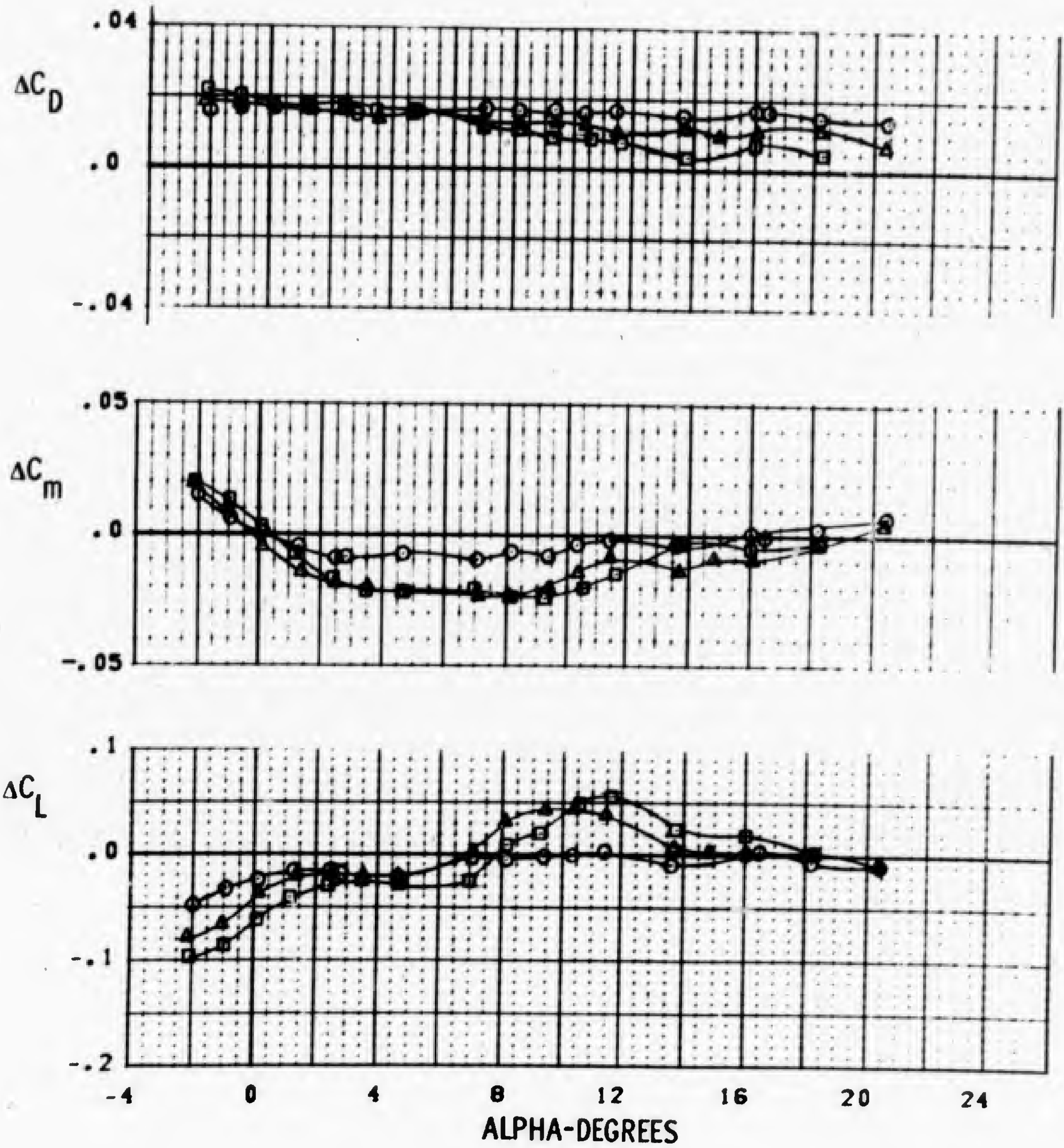
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 16T TF-216	PN 63 - PN 49	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 72 - PN 49	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 78 - PN 49	K1	5/0	3 SEGM. 20/-20

FIGURE 12.8a DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.7



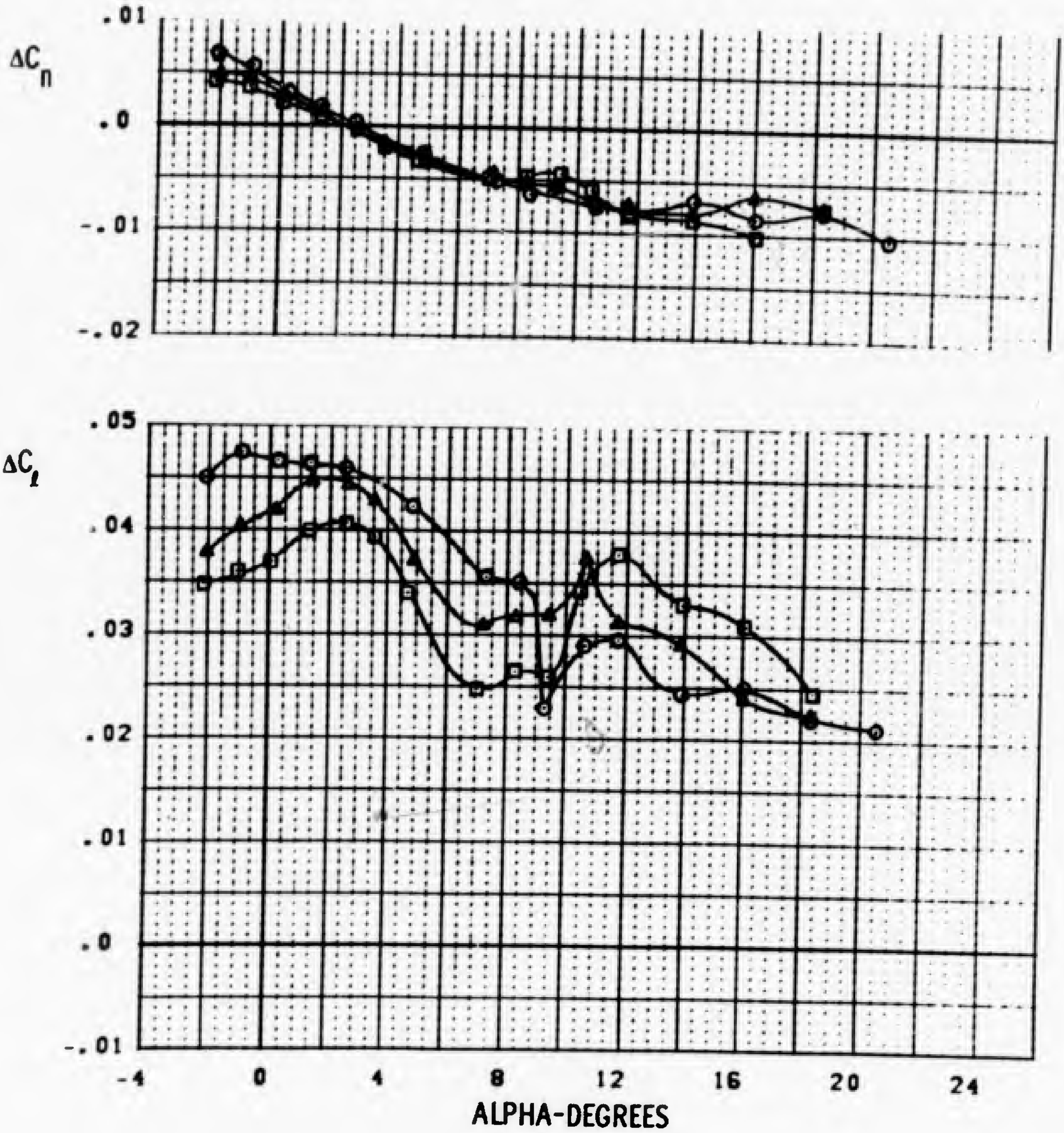
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON (L/R)
O	PWT 16T TF-216	PN 62 - PN 50	K1	0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 71 - PN 50	K1	10/0	3 SEGM. 20/-20
Δ	PWT 16T TF-216	PN 77 - PN 50	K1	5/0	3 SEGM. 20/-20

FIGURE 128b DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.8



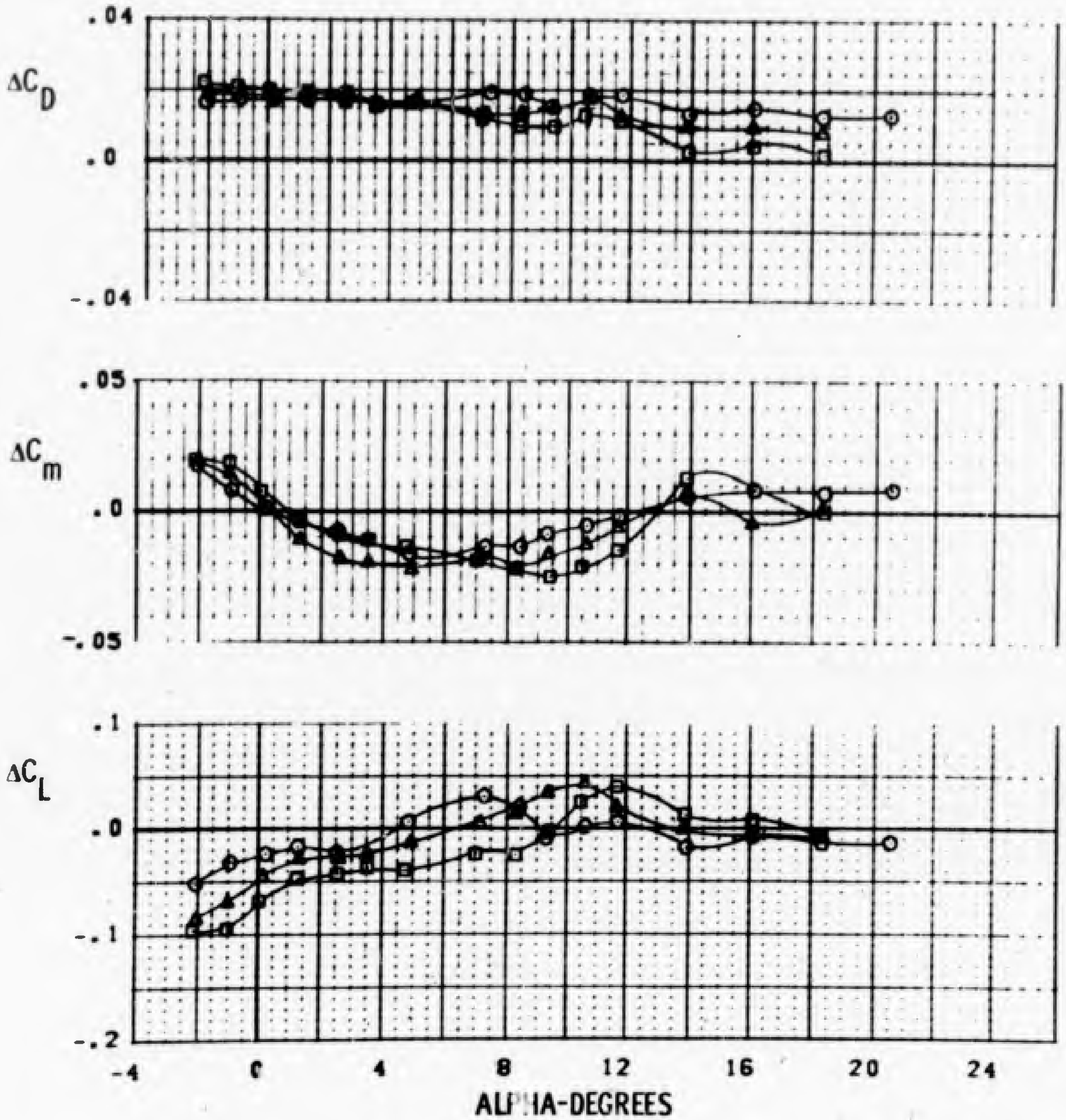
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON (L/R)
⊙	PWT 16T TF-216	PN 62 - PN 50	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 71 - PN 50	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 77 - PN 50	K1	5/0	3 SEGM. 20/-20

FIGURE 128b DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.8



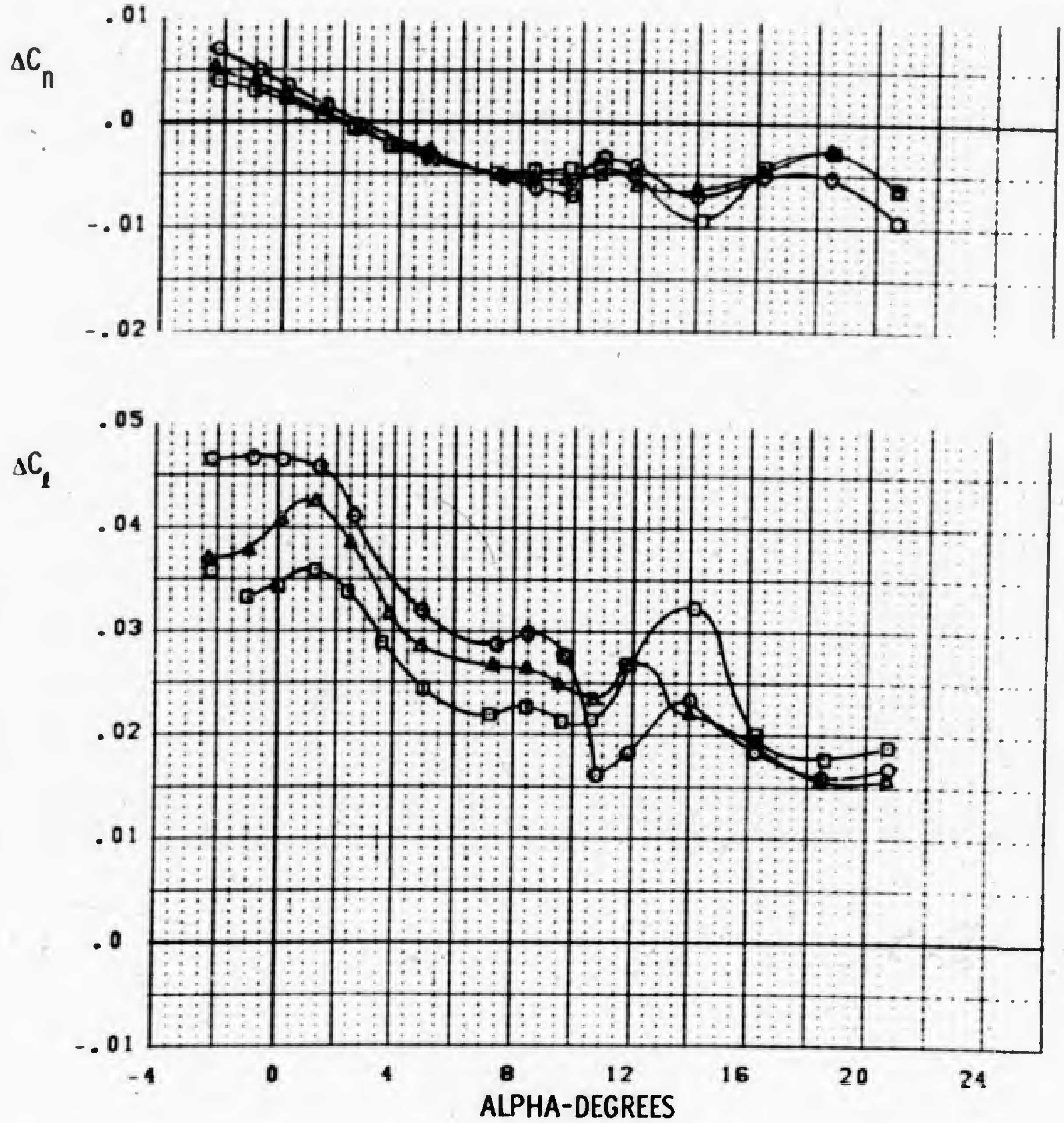
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
○	PWT 16T TF-216	PN 58 - PN 51	K1	0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 67 - PN 51	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 76 - PN 51	K1	5/0	3 SEGM. 20/-20

FIGURE 128c DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.85



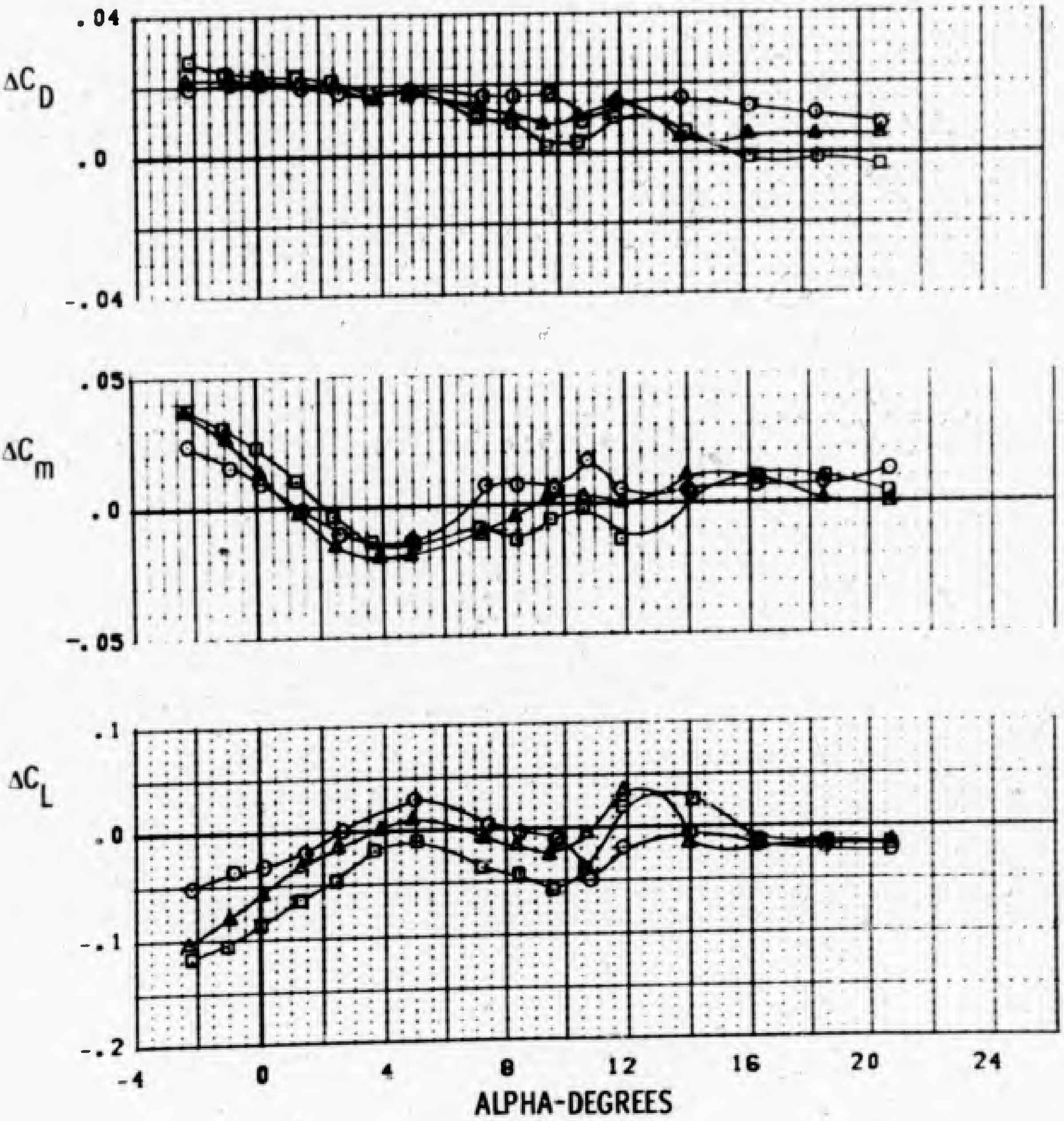
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 16T TF-216	PN 58 - PN 51	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 67 - PN 51	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 76 - PN 51	K1	5/0	3 SEGM. 20/-20

FIGURE 128c DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.85



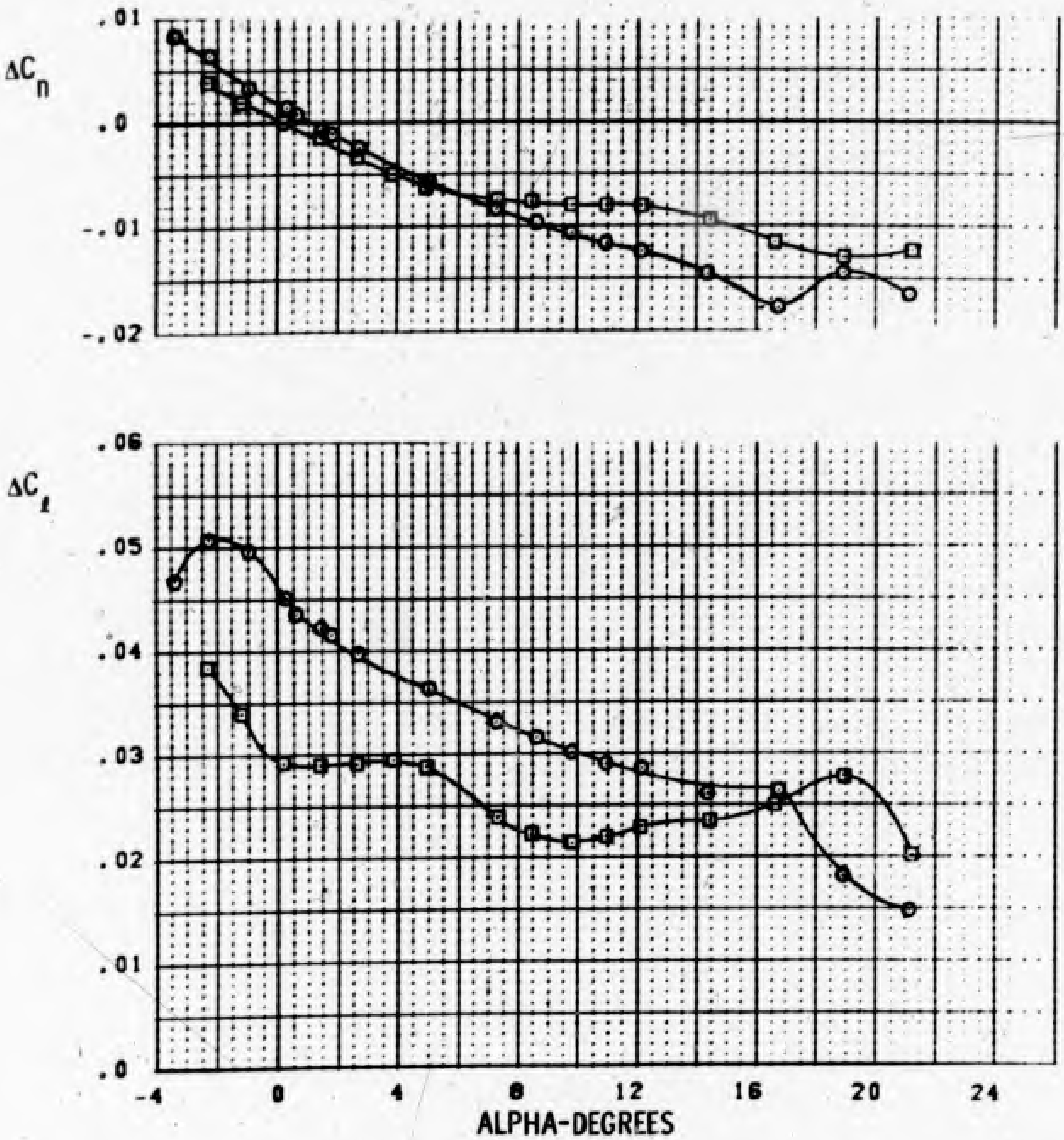
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
○	PWT 16T TF-216	PN 59 - PN 52	K1	0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 68 - PN 52	K1	10/0	3 SEGM. 20/-20
△	PWT 16T TF-216	PN 75 - PN 52	K1	5/0	3 SEGM. 20/-20

FIGURE 128d DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.9



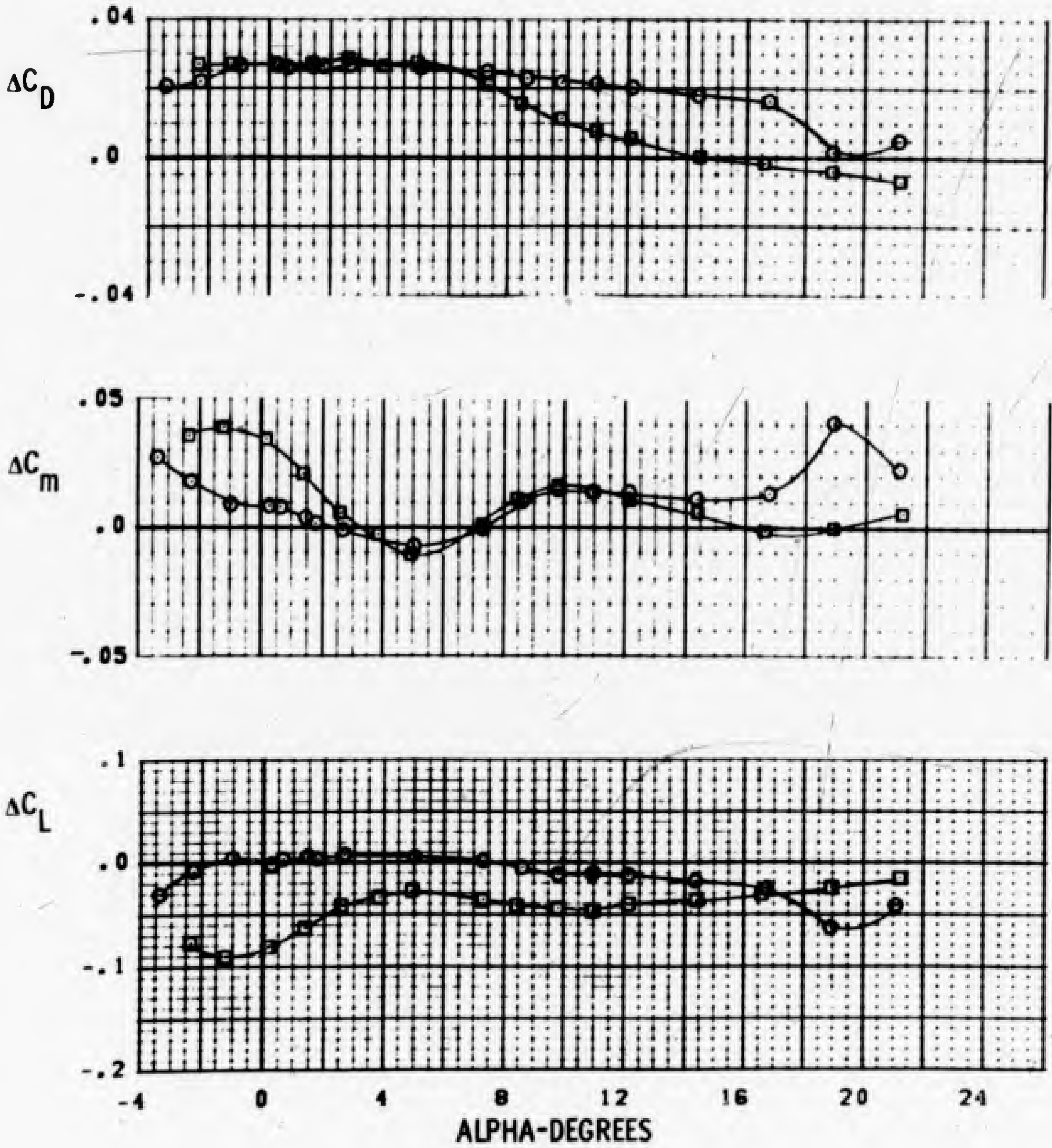
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
○	PWT 16T TF-216	PN 59 - PN 52	K1	0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 68 - PN 52	K1	10/0	3 SEGM. 20/-20
▲	PWT 16T TF-216	PN 75 - PN 52	K1	5/0	3 SEGM. 20/-20

FIGURE 128d DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.9



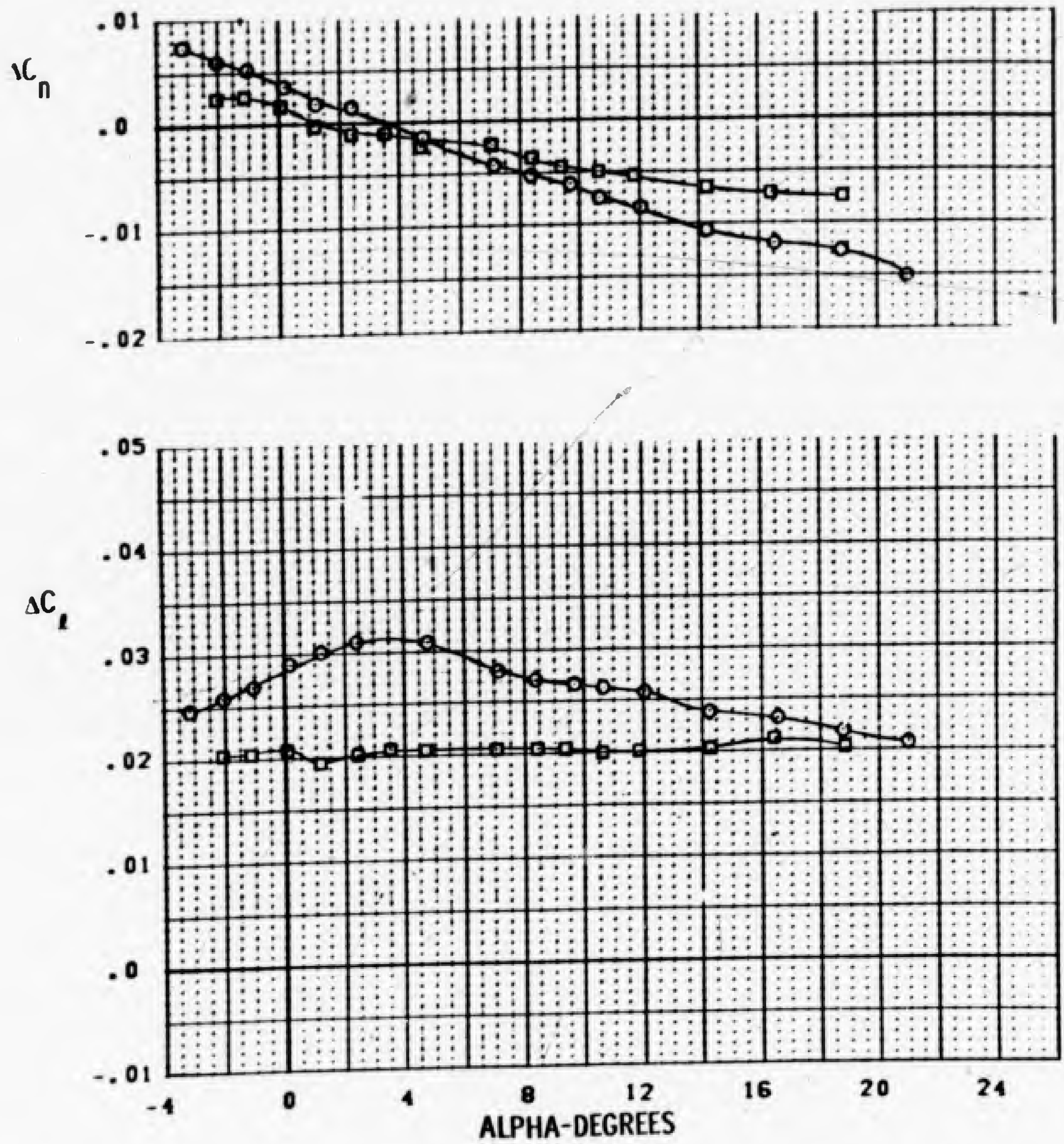
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
O	PWT 16T TF-216	PN 60 - PN 53	K1 0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 69 - PN 53	K1 10/0	3 SEGM. 20/-20

FIGURE 128e DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.95



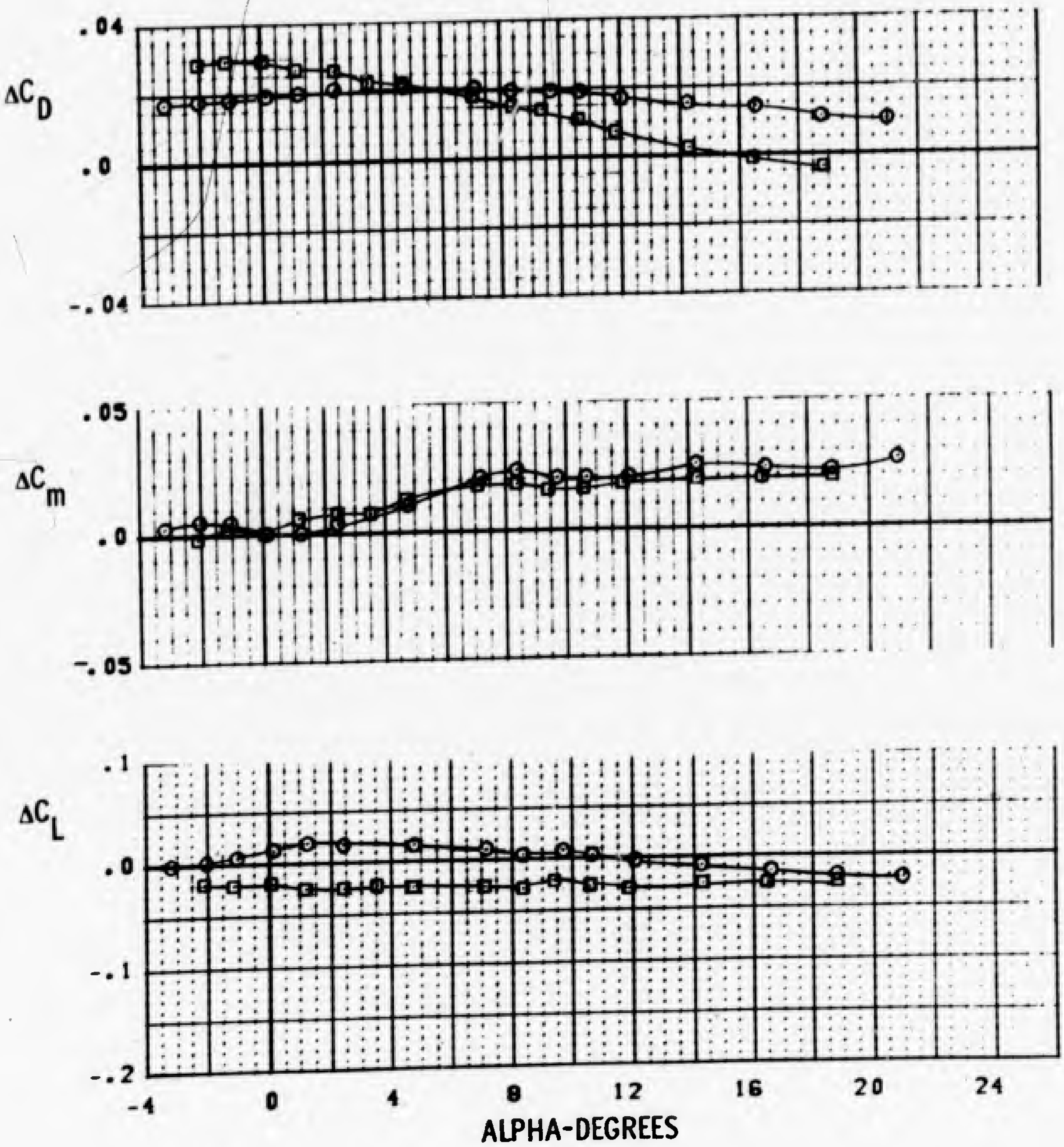
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 16T TF-216	PN 60 - PN 53	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 69 - PN 53	K1	10/0	3 SEGM. 20/-20

FIGURE 128e DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 0.95



SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
O	PWT 16T TF-216	PN 61 - PN 54	K1 0/0	3 SEGM. 20/-20
□	PWT 16T TF-216	PN 70 - PN 54	K1 10/0	3 SEGM. 20/-20

FIGURE 128f DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 1.2



SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 16T TF-216	PN 61 - PN 54	K1	0/0	3 SEGM. 20/-20
⊡	PWT 16T TF-216	PN 70 - PN 54	K1	10/0	3 SEGM. 20/-20

FIGURE 128f DIFFERENTIAL L.E. FLAP WITH EXTENDED SPAN AILERONS
M = 1.2

Table XI DIFFERENTIAL L.E. FLAP ROLL CONTROL WITH MID SPAN AILERONS INCREMENTAL DATA SUMMARY

Mid Span Ailerons $\pm 20^0$

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.7	K1	0/0	-0.90300	-0.02927	0.00796	0.01152	0.03650	0.00250	PWT 4T	215	268
			1.31100	-0.01805	-0.00352	0.01125	0.03680	0.00290			
			3.60300	-0.01371	-0.00747	0.01186	0.03650	0.00010			
			5.89500	-0.01233	-0.00410	0.01256	0.03480	-0.00220			
			8.17700	-0.00564	-0.00042	0.01323	0.03174	-0.00472			
			10.36600	-0.01907	0.00324	0.00960	0.02478	-0.00582			
			12.52400	-0.01364	0.00781	0.00984	0.02331	-0.00780			
			14.65400	-0.01538	0.00292	0.00694	0.01958	-0.00710			
			16.79999	-0.01040	-0.00220	0.00865	0.01790	-0.00789			
			18.95999	-0.00986	0.00424	0.00780	0.01453	-0.00466			
			21.14099	0.00307	0.00021	0.01350	0.01419	-0.00619			
0.7	K1	5/0	-1.02000	-0.04832	0.00656	0.01770	0.03339	0.00291	PWT 4T	312	268
			1.29100	-0.02522	-0.00948	0.01552	0.03570	0.00330			
			3.52300	-0.02817	-0.01292	0.01484	0.03560	0.00110			
			5.84800	-0.02341	-0.01485	0.01255	0.03440	-0.00150			
			8.09500	-0.01377	-0.01276	0.00672	0.03390	-0.00270			
			10.33700	0.01617	-0.01829	0.00718	0.02756	-0.00421			
			12.50500	0.00236	-0.01111	0.00808	0.02850	-0.00650			
			14.65400	-0.00678	-0.01068	0.00734	0.02428	-0.00740			
			16.80800	0.00596	-0.00198	0.01049	0.02190	-0.00860			
			18.92999	-0.00623	0.00573	0.00622	0.01976	-0.00771			
			21.12399	-0.00272	0.00968	0.00666	0.02099	-0.01258			
0.7	K1	0/10	0.13000	-0.03841	-0.01770	0.01645	0.03949	0.00691	PWT 4T	419	428
			2.39000	-0.03353	-0.02242	0.01263	0.03951	0.00351			
			4.63000	-0.02947	-0.02347	0.00944	0.03790	0.00020			
			6.93800	-0.02466	-0.02023	0.00736	0.03620	-0.00350			
			9.18800	-0.02070	-0.02323	0.00029	0.02916	-0.00769			
			11.37800	-0.00551	-0.02401	-0.00780	0.01690	-0.01060			
			13.54600	0.00057	-0.01630	-0.00970	0.01320	-0.01060			
			15.71800	-0.00177	-0.02020	-0.00680	0.01319	-0.00910			
			17.78999	-0.00542	-0.01338	-0.00664	0.01172	-0.00731			

Table XI CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.7	K1	10/0	0.08500	-0.05911	-0.00230	0.01281	0.03009	0.00301	PWT 4T	426	438
			2.32300	-0.03664	-0.01599	0.01000	0.03301	0.00171			
			4.64700	-0.02770	-0.02267	0.00890	0.03400	-0.00030			
			6.86800	-0.02809	-0.02192	0.00478	0.03239	-0.00220			
			9.21500	0.00093	-0.02598	-0.00107	0.03388	-0.00230			
			11.37200	0.02093	-0.02204	-0.00470	0.03330	-0.00330			
			13.52400	0.01222	-0.01425	-0.00776	0.03099	-0.00530			
			15.72300	0.00365	-0.01502	-0.00432	0.02599	-0.00810			
			17.80600	-0.00262	-0.00749	-0.00462	0.02091	-0.00781			
0.7	K1	15/0	-1.03500	-0.08652	0.02235	0.02004	0.02629	-0.00168	PWT 4T	180	268
			-0.99500	-0.08305	0.01970	0.01988	0.02639	-0.00029			
			1.26500	-0.06001	0.00705	0.01507	0.02730	-0.00050			
			3.55000	-0.04246	-0.00314	0.01188	0.03040	-0.00190			
			5.93100	-0.02927	-0.00930	0.00915	0.03050	-0.00380			
			8.07800	-0.02153	-0.01065	0.00376	0.02780	-0.00440			
			10.32400	0.00006	-0.00913	-0.00462	0.02435	-0.00481			
			12.46400	0.03032	-0.01936	-0.00636	0.02817	-0.00559			
			14.72500	0.00751	-0.00854	0.02830	0.03100	-0.00840			
			16.91899	0.01583	-0.00075	-0.00533	0.02381	-0.00984			
			18.98000	-0.00468	0.01072	-0.00955	0.01962	-0.00853			
			21.10799	0.00495	0.01328	-0.00714	0.02058	-0.01178			
0.8	K1	0/0	-0.89000	-0.03096	0.00565	0.01227	0.03510	0.00220	PWT 4T	214	267
			1.37200	-0.01648	-0.00658	0.01199	0.03560	0.00310			
			3.71500	-0.01766	-0.01072	0.01198	0.03550	0.00051			
			6.06300	-0.01542	-0.00760	0.01217	0.03332	-0.00230			
			10.50800	-0.01666	0.00651	0.00970	0.02258	-0.00578			
			12.69200	-0.00901	0.00862	0.01005	0.02190	-0.00660			
			14.86500	-0.01868	0.01576	0.00758	0.01950	-0.00610			
			19.21799	-0.00923	0.01183	0.01048	0.01500	-0.00480			
			21.38199	-0.01111	0.01001	0.00907	0.01389	-0.00520			

Table XI CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.8	K1	5/0	-1.02600	-0.05700	0.00599	0.01640	0.03139	0.00322	PWT 4T	311	267
			1.32800	-0.02454	-0.01167	0.01400	0.03410	0.00300			
			3.68500	-0.02121	-0.01822	0.01369	0.03480	0.00041			
			6.01500	-0.02065	-0.01888	0.01066	0.03133	-0.00169			
			8.34500	0.00911	-0.02045	0.01050	0.02950	-0.00299			
			10.51500	0.01353	-0.01148	0.00809	0.02918	-0.00459			
			12.71700	0.00283	0.00221	0.00514	0.02690	-0.00640			
			14.90200	-0.01262	0.00177	0.00521	0.02360	-0.00720			
			17.01700	-0.01491	-0.00192	0.00522	0.02058	-0.00660			
			19.21399	-0.00141	0.00567	0.00909	0.01950	-0.00910			
			21.39099	-0.01029	0.00858	0.00529	0.01860	-0.00950			
0.8	K1	0/10	0.17900	-0.04125	-0.01821	0.01825	0.03870	0.00691	PWT 4T	420	440
			2.41200	-0.02822	-0.02456	0.01538	0.03871	0.00361			
			4.78500	-0.02438	-0.02660	0.01222	0.03730	0.00040			
			7.07800	-0.01446	-0.02742	0.00973	0.03447	-0.00308			
			9.39000	-0.02039	-0.02702	0.00222	0.02488	-0.00679			
			11.61600	-0.00388	-0.01718	-0.00352	0.01668	-0.00891			
			13.81700	0.00376	-0.01148	-0.00535	0.01330	-0.00810			
			15.87900	0.00023	-0.01427	-0.00442	0.01330	-0.00750			
			18.07500	-0.01450	-0.01407	-0.00604	0.01361	-0.00750			
0.8	K1	10/0	0.11900	-0.06062	0.00059	0.01459	0.02759	0.00281	PWT 4T	427	440
			2.44700	-0.03288	-0.01627	0.01246	0.03111	0.00141			
			4.75900	-0.02734	-0.02368	0.01127	0.03151	-0.00079			
			7.10400	-0.03052	-0.02341	0.00746	0.02596	-0.00269			
			9.42800	-0.00785	-0.02098	0.00287	0.02570	-0.00250			
			11.58400	0.02636	-0.02004	0.00019	0.02849	-0.00340			
			13.80000	0.00712	-0.00108	-0.00480	0.03020	-0.00640			
			15.94100	0.00084	0.00078	-0.00219	0.02519	-0.00780			
			18.05800	-0.01491	-0.00021	-0.00567	0.01952	-0.00570			

Table XI CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.6	K1	15/0	-0.50000	[illegible]	0.01687	0.02095	0.02570	[illegible]	PWT 4T	170	[illegible]
			-0.98700	-0.08610	0.01763	0.02156	0.02570	-0.00048			
			1.22400	-0.06097	0.00657	0.01705	0.02539	0.00021			
			3.62500	-0.05357	-0.00269	0.01508	0.02621	-0.00145			
			6.04500	-0.06673	-0.00102	0.01133	0.01912	-0.00320			
			8.27200	-0.05634	-0.01226	0.00467	0.01550	-0.00347			
			10.46300	-0.02016	-0.01438	-0.00093	0.01726	-0.00337			
			12.67500	-0.00521	0.00117	-0.00813	0.02610	-0.00450			
			14.83600	0.00929	0.00409	-0.00757	0.03139	-0.00930			
			17.03199	-0.01199	0.01225	-0.01245	0.02460	-0.00880			
			19.23799	-0.00071	0.01356	-0.00589	0.01941	-0.00750			
0.85	K1	0/0	-1.37500	-0.02990	0.00621	0.01187	0.03501	0.00632	PWT 16T	11	51
			-0.32900	-0.01569	0.00021	0.01203	0.03591	0.00529			
			0.27400	-0.01438	-0.00586	0.01228	0.03571	0.00351			
			1.43800	-0.00900	-0.01020	0.01204	0.03629	0.00251			
			2.58700	-0.00821	-0.01443	0.01149	0.03633	0.00130			
			4.35400	0.01539	-0.01855	0.01274	0.03401	-0.00110			
			7.14600	0.03137	-0.01471	0.01529	0.02439	-0.00360			
			9.47100	0.00143	-0.00920	0.01344	0.01868	-0.00434			
			11.71000	-0.00534	-0.00076	0.01229	0.01979	-0.00518			
			14.01200	-0.01729	0.00463	0.00941	0.01709	-0.00423			
			16.25099	-0.00519	0.00759	0.01124	0.01747	-0.00545			
			18.45999	-0.02461	0.00056	0.01168	0.01435	-0.00469			

Table XI CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.85	K1	5/0	-2.03000	-0.05902	0.01141	0.01654	0.03080	0.00450	PWT 16T	26	51
			-0.93200	-0.05034	0.00468	0.01549	0.03090	0.00379			
			0.23200	-0.03404	-0.00586	0.01421	0.03300	0.00280			
			1.31700	-0.01937	-0.01380	0.01345	0.03469	0.00199			
			2.58000	-0.02127	-0.01710	0.01368	0.03452	0.00070			
			4.79400	-0.02293	-0.01326	0.01138	0.02799	-0.00130			
			7.12400	-0.00529	-0.01192	0.00848	0.02407	-0.00260			
			8.31300	0.01056	-0.01938	0.01007	0.02660	-0.00350			
			9.49400	0.02727	-0.01325	0.01177	0.02643	-0.00435			
			10.60300	0.02034	-0.00604	0.01062	0.02660	-0.00508			
			11.70900	0.00903	0.00100	0.00723	0.02409	-0.00578			
			13.92100	-0.00863	0.00923	0.00450	0.02104	-0.00602			
			16.17999	-0.01057	0.00069	0.00580	0.01728	-0.00458			
			18.52139	-0.00759	-0.00199	0.00603	0.01438	-0.00394			
0.85	K1	10/0	-2.11500	-0.06401	0.00673	0.01385	0.02840	0.00301	PWT 16T	32	51
			-1.11100	-0.06087	0.00518	0.01726	0.02918	0.00254			
			0.08900	-0.04955	-0.00322	0.01588	0.02939	0.00173			
			1.22000	-0.03432	-0.01065	0.01514	0.03117	0.00116			
			2.47600	-0.03670	-0.01167	0.01515	0.03030	-0.00010			
			4.77700	-0.04127	-0.01232	0.01110	0.02339	-0.00220			
			7.05400	-0.04412	-0.01780	0.00453	0.01715	-0.00303			
			8.18300	-0.02859	-0.02681	0.00542	0.01674	-0.00299			
			9.35200	-0.01231	-0.02868	0.00322	0.01964	-0.00271			
			10.47500	0.02390	-0.02230	0.00750	0.02840	-0.00450			
			11.64500	0.03661	-0.01253	0.00614	0.03160	-0.00619			
			13.95500	0.00058	0.01449	-0.00346	0.02336	-0.00522			
			16.15900	0.00761	0.00244	0.00138	0.02249	-0.00686			
			18.39000	-0.00361	-0.01357	-0.00129	0.01612	-0.00444			

Table XI CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.9	K1	0/0	-0.88700	-0.03067	0.00832	0.01358	0.03290	0.00320	PWT 4T	213	264
			1.51800	-0.01989	-0.00487	0.01316	0.03330	0.00230			
			3.54100	0.00469	-0.01499	0.01232	0.03039	-0.00020			
			6.29000	0.01849	-0.01223	0.01306	0.02697	-0.00251			
			8.59300	-0.00313	-0.00545	0.01124	0.02310	-0.00420			
			10.71200	-0.04597	0.00309	0.00757	0.01825	-0.00470			
			13.00600	-0.01891	0.00555	0.01082	0.01980	-0.00589			
			15.09500	-0.01971	0.00773	0.00973	0.01610	-0.00449			
			17.35100	-0.01172	0.00826	0.01071	0.01380	-0.00350			
			19.48499	-0.00406	0.00727	0.01260	0.01317	-0.00479			
0.9	K1	5/0	-1.04300	-0.07098	0.01529	0.01649	0.02737	0.00304	PWT 4T	310	264
			1.38700	-0.03144	-0.01000	0.01471	0.03180	0.00199			
			3.86300	-0.01427	-0.01677	0.01370	0.02630	-0.00040			
			6.19600	-0.01205	-0.01454	0.01059	0.02040	-0.00190			
			8.53000	-0.02564	-0.01524	0.00340	0.01862	-0.00269			
			10.77000	-0.01805	-0.01674	0.00394	0.01952	-0.00320			
			12.90100	-0.00948	0.00175	0.00523	0.02170	-0.00580			
			15.08600	-0.01718	0.01918	0.00182	0.01810	-0.00579			
			17.28799	-0.00722	0.00840	0.00519	0.01591	-0.00422			
			19.43500	-0.01048	-0.00052	0.00509	0.01293	-0.00244			
0.9	K1	0/10	0.14500	-0.04540	-0.01506	0.02078	0.03549	0.00680	PWT 4T	418	441
			2.56300	-0.02851	-0.02330	0.01776	0.03590	0.00360			
			4.98200	-0.00736	-0.02602	0.01429	0.03180	0.00040			
			7.30300	-0.00771	-0.02665	0.01024	0.02643	-0.00230			
			9.53900	-0.02119	-0.03328	0.00427	0.02385	-0.00509			
			11.83800	-0.03286	-0.01986	-0.00068	0.01849	-0.00680			
			14.05200	-0.00438	-0.00630	-0.00251	0.01318	-0.00619			
			16.24799	0.00571	-0.01040	-0.00071	0.00795	-0.00337			

Table XI CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.9	K1	10/0	0.13200	-0.07342	0.01038	0.01696	0.02289	0.00171	PWT 4T	425	441
			2.52800	-0.04617	-0.00572	0.01527	0.02389	0.00021			
			4.99700	-0.02260	-0.01668	0.01249	0.01870	-0.00140			
			7.30400	-0.02020	-0.01824	0.00902	0.01293	-0.00230			
			9.59600	-0.02996	-0.02008	0.00263	0.01553	-0.00229			
			11.76100	-0.04627	-0.01848	-0.00596	0.02222	-0.00197			
			13.98900	-0.00530	-0.00430	-0.00541	0.02360	-0.00460			
			16.14000	-0.00576	0.01744	-0.00512	0.01971	-0.00640			
0.5	K1	15/0	-1.09900	-0.09873	0.02009	0.02389	0.02339	0.00106	PWT 4T	178	264
			1.33500	-0.09168	0.01774	0.01979	0.01850	0.00089			
			3.75200	-0.07102	-0.00028	0.01683	0.01488	-0.00139			
			8.35100	-0.07887	-0.02278	0.00221	0.00888	-0.00106			
			10.63200	-0.07514	-0.01779	-0.00444	0.01043	-0.00020			
			12.87400	-0.03407	-0.00713	-0.00741	0.01580	-0.00010			
			15.08400	-0.02176	0.00610	-0.01039	0.02040	-0.00309			
			17.26500	-0.00906	0.01221	-0.00980	0.01991	-0.00403			
			19.43799	-0.01244	0.02140	-0.01268	0.01663	-0.00354			
1.2	K1	0/0	-0.52800	0.00648	0.00468	0.01385	0.01613	0.00411	PWT 4T	216	269
			1.40600	0.01055	0.00615	0.01463	0.01903	0.00248			
			3.79500	0.01780	0.00554	0.01708	0.02170	0.00070			
			6.25000	0.01092	0.01640	0.01689	0.02020	-0.00100			
			8.59600	0.00820	0.02344	0.01625	0.01891	-0.00239			
			10.89200	0.00419	0.02067	0.01615	0.01860	-0.00420			
			13.20700	-0.00004	0.02264	0.01541	0.01840	-0.00500			
			15.47200	-0.00650	0.02213	0.01413	0.01832	-0.00720			
			17.68900	-0.02201	0.03114	0.00922	0.01909	-0.01060			
			19.87999	-0.02960	0.03660	0.00660	0.01600	-0.00940			

Table XI CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
1.2	K1	5/0	-1.05200	-0.00371	-0.00243	0.02519	0.01480	0.00300	PWT 4T	313	269
			1.31500	-0.00098	-0.00369	0.02473	0.01611	0.00159			
			3.74200	-0.00262	0.00330	0.02342	0.01739	0.00021			
			6.10500	-0.00816	0.01271	0.02078	0.01680	-0.00091			
			8.48200	-0.01171	0.01351	0.01730	0.01550	-0.00140			
			10.81600	-0.01385	0.01539	0.01398	0.01650	-0.00270			
			13.16000	-0.01548	0.01562	0.01145	0.01700	-0.00400			
			15.39400	-0.01542	0.01748	0.00987	0.01780	-0.00550			
			17.60500	-0.01794	0.01743	0.00676	0.01858	-0.00620			
			19.84698	-0.02652	0.02517	0.00267	0.01771	-0.00641			
1.2	K1	10/0	-2.27100	-0.01794	-0.00700	0.02486	0.01405	0.00190	PWT 4T	428	269
			-2.27100	-0.01824	-0.00630	0.02466	0.01405	0.00200			
			-2.26800	-0.01831	-0.00549	0.02497	0.01405	0.00200			
			-2.26600	-0.01739	-0.01122	0.02498	0.01435	0.00180			
			-2.24000	-0.01797	-0.00822	0.02501	0.01415	0.00190			
			0.11400	-0.01983	-0.00568	0.02328	0.01375	0.00030			
			2.44300	-0.02308	0.00164	0.02012	0.01323	-0.00024			
			4.81900	-0.03049	0.01636	0.01510	0.01244	-0.00061			
			7.22900	-0.03460	0.03121	0.00939	0.01275	-0.00060			
			9.56000	-0.03816	0.03912	0.00259	0.01255	-0.00065			
			11.90200	-0.03878	0.04205	-0.00249	0.01428	-0.00159			
			14.19000	-0.03855	0.04307	-0.00762	0.01525	-0.00195			
			16.44499	-0.03652	0.04590	-0.01045	0.01698	-0.00310			
			18.66499	-0.03582	0.05204	-0.01387	0.01639	-0.00313			
			20.87299	-0.03798	0.05762	-0.01785	0.01791	-0.00335			

Table XI CONT'D											
MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
1.2	K1	0/10	-2.27500	-0.02137	-0.00344	0.02374	0.01865	0.00990	PWT 4T	421	269
			-1.09300	-0.02076	-0.00236	0.02459	0.02070	0.00920			
			0.09100	-0.02267	-0.00161	0.02212	0.02315	0.00830			
			2.47900	-0.02277	-0.00093	0.01957	0.02774	0.00596			
			4.90500	-0.02501	0.00633	0.01591	0.02915	0.00249			
			7.22300	-0.03125	0.02308	0.01033	0.02635	-0.00040			
			9.64000	-0.03786	0.03526	0.00313	0.02465	-0.00335			
			11.94200	-0.03329	0.03187	-0.00079	0.02408	-0.00637			
			14.25100	-0.02890	0.03157	-0.00404	0.02195	-0.00815			
			16.47699	-0.02784	0.03301	-0.00743	0.02019	-0.00940			
			18.69599	-0.02808	0.04012	-0.01000	0.01869	-0.01139			
1.2	K1	15/0	-3.35600	-0.02763	0.01209	0.03180	0.01220	-0.00190	PWT 4T	181	269
			-1.06900	-0.03615	0.01477	0.03021	0.00890	-0.00060			
			1.22500	-0.04515	0.01837	0.02747	0.00669	-0.00190			
			3.65800	-0.05355	0.02536	0.02355	0.00547	-0.00258			
			6.03000	-0.05465	0.02595	0.01796	0.00609	-0.00201			
			8.42600	-0.04483	0.02309	0.01248	0.00790	-0.00210			
			10.66400	-0.04182	0.02122	0.00545	0.00979	-0.00231			
			13.06000	-0.04681	0.02316	-0.00167	0.01058	-0.00232			
			15.29000	-0.04480	0.02516	-0.00716	0.01260	-0.00290			
			17.55099	-0.03956	0.02915	-0.01118	0.01397	-0.00330			
			19.80099	-0.04705	0.03334	-0.01837	0.01393	-0.00303			
			22.01799	-0.03484	0.02708	-0.01939	0.01570	-0.00550			

Table XII DIFFERENTIAL L.E. FLAP ROLL CONTROL WITH EXTENDED SPAN AILERONS INCREMENTAL DATA SUMMARY

3 Segment Ailerons $\pm 20^0$

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.7	K1	0/0	-2.70100	-0.04059	0.01231	0.01480	0.04787	0.00837	PWT 16T	43	49
			-2.13700	-0.04019	0.01029	0.01529	0.04982	0.00762			
			-0.96400	-0.03082	0.00449	0.01549	0.05118	0.00609			
			0.20100	-0.02083	-0.00278	0.01543	0.04949	0.00409			
			1.29700	-0.01853	-0.00763	0.01547	0.04843	0.00220			
			2.27800	-0.01601	-0.01003	0.01535	0.04895	0.00089			
			3.47400	-0.01493	-0.01009	0.01368	0.04835	-0.00110			
			4.49700	-0.01648	-0.01036	0.01420	0.04759	-0.00240			
			6.89800	-0.00520	-0.00565	0.01555	0.04359	-0.00610			
			7.98300	-0.00217	-0.00556	0.01721	0.03942	-0.00700			
			9.14300	-0.00818	-0.00613	0.01635	0.03544	-0.00762			
			10.21500	-0.00632	-0.00559	0.01626	0.03281	-0.00960			
			11.27300	-0.00829	-0.00261	0.01540	0.03238	-0.00969			
			13.69500	-0.00752	0.00020	0.01257	0.03055	-0.01048			
			15.82700	-0.00424	-0.00466	0.01426	0.02850	-0.01160			
			18.06599	0.00085	0.00166	0.01460	0.02557	-0.01055			

Table XII CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.7	K1	5/0	-2.09400	-0.07184	0.01407	0.01751	0.04431	0.00581	PWT 16T	78	49
			-1.01900	-0.05739	0.00671	0.01649	0.04667	0.00479			
			0.12600	-0.03653	-0.00583	0.01569	0.04885	0.00338			
			1.12400	-0.02659	-0.01194	0.01500	0.04847	0.00201			
			2.28100	-0.02336	-0.01510	0.01494	0.04926	0.00039			
			3.39300	-0.02547	-0.01594	0.01285	0.04884	-0.00100			
			4.45000	-0.02684	-0.01702	0.01329	0.04779	-0.00261			
			6.81500	-0.01280	-0.01740	0.00967	0.04311	-0.00490			
			7.93200	0.00403	-0.01797	0.00779	0.04291	-0.00530			
			9.13100	0.02090	-0.02014	0.00803	0.04347	-0.00581			
			10.21200	0.01696	-0.01524	0.00775	0.03911	-0.00710			
			11.35400	0.01012	-0.01486	0.00743	0.03814	-0.00870			
			13.60100	0.00771	-0.01281	0.00872	0.03562	-0.01103			
			15.76500	0.00709	-0.00771	0.00931	0.03168	-0.01248			
			17.95999	0.00943	0.00214	0.00971	0.02991	-0.01330			
			20.15999	0.00319	0.00306	0.00840	0.02931	-0.01502			

Table XII CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	DATA RUN	BASE RUN
0.7	K1	10/0	-2.09500	-0.09245	0.01656	0.02041	0.04041	0.00471	PWT 16T	72	49
			-1.14700	-0.08485	0.01202	0.01866	0.04143	0.00428			
			-0.00500	-0.05976	0.00027	0.01701	0.04340	0.00256			
			1.16500	-0.04941	-0.00901	0.01577	0.04465	0.00181			
			2.27200	-0.03511	-0.01509	0.01528	0.04755	0.00069			
			3.41800	-0.02902	-0.01675	0.01334	0.04825	-0.00110			
			4.60200	-0.02788	-0.01923	0.01362	0.04719	-0.00250			
			4.75600	-0.03040	-0.01886	0.01303	0.04635	-0.00281			
			6.80400	-0.01777	-0.01975	0.01044	0.04251	-0.00480			
			7.92500	-0.00150	-0.02325	0.00815	0.04051	-0.00500			
			9.16800	0.02354	-0.02918	0.00647	0.04275	-0.00462			
			10.15600	0.03857	-0.02554	0.00386	0.04543	-0.00529			
			11.37800	0.04165	-0.02129	0.00179	0.04616	-0.00660			
			13.59900	0.01082	-0.01657	0.00030	0.03712	-0.00963			
			15.76400	0.02085	-0.00924	0.00455	0.03648	-0.01358			
			17.97499	0.01468	0.00005	0.00401	0.03321	-0.01470			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.8	K1	C/C	-1.99700	-0.04861	0.01531	0.01618	0.04781	0.00719	PWT 16T	62	50
			-0.93700	-0.03232	0.00611	0.01713	0.04862	0.00571			
			0.14800	-0.02365	0.00072	0.01700	0.04797	0.00389			
			1.30800	-0.01635	-0.00451	0.01701	0.04740	0.00200			
			2.48100	-0.01484	-0.00869	0.01700	0.04791	0.00041			
			2.83500	-0.01852	-0.00834	0.01526	0.04746	-0.00006			
			4.65300	-0.02201	-0.00696	0.01597	0.04529	-0.00261			
			7.05400	-0.00299	-0.00952	0.01746	0.03754	-0.00560			
			8.16500	-0.00524	-0.00628	0.01682	0.03210	-0.00629			
			9.36500	-0.00097	-0.00786	0.01695	0.02932	-0.00710			
			10.35400	-0.00047	-0.00369	0.01613	0.02734	-0.00731			
			11.43600	0.00298	-0.00187	0.01669	0.02819	-0.00800			
			13.65700	-0.00923	-0.00346	0.01543	0.02862	-0.00887			
			16.04300	0.00051	0.00088	0.01700	0.02651	-0.00922			
			16.48599	0.00329	-0.00038	0.01682	0.02607	-0.00913			
			18.19899	-0.00725	0.00263	0.01508	0.02430	-0.00979			
			20.44398	-0.01069	0.00706	0.01413	0.02322	-0.01093			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.8	K1	5/0	-2.11400	-0.07824	0.01952	0.01969	0.04117	0.00588	PWT 16T	77	50
			-1.03200	-0.06598	0.01043	0.01803	0.04150	0.00441			
			0.15800	-0.03665	-0.00462	0.01699	0.04447	0.00219			
			1.27750	-0.01875	-0.01424	0.01706	0.04650	0.00170			
			2.44500	-0.01859	-0.01820	0.01572	0.04671	0.00011			
			3.54400	-0.01959	-0.01955	0.01438	0.04645	-0.00150			
			4.47900	-0.01963	-0.02155	0.01530	0.04479	-0.00300			
			7.11000	0.00353	-0.02315	0.01264	0.03731	-0.00481			
			8.14200	0.02193	-0.02295	0.01344	0.03967	-0.00509			
			9.40600	0.04268	-0.01792	0.01353	0.03889	-0.00589			
			10.37600	0.04428	-0.01176	0.01256	0.03673	-0.00631			
			11.49100	0.03592	-0.00811	0.01084	0.03683	-0.00791			
			13.77200	0.00813	-0.01340	0.01196	0.03240	-0.00970			
			14.82400	0.00430	-0.00848	0.00971	0.02965	-0.00920			
			16.07599	0.00229	-0.00361	0.01138	0.02571	-0.00443			
			19.21700	0.00064	-0.00363	0.01140	0.02550	-0.01060			
			20.34299	-0.00514	0.00440	0.00738	0.02474	-0.01087			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.8	K1	10/0	-2.11200	-0.09733	0.01983	0.02189	0.03759	0.00469	PWT 16T	71	50
			-0.98000	-0.08625	0.01355	0.02027	0.03731	0.00360			
			0.08800	-0.06135	0.00316	0.01836	0.03835	0.00239			
			1.22600	-0.04072	-0.00698	0.01819	0.04100	0.00130			
			2.40500	-0.02956	-0.01636	0.01818	0.04330	-0.00030			
			3.48900	-0.02366	-0.02157	0.01624	0.04454	-0.00161			
			4.69400	-0.02863	-0.02189	0.01685	0.04300	-0.00320			
			7.00400	-0.02477	-0.02031	0.01206	0.03400	-0.00470			
			8.16900	0.00965	-0.02353	0.01123	0.03431	-0.00489			
			9.26200	0.02101	-0.02391	0.00889	0.03437	-0.00470			
			10.57500	0.04838	-0.01998	0.00853	0.03933	-0.00580			
			11.64900	0.05550	-0.01457	0.00758	0.04094	-0.00718			
			13.79900	0.02378	-0.00320	0.00363	0.03769	-0.01029			
			16.05895	0.01863	-0.00483	0.00731	0.03231	-0.01062			
			18.28495	0.00135	-0.00318	0.00465	0.02867	-0.01125			

Table XII CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.85	K1	0/0	-2.08300	-0.05130	0.01795	0.01676	0.04500	0.00680	PWT 16T	58	51
			-0.92000	-0.03135	0.00787	0.01752	0.04750	0.00569			
			0.26300	-0.02416	0.00115	0.01762	0.04670	0.00311			
			1.33600	-0.01743	-0.00355	0.01737	0.04640	0.00190			
			2.52100	-0.02268	-0.00695	0.01693	0.04601	0.00030			
			4.85000	0.00622	-0.01600	0.01703	0.04231	-0.00260			
			7.30000	0.03120	-0.01318	0.01938	0.03558	-0.00511			
			8.42800	0.02086	-0.01323	0.01906	0.03516	-0.00637			
			9.32300	-0.00875	-0.00827	0.01525	0.02283	-0.00562			
			10.62000	0.00216	-0.00535	0.01875	0.02900	-0.00748			
			11.73400	0.00670	-0.00195	0.01876	0.02959	-0.00808			
			13.93400	-0.01837	0.00568	0.01324	0.02435	-0.00682			
			16.10500	-0.00772	0.00862	0.01485	0.02500	-0.00850			
			18.35899	-0.01340	0.00721	0.01264	0.02201	-0.00782			
			20.56898	-0.01355	0.00865	0.01299	0.02110	-0.01039			
0.85	K1	5/0	-2.02700	-0.08363	0.01983	0.01934	0.03780	0.00490	PWT 16T	76	51
			-0.59300	-0.06955	0.01484	0.01895	0.04029	0.00437			
			0.16400	-0.04328	0.00028	0.01809	0.04189	0.00271			
			1.36200	-0.02760	-0.01063	0.01825	0.04480	0.00140			
			2.59200	-0.02677	-0.01719	0.01822	0.04443	-0.00040			
			3.53600	-0.02265	-0.01894	0.01520	0.04287	-0.00160			
			4.91000	-0.01254	-0.02163	0.01619	0.03712	-0.00320			
			7.19000	0.00666	-0.01648	0.01342	0.03089	-0.00420			
			8.30000	0.01622	-0.02116	0.01360	0.03180	-0.00500			
			9.37300	0.03397	-0.01585	0.01539	0.03188	-0.00541			
			10.63500	0.04419	-0.01243	0.01776	0.03750	-0.00727			
			11.64900	0.02126	-0.00578	0.01262	0.03119	-0.00718			
			13.83600	0.00004	0.00634	0.00963	0.02910	-0.00810			
			16.05699	-0.00483	-0.00457	0.00974	0.02408	-0.00639			
			18.33199	-0.00930	0.00130	0.00840	0.02250	-0.00720			

Table XII CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.85	K1	10/0	-2.13000	-0.09531	0.01963	0.02246	0.03480	0.00421	PWT 16T	67	51
			-1.01500	-0.09351	0.01868	0.02099	0.03599	0.00367			
			0.07600	-0.06869	0.00771	0.01989	0.03689	0.00223			
			1.32200	-0.04703	-0.00286	0.01953	0.03999	0.00099			
			2.55900	-0.04265	-0.00910	0.01944	0.04062	-0.00040			
			3.53000	-0.03750	-0.01060	0.01638	0.03937	-0.00190			
			4.72600	-0.03981	-0.01349	0.01645	0.03397	-0.00320			
			7.03600	-0.02353	-0.01861	0.01230	0.02475	-0.00479			
			8.31100	-0.02443	-0.02191	0.00953	0.02640	-0.00470			
			9.42300	-0.00226	-0.02495	0.00963	0.02586	-0.00431			
			10.49100	0.02570	-0.02091	0.01262	0.03419	-0.00580			
			11.71200	0.04021	-0.01448	0.01142	0.03779	-0.00788			
			13.92100	0.01317	0.01273	0.00280	0.03294	-0.00872			
			16.10395	0.00864	0.00797	0.00430	0.03090	-0.01000			
			18.36600	-0.00672	0.00010	0.00186	0.02451	-0.00752			
0.9	K1	0/0	-2.18500	-0.05140	0.02420	0.01977	0.04654	0.00694	PWT 16T	59	52
			-0.82800	-0.03587	0.01549	0.02106	0.04680	0.00501			
			0.14700	-0.03181	0.00940	0.02087	0.04660	0.00339			
			1.46200	-0.01887	-0.00109	0.01980	0.04586	0.00159			
			2.65100	0.00055	-0.01023	0.01812	0.04108	-0.00040			
			4.95100	0.02931	-0.01292	0.01855	0.03200	-0.00290			
			7.42400	0.00426	0.00766	0.01661	0.02862	-0.00540			
			8.48400	-0.00407	0.00757	0.01673	0.02977	-0.00620			
			9.69800	-0.01175	0.00634	0.01698	0.02764	-0.00697			
			9.74600	-0.00937	0.00572	0.01728	0.02739	-0.00701			
			10.77600	-0.04937	0.01639	0.00921	0.01604	-0.00337			
			11.86000	-0.01961	0.00547	0.01480	0.01816	-0.00409			
			14.02900	-0.00622	0.00482	0.01557	0.02328	-0.00718			
			16.22600	-0.01787	0.00646	0.01349	0.01831	-0.00501			
			18.48395	-0.02060	0.00771	0.01146	0.01590	-0.00520			
			20.73439	-0.02328	0.01229	0.00798	0.01671	-0.00946			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.9	K1	5/0	-2.28600	-0.10326	0.03713	0.02195	0.03706	0.00536	PWT 16T	75	52
			-0.96000	-0.08063	0.02659	0.02174	0.03780	0.00390			
			0.11600	-0.05819	0.01321	0.02083	0.04080	0.00278			
			1.32500	-0.03296	-0.00235	0.02118	0.04257	0.00115			
			2.50100	-0.01325	-0.01457	0.02034	0.03858	-0.00071			
			3.85200	0.00234	-0.01929	0.01634	0.03178	-0.00240			
			4.87800	0.01035	-0.01863	0.01752	0.02851	-0.00330			
			7.29900	-0.00826	-0.01099	0.01331	0.02670	-0.00500			
			8.39700	-0.01524	-0.00403	0.01127	0.02629	-0.00530			
			9.50800	-0.02528	0.00294	0.00866	0.02490	-0.00561			
			10.67600	-0.00430	0.00322	0.01097	0.02345	-0.00511			
			11.89600	0.03594	0.00074	0.01577	0.02674	-0.00611			
			13.98700	-0.01529	0.01084	0.00467	0.02207	-0.00629			
			16.20499	-0.01548	0.00912	0.00544	0.01923	-0.00453			
			18.47099	-0.01794	0.00126	0.00533	0.01560	-0.00250			
			20.70299	-0.01505	-0.00043	0.00537	0.01586	-0.00620			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.9	1	10/0	-2.17100	-0.11836	0.03729	0.02727	0.03574	0.00404	PWT 16T	68	[illegible]
			-1.01900	-0.10586	0.03091	0.02405	0.03319	0.00239			
			0.04400	-0.08708	0.02328	0.02267	0.03420	0.00213			
			1.28500	-0.06421	0.01013	0.02271	0.03584	0.00044			
			2.40700	-0.04550	-0.00349	0.02154	0.03376	-0.00071			
			3.62600	-0.01821	-0.01340	0.01765	0.02882	-0.00230			
			5.01900	-0.00980	-0.01411	0.01847	0.02442	-0.00361			
			7.20400	-0.03626	-0.00825	0.01082	0.02167	-0.00489			
			8.46800	-0.04226	-0.01315	0.00894	0.02270	-0.00470			
			9.55800	-0.05844	-0.00564	0.00211	0.02122	-0.00450			
			10.62100	-0.03830	-0.00186	0.00350	0.02146	-0.00404			
			11.83500	0.01933	-0.01378	0.01036	0.02680	-0.00518			
			14.13300	0.02620	0.00368	0.00600	0.03218	-0.00949			
			16.23199	-0.01227	0.01010	-0.00108	0.02010	-0.00420			
			18.55899	-0.01527	0.01001	-0.00149	0.01780	-0.00262			
			20.70099	-0.01763	0.00359	-0.00352	0.01885	-0.00620			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.95	K1	0/0	-3.36800	-0.03002	0.02698	0.02075	0.04680	0.00830	PWT 16T	60	53
			-2.25900	-0.00778	0.01768	0.02209	0.05080	0.00640			
			-0.96500	0.00436	0.00897	0.02670	0.04970	0.00331			
			0.27700	-0.00092	0.00855	0.02655	0.04508	0.00139			
			0.63900	0.00267	0.00801	0.02587	0.04360	0.00073			
			1.45800	0.00591	0.00412	0.02637	0.04226	-0.00071			
			1.80400	0.00411	0.00197	0.02651	0.04152	-0.00117			
			2.67700	0.00727	-0.00080	0.02656	0.03981	-0.00242			
			5.02700	0.00488	-0.00703	0.02607	0.03630	-0.00580			
			7.30100	0.00175	-0.00038	0.02498	0.03310	-0.00840			
			8.62900	-0.00520	0.01023	0.02294	0.03150	-0.00970			
			9.81300	-0.01108	0.01473	0.02177	0.03010	-0.01071			
			10.96100	-0.01167	0.01373	0.02125	0.02901	-0.01169			
			12.14900	-0.01219	0.01362	0.02037	0.02850	-0.01250			
			14.37500	-0.01847	0.01093	0.01806	0.02510	-0.01460			
			16.77899	-0.02475	0.01313	0.01633	0.02629	-0.01777			
			18.93799	-0.06314	0.04114	0.00152	0.01913	-0.01446			
			21.13699	-0.04096	0.02253	0.00495	0.01471	-0.01654			

Table XII CONT'D

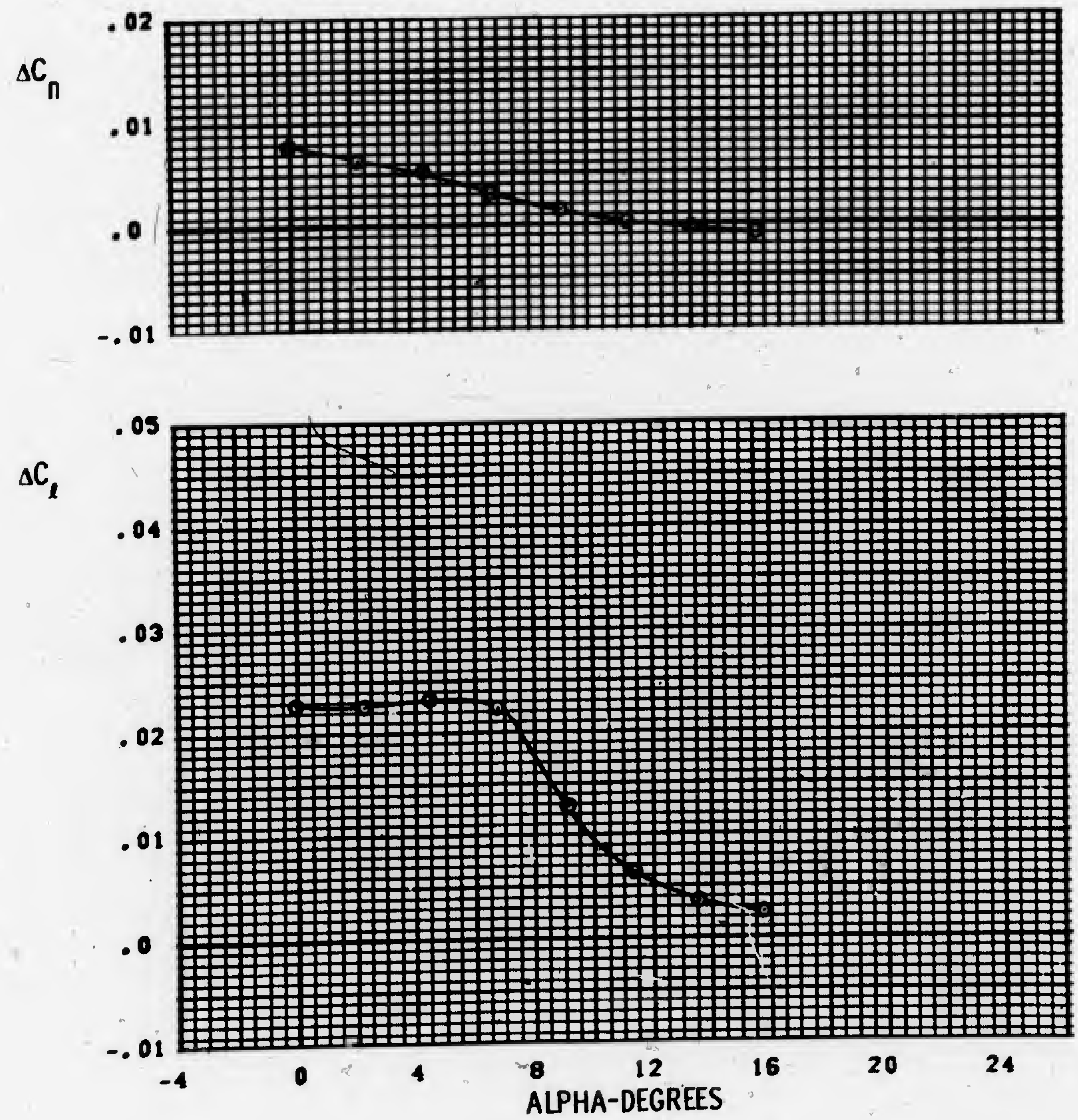
MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.95	K1	10/0	-2.35000	-0.07709	0.02533	0.02717	0.03840	0.00390	PWT 16T	69	53
			-1.21900	-0.09047	0.03263	0.02698	0.03402	0.00202			
			0.16900	-0.08197	0.03427	0.02734	0.02925	0.00005			
			1.41000	-0.06214	0.02084	0.02745	0.02903	-0.00151			
			2.59200	-0.04113	0.00563	0.02830	0.02910	-0.00320			
			3.84100	-0.03347	-0.00269	0.02627	0.02946	-0.00491			
			4.93700	-0.02777	-0.01081	0.02744	0.02879	-0.00609			
			7.32000	-0.03582	0.00103	0.02110	0.02380	-0.00740			
			8.44700	-0.04167	0.01117	0.01579	0.02219	-0.00769			
			9.80400	-0.04380	0.01633	0.01121	0.02130	-0.00801			
			10.97100	-0.04733	0.01401	0.00773	0.02201	-0.00799			
			12.12700	-0.04001	0.01066	0.00569	0.02290	-0.00810			
			14.43800	-0.03686	0.00565	0.00033	0.02343	-0.00951			
			16.62599	-0.02991	-0.00115	-0.00153	0.02496	-0.01155			
			18.95699	-0.02388	-0.00002	-0.00408	0.02772	-0.01334			
			21.22198	-0.01470	0.00563	-0.00707	0.02310	-0.01245			

Table XII CONT'D

MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
1.2	K1	0/0	-3.17600	-0.00017	0.00314	0.01734	0.02491	0.00741	PWT 16T	51	54
			-2.02800	0.00174	0.00517	0.01786	0.02583	0.00600			
			-1.02500	0.00688	0.00487	0.01837	0.02634	0.00515			
			0.15900	0.01289	0.00051	0.01928	0.02903	0.00348			
			1.23300	0.02011	0.00029	0.02013	0.03005	0.00192			
			2.42000	0.01749	0.00407	0.02102	0.03101	0.00150			
			4.79100	0.01647	0.01047	0.02140	0.03068	-0.00151			
			7.16100	0.01123	0.02079	0.02070	0.02801	-0.00421			
			8.39100	0.00351	0.02365	0.01985	0.02708	-0.00530			
			9.69900	0.00694	0.02039	0.01951	0.02668	-0.00612			
			10.66500	0.00314	0.02064	0.01890	0.02621	-0.00749			
			12.06400	-0.00285	0.02033	0.01713	0.02571	-0.00852			
			14.26400	-0.00798	0.02476	0.01521	0.02379	-0.01003			
			16.59290	-0.01435	0.02323	0.01390	0.02307	-0.01107			
			18.78600	-0.01939	0.02228	0.01110	0.02175	[illegible]			
			20.95300	-0.02243	0.02616	0.01064	[illegible]	[illegible]			
1.2	K1	10/0	-2.08900	-0.01321	-0.00151	0.02855	0.02031	0.002[illegible]	PWT 16T	[illegible]	54
			-1.14300	-0.02063	0.00223	0.02936	0.02040	0.00263			
			0.07800	-0.01891	0.00026	0.02920	0.02080	0.00175			
			1.16400	-0.02479	0.00622	0.02654	0.01943	-0.00026			
			2.42400	-0.02442	0.00804	0.02647	0.02021	-0.00100			
			3.54200	-0.02223	0.00772	0.02256	0.02063	-0.00101			
			4.72500	-0.02525	0.01288	0.02221	0.02047	-0.00231			
			7.08500	-0.02604	0.01782	0.01848	0.02040	-0.00230			
			8.40100	-0.02834	0.01844	0.01505	0.02044	-0.00359			
			9.40100	-0.02198	0.01570	0.01398	0.02022	-0.00450			
			10.60700	-0.02360	0.01611	0.01096	0.02001	[illegible]			
			11.38900	-0.02368	0.01781	0.00740	0.02[illegible]	-0.00543			
			14.30600	-0.02500	0.01303	0.00247	0.02019	-0.00654			
			16.47695	-0.02715	0.01[illegible]	-0.00053	0.02109	-0.00711			
			19.35699	-0.02561	0.01579	-0.00384	0.02022	-0.00742			

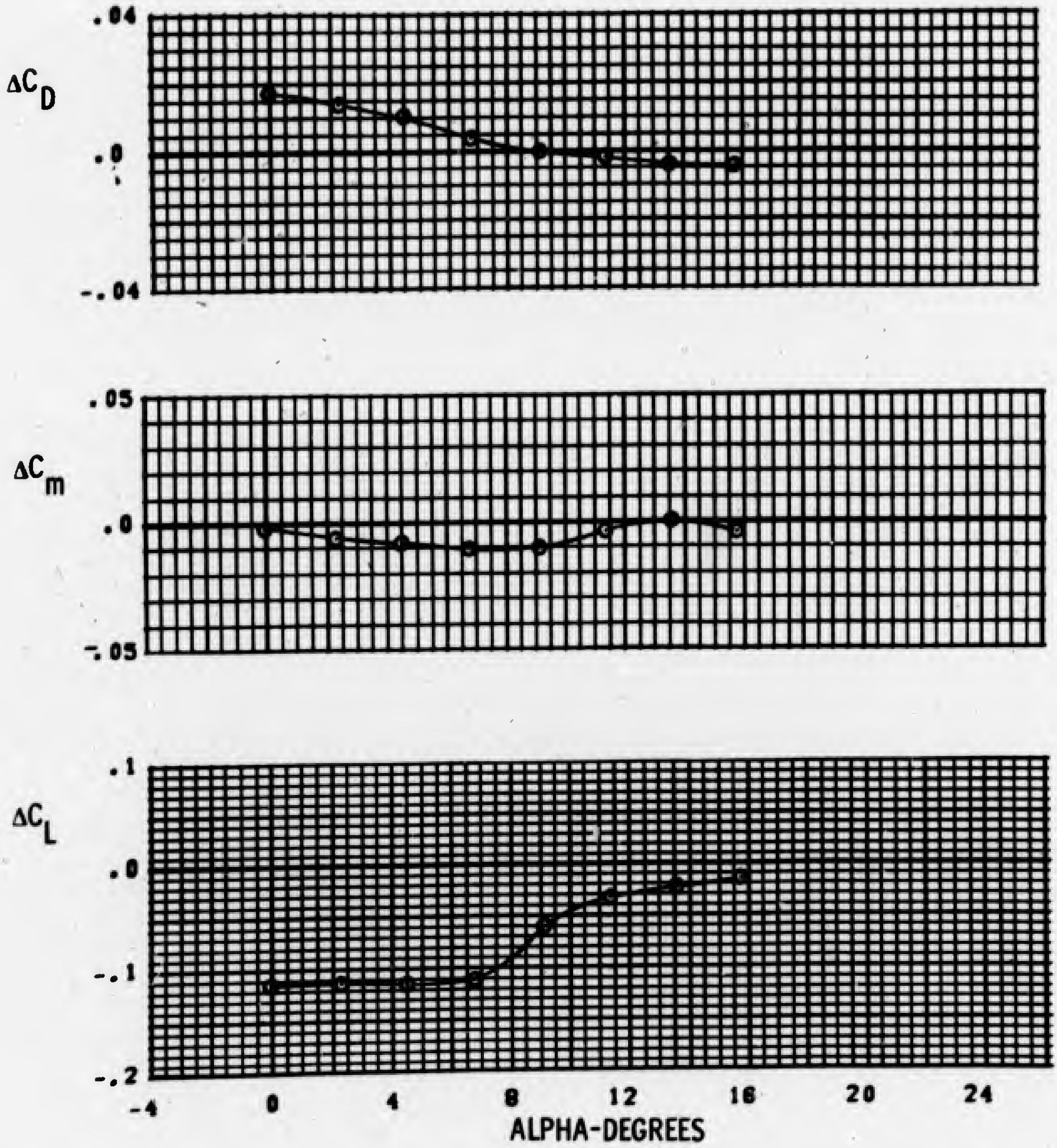
4. VENTED SPOILER

Plotted incremental characteristics for the vented spoiler are shown in Figure 129. Corresponding numeral values are given in Table XIII.



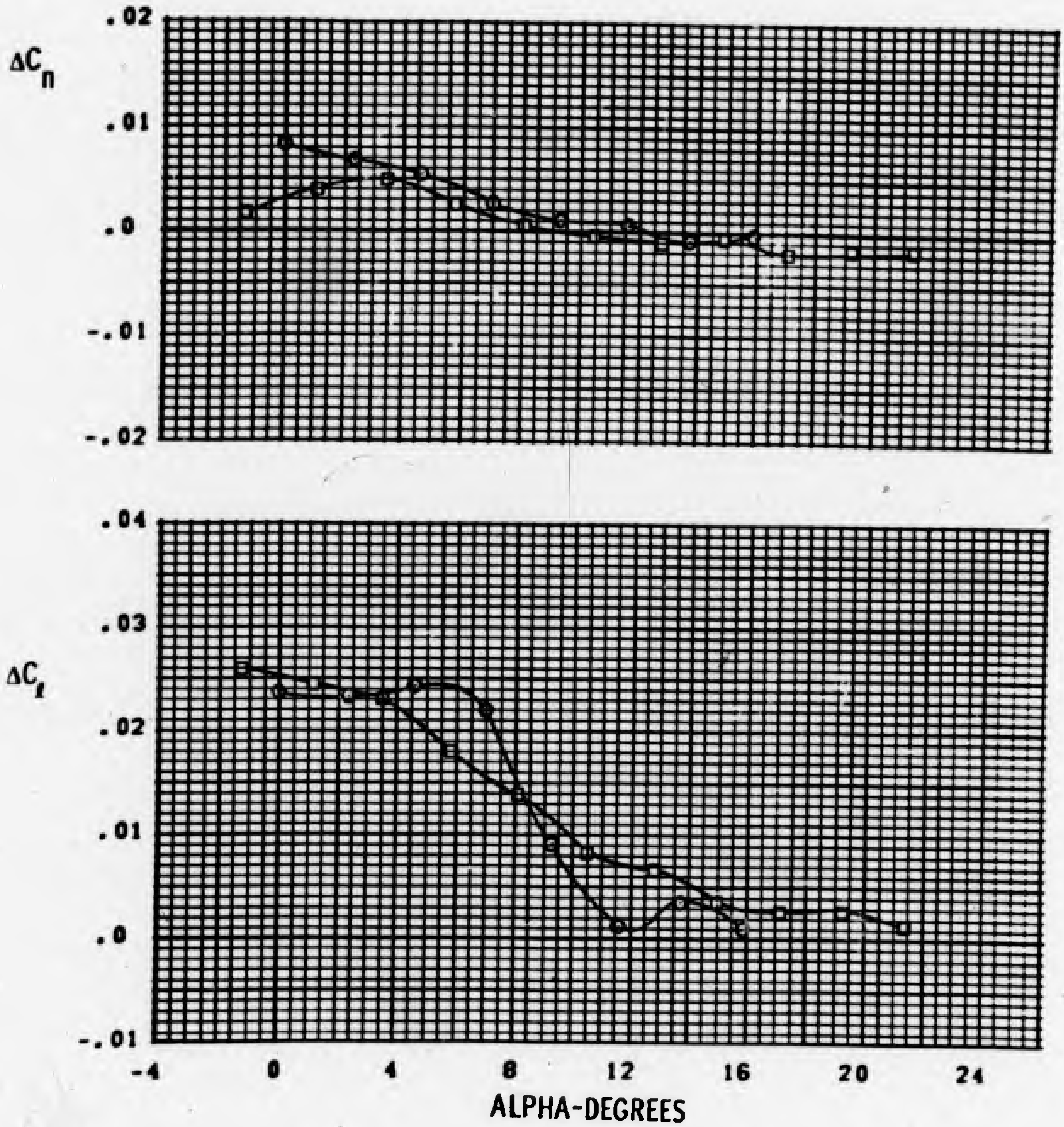
SYM	TEST	INCREMENT	L.E. (L/R)	SPOILER
⊙	PWT 4T TC-043	PN 461 -PN 438	K1 0/0	RH -90

FIGURE 129a VENTED SPOILER EFFECTS
M = 0.7



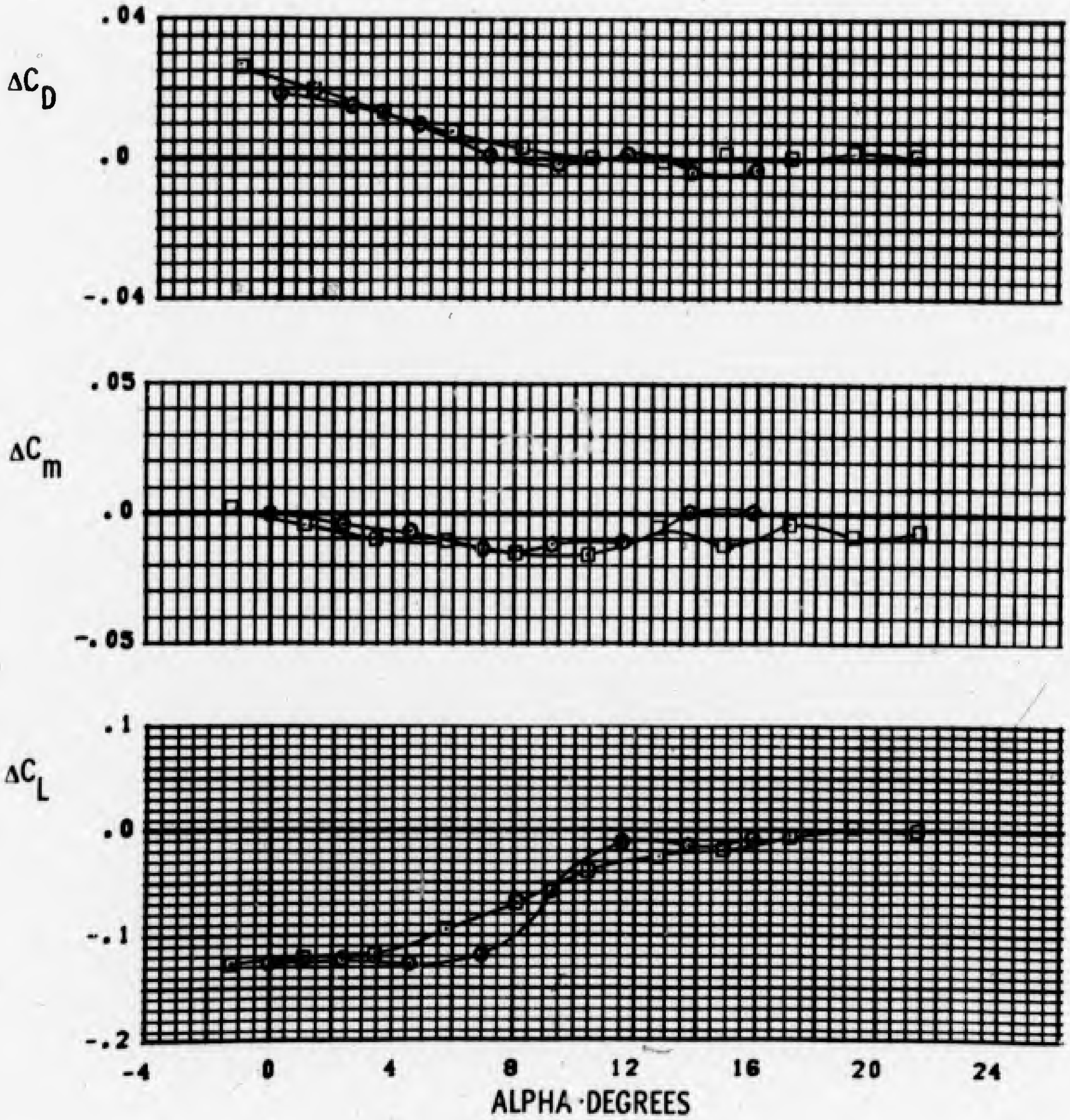
SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 461 -PN 438	K1	0/0	RH -90

FIGURE 129a VENTED SPOILER EFFECTS
M = 0.7



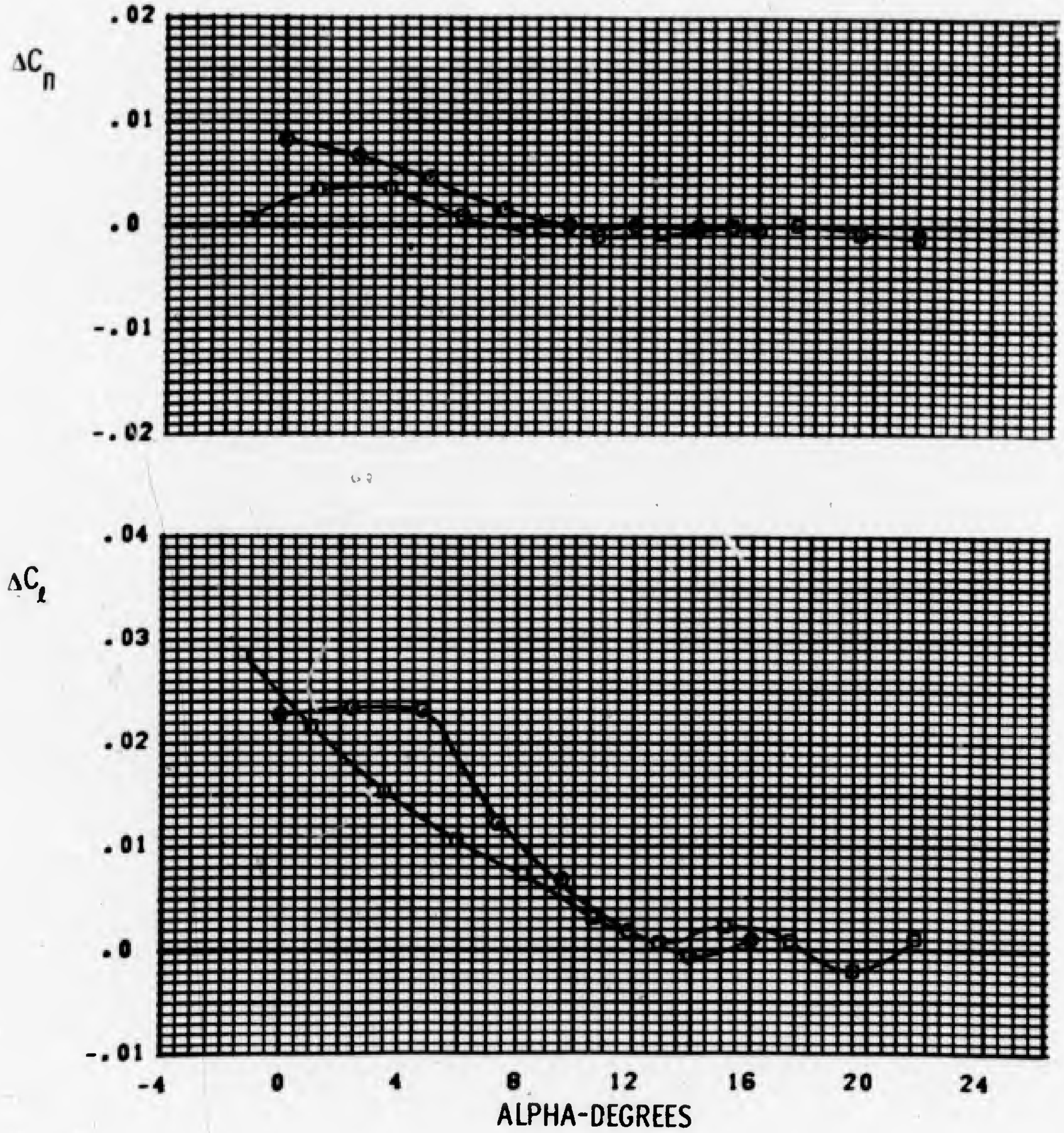
SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 462 -PN 440	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 173 -PN 127	K1	10/10	RH -90

FIGURE 129b VENTED SPOILER EFFECTS
M = 0.8



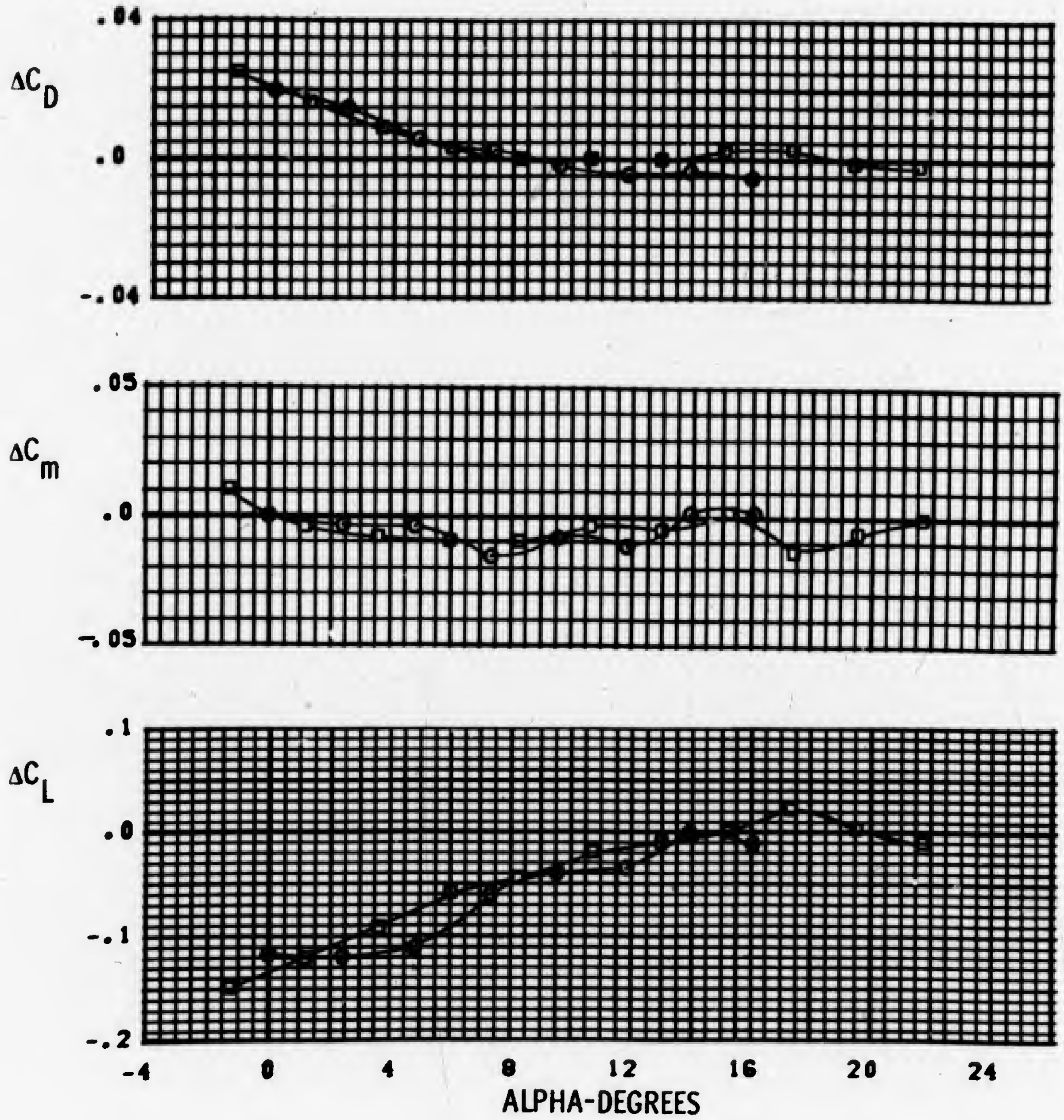
SYM	TEST	INCREMENT	L...	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 462 -PN 440	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 173 -PN 127	K1	10/10	RH -90

FIGURE 129b VENTED SPOILER EFFECTS
M = 0.8



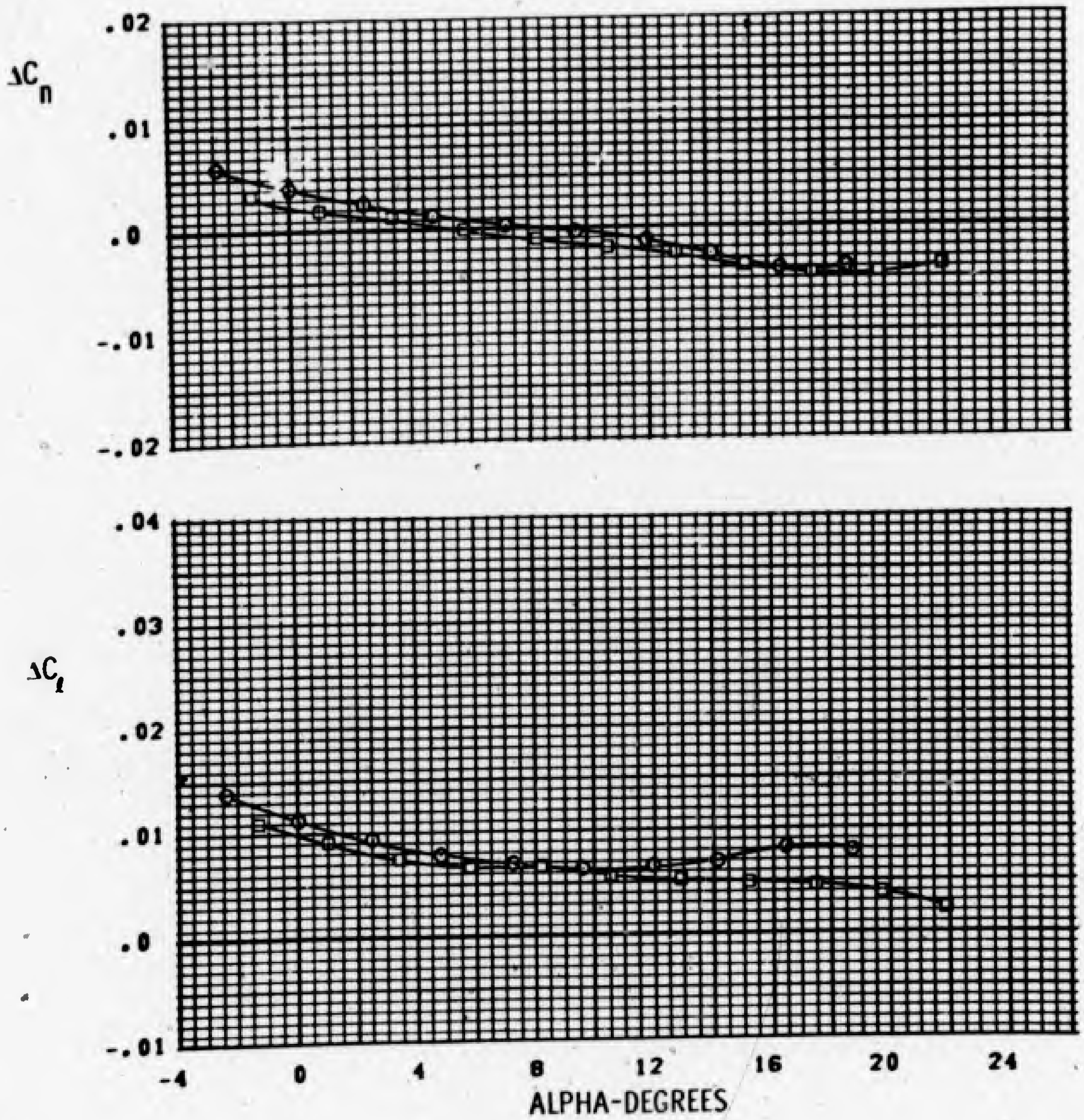
SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 460 -PN 441	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 172 -PN 126	K1	10/10	RH -90

FIGURE 129c VENTED SPOILER EFFECTS
M = 0.9



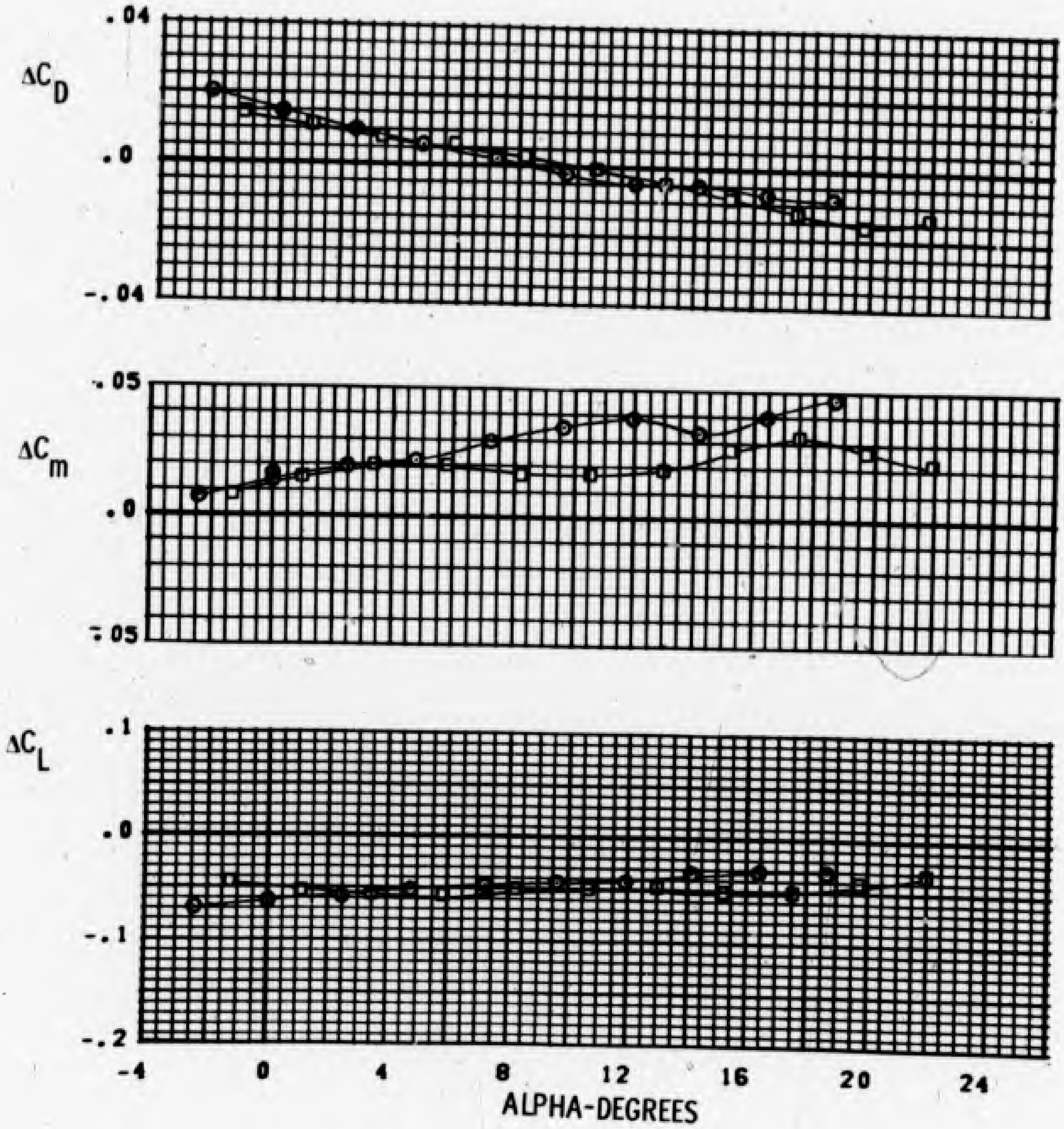
SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 460 -PN 441	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 172 -PN 126	K1	10/10	RH -90

FIGURE 129c VENTED SPOILER EFFECTS
M = 0.9



SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 463 -PN 269	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 174 -PN 129	K1	10/10	RH -90

FIGURE 129d VENTED SPOILER EFFECTS
M = 1.2



SYM	TEST	INCREMENT	L.E.	(L/R)	SPOILER
⊙	PWT 4T TC-043	PN 463 -PN 269	K1	0/0	RH -90
⊡	PWT 4T TC-043	PN 174 -PN 129	K1	10/10	RH -90

FIGURE 129d VENTED SPOILER EFFECTS
M = 1.2

Table XIII VENTED SPOILER CONTROL INCREMENTAL DATA SUMMARY

Right Hand Spoiler Deflected 90^{0} Up — Ailerons Neutral

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
0.7	K1	0/0	-0.05400	-0.11500	-0.00173	0.01734	0.02277	0.00783	PWT 4T	461	438
			2.27100	-0.11389	-0.00583	0.01390	0.02252	0.00632			
			4.48400	-0.11539	-0.00744	0.01082	0.02321	0.00520			
			6.77800	-0.11111	-0.01008	0.00409	0.02228	0.00311			
			9.12500	-0.06052	-0.00984	0.00011	0.01270	0.00142			
			11.36600	-0.03283	-0.00335	-0.00171	0.00630	0.00020			
			13.56300	-0.02270	0.00055	-0.00397	0.00350	-0.00040			
			15.74000	-0.01501	-0.00379	-0.00433	0.00238	-0.00089			
0.8	K1	0/0	-0.01300	-0.12586	0.00013	0.01855	0.02368	0.00833	PWT 4T	462	440
			2.34200	-0.12225	-0.00391	0.01518	0.02332	0.00672			
			4.60800	-0.12689	-0.00667	0.00963	0.02431	0.00541			
			6.97600	-0.11777	-0.01343	0.00105	0.02202	0.00263			
			9.26800	-0.05805	-0.01175	-0.00144	0.00910	0.00112			
			11.58700	-0.01101	-0.01086	0.00119	0.00119	0.00070			
			13.75100	-0.01529	0.00075	-0.00363	0.00351	-0.00080			
			15.89300	-0.00796	0.00085	-0.00316	0.00090	-0.00020			
0.8	K1	10/10	-1.27100	-0.12607	0.00255	0.02581	0.02586	0.00185	PWT 4T	173	127
			1.10000	-0.12077	-0.00373	0.01946	0.02438	0.00414			
			3.41800	-0.11662	-0.00890	0.01367	0.02293	0.00500			
			5.76000	-0.09394	-0.01038	0.00766	0.01800	0.00266			
			8.08600	-0.06799	-0.01412	0.00296	0.01371	0.00072			
			10.43900	-0.03785	-0.01549	0.00014	0.00809	-0.00023			
			12.74200	-0.02518	-0.00479	-0.00099	0.00656	-0.00087			
			14.91700	-0.01684	-0.01130	0.00089	0.00352	-0.00050			
			17.09200	-0.00642	-0.00291	-0.00007	0.00240	-0.00170			
			19.19899	0.00263	-0.00735	0.00151	0.00250	-0.00152			
			21.38599	-0.00041	-0.00597	0.00065	0.00120	-0.00131			

Table XIII CONT'D

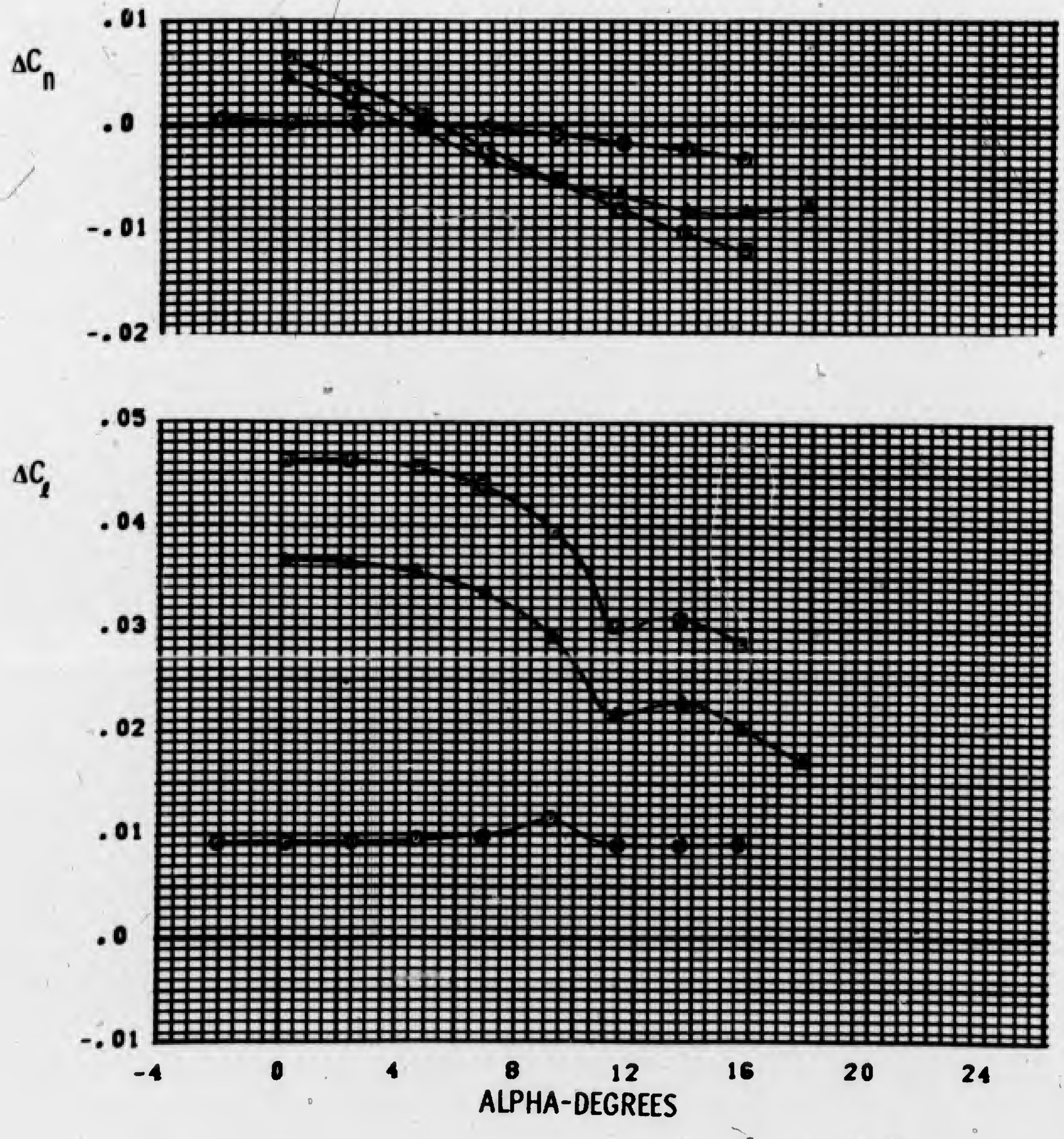
MACH	L.E. FLAP		ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE		
	TYPE	DEFL (L/R)							TUNNEL	DATA RUN	BASE RUN
0.9	K1	0/0	0.00700	-0.11732	0.00040	0.02003	0.02278	0.00831	PWT 4T	460	441
			2.42200	-0.11988	-0.00331	0.01501	0.02339	0.00671			
			4.81200	-0.11142	-0.00334	0.00589	0.02321	0.00451			
			7.37100	-0.06020	-0.01517	0.00274	0.01229	0.00150			
			9.57100	-0.03904	-0.00806	-0.00180	0.00674	0.00001			
			11.85400	-0.03470	-0.01096	-0.00432	0.00180	-0.00000			
			13.94200	-0.00074	0.00179	-0.00329	-0.00059	-0.00019			
			16.06898	-0.01169	0.00162	-0.00519	0.00093	-0.00051			
0.9	K1	10/10	-1.31500	-0.14726	0.01165	0.02518	0.02893	0.00059	PWT 4T	172	126
			1.09000	-0.11778	-0.00333	0.01663	0.02180	0.00363			
			3.55200	-0.09047	-0.00741	0.00928	0.01548	0.00369			
			5.94200	-0.05739	-0.00884	0.00358	0.01060	0.00091			
			8.24000	-0.04338	-0.00899	0.00033	0.00748	-0.00039			
			10.61200	-0.01842	-0.00337	-0.00002	0.00328	-0.00117			
			12.87000	-0.01087	-0.00417	-0.00004	0.00076	-0.00079			
			15.14400	0.00189	0.00287	0.00211	0.00238	-0.00011			
			17.37299	0.02393	-0.01224	0.00348	0.00100	0.00010			
			19.48700	0.00513	-0.00552	-0.00044	-0.00190	-0.00090			
			21.60999	-0.00800	0.00037	-0.00193	0.00109	-0.00130			
1.2	K1	0/0	-2.38200	-0.06908	0.00764	0.02029	0.01386	0.00610	PWT 4T	463	269
			0.01600	-0.06347	0.01646	0.01467	0.01123	0.00399			
			0.03800	-0.06224	0.01365	0.01513	0.01134	0.00409			
			2.51500	-0.05855	0.01959	0.00991	0.00925	0.00255			
			4.78900	-0.05145	0.02184	0.00594	0.00774	0.00128			
			7.23900	-0.04721	0.02918	0.00203	0.00685	0.00030			
			9.62100	-0.04405	0.03504	-0.00206	0.00635	-0.00035			
			11.95700	-0.04248	0.03850	-0.00468	0.00649	-0.00127			
			14.16400	-0.03361	0.03327	-0.00516	0.00685	-0.00255			
			16.46300	-0.03141	0.04009	-0.00744	0.00819	-0.00400			
			18.70000	-0.03163	0.04687	-0.00844	0.00778	-0.00388			

Table XIII CONT'D

MACH	L.E. FLAP TYPE	L.E. FLAP DEFL (L/R)	ALPHA	ΔC_L	ΔC_m	ΔC_D	ΔC_ℓ	ΔC_n	TEST REFERENCE TUNNEL	TEST REFERENCE DATA RUN	TEST REFERENCE BASE RUN
1.2	K1	10/10	-1.28300	-0.04360	0.00746	0.01498	0.01129	0.00340	PWT 4T	174	129
			1.05600	-0.05333	0.01517	0.01175	0.00939	0.00200			
			3.40900	-0.05498	0.01912	0.00865	0.00780	0.00131			
			5.84300	-0.05732	0.02019	0.00624	0.00680	0.00020			
			8.23200	-0.05035	0.01652	0.00335	0.00675	-0.00089			
			10.60800	-0.04845	0.01653	-0.00018	0.00597	-0.00188			
			12.93500	-0.04723	0.01909	-0.00419	0.00539	-0.00251			
			15.24300	-0.05243	0.02683	-0.00822	0.00500	-0.00360			
			17.52800	-0.05024	0.03210	-0.01249	0.00471	-0.00449			
			19.75000	-0.04233	0.02700	-0.01524	0.00389	-0.00450			
			21.95200	-0.03358	0.02222	-0.01306	0.00225	-0.00376			

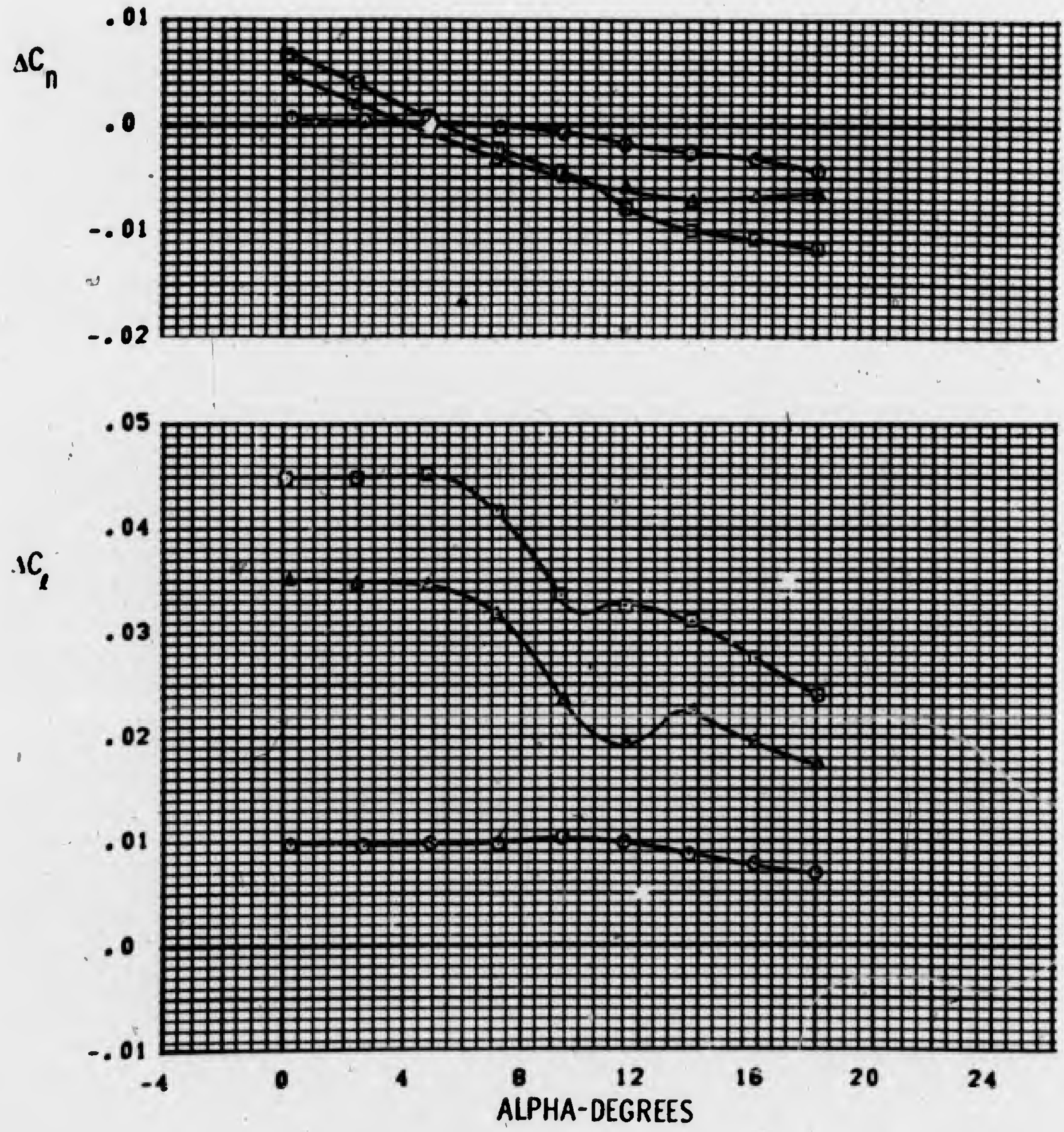
5. DIFFERENTIAL HORIZONTAL TAIL

Plotted comparison of lateral-directional moments for differential horizontal tail deflection used to provide roll control are given in Figure 130. Data is shown for the combined deflection of the mid-ailerons and horizontal tail and for the two devices used individually.



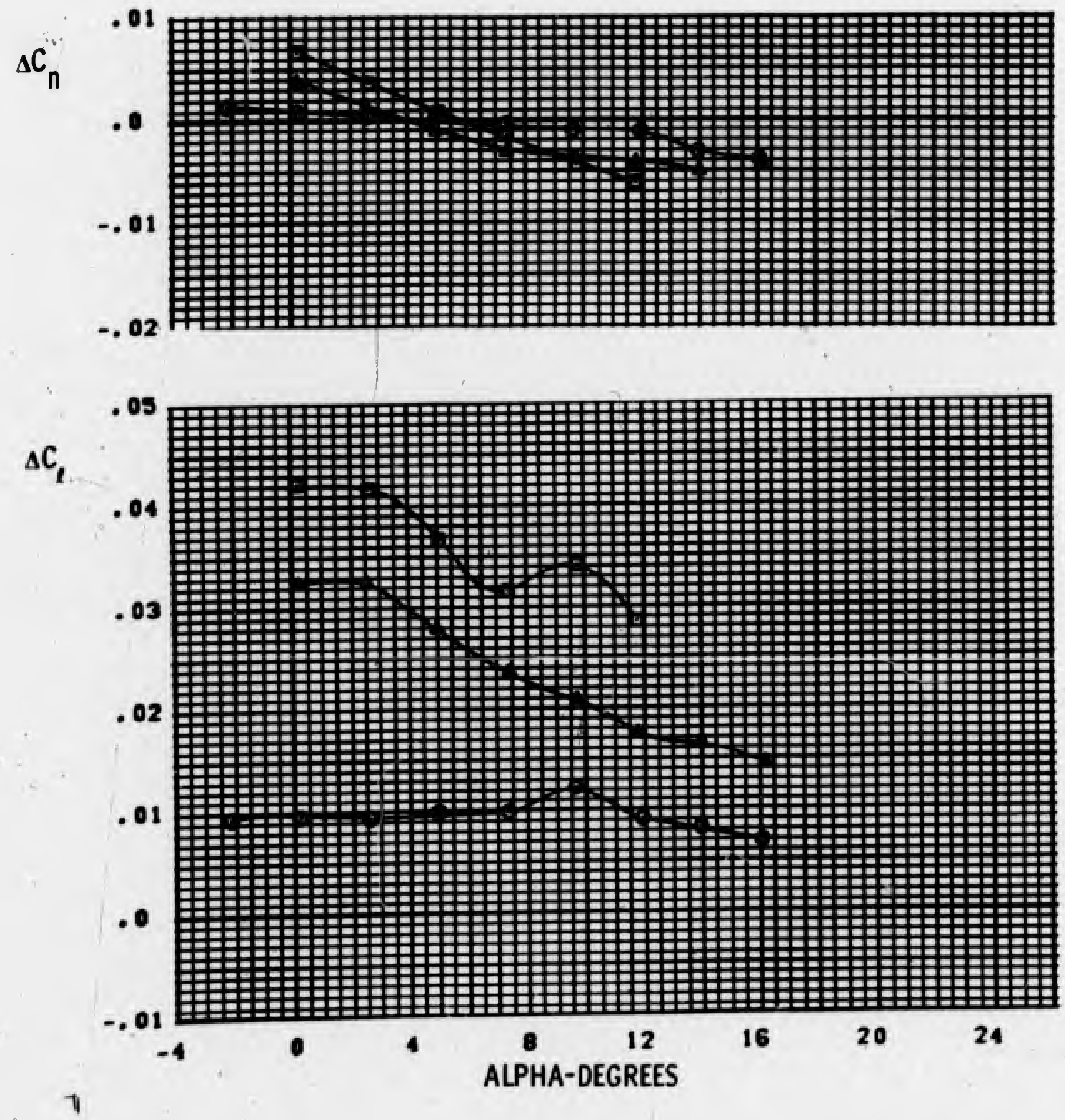
SYM	TEST	INCREMENT	HORIZ. TAIL (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 486 -PN 438	4/-4	NONE
⊡	PWT 4T TC-043	PN 492 -PN 438	4/-4	MID 20/-20
▲	PWT 4T TC-043	PN 410 -PN 438	0/0	MID 20/-20

FIGURE 130a DIFFERENTIAL HORIZONTAL TAIL EFFECTS (CLEAN L.E.)
M = 0.7



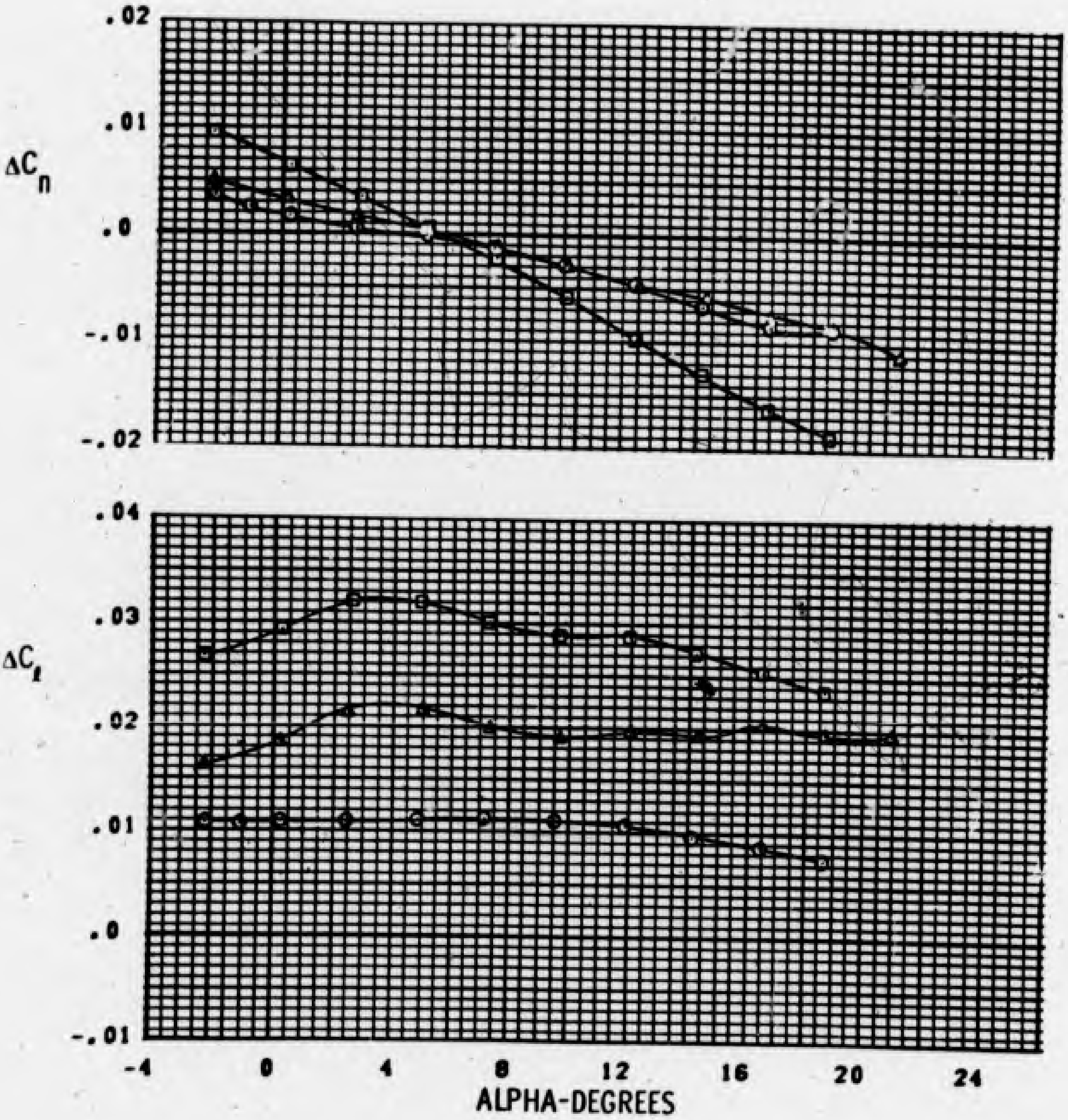
SYM	TEST	INCREMENT	HORIZ. TAIL (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 487 -PN 440	4/-4	NONE
⊡	PWT 4T TC-043	PN 493 -PN 440	4/-4	MID 20/-20
▲	PWT 4T TC-043	PN 411 -PN 440	0/0	MID 20/-20

FIGURE 130b DIFFERENTIAL HORIZONTAL TAIL EFFECTS (CLEAN L.E.)
M = 0.8



SYM	TEST	INCREMENT	HORIZ. TAIL (L/R)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 488 -PN 441	4/-4	NONE
⊡	PWT 4T TC-043	PN 494 -PN 441	4/-4	MID 20/-20
▲	PWT 4T TC-043	PN 412 -PN 441	0/0	MID 20/-20

FIGURE 130c DIFFERENTIAL HORIZONTAL TAIL EFFECTS (CLEAN L.E.)
M = 0.9

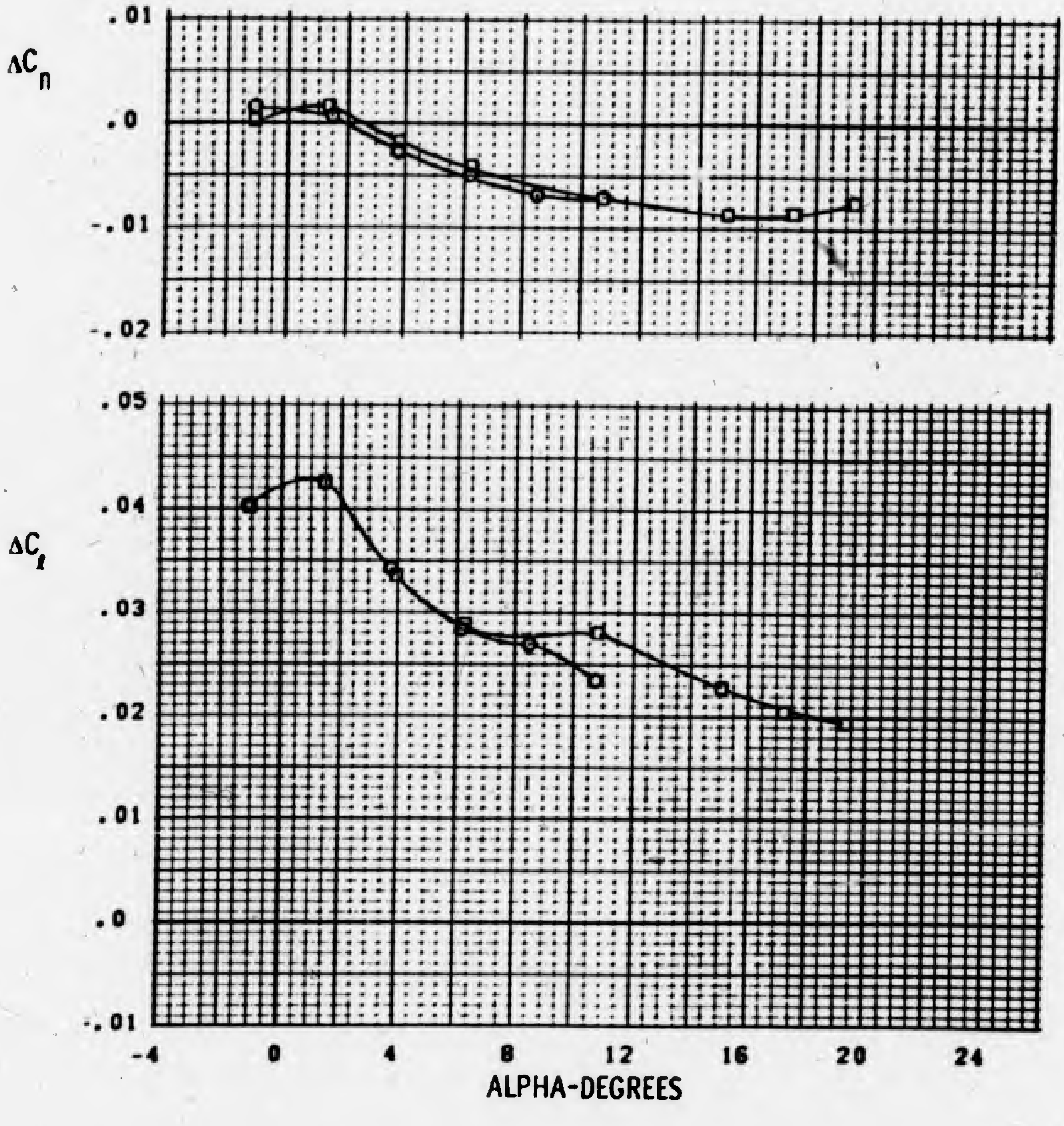


SYM		TEST	INCREMENT	HORIZ. TAIL (L/R)	AILERON (L/R)
⊙	PWT	4T TC-043	PN 489 -PN 269	4/-4	NONE
⊡	PWT	4T TC-043	PN 495 -PN 269	4/-4	MID 20/-20
▲	PWT	4T TC-043	PN 414 -PN 269	0/0	MID 20/-20

FIGURE 130d DIFFERENTIAL HORIZONTAL TAIL EFFECTS (CLEAN L.E.)
M = 1.2

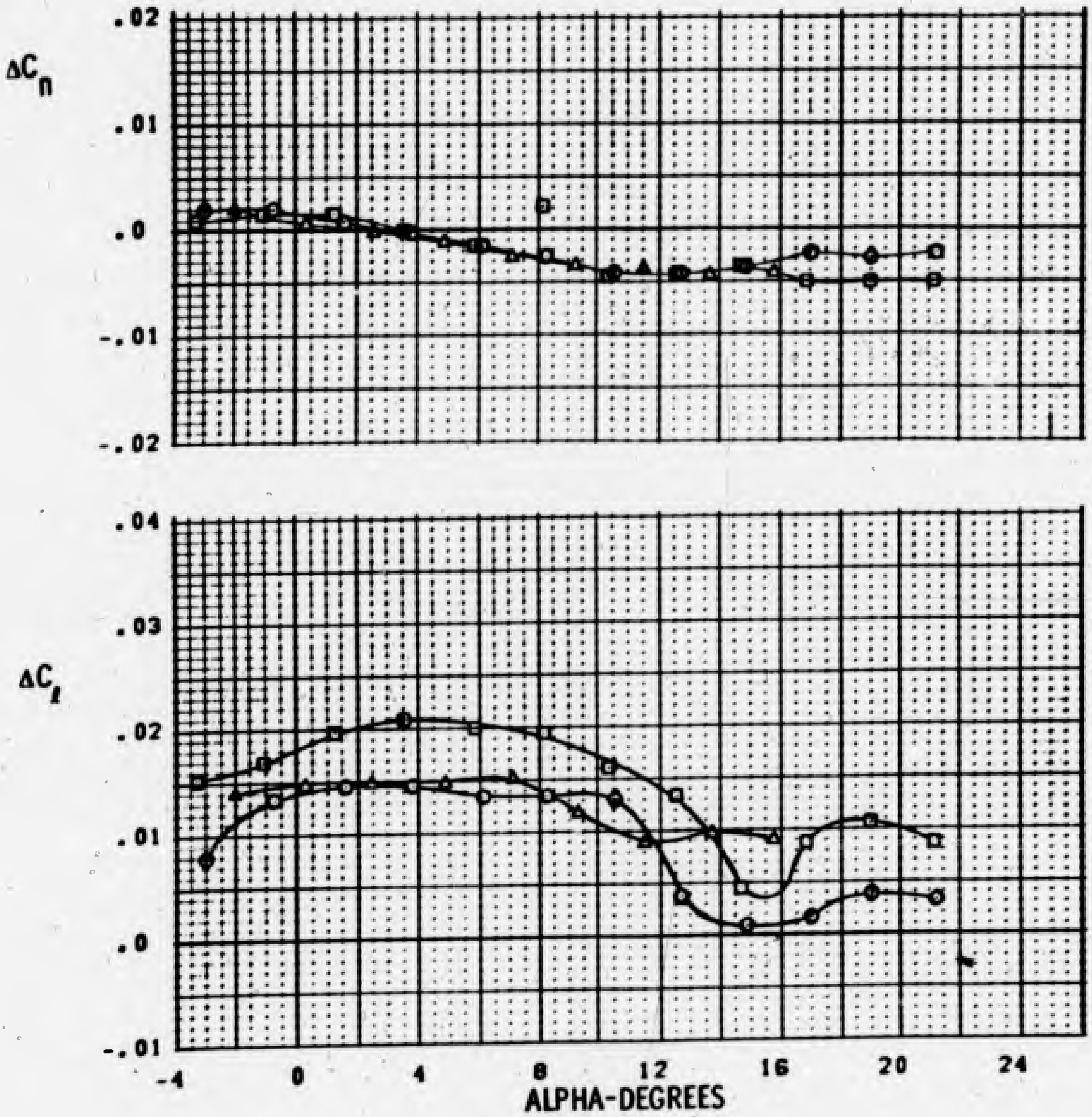
6. AUXILIARY DEVICES

Plotted data for the various devices investigated as aids to improve roll control are given in this subsection. Figure 131 illustrates typical vortex generator effects. Changes in longitudinal as well as lateral-directional characteristics resulting from trailing edge droop are shown in Figure 132. Representative effects produced with split trailing edge flaps are given in Figure 133. Figures 134 thru 136 illustrate that both the Kruger flap on the glove leading edge and the canopy fairing have neglibible effects on aileron characteristics.



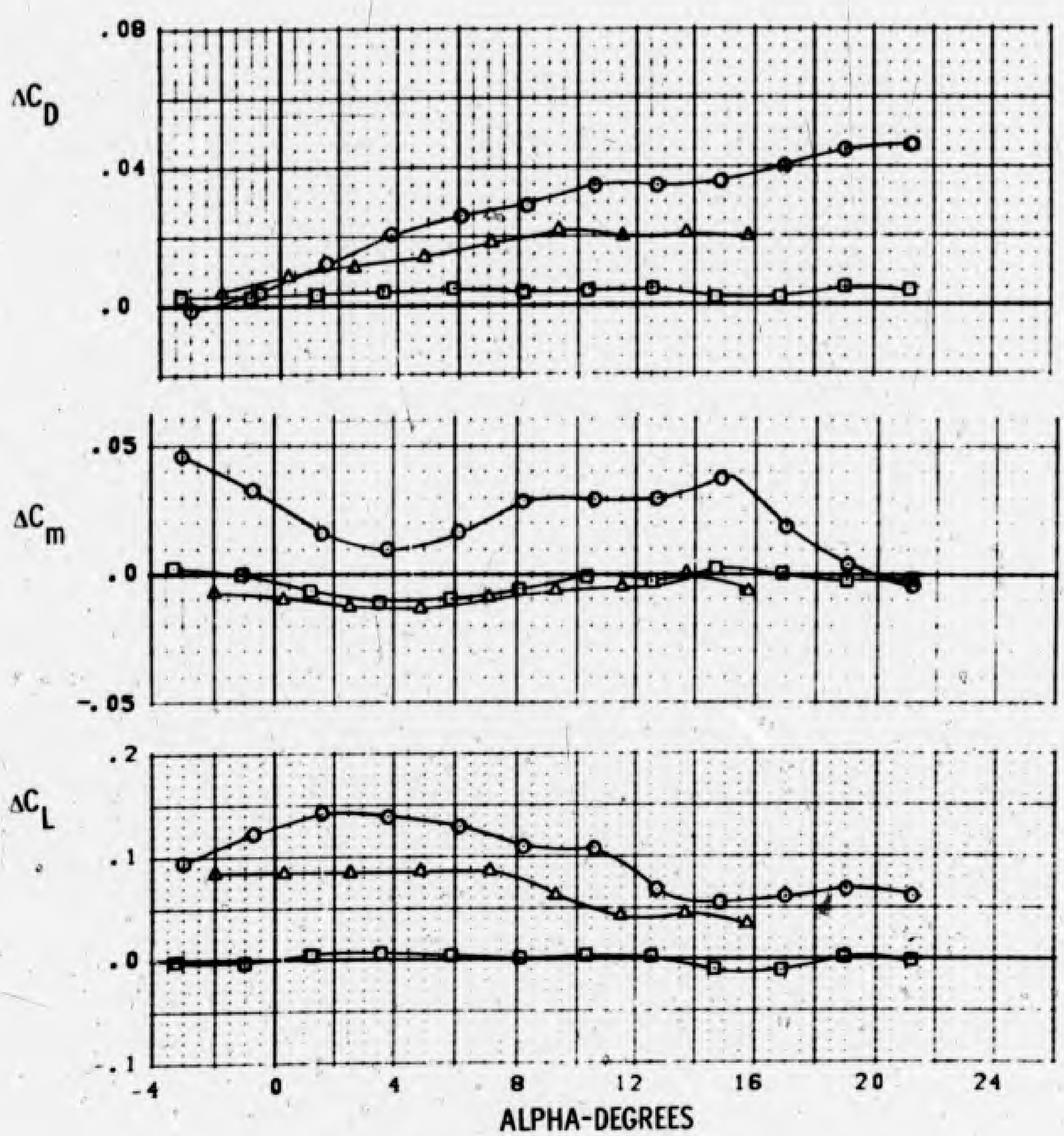
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)
⊙	PWT 4T TC-043	PN 303 -PN 445	K1	5/5	3 SEGM. 20/-20
⊡	PWT 4T TC-043	PN 227 -PN 241	K1+VG	5/5	3 SEGM. 20/-20

FIGURE 131 VORTEX GENERATOR EFFECTS ON EXTENDED SPAN AILERONS
M = 0.9



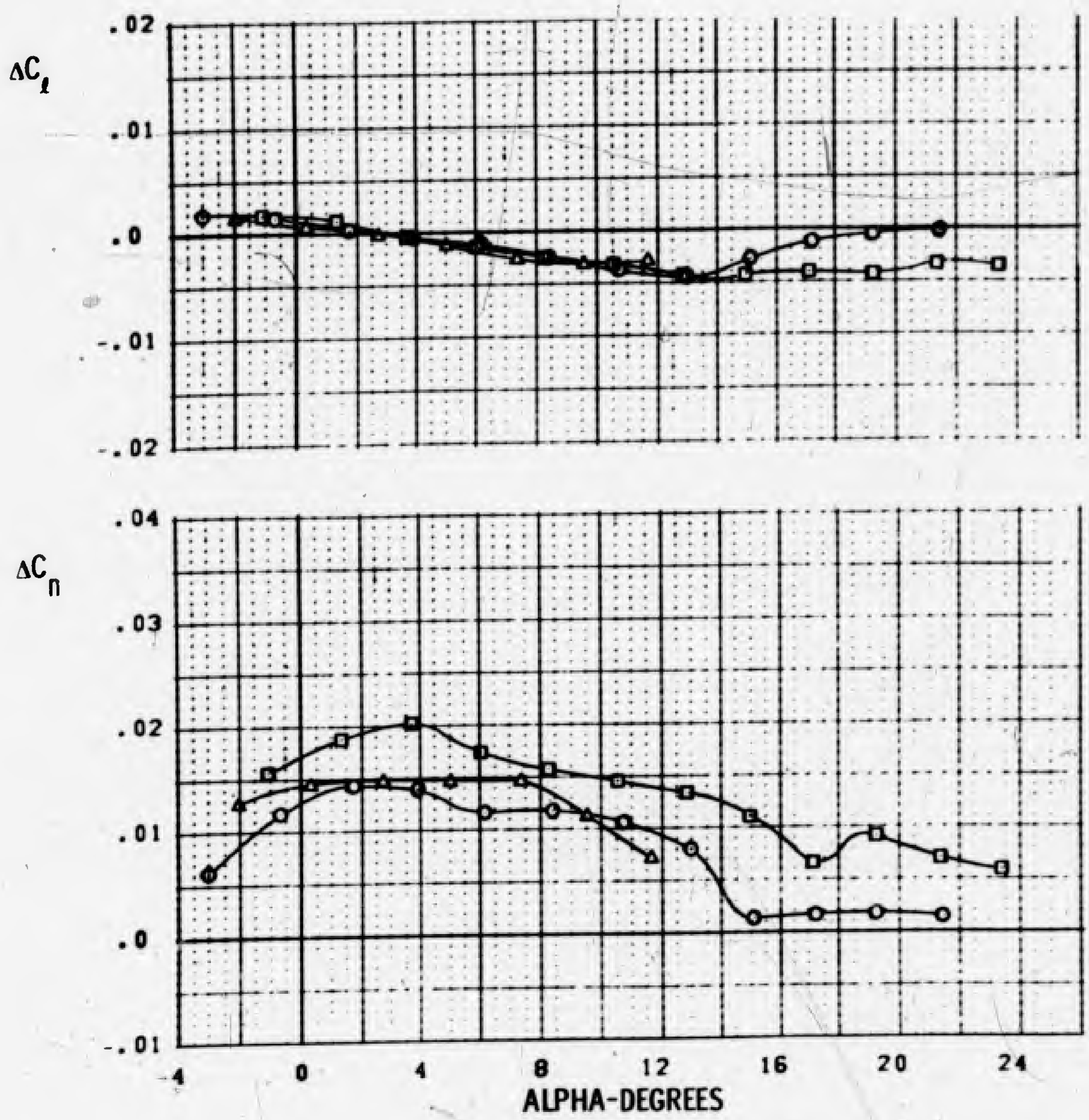
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
○	PWT 4T TC-043	PN 202 -PN 128	K1	10/10	MID	20/0 +10 DROOP
□	PWT 4T TC-043	PN 135 -PN 128	K1	10/10	MID	10/-10
△	PWT 4T TC-043	PN 468 -PN 438	K1	0/0	MID	20/0

FIGURE 132a TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.7



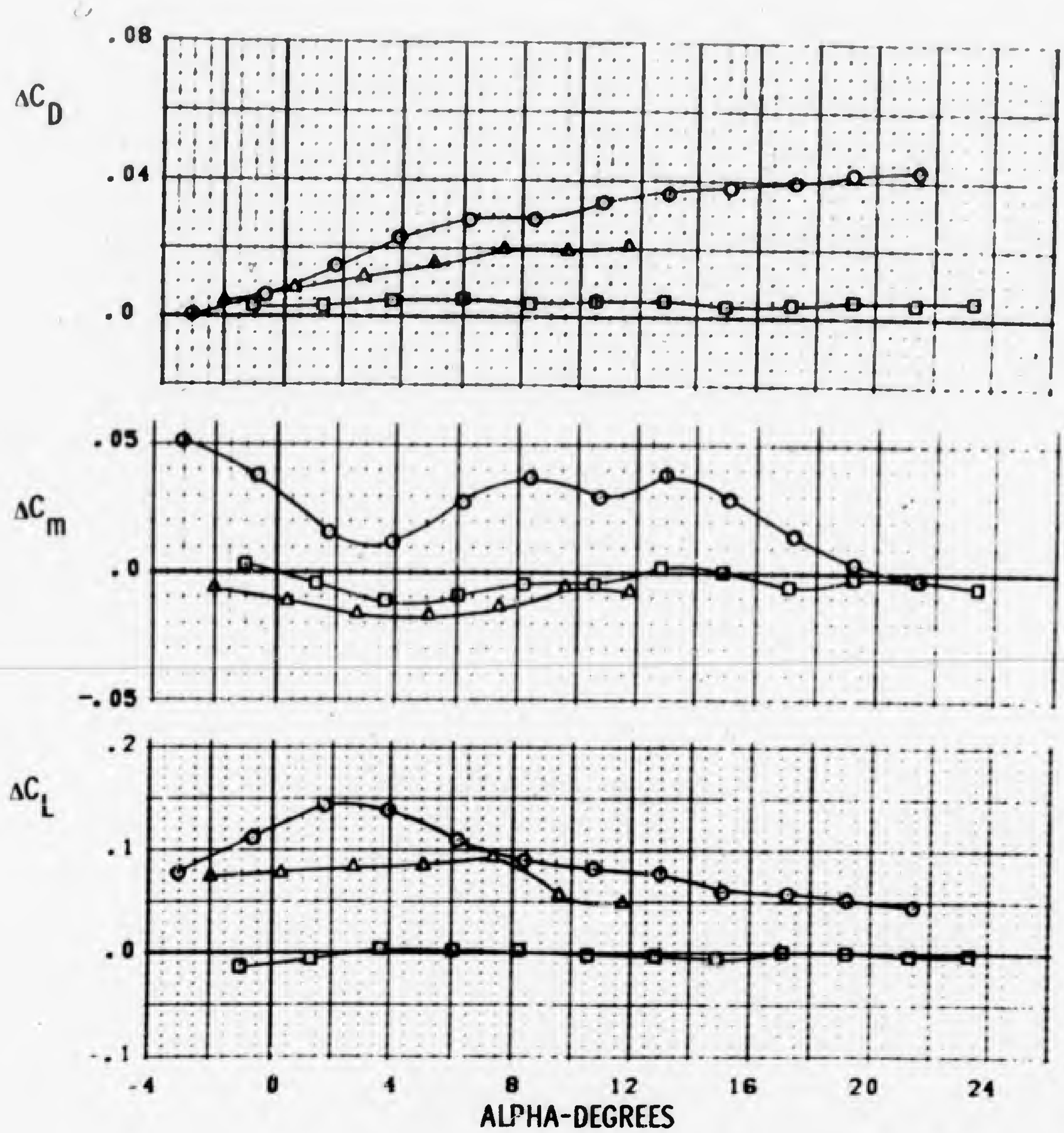
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 202 -PN 128	K1	10/10	MID	20/0 +10 DROOP
⊡	PWT 4T TC-043	PN 135 -PN 128	K1	10/10	MID	10/-10
△	PWT 4T TC-043	PN 468 -PN 438	K1	0/0	MID	20/0

FIGURE 132a TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.7



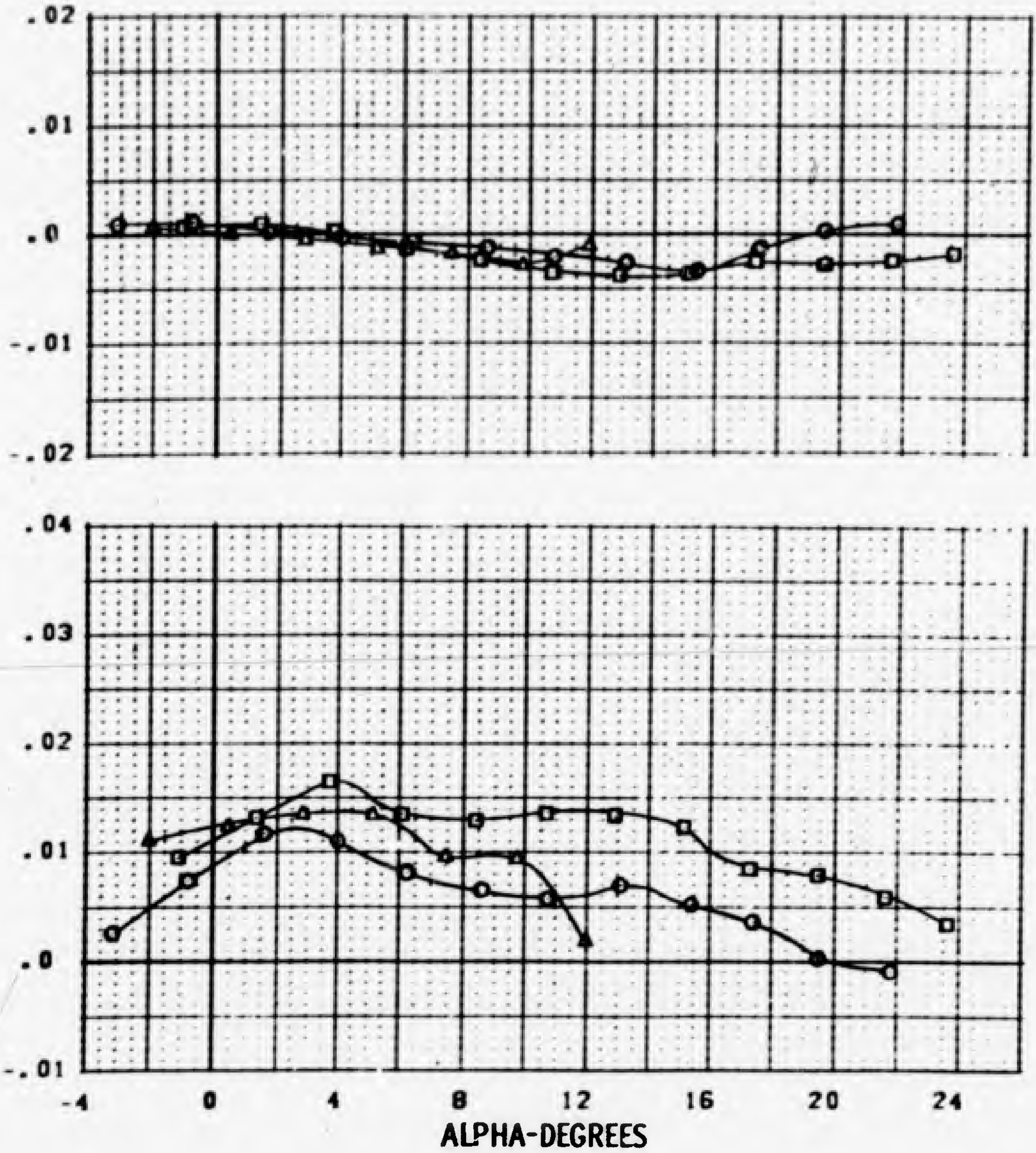
SYM	TEST	INCREMENT	L.E.	(L/R)	AILERON	(L/R)
○	PWT 4T TC-043	PN 200 -PN 127	K1	10/10	MID	20/0 +10 DROOP
□	PWT 4T TC-043	PN 134 -PN 127	K1	10/10	MID	10/-10
△	PWT 4T TC-043	PN 469 -PN 440	K1	0/0	MID	20/0

FIGURE 132b TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.8



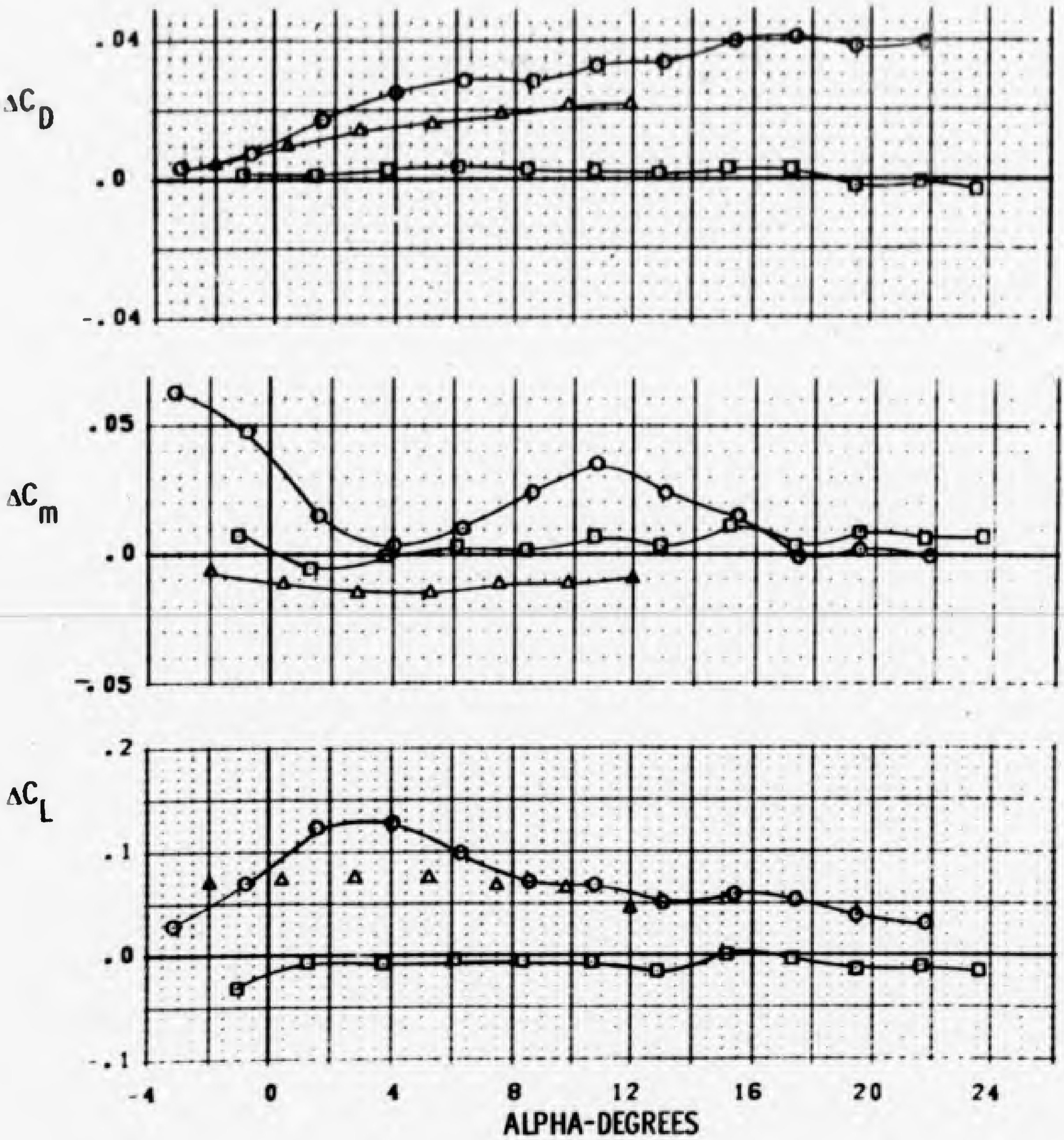
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
O	PWT 4T TC-043	PN 200 -PN 127	K1	10/10	MID	20/0 +10 DROOP
□	PWT 4T TC-043	PN 134 -PN 127	K1	10/10	MID	10/-10
Δ	PWT 4T TC-043	PN 469 -PN 440	K1	0/0	MID	20/0

FIGURE 132b TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.8



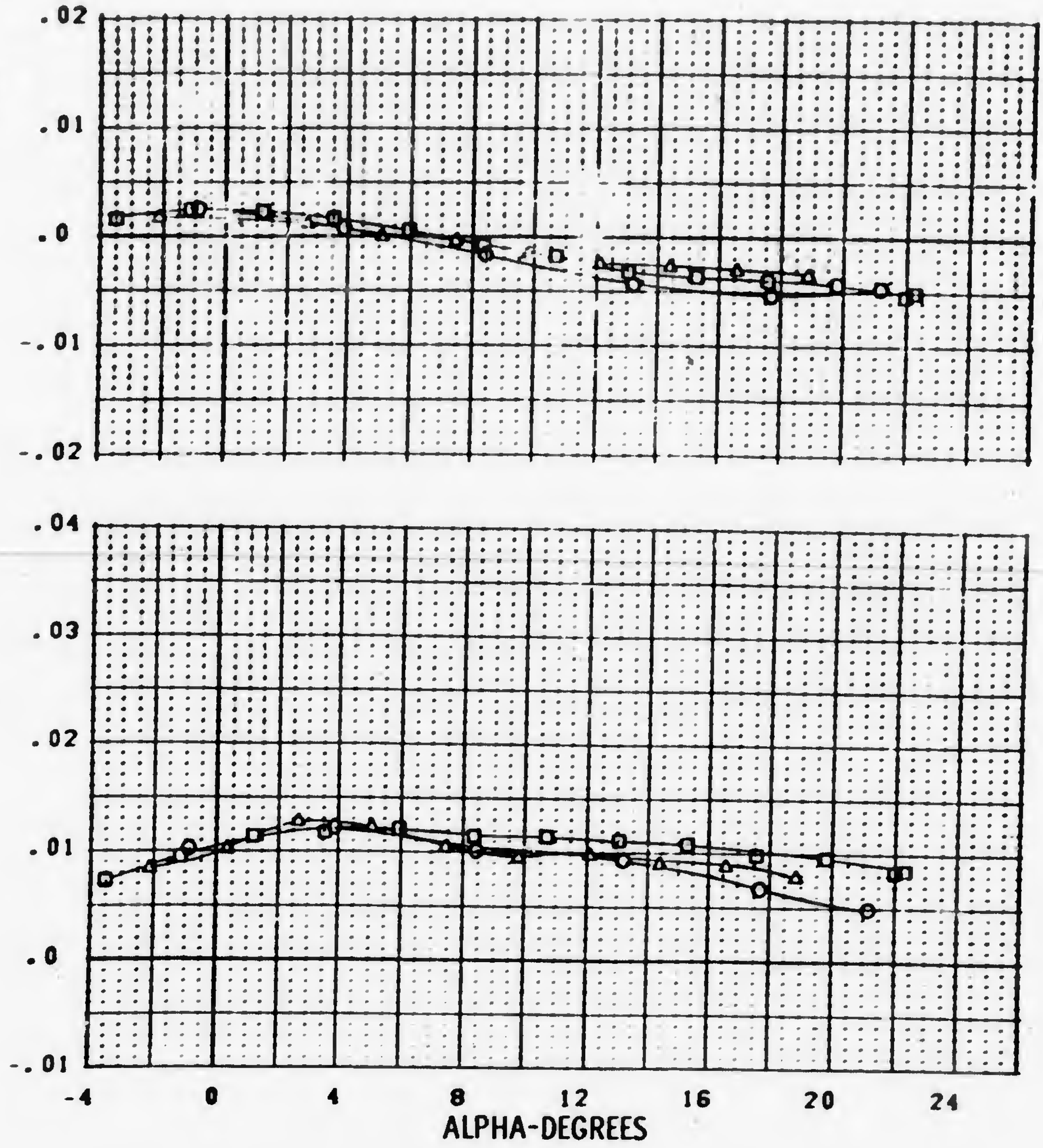
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
O	PWT 4T TC-043	PN 199 -PN 126	K1	10/10	MID	20/0 +10 DROOP
□	PWT 4T TC-043	PN 133 -PN 126	K1	10/10	MID	10/-10
Δ	PWT 4T TC-043	PN 467 -PN 441	K1	0/0	MID	20/0

FIGURE 132c TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.9



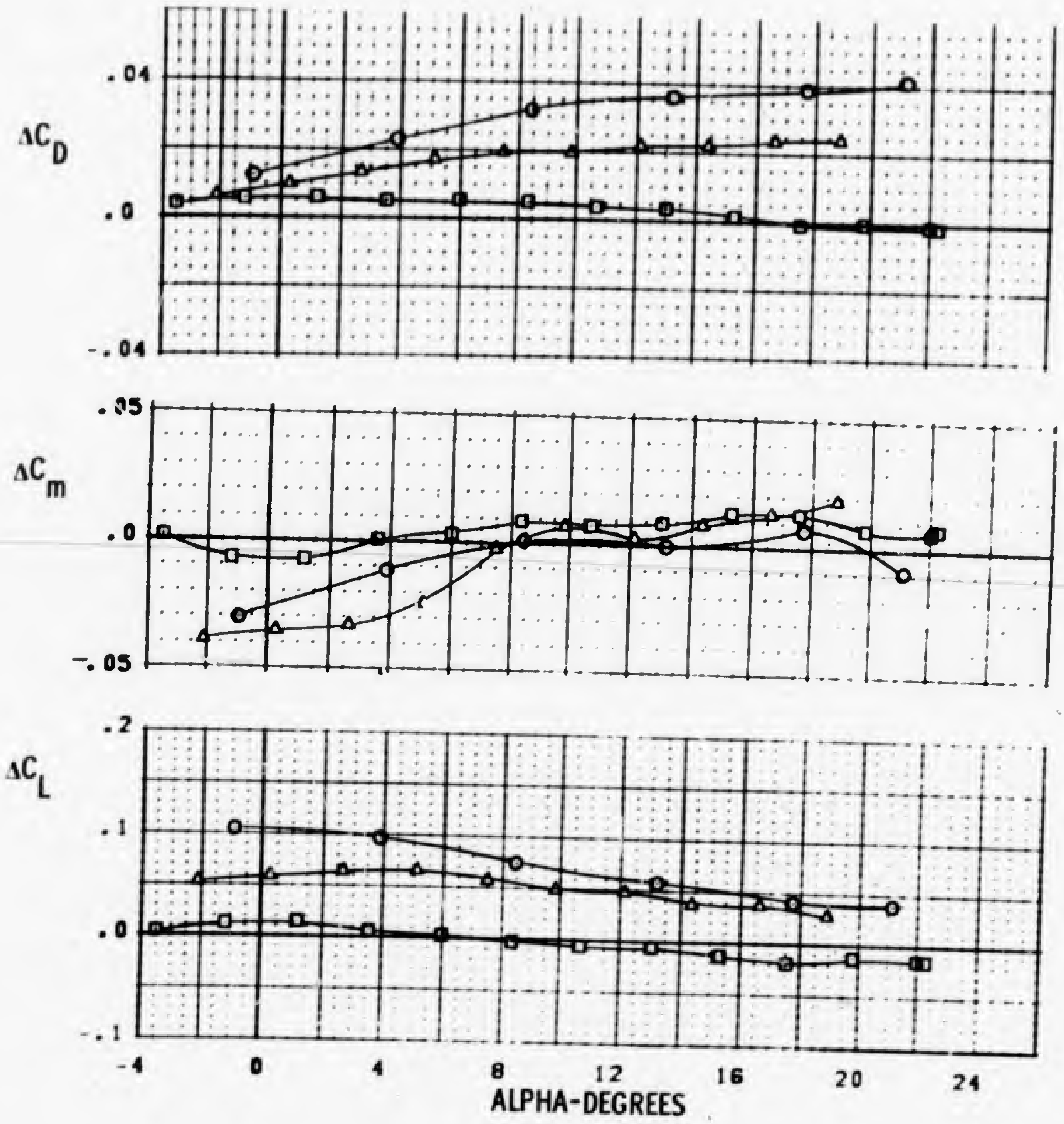
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
O	PWT 4T TC-043	PN 199 -PN 126	K1	10/10	MID	20/0 +10 DROOP
□	PWT 4T TC-043	PN 133 -PN 126	K1	10/10	MID	10/10
Δ	PWT 4T TC-043	PN 467 -PN 441	K1	0/0	MID	20/0

FIGURE 132c TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 0.9



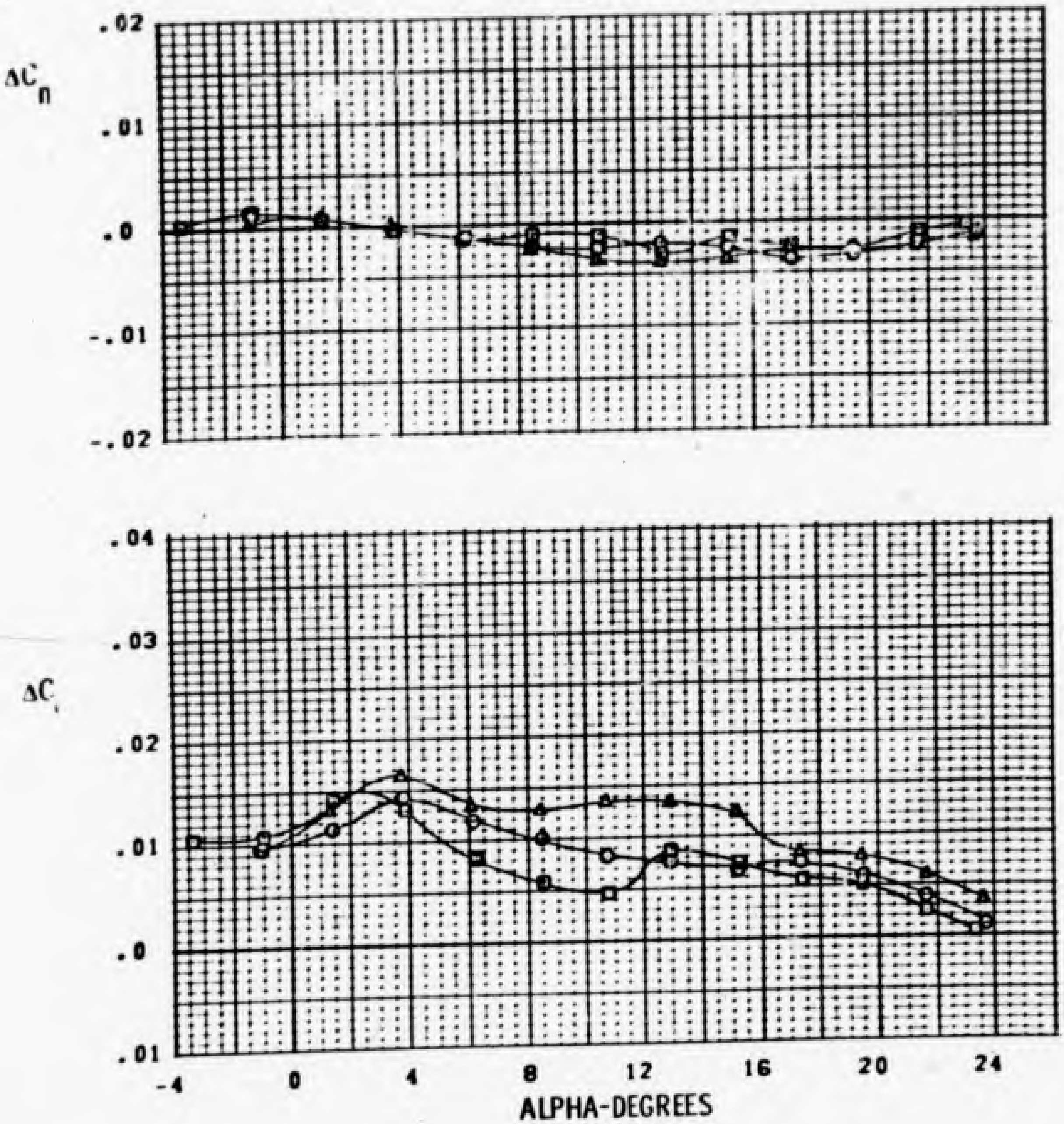
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
O	PWT 4T TC-043	PN 201 -PN 129	K1 10/10	MID 20/0 +10 DROOP
□	PWT 4T TC-043	PN 136 -PN 129	K1 10/10	MID 10/-10
Δ	PWT 4T TC-043	PN 470 -PN 269	K1 0/0	MID 20/0

FIGURE 132d TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 1.2



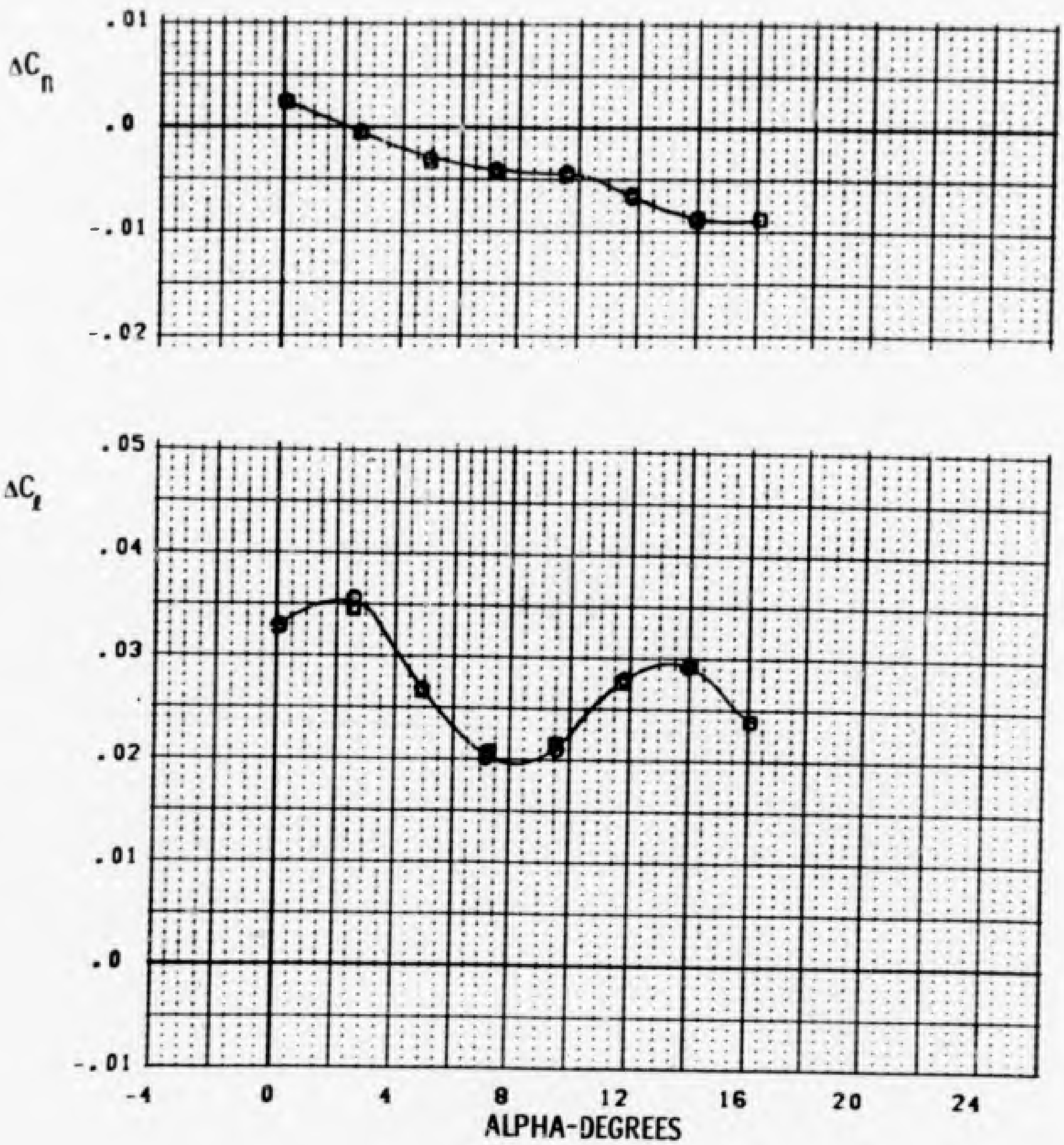
SYM	TEST	INCREMENT	L.E. (L/R)	AILERON (L/R)
○	PWT 4T TC-043	PN 201 -PN 129	K1 10/10	MID 20/0 +10 DROOP
□	PWT 4T TC-043	PN 136 -PN 129	K1 10/10	MID 10/-10
▲	PWT 4T TC-043	PN 470 -PN 269	K1 0/0	MID 20/0

FIGURE 132d TRAILING EDGE DROOP EFFECTS ON MID AILERONS
M = 1.2



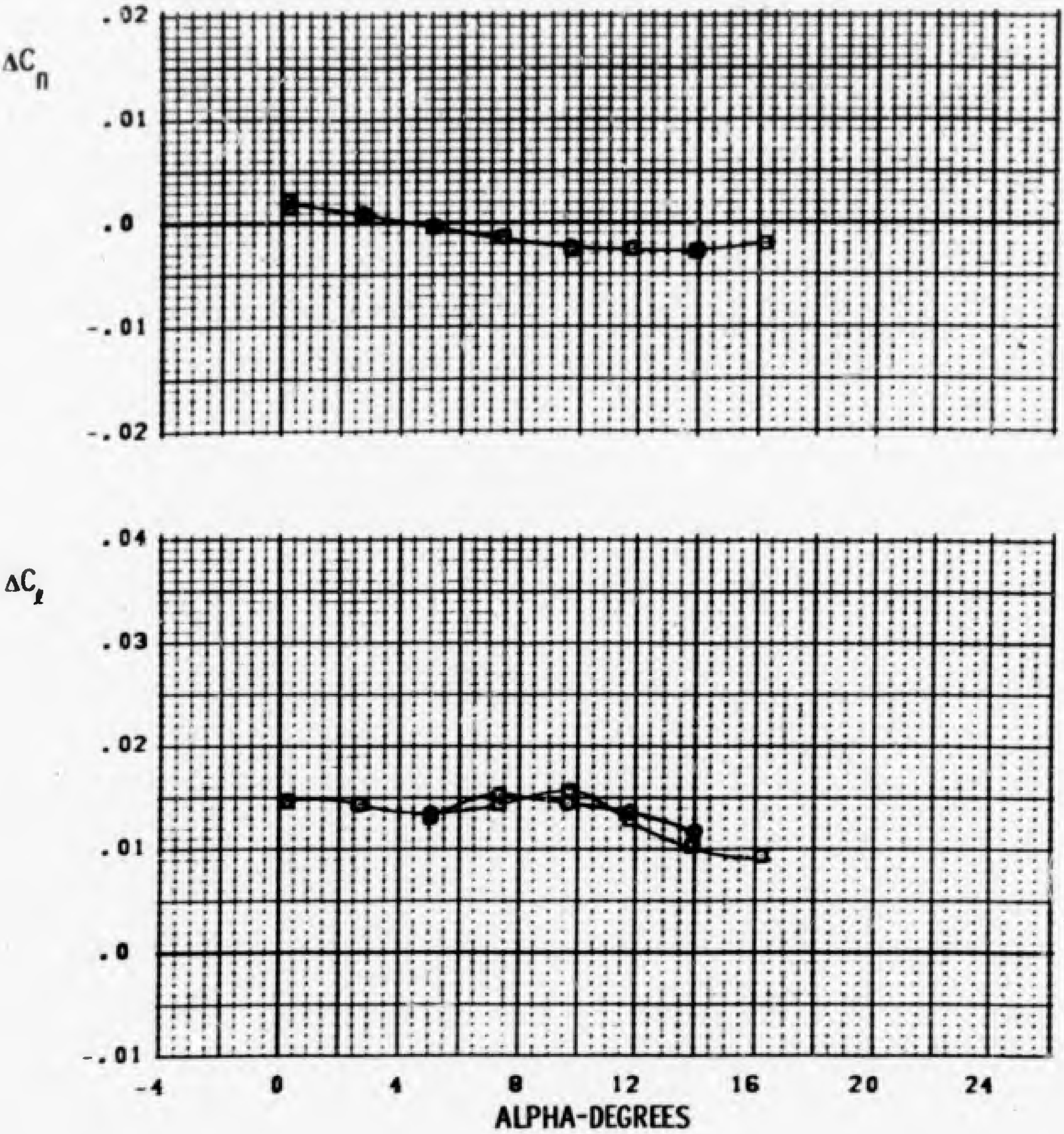
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	
⊙	PWT 4T TC-043	PN 154 -PN 126	K1	10/10	MID +F2	10/-10
⊡	PWT 4T TC-043	PN 161 -PN 126	K1	10/10	MID +F3	10/-10
▲	PWT 4T TC-043	PN 133 -PN 126	K1	10/10	MID	10/-10

FIGURE 133 SPLIT TRAILING EDGE FLAP EFFECTS ON MID AILERON
M = 0.9



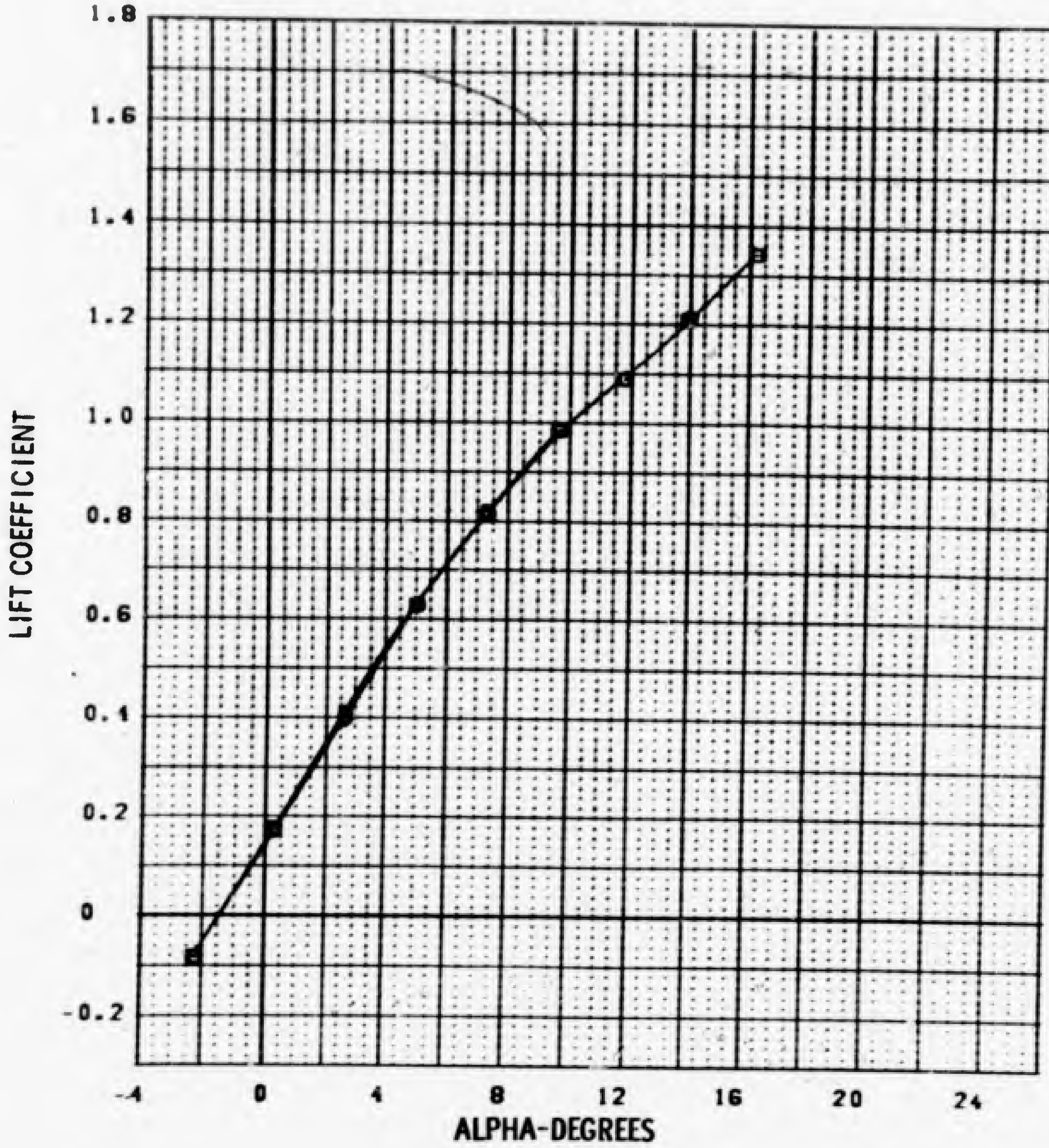
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)	KRUGER
⊙	PWT 4T TC-043	PN 518 -PN 441	K1	10/0	3 SEGM. 20/-20	ON
⊡	PWT 4T TC-043	PN 513 -PN 441	K1	10/0	3 SEGM. 20/-20	OFF

FIGURE 134 KRUGER LEADING EDGE GLOVE FLAP EFFECTS
M = 0.9



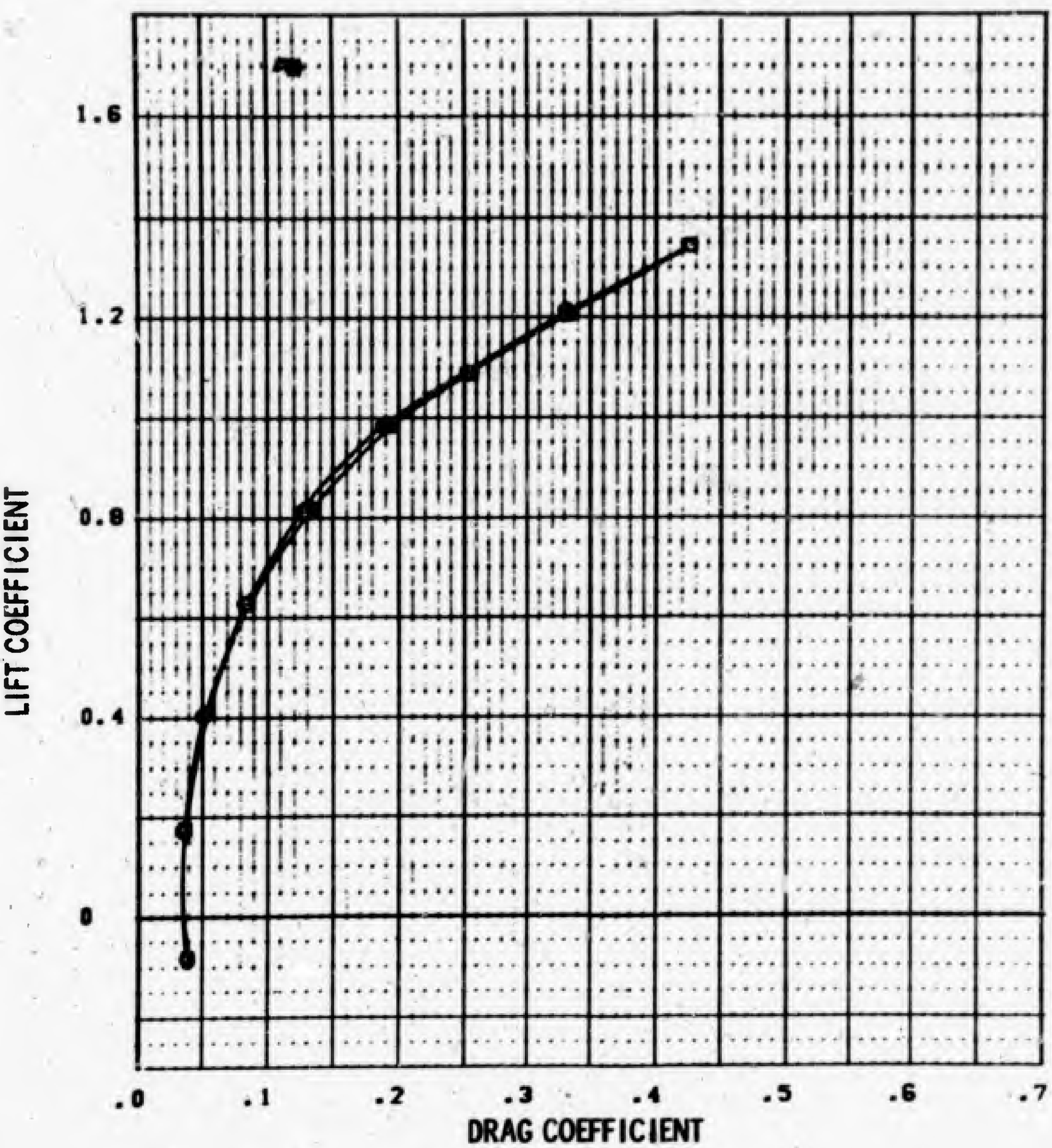
SYM	TEST	INCREMENT	L.E. (L/R)		AILERON (L/R)		FAIRING
○	PWT 4T TC-043	PN 482 -PN 441	K1	0/0	MID	10/-10	OFF
□	PWT 4T TC-043	PN 474 -PN 441	K1	0/0	MID	10/-10	ON

FIGURE 135 CANOPY FAIRING EFFECTS ON MID AILERONS
M = 0.9



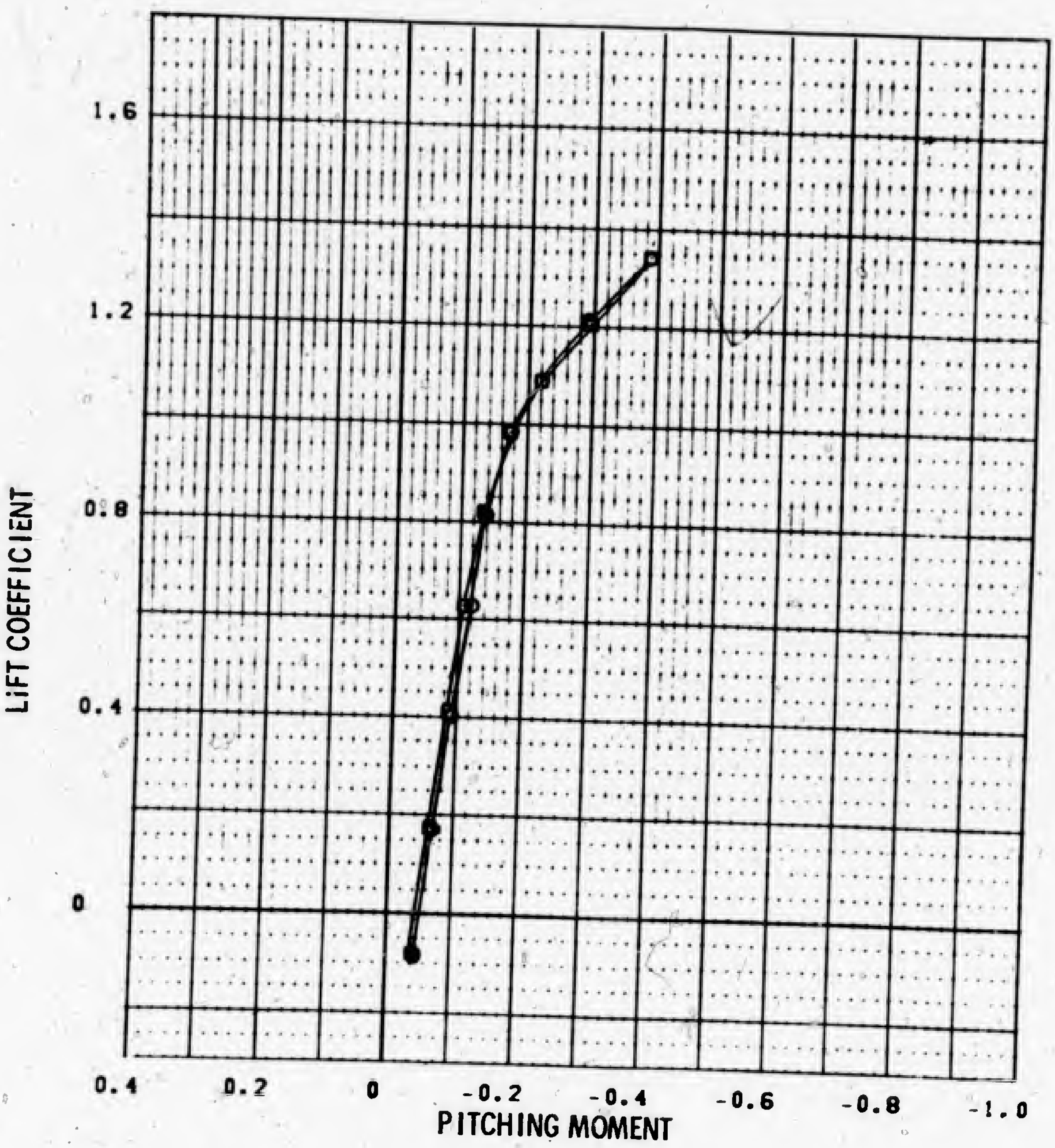
SYM	TEST	PART	AILERON (L/R)	CANOPY FNG.
○	PWT 4T TC-043	482	MID 10/-10	OFF
⊡	PWT 4T TC-043	474	MID 10/-10	ON

FIGURE 136 EFFECT OF CANOPY FAIRING
M = 0.9



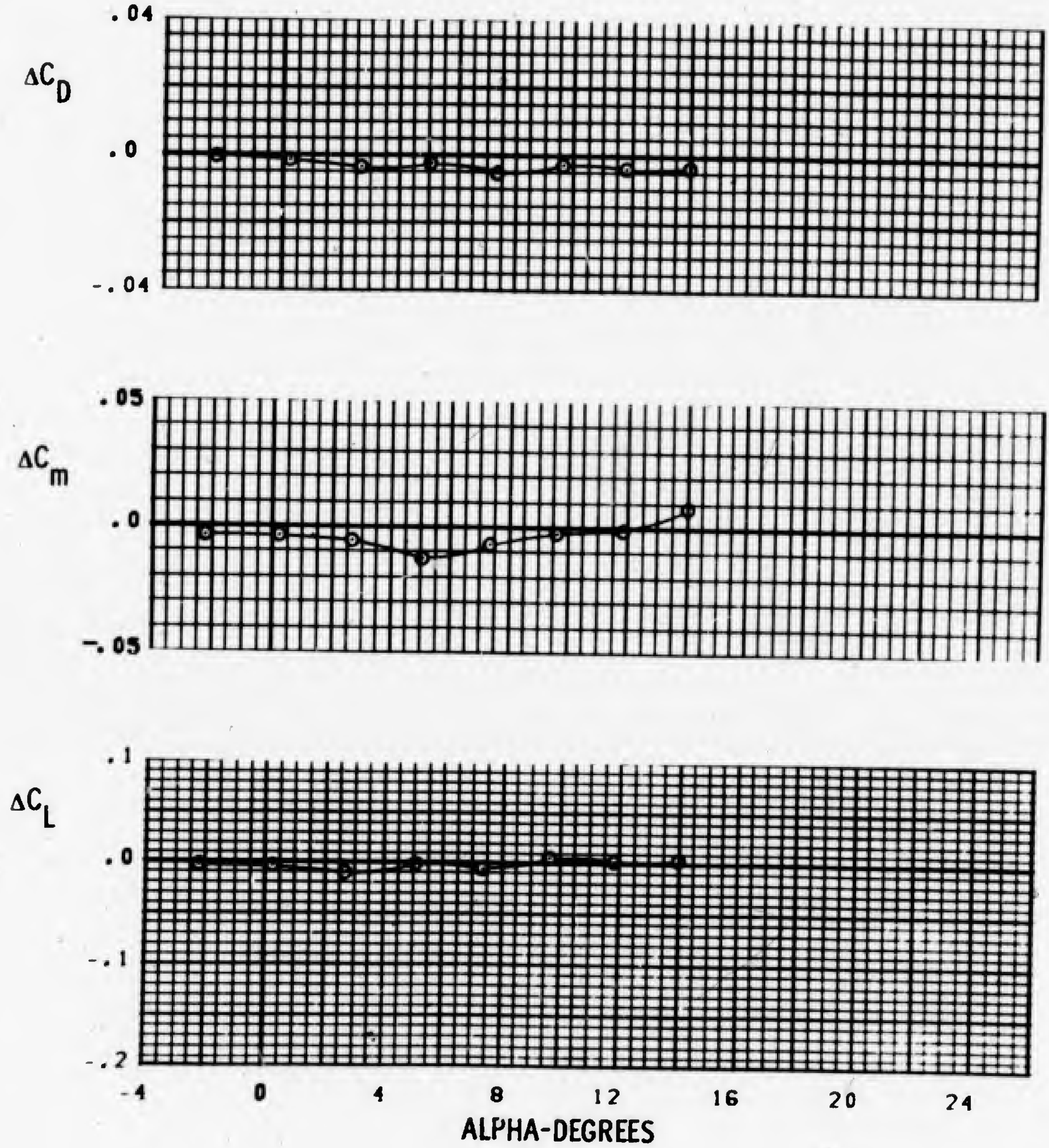
SYM	TEST	PART	AILERON (L/R)	CANOPY FNG.
⊙	PWT 4T TC-043	482	MID 10/-10	OFF
⊡	PWT 4T TC-043	474	MID 10/-10	ON

FIGURE 136 EFFECT OF CANOPY FAIRING
M = 0.9



SYM	TEST	PART	AILERON (L/R)	CANOPY FNG.
⊙	PWT 4T TC-043	482	MID 10/-10	OFF
⊡	PWT 4T TC-043	474	MID 10/-10	ON

FIGURE 136 EFFECT OF CANOPY FAIRING
M = 0.9



SYM	TEST	INCREMENT (OFF - ON)	AILERON (L/R)
⊙	PWT 4T TC-043	PN 482 - PN 474	MID 10/10

FIGURE 136 EFFECT OF CANOPY FAIRING
M = 0.9

APPENDIX VI TABULATED FORCE AND MOMENT DATA

Run by run tabulations of the stability axis force and moment coefficients are provided on the following pages. The geometric configuration for each run (part number) is provided in Tables II and III of Volume I, pages 45 thru 48.

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	7	1	0.899	0.0	1.139	0.3144	0.0481	-0.0708	0.0353	-0.0002
16T-216	7	2	0.900	0.0	4.448	0.6579	0.0863	-0.1146	0.0278	-0.0039
16T-216	7	3	0.898	0.0	6.436	0.8288	0.1247	-0.1306	0.0252	-0.0057
16T-216	7	4	0.899	0.0	8.755	1.0068	0.1878	-0.1725	0.0271	-0.0077
16T-216	7	5	0.900	0.0	9.664	1.0667	0.2152	-0.1944	0.0270	-0.0081
16T-216	7	6	0.899	0.0	19.966	1.6828	0.6674	-0.5930	0.0085	-0.0054
16T-216	7	7	0.899	0.0	20.847	1.7297	0.7105	-0.6270	0.0078	-0.0067
16T-216	7	8	0.898	0.0	23.061	1.8444	0.8340	-0.7025	0.0068	-0.0096
16T-216	7	9	0.897	0.0	29.286	2.0569	1.2065	-0.8668	-0.0048	-0.0138
16T-216	8	1	0.900	0.0	-2.017	-0.0323	0.0444	-0.0388	0.0363	0.0041
16T-216	8	2	0.900	0.0	0.281	0.2198	0.0443	-0.0591	0.0355	0.0012
16T-216	8	3	0.901	0.0	2.662	0.4789	0.0617	-0.0889	0.0309	-0.0019
16T-216	8	4	0.900	0.0	5.028	0.7153	0.0972	-0.1189	0.0270	-0.0043
16T-216	8	5	0.902	0.0	7.372	0.9066	0.1507	-0.1449	0.0259	-0.0060
16T-216	8	6	0.900	0.0	9.627	1.0672	0.2150	-0.1940	0.0267	-0.0077
16T-216	8	7	0.900	0.0	11.909	1.1471	0.2820	-0.2487	0.0150	-0.0057
16T-216	8	8	0.899	0.0	14.088	1.2964	0.3701	-0.3446	0.0159	-0.0063
16T-216	8	9	0.901	0.0	16.433	1.4604	0.4803	-0.4454	0.0135	-0.0062
16T-216	8	10	0.899	0.0	18.710	1.6127	0.5975	-0.5406	0.0112	-0.0063
16T-216	8	11	0.900	0.0	20.831	1.7355	0.7138	-0.6272	0.0076	-0.0067
16T-216	8	12	0.899	0.0	23.168	1.8520	0.8480	-0.7076	0.0070	-0.0096
16T-216	8	13	0.900	0.0	25.179	1.9361	0.9667	-0.7687	0.0040	-0.0124
16T-216	8	14	0.900	0.0	27.283	2.0090	1.0923	-0.8260	-0.0008	-0.0151
16T-216	8	15	0.900	0.0	29.356	2.0629	1.2152	-0.8753	-0.0057	-0.0136
16T-216	9	1	0.949	0.0	-2.082	-0.0710	0.0550	-0.0361	0.0383	0.0037
16T-216	9	2	0.951	0.0	0.373	0.2581	0.0577	-0.0691	0.0305	-0.0
16T-216	9	3	0.949	0.0	2.635	0.4832	0.0783	-0.1005	0.0276	-0.0026
16T-216	9	4	0.950	0.0	5.104	0.7209	0.1192	-0.1521	0.0260	-0.0053
16T-216	9	5	0.951	0.0	7.417	0.9357	0.1747	-0.2072	0.0243	-0.0075
16T-216	9	6	0.951	0.0	9.672	1.1278	0.2447	-0.2671	0.0225	-0.0088
16T-216	9	7	0.949	0.0	12.161	1.3416	0.3427	-0.3633	0.0220	-0.0104
16T-216	9	8	0.949	0.0	14.434	1.5267	0.4485	-0.4544	0.0209	-0.0120
16T-216	9	9	0.950	0.0	16.677	1.6921	0.5649	-0.5562	0.0203	-0.0140
16T-216	9	10	0.949	0.0	18.989	1.8112	0.6875	-0.6469	0.0145	-0.0145
16T-216	10	1	1.201	-0.0	-2.091	-0.0922	0.0686	0.0482	0.0186	0.0048
16T-216	10	2	1.202	-0.0	-0.920	0.0226	0.0658	0.0044	0.0195	0.0036
16T-216	10	3	1.203	0.0	0.266	0.1436	0.0673	-0.0435	0.0204	0.0021
16T-216	10	4	1.200	0.0	1.372	0.2583	0.0735	-0.0928	0.0217	0.0006
16T-216	10	5	1.202	0.0	2.588	0.3813	0.0845	-0.1422	0.0228	-0.0002
16T-216	10	6	1.201	0.0	4.921	0.6171	0.1198	-0.2374	0.0216	-0.0021
16T-216	10	7	1.200	0.0	7.166	0.8256	0.1678	-0.3174	0.0205	-0.0039
16T-216	10	8	1.201	0.0	9.491	1.0268	0.2341	-0.4040	0.0198	-0.0052
16T-216	10	9	1.201	0.0	12.034	1.2384	0.3756	-0.5110	0.0204	-0.0076
16T-216	10	10	1.201	0.0	14.365	1.4159	0.4246	-0.6125	0.0193	-0.0089
16T-216	10	11	1.198	0.0	16.588	1.5685	0.5309	-0.7066	0.0170	-0.0114
16T-216	10	12	1.200	0.0	18.957	1.7078	0.6510	-0.8115	0.0179	-0.0124
16T-216	10	13	1.198	0.0	21.155	1.8143	0.7691	-0.8916	0.0174	-0.0156

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	10	14	1.202	0.0	23.281	1.9110	0.8893	-0.9734	0.0157	-0.0176
16T-216	11	1	0.850	0.0	-1.975	-0.0300	0.0403	-0.0333	0.0364	0.0045
16T-216	11	2	0.850	0.0	-0.829	0.1002	0.0379	-0.0475	0.0372	0.0032
16T-216	11	3	0.850	0.0	0.274	0.2078	0.0395	-0.0595	0.0369	0.0016
16T-216	11	4	0.850	0.0	1.438	0.3217	0.0443	-0.0733	0.0373	0.0003
16T-216	11	5	0.850	0.0	2.587	0.4365	0.0521	-0.0872	0.0374	-0.0011
16T-216	11	6	0.850	0.0	4.854	0.6671	0.0824	-0.1126	0.0345	-0.0035
16T-216	11	7	0.850	0.0	7.196	0.8763	0.1334	-0.1350	0.0292	-0.0059
16T-216	11	8	0.850	0.0	9.471	0.9737	0.1889	-0.1684	0.0218	-0.0068
16T-216	11	9	0.850	0.0	11.710	1.0843	0.2588	-0.2316	0.0204	-0.0073
16T-216	11	10	0.850	0.0	14.012	1.2391	0.3466	-0.3130	0.0177	-0.0066
16T-216	11	11	0.849	0.0	16.251	1.3954	0.4451	-0.3877	0.0171	-0.0075
16T-216	11	12	0.851	0.0	18.460	1.5371	0.5553	-0.4894	0.0144	-0.0073
16T-216	11	13	0.848	0.0	20.682	1.6599	0.6718	-0.5709	0.0136	-0.0093
16T-216	12	1	0.800	0.0	-2.001	-0.0267	0.0385	-0.0319	0.0383	0.0050
16T-216	12	2	0.800	0.0	-0.842	0.0938	0.0360	-0.0447	0.0380	0.0034
16T-216	12	3	0.800	0.0	0.312	0.2029	0.0373	-0.0577	0.0378	0.0020
16T-216	12	4	0.799	0.0	1.386	0.3021	0.0413	-0.0719	0.0378	0.0006
16T-216	12	5	0.799	0.0	2.479	0.3993	0.0476	-0.0842	0.0380	-0.0007
16T-216	12	6	0.800	0.0	4.855	0.6228	0.0726	-0.1098	0.0361	-0.0040
16T-216	12	7	0.798	0.0	7.240	0.8418	0.1213	-0.1386	0.0324	-0.0065
16T-216	12	8	0.800	0.0	9.321	0.9344	0.1732	-0.1627	0.0230	-0.0074
16T-216	12	9	0.801	0.0	11.591	1.0598	0.2444	-0.2172	0.0214	-0.0082
16T-216	12	10	0.799	0.0	13.853	1.2053	0.3264	-0.2798	0.0205	-0.0083
16T-216	12	11	0.800	0.0	16.195	1.3623	0.4253	-0.3585	0.0181	-0.0081
16T-216	12	12	0.800	0.0	18.307	1.4993	0.5294	-0.4532	0.0150	-0.0077
16T-216	12	13	0.800	0.0	20.464	1.6258	0.6447	-0.5358	0.0147	-0.0099
16T-216	13	1	0.699	0.0	-2.009	-0.0272	0.0360	-0.0291	0.0407	0.0054
16T-216	13	2	0.699	0.0	-0.857	0.0833	0.0337	-0.0420	0.0399	0.0035
16T-216	13	3	0.699	0.0	0.204	0.1787	0.0346	-0.0542	0.0399	0.0020
16T-216	13	4	0.698	0.0	1.274	0.2732	0.0378	-0.0673	0.0397	0.0007
16T-216	13	5	0.698	0.0	2.296	0.3588	0.0427	-0.0792	0.0392	-0.0007
16T-216	13	6	0.699	0.0	4.538	0.5518	0.0605	-0.1065	0.0383	-0.0036
16T-216	13	7	0.699	0.0	6.897	0.7557	0.0986	-0.1333	0.0365	-0.0065
16T-216	13	8	0.698	0.0	8.119	0.8370	0.1292	-0.1467	0.0316	-0.0081
16T-216	13	9	0.699	0.0	9.146	0.8899	0.1575	-0.1599	0.0288	-0.0084
16T-216	13	10	0.700	0.0	10.269	0.9533	0.1882	-0.1773	0.0255	-0.0091
16T-216	13	11	0.699	0.0	11.409	1.0273	0.2239	-0.1984	0.0243	-0.0097
16T-216	13	12	0.699	0.0	13.650	1.1696	0.3015	-0.2504	0.0219	-0.0103
16T-216	13	13	0.699	0.0	15.739	1.2948	0.3834	-0.3181	0.0179	-0.0093
16T-216	13	14	0.699	0.0	18.122	1.4550	0.4974	-0.4125	0.0157	-0.0091
16T-216	13	15	0.699	0.0	20.380	1.5913	0.6161	-0.4971	0.0153	-0.0119
16T-216	14	1	0.699	0.0	-1.941	-0.0241	0.0357	-0.0313	0.0415	0.0052
16T-216	14	2	0.698	0.0	-0.931	0.0739	0.0337	-0.0436	0.0412	0.0034
16T-216	14	3	0.698	0.0	0.147	0.1689	0.0345	-0.0551	0.0402	0.0017
16T-216	14	5	0.701	0.0	2.175	0.3485	0.0422	-0.0800	0.0399	-0.0005

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	14	6	0.700	0.0	4.266	0.5216	0.0577	-0.1058	0.0384	-0.0034
16T-216	14	7	0.699	0.0	6.469	0.7208	0.0909	-0.1295	0.0363	-0.0068
16T-216	14	8	0.700	0.0	7.547	0.7968	0.1162	-0.1418	0.0327	-0.0078
16T-216	14	9	0.700	0.0	8.616	0.8549	0.1439	-0.1543	0.0305	-0.0083
16T-216	14	10	0.700	0.0	9.691	0.9176	0.1720	-0.1714	0.0282	-0.0093
16T-216	14	11	0.700	0.0	10.795	0.9867	0.2051	-0.1916	0.0250	-0.0100
16T-216	14	12	0.700	0.0	12.815	1.1134	0.2713	-0.2321	0.0228	-0.0108
16T-216	14	13	0.700	0.0	15.006	1.2441	0.3513	-0.2908	0.0191	-0.0100
16T-216	14	14	0.700	0.0	17.307	1.3963	0.4552	-0.3819	0.0166	-0.0091
16T-216	14	15	0.699	0.0	19.330	1.5246	0.5598	-0.4669	0.0161	-0.0100
16T-216	15	1	0.803	0.0	-1.968	-0.0269	0.0384	-0.0328	0.0395	0.0050
16T-216	15	2	0.803	0.0	-0.962	0.0771	0.0360	-0.0457	0.0396	0.0034
16T-216	15	3	0.799	0.0	0.126	0.1344	0.0368	-0.0579	0.0390	0.0020
16T-216	15	4	0.799	0.0	1.160	0.2795	0.0402	-0.0706	0.0390	0.0005
16T-216	15	5	0.802	0.0	2.254	0.3922	0.0460	-0.0833	0.0388	-0.0007
16T-216	15	6	0.800	0.0	4.409	0.5305	0.0660	-0.1072	0.0377	-0.0037
16T-216	15	7	0.800	0.0	6.534	0.7360	0.1052	-0.1334	0.0345	-0.0063
16T-216	15	8	0.800	0.0	7.688	0.8458	0.1316	-0.1405	0.0278	-0.0071
16T-216	15	9	0.801	0.0	8.706	0.8969	0.1567	-0.1539	0.0244	-0.0076
16T-216	15	10	0.800	0.0	9.739	0.9558	0.1866	-0.1727	0.0232	-0.0083
16T-216	15	11	0.800	0.0	10.878	1.0100	0.2205	-0.2025	0.0198	-0.0082
16T-216	15	12	0.801	0.0	13.062	1.1559	0.2967	-0.2595	0.0212	-0.0087
16T-216	15	13	0.800	0.0	15.221	1.2898	0.3807	-0.3241	0.0195	-0.0084
16T-216	15	14	0.800	0.0	17.322	1.4334	0.4795	-0.4129	0.0168	-0.0077
16T-216	15	15	0.800	0.0	19.551	1.5764	0.5957	-0.5097	0.0155	-0.0087
16T-216	16	1	0.852	0.0	-1.983	-0.0302	0.0401	-0.0336	0.0387	0.0047
16T-216	16	2	0.850	0.0	-0.869	0.0951	0.0376	-0.0492	0.0386	0.0031
16T-216	16	3	0.850	0.0	0.070	0.1902	0.0385	-0.0600	0.0383	0.0018
16T-216	16	4	0.850	0.0	1.220	0.3020	0.0423	-0.0725	0.0383	0.0003
16T-216	16	5	0.850	0.0	2.256	0.4010	0.0490	-0.0850	0.0384	-0.0009
16T-216	16	6	0.851	0.0	4.412	0.6251	0.0751	-0.1128	0.0366	-0.0034
16T-216	16	7	0.851	0.0	6.628	0.8297	0.1190	-0.1341	0.0314	-0.0057
16T-216	16	8	0.851	0.0	7.790	0.9100	0.1479	-0.1463	0.0280	-0.0067
16T-216	16	9	0.851	0.0	8.819	0.9201	0.1693	-0.1604	0.0198	-0.0069
16T-216	16	10	0.850	0.0	9.921	0.9331	0.2011	-0.1844	0.0203	-0.0073
16T-216	16	11	0.852	0.0	10.920	1.0472	0.2350	-0.2132	0.0225	-0.0082
16T-216	16	12	0.849	0.0	13.067	1.1760	0.3095	-0.2847	0.0196	-0.0075
16T-216	16	13	0.852	0.0	15.185	1.3248	0.3982	-0.3572	0.0183	-0.0071
16T-216	16	14	0.850	0.0	17.476	1.4769	0.5063	-0.4520	0.0162	-0.0073
16T-216	16	15	0.851	0.0	19.498	1.6059	0.6137	-0.5435	0.0145	-0.0080
16T-216	17	1	0.902	0.0	-1.988	-0.0287	0.0437	-0.0413	0.0372	0.0042
16T-216	17	2	0.898	0.0	-0.866	0.0965	0.0412	-0.0498	0.0373	0.0025
16T-216	17	3	0.902	0.0	0.255	0.2147	0.0437	-0.0606	0.0372	0.0013
16T-216	17	4	0.899	0.0	1.186	0.3142	0.0478	-0.0718	0.0367	-0.0001
16T-216	17	5	0.899	0.0	2.285	0.4345	0.0566	-0.0852	0.0344	-0.0014
16T-216	17	6	0.899	0.0	4.539	0.6671	0.0878	-0.1121	0.0297	-0.0037
16T-216	17	7	0.899	0.0	6.660	0.8525	0.1319	-0.1378	0.0271	-0.0056

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	17	8	0.898	0.0	7.772	0.9283	0.1594	-0.1487	0.0280	-0.0067
16T-216	17	9	0.900	0.0	8.813	1.0057	0.1900	-0.1728	0.0279	-0.0077
16T-216	17	10	0.900	0.0	9.897	1.0209	0.2163	-0.1915	0.0198	-0.0066
16T-216	17	11	0.899	0.0	11.045	1.0826	0.2522	-0.2263	0.0172	-0.0060
16T-216	17	12	0.899	0.0	13.186	1.2360	0.3339	-0.3124	0.0169	-0.0059
16T-216	17	13	0.899	0.0	15.368	1.3798	0.4275	-0.4064	0.0152	-0.0055
16T-216	17	14	0.900	0.0	17.535	1.5315	0.5359	-0.4989	0.0135	-0.0064
16T-216	17	15	0.900	0.0	19.642	1.6715	0.6497	-0.5882	0.0101	-0.0055
16T-216	18	1	0.951	0.0	-2.015	-0.0599	0.0536	-0.0401	0.0396	0.0036
16T-216	18	2	0.950	0.0	-0.881	0.1036	0.0514	-0.0586	0.0370	0.0015
16T-216	18	3	0.949	0.0	0.158	0.2295	0.0542	-0.0678	0.0329	0.0001
16T-216	18	4	0.950	0.0	1.216	0.3451	0.0621	-0.0795	0.0303	-0.0011
16T-216	18	5	0.951	0.0	2.319	0.4586	0.0751	-0.0976	0.0295	-0.0026
16T-216	18	6	0.951	0.0	4.567	0.6709	0.1086	-0.1404	0.0276	-0.0051
16T-216	18	7	0.951	0.0	6.707	0.8720	0.1565	-0.1899	0.0260	-0.0073
16T-216	18	8	0.950	0.0	7.786	0.9730	0.1869	-0.2182	0.0255	-0.0083
16T-216	18	9	0.951	0.0	8.928	1.0689	0.2216	-0.2468	0.0243	-0.0091
16T-216	18	10	0.950	0.0	10.084	1.1666	0.2603	-0.2800	0.0232	-0.0096
16T-216	18	11	0.951	0.0	11.173	1.2589	0.3024	-0.3213	0.0228	-0.0101
16T-216	18	12	0.950	0.0	13.351	1.4451	0.3980	-0.4118	0.0227	-0.0114
16T-216	18	13	0.949	0.0	15.545	1.6121	0.5055	-0.5029	0.0207	-0.0123
16T-216	18	14	0.951	0.0	17.684	1.7163	0.6103	-0.5781	0.0143	-0.0116
16T-216	18	15	0.949	0.0	19.864	1.8629	0.7412	-0.6954	0.0125	-0.0133
16T-216	19	1	1.199	-0.0	-1.990	-0.0858	0.0680	0.0415	0.0201	0.0042
16T-216	19	2	1.202	-0.0	-0.933	0.0189	0.0656	0.0035	0.0210	0.0036
16T-216	19	3	1.199	0.0	0.049	0.1245	0.0667	-0.0404	0.0222	0.0020
16T-216	19	4	1.200	0.0	1.155	0.2329	0.0720	-0.0826	0.0227	0.0009
16T-216	19	5	1.202	0.0	2.207	0.3447	0.0810	-0.1289	0.0236	0.0001
16T-216	19	6	1.198	0.0	4.336	0.5673	0.1106	-0.2301	0.0237	-0.0020
16T-216	19	7	1.199	-0.0	6.682	0.7859	0.1585	-0.3062	0.0212	-0.0030
16T-216	19	8	1.205	-0.0	7.771	0.8837	0.1858	-0.3463	0.0206	-0.0041
16T-216	19	9	1.200	0.0	8.888	0.9878	0.2192	-0.3896	0.0205	-0.0054
16T-216	19	10	1.202	0.0	9.908	1.0731	0.2513	-0.4329	0.0213	-0.0053
16T-216	19	11	1.201	0.0	11.104	1.1784	0.2947	-0.4851	0.0214	-0.0065
16T-216	19	12	1.196	0.0	13.333	1.3596	0.3869	-0.5805	0.0210	-0.0087
16T-216	19	13	1.198	0.0	15.435	1.5084	0.4825	-0.6782	0.0203	-0.0094
16T-216	19	14	1.201	0.0	17.688	1.6600	0.5976	-0.7866	0.0192	-0.0115
16T-216	19	15	1.198	0.0	19.734	1.7756	0.7070	-0.8742	0.0203	-0.0143
16T-216	22	1	0.899	0.0	1.019	0.2850	0.0490	-0.0681	0.0332	-0.0005
16T-216	22	2	0.899	0.0	4.361	0.6223	0.0836	-0.1071	0.0223	-0.0038
16T-216	22	3	0.898	0.0	6.396	0.7957	0.1196	-0.1288	0.0199	-0.0048
16T-216	22	4	0.899	0.0	8.666	0.9741	0.1765	-0.1675	0.0225	-0.0056
16T-216	22	5	0.898	0.0	9.616	1.0267	0.2043	-0.1864	0.0287	-0.0071
16T-216	22	6	0.899	0.0	11.930	1.1811	0.2806	-0.2457	0.0238	-0.0080
16T-216	22	7	0.898	0.0	18.603	1.5978	0.5833	-0.5406	0.0102	-0.0029
16T-216	23	1	0.898	0.0	-2.090	-0.0795	0.0489	-0.0277	0.0302	0.0018

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	23	2	0.859	0.0	-0.853	0.0674	0.0449	-0.0441	0.0302	0.0008
16T-216	23	3	0.899	0.0	0.263	0.1951	0.0461	-0.0591	0.0321	0.0001
16T-216	23	4	0.898	0.0	1.404	0.3260	0.0514	-0.0751	0.0328	-0.0011
16T-216	23	5	0.899	0.0	2.626	0.4550	0.0623	-0.0891	0.0287	-0.0023
16T-216	23	6	0.898	0.0	5.062	0.6826	0.0949	-0.1143	0.0215	-0.0043
16T-216	23	7	0.899	0.0	7.288	0.8615	0.1403	-0.1395	0.0216	-0.0053
16T-216	23	8	0.899	0.0	8.496	0.9567	0.1717	-0.1637	0.0222	-0.0058
16T-216	23	9	0.898	0.0	9.639	1.0423	0.2069	-0.1917	0.0267	-0.0070
16T-216	23	10	0.898	0.0	10.768	1.1120	0.2422	-0.2201	0.0283	-0.0081
16T-216	23	11	0.898	0.0	11.922	1.1804	0.2806	-0.2469	0.0241	-0.0081
16T-216	23	12	0.898	0.0	14.060	1.2913	0.3608	-0.3354	0.0167	-0.0069
16T-216	23	13	0.899	0.0	16.315	1.4407	0.4642	-0.4337	0.0137	-0.0055
16T-216	23	14	0.898	0.0	18.606	1.5937	0.5830	-0.5384	0.0101	-0.0029
16T-216	23	15	0.898	0.0	20.794	1.7268	0.7033	-0.6276	0.0090	-0.0047
16T-216	24	1	0.949	0.0	-2.184	-0.1290	0.0618	-0.0230	0.0328	0.0015
16T-216	24	2	0.950	0.0	-1.018	0.0347	0.0572	-0.0463	0.0299	-0.0001
16T-216	24	3	0.949	0.0	0.286	0.2136	0.0594	-0.0696	0.0272	-0.0015
16T-216	24	4	0.949	0.0	1.550	0.3545	0.0684	-0.0876	0.0260	-0.0026
16T-216	24	5	0.948	0.0	2.569	0.4613	0.0796	-0.1049	0.0253	-0.0035
16T-216	24	6	0.951	0.0	5.008	0.6894	0.1169	-0.1497	0.0216	-0.0056
16T-216	24	7	0.948	0.0	7.276	0.8978	0.1654	-0.1979	0.0194	-0.0068
16T-216	24	8	0.950	0.0	8.562	1.0109	0.2013	-0.2300	0.0187	-0.0072
16T-216	24	9	0.949	0.0	9.766	1.1192	0.2412	-0.2650	0.0183	-0.0076
16T-216	24	10	0.951	0.0	11.030	1.2311	0.2883	-0.3136	0.0184	-0.0077
16T-216	24	11	0.949	0.0	12.182	1.3343	0.3352	-0.3607	0.0192	-0.0083
16T-216	24	12	0.951	0.0	14.468	1.5227	0.4404	-0.4597	0.0195	-0.0096
16T-216	24	13	0.949	0.0	16.695	1.6904	0.5554	-0.5568	0.0201	-0.0114
16T-216	24	14	0.948	0.0	18.978	1.7830	0.6666	-0.6347	0.0085	-0.0062
16T-216	24	15	0.950	0.0	21.167	1.9208	0.8016	-0.7594	0.0050	-0.0054
16T-216	25	1	1.202	0.0	-2.048	-0.1015	0.0765	0.0410	0.0174	0.0026
16T-216	25	2	1.198	0.0	-0.997	0.0068	0.0734	-0.0058	0.0181	0.0006
16T-216	25	3	1.199	0.0	0.106	0.1119	0.0738	-0.0469	0.0185	0.0001
16T-216	25	4	1.202	0.0	1.237	0.2260	0.0778	-0.0920	0.0182	-0.0002
16T-216	25	5	1.200	0.0	2.530	0.3570	0.0875	-0.1463	0.0190	-0.0018
16T-216	25	6	1.202	0.0	4.776	0.5800	0.1174	-0.2346	0.0175	-0.0022
16T-216	25	7	1.198	0.0	7.126	0.8123	0.1662	-0.3238	0.0165	-0.0039
16T-216	25	8	1.203	0.0	8.444	0.9180	0.1993	-0.3649	0.0155	-0.0038
16T-216	25	9	1.200	0.0	9.646	1.0328	0.2363	-0.4168	0.0168	-0.0051
16T-216	25	10	1.200	0.0	10.750	1.1244	0.2733	-0.4601	0.0175	-0.0055
16T-216	25	11	1.200	0.0	11.981	1.2275	0.3192	-0.5136	0.0174	-0.0061
16T-216	25	12	1.199	0.0	14.268	1.4108	0.4163	-0.6171	0.0173	-0.0072
16T-216	25	13	1.200	0.0	16.609	1.5774	0.5284	-0.7262	0.0171	-0.0081
16T-216	25	14	1.200	0.0	18.932	1.7187	0.6477	-0.8277	0.0180	-0.0092
16T-216	25	15	1.199	0.0	21.045	1.8259	0.7615	-0.9081	0.0187	-0.0118
16T-216	26	1	0.849	0.0	-2.030	-0.0647	0.0451	-0.0277	0.0322	0.0027
16T-216	26	2	0.851	0.0	-0.932	0.0554	0.0414	-0.0424	0.0322	0.0017
16T-216	26	3	0.849	0.0	0.232	0.1842	0.0413	-0.0592	0.0342	0.0009

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	26	4	0.848	0.0	1.317	0.2995	0.0450	-0.0759	0.0357	-0.0002
16T-216	26	5	0.851	0.0	2.580	0.4228	0.0542	-0.0898	0.0356	-0.0017
16T-216	26	6	0.850	0.0	4.794	0.6235	0.0801	-0.1067	0.0285	-0.0037
16T-216	26	7	0.850	0.0	7.124	0.8337	0.1251	-0.1314	0.0239	-0.0049
16T-216	26	8	0.850	0.0	8.313	0.9320	0.1560	-0.1544	0.0267	-0.0057
16T-216	26	9	0.850	0.0	9.494	1.0007	0.1880	-0.1731	0.0295	-0.0068
16T-216	26	10	0.850	0.0	10.603	1.0497	0.2195	-0.1979	0.0272	-0.0070
16T-216	26	11	0.849	0.0	11.709	1.0986	0.2537	-0.2298	0.0247	-0.0079
16T-216	26	12	0.850	0.0	13.921	1.2419	0.3378	-0.3053	0.0217	-0.0084
16T-216	26	13	0.849	0.0	16.179	1.3854	0.4361	-0.3915	0.0169	-0.0066
16T-216	26	14	0.849	0.0	18.522	1.5378	0.5530	-0.4945	0.0144	-0.0065
16T-216	26	15	0.850	0.0	20.667	1.6640	0.6678	-0.5755	0.0147	-0.0087
16T-216	27	1	0.798	0.0	-2.041	-0.0585	0.0428	-0.0274	0.0337	0.0032
16T-216	27	2	0.798	0.0	-0.997	0.0509	0.0391	-0.0413	0.0337	0.0022
16T-216	27	3	0.798	0.0	0.222	0.1788	0.0388	-0.0582	0.0353	0.0010
16T-216	27	4	0.799	0.0	1.253	0.2818	0.0419	-0.0724	0.0360	-0.0001
16T-216	27	5	0.799	0.0	2.398	0.3884	0.0483	-0.0870	0.0365	-0.0013
16T-216	27	6	0.799	0.0	4.772	0.6066	0.0718	-0.1148	0.0347	-0.0040
16T-216	27	7	0.798	0.0	7.074	0.8196	0.1132	-0.1435	0.0319	-0.0053
16T-216	27	8	0.797	0.0	8.229	0.9076	0.1416	-0.1555	0.0340	-0.0058
16T-216	27	9	0.799	0.0	9.340	0.9835	0.1728	-0.1714	0.0340	-0.0064
16T-216	27	10	0.798	0.0	10.404	1.0079	0.2005	-0.1883	0.0265	-0.0065
16T-216	27	11	0.798	0.0	11.520	1.0710	0.2352	-0.2139	0.0261	-0.0079
16T-216	27	12	0.798	0.0	13.765	1.2015	0.3177	-0.2807	0.0228	-0.0088
16T-216	27	13	0.799	0.0	16.015	1.3529	0.4141	-0.3581	0.0193	-0.0083
16T-216	27	14	0.801	0.0	18.420	1.5072	0.5312	-0.4572	0.0172	-0.0091
16T-216	27	15	0.797	0.0	20.518	1.6284	0.6414	-0.5345	0.0177	-0.0117
16T-216	28	1	0.700	0.0	-1.988	-0.0502	0.0406	-0.0269	0.0358	0.0027
16T-216	28	2	0.700	0.0	-0.860	0.0628	0.0373	-0.0414	0.0361	0.0017
16T-216	28	3	0.700	0.0	0.160	0.1634	0.0370	-0.0549	0.0372	0.0006
16T-216	28	4	0.700	0.0	1.167	0.2526	0.0392	-0.0668	0.0374	-0.0004
16T-216	28	5	0.700	0.0	2.292	0.3505	0.0444	-0.0806	0.0372	-0.0015
16T-216	28	6	0.700	0.0	4.583	0.5426	0.0623	-0.1036	0.0354	-0.0042
16T-216	28	7	0.700	0.0	6.834	0.7433	0.0946	-0.1367	0.0332	-0.0061
16T-216	28	8	0.700	0.0	7.940	0.8348	0.1189	-0.1495	0.0343	-0.0063
16T-216	28	9	0.700	0.0	9.088	0.9049	0.1499	-0.1657	0.0325	-0.0070
16T-216	28	10	0.700	0.0	10.163	0.9703	0.1796	-0.1813	0.0312	-0.0079
16T-216	28	11	0.700	0.0	11.316	1.0378	0.2164	-0.2028	0.0271	-0.0088
16T-216	28	12	0.699	0.0	13.607	1.1817	0.2978	-0.2563	0.0246	-0.0106
16T-216	28	13	0.699	0.0	15.805	1.3092	0.3850	-0.3252	0.0196	-0.0101
16T-216	28	14	0.700	0.0	18.063	1.4631	0.4932	-0.4085	0.0186	-0.0110
16T-216	28	15	0.700	0.0	20.316	1.5929	0.6090	-0.4917	0.0187	-0.0149
16T-216	31	1	0.900	0.0	-2.166	-0.0985	0.0530	-0.0303	0.0296	0.0009
16T-216	31	2	0.898	0.0	-0.886	0.0526	0.0473	-0.0410	0.0271	-0.0004
16T-216	31	3	0.900	0.0	0.219	0.1705	0.0486	-0.0511	0.0268	-0.0010
16T-216	31	4	0.901	0.0	1.310	0.2920	0.0535	-0.0640	0.0262	-0.0021
16T-216	31	5	0.898	0.0	2.485	0.4212	0.0625	-0.0826	0.0241	-0.0031

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	31	6	0.902	0.0	4.864	0.6471	0.0926	-0.1142	0.0170	-0.0046
16T-216	31	7	0.900	0.0	7.101	0.8213	0.1346	-0.1445	0.0135	-0.0048
16T-216	31	8	0.901	0.0	8.633	0.9427	0.1729	-0.1789	0.0159	-0.0045
16T-216	31	9	0.900	0.0	8.407	0.9220	0.1662	-0.1714	0.0159	-0.0047
16T-216	31	10	0.900	0.0	9.438	1.0031	0.1947	-0.1986	0.0160	-0.0041
16T-216	31	11	0.900	0.0	10.608	1.0848	0.2309	-0.2277	0.0254	-0.0059
16T-216	31	12	0.900	0.0	11.838	1.1830	0.2744	-0.2640	0.0272	-0.0072
16T-216	31	13	0.898	0.0	14.105	1.3400	0.3643	-0.3532	0.0278	-0.0105
16T-216	31	14	0.899	0.0	16.288	1.4491	0.4548	-0.4275	0.0165	-0.0066
16T-216	31	15	0.899	0.0	18.492	1.5400	0.5641	-0.5271	0.0129	-0.0037
16T-216	31	16	0.906	0.0	20.763	1.7699	0.7130	-0.6547	0.0067	-0.0016
16T-216	32	1	0.849	0.0	-2.115	-0.0782	0.0479	-0.0318	0.0302	0.0012
16T-216	32	2	0.849	0.0	-1.111	0.0267	0.0436	-0.0406	0.0304	0.0005
16T-216	32	3	0.849	0.0	0.089	0.1549	0.0428	-0.0558	0.0306	-0.0002
16T-216	32	4	0.851	0.0	1.200	0.2737	0.0462	-0.0718	0.0322	-0.0010
16T-216	32	5	0.852	0.0	2.476	0.3978	0.0544	-0.0834	0.0314	-0.0025
16T-216	32	6	0.848	0.0	4.777	0.6036	0.0796	-0.1056	0.0239	-0.0046
16T-216	32	7	0.848	0.0	7.054	0.7891	0.1197	-0.1365	0.0170	-0.0054
16T-216	32	8	0.852	0.0	8.183	0.8940	0.1481	-0.1601	0.0168	-0.0052
16T-216	32	9	0.850	0.0	9.352	0.9543	0.1755	-0.1849	0.0228	-0.0052
16T-216	32	10	0.852	0.0	10.495	1.0477	0.2128	-0.2104	0.0290	-0.0064
16T-216	32	11	0.850	0.0	11.645	1.1215	0.2501	-0.2409	0.0322	-0.0083
16T-216	32	12	0.852	0.0	13.955	1.2534	0.3313	-0.3012	0.0240	-0.0086
16T-216	32	13	0.848	0.0	16.159	1.4043	0.4307	-0.3885	0.0221	-0.0089
16T-216	32	14	0.850	0.0	18.391	1.5340	0.5386	-0.4902	0.0162	-0.0071
16T-216	33	1	0.800	0.0	-2.079	-0.0745	0.0459	-0.0287	0.0316	0.0018
16T-216	33	2	0.798	0.0	0.100	0.1494	0.0403	-0.0545	0.0316	-0.0
16T-216	33	3	0.798	0.0	2.451	0.3890	0.0497	-0.0914	0.0359	-0.0018
16T-216	33	4	0.799	0.0	4.673	0.5894	0.0714	-0.1139	0.0319	-0.0046
16T-216	33	5	0.798	0.0	7.007	0.7759	0.1096	-0.1367	0.0229	-0.0054
16T-216	33	6	0.798	0.0	9.263	0.9389	0.1620	-0.1770	0.0274	-0.0050
16T-216	33	7	0.798	0.0	10.395	1.0369	0.1983	-0.2004	0.0341	-0.0061
16T-216	33	8	0.799	0.0	11.543	1.1117	0.2348	-0.2269	0.0356	-0.0075
16T-216	33	9	0.798	0.0	13.746	1.2120	0.3095	-0.2757	0.0258	-0.0091
16T-216	33	10	0.798	0.0	15.567	1.3563	0.4046	-0.3558	0.0220	-0.0092
16T-216	33	11	0.798	0.0	18.233	1.5008	0.5156	-0.4551	0.0186	-0.0086
16T-216	33	12	0.797	0.0	20.441	1.6312	0.6341	-0.5455	0.0170	-0.0088
16T-216	37	1	0.852	0.0	0.843	0.2934	0.0298	-0.0596	0.0011	-0.0019
16T-216	37	2	0.850	0.0	3.831	0.5815	0.0551	-0.0863	0.0008	-0.0022
16T-216	37	3	0.850	0.0	5.714	0.7423	0.0868	-0.1053	0.0010	-0.0023
16T-216	37	4	0.851	0.0	7.898	0.8943	0.1364	-0.1300	-0.0013	-0.0023
16T-216	37	5	0.852	0.0	8.717	0.9338	0.1575	-0.1484	0.0032	-0.0026
16T-216	37	6	0.852	0.0	9.790	0.9945	0.1878	-0.1775	0.0017	-0.0028
16T-216	37	7	0.851	0.0	17.380	1.4953	0.4969	-0.4635	0.0005	-0.0032
16T-216	38	1	0.852	0.0	-1.955	0.0315	0.0272	-0.0431	0.0020	-0.0019
16T-216	38	2	0.851	0.0	-0.926	0.1331	0.0252	-0.0500	0.0015	-0.0021

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	38	3	0.851	0.0	0.133	0.2313	0.0266	-0.0567	0.0012	-0.0021
16T-216	38	4	0.851	0.0	1.221	0.3359	0.0310	-0.0647	0.0012	-0.0021
16T-216	38	5	0.851	0.0	2.225	0.4320	0.0375	-0.0738	0.0010	-0.0025
16T-216	38	6	0.850	0.0	4.471	0.6444	0.0650	-0.0960	0.0005	-0.0024
16T-216	38	7	0.849	0.0	6.591	0.8141	0.1057	-0.1179	0.0020	-0.0025
16T-216	38	8	0.851	0.0	7.641	0.8924	0.1310	-0.1306	0.0023	-0.0027
16T-216	38	9	0.851	0.0	8.672	0.9334	0.1565	-0.1520	0.0038	-0.0028
16T-216	38	10	0.850	0.0	9.814	1.0025	0.1889	-0.1802	0.0027	-0.0027
16T-216	38	11	0.851	0.0	10.829	1.0570	0.2225	-0.2168	0.0013	-0.0026
16T-216	38	12	0.851	0.0	13.013	1.2043	0.3019	-0.2967	-0.0	-0.0023
16T-216	38	13	0.850	0.0	15.227	1.3535	0.3936	-0.3710	-0.0	-0.0025
16T-216	38	14	0.850	0.0	17.369	1.4960	0.4962	-0.4638	0.0004	-0.0030
16T-216	38	15	0.850	0.0	19.501	1.6275	0.6080	-0.5543	-0.0005	-0.0015
16T-216	38	16	0.852	0.0	5.499	0.7345	0.0834	-0.1069	0.0010	-0.0022
16T-216	38	17	0.851	0.0	3.327	0.5370	0.0483	-0.0842	0.0009	-0.0024
16T-216	39	1	0.700	0.0	-1.970	0.0215	0.0244	-0.0363	0.0020	-0.0018
16T-216	39	2	0.701	0.0	-0.954	0.1121	0.0227	-0.0431	0.0017	-0.0017
16T-216	39	3	0.700	0.0	0.102	0.2000	0.0237	-0.0498	0.0013	-0.0018
16T-216	39	4	0.700	0.0	1.061	0.2339	0.0266	-0.0587	0.0011	-0.0019
16T-216	39	5	0.700	0.0	2.179	0.3819	0.0319	-0.0701	0.0017	-0.0019
16T-216	39	6	0.700	0.0	4.200	0.5523	0.0479	-0.0937	0.0007	-0.0022
16T-216	39	7	0.700	0.0	6.452	0.7426	0.0820	-0.1246	0.0007	-0.0024
16T-216	39	8	0.700	0.0	7.471	0.8097	0.1049	-0.1354	0.0014	-0.0022
16T-216	39	9	0.700	0.0	8.702	0.8797	0.1369	-0.1522	0.0029	-0.0024
16T-216	39	10	0.700	0.0	9.618	0.9372	0.1619	-0.1685	0.0020	-0.0025
16T-216	39	11	0.700	0.0	10.657	1.0034	0.1937	-0.1890	0.0003	-0.0024
16T-216	39	12	0.700	0.0	12.869	1.1475	0.2681	-0.2360	-0.0005	-0.0023
16T-216	39	13	0.700	0.0	14.965	1.2623	0.3455	-0.2988	-0.0023	-0.0009
16T-216	39	14	0.699	0.0	17.253	1.4098	0.4485	-0.3904	-0.0013	-0.0014
16T-216	39	15	0.699	0.0	19.268	1.5395	0.5527	-0.4738	0.0006	-0.0037
16T-216	40	1	0.803	0.0	-1.952	0.0236	0.0254	-0.0402	0.0018	-0.0016
16T-216	40	2	0.800	0.0	-0.900	0.1238	0.0232	-0.0464	0.0013	-0.0020
16T-216	40	3	0.802	0.0	0.114	0.2175	0.0244	-0.0536	0.0013	-0.0018
16T-216	40	4	0.801	0.0	1.134	0.3066	0.0281	-0.0615	0.0011	-0.0020
16T-216	40	5	0.801	0.0	2.268	0.4107	0.0344	-0.0716	0.0012	-0.0021
16T-216	40	6	0.803	0.0	4.362	0.6075	0.0549	-0.0954	0.0009	-0.0021
16T-216	40	7	0.802	0.0	6.450	0.7842	0.0911	-0.1189	0.0015	-0.0024
16T-216	40	8	0.803	0.0	7.553	0.8561	0.1164	-0.1307	0.0013	-0.0024
16T-216	40	9	0.803	0.0	8.684	0.9127	0.1459	-0.1481	0.0019	-0.0024
16T-216	40	10	0.803	0.0	9.756	0.9734	0.1781	-0.1759	0.0015	-0.0024
16T-216	40	11	0.802	0.0	10.783	1.0342	0.2102	-0.2006	0.0009	-0.0025
16T-216	40	12	0.803	0.0	12.942	1.1692	0.2843	-0.2622	-0.0008	-0.0019
16T-216	40	13	0.802	0.0	15.096	1.3016	0.3683	-0.3335	-0.0012	-0.0014
16T-216	40	14	0.801	0.0	17.355	1.4626	0.4761	-0.4269	-0.0015	-0.0011
16T-216	40	15	0.802	0.0	19.494	1.5987	0.5891	-0.5211	-0.0005	-0.0023
16T-216	40	16	0.803	-0.0	-2.952	-0.0789	0.0306	-0.0315	0.0019	-0.0014
16T-216	41	1	0.904	-0.0	-2.962	-0.0842	0.0351	-0.0514	0.0013	-0.0018

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	41	2	0.900	0.0	-1.892	0.0385	0.0281	-0.0552	0.0014	-0.0018
16T-216	41	3	0.900	0.0	-0.860	0.1449	0.0267	-0.0588	0.0011	-0.0021
16T-216	41	4	0.900	0.0	0.183	0.2490	0.0290	-0.0627	0.0011	-0.0021
16T-216	41	5	0.901	0.0	1.171	0.3441	0.0344	-0.0683	0.0005	-0.0022
16T-216	41	6	0.900	0.0	2.212	0.4427	0.0435	-0.0750	0.0001	-0.0023
16T-216	41	7	0.900	0.0	4.472	0.6561	0.0751	-0.1038	-0.0007	-0.0024
16T-216	41	8	0.900	0.0	6.564	0.8504	0.1193	-0.1417	0.0	-0.0027
16T-216	41	9	0.900	0.0	7.790	0.9551	0.1512	-0.1628	0.0010	-0.0027
16T-216	41	10	0.900	0.0	8.897	1.0437	0.1839	-0.1807	0.0024	-0.0031
16T-216	41	11	0.900	0.0	9.890	1.0709	0.2084	-0.2030	0.0078	-0.0043
16T-216	41	12	0.899	0.0	10.962	1.1085	0.2402	-0.2344	0.0041	-0.0034
16T-216	41	13	0.901	0.0	13.151	1.2565	0.3238	-0.3214	0.0009	-0.0024
16T-216	41	14	0.899	0.0	15.248	1.3978	0.4143	-0.4115	0.0008	-0.0025
16T-216	41	15	0.899	0.0	17.477	1.5519	0.5251	-0.5088	0.0033	-0.0047
16T-216	41	16	0.900	0.0	19.614	1.6900	0.6416	-0.6000	-0.0003	-0.0014
16T-216	42	1	0.952	-0.0	-3.111	-0.1981	0.0466	-0.0303	0.0007	-0.0019
16T-216	42	2	0.952	0.0	-1.964	-0.0380	0.0372	-0.0518	0.0016	-0.0020
16T-216	42	3	0.951	0.0	-0.897	0.1163	0.0340	-0.0712	0.0017	-0.0022
16T-216	42	4	0.951	0.0	0.080	0.2353	0.0367	-0.0765	0.0010	-0.0024
16T-216	42	5	0.951	0.0	1.189	0.3532	0.0446	-0.0869	0.0007	-0.0025
16T-216	42	6	0.951	0.0	2.238	0.4600	0.0556	-0.0995	0.0004	-0.0024
16T-216	42	7	0.951	0.0	4.459	0.6700	0.0883	-0.1344	0.0002	-0.0026
16T-216	42	8	0.950	0.0	6.610	0.8775	0.1363	-0.1889	-0.0	-0.0025
16T-216	42	9	0.950	0.0	7.764	0.9847	0.1687	-0.2216	0.0003	-0.0023
16T-216	42	10	0.950	0.0	8.948	1.0956	0.2072	-0.2593	0.0003	-0.0022
16T-216	42	11	0.951	0.0	9.995	1.1908	0.2449	-0.2946	0.0004	-0.0021
16T-216	42	12	0.951	0.0	11.073	1.2837	0.2868	-0.3346	0.0006	-0.0021
16T-216	42	13	0.950	0.0	13.309	1.4732	0.3856	-0.4216	0.0002	-0.0019
16T-216	42	14	0.950	0.0	15.515	1.6461	0.4961	-0.5199	-0.0003	-0.0012
16T-216	42	15	0.950	0.0	17.782	1.8211	0.6272	-0.6375	0.0007	-0.0029
16T-216	42	16	0.951	0.0	19.780	1.9109	0.7377	-0.7276	-0.0004	-0.0029
16T-216	43	1	0.999	-0.0	-3.111	-0.2036	0.0608	-0.0001	0.0020	-0.0009
16T-216	43	2	1.000	-0.0	-2.040	-0.0765	0.0528	-0.0313	0.0020	-0.0011
16T-216	43	3	1.000	0.0	-0.999	0.0599	0.0497	-0.0640	0.0021	-0.0014
16T-216	43	4	1.000	0.0	0.137	0.2068	0.0512	-0.0929	0.0014	-0.0018
16T-216	43	5	1.000	0.0	1.085	0.3214	0.0563	-0.1019	0.0010	-0.0016
16T-216	43	6	1.000	0.0	2.240	0.4454	0.0686	-0.1198	0.0010	-0.0019
16T-216	43	7	1.000	0.0	4.477	0.6670	0.1032	-0.1841	0.0005	-0.0021
16T-216	43	8	1.000	0.0	6.557	0.8795	0.1517	-0.2699	0.0006	-0.0020
16T-216	43	9	1.001	0.0	7.806	1.0027	0.1984	-0.3266	0.0006	-0.0021
16T-216	43	10	1.000	0.0	8.816	1.1031	0.2226	-0.3760	0.0007	-0.0022
16T-216	43	11	1.001	0.0	9.981	1.2144	0.2662	-0.4362	0.0009	-0.0023
16T-216	43	12	1.001	0.0	11.169	1.3267	0.3154	-0.5012	0.0009	-0.0025
16T-216	43	13	1.000	0.0	13.209	1.5121	0.4108	-0.6174	0.0006	-0.0024
16T-216	43	14	0.999	0.0	15.411	1.6911	0.5246	-0.7370	0.0004	-0.0019
16T-216	43	15	1.000	0.0	17.634	1.8533	0.6512	-0.8503	0.0011	-0.0024
16T-216	43	16	1.001	0.0	19.789	1.9718	0.7784	-0.9448	-0.0016	-0.0025

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	44	1	1.100	-0.0	-3.054	-0.1875	0.0597	0.0283	0.0016	-0.0014
16T-216	44	2	1.104	0.0	-1.983	-0.0775	0.0538	0.0025	0.0016	-0.0018
16T-216	44	3	1.102	0.0	-1.041	0.0247	0.0512	-0.0306	0.0014	-0.0021
16T-216	44	4	1.101	0.0	0.097	0.1501	0.0524	-0.0702	0.0016	-0.0017
16T-216	44	5	1.101	0.0	1.115	0.2661	0.0577	-0.1071	0.0014	-0.0020
16T-216	44	6	1.103	0.0	2.209	0.3864	0.0673	-0.1451	0.0006	-0.0024
16T-216	44	7	1.103	0.0	4.353	0.6090	0.0971	-0.2043	0.0006	-0.0020
16T-216	44	8	1.101	0.0	6.580	0.8296	0.1445	-0.2778	0.0007	-0.0020
16T-216	44	9	1.100	0.0	7.757	0.9410	0.1763	-0.3225	0.0008	-0.0019
16T-216	44	10	1.104	0.0	8.904	1.0455	0.2115	-0.3705	0.0006	-0.0019
16T-216	44	11	1.104	0.0	9.872	1.1331	0.2446	-0.4135	0.0010	-0.0020
16T-216	44	12	1.098	0.0	11.039	1.2472	0.2898	-0.4720	0.0008	-0.0015
16T-216	44	13	1.105	0.0	13.323	1.4262	0.3872	-0.5849	0.0009	-0.0018
16T-216	44	14	1.096	0.0	15.413	1.5911	0.4895	-0.7009	0.0004	-0.0020
16T-216	44	15	1.101	0.0	15.427	1.5998	0.4925	-0.7081	0.0007	-0.0016
16T-216	44	16	1.104	0.0	17.621	1.7445	0.6083	-0.8149	-0.0002	-0.0022
16T-216	44	17	1.100	0.0	19.759	1.8428	0.7211	-0.8902	-0.0010	-0.0032
16T-216	45	1	1.200	-0.0	-3.019	-0.1849	0.0579	0.0748	0.0020	-0.0012
16T-216	45	2	1.201	-0.0	-2.005	-0.0880	0.0522	0.0389	0.0018	-0.0011
16T-216	45	3	1.202	-0.0	-1.073	0.0052	0.0495	0.0037	0.0018	-0.0010
16T-216	45	4	1.203	0.0	0.108	0.1223	0.0502	-0.0454	0.0013	-0.0015
16T-216	45	5	1.203	0.0	1.108	0.2237	0.0546	-0.0885	0.0008	-0.0019
16T-216	45	6	1.203	0.0	2.186	0.3336	0.0629	-0.1354	0.0002	-0.0023
16T-216	45	7	1.203	0.0	4.266	0.5441	0.0901	-0.2294	-0.0005	-0.0021
16T-216	45	8	1.201	0.0	6.540	0.7768	0.1375	-0.3242	-0.0003	-0.0023
16T-216	45	9	1.200	0.0	7.605	0.8720	0.1642	-0.3627	0.0001	-0.0022
16T-216	45	10	1.200	0.0	8.753	0.9747	0.1974	-0.4058	0.0003	-0.0022
16T-216	45	11	1.200	0.0	9.894	1.0754	0.2344	-0.4503	0.0003	-0.0021
16T-216	45	12	1.202	0.0	10.922	1.1636	0.2715	-0.4950	0.0005	-0.0017
16T-216	45	13	1.202	0.0	13.203	1.3588	0.3663	-0.5996	0.0004	-0.0017
16T-216	45	14	1.201	0.0	15.406	1.5238	0.4686	-0.6998	0.0004	-0.0020
16T-216	45	15	1.200	0.0	17.692	1.6774	0.5862	-0.8053	0.0004	-0.0026
16T-216	45	16	1.200	0.0	19.722	1.7961	0.6964	-0.8913	0.0006	-0.0029
16T-216	46	1	0.853	0.0	-2.993	-0.0951	0.0309	-0.0344	0.0016	-0.0021
16T-216	46	2	0.853	0.0	-1.936	0.0142	0.0247	-0.0431	0.0017	-0.0022
16T-216	46	3	0.852	0.0	-0.968	0.1113	0.0227	-0.0499	0.0014	-0.0021
16T-216	46	4	0.852	0.0	0.073	0.2096	0.0237	-0.0557	0.0009	-0.0022
16T-216	46	5	0.852	0.0	1.192	0.3168	0.0279	-0.0647	0.0010	-0.0022
16T-216	46	6	0.852	0.0	2.273	0.4204	0.0351	-0.0734	0.0010	-0.0023
16T-216	46	7	0.853	0.0	4.435	0.6264	0.0610	-0.0943	0.0007	-0.0024
16T-216	46	8	0.853	0.0	6.486	0.7943	0.0999	-0.1143	0.0017	-0.0025
16T-216	46	9	0.853	0.0	7.672	0.8677	0.1267	-0.1276	-0.0014	-0.0024
16T-216	46	10	0.853	0.0	8.702	0.9269	0.1527	-0.1476	0.0052	-0.0027
16T-216	46	11	0.853	0.0	9.723	0.9845	0.1813	-0.1728	0.0037	-0.0029
16T-216	46	12	0.853	0.0	10.808	1.0388	0.2158	-0.2116	0.0018	-0.0028
16T-216	46	13	0.852	0.0	12.986	1.1897	0.2952	-0.2903	0.0004	-0.0020
16T-216	46	14	0.851	0.0	15.180	1.3368	0.3848	-0.3628	-0.0003	-0.0022
16T-216	46	15	0.850	0.0	17.340	1.4745	0.4847	-0.4498	0.0004	-0.0031

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	46	16	0.849	0.0	19.482	1.6112	0.5979	-0.5454	-0.0007	-0.0012
16T-216	47	1	0.903	0.0	-2.974	-0.0960	0.0334	-0.0506	0.0012	-0.0020
16T-216	47	2	0.903	0.0	-1.951	0.0188	0.0270	-0.0563	0.0017	-0.0021
16T-216	47	3	0.902	0.0	-0.854	0.1322	0.0249	-0.0582	0.0014	-0.0022
16T-216	47	4	0.901	0.0	0.147	0.2321	0.0269	-0.0618	0.0013	-0.0021
16T-216	47	5	0.900	0.0	1.271	0.3390	0.0327	-0.0682	0.0007	-0.0022
16T-216	47	6	0.900	0.0	2.240	0.4321	0.0413	-0.0743	0.0004	-0.0024
16T-216	47	7	0.900	0.0	4.338	0.6316	0.0700	-0.1000	-0.0004	-0.0024
16T-216	47	8	0.900	0.0	6.581	0.8368	0.1158	-0.1372	0.0003	-0.0027
16T-216	47	9	0.899	0.0	7.663	0.9305	0.1438	-0.1576	0.0009	-0.0027
16T-216	47	10	0.899	0.0	8.872	1.0295	0.1791	-0.1771	0.0022	-0.0030
16T-216	47	11	0.899	0.0	9.958	1.0852	0.2091	-0.1980	0.0033	-0.0032
16T-216	47	12	0.899	0.0	10.888	1.0836	0.2323	-0.2272	0.0029	-0.0029
16T-216	47	13	0.900	0.0	13.063	1.2291	0.3133	-0.3107	-0.0011	-0.0013
16T-216	47	14	0.899	0.0	15.234	1.3813	0.4069	-0.4027	0.0015	-0.0029
16T-216	47	15	0.898	0.0	17.484	1.5377	0.5181	-0.5004	0.0032	-0.0047
16T-216	47	16	0.897	0.0	19.646	1.6747	0.6344	-0.5907	-0.0	-0.0016
16T-216	48	1	0.901	-0.0	-2.794	-0.0949	0.0331	-0.0472	-0.0011	-0.0015
16T-216	48	2	0.900	-0.0	-1.821	-0.0078	0.0280	-0.0540	-0.0011	-0.0013
16T-216	48	3	0.902	-0.0	-0.715	0.1234	0.0263	-0.0588	-0.0007	-0.0011
16T-216	48	4	0.902	-0.0	0.202	0.2151	0.0278	-0.0619	-0.0005	-0.0011
16T-216	48	5	0.900	-0.0	1.309	0.3250	0.0332	-0.0685	-0.0008	-0.0012
16T-216	48	6	0.898	-0.0	2.424	0.4309	0.0428	-0.0765	-0.0006	-0.0011
16T-216	48	7	0.898	-0.0	4.483	0.6202	0.0709	-0.0993	-0.0004	-0.0009
16T-216	48	8	0.901	0.0	6.736	0.8367	0.1200	-0.1444	0.0003	-0.0011
16T-216	48	9	0.903	0.0	7.856	0.9369	0.1493	-0.1676	0.0010	-0.0011
16T-216	48	10	0.904	0.0	9.092	1.0453	0.1876	-0.1931	0.0026	-0.0015
16T-216	48	11	0.904	0.0	10.042	1.1103	0.2167	-0.2135	0.0027	-0.0015
16T-216	48	12	0.904	0.0	10.994	1.0949	0.2374	-0.2340	0.0037	-0.0017
16T-216	48	13	0.902	0.0	13.162	1.2252	0.3154	-0.3127	-0.0004	-0.0005
16T-216	48	14	0.898	0.0	15.360	1.3737	0.4083	-0.4070	0.0027	-0.0025
16T-216	48	15	0.900	0.0	17.573	1.5298	0.5192	-0.5047	0.0046	-0.0049
16T-216	48	16	0.900	0.0	19.748	1.6707	0.6368	-0.5974	0.0017	-0.0022
16T-216	48	17	0.900	0.0	17.685	1.5378	0.5248	-0.5090	0.0047	-0.0048
16T-216	48	18	0.901	0.0	15.453	1.3875	0.4152	-0.4114	0.0029	-0.0026
16T-216	48	19	0.902	0.0	13.253	1.2511	0.3225	-0.3163	0.0037	-0.0022
16T-216	48	20	0.902	0.0	11.122	1.0898	0.2391	-0.2336	0.0030	-0.0016
16T-216	48	21	0.901	0.0	10.158	1.1011	0.2168	-0.2066	0.0028	-0.0014
16T-216	48	22	0.900	0.0	9.005	1.0284	0.1823	-0.1829	0.0026	-0.0014
16T-216	48	23	0.900	0.0	7.928	0.9372	0.1501	-0.1674	0.0011	-0.0009
16T-216	48	24	0.900	0.0	6.840	0.8394	0.1208	-0.1414	0.0007	-0.0011
16T-216	49	1	0.700	0.0	-3.014	-0.0999	0.0310	-0.0236	0.0017	-0.0021
16T-216	49	2	0.700	0.0	-1.940	0.0037	0.0255	-0.0329	0.0018	-0.0020
16T-216	49	3	0.700	0.0	-0.905	0.0946	0.0236	-0.0401	0.0015	-0.0021
16T-216	49	4	0.700	0.0	0.230	0.1914	0.0246	-0.0470	0.0010	-0.0023
16T-216	49	5	0.700	0.0	1.251	0.2815	0.0278	-0.0554	0.0016	-0.0022
16T-216	49	6	0.700	0.0	2.350	0.3730	0.0332	-0.0666	0.0009	-0.0023

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_M	C_ℓ	C_n
16T-216	49	7	0.699	0.0	4.545	0.5615	0.0514	-0.0924	0.0006	-0.0025
16T-216	49	8	0.699	0.0	6.852	0.7550	0.0871	-0.1235	0.0011	-0.0024
16T-216	49	9	0.699	0.0	7.971	0.8304	0.1127	-0.1370	0.0014	-0.0024
16T-216	49	10	0.699	0.0	9.049	0.8899	0.1424	-0.1488	0.0009	-0.0025
16T-216	49	11	0.699	0.0	10.231	0.9620	0.1765	-0.1699	0.0014	-0.0023
16T-216	49	12	0.699	0.0	11.289	1.0290	0.2097	-0.1901	-0.0	-0.0019
16T-216	49	13	0.699	0.0	13.545	1.1672	0.2886	-0.2435	-0.0014	-0.0018
16T-216	49	14	0.698	0.0	15.809	1.3004	0.3766	-0.3160	-0.0022	-0.0006
16T-216	49	15	0.698	0.0	18.003	1.4399	0.4794	-0.4059	-0.0017	-0.0007
16T-216	49	16	0.698	0.0	20.179	1.5762	0.5934	-0.4907	-0.0006	-0.0025
16T-216	50	1	0.799	0.0	-3.111	-0.1124	0.0342	-0.0280	0.0017	-0.0018
16T-216	50	2	0.798	0.0	-2.061	-0.0101	0.0278	-0.0357	0.0015	-0.0021
16T-216	50	3	0.798	0.0	-1.005	0.0923	0.0249	-0.0424	0.0014	-0.0019
16T-216	50	4	0.800	0.0	0.243	0.2046	0.0262	-0.0500	0.0010	-0.0020
16T-216	50	5	0.800	0.0	1.370	0.3054	0.0300	-0.0592	0.0010	-0.0020
16T-216	50	6	0.800	0.0	2.384	0.3989	0.0357	-0.0677	0.0011	-0.0021
16T-216	50	7	0.799	0.0	4.728	0.6173	0.0598	-0.0945	0.0008	-0.0023
16T-216	50	8	0.801	0.0	7.023	0.8138	0.1027	-0.1201	0.0006	-0.0023
16T-216	50	9	0.801	0.0	8.246	0.8766	0.1317	-0.1349	-0.0009	-0.0022
16T-216	50	10	0.800	0.0	9.374	0.9432	0.1628	-0.1551	0.0013	-0.0022
16T-216	50	11	0.800	0.0	10.464	0.9950	0.1958	-0.1818	0.0017	-0.0023
16T-216	50	12	0.799	0.0	11.460	1.0562	0.2287	-0.2098	0.0014	-0.0023
16T-216	50	13	0.799	0.0	13.716	1.2042	0.3101	-0.2734	-0.0015	-0.0013
16T-216	50	14	0.799	0.0	15.984	1.3440	0.4022	-0.3498	-0.0012	-0.0015
16T-216	50	15	0.798	0.0	18.219	1.4950	0.5121	-0.4474	-0.0015	-0.0009
16T-216	50	16	0.798	0.0	20.491	1.6309	0.6344	-0.5411	-0.0005	-0.0025
16T-216	51	1	0.852	0.0	-3.092	-0.1118	0.0353	-0.0320	0.0014	-0.0019
16T-216	51	2	0.852	0.0	-2.045	-0.0072	0.0286	-0.0390	0.0014	-0.0018
16T-216	51	3	0.851	0.0	-0.888	0.1102	0.0258	-0.0474	0.0013	-0.0021
16T-216	51	4	0.851	0.0	0.244	0.2194	0.0271	-0.0534	0.0012	-0.0019
16T-216	51	5	0.851	0.0	1.354	0.3223	0.0317	-0.0624	0.0010	-0.0022
16T-216	51	6	0.850	0.0	2.484	0.4353	0.0393	-0.0718	0.0011	-0.0024
16T-216	51	7	0.850	0.0	4.832	0.6499	0.0692	-0.0938	0.0005	-0.0024
16T-216	51	8	0.849	0.0	7.215	0.8465	0.1185	-0.1205	-0.0002	-0.0023
16T-216	51	9	0.850	0.0	8.312	0.9214	0.1459	-0.1350	0.0001	-0.0022
16T-216	51	10	0.850	0.0	9.400	0.9687	0.1735	-0.1572	0.0033	-0.0025
16T-216	51	11	0.850	0.0	10.495	1.0238	0.2053	-0.1881	0.0006	-0.0019
16T-216	51	12	0.850	0.0	11.559	1.0786	0.2406	-0.2251	0.0006	-0.0021
16T-216	51	13	0.850	0.0	13.832	1.2448	0.3295	-0.3115	0.0007	-0.0024
16T-216	51	14	0.850	0.0	16.100	1.3909	0.4264	-0.3888	-0.0004	-0.0020
16T-216	51	15	0.849	0.0	18.332	1.5341	0.5367	-0.4847	0.0001	-0.0027
16T-216	51	16	0.849	0.0	20.530	1.6677	0.6582	-0.5771	-0.0008	-0.0011
16T-216	52	1	0.901	0.0	-3.120	-0.1245	0.0388	-0.0442	0.0012	-0.0021
16T-216	52	2	0.899	0.0	-1.956	0.0051	0.0305	-0.0508	0.0014	-0.0019
16T-216	52	3	0.899	0.0	-0.955	0.1121	0.0282	-0.0553	0.0013	-0.0020
16T-216	52	4	0.900	0.0	0.341	0.2383	0.0307	-0.0593	0.0013	-0.0021
16T-216	52	5	0.899	0.0	1.515	0.3541	0.0374	-0.0658	0.0005	-0.0024

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	52	6	0.899	0.0	2.557	0.4555	0.0474	-0.0727	0.0002	-0.0025
16T-216	52	7	0.900	0.0	4.961	0.6741	0.0826	-0.1026	0.0006	-0.0025
16T-216	52	8	0.900	0.0	7.292	0.8950	0.1361	-0.1464	-0.0002	-0.0022
16T-216	52	9	0.900	0.0	8.466	0.9895	0.1680	-0.1656	-0.0004	-0.0022
16T-216	52	10	0.900	0.0	9.611	1.0832	0.2042	-0.1952	0.0018	-0.0023
16T-216	52	11	0.900	0.0	10.652	1.1269	0.2344	-0.2208	0.0073	-0.0038
16T-216	52	12	0.900	0.0	11.873	1.1729	0.2717	-0.2522	0.0040	-0.0031
16T-216	52	13	0.900	0.0	14.006	1.3083	0.3579	-0.3487	0.0001	-0.0020
16T-216	52	14	0.899	0.0	16.237	1.4558	0.4581	-0.4380	0.0022	-0.0040
16T-216	52	15	0.899	0.0	18.493	1.6056	0.5740	-0.5346	0.0025	-0.0042
16T-216	52	16	0.899	0.0	20.923	1.7519	0.7095	-0.6343	-0.0013	0.0002
16T-216	53	1	0.949	0.0	-3.385	-0.2400	0.0524	-0.0221	0.0007	-0.0020
16T-216	53	2	0.950	0.0	-2.258	-0.1064	0.0422	-0.0407	0.0007	-0.0020
16T-216	53	3	0.949	0.0	-0.676	0.1208	0.0360	-0.0670	0.0014	-0.0022
16T-216	53	4	0.949	0.0	-0.970	0.0774	0.0359	-0.0628	0.0013	-0.0019
16T-216	53	5	0.950	0.0	0.345	0.2451	0.0397	-0.0753	0.0011	-0.0023
16T-216	53	6	0.952	0.0	1.517	0.3684	0.0490	-0.0869	0.0003	-0.0024
16T-216	53	7	0.950	0.0	2.573	0.4725	0.0600	-0.0993	0.0006	-0.0025
16T-216	53	8	0.949	0.0	4.979	0.7045	0.0980	-0.1409	0.0003	-0.0021
16T-216	53	9	0.949	0.0	7.294	0.9274	0.1526	-0.2023	0.0002	-0.0021
16T-216	53	10	0.950	0.0	8.589	1.0430	0.1926	-0.2436	0.0001	-0.0020
16T-216	53	11	0.950	0.0	9.662	1.1422	0.2292	-0.2793	0.0002	-0.0019
16T-216	53	12	0.949	0.0	10.888	1.2484	0.2749	-0.3201	0.0002	-0.0018
16T-216	53	13	0.949	0.0	12.177	1.3591	0.3288	-0.3700	0.0001	-0.0019
16T-216	53	14	0.949	0.0	14.361	1.5446	0.4325	-0.4621	0.0005	-0.0018
16T-216	53	15	0.948	0.0	16.752	1.7266	0.5590	-0.5693	-0.0003	-0.0014
16T-216	53	16	0.948	0.0	19.002	1.8727	0.6899	-0.6802	0.0007	-0.0035
16T-216	53	17	0.950	0.0	21.264	1.9910	0.8261	-0.7884	0.0003	-0.0025
16T-216	54	1	1.201	-0.0	-3.213	-0.2131	0.0630	0.0866	0.0020	-0.0003
16T-216	54	2	1.201	0.0	-2.163	-0.1119	0.0562	0.0485	0.0018	-0.0007
16T-216	54	3	1.200	0.0	-1.131	-0.0113	0.0527	0.0082	0.0016	-0.0015
16T-216	54	4	1.200	0.0	0.089	0.1098	0.0530	-0.0409	0.0011	-0.0021
16T-216	54	5	1.201	0.0	1.227	0.2337	0.0586	-0.0924	0.0006	-0.0018
16T-216	54	6	1.200	0.0	2.387	0.3419	0.0671	-0.1388	0.0003	-0.0019
16T-216	54	7	1.200	0.0	4.892	0.6007	0.1032	-0.2501	-0.0002	-0.0021
16T-216	54	8	1.200	0.0	7.077	0.8145	0.1512	-0.3366	-0.0001	-0.0021
16T-216	54	9	1.200	0.0	8.336	0.9309	0.1856	-0.3829	-0.0002	-0.0019
16T-216	54	10	1.200	0.0	9.447	1.0256	0.2190	-0.4264	0.0002	-0.0020
16T-216	54	11	1.200	0.0	10.798	1.1444	0.2661	-0.4815	0.0003	-0.0019
16T-216	54	12	1.199	0.0	11.905	1.2402	0.3093	-0.5303	0.0004	-0.0019
16T-216	54	13	1.201	0.0	14.376	1.4415	0.4176	-0.6458	0.0002	-0.0016
16T-216	54	14	1.200	0.0	16.499	1.5914	0.5208	-0.7409	-0.0004	-0.0023
16T-216	54	15	1.199	0.0	18.921	1.7422	0.6481	-0.8472	0.0005	-0.0031
16T-216	54	16	1.198	0.0	21.025	1.8456	0.7623	-0.9287	0.0004	-0.0031
16T-216	57	1	0.848	0.0	1.025	0.2716	0.0475	-0.0617	0.0476	0.0002
16T-216	57	2	0.850	0.0	4.294	0.5987	0.0776	-0.1054	0.0450	-0.0044
16T-216	57	3	0.850	0.0	6.299	0.7974	0.1150	-0.1241	0.0370	-0.0065

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	57	4	0.850	0.0	8.598	0.9629	0.1736	-0.1552	0.0378	-0.0088
16T-216	57	5	0.849	0.0	9.456	0.9632	0.1904	-0.1658	0.0259	-0.0080
16T-216	57	6	0.849	0.0	11.662	1.0916	0.2633	-0.2310	0.0297	-0.0101
16T-216	57	7	0.849	0.0	18.436	1.5273	0.5549	-0.4824	0.0220	-0.0106
16T-216	58	1	0.850	0.0	-3.155	-0.1866	0.0518	-0.0055	0.0439	0.0065
16T-216	58	2	0.850	0.0	-2.083	-0.0623	0.0455	-0.0208	0.0464	0.0050
16T-216	58	3	0.850	0.0	-0.920	0.0756	0.0434	-0.0393	0.0488	0.0036
16T-216	58	4	0.850	0.0	0.263	0.1970	0.0448	-0.0524	0.0479	0.0012
16T-216	58	5	0.849	0.0	1.336	0.3032	0.0490	-0.0658	0.0474	-0.0003
16T-216	58	6	0.850	0.0	2.521	0.4160	0.0567	-0.0791	0.0471	-0.0021
16T-216	58	7	0.849	0.0	4.850	0.6576	0.0866	-0.1100	0.0428	-0.0050
16T-216	58	8	0.849	0.0	7.300	0.8835	0.1400	-0.1348	0.0354	-0.0074
16T-216	58	9	0.850	0.0	8.428	0.9473	0.1679	-0.1506	0.0356	-0.0086
16T-216	58	10	0.849	0.0	9.323	0.9566	0.1868	-0.1639	0.0259	-0.0081
16T-216	58	11	0.850	0.0	10.620	1.0324	0.2282	-0.1978	0.0296	-0.0094
16T-216	58	12	0.849	0.0	11.734	1.0981	0.2662	-0.2337	0.0302	-0.0102
16T-216	58	13	0.849	0.0	13.934	1.2330	0.3471	-0.3093	0.0250	-0.0092
16T-216	58	14	0.849	0.0	16.105	1.3835	0.4415	-0.3804	0.0246	-0.0105
16T-216	58	15	0.848	0.0	18.359	1.5223	0.5508	-0.4786	0.0221	-0.0105
16T-216	58	16	0.851	0.0	20.569	1.6535	0.6706	-0.5680	0.0203	-0.0115
16T-216	59	1	0.898	0.0	-3.307	-0.2315	0.0586	0.0003	0.0449	0.0071
16T-216	59	2	0.899	0.0	-2.185	-0.0718	0.0519	-0.0253	0.0479	0.0050
16T-216	59	3	0.899	0.0	-0.828	0.0886	0.0495	-0.0402	0.0481	0.0030
16T-216	59	4	0.899	0.0	0.147	0.1876	0.0512	-0.0493	0.0479	0.0013
16T-216	59	5	0.899	0.0	1.462	0.3300	0.0569	-0.0666	0.0464	-0.0008
16T-216	59	6	0.899	0.0	2.651	0.4650	0.0669	-0.0841	0.0413	-0.0029
16T-216	59	7	0.900	0.0	4.951	0.7025	0.1010	-0.1154	0.0326	-0.0054
16T-216	59	8	0.900	0.0	7.424	0.9099	0.1563	-0.1409	0.0284	-0.0076
16T-216	59	9	0.900	0.0	8.484	0.9870	0.1853	-0.1585	0.0294	-0.0084
16T-216	59	10	0.899	0.0	9.746	1.0795	0.2254	-0.1928	0.0299	-0.0095
16T-216	59	11	0.900	0.0	9.698	1.0751	0.2237	-0.1910	0.0299	-0.0094
16T-216	59	12	0.899	0.0	10.776	1.0822	0.2474	-0.2076	0.0230	-0.0071
16T-216	59	13	0.899	0.0	11.860	1.1528	0.2861	-0.2464	0.0222	-0.0072
16T-216	59	14	0.899	0.0	14.029	1.3036	0.3745	-0.3448	0.0234	-0.0092
16T-216	59	15	0.900	0.0	16.226	1.4372	0.4711	-0.4311	0.0205	-0.0090
16T-216	59	16	0.897	0.0	18.484	1.5844	0.5850	-0.5265	0.0184	-0.0094
16T-216	59	17	0.898	0.0	20.735	1.7173	0.7070	-0.6143	0.0157	-0.0096
16T-216	60	1	0.949	0.0	-3.368	-0.2680	0.0730	0.0046	0.0475	0.0063
16T-216	60	2	0.949	0.0	-2.259	-0.1143	0.0643	-0.0230	0.0515	0.0044
16T-216	60	3	0.950	0.0	-0.565	0.0825	0.0626	-0.0539	0.0510	0.0014
16T-216	60	4	0.949	0.0	0.639	0.2787	0.0679	-0.0702	0.0445	-0.0016
16T-216	60	5	0.950	0.0	0.277	0.2359	0.0660	-0.0662	0.0462	-0.0009
16T-216	60	6	0.951	0.0	1.804	0.4008	0.0785	-0.0883	0.0419	-0.0036
16T-216	60	7	0.950	0.0	1.458	0.3681	0.0749	-0.0822	0.0426	-0.0031
16T-216	60	8	0.950	0.0	2.677	0.4898	0.0882	-0.1019	0.0404	-0.0049
16T-216	60	9	0.951	0.0	5.027	0.7139	0.1252	-0.1492	0.0366	-0.0079
16T-216	60	10	0.951	0.0	7.301	0.9248	0.1778	-0.2029	0.0333	-0.0105

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
16T-216	60	11	0.950	0.0	8.629	1.0415	0.2169	-0.2347	0.0316	-0.0117
16T-216	60	12	0.950	0.0	9.813	1.1442	0.2566	-0.2696	0.0303	-0.0126
16T-216	60	13	0.950	0.0	10.961	1.2430	0.2992	-0.3092	0.0292	-0.0135
16T-216	60	14	0.950	0.0	12.149	1.3445	0.3480	-0.3553	0.0286	-0.0144
16T-216	60	16	0.950	0.0	14.375	1.5272	0.4513	-0.4518	0.0266	-0.0164
16T-216	60	17	0.950	0.0	16.779	1.7036	0.5769	-0.5575	0.0260	-0.0192
16T-216	60	18	0.949	0.0	18.938	1.8054	0.6877	-0.6359	0.0188	-0.0179
16T-216	60	19	0.949	0.0	21.137	1.9434	0.8234	-0.7598	0.0155	-0.0191
16T-216	61	1	1.202	-0.0	-3.176	-0.2097	0.0801	0.0884	0.0268	0.0071
16T-216	61	2	1.202	0.0	-2.028	-0.0970	0.0736	0.0484	0.0276	0.0052
16T-216	61	3	1.202	0.0	-1.025	0.0061	0.0711	0.0088	0.0284	0.0036
16T-216	61	4	1.200	0.0	0.159	0.1297	0.0726	-0.0433	0.0301	0.0014
16T-216	61	5	1.199	0.0	1.233	0.2444	0.0783	-0.0882	0.0307	0.0001
16T-216	61	6	1.202	0.0	2.420	0.3628	0.0886	-0.1362	0.0313	-0.0004
16T-216	61	7	1.202	0.0	4.781	0.6057	0.1230	-0.2347	0.0307	-0.0036
16T-216	61	8	1.200	0.0	7.161	0.8335	0.1742	-0.3189	0.0279	-0.0063
16T-216	61	9	1.199	0.0	8.391	0.9395	0.2071	-0.3614	0.0269	-0.0072
16T-216	61	10	1.202	0.0	9.699	1.0547	0.2473	-0.4163	0.0269	-0.0081
16T-216	61	11	1.199	0.0	10.669	1.1362	0.2805	-0.4556	0.0265	-0.0094
16T-216	61	12	1.202	0.0	12.064	1.2503	0.3334	-0.5174	0.0261	-0.0104
16T-216	61	13	1.200	0.0	14.264	1.4244	0.4280	-0.6158	0.0240	-0.0123
16T-216	61	14	1.199	0.0	16.593	1.5829	0.5397	-0.7218	0.0227	-0.0143
16T-216	61	15	1.201	0.0	18.786	1.7144	0.6521	-0.8190	0.0222	-0.0158
16T-216	61	16	1.199	0.0	20.993	1.8216	0.7706	-0.9013	0.0210	-0.0183
16T-216	62	1	0.803	0.0	-3.212	-0.1912	0.0505	-0.0033	0.0445	0.0065
16T-216	62	2	0.803	0.0	-1.997	-0.0525	0.0438	-0.0208	0.0493	0.0051
16T-216	62	3	0.804	0.0	-0.937	0.0661	0.0421	-0.0367	0.0500	0.0038
16T-216	62	4	0.804	0.0	0.148	0.1724	0.0431	-0.0487	0.0490	0.0019
16T-216	62	5	0.803	0.0	1.308	0.2835	0.0468	-0.0632	0.0484	0.0
16T-216	62	6	0.798	0.0	2.835	0.4224	0.0556	-0.0812	0.0485	-0.0022
16T-216	62	7	0.804	0.0	2.481	0.3931	0.0537	-0.0775	0.0490	-0.0017
16T-216	62	8	0.802	0.0	4.653	0.5883	0.0750	-0.1006	0.0461	-0.0049
16T-216	62	9	0.801	0.0	7.054	0.8124	0.1209	-0.1300	0.0381	-0.0079
16T-216	62	10	0.800	0.0	8.165	0.8672	0.1466	-0.1402	0.0313	-0.0085
16T-216	62	11	0.800	0.0	9.365	0.9417	0.1795	-0.1628	0.0306	-0.0093
16T-216	62	12	0.800	0.0	10.354	0.9893	0.2086	-0.1828	0.0290	-0.0096
16T-216	62	13	0.800	0.0	11.436	1.0577	0.2446	-0.2110	0.0296	-0.0103
16T-216	62	14	0.799	0.0	13.657	1.1911	0.3234	-0.2752	0.0272	-0.0102
16T-216	62	15	0.799	0.0	16.043	1.3485	0.4221	-0.3515	0.0253	-0.0107
16T-216	62	16	0.798	0.0	18.199	1.4864	0.5262	-0.4439	0.0228	-0.0107
16T-216	62	17	0.799	0.0	20.444	1.6174	0.6460	-0.5321	0.0227	-0.0134
16T-216	62	18	0.800	0.0	16.486	1.3812	0.4437	-0.3721	0.0248	-0.0105
16T-216	63	1	0.700	0.0	-3.130	-0.1567	0.0468	-0.0079	0.0478	0.0071
16T-216	63	2	0.698	0.0	-2.701	-0.1103	0.0442	-0.0140	0.0496	0.0063
16T-216	63	3	0.698	0.0	-2.137	-0.0554	0.0418	-0.0209	0.0516	0.0056
16T-216	63	4	0.699	0.0	-0.964	0.0586	0.0392	-0.0352	0.0527	0.0040
16T-216	63	5	0.700	0.0	0.201	0.1681	0.0400	-0.0496	0.0505	0.0018

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	63	6	0.699	0.0	1.297	0.2668	0.0435	-0.0635	0.0500	-0.0
16T-216	63	7	0.699	0.0	2.278	0.3510	0.0482	-0.0759	0.0499	-0.0014
16T-216	63	8	0.699	0.0	3.474	0.4546	0.0562	-0.0899	0.0491	-0.0035
16T-216	63	9	0.699	0.0	4.497	0.5409	0.0652	-0.1022	0.0482	-0.0049
16T-216	63	10	0.699	0.0	6.898	0.7529	0.1037	-0.1297	0.0447	-0.0085
16T-216	63	11	0.700	0.0	7.883	0.8223	0.1279	-0.1415	0.0408	-0.0094
16T-216	63	12	0.699	0.0	9.193	0.8905	0.1629	-0.1575	0.0364	-0.0101
16T-216	63	13	0.699	0.0	10.215	0.9547	0.1923	-0.1752	0.0342	-0.0109
16T-216	63	14	0.699	0.0	11.273	1.0197	0.2246	-0.1924	0.0324	-0.0116
16T-216	63	16	0.699	0.0	13.695	1.1685	0.3070	-0.2481	0.0291	-0.0122
16T-216	63	17	0.699	0.0	15.827	1.2973	0.3917	-0.3214	0.0263	-0.0122
16T-216	63	18	0.698	0.0	18.066	1.4447	0.4973	-0.4067	0.0239	-0.0117
16T-216	63	19	0.699	0.0	20.242	1.5758	0.6118	-0.4908	0.0236	-0.0149
16T-216	66	1	0.850	0.0	0.987	0.2309	0.0488	-0.0579	0.0394	-0.0005
16T-216	66	2	0.849	0.0	4.174	0.5487	0.0766	-0.0985	0.0369	-0.0051
16T-216	66	3	0.851	0.0	6.217	0.7335	0.1093	-0.1251	0.0265	-0.0068
16T-216	66	4	0.851	0.0	8.501	0.9139	0.1604	-0.1613	0.0246	-0.0069
16T-216	66	5	0.850	0.0	9.400	0.9654	0.1825	-0.1810	0.0285	-0.0069
16T-216	66	6	0.851	0.0	11.660	1.1218	0.2555	-0.2426	0.0377	-0.0097
16T-216	66	7	0.849	0.0	18.367	1.5307	0.5407	-0.4863	0.0255	-0.0109
16T-216	67	1	0.850	0.0	-3.242	-0.2325	0.0610	-0.0098	0.0391	0.0038
16T-216	67	2	0.850	0.0	-2.130	-0.1110	0.0516	-0.0188	0.0362	0.0024
16T-216	67	3	0.850	0.0	-1.015	0.0038	0.0471	-0.0278	0.0373	0.0016
16T-216	67	4	0.850	0.0	0.076	0.1345	0.0468	-0.0448	0.0381	0.0003
16T-216	67	5	0.850	0.0	1.322	0.2723	0.0511	-0.0650	0.0410	-0.0012
16T-216	67	6	0.850	0.0	2.559	0.3995	0.0597	-0.0816	0.0417	-0.0028
16T-216	67	7	0.850	0.0	3.530	0.4934	0.0690	-0.0922	0.0402	-0.0043
16T-216	67	8	0.850	0.0	4.726	0.6004	0.0843	-0.1063	0.0345	-0.0056
16T-216	67	9	0.852	0.0	7.036	0.8082	0.1271	-0.1371	0.0246	-0.0071
16T-216	67	10	0.850	0.0	8.311	0.8969	0.1554	-0.1569	0.0265	-0.0069
16T-216	67	11	0.850	0.0	9.423	0.9676	0.1838	-0.1828	0.0291	-0.0068
16T-216	67	12	0.851	0.0	10.491	1.0493	0.2179	-0.2089	0.0348	-0.0077
16T-216	67	13	0.850	0.0	11.712	1.1300	0.2580	-0.2454	0.0384	-0.0100
16T-216	67	14	0.850	0.0	13.921	1.2637	0.3361	-0.3018	0.0336	-0.0111
16T-216	67	15	0.849	0.0	16.104	1.3998	0.4309	-0.3810	0.0305	-0.0120
16T-216	67	16	0.850	0.0	18.366	1.5294	0.5404	-0.4860	0.0246	-0.0102
16T-216	67	17	0.849	0.0	20.772	1.6637	0.6690	-0.5857	0.0215	-0.0085
16T-216	68	1	0.902	0.0	-3.413	-0.2845	0.0687	-0.0053	0.0397	0.0038
16T-216	68	2	0.906	0.0	-2.171	-0.1372	0.0593	-0.0123	0.0371	0.0021
16T-216	68	3	0.899	0.0	-1.019	-0.0006	0.0524	-0.0241	0.0345	0.0010
16T-216	68	4	0.897	0.0	0.044	0.1223	0.0528	-0.0351	0.0355	0.0001
16T-216	68	5	0.900	0.0	1.285	0.2672	0.0588	-0.0544	0.0365	-0.0017
16T-216	68	6	0.901	0.0	2.407	0.3944	0.0675	-0.0752	0.0340	-0.0032
16T-216	68	7	0.899	0.0	3.626	0.5345	0.0807	-0.0994	0.0292	-0.0048
16T-216	68	8	0.900	0.0	5.019	0.6698	0.1024	-0.1178	0.0250	-0.0061
16T-216	68	9	0.899	0.0	7.204	0.8504	0.1449	-0.1530	0.0217	-0.0071
16T-216	68	10	0.901	0.0	8.468	0.9475	0.1770	-0.1788	0.0223	-0.0069

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	68	11	0.899	0.0	9.598	1.0237	0.2059	-0.2005	0.0230	-0.0068
16T-216	68	12	0.899	0.0	10.621	1.0873	0.2370	-0.2219	0.0286	-0.0078
16T-216	68	13	0.901	0.0	11.835	1.1908	0.2809	-0.2650	0.0309	-0.0083
16T-216	68	14	0.900	0.0	14.133	1.3429	0.3696	-0.3501	0.0324	-0.0116
16T-216	68	15	0.900	0.0	16.232	1.4432	0.4568	-0.4277	0.0273	-0.0082
16T-216	68	16	0.899	0.0	18.559	1.5943	0.5762	-0.5273	0.0202	-0.0069
16T-216	68	17	0.898	0.0	20.701	1.7209	0.6936	-0.6216	0.0179	-0.0065
16T-216	69	1	0.948	0.0	-3.480	-0.3274	0.0822	0.0120	0.0406	0.0034
16T-216	69	2	0.948	0.0	-2.350	-0.1944	0.0702	-0.0038	0.0391	0.0019
16T-216	69	3	0.949	0.0	-1.219	-0.0486	0.0641	-0.0199	0.0352	0.0001
16T-216	69	4	0.949	0.0	0.169	0.1417	0.0664	-0.0396	0.0304	-0.0022
16T-216	69	5	0.951	0.0	1.410	0.2950	0.0756	-0.0650	0.0294	-0.0039
16T-216	69	6	0.952	0.0	2.592	0.4332	0.0891	-0.0940	0.0297	-0.0057
16T-216	69	7	0.951	0.0	3.841	0.5613	0.1063	-0.1239	0.0299	-0.0072
16T-216	69	8	0.951	0.0	4.932	0.6722	0.1247	-0.1509	0.0291	-0.0082
16T-216	69	9	0.951	0.0	7.320	0.8890	0.1745	-0.2021	0.0240	-0.0095
16T-216	69	10	0.950	0.0	8.447	0.9881	0.2040	-0.2279	0.0223	-0.0097
16T-216	69	11	0.949	0.0	9.804	1.1107	0.2457	-0.2677	0.0215	-0.0099
16T-216	69	12	0.951	0.0	10.971	1.2082	0.2861	-0.3093	0.0222	-0.0098
16T-216	69	13	0.951	0.0	12.127	1.3148	0.3324	-0.3574	0.0230	-0.0100
16T-216	69	14	0.950	0.0	14.438	1.5136	0.4369	-0.4599	0.0239	-0.0113
16T-216	69	15	0.950	0.0	16.626	1.6871	0.5508	-0.5648	0.0247	-0.0130
16T-216	69	16	0.950	0.0	18.957	1.8459	0.6832	-0.6780	0.0284	-0.0165
16T-216	69	17	0.949	0.0	21.222	1.9741	0.8165	-0.7807	0.0209	-0.0149
16T-216	70	1	1.201	0.0	-3.225	-0.2332	0.0926	0.0888	0.0227	0.0040
16T-216	70	2	1.199	0.0	-2.089	-0.1229	0.0845	0.0441	0.0221	0.0018
16T-216	70	3	1.200	0.0	-1.143	-0.0331	0.0821	0.0109	0.0220	0.0012
16T-216	70	4	1.203	0.0	0.078	0.0898	0.0822	-0.0402	0.0219	-0.0003
16T-216	70	5	1.201	0.0	1.164	0.1926	0.0844	-0.0794	0.0201	-0.0021
16T-216	70	6	1.199	0.0	2.424	0.3213	0.0941	-0.1324	0.0205	-0.0029
16T-216	70	7	1.202	0.0	3.542	0.4390	0.1063	-0.1824	0.0207	-0.0030
16T-216	70	8	1.200	0.0	4.725	0.5582	0.1230	-0.2298	0.0203	-0.0044
16T-216	70	9	1.201	0.0	7.085	0.7892	0.1699	-0.3190	0.0203	-0.0044
16T-216	70	10	1.205	0.0	8.401	0.9081	0.2026	-0.3670	0.0203	-0.0055
16T-216	70	11	1.201	0.0	9.401	0.9997	0.2316	-0.4089	0.0205	-0.0065
16T-216	70	12	1.200	0.0	10.607	1.1010	0.2704	-0.4576	0.0203	-0.0068
16T-216	70	13	1.202	0.0	11.869	1.2074	0.3153	-0.5109	0.0205	-0.0073
16T-216	70	14	1.199	0.0	14.306	1.4098	0.4170	-0.6235	0.0204	-0.0082
16T-216	70	15	1.201	0.0	16.477	1.5627	0.5188	-0.7209	0.0207	-0.0094
16T-216	70	16	1.200	0.0	18.857	1.7126	0.6409	-0.8246	0.0207	-0.0105
16T-216	70	17	1.201	0.0	21.032	1.8252	0.7574	-0.9088	0.0222	-0.0140
16T-216	71	1	0.809	0.0	-3.242	-0.2243	0.0593	-0.0089	0.0390	0.0038
16T-216	71	2	0.805	0.0	-2.112	-0.1124	0.0500	-0.0155	0.0391	0.0026
16T-216	71	3	0.804	0.0	-0.980	0.0083	0.0452	-0.0290	0.0387	0.0017
16T-216	71	4	0.807	0.0	0.088	0.1293	0.0444	-0.0459	0.0394	0.0004
16T-216	71	5	0.809	0.0	1.226	0.2518	0.0477	-0.0650	0.0420	-0.0007
16T-216	71	6	0.805	0.0	2.405	0.3713	0.0541	-0.0843	0.0444	-0.0024

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	71	7	0.803	0.0	3.489	0.4782	0.0633	-0.1019	0.0455	-0.0038
16T-216	71	8	0.798	0.0	4.694	0.5855	0.0763	-0.1160	0.0438	-0.0055
16T-216	71	9	0.796	0.0	7.004	0.7874	0.1144	-0.1402	0.0346	-0.0070
16T-216	71	10	0.794	0.0	8.169	0.8823	0.1411	-0.1575	0.0335	-0.0071
16T-216	71	11	0.795	0.0	9.262	0.9576	0.1686	-0.1770	0.0354	-0.0069
16T-216	71	12	0.795	0.0	10.575	1.0502	0.2080	-0.2049	0.0410	[illegible]
16T-216	71	13	0.796	0.0	11.649	1.1241	0.2431	-0.2297	0.0421	[illegible]
16T-216	71	14	0.799	0.0	13.799	1.2331	0.3171	-0.2794	0.0362	-0.0116
16T-216	71	15	0.799	0.0	16.059	1.3677	0.4132	-0.3570	0.0311	-0.0121
16T-216	71	16	0.799	0.0	18.285	1.5003	0.5203	-0.4533	0.0272	-0.0122
16T-216	71	17	0.800	0.0	20.493	1.6191	0.6356	-0.5429	0.0243	-0.0113
16T-216	72	1	0.699	0.0	-3.194	-0.2047	0.0544	-0.0073	0.0406	0.0038
16T-216	72	2	0.700	0.0	-2.095	-0.1037	0.0467	-0.0150	0.0422	0.0027
16T-216	72	3	0.700	0.0	-1.147	-0.0115	0.0427	-0.0264	0.0430	0.0022
16T-216	72	4	0.700	0.0	-0.005	0.1116	0.0414	-0.0453	0.0445	0.0007
16T-216	72	5	0.699	0.0	1.165	0.2245	0.0433	-0.0637	0.0462	-0.0004
16T-216	72	6	0.699	0.0	2.272	0.3314	0.0481	-0.0809	0.0485	-0.0014
16T-216	72	7	0.699	0.0	3.418	0.4357	0.0554	-0.0959	0.0490	-0.0035
16T-216	72	8	0.699	0.0	4.756	0.5488	0.0677	-0.1141	0.0470	-0.0053
16T-216	72	9	0.699	0.0	4.602	0.5384	0.0661	-0.1124	0.0478	-0.0050
16T-216	72	10	0.700	0.0	6.804	0.7332	0.0968	-0.1426	0.0436	-0.0072
16T-216	72	11	0.699	0.0	7.925	0.8258	0.1198	-0.1597	0.0419	-0.0074
16T-216	72	12	0.699	0.0	9.168	0.9207	0.1523	-0.1801	0.0437	-0.0071
16T-216	72	13	0.699	0.0	10.156	0.9960	0.1782	-0.1941	0.0468	-0.0076
16T-216	72	14	0.699	0.0	11.378	1.0761	0.2146	-0.2135	0.0461	-0.0087
16T-216	72	15	0.699	0.0	13.599	1.1812	0.2910	-0.2618	0.0357	-0.0114
16T-216	72	16	0.699	0.0	15.764	1.3186	0.3794	-0.3238	0.0343	-0.0142
16T-216	72	17	0.699	0.0	17.975	1.4528	0.4821	-0.4047	0.0315	-0.0154
16T-216	72	18	0.699	0.0	20.230	1.5817	0.5987	-0.4929	0.0294	-0.0175
16T-216	75	1	0.900	0.0	-3.281	-0.2594	0.0619	-0.0007	0.0396	0.0048
16T-216	75	2	0.901	0.0	-2.286	-0.1349	0.0548	-0.0118	0.0384	0.0034
16T-216	75	3	0.898	0.0	-0.980	0.0288	0.0500	-0.0286	0.0391	0.0019
16T-216	75	4	0.898	0.0	0.116	0.1582	0.0511	-0.0454	0.0421	0.0007
16T-216	75	5	0.900	0.0	1.325	0.3024	0.0575	-0.0671	0.0432	-0.0012
16T-216	75	6	0.901	0.0	2.501	0.4368	0.0672	-0.0869	0.0388	-0.0032
16T-216	75	7	0.901	0.0	3.852	0.5756	0.0827	-0.1081	0.0322	-0.0049
16T-216	75	8	0.899	0.0	4.878	0.6769	0.0989	-0.1202	0.0291	-0.0058
16T-216	75	9	0.900	0.0	7.299	0.8873	0.1496	-0.1575	0.0265	-0.0072
16T-216	75	10	0.900	0.0	8.397	0.9688	0.1774	-0.1685	0.0259	-0.0075
16T-216	75	11	0.900	0.0	9.508	1.0495	0.2096	-0.1896	0.0265	-0.0079
16T-216	75	12	0.900	0.0	10.676	1.1235	0.2461	-0.2182	0.0307	-0.0089
16T-216	75	13	0.900	0.0	11.896	1.2103	0.2884	-0.2530	0.0307	-0.0092
16T-216	75	14	0.900	0.0	13.987	1.2918	0.3618	-0.3370	0.0222	-0.0083
16T-216	75	15	0.899	0.0	16.205	1.4382	0.4621	-0.4276	0.0214	-0.0085
16T-216	75	16	0.899	0.0	18.471	1.5862	0.5782	-0.5324	0.0181	-0.0067
16T-216	75	17	0.899	0.0	20.703	1.7236	0.7026	-0.6257	0.0149	-0.0064
16T-216	76	1	0.854	0.0	-3.295	-0.2327	0.0574	-0.0067	0.0397	0.0047

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	76	2	0.850	0.0	-2.027	-0.0890	0.0479	-0.0193	0.0392	0.0031
16T-216	76	3	0.851	0.0	-0.993	0.0300	0.0450	-0.0318	0.0416	0.0023
16T-216	76	4	0.850	0.0	0.164	0.1684	0.0451	-0.0527	0.0431	0.0008
16T-216	76	5	0.849	0.0	1.362	0.2955	0.0500	-0.0731	0.0458	-0.0008
16T-216	76	6	0.852	0.0	2.592	0.4184	0.0589	-0.0900	0.0455	-0.0028
16T-216	76	7	0.850	0.0	3.536	0.5088	0.0679	-0.1006	0.0437	-0.0040
16T-216	76	8	0.850	0.0	4.910	0.6438	0.0870	-0.1163	0.0376	-0.0056
16T-216	76	9	0.850	0.0	7.190	0.8511	0.1314	-0.1367	0.0307	-0.0065
16T-216	76	10	0.850	0.0	8.300	0.9368	0.1592	-0.1560	0.0319	-0.0072
16T-216	76	11	0.850	0.0	9.373	1.0015	0.1882	-0.1725	0.0351	-0.0079
16T-216	76	12	0.850	0.0	10.635	1.0752	0.2277	-0.2054	0.0381	-0.0092
16T-216	76	13	0.850	0.0	11.699	1.1101	0.2587	-0.2362	0.0318	-0.0093
16T-216	76	14	0.851	0.0	13.836	1.2451	0.3393	-0.3053	0.0298	-0.0105
16T-216	76	15	0.851	0.0	16.057	1.3833	0.4343	-0.3919	0.0237	-0.0084
16T-216	76	16	0.849	0.0	18.332	1.5248	0.5451	-0.4834	0.0226	-0.0099
16T-216	76	17	0.850	0.0	20.651	1.6578	0.6682	-0.5770	0.0207	-0.0097
16T-216	77	1	0.801	0.0	-3.164	-0.2035	0.0539	-0.0071	0.0409	0.0049
16T-216	77	2	0.802	0.0	-2.194	-0.1013	0.0473	-0.0152	0.0427	0.0038
16T-216	77	3	0.802	0.0	-1.032	0.0238	0.0430	-0.0318	0.0429	0.0025
16T-216	77	4	0.800	0.0	0.158	0.1603	0.0431	-0.0541	0.0455	0.0012
16T-216	77	5	0.799	0.0	1.377	0.2873	0.0471	-0.0735	0.0475	-0.0003
16T-216	77	6	0.799	0.0	2.489	0.3901	0.0535	-0.0871	0.0478	-0.0020
16T-216	77	7	0.799	0.0	3.543	0.4873	0.0620	-0.1005	0.0474	-0.0037
16T-216	77	8	0.799	0.0	4.679	0.5931	0.0745	-0.1155	0.0456	-0.0053
16T-216	77	9	0.799	0.0	7.110	0.8218	0.1174	-0.1443	0.0378	-0.0071
16T-216	77	10	0.799	0.0	8.143	0.9032	0.1427	-0.1566	0.0389	-0.0073
16T-216	77	11	0.799	0.0	9.406	0.9374	0.1773	-0.1758	0.0402	-0.0080
16T-216	77	12	0.799	0.0	10.376	1.0351	0.2057	-0.1934	0.0384	-0.0086
16T-216	77	13	0.799	0.0	11.481	1.0964	0.2403	-0.2185	0.0382	-0.0102
16T-216	77	14	0.799	0.0	13.722	1.2127	0.3223	-0.2870	0.0309	-0.0110
16T-216	77	15	0.800	0.0	14.824	1.2768	0.3649	-0.3192	0.0283	-0.0106
16T-216	77	16	0.799	0.0	16.076	1.3525	0.4181	-0.3625	0.0255	-0.0099
16T-216	77	17	0.799	0.0	18.217	1.4955	0.5236	-0.4510	0.0250	-0.0115
16T-216	77	18	0.799	0.0	20.393	1.6169	0.6365	-0.5326	0.0242	-0.0133
16T-216	78	1	0.701	0.0	-3.121	-0.1854	0.0502	-0.0075	0.0432	0.0048
16T-216	78	2	0.699	0.0	-2.094	-0.0830	0.0438	-0.0175	0.0461	0.0038
16T-216	78	3	0.699	0.0	-1.019	0.0272	0.0403	-0.0326	0.0482	0.0027
16T-216	78	4	0.699	0.0	0.126	0.1456	0.0402	-0.0522	0.0499	0.0011
16T-216	78	5	0.699	0.0	1.124	0.2437	0.0424	-0.0663	0.0500	-0.0002
16T-216	78	6	0.699	0.0	2.281	0.3439	0.0478	-0.0810	0.0502	-0.0019
16T-216	78	7	0.699	0.0	3.393	0.4371	0.0547	-0.0948	0.0496	-0.0034
16T-216	78	8	0.700	0.0	4.450	0.5265	0.0639	-0.1083	0.0484	-0.0051
16T-216	78	9	0.699	0.0	6.815	0.7391	0.0962	-0.1404	0.0442	-0.0073
16T-216	78	10	0.699	0.0	7.932	0.8318	0.1196	-0.1545	0.0443	-0.0077
16T-216	78	11	0.699	0.0	9.131	0.9158	0.1528	-0.1704	0.0444	-0.0083
16T-216	78	12	0.699	0.0	10.212	0.9778	0.1837	-0.1848	0.0405	-0.0094
16T-216	78	13	0.700	0.0	11.354	1.0431	0.2194	-0.2065	0.0381	-0.0106
16T-216	78	14	0.698	0.0	13.601	1.1782	0.2995	-0.2581	0.0342	-0.0128

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	78	15	0.700	0.0	15.765	1.3049	0.3842	-0.3223	0.0295	-0.0131
16T-216	78	16	0.699	0.0	17.960	1.4466	0.4871	-0.4020	0.0282	-0.0140
16T-216	78	17	0.699	0.0	20.160	1.5782	0.6008	-0.4869	0.0277	-0.0175
16T-216	81	1	0.900	0.0	-3.310	-0.2216	0.0484	0.0001	0.0331	0.0024
16T-216	81	2	0.899	0.0	-2.008	-0.0493	0.0403	-0.0271	0.0357	0.0008
16T-216	81	3	0.901	0.0	-0.974	0.0792	0.0378	-0.0376	0.0346	-0.0005
16T-216	81	4	0.899	0.0	0.385	0.2188	0.0400	-0.0487	0.0347	-0.0019
16T-216	81	5	0.897	0.0	1.442	0.3387	0.0461	-0.0626	0.0329	-0.0031
16T-216	81	6	0.899	0.0	2.614	0.4686	0.0571	-0.0791	0.0283	-0.0042
16T-216	81	7	0.900	0.0	3.811	0.5882	0.0730	-0.0939	0.0250	-0.0049
16T-216	81	8	0.900	0.0	4.922	0.6873	0.0915	-0.1072	0.0243	-0.0055
16T-216	81	9	0.899	0.0	7.315	0.8962	0.1449	-0.1383	0.0229	-0.0066
16T-216	81	10	0.899	0.0	8.407	0.9837	0.1749	-0.1554	0.0222	-0.0068
16T-216	81	11	0.900	0.0	9.599	1.0703	0.2098	-0.1791	0.0204	-0.0070
16T-216	81	12	0.899	0.0	10.714	1.1423	0.2445	-0.2047	0.0151	-0.0060
16T-216	81	13	0.899	0.0	11.715	1.1616	0.2738	-0.2468	0.0158	-0.0062
16T-216	81	14	0.900	0.0	14.041	1.3060	0.3668	-0.3481	0.0181	-0.0080
16T-216	81	15	0.899	0.0	16.279	1.4567	0.4691	-0.4400	0.0154	-0.0078
16T-216	81	16	0.899	0.0	18.541	1.6132	0.5867	-0.5331	0.0131	-0.0073
16T-216	81	17	0.899	0.0	20.754	1.7378	0.7067	-0.6216	0.0102	-0.0051
16T-216	82	1	1.200	0.0	-3.118	-0.2051	0.0714	0.0834	0.0234	0.0003
16T-216	82	2	1.201	0.0	-2.086	-0.1023	0.0652	0.0423	0.0234	-0.0003
16T-216	82	3	1.201	0.0	-0.883	0.0165	0.0620	-0.0054	0.0237	-0.0015
16T-216	82	4	1.201	0.0	0.191	0.1271	0.0631	-0.0495	0.0239	-0.0021
16T-216	82	5	1.201	0.0	1.299	0.2400	0.0684	-0.0957	0.0242	-0.0025
16T-216	82	6	1.200	0.0	2.388	0.3521	0.0775	-0.1416	0.0245	-0.0032
16T-216	82	7	1.200	0.0	3.640	0.4819	0.0932	-0.1967	0.0245	-0.0039
16T-216	82	8	1.200	0.0	4.710	0.5927	0.1108	-0.2415	0.0236	-0.0045
16T-216	82	9	1.201	0.0	7.108	0.8208	0.1623	-0.3282	0.0215	-0.0057
16T-216	82	10	1.201	0.0	8.305	0.9308	0.1947	-0.3725	0.0207	-0.0064
16T-216	82	11	1.200	0.0	9.654	1.0513	0.2366	-0.4257	0.0200	-0.0076
16T-216	82	12	1.200	0.0	10.673	1.1365	0.2714	-0.4661	0.0194	-0.0083
16T-216	82	13	1.200	0.0	11.876	1.2395	0.3176	-0.5181	0.0186	-0.0088
16T-216	82	14	1.200	0.0	14.293	1.4345	0.4223	-0.6306	0.0168	-0.0099
16T-216	82	15	1.199	0.0	16.633	1.5998	0.5357	-0.7388	0.0151	-0.0108
16T-216	82	16	1.198	0.0	18.789	1.7338	0.6494	-0.8353	0.0142	-0.0115
16T-216	82	17	1.199	0.0	21.031	1.8418	0.7691	-0.9174	0.0122	-0.0115
16T-216	83	1	0.848	0.0	-3.210	-0.1913	0.0434	0.0002	0.0307	0.0018
16T-216	83	2	0.851	0.0	-1.960	-0.0399	0.0364	-0.0202	0.0353	0.0008
16T-216	83	3	0.849	0.0	-0.971	0.0791	0.0347	-0.0362	0.0364	-0.0001
16T-216	83	4	0.850	0.0	0.169	0.1955	0.0360	-0.0483	0.0359	-0.0013
16T-216	83	5	0.851	0.0	1.476	0.3199	0.0414	-0.0623	0.0355	-0.0027
16T-216	83	6	0.849	0.0	2.558	0.4289	0.0489	-0.0740	0.0354	-0.0036
16T-216	83	7	0.850	0.0	3.622	0.5407	0.0604	-0.0899	0.0343	-0.0045
16T-216	83	8	0.850	0.0	3.662	0.5466	0.0609	-0.0899	0.0343	-0.0044
16T-216	83	9	0.850	0.0	4.939	0.6747	0.0805	-0.1100	0.0309	-0.0054
16T-216	83	10	0.850	0.0	7.242	0.8718	0.1290	-0.1306	0.0250	-0.0065

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
16T-216	83	11	0.851	0.0	8.420	0.9375	0.1578	-0.1421	0.0253	-0.0070
16T-216	83	12	0.850	0.0	9.504	0.9942	0.1871	-0.1627	0.0248	-0.0076
16T-216	83	13	0.851	0.0	10.668	1.0461	0.2204	-0.1930	0.0207	-0.0071
16T-216	83	14	0.850	0.0	11.594	1.0974	0.2529	-0.2265	0.0187	-0.0070
16T-216	83	15	0.850	0.0	13.917	1.2515	0.3418	-0.3145	0.0177	-0.0068
16T-216	83	16	0.850	0.0	16.261	1.4093	0.4445	-0.3921	0.0166	-0.0070
16T-216	83	17	0.849	0.0	18.331	1.5417	0.5474	-0.4834	0.01[illegible]	-0.0078
16T-216	83	18	0.849	0.0	20.588	1.6724	0.6685	-0.5734	0.0135	-0.0071
16T-216	84	1	0.801	0.0	-3.163	-0.1730	0.0409	-0.0047	0.0310	0.0016
16T-216	84	2	0.800	0.0	-1.982	-0.0396	0.0352	-0.0189	0.0370	0.0008
16T-216	84	3	0.800	0.0	-0.892	0.0806	0.0334	-0.0343	0.0376	-0.0001
16T-216	84	4	0.800	0.0	0.199	0.1854	0.0345	-0.0463	0.0364	-0.0014
16T-216	84	5	0.800	0.0	1.356	0.2939	0.0387	-0.0595	0.0367	-0.0024
16T-216	84	6	0.800	0.0	2.401	0.3912	0.0446	-0.0712	0.0364	-0.0031
16T-216	84	7	0.800	0.0	3.560	0.4980	0.0539	-0.0838	0.0356	-0.0043
16T-216	84	8	0.800	0.0	4.709	0.6043	0.0672	-0.0966	0.0338	-0.0054
16T-216	84	9	0.800	0.0	6.985	0.8146	0.1104	-0.1281	0.0282	-0.0065
16T-216	84	10	0.800	0.0	8.148	0.8897	0.1380	-0.1408	0.0260	-0.0069
16T-216	84	11	0.799	0.0	9.266	0.9417	0.1673	-0.1566	0.0233	-0.0074
16T-216	84	12	0.799	0.0	10.426	1.0087	0.2037	-0.1830	0.0225	-0.0076
16T-216	84	13	0.799	0.0	11.533	1.0702	0.2402	-0.2157	0.0205	-0.0079
16T-216	84	14	0.800	0.0	13.783	1.2200	0.3234	-0.2814	0.0183	-0.0070
16T-216	84	15	0.800	0.0	16.049	1.3657	0.4177	-0.3534	0.0176	-0.0071
16T-216	84	16	0.799	0.0	18.402	1.5163	0.5331	-0.4567	0.0171	-0.0087
16T-216	84	17	0.799	0.0	20.496	1.6360	0.6446	-0.5360	0.0158	-0.0093
16T-216	85	1	0.699	0.0	-3.137	-0.1522	0.0386	-0.0045	0.0350	0.0015
16T-216	85	2	0.699	0.0	-1.956	-0.0276	0.0331	-0.0200	0.0396	0.0007
16T-216	85	3	0.700	0.0	-1.051	0.0594	0.0315	-0.0299	0.0399	-0.0002
16T-216	85	4	0.698	0.0	0.150	0.1688	0.0323	-0.0438	0.0388	-0.0013
16T-216	85	5	0.699	0.0	1.168	0.2594	0.0351	-0.0558	0.0385	-0.0023
16T-216	85	6	0.699	0.0	2.230	0.3525	0.0401	-0.0677	0.0382	-0.0031
16T-216	85	7	0.699	0.0	3.333	0.4470	0.0475	-0.0800	0.0379	-0.0040
16T-216	85	8	0.649	0.0	4.599	0.5532	0.0587	-0.0964	0.0370	-0.0052
16T-216	85	9	0.699	0.0	6.803	0.7535	0.0936	-0.1309	0.0345	-0.0069
16T-216	85	10	0.699	0.0	7.890	0.8337	0.1193	-0.1442	0.0314	-0.0075
16T-216	85	11	0.699	0.0	9.024	0.9063	0.1500	-0.1544	0.0260	-0.0079
16T-216	85	12	0.700	0.0	10.203	0.9684	0.1840	-0.1725	0.0246	-0.0084
16T-216	85	13	0.700	0.0	11.290	1.0345	0.2183	-0.1927	0.0232	-0.0086
16T-216	85	14	0.699	0.0	13.564	1.1785	0.2974	-0.2431	0.0207	-0.0089
16T-216	85	15	0.699	0.0	15.761	1.3112	0.3840	-0.3121	0.0181	-0.0073
16T-216	85	16	0.699	0.0	18.040	1.4561	0.4909	-0.4017	0.0178	-0.0088
16T-216	85	17	0.699	0.0	20.298	1.5938	0.6111	-0.4925	0.0172	-0.0112

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	13	1	0.890	-0.0	-0.101	-0.1260	0.0256	0.0263	0.0001	-0.0003
04T- 43	13	2	0.896	-0.0	-0.104	-0.1276	0.0253	0.0258	0.0001	0.0
04T- 43	13	3	0.895	0.0	2.066	0.0875	0.0251	-0.0328	0.0001	0.0001
04T- 43	13	4	0.895	0.0	4.225	0.2901	0.0340	-0.0907	0.0003	-0.0004
04T- 43	13	5	0.895	0.0	6.377	0.4892	0.0544	-0.1489	-0.0010	-0.0007
04T- 43	13	6	0.901	0.0	8.542	0.6947	0.0964	-0.2081	-0.0001	0.0002
04T- 43	13	7	0.889	0.0	10.649	0.8109	0.1435	-0.2189	0.0016	-0.0002
04T- 43	13	8	0.892	0.0	12.749	0.9233	0.2037	-0.2431	0.0015	-0.0001
04T- 43	13	9	0.900	0.0	14.847	1.0479	0.2716	-0.3301	0.0	0.0004
04T- 43	13	10	0.899	0.0	16.936	1.1863	0.3528	-0.4385	-0.0012	0.0013
04T- 43	13	11	0.895	0.0	19.044	1.3504	0.4541	-0.5417	-0.0007	0.0002
04T- 43	13	12	0.896	0.0	21.145	1.4910	0.5604	-0.6532	-0.0015	0.0008
04T- 43	13	13	0.897	0.0	11.698	0.8622	0.1728	-0.2259	0.0022	0.0001
04T- 43	13	14	0.899	0.0	23.255	1.6254	0.6761	-0.7640	-0.0017	0.0010
04T- 43	13	15	0.899	0.0	25.370	1.7468	0.7985	-0.8355	-0.0013	0.0003
04T- 43	13	16	0.896	0.0	20.104	1.4229	0.5050	-0.5919	-0.0005	0.0018
04T- 43	14	1	1.198	0.0	-0.047	-0.1485	0.0563	0.1864	-0.0006	-0.0008
04T- 43	14	2	1.203	0.0	2.099	0.0719	0.0564	0.0248	-0.0003	-0.0010
04T- 43	14	3	1.201	0.0	4.237	0.2748	0.0673	-0.1202	-0.0001	-0.0013
04T- 43	14	4	1.201	0.0	6.375	0.4817	0.0908	-0.2734	-0.0007	-0.0012
04T- 43	14	5	1.202	0.0	8.510	0.6885	0.1305	-0.4263	-0.0013	-0.0001
04T- 43	14	6	1.193	0.0	10.645	0.8888	0.1843	-0.5687	-0.0006	-0.0016
04T- 43	14	7	1.206	0.0	12.784	1.0498	0.2480	-0.6652	-0.0011	-0.0016
04T- 43	14	8	1.195	0.0	14.915	1.2293	0.3294	-0.7926	-0.0008	-0.0016
04T- 43	14	9	1.205	0.0	17.045	1.3772	0.4165	-0.9023	-0.0012	-0.0016
04T- 43	14	10	1.203	0.0	19.142	1.4898	0.5049	-0.9766	-0.0012	-0.0017
04T- 43	14	11	1.203	0.0	21.260	1.6067	0.6051	-1.0577	-0.0022	-0.0008
04T- 43	14	12	1.202	0.0	23.366	1.7128	0.7102	-1.1312	-0.0025	-0.0010
04T- 43	14	13	1.194	0.0	25.467	1.8196	0.8246	-1.2158	-0.0031	-0.0016
04T- 43	17	1	0.896	0.0	4.986	0.3736	0.0415	-0.1229	-0.0	-0.0008
04T- 43	17	2	0.897	0.0	8.007	0.6648	0.0869	-0.2200	-0.0004	-0.0010
04T- 43	17	3	0.896	0.0	9.809	0.7736	0.1270	-0.2215	-0.0001	-0.0007
04T- 43	17	4	0.894	0.0	12.749	0.9194	0.2037	-0.2511	0.0014	-0.0008
04T- 43	20	1	0.031	0.2	-1.001	-0.4150	0.4156	0.2337	-0.0107	0.0387
04T- 43	20	2	0.888	0.0	1.145	0.2904	0.0327	-0.0789	-0.0002	-0.0027
04T- 43	20	3	0.898	0.0	4.481	0.5688	0.0670	-0.0796	-0.0002	-0.0019
04T- 43	20	4	0.899	0.0	6.479	0.7253	0.1028	-0.0856	0.0007	-0.0011
04T- 43	20	5	0.897	0.0	8.802	0.8945	0.1572	-0.0895	0.0023	-0.0022
04T- 43	20	6	0.900	0.0	9.717	0.9503	0.1814	-0.0904	0.0030	-0.0018
04T- 43	20	7	0.895	0.0	11.876	1.0105	0.2314	-0.0571	-0.0046	0.0012
04T- 43	23	1	0.892	0.0	-0.883	0.1207	0.0268	-0.0879	0.0008	-0.0031
04T- 43	23	2	0.897	0.0	-3.355	-0.1247	0.0376	-0.0839	0.0003	-0.0040
04T- 43	23	3	0.895	0.0	1.497	0.3181	0.0354	-0.0816	0.0002	-0.0024
04T- 43	23	4	0.902	0.0	3.846	0.5117	0.0586	-0.0830	-0.0001	-0.0023
04T- 43	23	5	0.902	0.0	6.195	0.7007	0.0971	-0.0926	0.0006	-0.0023
04T- 43	23	6	0.893	0.0	8.527	0.8805	0.1499	-0.1005	0.0007	-0.0020

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	23	7	0.895	0.0	10.818	1.0114	0.2092	-0.0904	0.0033	-0.0027
04T- 43	23	8	0.895	0.0	13.004	1.0633	0.2639	-0.0585	0.0012	-0.0024
04T- 43	23	9	0.900	0.0	15.169	1.1308	0.3295	-0.0413	0.0015	-0.0015
04T- 43	26	1	0.897	0.0	-0.895	0.1131	0.0276	-0.0864	0.0008	-0.0023
04T- 43	26	2	0.895	0.0	-3.343	-0.1276	0.0381	-0.0816	0.0008	-0.0028
04T- 43	26	3	0.897	0.0	1.507	0.3217	0.0361	-0.0814	0.0003	-0.0019
04T- 43	26	4	0.896	0.0	3.888	0.5202	0.0582	-0.0789	0.0001	-0.0017
04T- 43	26	5	0.898	0.0	6.246	0.7104	0.0980	-0.0872	0.0004	-0.0015
04T- 43	26	6	0.900	0.0	8.584	0.8888	0.1526	-0.0988	0.0006	-0.0015
04T- 43	26	7	0.898	0.0	10.850	1.0219	0.2129	-0.0907	0.0016	-0.0012
04T- 43	26	8	0.898	0.0	13.000	1.0632	0.2653	-0.0556	0.0048	-0.0020
04T- 43	26	9	0.896	0.0	15.156	1.1245	0.3285	-0.0403	0.0034	-0.0026
04T- 43	29	1	0.898	0.0	~~-3.837~~	~~-1.4878~~	~~0.1077~~	~~-0.0408~~	~~0.0004~~	~~-0.0046~~
04T- 43	29	2	0.899	0.0	3.897	0.5243	0.0589	-0.0812	-0.0002	-0.0016
04T- 43	29	3	0.887	0.0	6.236	0.7089	0.0956	-0.0796	-0.0	-0.0018
04T- 43	29	4	0.899	0.0	8.574	0.8855	0.1521	-0.0936	0.0010	-0.0018
04T- 43	29	5	0.899	0.0	13.047	1.0948	0.2726	-0.0611	0.0028	-0.0015
04T- 43	29	6	0.898	0.0	15.174	1.1358	0.3330	-0.0472	-0.0005	-0.0009
04T- 43	30	1	0.898	0.0	-0.898	0.1123	0.0278	-0.0881	0.0006	-0.0024
04T- 43	30	2	0.894	0.0	-3.343	-0.1267	0.0383	-0.0836	0.0001	-0.0032
04T- 43	30	3	0.898	0.0	1.510	0.3239	0.0360	-0.0818	0.0	-0.0022
04T- 43	30	4	0.898	0.0	1.510	0.3239	0.0360	-0.0820	0.0001	-0.0021
04T- 43	30	5	0.897	0.0	3.891	0.5224	0.0580	-0.0786	-0.0004	-0.0020
04T- 43	30	6	0.898	0.0	6.257	0.7186	0.0989	-0.0873	-0.0002	-0.0018
04T- 43	30	8	0.900	0.0	10.839	1.0050	0.2100	-0.0811	0.0029	-0.0017
04T- 43	30	9	0.899	0.0	12.987	1.0486	0.2624	-0.0570	-0.0002	-0.0005
04T- 43	30	10	0.896	0.0	15.163	1.1302	0.3316	-0.0426	0.0031	-0.0022
04T- 43	30	11	0.899	0.0	15.918	1.1485	0.3535	-0.0401	0.0020	-0.0017
04T- 43	31	1	0.795	0.0	-0.919	0.0911	0.0251	-0.0667	0.0006	-0.0016
04T- 43	31	2	0.797	0.0	-3.283	-0.1166	0.0338	-0.0678	0.0008	-0.0023
04T- 43	31	3	0.798	0.0	1.421	0.2790	0.0300	-0.0572	0.0003	-0.0013
04T- 43	31	4	0.801	0.0	3.762	0.4680	0.0450	-0.0508	0.0004	-0.0010
04T- 43	31	5	0.802	0.0	6.111	0.6569	0.0750	-0.0401	0.0	-0.0009
04T- 43	31	6	0.798	0.0	8.382	0.8004	0.1200	-0.0242	0.0013	-0.0005
04T- 43	31	7	0.797	0.0	8.375	0.7982	0.1198	-0.0241	0.0007	-0.0006
04T- 43	31	8	0.803	0.0	10.590	0.8962	0.1727	-0.0101	0.0011	-0.0007
04T- 43	31	9	0.800	0.0	12.769	0.9874	0.2352	-0.0018	0.0005	-0.0
04T- 43	31	10	0.798	0.0	12.757	0.9796	0.2325	0.0002	0.0013	-0.0002
04T- 43	31	11	0.800	0.0	14.926	1.0462	0.2927	0.0189	0.0004	0.0003
04T- 43	31	12	0.802	0.0	17.107	1.1177	0.3589	0.0341	0.0002	0.0005
04T- 43	32	1	0.700	0.0	-0.931	0.0794	0.0228	-0.0550	0.0004	-0.0012
04T- 43	32	2	0.698	0.0	-3.237	-0.1094	0.0313	-0.0606	0.0010	-0.0020
04T- 43	32	3	0.700	0.0	1.351	0.2514	0.0278	-0.0458	0.0001	-0.0008
04T- 43	32	4	0.699	0.0	3.630	0.4218	0.0399	-0.0380	0.0003	-0.0005
04T- 43	32	5	0.699	0.0	5.913	0.5932	0.0627	-0.0275	0.0003	-0.0002

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	32	6	0.700	0.0	8.173	0.7396	0.1018	-0.0121	-0.0001	0.0003
04T- 43	32	7	0.696	0.0	10.372	0.8596	0.1561	0.0022	-0.0011	0.0007
04T- 43	32	8	0.697	0.0	12.571	0.9630	0.2154	0.0152	-0.0041	0.0014
04T- 43	32	9	0.699	0.0	14.711	1.0175	0.2718	0.0419	-0.0003	0.0017
04T- 43	32	10	0.700	0.0	16.851	1.0757	0.3332	0.0573	-0.0005	0.0021
04T- 43	32	11	0.699	0.0	18.966	1.1363	0.4025	0.0578	0.0026	-0.0015
04T- 43	32	12	0.700	0.0	21.124	1.2032	0.4796	0.0536	0.0025	-0.0008
04T- 43	33	1	1.205	-0.0	-1.053	0.0965	0.0498	-0.0483	0.0003	-0.0015
04T- 43	33	2	1.202	-0.0	-3.425	-0.1775	0.0601	-0.0224	0.0003	-0.0027
04T- 43	33	3	1.204	0.0	1.361	0.2127	0.0543	-0.0794	0.0	-0.0013
04T- 43	33	4	1.205	0.0	3.775	0.4130	0.0746	-0.1099	-0.0007	-0.0014
04T- 43	33	5	1.202	0.0	6.170	0.6148	0.1122	-0.1392	-0.0007	-0.0010
04T- 43	33	6	1.203	0.0	8.561	0.7996	0.1643	-0.1592	-0.0005	-0.0008
04T- 43	33	7	1.206	0.0	8.561	0.7963	0.1635	-0.1587	-0.0005	-0.0007
04T- 43	33	8	1.203	0.0	10.927	0.9598	0.2273	-0.1728	-0.0003	-0.0008
04T- 43	33	9	1.203	0.0	13.251	1.1073	0.3024	-0.1886	-0.0002	-0.0009
04T- 43	33	10	1.206	0.0	14.134	1.1572	0.3327	-0.1940	-0.0001	-0.0009
04T- 43	36	1	0.899	0.0	-0.968	0.0726	0.0361	-0.0850	0.0003	-0.0030
04T- 43	36	2	0.893	0.0	3.818	0.4992	0.0596	-0.0894	0.0004	-0.0025
04T- 43	36	1	0.899	0.0	-0.968	0.6851	0.0933	-0.0931	0.0003	-0.0024
04T- 43	36	2	0.893	0.0	3.818	0.8548	0.1376	-0.0876	0.0004	-0.0019
04T- 43	36	3	0.900	0.0	6.197	0.6851	0.0933	-0.0931	0.0005	-0.0024
04T- 43	36	4	0.893	0.0	8.519	0.8548	0.1376	-0.0876	0.0005	-0.0019
04T- 43	36	5	0.896	0.0	13.044	1.0753	0.2547	-0.0515	0.0001	-0.0006
04T- 43	36	6	0.900	0.0	15.229	1.1599	0.3254	-0.0427	0.0034	-0.0031
04T- 43	37	1	0.899	0.0	-0.963	0.0746	0.0363	-0.0840	0.0	-0.0027
04T- 43	37	2	0.894	0.0	-3.350	-0.1349	0.0494	-0.0765	0.0002	-0.0035
04T- 43	37	3	0.898	0.0	1.459	0.2991	0.0391	-0.0869	0.0004	-0.0023
04T- 43	37	4	0.896	0.0	3.834	0.4980	0.0595	-0.0873	0.0001	-0.0022
04T- 43	37	5	0.901	0.0	6.190	0.6871	0.0924	-0.0903	0.0001	-0.0022
04T- 43	37	6	0.898	0.0	8.535	0.8556	0.1387	-0.0881	0.0008	-0.0017
04T- 43	37	7	0.902	0.0	10.800	0.9887	0.1959	-0.0798	0.0031	-0.0020
04T- 43	37	8	0.899	0.0	13.041	1.0787	0.2555	-0.0581	0.0020	-0.0019
04T- 43	37	9	0.898	0.0	15.206	1.1523	0.3222	-0.0383	0.0037	-0.0027
04T- 43	38	1	0.797	0.0	-0.965	0.0632	0.0305	-0.0660	0.0006	-0.0024
04T- 43	38	2	0.798	0.0	-3.306	-0.1330	0.0432	-0.0641	-0.0001	-0.0035
04T- 43	38	3	0.798	0.0	1.380	0.2656	0.0306	-0.0643	0.0003	-0.0019
04T- 43	38	4	0.803	0.0	3.727	0.4574	0.0443	-0.0600	0.0003	-0.0016
04T- 43	38	5	0.801	0.0	6.053	0.6410	0.0699	-0.0518	-0.0006	-0.0016
04T- 43	38	6	0.796	0.0	8.392	0.8083	0.1095	-0.0383	-0.0003	-0.0011
04T- 43	38	7	0.799	0.0	10.600	0.9187	0.1605	-0.0211	-0.0007	-0.0005
04T- 43	38	8	0.800	0.0	12.782	1.0005	0.2204	-0.0085	0.0	0.0
04T- 43	38	9	0.797	0.0	14.974	1.0820	0.2891	0.0064	0.0017	-0.0005
04T- 43	38	10	0.798	0.0	17.127	1.1478	0.3548	0.0157	0.0008	0.0003
04T- 43	41	1	0.700	0.0	-0.972	0.0593	0.0280	-0.0630	0.0007	-0.0024

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	41	2	0.698	0.0	3.608	0.4170	0.0384	-0.0488	0.0003	-0.0013
04T- 43	41	3	0.698	0.0	8.163	0.7509	0.0901	-0.0270	0.0001	-0.0007
04T- 43	41	4	0.698	0.0	12.574	0.9727	0.2017	0.0064	-0.0011	0.0005
04T- 43	41	5	0.698	0.0	12.584	0.9762	0.2022	0.0087	-0.0019	0.0008
04T- 43	41	6	0.697	0.0	22.013	1.2738	0.5131	0.0526	0.0034	-0.0018
04T- 43	42	1	0.700	0.0	-0.969	0.0551	0.0283	-0.0549	0.0003	-0.0022
04T- 43	42	2	0.700	0.0	-3.262	-0.1295	0.0404	-0.0543	-0.0001	-0.0029
04T- 43	42	3	0.699	0.1	~~-2.563~~	~~-2.2809~~	~~0.0900~~	~~-0.0253~~	~~-0.0007~~	~~-0.0052~~
04T- 43	42	4	0.697	0.0	3.610	0.4149	0.0385	-0.0428	-0.0001	-0.0012
04T- 43	42	5	0.697	0.0	5.905	0.5889	0.0584	-0.0348	-0.0	-0.0009
04T- 43	42	6	0.697	0.0	8.145	0.7490	0.0901	-0.0211	-0.0003	-0.0006
04T- 43	42	7	0.697	0.0	10.409	0.8794	0.1401	-0.0026	0.0004	-0.0002
04T- 43	42	8	0.698	0.0	12.570	0.9670	0.2006	0.0146	0.0008	0.0002
04T- 43	42	9	0.700	0.0	14.794	1.0519	0.2673	0.0313	0.0004	0.0007
04T- 43	42	11	0.697	0.0	16.890	1.1302	0.3351	0.0440	0.0009	0.0012
04T- 43	42	12	0.700	0.0	19.050	1.1923	0.4075	0.0495	0.0021	-0.0005
04T- 43	42	13	0.701	0.0	21.194	1.2444	0.4801	0.0550	0.0035	-0.0024
04T- 43	43	1	1.200	0.0	-1.116	-0.0223	0.0593	-0.0486	-0.0004	-0.0026
04T- 43	43	2	1.204	0.0	-3.507	-0.2009	0.0723	-0.0213	-0.0003	-0.0029
04T- 43	43	3	1.205	0.0	1.276	0.1678	0.0600	-0.0773	-0.0009	-0.0026
04T- 43	43	4	1.204	0.0	3.680	0.3697	0.0755	-0.1094	-0.0011	-0.0027
04T- 43	43	5	1.201	0.0	6.029	0.5243	0.1029	-0.1314	-0.0011	-0.0025
04T- 43	43	6	1.203	0.0	8.523	0.7682	0.1571	-0.1545	-0.0011	-0.0020
04T- 43	43	7	1.206	0.0	10.900	0.9314	0.2163	-0.1672	-0.0010	-0.0017
04T- 43	43	8	1.204	0.0	13.278	1.0853	0.2893	-0.1747	-0.0012	-0.0016
04T- 43	43	9	1.203	0.0	15.484	1.2021	0.3645	-0.1850	-0.0011	-0.0015
04T- 43	43	10	1.201	0.0	6.112	0.5827	0.1078	-0.1384	-0.0014	-0.0023
04T- 43	46	1	0.904	0.0	-1.013	0.0477	0.0473	-0.0834	0.0012	-0.0029
04T- 43	46	2	0.903	0.0	3.770	0.4611	0.0668	-0.0978	0.0018	-0.0025
04T- 43	46	3	0.902	0.0	6.119	0.6466	0.0965	-0.1024	0.0012	-0.0026
04T- 43	46	4	0.904	0.0	8.432	0.8064	0.1362	-0.0983	0.0014	-0.0025
04T- 43	46	5	0.899	0.0	12.998	1.0775	0.2465	-0.0693	0.0038	-0.0032
04T- 43	46	6	0.901	0.0	15.950	1.2078	0.3401	-0.0512	0.0015	-0.0006
04T- 43	47	1	0.898	0.0	-1.010	0.0483	0.0481	-0.0823	0.0010	-0.0025
04T- 43	47	2	0.901	0.0	-3.367	-0.1461	0.0618	-0.0709	0.0010	-0.0031
04T- 43	47	3	0.903	0.0	1.370	0.2458	0.0483	-0.0810	0.0017	-0.0020
04T- 43	47	4	0.902	0.0	3.764	0.4625	0.0667	-0.0944	0.0015	-0.0020
04T- 43	47	5	0.899	0.0	6.108	0.6422	0.0948	-0.0943	0.0009	-0.0019
04T- 43	47	6	0.915	0.0	8.432	0.8026	0.1359	-0.0972	0.0019	-0.0019
04T- 43	47	7	0.906	0.0	10.720	0.9407	0.1824	-0.0800	0.0034	-0.0020
04T- 43	47	8	0.898	0.0	12.954	1.0530	0.2401	-0.0586	0.0008	-0.0011
04T- 43	47	9	0.903	0.0	15.218	1.1628	0.3116	-0.0505	0.0001	-0.0004
04T- 43	48	1	0.798	0.0	-1.012	0.0330	0.0399	-0.0616	0.0001	-0.0021
04T- 43	48	2	0.796	0.0	-3.325	-0.1407	0.0541	-0.0609	0.0006	-0.0030
04T- 43	48	3	0.798	0.0	1.347	0.2395	0.0374	-0.0636	0.0011	-0.0016

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	48	4	0.796	0.0	3.687	0.4368	0.0481	-0.0624	0.0013	-0.0014
04T- 43	48	5	0.796	0.0	5.895	0.5452	0.0680	-0.0579	0.0011	-0.0015
04T- 43	48	6	0.798	0.0	8.274	0.7547	0.1065	-0.0434	0.0005	-0.0011
04T- 43	48	7	0.799	0.0	10.591	0.9087	0.1528	-0.0297	0.0004	-0.0006
04T- 43	48	8	0.799	0.0	12.837	1.0364	0.2133	-0.0120	0.0009	-0.0003
04T- 43	48	9	0.801	0.0	15.030	1.1061	0.2759	0.0110	0.0005	0.0001
04T- 43	49	1	0.700	0.0	-1.012	0.0278	0.0369	-0.0545	0.0004	-0.0019
04T- 43	49	2	0.700	0.0	-3.281	-0.1401	0.0508	-0.0555	0.0005	-0.0027
04T- 43	49	3	0.699	0.0	1.282	0.2198	0.0332	-0.0544	0.0010	-0.0014
04T- 43	49	4	0.701	0.0	3.582	0.3989	0.0400	-0.0498	0.0006	-0.0012
04T- 43	49	5	0.697	0.0	5.734	0.5082	0.0566	-0.0549	0.0007	-0.0011
04T- 43	49	6	0.698	0.0	8.142	0.7256	0.0890	-0.0343	0.0004	-0.0008
04T- 43	49	7	0.699	0.0	10.437	0.8822	0.1305	-0.0177	0.0010	-0.0005
04T- 43	49	8	0.700	0.0	12.590	0.9924	0.1835	0.0010	0.0007	-0.0001
04T- 43	49	9	0.700	0.0	14.718	1.0649	0.2494	0.0212	0.0010	0.0005
04T- 43	49	10	0.699	0.0	16.941	1.1341	0.3234	0.0319	-0.0	0.0021
04T- 43	49	11	0.700	0.0	19.119	1.2028	0.3989	0.0424	0.0008	0.0009
04T- 43	50	1	1.202	0.0	-1.176	-0.0498	0.0732	-0.0488	0.0003	-0.0024
04T- 43	50	2	1.204	0.0	-3.554	-0.2244	0.0869	-0.0173	0.0002	-0.0039
04T- 43	50	3	1.204	0.0	1.219	0.1382	0.0721	-0.0796	0.0002	-0.0017
04T- 43	50	4	1.204	0.0	3.546	0.3204	0.0838	-0.1081	0.0003	-0.0018
04T- 43	50	5	1.204	0.0	6.025	0.5294	0.1110	-0.1364	0.0001	-0.0016
04T- 43	50	6	1.203	0.0	8.396	0.7248	0.1534	-0.1568	-0.0	-0.0013
04T- 43	50	7	1.202	0.0	10.850	0.8965	0.2099	-0.1658	0.0	-0.0013
04T- 43	50	8	1.204	0.0	13.172	1.0437	0.2741	-0.1716	-0.0004	-0.0010
04T- 43	50	9	1.205	0.0	14.957	1.1491	0.3324	-0.1798	-0.0002	-0.0011
04T- 43	50	10	1.205	0.0	10.811	0.8907	0.2073	-0.1651	-0.0	-0.0012
04T- 43	50	11	1.207	0.0	4.961	0.5097	0.0995	-0.1332	-0.0	-0.0015
04T- 43	50	12	1.207	0.0	4.787	0.4240	0.0940	-0.1217	-0.0	-0.0017
04T- 43	53	1	0.904	0.0	-1.052	0.0225	0.0609	-0.0775	0.0007	-0.0025
04T- 43	53	2	0.897	0.0	3.596	0.3702	0.0698	-0.0787	0.0015	-0.0020
04T- 43	53	3	0.902	0.0	5.980	0.5777	0.0975	-0.0973	0.0024	-0.0022
04T- 43	53	4	0.896	0.0	8.308	0.7528	0.1344	-0.0989	0.0009	-0.0022
04T- 43	53	5	0.901	0.0	12.913	1.0331	0.2353	-0.0736	0.0021	-0.0022
04T- 43	53	6	0.900	0.0	16.055	1.1841	0.3259	-0.0592	0.0024	-0.0034
04T- 43	54	1	0.897	0.0	~~-4.544~~	~~-2.6859~~	~~0.2129~~	~~-0.0146~~	~~0.0010~~	~~-0.0054~~
04T- 43	54	2	0.903	0.0	-3.351	-0.1431	0.0734	-0.0701	0.0004	-0.0028
04T- 43	54	3	0.895	0.0	1.298	0.1853	0.0582	-0.0695	0.0001	-0.0016
04T- 43	54	4	0.898	0.0	3.667	0.3821	0.0719	-0.0818	0.0014	-0.0018
04T- 43	54	5	0.900	0.0	6.021	0.5867	0.0986	-0.0968	0.0020	-0.0020
04T- 43	54	6	0.901	0.0	8.382	0.7636	0.1372	-0.1025	0.0020	-0.0020
04T- 43	54	7	0.898	0.0	10.659	0.9149	0.1842	-0.0937	0.0011	-0.0017
04T- 43	54	8	0.903	0.0	12.925	1.0327	0.2356	-0.0725	0.0020	-0.0020
04T- 43	54	9	0.901	0.0	15.159	1.1367	0.2964	-0.0585	0.0022	-0.0026
04T- 43	54	10	0.901	0.0	17.423	1.2374	0.3698	-0.0543	0.0016	-0.0025

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	55	1	0.799	0.0	-1.038	0.0194	0.0512	-0.0641	0.0002	-0.0017
04T- 43	55	2	0.800	0.0	-3.345	-0.1466	0.0653	-0.0584	0.0005	-0.0025
04T- 43	55	3	0.800	0.0	1.284	0.2028	0.0467	-0.0640	0.0013	-0.0012
04T- 43	55	4	0.801	0.0	3.630	0.3870	0.0549	-0.0632	0.0032	-0.0013
04T- 43	55	5	0.803	0.0	5.929	0.5590	0.0765	-0.0610	0.0031	-0.0013
04T- 43	55	6	0.802	0.0	8.208	0.7047	0.1081	-0.0537	0.0020	-0.0012
04T- 43	55	7	0.799	0.0	10.445	0.8442	0.1487	-0.0392	0.0024	-0.0010
04T- 43	55	8	0.800	0.0	12.737	0.9854	0.1983	-0.0206	0.0018	-0.0007
04T- 43	55	9	0.800	0.0	15.017	1.1183	0.2638	-0.0058	0.0017	-0.0004
04T- 43	55	10	0.801	0.0	17.147	1.1915	0.3321	-0.0178	0.0002	-0.0003
04T- 43	55	11	0.797	0.0	18.818	1.2269	0.3881	0.0038	0.0024	-0.0008
04T- 43	56	1	0.700	0.0	-1.044	0.0079	0.0469	-0.0558	0.0004	-0.0017
04T- 43	56	2	0.700	0.0	-3.285	-0.1498	0.0622	-0.0542	0.0003	-0.0027
04T- 43	56	3	0.699	0.0	1.226	0.1839	0.0403	-0.0555	0.0005	-0.0014
04T- 43	56	4	0.700	0.0	3.553	0.3708	0.0444	-0.0554	0.0017	-0.0011
04T- 43	56	5	0.698	0.0	5.814	0.5482	0.0612	-0.0516	0.0017	-0.0007
04T- 43	56	6	0.699	0.0	8.103	0.7018	0.0911	-0.0425	0.0026	-0.0010
04T- 43	56	7	0.700	0.0	10.304	0.8348	0.1290	-0.0306	0.0011	-0.0007
04T- 43	56	8	0.699	0.0	12.585	0.9729	0.1767	-0.0144	0.0020	-0.0007
04T- 43	56	9	0.696	0.0	14.752	1.0990	0.2345	0.0003	0.0003	-0.0006
04T- 43	56	10	0.697	0.0	16.939	1.1729	0.3082	0.0096	-0.0008	0.0002
04T- 43	56	11	0.698	0.0	19.092	1.2233	0.3853	0.0335	0.0014	-0.0001
04T- 43	57	1	1.205	0.0	-1.225	-0.0746	0.0662	-0.0447	0.0004	-0.0026
04T- 43	57	2	1.204	0.0	-3.584	-0.2396	0.1017	-0.0161	0.0	-0.0022
04T- 43	57	3	1.206	0.0	1.180	0.1037	0.0863	-0.0763	0.0004	-0.0022
04T- 43	57	4	1.207	0.0	3.457	0.2746	0.0948	-0.1029	0.0007	-0.0021
04T- 43	57	5	1.203	0.0	5.887	0.4694	0.1161	-0.1284	0.0008	-0.0019
04T- 43	57	6	1.204	0.0	8.309	0.6676	0.1537	-0.1529	0.0009	-0.0016
04T- 43	57	7	1.205	0.0	10.726	0.8493	0.2049	-0.1694	0.0002	-0.0015
04T- 43	57	8	1.204	0.0	13.035	0.9984	0.2646	-0.1712	0.0006	-0.0018
04T- 43	57	9	1.204	0.0	15.404	1.1388	0.3373	-0.1785	0.0004	-0.0019
04T- 43	60	1	0.900	0.0	-0.908	0.1090	0.0282	-0.0914	0.0002	-0.0025
04T- 43	60	2	0.904	0.0	3.919	0.0109	0.0731	-0.0827	-0.0010	-0.0023
04T- 43	60	3	0.903	0.0	6.300	0.7398	0.1034	-0.0917	-0.0005	-0.0020
04T- 43	60	4	0.903	0.0	8.639	0.9011	0.1580	-0.0920	0.0004	-0.0017
04T- 43	60	5	0.899	0.0	13.037	1.0712	0.2740	-0.0602	0.0010	-0.0019
04T- 43	60	6	0.901	0.0	15.463	1.1424	0.3450	-0.0391	0.0014	-0.0017
04T- 43	61	1	0.901	0.0	-0.905	0.1111	0.0284	-0.0916	0.0002	-0.0024
04T- 43	61	2	0.903	0.0	-3.359	-0.1369	0.0403	-0.0854	0.0008	-0.0031
04T- 43	61	3	0.900	0.0	1.539	0.3277	0.0369	-0.0825	0.0001	-0.0021
04T- 43	61	4	0.901	0.0	3.915	0.5350	0.0606	-0.0818	-0.0010	-0.0021
04T- 43	61	5	0.899	0.0	6.295	0.7379	0.1030	-0.0881	-0.0007	-0.0018
04T- 43	61	6	0.902	0.0	8.616	0.9024	0.1583	-0.0923	0.0004	-0.0015
04T- 43	61	7	0.898	0.0	10.785	0.9566	0.2047	-0.0661	0.0025	-0.0019
04T- 43	61	8	0.893	0.0	12.969	1.0489	0.2674	-0.0497	0.0045	-0.0026
04T- 43	61	9	0.900	0.0	15.196	1.1267	0.3346	-0.0385	0.0014	-0.0014

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	62	1	0.801	0.0	-0.911	0.0962	0.0242	-0.0689	0.0004	-0.0021
04T- 43	62	2	0.800	0.0	-3.282	-0.1137	0.0333	-0.0719	0.0006	-0.0025
04T- 43	62	3	0.799	0.0	1.425	0.2830	0.0300	-0.0600	0.0003	-0.0015
04T- 43	62	4	0.798	0.0	3.787	0.4740	0.0461	-0.0516	0.0003	-0.0014
04T- 43	62	5	0.802	0.0	6.150	0.6607	0.0782	-0.0386	-0.0	-0.0011
04T- 43	62	6	0.799	0.0	8.397	0.7962	0.1240	-0.0245	0.0004	-0.0007
04T- 43	62	7	0.802	0.0	10.615	0.8966	0.1799	-0.0149	0.0009	-0.0006
04T- 43	62	8	0.801	0.0	12.789	0.9770	0.2360	0.0008	0.0010	-0.0004
04T- 43	62	9	0.800	0.0	14.928	1.0368	0.2933	0.0161	0.0007	-0.0001
04T- 43	62	10	0.800	0.0	17.098	1.1172	0.3615	0.0286	0.0008	-0.0001
04T- 43	63	1	0.698	0.0	-0.928	0.0855	0.0255	-0.0600	0.0002	-0.0021
04T- 43	63	2	0.700	0.0	-3.243	-0.1025	0.0299	-0.0667	0.0006	-0.0031
04T- 43	63	3	0.702	0.0	1.335	0.2555	0.0275	-0.0501	0.0001	-0.0014
04T- 43	63	4	0.699	0.0	3.609	0.4240	0.0537	-0.0413	0.0003	-0.0012
04T- 43	63	5	0.697	0.0	5.936	0.5978	0.0668	-0.0293	0.0004	-0.0010
04T- 43	63	6	0.698	0.0	8.184	0.7461	0.1080	-0.0151	0.0006	-0.0006
04T- 43	63	7	0.698	0.0	10.362	0.8403	0.1584	0.0031	-0.0011	-0.0001
04T- 43	63	8	0.699	0.0	12.545	0.9253	0.2129	0.0233	-0.0039	0.0013
04T- 43	63	9	0.698	0.0	14.701	1.0038	0.2721	0.0360	-0.0010	0.0010
04T- 43	63	10	0.700	0.0	16.867	1.0714	0.3352	0.0486	0.0012	0.0008
04T- 43	63	11	0.699	0.0	18.971	1.1369	0.4044	0.0519	0.0026	-0.0026
04T- 43	63	12	0.698	0.0	21.119	1.2110	0.4838	0.0473	0.0026	-0.0026
04T- 43	64	1	1.204	0.0	-1.055	0.0071	0.0499	-0.0507	0.0001	-0.0025
04T- 43	64	2	1.205	0.0	-3.415	-0.1744	0.0603	-0.0262	0.0004	-0.0024
04T- 43	64	3	1.206	0.0	1.387	0.2161	0.0542	-0.0815	-0.0011	-0.0026
04T- 43	64	4	1.205	0.0	3.748	0.4144	0.0743	-0.1103	-0.0011	-0.0024
04T- 43	64	5	1.204	0.0	6.182	0.6202	0.1131	-0.1412	-0.0008	-0.0020
04T- 43	64	6	1.207	0.0	8.610	0.8050	0.1667	-0.1625	-0.0006	-0.0016
04T- 43	64	7	1.203	0.0	10.956	0.9680	0.2315	-0.1759	-0.0004	-0.0017
04T- 43	64	8	1.204	0.0	13.284	1.1125	0.3065	-0.1903	-0.0004	-0.0017
04T- 43	67	1	0.900	0.0	-0.955	0.0830	0.0324	-0.0895	0.0025	-0.0021
04T- 43	67	2	0.902	0.0	3.860	0.5118	0.0617	-0.0911	0.0026	-0.0015
04T- 43	67	3	0.901	0.0	6.231	0.6993	0.0973	-0.0915	0.0041	-0.0026
04T- 43	67	4	0.904	0.0	8.563	0.8845	0.1508	-0.1003	0.0018	-0.0031
04T- 43	67	5	0.901	0.0	13.062	1.0925	0.2721	-0.0679	-0.0011	-0.0019
04T- 43	68	1	0.902	0.0	-0.961	0.0795	0.0325	-0.0893	0.0025	-0.0012
04T- 43	68	2	0.901	0.0	-3.384	-0.1482	0.0459	-0.0814	-0.0013	-0.0025
04T- 43	68	3	0.901	0.0	1.467	0.3037	0.0382	-0.0876	0.0018	-0.0018
04T- 43	68	4	0.900	0.0	3.849	0.5061	0.0602	-0.0880	0.0023	-0.0018
04T- 43	68	5	0.899	0.0	6.235	0.7033	0.0979	-0.0916	0.0040	-0.0024
04T- 43	68	6	0.902	0.0	8.567	0.8750	0.1495	-0.0947	0.0018	-0.0028
04T- 43	68	7	0.902	0.0	10.825	0.9725	0.2032	-0.0756	0.0002	-0.0025
04T- 43	68	8	0.905	0.0	13.050	1.0862	0.2704	-0.0660	-0.0040	-0.0008
04T- 43	68	9	0.899	0.0	15.169	1.1258	0.3279	-0.0415	-0.0022	-0.0006
04T- 43	71	1	0.857	0.0	-1.008	0.0513	0.0467	-0.0851	0.0005	-0.0030

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
C4T- 43	71	2	C.903	C.C	3.762	C.4651	0.0699	-0.1004	0.0003	-C.0026
04T- 43	71	3	C.897	C.0	6.129	0.6497	0.0962	-0.1015	0.0004	-0.0024
04T- 43	71	4	C.898	C.0	8.434	C.8080	0.1359	-0.0966	-0.0002	-C.002C
04T- 43	71	5	C.902	C.0	12.985	1.0714	0.2486	-0.0698	-0.0019	-C.0004
04T- 43	71	6	C.904	C.0	15.136	1.1709	0.3161	-0.0605	-0.0007	-C.0002
C4T- 43	72	1	C.901	C.0	-1.C09	C.0512	0.0476	-0.0857	0.0001	-0.0027
04T- 43	72	2	C.898	C.0	-3.337	-0.1357	0.0601	-0.0792	0.0011	-0.0031
04T- 43	72	3	C.902	C.0	1.361	0.2526	0.0494	-0.0888	-0.0008	-0.0024
04T- 43	72	4	C.899	C.0	3.760	0.4643	0.0660	-0.0979	-0.0004	-C.0023
04T- 43	72	5	C.900	C.C	6.102	C.6504	0.0962	-0.1034	0.0006	-0.0023
04T- 43	72	6	C.901	C.0	8.421	C.8123	0.1367	-0.0997	0.0011	-0.0022
04T- 43	72	7	C.901	C.0	1C.762	C.9617	0.1882	-0.0875	0.0C14	-C.0020
04T- 43	72	8	C.902	C.0	12.978	1.0548	0.2446	-0.0661	-0.0012	-0.0005
04T- 43	72	9	C.9C2	C.C	15.252	1.1699	0.3184	-0.0584	0.0009	-0.0C15
04T- 43	73	1	C.8C0	C.0	-1.011	0.0397	0.0398	-0.0703	0.0003	-C.0023
04T- 43	73	2	C.801	0.0	-3.3C8	-0.1355	0.0529	-0.0690	0.0004	-0.0028
04T- 43	73	3	C.8C1	C.0	1.397	C.2507	0.0376	-0.0723	0.0001	-0.0018
04T- 43	73	4	C.8C0	C.0	3.734	C.4401	0.0489	-0.0685	0.0006	-0.0018
04T- 43	73	5	C.802	C.0	6.C01	C.6079	0.0735	-0.0610	-0.0001	-0.0016
04T- 43	73	6	C.799	C.0	8.324	0.7622	0.1084	-0.0481	-0.0003	-0.0013
04T- 43	73	7	C.802	C.0	10.606	C.9108	0.1564	-0.0344	-0.0001	-C.001C
04T- 43	73	8	C.802	C.0	12.832	1.0278	0.2165	-0.0152	-0.0008	-C.0002
04T- 43	73	9	C.798	C.0	14.997	1.0965	0.2803	0.0045	0.0003	-0.0003
04T- 43	73	10	C.799	C.0	17.153	1.1647	0.3513	0.0061	0.0002	0.0
04T- 43	74	1	C.701	C.0	-1.CC7	C.0368	0.0367	-0.0638	0.0002	-C.0022
04T- 43	74	2	C.699	C.0	-3.286	-0.1366	0.0501	-0.0651	0.0005	-0.0030
04T- 43	74	3	C.700	C.0	1.296	C.2271	0.0333	-0.0631	-0.0003	-0.0018
04T- 43	74	4	C.700	C.0	3.579	0.4018	0.0407	-0.0578	-0.0001	-0.0C15
04T- 43	74	5	C.700	C.0	5.842	0.5696	0.0600	-0.0495	0.0005	-C.0013
04T- 43	74	6	C.698	C.0	8.159	0.7304	0.0910	-0.0365	0.0001	-C.0010
04T- 43	74	7	C.698	C.0	1C.367	0.8720	0.1325	-0.0212	-0.0008	-0.0008
04T- 43	74	8	C.699	C.0	12.584	0.9846	0.1902	-0.0036	-0.0004	-C.0C06
04T- 43	74	9	C.699	0.0	14.775	1.0661	0.2589	C.0165	-0.0004	-0.0
04T- 43	74	1C	C.697	C.0	16.926	1.1421	0.3280	0.0296	-0.0003	C.0018
04T- 43	74	11	C.699	C.0	19.083	1.2036	0.4017	0.0350	0.0013	-0.0002
04T- 43	77	1	C.899	C.0	-C.985	0.0610	0.0429	-0.0807	-0.0003	-0.005C
04T- 43	77	2	C.899	C.0	3.793	0.4771	0.0635	-0.0908	-0.0036	-0.CC28
04T- 43	77	3	C.897	C.0	6.144	C.6630	0.0950	-C.0942	-0.0037	-0.0027
C4T- 43	77	4	C.900	C.0	8.481	C.8343	0.1392	-0.0943	-0.0038	-0.0014
04T- 43	77	5	C.899	C.0	12.986	1.0613	0.2487	-0.0557	-0.0011	C.0C04
C4T- 43	77	6	C.899	C.0	15.658	1.1795	0.3343	-0.0460	0.0091	-0.0050
04T- 43	78	1	C.894	C.0	-0.978	0.0634	0.0424	-0.0788	-0.0003	-0.0038
C4T- 43	78	2	C.897	C.0	-3.346	-0.1349	0.0564	-0.0722	0.0019	-0.0C44
C4T- 43	78	3	C.895	C.0	1.414	0.2729	0.0453	-C.0818	-0.0045	-0.0C32
04T- 43	78	4	C.887	C.0	3.792	C.4756	0.0607	-0.0820	-0.0031	-C.0026

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	78	5	0.899	0.0	6.157	0.6664	0.0957	-0.0920	-0.0032	-0.0023
04T- 43	78	6	0.896	0.0	8.465	0.8242	0.1363	-0.0830	-0.0028	-0.0011
04T- 43	78	7	0.898	0.0	10.755	0.9610	0.1888	-0.0715	0.0001	-0.0007
04T- 43	78	8	0.896	0.0	12.990	1.0632	0.2478	-0.0520	-0.0014	0.0009
04T- 43	78	9	0.896	0.0	15.215	1.1586	0.3186	-0.0404	0.0049	0.0009
04T- 43	79	1	0.800	0.0	-0.980	0.0501	0.0369	-0.0592	-0.0014	-0.0042
04T- 43	79	2	0.801	0.0	-3.299	-0.1313	0.0500	-0.0580	0.0010	-0.0043
04T- 43	79	3	0.801	0.0	1.380	0.2548	0.0355	-0.0596	-0.0021	-0.0031
04T- 43	79	4	0.798	0.0	3.723	0.4508	0.0475	-0.0561	-0.0010	-0.0024
04T- 43	79	5	0.802	0.0	6.055	0.6239	0.0732	-0.0474	-0.0032	-0.0023
04T- 43	79	6	0.795	0.0	8.316	0.7734	0.1079	-0.0337	-0.0043	-0.0014
04T- 43	79	7	0.799	0.0	10.601	0.9174	0.1587	-0.0192	0.0002	-0.0002
04T- 43	79	8	0.801	0.0	12.824	1.0189	0.2180	-0.0010	0.0065	-0.0004
04T- 43	79	9	0.800	0.0	14.987	1.0930	0.2882	0.0129	0.0059	-0.0015
04T- 43	79	10	0.800	0.0	17.128	1.1547	0.3514	0.0142	0.0031	-0.0016
04T- 43	80	1	0.697	0.0	-0.980	0.0450	0.0341	-0.0499	-0.0016	-0.0039
04T- 43	80	2	0.700	0.0	-3.258	-0.1281	0.0467	-0.0511	0.0005	-0.0044
04T- 43	80	3	0.699	0.0	1.323	0.2347	0.0317	-0.0479	-0.0019	-0.0033
04T- 43	80	4	0.699	0.0	3.608	0.4110	0.0403	-0.0417	-0.0010	-0.0022
04T- 43	80	5	0.701	0.0	5.892	0.5820	0.0601	-0.0340	-0.0008	-0.0018
04T- 43	80	6	0.700	0.0	8.163	0.7439	0.0915	-0.0207	-0.0009	-0.0013
04T- 43	80	7	0.701	0.0	10.399	0.8746	0.1358	-0.0030	0.0027	-0.0006
04T- 43	80	8	0.701	0.0	12.597	0.9738	0.1936	0.0154	0.0069	-0.0001
04T- 43	80	9	0.700	0.0	14.765	1.0589	0.2622	0.0318	0.0026	-0.0006
04T- 43	80	10	0.699	0.0	16.907	1.1259	0.3290	0.0444	0.0022	-0.0008
04T- 43	80	11	0.700	0.0	19.047	1.1891	0.4015	0.0527	0.0028	-0.0022
04T- 43	80	12	0.700	0.0	21.194	1.2537	0.4781	0.0580	0.0046	-0.0046
04T- 43	81	1	1.199	0.0	-1.150	-0.0407	0.0691	-0.0448	-0.0023	-0.0059
04T- 43	81	2	1.203	0.0	-3.504	-0.2177	0.0827	-0.0135	-0.0013	-0.0050
04T- 43	81	3	1.202	0.0	1.219	0.1518	0.0691	-0.0791	-0.0035	-0.0048
04T- 43	81	4	1.204	0.0	3.632	0.3522	0.0828	-0.1116	-0.0054	-0.0042
04T- 43	81	5	1.204	0.0	6.062	0.5626	0.1125	-0.1392	-0.0059	-0.0034
04T- 43	81	6	1.202	0.0	8.483	0.7594	0.1585	-0.1581	-0.0043	-0.0027
04T- 43	81	7	1.203	0.0	10.859	0.9250	0.2160	-0.1667	-0.0043	-0.0016
04T- 43	81	8	1.204	0.0	13.212	1.0766	0.2858	-0.1737	-0.0039	-0.0010
04T- 43	81	9	1.204	0.0	14.624	1.1606	0.3333	-0.1794	-0.0034	-0.0010
04T- 43	84	1	0.896	0.0	-0.977	0.0673	0.0452	-0.0842	-0.0042	-0.0061
04T- 43	84	2	0.900	0.0	3.775	0.4619	0.0663	-0.0838	-0.0158	-0.0038
04T- 43	84	3	0.899	0.0	6.148	0.6631	0.1011	-0.0943	-0.0137	-0.0021
04T- 43	84	4	0.896	0.0	8.450	0.8153	0.1428	-0.0880	-0.0125	0.0004
04T- 43	84	5	0.897	0.0	12.927	1.0312	0.2484	-0.0579	0.0017	0.0016
04T- 43	84	6	0.898	0.0	15.863	1.1564	0.3372	-0.0490	0.0065	-0.0017
04T- 43	85	1	0.899	0.0	-0.979	0.0657	0.0455	-0.0833	-0.0044	-0.0060
04T- 43	85	2	0.897	0.0	-3.345	-0.1300	0.0578	-0.0777	0.0043	-0.0056
04T- 43	85	3	0.900	0.0	1.396	0.2595	0.0489	-0.0774	-0.0130	-0.0053

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	85	4	0.895	0.0	3.777	0.4642	0.0658	-0.0819	-0.0156	0.0038
04T- 43	85	5	0.897	0.0	6.152	0.6630	0.1000	-0.0916	-0.0134	-0.0019
04T- 43	85	6	0.898	0.0	8.467	0.8278	0.1455	-0.0931	-0.0119	0.0003
04T- 43	85	7	0.897	0.0	10.724	0.9555	0.1979	-0.0811	-0.0056	0.0013
04T- 43	85	8	0.898	0.0	12.922	1.0321	0.2489	-0.0565	0.0022	0.0012
04T- 43	85	9	0.898	0.0	15.164	1.1351	0.3171	-0.0507	0.0061	-0.0013
04T- 43	86	1	0.601	0.0	-0.980	0.0573	0.0386	-0.0675	-0.0025	-0.0045
04T- 43	86	2	0.799	0.0	-3.309	-0.1278	0.0511	-0.0656	0.0023	-0.0045
04T- 43	86	3	0.801	0.0	1.367	0.2502	0.0391	-0.0636	-0.0058	-0.0034
04T- 43	86	4	0.802	0.0	3.697	0.4362	0.0519	-0.0598	-0.0074	-0.0024
04T- 43	86	5	0.801	0.0	6.028	0.6125	0.0775	-0.0518	-0.0107	-0.0011
04T- 43	86	6	0.801	0.0	8.291	0.7576	0.1166	-0.0413	-0.0088	0.0009
04T- 43	86	7	0.800	0.0	10.500	0.8718	0.1628	-0.0277	-0.0028	0.0028
04T- 43	86	8	0.799	0.0	12.747	0.9869	0.2187	-0.0148	0.0061	0.0026
04T- 43	86	9	0.801	0.0	14.951	1.0765	0.2795	0.0033	0.0134	-0.0008
04T- 43	86	10	0.802	0.0	17.117	1.1514	0.3476	0.0057	0.0139	-0.0026
04T- 43	86	11	0.801	0.0	19.223	1.1934	0.4174	0.0008	0.0125	-0.0093
04T- 43	87	1	0.700	0.0	-0.987	0.0479	0.0359	-0.0608	-0.0033	-0.0044
04T- 43	87	2	0.699	0.0	-3.289	-0.1298	0.0486	-0.0612	0.0010	-0.0052
04T- 43	87	3	0.700	0.0	1.328	0.2302	0.0349	-0.0553	-0.0052	-0.0029
04T- 43	87	4	0.701	0.0	3.593	0.4053	0.0431	-0.0509	-0.0041	-0.0015
04T- 43	87	5	0.699	0.0	5.894	0.5824	0.0640	-0.0424	-0.0039	-0.0003
04T- 43	87	6	0.700	0.0	8.134	0.7293	0.0994	-0.0305	-0.0011	0.0014
04T- 43	87	7	0.700	0.0	10.339	0.8467	0.1450	-0.0180	0.0028	0.0031
04T- 43	87	8	0.699	0.0	12.549	0.9636	0.1974	-0.0006	0.0102	0.0037
04T- 43	87	9	0.701	0.0	14.726	1.0532	0.2562	0.0178	0.0160	0.0016
04T- 43	87	10	0.699	0.0	16.855	1.1111	0.3213	0.0333	0.0145	-0.0015
04T- 43	87	11	0.700	0.0	18.977	1.1571	0.3898	0.0305	0.0138	-0.0076
04T- 43	87	12	0.702	0.0	21.119	1.2311	0.4691	0.0303	0.0136	-0.0103
04T- 43	88	1	1.204	0.0	-1.154	-0.0398	0.0714	-0.0488	-0.0049	-0.0061
04T- 43	88	2	1.203	-0.0	-3.530	-0.2177	0.0846	-0.0188	-0.0021	-0.0058
04T- 43	88	3	1.200	0.0	1.257	0.1639	0.0727	-0.0860	-0.0084	-0.0064
04T- 43	88	4	1.203	0.0	3.653	0.3638	0.0877	-0.1156	-0.0138	-0.0053
04T- 43	88	5	1.202	0.0	6.066	0.5655	0.1185	-0.1432	-0.0153	-0.0034
04T- 43	88	6	1.204	0.0	8.480	0.7574	0.1642	-0.1648	-0.0131	-0.0010
04T- 43	88	7	1.204	0.0	10.859	0.9307	0.2228	-0.1793	-0.0107	0.0011
04T- 43	88	8	1.202	0.0	13.184	1.0787	0.2916	-0.1863	-0.0095	0.0031
04T- 43	88	9	1.204	0.0	14.815	1.1759	0.3469	-0.1977	-0.0085	0.0045
04T- 43	91	1	0.898	0.0	-0.990	0.0539	0.0433	-0.0750	0.0186	0.0038
04T- 43	91	2	0.897	0.0	3.855	0.4971	0.0663	-0.0873	0.0210	0.0022
04T- 43	91	3	0.899	0.0	6.208	0.6339	0.1002	-0.0907	0.0207	0.0006
04T- 43	91	4	0.898	0.0	8.539	0.8534	0.1454	-0.0873	0.0209	-0.0006
04T- 43	91	5	0.899	0.0	13.057	1.0847	0.2637	-0.0552	0.0165	-0.0030
04T- 43	91	6	0.899	0.0	16.134	1.1558	0.3531	-0.0349	0.0149	-0.0031
04T- 43	92	1	0.895	0.0	-0.993	0.0514	0.0437	-0.0736	0.0192	0.0039

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	92	2	0.895	0.0	-3.406	-0.1678	0.0591	-0.0616	0.0178	0.0020
04T- 43	92	3	0.902	0.0	1.434	0.2823	0.0468	-0.0630	0.0211	0.0044
04T- 43	92	4	0.898	0.0	3.810	0.4951	0.0661	-0.0879	0.0209	0.0023
04T- 43	92	5	0.902	0.0	6.191	0.6810	0.0998	-0.0901	0.0207	0.0007
04T- 43	92	6	0.898	0.0	8.534	0.8517	0.1449	-0.0847	0.0201	-0.0004
04T- 43	92	7	0.898	0.0	10.805	0.9827	0.2006	-0.0724	0.0189	-0.0019
04T- 43	92	8	0.901	0.0	13.029	1.0822	0.2624	-0.0549	0.0176	-0.0031
04T- 43	92	9	0.899	0.0	15.226	1.1371	0.3251	-0.0293	0.0155	-0.0031
04T- 43	95	1	0.900	0.0	-1.025	0.0325	0.0417	-0.0705	0.0191	-0.0005
04T- 43	95	2	0.902	0.0	3.836	0.4966	0.0657	-0.0888	0.0221	-0.0020
04T- 43	95	3	0.899	0.0	6.188	0.6782	0.0979	-0.0873	0.0202	-0.0030
04T- 43	95	4	0.896	0.0	8.513	0.8388	0.1414	-0.0789	0.0192	-0.0036
04T- 43	95	5	0.902	0.0	13.035	1.0835	0.2631	-0.0551	0.0148	-0.0048
04T- 43	95	6	0.898	0.0	16.476	1.1614	0.3636	-0.0396	0.0132	-0.0054
04T- 43	96	1	0.896	0.0	-1.019	0.0359	0.0413	-0.0705	0.0190	0.0003
04T- 43	96	2	0.898	0.0	-3.413	-0.1803	0.0559	-0.0577	0.0155	-0.0006
04T- 43	96	3	0.896	0.0	1.436	0.2779	0.0435	-0.0200	0.0228	-0.0
04T- 43	96	4	0.895	0.0	1.435	0.2780	0.0438	-0.0801	0.0228	-0.0
04T- 43	96	5	0.896	0.0	3.837	0.4919	0.0641	-0.0840	0.0223	-0.0017
04T- 43	96	6	0.898	0.0	6.189	0.6737	0.0969	-0.0834	0.0202	-0.0027
04T- 43	96	7	0.898	0.0	8.514	0.8362	0.1411	-0.0771	0.0196	-0.0035
04T- 43	96	8	0.897	0.0	10.738	0.9487	0.1927	-0.0600	0.0163	-0.0037
04T- 43	96	9	0.899	0.0	13.014	1.0615	0.2576	-0.0473	0.0150	-0.0042
04T- 43	96	10	0.894	0.0	15.178	1.1284	0.3210	-0.0283	0.0122	-0.0035
04T- 43	99	1	0.898	0.0	-0.999	0.0513	0.0397	-0.0776	0.0111	-0.0021
04T- 43	99	2	0.897	0.0	3.849	0.5062	0.0648	-0.0908	0.0156	-0.0036
04T- 43	99	3	0.897	0.0	6.205	0.6894	0.0981	-0.0914	0.0158	-0.0041
04T- 43	99	4	0.897	0.0	8.525	0.8621	0.1499	-0.0910	0.0145	-0.0043
04T- 43	99	5	0.897	0.0	13.035	1.0783	0.2601	-0.0538	0.0140	-0.0052
04T- 43	99	6	0.897	0.0	15.871	1.1665	0.3460	-0.0646	0.0117	-0.0054
04T- 43	100	1	0.898	0.0	-1.008	0.0455	0.0397	-0.0749	0.0102	-0.0016
04T- 43	100	2	0.894	0.0	-3.399	-0.1707	0.0530	-0.0608	0.0081	-0.0036
04T- 43	100	3	0.898	0.0	1.443	0.2908	0.0431	-0.0871	0.0169	-0.0021
04T- 43	100	4	0.900	0.0	3.846	0.5031	0.0646	-0.0895	0.0164	-0.0032
04T- 43	100	5	0.900	0.0	6.201	0.6910	0.0986	-0.0924	0.0154	-0.0038
04T- 43	100	6	0.899	0.0	8.499	0.8528	0.1430	-0.0867	0.0140	-0.0038
04T- 43	100	7	0.899	0.0	10.780	0.9694	0.1963	-0.0687	0.0123	-0.0039
04T- 43	100	8	0.899	0.0	13.020	1.0719	0.2586	-0.0529	0.0133	-0.0047
04T- 43	100	9	0.897	0.0	15.201	1.1356	0.3223	-0.0342	0.0125	-0.0051
04T- 43	103	1	0.898	0.0	-1.040	0.0250	0.0482	-0.0715	0.0065	-0.0021
04T- 43	103	2	0.900	0.0	3.752	0.4467	0.0674	-0.0894	0.0179	-0.0030
04T- 43	103	3	0.899	0.0	6.100	0.6393	0.0977	-0.0953	0.0162	-0.0038
04T- 43	103	4	0.899	0.0	8.405	0.7935	0.1357	-0.0882	0.0154	-0.0046
04T- 43	103	5	0.900	0.0	13.001	1.0707	0.2478	-0.0630	0.0132	-0.0051
04T- 43	103	6	0.900	0.0	15.935	1.1864	0.3364	-0.0405	0.0104	-0.0052

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	104	1	0.897	0.0	-1.034	0.0306	0.0494	-0.0750	0.0048	-0.0018
04T- 43	104	2	0.897	0.0	-3.396	-0.1686	0.0638	-0.0620	0.0057	-0.0021
04T- 43	104	3	0.899	0.0	1.348	0.2361	0.0504	-0.0805	0.0104	-0.0019
04T- 43	104	4	0.896	0.0	3.745	0.4528	0.0680	-0.0902	0.0171	-0.0028
04T- 43	104	5	0.897	0.0	6.097	0.6376	0.0969	-0.0922	0.0156	-0.0036
04T- 43	104	6	0.902	0.0	8.403	0.7919	0.1353	-0.0874	0.0150	-0.0042
04T- 43	104	7	0.892	0.0	10.690	0.9226	0.1797	-0.0663	0.0160	-0.0046
04T- 43	104	8	0.899	0.0	12.966	1.0560	0.2442	-0.0577	0.0158	-0.0056
04T- 43	104	9	0.897	0.0	15.204	1.1548	0.3118	-0.0451	0.0137	-0.0056
04T- 43	107	1	0.900	0.0	-1.050	0.0193	0.0510	-0.0712	0.0149	-0.0005
04T- 43	107	2	0.897	0.0	3.752	0.4431	0.0688	-0.0882	0.0242	-0.0013
04T- 43	107	3	0.898	0.0	6.074	0.6288	0.0970	-0.0910	0.0202	-0.0029
04T- 43	107	4	0.899	0.0	8.418	0.7928	0.1367	-0.0868	0.0159	-0.0036
04T- 43	107	5	0.896	0.0	12.976	1.0507	0.2446	-0.0570	0.0156	-0.0051
04T- 43	107	6	0.899	0.0	15.511	1.1854	0.3284	-0.0492	0.0146	-0.0062
04T- 43	108	1	0.898	0.0	-1.053	0.0174	0.0512	-0.0706	0.0150	-0.0001
04T- 43	108	2	0.899	0.0	-3.421	-0.1838	0.0662	-0.0565	0.0139	-0.0014
04T- 43	108	3	0.897	0.0	1.339	0.2280	0.0510	-0.0773	0.0195	0.0003
04T- 43	108	4	0.899	0.0	3.732	0.4420	0.0695	-0.0988	0.0243	-0.0011
04T- 43	108	5	0.899	0.0	6.098	0.6295	0.0970	-0.0892	0.0199	-0.0020
04T- 43	108	6	0.901	0.0	8.406	0.7912	0.1364	-0.0860	0.0159	-0.0033
04T- 43	108	7	0.899	0.0	10.695	0.9270	0.1833	-0.0714	0.0159	-0.0038
04T- 43	108	8	0.900	0.0	12.954	1.0454	0.2425	-0.0552	0.0154	-0.0044
04T- 43	108	9	0.896	0.0	15.221	1.1642	0.3157	-0.0438	0.0134	-0.0047
04T- 43	111	1	0.899	0.0	-1.028	0.0325	0.0547	-0.0733	0.0167	0.0027
04T- 43	111	2	0.897	0.0	3.752	0.4511	0.0712	-0.0913	0.0223	0.0027
04T- 43	111	3	0.898	0.0	6.085	0.6439	0.1008	-0.0968	0.0212	0.0004
04T- 43	111	4	0.898	0.0	8.418	0.7962	0.1385	-0.0871	0.0180	-0.0012
04T- 43	111	5	0.897	0.0	12.957	1.0476	0.2448	-0.0573	0.0160	-0.0036
04T- 43	111	6	0.901	0.0	15.577	1.1754	0.3291	-0.0478	0.0133	-0.0032
04T- 43	112	1	0.899	0.0	-1.030	0.0309	0.0549	-0.0726	0.0168	0.0036
04T- 43	112	2	0.902	0.0	-3.399	-0.1710	0.0697	-0.0584	0.0164	0.0010
04T- 43	112	3	0.899	0.0	1.352	0.2286	0.0546	-0.0766	0.0198	0.0047
04T- 43	112	4	0.898	0.0	3.741	0.4495	0.0714	-0.0908	0.0224	0.0029
04T- 43	112	5	0.900	0.0	6.105	0.6428	0.1010	-0.0967	0.0214	0.0004
04T- 43	112	6	0.897	0.0	8.412	0.7998	0.1590	-0.0884	0.0179	-0.0010
04T- 43	112	7	0.897	0.0	10.731	0.9449	0.1888	-0.0782	0.0170	-0.0025
04T- 43	112	8	0.899	0.0	12.982	1.0633	0.2496	-0.0636	0.0189	-0.0047
04T- 43	112	9	0.901	0.0	15.199	1.1504	0.3143	-0.0475	0.0131	-0.0021
04T- 43	113	1	0.801	0.0	-1.009	0.0374	0.0461	-0.0655	0.0207	0.0050
04T- 43	113	2	0.800	0.0	-3.313	-0.1363	0.0607	-0.0628	0.0191	0.0021
04T- 43	113	3	0.801	0.0	1.349	0.2379	0.0431	-0.0688	0.0225	0.0050
04T- 43	113	4	0.800	0.0	3.689	0.4370	0.0535	-0.0680	0.0211	0.0028
04T- 43	113	5	0.799	0.0	6.027	0.6125	0.0782	-0.0604	0.0202	0.0009
04T- 43	113	6	0.800	0.0	8.295	0.7645	0.1124	-0.0486	0.0193	-0.0006

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	113	7	0.801	0.0	10.603	0.8123	0.1599	-0.0355	0.0188	-0.0019
04T- 43	113	8	0.799	0.0	12.843	1.0255	0.2178	-0.0169	0.0153	-0.0031
04T- 43	113	9	0.803	0.0	15.068	1.1144	0.2850	0.0026	0.0157	-0.0045
04T- 43	113	10	0.799	0.0	17.144	1.1641	0.3514	0.0086	0.0149	-0.0056
04T- 43	114	1	0.701	0.0	-1.006	0.0351	0.0426	-0.0604	0.0206	0.0038
04T- 43	114	2	0.699	0.0	-3.294	-0.1330	0.0572	-0.0598	0.0197	0.0016
04T- 43	114	3	0.700	-0.0	1.314	0.2253	0.0386	-0.0623	0.0227	0.0093
04T- 43	114	4	0.701	0.0	3.586	0.4053	0.0449	-0.0576	0.0211	0.0028
04T- 43	114	5	0.699	0.0	5.867	0.5790	0.0642	-0.0502	0.0206	0.0011
04T- 43	114	6	0.699	0.0	8.151	0.7367	0.0936	-0.0384	0.0191	-0.0003
04T- 43	114	7	0.698	0.0	10.433	0.8921	0.1364	-0.0244	0.0182	-0.0017
04T- 43	114	8	0.700	0.0	12.588	0.9938	0.1900	-0.0037	0.0172	-0.0029
04T- 43	114	9	0.699	0.0	14.751	1.0689	0.2583	0.0116	0.0159	-0.0045
04T- 43	114	10	0.700	0.0	16.936	1.1433	0.3458	0.0293	0.0142	-0.0049
04T- 43	114	11	0.699	0.0	19.052	1.2027	0.4017	0.0379	0.0142	-0.0052
04T- 43	114	12	0.698	0.0	21.216	1.2669	0.4796	0.0456	0.0137	-0.0058
04T- 43	115	1	1.201	0.0	-1.159	-0.0380	0.0807	-0.0550	0.0108	0.0020
04T- 43	115	2	1.201	0.0	-3.479	-0.2011	0.0930	-0.0301	0.0107	0.0025
04T- 43	115	3	1.203	0.0	1.198	0.1387	0.0799	-0.0823	0.0120	0.0013
04T- 43	115	4	1.203	0.0	3.565	0.3188	0.0915	-0.1086	0.0135	-0.0004
04T- 43	115	5	1.202	0.0	6.022	0.5207	0.1174	-0.1325	0.0142	-0.0024
04T- 43	115	6	1.200	0.0	8.422	0.7173	0.1583	-0.1489	0.0127	-0.0043
04T- 43	115	7	1.203	0.0	10.781	0.8703	0.2091	-0.1493	0.0113	-0.0060
04T- 43	115	8	1.201	0.0	13.134	1.0222	0.2742	-0.1561	0.0109	-0.0077
04T- 43	115	9	1.202	0.0	15.450	1.1590	0.3512	-0.1695	0.0108	-0.0096
04T- 43	118	1	0.900	0.0	-1.041	0.0234	0.0555	-0.0699	0.0077	0.0007
04T- 43	118	2	0.900	0.0	3.716	0.4427	0.0719	-0.1043	0.0131	-0.0007
04T- 43	118	3	0.900	0.0	6.066	0.6497	0.1025	-0.1433	0.0124	-0.0027
04T- 43	118	4	0.897	0.0	8.366	0.8267	0.1440	-0.1832	0.0101	-0.0034
04T- 43	118	5	0.894	0.0	12.875	1.1662	0.2745	-0.3037	0.0076	-0.0043
04T- 43	118	6	0.901	0.0	23.710	1.7695	0.7906	-0.7249	0.0039	-0.0067
04T- 43	119	1	0.901	0.0	-1.041	0.0209	0.0569	-0.0668	0.0075	0.0011
04T- 43	119	2	0.900	0.0	-3.425	-0.1700	0.0704	-0.0648	0.0086	-0.0005
04T- 43	119	3	0.896	0.0	1.334	0.2195	0.0555	-0.0681	0.0096	0.0015
04T- 43	119	4	0.897	0.0	3.753	0.4453	0.0722	-0.1009	0.0126	-0.0002
04T- 43	119	5	0.901	0.0	6.105	0.6519	0.1032	-0.1410	0.0121	-0.0022
04T- 43	119	6	0.897	0.0	8.266	0.8160	0.1411	-0.1760	0.0099	-0.0028
04T- 43	119	7	0.896	0.0	10.677	0.9979	0.2003	-0.2267	0.0110	-0.0033
04T- 43	119	8	0.898	0.0	12.938	1.1613	0.2746	-0.3004	0.0078	-0.0034
04T- 43	119	9	0.898	0.0	15.183	1.3179	0.3628	-0.3870	0.0057	-0.0033
04T- 43	119	10	0.898	0.0	17.331	1.4487	0.4581	-0.4568	0.0066	-0.0055
04T- 43	119	11	0.898	0.0	19.455	1.5506	0.5598	-0.5577	0.0053	-0.0039
04T- 43	119	12	0.899	0.0	21.598	1.6616	0.6716	-0.6434	0.0043	-0.0043
04T- 43	119	13	0.898	0.0	22.668	1.7173	0.7305	-0.6811	0.0044	-0.0051
04T- 43	120	1	0.791	0.0	-1.019	0.0225	0.0470	-0.0525	0.0108	0.0026

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	120	2	0.791	0.0	-3.305	-0.1521	0.0621	-0.0464	0.0100	0.0016
04T- 43	120	3	0.799	0.0	1.280	0.2260	0.0437	-0.0663	0.0120	0.0024
04T- 43	120	4	0.803	0.0	3.639	0.4373	0.0551	-0.0882	0.0109	0.0006
04T- 43	120	5	0.799	0.0	5.986	0.6315	0.0819	-0.1186	0.0102	-0.0012
04T- 43	120	6	0.801	0.0	8.235	0.7974	0.1194	-0.1440	0.0089	-0.0022
04T- 43	120	7	0.798	0.0	10.537	0.9748	0.1729	-0.1869	0.0095	-0.0023
04T- 43	120	8	0.803	0.0	12.790	1.1302	0.2446	-0.2394	0.0091	-0.0027
04T- 43	120	9	0.800	0.0	14.940	1.2636	0.3261	-0.3054	0.0090	-0.0043
04T- 43	120	10	0.802	0.0	17.153	1.3774	0.4219	-0.3985	0.0071	-0.0044
04T- 43	120	11	0.799	0.0	19.278	1.4939	0.5238	-0.4911	0.0063	-0.0049
04T- 43	120	12	0.801	0.0	21.414	1.6009	0.6330	-0.5657	0.0073	-0.0062
04T- 43	120	13	0.801	0.0	23.452	1.6999	0.7454	-0.6400	0.0065	-0.0063
04T- 43	121	1	0.702	0.0	-1.015	0.0183	0.0435	-0.0437	0.0108	0.0026
04T- 43	121	2	0.699	0.0	-1.011	0.0206	0.0437	-0.0441	0.0109	0.0028
04T- 43	121	3	0.699	0.0	-3.367	-0.1574	0.0592	-0.0362	0.0102	0.0019
04T- 43	121	4	0.702	0.0	1.310	0.2192	0.0388	-0.0592	0.0120	0.0023
04T- 43	121	5	0.701	0.0	3.554	0.4121	0.0466	-0.0814	0.0112	0.0006
04T- 43	121	6	0.700	0.0	5.906	0.6094	0.0691	-0.1124	0.0112	-0.0011
04T- 43	121	7	0.700	0.0	8.076	0.7859	0.1023	-0.1455	0.0101	-0.0021
04T- 43	121	8	0.698	0.0	10.409	0.9677	0.1524	-0.1829	0.0094	-0.0027
04T- 43	121	9	0.697	0.0	12.531	1.1113	0.2182	-0.2342	0.0091	-0.0033
04T- 43	121	10	0.699	0.0	14.766	1.2275	0.3043	-0.2925	0.0072	-0.0041
04T- 43	121	11	0.700	0.0	16.821	1.3414	0.3893	-0.3557	0.0065	-0.0044
04T- 43	121	12	0.700	0.0	19.050	1.4587	0.4929	-0.4403	0.0072	-0.0052
04T- 43	121	13	0.699	0.0	21.239	1.5823	0.6058	-0.5146	0.0076	-0.0061
04T- 43	121	14	0.699	0.0	23.238	1.6309	0.7125	-0.5792	0.0075	-0.0067
04T- 43	122	1	1.201	0.0	-1.142	-0.0661	0.0850	-0.0026	0.0024	-0.0009
04T- 43	122	2	1.200	0.0	-3.460	-0.2589	0.0998	0.0687	0.0021	-0.0004
04T- 43	122	3	1.201	0.0	1.184	0.1428	0.0853	-0.0919	0.0043	-0.0012
04T- 43	122	4	1.199	0.0	3.548	0.3623	0.1001	-0.1839	0.0051	-0.0017
04T- 43	122	5	1.202	0.0	5.981	0.5989	0.1305	-0.2780	0.0060	-0.0028
04T- 43	122	6	1.201	0.0	8.367	0.8343	0.1808	-0.3710	0.0052	-0.0033
04T- 43	122	7	1.201	0.0	10.713	1.0353	0.2451	-0.4597	0.0048	-0.0037
04T- 43	122	8	1.201	0.0	12.948	1.2245	0.3242	-0.5560	0.0054	-0.0051
04T- 43	122	9	1.200	0.0	15.351	1.4155	0.4260	-0.6676	0.0059	-0.0065
04T- 43	122	10	1.200	0.0	17.508	1.5696	0.5295	-0.7677	0.0067	-0.0078
04T- 43	122	11	1.201	0.0	19.800	1.7116	0.6475	-0.8654	0.0069	-0.0097
04T- 43	122	12	1.204	0.0	22.078	1.8213	0.7672	-0.9483	0.0073	-0.0108
04T- 43	122	13	1.202	0.0	23.491	1.8903	0.8480	-1.0039	0.0081	-0.0127
04T- 43	125	1	0.899	0.0	-1.005	0.0438	0.0517	-0.0717	0.0010	-0.0026
04T- 43	125	2	0.896	0.0	3.706	0.4459	0.0672	-0.0903	0.0025	-0.0024
04T- 43	125	3	0.897	0.0	6.158	0.6615	0.0997	-0.1303	0.0011	-0.0025
04T- 43	125	4	0.894	0.0	8.400	0.8478	0.1427	-0.1793	0.0014	-0.0023
04T- 43	125	5	0.899	0.0	12.910	1.1905	0.2737	-0.3054	0.0024	-0.0021
04T- 43	125	6	0.901	0.0	23.730	1.7777	0.7910	-0.7245	0.0012	-0.0023
04T- 43	126	1	0.896	0.0	-1.007	0.0431	0.0519	-0.0724	0.0010	-0.0021

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	126	2	0.899	0.0	-3.395	-0.1394	0.0660	-0.0798	0.0008	-0.0028
04T- 43	126	3	0.899	0.0	1.400	0.2335	0.0521	-0.0695	0.0033	-0.0019
04T- 43	126	4	0.896	0.0	3.711	0.4447	0.0678	-0.0914	0.0030	-0.0021
04T- 43	126	5	0.899	0.0	6.138	0.6590	0.0998	-0.1303	0.0018	-0.0020
04T- 43	126	6	0.897	0.0	8.351	0.8429	0.1423	-0.1779	0.0015	-0.0019
04T- 43	126	7	0.895	0.0	10.734	1.0222	0.2006	-0.2417	0.0031	-0.0014
04T- 43	126	8	0.893	0.0	12.924	1.1854	0.2721	-0.3013	0.0014	-0.0011
04T- 43	126	9	0.898	0.0	15.180	1.3355	0.3604	-0.3783	0.0002	-0.0015
04T- 43	126	10	0.897	0.0	17.292	1.4427	0.4502	-0.4395	0.0007	-0.0012
04T- 43	126	11	0.899	0.0	19.473	1.5577	0.5585	-0.5489	0.0008	-0.0013
04T- 43	126	12	0.899	0.0	21.666	1.6791	0.6748	-0.6400	0.0005	-0.0012
04T- 43	126	13	0.899	0.0	23.733	1.7810	0.7929	-0.7240	0.0015	-0.0021
04T- 43	127	1	0.798	0.0	-1.024	0.0235	0.0445	-0.0582	0.0005	-0.0021
04T- 43	127	2	0.801	0.0	-3.274	-0.1453	0.0590	-0.0523	0.0009	-0.0026
04T- 43	127	3	0.804	0.0	1.327	0.2320	0.0410	-0.0720	0.0013	-0.0017
04T- 43	127	4	0.801	0.0	3.656	0.4432	0.0515	-0.0916	0.0016	-0.0017
04T- 43	127	5	0.798	0.0	6.073	0.6479	0.0790	-0.1208	0.0016	-0.0020
04T- 43	127	6	0.801	0.0	8.206	0.8066	0.1156	-0.1513	-0.0	-0.0016
04T- 43	127	7	0.802	0.0	10.602	0.9970	0.1721	-0.1953	-0.0002	-0.0006
04T- 43	127	8	0.798	0.0	12.856	1.1596	0.2455	-0.2544	0.0010	0.0
04T- 43	127	9	0.801	0.0	14.880	1.2677	0.3190	-0.3069	0.0020	-0.0003
04T- 43	127	10	0.801	0.0	17.082	1.3774	0.4147	-0.3961	0.0006	-0.0003
04T- 43	127	11	0.799	0.0	19.300	1.4923	0.5182	-0.4829	0.0005	-0.0008
04T- 43	127	12	0.804	0.0	21.431	1.6052	0.6295	-0.5619	0.0007	-0.0011
04T- 43	127	13	0.802	0.0	23.486	1.7130	0.7451	-0.6363	0.0011	-0.0014
04T- 43	128	1	0.698	0.0	-1.030	0.0121	0.0414	-0.0491	0.0003	-0.0022
04T- 43	128	2	0.700	0.0	-3.336	-0.1594	0.0565	-0.0406	0.0009	-0.0026
04T- 43	128	3	0.701	0.0	1.244	0.2078	0.0366	-0.0653	0.0013	-0.0018
04T- 43	128	4	0.700	0.0	3.601	0.4150	0.0439	-0.0865	0.0006	-0.0018
04T- 43	128	5	0.701	0.0	5.937	0.6145	0.0661	-0.1193	0.0006	-0.0018
04T- 43	128	6	0.699	0.0	8.196	0.8022	0.1012	-0.1561	-0.0	-0.0015
04T- 43	128	7	0.699	0.0	10.448	0.9812	0.1491	-0.1947	-0.0001	-0.0008
04T- 43	128	8	0.701	0.0	12.517	1.1154	0.2127	-0.2382	0.0011	-0.0003
04T- 43	128	9	0.702	0.0	14.726	1.2370	0.2987	-0.3021	0.0037	-0.0004
04T- 43	128	10	0.700	0.0	16.918	1.3520	0.3901	-0.3616	0.0006	0.0001
04T- 43	128	11	0.700	0.0	19.047	1.4605	0.4874	-0.4349	-0.0002	0.0002
04T- 43	128	12	0.699	0.0	21.232	1.5837	0.6002	-0.5095	0.0009	-0.0007
04T- 43	128	13	0.698	0.0	23.245	1.6938	0.7119	-0.5800	0.0013	-0.0015
04T- 43	129	1	1.202	0.0	-1.184	-0.0853	0.0811	-0.0020	0.0007	-0.0024
04T- 43	129	2	1.205	-0.0	-3.539	-0.2852	0.0959	0.0775	0.0010	-0.0025
04T- 43	129	3	1.206	0.0	1.165	0.1339	0.0801	-0.0974	0.0004	-0.0025
04T- 43	129	4	1.204	0.0	3.478	0.3590	0.0951	-0.1972	0.0003	-0.0023
04T- 43	129	5	1.202	0.0	5.886	0.5989	0.1253	-0.2928	0.0002	-0.0024
04T- 43	129	6	1.202	0.0	8.409	0.8489	0.1789	-0.3894	-0.0005	-0.0023
04T- 43	129	7	1.200	0.0	10.754	1.0537	0.2449	-0.4741	-0.0010	-0.0020
04T- 43	129	8	1.199	0.0	13.076	1.2549	0.3291	-0.5760	-0.0011	-0.0021
04T- 43	129	9	1.203	0.0	13.067	1.2495	0.3275	-0.5741	-0.0011	-0.0021

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T-	43	129	10 1.202	0.0	15.259	1.4286	0.4218	-0.6805	-0.0011	-0.0025
04T-	43	129	11 1.202	0.0	17.639	1.6014	0.5377	-0.7919	-0.0008	-0.0022
04T-	43	129	12 1.202	0.0	19.890	1.7376	0.6545	-0.8820	-0.0009	-0.0022
04T-	43	129	13 1.202	0.0	22.050	1.8439	0.7700	-0.9586	0.0003	-0.0036
04T-	43	129	14 1.204	0.0	22.645	1.8719	0.8032	-0.9814	0.0005	-0.0038
04T-	43	132	1 0.899	0.0	-1.059	0.0118	0.0531	-0.0666	0.0105	-0.0021
04T-	43	132	2 0.897	0.0	-3.430	-0.1851	0.0682	-0.0629	0.0110	-0.0018
04T-	43	132	3 0.905	0.0	1.328	0.2181	0.0541	-0.0732	0.0165	-0.0011
04T-	43	132	4 0.899	0.0	3.726	0.4358	0.0701	-0.0926	0.0203	-0.0023
04T-	43	132	5 0.902	0.0	6.083	0.6503	0.1031	-0.1306	0.0159	-0.0039
04T-	43	132	6 0.904	0.0	8.384	0.8342	0.1456	-0.1791	0.0137	-0.0044
04T-	43	132	7 0.903	0.0	9.082	-0.8554	-0.1608	-0.2291	0.0150	-0.0071
04T-	43	132	8 0.903	0.0	23.720	1.7719	0.7926	-0.7237	0.0046	-0.0041
04T-	43	133	1 0.900	0.0	-1.066	0.0071	0.0539	-0.0653	0.0105	-0.0015
04T-	43	133	2 0.905	0.0	-3.432	-0.1898	0.0695	-0.0635	0.0103	-0.0021
04T-	43	133	3 0.899	0.0	1.330	0.2211	0.0534	-0.0748	0.0164	-0.0009
04T-	43	133	4 0.899	0.0	3.732	0.4381	0.0710	-0.0921	0.0195	-0.0019
04T-	43	133	5 0.903	0.0	6.093	0.6509	0.1030	-0.1266	0.0153	-0.0033
04T-	43	133	6 0.902	0.0	8.398	0.8404	0.1464	-0.1773	0.0144	-0.0043
04T-	43	133	7 0.899	0.0	10.685	1.0120	0.2021	-0.2335	0.0167	-0.0050
04T-	43	133	8 0.901	0.0	12.905	1.1682	0.2731	-0.2971	0.0147	-0.0049
04T-	43	133	9 0.901	0.0	15.174	1.3354	0.3636	-0.3668	0.0124	-0.0052
04T-	43	133	10 0.907	0.0	17.339	1.4420	0.4556	-0.4382	0.0091	-0.0038
04T-	43	133	11 0.903	0.0	19.451	1.5426	0.5555	-0.5389	0.0086	-0.0041
04T-	43	133	12 0.900	0.0	21.633	1.6663	0.6720	-0.6318	0.0063	-0.0037
04T-	43	133	13 0.904	0.0	23.618	1.7608	0.7833	-0.7122	0.0049	-0.0039
04T-	43	134	1 0.800	0.0	-1.045	0.0094	0.0480	-0.0552	0.0161	-0.0003
04T-	43	134	2 0.799	0.0	-3.342	-0.1649	0.0632	-0.0463	0.0140	-0.0013
04T-	43	134	3 0.801	0.0	1.321	0.2259	0.0441	-0.0758	0.0200	-0.0005
04T-	43	134	4 0.799	0.0	3.715	0.4518	0.0569	-0.1029	0.0218	-0.0020
04T-	43	134	5 0.801	0.0	6.045	0.6430	0.0839	-0.1292	0.0189	-0.0035
04T-	43	134	6 0.798	0.0	8.257	0.8120	0.1207	-0.1568	0.0157	-0.0042
04T-	43	134	7 0.801	0.0	12.832	1.1557	0.2493	-0.2514	0.0143	-0.0042
04T-	43	134	8 0.800	0.0	14.954	1.2663	0.3256	-0.3093	0.0130	-0.0045
04T-	43	134	9 0.804	0.0	17.128	1.3807	0.4209	-0.4031	0.0071	-0.0045
04T-	43	134	10 0.801	0.0	19.251	1.4897	0.5209	-0.4827	0.0096	-0.0050
04T-	43	134	11 0.801	0.0	21.379	1.6002	0.6312	-0.5626	0.0078	-0.0043
04T-	43	134	12 0.803	0.0	23.388	1.7061	0.7446	-0.6387	0.0069	-0.0050
04T-	43	134	13 0.801	0.0	10.550	0.9911	0.1756	-0.1987	0.0143	-0.0038
04T-	43	135	1 0.701	0.0	-1.033	0.0097	0.0441	-0.0485	0.0172	-0.0008
04T-	43	135	2 0.700	0.0	-3.289	-0.1575	0.0589	-0.0386	0.0162	-0.0016
04T-	43	135	3 0.700	0.0	1.255	0.2137	0.0401	-0.0717	0.0211	-0.0003
04T-	43	135	4 0.700	0.0	3.553	0.4166	0.0479	-0.0966	0.0215	-0.0018
04T-	43	135	5 0.702	0.0	5.878	0.6138	0.0705	-0.1277	0.0207	-0.0033
04T-	43	135	6 0.700	-0.0	8.145	0.7992	0.1047	-0.1607	0.0194	0.0007
04T-	43	135	7 0.700	0.0	10.345	0.9761	0.1517	-0.1939	0.0160	-0.0054

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	135	8	0.697	0.0	12.559	1.1194	0.2193	-0.2420	0.0144	-0.0046
04T- 43	135	9	0.701	0.0	14.725	1.2266	0.3009	-0.2994	0.0082	-0.0040
04T- 43	135	10	0.701	0.0	16.877	1.3384	0.3903	-0.3598	0.0094	-0.0045
04T- 43	135	11	0.700	0.0	19.028	1.4599	0.4919	-0.4361	0.0103	-0.0049
04T- 43	135	12	0.701	0.0	21.186	1.5800	0.6023	-0.5100	0.0095	-0.0058
04T- 43	135	13	0.701	0.0	23.249	1.6870	0.7136	-0.5785	0.0090	-0.0062
04T- 43	136	1	1.204	0.0	-1.151	-0.0701	0.0866	-0.0099	0.0102	0.0001
04T- 43	136	2	1.204	0.0	-3.495	-0.2771	0.0995	0.0780	0.0082	-0.0009
04T- 43	136	3	1.206	0.0	1.178	0.1491	0.0861	-0.1052	0.0117	-0.0002
04T- 43	136	4	1.204	0.0	3.549	0.3726	0.1014	-0.1990	0.0120	-0.0007
04T- 43	136	5	1.205	0.0	5.994	0.6124	0.1331	-0.2934	0.0123	-0.0018
04T- 43	136	6	1.205	0.0	8.394	0.8443	0.1835	-0.3801	0.0110	-0.0032
04T- 43	136	7	1.205	0.0	10.694	1.0424	0.2471	-0.4643	0.0105	-0.0038
04T- 43	136	8	1.204	0.0	13.044	1.2414	0.3304	-0.5641	0.0101	-0.0052
04T- 43	136	9	1.206	0.0	15.312	1.4194	0.4260	-0.6696	0.0096	-0.0062
04T- 43	136	10	1.208	0.0	17.585	1.5794	0.5345	-0.7761	0.0090	-0.0061
04T- 43	136	11	1.206	0.0	19.817	1.7201	0.6508	-0.8714	0.0086	-0.0065
04T- 43	136	12	1.205	0.0	22.028	1.8279	0.7681	-0.9515	0.0085	-0.0090
04T- 43	136	13	1.205	0.0	22.317	1.8411	0.7836	-0.9610	0.0088	-0.0088
04T- 43	139	1	0.900	0.0	-1.143	-0.0416	0.0624	-0.0545	0.0261	-0.0001
04T- 43	139	2	0.899	0.0	3.733	0.4508	0.0806	-0.1040	0.0318	-0.0023
04T- 43	139	3	0.898	0.0	6.119	0.6672	0.1114	-0.1353	0.0219	-0.0043
04T- 43	139	4	0.904	0.0	8.420	0.8464	0.1551	-0.1828	0.0201	-0.0057
04T- 43	139	5	0.901	0.0	12.951	1.1899	0.2893	-0.2956	0.0231	-0.0084
04T- 43	139	6	0.904	0.0	23.701	1.7539	0.7957	-0.7174	0.0079	-0.0056
04T- 43	140	1	0.903	0.0	-1.148	-0.0446	0.0633	-0.0528	0.0255	-0.0005
04T- 43	140	2	0.902	0.0	-3.552	-0.2602	0.0811	-0.0456	0.0240	-0.0012
04T- 43	140	3	0.899	0.0	1.310	0.2064	0.0627	-0.0769	0.0298	0.0008
04T- 43	140	4	0.903	0.0	3.753	0.4566	0.0828	-0.1063	0.0308	-0.0017
04T- 43	140	5	0.905	0.0	6.135	0.6690	0.1134	-0.1386	0.0214	-0.0041
04T- 43	140	6	0.901	0.0	8.395	0.8427	0.1539	-0.1810	0.0203	-0.0054
04T- 43	140	7	0.905	0.0	10.709	1.0283	0.2160	-0.2371	0.0226	-0.0064
04T- 43	140	8	0.901	0.0	12.945	1.1940	0.2881	-0.2940	0.0235	-0.0081
04T- 43	140	9	0.902	0.0	15.174	1.3223	0.3726	-0.3579	0.0170	-0.0074
04T- 43	140	10	0.903	0.0	17.336	1.4346	0.4640	-0.4334	0.0151	-0.0073
04T- 43	140	11	0.905	0.0	19.449	1.5409	0.5670	-0.5404	0.0141	-0.0073
04T- 43	140	12	0.902	0.0	21.620	1.6544	0.6791	-0.6291	0.0113	-0.0058
04T- 43	140	13	0.901	0.0	23.694	1.7406	0.7895	-0.7073	0.0082	-0.0052
04T- 43	141	1	0.802	0.0	-1.109	-0.0312	0.0556	-0.0492	0.0294	0.0002
04T- 43	141	2	0.800	0.0	-3.417	-0.2137	0.0720	-0.0375	0.0238	-0.0006
04T- 43	141	3	0.801	0.0	1.264	0.1994	0.0520	-0.0773	0.0358	0.0013
04T- 43	141	4	0.801	0.0	3.646	0.4325	0.0642	-0.1099	0.0375	-0.0013
04T- 43	141	5	0.801	0.0	5.986	0.6428	0.0924	-0.1365	0.0308	-0.0038
04T- 43	141	6	0.800	0.0	8.252	0.8157	0.1288	-0.1659	0.0254	-0.0055
04T- 43	141	7	0.800	0.0	10.544	1.0085	0.1860	-0.2157	0.0280	-0.0069
04T- 43	141	8	0.799	0.0	12.755	1.1473	0.2555	-0.2626	0.0248	-0.0075

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	141	9	0.803	0.0	14.914	1.2514	0.3329	-0.3181	0.0227	-0.0090
04T- 43	141	10	0.800	0.0	17.062	1.3584	0.4243	-0.3963	0.0192	-0.0084
04T- 43	141	11	0.802	0.0	19.211	1.4816	0.5284	-0.4830	0.0172	-0.0083
04T- 43	141	12	0.800	0.0	21.350	1.5885	0.6374	-0.5663	0.0145	-0.0072
04T- 43	141	13	0.800	0.0	23.463	1.6931	0.7505	-0.6338	0.0130	-0.0077
04T- 43	142	1	0.701	0.0	-1.093	-0.0312	0.0530	-0.0446	0.0304	0.0002
04T- 43	142	2	0.699	0.0	-3.353	-0.2036	0.0686	-0.0314	0.0248	-0.0002
04T- 43	142	3	0.701	0.0	1.204	0.1797	0.0483	-0.0720	0.0358	0.0010
04T- 43	142	4	0.701	0.0	3.526	0.3996	0.0556	-0.1021	0.0373	-0.0012
04T- 43	142	5	0.698	0.0	5.840	0.6000	0.0780	-0.1355	0.0362	-0.0037
04T- 43	142	6	0.698	0.0	8.075	0.7875	0.1114	-0.1713	0.0340	-0.0058
04T- 43	142	7	0.698	0.0	10.341	0.9755	0.1613	-0.2111	0.0313	-0.0079
04T- 43	142	8	0.699	0.0	12.554	1.1252	0.2281	-0.2529	0.0260	-0.0088
04T- 43	142	9	0.698	0.0	14.695	1.2190	0.3083	-0.3069	0.0171	-0.0084
04T- 43	142	10	0.701	0.0	16.829	1.3243	0.3948	-0.3634	0.0179	-0.0085
04T- 43	142	11	0.700	0.0	18.995	1.4513	0.4968	-0.4406	0.0172	-0.0092
04T- 43	142	12	0.700	0.0	21.173	1.5702	0.6069	-0.5136	0.0158	-0.0094
04T- 43	142	13	0.699	0.0	23.243	1.6853	0.7206	-0.5811	0.0148	-0.0104
04T- 43	143	1	1.206	0.0	-1.160	-0.0729	0.0962	-0.0051	0.0201	0.0023
04T- 43	143	2	1.206	0.0	-3.501	-0.2367	0.1071	0.0887	0.0172	0.0039
04T- 43	143	3	1.204	0.0	1.197	0.1497	0.0965	-0.1009	0.0217	0.0013
04T- 43	143	4	1.203	0.0	3.564	0.3723	0.1114	-0.1909	0.0213	-0.0003
04T- 43	143	5	1.205	0.0	5.952	0.6075	0.1422	-0.2818	0.0215	-0.0027
04T- 43	143	6	1.204	0.0	8.391	0.8421	0.1922	-0.3670	0.0186	-0.0045
04T- 43	143	7	1.206	0.0	10.705	1.0409	0.2559	-0.4582	0.0183	-0.0061
04T- 43	143	8	1.204	0.0	13.009	1.2348	0.3371	-0.5541	0.0175	-0.0080
04T- 43	143	9	1.206	0.0	15.311	1.4127	0.4333	-0.6567	0.0162	-0.0091
04T- 43	143	10	1.203	0.0	17.574	1.5764	0.5425	-0.7635	0.0154	-0.0095
04T- 43	143	11	1.205	0.0	19.805	1.7105	0.6565	-0.8579	0.0145	-0.0107
04T- 43	143	12	1.205	0.0	22.016	1.8168	0.7723	-0.9397	0.0140	-0.0133
04T- 43	143	13	1.206	0.0	23.104	1.8649	0.8320	-0.9807	0.0142	-0.0133
04T- 43	146	1	0.897	0.0	-0.876	0.1046	0.0541	-0.0604	-0.0007	-0.0031
04T- 43	146	2	0.895	0.0	3.991	0.5642	0.0838	-0.1059	0.0016	-0.0032
04T- 43	146	3	0.897	0.0	6.288	0.7475	0.1193	-0.1407	0.0019	-0.0031
04T- 43	146	4	0.895	0.0	8.528	0.9062	0.1613	-0.1904	0.0022	-0.0025
04T- 43	146	5	0.900	0.0	13.051	1.2253	0.2940	-0.3183	-0.0006	-0.0012
04T- 43	146	6	0.893	0.0	23.709	1.7815	0.8054	-0.7217	0.0008	-0.0026
04T- 43	147	1	0.905	0.0	-0.890	0.0955	0.0564	-0.0591	-0.0005	-0.0023
04T- 43	147	2	0.903	0.0	-3.314	-0.1182	0.0675	-0.0631	0.0013	-0.0028
04T- 43	147	3	0.899	0.0	1.548	0.3186	0.0614	-0.0709	0.0017	-0.0024
04T- 43	147	4	0.899	0.0	3.933	0.5526	0.0838	-0.1043	0.0015	-0.0024
04T- 43	147	5	0.899	0.0	6.268	0.7354	0.1176	-0.1350	0.0018	-0.0024
04T- 43	147	6	0.899	0.0	8.552	0.9078	0.1629	-0.1858	0.0026	-0.0019
04T- 43	147	7	0.898	0.0	10.770	1.0659	0.2185	-0.2449	0.0021	-0.0014
04T- 43	147	8	0.902	0.0	12.988	1.2173	0.2913	-0.3134	-0.0002	-0.0011
04T- 43	147	9	0.901	0.0	15.286	1.3835	0.3862	-0.3864	0.0014	-0.0020

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	147	10	0.901	0.0	17.399	1.4788	0.4760	-0.4520	0.0009	-0.0016
04T- 43	147	11	0.900	0.0	19.527	1.5802	0.5797	-0.5525	0.0003	-0.0009
04T- 43	147	12	0.898	0.0	21.673	1.6959	0.6946	-0.6424	0.0004	-0.0012
04T- 43	147	13	0.894	0.0	23.720	1.7666	0.7992	-0.7077	0.0003	-0.0013
04T- 43	148	1	0.798	0.0	-0.918	0.0841	0.0466	-0.0486	0.0009	-0.0022
04T- 43	148	2	0.798	0.0	-3.244	-0.1133	0.0597	-0.0399	0.0014	-0.0027
04T- 43	148	3	0.800	0.0	1.523	0.3185	0.0482	-0.0753	0.0016	-0.0022
04T- 43	148	4	0.804	0.4	~~-1.588~~	~~-2.2832~~	~~0.0155~~	-0.4879	-0.0048	-0.0892
04T- 43	148	5	0.802	0.0	6.209	0.7315	0.0975	-0.1306	0.0022	-0.0020
04T- 43	148	6	0.797	0.0	8.396	0.8905	0.1367	-0.1561	0.0016	-0.0017
04T- 43	148	7	0.801	0.0	10.679	1.0630	0.1937	-0.1999	0.0009	-0.0010
04T- 43	148	8	0.800	0.0	12.854	1.2005	0.2643	-0.2597	0.0016	-0.0008
04T- 43	148	9	0.798	0.0	15.055	1.3279	0.3505	-0.3177	0.0002	-0.0003
04T- 43	148	10	0.799	0.0	17.195	1.4294	0.4435	-0.4050	-0.0021	0.0004
04T- 43	148	11	0.799	0.0	19.318	1.5392	0.5452	-0.4930	-0.0008	-0.0001
04T- 43	148	12	0.801	0.0	21.511	1.6416	0.6579	-0.5752	0.0004	-0.0008
04T- 43	148	13	0.799	0.0	23.521	1.7379	0.7685	-0.6441	0.0005	-0.0010
04T- 43	149	1	0.700	0.0	-0.930	0.0708	0.0433	-0.0420	0.0007	-0.0024
04T- 43	149	2	0.700	0.0	-3.219	-0.1190	0.0562	-0.0296	0.0012	-0.0030
04T- 43	149	3	0.700	0.0	1.368	0.2893	0.0424	-0.0696	0.0021	-0.0021
04T- 43	149	4	0.699	0.0	3.736	0.5017	0.0539	-0.0961	0.0016	-0.0021
04T- 43	149	5	0.700	0.0	5.981	0.6912	0.0789	-0.1250	0.0017	-0.0020
04T- 43	149	6	0.698	0.0	8.172	0.8708	0.1154	-0.1571	0.0013	-0.0016
04T- 43	149	7	0.696	0.0	10.468	1.0576	0.1687	-0.1965	0.0004	-0.0011
04T- 43	149	8	0.700	0.0	12.692	1.1341	0.2374	-0.2409	0.0003	-0.0007
04T- 43	149	9	0.701	0.0	12.699	1.1851	0.2376	-0.2407	0.0002	-0.0007
04T- 43	149	10	0.700	0.0	14.776	1.2660	0.3190	-0.2981	-0.0036	0.0
04T- 43	149	11	0.697	0.0	16.996	1.4015	0.4154	-0.3649	-0.0015	0.0002
04T- 43	149	12	0.698	0.0	19.055	1.5110	0.5132	-0.4412	-0.0009	0.0003
04T- 43	149	13	0.700	0.0	21.281	1.6252	0.6274	-0.5186	0.0009	-0.0010
04T- 43	149	16	0.700	0.0	-0.922	0.0749	0.0426	-0.0406	0.0007	-0.0024
04T- 43	150	1	1.206	0.0	-1.094	-0.0191	0.0886	-0.0399	0.0013	-0.0027
04T- 43	150	2	1.205	0.0	-3.487	-0.2380	0.0989	0.0537	0.0016	-0.0044
04T- 43	150	3	1.204	0.0	1.279	0.2119	0.0925	-0.1381	0.0012	-0.0022
04T- 43	150	4	1.203	0.0	3.654	0.4382	0.1113	-0.2282	0.0012	-0.0022
04T- 43	150	5	1.205	0.0	6.060	0.6767	0.1458	-0.3173	0.0013	-0.0024
04T- 43	150	6	1.203	0.0	8.519	0.9127	0.2007	-0.4076	0.0007	-0.0025
04T- 43	150	7	1.202	0.0	10.829	1.1105	0.2688	-0.4905	0.0001	-0.0024
04T- 43	150	8	1.205	0.0	13.118	1.2997	0.3521	-0.5878	-0.0	-0.0028
04T- 43	150	9	1.205	0.0	15.373	1.4822	0.4523	-0.7020	-0.0004	-0.0031
04T- 43	150	10	1.204	0.0	17.711	1.6428	0.5663	-0.8059	-0.0003	-0.0031
04T- 43	150	11	1.204	0.0	19.949	1.7697	0.6814	-0.8912	-0.0007	-0.0028
04T- 43	150	12	1.203	0.0	21.678	1.8585	0.7761	-0.9566	0.0005	-0.0045
04T- 43	153	1	0.899	0.0	-0.994	0.0413	0.0540	-0.0598	0.0107	-0.0015
04T- 43	153	2	0.900	0.0	3.871	0.5003	0.0785	-0.0991	0.0165	-0.0034
04T- 43	153	3	0.902	0.0	6.158	0.6929	0.1111	-0.1358	0.0131	-0.0039

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	153	4	0.904	0.0	8.432	0.8733	0.1557	-0.1872	0.0104	-0.0040
04T- 43	153	5	0.902	0.0	12.989	1.1993	0.2857	-0.3077	0.0084	-0.0033
04T- 43	153	6	0.901	0.0	21.713	1.6871	0.6901	-0.6468	0.0040	-0.0039
04T- 43	153	7	0.903	0.0	21.714	1.6871	0.6900	-0.6485	0.0040	-0.0040
04T- 43	154	1	0.897	0.0	-1.017	0.0344	0.0556	-0.0600	0.0105	-0.0009
04T- 43	154	2	0.901	0.0	-3.427	-0.1773	0.0693	-0.0561	0.0102	-0.0013
04T- 43	154	3	0.900	0.0	1.405	0.2591	0.0582	-0.0722	0.0146	-0.0011
04T- 43	154	4	0.900	0.0	3.822	0.4943	0.0782	-0.0989	0.0172	-0.0024
04T- 43	154	5	0.901	0.0	6.150	0.6935	0.1113	-0.1339	0.0137	-0.0035
04T- 43	154	6	0.899	0.0	8.505	0.8819	0.1572	-0.1875	0.0117	-0.0039
04T- 43	154	7	0.898	0.0	10.731	1.0528	0.2146	-0.2399	0.0113	-0.0039
04T- 43	154	8	0.895	0.0	12.933	1.1879	0.2800	-0.2997	0.0089	-0.0031
04T- 43	154	9	0.902	0.0	15.177	1.3522	0.3749	-0.3762	0.0068	-0.0040
04T- 43	154	10	0.900	0.0	17.350	1.4544	0.4653	-0.4469	0.0080	-0.0049
04T- 43	154	11	0.904	0.0	19.435	1.5679	0.5717	-0.5490	0.0067	-0.0047
04T- 43	154	12	0.897	0.0	21.664	1.6830	0.6863	-0.6439	0.0043	-0.0035
04T- 43	154	13	0.901	0.0	23.724	1.7748	0.8003	-0.7255	0.0026	-0.0034
04T- 43	154	15	0.898	0.0	-1.085	0.0239	0.0549	-0.0579	0.0105	-0.0006
04T- 43	155	1	0.802	0.0	-0.990	0.0389	0.0472	-0.0519	0.0162	0.0003
04T- 43	155	2	0.798	0.0	-3.321	-0.1513	0.0618	-0.0407	0.0138	-0.0013
04T- 43	155	3	0.800	0.0	1.427	0.2710	0.0463	-0.0775	0.0203	-0.0005
04T- 43	155	4	0.801	0.0	3.805	0.4977	0.0614	-0.1074	0.0219	-0.0021
04T- 43	155	5	0.799	0.0	6.078	0.6878	0.0910	-0.1326	0.0189	-0.0035
04T- 43	155	6	0.801	0.0	8.348	0.8550	0.1305	-0.1607	0.0143	-0.0041
04T- 43	155	7	0.801	0.0	10.618	1.0304	0.1855	-0.2046	0.0138	-0.0044
04T- 43	155	8	0.801	0.0	12.830	1.1794	0.2566	-0.2553	0.0119	-0.0046
04T- 43	155	9	0.800	0.0	15.005	1.2805	0.3361	-0.3129	0.0099	-0.0045
04T- 43	155	10	0.799	0.0	17.094	1.3930	0.4271	-0.3981	0.0085	-0.0044
04T- 43	155	11	0.799	0.0	19.228	1.5011	0.5273	-0.4846	0.0076	-0.0040
04T- 43	155	12	0.800	0.0	21.424	1.6099	0.6403	-0.5656	0.0066	-0.0043
04T- 43	155	13	0.800	0.0	23.482	1.7116	0.7524	-0.6339	0.0055	-0.0044
04T- 43	156	1	0.700	0.0	-0.976	0.0457	0.0439	-0.0477	0.0179	0.0005
04T- 43	156	2	0.699	-0.0	-3.372	-0.2082	0.0548	-0.0035	0.0146	0.0018
04T- 43	156	3	0.700	0.0	1.329	0.2549	0.0419	-0.0741	0.0216	-0.0002
04T- 43	156	4	0.700	0.0	3.617	0.4619	0.0523	-0.1030	0.0228	-0.0018
04T- 43	156	5	0.698	0.0	5.923	0.6572	0.0761	-0.1352	0.0221	-0.0034
04T- 43	156	6	0.699	0.0	8.160	0.8459	0.1125	-0.1696	0.0199	-0.0043
04T- 43	156	7	0.702	0.0	10.460	1.0232	0.1630	-0.2031	0.0168	-0.0051
04T- 43	156	8	0.702	0.0	12.590	1.1356	0.2270	-0.2443	0.0126	-0.0047
04T- 43	156	9	0.700	0.0	14.738	1.2397	0.3101	-0.2988	0.0082	-0.0040
04T- 43	156	10	0.701	0.0	16.884	1.3627	0.4007	-0.3660	0.0081	-0.0039
04T- 43	156	11	0.702	0.0	19.071	1.4806	0.5035	-0.4439	0.0086	-0.0044
04T- 43	156	12	0.696	0.0	21.133	1.5993	0.6110	-0.5146	0.0087	-0.0052
04T- 43	156	13	0.700	0.0	23.276	1.7032	0.7247	-0.5838	0.0072	-0.0054
04T- 43	157	1	1.202	0.0	-1.131	-0.0433	0.0885	-0.0293	0.0114	0.0001
04T- 43	157	2	1.202	0.0	-3.478	-0.2507	0.0993	0.0580	0.0097	0.0010

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	157	3	1.203	0.0	1.242	0.1856	0.0904	-0.1230	0.0129	-0.0004
04T- 43	157	4	1.205	0.0	3.596	0.4010	0.1069	-0.2118	0.0130	-0.0008
04T- 43	157	5	1.204	0.0	6.005	0.6379	0.1403	-0.3030	0.0133	-0.0023
04T- 43	157	6	1.204	0.0	8.397	0.8650	0.1911	-0.3864	0.0120	-0.0035
04T- 43	157	7	1.204	0.0	10.746	1.0628	0.2564	-0.4702	0.0113	-0.0044
04T- 43	157	8	1.203	0.0	13.056	1.2537	0.3379	-0.5642	0.0107	-0.0061
04T- 43	157	9	1.204	0.0	15.332	1.4318	0.4344	-0.6702	0.0095	-0.0070
04T- 43	157	10	1.204	0.0	17.607	1.5906	0.5432	-0.7714	0.0085	-0.0073
04T- 43	157	11	1.203	0.0	19.837	1.7298	0.6594	-0.8670	0.0073	-0.0077
04T- 43	157	12	1.203	0.0	22.064	1.8475	0.7821	-0.9547	0.0056	-0.0090
04T- 43	160	1	0.901	0.0	-0.957	0.0569	0.0580	-0.0540	0.0114	-0.0007
04T- 43	160	2	0.900	0.0	3.891	0.5354	0.0855	-0.1065	0.0155	-0.0029
04T- 43	160	3	0.899	0.0	6.234	0.7239	0.1185	-0.1383	0.0100	-0.0034
04T- 43	160	4	0.901	0.0	8.499	0.9025	0.1650	-0.1910	0.0076	-0.0033
04T- 43	160	5	0.894	0.0	13.028	1.2211	0.2959	-0.3115	0.0092	-0.0040
04T- 43	160	6	0.899	0.0	22.300	1.7255	0.7331	-0.6742	0.0025	-0.0025
04T- 43	161	1	0.897	0.0	-0.962	0.0540	0.0591	-0.0539	0.0118	-0.0004
04T- 43	161	2	0.897	0.0	-3.384	-0.1667	0.0714	-0.0472	0.0114	-0.0024
04T- 43	161	3	0.899	0.0	1.468	0.2976	0.0636	-0.0739	0.0174	-0.0012
04T- 43	161	4	0.899	0.0	3.875	0.5311	0.0849	-0.1035	0.0160	-0.0025
04T- 43	161	5	0.898	0.0	6.239	0.7227	0.1181	-0.1362	0.0102	-0.0031
04T- 43	161	6	0.902	0.0	6.258	0.7292	0.1197	-0.1391	0.0099	-0.0030
04T- 43	161	7	0.900	0.0	8.531	0.9040	0.1651	-0.1896	0.0074	-0.0028
04T- 43	161	8	0.903	0.0	10.764	1.0686	0.2224	-0.2472	0.0077	-0.0025
04T- 43	161	9	0.896	0.0	12.980	1.2197	0.2940	-0.3093	0.0101	-0.0044
04T- 43	161	10	0.899	0.0	15.253	1.3772	0.3865	-0.3840	0.0075	-0.0030
04T- 43	161	11	0.900	0.0	17.393	1.4760	0.4797	-0.4532	0.0063	-0.0036
04T- 43	161	12	0.897	0.0	19.516	1.5822	0.5841	-0.5539	0.0057	-0.0041
04T- 43	161	13	0.900	0.0	21.689	1.6915	0.6980	-0.6490	0.0029	-0.0023
04T- 43	161	14	0.902	0.0	23.352	1.7540	0.7844	-0.7093	0.0017	-0.0025
04T- 43	162	1	0.800	0.0	-0.940	0.0654	0.0505	-0.0491	0.0177	0.0008
04T- 43	162	2	0.800	0.0	1.456	0.2995	0.0513	-0.0785	0.0224	-0.0003
04T- 43	162	3	0.793	0.0	-3.281	-0.1379	0.0636	-0.0359	0.0149	-0.0004
04T- 43	162	4	0.801	0.0	1.435	0.2980	0.0515	-0.0779	0.0223	-0.0003
04T- 43	162	5	0.800	0.0	3.812	0.5267	0.0680	-0.1075	0.0228	-0.0019
04T- 43	162	6	0.801	0.0	6.144	0.7168	0.0986	-0.1318	0.0193	-0.0033
04T- 43	162	7	0.800	0.0	8.368	0.8777	0.1376	-0.1599	0.0135	-0.0039
04T- 43	162	8	0.801	0.0	10.633	1.0503	0.1935	-0.2040	0.0130	-0.0044
04T- 43	162	9	0.799	0.0	12.849	1.1384	0.2636	-0.2599	0.0096	-0.0040
04T- 43	162	10	0.800	0.0	15.018	1.3048	0.3483	-0.3141	0.0099	-0.0047
04T- 43	162	11	0.800	0.0	17.148	1.4107	0.4400	-0.3981	0.0070	-0.0039
04T- 43	162	12	0.801	0.0	19.286	1.5258	0.5434	-0.4907	0.0064	-0.0037
04T- 43	162	13	0.800	0.0	21.425	1.6239	0.6524	-0.5717	0.0052	-0.0029
04T- 43	162	14	0.800	0.0	23.389	1.7208	0.7605	-0.6404	0.0054	-0.0045
04T- 43	165	1	0.903	0.0	-0.944	0.0713	0.0541	-0.0651	-0.0007	-0.0026
04T- 43	165	2	0.899	0.0	3.872	0.5116	0.0775	-0.1002	0.0019	-0.0026

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	165	3	0.896	0.0	6.192	0.7108	0.1111	-0.1347	0.0016	-0.0025
04T- 43	165	4	0.900	0.0	8.482	0.8897	0.1564	-0.1927	0.0012	-0.0019
04T- 43	165	5	0.898	0.0	12.981	1.2192	0.2875	-0.3109	-0.0023	-0.0002
04T- 43	165	6	0.902	0.0	22.476	1.7344	0.7331	-0.6806	0.0002	-0.0016
04T- 43	166	1	0.900	-0.0	-0.945	0.0716	0.0544	-0.0661	-0.0006	-0.0022
04T- 43	166	2	0.899	-0.0	-3.328	-0.1252	0.0666	-0.0720	0.0010	-0.0027
04T- 43	166	3	0.900	0.0	1.443	0.2790	0.0571	-0.0724	0.0015	-0.0022
04T- 43	166	4	0.900	0.0	3.872	0.5127	0.0780	-0.1021	0.0022	-0.0023
04T- 43	166	5	0.899	0.0	6.183	0.7063	0.1104	-0.1371	0.0010	-0.0021
04T- 43	166	6	0.902	0.0	8.546	0.8988	0.1591	-0.1963	0.0012	-0.0018
04T- 43	166	7	0.901	0.0	10.733	1.0690	0.2154	-0.2498	0.0032	-0.0017
04T- 43	166	8	0.899	0.0	13.055	1.2269	0.2905	-0.3131	-0.0007	-0.0004
04T- 43	166	9	0.899	0.0	15.224	1.3679	0.3764	-0.3760	0.0042	-0.0020
04T- 43	166	10	0.901	0.0	17.369	1.4761	0.4681	-0.4620	-0.0032	-0.0012
04T- 43	166	11	0.897	0.0	19.495	1.5725	0.5699	-0.5504	0.0010	-0.0020
04T- 43	166	12	0.899	0.0	21.665	1.6875	0.6848	-0.6427	0.0	-0.0009
04T- 43	166	13	0.899	0.0	23.543	1.7724	0.7987	-0.7156	0.0011	-0.0025
04T- 43	167	1	0.799	-0.0	-0.953	0.0626	0.0451	-0.0560	0.0003	-0.0019
04T- 43	167	2	0.797	-0.0	-3.274	-0.1253	0.0591	-0.0489	0.0009	-0.0024
04T- 43	167	3	0.801	0.0	1.429	0.2810	0.0445	-0.0752	0.0013	-0.0017
04T- 43	167	4	0.800	0.0	3.735	0.4963	0.0579	-0.1006	0.0011	-0.0018
04T- 43	167	5	0.798	0.0	6.082	0.6942	0.0880	-0.1276	0.0010	-0.0017
04T- 43	167	6	0.800	0.0	8.344	0.8643	0.1286	-0.1574	-0.0001	-0.0014
04T- 43	167	7	0.802	0.0	10.627	1.0377	0.1839	-0.1986	-0.0002	-0.0007
04T- 43	167	8	0.801	0.0	12.850	1.1880	0.2562	-0.2589	0.0020	-0.0006
04T- 43	167	9	0.800	0.0	15.009	1.3001	0.3371	-0.3189	0.0021	-0.0005
04T- 43	167	10	0.802	0.0	17.099	1.4007	0.4270	-0.4013	0.0001	-0.0004
04T- 43	167	11	0.800	0.0	19.274	1.5150	0.5304	-0.4912	0.0	-0.0004
04T- 43	167	12	0.799	0.0	21.441	1.6207	0.6418	-0.5701	0.0011	-0.0017
04T- 43	167	13	0.800	0.0	23.354	1.7153	0.7472	-0.6380	0.0012	-0.0021
04T- 43	168	1	0.700	-0.0	-0.968	0.0516	0.0427	-0.0489	0.0002	-0.0022
04T- 43	168	2	0.698	-0.0	-3.277	-0.1316	0.0570	-0.0383	0.0008	-0.0026
04T- 43	168	3	0.699	0.0	1.324	0.2549	0.0403	-0.0694	0.0011	-0.0017
04T- 43	168	4	0.703	0.0	3.652	0.4636	0.0495	-0.0945	0.0006	-0.0017
04T- 43	168	5	0.700	0.0	5.943	0.6599	0.0734	-0.1249	0.0009	-0.0015
04T- 43	168	6	0.698	0.0	8.197	0.8479	0.1105	-0.1629	0.0004	-0.0012
04T- 43	168	7	0.700	0.0	10.420	1.0230	0.1591	-0.2007	0.0005	-0.0007
04T- 43	168	8	0.699	0.0	12.604	1.1435	0.2257	-0.2434	-0.0013	-0.0002
04T- 43	168	9	0.700	0.0	14.743	1.2516	0.3094	-0.3003	0.0023	-0.0001
04T- 43	168	10	0.701	0.0	16.886	1.3674	0.4007	-0.3724	-0.0015	0.0010
04T- 43	168	11	0.699	0.0	19.027	1.4854	0.5009	-0.4451	-0.0003	0.0004
04T- 43	168	12	0.701	0.0	21.193	1.5994	0.6109	-0.5184	0.0014	-0.0009
04T- 43	168	13	0.698	0.0	23.268	1.7081	0.7247	-0.5883	0.0011	-0.0011
04T- 43	169	1	1.203	-0.0	-1.141	-0.0515	0.0848	-0.0232	0.0009	-0.0026
04T- 43	169	2	1.203	-0.0	-3.486	-0.2530	0.0970	0.0574	0.0011	-0.0028
04T- 43	169	3	1.205	0.0	1.218	0.1700	0.0858	-0.1161	0.0007	-0.0025

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	169	4	1.203	0.0	3.605	0.3956	0.1026	-0.2105	0.0006	-0.0023
04T- 43	169	5	1.204	0.0	5.969	0.6305	0.1350	-0.3008	0.0004	-0.0024
04T- 43	169	6	1.204	0.0	8.413	0.8692	0.1875	-0.3913	0.0001	-0.0023
04T- 43	169	7	1.202	0.0	10.730	1.0706	0.2537	-0.4756	-0.0004	-0.0023
04T- 43	169	8	1.202	0.0	13.061	1.2645	0.3364	-0.5716	-0.0005	-0.0027
04T- 43	169	9	1.204	0.0	15.366	1.4458	0.4354	-0.6807	-0.0008	-0.0030
04T- 43	169	10	1.202	0.0	17.629	1.6064	0.5451	-0.7836	-0.0005	-0.0030
04T- 43	169	11	1.203	0.0	19.880	1.7372	0.6601	-0.8716	-0.0009	-0.0027
04T- 43	169	12	1.203	0.0	22.051	1.8492	0.7786	-0.9509	-0.0010	-0.0033
04T- 43	172	1	0.902	0.0	-1.315	-0.1277	0.0789	-0.0617	0.0299	-0.0016
04T- 43	172	2	0.901	0.0	-3.676	-0.3108	0.1018	-0.0536	0.0305	-0.0053
04T- 43	172	3	0.904	0.0	1.090	0.0912	0.0687	-0.0732	0.0248	0.0017
04T- 43	172	4	0.897	0.0	3.552	0.3397	0.0760	-0.0973	0.0185	0.0016
04T- 43	172	5	0.900	0.0	5.942	0.5843	0.1008	-0.1360	0.0125	-0.0011
04T- 43	172	6	0.899	0.0	8.240	0.7903	0.1405	-0.1845	0.0090	-0.0023
04T- 43	172	7	0.897	0.0	10.612	0.9946	0.1976	-0.2418	0.0063	-0.0026
04T- 43	172	8	0.897	0.0	12.870	1.1705	0.2703	-0.3040	0.0022	-0.0019
04T- 43	172	9	0.898	0.0	15.144	1.3350	0.3611	-0.3742	0.0026	-0.0016
04T- 43	172	10	0.898	0.0	17.373	1.4709	0.4577	-0.4558	0.0017	-0.0011
04T- 43	172	11	0.837	0.0	19.487	1.5636	0.5588	-0.5550	-0.0011	-0.0022
04T- 43	172	12	0.902	0.0	21.610	1.6680	0.6699	-0.6373	0.0016	-0.0025
04T- 43	173	1	0.798	0.0	-1.271	-0.1211	0.0719	-0.0550	0.0264	-0.0003
04T- 43	173	2	0.801	0.0	-3.579	-0.2830	0.0926	-0.0474	0.0259	-0.0020
04T- 43	173	3	0.802	0.0	1.100	0.0911	0.0608	-0.0744	0.0256	0.0024
04T- 43	173	4	0.800	0.0	3.418	0.3050	0.0641	-0.0985	0.0245	0.0033
04T- 43	173	5	0.803	0.0	5.760	0.5231	0.0831	-0.1274	0.0196	0.0007
04T- 43	173	6	0.801	0.0	8.086	0.7294	0.1165	-0.1637	0.0138	-0.0009
04T- 43	173	7	0.798	0.0	10.439	0.9462	0.1684	-0.2078	0.0079	-0.0009
04T- 43	173	8	0.737	0.0	12.742	1.1262	0.2408	-0.2562	0.0075	-0.0009
04T- 43	173	9	0.803	0.0	14.917	1.2527	0.3215	-0.3197	0.0055	-0.0008
04T- 43	173	10	0.803	0.0	17.092	1.3715	0.4151	-0.3994	0.0030	-0.0020
04T- 43	173	11	0.799	0.0	19.199	1.4897	0.5150	-0.4863	0.0030	-0.0023
04T- 43	173	12	0.801	0.0	21.386	1.6024	0.6278	-0.5662	0.0019	-0.0024
04T- 43	174	1	1.204	0.0	-1.283	-0.1373	0.0967	0.0088	0.0120	0.0010
04T- 43	174	2	1.202	0.0	-3.668	-0.3461	0.1182	0.0847	0.0156	0.0017
04T- 43	174	3	1.205	0.0	1.056	0.0704	0.0919	-0.0778	0.0098	-0.0005
04T- 43	174	4	1.204	0.0	3.409	0.2973	0.1033	-0.1751	0.0081	-0.0010
04T- 43	174	5	1.206	0.0	5.843	0.5372	0.1310	-0.2709	0.0070	-0.0022
04T- 43	174	6	1.202	0.0	8.232	0.7810	0.1784	-0.3661	0.0063	-0.0032
04T- 43	174	7	1.203	0.0	10.608	0.9925	0.2406	-0.4523	0.0050	-0.0039
04T- 43	174	8	1.204	0.0	12.935	1.1911	0.3186	-0.5493	0.0043	-0.0046
04T- 43	174	9	1.205	0.0	15.243	1.3749	0.4129	-0.6529	0.0039	-0.0061
04T- 43	174	10	1.203	0.0	17.528	1.5431	0.5198	-0.7546	0.0039	-0.0067
04T- 43	174	11	1.203	0.0	19.750	1.6868	0.6320	-0.8494	0.0030	-0.0067
04T- 43	174	12	1.203	0.0	21.952	1.8055	0.7517	-0.9329	0.0025	-0.0073
04T- 43	177	1	0.896	0.0	-1.098	-0.0368	0.0557	-0.0256	0.0237	-0.0019

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	177	2	0.886	0.0	-3.536	-0.2696	0.0710	-0.0099	0.0307	-0.0038
04T- 43	177	3	0.894	0.0	3.823	0.4459	0.0776	-0.0800	0.0173	-0.0041
04T- 43	177	4	0.898	0.0	6.107	0.6514	0.1107	-0.1221	0.0111	-0.0045
04T- 43	177	5	0.899	0.0	8.362	0.8150	0.1555	-0.1668	0.0103	-0.0033
04T- 43	177	6	0.900	0.0	12.899	1.1233	0.2846	-0.2806	0.0176	-0.0025
04T- 43	177	7	0.900	0.0	23.688	1.7320	0.7904	-0.6811	0.0129	-0.0031
04T- 43	178	1	0.895	0.0	-1.099	-0.0369	0.0546	-0.0265	0.0242	-0.0013
04T- 43	178	2	0.895	0.0	-3.449	-0.2710	0.0707	-0.0110	0.0312	-0.0046
04T- 43	178	3	0.897	0.0	1.335	0.1992	0.0571	-0.0408	0.0194	-0.0015
04T- 43	178	4	0.900	0.0	3.752	0.4414	0.0770	-0.0779	0.0154	-0.0037
04T- 43	178	5	0.901	0.0	~~2.419~~	~~-1.4175~~	~~-0.0488~~	-0.0552	0.0091	-0.0061
04T- 43	178	6	0.902	0.0	8.351	0.8170	0.1559	-0.1630	0.0105	-0.0028
04T- 43	178	7	0.897	0.0	10.632	0.9707	0.2135	-0.2121	0.0144	-0.0019
04T- 43	178	8	0.896	0.0	12.874	1.1259	0.2837	-0.2745	0.0171	-0.0013
04T- 43	178	9	0.898	0.0	15.084	1.2695	0.3674	-0.3580	0.0217	-0.0044
04T- 43	178	10	0.898	0.0	17.265	1.4108	0.4638	-0.4368	0.0214	-0.0060
04T- 43	178	11	0.896	0.0	19.438	1.5278	0.5646	-0.5134	0.0186	-0.0059
04T- 43	178	12	0.901	0.0	21.619	1.6383	0.6793	-0.6078	0.0141	-0.0028
04T- 43	178	13	0.895	0.0	23.690	1.7253	0.7879	-0.6767	0.0137	-0.0035
04T- 43	179	1	0.806	0.0	-0.990	-0.0216	0.0479	-0.0214	0.0271	-0.0025
04T- 43	179	1	0.806	0.0	-0.987	-0.0205	0.0485	-0.0206	0.0271	-0.0027
04T- 43	179	2	0.802	0.0	-3.425	-0.2404	0.0645	-0.0013	0.0302	-0.0058
04T- 43	179	3	0.804	0.0	1.224	0.1938	0.0485	-0.0457	0.0267	-0.0018
04T- 43	179	4	0.800	0.0	3.629	0.4131	0.0628	-0.0785	0.0276	-0.0034
04T- 43	179	5	0.809	0.0	6.045	0.6145	0.0924	-0.1059	0.0210	-0.0050
04T- 43	179	6	0.800	0.0	8.232	0.7845	0.1330	-0.1453	0.0174	-0.0049
04T- 43	179	7	0.805	0.0	10.463	0.9474	0.1893	-0.1901	0.0185	-0.0043
04T- 43	179	8	0.799	0.0	12.679	1.0824	0.2534	-0.2344	0.0274	-0.0053
04T- 43	179	9	0.794	0.0	14.836	1.2209	0.3322	-0.2915	0.0323	-0.0091
04T- 43	179	10	0.800	0.0	17.082	1.3400	0.4226	-0.3646	0.0251	-0.0095
04T- 43	179	11	0.801	0.0	19.238	1.4686	0.5286	-0.4581	0.0212	-0.0096
04T- 43	179	12	0.800	0.0	21.422	1.5775	0.6419	-0.5494	0.0202	-0.0111
04T- 43	179	13	0.803	0.0	23.462	1.6784	0.7534	-0.6195	0.0174	-0.0099
04T- 43	179	14	0.805	0.1	6.656	-1.3015	-0.1703	-0.1146	0.0192	-0.0061
04T- 43	180	1	0.704	0.0	-0.999	-0.0282	0.0446	-0.0157	0.0278	-0.0023
04T- 43	180	2	0.704	0.0	-3.433	-0.2344	0.0603	0.0022	0.0295	-0.0039
04T- 43	180	3	0.704	0.0	1.265	0.1794	0.0439	-0.0432	0.0285	-0.0023
04T- 43	180	4	0.698	0.0	3.550	0.3828	0.0541	-0.0764	0.0316	-0.0037
04T- 43	180	5	0.691	0.0	5.931	0.5975	0.0783	-0.1151	0.0319	-0.0055
04T- 43	180	6	0.698	0.0	8.078	0.7687	0.1154	-0.1463	0.0290	-0.0059
04T- 43	180	7	0.699	0.0	10.324	0.9169	0.1674	-0.1777	0.0271	-0.0058
04T- 43	180	8	0.696	0.0	12.464	1.0757	0.2313	-0.2273	0.0294	-0.0062
04T- 43	180	9	0.697	0.0	14.725	1.1822	0.3455	-0.2703	0.0313	-0.0089
04T- 43	180	10	0.700	0.0	16.919	1.3072	0.3968	-0.3407	0.0241	-0.0097
04T- 43	180	11	0.701	0.0	18.980	1.4124	0.4904	-0.4197	0.0216	-0.0116
04T- 43	180	12	0.695	0.0	21.108	1.5371	0.5997	-0.4961	0.0217	-0.0139
04T- 43	180	13	0.696	0.0	23.196	1.6463	0.7119	-0.5609	0.0208	-0.0147

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	180	15	0.699	0.0	-1.035	-0.0348	0.0449	-0.0128	0.0277	-0.0037
04T- 43	181	1	1.204	0.0	-1.069	-0.0663	0.0836	0.0267	0.0107	-0.0030
04T- 43	181	2	1.203	0.0	-3.356	-0.2671	0.0969	0.1034	0.0139	-0.0034
04T- 43	181	3	1.204	0.0	1.225	0.1507	0.0853	-0.0624	0.0080	-0.0045
04T- 43	181	4	1.202	0.0	3.658	0.3847	0.1053	-0.1581	0.0063	-0.0049
04T- 43	181	5	1.203	0.0	6.030	0.6240	0.1421	-0.2575	0.0068	-0.0045
04T- 43	181	6	1.198	0.0	8.426	0.8544	0.1959	-0.3510	0.0085	-0.0046
04T- 43	181	7	1.198	0.0	10.664	1.0477	0.2605	-0.4378	0.0103	-0.0049
04T- 43	181	8	1.204	0.0	13.060	1.2350	0.3447	-0.5348	0.0107	-0.0054
04T- 43	181	9	1.204	0.0	15.290	1.4041	0.4380	-0.6347	0.0128	-0.0059
04T- 43	181	10	1.202	0.0	17.551	1.5599	0.5449	-0.7397	0.0138	-0.0063
04T- 43	181	11	1.203	0.0	19.801	1.6888	0.6574	-0.8305	0.0144	-0.0067
04T- 43	181	12	1.204	0.0	22.018	1.7953	0.7729	-0.9169	0.0154	-0.0093
04T- 43	184	1	0.898	0.0	-0.934	0.0525	0.0443	-0.0602	-0.0021	-0.0056
04T- 43	184	2	0.899	0.0	3.773	0.4465	0.0670	-0.0816	-0.0144	-0.0039
04T- 43	184	3	0.898	0.0	6.113	0.6559	0.1015	-0.1204	-0.0119	-0.0023
04T- 43	184	4	0.899	0.0	8.435	0.8490	0.1502	-0.1736	-0.0111	-0.0002
04T- 43	184	5	0.896	0.0	12.898	1.1483	0.2769	-0.2917	0.0018	0.0014
04T- 43	184	6	0.898	0.0	23.727	1.7620	0.7887	-0.7045	0.0050	0.0024
04T- 43	185	1	0.894	0.0	-0.888	0.0555	0.0441	-0.0601	-0.0017	-0.0056
04T- 43	185	2	0.897	0.0	-3.371	-0.1518	0.0573	-0.0590	0.0078	-0.0054
04T- 43	185	3	0.896	0.0	1.405	0.2338	0.0480	-0.0569	-0.0124	-0.0051
04T- 43	185	4	0.901	0.0	~~-0.122~~	~~-1.6553~~	~~0.0119~~	~~-0.0157~~	~~-0.0150~~	~~-0.0079~~
04T- 43	185	5	0.901	0.0	6.165	0.6561	0.1017	-0.1219	-0.0118	-0.0024
04T- 43	185	6	0.898	0.0	8.429	0.8422	0.1487	-0.1724	-0.0112	-0.0001
04T- 43	185	7	0.897	0.0	10.521	0.9741	0.2001	-0.2260	-0.0027	0.0005
04T- 43	185	8	0.905	0.0	12.920	1.1525	0.2790	-0.2966	0.0023	0.0013
04T- 43	185	9	0.898	0.0	14.990	1.2863	0.3555	-0.3731	0.0044	0.0004
04T- 43	185	10	0.895	0.0	17.289	1.4266	0.4526	-0.4551	0.0073	-0.0002
04T- 43	185	11	0.897	0.0	19.523	1.5532	0.5607	-0.5398	0.0063	-0.0022
04T- 43	185	12	0.901	0.0	21.719	1.6673	0.6778	-0.6324	0.0038	0.0016
04T- 43	185	13	0.897	0.0	23.735	1.7599	0.7881	-0.7039	0.0049	0.0023
04T- 43	186	1	0.801	0.0	-0.896	0.0520	0.0378	-0.0509	-0.0006	-0.0044
04T- 43	186	2	0.795	0.0	-3.364	-0.1501	0.0514	-0.0384	0.0055	-0.0049
04T- 43	186	3	0.798	0.0	1.384	0.2435	0.0387	-0.0622	-0.0032	-0.0032
04T- 43	186	4	0.797	0.0	3.704	0.4415	0.0521	-0.0817	-0.0052	-0.0025
04T- 43	186	5	0.798	0.0	6.020	0.6352	0.0806	-0.1102	-0.0084	-0.0016
04T- 43	186	6	0.805	0.0	8.283	0.8050	0.1248	-0.1457	-0.0079	-0.0001
04T- 43	186	7	0.801	0.0	10.544	0.9568	0.1805	-0.1901	-0.0013	0.0018
04T- 43	186	8	0.800	0.0	12.712	1.0959	0.2441	-0.2478	0.0063	0.0025
04T- 43	186	9	0.804	0.0	14.938	1.2439	0.3263	-0.3113	0.0121	0.0004
04T- 43	186	10	0.797	0.0	17.078	1.3770	0.4174	-0.3992	0.0105	0.0005
04T- 43	186	11	0.799	0.0	19.248	1.4784	0.5162	-0.4806	0.0060	-0.0011
04T- 43	186	12	0.799	0.0	21.385	1.5901	0.6280	-0.5641	0.0064	-0.0029
04T- 43	186	13	0.798	0.0	23.455	1.6970	0.7428	-0.6346	0.0062	-0.0031
04T- 43	186	15	0.800	0.0	-0.968	0.0439	0.0377	-0.0488	-0.0006	-0.0047

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	187	1	0.701	-0.0	-0.581	0.0336	0.0354	-0.0435	-0.0012	-0.0043
04T- 43	187	2	0.700	0.0	-3.269	-0.1492	0.0481	-0.0307	0.0036	-0.0051
04T- 43	187	3	0.702	0.0	1.394	0.2288	0.0352	-0.0593	-0.0027	-0.0029
04T- 43	187	4	0.702	0.0	3.628	0.4153	0.0447	-0.0812	-0.0021	-0.0017
04T- 43	187	5	0.700	0.0	5.866	0.6060	0.0668	-0.1117	-0.0020	-0.0008
04T- 43	187	6	0.698	0.0	8.178	0.7874	0.1075	-0.1465	-0.0012	0.0005
04T- 43	187	7	0.696	0.0	10.381	0.9333	0.1607	-0.1859	0.0037	0.0027
04T- 43	187	8	0.700	0.0	12.536	1.0723	0.2216	-0.2281	0.0108	0.0034
04T- 43	187	9	0.700	0.0	12.537	1.0733	0.2219	-0.2280	0.0108	0.0033
04T- 43	187	10	0.699	0.0	12.534	1.0737	0.2220	-0.2280	0.0108	0.0033
04T- 43	187	11	0.698	0.0	14.669	1.2070	0.2961	-0.2814	0.0140	0.0021
04T- 43	187	12	0.695	0.0	16.898	1.3264	0.3874	-0.3627	0.0107	0.0007
04T- 43	187	13	0.699	0.0	19.010	1.4382	0.4865	-0.4494	0.0090	-0.0026
04T- 43	187	14	0.698	0.0	21.178	1.5527	0.5938	-0.5203	0.0083	-0.0038
04T- 43	187	15	0.697	0.0	23.182	1.6675	0.7051	-0.5831	0.0086	-0.0043
04T- 43	187	16	0.697	0.0	10.407	0.9286	0.1601	-0.1833	0.0049	0.0023
04T- 43	187	17	0.697	0.0	10.411	0.9305	0.1606	-0.1842	0.0050	0.0023
04T- 43	188	1	1.206	-0.0	-1.112	-0.0627	0.0712	0.0047	-0.0031	-0.0064
04T- 43	188	2	1.204	-0.0	-3.471	-0.2636	0.0846	0.0820	-0.0002	-0.0058
04T- 43	188	3	1.205	0.0	1.259	0.1563	0.0732	-0.0865	-0.0070	-0.0062
04T- 43	188	4	1.203	0.0	3.613	0.3773	0.0908	-0.1805	-0.0099	-0.0048
04T- 43	188	5	1.204	0.0	5.957	0.6015	0.1244	-0.2737	-0.0111	-0.0030
04T- 43	188	6	1.199	0.0	8.438	0.8412	0.1795	-0.3722	-0.0093	-0.0013
04T- 43	188	7	1.204	0.0	10.680	1.0345	0.2438	-0.4569	-0.0079	0.0001
04T- 43	188	8	1.203	0.0	13.036	1.2272	0.3268	-0.5502	-0.0072	0.0017
04T- 43	188	9	1.205	0.0	15.339	1.4022	0.4230	-0.6540	-0.0059	0.0030
04T- 43	188	10	1.204	0.0	17.567	1.5612	0.5297	-0.7598	-0.0036	0.0037
04T- 43	188	11	1.203	0.0	19.818	1.6943	0.6435	-0.8468	-0.0016	0.0034
04T- 43	188	12	1.205	0.0	22.025	1.8005	0.7596	-0.9262	0.0008	0.0026
04T- 43	191	1	0.898	0.0	-0.774	0.1234	0.0579	-0.0171	0.0015	-0.0017
04T- 43	191	2	0.901	0.0	4.084	0.6107	0.0974	-0.1020	0.0032	-0.0022
04T- 43	191	3	0.899	0.0	6.284	0.7825	0.1325	-0.1304	0.0032	-0.0023
04T- 43	191	4	0.898	0.0	8.613	0.9496	0.1787	-0.1725	0.0050	-0.0026
04T- 43	191	5	0.900	0.0	13.015	1.2703	0.3167	-0.2899	0.0050	-0.0028
04T- 43	191	6	0.900	0.0	21.721	1.7212	0.7181	-0.6445	-0.0009	0.0001
04T- 43	192	1	0.903	0.0	-0.703	0.1300	0.0588	-0.0191	0.0018	-0.0017
04T- 43	192	2	0.894	-0.0	-3.177	-0.0983	0.0669	-0.0109	0.0014	-0.0019
04T- 43	192	3	0.899	0.0	1.604	0.3746	0.0690	-0.0573	0.0048	-0.0023
04T- 43	192	4	0.904	0.0	3.996	0.6002	0.0960	-0.1014	0.0032	-0.0023
04T- 43	192	5	0.898	0.0	6.365	0.7895	0.1343	-0.1323	0.0030	-0.0022
04T- 43	192	6	0.900	0.0	8.575	0.9493	0.1791	-0.1734	0.0043	-0.0023
04T- 43	192	7	0.900	0.0	10.817	1.1191	0.2400	-0.2336	0.0056	-0.0025
04T- 43	192	8	0.898	0.0	13.072	1.2583	0.3146	-0.2910	0.0048	-0.0027
04T- 43	192	9	0.897	0.0	15.369	1.4065	0.4076	-0.3711	0.0011	-0.0027
04T- 43	192	10	0.898	0.0	17.393	1.5021	0.4953	-0.4487	0.0009	-0.0011
04T- 43	192	11	0.902	0.0	19.598	1.6135	0.6035	-0.5451	0.0021	-0.0025
04T- 43	192	12	0.900	0.0	21.795	1.7075	0.7138	-0.6289	-0.0005	0.0

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	193	1	0.807	0.0	-0.602	0.1873	0.0485	-0.0223	0.0041	-0.0019
04T- 43	193	2	0.802	0.0	-3.020	-0.0336	0.0562	-0.0013	0.0017	-0.0027
04T- 43	193	3	0.801	0.0	1.707	0.4190	0.0556	-0.0605	0.0034	-0.0021
04T- 43	193	4	0.799	0.0	4.034	0.6227	0.0776	-0.0867	0.0028	-0.0021
04T- 43	193	5	0.800	0.0	6.311	0.7848	0.1109	-0.0982	0.0043	-0.0021
04T- 43	193	6	0.804	0.0	8.545	0.9360	0.1521	-0.1155	0.0050	-0.0022
04T- 43	193	7	0.803	0.0	10.682	1.0834	0.2072	-0.1654	0.0018	-0.0016
04T- 43	193	8	0.800	0.0	12.943	1.2317	0.2822	-0.2214	0.0004	-0.0008
04T- 43	193	9	0.803	0.0	15.151	1.3543	0.3686	-0.2868	-0.0007	-0.0009
04T- 43	193	10	0.802	0.0	17.153	1.4413	0.4561	-0.3813	-0.0013	-0.0001
04T- 43	193	11	0.800	0.0	19.400	1.5652	0.5666	-0.4824	-0.0007	-0.0001
04T- 43	193	12	0.800	0.0	21.539	1.6648	0.6783	-0.5673	0.0003	-0.0016
04T- 43	193	13	0.801	0.0	23.520	1.7323	0.7746	-0.6142	0.0009	-0.0013
04T- 43	194	1	0.700	0.0	-0.632	0.1972	0.0441	-0.0246	0.0037	-0.0019
04T- 43	194	2	0.701	0.0	-3.092	-0.0216	0.0512	0.0016	0.0012	-0.0024
04T- 43	194	3	0.700	0.0	1.581	0.4014	0.0487	-0.0570	0.0029	-0.0020
04T- 43	194	4	0.699	0.0	3.969	0.6013	0.0667	-0.0842	0.0021	-0.0021
04T- 43	194	5	0.702	0.0	6.011	0.7551	0.0914	-0.1019	0.0015	-0.0020
04T- 43	194	6	0.700	0.0	8.348	0.9317	0.1320	-0.1271	0.0022	-0.0019
04T- 43	194	7	0.700	0.0	10.595	1.0932	0.1847	-0.1595	0.0019	-0.0018
04T- 43	194	8	0.699	0.0	12.748	1.2105	0.2555	-0.2125	0.0009	-0.0013
04T- 43	194	9	0.698	0.0	14.768	1.2717	0.3318	-0.2628	0.0009	-0.0010
04T- 43	194	10	0.698	0.0	16.887	1.4041	0.4242	-0.3372	-0.0029	0.0005
04T- 43	194	11	0.698	0.0	19.121	1.5319	0.5332	-0.4259	-0.0004	-0.0004
04T- 43	194	12	0.699	0.0	21.280	1.6360	0.6412	-0.5015	0.0011	-0.0015
04T- 43	194	13	0.699	0.0	23.339	1.7405	0.7541	-0.5720	0.0005	-0.0008
04T- 43	195	1	1.204	0.0	-0.850	0.0486	0.0900	-0.0372	0.0022	-0.0022
04T- 43	195	2	1.202	0.0	-3.263	-0.1597	0.0975	0.0394	0.0021	-0.0022
04T- 43	195	3	1.202	0.0	1.426	0.2539	0.0974	-0.1218	0.0023	-0.0020
04T- 43	195	4	1.200	0.0	3.758	0.4726	0.1182	-0.2037	0.0028	-0.0018
04T- 43	195	5	1.202	0.0	6.246	0.7192	0.1582	-0.2999	0.0031	-0.0022
04T- 43	195	6	1.203	0.0	8.502	0.9244	0.2099	-0.3868	0.0021	-0.0025
04T- 43	195	7	1.201	0.0	10.923	1.1284	0.2815	-0.4788	0.0019	-0.0029
04T- 43	195	8	1.202	0.0	13.196	1.3176	0.3676	-0.5805	0.0018	-0.0038
04T- 43	195	9	1.201	0.0	15.537	1.4962	0.4710	-0.6903	0.0013	-0.0045
04T- 43	195	10	1.202	0.0	17.718	1.6430	0.5776	-0.7859	0.0010	-0.0047
04T- 43	195	11	1.203	0.0	19.947	1.7755	0.6954	-0.8816	0.0008	-0.0043
04T- 43	195	12	1.201	0.0	21.329	1.8493	0.7721	-0.9414	0.0008	-0.0046
04T- 43	198	1	0.895	0.0	-0.724	0.1411	0.0592	-0.0256	0.0094	-0.0014
04T- 43	198	2	0.899	0.0	4.053	0.6023	0.0968	-0.0911	0.0139	-0.0027
04T- 43	198	3	0.899	0.0	6.287	0.7708	0.1313	-0.1223	0.0100	-0.0030
04T- 43	198	4	0.898	0.0	8.596	0.9314	0.1760	-0.1606	0.0085	-0.0032
04T- 43	198	5	0.898	0.0	13.087	1.2473	0.3131	-0.2839	0.0084	-0.0041
04T- 43	198	6	0.900	0.0	21.807	1.7073	0.7176	-0.6344	-0.0006	-0.0009
04T- 43	199	1	0.899	0.0	-0.755	0.1333	0.0595	-0.0243	0.0086	-0.0009
04T- 43	199	2	0.898	0.0	-3.118	-0.0891	0.0681	-0.0161	0.0035	-0.0017

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	199	3	0.899	0.0	1.607	0.3755	0.0707	-0.0562	0.0150	-0.0017
04T- 43	199	4	0.901	0.0	4.031	0.6003	0.0971	-0.0928	0.0138	-0.0023
04T- 43	199	5	0.902	0.0	6.273	0.7691	0.1312	-0.1231	0.0100	-0.0027
04T- 43	199	6	0.902	0.0	8.603	0.9324	0.1767	-0.1605	0.0082	-0.0031
04T- 43	199	7	0.897	0.0	10.791	1.0937	0.2350	-0.2083	0.0088	-0.0035
04T- 43	199	8	0.897	0.0	13.084	1.2473	0.3122	-0.2828	0.0083	-0.0038
04T- 43	199	9	0.901	0.0	15.415	1.4064	0.4101	-0.3698	0.0054	-0.0046
04T- 43	199	10	0.899	0.0	17.451	1.5042	0.4990	-0.4484	0.0043	-0.0026
04T- 43	199	11	0.900	0.0	19.490	1.5968	0.5977	-0.5476	0.0011	-0.0010
04T- 43	199	12	0.904	0.0	21.836	1.7182	0.7239	-0.6474	-0.0004	-0.0004
04T- 43	200	1	0.804	0.0	-0.647	0.1693	0.0504	-0.0225	0.0124	-0.0005
04T- 43	200	2	0.802	0.0	-3.016	-0.0480	0.0580	-0.0018	0.0070	-0.0007
04T- 43	200	3	0.802	0.0	1.759	0.4146	0.0581	-0.0600	0.0157	-0.0014
04T- 43	200	4	0.803	0.0	3.933	0.6050	0.0779	-0.0831	0.0155	-0.0022
04T- 43	200	5	0.800	0.0	6.191	0.7618	0.1094	-0.0948	0.0131	-0.0030
04T- 43	200	6	0.801	0.0	8.430	0.9140	0.1497	-0.1184	0.0117	-0.0040
04T- 43	200	7	0.798	0.0	10.747	1.0891	0.2105	-0.1696	0.0104	-0.0043
04T- 43	200	8	0.803	0.0	12.986	1.2441	0.2866	-0.2197	0.0090	-0.0044
04T- 43	200	9	0.804	0.0	15.107	1.3392	0.3669	-0.2870	0.0031	-0.0031
04T- 43	200	10	0.799	0.0	17.244	1.4433	0.4620	-0.3877	0.0022	-0.0016
04T- 43	200	11	0.805	0.0	19.255	1.5423	0.5581	-0.4776	0.0022	-0.0014
04T- 43	200	12	0.805	0.0	21.456	1.6519	0.6740	-0.5649	0.0021	-0.0013
04T- 43	200	13	0.797	0.0	23.518	1.7496	0.7845	-0.6270	0.0025	-0.0027
04T- 43	201	1	1.200	0.0	-0.883	0.0473	0.0932	-0.0443	0.0108	0.0001
04T- 43	201	2	1.202	0.0	3.880	0.4954	0.1231	-0.2242	0.0125	-0.0016
04T- 43	201	3	1.202	0.0	8.452	0.9264	0.2120	-0.3897	0.0096	-0.0040
04T- 43	201	4	1.201	0.0	13.224	1.3247	0.3719	-0.5833	0.0082	-0.0065
04T- 43	201	5	1.203	0.0	17.720	1.6469	0.5810	-0.7881	0.0059	-0.0076
04T- 43	201	6	1.204	0.0	21.186	1.8403	0.7655	-0.9364	0.0047	-0.0077
04T- 43	202	1	0.698	0.0	-0.700	0.1626	0.0446	-0.0184	0.0137	-0.0002
04T- 43	202	2	0.699	0.0	-2.988	-0.0397	0.0533	0.0041	0.0087	-0.0006
04T- 43	202	3	0.699	0.0	1.605	0.3815	0.0502	-0.0524	0.0157	-0.0010
04T- 43	202	4	0.698	0.0	3.826	0.5726	0.0666	-0.0800	0.0151	-0.0021
04T- 43	202	5	0.699	0.0	6.129	0.7594	0.0951	-0.1059	0.0140	-0.0033
04T- 43	202	6	0.698	0.0	8.250	0.9168	0.1313	-0.1284	0.0134	-0.0041
04T- 43	202	7	0.701	0.0	10.577	1.0976	0.1877	-0.1686	0.0130	-0.0049
04T- 43	202	8	0.699	0.0	12.737	1.1948	0.2561	-0.2154	0.0051	-0.0046
04T- 43	202	9	0.699	0.0	14.906	1.3010	0.3419	-0.2697	0.0043	-0.0040
04T- 43	202	10	0.700	0.0	17.046	1.4195	0.4361	-0.3471	0.0022	-0.0023
04T- 43	202	11	0.699	0.0	19.061	1.5292	0.5333	-0.4314	0.0036	-0.0026
04T- 43	202	12	0.699	0.0	21.245	1.6450	0.6473	-0.5139	0.0041	-0.0031
04T- 43	202	13	0.700	0.0	23.368	1.7578	0.7663	-0.5865	0.0034	-0.0030
04T- 43	205	1	0.897	0.0	-1.065	-0.0484	0.0603	-0.0540	0.0273	-0.0004
04T- 43	205	2	0.905	0.0	3.781	0.4544	0.0802	-0.1081	0.0322	-0.0016
04T- 43	205	3	0.898	0.0	6.060	0.6402	0.1071	-0.1348	0.0258	-0.0037
04T- 43	205	4	0.898	0.0	8.360	0.8200	0.1495	-0.1763	0.0231	-0.0048

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	205	5	0.896	0.0	12.909	1.1635	0.2801	-0.2855	0.0220	-0.0068
04T- 43	205	6	0.899	0.0	21.619	1.6479	0.6746	-0.6261	0.0117	-0.0072
04T- 43	206	1	0.858	0.0	-1.062	-0.0481	0.0601	-0.0521	0.0270	-0.0012
04T- 43	206	2	0.897	0.0	-3.688	-0.2873	0.0804	-0.0448	0.0240	-0.0019
04T- 43	206	3	0.898	0.0	1.308	0.2037	0.0604	-0.0816	0.0339	0.0008
04T- 43	206	4	0.900	0.0	3.721	0.4476	0.0783	-0.1066	0.0324	-0.0013
04T- 43	206	5	0.896	0.0	6.073	0.6404	0.1068	-0.1339	0.0255	-0.0036
04T- 43	206	6	0.901	0.0	8.403	0.8231	0.1507	-0.1769	0.0227	-0.0048
04T- 43	206	7	0.897	0.0	10.632	0.9842	0.2381	-0.2311	0.0242	-0.0059
04T- 43	206	8	0.899	0.0	12.911	1.1648	0.2811	-0.2894	0.0219	-0.0065
04T- 43	206	9	0.898	0.0	15.170	1.3131	0.3684	-0.3502	0.0194	-0.0078
04T- 43	206	10	0.893	0.0	17.289	1.4176	0.4547	-0.4252	0.0154	-0.0067
04T- 43	206	11	0.900	0.0	19.440	1.5283	0.5591	-0.5326	0.0129	-0.0061
04T- 43	207	1	0.799	0.0	-1.052	-0.0397	0.0542	-0.0486	0.0302	-0.0020
04T- 43	207	2	0.802	0.0	-3.454	-0.2352	0.0713	-0.0375	0.0243	-0.0013
04T- 43	207	3	0.799	0.0	1.272	0.1867	0.0497	-0.0767	0.0365	0.0014
04T- 43	207	4	0.802	0.0	3.619	0.4154	0.0621	-0.1089	0.0377	-0.0019
04T- 43	207	5	0.801	0.0	6.015	0.6231	0.0898	-0.1383	0.0331	-0.0037
04T- 43	207	6	0.800	0.0	8.291	0.7910	0.1264	-0.1651	0.0272	-0.0052
04T- 43	207	7	0.803	0.0	10.506	0.9736	0.1793	-0.2107	0.0260	-0.0069
04T- 43	207	8	0.803	0.0	12.744	1.1261	0.2478	-0.2559	0.0233	-0.0081
04T- 43	207	9	0.801	0.0	14.877	1.2307	0.3244	-0.3137	0.0208	-0.0087
04T- 43	207	10	0.804	0.0	17.073	1.3480	0.4190	-0.3913	0.0185	-0.0084
04T- 43	207	11	0.801	0.0	19.018	1.4617	0.5139	-0.4727	0.0169	-0.0085
04T- 43	208	1	0.700	0.0	-1.078	-0.0417	0.0505	-0.0424	0.0313	-0.0009
04T- 43	208	2	0.698	0.0	-3.418	-0.2266	0.0673	-0.0288	0.0252	-0.0011
04T- 43	208	3	0.701	0.0	1.220	0.1703	0.0457	-0.0711	0.0373	0.0002
04T- 43	208	4	0.700	0.0	3.513	0.3738	0.0536	-0.0999	0.0375	-0.0026
04T- 43	208	5	0.700	0.0	5.839	0.5739	0.0744	-0.1327	0.0366	-0.0038
04T- 43	208	6	0.699	0.0	8.061	0.7616	0.1081	-0.1682	0.0347	-0.0058
04T- 43	208	7	0.699	0.0	10.367	0.9492	0.1575	-0.2074	0.0322	-0.0079
04T- 43	208	8	0.698	0.0	12.511	1.0812	0.2185	-0.2437	0.0235	-0.0092
04T- 43	208	10	0.701	0.0	16.856	1.3156	0.3898	-0.3586	0.0180	-0.0089
04T- 43	208	11	0.700	0.0	18.978	1.4334	0.4875	-0.4303	0.0165	-0.0089
04T- 43	208	12	0.700	0.0	21.163	1.5614	0.6000	-0.5016	0.0161	-0.0100
04T- 43	208	13	0.701	0.0	22.133	1.6606	0.7035	-0.5606	0.0147	-0.0104
04T- 43	209	1	1.207	0.0	-1.068	-0.0639	0.0926	-0.0097	0.0192	0.0014
04T- 43	209	2	1.203	0.0	-3.545	-0.2844	0.1085	0.0770	0.0172	0.0031
04T- 43	209	3	1.203	0.0	1.217	0.1536	0.0928	-0.0995	0.0207	0.0013
04T- 43	209	4	1.201	0.0	3.603	0.3810	0.1086	-0.1900	0.0213	-0.0004
04T- 43	209	5	1.204	0.0	6.007	0.6164	0.1405	-0.2789	0.0209	-0.0025
04T- 43	209	6	1.202	0.0	8.398	0.8429	0.1904	-0.3624	0.0188	-0.0041
04T- 43	209	7	1.201	0.0	10.730	1.0428	0.2553	-0.4520	0.0190	-0.0063
04T- 43	209	8	1.203	0.0	13.080	1.2336	0.3366	-0.5481	0.0190	-0.0083
04T- 43	209	9	1.204	0.0	15.409	1.4153	0.4347	-0.6519	0.0175	-0.0096
04T- 43	209	10	1.203	0.0	17.577	1.5696	0.5385	-0.7513	0.0170	-0.0102

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	209	11	1.202	0.0	19.868	1.7083	0.6557	-0.8476	0.0160	-0.0120
04T- 43	209	12	1.203	0.0	22.033	1.8125	0.7690	-0.9312	0.0166	-0.0158
04T- 43	212	1	0.897	0.0	-0.861	0.0569	0.0436	-0.0409	0.0341	-0.0002
04T- 43	212	2	0.901	0.0	3.965	0.5371	0.0756	-0.0967	0.0308	-0.0031
04T- 43	212	3	0.898	0.0	6.322	0.7572	0.1167	-0.1244	0.0272	-0.0052
04T- 43	212	4	0.898	0.0	8.587	0.9120	0.1708	-0.1521	0.0252	-0.0065
04T- 43	212	5	0.901	0.0	12.950	1.1487	0.3058	-0.2676	0.0198	-0.0075
04T- 43	212	6	0.901	0.0	21.663	1.6444	0.7017	-0.6122	0.0118	-0.0071
04T- 43	213	1	0.899	0.0	-0.887	0.0525	0.0432	-0.0394	0.0338	0.0009
04T- 43	213	2	0.899	0.0	-3.460	-0.2370	0.0590	-0.0101	0.0349	-0.0015
04T- 43	213	3	0.898	0.0	1.518	0.2881	0.0511	-0.0643	0.0342	-0.0001
04T- 43	213	4	0.900	0.0	3.941	0.5341	0.0748	-0.0944	0.0309	-0.0025
04T- 43	213	5	0.898	0.0	6.290	0.7501	0.1160	-0.1208	0.0279	-0.0046
04T- 43	213	6	0.902	0.0	8.593	0.9120	0.1709	-0.1494	0.0248	-0.0059
04T- 43	213	7	0.895	0.0	10.712	1.0050	0.2278	-0.1932	0.0223	-0.0064
04T- 43	213	8	0.896	0.0	13.006	1.1489	0.3071	-0.2676	0.0211	-0.0071
04T- 43	213	9	0.899	0.0	15.095	1.2722	0.3880	-0.3568	0.0174	-0.0058
04T- 43	213	10	0.896	0.0	17.351	1.4132	0.4881	-0.4441	0.0153	-0.0055
04T- 43	213	11	0.899	0.0	19.485	1.5388	0.5924	-0.5294	0.0151	-0.0071
04T- 43	213	12	0.898	0.0	21.658	1.6493	0.7045	-0.6145	0.0120	-0.0065
04T- 43	214	1	0.800	0.0	-0.890	0.0436	0.0388	-0.0332	0.0365	0.0
04T- 43	214	2	0.799	0.0	-3.352	-0.1987	0.0507	-0.0064	0.0345	-0.0009
04T- 43	214	3	0.801	0.0	1.373	0.2510	0.0438	-0.0598	0.0369	0.0010
04T- 43	214	4	0.801	0.0	3.715	0.4566	0.0603	-0.0874	0.0369	-0.0014
04T- 43	214	5	0.801	0.0	6.063	0.6674	0.0935	-0.1127	0.0352	-0.0041
04T- 43	214	7	0.800	0.0	10.508	0.9534	0.2012	-0.1701	0.0238	-0.0067
04T- 43	214	8	0.798	0.0	12.692	1.0793	0.2720	-0.2273	0.0232	-0.0074
04T- 43	214	9	0.800	0.0	14.865	1.1946	0.3484	-0.2847	0.0205	-0.0069
04T- 43	214	11	0.800	0.0	19.218	1.4590	0.5439	-0.4590	0.0168	-0.0065
04T- 43	214	12	0.802	0.0	21.382	1.5737	0.6570	-0.5502	0.0150	-0.0076
04T- 43	215	1	0.712	0.0	-0.903	0.0337	0.0361	-0.0281	0.0379	0.0005
04T- 43	215	2	0.714	0.0	-3.345	-0.1945	0.0466	-0.0001	0.0349	0.0007
04T- 43	215	3	0.714	0.0	1.311	0.2251	0.0402	-0.0541	0.0380	0.0011
04T- 43	215	4	0.713	0.0	3.603	0.4160	0.0546	-0.0814	0.0377	-0.0017
04T- 43	215	5	0.712	0.0	5.895	0.6117	0.0810	-0.1094	0.0362	-0.0039
04T- 43	215	6	0.713	0.0	8.177	0.7905	0.1274	-0.1375	0.0330	-0.0062
04T- 43	215	8	0.710	0.0	12.524	1.0353	0.2494	-0.2013	0.0245	-0.0084
04T- 43	215	9	0.700	0.0	14.654	1.1553	0.3216	-0.2570	0.0199	-0.0076
04T- 43	215	10	0.701	0.0	16.796	1.2736	0.4051	-0.3369	0.0181	-0.0076
04T- 43	215	11	0.701	0.0	18.960	1.4060	0.5068	-0.4253	0.0165	-0.0077
04T- 43	215	12	0.700	0.0	21.141	1.5370	0.6220	-0.5104	0.0153	-0.0083
04T- 43	215	13	0.701	0.0	23.201	1.6379	0.7306	-0.5757	0.0144	-0.0097
04T- 43	215	14	0.701	0.0	10.366	0.9003	0.1829	-0.1661	0.0275	-0.0068
04T- 43	216	1	1.201	0.0	-0.928	-0.0099	0.0674	0.0110	0.0179	0.0017
04T- 43	216	2	1.202	0.0	-3.498	-0.2541	0.0805	0.1021	0.0168	0.0035

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	216	3	1.202	0.0	1.406	0.2244	0.0740	-0.0822	0.0203	-0.0001
04T- 43	216	4	1.201	0.0	3.795	0.4697	0.1002	-0.1837	0.0225	-0.0016
04T- 43	216	5	1.202	0.0	6.250	0.7114	0.1454	-0.2761	0.0209	-0.0035
04T- 43	216	6	1.201	0.0	8.596	0.9219	0.2051	-0.3571	0.0195	-0.0049
04T- 43	216	7	1.202	0.0	10.892	1.1131	0.2785	-0.4470	0.0191	-0.0068
04T- 43	216	8	1.202	0.0	13.207	1.2933	0.3677	-0.5416	0.0185	-0.0081
04T- 43	216	9	1.202	0.0	15.472	1.4551	0.4679	-0.6459	0.0185	-0.0102
04T- 43	216	10	1.204	0.0	17.689	1.5866	0.5721	-0.7348	0.0189	-0.0136
04T- 43	216	11	1.201	0.0	19.880	1.7110	0.6866	-0.8309	0.0165	-0.0131
04T- 43	216	12	1.204	0.0	22.065	1.8124	0.8032	-0.9182	0.0166	-0.0152
04T- 43	219	1	0.898	0.0	-1.005	-0.0157	0.0506	-0.0390	0.0316	-0.0007
04T- 43	219	2	0.899	0.0	3.845	0.4990	0.0750	-0.1033	0.0290	-0.0033
04T- 43	219	3	0.898	0.0	6.203	0.7172	0.1107	-0.1350	0.0235	-0.0053
04T- 43	219	4	0.898	0.0	8.640	0.9188	0.1641	-0.1716	0.0226	-0.0069
04T- 43	219	5	0.901	0.0	12.957	1.1661	0.2943	-0.2710	0.0172	-0.0068
04T- 43	219	6	0.898	0.0	21.612	1.6428	0.6882	-0.6284	0.0119	-0.0094
04T- 43	220	1	0.897	0.0	-0.978	-0.0136	0.0501	-0.0367	0.0314	-0.0006
04T- 43	220	2	0.899	0.0	-3.536	-0.2676	0.0679	-0.0176	0.0267	-0.0009
04T- 43	220	3	0.897	0.0	1.403	0.2542	0.0537	-0.0732	0.0344	-0.0002
04T- 43	220	4	0.895	0.0	3.816	0.4946	0.0742	-0.0997	0.0294	-0.0027
04T- 43	220	5	0.901	0.0	6.253	0.7201	0.1112	-0.1323	0.0232	-0.0048
04T- 43	220	6	0.899	0.0	8.532	0.9080	0.1611	-0.1655	0.0231	-0.0065
04T- 43	220	7	0.900	0.0	10.767	1.0527	0.2222	-0.2154	0.0236	-0.0066
04T- 43	220	8	0.900	0.0	12.997	1.1646	0.2945	-0.2680	0.0173	-0.0062
04T- 43	220	9	0.898	0.0	15.095	1.2731	0.3742	-0.3460	0.0174	-0.0075
04T- 43	220	10	0.902	0.0	17.289	1.4044	0.4725	-0.4505	0.0159	-0.0083
04T- 43	220	11	0.894	0.0	19.403	1.5193	0.5706	-0.5351	0.0139	-0.0071
04T- 43	220	12	0.898	0.0	21.617	1.6434	0.6889	-0.6254	0.0121	-0.0086
04T- 43	221	1	0.802	0.0	-0.965	-0.0056	0.0451	-0.0331	0.0345	0.0012
04T- 43	221	2	0.800	0.0	-3.409	-0.2277	0.0609	-0.0102	0.0275	-0.0009
04T- 43	221	3	0.798	0.0	1.392	0.2308	0.0454	-0.0642	0.0372	0.0015
04T- 43	221	4	0.800	0.0	3.687	0.4382	0.0606	-0.0904	0.0372	-0.0010
04T- 43	221	5	0.802	0.0	6.015	0.6494	0.0883	-0.1243	0.0365	-0.0031
04T- 43	221	6	0.801	0.0	8.359	0.8553	0.1340	-0.1553	0.0343	-0.0053
04T- 43	221	7	0.798	0.0	10.564	0.9916	0.1921	-0.1861	0.0281	-0.0064
04T- 43	221	8	0.799	0.0	12.714	1.0836	0.2596	-0.2318	0.0231	-0.0069
04T- 43	221	9	0.802	0.0	14.942	1.2087	0.3432	-0.3048	0.0217	-0.0072
04T- 43	221	10	0.801	0.0	17.024	1.3298	0.4293	-0.3790	0.0198	-0.0067
04T- 43	221	11	0.801	0.0	19.228	1.4616	0.5341	-0.4656	0.0187	-0.0090
04T- 43	221	12	0.803	0.0	21.392	1.5801	0.6463	-0.5470	0.0165	-0.0093
04T- 43	222	1	0.711	0.0	-0.959	-0.0054	0.0428	-0.0307	0.0363	0.0004
04T- 43	222	2	0.700	0.0	-3.347	-0.2147	0.0572	-0.0067	0.0296	0.0001
04T- 43	222	3	0.700	0.0	1.780	0.1998	0.0416	-0.0563	0.0377	0.0017
04T- 43	222	4	0.700	0.0	3.568	0.3918	0.0532	-0.0825	0.0375	-0.0002
04T- 43	222	5	0.699	0.0	5.820	0.5819	0.0756	-0.1139	0.0370	-0.0025
04T- 43	222	6	0.702	0.0	8.123	0.7735	0.1117	-0.1447	0.0348	-0.0048

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	222	7	0.700	0.0	10.414	0.9383	0.1706	-0.1834	0.0288	-0.0067
04T- 43	222	8	0.702	0.0	12.498	1.0489	0.2387	-0.2190	0.0253	-0.0074
04T- 43	222	9	0.699	0.0	14.654	1.1762	0.3154	-0.2713	0.0209	-0.0075
04T- 43	222	10	0.697	0.0	16.866	1.2888	0.4418	-0.3436	0.0178	-0.0068
04T- 43	222	11	0.700	0.0	18.986	1.4299	0.5038	-0.4261	0.0181	-0.0084
04T- 43	222	12	0.699	0.0	21.157	1.5507	0.6120	-0.4983	0.0156	-0.0078
04T- 43	223	1	1.202	0.0	-1.026	-0.0534	0.0786	0.0093	0.0188	0.0025
04T- 43	223	2	1.201	0.0	-3.476	-0.2763	0.0936	0.0969	0.0173	0.0040
04T- 43	223	3	1.202	0.0	1.295	0.1754	0.0806	-0.0854	0.0211	0.0011
04T- 43	223	4	1.202	0.0	3.679	0.4138	0.0998	-0.1800	0.0219	-0.0007
04T- 43	223	5	1.201	0.0	6.108	0.6558	0.1390	-0.2697	0.0206	-0.0027
04T- 43	223	6	1.202	0.0	8.458	0.8681	0.1925	-0.3478	0.0191	-0.0038
04T- 43	223	7	1.204	0.0	10.795	1.0682	0.2618	-0.4422	0.0190	-0.0056
04T- 43	223	8	1.203	0.0	13.133	1.2596	0.3487	-0.5412	0.0183	-0.0075
04T- 43	223	9	1.204	0.0	15.415	1.4306	0.4470	-0.6452	0.0174	-0.0089
04T- 43	223	10	1.203	0.0	17.683	1.5857	0.5576	-0.7485	0.0165	-0.0095
04T- 43	223	11	1.202	0.0	19.883	1.7119	0.6707	-0.8398	0.0159	-0.0106
04T- 43	223	12	1.203	0.0	22.031	1.8162	0.7861	-0.9248	0.0158	-0.0131
04T- 43	226	1	0.897	0.0	-1.107	-0.0384	0.0559	-0.0305	0.0419	-0.0027
04T- 43	226	2	0.899	0.0	3.788	0.4937	0.0794	-0.1010	0.0362	-0.0046
04T- 43	226	3	0.901	0.0	6.259	0.7200	0.1171	-0.1305	0.0302	-0.0068
04T- 43	226	4	0.896	0.0	8.518	0.8987	0.1643	-0.1600	0.0281	-0.0084
04T- 43	226	5	0.898	0.0	12.939	1.1477	0.2951	-0.2665	0.0277	-0.0093
04T- 43	226	6	0.895	0.0	21.562	1.6131	0.6795	-0.6094	0.0181	-0.0115
04T- 43	226	7	0.897	0.0	23.666	1.7119	0.7927	-0.6799	0.0155	-0.0134
04T- 43	227	1	0.902	0.0	-1.111	-0.0457	0.0553	-0.0223	0.0405	-0.0020
04T- 43	227	2	0.899	0.0	-3.538	-0.2938	0.0714	-0.0013	0.0327	-0.0023
04T- 43	227	3	0.896	0.0	1.401	0.2487	0.0588	-0.0685	0.0438	-0.0006
04T- 43	227	4	0.901	0.0	3.896	0.5044	0.0805	-0.1002	0.0354	-0.0041
04T- 43	227	5	0.898	0.0	6.286	0.7202	0.1157	-0.1270	0.0304	-0.0064
04T- 43	227	9	0.896	0.0	15.044	1.2608	0.3748	-0.3453	0.0235	-0.0092
04T- 43	227	10	0.898	0.0	17.289	1.4018	0.4753	-0.4432	0.0212	-0.0098
04T- 43	227	11	0.896	0.0	19.358	1.5008	0.5689	-0.5320	0.0202	-0.0090
04T- 43	227	13	0.895	0.0	23.659	1.7274	0.8004	-0.6906	0.0162	-0.0128
04T- 43	227	14	0.901	0.0	10.762	1.0592	0.2303	-0.2083	0.0300	-0.0087
04T- 43	228	1	0.797	0.0	-1.030	-0.0176	0.0496	-0.0279	0.0460	-0.0010
04T- 43	228	2	0.805	0.0	-3.458	-0.2493	0.0656	-0.0003	0.0344	-0.0013
04T- 43	228	3	0.797	0.0	1.331	0.2231	0.0497	-0.0610	0.0485	-0.0
04T- 43	228	4	0.803	0.0	3.777	0.4489	0.0666	-0.0912	0.0466	-0.0024
04T- 43	228	5	0.801	0.0	6.050	0.6489	0.0927	-0.1225	0.0441	-0.0045
04T- 43	228	6	0.801	0.0	8.302	0.8412	0.1362	-0.1502	0.0389	-0.0068
04T- 43	228	7	0.802	0.0	10.574	0.9813	0.1961	-0.1860	0.0338	-0.0080
04T- 43	228	8	0.804	0.0	12.713	1.0984	0.2653	-0.2328	0.0304	-0.0089
04T- 43	228	9	0.804	0.0	14.871	1.1947	0.3431	-0.3054	0.0273	-0.0086
04T- 43	228	10	0.797	0.0	17.038	1.3205	0.4325	-0.3799	0.0262	-0.0088
04T- 43	228	11	0.800	0.0	19.190	1.4420	0.5316	-0.4585	0.0265	-0.0133

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T-43	228	12	0.801	0.0	21.293	1.5572	0.6404	-0.5400	0.0250	-0.0120
04T-43	229	1	0.698	0.0	-1.058	-0.0236	0.0468	-0.0228	0.0472	-0.0011
04T-43	229	2	0.699	0.0	-3.400	-0.2285	0.0610	0.0009	0.0376	-0.0009
04T-43	229	4	0.700	0.0	3.642	0.3941	0.0579	-0.0784	0.0484	-0.0022
04T-43	229	5	0.698	0.0	5.772	0.5712	0.0792	-0.1073	0.0467	-0.0039
04T-43	229	6	0.700	0.0	8.080	0.7634	0.1151	-0.1392	0.0434	-0.0065
04T-43	229	7	0.697	0.0	10.309	0.9241	0.1718	-0.1782	0.0385	-0.0086
04T-43	229	8	0.698	0.0	12.510	1.0447	0.2426	-0.2170	0.0350	-0.0097
04T-43	229	9	0.697	0.0	14.610	1.1528	0.3142	-0.2684	0.0294	-0.0098
04T-43	229	10	0.698	0.0	16.806	1.2735	0.4000	-0.3378	0.0273	-0.0099
04T-43	229	11	0.699	0.0	18.936	1.4022	0.4990	-0.4184	0.0277	-0.0115
04T-43	229	12	0.700	0.0	21.178	1.5349	0.6135	-0.4957	0.0253	-0.0118
04T-43	230	1	1.201	0.0	-1.122	-0.0588	0.0819	0.0135	0.0255	0.0022
04T-43	230	2	1.200	0.0	-3.372	-0.2632	0.0962	0.0938	0.0242	0.0033
04T-43	230	3	1.202	0.0	1.285	0.1805	0.0854	-0.0857	0.0291	0.0006
04T-43	230	4	1.202	0.0	3.648	0.4187	0.1046	-0.1810	0.0305	-0.0018
04T-43	230	5	1.201	0.0	6.088	0.6609	0.1443	-0.2693	0.0288	-0.0043
04T-43	230	6	1.201	0.0	8.509	0.8784	0.1990	-0.3489	0.0264	-0.0061
04T-43	230	8	1.199	0.1	~~9.179~~	~~-0.4813~~	-0.0446	-0.4787	0.0245	-0.0114
04T-43	230	9	1.197	0.0	15.391	1.4375	0.4530	-0.6443	0.0233	-0.0130
04T-43	230	10	1.204	0.0	17.695	1.5807	0.5602	-0.7409	0.0215	-0.0138
04T-43	230	11	1.199	0.0	19.848	1.7084	0.6725	-0.8319	0.0209	-0.0153
04T-43	230	12	1.203	0.0	22.137	1.8157	0.7940	-0.9211	0.0201	-0.0179
04T-43	230	13	1.200	0.0	10.798	1.0759	0.2668	-0.4392	0.0263	-0.0078
04T-43	230	14	1.203	0.5	-0.893	0.0137	0.0555	0.0134	-0.0086	-0.0565
04T-43	232	1	0.898	0.6	-1.018	-0.0708	1.0531	-0.0441	-0.0072	-0.1319
04T-43	232	3	0.893	0.0	1.228	0.2357	0.0579	-0.0699	0.0458	0.0004
04T-43	232	4	0.899	0.0	3.460	0.4675	0.0757	-0.0996	0.0380	-0.0031
04T-43	232	5	0.691	0.8	1.517	7.9760	0.4265	-6.9969	-0.0119	-0.1617
04T-43	232	6	0.895	0.7	9.915	5.6238	1.0765	-4.4358	-0.0126	-0.1652
04T-43	232	10	0.896	0.0	16.308	1.3435	0.4322	-0.4294	0.0237	-0.0087
04T-43	232	11	0.895	0.0	18.352	1.4631	0.5276	-0.5259	0.0225	-0.0089
04T-43	232	14	0.898	0.0	9.985	1.0163	0.2091	-0.2047	0.0297	-0.0084
04T-43	232	15	0.896	0.8	-0.931	0.0458	0.1249	0.0050	-0.0104	-0.1441
04T-43	233	2	0.798	0.0	-3.233	-0.2235	0.0627	-0.0131	0.0363	0.0033
04T-43	233	3	0.801	0.0	1.260	0.2244	0.0502	-0.0724	0.0496	0.0013
04T-43	233	4	0.801	0.0	3.394	0.4187	0.0632	-0.0981	0.0475	-0.0018
04T-43	233	5	0.801	0.0	5.529	0.6062	0.0872	-0.1271	0.0449	-0.0047
04T-43	233	6	0.613	1.0	-0.935	0.1276	0.1196	-0.0609	-0.0050	-0.2209
04T-43	233	8	0.803	0.0	11.948	1.0492	0.2409	-0.2361	0.0303	-0.0101
04T-43	233	10	0.802	1.0	~~18.204~~	6.1278	2.1105	-4.9203	-0.0693	-0.2362
04T-43	233	11	0.801	0.0	18.259	1.4049	0.4949	-0.4650	0.0273	-0.0110
04T-43	233	12	0.798	0.0	20.340	1.5231	0.5992	-0.5527	0.0269	-0.0126
04T-43	233	13	0.798	0.0	22.308	1.6229	0.7032	-0.6275	0.0243	-0.0120
04T-43	233	14	0.797	0.0	9.860	0.9466	0.1780	-0.1913	0.0330	-0.0089
04T-43	233	15	0.800	0.0	-1.021	-0.0069	0.0496	-0.0387	0.0471	0.0039

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	234	1	0.700	0.0	-1.016	-0.0057	0.0461	-0.0401	0.0489	0.0047
04T- 43	234	2	0.696	-0.0	-3.215	-0.2057	0.0583	-0.0173	0.0389	0.0067
04T- 43	234	3	0.698	0.0	1.175	0.1984	0.0456	-0.0678	0.0515	0.0022
04T- 43	234	4	0.695	0.0	3.326	0.3800	0.0556	-0.0925	0.0495	-0.0009
04T- 43	234	6	0.697	0.0	7.606	0.7283	0.1075	-0.1508	0.0438	-0.0070
04T- 43	234	7	0.698	0.0	9.732	0.8827	0.1587	-0.1891	0.0374	-0.0097
04T- 43	234	10	0.698	0.0	16.009	1.2349	0.3697	-0.3412	0.0271	-0.0111
04T- 43	234	12	0.694	0.0	20.162	1.4831	0.5642	-0.5019	0.0270	-0.0136
04T- 43	234	13	0.696	0.0	22.176	1.5847	0.6655	-0.5720	0.0241	-0.0122
04T- 43	235	1	1.198	0.0	-1.015	-0.0287	0.0787	-0.0035	0.0255	-0.0082
04T- 43	235	2	1.197	-0.0	-3.190	-0.2294	0.0988	0.0708	0.0253	0.0031
04T- 43	235	4	1.200	0.0	3.376	0.4053	0.1020	-0.1789	0.0322	-0.0022
04T- 43	235	5	1.202	0.0	5.625	0.6241	0.1363	-0.2593	0.0304	-0.0043
04T- 43	235	7	1.201	0.0	10.020	1.0159	0.2451	-0.4187	0.0270	-0.0075
04T- 43	235	9	1.204	0.0	14.343	1.3700	0.4111	-0.6220	0.0246	-0.0130
04T- 43	235	10	1.198	0.0	16.515	1.5221	0.5115	-0.7134	0.0231	-0.0146
04T- 43	235	11	1.201	0.0	18.629	1.6508	0.6164	-0.8059	0.0220	-0.0151
04T- 43	235	12	1.202	0.0	20.709	1.7627	0.7266	-0.8999	0.0215	-0.0175
04T- 43	235	13	1.200	0.0	22.702	1.8520	0.8356	-0.9911	0.0228	-0.0221
04T- 43	235	14	1.201	0.0	9.989	1.0228	0.2442	-0.4225	0.0270	-0.0076
04T- 43	235	15	1.197	-0.0	-1.053	-0.0339	0.0819	-0.0053	0.0279	0.0021
04T- 43	236	1	0.894	0.0	-1.173	-0.0521	0.0534	-0.0282	0.0394	-0.0021
04T- 43	236	2	0.900	0.0	-3.763	-0.3123	0.0749	-0.0053	0.0315	-0.0045
04T- 43	236	3	0.899	0.0	1.472	0.2522	0.0594	-0.0723	0.0425	-0.0004
04T- 43	236	4	0.899	0.0	4.151	0.5250	0.0833	-0.1059	0.0350	-0.0034
04T- 43	236	5	0.904	0.0	6.582	0.7426	0.1227	-0.1366	0.0301	-0.0056
04T- 43	236	6	0.899	0.0	9.016	0.9312	0.1779	-0.1683	0.0292	-0.0072
04T- 43	236	7	0.900	0.0	11.356	1.0914	0.2482	-0.2222	0.0300	-0.0082
04T- 43	236	9	0.892	0.0	11.286	1.0808	0.2437	-0.2160	0.0322	-0.0082
04T- 43	237	2	0.802	0.0	-3.453	-0.2421	0.0661	-0.0080	0.0341	-0.0024
04T- 43	237	5	0.801	0.0	6.335	0.6784	0.0978	-0.1313	0.0431	-0.0046
04T- 43	237	6	0.801	0.0	8.703	0.8723	0.1466	-0.1599	0.0380	-0.0064
04T- 43	237	7	0.802	0.0	10.895	0.9976	0.2062	-0.1960	0.0316	-0.0075
04T- 43	237	8	0.801	0.0	13.187	1.1099	0.2824	-0.2454	0.0304	-0.0089
04T- 43	237	9	0.803	0.0	15.267	1.2256	0.3617	-0.3205	0.0284	-0.0088
04T- 43	237	12	0.801	0.0	-1.145	-0.0317	0.0509	-0.0299	0.0435	-0.0014
04T- 43	240	1	0.890	0.0	-1.034	0.0457	0.0393	-0.0572	0.0009	-0.0024
04T- 43	240	2	0.891	0.0	3.818	0.5034	0.0637	-0.0909	0.0020	-0.0027
04T- 43	240	3	0.891	0.0	6.290	0.7240	0.1018	-0.1283	0.0012	-0.0023
04T- 43	240	4	0.889	0.0	8.617	0.9156	0.1523	-0.1658	0.0018	-0.0017
04T- 43	240	5	0.889	0.0	12.842	1.1803	0.2812	-0.2706	0.0029	-0.0016
04T- 43	240	6	0.885	0.0	21.668	1.6747	0.6883	-0.6374	0.0003	-0.0021
04T- 43	241	1	0.895	0.0	-0.940	0.0525	0.0391	-0.0564	0.0005	-0.0022
04T- 43	241	2	0.890	0.0	-3.416	-0.1562	0.0537	-0.0584	0.0010	-0.0031
04T- 43	241	3	0.892	0.0	1.407	0.2773	0.0418	-0.0692	0.0012	-0.0021

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	241	4	0.898	0.0	3.748	0.4875	0.0616	-0.0867	0.0016	-0.0022
04T- 43	241	5	0.903	0.0	6.225	0.7124	0.1009	-0.1281	0.0015	-0.0023
04T- 43	241	6	0.894	0.0	8.460	0.8978	0.1477	-0.1614	0.0016	-0.0016
04T- 43	241	7	0.899	0.0	10.780	1.0715	0.2147	-0.2085	0.0017	-0.0013
04T- 43	241	8	0.900	0.0	12.920	1.1858	0.2837	-0.2820	0.0	-0.0002
04T- 43	241	9	0.899	0.0	15.150	1.3035	0.3699	-0.3592	0.0004	-0.0009
04T- 43	241	10	0.900	0.0	17.207	1.4093	0.4569	-0.4506	0.0006	-0.0013
04T- 43	241	11	0.901	0.0	19.548	1.5459	0.5710	-0.5500	0.0005	-0.0017
04T- 43	241	12	0.899	0.0	21.673	1.6606	0.6838	-0.6353	0.0005	-0.0021
04T- 43	242	1	0.800	0.0	-0.896	0.0499	0.0345	-0.0471	0.0018	-0.0026
04T- 43	242	2	0.799	0.0	-3.349	-0.1535	0.0483	-0.0360	0.0019	-0.0031
04T- 43	242	4	0.799	0.0	3.802	0.4577	0.0508	-0.0786	-0.0003	-0.0024
04T- 43	242	5	0.800	0.0	6.118	0.6626	0.0783	-0.1108	-0.0021	-0.0022
04T- 43	242	6	0.801	0.0	8.380	0.8514	0.1216	-0.1426	0.0011	-0.0016
04T- 43	242	7	0.801	0.0	10.514	0.9948	0.1802	-0.1787	0.0032	-0.0010
04T- 43	242	8	0.801	0.0	12.645	1.1028	0.2497	-0.2420	0.0034	-0.0009
04T- 43	242	10	0.802	0.0	17.034	1.3562	0.4235	-0.3872	-0.0001	-0.0002
04T- 43	242	11	0.799	0.0	19.176	1.4786	0.5249	-0.4768	0.0019	-0.0020
04T- 43	242	12	0.798	0.0	21.309	1.5918	0.6345	-0.5560	0.0008	-0.0020
04T- 43	243	1	0.700	0.0	-0.924	0.0420	0.0320	-0.0405	0.0018	-0.0025
04T- 43	243	2	0.697	0.0	-3.346	-0.1574	0.0458	-0.0280	0.0020	-0.0034
04T- 43	243	3	0.699	0.0	1.314	0.2334	0.0319	-0.0547	0.0014	-0.0023
04T- 43	243	4	0.701	0.0	3.645	0.4231	0.0450	-0.0767	0.0003	-0.0024
04T- 43	243	5	0.699	0.0	5.941	0.6120	0.0682	-0.1076	-0.0016	-0.0022
04T- 43	243	6	0.698	0.0	8.095	0.7919	0.1024	-0.1407	0.0005	-0.0016
04T- 43	243	7	0.702	0.0	10.325	0.9420	0.1582	-0.1779	0.0019	-0.0007
04T- 43	243	8	0.702	0.0	12.553	1.0680	0.2316	-0.2217	0.0011	-0.0004
04T- 43	243	9	0.699	0.0	14.660	1.1940	0.3085	-0.2773	-0.0005	-0.0001
04T- 43	243	10	0.699	0.0	16.857	1.3195	0.3979	-0.3525	-0.0005	0.0011
04T- 43	243	11	0.699	0.0	19.072	1.4509	0.5024	-0.4369	0.0004	-0.0001
04T- 43	243	12	0.697	0.0	21.113	1.5593	0.6034	-0.5067	0.0001	-0.0004
04T- 43	243	13	0.700	0.0	-1.005	0.0342	0.0322	-0.0388	0.0018	-0.0025
04T- 43	244	1	0.900	0.0	-1.024	0.0329	0.0415	-0.0539	-0.0005	-0.0028
04T- 43	244	2	0.900	0.0	-3.423	-0.1604	0.0562	-0.0573	0.0008	-0.0035
04T- 43	244	3	0.901	0.0	1.546	0.2797	0.0439	-0.0663	0.0003	-0.0024
04T- 43	244	4	0.901	0.0	4.093	0.5091	0.0670	-0.0864	-0.0004	-0.0023
04T- 43	244	5	0.899	0.0	6.586	0.7271	0.1065	-0.1246	-0.0016	-0.0019
04T- 43	244	6	0.899	0.0	8.891	0.9230	0.1603	-0.1671	0.0001	-0.0016
04T- 43	244	7	0.904	0.0	11.439	1.1126	0.2373	-0.2243	0.0001	-0.0014
04T- 43	245	1	0.800	0.0	-0.977	0.0355	0.0363	-0.0456	0.0015	-0.0028
04T- 43	245	2	0.803	0.0	-3.475	-0.1561	0.0512	-0.0364	0.0020	-0.0034
04T- 43	245	4	0.798	0.0	3.808	0.4510	0.0515	-0.0769	-0.0009	-0.0024
04T- 43	245	3	0.801	0.0	1.541	0.2580	0.0380	-0.0580	0.0001	-0.0025
04T- 43	245	5	0.800	0.0	6.213	0.6631	0.0639	-0.1097	-0.0029	-0.0022
04T- 43	245	6	0.798	0.0	8.632	0.8587	0.1274	-0.1426	0.0001	-0.0015
04T- 43	245	7	0.801	0.0	10.830	0.9980	0.1873	-0.1814	0.0002	-0.0008

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	245	8	0.802	0.0	13.039	1.1129	0.2623	-0.2404	0.0001	-0.0005
04T- 43	245	9	0.799	0.0	17.828	1.3986	0.4577	-0.4060	0.0001	-0.0005
04T- 43	246	1	1.202	0.0	-1.147	-0.0669	0.0663	0.0096	0.0019	-0.0030
04T- 43	246	2	1.202	0.0	3.724	0.4123	0.0862	-0.1927	0.0007	-0.0027
04T- 43	246	3	1.202	0.0	8.343	0.8695	0.1782	-0.3748	-0.0	-0.0028
04T- 43	246	4	1.201	0.0	12.992	1.2656	0.3350	-0.5622	-0.0011	-0.0033
04T- 43	246	5	1.201	0.0	17.588	1.6067	0.5491	-0.7813	-0.0018	-0.0032
04T- 43	246	6	1.205	0.0	21.913	1.8399	0.7786	-0.9494	-0.0022	-0.0043
04T- 43	246	7	1.205	0.0	10.864	1.0854	0.2534	-0.4672	-0.0007	-0.0025
04T- 43	246	8	1.205	0.0	-1.144	-0.0661	0.0663	0.0103	0.0019	-0.0027
04T- 43	247	1	0.896	-0.0	-1.013	0.0353	0.0417	-0.0459	-0.0019	-0.0030
04T- 43	247	2	0.900	0.0	-3.210	-0.1370	0.0549	-0.0551	0.0009	-0.0034
04T- 43	247	3	0.900	0.0	1.165	0.2414	0.0426	-0.0571	-0.0022	-0.0028
04T- 43	247	4	0.896	0.0	3.397	0.4443	0.0599	-0.0719	-0.0024	-0.0025
04T- 43	247	5	0.898	0.0	5.737	0.6538	0.0926	-0.1058	-0.0023	-0.0026
04T- 43	247	6	0.898	0.0	7.792	0.8344	0.1343	-0.1458	-0.0019	-0.0025
04T- 43	247	7	0.898	0.0	9.914	1.0016	0.1902	-0.1852	-0.0007	-0.0023
04T- 43	247	8	0.902	0.0	12.187	1.1351	0.2604	-0.2575	0.0043	-0.0029
04T- 43	247	9	0.899	0.0	14.099	1.2233	0.3257	-0.3292	0.0005	-0.0013
04T- 43	247	10	0.897	0.0	16.263	1.3546	0.4175	-0.4299	0.0	-0.0012
04T- 43	247	11	0.889	0.0	18.424	1.4663	0.5116	-0.5185	0.0002	-0.0014
04T- 43	247	12	0.896	0.0	18.440	1.4795	0.5182	-0.5292	0.0002	-0.0013
04T- 43	247	13	0.900	0.0	20.364	1.5987	0.6209	-0.6183	0.0004	-0.0015
04T- 43	247	14	0.893	0.0	10.020	1.0051	0.1910	-0.1846	-0.0003	-0.0019
04T- 43	248	1	0.800	-0.0	-1.009	0.0381	0.0363	-0.0423	0.0011	-0.0026
04T- 43	248	2	0.799	-0.0	-3.207	-0.1429	0.0484	-0.0339	0.0016	-0.0028
04T- 43	248	3	0.798	0.0	1.126	0.2295	0.0362	-0.0561	0.0001	-0.0025
04T- 43	248	4	0.799	0.0	3.342	0.4114	0.0498	-0.0711	-0.0013	-0.0025
04T- 43	248	5	0.798	0.0	5.589	0.6046	0.0727	-0.1013	-0.0031	-0.0022
04T- 43	248	6	0.798	0.0	7.696	0.7865	0.1080	-0.1339	-0.0008	-0.0020
04T- 43	248	7	0.800	0.0	9.802	0.9426	0.1598	-0.1682	-0.0003	-0.0018
04T- 43	248	8	0.799	0.0	11.983	1.0464	0.2269	-0.2257	0.0003	-0.0015
04T- 43	248	9	0.797	0.0	13.993	1.1697	0.3001	-0.2931	-0.0011	-0.0010
04T- 43	248	10	0.797	0.0	16.143	1.2987	0.3851	-0.3710	-0.0002	-0.0010
04T- 43	248	11	0.795	0.0	16.124	1.3008	0.3863	-0.3715	-0.0001	-0.0010
04T- 43	248	12	0.796	0.0	18.275	1.4311	0.4854	-0.4653	0.0007	-0.0016
04T- 43	248	13	0.796	0.0	20.223	1.5441	0.5852	-0.5513	0.0011	-0.0025
04T- 43	248	14	0.797	0.0	9.841	0.9438	0.1600	-0.1690	-0.0001	-0.0018
04T- 43	248	15	0.796	-0.0	-0.965	0.0430	0.0363	-0.0434	0.0013	-0.0026
04T- 43	249	1	0.698	-0.0	-0.965	0.0403	0.0361	-0.0381	0.0016	-0.0023
04T- 43	249	2	0.698	-0.0	-3.122	-0.1372	0.0448	-0.0288	0.0017	-0.0025
04T- 43	249	3	0.698	0.0	1.130	0.2199	0.0331	-0.0531	0.0010	-0.0019
04T- 43	249	4	0.699	0.0	3.3[illegible]1	0.3968	0.0448	-0.0725	-0.0001	-0.0022
04T- 43	249	5	0.700	0.0	5.527	0.5709	0.0653	-0.1015	-0.0016	-0.0021
04T- 43	249	7	0.699	-0.0	-0.987	0.0383	0.0335	-0.0382	0.0015	-0.0023
04T- 43	249	8	0.698	0.0	3.267	0.3913	0.0440	-0.0711	-0.0	-0.0021

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T-	43	249	9 0.697	0.0	7.579	0.7354	0.0946	-0.1330	-0.0016	-0.0019
04T-	43	249	10 0.697	0.0	9.719	0.8966	0.1443	-0.1717	-0.0007	-0.0015
04T-	43	249	11 0.698	0.0	11.841	1.0231	0.2114	-0.2156	-0.0001	-0.0013
04T-	43	249	12 0.697	0.0	13.950	1.1515	0.2835	-0.2657	0.0004	-0.0013
04T-	43	249	13 0.696	0.0	16.070	1.2688	0.3651	-0.3378	-0.0009	-0.0002
04T-	43	249	14 0.697	0.0	18.062	1.3832	0.4533	-0.4190	-0.0004	-0.0002
04T-	43	249	15 0.696	0.0	20.145	1.5052	0.5565	-0.5009	0.0	-0.0011
04T-	43	250	1 1.203	-0.0	-1.057	-0.0389	0.0643	-0.0012	0.0017	-0.0028
04T-	43	250	2 1.201	-0.0	-3.185	-0.2208	0.0760	0.0658	0.0020	-0.0027
04T-	43	250	3 1.201	0.0	1.077	0.1531	0.0652	-0.0753	0.0012	-0.0033
04T-	43	250	4 1.201	0.0	3.232	0.3610	0.0802	-0.1618	0.0007	-0.0033
04T-	43	250	5 1.201	0.0	5.652	0.6031	0.1163	-0.2623	0.0006	-0.0033
04T-	43	250	6 1.201	0.0	7.715	0.7982	0.1609	-0.3389	0.0002	-0.0031
04T-	43	250	7 1.201	0.0	10.033	1.0002	0.2256	-0.4256	-0.0004	-0.0032
04T-	43	250	8 1.200	0.0	12.196	1.1809	0.3008	-0.5153	-0.0008	-0.0035
04T-	43	250	9 1.201	0.0	13.345	1.2336	0.3370	-0.5497	-0.0011	-0.0034
04T-	43	250	10 1.200	0.0	14.364	1.3560	0.3910	-0.6221	-0.0012	-0.0035
04T-	43	250	13 1.203	0.0	16.413	1.5028	0.4850	-0.7165	-0.0015	-0.0035
04T-	43	250	14 1.199	0.0	18.628	1.6439	0.5963	-0.8065	-0.0013	-0.0033
04T-	43	250	15 1.199	0.0	20.647	1.7528	0.7019	-0.8919	-0.0018	-0.0033
04T-	43	250	16 1.202	0.0	9.868	0.9814	0.2184	-0.4163	-0.0004	-0.0033
04T-	43	250	17 1.202	0.0	-0.966	-0.0287	0.0634	-0.0031	0.0016	-0.0031
04T-	43	253	1 0.899	0.0	-1.003	0.0451	0.0431	-0.0642	0.0017	-0.0041
04T-	43	253	2 0.902	0.0	-3.475	-0.1582	0.0589	-0.0667	0.0033	-0.0045
04T-	43	253	3 0.898	0.0	1.533	0.2683	0.0456	-0.0700	-0.0036	-0.0037
04T-	43	253	4 0.896	0.0	3.892	0.4796	0.0648	-0.0900	-0.0028	-0.0033
04T-	43	253	5 0.900	0.0	6.063	0.6606	0.0957	-0.1215	-0.0026	-0.0031
04T-	43	253	6 0.900	0.0	8.380	0.8528	0.1423	-0.1730	-0.0038	-0.0022
04T-	43	253	7 0.897	0.0	10.844	1.0522	0.2094	-0.2451	-0.0023	-0.0010
04T-	43	253	8 0.902	0.0	12.976	1.2057	0.2822	-0.2976	0.0013	-0.0006
04T-	43	253	9 0.894	0.0	15.123	1.3199	0.3589	-0.3580	0.0036	-0.0009
04T-	43	253	10 0.900	0.0	17.275	1.4378	0.4545	-0.4528	0.0045	-0.0046
04T-	43	253	11 0.903	0.0	19.425	1.5469	0.5563	-0.5473	0.0028	-0.0025
04T-	43	253	12 0.897	0.0	21.574	1.6654	0.6691	-0.6327	0.0011	-0.0011
04T-	43	254	1 0.800	0.0	-0.890	0.0452	0.0368	-0.0525	0.0007	-0.0033
04T-	43	254	2 0.805	0.0	3.787	0.4654	0.0507	-0.0906	-0.0008	-0.0025
04T-	43	254	3 0.801	0.0	8.263	0.8322	0.1182	-0.1570	-0.0056	-0.0020
04T-	43	254	4 0.800	0.0	12.834	1.1412	0.2472	-0.2498	0.0052	0.0002
04T-	43	254	5 0.801	0.0	17.096	1.3710	0.4172	-0.3972	0.0016	-0.0005
04T-	43	254	6 0.799	0.0	18.083	1.3960	0.4473	-0.4118	0.0013	-0.0001
04T-	43	254	7 0.775	0.0	20.514	1.5370	0.5735	-0.5162	0.0023	-0.0019
04T-	43	257	1 0.701	0.0	-1.005	0.0269	0.0348	-0.0472	0.0009	-0.0033
04T-	43	257	2 0.700	0.0	-3.369	-0.1586	0.0490	-0.0360	0.0030	-0.0037
04T-	43	257	3 0.701	0.0	1.342	0.2389	0.0329	-0.0666	0.0002	-0.0027
04T-	43	257	5 0.701	0.0	5.928	0.6182	0.0660	-0.1216	-0.0001	-0.0023
04T-	43	257	4 0.701	0.0	3.475	0.4107	0.0421	-0.0857	0.0005	-0.0023

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	257	6	0.698	0.0	8.132	0.8033	0.1006	-0.1585	-0.0016	-0.0020
04T- 43	257	7	0.699	0.0	10.245	0.9615	0.1490	-0.1938	0.0008	-0.0003
04T- 43	257	8	0.698	0.0	12.580	1.1036	0.2219	-0.2400	0.0054	0.0009
04T- 43	257	9	0.701	0.0	14.741	1.2117	0.3021	-0.2962	0.0017	0.0007
04T- 43	257	10	0.696	0.0	16.788	1.3322	0.3860	-0.3605	0.0019	0.0016
04T- 43	257	11	0.698	0.0	19.033	1.4549	0.4901	-0.4394	0.0024	-0.0006
04T- 43	257	12	0.699	0.0	21.097	1.5741	0.5959	-0.5095	0.0029	-0.0015
04T- 43	258	1	1.205	0.0	-1.193	-0.0759	0.0708	0.0056	0.0002	-0.0041
04T- 43	258	2	1.203	-0.0	-3.510	-0.2746	0.0857	0.0858	0.0013	-0.0041
04T- 43	258	3	1.205	0.0	1.185	0.1492	0.0707	-0.0918	-0.0008	-0.0042
04T- 43	258	4	1.203	0.0	3.544	0.3805	0.0874	-0.1923	-0.0021	-0.0036
04T- 43	258	5	1.203	0.0	6.028	0.6306	0.1239	-0.2933	-0.0030	-0.0032
04T- 43	258	6	1.203	0.0	8.402	0.8549	0.1766	-0.3817	-0.0024	-0.0027
04T- 43	258	7	1.203	0.0	10.782	1.0613	0.2458	-0.4701	-0.0028	-0.0021
04T- 43	258	8	1.200	0.0	13.103	1.2602	0.3308	-0.5725	-0.0028	-0.0018
04T- 43	258	9	1.200	0.0	15.280	1.4342	0.4253	-0.6787	-0.0022	-0.0018
04T- 43	258	10	1.202	0.0	17.632	1.6023	0.5403	-0.7886	-0.0020	-0.0013
04T- 43	258	12	1.207	0.0	21.964	1.8353	0.7668	-0.9542	-0.0014	-0.0017
04T- 43	261	1	0.901	0.0	-0.905	0.0817	0.0300	-0.0509	0.0012	-0.0025
04T- 43	261	2	0.901	0.0	4.136	0.5424	0.0650	-0.0834	0.0006	-0.0025
04T- 43	261	3	0.901	0.0	6.643	0.7612	0.1107	-0.1179	0.0013	-0.0021
04T- 43	261	4	0.901	0.0	9.007	0.9467	0.1712	-0.1568	0.0013	-0.0018
04T- 43	261	5	0.899	0.0	12.817	1.1567	0.2873	-0.2581	0.0026	-0.0021
04T- 43	262	1	0.901	0.0	-0.862	0.0859	0.0295	-0.0495	0.0009	-0.0023
04T- 43	262	2	0.899	0.0	-3.559	-0.1844	0.0438	-0.0323	-0.0	-0.0028
04T- 43	262	3	0.903	0.0	1.643	0.3178	0.0389	-0.0613	0.0009	-0.0023
04T- 43	262	4	0.902	0.0	4.164	0.5440	0.0652	-0.0828	0.0005	-0.0022
04T- 43	262	5	0.901	0.0	6.539	0.7501	0.1081	-0.1142	0.0013	-0.0018
04T- 43	262	6	0.898	0.0	9.014	0.9401	0.1694	-0.1519	0.0018	-0.0016
04T- 43	262	7	0.902	0.0	11.331	1.0960	0.2407	-0.2118	-0.0020	-0.0007
04T- 43	262	8	0.903	0.0	13.399	1.1843	0.3089	-0.2840	0.0003	-0.0014
04T- 43	263	1	0.800	0.0	-0.914	0.0691	0.0266	-0.0369	0.0013	-0.0020
04T- 43	263	2	0.801	0.0	-3.379	-0.1554	0.0377	-0.0211	0.0012	-0.0030
04T- 43	263	3	0.800	0.0	1.455	0.2718	0.0321	-0.0521	0.0012	-0.0019
04T- 43	263	4	0.803	0.0	3.857	0.4834	0.0492	-0.0758	0.0013	-0.0018
04T- 43	263	5	0.801	0.0	6.339	0.7004	0.0858	-0.1052	0.0015	-0.0016
04T- 43	263	6	0.801	0.0	8.581	0.8627	0.1362	-0.1356	0.0016	-0.0013
04T- 43	263	7	0.798	0.0	10.925	0.9851	0.2019	-0.1791	0.0017	-0.0008
04T- 43	264	1	0.898	0.0	-0.892	0.0827	0.0296	-0.0477	0.0009	-0.0023
04T- 43	264	2	0.907	0.0	-3.398	-0.1699	0.0430	-0.0343	-0.0002	-0.0030
04T- 43	264	3	0.899	0.0	1.593	0.3150	0.0382	-0.0598	0.0009	-0.0024
04T- 43	264	4	0.895	0.0	3.883	0.5244	0.0615	-0.0787	0.0005	-0.0023
04T- 43	264	5	0.896	0.0	6.207	0.7250	0.1009	-0.1073	0.0009	-0.0021
04T- 43	264	6	0.899	0.0	8.591	0.9150	0.1596	-0.1439	0.0017	-0.0017
04T- 43	264	7	0.899	0.0	10.753	1.0536	0.2214	-0.1973	0.0041	-0.0017

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	264	8	0.899	0.0	12.861	1.1592	0.2906	-0.2668	0.0013	-0.0012
04T- 43	264	9	0.899	0.0	15.066	1.2902	0.3770	-0.3634	0.0013	-0.0013
04T- 43	264	10	0.902	0.0	17.347	1.4247	0.4772	-0.4522	0.0015	-0.0020
04T- 43	264	11	0.900	0.0	19.403	1.5383	0.5754	-0.5334	0.0020	-0.0024
04T- 43	264	12	0.899	0.0	21.595	1.6601	0.6931	-0.6209	0.0001	-0.0
04T- 43	267	1	0.804	0.0	-0.382	0.0753	0.0265	-0.0389	0.0014	-0.0022
04T- 43	267	2	0.803	0.0	-3.249	-0.1433	0.0364	-0.0239	0.0015	-0.0026
04T- 43	267	3	0.805	0.0	1.371	0.2673	0.0318	-0.0532	0.0013	-0.0021
04T- 43	267	4	0.802	0.0	3.757	0.4815	0.0489	-0.0775	0.0014	-0.0019
04T- 43	267	5	0.802	0.0	6.145	0.6901	0.0825	-0.1061	0.0019	-0.0018
04T- 43	267	6	0.806	0.0	8.3[illegible]9	0.8529	0.1320	-0.1352	0.0019	-0.0014
04T- 43	267	7	0.802	0.0	10.579	0.9740	0.1935	-0.1780	0.0012	-0.0009
04T- 43	267	8	0.805	0.0	12.786	1.0934	0.2650	-0.2335	0.0013	-0.0006
04T- 43	267	9	0.803	0.0	14.900	1.2153	0.3421	-0.3015	0.0010	-0.0008
04T- 43	267	10	0.803	0.0	17.095	1.3528	0.4356	-0.3780	0.0005	-0.0007
04T- 43	267	11	0.802	0.0	19.210	1.4678	0.5330	-0.4705	0.0018	-0.0021
04T- 43	267	12	0.803	0.0	21.406	1.5861	0.6492	-0.5612	0.0011	-0.0024
04T- 43	268	1	0.698	0.0	-0.942	0.0598	0.0245	-0.0358	0.0014	-0.0020
04T- 43	268	2	0.700	-0.0	-3.265	-0.1421	0.0334	-0.0196	0.0017	-0.0024
04T- 43	268	3	0.702	0.0	1.303	0.2425	0.0289	-0.0505	0.0012	-0.0018
04T- 43	268	4	0.701	0.0	3.564	0.4264	0.0423	-0.0734	0.0012	-0.0018
04T- 43	268	5	0.701	0.0	5.888	0.6235	0.0683	-0.1052	0.0012	-0.0018
04T- 43	268	6	0.700	0.0	8.096	0.7916	0.1120	-0.1359	0.0014	-0.0017
04T- 43	268	7	0.699	0.0	10.255	0.9127	0.1699	-0.1673	0.0012	-0.0015
04T- 43	268	8	0.697	0.0	12.511	1.0482	0.2391	-0.2098	0.0028	-0.0010
04T- 43	268	9	0.699	0.0	14.712	1.1740	0.3167	-0.2613	0.0012	-0.0006
04T- 43	268	10	0.701	0.0	16.813	1.2849	0.3971	-0.3353	0.0003	-0.0005
04T- 43	268	11	0.698	0.0	19.000	1.4183	0.5009	-0.4313	0.0002	0.0003
04T- 43	268	12	0.697	0.0	21.157	1.5348	0.6093	-0.5112	0.0020	-0.0031
04T- 43	269	1	1.206	0.0	-1.051	-0.0285	0.0533	0.0113	0.0011	-0.0021
04T- 43	269	2	1.204	-0.0	-3.376	-0.2413	0.0652	0.0921	0.0018	-0.0024
04T- 43	269	3	1.205	0.0	1.258	0.1991	0.0579	-0.0821	0.0017	-0.0024
04T- 43	269	4	1.205	0.0	3.794	0.4518	0.0831	-0.1892	0.0013	-0.0026
04T- 43	269	5	1.200	0.0	6.202	0.6961	0.1273	-0.2907	0.0008	-0.0023
04T- 43	269	6	1.204	0.0	8.429	0.8995	0.1835	-0.3742	0.0007	-0.0025
04T- 43	269	7	1.203	0.0	10.906	1.1101	0.2628	-0.4682	0.0006	-0.0025
04T- 43	269	8	1.205	0.0	13.169	1.2905	0.3506	-0.5625	0.0005	-0.0026
04T- 43	269	9	1.206	0.0	15.365	1.4545	0.4485	-0.6633	0.0001	-0.0031
04T- 43	269	10	1.201	0.0	17.722	1.6108	0.5645	-0.7674	0.0002	-0.0030
04T- 43	269	11	1.201	0.0	19.880	1.7406	0.6800	-0.8675	-0.0002	-0.0030
04T- 43	269	12	1.205	0.0	22.041	1.8311	0.7935	-0.9448	0.0005	-0.0037
04T- 43	272	1	0.896	0.0	-0.962	0.0870	0.0283	-0.0523	-0.0004	-0.0038
04T- 43	272	2	0.900	0.0	-3.157	-0.1360	0.0409	-0.0412	0.0010	-0.0025
04T- 43	272	3	0.896	0.0	1.232	0.2915	0.0373	-0.0639	0.0005	-0.0031
04T- 43	272	4	0.897	0.0	3.519	0.4944	0.0577	-0.0799	0.0008	-0.0028
04T- 43	272	5	0.901	0.0	5.680	0.6828	0.0934	-0.1082	0.0006	-0.0025

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	272	6	0.897	0.0	7.920	0.8697	0.1452	-0.1454	0.0005	-0.0028
04T- 43	272	7	0.897	0.0	9.996	1.0080	0.2017	-0.1900	0.0024	-0.0032
04T- 43	272	8	0.899	0.0	12.052	1.1204	0.2650	-0.2529	0.0044	-0.0034
04T- 43	272	9	0.896	0.0	14.157	1.2292	0.3420	-0.3488	-0.0	-0.0021
04T- 43	272	10	0.897	0.0	16.292	1.3678	0.4343	-0.4438	0.0007	-0.0022
04T- 43	272	11	0.900	0.0	18.390	1.5003	0.5357	-0.5373	0.0024	-0.0034
04T- 43	272	12	0.900	0.0	20.450	1.6116	0.6398	-0.6222	0.0009	-0.0020
04T- 43	273	1	0.798	0.0	-0.922	0.0774	0.0266	-0.0458	0.0014	-0.0028
04T- 43	273	2	0.796	0.0	-3.129	-0.1270	0.0354	-0.0316	0.0017	-0.0030
04T- 43	273	3	0.798	-0.0	-3.130	-0.1278	0.0360	-0.0318	0.0017	-0.0029
04T- 43	273	4	0.800	0.0	1.193	0.2576	0.0322	-0.0591	0.0012	-0.0027
04T- 43	273	5	0.800	0.0	3.444	0.4470	0.0472	-0.0790	0.0012	-0.0027
04T- 43	273	6	0.802	0.0	5.593	0.6366	0.0743	-0.1057	0.0012	-0.0027
04T- 43	273	7	0.801	0.0	7.769	0.8082	0.1186	-0.1370	0.0011	-0.0028
04T- 43	273	8	0.801	0.0	9.852	0.9246	0.1727	-0.1737	0.0006	-0.0026
04T- 43	273	9	0.799	0.0	11.991	1.0506	0.2419	-0.2325	-0.0	-0.0026
04T- 43	273	10	0.801	0.0	13.996	1.1608	0.3097	-0.2907	0.0001	-0.0022
04T- 43	273	11	0.801	0.0	16.104	1.2910	0.3948	-0.3700	-0.0005	-0.0018
04T- 43	273	12	0.800	0.0	18.185	1.4244	0.4915	-0.4602	0.0	-0.0021
04T- 43	273	13	0.800	0.0	20.320	1.5422	0.5994	-0.5623	0.0014	-0.0039
04T- 43	274	1	0.694	0.0	-0.966	0.0650	0.0254	-0.0434	0.0014	-0.0029
04T- 43	274	2	0.697	-0.0	-3.076	-0.1199	0.0338	-0.0298	0.0018	-0.0032
04T- 43	274	3	0.698	0.0	1.153	0.2374	0.0303	-0.0574	0.0012	-0.0027
04T- 43	274	4	0.699	0.0	3.405	0.4170	0.0435	-0.0798	0.0011	-0.0026
04T- 43	274	5	0.696	0.0	5.518	0.5948	0.0659	-0.1097	0.0011	-0.0026
04T- 43	274	6	0.698	0.0	7.594	0.7581	0.1044	-0.1415	0.0010	-0.0026
04T- 43	274	7	0.695	0.0	9.738	0.8892	0.1600	-0.1748	0.0013	-0.0027
04T- 43	274	8	0.698	0.0	11.786	1.0041	0.2190	-0.2141	0.0	-0.0025
04T- 43	274	9	0.698	0.0	13.905	1.1299	0.2914	-0.2663	0.0	-0.0027
04T- 43	274	10	0.695	0.0	15.970	1.2499	0.3698	-0.3327	-0.0005	-0.0020
04T- 43	274	11	0.696	0.0	18.061	1.3732	0.4625	-0.4293	0.0007	-0.0035
04T- 43	274	12	0.697	0.0	20.219	1.4992	0.5706	-0.5256	0.0012	-0.0045
04T- 43	275	1	1.205	0.0	-1.009	-0.0100	0.0527	0.0008	0.0013	-0.0034
04T- 43	275	2	1.204	-0.0	-3.149	-0.2008	0.0620	0.0666	0.0016	-0.0033
04T- 43	275	3	1.202	0.0	1.157	0.1981	0.0576	-0.0836	0.0011	-0.0039
04T- 43	275	4	1.200	0.0	3.413	0.4193	0.0798	-0.1764	0.0008	-0.0040
04T- 43	275	5	1.200	0.0	5.540	0.6312	0.1152	-0.2660	0.0007	-0.0037
04T- 43	275	6	1.203	0.0	7.818	0.8436	0.1684	-0.3540	0.0006	-0.0037
04T- 43	275	7	1.201	0.0	10.070	1.0411	0.2365	-0.4415	0.0005	-0.0039
04T- 43	275	8	1.201	0.0	12.169	1.2140	0.3131	-0.5287	0.0001	-0.0043
04T- 43	275	9	1.203	0.0	14.312	1.3776	0.4027	-0.6278	0.0001	-0.0040
04T- 43	275	10	1.202	0.0	16.426	1.5253	0.5021	-0.7197	0.0003	-0.0046
04T- 43	275	11	1.201	0.0	18.555	1.6562	0.6100	-0.8120	-0.0	-0.0048
04T- 43	275	12	1.201	0.0	20.672	1.7622	0.7203	-0.8967	0.0006	-0.0056
04T- 43	278	1	0.897	0.0	-0.978	0.0318	0.0420	-0.0361	0.0334	0.0011
04T- 43	278	2	0.889	0.0	-3.574	-0.2629	0.0572	-0.0002	0.0322	-0.0014

TEST	RUN	PT	MACH	SWEEP (DEG)	ALFHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	278	3	0.890	0.0	1.686	0.2925	0.0494	-0.0614	0.0336	0.0005
04T- 43	278	4	0.899	0.0	4.263	0.5560	0.0772	-0.0919	0.0292	-0.0020
04T- 43	278	5	0.898	0.0	6.656	0.7671	0.1200	-0.1152	0.0245	-0.0040
04T- 43	278	6	0.899	0.0	9.021	0.9238	0.1782	-0.1492	0.0244	-0.0052
04T- 43	278	7	0.900	0.0	11.258	1.0410	0.2423	-0.1957	0.0218	-0.0057
04T- 43	278	8	0.900	0.0	13.472	1.1538	0.3157	-0.2625	0.0182	-0.0054
04T- 43	279	1	0.801	0.0	-0.991	0.0273	0.0373	-0.0298	0.0361	0.0017
04T- 43	279	2	0.802	0.0	-3.517	-0.2204	0.0500	-0.0008	0.0312	0.0003
04T- 43	279	3	0.801	0.0	1.485	0.2547	0.0425	-0.0564	0.0359	0.0014
04T- 43	279	4	0.799	0.0	3.869	0.4632	0.0587	-0.0835	0.0363	-0.0011
04T- 43	279	5	0.803	0.0	6.527	0.7002	0.0984	-0.1110	0.0339	-0.0040
04T- 43	279	6	0.801	0.0	8.573	0.8459	0.1452	-0.1352	0.0264	-0.0051
04T- 43	279	7	0.801	0.0	10.872	0.9523	0.2053	-0.1656	0.0226	-0.0058
04T- 43	279	8	0.801	0.0	13.112	1.0739	0.2778	-0.2158	0.0231	-0.0065
04T- 43	279	9	0.800	0.0	15.353	1.1978	0.3582	-0.2802	0.0202	-0.0063
04T- 43	280	1	1.202	0.0	-1.020	-0.0188	0.0677	0.0128	0.0178	0.0019
04T- 43	280	2	1.202	0.0	-3.597	-0.2577	0.0809	0.1004	0.0161	0.0028
04T- 43	280	3	1.203	0.0	1.419	0.2188	0.0741	-0.0826	0.0199	0.0
04T- 43	280	4	1.203	0.0	4.056	0.4815	0.1028	-0.1880	0.0215	-0.0017
04T- 43	280	5	1.203	0.0	6.592	0.7235	0.1500	-0.2764	0.0203	-0.0033
04T- 43	280	6	1.203	0.0	9.027	0.9316	0.2121	-0.3582	0.0183	-0.0049
04T- 43	280	7	1.203	0.0	11.440	1.1270	0.2903	-0.4515	0.0190	-0.0071
04T- 43	280	8	1.199	0.0	13.815	1.3081	0.3832	-0.5463	0.0179	-0.0088
04T- 43	283	1	0.894	0.0	-0.956	0.0534	0.0443	-0.0492	0.0343	0.0015
04T- 43	283	2	0.894	0.0	-3.237	-0.2018	0.0550	-0.0257	0.0347	0.0039
04T- 43	283	3	0.895	0.0	1.220	0.2665	0.0508	-0.0714	0.0343	-0.0009
04T- 43	283	4	0.895	0.0	3.432	0.4862	0.0698	-0.0982	0.0323	-0.0034
04T- 43	283	5	0.895	0.0	5.671	0.7020	0.1063	-0.1255	0.0269	-0.0056
04T- 43	283	6	0.898	0.0	7.918	0.8704	0.1574	-0.1495	0.0234	-0.0072
04T- 43	283	7	0.897	0.0	10.008	0.9855	0.2115	-0.1963	0.0181	-0.0073
04T- 43	283	8	0.899	0.0	12.033	1.0935	0.2756	-0.2529	0.0188	-0.0078
04T- 43	283	9	0.897	0.0	14.102	1.2154	0.3518	-0.3417	0.0174	-0.0083
04T- 43	283	10	0.898	0.0	16.269	1.3514	0.4444	-0.4418	0.0152	-0.0064
04T- 43	283	11	0.900	0.0	18.429	1.4812	0.5458	-0.5304	0.0144	-0.0069
04T- 43	283	12	0.901	0.0	20.404	1.5926	0.6461	-0.6095	0.0135	-0.0074
04T- 43	283	13	0.897	0.0	22.447	1.6937	0.7551	-0.6875	0.0123	-0.0080
04T- 43	284	1	0.801	0.0	-1.010	0.0390	0.0404	-0.0460	0.0371	0.0024
04T- 43	284	2	0.800	0.0	-3.215	-0.1812	0.0493	-0.0204	0.0340	0.0039
04T- 43	284	3	0.799	0.0	1.155	0.2398	0.0441	-0.0714	0.0365	-0.0002
04T- 43	284	4	0.801	0.0	3.407	0.4351	0.0590	-0.0982	0.0364	-0.0027
04T- 43	284	5	0.801	0.0	5.547	0.6271	0.0860	-0.1237	0.0348	-0.0055
04T- 43	284	6	0.799	0.0	7.686	0.7953	0.1297	-0.1470	0.0278	-0.0077
04T- 43	284	7	0.801	0.0	9.875	0.9234	0.1862	-0.1837	0.0227	-0.0087
04T- 43	284	8	0.799	0.0	11.941	1.0406	0.2510	-0.2327	0.0215	-0.0097
04T- 43	284	9	0.801	0.0	14.033	1.1491	0.3217	-0.2942	0.0214	-0.0102
04T- 43	284	10	0.800	0.0	16.123	1.2701	0.4019	-0.3617	0.0187	-0.0096

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	284	11	0.797	0.0	18.286	1.4104	0.5034	-0.4592	0.0177	-0.0093
04T- 43	284	12	0.798	0.0	20.407	1.5225	0.6081	-0.5507	0.0165	-0.0098
04T- 43	284	13	0.799	0.0	22.302	1.6197	0.7114	-0.6276	0.0156	-0.0114
04T- 43	285	1	0.695	0.0	-1.006	0.0340	0.0367	-0.0456	0.0384	0.0028
04T- 43	285	2	0.695	0.0	-3.140	-0.1631	0.0449	-0.0227	0.0365	0.0046
04T- 43	285	3	0.698	0.0	1.119	0.2180	0.0404	-0.0689	0.0376	0.0003
04T- 43	285	4	0.697	0.0	3.264	0.3920	0.0525	-0.0941	0.0373	-0.0021
04T- 43	285	5	0.698	0.0	5.450	0.5717	0.0749	-0.1236	0.0357	-0.0051
04T- 43	285	6	0.696	0.0	7.611	0.7537	0.1153	-0.1520	0.0332	-0.0079
04T- 43	285	7	0.697	0.0	9.623	0.8740	0.1667	-0.1829	0.0260	-0.0088
04T- 43	285	8	0.699	0.0	11.854	0.9882	0.2294	-0.2201	0.0229	-0.0100
04T- 43	285	9	0.699	0.0	13.906	1.1083	0.2963	-0.2633	0.0214	-0.0111
04T- 43	285	10	0.697	0.0	16.013	1.2348	0.3767	-0.3325	0.0182	-0.0104
04T- 43	285	11	0.698	0.0	18.049	1.3473	0.4638	-0.4195	0.0173	-0.0109
04T- 43	285	12	0.696	0.0	20.146	1.4697	0.5686	-0.5111	0.0164	-0.0116
04T- 43	285	13	0.700	0.0	22.163	1.5730	0.6720	-0.5792	0.0148	-0.0110
04T- 43	286	1	1.224	0.0	-1.012	-0.0041	0.0671	-0.0005	0.0188	0.0010
04T- 43	286	2	1.220	-0.0	-3.239	-0.2108	0.0769	0.0746	0.0170	0.0027
04T- 43	286	3	1.199	-0.0	-3.237	-0.2133	0.0772	0.0703	0.0176	0.0026
04T- 43	286	4	1.198	0.0	-1.003	-0.0015	0.0680	-0.0057	0.0195	0.0010
04T- 43	286	5	1.207	-0.0	-3.237	-0.2120	0.0767	0.0723	0.0173	0.0027
04T- 43	286	6	1.200	0.0	1.156	0.2159	0.0736	-0.0906	0.0216	-0.0011
04T- 43	286	7	1.200	0.0	3.436	0.4447	0.0972	-0.1840	0.0234	-0.0032
04T- 43	286	8	1.199	0.0	5.724	0.6671	0.1373	-0.2681	0.0219	-0.0049
04T- 43	286	9	1.201	0.0	7.795	0.8503	0.1856	-0.3385	0.0204	-0.0059
04T- 43	286	10	1.199	0.0	10.123	1.0485	0.2547	-0.4291	0.0197	-0.0078
04T- 43	286	11	1.192	0.0	12.165	1.2189	0.3306	-0.5200	0.0192	-0.0097
04T- 43	286	12	1.201	0.0	14.373	1.3771	0.4210	-0.6148	0.0186	-0.0109
04T- 43	286	13	1.204	0.0	16.463	1.5094	0.5147	-0.7002	0.0183	-0.0131
04T- 43	286	14	1.199	0.0	18.624	1.6428	0.6236	-0.7953	0.0176	-0.0143
04T- 43	286	15	1.200	0.0	20.702	1.7449	0.7319	-0.8866	0.0166	-0.0157
04T- 43	286	16	1.198	0.0	22.704	1.8429	0.8444	-0.9774	0.0152	-0.0168
04T- 43	286	17	1.202	0.0	9.996	1.0399	0.2490	-0.4232	0.0197	-0.0073
04T- 43	289	1	0.897	0.0	-1.093	-0.0277	0.0514	-0.0360	0.0309	0.0
04T- 43	289	2	0.895	0.0	3.776	0.4923	0.0738	-0.1013	0.0286	-0.0029
04T- 43	289	3	0.896	0.0	6.167	0.7027	0.1086	-0.1306	0.0224	-0.0045
04T- 43	289	4	0.898	0.0	8.554	0.8903	0.1589	-0.1703	0.0196	-0.0060
04T- 43	289	5	0.898	0.0	12.817	1.1480	0.2859	-0.2695	0.0195	-0.0079
04T- 43	289	6	0.898	0.0	21.723	1.6610	0.6984	-0.6374	0.0114	-0.0074
04T- 43	291	1	0.896	0.0	-1.088	-0.0238	0.0508	-0.0370	0.0304	-0.0006
04T- 43	291	2	0.899	0.0	-3.491	-0.2630	0.0680	-0.0199	0.0254	-0.0003
04T- 43	291	3	0.895	0.0	1.400	0.2543	0.0535	-0.0756	0.0337	0.0002
04T- 43	291	4	0.899	0.0	3.820	0.4997	0.0755	-0.1042	0.0280	-0.0027
04T- 43	291	5	0.895	0.0	6.133	0.6964	0.1070	-0.1300	0.0229	-0.0044
04T- 43	291	6	0.903	0.0	8.606	0.8929	0.1618	-0.1677	0.0211	-0.0057
04T- 43	291	7	0.902	0.0	10.693	1.0398	0.2214	-0.2198	0.0264	-0.0078

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	291	8	0.856	0.0	12.915	1.1666	0.2922	-0.2728	0.0196	-0.0072
04T- 43	291	9	0.899	0.0	15.143	1.3039	0.3792	-0.3431	0.0168	-0.0063
04T- 43	291	10	0.903	0.0	17.260	1.4047	0.4688	-0.4470	0.0158	-0.0076
04T- 43	291	11	0.901	0.0	19.509	1.5303	0.5769	-0.5453	0.0138	-0.0067
04T- 43	291	12	0.898	0.0	21.497	1.6324	0.6786	-0.6234	0.0122	-0.0072
04T- 43	291	13	0.896	0.0	23.592	1.7355	0.7941	-0.6957	0.0107	-0.0084
04T- 43	292	1	0.801	0.0	-1.048	-0.0050	0.0458	-0.0364	0.0337	0.0008
04T- 43	292	2	0.802	0.0	-3.318	-0.2108	0.0595	-0.0161	0.0270	0.0001
04T- 43	292	3	0.799	0.0	1.354	0.2353	0.0458	-0.0699	0.0369	0.0009
04T- 43	292	4	0.801	0.0	3.550	0.4354	0.0592	-0.0955	0.0360	-0.0017
04T- 43	292	5	0.798	0.0	5.933	0.6527	0.0886	-0.1315	0.0343	-0.0042
04T- 43	292	6	0.805	0.0	8.369	0.8625	0.1362	-0.1635	0.0312	-0.0061
04T- 43	292	7	0.804	0.0	10.560	0.9917	0.1917	-0.1970	0.0246	-0.0070
04T- 43	292	8	0.803	0.0	12.738	1.1149	0.2613	-0.2466	0.0211	-0.0075
04T- 43	292	9	0.803	0.0	14.817	1.2091	0.3377	-0.3035	0.0213	-0.0082
04T- 43	292	10	0.801	0.0	17.039	1.3342	0.4293	-0.3884	0.0176	-0.0071
04T- 43	292	11	0.802	0.0	19.160	1.4682	0.5330	-0.4733	0.0181	-0.0090
04T- 43	292	12	0.803	0.0	21.402	1.5722	0.6420	-0.5492	0.0163	-0.0099
04T- 43	292	13	0.804	0.0	23.383	1.6778	0.7525	-0.6174	0.0147	-0.0101
04T- 43	293	1	0.700	0.0	-1.039	-0.0037	0.0431	-0.0336	0.0356	-0.0008
04T- 43	293	2	0.700	0.0	-3.338	-0.2072	0.0567	-0.0099	0.0286	-0.0003
04T- 43	293	3	0.699	0.0	1.243	0.2052	0.0421	-0.0615	0.0374	0.0002
04T- 43	293	4	0.700	0.0	3.560	0.4013	0.0537	-0.0886	0.0366	-0.0025
04T- 43	293	5	0.701	0.0	5.820	0.5899	0.0752	-0.1209	0.0352	-0.0043
04T- 43	293	6	0.702	0.0	7.983	0.7744	0.1092	-0.1537	0.0331	-0.0064
04T- 43	293	7	0.702	0.0	10.254	0.9414	0.1650	-0.1883	0.0273	-0.0085
04T- 43	293	8	0.700	0.0	12.544	1.0586	0.2378	-0.2343	0.0184	-0.0083
04T- 43	293	9	0.702	0.0	14.645	1.1765	0.3137	-0.2793	0.0195	-0.0085
04T- 43	293	10	0.697	0.0	16.730	1.3025	0.3980	-0.3463	0.0177	-0.0079
04T- 43	293	11	0.701	0.0	18.916	1.4205	0.4964	-0.4233	0.0176	-0.0093
04T- 43	293	12	0.699	0.0	21.190	1.5553	0.6127	-0.5009	0.0167	-0.0107
04T- 43	293	13	0.697	0.0	23.227	1.6722	0.7263	-0.5702	0.0150	-0.0106
04T- 43	294	1	1.197	0.0	-1.092	-0.0483	0.0784	0.0049	0.0178	0.0012
04T- 43	294	2	1.205	0.0	-3.447	-0.2584	0.0924	0.0894	0.0166	0.0024
04T- 43	294	3	1.206	0.0	1.285	0.1806	0.0809	-0.0859	0.0202	-0.0003
04T- 43	294	4	1.204	0.0	3.710	0.4191	0.1009	-0.1814	0.0215	-0.0019
04T- 43	294	5	1.203	0.0	5.998	0.6456	0.1373	-0.2670	0.0201	-0.0037
04T- 43	294	6	1.198	0.0	8.504	0.8722	0.1936	-0.3512	0.0184	-0.0048
04T- 43	294	7	1.206	0.0	10.801	1.0600	0.2606	-0.4418	0.0187	-0.0068
04T- 43	294	8	1.199	0.0	13.024	1.2426	0.3417	-0.5324	0.0183	-0.0090
04T- 43	294	9	1.205	0.0	15.343	1.4112	0.4389	-0.6326	0.0173	-0.0102
04T- 43	294	10	1.202	0.0	17.534	1.5595	0.5429	-0.7293	0.0165	-0.0108
04T- 43	294	11	1.204	0.0	19.868	1.6937	0.6610	-0.8257	0.0156	-0.0116
04T- 43	294	12	1.206	0.0	21.940	1.7901	0.7690	-0.9052	0.0158	-0.0149
04T- 43	295	1	0.898	0.0	-1.125	-0.0327	0.0513	-0.0334	0.0289	-0.0006
04T- 43	295	2	0.900	0.0	-3.596	-0.2702	0.0697	-0.0172	0.0246	-0.0028

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	295	3	0.898	0.0	1.597	0.2740	0.0556	-0.0761	0.0324	-0.0003
04T- 43	295	4	0.899	0.0	4.176	0.5293	0.0793	-0.1039	0.0261	-0.0028
04T- 43	295	5	0.901	0.0	6.461	0.7237	0.1141	-0.1320	0.0208	-0.0043
04T- 43	295	6	0.897	0.0	9.004	0.9049	0.1687	-0.1715	0.0220	-0.0056
04T- 43	295	7	0.900	0.0	11.171	1.0441	0.2303	-0.2293	0.0230	-0.0065
04T- 43	295	8	0.898	0.0	13.554	1.2014	0.3141	-0.2828	0.0195	-0.0075
04T- 43	296	1	0.800	0.0	-1.079	-0.0109	0.0460	-0.0353	0.0327	0.0007
04T- 43	296	2	0.803	0.0	-3.568	-0.2300	0.0628	-0.0144	0.0251	-0.0010
04T- 43	296	3	0.802	0.0	1.334	0.2327	0.0458	-0.0681	0.0355	-0.0001
04T- 43	296	4	0.799	0.0	3.799	0.4568	0.0616	-0.0976	0.0354	-0.0024
04T- 43	296	5	0.802	0.0	6.300	0.6802	0.0935	-0.1327	0.0332	-0.0043
04T- 43	296	6	0.803	0.0	8.719	0.8793	0.1437	-0.1621	0.0294	-0.0061
04T- 43	296	7	0.801	0.0	10.884	1.0079	0.2018	-0.2018	0.0241	-0.0071
04T- 43	296	8	0.797	0.0	13.124	1.1163	0.2732	-0.2483	0.0190	-0.0074
04T- 43	297	1	0.694	0.0	-0.991	0.0083	0.0445	-0.0332	0.0352	0.0015
04T- 43	297	2	0.693	0.0	-3.216	-0.1915	0.0566	-0.0103	0.0289	0.0024
04T- 43	297	3	0.696	0.0	1.204	0.2074	0.0429	-0.0601	0.0367	-0.0006
04T- 43	297	4	0.698	0.0	3.282	0.3826	0.0527	-0.0844	0.0358	-0.0029
04T- 43	297	5	0.697	0.0	5.353	0.5553	0.0718	-0.1147	0.0346	-0.0051
04T- 43	297	6	0.694	0.0	7.699	0.7490	0.1054	-0.1481	0.0315	-0.0077
04T- 43	297	7	0.695	0.0	9.642	0.8994	0.1512	-0.1814	0.0275	-0.0100
04T- 43	297	8	0.694	0.0	11.891	1.0300	0.2708	-0.2287	0.0196	-0.0107
04T- 43	297	9	0.699	0.0	13.920	1.1274	0.2886	-0.2698	0.0188	-0.0108
04T- 43	297	10	0.696	0.0	15.972	1.2560	0.3679	-0.3324	0.0178	-0.0109
04T- 43	297	11	0.699	0.0	18.086	1.3715	0.4600	-0.4162	0.0159	-0.0102
04T- 43	297	12	0.697	0.0	20.224	1.4991	0.5656	-0.4954	0.0164	-0.0119
04T- 43	297	13	0.693	0.0	22.151	1.6020	0.6642	-0.5625	0.0150	-0.0119
04T- 43	297	15	0.696	0.0	-1.047	0.0009	0.0441	-0.0328	0.0353	0.0026
04T- 43	298	1	0.803	0.0	-1.053	-0.0011	0.0470	-0.0352	0.0337	0.0016
04T- 43	298	2	0.797	0.0	-3.180	-0.1990	0.0601	-0.0164	0.0278	0.0026
04T- 43	298	3	0.790	0.0	1.278	0.2323	0.0467	-0.0680	0.0361	-0.0006
04T- 43	298	4	0.802	0.0	3.317	0.4200	0.0593	-0.0929	0.0356	-0.0030
04T- 43	298	5	0.791	0.0	5.555	0.6130	0.0831	-0.1245	0.0338	-0.0055
04T- 43	298	6	0.799	0.0	7.612	0.7940	0.1189	-0.1517	0.0307	-0.0076
04T- 43	298	7	0.798	0.0	9.881	0.9551	0.1752	-0.1876	0.0244	-0.0093
04T- 43	298	8	0.800	0.0	11.900	1.0508	0.2341	-0.2349	0.0182	-0.0097
04T- 43	298	9	0.802	0.0	14.038	1.1636	0.3118	-0.2920	0.0203	-0.0105
04T- 43	298	10	0.797	0.0	16.076	1.2773	0.3911	-0.3692	0.0177	-0.0093
04T- 43	298	11	0.799	0.0	18.311	1.4182	0.4942	-0.4612	0.0174	-0.0101
04T- 43	298	12	0.803	0.0	20.341	1.5325	0.5968	-0.5457	0.0165	-0.0108
04T- 43	298	13	0.792	0.0	22.203	1.6224	0.6912	-0.6114	0.0152	-0.0110
04T- 43	299	1	0.896	0.0	-1.022	-0.0058	0.0511	-0.0385	0.0306	0.0008
04T- 43	299	2	0.893	0.0	-3.284	-0.2297	0.0652	-0.0194	0.0247	0.0011
04T- 43	299	3	0.896	0.0	1.157	0.2433	0.0531	-0.0735	0.0325	-0.0013
04T- 43	299	4	0.892	0.0	3.465	0.4772	0.0728	-0.0998	0.0291	-0.0039
04T- 43	299	5	0.898	0.0	5.596	0.6564	0.0994	-0.1213	0.0238	-0.0057

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	299	6	0.898	0.0	7.888	0.8499	0.1466	-0.1587	0.0202	-0.0076
04T- 43	299	7	0.894	0.0	9.932	0.9858	0.1960	-0.2053	0.0223	-0.0084
04T- 43	299	8	0.900	0.0	12.093	1.1272	0.2679	-0.2646	0.0217	-0.0092
04T- 43	299	9	0.900	0.0	14.234	1.2490	0.3465	-0.3444	0.0190	-0.0088
04T- 43	299	10	0.903	0.0	16.223	1.3497	0.4275	-0.4253	0.0158	-0.0090
04T- 43	299	11	0.897	0.0	18.321	1.4695	0.5241	-0.5245	0.0149	-0.0089
04T- 43	299	12	0.896	0.0	20.435	1.5877	0.6311	-0.6184	0.0117	-0.0061
04T- 43	299	13	0.896	0.0	22.392	1.6862	0.7354	-0.6934	0.0110	-0.0085
04T- 43	300	1	1.203	0.0	-1.029	-0.0333	0.0787	-0.0007	0.0182	0.0008
04T- 43	300	2	1.203	0.0	-3.166	-0.2283	0.0900	0.0757	0.0170	0.0024
04T- 43	300	3	1.203	0.0	1.262	0.1894	0.0819	-0.0908	0.0210	-0.0011
04T- 43	300	4	1.202	0.0	3.312	0.3895	0.0982	-0.1702	0.0220	-0.0027
04T- 43	300	5	1.200	0.0	5.494	0.6048	0.1303	-0.2512	0.0205	-0.0045
04T- 43	300	6	1.201	0.0	7.694	0.8053	0.1765	-0.3273	0.0191	-0.0056
04T- 43	300	7	1.202	0.0	9.987	1.0012	0.2387	-0.4150	0.0184	-0.0072
04T- 43	300	8	1.194	0.0	12.160	1.1912	0.3159	-0.5144	0.0185	-0.0092
04T- 43	300	9	1.199	0.0	14.336	1.3511	0.4025	-0.6076	0.0177	-0.0106
04T- 43	300	10	1.203	0.0	16.480	1.4965	0.4970	-0.6986	0.0162	-0.0116
04T- 43	300	11	1.201	0.0	18.546	1.6260	0.5999	-0.7875	0.0155	-0.0119
04T- 43	300	12	1.204	0.0	20.695	1.7388	0.7102	-0.8852	0.0159	-0.0141
04T- 43	300	13	1.201	0.0	22.677	1.8332	0.8196	-0.9652	0.0140	-0.0153
04T- 43	300	14	1.193	0.0	10.050	1.0054	0.2390	-0.4134	0.0185	-0.0075
04T- 43	302	1	0.898	0.0	-1.122	-0.0509	0.0555	-0.0242	0.0413	-0.0008
04T- 43	302	2	0.901	0.0	3.849	0.5096	0.0814	-0.1086	0.0351	-0.0048
04T- 43	302	3	0.896	0.0	6.195	0.7116	0.1138	-0.1330	0.0293	-0.0068
04T- 43	302	4	0.900	0.0	8.529	0.8928	0.1660	-0.1651	0.0267	-0.0085
04T- 43	302	5	0.896	0.0	12.941	1.1644	0.2956	-0.2674	0.0290	-0.0103
04T- 43	302	6	0.900	0.0	21.594	1.6238	0.6827	-0.6195	0.0179	-0.0106
04T- 43	303	1	0.899	0.0	-1.113	-0.0461	0.0556	-0.0237	0.0410	-0.0006
04T- 43	303	2	0.892	0.0	-3.507	-0.2846	0.0708	-0.0035	0.0322	-0.0026
04T- 43	303	3	0.898	0.0	1.469	0.2619	0.0591	-0.0733	0.0435	-0.0010
04T- 43	303	4	0.899	0.0	3.778	0.5043	0.0797	-0.1059	0.0354	-0.0042
04T- 43	303	5	0.901	0.0	6.195	0.7156	0.1148	-0.1326	0.0293	-0.0064
04T- 43	303	6	0.898	0.0	8.498	0.8701	0.1637	-0.1622	0.0286	-0.0062
04T- 43	303	7	0.899	0.0	10.738	1.0371	0.2254	-0.2191	0.0266	-0.0085
04T- 43	303	8	0.899	0.0	12.990	1.1897	0.3017	-0.2738	0.0303	-0.0108
04T- 43	303	9	0.897	0.0	15.104	1.2941	0.3808	-0.3465	0.0232	-0.0084
04T- 43	303	10	0.897	0.0	17.235	1.4018	0.4711	-0.4465	0.0229	-0.0106
04T- 43	303	11	0.900	0.0	19.450	1.5207	0.5753	-0.5383	0.0197	-0.0098
04T- 43	303	12	0.899	0.0	21.579	1.6352	0.6870	-0.6231	0.0182	-0.0104
04T- 43	303	13	0.899	0.0	23.690	1.7331	0.8014	-0.6976	0.0157	-0.0111
04T- 43	304	1	0.800	0.1	-4.570	-2.2915	0.2185	0.0399	0.0441	0.0001
04T- 43	304	2	0.800	0.0	-3.450	-2.2452	0.0654	-0.0022	0.0345	-0.0002
04T- 43	304	3	0.799	0.0	1.344	0.2261	0.0504	-0.0640	0.0494	0.0010
04T- 43	304	4	0.801	0.0	3.638	0.4395	0.0647	-0.0939	0.0480	-0.0024
04T- 43	304	5	0.802	0.0	6.007	0.6505	0.0926	-0.1280	0.0439	-0.0052

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	304	6	0.802	0.0	8.356	0.8545	0.1385	-0.1596	0.0372	-0.0078
04T- 43	304	7	0.801	0.0	10.590	1.0148	0.1990	-0.2018	0.0343	-0.0092
04T- 43	304	8	0.801	0.0	12.633	1.0941	0.2599	-0.2412	0.0286	-0.0093
04T- 43	304	9	0.8[illegible]	0.0	14.816	1.2116	0.3422	-0.3063	0.0280	-0.0102
04T- 43	304	10	0.804	0.0	17.077	1.3327	0.4352	-0.3894	0.0253	-0.0093
04T- 43	304	11	0.802	0.0	19.179	1.4556	0.5350	-0.4609	0.0264	-0.0120
04T- 43	304	12	0.802	0.0	21.356	1.5674	0.6443	-0.5478	0.0242	-0.0125
04T- 43	304	13	0.802	0.0	23.461	1.6768	0.7605	-0.6168	0.0225	-0.0133
04T- 43	304	14	0.801	0.0	-1.067	-0.0231	0.0501	-0.0252	0.0446	-0.0006
04T- 43	305	1	0.698	0.0	-1.053	-0.0170	0.0478	-0.0277	0.0476	-0.0007
04T- 43	305	2	0.700	0.0	-3.351	-0.2280	0.0608	0.0	0.0365	0.0007
04T- 43	305	3	0.700	0.0	1.303	0.2012	0.0464	-0.0569	0.0507	0.0015
04T- 43	305	4	0.701	0.0	3.519	0.3911	0.0575	-0.0842	0.0493	-0.0021
04T- 43	305	5	0.699	0.0	5.834	0.5954	0.0801	-0.1180	0.0475	-0.0047
04T- 43	305	6	0.699	0.0	8.104	0.7760	0.1154	-0.1510	0.0441	-0.0077
04T- 43	305	7	0.700	0.0	10.289	0.9404	0.1694	-0.1886	0.0389	-0.0094
04T- 43	305	8	0.700	0.0	12.454	1.0384	0.2377	-0.2294	0.0269	-0.0097
04T- 43	305	9	0.699	0.0	14.599	1.1707	0.3155	-0.2759	0.0305	-0.0111
04T- 43	305	10	0.701	0.0	16.747	1.2824	0.3982	-0.3423	0.0262	-0.0100
04T- 43	305	11	0.700	0.0	18.970	1.4130	0.5011	-0.4236	0.0271	-0.0121
04T- 43	305	12	0.701	0.0	21.110	1.5354	0.6090	-0.4954	0.0256	-0.0130
04T- 43	305	13	0.699	0.0	23.216	1.6536	0.7249	-0.5671	0.0240	-0.0143
04T- 43	306	1	1.203	0.0	-1.093	-0.0510	0.0837	0.0077	0.0261	0.0020
04T- 43	306	2	1.202	0.0	-3.402	-0.2625	0.0975	0.0924	0.0246	0.0036
04T- 43	306	3	1.201	0.0	1.326	0.1903	0.0870	-0.0933	0.0295	0.0003
04T- 43	306	4	1.203	0.0	3.639	0.4220	0.1068	-0.1867	0.0304	-0.0022
04T- 43	306	5	1.204	0.0	6.080	0.6620	0.1453	-0.2763	0.0282	-0.0048
04T- 43	306	6	1.203	0.0	8.504	0.8814	0.2002	-0.3578	0.0261	-0.0065
04T- 43	306	7	1.204	0.0	10.806	1.0771	0.2685	-0.4495	0.0255	-0.0091
04T- 43	306	8	1.203	0.0	13.128	1.2657	0.3540	-0.5456	0.0241	-0.0115
04T- 43	306	9	1.202	0.0	15.435	1.4409	0.4543	-0.6519	0.0226	-0.0131
04T- 43	306	10	1.203	0.0	17.601	1.5870	0.5587	-0.7511	0.0210	-0.0135
04T- 43	306	11	1.205	0.0	19.842	1.7139	0.6723	-0.8448	0.0198	-0.0150
04T- 43	306	12	1.202	0.0	22.067	1.9233	0.7922	-0.9328	0.0198	-0.0186
04T- 43	306	13	1.205	0.0	22.892	1.8585	0.8371	-0.9654	0.0198	-0.0184
04T- 43	309	1	0.896	0.0	-1.041	-0.0009	0.0467	-0.0344	0.0289	0.0005
04T- 43	309	2	0.897	0.0	3.847	0.5058	0.0737	-0.0951	0.0273	-0.0032
04T- 43	309	3	0.896	0.0	6.212	0.7152	0.1105	-0.1225	0.0208	-0.0044
04T- 43	309	4	0.899	0.0	8.535	0.8945	0.1636	-0.1601	0.0207	-0.0049
04T- 43	309	5	0.901	0.0	17.951	1.1574	0.2995	-0.2682	0.0217	-0.0068
04T- 43	309	6	0.899	0.0	23.726	1.7431	0.8103	-0.6934	0.0122	-0.0062
04T- 43	310	1	0.897	0.0	-1.043	-0.0035	0.0469	-0.0316	0.0282	0.0007
04T- 43	310	2	0.898	0.0	-3.568	-0.2829	0.0643	-0.0050	0.0309	-0.0010
04T- 43	310	3	0.897	0.0	1.387	0.2643	0.0522	-0.0688	0.0327	-0.0004
04T- 43	310	4	0.900	0.0	3.863	0.5083	0.0750	-0.0953	0.0268	-0.0027
04T- 43	310	5	0.898	0.0	6.196	0.7120	0.1113	-0.1217	0.0213	-0.0040

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T-	43	310	6	0.899	0.0	8.530	0.8845	0.1615	-0.1582	0.0203	-0.0044
04T-	43	310	7	0.898	0.0	10.770	1.0364	0.2259	-0.2146	0.0236	-0.0049
04T-	43	310	8	0.898	0.0	12.901	1.1521	0.2974	-0.2668	0.0230	-0.0070
04T-	43	310	9	0.894	0.0	15.086	1.2742	0.3797	-0.3450	0.0194	-0.0071
04T-	43	310	10	0.898	0.0	17.288	1.4140	0.4798	-0.4415	0.0174	-0.0062
04T-	43	310	11	0.900	0.0	19.435	1.5296	0.5822	-0.5352	0.0149	-0.0048
04T-	43	310	12	0.898	0.0	21.620	1.6470	0.6970	-0.6198	0.0132	-0.0051
04T-	43	310	13	0.897	0.0	23.665	1.7320	0.8043	-0.6880	0.0129	-0.0066
04T-	43	311	1	0.801	0.0	-1.026	0.0050	0.0435	-0.0320	0.0328	0.0010
04T-	43	311	2	0.800	0.0	-3.385	-0.2234	0.0572	-0.0057	0.0301	0.0011
04T-	43	311	3	0.803	0.0	1.328	0.2391	0.0457	-0.0646	0.0354	0.0009
04T-	43	311	4	0.800	0.0	3.685	0.4504	0.0618	-0.0946	0.0362	-0.0015
04T-	43	311	5	0.803	0.0	6.015	0.6579	0.0913	-0.1234	0.0332	-0.0035
04T-	43	311	6	0.805	0.0	8.349	0.8584	0.1414	-0.1550	0.0314	-0.0044
04T-	43	311	7	0.801	0.0	10.519	0.9342	0.1999	-0.1883	0.0304	-0.0055
04T-	43	311	8	0.802	0.0	12.717	1.0925	0.2679	-0.2344	0.0282	-0.0072
04T-	43	311	9	0.802	0.0	14.902	1.2028	0.3474	-0.2998	0.0246	-0.0080
04T-	43	311	10	0.803	0.0	17.017	1.3330	0.4375	-0.3772	0.0211	-0.0073
04T-	43	311	11	0.800	0.0	19.214	1.4666	0.5423	-0.4650	0.0213	-0.0112
04T-	43	311	12	0.801	0.0	21.391	1.5750	0.6537	-0.5520	0.0197	-0.0119
04T-	43	311	13	0.803	0.0	23.412	1.6725	0.7627	-0.6170	0.0181	-0.0123
04T-	43	312	1	0.701	0.0	-1.020	0.0047	0.0425	-0.0287	0.0348	0.0009
04T-	43	312	2	0.700	0.0	-3.313	-0.2096	0.0547	-0.0016	0.0313	0.0003
04T-	43	312	3	0.697	0.0	1.291	0.2163	0.0444	-0.0599	0.0369	0.0015
04T-	43	312	4	0.700	0.0	3.523	0.3949	0.0569	-0.0859	0.0368	-0.0007
04T-	43	312	5	0.699	0.0	5.848	0.5967	0.0804	-0.1195	0.0358	-0.0032
04T-	43	312	6	0.702	0.0	8.099	0.7780	0.1189	-0.1487	0.0351	-0.0042
04T-	43	312	7	0.700	0.0	10.337	0.9338	0.1796	-0.1871	0.0303	-0.0052
04T-	43	312	8	0.699	0.0	12.505	1.0502	0.2470	-0.2198	0.0297	-0.0071
04T-	43	312	9	0.700	0.0	14.654	1.1639	0.3220	-0.2706	0.0246	-0.0079
04T-	43	312	10	0.699	0.0	16.808	1.2906	0.4074	-0.3371	0.0221	-0.0083
04T-	43	312	11	0.701	0.0	18.930	1.4078	0.5038	-0.4225	0.0217	-0.0107
04T-	43	312	12	0.701	0.0	21.124	1.5303	0.6143	-0.5003	0.0221	-0.0147
04T-	43	312	13	0.701	0.0	23.196	1.6389	0.7253	-0.5663	0.0201	-0.0145
04T-	43	313	1	1.202	0.0	-1.052	-0.0323	0.0785	0.0079	0.0166	0.0006
04T-	43	313	2	1.202	0.0	-3.432	-0.2543	0.0917	0.0950	0.0162	0.0020
04T-	43	313	3	1.204	0.0	1.315	0.2038	0.0832	-0.0882	0.0174	-0.0010
04T-	43	313	4	1.205	0.0	3.742	0.4440	0.1060	-0.1837	0.0182	-0.0021
04T-	43	313	5	1.203	0.0	6.105	0.6781	0.1463	-0.2739	0.0175	-0.0034
04T-	43	313	6	1.203	0.0	8.482	0.8973	0.2025	-0.3567	0.0161	-0.0041
04T-	43	313	7	1.204	0.0	10.816	1.0886	0.2739	-0.4494	0.0170	-0.0053
04T-	43	313	8	1.204	0.0	13.160	1.2743	0.3617	-0.5455	0.0171	-0.0071
04T-	43	313	9	1.202	0.0	15.394	1.4410	0.4598	-0.6471	0.0180	-0.0085
04T-	43	313	10	1.201	0.0	17.605	1.5851	0.5655	-0.7448	0.0184	-0.0092
04T-	43	313	11	1.203	0.0	19.847	1.7121	0.6809	-0.8408	0.0182	-0.0101
04T-	43	313	12	1.203	0.0	22.060	1.8138	0.8000	-0.9284	0.0190	-0.0132
04T-	43	313	13	1.203	0.0	24.123	1.9114	0.9192	-1.0247	0.0161	-0.0122

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	316	1	0.901	0.0	-1.083	-0.0226	0.0505	-0.0346	0.0257	-0.0005
04T- 43	316	2	0.899	0.0	3.798	0.4348	0.0751	-0.0941	0.0234	-0.0039
04T- 43	316	3	0.900	0.0	6.135	0.6851	0.1094	-0.1232	0.0150	-0.0048
04T- 43	316	4	0.897	0.0	8.415	0.8537	0.1562	-0.1642	0.0153	-0.0043
04T- 43	316	5	0.898	0.0	12.949	1.1704	0.2969	-0.2719	0.0251	-0.0063
04T- 43	316	6	0.897	0.0	23.627	1.7245	0.8363	-0.7034	0.0122	-0.0033
04T- 43	401	1	0.903	0.0	1.067	0.2286	0.0490	-0.0558	0.0343	0.0001
04T- 43	401	2	0.900	0.0	4.440	0.5596	0.0809	-0.1004	0.0285	-0.0031
04T- 43	401	3	0.905	0.0	6.457	0.7413	0.1191	-0.1286	0.0254	-0.0047
04T- 43	401	4	0.900	0.0	8.747	0.9075	0.1719	-0.1540	0.0239	-0.0059
04T- 43	401	5	0.898	0.0	9.647	0.9717	0.1975	-0.1764	0.0247	-0.0065
04T- 43	401	6	0.902	0.0	11.823	1.0873	0.2644	-0.2321	0.0184	-0.0062
04T- 43	401	7	0.902	0.0	22.937	1.6953	0.7643	-0.6200	0.0126	-0.0078
04T- 43	402	1	0.900	0.0	7.424	0.8236	0.1387	-0.1292	0.0247	-0.0051
04T- 43	402	2	0.901	0.0	9.605	0.9758	0.1981	-0.1711	0.0261	-0.0066
04T- 43	402	3	0.904	0.0	11.838	1.0869	0.2651	-0.2235	0.0185	-0.0061
04T- 43	402	4	0.902	0.0	14.007	1.2070	0.3419	-0.2977	0.0145	-0.0057
04T- 43	402	5	0.901	0.0	16.231	1.3355	0.4326	-0.3826	0.0176	-0.0067
04T- 43	402	6	0.897	0.0	18.334	1.4619	0.5302	-0.4625	0.0170	-0.0071
04T- 43	402	7	0.904	0.0	20.564	1.5933	0.6458	-0.5484	0.0143	-0.0066
04T- 43	402	8	0.903	0.0	22.788	1.6390	0.7626	-0.6230	0.0133	-0.0077
04T- 43	404	2	0.024	0.1	-1.000	-0.0021	0.0832	0.0012	-0.0112	-0.0018
04T- 43	404	3	0.024	-0.0	4.001	-0.1799	0.1428	0.5773	0.0042	0.0075
04T- 43	404	6	0.025	-0.1	19.008	0.2195	0.3445	0.0756	0.0279	0.0182
04T- 43	404	7	0.025	0.0	24.010	0.0284	0.3165	-0.4307	0.0238	0.0022
04T- 43	404	8	0.025	0.0	19.008	0.2181	0.3469	0.0759	0.0195	-0.0008
04T- 43	404	9	0.025	0.0	14.005	0.2146	0.2772	0.4806	0.0155	-0.0044
04T- 43	404	10	0.025	-0.0	9.002	-0.0305	0.1610	0.6342	0.0171	0.0112
04T- 43	404	11	0.024	0.1	4.001	0.0264	0.1640	0.5740	0.0220	0.0054
04T- 43	404	12	0.024	0.1	-1.000	0.1842	0.0854	-0.1615	0.0082	-0.0010
04T- 43	406	1	0.024	-0.2	-1.000	0.0022	0.1162	-0.0038	-0.0066	0.0249
04T- 43	406	2	0.024	-0.1	4.001	-0.1960	0.0982	0.0909	-0.0040	0.0093
04T- 43	406	3	0.024	-0.1	9.002	-0.0585	0.0984	0.0185	0.0109	0.0149
04T- 43	406	4	0.022	-0.2	13.994	-0.2022	0.1235	0.1386	0.0084	0.0251
04T- 43	406	5	0.250	-0.0	19.047	-0.0016	0.0011	0.0023	0.0	0.0001
04T- 43	406	6	0.022	-0.3	24.040	-0.1831	0.0741	0.2311	0.0462	0.0271
04T- 43	406	7	0.022	-0.2	19.027	-0.1624	0.0437	0.0891	0.0261	0.0270
04T- 43	406	8	0.022	-0.3	14.024	-0.1921	0.0524	0.1419	0.0275	0.0479
04T- 43	407	1	0.852	0.0	1.030	0.2171	0.0442	-0.0570	0.0358	0.0011
04T- 43	407	2	1.045	0.0	4.357	0.3456	0.0549	-0.0637	0.0230	-0.0016
04T- 43	407	3	0.849	0.0	4.357	0.5210	0.0711	-0.0957	0.0347	-0.0024
04T- 43	407	4	0.847	0.0	6.359	0.7038	0.1052	-0.1201	0.0312	-0.0040
04T- 43	407	5	0.848	0.0	8.617	0.8737	0.1574	-0.1465	0.0281	-0.0056
04T- 43	407	6	0.849	0.0	9.543	0.9331	0.1823	-0.1645	0.0287	-0.0062
04T- 43	407	7	0.949	0.0	11.690	1.0349	0.2445	-0.2127	0.0208	-0.0060

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	407	8	0.849	0.0	20.390	1.5419	0.6135	-0.4981	0.0166	-0.0070
04T- 43	408	1	0.850	0.0	0.225	0.1439	0.0417	-0.0486	0.0360	0.0021
04T- 43	408	2	0.849	0.0	0.224	0.1437	0.0417	-0.0486	0.0359	0.0021
04T- 43	408	3	0.849	0.0	0.223	0.1435	0.0417	-0.0488	0.0359	0.0021
04T- 43	408	4	0.851	0.0	0.223	0.1438	0.0416	-0.0489	0.0359	0.0021
04T- 43	408	5	0.849	0.0	0.223	0.1442	0.0418	-0.0491	0.0359	0.0020
04T- 43	408	6	0.849	0.0	0.218	0.1436	0.0418	-0.0493	0.0359	0.0021
04T- 43	409	1	0.850	0.0	0.220	0.1439	0.0416	-0.0494	0.0359	0.0021
04T- 43	409	2	0.849	0.0	2.540	0.3588	0.0528	-0.0763	0.0360	-0.0002
04T- 43	409	3	0.846	0.0	4.927	0.5865	0.0793	-0.1049	0.0349	-0.0027
04T- 43	409	4	0.848	0.0	7.226	0.7959	0.1246	-0.1240	0.0291	-0.0045
04T- 43	409	5	0.848	0.0	9.542	0.9293	0.1829	-0.1593	0.0258	-0.0058
04T- 43	409	6	0.850	0.0	13.878	1.1569	0.3218	-0.2695	0.0221	-0.0071
04T- 43	409	7	0.848	0.0	16.033	1.2883	0.4086	-0.3418	0.0200	-0.0067
04T- 43	409	8	0.850	0.0	18.182	1.4211	0.5060	-0.4143	0.0189	-0.0072
04T- 43	410	1	0.700	0.0	-2.182	-0.0936	0.0399	-0.0177	0.0386	0.0051
04T- 43	410	2	0.700	0.0	0.156	0.1151	0.0370	-0.0439	0.0386	0.0025
04T- 43	410	3	0.700	0.0	2.396	0.3050	0.0452	-0.0706	0.0385	0.0002
04T- 43	410	4	0.701	0.0	4.671	0.4932	0.0630	-0.0977	0.0378	-0.0022
04T- 43	410	5	0.699	0.0	6.980	0.6903	0.0959	-0.1254	0.0358	-0.0052
04T- 43	410	6	0.700	0.0	9.253	0.8522	0.1510	-0.1522	0.0292	-0.0070
04T- 43	410	7	0.700	0.0	11.384	0.9763	0.2136	-0.1905	0.0239	-0.0075
04T- 43	410	8	0.698	0.0	13.612	1.0994	0.2855	-0.2222	0.0247	-0.0090
04T- 43	410	9	0.699	0.0	15.725	1.2148	0.3616	-0.2760	0.0212	-0.0086
04T- 43	410	10	0.699	0.0	17.736	1.3386	0.4505	-0.3547	0.0190	-0.0084
04T- 43	410	11	0.700	0.0	19.962	1.4482	0.5500	-0.4293	0.0185	-0.0096
04T- 43	410	12	0.700	0.0	22.208	1.5731	0.6697	-0.5044	0.0173	-0.0096
04T- 43	411	1	0.797	0.0	-2.214	-0.0998	0.0430	-0.0218	0.0370	0.0050
04T- 43	411	2	0.799	0.0	0.211	0.1368	0.0398	-0.0501	0.0371	0.0024
04T- 43	411	3	0.799	0.0	2.430	0.3327	0.0493	-0.0754	0.0371	0.0001
04T- 43	411	4	0.795	0.0	4.811	0.5457	0.0700	-0.1032	0.0371	-0.0025
04T- 43	411	5	0.801	0.0	7.133	0.7597	0.1126	-0.1284	0.0353	-0.0048
04T- 43	411	6	0.801	0.0	9.429	0.9108	0.1704	-0.1601	0.0257	-0.0061
04T- 43	411	7	0.800	0.0	11.563	1.0141	0.2318	-0.1970	0.0204	-0.0065
04T- 43	411	8	0.801	0.0	13.768	1.1286	0.3069	-0.2485	0.0241	-0.0076
04T- 43	411	9	0.800	0.0	15.910	1.2519	0.3886	-0.3093	0.0213	-0.0073
04T- 43	411	10	0.799	0.0	18.097	1.3888	0.4868	-0.3868	0.0197	-0.0073
04T- 43	411	11	0.797	0.0	20.291	1.5169	0.5976	-0.4749	0.0178	-0.0071
04T- 43	411	12	0.797	0.0	22.444	1.6178	0.7114	-0.5537	0.0180	-0.0102
04T- 43	412	1	0.902	0.0	-2.251	-0.1132	0.0503	-0.0319	0.0351	0.0042
04T- 43	412	2	0.902	0.0	0.225	0.1492	0.0469	-0.0554	0.0344	0.0015
04T- 43	412	3	0.898	0.0	2.580	0.3811	0.0596	-0.0806	0.0342	-0.0009
04T- 43	412	4	0.897	0.0	5.024	0.6244	0.0911	-0.1102	0.0298	-0.0031
04T- 43	412	5	0.901	0.0	7.396	0.8321	0.1417	-0.1369	0.0267	-0.0051
04T- 43	412	6	0.904	0.0	9.720	0.9777	0.2018	-0.1771	0.0245	-0.0056

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	412	7	0.899	0.0	11.795	1.0793	0.2630	-0.2215	0.0191	-0.0053
04T- 43	412	8	0.899	0.0	13.991	1.1987	0.3430	-0.2963	0.0187	-0.0058
04T- 43	412	9	0.905	0.0	16.171	1.3314	0.4340	-0.3800	0.0173	-0.0053
04T- 43	412	10	0.900	0.0	18.345	1.4699	0.5377	-0.4660	0.0173	-0.0058
04T- 43	412	11	0.900	0.0	20.508	1.5844	0.6435	-0.5450	0.0157	-0.0060
04T- 43	412	12	0.900	0.0	22.708	1.6891	0.7591	-0.6191	0.0145	-0.0070
04T- 43	413	1	0.949	0.0	-2.354	-0.1634	0.0601	-0.0291	0.0358	0.0040
04T- 43	413	2	0.946	0.0	0.186	0.1512	0.0560	-0.0632	0.0342	0.0009
04T- 43	413	3	0.948	0.0	2.785	0.4210	0.0747	-0.0925	0.0281	-0.0017
04T- 43	413	4	0.947	0.0	5.049	0.6360	0.1075	-0.1287	0.0253	-0.0036
04T- 43	413	5	0.947	0.0	7.410	0.8475	0.1602	-0.1753	0.0239	-0.0055
04T- 43	413	6	0.950	0.0	9.844	1.0469	0.2314	-0.2300	0.0223	-0.0072
04T- 43	413	7	0.948	0.0	12.096	1.2276	0.3110	-0.2954	0.0223	-0.0081
04T- 43	413	8	0.943	0.0	14.259	1.3764	0.3957	-0.3551	0.0216	-0.0089
04T- 43	413	9	0.948	-0.0	16.403	1.4341	0.4735	-0.4136	0.0090	-0.0013
04T- 43	413	10	0.946	0.0	18.501	1.5394	0.5695	-0.5075	0.0147	-0.0060
04T- 43	413	11	0.947	0.0	20.775	1.6691	0.6902	-0.6071	0.0113	-0.0052
04T- 43	413	12	0.948	0.0	22.918	1.7618	0.8033	-0.6766	0.0098	-0.0056
04T- 43	414	1	1.188	-0.0	-2.226	-0.1393	0.0719	0.0504	0.0181	0.0026
04T- 43	414	2	1.196	-0.0	-2.231	-0.1393	0.0717	0.0536	0.0179	0.0026
04T- 43	414	3	1.197	-0.0	0.210	0.0964	0.0682	-0.0337	0.0201	0.0008
04T- 43	414	4	1.196	-0.0	2.482	0.3259	0.0824	-0.1246	0.0224	-0.0007
04T- 43	414	5	1.194	-0.0	4.963	0.5743	0.1182	-0.2197	0.0224	-0.0020
04T- 43	414	6	1.196	0.0	7.325	0.7874	0.1674	-0.2940	0.0205	-0.0035
04T- 43	414	7	1.196	0.0	9.700	0.9848	0.2319	-0.3708	0.0195	-0.0055
04T- 43	414	8	1.195	0.0	12.058	1.1760	0.3139	-0.4664	0.0199	-0.0075
04T- 43	414	9	1.196	0.0	14.307	1.3442	0.4053	-0.5584	0.0195	-0.0087
04T- 43	414	10	1.197	0.0	16.515	1.4924	0.5057	-0.6508	0.0204	-0.0105
04T- 43	414	11	1.195	0.0	18.676	1.6248	0.6137	-0.7425	0.0196	-0.0118
04T- 43	414	12	1.193	0.0	20.910	1.7423	0.7316	-0.8346	0.0197	-0.0149
04T- 43	414	13	1.190	0.0	23.076	1.8365	0.8507	-0.9153	0.0177	-0.0156
04T- 43	417	1	0.902	0.0	0.994	0.2041	0.0546	-0.0763	0.0379	0.0033
04T- 43	417	2	0.903	0.0	4.397	0.5466	0.0839	-0.1125	0.0343	-0.0011
04T- 43	417	3	0.901	0.0	6.419	0.7293	0.1172	-0.1398	0.0325	-0.0035
04T- 43	417	4	0.903	0.0	8.735	0.9036	0.1691	-0.1759	0.0294	-0.0064
04T- 43	417	5	0.902	0.0	9.633	0.9688	0.1920	-0.1998	0.0275	-0.0073
04T- 43	417	6	0.902	0.0	11.789	1.0380	0.2541	-0.2389	0.0204	-0.0082
04T- 43	417	7	0.900	0.0	20.511	1.5897	0.6266	-0.5589	0.0128	-0.0074
04T- 43	418	1	0.903	0.0	-2.271	-0.1124	0.0591	-0.0503	0.0310	0.0067
04T- 43	418	2	0.904	0.0	-2.270	-0.1125	0.0591	-0.0504	0.0310	0.0067
04T- 43	418	3	0.902	0.0	0.145	0.1232	0.0530	-0.0714	0.0373	0.0044
04T- 43	418	4	0.898	0.0	2.563	0.3643	0.0637	-0.0950	0.0376	0.0013
04T- 43	418	5	0.902	0.0	4.982	0.6025	0.0922	-0.1205	0.0336	-0.0018
04T- 43	418	6	0.901	0.0	7.303	0.8020	0.1351	-0.1506	0.0294	-0.0044
04T- 43	418	7	0.900	0.0	9.539	0.9605	0.1893	-0.2002	0.0275	-0.0070
04T- 43	418	8	0.900	0.0	11.838	1.0941	0.2560	-0.2403	0.0201	-0.0080

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T-	43 418	9	0.901	0.0	14.052	1.2233	0.3330	-0.3114	0.0154	-0.0070
04T-	43 418	10	0.904	0.0	16.248	1.3652	0.4257	-0.4027	0.0109	-0.0045
04T-	43 418	11	0.901	0.0	18.422	1.4922	0.5270	-0.4841	0.0124	-0.0054
04T-	43 419	1	0.698	0.0	-2.177	-0.0880	0.0493	-0.0415	0.0364	0.0076
04T-	43 419	2	0.700	0.0	0.130	0.1032	0.0439	-0.0609	0.0415	0.0048
04T-	43 419	3	0.699	0.0	2.390	0.2932	0.0479	-0.0848	0.0417	0.0016
04T-	43 419	4	0.698	0.0	4.630	0.4854	0.0624	-0.1113	0.0402	-0.0017
04T-	43 419	5	0.697	0.0	6.938	0.6850	0.0936	-0.1403	0.0383	-0.0053
04T-	43 419	6	0.699	0.0	9.188	0.8479	0.1407	-0.1723	0.0293	-0.0091
04T-	43 419	7	0.698	0.0	11.378	0.9907	0.1969	-0.2093	0.0192	-0.0115
04T-	43 419	8	0.701	0.0	13.546	1.1204	0.2675	-0.2455	0.0151	-0.0113
04T-	43 419	9	0.698	0.0	15.718	1.2416	0.3513	-0.3009	0.0142	-0.0093
04T-	43 419	10	0.701	0.0	17.790	1.3549	0.4391	-0.3704	0.0131	-0.0079
04T-	43 420	1	0.800	0.0	-2.212	-0.0930	0.0528	-0.0462	0.0341	0.0073
04T-	43 420	2	0.800	0.0	0.179	0.1167	0.0462	-0.0658	0.0407	0.0048
04T-	43 420	3	0.799	0.0	2.412	0.3204	0.0528	-0.0896	0.0419	0.0017
04T-	43 420	4	0.799	0.0	4.785	0.5367	0.0720	-0.1163	0.0397	-0.0014
04T-	43 420	5	0.801	0.0	7.078	0.7466	0.1096	-0.1442	0.0380	-0.0046
04T-	43 420	6	0.797	0.0	9.390	0.8941	0.1587	-0.1762	0.0271	-0.0080
04T-	43 420	7	0.799	0.0	11.616	1.0257	0.2200	-0.2113	0.0177	-0.0095
04T-	43 420	8	0.797	0.0	13.817	1.1600	0.2947	-0.2647	0.0150	-0.0085
04T-	43 420	9	0.797	0.0	15.879	1.2725	0.3745	-0.3285	0.0151	-0.0081
04T-	43 420	10	0.798	0.0	18.075	1.3978	0.4733	-0.4108	0.0160	-0.0082
04T-	43 421	1	1.197	-0.0	-2.275	-0.1619	0.0833	0.0504	0.0204	0.0075
04T-	43 421	2	1.199	-0.0	0.091	0.0614	0.0777	-0.0365	0.0247	0.0058
04T-	43 421	3	1.199	-0.0	2.479	0.2980	0.0896	-0.1346	0.0288	0.0035
04T-	43 421	4	1.197	0.0	4.905	0.5395	0.1194	-0.2297	0.0299	0.0001
04T-	43 421	5	1.197	0.0	7.223	0.7581	0.1634	-0.3059	0.0270	-0.0029
04T-	43 421	6	1.199	0.0	9.640	0.9646	0.2254	-0.3849	0.0252	-0.0059
04T-	43 421	7	1.196	0.0	11.942	1.1594	0.3022	-0.4795	0.0244	-0.0092
04T-	43 421	8	1.196	0.0	14.251	1.3424	0.3948	-0.5806	0.0221	-0.0112
04T-	43 421	9	1.198	0.0	16.477	1.5004	0.4958	-0.6794	0.0202	-0.0124
04T-	43 421	10	1.197	0.0	18.685	1.6407	0.6061	-0.7720	0.0188	-0.0147
04T-	43 421	11	1.199	-0.0	-1.093	-0.0531	0.0781	0.0104	0.0225	0.0068
04T-	43 424	1	0.902	0.0	0.951	0.1792	0.0519	-0.0550	0.0255	-0.0010
04T-	43 424	2	0.896	0.0	4.350	0.5253	0.0801	-0.1022	0.0227	-0.0033
04T-	43 424	3	0.895	0.0	6.394	0.7123	0.1138	-0.1293	0.0176	-0.0043
04T-	43 424	5	0.897	0.0	9.518	0.9456	0.1861	-0.1868	0.0187	-0.0039
04T-	43 424	6	0.901	0.0	11.782	1.0839	0.2515	-0.2382	0.0254	-0.0041
04T-	43 424	7	0.900	0.0	20.454	1.5886	0.6248	-0.5497	0.0159	-0.0029
04T-	43 425	1	0.897	0.0	-2.377	-0.1665	0.0576	-0.0253	0.0289	0.0010
04T-	43 425	2	0.900	0.0	0.132	0.0939	0.0492	-0.0459	0.0247	-0.0007
04T-	43 425	3	0.900	0.0	2.528	0.3434	0.0610	-0.0772	0.0256	-0.0021
04T-	43 425	4	0.899	0.0	4.997	0.5886	0.0906	-0.1113	0.0205	-0.0036
04T-	43 425	5	0.900	0.0	7.304	0.7896	0.1339	-0.1422	0.0158	-0.0044

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	425	6	0.899	0.0	9.596	0.9561	0.1892	-0.1881	0.0192	-0.0042
04T- 43	425	7	0.898	0.0	11.761	1.0759	0.2483	-0.2371	0.0239	-0.0032
04T- 43	425	8	0.898	0.0	13.989	1.2186	0.3275	-0.3069	0.0258	-0.0054
04T- 43	425	9	0.899	0.0	16.140	1.3473	0.4164	-0.3707	0.0226	-0.0075
04T- 43	426	1	0.699	0.0	-2.223	-0.1329	0.0468	-0.0181	0.0316	0.0029
04T- 43	426	2	0.701	0.0	0.089	0.0790	0.0394	-0.0452	0.0321	0.0009
04T- 43	426	3	0.700	0.0	2.323	0.2646	0.0450	-0.0778	0.0352	-0.0002
04T- 43	426	4	0.700	0.0	4.647	0.4886	0.0620	-0.1107	0.0363	-0.0022
04T- 43	426	5	0.699	0.0	6.868	0.6776	0.0900	-0.1410	0.0345	-0.0040
04T- 43	426	6	0.700	0.0	9.215	0.8714	0.1400	-0.1754	0.0340	-0.0037
04T- 43	426	7	0.699	0.0	11.372	1.0168	0.1998	-0.2062	0.0356	-0.0042
04T- 43	426	8	0.701	0.0	13.524	1.1308	0.2687	-0.2430	0.0329	-0.0060
04T- 43	426	9	0.696	0.0	15.723	1.2473	0.3540	-0.2959	0.0270	-0.0083
04T- 43	426	10	0.699	0.0	17.806	1.3586	0.4418	-0.3651	0.0223	-0.0084
04T- 43	427	1	0.799	0.0	-2.261	-0.1390	0.0505	-0.0206	0.0302	0.0018
04T- 43	427	2	0.800	0.0	0.119	0.0919	0.0426	-0.0466	0.0296	0.0007
04T- 43	427	3	0.799	0.0	2.462	0.3200	0.0501	-0.0817	0.0334	-0.0005
04T- 43	427	4	0.798	0.0	4.759	0.5314	0.0703	-0.1131	0.0339	-0.0026
04T- 43	427	5	0.796	0.0	7.104	0.7328	0.1078	-0.1405	0.0295	-0.0042
04T- 43	427	6	0.799	0.0	9.428	0.9091	0.1603	-0.1707	0.0279	-0.0037
04T- 43	427	7	0.799	0.0	11.584	1.0541	0.2226	-0.2133	0.0295	-0.0049
04T- 43	427	8	0.796	0.0	13.800	1.1624	0.2946	-0.2539	0.0319	-0.0068
04T- 43	427	9	0.798	0.0	15.941	1.2768	0.3793	-0.3155	0.0270	-0.0084
04T- 43	427	10	0.799	0.0	18.058	1.3963	0.4729	-0.3963	0.0219	-0.0064
04T- 43	428	1	1.186	0.0	-2.266	-0.1571	0.0845	0.0423	0.0161	-0.0006
04T- 43	428	2	1.191	0.0	-2.240	-0.1553	0.0844	0.0444	0.0159	-0.0005
04T- 43	428	3	1.194	0.0	-2.271	-0.1581	0.0844	0.0467	0.0156	-0.0005
04T- 43	428	4	1.195	0.0	-2.271	-0.1584	0.0845	0.0474	0.0158	-0.0004
04T- 43	428	5	1.197	0.0	-2.268	-0.1582	0.0844	0.0481	0.0158	-0.0004
04T- 43	428	6	1.196	0.0	0.114	0.0665	0.0783	-0.0415	0.0153	-0.0022
04T- 43	428	7	1.195	0.0	2.443	0.2941	0.0898	-0.1305	0.0143	-0.0028
04T- 43	428	8	1.196	0.0	4.818	0.5252	0.1170	-0.2160	0.0132	-0.0030
04T- 43	428	9	1.195	0.0	7.229	0.7553	0.1626	-0.2980	0.0134	-0.0031
04T- 43	428	10	1.195	0.0	9.560	0.9575	0.2223	-0.3780	0.0131	-0.0032
04T- 43	428	11	1.193	0.0	11.903	1.1508	0.2990	-0.4677	0.0146	-0.0044
04T- 43	428	12	1.198	0.0	14.190	1.3282	0.3885	-0.5663	0.0154	-0.0050
04T- 43	428	13	1.196	0.0	16.445	1.4896	0.4912	-0.6652	0.0170	-0.0061
04T- 43	428	14	1.194	0.0	18.665	1.6317	0.6011	-0.7591	0.0165	-0.0055
04T- 43	428	15	1.198	0.0	20.873	1.7442	0.7143	-0.8454	0.0180	-0.0081
04T- 43	431	1	0.898	0.0	1.042	0.2269	0.0419	-0.0661	-0.0048	-0.0041
04T- 43	431	2	0.902	0.0	4.388	0.5313	0.0722	-0.0954	-0.0053	-0.0030
04T- 43	431	3	0.902	0.0	6.386	0.7043	0.1050	-0.1248	-0.0049	-0.0020
04T- 43	431	4	0.898	-0.0	8.672	0.8905	0.1553	-0.1677	-0.0034	-0.0004
04T- 43	431	5	0.898	-0.0	9.562	0.9556	0.1782	-0.1882	-0.0020	0.0003
04T- 43	431	6	0.899	-0.0	11.843	1.1354	0.2496	-0.2468	0.0008	0.0017
04T- 43	431	7	0.899	-0.0	20.499	1.6001	0.6171	-0.5638	0.0047	0.0017

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	432	1	0.903	0.0	-2.218	-0.0662	0.0460	-0.0610	0.0042	-0.0050
04T- 43	432	2	0.902	0.0	0.168	0.1475	0.0400	-0.0637	-0.0032	-0.0046
04T- 43	432	3	0.899	0.0	2.594	0.3701	0.0516	-0.0789	-0.0054	-0.0037
04T- 43	432	4	0.899	0.0	4.915	0.5816	0.0794	-0.1040	-0.0049	-0.0028
04T- 43	432	5	0.893	0.0	7.321	0.7838	0.1224	-0.1383	-0.0045	-0.0015
04T- 43	432	6	0.900	-0.0	9.580	0.9598	0.1795	-0.1925	-0.0019	0.0002
04T- 43	432	7	0.900	-0.0	11.840	1.1322	0.2488	-0.2457	0.0005	0.0017
04T- 43	432	8	0.901	-0.0	13.944	1.2370	0.3199	-0.3150	0.0080	0.0003
04T- 43	432	9	0.899	0.0	16.171	1.3717	0.4109	-0.3920	0.0093	-0.0025
04T- 43	432	10	0.898	-0.0	18.338	1.4346	0.5093	-0.4763	0.0067	-0.0008
04T- 43	433	1	0.699	0.0	-2.131	-0.0667	0.0377	-0.0378	0.0006	-0.0045
04T- 43	433	2	0.699	0.0	0.140	0.1248	0.0315	-0.0534	-0.0017	-0.0035
04T- 43	433	3	0.701	0.0	2.453	0.3192	0.0365	-0.0718	-0.0006	-0.0020
04T- 43	433	4	0.699	0.0	4.681	0.5086	0.0525	-0.0965	-0.0002	-0.0014
04T- 43	433	5	0.698	-0.0	6.978	0.7033	0.0834	-0.1309	-0.0	-0.0003
04T- 43	433	6	0.701	-0.0	9.221	0.8736	0.1313	-0.1637	0.0035	0.0019
04T- 43	433	7	0.699	-0.0	11.436	1.0171	0.1892	-0.1978	0.0117	0.0036
04T- 43	433	8	0.700	-0.0	13.587	1.1427	0.2614	-0.2414	0.0113	0.0031
04T- 43	433	9	0.701	-0.0	15.700	1.2521	0.3430	-0.2964	0.0084	0.0016
04T- 43	433	10	0.700	-0.0	17.893	1.3775	0.4393	-0.3781	0.0084	0.0001
04T- 43	434	1	0.800	0.0	-2.151	-0.0647	0.0398	-0.0436	0.0013	-0.0046
04T- 43	434	2	0.800	0.0	0.185	0.1385	0.0336	-0.0573	-0.0016	-0.0037
04T- 43	434	3	0.798	0.0	2.519	0.3447	0.0406	-0.0757	-0.0007	-0.0023
04T- 43	434	4	0.798	0.0	4.823	0.5478	0.0605	-0.0985	-0.0015	-0.0018
04T- 43	434	5	0.798	0.0	7.127	0.7408	0.0978	-0.1270	-0.0038	-0.0007
04T- 43	434	6	0.799	-0.0	9.371	0.8998	0.1474	-0.1602	0.0011	0.0015
04T- 43	434	7	0.801	-0.0	11.585	1.0420	0.2103	-0.2032	0.0078	0.0027
04T- 43	434	8	0.799	-0.0	13.783	1.1736	0.2858	-0.2600	0.0077	0.0019
04T- 43	434	9	0.800	-0.0	15.914	1.2839	0.3658	-0.3229	0.0089	-0.0001
04T- 43	434	10	0.798	-0.0	18.072	1.4097	0.4622	-0.4056	0.0062	0.0006
04T- 43	435	1	1.197	0.0	-2.273	-0.1644	0.0708	0.0493	-0.0017	-0.0061
04T- 43	435	2	1.196	0.0	0.054	0.0503	0.0641	-0.0370	-0.0039	-0.0063
04T- 43	435	3	1.198	0.0	2.429	0.2786	0.0741	-0.1324	-0.0058	-0.0051
04T- 43	435	4	1.195	0.0	4.825	0.5168	0.1022	-0.2293	-0.0065	-0.0036
04T- 43	435	5	1.196	0.0	7.181	0.7473	0.1477	-0.3182	-0.0052	-0.0020
04T- 43	435	6	1.195	0.0	9.589	0.9635	0.2109	-0.4007	-0.0044	-0.0005
04T- 43	435	7	1.195	-0.0	11.887	1.1565	0.2870	-0.4876	-0.0040	0.0009
04T- 43	435	8	1.194	-0.0	14.190	1.3456	0.3804	-0.5963	-0.0027	0.0018
04T- 43	435	9	1.195	-0.0	16.415	1.5092	0.4826	-0.6947	-0.0008	0.0019
04T- 43	435	10	1.192	-0.0	18.681	1.6578	0.5972	-0.7919	0.0004	0.0030
04T- 43	438	1	0.701	0.0	-2.115	-0.0501	0.0291	-0.0270	0.0023	-0.0024
04T- 43	438	2	0.700	0.0	0.172	0.1452	0.0265	-0.0435	0.0020	-0.0021
04T- 43	438	3	0.701	0.0	2.474	0.3336	0.0356	-0.0631	0.0022	-0.0019
04T- 43	438	4	0.700	0.0	4.697	0.5205	0.0535	-0.0886	0.0023	-0.0019
04T- 43	438	5	0.699	0.0	6.976	0.7149	0.0868	-0.1206	0.0021	-0.0018
04T- 43	438	6	0.699	0.0	9.237	0.8720	0.1416	-0.1497	0.0001	-0.0014

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	438	7	0.700	0.0	11.369	0.9957	0.2044	-0.1841	0.0023	-0.0009
04T- 43	438	8	0.701	0.0	13.570	1.1212	0.2780	-0.2297	0.0019	-0.0007
04T- 43	438	9	0.700	0.0	15.699	1.2423	0.3573	-0.2800	0.0010	-0.0002
04T- 43	438	10	0.702	0.0	17.841	1.3632	0.4479	-0.3589	0.0019	-0.0006
04T- 43	439	1	0.800	0.0	-2.114	-0.0488	0.0308	-0.0328	0.0022	-0.0024
04T- 43	439	2	0.799	0.0	0.200	0.1595	0.0276	-0.0472	0.0020	-0.0021
04T- 43	439	3	0.797	0.0	2.512	0.3588	0.0379	-0.0659	0.0023	-0.0019
04T- 43	440	1	0.796	0.0	-2.111	-0.0495	0.0303	-0.0326	0.0022	-0.0024
04T- 43	440	2	0.801	0.0	0.227	0.1523	0.0279	-0.0479	0.0020	-0.0021
04T- 43	440	3	0.796	0.0	2.522	0.3580	0.0379	-0.0659	0.0023	-0.0019
04T- 43	440	4	0.797	0.0	4.890	0.5705	0.0608	-0.0908	0.0024	-0.0018
04T- 43	440	5	0.799	0.0	7.214	0.7729	0.1023	-0.1184	0.0036	-0.0015
04T- 43	440	6	0.798	0.0	9.427	0.9169	0.1574	-0.1497	0.0022	-0.0012
04T- 43	440	7	0.797	0.0	11.552	1.0259	0.2213	-0.1924	0.0010	-0.0006
04T- 43	440	8	0.800	0.0	13.779	1.1541	0.2986	-0.2521	0.0017	-0.0004
04T- 43	440	9	0.798	0.0	15.915	1.2743	0.3803	-0.3153	0.0018	-0.0006
04T- 43	440	10	0.801	0.0	18.122	1.4153	0.4815	-0.3985	0.0024	-0.0007
04T- 43	441	1	0.900	0.0	-2.156	-0.0595	0.0346	-0.0457	0.0020	-0.0025
04T- 43	441	2	0.899	0.0	0.266	0.1806	0.0321	-0.0569	0.0018	-0.0024
04T- 43	441	3	0.897	0.0	2.656	0.4014	0.0465	-0.0723	0.0017	-0.0023
04T- 43	441	4	0.900	0.0	5.026	0.6138	0.0785	-0.0949	0.0018	-0.0022
04T- 43	441	5	0.897	0.0	7.354	0.8141	0.1259	-0.1246	0.0030	-0.0021
04T- 43	441	6	0.897	0.0	9.693	0.9935	0.1892	-0.1699	0.0037	-0.0019
04T- 43	441	7	0.900	0.0	11.845	1.1274	0.2569	-0.2206	0.0016	-0.0012
04T- 43	441	8	0.903	0.0	13.979	1.2233	0.3325	-0.3022	0.0022	-0.0008
04T- 43	441	9	0.902	0.0	16.159	1.3542	0.4223	-0.3889	0.0029	-0.0011
04T- 43	441	10	0.900	0.0	18.316	1.4824	0.5220	-0.4712	0.0042	-0.0019
04T- 43	444	2	0.901	0.0	1.060	0.2385	0.0410	-0.0732	0.0009	-0.0015
04T- 43	444	3	0.905	0.0	4.383	0.5306	0.0708	-0.0977	0.0010	-0.0017
04T- 43	444	4	0.901	0.0	6.355	0.7001	0.1014	-0.1272	0.0008	-0.0015
04T- 43	444	5	0.904	0.0	8.730	0.9094	0.1555	-0.1789	0.0009	-0.0012
04T- 43	444	6	0.903	0.0	9.660	0.9816	0.1794	-0.1914	0.0022	-0.0013
04T- 43	444	7	0.901	0.0	11.877	1.1492	0.2500	-0.2541	0.0035	-0.0016
04T- 43	445	1	0.904	-0.0	-2.225	-0.0701	0.0475	-0.0605	0.0006	-0.0023
04T- 43	445	2	0.903	-0.0	0.307	0.1663	0.0396	-0.0692	0.0007	-0.0018
04T- 43	445	3	0.898	-0.0	2.662	0.3826	0.0505	-0.0826	0.0012	-0.0017
04T- 43	445	4	0.901	-0.0	5.055	0.5901	0.0800	-0.1065	0.0011	-0.0016
04T- 43	445	5	0.902	-0.0	7.280	0.7802	0.1194	-0.1436	0.0008	-0.0014
04T- 43	445	6	0.902	-0.0	9.666	0.9859	0.1807	-0.1922	0.0026	-0.0013
04T- 43	445	7	0.900	0.0	11.949	1.1443	0.2499	-0.2516	0.0038	-0.0017
04T- 43	446	1	0.699	-0.0	-2.126	-0.0696	0.0382	-0.0386	0.0016	-0.0021
04T- 43	446	2	0.700	-0.0	0.154	0.1303	0.0305	-0.0574	0.0017	-0.0017
04T- 43	446	3	0.701	-0.0	2.435	0.3219	0.0348	-0.0734	0.0016	-0.0015

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	447	1	0.799	-0.0	-2.177	-0.0715	0.0411	-0.0461	0.0014	-0.0020
04T- 43	447	2	0.801	-0.0	0.296	0.1535	0.0329	-0.0641	0.0018	-0.0016
04T- 43	447	3	0.801	-0.0	2.542	0.3554	0.0388	-0.0792	0.0018	-0.0013
04T- 43	447	4	0.799	-0.0	4.871	0.5609	0.0606	-0.1064	0.0018	-0.0011
04T- 43	447	5	0.800	-0.0	7.242	0.7701	0.0973	-0.1388	0.0012	-0.0010
04T- 43	447	6	0.795	-0.0	9.489	0.9347	0.1470	-0.1635	0.0028	-0.0006
04T- 43	447	7	0.795	-0.0	11.683	1.0641	0.2119	-0.2087	0.0008	-0.0003
04T- 43	447	8	0.796	-0.0	13.893	1.1870	0.2933	-0.2665	0.0005	0.0003
04T- 43	447	9	0.799	-0.0	15.967	1.2989	0.3754	-0.3389	0.0030	-0.0004
04T- 43	447	10	0.798	-0.0	18.110	1.4233	0.4704	-0.4160	0.0031	-0.0007
04T- 43	448	1	0.702	-0.0	-2.168	-0.0737	0.0383	-0.0402	0.0016	-0.0021
04T- 43	448	2	0.701	-0.0	0.166	0.1303	0.0309	-0.0586	0.0017	-0.0017
04T- 43	448	3	0.701	-0.0	2.476	0.3054	0.0356	-0.0733	0.0016	-0.0016
04T- 43	448	4	0.701	-0.0	4.757	0.5152	0.0531	-0.1020	0.0016	-0.0013
04T- 43	448	5	0.696	-0.0	6.956	0.6922	0.0797	-0.1328	0.0019	-0.0012
04T- 43	448	6	0.698	-0.0	9.226	0.8829	0.1239	-0.1677	0.0016	-0.0010
04T- 43	448	7	0.699	-0.0	11.455	1.0252	0.1903	-0.2037	0.0017	-0.0005
04T- 43	448	8	0.698	-0.0	13.592	1.1334	0.2632	-0.2428	0.0019	-0.0003
04T- 43	448	9	0.696	-0.0	15.785	1.2691	0.3505	-0.3072	0.0030	-0.0001
04T- 43	448	10	0.696	-0.0	17.782	1.3823	0.4388	-0.3721	0.0025	0.0003
04T- 43	449	1	1.195	-0.0	-2.338	-0.1711	0.0703	0.0422	0.0012	-0.0024
04T- 43	449	2	1.195	-0.0	-2.338	-0.1711	0.0706	0.0421	0.0012	-0.0024
04T- 43	449	3	1.197	-0.0	-2.334	-0.1707	0.0705	0.0435	0.0012	-0.0023
04T- 43	449	4	1.198	-0.0	0.067	0.0467	0.0628	-0.0429	0.0010	-0.0025
04T- 43	449	5	1.197	-0.0	2.415	0.2724	0.0716	-0.1370	0.0007	-0.0022
04T- 43	449	6	1.196	-0.0	4.929	0.5305	0.1008	-0.2415	0.0006	-0.0020
04T- 43	449	7	1.193	-0.0	7.223	0.7598	0.1469	-0.3257	0.0005	-0.0020
04T- 43	449	8	1.191	0.0	9.523	0.9558	0.2063	-0.4014	0.0006	-0.0017
04T- 43	449	9	1.195	0.0	11.930	1.1630	0.2868	-0.4924	0.0008	-0.0017
04T- 43	449	10	1.192	0.0	14.233	1.3591	0.3827	-0.6065	0.0009	-0.0019
04T- 43	449	11	1.199	0.0	16.468	1.5159	0.4843	-0.7048	0.0012	-0.0021
04T- 43	449	12	1.196	0.0	18.757	1.6679	0.6015	-0.8025	0.0013	-0.0018
04T- 43	449	13	1.196	0.0	20.926	1.7863	0.7176	-0.8861	0.0005	-0.0015
04T- 43	449	15	1.198	-0.0	0.023	0.0422	0.0629	-0.0390	0.0009	-0.0024
04T- 43	452	1	0.902	0.0	1.115	0.2541	0.0386	-0.0679	-0.0009	-0.0030
04T- 43	452	2	0.902	0.0	4.423	0.5501	0.0704	-0.0937	-0.0017	-0.0024
04T- 43	452	3	0.901	0.0	6.476	0.7285	0.1056	-0.1242	-0.0015	-0.0017
04T- 43	452	4	0.904	0.0	8.759	0.9214	0.1602	-0.1689	0.0012	-0.0008
04T- 43	452	5	0.900	0.0	9.659	0.9717	0.1844	-0.1877	0.0024	-0.0006
04T- 43	452	6	0.901	-0.0	11.914	1.1467	0.2550	-0.2411	0.0021	0.0010
04T- 43	452	7	0.900	0.0	16.240	1.3631	0.4192	-0.3914	0.0043	-0.0013
04T- 43	453	1	0.899	0.0	-2.180	-0.0633	0.0405	-0.0511	0.0011	-0.0042
04T- 43	453	2	0.898	0.0	0.300	0.1751	0.0358	-0.0628	-0.0016	-0.0034
04T- 43	453	3	0.904	0.0	2.654	0.3942	0.0502	-0.0784	-0.0008	-0.0026
04T- 43	453	4	0.896	0.0	5.033	0.6040	0.0783	-0.1015	-0.0020	-0.0022
04T- 43	453	5	0.893	0.0	7.321	0.7953	0.1216	-0.1331	-0.0007	-0.0013

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	453	6	0.892	0.0	9.680	0.9775	0.1810	-0.1821	0.0026	-0.0004
04T- 43	453	7	0.898	-0.0	11.908	1.1516	0.2560	-0.2380	0.0036	0.0003
04T- 43	453	8	0.902	0.0	14.070	1.2388	0.3299	-0.3093	0.0056	-0.0009
04T- 43	453	9	0.900	0.0	16.221	1.3646	0.4180	-0.3870	0.0051	-0.0019
04T- 43	453	10	0.900	0.0	18.341	1.4847	0.5171	-0.4780	0.0036	0.0005
04T- 43	454	1	0.699	0.0	-2.160	-0.0616	0.0332	-0.0322	0.0002	-0.0036
04T- 43	454	2	0.699	0.0	0.203	0.1407	0.0293	-0.0499	0.0003	-0.0025
04T- 43	454	3	0.698	0.0	2.427	0.3249	0.0350	-0.0666	0.0007	-0.0017
04T- 43	454	4	0.698	0.0	4.792	0.5231	0.0535	-0.0945	0.0008	-0.0013
04T- 43	454	5	0.696	0.0	7.022	0.7041	0.0830	-0.1273	0.0016	-0.0004
04T- 43	454	6	0.697	-0.0	9.232	0.8797	0.1327	-0.1602	0.0057	0.0016
04T- 43	454	7	0.700	-0.0	11.424	0.9926	0.1930	-0.1892	0.0067	0.0014
04T- 43	454	8	0.699	-0.0	13.620	1.1296	0.2705	-0.2359	0.0069	0.0007
04T- 43	454	9	0.701	-0.0	15.786	1.2534	0.3532	-0.2929	0.0079	-0.0007
04T- 43	454	10	0.698	0.0	17.868	1.3697	0.4433	-0.3733	0.0064	-0.0013
04T- 43	455	1	0.800	0.0	-2.141	-0.0620	0.0357	-0.0337	0.0005	-0.0036
04T- 43	455	2	0.801	0.0	0.200	0.1444	0.0304	-0.0547	0.0002	-0.0026
04T- 43	455	3	0.800	0.0	2.530	0.3499	0.0384	-0.0703	0.0009	-0.0016
04T- 43	455	4	0.797	0.0	4.908	0.5572	0.0603	-0.0961	0.0006	-0.0014
04T- 43	455	5	0.792	0.0	7.216	0.7445	0.0956	-0.1252	0.0008	-0.0005
04T- 43	455	6	0.797	-0.0	9.446	0.9232	0.1508	-0.1555	0.0064	0.0009
04T- 43	455	7	0.795	-0.0	11.615	1.0263	0.2106	-0.1902	0.0042	0.0013
04T- 43	455	8	0.800	-0.0	13.783	1.1591	0.2911	-0.2548	0.0053	0.0004
04T- 43	455	9	0.795	-0.0	15.947	1.2653	0.3697	-0.3183	0.0060	-0.0004
04T- 43	455	10	0.797	0.0	18.176	1.4202	0.4764	-0.4072	0.0056	-0.0012
04T- 43	456	1	1.197	0.0	-2.267	-0.1579	0.0638	0.0506	-0.0011	-0.0045
04T- 43	456	2	1.196	0.0	-2.265	-0.1574	0.0643	0.0499	-0.0010	-0.0046
04T- 43	456	3	1.193	0.0	0.138	0.0666	0.0582	-0.0375	-0.0025	-0.0043
04T- 43	456	4	1.198	0.0	2.399	0.2871	0.0697	-0.1285	-0.0033	-0.0036
04T- 43	456	5	1.193	0.0	4.914	0.5445	0.1007	-0.2338	-0.0029	-0.0025
04T- 43	456	6	1.197	0.0	7.274	0.7660	0.1483	-0.3179	-0.0022	-0.0018
04T- 43	456	7	1.200	0.0	9.635	0.9805	0.2140	-0.4022	-0.0019	-0.0009
04T- 43	456	8	1.197	0.0	12.041	1.1834	0.2965	-0.4933	-0.0010	-0.0002
04T- 43	456	9	1.198	0.0	14.341	1.3694	0.3927	-0.6006	-0.0	0.0001
04T- 43	456	10	1.199	0.0	16.4[illegible]	1.5176	0.4884	-0.6932	0.0011	-0.0001
04T- 43	456	11	1.197	0.0	18.627	1.6624	0.6021	-0.7898	0.0023	0.0001
04T- 43	456	12	1.198	0.0	20.980	1.7300	0.7242	-0.8744	0.0050	-0.0006
04T- 43	459	1	0.903	0.0	0.865	0.1207	0.0530	-0.0609	0.0247	0.0056
04T- 43	459	2	0.896	0.0	4.170	0.4199	0.0736	-0.0904	0.0260	0.0032
04T- 43	459	3	0.904	0.0	6.277	0.6458	0.1063	-0.1208	0.0180	0.0005
04T- 43	459	4	0.905	0.0	8.660	0.8750	0.1612	-0.1640	0.0135	-0.0020
04T- 43	459	5	0.900	0.0	9.611	0.9530	0.1871	-0.1795	0.0109	-0.0021
04T- 43	459	6	0.903	0.0	11.881	1.1271	0.2621	-0.2353	0.0119	-0.0030
04T- 43	460	1	0.903	0.0	-2.442	-0.2142	0.0624	-0.0359	0.0259	0.0076
04T- 43	460	2	0.906	0.0	0.007	0.0376	0.0524	-0.0553	0.0246	0.0059

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	460	3	0.904	0.0	2.422	0.2599	0.0601	-0.0741	0.0251	0.0044
04T- 43	460	4	0.898	0.0	4.812	0.4832	0.0815	-0.0962	0.0250	0.0023
04T- 43	460	5	0.904	0.0	7.371	0.7552	0.1291	-0.1401	0.0153	-0.0006
04T- 43	460	6	0.895	0.0	9.571	0.9451	0.1841	-0.1756	0.0104	-0.0019
04T- 43	460	7	0.895	0.0	11.854	1.0931	0.2529	-0.2319	0.0034	-0.0012
04T- 43	460	8	0.895	0.0	13.942	1.2209	0.3279	-0.2990	0.0016	-0.0010
04T- 43	460	9	0.889	0.0	16.069	1.3371	0.4134	-0.3837	0.0038	-0.0016
04T- 43	460	10	0.903	0.0	18.334	1.4878	0.5260	-0.4788	0.0061	-0.0033
04T- 43	461	1	0.700	0.0	-2.317	-0.1830	0.0524	-0.0253	0.0248	0.0070
04T- 43	461	2	0.700	0.0	-0.054	0.0109	0.0441	-0.0436	0.0248	0.0057
04T- 43	461	3	0.699	0.0	2.271	0.2031	0.0487	-0.0672	0.0247	0.0044
04T- 43	461	4	0.699	0.0	4.484	0.3872	0.0626	-0.0936	0.0255	0.0033
04T- 43	461	5	0.699	0.0	6.778	0.5869	0.0880	-0.1279	0.0244	0.0013
04T- 43	461	6	0.700	0.0	9.125	0.3037	0.1390	-0.1581	0.0129	-0.0
04T- 43	461	7	0.701	0.0	11.366	0.9627	0.2026	-0.1874	0.0066	-0.0007
04T- 43	461	8	0.699	0.0	13.563	1.0981	0.2738	-0.2290	0.0054	-0.0011
04T- 43	461	9	0.702	0.0	15.740	1.2296	0.3547	-0.2853	0.0034	-0.0011
04T- 43	461	10	0.699	0.0	17.854	1.3599	0.4463	-0.3621	0.0024	-0.0009
04T- 43	462	1	0.798	0.0	-2.337	-0.1929	0.0557	-0.0289	0.0262	0.0076
04T- 43	462	2	0.798	0.0	-0.013	0.0147	0.0467	-0.0462	0.0257	0.0062
04T- 43	462	3	0.800	0.0	2.342	0.2204	0.0523	-0.0684	0.0256	0.0048
04T- 43	462	4	0.799	0.0	4.608	0.4183	0.0677	-0.0945	0.0267	0.0036
04T- 43	462	5	0.799	0.0	6.976	0.6344	0.0991	-0.1290	0.0255	0.0011
04T- 43	462	6	0.797	0.0	9.268	0.8485	0.1520	-0.1592	0.0114	-0.0001
04T- 43	462	7	0.800	0.0	11.597	1.0169	0.2237	-0.2042	0.0022	0.0001
04T- 43	462	8	0.799	0.0	13.751	1.1372	0.2940	-0.2506	0.0052	-0.0012
04T- 43	462	9	0.800	0.0	15.893	1.2651	0.3763	-0.3138	0.0027	-0.0008
04T- 43	462	10	0.797	0.0	18.130	1.4099	0.4782	-0.3982	0.0031	-0.0014
04T- 43	463	1	1.197	0.0	-2.382	-0.2194	0.0804	0.0652	0.0156	0.0037
04T- 43	463	2	1.196	0.0	0.038	0.0166	0.0706	-0.0191	0.0129	0.0016
04T- 43	463	3	1.197	0.0	2.515	0.2658	0.0803	-0.1156	0.0103	0.0001
04T- 43	463	4	1.197	0.0	4.789	0.5013	0.1073	-0.2093	0.0085	-0.0011
04T- 43	463	5	1.196	0.0	7.239	0.7436	0.1555	-0.3004	0.0075	-0.0022
04T- 43	463	6	1.195	0.0	9.621	0.9568	0.2196	-0.3844	0.0069	-0.0029
04T- 43	463	7	1.196	0.0	11.957	1.1514	0.2989	-0.4735	0.0063	-0.0041
04T- 43	463	8	1.194	0.0	14.164	1.3312	0.3898	-0.5749	0.0070	-0.0056
04T- 43	463	9	1.195	0.0	16.463	1.4959	0.4951	-0.6717	0.0082	-0.0070
04T- 43	463	10	1.196	0.0	18.700	1.6380	0.6084	-0.7659	0.0079	-0.0072
04T- 43	463	12	1.198	0.0	0.016	0.0132	0.0701	-0.0154	0.0128	0.0015
04T- 43	466	1	0.901	0.0	1.257	0.3457	0.0481	-0.0754	0.0149	-0.0026
04T- 43	466	2	0.898	0.0	4.644	0.6544	0.0877	-0.1038	0.0154	-0.0032
04T- 43	466	3	0.902	0.0	6.614	0.8195	0.1274	-0.1292	0.0140	-0.0038
04T- 43	466	4	0.901	0.0	8.870	0.9999	0.1975	-0.1635	0.0128	-0.0043
04T- 43	466	5	0.899	0.0	9.806	1.0700	0.2154	-0.1853	0.0130	-0.0046
04T- 43	466	6	0.900	0.0	11.951	1.1762	0.2820	-0.2360	0.0033	-0.0022

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	467	1	0.900	0.0	-2.006	0.0260	0.0398	-0.0526	0.0130	-0.0017
04T- 43	467	2	0.899	0.0	0.440	0.2693	0.0432	-0.0690	0.0142	-0.0024
04T- 43	467	3	0.899	0.0	2.842	0.4953	0.0635	-0.0886	0.0153	-0.0029
04T- 43	467	4	0.900	0.0	5.213	0.7063	0.0990	-0.1121	0.0152	-0.0034
04T- 43	467	5	0.900	0.0	7.507	0.8943	0.1490	-0.1386	0.0128	-0.0038
04T- 43	467	6	0.899	0.0	9.786	1.0659	0.2142	-0.1828	0.0130	-0.0047
04T- 43	467	7	0.897	0.0	11.983	1.1794	0.2833	-0.2354	0.0036	-0.0022
04T- 43	468	1	0.700	0.0	-1.954	0.0451	0.0325	-0.0342	0.0161	-0.0005
04T- 43	468	2	0.699	0.0	0.335	0.2421	0.0350	-0.0545	0.0168	-0.0014
04T- 43	468	3	0.698	0.0	2.587	0.4272	0.0472	-0.0766	0.0171	-0.0021
04T- 43	468	4	0.699	0.0	4.894	0.6215	0.0703	-0.1041	0.0170	-0.0031
04T- 43	468	5	0.699	0.0	7.146	0.8135	0.1087	-0.1313	0.0170	-0.0044
04T- 43	468	6	0.700	0.0	9.321	0.9392	0.1654	-0.1567	0.0120	-0.0047
04T- 43	468	7	0.700	0.0	11.529	1.0475	0.2293	-0.1921	0.0110	-0.0046
04T- 43	468	8	0.700	0.0	13.716	1.1749	0.3041	-0.2323	0.0114	-0.0051
04T- 43	468	9	0.701	0.0	15.802	1.2833	0.3810	-0.2909	0.0099	-0.0044
04T- 43	468	10	0.699	0.0	17.977	1.4063	0.4761	-0.3755	0.0091	-0.0046
04T- 43	469	1	0.798	0.0	-1.989	0.0385	0.0350	-0.0398	0.0151	-0.0008
04T- 43	469	2	0.798	0.0	0.361	0.2530	0.0371	-0.0605	0.0164	-0.0015
04T- 43	469	3	0.799	0.0	2.750	0.4627	0.0525	-0.0842	0.0173	-0.0023
04T- 43	469	4	0.798	0.0	5.059	0.6716	0.0794	-0.1092	0.0171	-0.0032
04T- 43	469	5	0.798	0.0	7.390	0.8774	0.1266	-0.1343	0.0181	-0.0043
04T- 43	469	6	0.795	0.0	9.592	0.9829	0.1821	-0.1585	0.0133	-0.0045
04T- 43	469	7	0.800	0.0	11.689	1.0838	0.2468	-0.2021	0.0082	-0.0037
04T- 43	470	1	1.196	0.0	-2.145	-0.0754	0.0654	0.0115	0.0097	-0.0007
04T- 43	470	2	1.196	0.0	0.242	0.1576	0.0658	-0.0759	0.0117	-0.0010
04T- 43	470	3	1.193	-0.0	2.632	0.4020	0.0853	-0.1727	0.0137	-0.0015
04T- 43	470	4	1.195	0.0	5.066	0.6478	0.1237	-0.2663	0.0129	-0.0024
04T- 43	470	5	1.192	0.0	7.454	0.8685	0.1783	-0.3338	0.0109	-0.0031
04T- 43	470	6	1.193	0.0	9.819	1.0664	0.2473	-0.4194	0.0100	-0.0041
04T- 43	470	7	1.192	0.0	12.090	1.2534	0.3305	-0.5147	0.0100	-0.0053
04T- 43	470	8	1.199	0.0	14.364	1.4185	0.4259	-0.6087	0.0090	-0.0058
04T- 43	470	9	1.195	0.0	16.599	1.5734	0.5331	-0.7047	0.0087	-0.0060
04T- 43	470	10	1.196	0.0	18.864	1.7081	0.6496	-0.8014	0.0079	-0.0070
04T- 43	473	1	0.900	0.0	1.104	0.2607	0.0404	-0.0715	0.0165	-0.0019
04T- 43	473	2	0.902	0.0	4.462	0.5749	0.0755	-0.1013	0.0146	-0.0021
04T- 43	473	3	0.903	0.0	6.456	0.7435	0.1126	-0.1234	0.0161	-0.0030
04T- 43	473	4	0.902	0.0	8.763	0.9185	0.1673	-0.1528	0.0184	-0.0041
04T- 43	473	5	0.903	0.0	9.703	0.9834	0.1940	-0.1725	0.0188	-0.0043
04T- 43	473	6	0.901	0.0	11.839	1.0792	0.2585	-0.2219	0.0095	-0.0022
04T- 43	474	1	0.902	0.0	-2.206	-0.0820	0.0394	-0.0421	0.0177	0.0007
04T- 43	474	2	0.903	0.0	0.280	0.1786	0.0372	-0.0640	0.0165	-0.0007
04T- 43	474	3	0.902	0.0	2.673	0.4122	0.0546	-0.0875	0.0161	-0.0017
04T- 43	474	4	0.902	0.0	5.054	0.6282	0.0858	-0.1078	0.0148	-0.0025
04T- 43	474	5	0.898	0.0	7.371	0.8263	0.1328	-0.1343	0.0173	-0.0035

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_l	C_n
04T- 43	474	6	0.901	0.0	9.707	0.9830	0.1936	-0.1740	0.0194	-0.0046
04T- 43	474	7	0.899	0.0	11.815	1.0876	0.2561	-0.2207	0.0145	-0.0038
04T- 43	474	8	0.898	0.0	13.940	1.2086	0.3322	-0.2975	0.0124	-0.0036
04T- 43	474	9	0.902	0.0	16.243	1.3428	0.4270	-0.3877	0.0123	-0.0032
04T- 43	475	1	0.701	0.0	-2.102	-0.0458	0.0317	-0.0293	0.0214	0.0016
04T- 43	475	2	0.701	0.0	0.248	0.1582	0.0301	-0.0524	0.0213	0.0003
04T- 43	475	3	0.699	0.0	2.449	0.3387	0.0396	-0.0751	0.0214	-0.0009
04T- 43	475	4	0.700	0.0	4.735	0.5300	0.0581	-0.1019	0.0212	-0.0022
04T- 43	475	5	0.698	0.0	7.048	0.7232	0.0913	-0.1306	0.0203	-0.0037
04T- 43	475	6	0.700	0.0	9.210	0.8561	0.1440	-0.1542	0.0157	-0.0041
04T- 43	475	7	0.699	0.0	11.434	0.9907	0.2085	-0.1884	0.0163	-0.0044
04T- 43	475	8	0.699	0.0	13.562	1.1138	0.2797	-0.2290	0.0136	-0.0047
04T- 43	475	9	0.701	0.0	15.716	1.2347	0.3594	-0.2846	0.0127	-0.0048
04T- 43	475	10	0.698	0.0	17.871	1.3597	0.4504	-0.3650	0.0106	-0.0040
04T- 43	476	1	0.800	0.0	-2.151	-0.0596	0.0342	-0.0329	0.0197	0.0016
04T- 43	476	2	0.802	0.0	0.232	0.1533	0.0318	-0.0560	0.0202	0.0004
04T- 43	476	3	0.799	0.0	2.542	0.3638	0.0425	-0.0789	0.0205	-0.0008
04T- 43	476	4	0.799	0.0	4.928	0.5773	0.0654	-0.1056	0.0210	-0.0022
04T- 43	476	5	0.797	0.0	7.253	0.7806	0.1062	-0.1238	0.0207	-0.0033
04T- 43	476	6	0.799	0.0	9.451	0.9013	0.1591	-0.1483	0.0167	-0.0038
04T- 43	476	7	0.799	0.0	11.608	1.0281	0.2269	-0.2010	0.0112	-0.0034
04T- 43	476	8	0.799	0.0	13.808	1.1458	0.3013	-0.2517	0.0143	-0.0041
04T- 43	476	9	0.801	0.0	15.909	1.2642	0.3816	-0.3137	0.0121	-0.0037
04T- 43	477	1	1.196	0.0	-2.208	-0.1318	0.0624	0.0458	0.0081	0.0001
04T- 43	477	2	1.195	0.0	0.204	0.0977	0.0595	-0.0402	0.0095	-0.0006
04T- 43	477	3	1.195	0.0	2.510	0.3267	0.0736	-0.1303	0.0107	-0.0009
04T- 43	477	4	1.194	0.0	4.969	0.5721	0.1082	-0.2256	0.0112	-0.0016
04T- 43	477	5	1.195	0.0	7.352	0.7955	0.1593	-0.3074	0.0111	-0.0023
04T- 43	477	6	1.194	0.0	9.657	0.9719	0.2234	-0.3852	0.0115	-0.0030
04T- 43	477	7	1.194	0.0	11.991	1.1817	0.3044	-0.4740	0.0117	-0.0045
04T- 43	477	8	1.195	0.0	14.296	1.3581	0.3993	-0.5748	0.0119	-0.0054
04T- 43	477	9	1.198	0.0	16.514	1.5077	0.5004	-0.6649	0.0130	-0.0060
04T- 43	477	10	1.199	0.0	18.708	1.6440	0.6113	-0.7628	0.0130	-0.0069
04T- 43	480	1	0.699	0.0	-2.098	-0.0473	0.0311	-0.0326	0.0211	0.0022
04T- 43	480	2	0.700	0.0	0.171	0.1492	0.0290	-0.0537	0.0210	0.0008
04T- 43	480	3	0.702	0.0	2.435	0.3371	0.0382	-0.0775	0.0211	-0.0005
04T- 43	480	4	0.699	0.0	4.726	0.5265	0.0566	-0.1027	0.0209	-0.0019
04T- 43	480	5	0.700	0.0	7.008	0.7226	0.0900	-0.1323	0.0207	-0.0035
04T- 43	480	6	0.701	0.0	9.226	0.8692	0.1437	-0.1559	0.0168	-0.0038
04T- 43	480	7	0.699	0.0	11.456	0.9978	0.2085	-0.1901	0.0160	-0.0041
04T- 43	480	8	0.699	0.0	13.593	1.1163	0.2796	-0.2278	0.0143	-0.0046
04T- 43	480	9	0.698	0.0	15.723	1.2393	0.3604	-0.2826	0.0133	-0.0048
04T- 43	480	10	0.698	0.0	17.887	1.3710	0.4541	-0.3547	0.0114	-0.0046
04T- 43	481	1	0.800	0.0	-2.142	-0.0582	0.0335	-0.0357	0.0194	0.0019
04T- 43	481	2	0.800	0.0	0.212	0.1468	0.0311	-0.0564	0.0202	0.0007

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	481	3	0.800	0.0	2.554	0.3642	0.0421	-0.0821	0.0206	-0.0005
04T- 43	481	4	0.799	0.0	4.875	0.5716	0.0637	-0.1075	0.0209	-0.0020
04T- 43	481	5	0.799	0.0	7.204	0.7745	0.1042	-0.1333	0.0211	-0.0021
04T- 43	481	6	0.800	0.0	9.396	0.8978	0.1562	-0.1512	0.0170	-0.0036
04T- 43	481	7	0.798	0.0	11.653	1.0322	0.2250	-0.1966	0.0122	-0.0033
04T- 43	481	8	0.799	0.0	13.803	1.1487	0.2987	-0.2426	0.0147	-0.0040
04T- 43	481	9	0.800	0.0	15.948	1.2752	0.3825	-0.3070	0.0121	-0.0034
04T- 43	482	1	0.901	0.0	-2.205	-0.0839	0.0389	-0.0458	0.0176	0.0011
04T- 43	482	2	0.901	0.0	0.265	0.1732	0.0360	-0.0676	0.0164	-0.0002
04T- 43	482	3	0.900	0.0	2.669	0.4013	0.0514	-0.0926	0.0160	-0.0013
04T- 43	482	4	0.901	0.0	5.085	0.6290	0.0840	-0.1207	0.0153	-0.0024
04T- 43	482	5	0.897	0.0	7.358	0.8130	0.1276	-0.1410	0.0183	-0.0035
04T- 43	482	6	0.902	0.0	9.651	0.9848	0.1894	-0.1752	0.0181	-0.0043
04T- 43	482	7	0.898	0.0	11.830	1.0902	0.2528	-0.2223	0.0152	-0.0037
04T- 43	482	8	0.898	0.0	14.010	1.2157	0.3317	-0.2922	0.0138	-0.0036
04T- 43	483	1	1.198	0.0	-2.258	-0.1414	0.0619	0.0403	0.0087	0.0006
04T- 43	483	2	1.198	0.0	0.132	0.0942	0.0573	-0.0489	0.0097	-0.0001
04T- 43	483	3	1.195	0.0	2.515	0.3350	0.0716	-0.1435	0.0109	-0.0005
04T- 43	483	4	1.192	0.0	4.982	0.5848	0.1071	-0.2382	0.0115	-0.0012
04T- 43	483	5	1.191	0.0	7.334	0.8047	0.1578	-0.3139	0.0115	-0.0020
04T- 43	483	6	1.189	0.0	9.678	1.0062	0.2237	-0.3909	0.0118	-0.0028
04T- 43	483	7	1.193	0.0	11.994	1.1904	0.3049	-0.4780	0.0124	-0.0040
04T- 43	483	8	1.191	0.0	14.274	1.3691	0.3993	-0.5770	0.0128	-0.0052
04T- 43	483	9	1.188	0.0	16.533	1.5164	0.5019	-0.6565	0.0142	-0.0056
04T- 43	483	10	1.186	0.0	18.759	1.6578	0.6156	-0.7600	0.0141	-0.0071
04T- 43	486	1	0.700	0.0	-2.147	-0.0408	0.0305	-0.0426	0.0114	-0.0017
04T- 43	486	2	0.700	0.0	-2.901	-0.1055	0.0345	-0.0367	0.0114	-0.0017
04T- 43	486	3	0.701	0.0	-2.899	-0.1047	0.0343	-0.0374	0.0115	-0.0017
04T- 43	486	4	0.702	0.0	-2.087	-0.0346	0.0302	-0.0435	0.0115	-0.0017
04T- 43	486	5	0.702	0.0	0.228	0.1623	0.0285	-0.0616	0.0112	-0.0018
04T- 43	486	6	0.699	0.0	2.481	0.3479	0.0384	-0.0820	0.0115	-0.0018
04T- 43	486	7	0.698	0.0	4.721	0.5259	0.0566	-0.1034	0.0113	-0.0019
04T- 43	486	8	0.698	0.0	6.924	0.7151	0.0892	-0.1312	0.0119	-0.0020
04T- 43	486	9	0.700	-0.0	9.197	0.8693	0.1435	-0.1579	0.0117	-0.0024
04T- 43	486	10	0.698	-0.0	11.452	0.9941	0.2092	-0.1856	0.0112	-0.0027
04T- 43	486	11	0.699	-0.0	13.570	1.1078	0.2809	-0.2229	0.0109	-0.0031
04T- 43	486	12	0.701	-0.0	15.655	1.2194	0.3556	-0.2691	0.0101	-0.0036
04T- 43	486	13	0.700	0.0	17.851	1.3316	0.4423	-0.3353	0.0096	-0.0047
04T- 43	487	1	0.798	0.0	-2.120	-0.0376	0.0323	-0.0485	0.0118	-0.0014
04T- 43	487	2	0.803	0.0	-2.119	-0.0371	0.0328	-0.0486	0.0118	-0.0014
04T- 43	487	3	0.797	0.0	-2.117	-0.0367	0.0324	-0.0436	0.0118	-0.0014
04T- 43	487	4	0.797	0.0	0.253	0.1746	0.0302	-0.0655	0.0116	-0.0015
04T- 43	487	5	0.801	0.0	2.631	0.3795	0.0423	-0.0861	0.0113	-0.0015
04T- 43	487	6	0.799	0.0	4.942	0.5828	0.0654	-0.1069	0.0122	-0.0017
04T- 43	487	7	0.799	-0.0	7.266	0.7808	0.1084	-0.1323	0.0132	-0.0017
04T- 43	487	8	0.801	-0.0	9.434	0.9190	0.1636	-0.1601	0.0125	-0.0019

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	487	9	0.797	-0.0	11.542	1.0206	0.2257	-0.1984	0.0109	-0.0024
04T- 43	487	10	0.798	-0.0	13.706	1.1426	0.3003	-0.2521	0.0103	-0.0030
04T- 43	487	11	0.800	-0.0	15.908	1.2691	0.3851	-0.3136	0.0095	-0.0038
04T- 43	487	12	0.799	0.0	18.051	1.4011	0.4800	-0.3833	0.0092	-0.0051
04T- 43	488	1	0.900	0.0	-2.155	-0.0477	0.0369	-0.0607	0.0114	-0.0011
04T- 43	488	2	0.902	0.0	-2.155	-0.0488	0.0371	-0.0614	0.0114	-0.0011
04T- 43	488	3	0.901	0.0	0.204	0.1871	0.0343	-0.0748	0.0113	-0.0015
04T- 43	488	4	0.897	0.0	2.616	0.4108	0.0497	-0.0910	0.0110	-0.0019
04T- 43	488	5	0.892	0.0	4.979	0.6152	0.0806	-0.1081	0.0117	-0.0020
04T- 43	488	6	0.895	0.0	7.366	0.8071	0.1295	-0.1381	0.0129	-0.0024
04T- 43	488	7	0.898	0.0	9.648	1.0076	0.1965	-0.1842	0.0159	-0.0029
04T- 43	488	8	0.899	-0.0	11.949	1.1478	0.2693	-0.2358	0.0107	-0.0023
04T- 43	488	9	0.896	0.0	13.974	1.2134	0.3343	-0.2997	0.0104	-0.0039
04T- 43	488	10	0.893	0.0	16.080	1.3373	0.4200	-0.3792	0.0097	-0.0050
04T- 43	488	11	0.904	0.0	18.444	1.4907	0.5354	-0.4742	0.0108	-0.0072
04T- 43	489	1	1.194	-0.0	-1.054	-0.0268	0.0565	0.0056	0.0124	0.0001
04T- 43	489	2	1.197	-0.0	-2.198	-0.1261	0.0604	0.0414	0.0125	0.0012
04T- 43	489	3	1.197	-0.0	-2.199	-0.1271	0.0605	0.0419	0.0125	0.0012
04T- 43	489	4	1.198	-0.0	0.253	0.0943	0.0569	-0.0397	0.0124	-0.0009
04T- 43	489	5	1.195	-0.0	2.473	0.2952	0.0691	-0.1200	0.0119	-0.0019
04T- 43	489	6	1.195	-0.0	4.840	0.5408	0.1017	-0.2204	0.0118	-0.0024
04T- 43	489	7	1.194	0.0	7.196	0.7607	0.1505	-0.3029	0.0119	-0.0037
04T- 43	489	8	1.202	0.0	9.555	0.9712	0.2160	-0.3866	0.0115	-0.0053
04T- 43	489	9	1.200	0.0	11.913	1.1654	0.2981	-0.4711	0.0110	-0.0074
04T- 43	489	10	1.198	0.0	14.156	1.3434	0.3911	-0.5659	0.0097	-0.0096
04T- 43	489	11	1.195	0.0	16.475	1.5047	0.4981	-0.6607	0.0086	-0.0115
04T- 43	489	12	1.195	0.0	18.667	1.6406	0.6080	-0.7514	0.0075	-0.0120
04T- 43	492	1	0.703	0.0	-2.175	-0.0812	0.0431	-0.0395	0.0480	0.0071
04T- 43	492	2	0.703	0.0	0.123	0.1250	0.0399	-0.0620	0.0483	0.0044
04T- 43	492	3	0.702	0.0	2.401	0.3138	0.0488	-0.0861	0.0485	0.0017
04T- 43	492	4	0.702	0.0	4.703	0.5056	0.0664	-0.1113	0.0481	-0.0009
04T- 43	492	5	0.698	0.0	6.898	0.6918	0.0965	-0.1312	0.0461	-0.0042
04T- 43	492	6	0.698	0.0	9.225	0.8585	0.1538	-0.1521	0.0396	-0.0066
04T- 43	492	7	0.698	0.0	11.389	0.9862	0.2168	-0.1866	0.0325	-0.0090
04T- 43	492	8	0.705	0.0	13.545	1.0964	0.2870	-0.2162	0.0328	-0.0111
04T- 43	492	9	0.703	0.0	15.671	1.2176	0.3647	-0.2661	0.0296	-0.0123
04T- 43	492	10	0.701	0.0	17.850	1.3399	0.4551	-0.3370	0.0258	-0.0127
04T- 43	493	1	0.800	0.0	-2.268	-0.0946	0.0459	-0.0418	0.0461	0.0074
04T- 43	493	2	0.799	0.0	0.100	0.1360	0.0427	-0.0654	0.0468	0.0047
04T- 43	493	3	0.800	0.0	2.437	0.3412	0.0525	-0.0895	0.0472	0.0021
04T- 43	493	4	0.795	0.0	4.803	0.5501	0.0741	-0.1143	0.0476	-0.0009
04T- 43	493	5	0.797	0.0	7.164	0.7653	0.1154	-0.1345	0.0452	-0.0038
04T- 43	493	6	0.800	0.0	9.335	0.9076	0.1701	-0.1537	0.0358	-0.0058
04T- 43	493	7	0.797	0.0	11.572	1.0144	0.2344	-0.1859	0.0335	-0.0084
04T- 43	493	8	0.799	0.0	13.733	1.1274	0.3073	-0.2369	0.0328	-0.0104
04T- 43	493	9	0.797	0.0	15.902	1.2476	0.3898	-0.2932	0.0293	-0.0114

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	493	10	0.791	0.0	18.073	1.3809	0.4845	-0.3622	0.0264	-0.0124
04T- 43	494	1	0.904	0.0	-2.261	-0.1068	0.0516	-0.0486	0.0442	0.0073
04T- 43	494	2	0.898	0.0	-2.253	-0.1026	0.0505	-0.0494	0.0443	0.0073
04T- 43	494	3	0.903	0.0	-2.253	-0.1047	0.0515	-0.0492	0.0443	0.0073
04T- 43	494	4	0.905	0.0	0.225	0.1621	0.0489	-0.0714	0.0440	0.0042
04T- 43	494	5	0.900	0.0	2.660	0.4022	0.0636	-0.0948	0.0435	0.0013
04T- 43	494	6	0.901	0.0	5.064	0.6392	0.0964	-0.1182	0.0385	-0.0014
04T- 43	494	7	0.900	0.0	7.406	0.8362	0.1430	-0.1326	0.0347	-0.0036
04T- 43	494	8	0.901	0.0	9.754	1.0058	0.2091	-0.1637	0.0377	-0.0062
04T- 43	494	9	0.899	0.0	11.799	1.0811	0.2673	-0.2119	0.0302	-0.0073
04T- 43	495	1	1.198	-0.0	-2.259	-0.1335	0.0749	0.0444	0.0285	0.0071
04T- 43	495	2	1.199	-0.0	0.246	0.1067	0.0710	-0.0439	0.0308	0.0039
04T- 43	495	3	1.196	0.0	2.614	0.3405	0.0876	-0.1338	0.0231	0.0011
04T- 43	495	4	1.197	0.0	4.937	0.5663	0.1201	-0.2195	0.0327	-0.0018
04T- 43	495	5	1.195	0.0	7.279	0.7790	0.1687	-0.2908	0.0307	-0.0047
04T- 43	495	6	1.192	0.0	9.630	0.9755	0.2326	-0.3633	0.0294	-0.0084
04T- 43	495	7	1.191	0.0	11.974	1.1653	0.3142	-0.4541	0.0291	-0.0127
04T- 43	495	8	1.201	0.0	14.195	1.3202	0.3998	-0.5372	0.0273	-0.0161
04T- 43	495	9	1.200	0.0	16.452	1.4745	0.5027	-0.6277	0.0254	-0.0193
04T- 43	495	10	1.196	0.0	18.653	1.6063	0.6105	-0.7126	0.0237	-0.0221
04T- 43	498	1	0.024	-0.2	-1.001	-0.8442	0.0531	0.0198	-0.0068	0.0017
04T- 43	498	2	0.024	-0.1	4.079	-1.0134	-0.0439	0.0793	-0.0045	0.0082
04T- 43	498	3	0.024	-0.1	9.011	-1.0301	-0.0129	0.1089	0.0100	0.0142
04T- 43	498	4	0.024	-0.2	13.993	-0.8356	-0.1528	0.1069	0.0170	0.0209
04T- 43	498	5	0.024	-0.3	18.975	-1.0687	-0.3348	0.0828	0.0323	0.0219
04T- 43	498	6	0.024	-0.3	24.009	-0.7566	-0.2760	0.0141	0.0297	0.0285
04T- 43	498	7	0.024	-0.3	19.076	-0.9082	-0.2710	0.0758	0.0327	0.0221
04T- 43	498	8	0.024	-0.2	14.009	2.7694	0.8304	0.0176	0.0161	0.0239
04T- 43	498	9	0.022	-0.2	9.014	0.9247	0.2589	0.0746	0.0071	-0.0057
04T- 43	498	10	0.024	-0.0	3.992	0.4485	0.1782	0.2164	0.0037	0.0067
04T- 43	498	11	0.024	-0.0	-0.989	0.4164	0.0753	-0.0105	0.0097	0.0008
04T- 43	499	1	0.687	0.0	-2.046	-0.0535	0.0349	-0.0478	0.0473	0.0054
04T- 43	499	2	0.698	0.0	-2.050	-0.0540	0.0376	-0.0484	0.0475	0.0055
04T- 43	499	3	0.700	0.0	-2.047	-0.0534	0.0387	-0.0488	0.0474	0.0055
04T- 43	499	4	0.699	0.0	-2.045	-0.0523	0.0380	-0.0492	0.0475	0.0055
04T- 43	499	5	0.699	0.0	0.180	0.1311	0.0362	-0.0455	0.0474	0.0029
04T- 43	499	6	0.700	0.0	2.219	0.2815	0.0430	-0.0392	0.0474	0.0009
04T- 43	499	7	0.699	0.0	4.387	0.4313	0.0562	-0.0313	0.0471	-0.0013
04T- 43	499	8	0.696	0.0	6.537	0.5956	0.0801	-0.0245	0.0457	-0.0043
04T- 43	499	9	0.696	0.0	8.726	0.7540	0.1268	-0.0191	0.0399	-0.0064
04T- 43	499	10	0.695	0.0	10.773	0.8425	0.1765	0.0009	0.0321	-0.0075
04T- 43	499	11	0.697	0.0	12.884	0.9437	0.2331	0.0146	0.0303	-0.0093
04T- 43	499	12	0.695	0.0	14.998	1.0254	0.2915	0.0358	0.0269	-0.0097
04T- 43	499	13	0.699	0.0	17.036	1.0757	0.3488	0.0530	0.0218	-0.0069
04T- 43	499	14	0.697	0.0	19.112	1.1332	0.4163	0.0547	0.0219	-0.0084
04T- 43	499	15	0.699	0.0	21.266	1.2001	0.4942	0.0473	0.0216	-0.0086

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	499	16	0.699	0.0	23.224	1.2632	0.5701	0.0433	0.0204	-0.0079
04T- 43	500	1	0.798	0.0	-2.094	-0.0589	0.0407	-0.0510	0.0455	0.0053
04T- 43	500	2	0.794	0.0	-2.098	-0.0588	0.0380	-0.0510	0.0456	0.0054
04T- 43	500	3	0.799	0.0	0.137	0.1449	0.0396	-0.0533	0.0459	0.0028
04T- 43	500	4	0.797	0.0	2.288	0.3177	0.0462	-0.0481	0.0464	0.0006
04T- 43	500	5	0.796	0.0	4.486	0.4946	0.0634	-0.0418	0.0468	-0.0018
04T- 43	500	6	0.801	0.0	6.630	0.6740	0.0952	-0.0366	0.0439	-0.0045
04T- 43	500	7	0.796	0.0	8.827	0.9108	0.1421	-0.0291	0.0341	-0.0065
04T- 43	500	8	0.794	0.0	10.854	0.8870	0.1919	-0.0155	0.0287	-0.0072
04T- 43	500	9	0.797	0.0	12.952	0.9740	0.2505	-0.0004	0.0271	-0.0080
04T- 43	500	10	0.795	0.0	15.045	1.0380	0.3075	0.0210	0.0255	-0.0075
04T- 43	500	11	0.800	0.0	17.194	1.1152	0.3751	0.0364	0.0221	-0.0056
04T- 43	500	12	0.796	0.0	19.304	1.1708	0.4418	0.0383	0.0205	-0.0029
04T- 43	500	13	0.787	0.0	21.336	1.2216	0.5140	0.0241	0.0216	-0.0067
04T- 43	500	14	0.800	0.0	23.398	1.2860	0.5973	0.0136	0.0214	-0.0083
04T- 43	501	1	0.899	0.0	-0.942	0.0585	0.0421	-0.0642	0.0433	0.0034
04T- 43	501	2	0.901	0.0	-2.113	-0.0679	0.0454	-0.0594	0.0434	0.0049
04T- 43	501	3	0.904	0.0	0.113	0.1569	0.0452	-0.0635	0.0439	0.0022
04T- 43	501	4	0.900	0.0	2.296	0.3519	0.0558	-0.0675	0.0442	-0.0003
04T- 43	501	5	0.892	0.0	4.586	0.5828	0.0815	-0.0801	0.0405	-0.0027
04T- 43	501	6	0.892	0.0	6.744	0.7694	0.1221	-0.0940	0.0358	-0.0048
04T- 43	501	7	0.896	0.0	8.854	0.9107	0.1741	-0.0891	0.0373	-0.0066
04T- 43	501	8	0.902	0.0	10.947	0.9688	0.2243	-0.0584	0.0248	-0.0064
04T- 43	501	9	0.903	0.0	13.093	1.0435	0.2809	-0.0447	0.0222	-0.0064
04T- 43	501	10	0.899	0.0	15.181	1.0968	0.3391	-0.0296	0.0200	-0.0048
04T- 43	501	11	0.907	0.0	17.379	1.1980	0.4221	-0.0384	0.0180	-0.0032
04T- 43	501	12	0.896	-0.0	19.406	1.2415	0.4829	-0.0237	0.0167	0.0002
04T- 43	501	13	0.903	0.0	21.507	1.2920	0.5589	-0.0290	0.0171	-0.0011
04T- 43	501	14	0.893	0.0	23.556	1.3422	0.6351	-0.0300	0.0172	-0.0028
04T- 43	502	1	1.199	0.0	-2.110	-0.0756	0.0653	-0.0352	0.0240	0.0021
04T- 43	502	2	1.197	0.0	0.057	0.1115	0.0640	-0.0657	0.0270	0.0008
04T- 43	502	3	1.196	0.0	2.306	0.3121	0.0776	-0.0997	0.0296	-0.0012
04T- 43	502	4	1.199	0.0	4.548	0.5066	0.1041	-0.1279	0.0295	-0.0031
04T- 43	502	5	1.195	0.0	6.715	0.6836	0.1428	-0.1441	0.0279	-0.0049
04T- 43	502	6	1.198	0.0	8.923	0.8414	0.1924	-0.1557	0.0264	-0.0070
04T- 43	502	7	1.193	0.0	11.102	0.9903	0.2532	-0.1667	0.0245	-0.0094
04T- 43	502	8	1.196	0.0	13.248	1.1139	0.3196	-0.1736	0.0229	-0.0104
04T- 43	502	9	1.196	0.0	15.455	1.2265	0.3970	-0.1753	0.0217	-0.0122
04T- 43	502	10	1.196	0.0	17.524	1.3172	0.4750	-0.1785	0.0216	-0.0143
04T- 43	502	11	1.194	0.0	19.707	1.4060	0.5636	-0.1930	0.0208	-0.0143
04T- 43	502	12	1.193	0.0	21.829	1.4723	0.6523	-0.2023	0.0199	-0.0169
04T- 43	502	13	1.194	0.0	23.901	1.5294	0.7412	-0.2077	0.0177	-0.0180
04T- 43	505	1	0.903	0.0	1.031	0.2264	0.0552	-0.0792	0.0327	-0.0002
04T- 43	505	2	0.903	0.0	6.441	0.7274	0.1179	-0.1460	0.0218	-0.0041
04T- 43	505	3	0.903	0.0	8.718	0.9161	0.1699	-0.1817	0.0224	-0.0058
04T- 43	505	4	0.900	0.0	9.581	0.9645	0.1910	-0.1943	0.0235	-0.0061

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	505	5	0.904	0.0	11.769	1.0919	0.2548	-0.2491	0.0201	-0.0059
04T- 43	505	6	0.899	0.0	16.205	1.3540	0.4281	-0.3980	0.0150	-0.0056
04T- 43	506	1	0.901	0.0	-2.275	-0.1447	0.0587	-0.0315	0.0303	0.0035
04T- 43	506	2	0.905	0.0	0.193	0.1289	0.0519	-0.0659	0.0312	0.0010
04T- 43	506	3	0.899	0.0	2.600	0.3815	0.0643	-0.1005	0.0305	-0.0013
04T- 43	506	4	0.903	0.0	4.930	0.5979	0.0924	-0.1241	0.0242	-0.0031
04T- 43	506	5	0.902	0.0	7.290	0.7957	0.1331	-0.1522	0.0216	-0.0043
04T- 43	506	6	0.903	0.0	9.568	0.9647	0.1915	-0.1913	0.0236	-0.0061
04T- 43	506	7	0.903	0.0	11.761	1.0893	0.2542	-0.2442	0.0208	-0.0058
04T- 43	506	8	0.904	0.0	13.935	1.2188	0.3331	-0.3025	0.0153	-0.0054
04T- 43	506	9	0.901	0.0	16.154	1.3458	0.4247	-0.3934	0.0151	-0.0052
04T- 43	507	1	0.701	0.0	-2.218	-0.1164	0.0490	-0.0291	0.0342	0.0044
04T- 43	507	2	0.700	0.0	0.108	0.0999	0.0417	-0.0579	0.0363	0.0024
04T- 43	507	3	0.700	0.0	2.343	0.2951	0.0470	-0.0843	0.0382	-0.0001
04T- 43	507	4	0.702	0.0	4.654	0.4893	0.0645	-0.1147	0.0376	-0.0025
04T- 43	507	5	0.701	0.0	6.925	0.6812	0.0928	-0.1429	0.0353	-0.0051
04T- 43	507	6	0.702	0.0	9.179	0.8563	0.1386	-0.1718	0.0327	-0.0077
04T- 43	507	7	0.701	0.0	11.322	0.9949	0.2021	-0.2080	0.0246	-0.0086
04T- 43	507	8	0.699	0.0	13.512	1.1177	0.2757	-0.2501	0.0183	-0.0087
04T- 43	507	9	0.703	0.0	15.689	1.2432	0.3575	-0.2978	0.0203	-0.0094
04T- 43	507	10	0.699	0.0	17.809	1.3592	0.4473	-0.3715	0.0177	-0.0094
04T- 43	508	1	0.800	0.0	-2.234	-0.1231	0.0520	-0.0304	0.0318	0.0041
04T- 43	508	2	0.802	0.0	0.153	0.1100	0.0450	-0.0609	0.0366	0.0023
04T- 43	508	3	0.800	0.0	2.410	0.3257	0.0519	-0.0907	0.0373	-0.0002
04T- 43	508	4	0.798	0.0	4.829	0.5434	0.0740	-0.1218	0.0365	-0.0027
04T- 43	508	5	0.798	0.0	7.148	0.7512	0.1091	-0.1487	0.0332	-0.0050
04T- 43	508	6	0.800	0.0	9.376	0.9172	0.1604	-0.1733	0.0275	-0.0068
04T- 43	508	7	0.799	0.0	11.576	1.0291	0.2226	-0.2158	0.0215	-0.0073
04T- 43	508	8	0.798	0.0	13.749	1.1484	0.3000	-0.2628	0.0211	-0.0082
04T- 43	508	9	0.801	0.0	15.908	1.2640	0.3822	-0.3317	0.0197	-0.0079
04T- 43	508	10	0.798	0.0	18.089	1.3964	0.4785	-0.4087	0.0188	-0.0088
04T- 43	509	1	1.193	0.0	4.949	0.5361	0.1162	-0.2261	0.0212	-0.0020
04T- 43	509	2	1.194	0.0	-2.281	-0.1493	0.0807	0.0411	0.0166	0.0024
04T- 43	509	3	1.194	0.0	0.067	0.0611	0.0752	-0.0381	0.0179	0.0008
04T- 43	509	4	1.195	0.0	2.448	0.2874	0.0863	-0.1316	0.0211	-0.0005
04T- 43	509	5	1.193	0.0	4.890	0.5301	0.1153	-0.2252	0.0212	-0.0018
04T- 43	509	6	1.193	0.0	7.217	0.7472	0.1592	-0.2995	0.0195	-0.0037
04T- 43	509	7	1.192	0.0	9.533	0.9483	0.2184	-0.3743	0.0184	-0.0057
04T- 43	509	8	1.191	0.0	11.907	1.1452	0.2971	-0.4677	0.0186	-0.0078
04T- 43	509	9	1.198	0.0	14.149	1.3101	0.3835	-0.5569	0.0177	-0.0093
04T- 43	509	10	1.199	0.0	16.390	1.4674	0.4835	-0.6513	0.0168	-0.0103
04T- 43	509	11	1.198	0.0	18.630	1.6113	0.5946	-0.7459	0.0153	-0.0103
04T- 43	509	12	1.201	0.0	0.096	0.0583	0.0753	-0.0351	0.0177	0.0006
04T- 43	512	1	0.901	0.0	0.958	0.1665	0.0587	-0.0472	0.0364	-0.0010
04T- 43	512	2	0.902	0.0	4.381	0.5313	0.0902	-0.1125	0.0320	-0.0055

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	512	3	0.901	0.0	6.383	0.7197	0.1238	-0.1401	0.0256	-0.0065
04T- 43	512	4	0.902	0.0	8.687	0.8928	0.1745	-0.1778	0.0255	-0.0071
04T- 43	512	5	0.906	0.0	9.584	0.9660	0.2009	-0.2032	0.0261	-0.0075
04T- 43	512	6	0.905	0.0	11.837	1.1249	0.2687	-0.2554	0.0289	-0.0078
04T- 43	513	1	0.904	0.0	-2.379	-0.1877	0.0635	-0.0098	0.0359	0.0019
04T- 43	513	2	0.907	0.0	0.156	0.0891	0.0571	-0.0371	0.0347	-0.0001
04T- 43	513	3	0.903	0.0	2.574	0.3496	0.0709	-0.0769	0.0365	-0.0029
04T- 43	513	4	0.905	0.0	4.982	0.6003	0.0998	-0.1212	0.0284	-0.0056
04T- 43	513	5	0.901	0.0	7.328	0.7370	0.1424	-0.1489	0.0238	-0.0064
04T- 43	513	6	0.903	0.0	9.591	0.9673	0.1992	-0.1964	0.0253	-0.0066
04T- 43	513	7	0.906	0.0	11.847	1.1330	0.2707	-0.2544	0.0291	-0.0075
04T- 43	513	8	0.905	0.0	14.020	1.2580	0.3460	-0.3127	0.0316	-0.0095
04T- 43	513	9	0.904	0.0	16.148	1.3556	0.4273	-0.3856	0.0268	-0.0099
04T- 43	513	10	0.902	0.0	18.348	1.4767	0.5263	-0.4651	0.0242	-0.0089
04T- 43	514	1	0.702	0.0	-2.248	-0.1470	0.0512	-0.0123	0.0407	0.0026
04T- 43	514	2	0.701	0.0	0.045	0.0755	0.0364	-0.0439	0.0435	0.0010
04T- 43	514	3	0.701	0.0	2.423	0.2995	0.0516	-0.0825	0.0481	-0.0013
04T- 43	514	4	0.701	0.0	4.703	0.4940	0.0690	-0.1133	0.0485	-0.0039
04T- 43	514	5	0.701	0.0	6.937	0.6838	0.0971	-0.1436	0.0455	-0.0061
04T- 43	514	6	0.701	0.0	9.108	0.8627	0.1449	-0.1758	0.0437	-0.0059
04T- 43	514	7	0.703	0.0	11.432	1.0195	0.2088	-0.2120	0.0451	-0.0073
04T- 43	514	8	0.701	0.0	13.552	1.1311	0.2779	-0.2502	0.0401	-0.0096
04T- 43	514	9	0.699	0.0	15.721	1.2537	0.3624	-0.3050	0.0380	-0.0128
04T- 43	514	10	0.699	0.0	17.844	1.3616	0.4513	-0.3753	0.0335	-0.0144
04T- 43	515	1	0.800	0.0	-2.270	-0.1550	0.0541	-0.0146	0.0382	0.0027
04T- 43	515	2	0.803	0.0	0.095	0.0905	0.0475	-0.0478	0.0401	0.0007
04T- 43	515	3	0.805	0.0	2.502	0.3332	0.0575	-0.0876	0.0460	-0.0016
04T- 43	515	4	0.801	0.0	2.494	0.3310	0.0572	-0.0874	0.0460	-0.0015
04T- 43	515	5	0.799	0.0	4.777	0.5402	0.0785	-0.1191	0.0460	-0.0044
04T- 43	515	6	0.801	0.0	7.151	0.7397	0.1162	-0.1436	0.0376	-0.0063
04T- 43	515	7	0.801	0.0	9.402	0.9208	0.1683	-0.1794	0.0362	-0.0061
04T- 43	515	8	0.796	0.0	11.652	1.0690	0.2333	-0.2230	0.0414	-0.0078
04T- 43	515	9	0.800	0.0	13.766	1.1684	0.3030	-0.2641	0.0371	-0.0095
04T- 43	518	1	0.899	0.0	-2.376	-0.1857	0.0636	-0.0200	0.0364	0.0022
04T- 43	518	2	0.902	0.0	0.059	0.0783	0.0560	-0.0421	0.0348	0.0001
04T- 43	518	3	0.900	0.0	2.595	0.3476	0.0694	-0.0795	0.0374	-0.0027
04T- 43	518	4	0.900	0.0	4.938	0.5906	0.0958	-0.1196	0.0287	-0.0052
04T- 43	518	5	0.896	0.0	7.233	0.7839	0.1362	-0.1479	0.0230	-0.0061
04T- 43	518	6	0.902	0.0	9.568	0.9499	0.1919	-0.1934	0.0246	-0.0062
04T- 43	518	7	0.900	0.0	11.836	1.1183	0.2607	-0.2480	0.0296	-0.0079
04T- 43	518	8	0.902	0.0	13.952	1.2356	0.3298	-0.3084	0.0313	-0.0096
04T- 43	519	1	0.697	0.0	-2.265	-0.1543	0.0529	-0.0199	0.0409	0.0029
04T- 43	519	2	0.702	0.0	0.073	0.0696	0.0447	-0.0464	0.0430	0.0009
04T- 43	519	3	0.702	0.0	2.318	0.2923	0.0507	-0.0807	0.0475	-0.0011
04T- 43	519	4	0.701	0.0	4.599	0.4779	0.0670	-0.1107	0.0484	-0.0036

TEST	RUN	PT	MACH	SWEEP (DEG)	ALPHA (DEG)	C_L	C_D	C_m	C_ℓ	C_n
04T- 43	519	5	0.699	0.0	6.892	0.6748	0.0938	-0.1410	0.0454	-0.0058
04T- 43	519	6	0.700	0.0	9.173	0.8571	0.1407	-0.1713	0.0434	-0.0057
04T- 43	519	7	0.701	0.0	11.373	1.0079	0.1977	-0.2046	0.0468	-0.0068
04T- 43	519	8	0.701	0.0	13.467	1.0951	0.2612	-0.2593	0.0393	-0.0096
04T- 43	519	9	0.699	0.0	15.563	1.2003	0.3369	-0.3262	0.0377	-0.0137
04T- 43	519	10	0.698	0.0	17.671	1.2999	0.4204	-0.4064	0.0337	-0.0159
04T- 43	520	1	0.802	0.0	-2.274	-0.1580	0.0560	-0.0218	0.0385	0.0027
04T- 43	520	2	0.796	0.0	0.090	0.0832	0.0468	-0.0490	0.0396	0.0007
04T- 43	520	3	0.798	0.0	2.421	0.3163	0.0558	-0.0849	0.0452	-0.0015
04T- 43	520	4	0.798	0.0	4.735	0.5236	0.0761	-0.1128	0.0444	-0.0043
04T- 43	520	5	0.800	0.0	7.115	0.7290	0.1119	-0.1382	0.0364	-0.0058
04T- 43	520	6	0.800	0.0	9.374	0.8975	0.1594	-0.1660	0.0324	-0.0058
04T- 43	520	7	0.799	0.0	11.546	1.0419	0.2211	-0.2141	0.0402	-0.0070
04T- 43	520	8	0.799	0.0	13.661	1.1378	0.2860	-0.2717	0.0377	-0.0094
04T- 43	520	9	0.800	0.0	15.787	1.2362	0.3634	-0.3523	0.0350	-0.0132
04T- 43	520	10	0.799	0.0	17.950	1.3455	0.4522	-0.4282	0.0306	-0.0137

THIS JOB IS COMPLETE.

Unclassified
Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) General Dynamics Fort Worth Division	2a. REPORT SECURITY CLASSIFICATION Unclassified 2b. GROUP N/A

3. REPORT TITLE

Wing Roll Control Devices for Transonic High Lift Conditions

4. DESCRIPTIVE NOTES (Type of report and inclusive dates)

Interim Technical Report (Work accomplished from 1 Jan 1969 to 1 Dec 1969

5. AUTHOR(S) (First name, middle initial, last name)

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6. REPORT DATE	7a. TOTAL NO. OF PAGES	7b. NO. OF REFS
July 1970	541 440	28

8a. CONTRACT OR GRANT NO. F33615-69-C-1225 b. PROJECT NO. 8219 c. Task No. 821902 d.	9a. ORIGINATOR'S REPORT NUMBER(S) 9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) AFFDL-TR-69-124 Pt.I, Vol. II

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11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY
None	AFFDL (FDCC) Wright-Patterson AFB, Ohio 45433

13. ABSTRACT

The Wing Mounted Roll Control Study (Contract F33615-69-C-1225) was an investigation of various methods for improving control effectiveness at high-lift transonic conditions. Emphasis was placed upon the use of leading edge devices as primary controls and also as auxiliary devices with conventional controls. Selected configurations were tested in AEDC 4T facility and limited validation was obtained in the AEDC 16T facility. Control configurations investigated included leading edge flaps and ailerons both singly and in combination, as well as spoilers, differential horizontal tail and several auxiliary devices. Use of differential leading edge deflection significantly improved aileron effectiveness at high angle of attack transonic conditions. Because of the important effects that the wing-body configuration has upon wing mounted control devices, considerable data and analysis is presented for the longitudinal characteristics. Testing of the same model in two different size facilities provided significant information on wall interference effects at transonic conditions.

DD FORM 1 NOV 65 1473

Unclassified
Security Classification

Unclassified
Security Classification

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Aerodynamic Controls						
High Lift						
Transonic						
Leading Edge Devices						
Roll Control						
Maneuvering						

Unclassified
Security Classification